

WIRELESS WORLD

ELECTRONICS &

June 1984 85p.

Multi-standard modem

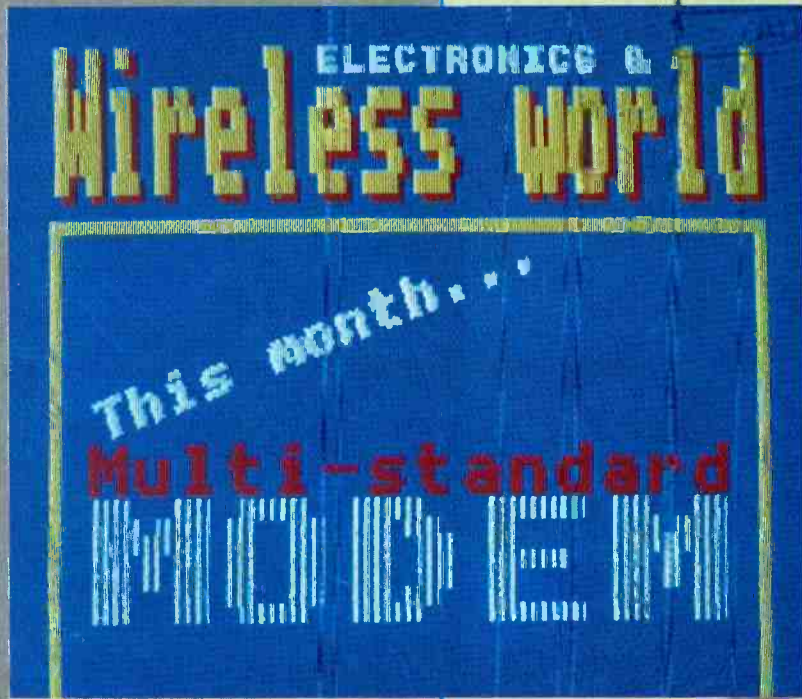
Emulators

Computer cassette recorder

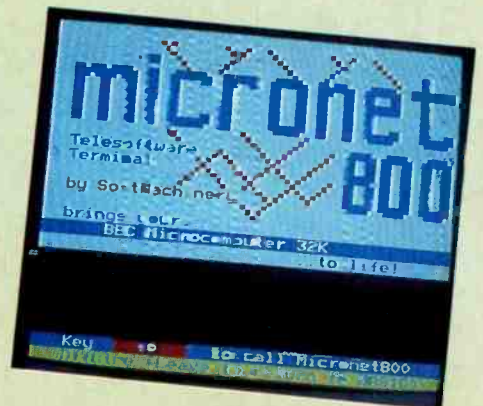
Cellular radio



DEFENCE SCIENTIFIC ESTABLISHMENT
3 SEP 1984



CKLAND



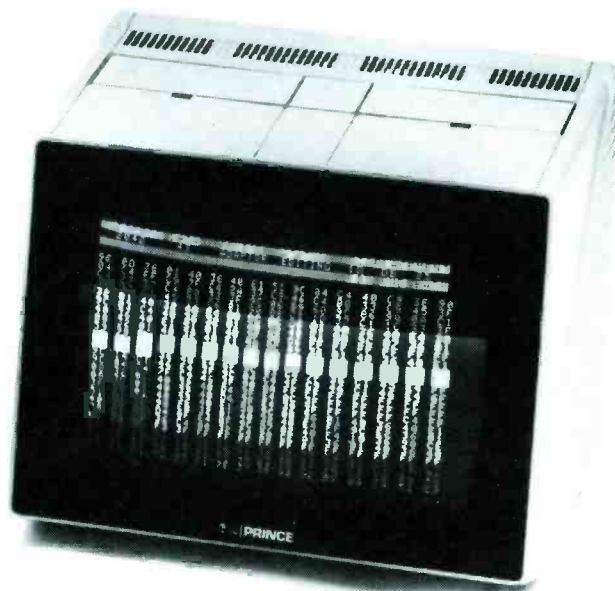
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EP8000 EPROM EMULATOR PROGRAMMER

**NEW
PRODUCT**



The new microprocessor controlled EP8000 Emulator Programmer will program and emulate all EPROMs up to 8k x 8 sizes, and can be extended to program other devices such as 16k x 8 EPROMs, Bipolar PROMs, single chip microprocessors with external modules.

Personality cards and hardware changes are not required as the machine configures itself for the different devices.

The EP4000 with 4k x 8 static RAM is still available with EPROM programming and emulation capacity up to 4k x 8 sizes.

- EP8000 8k x 8 Emulator Programmer – £695 + £12 delivery
- BSC8 Buffered emulation cable – £49
- SA27128 Programming adaptor – £69
- SA25128 Programming adaptor – £69
- EP4000 4k x 8 Emulator Programmer – £545 + £12 de-

FEATURES

- Software personality programming/emulation of all EPROMs up to 8k x 8 bytes including 2704, 2708, 2716(3), 2508, 2758A, 2758B, 2516, 2716, 2532, 2732, 2732A, 68732-0, 68732-1, 68766, 68764, 2564, 2764. Programs 25128, 27128 with adaptors.
- No personality cards/characterisers required.
- Use as stand alone programmer, slave programmer, or EPROM development system.
- Checks for misplaced and reversed insertion, and shorts on data lines.
- Memory mapped video output allows full use of powerful editing facilities.
- Built-in LED display for field use.
- Powerful editing facilities include: Block/Byte move, insert, delete, match, highlight, etc.
- Comprehensive input/output – RS232C serial port, parallel port, cassette, printer O/P, DMA.
- Extra 1k x 8 scratchpad RAM for block moving.

- livery ● BSC4 Buffered emulation cable – £39
- BP4 (TEXAS) Bipolar PROM Module – £190
- Prinz video monitor – £99
- UV141 EPROM Eraser with timer – £78
- GP100A 80 column printer – £225
- GR1 Centronics interface – £65

VAT should be added to all prices

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Tel: Plymouth (0752) 332961
Telex: 42513

Unit E, Huxley Close, Newnham Industrial Estate, Plymouth PL7 4JN

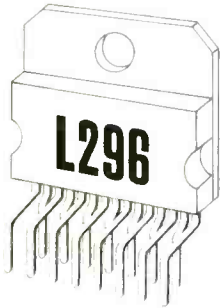
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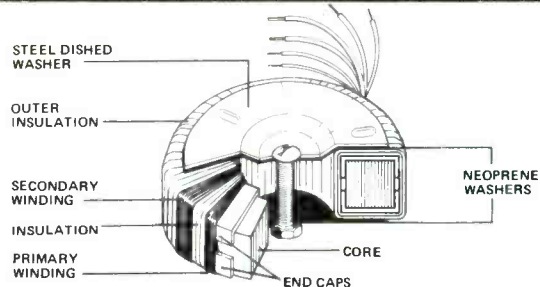
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CIRCLE 38 FOR FURTHER DETAILS.

ELECTRONICS & Wirelessworld

over 70 years in independent electronics publishing

June 1984

Volume 90 number 1581

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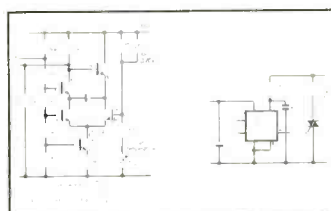
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CASSETTE RECORDER

by A. J. Ewins

Micro-controlled cassette recorder

Solenoid-operated cassette mechanism allows control of functions by push-button or microcomputer. Software to be described enables recorder to SAVE or LOAD automatically.

As a storage medium for microcomputer programs, the cassette recorder is probably still the most widely used device, as a large number of the latest pieces of software are written for it. Microcomputers are a familiar sight in schools, offices and homes, and the cassette recorder is still very popular. The storage capacity of a cassette tape is impressive, a C60 high fidelity tape can store up to 7500 bytes of data when recorded at a rate of 2400 baud — 1.5MBps. If two channels recording is possible, however, cassette recorders can not be used in an automatic SAVE and LOAD mode unless all the

Control elements

The micro-controlled cassette

EMULATORS

In-circuit emulation

John Ferguson discusses the principle of emulators and illustrates their use by reference to several commercial units.

by John D. Ferguson*

The technique of in-circuit emulation is a powerful one, and it is used in a wide range of applications, from the design of new hardware to the debugging of existing hardware. It is a technique which allows the user to observe the internal operation of a device, and to control it in real time. This is done by replacing the original device with an emulator, which mimics its behaviour. The emulator is connected to the device, and the user can observe the internal signals and control the device through the emulator. This is done by replacing the original device with an emulator, which mimics its behaviour. The emulator is connected to the device, and the user can observe the internal signals and control the device through the emulator.

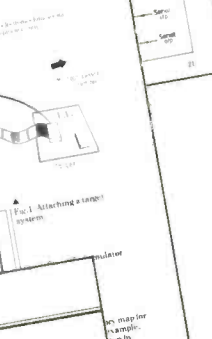


Fig. 1. Block diagram of cassette recorder for data storage. Cassette deck is SP225F from Hans Electronics.

SPEECH RECOGNITION

By Tom Ivall

Automatic speech recognition

Speaking communication between man and machine is needed for many applications — in military use, where hands are otherwise occupied, where the communicator is disabled or where it is simply more convenient. Tom Ivall reports on two recent meetings.

Man's ability to speak is one of his most valuable assets. It is a skill which has enabled him to communicate with others and to pass on his knowledge and experience. This ability is also what makes him a unique individual. However, this ability is not always used to its full potential. In many situations, the hands of the communicator are occupied, or the communicator is disabled. This is where automatic speech recognition (ASR) can be of great help. ASR allows the user to communicate with a machine using only their voice. This is done by replacing the original device with an emulator, which mimics its behaviour. The emulator is connected to the device, and the user can observe the internal signals and control the device through the emulator.

Front cover illustrates some communications software and pages from Prestel, one of the databases which can be accessed through our modem design.

NEXT MONTH

Graphics display and up to 32 lines of 96 characters are provided by the v.d.u. circuit of John Adam's microcomputer.

Two-metre transceivers for the radio amateur: as May's RAE candidates await their pass slips, a survey of equipment for this popular band for the beginner.

Timebase correction for C-format vtrs is explained in the second installment of John Watkinson's four-part series on variable speed video.

Multi-standard modem: details of the interface to the telephone line, plus suggestions for software and some databases to dial up.

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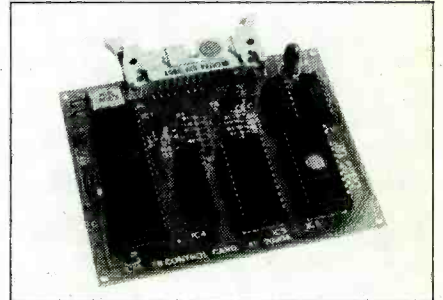
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C	1.2V	2.2AH	01-12024	2.35	1.99
D	1.2V	4.0AH	01-12044	3.05	2.85
PP3	8.4V	110mAH	01-84054	3.70	3.50
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CH8/RX Multi-purpose Charger			01-02204		9.40

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Battery Adaptor 01-12001 0.96
Sold in pairs: one to convert AA size to C size and one to convert C to D size. Both may be used together to convert an AA to D size.

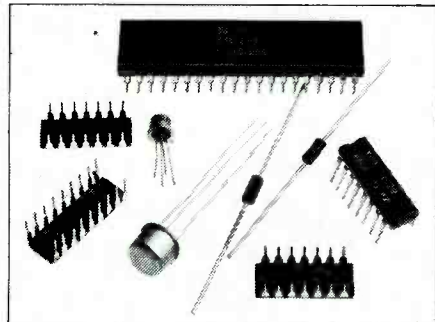
Semiconductors

Linear IC's

LM301AN	DIL version	61-03011	0.44
LM308CN	DIL version	61-03081	0.65
LM311CN	Popular comparator	61-00311	0.46
LM324	Low power quad op amp	61-03240	0.67
LM339N	Low power quad comparator	61-03390	0.68
LM346	Programmable quad op amp	61-00346	3.72
LF347	Quad Bi-FET op amp	61-00347	1.82
LM348	Quad 741 type op amp	61-03480	1.26
LF351	Bi-FET op amp	61-03510	0.49
LF353	Dual version of LF351	61-03530	0.76
LM380N	IW AF power amp	61-00380	1.00
NE555N	Multi-purpose low cost timer	61-05550	0.45

for a better service.

NE556N	Dual version of the 555	61-05560	0.50
uA741CN	DIL low cost op amp	61-07411	0.22
uA747CN	Dual 741 op amp	61-07470	0.70
uA748CN	741 with external frequency comp	61-04780	0.40
HA1388	18W PA from 14V	61-01388	2.75
TDA2002	8W into 2 ohms power amp	61-02002	1.25
ULN2283	1W max. 3-12V power amp	61-02283	1.00
MC3357	Low power NBFM IF system and detector	61-03357	2.85
ULN3859	Low current dual conversion NBFM IF and detector	61-03859	2.95
LM3900	Quad norton amp	61-39000	0.60
LM3909N	8-pin DIL LED flasher	61-39090	0.68
KB4445	Radio control 4 channel encoder and RF	61-04445	1.29
KB4446	Radio control 4 channel receiver and decoder	61-04446	2.75
ICM7555	Low power CMOS version of timer	61-75550	0.98
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TK10170	5 channel version of KB4445	61-10170	1.87
HA12002	Protection monitor system for amps, PSUx, TXs etc	61-12002	1.22
HA12017	83dB S/N phono preamp 0.001% THD	61-12017	0.80
MC14412	300 baud MODEM controller (Eduro/US specs)	61-14412	6.85



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6116-3	16K (2kx8) CMOS RAM 200nS	26-36116	6.68
Z6132-6	32K (4kx8) quas. RAM 350nS	26-06132	15.00
4116-2	16K (16kx1) 150nS	26-24116	1.59
2764	64K (8kx8) 450nS	26-02764	9.50
2732	32K (4kx8) 450nS	26-02732	5.70

Voltage Regulators

7805	5V 1A positive	27-78052	0.40
7812	12V 1A positive	27-78122	0.40
7815	15V 1A positive	27-78152	0.40
7905	5V 1A negative	27-79052	0.49
7912	12V 1A negative	27-79122	0.49
7915	15V 1A negative	27-79152	0.49

Transistors

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BC212	General purpose	58-00212	0.10
BC237	Plastic BC107	58-00237	0.08
BC238	Plastic BC108	58-00238	0.08
BC239	Plastic BC109	58-00239	0.08
BC307	Complement to BC237	58-00307	0.08
BC308	Complement to BC238	58-00308	0.08

BC309	Complement to BC239	58-00309	0.08
BC327	Driver/power stage	58-00327	0.13
BC337	Driver/power stage	58-00337	0.13
MPSA13	NPN Darlington	58-04013	0.30
MPSA63	PNP Complement to MPSA13	58-04063	0.30
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3SK51	Dual gate MOSFET-VHF amp	60-04051	0.60
3SK88	Dual gate MOSFET-Ultra lo noise	60-04088	0.99
TIP31A	Output stage	58-15031	0.35
TIP32A	Complement to TIP31A	58-15032	0.35
VN66AF	VMOS Power FET	60-02066	0.95
ZTX3866	E-line version 2N3866	58-03866	0.45
IN4001	Rectifier diode	12-40016	0.06
IN4002	Rectifier diode	12-40026	0.07
IN4148	General purpose silicon	12-41486	0.05

Silicon Controlled Rectifiers

BRY55-100	100V .8A	52-55100	0.50
C106DI	400V 4.0A	52-00106	0.70
C122DI	400V 8.0A	52-00122	1.45

3mm Diameter LEDs

V178P	Red	15-01780	0.15
V179P	Green	15-01790	0.16
V180P	Yellow	15-01800	0.18

5mm Diameter LEDs

CQY40L	Red	15-10400	0.12
CQY72L	Green	15-10720	0.15
CQY74L	Yellow	15-10740	0.15

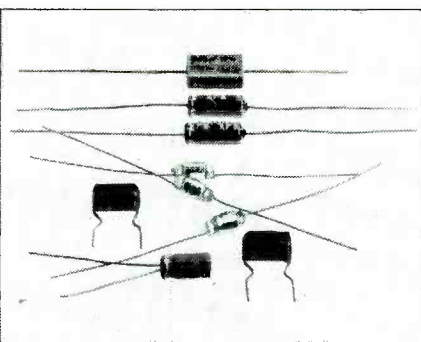
Infra-Red LEDs

CQY99	Emitter	15-10990	0.56
BPW41	Detector	15-30410	1.51

Tri Colour LED

V518	Orange-Green-Yellow	15-05180	0.60
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Capacitors



Aluminium Electrolytics Radial PCB Mounting

10u	16V	05-10606	0.24
47u	16V	05-47606	0.28
47u	25V	05-47607	0.28
470u	6.3V	05-47705	0.36
470u	16V	05-47706	0.48

Tantalum Beads

1uF	35V	05-10501	0.18
10uF	16V	05-10601	0.28
47uF	6.3V	05-47601	0.45
47uF	16V	05-47602	0.92

Monolithic Capacitors

1n	04-10204	0.39
10n	04-10304	0.42
100n	04-10404	0.45

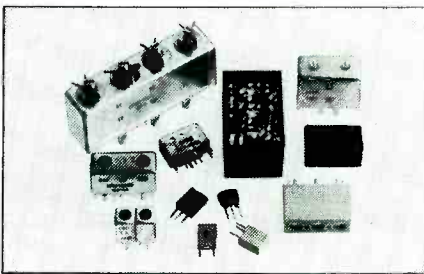
Low Voltage Disc Ceramic

1n	04-10203	0.20
10n	04-10303	0.20

Polyester (C280)

10n	04-10305	0.18
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Basic leap-frog

There is evidence that universities running courses for electronic engineers are playing leap-frog.

Circuit design does not seem to be considered a vital part of the curriculum, perhaps because many of the circuit functions that used to be taught are now contained in integrated circuits. The effect of this, in recent times, is that new graduates are somewhat diffident in the basics of circuit design, though fully proficient in the development of i.cs.

"They all know how to shuffle little black bugs around on a board, but ask them to design a feedback amplifier and they want to go home" is how one manufacturer describes a recent influx of design staff.

Clearly, education and

training must move with the times, but such a policy of leap-frogging the basics of design to concentrate on using modules of other people's design does appear to be a little short-sighted. There is obviously a lower level of complexity below which one simply buys and fits — no one wants to make resistors and capacitors — but, since i.cs now constitute the largest part of most designs, it surely makes sense to know enough circuit design to understand how they work. Not to do so is not to be an electronic engineer at all. It has always been the case in the past that an engineer should be familiar with the design and construction of components such as inductors and

transformers, delay lines, power supplies and thermionic devices, even though they were usually bought 'off the peg' and fitted. Nothing has changed — but i.cs are commonly connected together to form a highly complicated piece of equipment, the 'designer' having only a hazy notion of what the individual components are doing. Time in a university course is limited, and our industry has evolved so rapidly that a great deal of new technology must now be taught, but even so, to gloss over the rudiments of any subject is a practice fraught with danger. We may still see a generation of highly skilled designers who are unable to design.

Telephone hang-up

The home computer magazines are calling 1984 the year of the modem. As an entertainment medium. The modem has a lot to recommend it — certainly when you compare it with the handful of games cassettes you might get for the same money. So it's a pity that the majority of modems available to the impecunious home user are (how can I put it?) illegal. Illegal to use, anyway.

The problem is that anything you connect to a telephone line has by law to be scrutinised by the British Approval Board for Telecommunications — Babtee to its intimats. But getting a device approved by BAPT is a slow business, and not a course to embark upon unless you have kilopounds to spare. All right for commercial manufacturers, perhaps, but how about the poor home constructor?

BAPT cannot vet a construction kit, still less a paper design. So anyone who wants to build our multi-standard modem may face the icy blast of official disapproval — along with all the other people using bootleg modems.

Most of these illicit modems are undoubtedly perfectly sanitary from a technical point of

view. And BT's chances of catching people using them can hardly be very great. BT, who are probably more concerned about the menace of improted cordless telephones, may even be happy to take the extra revenue.

Nobody stands to gain from doing damage to the telephone

network, least of all the modem users themselves. So who are they harming? In some countries the telephone authorities can provide simple isolators for connecting subscribers' equipment to their lines. Would it be such a sacrifice to allow that in Britain?

Alternative energy

Did you know that on the larger wind generators, it's predicted that a broken blade could fly through the air for up to 2km? Imagine the devastation should such an object hit an unsuspecting bus queue from the back.

We're about to set up a campaign against these lethal devices before it's too late; electronic safety measures are fine but they can't hold back a broken blade once it has set off at around Mach 0.9. Current propaganda has convinced us that nuclear power stations are the only option for alternative energy, especially the extra safe ones that we use in the UK. The only slight reservation we still

have is about the possible leakage of one of the massive chlorine tanks used for water purification, but we haven't found any figures on this subject yet, so our money is on nuclear energy.

After all, even when the dead weight of Britain's industry has been cleared — iron foundries, heavy engineering and the like — we'll still need a lot of electricity to power the computers used by the millions of retrained workers. And workers not prepared to retrain will have lots of spare time in which they'll be using their electric-powered microwave ovens and dish washers. That is, when they realise that fish and chips with v.a.t. are a little over the top.

£10million Alvey contracts

Two contracts worth £10million in the Alvey Programme of advanced information technology placed last month are the first major contracts in the five year £350million collaborative project. Alvey (*WW* page 31 December 1982) was given the go-ahead a year ago and under it the Government will fund 50% of industrial costs and 100% of university costs. The first for what is called an "integrated project support environment", is a multi-language advanced software tool that aims to support developers of real-time distributed computing systems at the centre of large complex systems such as industrial process control, avionics, and advanced communication systems. The £3.6million project, called Aspect, is a 'first-generation' IPSE led by Systems Designers who will use their IPSE 'Perspective' that supports production of Pascal programs for embedded applications, University of York who developed an Ada compiler, MARI with the 'Newcastle Connection' software for linking distributed Unix machines, as well as ICL with Perq expertise and GEC, with Series 63 computers. (A second generation

IPSE will support distributed software development, and a third generation will contain knowledge-based tools to give 'intelligent' support to software developers, otherwise called an 'information systems factory'.)

Announcing the contract Kenneth Baker, minister for information technology, said Aspect will play a vital role in increasing productivity throughout the software engineering community: "The Alvey Programme aims to turn writing software from a craft into an engineering discipline" he said.

A consortium led by ICL has been awarded the second contract, worth £6.5million over five years, for a large scale demonstrator project to evaluate the role of new computing technologies in the formulation, interpretation and application of complex policies and rules. A team of DHSS officials will work with the consortium of ICL, Logica, Imperial College, Universities of Lancaster and Surrey. The project will cover investigations of intelligent knowledge-based systems and man-machine interfaces, as well as software engineering techniques.



Pointing a satellite

Ways of improving the orientation of satellites in space are to be investigated by Marconi Space and Defence on behalf of the European Space Agency. The study is to concentrate on the problems presented by large, flexible solar power panels which are to be used on the very large telecommunications satellites. Large satellites with high output powers need to be manoeuvred with a high degree of accuracy to ensure that their communications antennae are correctly oriented with respect to Earth receivers; even a tenth of a degree error in the direction of a communications beam can mean a serious loss of data. In addition some satellites use very narrow beams, making the need for accuracy even more important. Greater precision has been achieved already in smaller craft where the solar energy panels are attached to the body of the craft. In the large craft however, the panels tend to flex under the impulses generated by correction thruster rockets. The flexing can introduce unwanted movement in the craft and further compensation is required, which in the extreme case can lead to a 'hunting' effect; wasteful in fuel and reducing the life of the satellite. The study is to take a mathematical approach to the problem. There is an algebraic theorem by Sturm, proposed in 1836, which may be used to calculate a correctly timed sequence of thruster commands. The commands should correct the pointing of the craft and take into account the vibration of any flexible parts at the same time. The research programme will

also look at the modes of vibration of such flexible structures by using a single sensor, typically a gyroscope, attached to the spacecraft. By adopting these techniques it should be possible to improve the accuracy of pointing the satellite from the present 0.15° to better than 0.05°

TV deliveries record

More than 4½ million television sets were delivered to the trade in 1983, a record for the industry according to BREMA, and nearly 17% higher than the previous year. The trend toward portables increasing their share continued, with the small screen segment taking 36%, an increase of 16%. Both teletext and small-screen monochrome deliveries were 12% up on 1982. Surprisingly however deliveries of video recorders and of music centres, the other two main categories that Brema analyse, have levelled off and show no growth over the previous year. For video this was in some measure due to rising prices of the more 'sophisticated' machines coming onto the market, say Brema, together with a run-down of stocks in the wake of uncertainties relating to format trends and the level of Japanese imports following the recent MITI and EEC agreement.

Efp conferences

Electronics for Peace is organising three regional Saturday conferences this summer for electronics and computing engineers to meet and discuss the wider social and military implications of the electronics industry.

The dates and places are
Saturday June 2nd, Sheffield
Saturday June 9th, Bristol
Saturday June 16th, London.
Details from Efp, 151 Courthouse Road, Maidenhead, Berks, or tel. (evenings) 0892-46354 or 0628-20225.

For Ambit read Cirkit

Following rapidly on the report that Ambit, the component distributors, were to move to Broxbourne, was another report that they have been sold to A.F. Bulgin & Co. Bulgin are to combine this company with others (Solent Component Supplies, Broxlea Ltd and Projex Distribution) into a single company to be known as Cirkit. The new company will retain the

policy of Ambit of selling components in small quantities to the home constructor as well as in bulk to industry. The catalogues of all the different companies listing over 10 000 different products are to be combined into a single consolidated catalogue later in the year. Cirkit commences trading from Broxbourne, Herts, from May 1st.

Adaptive delta modulation for tv sound

With an eye to satellite and cable reception for tv sound, Dolby Laboratories have developed a digital encode-decode system that could also be used for terrestrial broadcasting of stereophonic tv. The new digital audio system — shown at Eurocast, Basel, in May — has already been licensed to General Instrument in the USA for use in its satellite tv plans. Under the terms of the licensing agreement, General Instrument will build subscriber decoders and Dolby will manufacture encoders for use at the up-link satellite station or at the cable system head-end.

The specifications of the process, a form of adaptive delta modulation, are comparable to those of the Compact Disc: 'The high cost of the CD process and of other promised home digital home media may well impede the growth of consumer acceptance of digital audio' say Dolby Labs. The Dolby/GI pact they say will allow tv audio to be the first to deliver digital audio quality to the regular consumer.

Dolby aimed at a narrow bandwidth, around 200 to 350kbit/s, the exact rate being chosen to suit the transmission system, and chose delta modulation rather than p.c.m.

because of superior performance at low data rates and lower sensitivity to errors. No precision components are needed in the decoder, the performance and bandwidth advantages being gained by placing more complex circuitry in the transmission encoders. The system is said to be particularly useful for electronic delivery systems such as cable tv, satellite-delivered programmes and d.b.s. audio systems, where minimal error correction will lead to cheaper decoder designs.

Dolby Laboratories must be hoping to have more luck in interesting the BBC in this development than they did with the analogue Dolby f.m. scheme; the BBC have said they are now considering a digital system for stereophonic television.

934MHz Club UK

A club for users of 934MHz Citizens' Band has been formed to encourage and further the use of this band and to represent users to the official bodies concerned with radio communications. There will be a quarterly magazine to keep members informed of news and events with details of new equipment, letters and technical queries. Projected is a National QSL bureau for use by members, with club log books and QSL cards. The club organizers have already written to those users that they know of and have had a good response but they are aware that there is a large number of users that they haven't contacted but who might like to join. Details from the Honorary Secretary, 934MHz Club UK, Glenys Anthony, PO Box 424, Chelmsford, Essex CM6 3UR.

New Research Head at BBC

Bruce Moffat has been appointed the new Head of BBC Engineering Research Department, where he has spent most of his working career. He has undertaken investigations into the causes and prevention of head clogging in video tape recorders, and into the possible techniques for digital television recording. As Head of the baseband systems section he worked on the development of multi-channel digital audio

transmission systems and near-instantaneous digital companding, the forerunner of Nicam, accepted by the CCIR as part of a system for satellite broadcasting. On transferring to the storage and recording section he managed many projects including real-time digital audio signal processing, which has made feasible the development of a digital sound mixing desk. Another project was digital multi-image storing and

animation. As head of the studio group he became responsible for the workings of several sections. Dr. Moffat has written or contributed to numerous papers, mostly on digital audio and video techniques. He also serves as chairman of the UK CCIR working group on high-definition tv.

6809 newsletter

First issue of the 6809 User Group Newsletter (March-April) is priced at 75 pence but subsequent issues will cost 50p, according to its editor Paul Hills, and includes a free 6809 instruction card. "After long pauses and polite arguments" says Paul "we exist" and although only a small group he believes '6809' will stay alive because for every reader 90% of it is relevant. "Looking through another newsletter, I found *only* one out of 13 articles that were relevant to my interests." The first issue contains articles on an assembly course for upgrading from 6502, software for 6809 based microcomputer with normal memory-mapped screen, interfacing 76489 sound generator, and is available from Paul Hills at 28 Woburn Road, Launceston, Cornwall.

Electronics consultancy

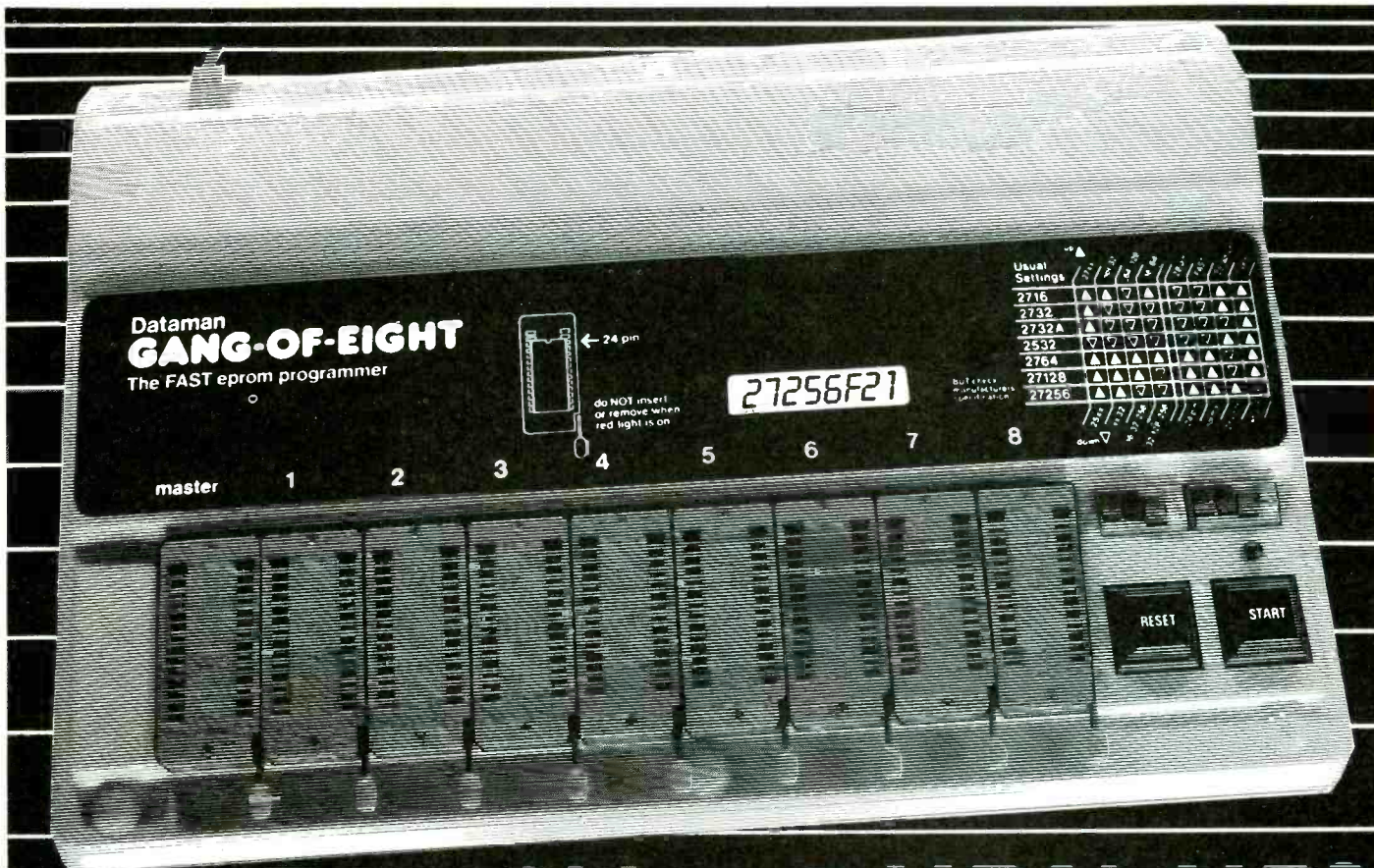
John Woodgate, B.Sc (Eng), A.M.I.E.E., with over 25 years of product design and marketing experience, has left ITT Consumer Products (UK) as products manager to set up his own consultancy J.M. Woodgate & Associates. Currently specializing in standards advice, he is chairman of two BSI committees on electronic equipment for domestic and educational use, as well as being involved with international standards work. J.M. Woodgate also offer prototype design and evaluation of audio and video equipment, display equipment for exhibitions and consultancy in marketing. 3 Bramfield Road East, Rayleigh, Essex SS6 8RG.

Optical data storage

Two agreements have been signed for the development of laser-read disc systems for the storage of computer data. The first is between Philips and the US Computer manufacturer, Control Data. They plan to extend their existing co-operation in optical disc storage development to also include the design, manufacture and marketing of optical recording peripherals and associated media for use with computers. The discs are likely to be only written on once to give a permanent record of up to a billion characters. The reading process will be similar to that used in Laservision and compact discs. The jointly owned

company is to be known as Optical Storage International (OSI).

With a slight rearrangement of the initials we get OIS, Optical Information Systems, another joint company this time formed by an agreement between Acorn Computers and BSR International. They too intend to develop a new digital, optical data storage. BSR is to provide the high volume manufacturing facilities while Acorn uses their computer technology know-how. Their first joint product will be a compact laser disc drive with significantly greater storage capacity, and faster access time than presently available with conventional floppy discs.



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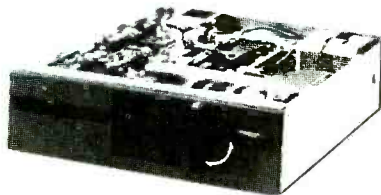
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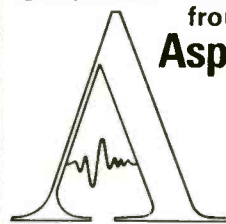
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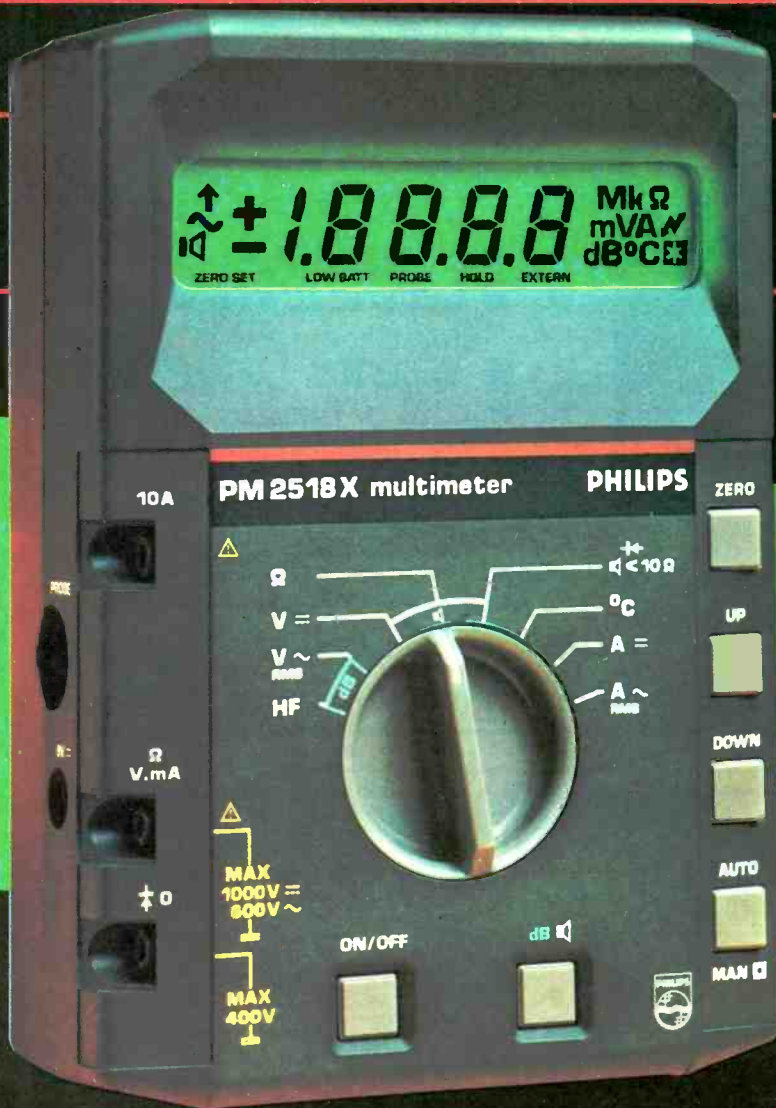
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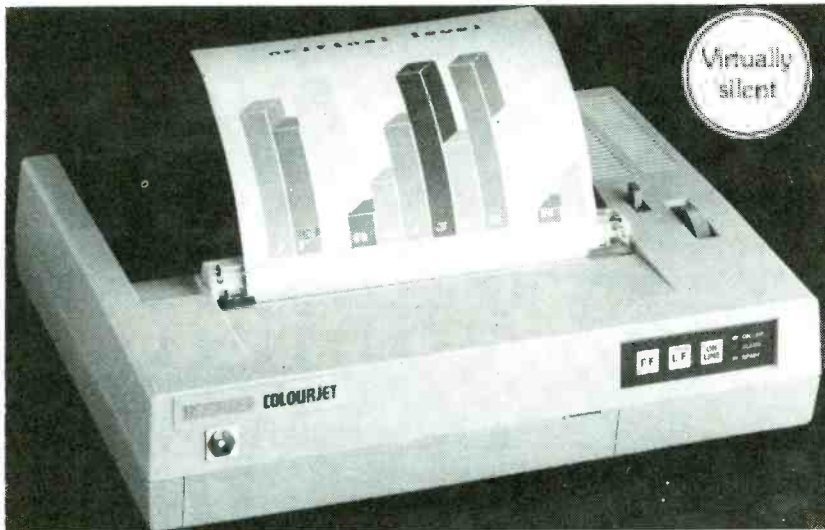
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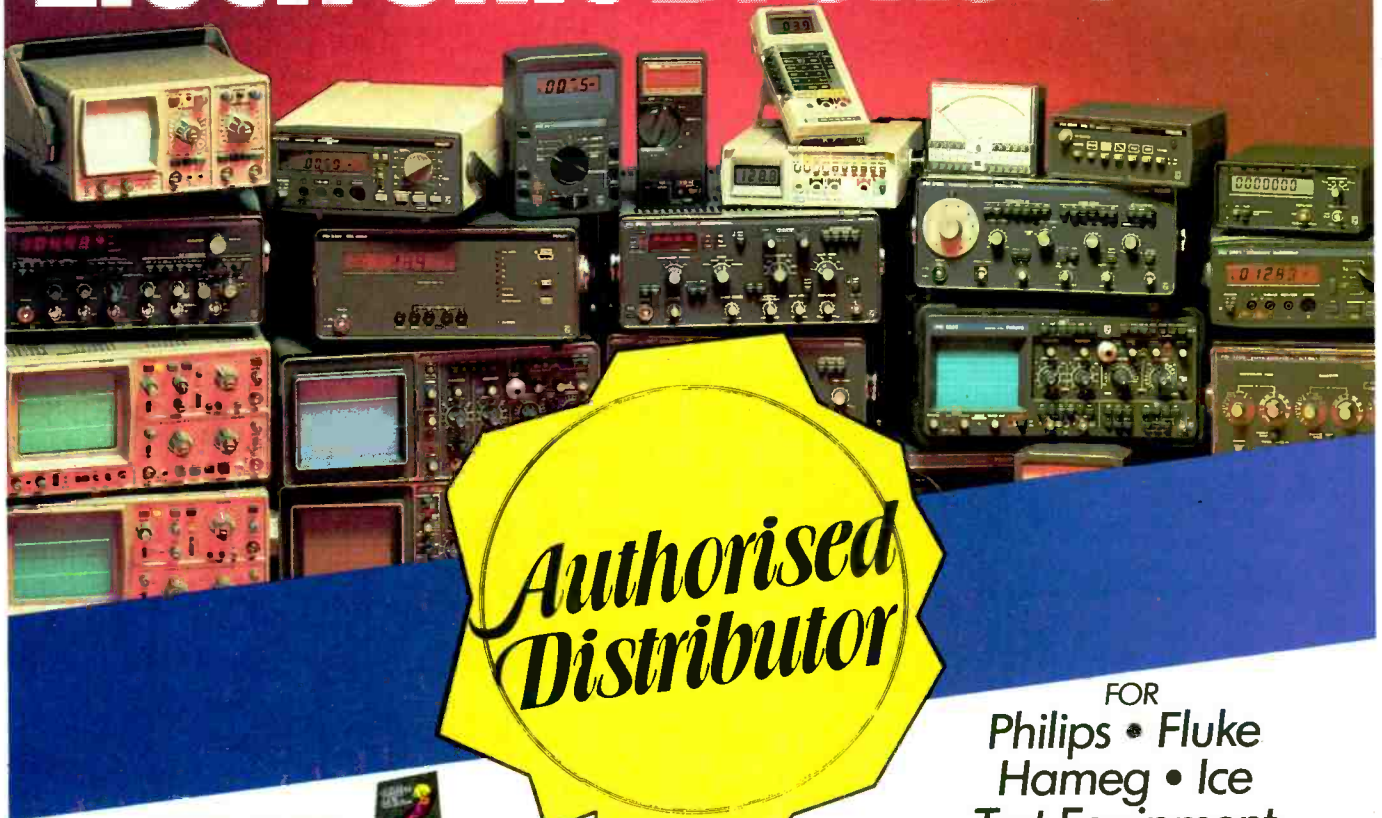
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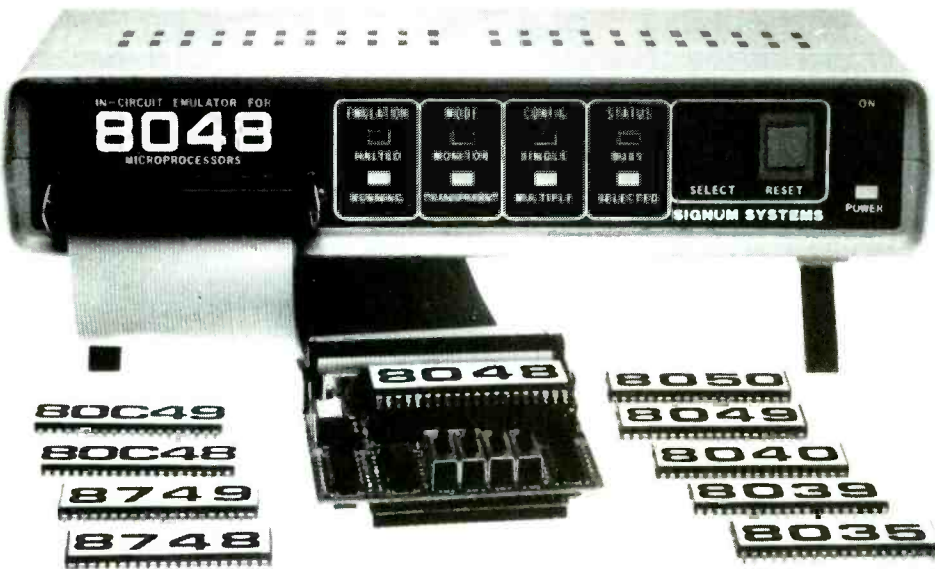
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AC142K 0.23	BD132 0.25	BU407 0.75	DBA90 0.80	2N 5299 0.30	2SB405 0.22	PCF804 0.50	LED 5mm
AC142K 0.23	BD133 0.25	BU407 0.75	DBA90 0.80	2N 5299 0.30	2SB405 0.22	PCF804 0.50	LED 5mm
AC153K 0.23	BD135 0.20	BU408 1.00	DBA90 0.80	2N 5299 0.30	2SB405 0.22	PCF804 0.50	LED 5mm
AC15 0.18	BD140 0.20	BU500 1.15	DBA110 0.20	2N 6109 0.40	2SC460 0.24	PCF805 0.55	LED 5mm
AC176K 0.20	BD138 0.20	BU526 1.00	DBA112 0.60	2N 6107 0.40	2SC495 0.60	PCF805 0.55	LED 5mm
AC187 0.15	BD139 0.20	BU526 1.00	DBA202 1.80	2N 6109 0.40	2SC733 0.40	PCF805 0.55	LED 5mm
AC187K 0.20	BD140 0.20	BU526 1.00	DBA202 1.80	2N 6109 0.40	2SC716 1.40	PCF805 0.55	LED 5mm
AC180 0.17	BD144 0.90	BU526 1.00	DBA202 1.80	2N 6109 0.40	2SC112Y 1.55	PCF805 0.55	LED 5mm
AC188K 0.23	BD150 0.30	BU526 1.00	DBA230 1.40	2N 6109 0.40	2SC1279 0.24	PCF805 0.55	LED 5mm
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ACY19 0.44	BD158 0.38	BU526 1.00	DBA230 1.40	2N 6109 0.40	2SC1279 0.24	PCF805 0.55	LED 5mm
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AD149 0.45	BD175 0.30	BU526 1.00	DBA230 1.40	2N 6109 0.40	2SC1279 0.24	PCF805 0.55	LED 5mm
AD161 0.22	BD177 0.30	BU526 1.00	DBA230 1.40	2N 6109 0.40	2SC1279 0.24	PCF805 0.55	LED 5mm
AD162 0.22	BD179 0.32	BU526 1.00	DBA230 1.40	2N 6109 0.40	2SC1279 0.24	PCF805 0.55	LED 5mm
AF124 0.28	BD181 0.45	BU526 1.00	DBA230 1.40	2N 6109 0.40	2SC1279 0.24	PCF805 0.55	LED 5mm
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AF127 0.25	BD203 0.42	BU526 1.00	DBA230 1.40	2N 6109 0.40	2SC1279 0.24	PCF805 0.55	LED 5mm
AF139 0.22	BD204 0.42	BU526 1.00	DBA230 1.40	2N 6109 0.40	2SC1279 0.24	PCF805 0.55	LED 5mm
AF239 0.22	BD222 0.31	CA270 0.40	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
AL112 0.18	BD232 0.31	CA270 0.40	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
AL113 0.80	BD232 0.31	CA3089 1.50	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
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AV106 1.80	BD355 0.38	MJ2500 1.00	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BA145 0.10	BD357 0.40	MJ2955 0.55	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BA148 0.10	BD358 0.40	MJ3000 1.15	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BA154 0.06	BD365 0.80	MJ3000 1.15	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BA154 0.06	BD365 0.80	MJ3000 1.15	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BA157 0.12	BF180 0.16	MJE304 0.30	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
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BB105B 0.16	BF184 0.20	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BB205B 0.24	BF194 0.05	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC107 0.07	BF194 0.05	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC108 0.07	BF195 0.05	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC109 0.07	BF196 0.05	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC115 0.10	BF199 0.06	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC118 0.11	BF200 0.16	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC140 0.19	BF257 0.18	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC141 0.19	BF258 0.18	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC142 0.19	BF259 0.18	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC164 0.06	BF336 0.20	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC147 0.05	BF337 0.20	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC148 0.05	BF338 0.20	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC157 0.05	BF422 0.30	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC159 0.05	BF428 0.19	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC182 0.06	BF481 0.10	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC192L 0.06	BF529 0.20	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
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BC213 0.06	BF592 0.14	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm
BC214 0.06	BF657 0.25	MJE520 0.36	TP120 0.18	IN 4400 0.06	2SD234 4.30	PCF805 0.55	LED 5mm

Stereo on tv

Some ten years ago, American television engineers put 'stereo sound' at the top of those developments they expected to see introduced during the next decade. Sure enough, Japan has had some stereo tv for several years, the Federal Republic of Germany for rather fewer, using its own two-carrier system; the BBC has been experimenting with several systems, including digital stereo test transmissions from Wenvoe and Crystal Palace. British hopes are also pinned on the multiplexed digital sound and data channels of the C-MAC/packet satellite transmission system that can provide up to about eight mono or four high-quality stereo channels per transmission. In the USA, the industry (EIA) has been attempting to evaluate three different systems for several years and has picked a Zenith f.m. system using a 31kHz subcarrier and with a 78kHz sub-carrier possible as a bilingual channel.

EIA also favours the use of dbx noise reduction to provide amplitude companding to reduce the dynamic range during transmission. It is claimed that suitable stereo decoding could be provided for \$25 (plus the cost of the extra audio amplifier/loudspeaker unless used with an existing external amplifier). Stereo tv sets for this system are likely to appear in prototype form at the Chicago Consumer Electronics Show this June.

Broadcasters have been concerned that, as for medium-wave a.m. — stereo, the FCC would leave the systems decision to the marketplace. In fact, FCC has refused to come out in favour of a single system but has announced that it will enforce interference protection for Zenith-dbx transmissions which, in effect, prevents rival systems using the subcarrier frequency, and makes Zenith-dbx virtually the American standard. So it is the green light for Zenith-dbx but still leaving at least three other systems in contention in Europe. Meanwhile v.c.r.-type stereo tv sets are being marketed in the UK, including those with pseudo-stereo circuitry for use on mono television broadcasts. Some broadcasters have been recording at least some

programmes in stereo for several years, aided by the stereo tracks of the lin "A" format.

While some programmes, such as stage opera, are a natural for stereo, this is not true of many others, where we are used to sudden changes in camera angles, etc. There are still some people who argue that you need a much wider and larger screen before stereo is effective — but the experience with simulcasts has shown that this does not deter enthusiasts for a wider "sound stage".

Digital distortions

Chris Dillon, a lecturer in electronics at The Open University, agrees with some of the speakers at the research meeting organized last year by The Royal Society (*Communications Commentary*, October 1983) that the impact of digital techniques is tending to distort the whole emphasis of formal electronic engineering training with many young engineers and others believing that "everything will be digital once the speed limitations of digital integrated circuits have been overcome." The result is that industry is finding it extremely difficult to recruit enough competent analogue engineers. As one recruiter put it: "They can all connect matchboxes together but we can't find enough people who understand how a simple emitter-follower works". In his own field of crystal filter design, manufacturers are facing a chronic shortage of design engineers, Chris Dillon believes. One also hears of trainee r.f. engineers being tempted into industry even before completing their training as broadcast field engineers.

The basic problem is partly that many of those who make decisions in government and education are profoundly dazzled by the euphoria surrounding "new technology" and "information technology" and fail to appreciate the skills really required from electronics engineers now and in the future.

The way in which British and European firms are losing out in fields in which they were formerly up with the leaders was all too evident at a recent Royal Television Society meeting on electronic cameras. Although the

world's first "automatic" camera was the Marconi Mark VIII a decade ago, a succession of speakers described recently installed computerized cameras in re-equipped British tv studios. All the cameras actually installed during the past two or three years appeared to be of American or Japanese manufacture.

NAB more technical

The character of the large annual shindig of the American National Association of Broadcasters (this year at Las Vegas, April 28 to May 2) appears to be changing. The 'international' aspects are increasingly being emphasized and this year an extra full day of technical sessions on the Saturday was inserted into the programme as a sign that NAB is expanding beyond a trade show to the level of a full-blown technical conference. This year's technical talking points were multichannel tv sound; solid-state (c.c.d.) cameras; analogue "component" recording and cartridge machines; high-efficiency and computerized directional m.f. aerials; and the use of microprocessors in transmitters.

The United States Information Agency is seeking a large increase in funds for the financial year next September with plans to spend a billion dollars over the next five years to modernize "Voice of America" equipment. USIA is currently busy establishing a "Worldnet" of tv circuits based on satellites; Euronet linking Washington with European capitals became operational last October and has been followed by Arnet for South America. During 1985, tv circuits will be leased for up to three hours, five days a week, to the Pacific, Africa and the Middle East.

Multipath and radiodata

For many sub-carriers on v.h.f./f.m. broadcasts in the USA have been used to carry a second mono channel in the system known as SCA (subsidiary communications authorization), or often called storecasting since its original use

was to provide uninterrupted background music in department stores. More recently it has been deregulated by the FCC to permit its use for many applications, including a further sub-carrier that can be used for radiopaging.

SCA has always been frowned upon in Europe on the grounds that in some circumstances, particularly under multipath conditions, the quality of the main stereo channel can be degraded by cross-talk. However, over the past few years, European broadcasters have been developing a radiodata system to carry identification, switching and information data signals, but not a mono audio channel, on v.h.f. broadcasts. There have been several field trials in various countries including Sweden, whose system has come near to acceptance by EBU, and has recently been undergoing further field trials by the BBC at Wrotham, Kent.

The level of the data signals, it was thought, would be low enough to avoid interference with the stereo signal even under bad multipath conditions. This does not seem to have proved the case since there have been a few, but very vocal, complaints from listeners. Wrotham now uses 'mixed' polarization which, in some terrains, can increase the amount of multipath. Now the EBU and BBC will have to decide whether the complaints are few enough to be ignored — or whether once again it is a question of back to the drawing board. Multiplexing works well when the radio path is good — but can prove a real problem in some circumstances. Even supersonic control signals can present difficulties.

Baird in history

One of the very few surviving 30-line televisions, made for the Baird company by Plessey around 1930, has been carefully restored by Ian Moth of Plessey Radar and loaned for exhibition at the Arreton Wireless Museum on the Isle of Wight, run by Douglas Byrne, G3KPO.

As a historical curiosity, 30-line televisions deserve to be carefully preserved. But I have been surprised to find how furiously a number of people still resent any suggestion that Baird's low-definition tv system was barely "true television"

since, even in its final broadcast form, it contained no real sync. signals. The televisions, by the time they reached the market, included a phonic wheel system that had to depend upon the black edge of the picture, as a crude and most uncertain form of synchronization. The instructions recommended running the motor for some 15 minutes before attempting to lock the picture! There were no sync. pulses and these would have been virtually impossible to transmit on medium waves.

Logie Baird *does* deserve a firm place in the history of television but primarily for the interest he stirred up that led so quickly to the development of high-definition tv on v.h.f. In 1959, Peter Eckersley, who as first chief engineer of the BBC recognized the futility of the Baird 30-line system, wrote in *Wireless World*: "Baird stood above his contemporaries in imagination, but, as events proved, below them in knowledge... I was truly sorry for him. He was 'fooled to the top of his bent; told by a sensation-seeking press that he was the world's greatest technical genius, dazzled by the prospect of millions of money... how fatal to hopes are the brute facts of physics."

Yet there are still those who believe that he was the sole inventor of television and refuse to question the way in which his early demonstrations were 'contrived' (to quote Frank Haynes) or to realise that much of what was published about them was more a tribute to Baird's imagination than his actual results, innovative experimenter though he undoubtedly was. It is essentially a sad story but not one that should be buried in myths.

Amateur Radio

Cable woes

The problems experienced by radio amateurs in the Milton Keynes area due to radiation of signals from the BT cable tv system within the amateur 144MHz band has proved harder to overcome than originally

appeared. Despite additional filtering interference to local amateurs continued and has led to the offending channel being taken out of service.

In the USA it is not only radio amateurs who are affected by wide-band cable distribution. During 1983, the FCC fined cable systems a total of more than \$200,000 for violations of the rules under which channels within the aeronautical bands can be used; this is permitted subject to prior clearance and a specified maximum level of signal leakage. It would appear that some cable operators have infringed both these conditions, and a number have been ordered to cease using these frequencies.

Meanwhile throughout the world, the list of consumer appliances, car electronics etc. that have proved to be either susceptible to local transmitters or alternatively to radiate r.f. interference or electrical noise continues to grow. Electronic telephone handsets with i.c. amplifiers; cordless telephones; smoke detectors; v.c.r. machines; microwave ovens; microprocessor controls; home computers, etc., etc. Yet many of the problems could have been avoided if the designers had paid more attention to basic questions of electromagnetic compatibility and had some screening, by-pass capacitors, r.f. chokes, etc.

40 years on

With the approach of the 40th anniversary of D-Day, June 6, 1944, several groups of amateurs are planning to participate in events designed to mark that event. The G-QRP Club, for instance, is organizing a contest in which its members will design and construct a modern 'suitcase' two-way h.f. set in recognition of the role played by such sets in 1944, including the use of the B2 by the Jedburgh and SAS groups who dropped by parachute into Normandy.

Sid Hall, G3BR (53 New Street Hill, Bromley, Kent) has been compiling lists of the radio amateurs who joined the Civilian Wireless Reserve in 1938-39 and subsequently served at the outbreak of war in the RAF in the W/T Emergency Fitting Parties, or with the Wireless Intelligence Screen which included the "Early Birds" who reached France on September 5, 1939. He has

traced no less than 120 former C.W.R. members, most of them still active radio amateurs. Some 50 have joined in the s.s.b. nets he runs on 3760kHz at 10a.m. local time on the first Monday of each month or on the second Mondays on about 7050kHz.

The Emergency Fitting Parties, whose commanding officer was (the Rev.) H.A.M. Whyte, now VE3BWY but a leading pre-war dx operator as G6WY, absorbed more of the C.W.R. members than the Y service and were formed to install emergency radio equipment at RAF airfields. Some units helped install early radar equipment and also later helped jam and disrupt the German navigational aids.

Silent Uosat

Following a perfect launch on March 1, beacon signals from Surrey University's Uosat-2 satellite were well received on 145.825MHz during the first three orbits, but then ceased. It was thought that a 30-day switching sequence written into the software would bring the satellite back under control. Up to the time of writing, however, this has not happened and hopes are fading.

The RSGB has expressed concern that the intermediate frequencies being proposed for 12GHz DBS receivers could prove vulnerable to interference from strong local signals from transmitters working in either the 1.3GHz or 144MHz bands.

Here and there

The Chinese Radio Sports Association has now applied to join the IARU as a further move towards restarting normal amateur radio in that country. In view of the continued use of frequencies in the 'exclusive' amateur band between 7000 and 7100kHz by Chinese external-broadcast transmitters, as noted by R. E. Knowles, ZL1BAD, in the March 'Letters' (my earlier report of the apparent reduction of this nuisance proved short-lived although spring 1983 did see a noticeable improvement in Europe) not every society may feel inclined to vote the Chinese in; others may hope that the Chinese could exert more influence on their broadcasting authorities from within IARU. A

headquarters station, BY1PK, in Peking became active in March 1982 after 16 years of no amateur radio in China. But very few other stations have yet been permitted.

The British Amateur Radio Teleprinter Group has launched an ambitious new quarterly magazine called 'Datacom' replacing the former BARTG Newsletter. The first issue, which runs to 108 pages, includes a special feature on 'packet radio' and also information on the r.t.t.y. repeater located at Cambridge. Editor is Ian Wade, G3NRW, but for membership details contact John Beedie, G6MOK, 161 Tudor Road, Hayes, Middlesex (01-561 0010).

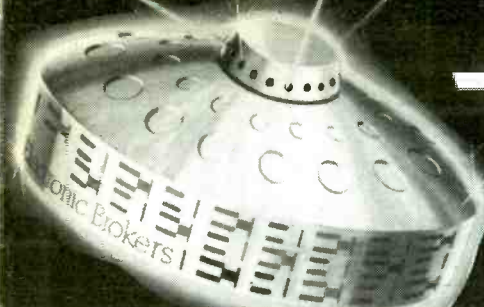
June mobile rallies include: June 3 Spalding (Springfields, Spalding), Welsh mobile rally at Barry Leisure Centre, Holton Road, Barry and RAIBC Picnic, Broadlands, Romsey, Hants; June 10 Elvaston Castle Country Park, 5 miles south-east of Derby; June 17 RNARS rally at HMS Mercury, near Petersfield, Hants and Denby Dale rally at Shelley High School, nr Skelmanthorpe, Huddersfield; June 24 Longleat rally at Longleat Park, Warminster.

A former Californian radio amateur, Richard Burton, is serving an 18-month prison sentence for continuing to operate his transmitter after his licence had been cancelled by the FCC for repeated use of obscene language.

At the Amberley Chalk Pits Museum and open-air industrial history centre, near Arundel, Ron Ham has recently completed the assembly of a "vintage amateur radio shack" in tribute to old-time radio amateurs including G2YL, G6YL and G2NM.

The RSGB National VHF Convention held at Esher at the end of March was attended by over 2500 people, considerably more than in 1983.

PAT HAWKER, G3VA



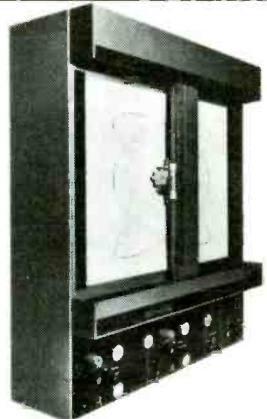
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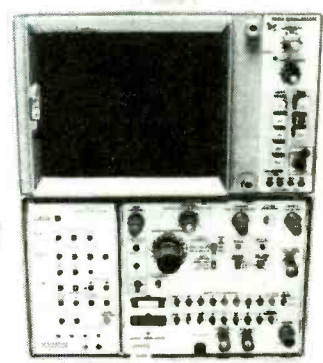


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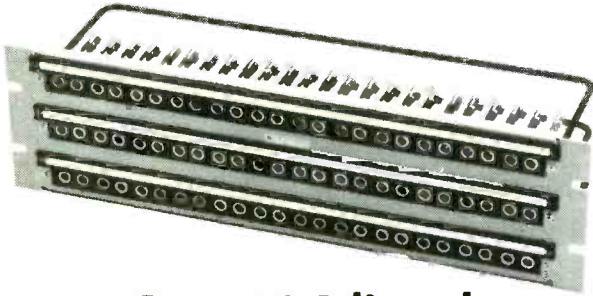
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VALVES		Minimum Order £1	*SPECIAL QUALITY	VALVES VAT IS INCLUDED							
A1065	1.40	EF89	1.60	PFL200	1.10	Z801U	3.75	6BW6	6.20	6Y6G	0.90
A2293	8.80	EF91	1.50		2.80*	Z803U	16.00	6BW7	1.80	6Z4	0.70
A2900	13.75	EF92	2.90	PL36	1.10	Z900T	2.45	6C4	0.60	6Z5	0.70
AR8	0.75	EF95	0.65	PL81	0.85	1A3	1.40	6C5	0.55	11E2	1.50
ARP3	0.70	EF96	0.60	PL82	0.70	1L4	0.50	6CH6	8.20	12A6	1.00
ATP4	0.60	EF183	0.80	PL83	0.60	1R5	0.80	6CL6	2.75	12AT6	0.70
B12H	3.90	EF184	0.80	PL84	0.95	1S4	0.45	6CW4	8.50	12AT7	0.85
CY31	1.40	EF812	0.75	PL504	1.00	1S5	0.45	6CX8	3.80	12AU7	0.60
DAP96	0.70	EFL200	1.85	PL508	2.40	1T4	0.45	6CY5	1.15	12AV6	0.60
DET72	28.50	EH90	0.85	PL509	5.30	1U4	0.40	6D6	0.70	12AX7	0.65
DF36	0.70	EL32	1.10	PL519	5.80	1X2B	1.40	6F6	1.60	12BA6	0.90
DH76	0.75	EL34	1.80	PL802(SE)	2.95	2X2A	2.50	6F6GB	1.10	12BE6	1.25
DL92	0.60		3.50*	PY80	0.70	3A4	0.70	6F7	2.80	12BH7	
DY86/87	0.65	EL37	5.20	PY81/800	0.85	3AT2	2.40	6F8G	0.85	12E1	2.30/2.95*
DY802	0.70	EL82	0.70	PY82	0.85	3BZ8	12.00	6F12	1.15	12J5GT	0.55
E92CC	2.80	EL84	0.80	PY88	0.60		19.50*	6F14	1.30	12K7GT	0.70
E180F	7.70	EL86	0.95	PY500A	2.10	3D6	0.50	6F15	1.30	12K8GT	0.80
E182CC	6.25	EL90	1.00	QQV03/10	3.20	3E29	19.00	6F17	0.75	12Q7GT	0.60
EA76	2.25	EL91	4.20		7.50*	3S4	0.60	6F23	0.75	12S07	0.65
EABC80	0.80	EL95	0.80	QQV03-20A	4B32	18.25	6F24	1.75	12S07	0.65	
EB91	0.60	EL504	1.70	QQV03-25A	5R4GY	1.80	6F33	10.50	12S17	0.70	
EB93	1.15	EL509	3.95		5LUG	0.75	6FH8	17.80	12S17	0.70	
EB93	0.30	EL519	6.90		36.50	5V4G	0.75	6GA8	1.95	12S07	1.45
EBF80	0.60	EL821	8.20	QQV06/40A	5Y3GT	0.95	6GH8A	1.95	12S07GT	0.85	
EBF83	0.60	EL822	9.95		19.50/36.50*	5Z3	1.50	6H6	1.60	12Y4	0.70
EBF89	0.80	EL80(SE)	2.80	QQV03-12	4.20	5Z4G	0.75	6JU6	5.85	13D5	0.90
EC52	0.65	EM80	0.85	SP61	1.80	5Z4GT	1.05	6L4	2.00	19A05	0.85
EC91	4.40	EM87	1.30	TT21	23.00	6Z0L2	0.90	6JAWA	2.30	19G3	11.50
EC92	0.85	EY51	0.95	TT22	23.00	6AB7	0.70	6J5	0.90	19G6	8.50
ECC81	0.85	EY81	0.65	UABC80	0.75	6AC7	1.15	6J5GT	0.85	19H5	39.50
ECC82	0.60	EY86/87	0.60	UAF42	1.20	6AG5	0.60	6J6	0.65	20D1	0.80
ECC83	0.65	EY88	0.65	UBF80	0.70	6AH6	1.15	6J6W	4.85	20E1	1.30
ECC84	0.60	EZ80	0.70	UBF89	0.70	6AK5	0.65	6JEC	4.85	20P1	0.65
ECC85	0.60	EZ81	0.70	UC84	0.85	6AK8	0.60	6JSEC	0.80	25L6GT	0.95
ECC88	0.80	GM4	5.90	UCC85	0.70	6AL5	0.60	6K7	4.50	25Z4G	0.75
ECC189	0.95	GY501	1.30	UCF80	1.30	6AL5W	0.85	6KD6	2.80	35W4	0.80
ECC804	0.90	GZ32	1.05	UCH42	1.65	6AM5	4.20	6L6G	3.70	85A2 140 2.55*	
ECF80	0.85	GZ33	4.20	UCH81	0.75	6AM6	1.50	6L6GT	1.80	807 1.60/2.40*	
ECF82	0.85	GZ34	2.75	UC182	0.95	6AN8A	2.50	6L8	0.70	81319.32 68.50*	
ECF801	1.05	GZ37	3.95	UF1	1.35	6AQ4	3.40	6L18	0.70	829B	24.00
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ECH42	1.20	K188	10.50	UF85	0.95	6A05W	1.80	60T7	1.30	866E	3.80
ECH81	0.70		13.80*	UL84	0.95	6AS6	1.15	6A7	1.80	866E	6.25
ECH84	0.80	ML4	2.80	UM80	0.90	6AT6	0.90	6S67	1.50	931A	19.80
ECL80	0.70	ML6	2.80	UM84	0.70	6A16	0.60	6S7	1.50	954	1.20
ECL82	0.75	NL09	9.90	UY82	0.70	6AV6	0.85	6S7J	1.40	955	1.20
ECL85	0.80	QA2	0.70	UY85	0.85	6AX6GT	1.30	6SK7	1.50	955	1.20
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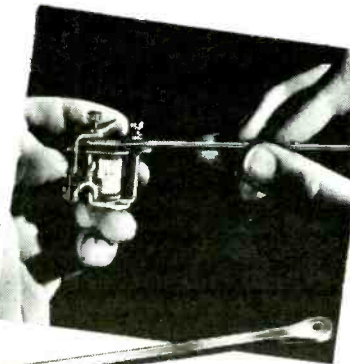
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METAL FILM		7499	74LS169	4080	19p		AC128	35p	BC465	35p	BSX23	24p	ZTX509	14p
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0.4 W EXTRA		7501	74LS171	4082	19p		AC130	35p	BC467	35p	BSX25	24p	ZTX511	14p
LOW NOISE		7502	74LS172	4083	49p		AC131	35p	BC468	35p	BSX26	24p	ZTX512	14p
100T TO 10M		7503	74LS173	4084	49p		AC132	35p	BC469	35p	BSX27	24p	ZTX513	14p
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LOW NOISE		7510	74LS180	4091	60p		AC139	35p	BC476	35p	BSX34	24p	ZTX520	14p
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As above with DP Mains Switch		7527	74LS197	4108	60p		AC156	35p	BC493	35p	BSX51	24p	ZTX537	14p
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As above with DP Mains Switch		7551	74LS221	4132	60p		AC180	35p	BC517	35p	BSX75	24p	ZTX561	14p
As above with DP Mains Switch		7552	74LS222	4133	60p		AC181	35p	BC518	35p	BSX76	24p	ZTX562	14p
As above with DP Mains Switch		7553	74LS223	4134	60p		AC182	35p	BC519	35p	BSX77	24p	ZTX563	14p
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As above with DP Mains Switch		7558	74LS228	4139	60p		AC187	35p	BC524	35p	BSX82	24p	ZTX568	14p
As above with DP Mains Switch		7559	74LS229	4140	60p		AC188	35p	BC525	35p	BSX83	24p	ZTX569	14p
As above with DP Mains Switch		7560	74LS230	4141	60p		AC189	35p	BC526	35p	BSX84	24p	ZTX570	14p
As above with DP Mains Switch		7561	74LS231	4142	60p		AC190	35p	BC527	35p	BSX85	24p	ZTX571	14p
As above with DP Mains Switch		7562	74LS232	4143	60p		AC191	35p	BC528	35p	BSX86	24p	ZTX572	14p
As above with DP Mains Switch		7563	74LS233	4144	60p		AC192	35p	BC529	35p	BSX87	24p	ZTX573	14p
As above with DP Mains Switch		7564	74LS234	4145	60p		AC193	35p	BC530	35p	BSX88	24p	ZTX574	14p
As above with DP Mains Switch		7565	74LS235	4146	60p		AC194	35p	BC531	35p	BSX89	24p	ZTX575	14p
As above with DP Mains Switch		7566	74LS236	4147	60p		AC195	35p	BC532	35p	BSX90	24p	ZTX576	14p
As above with DP Mains Switch		7567	74LS237	4148	60p		AC196	35p	BC533	35p	BSX91	24p	ZTX577	14p
As above with DP Mains Switch		7568	74LS238	4149	60p		AC197	35p	BC534	35p	BSX92	24p	ZTX578	14p
As above with DP Mains Switch		7569	74LS239	4150	60p		AC198	35p	BC535	35p	BSX93	24p	ZTX579	14p
As above with DP Mains Switch		7570	74LS240	4151	60p		AC199	35p	BC536	35p	BSX94	24p	ZTX580	14p
As above with DP Mains Switch														

Micro-controlled cassette recorder

by A. J. Ewins

Solenoid-operated cassette mechanism allows control of functions by push-button or microcomputer. Software to be described enables recorder to SAVE or LOAD automatically.

As a storage medium for micro-computer programs, the cassette tape-recorder is probably still the most widely used device, in spite of the falling prices of disc drives. Unless you are a Sinclair Spectrum owner, with a Microdrive, the cost of disc drives and controlling electronics is still very high. The storage capacity of a cassette tape is impressive; a C60 tape can store up to 750Kbytes of data when recorded at a rate of 2400 baud — 1.5Mbyte, if twin-channel recording is possible. However, cassette recorders cannot be used in an automatic SAVE and LOAD mode unless all the functions of the deck can be controlled by the microcomputer.

For some time now, Hart Electronics have been selling an entirely solenoid-controlled cassette deck of excellent quality. This series of articles describes the design of controlling electronics for this deck, enabling it to be operated by electrical push-buttons or direct from the 8-bit parallel output port of a microcomputer. Additionally, there is a design for a highly reliable f.s.k. system of electronics that enables the data from the microcomputer's serial line output (RS232 or t.t.l. level) to be recorded at a rate of 2400 baud. An electronic counter, clocked by the cassette deck's motion sensor, can be 'read' and 'reset' by the microcomputer via an additional 8-bit I/O port. This enables the tape to be wound or rewound to any desired position for the automatic SAVEing and LOADING of programs. The record/playback electronics are briefly discussed, since they are based on Linsley Hood's excellent design of a few years ago.*

Finally, examples of controlling software, developed on the author's UK101 microcomputer (a 6502 based machine) will be presented in a following article to illustrate how the various functions of the cassette deck may be automatically controlled. The program structure for the entirely automatic control of the cassette deck for SAVEing and LOADING of programs will also be discussed.

A block circuit diagram of the overall system is shown in Fig.1.

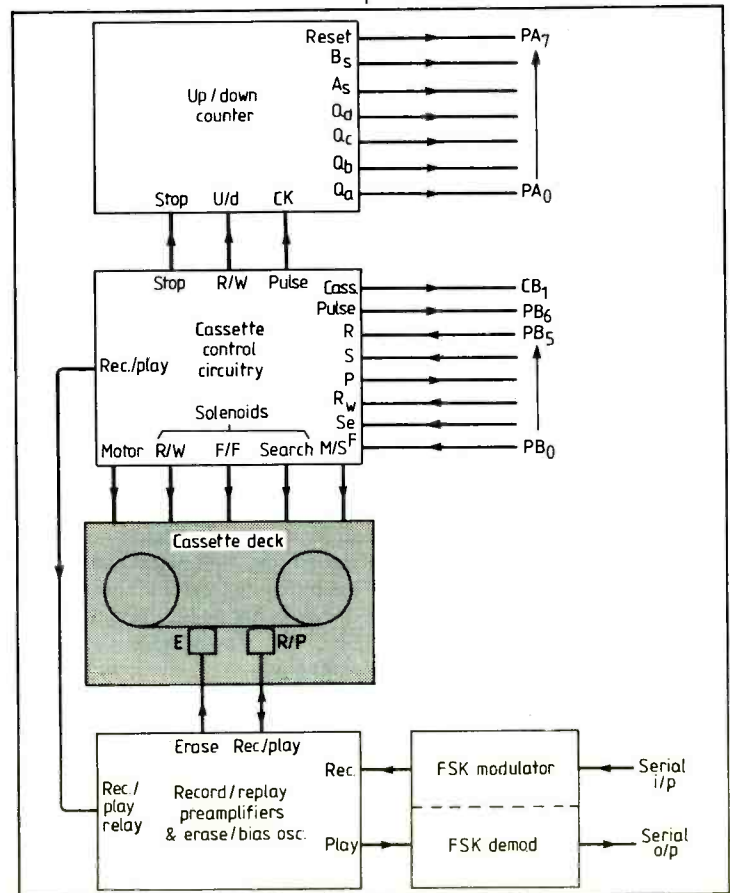
Control electronics

The solenoid-controlled cassette deck used in this design is the SF925F. Apart from its ability to be controlled electrically, it has all the usual specifications of a first-class cassette-deck mechanism; in particular a 12 volt motor with built-in electronic speed control and a wow and flutter figure of less than 0.08% weighted r.m.s. (0.2% DIN, r+p). Features which are specifically related to the design of the control electronics are micro switches to sense cassette-in-place and record prevention tab; a 3-digit memory counter with rotating magnet and Hall effect i.c. for motion sensing; and three solenoids which need an initial voltage of 16-24V, with a hold voltage of 7-10V. Current consumption per solenoid is 300mA at 12V.

Of the three solenoids, there are two main ones; one to control the fast forward, FF, function and one to control the rewind, R/W. The third allows the record/play-

back head to be lightly engaged during fast forward or backward winding. This is called the 'search' mode and the solenoid is referred to as the 'search' solenoid. For correct operation the deck, motor and solenoids must be operated in a particular sequence. For the record/playback sequence it is essential that the motor is switched on first and allowed to run up to speed before energizing the relevant solenoids. Although not essential in the fast-forward and rewind

Fig.1. Block diagram of cassette recorder for data or program storage. Cassette deck is SF925F from Hart Electronics.



*Wireless World, May, June, August, 1976. Reprinted in High-fidelity Designs, Vol. 2.

CASSETTE RECORDER

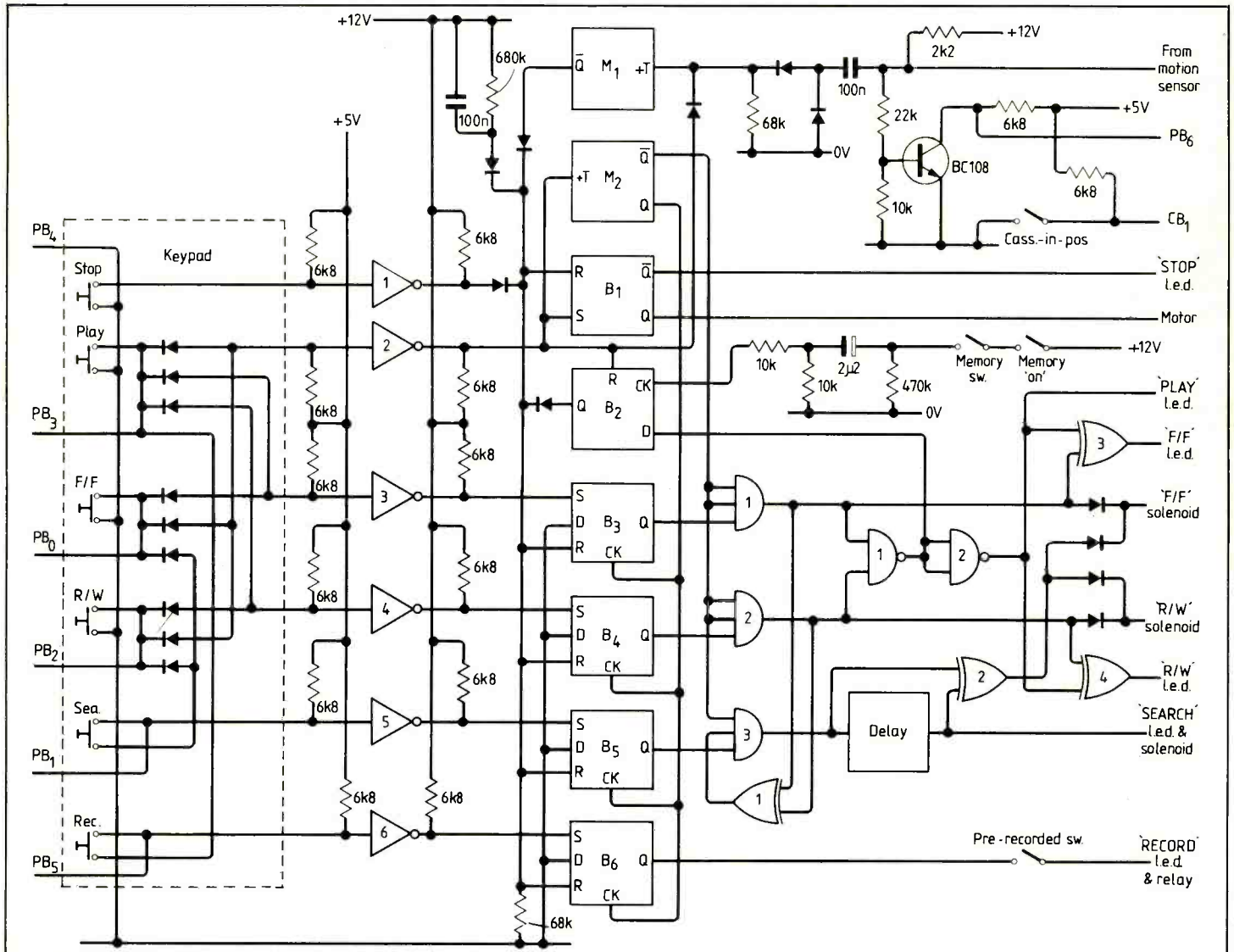


Fig. 2. Control circuitry for either push-button or computer-controlled operation.

sequences it is good practice to do so. Assuming then that the motor is switched on first, the usual type functions are performed in the following ways:

1. Fast forward — energize the FF solenoid.
2. Rewind — energize the R/W solenoid.
3. Play/record — energize the FF and R/W solenoids simultaneously. (For this function the momentum of the motor is used to assist the raising of the head/pinch-roller plate.)
4. Fast forward search — energize FF and R/W solenoids simultaneously and after a short delay (0.5s) energize the 'search' solenoid and de-energize the R/W solenoid.
5. Rewind search — as for F/F/S above, but in this case, after the short delay, energize the 'search' solenoid and de-energize the FF solenoid. (N.b., in this mode and the preceding one, the energizing of the 'search' solenoid may be carried out simultaneously with

the de-energizing of the R/W or FF solenoids; the slightly 'slugged' response of the de-energized solenoids will ensure that they drop out after the 'search' solenoid has energized.)

It is possible to switch from one function to another directly, provided that the previous function is cancelled first.

The circuit of the control electronics required to perform all the above functions in the correct sequence of motor and solenoids is shown in Fig. 2. It has been designed to be controlled by either push-button switches via diode-Or logic or by the correct selection of logic input lines from the 8-bit I/O port of a microcomputer. It is, of course, perfectly possible to control the energizing of the motor and solenoids in the correct order *directly* from the I/O lines of a micro, letting the software within the computer determine the necessary sequence of events. The author chose to design the control circuitry

specifically to allow manual operation so that the cassette deck could be operated in 'stand alone' mode and to allow its control to be overridden during software development.

To understand the operation of the control circuitry, consider its control via the six push-button switches. All the logic control elements are contained in c.mos digital i.c.s, except for the six inverting input buffers, which are contained in a low powered t.t.l. logic circuit type 74L05. These act as interfaces between the 12V logic levels of the control circuitry and the 5V t.t.l. levels from a microcomputer. The outputs of the six inverters are open-collectors, so 6k8 resistors are used as pull-ups to the 12V line. The inputs to the six inverters are normally open-circuit, and they are also pulled-up via 6k8 resistors, this time to the 5V rail. With the inputs to the six inverters at logic 1 level, their outputs are at logic 0 and no functions will be operating. The 100nF capacitor

in parallel with the 680k resistor and connected between the 12V rail and the reset, R, input of flip-flops B1 and B3 to B6 via a silicon diode ensure that all functions are held off during power-up.

Suppose that the fast-forward function is selected by pressing the FF push-button. The inputs to inverters 2 and 3 will be grounded via the keypad diode-Or logic. Their outputs will thus go high to logic 1. A high on the set, S, input of B1 sets its Q output high and its \bar{Q} output low. The motor is thus switched on and the stop led off. Simultaneously, a high on the set, S, input of B3 sets its Q output high. However, at the same time, the monostable, M2, has been triggered by the output of inverter 2 so that its \bar{Q} output goes low. The output from And 1 thus stays low until \bar{Q} of M2 goes high. When it does so, after the monostable, M2, delay period of about half-a-second, the FF solenoid is energized and the cassette deck goes into the fast-forward function. The Q output of M2, which goes high when M2 is triggered, is used to clock all four flip-flops, B3 to B6, resetting to zero (via the logic 0 on their D inputs) all those whose set inputs are not simultaneously high. In this manner previous functions are automatically cancelled before the new one is selected.

The successful operation of any function depends on the operation of the push-buttons being momentary. This is because of the mode of operation of the motion sensing circuitry and the monostable, M1. When the cassette deck is running with a cassette in position, the output from the motion sensor is a train of positive pulses. This train of pulses is fed to the trigger input, +T, of M1 via the 100nF capacitor and associated diodes and 68k resistor. The monostable, M1, is operated in a retriggerable mode so that its \bar{Q} output will remain low so long as it is continuously triggered. In the event of tape motion ceasing, the pulse train to the trigger input of M1 will also cease and its \bar{Q} output will eventually go high (after a delay of about 2s). When it does, flip-flops B1 and B3 to B6 are reset and the function in operation is cancelled. Prior to the operation of any function the \bar{Q} output of M1 is always high. For a function to operate it is therefore necessary to trigger the \bar{Q} output of M1 low at the same time the function is selected. This is achieved by the

diode link from the output of inverter 2 to the +T input of M1. If a push-button such as FF is held pressed, the output of inverter 2 remains high and so does the +T input of M1. M1 cannot be retriggered whilst +T remains high. Thus, at the end of the period of M1's temporary state, \bar{Q} of M1 will again go high, cancelling the selected function. Thus no function button should be held pressed for more than about 2 seconds. It is perfectly natural to operate the push-buttons momentarily and this feature is of no consequence; in fact it can be used to cancel a function wrongly selected.

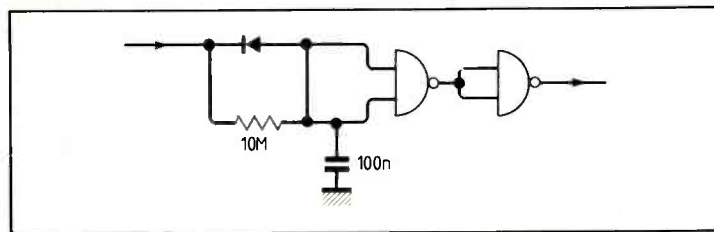


Fig. 3. Delay circuit to energize search solenoid.

Selection and operation of the rewind function is carried out in a similar manner to the fast-forward function by pressing the R/W button. In this case the R/W solenoid is energized via inverter 4, flip-flop B4, and And 2. The play function selection may also be readily understood as pressing the Play button merely energizes both FF and R/W solenoids simultaneously, after the motor run-up delay period of half a second. The record function is selected by pressing both Play and Record buttons together. The Record button is linked to the Play button such that Record will only operate with the Play button and no other. The record function operates exactly as for Play but with the addition of energizing a record relay via logic signals from inverter 6 and flip-flop B6. No delay is imposed between pressing Record/Play and the operation of the record relay. This gives the Record electronics of the cassette deck time to settle before recording actually begins. The 'pre-recorded' tab microswitch is wired in series with the Q output of B6 and the record relay driver transistor, thus preventing a cassette from being recorded that has had its pre-recorded tab removed.

The remaining functions not so far described, and involving a little more circuit sophistication, are those of the fast-forward and rewind search modes. The Stop function, it is hoped, speaks for itself and merely cancels all func-

tions by resetting flip-flops B1 and B3 to B6. The Search functions are selected by pressing the Search button together with the desired FF or R/W button. The Search button only functions when pressed with FF or R/W; not on its own or with any other button. If all three buttons are pressed together the Play function results. When the search function is selected, the Q output of B5 is set high. A high output from And 3 occurs only after the usual delay period and only if the output from And 1 or And 2 is high; not if neither And 1 nor And 2 is high, nor if both are high. This logic is determined by the

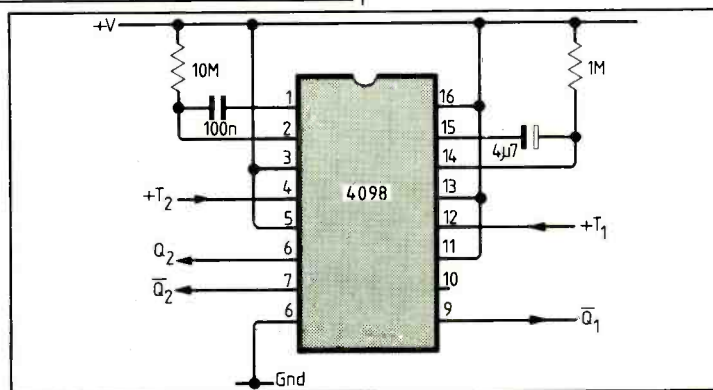


Fig. 4. Circuit of delay flip-flops M1 and M2.

exclusive-Or gate, XOR 1, and its output to the input of And 3. A high output from And 3 immediately operates both R/W and FF solenoids via XOR 2 and the two silicon diodes. After a delay of about half-a-second the output from the delay circuit goes high, energizing the search solenoid. As both inputs to XOR 2 are now high, its output goes low. Either the R/W or FF solenoid will thus drop out, the other remaining energized by the high on the output of And 1 or And 2, depending on which search function was selected.

The cassette deck counter is fitted with a 'memory' function, which is simply a switch closure associated with the 000 count. When a part of the tape is found to which the operator may wish to return at a later time, the counter is simply reset. Winding forward or back to this 000 count position results in the memory switch contacts closing. To stop the R/W or FF functions when this condition is reached, the flip-flop B2 is

CASSETTE RECORDER

included. The $2\mu\text{F}$ capacitor, diode and 470k and 10k resistors debounce the memory switch contacts, so that reliable operation of the memory switch is achieved. When the memory switch contacts close, B2 is clocked. If the D input is high, then the Q output will go high, resetting flip-flops B3 to B6 and B1, cancelling the selected function. The D input is taken from the output of Nand 1, so that it is high for all functions except Play or Record. The memory function thus operates only when in the FF, R/W or two search modes.

In addition to operating the

computer. The cassette-position microswitch is also connected to a 6k8 resistor from the 5V line to provide a logic signal that can be read by the microcomputer. The delay circuit, shown in Fig. 3, is made up from the two remaining 2 i.p. Nand gates of a quad i.c., type 4093, which has Schmitt trigger inputs. Figure 4 shows the detailed circuit of the two monostables, M1 and M2, using an i.c. type 4098 or 4538. The motion sensor of the cassette deck mechanism is a Hall-effect i.c. There are three connections to it; two are the supply rails, 0 and +12V and the third is the out-

noids and capacitors is also connected, via diodes, to a 10V peak, unsmoothed, d.c. supply. Thus, at the instant of energizing, the initial voltage across a solenoid will be nearly 20V, and will fall to a 'holding' voltage of about 10V provided by the 10V unsmoothed d.c. supply. Since the voltage drop across a 220 ohm resistor is about 11V (when its solenoid is energized) it must be capable of dissipating $(11^2/220)$ watts, i.e. just over 0.5W. 1 watt resistors should therefore be used. The value of the 220 ohm resistors is chosen to be low enough for the 2200 μF capacitors to charge to a

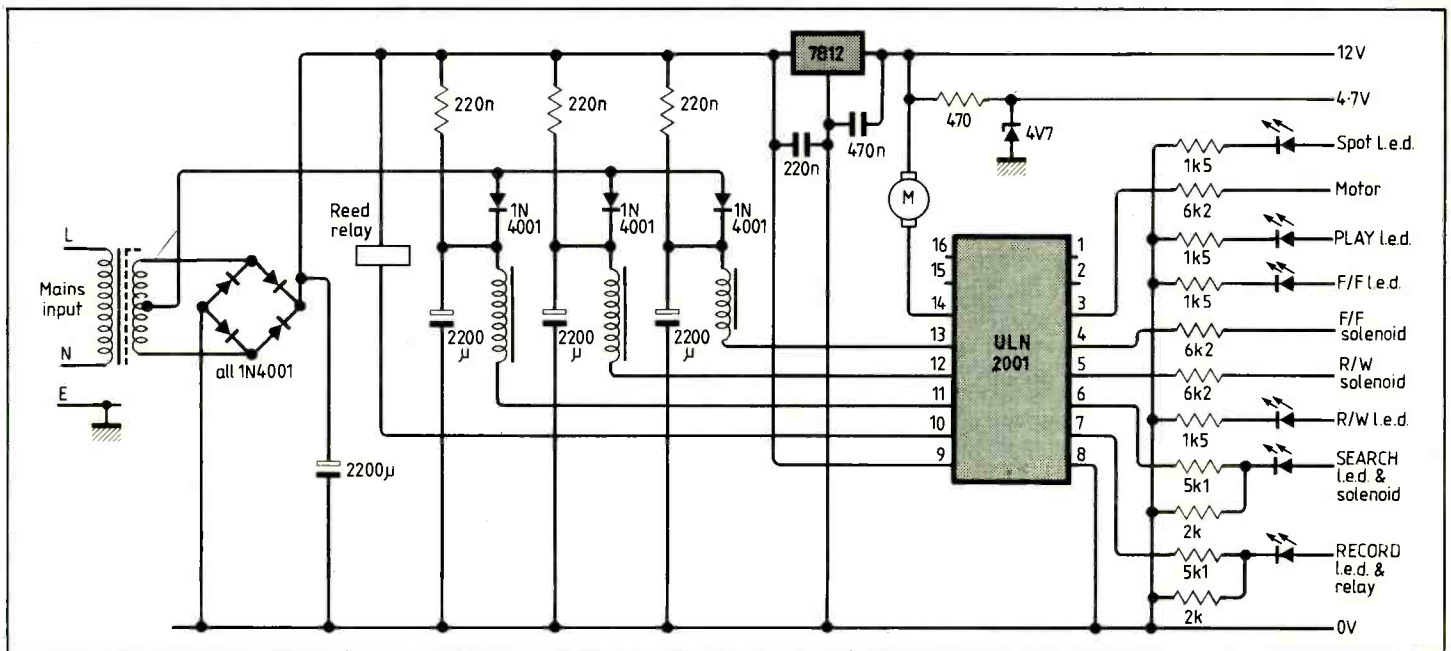


Fig. 5. Power supply for control circuitry.

required solenoids for a particular function, the control circuitry provides logic signals to illuminate a number of leds to show the function in operation. The operation of the stop, search and record leds is straightforward and needs no further explanation. However, it is necessary to decode the FF and R/W logic signals to provide led indications for the FF, R/W and Play functions. The play led is illuminated when both FF and R/W solenoids are energized by a signal provided by Nand 1's output inverted by Nand 2. The FF led needs to be illuminated when the FF solenoid is energized, but not when FF and R/W solenoids are energized; XOR 3 provides this signal. In a similar manner XOR 4 provides the signal for the R/W led.

The BC108 transistor and associated resistors converts the train of pulses from the motion sensor (at a 12V signal level) to a 5V level suitable for reading from the 8-bit I/O port of the micro-

put to the control circuitry. The i.c. was found to operate better with the addition of the 2k2 pull-up resistor as shown in Fig. 2. Connection details to the i.c. are supplied with the deck.

To drive the motor and solenoids of the cassette deck and the record relay from the logic signals of the control circuitry, it is obviously necessary to provide suitable driver stages. A suitable circuit is shown in Fig. 5, together with a power supply to drive the cassette deck, control circuitry and solenoids. The i.c. ULN2001, contains seven stages of Darlington transistors capable of sinking up to 500mA each. It is therefore capable of driving the solenoids, motor and relay directly. 'B' type c.mos devices are quite capable of delivering up to 10mA at a supply voltage of 12V.

To achieve a high switch-on voltage for the solenoids, 2200 μF capacitors are charged from a 20V supply through 220 ohm resistors. The supply side of the sole-

high voltage during the period of M2's 0.5 second delay. Thus no problems should occur when switching from one function to another when both use the same solenoid.

The motor of the cassette deck requires a stabilized voltage of 12V, which is supplied by the 1 amp regulator i.c., type 7812, fed from the 20V unregulated, d.c. supply. The c.mos logic circuitry is also supplied by this 12V source.


Flip-flops, B1 to B6, are all halves of dual, D-type flip-flop i.c., type 4013. Thus three such i.c.s are required. The three triple i.p. And gates are all contained in an i.c., type 4073. The four, 2 i.p. exclusive-Or gates are all contained in the 4070. Finally, the two, 2 i.p. Nand gates are the other half of a quad, 2 i.p. Nand gate i.c., type 4093, the first half being used by the delay circuit.

In the next part of the article, the f.s.k. modulator/demodulator, will be described.

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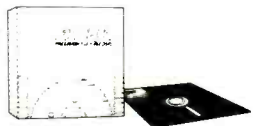
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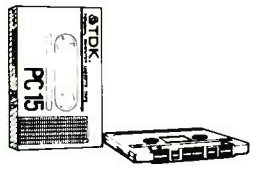
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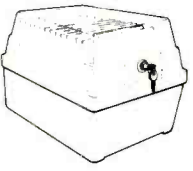
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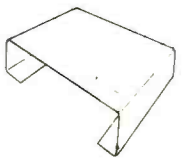
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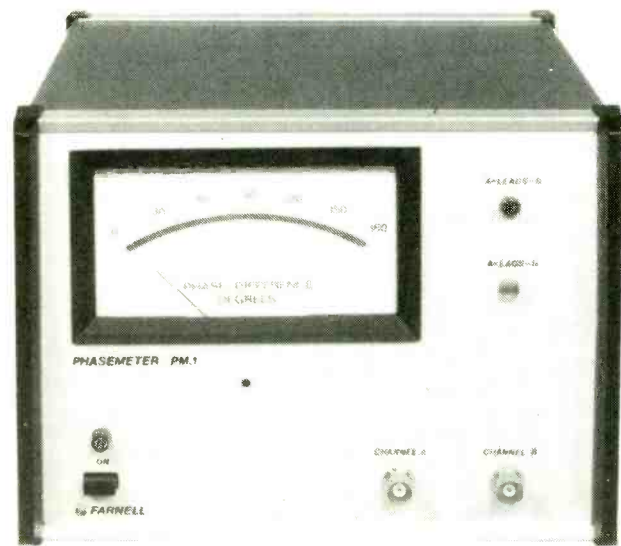
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CIRCLE 45 FOR FURTHER DETAILS.

Fibre optic communications

by Brett Wilson

Part 2 — optical sources, detectors and receivers

This second article looks at the different types of optical sources and detectors available and clarifies the best combinations for different types of system.

Optical sources for fibre transmission systems must be compatible with the fibre characteristics. They should be small, reliable, inexpensive and efficient in the conversion of electrical input power to optical power coupled into the fibre. In addition it must be possible to modulate them at high data rates, preferably directly. Two main candidates have emerged; light emitting diodes and injection laser diodes. Both devices operate in a forward-biased mode (low voltage, high current) and emit light as a result of hole-electron combination at the p-n junction. Direct modulation is possible for both l.e.d.s and i.l.d.s by varying the drive current, although there are certain complications for i.l.d.s at very high data rates.

The early infra-red gallium arsenide l.e.d.s operating at $0.9\mu\text{m}$ are no longer used since their emission is too near to an OH water absorption peak to result in reliable low-loss transmission. They have been replaced by aluminium-gallium arsenide types with an output wavelength of $0.85\mu\text{m}$. Because of the broad spectral width of l.e.d.s ($50\text{-}100\text{nm}$ being typical) and non-coherence they are best suited for applications in multi-mode fibre systems.

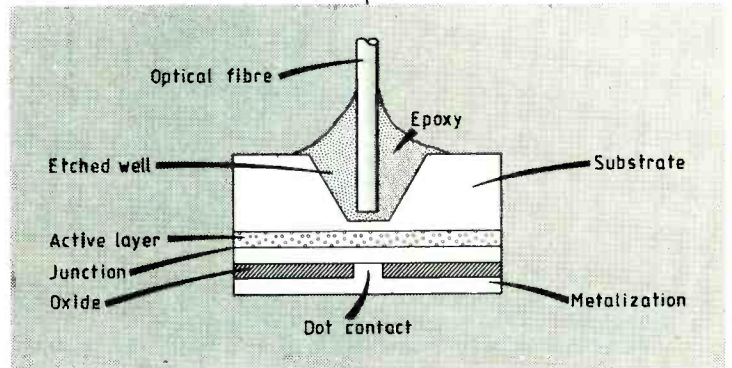
Longer wavelength operation at the $1.3\mu\text{m}$ dispersion minimum for optical fibres is made possible by InGaAsP heterostructure materials, allowing the use of l.e.d.s in up-graded communication links. However, they have only recently become commercially available at the longer wavelength, in contrast to the $0.85\mu\text{m}$ AlGaAs l.e.d.s that have been on the market for several years. The reliability of l.e.d.s is extremely good with mean lifetimes in excess of 10^9 hours being

predicted from accelerated ageing tests.

The Burrus-type geometry has been the basic design over several years for the surface-emitting l.e.d.s specifically intended for coupling to optical fibres, Fig. 1. It is characterized by small contact area and an etched well for butt coupling to a fibre end. It is important that the etched well in the Burrus-fabricated l.e.d. does not reach down to the thin active layer or surface contamination can drastically reduce the serviceable life of the device. A small emitting area is obtained by localizing the drive current by etching only a small contact on the underside of the device.

Depending on the core size and numerical aperture of the fibre used it is practical to launch optical powers of around 50 to $100\mu\text{W}$ into a fibre, although $25\mu\text{W}$ at an l.e.d. drive current of 100mA is more typical. Up to $300\mu\text{W}$ can be attained with specially optimized fibres. The Burrus l.e.d. can be supplied with the attached fibre pigtail ready terminated in an SMA-style connector or left bare where direct low-loss fusion splices are intended. A variation on the basic Burrus design is to locate a truncated glass microsphere lens in the etched well for increased optical coupling efficiency.

Mainly because of the lower current densities encountered, l.e.d.s are more reliable than injection laser diodes and do not need output stabilization since their output power varies little with temperature. Direct drive current modulation up to about 150MHz is obtainable, higher in specially optimized devices, but at the expense of available optical power¹. Linear intensity modulation can be used for l.e.d.s in an analogue system because their input/output characteristics is substantially linear up to about 80% of their maximum light output, Fig. 3(a).



A new edge-emitting type of l.e.d. can ultimately couple more power into a fibre by virtue of a narrower light confinement angle, leading to better coupling efficiencies. In addition, it exhibits a narrower spectral width than the surface-emitting type of l.e.d., resulting in a greater maximum bandwidth-distance product through the restrictions of fibre material wavelength dispersion (discussed in Part 1).

The injection laser diode (i.l.d.) also relies on heterojunctions to confine injected carriers to the diode active layer with the attendant refractive-index steps forming a waveguide to confine light to the same active region, Fig. 2. Partially reflecting surfaces at the light emission faces are formed by the refractive-index difference between diode material and air. There are several alternative ways of producing confinement in the lateral direction, the earliest of which was the oxide-defined stripe of Fig. 2. When the injected current

Fig.1. The most successful general-purpose l.e.d. for optical fibres is produced by permanently bonding a fibre 'pigtail' into the l.e.d. itself.

Fig.2 An injection laser diode must have some method of containing the light within a narrow portion of the active layer between the end mirrors.

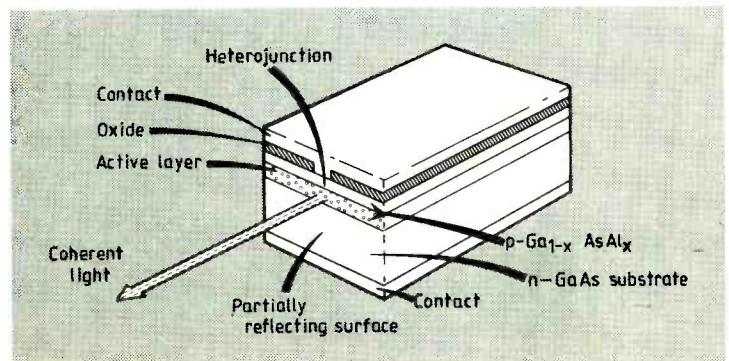


Fig. 3. Injection lasers can launch more power into a fibre than an l.e.d. but their non-linear behaviour requires more complex drive circuits.

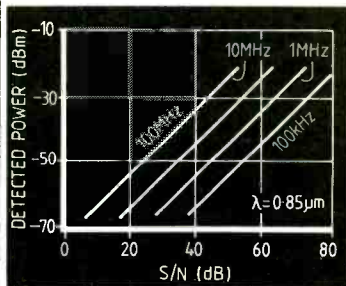
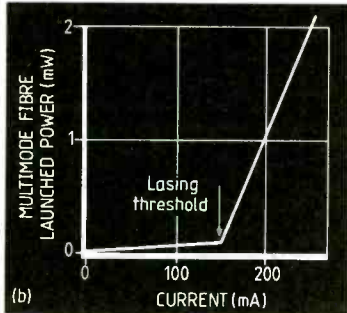
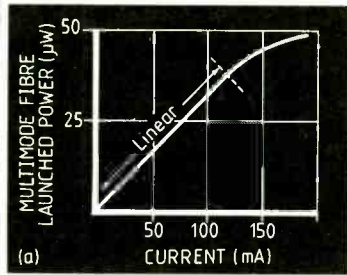


Fig. 4. For a given wavelength and data rate there is a linear relationship between received power and signal to noise ratio.

density is sufficiently high to cause the necessary population inversion, gain rather than loss occurs in the active layer and coherent oscillations are produced in one or more cavity modes.

Early i.l.d. lifetimes were very short, but have been improved to around 10^6 hours by paying close attention to processing and coating the mirror facets, along with the provision of adequate heat-sinking². Again AlGaAs formulations are used to produce continuous infra-red light at around $0.85\mu\text{m}$ but with a much narrower spectral width, typically 2nm. Unlike l.e.ds, laser diode

Fig. 5. A p-i-n diode photodetector operates by converting photons into electron-hole pairs in a region of low electric field gradient.

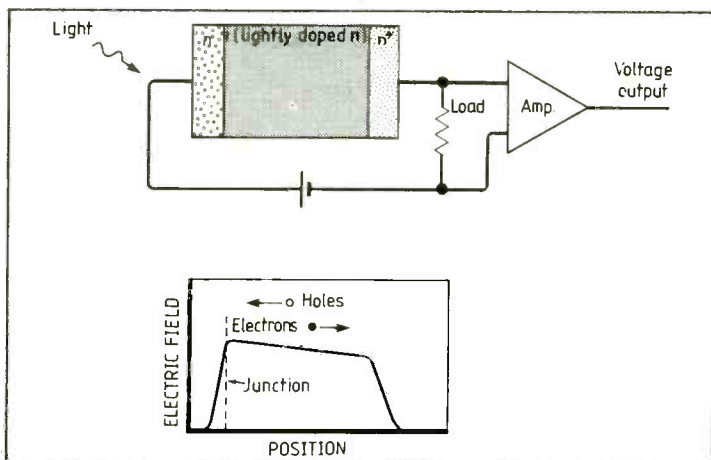


exhibit a threshold effect below which coherent light is not emitted. Injection lasers used with first-generation fibre optic systems usually exhibit a threshold around 150mA and are able to couple perhaps as much as 2mW of light into the fibre for an extra 100mA drive current, Fig. 3. The higher coupling efficiency is simply a result of the much narrower light confinement angle of the i.l.d. interfacing more effectively to the requirements of an optical fibre. For a similar drive power an i.l.d. can launch about 10 to 20dB more light power than an l.e.d. into a fibre.

The main research interest has now shifted to i.l.ds fabricated from InGaAsP that emit at longer wavelengths ($1.3\mu\text{m}$), where the dispersion minimum of fibres allows a very high potential bandwidth-distance product. Various configurations are currently being tried to obtain the lowest lasing threshold and highest optical powers. The stripe geometry and the newer buried heterostructure devices, both emitting at $1.3\mu\text{m}$, are commercially available and are currently used in the more demanding roles.

Multimode rather than monomode operation is most common for i.l.ds with useful output powers in the 2 to 10mW range. In fact, multimode lasers are preferred as sources for multimode fibres to reduce modal noise. Single-mode lasers are obviously required for ultra-high bit-rate systems using narrow monomode fibres. Unfortunately the lasing threshold of InGaAsP lasers is strongly temperature sensitive (much more so than the $0.85\mu\text{m}$ AlGaAs types) and, in common with most lasers, they tend to break into multimode operation when modulated rapidly. The effect is reduced by biasing the laser to just below its temperature-sensitive threshold, but at the expense of increased drive circuit complexity. Recently, stable single-mode operation in an InGaAsP laser has been demonstrated using a distributed feedback technique to enable modulation up to around 1GHz.

The decision to use an l.e.d. or an i.l.d. source will be made on grounds of intended repeater spacing, maximum modulation rate and system cost and reliability. Light emitting diodes are used almost exclusively in short-haul low-to-medium data rate systems, with i.l.ds being chosen

for the long-haul high data-rate links. Single-mode i.l.ds would be used for the most demanding monomode fibre applications. There is however an overlapping range of distances and modulation rates in the middle ground where $1.3\mu\text{m}$ l.e.ds and i.l.ds compete, and the final choice in this area is often determined by reliability and commercial factors.

Optical detectors

An optical detector is essentially a photon to electron converter. The conversion is a statistical process and even with a noiseless amplifier connected to the detector there is a theoretical lower limit on detection sensitivity for specified error rates.

The consequence of this fundamental statistical sensitivity can be seen at work when considering detection of digital information with specified error rates. Information is transmitted in the form of 'marks' and 'spaces' and reaches the detector as pulses of energy E or 0. If no electrons are emitted from the photon detector in the appropriate time slot the assumption is that a space was received. Even if only one electron is emitted it must be assumed that a mark was intended since our idealized detector produces no electrons in the absence of an optical input pulse. However, even in the presence of a pulse of energy E it is still possible for the detector to emit no electrons at all and hence make an error by misdetecting a mark as a space. From the Poisson distribution that governs the behaviour of the detector it can be shown⁴ that even a perfect photodetector must sense at least 21 photons for there to be a 10^{-9} probability of misinterpretation. (10^{-9} is a common value for an acceptable bit-error rate in digital communication systems.) This lower limit on the sensitivity of a binary digital receiver is usually referred to as the quantum limit and is a convenient measure against which real digital detectors can be judged.

There is also a quantum limit for analogue systems, this time relating detector sensitivity to output signal to noise ratio, even assuming noiseless electronics. It turns out that the minimum detected optical pulse power is given by twice the product of the signal to noise ratio, the bandwidth and the photon energy. Fig.

4 illustrates this relationship for different bandwidths at the optical wavelength of $0.85\mu\text{m}$. This again is the quantum limit and real detectors, and receivers fall short of this limit.

The p-i-n diode, Fig. 5, is the simplest optical detector suitable for fibre optic systems. It is composed of an n^+ substrate, a lightly doped intrinsic n-region i, and a thin p-zone. Operated with a reverse bias, mobile carriers to leave the p-n junction producing a zone of moderate electric field on both sides of the junction into the i-region. Because it is only lightly doped this field extends deeply. Incident light power is mainly absorbed in the i-region (the p-region is extremely thin), causing electron-hole pairs to be generated. These carriers are separated by the influence of the electric field in the i-region and represent a reverse diode current that can be amplified.

For detectors operating at wavelengths shorter than $1\mu\text{m}$ the p-i-n diode material is silicon but at longer wavelengths, the popular $1.3\mu\text{m}$ window for example, other materials must be used because the quantum efficiency of silicon drops rapidly at around $1\mu\text{m}$: it becomes transparent and fails to convert photons to electrons. Germanium is often used beyond $1\mu\text{m}$, with complex materials such as InGaAs becoming increasingly popular. Unfortunately there is presently a penalty to be paid in the size of the residual dark current ($<n\text{A}$ for Si, maybe $5n\text{A}$ for InGaAs) currently setting a higher practical limit on the minimum incident optical power which the longer wavelength devices can be used to detect.

The second popular type of photodetector, the avalanche photodetector (a.p.d.) shown in Fig. 6, has the advantage of internally multiplying the primary detected photocurrent by an avalanche process, thus increasing the signal detection sensitivity. However, because the avalanche multiplication is statistical in nature some excess noise is generated.

The fabrication of an a.p.d., Fig. 6, is very similar to the p-i-n diode just discussed except that the high electric field region in the p-type zone produces the desired avalanche process to amplify the primary signal current. The signal multiplication of the a.p.d. depends on the applied reverse bias voltage and the temperature.

In contrast to p-i-n diodes where reverse bias voltages of around 10-20V are typical, an a.p.d. may require up to several hundred volts to produce an avalanche gain of 100. High performance systems normally require that the gain of the a.p.d. is temperature stabilized and will probably include a measure of automatic gain control operating via the reverse bias voltage.

The frequency response of p-i-n and a.p.d.s is similar, with transition times across the lightly doped intrinsic region less than 1ns, making them both usable up to around 1GHz. The main advantage of a.p.d.s over p-i-n diodes is simply greater gain-bandwidth product due to the inbuilt gain, permitting lower detected optical powers for the same error rate or signal-to-noise ratio.

Again silicon is the usual material for short wavelengths ($<1\mu\text{m}$), with Ge, InGaAsP and AlGaAsP becoming popular at the longer wavelengths around $1.3\mu\text{m}$. Ultimately germanium will be superseded by the newer materials due to its poorer dark current ($\approx 500n\text{A}$) and high excess noise.

Practical optical receivers

Because of the very small output signal available from a photodetector noise in the preamplifier input stage is a serious problem. For a real receiver this results in the required number of detected photons per data bit being much higher than the quantum limit of 21 photons for a 10^{-9} error rate. Typical figures at $1.3\mu\text{m}$ are around 400 photons per bit with an a.p.d. and 1000 photons per bit with a p-i-n diode when both are used with optimized receiver preamplifiers at 100Mbit per second. That this ratio is not as large as might be expected, considering the inbuilt gain of the a.p.d., is mainly due to the higher dark current and the fact that the avalanche process itself contributes a certain amount of excess noise.

The most popular form of optical receiver front end is the simple trans-impedance amplifier configuration, Fig. 7(a), where the output voltage is given by the product of the input (photodetector) current and the feedback impedance. This approach to front-end design has supplanted the earlier high impedance integrating amplifier, (b), that suffered from problems of complex equalization

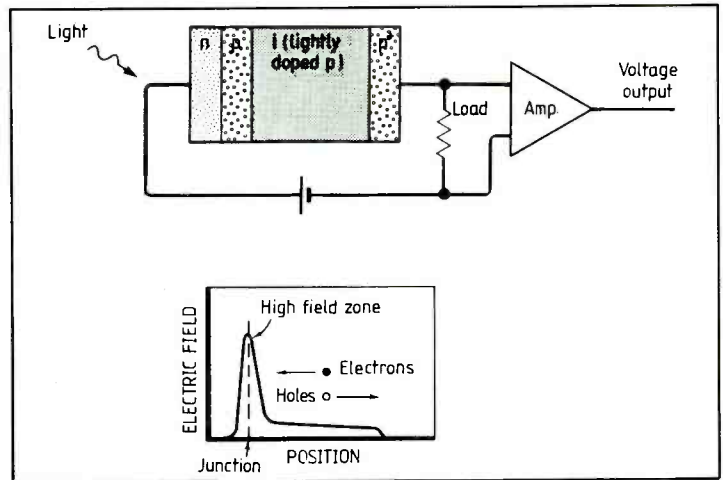


Fig. 6. High field gradient in an avalanche photodiode causes the photo-electrons to multiply by an avalanche process.

to retrieve the pulse shape. But careful choice of values of feedback resistance for the transimpedance amplifier is still because of relative noise contributions and restricted phase margins arising from stray capacitance in the feedback loop. In general, an upper limit of around $5M\Omega$ at low data rates ($<1\text{Mbit/s}$) decreasing to perhaps $10k\Omega$ at 500Mbit/s is commonly encountered. Lower values also help to maintain receiver dynamic range. Calculations for optimum receiver sensitivity usually point to the importance of a restricted bandwidth to reduce various noise contributions, often resulting in the upper -3dB point being significantly less than the data rate used⁵.

The transistor used as the first active device in the preamplifier obviously plays a major part in the performance of the receiver. It is here that rapid developments are occurring and most performance figures are soon improved on.

Gallium arsenide m.o.s. fets and silicon bipolar microwave transistors have probably been the most effective combination with the p-i-n photodiodes, although the silicon short-channel m.o.s. fet is showing promise. At lower data rates ($<10\text{Mbit/s}$) a silicon junction f.e.t. has a superior performance because it does not suffer from the $1/f$ noise associated with GaAs and Si f.e.t.s. Silicon

Fig. 7. Transimpedance amplifier is replacing the high impedance integrating amplifier as the preferred optical receiver preamp configuration.

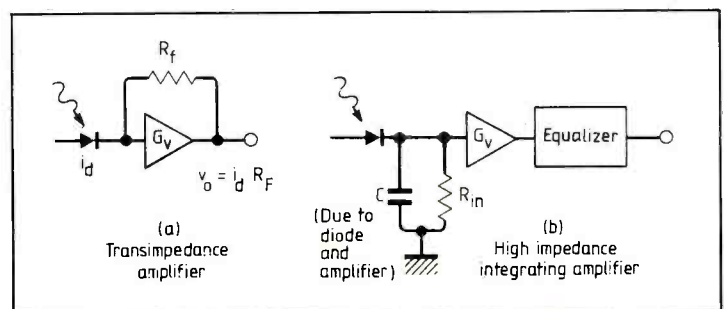
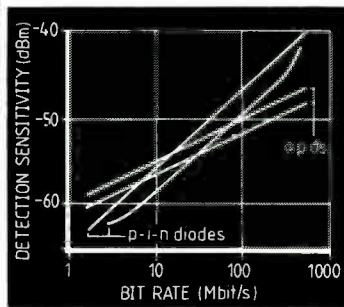


Fig. 8. Choice between a p-i-n and a.p.d. detector for optimum receiver sensitivity depends on data rate.



devices possess the advantage over GaAs ones in that they can be integrated into a preamplifier chip with present silicon technology.

Performance zones of 1.3 μ m receivers based around p-i-n diodes and a.p.d.s, followed by the best choice of the devices discussed above, are shown in Fig. 8. Even taking into account their higher dark current and excess noise a.p.d.s will provide around 5dB higher sensitivity than the InGaAs p-i-n diode for data rates beyond about 100Mbit/s. At lower data rates p-i-n diodes display better sensitivities of their lower dark current.

At the longer wavelengths where experience of the technology is still limited no clear optimum choice has emerged that can satisfy all of the requirements for inexpensive fast and sensitive optical receivers.

Recent research⁶ has been stimulated in the area of coherent transmission and detection because of the promise of detection sensitivities approaching the quantum limit without using a high performance a.p.d. receiver. For these techniques of phase shift keying and frequency shift keying stabilized monochromatic sources with a high spectral purity are needed as transmitters and receiver local oscillators, ruling out the use of l.e.d.s. To achieve the best performance the carrier source and the local oscillator laser must operate in a single mode with their frequencies maintained to within a small fraction of the data rate. The behaviour of lasers under direct frequency modulation is complicated and investigations are still in their early stages for application of coherent transmission to fibre optic systems.

To be continued

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Developments in cellular radio

Cellular radio-telephone systems are now in service or are being installed in many countries, Britain included: Richard Lambley reports on the current scene with particular reference to Europe

Cellular radio systems have their roots in the late 1960s when proposals for such a service were made in the US by Bell Laboratories and others. Two systems were subsequently licensed by the FCC to undergo field trials: the Advanced Mobile Telephone System (AMPS) in Chicago and the American Radio Telephone Service (ARTS) in Washington DC.

Installed by Motorola using Dynatrac equipment, ARTS currently serves an area some 80 miles long extending from the Northern Virginia suburbs of Washington to the city of Baltimore in Maryland. Initially the area was divided into eight cells with between three and 16 channels allocated to each one. The base stations, with an e.r.p. of 100 watts covered a radius of about 11 miles with large overlaps. In the final designs for the Washington area, aerial height was reduced from 150 to 60-70 metres above sea-level to reduce interference. Landlines have been used to link the base stations, but microwave links are to replace them.

Unlike the Chicago system, ARTS was designed to serve portable units as well as car telephones, and special attention was given to the problem of providing good performance inside buildings. A form of diversity reception was adopted with six-sector base station receivers and 17dB-gain aerials: the two best aerials are combined in the i.f. section to reduce fading and multipath distortion.

Another problem occurred at first during hand-off between adjacent cells, when fluttering signal strengths were liable to cause repeated switching back and forth. To help counteract such disturbances the control computer now waits 15 seconds before handing back.

Despite a few difficulties with adjacent channel selectivity,

ARTS has worked well. According to Andrew Lamothe, former technical director of Cellular Radio Corporation, customers make more calls than other radio telephone users and talk for longer: 260 to 280 minutes per month as against 60 or 70. This he attributes to the greater clarity and reliability of the cellular service. Subscribers are willing to use it for important business calls, including long-distance and international calls, as well as just for ringing in to their offices.

ARTS was awarded a full operating licence in December 1983. It now has over 1000 subscribers, new ones being added at a rate of 30 a day in spite of heavy call charges and the high cost of the equipment. Mr Lamothe quotes prices in the region of \$2400-\$2700 plus taxes, aerials and installation.

By the end of 1984, cellular radio networks are expected to be in service in 24 US cities, some of which will have more than one system. Specifications of the subscriber's equipment for ARTS and AMPS have been standardized by the FCC so that the same telephones should be usable on any network in the US.

Canada

Canada's Department of Communications policy is to encourage growth of the service on a competitive basis with a minimum of regulation. Two contrasting cellular radio systems have been licensed, and the first to enter service is Aurora, an automatic roaming radio system from Novatel Communications Ltd.

Instead of the large central switching centres favoured by other systems for linking cell-sites to the public telephone network, Aurora is based on distributed switching nodes with interconnections at local telephone exchanges. This avoids the expense of installing dedicated

trunk cables and greatly reduces starting up cost. Aurora is therefore suited to serving rural areas as well as big cities. Aurora has a central control point (the master mobile centre), but it has no real-time control over the operation of the network: its functions are connected mainly with administration and maintenance.

Source: 'International Developments in Cellular Radio', a seminar sponsored by the Mobile Radio Users' Association (London, February 1984).

What is cellular radio?

Cellular radio provides a way of satisfying the large demand for mobile communications by extending the public automatic telephone network to users on the move.

To achieve this goal with conventional mobile radio technology would mean an unacceptably large bandwidth requirement. A base-station serving mobile users in a city of moderate size might have to handle thousands of calls at once during busy times. Further, the number of radio channels available would have to be twice the number of telephone calls in progress, as telephone users expect full duplex communication — push-to-talk operation would not be acceptable in a public service.

By dividing the territory to be covered by the radio system into smaller units or cells, each one served by its own low-power base station, a cellular network can handle the same traffic with far fewer radio channels. The frequencies used in each cell can be re-used in other cells at a distance. In effect, a cellular system has solved the problem of frequency availability by trading it for a high degree of complexity in its network of base stations and switching centres. A large demand for channels in any particular area — a city-centre, for example — can be satisfied by dividing it into sub-cells (cell-splitting) and serving each sub-cell from a base station of even lower power.

However, in practice there is a lower limit to cell size and thus to the traffic capacity of the system. Although a cell could be set up to cover an area as small as, say, an

hotel or even an airport departure lounge, there would be a risk that a well-sited caller within that building might unwittingly access distant base stations as well as the local one.

To be attractive to the potential subscriber, a cellular radio telephone must feel just like an ordinary wired telephone. The user, whether in a car or on foot, must be able to dial outgoing calls direct and to receive incoming dialled calls too. Most cellular systems offer the full range of services available on the public network and often more.

As neither party to a call can be expected to know precisely where the mobile user is, the call must be routed through the appropriate base station automatically. Moreover, the mobile user is liable to wander out of one cell and into another as the call progresses. To cope with this, the system must re-route the call through the new base station, switching the call to new radio channels without interrupting it. This procedure, known in the jargon as 'hand-off', is one of the distinguishing features of cellular systems.

The cellular radio systems now in service are expensive to the user both in call charges and in the price of the mobile equipment. The cost of establishing a network is heavy, and it may seem unlikely that cellular radio will replace the ordinary wired telephone, at least in urban areas. But to business users who can justify it, cellular radio offers some attractive prospects: the 'carry anywhere' pocket telephone, for example.

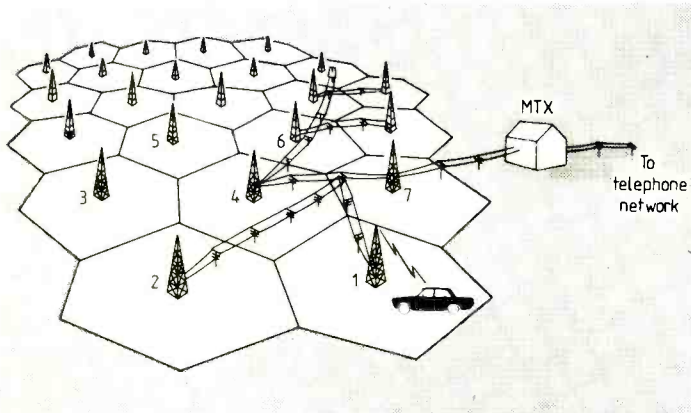


Fig. 1. Typical layout of a cellular radio network. A minimum of seven frequency groups is required, but the same frequencies can be re-used in other cell clusters.

The system began field trials in Alberta in 1981 and entered commercial service in mid-1983. By the end of the year it is expected to cover three quarters of the province using 123 cell sites. The frequencies used are in the 400MHz region.

Canada's other cellular system, now being installed in Montreal and Toronto, will be ready for business in September. This 800MHz system has a centralized architecture, with a 'mobile telephone exchange' acting as a control and switching node to connect mobile subscribers to the public switched telephone network.

Problems have been encountered with wired links in the system: among them echo, noise and signal loss. According to Bell Canada, echo-cancellation equipment is now included to improve transmission performance with the aim of providing a sound quality not worse than on the ordinary telephone network.

The service is designed to emulate the public facilities such as call forwarding and conference calls. Services are available to roaming subscribers as well.

United Kingdom

The system adopted for use in Britain, TACS, is modelled on the Chicago AMPS. Two companies have been licensed to provide a service: Racal Millicom and Telecom-Securior Cellular Radio. As it stands, AMPS is unsuitable for direct application in Britain because of differing frequency

allocations and channel spacings in the two sides of the Atlantic. In addition, there is a need for a nationwide roaming capacity, a facility not required in the US. The British network also has to allow for inter-systems roaming, so that a Telecom-Securior subscriber can wander into Racal's areas and vice versa.

TACS (it stands for 'total access communications system') is due to begin operations in 1985. It will use the band 890-960MHz (there is a gap in the middle for c.b.) with a channel spacing of 25kHz: this implies tighter filtering and narrower frequency deviation than in the American 30kHz systems. John Carrington, chief executive of Telecom-Securior Cellular Radio Ltd expects an initial demand for between 10 000 and 25 000 mobile sets when the trial service begins later this year, using equipment already ordered. These would be available through independent retailers who would 'front' the system on behalf of TSCR. Cellular radio, he says, would not be suitable for private mobile radio users such as taxi fleets, who already had an effective system, though it would have to compete with p.m.r. on price.

West Germany

A more technically complex cellular system is the C-900 system of Siemens. A C-system is already in operation in Germany on 450MHz and will enter full public service in October. The network of 35 base stations is to be expanded rapidly to 95, covering about 70% of the Federal Republic. The system should have a capacity of over 100 000 subscribers: but the 900MHz version now being planned is expected to be able to handle more than two million. The system has many advanced features designed to secure efficiency of spectrum use, freedom from interference and privacy.

A critical problem in mobile radio is in defining cell boundaries. The limits marked by field-strength distribution and signal quality are not always ideal from the point of view of traffic management. To get round this, the C-system can adjust cell boundaries dynamically, spreading the traffic load over adjacent cells. In this mode, adjoining base stations compare the signals from each mobile and so measure its position. Having done this they can force hand-off from one cell to another on the criterion of distance alone, even though signal quality is still perfectly satisfactory.

Another special feature of the C-system is mutual power control of both the mobile and the base

station. When the two are close together, power is reduced to minimize interference elsewhere. The system also offers intra-cell hand-off; calls may be switched automatically to alternative frequencies if co-channel interference occurs.

Signalling in the C-system is more complicated than in other cellular systems. Each base station identifies all the mobiles within its area by interrogating them automatically over a data channel. The network then knows whether an individual subscriber is available and where he is to be found. When the mobile subscriber is called, or when he initiates a call, a suitable pair of speech channels is allocated by the computer and the connection made. This procedure avoids ineffective use of radio channels by assigning them only when both parties are ready to speak: according to Siemens it saves about 30% of channel capacity.

To make features such as intra-cell hand-off possible, data communications are maintained even during the call. The speech is time compressed, each 12.5ms segment being squeezed into 10ms to make room for a 5.28kbit/s f.s.k. data burst.

A dynamic four-band scrambling procedure is applied to the speech signals, with 256 possible key combinations. The correct key is selected automatically when the call is set up and different keys are used for subsequent calls.

System architecture is decentralized, and the modular switching equipment can be expanded to match traffic requirements. C-900 is due to be introduced in Germany in 1987.

Scandinavia

If you disregard a small system installed by Cable and Wireless in Qatar in 1978, the cellular network longest established in public service is the Nordic Mobile Telephone System (NMT). Opened in Sweden in 1981 this 450MHz network now covers large parts of Sweden, Norway, Finland and Denmark, and in January this year was serving over 75 000 subscribers. The system is also in operation in Spain, Tunisia and Saudi Arabia, and has lately been selected by the Netherlands, Austria and Ireland.

Each cluster of base stations is linked to a 'mobile telephone exchange' (MTX), a standard AXE-10 digital exchange, which provides interfacing with the public switched telephone network. One channel at each base station is designated a calling channel; and when someone dials the number of mobile sub-

Some cellular radio systems compared

	TACS (UK)	FCC (USA)	NMT	NTT (Japan)	C-system
Frequency (MHz)	860-960	825-890	450-470 (860-960)	900	450 (900)
Channel spacing (kHz)	25	30	25	25	
Duplex spacing (MHz)	45	45	10 (45)	55	
Signalling (kbit/s)	8	10	1.2	0.3	5.28
Signalling channel	separate	separate	combined	separate	both
Scrambling	no	no	no	no	yes

(Main source: Ericsson)

scriber, a calling signal is broadcast over all the calling channels in the traffic area. When the mobile detects this call, it returns an acknowledgement on the same frequency. Speech channels are then assigned by the MTX.

When the mobile subscriber initiates a call, the equipment hunts for a clear traffic channel on which to call the base station. On receiving the signal the MTX checks the number dialed and the category of the subscriber and sets up the call.

Transmission quality of every call is monitored by means of a 4kHz pilot tone which is added to the speech channel by the base station and looped back by the mobile. If reception deteriorates the mobile transmits a hand-off request to the MTX, which then attempts to find a more suitable routing for the call. Adjacent base stations make field-strength measurements on the traffic channel, and if one of them is able to offer better transmission quality, and has a free channel available, the call is switched over.

Each mobile is registered on one particular MTX, the 'home exchange'. If it moves into the area of another MTX, any calls are automatically re-routed. The system permits subscribers to roam without restriction throughout the four Nordic countries, though at the behest of the PTT authorities 'country' switches are fitted to the mobile sets.

A practical problem with any cellular radio system is the question of call charges. A subscriber dialling a mobile user has no way of knowing in advance whether the recipient of the call is in the next street or in another country. The Scandinavian countries have taken what seems a reasonable line by charging a flat rate corresponding to an ordinary medium-distance call.

NMT's 180-channel allocation was thought very generous at the time the network was being planned, according to Christina Callmer of Ericsson Radio Systems. However, fully capacity is likely to be reached much sooner than had been expected and plans for a 900 MHz version were now being finalized.

France

The move towards cellular radio has taken France in a rather different direction, Matra Radiocommunications is now installing a national radiotelephone network which combines a public telephone service with private business communications.

The RTA system is founded upon cellular principles, but seems to place more restrictions on the user than other systems. Subscribers can access only the

repeater stations with which they are registered. There is a three-tier service: access to one station only, up to ten stations (which need not be adjacent) or, for certain users, nationwide coverage.

RTA offers business users the option of a private communication system using push-to-talk simplex operation; this is available as well as or instead of the ordinary car telephone service. These closed user groups use the same technical facilities as the public service.

As with some other cellular systems. RTA can give certain users priority when there is a queue of cells waiting to be set up. At busy times repeater stations may invoke an automatic time limit facility which informs users that the call may be cut short: the limit is programmable between 30 seconds and 16 minutes.

Frequencies assigned to the RTA network are 173-223 MHz and 406-430MHz, with 12.5kHz channel spacing. Repeater stations have a transmitter power of 50W and cover a radius of 20-30km. Connections between them are via the existing public switched telephone network; and this, according to Michel Canitrot of Matra, has helped to make RTA significantly cheaper to set up than other cellular systems. The network is modular in form, with no centralized control.

The user's view

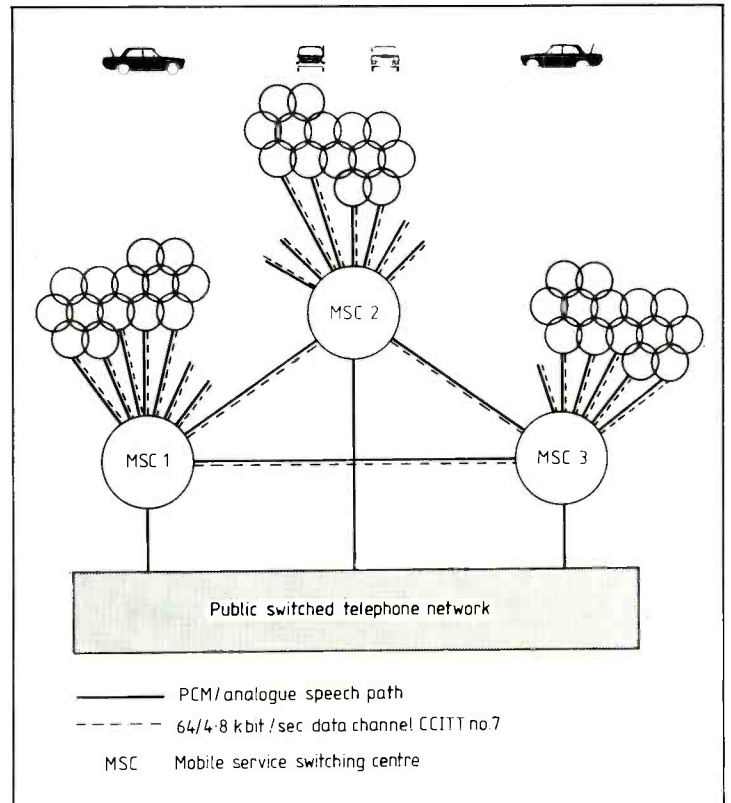
In Britain, the Mobile Radio Users' Association has encouraged the development of the new services and technology, particularly cellular radio for its effective use of frequencies. Nevertheless, according to Walter Stevenson of the MRUA, there is still a requirement for conventional mobile radio and paging systems, at least in the short term. Most vehicles operate within a limited area and are unlikely to need a nationwide roaming facility.

But Mr Stevenson is nervous that the Government is trying to force cellular radio as the sole solution to the mobile user's problems. Additional frequencies are urgently needed as well.

The future

The next two or three years will see the introduction of a patchwork of mutually incompatible cellular systems all over Western Europe; only Italy, Portugal and Switzerland have not yet made a choice. Some countries will have more than one system.

However, one market analyst, Malcolm Ross of Arthur D. Little International, thinks that there is no need for a European standard in the short term since the market



for mobile radio on a national basis is so big that it should be dealt with first. Quoting statistics to the effect that only 25% of telephone calls to offices reach the right person, Mr Ross predicts a big demand for pocket telephones for businessmen. And he suggests that before the end of the decade a mobile telephone may become cheaper than a wired line, costing perhaps as little as \$120 for a consumer model.

Nevertheless, steps are being taken to overcome the present lack of standardization. A working party under the CEPT is discussing the possibility of a pan-European mobile telephone system, and it is probable that this will be a 900MHz cellular system. The total bandwidth for cellular radio in Europe will eventually be 50MHz and of this only 15MHz has so far been released in Britain.

Fig. 2. The German C system has separate data links for setting up speech channels at the start of each cell. As the call proceeds it is controlled and monitored by another data signal multiplexed with the speech.

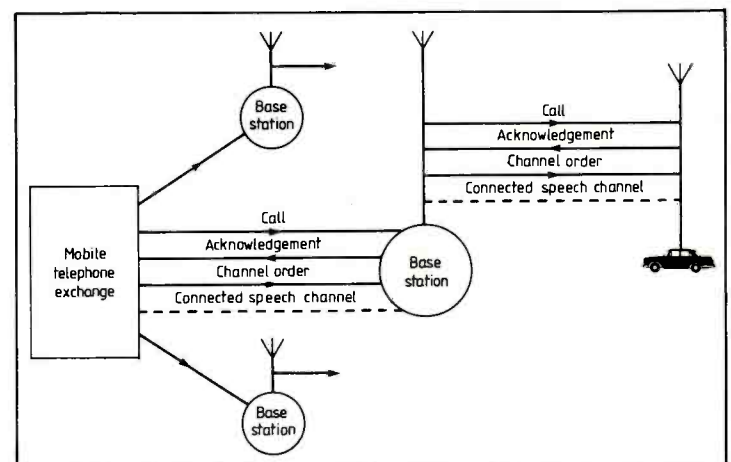


Fig. 3. Call set-up procedure with the Scandinavian NMT system. Signalling takes place on a calling channel and a speech channel is then allocated by mobile telephone exchange.

by A. E. Cawkell

The information society

2—Politics of telecommunications

The growth of infrastructure services and the influence of politics on British Telecom and its operations.



Political, technical, and economic factors impede the formation of a unified network in the foreseeable future.

Private industry is unlikely to introduce networks or services unless it considers that the market will return an adequate short or medium term profit. For PTT monopolies this aspect is less important, consequently marketing skills are also of less importance to them.

The PTTs possessed the cables, and with EEC backing, added the facilities to provide the Euronet network. Upon it ride the host computers, mainly privately owned, which provide services for a fee. Consequently the desirable objectives of providing scientific information services, and encouraging the generation of European-compiled databases has been achieved.

However the absence of a market-driven approach can be disadvantageous. The Prestel service would have been long since shut down had it been a commercial system.

In the United States, a range of new services is gradually appearing in consequence of market forces. The country also possesses a strong electronics industry, a propensity to innovate, and a large number of people with some disposable income. I was able to observe the market-driven entrepreneurial approach at work during a visit in 1981.

Communication networks for home computers were being operated by two companies, The Source and Compuserve. Compuserve's Micronet was gatewayed to Tymnet. Charges were \$5 per hour plus \$2 for Tymnet. The

Source and Compuserve then had about 8000 subscribers, mainly with TRS80s or Apple 2s. Compuserve offered Micronet terminal programs for both machines and a videotex program for TRS80s.

The Source and Compuserve are also information providers. Compuserve provided a range of services included with its \$5/hour fee — for instance an electronic mail service for all listed users — but charged extra for special services like access to 32 000 continuously updated stocks in its Microquote service. A set of detailed information about a stock cost 5 cents.

Perceiving that it might have a customer base, a bank in Knoxville concluded an agreement with Compuserve and Radio Shack who supplied TRS80 microcomputers, and offered banking services for viewing statements, paying bills etc., by the page (videotex) at \$5 per hour. Users also required the TRS80's videotex program. The service included the provision of a special modem for use with a TRS80 into which a magnetic card carrying an encryption key had to be inserted. At that time about 300 people used this service.

It was not clear whether prices for domestic users had dropped to a level which made success probable. The fact is that a structure has been gradually assembled in which operational costs were shared by many. Consequently an information provider or customer could join at a low incremental cost. There was no public financial burden. The foundation of the undertaking was the existence of a corps of people with a common

self-interest — they were computer buffs. However there is no reason why business and professional users could not use the common resource and some did.

This kind of approach seems to be prospering according to a September 1983 article²⁴. The Source, now owned by Reader's Digest, has expanded greatly and Compuserve, a subsidiary of H & R Block, has over 20,000 subscribers.

The politics of telecommunications

The fusion, usefulness, modification, or convergence of the networks shown in Fig. 1 will obviously be affected by control, administration, and investment. The best way of administering the UK telephone system, currently being modified into a digital telephone/data system, is controversial. The consensus of opinion was, and still is, in countries where information technology is less advanced, that a regulated monopoly is the best way to run a national telephone system.

The classic case for monopolies is set out in references 25 and 26. A 'natural monopoly' is a service or industry in which it assumed that economies of scale make it cheaper for one organization to produce a product or provide a service than for two or more to do so. Regulations can be imposed by the government to set prices which are in line with costs. The result, says the conventional wisdom, is a service provided at relatively low cost, obtained by regulating the prices charged by a single organization

which is able to operate at the scale needed to achieve maximum economies.

'Cream-skimming' is one of the major factors used in pro-monopoly arguments. Competitors could provide new profitable business services, eroding the incumbent's (British Telecom in the UK) revenues needed to fulfil its social obligation to provide loss-making rural telephone services.

In the 1960s the US telephone network started to be pressed into service for data transmission, since it was the only ubiquitous network available. It became very difficult to determine where telecommunications ended and information processing began. New requirements prompted the following questions: would consumer's needs be best fulfilled by entrusting all services to the traditional carriers? was it rational to extend the monopolistic structure to control the closely associated technology and processing involving modems, terminals, private line and microwave facilities, special data services, communication satellites, etc.?²⁷

The British Post Office depreciates plant and equipment over 25 years. The organization's finances and price structures are arranged accordingly. But in the computer/data processing industry, obsolescence proceeds on five-year or less cycle, not because equipment has by then come to the end of its useful life, but because it is replaced by something better and cheaper.

The wind of change which first blew in the United States was not generated so much because the regulated monopoly for the telephone network was found wanting, although it had its critics, but because the telephone system, once a definable entity, was becoming the major component in a total information system.

One of British Telecom's (then the Post Office) strategy directors said²⁸ back in 1977 "The absence of competition removes information about markets which could otherwise be inferred from competitors. Changeable government policies influence the amount of investment, borrowing, and the levels of tariffs. The UK Post Office...lays down procedures for its 237 000 staff, whose working lives are spent usually in a single organization, in 112 000 separate instructions varying from 1 to 100 pages in length. Size, complexity, plant life of 40 years etc., all militate against rapid change".

Egalitarianism requires the generation of wealth to support it. Wealth-generating companies have to compete internationally, and for them a poor telecomms system is an expensive overhead.

"The competitiveness of UK industry depends in part on the efficiency and related costs of the telecommunications services, especially compared with the USA and Japan. The UK and European computer, telecommunications and electronics industries need to expand at a rate at least commensurate with world demand so as to provide substitute jobs for those being abolished in declining industries"²⁹.

In a recent press release, BT claimed "Major achievements including...a reduction in the line waiting list from 122 000 to 20 000...a net growth of 5.6% despite the long recession radiopaging...new electronic mail system...lowest failed calls on record - local 1.3%, trunk 2.7%...longest fibre-optic cable in the world...etc., etc."³⁰.

One critic disagrees, using the standard anti-monopoly argument; "I love to see people making profits but monopoly profits are something else. A monopoly profit is the difference between how much they can get away with charging and how much they can get away with wasting. If you can't take your business elsewhere then there is no market, no competition, no price mechanism"³¹.

Various criticisms have been levelled at BT. Its charges for telephone services have consistently been near the top of inter-country comparison tables^{32,33,34}. Its differential pricing policy has been questioned; according to reference³⁵, the cost of a PABX per extension in London was £650, but £198 in Dublin for a similar PABX. It was suggested that this was because BT's specifications for home suppliers are unnecessarily tight.

In the same article some calculations were made showing that a London-New York private satellite link, if it was allowed, would cost £53 000 a year, compared with the BT tariff of £565 000 for a similar link. The BT price for a single-circuit leased link between London and New York was £49 900 a year, while a coast-to-coast link of about the same length in the USA cost £4500 a year. In a recent letter to the Financial Times, a reader complained that increases of 17% and 7% announced by BT in the last two years were misleading. Charges in the writer's company increased from £80 000 in 1980 to £150 000 in 1982.³⁶

Government policies for the Post Office 'protect inefficiency, remove incentives to self-improvement, penalise consumers and lower the gross national product' according to a well known authority writing in 1975³⁷. BT added a high surcharge to certain services provided via Tymnet, an

efficient US network with a London node (access point). Tymnet would not agree to it, so users had to dial the Tymnet node in Paris at a cost almost as great.

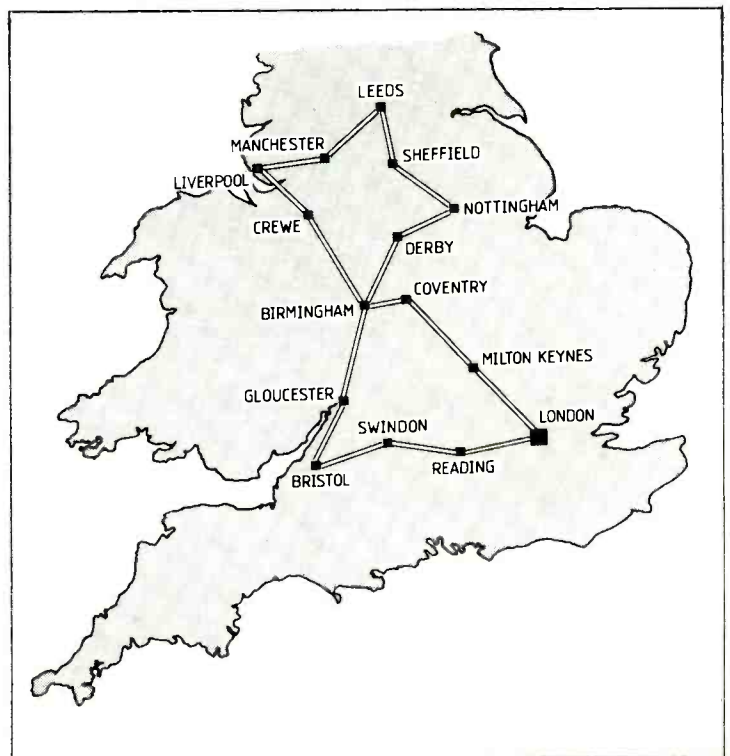
A better way of doing it?

A Conservative government was returned to power in May 1979, having released a document proposing policies for information technology in the previous month. It presented the British Telecommunications Bill in November 1980, proposing to split Postal and Telecommunications services as recommended in the earlier Carter report³⁸ and to allow competition controlled by the Department of Trade and Industry (DTI). Connection to the BT network would be allowed by others who could set up their own networks or services.

BT would retain its monopoly over the Public Switched Telephone Network (PSTN). The government would dispose of its shares in Cable and Wireless.

In the Beesley report of April 1981³⁹ it was said that the consumer benefits of allowing competition would outweigh any BT loss of revenue. BT should be free to set prices and compete for non-voice services, subject to DTI regulation. It seemed likely that cream skimming and leased line price increases would follow. The bill became the British Telecommunications Act on October 1st 1981. The Labour opposition stated that it would re-possess BT assets without compensation if returned to power.

Fig. 1. Project Mercury's proposed trunk network, which is intended to employ optical fibres, microwave and cellular radio and satellite communications.



Mercury

In June 1981, a consortium set up by Barclays Bank, Cable and Wireless and British Petroleum sought permission to set up a communications network to be called Mercury, in the first instance to link up a limited number of UK cities. High capacity optical-fibre cables would be laid alongside British Rail lines, and the system would include microwave and cellular radio communications with satellite extensions to other parts of the country. The government granted a 25 year licence to Mercury in February 1982.

Mercury started preliminary operation in the City of London during April 1983 with a point to point microwave service. Its proposed network is shown in Fig. 2. Later, Mercury announced that it would establish a transatlantic link via a spur from its network to an earth station in the London docks and an Intelsat satellite⁴⁰.



The 1982 Bill

A new Telecommunications Bill was introduced in October 1982. Its main purpose is to sell 51% of British Telecom — in other words to 'privatise' it. The government also proposed to set up an Office of Telecommunications (OFTEL) early in 1984, and to grant an operating license to BT as its first act. The Bill was lost in the general election of June 1983, re-introduced when the Conservatives were returned to power, and received its second reading in July in 1983.

Also in 1983, Professor Littlechild, an advocate of free markets, reported as requested to the DTI⁴¹. In responding to terms of reference including 'regulation with a light rein' he said that new competitors should be encouraged, and that for five years after privatisation BT should be required to keep its price increases below the rise in the retail price index.

Opinions have been expressed about the timing of liberalisation, a relatively non-controversial issue, and privatisation, a controversial separate issue, but linked with or merged into liberalisation in the minds of many people. Perhaps it would have been better to let the liberalisation dust settle before risking general mudiness produced by the rain of privatisation. The case against privatisation has been well presented by BT's management trade union — the Association of Telecom executives⁴².

BT's 1982/83 results showed the replacement cost of net assets at over £16 000M, income at

£6377M and net profit down from £458M to £365M, a return on capital of 5.8%³⁰.

The threat of deregulation and then privatisation produced a remarkable effect. BT concluded an agreement with Satellite Business Systems for a transatlantic business service, and joined in with a UK private industry consortium to provide a direct broadcast satellite (DBS). The 18 month waiting time for services in the City of London has been cut to 3 months.

In October 1982 BT took three full pages in the Financial Times to advertise Teletex, satellite, facsimile, business systems, Prestel, and digital overlay services. It will offer complete packages to companies for external and internal private services, the latter using Local Area Networks (LANs) — strong competition for Mercury.

Also in October government announced that BT's operating licence would include obligations to provide rural telephone services, kiosks, and emergency services, which are lossmakers. Competitors would have no such obligations. On the other hand an organisation which has for so long not needed to take much account of its customers will take time to re-orient itself. The intent is there, but the proof of ability to sell into a competitive market is awaited.

To be continued

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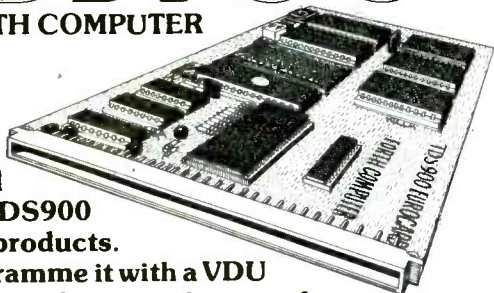
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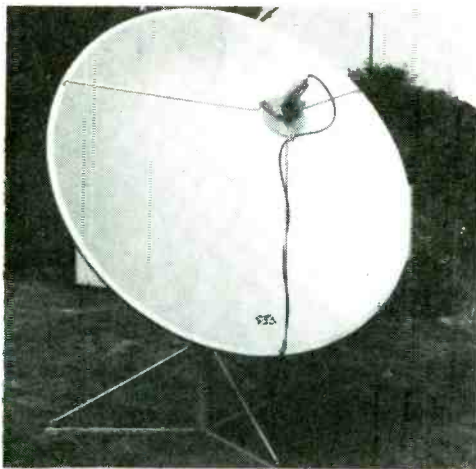
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SC84 Micro-computer

This second section of the SC84 professional microcomputer for engineers and enthusiasts — the input/output interface — provides control for any floppy-disc drive, three parallel ports, an RS232 serial port and more.



As well as providing basic serial, parallel, keyboard and disc input/output, this board also provides some system control and special facilities. At its heart is the Mostek STI, the MK3801N-6. This device is one of several types recently introduced which provide a set of peripheral facilities; for those familiar with Z80 peripherals, it combines a CTC, a PIO, an SIO and an interrupt controller. As befits the complexity of most Z80 peripherals, it has 24 internal registers, 16 of which are directly addressable and eight of which are indirectly addressable, and 16 sources of interrupts.

The STI comprises an eight-bit parallel port, a universal synchronous/asynchronous receiver transmitter (usart) for serial i/o, and four counter/timers, two of which are able to provide delays, count events and measure pulse widths, and two of which are only capable of providing delays. In delay mode, each timer switches the state of an individual output pin at precise intervals so the generators may be used to generate accurate frequency signals up to 500kHz — even four-part music. The two limited capability timers provide internal timing and/or determine usart bit rates.

The parallel i/o port has three features. It can be used just as an i/o port and as such each line may be configured as an input or output. Alternatively, some pins have special functions. Two are event and pulse-measurement inputs for the timers and two are

'handshake' lines for the usart. Thirdly, each line of the port may be used as a Z80 interrupt line. This is especially useful as the Z80 interrupt system is excellent but difficult to use with non-Z80 i.cs, a good example of this being control of a floppy disc drive. There is no Z80 disc controller and yet interrupts are really useful in a disc interface because of high data-transfer rates. The STI is the answer to this, providing 16 distinct interrupts each with its own priority. These could be integrated into a larger system, but the STI is so versatile that it is the only Z80 peripheral i.c. in the basic computer. If there is a blemish in the STI design it is that usart receiver and transmitter handshake lines are both outputs, presumably for compatibility with another rather odd Z80 device. This is unfortunate as logic would dictate that handshaking signals pass in the opposite direction to the data they are controlling, but the STI signals indicate that either the receiver or transmitter in the usart is empty. The former signal correctly warns external devices that the receiver is not ready but the latter is the wrong way round, the handshake being required from the external device to the STI and not away from it. As a result, these signals are disabled in this design and their i/o port lines provide handshaking in the conventional manner. It's a pity that this option was not designed into the chip.

Floppy-disc drive interfacing

is handled by a Fujitsu MB8877A which is an improved and yet cheaper version of the common 1793 controller. The Fujitsu device only requires a +5V supply but for readers with a 1793 to hand, +12V is available on the p.c.b. so either part may be used. To the Z80, the controller looks like a specialized microcontroller with its own instruction set, comprising instructions to reset the system (i.e. move the head of the selected drive to the outermost track, track zero, as a means of getting the head over a known track), move the head to a particular track on the disc, and read or write one or more sectors or a complete track. Inside the con-

by J.H. Adams

Table 1. Signal connections for typical drives.

Signal	Sony D32 3.5in	Std 34 way for 5.25in	Std 50 way for 8in
READY	26	6	22
RDDATA	24	30	46
WPRT	22	28	44
TR00	20	26	42
INDEX	18	8	20
SIDE	16	32	14
HLD	14, 1	16, 2	18
WG	12	24	40
WD	10	22	38
LC	—	—	—
STEP	8	20	36
DIRC	6	18	34
SEL1	4	12	28
SELO	2	10	26
GND	7-25	1-33	1-49

The 5.25in pattern is used on BASF, Canon, Shugart and Tandon drives and the 8in pattern is used on DRE 7100 and 7200 types. Many other drives conform to these standards, but connections should be confirmed before the drive is used. Ground connections are joined over the range of odd-numbered pins indicated.

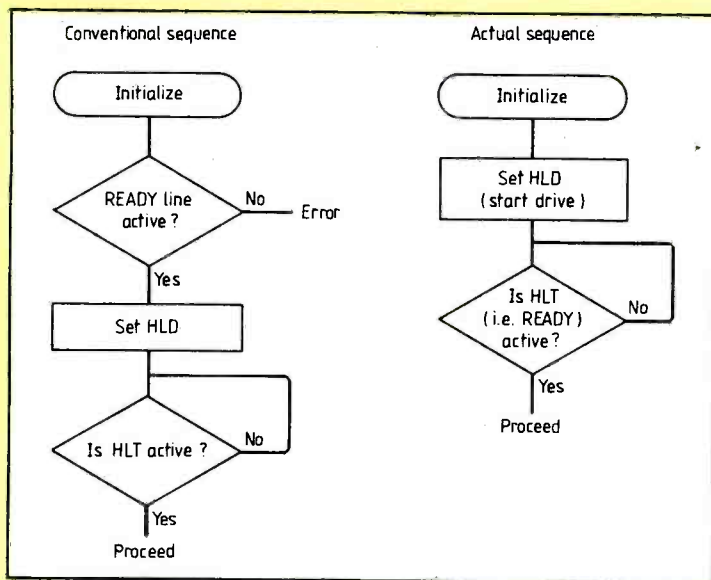


Fig. 3. Floppy-disc controller read/write execution sequence.

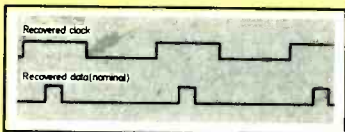


Fig. 1. The only requirements on disc data pulses are that they should not start within 40ns of a clock edge and that they must be entirely within one clock half cycle or must not be longer than 300ns for 8in double density or 600ns for 8in single density. This gives a wide margin of error in data recovery.

Fig. 2. Floppy-disc, serial and parallel input/output are provided by this section (far right). Heart of the circuit is the 3801, containing a parallel port, a usart for serial communications, four counter/timers and an interrupt controller.

troller there are several parameter registers which are loaded with the track and sector numbers required before a command is executed and read from or written to during data transfers between disc and Z80. The controller has two interrupt channels to the Z80 through the STI. One, DRQ, indicates that the controller is ready for data transfer, the other, INTRQ, that the controller has completed a command. In response to the second type, the system can read a status register within the controller to determine whether or not command execution ended satisfactorily, or whether an error pre-empted the command, e.g. the sector could not be found, or a write operation was attempted on a protected disc. The circuit handles both single and double density for all sizes of floppy disc. Switch S_{201} selects double density when closed and S_{202} is shown in the 5.25in, 3.25in and 3.5in/300rev/min drive position (the other is for 3.5in/600rev/min and 8in).

The MB8877A does not provide all of the facilities required for interfacing disc drives to a system. Data separation and regeneration of the data clocking signal is achieved by the SMC9216B (the B version, which is more expensive, only being required for double density) and write pre-compensation by the 74LS195. It

is possible to get all of these facilities in one i.c. but at considerably greater expense and complexity.

Data is recorded on disc by converting the stream of data bytes into serial form and recording the occurrence of binary 'ones' by reversing the sense of the flux recorded on the disc. The rate at which these flux reversals are made, and hence the amount of data stored, is limited by the calibre of the disc and recording head in the same way that higher frequencies are limited in audio systems. On playback these transitions are sensed, amplified and returned to digital form. Different systems have drives running at different speeds; discs change shape and data may consist of long strings of binary zeros, leaving long intervals where no transitions come from the disc. Thus additional and more regular information must be written on the disc to keep the playback process in step with the original recording rate. For this reason, extra flux transitions are inserted into the recording; for single-density recording an extra transition is inserted between every data bit period, making sure that there is a lot of synchronizing information available during playback but reducing the amount of data transferred by half. In double density recording, extra transitions are only inserted between bit periods corresponding to two adjacent zeros in the data bit stream, ensuring that an all-zeros sequence still contains some synchronizing data but, by being inserted in a natural gap in the bit stream, retaining the speed of the ideal system and not asking for a recording density, i.e. a frequency response, greater than that needed for single density. One method gives easier decoding at the expense of storage capacity, the other optimises storage at the expense of decoding complexity. Note that the physical requirement on the drive is the same for both methods so descriptions of some drives as being 'suitable for double density' — and the price premium — can be misleading.

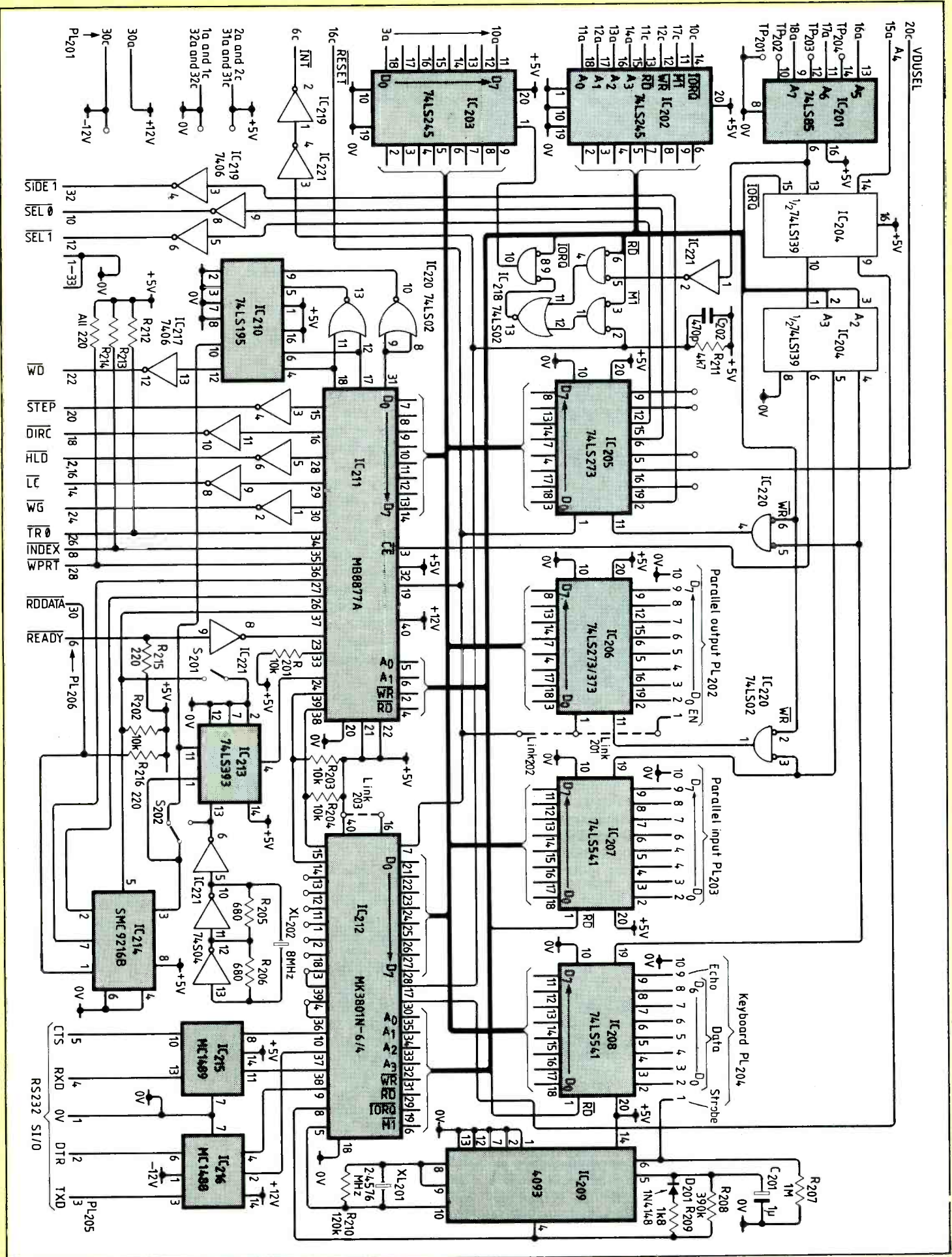
Two data input signals are required by the controller. One is raw data from the disc drive, the other a clock signal derived from the data. The relationship between these two is that each half cycle of the clock signal is a window in which a data pulse must lie. There are two

approaches to recovering the original clock signal — analogue and digital. The analogue technique uses a phase-locked loop with a fast lock-up time. This is an effective technique but requires adjustment of components for correct working and a fair amount of circuitry, not the least because the recovered frequency differs between densities and disc size. The digital technique used here requires just one, albeit rather expensive, eight-pin i.c. which extracts the clock signal from all permutations of density and disc size without adjustment. It works by dividing an 8MHz signal to the nominal clock rate — 125kHz for 5in single density up to 500kHz for 3.5in/8in double density — and adding or dropping a divider count to keep incoming data pulses two counts short of the maximum divider count. This roughly phase-locks data pulses to the counter rate, i.e. data pulses definitely fall within a window framed by the state of the most-significant counter bit. The data pulse is not centralized within the window as it would be ideally, but more than adequately meets controller-input specifications.

As hinted earlier, to get more data on a disc requires better and hence more expensive discs and drive heads. In practice the head in particular will not be grossly over-specified. Adjacent flux changes interact. As flux changes become closer together, the effect of this interference becomes more noticeable and transitions appear to be displaced on the disc and hence in time. Fortunately, the sense of the error is predictable, although its magnitude varies from drive type to type, so a correction — write pre-compensation — can be made before data is written on the disc. The algorithm sensing whether a pulse should be written late, on time or early is implemented in the controller, and the 74LS195 parallel-loading shift register produces a compensation of 250ns, 0 or -250ns, these being values shown to suit most drives. Again, the digital solution is preferred, the write pulse loading a single bit into a shift register being clocked every 250ns. The bit lines come from the controller EARLY and LATE pins and from a gate which derives a NOMINAL signal (logically *not early or late*). At the output of the register a bit appears for one clock period, 250ns, which is either late, 250ns later or 250ns

Table 2. Formatted capacities for single-sided drives.

Disc size	Tracks	Single density	Double density
3.5"	70	140K	350K
3.5"	80	160K	400K
5.25"	35	70K	175K
5.25"	40	80K	200K
5.25"	80	160K	400K
8"	77	250K	616K



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Speed 1 to 38 400 baud, separate receiver and transmitter clocks
Format synchronous 5-8 bit, auto-search and sync. asynchronous 5-8 bit, 1, 1.5 or 2 stop bits
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Disc I/O

Output lines can sink 40mA. Input lines terminated with 220Ω to +5V. Bus lines are active low but have the following specification.

Signal Direction Function

Signal	Direction	Function
READY	Input	Implies disc in drive and rotating at correct speed
RDDATA	Input	Raw data consisting of (nominally) 250ns pulses
WPRT	Input	Indicates disc in drive is write protected
INDEX	Input	Pulses once every disc revolution
TR00	Input	Indicates that head is over the outermost track
WG	Output	Enables disc write circuitry
WD	Output	Data to be written to disc
LC	Output	Indicates that the write current should be reduced
HLD	Output	Loads drive head against disc
DIRC	Output	Sets direction of head stepping. Active means step in
STEP	Output	Steps head one track in direction set by DIRC
SELO	Output	Selects Drive 0
SEL1	Output	Selects Drive 1
SIDE	Output	Selects Side 1

command. In this system the drive motor is turned on by the HLD signal, drive connections labelled Head load and Motor on, or the like, being connected together. READY being inactive does not abort the command; the controller simply starts the drive and waits for READY. What of the time delay between sensible data coming from the disc and the missing pause normally inserted by the monostable device to give the head time to load, and is it a good idea to accelerate the disc with the head already loaded against it? Some drives such as the Tandon TM100 do not have a separate head-loading mechanism and those machines that do usually gate READY with the loading signal within drive so the head will not load until the disc is up to speed. Head loading and settling delay and the time taken to get up to speed amount to less than one revolution, and as the controller has to have counted five revolutions before it gives up attempting a command, this system optimizes the delay between a command being issued and its completion while using the barest minimum of hardware and software. As an example, the disc operating system loads and the directory is scanned and noted in just over 1s when using double density.

Some drives do not give a READY signal, if so, leave the READY input to the computer open or wire it to the 5V supply. Also, some drives have optional links on their circuit boards, one of which offers the choice of head loading being solely controlled by the drive-select line or by a combination of drive select and head load inputs. If so, use the latter option. Advice on using different types of drive will be available through the users' group.

Nominal allocation of drives is that there are two drives designated A and B by the disc operating system, dos, hardware selection being by control lines SELO and SEL1 respectively. If double-sided drives are used, the reverse side of drive A will be designated C and that of drive B, D. This is nominal as the selection of each logical drive surface can be altered temporarily. Open-collector drivers are used between the interface and drive. It is important that the total length of the cable does not exceed 3m (less for the 3.5in drives) and preferably as short as possible. Where more than one drive is used, drive-sig-

nal connectors are wired in parallel, from the computer to the nearest drive, then from this drive to the next etc. The only exceptions to this are the SEL signals which are individual to each drive although possibly carried by the same cable. You will find that 5.25in and 8in drives contain a pack of resistors usually in a dual-in-line package plugged into an i.c. socket wired to the signal connectors and probably labelled 220/330Ω. These packs must be removed from all but the physically furthest drive from the computer. It is good practice to provide a separate, well-rated, power supply for the drives. Disc drives tend to take large amounts of current when the drive motor starts and when the head loads. This can momentarily overload the supply with devastating results if the computer shares the same power source. Also the ground lead between the drive and interface, which should be substantial, is happier when it only carries signals.

Table 1 gives connections to widely used disc drives. There are many second-hand drives around at the moment; buying such drives is rather like buying a second-hand car — there are bargains but there is also rubbish. In particular, I would advise personal inspection and that you watch out for incomplete drives (large areas of p.c.b. without any components) unless they are a bargain and information on the missing parts is available, worn down head pads (the pad that pushes the disc onto the head) and, at least in the U.K., for drives with 110V and/or 60Hz motors. *Caveat emptor.* I would recommend that you obtain a drive with a distinct head-loading mechanism (usually a solenoid) rather than one that puts the head to the disc as soon as the door of the drive is closed. As to the choice between two single-sided drives and one double-sided one, there are many advantages to using two drives, such as the ease with which back-up copies of discs can be made, reduced head replacement costs and that the computer remains useful when one drive is out of action. Many types of drive — Sony, Canon/BASF, DRE, Shugart and CDC — have been used with the computer and the names given in the table are not intended as an indication of merit. Table 2 gives some typical capacities for drives used in single and double density modes.

later still, this being an effective method of simulating early, nominal or late write pulses.

Interfacing to the drives is standard in its signals although you will see that the READY line from the drive, generally indicating that there is a disc in the drive and that it is rotating at the required speed, is not taken to the READY input of the controller (which is instead wired permanently active) but to the HLT (head-loaded test) input of the controller i.c. — an input usually driven by a monostable device triggered by the leading edge of the HLD (head load) signal coming from the controller. Part of the algorithm followed by the controller when executing one of its read or write commands is shown in the flow diagrams. One can see that if READY is used conventionally, extra software and hardware must be provided to start up the disc motors (unless they are left continuously running, which will shorten the life of both disc and drive motor) and then wait for the speed to stabilize before attempting to execute a controller

A listing of SC84's machine-code operating system — MCOS — can be obtained by sending an s.a.e. to *Wireless World* SC84, Room L303, Quadrant House, The Quadrant, Sutton, Surrey SM2 5AS. Details of how to obtain other software including the disc operating-system and Basic were given last month together with a source of p.c.bs and newsletter information.

John Adams has recently designed a switch-regulated p.s.u. for SC84 and we hope to publish its design in the near future. He also plans to provide SC84's two eproms ready programmed; for details send an s.a.e. to the author at 5 The Close, Radlett, Herts.

V.D.U. interfacing, memory and control are detailed in the next article following a description of parallel I/O options and keyboard input.

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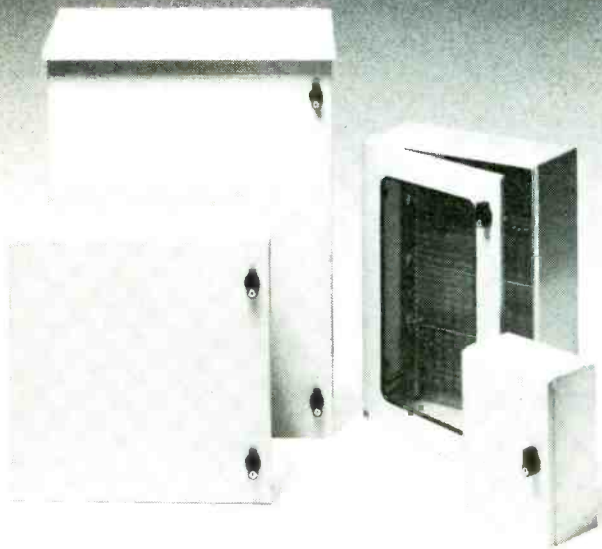
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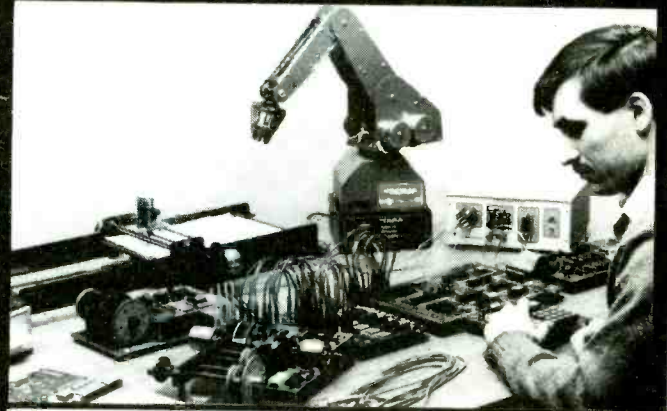
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Multi-standard modem

by Richard Lambley

Circuit details of an f.s.k. modem suitable for any microcomputer with an RS232-compatible serial port

Since the Am7910 i.c. is billed as a single-chip modem, you may wonder at the number of additional components it takes to make it work.

It is certainly possible to connect the device direct to a uart with the addition of little more than the interface to the telephone line. But the circuit of Fig.1 is for a stand-alone modem, and as such it has to be able to drive an RS232 line and receive from it. In addition, switching is needed to select the various modes of operation, and gating of the data and handshake signals may be necessary. Nevertheless, in many applications it will be possible to omit some of the components shown.

Selection of the signalling mode of the Am 7910 (IC₈) is by way of the five inputs MC₀ to MC₄. Of the 32 possible configurations only 19 are available to the user, the others being reserved by the manufacturer. The ten-way switch suggested for the mode selector S₁ reduces the user's chances of stumbling upon the one of the reserved modes (see table 1). The Am7910 makes extensive use of digital signal processing and there are no external filters to adjust, which simplifies greatly this part of the circuit.

Between S₁ and the control inputs of the Am7910 is a t.t.l. priority encoder IC₇. The circuit diagram shows pull-up resistors R₁₁₋₁₄ at its outputs to ensure that the encoder will drive the cmos logic reliably; but if a 74C series device is used instead (74HC147 or 74HCT147) the resistors should be omitted.

The use of a priority encoder may seem a little untidy here, since it would have been possible to use a b.c.d. switch and connect it direct to the 7910. However, it is difficult to specify a b.c.d. switch which every constructor can be certain of obtaining. The cheapest sort is a printed-circuit

mounting rotary type which stands upright on the board; but this would mean having the controls sticking out of the top of the box. The alternative, fitting the controls to a second p.c.b. would involve additional wiring and extra cost. An edge-wise thumb-wheel switch would have been neat, but difficult to interpret unless you had a look-up table constantly to hand.

In any case, gating is needed to control the operation of the modem, and the arrangement shown here simplifies it a little. For example, position 9 of S₁, which is used solely to provide a means of testing the narrow-band back channel in the CCITT V.23 mode, gives automatic selection of the test mode. This loops the output of the Am7910's transmitter back to the input of its receiver and at the same time inhibits the line-seize relay RL₁, if fitted. Decoding of the select lines would otherwise be needed to achieve this.

For other signalling standards, the test mode is selected by S₂, which can be a double-pole

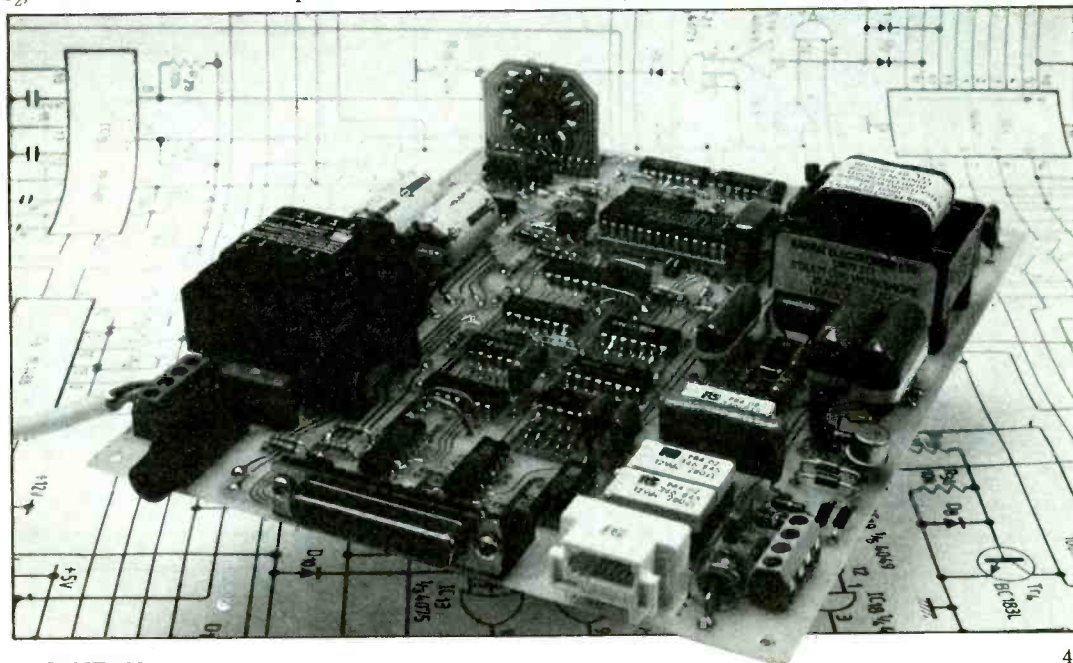
double-throw toggle switch with a centre-off position. In the test position, S₂ causes the output of the Am7910 to be looped back and it adjusts the device's transmit and receive filters to the same setting. This allows the user to test the modem off-line.

A further possibility here is remote-testing of the modem. Data received by the Am7910 can be connected straight into its transmit input and so looped back along the telephone line for tests by the computer at the other end; but the value of this to the private user seems relatively small and so the facility has not been implemented.

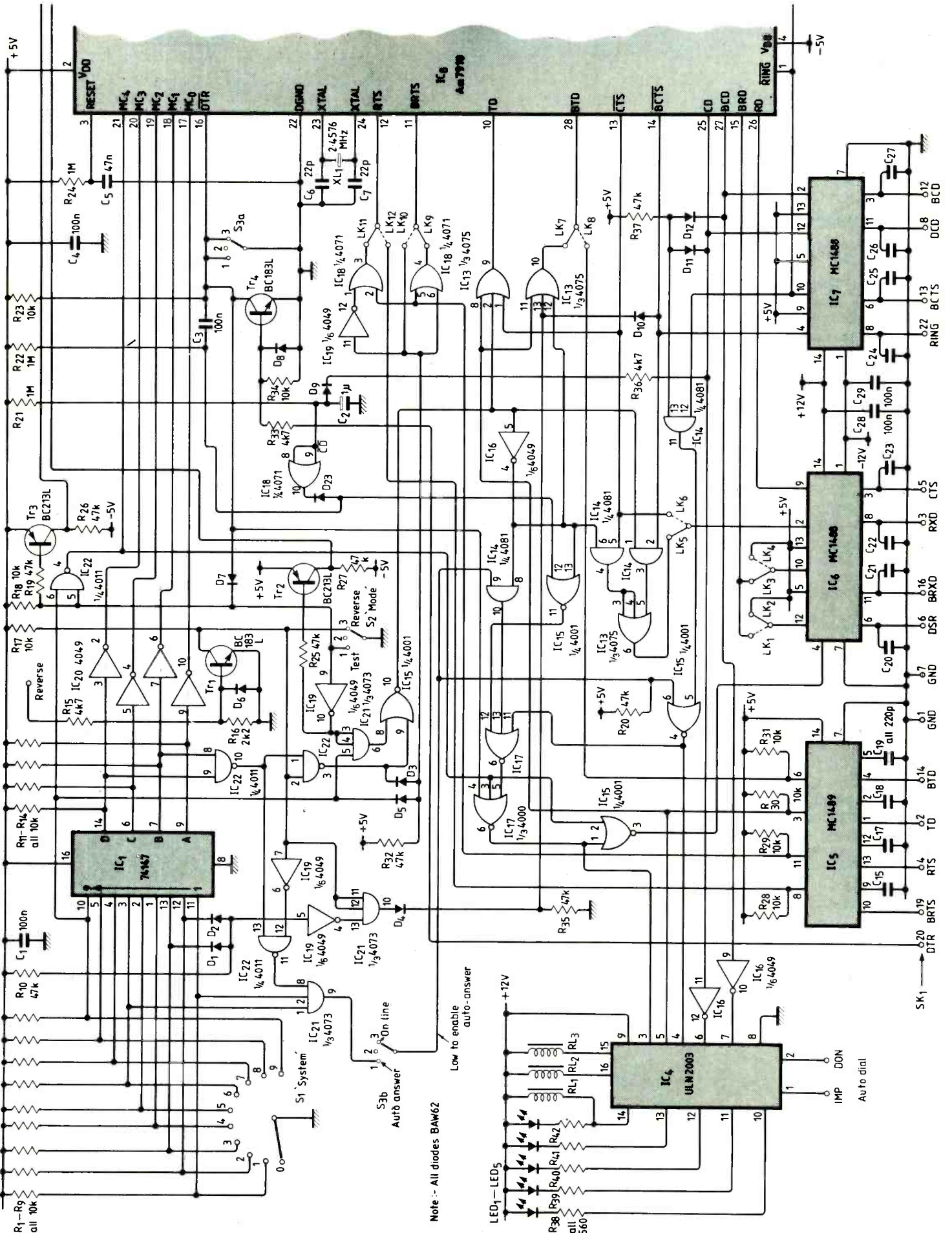
RS232 interface

Some microcomputers have a full RS232 interface brought out to a 25-way D-connector, and the circuit board designed for this project has space for a corresponding socket. The RS232 interface includes data and handshake lines for both the main channel and the back channel (secondary transmit data, secondary clear-

A ready-made printed circuit board for this project will be available shortly. The board, measuring 200mm x 160mm, will be double-sided, with plated-through holes to allow the use of i.c. sockets and to avoid the need for the through-the-board links seen in this prototype. Details next month.



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Note: All diodes BAW62

to-send and so on); and with an arrangement of this sort the RS232 drivers and receivers on the board can be linked direct to the corresponding pins on the Am7910. These links are shown dotted in Fig. 1.

However, the contractor may wish to connect the modem to a computer with a less comprehensive serial interface. The BBC Microcomputer, for example, has an RS423 serial port. This is compatible electrically with the RS232 standard but has its connections brought out to a five-pin domino (reversible DIN) connector. Here the only lines available are a data line in each direction and the associated clear-to-send and request-to-send lines. In the 300 baud modes, these lines must be linked to the main channel connections of the Am7910; but in the CCITT V.23 and Bell 202 modes, it is necessary to switch some of them to the corresponding back-channel pins.

Thus, for accessing Viewdata systems such as Prestel, data to be sent back to the Viewdata computer must be applied to the BTD input, and the clear-to-send signal taken from the BCTS pin. Wide-band data from Prestel appears on the RD pin as does received data in the 300 baud modes.

Normally the RTS output from

the local computer would be wired to the RTS input of the modem, and the CTS output of the modem to the CTS input of the computer. However, this may not always give the right results, and some experiment may be required. One possibility might be to connect RTS from the computer to DTR on the modem. With some low-cost commercial Viewdata modems the RTS connection is omitted and the input of the modem is wired so that RTS is asserted whenever the device is powered.

A feature of this design is that it allows the user to operate the asymmetrical V.23 and Bell 202 standards in the reverse direction, sending 1200 baud signals while receiving on the back-channel. This makes it possible to communicate with the many individuals who have standard 1200/75 baud Prestel modems. This mode is entered by switching S_2 to the 'reverse' position. The same result can be effected by applying a high level to the free end of R_{15} . With suitable software, both computers could send at 1200 baud alternately.

The switching logic is complicated slightly by the fact that the Bell 202 mode does not allow duplex communication in the sense that the V.23 modes do. The back channel carrier, instead

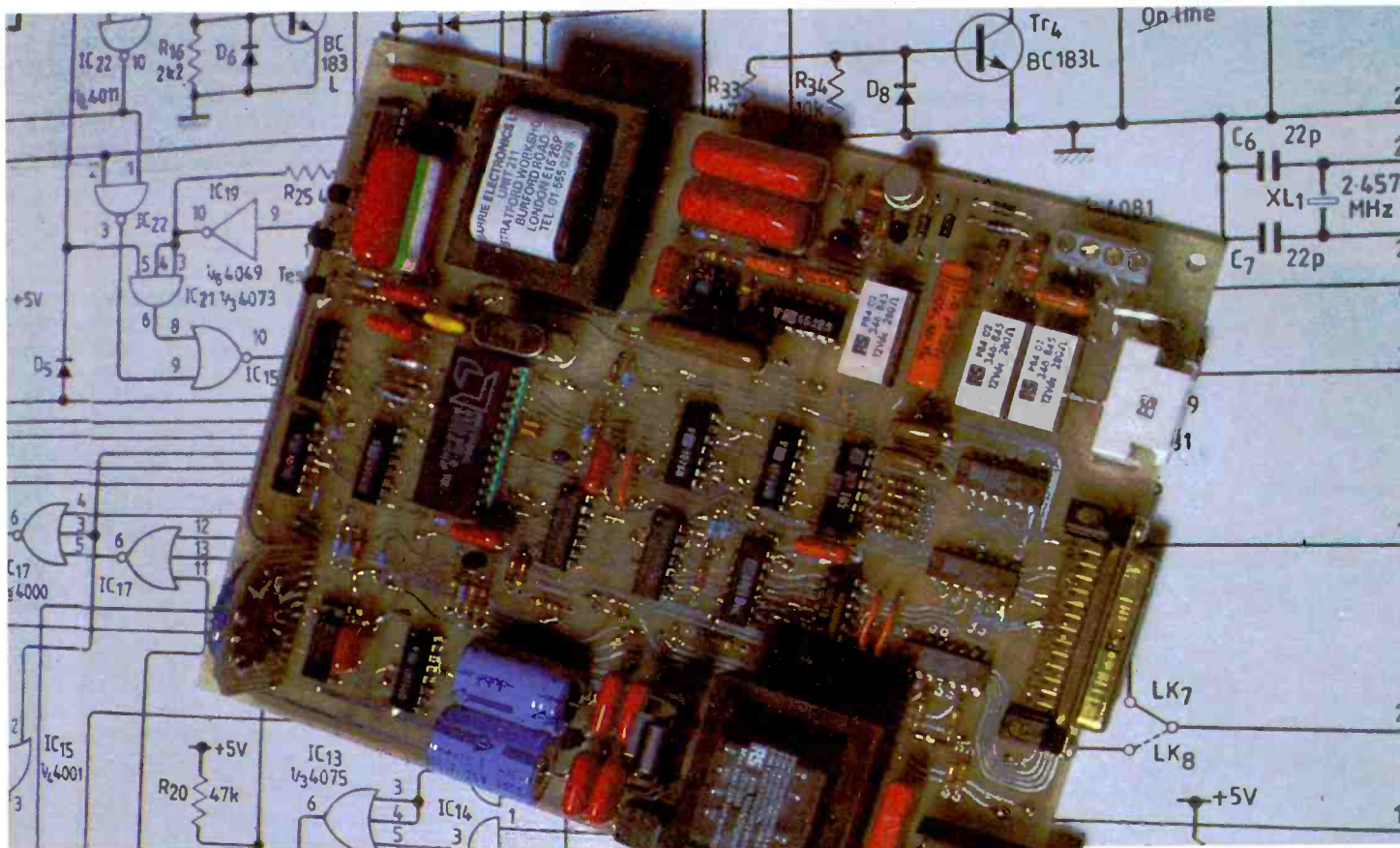
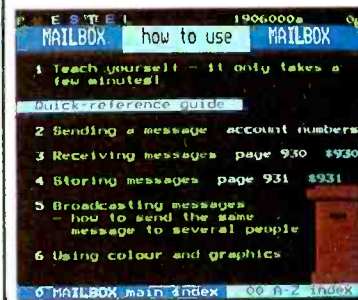
of being modulated with Ascii data by frequency-shift keying, is merely keyed on and off by the BRTS line. When BRTS is low in the Bell 202 mode, a 387Hz tone appears at the Am7910's TC output. The BTD input is therefore without a function to perform in this mode and is fixed at +5V by a section of IC_{13} . In the same way, the BCTS and BRD pins carry meaningful signals only in the V.23 mode.

Managing the Bell half-duplex mode is likely to be a complicated business for most home computers. The low signalling rate in the back channel (not more than 5 bit/s) is outside the scope of a simple serial interface and will entail the use of some other i/o port. Fortunately I have not yet come across any U.K. systems which follow this standard.

The RD and BRD outputs, carrying received data in the main and back channels respectively can be gated together at the RS232 driver (part of IC_6). Internal logic in the Am7910 ensures that in normal use only one is active at a time.

Capacitors can be connected across the outputs of the line-drivers ($IC_{6,7}$) and to the response control pins of the receiver (IC_5) for adjusting the signal rise and fall times. Ideally these should be restricted to conform with the

Using the modem board (bottom) in the 1200/75 baud mode; two frames from Prestel.



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Table 1: mode selection using switches S_1 and S_2 . An equaliser is available in the 1200 baud modes to compensate for poor high-frequency performance over long lines.

S_1 , signalling mode	normal	test
0 Bell 103 300 baud	originate	originate loopback
1 Bell 103 300 baud	answer	answer loopback
2 Bell 202 1200 baud	half-duplex	main channel loopback
3 Bell 202 1200 baud	with equaliser	loopback with equaliser
4 CCITT V.21 300 baud	originate	originate loopback
5 CCITT V.21 300 baud	answer	answer loopback
6 CCITT V.23 mode 1	1200/75 baud	main channel loopback
7 CCITT V.23 mode 1	1200/75 with eq	main ch. loopback with eq.
8 CCITT V.23 mode 2	600/75 baud	main channel loopback
9 CCITT V.23 (test)	(reserved)	back channel loopback

In other modes, it is probably useful to have the relay enabled whenever the modem is in a normal transmission mode and switched on-line. This would allow user-to-user communication where the connection is first established in voice. Further conversation might be necessary after the exchange of data, and the operator could thus avoid accidentally dropping the line on switching back to the telephone receiver.

Acquisition of carrier is indicated by leds, one for the main

input remains low while the call proceeds as it has no further effect.

The auto-answer mode can be enabled only when a suitable signalling standard has been selected by S_1 ; that is, in one of the 300 baud answer modes or in a reverse half-duplex mode.

Component notes

The following notes relate mainly to the ready-made printed circuit board for this project, details of which will appear in the next part.

Switch S_1 is a miniature printed circuit-mounting switch wafer — RS Components type 327-591 is suitable. For the other switches, double-throw centre-off toggle switches can be used. S_3 should be a double-pole type, S_2 single-pole.

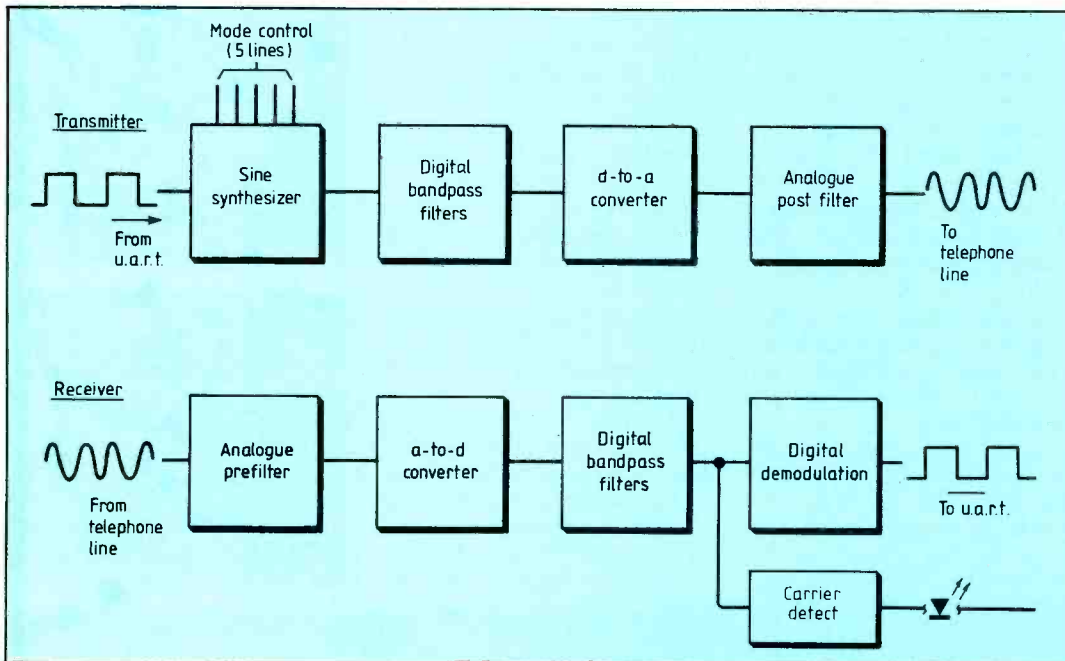
Relay RL_1 is miniature p.c.-mounting telecommunications type, such as RS Components' 346-845 or Farnell Electronic Components' 170-529. Other miniature relays may not have contacts suitable for the voltages encountered across telephone lines.

There will be space on the p.c.b. for two additional relays of the same type, RL_2 and RL_3 ; these are for an optional auto-dialling facility. Drivers are provided in the ULN2003 and the connections brought out to the terminals marked IMP and DON.

The D-connector for the R232 line is a 25-way socket. The printed circuit will accept a p.c.-mounting version, RS Components' 125-856 or equivalent. If a full RS232 interface is not required one of the MC1488 line drivers may be omitted and a cheaper connector used. Some low-cost Prestel modems use a 6-pin DIN socket. The reversible domino connector fitted to the BBC Micro might appear to have the advantage that it could be turned round if the RS423 connections happened to be back-to-front; but as it is, it has unfortunately not been wired symmetrically.

The transistors are general-purpose small-signal silicon types: the p.c.b. will take BC183L and BC213L. Diodes are BAW62 or other silicon signal diodes, except where indicated otherwise. The crystal is a standard-value parallel resonance type and should be available at low cost.

Details of the interface to the telephone line will follow next month.



RS32 specifications, although for driving short lines they can probably be omitted. Unused inputs of the MC1488s should be connected to the +5V line.

For normal transmission in, say, one of the 300 baud modes, S_2 would be in its centre (off) position and S_3 in the on-line position. In this condition, the Am7910 would be enabled by DTR and the line-seize relay RL_1 would be closed. For accessing Prestel, however, it is desirable that the relay remain closed only so long as the incoming carrier is being received. This allows the user to disconnect in the conventional way by sending *90#, which causes the Prestel computer to send its sign-off page and then drop carrier.

When the call is first set up, the relay closes for a brief period as S_3 is switched on-line. The Am7910 should detect the carrier within about 15ms. Its CD output will go low and via R_{36} and D_9 will maintain the relay for the rest of the call.

channel and one for the back channel. The receiver in the Am7910 is more than adequate: its sensitivity is good enough to cope with signals of -43dBm and below.

The line connection can be broken at any time by switching S_3 to its centre position or S_2 to 'test'. This will disable the Am7910 (its DTR terminal acts as a chip-select) and, via IC_{17} , cause RL_1 to drop out.

Automatic answering is possible with the Am7910 if a suitable line interface is connected. When pin 3 is taken low by a ringing detector, an auto-answer sequence is activated. The modem sends a period of silence followed by an answer tone for the calling modem to detect and so to complete the setting up of the call. In this design, the RING signal is stretched by a monostable IC_{12} in the line interface section (to be described later) and used to hold RL_1 , until an incoming carrier signal is available to take over. It does not matter that the RING

Further reading

Am7910 data sheet: Advanced Micro Devices (U.K.) Ltd, A.M.D. House, Goldsworth Road, Woking, Surrey. Tel: 04862-22121.

The chip heard around the world: application note on the Am7910 published by Advanced Micro Devices.

Frank J. Derfler jr.: Microcomputer data communication systems. A Spectrum book, Prentice-Hall International, 1982.



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2N3866 0.85	2SC710D 0.28	2SC1214 15.00	2SC1969 1.50	BLW60C 15.00	MRF309 42.00	MRF904 2.95	SD1012-3 10.00	SD1219 18.00
2N3926 11.26	2SC715D 0.40	2SC1221 10.00	2SC1971 4.00	BLW60FC 65.00	MRF316 55.00	MRF911 2.50	SD1012-4 10.50	SD1219-4 18.00
2N3927 11.82	2SC715E 0.40	2SC1221 10.00	2SC1972 11.00	BLW60G 65.00	MRF317 73.00	MRF915 22.50	SD1013 10.00	SD1220-1 9.50
2N4417 0.75	2SC717P 0.38	2SC1230 1.11	2SC1978 7.50	BLW78 61.80	MRF321 35.00	MRF917 43.00	SD1014-6 10.50	SD1222-5 11.00
2N4426 0.75	2SC730 4.10	2SC1263 5.00	2SC2001 0.45	BLW80 10.25	MRF323 35.00	MRF917 43.00	SD1018-6 13.00	SD1222-STUD 11.00
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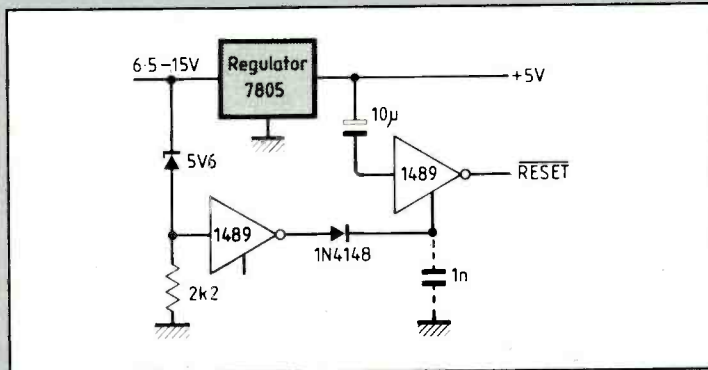
CIRCLE 30 FOR FURTHER DETAILS.

ELECTRONICS & WIRELESS WORLD JUNE 1984

POWER UP/DOWN RESET

Power failure in microprocessor systems causes spurious operation. This circuit was devised to prevent pulses being sent to an eeprom programmer on such occasions by initiating a microprocessor-reset signal when the supply falls below about 6.5V; it also provides power-on reset for about 100ms depending on the power-supply rise time.

Two spare RS232 line receivers are main elements of the circuit. If a stepless transition is required, add the capacitor



shown in broken lines. Threshold voltage is varied by connecting a resistor between the first receiver's response control input and ground or +5V. Values will

need to be changed if the 1489A receiver is used since this version has different thresholds.

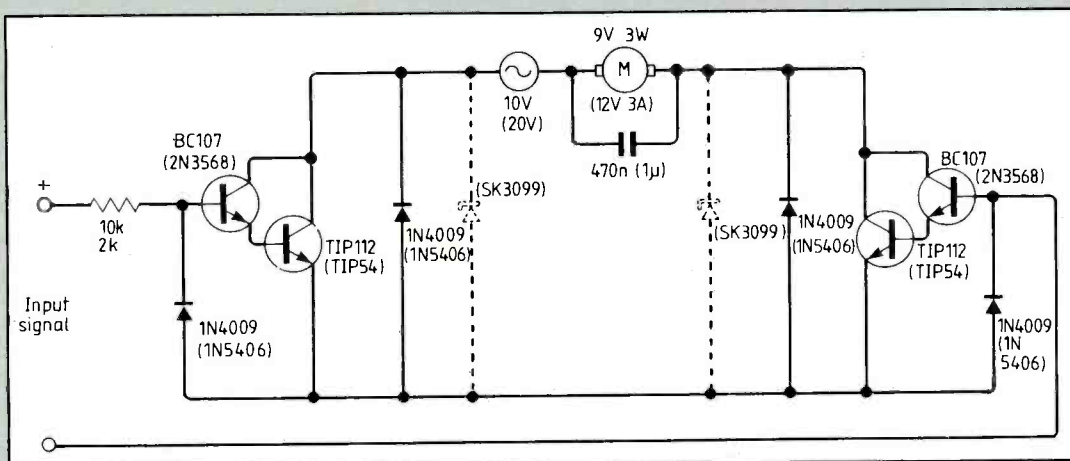
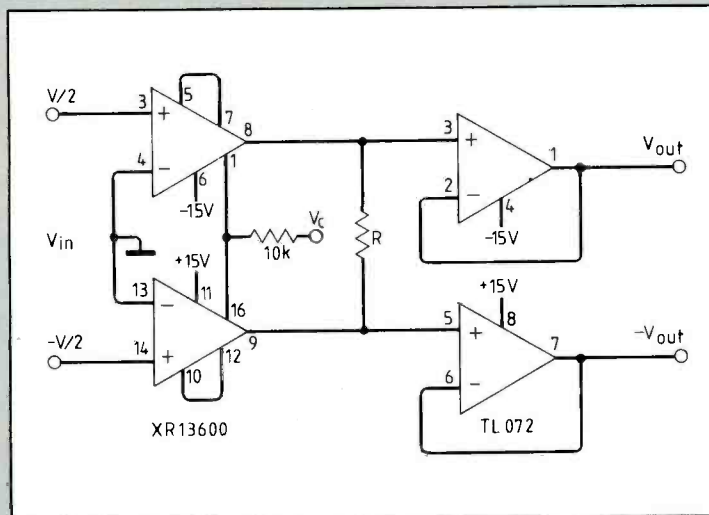
E. Wagner
London

DON'T WASTE GOOD IDEAS
We prefer circuit ideas with neat drawings and widely-spaced typescripts, but we would rather have scribbles on "the back of an envelope" than let good ideas be wasted. Submissions are judged on originality or usefulness — not excluding imaginative modifications to existing circuits so these points should be brought to the fore, preferably in the first sentence. Minimum payment of £30 is made for published circuits, normally early in the month following publication.

INSTRUMENTATION AMPLIFIER HAS DIFFERENTIAL OUTPUT

Combining a TL072 i.c. and an XR13600 transconductance op-amp produces an instrumentation amplifier with differential input and output. Transconductance of the op-amp is $V_{out1} = g_m R V_{in}$ and $V_{out2} = -g_m R V_{in}$ given by $g_m = I_B / V_T$ where $V_T = 26mV$. So gain of the amplifier may be set by varying bias current I_B to pins one and 16 only. For simplicity, only control voltage V_c is shown. The circuit may be useful in applications where V_{out} is above or below zero.

Kamil Kraus
Rokycany
Czechoslovakia

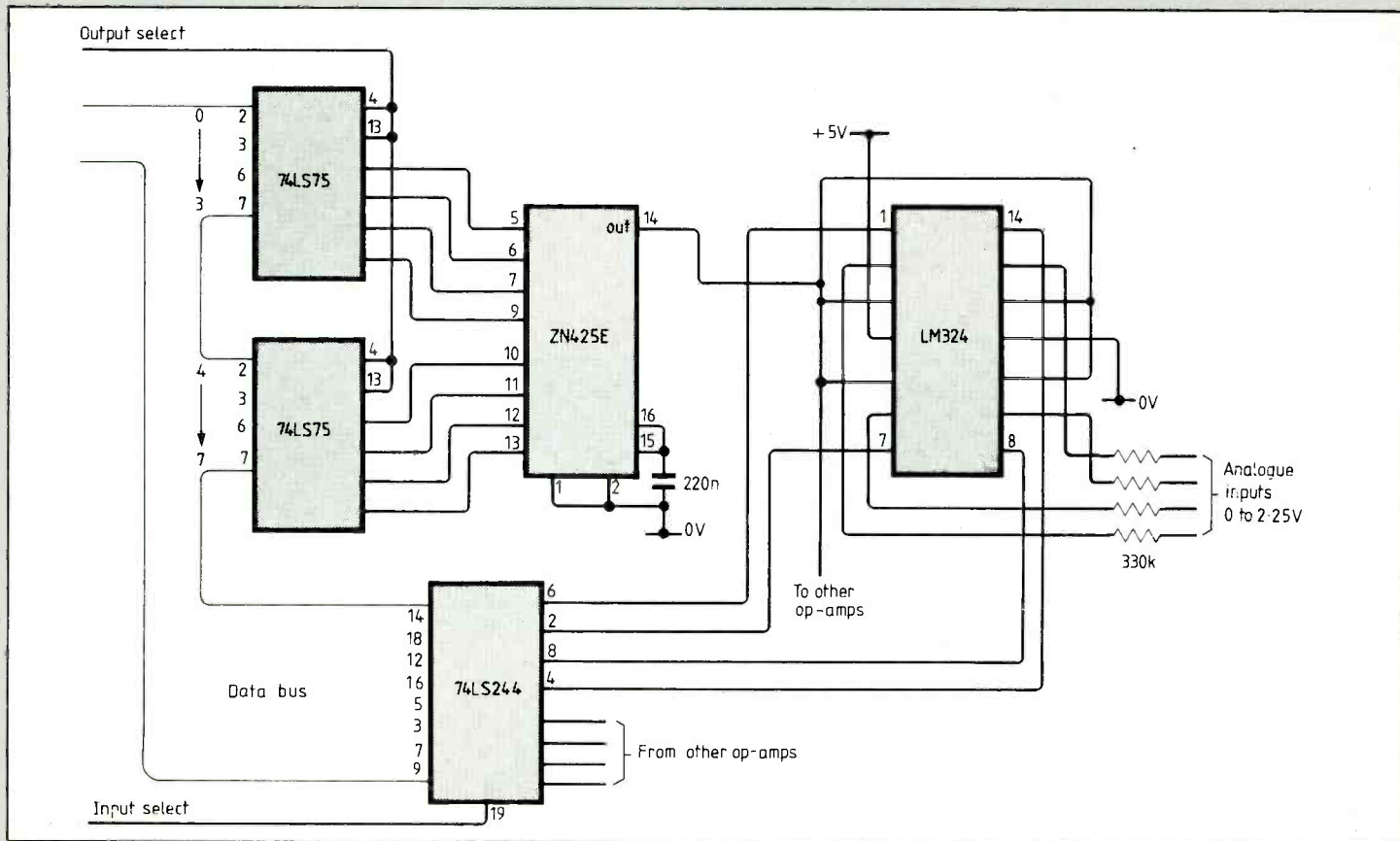


FORWARD/ REVERSE MOTOR CONTROL

Designed for use in a solar tracking system, this forward or

reverse motor controller has three advantages over conventional circuits — only an a.c. supply is required, one signal determines forward or reverse, and only four transistors are used. Polarity of the input signal determines direction of rotation and it is impossible to

switch both Darlington pairs together. Zener diodes are included for larger motors to prevent overvoltage damage during fast commutation.
J.A. Maldonado de la Fuente
Valparaiso
Chile



MULTI-CHANNEL A-TO-D CONVERSION

Excluding address decoding, this four channel analogue-to-digital converter for connecting to a computer requires only five inexpensive i. cs. One more 324 input comparator allows eight analogue channels to be

monitored. Further, the circuit needs only one 5V supply and is quite fast when the computer software is designed to determine the input value using successive approximation. Within the limits of the ZN425 output capability, expansion requires only further input comparators and 74LS44 buffers. K. P. Tibbetts
Preston
Lancashire.

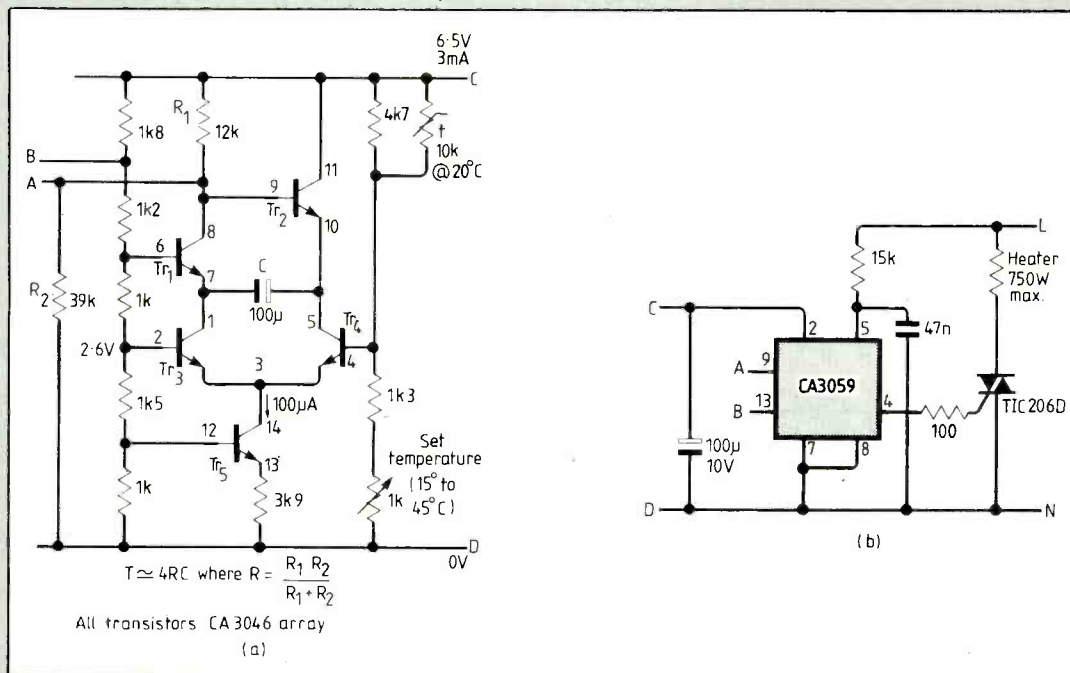
PROPORTIONAL TEMPERATURE CONTROLLER

In this simple proportional temperature controller designed for photographic processing, none of the transistors saturates so the circuit should be capable of functioning at high frequencies in

other applications.

Transistors $Tr_{1,2}$ form an emitter-coupled multivibrator whose period is approximately $4RC$ — 4 seconds for values shown. Mark-space ratio is controlled by the voltage difference between bases of $Tr_{3,4}$; plus and minus $20mV$ give about 25% and 75% respectively which corresponds to a proportional band of about 1K. With these component values, C is never reverse biased. A differential output of $\pm 500mV$ is available between points A and B, or a 1V output can be obtained from a $10k\Omega$ resistor in the collector of Tr_2 . Thermistor characteristics over the range 15 to $45^\circ C$ are linearized by the $4.7k\Omega$ resistor.

J.R. Hunt
Doncaster
Yorkshire



In-circuit emulation

John Ferguson discusses the principle of emulators and illustrates their use by reference to several commercial units.

by John D. Ferguson*

The technique of in-circuit emulation (i.c.e.) provides the engineer with a simple, yet effective means of testing hardware and evaluating software in a microcomputer system. Figure 1 illustrates the principle. The microprocessor is removed from the unit under test (target) and connection made to a second computer system (host) through a dual-in-line plug and ribbon cable. Normally the host computer uses a similar microprocessor to that removed from the target, to imitate or emulate the original processor. At first glance it might seem pointless to remove the original to have it replaced by another in the host, but the technique allows the host to get between the target system and its microprocessor, enabling it to monitor bus activity or to inject signals into the target system.

The technique was first introduced by Intel on their microprocessor development system (MDS) to help debug hardware and software problems encountered during the development phase of a project. Early development systems were essentially software orientated, providing editors, assemblers, linkers, and, to a limited extent, some facility to execute and debug the final machine code. However, to test hardware and software effectively it was necessary to commit the final code to eprom before transferring it to the unit under development. Any further debugging that was required was now carried out using a logic analyser. If faults were discovered the engineer returned to the development system to update the software before programming a new eprom.

The introduction of i.c.e. shortened this time-consuming procedure, allowing the design engineer to run the system under development directly from the MDS, thus eliminating the need to use eproms as a means of transporting software into the target system. Further, since the emulator has access to the target

system's buses during program execution, it can also be used as a debugging tool. To help with this task most emulators also provide on-board logic analyser functions.

In-circuit emulation is now a standard feature on development systems with some manufacturers, including Hewlett Packard, Genrad and Tektronix, providing a range of emulators covering a variety of 8 bit and 16 bit microprocessors. However, all of these systems are well outside the budget of most individuals or small companies involved in microprocessor system development. To fill this need several manufacturers, notably Microtek, are producing a range of low cost stand-

Hewlett Packard, the John Fluke Co. with their 9010 Troubleshooter and Solartron with their range of Micropods, are now producing

*Microelectronics Educational Development Centre.

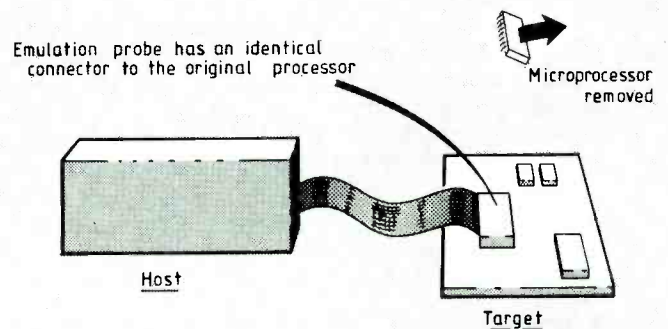


Fig.1. Attaching a target system.

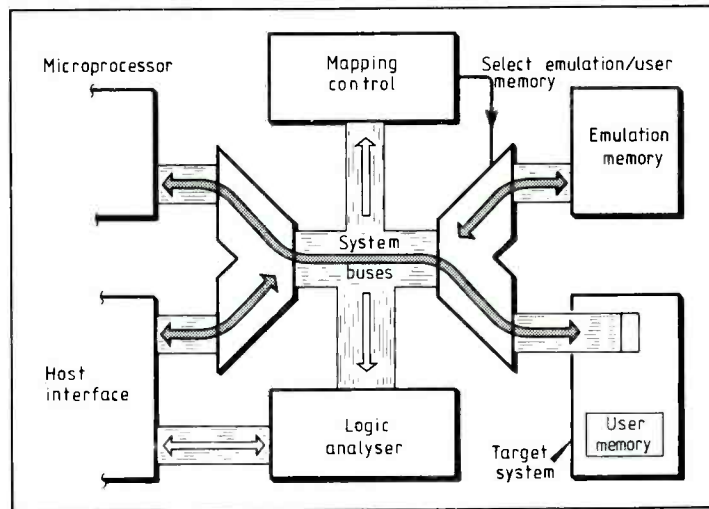
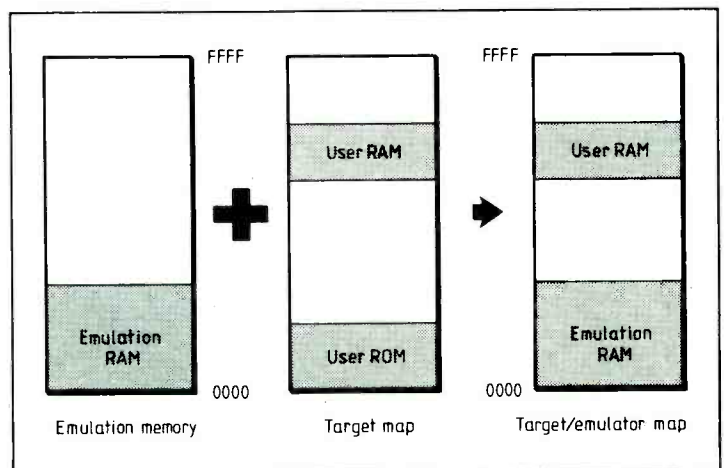


Fig.2. Simplified emulator architecture.

Fig.3. Mapping — constructing memory map for emulation. In this example, 'user rom' overwritten by emulation ram, allowing software to be loaded and tested by host system.

alone emulators that can be driven through an RS232 interface from either a v.d.u. or any popular microcomputer with a serial port.

The value of in-circuit emulation has also been acknowledged by those involved in microcomputer servicing, offering a simple method of injecting test or stimulus programs into a defective board. This can prove an essential facility if the unit under test does not respond to normal keyboard operation or, perhaps, as in the case of some controllers, does not contain a keyboard. Many manufacturers, including



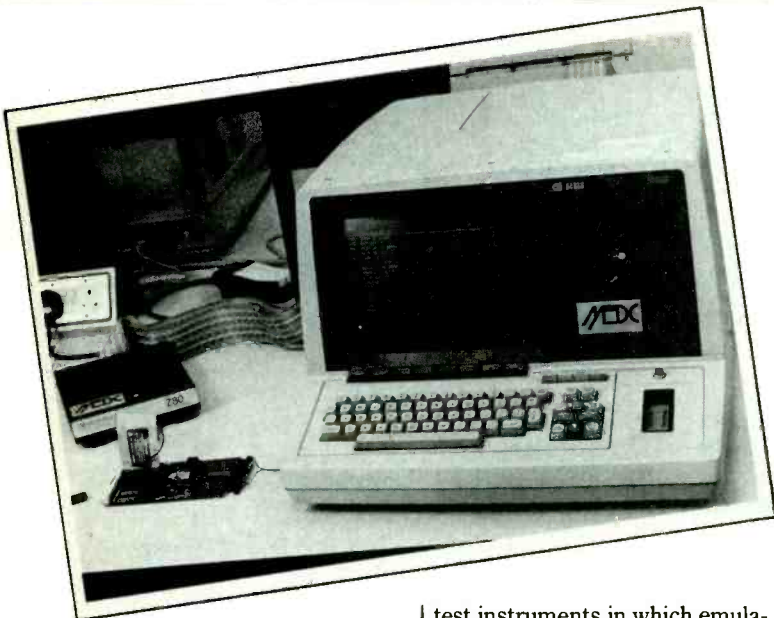


Fig. 4. HP64000 development system — an example of universal system supporting a range of microprocessor families.

Fig. 5. Example trace specifications on HP64000.

test instruments in which emulation is an essential ingredient.

Basic principles

Figure 2 shows a simplified diagram of an emulator's internal architecture. Control circuitry is used to allow either the host computer or the emulation processor

to gain access to the target system's buses.

Most emulators are equipped with random-access memory (emulation memory) that can be used to add to, or take the place of memory on the target board (user memory). This extra ram can often prove useful during program development, providing workspace for software before it is finally committed to rom.

The procedure of establishing a memory layout for the combination of emulator and target is called mapping. In microprocessor development systems this is normally accomplished from the keyboard during a configuration phase prior to emulation. Simpler systems (e.g. Microtek's MICE) use small in-line switches on the emulator's main printed circuit board.

An example of mapping is shown in Fig 3. In this arrangement the memory space occupied by user rom has been overwritten with emulation memory allowing the engineer to load and test different versions of software. After mapping has been decided, control circuitry ensures that all addresses established by the processor or host system are directed to the selected memory devices ie emulation or user memory.

Normally the target system's own clock would be used to run the emulator's microprocessor in 'real-time', thus ensuring that any critical timing of the target system hardware is maintained. If, however, the emulator is used without prototype hardware it can make use of an internal clock option.

Once configuration is complete the operator can then load the machine code into either emulation or user memory before running or single-stepping the program. As all designers are aware, prototypes seldom work first time and most projects would now enter a testing phase in which the engineer would call on the debugging capabilities of the emulator, which can be divided into four areas:

- memory/register display and modification
 - single step, single cycling
 - software breakpoints
 - trace analysis.
- The first three features are common to those found in most software debugging packages, e.g. DDT, ZSID. Trace analysis, however, is often enhanced by the inclusion of a logic analyser, allowing the operator to capture

bus activity, about some trigger event, in a trace buffer.

Emulation on the HP64000 development system

For ease of use and versatility, Hewlett Packard's 64000 development system, shown in Fig. 4, sets a high standard. The system offers a variety of options ranging from a stand-alone portable station, for use in the field, to a multi-user, hard-disc based network capable of supporting a wide spectrum of microprocessor families. Multi-user capability greatly eases the problem of integrating software produced by a team of engineers, allowing different areas of a project to be developed independently and yet allowing them to be easily shared between members of the team. Hardware options available for the 64000 include

- a wide range of 8 and 16 bit emulators
- a user-configurable emulator (a novel idea allowing customers to 'build' an emulator for any processor not supported by HP)
- state and timing analysis
- a range of eprom programmers.

In common with other systems the operator is provided with a wide range of debugging features for use under emulation. Symbolic debugging, where the operator can refer to program locations using labels defined in the source code, greatly eases use, especially when tracing routines generated by compiling high level language programs written in PASCAL or 'C'.

Depending on your needs (and assets) such a system offers many analysis options starting with a software logic analyser (not real-time) and progressing to plug-in cards that perform state and timing analysis on the emulation subsystem. Fault location with a logic analyser demands flexibility when defining the trigger event, or more completely the 'trace specification'. Figure 5 shows a variety of possible trace specifications highlighting the power of the analyser.

The systems have been on the market now for several years and most of the bugs have been removed. However, a few rough edges still remain, and some typical examples again from the HP 64000 include arithmetic problems evaluating relative jumps when disassembling Z80 code and a rather messy approach to

```

TRACE SPECIFICATION
trace after address = 8000H

CONTENTS OF TRACE BUFFER
ADDRESS, DATA, STATUS
AFTER 8000H FBH 1FH
+001 0006H LD A, FFH
+002 0008H INC HL
+003 0009H CP L
+004 000AH JP NZ, 0H
+005 0005H LD A,
+006 000AH L
+007 000P
+008
+009
+P
    
```

Using address alone to trigger the analyser

```

TRACE SPECIFICATION
trace only address = 8000H or address = 8100H

CONTENTS OF TRACE BUFFER
ADDRESS, DATA, STATUS
AFTER 8000H 00H 1FH
+001 8000H CAH 1FH
+002 8100H CAH 1FH
+003 8000H CBH 1FH
+004 8100H CBH 1FH
+005 8000H CCH
+006 8100H
+007 80H
+008
+P
    
```

Monitoring bus activity as the processor accesses address 8000H or 8100H

```

TRACE SPECIFICATION
trace in sequence data = 00H then
data = 00CH trigger after address = 8000H

CONTENTS OF TRACE BUFFER
ADDRESS, DATA, STATUS
SEQN 8000H AAH 1FH
SEQN 8000H CCH 1FH
AFTER 8000H CDH 1FH
+001 0006H LD A, FFH
+002 0008H INC HL
+003 0009H CP L
+004 000AH JP NZ,
+005 0005H L
+006 00H
+007
+P
    
```

Looking for a sequence on a data bus before triggering and capturing bus details after address 8000H

emulating the 8088/8086, where an emulation monitor program has to be linked to and loaded with the user program. Of the other development systems two families can be identified.

manufacture specific: this includes the INTEL MDS and the Motorola EXORmacs development system. Each system will normally deal with all that manufacturer's microprocessors often including devices not yet covered by the 'Universal' systems.

'Universal': examples include the Futuredata and Philips systems as well as the HP64000 detailed above. While covering a wider range of processors from different manufacturers, they are less likely to cope with the latest and fastest from any given supplier.

Low-cost solution - Microtek MICE

Microtek's 'Micro-In-Circuit-Emulator' (MICE) shown in Fig. 6 performs many of the functions found on a development system at a fraction of the cost. A range of personality cards allow MICE to emulate most industry standard microprocessors, including the 8088/8086, 68000, 8085, 6809 and the popular domestic processor, the 6502. Two models are available, differing in the size of the emulation ram and the trace facilities.

MICE I 8Kbytes emulation memory — not real-time trace.
MICE II 32K bytes emulation memory, expandable in blocks of 32Kbytes — real-time trace.
 Both models are controlled via an RS232 interface, using either a display terminal or a computer system with a compatible port.

Driving a stand-alone emulator from v.d.u. would only be satisfactory for a small development applications or when used in a servicing role (e.g. to check ram or form signatures of rom using its on-board test routines). The list commands, Fig. 7, includes a line assembler, useful for small routines or when patching a larger piece of software and two-pass disassembler that generates labels for all subroutine and jump instructions - a nice touch not found even in expensive systems, Fig. 8.

Serious applications, however, would utilise a host computer system allowing code generated by assemblers or compilers to be downloaded, in either Intel or Tektronix format, to the target system. When a host system is used it requires a driver program to communicate with the emulator. A range of routines is available for some popular systems:

- Apple
 - any CP/M machine
 - Digital Equipment minicomputers
 - Sharp Personal Computer
- Guidelines included in the manual should allow anyone with a reasonable skill in interface programming to generate a driver routine for their machine.

Trace facilities are good, allowing the operator to perform a real-time forward or backward trace capturing address, data and processor status information in a massive 2048 word buffer. However, there are limitations on the sophistication of the trigger event which is limited primarily to address and status, Fig. 9.

To summarize, in-circuit emulation has been available on a



range of development systems for several years, where it has proven its usefulness as part of the product development cycle. The appearance of low-cost, stand-alone emulators should widen the appeal of the technique. A list of suppliers follows.

Fig. 6. MICE can be operated from a v.d.u. or, as shown, from a computer system running a driver routine.

Fig. 9. Trace analysis with Microtek's MICE II.

```

>?
ASSEMBLY           A loc
BACKWARD TRACE    B [R] addr[c(q)]
CYCLE STEP        C
DISABLE           D N|H|C
ENABLE            E N|H|C
FORWARD TRACE     F [R] addr[c(q)]
EXECUTION         G [a][a2]]
BREAKPOINT       H [0|1|2|] | addr[c(q)] | 2 addr
INPUT            J
JUMP             J [a][a2]
LIST TRACE       L [step] | [a2] | [q] | [S] | [step]
MEMORY          M (C|S|D|S|S|E|S) | [a] | [a2] | [d] |
OUTPUT          O port d | [d2] | [d3] | [d4] |
REGISTER        R [A|X|B|X|C|X|D|X|S|P|B|S|I|D|I|D|S|E|S|S|C|S|I|P|F|S]
INSTRUCTION STEP S [S] | [c]
TRANSFER/TEST   T (C|S|D|S|S|E|S) | [a] | [a2] | [M] | [a3]
UPLOAD         U [a] | [a2] | [T] |
RESET          X [a] | [a2] |
DISASSEMBLY    Z [a] | [a2] |
DOWNLOAD       ? [a] | [a2] |
HELP           ? (INT) | (TEK)
ATTENTION     ?
>

```

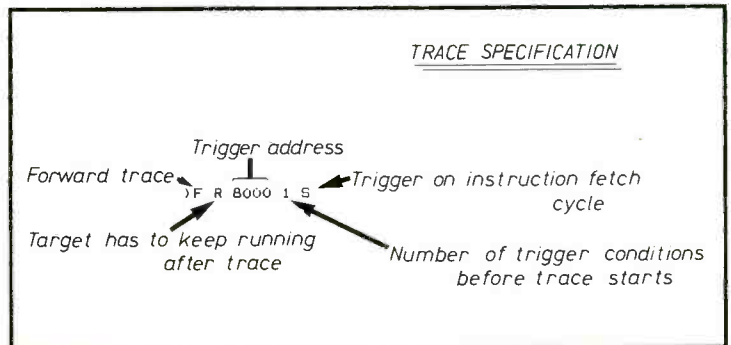
Fig. 7. MICE command summary.

```

>? 8000 8010
LOC   OBJ      LINE   LABEL   SOURCE CODE
8000  200680   0001   B8000   JSR 8006
8003  4C0080   0002           JMP 8000
8006  A904     0003   S8006   LDA #04
8008  8D1180   0004           STA 8011
800B  CE1180   0005   B800B   DEC 8011
800E  D0FB     0006           BNE 800B
8010  60       0007           RTS

```

Fig. 8. Two-pass disassembler on MICE.



FRAME	IFADDR	ADDRESS	DATA	STATUS	SPARE (8 BITS)
0000	8000	8000	20	S	11111111
0001		8001	06	R	11111111
0002		01BA	80	R	11111111
0003		01BA	80	W	11111111
0004		01B9	02	W	11111111
0005		8002	80	R	11111111
0006	8006	8006	A9	S	11111111
0007		8007	04	R	11111111
0008	8008	8008	8D	S	11111111
0009		8009	11	R	11111111
000A		800A	80	R	11111111
000B		8011	04	R	11111111
000C	800B	800B	-	-	-
000D		-	-	-	-
000E		-	-	-	-

The 'L' command displays the contents of the trace buffer in Hex.

DISPLAY TRACE IN HEX

Adding an 'S' to the 'L' command displays the trace buffer in mnemonic form

FRAME	ADDRESS	DATA	MNEMONIC-CODE
0000	8000	20	JSR 8006
0006	8006	A9	LDA #04
0008	8008	8D	STA 8011
000C	800B	CE	DEC 8011
0012	800E	D0	BNE 800B
0015	800B	CE	DEC 8011
001B	800E	D0	BNE 800B
001E	800B	CE	DEC 8011
0024	800E	D0	BNE 800B
0027	800B	CE	DEC 8011
002D	800E	D0	BNE 800B
002F	8010	60	RTS
0035	8003	4C	JMP
0038	8000	20	
003E			
0040			

DISPLAY TRACE IN MNEMONICS

EMULATOR SUPPLIERS

AMF Potter & Brumfield
AMF House
Brislington
Bristol
BS4 4AZ

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28 St Judes Road
Englefield Green
Egham
Surrey
TW20 0HB

General Instrument
Microelectronics Ltd
Times House
Ruislip
Middlesex
HA4 8LE

Intersil Datel (UK) Ltd
9th Floor
Snamprogetti House
Basing View
Basingstoke
Hants
RG21 2YS

Microsystem Services
11 Duke Street
High Wycombe
Bucks
HP13 6EE

Quarndon Electronics Ltd
Slack Lane
Derby
DE3 3ED

SGS-ATES (UK)
Planar House
Walton Street
Aylesbury
Bucks
HP21 7QJ

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Microelectronics Ltd
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B16 8QW

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Hants
RG24 0QG

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GU21 1JT

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Surrey
KT8 0SN

Arrow Computer Systems Ltd
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Stafford Road
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Surrey
SM6 8RW

Bleasdale Computer Systems Ltd
Francis House
Francis Street
London
SW1P 1DE

Bowthorpe Microsystems
41 Alston Drive
Bradwell Abbey
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Bucks
MK13 9HA

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168 Finchley Road
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Brookers Road
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RH14 9RZ

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Hants
SO5 8JY

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Kingsland Estate
Basingstoke
Hants
RG24 0QB

Digital Equipment Co Ltd
Worton Grange Industrial Estate
Imperial Way
Basingstoke Road
Reading
RG2 0TG

Eagle Controls (England) Ltd
Orchard Road
Royston
Herts
SG8 5HF

Fairchild Camera & Instruments
(UK) Ltd
230 High Street
Potters Bar
Herts
EN6 5BU

Ferranti Comp. Syst. Ltd
The Courtyard
20 Denmark Street
Wokingham
Berks
RG11 2BB

Fulcrum (Europe)
Valley House
Furleigh
Essex
CM3 6QH

Gemini Microcomputers Ltd
Oakfield Corner
Sycamore Road
Amersham
Bucks
HP6 5EQ

Giltspur Microsystems Ltd
74 Northbrook Street
Newbury
Berks
RG13 1AE

Golden River Co. Ltd
Churchill Road
Bicester
Oxon
OX6 7XT

Gould SEL Computer Systems Ltd
31 St Nicholas Way
Sutton
SM1 1EA

Harris Semiconductor Ltd
P. O. Box 27
145 Farnham Road
Slough
SL1 4XD

Hitachi Electronic Comp (UK) Ltd
Hitec House
221 Station Road
Harrow
Middlesex
HA1 2XL

Intel Corp (UK) Ltd
Pipers Way
Swindon SN3 1RJ

Intelligent Artifacts Ltd
Cambridge Road
Orwell
Royston
Herts
SG8 5QD

Jasmin Electronics Ltd
St Matthews Way
Leicester
LE1 2AA

Kode Ltd
Station Road
Calne Wilts
SN11 0JR

Lucas Logic Ltd
Welton Road
Wedgnoek Industrial Estate
Warwick
CV34 5PZ

Mostek UK
Masons House
1 Valley Drive
Kingsbury Road
London
NW9 9NJ

Motorola Ltd
Taylors Road
Stotfold
Hitchin
Herts SG5 4AY

Mullard Ltd
Mullard House
Torrington Place
London WC1E 7HD

National Semiconductor Ltd
Harpur Centre
301 Home Lane
Bedford
MK40 1TR

NEC Electronics (UK) Ltd
116 Stevenston Street
New Stevenston
Motherwell
Lanarks
ML1 4LT

Plessey Microsystems Ltd
Water Lane
Towcester
Northants
NN12 7JN

Plessey Peripheral Systems Ltd
3 Harrowden Road
Brackmills
Northants
NN4 0EB

RCA Solid State Ltd
Lincoln Way
Windmill Road
Sunbury-on-Thames
Middlesex
TW16 7HW

RCS Microsystems Ltd
Gresham House
Twickenham Road
Feltham
Middlesex
TW13 6HA

Rockwell International Inc.
Heathrow House
Bath Road
Hounslow
Middlesex
TW5 9QW

Sintrom Electronics Ltd
14 Arkwright Road
Reading
RG2 0LS

Spectra-Tek (UK) Ltd
Swinton Grange
Malton
N. Yorks
YO17 0QR

Syntek Inc.
Honeywell House
Charles Square
Bracknell
Berks
RG12 1EB

Techex Ltd
5B Roundways
Elliot Road
W. Howe
Bournemouth
BH1 8JJ

Texas Instruments,
Semiconductors Div.
Manton Lane
Bedford
MK41 7PA

Vako Electronics Ltd
Pass Street
Wemeth
Oldham
OL9 6HZ

Zilog (UK) Ltd
Zilog House
Moorbridge Road
Maidenhead
Berks
SL6 8PL

MICE details

ARS Computers
Doman Road
Camberley
Surrey

Hewlett Packard
South Queensferry
West Lothian
EH30 9TG

Solartron Electronics Group
Farnborough
Hampshire
GU14 7PW

Philips Electronics Instruments
York Street
Cambridge
CB1 2PX

INTEL Co (Ltd)
Piper's Way
Swindon
Wiltshire
SN3 1RJ

GenRad Ltd
Norrays Drive
Maidenhead
Berks
SL6 4BP

Motorola Ltd
York House
Empire Way
Wembley
Middlesex

Improving colour television decoding

by D. C. A. Read
B.Sc. (Eng),
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This article details the performance and setting up of the filters used in the add-on enhancement board of Figs 34 & 36 (March). It leads onto passive filter circuits that can be placed between tuner i.f. and PAL decoder circuits as an alternative to the add-on board, includes analysis of filter networks used in current receivers, and surveys suitable delay lines.

The three filters used in the extra board circuits shown in Fig. 34 and 36 have the following characteristics to suit the signal filtering requirements.

Chroma band-pass filter. The chroma is filtered by L_1 , L_2 and L_3 with capacitors C_5 , C_6 and C_7 (Fig. 34, March), and the insertion loss conformed approximately to a gaussian band-pass response centred on f_{sc} . If the bandwidth of this filter is narrow, it will result in: reduced chroma risetimes (up to $1\mu s$), reduced cross-colour because high-band luminance reaching U and V chroma demodulations is reduced, and a lower noise spectrum in the displayed chroma. However, with a very high 48 element aerial and steady-guy-wires through the roofs of neighbouring houses, a good signal-to-noise ratio was obtained. Hence, the decision was made that good chroma resolution (decreased risetimes) was required and that the resulting cross-colour increase would be tolerated.

In colour print 2 (top right-hand page 65, February issue) the increased chroma bandwidth results in the increased width of the band of cross-colour across the screen centre with this test signal, in practice, it widens mainly downwards. The faster chroma edges give a subjectively sharper picture and the greater noise spectrum, resulting from the wider bandwidth, was only apparent when viewing Outside Broadcasts (where greater noise with the video signal often occurs), but there are occasions when cross-colour is apparent. The lower trace of Fig. 52 shows the reasonable symmetry between the 0-6dB down points; note that a good i.f. will only roll off above 5.5MHz and the sound trap will bring the level well down by 6MHz. It is also important to have, ideally, a flat group delay response, or one that is symmetrical about f_{sc} as indicated in Fig. 53.

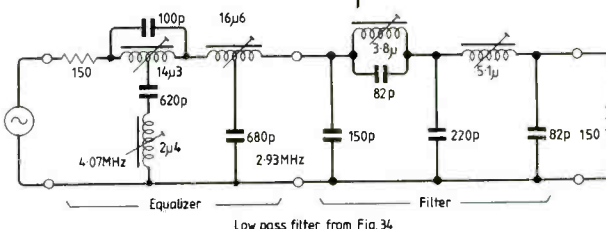
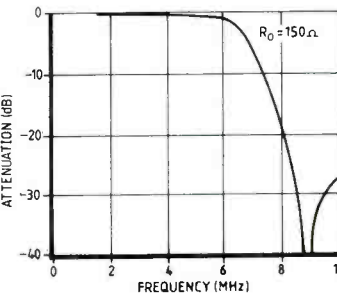
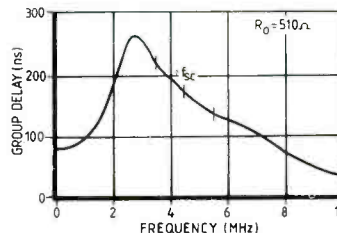
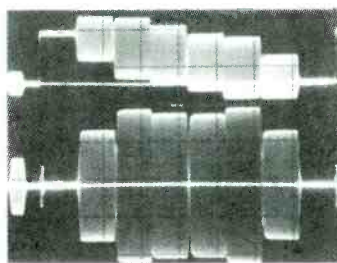
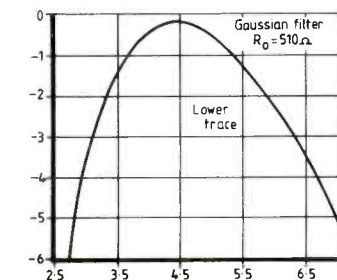
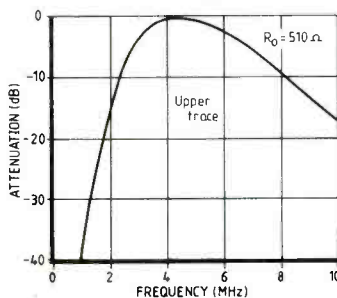
The luminance cancelling effect is slightly improved with a flat group delay, but the extra delay introduced by a phase equalizer (and the timing adjustment delay at DL_1) did not seem justified after viewing tests.

The filter is set up first adjusting for maximum f_{sc} at the filter output and then makes a small adjustment of all three cores for minimum 7.8kHz at the chroma transitions (with colour bar test signal). The oscilloscope is best locked to MS (mixed syncs) or the syncs with the incoming video.

Post-modifier low-pass filter. The modified output chrominance (V-axis switched) signals cancel chroma from the composite video present at the Tr_4 summing point to provide clean luminance (Fig. 34, March). A low-pass filter is required to remove other frequency products around $2f_{sc}$ and $3f_{sc}$, (as shown in the spectral energy diagram of Fig. 19, January) to obtain a clean 0-5.5MHz baseband signal. Components C_{20} , C_{23} , C_{24} and C_{26} with L_{11} and L_{12} form this filter and the group-delay phase equalizer is formed by C_{15} , C_{18} , C_{19} with L_8 , L_9 and L_{10} . Figure 54 shows the insertion loss of the filter which is flat to 5.5MHz and is more than 35dB down at $2f_{sc}$ (8.866MHz); L_{11} and C_{23} are in parallel resonance at $2f_{sc}$ to provide this part of the characteristic, L_{12} and the associated capacitors ensure the response remains greater than 35dB in the stop band. Figure 55 is the group delay characteristic of the filter plus equalizer; the insertion delay of 275ns is used to obtain the correct chrominance-to-luminance timing as required by the decoder chip inputs, i.e. to ensure chroma/luminance alignment.

The response is theoretically flat but because all the capacitor values have been rounded to preferred values and the adaptive f_{sc} notch added, the group delay is not as flat as it could be. However testing with a pulse and step signal, see Fig. 56, shows that the overall performance is good.

To set up this filter, it is best to use a 0-10MHz sweep with markers although a generator with set frequencies can be used. If there is difficulty in setting up it may be necessary to isolate the phase equalizer and obtain the correct performance from the filter and



These six installments of 'Improving colour tv decoding' have been the result of the gathering of information and investigation followed by the collection of much valued advice on how to knock the ideas into shape. I particularly wish to thank Dr Mino Gobetti, for keeping a fatherly theoretical eye on the planning; John Nash of ITCA, for patiently checking and adjusting the worst of the grammatical gaffs, and Cliff White of the BBC for invaluable help on practical aspects of design and construction.

Fig. 52. Amplitude response of chroma band-pass filter used in the circuit of Fig. 34 (March issue). Lower trace shows the 0-6dB area.

Fig. 52 (b). Shows the clean chroma, note the transitions, that can be achieved at the output of this band pass filter.

Fig. 53. Group delay response of the chroma band-pass filter.

Fig. 54. Insertion loss performance of the post modifier/modulator low-pass filter L_8 to L_{12} (Fig. 34 March issue).

Fig. 55. Group delay response of Fig. 34 low-pass filter.

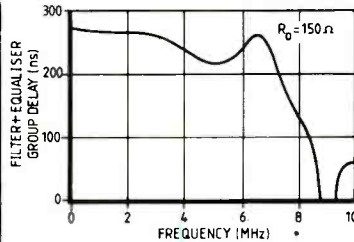


Fig. 56. 2T pulse and step edge. Performance for the low-pass filter shown in Fig. 34.

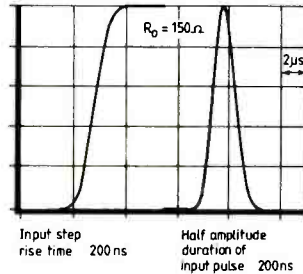


Fig. 57. Pre-sync filter insertion loss response (Fig. 36 March issue).

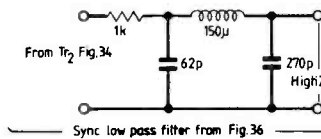
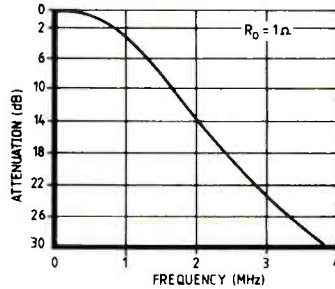


Fig. 58. Pre-sync filter group delay response.

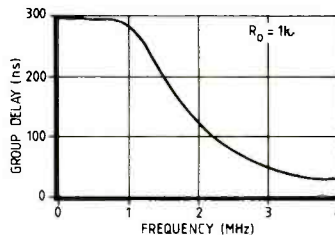


Fig. 59. Ferguson TX10 circuit: component used between the i.f. demodulator i.c. TDA2541 or 3541 and colour decoder i.c. TDA3561A.

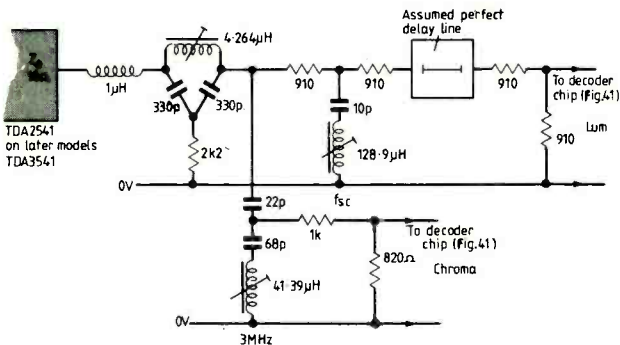
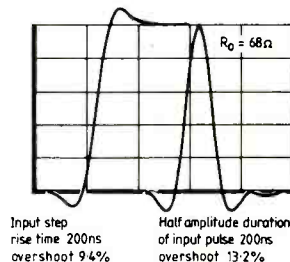


Fig. 60 Insertion loss performance of the 6MHz sound trap and the colour subcarrier notch in luminance path between i.f. and decoder.



equalizer separately before reconnecting. But if all the coils are tested for nominal inductance as stated on the circuit, and good quality 2%, 125V polystyrene capacitors have been used, the circuit should be easy to set up with all elements connected. As most test equipment has 75Ω input and output impedance, resistor networks to match the 150Ω filter can be used, as shown in the item 'Impedance matching' page 36, May issue.

IF output home tv receivers

The network used by the Thorn (Ferguson TX10) 26in. receiver in Fig. 59 has the amplitude performance luminance-signal shown in Fig. 60. At first sight, the network insertion loss curve indicates a good response, but the group delay curve, Fig. 61, shows a rise of delay to 320ns as the amplitude falls to 3dB.

As a result of the colour (f_{sc}) notch and (6MHz) sound trap not being group-delay equalized (giving a rising delay with increasing frequency), the luminance signal has asymmetrical rings, as the pulse and step test waveform in Fig. 62 shows. Since the pulse has a half-amplitude duration of 200ns its spectral bandwidth is within 5MHz. Hence, a notch at 4.43MHz will cause ringing. If the circuit is equalized, the rings will be halved in amplitude and distributed symmetrically about the pulse or step. The asymmetrical rings on a television screen appear as shown in Fig. 63, and will mar all the picture detail in a similar way to multipath ghosting with short delays involved.

Analyzing the chroma path, Fig. 64 shows the insertion loss characteristic. The rising response over the chroma bandwidth ($f_{sc} \pm 1\text{MHz}$) is shaped to provide a high-pass response such that, with the i.f. s.a.w. low-pass filter, a bandpass response is formed for the chroma modulation. Many s.a.w. filters are 3-6dB down as f_{sc} , and the rate of fall is similar to the rising response shown in Fig. 64. The end result is a somewhat narrow bandwidth, which is good for giving low cross-colour (little luminance energy reaching the chroma de-modulator), but is at the expense of very poor chroma risetimes resulting in limited chroma detail (the $f_{sc} \pm 1\text{MHz}$ points are approximately 12dB down). The group delay curve (Fig. 65) shows delay asymmetry about f_{sc} . In the range $f_{sc} \pm 1\text{MHz}$, the insertion delay with increasing frequency has a high rate of change and reverses in slope with a peak-to-peak delay of 300ns. As this is a delay comparable to the period of f_{sc} (225.5ns), these sidebands will, after passing

through the R-Y and B-Y demodulators, result in chroma rise and fall times being mistimed, with pre- or post overshoots; depending on the sideband distribution. There will also be visible moving Hanover-bar effects at the chroma transitions.

Line up of post modifier low-pass filter

The sweep or spot frequency generator can be applied to the powered board (Fig. 34, 36) at its normal video input with the appropriate resistor connected at R_2 as input termination. The filter should then be fed from and terminated in the correct resistances. If the luminance output is driving a 75Ω load, temporarily add 1kΩ across R_{38} and 100μF (6V) across C_{30} , plus a series resistor of 75Ω in the output to suit the input impedance of the test generator. Lift one end each of C_{18} and C_{25} , first adjust L_1 for a minimum output at 8.866MHz displayed on the oscilloscope or spectrum analyzer, then adjust L_2 for minimum output at 4.07MHz. Reconnect C_{18} and adjust L_3 for a maximally flat response over a range of frequencies from ± 1 to $\pm 2\text{MHz}$ about 4.07MHz, or short the delay equalizer L_3 and adjust L_9 for a minimum at 4.07MHz. Insertion-loss response of the equalizer should be flat to within 0.5dB.

Lift one end of C_{13} , short together the collector and emitter of Tr_5 , reconnect C_{25} and adjust L_{12} for a minimum value at f_{sc} (4.43361875MHz).

The remaining inductor, L_{10} , may be adjusted using a return loss bridge (being set for a minimum at 2.93MHz). Alternatively, isolate the output of this equalizer and correct an oscilloscope probe to the input, and adjust for a minimum at 2.93MHz. In practice it is easier to use a pulse and bar waveform or i.t.s. off air and adjust L_{10} for best bar corner shape (square-ness). Remove the collector/base short on Tr_5 and, if used, the 1kΩ across R_{38} and the 100μF in parallel with C_{30} . Reconnect C_{13} .

Pre-sync filter, Figs 57, 58

The pre-sync filter is required to improve the performance of the sync separator and to obtain the correct relative timing of video and 'sandcastle' pulse at the decoder chip blanking/clamping operation point. In order not to produce pre or post-transition overshoots on the filtered signal, the filter is designed to roll off in such a way that the group delay response is flat to the 3dB down point so that the sync separator chip then operates with clean input signals.

The filter operates from 1kΩ

source impedance, is terminated in a high impedance and achieves a minimum insertion loss of less than 1dB. No setting up is needed provided that the correct components have been used.

Philips filter circuit

The circuit of luminance and chrominance filter derived from a Mullard network is shown in Fig. 66 with the luminance amplitude performance in Fig. 67. The offset tapping of the 66µH coil was not made clear in the Mullard book. The luminance insertion-loss curve shows a rising response over the range 1.5 to 2.5MHz and a smooth fall to the 4.433MHz trap. The 3-4dB rise provides an aperture-correction effect and the smooth fall of the trap minimizes the group-delay distortion as shown in Fig. 68. This is readily equalized by one 'A' type equalizer section.

The overall effect of the notch and the equalizer results in overshoots and symmetrical rings. The overshoots occur because of the rising amplitude response; both the rings and overshoots are made symmetrical by having adequate group delay equalization. The pulse and step waveforms are shown in Fig. 69. The size of the symmetrical overshoots provides horizontal aperture correction (by operating along the tv line to enhance the horizontal detail of the picture i.e. vertical edges are sharper). The width of these overshoots is such that, when added to the broadcasters aperture-corrected pictures, they appear as a rather heavy thick outline — typically seen at the sides of faces or dark to bright clothing boundaries. For pictures that are not good initially and for smaller screens (less than 20in) this size of overshoot is beneficial; it would also help receivers that are operating at the end of a long transmission chain.

The chroma-patch circuit is shown in the lower part of Fig. 66, with its insertion loss characteristic in Fig. 70. The near symmetrical response (to 6 dB points) about f_{sc} is suitable for a flat amplitude response video source. If the video signal is fed from a typical domestic receiver i.f. then, if the centre frequency tuning point of the circuit is raised (so that the i.f. and filter responses together provide a symmetrical bandwidth), the 7.8 kHz twitter at chroma transitions will be minimized. Fig. 70 (s.a.w. filter) and Fig. 64 (TX10

chroma circuit) show that the rates of high-pass and low-pass cut off are nearly the same. Hence, since these responses are effectively in tandem a chroma bandpass results, albeit a somewhat narrow one.

The group-delay curve of Fig. 71 shows that both the upper and lower sidebands occurring at chroma transitions are time advanced with respect to the centre frequency f_{sc} ; the resulting amplitude and/or error is illustrated by the vector diagrams in Fig. 72.

Alternative filters designed as second option to comb filter circuit of Fig. 34

As a starting point it is assumed that all recently-designed receivers will use s.a.w. filters with the subcarrier down by between 2 and 6dB. This is equivalent to 35MHz in the i.f. bandpass as shown in Fig. 73 and represents a typical s.a.w. filter. Components such as RW 153P SY 153A (SW155 with f_{sc} 1dB down should be available later this year from SignalTech.) are designed for the UK PAL system I. With the comb filter replaced by an f_{sc} notch, and assuming a s.a.w. i.f. filter is in use, there will be no useful luminance energy above 4.1MHz. Fig. 74 shows the insertion loss of the notch which has a width and depth chosen as a compromise between conflicting picture effects. A narrow shallow notch would provide greater luminance resolution, because less luminance spectrum is removed, but would allow more of the sidebands generated at chroma transition through; a sharp cornered cut-off would result in rings being added to the luminance pulse and step components.

After subjective tests viewing differently shaped notches and with good quality live studio programmes, it was decided that a gentle roll off ± 650 kHz 3dB points, 16-18dB deep seemed a good compromise. The unequalized group delay curve of the notch in Fig. 74 is shown in Fig. 75. The 100ns in the group delay curve near to 4MHz can readily be equalised as shown in Fig. 76. The circuit of the filter and equalizer is shown in Fig. 77. The insertion delay of the filter is 290 ns and the filter was equalised up to this to suit the luminance/chrominance timing requirement of the decoder chip, ie, for the TDA 3561A or 3560, this is the delay between pin 10 lumin-

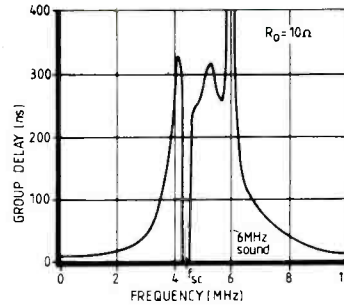


Fig. 61. Group delay response of the luminance path between i.f. output and colour-decoder input.

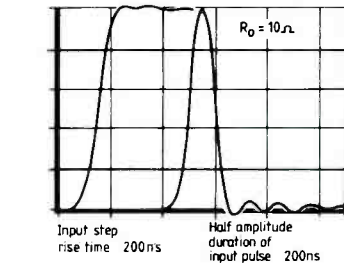


Fig. 62. 2T pulse and step waveforms having passed through the luminance path of i.f. output and decoder input.

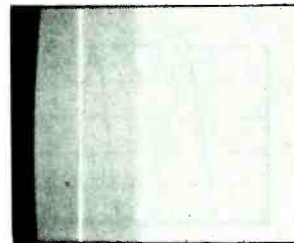


Fig. 63. Television screen display shows asymmetrical rings due to the lack of group-delay equalisation in the f_{sc} notch or sound traps used between i.f. and colour decoder.

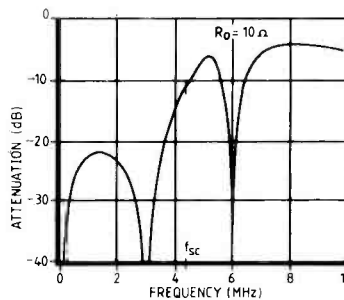


Fig. 64. Chroma path insertion loss characteristic for the network between the i.f. and chroma demodulation (Ferguson TX10 receiver).

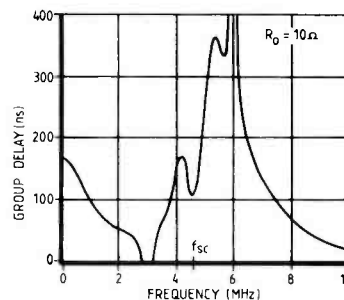


Fig. 65. Group delay response for the chroma output shown in the circuit of Fig. 59.

Fig. 66. Circuit taken from the Mullard book on consumer i.cs, March 1979. This 'application circuit' is fed with 2.7V pk-pk composite video from the i.f. stage and supplies 0.45V (sync bottom to white level) to the luminance input on pin 10.

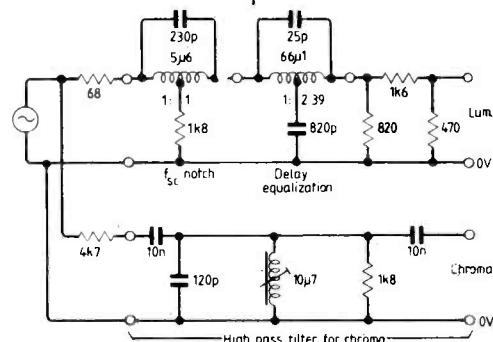


Fig. 67. Insertion-loss performance for the luminance path containing colour subcarrier notch and a delay equalizer.

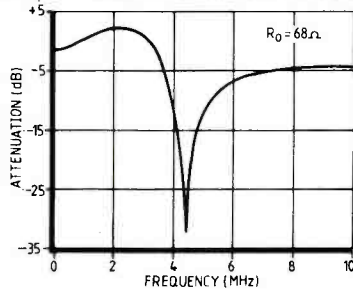


Fig. 68. Group-delay response of the luminance path up to the colour decoder chip, pin 10. In the full circuit of a receiver, a 270ns luminance delay line is also used; the performance of this is looked at separately.

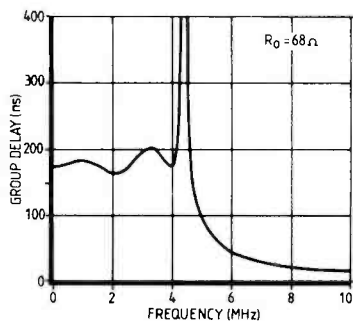


Fig. 69. 2T pulse and step output waveforms for the luminance path of Fig. 66, showing symmetrical overshoots obtained by good group-delay equalization.

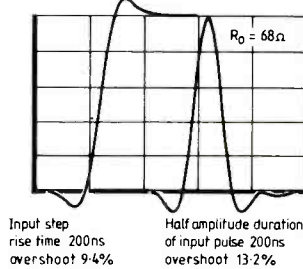


Fig. 70. Mullard/Philips chroma path insertion-loss characteristic for the network connected between i.f. output and chroma demodulator input (pin 3 for the TDA3560 and the more recent TDA3561A).

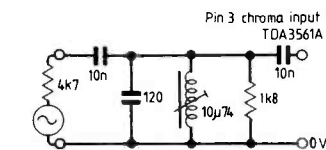
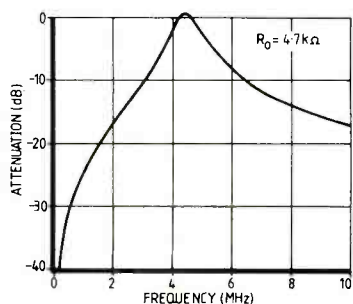
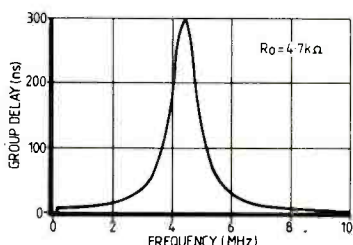


Fig. 71. Group-delay response for chroma circuit shown in Fig. 66 (lower part).



A postscript article will introduce an up-dated approach to the tuner/i.f. section of a home receiver, introducing recent i.f. surface-wave filters and the necessary adjustments to the i.f. output and decoder input filtering. It will briefly outline a tv tuner/i.f. demodulator marketed by SPT Video and built to

BBC design RC1/511 (about £1,000 to buy). And other methods of picture enhancement will be included, for instance scan/velocity modulation (turbo-scan is the Sony name for it), and use of a controlled switched equalizer with the signal taken from taps on a delay line.

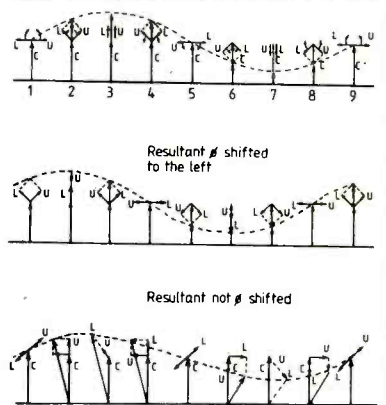


Fig. 72. Vector diagrams for double sideband amplitude modulation as applied in the chroma circuits. Broken line represents modulating voltage e.g. h.f. sideband. Balanced modulators are used for R-Y and B-Y modulation, see Fig. 6 (December). Carrier C is reinserted at demodulation by the burst-locked oscillator. Middle diagram shows the condition with both sidebands early. The error results in pre-shoots on chroma pulse and step waveform. Bottom diagram shows condition with one sideband early and one late, thus reducing resultant amplitude error and giving good pulse and step shape. Fig. 52(b) and 53 give similar performance.

Fig. 73. Typical s.a.w. insertion-loss and group-delay performance. Makers are vague about group delay performance. This affects bar corners of i.t.s. bar and on picture appears as a smear after sharp transitions.

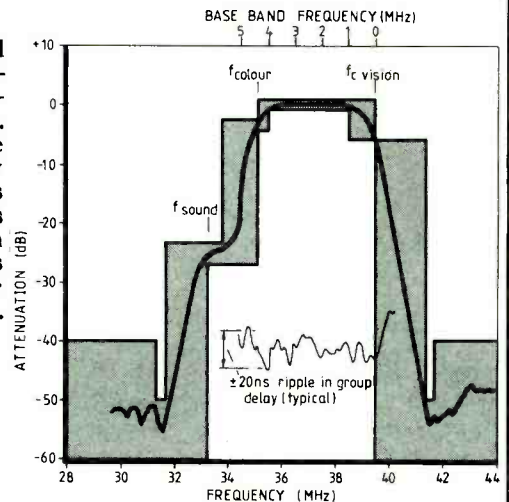


Fig. 74. Insertion loss of f_{sc} notch for use in luminance channel for the alternative circuits.

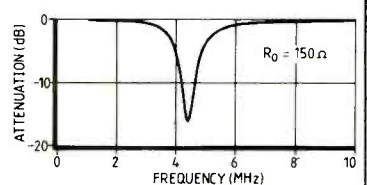


Fig. 75. Notch filter unequaled group-delay response.

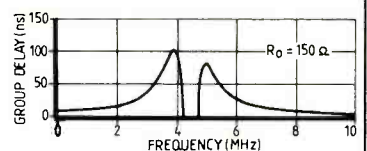
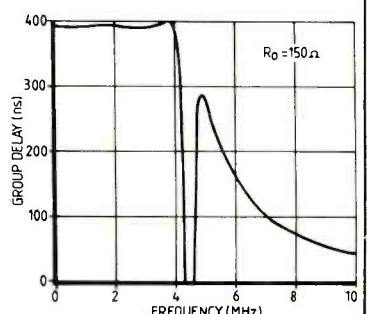


Fig. 76. Luminance notch filter with group-delay equalizer sections added one A and two Bs.



ance input and pin 3 chroma input. No luminance delay line is therefore required. The 2T pulse step performance of this equalized notch filter is shown in Fig.78. The overshoots of 2.1% for the pulse and 0.3% for the step are only visible when viewing electronically-generated test waveforms. This is because the group delay response is flat within a few nanoseconds up to 4MHz the amplitude response has fallen by 5dB, and continues to fall steeply. The group delay performance is therefore not important beyond this point. A suitable filter for the chroma path is an adaptation of the TX10 circuit. The width of the 6MHz trap can be reduced by increasing the capacitor values and reducing the inductors from 4.264 to 0.6μH. More importantly, this modification minimizes the group-delay effects in subcarrier area. Comparison of Fig.64 and 65 with 79 and 80 shows the modification. In the important area f_{sc} 40.5MHz there is now no group-delay reversal and a reasonable degree of symmetry exists. This improves the quality of the chroma waveform (after demodulation) at the chroma transition points. The revised circuit is shown in Fig. 81. The chroma band-pass characteristic is determined by the s.a.w. filter response (Fig.73) as it falls to the 'sound shelf', and by the high-pass response of the network between the i.f. and PAL decoder (Fig.79) If the additional circuit board of Fig.34 is used it will be further modified by the gaussian band-pass response (Fig.52) which has a reasonably symmetrical group delay response between the 0 to 6 dB down point. The sidebands of the chroma signal at the input of the demodulator have a fair degree of both phase and amplitude symmetry. Fig.82 shows the filter and the high-pass responses together representing the first two chroma-shaping components; the gaussian band-pass maintains the amplitude symmetry. The phase symmetry of the chroma sidebands is mainly determined by the two LC networks because the group delay response of the s.a.w. while mostly at low level (typically ± 10 ns), shows a number of high rate-of-change spikes. The phase response is mainly determined by the filter group delay curve, Fig.80, which shows that the sidebands are similarly leading and lagging either side of subcar-

rier f_{sc} . (Note: amplitude modulation, as used for chroma signals, generates symmetrical sidebands.) Where the receiver has a good tuner and i.f. response, or uses a s.a.w. filter which is of the order of the 1dB down at f_{sc} , then the extra board containing the circuit of Fig.34 (WW March issue) will result in the gaussian band-pass characteristic also affecting the chroma response. The lower trace of Fig.52 (WW April issue) shows that the amplitude symmetry of this band-pass filter is adequate. The group delay response, Fig.53, when added to the group delay response of the high-pass network (Fig.80 WW April issue), results in a reduced overall group delay error as shown in Fig.83.

Luminance delay lines

These should ideally be flat from 0-5.5 MHz and have zero group delay error. The performance of a selection of delay lines taken from receivers, professional monitors and video recorders is shown in Fig.84. The performance of these delay lines is adequate for the video recorders, where the bandwidth is of the order of 1.5 to 2.5 MHz, but in the application of an improved PAL colour decoder only the fourth delay line illustrated (using a glass tube) was worth considering. The order of delay required at the DL1 position in Fig.34 (March) is 240ns. By dismantling a tube delay line to adjust the turns (removing delicately about 20% of the 2 thou/48swg/0.04mm wire), a fair performance was obtained as shown in Fig.85 (delay line E). Delay line D would be adequate for the DL2 position in Fig.34.

A 240ns version of the delay line is made by Sprague part no. W3600.Z.145, colour-coded purple body with black rings and has a Z_0 of 1kΩ. However these are difficult to acquire: Sprague say a minimum order of a 1000 is required, they want a turnover of £15,000 p.a., and that no UK distributor has the product! From Mullard/Valvo, however, a 340 ns undipped delay line was obtained. After removing a proportionate number of turns to obtain the required delay ($\frac{60\text{mm}}{340\text{ns}} = \frac{x}{240\text{ns}}$) i.e. $x = 42$ mm, the results shown in Fig.85 (delay line E) were obtained. If this modified delay line is used, the chroma cancellation at Tr_8 emitter is less effective than for a perfect delay. This is so because,

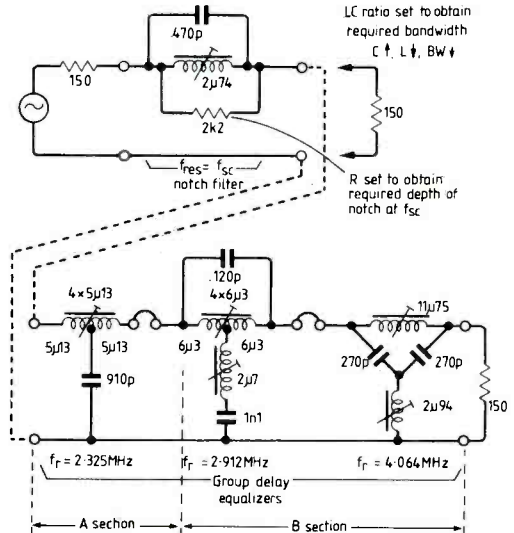


Fig.77. Circuit of notch filter with addition of a three-section equalizer.

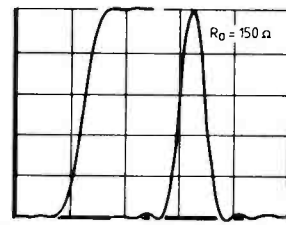


Fig.78. 2T pulse and step performance of the luminance notch filter with equalizer.

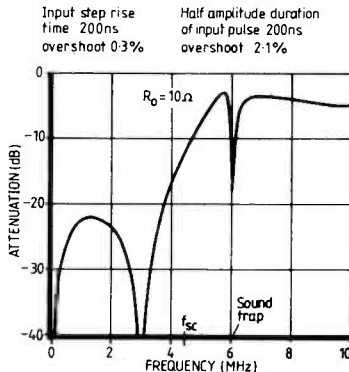


Fig.79. Chroma path insertion loss with the modified 6MHz sound trap.

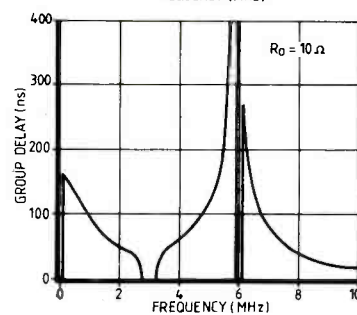


Fig.80. Group delay performance of the sound trap and chroma path filter.

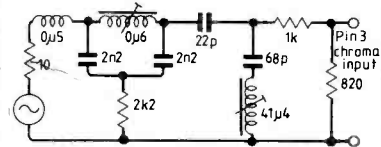


Fig.81. Circuit used in the alternative circuits for the chroma path up to the chroma decoder. L/C ratio determines notch width (see WW October 1952).

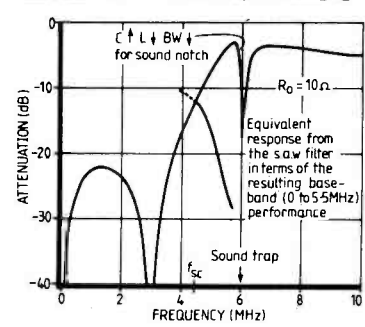
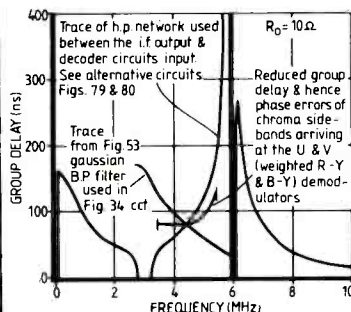


Fig.82. The surface wave filter characteristic, as it affects the baseband response, drawn together with high-pass filter curve from Fig.79, indicates the approximate band-pass shape required for chroma sideband symmetry.

Fig. 83. Chroma path group delay resulting from the high-pass network with 6MHz sound trap, Fig.81, and the gaussian filter of Fig.79.



over the range ± 1 MHz about f_{sc} , the delay line transverses from -8 to $+14$ ns whereas the gaussian filter performance (Fig.53) is $+20$ to -20 ns. Thus, the error is in the opposite direction. Adding $15 \mu\text{H}$ Painton/Sigma/RS chokes at each end of the delay line will redistribute the delay ripple and could change the shape across the chroma band to advantage as shown in lower traces of Fig.85.

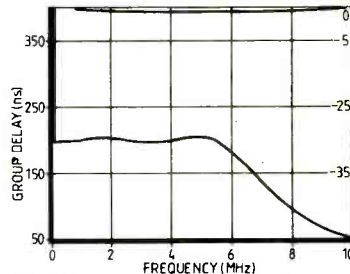
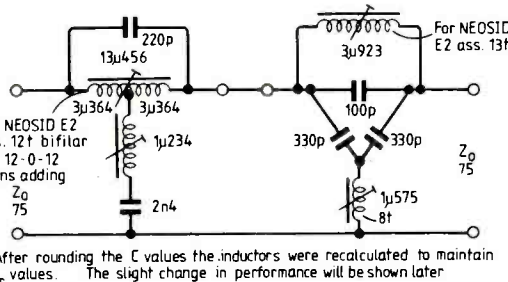
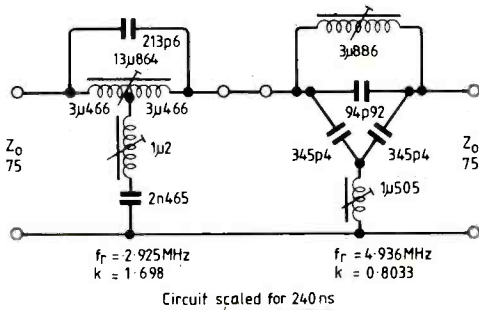
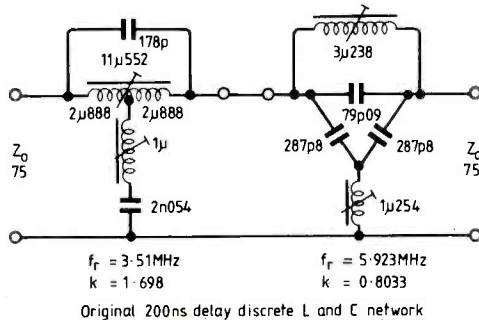
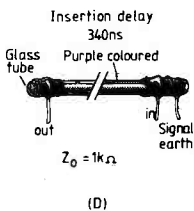
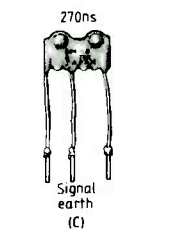
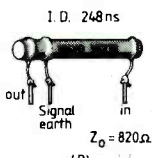
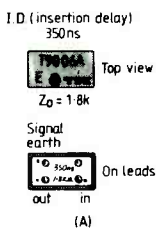
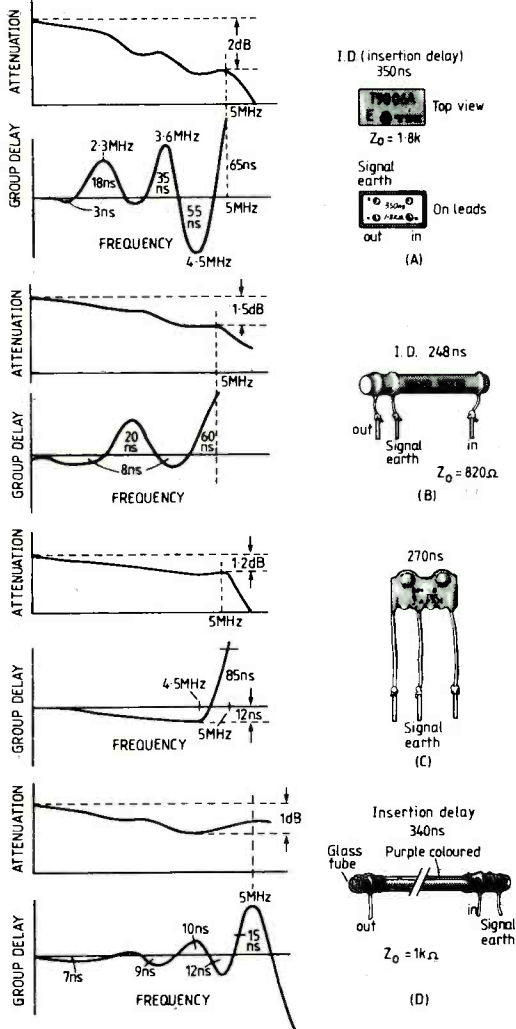


Fig.86. Insertion loss and delay performance of discrete LC delay line.

Fig. 84. Performance of four video delay lines (A, B, C and D) used in receivers, colour monitors or video recorders.



More luminance delay line options

In the prototype, two Matthey or Bal video delay lines are used each programmable in 5 ns steps up to a total of 155 ns because these give the best performance. An internal amplitude equalizer results in $1.8 k\Omega$ appearing to the signal earth across the line. So as to minimize d.c. disturbance if using these components, balance this by adding $1.8k\Omega$ to the $+12v$ raise for each line used. From agents or distributors the Matthey lines cost up to £36 each; if winding coils is possible the delay line can instead be constructed with discrete L and C components. From a past project a 200 ns delay circuit was utilised, giving performance as shown in Fig.86. By suitable scaling for 240 ns, L and C values are multiplied by 1.2 to divide the frequencies by the same factor. The original (200 ns) and the modified (240 ns) circuits are given in Fig.87 with the bottom circuit showing capacitors as preferred values. Insertion loss response is within 0.2 dB to 10MHz but the delay ripple, with the preferred C values, causes a slight loss in performance of the pulse-and-step test.

The 75 ohm characteristic impedance of the delay line matches most test equipment. However, the delay network can be tested within the circuit of Fig.34 as was the output filter connected between R_{23} and R_{36} . The components can again be scaled to give a characteristic impedance (Z_0) of 220Ω ; then R_9 and C_9 in Fig.34 would not be required. R_6 and R_7 should each then be replaced by 440Ω (or pairs of 220Ω). To scale Z_0 , L values are multiplied by $\frac{220}{75}$ and C values by $\frac{75}{220}$ (using the values from the middle circuit of Fig.87) before rounding the results to preferred values. (i.e. C is set to preferred values and L is then adjusted to return to the resonant frequencies).

Fig. 87 (above right). Two type B group delay sections providing 200 to 240ns of insertion delay, the value required in delay line position DL₁ Fig.34, March issue.

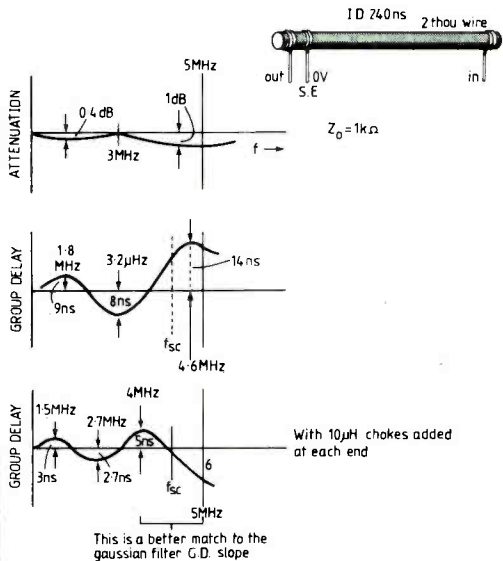


Fig.85. Rewound delay line (E), from which turns were removed until the correct delay value was obtained.

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SEMICONDUCTORS

AAL19 0.10	ASZ15 1.20	BC173 0.11	BD132 0.48	BF257 0.27	GEX51 5.00	OAZ207 1.50	OC205 2.75	ZTX504 0.21	2N1671 5.00	2N3819 0.30
AA19 0.17	ASZ16 1.10	BC177 0.28	BD135 0.40	BF259 0.28	G13M 1.50	OC26 2.50	OC206 2.50	ZTX508 0.24	2N1681 0.31	2N3820 0.39
AA30 0.17	ASZ17 1.00	BC178 0.28	BD136 0.40	BF336 0.34	K5100A 0.45	OC22 2.50	OC207 2.50	ZTX510 0.25	2N1694 0.05	2N3823 0.60
AA313 0.15	ASZ20 2.30	BC179 0.28	BD137 0.40	BF337 0.33	MJE340 0.60	OC23 4.00	OC208 2.00	ZTX511 0.25	2N1694 0.05	2N3866 1.00
AAZ15 0.15	ASZ21 2.50	BC182 0.11	BD138 0.48	BF338 0.36	MJE371 0.71	OC24 3.00	OC209 2.00	ZTX512 0.25	2N1694 0.05	2N3904 0.17
AAZ17 0.15	ASZ22 2.50	BC183 0.11	BD139 0.48	BF381 2.00	MJE372 0.71	OC25 1.00	OC210 2.00	ZTX513 0.25	2N1694 0.05	2N3906 0.17
AC107 0.55	AU113 2.50	BC184 0.11	BD140 0.50	BF528 2.25	MJE520 0.47	OC26 1.50	R2010B 2.00	ZTX514 0.25	2N1694 0.05	2N4058 0.20
AC125 0.25	BA145 0.13	BC212 0.11	BD141 2.00	BF561 2.00	MJE521 1.73	OC28 2.00	TI344 0.27	ZTX515 0.25	2N1694 0.05	2N4059 0.20
AC126 0.25	BA148 0.15	BC213 0.11	BD183 0.80	BFW10 0.97	MJE525 1.30	OC29 2.00	TI344 0.27	ZTX516 0.25	2N1694 0.05	2N4060 0.16
AC127 0.25	BA154 0.10	BC214 0.11	BD2137 0.54	BFW11 0.96	MPE102 0.35	OC36 1.50	TI209A 0.43	ZTX517 0.25	2N1694 0.05	2N4061 0.16
AC128 0.30	BA155 0.11	BC237 0.11	BD238 0.54	BFX84 0.30	MPE103 0.35	OC41 0.90	TI209A 0.43	ZTX518 0.25	2N1694 0.05	2N4062 0.16
AC141 0.28	BA156 0.10	BC238 0.12	BDX10 0.91	BFX85 0.30	MPE104 0.35	OC42 0.90	TI209A 0.43	ZTX519 0.25	2N1694 0.05	2N4124 0.16
AC143 0.28	BAW62 0.05	BC301 0.33	BD132 2.00	BFX87 0.30	MPE105 0.35	OC43 1.50	TI209A 0.43	ZTX520 0.25	2N1694 0.05	2N4286 0.15
AC144 0.28	BAX13 0.06	BC303 0.34	BD120 2.50	BFX88 0.30	MPSA06 0.26	OC44 0.85	TI209A 0.43	ZTX521 0.25	2N1694 0.05	2N4288 0.18
AC142K 0.35	BAX16 0.06	BC307 0.11	BDY60 2.75	BFY50 0.25	MPSA56 0.28	OC45 0.65	TI209A 0.43	ZTX522 0.25	2N1694 0.05	2N4289 0.18
AC176 0.30	BC107 0.16	BC308 0.11	BF115 0.35	BFY51 0.25	MPSU01 0.53	OC71 0.55	TI209A 0.43	ZTX523 0.25	2N1694 0.05	2N4400 0.11
AC187 0.28	BC108 0.16	BC327 0.12	BF152 0.16	BFY52 0.25	MPSU06 0.65	OC72 1.00	TI209A 0.43	ZTX524 0.25	2N1694 0.05	2N4401 0.11
AC188 0.28	BC109 0.16	BC328 0.12	BF153 0.16	BFY64 0.30	MPSU56 0.65	OC73 1.00	TI209A 0.43	ZTX525 0.25	2N1694 0.05	2N4402 0.11
AC197 1.30	BC113 0.15	BC337 0.12	BF154 0.17	BFY90 0.95	MPSU57 0.65	OC74 1.00	TI209A 0.43	ZTX526 0.25	2N1694 0.05	2N4403 0.11
AC198 1.15	BC114 0.15	BC338 0.12	BF159 0.17	BFY91 0.27	NKT401 3.50	OC75 0.65	TI209A 0.43	ZTX527 0.25	2N1694 0.05	2N4404 0.11
AC199 1.10	BC115 0.18	BCY30 1.25	BF160 0.17	BSX20 0.27	NKT403 2.50	OC76 1.00	TI209A 0.43	ZTX528 0.25	2N1694 0.05	2N4405 0.11
AC20 2.10	BC116 0.19	BCY31 1.50	BF167 0.24	BSX21 0.29	NKT404 2.20	OC77 1.00	TI209A 0.43	ZTX529 0.25	2N1694 0.05	2N4406 0.11
AC21 1.15	BC117 0.23	BCY32 1.50	BF173 0.30	BT106 1.20	OAS 1.20	OC81 0.65	TI209A 0.43	ZTX530 0.25	2N1694 0.05	2N4407 0.11
AC239 2.50	BC118 0.18	BCY33 1.10	BF177 0.35	BT107 400R	OAS 1.20	OC82 1.00	TI209A 0.43	ZTX531 0.25	2N1694 0.05	2N4408 0.11
AD149 0.75	BC120 0.18	BCY34 1.00	BF178 0.35	BU205 1.30	OAS 1.20	OC83 1.00	TI209A 0.43	ZTX532 0.25	2N1694 0.05	2N4409 0.11
AD161 0.35	BC126 0.18	BCY39 3.40	BF179 0.35	BU206 1.50	OAS 1.20	OC84 0.80	TI209A 0.43	ZTX533 0.25	2N1694 0.05	2N4410 0.11
AD162 0.35	BC135 0.15	BCY40 2.80	BF180 0.28	BU207 1.50	OAS 1.20	OC85 1.00	TI209A 0.43	ZTX534 0.25	2N1694 0.05	2N4411 0.11
AF106 0.35	BC136 0.19	BCY42 0.30	BF181 0.28	BU208 2.00	OAS 1.20	OC86 1.00	TI209A 0.43	ZTX535 0.25	2N1694 0.05	2N4412 0.11
AF114 0.75	BC137 0.19	BCY43 0.30	BF182 0.30	BU209 0.40	OAS 1.20	OC87 1.00	TI209A 0.43	ZTX536 0.25	2N1694 0.05	2N4413 0.11
AF115 0.75	BC147 0.12	BCY70 0.17	BF183 0.28	BU216 0.13	OAS 1.20	OC88 1.00	TI209A 0.43	ZTX537 0.25	2N1694 0.05	2N4414 0.11
AF116 0.75	BC148 0.12	BCY71 0.18	BF184 0.28	BU217 0.13	OAS 1.20	OC89 1.00	TI209A 0.43	ZTX538 0.25	2N1694 0.05	2N4415 0.11
AF117 0.75	BC149 0.13	BCY71 0.18	BF185 0.28	BZK61 0.17	OAS 1.20	OC90 1.00	TI209A 0.43	ZTX539 0.25	2N1694 0.05	2N4416 0.11
AF139 0.33	BC157 0.13	BCY72 0.17	BF194 0.14	Series	OAS 1.20	OC91 1.25	TI209A 0.43	ZTX540 0.25	2N1694 0.05	2N4417 0.11
AF186 1.00	BC158 0.13	BCZ11 1.75	BF195 0.12	BY288 0.10	OAS 1.20	OC92 1.25	TI209A 0.43	ZTX541 0.25	2N1694 0.05	2N4418 0.11
AF239 0.39	BC159 0.13	BD115 0.42	BF196 0.13	Series	OAS 1.20	OC93 1.25	TI209A 0.43	ZTX542 0.25	2N1694 0.05	2N4419 0.11
AFZ11 4.00	BC167 0.11	BD121 1.70	BF197 0.14	Series	OAS 1.20	OC94 1.25	TI209A 0.43	ZTX543 0.25	2N1694 0.05	2N4420 0.11
AFZ12 4.00	BC171 0.11	BD123 2.80	BF200 0.40	Series	OAS 1.20	OC95 1.25	TI209A 0.43	ZTX544 0.25	2N1694 0.05	2N4421 0.11
AS226 0.25	BC171 0.11	BD124 2.00	BF201 0.40	Series	OAS 1.20	OC96 1.25	TI209A 0.43	ZTX545 0.25	2N1694 0.05	2N4422 0.11
AS227 0.90	BC172 0.11	BD131 0.44	BF244 0.28	Series	OAS 1.20	OC97 1.25	TI209A 0.43	ZTX546 0.25	2N1694 0.05	2N4423 0.11

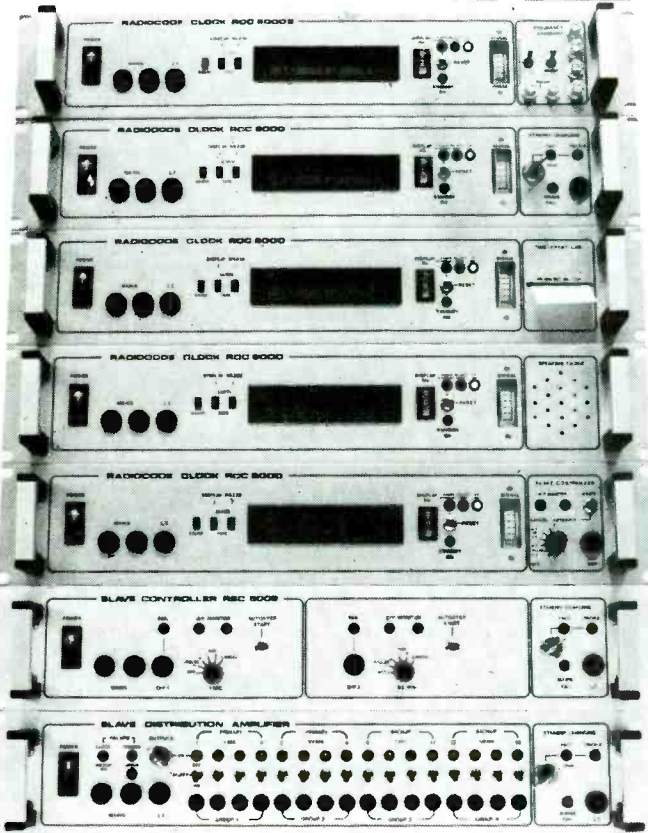
VALVES

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A2087 13.50	E180C 10.50	EF86 1.75	GU51 15.35	OZ4 3.50	QY125 5.00	UF42 2.10	4-400A 87.00	6CH6 13.00	12AY7A 4.00	5654 3.00
A2134 17.50	E180F 10.20	EF89 2.50	GU52 30.00	PC86 2.50	QY-250 68.00	UF80 1.75	4B3 20.00	6CL6 3.75	12BA6 3.50	5651 4.45
A2293 16.00	E280F 22.51	EF91 2.95	GU53 25.40	PC88 2.50	QY-440 74.20	UF85 1.75	4C35 78.00	6CW4 8.00	12BA6 2.50	5670 4.50
A2426 27.50	E280G 22.51	EF92 6.37	GU54 44.50	PC95 1.75	QY-500 175.00	UF89 2.00	4CX250B 45.00	6D2 1.50	12BE6 2.50	5675 28.00
A2521 25.00	E280H 22.51	EF93 1.50	GY501 3.00	PC97 1.75	QY-3000A 4.00	UL41 3.50	4CX350A 73.00	6DK6 3.00	12BH7 2.75	5687 3.50
A2900 15.00	E430C 7.50	EF98 2.00	GZ31 4.75	PC98 1.50	R10 420.00	UL84 1.75	4X150A 60.00	6E8B 4.75	12B77 3.00	5696 4.50
A3343 45.00	E430E 32.25	EF183 2.00	GZ34 3.00	PC98 2.00	R17 3.00	UL85 2.25	5B255M 35.00	6EA8 3.00	12E1 20.00	5718 7.50
AZ31 2.75	EACB0 1.25	EF184 2.00	GZ37 4.75	PC98 1.75	R18 3.00	VL5631 15.00	5C22 160.00	6E6 3.00	12E11TT 28.00	5725 5.50
BK448 114.90	EAC91 3.50	EF80S5 15.00	KT61 5.00	PC189 2.50	R19 9.24	XG1-2500 55.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5726 11.37
BK484 155.35	EAC92 3.50	EF80S6 15.00	KT66 12.00	PC189 1.60	R20 2.50	XG2-6400 141.90	5J180E 1650.00	6F23 1.60	12E14 65.00	5727 7.05
BS90 58.00	EAF01 2.00	EK90 1.75	KT77 Gold 9.00	PC189 1.60	RG3-250 32.68	XG5-500 26.60	5J180E 1650.00	6F23 1.60	12E14 65.00	5728 11.37
BS810 60.00	EB91 1.50	EL32 2.50	KT78 15.00	PC189 1.75	RG3-1250 59.50	XG6-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5729 7.05
BT5 58.95	EB93 2.50	EL34MU1 4.00	KTW62 2.50	PC189 1.75	RG4-1250 61.60	XRI-1600A 102.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5730 7.05
BT17 151.00	EB94 2.50	EL36 1.75	KTW63 2.50	PC189 1.75	RG4-3000 99.45	XRI-1600A 102.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5731 7.05
BT19 44.05	EB95 1.50	EL41 2.50	M8079 12.34	PC200 3.25	RG5-250 32.68	XRI-3200 81.97	5J180E 1650.00	6F23 1.60	12E14 65.00	5732 7.05
BT29 349.15	EB90 1.25	EL42 2.50	M8080 8.25	PC201 3.25	RG5-1250 45.75	XRI-3200A 81.97	5J180E 1650.00	6F23 1.60	12E14 65.00	5733 7.05
BT69 354.80	EBF8C 1.50	EL81 5.25	M8081 9.82	PC201 3.25	RG5-1250 45.75	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5734 7.05
BT95 129.90	EBF83 1.75	EL83 6.00	M8082 9.69	PC202 2.50	RG6-1250 59.50	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5735 7.05
CB131 4.00	EBF89 1.50	EL84 2.25	M8083 8.58	PC202 2.50	RG6-3000 99.45	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5736 7.05
CL33 4.00	EBL31 4.00	EL85 2.25	M8084 10.43	PC202 2.50	RG6-3000 99.45	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5737 7.05
CY31 3.00	EL30 1.25	EL90 2.50	M8079 12.34	PC202 3.25	RG6-1250 59.50	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5738 7.05
CIK 20.00	EC91 8.00	EL91 9.69	M8079 8.10	PCL82 2.00	RG6-3000 99.45	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5739 7.05
CV 22.00	EC92 1.75	EL95 2.00	M8079 6.15	PCL83 3.00	RG6-3000 99.45	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5740 7.05
DA1 22.00	EC157 380.00	EL156 30.00	M8099 8.00	PCL84 2.00	RG6-3000 99.45	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5741 7.05
DA4 25.00	EC33 4.50	EL360 8.50	M8100 9.52	PCL85 2.50	RG6-3000 99.45	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5742 7.05
DA42 18.70	EC35 4.50	EL360 8.50	M8136 10.33	PCL85 2.50	RG6-3000 99.45	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5743 7.05
DAF91 1.75	EC40 4.50	EL509 7.00	M8137 10.33	PCL85/85 2.50	RG6-3000 99.45	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5744 7.05
DAF96 1.75	EC81 1.75	EL821 13.00	M8140 6.00	PDS00 6.00	RG6-3000 99.45	XRI-6400 162.00	5J180E 1650.00	6F23 1.60	12E14 65.00	5745 7.05
DET22 35.00	EC82 1.75	EL822 13.97	M8141 6.50	PEE-40N 45.00	RG6-3000					

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The AM and PM series of Radiocode Clock equipment has been further expanded to include seven new models (from top) 8000S - combined clock, frequency standard and optional stopclock. **Internal standby power supply** - with dual rate constant current charger. **Time-event log** - prints hours, minutes, seconds, milliseconds and day of year, on receipt of a log pulse. **Speaking clock** - time announcement or audio recording. **Slave controller** - total control of single-standard master/slave systems ie one pulse/sec. **Dual standard slave controller** - total control of two different and independent slave systems, ie. one pulse/sec and one pulse/half min. **Slave distribution amplifier** - maximum flexibility for the largest master/slave installations requiring dual standard operation, multiple circuits and complete master/slave backup.

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A continuously expanding range of fully integrated software and hardware is available for both series of Radiocode Clock equipment. Standard options now include:

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- FSK record/replay system
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- Time code generators
- Intelligent slave systems
- Standard frequency outputs
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- Calibrated systems for increased accuracy

Radiocode Clocks Ltd*

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(*A Circuit Services Associate Co.)

CIRCLE 24 FOR FURTHER DETAILS.

MARCONI SIGNAL GENERATORS
TF2002A/S (illustrated) 10kHz-72MHz AM/FM £750
TF2002. As above but AM-only. £450

MARCONI TF1066B AM/FM Generator. 10-470MHz. 0.2uV-200mV output. FM Deviation up to ±100kHz.

MARCONI TF995A/5 AM/FM Generator. Narrow deviation model 995 covering 1.5-220MHz. £450. TF2015. 10-520MHz. AM/FM. TF144H. AM 10kHz-72MHz £295.

MARCONI TF1064B/5 AM/FM Signal generator covering in three ranges 68-108, 118-185 and 450-470MHz. FM fixed deviations of 3.5 & 10kHz. AM fixed 30%. £225

'DOLBY' NOISE WEIGHTING FILTERS
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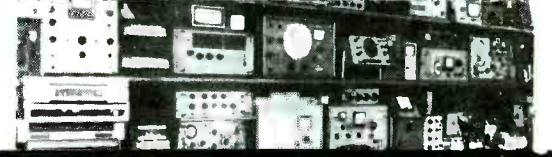
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Brand new stock of 'ASTROSYN' Type 20PM-A055 stepper motors. 28V DC. 24 steps per rev. 15 oz-in torque @ 100PPS. Body length 2 1/2", diameter 2", shaft 1/4" diam x 4 1/4" spirally threaded. Weight 16oz. Price each £15 (p&p 50p). Connections supplied. INC. VAT.

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MARCONI TF2600. Twelve ranges 1mV-300V FSD. Wide-band to 10MHz.
MARCONI TF2603. Frequency range 50kHz-1.5GHz. High Sensitivity from 300uV.
MARCONI TF2604. Electronic Multi-meter. AC/DC 300mV Full scale to 300V (1kV DC). Resistance ranged. AC Frequency range 20Hz-1500MHz.

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MARCONI TF1313 1/4% LCR Bridge
MARCONI TF868 LCR Bridge
MARCONI TF2604 Electronic Multi-Meter
MARCONI TF893A Audio Power Meters £85
MARCONI TF2502 RF Power Meters. DC-1GHz. 10w fsd £350.
MARCONI TF2701 In-Situ Universal Component Bridge £250.
HEWLETT-PACKARD 3450A Multi-Function Digital Multi-Meter.
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TEKTRONIX 2901 Time-mark Generator.
ROHDE & SCHWARZ Resonance Frequency Meter 470MHz-2.5GHz.
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AIRMEC Display Oscilloscope 279. 4-trace, 14x10" CRT £195.
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8" WINCHESTER
UNITED PERIPHERALS model 3100 Mini-disc drives (3 x 8" sealed platters) capable of over 19MBytes storage. External power supply requirements are 24V @ 3A and 5V @ 4A. Little used condition, believed OK but at the unbelievable price of just £125 are sold without guarantee. Price inclusive of VAT and carriage and copy of user-handbook.

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8" Shugart type SA800 Floppy disc drives. Small quantity available, single-sided up to 800KBytes of storage. Power requirements, 5V @ 1.3A. Little used, excellent condition. PRICE £90 - inclusive VAT and carriage and copy of user-handbook.

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TELEONIC SW2000 with 500-900MHz plug-in £175
TELEONIC SW2000 with 0-13MHz plug-in £150

FILE MANAGER SYSTEM MODEL 4907 Option 31 (Third disc drive). 4051 Graphic System compatible. GPIB (IEEE 488-1975) compatible.

PLEASE NOTE. All the pre-owned equipment shown has been carefully tested in our workshop and reconditioned where necessary. It is sold in first-class operational condition and most items carry a three months' guarantee. For our mail order customers we have a money-back scheme. Repairs and servicing to all equipment at very reasonable rates. PLEASE ADD 15% VAT TO ALL PRICES.

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New Stock

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DELIVERY (48Hrs) + £10 + VAT.

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ALL PRICES NOW INCLUDE VAT. CARRIAGE + £2 EACH.

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'TORIN' Type U62B1. 230V Cap'Start (supplied), very powerful (200W. 3,000rpm) centrifugal fans for large rack cooling or enclosure extraction applications. Overall dimensions 20x12 cms, outlet 6x4 cms. BRAND NEW. Surplus stock. £15 each inc. VAT, pp £1.50.

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- ★ 4 1/2" size, brand new £6. Postage each + 50p please.

WWW10

CIRCLE 19 FOR FURTHER DETAILS.

TRANSEL DOT MATRIX PRINTER Compact Serial Interface 230V. With info. £85 ea	51 B&K LEVEL RECORDER 2305, solid state. £400
TELETYPE ASR33 — DATA DYNAMIC 390 (Printer, Keyboard, Punch & Reader) RS232 £75	52 B&K MICROPHONE AMPLIFIER 2603 £200
RACAL MODEM type 2200/24 £100	53 B&K RANDOM NOISE GEN 1402 £125
TRISEMATRONS type 2202 Modem £70	54 B&K RMS AUDIO VOLTMETER 2410 £40
CREEO 75 TELEPRINTER. Very good condition £25 ea	55 B&K MICROPHONE 4111 with stand and cable. £35
9" MONITOR Cased. Non-standard, with info £20 ea	61 B&K AUDIO FREQ SPECTROMETER 2109 with level recorder 2304 £150
12" MONITOR Cased. Non-standard, with info £15 ea	65 WAYNE KERR UNIVERSAL BRIDGE B221 Mk 3 (meter adaptor) with low imp adaptor 0221 Mk 3 £75
AZTEC 20" Black and white MONITOR. Video In TV Style 20" MONITOR. Black and white. Video In £50 ea	67 WAYNE KERR UNIVERSAL BRIDGE B221 with low imp adaptor 0221 £35
	68 WAYNE KERR COMPONENT BRIDGE B521 £45
	69 WAYNE KERR VHF ADMITTANCE BRIDGE B801 £125
	70 WAYNE KERR AF SIG GEN S121 10Hz-120KHz £40
	72 ADVANCE PULSE GENERATOR PG52B £350
	74 ADVANCE DUAL STAB DC PS P.P.3 0-300V-1A twice Metered. £50
	75 SOLARTRON DVM A223 AC/DC/Dhm 4 1/2 digit £90
	76 AVO MULTIMETER CT471A (Ex-Ministry). £40
	79 AVO MULTIMETER 7X £25
	80 AVO MULTIMETER 8s from £45
	81 AVO TRANSISTOR TESTER TT169 with leads. As new (P&P £2). £20
	82 AVO VALVE CHARACTERISTIC METER VCM163 with data £250
	86 AIRMEC MODULATION METER 210 3-3000MHz AM/FM indicator with low imp adaptor 0221 Mk 3 £95
	90 BRANDENBURG POWER SUPPLY 374SEL 0-1000V £175
	91 BRANDENBURG POWER SUPPLY PM2500R 0-2.5kV £25
	95 TAYLDR INSULATION TESTER 130C 500V Max (P&P £3) £25
	97 GREEN SYNTHESISED DIGITAL SIGNAL GENERATOR TG1900 1Hz-9.9MHz Sine Square £600
	410 MARCONI SIG GEN TF2002B 10kHz-88MHz AM/FM £500
	411 MARCONI SIG GEN TF2012 400-520MHz FM £350
	412 MARCONI MOD METER TF2300S 2-1000MHz AM/FM £375
	413 S.E. LABS STROBE GMB £125
	414 RACAL/AIRMEC SIG GEN 365A1-320MHz AM/FM £325
	375 B & K TAPE RECORDER type 7001 £600
	380 H.P. SHF SIG GEN 620A7-11GHz £225
	381 H.P. CALORIMETRIC POWER METER 434A DC-12.4GHz 10mW-10W £250
	383 H.P. RF MILLIVOLTMETER 411A 500kHz-1GHz 10mW-10W £150
	367 MARCONI DIFF DC VOLTMETER TF2606 0-1100V £275
	390 GR FREQ METER & DISCRIMINATOR 1142-A £200
	392 CLAUDE LYONS VOLTAGE STAB TS2 AC 240V 12A £100
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SALE of TEST EQUIPMENT **1/2 PRICE!**

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£365 +15% VAT +£5 Securicor

The YC1000L is a laboratory grade instrument with versatile microprocessor control. It includes: a frequency (10Hz-600MHz, 0.02 ppm), a period (0.1S to 0.1uS), and a pulse counter (0-99,999,999, TTL level), a voltmeter (AC or DC to 999V, 3 ranges), a thermometer (remote sensor -29.0 to +99.9°C) plus a precision timer (24 hour clock providing: event or period, (local or remote) and alarm functions). Display is via 8 large fluorescent green digits and/or the inbuilt 5X7 (20 characters line 2 line second) Dot Matrix thermal printer.

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 SUITABLE FOR: TANDY · BBC · ORIC · NASCOM · GEMINI · ACORN · NEW BRAIN · DRAGON · ETC. ETC.
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 230/240V AC plus 8-0-8V 4A
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 size approx 4 1/2" dia x 1 1/2" high
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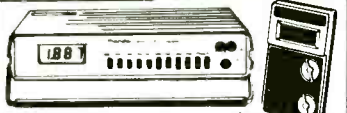
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up to 50KHz, 0.05% basic **£175.00**

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METEX 3000 30 range 10A AC/DC 20 Meg ohm (R) **£33.00**
6010 28 range 10A AC/DC 20 Meg ohm (PB) **£33.00**
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(UK C/P 65p). Size 110 x 45 x 185mm
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to 1000V AC 50uA to 10A DC, 3uA to 10A AC
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typical) **£115.00**
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(UK C/P 65p)
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10 Meg ohm **£20.83**
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10A AC/DC 100 Meg ohm **£29.13**
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	Budget	Deluxe	Deluxe	GARRARD
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FAMOUS LOUDSPEAKERS

MAKE	MODEL	SIZE	WATTS	OHMS	PRICE	POST
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GODDMANS	HIFAX	7 1/2 x 4 1/4	100	8	£30	£2
GODDMANS	HB WOFFER	8in	60	8	£12.50	£1
WHARFEDALE	WOFFER	8in	30	8	£9.50	£2
CELESTION	DISCO/GROUP	10in	50	8/16	£21	£2
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GODDMANS	HPD/DISCO	12in	120	8/15	£29.50	£2
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3amp, 6, 8, 10, 12, 16, 18, 20, 24, 30, 36, 40, 48, 60		£12.50	£2
5-8-10-16V. 1/2amp	£2.50 £1	0-8 12V 5amp	£5.00 £1
6V. 1/2amp	£2.00 £1	15-0-15V. 1amp	£5.00 £1
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9V. 3amp	£4.00 £1	20-0-20V 1amp	£3.50 £1
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9-0-9V 1amp	£3.50 £1	20-40-60V 1amp	£3.50 £2
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12V 3amp	£4.50 £1	17-0-17 2a	£4.00 £2
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32/500V	95p	50+50-50/350V	95p
125/500V	£2	8+8/500V	£1
		8+16/450V	75p
		16+16/350V	80p
		32+32/350V	85p
		16+16/450V	£1
		50+50/300V	50p
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BAKER LOUDSPEAKERS					
MODEL	INCHES	OHMS	WATTS	TYPE	PRICE
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MIDRANGE	10	8	100	MID	£25
MAJOR	12	4-8-16	30	HI-FI	£16
SUPERB	12	8-16	30	HI-FI	£26
WOFFER	12	8	80	HI-FI	£25
AUDITORIUM	15	8-16	60	Woofer	£37
DISCO/GROUP	12	4-8-16	45	PA	£16
DISCO/GROUP	12	4-8-16	75	PA	£20
DISCO/GROUP	12	8-16	100	PA	£26
DISCO/GROUP	15	8-16	100	PA	£35

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8x5in, £3; 8in, £4.50; 10in, £5; 12in, £6. 8in 25W £6.50. 60W £12.50
15 ohm, 2 1/4in, 3 1/2in, 5x3in, 6x4in, £2.50. 6 1/2in 10W £5. 8in £4. 10in £7.
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- ★ Weight: 400g inc. battery
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TARDY TRADERS

On reaching retirement I thought that I would like to undertake some electronic projects to keep me alert and active, so I set about getting information and components.

In the last two months I have sent for catalogues, perused them carefully and then ordered successively as plans matured and I discovered further suppliers. Although I have ordered from fourteen component suppliers advertising in a variety of journals, many of them four or five times, with individual orders worth from just over £4 to £126.

I am sorry for industry and can understand some of their poor performance if they have the same sort of experiences that I have had, as well as for other hobbyists who are treated as I have been. Only two of the firms were fully efficient (E&T) and always sent a correct order — the others all exhibited one or more of the following, often more than once.

1. Wrong items sent.
2. Items sent not as described in advertisement or catalogue.
3. Items sent short.
4. Items not of the quality advertised.
5. Items not of the value ordered.
6. Items out of tolerance — the classic case was one order of metal film 1% resistors which, when measured, were not even with 10% tolerance! What of those items the amateur cannot check, such as complex i. cs.
7. Despite 'phoning, items out of stock by the time the order reached the supplier.
8. Suppliers offering data do not send full information. Manufacturers' data is very slow, sometimes not sent at all, even if s.a.e. is sent, as I nearly always do — do they want orders?
9. Catalogues have misleading, downright misleading and clearly wrong information yet most disclaim responsibility if this results in damage — I wonder whether their disclaimer would stand up in law?
10. Some firms pack individual items and groups of like items: one just bundled the goods together in one jiffy bag.
11. Few firms send with the goods an invoice listing the items sent, a few send receipts and some send nothing of this sort.
12. Despatch is always promised the same day as receipt of order.

Despite being on the western fringe of the country I have overnight first-class post to and from most parts, yet only one firm has actually got goods back to me on the third day — the time for the majority from posting here is six days, so why advertise same day despatch? A moderately fast, reliable service would be more acceptable than a very fast unreliable one!

If this is the sort of thing that is going on throughout the industry and commerce on this scale then I think we as a nation have no future, for it is adding unnecessarily to costs and wasting time for productive work. This we certainly cannot afford in the present economic climate of the world and of our country.

*D. S. White
Gwynedd*

DOMESTIC EMC

The RSGB's 56th a.g.m. which was reported in the November 1983 issue of the Society's journal, *Radio Communication*, contained a number of references to the proposed new Telecommunications Bill. Similar to the Australian Radiocommunications Bill (Act), it replaces the old Wireless Telegraphy Act. However, unlike the Australian Act, the UK Bill seems to contain little or no legislation to cover the EMC problems with domestic electronic and entertainment equipment. When asked why this was not covered, the RSGB President replied that he considered this to be a most difficult area and that the Bill would prove unworkable if extended into this area.

Considering many European countries, the USA and Australia are addressing themselves very positively toward the effective EMC control needed to allow the complex electronic communications and control equipment, which will take us into the 21st century, to function correctly and efficiently: And, the constant flow of reports from the UK which indicate the EMC problems with domestic electronic and entertainment equipment is increasing at an alarming rate. It is therefore, indeed, most surprising to see the RSGB taking such a negative attitude towards a problem which has given UK amateurs such a headache for so many years.

No such difficulty or concern

was expressed, or is considered, by the world's most senior amateur radio society — The Wireless Institute of Australia. The WIA worked in close cooperation, as always, with the Australian Department of Communications in the production of the new Radiocommunications Bill. Indeed, the DOC and the WIA gave very special consideration and attention to the extensive and extremely comprehensive EMC section of the new Act.

*A.D. Tregale, VK3QQ
ARTAC International
Watsonia
Australia*

LICENCE REGULATIONS

There can be few British radio amateurs who have not, at some time, been in a situation where they would have dearly liked to ask the station to whom they were communicating to, for example, send a short greetings message to a friend or relation whom they haven't seen for years or, just ask simple route directions for a friend. For British amateurs this is designated, by the licensing authorities, as 'third-party' and is, in general, forbidden! Any sensible reason for these medieval and totally unnecessary restrictions, remains a mystery!

British amateurs, for years, have had to remember to be extremely careful to avoid mentioning, over-the-air, anything which could, even remotely, be considered 'third-party.' Not only for the fear of repercussions from the authorities, but in consideration of the other station, who also has to live under these austere and antiquated regulations. It appears that the British licensing authorities consider the Amateur Radio Service has progressed little since the days of Marconi, and spark transmitters.

Members of the Amateur Radio Service did, in the old days, a great deal of home construction and experimentation. There were two main reasons for this; the only radio equipment available was built by amateurs and enthusiasts and there was an obvious need to do extensive research into the basic concepts of our primary radio communication modes.

With modern communications technology we are, in the main, addressing ourselves to the more detailed and specialized areas.

Our previously developed primary communications systems allow us to communicate ideas and information about these specialised subjects, thereby promoting higher levels of national and international technological development. Equally important, in these days of world tension, is the development of national and international friendship, through communications. Fortunately, this latter area has been especially cared for by many of the new members of our service. Unlike the old days, when it was of prime importance to place great emphasis on the technical aspects of our primary communications systems, there is today a leaning towards communicating for friendship, with experimentation and research as closely related secondary subjects.

Modern economic trends are towards shorter working weeks, more leisure time, and increasing psychological pressure during the time at the work place: therefore, a greater number of people are looking for suitable relaxing hobbies and, amateur radio is indeed most suitable. Consequently, the obvious and simple extension for members of the British Amateur Radio Service would be the lifting of the third-party restrictions.

Australian amateurs shook off the third-party restriction shackles some three years ago, took a breath of the fresh air, and never looked back. It is indeed most refreshing not to need a barrister in the shack!

A.R.T.A.C. International would like to hear from anyone interested in the removal of this totally unnecessary restriction on the British Amateur Radio Service.

*A.D. Tregale, VK3QQ
ARTAC International
Watsonia
Australia*

ELECTRIC CHARGE FROM A RADIO WAVE

In his letter (January 1984) Peter Hesketh gives a step by step method of changing Professor Jennison's apparatus to produce an ideal waveguide bent into a circle. I agree with him that no amplifier is in principle necessary to maintain a wave in such a guide, and so far, his assumptions are completely justified. However, I do not see how he can use this idealised equipment, even in his imagination, to support Professor Jennison's contention.

Is it not true that the velocity in space of a guided electromagnetic wave is independent of the motion of the conductors that do the guiding? In other words, even in principle we cannot drive a waveguide backward so that the wave it carries is arrested in space.

Now this objection does not apply to the discrete component machine described in the article. The waves associated with such a machine are not electromagnetic waves in space, but as I said in my earlier letter, more like the waves we find on a polyphase machine. As such they have a velocity relative to the hardware of the machine. Perhaps Mr Hesketh has raised unwittingly a more serious objection to Professor Jennison's demonstration than at first occurred to me. We cannot use a machine that generates waves having a velocity which can be vectorially combined with the velocity of the machine to explain phenomenon where the waves have a velocity that is independent of the machine velocity.

Perhaps in what I say I am mistaken. I would certainly like to see Professor Jennison's defence of his apparatus.

Chris Parton
Department of Electrical & Electronic Engineering
Bell College of Technology
Hamilton

ENERGY SAVING

Mr Cummins states that he uses no supplementary heating and implies that for this reason he does not need thermostats in individual rooms.

I of course applaud his basic design approach but should be

very interested to know how in practice it copes it copes with three unavoidable sources of supplementary heat: (a) solar radiation, (b) people and (c) their reading lights and televisions. I find that the first alone, here in the temperate South at any rate, can entirely obviate the need for heat from the radiators in South-facing rooms even on cold days, and in specifying my central heating installation I considered room thermostats to be essential in South-facing rooms and highly desirable in other rooms whose occupancy was liable to vary much during heating hours.

Jan Leslie
London N 10

PROBLEMS IN SPECIAL RELATIVITY

I am sorry that Professor McCausland found my simple arithmetic derivation somewhat obscure. Had he persevered he would have discovered that C.F. Coleman was quite right. Dingle was, and McCausland is still, confused over the distinction between simultaneity and synchronicity, as the latter's comments on Coleman's letter now make clear.

McCausland states, correctly, that Einstein's procedure for synchronizing clocks was based upon the out and return journey of a light beam between clocks A and B. McCausland, (not Einstein) then adds, 'If the reading on B at the moment of reflection is halfway between the readings of A at emission and return of the flash, the clocks are synchronised'. Not true, as my worked example shows. This requirement actually means that clocks A and B both reach time, say 1200h simultaneously. He has tried to smuggle in simultaneity under the guise of synchronicity and it cannot be done. This is the advantage of a worked example — it uncovers the verbal ambiguities.

Let me spell it out. There is no observational procedure which will enable clock B to show the same time simultaneously with A that does not involve a vicious circle in the procedure. I challenge McCausland, or anybody, to produce one. McCausland's error is fundamental and the remainder of his argument now fails.

Statements involving the expression 'real effect' need clarifying. If I observed a physical phenomenon using the best instruments, the best scientific procedures, and after repeated measurements arrived at a result, I should be somewhat surprised if somebody said that my results were only an observational effect and that the real effect was something different. I should conclude that the someday either knew something that I did not, or was indulging in metaphysics. In either case I should ask for observational evidence.

J.C. Laine
Lymington
Hants

POWER OSCILLATOR

In the 1970 September and October issues of *Wireless World* you were good enough to publish details of my new 13 Watt sine wave oscillator, which resulted in some adverse comments from Thomas Roddam, one being about the cores used. In order to cut down on the number of cores used it was decided to try using a pair of E cores (Mullard FXI818) with the emitter and collector coils on the outer limbs. This arrangement works very well in practice as well as being much cheaper. The phase shift coil was also made using a pair of E cores (Mullard FXI652) The final design resulted in a unit 4in long by 1½ in wide and ¾ in thick, weighing 4 ounces. The oscillator in this form was used to drive a 13 Watt fluorescent 21 inch tube. A large number of these were used to provide lighting in a factory during the power cuts of the early 70s. A car ignition unit was also built and tested in a Fiat car on a tour of Europe. I still have the original unit and demonstrate it to those who show interest.

The oscillator was invented in 1959 to provide the bias and erase for a small high quality tape recorder for use in the news gathering business. The circuit was given the final patent in 1962 and also patented in Germany, Japan and America. I am the sole inventor of the oscillator as can be verified by the Patents Office. I must admit to being puzzled by the lack of interest and discussion about the oscillator which is quite a breakthrough in sine wave power oscillators. The

fact that the transistor does not need a heat sink and will continue to operate in temperatures up to 1200C I thought would have aroused some interest, particularly as the current falls with an increasing temperature. Also it can survive short circuit of the output indefinitely if capacitively coupled to the load, there being no current flow when oscillation ceases.

I am enclosing photographs of the fluorescent lighting unit and the ignition unit to show the coil assembly used for the emitter and collector coils.

H.L. Armer
Alvaston
Derby

THE MIND-FORG'D MANACLES

I'm pleased to see you quoting from Blake in your April editorial. Perhaps I could answer with another quotation:

Now I a fourfold vision see,
And a fourfold vision is given to me;
'Tis fourfold in my supreme delight
And threefold in soft Beulah's night
And twofold Always. May God us keep
From Single vision and
Newton's sleep!

The single vision which Blake so feared corresponds exactly to what you call the 'technicization of society' Many people outside of technology have noted the acceleration of this process but, lacking inside knowledge, have been unable to challenge it at its base. Their impotence has resulted in a blind despair of technology, a sort of a modern-day Luddism, whose danger is that it could lead to the formation of a dual society: technocratic and desperate on the one hand, anarchic and desperate on the other.

It is left up to engineers and technologists themselves to awake from Newton's sleep and, taking control of the process, direct it back towards the humanization of technology. The 'characteristic mode of thinking and feeling that determines the way machines and systems are designed, used and interact with people' must be consciously recognised and modified if there is to be a human future.

Tim Williams
Tunbridge Wells
Kent

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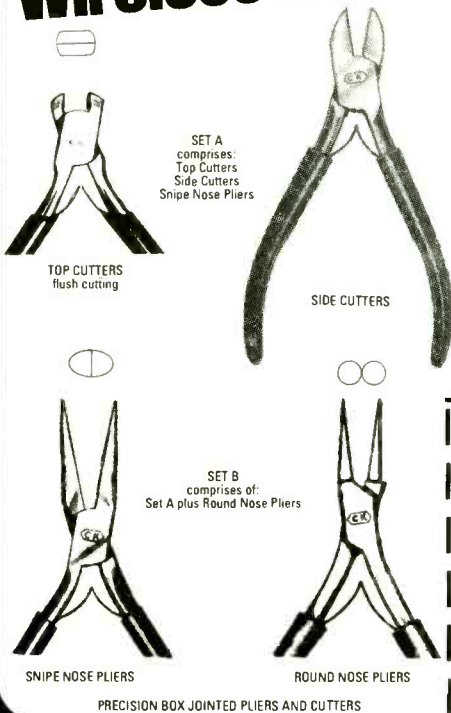
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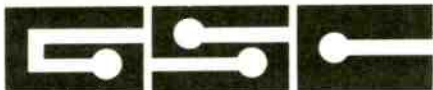
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Automatic speech recognition

Speaking communication between man and machine is needed for many applications — in military use, where hands are otherwise occupied, where the communicator is disabled or where it is simply more convenient. Tom Ivall reports on two recent meetings.

By Tom Ivall

Machines are needed to wreck a nice beach..... If you have read that sentence purely visually, as most people do, you will be somewhat puzzled. If, however, you heard it being read aloud, fairly quickly, you probably would have interpreted the last part of the continuous stream of sound as the entirely appropriate words ".... recognize speech."

This rather artificial example illustrates one of the characteristic problems in the automatic recognition of speech by electronic systems. Electronics can analyse the acoustic speech signal perfectly well in terms of amplitude, frequency, time and other such parameters, but how does it translate the result into a correct message — either in printed words or merely as data for controlling a machine — when such ambiguities are possible?

According to J. S. Bridle of the Joint Speech Research Unit (JSRU), who supplied this example, aural ambiguity is the most difficult problem of all. Another is the problem of continuity. In normal speech the words run together into a continuous stream of sound, as shown by the spectrogram of the two words "go away" in Fig.1, so how does a machine find the linguistic and semantic boundaries? In any case, the mouth movements required by particular junctions between spoken words modify the sounds of the syllables on either side of these boundaries.

Then there is the problem of variability of pronunciation — for example, in utterances of the

same word by different speakers, or in different rates of speaking, even by the same person. Finally, there is a big problem in the sheer complexity of the different levels of meaning in spoken language (e.g. if you say to a machine "Can you tell me the time?" you don't want it to just answer "Yes").

Mr Bridle was one of the speakers at a recent IERE colloquium on "Speech Input/Speech Output" held at the Royal Institution in London. This followed shortly after a similar London meeting, an IEE/IERE lecture on "Man-Machine Speech Interface" given by Dr J. Laver, a phonetician from Edinburgh University. Together these two meetings gave a useful picture of current activities and achievements in what is now called speech technology — mainly speech synthesis and speech recognition.

But why do we want this particular kind of man-machine interface? What is wrong with the established m.m.i. techniques using keyboards, v.d.u. screens, printers and the like? The most general answer seems to be that in some jobs the operator's hands and eyes are already heavily occupied, sometimes with multiple tasks. They should be kept as free as possible to concentrate on procedures that are more important than data input/output.

One group of speech interface applications is where technical solutions are being sought for very pressing reasons, such as helping the pilots of fighter aircraft to operate systems so that they can concentrate their main

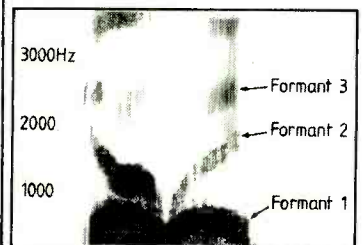
attention on tactics. Here, plenty of money is available. Dr Laver remarked, in a regretful tone, that "the military market constitutes the major driving force behind this technology."

A second, less pressing group of applications are the "hands busy" tasks in industry that require data entry — inspection, quality control, package sorting, office machinery, computerised map-making, handling very dirty materials — where operating a keyboard can be very inconvenient. Japanese banks have been using speech recognition for some years to help counter staff deal with customers' enquiries, and now a Japanese ship-building firm is trying it for engine control in a coal-carrying vessel.

Aids for the disabled, such as voice control of wheelchairs, are a socially useful group of applications (see, for example, April 1984 issues, News, p.59). Finally, there are those applications which are not really necessary in any urgent sense but exploit the wide availability of the ordinary telephone as a cheap form of speech input/output. Of course, this has a mass-market potential for the electronics manufacturers. New automated services now being tried out include telephone directory and train timetable enquiries, telephone banking, voice actuated dialling using keywords like "Mother", and voice actuation of telephone switchboards for disabled operators.

Much of the current commercial equipment for speech recog-

Fig.1. Spectrogram of spoken phrase "go away", showing formants. In some speech recognizers, spectrum analysis by filter banks provides acoustic information which subsequently has to be translated into linguistic/semantic data. (Horizontal scale is time; recording density is proportional to acoustic energy.)



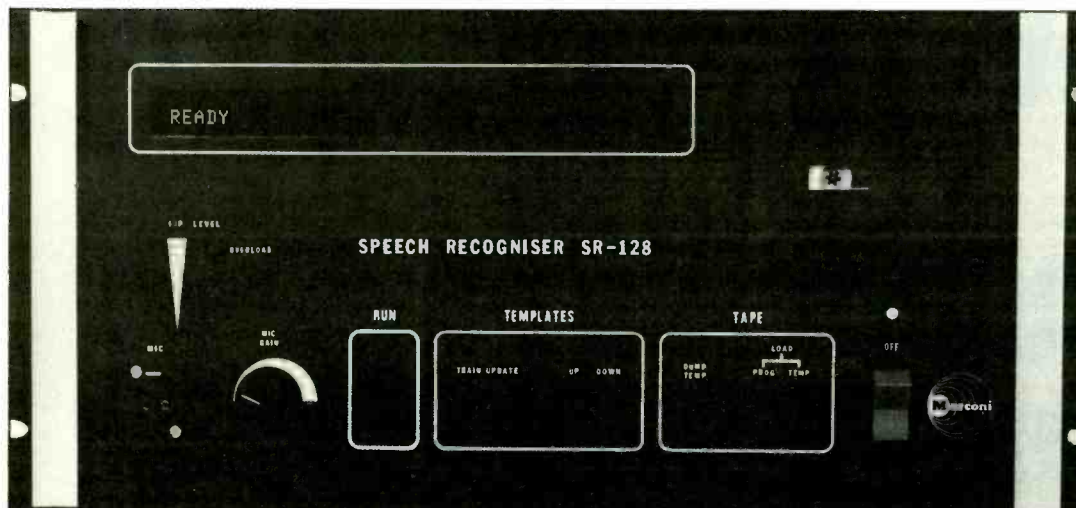


Fig. 2. The SR-128 connected-speech recognition system made by Marconi Space & Defence Systems uses a template-matching principle and has a maximum vocabulary of 240 words. Syntax can be applied to isolated keywords. Utterances can be up to 8s long and recognition response time is 50ms.

tion is in the form of desk-top or stand-alone units, of about the size of the Marconi SR-128 Speech Recognizer shown in Fig. 2. There are also i.c. chips and chip-sets which can be built into other equipment. These include what are basically general-purpose signal processor, which the user programs with speech recognition algorithms (e.g. Intel, Texas Instruments), and more specialized chip sets (e.g. NEC) designed specifically for speech recognition.

How, then, does this commercial equipment cope with the extremely difficult speech recognition problems outlined above? It achieves practical results, with reasonable accuracy at reasonable cost, by offering only limited capabilities. The range of spoken language parameters to which it can respond is deliberately restricted in the design.

Vocabulary is limited, to perhaps several hundred words rather than the several thousand desirable. Some recognizers will work only on isolated words, with pauses separating them from the preceding and following words. Most commercial recognizers are 'speaker dependent': they will only work with one particular voice, the one that has been used to 'train' them. The spoken words must be carefully enunciated and acoustic background noise must not be allowed to interfere — a real problem in aircraft cockpits, for example.

Thus the ambiguity problem discussed above is just side-stepped: the words can have only one prescribed meaning, or nothing at all. Overall the result, in the words of Dr J. N. Holmes of the JSRU, is that "communication with machines by speech is at present pathetically trivial compared with speech communica-

tion between humans." And Dr M. J. Underwood, of the Alvey Directorate, argued that available products with limited capabilities "are not all that easy to use", the difficulties arising from the fact that the systems do not necessarily match the users' jobs, skill or experience.

Dr Underwood was issuing a general warning against the "facile argument" that, because speech is man's most natural form of communication, spoken communication with computers and other machines must be worth doing. And J. Paterson of Logica joined him in the view that the problems of matching systems to applications were now more pressing than the purely technological problems of equipment design. Mr Paterson felt that a major goal in this applications task was minimizing access or transaction time, which was influenced by both the type of transaction and the error rate.

Technology

Most speech recognizers start with a signal processing section, which analyses the acoustic waveform of the spoken words. This is followed by a digital information processing section, basically programmed logic, which makes decisions about the linguistic/semantic meanings of the acoustic parameters presented to it, on the basis of some algorithm.

Dr Laver referred to a distinction that is often made, between systems based on the principle of 'template matching' and systems that extract specific phonetic features from the acoustic information. The important point here is that template matching — trying each input acoustic pattern, typically a whole word, against a vocabulary of stored reference

patterns — does not have to depend on any explicit theory of speech. The process would work just the same if the input and reference patterns were sound of dogs barking, whistles blowing or anything else that makes a noise. The basic simplicity of this template matching principle — and the fact that it can be used on continuous sequences of connected words as well as an isolated single words — makes it very attractive for use in commercial equipment. Its main drawbacks are that it tends to be speaker-dependent and limited in vocabulary. Dr Laver agreed with an American opinion that "template matching will not be able to attain human levels of performance."

The alternative principle, of extracting phonetic features, does, however, depend on explicit theories of speech. In general it uses phonemes — the smallest elements in speech sounds capable of indicating contrasts in meaning. Phonemes do not correspond simply to vowels and consonants. For example, the phonemes for 'p', 'i' and 't' in the word 'pit' are not the same phonemes as in other words using this vowel and these consonants, such as 'bit', 'pet' and 'pin'. The differences, mentioned by Dr Holmes as a particular problem in speech synthesis, are due to co-articulation: the sound of a driven vowel or consonant depends on the articulatory movements necessary to form the vowels and consonants immediately before or after it.

The use of phonemes, as against whole words, allows great flexibility and a high level of performance, but it also introduces considerable difficulties. Basically, how are phonemes identified from the extracted acoustic features? To begin with, only some of the information in the speech signal is relevant to the recognition process. Parameters that are in fact relevant can include peak values, frequency of zero crossings, times between prominent peaks, the sum of squares of waveform values over a period of time and so on.

Time varying patterns of local peaks in power spectra — the formants in Fig. 1 — are important clues to recognizing phonemes, especially their dynamic properties. Various electronic techniques being used include spectrum and cepstrum analysis, Fast Fourier Transforms, autocorrelation, and autoregression or linear

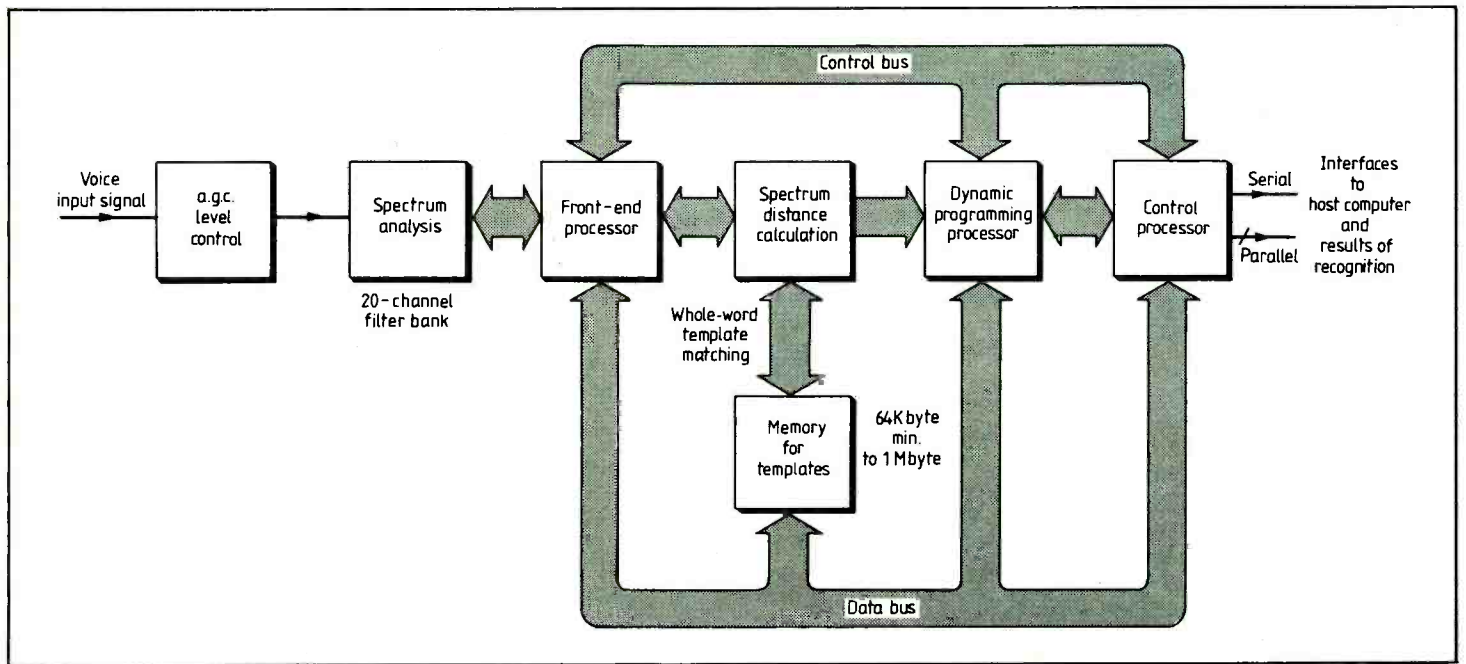


Fig. 3. This continuous-speech recognition system made by Logica is based on techniques developed at the JSRU. Using a template-matching dynamic programming algorithm, it has a vocabulary of 120 words expandable by extra storage to about 2000 words. Syntax and error correction strategies can be programmed in.

prediction. (See, for example, recent issues of *IEEE Trans. on Acoustics, Speech and Signal Processing*.)

Several lecturers agreed that the information processing stage, following feature extraction, will need much more research on how to use artificial intelligence in this field. Dr Laver pointed out that the Japanese were employing multi-disciplinary methods involving signal processing, computer technology, phonetics, linguistics, artificial intelligence and ergonomics to achieve very ambitious goals in a 100M dollar project up to the end of 1993. This would involve parallel processing at speeds of 40 million instructions per second in 1986 and 500 m.i.p.s. by 1989.

As an example of what is needed, Dr S. J. Young described work at Manchester University aimed at finding better forms of man-machine dialogue than those controlled by the rather rigid and artificial 'menu' type of interaction. He recommended a "data driven" dialogue control and described a prototype system in which knowledge necessary to run an intelligent and flexible dialogue is encoded in special kinds of data structures.

The two meetings, however, revealed rather more about the technology of current template-matching systems. These have achieved good results mainly through the use of a very powerful algorithm based on dynamic programming. J. Wilson demonstrated the Marconi SR-128 speech recognizer using this technique and J. S. Bridle explained the

broad principle. The Logica system shown in Fig. 3 is based on dynamic programming and this algorithm is programmed into some i.c. chip sets.

In this method, matching between an input pattern and a stored reference pattern is achieved by an optimisation technique, while time-normalisation copes with one of the oldest problems in automatic speech recognition: the variability of speaking rate. This amounts to a non-linear variation of the timing of the input pattern for a word, or sequence of words, relative to the time-scale of the reference pattern. With the dynamic programming algorithm, the timing differences between the two patterns are eliminated by dynamically distorting the time-scale of one to obtain maximum co-incidence with the other.

Dynamic programming — not to be confused with any kind of computer programming — is a mathematical technique used in optimisation problems and is useful where time-dependence and non-linearities are involved. For example, the control problem of steering a vessel to reach a desired destination by the optimum path (shortest or quickest) can be seen as a multi-stage decision process, in which the steering has to be repeatedly re-decided along the route to counteract the non-linearities introduced by currents, wind and other perturbations.

Inventory control in a factory is another example of a multi-stage decision process. The inventory of a particular item

depends on the previous day's inventory, the production quantity decision in the factory, and the random demand from customers. In general at each stage of a multi-stage decision process the current state or result is a function of (a) the state at the previous stage, (b) any action made by a decision, and (c) any random event that occurs.

In the template-matching speech recognizer, the two patterns, input and reference, are typically spectrum analyses produced by filter banks. The Fig. 3 system, for example, uses a bank of 20 bandpass filters. The information produced has the parameters shown in Fig. 1: energy/frequency with time.

Analogue digital conversion produces two patterns of stored digital data, which are compared. In Fig. 4 these two patterns, input (A) and reference (B), are shown in relation to each other as sequences of units called 'frames' ($a_1, a_2 \dots$ etc. and $b_1, b_2 \dots$ etc.). Each frame is a digital 'cross-section' of the spectrum analysis corresponding to a particular instant of time. If the A and B patterns were identical the curve relating them would be a straight line ($a = b$). In reality, the timing non-linearities make the curve a crooked one, such as the one shown, with its sequence of points, $c_1, c_2 \dots$ etc., indicating the timing differences between the patterns.

This curve is a function which maps the pattern A time-scale onto the pattern B time-scale — a 'time-scale distortion' function. The dynamic programming algo-

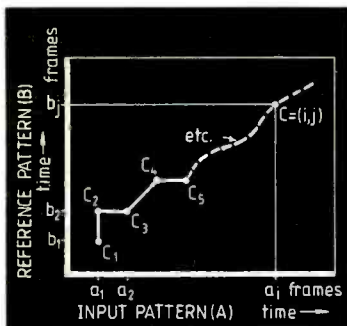


Fig. 4. In the dynamic programming algorithm for speech recognition, timing non-linearities in the input speech pattern relative to the reference (template) pattern are eliminated by distorting the time-scale of one relative to the other. In this graph, input and reference patterns consisting of spectrum analysis 'frames' are related to each other by a 'time-scale distortion' function.

algorithm finds the optimum path for the curve in this multi-stage process, from the many paths possible — that is, the best correspondence between the time-scales of patterns A and B. It does this by computing a 'score', which is the sum of the frame dissimilarities, called 'distances' (see Fig. 3), for the best way of aligning a given number of input frames with a given number of reference frames. This is computed for all the reference patterns (templates), and the score giving the smallest sum is defined as the optimum path and the best match. This smallest sum is the residual, time-normalized 'distance' value — what remains after the timing differences between the two patterns have been eliminated.

The same dynamic programming principle can be extended from single-word template matching to matching sequences of connected words as in continuous speech. The Logica system in Fig. 3 has this ability, and J. Wilson of Marconi demonstrated the process in action on the SR-128 speech recognizer. An aid to correct recognition, built into both the Logica and Marconi systems, is the con-

straint of syntax — the normal order in which successive words are arranged in a given language. A set of word sequence rules is programmed into the recognizer and this reduced the number of word choices possible at any point in a phrase. This not only improves recognition accuracy but also reduced the amount of computation required.

Mr Bridle also presented some results of speech recognition research on isolated words being done by P. K. Moore of the Royal Signals and Radar Establishment. This work aims at producing better word models by using stochastic series called Markov chains*. Mr Bridle showed spectrograms of words which sound rather similar ("nine" and "five"; "league" and "leak") and therefore might be confused in automatic recognition systems. He said that the Markov modelling gave results in distinguishing between these than could be obtained by conventional comparison of the whole-word patterns.

There was much lively discussion on the question of whether speech synthesizers should be made to sound 'natural' or decidedly machine-like. Some of the

demonstrations of synthesized speech were hardly distinguishable from human utterances, but one member of the audience declared roundly that he would always want to know whether he was speaking to a person or a machine. This was particularly important in large organizations where sometimes one never met face-to-face certain people one was dealing with! Another participant suggested that interactive speech interface systems should always use "jovial" sounding synthesized speech, while one-way announcement systems should have a "short and professional" manner.

Dr Laver felt that when man-machine speech interaction becomes commonplace we shall certainly have to consider the apparent 'personality' characteristics in synthesized voices. An unsuitable tone of voice could make a human operator react badly, depending on his particular life experience, and so be counter-productive. The jargon term 'user friendly' will certainly become much more pertinent than it is at present.

* Named after A. A. Markov who published in 1913 a statistical study of digraphs in Pushkin's poetic novel (subsequently Tchaikovsky's opera) *Eugene Onegin*.

LITERATURE RECEIVED

A company has been formed to offer a mail-order catalogue service for test and measuring instruments, with cables, connectors, kits and accessories. There is no minimum order and the catalogue is aimed at the small business and home constructor. Supercat Electronics Ltd, PO Box 201, St. Albans, Herts AL1 4EN. EWW 258

Over 1300 new products are included in the latest edition of the Verospeed catalogue, which in its 400 pages covers a total of 7500 products, telephone and computer connectors and cabling, keyboards, proximity and microswitches, a wide range of test equipment and many tools and accessories. Verospeed, Stansted Road, Boyatt Wood, Eastleigh, Hants SO5 4ZY. EWW 259

Weir Electronics have published an introductory leaflet outlining the capabilities of their display division which specializes in the design and manufacture of data display monitors. Described is a wide range of monochrome and colour video display modules with brief performance specifications. Weir Display Division, Durban Road, Bognor Regis PO22 9RW. EWW 260

Texas Instruments has published a Master selection guide on its semiconductor ranges. The 114-page guide gives outline data and packaging information on all TI components including memories, logic arrays, digital products, linear products, telecommunications circuits, opto-electronics, and power and small signal devices. Included are details of TI's latest products. Copies are available free from any TI distributor or by phoning TI at Bedford (0234) 223000. EWW 250

The extensive Cube range of Eurocards, rack-mounted computers and peripherals has been described in detail with extensive illustrations specifications and technical information in a 150-page catalogue. Development systems based on Eurocards are a speciality of the company and they produce direct, and often enhanced replacements for the Acorn range. A new range of Delegate/Unicube modules are designed for industrial and laboratory control. There is also an extensive range of add-ons for the BBC microcomputer. Control Universal Ltd, Unit 2, Anderson's Court, Newnham Road, Cambridge CB3 9EZ. EWW 251

The specialist computer company, Unit C, has published a useful pocket-sized guide to its range of 68000 VME and Pascal-2 products. The guide describes the 68000 VME and Q-Bus hardware together with the Unix system III operating system and Pascal-2 supporting software. Development software is available for Unix/68000, DEC RSX/PDP or DEC VMS/VAX hosts. Stand-alone 68000 target support can also be provided by means of the pSOS real time executive. Unit C Ltd, Dominion Way West, Broadwater, Worthing, West Sussex. EWW 253

A catalogue lists software available for Torch computers, from Torch themselves and from other software houses. Over 140 programs are listed for the computers which are networked Unix and CP/M compatible operating systems. By purchasing the Torch add-on, the programs are also available to users of the BBC micro. Torch Computers Ltd, Abberley House, Great Shelford, Cambridge CB2 5LQ. EWW 254

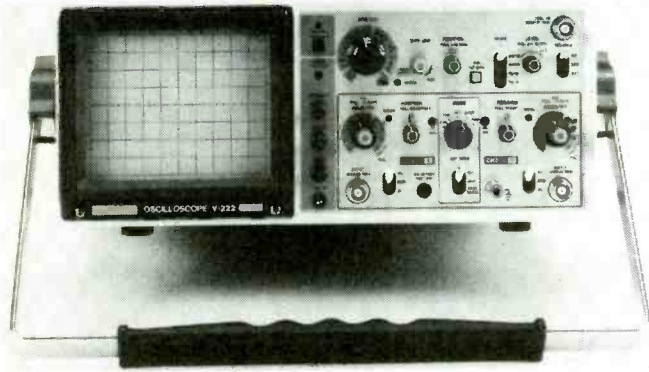
Ferranti Electronics has issued a colour brochure highlighting their new generation of power mosfets. The mosfets are suited to a wide range of switching and amplifying applications where high input impedance, high gain and fast switching is desired. The brochure gives basic mosfet information with the aid of clear diagrams, and there is a tabular selectors guide giving the range of devices on offer. Ferranti Electronics Ltd, Fields New Road, Chadderton, Oldham, Lancs OL9 8NP. EWW 255

A 16-page colour brochure gives full technical details of the recently-introduced Gould 5110 intelligent 100MHz oscilloscope system. The 5110 automates many oscilloscope measurements and has a built-in IEEE interface for use in automatic test systems. It is controlled by a keyboard/menu system. Numerous application examples are given and the instrument's operating modes and controls are clearly illustrated. Gould Design and Test Systems Division, Roebuck Road, Hainault, Ilford, Essex IG6 3UE. EWW 256



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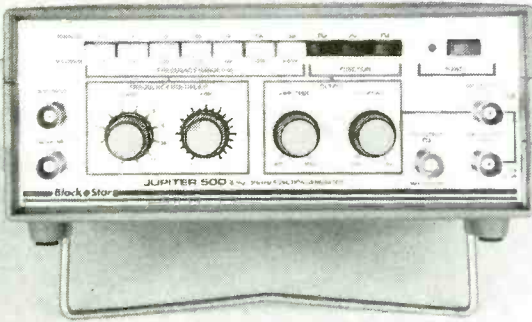
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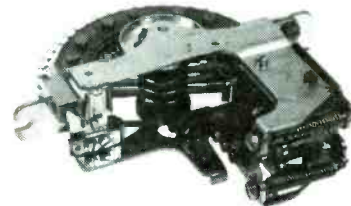


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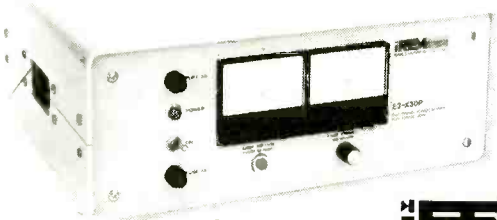
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AN612 2.15	MC1358 1.58	STK437 7.95	TBA560C 1.45	TD2532 1.95
AN7140 3.50	MC1485 3.00	STK439 3.95	TBA560QC 1.45	TD2540 1.25
AN7145 2.50	MC1486 1.25	TA7061AP 9.95	TBA570 1.00	TD2541 2.15
AN7150 2.95	MC145106P 7.95	TA7108P 1.00	TBA641A12 1.25	TD2550 2.15
BA521 3.35		TA7120P 1.65		TD2571 2.95
CA1352E 1.75	MC1723 0.50	TA7130P 1.65	TBA651R 2.50	TD2581 2.25
CA3086 0.46	MC3357 2.75	TA7146 2.95	TBA720A 2.45	TD2593 2.95
ET76016 2.50	ML2318 1.75	TA7176AP 2.95	TBA750Q 2.65	TD2600 5.50
HA1377 3.50	ML2329 2.50	TA7203 2.95	TBA800 0.89	TD2610 2.50
HA1156W 1.50	MSM5807 6.75	TA7204P 2.15	TBA810AS 1.65	TD2611A 1.95
HA1339A 2.95	PLL02A 5.75	TA7205AP 1.50	TBA810P 1.65	TD2620 2.15
HA1551 2.95	SAA500A 3.50	TA7222AP 1.80	TBA820M 0.75	TD2680A 2.75
LA1230 1.15	SAA1025 7.25	TA7227P 4.25	TBA820Q 1.45	TD2690 2.45
LA4102 2.95	SAA5010 6.35	TA7310P 1.80	TBA890 2.50	TD2690 2.45
LA4250 2.95	SAS560S 1.75	TA7313AP 2.95	TBA920 1.65	UPC566H 2.95
LA4400 4.15	SAS560S 1.75	TA7321 2.25	TBA950/2X 2.35	UPC575C 2.75
LA4420 1.95	SAS580 2.85	TA7611AP 2.95	TBA970 2.35	UPC1025H 2.60
LA4422 2.50	SL9018 4.85	TAA550 0.25	TBA990 1.49	UPC1028H 1.95
LA4430 2.50	SL917B 6.65	TAA570 1.95	TBA1441 2.15	UPC1032H 1.50
LC7120 3.25	SL1310 1.80	TAA621AXI 3.50	TCA270 1.10	UPC1156H 2.75
LC7130 3.50	SL1327 1.10	TC8650 2.50	TCA270SQ 1.10	UPC1158H 0.75
LC7131 5.50	SL1327Q 1.10	TC8800 2.15	TCA650 2.50	UPC1167C2 2.15
LC7137 5.50	SN76003N 1.95	TC9A00 1.65	TC9A40 2.20	UPC1181H 1.15
LM324N 0.45	SN76013N 1.95	TDA440 2.20	TDA1001 1.95	UPC1182H 2.95
LM380N 0.95	SN76023N 1.95	TDA1004A 3.25	TDA1001 1.95	UPC1185H 3.95
LM383T 2.95	SN76033N 1.95	TDA1006A 2.50	TDA1004A 3.25	UPC1191V 1.50
M51513L 2.30	SN76110N 0.89	TDA1011 2.15	TDA1006A 2.50	UPC1350C 2.95
M51515L 2.95	SN76115N 1.25	TDA1035 2.50	TDA1011 2.15	UPC1353C 2.45
M51521L 1.50	SN76110N 0.89	TDA1037 1.95	TDA1035 2.50	UPC1365C 3.95
NB3712 2.00	SN76220D 2.95	TDA1170 1.95	TDA1037 1.95	UPC2002H 3.95
MC1307P 1.00	SN76227N 1.65	TDA1190 2.15	TDA1170 1.95	555 0.35
MC1310P 1.50	SN76533N 1.65	TDA1270Q 3.95	TDA1190 2.15	556 0.42
MC1327 0.95	SN76544N 1.95	TDA1327 1.70	TDA1270Q 3.95	723 0.50
MC1327Q 0.95	SN76570N 1.00	TDA2002 1.95	TDA1327 1.70	741 0.35
MC1330P 0.76	SN76650N 1.15	TDA2020 2.45	TDA2002 1.95	747 0.35
MC1349P 1.20	SN76660N 0.80	TDA2030 2.80	TDA2020 2.45	748 0.35
MC1350P 0.95	STK014 7.95	TDA2522 1.95	TDA2030 2.80	7808 0.60
			TDA2522 1.95	

SEMICONDUCTORS

AAV12 0.25	BC182LB 0.10	BD234 0.35	BFR81 0.25	TIP34B 0.75
AC127 0.20	BC183 0.10	BD237 0.40	BFR88 0.30	TIP41 0.45
AC128 0.28	BC183L 0.09	BD238 0.40	BFR90 1.50	TIP41C 0.45
AC128K 0.32	BC184LB 0.09	BD241 0.40	BFR91 1.75	TIP42C 0.47
AC141 0.28	BC204 0.10	BD242 0.50	BFT42 0.28	TIP47 0.65
AC141K 0.34	BC207B 0.13	BD246 0.60	BFT43 0.28	TIP120 0.60
AC142K 0.30	BC208B 0.13	BD376 0.32	BFW92 0.85	TIP125 0.65
AC176 0.22	BC212 0.09	BD410 0.55	BFX29 0.30	TIP142 1.75
AC176K 0.31	BC212L 0.09	BD434 0.55	BFX94 0.55	TIP145 0.65
AC187 0.25	BC212LA 0.09	BD437 0.50	BFX95 0.32	TIP161 2.95
AC187K 0.28	BC213 0.09	BD438 0.60	BFX86 0.30	TIP295S 0.80
AC188 0.25	BC213L 0.09	BD506 0.50	BFX88 0.25	TIP305S 0.55
AC188K 0.37	BC214 0.09	BD508 0.60	BFY50 0.21	TIS91 0.20
AD142 0.79	BC214C 0.09	BD538 0.65	BFY51 0.21	TV106/2 1.50
AD143 0.82	BC214L 0.09	BD597 0.75	BFY52 0.25	2N2905 0.40
AD149 0.70	BC237B 0.09	BD697 1.10	BFY90 0.77	2N2905 0.40
AD161 0.39	BC238 0.09	BD698 1.10	BLY48 1.75	2N3053 0.40
AD162 0.39	BC239 0.12	BD707 0.80	BR100 0.26	2N3054 0.59
AD161/2 0.90	BC251A 0.12	BD732 1.50	BR101 0.49	2N3055 0.52
AF114 1.50	BC252A 0.15	BDY57 1.65	BRCC4443 0.85	2N3072 0.12
AF124 0.65	BC258 0.25	BF115 0.35	BT100A/01 0.12	2N3072 0.12
AF125 0.35	BC258A 0.39	BF119 0.65		2N3074 0.12
AF126 0.32	BC284 0.30	BF127 0.24		2N3706 0.12
AF127 0.40	BC300 0.30	BF154 0.12		2N3706 0.12
AF139 0.40	BC301 0.30	BF158 0.22		2N3707 1.95
AF178 1.95	BC303 0.26	BF160 0.27		2N3792 1.35
AF239 0.42	BC307B 0.09	BF167 0.24		2N4227 1.50
AU106 3.25	BC327 0.10	BF173 0.22		2N4444 1.15
AU110 2.00	BC328 0.10	BF177 0.38		2N5294 0.42
BC107A 0.11	BC337 0.10	BF178 0.26		2N5296 0.48
BC107B 0.11	BC338 0.09	BF179 0.34		2N5298 0.60
BC108 0.10	BC347A 0.13	BF180 0.29		2N5496 0.65
BC108A 0.11	BC461 0.35	BF181 0.29		2N5715 0.60
BC108B 0.12	BC478 0.20	BF182 0.29		2SC495 0.80
BC109 0.10	BC527 0.20	BF183 0.29		2SC496 0.80
BC109B 0.12	BC547 0.10	BF184 0.28		2SC1096 0.80
BC109C 0.12	BC548 0.10	BF185 0.28		2SC1205 2.50
BC114 0.11	BC549A 0.08	BF194 0.11		2SC1172 2.20
BC116A 0.15	BC550 0.08	BF195 0.11		2SC1173 1.15
BC117 0.19	BC557 0.08	BF196 0.11		2SC1306 1.00
BC119 0.24	BC557B 0.08	BF197 0.11		2SC1307 1.50
BC125 0.25	BC558 0.10	BF199 0.11		2SC1364 0.50
BC139 0.20	BC558A 0.10	BF203 0.14		2SC1449 0.80
BC140 0.31	BD115 0.30	BF209 0.14		2SC1678 1.25
BC141 0.25	BD116 0.60	BF220 0.40		2SC1909 1.95
BC142 0.21	BD124P 0.59	BF241 0.15		2SC1945 2.65
BC143 0.24	BD131 0.32	BF245 0.30		2SC1953 0.95
BC147 0.09	BD132 0.35	BF256/LC 0.28		2SC1957 0.80
BC147B 0.09	BD133 0.40	BF257 0.28		2SC1969 1.95
BC148A 0.09	BD135 0.30	BF258 0.28		2SC2028 1.15
BC148B 0.09	BD136 0.30	BF259 0.28		2SC2029 1.95
BC149 0.09	BD137 0.32	BF271 0.26		2SC2078 1.45
BC157 0.12	BD138 0.30	BF273 0.13		2SC2091 0.85
BC158 0.09	BD139 0.32	BF336 0.34		2SC2098 2.50
BC159 0.09	BD140 0.30	BF337 0.29		2SC2166 1.95
BC160 0.28	BD144 1.10	BF338 0.32		2SC2174 0.80
BC161 0.28	BD159 0.65	BF355 0.37		2SC2371 0.36
BC170B 0.15	BD160 1.50	BF362 0.38		2SD234 0.50
BC171 0.09	BD166 0.55	BF363 0.38		3N211 1.95
BC171A 0.10	BD179 0.72	BF371 0.20		3SK45 0.70
BC172C 0.10	BD182 0.70	BF394 0.19		3SK88 0.55
BC172B 0.10	BD201 0.83	BF457 0.32		
BC172C 0.10	BD202 0.65	BF458 0.36		
BC173B 0.10	BD203 0.78	BF459 0.36		
BC174 0.09	BD204 0.70	BF467 0.68		
BC174A 0.09	BD222 0.46	BF595 0.23		
BC177 0.15	BD225 0.48	BF596 0.25		
BC178 0.15	BC232 0.35	BFR39 0.23		
BC182 0.10	BD233 0.35	BFR40 0.23		
		BFR41 0.25		

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BA154 0.06	BY223 0.90	IN4148 0.06
BA155 0.13	BY299-800 0.22	IN4448 0.10
BA156 0.15	BYX10 0.20	IN540 0.12
BA157 0.30	BYX36-150R 0.20	IN5402 0.14
BA158 0.04	BYX38-600R 0.60	IN5403 0.12
BA166 0.06	BYX55-600 0.30	IN5404 0.12
BB105B 0.30	BYX71-600 1.10	IN5405 0.13
BT151 0.79	BZY95C30 0.35	IN5406 0.13
BY126 0.10	OA47 0.09	IN5407 0.16
BY127 0.11	OA50 0.05	IN5408 0.16
BY133 0.15	OA91 0.06	ITT44 0.04
BY164 0.45	OA95 0.06	ITT923 0.15
BY176 1.20	OA202 0.10	ITT2002 0.10
BY179 0.63	IN914 0.04	
BY182 0.55	IN4001 0.04	
BY184 0.35	IN4002 0.04	
	IN4003 0.04	

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IN4005 0.05	Prices available on request
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IN4007 0.02	
IN4148 0.06	
IN4448 0.10	
IN540 0.12	
IN5402 0.14	
IN5403 0.12	
IN5404 0.12	
IN5405 0.13	
IN5406 0.13	
IN5407 0.16	
IN5408 0.16	
ITT44 0.04	
ITT923 0.15	
ITT2002 0.10	

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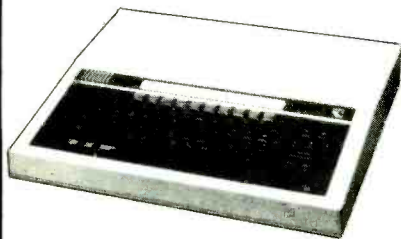


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A1714 18.50	EAAB1 0.60	EF806S 14.50	HL90 0.70	PC185 0.80	RG4-1000 10.00	U029 4.50	3CX3 2.50	6BW4 1.50	7Y4 1.95	95A1 6.50
A1998 11.50	EABC80 0.70	EF812 0.65	HL92 1.50	PC186 0.85	RK.20A 12.00	U030 1.50	3CY5 1.50	6BW6 5.35	888 2.50	108C1 1.50
A2087 11.50	EAC31 2.50	EF812 0.65	HL133/DD 3.50	PC1200 1.60	RL16 1.50	U031 1.50	3D6 4.50	6BW7 1.50	8F07 1.95	150B2 6.95
A2134 14.95	EAF42 1.20	EF812 0.65	HY90 1.00	PC1800 0.80	RPL16 12.00	W279 1.00	3D21A 29.50	6BW8 6.00	10F1 0.75	150C2 2.15
A2293 6.50	EAF801 3.50	EF812 0.65	HVR2 3.00	PC1805 0.90	RPY13 2.50	W739 1.50	3D22 19.50	6BX6 4.48	10G6 1.95	150C4 1.15
A2521 21.00	EB34 1.50	EF812 0.65	JPS-7A 60.00	PD500 3.50	RPY43 2.50	X24 1.00	3W4GT 2.50	6BX7GT 3.50	10P14 2.50	158BT 1.50
A2599 37.50	EB41 3.95	EF812 0.65	K391A 95.00	PD510 3.85	RPY82 2.50	X66L 4.95	4B551B 115.00	6BZ 2.50	10P18 2.75	274A 15.00
A2900 11.50	EB91 0.60	EF812 0.65	K3118 85.00	PEN40D 2.00	RR3 25.00	X76M 1.95	4-250A 65.00	6C4 1.10	10P18 2.75	307 5.00
A3042 24.00	EB33 2.50	EF812 0.65	KR6/3 45.00	PEN40DD 2.50	RS613 45.00	X82D 1.50	4B07A 1.75	6C5 1.95	10P18 2.75	328A 15.00
A3283 24.00	EB41 3.95	EF812 0.65	KT8C 7.00	PEN45 3.00	RS685 54.95	XFW47 1.50	4C27 25.00	6C6 2.50	10P18 2.75	388A 17.50
AC/HL/DD 4.00	EB31 3.50	EF812 0.65	KT33C 1.00	PEN45DD 3.00	RS688 52.15	XFWS0 1.50	4C28 25.00	6C8G 1.50	11E2 16.50	425A5 8.00
AC/THI 4.00	EB30 0.90	EF812 0.65	KT36 2.00	PEN46 2.00	S6F17 5.95	XG2-6400 35.00	4CX250B 1T 37.50	6C8H 1.50	12A 5.00	431U 2.50
AC/V2 4.00	EB33 2.50	EF812 0.65	KT44 4.00	PF1200 1.25	S6F33 28.95		4CX250B 1T 37.50	6C8J 1.50	12A15 1.00	572B 35.00
AC/V2 PEN 8.50	EB33 2.50	EF812 0.65	KT45 4.00	PL21 2.50	S6F33 28.95		4CX250B 1T 37.50	6C8K 1.50	12A16 0.65	705A 8.00
AH225 39.00	EB31 3.50	EF812 0.65	KT61 4.00	PL3 0.95	S30/2K 12.00		4CX250B 1T 37.50	6C8L 1.50	12A17 1.15	708A 8.00
AC/HZ38 39.00	EB31 3.50	EF812 0.65	KT63 2.00	PL38 1.50	S104/K 10.00		4CX250B 1T 37.50	6C8M 1.50	12A18 2.50	715A 8.00
AL60 6.00	EB31 3.50	EF812 0.65	KT66 OSRAM 10.50	PL81 0.72	S109/K 15.00		4CX250B 1T 37.50	6C8N 1.50	12A19 1.00	715B 45.00
AN1 14.00	EB31 3.50	EF812 0.65	KT66 GEC 14.95	PL81A 0.72	S130 5.95		4CX250B 1T 37.50	6C8P 1.50	12A20 0.55	725A 275.00
ARP12 0.70	EB11 2.50	EF812 0.65	KT77 Gold Line 19.95	PL82 0.60	S130P 5.95		4CX250B 1T 37.50	6C8Q 1.50	12A21 0.85	803 14.95
ARP34 1.25	EB21 2.00	EF812 0.65	KT77 Gold Line 19.95	PL83 0.52	SC1/B00 5.00		4CX250B 1T 37.50	6C8R 1.50	12A22 0.85	805 39.00
ARP35 2.00	EC52 0.75	EF812 0.65	KT81 7.00	PL84 0.78	SC1/1200 5.00		4CX250B 1T 37.50	6C8S 1.50	12A23 0.85	807 1.60
BL63 2.00	EC52 0.75	EF812 0.65	KT81 7.00	PL85 1.75	SC1/2000 9.00		4CX250B 1T 37.50	6C8T 1.50	12A24 1.95	810 55.00
BS450 67.00	EC80 9.50	EF812 0.65	KT81 7.00	PL302 1.00	SD6000M 9.00		4CX250B 1T 37.50	6C8U 1.50	12A25 1.95	811A 12.95
BS810 55.00	EC81 7.95	EF812 0.65	KT81 7.00	PL345 12.50	SP2 1.50		4CX250B 1T 37.50	6C8V 1.50	12A26 1.95	813 USA 59.50
BS814 55.00	EC86 1.00	EF812 0.65	KT81 7.00	PL500 1.10	SP2 1.50		4CX250B 1T 37.50	6C8W 1.50	12A27 1.95	833A 115.00
CIK 16.00	EC88 1.00	EF812 0.65	KT81 7.00	PL504 1.15	SP42 3.00		4CX250B 1T 37.50	6C8X 1.50	12A28 1.95	866A 3.50
C3JA 18.00	EC90 1.10	EF812 0.65	KT81 7.00	PL508 1.95	SS501 35.00		4CX250B 1T 37.50	6C8Y 1.50	12A29 1.95	872A 19.00
C1108 54.95	EC92 1.25	EF812 0.65	KT81 7.00	PL509 4.85	ST11 1.50		4CX250B 1T 37.50	6C90 1.50	12A30 1.95	873 60.00
C1112G 70.00	EC92 1.25	EF812 0.65	KT81 7.00	PL519 4.95	STV280/40 1.50		4CX250B 1T 37.50	6C91 1.50	12A31 1.95	884 8.00
C1134 32.00	EC93 1.50	EF812 0.65	KT81 7.00	PL802 5.95	STV280/40 1.50		4CX250B 1T 37.50	6C92 1.50	12A32 1.95	890 9.95
C1148A 115.00	EC95 7.00	EF812 0.65	KT81 7.00	PL802T 3.50	STV280/40 1.50		4CX250B 1T 37.50	6C93 1.50	12A33 1.95	954 1.00
C1149/1 130.00	EC97 1.10	EF812 0.65	KT81 7.00	PL820 3.95	STV280/40 1.50		4CX250B 1T 37.50	6C94 1.50	12A34 1.95	955 1.00
C1150/1 135.00	EC99 1.25	EF812 0.65	KT81 7.00	PL820T 3.95	STV280/40 1.50		4CX250B 1T 37.50	6C95 1.50	12A35 1.95	958A 1.00
C134 32.00	EC99 1.25	EF812 0.65	KT81 7.00	PL821 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C96 1.50	12A36 1.95	1299A 0.60
CCV 2.60	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C97 1.50	12A37 1.95	1619 2.60
CC3L 2.00	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C98 1.50	12A38 1.95	1626 3.00
CL33 3.90	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A39 1.95	2050V 9.50
CV Nos Prices on request	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A40 1.95	2050 7.00
D63 1.20	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A41 1.95	3545 4.00
DAF91 0.70	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A42 1.95	4313C 9.00
DAF96 0.65	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A43 1.95	4328D 9.00
DC70 1.75	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A44 1.95	5642 9.50
DC90 1.20	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A45 1.95	5651 2.50
DCX4-1000 12.00	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A46 1.95	5656 1.95
DCX4-5000 25.00	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A47 1.95	5670 3.50
DET16 28.50	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A48 1.95	5672 4.50
DET18 28.50	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A49 1.95	5675 2.50
DET24 39.00	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A50 1.95	5675 2.50
DET25 22.00	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A51 1.95	5675 2.50
DF91 0.70	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A52 1.95	5675 2.50
DF92 0.65	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A53 1.95	5675 2.50
DF96 0.65	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A54 1.95	5675 2.50
DF97 1.00	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A55 1.95	5675 2.50
DH63 1.20	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A56 1.95	5675 2.50
DH77 0.90	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A57 1.95	5675 2.50
DH79 0.56	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A58 1.95	5675 2.50
DH149 2.00	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A59 1.95	5675 2.50
DK91 0.90	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A60 1.95	5675 2.50
DK92 1.20	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A61 1.95	5675 2.50
DK96 2.00	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A62 1.95	5675 2.50
DL35 1.00	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A63 1.95	5675 2.50
DL63 1.00	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A64 1.95	5675 2.50
DL70 2.50	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A65 1.95	5675 2.50
DL73 2.50	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A66 1.95	5675 2.50
DL91 1.50	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A67 1.95	5675 2.50
DL92 1.50	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A68 1.95	5675 2.50
DL93 1.10	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A69 1.95	5675 2.50
DL94 2.50	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A70 1.95	5675 2.50
DL96 2.50	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A71 1.95	5675 2.50
DL98 2.50	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50		4CX250B 1T 37.50	6C99 1.50	12A72 1.95	5675 2.50
DL99 1.50	EC99 1.25	EF812 0.65	KT81 7.00	PL822 2.95	STV280/40 1.50					

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NEW TORCH Z80 PACK PRICE £699.
SOFTWARE PACKAGE INCLUDES Z80 BASIC

Phone for details about the 20Mbyte Hard Disc Pack, and the 68000 Hard Disc Pack with UNIX Operating System. NOW AVAILABLE — The TORCH Z80 SECOND PROCESSOR CARD — for those who already have suitable disc drives. The card is supplied with all the free software, as detailed above, presenting a very attractive package. £299.

ACORN IEEE INTERFACE

A full implementation of the IEEE-488 standard, providing computer control of compatible scientific & technical equipment, at a lower price than other systems. Typical applications are in experimental work in academic and industrial laboratories. The interface can support a network of up to 14 other compatible devices, and would typically link several items of test equipment allowing them to run with the optimum of efficiency. The IEEE Filing System ROM is supplied. £282.

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We have a large selection of books on the BBC and other titles. Please ask for details. No VAT on books.

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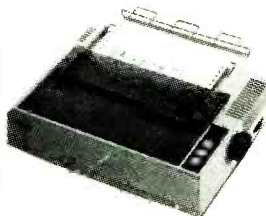
All prices in this double page spread are subject to change without notice.

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Computer Grade Cassette 10 off.	£4.50c
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A fully self-contained mains-powered eprom programmer housed in an attractive finished case. It is able to program 2716, 2732/32A, 2764 & 27128's in a single pass. It is supplied with vastly superior software when compared to any currently available similar programmer. In addition to normal eprom programming, you are now able to load your favourite basic programs onto eprom.

EPROM PROGRAMMER:

* Menu Driven Software provides user friendly options for programming the eprom with:

- a) Basic programs.
 - b) Ram resident programs.
 - c) Any other program.
- * Programmer can read, blank-check, program & verify at any address/addresses on the Eprom.
- * Personality selection is simplified by a single rotary switch.
- * Programming voltage selector switch.
- * Full Editor with ASCII Disassembler, allowing direct

modification of memory data in HEX or ASCII.

- * Continuous display of time left for completion of programming.
- * Continuous display of current addresses as they are being programmed.

The programmer comes complete with cables, software & operating manual. £89 + £2.50 carriage. Software on disc £2 extra.

SMARTMOUTH:

The original 'infinite speech'. Still the best. A ready built totally self contained speech synthesiser unit, attractively packaged with built-in speaker, AUX output socket etc. — no installation problems! It allows the creation of any English word, with both ease and simplicity, while, at the same time being very economical in memory usage. You can easily add speech to most existing programs. Due to its remarkable infinite vocabulary, its uses spread throughout the whole spectrum of computer applications — these include industrial, commercial, educational, scientific, recreational etc. No specialist installation — no need to open your computer, simply plugs into the user port — and due to the simple software, no ROMS are needed. SMARTMOUTH is supplied with demo and development programs on cassette, and full software instructions. £37 + £2.50 carriage.

EPROM ERASERS

UV1T Eraser with built-in timer and mains indicator. Built-in safety interlock to avoid accidental exposure to the harmful UV rays. It can handle up to 5 eproms at a time with an average erasing time of about 20 mins. £59 + £2 p&p.

UV1 as above but without the timer. £47 + £2 p&p.

CONNECTOR SYSTEMS

I.D. CONNECTORS

(Speedblock Type)			
No of ways	Header	Receptacle	Edge Conn.
10	90p	85p	120p
20	145p	125p	195p
26	175p	150p	240p
34	200p	160p	320p
40	220p	190p	340p
50	235p	200p	390p

D CONNECTORS

No. of ways			
MALE			
Solder	80p	105p	160p
Angled	150p	210p	250p
FEMALE			
Solder	105p	160p	200p
Angled	165p	215p	290p
Hoods	90p	85p	90p
IDC 15-way plug	340p	Socket	400p
IDC 25-way plug	385p	Socket	450p

TEXTUOL ZIF

SOCKETS	24-pin	£5.75
	40-pin	£9.75

DIL SWITCHES

4-way	70p	8-way	130p
6-way	100p	10-way	150p

JUMPER LEADS

24" Ribbon Cable with Headers				
1 end	14-pin	16-pin	24-pin	40-pin
2 ends	145p	165p	240p	350p
	210p	230p	345p	540p
24" Ribbon Cable with Sockets				
1 end	20-pin	26-pin	34-pin	40-pin
2 ends	160p	200p	280p	300p
	290p	370p	480p	525p

RS 232 JUMPERS

(25-way D)	
24" Single end Male	£5.00
24" Single end Female	£5.25
24" Female-Female	£10.00
24" Male-Male	£9.50
24" Male-Female	£9.50

DIL HEADERS

Solder Type		
IDC Type		
14pin	40p	100p
16pin	50p	110p
24pin	100p	150p
40pin	200p	225p

AMPHENOL CONNECTORS

Solder		
IDC		
36-way plug Centronics	£5.25	£5.25
36-way socket Centronics	£5.50	£5.50
24-way plug IEEE	£5.00	£4.75
24-way socket IEEE	£5.00	£4.75
PCB Mtg Skt Ang pin		
24-way 500p	£6.50	
Female 550p		

RIBBON CABLE

(Grey/meter)	
10 way	40p
16 way	60p
20 way	85p
26 way	120p
34 way	160p
40 way	180p
50 way	200p
64 way	280p

EURO CONNECTORS

Plug	
Skt.	
DIN 41617	160p
21-way	165p
31-way	170p
DIN 41612	
2x32-way St. Pin	230p
2x32-way Ang. Pin	275p
3x32-way St. Pin	260p
3x32-way Ang. Pin	375p
1 DC Skt A - B	275p
A - C	350p
For 2 x 32-way please specify spacing (A - B, A - C)	

EDGE CONNECTORS

0.1"	
0.156"	
2x6-way (Commodore)	300p
2x10 way (Commodore)	150
2x12-way (Vic 20)	350p
2x18-way	140p
2x23-way (ZX81)	220p
2x25-way	225p
2x28-way (Spectrum)	200p
2x36-way	250p
1x43-way	260p
2x22-way	190p
2x43-way	395p
1x77-way	400p
2x50-way (S100conn)	500p

TEST CLIPS

14-pin	375p
40-pin	£10.30
16-pin	400p

7A SERIES table listing components like 7400 POA100P, 7401 90P, 7402 100P, etc., with prices and quantities.

LINEAR ICs table listing components like AD7588, AD7589, AD7590, etc., with prices and quantities.

COMPUTER COMPONENTS table listing CPUs (8088, 8086), CONTROLLER, MEMORIES, SUPPORT DEVICES, ROMs/PROMs, EPROMs, LOW PROFILE SOCKETS BY TI, WIRE WRAP SOCKETS BY TI, TRIACS PLASTIC, BRIDGE RECTIFIERS, PCB MOUNTING RELAYS, ZENERs, and DISC CONTROL ICs.

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NEW LIGHT ON MULTIMETER

An optional feature of the new Philips PM 2518 Multimeter is a low-power electroluminescent strip which acts as a back light for the large l.c.d. The display is automatically illuminated when the ambient light level is too low. This enables the use of the meter in dark and awkward places such as testing equipment on site and in photographic darkrooms. The backlight also switches itself off automatically if no reading has been taken for 30s. With the back light illuminated, the meter still has a battery life of some 200 hours.

The meter uses a microprocessor linked to other i.c.s internally by the Philips/Intel I²C (inter integrated circuit) bus. An I²C adaptor will be offered as an option which will allow users of the meters to carry out maintenance and calibration tests with the meter interfaced to a computer.

Facilities offered by the meter are claimed to match those of many bench multimeters. It is autoranging and offers a basic d.c. accuracy to within 0.1%. Alternating voltage and current measurements are true r.m.s. Voltage measurements are up to 1kV and (with a special high current probe) current measurements are up to 30A. Resistance range is between 1k Ω and 100M Ω with a resolution in the 1k Ω range of 100m Ω . There is also a diode test facility, a dB scale, a beeper output for continuity testing which also acts as a warning if any range is exceeded. Temperature readings between -60 and 200°C are possible with an optical temperature probe. There is very little bandwidth (10Hz to 100kHz) for a.c. measurement which combined with the true r.m.s. reading is very suitable for audio measurement. Bandwidth may be increased further with h.f. probes, up to 1GHz. Safety test leads are provided which are unaffected by, for example, burning with a soldering iron. A wide range of optional accessories are available including the various probes mentioned above. The basic costs £165; with back light it comes to £199. Pye Unicam Ltd, York Street, Cambridge CB1 2PX.

EWV 210



EPROM ERASERS

Three new low-cost eprom erasers have been designed for use in the laboratory, classroom and by the hobbyist. All three versions use a simple drawer construction for easy access. The drawer is lined with high-density anti-static foam to hold (depending on the model) 20 or 40 devices to be erased at one time. A low-power light source has been selected to keep the unit cool while emitting the correct level to the eproms. The tube is fully enclosed. Unit 82 for 20 devices costs £31.25, 84 takes 40 devices and costs £44.95 and for a further £10, Unit 84T may be purchased and this includes a timeswitch to prevent over-cooking the chips. Time is variable between 10 and 30 minutes. An l.e.d. indicates when the unit is working. J. P. Designs, 37 Oyster Row, Cambridge CB5 8LJ.

EWV 211

INDUSTRIAL CONTROLLER

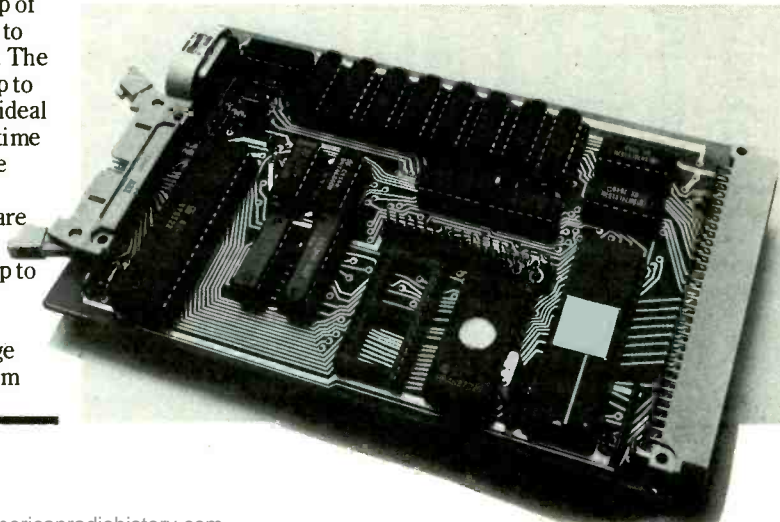
A single board computer based around a 6809 processor has been especially produced to suit the needs of the engineer and process designer. The 6809 has a wealth of readily available software and programs may be developed quite easily for a particular application. This single Eurocard may be interfaced with the Acorn/BBC computer, which may then be used as a development system for the software that will run on the controller. The system may be used to write programs in the control language PL9, or any of a number of languages including BCPL, Pascal, C or assembler. The use of the board is very flexible and the memory map of the system can be redefined to any preferred configuration. The control board can address up to 64K of read/write memory, ideal for applications where real-time data storage is required. The board incorporates battery back-up circuitry and there are two sockets for eight-bit memories such as eproms up to 16K, or 8K c.mos or n.mos read/write memories.

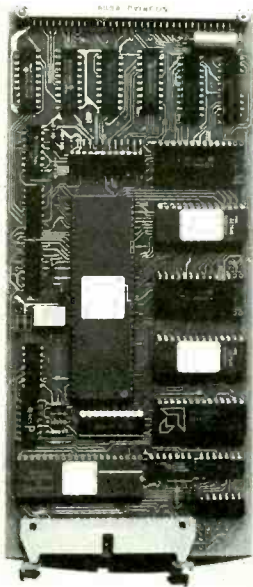
Thus its capabilities range from a device with 32K of rom

and 32K of ram or just 4K of rom and 56K of ram or in a minimal configuration of 4K rom and 2K of ram. So superfluous functions may be removed, thus cutting the cost of the controller card. The on-board versatile interface adaptor provides two 8-bit parallel t.t.l.-level i/o ports with protocol control lines and there are a pair of interval timers for real-time interrupts. The v.i.a. communicates with the outside world through a 26-way connector. Microprocessor control, data and address lines are available through a 64-way edge connector and not only will this connect to a host computer but may also be used to connect

other cards such as extra digital i/o, a-to-d and d-to-a converters, opto-isolated mains switches and any other Acorn-bus compatible circuits. The board may also be used as a second processor for the Acorn/BBC computer by way of an interface board and may then be used to run Flex software. The basic price for the 6809 board is £229, another £20 will get you the 6809-to-BBC interface, software on floppy disc to link the BBC and 6809 is £10 and also on disc is an unconfigured Flex with assembler and editor and full operational manual for £130. Cambridge Microprocessor Systems Ltd, 11 St. Margarets Road, Girton, Cambridge CB3 0LT.

EWV 212





BUILD A 16-BIT CONTROLLER

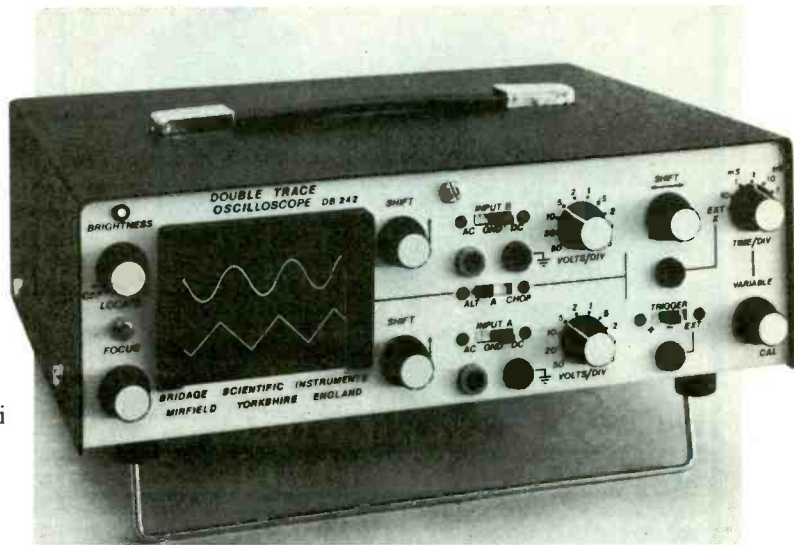
A microcomputer dual-processor controller card is built around the Motorola 68000 and 68701 processors. It features on-card eeprom (up to 32Kbytes) and ram (16Kbytes), a real-time clock, serial RS232 interface and a parallel printer port. The card is designed to the G64 bus specification and comes on an extended Eurocard. This card may be combined with a 256Kbyte memory card and a dual-density disc controller to form the SAT-16 computer system. The control system gives four selectable data transmission rates, an on-card self test that is carried out each time there is a power reset, direct memory access operation and is easily expandable. Interfacing to the G64 bus is provided by tri-state buffers, data transfers are asynchronous for off-card memory and on-card resources but synchronous for peripherals. Any existing eight-bit peripheral which is G64 compatible may be used directly with the Sat-16 card.

The 68701 contains software programmed within it that provides the user with the normal communications dialogue with its co-processor the 68000 and a number of user commands. The software is installed within the 68701 at manufacture but may be modified, although a 68701 programmer is needed for this.

The system is aimed at giving would-be 16-bit users a system at

LOW-COST OSCILLOSCOPE

This general purpose, dual-trace oscilloscope costs £225 and is made by Bridge, in Skipton, N. Yorkshire. The DB242 has been specially developed to cater to the needs of educational and industrial laboratories, and test and service bays. Small in size and portable, the oscilloscope is also suitable for radio, tv and hi-fi maintenance. Ease and speed of use have been considered important in producing an instrument which the makers claim is easy to understand and yet versatile. The display has a medium-persistence phosphor on a 60 by 50mm screen which has a calibrated graticule. There is a trace location button and an auto brightline triggering system. Sensitivity can be varied from 50mV/cm in independent



switched sequences for each channel. Sweep speeds can be varied from 1µs/cm to 0.2s/cm using a calibrated switch. The scope complies with British and EEC safety standards and has been made with safety in mind. A

cheaper single-trace version with the same general specification costs £195. Bridge Scientific Instruments Ltd, 63 High Street, Skipton, North Yorks. BD23 1EF. EWW 231

LOGIC ANALYSER FOR HOME MICRO

An add-on unit which turns the Acorn/BBC computer into a logic analyser is available. The Hawk 3210S is controlled from the computer's keyboard and provides 32 t.t.l. or variable threshold input channels. The computer with disc drives, monitor and printer is used to provide diagnostic processing, display, recording and hard copy facilities. Once data has been recorded on disc it can be processed by the computer as the requires.

Each channel captures 1024 samples, including any glitches, timed by an internal clock programmed to run at 10MHz, or by an external clock. Triggers may be programmed in binary, octal, hex, decimal or ASCII for each channel and pre or post triggering can be varied by up to 1024 samples delay.

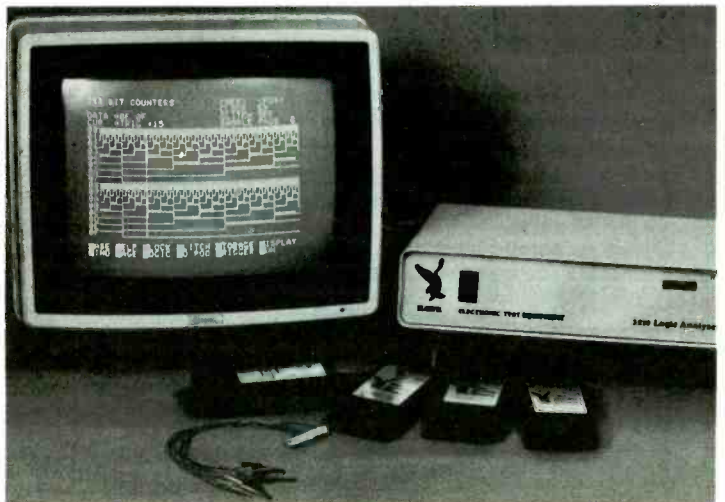
In timing mode the system can display 16 out of the 32 channels concurrently for comparison, while in parallel mode all 32 channels can be

displayed in the chosen format. Glitches are detectable to 30MHz and their display is optional, as an overlay to other data. The unit is menu driven, with on-screen prompts and a 'help' display page. Most programming selections are made by a single key input.

Another version of the unit is available for use with Apple II and IIe computers. Hawk Electronic Test Equipment, Bircholt Park Industrial Estate, Maidstone, Kent ME15 9XT. EWW 232

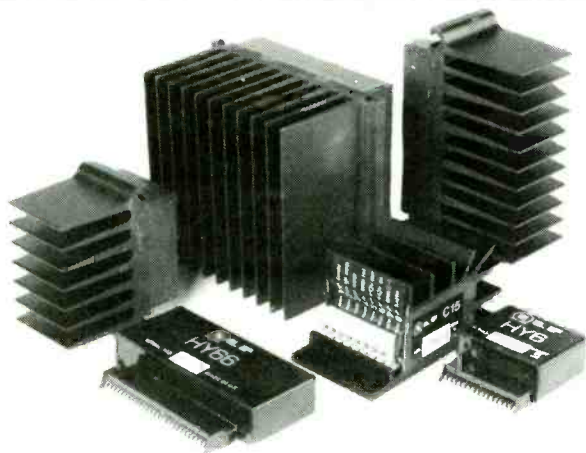
a reasonable cost which can be for single-board applications or expanded as required.

Built and tested the c.p.u. card costs £299; in kit form it's £280, and a starter kit which includes the bare p.c.b., p.a.l. devices, 68701, i/o software and full documentation is £150. Built modules, kit or bare boards are available for the RS232/printer adaptor, a six-slot back board and a bus terminator board. Satellite Services Ltd, 9 King Street, Sileby, Leics LE12 7LZ. EWW 230



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PREAMPLIFIER MODULES

All modules are supplied with in line connectors but require potentiometers, switches etc. If used with our power amps they are powered from the appropriate Power Supply.

Type	Application	Functions	Price
HY6	Mono Pre Amp	Full Hi Fi facilities	£7.95
HY66	Stereo Pre-Amp	Full Hi Fi facilities	£4.95
HY73	Guitar Pre-Amp	Two Guitars plus Microphone	£15.95
HY78	Stereo Pre-Amp	As HY66 less tone controls	£14.95

MOUNTING BOARDS: For ease of construction we recommend the B6 for HY6 £0.95 B66 for HY66-78 £1.45.

BIPOLAR MODULES

Ideal for Hi Fi, Full load line protection integral Heatsink, slew rate 15v/μs

Distortion less than 0.01%

Type	Output Power Watts (rms)	Load Impedance Ω	Price	Type	Output Power Watts (rms)	Load Impedance Ω	Price
HY30	15	4-8	£8.95	HY244	120	4	£26.95
HY60	30	4-8	£9.95	HY248	120	8	£26.95
HY6060	30 + 30	4-8	£19.45	HY364	180	4	£39.95
HY124	60	4	£20.95	HY368	180	8	£39.95
HY128	60	8	£20.95				

MOSFET MODULES

Ideal for Disco's, public address and applications with complex loads (line transformers etc.). Integral Heatsink slew rate 20v/μs distortion less than 0.01%

Type	Output Power Watts (rms)	Load Impedance Ω	Price	Type	Output Power Watts (rms)	Load Impedance Ω	Price
MOS128	60	4-8	£30.45	MOS364	180	4	£45.95
MOS248	120	4-8	£39.95				

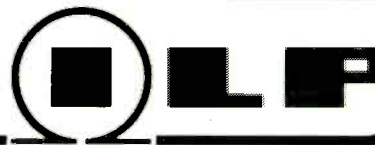
POWER SUPPLY UNITS

Type	For Use With	Price	Type	For Use With	Price
PSU212	1 or 2 HY30	£11.95	PSU542	1 HY248	£17.95
PSU412	1 or 2 HY60, 1 HY6060, 1 HY124	£13.95	PSU552	1 MOS248	£19.95
PSU422	1 HY128	£15.95	PSU712	2 HY244	£21.95
PSU432	1 MOS128	£16.95	PSU722	2 HY248	£22.95
PSU512	2 HY128, 1 HY244	£17.45	PSU732	1 HY364	£22.95
PSU522	2 HY124	£17.45	PSU742	1 HY368	£24.45
PSU532	2 MOS128	£17.95	PSU752	2 MOS248, 1 MOS368	£17.95

All the above are for 240v operation.

FOR FREE DATA PACK PLEASE WRITE TO OUR SALES DEPT.

Post to: ILP Electronics Ltd., Dept. 6
Graham Bell House, Roper Close,
Canterbury, Kent. CT2 7EP
Tel: (0227) 54778 Telex: 965780



CIRCLE 65 FOR FURTHER DETAILS.

Happy Memories

Part type	1 off	25-99	100 up
4116 200ns	1.25	1.15	1.10
4164 200ns	4.95	4.40	4.20
2016 150ns	4.75	4.25	4.05
6116 150ns Low power	Call	Call	Call
6264 150ns	Call	Call	Call
2716 450ns 5 volt	3.85	3.45	3.30
2732 450ns Intel type	4.20	3.75	3.60
2532 450ns Texas type	3.85	3.45	3.30
2764 250ns	Call	Call	Call
27128 300ns	Call	Call	Call

Z80A-CPU	£2.99	Z80A-P10	£2.99	Z80A-CTC	£2.99
6522 PIA	£3.70	7805 reg	£0.50	7812 reg	£0.50

Low profile IC sockets:	Pins	8	14	16	18	20	22	24	28	40
	Pence	12	13	14	16	18	22	24	27	38

Soft-sectored floppy discs per 10 in plastic library case:
5 inch SSSD £17.00 5 inch SSDD £19.25 5 inch DSDD £21.00
5 inch SSQD £23.95 5 inch DSQD £26.35

74LS series TTL, large stocks at low prices with DIY discounts starting at a mix of just 25 pieces. Write or phone for list

Please add 50p post & packing to orders under £15 and VAT to total Access & Visa welcome. 24 hr phone service on (054 422) 618 Government & Educational orders welcome, £15 minimum Trade accounts operated, phone or write for details

**HAPPY MEMORIES (WW)
Gladestry, Kington
Herefordshire HR5 3NY
Tel: (054 422) 618 or 628**

pantechnic

THE POWERFET SPECIALISTS

OEM USERS

Pantechnic present the most adaptable high-powered amplifier ever.

FET SYSTEM AMP

Features:

- HIGH POWER up to 1.2kW (single ended)
 - LOW VOLUME. 1/16 Cubic foot inc. Heatsink
 - VERSATILE. Delivers more than 1kW into 1/2 to 8 ohms
- OR 2 x 600W into 2 to 8Ω
OR 4 x 300W into 2 to 4Ω (200W into 8Ω)
- OR { 1 x 600W into 2 to 8Ω
1 x 300W into 2 to 4Ω
1 x 150W into 4 to 8Ω
- Etc., etc.

Having been closely involved in a wide variety of OEM applications of their amp boards. Pantechnic became aware of numerous implementation problems often left untackled by other amp board manufacturers. These problems specifically of size and thermal efficiency became particularly aggravated at high powers and considerably lengthened OEM product development time.

By including thermal design in the totality of board design it has been possible to reduce the size of the electronics, and increase the efficiency of the transistor to heatsink thermal circuit. The combined effect of this has been to dramatically increase the volumetric efficiency of the amplifier/heatsink assembly. The SYSTEM Amp offers 1.2kW of power in a space of 180mm x 102mm x 77mm, excluding PSU and Fan.

The basis of this considerable advance is the PANTECH 74 Heat Exchanger, designed and manufactured by us. By eliminating the laminar air flow found in conventional, extruded heatsinks, heat transfer to the environment is greatly enhanced.

The flexibility of the 1.2kW amp stems from its division into 4 potentially separate amplifiers of 300W each (downrateable with cost savings to 150W). These can be paralleled, increasing current capability or seriesed (bridged in pairs) doubling voltage capability. In consequence a large variety of amplifier/load strategies can be implemented.

As ever Pantechnic offer a full range of customising options including DC coupling, ultra-high slew, etc. Contact Phil Rimmer on 01-361 8715 with your particular application problem.

P.S. Specs, as ever, are exemplary.

A wide range of other amplifiers and other modules available.

Price and Delivery
PANTECHNIC (Dept. WW6)
132 HIGH ROAD,
NEW SOUTHGATE,
LONDON N11 1PG

Technical Enquiries
contact
Phil Rimmer
on
01-361 8715

CIRCLE 58 FOR FURTHER DETAILS.

6VA MINIATURE TX 240V AC Input 12-0-12V Output P.C. Mounting + Internal thermal overload protection. £25 for 10 + VAT £115 for 50 + VAT, £210 for 100 + VAT, £950 for 500 + VAT. Sample sent for £3 + 75p P and P (£4.30 inc. vat).

MINIATURE SKELETON Preset horizontal mounting 220R @ 0.1W 5.1MM X 10.2MM pitch, £35 for 1,000 + VAT.

BERG LOW PROFILE 14-PIN DUAL IN-LINE IC SOCKET manufactured from glass filled polyester to UL94V-0. £7 for 100, £31 for 500, £56 for 1000, £256 for 5,000, £460 for 10,000 £2,100 for 50,000, £3,700 for 100,000. Sample 10 sent for £1.20 + 30p P and P (£1.72 inc. VAT)

BERG LOW PROFILE 16 PIN DUAL IN-LINE IC SOCKET as above £8 per 100, £36 for 500, £65 for 1,000, £295 for 5,000, £530 for 10,000, £2,390 for 50,000, £4,300 for 100,000. Sample 10 sent for £1.40 + 30p p&p (£1.96 inc VAT).

215MA 32mm QUICK BLOW GLASS FUSE £5 for 100, £48 for 1,000.

TO3 HEATSINK. Efficient space saving to 03 Heatsink. Suitable for on-board mounting. Flat surfaces ensure high thermal conductivity. Pre-drilled to accept any standard TO3 device. Height 12mm, width 36mm, length 47mm black anodised finish. £20 for 100 + VAT, £150 for 1,000 + VAT, sample 10 sent for £2.50 + VAT and p&p.

HIGH POWER SILICON BRIDGE RECTIFIER. 25 amp 600V single hole fixing 250 (1/4") push on connector terminals, manufactured by I.R. £20 for 10, £90 for 50, £175 for 100, £800 for 500, £1,450 for 1,000. Special quotations for larger quantities. Sample sent for £2.50 + 25p p&p (£3.16 inc VAT).

METAL FILM RESISTOR TYPE FZ4. Manufactured by C.G.S. semi precision with a standard tolerance of $\pm 2\%$ and a temperature co-efficient of better than 100 ppm/oc. We have a full range in stock from 100R to 1M Ω . All bondoliered. £2.50 per 1,000 any one value.

ZENER DIODES manufactured by Thompson C.F. all bandoliered. BZX79 C18 — BZX79C20 — BZX83 — C20, £12 for 1,000 of one type, £15 per 1,000 assorted. Sample 100 sent for £3 + 25p p&p (£3.74 inc. VAT).

STEREO CASSETTE FRONT LOADING REPLAY MECHANISM for in-car entertainment complete with motor and pre-amplifier. Manufactured in UK under licence of Staar S.A. £45 for 10 + VAT £205 for 50 + VAT £375 for 100 + VAT. Sample for £5 + £1.50 p&p (£7.48 inc VAT).

TERMS C.W.O. Please add 5% to all orders for carriage plus 15% VAT. Export enquiries welcome. We find it impossible to advertise all we stock. Please telephone or write for further enquiries. Personal callers always welcome.

ELECTRONIC EQUIPMENT CO.

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TYSSON STREET, LONDON, E.8
TELEPHONE: 01-249 5217
TELEX: 9853906 EECO.G

CIRCLE 52 FOR FURTHER DETAILS.

Tiny BASIC Eurocard Computers using the INS 8073 plus

FULL RANGE OF INTERFACES

£185 BUYS PROCESSOR CARD WITH 48 io, 2Kram, RS232, EPROM PROGRAMMER, CLOCK FUNCTION, WATCHDOG etc

ALL SYSTEMS AUTO-START & RE-START FOR RELIABILITY

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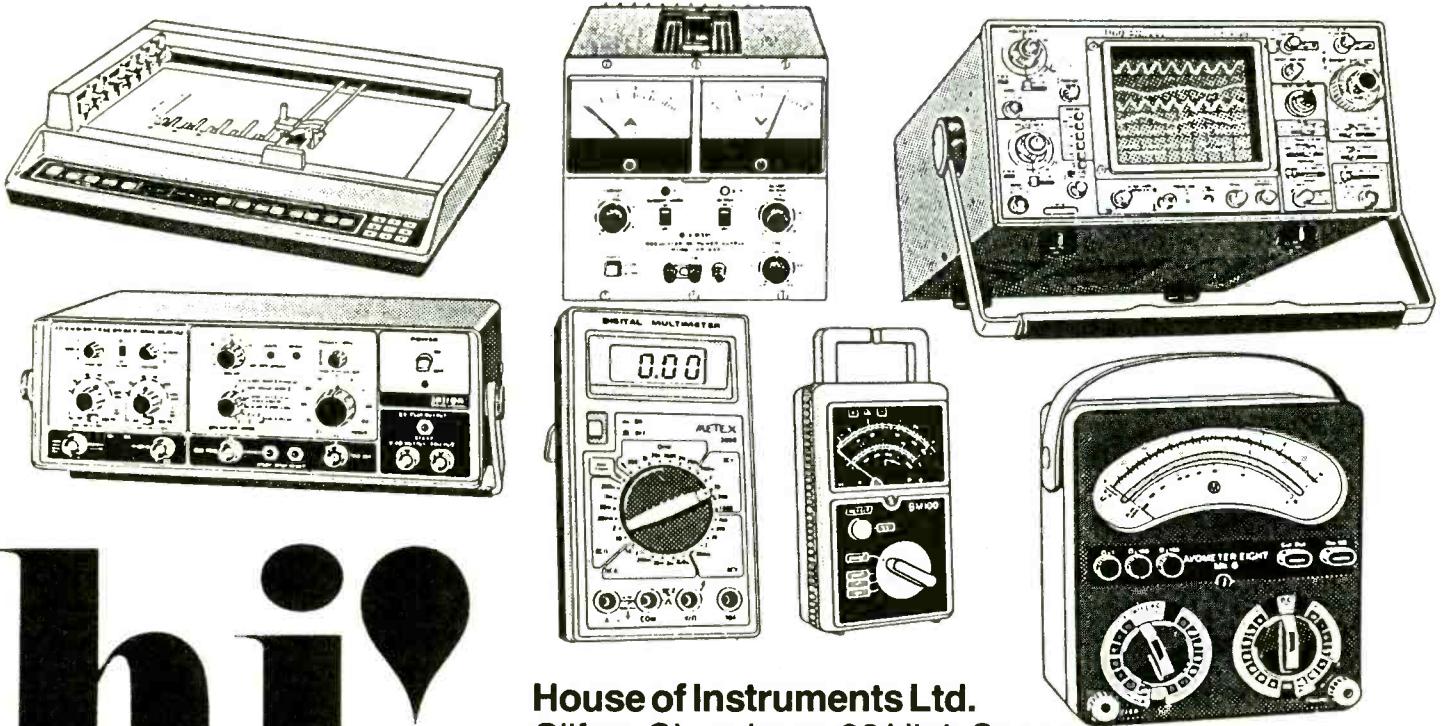
Broadway
Dukinfield
Cheshire
SK16 4UU

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CIRCLE 64 FOR FURTHER DETAILS.

Total Test and Measurement Capability

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Telephone: (0799) 24922 Telex: 818750

CIRCLE 39 FOR FURTHER DETAILS.

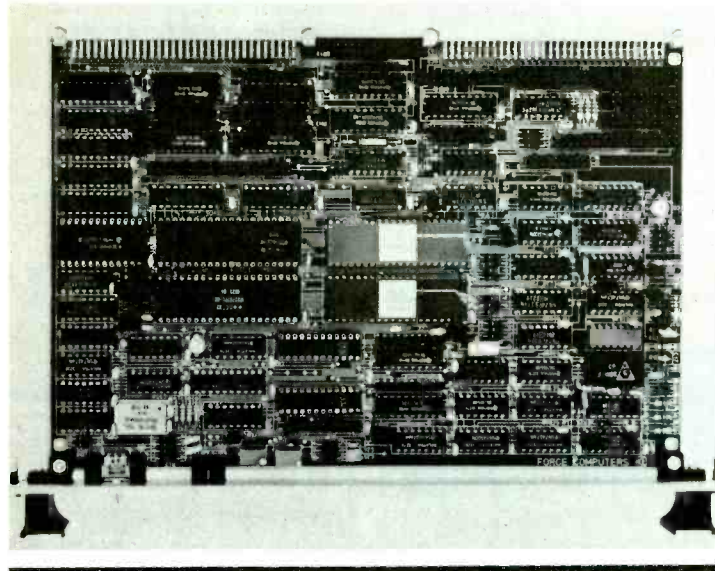


WINCHESTER/ FLOPPY DISC CONTROLLER

Compatible with the VME bus, the Force disc drive controller features user-programmable d.m.a. channels, up to 16Kbytes of dual-port ram, and double Eurocard sized p.c.b. with DIN 41612 connectors.

The board is capable of supporting up to four floppy-disc drives and up to three hard-disc 5 $\frac{1}{4}$ in drives. It generates interrupts with user-selectable

interrupt levels, and auto interrupt vectors. The SYS68K/WFC-1, allows a programmable sector size up to 1Kbyte, and provides automatic track formatting for hard discs. The data transfer rate is up to 5Mbit/s. Available from Microsystem Services, PO Box 37, Lincoln Road, Cressex Industrial Estate, High Wycombe, Bucks. HP12 3XJ. EWW 213



VIDEO SYNCHRONIZER FOR THE BEEB

A device to synchronize the RGB output of the Acorn/BBC computer to a video signal allows it to be used as a low cost alternative to professional tv caption and graphics generators. The Beeb-Lock is housed in a small case and is connected to the computer's p.c.b. with a few simple connections. The unit includes a PAL colour encoder and colour genlock system to convert the RGB output from the computer into a synchronous PAL colour signal which can be combined with a video signal through a vision mixer. One version, BL.2K, includes a mix/key circuit and provides a complete system for those users who require a basic title and caption insertion or fade facility. Another model, BL.3 is fitted with a Micropal board instead of the PAL encoder. This decodes the reference video signal into

RGB components prior to combining them with the RGB output taken directly from the computer. The final output is a linear RGB signal which can be displayed directly on a colour monitor.

A future enhancement, available toward the end of the year, is to be a colour mapping board which will be able to select eight colours from several million variations. This makes possible the selection of several shades of the same colour for use in shadow and modelling effects.



SWITCHING MULTIPLEXER FOR NETWORKS

A solution to the problems of interconnecting dispersed multi-terminal data processors is offered by Babynet, a switching multipoint multiplexer. It combines switching (port selection and contention) with multipoint multiplexing. The switching capability allows dynamic mapping of connections between remote terminals to a computer. Remote ports can be permanently mapped to a particular computer port, mapped on terminal connection to one of a predetermined group of computer ports, or routed to one port of a user specified group. All port groups are designated by alphanumeric strings so that the terminal user could specify, for example, 'PDP11', 'VAX' or 'Accounting' on connection. This allows a large number of terminals to use a small number of computer ports, and also allows one terminal to be connected to a number of computer systems.

The multiplexer used a single communications line with its own polling method called 'Adaptive

Polling Technique'. With APT, Babynet continually monitors remote station activity and polls active stations at a much higher rate than inactive ones. This results in a faster response time for terminal users.

Babynet is an expandable system with three functions (master, master expansion and node) all in the same piece of hardware. All units start as two channels and may be upgraded in increments of three channels. A master can have up to 22 ports and up to eight nodes, each with eight ports.

The configuration of each Babynet is a simple matter of pushing the right buttons on the front panel. A control console may also be used, if needed. Each Babynet also capable of self-testing, terminal testing and diagnostic functions. The system is transparent to the user; no systems or applications programming is necessary. It works not only with v.d.u. terminals but also with virtually any asynchronous RS232 device including printers and bar-code readers. Error detection and correction is built in to the system and is completely automatic. The Babynet system is designed for unattended operation. Start-up is completely automatic and preprogrammed configurations are retained even when the power is off. Network Products Ltd, 387 Sykes Road, Slough Trading Estate, Slough, Berks. EWW 215

The price of the basic Beeb-Lock, which is powered from the computer's auxiliary socket, is £193 An enhanced version. BL.2 may be expanded by the addition of optional p.c.b.s and includes a mains power supply for £240. Models BL.2K and BL.3 mentioned above are £330 and £260 respectively. Two-channel video mixers are available from the same designer/manufacturers: Video Electronics Ltd, Wigan Road, Atherton, Manchester M29 0RH. EWW 214

MINIATURE SOCKET

The high-profile version of the Harwin sub-miniature socket is designed to give a maximum protrusion below a p.c.b. of less than 1mm. This means that the socket's tail will be untouched by any conventional lead cropping process. Inside the socket is a four-leaf beryllium copper contact designed to accept the leg of any standard i.c. Use of the socket allows high density packing of i.c.s and offers lower than average insertion/withdrawal force. Harwin Engineers SA. Fitzherberts Road, Farlington, Portsmouth, Hants PO6 1RT EWW 216

D.I.L. LINKS

Programmable links offer a low-cost alternative to d.i.p. switches for many applications where frequent changes are not necessary. The Series 680 programmable headers from Aries can be operated by simply severing the links between pins. One style of header can be used to program connections between both adjacent and opposite pins. It has a plain cover through which opposite links may be broken. A hand tool is available for small production runs or an arbour press for bulk programming. The headers may also be bought



pre-programmed. Aries Electronics Ltd, Alfred House, 127 Otlands Drive, Weybridge, Surrey KT13 9LB.

WW 227

BORROW AN OSCILLOSCOPE

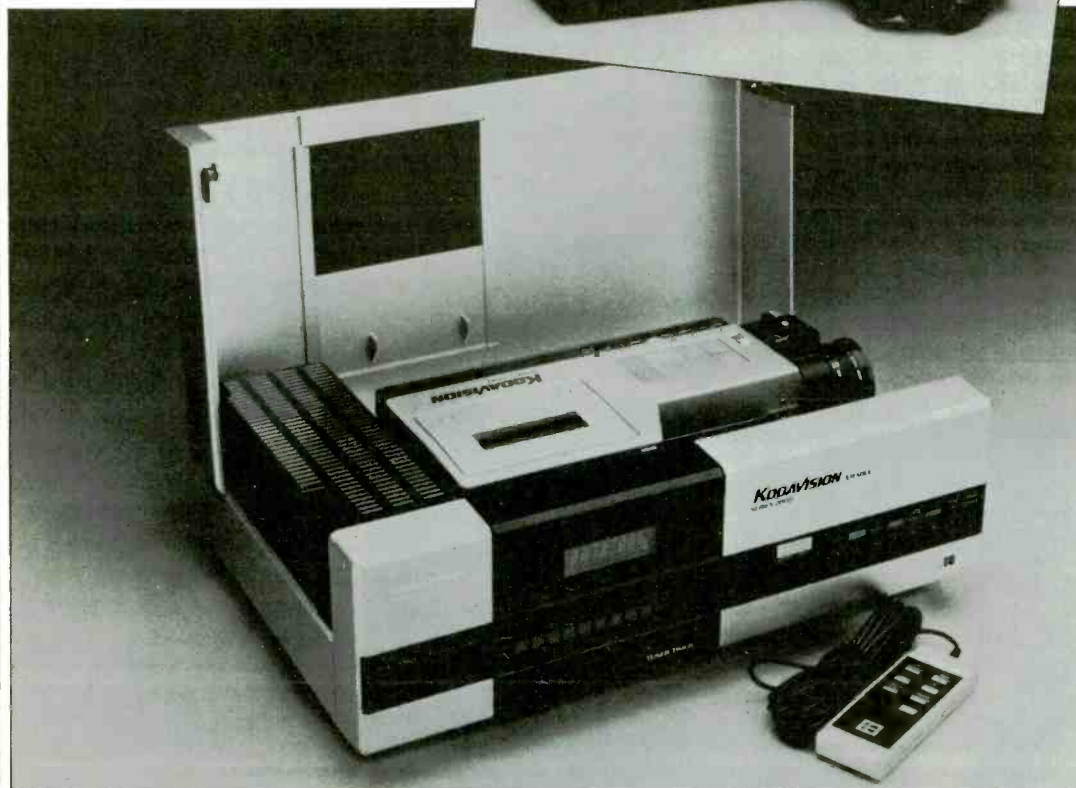
If you have sudden need of an oscilloscope, perhaps for prototype testing, you can hire one from Microlease. For example they now have the latest Nicolet 3091 portable digital oscilloscope which uses 12-bit digitizing and is claimed to be ten times more accurate than analogue instruments. It may be used for field calibration, fault diagnosis, or transient analysis, in mechanical, electrical, acoustical and biological applications. It may be linked to a computer by way of an RS232 interface, and to plotters and chart recorders for waveform

printouts. Weekly rental is from £70, including bubble memory cassette. Microlease plc, Forbes House, Whitefriars Estate, Tudor Road, Harrow, Middlesex HA3 5SS. WW 226

WIREWRAPO TOOL

This bit and sleeve combination is able to cut off excess wire for cable, wire harness or reel, strip the proper length of insulation, and wrap the correct number of turns onto the terminal. This eliminates the need for pre-cutting or pre-stripping the wire. Used in the same way as conventional wire wrapping tool bits and sleeves, the CSW sets are available for 0.50, 0.40 and 0.25mm wire and a wide range of terminal sizes. OK Industries UK Ltd, Dutton Lane, Eastleigh, Hants SO5 4AA. WW 229

Extending their horizons from the purely photographic to other images, Kodak have produced a home video system. The core element is a video camera/recorder (Camcorder) which uses 8mm wide tape in cassettes about the same size as audio compact cassettes and lasting for 60 minutes for PAL signals or 90 minutes with NTSC. The Camcorder is no larger than an average amateur movie camera and weighs 2.4kg, yet a similar quality to the average video cassette recorder is claimed. This has been achieved, says Kodak, through the use of cobalt-nickel metal tapes, amorphous metal recording heads in the helical scan recorder and the development of a new 0.3in (85mm) Newvicon tube. For display on a domestic tv, the Camcorder fits into a 'cradle' which provides the electronics and also acts as a battery charger for the camera. The camera has all the moving parts and so acts as the heart of the system. The cradle may be fitted optionally with a tuner/timer for the recording of programmes off-air. Soon to be launched in the US, the UK version may be available towards the end of the year.



ANTI-STATIC CARPET SPRAY

An anti-static aerosol spray, ASP 40, has been designed for use on carpets and/or video screens in static-sensitive environments. A walk across a carpet can generate a charge of up to 10 000V, according to the spray manufacturers. This can damage electronic components or cause data glitches in computer equipment. A single canister of the spray can treat up to 20 square metres of carpet. The treatment lasts for two to three months and during this time the carpet has the additional property of being dirt repelling. A video screen will remain clean and static-free for six to eight weeks. £4.20 for a single can, £3.90 each for a pack of six. Technotrend Ltd, The Town House, Chobham, Surrey GU24 6AF. WW 228

If you would like more information on any of the items featured here, enter the appropriate WW reference number(s) on the reply-paid card bound in this issue. Overseas cards require a stamp.

AMAZED FUSED LOGIC

A software package for designing integrated fused logic from Mullard is called AMAZE, which stands for automated map and zap entry. Another acronym involved is BLAST for Boolean logic and state transfer, the first package within Amaze which also includes a device programmer interface and a simulator.

Blast allows the designer to assign pin mnemonics and functions, and to write Boolean equations which are compiled into programming table. Data entry is by way of a menu screen display and the data is checked for consistency and legality before progress to subsequent screens is allowed. Complex functions are reduced to a sum of products by a resident logic processing program.

The DPI (device programmer interface) can download

compiled program tables in selected formats. It can also 'upload' the tables from existing devices for editing and simulation.

The simulator can be run manually or automatically. In manual mode the operator can assign input vector and then observe the resulting output; in automatic mode the simulator creates a test vector file for production testing of the programmed device.

The first release of AMAZE contains the Blast and DPI modules for 82S153 and 82S159 devices and is suitable for use on VAX, VM53.2 or later computers. Personal computer versions will be released later in the year along with the rest of the integrated fuse logic range including the simulator module. Mullard Ltd, Mullard House, Torrington Place, London WC1E 7HD.

EWV 222

MEASUREMENT AND CONTROL INTERFACE

A complete interface system in a single compact package can provide a link between any GPIB controller and the sensors and actuators of laboratory and process automation systems. A single p.c. motherboard accepts plug-in modules which may be configured to provide conditioning and conversion for any combination of analogue and digital input or output signals. Functions currently available

include digital input and output; pulse, event and up/down counting; frequency measurement; real-time clock; and thermocouple, strain gauge and real-time display inputs.

Fully compatible with IEEE 488 and IEC625-1 specifications, the Di-An DMS550 is designed to operate with eight-bit binary characters and enables the transmission and receipt of GPIB data at a maximum rate of 250kHz. Available from STC Instrument Services, Edinburgh Way, Harlow, Essex CM20 2DF.

EWV 223



HEAR AUNTIE FROM ANYWHERE

Specifically designed for the reception of the BBC World Service, the Liniplex F1 h.f. receiver has nine fixed crystal-controlled channels tuned to the frequencies most used by the BBC in various locations around the world. The 5 to 26.5MHz band is also tunable for reception of other s.w. stations. Crystals may be easily changed if a different frequency is required on any of the pre-set channels.

The receiver incorporates a patented a.m. phase-locked demodulator which uses a phase-error signal to control a voltage-controlled oscillator and

the set stays tuned even during a temporary loss of a pilot carrier signal. This is especially useful in areas of multi-path reception and also helps cut out distortion caused by fading signals. Double or single sideband reception is possible and upper, lower or both sidebands may be selected at will. This facility offers the choice of least interference from transmitters at adjacent frequencies. The ability to use a balanced antenna indoors also helps to reduce local interference. Despite its die-cast aluminium case, which is strong and offers electromagnetic shielding, the Liniplex F1 weighs only 1.85kg and is small enough to be slipped into a briefcase. Phase Track Ltd, 132 Queens Road, Reading, Berks RG1 4DG.

EWV 224

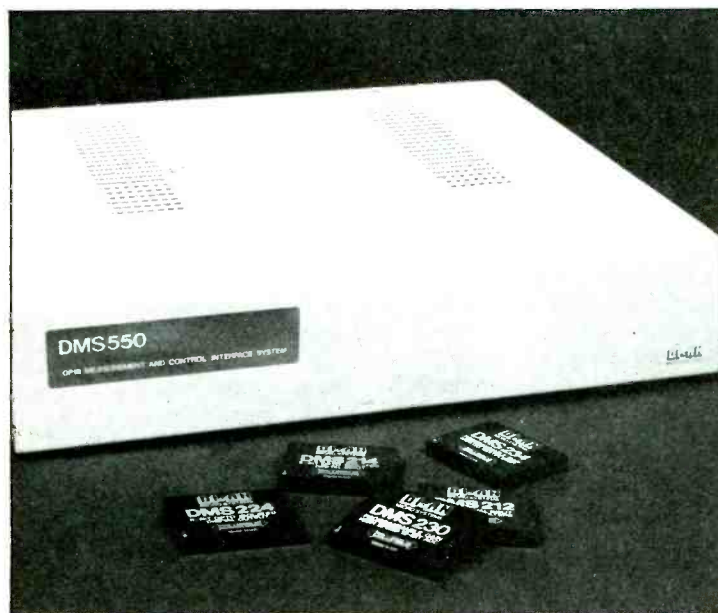
FAST PROMS

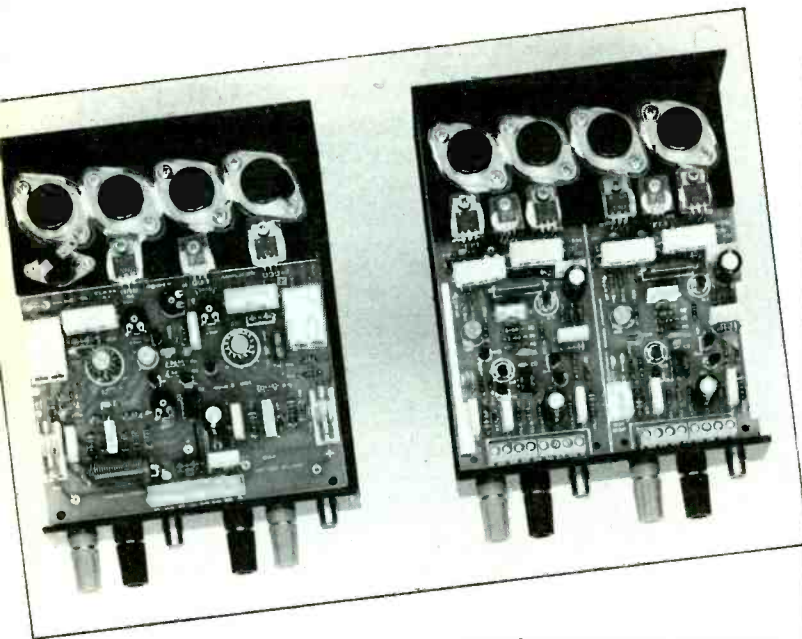
Two 2048byte, edge-triggered, D-type registered proms are claimed to be 20% faster than comparable devices. These bipolar devices consume half the power of a standard prom with an external register. The RA 1681 and RA 1681A are available with synchronous or asynchronous operation and have maximum clock-to-output response times of 20 and 15ns respectively. They feature a flexible initialization scheme which offers a start-up and time-out sequencing of 16 programmable words to provide controlled systems start-up.

The proms are designed to hold microprogrammable control storage, state sequencers, next-address generation and mapping other proms in a wide

range of computer systems. The synchronous devices may be used when multiple registered proms are bussed together to provide increased word length. Asynchronous versions are used when multiple gates are not in use or when the outputs are to be gated on to a data bus. The devices are available with a variety of access modes, refresh modes and set-up modes. Both types includes two externally controlled modes, one access and one refresh. The two auto-access modes of 1681A operate in 130ns, worst case and thus eliminate the wait states usually encountered in fast microprocessor systems. Monolithic Memories Ltd, 1 Queens Road, Farnborough, Hants GU14 6DJ.

EWV 225





BENCH POWER AMPS

Two power amplifiers, a 200W stereo and a 300W mono, are presented in open frame form for o.e.m. and hobby use. S200 the stereo module consists of two completely independent amplifiers which may be operated with separate power supplies, and at different frequencies. The amplifiers may be used for bench testing of equipment and one example has been the amplification of outputs from accelerometers in vibration analysis. With bench use in mind, all connections use screws so that different power supplies or inputs and outputs may be quickly connected. The open

metal frame provides a very large external heatsink.

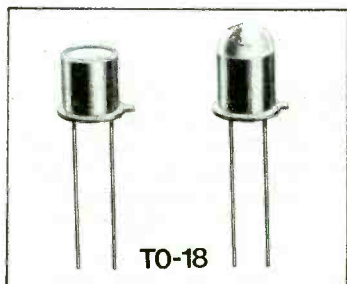
Both the S200 and the M300 amplifiers although rated at their maximum powers may, of course be used at lower power ratings by reducing power supply voltages. In addition the M300 includes preset potentiometers to adjust the gain, allowing ratings to be set precisely. S200 costs £48.50 and M300, £43.50. There is in addition an amplifier drive board which is a complete amplifier without the output power transistors. These may be selected to build amplifier designs from 60 to 250W into 8Ω or 100 to 300W into 4Ω. This module, D100, costs £23.50. XTR Electronics, 335 Holdenhurst Road, Bournemouth, Dorset BH8 8BT. EWW 217

Ge DIODES IDEAL FOR FIBRE OPTICS

A spectral response between 0.5 and 1.8μm, peaking at 1.5μm is claimed to be the ideal wavelength for maximum efficiency in a fibre optical cable and is the wavelength of greatest sensitivity of some new germanium light-receiving diodes. They are available in a TO-18 package with an active receiving diameter of 1mm and a choice of window or lens. Responsivity is up to 0.7A/W, rise time is as low as 10ns and 'dark' current is only 5μA.

The GM5 photodiode may be used in photovoltaic or photoconductive modes and applications include optical communications, optical power

measurement, fibre attenuation measurements, laser burn-in monitoring etc. as well as spectrophotometers and pyrometers. US prices are approximately \$75 each for small quantities. A GM8 photodiode, with a 5mm active diameter in a TO-8 package, costs \$130. Germanium Power Devices Corp. PO Box 3065, Shawsheen Village Station, Andover, MA 01810 USA. EWW 218



SOLID-STATE RELAYS

Housed in standard 14 and 16-pin d.i.l. packages, the range of MSI solid-state relays use thick-film hybrid circuits to combine the handling of high power in a physically small volume. There are three d.c. relays and seven a.c. types with a wide choice of current and voltage ratings, optical or transformer isolation and synchronous or zero-voltage switching.

One of the range is the E24E-2H which has 1A current rating and is housed in a 16-pin package. Input/output isolation is 400Vr.m.s. and the use of anti-parallel s.c.r.s in the power switch ensures enhanced rise time, surge current and thermal characteristics. The device switches at zero volts and requires an input signal of 8mA at 5V. The output switch has a peak voltage rating of 600V and is therefore safe to use with 240V a.c. supplies. Others in the range include the E40-1 which will switch a.c. or d.c. up to 80mA at 60V; E41-2H is rated 1A and has a triac output up to 600V; E43-1 for d.c. switching of 500mA, 60V and the E43-2 also for d.c. at 200mA, 250V. The use of ceramic sealed packages ensures that they are hermetically sealed. They are good conductors of heat and maintain a good safety margin on junction operating temperatures. Elyon Electronics Ltd, 23 Croydon Road, Reigate, Surrey. RH2 0LY. EWW 219

68008 EMULATOR

An addition to the MICE-II range of in-circuit emulators is one for the M68008 processor. It may be used as a stand-alone program development/debugging system or in conjunction with a target computer to allow off-line debugging. The MICE system in such a master-slave configuration can be used to evaluate a number of different processors easily by a simple change of a 'personality' card in the unit. The system can be extended to include several work stations and a Multi-MICE unit can be used to emulate a multiprocessor system. The emulator allows the user to run the target system in real time, eliminating wait states and using

none of the host's memory space. MICE software allow the inclusion of two breakpoints, includes a resident assembler/disassembler, a real-time forward trace for up to 2048 cycles, instruction step or cycle step through a program. There is 32K of emulator memory, expandable in 32K sections. The system as designed to be easy to use and has 23 commands common to all the emulators regardless of the target processor. It is portable and lightweight, permitting on-site testing. ARS Microsystems Ltd, Doman Road, Camberley, Surrey GU15 3DF. EWW 220

DIGITAL TIMESWITCH

A digital electronic time switch can provide up to 84 separate on or off settings in a week — 12 settings for each day. The program may be set for each individual day or a group of up to six settings may be repeated automatically every day. The current time is shown on a display which can also indicate the status of any function or program. A built in battery can retain the program. A built in



battery can retain the program and clock time during a power failure and the battery is automatically recharged when the power is restored. The program may be easily overridden at any time without affecting the memory and operation will revert to the program when the next switch-time is reached. Applications include the switching of heating or air conditioning plant, or manufacturing processes up to a rating of 220V, 10A a.c. Highland Electronics Ltd, 8 Old Steine, Brighton East Sussex BN1 1EJ. EWW 221

Appointments

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1926

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The successful candidate will be fully conversant with BS 415 1979 and have a good knowledge of other standards relating to domestic electronic equipment.

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Bill Jeanes - Technical Director
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(2605)

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Job Description and application form from the Administration Department, tel Exeter (0392) 77883 ext 2007.
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(2589)



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(2593)



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(1935)

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Application forms and further details are available from the Senior Administrative Officer at the above address. Completed application forms should be returned to EO/Estab 3a Room 255a County Hall London SE1 7PB within 14 days of the appearance of this advertisement.

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Please indicate areas in which you are prepared to work:				Are you a houseowner?	Are you willing to relocate?
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Secondary School Qualifications:

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CAREER HISTORY

From/To	Company	Job Title/Description	Salary

Please indicate any Companies you do not wish us to contact.

If you wish to detail further aspects of your experience or job requirements, please continue on a separate sheet.

(2450)

UNIVERSITY OF BIRMINGHAM DEPARTMENT OF ELECTRONIC AND ELECTRICAL ENGINEERING

Postdoctoral Research Fellowship

Applications are invited for the above post which is funded by the MOD. The work is concerned with signal handling in high frequency receivers using digital techniques for filtering and demodulation. There are prospects for a wide range of work and also collaboration with other establishments. Both theoretical and practical skills are required and an ability to direct and to liaise with other staff will be important.

The post is tenable for up to one year from the soonest possible date.

The salary is on the Research Fellow 1A scale £7,190-£11,615 plus superannuation. For further particulars phone 021-472 1301 ext. 2559, quoting reference S3.

No formal application form. Three copies of application, including full Curriculum Vitae and naming three referees to Assistant Registrar, (Science and Engineering), P O Box 363, BIRMINGHAM, B15 2TT by 4 June 1984. (2578)

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(2519)

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Needs Digital Electronics Repair Technicians for expansion of the facility for instrument repair, maintenance and calibration.

Candidates' background should include:-

- ★ Bachelors or associate degree or equivalent military/Technical training.
- ★ Minimum 4 years' hands-on digital experience on micro-mini computers, peripherals, data acquisition systems, micro-processor controlled test instruments.
- ★ Trouble-shooting and repair capability to component level (experience with current model minis, micros and GPIB a big advantage).

Salary is competitive, benefits include annual repatriation, housing and transportation allowances.

Candidates possessing the above requirements should only apply to the following address within one week of the release of this advertisement furnishing details resume of their educational qualifications and experience, attaching copies of their degrees and transcripts, giving names and addresses of four referees, including their present employer, if possible, and the present position held.



Mr. Ali A. Jaman, Director General,
Financial and Admin. Affairs,
Research Institute - University
of Petroleum and Minerals, P.O.
Box 7177, Dammam - 31462,
Saudi Arabia.

2546

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SATELLITE TVRO ELECTRONICS

The expansion of our Development operation has created the requirement for an additional Engineer to work on the design and production development of a new range of satellite television receiving equipment for both professional and consumer applications.

Suitable candidates would preferably hold a relevant degree or HND and have several years experience in commercial product design and development. More important, they should be able to demonstrate aptitude and flair, a genuine interest in the technology of RF, logic and baseband circuitry, and the ability to work without supervision.

Satellite TV Antenna Systems Limited is a small and highly professional British Company with strong prospects of fast growth in this emerging technology and is located in new facilities in Wales.

Salary and benefits are negotiable.

Applications in writing please together with a current C.V.

Mr. P.M. Gray, Managing Director,
Satellite TV Antenna Systems Ltd.,
10 Market Square, STAINES TW18 4RH, Middx.

(2587)

TEST PLANNING TRIALS SUPPORT INTEGRATION & TEST

Are you ready for a commitment to Engineering Excellence?

STC Defence Systems has one of the most impressive growth records in the international defence market. In the short space of 3 years we have more than doubled in size — in both turnover and manpower. Major development projects currently in hand are the direct result of solving technical problems through a commitment to engineering excellence. Increased activity in a wide range of advanced technology fields, such as specialist communications equipment, guidance and control systems and general data communications systems is continuing our record of expansion and has now created the following positions for experienced Electronics Professionals at our Basildon location:

Test Planning

Senior Engineers (up to £13k pa)

We're looking for Senior Engineers to plan a major role in the preparation and planning of test programmes. Working closely with prototype manufacturers and external suppliers, you'll develop stringent test specifications and schedules — from single modules through to complete systems. You'll be involved in extensive customer contact and maintain close liaison with internal trial's support teams. The positions call for the highest standards of professionalism. A degree or HNC level qualification is essential, coupled with at least 4 years' relevant experience in an electronics environment or technical support role.

Trials Support

We are looking for Engineers at all levels to play a key role in conducting acceptance trials pre- and post-product handover, providing a complete testing service to Project Leaders and other Departments as required.

Senior Engineer (£12-£13k pa)

You should be qualified to degree level or equivalent with around 5-7 years' experience in operational test or in the evaluation of electronic equipment in an operational environment.

Engineer (£8-£9k pa)

Aged 23 years +, you'll be qualified to at least HNC level with at least 3 years' relevant experience, possibly gained in

an installation or commissioning role with a major user or supplier of electronic equipment.

Systems Integration & Test

We're looking for people from Section Head to Engineer level to be responsible for the integration of the hardware and software elements of complex high technology systems. You will be involved in producing proposals on software simulation and hardware modelling to meet stringent product requirements for harsh environments and for identifying and conducting test programmes.

Section Head (£13-£14k pa)

Qualified to degree level or equivalent, you should have 5-7 years' proven experience including a sound background in both hardware and software.

Senior Engineers (£12-£13k pa)

Aged 25 years + you'll be qualified to degree/HNC level with around 3 years' sound relevant experience.

We would like to discuss all these key positions with Engineers who are looking for their next challenge in Electronics. Necessary personal qualities include the ability to work to deadlines and under pressures, with the minimum of supervision. Working with STC Defence Systems will bring you exceptional opportunity to grow within a young, dynamic environment and share in the company's success. Very competitive salaries are offered together with an attractive range of benefits including an exceptional relocation package where appropriate.

Please send your c.v. to our consultant, John Faith at Cambridge Recruitment Consultants, 1a Rose Crescent, Cambridge CB2 3LL, quoting reference TP/TS/TC or telephone Cambridge (0223) 311316 for an application form. These positions are open to both men and women.

STC TELECOMMUNICATIONS



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ADVANCED BROADCAST TECHNOLOGY TV STUDIO AUDIO & VIDEO SYSTEMS TO £18000

Dedication to engineering excellence and technical innovation has established our client as one of the world's leaders in the design, development and manufacture of TV Studio equipments and systems for a wide range of applications within the broadcast industry. Continued expansion and total commitment to an exciting and dynamic development programme has created unique career opportunities for a small number of engineering professionals to play major roles in the conception, design and development of new broadcast systems or equipment for the future. This will require an interest and awareness of the latest technologies and state-of-the-art in one or more of the following areas:

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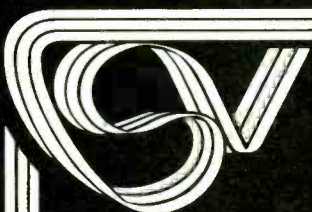
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Our clients offer top negotiable salaries and benefits including generous relocation in the Home Counties, excellent technical facilities and a green fields working environment second to none.

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Applications in writing, with C.V. please to
The National Facilities Director, The SNV Group,
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Salaries will conform to the Company Staff Grading system, currently under review. Company BUPA scheme.

TECHNICAL ENGINEERING MANAGER-Facilities

(SNV London)

Responsible for the day to day operation of the edit suites and technical areas at our Charlotte Street premises; the successful applicant will have practical 'hands on' engineering knowledge of VTR's (including 1", BVU and LB), editing control systems and broadcast cameras, and will be capable of supervising and training staff as well as handling future planning and development. Working closely with the Facilities and Hire Manager and reporting to the National Facilities Director, this is a challenging position with good potential for personal development. Salary by negotiation.

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(SNV London, South, West, North and North East)

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Appointments

Electronics Engineers £9561 Communications Design in High Tech Country

At H.M. Government Communications Centre we're using the very latest ideas in electronics technology to design and develop sophisticated communications systems and installations for special Government needs at home and overseas.

With full technical support facilities on hand, it's an environment where you can see your ideas progress from initial concepts through prototype construction, tests and evaluation, to the pre-production phase, with a chance to influence every stage. Working conditions are pleasant, the surroundings are attractive, and the career prospects are excellent.

Ideally we're looking for men and women who have studied electronics to degree level or equivalent and have had some experience of design, whether obtained at work or through hobby activities. Appointments will be made as Higher Scientific Officer (£7149-£9561) or Scientific Officer (£5682-£7765) according to qualifications and experience.

For further details please write to the address given below. As our careful selection process takes some time, it would be particularly helpful if you could detail your qualifications, your personal fields of interest and practical experience, and describe the type of working environment most suited to your career plans.

The Recruitment Officer, HMGCC, Hanslope Park, Buckinghamshire MK19 7BH.

(2448)

COMMUNICATIONS ENGINEERS AND TECHNICIANS

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Engineers who have a broad experience of single channel, microwave and multiplex equipments and understand the parameters of these systems.

Vacancies exist both at Great Yarmouth and Aberdeen with opportunities for occasional overseas travel. You will be involved in the design and planning of complete communications systems, as well as their implementation.

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For on-going projects in the UK and overseas, we require engineers and technicians able to install and maintain a wide range of communications equipment from microwave and multiplex, to VHF, HF and UHF systems and probably some PABX knowledge.

Whether you are working in the North Sea or Middle East you can expect to receive a competitive salary plus allowances and attractive work/leave cycles.

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Please apply in writing to: R. D. Elliott, Group Personnel
Director, Inspectorate EaE Group Limited,
284/5 Southtown Road, Great Yarmouth,
Norfolk NR31 0JB

Inspectorate EaE
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(2603)

ELECTRONICS ENGINEERS for MARINE SYSTEMS

Hunting Surveys & Consultants Limited requires Electronics Engineers to work on both the theoretical and practical aspects of Marine Survey Instrumentation Systems.

They must be qualified to degree level with a broad electronics experience but having an emphasis on digital circuitry, computing and microprocessing techniques. Software experience will be necessary.

Applicants (preferred age 23-30) will need to be physically fit and prepared to undertake periods of operational work in the North Sea and Overseas. Engineers appointed must be capable of working with minimum supervision to take overall responsibility for initial circuit design, prototype building and testing, board layouts, circuit diagrams and documentation. This work often involves the production of working prototypes to be used in the field within days.

If you believe that you are suitably qualified and could be happy working under these demanding but stimulating conditions, please apply in writing to:-



The Personnel Manager
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The potential for expansion in the export markets for our products means that we need to recruit a Regional Sales Manager to realise this targeted increase in exports.

Applicants must have a technical qualification in electronics with a background in the radio communications industry. We also require a minimum of two years experience of technical selling in either the U.K. or export markets with a track record that testifies to the ability to achieve targets in a highly competitive industry. A second language (French or Spanish) would be an

advantage.

We offer an attractive salary package including company car, over five weeks annual leave, staff pension and free life assurance scheme. Assistance with relocation is available in appropriate cases.

This is an excellent opportunity for an ambitious professional to develop his/her career in export selling.

If you have the drive and enthusiasm to join Britain's fastest growing electronics group then please contact:-

The Personnel Officer,
Racal Dana Instruments Ltd., Duke Street, Windsor,
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DEPARTMENT OF ELECTRICAL AND ELECTRONIC ENGINEERING

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1. Electronics and Electrical Power.
2. Microprocessors and their applications.
3. Software Engineering.

Salary within the range: £5,649 - £9,735 plus £987 p.a. London Allowance.

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(2575)



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ELECTRONICS TECHNICIAN

The Electronics and Computer Services Department of Inco's Refinery in North West London is concerned with the construction and installation of process control equipment, and the maintenance of bought-in hardware.

A vacancy now exists for a suitably qualified person with demonstrable practical and logical ability to assist with the work of the department.

Salary will be based on experience at c. £8,000. In addition, an excellent benefits package is available to the successful candidate.

Please write or telephone for an application form to:

Mr. Jeff Parkin, Refinery Engineer,
Inco Europe Limited Bashley Road, London NW10 6SN.
(Tel: 01-965 6031 Ext.41)



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Fully trained ELECTRONIC TECHNICIANS

With a minimum of five years experience in servicing, maintenance and repair, including defect diagnosis, of various types of military ground based electronic equipment. These unaccompanied posts include free accommodation, medical care and free air travel to the UK for frequent leave periods. Attractive salary with bonus and allowances normally free of UK Tax. For further information write to:- **Company Personnel Manager, Airwork Limited, Bournemouth - Hurn Airport, Christchurch, Dorset BH23 6EB.**



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1983

Appointments

PRINCIPLE DESIGN ENG. to £17.5K PRINCIPLE QUALITY ENG. to £15K

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You will be part of a professional team of engineers, managers, systems analysts and modelling consultants. You will help to maintain our client's position as world leader in their field by successfully dealing with a continuous influx of new projects. These future developments will offer you considerable opportunities to exercise your personal initiative, innovative, technical and managerial skills from the product's conception through to customer acceptance. As a candidate you will have a degree in electronics and **experience in one or more of the following:**

DIGITAL SIGNAL PROCESSING, SPREAD SPECTRUM TECHNIQUES, COMMUNICATIONS PROCESSING, WIDEBAND ANALOGUE CIRCUIT TECHNIQUES with LSI, VLSI and HYBRID DESIGN TECHNIQUES.

Our client also requires:

**DESIGN AND DEVELOPMENT ENGINEERS
SYSTEMS and SCIENTIFIC ANALYSTS
SYSTEMS MODELLING CONSULTANT
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