

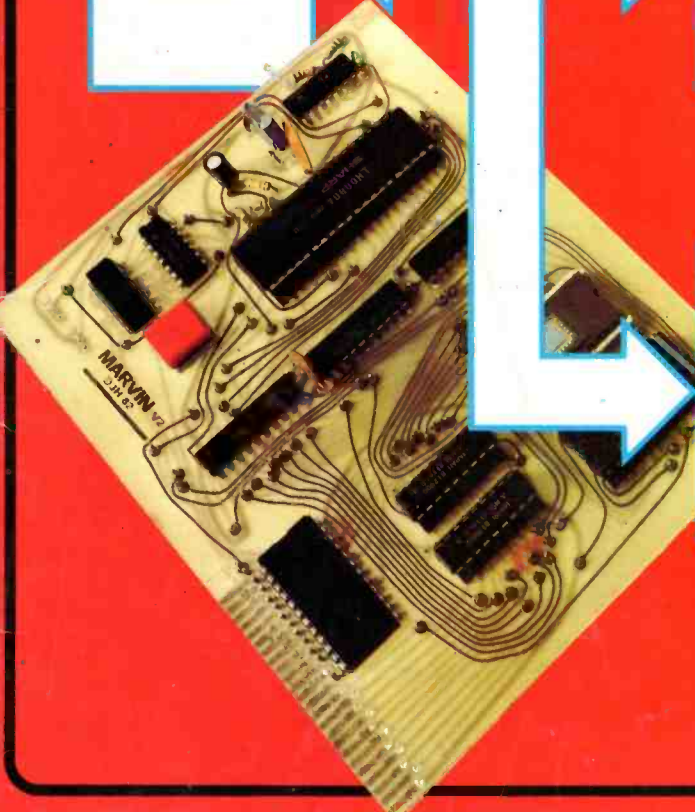
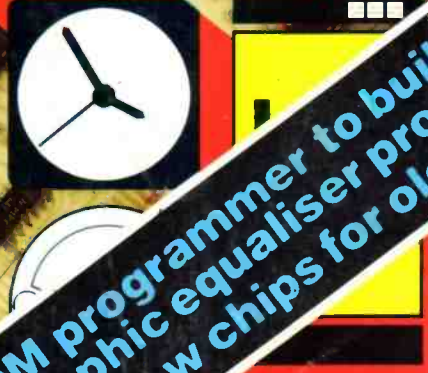
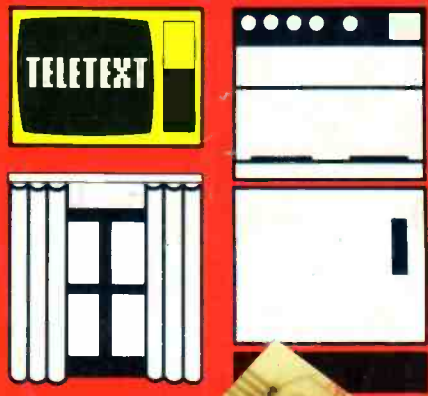
electronics today

INTERNATIONAL

AUGUST 1983 85p

ANIMATE YOUR LIFE

Z80-based control computer for home, industrial and laboratory control
modular construction for maximum flexibility



PLUS EPROM programmer to build
High quality graphic equaliser project
IC update: new chips for old

Star sounds **

Star quality **

Star features **

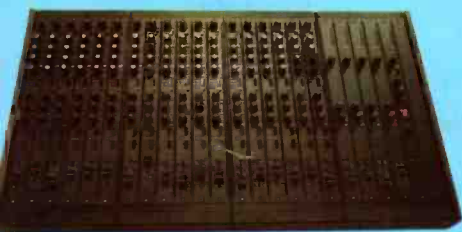
BIG NEWS ABOUT OUR LATEST ADVANCES IN ROBOTICS SEE INSIDE BACK COVER

Free SECURICOR DELIVERY on all orders over £100 (UK mainland only) Add just £2.50 on lower price orders



DJ90 Stereo Mixer — this is a really versatile new mixer that enables the constructor DJ to produce a professional performance every time. There are two stereo inputs for magnetic cartridges, a stereo auxiliary input and mike input. Other 'plus' features are auto-panning for fast or slow slider controls, multi-mixing, ducking, interrupt, input modulation, in short everything... the whole works — AND — under £100 complete! Complete kit £97.50 + VAT

TRANSCENDENT 2000 — Although only a 3 octave keyboard the '2000' features the same design ingenuity, careful engineering and quality components of its larger brethren. The kit is well within the scope of the first time builder — buy it, build it — play it! You will know you have made the right choice. Complete kit £165.00 + VAT



This versatile modular mixer, featured as a constructional article in Practical Electronics can be built up to a maximum of 24 inputs, 4 outputs and an auxiliary channel. Each input channel has Mic and Line inputs, variable gain, bass and treble controls and a parametric middle frequency equalizer. There are send and return jacks, auxiliary, pan and fader controls and output and group switching. The output channels have PPM displays and record and studio outputs. The auxiliary channel also has a PPM display and there is a headphone monitor jack and a built-in talk-back microphone. The mixer modules plug into base units each of which takes up to 6 channels. To eliminate hum, the power supply is in a separate cabinet.

SALES COUNTER Collect your order from the factory. Open 9-12/1-4.30 Mon-Thurs. Easy parking, no waiting

Digital Delay Line — With its ability to give delay times from 1.6 mSecs to up to 1.6 secs. Many powerful effects including phasing, flanging, A.D.T., chorus, echo &



vibrato are obtained. The basic kit is extended in 400 mS steps up to 1.6 secs. Simply by adding more parts to the PCB. Compare with units costing over £1,000! Complete kit (400 mS delay) £130 + VAT Parts for extra 400 mS delay £9.50 + VAT

KIT PRICES

Input channel	£19.90	Base unit and wooden front	£27.50
Output channel	£18.50	Pair of mahogany end cheeks	£12.50
Auxiliary channel	£22.50	Power Supply and cabinet	£19.50
Blank Panel	£3.00		

All prices are VAT exclusive

TRANSCENDENT POLYSYNTH — A four octave polyphonic synthesiser with outstanding design characteristics and versatility and performance to match. Complete kit £275.00 plus VAT (single voice) Extra voice (up to three-more) £42.00 plus VAT



Free Soldering Practise Kit on request with your first kit — useful tips, well illustrated.

MPA 200 — is a low price, high power 100W amplifier. Its smart styling, professional appearance and performance, make it one of our most popular designs. With adaptable inputs the mixer accepts a variety of sources yet straightforward construction makes it ideal for

the first time builder. Complete kit £49.90 + VAT. Chromatque 5000 — a 5 channel lighting system powerful enough for professional discos yet controllable for home-effects. Sound to light, strobe to music level, random or sequential effects — each channel can handle up to 500W yet minimal wiring is needed with our unique single board design. Complete kit £49.50 + VAT



Component packs for most kits are available See our great free catalogue, full details of all our range

ETI VOCODER — 14 channels, each with independent level control, for maximum versatility and intelligibility. Two input amplifiers — for speech/excitation — each with level control and tone control. The Vocoder is a powerful yet flexible machine that is interesting to build and thanks to our easy to follow construction manual, is within the capability of most enthusiasts. Complete kit £175.00 + VAT

SP2 200 twice the power with two of the reliable, durable and economic amps from the MPA 200, fed by separate power supplies from a common toroidal transformer. Superb finish and quality components throughout — up to (even over) the standard of high priced factory-built units! Complete kit £64.90 + VAT



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electronics today

INTERNATIONAL AUGUST 1983 VOL 12 NO 8

AN ARGUS SPECIALIST PUBLICATION

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ANIMATE YOUR LIFE

Z80-based control computer for home, industrial and laboratory control modular construction for maximum flexibility

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Complete kit containing artwork PCB, and all necessary process materials
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Perfect results everytime. Kit contains: Lamp, Holder & Shade together with full instructions for DIY Unit which offers PCB, Precision Photo, Label & Panel manufacture
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	TOTAL	£ :	£ :
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ETI/8/83

T.V. SOUND TUNER

BUILT AND TESTED

In the cut-throat world of consumer electronics, one of the questions designers apparently ponder over is "Will anyone notice if we save money by chopping this out?" In the domestic TV set, one of the first casualties seems to be the sound quality. Small speakers and no tone controls are common and all this is really quite sad, as the TV companies do their best to transmit the highest quality sound. Given this background a compact and independent TV tuner that connects direct to your Hi-Fi is a must for quality reproduction. The unit is mains-operated. This TV SOUND TUNER offers full UHF coverage with 5 pre-selected tuning controls. It can also be used in conjunction with your video recorder. Dimensions: 11 1/4" x 8 1/2" x 3 1/4"



£24.95 + £2.00p&p.

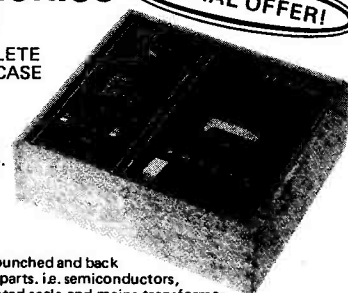
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SPECIAL OFFER!

ONLY £31.00 plus £2.75 p&p.

• NOISE REDUCTION SYSTEM. • AUTO STOP. • TAPE COUNTER. • SWITCHABLE E.Q. • INDEPENDENT LEVEL CONTROLS. • TWIN V.U. METER. • WOW & FLUTTER 0.1%. • RECORD/PLAYBACK I.C. WITH ELECTRONIC SWITCHING. • FULLY VARIABLE RECORDING BIAS FOR ACCURATE MATCHING OF ALL TYPES.

Kit includes tape transport mechanism, ready punched and back printed quality circuit board and all electronic parts, i.e. semiconductors, resistors, capacitors, hardware, top cover, printed scale and mains transformer. You only supply solder & hook-up wire. Featured in April P.E. reprint 50p. Free with kit.



STEREO TUNER KIT

This easy to build 3 band stereo AM/FM tuner kit is designed in conjunction with P.E. (July '81). For ease of construction and alignment it incorporates three Mullard modules and an I.C. IF System. FEATURES: VHF, MW, LW Bands, interstation muting and AFC on VHF. Tuning meter. Two back printed PCB's. Ready made chassis and scale. Aerial: AM-ferrite rod, FM-75 or 300 ohms. Stabilised power supply with 'C' core mains transformer. All components supplied are to P.E. strict specification. Front scale size 10 1/2" x 2 1/2" approx. Complete with diagram and instructions.

SPECIAL OFFER! £13.95 + £2.50 p&p. Self assembly simulated wood cabinet sleeve to suit tuner only. Finish size: 11 1/4" x 8 1/2" x 3 1/4". £3.50 Plus £1.50 p&p.



STEREO CASSETTE DECK

Stereo cassette tape deck transport with electronics. Manufacturer's surplus -- brand new and operational -- sold without warranty.

£11.95 plus £2.50 p&p.

Just requires mains transformer and input/output sockets and a volume control to complete. Supplied with full connection details.



125W HIGH POWER AMP MODULES

The power amp kit is a module for high power applications - disco units, guitar amplifiers, public address systems and even high power domestic systems. The unit is protected against short circuiting of the load and is safe in an open circuit condition. A large safety margin exists by use of generously rated components, result, a high powered rugged unit. The PC board is back printed, etched and ready to drill for ease of construction and the aluminium chassis is preformed and ready to use. Supplied with all parts, circuit diagrams and instructions.

ACCESSORIES: Stereo/mono mains power supply kit with transformer: £10.50 plus £2.00 p&p.



SPECIFICATIONS: Max. output power (RMS): 125 W. Operating voltage (DC): 50 - 80 max. Loads: 4 - 16 ohm. Frequency response measured @ 100 watts: 25Hz - 20KHz. Sensitivity for 100w: 400mV @ 47K. Typical T.H.D. @ 50 watts, 4 ohms: 0.1%. Dimensions: 205x90 and 190x36mm.

KIT £10.50 +£1.15 p&p. BUILT £14.25 +£1.15 p&p.

AUDAX 8"

HIGH QUALITY 40 WATTS RMS BASS/MIDRANGE Ideal for either Hi-Fi or Disco use this speaker features an aluminium voice coil a heavy 70mm diameter magnet. Frequency res: 20Hz to 7KHz. Impedance: 8 ohms. £5.95 +£2.20 P&P.

AUDAX 40W Ferro-Fluid Hi-Fi Tweeter

X/over on 5kHz - 22kHz. 60mm square. 8 ohm. £5.50 +60p p&p.



SPEAKER BARGAINS

2 WAY 10 WATT SPEAKER KIT 8" bass/mid range and 3 1/4" tweeter. Complete with screws, wire, crossover components and cabinet. All wood pre-cut -- no cutting required. Finish - chipboard covered wood simulate. size 14 1/2" x 8 3/4" x 4". PAIR for ONLY £12.50 plus £1.75 p&p.



All mail to: 21E HIGH STREET, ACTON, W3 6NG.

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MULLARD SPEAKER KITS

Purposely designed 40 watt R.M.S. and 30 watt R.M.S. 8 ohm speaker systems recently developed by MULLARD'S specialist team in Belgium. Kits comprise Mullard woofer (8" or 5") with foam surround and aluminium voice coil. Mullard 3" high power domed tweeter. Built and tested crossover based on Mullard circuit, combining low loss components, glass fibre board and recessed loudspeaker terminals. SUPERB SOUNDS AT LOW COST. Kits supplied in polystyrene packs complete with instructions.

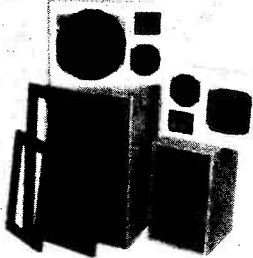
8" 40W system — recommended cabinet size 240 x 216 x 445mm
Price £14.90 each + £2.00 P & P.

5" 30W system — recommended cabinet size 160 x 176 x 295mm
Price £13.90 each + £1.50 P & P.

Designer approved flat pack cabinet kits, including grill fabric. Can be finished with iron on veneer or self adhesive vinyl etc.

8" system cabinet kit £8.00 each + £2.50 P & P.

5" system cabinet kit £7.00 each + £2.00 P & P.



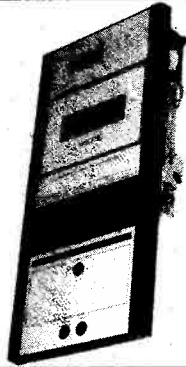
STEREO CASSETTE TAPE DECK MODULE

Comprising of a top panel and tape mechanism coupled to a record/play back printed board assembly. Supplied as one complete unit for horizontal installation into cabinet or console of own choice. These units are brand new, ready built and tested.

Features: Three digit tape counter. Autostop. Six piano type keys, record, rewind, fast forward, play, stop and eject. Automatic record level control. Main inputs plus secondary inputs for stereo microphones. Input Sensitivity: 100mV to 2V. Input impedance: 68K. Output level: 400mV to both left and right hand channels. Output impedance: 10K. Signal to noise ratio: 45dB. Wow and flutter: 0.1%. Power Supply requirements: 18V DC at 300mA. Connections: The left and right hand stereo inputs and outputs are via individual screened leads, all terminated with phono plugs (phono sockets provided). Dimensions: Top panel 5 1/2" x 11 1/2". Clearance required under top panel 2 1/2". Supplied complete with circuit diagram and connecting diagram. Attractive black and silver finish.

Price £28.70 + £2.50 postage and packing.

Supplementary parts for 18V D.C. power supply (transformer, bridge rectifier and smoothing capacitor) £3.50.



LOUDSPEAKERS

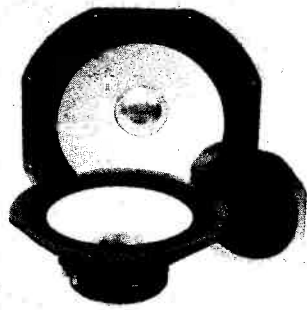
THREE QUALITY POWER LOUD-SPEAKERS (15", 12" and 8" See Photo). Ideal for both Hi-Fi and Disco applications. All units have attractive cast aluminium (ground finish) fixing escutcheons.

Specification and Prices.

15" 100 watt R.M.S. Impedance 8 ohms. 50 oz. magnet. 2" aluminium voice coil. Res. Freq. 20 Hz. Freq. Resp. to 2.5KHz. Sens. 97dB. Price: £34.00 each + £3.00 P&P

12" 100 watt R.M.S. Impedance 8 ohms. 50 oz. magnet. 2" aluminium voice coil. Res. Freq. 25Hz. Freq. Resp. to 4 KHz. Sens. 95dB. Price: £24.50 each + £3.00 P&P

8" 50 watt R.M.S. Impedance 8 ohms. 20 oz. magnet. 1 1/2" aluminium voice coil. Res. Freq. 40Hz. Freq. Resp. to 6 KHz. Sens. 92dB. Black Cone. Price: £9.50 each. Also available with black protective grille. Price: £9.99 each. P&P £1.50.



12" 85 watt R.M.S. McKENZIE C1286GP (LEAD GUITAR, KEYBOARD, DISCO) 2" aluminium voice coil, aluminium centre dome, 8 ohm imp., Res. Freq. 45Hz., Freq. Resp. to 6.5KHz., Sens. 98dB. Price: £22.00 + £3 carriage.

12" 85 watt R.M.S. McKENZIE C1286TC (P.A., DISCO) 2" aluminium voice coil. Twin cone. 8 ohm imp., Res. Freq. 45Hz., Freq. Resp. to 14KHz. Price £22 + £3 carriage.

15" 150 watt R.M.S. McKENZIE C15 (BASS GUITAR, P.A.) 3" aluminium voice coil. Die cast chassis. 8 ohm imp., Res. Freq. 40Hz., Freq. Resp. to 4KHz. Price: £47 + £4 carriage.

PIEZO ELECTRIC TWEETERS - MOTOROLA

Join the Piezo revolution. The low dynamic mass (no voice coil) of a Piezo tweeter produces an improved transient response with a lower distortion level than ordinary dynamic tweeters. As a crossover is not required these units can be added to existing speaker systems of up to 100 watts (more if 2 put in series). FREE EXPLANATORY LEAFLETS SUPPLIED WITH EACH TWEETER.

TYPE 'A' (KSN2036A) 3" round with protective wire mesh, ideal for bookshelf and medium sized Hi-fi speakers. Price £4.29 each.

TYPE 'B' (KSN1005A) 3 1/2" super horn. For general purpose speakers, disco and P.A. systems etc. Price £4.99 each.

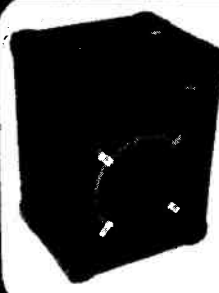
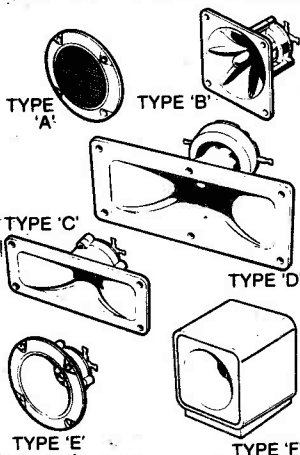
TYPE 'C' (KSN6016A) 2" x 5" wide dispersion horn. For quality Hi-fi systems and quality discos etc. Price £5.99 each.

TYPE 'D' (KSN1025A) 2" x 6" wide dispersion horn. Upper frequency response retained extending down to mid range (2KHz). Suitable for high quality Hi-fi systems and quality discos. Price £7.99 each.

TYPE 'E' (KSN1038A) 3 3/4" horn tweeter with attractive silver finish trim. Suitable for Hi-fi monitor systems etc. Price £4.99 each.

TYPE 'F' (KSN1057A) Cased version of type 'E'. Free standing satellite tweeter. Perfect add on tweeter for conventional loudspeaker systems. Price £10.75 each

P&P 20p ea. (or SAE for Piezo leaflets).



OMP 80 LOUDSPEAKER

The very best in quality and value.

Ported tuned cabinet in hard-wearing black vinylite with protective corners and carry handle. Built and tested, employing 10in British driver and Piezo tweeter. Spec: 80 watts RMS; 8 ohms; 45Hz-20KHz; Size: 20in x 15in x 12in; Weight: 30 pounds.

Price: £49.00 each
£90 per pair
Carriage: £5 each £7 per pair

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3 WATT FM TRANSMITTER 3 WATT 85/115MHz varicap controlled, professional performance. Range up to 3 miles 35 x 84 x 12 mm (12 volt) Price: £12.49p

SINGLE CHANNEL RADIO CONTROLLED TRANSMITTER/RECEIVER 27MHz Range up to 500 metres. Double coded modulation. Receiver output operates relay with 2amp/240 volt contacts. Ideal for many applications. Receiver 90 x 70 x 22 mm 9/12 volt) Price: £16.49 Transmitter 80 x 50 x 15 mm (9/12 volt) Price £10.29 P&P All Kits +50p. S.A.E. for complete list.



3 watt FM Transmitter

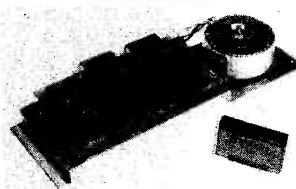
BSR P256 TURNTABLE

P256 turntable chassis ● S shaped tone arm ● Belt driven ● Aluminium platter ● Precision calibrated counter balance ● Anti-skate (bias device) ● Damped cueing lever ● 240 volt AC operation (Hz) ● Cut-out template supplied ● Completely manual arm. This deck has a completely manual arm and is designed primarily for disco and studio use where all the advantages of a manual arm are required.

Price £31.35 each. £2.50 P&P



OMP POWER AMPLIFIER MODULE



New model.
Improved specification

NEW OMP100 Mk.II POWER AMPLIFIER MODULE Power Amplifier Module complete with integral heat sink, toroidal transformer power supply and glass fibre p.c.b. assembly. Incorporates drive circuit to power a compatible LED Vu meter. New improved specification makes this amplifier ideal for P.A., instrumental and Hi-Fi applications.

SPECIFICATION
Output Power:— 110 watts R.M.S.
Loads:— Open and short circuit proof 4/16 ohms.
Frequency Response:— 15Hz - 30KHz -3dB. T.H.D.:— 0.01%
S.N.R. (Unweighted):— -118dB ±3.5dB
Sensitivity for Max Output:— 500mV @ 10K.
Size:— 360 x 115 x 72 mm
Price:— £31.99 + £2.00 P&P
Vu Meter Price:— £7.00 + 50p P&P.

HOME PROTECTION SYSTEM

Better to be 'Alarmed' than terrified. Thandar's famous 'Minder' Burglar Alarm System. Superior microwave principle. Supplied as three units, complete with interconnection cable. FULLY GUARANTEED.

Control Unit — Houses microwave radar unit, range up to 15 metres adjustable by sensitivity control. Three position, key operated fascia switch — off — test — armed. 30 second exit and entry delay.

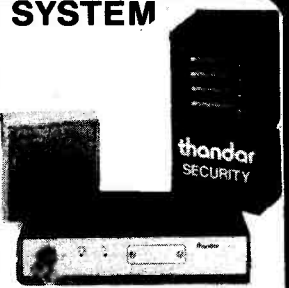
Indoor alarm — Electronic swept freq. siren. 104dB output.

Outdoor Alarm — Electronic swept freq. siren. 98dB output. Housed in a tamper-proof heavy duty metal case.

Both the control unit and outdoor alarm contain rechargeable batteries which provide full protection during mains failure. Power requirement 200/260 Volt AC 50/60Hz. Expandable with door sensors, panic buttons etc. Complete with instructions. SAVE OVER £100 Usual price £228.85

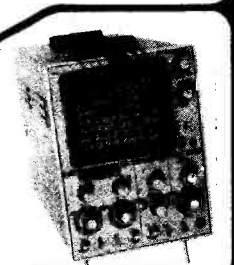
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British model. 12 month guarantee. 20 MHz Band Width.
Specification: ● CH1, CH2: 5mV/div-20V/div. ● Time Base: 1 Sec/div-100ns/div. ● XY Facility: Matched XY inputs. ● Trigger Level control ± slope selection. ● Auto, normal, TV Triggering. ● Z-Modulation. ● CAL output 1V 1KHz. ● Sweep output 0.9V. ● Graticule blue ruled 10 x 8 cm. (5" C.R.T.) Very sharp trace. ● Size: H235mm, W177mm, D360mm. ● Weight: 6.5 Kgs. ● Supply: 200-240 V. 40-60Hz. ● Price: £241.50 — FREE Securicor Delivery. Probes: X1 £8.05, X1/X10 Switched £10.93.



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MONTH

64K DRAM

A little short on memory? ETI comes to the rescue with this project which is just the ticket for 6502 or 6800 based systems. Latching it into your system just couldn't be easier, because the DRAM board uses an EPROM to do the address decoding. No more lash-ups, just program the PROM to define where the memory goes in the micro's space. Why didn't we think of it before?

Smart NiCad Charger

Now there have been plenty of NiCad chargers that have graced these pages — but this one will automatically rejuvenate worn out cells. (Wonder if it would work on the cells in the Editor's brain?)

New Series: Audio Design

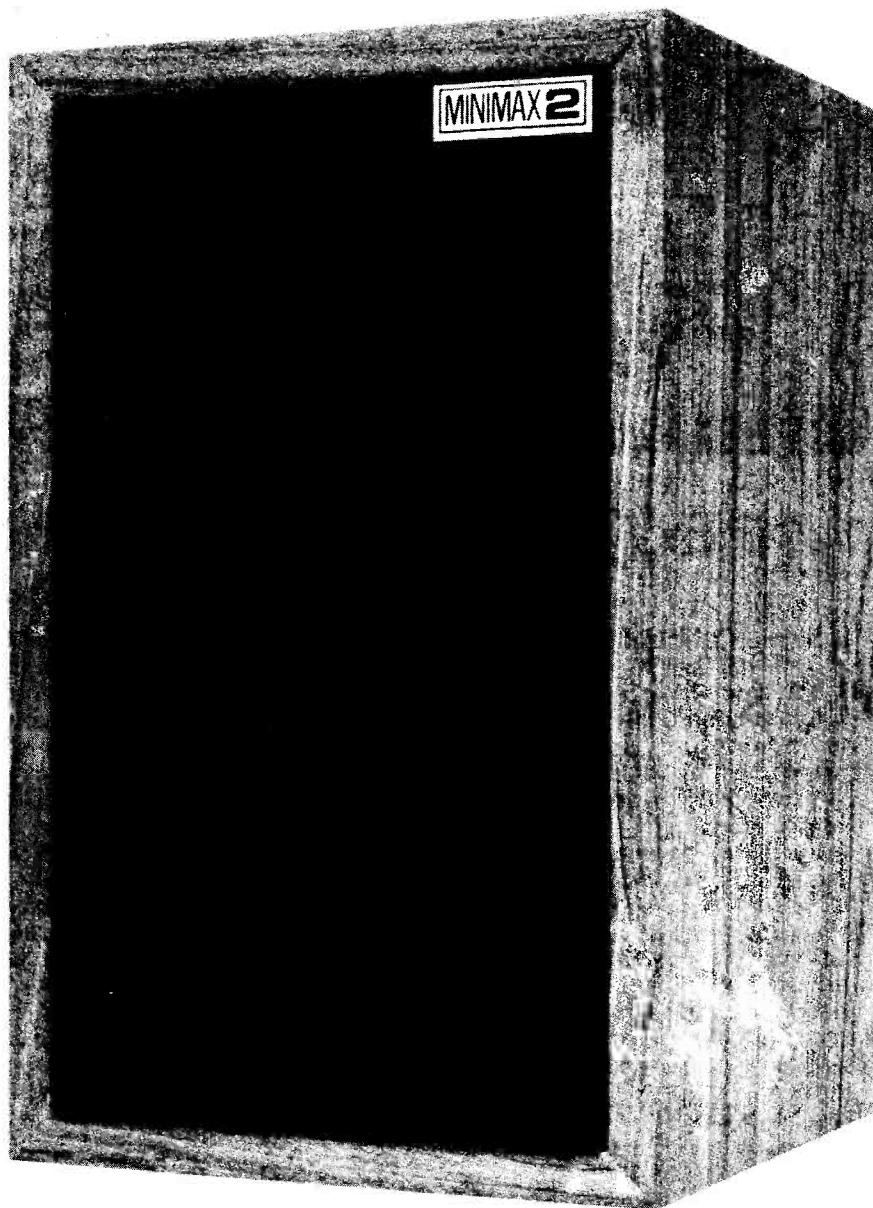
John Linsley Hood is one of the best known audio designers, and he'll be guest-writing this series for us. The emphasis will be on practicalities, with easy-to-follow explanations and simple but useful calculations. Although as little as possible be assumed about the level of expertise of the reader, there will be something here for even the most experienced of you.

Audiophile review

The Videotone Minimax speakers have provided a touch-stone in price-effective audio for many years. Now there's a Mark II version — can it be as good, or, possibly, even better? Our intrepid Audiophile investigates.

The Digger

No, nothing to do with our Australian colleagues, but a useful little device for digging around inside digital circuits — a logic oscilloscope trigger. The idea is very simple, really, all you do is . . . but if we told you that, you might not buy next month's mag, mightn't you?



ALL THIS AND MORE IN THE SEPTEMBER ISSUE OF ETI, ON SALE AUGUST THE 5th. PLACE YOUR ORDER NOW, OR RISK MISSING OUT!

Articles described here are in an advanced state of preparation. However, circumstances may dictate changes to the final contents.

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Assembler & Disassembler
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to make programs readable without using more memory
64K RAM using latest technology 64K DRAMS
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MON	SON	ON	DATA	NUMBER	DIM
	BIT	GOTO	READ	RENUM	DEF
FUNCTIONS	CRB	GOSUB	RESTOR	BOOT	NEW
ABS	CRF	POP	RETURN	GRAPH	END
ADR	MEM	REM	STOP	TEXT	BIT
ASC	MWD	FOR	TIME	PLOT	CRB
ATN	LEN	NEXT	WAIT	UNPLOT	CRF
SIN	MCH	ERROR	SAVE	COLOUR	MEM
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DIGEST



Smart Cable

The SC817 SMART CABLE from KPG-Hardware House provides a simple, low cost method of interfacing 98% of RS232 equipment. Ideal for equipment salesmen and engineers the Smart Cable's unique logic senses the RS232 configuration at each end and automatically configures the

correct pin to pin connection. Providing male to male and male to female connection the Smart Cable totally eliminates the need for break out boxes, debugging cables and custom cables. KPG-Hardware House, 578-586 Chiswick High Road, London W4 5RP.

New Current Probe

The Model 711 Miniature Wide-band Current Probe manufactured by American Laser Systems, California, measures wideband current pulses without loading the circuit being tested. It induces no appreciable capacitive nor inductive effects on circuitry, therefore the signal under measurement does not change. The 711 exhibits only 0.02 ohm shunted by 4 μ H insertion impedance. The current is sensed by placing the conductor through the centre of the probe, which will accept a maximum lead diameter of No. 20 AWG. For general use as a test probe with oscilloscopes and test equipment,

Model 711 is available in a potted package with a 3ft co-ax cable and standard BNC connector. The UK agent is Dynamic Technology Limited, Zonal House, Alliance Road, Acton, London W3 0BA.

Whoops!

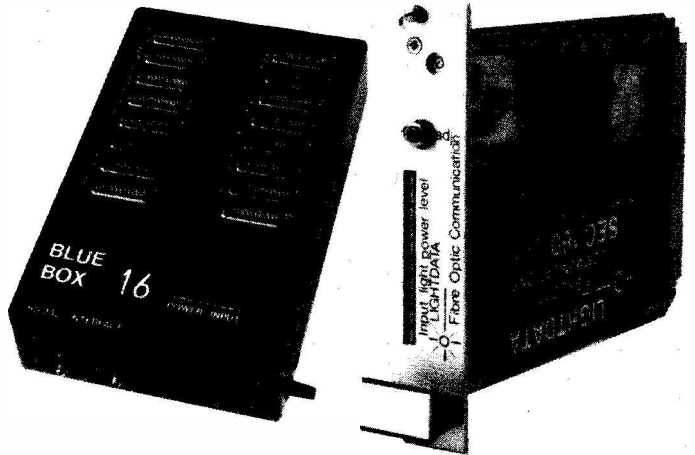
Stotron Ltd were just a little annoyed with us for saying that their latest catalogue was dated 1982 (Digest Shorts, June). In fact, they have now supplied us with their latest, 1983/4 catalogue, to prove that the other dropped through a worm-hole in

TOBIE Award For LCD Team

The TOBIE Award for Research Achievement has this year been won by the Physics Research team at the Royal Signals and Research Establishment, Malvern. For some years now this team has been working on the various uses of liquid crystals, including displays and addressing methods, this technology has made possible the 128 x 256 matrix liquid crystal cell developed in conjunction with Scopex Instruments Ltd., for use in the Voyager digital storage oscilloscope.

Many of the Voyager's ap-

plications are, apparently, linked to water or marine life. For instance, Water Boards find its lightness and ease of handling very useful on certain of their very remote pumping and control locations, and one of the strangest of applications to date has been for use on an expedition to the Amazon where it will be used for tests on a type of electric fish. Scopex ask: is this the dawn of a new era in ATE (Aquatic Test Equipment)? Scopex Instruments Limited, Pixmore House, Pixmore Avenue, Letchworth, Herts SG6 1HZ. Tel (04626) 72771.



The Bead's Needs

A new range of ferrite beads manufactured by Stackpole are available exclusively to UK manufacturers from Walmore Electronics Ltd, 374 City Road, 11-15 Betterton Street, Drury Lane, London WC2H 9BS. Particularly interesting is a lead tape bead for use with automatic insertion equipment.

Ferrite beads are a simple, inexpensive, yet effective way to obtain RF decoupling, shielding and parasitic suppression without sacrificing low frequency power or signal level. Unlike conventional RF chokes, beads are compact, have no DC losses, and will not couple to stray capacity and introduce detuning or spurious oscillations. Installation of beads is easy. Simply slip over the appropriate conductor for the desired noise suppression or high frequency isolation.

Fibre Optic Links

Lightdata have two new L modules: on the left is the Blue Box 16-channel RS232 to fibre optic interface that is, apparently, simplicity itself to set up and use. It is intended to be mounted on a wall, and can provide a link over up to 1 km of optic cable. On the right is a Eurocard mounted version that requires a single 5 V supply. Lightdata, 4 Lias Road, Porthcawl, Mid Glamorgan, Wales CF36 3AH.

Energy In The Outback

A new \$250,000 Solar Energy Research Centre is to be built in Western Australia. It will be located next to the site earmarked for a proposed new technology park, which is to be established at the Western Australian Institute of Technology in Bentley.

The new centre will contain testing and monitoring equipment, computer facilities for automated data analysis, an information and display area, and office space for the staff of the Solar Energy Research Institute of Western Australia (SERIWA). Outside areas will be used to test various types of solar equipment.

the space-time continuum (that's our story, and we're sticking to it).

Stotron would also like us to point out that while they do continue to have offices in Hastings, readers should write to them at 72 Blackheath Road, Greenwich, London SE10 8DA, to obtain their copy of the catalogue.

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7100 Single sided £225.00 + Carr. 7200 Double sided £295 + Carr.
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For more information or details of other types of ex. stock modems contact sales office.

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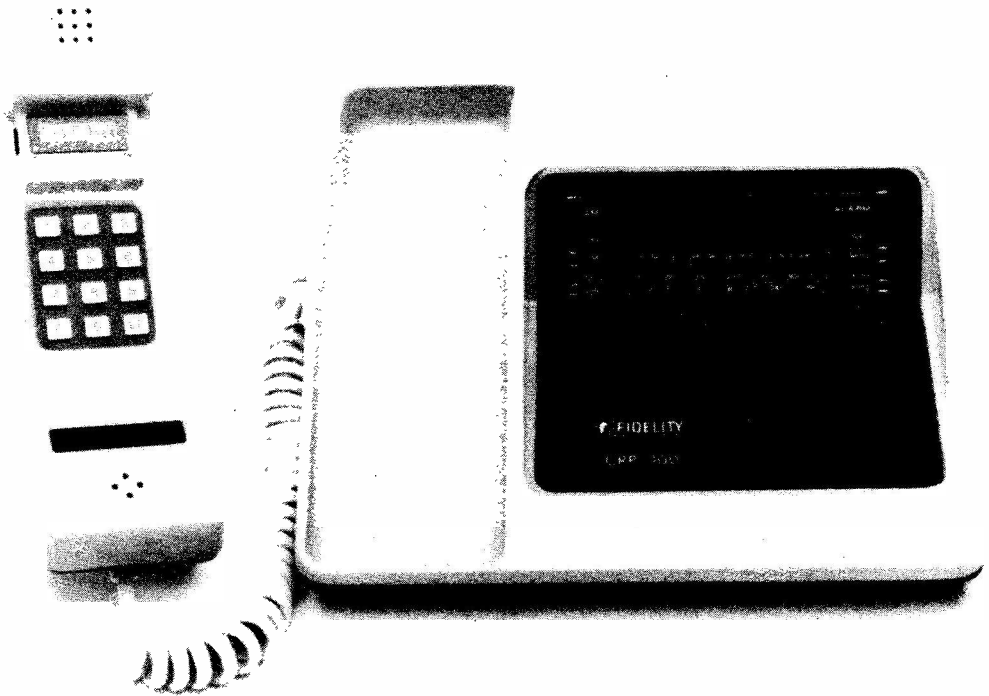


The Phone That Thinks It's A Clock

The new Clock Radio Phone from Fidelity Radio, the CRP 100, is a compact unit incorporating the three facilities of radio, alarm clock and telephone. Operation is precisely the same as a conventional clock radio but with an automatic cut off when the telephone receiver is lifted. British Telecom approval is already applied for and the CRP 100 can be installed by connection to the mains and a standard British Telecom socket. The Clock Radio Phone is expected to retail at around £69, and should be in the shops by September.

Also from Fidelity is a new colour television chassis design, the ZX 3000. The chassis is smaller, more advanced with reduced component volume and covers eight programme channels. Advantages across the range include greater reliability, less weight and an even more economical price for high quality vision and sound reproduction.

You'll find the new chassis in some new models, the CTV 22T and CTV 20T Teletext models, the CTV 22R remote control model and a new 14 inch colour monitor. The existing CTV 20R and CTV 14S portable will continue in the range but with the new chassis.



Micros Go Down The Drain

Intel Corp has introduced its "Data Pipeline" hardware and software designed to link mainframe computer data bases with personal computers. The Data Pipeline is built around Intel's Data-Base Information System, iDIS 86/735, a microcomputer-based "traffic-manager" that interprets, stores and distributes mainframe data to and from terminals and personal computers. The Data Pipeline uses an enhanced version of Intel's System 2000 Data-Base Management System (DBMS). System 2000 currently handles data storage and retrieval in hundreds of large mainframe computer installations.

New Data Pipeline extensions to System 2000 provide a relational data-base capability, graphics and a fourth-generation software architecture, System 2000 On-Line Operation (SOLO).

Intel also has broadened its 700 family of Data-Base Information Systems with the iDIS 86/730, an iDIS version aimed at original equipment manufacturers and large-volume end users. Intel Corporation S.A., Rue du Moulin a Papier, 51, Boite 1, B-1160 Brussels, Belgium.

Speedy Prototypes

Computing Techniques (Mfg) Limited has introduced a fast and economic service on operational amplifiers designed and built to special requirements. Now, all but the most exacting orders can be met in two weeks or less. Many orders can be turned round in as little as seven days, and this British company is offering prices at up to 25% lower than those quoted by other major

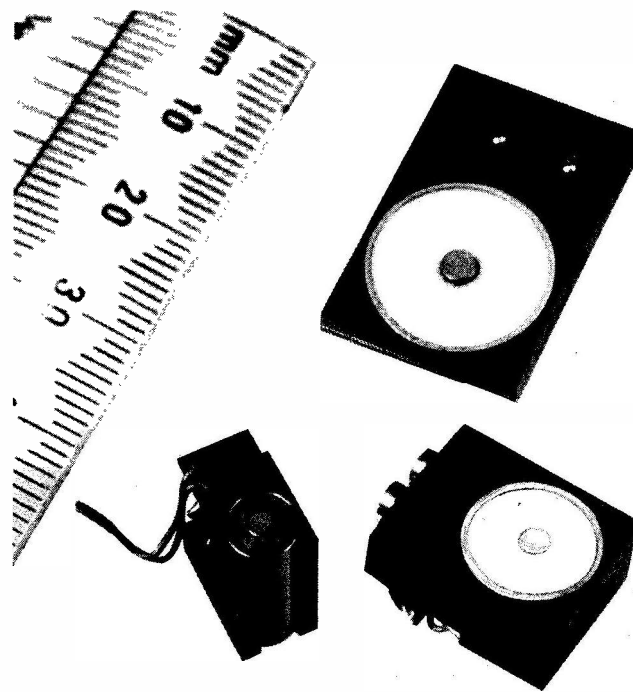
manufacturers.

The service should prove of great interest to small and medium quantity users, who often experience difficulty in easily, or economically, meeting specifications when selecting standard linear integrated circuits from the major suppliers. Computing Techniques supplies a complete, packaged operational amplifier which it guarantees will

meet the customer's specification, however tight. Computing Techniques (Mfg) Ltd, Brookers Road, Billingshurst, West Sussex RH14 9RZ.

Please . . .

At the time of writing, ETI is still without a replacement for Peter Green, our former deputy editor turned Computing Today. So please, keep your enquiries of us to a minimum, and follow the guidelines on page 70.



A Little Pull Helps

Miniature solenoids for use where space is at a premium have been introduced by Magnetic Components to augment its established recording head capability. Manufactured to meet manufacturers' specific requirements, the units are expected to have particular application to electronic security locks, access controls, low power system controllers, printer mechanisms, electronic camera shutters, etc.

Typical is one producing a latch pull force of 150 gms when 1.9 volts D.C. is applied to the 75 ohms coil. In addition to the solenoid component, MCL provides methods of controlling the unlatching force so as to give a higher level of release time repeatability; this is achieved by a specially developed keeper and/or the use of 'kick-off' electronic circuitry. Magnetic Components Limited, Bridge Wharf Industrial Estate, Chertsey, Surrey KT16 8LJ.

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SPARK DURATION — 500µs, STORED ENERGY — 135mJ
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We challenge any manufacturer to publish better performance figures. Before you buy any other make, ask for the facts, its probably only an inductive system. But if an inductive system is what you really want, we'll still give you a good deal.
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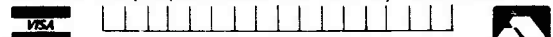
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What Is It?

We know what it is — but do you? We get all sorts of obscure objects passing under our noses here at ETI, but this particular one seems to mark a new all-time height in enigma.

Actually, it's use is pretty boring, so we're not giving any prizes for the correct answer. However, the most ingenious incorrect answer will get some prize, though what it is, we haven't decided. It could be a guided tour of the ETI office, or it may even be one of these things — you'll have to wait and see.

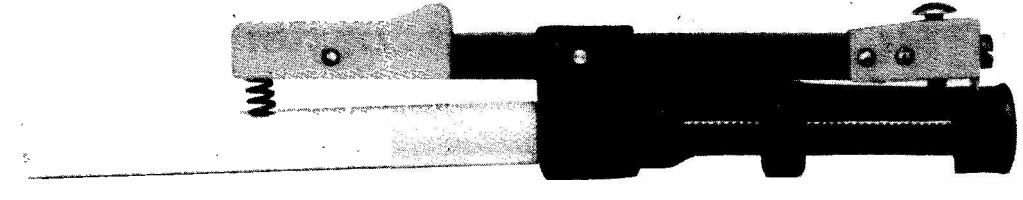
Filters For CD

RIFA have introduced a new series of hybrid active filters, which have been designed for anti-aliasing applications in equipment such as digital audio systems. Constructed in RIFA's thick film process, the PBA 3167 and PBA 3179 hybrid active filters feature an extremely flat response over their operational passband. Included in their circuitry is a group-delay equalising network, which effects a constant group-delay response within $+10\mu\text{s}$ up to 19KHz in the case of the PBA 3167, and up to 13.5 KHz for the PBA 3179.

Cut off frequencies are specified as 20KHz (3167) and 15KHz (3179). Accordingly, the filters are ideally suited for applications in digital audio systems having sampling frequencies from 48 to 50KHz, or 32KHz. RIFA AB, Market Chambers, Shelton Square, Coventry.

Noisy Fault Locator

A new British manufactured and designed portable Audio/Visual faults locator is now available from Antron Electronics Ltd, Hamilton House, 39 Kings Road, Haslemere, Surrey GU27 2QA. Codenamed Toneohm 700, the instrument is used to locate short and partial short circuits caused by solder bridges, poor etching, partial device failure, i.e. substrate shorts, leaking capacitors etc., by tone or meter readout without removing com-



More Motorola Manuals

Motorola have been busy scribbling away, and the following new books bring the total number of Motorola technical publications up to 22: B012A — 8 bit Microprocessor Data Manual; B012B — 16 bit Microprocessor Data Manual; B001 — A/D and D/A Conversion Manual; B0015 — Switchmode and TMOS Power

Transistors; B038 — Linear/Switchmode Voltage.

These are available from Motorola Distributors, or write to

Motorola's European Literature Centre (at Milton Keynes) for the leaflet, describing each publication and detailing prices. Motorola Semiconductors, 88 tanners Drive, Blakelands, Milton Keynes.

Accurate Robot

Zehntel's Series 600 Robotic Board Handling System, the first fully operational robot aid for automatic testing equipment, is described in a 4 page brochure. The RBHS is easily programmed and has a unique 6 axis motion. Positioning accuracy is 0.022", believed to be the best available.

As well as loading and unloading boards at the test head, the RBHS can also be used for light mechanical tasks connected with testing, such as operating switches etc. It will also handle simple assembly tasks if required. Zehntel Limited, 62 Tanners Drive, Blakelands, Milton Keynes MK14 5BP.

Shorts

- United Components Ltd, Unit 5, Wye Estate, London Road, High Wycombe, Bucks HP11 1LH now carry stocks of Clare Reed and mercury wetted relays, as well as many other GI and related companies' products.

- Any manufacturer wishing to exhibit at the fourth Middle East Electricity and Electronics Exhibition in Kuwait in January 1984 should contact the British Electrical and Allied Manufacturers' Association (BEAMA) at 8 Leicester Street, London WC2H 7BN.

- Peripheral Hardware Ltd, Unit 13, Monkspath Industrial park, Highlands Road, Shirley, West Midlands B90 4NY have been appointed as an authorised dealer for Epson printers and personal computers.

- Apples have fallen. A new 256K Apple III will now cost a mere £2,395 (it was £2,869); the 128K Apple III is no longer available. Apple Computer (UK) Ltd, Eastman Way, Hemel Hempstead, Herts HP2 7QH.

- AKG are setting up a studio sound award, for professional and non-professional sound engineers. Details from AKG Acoustics Ltd, 191 The Vale, London W3 7QS.

- Instem Computer Systems Limited, formerly known as Kratos, has launched a new software programme for the Hewlett Packard HP-86 microcomputer to perform industrial monitoring and control functions using Instem's range of Link-On input/output stations. Instem Computer Systems Limited, Walton Industrial Estate, Ston, Staffordshire, ST15 0LT.

- One of the consequences of the general election being called at fairly short notice was the fall of a bill that would have made it illegal to sell "any machine capable of reproducing a sound recording . . . where the naute of the machine is such that the primary or substantial use to which it will be likely to be put is likely to result in the unauthorised making of any record embodying the recording . . .". Sounds like a cassette deck they were talking about, doesn't it?

- Thorn EMI have just released a leaflet describing a new range of rubidium caesium photocathode photomultiplier tubes. Contact the Sales Department, Thorn EMI Electron Tubes Limited, Bury Street, Ruislip, Middlesex HA4 7TA.

- Belling Lee have published a comprehensive 64 page catalogue of their range of RFI filters for up to 800 amps. Belling Lee, 540 Great Cambridge road, Enfield, EN1 3QU.

- Cotswold Electronics, Unit T1, Kingsville road, Kingsditch Trading Estate, Cheltenham GL51 9NX have issued a leaflet describing their "budget range" of toroidal mains transformers.

- Tasbian, the automated electronic assembly plant near Plymouth, have also issued a leaflet, describing their design, manufacturing and test facilities. Tasbian Ltd, 2/3 Burrington Way, Plymouth, Devon PL5 3LS.

- You'll no doubt be pleased to hear that the 20 companies involved in the development of magnetic disc stills cameras have reached agreement of standardisation of the disc. This should prevent the usual problem of a multiplicity of standards confusing the consumer, such as happened in video.

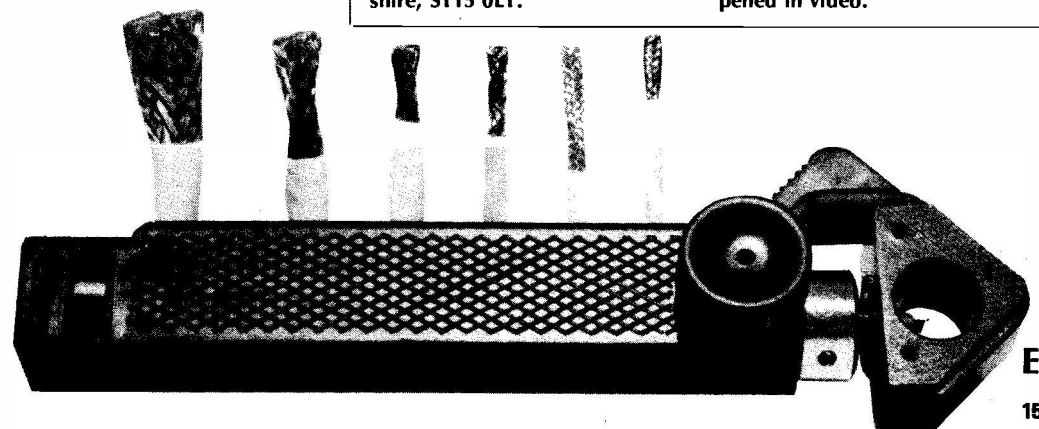
Twin Stripper

AB Engineering Company has developed a unique new cable stripper for the fast and safe removal of outer sheathing from twisted pair coaxial cables. Also suitable for other cables of irregular cross section, the new Coax-3 incorporates a spring loaded cutting head which when revolved accurately follows contours to produce a precise circumferential cut to a pre-determined depth. The operator then simply twists the cutting blade through 90 degrees and the outer sheathing is separated along the axis of the cable for ease of removal. AB Engineering Co., Timber Lane, Woburn, Milton Keynes MK17 9PL.

ponents or cutting tracks.

The instrument has four ranges to allow resistance measurement up to 20k and D.C. voltages between $\pm 20\text{V}$ to be made, so giving a complete range of diagnostic capability in one instrument. Kelvin needle probes are used for fault finding and are protected against accidental connection up to $\pm 30\text{V}$.

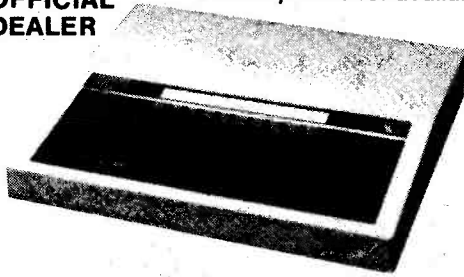
The instrument can also source a test voltage to stimulate circuit under test, with a maximum output voltage of 0.55V and maximum output current 150mA.



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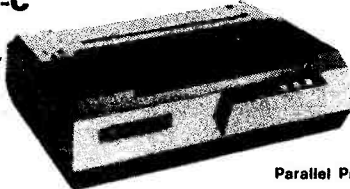
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One of the ironies of life is that the largest single factor in determining how well any sound system performs has nothing to do with the system itself: it is the room.

Now you could adopt an all-or-nothing approach and take a pneumatic drill to your listening room, to get rid of all those resonances, throw out all the furniture, because it's too absorbent, and keep everyone else out of the listening area, because clothes absorb sound too (and bodies, so it's no good asking your friends to go naked). However this could lead to a certain amount of domestic unrest, and anyway, would be impractical at a large scale concert.

A less radical approach that has fewer disadvantages is to tailor the response of the electronics so that the overall response of the audio system plus the room is neutral. This is most usually done with a graphic equaliser.

While octave equalisers do have some use, most equalisers supplied for domestic use are pure gimmickry. If you're taking your equalisation seriously, the only real option is a $\frac{1}{3}$ -octave device, which, by pure coincidence, is what we're about to describe here.

The ETI $\frac{1}{3}$ -octave equaliser is of sufficient quality not to seriously degrade the sound of a high quality system. It should be noted however, that the use of any $\frac{1}{3}$ -octave equaliser will affect the performance of the system simply because it is in circuit. Each of the filters has a

$\frac{1}{3}$ OCTAVE EQUALISER

relatively high Q and will therefore cause significant modification to the overall phase linearity as well as the frequency response when cut or boost is applied. I have seen many otherwise high quality systems degraded significantly by the excessive use of $\frac{1}{3}$ -octave equalisers and we do not recommend the incorporation of these units into a high quality system unless a specific need is apparent. Nevertheless, when modification of the frequency response is required, no matter how drastic or how modest, a $\frac{1}{3}$ -octave graphic equaliser is an almost ideal way of doing this.

Each channel of the equaliser is controlled by a separate slider potentiometer so the array of pots gives an approximate indication of the response inserted.

Design

Each filter is formed by a series resonant network incorporated into the feedback loop of a high quality operational amplifier. In this case we have used the NE5534N.

'Gyrators' are used to simulate

In order to illustrate the principle of operation of the graphic equaliser we first need to consider the operation of a simplified version of a single stage, as illustrated in Figure 1. Here, the input signal is fed to the non-inverting input of an op-amp through a 10k resistor. A potentiometer is connected between the non-inverting inputs with its wiper going to signal common (ground) via a network represented by Z. Here, a series-resonant circuit is employed. Feedback is provided between the op-amp output and the inverting input.

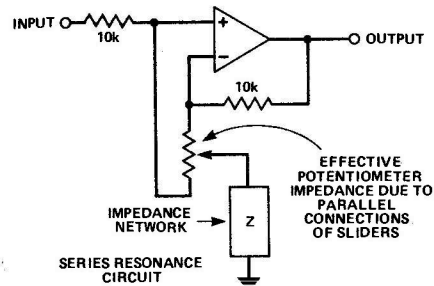
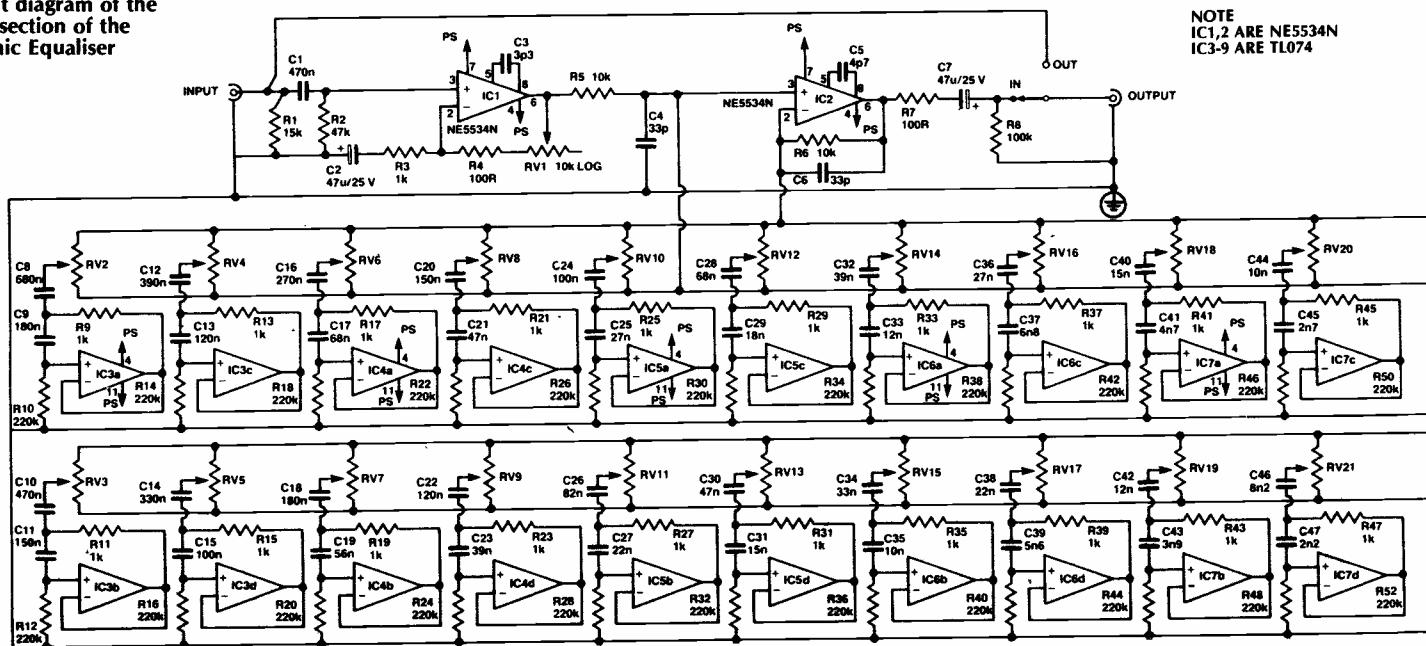


Fig. 1

The input resistor forms a potential divider with part of the potentiometer

Circuit diagram of the main section of the Graphic Equaliser



GRAPHIC

Is your listening room/concert hall dull and lifeless? Or does it echo and ring like the Whispering Gallery? David Tilbrook comes to the rescue with a project that will help get your response into shape.

HOW IT WORKS

(from the op-amp + input to the wiper) and the impedance Z to common. The feedback resistor also forms a potential divider with the end of the pot from the inverting input and the impedance Z to ground.

If the wiper of the pot is set to mid-travel, the attenuation of the input signal due to the potential divider is compensated by the gain of the op-amp and the overall gain from input to output is unity. If the pot wiper is now moved toward that end of the pot connected to the op-amp's inverting input, the gain of the stage is increased as the feedback ratio is reduced owing to a reduction of the impedance from the op-amp's inverting input to common. At the same time less attenuation of the input signal occurs as the impedance from the non-inverting input to common is decreased. The stage will have gain, maximum gain being determined by the impedance of the series resonant networks. If this is low, gain will be high. Series resonant networks exhibit very low impedance at resonance, rising either side of that frequency.

When the wiper of the pot is moved toward the non-inverting input of the op-amp, the attenuation due to the input potential divider is increased. The gain of the op-amp is decreased at the same time as the feedback ratio is increased because the impedance from the inverting input to common is increased. Once again, the overall gain of the circuit is a function of the impedance of the series resonant circuit, but this time the gain is at a minimum — in fact, attenuation occurs.

By choosing a suitable Q for the series resonant network, the bandwidth

can be set to cover a desired frequency range. The potentiometer then sets gain or attenuation of the stage at the centre of the chosen frequency band.

The technique just described above can be used whenever it is desired to incorporate a relatively large number of filters into the signal path as in graphic equalisers or tone controls. The filter networks need not be bandpass or notch filters, simpler bass and treble controls can also be used.

Once this basic configuration is set up, all that remains is to design the filter networks. As mentioned before, series resonant networks were used since these give the required characteristic of low impedance at the resonant frequency. In their simplest form these networks consist of an inductor, capacitor and resistor in series. At the resonant frequency, the impedance of the circuit is equal to that of the resistor assuming a perfect inductor and capacitor were used. To eliminate the inductor an op-amp circuit has been used to simulate the characteristics of an inductor. Such a circuit is called a 'gyrator'.

The gyrator circuit can provide both the inductance and the series resistance required in the network so this can simply be placed in series with the capacitor to form the required resonant circuit. This is shown in block diagram form in Fig. 2.

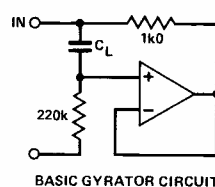
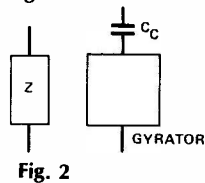


Fig. 3

Figure 3 shows the general circuit of the gyrator used in this project. The amount of inductance 'generated' by this circuit is given by the simple equation:

$$L = 1k \times 220k \times C_L \text{ in Henries}$$

where the value of C_L is in Farads

The equivalent circuit of the gyrator is shown in Fig. 4. The series resistance is equal to the 1k resistor while the 220k resistor becomes the parallel resistance of the coil. This value is high enough not to affect circuit operation drastically. The resonant frequency of this filter is given by the standard formula:

$$F = \frac{1}{2\pi\sqrt{LC}} \text{ in Hertz}$$

The general circuit, simplified, of the Third-Octave Graphic Equaliser is shown in Fig. 5. IC1 is simply a variable gain stage which also provides some input buffering. IC2 is the filter stage with a group of 28 gyrator circuits, all connected in parallel, in the feedback circuit. Commencing at a centre frequency of 31.5 Hz, each gyrator filter has a Q chosen such that its bandwidth covers one-third of an octave. Thus the upper and lower the 3 dB points of adjacent filters 'touch'. A total of 28 filters are required to cover the audio frequency band. Filters are not placed on the band limits of 20 Hz and 20 kHz as they are not really required. To reduce the IC count a set of seven quad op-amps (TL074s or uA774s) are used for the gyrators.

Slide pots are used to set the gain or attenuation inserted for each third-octave band as it is easy to see, at a glance, how much gain or attenuation has been set and, as all the pots are lined up in parallel across the front panel, one can instantly see the total modification made to the audio system's frequency response.

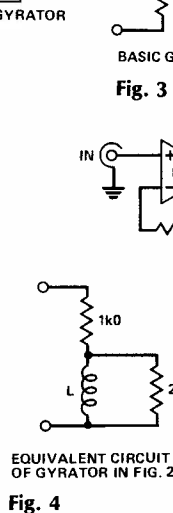
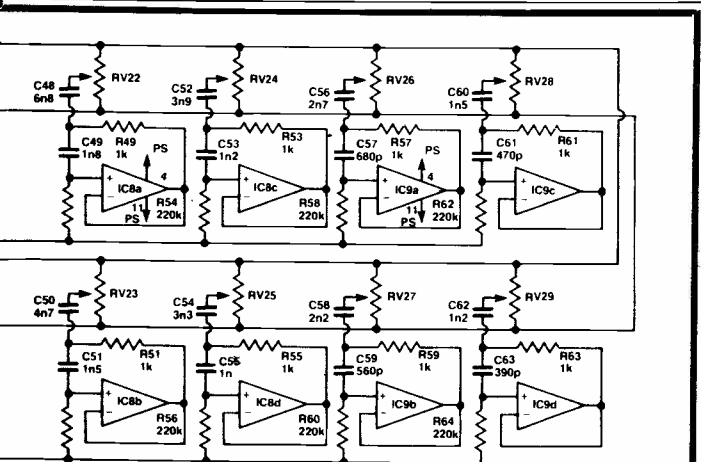


Fig. 4

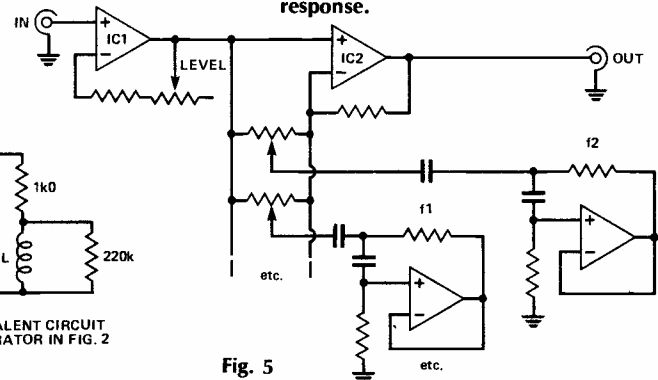


Fig. 5

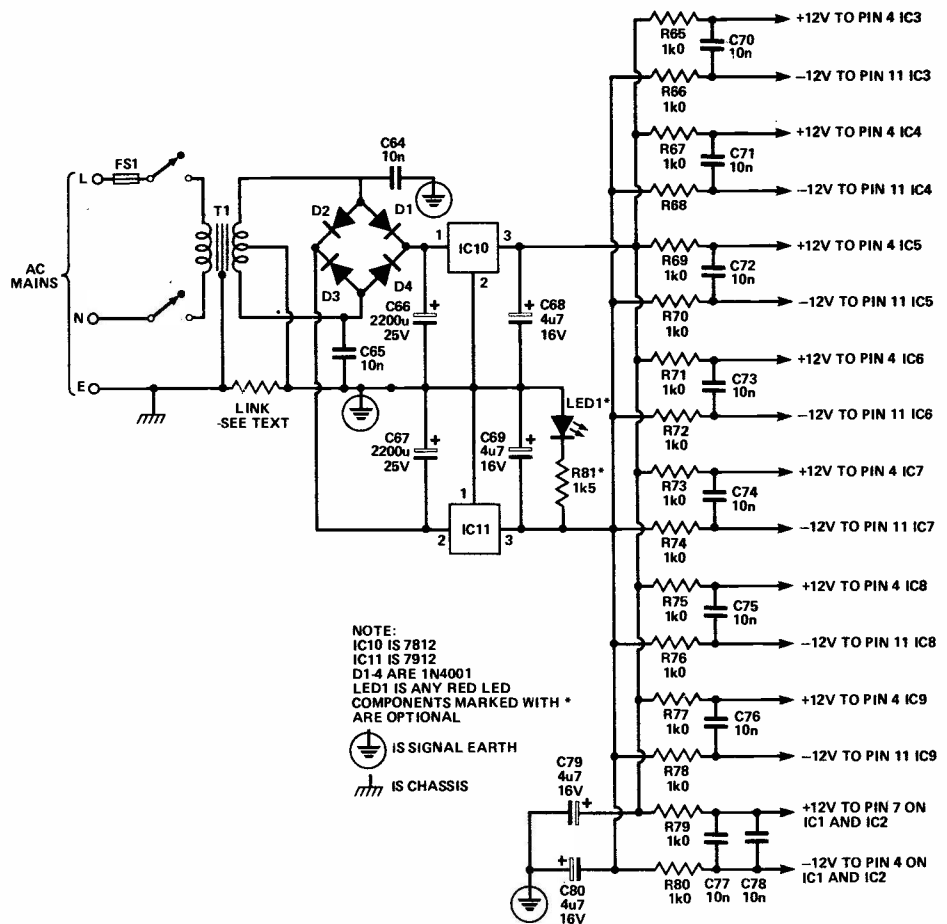
PROJECT : Graphic Equaliser

the inductors necessary for the series of band-pass filters so there are no coils to wind. The gyrator is covered in more detail in the How it Works section, but the main problem associated with this approach is caused by phase shifts occurring in the op-amps used in the gyrators. The basic principle of a gyrator is to invert the phase response of a capacitor to simulate the characteristics of an inductor. The problem is that all amplifiers introduce a phase shift which increases towards the extremes of the frequency response. For this reason, care must be taken when choosing op-amps for use in gyrators at the top end of the frequency spectrum. This problem is accentuated when the Q of the filters concerned is increased. Since the Q of the filters must be higher in a $\frac{1}{3}$ -octave equaliser, an op-amp with greater phase linearity at high frequencies must be used. Fortunately, op-amps with the desired characteristics are not difficult to obtain and we are using the TL074 or uA774. These are both quad FET op-amps with almost identical performance and are capable of excellent results in the circuit, even in the top-most filter.

Earthing

In any large multi-component audio system, earthing is a continuous nightmare because of hum loops. The theory says that the entire audio circuit should be earthed at only one point. However, adding an extra earth connection can sometimes cure a hum that you've spent many hours chasing round the circuit — this is one of those occasions when the best approach is to leave it like that (but keep your fingers firmly crossed), hope it holds while the band is playing, and forget about it afterwards . . .

The other problem is deciding exactly where this one earth should be in the first place. Some people say the very start of the signal path — or, at least, as close as you can get to it. Others say that it should be at the power amp input. But everyone agrees — it's definitely never at the graphic equaliser. OK, then, what connection should there be between the mains earth and the graphic equaliser electronics? Some opt for a capacitor (100n is a reasonable value); others use a resistor (10 to 100R). We've left this up to you. However, all agree that there must also be a very low



Circuit of the power supply for the Graphic Equaliser.

impedance path to earth through the rest of the equipment for safety reasons: if there isn't, you're asking for a nasty shock. Note also that you must use insulated audio input and output sockets, and be careful not to inadvertently connect the signal and mains earth in any other way — watch how you secure the PCB to the case, for example.

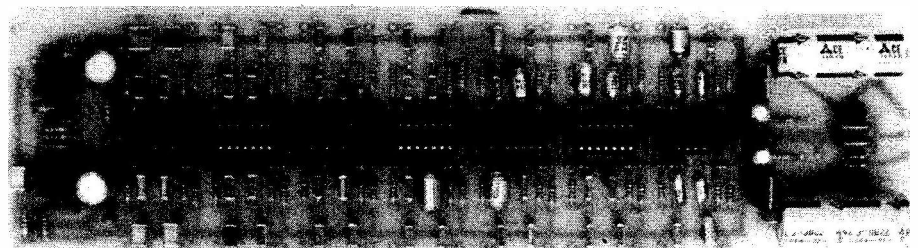
Capacitors

One possible area of trouble is in finding a supplier for the capacitors. If you look at the Parts List, you'll see that lots of the capacitors are in the E12 series: we hadn't realised how many suppliers had switched to supplying just the E6 series until we tried to locate a

supplier for a suitable type. In the end, we used Siemens polycarbonate layer types from Cricklewood for all the capacitors above 10n in value, and mixture of these and polystyrene for those under 1n0. Ours were all 5% types or better, and we'd strongly suggest that you use 5% tolerance or better for all the capacitors in the gyrators. We've designed the PCB so that it should accommodate most types you're likely to want to use.

Next month we will give constructional details of the Graphic Equaliser, including details of a super specially designed case from Newrad Instruments.

ETI



This is the completed PCB — more details next month.

CARBON FILM 5% H 182 100 20 10M 15W E24 2p 15W E27 2p 15W E27 3p 15W E27 4p 15W E27 5p 15W E27 6p	IDEAL AS MAINS SUPPRESSORS 1000V 15F 22h 15F 35p 15F 47p 15F 55p 15F 65p 15F 75p 15F 85p	100.0V 32p MANY MORE CARBON ORS IN STOCK P.L.S. PHONE 100mA 6.0-8V 9.0V, 12.0-12V 10-15V 95p	2.5 x 17 2.99 2.5 x 17 3.85 4.7V 17 4.93 Vj Board 1.92 Dig Board 3.90 Track Cutter 1.48 37 way 2.50 Pin Insertor 1.79 100 Pins 55p	CONDUCTORS R3 9x5x2 1.15 R4 11x6x3 3.85 R5 11x7x4 3.75 R6 13x8x4 4.75 R7 15x8x4 7.35	VEROBONES V1 3x2x1 1.15 V2 120x80 55p V3 180x110x55 V5 220x174x 100mm 10.40 15mm 10.40 16V 171x121x 75mm 5.65 REMOTE (Handheld) BOX 94x61x22.5mm White 89p	VEROBONES V1 3x2x1 1.15 V2 120x80 55p V3 180x110x55 V5 220x174x 100mm 10.40 15mm 10.40 16V 171x121x 75mm 5.65 REMOTE (Handheld) BOX 94x61x22.5mm White 89p	PCB RELAYS 24VAC 10 Rps C contacts SPDT 1x1/2 6v 72D 2.75 12V 285V 2.75 24V 1150V 2.95 48V 4600V 3.04	2N1102 35p 2N1127 35p 2N1218 25p 2N1218A 25p 2N1219 25p 2N2220 25p 2N2222 25p 2N2223 2.60 2N223A 4.15 2N2918 35p 2N2919 35p 2N2919A 35p 2N2920 35p 2N2921 3.47 2N2922 3.47 2N2923 2.5p 2N2924 1.5p 2N2925 1.5p 2N2926 1.0p 2N3010 75p 2N3011 65p 2N3012 65p 2N3013 27p 2N3014 1.85 2N3015 1.85 2N3055A 1.20 2N3056 1.85 2N3058 1.85 2N3059 1.85 2N3059A 1.85 2N3059B 1.85 2N3059C 1.85 2N3059D 1.85 2N3059E 1.85 2N3059F 1.85 2N3059G 1.85 2N3059H 1.85 2N3059I 1.85 2N3059J 1.85 2N3059K 1.85 2N3059L 1.85 2N3059M 1.85 2N3059N 1.85 2N3059O 1.85 2N3059P 1.85 2N3059Q 1.85 2N3059R 1.85 2N3059S 1.85 2N3059T 1.85 2N3059U 1.85 2N3059V 1.85 2N3059W 1.85 2N3059X 1.85 2N3059Y 1.85 2N3059Z 1.85	2N6126 75p 2N6127 75p 2N6130 75p 2N6131 75p 2N6132 75p 2N6133 75p 2N6134 75p 2N6135 75p 2N6136 75p 2N6137 75p 2N6138 75p 2N6139 75p 2N6140 75p 2N6141 75p 2N6142 75p 2N6143 75p 2N6144 75p 2N6145 75p 2N6146 75p 2N6147 75p 2N6148 75p 2N6149 75p 2N6150 75p 2N6151 75p 2N6152 75p 2N6153 75p 2N6154 75p 2N6155 75p 2N6156 75p 2N6157 75p 2N6158 75p 2N6159 75p 2N6160 75p 2N6161 75p 2N6162 75p 2N6163 75p 2N6164 75p 2N6165 75p 2N6166 75p 2N6167 75p 2N6168 75p 2N6169 75p 2N6170 75p 2N6171 75p 2N6172 75p 2N6173 75p 2N6174 75p 2N6175 75p 2N6176 75p 2N6177 75p 2N6178 75p 2N6179 75p 2N6180 75p 2N6181 75p 2N6182 75p 2N6183 75p 2N6184 75p 2N6185 75p 2N6186 75p 2N6187 75p 2N6188 75p 2N6189 75p 2N6190 75p 2N6191 75p 2N6192 75p 2N6193 75p 2N6194 75p 2N6195 75p 2N6196 75p 2N6197 75p 2N6198 75p 2N6199 75p 2N6200 75p	BC187A 10p BC187B 10p BC187C 10p BC187D 10p BC187E 10p BC187F 10p BC187G 10p BC187H 10p BC187I 10p BC187J 10p BC187K 10p BC187L 10p BC187M 10p BC187N 10p BC187O 10p BC187P 10p BC187Q 10p BC187R 10p BC187S 10p BC187T 10p BC187U 10p BC187V 10p BC187W 10p BC187X 10p BC187Y 10p BC187Z 10p	BC609 35p BC610 35p BC611 35p BC612 35p BC613 35p BC614 35p BC615 35p BC616 35p BC617 35p BC618 35p BC619 35p BC620 35p BC621 35p BC622 35p BC623 35p BC624 35p BC625 35p BC626 35p BC627 35p BC628 35p BC629 35p BC630 35p BC631 35p BC632 35p BC633 35p BC634 35p BC635 35p BC636 35p BC637 35p BC638 35p BC639 35p BC640 35p BC641 35p BC642 35p BC643 35p BC644 35p BC645 35p BC646 35p BC647 35p BC648 35p BC649 35p BC650 35p BC651 35p BC652 35p BC653 35p BC654 35p BC655 35p BC656 35p BC657 35p BC658 35p BC659 35p BC660 35p BC661 35p BC662 35p BC663 35p BC664 35p BC665 35p BC666 35p BC667 35p BC668 35p BC669 35p BC670 35p BC671 35p BC672 35p BC673 35p BC674 35p BC675 35p BC676 35p BC677 35p BC678 35p BC679 35p BC680 35p BC681 35p BC682 35p BC683 35p BC684 35p BC685 35p BC686 35p BC687 35p BC688 35p BC689 35p BC690 35p BC691 35p BC692 35p BC693 35p BC694 35p BC695 35p BC696 35p BC697 35p BC698 35p BC699 35p BC700 35p
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BD 124 (Mullard)

THE MOTOCAR

Could this fairly ordinary looking Lancia car be the Car Of The Future? Motorola certainly think so. Read on and see if you agree.

At a press conference recently, Motorola revealed their Motocar (who says ETI has a monopoly on bad puns?). It's a Lancia Delta with a lot of electronics where there used to be switches and yards and yards of copper wire.

Even though they were very nice to us, impressing the press wasn't Motorola's reason for spending the equivalent of several Rolls Royces on building the car. Their main targets are the car and car component manufacturers. Not only are Motorola trying to persuade them that they need to bring car electrics up to date, but that they should use Motorola products to do this; and further, that they should work closely with Motorola to get the products they need. So, the car itself is by no means a finished design, it's a try out for a large number of different ideas.

Why Go Electronic?

Conventionally-wired cars have been around for quite a while now, so why should anyone want to change? Well, from the manufacturers' point of view, there are a number of good reasons.

Firstly, and always firstly in manufacturing, there's cost. At present, a wiring loom for a car costs around £35. Motorola's electronic system, with a great host of additional features that we'll be looking at in a moment, would cost around £100 to build after a tidy up of the prototype. Obviously, Motorola learned a few things during the building, and some newer components better suited to the project have since come on the market, so with a little optimisation, the cost could probably be halved to £50. However, once you start to use specially made components, a lot more cost saving can be carried out, and the price would easily go below that of the conventional loom, especially if the price of copper rises. And the electronic system will almost certainly be a lot easier to install.

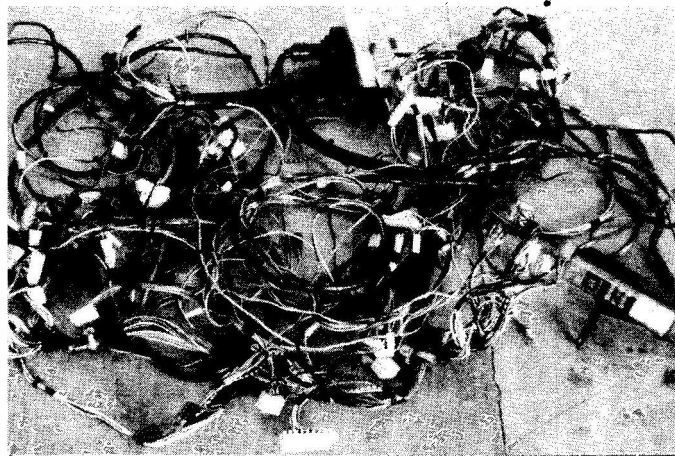
Secondly, there's reliability. Well designed electronics should always be much more reliable than electro-mechanics. An electronic loom would considerably reduce the number of connectors in the system. Not only would this improve the car's reliability after sale, it would also cut down on manufacturing costs. Did you know that around 40% of all cars straight off the production line require some remedial work to be done on their electrical systems?

Thirdly, by using electronic control, the engine's performance can be much improved. Fuel efficiency is very important in Europe, but over in the States, tough anti-pollution legislation has led to emphasis on emission control. It was, in fact, this legislation that provoked the interest in electronic engine control in the first place — who says that conservation is always bad for industry?

Finally, an electronic control system can offer driver and servicing facilities very much more easily than the conventional system; for example, fault finding and fault monitoring can be automated.

Why The Rush?

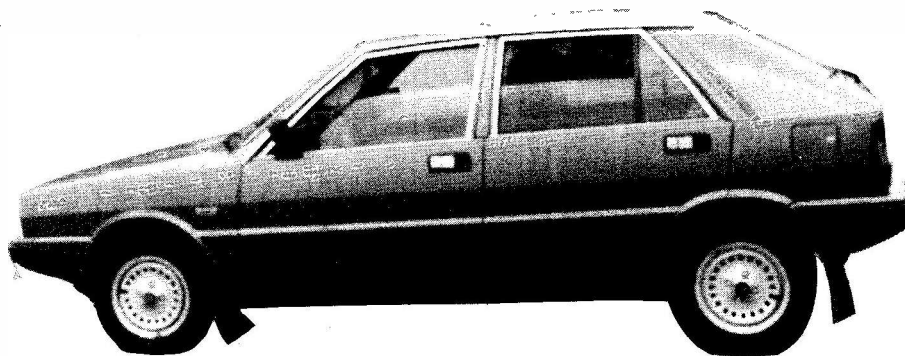
Motorola are keen to get into the market as soon as possible. They reckon that by 1987, 7% of the European semiconductor market will be for cars. Naturally, they're expecting a certain amount of competition, but they hope that their early start will catch their competitors napping.

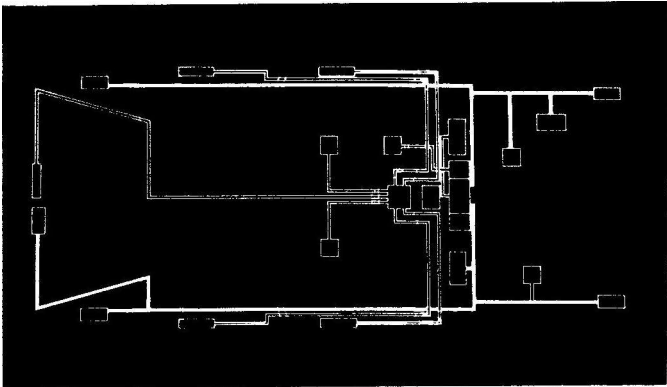


This is what the Motocar no longer has — a conventional (messy) wiring loom containing about 500 metres of wire.

Take A Bus

At the heart of Motorola's electronics is a four-wire multiplexed bus. This links the master control unit to a number of outstations that are responsible for controlling





The layout of the main bus and the fibre-optic bus: the fibre optic bus radiates out from where you'd expect the gearshift to be. The main bus is in a H-shape and is drawn with a solid white line.

and monitoring the car's functions. The master control has a separate interface with the controls on the steering column, and there is also a completely separate fibre optic system that controls some 'luxury' items.

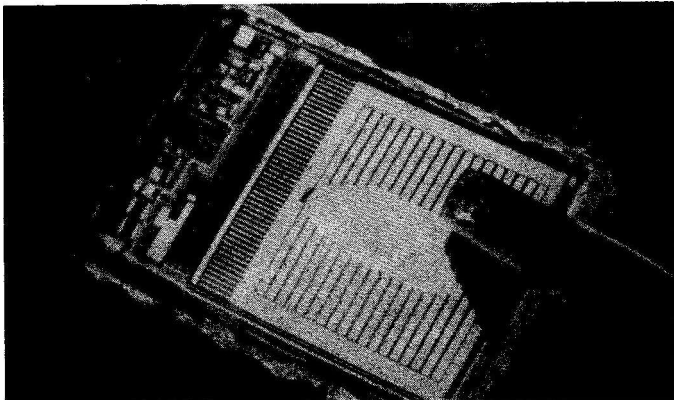
The four wires of the bus have the following functions: power (positive, negative return through chassis), signal earth, data, and bus control. Data transmission is sequential and bidirectional in half duplex mode with auto-clocking and RZ. The control line is used to sort out which unit is sending what to where. The power line is for the controlled devices as well as for the outstations themselves, so it has to be fairly meaty. All the other conductors can be light weight.

Outstations

All the outstations are based on the Motorola MC6805P2 microprocessor, as is the master control unit. Motorola now say that they would now use the cheaper and more appropriate MC6804P2, but it was not available when the design work was done.

The simplest of the outstations are the load-switching units, of which there are six, all identical. Each is capable of switching eight loads of up to 10 A, although in the present car, the most that is used in any one unit is seven (some units switch rather fewer). Because N-channel devices are cheaper to make than P-channel ones, N-channel T-MOS FETs are used to switch between the ground connection to the controlled devices and the car chassis; this means that the controlled load is always at positive supply potential with respect to the chassis, and this could lead to a corrosion problem.

Motorola's proposed solution is to use an on-board DC to DC converter to provide a higher voltage supply of 30 V. This will allow the N-channel FETs to switch reliably at the standard supply voltage (nominal 12 V) in common drain mode, even when the system is suffering from a



Motorola's smart power device — to be used for future load switching stations.

reduction in supply voltage (for instance, while the battery is turning over the engine on the starter motor). Surprising though this may seem, it is apparently cheaper to do this than to use P-channel FETs.

Each load switching unit has an A-to-D converter on board, so that it can measure, for example, the output from the petrol tank gauge. It also has a load-state monitor that can sense blown bulbs. This information is all transmitted back along the bus to the central control.

Further development of the load switching unit will almost certainly involve Motorola's smart power device, soon to enter production. These devices have a T-MOS power transistor with logic and drive components on the same chip (together with, perhaps, a DC to DC converter). These may make it feasible to use single load switching units, with each load on the bus having its own dedicated switching unit. In order to avoid increasing the number of connections by using these units, they may well be housed within the controlled load itself.

Condition Monitoring

Hard at work just gathering and transmitting data is the vehicle condition monitor, one of the four other types of outstation. It sits inside the engine compartment and monitors fluid levels and other information to be presented to the driver. A single A-to-D is used to monitor the alternator output, and, as well as being used to provide the system's equivalent of an ignition warning light, this also determines the control of the battery charging.

The other three outstations are semi-autonomous in that they are not under direct central control: for instance, you could not have the engine control unit having to deal with an interrupt when it was just about to fire a spark plug. Besides the engine control unit, there are the cruise control, so that you can take your foot off the accelerator and the car will maintain a steady (and legal) speed, and the climate control, a posh phrase for an air conditioner control unit.

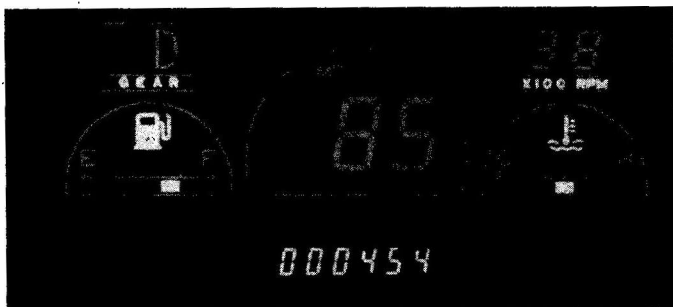
The engine control has a pressure transducer in the inlet manifold; it also measures the position of the distributor arm in 0.35° increments (by using a phase locked loop to multiply up the output from a position sensor). Thus it can control the spark and fuel injection timing to a resolution of 0.35°; it can also control the amount of fuel injected. However, the opening and closing of the inlet and outlet valves is still done mechanically.

Alternative Bus

To avoid running lots of wires from the controls mounted on the steering column, Motorola engineered a much more simple multiplexed bus to link the steering column to the central control unit. It's a three wire bus, with unidirectional data flow; the encoding is done with standard CMOS, rather than a microprocessor (shame!).

Gone is the familiar needle and dial speedo — it's replaced by a fluorescent digital display, as in the latest Maestro. The display itself is an off the shelf Futaba plasma display, driven by (you've guessed it) a dedicated microprocessor, this time an MC6801. To be fair, the micro is kept busy displaying a range of messages (in a choice of several languages and imperial or metric units) on two separate LCD displays to tell the driver about the state of the car, distance travelled, etc. For instance, it is this that will tell you if one of bulbs has blown.

One interesting feature is the use of an EEPROM to store the odometer reading. When the ignition is turned off, power is held on long enough to allow the old reading to be erased and the new one written into the EEPROM. Motorola have put quite a lot of thought into developing a system that is as secure as possible, to prevent

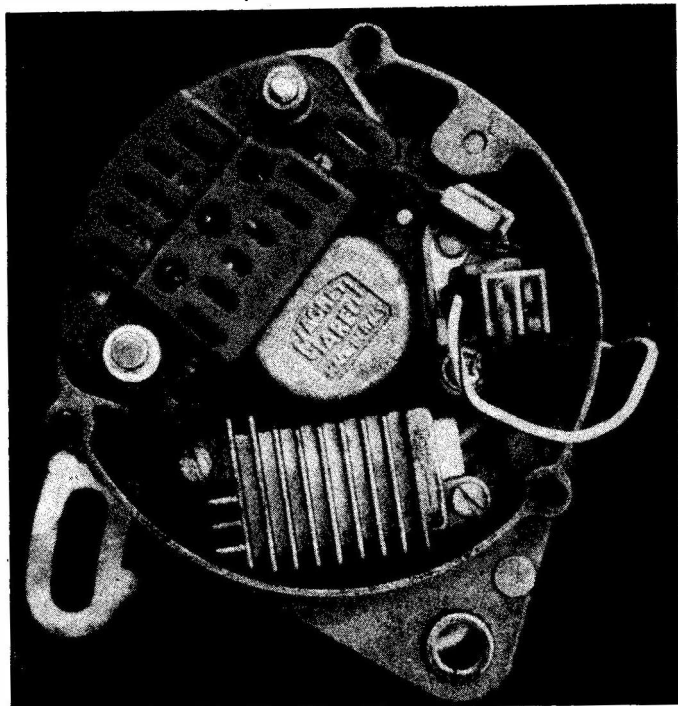


The Futaba display used, in full action. Unfortunately, you can't see that the figures are in a rather reassuring green, and the main beam indicator is in a baby blue . . .

unscrupulous dealers from being able to wind back the reading.

Multiplexed?

Motorola claim that rather than confusing the poor mechanic, the multiplexed bus system should make ser-



Above: one nice touch not mentioned so far is that Motorola have tackled the problem of supply line transients at source, the alternator, by replacing three out of nine of the diodes with transient suppression types.

The present test unit (right) is just a little bigger than a hand-held calculator (though this does depend on how big your hands are . . .) Apparently the production model would need little more than a (yes, another) microprocessor, some ROM (possibly on board the micro) and a display.



vice and repair easier — but only provided that the garage buys a special adapter! This special unit would, when plugged into the car, take control of the bus and run the car through a test sequence, with a readout that tells the mechanic what needs attention. The special adaptor units should be around the size of a largish pocket calculator and cost about £150 (a special one will be needed for each car type).

Shine A Light

The other multiplex system uses optical fibres to control seat positioning servos, windows, door locking and window mirror positioning. This system is entirely separate from the other bus system, and it has its own control unit; it's also arranged in a different way, as a star network. Each unit has its own line running back to the control unit: this was necessary because of the lack of T-junctions for optical fibres.

Motorola's optical fibre system is unusual in two ways. Firstly, the same devices are used as transmitters and receivers, thus allowing two-way transmission along a single fibre. Because only short transmission distances are involved, signal strength is not a problem and a relatively inefficient detector can be tolerated.

Secondly, visible light is used because this will make it easier for a "mechanic" (perhaps Motorola had better invent a new term for this person while they're at it) to detect if a signal is present. The cost of the components needed for a visible light system is also considerably lower than those for an infra-red system.

Motorola say that fibre optic systems are used because they offer higher noise immunity and lower weight than copper wire systems. However, the fact that they've been confined to the luxury features of the car is probably evidence of a reliability problem — or is it just my cynicism?

Parting Shot

One last system that we haven't mentioned yet is the radio. It too (yes!) uses a dedicated microprocessor, and even though it's a Grundig radio, the micro is a Motorola MC6220. It's worth reflecting that Motorola started out by making car radios; having partially surrendered that market and gone on to greener pastures, they're now set to invade the rest of the car.

ETI

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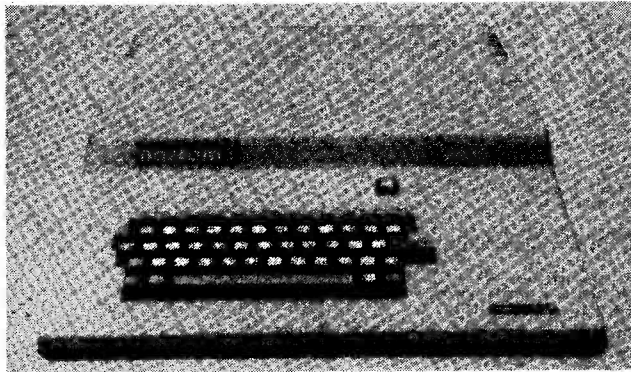
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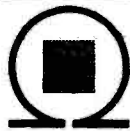
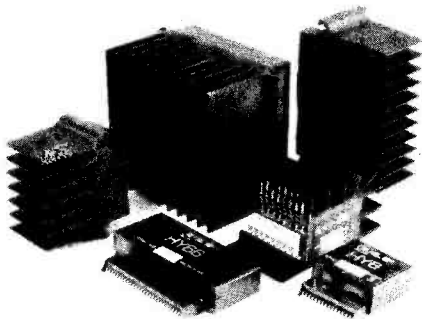
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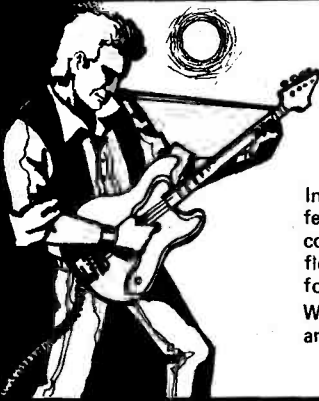
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BIPOLAR MODULES

Module Number	Output Power Watts rms	Load Impedance Ω	DISTORTION		Supply Voltage Typ	Size mm	WT gms	Price inc. VAT
			T.H.D. Typ at 1KHz	I.M.D. 60Hz/7KHz 4:1				
HY30	15	4-8	0.015%	<0.006%	± 18	76 x 68 x 40	240	£8.40
HY60	30	4-8	0.015%	<0.006%	± 25	76 x 68 x 40	240	£9.55
HY6060	30 + 30	4-8	0.015%	<0.006%	± 25	120 x 78 x 40	420	£18.69
HY124	60	4	0.01%	<0.006%	± 26	120 x 78 x 40	410	£20.75
HY128	60	8	0.01%	<0.006%	± 35	120 x 78 x 40	410	£20.75
HY244	120	4	0.01%	<0.006%	± 35	120 x 78 x 50	520	£25.47
HY248	120	8	0.01%	<0.006%	± 50	120 x 78 x 50	520	£25.47
HY364	180	4	0.01%	<0.006%	± 45	120 x 78 x 100	1030	£38.41
HY368	180	8	0.01%	<0.006%	± 50	120 x 78 x 100	1030	£38.41

Protection: Full load line. Slew Rate: 15v/ μ s. Risetime: 5 μ s. S/N ratio: 100db. Frequency response (-3dB) 15Hz - 50KHz. Input sensitivity: 500mV rms. Input Impedance: 100K Ω . Damping factor: 100Hz >400.

PRE-AMP SYSTEMS

Module Number	Module	Functions	Current Required	Price inc. VAT
HY6	Mono pre amp	Mic/Mag. Cartridge/Tuner/Tape/Aux + Vol/Bass/Treble	10mA	£7.60
HY66	Stereo pre amp	Mic/Mag. Cartridge/Tuner/Tape/Aux + Vol/Bass/Treble/Balance	20mA	£14.32
HY73	Guitar pre amp	Two Guitar (Bass Lead) and Mic + separate Volume Bass Treble + Mix	20mA	£15.36
HY78	Stereo pre amp	As HY66 less tone controls	20mA	£14.20

Most pre-amp modules can be driven by the PSU driving the main power amp. A separate PSU 30 is available purely for pre amp modules if required for £5.47 (inc. VAT). Pre-amp and mixing modules in 18 different variations. Please send for details.

Mounting Boards

For ease of construction we recommend the B6 for modules HY6-HY13 £1.06 (inc. VAT) and the B66 for modules HY66-HY78 £1.29 (inc. VAT).

POWER SUPPLY UNITS (Incorporating our own toroidal transformers)

Model Number	For Use With	Price inc. VAT	Model Number	For Use With	Price inc. VAT	Model Number	For Use With	Price inc. VAT
PSU 21X	1 or 2 HY30	£11.93	PSU 52X	2 x HY124	£17.07	PSU 72X	2 x HY248	£22.54
PSU 41X	1 or 2 HY60, 1 x HY6060, 1 x HY124	£13.83	PSU 53X	2 x MOS128	£17.86	PSU 73X	1 x HY364	£22.54
PSU 42X	1 x HY128	£15.90	PSU 54X	1 x HY248	£17.86	PSU 74X	1 x HY368	£24.20
PSU 43X	1 x MOS128	£16.70	PSU 55X	1 x MOS248	£19.52	PSU 75X	2 x MOS248, 1 x MOS368	£24.20
PSU 51X	2 x HY128, 1 x HY244	£17.07	PSU 71X	2 x HY244	£21.75			

Please note: X in part no. indicates primary voltage. Please insert "0" in place of X for 110V, "1" in place of X for 220V, and "2" in place of X for 240V.

MOSFET MODULES

Module Number	Output Power Watts rms	Load Impedance Ω	DISTORTION		Supply Voltage Typ	Size mm	WT gms	Price inc. VAT
			T.H.D. Typ at 1KHz	I.M.D. 60Hz/7KHz 4:1				
MOS 128	60	4-8	<0.005%	<0.006%	± 45	120 x 78 x 40	420	£30.41
MOS 248	120	4-8	<0.005%	<0.006%	± 55	120 x 78 x 80	850	£39.86
MOS 364	180	4	<0.005%	<0.006%	± 55	120 x 78 x 100	1025	£45.54

Protection: Able to cope with complex loads without the need for very special protection circuitry (fuses will suffice).

Slew rate: 20v/ μ s. Rise time: 3 μ s. S/N ratio: 100db. Frequency response (-3dB): 15Hz - 100KHz. Input sensitivity: 500mV rms. Input impedance: 100K Ω . Damping factor: 100Hz >400.

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C1515

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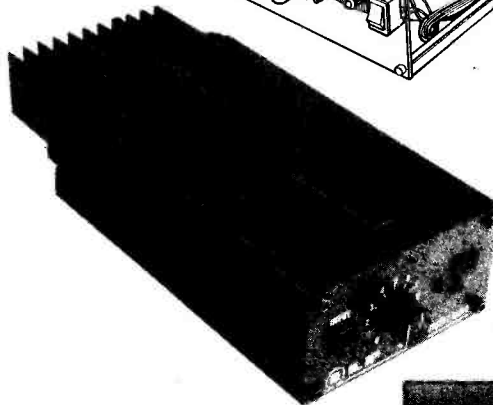
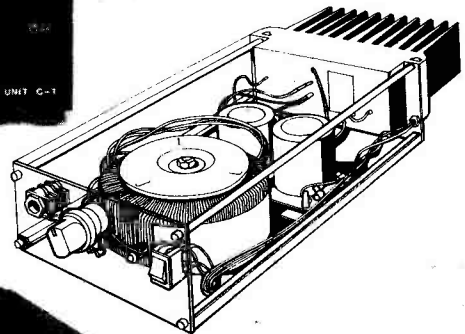
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POWER AMPS: The UP series feature a clean line front panel incorporating on/off switch and concealed indicator. They are designed to compliment the style of the UC1 pre-amp. Performance for each unit which includes the appropriate power supply, is as specified on the facing page.

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UP3X	60W/8Ω	Bipolar	Mono	HiFi	£54.95
UP4X	120W/4Ω	Bipolar	Mono	HiFi	£74.95
UP5X	120W/8Ω	Bipolar	Mono	HiFi	£74.95
UP6X	60W/4-8Ω	MOS	Mono	HiFi	£64.95
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TV STORAGE SCOPE

The Tele-Scope 200S is a storage oscilloscope which utilises a number of electronic techniques to convert signals into a form suitable for display on a television screen. The unit is designed around the latest technology in analogue-to-digital conversion, using the Ferranti ZN441 flash converter to convert the input signal to a six-bit binary word at a point in time, which is determined by the sample rate. This sample rate can be selected to be up to 10 million samples per second (or one sample producing one word every 100 nS).

The resulting words are stored in one of two memories, which take it in turns to store the incoming

data and display the stored data. In manual trigger mode, the incoming signal controls the changeover of the two memories, so if the input signal only occurs once, or is removed, the last signal is displayed on the screen. When measuring DC levels, the auto trigger mode is used to give a continuous trigger, as the DC level has no recognisable transitions for the circuit to begin operation.

Functional Description

The analogue input is taken via the input coaxial socket to a switchable attenuator and is buffered with a source-coupled FET. A second FET in the source of this buffer puts a DC offset on the

buffer, which can be varied to produce a shift in the position of the display.

The resultant analogue signal is fed to the analogue-to-digital flash converter which produces a six-bit word for each sample. The sample rate can be up to 10 MHz (one sample every 100 nS), and is selected using the front panel switch marked 'width' in the same way that a conventional scope has a time base selector. The six-bit word will appear on the data bus and the input address clock, which is running at the sample rate, writes the data in to the selected memory.

When both the memory cycle and frame scan are completed, the memory is switched to read and the

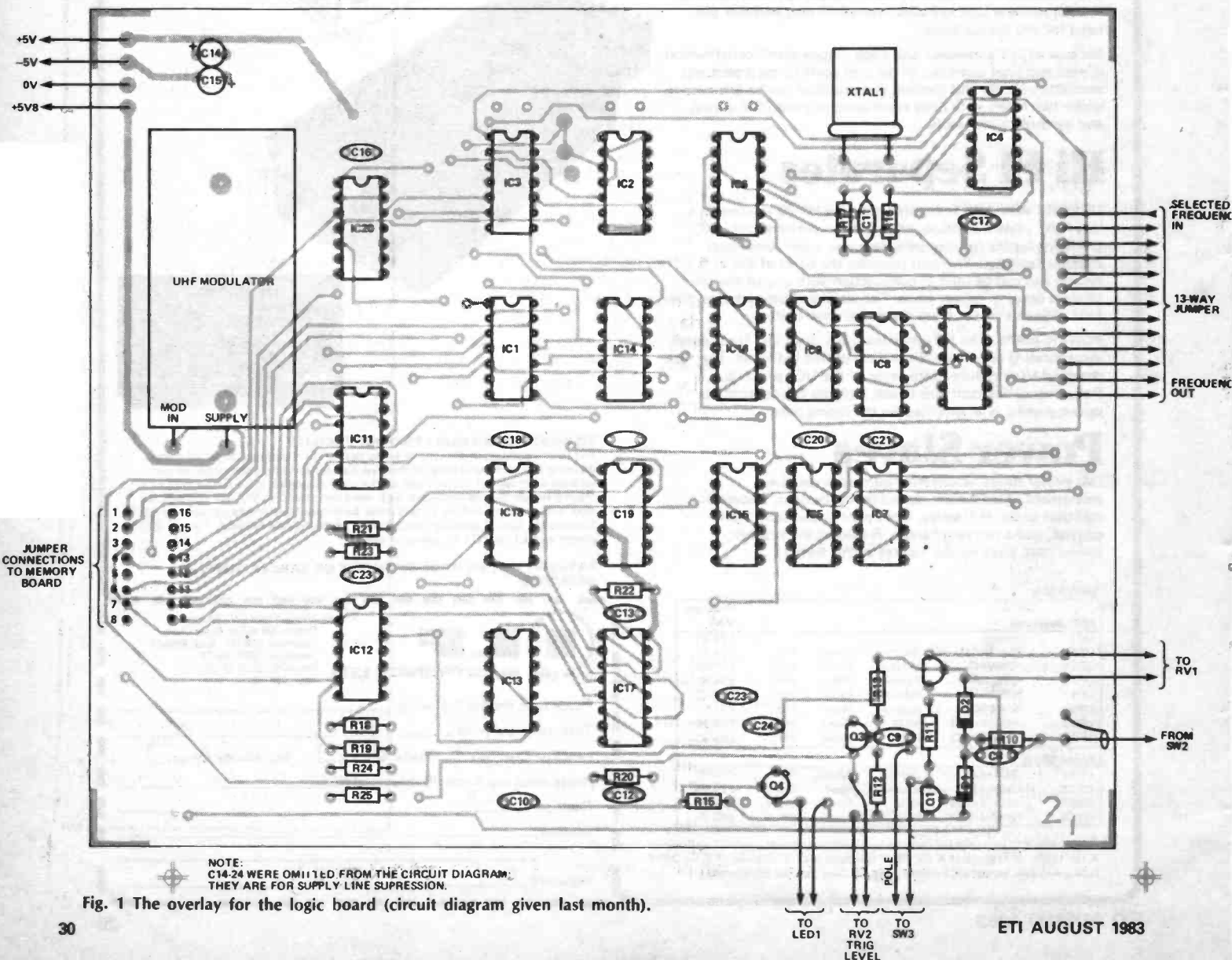


Fig. 1 The overlay for the logic board (circuit diagram given last month).

We conclude our description of this innovative piece of test gear with the circuit of the data processing board and full constructional details. Design and development by Ian Gooderson.

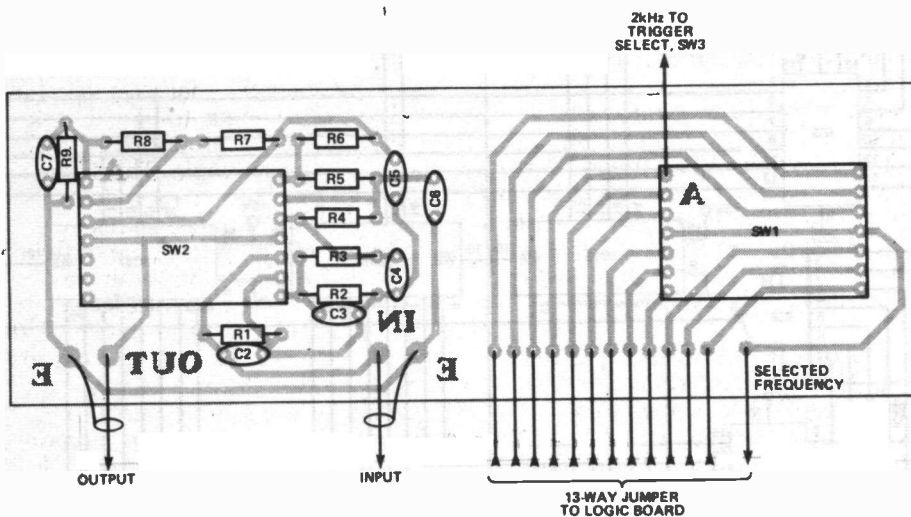


Fig. 2 Overlay for the front panel PCB, containing the input attenuator.

output address counter is routed to this memory for the output sequence to begin. The output address counter is cycled at 5 MHz and the six-bit words are output to a comparator, which compares the word to the video line number. If the six-bit word and the line number are equal, the comparator outputs a data bit to the video summing amplifier.

This data is then mixed with the line and frame sync pulses and output to the UHF modulator. The display has a memory map which is 247 pixels wide by 64 pixels high; each pixel is 200 nS wide and four lines high, utilising a screen area of 49.4 nS wide and 256 lines high. This data is repeated on the second field of the interlaced TV scan to prevent any flashing on the display, even at high input frequencies.

The memories are addressed by two counters and during the input cycle the input address counter is running at the same rate as the A-to-D, storing each data bit in a separate serial memory location. The output address counter is running at a constant 5 MHz as the display time is constant.

Construction

The Tele-Scope contains two double-sided, plated-through hole circuit boards, one for the data storage and routing, one for the control logic and analogue input buffering. The case cover has a

small PCB on the reverse, which holds some of the components associated with the input and trigger controls and the corresponding input sockets. The power supply board is mounted in the rear of the case, with the transformer to the left (viewed from the front).

First build the data storage and routing board (the circuitry for this board is described in this month's article). All the components are mounted on the circuit board (see the overlay in Fig. 5). All the connections to this board are made via a 16-way jumper lead to the control logic board (whose circuitry was described last month). All the ICs used are LS TTL series, with the exception of the memories and the ZN441. Although this latter chip is not static-sensitive, great care should be taken when handling it because it is the single most costly item in the equipment. For this reason it should be mounted in a 24-pin IC socket.

Next, build the control logic/input buffer board. All the chips on this board are LS TTL, with no special handling problems for them or any of the other discrete components used. A 16-way jumper lead connects this board to the data processing PCB. A 13-way length of ribbon cable should also be connected at the other end of the PCB at this point in the proceedings, for later connection to the sampling frequency selector

PARTS LIST — LOGIC BOARD

Resistors (all 1/4W, 5% except where stated)

R1	560k 2%
R2	270k 2%
R3	180k 2%
R4	56k 2%
R5	27k 2%
R6	18k 2%
R7	5k6 2%
R8, 9	2k7 2%
R10, 15	10k
R11	220R
R12	1M0
R13	470k
R14, 25	47R
R16, 17	330R
R18, 19	270R
R20	4k7
R21, 23	1k0
R22	56k
R24	470R

Potentiometers

RV1,2	10k linear
-------	------------

Capacitors (all ceramic except where stated)

C1,8-10,16-24	100nF
C2	100pF
C3, 5	20pF
C4	120pF
C6	68pF
C7	10pF
C11	27pF
C12, 13	2n2
C14,15	22uF 16 V PCB electrolytic

Semiconductors

IC1	74LS04
IC2, 6, 11	74LS74
IC3	74LS10
IC4	74LS00
IC5, 7-10	74LS90
IC12	74LS03
IC13-16, 19	74LS93
IC17	74LS123
IC18	74LS73
IC20	74LS08
Q1-3	2N3819
Q4	BC107
D1, 2	1N4148
LED1	red LED

Miscellaneous

SW1	SPDT slide switch
SW2	9-way PCB-mounting rotary switch
SW3	2-pole, 3-way slide switch (only one half used)
SW4	12-way PCB-mounting rotary switch
XTAL1	10 MHz
PCBs (see Buylines); UHF modulator type UM 1111E36; ribbon cable; sloping front case (see Buylines); screened cable for input; PCB pillars; power supply board (see Buylines).	

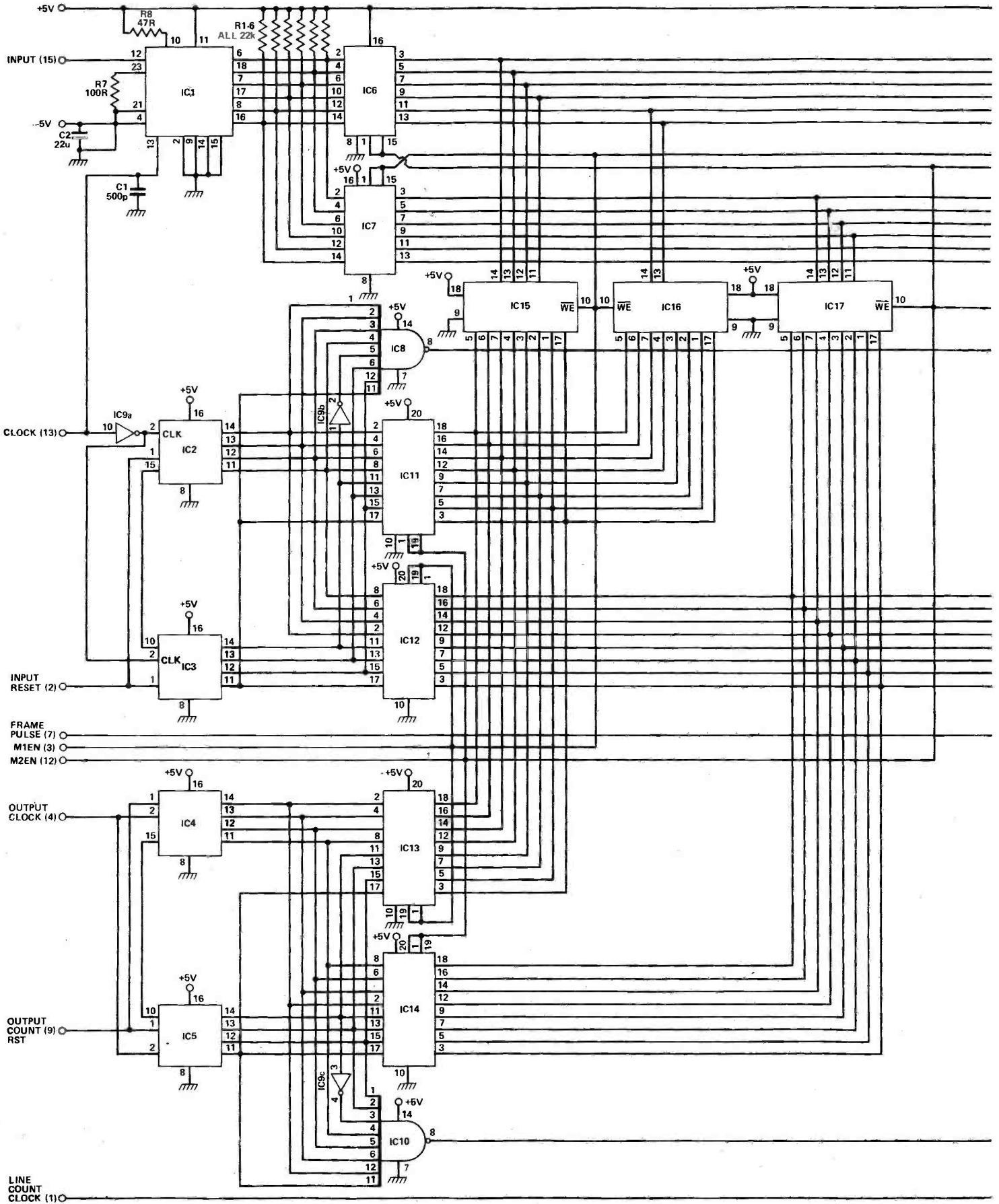
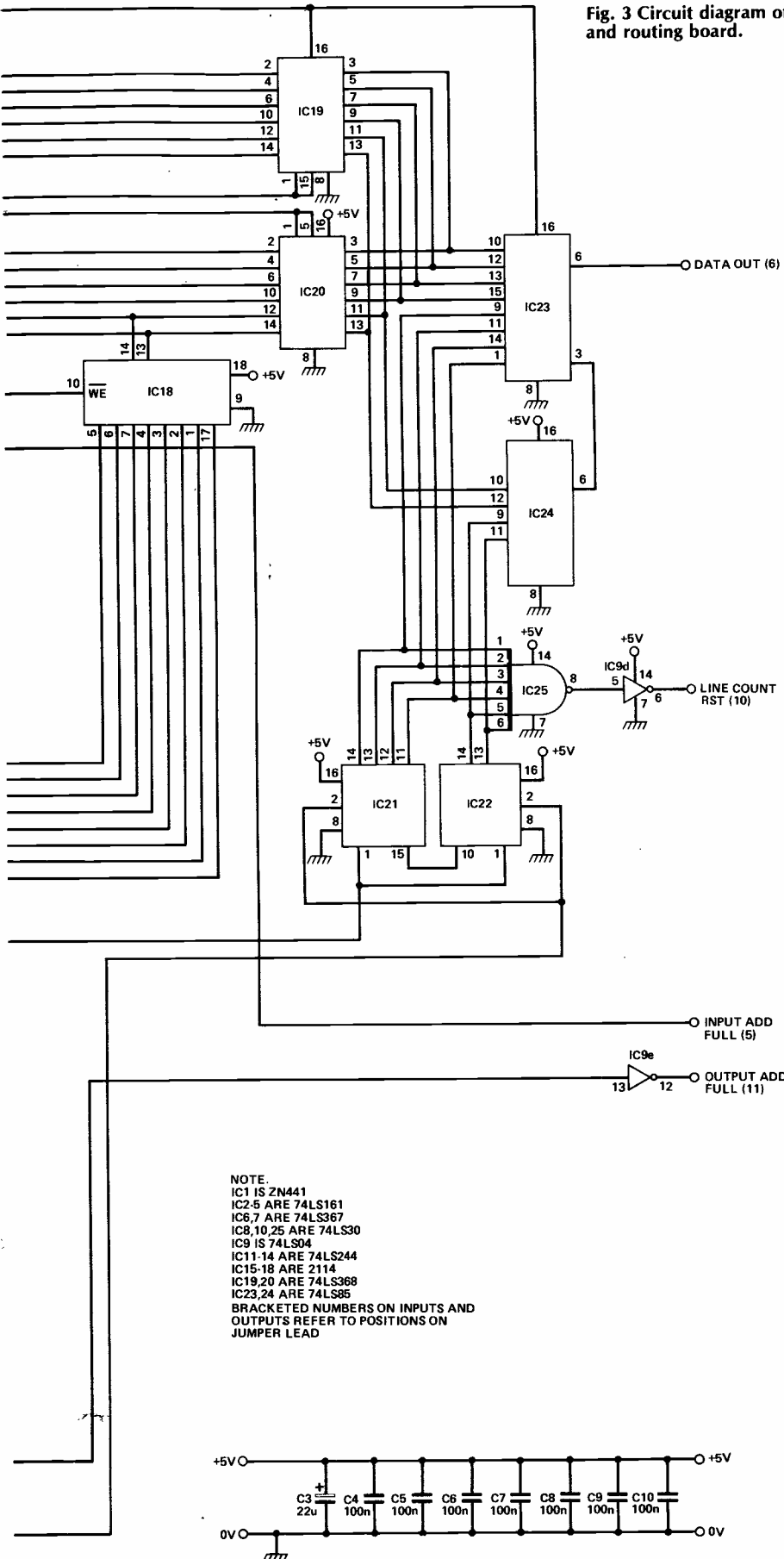


Fig. 3 Circuit diagram of the data storage and routing board.



NOTE:
 IC1 IS ZN441
 IC2-5 ARE 74LS161
 IC6,7 ARE 74LS367
 IC8,10,25 ARE 74LS30
 IC9 IS 74LS04
 IC11-14 ARE 74LS244
 IC15-18 ARE 2114
 IC19,20 ARE 74LS368
 IC23,24 ARE 74LS85
 BRACKETED NUMBERS ON INPUTS AND
 OUTPUTS REFER TO POSITIONS ON
 JUMPER LEAD

HOW IT WORKS

IC1 is the ZN441 A-to-D converter. This converts the analogue input signal into a six-bit binary word at rates up to 10 million samples a second. The six-bit word from each sample is then passed to the memory buffers IC6 and IC7. If IC6 and IC20 are selected, then data is written to the memory block IC15, 16. In this case IC19 and IC7 are in the high impedance output mode, and IC20 enables data from the second memory block, IC17, 18, to be read to the comparator IC23, 24. The memory and buffer enables also select the address buffers, routing the input addressing to IC15, 16, and the output addressing to IC17, 18 in this example. In other words, in this phase of the operation IC11 is allowing the synchronous counters IC2 and IC3, which are acting as an eight-bit address counter, to cycle IC15, 16 synchronously with the sample rate, while IC14 is allowing the output address counter IC4, 5 to address IC17, 18. IC12, 13 are disabled to block the respective unwanted address lines. On the alternate phase, ICs 11 and 14 would be disabled, ICs 12 and 13 would be enabled, and the two memory blocks IC15, 16 and IC17, 18 would receive the opposite sets of address signals. The output of IC8 goes low when the input address cycle is completed, while the output of IC10 goes low when the output address cycle is complete.

IC21, 22 form the 256-line counter, which is advanced every four video lines for a total of 64 steps. This six-bit output is compared with the six-bit output from the memory by IC23, 24, and when these are equal, a data bit is output to the video summing circuit. The output of IC25 goes low when a count of 256 is completed.

When the input cycle is complete (the input memory block is full), the input clock is disabled. The output clock is only enabled for 256 lines of the scan and is therefore disabled during the first and last lines of the display and the frame flyback time. When the input address is completed and the frame scan is completed, the memories are switched over and the new data is output to the comparator. The video data is therefore refreshed every 50 mS unless the incoming data cycle is longer.

The power supply unit has regulated +5 V and -5 V rails at 650 mA and 160 mA respectively, with a separate 5V8 supply for the UHF modulator.

Oops

A couple of errors crept into the first part: IC6a pin 3 is connected to IC7 pin 12, etc, and not as shown; the supply line decoupling capacitors were not shown, and they are C15 (22u tant) and C16-24 (100n ceramic) on the +5 V line and C16 (22u tant) on the -5 V line. Additionally, R14 has now been omitted. (Note that all the above component numbering refers to the logic board circuit diagram, published last month).

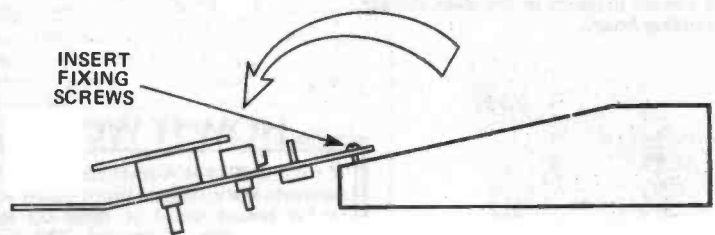


Fig. 4 This is how you attach the front panel to the box to make it easier to do the interconnecting

switch (see the overlay in Fig. 1). Incidentally, Q4 was incorrectly identified on the circuit diagram last month — it is actually a BC107.

The power supply is mounted on a single-sided PCB and is supplied ready-built with the kit. The front panel switches are also PCB-mounted as described earlier (see Figs. 2 and 6):

With the boards completed, the data processing board can be connected to the control logic

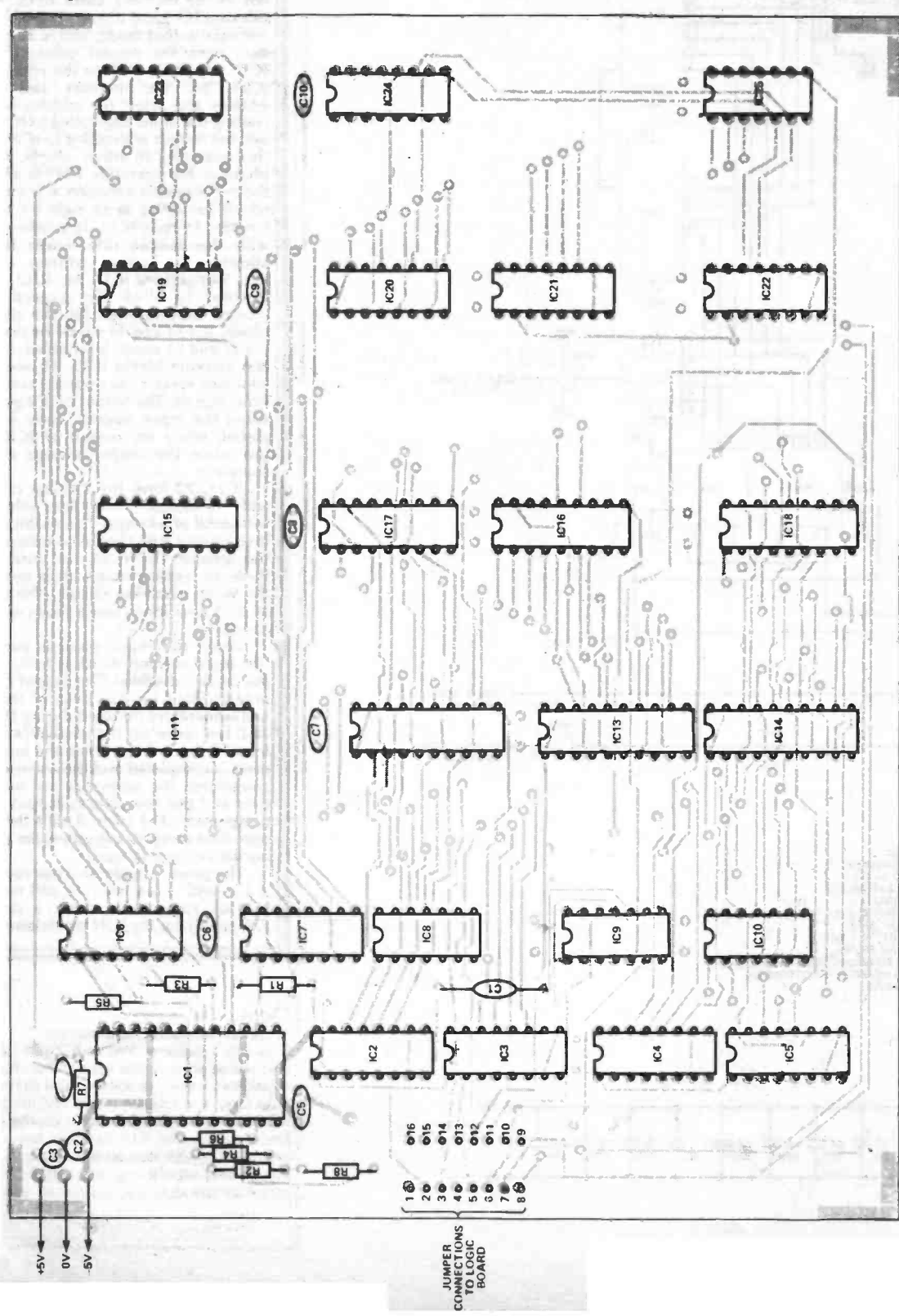
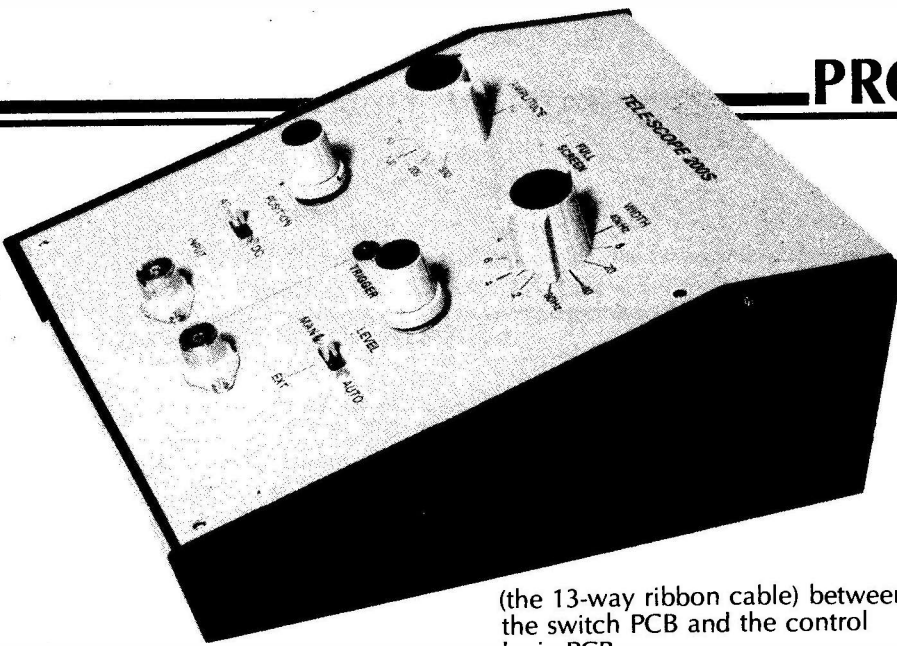


Fig. 5 Overlay of the data storage board



(the 13-way ribbon cable) between the switch PCB and the control logic PCB.

board using the 16-way jumper. The data processing board is then mounted on the base of the case with adhesive pillars, and the logic board is mounted on top of it, again using adhesive pillars. These special pillars are supplied with the kit and are required because there isn't enough space between tracks on either PCB to allow for fixing holes to be drilled. The power supply is fitted to the rear of the case, with the supply leads being soldered to the upper PCB. Don't forget to drill access holes in the rear of the case for the mains lead and UHF TV cable first, though!

Now mount the controls on the lid of the case. The lid should be screwed face down in the open position, using one pair of holes only, in order to make the front panel wiring easier. Figure 4 makes this clear.

First the input lines should be connected to the AC/DC input switch with C1 mounted directly across the switch terminals. Next wire the trigger switch (see Fig. 6) and the trigger LED, and finally connect the frequency selector lead

Operation

First switch on your television and tune in the Tele-Scope signal on an unused channel select button. Set the trigger switch to auto and locate the trace (a white line) using the position control. Set the voltage control to 10 V full screen and the full screen width control (the time base) to 80 Hz FSW. On touching the input socket with your finger, a 50 Hz sine wave will be displayed (due to mains pick-up).

By switching to manual trigger and adjusting the trigger level, it is possible to remove your finger and keep the sine wave display on the screen. This feature of the Tele-Scope allows you to do some interesting experiments — for instance, you can examine the EMF induced in a coil when a bar magnet is dropped through it.

Try using the Tele-Scope as a sampling scope on repetitive waveforms above 250 kHz (not calibrated, but it works). You can even capture one-shot events up to 250 kHz.

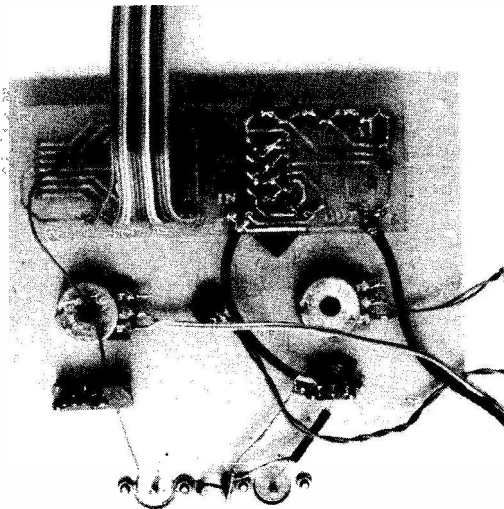


Fig. 6 Wiring the back of the front panel.

THE ZN441

The ZN441 is an ultra-high-speed parallel (flash) A-to-D converter comprising an array of 64 strobed comparators and encoding logic. A reference voltage applied across a tapped resistor chain defines 63 quantisation levels plus overrange and underrange, one input of each comparator being connected to the resistor string, while the other inputs are commoned and connected to the analogue input. When an analogue input is applied, all the comparators whose reference voltage is less than the analogue input will change state, ie if the input voltage is $V_{REF} \cdot n/64$ then n comparators will have tripped. The comparator outputs are decoded into a 1-of-64 format by NOR gates and then re-encoded into binary by a high-speed ROM.

Two or four ZN441s can be stacked to give a seven- or eight-bit converter with a minimum of external components. Applications include high-speed data acquisition, video an radar data conversion, digital signal storage and image processing.

PARTS LIST — DATA BOARD

Resistors (all $\frac{1}{4}W$, 5%)

R1-6 2k2
R7 100R

Capacitors

C1, 2 22uF 16 V PCB electrolytic
C3-9 100nF ceramic

Semiconductors

IC1 ZN441
IC2-5, 21, 22 74LS161
IC6, 7 74LS367
IC8, 10, 25 74LS30
IC9 74LS04
IC11-14 74LS244
IC15-18 2114
IC19, 20 74LS368
IC23, 24 74LS85

Miscellaneous

PCB (see Buylines); 24 pin IC socket for IC1.

ETI

BUYLINES

Hawk Electronics Test Equipment supply a full kit of parts for this project. All PCBs, the case (drilled and screen-printed), the ZN441 and all the other components are included, together with a comprehensive manual. The kit price is £89. The 'Tele-Scope' is also available built and tested for £109.

The manual may be purchased separately for £1.50 (no VAT required) refunded on the subsequent purchase of a kit or finished circuit.

Prices exclude 15% VAT, and postage and packing is £2.95 extra. The case, A-to-D converter, and the PCBs may all be purchased separately.

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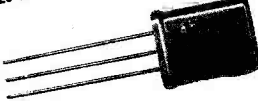
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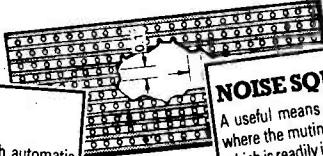
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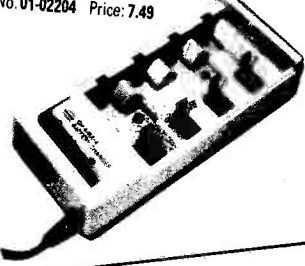
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IC UPDATE

Dear Reader,

What we've indulged in here is a slightly speculative venture, in that neither of the two ICs featured this month are actually available to the hobbyist, so far as we know (if you're in industry, then you'll be able to get the LM2877/8 from your Nat Semi supplier, and the RC4193 from Raytheon). However, we think that by bringing these to the light of day, we shall motivate someone, somewhere to stock them. And far be it from us to suggest our advertisers, but a word in their ear from you may not go amiss . . .

RC4193 Switched Mode PSU

What, not another switched mode PSU? Well, yes, but this one can keep your tranny going for longer, amongst many other applications.

The RC4193 is a monolithic switching regulator IC that, with very few external components is capable of stepping up or down, or inverting, with a typical efficiency of 80%.

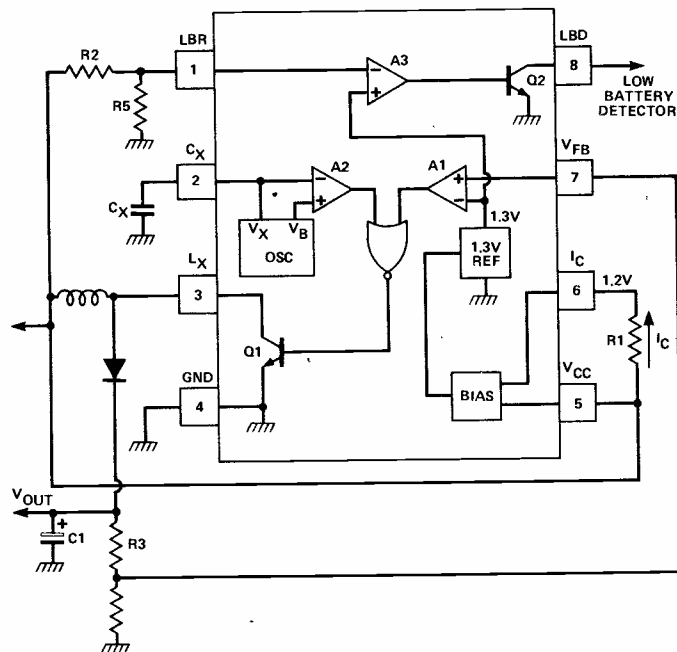


Fig. 1 RC4193 functional diagram.

Principles of Operation

The circuit has an on chip 1.31 V band gap reference with a typical TC of 50ppm. In addition to setting the bias currents in the 4193, this voltage is used as the reference at the input of comparators A1 and A3. The 1.31 V at the input of A1 is used as the threshold to compare to the feedback output voltage at pin 7 (V_{FB}). The output of A1 is fed to a NOR gate which is used to gate the output of the oscillator comparator (A2) which turns off Q1 whenever

V_{FB} is greater than 1.31V. Note when the output of A1 of A2 is high the switch transistor Q1 cannot turn on.

The oscillator has its frequency determined by a single capacitor C_x and outputs two waveforms, a square wave V_b and a saw tooth V_x (which appears at pin 2) both of which appear at the input of A2. The portions of the waveform where Q1 can be saturated as a result of the oscillator, are labelled T_c in Fig. 2, and the portion of the waveform where Q1 would be off is labelled T_o . Q1 can

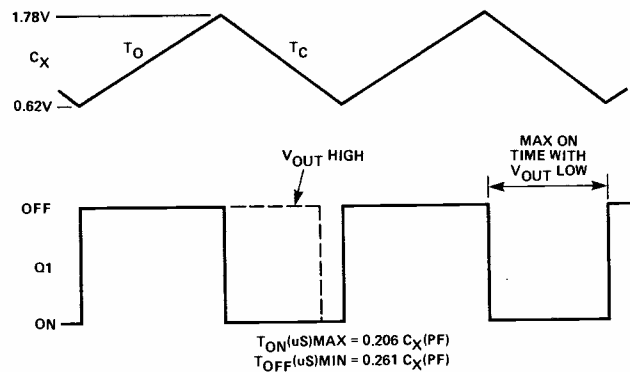


Fig. 2 Switching timing diagram.

be saturated only when V_{FB} is less than 1.31V. The voltage of the sense line from the R3/R4 voltage divider at the V_{FB} pin is directly proportional to the output voltage V_{OUT} , where $V_{OUT} = 1.31 (R3 + R4)/R4$. When V_{FB} is less than 1.31V, Q1 will saturate on every negative going oscillator cycle until V_{OUT} reaches the programmed value.

The 4193 also includes an uncommitted comparator and output transistor shown as A3 and Q2 in Fig. 1. The 1.31V internal reference is used as the threshold at the + input of A3. The voltage divider R2/R5 is used to determine the voltage at which Q2 switches. When the voltage at LBR (pin 1) falls below 1.31V then Q2 will saturate. A3 has about 0.7 μ A of hysteresis to produce a positive turn on/turn off at LBD (pin 8). The voltage at which Q2 switches is determined by $V = 1.31 (R2 + R5)/R5$.

Absolute Maximum Ratings

Internal Power Dissipation	500mW
Supply Voltage (without external series pass transistor)	24V
Operating Temperature Range	0°C to +70°C
Switch Current (I _{sw})	150mA
Reference Set Current (I _c)	1mA
V _{FB} , LBR, C _v Voltage	
L _v , LBD Voltage	24V

ed with any input between 9.3V and 2.4V.

If a lower supply voltage can be tolerated, the output of the 4193 can be set to start regulating at 7V (1.16V/Cell), effectively keeping the 4193 in its quiescent state (drawing only 150μA) until the battery voltage falls to 7.5V. Below 7.5V the 4193 will regulate the V_{OUT} at 7.0V until the battery falls below 2.4V. In this circuit R2 and R5 are used to indicate a low battery condition when the input voltage falls below 5.9V; any other voltage can be selected by changing the value of R2. If the Low Battery Detector circuitry is not going to be used, leave pin 1 and 8 unconnected. As mentioned previously, the top of R5 can also be connected to V_{OUT} when a low output indication is

PARAMETERS	CONDITIONS	MIN	TYP	MAX	UNITS
Supply Voltage, V _{CC}		2.4		24	V
Reference Voltage (internal), V _{REF}		1.24	1.31	1.38	V
Switch Current, I _{sw}	V ₃ = 400mV	75	100		mA
Quiescent Current, I _{CC}	Measure at Pin 5 I ₃ = 0		135	200	μA
Efficiency			80		%
Line Regulation	0.5V _O < V _{CC} < V _O		0.08	0.5	% V _{OUT}
Load Regulation	V _{CC} = 0.5V _O P _I = 150mW		0.2	0.5	% V _{OUT}
Operating Frequency, f _o		0.1	25	150	kHz
Reference Set Current, I _c		1	5	50	μA
Switch Voltage	I ₃ = 100mA		0.4	1	V
Switch Leakage Current	V ₃ = 24V		0.01	5	μA
Supply Current (Disabled)	I _c < 0.01μA		0.1	5	μA
Low Battery Bias Current	V ₁ = 1.2V		0.7		μA
Capacitor Charging Current			5.0		μA
Capacitor Threshold Voltage +			1.78		V
Capacitor Threshold Voltage -			0.62		V
Feedback Input Current	V ₇ = 1.3V		0.1		μA
Low Battery Output Current	V ₈ = 0.4V, V ₁ = 1.1V	100	600		μA

Table 1 Electrical characteristics

The 4193 series circuits contain an internal bias network which maintains the correct operating currents to the 4193 independent of temperature and input voltage variations. The internal bias network is turned on by supplying a current I_c between 1μA and 100μA into pin 1, and no change will result in the operating characteristics when I_c is varied over this range. To shut down the 4193, simply force pin 1 to less than 0.5V by using a mechanical switch or open collector transistor. The quiescent current in the 4193 will fall to less than 5μA (typically less than 0.1μA).

Design Equations

Table 2 is a set of design equations which can be used to determine resistor, capacitor and inductor values for step-down, step-up and voltage inverting applications. To use the equations, you determine the oscillator frequency (f_o), input voltage (V_{IN}), output voltage (V_{OUT}) and maximum output load current (I_L).

Basic Step-Up Switching Regulator

Figure 5 is the basic low current step-up configuration to be used for most battery powered applications requiring less than 150mW of load power (when V_{IN} > 0.5 V_{OUT}).

The output voltage V_{OUT} is determined by the expression 1.31 (R3 - R4)/R4; in this case V_{OUT} would be 9.0V. This configuration makes a good substitute for a 9V transistor battery, since a stable output voltage will be achieved

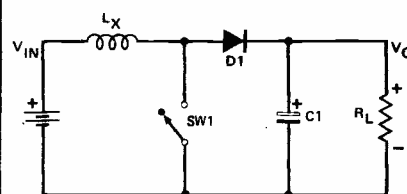


Fig. 3 Basic circuit for stepping up mode.

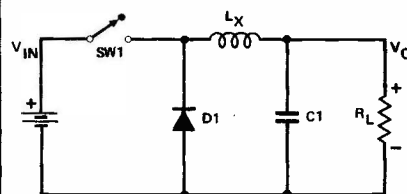


Fig. 4 Basic stepping down circuit.

	Step Up	Step Down	Inverting
R1(M)	$\frac{V_{IN} - 1.2}{5\mu A}$	$\frac{V_{IN} - 1.2}{5\mu A}$	$\frac{V_{IN} - 1.2}{5\mu A}$
R2(M)	$\frac{V_{IN} - 1.31}{5\mu A}$	$\frac{V_{IN} - 1.31}{5\mu A}$	$\frac{V_{IN} - 1.31}{5\mu A}$
R3*	$\frac{V_{OUT} - 1.31}{I_1}$	$\frac{V_{OUT} - 1.31}{I_1}$	$\frac{V_{OUT}}{I_1}$
R4*	$\frac{1.31}{I_1}$	$\frac{1.31}{I_1}$	$\frac{1.31}{I_1}$
R5	261kΩ	261kΩ	261kΩ
C _x (pF)	$\frac{2.14 \times 10^6}{f_o}$	$\frac{2.14 \times 10^6}{f_o}$	$\frac{2.14 \times 10^6}{f_o}$
L _x	$\frac{0.3V_8(V_{OUT} - V_{IN})}{f_o I_{LOAD} V_{IN}}$	$\frac{0.3V_{OUT}}{f_o I_{LOAD}}$	$\frac{0.3V_{IN} V_{OUT} }{f_o I_{LOAD}(V_{IN} + V_{OUT})}$
Cl	$\frac{2V_{OUT} - V_{IN}}{4f_o V_{OUT} V_R}$	$\frac{I_{LOAD}}{4f_o V_R}$	$\frac{0.15I_{LOAD}N + 2 V_{OUT} }{f_o V_{IN}(V_{IN} + V_{OUT})V_R}$
R6	$\frac{35V_{IN}}{I_{LOAD}V_{OUT}}$	$\frac{35}{I_{LOAD}}$	$\frac{35V}{I_{LOAD}(V_{IN} + V_{OUT})}$
R7	$\frac{R6}{7}$	$\frac{R6}{7}$	$\frac{R6}{7}$

Units are ohms, farads, henries, and hertz unless indicated otherwise.
I₁ = current into pin 1; recommended value 100μA.

Table 2 Design equations for the three modes.

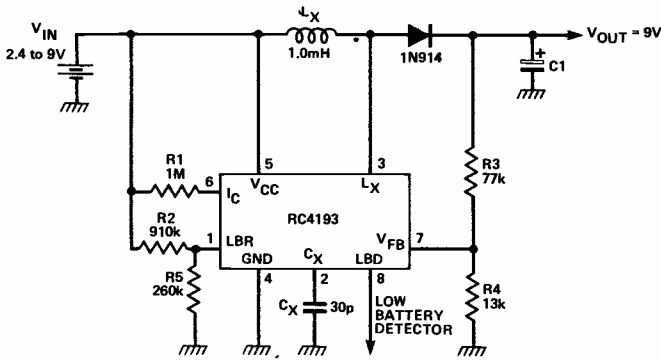


Fig. 5 RC4193 low current step-up mode.

desired.

A feature of the 4193 is the ability to shut off when pin 6 is forced below 0.5V. An example of this feature is shown in Fig. 6. In this circuit as long as V_c remains low the output will regulate to 5V. This type of circuit can be used to back up the main supply voltage when line interruptions occur, a particularly useful feature when using volatile memory systems.

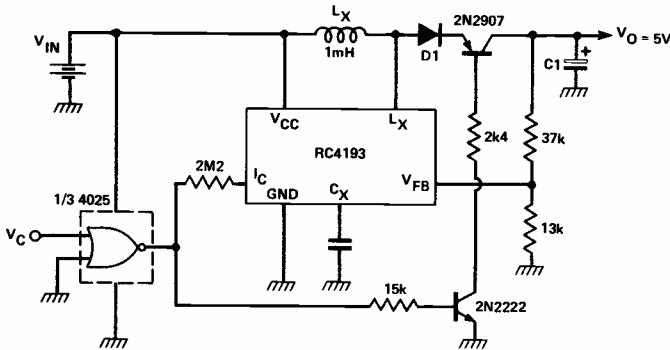


Fig. 6 RC4193 battery-back-up circuit.

In step-up application, power to the 4193 can be derived from the output voltage by connecting the V_{CC} pin and the top of R_1 to the output voltage (for example see Fig. 7). One requirement is that the battery voltage must be greater than 3.0V when the circuit is energized or else there is not enough voltage at the V_{CC} pin to operate the 4193. However, once running, the battery can decay to 1.0V before the circuit stops operating.

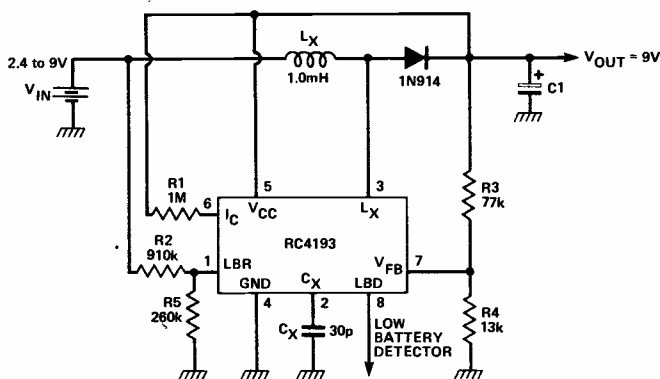


Fig. 7 Bootstrapping the supply to the RC4193.

Basic Step-Down Switching Regulator

Since the switch transistor in the 4193 is in parallel with the load a method must be used to convert it to a series connection; the circuit of Fig. 8 accomplishes this.

The 2N2907 replaces S1 of Figure 4, and R_6 and R_7 are added to provide the base drive to the 2N2907 in the correct polarity to operate the circuit properly; refer to Table 2 for equations for component values. Since the L_X pin is capable of sinking 100mA, high current switching transistors can be used in place of the 2N2907.

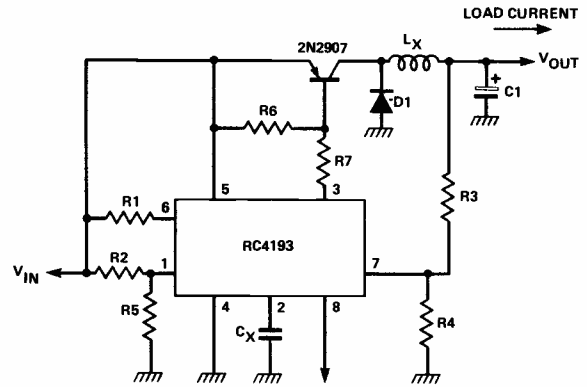


Fig. 8. RC4193 step-down mode.

Greater Than 30 Volt Application

Adding a zener diode in series with the base of the 2N2907 allows the input voltage to increase by the value of the zener, with only a slight decrease in efficiency. As an example, if a 24V zener is used, the maximum input voltage can go to 48V.

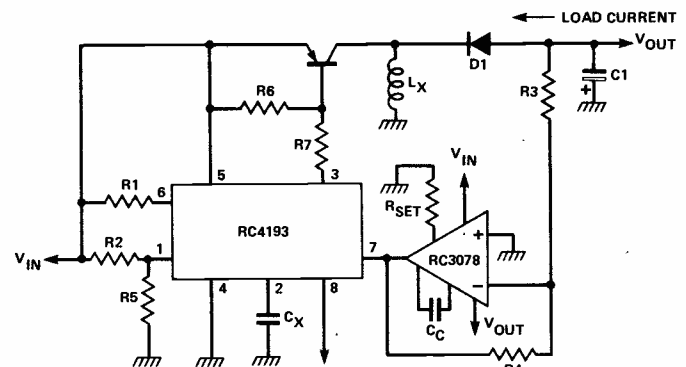


Fig. 9 RC4193 used as an inverter-regulator.

Inverting Switching Regulator

Many single-supply systems require an occasional negative voltage for a specific application; this circuit will meet those needs.

The circuit is similar to the type used in Fig. 8, except the location of L_X and the diode are reversed and a micropower op-amp RC3078 is added to provide inversion for the sense voltage. The output voltage is $1.31 R_3/R_4$.

The RC3078 operates at a closed-loop gain of close to one in most applications, therefore the value of C_c must be such to frequency compensate the RC3078 for unity gain conditions. The value for R_{SET} will determine the quiescent current in the 3078 and for micropower applications can be set to operate at approximately $10\mu A$. Where a larger amount of amplifier quiescent current can be tolerated, a ground sensing op-amp such as the LM324 or RC3403A can be used, eliminating the need for R_{SET} and C_c .

An important point is that pin 7 must be below 1.3V when $|V_{OUT}|$ is below the design output voltage or else the circuit will not start.

Due to their output stage design, op-amp types similar in design to the 741 may cause the circuit to not start properly since they fail to keep pin 7 below 1.3V when power is first applied.

LM2877/8 Audio Power Amps

The LM379 has had a good innings as linear ICs go, but it's now being replaced by the LM2877 and LM2878 in manufactured equipment.

The LM2877/8 are monolithic dual power amplifiers designed to deliver 4W (2877) or 5W (2878) continuous into eight ohm loads. Each power amplifier is biased from a common internal regulator to provide good power supply rejection and output centering. Both devices are internally compensated for gains greater than 10 and come in 11-lead single in-line packages.

Absolute maximum ratings

Supply voltage	26 V (35 V 2878)
Input voltage	+0.7 V
Operating temperature	0°C to +70°C
Junction temperature	150°C

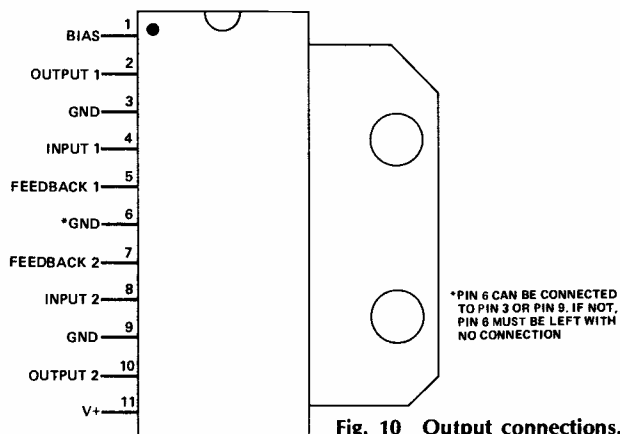


Fig. 10 Output connections.

Electrical Characteristics for LM2877: Where those of the LM2278 differ, they are given in brackets; otherwise the same figure applies.

$V_S = 20V$ (22V), $T_{TAB} = 25^\circ C$, $R_L = 8\Omega$, $A_v = 50$ (34 dB) unless otherwise specified

Note 1: For operation at ambient temperatures greater than 25°C, the LM2877 must be derated on a maximum 150°C junction temperature using a thermal resistance which depends upon device mounting techniques.

PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
Total Supply Current	$P_O = 0W$		25(10)	50	mA
Operating Supply Voltage		6		24(35)	V
Output Power/Channel	$f = 1 \text{ kHz}$, THD = 10%, $T_{TAB} = 25^\circ C$ $V_S = 20V$ $V_S = 12V$, $R_L = 4\Omega$	4.0(5.0)	4.5(5.5)		W
Distortion, THD	$f = 1 \text{ kHz}$, $V_S = 20V$ $P_O = 50 \text{ mW/Channel}$ $P_O = 2W/Channel$		0.1(0.2)		%
			0.07(0.14)	1	%
Output Swing	$R_L = 8\Omega$		$V_S - 4$ ($V_S - 6$)		Vp-p
Channel Separation	$C_F = 50 \mu F$, $C_{IN} = 0.1 \mu F$, $f = 1 \text{ kHz}$ Output Referred $V_S = 20V$, $V_O = 4 \text{ Vrms}$	-50	-70		dB
PSRR Power Supply Rejection Ratio	$C_F = 50 \mu F$, $C_{IN} = 0.1 \mu F$, $f = 120 \text{ Hz}$, Output Referred $V_S = 20V$, $V_{RIPPLE} = 1 \text{ Vrms}$	-50	-68(-60)		dB
Noise	Equivalent Input Noise $R_S = 0$, $C_{IN} = 0.1 \mu F$, BW = 20 Hz-20 kHz		2.5		μV
Open Loop Gain	$R_S = 0$, $f = 1 \text{ kHz}$, $R_L = 8\Omega$		70		dB
Input Offset Voltage			15		mV
Input Bias Current			50(100)		nA
Input Impedance	Open Loop		4		M Ω
DC Output Level	$V_S = 20V$ (22V)	9(10)	10(11)	11(12)	V
Slew Rate			2.0		V/ μs
Power Bandwidth			65		kHz
Current Limit			1.0(1.5)		A

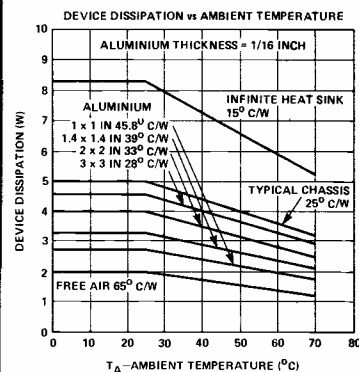


Fig. 11 Device dissipation vs. ambient temperature (LM2877).

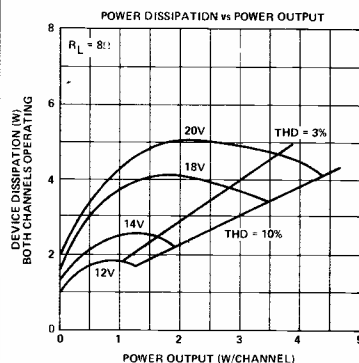


Fig. 12 Power dissipation vs. power output (LM2877).

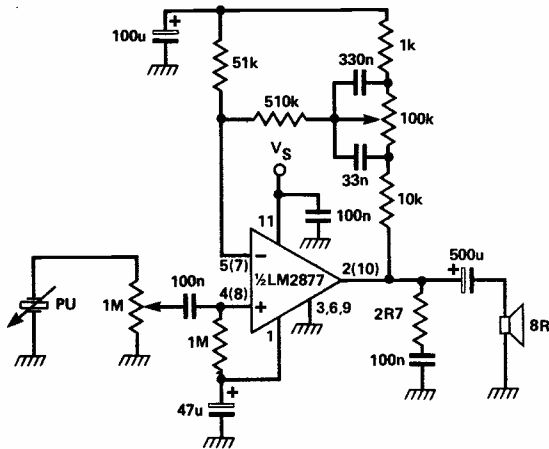


Fig. 13 Ceramic PU amplifier with bass control.

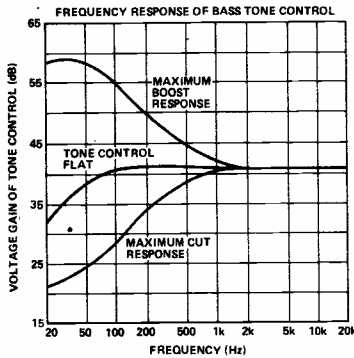


Fig. 14 Frequency response of bass control in Fig. 13.

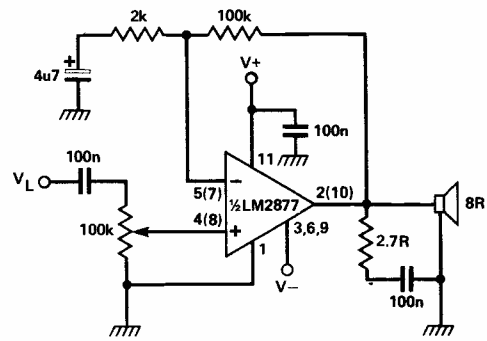


Fig. 15 Non-inverting amplifier using split supply.

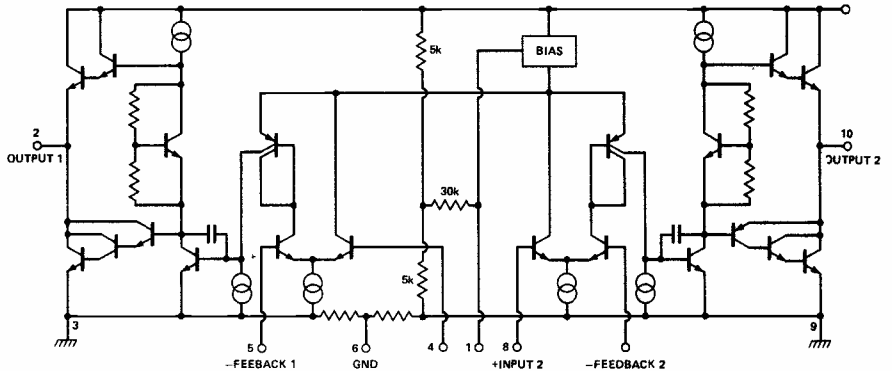
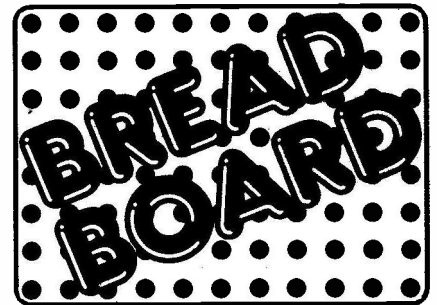


Fig. 16 Internal circuit.

Next month we'll take a look at a few more newcomer ICs.

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UNIVERSAL EPROM PROGRAMMER

Get to grips with the bits using our Universal EPROM programmer. Design and development by Mike Bedford.

EPROMs provide a convenient means of storing commonly used software, but many micro-computer users are deterred from using this media due to the difficulties of erasure and programming. EPROM programmers are both commercially available and have been featured as constructional articles in some magazines, but the former are relatively expensive and the latter tend to be limited as regards types of EPROM supported. For these reasons, it was considered appropriate to develop a universal EPROM programmer which could be built by the amateur for a modest sum. The programmer presented here will support the following EPROMs: 2758, 2716, 2516, 2732, 2732A, 2532, 2764, 2564, 27128 and 27256. This list includes every single supply version of the 27-Series and 25-Series devices up to and including 256k bit capacity, which seems likely to be the largest EPROM which will be produced as further development will probably be of EAROMs and EEPROMs. The programmer is intended for use in conjunction with a 6502 computer system and appropriate software is presented. Although the hardware is designed to support the 27256, this one EPROM is not as yet supported by the software due to lack of preliminary data on this device, the chip itself having not been released by the manufacturer at the time of writing. To complete the requirements for programming EPROMs, some hints are given on building an erasure unit.

Hardware

The hardware has been designed for a Tangerine Microtan system, the physical dimensions of the circuit board being selected such that it will plug directly into the system rack. Non-Tangerine users should not be deterred,

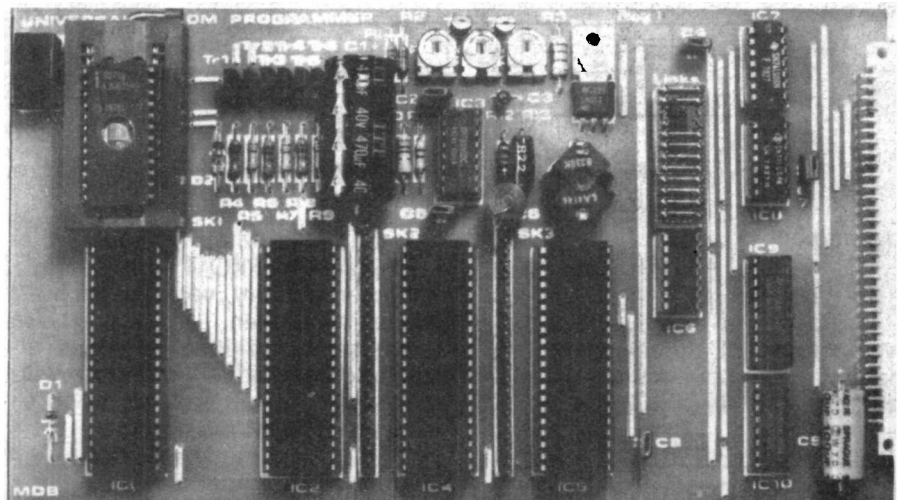
however, as electronically it should be quite simple to interface this card to any computer using the 6502 or 6809 processors. No special power supplies are required as all voltages required for programming are derived from a single +5v supply.

Although the PCB has sufficient space for a zero insertion force socket to be mounted on board, it is probably more convenient, especially if the card is to be rack mounted, to mount this socket in a separate console, making a connection with a length of ribbon cable. Note that a switch should be provided on the console to isolate V_{pp} and V_{cc} on pins 1 and 28 respectively. This is necessary since inserting or removing an EPROM with these supplies present may result in its destruction.

If the console is not used, switch SW1 should be mounted on board to isolate these supplies. On EPROMs which have V_{pp} and V_{cc} on other pins, these supplies may be isolated under program control. It will also be noticed that only a single zero insertion force socket

has been provided on PCB. This decision was taken on grounds of economy and some constructors may prefer to add a 24-pin socket in addition. If a single 28-pin socket is used, 24-pin devices should be inserted into the bottom part of the socket, ie leaving pins 1, 2, 27 and 28 empty. Table 1 shows the pin outs of all EPROMs which are supported.

The programmer applies a TTL level to all pins with the exception of pin 1 which is connected to V_{pp} , pin 14 (0V) and pin 28 (+5v). V_{pp} is program selectable to +25 V, +21 V or +5 V and may also be applied to pins 22 and 23 as an alternative to a TTL level. To summarise this information, the programmer may be considered as a glorified 29-bit output port. This being the case, and since the circuitry required to implement the above would not completely fill a 8" x 4½" PCB, it seemed appropriate at the cost of only two more ICs to add four additional 8-bit output ports to make maximum use of the board space available. These ports are completely independent from the



The Universal EPROM Programmer. Note that this prototype differs slightly from the final version — in particular, the component numbering is completely different!

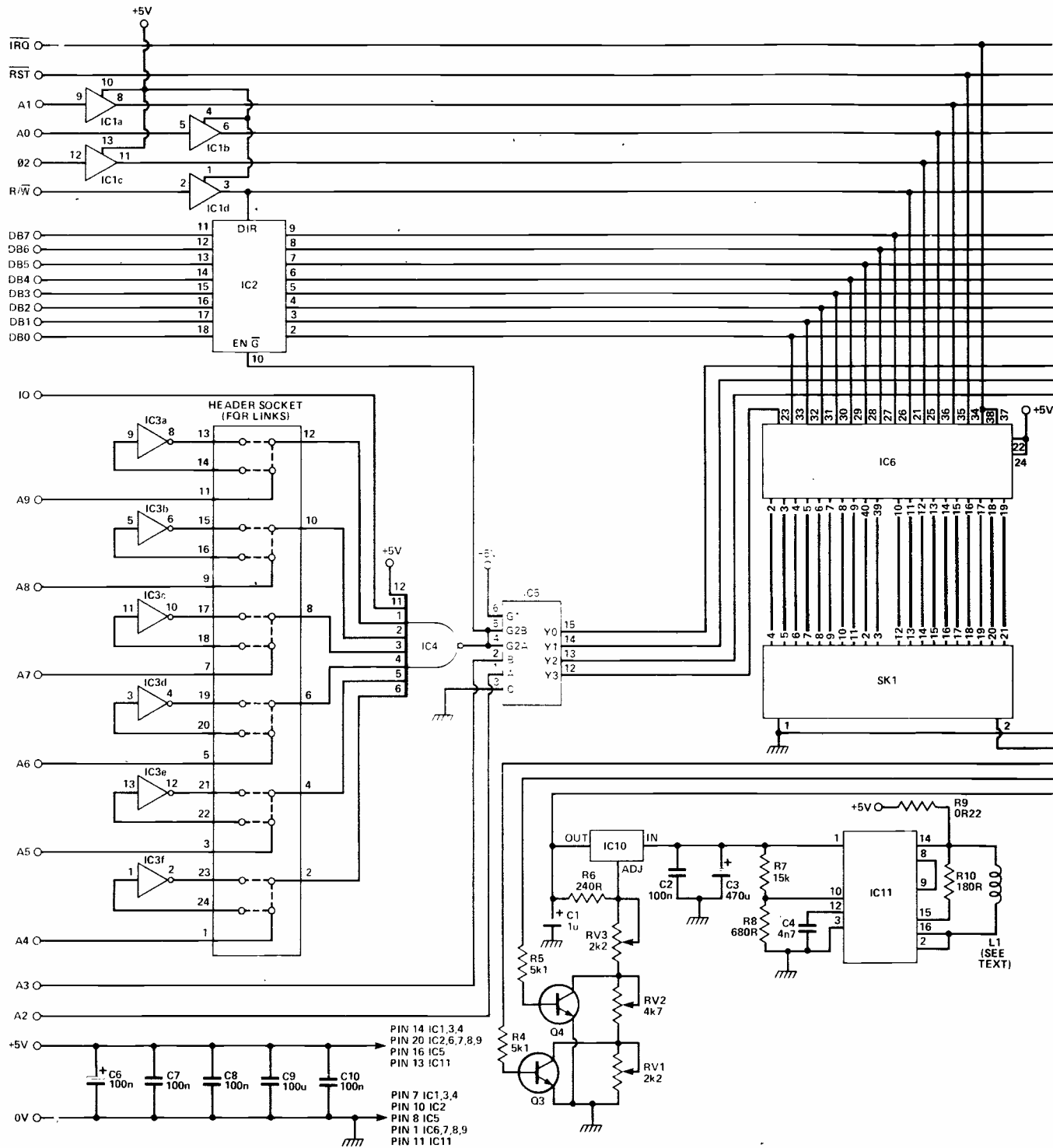


Fig. 1 Circuit diagram of the Universal EPROM Programmer.

programmer.

Software

In order to be a useful development tool, the following functions are the minimum requirements of an EPROM programmer:

1. Read data from an EPROM into computer memory;
2. Compare the contents of an EPROM with the contents of computer memory;

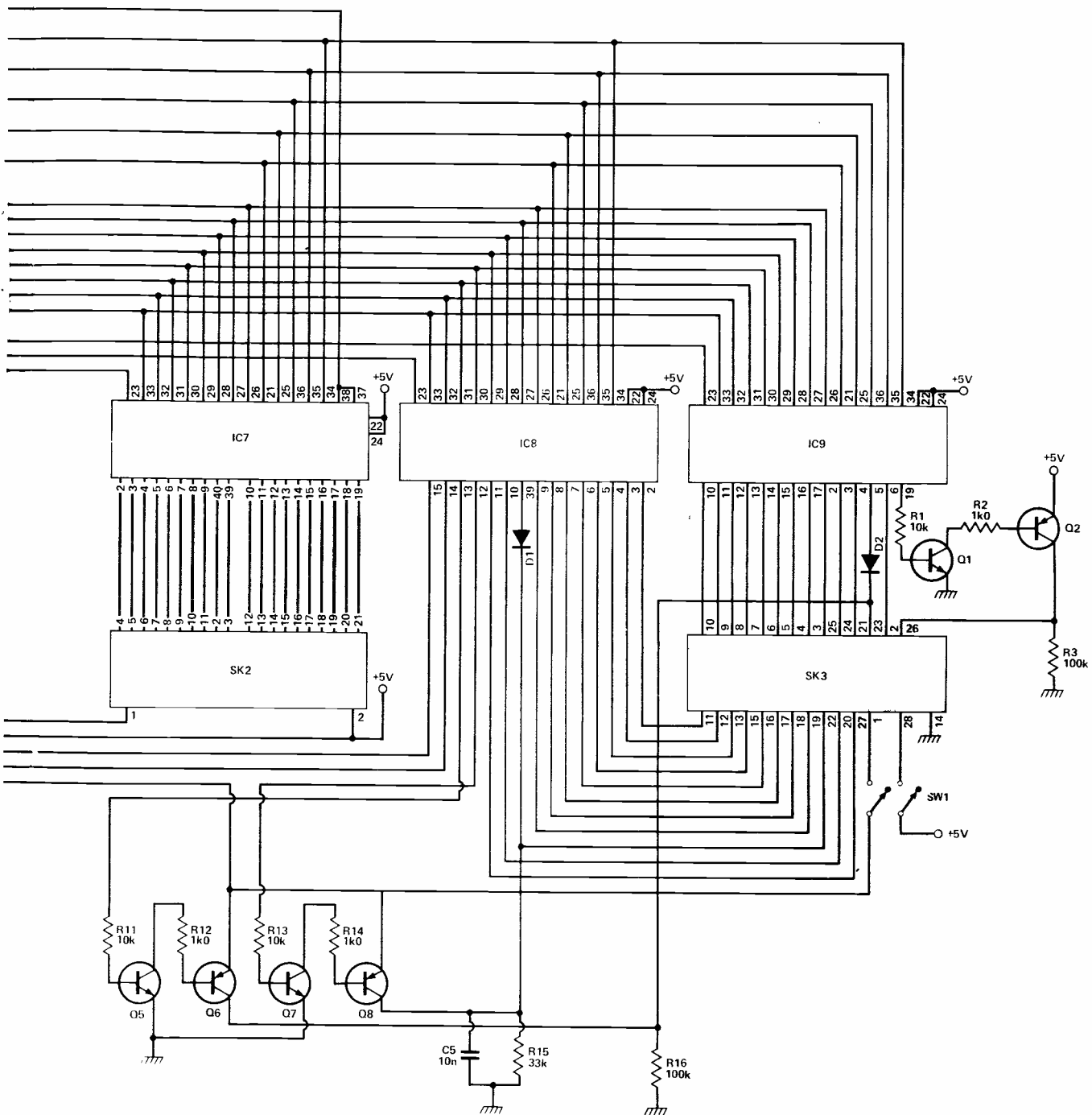
3. Test an EPROM for erasure;
4. Program an EPROM from data in computer memory, verifying each byte as it is written.

In fact, some additional functions have also been added and these will be described under the section on using the EPROM programmer.

Table 2 is a mode selection table for all supported devices, showing the read, program, verify and standby modes, these being the modes necessary to implement the

The design is based around four 6821 20-bit PIOs. The circuitry comprising IC3, IC4 and IC5 provides the interface to the Tangerine bus and, in conjunction with the links, allows the board to be configured to occupy a 16-byte block within the 1k I/O area. IC1 and IC2 are used to buffer various signals in order that no more than one TTL load is presented to any bussed input. Of the four 6821s, IC6 and IC7 provide the four independent I/O ports. These being connected to the outside world via SK1 and SK2, whereas IC8 and IC9 are used to drive the EPROM programmer. Most of the signals required to drive the pro-

PROJECT : EPROM Programmer



HOW IT WORKS

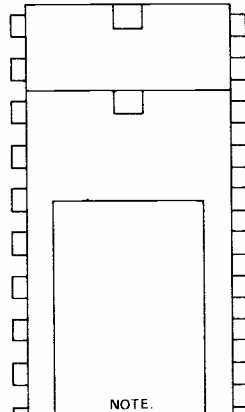
grammer are TTL levels and are taken directly from the two 6821s to the ZIF socket, SK3. Pin 26 on SK3 is slightly different in that although it is a pure TTL signal on all 28 pin devices, it is the V_{cc} supply on all EPROMs in 24-pin packages and hence requires a much greater current capacity than is available from a port on a 6821. Q1 and Q2 are therefore used to switch the +5 V supply to SK3 pin 26 under the control of IC9/CB2 (pin 19). A similar technique is used to switch V_{pp} onto SK3 pins 22 and 23 using transistor pairs Q5/Q6 and Q7/Q8 respectively. Since these two pins on SK3 are also required to present TTL

levels under different conditions, they are also connected to 6821 ports, isolating these signals by use of Germanium diodes D1 and D2 respectively.

It should be noted that when a 6821 is required to drive a transistor, a 'B' port is used, these having a greater current sourcing capacity than 'A' ports, and when a port needs to be isolated by a diode, an 'A' port is used as these give a full +5 V high signal so that, even allowing for the voltage drop across the diode, a good TTL high is presented. The V_{pp} supply is generated from the +5 V supply using IC11, a 78S40 switching regulator IC, in connection with timing

components L1 and C4. Although this component should be capable of regulating V_{pp} to within the required limits, experiments showed that it is advisable to select R7 and R8 such that IC11 would output about +30 V and use a separate LM317MP regulator to give the required voltage. Since V_{pp} may need to be +25 V, +21 V or +5 V, Q3 and Q4 are used, to switch out portions of the resistor chain between the regulator adjust terminal and 0 V hence altering the output voltage. These two transistors are connected to IC8 PB4 and PB5 (pins 14 and 15) hence allowing V_{pp} to be changed under program control.

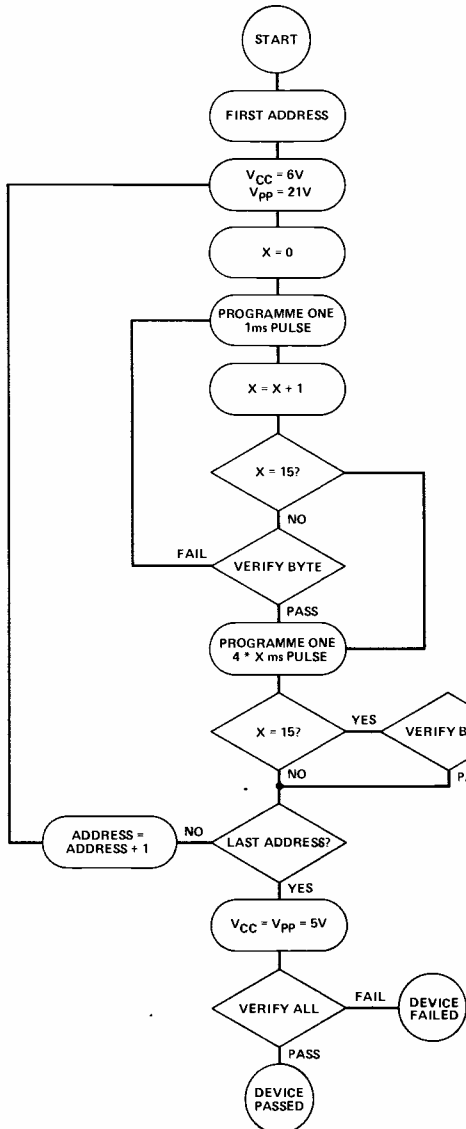
27 256	27 128	25 64	27 64	25 32	27 32/ 32A	27/ 25 16	27 58	IC/ PIN
VPP	VPP	VPP	VPP					/1
A12	A12	$\overline{CS1}$	A12					/2
A7	A7	A7	A7	A7	A7	A7	A7	1/3
A6	A6	A6	A6	A6	A6	A6	A6	2/4
A5	A5	A5	A5	A5	A5	A5	A5	3/5
A4	A4	A4	A4	A4	A4	A4	A4	4/6
A3	A3	A3	A3	A3	A3	A3	A3	5/7
A2	A2	A2	A2	A2	A2	A2	A2	6/8
A1	A1	A1	A1	A1	A1	A1	A1	7/9
A0	A0	A0	A0	A0	A0	A0	A0	8/10
D0	D0	D0	D0	D0	D0	D0	D0	9/11
D1	D1	D1	D1	D1	D1	D1	D1	10/12
D2	D2	D2	D2	D2	D2	D2	D2	11/13
GND	GND	GND	GND	GND	GND	GND	GND	12/14



NOTE:
 1) PIN NUMBERS TO 28 PIN PACKAGES. SUBTRACT 2 FROM PINS 3-26 FOR 24 PIN PACKAGE PIN NUMBERS.
 2) OE (27 SERIES) IS EQUIVALENT TO CS (25 SERIES).
 3) CE/PGM (27 SERIES) IS EQUIVALENT TO PD/PGM (NOT PD/PGM) (25 SERIES).

IC PIN	27 58	27/ 25 16	27/ 32 32A	25 32	27 64	25 64	27 128	27 256
/28					VCC	VCC	VCC	VCC
/27					\overline{PGM}	$\overline{CS2}$	\overline{PGM}	A14
24/26	VCC	VCC	VCC	VCC	N/C	N/C	A13	A13
23/25	A8	A8	A8	A8	A8	A8	A8	A8
22/24	A9	A9	A9	A9	A9	A9	A9	A9
21/23	VPP	VPP	A11	VPP	A11	A12	A11	A11
20/22	\overline{OE}	\overline{OE}	$\overline{OE}/$ VPP	PD/ PGM	\overline{OE}	PD/ PGM	\overline{OE}	\overline{OE}
19/21	AR	A10	A10	A10	A10	A10	A10	A10
18/20	$\overline{CE}/$ PGM	$\overline{CE}/$ PGM	\overline{CE}	A11	\overline{CE}	A11	\overline{CE}	\overline{CE}
17/19	D7	D7	D7	D7	D7	D7	D7	D7
16/18	D6	D6	D6	D6	D6	D6	D6	D6
15/17	D5	D5	D5	D5	D5	D5	D5	D5
14/16	D4	D4	D4	D4	D4	D4	D4	D4
13/15	D3	D3	D3	D3	D3	D3	D3	D3

Table 1 Pin-outs of all the EPROMs our programmer will process.



EPROM TYPE	FUNCTION	PIN	MODE				
			READ	STANDBY	PROGRAMME	VERIFY	
2758, 27/2516	*AR	19	VIL	VIL	VIL	VIL	
	$\overline{CE}/$ PGM	18	VIL	VIH	VIL → VIH	VIL	
	\overline{OE} VPP	20 21	VIL +5 V	X +5 V	VIH +25 V	VIL +25 V	
2732/32A	\overline{CE} $\overline{OE}/$ VPP	18 20	VIL VIL	VIH X	VIL **VPP	— —	
	2532	PD/PGM VPP	20 21	VIL +5 V	VIH +5 V	VIH → VIL +25 V	— —
2764, 27128	\overline{CE} \overline{OE} PGM VPP	20 22 27 1	VIL VIL VIH +5 V	VIH X X +5 V	VIL X VIH → VIL +21 V	VIL VIL VIH +21 V	
	2564	PD/PGM $\overline{CS1}$ $\overline{CS2}$ VPP	22 21 27 1	VIL VIL VIL +5 V	VIH X X +5 V	VIH → VIL VIL VIL +25 V	— — — —

NOTES:
 X = DON'T CARE
 * AR IS ONLY ON THE 2758
 ** VPP IS +25 V ON THE 2732, +21 V ON THE 2732A

Table 2 (above) Mode selection table.

Fig. 2 (left) Flowchart for intelligent programming mode.

functions mentioned. It may be noticed that some devices can perform both read and verify. Functionally, these modes are the same but verify is carried out with V_{pp} high, hence simplifying the program/verify process. From this table it may be seen that there is a great deal in common between the various EPROMs, hence simplifying the design of software.

PROJECT : EPROM Programmer

To get the full picture, the timing diagrams of each device should be scrutinised, but for the general user this information is probably not relevant. To summarise, however, EPROMs generally require about 50 ms to program each byte giving total programming times of from around 50 seconds for a 2758 to 13 minutes for a 27256. You may consider these times rather long, especially for the larger devices and although not implemented in the software presented here, there is an alternative programming method referred to as the *intelligent programming mode* which can reduce programming times by a factor of six for the 2764, 27128 and 27256. Figure 2 is a flow diagram of the functions which need to be performed in order to implement this method of programming. Notice that V_{cc} needs to be increased to +6V for this process to

be carried out and that there is no provision in the hardware to select this value of V_{cc} under program control. This need present no great problem, however, to the user wishing to implement this mode, as +6v may be switchable from the programming console, perhaps by deriving this voltage from the system +12v supply.

Any additions to, or modifications of the software will need to be made in the light of the information presented in Tables 3 and 4. These may be described as a programmer's view of the EPROM programmer, Table 3 showing the address of each register and Table 4 indicating which bits of the various 6821 ports connect to which EPROM pins or perform the various control functions required.

Construction And Alignment

Although the circuit of the programmer is of sufficient complexity that if it were to be produced commercially it would probably be double sided, it is not so complex that a single sided board would be impossible to design. It was considered that cost would be of prime importance to an amateur building a one-off project, and on these grounds it was artworked as a single-sided board. As a result of this, a number of insulated wire links need to be inserted prior to fitting the components. No special instructions are required on the fitting of components with the exception of socket SK3 and switch SW1. If a separate programming console is to be used, then an ordinary low profile DIL socket should be used as SK3, and two wire links should

Table 3 Register addresses.

FUNCTION	6821 NUMBER	REGISTER	OFFSET FROM BASE
	IC9	DDRA/ORA	00
	IC9	CRA	01
REGISTERS	IC9	DDRB/ORB	02
FOR	IC9	CRB	03
EPROM	IC8	DDRA/ORA	04
PROGRAMMER	IC8	CRA	05
	IC8	DDRB/ORB	06
	IC8	CRB	07
	IC7	DDRA/DRA	08
REGISTERS	IC7	CRA	09
FOR	IC7	DDRB/ORB	10
GENERAL	IC7	CRB	11
PURPOSE	IC6	DDRA/ORA	12
I/O	IC6	CRA	13
PORTS	IC6	DDRB/ORB	14
	IC6	CRB	15

Table 4 Port functions.

6821 NUMBER/PORT	SK3 PIN NO.	PROGRAMMER FUNCTION
IC9/PB0	10	A0
IC9/PB1	9	A1
IC9/PB2	8	A2
IC9/PB3	7	A3
IC9/PB4	6	A4
IC9/PB5	5	A5
IC9/PB6	4	A6
IC9/PB7	3	A7
IC9/PA0	25	A8
IC9/PA1	24	A9
IC9/PA2	21	A10 (EXCEPT 2758), AR (2758)
IC9/PA3	23	A11 (2732/32A/64/128/256), A12 (2564)
IC9/PA4	2	A12 (2764/128/256), $\overline{CS1}$ (2564)
IC9/CB2	26	A13 (27128/256), VCC (2758/16/32/32A, 2516/32)
IC8/PA0	11	D0
IC8/PA1	12	D1
IC8/PA2	13	D2
IC8/PA3	15	D3
IC8/PA4	16	D4
IC8/PA5	17	D5
IC8/PA6	18	D6
IC8/PA7	19	D7
IC8/CA2	22	\overline{OE} (2758/16/38/32A/64/128/256, 2516), PD/ \overline{PGM} (2532/64)
IC8/PB0	20	A11 (2532/64), $\overline{CE}/\overline{PGM}$ (2758/16, 2516), \overline{CE} (REMAINDER)
IC8/PB1	27	\overline{PGM} (2764/128), $\overline{CS2}$ (2564), A14 (27256)
IC8/PB2	22	VPP (2732/32A)
IC8/PB3	23	VPP (2758/16, 2516/32)
IC8/PB4	—	VPP + 5V SELECT*
IC8/PB5	—	VPP + 21V SELECT*

*NOT (VPP + 5) AND NOT (VPP + 21V) = + 25V SELECT

replace SW1. On the other hand, if the programmer is intended to be self contained on a single board, a zero insertion force DIL socket should be used as SK3 and switch SW1 is needed. Once the construction is complete, the links need to be configured to place the board at the desired address. The offset from the start of the I/O area is 16 times the binary number represented by the links. The best way to illustrate exactly how the links are used is probably graphically; Fig. 3 shows a few examples.

The other part of the circuit which requires setting up is associated with V_{pp} generation. This is very important as EPROMs will be destroyed if V_{pp} is more than 0V5 too high. The best way to check this

is with a voltmeter probe on the output of IC2, with IC8 removed from its socket. Apply +5 V to pin 14 of the IC8 socket and adjust RV3 until +5 V is recorded on the test meter. Now replace +5 V on pin 14 by +5 V on pin 13 of IC8 socket and adjust RV2 for +21 V on the meter. Finally, remove +5 V from pin 13 of IC8 socket and adjust RV1 for a potential of +25 V at IC2 output. Setting up is now complete.

Using The Programmer

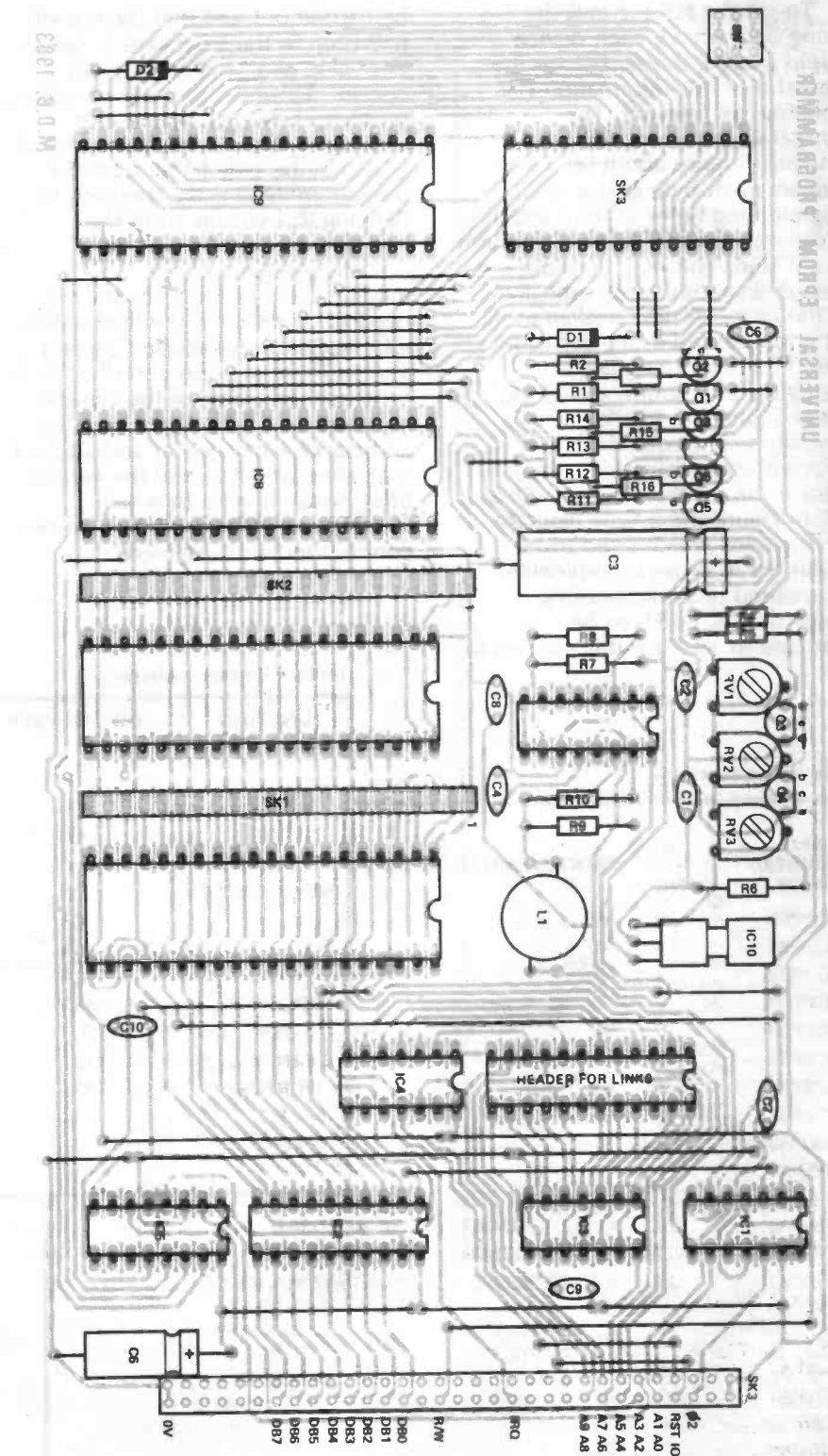
The first stage in using the EPROM programmer is to load and run the support package software which is written in BASIC and assembly code. The user will first be prompted for EPROM type, valid responses being 2758, 2716, 2516, 2732, 2732A, 2532, 2764, 2564 and 27128. A request for a base address will then be made and the user should respond with a four-figure hexadecimal number. The base address is the address relative to which all references to computer internal memory are made and this means that the user does not need to be concerned with the actual absolute addresses in computer memory. The reasons for being able to select the base address are two fold. Firstly, to fit in with the memory map of any computer on which the software may be run and, secondly, to allow more than one set of data to be maintained at one time by using different base addresses. A table showing all the commands available will be printed before the *? prompt appears on the screen. When this prompt indicates that the program is waiting for input of a command, it is safe to insert or remove EPROMs from the ZIF socket, provided, of course, that the isolating switch is in the OFF position for 28 pin devices.

The following describes the function of the EPROM programmer support package commands. It should be noted that in each case, either the whole word or the initial letter may be used:-

(N)EW, (B)ASE These two commands cause the user to be prompted for a new EPROM type or a new base address respectively, hence allowing these two

parameters to be altered without exiting and re-running the program. **(T)EST** This performs a test on the EPROM, reporting whether or not it has been erased.

(R)EAD, (P)ROGRAMME, (V)ERIFY These commands cause the user to be prompted for start and finish addresses which should be entered



Overlay diagram of the programmer.

as two four-figure hexadecimal numbers separated by a comma. These addresses define the portion of the EPROM to be used and also the portion of computer internal memory into which data will be written for a read operation or from which data will be read for program or verify operations. The computer

addresses are offset from the base address. In program and verify, any discrepancies between EPROM and computer memory will be reported. Such discrepancies will be printed, one per line, stopping after every 16 lines. Pressing return at this point will return to the *? prompt, whereas pressing any other key will

PROJECT : EPROM Programmer

PARTS LIST

RESISTORS (all $\frac{1}{4}$ W 5% unless stated)

R1, 11, 13	10k
R2, 12, 14	1k0
R3, 16	100k
R4, 5	5k1
R6	240R
R7	15k
R8	680R
R9	OR22 wire wound
R10	180R, 1W
R15	33k
RV1, 3	2k2 min horizontal preset
RV2	4k7 min horizontal preset

CAPACITORS

C1	1u 35 V axial electrolytic
C2, 7, 8, 9,	
10	100n ceramic
C3	470u 35 V axial electrolytic
C4	4n7 polyester
C5	10n ceramic
C6	100u 6V3 axial electrolytic
C10	10n ceramic

SEMICONDUCTORS

IC1	74LS126
IC2	74LS245
IC3	74LS04
IC4	74LS30
IC5	74LS138
IC6, 7, 8, 9	MC6821 (or similar)
IC10	LM317M
IC11	78S40
Q1, 3, 4, 5,	
7	BC184L
Q2, 6, 8	BC214L
D1, 2	OA91

MISCELLANEOUS

L1	34 turns 24 swg wire on RM6 pot core (AL = 250)
SK1, 2	0.1" pitch 22-way male molex connectors (or shorter ones made up to required length)
SK3	28 pin zero insertion force socket (or ordinary socket is console is used, see text)
SW1	two pole single throw switch (omit if using console)

One 16-way and one 80-way DIL headers and sockets; edge connector (2 x 32-way A+B DIN Euro connector, male angled pins, for Tangerine) PCB, wire, etc.

continue the programming or verification.

(L)IST, (M)ODIFY These commands probably duplicate facilities available in the computer monitor but are included here to allow minimum changes to be made to computer memory or data to be checked without the need to exit from this package. LIST will request start and finish addresses and will list on the screen the addresses and data of the portion of memory requested, offset from the base address. The listing will stop after every 16 lines at which point pressing return will exist to the *? prompt, whereas pressing any other key will continue with the listing.

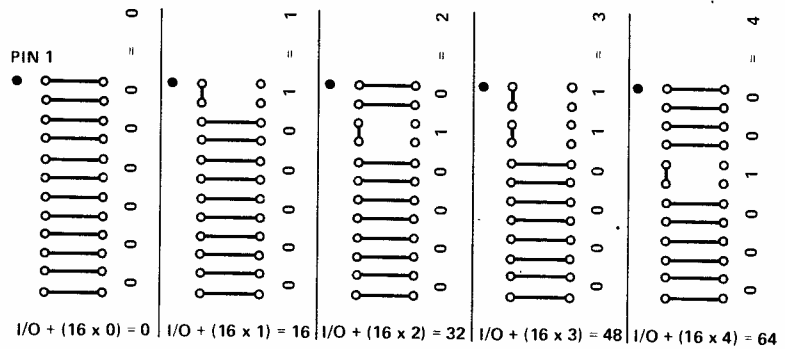


Fig. 3 Setting the address offset by wire links.

MODIFY will prompt for a single address, the contents of the base address offset by the value given being displayed on the screen. Entering an X at this point will return to the *? prompt leaving the data in that location unchanged, whereas entering a two-figure hexadecimal number will cause the relevant address to be updated with the data entered.

(H)ELP Lists all the commands available and reminds the user of the currently selected EPROM type and base address.

(E)XIT Causes the program to terminate.

In the above commands, any wrongly entered information will result in self-explanatory error messages. The one error message which, perhaps, requires a word of explanation is TYPE/RANGE INCOMPATIBLE. This error is a result of entering a start and finish address to any command which defines a range larger than the capacity of the selected EPROM type.

Erasing EPROMs

EPROMs are erased by exposure to ultra-violet light through the transparent window on the top of the package. Small commercially available erasing units with capacities of up to six chips cost typically in the £40-£50 region. If the requirements for erasing EPROMs are considered, it becomes obvious that an erasing unit can be constructed for considerably less than the price of commercial equipment. The requirements stated by EPROM manufacturers to erase such a device are a 20 to 30 minute exposure of 2357 Å (253.7 nm) wavelength ultra-violet light at an intensity of 12000 uW/cm². The Philips TUV 15 W tube emits UV at the required wavelength and at an intensity of 37 uW/cm² at about one inch from the tube, the distance metre from the tube, which

corresponds to about 12000 uW/cm² at a distance of one inch, as used in most EPROM erasers.

The tube costs in the region of £10 and will fit into an ordinary 15" fluorescent light fitting, it provides the basis for a relatively inexpensive unit which could accommodate about ten ICs.

A few words of caution are appropriate at this point. Ultra-violet radiation, and in particular shortwave UV as emitted by the TUV 15 W, is harmful to both the eyes and the skin. It is therefore essential to build the tube into a light-tight cabinet, ideally with a micro switch fitted under the lid to isolate the supply when opened, which will prevent UV light from coming into contact with skin or eyes.

EPROMs may also be erased by UV of longer wavelength (3000 Å - 4000 Å) although longer exposure times will probably be required. Since 'black light' tubes of the type used for disco lighting emit at about 3500 Å and are more easily available than short-wave UV tubes, it may be worthwhile experimenting with this type of light source.

One final point on the topic of erasing EPROMs is that both sunlight and ordinary fluorescent tubes emit some radiation in the 3000 Å - 4000 Å region with the result that prolonged exposure to these light sources will result in erasure. For this reason it is recommended that an opaque adhesive label is used to cover the windows of programmed EPROMs.

Next month, we'll describe the software for the unit.

ETI

BUYLINES

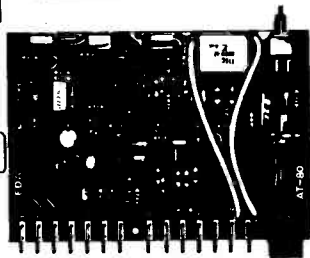
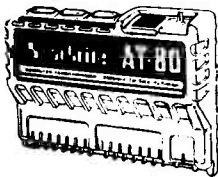
There should be relatively few problems in obtaining components for this project. The 0.22R resistor can be found in several suppliers' lists, including Watford's. The RM6 potcore is available from RS Components. our PCB service — see page 77 for details.

Step-by-step fully illustrated assembly and fitting instructions are included together with circuit descriptions. Highest quality components are used throughout.

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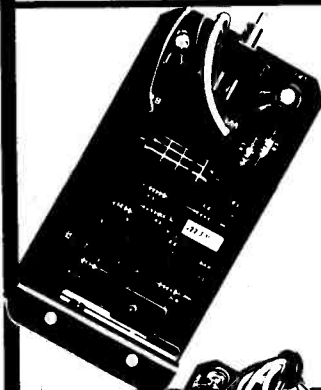


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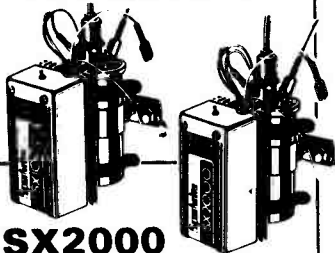
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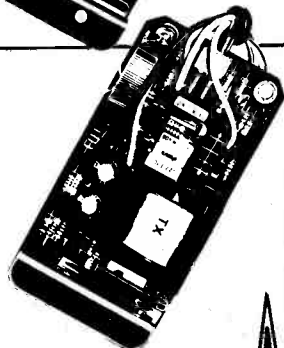


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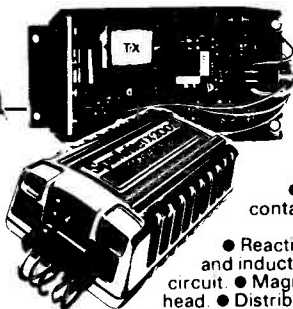


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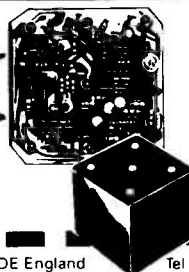


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READ/WRITE

Hyconomiser

Dear Sir,

I have been a more or less regular reader of ETI since its inception and I think generally you do a pretty good job; however, you have now made a serious error by recommending a product which you are not really qualified to pronounce upon. I refer to the feature on the Hyconomiser in your June issue.

If, instead of questioning the garages involved in selling the device, who you must admit have a vested interest, you had spoken to a recognised authority on the subject, I am sure you would have been told not to waste your time on it, and certainly not to give any recommendation. Talking to garage mechanics about engine fuelling and exhaust emission technology (a subject not far behind aerospace and electronics for expenditure and complexity) is rather like asking an electrician to comment on the latest microprocessor.

For many years, including a number as a senior development engineer at Jaguar Cars, fuel economy had been a specialist subject of mine and devices such as the Hyconomiser invariably come my way for appraisal. In fact, two or three years ago this device was being marketed as the PED with a rather different story behind it. I enclose a copy of the advertising material relevant to that incarnation which you will see employs the same diagram you reproduced. In an attempt to win me over I was visited by the alleged inventor of the device, a certain Canadian called Andrew MacGuire, and was presented with an impressively thick report, produced in the USA, purporting to show how effective it was. To the uninitiated it was most convincing but on close examination most of the tests were based on unrealistic baseline figures, in one case an exhaust CO level of 8% (a vastly over-rich condition) was used as a basis for comparison. I still have a copy of the report if you should wish to see it.

Whilst it may be that your reviewer obtained a measurable improvement after fitting the device, any air bleed into the inlet manifold (which in essence is what the Hyconomiser is) will have a mixture

weakening effect more or less compensating for wear of the carburettor metering orifice. For the car in question a new carburettor, or even simply replacing the metering needle costing about £3, would undoubtedly have shown similar, if not better gains. In any event the only way to test a device such as this is under carefully controlled conditions and even then so many variables can be involved that results are likely to have a spread of 10% or so.

As for the claim that fuel droplets are broken up with sonic waves generated by three pulsating balls, if you believe that I would also expect you to look for fairies at the bottom of your garden. For sonic waves to pulverise fuel droplets it is necessary for a large amount of energy to be expended in shearing the mixture and even then economy gains are unlikely to exceed 10%.

The claim that the device maintains the air/fuel ratio close to stoichiometric is quite unfounded. If you can find out how this is achieved pleased let me know — nobody has been able to explain to me how it can happen.

Finally, if a device such as this was able to offer the improvements claimed, the motor manufacturers would be already using it rather than running multi-million pound retooling programmes to obtain relatively modest gains, and electronic engine management systems (surely a more appropriate subject for you to become involved in) would be unnecessary.

If you wish to maintain the high reputation of your magazine I think you would be well advised to print a retraction on the subject as soon as possible.

Yours faithfully

Roger Bywater

Roger Bywater Engineering Ltd
Stockport
Cheshire

The author replies:

Much more about the Hyconomiser, its inventor and history was known to me before undertaking the review, but my brief from the editor was to confine the report to 1,000 words so much had to be omitted. The device reduces pollution as well as effects fuel economy. In Canada where it was first produced, pollution control

is of greater interest than economy because of government controls, hence it was called the PED., (Pollution Elimination Device). Out of 400 devices tested by the American Environmental Protection Agency, the PED came out first. To the British motorist economy is the more important factor, hence the change of name. There is nothing sinister in that.

Mr Bywater scorns the idea that sonic waves produced by plastic balls can break up fuel droplets. Perhaps he would likewise scorn the suggestion that a piece of flapping paper could permanently damage scores of human eardrums at a range of many yards, yet if he would visit his nearest disco he will find loudspeaker cones doing just that. It is the power actuating the medium, not the medium itself that is important. Here, the power is provided by the vacuum generated by the engine intake or induction stroke. If this has sufficient power to atomise fuel from the carburettor in the first place why should it be insufficient to complete the job by means of the Hyconomiser?

The balls are in fact tuned to resonance, and when resonating any physical object is capable of high amplitude oscillation which can even be destructive, as any student of mechanical stress engineering would know. The effect has in fact been observed in tests carried out by a motor manufacturer. An intake manifold with transparent quartz window was assembled to a production engine. With normal running, drops of fuel could be seen coursing the over the inside surfaces to be ejected with the exhaust, but when Hyconomiser was switched in by a control valve, the drops instantly vaporised into a mist. Special rapid-exposure photographic techniques and precision measurements revealed the particle size to be in the region of eight microns.

The motor manufacturer, (a well-known name that I cannot reveal at present) will in fact be using the Hyconomiser in future production models. It has not been used before because car design and planning is usually at least three years ahead of current production. Other manufacturers are actively considering it.

Mr Bywater's assertion that my economy figures were due to a leaner mixture produced by bleeding air past the carburettor can be refuted on two counts. First, the carburettor mixture setting must be made slightly richer before fitting the Hyconomiser to compensate for the extra air thus restoring the correct air/fuel ratio. Se-

cond, when the device went off tune for reasons described in my review, the consumption climbed to its former figure. On re-tuning, the economy returned. According to Mr Bywater tuning should have made no difference as air was still passing through. He alleges that the air bleed merely neutralizes wear in the fuel needle and orifice of the carburettor, and that a replacement would have the same result. However, the device has been fitted to brand new cars with notable economy improvements.

The 8% CO emission figure he complains of does indeed represent an abnormally rich mixture, some 9:1 air/fuel ratio. However, this was merely the starting point of a graph plot which shows the comparative CO emissions with and without the Hyconomiser, over a wide range of mixtures from 9:1 to 20:1. You have to start a plot somewhere, usually it is best to do so outside of the area of interest so that a complete picture is presented.

As to the question as to how the stoichiometric (optimum) 14.6:1 ratio is maintained by the device, this is done firstly by improved atomisation and distribution of fuel. Thus the anomalies of lean and rich areas in different cylinders and parts thereof are avoided. Secondly, the lowest ball in the Hyconomiser seats against its exit orifice. This expands and contracts according to the vacuum in the inlet manifold and so controls the airflow. Thereby the amount of air, hence mixture ratio, varies in response to engine speed and throttle setting, so compensating for the mixture vagaries produced by the carburettor under differing conditions.

Garages who fit the Hyconomiser may indeed, as Mr Bywater says, have a vested interest, but not of the sort he insinuates. All those I contacted were reputable main-agent establishments with large factory-trained staffs and the latest in electronic tuning and diagnostic equipment. Their vested interest is in their reputation which would soon be in tatters if they fitted rubbish that didn't work. As the proprietor of a fuel injection and economy development company, may I suggest that HE is the one that has a vested interest in knocking the Hyconomiser!

Vivian Capel.

We doubt whether we have heard the last of this topic. For those of you still sending us missives by various means, the Hyconomiser is now made under licence by: Atwell Construction Ltd, Station Road, Wrington, Avon, Tel: Bristol 719441.

Compact Disc

Dear Sir,

The article in your May '83 issue concerning recommended high-quality turntable systems was punctuated by a small section on the new Compact Disc format. As the author observes, 'in about a year' CD players will be altogether affordable, probably considerably cheaper than specialist analogue turntables and therefore likely to oust them on grounds of both performance and value. At that time, second hand (one year old), once-expensive analogue players would presumably be demoted to duties such as door-stopping or pot-throwing in view of their likely marketability. I would therefore query the advisability of any recommendation to buy high quality analogue disc equipment.

Of course, my premis in such a sweeping statement is that CD will be a vastly superior format, bringing me onto my second beef; why so little space for such an important breakthrough, about which plentiful information has been distributed in advance certainly to many Hi-Fi magazines who have seen fit to publish reports on the subject? Now I would not expect you to give a high priority to reporting on Hi-Fi matters normally, though surely the presence of an audio article anyway might have been used to better advantage.

I would certainly be interested to know what levels of fidelity are claimed for the pressing and then optimal reading of vinyl discs so that these could be compared with the plentiful information available for digital format.

The world of audio performance assessment has become altogether cluttered with highly subjective judgement. Hi-Fi magazines persist in, what seems to me, the odious convention of allowing poets with 'golden ears' to subjectively assess nebulous qualities, transferring little hard information to the reader. For reference, it would be interesting to see, published alongside a reviewer's observations, the results of a thorough hearing test performed on him at a relevant time. Could controlled levels of distortion, on identical pieces of recorded music, be used to test a 'golden auditor's' true calibration?

Personally, I find it difficult to give more credence to the doubtless limited-bandwidth response of ageing reviewers than laboratory test equipment. Admittedly, standards of distortion measurement are confusing, and it is not sufficiently relevant

to music reproduction to be testing pure tones, but why not simply compare 'scope photos of microphone signals at the recording studio with the ultimate, played-back signal from analogue and digital discs? Could such a test be arranged or would vested interests prevent it?

An article devoted to bringing more rigour into Hi-Fi assessment along these lines would certainly have my fullest attention, and should not be irrelevant to the aims of your magazine, since it would not labour the subject of the Hi-Fi market or the present state of the manufactured art, but would deal rather with 'transduction'.

Yet more relevant, of general interest and, as yet, unreported (to my knowledge) would be an investigation of the digital disc format and its protocol; how are the discs manufactured, what is this error correction business? Would it be at all possible to produce an alternative erasable and programmable, ideally compatible, optical recording system, perhaps by populating a disc fully with reflective logic cells but positioning an optically switchable window in front of each?

Presumably it is the variability in performance of D-to-A convertors that accounts for the present variability in CD player performance. Would it be conceivably possible to delay the mapping to as late a stage as possible, having a (perhaps integral) D-to-A power output stage, or is the process of amplification (and transduction) best left to conventional analogue techniques? An acquaintance has described to me his attempts to make a digital switching amplifier. (A-to-D-to-A), but, presumably digital speakers could not successfully operate composed of an array of switching drivers, (one twice the size of the next) whilst the idea of linear stepper motors attached to conventional diaphragm(s) would seem unrealistic.

Any ideas?

Yours faithfully

Mr P.E. Cox

Derby

Mr Cox raises far too many points for us to answer in the space available! Suffice to say that CD will not make analogue players obsolete because there will still be a lot of analogue discs around for many years to come. We'll obviously be reporting further on CD in the future.

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TOROIDALS

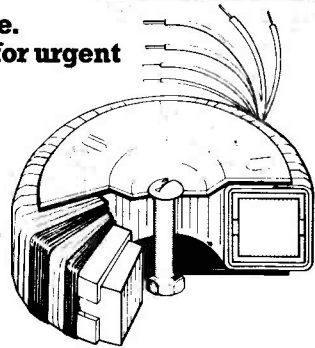
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NEW! NEW! NEW!																		
15 VA 62 x 34mm 0.35Kg Regulation 19%	0x010	6+6	1.25	£5.12 + p & p £0.78 + VAT £0.89 TOTAL £6.79	120 VA 90 x 40mm 1.2Kg Regulation 11%	4x010	6+6	10.00	£7.42 + p & p £1.72 + VAT £1.37 TOTAL £10.51	300 VA 110 x 50mm 2.6Kg Regulation 6%	7x013	15+15	10.00	£10.88 + p & p £2.05 + VAT £1.94 TOTAL £14.87				
	0x011	9+9	0.83			4x011	9+9	6.66			7x014	18+18	8.33					
	0x012	12+12	0.63			4x012	12+12	5.00			7x015	22+22	6.82					
	0x013	15+15	0.50			4x013	15+15	4.00			7x016	25+25	6.00					
	0x014	18+18	0.42			4x014	18+18	3.33			7x017	30+30	5.00					
	0x015	22+22	0.34			4x015	22+22	2.72			7x018	35+35	4.28					
	0x016	25+25	0.30			4x016	25+25	2.40			7x026	40+40	3.75					
	0x017	30+30	0.25			4x017	30+30	2.00			7x025	45+45	3.33					
						4x018	35+35	1.71			7x033	50+50	3.00					
			4x028	110		1.09	7x028	110			2.72							
			4x029	220	0.54	7x029	220	1.36										
			4x030	240	0.50	7x030	240	1.25										
30 VA 70 x 30mm 0.45Kg Regulation 18%	1x010	6+6	2.50	£5.49 + p & p £1.10 + VAT £0.99 TOTAL £7.58	160 VA 110 x 40mm 1.8Kg Regulation 8%	5x011	9+9	8.89	£8.43 + p & p £1.72 + VAT £1.52 TOTAL £11.67	500 VA 140 x 60mm 4Kg Regulation 4%	8x016	25+25	10.00	£14.38 + p & p £2.40 + VAT £2.52 TOTAL £19.30				
	1x011	9+9	1.66			5x012	12+12	6.66			8x017	30+30	8.33					
	1x012	12+12	1.25			5x013	15+15	5.33			8x018	35+35	7.14					
	1x013	15+15	1.00			5x014	18+18	4.44			8x026	40+40	6.25					
	1x014	18+18	0.83			5x015	22+22	3.63			8x025	45+45	5.55					
	1x015	22+22	0.68			5x016	25+25	3.20			8x033	50+50	5.00					
	1x016	25+25	0.60			5x017	30+30	2.66			8x042	55+55	4.54					
1x017	30+30	0.50	5x018	35+35		2.28	8x028	110			4.54							
50 VA 80 x 35mm 0.9Kg Regulation 13%	2x010	6+6	4.16	£6.13 + p & p £1.35 + VAT £1.12 TOTAL £8.60		225 VA 110 x 45mm 2.2Kg Regulation 7%	6x012	12+12			9.38	£9.81 + p & p £2.05 + VAT £1.78 TOTAL £13.64	625 VA 140 x 75mm 5Kg Regulation 4%		9x017	30+30	10.41	£17.12 + p & p £2.55 + VAT £2.95 TOTAL £22.62
	2x011	9+9	2.77				6x013	15+15			7.50				9x018	35+35	8.92	
	2x012	12+12	2.08		6x014		18+18	6.25	9x026	40+40	7.81							
	2x013	15+15	1.66		6x015		22+22	5.11	9x025	45+45	6.94							
	2x014	18+18	1.38		6x016		25+25	4.50	9x033	50+50	6.25							
	2x015	22+22	1.13		6x017		30+30	3.75	9x042	55+55	5.68							
	2x016	25+25	1.00		6x018		35+35	3.21	9x028	110	5.68							
2x017	30+30	0.83	6x026	40+40	2.81		9x029	220	2.84									
80 VA 90 x 30mm 1Kg Regulation 12%	3x010	6+6	6.64	£6.66 + p & p £1.72 + VAT £1.26 TOTAL £9.64	6x019		25+25	4.50	9x030	240	2.60							
	3x011	9+9	4.44		6x017		30+30	3.75										
	3x012	12+12	3.33		6x018	35+35	3.21											
	3x013	15+15	2.66		6x026	40+40	2.81											
	3x014	18+18	2.22		6x025	45+45	2.50											
	3x015	22+22	1.81		6x033	50+50	2.25											
	3x016	25+25	1.60		6x028	110	2.04											
3x017	30+30	1.33	6x029	220	1.02													
3x028	110	0.72	6x030	240	0.93													
3x029	220	0.36																
3x030	240	0.33																

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TECH TIPS

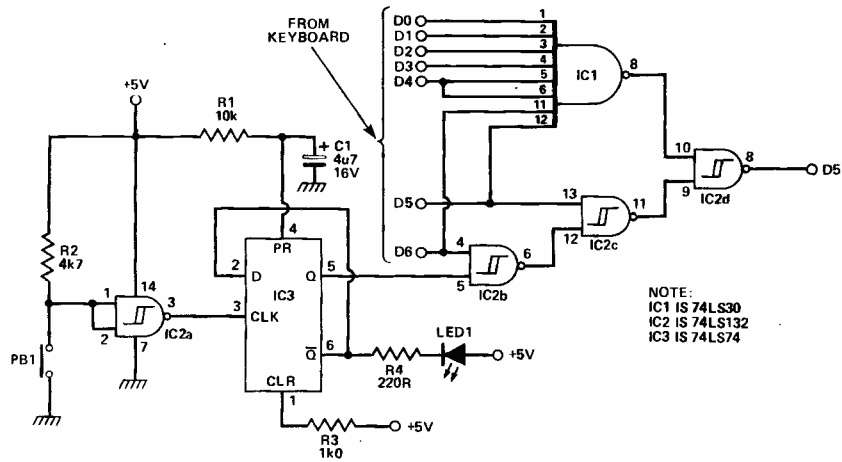
Keyboard Alphanumeric Lock Switch

G. Franklin, Mid Glamorgan

If your ASCII keyboard is like mine, then you too will have become tired of having to press 'SHIFT' for capital letters. SHIFT lock is useless because you have to 'unlock' to use the numbers. This circuit does away with this problem by providing you with yet another key to press. This is the 'ALPHA LOCK' switch.

If you study the ASCII codes you will find that to change 'a' into 'A' requires only the removal of the logic '1' on the data bit 5 line (of the 8 bit bus from the keyboard to your computer).

e.g.:-
 ASCII code a A
 in binary:- 0110 0001 0100 0001
 We require to alter the complete alphabet, this stretches from a (\$61)



NOTE:
 IC1 IS 74LS30
 IC2 IS 74LS132
 IC3 IS 74LS74

to z (\$7A). The circuit cheats slightly, by altering codes \$60 to \$7F inclusive, the only problem with this is that \$7F is the ASCII code for 'DELETE'. IC1 deals with this, by detecting the \$7F code and making sure D5 stays at a logic 1 via the NAND gate at the end of the circuit.

One quarter of the 74LS132 is used to give a degree of switch bounce to S1. Every time S1 is pressed, the Q output of the latch (IC 3) will change, R1 and C1 ensure that on power-up the output is at a logic 1. This, along

with data bit 6 being 'HIGH' will make D5' a 'LOW', thus shifting a \$60 code down to \$40 (unless of course it was the 'DELETE' key that was pressed). The LED will come on to show when the ALPHA mode is selected. To insert this circuit into your keyboard, it is only necessary for D5' to come via this circuit, D5' then continuing in its place to the computer, the other data lines just connect to the circuit. The only other requirement is that you insert a switch somewhere.

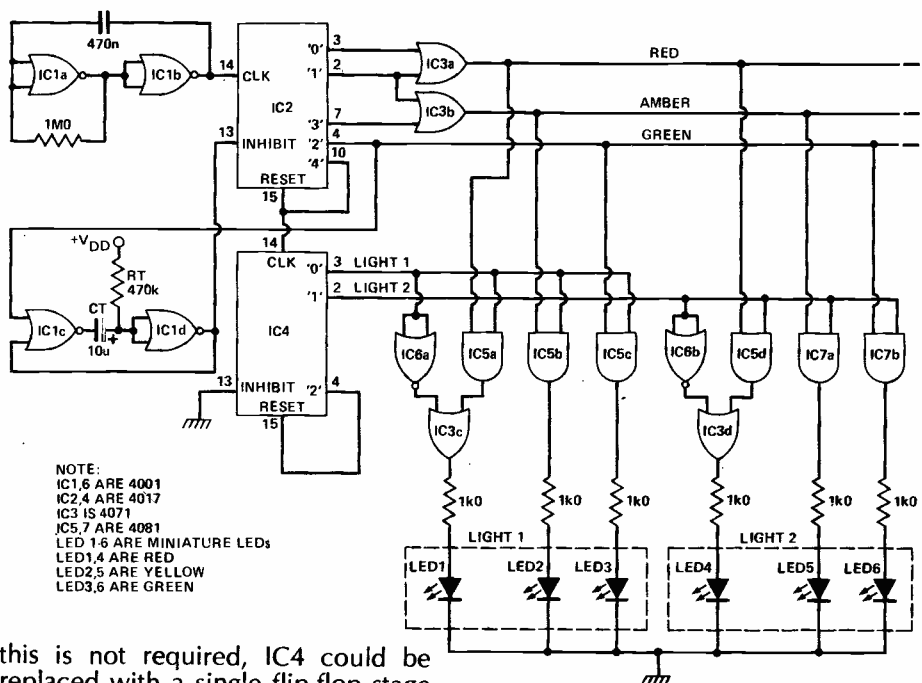
Controller For Model Traffic Lights

P. Bailey, Glasgow

The circuit shown was devised to control LED traffic lights at a road junction in a model railway layout, for added realism. IC2, a decade counter, together with IC3a and IC3b, generates the normal traffic light sequence continuously at a rate determined by the oscillator formed around IC1a and IC1b. A monostable formed by IC1c and IC1d is triggered by a '1' on the 'GREEN' output, and inhibits IC2 for a period set by C_T and R_T, thus causing the green light to be on for a longer period than the others.

IC4 selects either LIGHT 1 or LIGHT 2 to display the sequence, these being selected alternately. When one light is changing or at green, the other is held at red.

The controller is easily expanded to operate more than two lights by using further outputs from IC4, but if



NOTE:
 IC1,6 ARE 4001
 IC2,4 ARE 4017
 IC3 IS 4071
 IC5,7 ARE 4081
 LED 1,6 ARE RED
 LED2,5 ARE YELLOW
 LED3,6 ARE GREEN

this is not required, IC4 could be replaced with a single flip-flop stage (eg a 4013), set to toggle, LIGHT 1 and LIGHT 2 being connected to the Q and Q' outputs respectively. With a little ingenuity, realistic-looking traffic

lights can be constructed from miniature LEDs and empty pen refill tubes.

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THANDAR TM351

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Accessories: Carrying case £6.84. Universal test lead set £12.65. Service Manual £3.00.



THANDAR TM353

● Bench/portable ● 3½-digit 0.5" LCD ● 0.25% basic accuracy ● 26 ranges ● Battery life typically 3000 hrs ● Complete with batteries & test leads £86.25. Accessories as TM351.



THANDAR TM354

● Pocket size ● 3½-digit 0.5" LCD. ● 0.75% basic accuracy. ● 14 ranges ● Battery life 200 hrs £45.94. Carrying case £3.45. Universal test lead set £12.65. Service Manual £3.00.



THANDAR TM451

● Bench/portable ● 4½-digit 0.4" LCD ● 0.03% basic accuracy ● Full auto-ranging or manual ● Sample hold ● Audible continuity test ● Complete with battery and leads £171.35. AC Adaptor £7.99. Universal test leads £12.65. Service Manual £3.00.



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TG105 Pulse 5 Hz to 5 MHz £97.75



FREQUENCY COUNTERS

THANDAR TF200 10 Hz to 200 MHz

● Bench/portable ● 8-digit Liquid Crystal Display. ● Frequency range 10 Hz - 200 MHz ● Resolution better than 1 ppm ● Sensitivity typically 10mVrms ● Time base accuracy 0.3 ppm. ● Battery life 200 hours ● Frequency, time average period, totalize & reset; 2 ranges, 5 gate times; external clock facility ● Complete with batteries. £166.75.



THANDAR TF040 10 Hz to 40 MHz

● Bench/portable ● 8-digit Liquid Crystal Display. ● Frequency range 10 Hz - 40 MHz ● Resolution 1 Hz. ● Sensitivity 40 mV rms. ● Timebase accuracy 0.5 ppm ● Battery life 80 hours. ● Frequency, totalize & reset; 2 gate times ● Complete with batteries. £126.50.

ACCESSORIES FOR TF200 & TF040 AC adaptor £7.99, Carrying case £6.48, X1 Probe £8.05, X10 Probe £8.20, Service manual £3.00. TP600 prescaler £51.75. TP1000 prescaler £74.75.



THANDAR PFM200A 20 Hz to 200 MHz

● Pocket size ● 8-digit LED display ● Frequency range 20 Hz - 200 MHz. ● Resolution 0.1 Hz. Sensitivity typically 10 mV rms. Timebase accuracy 2 ppm ● Battery life 10 hours. ● Frequency; 2 ranges, 4 gate times ● BNC input sockets £77.62. Accessories: Carrying case £3.45, AC adaptor £7.99, X1 probe £8.05, X10 probe £9.20, Service Manual £3.00.

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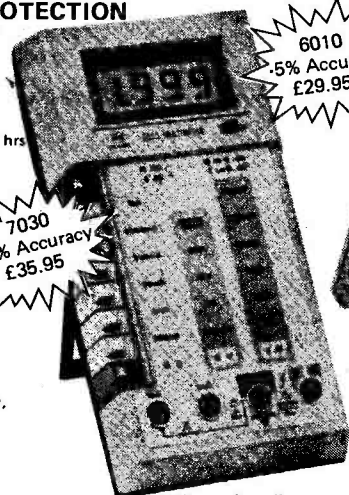
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- Decibels: -20 to +22dB
- DC Current: 0-50, 500µA, 0-5, 50, 500mA
- Ohmmeter: 0-6 Megohms in 4 ranges. 30 ohms Centre Scale
- Power Supply: One 1.5V size 'A' battery (incl)
- Size & Weight: 135 x 91 x 39mm, 280gr.

HM 101 POCKET SIZE MULTIMETER SPECIFICATION

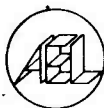
- DC & AC Voltage: 0-10, 50, 250, 1000 volts, 2000 ohms/volts
- Decibels: -10 to +22dB
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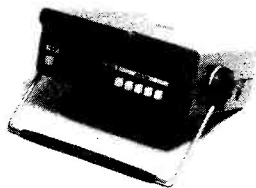
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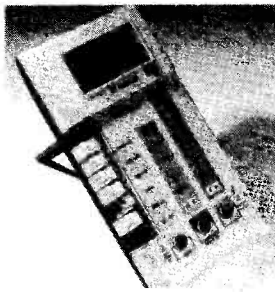
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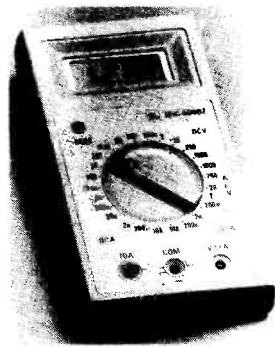
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OR 1 x 300W into 2 to 4Ω
1 x 150W into 4 to 8Ω
- Etc. Etc.

Having been closely involved in a wide variety of OEM applications of their amp boards, Pantechnic became aware of numerous implementation problems often left untackled by other amp board manufacturers. These problems specifically of size and thermal efficiency became particularly aggravated at high powers and considerably lengthened OEM product development time.

By including thermal design in the totality of board design it has been possible to reduce the size of the electronics, and increase the efficiency of the transistor to heatsink thermal circuit. The combined effect of this has been to dramatically increase the volumetric efficiency of the amplifier/heatsink assembly. The SYSTEM Amp offers 1.2KW of power in a space of 102mm x 102mm x 77mm, excluding PSU and Fan.

The basis of this considerable advance is the PANTECH 74 Heat Exchanger, newly designed and manufactured by us. By eliminating the laminar air flow found in conventional, extruded heat sinks, heat transfer to the environment is greatly enhanced.

The flexibility of the 1.2KW amp stems from its division into 4 potentially separate amplifiers of 300W each (downrateable with cost savings to 150W.) These can be paralleled, increasing current capability or seriesed (bridged in pairs) doubling voltage capability. In consequence a large variety of amplifier/load strategies can be implemented.

As ever Pantechnic offer a full range of customising options including DC coupling, ultra high slew etc. Contact Phil Rimmer on 01-800 6667 with your particular application problem. P.S. Specs, as ever, are exemplary.

OTHER POWERFET AMPLIFIER MODULES

Model	Price	Range (Rms)	Dyn-loads	Notes
*PFA100	20.65	50-150W	4Ω, 8Ω	Physically small (32 x 78 x 108mm)
*PFA200	27.35	100-300W	4Ω, 8Ω	High watts/C ratio
PFA/HV	36.04	200-300W	4Ω, 8Ω, 16Ω	5dB dynamic headroom Drives 70V line direct.
*PFA500	42.00	250-600W	2Ω, 4Ω, 8Ω	25A cont. output current.

mounted on type 74 Heat Exchanger (see below).

*The power output of these amplifiers can be increased by approx 15% with no diminution in quality by adding PSU102 (£7.61) to your existing power supply.

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RADIO CONTROL SERVO FAIL-SAFE

Up, up and away? Bring your model aircraft down to earth *without* a bump using the ETI Conservo. Phil Walker shows you how to make your servos fail safe.

No-one who has spent many hours and pounds constructing their radio-controlled boat, plane or animated aardvark would want it to sail, fly or crawl out of range of their transmitter. However, there is always the remote possibility that some nasty little gremlin will creep in and throw the spanner in the works. When that happens all your controls may well be stuck in the last position you used; and by a well-known Law of Nature (Lex Divoti*), the position will make it as hard as possible to retrieve your model.

Help is at hand! This project will set your servos to any position you require (if you fit it beforehand) and if set up correctly your precious model should sail, fly or waddle home safely.

Use

The ETI Conservo is simply connected into the servo leads (get the polarity right) and the variable resistor can then be set to make the servo take up what you hope is a safe position. This setting is best done with slightly used batteries, to get a true position. Do not have the radio link operating while doing this or you won't be able to make the setting.

If your system uses low voltage (ie, around 3.6 volts) don't forget to increase the size of C2 to its higher value.

The Circuit

The circuit of this project is designed around a 4093 CMOS quad Schmitt trigger. This device will operate down to quite low supply voltages while still providing reliable switching performance.

One section of the device (IC1a) is used to detect the possibility that the input signal has stuck at a high

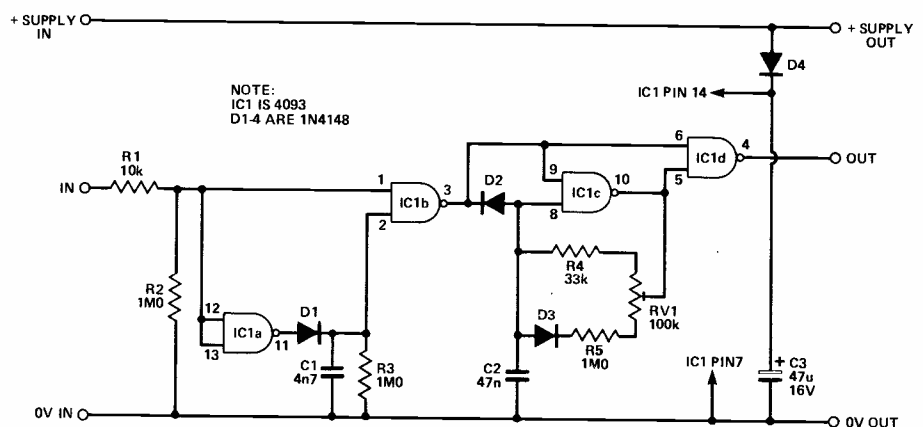


Fig. 1 Circuit diagram of the Conservo.

HOW IT WORKS

R1 and R2 protect the inputs of the CMOS devices from overload or static damage. The normal input to the device is a series of 1 to 2 ms positive pulses repeated at about 20 ms period. When the input is low, IC1a holds C1 high via D1 thus maintaining IC1b pin 2 at a high level.

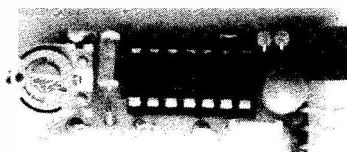
When a pulse arrives, the output of IC1b goes low, discharges C2 and forces the output of IC1d high for the duration of the pulse. When the input pulse goes low again, C2 starts to charge via RV1 and R4 but will be discharged again by another input pulse before its voltage reaches the trigger threshold of IC1c. This means that the output of IC1c will stay high permanently in normal operation.

If another pulse does not arrive and the input stays low, the output of IC1b will stay high and C2 will charge up until its voltage reaches the threshold of IC1c

whose output will then go low and discharge C2 via RV1, R5 and D3 until the lower threshold of IC1c is reached. IC1c's output will then go high again and the cycle will repeat. When the output of IC1c is low, the output of IC1d will be forced high. The component values used in the circuit are such that this cycle approximates to the normal servo control signal with RV1 controlling the pulse width.

If for any reason the input sticks at a high level, C1 which is normally kept charged up by IC1d will have time to discharge effectively putting a low level on the input to IC1b. This will cause the same sequence of events to occur as when the input stuck low but after a short delay.

Finally, D4 and C3 form a reserve power supply to ensure that the circuit is not affected by supply line transients.



A small project (this is actual size) but a long name — and a large degree of usefulness.

level. Since normally the input only goes high for relatively short periods at a time, the output from IC1d spends most of the time at a high level. This fact is used to charge a capacitor to near the supply potential. This capacitor can only be discharged by a resistor connected in parallel with it and then only if it has enough time to do so. In normal operation this will not be the case.

The second part of IC1 (IC1b) combines the original input signal with the 'stuck at high' signal and its output goes high when either is low. Note that this output only usually goes low when normal control pulses are being received. The low periods of the output from IC1b are used to discharge the timing capacitor of the oscillator formed around IC1c. The output from this oscillator would normally be a series of low going pulses of approximately the same frequency as the usual control pulses. The width of these pulses can be set by the variable resistor to simulate any servo position required. However these pulses will only be generated if the normal input fails to discharge the timing capacitor within a reasonable time.

The output from the gated oscillator described above and the output from IC1b are combined in IC1d to give the final output from the unit.

In normal operation the output will follow the input with no alteration as C1 will not discharge enough and C2 will not charge enough to have any effect. In a fault condition, however, the output from IC1b will stay at a high level (driven either by the input being low or by IC1a detecting the input high) and enable the gated oscillator (IC1c) whose output will be passed on to the servo being controlled. This will send the controlled servo to its preset position.

Construction

This should pose no real problems provided that care is taken to put the diodes, IC1 and C3 the right way round. This is a little more awkward than usual since some components must be mounted vertically to conserve PCB area.

A socket is recommended for IC1 — at least the first time you build it. Take care when handling IC1 to discharge yourself of any static charge. This also applies to your soldering iron which must be earthed. CMOS devices are still

delicate things.

RV1 can be either vertical or horizontal mounting and the PCB is laid out for both. If you want to save space and weight use a vertical mounting device and cut off the end of the PCB as shown by the dotted line. Inputs and outputs can be soldered directly to the board or alternatively, there are some 0.1 in. pitch PCB connectors available from Maplin in 3 way versions which would do the job.

The whole unit could be mounted in a box or possibly just varnished to keep out moisture (but not if the device is likely to be immersed!). For use on low voltages, ie less than 5 V, it may be necessary to increase the value of C2 up to 100nF in order to maintain the required output timing.

PARTS LIST

RESISTORS (¼W 5% carbon film)

R1	10k
R2,3,5	1M0
R4	47k
RV1	100k min. preset horizontal or vertical mounting

CAPACITORS

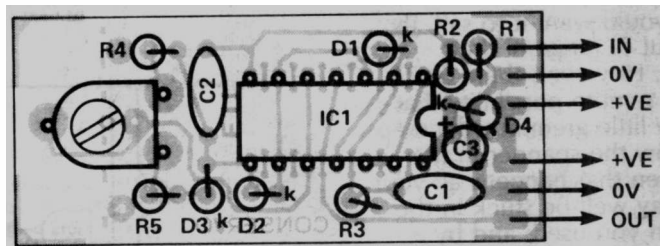
C1	4n7F min. layer polycarbonate
C2	47nF min. layer polycarbonate (100nF for 3.6 volt operation)
C3	47uF 16 V min electrolytic

SEMICONDUCTORS

D1,2,3,4	1N4148
IC1	4093

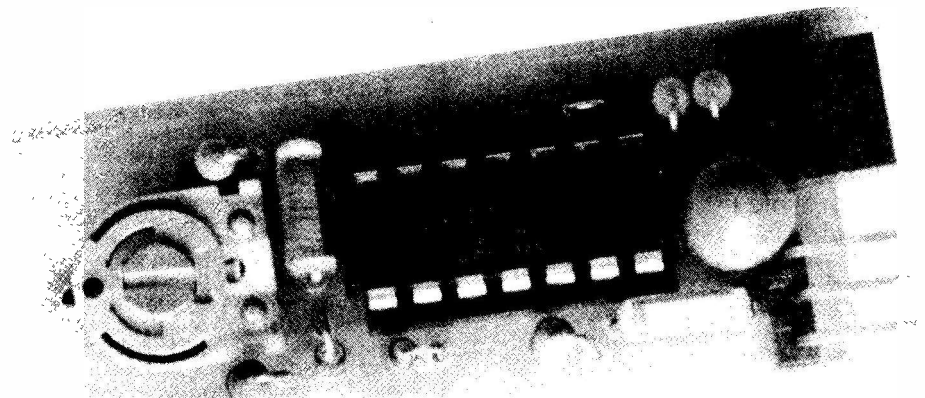
MISCELLANEOUS

PCB: see Buylines. 2 off 3 way 0.1 in. connectors (if required).



k = CATHODE

Fig. 2 Overlay diagram of the Conservo. Here we show a horizontal preset, but a vertical one could be used to save space — just cut the PCB along the marked line.



FOOTNOTE

*For those of you who are not scholars of Latin, Lex Divoti is a Law of Nature known by a number of names, most of them not printable, but can be summed up as: "If something can possibly go wrong, it will, at the most inconvenient moment and in the way that causes maximum damage."

BUYLINES

None of the components in this project should be at all difficult to obtain. The PCB is available through our PCB service — see page 77 for details.

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709	25	LM3915	175	LOGIC ICs				4521	90	LS02	11	LS156	33	0.22/35	12	2V7-33V500MW	7
741	14	LM3915	195	AY5-2376	590	4008	11	4522	105	LS03	11	LS157	25	0.33/35	12	5V1-75V 1.3W	14
748	35	LM13600	105	MC1488	55	4009	34	4526	55	LS04	12	LS158	27	0.47/35	12	BRIDGE RECTIFIERS	
9400CJ	345	MC1498	68	MC1489	55	4011	11	4527	65	LS05	12	LS160	30	0.68/35	12	1A/100V	20
AY-3-1270	710	MC3340	120	MM5303	625	4012	14	4528	45	LS08	12	LS161	35	1.0/35	12	1A/400V	23
AY-3-8910	370	MF10CN	350	MMS307	1250	4013	20	4531	65	LS09	12	LS162	35	1.5/35	14	1A/800V	25
AY-3-8912	540	ML924	195	MMS507	700	4015	39	4532	60	LS10	12	LS163	35	2.2/35	16	2A/100V	36
CA3046	60	NE529	225	MMS507	700	4016	20	4533	60	LS11	12	LS164	35	3.3/35	17	2A/200V	40
CA3080	65	NE531	135	MMS6114	365	4017	32	4538	80	LS12	12	LS165	40	10/25	18	2A/400V	40
CA3089	190	NE544	180	TMS6011	75	4020	42	4543	60	LS14	22	LS168	80	15/25	24	2A/800V	52
CA3080AQ	370	NE555	18	ULN2003	75	4021	39	4545	35	LS15	12	LS170	70	22/16	14	25/100V	36
CA3130E	85	NE556	45	8T26	99	4022	49	4555	35	LS20	12	LS171	47	33/16	14	25/200V	27
CA3140E	38	NE565	110	8T28	120	4023	39	4556	35	LS21	12	LS173	47	33/16	14	25/400V	27
CA3161E	100	NE566	140	8T95	90	4024	32	4558	100	LS22	12	LS174	36	4.7/16	16	25/400V	40
CA3189	200	NE567	100	8T97	90	4025	12	4584	40	LS22	12	LS175	36	6.8/16	16	25/600V	52
CA3240E	110	NE570	370	81LS95	80	4027	20	4585	50	LS27	12	LS181	87	10/16	18	REGULATORS	
ICL7106	680	NE571	370	81LS96	80	4028	47	COMPUTER ICs				LS183	105	15/16	27	78L05	30
ICL7611	95	RC4136	55	81LS97	80	4029	37	1802	650	LS32	13	LS190	35	22/16	27	78L12	30
ICL7621	180	RC4558	45	81LS98	85	4029	43	2650A	1175	LS33	14	LS191	35	33/16	40	78L15	60
ICL7622	180	SL490	250	6522	310	4035	45	6502	320	LS37	14	LS193	35	47/16	40	78L24	30
ICL8038	290	SL76477	380	6532	675	4040	40	6800	220	LS38	14	LS194	36	100/16	75	78L25	30
ICL8211A	150	SP8629	250	6821	110	4042	38	6802	250	LS40	12	LS195	32	15/10	22	78L26	30
ICM7224	775	TBA120S	70	6845	650	4043	40	6809	615	LS47	35	LS196	43	22/10	22	78L27	30
ICM7555	80	TBA800	75	6847	650	4044	41	8035	345	LS48	40	LS197	45	47/10	35	78L30	30
LF353	85	TBA810	95	6850	110	4049	21	8035	345	LS49	50	LS221	50	100/10	55	78L31	36
LF358	90	TBA820	70	6852	250	4050	42	8060	1090	LS51	14	LS240	55	100/6.3	42	78L32	36
LM10	325	TBA950	220	6875	485	4052	48	8080A	345	LS54	14	LS241	55	63V MINI MONOLYTHIC CERAMIC		78L35	36
LM301A	24	TDA1008	310	8155	350	4052	48	8085A	345	LS55	14	LS242	55	10nF	10	78L36	36
LM311	70	TDA1022	480	8212	110	4053	48	Z80A	315	LS56	16	LS243	55	22nF	10	78L37	36
LM318	120	TDA1024	115	8216	100	4066	22	MEMORIES				LS244	55	47nF	10	78L39	36
LM324	30	TL061	40	8224	110	4068	14	2101	395	LS75	16	LS245	55	68nF	10	78L40	36
LM334Z	90	TL062	60	8226	250	4069	13	2114(200ns)	85	LS76	16	LS251	28	100nF	14	78H05-5A/5V	550
LM335Z	120	TL064	95	8228	220	4071	13	2532	295	LS78	17	LS253	28			RESISTORS	
LM339	45	TL071	25	8243	270	4072	13	2708	225	LS83	33	LS257	29	1N4001	4	Carbon Film,	
LM348	60	TL072	45	8250	865	4073	13	2764	225	LS85	39	LS258	32	1N4002	4	High Stab 5%	
LM358	55	TL074	95	8251	250	4075	13	2764	225	LS86	15	LS259	53	1N4003	5	1/4W 10Ω-1M	
LM377	165	TL081	24	8253	400	4076	44	2764	225	LS88	39	LS266	18	1N4004	6	1/4W 10Ω-10M	
LM380	65	TL082	45	8255	400	4078	13	2764	225	LS89	22	LS267	30	1N4005	5	Metal Oxide/Film	
LM381	120	TL084	90	8257	400	4081	12	2716(5V)	210	LS90	22	LS279	53	1N4006	7	2% Met. Film E24	
LM382	110	TL170	49	8259	395	4082	12	2764	210	LS92	25	LS283	38	1N4007	4	1% Met. Film E24	
LM384	130	UA2240	115	8279	385	4093	23	2764	210	LS93	36	LS283	38	1N4148	2		
LM386	65	ULN2003	75	8832	250	4099	70	4116(200ns)	80	LS95	21	LS290	40	1N5401	12		
LM387	120	ULN2004	75	9602	220	4502	50	4118-3	325	LS109	21	LS293	40	1N5404	14		
LM393	95	XR2206	285	Z80ACTC	260	4508	110	4164	420	LS112	20	LS366	27	1N5407	12		
LM711	60	ZN414	79	Z80ADART	775	4510	45	5101(450ns)	150	LS113	20	LS367	27	1N5408	14		
LM725	325	ZN423	130	Z80ADMA	975	4511	45	5204	725	LS114	21	LS368	27	1N5409	14		
LM733	69	ZN424	130	Z80AP10	270	4512	42	6116(150ns)	375	LS123	34	LS368	27	1N5410	12		
LM747	60	ZN425E	340	Z80AEB	320	4514	110	6514	330	LS126	25	LS368	27	1N5411	12		
LM1458	40	ZN426E	290	Z80AEB	320	4514	110	6810	115	LS132	29	MICRO-MINI 100V CERAM PLATE CAPS					
LM2917	185	ZN427E	575	Z80AEB	320	4515	110			LS136	23	1pF 10nF	7	BEADS			
LM3900	45	ZN428E	395	Z80AEB	320	4516	50			LS138	24			ZENER DIODES			
										LS139	27			BRIDGE RECTIFIERS			
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Z80 CONTROLLER COMPUTER

This article describes the design and construction of a simple microcomputer control unit. (We called it MARVIN for reasons that would take too long to explain.) The unit is designed specifically for control functions which usually require complex purpose-built hardware. Consisting of a microprocessor and support chips, the unit is cheap enough to be used as an alternative to hard-wired logic with the advantage that its function is determined by easily-changed software.

The system can be used in conjunction with analogue devices, heavy duty switching, light dimmers, remote controllers, etc, to control anything from a Stirling Moss style computer controlled futuristic home to a morse code tutor.

Since there are so many possible uses, the construction of only the central computer parts (CPU, I/O, interrupt board) will be described; you will be left to chose external circuits according to your needs. Some additional interfaces will be available from the kit suppliers (see Buylines for details).

Split Personality

For maximum flexibility, MARVIN is divided into a CPU

board and two other types of board. The CPU board houses the microprocessor, a 2K EPROM containing the operating system, a second 2K of EPROM for the user's programs, 1K of RAM accessible to both the operating system and the users, and the selection circuitry for the various types of external port

details of programming will be given in a further article.

Since the I/O ports are on individual boards, you can add as many or as few as you need. MARVIN's I/O board provides 16 latched output lines and 16 input lines, which are TTL compatible. You can use up to five of these

boards.

The other type of board we shall describe provides up to eight individual lines which can interrupt the CPU. These are useful for allowing external devices to force the CPU to carry out a pre-designated routine. A typical use might be for controlling devices that need servicing at regular intervals, using an external clock to provide the timing.

This first part describes the functioning and construction of the CPU

board. This will be followed by a description of MARVIN's I/O and interrupt board and of MARVIN's operating system.

EPROMs

A Z80A running at 4 MHz theoretically needs memory capable of 375 nS access time. Most 2716s have an access time of 450 nS and although some may work adequately, it is strongly recommended that for reliable operation you make sure that you buy 350 nS EPROMs. If you decide

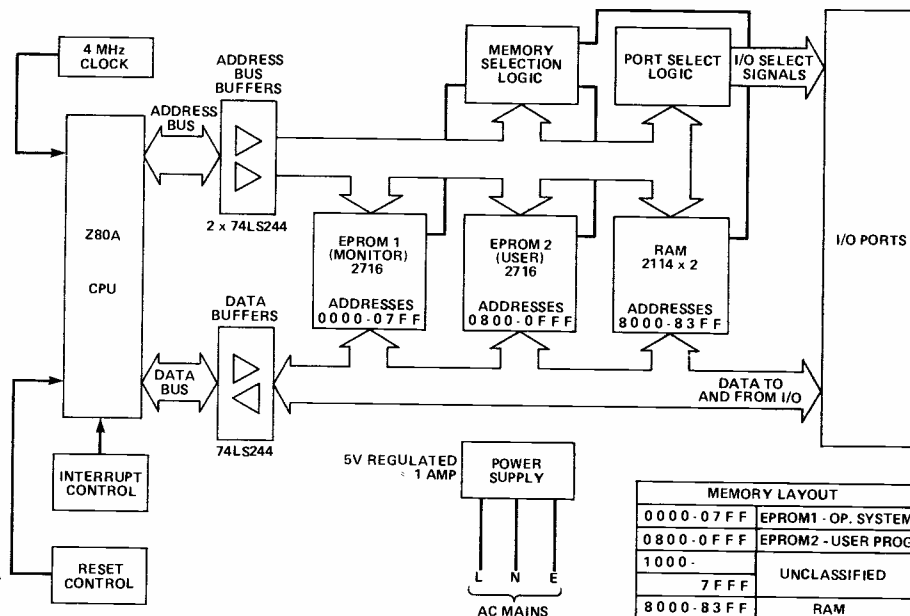


Fig. 1 Block diagram of Marvin.

MEMORY LAYOUT	
0 0 0 0 - 0 7 F F	EPROM1 - OP. SYSTEM
0 8 0 0 - 0 F F F	EPROM2 - USER PROG
1 0 0 0 -	
7 F F F	UNCLASSIFIED
8 0 0 0 - 8 3 F F	RAM

board.

Although 2K of program may seem small in comparison with the memory capacity of a personal computer, it will hold a surprisingly complex machine code program, of up to nearly 1000 instructions.

Several of the routines that you are likely to need are built into the operating system, and are directly accessible to the user by simple two-byte instructions. Your program must be inserted into the EPROM before use by a suitable PROM programming unit. Some further

Computer projects are usually complex affairs, as anyone who saw the Cortex will testify. This one isn't. Design and development by Peter Grigson and David Harris.

to make do with 450 nS types, then the crystal should be changed to 3.2768 MHz.

Also, we suggest that you should use a zero insertion force socket for the user EPROM, as

you'll probably be taking it in and out quite a lot.

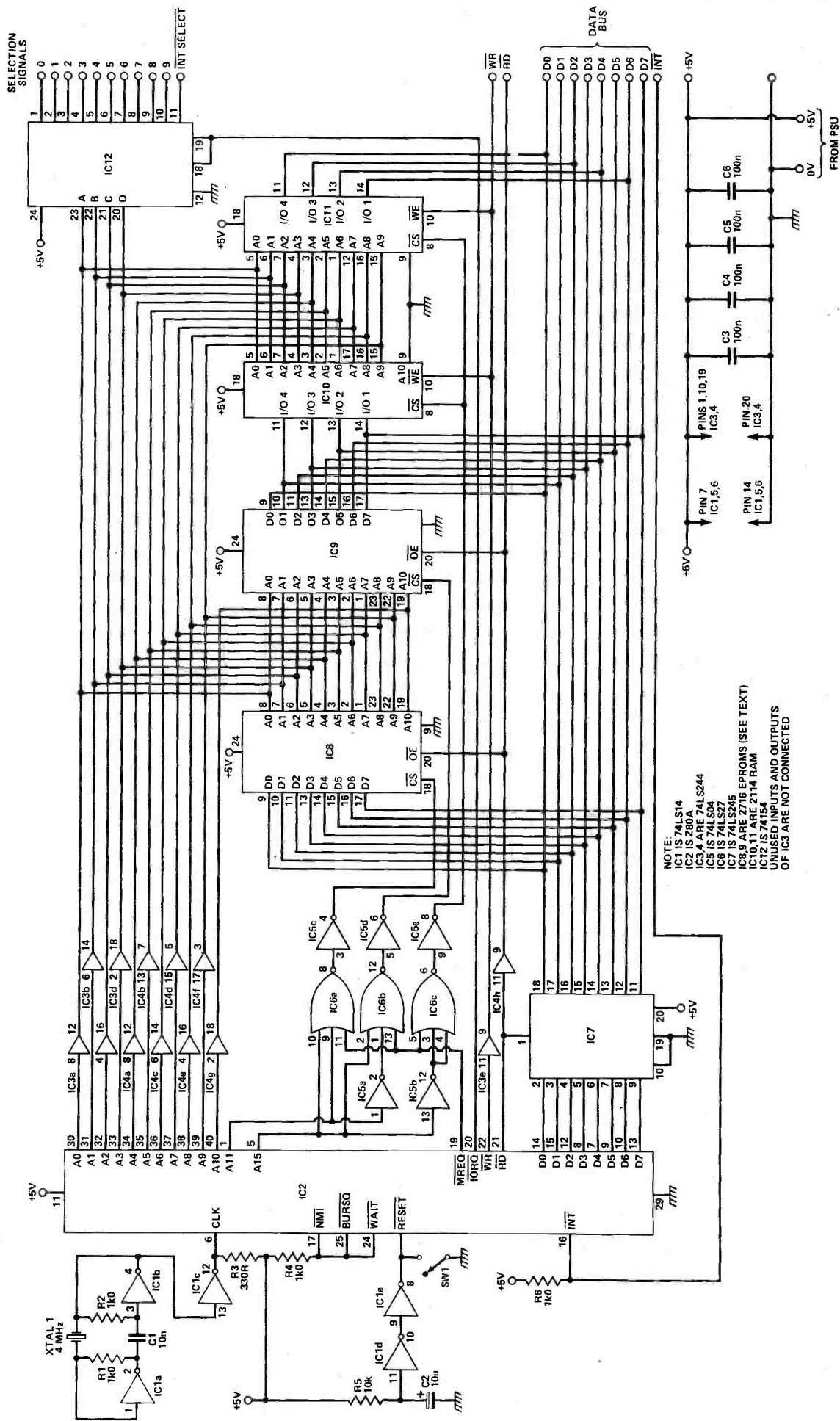
Construction

The component layout of the PCB is shown in Fig. 4. The PCB is

double sided, but as PCBs with plated through holes are expensive, pins have been used to make connections between the two sides. The PCB is difficult to make unless you have access to suitable

equipment: see Buylines for the source of the PCB. If you do make it yourself, you must be very careful to align the two sides accurately. All the holes are cut using a 0.8 mm (or approx) drill.

Fig. 2. Circuit diagram of Marvin's main board.



NOTE:
 IC1 IS 74LS14
 IC2 IS Z80A
 IC3,4 ARE 74LS244
 IC5 IS 74LS04
 IC6 IS 74LS27
 IC7 IS 74LS246
 IC8,9 ARE 2716 EPROMS (SEE TEXT)
 IC10,11 ARE 2114 RAM
 IC12 IS 74LS123
 UNUSED INPUTS AND OUTPUTS
 OF IC3 ARE NOT CONNECTED

HOW IT WORKS

Schmitt triggers IC1a and b form a standard oscillator circuit whose frequency is stabilised at 4 MHz by XTAL1; the output from this oscillator is buffered by IC1c and fed into the clock input of the Z80 CPU, IC2 (R3 is necessary to fulfil the Z80's input requirements as it has no internal pull-up resistor). NMI, BUSRQ, and WAIT inputs are not used in this design, so they are tied high by resistor R4.

At switch-on, execution would begin at a random location in the memory but for C2 (via IC1d and e) holding RESET low until voltages and internal CPU register contents stabilise. The CPU may be reset at any future time by momentarily closing SW1 (note that debouncing is unnecessary). After being

reset, the Z80 will begin by fetching an instruction from memory location 0000 hexadecimal, and executing it. Therefore, it places this address on the address bus and then takes MREQ and then RD low.

The memory selection logic, ICs 5 and 6, detects that this address is less than 07FFH and enables IC8, the EPROM containing the operating system. MARVIN then proceeds with the initialisation program in the operating system.

The address bus is buffered by most of two 74LS244s, ICs 3 and 4, and the data bus by a single 74LS245, IC7. As data can pass to and from the CPU, IC7 has to be a bidirectional device. ICs EPROMs, ICs 8 and 9, and the RAM, ICs

10 and 11 have their address and data lines permanently wired to the buses, but each has an individual selection line (CS) that takes its bus connections to a high impedance state until the selection line is pulled low by the memory selection logic.

The output enable inputs (OE) on the EPROMs are connected to RD (read) from the Z80, and the RAMs' WE (write enable) inputs are connected to WR (write).

If the MPU wants to perform an output or input operation it takes IORQ low; address lines A0 and A3 will contain (in binary, of course) the number of the port to be selected. Either RD or WR can be low, depending on whether the port is to be read from or written to.

IC12 is a four to 16 line decoder, and it's used to provide an individual selection line for each port. IC12 is active only when IORQ is low, so port boards may be selected by one of these lines and either RD and WR. Only one interrupt board is usable, so there is only one interrupt selection line, INT SELECT.

The interrupt line itself, INT, is normally held high by R3; however, it may be pulled low by a suitable external device. Because we have chosen to use INT rather than NMI (non maskable interrupt), it is possible to program MARVIN to ignore interrupts. If this has not been done, the result of pulling INT low will be to make the CPU service the interrupt according to your predesignated routine.

PARTS LIST

RESISTORS (all 1/4 W 5%)	
R1, 2, 4, 6	1k0
R3	330R
R5	10k
CAPACITORS	
C1	10n ceramic
C2	10u axial electrolytic
C3, 4, 5, 6	100n ceramic or polyester
SEMICONDUCTORS	
IC1	74LS14 or 7414
IC2	Z80A
IC3, 4	74LS244
IC5	74LS04 or 7404
IC6	74LS27 or 7427
IC7	74LS245
IC8, 9	2716 EPROM (see text)
IC10, 11	2114 RAM (300nS or less)
IC12	74154
MISCELLANEOUS	
SW1	push to make single pole switch as required
XTAL1	4 MHz crystal (see text)
IC sockets: one 40 pin, two 24 pin, two 18 pin; Veropins (about 130); PCB; edge connector if required; ribbon cable.	

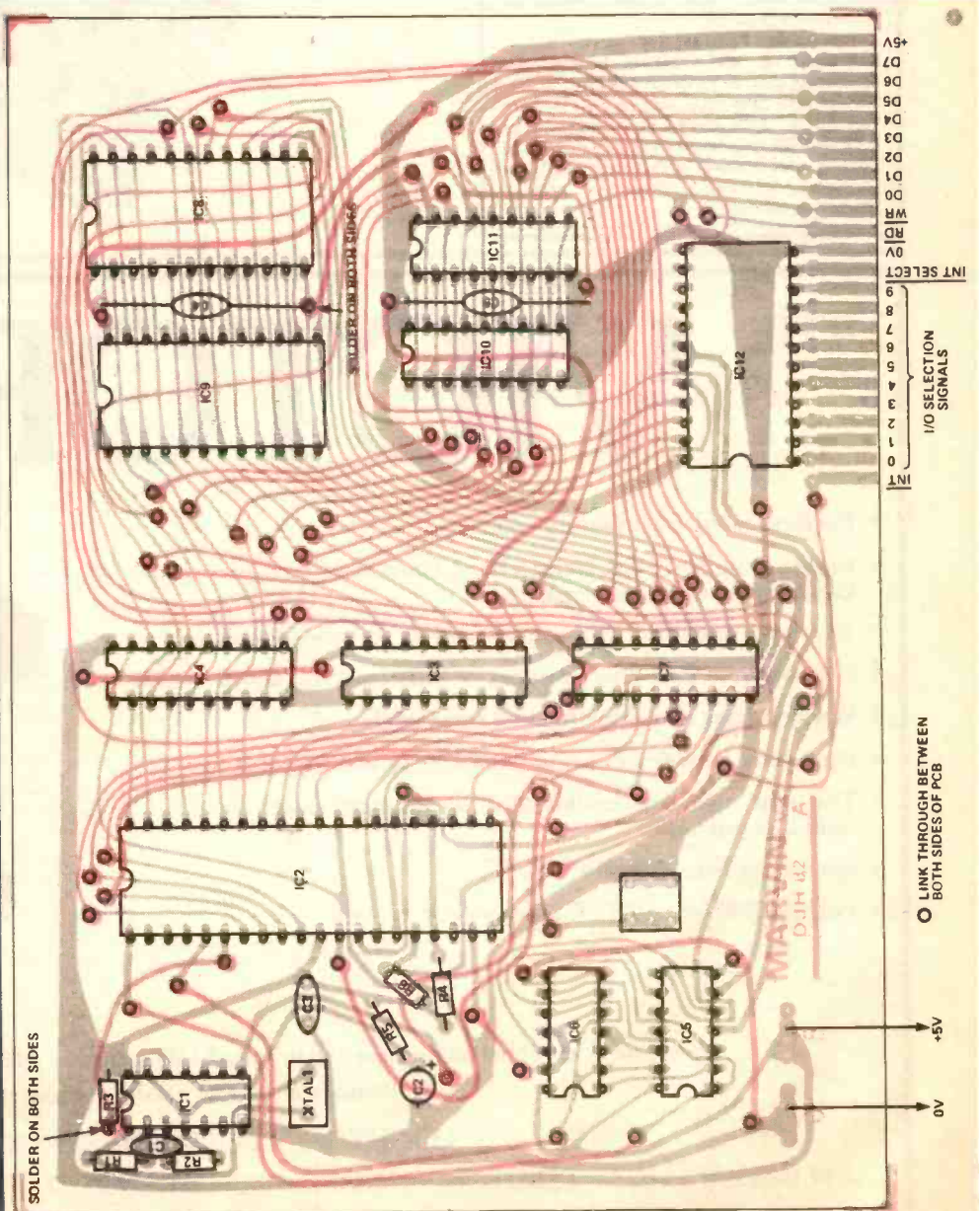


Fig. 3 Overlay diagram.

ICs 2,8,9,10,11 should be socketed as they are NMOS devices; Sockets are optional for the remaining TTL ICs, and there should be no problems in soldering them directly provided the usual precautions are observed.

To proceed with the construction, first insert and solder, on the underside only, all the TTL ICs, and the sockets for the NMOS. It is a good idea to use a fine-tipped soldering iron and to be careful to check that you do not make any bridges between tracks, especially where they pass between IC pins.

Next insert and solder the crystal, resistors and capacitors

(noting the polarity of C1). Where there are pads on both sides of the board the components' leads should be soldered to both. There will remain a large number of unused holes, and many of these are used for the pins that link tracks on both sides of the board. You can tell these holes by looking to see if there are pads on both sides of the hole: if this is the case, then you should insert a pin and solder on **both** sides.

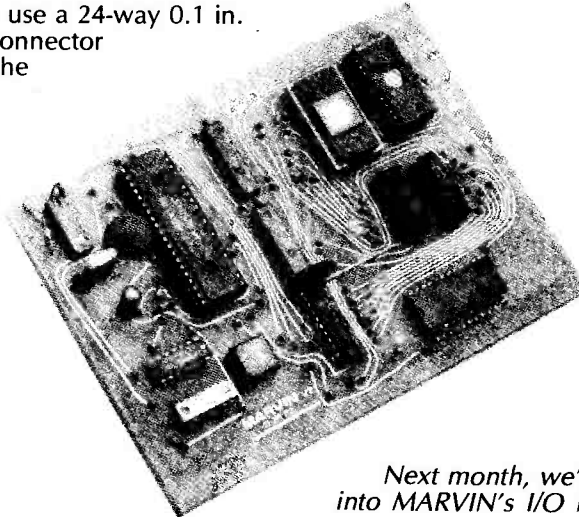
You can use a 24-way 0.1 in. pitch edge connector to connect the

board to the others; we recommend that power connections to all the boards be hard-wired to the positions provided and not taken through the connector. If you're very cost-conscious, you could hard-wire direct; holes have been provided for you to insert pins for this purpose next to the edge connector strips.

Finally, solder SW1 (reset) into position, or, if you prefer, take off wires to a control panel.

BUYLINES

The following will be available from ARK Electronics, Ashes Lane, Wentworth, Rotherham, S. Yorks S62 7TY:
EPROM containing the monitor program, 4 MHz clock, £6.00; 3 MHz (or lower) clock £4.00;
Double sided PCB, £6.00;
Complete 4 MHz kit excluding the operating system EPROM £26.00.
Please add 50p p&p and make cheques payable to ARK Electronics. Sending an SAE to ARK will secure further details of D-to-A and A-to-D converters, lighting dimmers, remote controllers and a speech synthesiser.

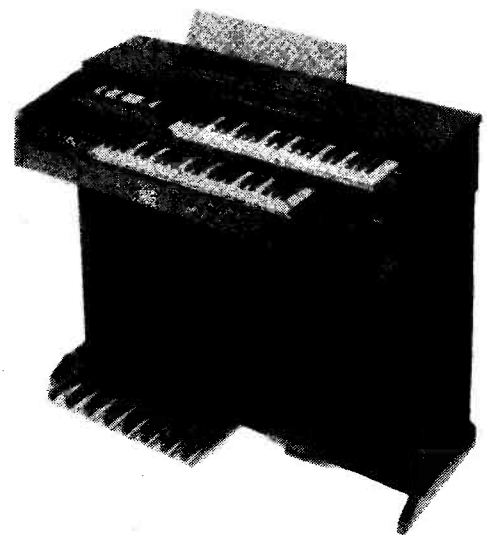


Next month, we'll be delving into MARVIN's I/O boards.

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Interak 1

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It's the oldest trick in the book to grab your attention with a stupid title, but in this case there's a grain of truth in the statement above.

The Interak 1 Computer System is a 4MHz Z80A development system, one which you build yourself, perhaps for enthusiastic home use, or more often for industrial or educational purposes.

The fundamental structure is a 3U 19" rack which has space for 13 cards ("International" size, i.e. 4.5" x 8") on 1" pitch, with space for a power supply at one end of the rack. International size — rack mounting: Inter-rak Interak!

13 cards 4.5" by 8" gives a total potential board area of over 400 square inches, enough for a couple of hundred chips or more; there's no real limit on what that could do is there? (It would leave a few of today's marvels a bit in the shade eh?)

But don't be scared, you don't have to build a Frankenstein's monster until you're ready. The first few cards are pretty straightforward: First the VDU-K, which can be connected to your own T.V. (or monitor), then the Z80A-CPU card, the brains; then dynamic RAM, and finally the Keyboard interface (to any standard parallel ASCII keyboard), and you've got a computer — with the ultimate resource: 9 empty slots for the future. (Perhaps use one of them for a 2400 baud tape interface or later floppy disks.)

Example prices (excluding VAT), everything is available separately and full after sales service in case you make a mistake: Z80A CPU card £10.95, Manual £1.50, Main Parts £13.41.

40 type-written pages of description, specification, price lists etc. are yours for the asking (a 25p stamp and/or SAE is a help, but not essential), or telephone if you prefer. You'll have to live with your computer for a long time, so make the effort and find out all about Interak now; a couple of minutes is all it takes to ask for a leaflet!

Greenbank

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7407	19p	7440	14p
7408	13p	7442	30p
7409	13p	7444	85p
7410	13p	7446	56p
7411	15p	7447	36p
7412	17p	7448	43p
7413	17p	7450	14p
7414	23p	7451	14p
7416	19p	7453	14p
7417	19p	7454	14p
7420	14p	7460	14p
7421	19p	7472	22p
7422	19p	7473	24p
		7474	19p
		7475	26p
		7476	25p
		7480	45p
		7482	86p
		7483	30p
		7485	80p
		7486	19p
		7489	180p
		7491	19p
		7491	34p
		7491	24p
		7493	24p
		7497	33p
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		74100	78p
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		74108	24p

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4000	10p	4020	42p
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4007	14p	4024	33p
4008	36p	4025	12p
4009	24p	4026	75p
4010	24p	4027	20p
4011	10p	4028	49p
4012	15p	4029	45p
4013	20p	4030	14p
4014	48p	4031	125p
4015	40p	4034	140p
4016	20p	4035	249p
4017	30p	4039	280p
4018	45p	4040	40p
4019	25p	4041	40p
		4042	38p
		4043	40p
		4044	40p
		4046	40p
		4047	35p
		4048	38p
		4049	21p
		4050	21p
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We receive a very large number of enquiries. Would prospective enquirers please note the following points:

- We undertake to do our best to answer enquiries relating to difficulties with ETI projects, in particular non-working projects, difficulties in obtaining components, and errors that you think we may have made. We do not have the resources to adapt or design projects for readers (other than for publication), nor can we predict the outcome if our projects are used beyond their specifications;

- Where a project has apparently been constructed correctly but does not work, we will need a description of its behaviour and some sensible test readings and drawings of oscillograms if appropriate. With a bit of luck, by taking these measurements you'll discover what's wrong yourself. Please do not send us any hardware (except as a gift!);

- Other than through our letters page, Read/Write, we will not reply to enquiries relating to other types of article in ETI. We may make some exceptions where the enquiry is very straightforward or where it is important to electronics as a whole;

- **We will not reply to queries that are not accompanied by an SAE** (or international reply coupon). **We are not able to answer enquiries over the telephone.** We try to answer promptly, but we receive so many enquiries that this cannot be guaranteed.

- Be brief and to the point in your enquiries. Much as we enjoy reading your opinions on world affairs, the state of the electronics industry, and so on, it doesn't help our already overloaded enquiries service to have to plough through several pages to find exactly what information you want.

Subscriptions

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Send your order and money to: ETI Subscriptions Department, 513 London Road, Thornton Heath, Surrey CR4 6AR (cheques should be made payable to ASP Ltd). Note that we run special offers on subscriptions from time to time (though usually only for UK subscriptions, sorry).

ETI should be available through newsagents, and if readers have difficulty in obtaining issues, we'd like to hear about it.

Backnumbers

Below we list the backnumbers that are available from our backnumbers department. Please note that this list will be out of date if you use an old copy of the magazine. Backnumbers cost £1.50 (UK or overseas by surface mail) and are available from: ETI Backnumbers Department, 513 London Road, Thornton Heath, Surrey CR4 6AR (cheques should be made payable to ASP Ltd).

Even if the copy of ETI you need is not listed, all may not be lost, because we run a photocopying service. For £1.50 (UK and overseas) we will photocopy an entire article (note that parts of a series of articles count as separate articles). Your request should clearly state what article you require and the month and year in which it appeared (the index for 1980 and 1981 was published in January 1982, and the index for

1982 appeared in December 1982). Send your request to ETI Photocopies, Argus Specialist Publications Ltd, 145 Charing Cross Road, London WC2H 0EE (cheques should be made out to ASP Ltd).

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Write For ETI

We are always looking for new contributors to the magazine, and we pay a competitive page rate. If you have built a project or you would like to write a feature on a topic that would interest ETI readers, let us have a description of your proposal, and we'll get back to you to say whether or not we're interested and give you you all the boring details.

We don't bother with the bureaucracy for Tech Tips — all you do is to send in your idea, stating clearly if you want an acknowledgement of receipt. If possible, please type your explanation of why the circuit is different, what it does and how it works, on a separate sheet from the circuit diagram; both sheets should carry your name, address and the circuit title. We'll let you know (within a month or so) if we want to use your Tech Tip.

Trouble With Advertisers

So far as we know, all our advertisers work hard to provide a good service to our readers. However, problems can occur, and in this event you should:

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2. Keep a copy of all correspondence.
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If you exhaust the above procedure and still do not obtain a satisfactory response from the supplier, then please drop us a line. We are not able to help directly, because basically the dispute is between you and the supplier, but a letter from us can sometimes help to get the matter sorted out. But please, don't write to us until you have taken all reasonable steps yourself to sort out the problem.

We are a member of the mail order protection scheme, and this means that, subject to certain conditions, if a supplier goes bankrupt or into liquidation between cashing your cheque and supplying the goods for which you have paid, then it may be possible for you to obtain compensation. From time to time, we publish details of the scheme near our classified ads, and you should look there for further details.

OOPS!

We have in the past published small corrections to projects on the letters page, and major corrections separately. From now on corrections will appear on this page, and will be repeated for several months (just to increase our embarrassment). If a correction is too large to fit on here, we will publish it just once, but will note the fact that a correction does exist, and that copies of it can be obtained from us provided you send in an SAE. But please — request copies only if you really do need them; if this service is abused, we may be forced to withdraw it.

ZX A to D (Jan '83)

D2 is shown the wrong way round on the overlay; wires on the RH side of the switch SW1 should go to top contacts. Some of the early PCBs had an error: pins 2 & 4 of IC1 should go to pin 16 (top) of edge connector (published foil pattern is OK).

.Stage Lighting Unit (Jan, Feb, April, May '83)

Transformer specs are as follows: Primaries all 250 V; secondaries T1: 0-6, 0-6 V, 12 VA tot; T2: 0-12, 0-12 V, 12 VA tot; T3: 0-6 V, 3 VA. ICs 34, 35, 36 are 7805 5V regulators.

ZX Sound Board Design Comp. results, Feb '83)

The first line of the program has to be entered in reverse order to get it to go in (COS, GOSUB, COPY, ASN and RND are functions). The line should read:

```
10 REM : "Y - =?COS GOSUB 5 COP  
Y ??ASN ?RND??RND
```

Alarm Module (MARCH '83)

R21 is 220k (parts list OK, circuit diagram wrong) Q5 is BC182L (left off parts list).

Max Min Thermometer (April '83)

A revised foil pattern was published in July ETI. To get original PCB to work, replace D4 and D5 with wire links, cut tracks from pins 7 and 8 on IC6, and solder 15k resistor across cut — remove ICs while doing this! (It's messy but it works.)

Real Time Clock (April '83)

Frequency of XTAL1 is 32.768 kHz.

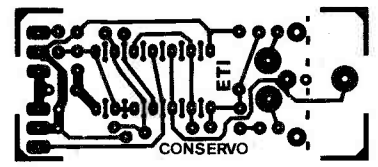
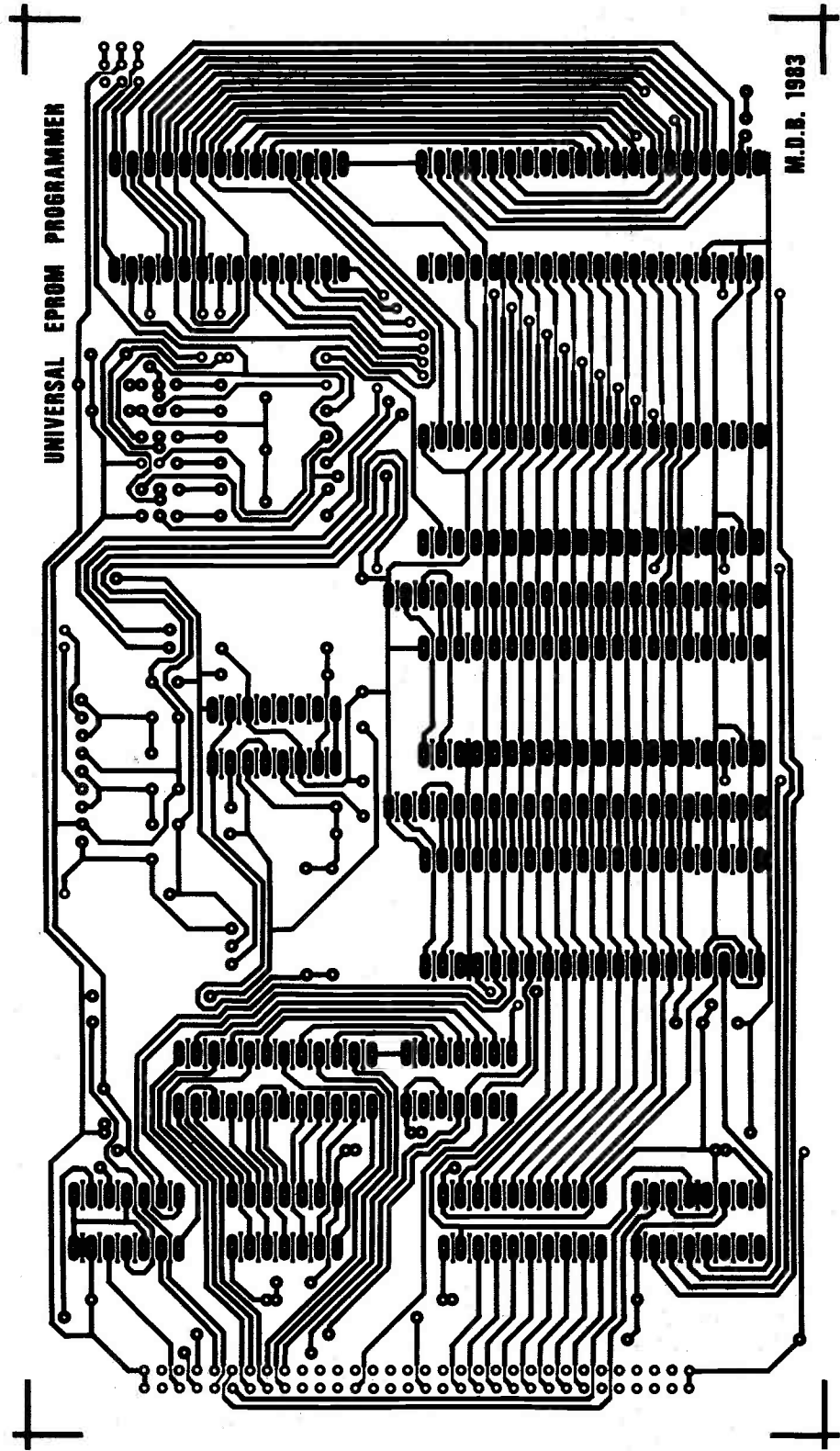
NDFL Power Amplifier (May '83)

C13 is 33p (parts list correct, circuit diagram wrong). Table 1: lengths of wire quoted do not allow for lead lengths — add 40 mm or so to them. This is particularly important for L3. Resistors R29 and R30 can be wire-wound types, it isn't necessary to use carbon types (their inductance will be small).

Flash Sequencer (July '83)

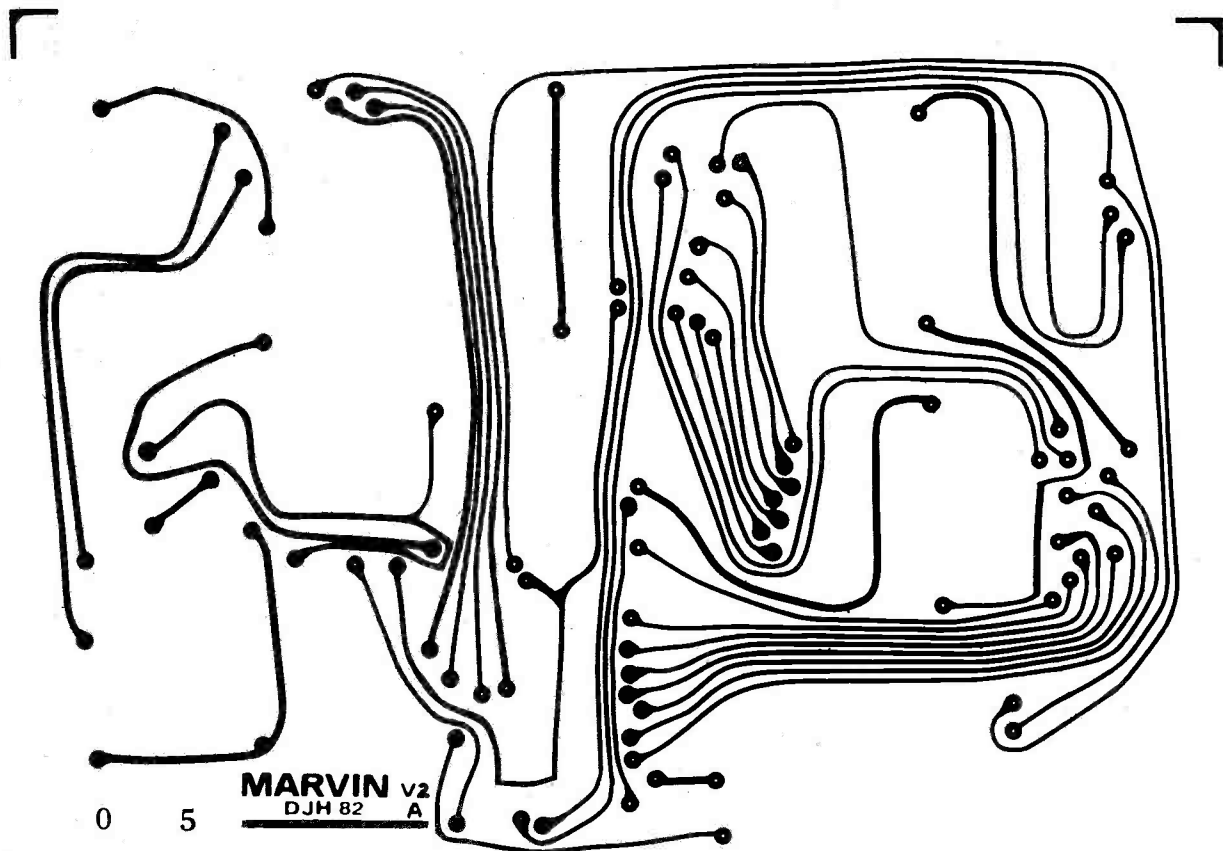
Q1 should be BC184L; Q2-5 should be BC182L.

PCB FOIL PATTERNS

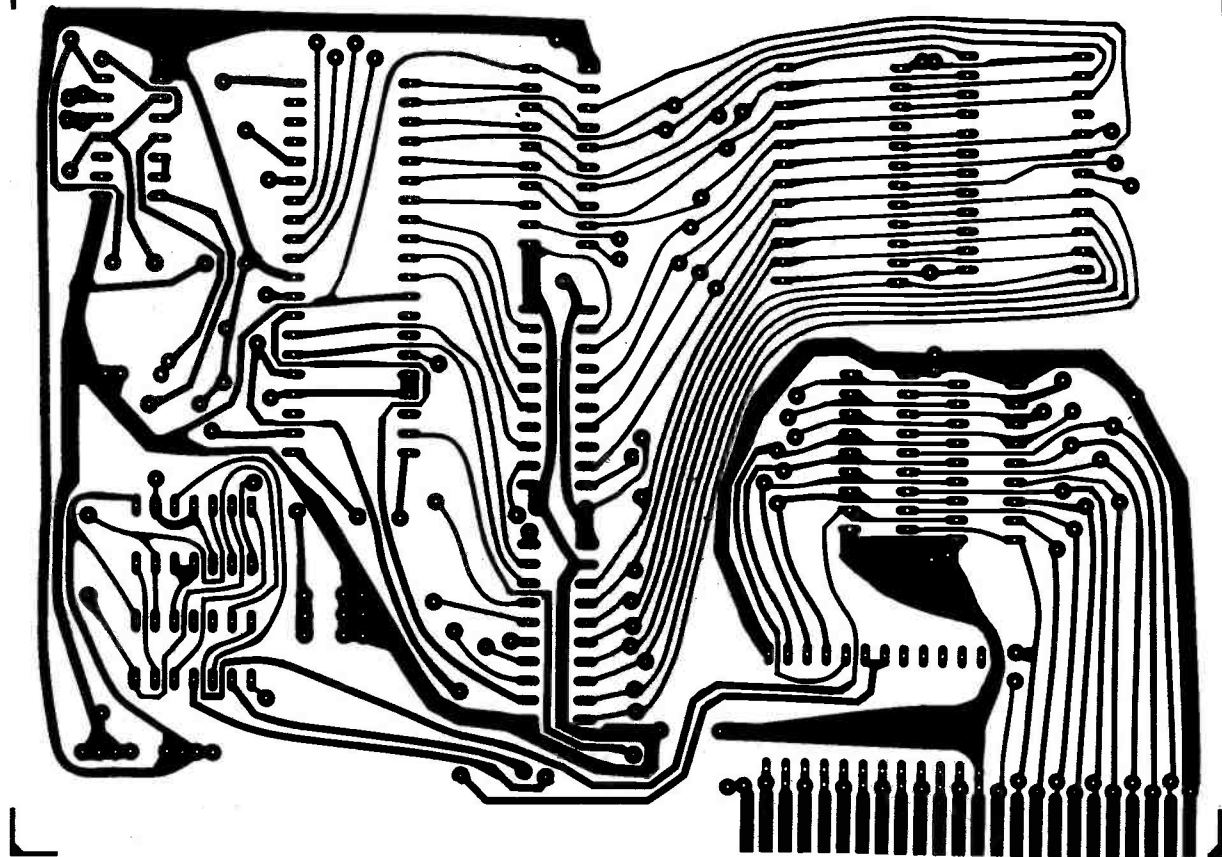


The Servo Fail-Safe

Universal EPROM Programmer



Marvin (component side)



Marvin (solder side)

HOME COMPUTERS

AQUARIUS



AQUARIUS: The brand new Aquarius Personal Computer is part of Mattel Electronics latest developments in advanced technology and offers full home computing facilities, as well as extensive game play, using a very wide range of plug in cartridges. Since Aquarius is a Mattel Electronics product, it benefits by the company's wide experience of producing high

technology equipment, as well as their game programming expertise which is evident from the advanced games which have been produced for the Intellivision. Aquarius costs £79 and comes with microsoft basic built in. It is so simple to use that you'll be writing your first programs within minutes of taking the machine out of its box. You can even record the programs on your own cassette recorder at home, so you can use them again at a later date. Most available domestic tape recorders are compatible with the Aquarius.

A POWERFUL MACHINE: For all its simplicity, it is also very sophisticated. It has a 280A processor and 8K of built in ROM as well as 4K of RAM, which is user expandable to 52K. It has a display of 40x24 characters, and a graphic resolution of 320x192 with a total character set of 256 (including the complete ASCII set with upper and lower case letters, numbers and additional graphic symbols). The keyboard has 49 full stroke moving keys, unlike some of the cheaper machines which have membrane keyboards. The size of the machine (excluding any of the additional peripherals), is 13"x6"x2".

PERIPHERALS: It is very easy to increase the capabilities of your Aquarius as all the peripherals plug straight into one another. You can add a Printer, a Modem, a Data Recorder, Mini Expander and other items. All of the peripherals are very easy to install and what is more, they're easy to use. But the best news of all is, they're easy to afford.

CPM OPERATING CAPABILITY: The Aquarius is capable of being expanded to 52K RAM and later in 1983 a disk drive will be available for it, with the commercial CPM business operating system. This will allow you access to one of the largest software libraries in the world, with literally hundreds of programs available for you to use.

CARTRIDGES: Various sophisticated programs will be launched on plug in cartridges such as a Visicalc type spreadsheet and a word processor. In addition there will be dozens of games and utilities and alternative languages such as Logo, which combined with the built in microsoft basic gives an unbeatable combination of high quality programming ability.

MATTEL AQUARIUS - £68.70 + VAT = £79

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ATARI 400/800



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ATARI 400/800: With the Atari Personal Computers, you can play the ultimate in T.V. games, teach yourself new subjects or skills, balance budgets, and even write your own computer programs in Basic.

SPECIFICATIONS: Both the Atari 400 and 800 can display in up to 16 colours, each with 16 intensities. They have four independent sound synthesizers for music tunes/game sounds, giving four octaves with variable volume and tone control on your T.V.'s speaker. The display graphics

are of amazing quality, having a detailed resolution of 320 x 192, comprising 24 lines of 40 characters. Atari personal computers have a standard 10K ROM operating system. In addition the standard Atari 400 (£149) comes with 16K of RAM, and the expanded version with 48K (£198). The Atari 800 (£299) comes with 48K as standard. Both the 400 and 800 are now supplied with a FREE £40 Basic Programming Kit, which includes the Basic Programming Cartridge, as well as a 120 page Basic Reference Manual and the 184 page Self Teaching Manual by Bill Carris called 'Inside Atari Basic', so you can begin programming straight away, without buying any 'extras'. Even a mains plug is supplied!

OVER 500 PROGRAMS AVAILABLE: The Atari computers are supported by well over 500 programs available for your use, a larger selection than you will find on any other television game or home computer! The wide selection puts Atari way ahead of the competition. Just fill in the coupon and we will be pleased to send you a full price list which gives details of our range of software available for entertainment, home education, programming and home office use. We think you'll agree when we say it's quite impressive.

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ATARI 400 48K - £172.17+VAT=£198

ATARI 800 48K - £260.00+VAT=£299

£149

COLECOVISION



THE SYSTEM: The CBS Colecovision offers new standards in video game play. The excellent graphics are well implemented with arcade titles such as Zaxxon, Lady Bug, Gorf, Wizard of Wor, Carnival, Mouse Trap and the lovable Smurfs. The console comes supplied with a three screen arcade quality version of DONKEY KONG. Parker and other companies have also announced ranges of cartridges for Colecovision, to further enhance the wide range of quality titles available for this new television games machine.

THE CONSOLE: The CBS Colecovision video games system has advanced technology which produces superlative graphics resolution and excellent sound effects. The styling of the console and hand controllers has been carefully researched; the console is designed to complement modern hi-tech equipment, and has clear features for easy operation. The hand controllers allow fingertip control via the 8 direction joystick, and feature 2 independent fire buttons. The push button keyboard is used for game selection and for game control with some cartridges. The hand controllers are detachable and are connected to six feet of telephone coil cable, storing neatly away in the console when not in use.

ATARI EXPANSION MODULE: The Atari converter module allows Atari VCS software cartridges to be played on the Colecovision console, allowing owners the freedom to purchase from the extensive range of Atari compatible cartridges. It also means that existing Atari owners can buy the CBS Colecovision games system without discarding their software library. Silica Shop offer part exchange facilities if you wish to upgrade.

TURBO EXPANSION MODULE: The Turbo Driver Expansion Module allows you to actually drive the vehicle that appears on your T.V. screen. The module consists of a steering wheel, dashboard and accelerator pedal. One hand controller is mounted on the dashboard to provide a gear change unit. The module comes complete with a Turbo Driver cartridge, the first of several cartridges to make use of the module, which provides all the action of sitting in the driving seat. This facility is unique to CBS Colecovision.

HOME COMPUTER EXPANSION MODULE: The Home Computer Module scheduled for late 1983, allows conversion of the games unit into a sophisticated Home Computer. This flexibility of design is an important feature of the CBS Colecovision System.

COLECOVISION - £127.82 + VAT = £147

£147

VECTREX



THE SYSTEM: Vectrex is a totally unique Home Arcade System, which has been exclusively designed and engineered to duplicate real arcade game play. Complete with its own monitor display, Vectrex won't cause any arguments over the use of the family's television because it has its own built in screen.

THE SCREEN: Vectrex does not use ordinary display techniques, instead it uses vector scanning to control the images on the screen. With this scanning method, the gun only updates the area of the screen that has changed, whereas a normal T.V. re-transmits the ENTIRE screen 50 times a minute. It is this that gives Vectrex its speed, and means that very little computer power is required for screen control, and the results provide very fast responding and clear images. These 'Vector Graphics' are used in several arcade games such as Asteroids and Battlezone, to give you incredibly high resolution and quality. Vectrex brings all of this from the arcade right into your living room. The Vectrex screen is capable of displaying 80 columns by 40 lines, which is significant to the extensive developments planned for the system.

EXCITING SOUNDS AND ELECTRONICS: Vectrex has an advanced microprocessor with more speed and power and exciting effects than many home video games systems.

REAL ARCADE CONTROLS: Vectrex has a unique control panel, similar to those used in many real arcade games, with 4 concave action buttons and a full 360° self centering joystick. This control panel has a 4 foot detachable cord for maximum player freedom.

REAL ARCADE GRAPHICS: Vectrex has its own 9 inch vertical screen and unlike a conventional T.V. screen, uses advanced display technology to achieve brilliant, high resolution imagery and superb game play never before possible. The Vectrex display provides special effects too, such as 3-D rotation and zooming in and out, which a regular T.V. cannot match. Using a black and white monitor, each Vectrex game comes supplied with its own coloured plastic screen overlay to add to the excitement of game play. The range of Vectrex cartridges (£21.95 each), gives a good selection of arcade games such as Berzerk, Scramble, Rip-Off and Bomber Attack. Vectrex comes complete with a fast paced 'Minestorm' game built into memory.

VECTREX: Vectrex has an advanced state-of-the-art microprocessor with more speed than other T.V. games

VECTREX - £129.57 + VAT = £149.00

£149

WHO ARE SILICA SHOP?

Silica Shop are one of the leading specialist suppliers of Video Games & Personal Computers. We consider that our service, to those who already own or to those who are interested in any products in our range, cannot be matched by any other supplier. Just look at what we have to offer:

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ATARI

ATARI VCS (2600) - THE NO 1 BRAND LEADER IN THE U.K.

ATARI: The Atari Video Computer System known as the Atari VCS or the 2600 has now become the T.V. game brand leader. In the U.K. there are over 700,000 owners of the VCS with access to a range of over 200 different plug in cartridges, each having a multitude of different variations and difficulty levels. Every system comes complete with the main console, two individual joystick controllers, a pair of paddle controllers, aerial splitter, mains adaptor and a 27 game Combat cartridge. It gives you bright crisp graphics, realistic sound effects and even specially designed circuits for the protection of your Television Set.

SECONDHAND GAMES: We currently have several secondhand Atari VCS units in stock which we are selling for only £49 (inc VAT). This price includes the Console, with Combat Cartridge and all the accessories, as well as a 12 month guarantee. **£49**
We also have stocks of several secondhand cartridges many at half price (all with 12 months guarantee). We will normally buy back secondhand units and cartridges at one third of our standard price.

EXTENSIVE CARTRIDGE RANGE: The Atari VCS is so popular that in addition to Atari's own cartridges, there are over 150 compatible cartridges, produced by at least a dozen different third party manufacturers. Silica Shop has one of the largest cartridge selections available in the U.K. Our range of over 200 titles (printed either side of this column), includes items in stock now, as well as many of the new releases for later in 1983.

SILICA ATARI CLUB: Silica Shop has over 20,000 Atari VCS club members registered on our computer. As a specialist company we are able to obtain advance information about new developments and send detailed catalogues to all of our club members, enabling them to evaluate new products before they buy. This is a totally FREE service, to receive your copies complete the coupon below.

SERVICE CENTRE: Atari International (UK) Inc has recently appointed Silica Shop as an authorised Atari Service Centre. This means that we can now service your Atari VCS or 400/800 (under guarantee if applicable), whether or not you purchased it from us.

VCS COMPUTER KEYBOARD: A keyboard will soon be launched to convert the VCS into a fully programmable home computer. For further details, join our club by completing the coupon below. We will then let you know when further information is available.

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We stock a wide range of accessories for the Atari VCS and 400/800 personal computers. The same accessories can be used on the Commodore VIC range of computers. The Wico range can also be used with the Texas Instruments computers on purchasing a special adaptor. To give you an idea of the range available, just take a look at the following list:



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ACTIVISION: Happy Trails, Pitfall, Stampede.

CBS: Blue Print, Carnival, Donkey Kong, Gorf, Mousetrap, Smurf, Solar Fox, Turbo, Venture, Wizard of War, Zaxxon.

IMAGIC: Bezer, Dracula, Ice Trek, Nova Blast, Satecracker, Swords & Serpents, Tropical Trouble, White Water.

PARKER: James Bond 007, Lord of the Rings, Popeye, Q-Bert, Spiderman, Star Wars, Super Cobra, Tutankham.

COMPUTER KEYBOARD: In July/August 1983, Mattel will be launching their new £89, 49-key computer keyboard attachment called "Lucky" which is fully programmable and has microsoft basic built in. It will transform your Master Component into a home computer. The adaptor also accepts a 6 note polyphonic music synthesiser and full size 49-key piano keyboard that will make learning music as easy as playing games. **£98**

MATTEL CONSOLE £85.22 + VAT = £98.00

VIDEO GAME CLUB

In a fast moving market like video games, it is difficult to keep up to date with all the developments that take place. With new programmes and accessories being introduced at a fast rate by several different manufacturers, it is impossible to get all the information you require from one manufacturer alone. It is for this reason, that we have set up owners clubs for the more popular video games and home computers, to keep you fully up to date with what is going on with your particular machine. As far as we know, Silica Shop are the only company to offer such clubs, but that is not surprising since we are the specialists. We currently have FREE clubs for the Atari VCS, Atari 400/800 home computers, and Mattel Intellivision. Soon we will have clubs for Colecovision, Aquarius and Vectrex. So if you own one of these machines, fill in the coupon opposite, and we will enrol you FREE OF CHARGE in the club relevant to your computer or video game.

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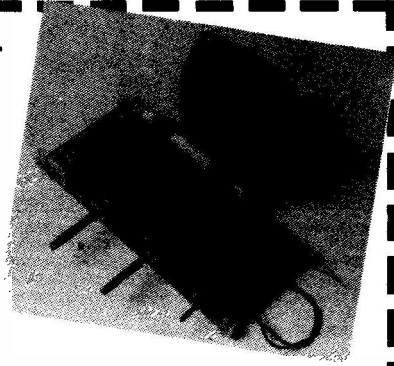
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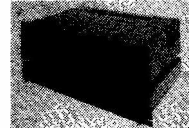
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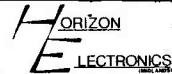
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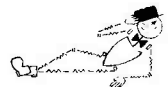
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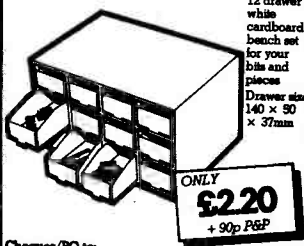
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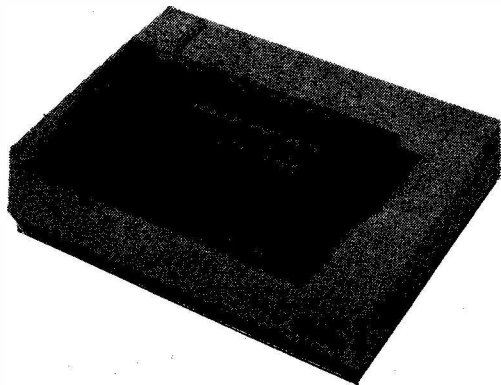
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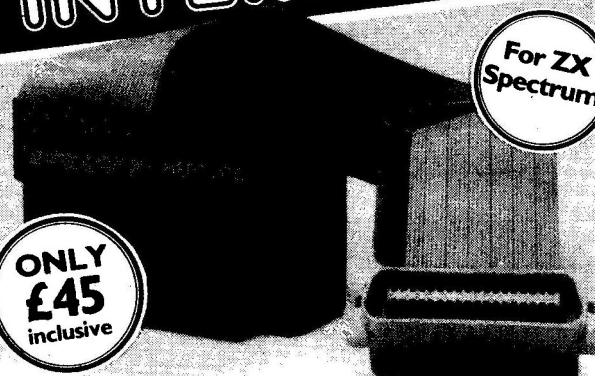
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MICROGRASP, INTERFACE BOARD AND ZX81

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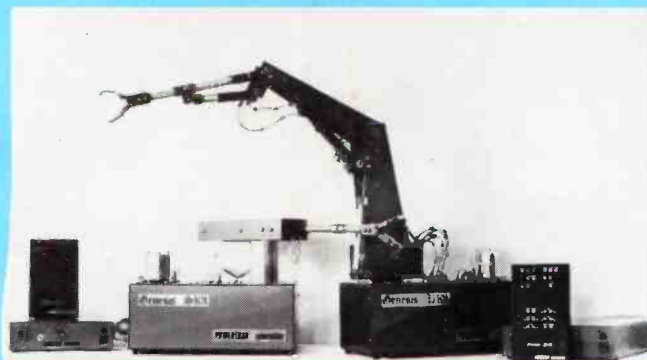
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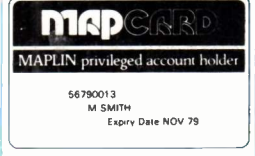
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