Florida Power
CORPORATION

INTEROFFICE CORRESPONDENCE

Nuclear Engineering Design (NED)	NA1E	3582
Office	MAC	Telephone

SUBJECT: Crystal River Unit 3
Quality Document Transmittal - Analysis/Calculation

TO: Records Management - NR2A

The following analysis/calculation package is submitted as the QA Record copy:

DOCNO (FPC DOCUMENT IDENTIFICATION NUMBER)	REV	SYSTEM(S)	TOTAL PAGES TRANSMITTED
S96-0130	0	MS	21

TITLE

Qualification of Pipe Supports MSH-13B and MSH-27B

KWDS (IDENTIFY KEYWORDS FOR LATER RETRIEVAL)

Hangers, Pipe Supports

DXREF (REFERENCES OR FILES - LIST PRIMARY FILE FIRST)

Problem Report 96-0180

M75-0012

M75-0013

VEND (VENDOR NAME)	VENDOR DOCUMENT NUMBER (DXREF)	SUPERSEDED DOCUMENTS (DXREF)
n/a	n/a	n/a

TAG

MSH-13B

MSH-27B

PART NO

COMMENTS (USAGE RESTRICTIONS, PROPRIETARY, ETC.)

NOTE:
Use Tag number only for valid tag numbers (i.e., RCV-8, SWV-34, DCH-99), otherwise; use Part number field (i.e., CSC14599, AC1459). If more space is required, write "See Attachment" and list on separate sheet.

DESIGN ENGINEER	DATE	VERIFICATION ENGINEER	DATE	SUPERVISOR, NUCLEAR ENG.	DATE
A. Glenn Rof	8/1/96	D. Boshwood	8/1/96	B. Pobrawsky	8/1/96

cc: MAR Office (If MAR Related) ☐ Yes ☒ No
Mgr. Nucl. Config. Mgt.
Mgr., Nucl. Eng. Design
(Original) w/attach

Plant Document Updates Required ☐ Yes ☒ No (If Yes, send copy of the Calculation Review form to Nuclear Licensing and a copy of the Calculation to the Responsible Organization(s) identified in Part III on the Calculation Review form.)

A/E ______________ ☐ Yes ☒ No
(If yes, Transmit w/attach)

9608140088 960807
PDR ADOCK 05000302
P PDR

RET: Life of Plant RESP: Nuclear Engineering

Florida Power Corporation

ANALYSIS/CALCULATION SUMMARY

DOCUMENT IDENTIFICATION NUMBER	DISCIPLINE	CONTROL NO	REVISION LEVEL
	S	96-0130	0

TITLE	CLASSIFICATION (CHECK ONE)
Qualification of Pipe Supports MSH-13B and MSH-27B	■ Safety Related ☐ Non Safety Related
	MAR/SP/CGWR/PEERE NUMBER: n/a
	VENDOR DOCUMENT NUMBER: n/a

	REVISION APPROVALS	ITEMS REVISED
Design Engineer	C. Glenn Pugh (signature)	Original Issue
Date	8/1/96	
Verification Engineer	D. C. Backwood (signature)	
Date/Method*	8/1/96 R	
Supervisor	A. Petrowsky (signature)	
Date	8/1/96	

*VERIFICATION METHODS: R - Design Review; A - Alternate Calculation; T - Qualification Testing

DESCRIBE BELOW IF METHOD OF VERIFICATION WAS OTHER THAN DESIGN REVIEW

PURPOSE SUMMARY

The purpose of this calculation is to provide detailed qualification calculations for pipe supports MSH-13B and MSH-27B.

RESULTS SUMMARY

Pipe supports are qualified to the piping analysis loads.

SECTION I PURPOSE:

The purpose of this calculation is to provide technical qualification of two Main Steam Pipe Supports MSH-13B and MSH-27B. This specific calculation is to supplement calculations sent to FPC by Parsons Power Group, Inc.. A copy of these calculations is included as Attachment 5 for reference.

SECTION II DESIGN INPUTS:

This calculation uses the following items as design inputs. The design loads are taken from the "Analysis of Record" for the appropriate piping system.

MSH-13B:

This hanger is located on Drawing 305-753 (Reference 1). It is part of analysis CR-6. This analysis is filed under FPC Calculation Number M75-0013 (Reference 3). The pipe support load summary sheets for this hanger list the following loads:

Deadweight: -7208 lbs.
Thermal: -2323 lbs.
Seismic: +/- 6796 lbs.

MSH-27B:

This hanger is located on Drawing 305-752 (Reference 2). It is part of analysis CR-5. This analysis is filed under FPC Calculation Number M75-0012 (Reference 4). The pipe support load summary sheets for this hanger list the following loads:

Deadweight: -6070 lbs.
Thermal: -2597 lbs.
Seismic: +/- 9892 lbs.

SECTION III ASSUMPTIONS:

Any assumptions used in this calculation will be stated in the body of the calculation. Any assumptions made will not require further action.

SECTION IV REFERENCES:

1. Drawing 305-753, Revision 1

2. Drawing 305-752, Revision 2

3. Analysis Calculation M75-0013, Revision 0

4. Analysis Calculation M75-0012, Revision 0

5. Pipe Support Drawing for MSH-13B, Revision 1

6. Pipe Support Drawing for MSH-27B, Revision 1

7. "Pipe Hangers and Supports," by Power Piping Company, Catalog 90.

8. "Manual of Steel Construction," by American Institute of Steel Construction, Seventh Edition

9. Drawing 521-212, Revision 11

10. DCN 96-217

11. "Load Capacity Data Sheets for Component Standard Supports," by Power Piping Company.

SECTION V DETAILED CALCULATIONS:

Section V.1 Design Loads:

From Section II, use the following for analysis loads:

MSH-13B:

Deadweight: -7208 lbs.
Thermal: -2323 lbs.
Seismic: +/- 6796 lbs.

Or, use 7208 + 2323 + 6796 = 16327 lbs. acting downward (applying tension load to rods). In an seismic event, the vertical seismic uplift (6796 lbs.) will not exceed the dead load on the pipe. Therefore, no uplift considerations for this hanger.

MSH-27B:

Deadweight: -6070 lbs.
Thermal: -2597 lbs.
Seismic: +/- 9892 lbs.

Or, use 6070 + 2597 + 9892 = 18559 lbs. acting downward (applying tension load to rods). In an seismic event, the vertical seismic uplift (9892 lbs.) will exceed the dead loads on the pipe by 9892 - 6070 = 3822 lbs. Therefore, this rod must be designed for uplift considerations.

For the design verification of these supports, use 19000 lbs (Faulted) as a tension load. Use 4000 lbs. (Faulted) as a compression load.

SECTION V DETAILED CALCULATIONS (Continued):

Section V.2 Hanger Component Qualification:

Both hangers have some hanger components in common. This section of the calculation will qualify the Power Piping Components. Allowable loads are taken from Reference 7. The below comparison is conservative since it compares the Normal/Upset allowable loads to the Faulted applied loads.

2" Diameter Rods:

The straight rods and the eye rods are considered to have the same allowable loads. The Power Piping Catalog lists the Normal/Upset allowable load of 20690 pounds > 19000 pounds.

Therefore, acceptable

Hanger Attachment, Figure 203:

The hanger attachment, Figure 203, has a published allowable load of 22000 pounds (using a 2" diameter bolt) > 19000 pounds.

Therefore, acceptable

Clevis

Per the Power Piping Catalog, clevises are designed to develop the full strength of the hanger rod with that used. Therefore, the Normal/Upset allowable load is 20690 pounds > 19000 pounds.

Therefore, acceptable

Turnbuckle:

The hanger drawing refers to a turnbuckle with a 12" opening. This corresponds to a Power Piping Figure 166 for 2" diameter rod. The catalog lists a Normal/Upset allowable loads of 37,200 pounds > 19000 pounds.

Therefore, acceptable

SECTION V DETAILED CALCULATIONS (Continued):

Section V.2 Hanger Component Qualification (Continued):

Pipe Clamp:

Support MSH-13B references a Power Piping Figure 224 pipe clamp. Support MSH-27B references a Power Piping Figure 225 pipe clamp.

The allowable Normal/Upset load for the Figure 224 is 16200 pounds. This is greater than the applied Normal/Upset load. The allowable faulted load is 30450 pounds. This is greater than the faulted load of 16327 for MSH-13B.

The allowable Normal/Upset load for the Figure 225 (MSH-27B) is 20600 pounds > 19000 pounds.

Therefore, acceptable

SECTION V DETAILED CALCULATIONS (Continued):

Section V.3 Weld Qualification:

Both Hanger Drawings reference a Figure 203 beam attachment. Power Piping Catalog shows this to be flat plate, 3/4" thick x 6" long.

Faulted Loads:

$Fx := 19000 \cdot lbf$

$Fy := Fx \cdot \sin(4 \cdot deg)$

$Fy = 1325.373 \cdot lbf$

$Fz := Fx \cdot \sin(4 \cdot deg)$

$Fz = 1325.373 \cdot lbf$

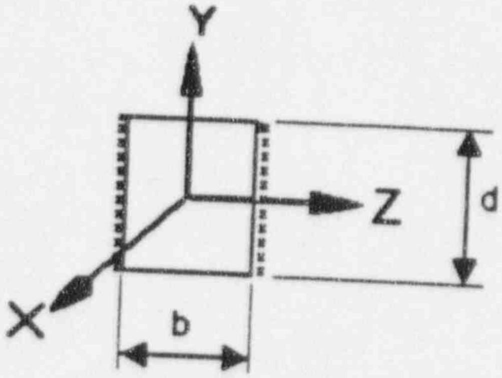
$Mx := 0 \cdot lbf \cdot in$

$My := Fz \cdot 3.5 \cdot in$

$My = 4638.806 \cdot lbf \cdot in$

$Mz := Fy \cdot 3.5 \cdot in$

$Mz = 4638.806 \cdot lbf \cdot in$



Weld Properties:

$d := 6 \cdot in$ $\quad b := .75 \cdot in$

$Aw := d \cdot 2 \cdot 1 \cdot in$ $\quad Aw = 12 \cdot in^2$ $\quad Cy := \frac{b}{2}$

$Sy := d \cdot b \cdot 1 \cdot in$ $\quad Sy = 4.5 \cdot in^3$ $\quad Cz := \frac{d}{2}$

$Sz := \frac{d^2}{3} \cdot 1 \cdot in$ $\quad Sz = 12 \cdot in^3$ $\quad Cy = 0.375 \cdot in$

$Jwx := \frac{d}{6} \cdot \left(3 \cdot b^2 + d^2\right) \cdot 1 \cdot in$ $\quad Jwx = 37.688 \cdot in^4$ $\quad Cz = 3 \cdot in$

General Weld Equation:

$$fw := \sqrt{\left(\frac{Fx}{Aw} + \frac{My}{Sy} + \frac{Mz}{Sz}\right)^2 + \left(\frac{Fy}{Aw} + Mx \cdot \frac{Cy}{Jwx}\right)^2 + \left(\frac{Fz}{Aw} + Mx \cdot \frac{Cz}{Jwx}\right)^2}$$

$$fw = 3004.809 \cdot \frac{lbf}{in^2}$$

SECTION V DETAILED CALCULATIONS (Continued):

Section V.3 Weld Qualification (Continued):

For general A-36 type material and E60 electrodes (assumed for older hangers), the controlling allowable stress will be the shear in the weld material.

$$tw := \frac{fw\cdot(1\cdot in)}{1.33\cdot 0.3\cdot 0.707\cdot 60000\cdot psi} \qquad tw = 0.178\cdot in$$

Weld symbol shown on drawings indicate a partial penetration weld with 1/8" and 1/4" prep shown. Field walkdowns show the attachments to have a fillet weld cap. The existing fillet weld with the assumed partial penetration weld exceeds the "tw" above.

Normal / Upset Loads:

$$Fx := 9531\cdot lbf$$

$$Fy := Fx\cdot \sin(4\cdot deg)$$

$$Fy = 664.849\cdot lbf$$

$$Fz := Fx\cdot \sin(4\cdot deg)$$

$$Fz = 664.849\cdot lbf$$

$$Mx := 0\cdot lbf\cdot in$$

$$My := Fz\cdot 3.5\cdot in$$

$$My = 2326.971\cdot lbf\cdot in$$

$$Mz := Fy\cdot 3.5\cdot in$$

$$Mz = 2326.971\cdot lbf\cdot in$$

General Weld Equation:

$$fw := \sqrt{\left(\frac{Fx}{Aw}+\frac{My}{Sy}+\frac{Mz}{Sz}\right)^2+\left(\frac{Fy}{Aw}+Mx\cdot\frac{Cy}{Jwx}\right)^2+\left(\frac{Fz}{Aw}+Mx\cdot\frac{Cz}{Jwx}\right)^2}$$

$$fw = 1507.307\cdot\frac{lbf}{in^2}$$

$$tw := \frac{fw\cdot(1\cdot in)}{0.30\cdot 0.707\cdot 60000\cdot psi} \qquad tw = 0.118\cdot in$$

Acceptable by comparison

SECTION V DETAILED CALCULATIONS (Continued):

Section V.4 Uplift (Compression) Check:

To check the support for the compression load, need to find the pin-to-pin length of the rod. The drawing shows a dimension of 10'-0 1/4" from centerline of pipe to bottom of beam. The hanger attachment has a 3.5" dimension from bottom of beam to bolt. From the pipe centerline to the top bolt of the clamp is 21 3/4". Therefore, use a rod length of 10'- 0 1/4" - 3 1/2" - 21 3/4" = 95". (MSH-27B)

Reference 8 gives the properties of the round rod as:

Moment of Inertia: $I = \frac{\pi \cdot (2 \cdot in)^4}{64}$ $I = 0.785 \cdot in^4$

Cross-sectional Area: $A = \frac{\pi \cdot (2 \cdot in)^2}{4}$ $A = 3.142 \cdot in^2$

Radius of Gyration: $r = \frac{2 \cdot in}{4}$ $r = 0.5 \cdot in$

Modulus of Elasticity: $E = 29000000 \cdot psi$

Length Factor: $K = 1$

Length: $L = 95 \cdot in$

Euler Buckling load is defined as:

$P = \frac{I \cdot \pi^2 \cdot E}{(K \cdot L)^2}$ $P = 24908.089 \cdot lbf$ Greater than 4000# assumed compression load

Allowable Compressive stress as defined by AISC is:

$\frac{K \cdot L}{r} = 190$

$Fa = \frac{12 \cdot \pi^2 \cdot E}{23 \cdot \left(\frac{K \cdot L}{r}\right)^2}$ $Fa = 4136.604 \cdot psi$

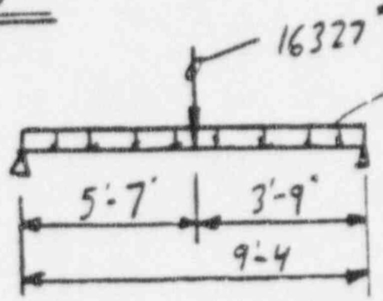
$P = Fa \cdot A$ $P = 12995.525 \cdot lbf$ Greater than 4000# assumed compression load

SECTION V DETAILED CALCULATIONS (Continued):

Section V.5 Building Steel Check:

The hanger drawing for MSH-27B shows an existing 24WF68. However, Drawing 521-212 shows this beam to be a 24WF76. This does not affect this calculation. However, this discrepancy is being resolved by DCN 96-217. Hanger MSH-13B attaches to an 12WF31. Recent walkdowns show miscellaneous conduits and smallbore pipe also attach to these structural members.

MSH-13B:



w = 31#/ft (W12x31)
\+ 100#/ft TO ACCOUNT FOR CONDUIT SUPPORT

131

R = 7171   R 10378

M_{MAX} = 37998 #-ft   FROM AISC, 7th EDITION, PAGE 2-97, w/ L_b = 9½' M_{MAX} = 72 K-ft

∴ OKAY

MSH-27B:

ACCEPTABLE BY COMPARISON

SECTION VI RESULTS/CONCLUSIONS:

The detailed calculations show the pipe supports, MSH-13B and MSH-27B, to be qualified to the design loads.

SECTION VII ATTACHMENTS:

Attachment 1: Copy of Pipe Support Drawing MSH-13B for reference, one page.

Attachment 2: Copy of Pipe Support Drawing MSH-27B for reference, one page.

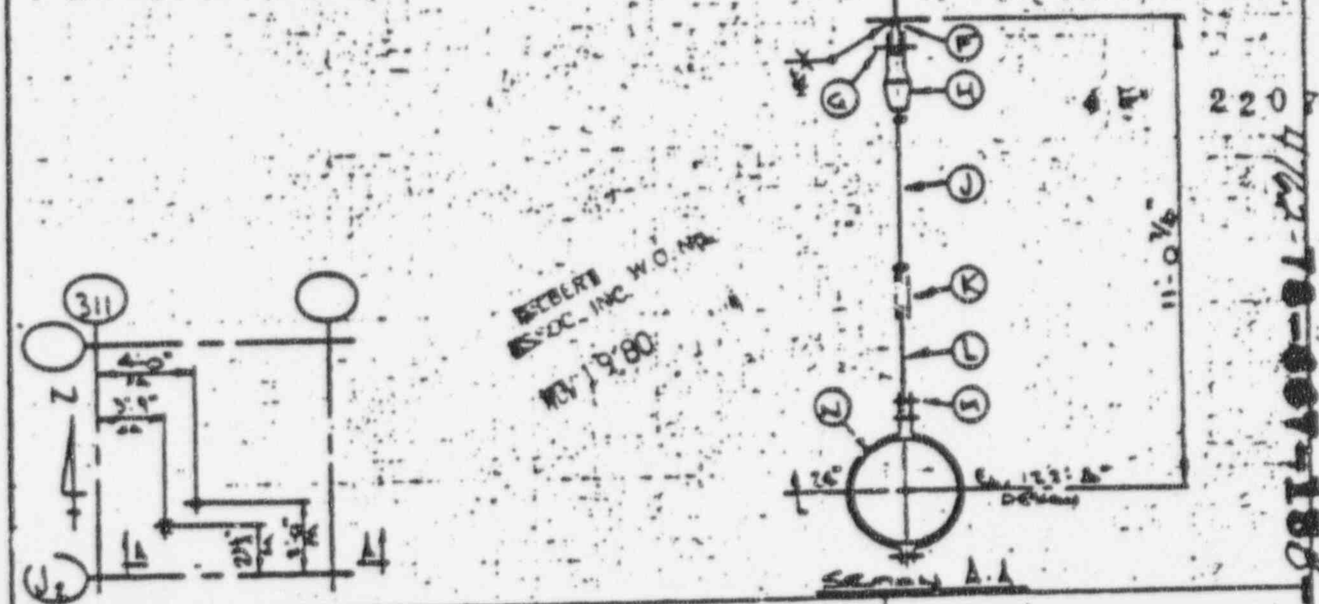
Attachment 3: Copy of pipe support load summary sheet from M75-0012 for MSH-27B, one page.

Attachment 4: Copy of pipe support load summary sheet from M75-0013 for MSH-13B, one page.

Attachment 5: Copy of existing calculations of MSH-13B and MSH-27B as found by Parson Power Group, Inc., five pages.

POWER PIPING COMPANY PITTSBURGH, PA. 15233	FLORIDA POWER CORPORATION CRYSTAL RIVER - UNIT #3 P.O. PR3-1403

FIELD NOTE:
1. THIS SHT. REPLACES MK. NO. MSH-13 SHT. NO. 39045 AND MSH-13 SHT. NO. 39043 MK. NO. MSH-13A SHT. NO. 39012



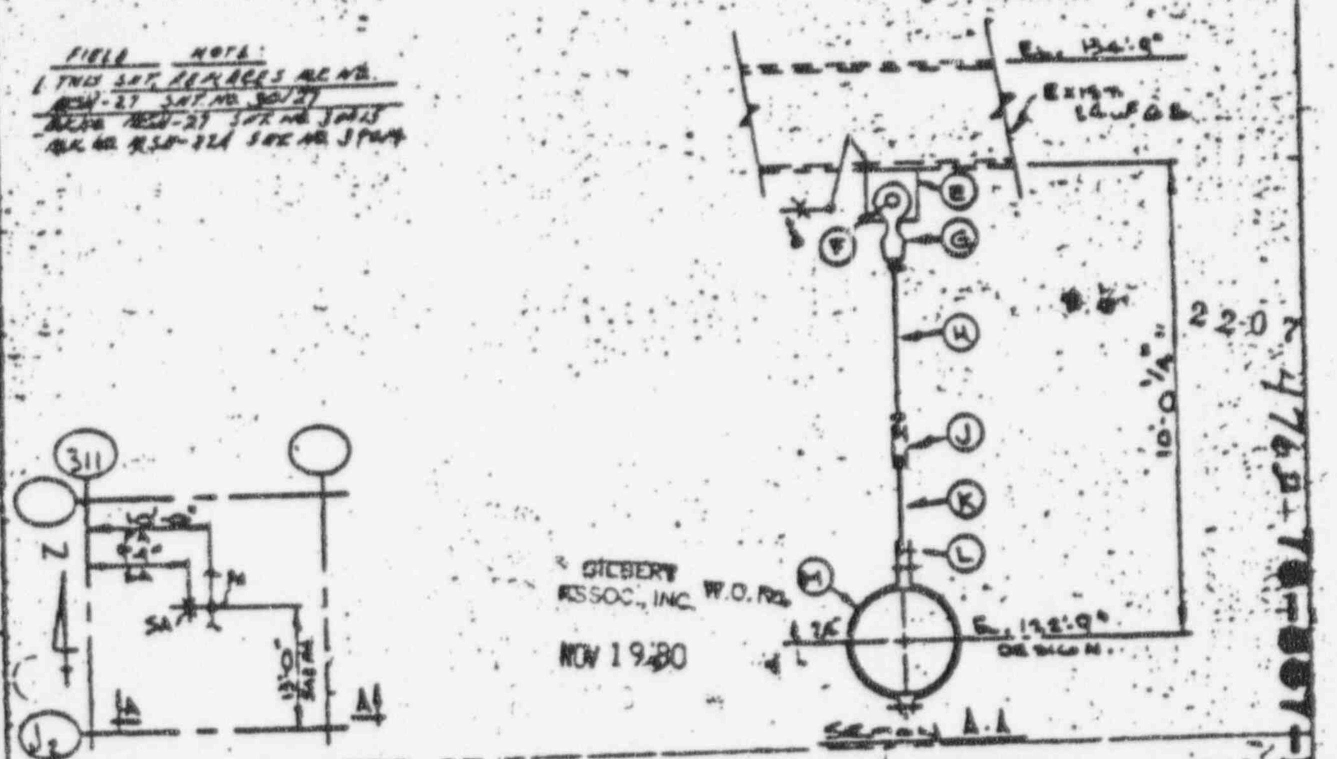
MK.		MAIN STEAM	REQD. MK	MSH-13B
○	QUAN.	[X] INSPECTION [ ] HOT & COLD DWG. [ ] SPECIAL PAINT	ASTM	MFG
F	1	2" HGR. ATTACH. R. FIG. 20A - DRILL 2 1/16" ϕ	575	
G	1	2" ϕ x 8 1/2" LG. ALLOY STUD w/ 2 HVY. & 3 1/8" THD. EA. END	193/194	MF-348
H	1	#5 CLEVIS TAP. 2" PIN HOLE - 2 1/16" ϕ GRIP. 1 1/4"		
J	1	2" ϕ ROD x 4'-9" LG. w/ 12" THD. & LH EA. END	575	
K	1	2" TURNBUCKLE x 12" OPENING		
L	1	2" ϕ EYEROD x 3'-0" LG. w/ 12" LH. THD. DRILL 2 1/16" ϕ	575	
M	3	2" ϕ x 10 1/2" LG. ALLOY STUD w/ 2 HVY. & 3 1/2" THD. EA. END	193/194	MF-348
N	1	24" SPECIAL PIPE CLAMP FIG. 224 (LESS TOP		
		BOLT & DRILL TOP BOLT HOLE 2 1/16" ϕ WT. 222#		
	1	DRAWING		
	1	ASSEMBLY		

Attachment 1
Analysis/Calculation
S96-0130, Rev. 0
Page 1 of 1

REF. DWG. HD-306-013 Rel. 2	D GAT	R RL	C KSM		ISSUE
REVISIONS 1. AS BUILT PER MAR 791271 GEC	REL. DATE	OCT 03 1975		AUTH 3926-N	
ES	PROJ. ENGR.	LENCZEWSKI		SHEET 39036	REV. 1

POWER PIPING COMPANY
PITTSBURGH, PA. 15233

FLORIDA POWER CORPORATION
CRYSTAL RIVER - UNIT #3
P. O. PR3-1403



REQD. BY: MSH-27B

MAIN STEAM

MK	QUAN.	X INSPECTION / HOT & COLD NO / SPECIAL PAINT	ASTM	MRS
E	1	2" Hgr. Attach. ... 2 1/16" ø	575	
F	1	2" ø x 8 1/2" Lg. Alloy Stud w/(2) Hvy. ... Thd. Ea. End	193/B16	
G	1	#5 Clevis Tap 2" ... Grip 1 1/4"		
H	1	2" ø Rod x 3'-11" Lg. w/ 12" Thd. & Hvy. Ea. End	575	
J	1	2" Turnbuckle x 12" Opening		
K	1	2" ø x 3'-0" Lg. Eyerod w/ 12" L.H. Thd. ...	575	
L	1	1 1/2" ø x ... Lg. Alloy Stud w/(2) Hvy. ... Thd. Ea. End	193/B16	
M	1	24" Special Rod Clamp Fig. 225 (Less Top		
		Bolt) Drill Top Bolt Hole 2 5/16" ø Wt.=300#		

	1	Drawing
	1	Assembly

Attachment 2
Analysis/Calculation
S96-0130, Rev. 0
Page 1 of 1

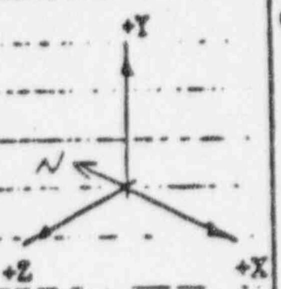
REF. DWG. HD-304-027 Rev. 2
REVISIONS REV. 1 AS BUILT PER ... 70-12-71

REL. DATE OCT 03 1975
CHKD. ENGR. LEWCZEWSKI
AUTH. 3326-W
SHEET 39037
REV. 1

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT Florida Power Corporation	Page 7 of 17
	PROJECT Crystal River Unit #3	W.O. 04-4203-C71
SYSTEM MS		ORIGINATOR [illegible] DATE 5-2-74
CALCULATION FOR CR - 5A Pipe Supports		REVIEWER S Fernandez DATE 1/7/75

Comments

Note: All loads act on pipe.
Positive directions are shown here.



ANALYSIS/CALCULATION
DOC ID M-75-0017 ATT 0
REV 0 SHEET 20 OF 27

Mk. No.	analysis	Mx	My	Mz	Fx	Fy	Fz
MSH-27	deadload					5070	
Sheet No.	seismic					9802	
30127	thermal					2597	
Type	calc. load (+)					15559	
[illegible]	allow. load (+)						
Analysis	calc. load (-)					-[illegible]	
point HO	allow. load (-)						

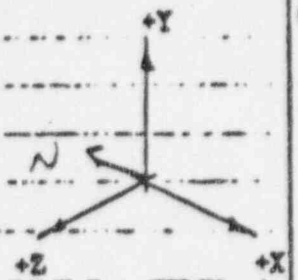
Mk. No.	analysis	Mx	My	Mz	Fx	Fy	Fz
[illegible]	deadload					0	0
Sheet No.	seismic					2174	5302
30112 1	thermal					0	0
Type	calc. load (+)					2174	5302
[illegible]	allow. load (+)						
Analysis	calc. load (-)					-2174	-5302
point (HP) PP	allow. load (-)						

Mk. No.	analysis	Mx	My	Mz	Fx	Fy	Fz
MSH-21[illegible]	deadload					18616	
Sheet No.	seismic					5240	
	thermal					-1569	
Type	calc. load (+)					25856	
Rigid	allow. load (+)						
Analysis	calc. load (-)						
point HQ	allow. load (-)						

Attachment 3
Analysis/Calculation
S96-0130, Rev. 0
Page 1 of 1

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT Florida Power Corporation	Page 7 of 16
	PROJECT Crystal River Unit #3	W.O. 04-4203-C71
SYSTEM MS		ORIGINATOR [illegible] DATE 4/2/74
CALCULATION FOR CR - 6B Pipe Supports		REVIEWER S Ferrarello DATE 1/4/75

Note: All loads act on pipe.
Positive directions are shown here.



~~ANALYSIS/CALCULATION DOC ID [illegible] ATT REV 0 SHEET 19 OF [illegible]~~

Comments

Mk. No.	analysis	Mx	My	Mz	Fx	Fy	Fz
MSH-12	deadload					2549	
Sheet No.	seismic					2[illegible]	
[illegible]	thermal					0	
Type	calc. load (+)					[illegible]571	
S[illegible]	allow. load (+)						
Analysis	calc. load (-)					—	
point HQ	allow. load (-)						

Mk. No.	analysis	Mx	My	Mz	Fx	Fy	Fz
[illegible]-227	deadload				0		
Sheet No.	seismic				[illegible]		
	thermal				0		
Type	calc. load (+)				10262		
H[illegible]	allow. load (+)						
Analysis	calc. load (-)				-10262		
point HP	allow. load (-)						

Mk. No.	analysis	Mx	My	Mz	Fx	Fy	Fz
MSH-13	deadload					7208	
Sheet No.	seismic					6796	
	thermal					2323	
Type	calc. load (+)					16327	
Rigid	allow. load (+)						
Analysis	calc. load (-)					—	
point H3	allow. load (-)						

Attachment 4
Analysis/Calculation
S96-0130, Rev. 0
Page 1 of 1

Gilbert/Commonwealth ENGINEERS/CONSULTANTS CALCULATION	SUBJECT FIT/CR03 POTENTIAL EFFECTS OF OTSG OVERFILL		IDENTIFIER 5500-035-MS-13	PAGE 1 OF 3 PAGES
	REV. 0	1	2	3
	MICROFILMED			
	ORIGINATOR T. BYRNE			
	DATE 6-26-85			

NUCLEAR SAFETY RELATED

MK. NO. W.O. 04-5500-035
MSH-013B

1.0) OBJECTIVE
EVALUATE PIPE SUPPORT FOR EFFECTS FROM OTSG OVERFILL

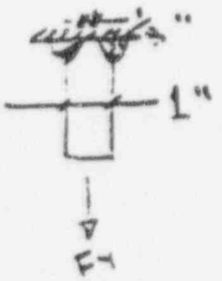
2.0) DESIGN LOAD (ANALYSIS CR-6)
OWT = +0/- 24911# THER. = +0/- 2323#
TOTAL = +0/- 27234#
USE FAULTED ALLOWABLES.

3.0)

COMPONENTS	ACTUAL	≤	ALLOW.**
¾" HGR. ATTACH R (203)	27234	≤	44000#
#5 CLEVIS (161)	27234	≤	41260#
2"Φ ROD (61)	27234	≤	41260#
2" TURNBUCKLE	27234	≤	41260#
2"Φ EYEROD	27234	≤	41260#
24" PIPE CLAMP (224)	27234	≤	30450#

** USE FAULTED ALLOW. FROM POWER PIPING NF CATALOG

4.0) WELD (PART 203)



$F_Y = 27234^{\#}$
$A_W = 14"$
$W = .875"$

$$f = \frac{F_Y}{A_W} = 1945\ \#/in$$

$$\sigma = \frac{f}{.707W} = \frac{1945}{.707(.875)} = 3145\ PSI$$

∴ OK

=========================
Attachment 5
Analysis/Calculation
S96-0130, Rev. 0
Page 1 of 5
=========================

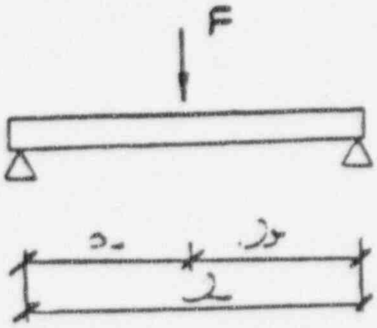
NUCLEAR SAFETY RELATED

Mk. No
MSH-0138

W.O. 09-5200-035

5.0) Spring Constant
W12 x 31

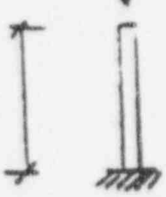
$a = 67.25"$
$b = 45.5"$
$l = 112.75"$



Properties
For Beam See
Std. Calc. = S-SC1-212
$E = 27.7 \times 10^6$ PSI
$I = 238$ IN^4
$S = 39.5$ IN^3

$$K_1 = \frac{3EIl}{a^2 b^2} = \frac{3(27.7\times10^6)(238)112.75}{67.25^2 (45.5)^2} = 238170 \text{ LBS/IN}$$

2" φ Rod



$l = 122"$
$A = \pi r^2 = \pi 1^2 = 3.14$ IN^2
$E = 27.7 \times 10^6$ PSI

$$K_2 = \frac{AE}{l} = \frac{3.14(27.7\times10^6)}{122} = 712934 \text{ LBS/IN}$$

Combine K's

$$K = \frac{1}{\frac{1}{K_1} + \frac{1}{K_2}} = \frac{1}{\frac{1}{238170} + \frac{1}{712934}} = 1.8 \times 10^5 \text{ LBS/IN}$$

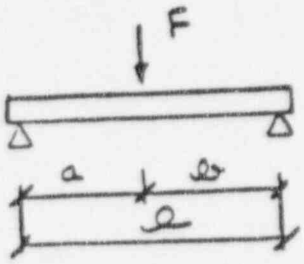
========================
Attachment 5
Analysis/Calculation
S96-0130, Rev. 0
Page 2 of 5
========================

NUCLEAR SAFETY RELATED

MK. NO
MSH-013B

W.O. 04-5500-035

6.0) W12×31



F = 27234#
a = 67.25"
b = 45.5"
l = 112.75"

PROPERTIES
I = 239. IN^4
S = 39.5 IN^3

$$M_{max} = \frac{F a b}{l} = \frac{27234(67.25)(45.5)}{112.75} = 739092 \text{ \#IN}$$

$$\sigma = \frac{M}{S} = \frac{739092}{39.5} = 18711 \text{ PSI} \leq 21600 \text{ PSI}$$

∴ OK

7.0) CONCLUSION
SUPPORT OK FOR OTSG OVERFILL.

Attachment 5
Analysis/Calculation
S96-0130, Rev. 0
Page 3 of 5

Gilbert/Commonwealth ENGINEERS/CONSULTANTS CALCULATION	SUBJECT FPC/CR#3 Potential Effects of OTSG Overfill			IDENTIFIER 5530-033-MS-27	PAGE 1 OF 1 PAGES
	REV. 0	1	2	3	
	MICROFILMED				
	ORIGINATOR T. BYRNE				
	DATE 6-25-85				

NUCLEAR SAFETY RELATED

MK. No: MSH-027B

W.O. C4-5530-0[illegible]

1.0) OBJECTIVE

EVALUATE PIPE SUPPORT FOR EFFECTS FROM OTSG OVERFILL

2.0) DESIGN LOAD (ANALYSIS [illegible])

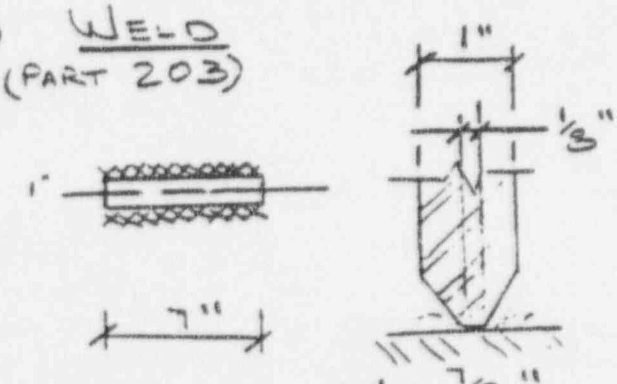
DWT + THER. = -26081 #

USE FAULTED ALLOWABLES FROM POWER PIPING'S NF CATALOG

3.0) COMPONENTS

	ACTUAL	≤	ALLOW.
2" HGR. ATTACH. R (203)	26081	≤	44000 #
#5 CLEVIS (161)	26081	≤	41260 #
2" ϕ ROD (81)	26081	≤	41260 #
2" ϕ TURNBUCKLE	26081	≤	41260 #
2" ϕ EYEROD	26081	≤	41260 #
24" ϕ PIPE CLAMP (223)	26081	≤	38730 #

4.0) WELD (PART 203)



$F_Y = 26081$ #

$A_W = 14$"

$f = \frac{F_Y}{A_W} = 1863$ #/IN

$\sigma = \frac{f}{.707 w} = \frac{1863}{.707(.875)} =$

$= 3011$ PSI

5.0) CONCLUSION

SUPPORT OK [illegible] NORMAL ALLOWABLES.

Attachment 5
Analysis/Calculation
S96-0130, Rev. 0
Page 4 of 5

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT FLORIDA POWER CORPORATION PROJECT CRYSTAL RIVER UNIT #3	FILING CODE 3? MSH-2? W.O. 4203 PAGE 1 of 1
SYSTEM Main Steam		ORIGINATOR DATE
CALCULATION FOR MSH-27		REVIEWER B Stevens DATE 6-19-74

RIGID ROD WITH COMPRESIVE LOAD

ROD IS 10 FT LONG $d = 2"$

$$P_{CR} = \frac{\pi^2 EI}{L^2}$$

$$I = \frac{\pi d^4}{64} = .049 d^4 = .784$$

$$f_{CR} = \frac{(3.14)^2(29,000,000)(.784)}{122^2}$$

$$f_{CR} = \frac{(9.8596)(29,000,000)(.784)}{14,884} = 15,060.995 \text{*}$$

TENSION

$$S = \frac{P}{A} =$$

$$9000 = \frac{P}{3.1416}$$

$P = 28,274.4$ *

USE 2" DIA ROD

RESULTS

Attachment 5
Analysis/Calculation
S96-0130, Rev. 0
Page 5 of 5

Pipe Stress Analysis Specification

Basic Guideline for the design of piping has been the Code for Pressure Piping B31.1.0-1967 and those portions of Code Case N7. In accordance with this code, Deadweight/Pressure, Thermal, Seismic and any additional transient type of loading must be considered.

The original design methodology used GAI Topical Report No. 1729, "Dynamic Analysis of Vital Piping Systems Subjected to Seismic Motion" as a guideline. A copy of this guideline is attached to this document. For all new or revised piping analyses completed today, Piping Analysis Design Guide MDG-1 is followed as a guideline.

Design Basis Loading Conditions for Main Steam System

Requirement Outline - R.O. 2891 and Enhanced Design Basis Document (EDBD) - Section 6/10

Design Pressure = 1050 psi
Operating Temperature= 590 degrees F

Seismic Input - Reference: Environmental and Seismic Qualification Program Manual (ESQPM) - Section 5

The response spectra used in the analysis was Curve CRW2. This curve is a response spectra that was developed for analysis of piping supported by the Reactor Building Shell at Elevation 123.00. Response spectra, CRW2, was used since a significant portion of the mass of this system, in particular the relief valves, will be directly accelerated by the Reactor Building Shell and it was felt that it was a more conservative response spectra curve than the ground response curve due to the two peaks which occur at 4 to 5 Hz and 14 to 18 Hz.

While this curve is not contained in the ESQPM, it was developed using the same methodology as the original curves. Response curve CRW2 utilized lower margins to envelop the derived response spectra in peak regions of amplifications when compared to the base curve, CR-R2, which is contained in the ESQPM as Figure 2.

Seismic response spectra were developed using the response spectrum method. The inherent conservatism of the response spectrum method is discussed in FSAR Section 5.4.5.1 and demonstrated in FSAR Figure 5-29 and 5-30.

Design Basis Loading Conditions for Main Steam System (cont'd)

As documented in the FSAR, period domain broading of the response spectra was implemented on the analytical derived curves to establish "design envelope" values. Conservatively, additional acceleration value enveloping was applied in the regions of amplified response. The magnitude of margin between the analytical derived peak acceleration and the "design envelope" value was established at the judgement of the senior engineer tasked with development of the response curves. Specific margin amplification percentage varies from building to building and level to level within a given structure. The implied basis for this variable was to provide additional conservatism to the CR3 design, since typically seismic design conditions did not govern CR3 design.

Based upon review of original design documentation, Curve CRW2 was established specifically for the piping analysis of containment anchored piping in the intermediate building. The period domain broading of CRW2 is identical to the basic design envelop, CRR2. The acceleration amplitude margin was reduced to a minimum of 5% above the analytical derived acceleration value

Analysis Criteria and Methodology

During the original design of CR3, those piping systems which required computer analyses were analyzed on main frame program - "Pipe Stress Analysis - M003".

Various computer analyses were completed on safety related systems. For the Main Steam system, a deadweight, thermal, seismic, safety valve discharge loading were all computer analyzed. For steam hammer, a simplified, conservative, manual calculation was performed to document this loading condition.

The deadweight/longitudinal pressure analysis was completed with the supports placed at specified locations based on field information. This analysis checked the deadweight/pressure stress and this value was compared to the B31.1 Code allowable of Sh.

Using the same field supplied support information, the thermal analysis was completed to insure that all code allowables were met. The thermal stress value was compared to the B31.1 Code Allowable of Sa. Where required, the Maximum Seismic Anchor Movement Stress was included with the thermal stress.

Analysis Criteria and Methodology (cont'd)

Upon completion of successful deadweight and thermal analyses, the seismic (and transient loadings, if any) analysis was performed to insure code allowables were not exceeded. Snubbers and other necessary restraints were added to the system to control the seismic loadings. The combined primary stresses produced by the MHE (0.10g horizontal ground acceleration) are maintained at less than or equal to 120% of the code allowable stresses from ANSI B31.1.0-1967, plus code case N-7 for duration up to 1% of the operating period.

To obtain the Operating Basis Earthquake (OBE) stress levels and support loadings, the seismic analysis involved choosing the appropriate response spectrum curve and analyzing a two dimensional earthquake (i.e. x-y quake and a y-z quake). The loadings and stresses from this analysis were then doubled to obtain the Safe Shutdown Earthquake (SSE) values. The results of these two separate earthquakes were reviewed and the largest values (stresses and support loads) were documented. The seismic stresses were then combined with the deadweight/pressure stresses and compared a code allowable of 1.2 Sh. This is a very conservative allowable whereas, methodology that is used for a plant in a comparable time frame compares the OBE stress levels to 1.2 Sh and the SSE stress levels to 1.8 Sh (Reference ASME Section III, Subsection NC, 1971 through Winter 1973 Addenda). Upon successful completion of the seismic analysis, the deadweight and thermal analyses were again analyzed if seismic restraints, other than snubbers were added to the system.

It should be noted, piping analysis CR-5 modeled a significant portion of the non-safety, Seismic Class S-III main piping run from the class break to the Turbine connection. This was done for overlap purposes to determine the effects the non-safety piping had on the safety related piping. Regulatory Guide 1.29, Section C.3 states the following:

> "Seismic Category I <u>design</u> requirements should extend to the first seismic restraint beyond the defined boundaries. Those portions of structures, systems, or components that form interfaces between Seismic Category and non-Seismic Category I features should be <u>designed</u> to Seismic Category I requirements."

Analysis Criteria and Methodology (cont'd)

The non-safety supports after the class break have been designed accounting for the seismic loadings. Therefore, the intent of Regulatory Guide 1.29 has been met. Various flow transients were required to be analyzed to account for any other type of dynamic loading in nature. For the Main Steam Line those analyses included Relief (Safety) Valve Discharge and Steam Hammer.

Relief Valve Discharge forces were originally documented by manual calculations and were then subsequently backed-up by computer generated results. The stress results of this analysis were combined with the deadweight/pressure and SSE stress levels and compared to 1.2 Sh. A copy of the manual calculations has been included with this document.

Also as a part of the safety valve analyses, the movements of the Main Steam Safety Valves relative to the discharge piping were calculated to assist in the design of the flexonic connections at the valve/piping interface. A copy of the manual calculations documenting these movements is included with this document.

The steam hammer analysis for this piping system was a simplified, conservative, manual calculation that provided the necessary documentation that when valve closure did occur, the system would be capable of withstanding any unbalanced forces that was created by the pressure wave traveling through the pipe. During this calculation, the seismic restraints (snubbers/rigid supports) were considered the main restraints in the piping system. Rod supports were only considered active in the vertical downward direction. A copy of the Steam Hammer Analysis by MZ Lee dated 11/2/73 is attached to this document.

The final phase of the design for the Main Steam piping system was visual observation during functional testing and during Initial Operation. For the Main Steam system one of the most critical loading conditions was the observation of a Turbine Trip. The final results of the steam hammer visual inspection was quite favorable. A few supports did require minor modifications; however, in general the system responded favorably and was capable of withstanding all loadings. A copy of the Report entitled "Main Steam and Feedwater - Steam Hammer Observations and Instrumentation" dated May 31, 1977 covering the observations and instrumentation has been attached to this document.

Qualification Criteria and Methodology on Rod Hangers

The ability of an item of pipe support hardware to resist forces due to static and dynamic events is a function of the physical properties and installation details specified for the hardware.

For static dead weight evaluations, all hardware capable of resisting vertical forces are modeled as active. For analysis of dynamic transients, only hardware which can resist load reversals without undergoing non linear or non elastic deflections is considered effective. In the seismic analyses where the spring constants were inserted into the analysis, the seismic loading was minimal when compared to the deadweight loading. Since the seismic loading never exceeded the deadweight loading, the supports remained within the elastic range and thus would be acceptable for the minimal seismic loading that has occurred. Generalities regarding the applicability of a hardware component are not used to classify the resistance capability of hardware. Specific installation parameters are evaluated to establish the load resistance capability of individual hardware items.

Installation parameters evaluated to establish the resistance capability of hardware include:

- Physical strength of the hardware component to resist tension forces and compression force. Buckling criteria governs this review and is based upon the components length and cross sectional properties. AISC and SSRC (Structural Stability Research Council) criteria for limiting slenderness ratios, kl/r, to 200 governs component members.
- Hardware fit up can not permit a gap movement or unrestrained deflection beyond the industry standard of 1/8" under a load reversal.
- The supported piping system must be of sufficient physical size to provide inherent lateral support to potential compression members which form "pinned" columns.

A rod hanger supported by a spring can would not be effective for dynamic events if the upper working range of the spring can is exceeded and the spring has no downward deflection since the rod bearing plate can uplift from the spring coil resulting in gap movement.

Qualification Criteria and Methodology on Rod Hangers (cont'd)

A larger diameter rod with attachment hardware at the pipe and structural attachment point which preclude gap movement is effective for dynamic loads if the stability slenderness ratio criteria is complied with. Behavior of large diameter rods meeting the stability fit up criteria and rigid struts are identical from a piping analysis standpoint.

MOVEMENTS OF MAIN STEAM
SAFETY VALVES RELATIVE TO DISCHARGE
PIPING

MOVEMENTS OF MAIN STEAM
SAFETY VALVES RELATIVE TO DISCHARGE
PIPING

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT: FPC	FILING CODE:	
	PROJECT: CR UNIT 3	W.O.: 4403-07	PAGE: 1 OF 2
SYSTEM: Notes for Calculations of Safety		ORIGINATOR: A. ECKENROTH	DATE: 12/5/73
CALCULATION FOR: Valve Movements		REVIEWER: M. Z. Lee	DATE: 12/5/73

RESULTS

① Safety Valves may be closed or open. Therefore both conditions are considered.

② Data from the seismic analysis is the sum of X and Y or Y and Z movement.

③ Seismic movement may be positive or negative. Therefore both conditions are considered.

④ Axial and lateral movement are calculated separately so that the worst condition is found in each case. For examples a positive seismic value may be used to calculate axial movement while the negative value is used to calculate lateral movement.

⑤ The largest possible lateral movement in the XY plane not including stack movement is calculated. The smallest

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PROJECT

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W.O.

SYSTEM

ORIGINATOR

DATE

CALCULATION FOR

REVIEWER

DATE

RESULTS

possible is also calculated. This figure is used to calculate the maximum lateral movement off the XY plane including stack movement.

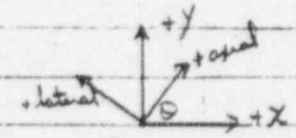
FILING CODE

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT FPC	FILING CODE	
	PROJECT CR UNIT 3	W.O. 4203-027	PAGE 1 OF 6
SYSTEM CR - 3		ORIGINATOR A. ECKENROTH	
		DATE 11/30/73	
CALCULATION FOR Movement on Safety Valve MSV - 46F		REVIEWER M. Z. Lee	
		DATE 12/5/73	

RESULTS

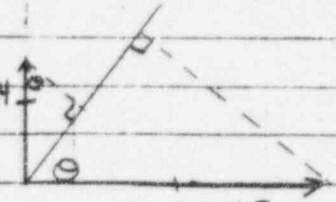
Thermal (original run) movements @ Pt HO-51

ΔX = +.3043"
ΔY = +.1754"
ΔZ = +.8246"



θ = 53°

Facing East



Axial Mov't = (0.1754) Sin θ + (0.3043) Cos θ
0.1401 + 0.1831 =
+0.3232"

Lateral Mov't in XY Plane =
(0.1754) Cos θ − (0.3043) Sin θ
.1056 − .2430 =
−0.1374

Lateral Mov't off XY Plane (ΔZ = 0.8246")

Absolute Lateral Mov't = $\sqrt{(0.8246)^2 + (\text{Lateral Mov't in XY})^2}$

$\sqrt{(0.8246)^2 + (0.1374)^2}$ =

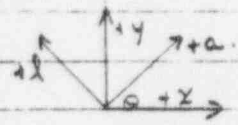
0.8359"

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE
	PROJECT	W.O. / PAGE 2 OF 6
SYSTEM		ORIGINATOR
		DATE
CALCULATION FOR		REVIEWER M. Z. Lee
		DATE 12/5/73

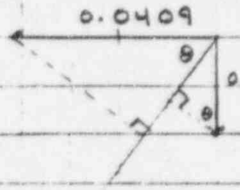
RESULTS

Safety Valve Loads (case No. 2) mov't @ Pt. HO-51

$\Delta X = -0.0409"$
$\Delta Y = -0.0046"$
$\Delta Z = +0.0614"$



θ = 53°
Facing East



Axial Mov't = $(-0.0046)\sin\theta + (-0.0409)\cos\theta$
$(-0.0037) + (-0.0246) =$
$-0.0283"$ or 0"

Lateral Mov't in XY Plane =
$(-.0046)\cos\theta - (-.0409)\sin\theta$
$(-.0028) - (-.0327) =$
$+.0299"$ or 0"

Lateral Mov't off XY Plane ($\Delta Z = +.0614"$)

Absolute Lateral Mov't = $\sqrt{(0.0614)^2 + (\text{Lateral Mov't in XY})^2}$

$\sqrt{(0.0614)^2 + (0.0299)^2} =$

0.0683" or 0"

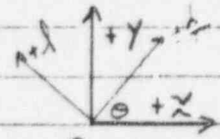
FILING

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
	PROJECT	W.O.	PAGE 3 OF 6
SYSTEM		ORIGINATOR	
		DATE	
CALCULATION FOR		REVIEWER M. Z. Lee	
		DATE 12/5/73	

RESULTS

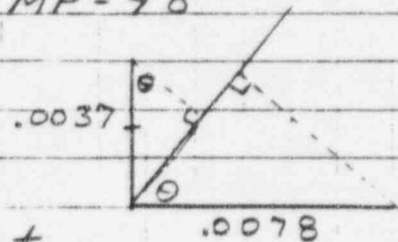
Seismic Mov't. @ Pt MP-48

$\Delta X = \pm 0.0078''$
$\Delta Y = \pm 0.0037''$
$\Delta Z = \pm 0.0278''$



$\theta = 53°$

Facing East



Axial Mov't = (.0037) Sin θ + (.0078) Cos θ
.0030 + .0047 =
± .0077"

Lateral Mov't in XY Plane =
(±.0037) Cos θ − (±.0078) Sin θ
(±.0022) − (±.0062) =
±.0040"

Lateral Mov't off XY Plane ($\Delta Z = \pm .0278''$)

Absolute Lateral Mov't = $\sqrt{(.0278)^2 + (\text{Lateral Mov't in XY})^2}$

$\sqrt{(.0278)^2 + (.0040)^2}$ =

0.0280

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CLIENT	FILING CODE
PROJECT	W.O. / PAGE 4 OF 6
SYSTEM	ORIGINATOR / DATE
CALCULATION FOR	REVIEWER M. Z. Lee / DATE 12/5/73

Stack Mov't due to Thermal Expansion:

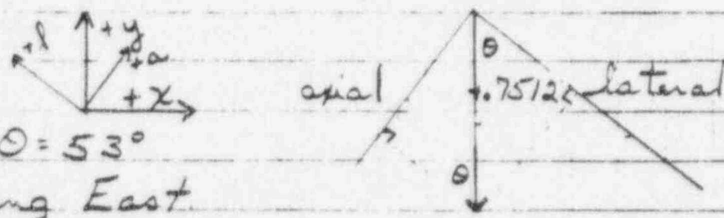
ELEV. of anchor in roof = 149'-0"

ELEV. of safety valve = 128'-3"

Length of stack = 20'-9"

*Expansion of A106-GR.B steel @ 500°F = .0362 in./ft. of pipe

20.75 ft x .0362 in/ft = 0.7512 in



θ = 53°
Facing East

	RESULTS
Axial Mov't = (-0.7512) Sin θ =	-.5999" (compressive)
Lateral Mov't in XY Plane = (-0.7512) Cos θ =	-.4521"

*Temperature is found in pipe specifications (page 65) for Safety Valve Relief Lines.

FILING CODE

GAI 350 REV. 10-72

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
	PROJECT	W.O.	PAGE 5 OF 6
SYSTEM		ORIGINATOR	
CALCULATION FOR		DATE	
		REVIEWER M. Z. Lee	
		DATE 12/5/73	

	RESULTS
Total Mov't @ Pt. HO-51 =	
Thermal + Safety Valve + Seismic Mov't.	
Axial Mov't = (+.3232) + (-.0283) + (+.0077) =	+.3026"
	OR
When Safety Valve is Closed = (+.3232) + (+.0077) =	+.3309" (compressive)
Lateral Mov't in XY Plane = (-.1374) + (+.0299) + (+.0040) =	-.1035"
	OR
When Safety Valve is Closed = (-.1374) + (-.0040) =	-.1414"
Mov't in Z Direction = (+.8246) + (+.0614) + (+.0278) =	+.9138"
	OR
When Safety Valve is Closed = (+.8246) + (+.0278) =	+.8524"
Lateral Mov't off XY Plane =	
$\sqrt{(.9138)^2 + (.1414)^2}$ =	.9247"
Total Movement	
Axial Mov't = (.3309) + (.5999) =	.9308"
Lateral Mov't in XY Plane = (-.4521) - (-.1035) =	-.3486"
Lateral Mov't off XY Plane =	
$\sqrt{(.9138)^2 + (.3486)^2}$ =	.9780"

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
	PROJECT	W.O.	PAGE 6 OF 6
SYSTEM		ORIGINATOR	
		DATE	
CALCULATION FOR		REVIEWER M. Z. Lee	
		DATE 12/5/73	

MSV-46F Summary
MSEJ-4

DIRECTION	WITHOUT STACK MOVEMENT	WITH STACK MOVEMENT	RESULTS
AXIAL	.3309"	.9308"	Compression
X-Y	-.1414"	-.3486"	
Z	+.9138"	+.9138"	
LATERAL	.9247"	.9780"	

Design Conditions

Axial = .85" Compression max

Lateral = .81"

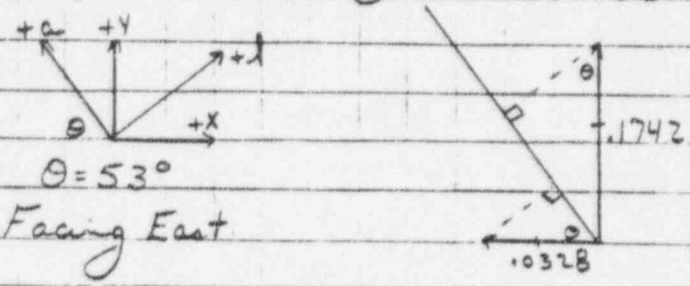
FILING CODE

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT FPC	FILING CODE	
	PROJECT CR UNIT 3	W.O.	PAGE 1 OF 6
SYSTEM CR-3		ORIGINATOR A. ECKENROTH DATE 12/6/73	
CALCULATION FOR Movement of Safety Valve MSV-42		REVIEWER M. Z. Lee DATE 12/08/73	

RESULTS

Thermal (original run) movements @ Pt HP-58

$\Delta X = -.0328"$
$\Delta Y = +.1742"$
$\Delta Z = +.9852"$



$\theta = 53°$
Facing East

Axial mov't = $(+.1742)\sin\theta - (-.0328)\cos\theta$
$(+.1391) - (-.0197) =$
$+.1588"$

Lateral Mov't in XY Plane =
$(+.1742)\cos\theta + (-.0328)\sin\theta =$
$(+.1048) + (-.0262) =$
$+.0786"$

Lateral Mov't off XY Plane ($\Delta Z = +.9852"$)

Absolute Lateral Mov't = $\sqrt{(.9852)^2 + (\text{Lat'l Mov't in XY})^2} =$

$$\sqrt{(.9852)^2 + (.0786)^2} =$$

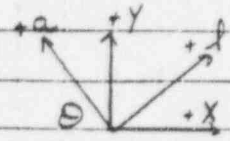
$.9883"$

Safety Valve Loads (case No. 2) mov't @ Pt. HP-58

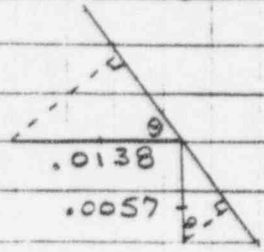
$\Delta X = -.0138"$

$\Delta Y = -.0057"$

$\Delta Z = +.0197"$ $\quad \theta = 53°$



Facing East



Axial Mov't = $(-.0057) \sin\theta - (-.0138) \cos\theta =$

$(-.0046) - (-.0083) =$

$+.0037"$ or $0"$

Lateral Mov't in XY Plane =

$(-.0057) \cos\theta + (-.0138) \sin\theta =$

$(-.0034) + (-.0110) =$

$-.0144"$ or $0"$

Lateral Mov't off XY Plane ($\Delta Z = +.0197$)

Absolute Lateral Mov't $= \sqrt{(.0197)^2 + (\text{Lateral Mov't in XY})^2}$

$= \sqrt{(.0197)^2 + (.0144)^2} =$

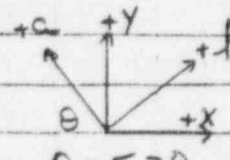
$.0244"$

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE
	PROJECT	W.O. / PAGE 3 of 6
SYSTEM		ORIGINATOR / DATE
CALCULATION FOR		REVIEWER / DATE

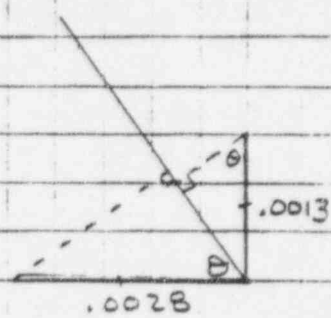
RESULTS

Seismic Mov't @ Pt MR-55

$\Delta X = \pm .0028''$
$\Delta Y = \pm .0013''$
$\Delta Z = \pm .0291''$ $\theta = 53^\circ$



Facing East



Axial Mov't $= (\pm .0013) \sin\theta - (\pm .0028) \cos\theta =$
$(\pm .0010) - (\pm .0017) =$
$\pm .0027''$

Lateral Mov't in XY Plane $=$
$(\pm .0013) \cos\theta + (\pm .0028) \sin\theta =$
$(\pm .0008) + (\pm .0022) =$
$\pm .0030''$

Lateral Mov't off XY Plane $= (\Delta Z = \pm .0291'')$

Absolute Lateral Mov't $= \sqrt{(.0291)^2 + (\text{Lateral Mov't in XY})^2}$

$\sqrt{(.0291)^2 + (.0030)^2} =$

$.0293''$

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RESULTS

Stack Mov't due to Thermal Expansion:

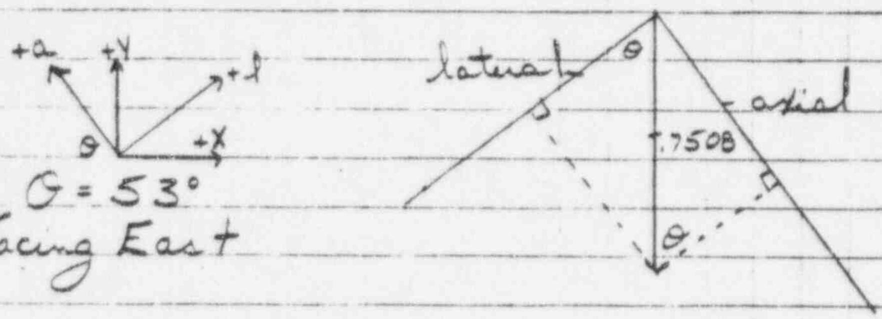
ELEV of anchor in roof = 149'-0"

ELEV of safety valve = 128'-3 1/8"

Length of stack = 20'-8 7/8"

* Expansion of A106-GR B steel @ 500°F = .0326 in/ft. of pipe

20.7396 ft x .0362 in/ft = .7508 in.



θ = 53°
Facing East

Axial Mov't = (-.7508) Sin θ = -.5996" (compressive)

Lateral Mov't in XY Plane = (-.7508) Cos θ = -.4518"

* Temperature is found in pipe specifications (page 65) for Safety Valve Relief Lines.

FILING CODE

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	RESULTS
Total Mov't @ Pt. HP-58 =	
Thermal + Safety Valve + Seismic Mov't	
Axial Mov't = (+.1588)+(+.0037)+(+.0027) =	+.1652"
	or
When Safety Valve is Closed = (+.1588)+(+.0027) =	+.1615" (compressive)
Lateral Mov't in XY Plane = (+.0786)+(-.0144)+(-.0030) =	+.0612"
	or
When Safety Valve is Closed = (+.0786)+(+.0030) =	+.0816"
Mov't in Z Direction = (+.9852)+(+.0197)+(+.0291) =	+1.0340"
When Safety Valve is Closed = (+.9852)+(+.0291) =	+1.0143"
Lateral Mov't off XY Plane = $\sqrt{(1.0340)^2+(.0816)^2}$ =	1.0372"
Total Movement	
Axial Mov't = (.5996)+(.1652) =	.7648"
Lateral Mov't in XY Plane = (-.4518) - (+.0816) =	-.5334"
Lateral Mov't off XY Plane = $\sqrt{(1.0340)^2+(.5334)^2}$ =	1.1635"

FILING CODE

GAI 350 REV. 10-72

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SYSTEM

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CALCULATION FOR

REVIEWER

DATE

RESULTS

MSV-42F Summary
MSEJ-3

DIRECTION	WITHOUT STACK MOVEMENT	WITH STACK MOVEMENT	RESULTS
AXIAL	.1652"	.7648"	Compression
XY	+.0816"	-.5334"	
Z	+1.0340"	+1.0340"	
LATERAL	1.0372"	1.1635"	

Design Conditions

Axial = 0.84"

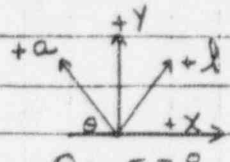
Lateral = 0.73"

FILING

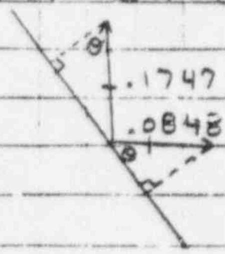
GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT FPC PROJECT CR UNIT 3	FILING CODE W.O. 4203007 PAGE 1 OF 6
SYSTEM CR-4		ORIGINATOR A ECKENROTH DATE 12/5/73
CALCULATION FOR Movement on Safety Valve MSV-40 F		REVIEWER M. Z. Lee DATE 12/5/73

Thermal (Revision #1) mov't @ Pt. DH-572

$\Delta X = +.0848''$
$\Delta Y = +.1747''$
$\Delta Z = +1.2388''$
$\theta = 53°$



Facing East



Axial Mov't = $(+.1747) \sin\theta - (+.0848) \cos\theta =$
$(+.1395) - (+.0510) =$
$+.0885''$

Lateral Mov't in XY Plane =
$(+.1747) \cos\theta + (+.0848) \sin\theta =$
$(+.1051) + (+.0677) =$
$+.1728''$

Lateral Mov't off XY Plane

Absolute Lateral Mov't =

$$\sqrt{(1.2388)^2 + (\text{Lateral Mov't in XY})^2}$$

$$\sqrt{(1.2388)^2 + (.1728)^2} =$$

$1.2508''$

RESULTS

FILING

GAI 350 REV. 10-72

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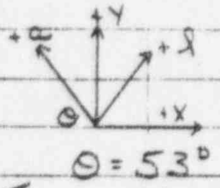
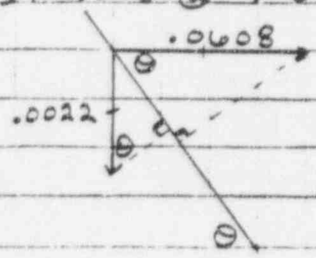
RESULTS

Safety Valve Loads (case #3) mov't @ Pt DH-572

ΔX = +.0608"
ΔY = −.0022"
ΔZ = +.0127"



Facing East



Axial Mov't = (−.0022) Sin θ − (+.0608) Cos θ =
(−.0018) − (+.0366) =
−.0384" or 0"

Lateral Mov't in XY Plane =
(−.0022) Cos θ + (+.0608) Sin θ =
(−.0013) + (+.0486) =
+.0473" or 0"

Lateral Mov't off XY Plane

Absolute Lateral Mov't =

$$\sqrt{(.0127)^2 + (\text{Lateral Mov't in XY})^2}$$

$$\sqrt{(.0127)^2 + (.0473)^2} =$$

.0490" or 0"

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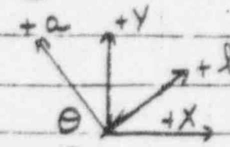
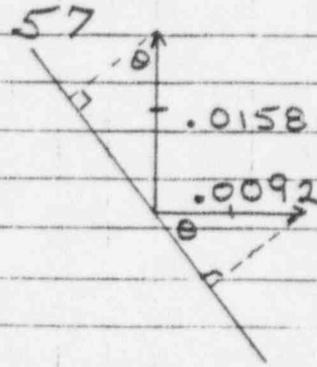
SYSTEM		ORIGINATOR DATE	
CALCULATION FOR		REVIEWER DATE	

Seismic Mov't @ Pt. MV-57

ΔX = ±.0092"
ΔY = ±.0158"
ΔZ = ±.0123"



θ = 53°
Facing East



Axial Mov't = (+.0158) Sin θ − (+.0092) Cos θ =
(+.0126) − (+.0055) =
+.0071"

Lateral Mov't in XY Plane =
= (±.0158) Cos θ + (±.0092) Sin θ =
(±.0095) + (±.0073) =
±.0168"

Lateral Mov't off XY Plane =

$$\sqrt{(.0123)^2 + (\text{Lateral Mov't in XY})^2}$$

$$\sqrt{(.0123)^2 + (.0168)^2} =$$

.0208"

RESULTS

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GAI 350 REV. 10-72

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Stack Mov't due to Thermal Expansion -

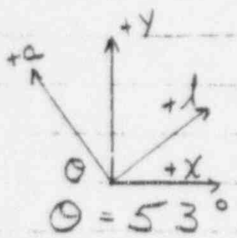
ELEV of anchor in roof = 149'-0"

ELEV of safety valve = 128'-0 5/16"

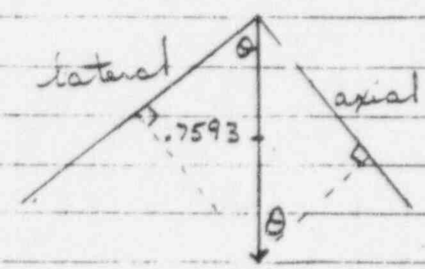
Length of stack = 20'-11 11/16"

* Expansion of A106 GR.B steel @ 500°F = .0362 in / ft. of pipe

20.9740 ft x .0362 in/ft. = .7593"



Facing East



	RESULTS
Axial Mov't = (-.7593) Sin θ =	-.6064" (compressive)
Lateral Mov't in XY Plane = (-.7593) Cos θ =	-.4570"

* Temperature is found in pipe specifications (page 65) for Safety Valve Relief Lines.

FILING CODE

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	RESULTS
Total Mov't @ Pt. DH-572 =	
Thermal + Safety Valve + Seismic Mov't	
Axial Mov't = (+.0885) + (-.0384) + (+.0071) =	+.0572"
	OR
When Safety Valve is closed = (+.0885) + (+.0071) =	+.0956" (compressive)
Lateral Mov't in XY Plane = (+.1728) + (+.0473) + (+.0168) =	+.2369"
	OR
When Safety Valve is closed = (+.1728) + (-.0168)	+.1560"
Mov't in Z Direction = (+1.2388) + (+.0127) + (+.0123) =	+1.2638"
	OR
When Safety Valve is closed = (+1.2388) + (+.0123) =	+1.2511"
Lateral Mov't off XY Plane = $\sqrt{(1.2638)^2 + (.2369)^2}$ =	1.2858"
Total Movement	
Axial Mov't = (.0956) + (.6064) =	.7020"
Lateral Mov't in XY Plane = (-.4570) − (+.1560) =	−.6130"
Lateral Mov't off XY Plane = $\sqrt{(1.2638)^2 + (.6130)^2}$ =	.9864"

FILING CODE

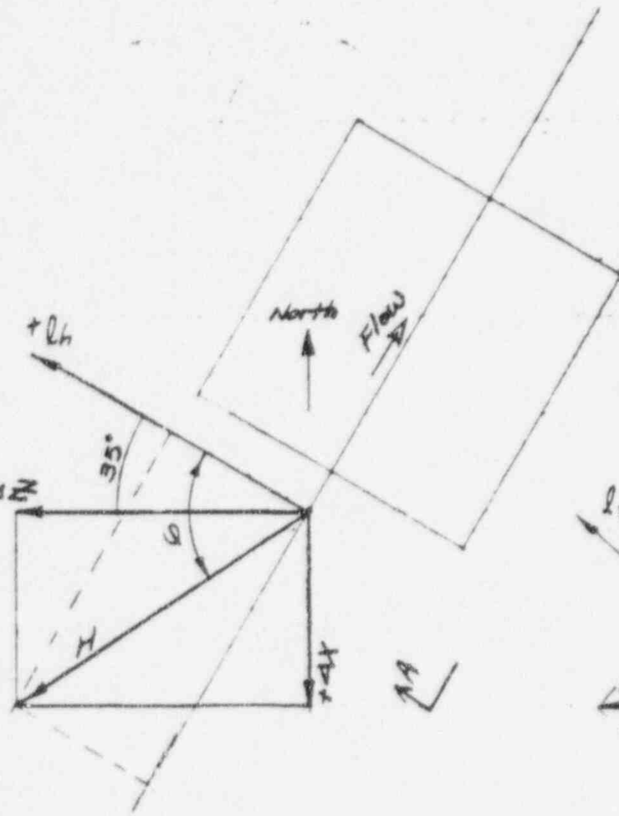
GAI 350 REV. 10-72

MSV-40F Summary
MSEJ-9

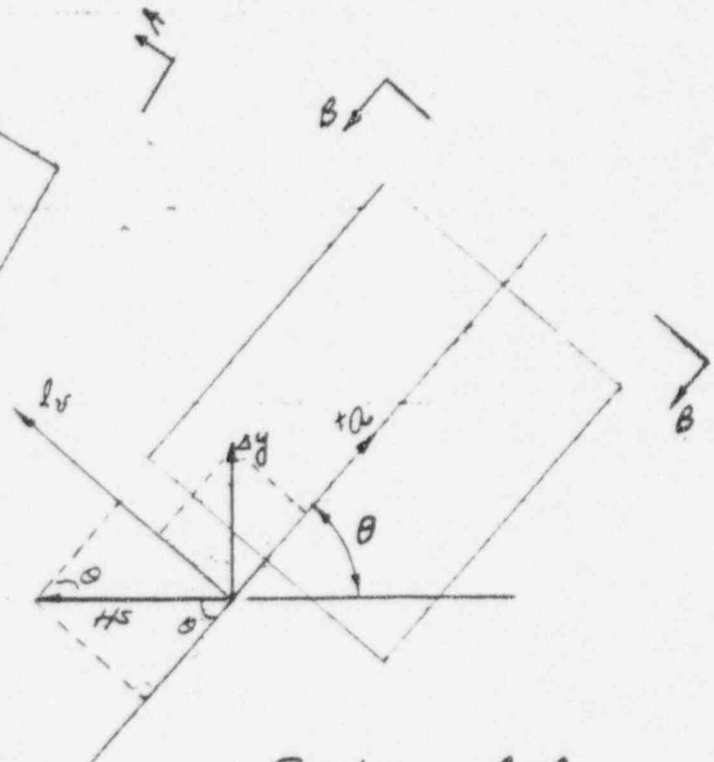
DIRECTION	WITHOUT STACK MOVEMENTS	WITH STACK MOVEMENTS
AXIAL	.0956"	.7020"
XY	+.2369"	-.6130"
Z	+1.2638"	+1.2638"
LATERAL	1.2858"	.9864"

Design Conditions
Axial = .84"
Lateral = 1.14"

Florida Power Corp.	MADE 12/4/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
Crystal River #3	CHK'D.	
MSEJ-7 Flexonic Joint on MSV-38	SQ. CF. / CF. DFN.	4203-27 WORK ORDER
Movements Calculation	ENG. M. Z. Lee	SIZE DRAWING REV
	REV. CH. APP. DATE	



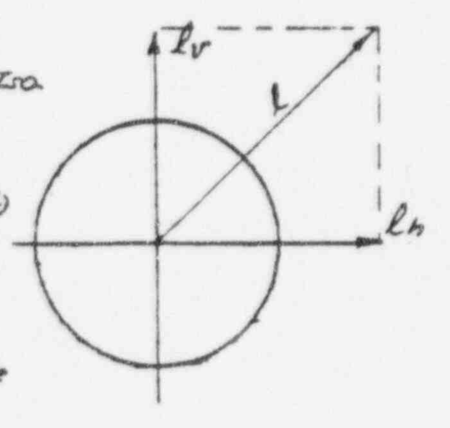
PLAN



Section A-A

Notes:

1. X-Y-Z matches with Iso.
2. a = axial movement
   l = lateral movement (⊥ axis of Flexonics)
   l_v = lateral movement in vertical plane
   l_h = lateral movement in horizontal plane



Section B-B

$$\vec{H} = \vec{\Delta Z} + \vec{\Delta X}$$

$$|H| = \sqrt{(\Delta Z)^2 + (\Delta X)^2}$$

$$\varphi = \tan^{-1}\frac{\Delta X}{\Delta Z} + 35°$$

$$Hs = |H| \cdot \sin\varphi$$

$$l_h = |H| \cdot \cos\varphi$$

$$l_v = HS \cdot \sin\theta + \vec{\Delta y}\cos\theta$$

$$|l| = \sqrt{l_v^2 + l_h^2}$$

$$a = \vec{y} \cdot \sin\theta - HS \cdot \cos\theta$$

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SYSTEM CR - 4		ORIGINATOR A ECKENROTH DATE 12/5/73
CALCULATION FOR Movement of Safety Valve MSV-38		REVIEWER M.Z. Lee DATE 12/6/73

Thermal (Revision #1) Mov't @ Pt. FH-662

RESULTS

$\Delta X = -.1676''$
$\Delta Y = +.1735''$
$\Delta Z = +.8552''$

$\vec{H} = \vec{\Delta Z} + \vec{\Delta X}$

$|H| = \sqrt{(.8552)^2 + (.1676)^2} = .8715''$

$\varphi = \tan^{-1}\frac{\Delta X}{\Delta Z} + 35° =$

$\tan^{-1}(-.19598) + 35° = -11° + 35° = 24°$

$HS = |H| \cdot \sin\varphi = (.8715)\sin\varphi = .3545''$

$a = \vec{y}\sin\Theta - HS\cos\Theta$

$= (+.1735)\sin\Theta - (+.3545)\cos\Theta =$
$(+.1386) - (+.2133) = -.0747''$

Axial Mov't = $-.0747''$

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RESULTS

$l_h = |H| \cdot \cos 6$

$= (.8715) \cos 6 = +.7962$

$l_v = HS \cdot \sin \Theta + \bar{\Delta y} \cos \Theta =$

$(+.3545) \sin \Theta + (+.1735) \cos \Theta =$
$.2831 + .1044 = .3875$

$|l| = \sqrt{l_v^2 + l_h^2} =$

$\sqrt{(.3875)^2 + (.7962)^2} = .8855"$

Lateral Mov't = .8855"

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RESULTS

Safety Valve (Case #3) Mov't @ Pt. EH-662

$\Delta X = +.0286''$

$\Delta Y = +.0122''$

$\Delta Z = +.0046''$

$$\vec{H} = \vec{\Delta Z} + \vec{\Delta X}$$

$$|H| = \sqrt{(+.0046)^2 + (.0286)^2} = .0290''$$

$$\theta = \tan^{-1}\frac{\Delta X}{\Delta Z} + 35° =$$

$$\tan^{-1}(+6.2174) + 35° =$$

$$81° + 35° = 116°$$

$$HS = |H| \cdot \sin\theta =$$

$$(.0290)\sin\theta = +.0261''$$

$$a = \vec{y}\sin\theta - HS\cos\theta$$

$$= (+.0122)\sin\theta - (+.0261)\cos\theta =$$

$$(+.0097) - (+.0157) = -.0060''$$

Axial Mov't = −.0060"

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RESULTS

$lh = |H| \cdot \cos \varphi$

$= (.0290) \cos \varphi = -.0127''$

$lv = HS \cdot \sin \Theta + \vec{\Delta Y} \cos \Theta =$

$(+.0261) \sin \Theta + (+.0122) \cos \Theta =$

$(+.0208) + (+.0073) = +.0281''$

$|l| = \sqrt{lv^2 + lh^2} =$

$\sqrt{(.0281)^2 + (.0127)^2} = .0308''$

Lateral Mov't = .0308"

FILING

GILBERT ASSOCIATES, INC.
ENGINEERS AND CONSULTANTS
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RESULTS

Seismic Mov't @ Pt MZ-66

$\Delta X = \pm .0009''$
$\Delta Y = \pm .0116''$
$\Delta Z = \pm .0088''$

$$\vec{H} = \overrightarrow{\Delta Z} + \overrightarrow{\Delta X}$$

$$|H| = \sqrt{(.0088)^2 + (.0009)^2} = .0092''$$

$$\phi = \tan^{-1}\frac{\Delta X}{\Delta Z} + 35° =$$

$$\tan^{-1}(\pm .1023) + 35° =$$

$$\pm 6° + 35° = 29° \text{ or } 42°$$

$$HS = |H| \sin\phi =$$

$$(.0092)\sin\phi = .0045 \text{ or } .0062$$

$$a = \vec{y}\sin\theta - HS\cos\theta =$$

$$(+.0116)\sin\theta - (+.0045)\cos\theta =$$

$$(+.0093) - (+.0027) = +.0066''$$

Axial Mov't = ±.0066"

FILING

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RESULTS

$\ell_h = |H| \cdot \cos 6 =$

$(.0092) \cos 6 = .0080''$

$\ell_v = HS \sin\theta + \vec{Ay} \cos\theta =$

$(+.0062) \sin\theta + (+.0116) \cos\theta =$

$(+.0050) + (+.0070) = .0120''$

$|\ell| = \sqrt{\ell_v^2 + \ell_h^2} =$

$\sqrt{(.0120)^2 + (.0080)^2} = .0144''$

Lateral Mov't = .0144"

FILING CODE

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Mov't on stack

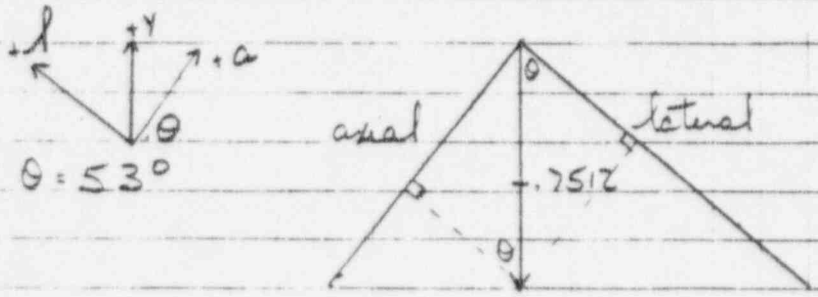
ELEV of anchor in roof = 149'-0"

ELEV of safety valve = 128'-3"

Length of stack = 20'-9"

Expansion of A106-GR B. steel @ 500°F = .0362 in/ft of pipe

20.75 ft x .0362" in/ft = .7512 in



	RESULTS
Axial Mov't = (-.7512) Sin θ =	-.5999"
(1w) Lateral Mov't = (-.7512) Cos θ =	-.4521"

FILING CODE

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
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RESULTS

<u>Total Mov't @ Pt. FH-662</u>

Thermal + Safety Valve + Seismic Mov't

Axial Mov't = (-.0747) + (-.0060) + (-.0066) = -.0873"

or

When Safety Valve is closed = (-.0747) + (+.0066) = -.0681" (elongation)

Lateral Mov't lv =

(+.3875) + (+.0281) + (+.0120) = +.4276"

or

When Safety Valve is closed = (+.3875) + (+.0120) = +.3995"

Lateral Mov't lh =

(+.7962) + (-.0127) + (+.0080) = +.7915"

or

When Safety Valve is closed = (+.7962) + (+.0080) = +.8042"

Absolute Lateral Mov't =

$\sqrt{(.4276)^2 + (.8042)^2}$ = .9108"

<u>Total Movement</u>

Axial Mov't = ($\pm$.5999) + (-.0873) = ~~-.6872"~~ + 0.5126

Lateral Mov't lv = (-.4521) - (+.4276) = -.8797"

Absolute Lateral Mov't =

$\sqrt{(.8797)^2 + (.8042)^2}$ = 1.1909"

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RESULTS

MSV-38 Summary
MSEJ-7

DIRECTION	WITHOUT STACK MOVEMENT	WITH STACK MOVEMENT
AXIAL	-.0873"	~~-.6872"~~ + 0.5126 (COMPRESSION)
lv	+.4276"	-.8797"
lh	+.8042"	+.8042"
LATERAL |l|	.9108"	1.1909"

Elongation (WITHOUT STACK MOV)

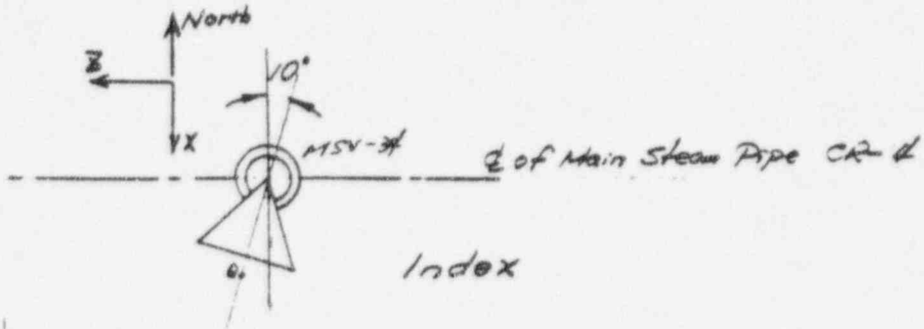
Design Conditions

Axial = 0.84" Compression

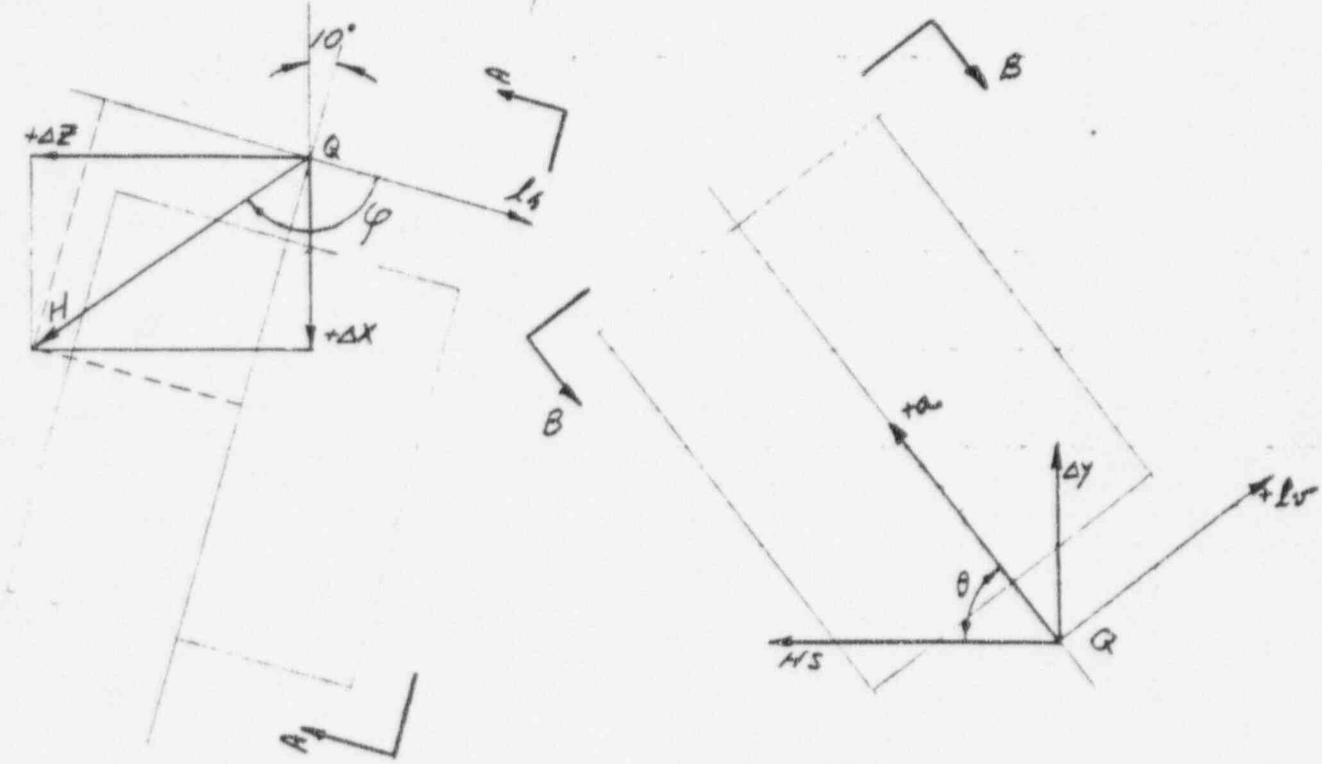
Lateral = 0.77"

FILING CODE

Florida Power Corp	MADE 12/6/73 CHK'D. GO. CF.	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
Crystal River #3	CF. DFM.	4203-007
MSEJ - 6 Flexonic Joint on MSV-34	ENG. M. Z. Lee	WORK ORDER / SIZE / DRAWING / REV.
Movement Calculation	REV. CK. APP. DATE	

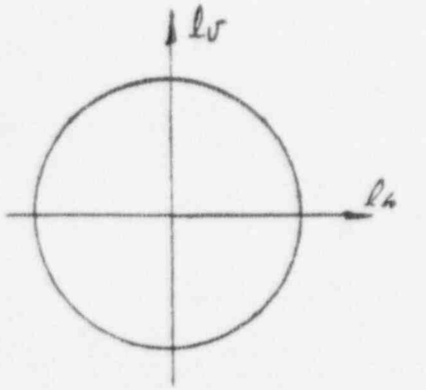


Index



Plon

Section A-A (Vertical Plane



$\vec{H} = \vec{\Delta x} + \vec{\Delta z}$

$|H| = \sqrt{(\Delta z)^2 + (\Delta x)^2}$

$\varphi = \tan^{-1}\left(\frac{\Delta z}{\Delta x}\right) + 80°$

$Hs = |H| \cdot \sin\varphi$

$l_h = |H| \cdot \cos\varphi$

$l_v = \Delta y \cos\theta - Hs \cdot \sin\theta$

$|l| = \sqrt{l_v^2 + l_h^2}$

$a = y \cdot \sin\theta + Hs \cos\theta$

Section B-B

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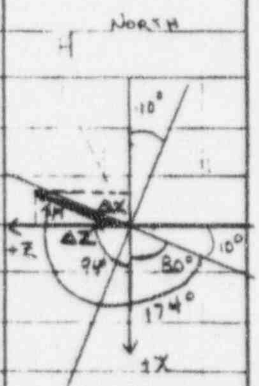
	PROJECT CR UNIT 3	W.O.	PAGE 1 OF 9
SYSTEM CR-4		ORIGINATOR A. ECKENROTH DATE 12/6/73	
CALCULATION FOR Movement of Safety Valve MSV-34		REVIEWER H.Z. Lee DATE 12/08/73	

Thermal (Revision #1) Mov't @ Pt GH-722

$\Delta X = -.0458''$
$\Delta Y = +.1745''$
$\Delta Z = +.7156''$

$$\vec{H} = \vec{\Delta X} + \vec{\Delta Z}$$

$$|H| = \sqrt{(.0458)^2 + (.7156)^2} = .7171''$$



$$\phi = \tan^{-1}\left(\frac{\Delta Z}{\Delta X}\right) + 80° =$$

$$\tan^{-1}(-15.6245) + 80° =$$

$$-94° + 80° = 174°$$

$$HS = |H| \sin\phi =$$

$$(.7171) \sin\phi = +.0750''$$

$$a = \vec{y}\sin\Theta + HS\cos\Theta =$$

$$(+.1745)\sin\Theta + (+.0750)\cos\Theta =$$

$$(+.1394) + (+.0451) = +.1845''$$

Axial Mov't = +.1845''

RESULTS

FILING CODE

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RESULTS

$$lh = |H| \cdot \cos 6$$

$$= (.7171) \cos 6 = -.7132$$

$$lv = \Delta y \cos \Theta - HS \sin \Theta =$$

$$(+.1745) \cos \Theta - (+.0750) \sin \Theta =$$

$$(+.1050) - (+.0599) =$$

$$+.0451''$$

$$|l| = \sqrt{lv^2 + lh^2} =$$

$$\sqrt{(.0451)^2 + (.7132)^2} = .7146''$$

Lateral Mov't = .7146"

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CALCULATION FOR		REVIEWER / DATE

RESULTS

Safety Valve (case #3) Mov't @ Pt. GH-722

$\Delta X = +.0167''$
$\Delta Y = -.0160''$
$\Delta Z = -.0007''$

$$\vec{H} = \vec{\Delta X} + \vec{\Delta Z}$$

$$|H| = \sqrt{(.0167)^2 + (.0007)^2} = .0167''$$

$$\phi = \tan^{-1}\left(\frac{\Delta Z}{\Delta X}\right) + 80° =$$

$$\tan^{-1}(-.0419) + 80° =$$

$$-2° + 80° = 78°$$

$$HS = |H| \sin \phi =$$

$$(.0167) \sin \phi = +.0163''$$

$$a = \vec{y} \cdot \sin\theta + HS \cos\theta =$$

$$(-.0160)\sin\theta + (+.0163)\cos\theta =$$
$$(-.0128) + (+.0098) =$$
$$-.0030''$$

Axial Mov't = $-.0030''$

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RESULTS

$lh = |H| \cdot \cos 6 =$

$(.0167) \cos 6 = +.0035''$

$lv = \Delta y \cos \Theta - H.S \cdot \sin \Theta =$

$(-.0160) \cos \Theta - (+.0163) \sin \Theta =$

$(-.0096) - (+.0130) =$

$-.0226''$

$|l| = \sqrt{lv^2 + lh^2} =$

$\sqrt{(.0226)^2 + (.0035)^2} = .0229''$

Lateral Movt = .0229"

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RESULTS

Seismic Mov't @ Pt. NB-72

$\Delta X = \pm .0028''$
$\Delta Y = \pm .0085''$
$\Delta Z = \pm .0085''$

$$\vec{H} = \overrightarrow{\Delta x} + \overrightarrow{\Delta z}$$

$$|H| = \sqrt{(.0028)^2 + (.0085)^2} = .0089''$$

$$\phi = \tan^{-1}\left(\frac{\Delta z}{\Delta x}\right) + 80^\circ =$$

$$\tan^{-1}(\pm 3.0357) + 80^\circ =$$

$$\pm 72^\circ + 80^\circ = 8^\circ \text{ or } 152^\circ$$

$$HS = |H| \cdot \sin\phi =$$

$$(.0089) \sin\phi = +.0012'' \text{ or } +.0042''$$

$$a = \vec{y} \sin\theta \;\; HS \cos\theta =$$

$$(+.0085) \sin\theta + (+.0042) \cos\theta =$$

$$(+.0068) + (+.0025) = +.0093''$$

Axial Mov't = +.0093"

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RESULTS

$\Delta h = |H| \cos 6 =$

$(.0089) \cos 6 = +.0088"$ or $-.0079"$

$\Delta v = \Delta Y \cos \theta - HS \sin \theta =$

$(\pm.0085) \cos \theta - (+.0042) \sin \theta =$

$(\pm.0051) - (+.0034) =$

$-.0085"$ or $+.0017"$

$|H| = \sqrt{\Delta v^2 + \Delta h^2} =$

$\sqrt{(.0085)^2 + (.0088)^2} =$

$.0122"$

Lateral Mov t = .0122"

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CALCULATION FOR		DATE REVIEWER DATE	

Mov't on stack

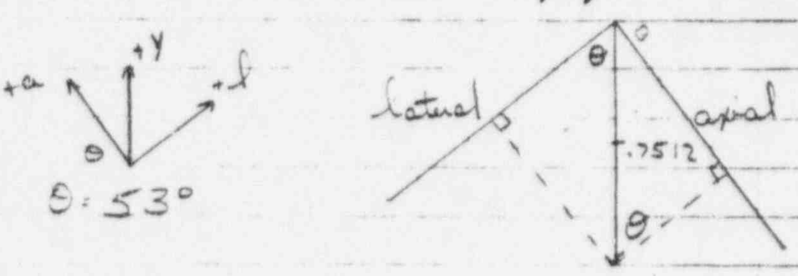
ELEV of anchor in roof = 149'-0"

ELEV of safety valve = 128'-3"

Length of stack = 20'-9"

Expansion of A106-GR B steel @ 500°F = .0362 in/ft. of pipe

20.75 ft x .0362 in/ft = .7512 in



	RESULTS
Axial Mov't = (-.7512) Sin θ =	-.5999" (compression)
(-l~) Lateral Mov't = (-.7512) Cos θ =	-.4521"

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CALCULATION FOR		DATE	
		REVIEWER	
		DATE	

	RESULTS
Total Mov't @ Pt GH-722	
Thermal + Safety Valve + Seismic Mov't	
Axial Mov't = (+.1845) + (-.0030) + (+.0093) =	+.1908"
	or
When Safety Valve is closed = (+.1845) + (+.0093) =	+.1938" (compression)
Lateral Mov't l_v = (+.0451) + (-.0226) + (-.0085) =	+.0140"
	or
When Safety Valve is closed (+.0451) + (+.0017)	+.0468"
Lateral Mov't l_h = (-.7132) + (+.0035) + (+.0088) =	-.7009"
	or
When Safety Valve is closed (-.7132) + (-.0079) =	-.7211"
Absolute Lateral Mov't |l| = $\sqrt{(.0468)^2 + (.7211)^2}$ =	.7226"
Total Movement	
Axial Mov't = (.5999) + (.1938) =	.7937"
Lateral Mov't l_v = (-.4521) - (+.0468) =	-.4989"
Absolute Lateral Mov't |l| = $\sqrt{(.4989)^2 + (.7211)^2}$ =	.8769"

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CALCULATION FOR

REVIEWER

DATE

RESULTS

MSV - 34 Summary
MSEJ - 6

DIRECTION	WITHOUT STACK MOVEMENT	WITH STACK MOVEMENT	
AXIAL	.1938"	.7937"	compression
l_v	+.0468"	-.4989"	
l_h	-.7211"	-.7211"	
LATERAL |l|	.7226"	.8769"	

Design Conditions

Axial = 0.84" compression

Lateral = 0.66"

FILING

GAI 350 REV. 10-72

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	PROJECT CR UNIT 3	W.O. 4203-027 / PAGE 1 OF 6
SYSTEM CR-5		ORIGINATOR A. ECKENROTH / DATE 12/3/73
CALCULATION FOR Movement on Safety Valve MSV-48F		REVIEWER M.Z. Lee / DATE 12/5/73

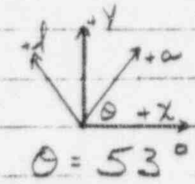
RESULTS

Thermal (Revision #1) movements @ Pt. EH-652

$\Delta X = +.1907''$

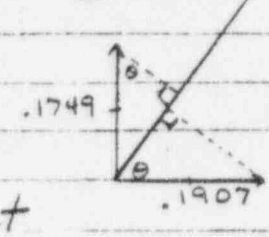
$\Delta Y = +.1749''$

$\Delta Z = +1.1043''$



$\theta = 53°$

Facing East



Axial Mov't = $(+.1749) \sin\theta + (+.1907)\cos\theta =$

$(+.1397) + (+.1148) =$

$+.2545''$

Lateral Mov't in XY Plane =

$(+.1749)\cos\theta - (+.1907)\sin\theta =$

$(+.1053) - (+.1523) =$

$-.0470$

Lateral Mov't off XY Plane ($\Delta Z = +1.1043$)

Absolute Lateral Mov't = $\sqrt{(1.1043)^2 + (\text{Lateral Mov't in XY})^2} =$

$\sqrt{(1.1043)^2 + (.0470)^2} =$

1.1053

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CALCULATION FOR		DATE
		REVIEWER M. Z. Loo
		DATE 10/5/73

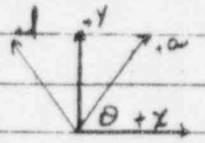
RESULTS

Safety Valve Loads (case # 2) mov't @ Pt EH-652

$\Delta X = +.0264"$

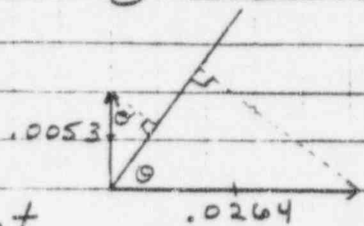
$\Delta Y = +.0053"$

$\Delta Z = -.0128"$



$\theta = 53°$

Facing East



Axial Mov't = (+.0053) Sin θ + (+.0264) Cos θ -

(+.0042) + (+.0159) =

+.0201" or 0"

Lateral Mov't in XY Plane =

(+.0053) Cos θ − (+.0264) Sin θ

(+.0032) − (+.0211) =

−.0179" or 0"

Lateral Mov't off XY-Plane - ($\Delta Z = -.0128"$)

Absolute Lateral Mov't = $\sqrt{(.0128)^2 + (\text{Lateral Mov't in XY})^2}$ =

$\sqrt{(.0128)^2 + (.0179)^2}$ =

.0220"

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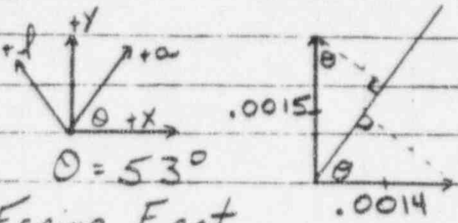
		DATE	
CALCULATION FOR		REVIEWER M. Z. Lee	
		DATE 12/5/73	
		RESULTS	

Seismic Mov't @ Pt. MW-65

$\Delta X = \pm .0014"$
$\Delta Y = \pm .0015"$
$\Delta Z = \pm .0018"$ $\theta = 53°$



Facing East

Axial Mov't = $(\pm .0015) \sin\theta + (\pm .0014) \cos\theta$ ·
$(\pm .0012) + (\pm .0008) =$
$\pm .0020"$

Lateral Mov't in XY Plane =

$(\pm .0015) \cos\theta - (\pm .0014) \sin\theta$
$(\pm .0009) - (\pm .0011) =$
$\pm .0002"$

Lateral Mov't off XY Plane =

Absolute Lateral Mov't = $\sqrt{(.0018)^2 + (\text{Lateral Mov't in } XY)^2} =$

$\sqrt{(.0018)^2 + (.0002)^2} =$

$.0018"$

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SYSTEM

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CALCULATION FOR

REVIEWER M. Z. Lee

DATE 12/5/73

RESULTS

Stack Mov't due to Thermal Expansion

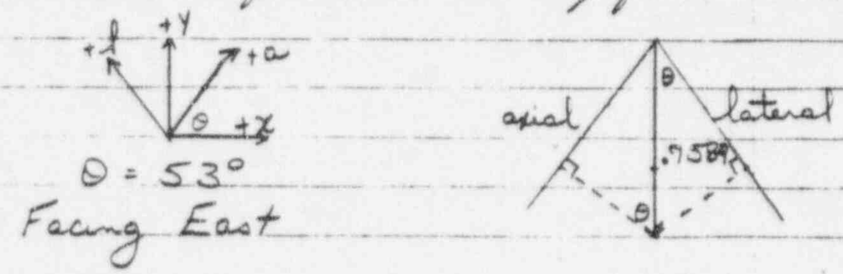
ELEV of anchor in roof = 149'-0"

ELEV of safety valve = 128'-0 7/16"

Length of stack = 20'-11 9/16"

* Expansion of A106 GR.B steel @ 500°F = .0362 in./ft. of pipe

20.9635 ft x .0362 in/ft = .7589 in



Axial Mov't = (-.7589) Sin θ = -.6061" (compressive)

Lateral Mov't in XY Plane = (-.7589) Cos θ = -.4567"

* Temperature is found in pipe specifications (page 65) for Safety Valve Relief Lines

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CALCULATION FOR		DATE	
		REVIEWER M.Z. Lee DATE 12/5/73	

Total Mov't @ Pt EH-652

Thermal + Safety Valve + Seismic Mov't

	RESULTS
Axial Mov't = (+.2545) + (+.0201) + (+.0020) =	+.2766"
	OR
When Safety Valve is closed = (+.2545) + (+.0020) =	+.2565" (compressive)
Lateral Mov't in XY Plane = (-.0470) + (-.0179) + (-.0002) =	-.0651"
	OR
When Safety Valve is closed = (-.0470) + (+.0002) =	-.0468"
Mov't in Z Direction = (+1.1043) + (-.0128) + (+.0018) =	+1.0933"
When Safety Valve is closed = (+1.1043) + (+.0018) =	+1.1061"
Lateral Mov't off XY Plane = $\sqrt{(1.1061)^2 + (.0651)^2}$ =	1.1080"

Total Movement

Axial Mov't = (.2766) + (.6061) =	.8827"
Lateral Mov't in XY Plane = (-.4567) - (-.0468) =	-.4099"
Lateral Mov't off XY Plane = $\sqrt{(1.1061)^2 + (.4099)^2}$ =	1.1796"

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CALCULATION FOR

ORIGINATOR

DATE

REVIEWER M. Z. Lee

DATE 12/5/73

RESULTS

MSV-48F Summary
MSEJ-14

DIRECTION	WITHOUT STACK MOVEMENT	WITH STACK MOVEMENT
AXIAL	.2766"	.8827"
XY	-.0651"	-.4099"
Z	+1.1061"	+1.1061"
LATERAL	1.1080"	1.1796"

Design Conditions

Axial = .84"

Lateral = 1.42"

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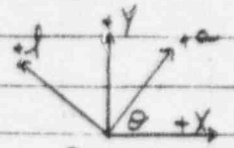
	PROJECT: CR UNIT 3	W.O.	PAGE 1 OF 6
SYSTEM: CR-5		ORIGINATOR: A. ECKENROTH	
CALCULATION FOR: Movement of Safety Valve MSV-36		DATE 12/6/73	
		REVIEWER: N. Z. Lee	
		DATE 12/8/73	

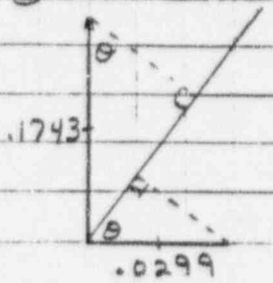
RESULTS

Thermal (Revision #1) movements @ Pt. IH-782

$\Delta X = +.0299"$
$\Delta Y = +.1743"$
$\Delta Z = +.8079"$ $\theta = 53°$



Facing East



Axial Mov't $= (+.1743)\sin\theta + (+.0299)\cos\theta =$
$(+.1392) + (+.0180) =$
$+.1572"$

Lateral Mov't in XY Plane $=$
$(+.1743)\cos\theta - (+.0299)\sin\theta =$
$(+.1049) - (+.0239) =$
$+.0810"$

Lateral Mov't off XY Plane $(\Delta Z = +.8079")$

Absolute Lateral Mov't $= \sqrt{(.8079)^2 + (\text{Lateral Mov't in XY})^2}$

$\sqrt{(.8079)^2 + (.0810)^2} =$

$.8120"$

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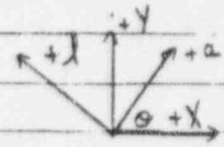
RESULTS

Safety Valve Loads (case #2) mov't @ Pt. IH-782

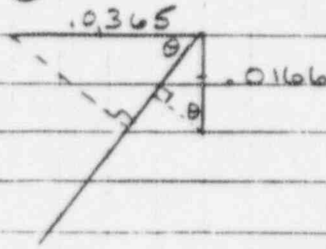
$\Delta X = -.0365"$

$\Delta Y = -.0166"$

$\Delta Z = -.0162"$ $\quad \theta = 53°$



Facing East



Axial Mov't = $(-.0166)\sin\theta + (-.0365)\cos\theta =$
$(-.0133) + (-.0220) =$
$-.0353"$ or $0"$

Lateral Mov't in XY Plane =
$(-.0166)\cos\theta - (-.0365)\sin\theta =$
$(-.0100) - (-.0292) =$
$+.0192"$ or $0"$

Lateral Mov't off XY Plane ($\Delta Z = -.0162"$)

Absolute Lateral Mov't = $\sqrt{(.0162)^2 + (\text{Lateral Mov't in XY})^2}$

$\sqrt{(.0162)^2 + (.0192)^2} =$

$.0251"$

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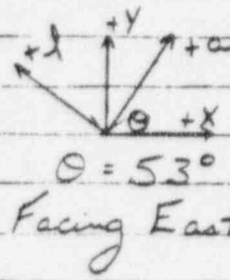
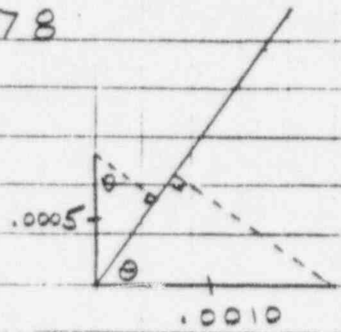
	RESULTS

Seismic Mov't @ Pt. NC-78

ΔX = ± .0010"
ΔY = ± .0005"
ΔZ = ± .0007"





Axial Mov't = (±.0005) Sin θ + (±.0010) Cos θ =
(±.0004) + (±.0006) =
±.0010"

Lateral Mov't in XY Plane =
(±.0005) Cos θ − (±.0010) Sin θ =
(±.0003) − (±.0008) =
±.0011"

Lateral Mov't off XY Plane (ΔZ = ±.0007")

Absolute Lateral Mov't = $\sqrt{(.0007)^2 + (\text{Lateral Mov't in XY})^2}$ =

$\sqrt{(.0007)^2 + (.0011)^2}$ =

.0013"

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CALCULATION FOR		REVIEWER DATE
		RESULTS

Stack Mov't due to Thermal Expansion

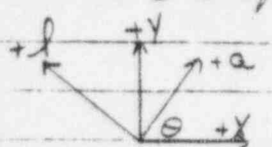
ELEV of anchor in roof = 149'-0"

ELEV of safety valve = 128'-7 1/8"

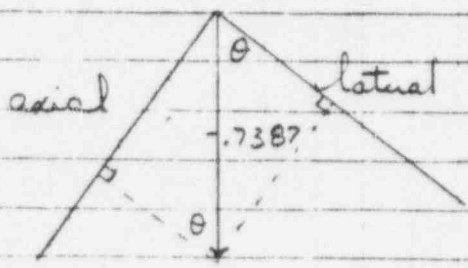
Length of stack = 20'-4 7/8"

* Expansion of A106 GR B steel @ 500°F = .0362 in/ft. of pipe

20.4063 ft x .0362 in/ft = .7387 in



θ = 53°
Facing East



Axial Mov't = (-.7387) Sin θ = **-.5900" (compressive)**

Lateral Mov't in XY Plane = (-.7387) Cos θ = **-.4446"**

* Temperature is found in pipe specifications (page 65) for Safety Valve Relief Lines

GAI 350 REV. 10-72

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CALCULATION FOR		REVIEWER / DATE

	RESULTS
Total Mov't @ Pt IH-782	
Thermal + Safety Valve + Seismic Mov't	
Axial Mov't = (+.1572) + (-.0353) + (+.0010) =	+.1229"
	or
When Safety Valve is closed = (+.1572) + (+.0010) =	+.1582" (compressive)
Lateral Mov't in XY Plane = (+.0810) + (+.0192) + (+.0011) =	+.1013"
When Safety Valve is closed = (+.0810) + (-.0011) =	+.0799"
Mov't in Z Direction = (+.8079) + (-.0162) + (+.0007) =	+.7924"
When Safety Valve is closed = (+.8079) + (+.0007)	+.8086"
Lateral Mov't off XY Plane = $\sqrt{(.8086)^2 + (.1013)^2}$ =	.8149"
Total Movement	
Axial Mov't = (.5900) + (.1582) =	.7482"
Lateral Mov't in XY Plane = (-.4446) - (+.1013) =	-.5459"
Lateral Mov't off XY Plane = $\sqrt{(.8086)^2 + (.5459)^2}$ =	.9756"

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CALCULATION FOR

DATE

REVIEWER

DATE

RESULTS

MSV-36 Summary
MSEJ-11

DIRECTION	WITHOUT STACK MOVEMENT	WITH STACK MOVEMENT	RESULTS
AXIAL	.1582"	.7482"	Compression
XY	+.1013"	-.5459"	
Z	+.8086"	+.8086"	
LATERAL	.8149"	.9756"	

Design Conditions

Axial = 0.9" compression

Lateral = 0.84"

FILING CODE

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT: FPC	FILING CODE	
	PROJECT: CR UNIT #3	W.O. 4243-027	PAGE 1 OF 6
SYSTEM: CR-6A		ORIGINATOR: A ECKENROTH	
		DATE 12/3/73	
CALCULATION FOR: Movement on Safety Valve MSV-47F		REVIEWER: M. Z. Lee	
		DATE 12/5/73	

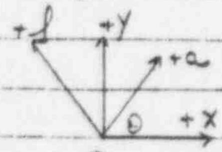
RESULTS

Thermal (Revision #1) movements @ Pt ID-723

$\Delta X = +.1752"$

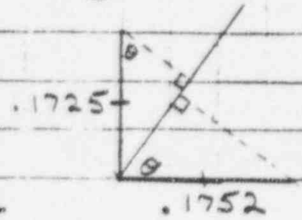
$\Delta Y = +.1725"$

$\Delta Z = +.9191"$



$\theta = 53°$

Facing East



Axial Mov't = (+.1725) Sin θ + (+.1752) Cos θ =
(+.1378) + (+.1054) =
+.2432"

Lateral Mov't in XY Plane =
(+.1725) Cos θ − (.1752) Sin θ =
(+.1038) − (+.1399) =
−.0361"

Lateral Mov't off XY Plane =

Absolute Lateral Mov't = $\sqrt{(.9191)^2 + (\text{Lateral Mov't in XY})^2}$ =

$\sqrt{(.9191)^2 + (.0361)^2}$ =

.9198"

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
	PROJECT	W.O.	PAGE 2 OF 6
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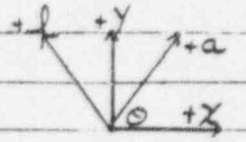
CALCULATION FOR		REVIEWER	DATE

RESULTS

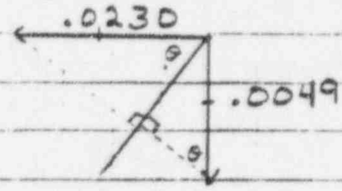
Safety Valve Loads (case #1) mov't @ Pt. ID-723

$\Delta X = -.0230''$
$\Delta Y = -.0049''$
$\Delta Z = +.0103''$



$\theta = 53°$

Facing East



Axial Mov't $= (-.0049)\sin\theta + (-.0230)\cos\theta =$
$(-.0039) + (-.0138) =$
$-.0177''$ or $0''$

Lateral Mov't in XY Plane $=$
$(-.0049)\cos\theta - (-.0230)\sin\theta$
$(-.0029) - (-.0184) =$
$+.0155''$ or $0''$

Lateral Mov't off. XY Plane $=$

Absolute Lateral Mov't $=$ $\sqrt{(.0103)^2 + (\text{Lateral Mov't in XY})^2} =$

$\sqrt{(.0103)^2 + (.0155)^2} =$

$.0186''$

FILING CODE

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT PROJECT	FILING CODE W.O. PAGE 3 OF 6
SYSTEM		ORIGINATOR
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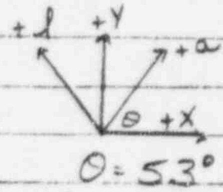
RESULTS

Seismic Mov't @ Pt. NA-72

$\Delta X = \pm .0089"$

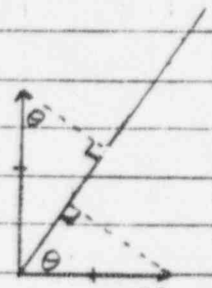
$\Delta Y = \pm .0231"$

$\Delta Z = \pm .0088"$



$\theta = 53°$

Facing East



Axial Mov't = $(\pm.0231)\sin\theta + (\pm.0089)\cos\theta$

$(\pm.0184) + (\pm.0054) =$

$\pm .0238"$

Lateral Mov't in XY Plane =

$(\pm.0231)\cos\theta - (\pm.0089)\sin\theta$

$(\pm.0139) - (\pm.0071) =$

$\pm .0068"$

Lateral Mov't off XY Plane

Absolute Lateral Mov't = $\sqrt{(.0088)^2 + (\text{Lateral Mov't in XY})^2} =$

$\sqrt{(.0088)^2 + (.0068)^2} =$

$.0111"$

FILING CODE

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE
	PROJECT	W.O. / PAGE 4 OF 6
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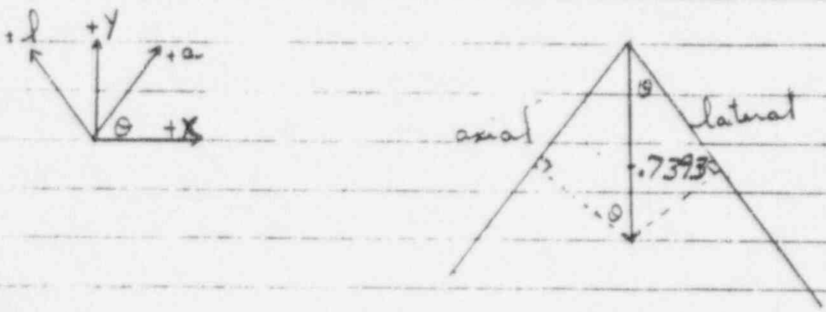
CALCULATION FOR		DATE / REVIEWER / DATE

	RESULTS
Stack Mov't due to Thermal Expansion	
ELEV. of anchor in roof = 149'-0"	
ELEV of safety valve = 128'-6 15/16"	
Length of stack = 20'-5 1/16"	
* Expansion of A106-GR B steel @ 500°F = .0362 in / ft. of pipe	
20.4219 ft x .0362 in/ft = .7393 in	
	
Axial Mov't = (-.7393) Sin θ =	-.5904" (compressive)
Lateral Mov't in XY Plane = (-.7393) Cos θ =	-.4449"
* Temperature is found in pipe specifications (page 65) for Safety Valve Relief Lines.	

GAI 350 REV. 10-72

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
	PROJECT	W.O.	PAGE 5 OF 6
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CALCULATION FOR		DATE	
		REVIEWER	
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	RESULTS
Total Mov't @ Pt. ID-723 =	
Thermal + Safety Valve + Seismic Mov't	
Axial Mov't = (+.2432) + (-.0177) + (+.0238) =	+.2493"
	OR
When Safety Valve is closed = (+.2432) + (+.0238) =	+.2670" (compressive)
Lateral Mov't in XY Plane = (-.0361) + (+.0155) + (+.0068) =	-.0138"
	OR
When Safety Valve is closed = (-.0361) + (-.0068) =	-.0429"
Mov't in Z Direction = (+.9191) + (+.0103) + (+.0088) =	+.9382"
	OR
When Safety Valve is closed = (+.9191) + (+.0088) =	+.9279"
Lateral Mov't off XY Plane = $\sqrt{(.9382)^2 + (.0429)^2}$ =	.9392"
Total Movement	
Axial Mov't = (.2493) + (.5904) =	.8397"
Lateral Mov't in XY Plane = (-.4449) - (-.0138) =	-.4311"
Lateral Mov't off XY Plane = $\sqrt{(.9382)^2 + (.4311)^2}$	1.0325"

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GAI 350 REV. 10-72

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE
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CALCULATION FOR		DATE / REVIEWER / DATE

MSV - 47F Summary
MSEJ - 18

DIRECTION	WITHOUT STACK MOVEMENT	WITH STACK MOVEMENT
AXIAL	.2670"	.8397"
XY	-.0429"	-.4311"
Z	+.9382"	+.9382"
LATERAL	.9392"	1.0325"

Design Conditions
Axial = .84"
Lateral = 1.32"

RESULTS

FILING CODE

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT FPC	FILING CODE	
	PROJECT	W.O.	PAGE 1 OF 6

SYSTEM CR-6A

ORIGINATOR A. ECKENROTH DATE 12/6/73

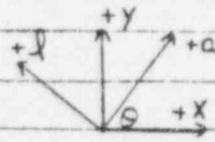
CALCULATION FOR Movement on Safety Valve MSV-35

REVIEWER M. Z. Lee DATE 12/08/73

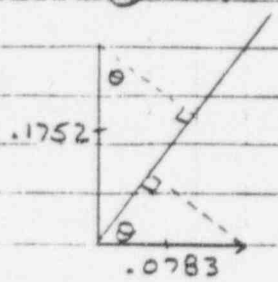
RESULTS

Thermal (Revision #1) movements @ Pt IG-853

ΔX = +.0783"
ΔY = +.1752"
ΔZ = +.6318"



θ = 53°
Facing East



Axial Mov't = (+.1752) Sin θ + (+.0783) Cos θ =
(+.1399) + (+.0471) =
+.1870"

Lateral Mov't in XY Plane =
(+.1752) Cos θ − (.0783) Sin θ
(+.1054) − (+.0625) =
+.0429"

Lateral Mov't off XY Plane (ΔZ = +.6318")

Absolute Lateral Mov't = $\sqrt{(.6318)^2 + (\text{Lateral Mov't in XY})^2}$ =

$\sqrt{(.6318)^2 + (.0429)^2}$ =

.6333"

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PROJECT

FILING CODE

W.O.

SYSTEM

ORIGINATOR

DATE

CALCULATION FOR

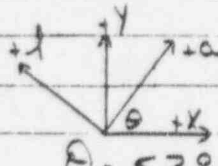
REVIEWER

DATE

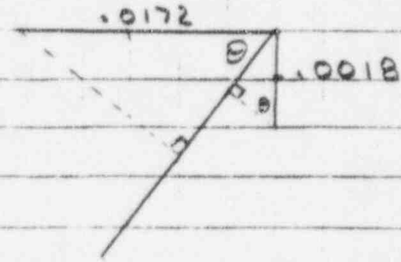
RESULTS

Safety Valve Loads (case #1) mov't @ Pt. IG-853

ΔX = −.0172"
ΔY = −.0018"
ΔZ = −.0013"



θ = 53°
Facing East



Axial Mov't = (−.0018) Sin θ + (−.0172) Cos θ =
(−.0014) + (−.0104) =
−.0118" or 0"

Lateral Mov't in XY Plane =
(−.0018) Cos θ − (−.0172) Sin θ =
(−.0010) − (−.0137) =
+.0127" or 0

Lateral Mov't off XY Plane (ΔZ = +.0013)

Absolute Lateral Mov't = $\sqrt{(.0013)^2 + (\text{Lateral Mov't in XY})^2}$ =

$\sqrt{(.0013)^2 + (.0127)^2}$ =

.0128"

FILING CODE

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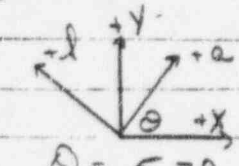
CALCULATION FOR		REVIEWER	
		DATE	

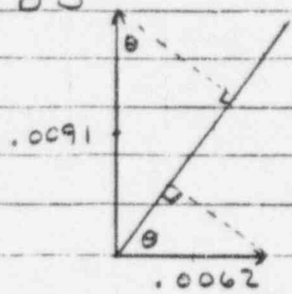
RESULTS

Seismic Mov't @ Pt. NG-85

$\Delta X = \pm .0062''$
$\Delta Y = \pm .0091''$
$\Delta Z = \pm .0160''$



θ = 53°
Facing East



Axial Mov't = $(\pm.0091)\sin\theta + (\pm.0062)\cos\theta =$
$(\pm.0073) + (\pm.0037) =$
$\pm.0110''$

Lateral Mov't in XY Plane =
$(\pm.0091)\cos\theta - (\pm.0062)\sin\theta$
$(\pm.0055) - (\pm.0050) =$
$\pm.0105''$

Lateral Mov't off XY Plane ($\Delta Z = \pm.0160''$)

Absolute Lateral Mov't $= \sqrt{(.0160)^2 + (\text{Lateral Mov't in XY})^2}$

$\sqrt{(.0160)^2 + (.0105)^2} =$

$.0191''$

FILING CODE

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CALCULATION FOR		REVIEWER / DATE

Stack Mov't due to Thermal Expansion

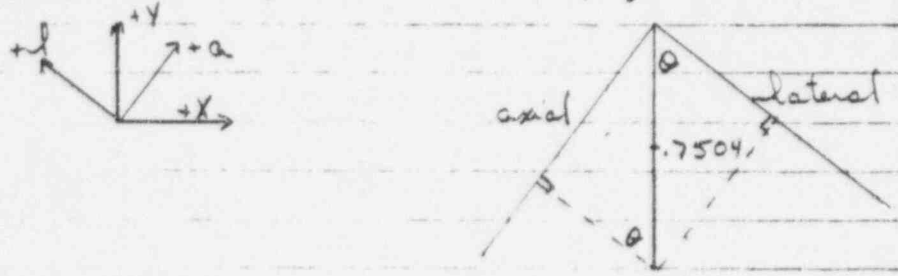
ELEV of anchor in roof = 149'-0"

ELEV of safety valve = 128'-3 1/4"

Length of stack = 20'-8 3/4"

*Expansion of A106 GR. B steel @ 500°F = .0362 in/ft of pipe

20.7292 ft x .0362 in/ft = .7504 in.



	RESULTS
Axial Mov't = (-.7504) Sin θ =	-.5993" (compressive)
Lateral Mov't = (-.7504) Cos θ =	-.4516"

*Temperature is found in pipe specifications (page 65) for Safety Valve Relief Lines

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
	PROJECT	W.O.	PAGE 5 OF 6
SYSTEM		ORIGINATOR	
CALCULATION FOR		DATE	
		REVIEWER	
		DATE	

	RESULTS
Total Mov't @ Pt IG-853	
Thermal + Safety Valve + Seismic Mov't	
Axial Mov't = (+.1870) + (-.0118) + (+.0110) =	+.1862"
	or
When Safety Valve is closed = (+.1870) + (+.0110)	+.1980 (compressive)
Lateral Mov't in XY Plane = (+.0429) + (+.0127) + (+.0105) =	+.0661"
	or
When Safety Valve is closed (+.0429) + (-.0105) =	+.0324"
Mov't in Z Direction = (+.6318) + (-.0013) + (+.0160) =	+.6465"
	or
When Safety Valve is closed (+.6318) + (+.0160) =	+.6478"
Lateral Mov't off XY Plane = $\sqrt{(.6478)^2 + (.0661)^2}$ =	.6512"
Total Movement	
Axial Mov't = (.5993) + (.1980) =	.7973"
Lateral Mov't in XY Plane = (-.4516) - (+.0661) =	-.5177"
Lateral Mov't off XY Plane = $\sqrt{(.6478)^2 + (.5177)^2}$ =	.8293"

FILING CODE

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
	PROJECT	W.O.	PAGE 6 OF 6
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CALCULATION FOR		DATE	
		REVIEWER	
		DATE	

MSV-35F Summary
MSEJ-15

DIRECTION	WITHOUT STACK MOVEMENT	WITH STACK MOVEMENT	RESULTS
AXIAL	.1980"	.7973"	Compression
XY	+.0661"	-.5177"	
Z	+.6478"	+.6478"	
LATERAL	.6512"	.8293"	

Design Conditions

Axial = 0.84"

Lateral = 0.76"

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	PROJECT	W.O. / PAGE OF
SYSTEM CR-3		ORIGINATOR G. ARAUZ / DATE 1-3-73
CALCULATION FOR Movement on Safety Valve MSV-46V		REVIEWER / DATE

RESULTS

Stack Mov't due to Thermal Expansion

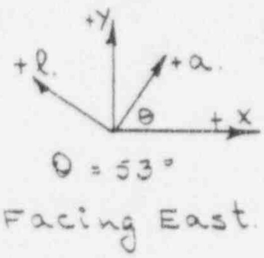
ELEV of anchor in roof = 149'-0"

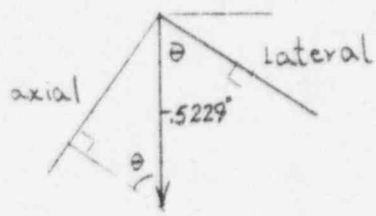
ELEV. of safety valve = 128'-3"

Length of stack = 20'-9"

Expansion of A106-GR. B steel @ 380°F = .0252 in/ft. of pipe.

20.75 ft x .0252 in/ft = 0.5229 in





Axial Mov't = (-0.5229) sin. θ = **-.4176"** (compressive)

Lateral Mov't in XY Plane = (-0.5229) cos. θ = **-.3147"**

..

FILING CODE

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
	PROJECT	W.O.	PAGE OF
SYSTEM		ORIGINATOR G. ARAUZ DATE 1-3-74	
CALCULATION FOR		REVIEWER DATE	

RESULTS

Total Mov't @ Pt. HO-51

Thermal + Safety Valve + Seismic Mov't

Axial Mov't = (+.3232) + (-.0283) + (+.0077) = +.3026"

OR

When Safety Valve is Closed = (+.3232) + (+.0077) = +.3309" (compressive)

Lateral Mov't in XY Plane =
(-.1374) + (+.0299) + (+.0040) = -.1035"

OR

When Safety Valve is Closed = (-.1374) + (-.0040) = -.1414"

Mov't in Z direction =
(+.8246) + (+.0614) + (+.0278) = +.9138"

OR

When safety Valve is closed = (+.8246) + (+.0278) = +.8524

Lateral Mov't off XY Plane =

$$\sqrt{(.9138)^2 + (.1414)^2} = .9247"$$

Total Movement

Axial Mov't = (.3309) + (.4176) = .7485

Lateral Mov't in XY Plane = (-.3147) - (-.1035) = -.2112"

Lateral Mov't off XY Plane =

$$\sqrt{(.9138)^2 + (.2112)^2} = .9379"$$

FILING CODE

GAI 350 REV. 10-72

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE
	PROJECT	W.O. / PAGE OF
SYSTEM		ORIGINATOR G. ARAUZ
CALCULATION FOR		DATE 1-3-74
		REVIEWER
		DATE

MSV-46F SUMMARY
MSEJ-4

DIRECTION	WITHOUT STACK MOVEMENT	WITH STACK MOVEMENT	RESULTS
AXIAL	.3309"	.7485"	Compression
X - Y	-.1414"	-.2112"	
Z	+.9138"	+.9138"	
LATERAL	.9247"	.9379"	

Design Conditions

Axial = .85" Compression max

Lateral = .81"

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT F P C. PROJECT CR # 3	FILING CODE	
		W.O.	PAGE OF
SYSTEM CR - 3		ORIGINATOR G. ARAUZ DATE 1-3-74	
CALCULATION FOR Movement of Safety Valve MSV-42		REVIEWER DATE	

STACK MOV'T DUE TO THERMAL EXPANSION

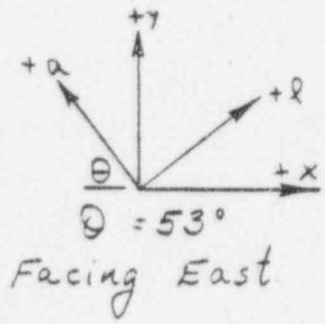
ELEV of ANCHOR IN ROOF = 149'-0"

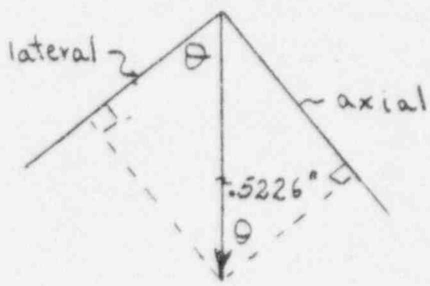
ELEV. OF SAFETY VALVE = 128'-3 1/8"

LENGTH OF STACK = 20'-8 7/8"

Expansion of A106-GR-B steel @ 380°F = .0252 in/ft. of pipe

20.7396 ft × .0252 in/ft = 0.5226 in





		RESULTS
Axial Mov't = (-.5226) sin θ	=	-.4174" (Compressive)
Lateral Mov't in XY Plane = (-.5226) cos θ	=	-.3145"

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
	PROJECT	W.O.	PAGE OF
SYSTEM		ORIGINATOR G. ARAUZ DATE 1-3-74	
CALCULATION FOR		REVIEWER DATE	

RESULTS

TOTAL MOV'T @ Pt. HP-58 =

Thermal + Safety Valve + Seismic Mov't

	RESULTS
Axial Mov't = (+.1588) + (+.0037) + (+.0027) =	+.1652" OR
When Safety Valve is closed = (+.1588) + (+.0027) =	+.1615" (compressive)
Lateral Mov't in xy Plane = (+.0786) + (-.0144) + (-.0030) =	+.0612" OR
When Safety is closed = (+.0786) + (+.0030) =	+.0816"
Mov't in Z Direction = (+.9852) + (+.0197) + (+.0291) =	+1.0340"
When Safety Valve is closed = (+.9852) + (+.0291) =	+1.0143"
Lateral Mov't off XY Plane = $\sqrt{(1.0340)^2 + (.0816)^2}$ =	1.0372"

Total Movement.

Axial Mov't = (.4174) + (.1652) =	.5826"
Lateral Mov't in XY Plane = (-.3145) - (+.0816) =	-.3961"
Lateral Mov't off XY Plane = $\sqrt{(1.0340)^2 + (.3961)^2}$ =	1.1073"

FILING

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE
	PROJECT	W.O. / PAGE OF
SYSTEM		ORIGINATOR G. ARAUZ DATE 1-3-74
CALCULATION FOR		REVIEWER DATE

MSY-42F SUMMARY
MSEJ-3

DIRECTION	WITHOUT STACK MOVEMENT	WITH STACK MOVEMENT	RESULTS
AXIAL	.1652"	.5826"	Compressive
XY	+.0816"	-.3961"	
Z	+1.0340"	1.0340"	
LATERAL	1.0372"	1.1073	

Design Conditions

Axial = 0.84"

Lateral = 0.73"

File

CR #3 II-21

CRYSTAL RIVER #3

Main Steam Pipe

Steam Hammer Analysis

S4203MS02A0

For final steam hammer restraints Please see Restraints [illegible] at the back of this report

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE S4203M502A0
	PROJECT Crystal River #3	W.O. 4203-027 PAGE 1 OF
SYSTEM Main Steam Ping		ORIGINATOR M.Z. Lee DATE 11/2/73
CALCULATION FOR Steam Hammer		REVIEWER
		DATE

RESULTS

Assumptions

1. Turbine emergency stop valves are energized to close when the turbine is operating at max load.

2. No steam is extracted or released from the main steam piping when the valve is closing and sometime thereafter.

3. Turbine emergency stop valves close according to the time history shown in Fig. 1.

4. Net travelling time of valve is 0.15 Sec.

FILING CODE

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE S4203MS02A0
	PROJECT Crystal River #3	W.O. / PAGE 2 OF
SYSTEM Main Steam Ping		ORIGINATOR M. Z. Lee DATE 11/2/73
CALCULATION FOR Steam Hammer		REVIEWER / DATE

DATA

Operating Conditions

Steam Pressure	1065.0	psia
Steam Temperature	600°	F
Flow Rate	2,784,350.	#/hr
Ratio of Specific Heat, Cp/Cv	1.27	
Pipe. I.D.	22.064	in

Calculated Initial Conditions

Steam Velocity	137.8	ft/sec
Acoustic Velocity	1,722.5	ft/sec
Pressure Drop in Valve	5.344	psi
Density	0.065644	lb-sec²/ft⁴
Entropy	1.4329	BTU/lb·°R
Specific Weight	2.1137	lbs/ft³

Valve Closing Time

Information obtained from Westinghouse

Total closing time	0.25	Sec
Valve travelling time	0.15	Sec

RESULTS

FILING CODE

GAI 350 REV. 10-72

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE S4203M502A0	
	PROJECT Crystol River #3	W.O.	PAGE 3 OF
SYSTEM Main Steam Piping		ORIGINATOR M.Z. Lee	
		DATE 11/2/73	
CALCULATION FOR Steam Hammer		REVIEWER	
		DATE	

RESULTS

Unbalanced Force

Maximum pressure increase due to stop valve closure computed by GAI Computer Program M015 is

$$\Delta p_{max} = 113.27 \text{ psi}$$

$\Delta p(\tau)$ is plotted in Fig. 1 along with $A(\tau)$ for dimensionless time τ.

Maximum slope of pressure increase curve is

$$\left.\frac{dp}{d\tau}\right|_{max} = \frac{\Delta p(0.7) - \Delta p(0.4)}{0.3} = \frac{58}{0.3} = 193 \text{ psi/wave length}$$

Unbalanced Force

$$F_{max} = \Delta p_{max} \cdot A = 113.27 \cdot \frac{\pi}{4} (22.064)^2 = 43309^{lb} = 43.3 \text{ Kips}$$

$$\left.\frac{dF}{d\tau}\right|_{max} = \left.\frac{d\Delta p}{d\tau}\right|_{max} A = 193 \times \frac{\pi}{4} (22.063)^2 = 73.7 \text{ Kips/wave length}$$

It is easily seen that the maximum axial thrust on i-th section of pipe with length l_i can be approximated by

$$U_i \leq \min \left[F_{max}, \frac{l_i}{\lambda} \left.\frac{dF}{d\tau}\right|_{max} \right]$$

where λ = length of pressure wave

FILING CODE

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For valve closing time $t_c = 0.15$ sec, the wave length is

$$\lambda = V_a t_c = 1722.5 \times 0.15 = 258 \text{ ft}$$

where V_a = acoustic velocity = 1722.5 ft/sec

Pressure gradient and unbalanced force gradient

$$\left.\frac{dp'}{dl}\right|_{max} = \frac{193}{258} = 0.75 \text{ psi/ft of pipe}$$

$$\left.\frac{dF}{dl}\right|_{max} = \frac{73.7}{258} = 0.286 \text{ Kips/ft of pipe}$$

RESULTS

FILING CODE

CAL 250 REV

S 4203 M502A0 p5

	MADE 11/2/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
	CHK'D.	
	DG. CF.	
Crystal River #3	CF. DFN.	4203-027
Main Steam Steam Hammer	ENG. M.Z. Lee	WORK ORDER / SIZE / DRAWING / REV.
	REV. CK. APP. DATE	

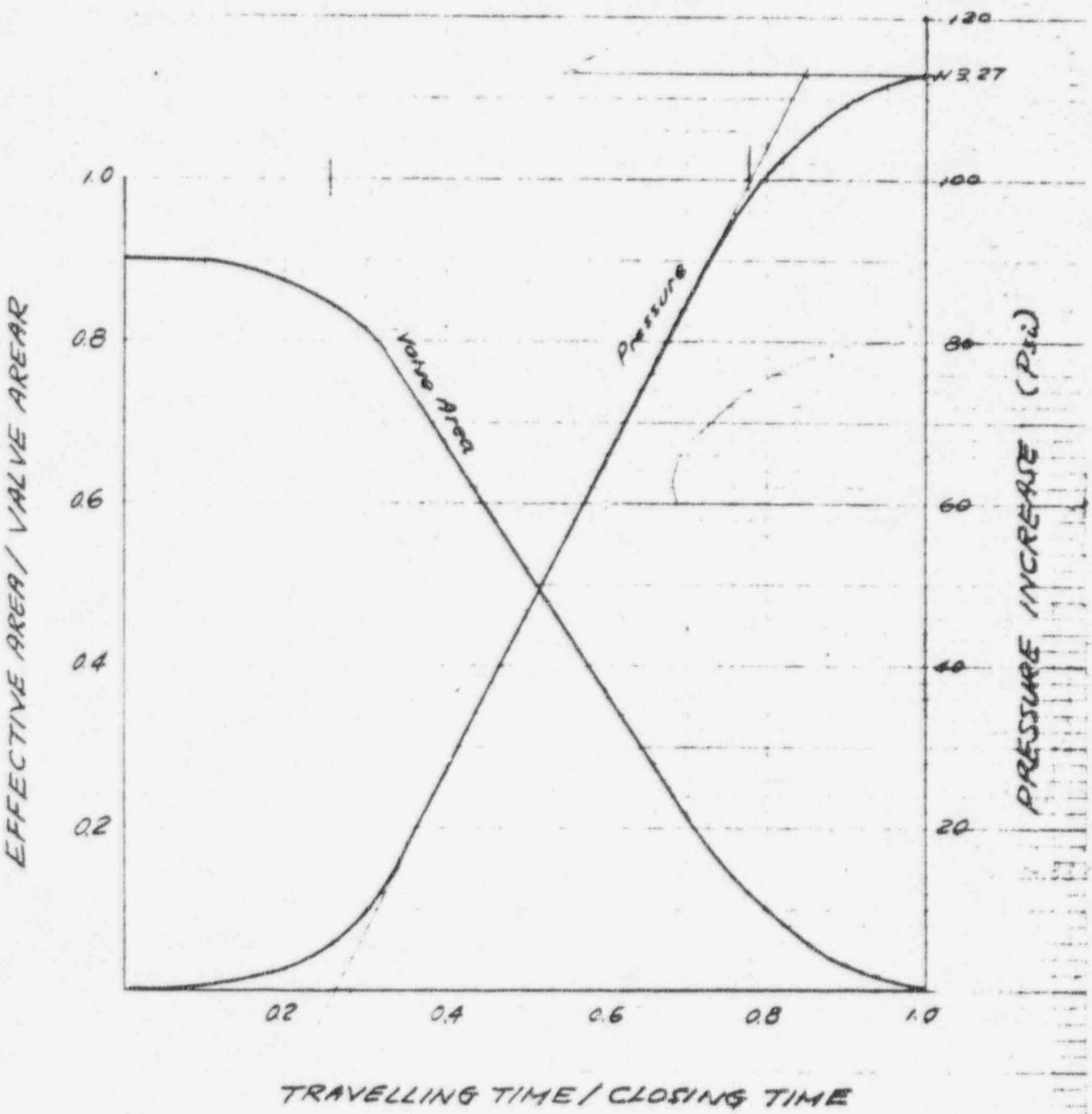

Fig. 1.

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CLIENT

PROJECT Crystal River #3

FILING CODE S4203 MS02A0
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SYSTEM Main Steam Piping

ORIGINATOR M. Z. Lee
DATE 11/2/73

CALCULATION FOR Steam Hammer

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DATE

RESULTS

Line CR-3A & Line CR-13A (Fig. 2)

Sec. No. i	Length l_i	Force U_i	Existing Snubber Capacity	Additional Snubber	Notes	Results
1	27.552	7.85	0 Kips		Connected to Turbine Stop valve	
2	29.438	8.4	49.5			MSH-237
3	67.25	19.2	49.5			-238
4	12.73	3.6	49.5			-239
5	23.75	6.6	49.5			-240
6	21.406	6.0	0		Restrained by Penetr. Anchor	
7	21.469	6.0	0		"	
8	16.88	4.7	0		"	
9	19.6	5.5	0	49.5 Kip		MSH-162
10	22.99	6.3	0	49.5		
11	9.67	2.7	0	30		
12	23.672	6.7	0		Connected to Steam Gen.	

FILING CODE

S4203 MS02 A0 107

Crystal River #3	MADE 11/2/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
Main Steam Piping	CHK'D.	
Steam Hammer	SQ. CF.	
	CF. DFN.	4203-027
	ENG. M. Z. Lee	WORK ORDER / SIZE / DRAWING / REV.
	REV. CK. APP. DATE	

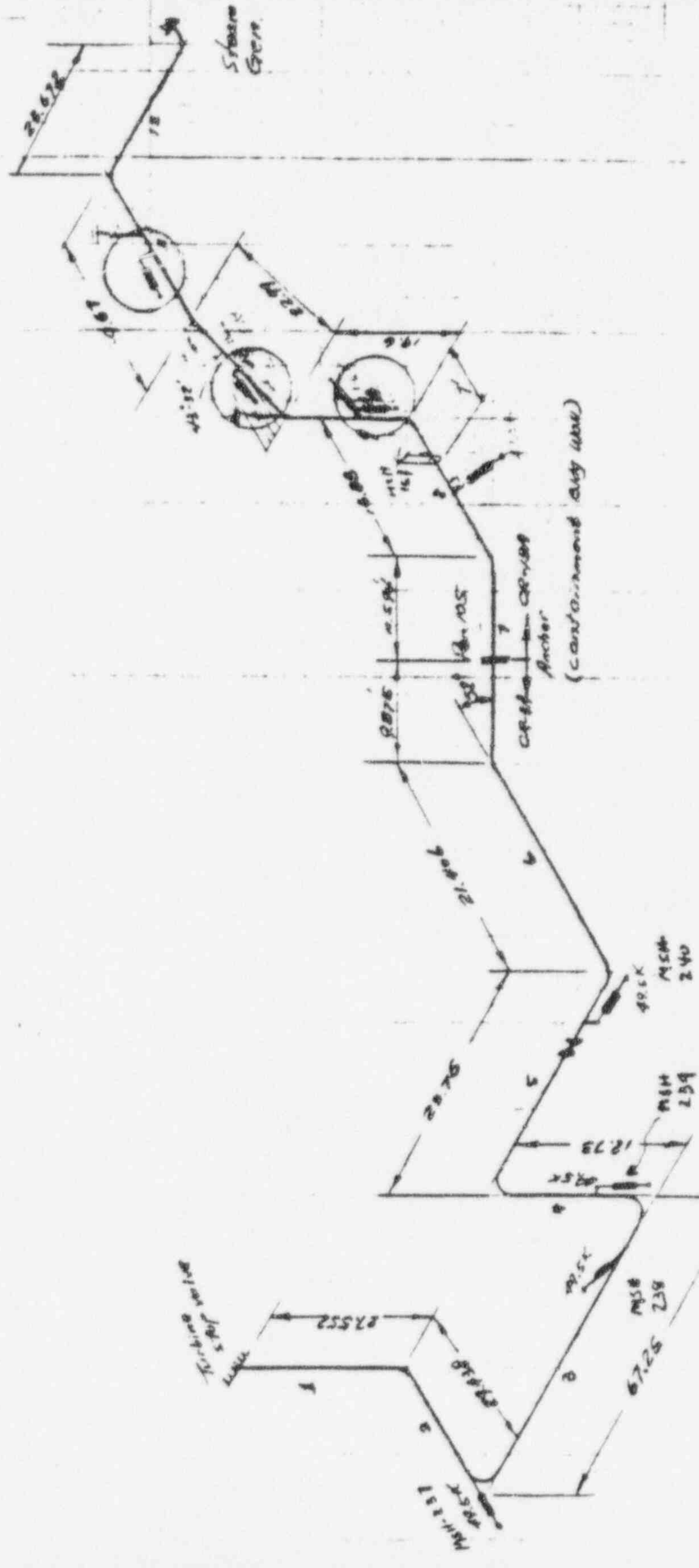

Fig. 2 Lines CR-3 & CR-13

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RESULTS

Line CR-3 Outside Containment Bldg.

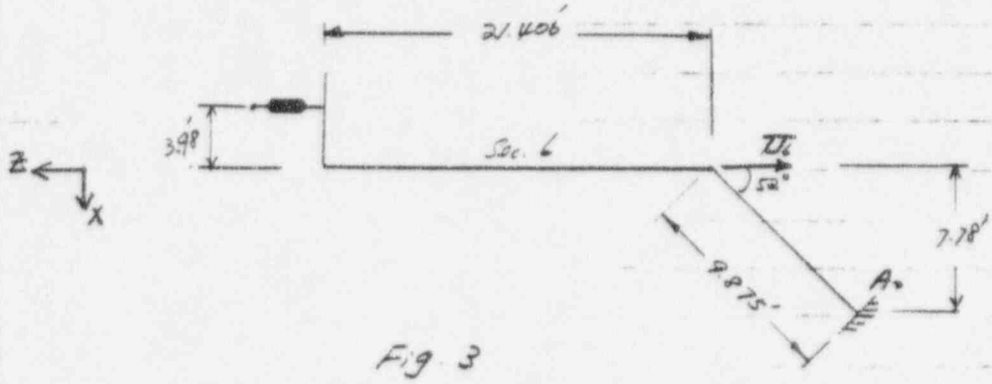

Fig. 3

Stresses at A_2 from Piping Stress Program

Vibration (Y-Z)	853 psi	
S.V. Discharge	761	
Pressure $(\frac{PD}{4t})$	6500	Stress Program gives DL & Pr stress = 4691

Allowable Stress $= 1.2 S_h = 18,000$ psi

Bending Stress at A_2 due to Steam Hammer.

$M = T_6 \sin 52° \times l$

$= T_6 \times (9.875 \times 12) \sin 52° = 93.4\ T_6$ lb-in

$S_b = \frac{M}{Z} = \frac{93.4}{388} T_6 = \frac{1}{4.16} T_6$

Let $S_b = 18,000 - 853 \times 2^{DLF} - 761 \times 1.5^{DLF} - 6500$

$= 8650$ psi

Then $T_6 = 4.16 \times 8,650 = 36,000^{lb} = 36$ Kips

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RESULTS

If the pressure wave has a form of Fig 1 the max unbalanced force on Sec 6 is 6 Kips

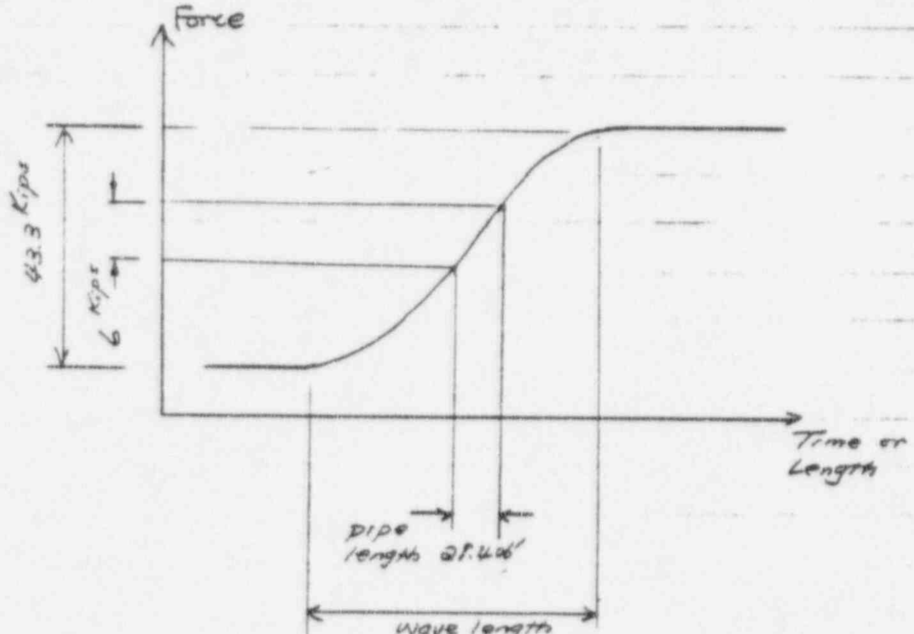

Fig. 4

Though the form of pressure wave may deviate from Fig 1 and results in steeper slope consequently larger unbalanced force, it is unlikely that the unbalanced force will reach say 20 Kips in the section of pipe 21' long when the normal wave length is 258 ft

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RESULTS

Line CR-13 Inside Pen. 105 (Ref. Fig. 2)

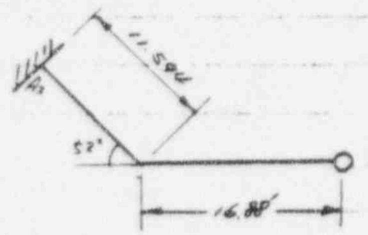

Fig. 5

Stresses at A_2 from Piping Stress Program

Vibration (X-Y)	516 psi
Pressure	6,500

Bending stress allowed for steam Hammer

$S_b = 18,000 - 516 \times 2 - 6500 = 10,468$ psi

$M = U_8 \times (11.594 \times 12) \sin 52° = 109.2\, U_8$

Let $\frac{M}{Z} = S_b = 10,468$

$U_8 = \frac{388}{109.2} \times 10,468 = 37,000$ lbs $= 37$ Kips

Calculated U_8 for max $\frac{dp}{dt}$ is 4.7 Kips.

No additional support is recommended.

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CALCULATION FOR Steam Hammer		DATE 11/2/73
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		RESULTS

Line CR-13A at EL 142'-10¾" Near Steam Gen.

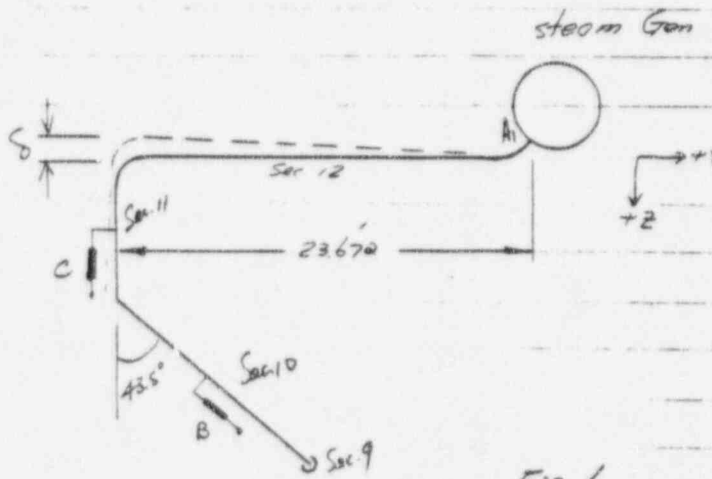

Fig. 6

Consider sec. 12 as a cantilever fixed at Gen.
Then

$$\delta = \frac{Pl^3}{3EI}, \quad \sigma = \frac{M}{Z} = \frac{Pl\,d/2}{I}$$

$$\therefore \delta = \frac{2}{3}\frac{\sigma}{E}\frac{l^2}{d} \quad \text{or} \quad \sigma = \frac{3}{2}\frac{Ed}{l^2}\delta$$

$$\sigma = \frac{3}{2}\frac{30\times10^6\times24}{(23.672\times12)^2}\delta = 13600\,\delta$$

Assume the snubber lock up at $\delta = \frac{1}{4}$", then

$$\sigma = 13,600\times\frac{1}{4} = 3,400 \text{ psi}$$

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RESULTS

Computer Piping stress program gives the following stresses

Vibration (x-Y)	1309 psi
Dead Load	824
Pressure (hand calculation)	6,500
Expansion	4,579

Combined Occasional stress

$S_b = 1309 + 824 + 6{,}500 + 3{,}400 = 12033$ psi
(Vib, D.L., Pr, St Hammer)

$< 1.2 S_h = 18{,}000$ psi

∴ A snubber can protect point A_1 from overstressing.

Snubber Capacity

Snubber	A	59.5 Kips	Sec. 9
	B	59.5 Kips	Sec. 10
	C	80.0 Kips.	Sec. 11

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RESULTS

Line CR-4 & Line CR-14A

Sec. No i	Length li	Force Ui	Existing Axial Snubber	Additional Axial Snubber	
1	27.552	7.9	0 Kips		Restrained by Turbine
2	35.94	10.3	49.5		
3	86.25	24.4	49.5		
4	12.58	3.6	49.5		
5	32.12	9.2	49.5		
6	20.646	5.9			Restrained by Pen. 106
7	21.355	6.1			Anchored at Pen. 106
8	14.479	4.2			Restrained by Pen. 106
9	31.578	9.1		49.5 Kips	
10	26.7	7.7	49.5		
11	26.513	7.6		30 Kips	
12	11.87	3.4		49.5 Kips	
13	20.125	5.8			Restrained by Steam Gen.

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Crystal River #3	MADE 11/2/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
	CHK'D.	
Main Steam Piping	DS. CF.	
	CF. DFN.	4203-027
Steam Hammer Analysis	ENG. M.Z. Lee	WORK ORDER / SIZE / DRAWING / REV.
	REV. CK. APP. DATE	

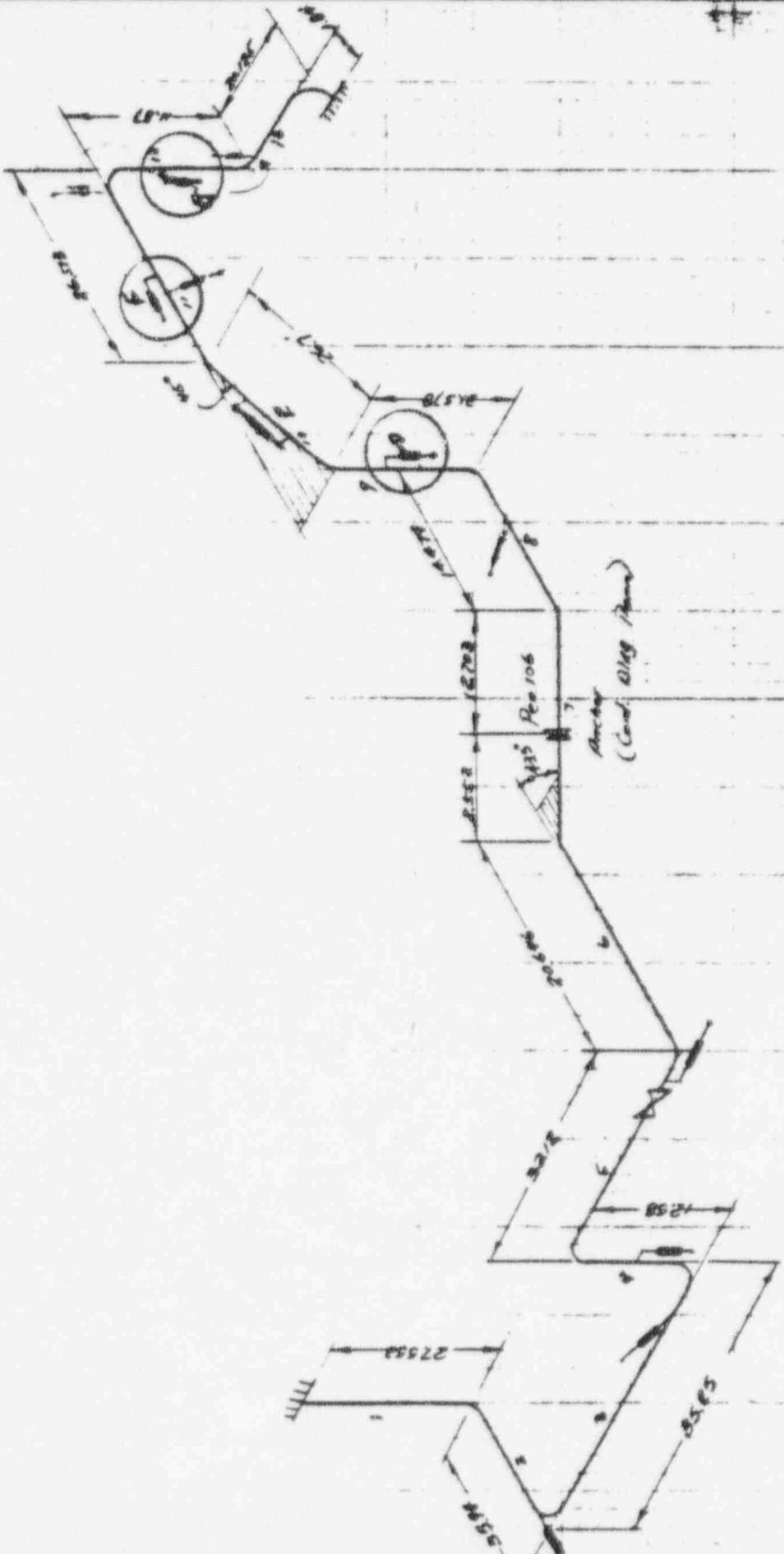

Fig. 7 Lines CR-4 & CR-14

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RESULTS

Stresses at Penetration 106

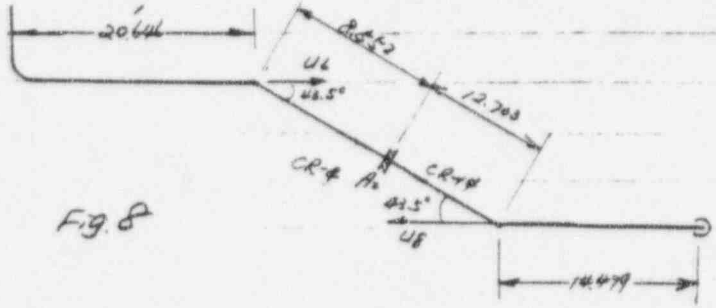

Fig. 8

Outside Pen. 106

Stresses from Piping Stress Program

Dead Load & Press.	4026 psi use	6500
Seismic		857
S. V. Disch.		357

Allowable Stress for steam Hammer

$$S_b = 18{,}000 - 6500 - 857 \times \overset{DLF}{2} - 357 \times \overset{DLF}{1.5} = 9{,}250$$

$$M = U_6 \times (8.552 \times 12) \sin 43.5^\circ = 70.7\, U_6 = S_b \cdot Z$$

$$U_6 = \frac{Z}{70.7} S_b = \frac{388}{70.7} \times 9250 = 50{,}700^{lb} > 43.3^{Kips}$$

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		RESULTS

Inside Pen. 106

Stresses from Piping Stress Program

Dead Load	349
Pressure	6,500
Seismic	1,126

Allowable Stress for Steam Hammer

$S_b = 18,000 - 349 - 6500 - 1,126 \times 2 = 9,101$

$M = U_B \times (12.703 \times 12) \sin 43.5° = 105\ U_B = S_b Z$

$U_B = \frac{Z S_b}{105} = \frac{388}{105} \times 9,101 = 33,700^{lbs} = 33.7^{Kips}$

Calculated U_B from max $\frac{dp}{dt}$ = 4.2 Kips.

Snubber Capacity

D	Sec. 9	49.5 Kps
E	Sec. 10	(49.5) Existing
F	Sec 11	30 Kips
G	Sec. 12	49.5 Kips.

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RESULTS

Line CR-5 & Line CR-15

Section i	Length l_i	Force u_i	Existing axial Snubber	Additional Axial Snubber	Notes
1	6.052	1.2 kips	kips		Restrained by Turb.
2	30.94	8.8	49.5		
3	67.0	19.	49.5		
4	28.0	8.0	49.5		
5	9.29	2.7	0	49.5 kip	No Y-Snubber on neighboring sections.
6	81.06	23.	49.5		
7	91.5	26			Anchored at Pen. 107
8	25.4	7.2		49.5 kip	
9	31.84	9.0		49.5	
10	26.87	7.6		/	Restrained by Snubbers on Secs 9 & 11
11	14.07	4.0		49.5	
12	8.32	2.4		30	Y-direction
13	16.26	4.6			

FILING CODE

Crystal River #3	MADE 11/2/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
Main Steam Piping	CHK'D. / DR. CP. / CP. DFN.	4203-027
Steam Hammer Analysis	ENG. M. Z. Lee	WORK ORDER · SIZE · DRAWING · REV.
	REV. CK. APP. DATE	

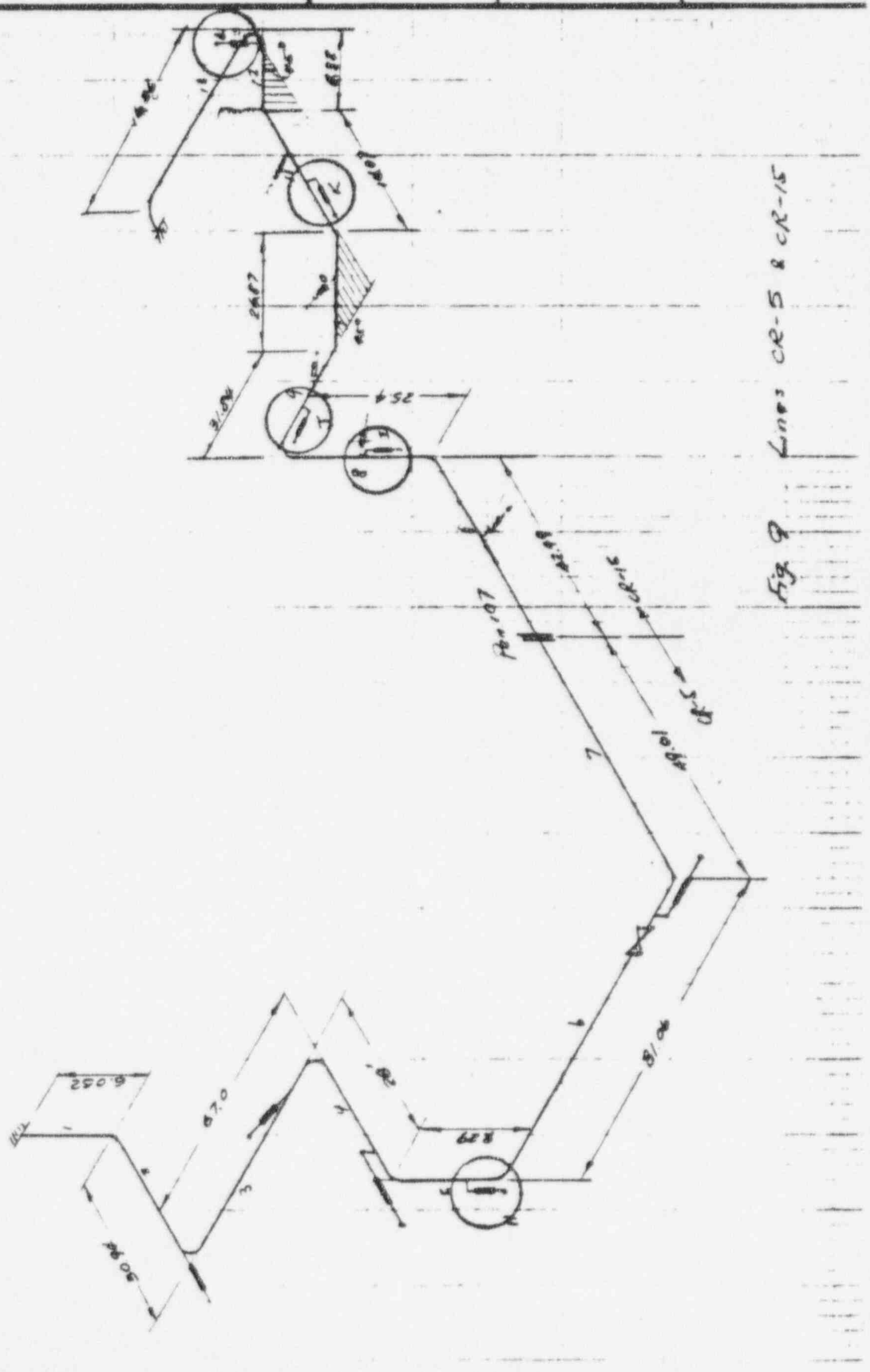

Fig. 9 Lines CR-5 & CR-15

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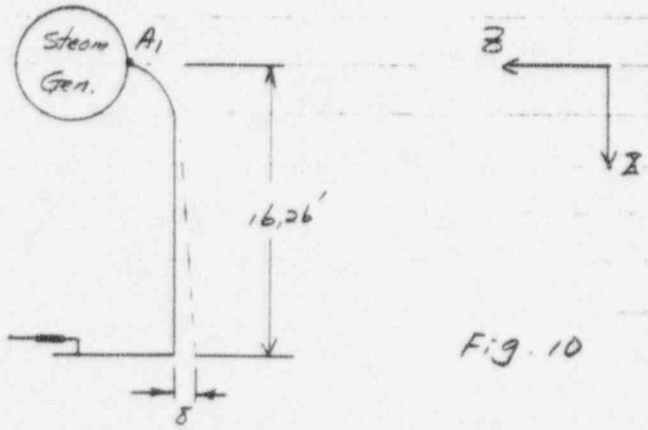

Fig. 10

$$\sigma = \frac{3}{2}\frac{Ed}{\ell^2}\delta = \frac{3}{2}\frac{30\times10^6\times24}{(16,26\times12)^2}\delta = 28,400\,\delta$$

Stresses at connection A_1 are

Vibration (Y-Z)	±104	psi
Dead Load	1058	psi
Pressure	6500	
Total	12,662	

If snubber lock up at $\frac{3}{16}$" displacement

$\sigma = 28,400 \times \frac{3}{16}" = \pm 5310$ psi

Max stress at A_1

$S_{max} = 12,662 + 5310 = 17,972$ psi $< 1.2\, S_h = 18,000$ psi

Snubber limits δ for both vibration and steam hammer as a result the stresses will be lower.

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CALCULATION FOR Steam Hammer		REVIEWER	DATE

be protected from overstress by using snubber

RESULTS

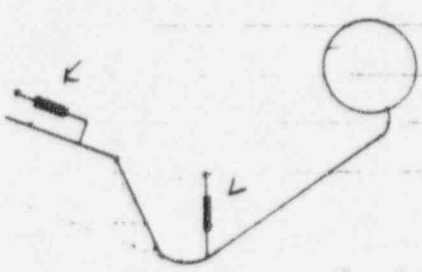

Fig. 11

Capacity of snubber in Y-direction

$43.3 \sin 45° = 30.6$ Kips

From $P = \frac{3EI}{\ell^3}\delta = \frac{3 \times 30 \times 10^6 \times 4653}{(16.26 \times 12)^3}\delta$

$= 56800\,\delta$

For $\delta = 1/8''$ $P = 56.8 \times \frac{1}{8} = 7.1$ Kips

Snubber Capacity $= 30.6 - 7.1 = 23.5$ Kips

Snubber Capacity

H	Sec. 5	49.5 Kips
I	Sec. 8	49.5
J	Sec. 9	49.5
K	Sec. 11	49.5
L	Sec 12	80

FILING CODE

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Line CR-6 & Line CR-16

RESULTS

Section i	Length l_i	Force U_i	Existing Axial Snubber	Additional Axial Snubber	Notes
1	6.052	1.7			Restrained by Turb.
2	36.938	10.6	49.5		
3	79.0	22.8	49.5		
4	28.0	8.0	49.5		
5	9.51	2.7	0	49.5	
6	98.568	28.2	49.5		
7	44.323	12.7			Restrained by Pen 108
8	33.078	9.5			Anchored at Pen 108
9	20.38	5.9			Restrained by Pen 108
10	19.474	5.6		49.5	
11	28.919	8.3		49.5	
12	16.615	7.6		30	Z-direction
13	17.026	4.9			

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Main Steam Piping	CHK'D.	
Steam Hammer Analysis	SQ. CF.	
	CF. DFN.	4203-027
	ENG. M. Z. Lee	WORK ORDER / SIZE / DRAWING / REV.
	REV. CH. APP. DATE	

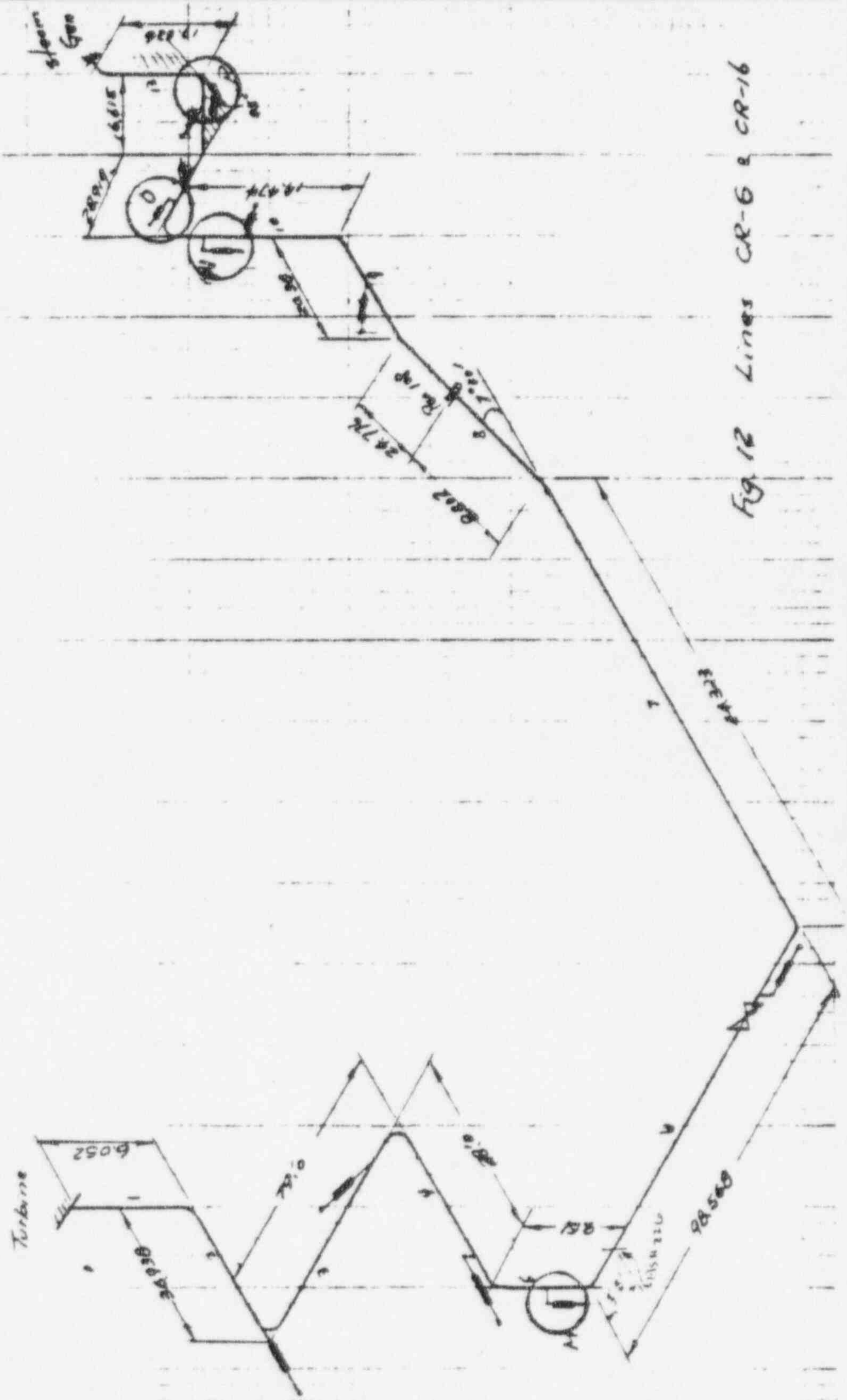

Fig. 12 Lines CR-6 & CR-16

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Summary

RESULTS

Max. Pressure Rise	113.27 psi
Max. Unbalanced Force	43.3 Kips
Wave Length for 0.15 Sec Valve Closing Time	258 ft/sec
Max Pressure Gradient	0.36 psi/ft pipe
Max Unbalance Force Gradient	0.286 Kips/ft pipe

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		REVIEWER
		DATE

RESULTS

Recommendations

Add 15 Snubbers as follows

Line No	Sec. No.	Capacity Kips	Orientation	Notes
3	9	49.5	Axial	
	10	49.5	Axial	
	11	30	Axial	
4	9	49.5	"	
	11	30	"	
	12	49.5	"	
5	5	49.5	"	
	8	49.5	"	
	9	49.5	"	} As close to Sec. 10 as is possible
	11	49.5	"	
	12n 13	30	Vertical	End of Sec. No 12 Near Sec. 13
6	5	49.5	Axial	
	10	49.5	"	
	11	49.5	"	Close to Sec. 12
	13	80	Z-dir.	Lower end of Sec. 13

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RESULTS

Steam Hammer Restraints on Branch Lines.

Pressure wave created by turbine trip may travell along all branches connected to the main steam pipes. As a result, steam hammer may hit those branches in the same way as it hits on the main lines. Therefore, it is necessory to provide proper restraints on the branch lines. The branches to be considered are

10" turbine by-pass to condender — 2 lines

6" main steam to moisture separator — 4 lines

6" main steam to emergency F.W. pump turbine — 2 Lines

Maximum unbalanced forces corresponds to pressure rise of 113.27 psi are calculated and restraints are located on sketches on the following pages.

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ORIGINATOR M. Z. Lee
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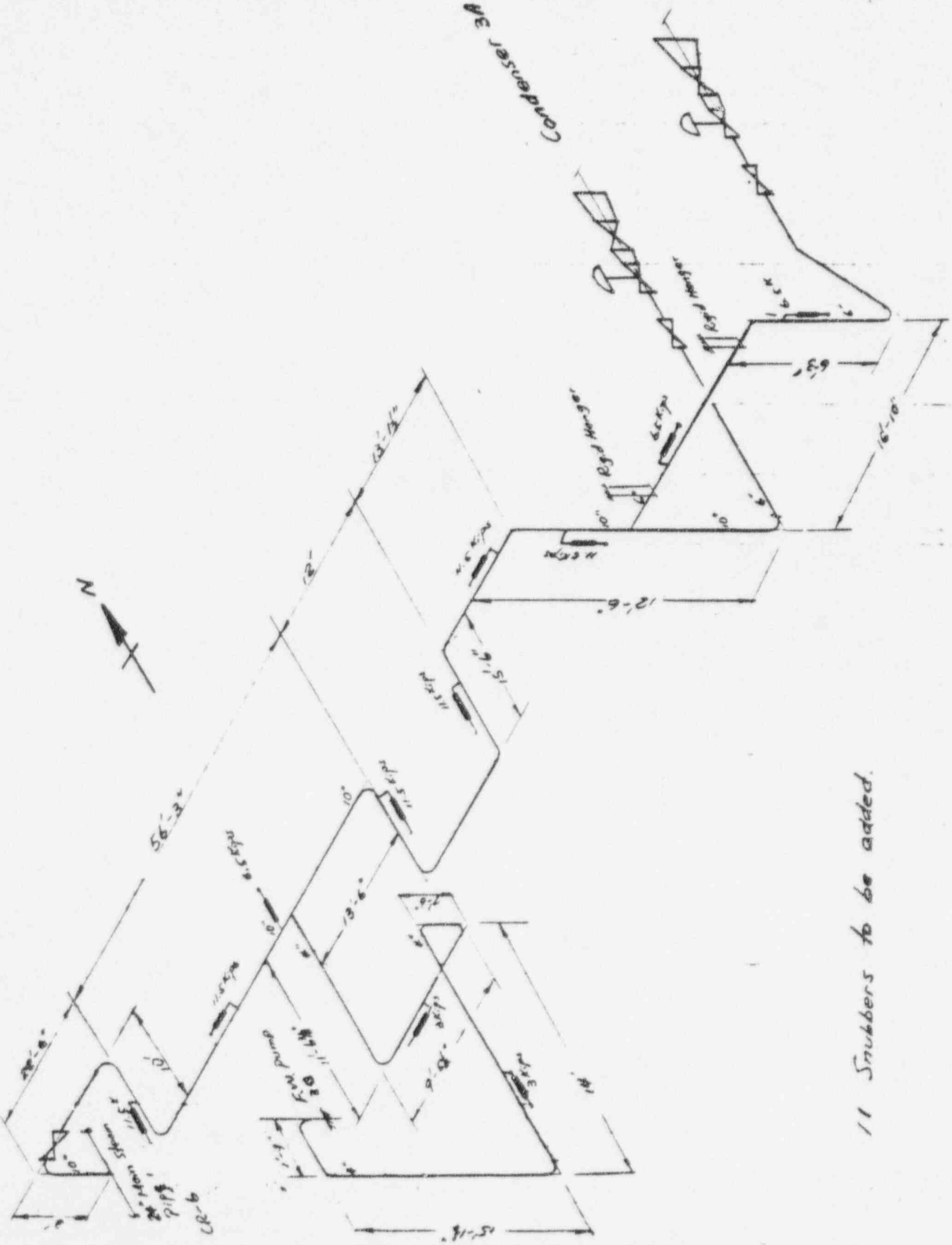
RESULTS

		10" SCH 60	6" SCH 40	4" SCH 40	
Flow Area A_f (in²)		74.7	28.9	17.73	
Max Unbalance Force $F = \Delta P_{max} \times A_f \div 1000$ (kip)		8.47	3.28	1.45	
$\frac{dF}{dl}\big/_{max}$ (lbs/ft)		56	22	11	
Calculated Unbalanced Force in Pipe Section with length l	l = 10 ft	560 lb	220	110	
	l = 20 ft	1,120	440	220	
	l = 30 ft	1,680	660	330	
	l = 40 ft	2,240	880	440	
	l = 50 ft	2,800	1,100	550	

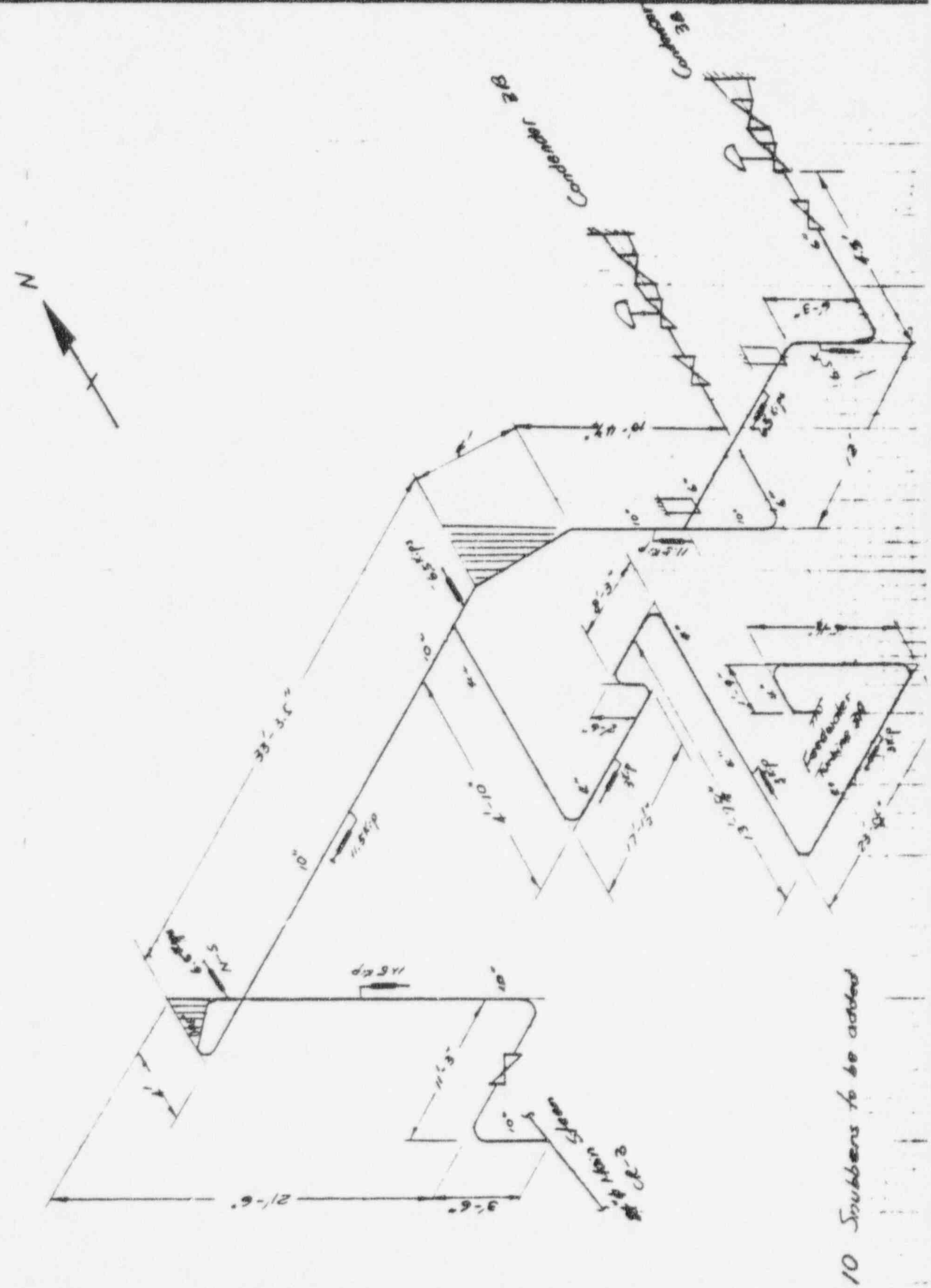
FILING CODE

CRYSTAL RIVER #3	MADE 11/30/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
	CHK'D.	
	SQ. CF.	
Main Steam By-Pass to Condenser #3A	CF. DFN.	4203-027
Main steam to Feedwater Pump Turbine #3B	ENG. M. Z. Lee	WORK ORDER / SIZE / DRAWING / REV.
STEAM HAMMER RESTRAINTS	REV. CK. APP. DATE	

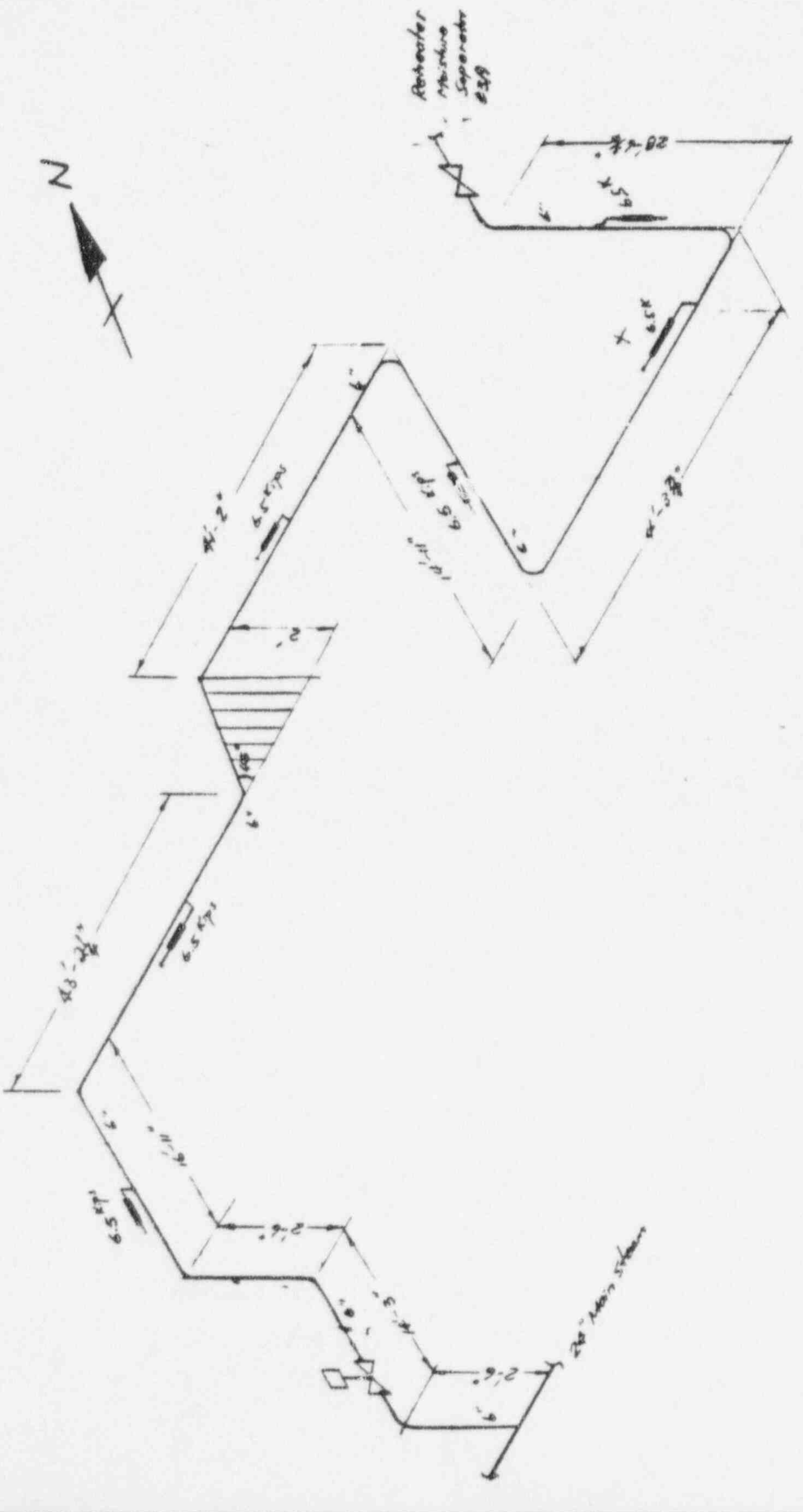


11 Snubbers to be added.

CRYSTAL RIVER #3	MADE 11/20/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
	CHK'D.	
	DG. CF.	
Main Steam By-Pass to Condenser 3B	CF. DFN.	
Main steam to Emergency Feedwater Pump	ENG. M.Z. Lee	4203-027 WORK ORDER · SIZE · DRAWING · KEY
Turbine 3A STEAM HAMMER RESTRAINTS	REV. CH. APP. DATE	

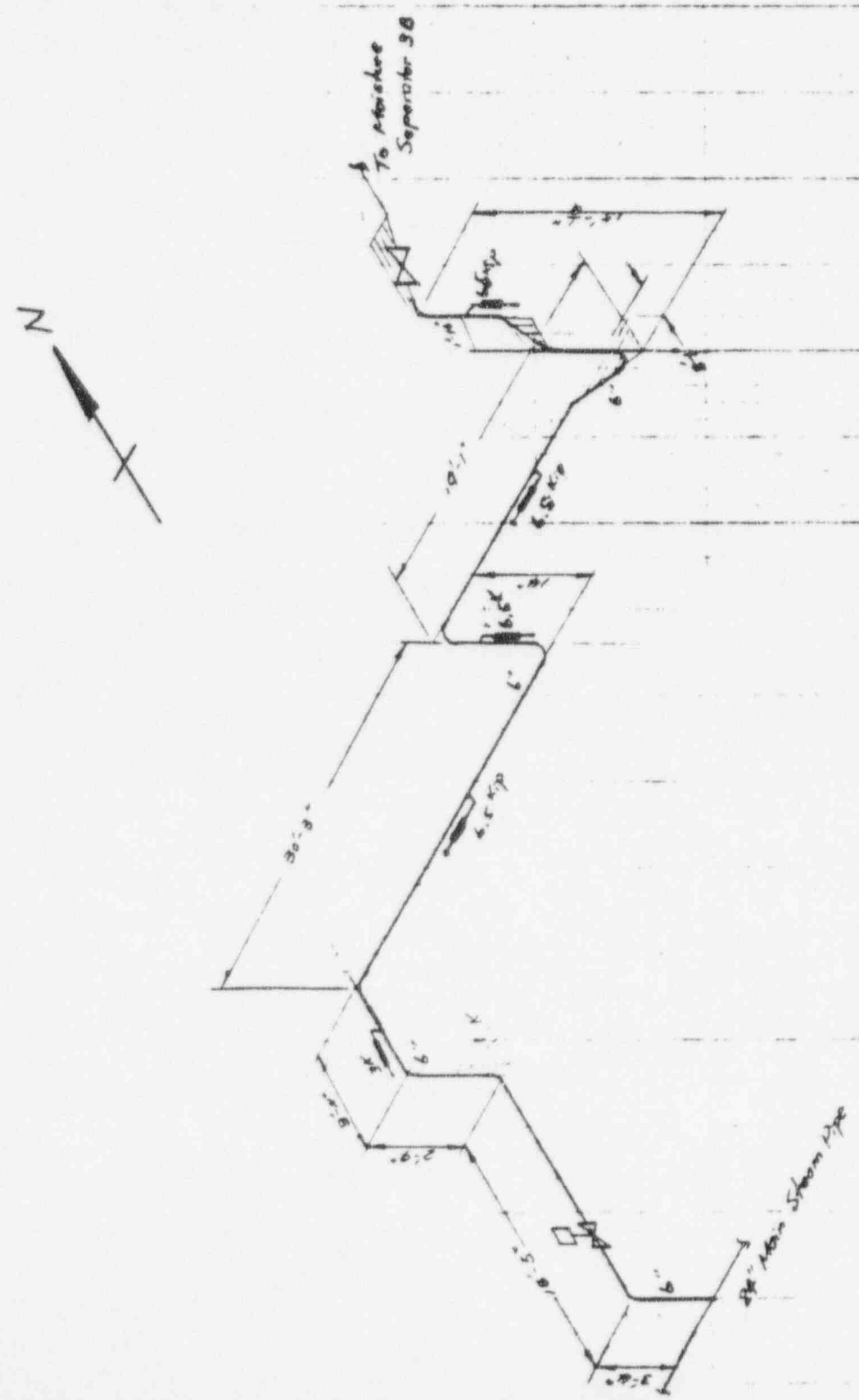


CRYSTAL RIVER #3	MADE 11/21/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
Main Steam Piping to #3A Moisture Separator Reheater Steam Hammer Restraints	CHK'D.	
	SQ. CF.	
	CF. DFN.	#203-027
	ENG. M. Z. Lee	WORK ORDER / SIZE / DRAWING / REV.
	REV. CH. APP. DATE	



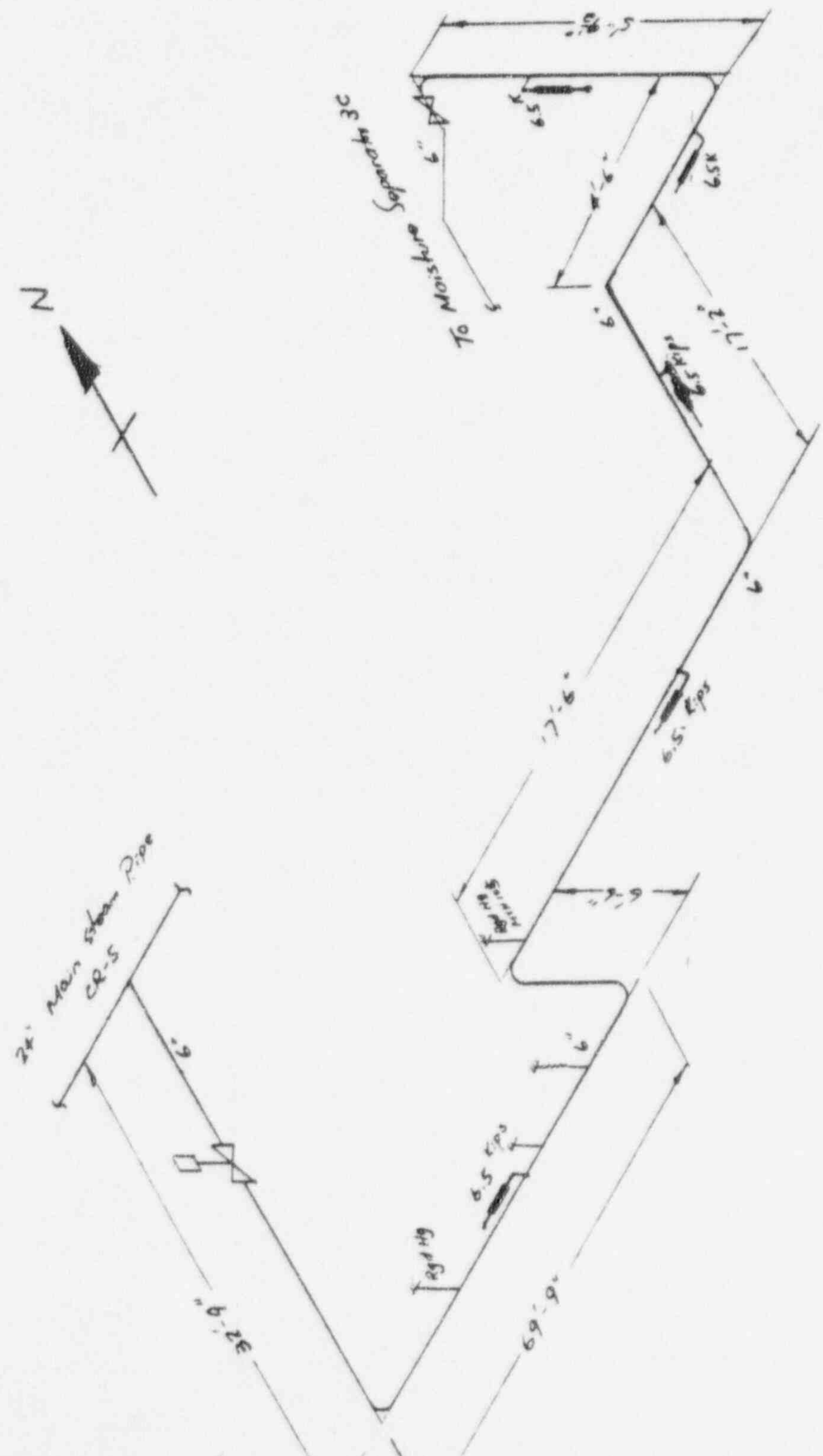
6 Snubbers to be added

CRYSTAL RIVER #3	MADE 11/20/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
	CHK'D.	
	SQ. CP.	
Main Steam Piping to Moisture Separator	CP. DFN.	4203-027
Reheater #3B Steam Hammer Restraints	ENG. M. Z. Lee	WORK ORDER / SIZE / DRAWING / REV.
	REV. CK. APP. DATE	



5 Snubbers to be added

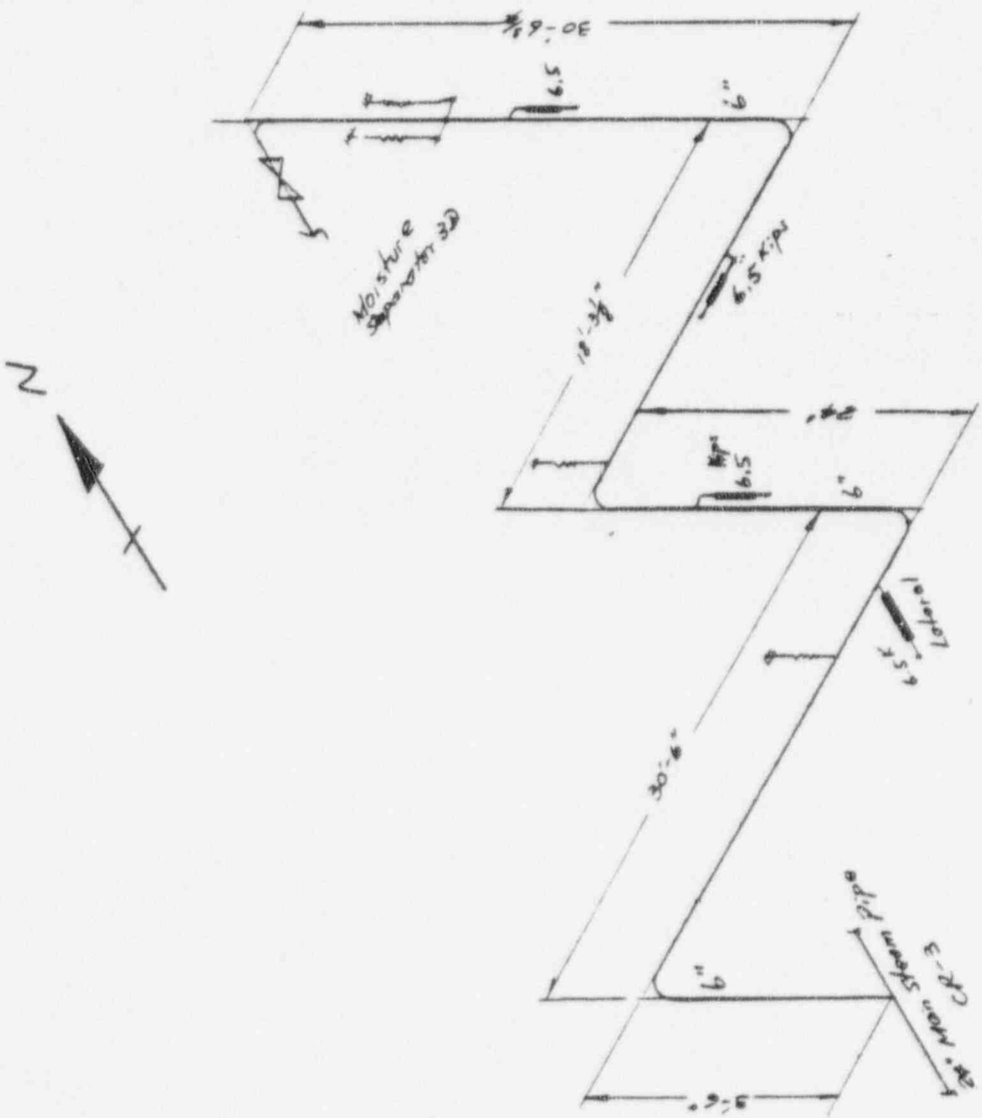
CRYSTAL RIVER #3	MADE 11/21/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
Main Steam Piping to Moisture Separator Reheater #3C	CHK'D.	
Steam Hammer Restraints	DG. CF.	
	CF. DFN.	4203-027 WORK ORDER / SIZE / DRAWING / REV.
	ENG. M. Z. Lee	
	REV. CK. APP. DATE	



Note: For illustration only. Dimensions given are approximate values.

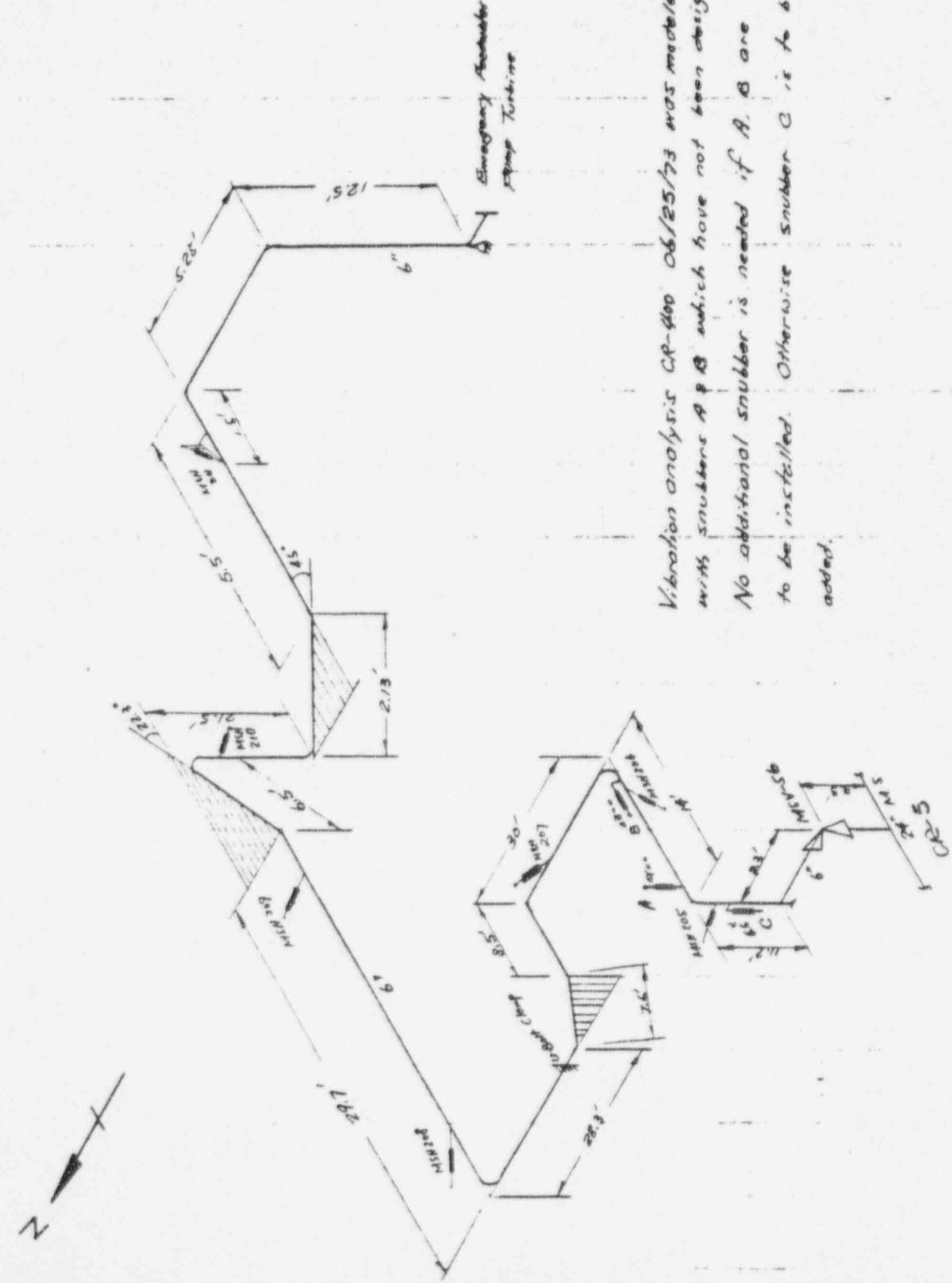
5 Snubbers to be added

CRYSTAL RIVER #3	MADE 11/20/73 CHK'D. SQ. CF.	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
Main Steam Piping to #3D Moisture	CF. DFN.	4203-027
Separator Reheater Steam Hammer	ENG. M Z Lee	WORK ORDER / SIZE / DRAWING / REV.
Restraints	REV. CK. APP. DATE	



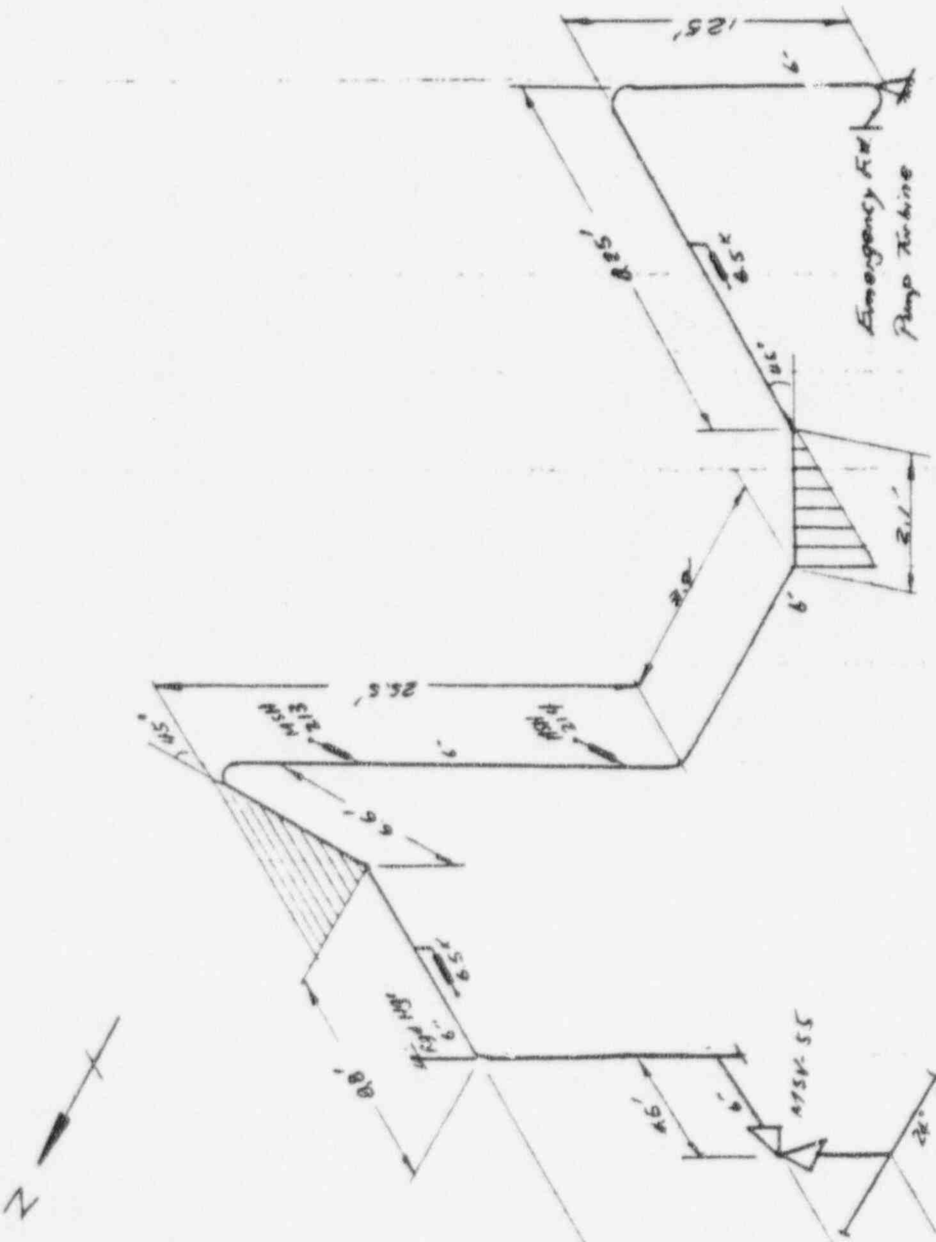
4 Snubbers to be added

CRYSTAL RIVER #3	MADE 11/21/73	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
	CHK'D.	
	BID. CF.	
Main Steam Piping to Emergency F.W.	CF. DFR.	4203-027
Pump Turbine Steam Hammer Restraints	ENG. M. Z. Lee	WORK ORDER / SIZE / DRAWING / REV.
	REV. CH. APP. DATE	



Vibration analysis CR-400 08/25/73 was modeled with snubbers A & B which have not been designed. No additional snubber is needed if A, B are to be installed. Otherwise snubber C is to be added.

CRYSTAL RIVER #3	MADE 11/21/73 CHK'D. EQ. CF.	GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PENNA.
Main Steam Piping to Emergency F.W. Pump Turbine Steam Hammer Restraint	CF. DFN. ENG. M. Z. Lee	4203-027 WORK ORDER / SIZE / DRAWING / REV
	REV. CH. APP. DATE	



2 Snubbers to be added

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE S4203MS02 A0
	PROJECT Crystal River #3	W.O. / PAGE 35 OF
SYSTEM Main Steam Piping		ORIGINATOR M. Z. Lee
CALCULATION FOR Steam Hammer		DATE 11/2/73
		REVIEWER
		DATE
		RESULTS

References

[1] Coccio, C. L. Steam Hammer in Turbine Piping Systems. Combustion, Feb. 1967

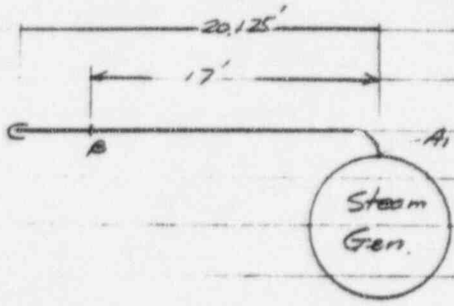
[2] Piping Stress Analysis File

CR-3 CR-13
CR-4 CR-14
CR-5 CR-15
CR 6 CR-16

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE
	PROJECT	W.O. / PAGE / OF
SYSTEM		ORIGINATOR M. Z. Lee / DATE 11/21/73
CALCULATION FOR		REVIEWER / DATE

RESULTS

Line CR-14 Section 13



Stress at A_1 from computer output

Dead Load	824 psi
X-Y Quake	1309
Y-Z Quake	461

Pressure

$\frac{PD}{4t} = \frac{1100 \times 24}{4 \times 0.968} =$ 6,820

Total 9,414

Provide a vertical snubber at B

$\delta = \frac{Pl^3}{3EI}$, $\sigma = \frac{M}{Z} = \frac{MD}{2I}$

$\therefore \sigma = \frac{3}{2}\frac{ED}{l^2}\delta = \frac{30 \times 10^6 \times 24}{2 \times (17 \times 12)^2}\delta = 26,000\ \delta$

Suppose snubber locks up at $\frac{1}{4}$" movement

$\sigma = 26,000 \times \frac{1}{4} = 6,500$

$9,414 + 6,500 = 15,914 < 18,000$

$\therefore$ Snubber can be placed at B

FILING CODE

FILE ______

GILBERT ASSOCIATES, INC.

TELEPHONE AND CONFERENCE MEMORANDUM

DATE 10/30/78 10:30 AM

BY: M. Z. Lee WORK ORDER NO. 4203-027

TELEPHONE CALL [X] CONFERENCE [ ]

WITH: Khemlani 595-3936 (Crystal River Project System Engineer)

COMPANY: Westinghouse, Lester Office

SUBJECT:

NOTES: Request information on Main Steam Turbine Emergency stop valve Closing Time for Crystal River Unit #3.

Ans.

Total closing Time = 250 milisec ✓

Includes signal etc.

Valve Travelling Time = 150 milisec ✓

Copies To:

GILBERT ASSOCIATES, INC. ENGINEERS AND CONSULTANTS READING, PA.	CLIENT	FILING CODE	
	PROJECT Crystal River #3	W.O. 4203-027	PAGE OF
SYSTEM Main Steam Piping Inside Containment Bldg.		ORIGINATOR M. Z Lee DATE 12/21/73	
CALCULATION FOR		REVIEWER DATE	

Steam Hammer Restraints (Revised)

RESULTS

Line CR-13

1. Add one axial snubber on Sec. 10 (Ref. Fig. 2 of original Report) Capacity 30 Kips
2. Modify MSH-151 to take 20 Kips upward force (Insert a saddle support between 24" pipe and 21WF62 above the pipe)

Line CR-14

1. Add a rigid vertical support near elbow of the vertical drop section upstream of MSH-152. Design Load 42 Kips downward; 35 Kips upward

Line CR-15

1. Add one vertical snubber near the the elbow between Sec. 12 & 13. Capacity 30 Kips.
2. Modify MSH-142 to take 44 Kips downward load; 20 Kips upward load

Desirable to move MSH-142 closer to elbow

Line CR-16

1. Add a 30 Kips axial snubber on Sec 12
2. Modify MSH-137 as recommended for MSH-142

GAI 350 REV. 10-72

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GILBERT ASSOCIATES, INC.
ENGINEERS AND CONSULTANTS
READING, PA.

CLIENT

PROJECT Crystal River #3

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SYSTEM Main steam Piping Inside Containment Bldg

ORIGINATOR M. Z. Lee
DATE 12/21/73

CALCULATION FOR

REVIEWER

DATE

RESULTS

	No. of Snubber to be added	No. of Rigid Support to be Modified
CR-13	1	1
CR-14		1
CR-15	1	1
CR-16	1	1
Total	3	4

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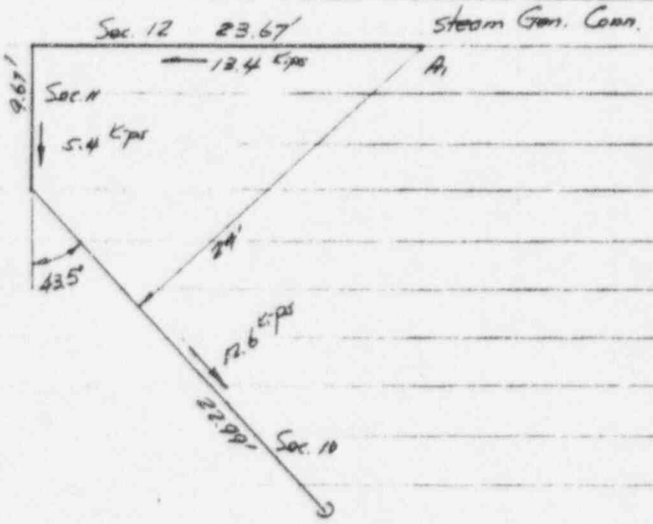
RESULTS

CR-13

Sections Near Steam Gen



$M_{A_1} = 5.4^{Kips} \times 23.67' + 12.6^{Kip} \times 24 = 430^{Kip\text{-}ft}$

Bending stress at A_1

$S_b = \frac{M_{A_1}}{Z} = \frac{430 \times 12}{388} = 13.3^{Ksi} = 13,300^{psi}$

Combined Stress at A_1 (p.10)

Vibration	1,309×2	2,618 (from Piping stress analysis)
Dead Load		824
Pressure		6,500
Steam Hammer		13,300
Total		22,242 > 18,000 = 1.2 S_h N.G.

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CALCULATION FOR		REVIEWER	
		DATE	

RESULTS

Suppose an axial snubber is installed on Sec. 10

Assume the snubber lock up at movement $\delta_{10} = \frac{1}{4}"$

Then $\delta_{11} = \frac{1}{4} \cdot \frac{1}{\cos 43.5°} = 0.344"$

Bending stress at A_1 corresponding to δ_{11} is

$\sigma = 13,600\ \delta_{11} = 13,600 \cdot 0.344 = 4,680$ psi
(p.11)

Combined Stress at A_1

Vibration	2,618
Dead Load	824
Pressure	6,500
Steam Hammer	4,680
Total	14,622 < 18,000 O.K

Since $\sigma = 4680$ (with snubber) $\ll S_b = 13,300$ (without Snubber)

and deflection $\propto$ stress

Without snubber sec. 10 may move axially

$\frac{1}{4} \times \frac{13,300}{4680} = 0.71"$

Therefore the snubber will be effective.

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RESULTS

Capacity of snubber on Sec. 10

$$12.6 + 5.4 \frac{1}{\cos 43.5^{\circ}} = 12.6 + 6.5 = 19.1^{\text{Kips}}$$

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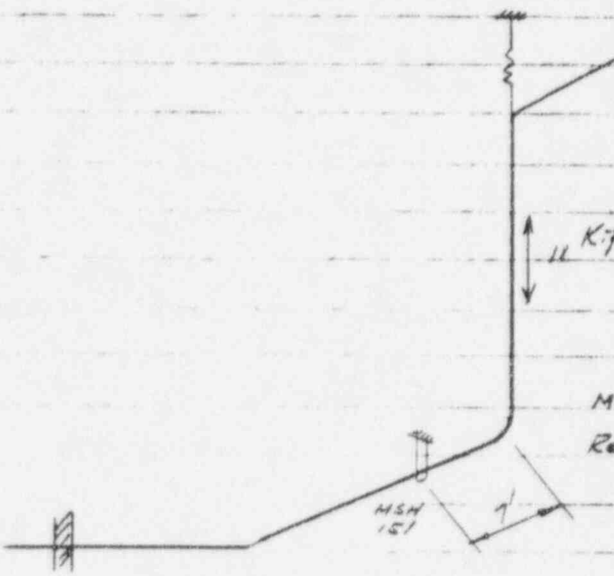
CR-13

Vertical Drop to Pennetration Anchor



MSH 151 operation load 31,300 lbs
Structure Design Load 32,000 lbs

RESULTS

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RESULTS

The effects of 11 ^{Kips} force on vertical drop section are obtained by Thermal Program.

1. MSH-151 will be subject to 16,000 ^{Kips} additional downward force

Combined loads of MSH-151

Seismic	2.045	Kips x 2 DLF
Dead wt	4.9	Kips
Steam Hammer	16.006	
Total	24.0	Kips

< 31.3 ^{Kips} hanger design load

∆ MSH-151 can take downward steam hammer load.

∆ MSH-151 must be modified to take 20 ^{Kip} upward load.

From stress summary of CR-14 (without steam hammer load)

$S_{max} = 10,817$ psi

Max stress due to steam hammer $= 1,801$ psi

$\therefore S'_{max} = 10,817 + 1,801 = 12,618$ psi

$< 18,000 = 1.2\ S_m$

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CR-13 Conclusion

1. Add one axial snubber on Sec 10
   Capacity 19.1 Kips min. use 30 Kip

2. Modify MSH-151 to take 20 Kips
   upward force
   (Insert saddle support between 24" pipe
   and 21WF62 above the pipe)

RESULTS

FILING CODE

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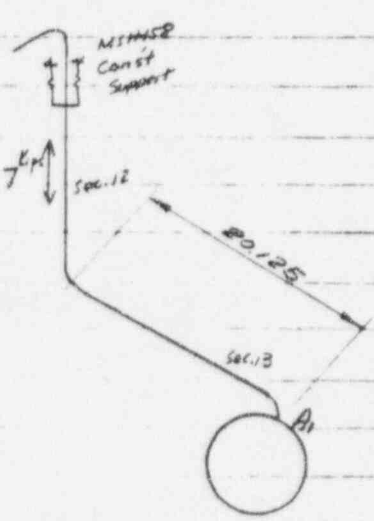
RESULTS

GR-14

Sec. 12 & Sec. 13 Near Steam Gen.



Bending stress at A_1 due to 7 kips steam hammer load acting on sec. 12

$$S_b = \frac{7000 \times 20.125 \times 12}{388} = 4{,}360 \text{ psi}$$

$$\delta = \frac{Pl^3}{3EI} = \frac{7000 \cdot (20.125 \times 12)^3}{90 \times 10^6 \times 4653} = 0.23''$$

Combined Stress at A_1

Dead Weight		925
Seismic	1305 x 2	2,610
Pressure		6,500
Steam Hammer		4,360
Total		14,395 $< 18{,}000 = 1.2 S_h$

No additional restraint is needed.

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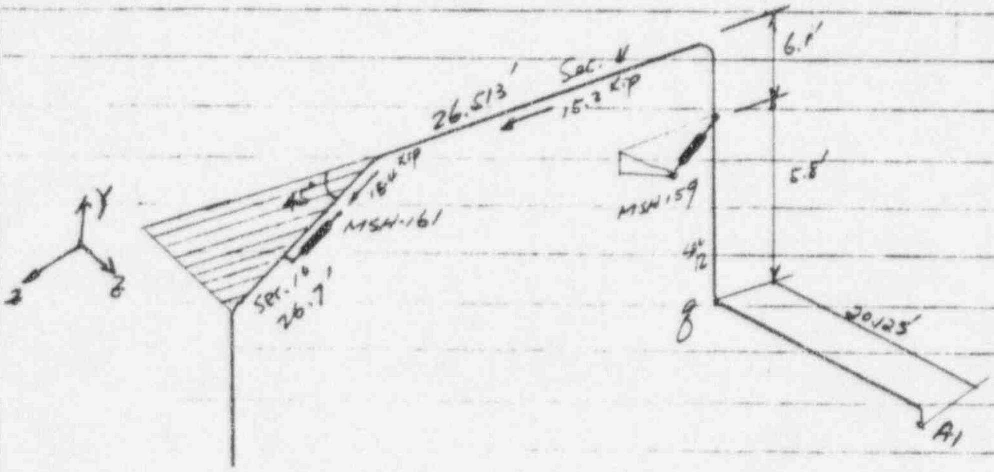
CR-14

Sec. 10 & Sec. 11



Restrain Capacity of MSH-161 = 49.5 Kips

Axial Thrust along Sec. 10

$= 15.2 \times \frac{1}{\cos 45°} + 15.4 = 21.5 + 15.4 = 37^{\text{Kips}}$
< 49.5

Assume movement of Sec. 10 is 1/4" axial, Then

Axial movement of Sec. 11 $= \frac{1}{4} \frac{1}{\cos 45°} = 0.354$

Movement at g with MSH-159 acting as support:

Assume MSH-159 lock up at movement $\frac{3}{16}$"

Then movement of g is

$(0.354 - \frac{3}{16}) \times \frac{5.8'}{6.1} = 0.168$"

RESULTS

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RESULTS

Stress imposed on A_1 due to movement of δ is

$$\sigma = \frac{3}{2}\frac{Ed}{\ell^2}\delta = \frac{90\times10^6\times24}{2\times(20.125\times12)^2}\delta = 18{,}300\,\delta$$

$$= 18{,}300\times0.165 = 3{,}080 \text{ psi}$$

Combined stress at A_1 (See Sec. 12)

$$14{,}395 + 3080 = 17{,}475^{\text{psi}} < 18{,}000 \text{ psi}$$

No additional support is required.

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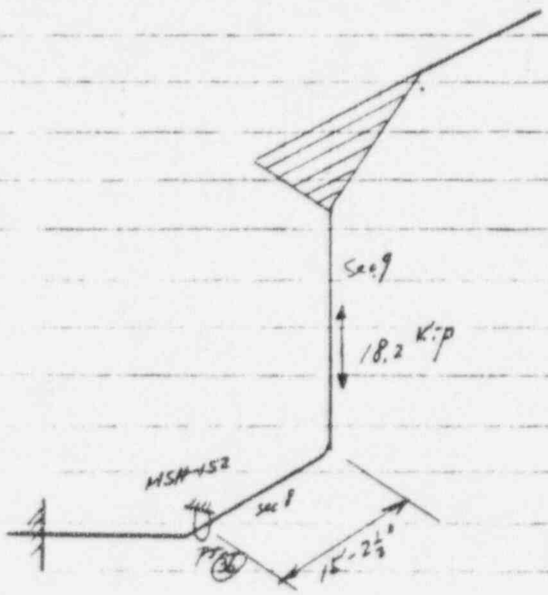
CR-14



RESULTS

Case 1

Put 18.2 Kip downward force on Sec. 9 (Steam Hammer stress Prog. Case 1)

stress at pt (36) = 8,074 psi

Combined stress at 26

Seismic	1,614 × 2 = 3,228	} 10,052	
D.W	324		
Pressure	6,500		
steam Hammer	8,074		
Total	18,126 > 18,000 = 1.2 S_h		N.G

Loads on MSH-152

DW.	6.5 Kips	
Seismic	10.05 × 2 = 20.1	
S. H	58,278	
	84.9 Kip	
Str. Design load	15.450 lbs	N.G

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RESULTS

Movement of Sec. 9 ≐ 0.43"

Need a snubber on Sec. 9

Case 2

Suppose Sec 9 moves 1/4" axially (Steam Hammer Load Case #2)

max S.H. stress = 4727 psi at pt 36

Combined S_{max} = 10,052 + 4727 = 14,780 psi < 18,000 = 1.2 S_h

Loads on MSH-152

DW	6.5	
Seismic + S.H	34.9	(with snubber on Sec. 9)
Total	41.4 Kips down	
	35 Kps up	

Case 4 A Better Design

1. Add another support between MSH142 & elbow. Without snubber on vertical sec max. stress is
   2,258 psi at pt 32 (New position of MSH-152)

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RESULTS

Load on Support at New Location

Steam Hammer Load = 23.3 K.P
D.L. 6.5 estimated
Seismic 15 from MSH-142
Thermo (negative) —
Total 42 K.P downward

35 K.P upward

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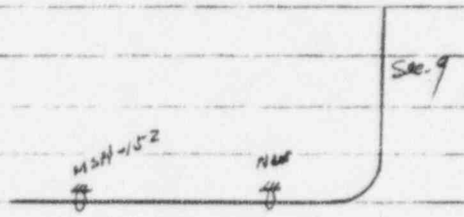
RESULTS

CR-14 Conclusion

1. Add a rigid support near elbow



Design Load 42 Kips tension
35 Kips compr.

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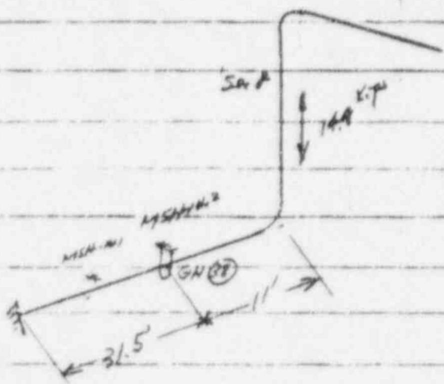
RESULTS

CR-15

Sec. 7 & Sec. 8 (vertical drop)



Applied 14.4 Kips on Sec. 8

max stress = 4,036 at pt 38

Fy = 20.2 Kips at MSH142

ΔY = +0.05" at MSH141

Pipe stress at pt (38)

Seismic	1332 × 2	= 2,664
D.W.		884
Pressure		6,500
Steam Hammer		4,036
Total		13,684 < 18,000 = 1.2 Sh

Pipe is O.K

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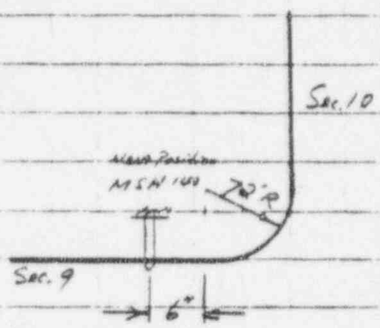
RESULTS

Support MSH-142 Loading

Seismic 5.65 × 2 = 11.3 Kips
Dead Load 7.414
Thermal (dd) 4.666
Steam Hammer 20.2
Total 43.58 downward

upward load
20.2 + 11.3 − 7.4 − 4.6 ≐ 20 Kip upward

Case 2.
Suppose MSH-142 is located at 6" from the elbow



Load on MSH-142
Seismic 11.3
Dead Load 7.414
Thermal 4.666
Steam Hammer 17.38
Total 40.86

Piping Stress due to steam hammer decreased to 2,955 from 4,036 psi

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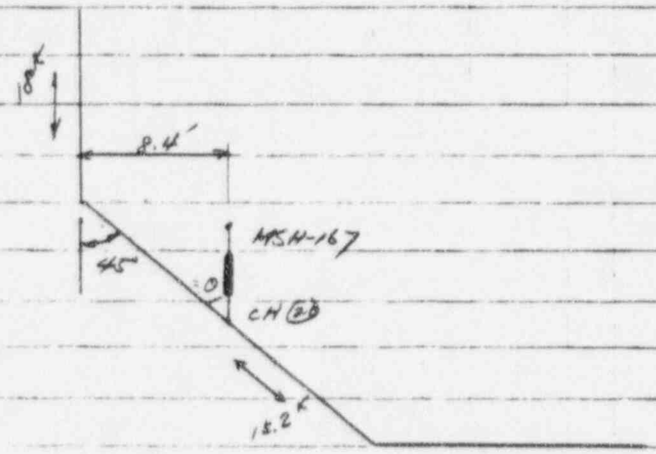
		RESULTS	

CR-15

Secs 9 & 10



Load on MSH-167

$\doteq \frac{15.2}{\cos 45^\circ} + 18 = 21.5 + 18 = 40$ Kips

Existing Seismic Snubber 49.5 Kips

Bending stress in pipe at CH (23)

$S_b = \frac{18,000 \times (8.4 \times 12)}{388} = 4,680$ psi

Seismic stress 875×2 =	1,750
Pressure	6,520
Dead Load	(–)
Total	12,950 < 18,000 = 1.2 S_h

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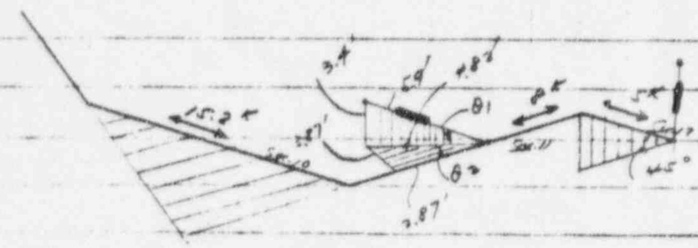
CR-15

Sec. 11



Axial Thrust on Sec. 11

$F = 8 + 5 \times 0.707 + 15.2 \times 0.707 = 22.3^{Kips}$

$\cos\theta_1 = 0.817 \qquad \cos\theta_2 = 0.595$

Load on Snubber

$\doteq \frac{F}{\cos\theta_1 \cos\theta_2} = \frac{22.3}{0.817 \times 0.595} = 46^{Kips}$

Existing Snubber MSH-166 is sized to 49.5 Kips

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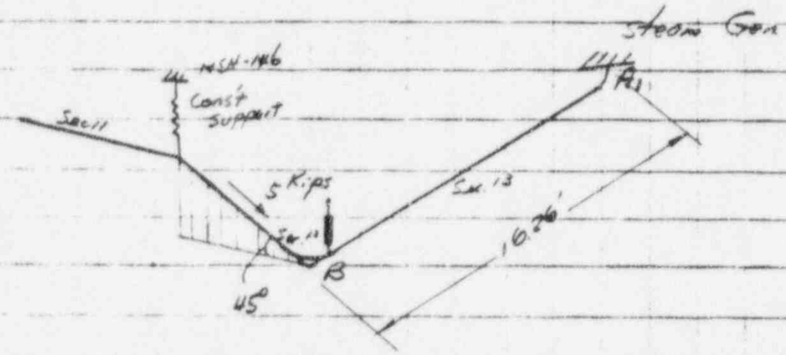

Vertical Component of 5 kip thrust on sec 12

$F_v = 5 \times 0.707 = 3.5$ Kips.

Bending Stress at A_1 due to F_v

$$S_b = \frac{F_v \times (16.25 \times 12)}{Z} = \frac{3{,}500 \times 16.25 \times 12}{388}$$

$= 1{,}760$

Combined Stress at A_1

Seismic	5104 × 2	= 10,208
Dead Wt		1,110
Pressure		6,500
Steam Hammer		1,760
Total		19,578 > 18,000 = 1.2 S_h

N.G.

Need additional restraint

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If a vertical snubber is placed at B and locks up at 1/4", then

$$\sigma = \frac{3}{2}\frac{Ed}{l^2}\delta = \frac{3}{2}\frac{30\times10^6\times24}{(16.26\times12)^2}\delta = 28{,}400\,\delta$$

$$= 28{,}400 \times \frac{1}{4} = 7{,}100 \text{ psi}$$

Combined stress at A_1 is

Dead wt	1,110
Pressure	6,500
Steam Hammer & Seismic (1/4" snubber movement)	7,100
Total	14,710 < 18,000 = 1.2 S_h

Load Capacity of snubber

Assume: Seismic stress at A_1 is caused by a concentrated load at B (F_S)

$$F_S = \frac{S_{b}\cdot Z}{l} = \frac{5104\times388}{16.25\times12} = 10{,}200 \text{ lbs}$$

$$F_S + F_V = 10.2 + 3.5 \doteq 14 \text{ Kips (min)}$$

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Conclusion

1. Add one vertical snubber near the elbow between Sec 12 & 13. Capacity 30 Kips

2. Modify MSH-H:
   44 Kip downward load
   20 Kip upward "

Both pipe stress & support load will be decreased by moving MSH+42 closer to elbow.

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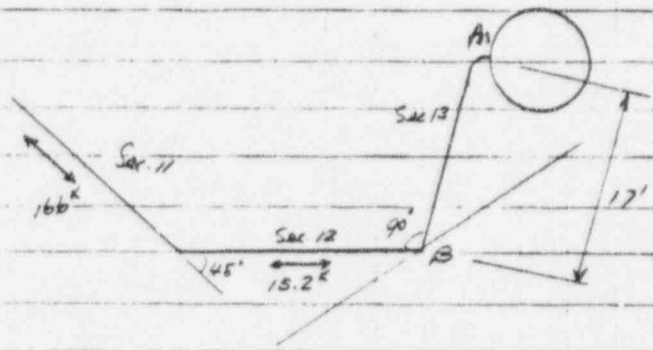
Sec 12 & Sec 13 Near Steam Gen



Stresses at A_1 (Piping stress program)

Seismic	1.132 × 2	= 2264
Pressure		6500
D. L.		405
Total		9,170

Axial force on Sec. 12

$P = 15.2 + 16.6 \cos 45° = 26.9$

Deflection at B

$$\delta = \frac{P l^3}{3EI} = \frac{26,900 \times (17 \times 12)^3}{3 \times 30 \times 10^6 \times 4653} = 0.545''$$

$$\sigma = \frac{Pl}{Z} = \frac{26,900 \times (17 \times 12)}{388} = 14,100 \text{ psi}$$

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Combined Stress at A_1

$$S_{max} = 14,100 + 9,170 = 23,270$$
$$> 18,000 = 1.2 S_h$$

Need restraint on Sec. 12

Snubber Capacity = 20 Kips

Suppose the snubber stops movement of B within 1/4"

$$\sigma = \frac{3}{2}\frac{Ed}{l^2}\delta = \frac{3}{2}\frac{30\times10^6\times 24}{(17\times12)^2}\delta = 23,100\,\delta$$

$$= 23,100 \times \frac{1}{4} = 5,780 \text{ psi at } A_1$$

Combined stress at A_1 is

$$S_{max} = 5,780 + 9,170 = 14,950$$
$$< 18,000 = 1.2 S_h$$

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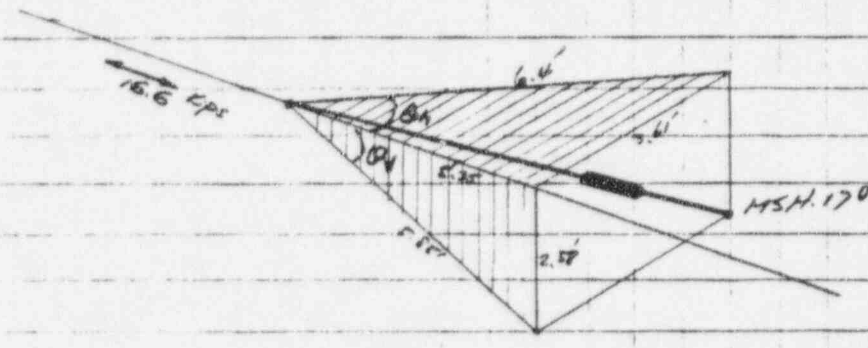
Sec. 11



$\cos \theta_h = \frac{5.25}{6.4} = 0.821$ $\cos \theta_v = \frac{5.25}{5.85} = 0.9$

$F_x = 16.6$ Kips

Load on MSH-170 due to F_x

$= F_x \frac{1}{\cos\theta_h \cos\theta_v} = 16.6 \frac{1}{0.821 \times 0.9} = 22.4^{Kips}$

Existing Capacity $49.5^{Kips} > 22.4^{Kips}$

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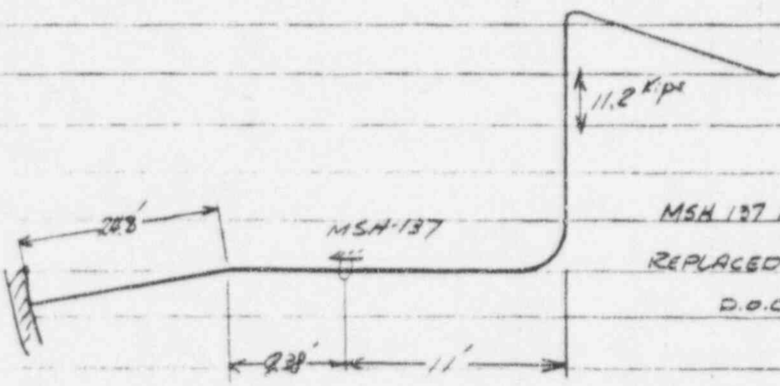
Sec. 10 (vertical drop)



MSH 137 IS VOID & REPLACED BY MSH 247 D.O.C. 1-18-77

Since the layout is close to that of CR-15 and with smaller axial thrust on the vertical section, the modification of MSH-142 on CR-15 can be applied to MSH137.

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Conclusion

1. Add one snubber on Sec. 12 (30 Kips)

2. Modify MSH-137 as recommended for MSH-142 of CR-15

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