

UNITED STATES OF AMERICA  
NUCLEAR REGULATORY COMMISSION

BEFORE THE ATOMIC SAFETY AND LICENSING BOARD

In the Matter of

TEXAS UTILITIES GENERATING  
COMPANY, et al.

(Comanche Peak Steam Electric Station  
Station, Units 1 and 2)

Docket Nos. 50-445-1  
and 50-446-1

CASE'S ANSWER TO APPLICANTS' STATEMENT OF MATERIAL FACTS  
AS TO WHICH THERE IS NO GENUINE ISSUE REGARDING THE EFFECTS OF  
GAPS ON STRUCTURAL BEHAVIOR UNDER SEISMIC LOADING CONDITIONS

in the form of

AFFIDAVIT OF CASE WITNESS MARK WALSH

1. Applicants state:

"All bolts in multiple bolt, bearing-type connections will react imposed shear loads within at most the distance of the bolt hole tolerances. (Iotti, Finneran Affidavit at 8 /1/.)"

I disagree with this statement (and with some of the statements in the Affidavit). At the point all bolts begin to react the shear loads (that is, when the last bolt will have received a 1 lb. shear load), the first bolt that has reacted the shear load may have the shear load of 1,000 lbs., and this may have exceeded the allowable shear capacity of the bolt. This is assuming that the first bolt that reacted the shear load has not failed when the last bolt begins to resist the shear load.

/1/ I believe that the actual citation should be at 4-5.

One of Applicants' primary arguments which is contained in the back-up Iotti/Finneran Affidavit is regarding the definition of "oversized" bolt holes. This is addressed in detail in answer 2. following.

One example of statements with which I disagree which is made in the Affidavit of Dr. Iotti and Mr. Finneran is found on page 5 of the Affidavit (last paragraph, continuing on page 6), wherein they cite "Structural Design Guide to AISC Specifications for Buildings," by Paul F. Rice and Edward S. Hoffman (Attachment B to Affidavit).

Although the one page (268) from that document which Applicants have attached appears to be accurate /2/, their discussion and the portion cited (which is out of context) are very misleading. (See Attachment A, pages 264 through 271 of the Rice/Hoffman text.) In the portion attached by Applicants, Messrs. Rice and Hoffman are only talking about connections that receive static loads (i.e., loads that do not change direction) because the yielding stress criteria is not applicable in friction-type connections, as will be discussed later. The connections referenced by Messrs. Rice and Hoffman specifically exclude the supports that have dynamic loads (as will be shown below) such as most of those supports at CPSES. In addition, the inelastic deformation in bearing-type connections is recognized by the AISC Code at 1.5.2.2, where the allowable bearing stress is  $1.35 F_y$ .

Therefore, the Applicants' statements are lacking reference to the

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/2/ It should be noted that I have not reviewed the entire text of the other reference cited by Applicants, "Plastic Design of Steel Frames," and cannot state whether or not it is taken out of context.

specific amount of inelastic deformation allowed by the AISC Code for a non-dynamically loaded structure.

On pages 265-266 of the Rice/Hoffman text, following a discussion of AISC and ASTM specifications, it is stated (the numbers Messrs. Rice and Hoffman have placed in parentheses refer to sections from AISC or ASTM):

"The use of ordinary (A307) bolts is limited by a number of Specification requirements. The allowable stresses are low: tension  $F_t = 20$  ksi on the threaded area; and shear  $F_v = 10$  ksi (1.5.2.1). The slip before full bearing is achieved on a group of ordinary bolts effectively rules out the sharing of stress in a mixed connection. Holes are to be taken as  $1/16$  in. larger than the nominal diameter (1.23.4), and the ordinary bolt does not expand to fill out the hole like a driven rivet nor can it be used for dependable friction. Stress sharing may not be assumed between ordinary bolts and rivets or welds (1.15.10; 1.15.11). In addition, low-strength bolts are not permitted in important field connections including . . . connections subject to vibration, impact, or stress reversal (1.15.12) . . ." (Emphases added.)

As discussed above, according to Messrs. Rice and Hoffmar (Applicants' own chosen authority), A307 bolts are not permitted in connections subject to vibration, such as those at Comanche Peak.

Applicants have admitted that the connections at Comanche Peak are subject to vibration. Applicants' witness Finneran stated, in regard to the support which Jack Doyle and I noticed that had failed during hydrotesting (Tr. 4793/15-4794/4):

"Q: (By Mr. Reynolds) Would you render an opinion on why the paint that Mr. Doyle talked about may have flaked during the flow of fluid through the pipe?

"BY WITNESS FINNERAN:

"A. I would say that possibly vibration may have been a cause for paint coming off of the deformed area during flow of fluid during the pipe; one possible cause.

"Q. Yes. So what you are saying is that it could have been that when the deformation was caused during construction, the paint cracked but remained on, and then when vibration occurred due to hydrostatic flow, the paint chipped off?

"BY WITNESS FINNERAN:

"A. It's a possibility. I couldn't say if that's exactly what happened." (Emphases added.)

And at Tr. 5002/24-5003/9, Mr. Finneran further testified:

"Q: (By Mr. Walsh) Is vibration a common occurrence at Comanche Peak?

"BY WITNESS FINNERAN:

"A. I think all piping systems that have fluids in them or flowing to them are possibly subject to some vibration.

"Q: How about other pipes, main steam? Will they have vibrating effects?

"BY WITNESS FINNERAN:

"A. Quite possibly there will be vibration in the main steam piping." (Emphases added.)

The ASME Code requires the Applicants to minimize vibration where it states:

"NF-3112.2 Design Mechanical Loads. . . . The requirements of (a), (b), and (c) below shall apply.

. . . (c) Component supports shall be designed to minimize vibration."

In addition, according to Messrs. Rice and Hoffman (Applicants' own chosen authority), Applicants are also barred from using A307 bolts because of stress reversal.

As indicated above, Messrs. Rice and Hoffman cited the AISC code (to which the Applicants are committed through Specification MS-46A), Section 1.15.12, which states, in part:

**"Field Connections**

"Rivets, high strength bolts or welds shall be used for the following connections:

. . . Connections for supports of running machinery, or of other live loads which produce impact or reversal of stress.

"In all other cases field connections may be made with A307 bolts." (Emphases added.)

CASE requested, through discovery on the issue of Applicants' Motion for Summary Disposition regarding generic stiffnesses, the drawings which the Applicants used in their Motion. Of the 60 supports which the Applicants provided (I count 59, but this is immaterial to this point), 52 had reversible loads which is a reversal of stress on the supporting connection. (See Attachment B, the referenced 59 drawings.) On the drawings, the reversal of loads is shown in the block listing the loads and the direction of the load is indicated as + or - . Of the 7 supports which do not contain reversible loads (CT-1-013-006-S22S, CT-1-013-004-S32S, MS-1-001-002-C72S, MS-1-01-001-C72S, CT-1-013-002-C42S, CC-2-011-719-A53R, CT-1-013-011-S22R), 5 are spring cans and 2 are rigid-type supports. Based on this random sample, 88% of these supports require high strength bolts due to the requirement of a reversal of stress (load) /3/, according to the AISC Code (to which the Applicants are committed in design specification MS-46A).

It is also obvious from the preceding discussions that Applicants are in violation of ANSI N45.2.11, 3. DESIGN INPUT REQUIREMENTS, 3.2 Requirements, which states, in part:

"The design input requirements should include the following where applicable:

"(9) Mechanical requirements such as vibration, stress, shock and reaction forces." (Emphases added.)

/3/ Stress is equal to the load divided by the cross-sectional area of the item under consideration.

2. Applicants state:

"Applicants' specifications for bolt hole tolerances are 1/16" for up to 1" diameter bolts and 1/8" for 1" and greater diameter bolts. (Iotti, Finneran Affidavit at 7.)"

I agree that this appears to be Applicants' current practice (although Applicants have not provided copies of the specifications themselves with their Motion for Summary Disposition). However, I do not agree with the implication, which is obviously that Applicants' specifications are acceptable. I maintain that Applicants' practice (or specifications) is contrary to applicable codes and NRC regulations.

One of Applicants' primary arguments which is contained in the back-up Iotti/Finneran Affidavit is regarding the definition of "oversized" bolt holes. This is a crucial argument for Applicants, because according to their own statement (bottom of page 6, Iotti/Finneran Affidavit):

"The 8th Edition of the AISC Manual of Steel Construction is quite instructive on this point. At page 5-58 of the Manual, Paragraph 1.23.4.3 (Attachment C) states 'Oversized holes may be used in any or all plies of friction-type connections, but they shall not be used in bearing-type connections.'" (Emphasis added.)

Applicants claim (Affidavit, page 7) that they use more stringent tolerances than defined by the AISC Code (to which Applicants are committed, according to their Design Specification MS-46A). A claim the Applicants make in the Iotti/Finneran Affidavit (page 7) is:

"AISC defines 'oversized' as  $d + 3/16$ " for bolts up to and including  $7/8$ " diameter,  $d + 1/4$ " for 1" bolts, and  $d + 5/16$ " for bolts greater than or equal to  $1\ 1-1/8$ " (sic) diameter."

I do not agree with Applicants' representation as to AISC's definition of "oversized." A point which the Applicants fail to make is as shown in Attachment C to their Affidavit, AISC Table 1.23.4, "Maximum Sizes of Fastener Holes, Inches" (emphasis added) -- that is, that these are the maximum size of holes. For a 1" diameter bolt, the maximum size hole for a standard hole is 1-1/16". If the hole is greater than 1-1/16" up to and including 1-1/4" for a 1" diameter bolt, the hole is considered oversized.

It is apparent that the Applicants do utilize an oversized hole for the 1" and greater bolts. As stated previously, paragraph 1.23.4.3 of Attachment C of the Applicants' affidavit (from 8th Edition, AISC Manual of Steel Construction, page 5-58), states:

"Oversized holes may be used in any or all plies of friction type connections, but they shall not be used in bearing type connections." (Emphasis added.)

It can be seen from what is shown above that bearing type connections can only be used with standard size holes. If the hole is greater than a standard size hole, bearing connections are not allowed. Therefore, the Applicants are not in compliance with the AISC Code to which they are committed (according to their design specification MS46-A).

On page 7 of Applicants' affidavit, they state:

"Thus, Applicants' specifications for bolt hole tolerances can definitely not be called 'oversized,' as that term is generally used in the construction industry."

Although the Applicants have not sized their bolt holes to the maximum allowed for an oversized condition, the bolt hole is still an

oversized hole (as discussed above). And, as the term is generally used in the construction industry, holes are considered to be oversized if they are over a standard sized hole, up to and including the maximum oversized hole allowed. Contrary to what Applicants state (Affidavit, page 7), they are not in compliance with standard industry practice.

There are several aspects of this matter of which the Board should be aware. One of the most important is whether or not Applicants even attempt to determine the size of bolt holes and, if so, how? During the 6/6/84 telephone conference call between Applicants/NRC Staff/and me, I requested documentation (original and all revisions of procedures or whatever other documentation exists) showing that QC inspectors inspect the whole tube steel base plates prior to inserting the bolt (which is the only way QC could be certain when inspecting that there were no oversize holes). (See 6/6/84 conference call Tr. 74-76.)

In Applicants' 7/15/84 letter to CASE President Juanita Ellis (received by CASE 7/16/84), Applicants' counsel stated (page 2, second full paragraph):

"Second were materials concerning Applicants' practice regarding the inspection of bolt holes in base plates, which relates to the motion concerning the effect of gaps. This information is attached. Copies of an example of the Material Identification Log, and the associated hanger drawing, for support H-BR-2-5B-001-009-3 are provided. This log is filled out by the QC inspector prior to release of materials, including base plates, from the fabrication shop. Although not separately called out on the log, one of the attributes of base plates the QC inspector examines is bolt hole size." (First emphasis in the original; second emphasis added.)

I agree with the statement of Applicants' counsel that the



inspection of base plates for bolt hole size is not separately called out on the Material Identification Log, and in reviewing these documents (see Attachment C), I see no reference to the QC inspectors' verifying the hole size.

There is additional information which indicates that QC inspectors do not inspect for oversize bolt holes. In the sworn affidavit of Howard J. "Robbie" Robinson (sent to the Board and parties with CASE's 11/28/83 Answer to Board's 10/25/83 Memorandum (Procedure Concerning Quality Assurance)), Mr. Robinson stated (page 7):

"My duties as general foreman over the fab shop consisted of fabricating items such as pipe hangers, cable tray hangers, and Q miscellaneous steel assemblies for subsequent installation in the field. . . I did, over a period of about three years, engage in an ongoing argument with one of the foremen within the steel hanger department whose duty was to install hangers in the field where he challenged the practice in the fab shop of drilling 1" holes in base plates to the code allowable of 1-1/16" diameter for a 1" bolt. His stand had been that we were allowed to overdrill the hole to a 1-1/8" diameter. . . he . . . made the statement to me that he had been drilling them oversize all along and intended to continue to. If he in fact did drill these holes oversize, and I believe that he did, one must assume that any subsequent QC inspection failed to identify this." (Emphases added.)

(See also discussion under answer 2. preceding.)

Further confirmation of what I believe to be the truth of this matter is to be found in a document concerning an investigation conducted by Applicants into allegations which had been made. (See Attachment D, 3/9/84 TUGCO Office Memorandum to Distribution from Jerry C. Walker, Subject: Resolution of QAI-0001, and the attached 2/22/84 TUGCO Office Memorandum from Boyce Grier to Antonio Vega, Subject: Investigation of Allegations QAI #0001.) Item 3, page 2, of the

2/22/84 Memorandum discusses allegations of an alleged that an oversize hole (1-1/2") had been drilled for a 1-1/4" Hilti bolt in a hanger base plate (i.e., a hole 1/4" larger in diameter than the bolt). Mr. Grier states that he subsequently identified the support in question as CC-2-070-002-A33R (copy of the as-built drawing for the support is Attachment F to his report). He further states:

"There is nothing in the documentation package for this pipe support to indicate a requirement for or the approval of an oversize hole. I reviewed the reports of the QC inspections for the Hilti installation for this support. These are contained in the following:

- "IRMH-19682, dated 7/1/81
- "IRMH-53200, dated 2/15/83
- "IRMH-53257, dated 2/22/83

"These reports do not indicate any nonconforming or unsatisfactory conditions. (Blacked-out) stated during his interview that he had no knowledge of oversize holes ever being drilled for Hilti bolts.

"I made inquiry of pipe support engineering (Jay Ryan) as to whether an oversize hole for a Hilti bolt in the support in question would be of concern. I was told that it would not be a problem.

"The allegation that an oversize hole had been drilled for a Hilti bolt could neither be confirmed or dismissed. It appears that physical inspection of the holes for the support in question would be the only way to resolve this matter. In view of the response from Engineering regarding the significance of this matter, it does not appear necessary to pursue the matter further." (Emphases added.)

Thus, the investigator reviewed the documentation packages and saw no indication of an oversize hole or of a requirement for or the approval of an oversize hole. He reviewed the reports of the QC inspections, which did not include the Material Identification Log which Applicants' counsel referenced as being the documentation I

requested regarding Applicants' practice for the inspection of bolt holes in base plates. When he checked with pipe support engineering (Jay Ryan), he was told that the 1/4" oversize bolt hole would be no problem, although no basis is given in the report for Jay Ryan's disposition of the problem. Based on Jay Ryan's position, the investigator ceased his investigation -- even though he admitted that he could neither confirm or dismiss the allegation.

Therefore, as demonstrated above, Applicants' statement that they have no oversize holes (including those greater than the 1/8" criteria Applicants claim to use) is without substance.

3. Applicants state:

"Test data indicate that bolts of the kind Applicants use have margins of safety for shear displacements equal to the maximum bolt hole tolerances ranging from 5.6 (1 1/4" super kwick Hilti) to 3.2 (1 1/4" Richmond Inserts). (Iotti, Finneran Affidavit at 8-9.)"

I agree with this statement, but I do not see where it is material to the Board. This statement discusses displacements only. For the Applicants to be in compliance with IE Bulletin 79-02, the factor of safety must be based on ultimate load, not displacement.

Using the test data shown in Attachment A to Applicants' testimony in September 1982 (Applicants' Exhibit 142D, admitted at Tr. 4794, Attachment B), for a 3/4" diameter Hilti bolt loaded in shear, the load at 1/8" displacement is 10,000 lbs. The allowable load as listed in the PSE Manual (see Attachment E, PSE Manual, Section V, Hilti Concrete Anchor Bolts, Rev. 0, 1/8/82, page 8 of 10, Figure 6) is 3,693 lbs. for

a 3/4" diameter Hilti with 9-1/4" embedment. Therefore at 1/8" displacement, the Hilti bolt has exceeded its allowable by  $10,000/3,693 = 2.71$ .

The same philosophy can be used for the Richmond insert. Referring to Applicants' Exhibit 142D, Attachment C, sheet labeled 5, at a displacement of .125" (1/8"), the shear load is approximately  $(14 + 16) / 2 = 15$  kips. The capacity for a 1" diameter A307 bolt is 7.85 kips. Therefore, the load in the bolt has exceeded the established allowable by  $15/7.85 = 1.91$ .

In addition, in the design of pipe supports at CPSES, the designer assumes the support is rigid at the bolted connections and does not move, and determines the stiffness of the support or determines the deflection for the support based on this assumption (that is, that the bolted connections don't move). Now the Applicants are stating that the bolted connections by themselves will move 1/8". It would appear that the Applicants are not utilizing appropriate design assumptions. Only if the Applicants were utilizing friction type connections, would their assumptions be proper.

At this time it would be appropriate to bring to the Board's attention what I believe Applicants are up to. The Applicants, in this Motion for Summary Disposition, are addressing the consequences of gaps in bearing type connections. The Applicants have claimed to this Board on the record (for example, Tr. 5154/18-5154/15, 5161/7-25, and 5208/1-17) that they utilize bearing type connections in the design of base

plates utilizing Hilti bolts. But in response to one of Cygna's questions in regards to Hilti bolts, the Applicants informed Cygna that they are designed as friction type connections and will not move because they are pretorqued. See Attachment F (copy of the 4/19/84 letter, with relevant attachments, from L. M. Popplewell, Project Engineering Manager, TUGCO, to Ms. Nancy Williams, Project Manager, Cygna Energy Services), wherein Applicants state (bottom of page 9):

"Using our design approach, the Hilti joints, since they are pretorqued, would perform as a friction joint within their working loads." (Emphasis added.)

This is a complete reversal of philosophy by the Applicants, not presented to the Licensing Board before. At Tr. 5208/1-7, Dr. Chang states that the loads due to pretorquing are to set the wedges and the pretorque value used is too small to be considered sufficient as a friction-type connection.

It is apparent that the Applicants are singing a different song in their response to Cygna. There is no indication within the Phase 3 Cygna Report that Cygna investigated whether or not the Hilti bolts are torqued sufficiently to be considered as a friction-type connection.

One must consider whether or not the statement made to Cygna is true (i.e., the pretorque provided to the Hilti bolts is sufficient to consider them as friction connections). The allowable shear force assuming a safety factor of 2 can be calculated by the following formula modified from the Applicants' Motion for Summary Disposition on cinched-up U-bolts, page 14 of Affidavit, modified to accommodate the shear force requirement:

$$V = (T/K \times D)(.4)/FS$$

where V = the allowable shear capacity

.4 = the coefficient of friction between concrete and steel

K = torque coefficient = .3

D = diameter of bolt (say, a 3/4" diameter)

T = the applied torque

FS = factor of safety = 2

The Brown & Root procedures shown in CASE Exhibit 669B (Attachment to Deposition/Testimony of CASE Witness Jack Doyle), sheet 10P, for a 3/4" diameter bolt has a required torque of 150 foot-lbs.

The allowable shear value is thus

$$1/2 ( (150)(12) / (.3)(.75) ) (.4) = 1,600 \text{ lbs.}$$

The allowable listed in the PSE Manual for a 3/4" diameter Hilti bolt is 3,693 lbs. or a  $(3693/1600)(100) = 231\%$  difference.

The above analysis does not include creep effects on the concrete; these effects will decrease the pretorqued value. The coefficient of friction between the nut and the Hilti bolt was assumed to be .3. Therefore, my analysis is on the very liberal side, and the Applicants' statement to Cygna that the Hilti bolt connection is a friction connection is lacking proper consideration.

In addition, when Brown & Root tested the Hilti bolts for compliance to IE Bulletin 79-02 and compared pretorque to ultimate load, they neglected to consider an important factor. This factor is that Brown & Root did not measure the load induced into the bolt due to

pretorquing, but rather the ultimate load due to pretorquing in a tension test. To have measured the pretorqued value would have required Brown & Root to measure the displacement of the bolt due to an applied load. When the bolt first begins to displace is when the pretorqued value is determined.

4. Applicants state:

"Consideration of all bolts in multiple bolt, bearing connections, with bolt hole tolerances equivalent to those used by Applicants, to react shear loads equally is accepted industry practice and is premised on the fact that the inelastic localized deformations that could result from self-limiting stresses do not unacceptably reduce the ultimate bolt capacity. (Iotti, Finneran Affidavit at 5-7.)"

I disagree with this statement. As already discussed above, accepted industry practice does not allow bearing-type connections when the bolt hole is greater than the maximum standard sized hole. The inelastic localized deformations that the Applicants are relying on have limitations that the Applicants failed to address, as shown above; i.e., allowable bearing stresses and when bearing connections can and cannot be used. Therefore, the conclusion that the Applicants have attempted to make is not complete and violates established code allowables and industry practice.

5. Applicants state:

"The report CASE relied on (CASE Exhibit 1001) to support its contention that at most two bolts may be considered to react shear loads in multiple bolt, bearing connections addressed connections in which bolt hole tolerances from 1.33 times bolt diameter, up to 1/2" for 1" bolts, may be present.

"These conditions could result in a safety factor for shear displacement of only 1.1. (Iotti, Finneran Affidavit at 9-10)."

I disagree with the first sentence. As stated above, the inelastic deformations that occur with the Applicants' position will exceed established code allowables (i.e. allowables based on load, not displacement) with these oversized holes the Applicants use. What Dr. Fisher (referenced in the Iotti/Finneran Affidavit) was addressing was a warning to engineers and designers of the new Code provisions; i.e., an allowance for excessively oversized holes in column base plates where tensile forces are not commonly seen, and the shear force is accommodated by the compressive load of the column. With the old Code (i.e., the 7th Edition), no oversized hole was allowed with A307 bolts to resist a shear load. But the new Code not only allows the oversized hole but the hole can be larger because, as Dr. Fisher states, columns are generally not experiencing tensile loads. Therefore, Dr. Fisher provides methods to accommodate connections for columns that do not contain sufficient compressive loads.

I partially agree with the second sentence, to the extent that it is correct when one considers displacement only, and not allowable stress, for a nuclear power plant.

6. Applicants state:

"In a seismic event, only the first quarter cycle loading could cause preferentially loaded bolts to deflect in shear.

"For the remainder of the cycles the bolts will equally react the loading (Iotti, Finneran Affidavit at 13.)"

I agree with the first and second sentences; however, they are not reflective of the true extent of the problem, as discussed in the following.



The Applicants' example and position is demonstrated in Figure 1 below. At the end of the first quarter cycle loading on a two-bolt base plate, the bolt that reacts first may deform at the peak of the cycle, as shown in Figure 1b below, as the Applicants state. And as shown in Figure 1c, the bolt is permanently deformed. In addition to this, Applicants have another flaw in their presentation. They assume that the bolt is behaving in a ductile manner, under a shear load. This assumption is not consistent with the following statement from NRC Regulatory Guide 1.124 ("Service Limits and Loading Combinations for Class 1 Linear-Type Component Supports," admitted at Tr. 5901, page 1.124-2, B.1.b.):

"The increase permitted by NF-3231.1 and F-1370(a) of Section III for shear stresses or shear stress range should not be more than 1.5 times the level A service limits because of the potential for non-ductile behavior." (Emphasis added.)

Nowhere in ASME NF are the level A service limits or the AISC Code for shear stress allowed to exceed the yield strength of the material. Therefore, the Applicants are in violation of the ASME code, as well as the AISC Code, when they allow the bolts to exceed the yield strength in shear and deform.

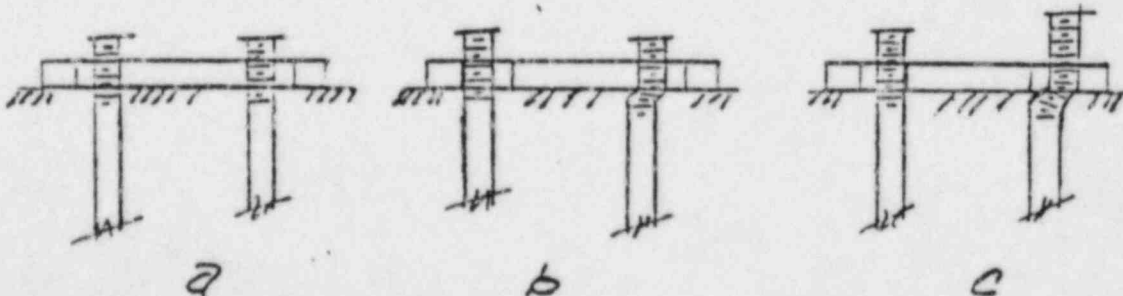


FIGURE 1

The above example consisted of a stiff plate and a flexible bolt. Another condition can also occur, and that is a stiff bolt and a flexible plate, as shown in Figure 2 following.

As shown in Figure 2b, at the end of a 1/4 cycle the original circular hole for bolt A has deformed into an elliptical type of configuration. At the end of the 1/2 cycle, there is now a gap on both sides of bolt A, as shown in Figure 2c below, and there is no bearing between bolt A and the plate. At the end of the 3/4 cycle, the hole for bolt B has now deformed into an elliptical type of configuration, as shown in Figure 2d. At the end of the first full cycle, as shown in Figure 2e below, there are now two permanently elliptical-type holes with gaps twice as large as before the cyclic motion began, and neither bolt A or B is in bearing. If the original gap for a 1" diameter bolt was 1/8", the gap now is 1/4", and this would definitely be considered an oversized hole in that particular direction. This is not allowed for bearing type connections, as Applicants should agree.

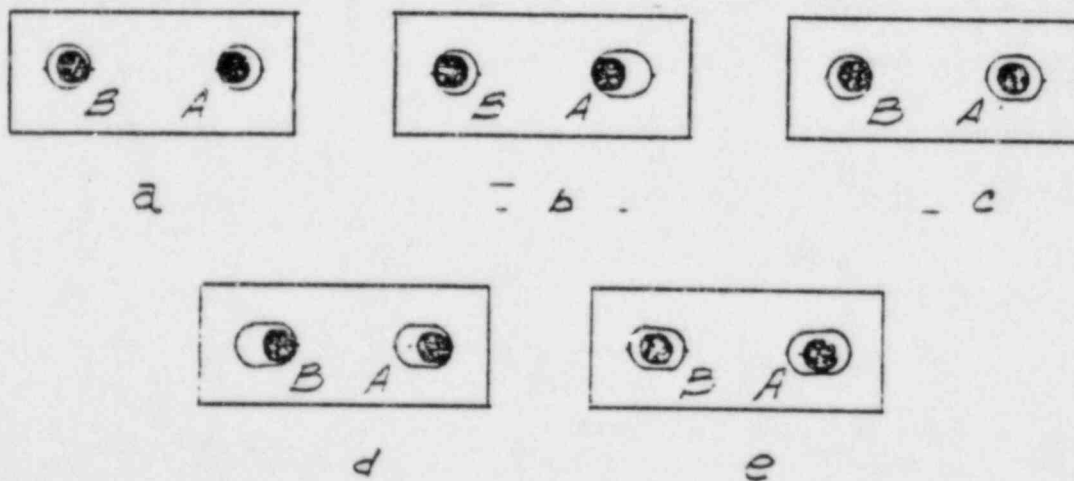


FIGURE 2

The deformation discussed in example 2 is possible since the AISC Code at 1.5.2.2 allows the bearing stress of the plate to exceed the yield strength of the plate in the bearing type connection. The deformation discussed in example 1 (the condition which the Applicants cite) is possible, but would conflict with Regulatory Guide 1.124. And nowhere in the AISC Code is the bolt stress allowed to exceed the yield strength in shear.

Example 2 is realistic when one considers the A307 bolt/tube steel/Richmond insert condition. When the axial force from the tube steel member is transferring this axial load to the bolt by means of shear, the NRC Special Inspection Team (SIT) (as well as the Applicants) claimed that approximately 85% of the axial force being transferred as shear is in the flange of the tube steel member closest to the concrete. The thickness of the tube steel is at most 1/2" thick and the bolt is 1-1/2" diameter (minimum) for supports within the containment. The bolt is designed for an allowable stress value equal to 10 ksi (from Table 1.5.2.1 of the AISC Code, 7th Edition), yet the allowable bearing stress of this thin tube steel member has an allowable of 48.6 ksi for yield strength equal to 36 ksi. The allowable capacity for a 1-1/2" diameter bolt is equal to 17.67 kips. Due to the high allowable for bearing stress, the allowable force for the tube steel member is equal to 36.45 kips. This high allowable will permit deformations for the bearing type connections when cyclic loads are not a consideration. For this reason, example 2 shown above is more realistic for the supports at Comanche Peak than the Applicants' example and position. In either case, the gap is an unacceptable

condition for a dynamically loaded structure, and is not permitted under the AISC Code, Section 1.15.12 discussed in item 1, page 3, of this affidavit.

7. Applicants state:

"The effect of gaps in seismic analyses cannot be defined in absolute terms. The effect is dependent on many factors, including the nature of the excitation (magnitude and distribution of frequencies), and the size, orientation and number of gaps. (Iotti, Finneran Affidavit at 13-14.)"

As indicated on page 14 of the Applicants' Affidavit, the existence of gaps in bearing type connections is a very complicated issue by the fact that non-linearities introduce additional impact loadings, as well as impact damping, and as the Applicants stated:

"Clearly, consideration of such effects would require complex analyses which depart from accepted practices." (Page 14 of Affidavit.) Not only do I agree with this statement, but the AISC Code has recognized the complexity of the gap in bearing type connections due to cyclic loads. Paragraph 1.15.12 Field Connections requires high strength bolts for supports which produce impact or reversal of stress, as discussed above in Answer 1, page 3 of this Affidavit.

Therefore, the complexity to which the Applicants refer is their own doing. The Applicants decided to use bearing type connections with low strength bolts, and consequently are now attempting to justify their erroneous decision. The Applicants have resorted to crying on the Board's shoulder about how complex it would be if they were required to analyze the supports as they now exist.

8. Applicants state:

"Impact damping also occurs in seismic events where gaps are present.

"To account for this damping, however, would require consideration of effects that require complex analyses which depart from accepted design practices. (Iotti, Finneran Affidavit at 14.)"

I agree with the first sentence.

I agree with the second sentence, as discussed above in answer 7.

However, I disagree with their back-up statement on page 14 of the Iotti/Finneran Affidavit, that the impact damping values would be greater than those specified by Regulatory Guide 1.61, for the following reasons: If the Applicants' position is that a higher damping value would be allowed for bearing type connections, it is obvious that Regulatory Guide 1.61 does not allow bearing type connections for cyclic loads, or it would have been listed as a specific item, with a higher damping value. But since bearing-type connections are not common industry practice for seismically qualified supports, Regulatory Guide 1.61 did not list it. Therefore, the Applicants' conclusion that a higher damping value should be allowed due to the bearing type connection would conflict with Regulatory Guide 1.61, as well as the AISC Code (to which Applicants are committed.)

9. Applicants state:

"Material damping will take place as the gap is transversed without a corresponding feed of energy from the seismic event.

"This is a beneficial effect for the seismic response of the system. (Iotti, Finneran Affidavit at 14-15.)"

I agree with the first sentence, as far as it goes, and if one is not concerned with the inelastic behavior and unpredictable behavior of the connection.

I disagree with the second sentence, because you lose the ability to predict the response of the system; you do not know where supports will be moving due to the bearing type connection; you do not know which supports will have the inelastic deformations of the bolts.

10. Applicants state:

"Each of the factors discussed in Findings 7-9 cannot be accounted for in the typical linear response spectrum analyses, as are used at Comanche Peak. (Iotti, Finneran Affidavit at 15.)"

I agree with this sentence, but that does not necessarily mean that the Applicants' position is a correct one. To begin with, IE Bulletin 79-02 required the Applicants to perform tests on expansion anchor bolts. The Applicants neglected to measure the amount of displacement that occurs at the allowable shear value. This is the Applicants' own negligence.

Another important factor which the Applicants were negligent on is the use of the Richmond insert/A307 bolt/tube steel connection. 10 CFR 50.34(a)(2) states:

"50.34 Contents of applications; technical information

"(a) Preliminary safety analysis report. Each application for a construction permit shall include a preliminary safety analysis report. The minimum information to be included shall consist of the following: . . .

"(2) A summary description and discussion of the facility, with special attention to design and operating characteristics, unusual or novel design features, and principal safety considerations." (Emphasis added.)

This Richmond insert/A307 bolt/tube steel connection is not mentioned in the Applicants PSAR, although it is unusual and novel, as I have stated and the Applicants' own witnesses have admitted. (See Walsh, Tr. 3145/6-3146/8; Krishnan, Finneran, Scheppele, Reedy, and Chang, Tr. 5061/18-5065/8.)

In addition, during the 7/3/84 meeting in Bethesda between the NRC Staff and Cygna Energy Services regarding the Cygna Phases 1 and 2 Independent Assessment Program, during a discussion between the Staff's Mr. Terao and Cygna's Ms. Williams, Mr. Terao also indicates that he recognizes that this is an unusual and novel design and points out the importance of the design organization's (such as Gibbs & Hill) having followed ANSI N45.2.11, Section 6.2, which states:

"The extent of the design verification required is a function of the importance of the safety of the item under construction, the complexity of the design, the degree of standardization, the state of the art, and the similarity with previously proven designs."

Mr. Terao discusses examples of an unconventional design, then states (7/3/84 Meeting Tr. 57):

"I don't really see that there's a problem with Richmond inserts, just like there is no problem with the modeling of dual function restraints, in other words, just the Richmond inserts alone, taken by themselves, there's no problem.

"But it has to do with the design considerations that go along with it. And one of design considerations is the use of the tube steel with the holes in it as anchorage for the Richmond insert."

(See full discussion, 7/3/84 Staff/Cygna meeting Tr. 50-57.)

11. Applicants state:

"Each of the factors discussed in Findings 7-9 can only be accounted for with difficulty by performing nonlinear time history analyses. (Iotti, Finneran Affidavit at 15.)"

I agree with this statement. Based upon this statement by itself, it would seem reasonable that the Board require the Applicants to either perform the non-linear time-history analysis which they reference above or utilize a friction-type connection in the supports that are already constructed. But, as discussed in answer 12. below, the utilization of a friction-type connection would validate the assumptions the designers used in their original analysis.

12. Applicants state:

"Identifying the effects of gaps by comparison of the results of nonlinear time history (with gaps) and response spectrum (without gaps) analyses is difficult and one may not discern whether particular results are attributable to differences in individual variables or assumptions or the analytical techniques themselves. (Iotti, Finneran Affidavit at 15-16.)"

I agree with this statement. From what the Applicants have just stated, it would appear that they must be required to install at all supporting connections a friction-type connection to validate their original assumptions, and to have them fabricated as friction-type connections. The Applicants may, in the future, state that their being required to redesign their supports for friction-type connections would be costly (in the hopes that the Board will give them yet a third chance), but as stated above in the previous answers, the Applicants should have done it right to begin with.

13. Applicants state:

"Comparison of the results obtained by response spectra analyses and nonlinear time history analyses which simulate actual gaps in systems show that



- "a) the seismic response spectrum method, which ignores the nonlinearities, is more conservative than the non-linear time domain method (which includes gaps), and
- "b) the effect of gaps on reduction of response frequency is negligible due to the transient nature of the seismic acceleration loading."

"(Iotti, Finneran Affidavit at 16-17.)"

I disagree with Applicants' statements, because if what Applicants state were true, the AISC Code would allow bearing type connections in dynamically loaded structures and supports -- it does not. If the Applicants wish to use the nonlinear time domain method (which includes gaps) to be less conservative than the response spectra method, that would be their option; but as stated above in answer 12, this is not realistic.

In summary, I believe that the Applicants did not properly consider the effects of gaps in the initial or final (i.e., vendor certified) design of pipe supports. The AISC Code does not allow bearing type connections in supports where there is a cyclic type load. The Applicants, on the majority of their supports, have cyclic type loads. They utilize bearing type connections and are therefore in conflict with the AISC Code (to which they are committed). The Applicants rely on references to inelastic deformations to justify their position but omit the consideration of full cyclic loads in the inelastic deformation discussions. They depend on damping factors that are not recognized by the NRC in Regulatory Guide 1.61 for a

justification, after the fact, of their negligence. Because of these gaps, the Applicants are not able to predict how these systems will react to imposed loadings.

If they planned to use this unusual and unique design, Applicants should have initially included it in their PSAR -- they did not. They freely admit that it would be difficult to properly analyze the as-built condition of the supports as they now exist. And finally, Applicants state that the gaps that do exist at Comanche Peak in pipe supports (which I believe are in violation of the AISC Code) are more conservative than the Code requires the Applicant to comply with. In essence, Applicants are trying to convince the Board that not complying with the AISC Code is conservative. I do not agree.

Attachments:

Attachment A -- "Structural Design Guide to AISC Specifications for Buildings," by Paul F. Rice and Edward S. Hoffman, pages 264 through 271 -- (see answer 1, page 2)

Attachment B -- 59 drawings (received on discovery re: Applicants' Motion for Summary Disposition regarding generic stiffnesses), demonstrating reversible loads -- (see answer 1, page 5)

Attachment C -- Copies of an example of the Material Identification Log and associated hanger drawing for support H-BR-2-5B-001-009-3, regarding Applicants' practice re: inspection of bolt holes in base plates -- (see answer 2, pages 8-9)

Attachment D -- 3/9/84 TUGCO Office Memorandum to Distribution from Jerry C. Walker, Subject: Resolution of QAI-0001, and attached 2/22/84 TUGCO Office Memorandum from Boyce Grier to Antonio Vega, Subject: Investigation of Allegations QAI #0001, regarding allegations of oversize bolt hole -- (see answer 2, pages 9-10)

Attachment E -- PSE Manual, Section V, Hilti Concrete Anchor Bolts, Rev. 0, 1/8/82, page 8 of 10, Figure 6, re: allowable load for Hilti bolt -- (see answer 3, pages 11-12)

Attachment F -- 4/19/84 letter with relevant attachments, from L. M. Popplewell, Project Engineering Manager, TUGCO, to Ms. Nancy Williams, Project Manager, Cygna Energy Services, advising Cygna that Hilti joints perform as a friction joint -- (see answer 3, page 13)

The preceding CASE's Answer to Applicants' Statement of Material Facts As To Which There Is No Genuine Issue was prepared under the personal direction of the undersigned, CASE Witness Mark Walsh. I can be contacted through CASE President, Mrs. Juanita Ellis, 1426 S. Polk, Dallas, Texas 75224, 214/946-9446.

My qualifications and background are already a part of the record in these proceedings. (See CASE Exhibit 841, Revision to Resume of Mark Walsh, accepted into evidence at Tr. 7278; see also Board's 12/28/83 Memorandum and Order (Quality Assurance for Design), pages 14-16.)

I have read the statements therein, and they are true and correct to the best of my knowledge and belief. I do not consider that Applicants have, in their Motion for Summary Disposition, adequately responded to the issues raised by CASE Witness Jack Doyle and me; however, I have attempted to comply with the Licensing Board's directive to answer only the specific statements made by Applicants.

Mark Walsh  
(Signed) Mark Walsh

STATE OF TEXAS

On this, the 12 day of August, 1984, personally appeared Mark Walsh, known to me to be the person whose name is subscribed to the foregoing instrument, and acknowledged to me that he executed the same for the purposes therein expressed.

Subscribed and sworn before me on the 12 day of August, 1984.

Samuel W. Nestor

Notary Public in and for the  
State of Texas  
SAMUEL W. NESTOR  
My Commission Expires  
1-31-85

My Commission Expires: \_\_\_\_\_

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OFFICE OF SECRETARY  
DOCKETING & SERVICES  
BRANCH

# Structural Design Guide to AISC Specifications for Buildings

Paul F. Rice  
Edward S. Hoffman



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LONDON TORONTO MELBOURNE

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This book is intended to  
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This Guide does not  
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## CONNECTIONS

### General

The latest AISC Specifications permit a wide variety of connections. The basic requirement, appropriate with the sophisticated combinations of different types of steel to be connected, different design requirements of connections, and different means of connections, is a performance requirement consistent with the overall development of the Specifications. This requirement states simply "... that the design of connections be consistent with the assumptions as to the type of construction..." (1.2). Each of the detailed requirements for the design of connections simply builds upon this basic requirement. By implicitly or explicitly requiring that the design of a particular type of connection be consistent with the design assumptions as to the type and amount of force to be transmitted, and rotation capacity (or rigidity) consistent with the rotation assumed necessary to develop the connection forces, the basic performance requirement is completed (1.2).

The Specifications explicitly recognize inelastic behavior in connections of members designed as elastic: "virtually unchanged" angles at the joints in rigid frames, "non-elastic" deformation of parts of connections in Type 2 and 3 construction, and "inelastic rotation" for wind connections with Type 2 construction (1.2). Elastic behavior in the connections of members under plastic design is implicitly recognized (2.1).

### Scope

For the purposes of this Chapter, connections are most conveniently considered as classified on two bases; (1) materials used (rivets, bolts, pins, or welds), and (2) the assumed behavior of the connection (design requirements: rigid, semi-rigid, or plastic for moment; shear transmission only; tensile or compressive force only; or combinations). In addition to forming joints between two or more steel members or parts of members, connections are required to elements composed of other structural materials. For composite action with concrete elements not bonded by encasement, shear connections are required (1.11.1). Shear connections may utilize specially designed shear connectors or standard welded stud connectors (1.11.4; 1.4.6). For connection of steel column bases to transmit any direct tension or shear, anchor bolts are required (1.22).

It is not intended in this presentation of a wide search in this area. (See explanations and illustrations overlooked or troublesome interpretations to the extension of such interpretations been desirable to extend plate connections were design to cover an applicable Code. During the interim revised to agree with the

### Rivets, Pins, and Bolts

**Rivets and Pins.** The requirements have been directed toward there has been little change the requirements for, as in little need for interpretations available under ASTM are given in Table 1.5. (1.14.2); computed as a diameter of the rivet hole

The use of pin connections in modern steel building, requiring special design. The requirements have remained unchanged from previous

Perhaps the most useful alterations or additions to construction, bearing-type (1.15.10). If used in connection strengthening existing connections to place loads, and the new

**Bolts.** Bolts may be classified A325, for  $F_t = 40$  ksi, and (A307) bolts are usable may be designed for either

The use of ordinary bolts The allowable stresses are 10 ksi (1.5.2.1). The specification rules out the  $\frac{1}{16}$  in. larger than the nominal fill out the hole like a ring may not be assumed. In addition, low-strength column splices in all cases where width/height <

It is not intended in this chapter to duplicate the design aids, detail data, and examples in the *AISC Handbook*, Part 4, Connections. Equally, space limitations do not permit presentation of a wide range of examples to illustrate even the recently published research in this area. (See "Selected References".) Rather, the purpose here is limited to explanations and illustrations of all applicable Specification requirements that might be overlooked or troublesome in routine work. This aim will include indication of reasonable interpretations to resolve apparent conflicts or ambiguities in the Specifications, and extension of such interpretations where the Specifications seem to have omissions. It has been desirable to extend this aim somewhat in that design aids for bearing plate and base plate connections were included as well as an extension of concrete bearing connection design to cover an apparent gap between the AISC Specifications and the ACI Building Code. During the interim between preparation and publication, AISC specifications were revised to agree with the latest ACI Building Code.

### Rivets, Pins, and Bolts

**Rivets and Pins.** The requirements for the use of rivets and pins were established many years ago and were in many AISC Specifications. Since most of the late research has been directed toward welded, and more recently high-strength bolted connections, there has been little change in the Specifications for the use of rivets. Familiarity with the requirements for, and a sharply reduced use of, rivets in building construction results in little need for interpretations of these Specifications. Rivets of Grades 1 and 2 are available under ASTM A502 (1.4.2). Allowable stresses (for tension and bearing only) are given in Table 1.5.2.1 (1.5.2.1). Net sections for tension members must be used (1.14.2); computed as prescribed (1.14.3); and allowance of  $\frac{1}{16}$  in. made plus the nominal diameter of the rivet holes (1.14.5).

The use of pin connections, originally popular in truss construction, has declined in modern steel building, and is usually encountered only for very special situations requiring special design. The general requirements for the use of pins are brief and essentially unchanged from previous Specifications (1.14.6).

Perhaps the most used application of these Specification requirements today will be in alterations or additions to existing buildings in which rivets or pins were used. For new construction, bearing-type connections can not be assumed to share stress with welds (1.15.10). If used in combination, the welds must be designed for the entire stress. In strengthening existing construction, bearing connections can be assumed to carry the in-place loads, and the new welds designed only for the additional stress (1.15.10).

**Bolts.** Bolts may be classified by strength as (1) low, A307, for  $F_t = 20$  ksi; and (2) high, A325, for  $F_t = 40$  ksi, and A490, for  $F_t = 54$  ksi . . . (1.5.2.1). The ordinary low strength (A307) bolts are usable only in bearing connections (1.5.2.2). The high strength bolts may be designed for either bearing or friction connections (1.5.2.1).

The use of ordinary (A307) bolts is limited by a number of Specification requirements. The allowable stresses are low: tension  $F_t = 20$  ksi on the threaded area; and shear  $F_v = 10$  ksi (1.5.2.1). The slip before full bearing is achieved on a group of ordinary bolts effectively rules out the sharing of stress in a mixed connection. Holes are to be taken as  $\frac{1}{16}$  in. larger than the nominal diameter (1.23.4), and the ordinary bolt does not expand to fill out the hole like a driven rivet nor can it be used for dependable friction. Stress sharing may not be assumed between ordinary bolts and rivets or welds (1.15.10; 1.15.11). In addition, low-strength bolts are not permitted in important field connections including column splices in all buildings with  $H \geq 200$  ft., and where width/height  $< 0.25$ ; also where width/height  $< 0.40$ , for  $H \geq 100$  ft.; beam-column or column-bracing connections

where  $H > 125$  ft.; frames carrying cranes with more than five-ton capacity; and connections subject to vibration, impact, or stress reversal (1.15.12); nor for flange-to-web nor cover plate-to-flange connections of built-up girders (1.10.4).

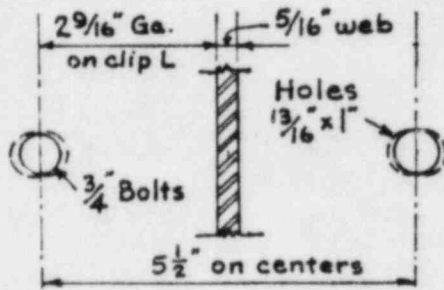
High strength bolts (1.16.1) and welds are considered essentially equivalent as connections, and, for friction-type joints assembled prior to the welding, the high-strength bolts may be assumed to share stress with welds in a mixed connection (1.15.10) or with rivets (1.15.11). Gross sections may be used for the design of compression members (1.14.2), and for the flanges of both built-up and rolled-shape girders provided the area of holes is equal to or less than fifteen percent of gross flange area (1.10.1). For tension members net section area is the basis of design (1.14.2). In friction-type joints resisting direct tension, the shear stress permitted with high strength bolts must be reduced (1.6.3).

**Slotted Holes for Bolted Shear Connections.** The use of short-slotted holes is permitted under 1974 AISC Specification for "Structural Joints Using ASTM A-325 or A-490 Bolts," Section 3, subject to the approval of the designer. They can be used in either friction-type or bearing-type connections, provided a washer is installed over the hole.

The normal hole size for a  $\frac{3}{4}$ "  $\phi$  bolt is  $\frac{13}{16}$ ", whereas a short-slotted hole is  $\frac{13}{16}$ " deep by 1" long (or  $\frac{3}{16}$ " longer in the horizontal dimension). While the Specifications state that the hole can be either vertical or horizontal, the authors suggest only the horizontal slotted method be used. End clip holes only would be slotted, not the holes in the connection beam or column. See sketch, a full scale view of the end clip holes and bolt relationship for a typical  $\frac{5}{16}$ " thick web.

The advantages to this system are many, several of which are:

1. Greater erection speed with less field burning of misaligned holes.
2. The use of one size clip angle with a set gauge will accommodate web thickness from  $\frac{3}{16}$ " to  $\frac{9}{16}$ ".
3. The reduction in sizes of clips to fabricate and stock should help reduce costs.
4. The speed of erection (and elimination of mill web thickness tolerance problems) should help reduce cost.



Short-slotted holes layout for clip  $\angle$  - shear connection

## Welds

**General.** Full penetration groove-welds can be designed for full development, same stress as the base metal (1.5.2.1), by selection of the specified matching electrode and welding process (1.17.2). For all fillet, plug, and slot welds, and partial penetration groove-welds, reduced permissible stresses upon the effective throat area (1.14.7) are specified (1.5.2.1). In no case may the stresses exceed that for the base metal, or if different, the weaker base metal (1.5.2.1).

**Special Considerations.** A number of minor special considerations arise in the specification of welding. Generally, net sections are not a consideration except for plug and slot welds in which the gross area of the holes is deducted to check the fifteen percent maximum allowed (1.10.1; 1.14.3). The Specifications require preheating for various conditions, including all work when the temperatures are below 32°F (1.23.6). Except for single- and double-angle or similar minor members, welds are to be laid out to avoid eccentric axial force or such eccentricity must be considered in the design of the connection

and the member connect to accommodate the need and the selection of the connection.

As previously noted, welds are required as a mixed connection prior to the welding, also important, though not generated in the operation strained, leave corresponding local inelastic yielding, but warping and lamellar tearing caution of a specified sequence avoid warping. Even after to retain adverse residual stresses, stress relief by heat service is not provided unless

The use of a proper sequence same can also be specified. Particularly with thicker members restrained and the result should be given to the practicable sequence as strains without developing the entire connection design economical to specify a

## Connection Design

**Classification.** In addition connections, certain are established. All connections support not less than shear in flexural members, all at allowable members are to be designed (1.15.2). These minimum of light members such as members are required to meet the minimum six kips strength of the member truss in which the minimum load for open web steel design stress or half the Joists; Examples.)

As noted previously, method or the design the transmission of shear members connected and tra

\*\*Commentary on Highly 1973.



capacity; and connection for flange-to-web nor

equivalent as connection high-strength bolts (1.15.10) or with rivets on members (1.14.2), and the area of holes is reduced. For tension members joints resisting direct load are reduced (1.6.3).

Drilled holes is permitted in A-325 or A-490 bolts can be used in either shear or tension. The hole is  $\frac{13}{16}$ " deep by specifications state that only the horizontal distance between the holes in the connection holes and bolt re-



Holes layout in shear connection

development, same matching electrode and partial penetration base metal, or if dif-

arise in the specification for plug and slot fifteen percent maximum for various connections (1.23.6). Except for laid out to avoid eccentricity of the connection

and the member connected (1.15.3). For the usual shear connection requiring flexibility to accommodate the necessary simple-end rotations assumed, the locations of the welds and the selection of the connection elements must be coordinated (1.15.4).

As previously noted, where welding at high-strength bolted friction-type joints is required as a mixed connection with shared stress, the final tightening of the bolts is required prior to the welding. The *sequence* of completing purely welded connections is also important, though not explicitly covered by the Specifications (1.23.6). The heat generated in the operations of welding creates intense shrinkage strains which, if restrained, leave corresponding residual stresses (1.23.6). These stresses can be relieved by local inelastic yielding, but where local inelastic yielding is also restrained or limited, warping and lamellar tearing\* may result. For many welded assemblies, the simple precaution of a specified *sequence* of welding may be employed to balance the strains and to avoid warping. Even after this precaution, certain complex assemblies may be expected to retain adverse residual stresses. For cases where this condition is anticipated or suspected, stress relief by heating must be specified by the Engineer (1.23.6). (Note: this service is not provided unless it has been specified and will normally be an added cost.)

The use of a proper *sequence* to avoid creation of shrinkage stresses or to minimize warping can also be specified in many connections where lamellar tearing might occur. Particularly with thicker sections, where both the direction of the shrinkage is completely restrained and the resulting stress is normal to the surface of the section, consideration should be given to the welding sequence. If the condition can not be eliminated by a practicable sequence as a first choice for a solution, it may be possible to relieve the strains without developing large stresses by use of soft wire "cushions" or by revision of the entire connection detail. At least for simple cases it should, of course, be more economical to specify a particular welding sequence. (See Examples this chapter.)

### Connection Design

**Classification.** In addition to the general requirements previously cited for the design of connections, certain arbitrary minimum design requirements for connections have been established. All connections for members carrying calculated stress must be "designed to support not less than six kips" (except lacing, sag bars, and girts), presumably six kips shear in flexural members, six kips tension in ties, and six kips bearing in compression members, all at allowable stress levels (1.15.1). Eccentric connections of axially loaded members are to be designed to transmit the resulting moments as well as the axial force (1.15.2). These minimum requirements naturally become most significant in the design of light members such as axially loaded members in trusses. Connections for such members are required to meet an additional requirement that they transmit the design load or the minimum six kips, whichever is larger, and develop at least half of the effective strength of the member (1.15.7). Note: joists are regarded as a special very limited-size truss in which the minimum connection capacity is simply specified as twice the design load for open web steel joists (4.5); or for the longspan and deep longspan joists, as the design stress or half the allowable strength of the member (103.5b). (See Chapter 4: Joists; Examples.)

As noted previously, connection types may be classified on the basis of the connection method or the design function. Broadly, connections may be described as *flexible* (for the transmission of shear only, 1.15.4), or *rigid* (maintaining the angle between the members connected and transmitting full moment capacity of the most flexible element at the

\*"Commentary on Highly Restrained Welded Connections," *Engineering Journal*, AISC, 10, No. 3, 1973.

joint as well as the shear, 1.15.5), or *semi-rigid* (transmitting a pre-determined fraction of the full moment capacity as a rigid joint and further loads in shear as a flexible joint with corresponding angle change to supply rotation for the additional loads, 1.15.5; 1.2).

**Flexible Connections.** "Flexible" connections are designed to transmit shear without exceeding allowable unit stresses on the connectors as a group or the connection as a whole. The use of an average capacity for each of several connector elements sharing the total load is justified by allowing self-limiting localized stresses determined by an elastic joint analysis to exceed the yield point and create inelastic localized deformations of the connector materials, or by inelastic deformations of the connection elements (1.15.4). The simplest examples of localized deformation occur in the assembly of bearing-type bolted connections where the cumulative tolerances permitted exist on (1) out-of-round in the bolts, (2) oversize holes ( $\frac{1}{16}$ " ), and (3) center-to-center location of the holes in the different elements connected. The extreme degree of such inelastic action occurs with a two-bolt bearing-type connection where one bolt is loosely fitted and one is very tight. Until the material of the connected element surrounding the loaded bolt or the bolt yields and deforms ( $+\frac{1}{16}$ " ), the load is not shared and a 50 percent adjustment will be developed as the load increases. For larger (and thus more important) members, more bolts or rivets will be required and the degree of adjustment required on each will be less. Lesser adjustments are required for a long line of bolts or rivets intended to share stress equally. Even if perfectly fitted, yielding and inelastic deformations occur, maximum at and beginning at the first loaded bolt or rivet, and decreasing to a minimum at the last. (See Figs. 5-1

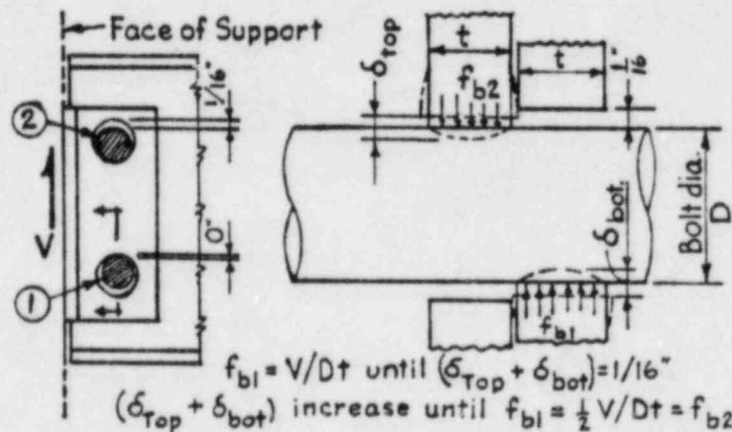


FIG. 5-1 Self-Limiting, Localized Deformations—Two Bolts.

and 5-2.) After this localized inelastic adjustment in the connectors for shear transmission, consider the inelastic adjustments that occur to reduce the "elastic theory" moments.

Inelastic deformation in the connection elements, typically angles, will occur and reduce the restraint which would transmit moment. The common double-angle shear bearing connection is extremely stiff longitudinally for the transmission of shear, and it depends upon the minor inelastic bearing deformations around each fastener to equalize the shear stresses in the fasteners. The same double-angle member is relatively flexible and will twist to permit a relatively large angular rotation reducing moment transmission. (See Fig. 5-3.)

Experience and tests confirm the practical assumptions of shear transfer only and the



Inelastic plates :  
ginning  
tuning  
 $\delta_2, \delta_3$   
in all

FIG. 5-2 Self-Limiting



FIG. 5-3 Self-Limiting Angles.

use of an average stress served in one series limits correspondingly the same for Figure 5-4 presents reported from these "s" (see Fig. 5-3) support. Coping t and required angle deep connections.

For Type 2 constant design drawings; all capacity for the section designed for one half

<sup>1</sup>"Moment-Rotation" Engineering Journal, AISC

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rs, more bolts or rivets  
be less. Lesser adjust-  
re stress equally. Even  
mum at and beginning  
he last. (See Figs. 5-1



Inelastic deformations occur successively in the plates at each fastener and in the fasteners, beginning and largest at the first loaded, and continuing until the elastic strains in the spaces  $s_1$ ,  $s_2$ ,  $s_3$ , and  $s_4$  become proportional to equal stress in all fasteners.

FIG. 5-2 Self-Limiting Deformations—Axial Stress on Line of Separate Fasteners.

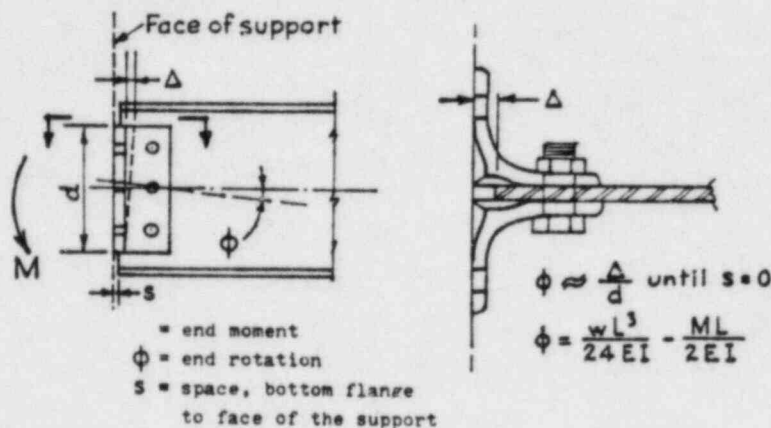
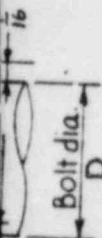


FIG. 5-3 Self-Limiting Deformation (Twist) in the Connection Elements (L) Two Angles.

use of an average shear stress per unit weld or separate fastener. The actual rotations observed in one series range from 0.84 to 0.97 times  $\Phi_0$ , the "simple beam rotation." These limits corresponding to moments ranging from three to sixteen percent were approximately the same for a single end plate connector or the common double-angle connector.<sup>1</sup> Figure 5-4 presents the usual device for an approximate analysis. An additional caution reported from these tests is that the moment stiffness increases abruptly when the space "s" (see Fig. 5-3) closes and the lower flange transmits compression to the face of the support. Coping the bottom flange where a quick analysis of the proportions of depth and required angle change show the usual clearance to be inadequate may be desirable for deep connections.

For Type 2 construction (flexible connections) all the reactions should be shown on the design drawings; alternatively, only those exceeding one half the tabulated uniform load capacity for the sections used, together with a general note that connections shall be designed for one half the capacity unless otherwise noted, should be shown.

<sup>1</sup>"Moment-Rotation Characteristics of Shear Connections," Kennedy, October, 1969, 6, No. 4, *Engineering Journal*, AISC.



$Dt = f_b 2$

Bolts.

ators for shear trans-  
the "elastic theory"

s, will occur and re-  
ble-angle shear bear-  
on of shear, and it  
fastener to equalize  
is relatively flexible  
oment transmission.

ansfer only and the

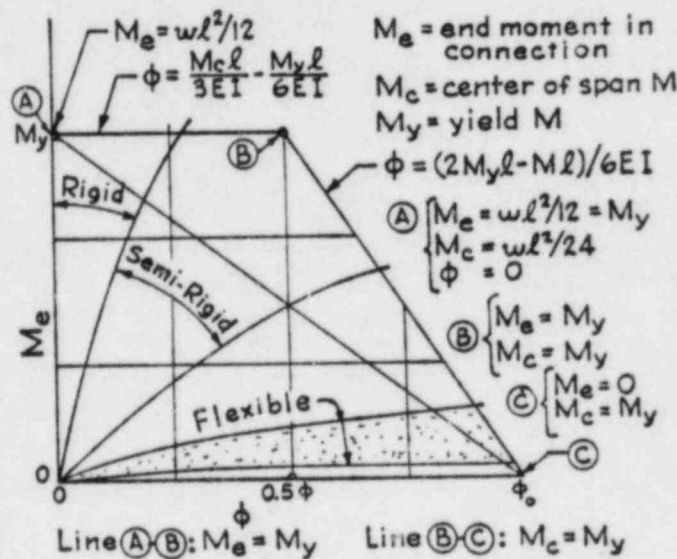
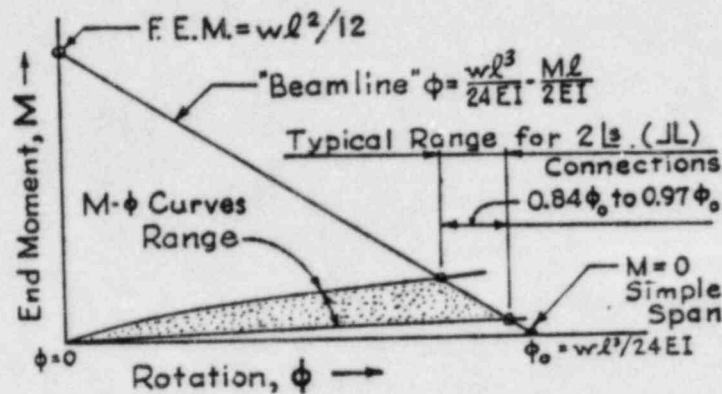


FIG 5-4 Uniformly Loaded Elastic Beam Line—Rotations at Connection.

**Rigid Connections (Type 1 Construction).** The AISC Specifications requirement is quite realistic: that rigid connections hold the original angles "virtually" unchanged (1.2). This requirement in elastic design is usually satisfied by connections designed to develop the full section of the flexural member or the full moment at yielding of the more flexible member connected. It will be noted from Fig. 5-4 that the rigid frame analysis ( $\Phi = 0$  at the allowable stress) may be satisfied by such a connection which would have a very small rotation at  $0.66$  to  $0.60F_y$ , but would be capable of a significant rotation at yielding of the flexural member (line A-B).

A diagram similar to Fig. 5-4 but with point A representing an end moment,  $M_e = M_p$ , and point C, a center span moment,  $M_c = M_p$ , can be prepared for plastic design. Connections capable of achieving full collapse load (hinges at both ends and center of span) would be required to reach  $\Phi = 0.5\Phi_0$ , point B. The simpler concept of "plastic redesign," where only end hinges are required to form at the factored load, would require connections with a somewhat less rotation capacity, along line A-B. See Fig. 5-5.

**Semi-Rigid Connections (Type 3 Construction).** (See Fig. 5-4.) Ideally, the semi-rigid connections for Type 3 construction will behave elastically between the  $\Phi = 0$  ordinate

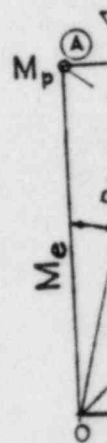


FIG. 5-

and the "rigid" connections determined end moments to develop the yield moment. In practical cases where plastic hinges are required, the excess moment capacity of the hinges only will form more rotation capacity.

### Masonry Bearing

**General.** The AISC Specifications on masonry and steel connections (1.5.5) allow low allowable stresses for concrete block, and hollow concrete masonry units. Values for steel are therefore not shown and brick laid in mortar. The AISC Specification is a conservative economy. \*\* The AISC Specification codes. For design of masonry bearing in beam bearing p

\*All mortars until  
\*\*Supplement N

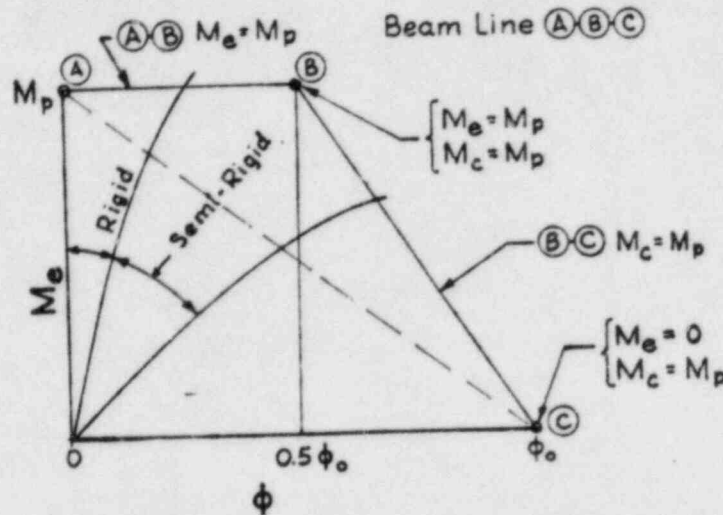


FIG. 5-5 Uniformly Loaded Plastic or Rotations at Connection.

and the "rigid" connection up to a predetermined end moment. Upon reaching this predetermined end moment ( $M_y$  for the connection), a rotation capacity sufficient to develop the yield moment at the center of the span,  $M_c = M_y$ , should be available. In practical cases where the nearest available rolled section will be above the design capacity required, the excess capacity will be provided at the midspan. As in plastic redesign, end hinges only will form at the full design load. Since these hinges are designed for  $M_e = M_y$ , more rotation capacity is required (to cross line B-C).

### Masonry Bearing Connections

**General.** The AISC Specifications provide very conservative allowable stresses for bearing on masonry and concrete which apply in the absence of Code (statutory Building Code) regulations (1.5.5). For all masonry laid up in mortar, most statutory codes also provide low allowable stresses. Usually, codes distinguish among solid masonry units, bricks or block, and hollow units as well as among different classes of mortar and masonry materials. Values so prescribed range in general from 50 psi to 400 psi. The AISC Specification is therefore seldom applicable since it includes only stone masonry,  $F_p = 0.400$  ksi, and brick laid in "cement" mortar,  $F_p = 0.250$  ksi (1.5.5). *The authors recommend use of the masonry bearing values prescribed in local Codes or those recommended by national associations dealing with masonry products.* For bearing stresses on concrete, the AISC Specifications,  $F_p = 0.35f'_c$  on the full area and  $F_p = 0.35f'_c \sqrt{A_2/A_1} \leq 0.70f'_c$  on fractions of the area, utilize recent ACI Building Code (ACI 318-71) refinements for economy.\*\* The ACI Building Code is of course usually applicable under local statutory codes. *For beam-bearing plates and column base plates on concrete, the authors recommend the use of bearing values prescribed by the ACI Building Code.*

**Beam Bearing Plates.** The approved design (Chapter 2, pp. 82-83, *AISC Handbook*) for beam bearing plates is the formula:

$$t = \sqrt{3 f_p (n)^3 / F_b}$$

(Continued on page 274)

\*All mortars utilize cementitious materials and the term "cement" can be quite properly applied to all.  
 \*\*Supplement No. 3, 1974.



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ENGINEERING USE ONLY

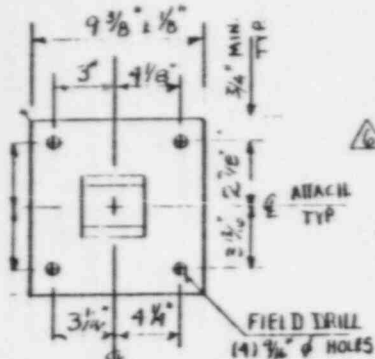
UPLINE 10-9-81 AS-BUILT

ENDORSED CERTIFIED

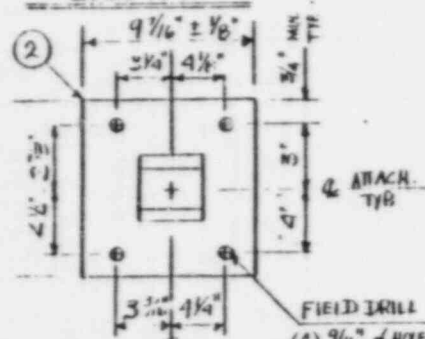
WING REV. NO. 6

DATE: 8/16/83

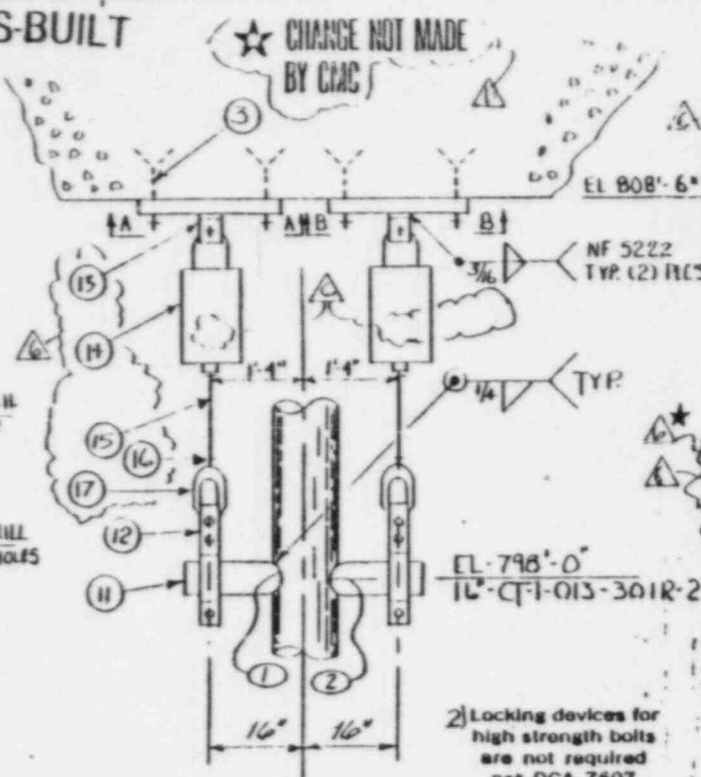
★ CHANGE NOT MADE BY CMC



ATTACH. MAY VARY ± 1/4" SECT. A-A



ATTACH. MAY VARY ± 1/4" SECT. B-B



2) Locking devices for high strength bolts are not required per DCA 7607

NOTE

1) By issue of rev. 4 of this Drawing, the following Documents are voided: CMC-55201

CONT' ABOVE

MVIS

X = +.272 / .006  
Y = +.340 / .009  
Z = +.019 / .142



THIRD PARTY INSPECTION CODE CLASS: ASME III-CL 2

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	L	CSS	PRIM	SEC	AISC
1	1/2" C.S. IP PER SECT A A (SA 36 / SA 515 GR 65)	1		X			X		
2	1/2" C.S. IP TYP SECT B B (SA 36 / SA 515 GR 65)	1		X			X		
3	1/2" x 5/16" MULTI KWIR POINT (1 3/4" DIA EMB)	4					X		
4	PRD-05 WELD BEAM ATTACH (SA 36)	2					X		
5	VSB-07 VARIABLE SPRING HI = 556	2					X		
6	CL = 572 MVT. 256 UP W/ TRAVEL STOP						X		
7	RET-05 END TURN ATTACH 1 1/4" x 1 1/4" LG	2					X		
8	REN-05 WELDLESS EYE NUT (A660-B)	2					X		
9	FIN-3/8 HEX HEAD NUT	4					X		
10	FIN-1/2 (D) HEX HEAD NUT 1 1/4" x 1 1/4" LG	1					X		
11	FIN-3/8 NUTS (SA 36)	4					X		
12	1/2" x 1/4" x 1/2" STAINLESS STEEL (SA 304)	4					X		
13	1/2" x 1/4" x 1/2" STAINLESS STEEL (SA 304)	4					X		
14	1/2" x 1/4" x 1/2" STAINLESS STEEL (SA 304)	4					X		
15	1/2" x 1/4" x 1/2" STAINLESS STEEL (SA 304)	4					X		
16	1/2" x 1/4" x 1/2" STAINLESS STEEL (SA 304)	4					X		
17	RET-05 WELDLESS EYE NUT (A660-B)	2					X		

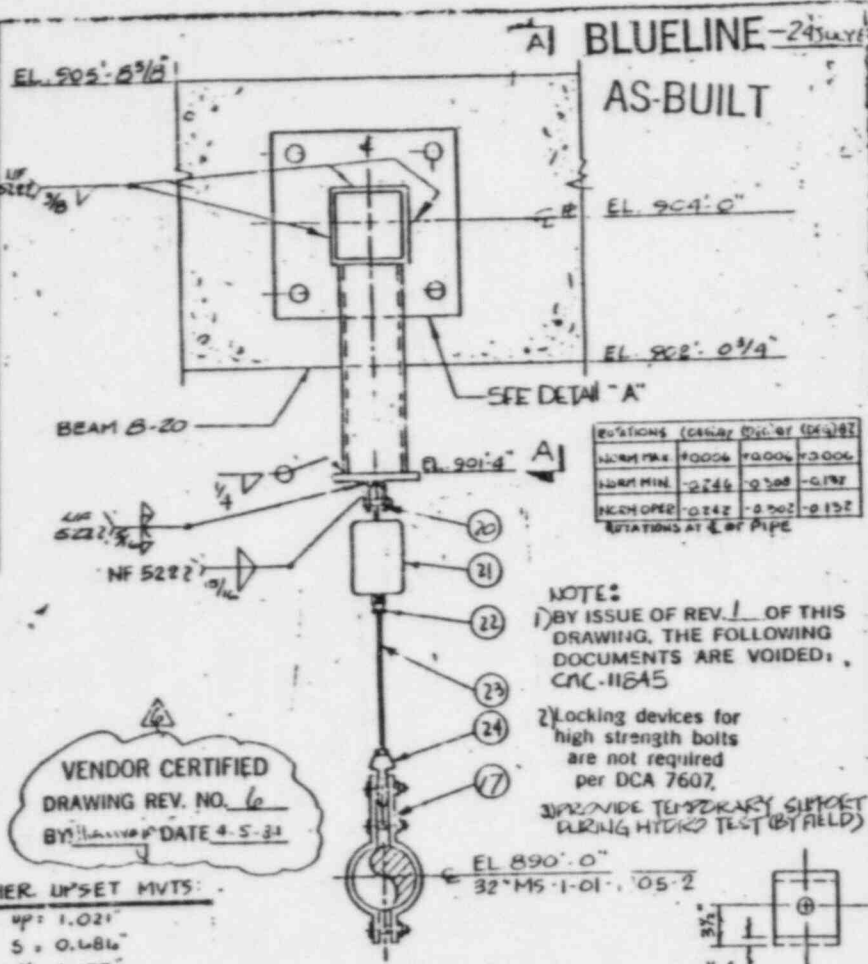
REV	DATE	BY	CHK	APP	DESCRIPTION
1	10/9/81	...	...	...	REV'D AS NOTED - REF: FMHSRI - SEE NIT 1
2	...	...	...	...	REV'D AS NOTED - REF: CMC 61288
3	...	...	...	...	REV'D AS NOTED - REF: CMC 61288
4	...	...	...	...	REV'D AS NOTED - REF: CMC 61288

REV	DATE	BY	CHK	APP	DESCRIPTION
1	10/9/81	...	...	...	ISSUED FOR CONST F.W. 1-10
2	...	...	...	...	REV'D AS NOTED - REF: CMC 61288
3	...	...	...	...	REV'D AS NOTED - REF: CMC 61288
4	...	...	...	...	REV'D AS NOTED - REF: CMC 61288

FOR OFFICE AND ENGINEERING USE ONLY

DRILL Iso. CT-1-SB-OB R.1  
I.P.D. Iso. CT-1-SB-OB-KV.3  
Data Point 254/PROB AP21-32 R.0  
Pipe Mat'l. SA 35B, CL 7, TP 304  
Insul. Bldg. SB

LEAVE VERTICAL CLEARANCE...  
 GIVE BRIDGE...  
 IN V. VERTICAL...  
 REVD VERTICAL...  
 REV'D ADJ. INDICATED...  
 IN PINK...  
 IN RED...  
 IN BLUE...  
 IN GREEN...  
 IN YELLOW...  
 IN PURPLE...  
 IN BROWN...  
 IN GRAY...  
 IN BLACK...  
 IN WHITE...

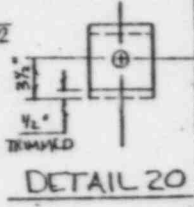


**NOTE:**

- BY ISSUE OF REV. 1 OF THIS DRAWING, THE FOLLOWING DOCUMENTS ARE VOIDED: CAC-11845
- Locking devices for high strength bolts are not required per DCA 7607.
- PROVIDE TEMPORARY SUPPORT DURING HYDRO TEST (BY FIELD)

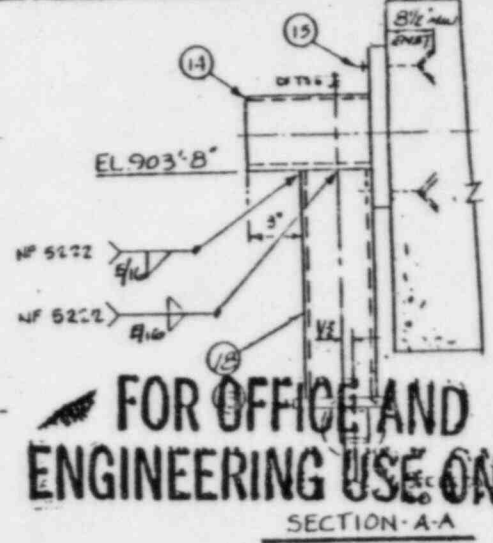
**VENDOR CERTIFIED**  
 DRAWING REV. NO. 6  
 BY: [Signature] DATE 4-5-81

**THER. UPSET MVTS:**  
 up: 1.021  
 S: 0.486  
 V: 1.177



ELEV. LKG SOUTH

ITEM NO	NO REQ'D	DESCRIPTION	WT.	ASME OR ASEN	PR. NO.	MIC.
1	1	605 16 WELDED BEAM ATTACH		SA 36		
2	1	YCB TO RUC HE END ATTACHMENT				
3	1	VARIABLE SPRING SUPPORT				
4	2	FIN 5" Ø HEAVY HEX NUT		SA 36		
5	1	RET. RING HANGER ROD END NUT		SA 36		
6	1	REN TO WELDLESS EYE NUT		SA 36		
7	1	PTC 605 2222 PIPE SLAVE				
8	1	TS 2 X 6 X 3/8		SA 36		
9	1	TS 2 X 6 X 3/8		SA 36		
10	8	RWP 1/2 EXCEPT 1 X 6 X 3/8 2PM		SA 36		
11	4	RAT 1/2 1 X 3 LG STUFS		SA 36		
12	8	FIN 1 1/4 Ø HWY HEX NUTS		SA 36		
13	1	FP 3/4 X 8 X 8		SA 36		
14	1	TS 8 X 8 X 1/2 X 9" LG		SA 36		
15	4	1/4" SUPER BULBS 13"		SA 36		
16	1	2" THK CSR PER DETAIL 'A'		SA 36		
17	1	PTC-320-2832 PIPE CLAMP		SA 36		
18	1	TS 2 X 6 X 3/8 X 2'-9" LONG		SA 36		
19	1	ASME B NAME PLATE W/ MARKING				



FIELD REVIEW OF SUPPORT DESIGN  
 AS BUILT CONDITION OK - ALL  
 DATE 7-27-80 REVIEWED BY: S. JAMES

**CPSES**  
 35-1195  
 CONTROL

LOCATION PLAN

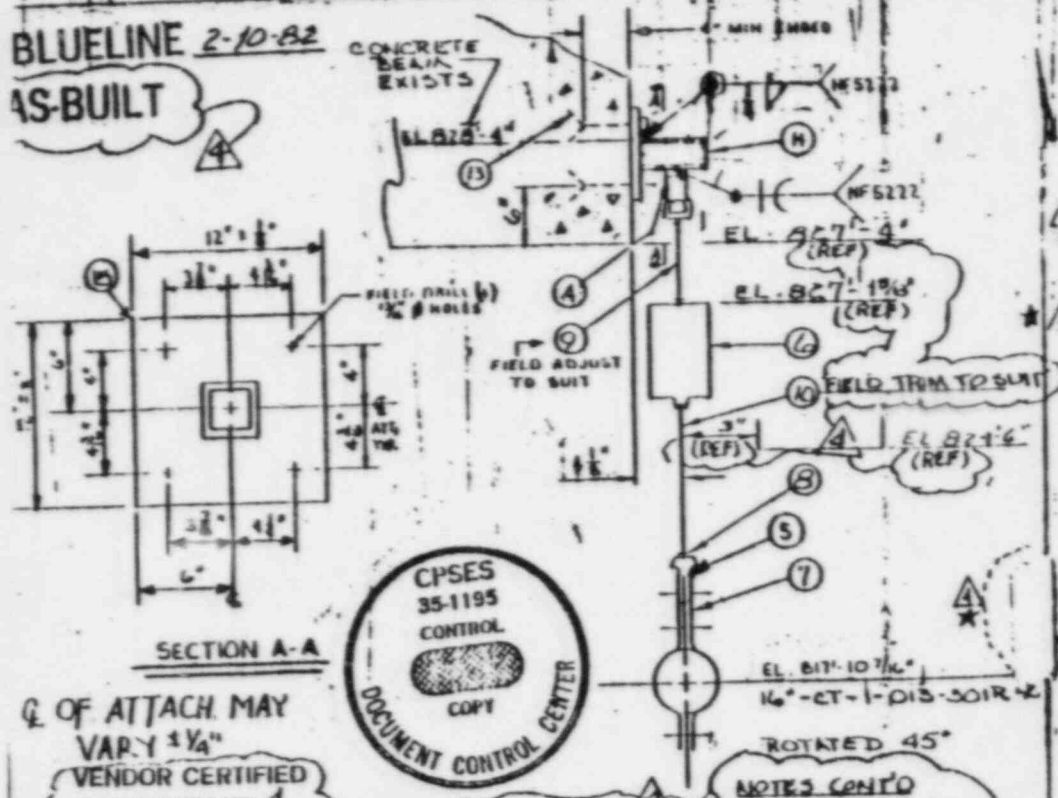
GRAM	ITER	HYDRO	ORE	ISE	ISIGHT	EMERG	PLD	INTS	INTE	DELTA	MECH	REFERENCE DRAWINGS	OWNER	PROJECT	ENGINEER	PRODUCTION ORDER	SERIAL NUMBER	SHEET
												MS-1-RB-02	TEXAS UTILITIES SERVICES INC.	COMANCHE PEAK UNITS NO. 1 & 2	GIBBS & HILL INC.	138	MR NO. MS 1001-002-6725	REV 6

**FOR OFFICE AND ENGINEERING USE ONLY**





BLUELINE 2-10-82  
AS-BUILT



Q. OF ATTACH. MAY VARY ± 1/4"

VENDOR CERTIFIED DRAWING REV. NO. 4

BY *[Signature]* DATE *1/15/82*

BRNL 150-CT-158-08 R-1

I.P.B. Iss. CT-1-58-08 R-1

Date Print 2/11/82

Pipe Mat'l SA-306/SA-312

Insul. 314g. S

NOTES

4) BY ISSUE OF REV. 2 OF THIS DRAWING, THE FOLLOWING DOCUMENTS ARE VOIDED:

CMC 33089

NOTES (CONT)

5) BY ISSUE OF REV. 3 OF THIS DRAWING, THE FOLLOWING DOCUMENTS ARE VOIDED:

CMC 3447

NOTES (CONT)

6) Locking devices for high strength bolts are not required per DCA 7637

NORM OPER DISP.	
DX	+0.047
DY	+0.180
DZ	-0.080

\* NOT CHANGED BY CMC

MOVEMENTS	
X	+0.202 / -0.041
Y	+0.796 / -0.121
Z	+0.070 / -0.450



THIRD PARTY INSPECTION

CODE CLASS: ASME-III-C

OFFICE AND

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	CEC	PRIN	MEC	PLANN
	HANGER ASSEMBLY CONSISTING OF:	ONE						
	MATERIALS LIST							
1	Carbon Steel (SA312 GR 65 or SA 36) Plate	1						
2	Detail A, TH-144							
3	3/4" x 1/2" Hilti Bolt with Concrete Anchors, TH-24	4						
4	Hilti (SA 36) 3/4" x 1 1/2" Long TH-14	1						
5	1/4" Fig. 66N W/Load Pin Steel Attachment	1						
6	1/4" Fig. 290N Eye Nut	2						
7	1/2" Fig. 38N W/Travel Stops (Not Load)	1						
8	1/4" Cold Load Steel	1						
9	1/2" Fig. 20XN Wire Clamp	1						
10	1/4" Reg Nuts (SA-307 GR)	4						
11	1/4" Fig. 140N W/Thread Full Length	1						
12	1/4" Fig. 140N W/12" Thread Both	1						
	Ends							
	HANGER ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG	1						
	MARK # CT-1 (C) - 002-5475							
	16" UT N.D.E./PAR 2.5.1 of the Unit							
	PFice Structure							
	Apply one coat of Carbor Zinc Oil to above mat'l except th'ds which shall be coated w/a rust preventative.							
13	1/2" x 7" x 1/2" HILTI ANCHOR	4						
14	TS 3/4" x 1/2" (A500 GRB) x 6" LG.							
15	3/4" R (SA36/SA312 GR 65) PER SEC A-A							

REV	DATE	BY	DESCRIPTION	CONDITIONS	Fz	Fy	Fz	Mz	My	Mz
1	1/12/82	FW	ISSUED FOR CONST.	DESIGN						
2	1/12/82	FW	REV'D AS NOTED, REF. FIELD MODIFIED HANGER SKETCH.	EMERGENCY						
3	11/12/82	FW	REV'D AS NOTED, REF. FIELD MODIFIED HANGER SKETCH.	FAULTED						
4	1/12/82	FW	REV'D AS NOTED, REF. FIELD MODIFIED HANGER SKETCH.							

CUSTOMER: Texas Utilities Service, Inc.

ORDER OR CONT. NO.: CF-0046

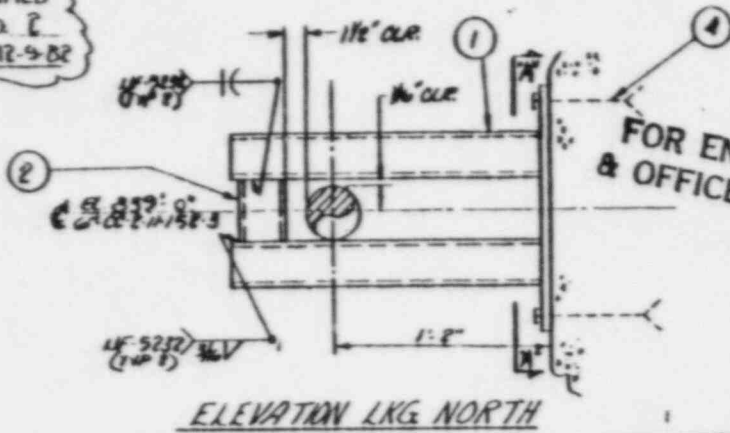
JOB NAME: Concho Park 1 & 2

MARK NO.: CT-1-DIS-002-5475

SHEET 1 OF 1 REV. 4

**AS-BUILT**

VENDOR CERTIFIED  
DRAWING REV. NO. 2  
BY BH DATE 12-9-82



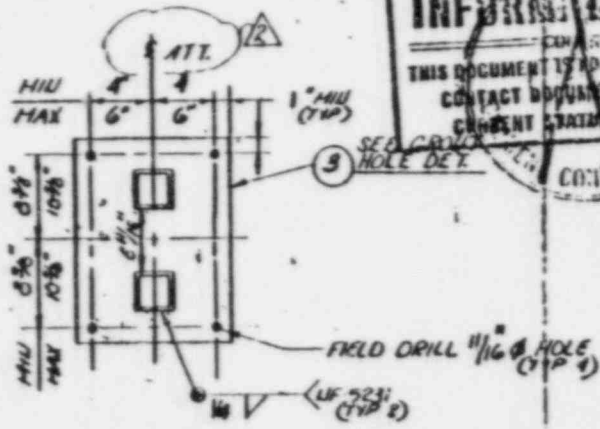
ELEVATION LKG NORTH

FOR ENGINEERING  
& OFFICE USE ONLY

ITEM NO	QTY REQ'D	MATERIAL DESCRIPTION	P.B.S.	L	C.S.	W.M.	SEC.	AISC
1	2	3/4x1/2x1/8 TUBE A500 GR.B.			X			
2	1	3/4x1/2x1/8 TUBE A500 GR.A.			X			
3	1	FX 50/1 SECT A-A (SA-515 GR.65)	X					
4	4	3/8x6\"/>						

APPLY OILY MNT OR G-DO JIC'S FILL TO ABOVE MAT'L EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE.

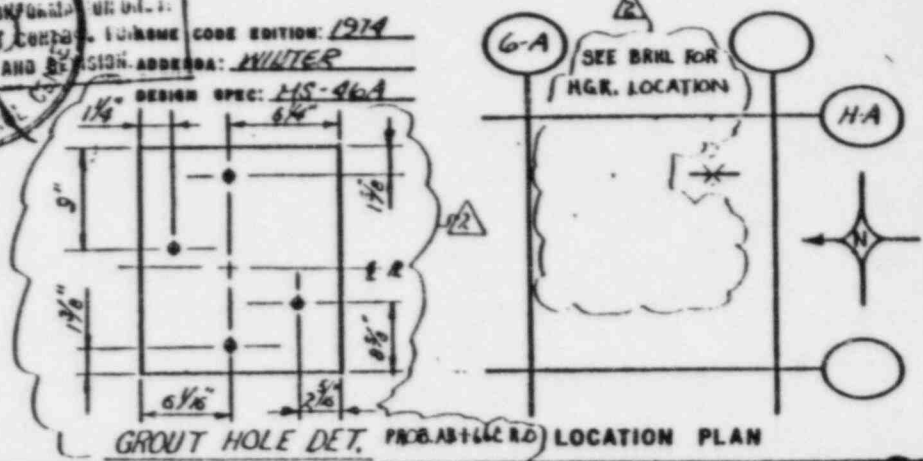
REV	DESCRIPTION	DATE	OWN	CHK'D	APP'VD
1	REV'D AS-BUILT SET CAP AS SH'D TO	12/9/82	TEH	Q	CBD
2	VENDOR CERTIFICATION, LTNW 59790				



SECTION "A-A"

NOTE:  
1. LOCKING DEVICES FOR HIGH STRENGTH BOLTS ARE NOT REQUIRED PER DCA 7602

**INFORMATION COPY**  
THIS DOCUMENT IS THE PROPERTY OF THE U.S. GOVERNMENT. IT IS TO BE RETURNED TO THE OFFICE OF THE ASSISTANT SECRETARY FOR PLANT AND FACILITIES, WASHINGTON, D.C. 20545. ADDRESS: WINTER DESIGN SPEC: HS-46A



GROUT HOLE DET. PROB. ABT. (L&RD) LOCATION PLAN

DATA PT	SUPPORT	LOADS (LBS)	PIPE	REF	BRHL	REV	MECHANICAL	REV	ELECTRICAL	REV	DESCRIPTION	DATE	OWN	CHK'D	APP'VD
2082	DESIGN	DESIGN	DESIGN	DESIGN	CC-2-AB-031	0	MI-0702	0	EI-0702	0	REV. AL NTD; REF. DCA 7407 (SEE REF.) WENG	5/21/81	DPH	JW	
VERT					FAB 190	REV	STRUCTURAL	REV	H.V.A.C	REV	REV. FAB 191-6) CPAC-35476, R.2) AS-BUILT				
E-S					CC-2-AB-031	0	S-0718	5	MI-0755	6	1 FC.	12-27-79	CAT.	IM	MPA
E-W															

NOTE: AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>	ABME CODE CLASS <u>3</u>
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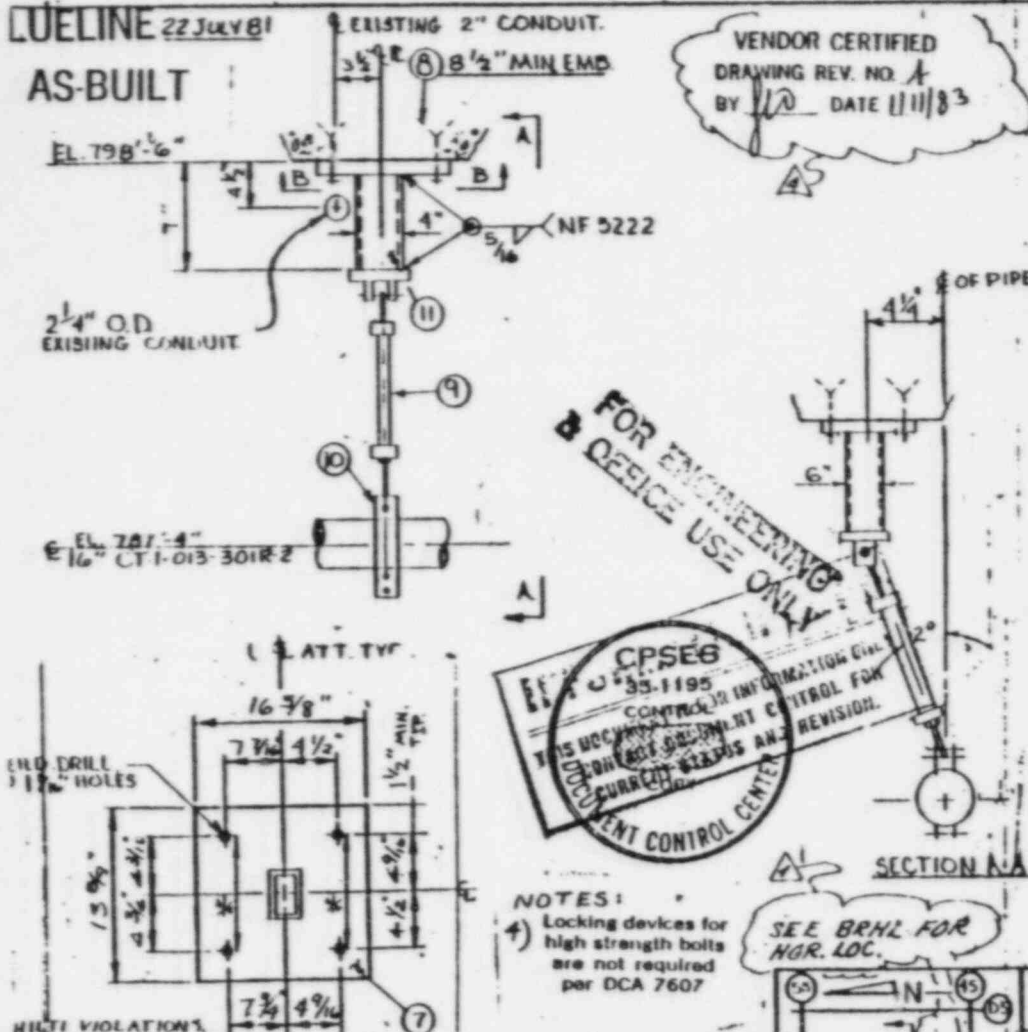
<b>CRS</b> Brown & Root, Inc HOUSTON, TEXAS 33-1193	CLIENT <u>T.U.S.I.</u> PLANT <u>COMANCHE PEAK</u> JOB NO. <u>K323</u>	SUPPORT NO. <u>CC-2-01-719-A23P</u> SHEET <u>1</u> OF <u>1</u> REV. <u>2</u>
--	---	---

FOR OFFICE AND

ENGINEERING USE ONLY

LOE LINE 22 JULY 81

AS-BUILT



VENDOR CERTIFIED  
DRAWING REV. NO. A  
BY *[Signature]* DATE 11/11/83

FOR ENGINEERING  
DESIGN USE ONLY

CPS&G  
35.1195  
CONTROL CENTER INFORMATION DIV.  
THIS DOCUMENT IS INFORMATIONAL ONLY  
AND IS NOT TO BE USED FOR  
CURRENT DESIGN AND REVISION.  
CONTROL CENTER

NOTES:  
1) Locking devices for high strength bolts are not required per DCA 7607

SEE BRHL FOR HGR. LOC.



THIRD PARTY INSPECTION  
CODE CLASS: ASME III-2

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PLS	CS	PTM	SEC	ATSC
7	1 1/4" C.S.P. Per Sec. B-B (SA 315 3165 OR SA 306)	1		X				
8	1-1/2" HILTI KWIK CONC. ANCHOR	4				X		
9	3/8" 30-30 SWAY STRUT C.C. B-10	1				X		
10	3/8" 30-30 PIPE CLAMP	1				X		
11	1/2" EL. 1/2" X 0-3/2" LONG STRUCTURAL TUBING (A-300 G-B)					X		

REV	DATE	OWN	CHK	APP	DESCRIPTION
A	10/11/83	Q	C	B	VENDOR CERTIFICATION REQ. BYN 62726

MARK# CT-1-013-011-522R  
PAINT: CARBO ZINC # 11

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN		-1723				
NORMAL & UPSET		-3683				
EMERGENCY		-6081				
FAULTED		-1769				

REV	DATE	OWN	CHK	APP	DESCRIPTION
A	5-29-80	D	W	K	ISSUED FOR CONST.
B	8/10/80	D	W	K	REVISED AS NOTED
C	8/10/80	D	W	K	FOR ITI REV. 11
D	8/10/80	D	W	K	REV'D AS NOTED REPTIT
E	8/10/80	D	W	K	CMC 53215, F.M.H.S.
F	8/10/80	D	W	K	REV'D AS NOTED REPTIT
G	8/10/80	D	W	K	REV'D AS NOTED REPTIT

CUSTOMER: Trade Utilities Service, Inc.  
ORDER OR CONT. NO. CP-0048  
JOB NAME: Comanche Peak I&E  
MARK NO. CT-1-013-011-522R  
SKETCH NO.  
SHEET 1 OF 1 REV. 7

BRHL Iso. CT-1-SB-08 Rev. 1  
BRP Iso. CT-1-SB-8 Rev. 3  
Data Point 250/PROB/18-1-32 R.O.  
Pipe Mat'l. SA 358 & 1-TP 304  
Insul. — Bldg. SA

T.O. 4802

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ENGINEERING USE ONLY



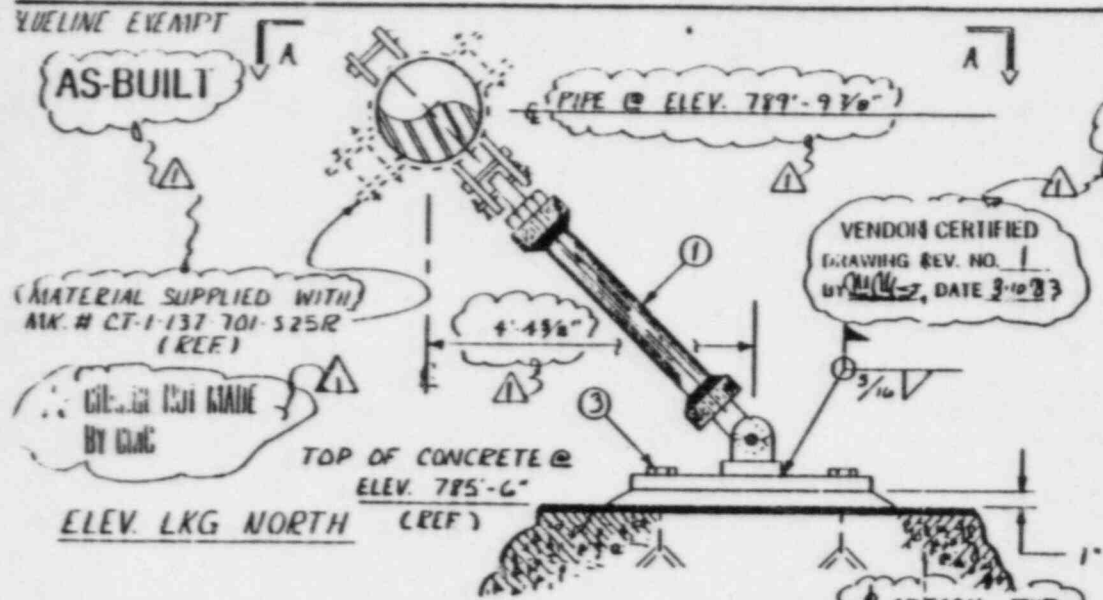


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 ENGINEER MUST BE RESPONSIBLE FOR DESIGN  
 STANDARDS AND SPECIFICATIONS.

**FOR ENGINEERING  
& OFFICE USE ONLY**

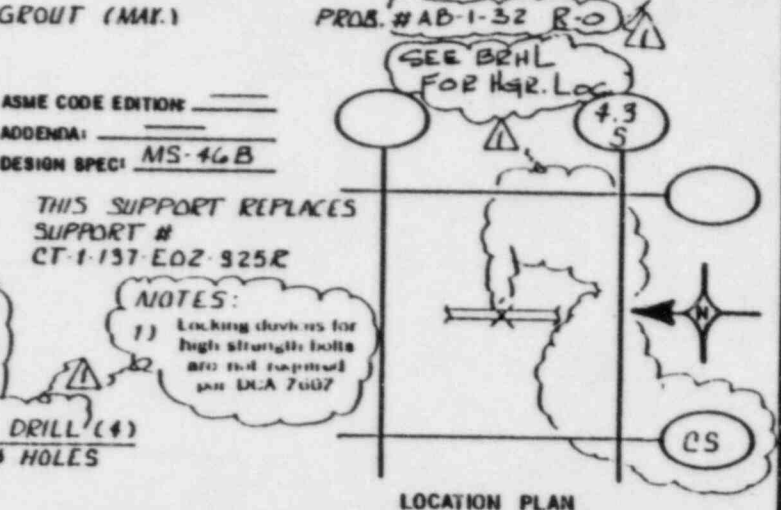
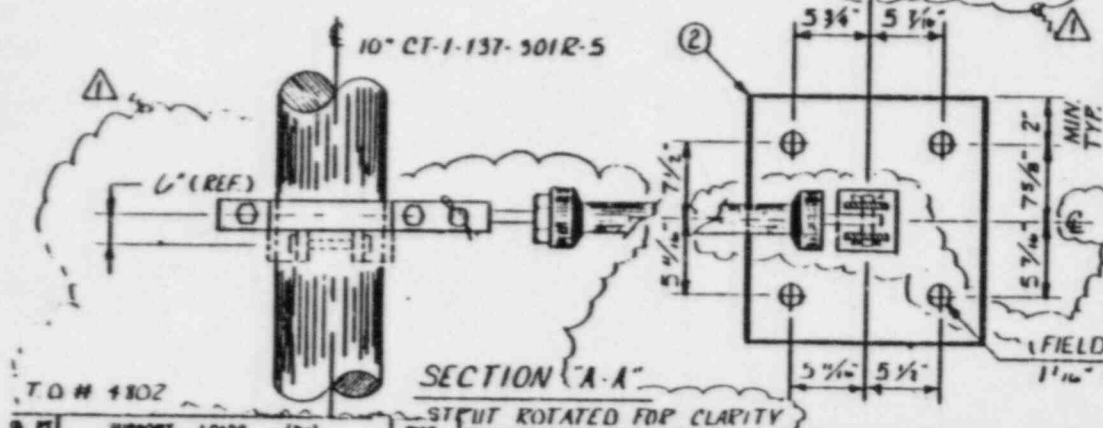
**FOR OFFICE AND  
ENGINEERING USE ONLY**



ITEM NO.	QTY. REQ'D.	MATERIAL DESCRIPTION	PS	CS	MIN	REL	AISC
1	1	SXS-20-PC SWAY STRUT; C-C=4'-7 3/4" WITH SPC-20-100 PIPE CLAMP (SA-36)					
2	1	1" THK. CARBON STEEL PLATE (A-36) (SEE SECTION 'A-A')					
3	4	1" x 1/2" LONG SUPER HILTI KWIK BOLT (75% MIN. E.M.B.)					
		PAINT: CARBO-ZINC # 11					

REV.	DESCRIPTION	DATE	OWN.	CHKD.	APPRD.
A	ISSUED FOR CONST. REF. P&ID	1/14/83	VLM	NHP	RAG
B	FOR P&ID (15/87)				
C	CORR. BELOW				



T.O.# 4802

NO.	DESIGN	REVISION	LEVEL	LIMITS	PIPE	MVTS	INCHES
1							
2							
3							
4							
5							

REV.	DATE	BY	CHKD.	APPRD.	DESCRIPTION
1					REV'D AS NOTED REF: DCA 66791K1
2					DCA 7607 (INT#1) AS-BUILT VERIFIED
3					REDESIGNATION CPPA260BZ

**Brown & Root, Inc.**  
 ENGINEERING AND CONSTRUCTION  
 HOUSTON, TEXAS

CLIENT T.U.S.I.  
 PLANT COMANCHE PEAK  
 JOB NO. 2323

SUPPORT NO. CT-1-137-702-925R  
 SHEET 1 OF 1 REV. 1





**FOR OFFICE AND ENGINEERING ONLY**

**FOR OFFICE AND ENGINEERING ONLY**

**LUELINE  
3-BUILT**

NDOR CERTIFIED  
DRAWING REV. NO. 5  
DATE 4/25/83

ITEM NO.

MATERIALS & OPERATIONS

SEISMIC SWAY STRUT ASSEMBLY CONSISTING OF

SMA-10 RO SMUUBER

C.S. R 1" x 8" x 8" (SA-36)

SPC-14 1/2" PIPE CLAMP

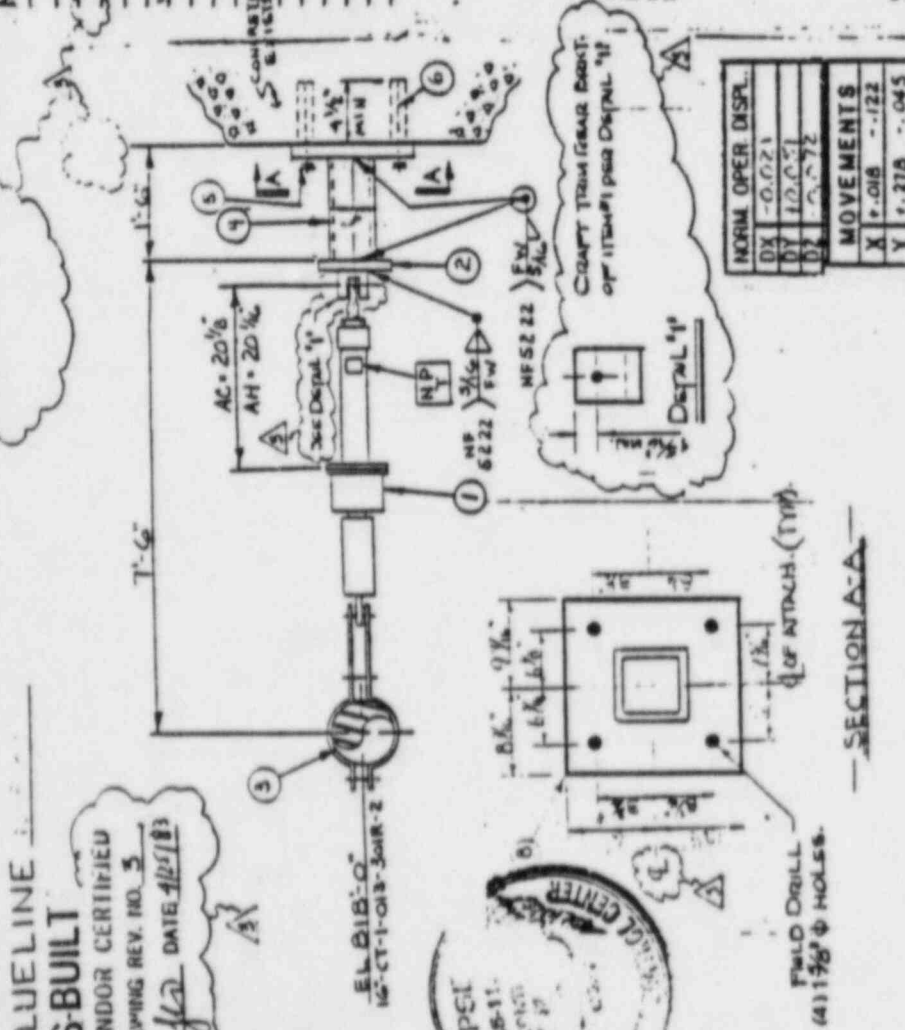
QUAN SHIP

ONE

**INFORMATION COPY**

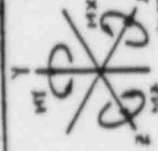
THIS DOCUMENT IS FOR INFORMATION ONLY  
CONTACT THE ENGINEERING DEPARTMENT  
FOR ANY INFORMATION

**FOR ENGINEERING & OFFICE USE ONLY**



SEE BRILL FOR HGR. LOCATION

T.O.# 4802



THIRD PARTY INSPECTION  
CODE CLASS: ASME III-2

LOCATING DIMENSIONS FOR HIGH STRENGTH BOLTS ARE NOT REQUIRED PER DCA 300

BRILL ISO. CT-1-58-008 Rev. 1  
I.P.S. ISO. CT-1-58-008 Rev. 5  
Date: 5/1/83 / FROM: AB-F-32 Rev. 0  
Pipe Mat: SA-35B CL-11P303  
Rev: 5-E

SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG MARK # CT-1-013-021-542K

NEW MATERIAL REQUIRED  
4 1/2" x 4" x 1/2" STRUCTURAL TUBING (A-500.70) GR. B) 1'-4 3/4" LONG, TW = 39 WF  
5 1/2" HEX NUT (SA-307 GR. B)  
6 1/2" x 8" x 1/2" FLANGE W/ THREAD FULL LENGTH  
7 1/2" x 1/2" CARBON STEEL (SA-36) LONG PLATE  
8 CARBON STEEL PLATE (SA-36) PER SECTION A-A (SA-36)

Approved By: S.E.L.  
Date: 6.20.79

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. 1

Brown & Root, Inc.

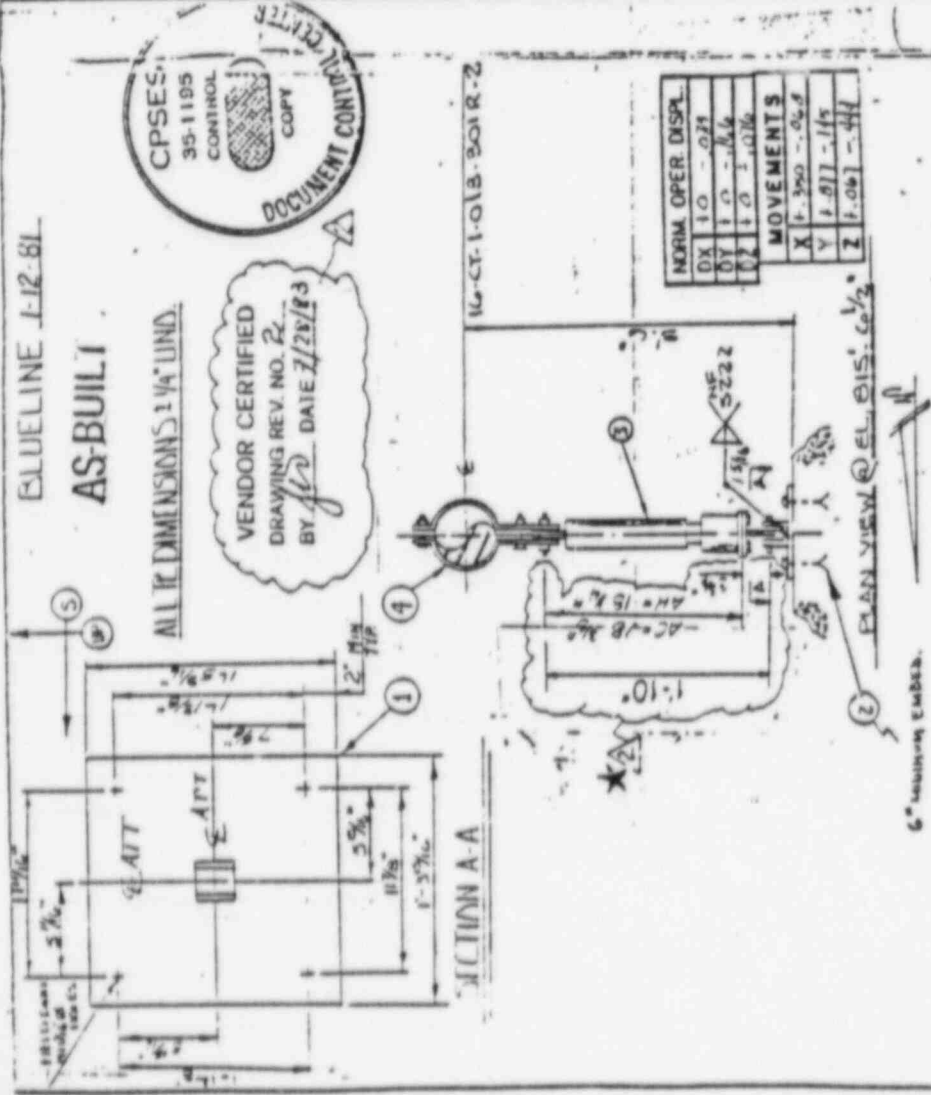
DESIGN NORMAL UPSET # 2738  
EMERGENCY # 247  
FAULTED

PIPE: M1-0662-REV.13 ELECT. 11-0402-01  
STEEL: S1-0605-REV.5 HV.A.C.I. REV. 6

DESCRIPTION  
ISSUED FOR CONST. REF. FIELD MODIFIED  
DANGER SKETCH 11 R; NPST, R.O.A  
STVS WITH RT NW 11359 R.O.A  
REV. 11-11-81 1) AS BUILT  
VENDOR CERTIFICATION REF#  
GT# 62726  
Rev. D. VALUOS Certification  
Rev. C. Valuos Certification

CUSTOMER Texas Industries Service, Inc.  
ORDER OR CONT. NO. CP-0056  
JOB NAME Coanche Peak 1 & 2  
MARK NO. CT-1-013-021-542K  
SKETCH NO.  
SHEET 1 OF 1 REV. 5

# FOR OFFICE AND ENGINEERING USE ONLY



**NOTES:**  
 Locking devices for high strength bolts also not required per UCA 7607

**★ CHANGE NOT MADE BY CMC**

PAGE: 100-CL-1-56-0-8-1  
 B.P.P. 180-CT-1-53-9-REV. B  
 Issue Point: 260/1000/40-1-12-81  
 Pipe Mat'l: SA 35B CL 1-11-30A  
 Insul: 110g-5B 7/6" 4802

ITEM NO.	REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC. NO.	WT.	QTY	UNIT	REV
1		C.S. 1/4" THK (SEE SECT. A-A)		SA-36					
2		ASA-1-12 (CNC WORK)							
3		SME-10-80	SNUBBER						
4		SA-36 1/4" DIA. 2" LONG	ANCHOR BOLT						
5		SPC-13-7/16	PIPE CLAMP	SA-36					
6		ACME 3/8" DIA. 1 1/2"							
SKETCH ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG MARK # CT-1-013-019-547K									
Apply one coat of CARCO ZINC RICH TO ABOVE MAT'L except threads which shall be coated w/a rust preventative.									
<b>FOR OFFICE AND ENGINEERING USE ONLY</b>									
Approved By: C.F.G. Date: 6-20-79 QUAN SHIP:									

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. \_\_\_\_\_ SHEET OF \_\_\_\_\_

**Brown & Root, Inc.**

REF. DRAWING NUMBERS: SA-06-17, REV. 5 ELECT. REV. B  
 STEEL: SA-35B, REV. 5 HV.A.C. 11-2-81

PIPE: SA-35B, REV. 5 ELECT. REV. B  
 STEEL: SA-35B, REV. 5 HV.A.C. 11-2-81

DESCRIPTION: ISSUED FOR CONSTRUCTION FIELD MODIFIED HANGER SKETCH, ITR-10 NPS 4" DIA. ORIENTED MT 1-3

LOCATION PLAN: SEE DETAIL FOR HGR. COORDINATE

THIRD PARTY INSPECTION: [ ]  
 CODE CLASS: ASME III-2

CUSTOMER: Texas Industrial Services, Inc.  
 ORDER OR CONT. NO.: CI-0046  
 JOB NAME: Concho Peak 1 & 2  
 MARK NO.: CI-1-013-019-547K  
 SKETCH NO.:  
 SHEET 1 OF 1 REV 1.3

# FOR OFFICE AND ENGINEERING USE ONLY

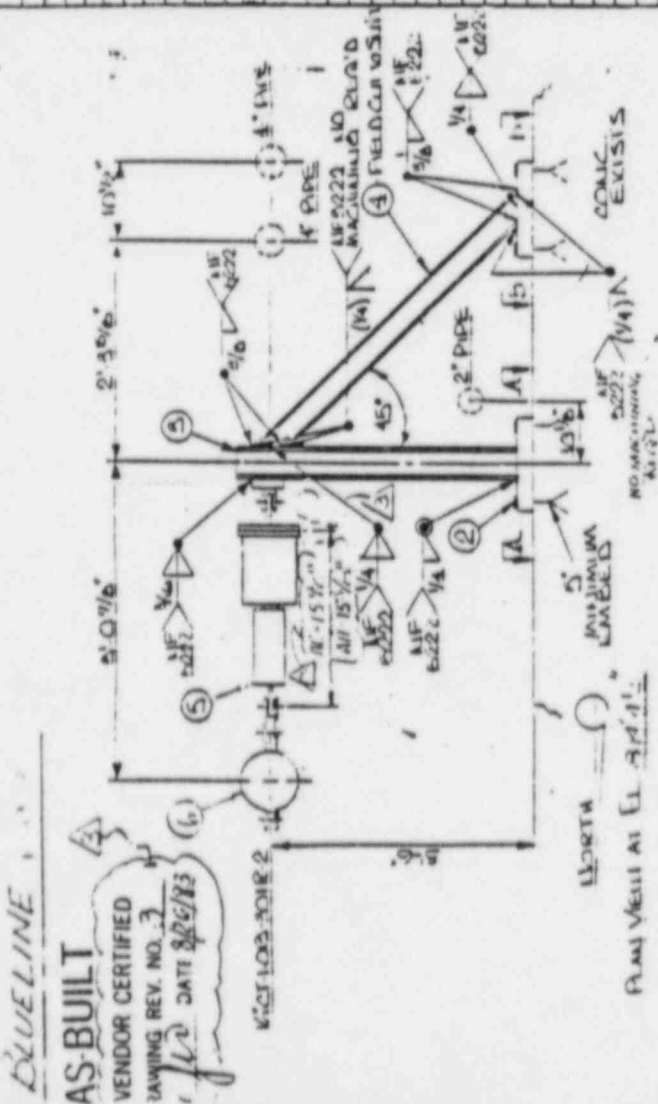
ITEM NO.	REQD NO.	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC NO.	WT.	QTY	UNIT
1	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
2	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
3	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
4	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
5	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
6	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
7	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
8	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
9	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
10	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
11	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
12	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
13	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
14	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
15	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
16	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
17	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
18	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
19	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
20	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
21	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
22	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
23	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
24	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
25	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
26	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
27	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
28	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
29	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
30	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
31	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
32	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
33	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
34	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
35	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
36	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
37	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
38	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
39	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
40	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
41	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
42	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
43	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
44	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
45	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
46	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
47	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
48	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
49	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC
50	1	1/2" x 1/2" x 1/2"	WELDED STEEL	SA-36		11	1	PC

SKETCH ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAP MARK # CT-1-013-018-842K

Apply one coat of Cadon Zinc-#11 to above and 1 coat of zinc-rich paint to be coated with epoxy primer, etc.

DESCRIPTION  
REV'D VENDOR CERT REF  
REV'D VENDOR CERT REF  
REV'D VENDOR CERT REF  
REV'D VENDOR CERT REF

Approved By: C.F.L.  
Date: 6-20-79



MOVEMENTS	
X	+0.007
Y	+0.007
Z	-0.002

NOTE  
4) Locking devices for high strength bolts are not required per DCA 7607

1810 100-114-011K1  
1810 100-114-011K2  
Data Point/PROG. 1811K0  
Pipe Mat'l SA-36, CL. 1, TP. 504  
Issued: \_\_\_\_\_ Bldg. 50

SEE NOTE FOR HANGER LOCATION

LOCATION PLAN

THIRD PARTY INSPECTION YES  NO

CODE CLASS: A-MV-III-2

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. \_\_\_\_\_ SHEET OF \_\_\_\_\_

Approved By: C.F.L.  
Date: 6-20-79

FOR BROWN & ROOT, INC.

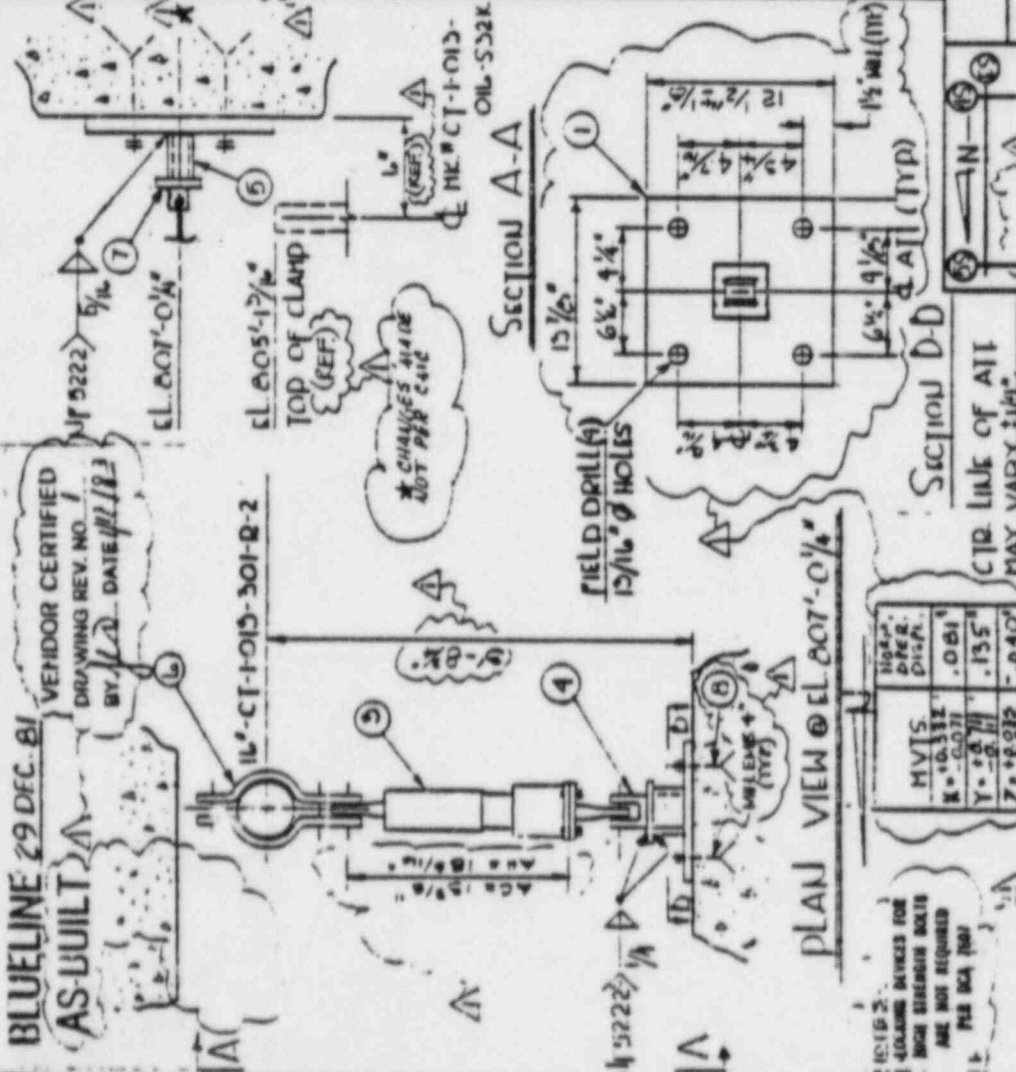
REF. DRAWING NUMBERS  
PIPE: 1810-114-011K1  
STEEL: 100-114-011K2

DESCRIPTION  
ELECTRICAL CONDUIT  
HV.A.C. CONDENSER

CUSTOMER: Texas Electric Service, Inc.  
ORDER OR CONT. NO.: CT-0846  
JOB NAME: \_\_\_\_\_  
MARK NO.: \_\_\_\_\_  
SKETCH NO.: \_\_\_\_\_

BLUELINE 29 DEC. 81  
AS-BUILT

VENDOR CERTIFIED  
DRAWING REV. NO. 1  
BY LD DATE 12/18/81



NOTE: 2. LOADING DEVICES FOR SHORE STRENGTH ARE NOT REQUIRED PER BIA 100

MVTs	R = 0.332	Y = 0.111	Z = 0.012
	R = 0.071	Y = 0.023	Z = 0.003
	R = 0.155	Y = 0.050	Z = 0.010

BRIB-180-CT-1-58-B R.1  
D.R.P. 180-CT-1-50-D-D5  
Data Point 30/PROD KE-1-37-R.0  
Pipe Mat'l. SA-250-CL-1IP-304  
Insul. Bldg. 5-D

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP
1	PCS PER SECTION D-D		
2	SA-250-CL-1IP-304		
3	SA-250-CL-1IP-304		
4	SA-250-CL-1IP-304		
5	SA-250-CL-1IP-304		
6	SA-250-CL-1IP-304		
7	SA-250-CL-1IP-304		
8	SA-250-CL-1IP-304		
9	SA-250-CL-1IP-304		
10	SA-250-CL-1IP-304		
11	SA-250-CL-1IP-304		
12	SA-250-CL-1IP-304		
13	SA-250-CL-1IP-304		
14	SA-250-CL-1IP-304		
15	SA-250-CL-1IP-304		
16	SA-250-CL-1IP-304		
17	SA-250-CL-1IP-304		
18	SA-250-CL-1IP-304		
19	SA-250-CL-1IP-304		
20	SA-250-CL-1IP-304		
21	SA-250-CL-1IP-304		
22	SA-250-CL-1IP-304		
23	SA-250-CL-1IP-304		
24	SA-250-CL-1IP-304		
25	SA-250-CL-1IP-304		
26	SA-250-CL-1IP-304		
27	SA-250-CL-1IP-304		
28	SA-250-CL-1IP-304		
29	SA-250-CL-1IP-304		
30	SA-250-CL-1IP-304		
31	SA-250-CL-1IP-304		
32	SA-250-CL-1IP-304		
33	SA-250-CL-1IP-304		
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43	SA-250-CL-1IP-304		
44	SA-250-CL-1IP-304		
45	SA-250-CL-1IP-304		
46	SA-250-CL-1IP-304		
47	SA-250-CL-1IP-304		
48	SA-250-CL-1IP-304		
49	SA-250-CL-1IP-304		
50	SA-250-CL-1IP-304		



MARK CT-1-013-522K  
PAINT: CARBO ZINC #11

FOR MATERIALS AND OPERATIONS SEE SKETCH NO.		SHEET OF	
CONDITIONS	Fx	Fy	Fz
DESIGN			
NORMAL & EMERGENCY			
FAULTED			
REF. DRAWING NUMBERS	D9		
PIPE: 180-CT-1-58-B R.1	ELECTRICAL		
STEEL: SA-250-CL-1IP-304	NV.A.C.F.I.P.304		
DESCRIPTION			
SPECIFIC FOR CONIST, DEF			
MARK NO. CT-1-013-522K			
CUSTOMER: Teasor Utilities Service, Inc.			
ORDER OR CONT. NO. CP-0046			
JOB NAME: Comanche Peak 1B			
MARK NO. CT-1-013-522K			
SKETCH NO.			
SHEET 1 OF 1 REV 1			

FOR OFFICE AND

TO 180Z

**INFORMATION COPY**

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CONTACT DISTRICT CONTROL FOR CURRENT  
PROJECT AND DESIGN.

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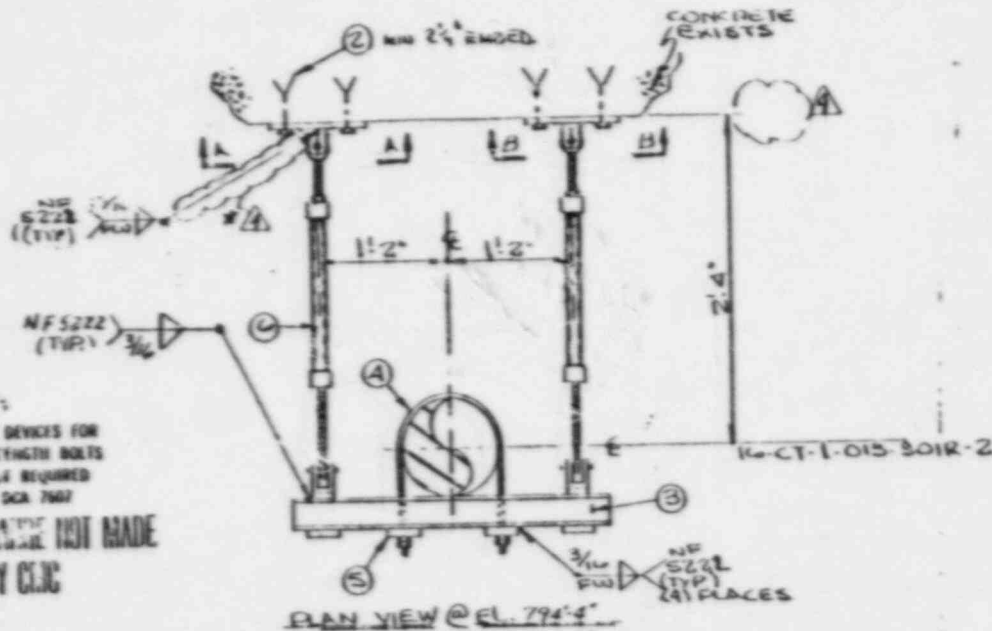
LINE 11-11-80

**BUILT**

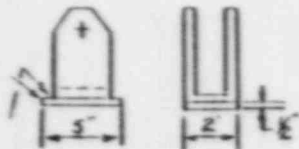
FOR CERTIFIED

REV. NO. 4

DATE 3/23/83



USE THE FOLLOWING DEVICES FOR  
STRENGTH BOLTS  
IF NOT REQUIRED  
PER DCA 7007  
CREATING TEXT MADE  
BY CJC



DETAIL 1  
T104802

MARK NO. CT-1-013-014-532R  
REV. NO. CT-1-013-014-532R  
DATE 3/23/83  
Pipe Mat'l. SA 350 CL 1 TP 204

MOVEMENTS	
X	0.016 / 0.017
Y	0.016 / 0.017
Z	



THIRD PARTY INSPECTION  
CODE CLASS: ASME III - 3

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	L	CBS	PRIV	SEC	AISC
1	R 1" x 1/8" x 9 3/8" (SA-36)	1		X					
2	BSA-12-5/2 CONC ANCHORS	2				X	X		
3	C 4 x 5.4 x 3'-8 3/4" (SA-36) P.F. 1"	2				X	X		
4	FWS-160 STD U-BOLT (SA-36) L=14 1/2"	1				X	X		
5	RWP-07 (SA-36)	4				X	X		
6	SAS-06-BA SWAY STRUT C.C. 3 1/2"	2				X	X		
7	R 1/2" x 2" x 5" (SA-36) SEE RETAIL	4		X			X		
8	R 1" x 9/16" x 10 3/8" (SA-36)	1		X			X		

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	3/23/83	CJC			REVISED VENDOR CERTIFICATION

MARK # CT-1-013-014-532R  
PAINT: CARBO ZINC #11

Approved By: CEC  
Date: 6-20-83

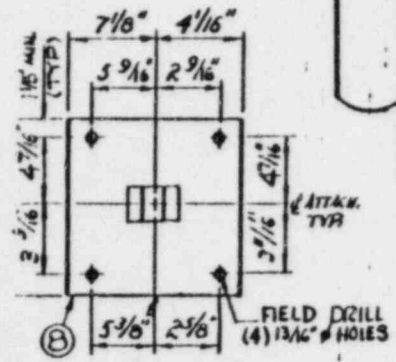
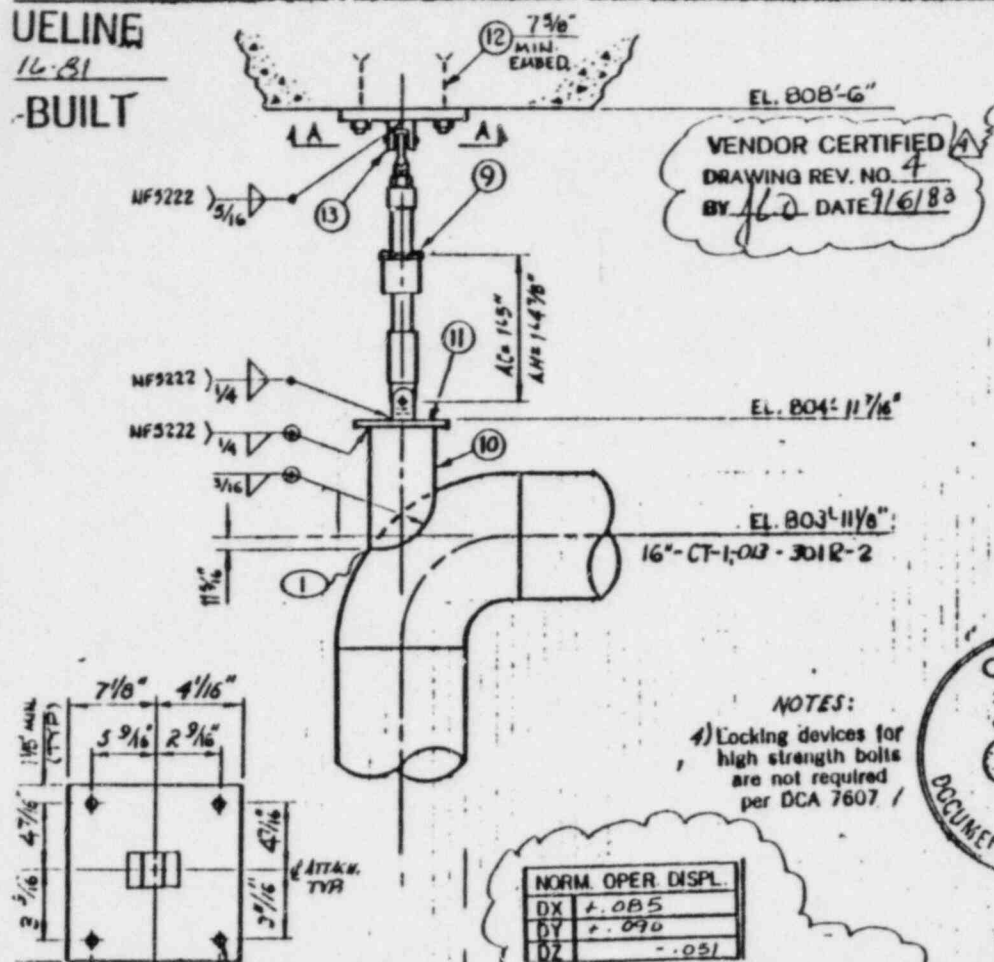
FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

Brown & Root, Inc.		CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
REF. DRAWING NUMBERS		DESIGN						
PIPE: M1 0602 REV SELECT: 01 05 9		NORMAL & VIBET						
STEEL: 1 0602 REV 12 HV.A.C. 25 21		EMERGENCY						
		FAULTED						

REV	DATE	OWN	CHK	APP	DESCRIPTION	CUSTOMER
1	11-11-80	CJC			SSDE FOR CONST, REF FIELD BONDING	Texas Utilities Service, Inc.
2	11-11-80	CJC			REV AS NOTED. REF CMC 48246	ORDER OR CONF ID: CP-0046
3	11-11-80	CJC			DCA 807 (SEE NOTE 1) AS C-11	JOB NAME: CMC 11192
4	11-11-80	CJC			REV 1 1 26	MARK NO. CT-1-013-014-532R
						SKETCH NO.:
						SHEET 1 OF 2
						REV. 4

# FOR OFFICE AND ENGINEERING USE ONLY

UELINE  
16-81  
BUILT



**SECTION A-A**  
 BRHL Iso. CT-1-SB-00BR.1  
 I.P.D. Iso. CT-1-SB-B Rev 3  
 Data Point 1233/PROB. AB-1-32 R.O  
 Pipe Mat'l. SA358 TP304  
 Insul. ~ Bldg. SB  
 T.O. 4802

NORM. OPER. DISPL.	
DX	+ .085
DY	+ .090
DZ	- .051

M.V.T.S.	
X	+ .342
Y	+ .46
Z	+ .074
	+ .22



THIRD PARTY INSPECTION  
 CODE CLASS: ASME III-2

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	CS	PRIM	SEC	AISC
8	CS PLATE, 7/8" THK, PER SECT A-A (SA36/SA516GR60)	1						
9	SMA-3-SO SNUBBER L=1'-7 3/16"	1						
10	8" SCH. 40S PIPE STANCHION H.W.B.B. L=1'-8 1/2" (CAST TP304)	1						
11	CS PLATE, 3/4" x 12" x 12" (SA36/SA516GR60)	1						
12	3/4" x 10" HILTI-KWIK CONC. ANCHORS	4						
13	HRS-10 DEAR BRACKET (AGRD/SA36)	2						

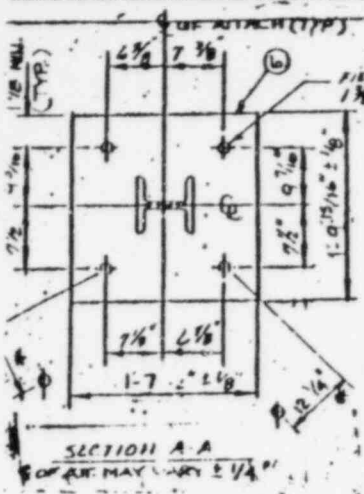
# FOR OFFICE AND ENGINEERING USE ONLY

REV	DATE	OWN	CNA	APP	DESCRIPTION
1	9/6/80	Q	[signature]	[signature]	VENDOR CERTIFICATION LETTER # 62726

FOR MATERIALS AND OPERATIONS SEE SKETCH NO.		SHEET OF					
CONDITIONS	Fx	Fy	Fz	Mx	My	Mz	
DESIGN							
NORMAL & UPSET		2156					
EMERGENCY		3392					
FAULTED							

REV	DATE	OWN	CNA	APP	DESCRIPTION	CUSTOMER Texas Utilities Service, Inc.	
1	9/6/80	Q	[signature]	[signature]	ISSUE FOR CONST. R.O. TITR.1	ORDER OR CONT. NO.	CP-0046
2	9/6/80	Q	[signature]	[signature]	REV'D AS NOTED REF. FAHS. MK # WAS CT-1-013-013-532K	JOB NAME	Comanche Peak 1 & 2
3	9/6/80	Q	[signature]	[signature]	REV'D AS NOTED REF. MK # WAS CT-1-001-013-532K	MARK NO	CT-1-013-013-532K
4	9/6/80	Q	[signature]	[signature]	REV'D AS NOTED REF. MK # WAS DCA 7607 SEE NR 4 AS BUILT	SKETCH NO.	
						SHEET 1 OF 1	REV. 4

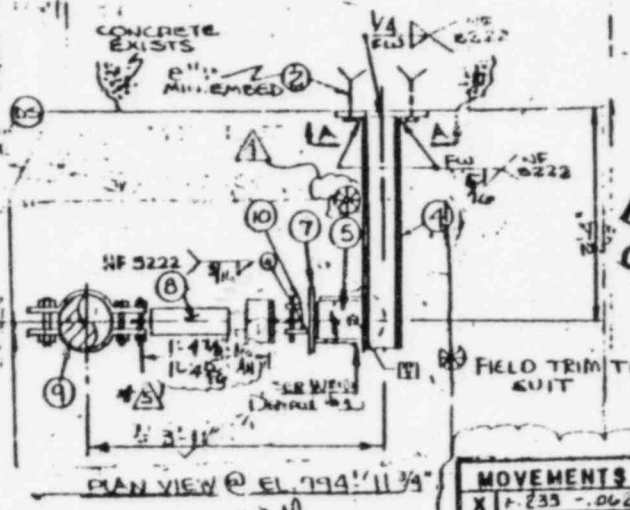
FOR OFFICE AND



**BLUELINE 27 JULY 81**  
**AS-BUILT** VENDOR CERTIFIED  
 DRAWING REV. NO. 5  
 BY JLD DATE 11/18/81

NOTE:  
 4) Locking devices for high strength bolts are not required per DCA 7607

MULTI VIOLATION: 1 1/2 HRS EXIST. PER MK# CT-1-013-007-522K



MOVEMENTS	
X	+ .235 - .062
Y	+ .281 - .049
Z	+ .003 - .015
NORM. OPER. DISPL.	
DX	.071
DY	.056
DZ	-.008

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	J	CSS	PRIM	SEC	AISC
2	1 1/4" X 12" MULTI KWIK CONC. ANCHORS (1144)	4							
4	W BOLT (SA-36) 2" L <sup>1/2</sup> LONG	1							
5	W X 12 (SA-36) 0" L <sup>1/2</sup> LONG SEE DET #1								
6	1" C.S. R. Per. Sec. A-A (SA-515 Gr. 65 or SA-36)								
7	1/2" X 8" X 0" B.L.G. C.S. TE (SA-36 or SA-515 Gr. 65)								
8	SMF-3-SO SHUBBER C.C. 1" L <sup>1/2</sup> L=2"								
9	SFC-10-160 PIPE CLAMP (SA-36)								
10	XRB-10 RIBB BRACKET (AL6B-D/SAB6)								

SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG  
 MARK # CT-1-013-012-532K

Apply one coat of Corbo-Bond #11 to above mat #1 except thro's which shall be coated w/ rust preventative.



REV	DATE	OWN	CHK	APP	DESCRIPTION
1	7/28	TE	TE	(Signature)	REV'D AS NOTED REF. CMC L5E14
2	11/18	Q	RA	(Signature)	REV'D PER 7607 TO CLEAR "AS-BUILT" VENDOR CERTIFICATION. REF. DCA 7607

Approved By: C.E.C.  
 Date: 6-20-79

FOR MATERIALS AND OPERATIONS SEE SKETCH NO.		SHEET OF		
Brown & Root, Inc.		CONDITIONS	Fx	Fy
REF. DRAWING NUMBERS		DESIGN	Mx	My
PIPE: 1" M.D. 10" O.C. REV. 19 ELECT. 51. REV. 5		NORMAL & UPSET	Mz	
STEEL: S1-0100Z REV. 12 H.V.A.C. REV. 7		EMERGENCY		
REV. DATE		FAULTED		
DESCRIPTION		CUSTOMER: Twp. Utilities Service, Inc.		
ISSUE FOR CONST. BASE PLATE ONLY REVISED AS NOTED PER ITT DWG		ORDER OR COMP. NO. CP-0046		
REV'D AS NOTED FOR EARTHQ. 1		JOB NAME: Cap-moche Peak I & 2		
REV'D AS NOTED FOR EARTHQ. 1		MARK NO. CT-1-013-012-532K		
		SKETCH NO.		
		SHEET OF 1 REV. 5		

NOT CHANGED BY CMC

TQ480Z

BRHL 150. CT-1-5B-008 REV. 1  
 BRHL 110. CT-1-5B-B REV. 3  
 Data Point 53/PROB# AB-1-32 Rev. 0  
 Pipe Mat'l. SA 350. Q. I. TP 204  
 Insul. Bldg. S.B.

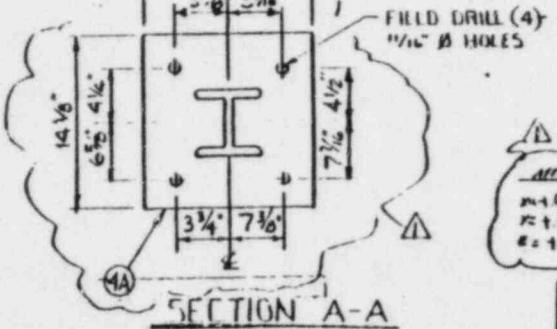
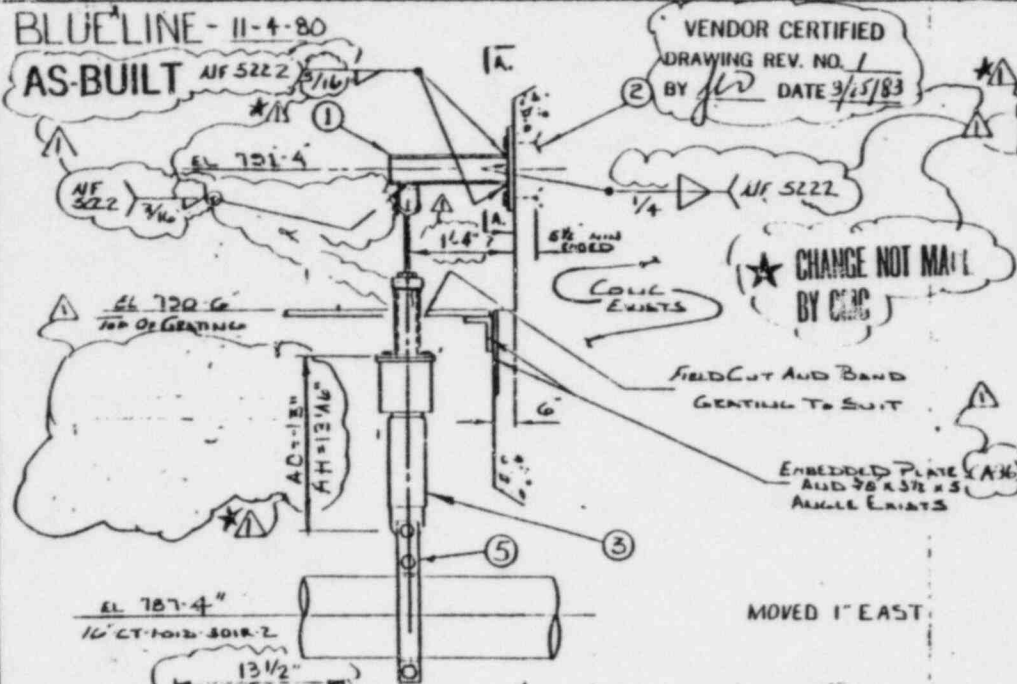


THIRD PARTY INSPECTION  
 CODE CLASS: ASME III-2

**FINAL COPY**  
 A DOCUMENT IS FOR INFORMATION ONLY  
 CONTACT PROJECT CONTROL FOR CURRENT  
 STATUS AND REVISION.

**FOR ENGINEERING  
 OFFICE USE ONLY**

**FOR OFFICE AND  
 ENGINEERING USE ONLY**



BRHL Iso. CT-1-SB-008, R1  
 BRP Iso. CT-1-SB-8 R1/3  
 Data Point: 246 / 11000 - AB-132 RD  
 Pipe Mat'l: SA 358 CL. 1, TB 205  
 Insul. - Bldg. SB

NOTE  
 M+0.03, -0.04  
 X+0.050, -0.243  
 Z+1.042, -1.96  
 TO.4802



**NORM. OPER DISPL.**

DX	+0.003"
DY	-0.057"
DZ	-0.048"

NOTES  
 LOCKING DEVICES FOR  
 HIGH STRENGTH BOLTS  
 ARE NOT REQUIRED  
 PER DCA 7602

THIRD PARTY INSPECTION YES  NO   
 CODE CLASS: ASME III-2

ITEM NO.	NO REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC. NO.	WT	PBS	L	CSB	PRIM	SEC	AISC
1	1	WAXIEXI-376"		SA36		17		X	X			
2	4	BSA58-B12	(BY FIELD)					X	X			
3	1	SMA-1 RD	SNUBBER			11		X	X			
4A	1	SHFT. K. 1000	TRANSITIONARY									
5	1	SPC DB-160	PIPE CLAMP	SA36		47		X				
1 PROVIDE TEMPORARY SPACER C=2A'56"							70					

SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG  
 MARK # CT-1-013-009-S22K

Apply one coat of Carbo Line #11 to above cat #1 except for the union shall be coated with rust preventative.

Approved By: C.E.L.  
 Date: 4-20-79

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

Brown & Root, Inc.

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN						
NORMAL & UPSET		329				
EMERGENCY		499				
FAULTED						

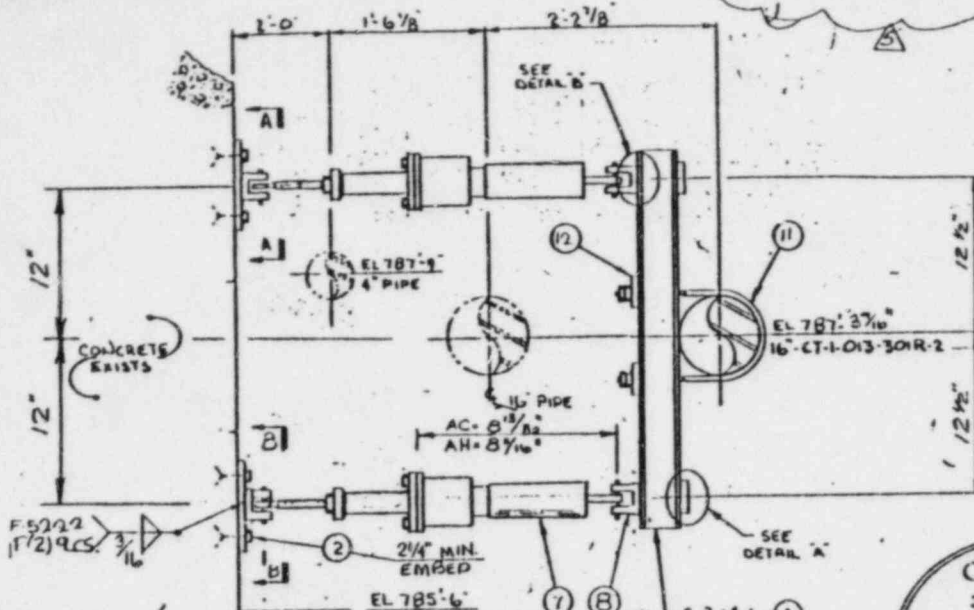
REV	DATE	OWN	CHK	APP	DESCRIPTION	CUSTOMER
1	11-4-80	M	JLD	JLD	ISSUE FOR CONST. REF. (EIT)	Texas Industrial Service, Inc.
2	05-25-83	V	JLD	JLD	REV AS NOTED REF. CH. 59159R-2	ORDER OR CONT. NO. CP-0046
3	03-11-83	V	JLD	JLD	REV AS NOTED REF. CH. 59159R-2	JOB NAME Coxar: the Peak 1 & 2
4	03-11-83	V	JLD	JLD	REV AS NOTED REF. CH. 59159R-2	MARK NO. CT-1-013-009-S22K
5	03-11-83	V	JLD	JLD	REV AS NOTED REF. CH. 59159R-2	SKETCH NO.
6	03-11-83	V	JLD	JLD	REV AS NOTED REF. CH. 59159R-2	SHEET 1 OF 1 REV. 1



BLUE LINE - 9 SEPT. 81

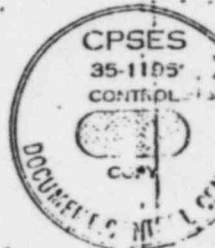
AS-BUILT

VENDOR CERTIFIED  
DRAWING REV. NO. 5  
BY BU DATE 3-15-84



ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	J	CSS	PRIM	SEC
	SEISMIC MECHANICAL SHOCK SUPPRESSOR CONSISTING OF:	ONE						
	MATERIALS EXISTS							
1	3/8" x 8" Carbon Steel (SA 515 GR 65 or SA 36) Plate 0' 8" Long, TW-14#	2		X				
2	1/2" x 5 1/2" Hilti Kwik Concrete Anchors (11141)	8						
3	1/2" x 1/2" Stroke, Flg. 307N Mechanical Shock Suppressor, W-113 3/4" Cold Setting, 1 1/4" Hot Setting, 1/4" H/Additional Rear Bracket, Load=2.1 Ordered in Pair	2						
4	C3x4-1 (SA-36) 2'-5" Long TW-18#	1						
5	7/8" Flg. 60N Washer Plate	1						
6	7/8"x16" Flg. 137N U Bolt, D=1" x 1 1/2", Developed Length=4' 5 3/4"	1						
7	EMA 1/2" CO GRABBER	2						
8	XRB-06 REAR BRACKET (AW50/6436)	4						
	SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG	1						
	MARK # CT-1-013-007-S22K	1						
9	1/2" CS R PER SECT 'A-A' (SA 36) SA 515 GR 65	1		X				
10	1/2" CS R PER SECT 'B-B' (SA 36) SA 515 GR 65	1			X			
11	FLG. 110 U BOLT, B=1 1/4" (SA 36)	1						
12	FLG. 60N WASHER PL.	4						
	Apply one coat of Carbo Zinc #11 to above mat'l except th'ds which shall be coated 1/2 mil protective.							
	ASME NAMEPLATE	1						
14	1/2" THK. TR 2"x2" (SA 36)	2						

FOR OFFICE AND ENGINEERING USE ONLY



MOVEMENTS

X	+ .019
Y	+ .041
Z	+ .043
DX	+ .016
DY	- .047
DZ	- .050

T.O. 4802



THIRD PARTY INSPECTION YES  NO   
CODE CLASS: ASME III-2

REV	DATE	OWN	CHK	APP	DESCRIPTION
8-17-83	83	RC	WJ	WJ	REV'D AS-BUILT VENDOR CERTIFIED
7-15-84	84	RC	WJ	WJ	REV'D VENDOR CERT., W/ENG-47275

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN						
NORMAL & UPSET					±711	
EMERGENCY					±213	
FAULTED						

REV	DATE	OWN	CHK	APP	DESCRIPTION	CUSTOMER
5-17-83	83	RC	WJ	WJ	ISSUED FOR CONST. BASE PLAT & CRIP	Texas Utilition Service
7-15-84	84	RC	WJ	WJ	REV'D AS-BUILT VENDOR CERTIFIED	ORDER OR CONT. NO. CP-0046
7-15-84	84	RC	WJ	WJ	REV'D AS-BUILT VENDOR CERTIFIED	JOB NAME Conanche Peak 1 & 2
7-15-84	84	RC	WJ	WJ	REV'D AS-BUILT VENDOR CERTIFIED	MARKING NO. CT-1-013-007-S22K
7-15-84	84	RC	WJ	WJ	REV'D AS-BUILT VENDOR CERTIFIED	SKETCH NO.
7-15-84	84	RC	WJ	WJ	REV'D AS-BUILT VENDOR CERTIFIED	SHEET 1 OF 2 REV. 1

NOTE  
14) LOCKING DEVICES FOR HIGH STRENGTH BOLTS ARE NOT REQUIRED PER DCA 7607

BRHL Iss. CF-1-08-000/R.1  
B.R.P. Iso. CT-1-58-8 REV. 3  
Data Point 44/PR28 = 28-1-32/R.O. 1  
Pipe Mat'l. SA 36 CL 1, TP 304  
Insul. Bldg. 58

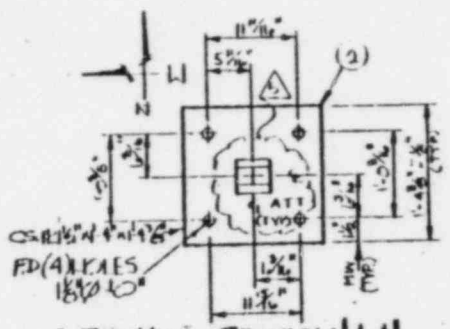
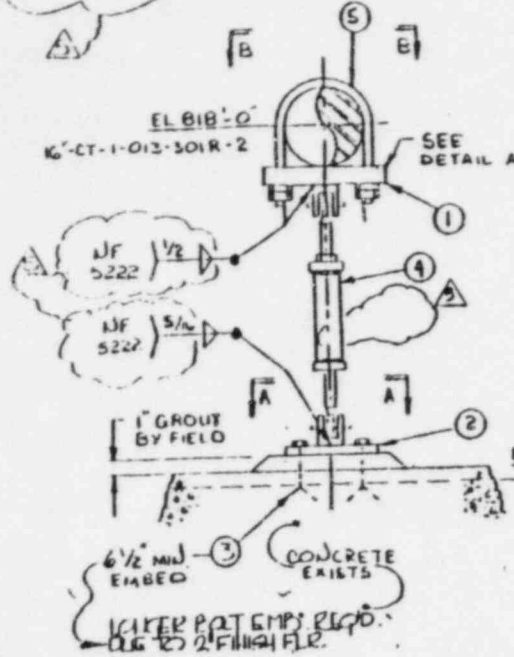
FIF/AN

FOR OFFICE AND

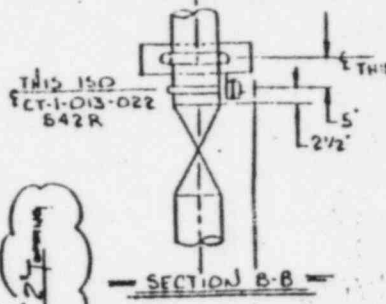
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# FOR OFFICE AND ENGINEERING USE ONLY

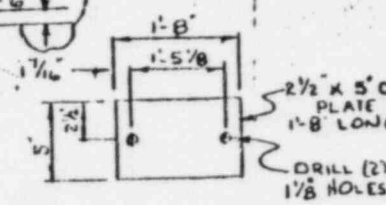
BLUELINE 12-B-30  
 VENDOR CERTIFIED  
 DRAWING REV. NO. 5  
 BY *[Signature]* DATE 12/1/83  
 AS-BUILT



PLAN VIEW SECTION 'A-A'



SECTION B-B



DETAIL A

NOTES:  
 BY ISSUE OF REV. 4 OF THIS DRAWING, THE FOLLOWING DOCUMENTS ARE VOIDED:  
 CMC 0964 RO

NOTES CONT.  
 Locking devices for high strength bolts are not required per DCA 7607

1. P. D. ISO. CT-1-SB-B Rev 5  
 Data Point: 100.100.100.100  
 Pipe No: 54358-CL 17304  
 Insl. Bldg. SB

To # 480

SEE BRN FOR HGR LOCATION

LOCATION PLAN

THIRD PARTY INSPECTION  
 CODE CLASS: ASME III-2

REV NO	DATE	BY	APP	DESCRIPTION
1	12/1/83	[Signature]	[Signature]	ISSUED FOR CONST. 112
2	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1
3	12/1/83	[Signature]	[Signature]	REDESIGNED & REDRAWN - ADDED 2R TO HGR. PLATE PW 2R PER ITT REV 3
4	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1
5	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

REV	DATE	BY	APP	DESCRIPTION
1	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1
2	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1
3	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1
4	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1
5	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1

Brown & Root, Inc.

REF. DRAWING NUMBERS  
 PIPE: M-0612 Rev 13 ELECT: 10602 Rev 1  
 STEEL: 51-CR05 Rev 9 H.V.A.C. 0605 Rev 1

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN						
NORMAL & UPSET						
EMERGENCY						
FAULTED						

REV	DATE	BY	APP	DESCRIPTION
1	12/1/83	[Signature]	[Signature]	ISSUED FOR CONST. 112
2	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1
3	12/1/83	[Signature]	[Signature]	REDESIGNED & REDRAWN - ADDED 2R TO HGR. PLATE PW 2R PER ITT REV 3
4	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1
5	12/1/83	[Signature]	[Signature]	REVISED PER CMC FILE AND ITT REV 1

CUSTOMER: ...  
 ORDER OR CONT NO. ...  
 JOB NAME: ...  
 MARK NO. CT-1-013-001-542R  
 SKETCH NO. ...  
 SHEET 1 OF 1 REV 5



**AS-BUILT**

**NOTES:**  
 1) Locking devices for high strength bolts are not required per DCA 7607

ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	P.B.S.	CS	PRIM	SEC.	AISC
1	1	SRS-08-PC SWAY STRUT					
		SPC-08-060 PIPE CLAMP					
2	1	SRS-03-PC SWAY STRUT					
		SPC-08-060 PIPE CLAMP					
4A	1	1" THK PL. PER SECT E (SA-36/SA515GR65)	X				
B	1	T.S. 1/4" X 4" X 4" X 4" 1 1/2" LG. (A-500 GR.B)		X	X		
10	1	CSR 1" THK PER SECT C-C SA-36 OR SA-515GR65	X			X	
11	2	5/8" X 8 1/2" HILTI KWIK CONCRETE ANCHORS			X		
12	4	1" X 12" SUPER HILTI CONCRETE ANCHORS			X		

APPLY ONE COAT OF CADZIN #11 TO ABOVE MAT'L EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE

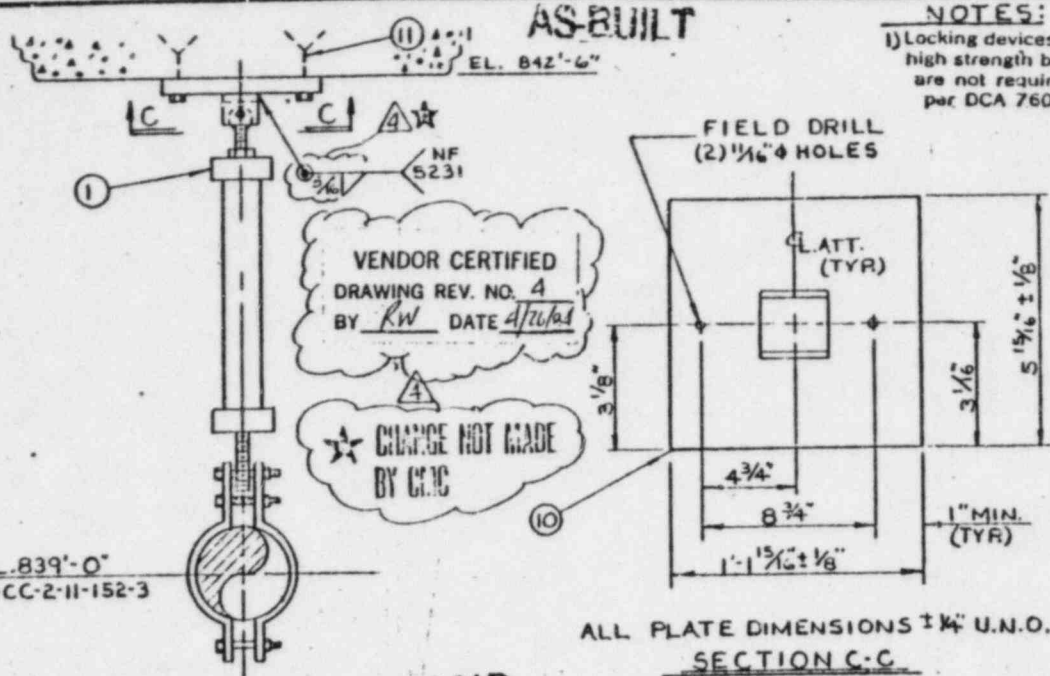
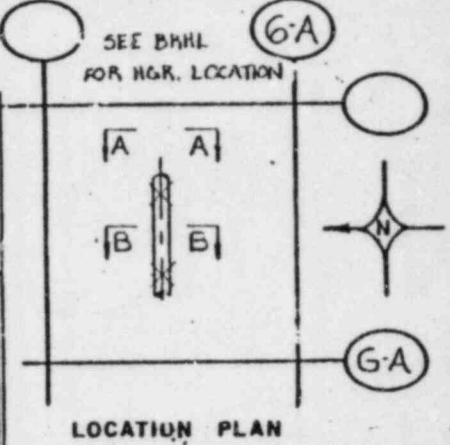
NO.	DESCRIPTION	DATE	CHKD.	CHAD.	APP'D.
1	VENDOR CERTIFICATION, REF. 57790	11/28/74	VM	RF	RF
2	REV VENDOR CERTIFICATION 9269	1/2/75	VM	RF	RF
3	REV VENDOR CERT.	4/23/75	VM	RF	RF

ASME CODE EDITION: 1974  
 ADDENDA: WINTER  
 DESIGN SPEC: MS-46A

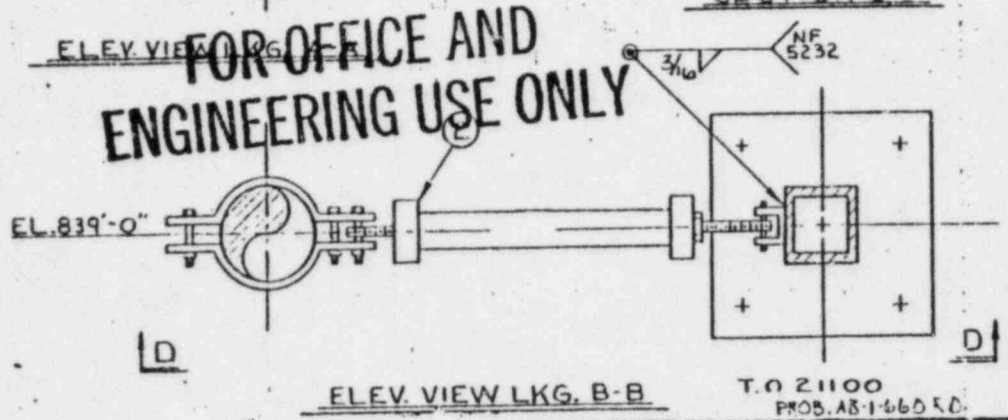
DATA PT.	SUPPORT	LOADS (Lbs)				PIPE MVTS (INCHES)
		A	B	C	D	
1088	DESIGN					
VERT.						0.025
N-S		-50	-901	-1058		
E-W		1103	1954	1111		0.017

DATA PT.	SUPPORT	LOADS (Lbs)				PIPE MVTS (INCHES)
		A	B	C	D	
2088	DESIGN					
VERT.						0.017
N-S		-1022	-1175	-2249		
E-W		-636	1552	741		0.011



ALL PLATE DIMENSIONS ± 1/4" U.N.O.  
 SECTION C-C



**FOR OFFICE AND ENGINEERING USE ONLY**

SEE LOAD LISTS

REV.	DESCRIPTION	DATE	DWN.	CHKD.	APP'D.
0	MECHANICAL				
1	ELECTRICAL				
2	STRUCTURAL				
3	MI-0755				

**Brown & Root, Inc.**  
 ENGINEERS AND CONTRACTORS  
 HOUSTON, TEXAS

CLIENT: T.U.S.I.  
 PLANT: COMANCHE PEAK  
 JOB NO. 2323

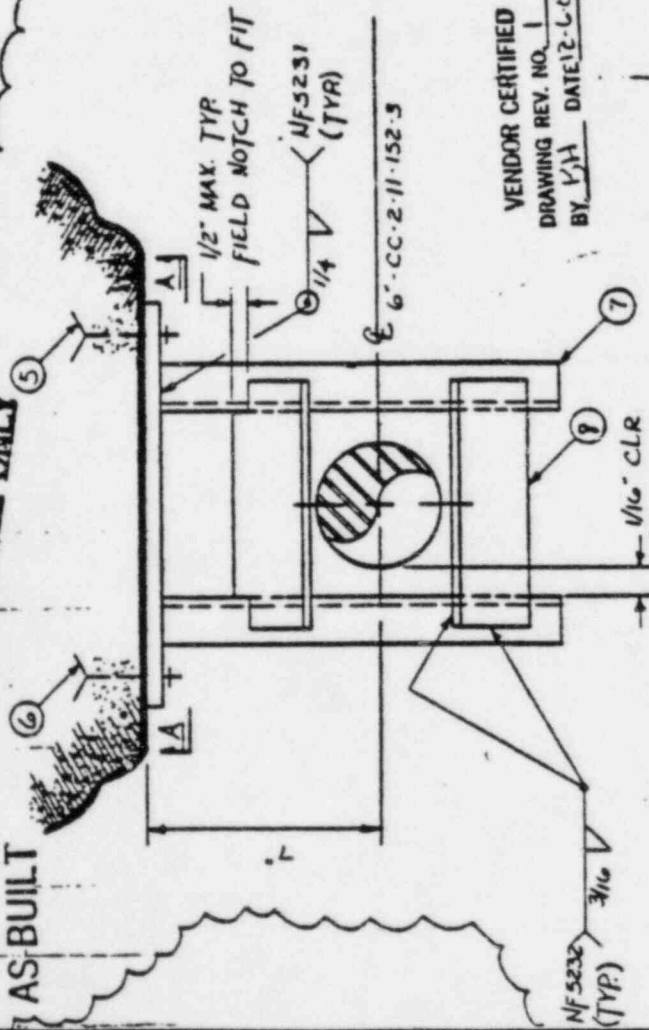
SUPPORT NO. CC-2-011-716-A53R  
 SHEET 1 OF 2 REV. 4

NOTE: AUTHORIZED NUCL. INSP. YES  NO   
 ASME CODE CLASS 3

**FOR OFFICE AND ENGINEERING USE ONLY**

FOR ENGINEERING  
OFFICE USE ONLY

AS BUILT



PLAN VIEW

① ELEV. 839'-9"

MVT'S	Y	10.028	-0.152
-------	---	--------	--------

NOTES:  
1) Locking devices for high strength bolts are not required per DA: A 7607

FIELD DRILL  
(4) 13/16" φ HOLES

VENDOR CERTIFIED  
DRAWING REV. NO. 1  
BY V.H. DATE 12-1-82

ITEM QTY NO. REQD.	MATERIAL	DESCRIPTION	2	3	4
1	5/8" THK CS PL	PER SECT. A-A (S.A.36)	X		
2	3/4" HT HILTI KWIK CONCRETE ANCHORS		X		
3	3/4" x 10" HILTI KWIK BOLTS		X		
4	1/4" x 3 1/2" x 1/4" LG. (S.A.36)		X		
5	1/4" x 3 1/2" x 1/2" LG. (S.A.36)		X		

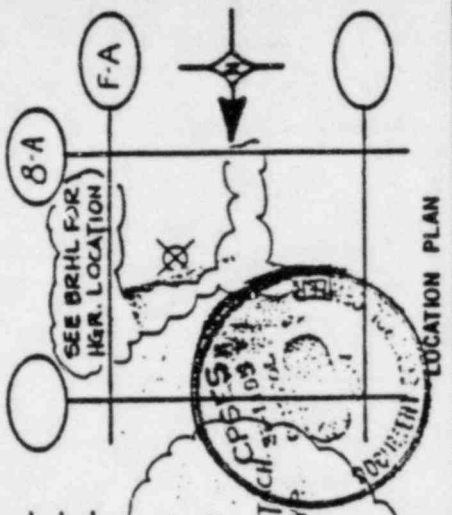
**INFORMATION COPY**

THIS DOCUMENT IS FOR INFORMATION ONLY. CONTACT BROWN & ROOT FOR ANY INFORMATION.

PAINT: CARBORING #11  
PROBLEM: PAB-1-66-REV-0

\* QTR. LINE OF ATT. MN VAR 1/8"

ASME CODE EDITION 1974  
ADDENDUM: WINTER  
DESIGN SPEC: MS-96A



LOCATION PLAN

SECTION A-A \*

DATE	REV	DESCRIPTION	DATE	CHKD.	APPRD.
12/1/82	1	REV'D AS NOTED PER CLK 6960E	12/1/82	RP	JFC
	2	REV'D AS NOTED PER CLK 7607 (ATTN) COMP ADMS	12/1/82	RP	JFC
	3	REV'D AS NOTED PER CLK 7607 (ATTN) COMP ADMS	12/1/82	RP	JFC
	4	REV'D AS NOTED PER CLK 7607 (ATTN) COMP ADMS	12/1/82	RP	JFC
	5	REV'D AS NOTED PER CLK 7607 (ATTN) COMP ADMS	12/1/82	RP	JFC

SUPPORT NO. CC-2-011-710-A53R  
SHEET 1 OF 1 REV. 1

CLIENT I.U.S.I.  
PLANT COMANCHE PEAK  
JOB NO. 2323

Brown & Root, Inc.  
HOUSTON, TEXAS



PIPE MVTB (INCHES) LIMITS  
DESIGN EXCL. C. 0  
VERT. 1/4" 1/2" 3/4" 1" 1 1/4" 1 3/4" 2" 2 1/2" 3" 3 1/2" 4" 4 1/2" 5" 5 1/2" 6" 6 1/2" 7" 7 1/2" 8" 8 1/2" 9" 9 1/2" 10" 10 1/2" 11" 11 1/2" 12" 12 1/2" 13" 13 1/2" 14" 14 1/2" 15" 15 1/2" 16" 16 1/2" 17" 17 1/2" 18" 18 1/2" 19" 19 1/2" 20" 20 1/2" 21" 21 1/2" 22" 22 1/2" 23" 23 1/2" 24" 24 1/2" 25" 25 1/2" 26" 26 1/2" 27" 27 1/2" 28" 28 1/2" 29" 29 1/2" 30" 30 1/2" 31" 31 1/2" 32" 32 1/2" 33" 33 1/2" 34" 34 1/2" 35" 35 1/2" 36" 36 1/2" 37" 37 1/2" 38" 38 1/2" 39" 39 1/2" 40" 40 1/2" 41" 41 1/2" 42" 42 1/2" 43" 43 1/2" 44" 44 1/2" 45" 45 1/2" 46" 46 1/2" 47" 47 1/2" 48" 48 1/2" 49" 49 1/2" 50" 50 1/2" 51" 51 1/2" 52" 52 1/2" 53" 53 1/2" 54" 54 1/2" 55" 55 1/2" 56" 56 1/2" 57" 57 1/2" 58" 58 1/2" 59" 59 1/2" 60" 60 1/2" 61" 61 1/2" 62" 62 1/2" 63" 63 1/2" 64" 64 1/2" 65" 65 1/2" 66" 66 1/2" 67" 67 1/2" 68" 68 1/2" 69" 69 1/2" 70" 70 1/2" 71" 71 1/2" 72" 72 1/2" 73" 73 1/2" 74" 74 1/2" 75" 75 1/2" 76" 76 1/2" 77" 77 1/2" 78" 78 1/2" 79" 79 1/2" 80" 80 1/2" 81" 81 1/2" 82" 82 1/2" 83" 83 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ITEM NO	QTY	RECD	MATERIAL	DESCRIPTION
1	1		PUM-360	
2	1		3/4" x 3/4" ANGLE SA-36	SEE DESIGN 1-A
3	1		1/2" x 3/4" ANGLE SA-36	SEE SECTION A-A
4	4		3/4" x 3/4" MULTI-KWIK CONCRETE ANCHOR	
5	4		3/4" x 3/4" MULTI-KWIK CONCRETE ANCHOR	
6	1		3/4" x 3/4" ANGLE 1-A-1-G	
34	1		3/4" x 3/4" C-5 PLATE 15/16" T.C. (S&S C.P. 5)	
35	1		1/2" x 3/4" ANGLE SA-36	
36	1		3/4" x 3/4" ANGLE SA-36	

REV	DESCRIPTION	DATE	CHKD	APPVD
1	REVISED PER CERTIFICATION	11-23-54		
2	REVISED PER CERTIFICATION	11-23-54		
3	REVISED PER CERTIFICATION	11-23-54		

ASME CODE EDITION: 1974  
 ADDENDA: 1/1/1978  
 DESIGN SPEC: MS-96A

PE. CERTIFICATION

FOR OFFICE AND ENGINEERING USE ONLY

FOR HGR LOCATION

8A

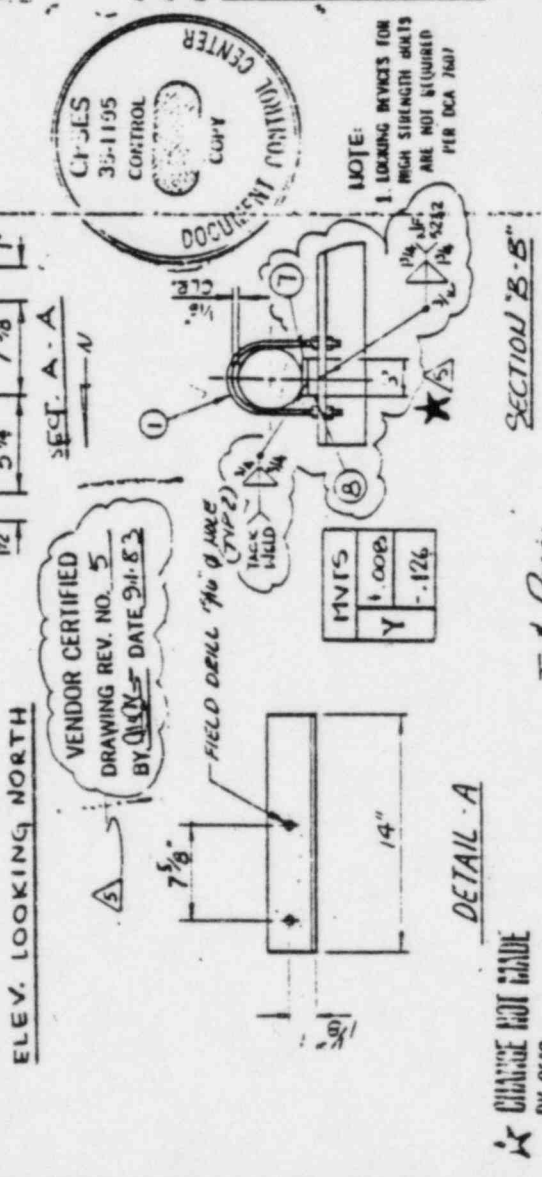
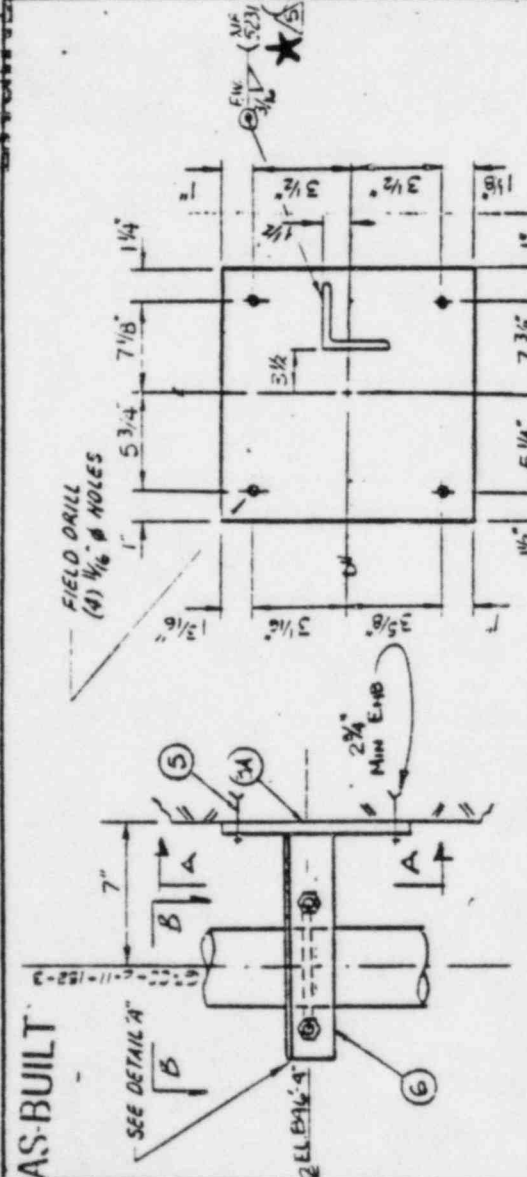
F.A.

LOCATION PLAN

PROB: # AB-1-66C REV O

REV	DESCRIPTION	DATE	CHKD	APPVD
1	REVISED PER CERTIFICATION	11-23-54		
2	REVISED PER CERTIFICATION	11-23-54		
3	REVISED PER CERTIFICATION	11-23-54		

SUPPORT NO. CC-2-11-709-1634  
 SHEET 1 OF 1 REV. 5



DATA PT	SUPPORT	LOADS	(LBS)	PIPE	STRESS ISO	REV	ELECTRICAL	REV	MECHANICAL	REV	CLIENT
210G	DESIGN	VERT	W-3	E-W	M2-3231-3G	8	EI-070	9	11-0762	4	T. U. S. I.
					DRILL ISO	4	H V A C	5	5-072	5	PLANT COMANCHIE
					CC-2-AB-052	1	M1-0756				JOB NO. 2323
											HOUSTON, TEXAS

AS-BUILT

CHANGE NOT MADE BY CHIC

FIELD DRILL #10 (TYPE 2) TACK WELD

NOTE: 1. LOCKING NUTS FOR HIGH STRENGTH BOLTS ARE NOT REQUIRED PER DCA 7601

CPSES 35-1195 CONTROL CENTER DOCUMENT CONTROL CENTER COPY

VENDOR CERTIFIED DRAWING REV. NO. 5 BY DATE 9-1-82

ELEV. LOOKING NORTH

SECTION B-B

DETAIL A

TO 2101

Brown & Root, Inc. ENGINEERING AND CONSTRUCTION HOUSTON, TEXAS

CPSES 35-1195

AS-BUILT

B.O.C. EL. 869'-4"

NF5232

EL. 865'-4"  
6" CC-2-1152-3

NOTES:


1 Locking devices for high strength bolts are not required per DCA 7607

ELEV. LKG. SOUTH

T.O. # 21101

DATA PT	SUPPORT	LOADS (lbs)	PIPE MVTB (INCHES)
DESIGN	WIND	LEVEL	LIMITS
2110			
VERT.		-1265	1185
N-S			
E-W			
NOTE	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>		
PK, E, JP, B, R, DN	ASME CODE CLASS 3		

STRESS ISO.	REV.	MECHANICAL	REV.	ELECTRICAL	REV.
MZ-3231-36	A	MI-0701	6	EI-0710-01	7
(BRILL) ISO.		STRUCTURAL		H.V.A.C.	
CC-2-AB-032	1	S-0735	2	MI-0758	4


**Brown & Root, Inc.**  
 ENGINEERS AND CONSTRUCTORS  
 HOUSTON, TEXAS

REV.	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
0	ISSUED FOR CONSTRUCTION	12/21/77			
1	REV'D. AS NOTED REF. CMG 19812	1/2/78			
2	DCA 7607 (SEE NF # 178-101)				

CLIENT T.U.S.I.  
 PLANT COMANCHE PEAK  
 JOB NO. 2323

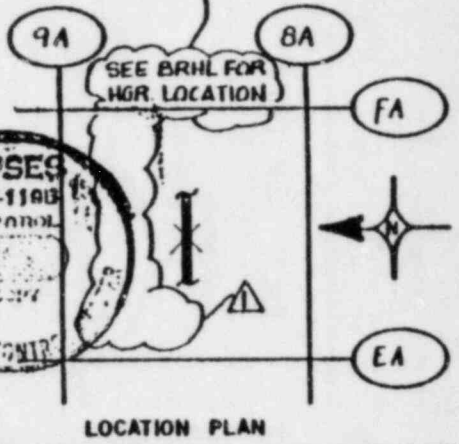
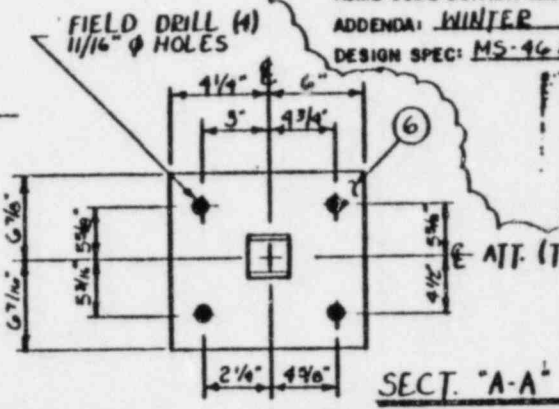
SUPPORT NO.	CC-2-011-705-A63R
SHEET	1 OF 1 REV. 1

MVTB	
X	0.006
	-0.019
Z	-0.009
	-0.012

VENDOR CERTIFIED  
DRAWING REV. NO. 1  
BY BH DATE 12-6-82

FOR ENGINEERING  
& OFFICE USE ONLY

ASME CODE EDITION 1974  
ADDENDA: WINTER  
DESIGN SPEC: MS-96A



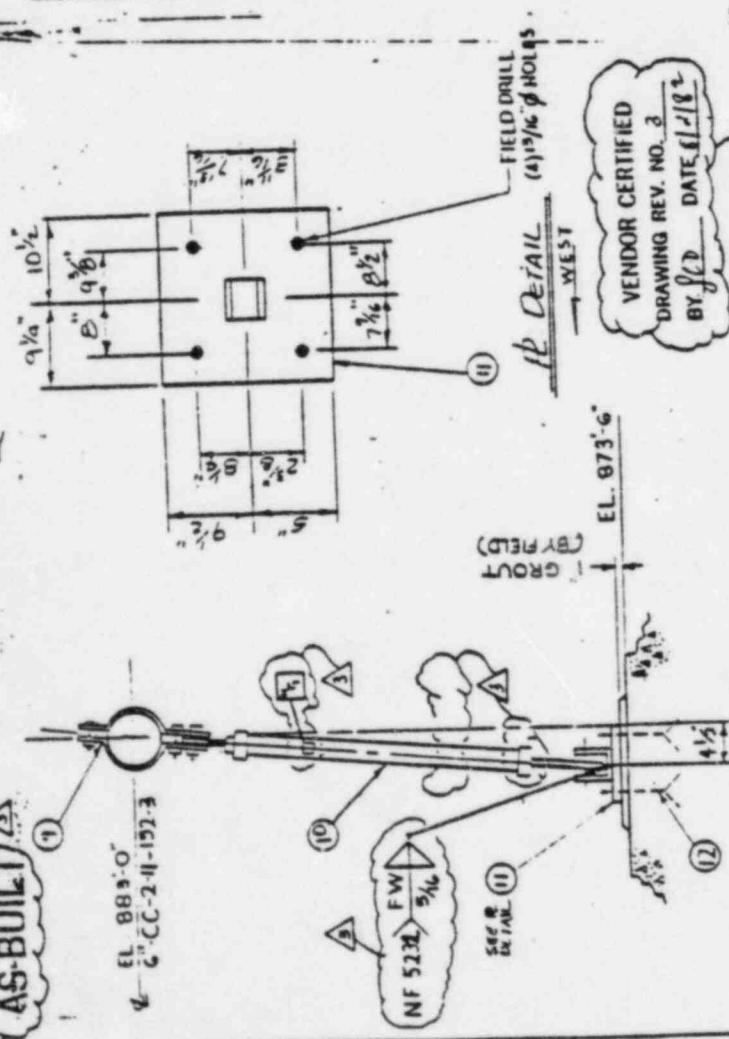
ITEM NO.	QTY. REQ'D.	MATERIAL DESCRIPTION	REV.	CHKD.	APPVD.
6	1	3/4" THK. CS PL. PER SECT. "A-A" (SA36/SA516GR65)			
7	4	5/8" x 8 1/2" HILTI KWIK ANCHOR BOLTS			
8	1	SPS-10-RD SWAY STRUT CC-2-16 3/4"			
9	1	SPC-10-060 PIPE CLAMP			

REV. DESCRIPTION DATE DWN. CHKD. APPVD.  
 VENDOR CERTIFICATION (QIN# 69792)

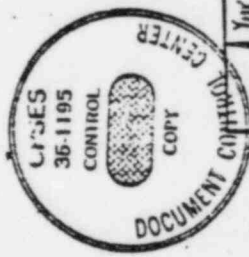
**INFORMATION**  
THIS DOCUMENT IS CONTACT DOCUMENT STATUS

FOR OFFICE AND  
ENGINEERING USE ONLY

**AS-BUILT**



ELEVATION LOOKING EAST



NOTE  
4) LOCKING DRIVETS FOR HIGH STRENGTH BOLTS ARE NOT REQUIRED PER DCA 2100

BRHL ISO. CC-2 AD-50-R1  
J.P.D. Inq. CC-2-AD-50-R1  
(Unit Point) LISZ AD-144-CD  
Pipe Mat'l. S1016-C-2-B  
Insnul. 1/2" B166-A  
To: 21000

ITEM NO.	MATERIALS & OPERATIONS	QUANTITY	SHIP
11	SEISMIC SWAY STRUT ASSEMBLY CONSISTING OF SMS (SWAY STRUT CLAMP) NO 5 PC-1-060	ONE	
10	SRS (SWAY STRUT) TYP PC, SIZE #14 GC DIA. = 100 9/16"	1	
11	1/2" THICK C-PLATE (SA-36 OR SA315 68.65) SEE DETAIL A	1	
12	3/4" Ø x 10' LONG. HILL KWINKI BOLT CONCRETE ANCHORS	4	
	56 NETL B-1 GRABBLE		
	SEISMIC ASSEMBLY SKETCH AND ENGINEERING BURDLE AND TAG MARK # CC-2-011-006-A73R		
	Apply Carbo-Zinc fill to above MAT'L except th'da which shall be treated with a TUBE preservative		

**FOR ENGINEERING & OFFICE USE ONLY**

REV	DATE	BY	CHK	APP	DESCRIPTION
1	~	~	~	~	REV'D AS BUILT REF. DRAWING
2	~	~	~	~	VENDOR CERTIFICATION
3	~	~	~	~	GTN# 53190

Approved By: C.F.C. Date: 4-23-19

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. 1	CONDITIONS	DESIGN	EMERGENCY	FAULTED
Brown & Root, Inc.	Fx	Fy	Fz	My
PIPE: 11" O.D. x 0.70" T.O. ELECT: 210V-3-Ø HV.A.C. 1400/155 E.S.				
STEEL: S-355 L-70				

**FOR OFFICE AND**

FOR OFFICE AND

CUSTOMER Texas Utilition Service, ORDER OR CONT. NO. CP-0018 JOB NAME Comanche Peak 1 & 2 MARK NO. CC-2-011-006-A73R SKETCH NO. SHEET 1 OF 1 REV. 5

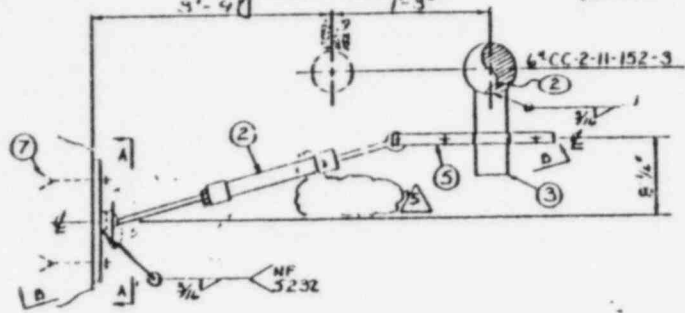
# FOR OFFICE AND ENGINEERING USE ONLY

**BLUELINE** \* CHANGE NOT PER. CAC

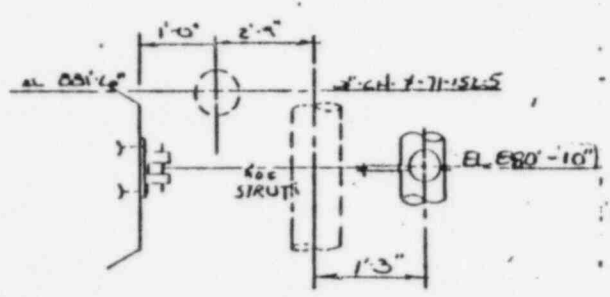
**AS-BUILT**

VENDOR CERTIFIED  
DRAWING REV. NO. 5  
BY *[Signature]* DATE 7/19/83

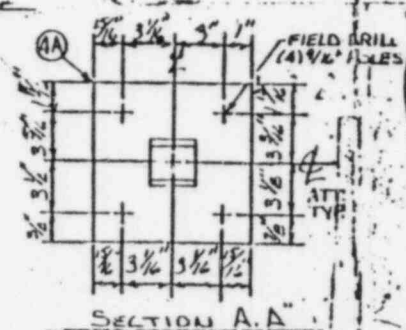
**NOTE:**  
1) Locking devices for high strength bolts are not required per DCA 7607



PLAN VIEW



SECTION B-B



SECTION A-A

SEE BRILL FOR HGR. LOCATION



THIRD PARTY INSPECTION YES  
CODE CLASS: ASME III-3

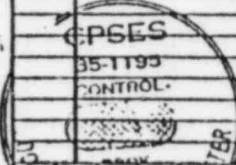
PARH ISO CC-2-AB-050 R.1  
I.P.D. Iso. CC-2-AB-50 R.O  
Data Point: 2131 AB+LLC R.O  
Pipe Mat'l: SA106C GR.B  
Insul: 1/2" EMP. A

ITEM NO.	NO REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC NO.	WT.	POS	L	CSS	PRIM	SEC	AIBC
1	1	ASA 12-512	Grass ANCHORS									
2	1	ERS DR RD	SWAY STRUT		07	20			X			
3	1	SAE 304 STAINLESS	PIPE CLAMP	SA 304	D	9			X	X		
4	1	ASA 12-512	Grass ANCHORS									
5	1	ERS DR RD	SWAY STRUT						X			
6	1	SAE 304 STAINLESS	PIPE CLAMP	SA 304	D	7			X	X		
7	1	ASA 12-512	Grass ANCHORS									

NO MAT'L BY GRINDER

SEISMIC ASSEMBLY SKETCH AND ENGINEERING  
BUNDLE AND TAG -  
MARK # CC-2-011-005-A73R

Apply Carso-Zinc fill to above mat'l except in as which shall be treated with a rust preventative



# FOR OFFICE AND ENGINEERING USE ONLY

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	7/19/83	BY	BY	BY	REV. AS NOTED REF. CAC 43587 DCA-7607 LEC NT-4 AS BUILT VENDOR CERTIFICATE; REF GTU #9770
2					REV. VENDOR CERT.

QUAN SHIP:

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. (SHEET OF

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz

REF. DRAWING NUMBERS  
PIPE: M-0103 ON P/O ELECT: M-0104 E.2  
STEEL: S-0135 E01Z HV.A.C.: M-0157 E.4

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	6-5-71	JW	BY	BY	ISSUE FOR CONST. FW 1-2
2	2-20-80	RY	BY	JW	REV. PER NPS1 REV CA
3	1-25-81	JC	BY	JW	REV. AS NOTED REF. CAC 3106 R1
4	11-26-81	BY	BY	JW	REV. AS NOTED REF. CAC 3357 R1 PHDP 1134 R.1

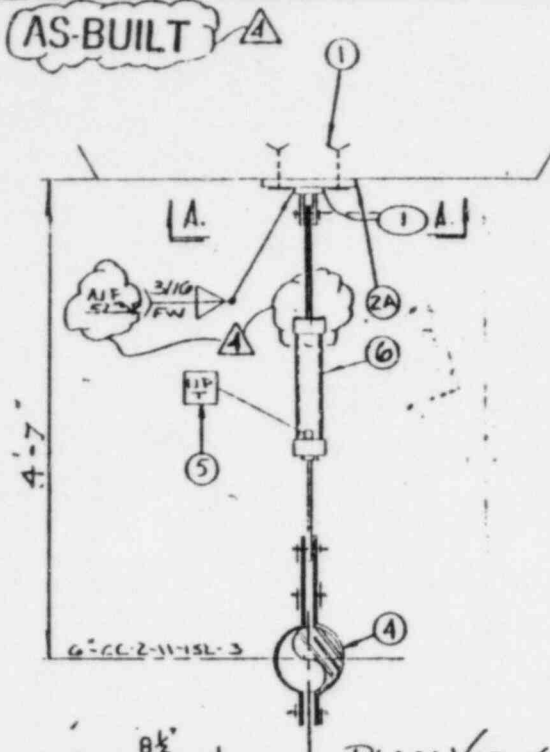
CUSTOMER Foxon Utilities Service, Inc  
ORDER OR CONT. NO. CP-0046  
JOB NAME Conanohe Peak 2 & 2  
MARK NO. CC-2-011-005-A73R  
SKETCH NO.  
SHEET 1 OF 1 REV. 5

TO: H 21101

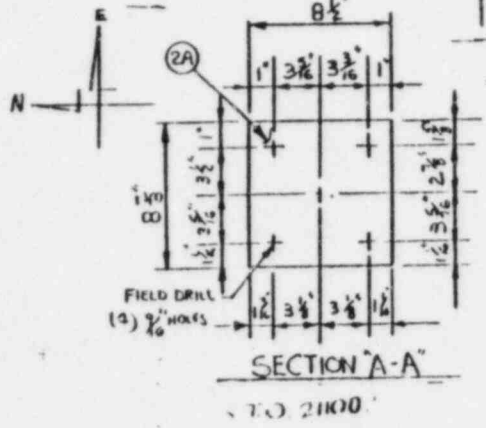
END SHEET



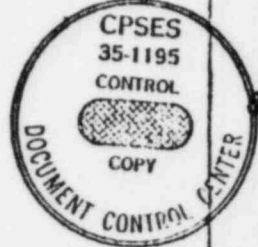
OTF CONT-  
CKING DEVICES FOR  
IN STRENGTH BOLTS  
ARE NOT REQUIRED  
PER DCA 7607



PLAN VIEW  
@ EL 877-10  
# NORTH #



VENDOR CERTIFIED  
DRAWING REV. NO. 4  
BY JCD DATE 2/11/82



BRHL ISO. CC-2-AD-50 REV. 1  
I.P.D. ISO. CC-2-RE-36-1.0  
Data Point 2129 / PAB16CRO  
Pipe Hat 1. SDR6 G.E.  
Insul. Y2. Rldg. A

SEE BRHL FOR IGR. LOCATION

THIRD PARTY INSPECTION YES  NO   
CODE CLASS: ASME III-3

ITEM NO.	NO REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC NO.	WT.	PBS	L	CSS	PRIM	SEC	AISC
1	4	BSA 12-512	CONC ANCHORS									
2	1	R 3/4 X 20		SA 306		7	X			X		
3	1	SWS 04-40	SWAY BRACE		670	20				X		
4	1	SFC 06-040	PIPE CLAMP	SA 306		19				X		
5	1	DWG 2078A	ASME III PLATE							X		
6	1	R 1/2 X 20 X 3/4	C.S. PLATE	SA 306						X		
		SWS-DL-RD	SWAY BRACE G.S. 3'-8"							X		

NO NOTED BY GRUNNELL

SEISMIC ASSEMBLY SKETCH AND ENGINEERING  
BUNDLE AND TAG  
MARK # CC-2-011-004-A73R

Apply Carbo-Zinc 211 to above  
mat'l except th'ds which shall  
be treated with a rust  
preventative

FOR ENGINEERING  
OFFICE USE ONLY

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CURRENT STATUS AND REVISIONS.

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	1-14-81	PJ	JP	[Signature]	REV. AS NOTED REF. DCA 7607 REV. NO. 4, SMC 76686 & PHHP 324 DELETED NT '31-3 (AS BUILT)
2		JR	PL	EFK	VENDOR CERTIFICATION REF. GIN # 59790

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. [A] SHEET OF [ ]

Brown & Root, Inc.  
ENGINEERING AND CONSTRUCTION

REF. DRAWING NUMBERS  
PIPE: MI-0705-01.R.D ELECT: 07-0704 R.3  
STEEL: S.C. 25 R.2 HV.A.C.: MI-0704 R.4

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN			-405			
NORMAL & UPSET			1478			
EMERGENCY			936			
FAULTED			1960			
			1011			
			11041			

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	6-5-79	JW	[Signature]	[Signature]	ISSUE FOR CONST FW 1
2	2-21-80	ED	[Signature]	[Signature]	REV. PER NIST REV. CA
3	4-26-80	RS	[Signature]	[Signature]	REV. AS NOTED REF. 00324

CUSTOMER: Texas Utilities Service, Inc.  
ORDER OR CONT. NO.: CP-0046  
JOB NAME: Comanche Peak 1 & 2  
MARK NO.: CC-2-011-004-A73R  
SKETCH NO.:  
SHEET 1 OF 1 REV. 4

FOR OFFICE AND  
ENGINEERING USE ONLY

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CONTACT DOCUMENT CONTROL FOR CURRENT  
STATUS AND REVISION.

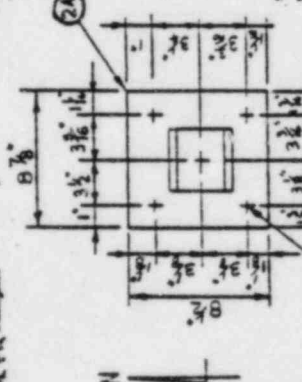
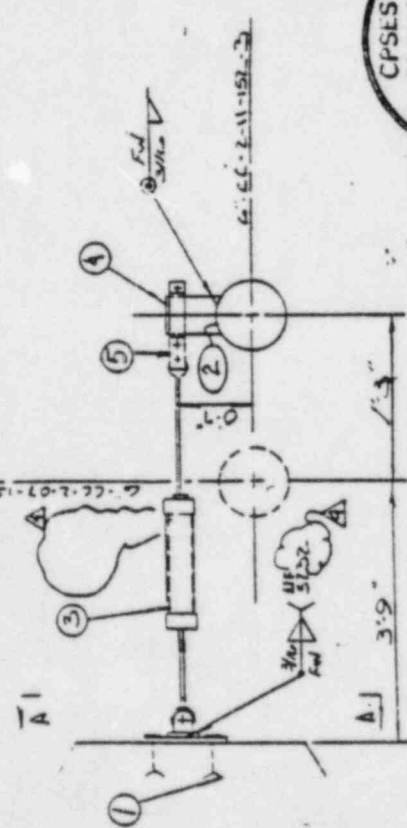
**AS-BUILT**

VENDOR CERTIFIED

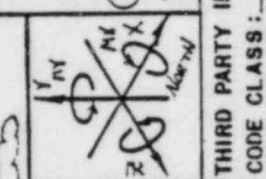
DRAWING REV. NO. 4

BY *RA* DATE 11/29/83

NOTE: COIL LOCKER DEVICES FOR HIGH STRENGTH BOLTS ARE NOT REQUIRED PER DCA 7607



SEE BRILL FOR IGR. LOC.



DRILL 180. CC-2-AB-50-R1  
I.P.D. 180. CC-2-AB-50-R1  
Job Point 113. APPROX. 16.746.00  
Site 1011. SAIDG 42.2

0.21100

THIRD PARTY INSPECTION  
CODE CLASS: ASME III.3

ITEM NO.	NO. REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC NO.	WT.	PAS	CS	PRIM	REC	AISC
1	1	PCA 12-512	1.0 IN. AN. 11 MS	SA 336							
2	1	PCA 12-512	C.S. PLATE	SA 336							
3	1	SWAY BRACKET	SWAY BRACKET	SA 336							
4	1	PIPE CLAMP	PIPE CLAMP	SA 336							
5	1	GENE III PLATE	GENE III PLATE	SA 336							
6	1	C.S. PLATE	C.S. PLATE	SA 336							

Approved By: GFC  
Date: 4-23-79

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. \_\_\_\_\_

CONDITIONS: DESIGN A, NORMAL UPSET, EMERGENCY 150%, FAULTED

REVISIONS:

REV.	DATE	BY	DESCRIPTION
1	11/29/83	RA	ISSUE FOR CONST.
2			REV PER NISI REV 04
3			REV'D AS NOTED IN 18010 20113

FOR ENGINEERING & OFFICE USE ONLY

QUAN. SHIP

CUSTOMER: Toston Utilities Baltimore, Md.

ORDER OR CONT. NO.: CP-0070

JOB NAME: Conchong 781112

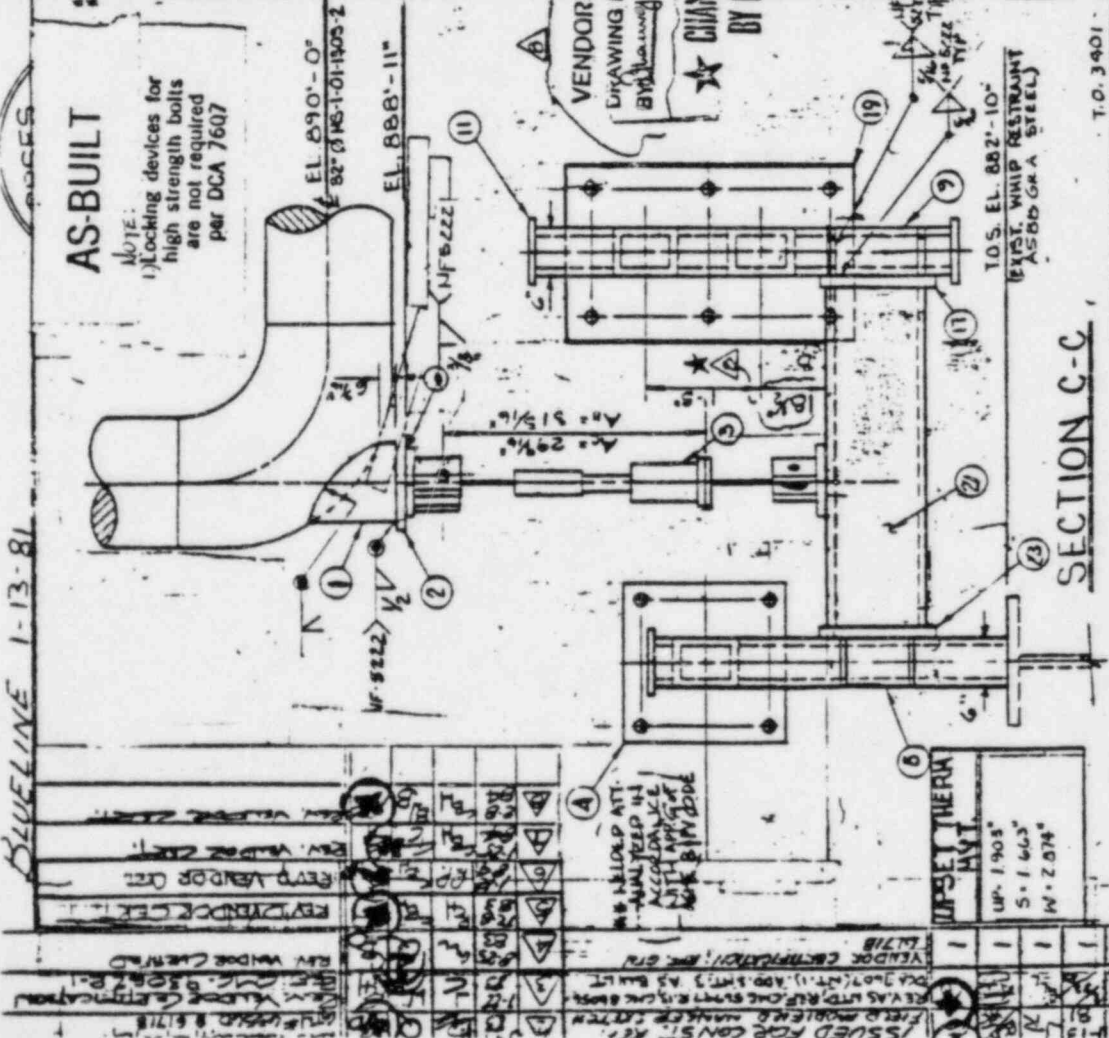
MARK NO.: CC-2-011-002-A13-R

SKETCH NO. \_\_\_\_\_

# FOR OFFICE AND

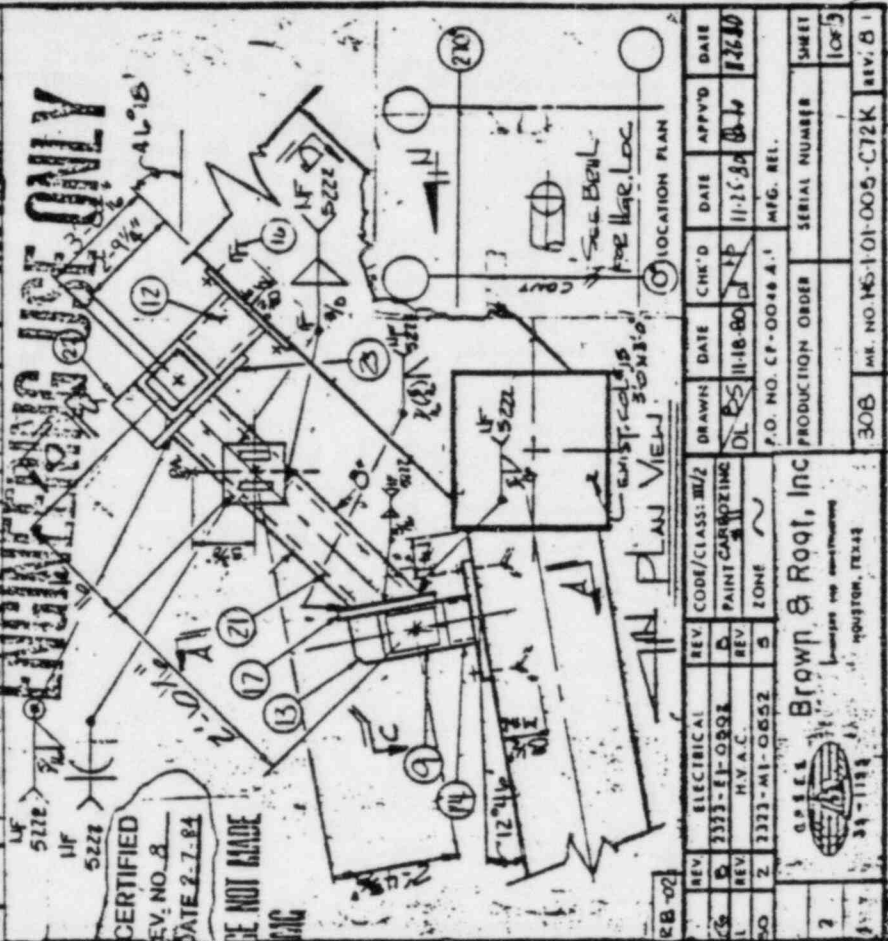
FOR OFFICE USE ONLY

BLUELINE 1-13-81



ITEM NO.	QTY	DESCRIPTION	WT.	ASME OR ASTM	MIC.
1	1	PR4 SCH 60		SA486B	
2	1	FP 1 1/2" X 2 1/2" X 2 1/2"		SA-36	
3	1	SMF-100-BA			
4	1	MECH SHUBBER			
5	1	1/2" CS HE			
6	1	TS 10 X 6 X .500		SA-36	
7	1	FP 1 1/2" X 1 1/2"		A-500 Q+B	
8	1	FP 1 1/2" X 1 1/2"		SA-36	
9	1	FP 1 1/2" X 1 1/2"		SA-36	
10	1	TS 10 X 6 X .500 X 5-07 1/2 FID CUT TO SUIT		A-500 Q+B	
11	1	FP 1 1/2" X 7 X 1 1/2"		SA-36	
12	1	TS 10 X 6 X .500 FID ITEM TO SUIT		SA-36	
13	2	FB 4 X 1 1/2 X 6"		A-500 Q+B	
14	2	TS 10 X 6 X .500"		SA-36	
15	6	1 1/4" Ø X 1 1/2" SERRATED NUT (SEE DET A)		SA-36	
16	4	1 1/4" Ø X 1 1/2" SERRATED WASH (SEE DET A)		SA-36	

FOR OFFICE USE ONLY



REV	DESCRIPTION	DATE	CHK'D	DATE	APPROV'D	DATE
1						
2						
3						
4						
5						
6						
7						
8						
9						
10						
11						
12						
13						
14						
15						
16						
17						
18						
19						
20						
21						
22						
23						

NO.	DESCRIPTION	DATE	CHK'D	DATE	APPROV'D	DATE
1						
2						
3						
4						
5						
6						
7						
8						
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20						
21						
22						
23						

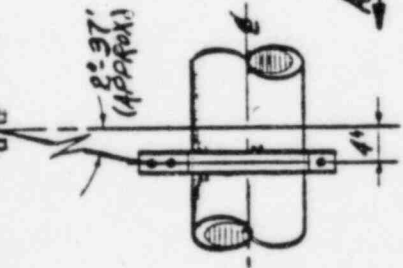
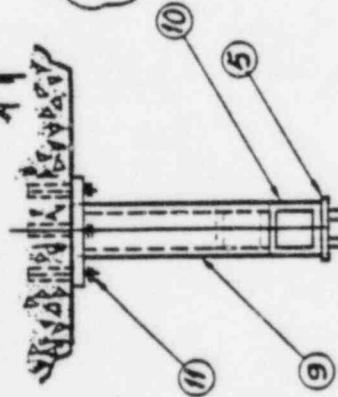
**Brown & Root, Inc.**  
Houston, Texas

**GIBBS & HILL INC.**  
ENGINEER

**TEXAS UTILITIES SERVICES INC.**  
PROJECT COMANCHE PEAK UNITS NO. 1 & 2

308 ME. NO. 15-101-005-C72K REV. B.1

BLUELINE 1-13-81  
AS-BUILT

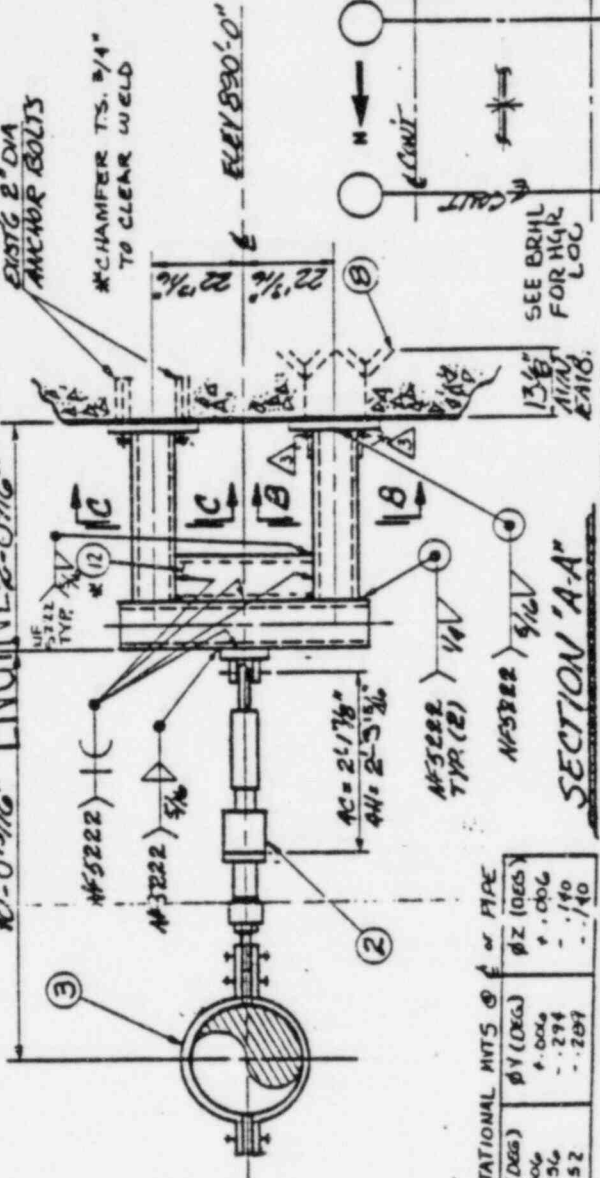


NOTES:  
1) Locking devices for high strength bolts are not required per ENCA 7607

JOURNAL (A) MAX	Ø Y (DEGS)	Ø Y (DEGS)	Ø Z (DEGS)
-.006	-.256	-.294	-.140
NORMAL (A) MIN	-.252	-.289	-.140
MINIMUM PER. NOM	-.252	-.289	-.140

76-5401

ENGINEER 2-0-71/6



ITEM NO	DESCRIPTION	QTY	WT.	ALIAS OR ASTM	MISC.
1	SMA-35-50 NCH-SNUMBER	1			
2	SMA-24-320 PIPE CLAMP	1			
3	ASME III NAME PLATE	1			
4	SMA-35-50 NCH-SNUMBER	1			
5	1/2" DIA X 3/4" L SUPER HI-TENK BOLT	2			
6	1/2" DIA X 3/4" L SUPER HI-TENK BOLT	2			
7	1/2" DIA X 3/4" L SUPER HI-TENK BOLT	2			
8	1/2" DIA X 3/4" L SUPER HI-TENK BOLT	2			
9	1/2" DIA X 3/4" L SUPER HI-TENK BOLT	2			
10	1/2" DIA X 3/4" L SUPER HI-TENK BOLT	2			
11	1/2" DIA X 3/4" L SUPER HI-TENK BOLT	2			
12	1/2" DIA X 3/4" L SUPER HI-TENK BOLT	2			
13	1/2" DIA X 3/4" L SUPER HI-TENK BOLT	2			

REV	ELECTRICAL	REV	CODE/CLASS	DATE	CHK'D	DATE	APPR'D	DATE
1	B1 SUPPORT ISO	1	NPSI-MS-1-88-02					
2	3333-11-0203	2						
3	3333-11-0203	3						
4	3333-11-0203	4						
5	3333-11-0203	5						

OWNER	TEXAS UTILITIES SERVICES INC.
PROJECT	COMANCHE PEAK UNITS NO. 1 & 2
ENGINEER	GIBBS & HILL INC.

BRHL ISOMETRIC	REV	3333-11-0206
MIS-1-EB-002	2	
FAB. ISOMETRIC	REV	3333-11-0206
MIS-1-EB-002	2	
PIPING	REV	3333-11-0206
3333-11-0206	2	
STRUCTURAL	REV	3333-11-0206
3333-11-0206	2	

BRHL ISOMETRIC	REV	3333-11-0206
MIS-1-EB-002	2	
FAB. ISOMETRIC	REV	3333-11-0206
MIS-1-EB-002	2	
PIPING	REV	3333-11-0206
3333-11-0206	2	
STRUCTURAL	REV	3333-11-0206
3333-11-0206	2	

OWNER	TEXAS UTILITIES SERVICES INC.
PROJECT	COMANCHE PEAK UNITS NO. 1 & 2
ENGINEER	GIBBS & HILL INC.

BRHL ISOMETRIC	REV	3333-11-0206
MIS-1-EB-002	2	
FAB. ISOMETRIC	REV	3333-11-0206
MIS-1-EB-002	2	
PIPING	REV	3333-11-0206
3333-11-0206	2	
STRUCTURAL	REV	3333-11-0206
3333-11-0206	2	

FOR OFFICE AND  
ENGINEERING USE ONLY

INFORMATION COPY

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CONTACT PROJECT ENGINEER FOR CURRENT  
STATUS AND HISTORY.

FOR ENGINEERING  
& OFFICE USE ONLY

FOR OFFICE AND  
ENGINEERING USE ONLY

BLUELINE EXEMPT

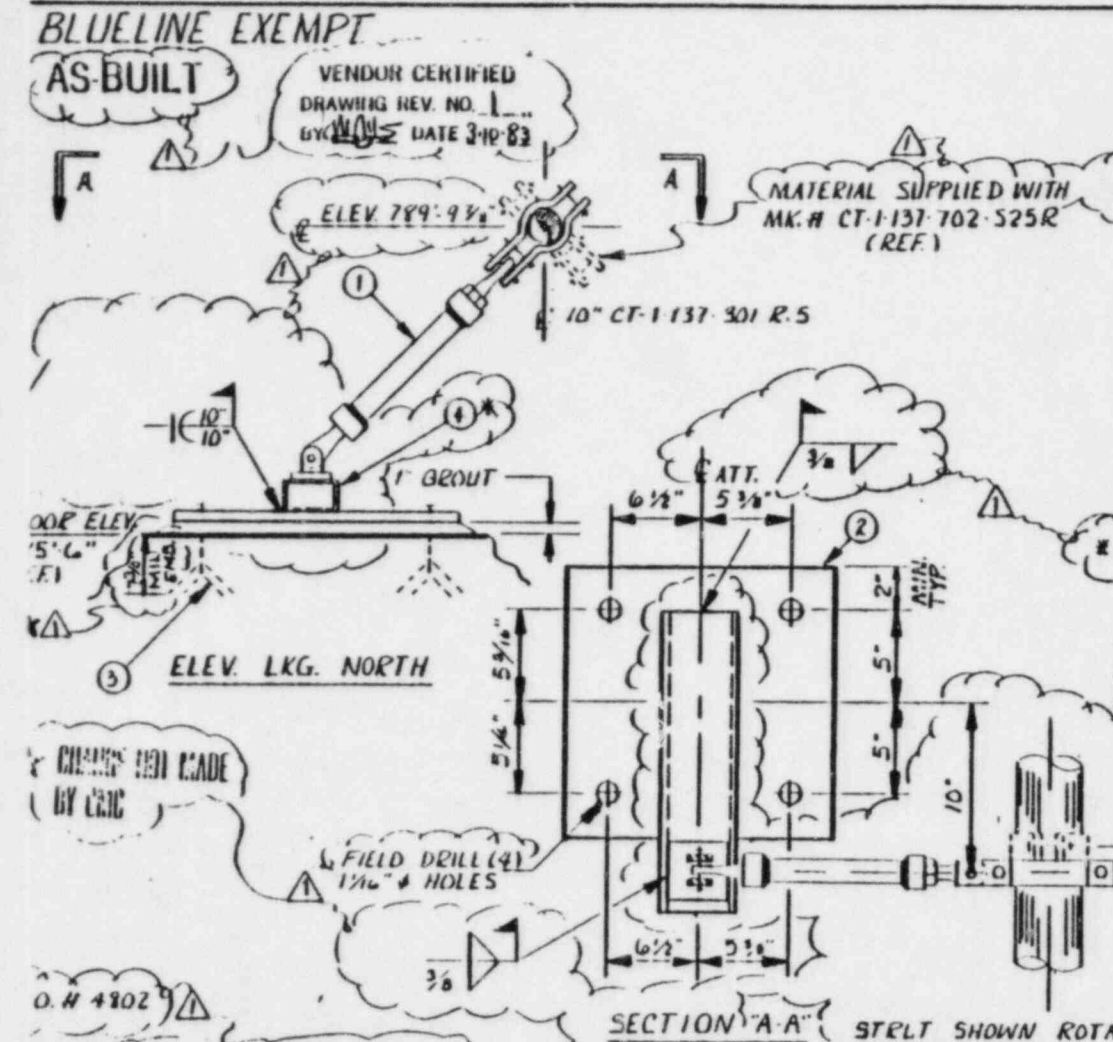
AS-BUILT

VENDOR CERTIFIED  
DRAWING REV. NO. 1  
BY WJL DATE 3-10-83

MATERIAL SUPPLIED WITH  
MK.# CT-1-137-702-S25R  
(REF.)

10" CT-1-137-301 R.S.

ELEV 789.93'



ITEM NO.	QTY. REQD.	MATERIAL DESCRIPTION	PS	CS	REC.	ASC.
1	1	SWAY STRUT SRS-20-PC CC=3'-7 1/2" WITH SPC-20-100 PIPE CLAMP (SA36)				
2	1	1" THK CARBON STEEL PLATE (A 36) (SEE SECTION "A-A")				
3	4	1" # 12 LG. SUPER HILTI KWIK BOLT				
4	1	TUBE STEEL 4" # 12 x 1/2" x 19 1/2" LG. (A500GRB)				

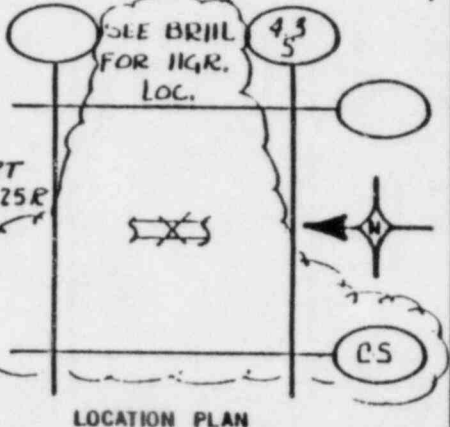
REV.	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
1	ISSUED FOR CONST REF P&E R.D.	7/18/83	VLP	WMP	RZJ
2	FIELD CUT TO SUIT				
3	DO NOT BELLOW				
4	PAINT CARBO ZINC # 11				

ASME CODE EDITION: ---  
ADDENDA: ---  
DESIGN SPEC: MS-46B

NOTES:  
1) THIS SUPPORT REPLACES SUPPORT # CT-1-137-E02-S25R  
2) To bring the new bolt to the correct fit, the old bolt should be replaced with ER-A 7017

PROB # AB-1-32-100

SEE BRILL FOR IGR. LOC.



SECTION "A-A" STEEL SHOWN ROTATED FOR CLARITY

NO.	SUPPORT LOADS (lbs)				PIPE WEIGHTS (INCHES)
	DESIGN	A	B	C	
1	3352	5271	4793		10.000
2	72	1624	1243		10.000
3					10.000
4					10.000
5	2401	4065	6508		10.000
6	173	1131	12279		10.000

BRHL 180. REV. MECHANICAL REV. ELECTRICAL REV. REV. DESCRIPTION DATE DWN. CHKD. APPVD.

CT-1-58-003 1 MI-0626 11 ET-02025 2 1 RVD AS NTD: REF: CMC 7/20/83 VLP ZEH CQ

FAB. NO. REV. STRUCTURAL REV. H.V.A.C. REV. (not used) 66908 R. DECA 7607 NEZ AS FULT ~ ~ ~ ~

CT-1-SM-003 5 ST 0600 17 MI-0650 6 10001 VERK&C&S (P&E) REF: CDDA 2/1/82 ~ ~ ~ ~

**Brown & Root, Inc.**  
ENGINEERS AND CONTRACTORS  
HOUSTON, TEXAS

CLIENT T.U.S.I.  
PLANT COMANCHE PEAK  
JOB NO. 2323

SUPPORT NO. CT-1-137-701-S25R  
SHEET 1 OF 1 REV. 1

ASME AUTHORIZED NUCL. INSP. YES  NO   
ASME CODE CLASS B1

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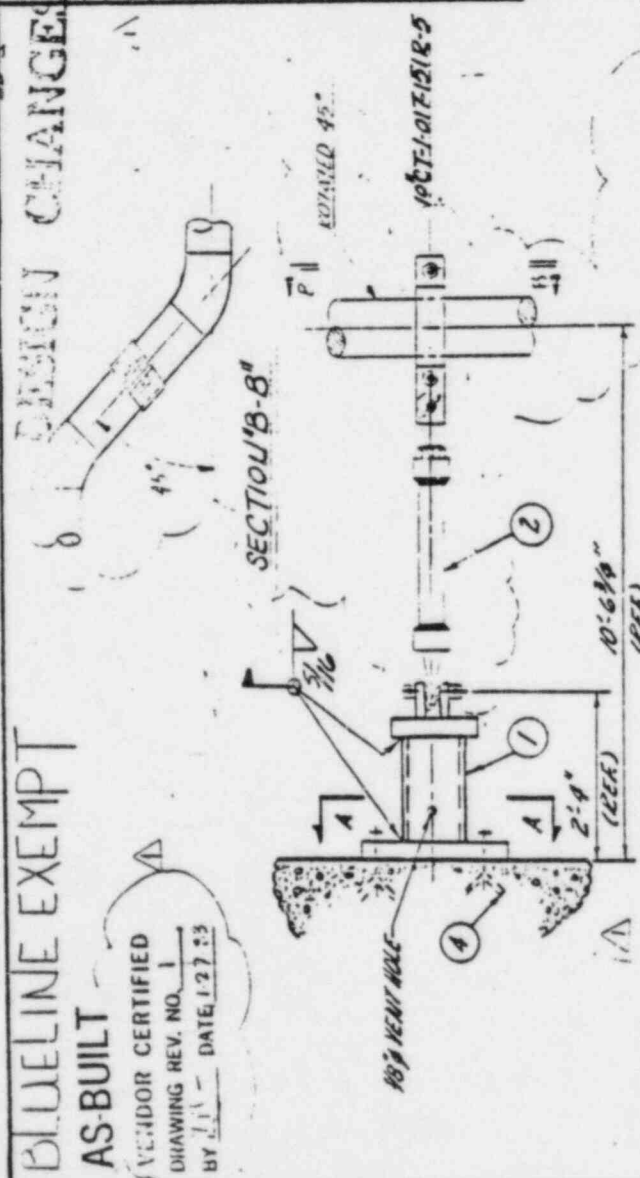
**BLUELINE EXEMPT**  
**AS-BUILT**

VENDOR CERTIFIED  
 DRAWING REV. NO. 1  
 BY            - DATE 1/27/83

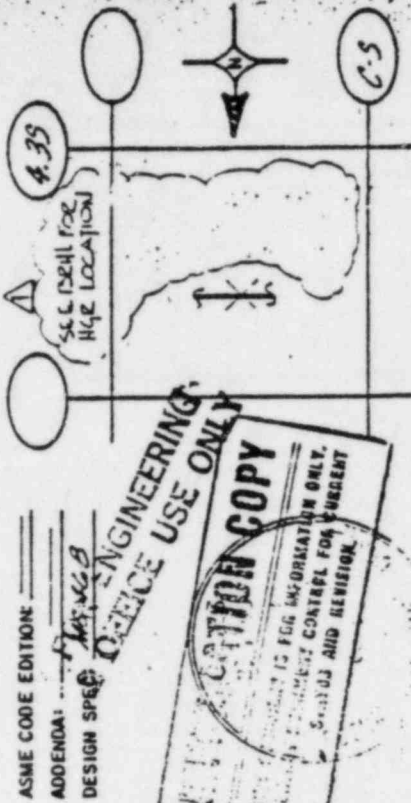
**DESIGN CHANGES**

ITEM NO.	QTY. REQD.	MATERIAL	DESCRIPTION
1	1	7.5 3/4" x 200' 2" PLG. COIL	SUPP. A. 300028
2	1	3/4" x 20' 0" PL. CC-8174	WELDED
3	1	SPC. 20-100	317
4	4	2" x 1/2" x 1/2" SEC. 30304 (A)	1/2" x 1/2" SUPER. HILD. AIR CORR. ANGLE
			(MIN. ENDS = 3 1/2')

REV.	DESCRIPTION	DATE	CHKD.	APPRD.
1	DCA 7607 (SECT. 1) AS BUILT			
2	VEHICLE CERTIFICATION OF DCA 7607			



PLAN VIEW @ EL. 108'-6" (REF.)



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 ENGINEERING OFFICE USE ONLY

**NOTES:**  
 Locking devices for high strength bolts are not required per DCA 7607

SEE CPPA # 14919  
 FOR E' NUMBER INFORMATION  
 10' 4802

DATE	PT	SUPPORT	LOADS	LIMITS	PIPE	WYS	INCHES	YES	NO
DESIGN									
VERT.									
N-S									
E-W									

REV.	DESCRIPTION	DATE	CHKD.	APPRD.
1	DESIGNED FOR COIL	1/11/83		
2	REV. AS NOTED	1/11/83		
3	REV. AS NOTED	1/11/83		

PLANT COMANCHE PEAK  
 JOB NO. 2323  
 SUPPORT NO. CFI-017-104-5222  
 SHEET 1 OF 1 REV. 1

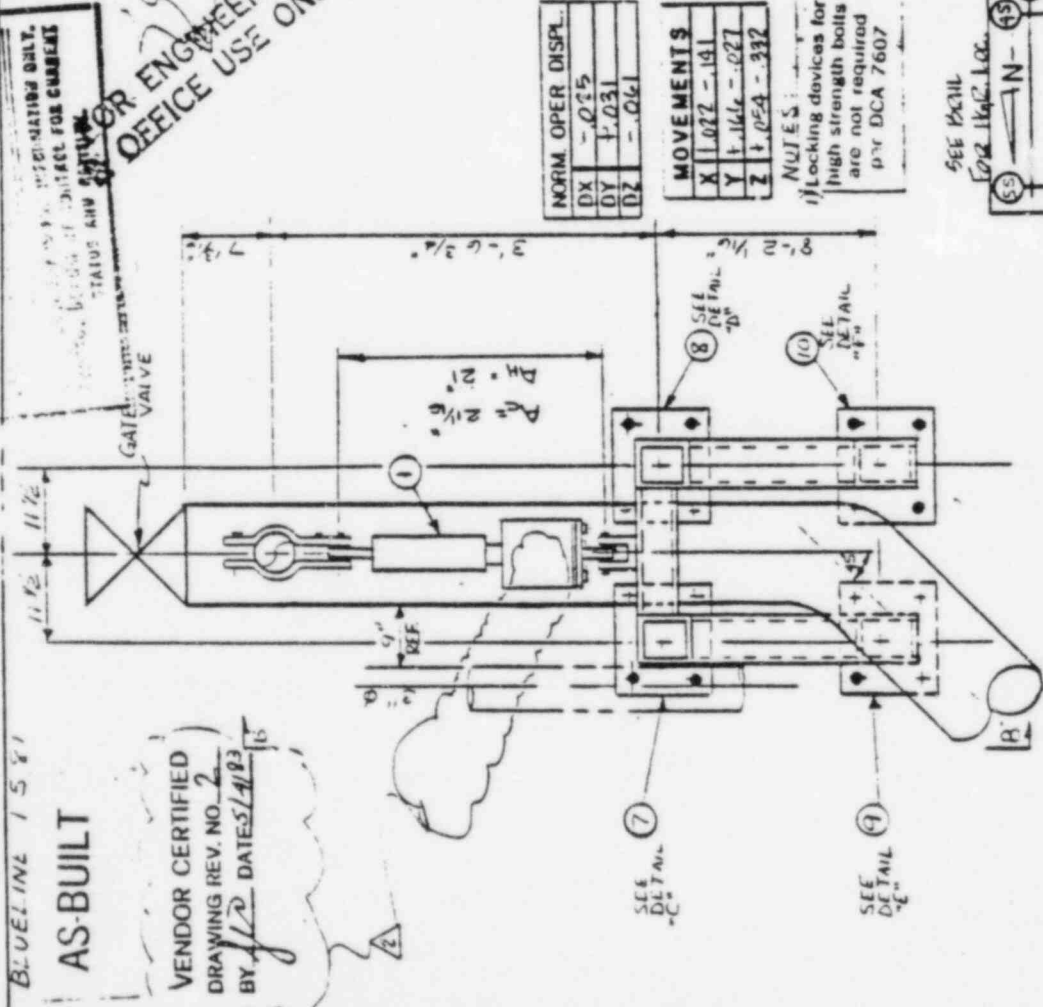
BROWN & ROOT, Inc.  
 HOUSTON, TEXAS

LOCATION PLAN

# FOR OFFICE AND

# ENGINEERING USE ONLY

BLUELINE 1581  
**AS-BUILT**  
 VENDOR CERTIFIED  
 DRAWING REV. NO. 2  
 BY *[Signature]* DATES 5/1/83  
 16



NORM. OPER. DISPL.

DX	-0.15
DY	+0.31
DZ	-0.61

MOVEMENTS

X	+0.22 - .141
Y	+0.166 - .021
Z	+0.054 - .332

NOTES:  
 1) Locking devices for high strength bolts are not required per DCA 7607

TOM 4902 PLAN VIEW C.F.L. 818'-0"

0.4 HL Iso. AT 1-58-0221  
 I.P.D. Iso. C.T.I.S.B.Y REV. 5  
 Data Point C600/B000/AB-L-322c  
 Pipe Mat'l. SA 308 CL 1 LP 304  
 Insul. \_\_\_\_\_ Bldg. S.B.



LOCATION PLAN  
 THIRD PARTY INSPECTION  
 CODE CLASS: ASME III-2

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	WT	SEC
1A	SMF-10 KO SNURRER	2		128	
1B	SMF-10 FORWARD STANCHION(SA312)	2		45	
2	P10 SCH 40 1 1/2" STANCHION(SA312)	3		136	
3	SFC-17 100 PIPE SLAMP(SA36)				
6	3/4" CS PL (BY FIELD)	16			
7	3/4" CS PL SEE DETAIL "C" (SA515 GRB/SAN)	1			
8	3/4" CS PL SEE DETAIL "D" (SA515 GRB/SAN)	1			
9	3/4" CS PL SEE DETAIL "E" (SA515 GRB/SAN)	1			
10	3/4" CS PL SEE DETAIL "F" (SA515 GRB/SAN)	1			
11	3/4" CS PL SEE DETAIL "G" (SA515 GRB/SAN)	1			
12	ASME III NAME PLATE	1			
13	TS 8" LG 1/2" X 1/2" LG (A500 GRB)	2			
14	TS 8" LG 1/2" X 1/2" LG (A500 GRB)	2			
15	TS 6" LG 1/2" X 1/2" LG (A500 GRB)	2			

DESCRIPTION

REVID VENDOR CERTIFICATION  
 REF. CHG 90074, 2, 1

MARK # CT-1-013-023-342K  
 PAINT: CARBO ZINC #11

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. \_\_\_\_\_ SHEET OF \_\_\_\_\_

BROWN & ROOT, INC.  
 ENGINEERS & CONSTRUCTORS

REF. DRAWING NUMBERS  
 PIPE: MI-0612 REV.13 ELECT. REV. 0602-01  
 STEEL: SI-0605 REV.1 HV.A.C.I. M16042

CONDITIONS  
 DESIGN NORMAL & UPRBT  
 EMERGENCY FAULTED

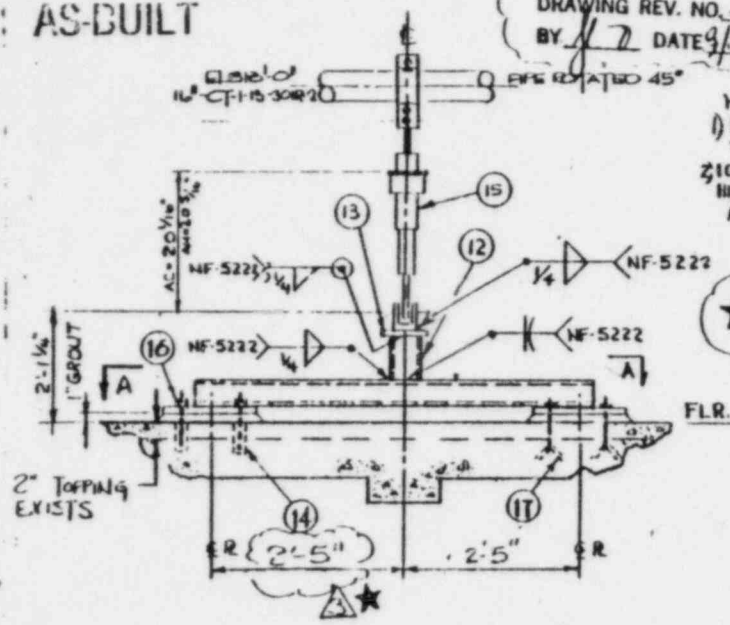
CUSTOMER Texas Utilities Service, Inc.  
 ORDER OR CONT. NO. CP-0046  
 JOB NAME Comanche Peak 1B.2  
 MARK NO. CT-1-013-023-342K  
 SKETCH NO. \_\_\_\_\_  
 SHEET 1 OF 3 REV. ?

CONT ABOVE

# FOR OFFICE AND ENGINEERING USE ONLY

BLUELINE 1-16-BL  
AS-BUILT

VENDOR CERTIFIED  
DRAWING REV. NO. 3  
BY 17 DATE 9/18/83



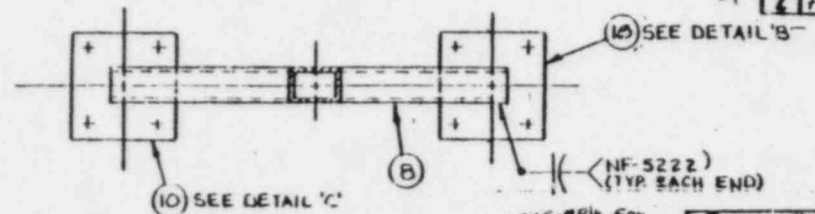
NOTE:  
1) PIPE MOVEMENT IS  
Y (UP)  $\frac{3}{8}$ " WHEN HOT.  
2) LOCKING BOLTS FOR  
HIGH STRENGTH BOLTS  
ARE NOT REQUIRED  
PER DCA 7507

★ CHANGE NOT MADE  
BY CMC

FLR. EL. 810'-6"

NORM. OPER. DISPL.	
DX	+ .023
DY	+ .154
DZ	- .04

MOVEMENTS	
X	+ .137 / - .029
Y	+ .711 / - .117
Z	+ .071 / - .451



SECTION A-A

SEE SPEC FOR  
1192.100  
T0.4802



DRILL 150 CT-1-28 000/6/1  
I.P.D. No. CT-1-28-B-REVS  
Data Point: G2/PB08 AF 1-31 R.O.  
Pipe Mat. 1.2A 358 CL.1 TP.204

THIRD PARTY INSPECTION  
CODE CLASS: ASME III-2

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	P&I	CBS	PRIM	SEC	AISC
	SEISMIC MECHANICAL SHOCK SUPPRESSOR CONSISTING OF:							
1	NO. 6 STROKE FIG. 307N MECHANICAL SHOCK SUPPRESSOR W/1" DIA. 16" O.D. PIPE, CARBON STEEL, LOAD 1887#	1						
2	T.S. 3/8" x 6" x 4" x 5" B.L.G. (A500 GR B)	1						
3	C.S. R 1" x 1/2" x 1/2" x 1/2" / DETAIL 'B' (SA 36/SA 515 GR B)	1						
4	C.S. R 1" x 1/2" x 1/2" x 1/2" / DETAIL 'C' (SA 36/SA 515 GR B)	1						
5	3/4" x 1/2" W/HT KWIK COND. ANCHOR	4						
6	IS. 3/4" x 1/2" x 1/2" x 1/2" L.G. (A500 GR B)	1						
7	C.S. R 3/4" x 1/2" x 1/2" x 1/2" (SA 36/SA 515 GR B)	1						
8	1/4" x 1/2" THREADED ROD FOR RICHMOND INSERT (FIELD CUT TO LENGTH) (SA 36)	4						
9	SMA-R.P.C. 1" x 1/2" x 1/2" x 1/2" UPTOP-919# W/SR-14-100 RUBBER W/ PIPE CLAMP	1						
10	SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG MARK # CT-1-013-020-542K	1						
11	EXN-1/2" HEX NUTS	8						
12	1/4" x 1/2" SUPER MULTI KWIK BOLTS - #13/16" MILL ERB.	4						
13	1" C.S.R. (PER DETAIL 'B') SA 36	4						
	Apply one coat of Carbo Zinc #11 to above mat'l except th'ds which shall be coated w/r dual preventative.							
REV	DATE	OWN	CNK	APP	DESCRIPTION			
1	9/18/83	VM	PC	HL	REV'D VENDOR CERT			
Approved By: J.F.C. Date: 9-30-83						QUAN	S.I.P.	

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

Brown & Root, Inc.		CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
REF. DRAWING NUMBERS		DESIGN						
PIPE: M1-0608-REV.3 ELECT: 2-REV.0		NORMAL & UPSET		15058				
STEEL: S1-0608-REV.4 HVAC: 2-REV.0		EMERGENCY		1911				
		FAULTED						
REV	DATE	OWN	CNK	APP	DESCRIPTION	CUSTOMER		
1	9/18/83	VM	PC	HL	ISSUED FOR CONST.	Tough Protection Services, Inc.		
2	10/10/83	VM	PC	HL	REF. NPSI R.O.-D	ORDER OR CONT. NO. CT-013		
3	11/10/83	VM	PC	HL	REV AS MTD. REF FIELD MODIFIED NAME	JOB NAME		
4	12/10/83	VM	PC	HL	REV AS MTD. REF MTD. MODIFIED NAME	MARK NO. CT-1-013-020-542K		
5	1/10/84	VM	PC	HL	REV AS MTD. REF MTD. MODIFIED NAME	SKETCH NO.		



**FOR ENGINEERING OFFICE USE ONLY**  
 THIS DRAWING IS FOR INFORMATION ONLY.  
 CONTACT ENGINEERING OFFICE FOR CURRENT STATUS AND REVISED.

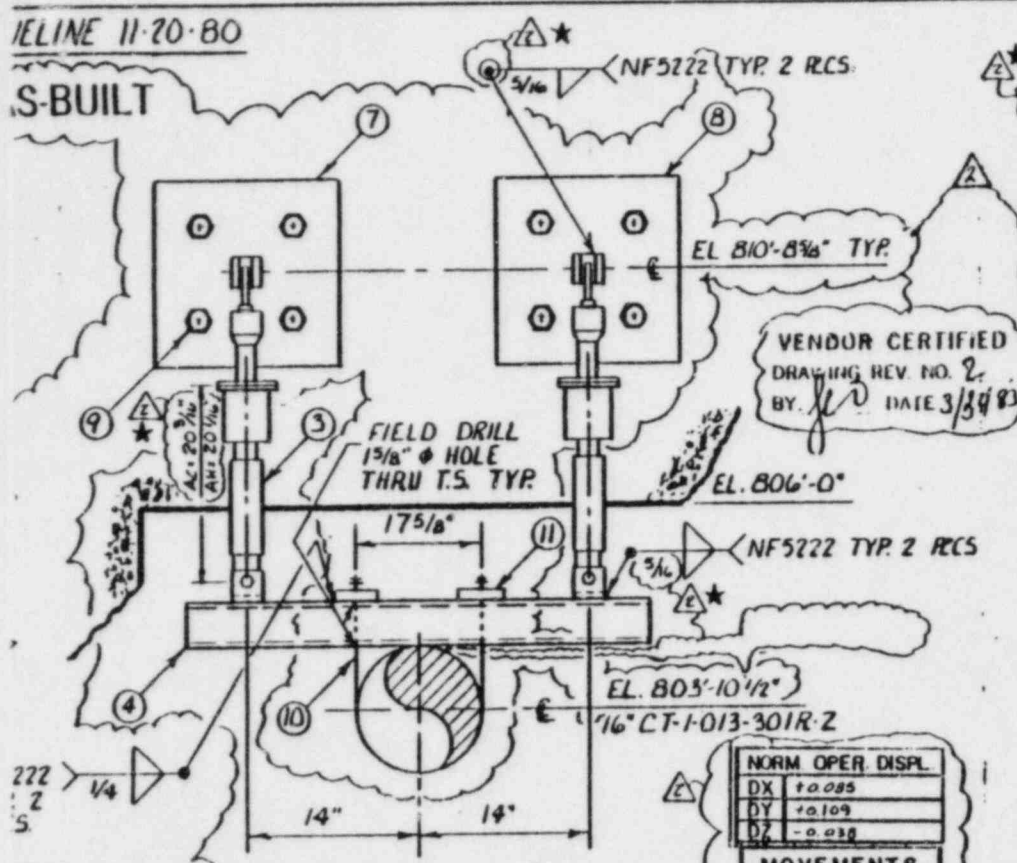
**FOR ENGINEERING OFFICE USE ONLY**

**FOR OFFICE AND**

**ENGINEERING OFFICE USE ONLY**

IELINE 11-20-80

S-BUILT



NOTES:  
 Locking devices for high strength bolts are not required per DCA 7607

★ CHANGE NOT MADE BY C.T.C.

DRILL ISO. CT-1-SB-008/R.1  
 I.P.D. ISO. CT-1-SB-8 REV. 5  
 Data Point 256/PROB.# AB-1-32/R.O  
 Pipe Mat'l. SA-358-CL1 TP304  
 Insul. Bldg. SB

NORM OPER. DISPL.	
DX	+0.085
DY	+0.109
DZ	-0.038
MOVEMENTS	
X	+0.336/-0.074
Y	+0.591/-0.098
Z	+0.031/-0.253

T.O.#4802



THIRD PARTY INSPECTION  
 CODE CLARS: ASME III-2

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	L	CBS	PRIM	SEC	AISC
3	SMALIO BA SNUBBLER C-C-B-T	2							
4	T.S. 3/4" x 4" x 4" x 2'-10" I.G. A500GRB	1							
7	1" T.S. R PER DETAIL A SA36 OR SA515GR65	1							
8	1" T.S. R PER DETAIL B SA36 OR SA515GR65	1							
9	1 1/2" x 1 1/2" SUPER MULTI KWIK BOLT	8							
10	1 1/2" x 1 1/2" ROD B-16 1/4" 11-5/16"	1							
11	DEVELOPED LENGTH 4'-3" SA36								
11	3/4" C.S. R 4" x 4" W/ 1 1/2" x 1 1/2" HOLE @ CENTER SA36	2							

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	2/2/83	JTN	WJH	[Signature]	ISSUED FOR CONST. - REF. I.T.T. R.1 - BASE PLATE ONLY
2	11-20-80	[Signature]	[Signature]	[Signature]	ISSUED FOR CONST. REF FIELD HANGERS SKETCH & REF I.T.T. R-2 & DELETED NOTE 1-3 & ADDED SH 2 OF 2

MARK # CT-1-015-016-337K  
 PAINT: CARBO ZINC # 11

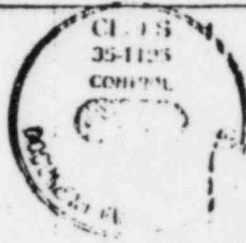
FOR MATERIALS AND OPERATIONS SEE SKETCH NO.		SHEET OF					
CONDITIONS	Fx	Fy	Fz	Mx	My	Mz	
DESIGN							
NORMAL & UPSET							
EMERGENCY							
FAULTED							

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	3/3/83	[Signature]	[Signature]	[Signature]	REV'D AS NY'D. REF: CMC 4/10/82.7 DCA 7607 NT 4 ASBUILT VENDOR CERTIFICATION, REF: GTN 6276

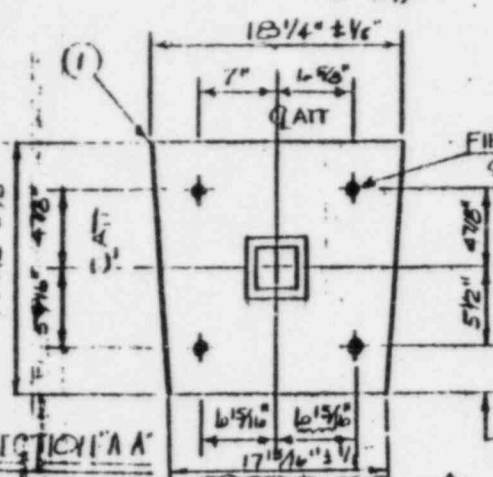
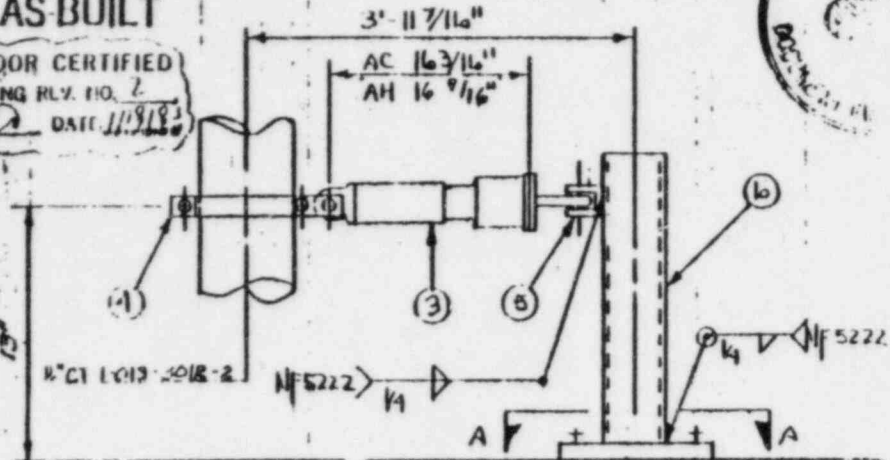
CUSTOMER Texas Utilities Service, Inc.  
 ORDER OR CONT. NO. CP-0046  
 JOB NAME Comanche Peak 1 & 2  
 MARK NO. CT-1-015-016-337K  
 SKETCH NO.

BLUELINE 12-18-81

AS-BUILT



VENDOR CERTIFIED  
DRAWING REV. NO. 2  
DATE 11/9/83



PLANVIEW @ ELEV. 803'-10 1/2" N

NOTES:  
1) Locking devices for high strength bolts are not required per DCA 7607

MOVEMENTS	
X	1.00 / 1.74
Y	1.57 / 0.58
Z	1.00 / 0.58
NORM OPER DISPL.	
DX	1.00 / 0.58
DY	1.57 / 0.58
DZ	1.00 / 0.58

CTR LINE OF ART MAY VARY ± 1/4"



THIRD PARTY INSPECTION  
CODE CLASS: ASME III-2

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	SEC	PRIM	SEC	ATSC
1	3/4" C.S. B. PER SECT "A-A" (CARB/ZINC GRUO5)						
2	1 1/2" HILTI KWIK BOLTS (16" MIN EMBED)						
3	SME-3-30 CHUBBER CO. 2 1/2"						
4	SFC-10-160 PIPE CLAMP (SA-36)						
5	XRB-16 REAR BRACKET (A-160/SA36)						
6	T.S. 4" x 1/2" x 1/2" x 1/2" (2-5004RF)						

FOR OFFICE USE ONLY

INFORMATION COPY

THIS DOCUMENT IS FOR INFORMATION ONLY. CONTACT BROWN & ROOT FOR STATUS AND REVISIONS.

MARK # CT-1-013-015-553R  
PAINT: CARBO ZINC # 11

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

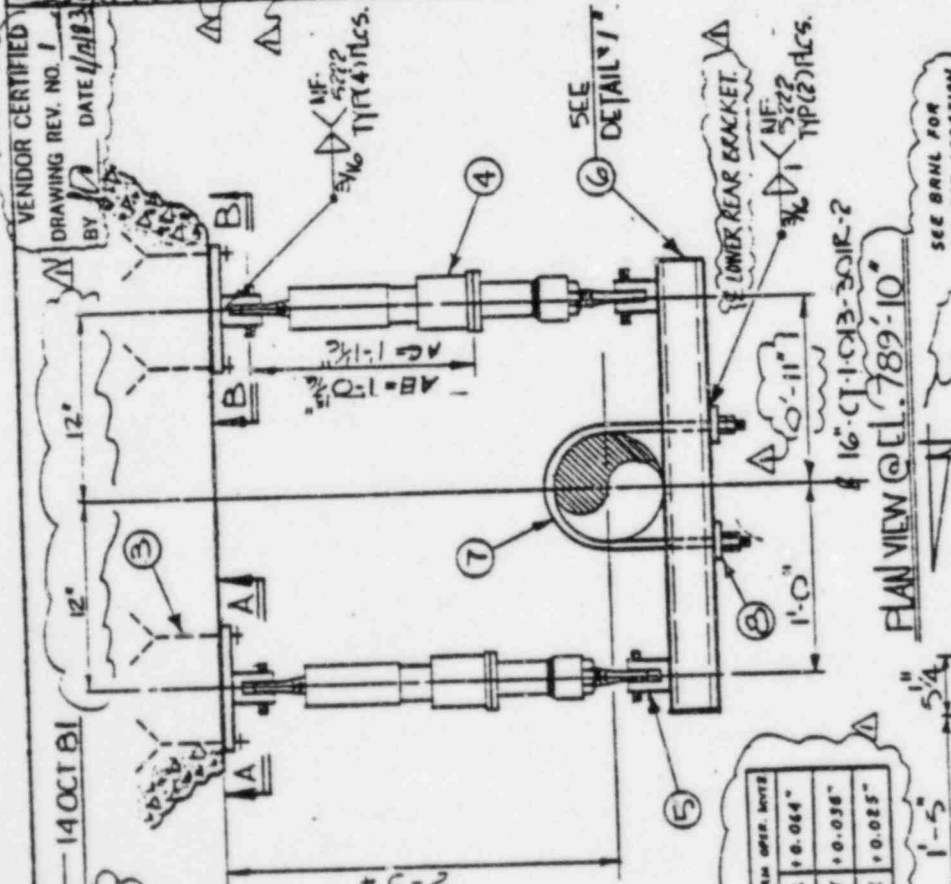
CONDITIONS	F x F y F z M x M y M z					
	DESIGN	NORMAL & UPSET	EMERGENCY	FAULTED		
	1990	1545				

REV	DATE	OWN	CHK	APP	DESCRIPTION	CUSTOMER
1					ISSUE FOR CONSTRUCTION	Texas Utilities Service, Inc.
2					REV. BY REV. 1 THIS REV. AS NOTED RE: 1207	ORDER OR CONT. NO. CP-0046
3					SEE INT. 11/16/83 SIDE AS-BUILT	JOB NAME Comanche Peak 198
4					VENDOR CERTIFICATION, REF. GTN # 68726	MARK NO. CT-1-013-015-553R
						SKETCH NO.
						SHEET OF REV. 2

UT-1-58-008 R.1  
BRP Iso. CT-1-SB-8 R-3  
Data Point 125W/PROP AB-1 SR R.O  
Pipe Mat'l. SA 358 CL TP 304  
Insul. Bldg. SP  
TOT 1502

FOR OFFICE AND ENGINEERING USE ONLY

**BLUELINE - 14 OCT 81**  
**AS-BUILT**



**MATERIALS & OPERATIONS**

ITEM NO.	DESCRIPTION	QUAN	SHIP
1	UPPER SECTION 1013-301R-2	1	
2	LOWER SECTION 1013-301R-2	1	
3	1/2" DIA. PIN (2)	2	
4	1/2" DIA. PIN (2)	2	
5	1/2" DIA. PIN (2)	2	
6	1/2" DIA. PIN (2)	2	
7	1/2" DIA. PIN (2)	2	
8	1/2" DIA. PIN (2)	2	
9	1/2" DIA. PIN (2)	2	
10	1/2" DIA. PIN (2)	2	
11	1/2" DIA. PIN (2)	2	
12	1/2" DIA. PIN (2)	2	
13	1/2" DIA. PIN (2)	2	
14	1/2" DIA. PIN (2)	2	
15	1/2" DIA. PIN (2)	2	
16	1/2" DIA. PIN (2)	2	
17	1/2" DIA. PIN (2)	2	
18	1/2" DIA. PIN (2)	2	
19	1/2" DIA. PIN (2)	2	
20	1/2" DIA. PIN (2)	2	
21	1/2" DIA. PIN (2)	2	
22	1/2" DIA. PIN (2)	2	
23	1/2" DIA. PIN (2)	2	
24	1/2" DIA. PIN (2)	2	
25	1/2" DIA. PIN (2)	2	
26	1/2" DIA. PIN (2)	2	
27	1/2" DIA. PIN (2)	2	
28	1/2" DIA. PIN (2)	2	
29	1/2" DIA. PIN (2)	2	
30	1/2" DIA. PIN (2)	2	
31	1/2" DIA. PIN (2)	2	
32	1/2" DIA. PIN (2)	2	
33	1/2" DIA. PIN (2)	2	
34	1/2" DIA. PIN (2)	2	
35	1/2" DIA. PIN (2)	2	
36	1/2" DIA. PIN (2)	2	
37	1/2" DIA. PIN (2)	2	
38	1/2" DIA. PIN (2)	2	
39	1/2" DIA. PIN (2)	2	
40	1/2" DIA. PIN (2)	2	
41	1/2" DIA. PIN (2)	2	
42	1/2" DIA. PIN (2)	2	
43	1/2" DIA. PIN (2)	2	
44	1/2" DIA. PIN (2)	2	
45	1/2" DIA. PIN (2)	2	
46	1/2" DIA. PIN (2)	2	
47	1/2" DIA. PIN (2)	2	
48	1/2" DIA. PIN (2)	2	
49	1/2" DIA. PIN (2)	2	
50	1/2" DIA. PIN (2)	2	
51	1/2" DIA. PIN (2)	2	
52	1/2" DIA. PIN (2)	2	
53	1/2" DIA. PIN (2)	2	
54	1/2" DIA. PIN (2)	2	
55	1/2" DIA. PIN (2)	2	
56	1/2" DIA. PIN (2)	2	
57	1/2" DIA. PIN (2)	2	
58	1/2" DIA. PIN (2)	2	
59	1/2" DIA. PIN (2)	2	
60	1/2" DIA. PIN (2)	2	
61	1/2" DIA. PIN (2)	2	
62	1/2" DIA. PIN (2)	2	
63	1/2" DIA. PIN (2)	2	
64	1/2" DIA. PIN (2)	2	
65	1/2" DIA. PIN (2)	2	
66	1/2" DIA. PIN (2)	2	
67	1/2" DIA. PIN (2)	2	
68	1/2" DIA. PIN (2)	2	
69	1/2" DIA. PIN (2)	2	
70	1/2" DIA. PIN (2)	2	
71	1/2" DIA. PIN (2)	2	
72	1/2" DIA. PIN (2)	2	
73	1/2" DIA. PIN (2)	2	
74	1/2" DIA. PIN (2)	2	
75	1/2" DIA. PIN (2)	2	
76	1/2" DIA. PIN (2)	2	
77	1/2" DIA. PIN (2)	2	
78	1/2" DIA. PIN (2)	2	
79	1/2" DIA. PIN (2)	2	
80	1/2" DIA. PIN (2)	2	
81	1/2" DIA. PIN (2)	2	
82	1/2" DIA. PIN (2)	2	
83	1/2" DIA. PIN (2)	2	
84	1/2" DIA. PIN (2)	2	
85	1/2" DIA. PIN (2)	2	
86	1/2" DIA. PIN (2)	2	
87	1/2" DIA. PIN (2)	2	
88	1/2" DIA. PIN (2)	2	
89	1/2" DIA. PIN (2)	2	
90	1/2" DIA. PIN (2)	2	
91	1/2" DIA. PIN (2)	2	
92	1/2" DIA. PIN (2)	2	
93	1/2" DIA. PIN (2)	2	
94	1/2" DIA. PIN (2)	2	
95	1/2" DIA. PIN (2)	2	
96	1/2" DIA. PIN (2)	2	
97	1/2" DIA. PIN (2)	2	
98	1/2" DIA. PIN (2)	2	
99	1/2" DIA. PIN (2)	2	
100	1/2" DIA. PIN (2)	2	

**INFORMATION**  
THIS DRAWING IS FOR THE  
PURPOSE OF THE  
CONSTRUCTION OF THE  
UTILITY.

**MOVEMENTS**

	MAX	MIN	OPER	NOTE
X	0.168	0.056	DX	0.064
Y	0.177	0.031	DY	0.036
Z	0.171	0.022	DZ	0.025

**FOR MATERIALS AND OPERATIONS SEE SKETCH NO. \_\_\_\_\_ SHEET OF \_\_\_\_\_**

**CONDITIONS**  
DESIGN  NORMAL & UPRIGHT  
EMERGENCY  FAULTED

**REF. DRAWING NUMBERS**  
F 12  
PIPE 1 M-0000 0013 ELECTRICIAN'S  
STEEL 54-0000 0011 HV.A.G. 10-0000 0004

**DESCRIPTION**  
ISSUED FOR CONST. REF. 10/11/81  
BY: [Signature]  
DATE: 10/11/81  
REVISED BY: [Signature]  
DATE: 10/11/81  
VENDOR CERTIFIED 17-07466276

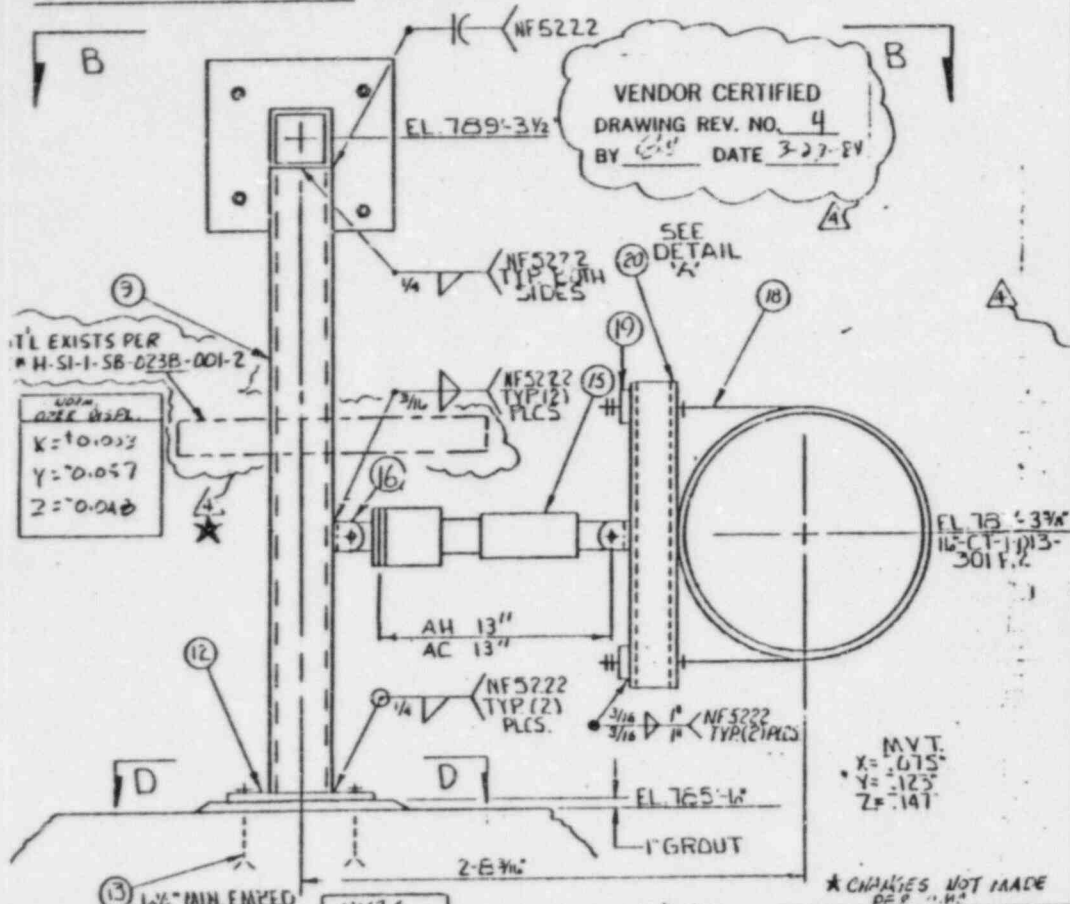
**CUSTOMER TAGS UTILITIES - 42062 IN**  
ORDER OR CONT. NO. CP-00046  
JOB NAME COMMERCIAL PEAK 112  
MARK NO. CT-1013-301R-2  
SKETCH NO. \_\_\_\_\_  
SHEET OF 2 REV. \_\_\_\_\_

**FOR OFFICIAL USE ONLY**

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**FOR OFFICIAL USE ONLY**

BLUELINE 2-14-81 AS-BUILT



VENDOR CERTIFIED  
DRAWING REV. NO. 4  
BY [Signature] DATE 3-27-81

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	L	CSS	PRIM	SEC	AISC
	SEISMIC MECHANICAL SHOCK SUPPORT ASSEMBLY CONSISTING OF:								
1	SHOCK SUPPORT ASSEMBLY	1							
2	PIPE 4x4x1/2 A53B	1							
3	FLANGE 16" DIA	1							
4	WASHER PL	2							
5	BOLT 1/2" DIA	1							
6	WASHER PL	1							
7	BOLT 1/2" DIA	1							
8	WASHER PL	1							
9	BOLT 1/2" DIA	1							
10	WASHER PL	1							
11	PIPE 4x4x1/2 A53B	1							
12	FLANGE 16" DIA	1							
13	WASHER PL	2							
14	BOLT 1/2" DIA	1							
15	WASHER PL	1							
16	BOLT 1/2" DIA	1							
17	WASHER PL	1							
18	BOLT 1/2" DIA	1							
19	WASHER PL	1							
20	FLANGE 16" DIA	1							

REVISIONS:

NO.	DATE	BY	DESCRIPTION
1	2-14-81	[Signature]	ISSUE FOR CONSTRUCTION
2	3-27-81	[Signature]	REVISED VENDOR CERTIFICATION

FOR OFFICE AND ENGINEERING USE ONLY

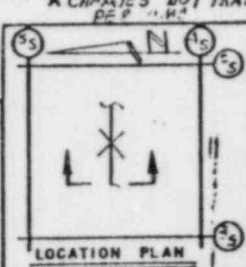
SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG  
MARK # CT-1-013-008-S22K

Apply Carbo Zinc #1 to above mat'l, except threads which shall be treated with a rust preventative

**NOTE**  
Locking devices for high strength bolts are not required per NFCA 7607

COORDINATE	VALUE
X	0.003
Y	0.057
Z	0.048

SEE BRILL FOR LOCATION



THIRD PARTY INSPECTION YES  NO   
CODE CLASS: ASME III-2

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

Brown & Root, Inc.

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN						
NORMAL & UPSET	2503					
EMERGENCY	753					
FAULTED						

REF. DRAWING NUMBERS  
PIPE: MI-0606 KEYLO ELECT: EI-0606 R12  
STEEL: SI-0600 REV 17 HV.A.C: MI-0650 R6

REV	DATE	DNW	CHK	APP	DESCRIPTION
1	11-26-80	[Signature]	[Signature]	[Signature]	ISSUE FOR CONSTRUCTION
2	2-14-81	[Signature]	[Signature]	[Signature]	REVISED VENDOR CERTIFICATION
3	3-27-81	[Signature]	[Signature]	[Signature]	REVISED VENDOR CERTIFICATION

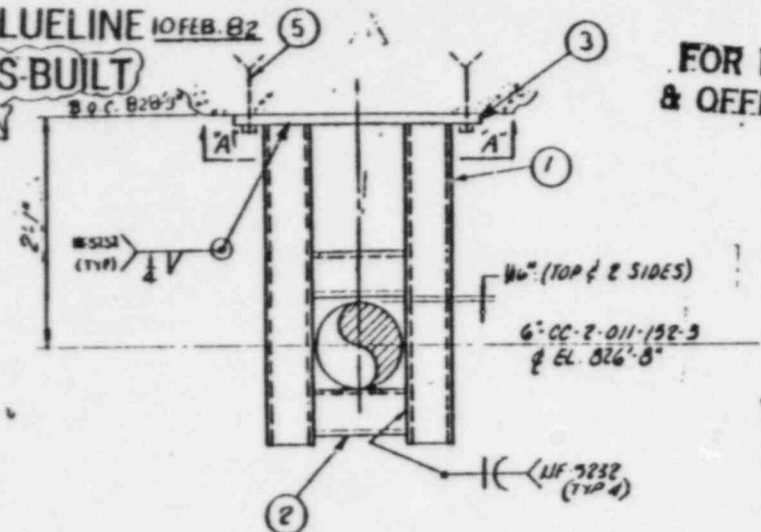
CUSTOMER: TEXAS UTILITIES SERVICE, INC.  
ORDER OR CONT. NO. CP-0046  
JOB NAME: COMANCHI PEAK 142  
MARK NO. CT-1-013-008-S22K  
SKETCH NO. [Blank]  
SHEET 1 OF 2 REV. 4

FOR OFFICE AND ENGINEERING USE ONLY

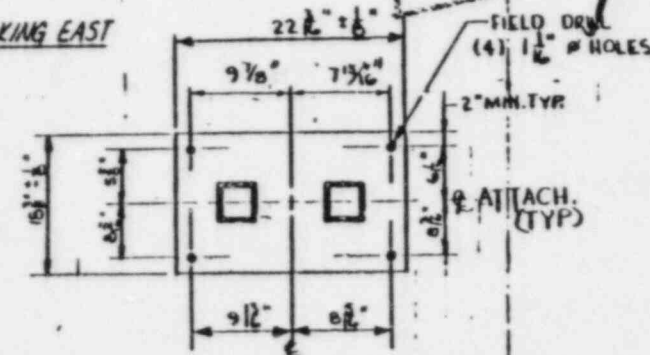
FOR OFFICE AND ENGINEERING USE ONLY

BLUELINE 10 FEB. 82  
AS-BUILT

FOR ENGINEERING  
& OFFICE USE ONLY



ELEVATION LOOKING EAST



SECTION 'A-A'  
2 OF ATTACH. MAY VARY 1/4"

MVTS
0000
2-00

ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	PAS	CS	PRIM	SEC	AISC
1	2	3X3X1/4X 2'-7 1/4" TUBE 1500 GR.B		X	X	X	
2	2	3X3X1/4X 6' TUBE 1500 GR.B		X	X	X	
3	1	7/8" CSIF SEE SECTION AA 236/SASISGR15	X		X	X	
4	4	1" X 9" MULTI-KWIK CONCRETE ANCHORS				X	
5	4	1" X 9" MULTI-KWIK CONCRETE ANCHORS MIN EMB'L"				X	

REV	DESCRIPTION	DATE	DWN	CHKD	APPVD
1	AS-BUILT YELLOW (ORIGINAL) (12/5/79)	2	2	2	2

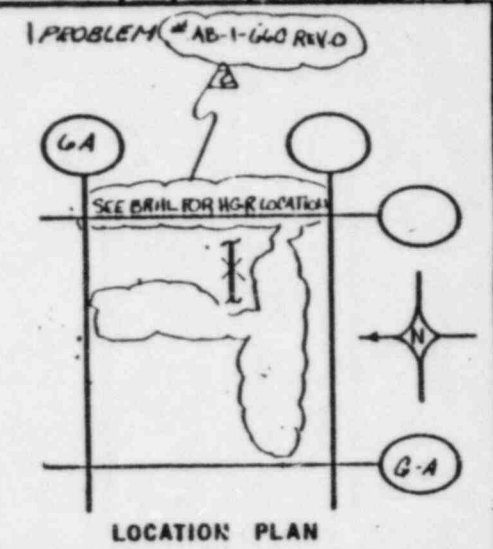
VENDOR CERTIFIED  
DRAWING REV. NO. 2  
BY BH DATE 12/18/82

NOTE:  
Locking devices for high strength bolts are not required per DCA 7607

TO # 21101

ASME CODE EDITION: 1974  
ADDENDA: WINTER  
DESIGN SPEC: MS-46A

P.R. CERTIFICATION



LOCATION PLAN

DATA PT	SUPPORT	LOADS (LBS)	PIPE	REF	BRW. ISO	REV	MECHANICAL	REV	ELECTRICAL	REV	DESCRIPTION	DATE	DWN	CHKD	APPVD
2075	DESIGN	135	12	CC-2-AR-004	1	11/0703	12	E10701-02	3	1	REV'D AS NOTED REF: E.M.H.S.	2/20/82	A.P.H.	1	1
	VERT	135	12	FAB. ISO	2	80713	3	H.V.A.C	6	0	1/80	12-27-79	C.A.T.	1	1
	N-S	135	12												
	E-W	135	12												

NOTE: AUTHORIZED NUCL. INSP. YES  NO   
ASME CODE CLASS 3

**CISES**  
Brown & Root, Inc  
ENGINEERS AND CONSTRUCTORS  
HOUSTON, TEXAS  
35-1195

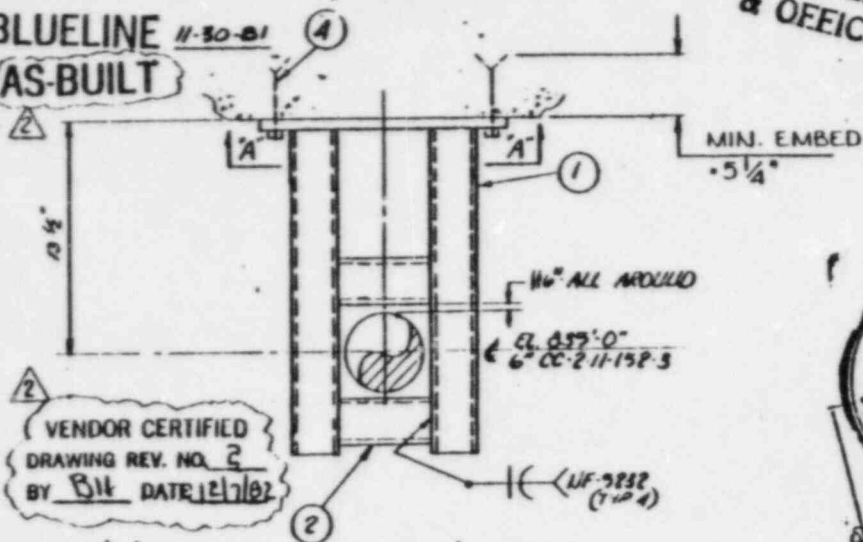
CLIENT: T.U.S.I.  
PLANT: COMANCHE PEAK  
JOB NO.: 2323

SUPPORT NO. CC-2-011-721-A135  
SHEET 1 OF 1 REV. 12

FOR OFFICE AND  
ENGINEERING USE ONLY

**FOR ENGINEERING & OFFICE USE ONLY**

**BLUELINE 11-30-81**  
**AS-BUILT**



VENDOR CERTIFIED DRAWING REV. NO. 2 BY BH DATE 12/7/82



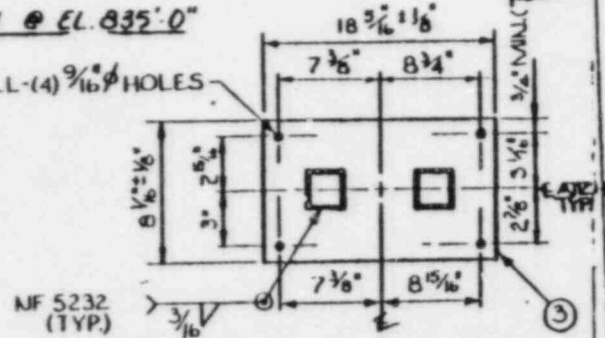
ITEM NO.	QTY REQ'D	MATERIAL	DESCRIPTION	PBS	L	W	THK	SEL	AISC
1	2	3X3X1/4X 20K TUBE	A500 GR.B.	X	X	X	X	X	X
2	2	3X3X1/4X 6W TUBE	A500 GR.B.	X	X	X	X	X	X
3	1	1/2" CGR PER SECT. A-A	SAS/ BASIS GR 65	X	X	X	X	X	X
4	4	1/2" X 7" HGTI-EMIR CONCRETE	ANCHORS	X	X	X	X	X	X

APPLY ONE COAT OF GALVALUME #11 TO ABOVE SURF EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE

REV	DESCRIPTION	DATE	DWR	CHKD	APPVD
1	VENDOR CERTIFICATION REF. QTH # 59740	~	~	~	~

MVTS.	
Y	0.006
	0.017

PLAN @ EL. 835'-0"  
FIELD DRILL-(4) 9/16" HOLES



**NOTE:**  
1) LOCKING DEVICES FOR HIGH STRENGTH BOLTS ARE NOT REQUIRED PER DCA 7607

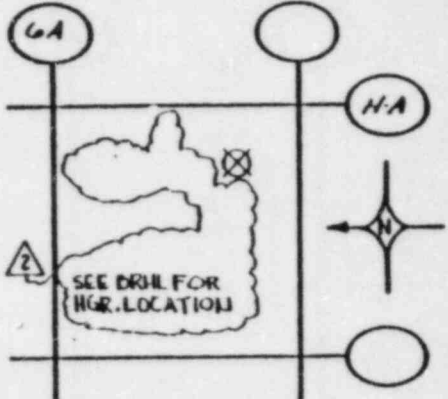
CTR LINE OF ATTACHMENT MAY VARY ± 1/4 INCH

**SECTION 'A-A'**

**PROBLEM # AD-166C**

ASME CODE EDITION: 1974  
ADDENDA: WINTER  
DESIGN SPEC: MS-46A

PR. CERTIFICATION



LOCATION PLAN

DATA PT	SUPPORT	LOADS (LBS)	PIPE WYER	PIPE UNCHEN
DESIGN	REVIEW	LEVEL	UNIT	
VERI.				
M-B				
E-W				

NOTE: AUTHORIZED NUCL. INSP. YES  NO   
ASME CODE CLASS 5

REF. DWGS	DRILL ISO	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	DWR	CHKD	APPVD
	CC-2-AB-031		MI-702	0	EL-701-02	3	2	REV AS NOTED, REV. DCA 10/21/81 (1) AS BUILT	12/7/81	CRH	J	RF
	FAB. ISO		STRUCTURAL		HVAC		1	REV'D AS NOTED, R.E. FHHS	11-30-81			
	CC-2-AB-031	0	8-718	3	MI-753	6	0	I.F.C.	12-27-79			

CPSES Brown & Root, Inc. ENGINEERS AND CONSTRUCTORS HOUSTON, TEXAS 35-1195

CLIENT: T.U.S.I.  
PLANT: COMANCHE PEAK  
JOB NO. 2323

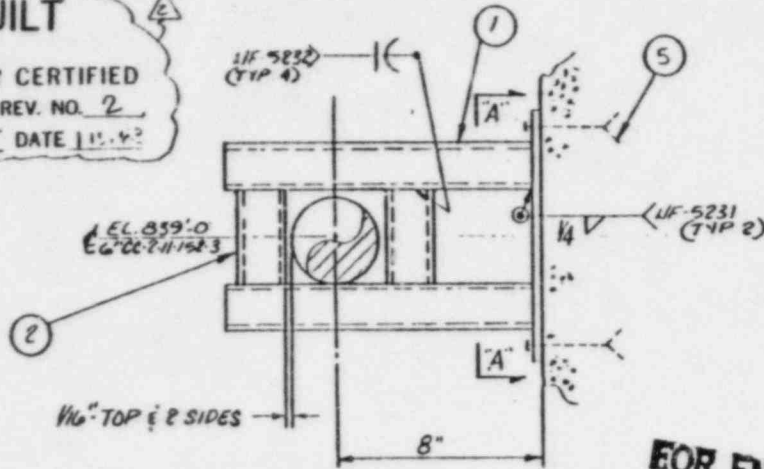
SUPPORT NO. CC-2-011-720-A13R  
SHEET 1 OF 1 REV. 2

**FOR OFFICE AND**

**ENGINEERING USE ONLY**

**AS-BUILT**

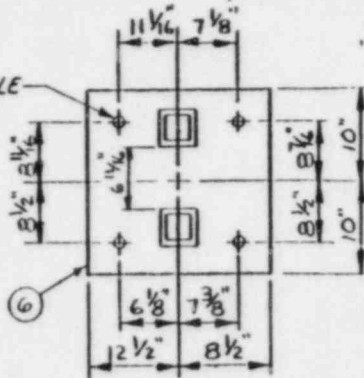
VENDOR CERTIFIED  
DRAWING REV. NO. 2  
BY: WLF DATE 11.15.79



ELEVATION LOOKING NORTH

FIELD DRILL  $1\frac{3}{8}$ "  $\phi$  HOLE (TYP 4)

NOTE:  
LOCKING DEVICES FOR  
HIGH STRENGTH BOLTS  
ARE NOT REQUIRED  
PER DCA 3502



SECTION "A-A"

**FOR ENGINEERING  
& OFFICE USE ONLY**

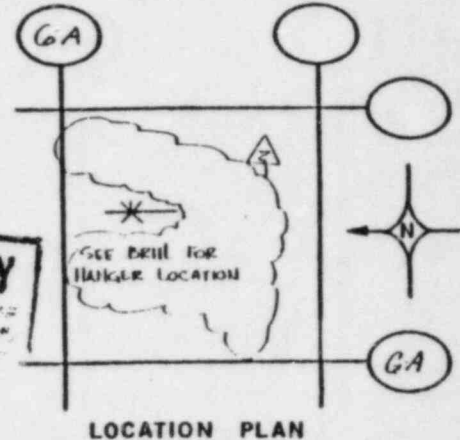
ITEM NO.	QTY REQ'D	MATERIAL	DESCRIPTION	PBS	CS	GR	SEC	AS
1	2	3X5X1/4X1.25" TUBE	A500 GR B.					
2	2	3X3X1/4X0.625" TUBE	A500 GR B.					
3	1	FL 10"	SA-36 SEE SECTION "A-A"	X				
4	4	3/4" X 3"	MULTI-KWIK CONCRETE ANCHOR		X			
5	4	3/4" X 7"	MULTI-KWIK CONCRETE ANCHOR		X			
6	1	C.S.R. 3/4" X 20" X 21"	SECT. A-A (SA 36/SA-515 GR 65)	X		X		

PAINT: CARBO ZINC #11

REV	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
A	VENDOR CERTIFICATION PER CPP, 8122	1/5/83	GLL	Q	CBD

PROBLEM \* AB-1-66c R.O.

ASME CODE EDITION: 1974  
ADDENDA: WINTER  
DESIGN SPEC: MS-46A



LOCATION PLAN

TO. 21100

DATA PT	SUPPORT	LOADS (LBS)	PIPE INVTS INCHES	BRHL ISO.	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	DWN.	APPVD.
208	DESIGN	INVERT LEVEL		CC-2 AB-031	0	M/C/D	0	E10102	23	1	REV AS BUILT, REF DCA 1607 (SEE REF. 1); WEHS,	6/11/81	DMH	WLF
VERT				FAB. ISO		STRUCTURAL		H.V.A.C		2	DESIGN, CHC-32932, AS-BUILT			
N-S				CC-2-A2-031	0	S/118	3	M10155	6	0	I.F.C.	12-20-79	C.A.T.	WLF
E-W														

NOTE: N, E, UP - S, W, OH	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>	ASME CODE CLASS 3
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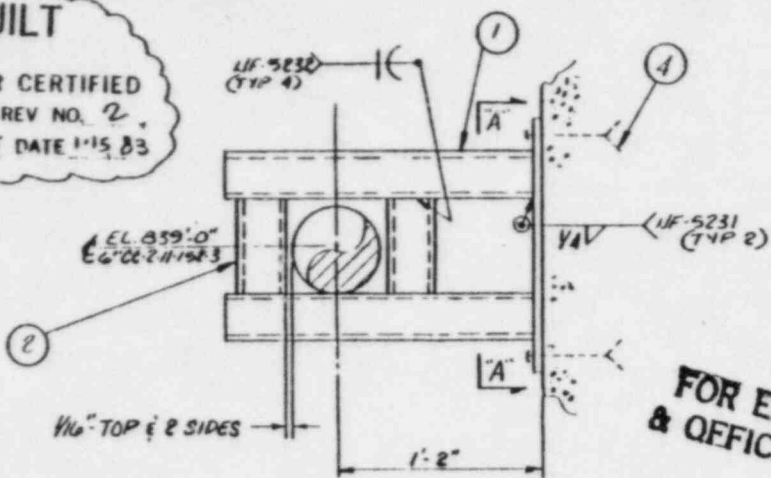
CPSES 35-1195	Brown & Root, Inc. ENGINEERS AND ARCHITECTS HOUSTON, TEXAS	CLIENT T.U.C.L.	PLANT COMMACHE PEAK	JOB NO. 2323	SUPPORT NO. CC-2-011-718-A53R	SHEET 1 OF 1 REV. 2
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**FOR OFFICE AND**

ENGINEERING DEPT. 10/24/79

AS-BUILT

VENDOR CERTIFIED  
DRAWING REV NO. 2  
BY: *[Signature]* DATE 1-15-83



FOR ENGINEERING & OFFICE USE ONLY

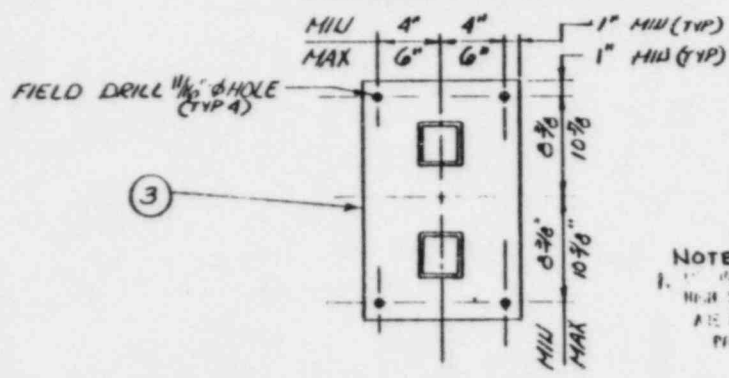
ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	P.B.S.	L.	C.S.	PRIM.	SEC.	AISC
1	2	3X3X1/4 X 1'-8 1/4" TUBE 4500 G.P.B.						
2	2	5X3X1/4 X 6 1/2" TUBE 4500 G.P.B.						
3	1	FL 3/8" SA-36 SEE SECTION "A-A"						
4	4	3/8" X 6" MULTI-KWIK CONCRETE ANCHORS						

REV	DESCRIPTION	DATE	OWN.	CHKD.	APPVD.
Δ	VENDOR CERTIFICATION, REF. GTN 59790	1/15/83	GL	Q	CB

APPLY 1/2" COAT OF ZINC RICH PAINT TO ABOVE PARTS EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE.

ELEVATION LOOKING NORTH



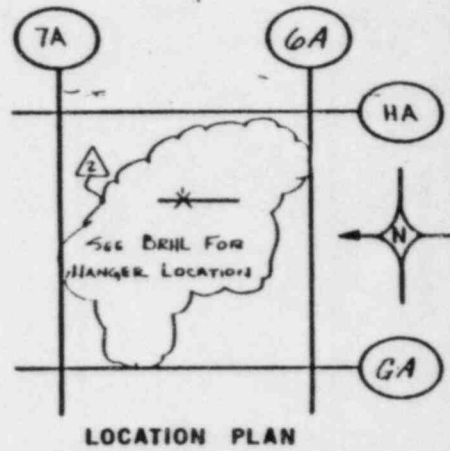
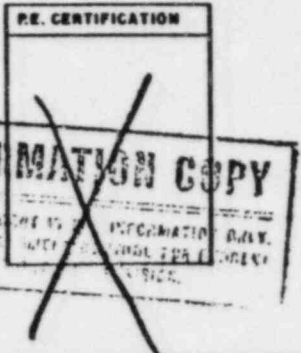
SECTION "A-A"



NOTE:  
1. ALL DIMENSIONS FOR HANGER SPACING SHALL BE NOT PERMITTED PER PIP 10-7

PROBLEM # AB-1-66C

ASME CODE EDITION: 1974  
ADDENDA: WINTER  
DESIGN SPEC: MS-46A



LOCATION PLAN

T.O. 21100

DATA PT	SUPPORT LOADS (LBS)	PIPE WYTS ONCHES	REF. DWGS	BRWL ISO	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	OWN	CHKD.	APPVD.
2086	DESIGN SERVICE LEVEL LIMITS		CC-2-AB-031	0	M/0702	0	E/0702	3	1	REV AS NOT'D, REF. DCA 7607 (SEE INT 1); WEM5	5-21-81	DMH	JW	PLM	
VERT.	-21.5	27.32	FAB. ISO	REV	STRUCTURAL	REV	H.V.A.C.	REV	REV	REV	WELDED PIPE & CHC 32942; AS-BUILT				
N-S			CC-2-AB-031	0	SQTAB	3	M/0755	6	0	I.F.C.	12-20-79	C.A.T.	W	M/11	
E-W															

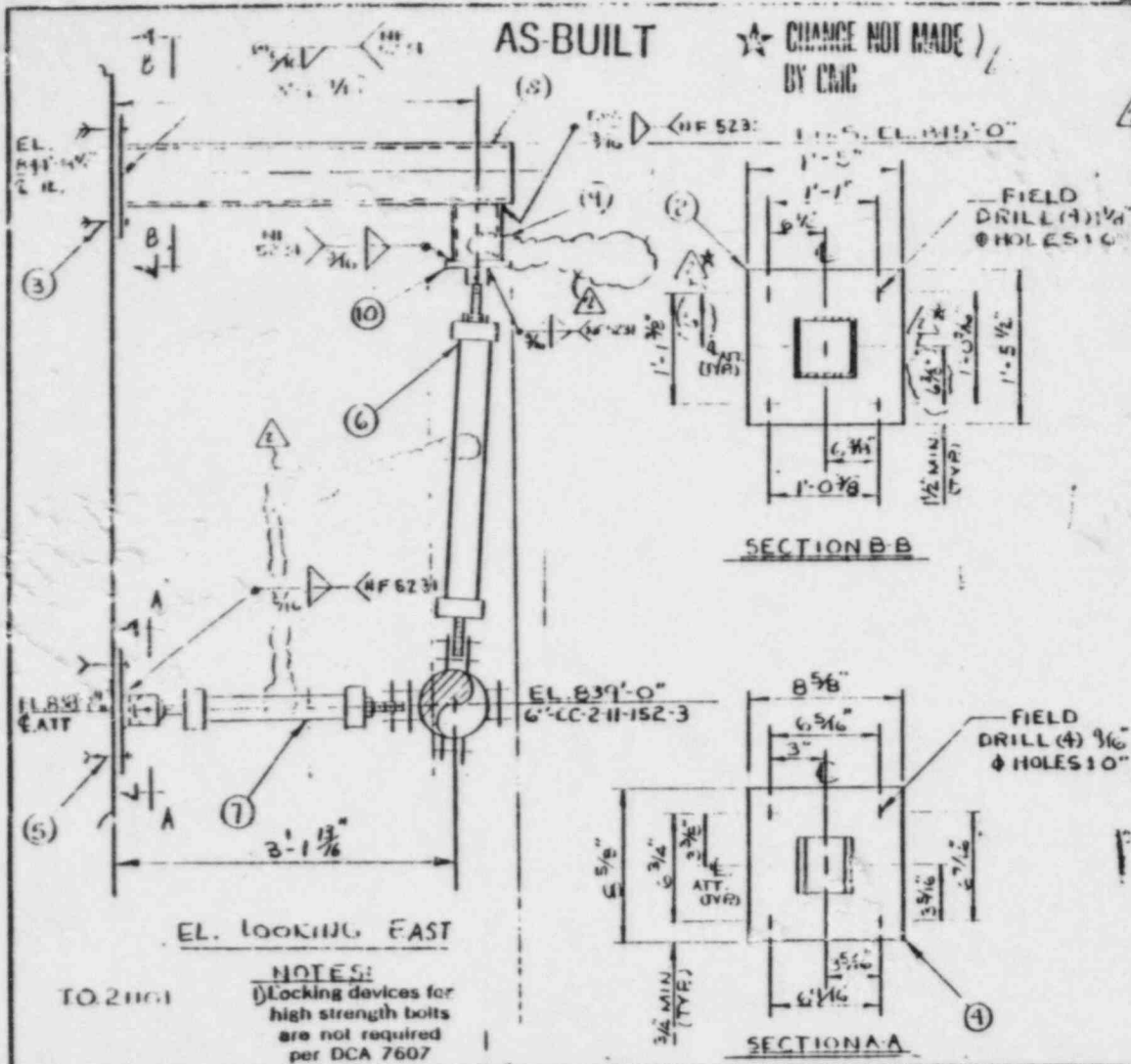
  

NOTE: N, S, UP - B, W, DN	AUTHORIZED NUCL. INSP. YES <input type="checkbox"/> NO <input type="checkbox"/>	ASME CODE CLASS <u>3</u>	CPSES 35-1195	Brown & Root, Inc. ENGINEERS AND ARCHITECTS HOUSTON, TEXAS	CLIENT: <u>T.U.S.I.</u>	PLANT: <u>COMANCHE PEAK</u>	JOB NO.: <u>2323</u>	SUPPORT NO.: <u>CC-2-011-717-A93R</u>	SHEET: <u>1</u> OF <u>1</u> REV. <u>2</u>
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FOR OFFICE AND



FOR OFFICE AND  
ENGINEERING USE ONLY



REV	QTY	MATERIAL	DESCRIPTION	PSS	...
1	1	1/2" SA-36	SEE SECTION F	X	X
2	1	1/2" SA-36	SEE SECTION F	X	X
3	4	1/2" HILTI KWIK CONCRETE ANCHOR		X	X
4	1	1/2" SA-36	SEE SECTION F	X	X
5	4	1/2" HILTI KWIK CONCRETE ANCHOR		X	X
6	1	SRS-08-PC	SRC-08-050	X	X
7	1	SRS-08-PC	SRC-09-060	X	X
8	1	...	...	Y	Y
9	1	...	...	Y	Y
10	1	...	...	Y	Y

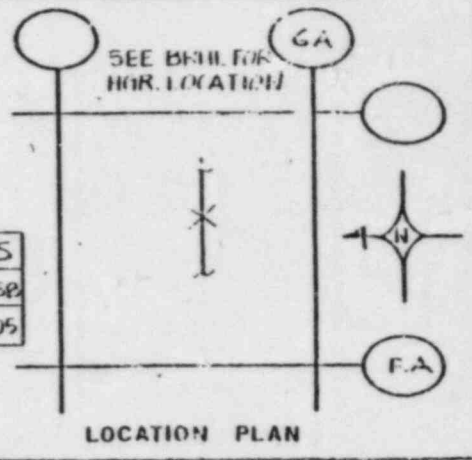
VENDOR CERTIFIED  
DRAWING REV. NO. 2  
BY [Signature] DATE 7/21/83

REV	DESCRIPTION	DATE	D.W.	CHECK	A.P.D.
1	VENDOR CERTIFICATION, GIN#59790	~	~	~	~
2	FIELD VENDOR CERTIFIED BY ICR, H. 7207	7/21/83	GLL	P.T.	Q

PROB: AB-1-CC-REV.  
ASME CODE EDITION: 1978  
ADDENDA: WINTER,  
DESIGN SPEC: H.S. - 46A



MV'S	10058
Z	0.105



DATA PT	SUPPORT	LOADS (LBS)	PIPE
2091	DESIGN	A	HT/2
VERT	...	...	...
N-S	...	...	...
E-W	...	...	...

NOTE: AUTHORIZED NUCL. INSP. YES  NO   
ASME CODE CLASS 3

REV	STRESS ISO	MECHANICAL	ELECTRICAL
1	M2-3231-23	M1-0702	E1-0702
2	BRHL-50	STRUCTURAL	HVAC
3	CC-2-AB-031	S-071B	M1-0755

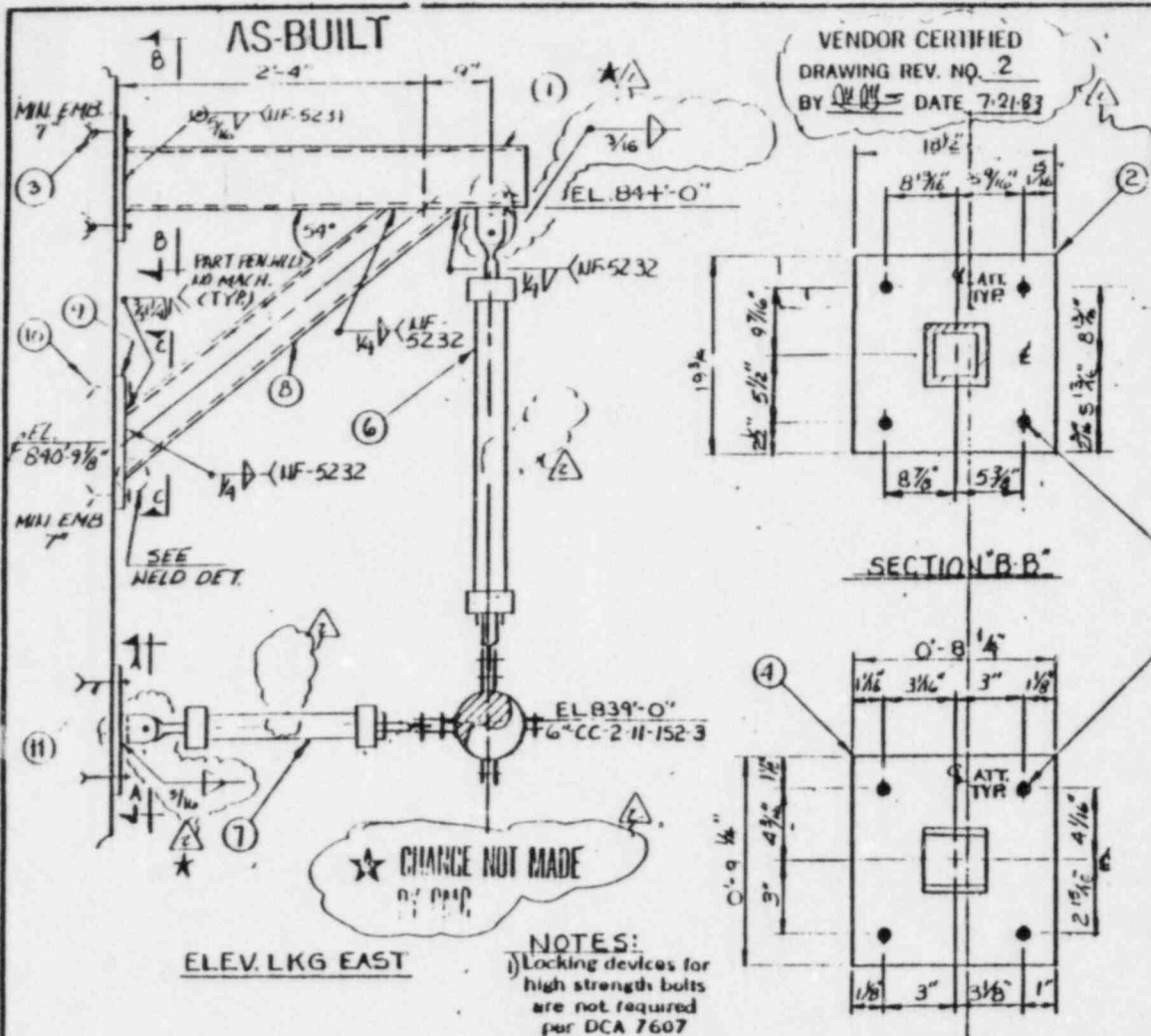
**Brown & Root, Inc.**  
ENGINEERS AND CONSTRUCTORS  
HOUSTON, TEXAS

REV	DESCRIPTION	DATE	D.W.	APPROV.
1	IFC	11-30-78	[Signature]	[Signature]
2	REVAS NOTED, NLE, CMC 36181, 31922	11/11/82	[Signature]	[Signature]
3	DCA 7607, SEE N71 AS BUILT			

CLIENT: T.U.S.I.  
PLANT: COMANCHE PEAK  
JOB NO: 2323

SUPPORT NO.	CC-2-011-115-A53R
SHEET	1 OF 1 REV. 2

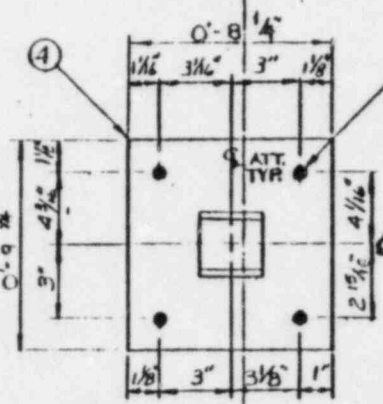
FOR OFFICE AND  
ENGINEERING USE ONLY



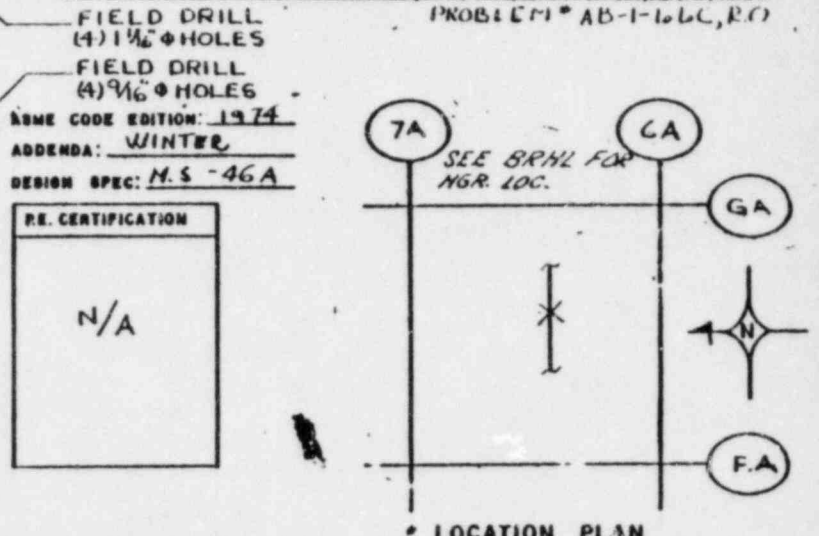
VENDOR CERTIFIED  
DRAWING REV. NO. 2  
BY *[Signature]* DATE 7-21-83

ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	P.B.S.	L	SS	MIN	SEC	AISC
1	1	T.S. C x C x 3/8 - 3-3/4" A-500, GR. B	X	X	X	X	X	X
2	1	R 1/4" SA-36, SEE SECTION 'B-B'	X	X	X	X	X	X
3	4	1" x 12" SUPER HILTI KWIK CONCRETE ANCHOR	X	X	X	X	X	X
4	1	R 1/2" SA-36, SEE SECTION 'A-A'	X	X	X	X	X	X
5	4	1/2" x 5 1/2" HILTI KWIK CONCRETE ANCHOR	X	X	X	X	X	X
6	1	SRS-08-PC SPC-08-060	X	X	X	X	X	X
7	1	SRS-08-PC SPC-08-060	X	X	X	X	X	X
7A	1	1 1/2" THICK G.G. PLATE PER SECT. B-B (SA-36 OR SA-515 OR SA-515 GR. 65)	X	X	X	X	X	X
7A	1	1" THICK C.S. PLATE PER SECT. A-A (SA-36 OR SA-515 GR. 65)	X	X	X	X	X	X
8	1	T.S. 5" x 5 1/2" x 4" x 10" LG. A-500 (W/PLATE TO SUIT)	X	X	X	X	X	X
9	1	1/2" THK. PER SECT. 'C-C' (SA-36 OR SA-515 GR. 65)	X	X	X	X	X	X
10	4	3/4" x 10" HILTI KWIK BOLTS	X	X	X	X	X	X
11	4	1/2" x 5 1/2" HILTI KWIK BOLTS	X	X	X	X	X	X
		FIELD DRILL (4) 1 1/2" HOLES						
		FIELD DRILL (4) 9/16" HOLES						
		NAME CODE EDITION: 1974						
		ADDENDA: WINTER						
		DESIGN SPEC: M.S. -46A						
		RE. CERTIFICATION						
		N/A						

SECTION 'B-B'



SECTION 'A-A'



DATA PT	SUPPORT LOADS (lbs)				PIPE WYTS (INCHES)
	DESIGN	A	B	C	
2073					
VERT.	-334	-1028	-1149	-1407	
	325	405	407		
H-S	-206A	-242B	-277C		
	1176	1731	1805		
H-W					+0.000
					0.000

NOTE: + H.E. AUTHORIZED NUCL. INSP. YES  NO   
- S.W. DN. ASME CODE CLASS

T.O. 21101

REV	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
0	IFC	10-14-79			
1	REV AS NTD. RE: CMC 7726 IR L DCA	11-19-81			
2	REV 7607 (SEE NOTE) AS BUILT				
3	REV VENDOR CERTIFICATION REV 612 4318				

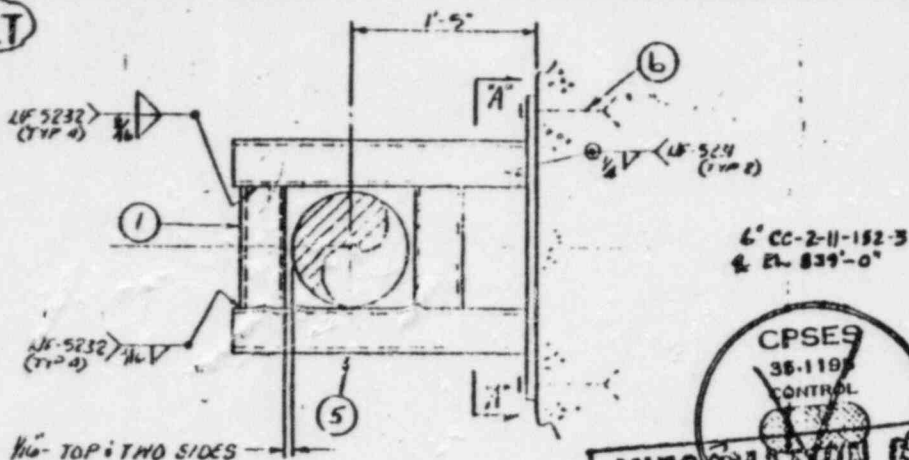
CPSES Brown & Root, Inc.  
ENGINEERS AND CONSTRUCTORS  
HOUSTON, TEXAS  
35-1125

REV	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
0	IFC	10-14-79			
1	REV AS NTD. RE: CMC 7726 IR L DCA	11-19-81			
2	REV 7607 (SEE NOTE) AS BUILT				
3	REV VENDOR CERTIFICATION REV 612 4318				

CLIENT TUSI  
PLANT COMANCHE PEAK  
JOB NO. 2323

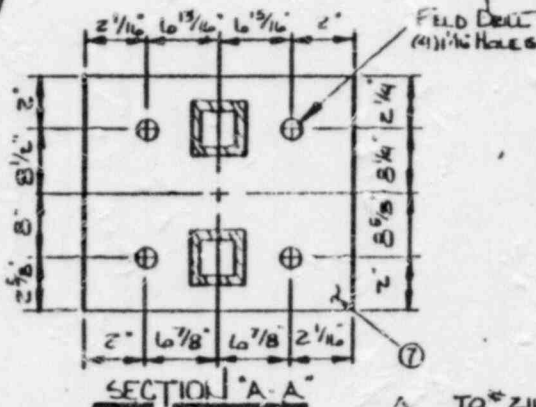
SUPPORT NO. CC-2-011-714-453R  
SHEET 1 OF 2 REV. 2

AS-BUILT



ELEVATION LOOKING NORTH

VENDOR CERTIFIED DRAWING REV. NO. 2 BY BH DATE 12-2-82



SECTION "A-A"

**CPSES**  
38-1197  
CONTROL  
**INFORMATION COPY**  
FOR ENGINEERING & OFFICE USE ONLY

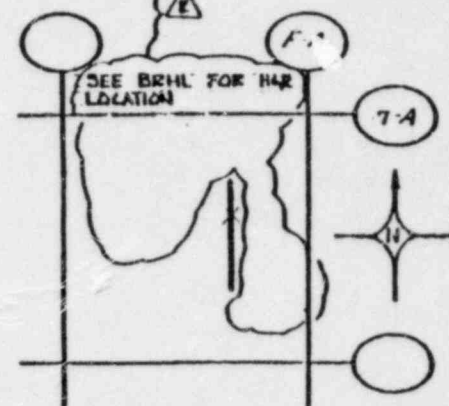
ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	P&S	U	W	SEC	AISC
1	2	XXXX 4X0'-6 3/4" WISE AS-BUILT					
2	2	XXXXXX-11					
3	7	XXXXXX-11					
4	2	XXXXXX-11					
5	2	1/4" X 4" X 4" TUBE STEEL I-11 LG (ASCOGRD)	X			X	
6	4	1" X 12" SUPER HILTS CONCRETE ANKERS				X	X
7	1	1X17 1/2" X 21 1/8" CS PLATE (SA515 GR 60 - SABL)	X			X	

DESCRIPTION	DATE	OWN	CHKD	AS-VD
VENDOR CERTIFICATION	12/16/82	RB	Q	ABD

ASME CODE EDITION: 1974  
ADDENDA: WINTER  
DESIGN SPEC: M-1-16A

RE. CERTIFICATION

PROBLEM = AB-1-66C R-O



LOCATION PLAN

DATA	SUPPORT LOADS (LBS)	PIPE NUTS (INCHES)	REF DWGS	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	LEN	CHKD	APPD
DESIGN	579	1 1/2"	CC-2-AB-32	1	M10752	5	E10111	12	1	REV AS-BUILT REF DWG 701 OF 111 WEM	12-20-81	RMB	WIP	CP
VERT	579	1 1/2"	FAB 150	1	80751	4	HVAC	REV	1	REV ENG TO TOR 2 (AS BUILT)	12-19-82	CAT	MG	MPD
H-S			CC-2-AB-033	1	80751	4	M10750	5	0	IFC				
E-W														

NOTE: AUTHORIZED NUCL. INSP. YES  NO   
ASME CODE CLASS: 2

**CPSEL**  
Brown & Root, Inc.  
HOUSTON, TEXAS

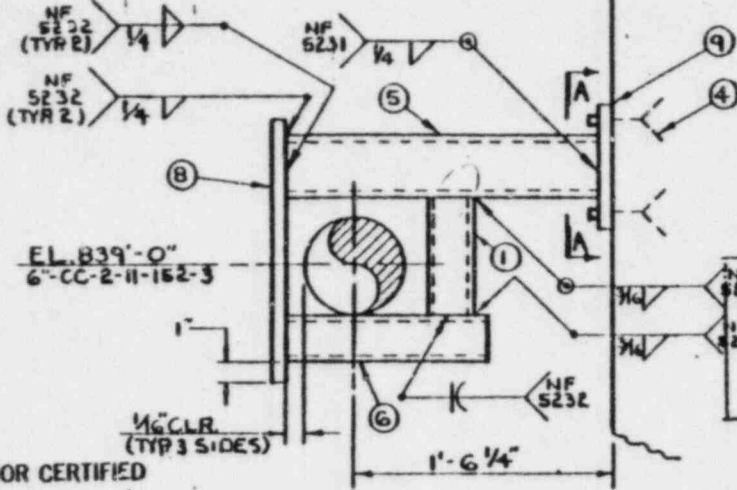
CLIENT: T.V.S.I.  
PLANT: COMBUSTION PEAK  
JOB NO.: 2323

SUPPORT NO. CC-2-0174-A53R  
SHEET 1 OF 1 REV. 3

FOR OFFICE AND

FOR ENGINEERING  
& OFFICE USE ONLY

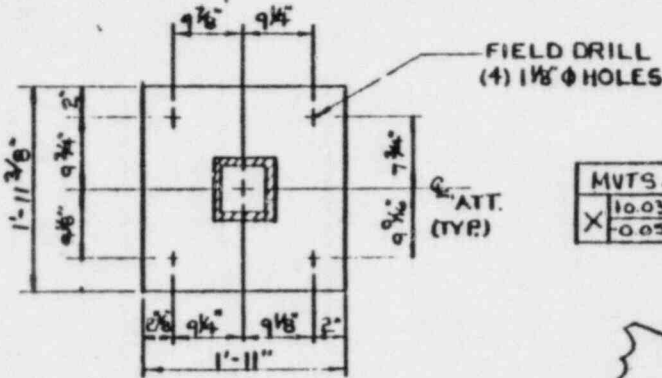
AS BUILT



EL. B39'-0"  
6-CC-2-11-152-3

VENDOR CERTIFIED  
DRAWING REV. NO. 1  
BY BH DATE 12/16/82

ELEV. VIEW LKG. NORTH



FIELD DRILL  
(4) 1 1/8" Ø HOLES

MVTS.
X 10.033
0.050

NOTES:  
Locking devices for high strength bolts are not required per DCA 7607

T.O. 21100

ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	REQ'D	ISSUED	REVISION	DATE	BY
1	1	T.S. 1/2" X 3" X 3" X 0'-6" LG. (A-500, GR. B)	X	X			
4	4	1" X 9" MULTI KWIK CONCRETE ANCHORS	X	X			
5	1	T.S. 1/4" X 6" X 6" X 2'-0" LG. (A-500, GR. B)	X	X			
6	1	FIELD TRIM TO SUIT					
7	1	T.S. 1/4" X 3" X 3" X 1'-2" LG. (A-500, GR. B)	X	X			
8	1	FIELD TRIM TO SUIT					
9	1	R. 1" X 8" X 1'-5" 1/4" LG. (SA-515 GR. 65 OR SA-36)	X	X			
9	1	R. 1" X 1'-11" X 1'-11" 3/4" LG. (SA-515 GR. 65 OR SA-36)	X	X			

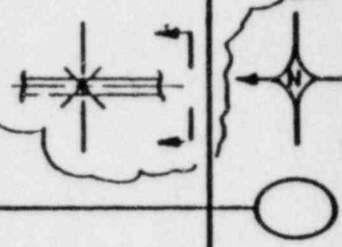
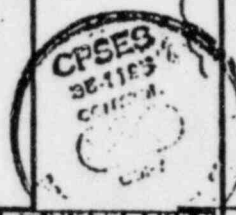
APPLY ONE COAT OF CARBO ZINC II TO ABOVE MATL EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE.

PROBLEM 18-1-66C/190

SEE BRILL FOR IGF LOCATION

ASME CODE EDITION: 1974  
ADDENDA: WINTER  
DESIGN SPEC: MS-46A

RE. CERTIFICATION



REV	DESCRIPTION	DATE	BY	CHKD	APP'D
1	GIN # 59790, AS BUILT				

LOCATION PLAN

DATA PT	SUPPORT LOADS (LBS)	PIPE HYDR. WEIGHT	REF DWGS	REV	MECHANICAL	REV	ELECTRICAL	REV	DESCRIPTION	DATE	OWN	CHKD	APP'D
2099	DESIGN	510	BRILL 150	1	MI-0702	8	EI-0711	9	REV AS NIP REF-CMC 9294 R 4, DCA 707	12/19/79	IB	J	AC
VER 1			FAB. 150	REV	STRUCTURAL	REV	H.V.A.C.	REV	SEE NIP VENDOR CERTIFICATION (SEE ABOVE)				
8-1			CC-2-AB-032	1	S-0721	4	MI-0756	5	IFC	12/19/79	C.A.T.	WA	AM

NOTE: AUTHORIZED NUCL. INSP. YES  NO   
ASME CODE CLASS 3

CPSES Brown & Root, Inc  
ENGINEERS AND CONTRACTORS  
HOUSTON, TEXAS  
35-195

CLIENT T.U.S.I.  
PLANT COMANCHE PEAK  
JOB NO. 2323

SUPPORT NO. CC-2-011-712-A228  
SHEET 1 OF 1 REV. 1

FOR OFFICE AND

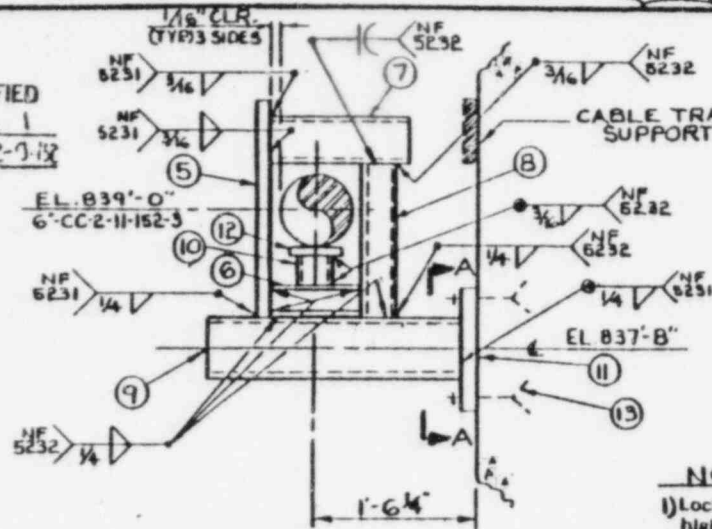
ENGINEERING USE ONLY

AS BUILT

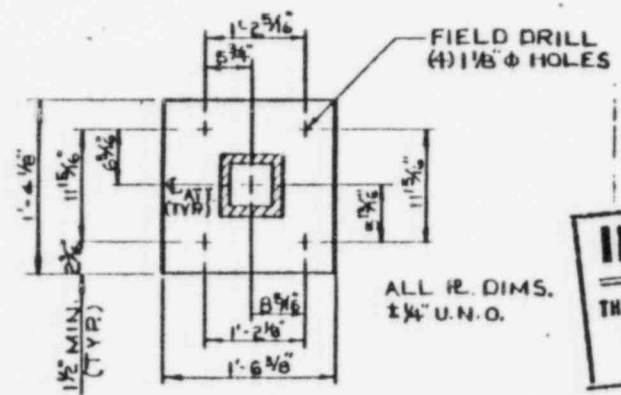
VENDOR CERTIFIED

DRAWING REV. NO. 1

BY PJ DATE 12-9-82



ELEV. LKG NORTH



SECTION A-A

**NOTES**

1) Locking devices for high strength bolts are not required per DCA 7607

T.O. 21100

ITEM NO	QTY REQ'D	MATERIAL DESCRIPTION	PBS	J	IS	PRINT	SEC	AISC
5	1	1" x 4 1/2" x 1/8" U.S. C.S.P. (SA-36 OR SA-515, GR. 65)	X					
6	1	W.G.Y. 12 x 0'-6 3/4" L.G. (SA-36)	X					
7	1	T.S. 1/4" x 4" x 4" x 0'-11" L.G. (A-500, GR. B)	X					
8	1	T.S. 1/4" x 4" x 4" x 1'-4 1/2" L.G. (A-500, GR. B)	X					
9	1	T.S. 1/4" x 6" x 6" x 0'-0 1/2" L.G. (A-500, GR. B)	X					
10	1	T.S. 1/4" x 3" x 3" x 0'-0 1/2" L.G. (A-500, GR. B)	X					
11	1	1" THK. C.S.P. / SECT. A (SA-36 OR SA-515, GR. 65)	X					
12	1	1" x 4" x 4" L.G. C.S.P. (SA-36 OR SA-515, GR. 65)	X					
13	4	1" φ x 9" L.G. HILTI KWIK CONCRETE ANCHORS						

APPLY ONE COAT OF CARBO ZINC #11 TO ABOVE MATE EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE.

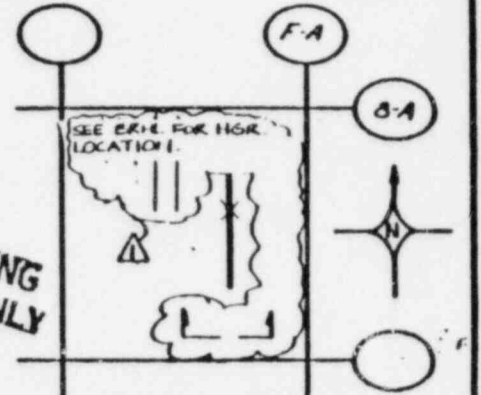
REV	DESCRIPTION	DATE	BY	CHKD.	APPD.
1	VENDOR CERT. REF. GTN # 52790				

PROB. # AB-1-66C, R-0

ASME CODE EDITION: 1974  
 APPENDIX: WALTER  
 DESIGN SPEC: HS-46A

**INFORMATION COPY**  
 THIS DOCUMENT IS FOR INFORMATION ONLY.  
 CONTACT BROWN & ROOT FOR CURRENT STATUS AND REVISION.

PER CERTIFICATION  
**FOR ENGINEERING & OFFICE USE ONLY**



LOCATION PLAN

DATA PT	SUPPORT	LOADS (LBD)	PIPE	REV	DESCRIPTION	DATE	DWR	CHKD.	APPVD.
R/OI	DESIGN	DESIGN	DESIGN	1	MI-0702	8/11/82	EWY	G	CRD
VERT	DESIGN	DESIGN	DESIGN	1	MI-0711	12/10/82	EWY	G	CRD
M-B	DESIGN	DESIGN	DESIGN	1	MI-0711	12/10/82	EWY	G	CRD
E-W	DESIGN	DESIGN	DESIGN	1	MI-0711	12/10/82	EWY	G	CRD

NOTE	AUTHORIZED NUCL. IMP. YES <input type="checkbox"/> NO <input checked="" type="checkbox"/>
ASME CODE CLASS	3

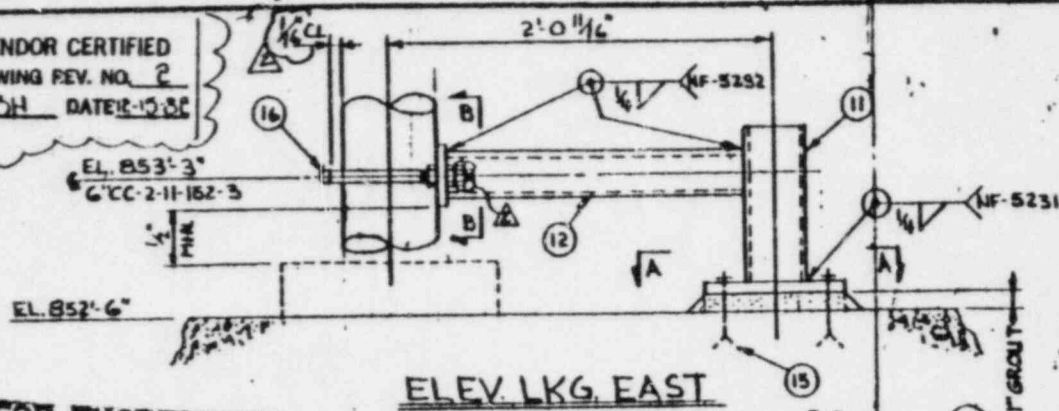
  

CLIENT	T.U.S.I.
PLANT	COMANCHE PEAK
JOB NO.	2323

SUPPORT NO.	CC-2-01711-A31R
SHEET	1 OF 1 REV. 1

VENDOR CERTIFIED  
DRAWING REV. NO. 2  
BY PH DATE: 1-2-82

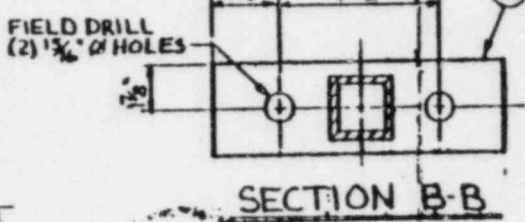
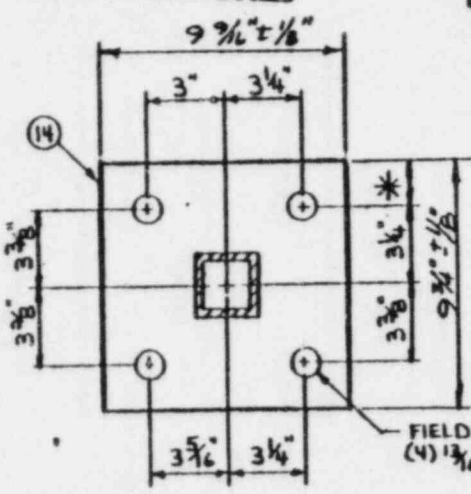


ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	PKS	LS	HT	WT	SEL	ASIS
1	1	PH-060						
2	1	2\"/>						
3	1	2\"/>						
4	1	1/2\"/>						
5	2	1/2\"/>						
11	1	T.S. 4x4 x 1/4 x 10\"/>						
12	1	T.S. 3x3 x 1/4 x 11 7/8\"/>						
13	1	C.S. 2\"/>						
14	1	C.S. 2\"/>						
15	4	3/4 x 7\"/>						
16	1	PH-060 U-BOLT						

APPLY ONE COAT OF CARBO ZINC #11 TO ABOVE WARE EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE.

REV	DESCRIPTION	DATE	OWN	CHKD	APPVD
A	VENDOR CATEGORICAL BIDDING	1/17/82	GLL	Q	CRD

FOR ENGINEERING & OFFICE USE ONLY



PROBLEM #10-1-CCC R/O

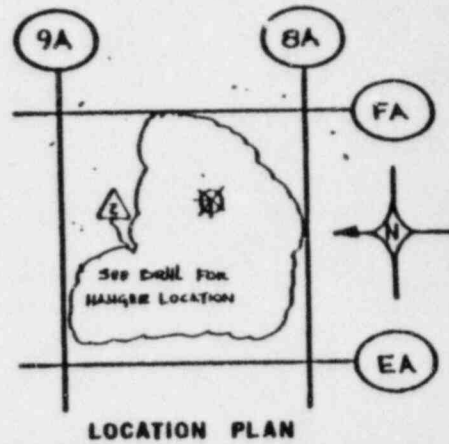
ASME CODE EDITION: 1974  
ADDENDA: WINTER  
DESIGN SPEC: HS-46A

RE. CERTIFICATION  
N/A

NOTE:  
1. LOCKING DEVICES FOR HIGH STRENGTH BOLTS SHALL NOT BE USED

THIS DOCUMENT IS FOR CONTACT EQUITY CURRENT ONLY

CONTROL CENTER



PK #11 \* EDGE DISTANCE ≥ 1/2\"/>

DATA PT	SUPPORT	LOADS (LBS)	PIPE	REF. DMSB	BRHL 180	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	OWN	CHKD	APPVD	
2107	DESIGN	1000	1/2\"/>														
VERT					CC-2-10-032	1	H-0701	6	21-0710-01	7	0	IPC	1/1/82	PH	Q	PH	
H-S					FAB 180	REV	STRUCTURAL	REV	H.V.A.C.	REV	1	REV AS HD, REF. CHG 42677R.24	6/1/81	DMH	RKT	PH	
E-W					CC-2-10-032	1	S-0728	2	H-0728	4	1	REV DCA 7607 (MT.1) AS BUILT					

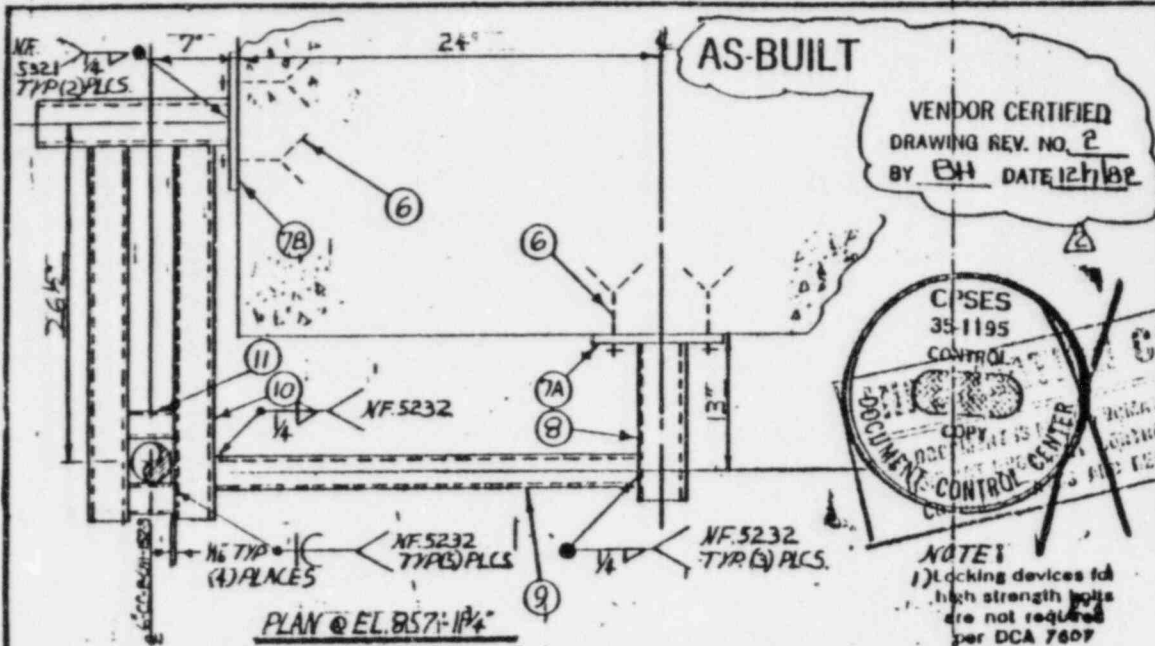
NOTE: AUTHORIZED NUCL. INSP. YES  NO   
ASME CODE CLASS 3

Brown & Root, Inc.  
HOUSTON, TEXAS

CLIENT: T.U.S.I.  
PLANT: COMANCHE PEAK  
JOB NO. 2323

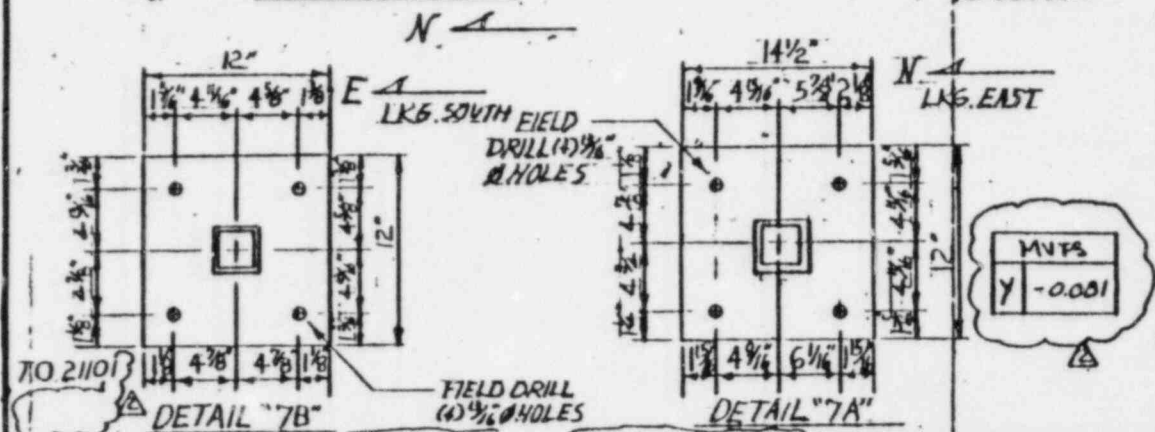
SUPPORT NO. CC-2-011-708-A63A  
SHEET 1 OF 1 REV. 2

FOR OFFICE AND ENGINEERING USE ONLY



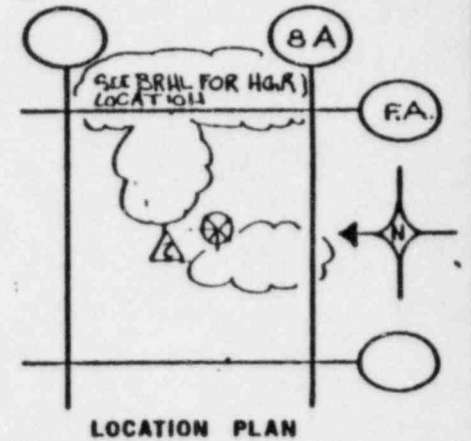
ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	PBS	L	CS	W	SEC	AISC
1	2	2" X 2" X 1/4" L.G. 7.5 (1500 GR. B)			X	X	X	
2	2	2" X 2" X 1/4" L.G. 7.5 (1500 GR. B)			X	X	X	
3	2	2" X 2" X 1/4" L.G. 7.5 (1500 GR. B)			X	X	X	
4	2	2" X 2" X 1/4" L.G. 7.5 (1500 GR. B)			X	X	X	
5	2	2" X 2" X 1/4" L.G. 7.5 (1500 GR. B)			X	X	X	
6	8	1/2" X 7" HILTI KWIK BOLT			X	X	X	
7A	7	1/2" R SEE DTL 7A (SA-36 OR SA515)	X				X	
7B	7	1/2" R SEE DTL 7A (SA-36 OR SA515)	X				X	
8	2	3" X 3" X 1/4" L.G. 7.5 (1500 GR. B)		X			X	
9	2	2" X 2" X 1/4" L.G. 7.5 (1500 GR. B)		X			X	
10	2	2" X 2" X 1/4" L.G. 7.5 (1500 GR. B)		X			X	
11	2	2" X 2" X 1/4" L.G. 7.5 (1500 GR. B)		X			X	

REV	DESCRIPTION	DATE	OWN	CHKD	APPRD
1	VENDOR CERTIFICATION, REF. GTW 59790	12/1/82	JD	Q	PLS



ASME CODE EDITION: 1974  
 ADDENDA: WINTER  
 DESIGN SPEC: MS-46A

RE. CERTIFICATION  
 N/A  
 FOR ENGINEERING  
 & OFFICE USE ONLY



DATA PT	SUPPORT	LOADS	(L&D)	PIPE
210B	DESIGN	REVIEW	LEVEL	WYTP
VERT.				DCHEN
H-B				
E-W				

BRHL 160	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	OWN	CHKD	APPRD
CC-2-AR-032	0	M-0701	6	E1-0710-01	17	Q	IFC	11/30/79			
FAB. 150	REV	STRUCTURAL	REV	H.V.A.S.	REV		REV DASH/D REF CMC 33446 R11/10/82 20/25 S.W.L				
CC-2-AB-032	1	S-072B	2	M-075B	4		IDEA 7607 (CENT.) W/ WENT AS BUILT				

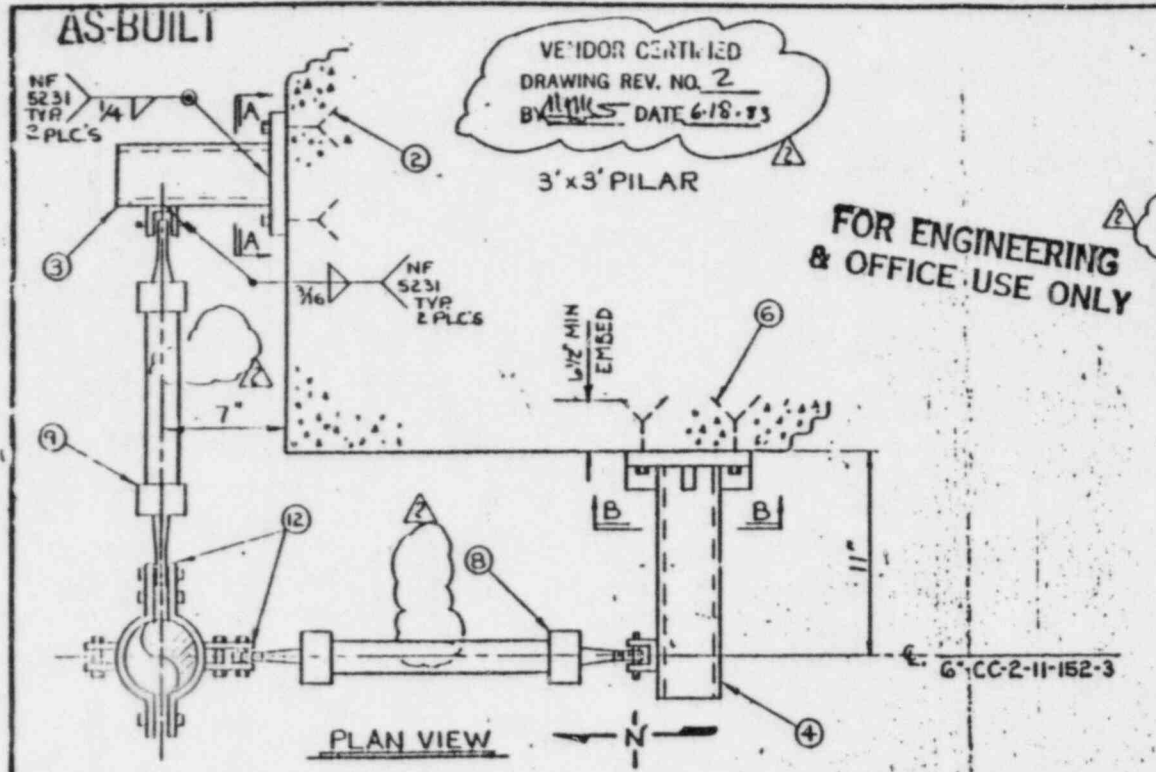
CPSES  
 Brown & Root, Inc.  
 HOUSTON, TEXAS  
 35-1195

CLIENT: T.U.S.I.  
 PLANT: COMANCHE PEAK  
 JOB NO.: 2323

SUPPORT NO.: CC-2-011-707-AG3A  
 SHEET 1 OF 1 REV. 2

FOR OFFICE AND  
 ENGINEERING USE ONLY

FOR OFFICE AND  
ENGINEERING USE ONLY

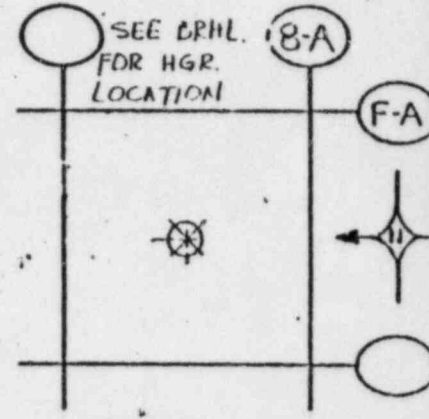


ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	PAS	L	CS	MS	FR
2	4	3/4"x7" HILTI KWIK CONCRETE ANCHORS			X		
3	1	T.S. 1/4"x3"x3" x 8 1/4" LG. (A-500-740, GR. B)	X			X	
4	1	T.S. 1/4"x3"x3" x 1'-2 1/4" LG. (A-500-740, GR. B)	X			X	
6	4	5/8"x8 1/2" HILTI KWIK CONCRETE ANCHORS			X		
7	4	1/2"x4"x3 1/4" LG. STIFFENER PLATE (SA-36 OR SA-515 GR. 65)	X			X	
8	1	SRF-08-R0 SWAY STRUT				X	
9	1	SRF-08-R0 SWAY STRUT				X	
10	1	3/4" C.S. PLATE PER SECT. A-A (SA-36 OR SA-515, GR. 65)	X			X	
11	1	3/4" C.S. PLATE PER SECT. B-B (SA-36 OR SA-515, GR. 65)	X			X	
12	2	SPC-08-060 C.S. PIPE CLAMP (SA-36 OR SA-515, GR. 65)	X			X	

REV	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
2	REV. WITHOR CLEARANCE REF ITR 11-87-72	7/2/73	SL	RL	PLM

ASME CODE EDITION: 1974  
ADDENDA: WINTER  
DESIGN SPEC: MS-46A

RE. CERTIFICATION  
N/A



NOTES:  
Locking devices for high strength bolts are not required per DCA 7607  
T.O. 21101



**INFORMATION COPY**  
THIS DOCUMENT IS FOR OFFICE USE ONLY.  
DO NOT BE USED FOR CONSTRUCTION.

PROCS AS-166 RD

DATA PT	SUPPORT LOADS (LBS)	PIPE NUTS ANCHORS
2109	DESIGN SERVICE LEVEL LIMITS	005 (100) 005 (100)
VERT.		
N-S		
E-W		

NOTE: AUTHORIZED NUCL. INSP. YES  NO   
ASME CODE CLASS 3

REF. DWGS	BRHL. ISO.	REV	MECHANICAL	REV	ELECTRICAL	REV	DESCRIPTION
CC-2-AB-052		1	MI-0701	6	EI-0710-01	7	0 I.F.C.
	FAB. ISO.	REV	STRUCTURAL	REV	H.V.A.C.	REV	
CC-2-AB-032		2	S-0728	2	MI-075A	4	REV. AS NOTED REF SMC 25157X30K70963 (CON DIA X 07 (CENT)) ADDED SHRT AS BUILT (CON) W/DR CERTIFICATION REF SMC 247150

Brown & Root, Inc.  
ENGINEERING AND CONSTRUCTION  
HOUSTON, TEXAS  
26-1105

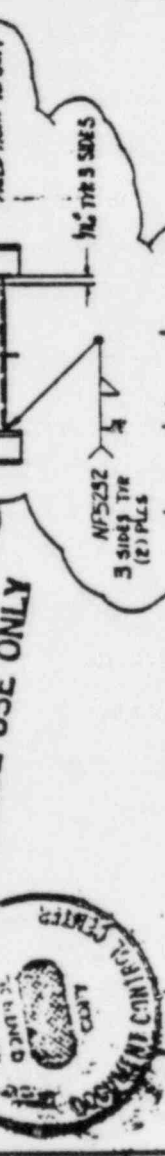
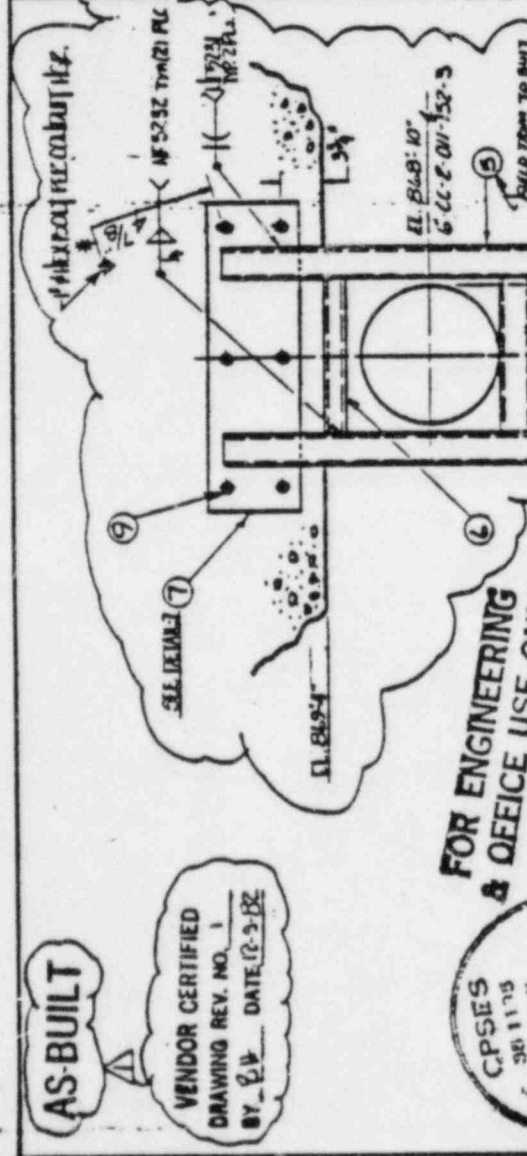
CLIENT T.U.  
PLANT COMANCHE PEAK  
JOB NO. 2323

SUPPORT NO. CC-2-011-706-A6-5R  
SHEET 1 OF 2 REV. 2



ITEM NO.	QTY. REQ'D.	MATERIAL DESCRIPTION
1	2	TS 1/2" x 1/2" x 1/2" A-308 GRB
2	2	TS 3/4" x 1/2" x 1/2" A-308 GRB
3	1	CS 1/2" (SEE DET.) SA 515 GR 65/15A-36
4	6	MULTI RIVET BOLTS 3/4" x 1/2"

REV.	DESCRIPTION	DATE	BY	CHKD.	APPVD.
1	AS-BUILT				



ASME CODE SECTION: **III**  
 APPENDIX: **VI**  
 DESIGN SPEC: **MS-4CA**

**AS-BUILT**

**PROCESSED AB-1-66-C-RO**

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 CONTACT DOCUMENT CONTROL FOR  
 CURRENT STATUS AND REVISIONS.

DATE	BY	CHKD.	APPVD.
9/20/79	M.H.M.	M.C.	
4/24/82	R.B.		

DATA PT.	SUPPORT	LOADS (lbs)	PIPE	WAVE	INCHES
7229	DESIGN	VERT.	DESIGN	DESIGN	DESIGN

REV.	DESCRIPTION	DATE	BY	CHKD.	APPVD.
1	REV. AS-BUILT REF. OME 2-10-82	2-10-82	R.B.		
2	REV. AS-BUILT REF. OME 2-10-82	2-10-82	R.B.		

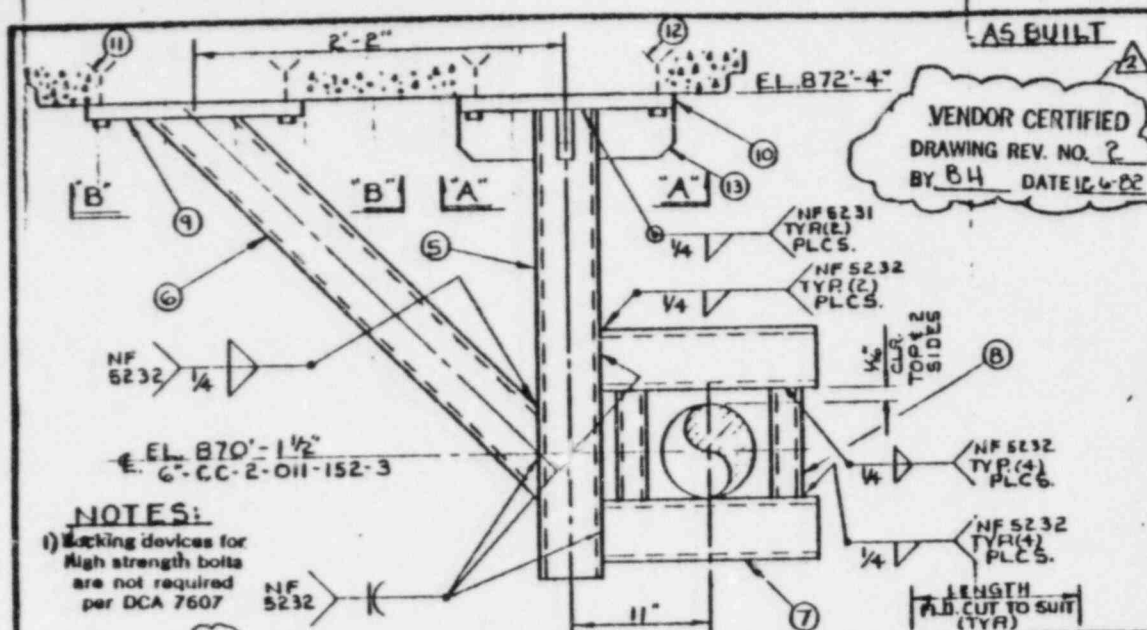
REV.	DESCRIPTION	DATE	BY	CHKD.	APPVD.
1	REV. AS-BUILT REF. OME 2-10-82	2-10-82	R.B.		
2	REV. AS-BUILT REF. OME 2-10-82	2-10-82	R.B.		

CLIENT: **U.S.I.**  
 PLANT: **COMANCHE PEAK**  
 JOB NO.: **2323**

**Brown & Root, Inc.**  
 HOUSTON, TEXAS

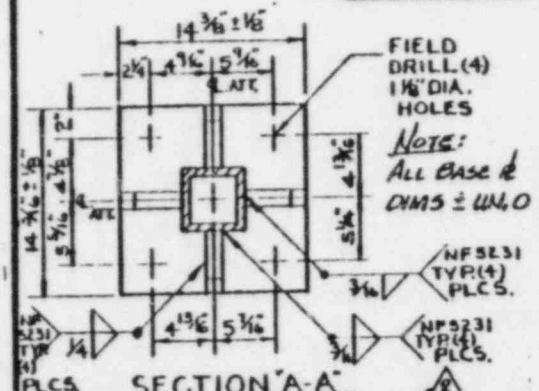
SUPPORT NO. **CC-E-11-702-A-3R**  
 SHEET **1** OF **1** REV. **1**



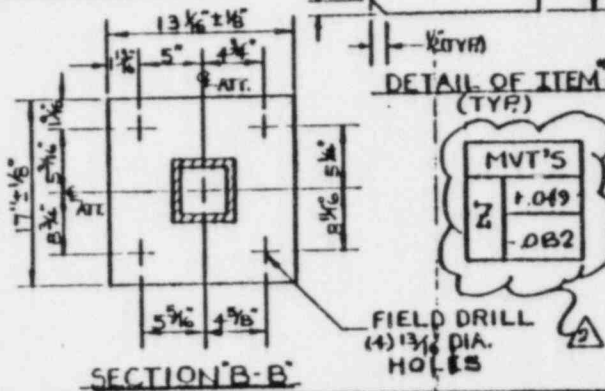
**NOTES:**  
 1) Backing devices for high strength bolts are not required per DCA 7607

T.O. 21101

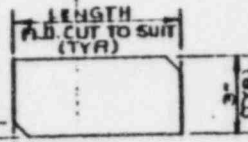
**ELEVATION LOOKING WEST**



**SECTION A-A**



**SECTION B-B**



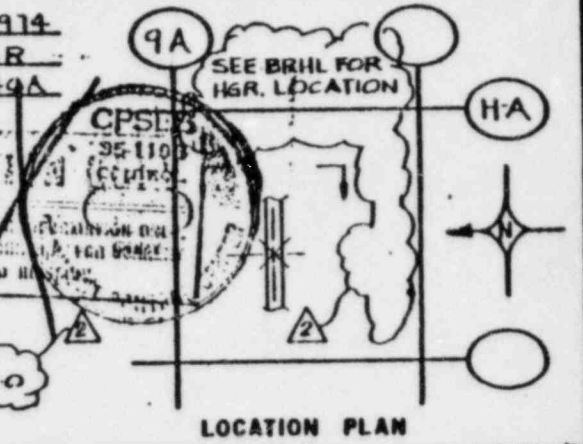
**DETAIL OF ITEM 13 (TYR)**

ITEM NO.	QTY REQD	MATERIAL DESCRIPTION	ABS	1	2	3	4	5	6
5	1	T.S. 1/4" X 4" X 4" X 2'-9 1/2" LG. (A-500, GR. B)							
6	1	T.S. 1/4" X 4" X 4" X 3'-8" LG. (A-500, GR. B)							
7	2	T.S. 1/4" X 4" X 4" X 1'-2 1/2" LG. (A-500, GR. B)							
8	2	T.S. 1/4" X 2" X 2" X 0'-6 1/4" LG. (A-500, GR. B)							
9	1	3/4" THK. C.S. PLATE PER SECT. B-B (SA-515 GR. 65 OR SA-36)							
10	1	3/4" THK. C.S. PLATE PER SECT. A-A (SA-515 GR. 65 OR SA-36)							
11	4	3/4" Ø X 10" LG. HILTI KWIK CONCRETE ANCHORS							
12	4	1" Ø X 12" LG. HILTI KWIK CONCRETE ANCHORS							
13	4	1/2" THK. C.S. PLATE (SA-36 OR SA-515 GR. 65) X 0'-3" WIDE X LENGTH TO BE FURNISHED BY FIELD							

REV	DESCRIPTION	DATE	OWN	CHKD	APPR
1	VENDOR CERTIFICATION, RET. GIN 39790	12/6/02	J	KE	HW

ASME CODE EDITION: 1914  
 ADDENDA: WINTER  
 DESIGN SPEC: MS-49A

**ASME CERTIFICATION**  
 CPSES 35-110  
 PROB # AB-146-R-D



DATA PT	SUPPORT	LOADS (LBS)	PIPE
		LIMIT	WYTS
2122	DESIGN		INCH
VERT.			
N-S			
E-W			

REF. DWGS	STRESS ISO.	REV.	MECHANICAL	REV.	ELECTRICAL	REV.
2	CC-2-AB-03E	1	S-0735	2	MI-0757	4

**CPSES**  
 Brown & Root, Inc.  
 HOUSTON, TEXAS

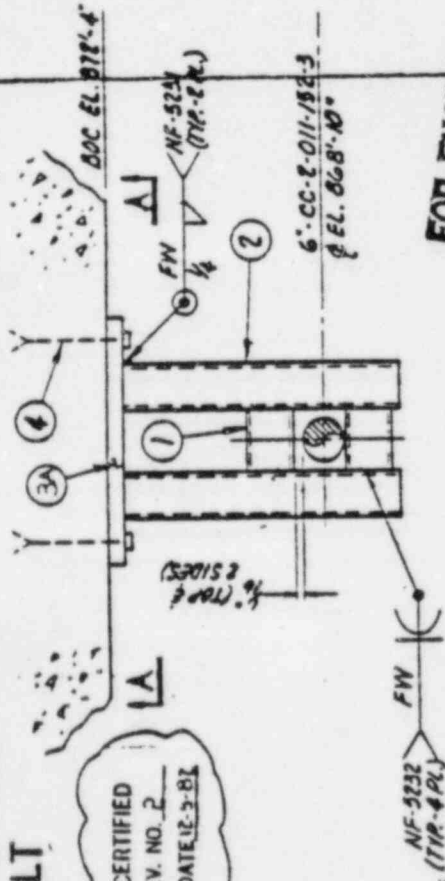
CLIENT: T.U.S.I.  
 PLANT: COMANCHE PEAK  
 JOB NO. 2323

SUPPORT NO. CC-2-11-701-A63R  
 SHEET 1 OF 1 REV. 2

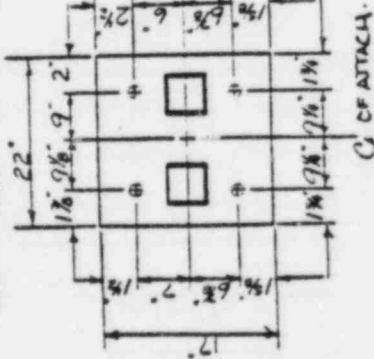
**FOR ENGINEERING OFFICE USE ONLY**  
**ENGINEERING USE ONLY**

**AS-BUILT**

VENDOR CERTIFIED  
DRAWING REV. NO. 2  
BY DW DATE 12-3-81



ELEVATION LOOKING EAST



NOTES:  
1) LOCKING DEVICES FOR HIGH STRENGTH BOLTS ARE NOT REQUIRED PER DCA 7407

T.O. 2/100

FOR ENGINEERING & OFFICE USE ONLY



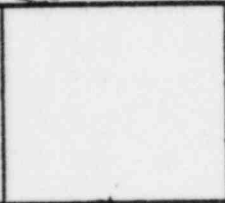
ITEM NO	QTY REQD	MATERIAL DESCRIPTION
1	2	4" x 4" x 1/2" GALV TUBE A-500-GR-B
2	2	4" x 4" x 1/2" GALV TUBE A-500-GR-B
3A	1	1/4" CS. R. PER SECTION A-A (EA. 20" x 2" x 5/8" GR. 5)
4	4	1/2" x 5/8" MULTI THREAD CONCRETE ANCHORS

APPLY ONE COAT OF EPOXY JUNG-811 TO ABOVE MALL EXCEPT INSURAGE WHICH SHOULD BE TREATED WITH A SUITABLE POLYURETHANE.

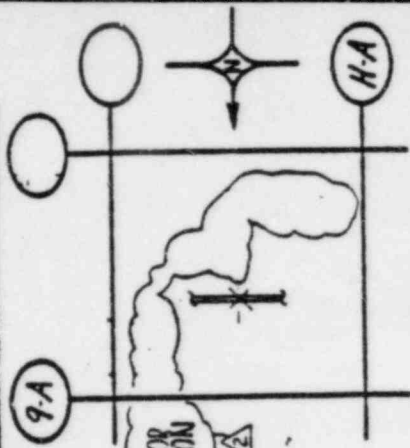
REV	DESCRIPTION	DATE	BY	CHKD.	APP'D.
1	VENDOR CERTIFICATION REF. C/N# 53750 5268	JF-10	G		CBD

ASME CODE SECTION: 1914  
ADDRESS: MINTEA  
DESIGN SPEC: MS-46A

PER CERTIFICATION



PROBLEM# AD-166C-PO



LOCATION PLAN

DATA PT	SUPPORT	LOADS	PIPE	DESIGN	REV	MECHANICAL	ELECTRICAL	REV	DESCRIPTION	DATE	OWN	CHRG	APPT
Z124	CC-2-A11-032	FAB 130	CC-2-A11-032	REV 1	MECHANICAL	REV 6	ELECTRICAL	REV 6	1 FC	9-28-79	W/M/K/E		
VERT	CC-2-A8-032	FAB 130	CC-2-A8-032	REV 1	STRUCTURAL	REV 8	H.V.A.C.	REV 1	REV AS MTD. REF. CMC 45430 R2	6-19-81	BT		
E-S									1 DIAL. EMB. 1-b. DCA 7407 (45430 R2) ONT				

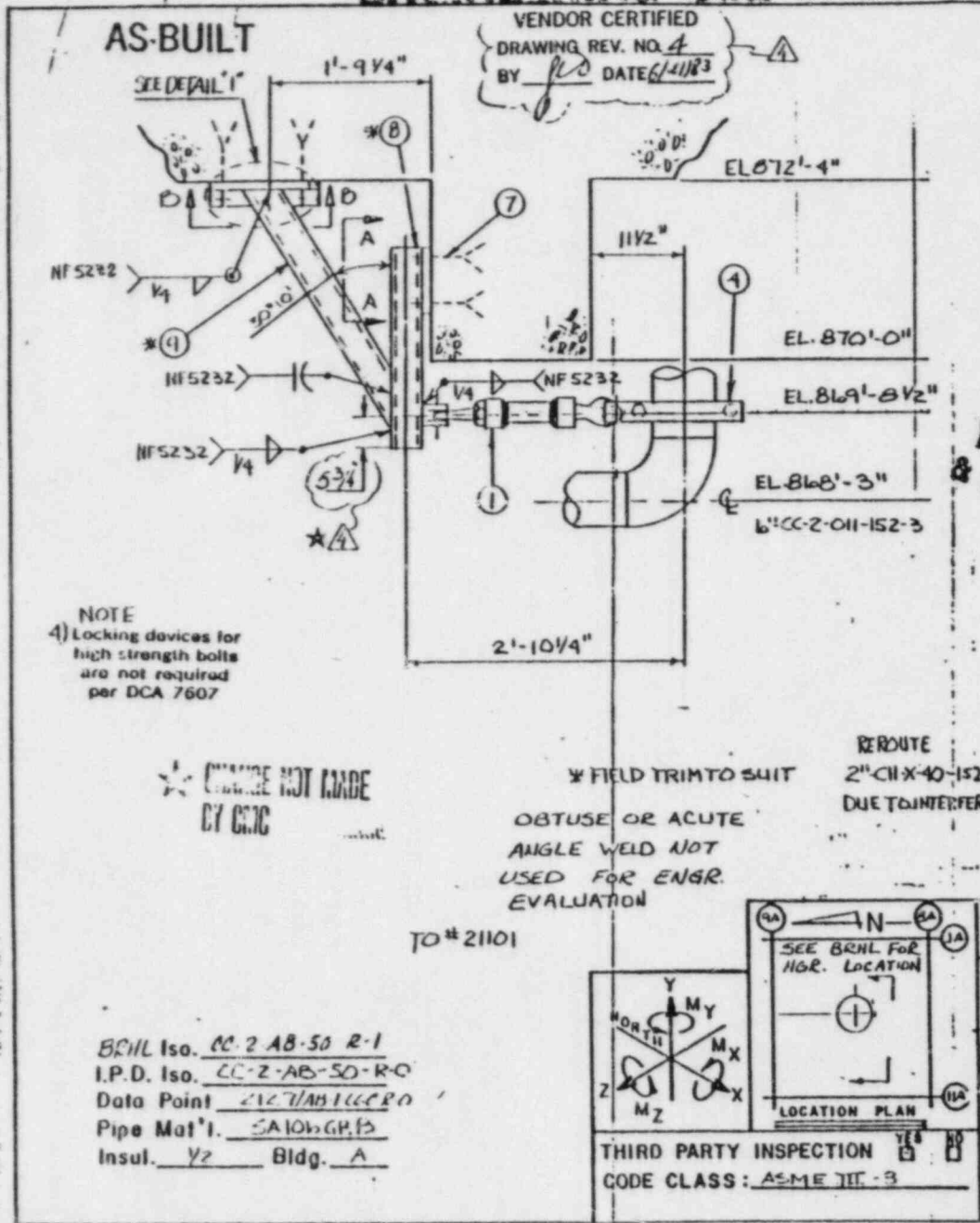
SUPPORT NO. CC-2-11-700-A63A  
SHEET 1 OF 1 REV. 2

CLIENT: T.O.S.I.  
PLANT: COMANCHE PEAK  
JOB NO. 2325

Brown & Root, Inc.  
HOUSTON, TEXAS  
35-1135

FOR OFFICE USE ONLY

# FOR ENGINEERING AND ENGINEERING ONLY



ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	L	CSS	PRIM.	SEC.
1	ORS-10-KO SWAY STRUT C.C. = 1'-8 1/4"							
2	SPC-10-060 PIPE CLAMP SA 36							
3	3/4" CS. TP PER DETAIL A-A SA 36							
4	3/4" CS. TP PER DETAIL B-B SA 36							
5	1.5 3/8" X 4" X 4" X 4" A-500 GR. B							
6	1.5 3/8" X 4" X 4" X 4" A-500 GR. B							
7	3/4" CS. TP PER DETAIL C-C SA 36							
8	3/4" CS. TP PER DETAIL D-D SA 36							
9	3/4" CS. TP PER DETAIL E-E SA 36							
10	3/4" CS. TP PER DETAIL F-F SA 36							
11	3/4" CS. TP PER DETAIL G-G SA 36							
12	3/4" CS. TP PER DETAIL H-H SA 36							

FOR ENGINEERING & OFFICE USE ONLY

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REV	DATE	OWN	CHK	APP	DESCRIPTION
1	6-5-78	JW	[Signature]	[Signature]	ADDED SHIT 2 AS BUILT. REV FOR CERTIFICATION. SEE AT 11:30 AM. REV'D VENDOR CERTIFICATION. REF. AISC 31-BOLTS.

MARK # CC-2-011-002-ALB3R  
PAINT: CARBO ZINC # 11

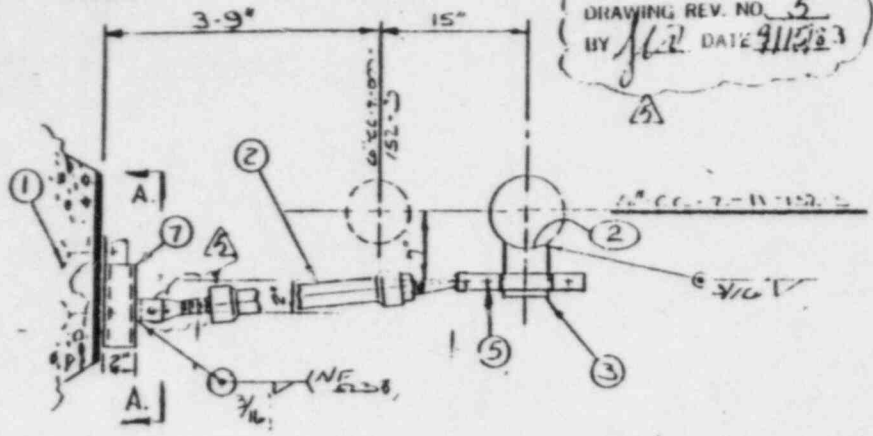
BROWN & ROOT, INC. ENGINEERS & CONSTRUCTORS		CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
REF. DRAWING NUMBERS		DESIGN						
PIPE: MI-0701-R7 ELECT: EL0703-R5		NORMAL & UPSET						
STEEL: S-0735-R2 HV.A.C.: MI-0757-R4		EMERGENCY						
		FAULTED						

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	6-5-78	JW	[Signature]	[Signature]	ISSUE FOR CONST. FW 1
2	6-11-78	ER	[Signature]	[Signature]	REV PER NPSI REV 0A
3	6-11-78	ER	[Signature]	[Signature]	REV. PER PIRP # 322.
4	6-11-78	ER	[Signature]	[Signature]	REV. PER NPSI REV. 0A

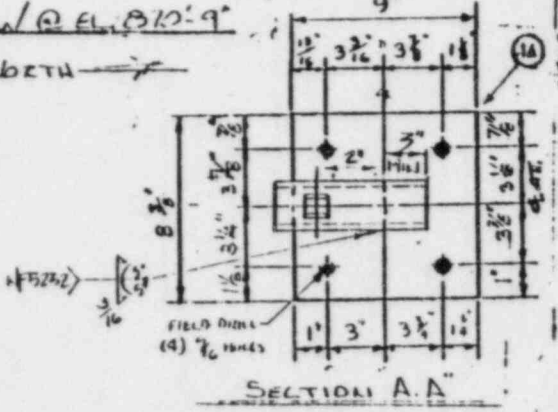
CUSTOMER Texas Utilities Service, Inc.  
ORDER OR CONT. NO. CP-0046  
JOB NAME Comanche Park 1A 2  
MARK NO. CC-2-011-002-ALB3R  
SKETCH NO. \_\_\_\_\_  
SHEET 1 OF 2 REV 4

AS-BUILT

VENDOR CERTIFIED  
DRAWING REV. NO. 5  
BY JLR DATE 9/11/83



PLAN VIEW @ EL. 810'-9"



NOTES:  
4) LOCKING DEVICES FOR HIGH STRENGTH BOLTS ARE NOT REQUIRED PER ICA 7107

ITEM NO.	NO REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC. NO.	WT.	PBS	CS	PHIL	REC	AIBC
1	4	B16 1/2" x 1/2" ERW	COIL ANCHOR								
2	1	1/2" x 1/2" x 1/2" SWAP	SWAP		67P	2.0		X			
3	1	1/2" x 1/2" x 1/2" STANCHION	STANCHION	A106 GR B				X	X		
4	1	1/2" x 1/2" x 1/2" C-9 PLATE	C-9 PLATE	A36				X	X		
5	1	1/2" x 1/2" x 1/2" PIPE CLAMP	PIPE CLAMP	A36				X	X		
6	1	1/2" x 1/2" x 1/2" ASME PLATE	ASME PLATE					X	X		
7	1	1/2" x 1/2" x 1/2" CS PLATE	CS PLATE	A36				X	X		
8	1	1/2" x 1/2" x 1/2" PIPE STEEL	PIPE STEEL	A36				X	X		

SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG  
MARK # CC-2-011-001-A63K

Apply Carbo-Zinc #11 to above mat 1 except th'ds which shall be treated with a rust preventative

NO MAT - BY GRIZZELL

REV	DATE	DWN	CNK	APP	DESCRIPTION
0					ISSUE FOR CONIT
1	7/1	JW			REV FOR NIS/REV CA
2	11/15	JR			REV AS UPD REF: CFC-310LZ PRR-0360
3	11/15	JR			REV AS UPD REF: CFC-310LZ PRR-0360 (SEE 11/4) AS BUILT WITH APPLIC

Approved by: CFC  
Date: 4-23-79

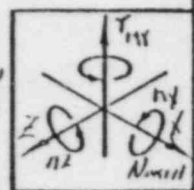
QUAN SHIP  
PBS  
CS

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

FOR OFFICE AND ENGINEERING USE ONLY

PRIN ISO CC-2-AD-50 P.1  
I.P.D. ISO CC-2-62-50 R.D  
Data Point: 12/1/83  
Pipe Mat'l: SA106 GR B  
Instl: 76 Bldr: A

SEE PLAN FOR HGR LOCATION



THIRD PARTY INSPECTION YES NO  
CODE CLASS: ASME III-B

Brown & Root, Inc.

REF. DRAWING NUMBERS

PIPE: 11-0701 - E-1/2 ELECT: 11-0701 E-1/2  
STEEL: S-0720 - E-1/2 HV.A.C.: 11-0701 E

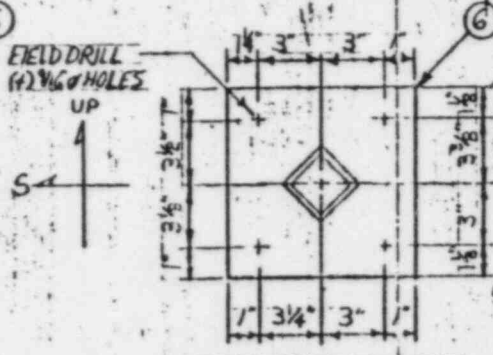
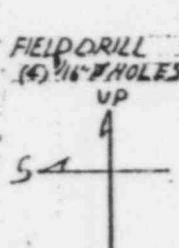
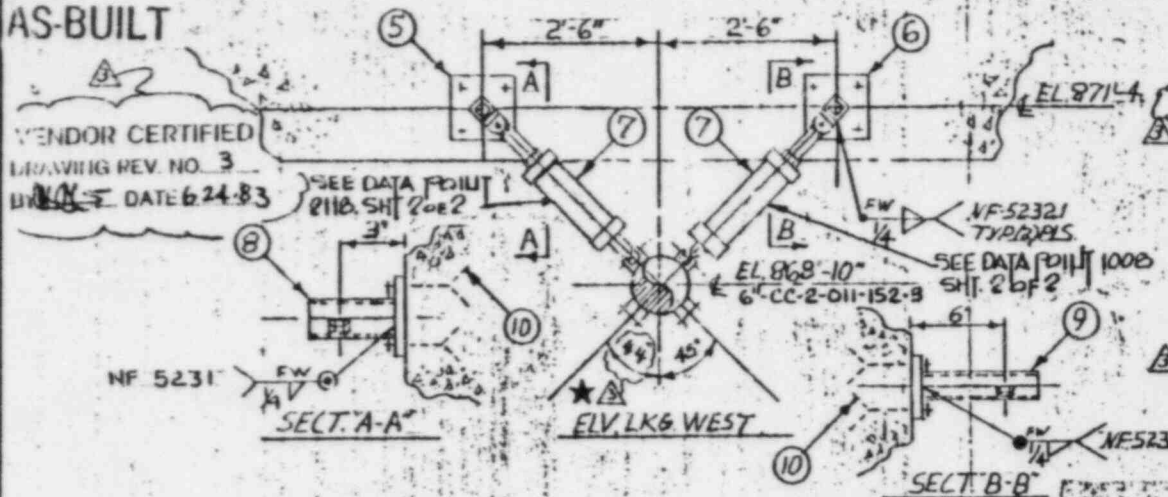
REV	DATE	DWN	CNK	APP	DESCRIPTION
0	6/8	JW			ISSUE FOR CONIT
1	7/1	JW			REV FOR NIS/REV CA
2	11/15	JR			REV AS UPD REF: CFC-310LZ PRR-0360
3	11/15	JR			REV AS UPD REF: CFC-310LZ PRR-0360 (SEE 11/4) AS BUILT WITH APPLIC

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN						
NORMAL & UPSET	1386	474				
EMERGENCY	1386	474				
FAULTED						

CUSTOMER Foxes Utilities Service  
ORDER OR CONT. NO. CP-0046  
JOB NAME Oconee Peak 2 & 2  
MARK NO. CC-2-011-001-A63K  
SKETCH NO.  
SHEET 1 OF 1 REV. 1

AS-BUILT

VENDOR CERTIFIED  
DRAWING REV. NO. 3  
DATE 6.24.83



WALL R. FACING WEST

WALL R. FACING WEST

NOTE:  
1) Locking devices for high strength bolts are not required per ECA 7807

★ CHANGE NOT MADE BY CMC

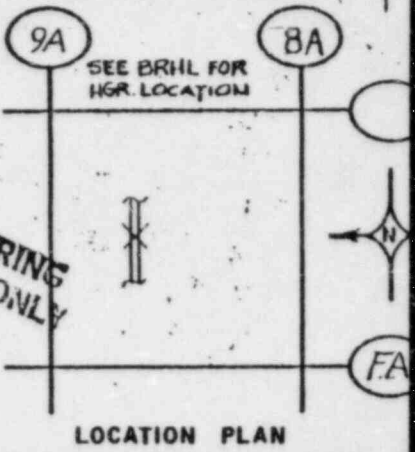
PROBLEM # AB-166C

REV	QTY	MATERIAL	DESCRIPTION	PBS	ISS	DATE
5	1	1/2" R.C.S. (SA-515 OR SA-36)		X		
6	1	1/2" R.C.S. (SA-515 OR SA-36)		X		
7	2	3/8" OB TYPE PC				
8	1	7/8" 1/4" x 1/2" x 3 1/2" LG AS500-74A-GR.B				
9	1	7/8" 1/4" x 1/2" x 3 1/2" LG AS500-74A-GR.B				
10	8	HILTI SWIK BOLTS 1/2" x 5 1/2"		X		

REV	DESCRIPTION	DATE	OWN	CHKD	APPRD
1	VENDOR CERT. (EICA) (HOLI, REF. GIL) 59790	12/80	J	BC	(Signature)
2	ADDED SH. 2, CMC 70905				
3	REV'D VENDOR CERT. REF. AICP # M-8041	6/83	RH	TS	(Signature)

ASME CODE EDITION: 1974  
ADDENDA: WINTER  
DESIGN SPEC: MS-46A

RE. CERTIFICATION  
FOR ENGINEERING & OFFICE USE ONLY



DATA PT	SUPPORT	LOADS (LBS)	PIPE
DESIGN	SEWER	LEVEL	NYTS
VERT		SEE SHEET 2 OF 2	INCHES
N-S			
E-W			

NOTE  
+N,E,UP  
-S,W,DN

AUTHORIZED NUCL. INSP. YES  NO

ASME CODE CLASS 3

REF. DWGS	STRESS ISO.	REV	MECHANICAL	REV	ELECTRICAL	REV
	M2-3231-36	A	MI-0701	6	EI-0703	6
	ISO.		STRUCTURAL		H.V.A.C	
	CC-2-AB-032	1	S-0735	2	MI-0757	4

CPSER Brown & Root, Inc.  
ENGINEERS AND CONSTRUCTORS  
HOUSTON, TEXAS  
28-1108

CLIENT	T.U.S.I.
PLANT	COMANCHE PEAK
JOB NO.	2323

SUPPORT NO.	CC-2-011-703-A63R
SHEET	1 OF 2 REV. 13

FOR OFFICE AND ENGINEERING USE ONLY

AS-BUILT

VENDOR CERTIFIED  
 DESIGNATED BY NO. 3  
 BY (W.M.) DATE 6-24-83

DATA PT.	SUPPORT LOADS (lbs)					PIPE MVTS (INCHES)
	DESIGN	SERVICE	LEVEL		LIMITS	
		A	B	C	D	
VERT.	-197	224	242	213	205	
N-S	+215	35	240	419	121	
E-W						
NOTE	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>					
P,N,E,UP	ASME CODE CLASS <u>3</u>					
S,W,DN						

DATA PT.	SUPPORT LOADS (lbs)					PIPE MVTS (INCHES)
	DESIGN	SERVICE	LEVEL		LIMITS	
		A	B	C	D	
VERT.	-270	347	387	591	176	
N-S	-270	542	347	591	176	
E-W						
NOTE	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>					
P,N,E,UP	ASME CODE CLASS <u>3</u>					
S,W,DN						

MVT'S	
Z	+104
	-185

MVT'S	
Z	+103
	-184

FOR ENGINEERING & OFFICE USE ONLY



DATA PT.	SUPPORT LOADS (lbs)					PIPE MVTS (INCHES)
	DESIGN	SERVICE	LEVEL		LIMITS	
		A	B	C	D	
VERT.						
N-S						
E-W						
NOTE	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>					
P,N,E,UP	ASME CODE CLASS <u>3</u>					
S,W,DN						

REF. DWGS.	STRESS ISO.	REV.	MECHANICAL	REV.	ELECTRICAL	REV.	DESCRIPTION	DATE	DWN.	CHKD.
	M2-3231-36	A					VEHICULAR CERTIFICATION REF. CH# 59790	11/2/82	P	186
	BRHL ISO.	REV.	STRUCTURAL	REV.	H.V.A.C.	REV.	CMC 76965			
	CC-2-AB-032	I					REV'D VENDOR CERTIFICATION REF. ILE 11A041	7/1/83	RM	186

**Brown & Root, Inc.**  
 ENGINEERS AND CONTRACTORS  
 HOUSTON, TEXAS

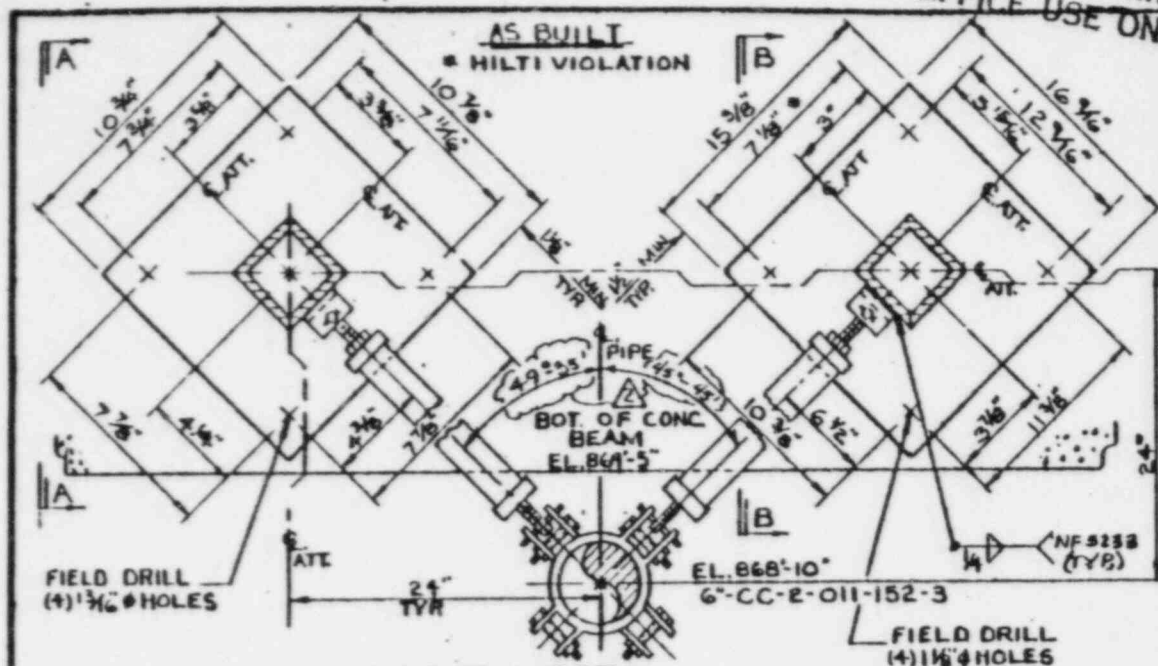
CLIENT T.U.S.I.  
 PLANT COMANCHE PEAK  
 JOB NO. 2323

SUPPORT NO. CC 2-011-703-A63R  
 SHEET 2 OF 2 REV. 3

FOR OFFICE AND

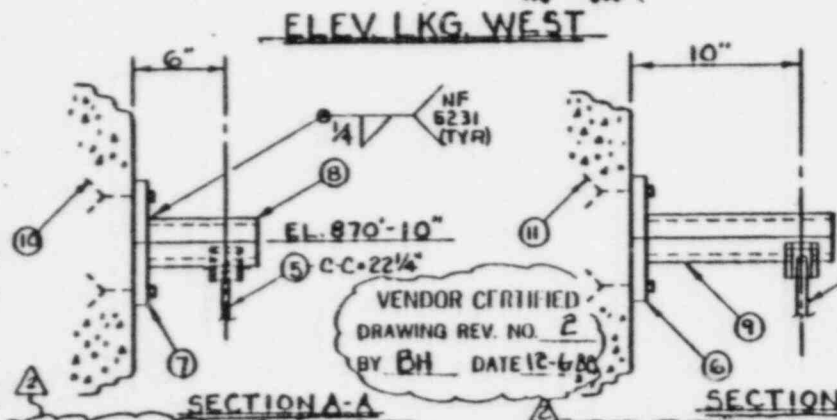
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REV NO	QTY REQ'D	MATERIAL DESCRIPTION	POS	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
5	2	SRS-08-PC SWAY STRUT																					
		W/ SPC-08-060 PIPE CLAMP																					
6	1	3/4" THK. C.S. RATE																					
		EA-34 OR SA-515GR.65																					
7	1	1/2" THK. C.S. RATE																					
		SA-36 OR SA-515GR.65																					
8	1	T.S. 3/8" X 4" X 4" X 0'-7" LG. (A-500 GR. B)																					
9	1	T.S. 3/8" X 4" X 4" X 0'-11" LG. (A-500 GR. B)																					
10	4	3/4" Φ X 10" LG. HILTI KWIK CONCRETE ANCHORS																					
11	4	1" Φ X 9" LG. HILTI KWIK CONCRETE ANCHORS																					

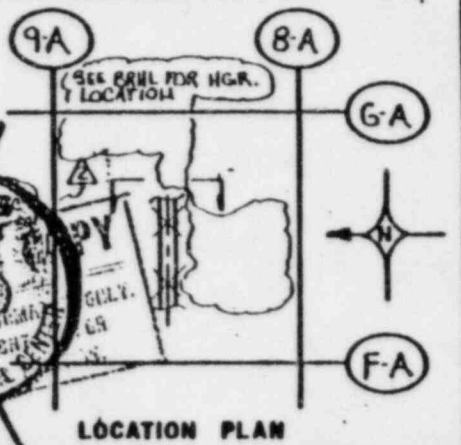
REV	DESCRIPTION	DATE	BY	CHKD.	APPVD.
1	VENDOR CERTIFICATION NF 5231 (TYR)	12/12			
2	CMC 76764 ADDED SHT 2 OF 2				



**NOTES:**  
 1) Locking devices for high strength bolts are not required per DCA 7607  
 2) ALL R. DIM 1/4" UNL

ASME CODE EDITION: 1974  
 ADDENDA: WINTER  
 DESIGN SPEC: MB-46A

RE. CERTIFICATION



DATA PT	SUPPORT	LOADS (LBS)	PIPE
DESIGN	SERVICE	LEVEL	HYDR
VERT			
E-S			
E-W			

NOTE: AUTHORIZED NUCL. INSP. YES  NO   
 ASME CODE CLASS 3

REV	MECHANICAL	REV	ELECTRICAL	REV
APRIL 190	MI-0701	6	EL-0703	6
FEB. 180	STRUCTURAL	REV	HVAC	REV
CC-2-AB-032	1 S-0735	2	MI-0757	4

CPSES Brown & Root, Inc  
 ENGINEERS AND CONSTRUCTORS  
 HOUSTON, TEXAS  
 33-1195

CLIENT: T.U.S.I.	SUPPORT NO. CC-2-11-704-A63R
PLANT: COMANCHE PEAK	SHEET 1 OF 2 REV. 2
JOB NO. 2323	

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AS-BUILT

VENDOR CERTIFIED  
 DRAWING REV. NO. 2  
 BY BH DATE 12-6-82

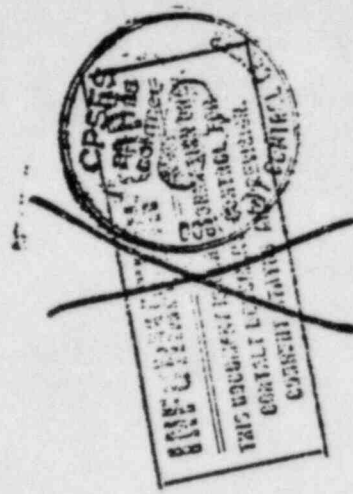
DATA PT	SUPPORT LOADS (lbs)				MVT'S
	DESIGN	LEVEL	LIMITS		
VERT.	11-5	132	0	0	X
U-S	11-5	132	0	0	Y
E-W	0	0	0	0	Z



DATA PT	SUPPORT LOADS (lbs)				MVT'S
	DESIGN	LEVEL	LIMITS		
VERT.	11-5	132	0	0	X
U-S	11-5	132	0	0	Y
E-W	0	0	0	0	Z



FOR ENGINEERING  
& OFFICE USE ONLY



TO # 21101

DATA PT	SUPPORT LOADS (lbs)	PIPE MVT'S (INCHES)	REF. DWRG.	DRILL ISO.	MECHANICAL	ELECTRICAL	REV.	DESCRIPTION	DATE	DWN.	CHKD.	APP.
DESIGN			CC-2-AB-032	M-0701	EI-0703	4	VENDOR CERTIFIED	12/11/82				
VERT.			CC-2-AB-032	1	2	4	COMANCHE PEAK					
U-S												
E-W												
NOTE	AUTHORIZED NUC. INSR. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>											
ASME CODE CLASS	3											
Brown & Root, Inc. HOUSTON, TEXAS								CLIENT T.U.S.I. PLANT COMANCHE PEAK JOB NO. 2323				
SUPPORT NO. CC-2-011-704-ABER												
SHEET 2 OF 2 REV. 2												

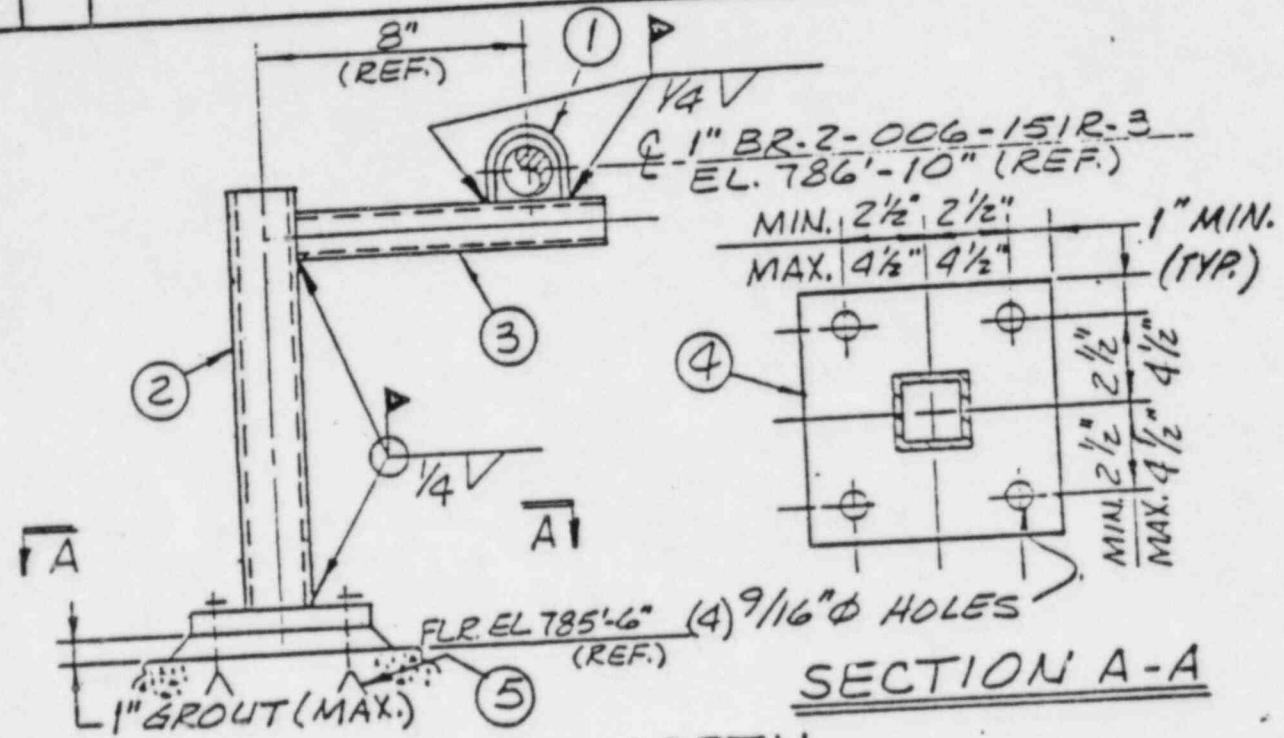
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ITEM NO.	QTY	MATERIAL DESCRIPTION	MATERIAL DESIG.
1	1	WELDED U-GUIDE - PUG - 010	SA-36
2	1	TS. 3 x 3 x .250 x 1'-4 1/2" LG. (CUT TO SUIT)	A500, GR.B
3	1	TS. 2 x 2 x .250 x 1'-1 1/2" LG. (CUT TO SUIT)	A500, GR.B
4	1	PIPE 5 3/4" THK. (SEE SECTION A-A)	SA-36
5	4	1/2" x 9" HILTI-KWIK BOLT (5 1/2" MIN. EMB.)	

'84

OFFICE DOCK  
BRANCH

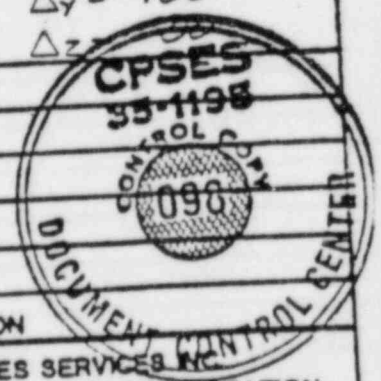
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ENGINEERING USE ONLY



ELEVATION LKG NORTH

NOTE:  
FOR GEN. NOTES, SEE CP-AA-001.

MAX. MVMTS. (IN.)  
 $\Delta x = -.11$   
 $\Delta y = .00$   
 $\Delta z = .00$



REV	DATE	DWN	CHKD	APPR	DESCRIPTION
0	11-16-83	E.C.	AG	HS	RELEASED FOR CONSTRUCTION
					TEXAS UTILITIES SERVICES INC. COMANCHE PEAK STEAM ELECTRIC STATION PIPE SUPPORT ENGINEERING
					DRAWING NO. H-BR-2-SB-001-009-3
					REV. 1-OF-1

PROB. #	DATA PT.	DESIGN SERVICE	LOADS (LBS)	LEVEL LIMITS	PIPE MVMT (INCHES)
			A	B	C
	VERT.	27	39	47	0
	+N,E,UP	N-S			-.10
	-S,W,DN	E-W	5	11	17

H. BR-2-SB-001-009-3  
KINDA DUNGA

MATERIAL IDENTIFICATION (M)

Mat'l Spec	Material Description	Quantity	Inst/ID Number	Required Hoop Stress (where applicable)	QC Verification A. Date	Notes
SA-36	U. Circle AIG-010	1				
A500GRB	T.S. 3" X 3/4" X 1/4"	1	W73541		9/24/82	
A500GRB	T.S. 2' X 2" X 1/4" X 1/4"	1	Y52430		9/24/82	
SA-36	R 7/4" X 10/4 X 9"	1	HJ0882		9/24/82	

#1  
#2  
#3  
9/24/82

## TEXAS UTILITIES GENERATING COMPANY

## OFFICE MEMORANDUM

To 000 DistributionDallas, Texas March 9, 1984Subject Resolution of QAI-0001

'84 AGO 15 P12:15

OFFICE OF SECURITY  
SECRETARY  
BR

The Quality Assurance Investigation listed above has been resolved to the satisfaction of the Manager, Quality Assurance. No further action is necessary at this time. Please contact the undersigned at 214-979-8890 if there are any questions on this matter.

Thank you.

*Jerry C. Walker*  
Jerry C. Walker

JCW:ln

Distribution: D. N. Chapman/QE File 3  
D. L. Andrews/Corporate Security  
Boyce Grier/CPSES QA  
Initiator (A. Vega)

CONFIDENTIAL

TEXAS UTILITIES GENERATING COMPANY

OFFICE MEMORANDUM

To A. Vega Glen Rose, Texas February 22, 1984

Subject Investigation of Allegations  
QAI #0001

In response to your request of 12/20/83 I have investigated the allegations forwarded with QAI #0001. This is the report of my findings.

I interviewed the alleger, [REDACTED], at his home to obtain additional information on the matters alleged in his letter to Doug Frankum. A copy of this letter is attached (Attachment A). My report of the interview is contained in Attachment B. During the interview I was given additional allegations as indicated in the interview report. These additional matters have also been investigated where practicable.

In the investigation, I interviewed two persons named by [REDACTED] in his allegations-- a QC inspector, [REDACTED], and a General Foreman, [REDACTED]. My reports of these interviews are contained in Attachment C and Attachment D. I also reviewed various procedures, records and documentation as appropriate. I have summarized the results of these activities and have developed my evaluation and conclusion for each allegation. These are discussed below.

1. Improper Marking of Hilti Bolts

The information regarding improper marking of Hilti bolts provided by [REDACTED] in the interview was essentially the same as that contained in his letter to Frankum. It should be noted that [REDACTED] had no first hand knowledge of this matter but was reporting what he was told. I interviewed [REDACTED] the QC inspector named by [REDACTED] as having received the star stamp found by the laborer, and she told me essentially the same story. She did state that the star stamp found and given to her was different from that used by QC to mark Super Hilti's and she felt if the stamp had been used the different marking would have been noticed on the Hilti. She had never noticed any evidence that the stamp was used by the craft. I interviewed [REDACTED], the General Foreman named by [REDACTED] who knew that a star stamp had been found and turned in to QC but he had not seen the stamp. [REDACTED] stated that he had no knowledge of the star stamp being used by craft personnel under his supervision.

The allegation of a star stamp being found and turned in to QC was confirmed. The allegation of it being used for improper marking of Hilti bolts was not confirmed.

2. Improper Welding

Based on additional information provided by [REDACTED] during the interview, I visited the area and identified the pipe support in question to be

BR-X-056-726-A53A. A copy of the as-built drawing for this support is attached (Attachment D). I reviewed the weld records for the saddle weld in question and found everything in order. This information was reviewed during my interview with [REDACTED]. It should be noted that the welding procedure specified in this case was WPS-18010 which provides for using "heliarc" procedure for the root and hot pass. After these first two passes it is optional whether "heliarc" or "stick" welding is used to complete the weld. Thus completing the entire weld in question using "heliarc" procedure as alleged by [REDACTED] is not improper. This is what was done according to the welding records. The records show the welding was done by [REDACTED]. There is no indication of any involvement by a welder named [REDACTED].

The allegation that the saddle for the pipe hanger in question was welded by heliarc procedure was confirmed and the procedure used was found to be proper. The allegation that the weld was improperly made by [REDACTED] was not confirmed.

### 3. Oversize Holes for Hilti Bolts

During the interview [REDACTED] made an allegation regarding an oversize hole (1½") being drilled in the floor for a 1¼" Hilti bolt in a hanger base plate. Based on information provided I visited the area and identified the support in question as CC-2-070-002-A33R. A copy of the as-built drawing for this support is attached (Attachment F). There is nothing in the documentation package for this pipe support to indicate a requirement for or the approval of an oversize hole. I reviewed the reports of the QC inspections for the Hilti installation for this support. These are contained in the following:

IRMH-19682, dated 7/1/81  
IRMH-53200, dated 2/15/83  
IRMH-53257, dated 2/22/83

These reports do not indicate any nonconforming or unsatisfactory conditions. [REDACTED] stated during his interview that he had no knowledge of oversize holes ever being drilled for Hilti bolts.

I made inquiry of pipe support engineering (Jay Ryan) as to whether an oversize hole for a Hilti bolt in the support in question would be of concern. I was told that it would not be a problem.


The allegation that an oversize hole had been drilled for a Hilti bolt could neither be confirmed or dismissed. It appears that physical inspection of the holes for the support in question would be the only way to resolve this matter. In view of the response from Engineering regarding the significance of this matter, it does not appear necessary to pursue the matter further.

A. Vega  
Page 3  
February 22, 1984

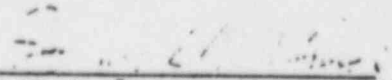
4. Torqueing of Hilti Bolts in Ceiling

It is my understanding that the allegation regarding QC inspectors relying on craft personnel to check the torqueing of Hilti bolts in places where access is limited has been investigated previously. This matter has been discussed in the Licensing Hearings before the ASLB and is recorded in the transcript for September 14, 1982, on pages 4537-4539 (Attachment G). In view of this, no further investigation of this matter was made.




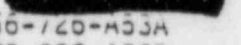
5. Damaged Threads on 1/2" Hilti Bolt

 did not provide sufficient information on the location of this problem to enable the matter to be investigated. Since it was described as an isolated case, it does not appear that further action is warranted at this time to resolve safety concerns. Of more concern is the alleged deliberate act for fraudulent purposes.

If you have questions or comments regarding any of the above matters or if you wish me to pursue anything further, please let me know.

  
Joyce H. Grier

BHG/b11

Attachments: A - Letter to Frankum from   
B - Interview with   
C - Interview with   
D - Interview with   
E - Drawing BR-X-056-126-A53A  
F - Drawing CC-2-070-002-A33R  
G - Hearing Transcript pp. 4537-4539

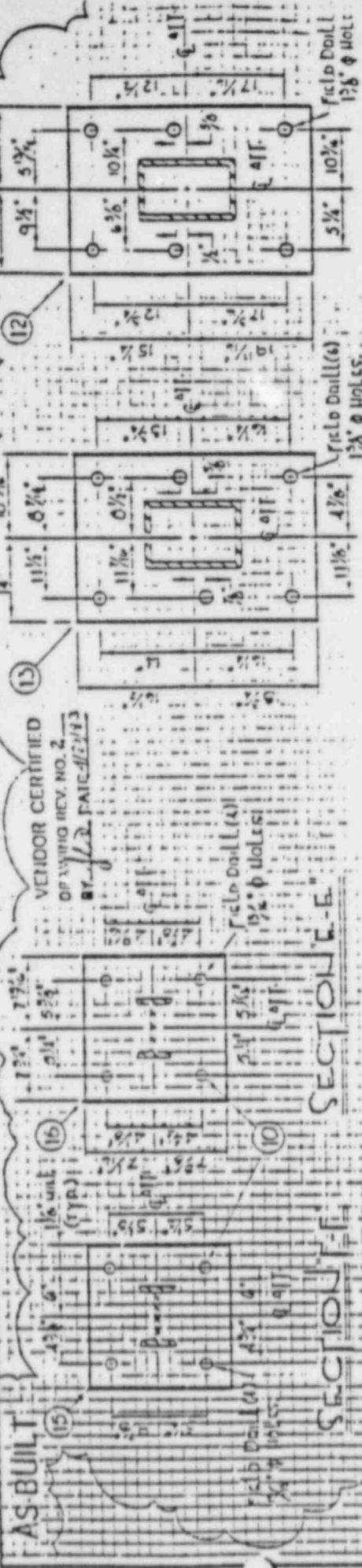
cc: D. N. Chapman  
D. L. Andrews  
R. G. Tolson





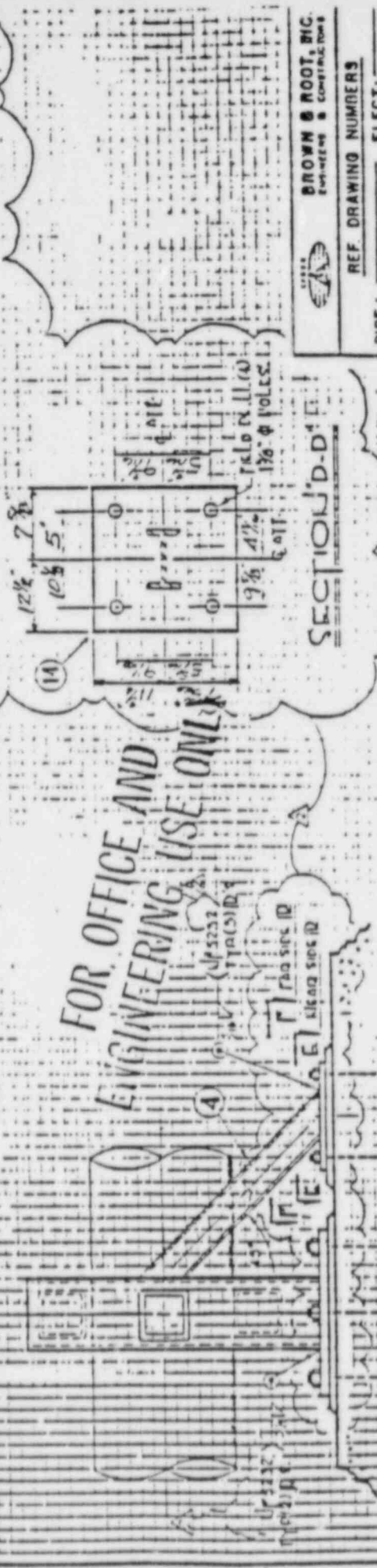
AS-BUILT

VENDOR CERTIFIED  
DRAWING REV. NO. 2  
BY J.R. PATRICK/ETP



SECTION 'C-C'

SECTION 'D-D'



FOR OFFICE AND  
ENGINEERING USE ONLY

SECTION 'A-A'

BROWN & ROOT, INC.  
ENGINEERS & CONTRACTORS

REF. DRAWING NUMBERS  
PIPE: \_\_\_\_\_ ELECT: \_\_\_\_\_  
STEEL: \_\_\_\_\_ HVAC: \_\_\_\_\_

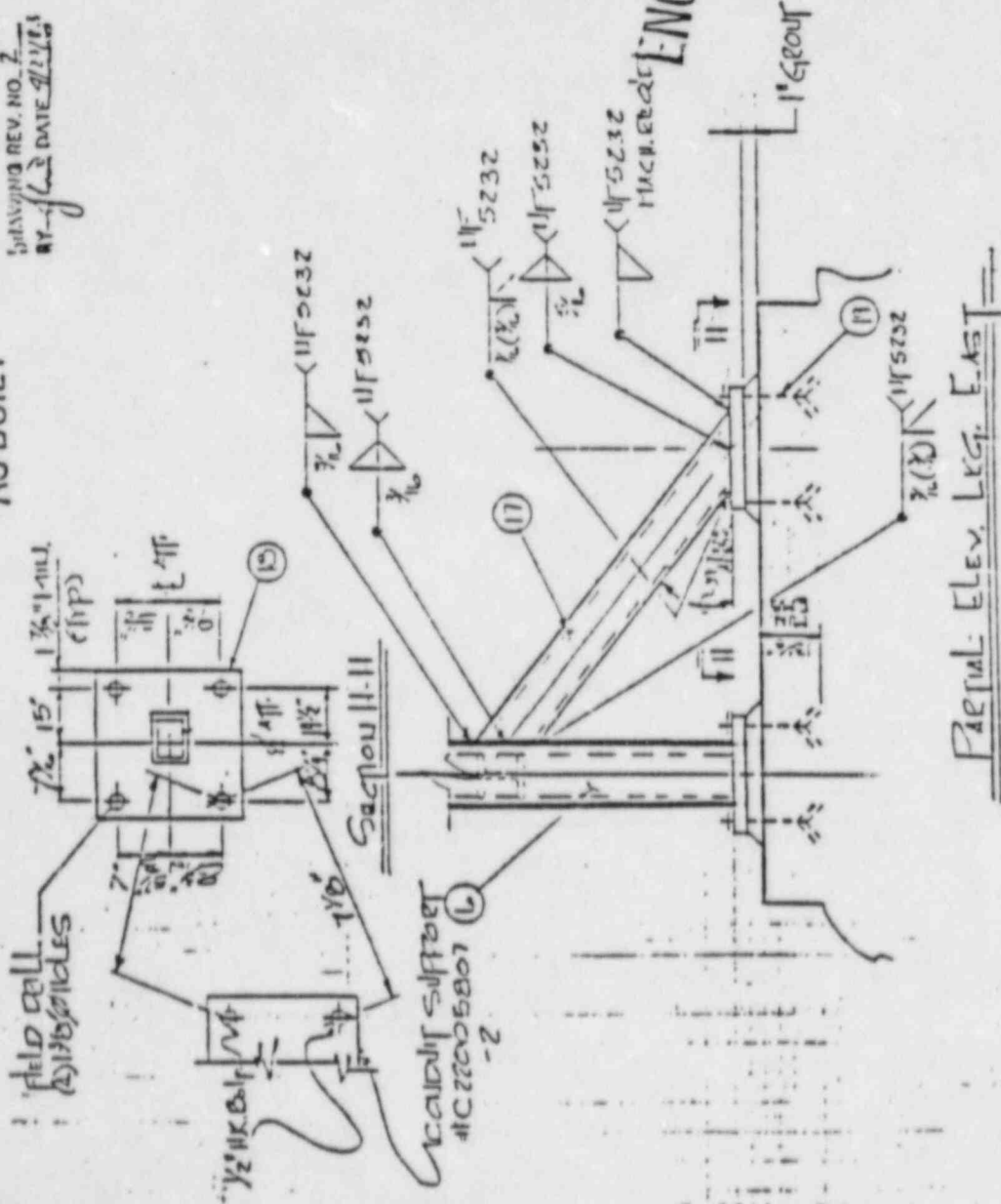
CUSTOMER: Texas Utilities Service, Inc.  
ORDER OR CONT. NO.: CP-0046  
JOB NAME: Comanche Peak 1B 2  
MARK: H.C.C.-2-070-002-025a  
SPEECH NO.: \_\_\_\_\_  
SHEET 2 OF 3 REV. 7

REV.	DATE	BY	CHKD.	DESCRIPTION
1	12/15/00	JR	ETP	ISSUE FOR CONST.
2	12/15/00	JR	ETP	REV AS NOTED. REV CMC
3	12/15/00	JR	ETP	REV AS NOTED. REV CMC
4	12/15/00	JR	ETP	REV AS NOTED. REV CMC
5	12/15/00	JR	ETP	REV AS NOTED. REV CMC
6	12/15/00	JR	ETP	REV AS NOTED. REV CMC
7	12/15/00	JR	ETP	REV AS NOTED. REV CMC
8	12/15/00	JR	ETP	REV AS NOTED. REV CMC
9	12/15/00	JR	ETP	REV AS NOTED. REV CMC
10	12/15/00	JR	ETP	REV AS NOTED. REV CMC
11	12/15/00	JR	ETP	REV AS NOTED. REV CMC
12	12/15/00	JR	ETP	REV AS NOTED. REV CMC
13	12/15/00	JR	ETP	REV AS NOTED. REV CMC
14	12/15/00	JR	ETP	REV AS NOTED. REV CMC
15	12/15/00	JR	ETP	REV AS NOTED. REV CMC
16	12/15/00	JR	ETP	REV AS NOTED. REV CMC
17	12/15/00	JR	ETP	REV AS NOTED. REV CMC
18	12/15/00	JR	ETP	REV AS NOTED. REV CMC
19	12/15/00	JR	ETP	REV AS NOTED. REV CMC
20	12/15/00	JR	ETP	REV AS NOTED. REV CMC
21	12/15/00	JR	ETP	REV AS NOTED. REV CMC
22	12/15/00	JR	ETP	REV AS NOTED. REV CMC
23	12/15/00	JR	ETP	REV AS NOTED. REV CMC
24	12/15/00	JR	ETP	REV AS NOTED. REV CMC
25	12/15/00	JR	ETP	REV AS NOTED. REV CMC
26	12/15/00	JR	ETP	REV AS NOTED. REV CMC
27	12/15/00	JR	ETP	REV AS NOTED. REV CMC
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29	12/15/00	JR	ETP	REV AS NOTED. REV CMC
30	12/15/00	JR	ETP	REV AS NOTED. REV CMC
31	12/15/00	JR	ETP	REV AS NOTED. REV CMC
32	12/15/00	JR	ETP	REV AS NOTED. REV CMC
33	12/15/00	JR	ETP	REV AS NOTED. REV CMC
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39	12/15/00	JR	ETP	REV AS NOTED. REV CMC
40	12/15/00	JR	ETP	REV AS NOTED. REV CMC
41	12/15/00	JR	ETP	REV AS NOTED. REV CMC
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43	12/15/00	JR	ETP	REV AS NOTED. REV CMC
44	12/15/00	JR	ETP	REV AS NOTED. REV CMC
45	12/15/00	JR	ETP	REV AS NOTED. REV CMC
46	12/15/00	JR	ETP	REV AS NOTED. REV CMC
47	12/15/00	JR	ETP	REV AS NOTED. REV CMC
48	12/15/00	JR	ETP	REV AS NOTED. REV CMC
49	12/15/00	JR	ETP	REV AS NOTED. REV CMC
50	12/15/00	JR	ETP	REV AS NOTED. REV CMC

THIRD PARTY INSPECTION  
CODE CLASS: ASME III-2

AS-BUILT


API/ASME CERTIFIED  
 DRAWING REV. NO. 2  
 BY DATE



FOR OFFICE AND  
 ENGINEERING USE ONLY

ATTACHMENT 7 - 3

10.21101

 <b>BROWN &amp; ROOT, INC.</b> ENGINEERING & CONSTRUCTION	
PIPE:	ELECT:
STEEL:	HVAC:
REF. DRAWING NUMBERS	
CUSTOMER	Texas Utilities Service, Inc.
ORDER OR CONT. NO.	CP-0046
JOB NAME	Comanche Peak 1B2
MARKING	CC-3-010-002-ASB
SKETCH NO.	
SHEET	3 OF 3
REV.	6

DATE	BY	DESCRIPTION
10/21/01	ALM	REVISION

THIRD PARTY INSPECTION  
 CODE CLASSI 431E III-2



SECTION V  
FIGURE 6

TEXAS UTILITIES SERVICES INC.  
Agent For  
DALLAS POWER & LIGHT COMPANY  
TEXAS ELECTRIC SERVICE COMPANY  
COMANCHE PEAK S.E.S.

ALLOWABLE LOADS FOR HILTI-KWIK AND SUPER HILTI KWIK BOLTS  
USING 4000 PSI CONCRETE, 5:1 SAFETY FACTOR, A.A. HANKS TESTING LAB REPORT  
NO. 873R AND HILTI LETTER DATED OCT. 27, 1980 / CPPA-7419 COVER LETTER

## HILTIS

BOLT DIA	EMB LENGTH	TENSION	SHEAR
1/2"	2 3/4"	1102	1663
	2 3/4"	1440	↓
	3 1/2"	1890	↓
	4 1/2"	2245	2046
	5 1/2"	2410	↓
	6"	2460	↓
5/8"	2 3/4"	1320	2312
	3 1/2"	1820	↓
	4 1/2"	2400	↓
	5 1/2"	2860	3087
	6 1/2"	3200	↓
	7 1/2"	3400	↓
3/4"	3 1/4"	2030	3427
	4"	2680	↓
	5"	3300	↓
	6"	3600	3693
	7"	4200	↓
	8"	4600	↓
1"	4 1/2"	3200	5375
	5"	3780	↓
	6"	4688	↓
	7"	↓	↓
	8"	↓	6898
	9"	↓	↓
1 1/4"	5 1/2"	4600	7136
	6 1/2"	5920	↓
	7 1/2"	6220	↓
	8 1/2"	6920	↓
	9 1/2"	7560	↓
	10 1/2"	8180	↓

## SUPER HILTIS

BOLT DIA.	EMB. LENGTH	TENSION	SHEAR
1/2"	3 1/4"	1997	2288
	4 1/4"	2956	↓
	5 1/4"	2956	↓
	6 1/4"	3029	↓
1"	6 1/2"	6993	5507
	8 1/2"	9951	↓
	10 1/2"	9951	↓
1 1/4"	8 1/8"	8540	8296
	10 5/8"	10736	↓
	13 1/8"	12984	↓

TEXAS UTILITIES GENERATING COMPANY

P. O. BOX 1002 · GLEN ROSE, TEXAS 76043

PROJECT FILE

April 19, 1984

DOCKETED  
USING

'84 AGO 15 P12:15

Cygn Energy Services  
101 California Street  
Suite 1000  
San Francisco, California 94111

CYGNA		189
JOB NO.:	84042	
DATE LOGGED:	5/14/84	
LOG NO.:	#9	
FILE:	2-1-1 Mc. CR	
CROSS REF. FILE	1-1 3rd 15 629	

Attention: Ms. Nancy Williams  
Project Manager

COMANCHE PEAK STEAM ELECTRIC STATION

Gentlemen:

In response to your handwritten questions provided to TUGCO on March 16, 19, 20, 21 and 22, enclosed is a copy of the questions followed by TUGCO's response. Several questions are still under review and will be answered shortly. In addition, questions asked via telephone to Dave Rencher on March 30, 1984, are presently being reviewed and responses will be forwarded by April 27th.

If there are any further questions or comments, please contact me or George Grace (Site Ext. 500).

Very truly yours,

TEXAS UTILITIES GENERATING COMPANY  
ENGINEERING DIVISION

*L. M. Popplewell*

L. M. Popplewell  
Project Engineering Manager

LMP/cp

*Distributive*  
NH Williams  
J. C. Minchillo  
E. Weirgart  
C. Wang  
M. Schulman  
84042 Project File (To Acuna)

working range (generally near mid-travel); a minimum  $\frac{1}{4}$ " travel exists beyond working range limits to reach a fully extended or retracted position. For most springs, more than  $\frac{1}{4}$ " is available. This is sufficient to account for the small seismic displacements. For box frames, the seismic movements for the supports listed were checked against the designs. In all cases, adequate clearance existed to allow combined thermal and seismic displacements.

## CYGNA COMMENT:

3. In reviewing certain MS supports, CYGNA has noted instances where beams with small gaps are used to provide stability, instead of tightening U-bolts (supports MS-1-004-003-S72R, for example). In these cases, no analysis is done on the "stability bumpers." CYGNA has performed calculations which show that the load on these "supports" could be quite high, assuming one accepts the instability of this structure during dynamic loading. Has TUSI used this design for any supports with static compressive loads? Also, where is the documentation for the integrity of this support arrangement in general?

## TUGCO RESPONSE:

3. The "bumpers" supplied on MS-1-004-003-S72R (in lieu of a snug U-bolt) for stability are designed to take an oscillating, momentary load (for a system at 20Hz, the applied load onto the bumpers will act less than 0.05 seconds). Hence, the nature of the cyclic load assures stability in that there is not sufficient time for a constant applied force to push the bumpers back and allow the pipe to lift up. The calculations which consider a static upward load are therefore erroneous. The stress in the bumper steel stays within its elastic limit under the impact load and hence will return to its original position when the load reverses and pushes down. This design has not been used on any supports which would experience a static compressive load. Structural acceptability of the bumpers is based on the momentary load of less than 0.05 second duration. Size of the members, welds, were judged adequate by inspection.

March 21, 1984

## CYGNA COMMENT:

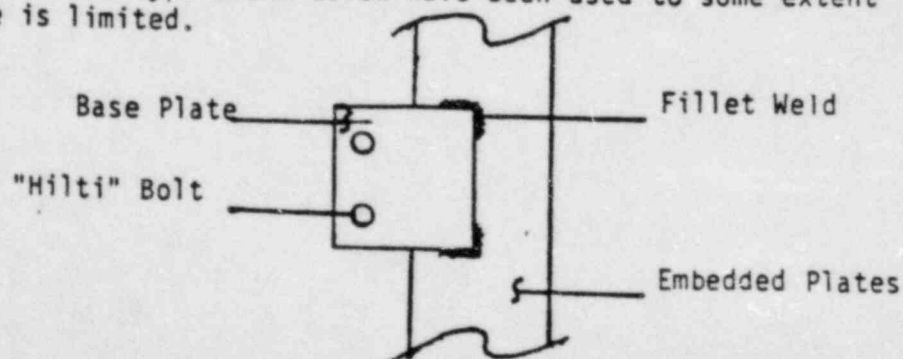
1. In reviewing MS-1-004-001-C72S, CYGNA had the following questions:
  - a) There appears to be a 7/16" flare bevel weld between items 15 and 22. This does not seem possible due to Item 34. Does TUSI have documentation conforming the size and configuration of this weld? Likewise, the weld (5/16") between 26 and 15?

- b) The model uses a fixed point at the embed plates (3, 6, 12, 15 joints). Spec. 2323-SS-30, Rev. 1, requires these to be treated as pin joints, unless the embedment is stiffened. Where is the stiffener in this calc, and has structural accepted this configuration?
- c) Per ASME Appendix XVII, Para. 2442, shear loads on connections with both welds and bolts must be taken by the welds alone. Item 16 is attached to Beam #21 with both welds and Hilti's. The weld sizing calculations done use the bolts to share the shear load. What is TUSI's standard practice in this type of connection? Is this weld acceptable?
- d) The weight of the constant support itself is not included in the support design load for the frame. A #53 constant weighs - 600 lb, or 5% of the design load.

What is TUSI's standard practice for spring anchorage design?

TUGCO RESPONSE:

1. (a) In the NPSI original design,  $\frac{1}{2}$ " wall tube steel was used and the  $\frac{7}{16}$ " flare bevel weld was possible. Modifications made at the site changed most of the steel members to  $\frac{3}{8}$ " wall tube. The weld between items 15 and 22 is a flare bevel weld such that the groove is filled and ground flush to facilitate installation of Item 34. CYGNA is correct in their observation that a  $\frac{7}{16}$ " flare bevel weld does not exist, the size was inadvertently not removed during the revision process. The stiffening effect of Item 34 on this joint assures structural acceptability. The  $\frac{5}{16}$ " flare bevel weld between items 26 and 15 is an acceptable weld since the tube steel thickness is  $\frac{3}{8}$ " (greater than  $\frac{5}{16}$ "). Documentation confirming the size of these welds is on file with QC in their inspection package. (b) See comments dated 3/22, response 1. (c) (Editorial: Items 15 and 19 are connected to beam 21, not item 16.) The connection to the beam via embedded plate (i.e., by welding) and via baseplate (i.e., by bolting) is at separate locations. As such, each is capable of resisting shear. It should be noted that Hilti joints are designed using bolt shear allowables based on ultimate test loads divided by 5. This is not the standard engineering approach to design a bearing or friction joint using code allowables for the bearing or friction condition. Using our design approach, the Hilti joints, since they are pre-torqued, would perform as a friction joint within their working loads. At ultimate loads all joints (bearing or friction) would act as bearing joints (i.e., slip would occur in the friction connection). (Following comments, in response to CYGNA's comment on TUSI's standard practice are provided here for information only). Connections of the type shown below have been used to some extent where space is limited.



DOCKETED  
USNRC

'84 AGO 15 P12:15

OFFICE OF SEISMIC  
DOCKETING & SERVICE  
BRANCH

UNITED STATES OF AMERICA  
NUCLEAR REGULATORY COMMISSION

BEFORE THE ATOMIC SAFETY AND LICENSING BOARD

In the Matter of	}}	
	}}	
TEXAS UTILITIES ELECTRIC	}}	Docket Nos. 50-445-1
COMPANY, <u>et al.</u>	}}	and 50-446-1
(Comanche Peak Steam Electric	}}	
Station, Units 1 and 2)	}}	

CERTIFICATE OF SERVICE

By my signature below, I hereby certify that true and correct copies of  
CASE's 8/13/84 Answer to Applicants' Motion for Summary Disposition Regarding  
the Effects of Gaps on Structural Behavior Under Seismic Loading Conditions

have been sent to the names listed below this 13th day of August, 1984,  
by: Express Mail where indicated by \* and First Class Mail elsewhere.

- |  |   |
|--|---|
| <p>* Administrative Judge Peter B. Bloch<br/>U. S. Nuclear Regulatory Commission<br/>4350 East/West Highway, 4th Floor<br/>Bethesda, Maryland 20814</p>          | <p>* Nicholas S. Reynolds, Esq.<br/>Bishop, Liberman, Cook, Purcell<br/>&amp; Reynolds<br/>1200 - 17th St., N. W.<br/>Washington, D.C. 20036</p>  |
| <p>* Ms. Ellen Ginsberg, Law Clerk<br/>U. S. Nuclear Regulatory Commission<br/>4350 East/West Highway, 4th Floor<br/>Bethesda, Maryland 20814</p>                | <p>* Geary S. Mizuno, Esq.<br/>Office of Executive Legal<br/>Director<br/>U. S. Nuclear Regulatory<br/>Commission<br/>Maryland National Bank Bldg.<br/>- Room 10105<br/>7735 Old Georgetown Road<br/>Bethesda, Maryland 20814</p> |
| <p>* Dr. Kenneth A. McCollom, Dean<br/>Division of Engineering,<br/>Architecture and Technology<br/>Oklahoma State University<br/>Stillwater, Oklahoma 74074</p> | <p>Chairman, Atomic Safety and Licensing<br/>Board Panel<br/>U. S. Nuclear Regulatory Commission<br/>Washington, D. C. 20555</p>  |
| <p>* Dr. Walter H. Jordan<br/>881 W. Outer Drive<br/>Oak Ridge, Tennessee 37830</p>  |   |



Chairman  
Atomic Safety and Licensing Appeal  
Board Panel  
U. S. Nuclear Regulatory Commission  
Washington, D. C. 20555

Renea Hicks, Esq.  
Assistant Attorney General  
Environmental Protection Division  
Supreme Court Building  
Austin, Texas 78711

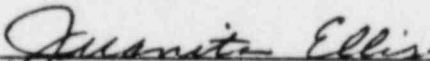
John Collins  
Regional Administrator, Region IV  
U. S. Nuclear Regulatory Commission  
611 Ryan Plaza Dr., Suite 1000  
Arlington, Texas 76011

Lanny A. Sinkin  
114 W. 7th, Suite 220  
Austin, Texas 78701

Dr. David H. Boltz  
2012 S. Polk  
Dallas, Texas 75224

Michael D. Spence, President  
Texas Utilities Generating Company  
Skyway Tower  
400 North Olive St., L.B. 81  
Dallas, Texas 75201

Docketing and Service Section  
(3 copies)  
Office of the Secretary  
U. S. Nuclear Regulatory Commission  
Washington, D. C. 20555

  
\_\_\_\_\_  
(Mrs.) Juanita Ellis, President  
CASE (Citizens Association for Sound Energy)  
1426 S. Polk  
Dallas, Texas 75224  
214/946-9446