Florida Power and Light Company Turkey Point Plant Unit No. 3 Docket Number 50-250

REACTOR CONTAINMENT BUILDING
INTEGRATED LEAKAGE RATE TEST
MARCH 20, 1979

Submitted to

The United States Nuclear Regulatory Commission

Pursuant to

Facility Operating License No. DPR-31

#### TABLE OF CONTENTS

- I. INTRODUCTION
- II. TEST SYNOPSIS
- III. TEST DATA SUMMARY
  - A. Plant Information
  - B. Technical Data
  - C. Test Results Type A Test
  - D. Test Results Type B and C Tests
  - E. Integrated Leakage Rate Measurement System
  - F. Permanent Plant Instrumentation I sed during Test
  - G. Information Retained at Plant
- IV. ANALYSIS AND INTERPRETATION
- APPENDIX A. Failed Test Report Type A Test
  - V. OPERATING PROCEDURE 13100.1 #3 ILRT MASTER COPY

#### I. INTRODUCTION

The reactor containment building Integrated Leakage Rate, Type A, Test, is performed to demonstrate that leakage through the primary reactor containment and systems and components penetrating primary containment does not exceed the allowable leakage rate specified in the Plant Technical Specifications.

The successful periodic Type A and supplemental verification tests were performed according to the requirements of the Turkey Point Plant, Unit 3, Technical Specifications and 10CFR50, Appendix J. The Turkey Point Plant Type A test method is the absolute method described in ANSI N45.4-1972, "Leakage Rate Testing of Containment Structures for Nuclear Reactors" and ANSI N274, "Containment System Leakage Testing Requirements", Draft No. 2, Rev. 3 - November 15, 1978. The leakage rate was calculated using formulas from ANSI N45.4-1972 and BN-TOP-1, Rev. 1. "Testing Criteria for Integrated Leakage Rate Testing of Primary Containment Structures for Nuclear Power Plants" (Total-Time) and ANSI N274 (Mass-Point). Type A and verification test durations were according to the criteria of BN-TOP-1.

The test results are reported in accordance with the requirements of 10CFR50, Appendix J, Section V.B.3.

### II. TEST SYNOPSIS

After initial pressurization to test pressure, a leak was discovered through the 3A Steam Generator steam line vent valve. The containment was depressurized to repair the valve, then the containment was repressurized to test pressure. A leak was discovered at the Personnel Airlock equalizing valve shaft seal (inner door). This leak was repaired, and no other leak paths were discovered.

The Type A test was started at 2245 on 3/19/79. At 1045 on 3/20/79, the Type A test was terminated with a calculated leakage rate of 0.034% per day, with an upper 95% confidence limit of 0.060% per day (Total-Time Method) and 0.031% per day, with an upper 95% confidence limit of 0.033% per day (Mass-Point Method). At 1245 on 3/20/79 a verification flow rate of 0.103% per day was established. The verification test was successfully completed at 1815 on 3/20/79.

### III. TEST DATA SUMMARY

### A. Plant Information

Owner	Florida Power and Light Company
Plant	Turkey Point Plant, Unit 3
Location	Homestead, Florida
Containment Type	Prestressed, post-tensioned concrete
NSSS Supplier, Type	Westinghouse, PWR
Date Test Completed	March 20, 1979

### B. Technical Data

1.	Containment Net Free Air Volume	1,550,000 cu. ft.
2.	Design Pressure	50 psig
3.	Design Temperature	276°F
4.	Calculated Peak Accident Pressure, Pa	50 psig
5.	Containment ILRT Average Temperature Limits	80 - 90°F
6.	Calculated Peak Accident Temperature	283°F

### C. Test Results - Type A Test

1.	Test Method	Absolute	Absolute		
2.	Data Analysis Techniques	Mass Point (per ANSI N274) and Total-Time (per BN-TOP-1			
3.	Test Pressure	25 psig			
4.	Maximum Allowable Leakage Rate, $L$ t	0.1029%/day			
5.	75% of L <sub>t</sub>	0.0772%/day			
6.	Integrated Leakage Rate Test Results	Leakage Rate, From Regres- sion Line (L <sub>tm</sub> )	At Upper 95%		
	<ul><li>a. Mass point analysis</li><li>b. Total-Time analysis</li></ul>	0.031 0.034	0.033 0.060		
7.	Verification Test Imposed Leakage Rate, L <sub>o</sub> , %/day	0.103			

8. Verification Test Results Leakage Rate, %/day

a. Mass Point Analysis

0.117

b. Total-Time Analysis

0.118

Verification Test Limits

Test Limits, %/day

- a. Mass Point Analysis
  - Upper Limit (L +L +0.25L ) 0.160
  - 2) Lower Limit (L +L -0.25L ) 0.108
- Total-Time Analysis
  - Upper Limit  $(L_0 + L_{tm} + 0.25L_a)$  0.163
  - Lower Limit (L +L -0.25L ) 0.111
- 10. Report Printouts

The Report Printouts of the Type A and verification test calculations are provided for the Mass Point and Total-Time Analyses. (Tables 2 through 7) Stabilization data is also provided. (Table 9)

Test Results - Type B and C Tests D.

> Test results for local leak rate tests performed since the previous 1976 Integrated Leak Rate Test are provided. (Table 9)

- Integrated Leakage Rate Measurement System E.
  - Absolute Pressure (1 channel)

Range:

0-100,000 counts

Accuracy:

0.015% of reading

Resolution:

0.001% F.S.

Range:

0-49 psi

Texas Instrument Model 145-02 Precision Pressure Instrument No. 1940

Bourdon Capsule #4433 Calibration Date: 12-15-78

Texas Instrument Model 145-02 Precision Pressure Instrument No. 1941

Bourdon Capsule #4434 Calibration Date: 12-15-78

#### 2. Drybulb Temperature (22 sensors)

Resistance Temperature Detectors - Leeds and Northrup Thermohm Model 8187-10-S, 3-lead, 100-ohm copper and Numatron numeric display model 900-9999-9999-1-5.

Limit of error: 0.2°F Static resistance: 100 ohms

Read out - Leeds & Northrup Numatron

Calibration Date: 2-14-79

Calibration Standard Thermometer -

Taylor Total Immersion Thermometers 18°F to 89°F .20°F

Divisions

S/N 63F3484 Calibration Date: 12-18-78 S/N 63F3640 Calibration Date: 12-18-78

RTD - Leeds & Northrup

100 ohm copper thermohms Catalog 8187-10-S Catalog No. 300-9999-9999-1-S Calibration Date: 3-10-79

#### 3. Dewpoint Temperature (4 sensors)

Dewpoint Temperature Systems - EG&; Inc. Dewpoint Hygrometer with 4 sensors.

Accuracy: 0.54°F Sensitivity: 0.18°F

Read out - Keithley Model 173 Auto Range DVM Calibration Date: 3-16-79

System Model 660-Cl Sensor Model 660-S2 Calibration Date

S/N 391	S/N 423	12-14-78
S/N 400	S/N 378	12-14-78
S/N 405	S/N 406	12-20-78
S/N 397	S/N 484	3-14-79

#### Verification Flow (1 channel)

Flowmeter-Brooks Hi-accuracy full view rotameter, Model 1110.

Range: 1.24-12.4 scfm
Accuracy: +0.1 scfm
Repeatability: 0.01 scfm

Calibration date: 1-12-79

5. Gauge Pressure (1 channel) - Not used directly in calculations.

Wallace & Tiernan Model 61A-1A-0100

Range: 0-100 psig
Accuracy: 0.1% F.S.
Sensitivity: 0.01% F.S.
Calibration Date: 3-13-79

6. Overall Instrumentation Selection Guideline (ISG) Value (from ANSI N274) based on ILRT instrumentation and an eleven hour minimum test duration:

+0.0257%/day

- Drybulb and Dewpoint Temperature Sensor Volume Fractions -See Table 1.
- F. Permanent Plant Instrumentation Used During Test
  None.
- G. Information Retained at Plant

The following information shall be retained by the owner and shall be made available for review at the Facility:

1. Access Procedure

Included in test procedure Section V.

2. Containment Penetrations

A listing of all containment penetrations, including the total number of like penetrations, penetration size and function.

3. Operating Instrument Status

No normal operating instrumentation was used for the leakage rate test.

4. Systems Status (at time of test)

A system line-up, showing required valve positions and status of piping systems, is contained in Section V, OP 13100.1.

5. Event Log

A continuous, sequential log of events from initial survey of containment to the Post Containment ILRT Final Inspection.

### 6. Instrumentation Validation

Documentation of instrumentation calibrations and standards. Included with the documentation is an error analysis of instrumentation.

### 7. Temperature Stabilization

Data to verify temperature stabilization criteria as established by test procedure is contained in Table 8.

### 8. Test Procedure

The working copy of test procedure including signature sign-off of procedural steps, is contained in Section V OP 13100.1.

### 9. Local Leak Rate Tests

The procedure and all data that verifies completion of penetrations and valve testing (B&C type tests) including as found leak rates - corrective action taken, and final leak rate.

### 10. Integrated Leak Rate Data

Computer printouts, manual data accumulation along with summary description of computer program.

#### 11. Quality Assurance

The Quality Assurance audit plan and checklist that was used to monitor ILRT with proper sign-offs.is contained in Section V, OP 13100.1.

### 12. Test Exceptions

A listing of all test exceptions including changes in containment system boundaries instituted by licensee to conclude successful testing is contained in Section V, OP 13100.1.

### 13. Instrumentation Malfunctions

There was no sensor malfunction, repairs, or methods used to redistribute volume fractions to operating instrumentation.

### 14. Confidence Limits

A review of confidence limits of test results with accompanying computer printouts where applicable.

### 15. Verification Leak Rates

Descriptions of methods used, superimposed leakage, with calibration information on totalizers and flowmeters along with calculations that were used to measure the verification leakage rate is contained in Section V, OP 13100.1

### 16. Graphs

Plots presenting data obtained during the test.

### 17. P&ID's

The P&ID's of systems readily available.

### IV. ANALYSIS AND INTERPRETATION

The Integrated Leakage Rate Test results at the upper 95% confidence level, L  $_{\rm tm}$ , 0.033%/day (Mass Point analysis) and 0.060 (Total Time analysis), satisfy the acceptance criteria. The acceptance criterion is L  $_{\rm tm} \leq 0.75 L_{\rm t} = 0.0772\%/$  day @ P  $_{\rm t} \geq$  25 psig.

Dewpoint #	Volume Fraction
1.	0.268
2.	0.267
3.	0.267
4.	0.198
	1.000
RTD #	
1.	0.1600
2.	0.3620
3.	0.0200
4.	0.0200
5.	0.0200
6.	0.0200
7.	0.0200
8.	0.0200
9.	0.0165
10.	0.0165
11.	0.0165
12.	0.0165
13.	0.0165
14.	0.0165
15.	0.0165
16.	0.0165
17.	0.0165
18.	0.0165
19.	0.0165
20.	0.0165
21.	0.1600
	1.0000

### SUMMARY DATA

TURKEY POINT UNIT 3 ILRT ALMAX = 0.102

VOL = 1550000.00

TIME	DATE	TEMP	PRESSURE
2245	319	538.888	41.9658
2300	319	538.877	41.9647
2315	319	538.868	41.9640
5330	319	538.851	41.9635
2345	319	538.849	41.9625
0	350	538.948	41.9619
15	350	538.839	41.9618
30	320	538.828	41.9605
45	320	538.823	41.9608
100	320	538.814	41.9592
115	350	538.806	41.9584
130	020	538.801	41.9578
145	380	538.796	41.9569
500	320	538.785	41.9568
215	320	538.787	41.9558
530	320	538.781	41.9553
245	380	538.776	41.9555
300	320	538.770	41.9544
315	380	538.764	41.9538
330	350	538.758	41.9528
345	320	538.748	41.9524
400	320	538.746	41.9517
415	320	538.737	41.9510
430	320	538.738	41.9510
445	320	538.731	41.9507
500	320	538.730	41.9495
515	320	538.723	41.9498
530	320	538.716	41.9490
545	320	538.707	41.9483
600		538.707	41.9474
615		538.704	41.9475
630		538.695	41.9467
645	320	538.695	41.9462
700		538.690	41.9458
715	350	538.687	41.9456
730	350	538.679	41.9450
745		538.679	41.9444
800	320	538.675	41.9446
815	320	138.667	41.9436
830	350	538.665	41.9433
845	350	538.660	41.9429
900	320	538.658	41.9431
915	350	538.656	41.9417
930		538.651	41.9420
945	350	538.650	41.9419
1000	350	538.645	41.9415
1015	350	538.650	41.9407
1030		538.649	41.9412
1045		538.651	41.9408
(	0	0.0	0.0

#### TURKEY POINT UNIT 3 ILET

## TREND REPORT LEAKAGE RATES (WEIGHT PERCENT/DAY) TOTAL-TIME ANALYSIS

TIME AND DATE AT STAFT OF TEST: 2245 0319 ELAPSED TIME: 12.00 HOUPS

MO. DATA POINTS	ELAPSED TIME	MEAN MEASURED LEAKAGE PATE	CALCULATED LEAKAGE PATE	CHG IN CALC L/P FROM LAST POINT	UPPER 95'
10	2.25	0.017	0.013		0.093
11	2.50	0.017	0.016	0.003	0.089
12	2.75	0.018	0.019	0.003	0.000
13	3.00	0.019	0.023	0.004	0.086
14	3.25	0.019	0.088	-0.001	0.081
15	3.50	0.020	0.026	0.004	0.082
16	3.75	0.021	0.028	0.008	0.081
17	4.00	0.021	0.028	-0.001	0.078
18	4.25	0.022	1. (29	0.001	0.077
19	4.50	0.023	0.031	0.002	0.078
20	4.75	0.083	0.033	0.001	0.077
21	5.00	0.023	0.033	0.000	0.076
22	5.25	0.024	0.034	0.001	0.075
83	5.50	0.024	0.034	0.000	0.075
24	5.75	0.025	0.034	0.000	0.074
25	6.00	0.025	0.034	-0.000	0.073
26	6.25	0.025	0.035	0.001	0.072
27	6.50	0.025	0.036	0.000	0.072
28	6.75	0.026	0.035	-0.000	0.071
29	7.00	0.026	0.035	-0.000	0.070
30	7.25	0.026	0.035	0.000	0.070
31	7.50	0.026	0.035	-0.000	0.069
35	7.75	0.026	0.035	-0.000	0.068
33	8.00	0.026	0.035	0.000	0.068
34	8.25	0.027	0.036	0.000	0.067
35	8.50	0.027	0.036	-0.000	0.067
36	3.75	0.027	0.035	-0.000	0.066
37	9.00	0.027	0.036	0.000	0.066
38	9.25	0.027	0.035	-0.000	0.065
39	9.50	0.027	0.035	-0.000	0.064
40	9.75	0.027	0.035	-0.000	0.064
41	10.00	0.027	0.035	-0.000	0.063
42	10.25	0.027	0.034	-0.000	0.063
43	10.50	0.027	0.035	0.000	0.063
44	10.75	0.027	0.034	-0.000	0.062
45		0.027	0.034	-0.000	0.061
	11.00	0.027	0.034	-0.000	0.061
46	11.50	0.027	0.034	0.000	0.061
47		0.028	0.034	-0.000	0.060
48 49	11.75	0.028	0.034	0.000	0.060

THE CALCULATED LEAKAGE RATE

0.034

### TURKEY POINT UNIT 3 ILPT

### LEAKAGE RATE (WEIGHT PERCENT/DAY) TOTAL-TIME ANALYSIS

TIME AND DATE AT START OF TEST: 2245 0319 ELAPSED TIME: 12.00 HOURS

TIME	TEMP.	PRESSURE (PSIA)	MEASURED LEAKAGE RATE	
2245	538.988	41.9658		
2300	538.877	41.9647	0.056	
2315	538.868	41.9640	0.029	
2330	538.851	41.9635	-0.044	
2345		41.9625	0.011	
0	538.848	41.9619	0.036	
15	538.839	41.9618	0.007	
3.0	538.828	41.9605	0.021	
45	538.823	41.9602	0.015	
100		41.9598	0.021	
115	538.806	41.9584	0.023	
130	538.801	41.9578	0.025	
145	538.796	41.9569	0.033	
200	538.785	41.9568	0.017	
215	538.787	41.9558	0.035	
230	538.781	41.9553	0.033	
245	538.776	41.9555	0.023	
300	538.770	41.9544	0.030	
315	538.764	41.9532	0.037	
330	538.758	41.9528	0.035	
345	538.748	41.9524	0.029	
400	538.746	41.9517	0.033	
415	538.737	41.9510	0.032	
430	538.738	41.9510	0.031	
445	538.731	41.9507	0.027	
500	538,730	41.9495	0.037	
515	538.723	41.9492	0.033	
530	538.716	41.9490	0.029	
545	538.707	41.9483	0.028	
600	538.707	41.9474	0.034	
615	538.704	41.9475	0.030	
630	538.695	41.9467	0.030	2340 014
1982 1983 1984	538.695	41.9462	0.033	2040 014
700	538.690	41.9458	0.032	
	538.687	41.9456	0.031	
	538.679		0.030	
745	538.679	41.9444	0.033	

### TABLE 4 (cont.)

### TURKEY POINT UNIT 3 ILPT

### LEAKAGE RATE (WEIGHT PERCENT/DAY) TOTAL-TIME ANALYSIS

TIME AND DATE AT START OF TEST: 2845 0319 ELAPSED TIME: 18.00 HOURS

800 538.675 41.9446 0.029 815 538.667 41.9436 0.030 830 538.665 41.9433 0.030 845 538.660 41.9429 0.029 900 538.658 41.9431 0.027 915 538.656 41.9417 0.033 930 538.651 41.9420 0.028 945 538.650 41.9419 0.028	IME TEMP. (R)	PRESSURE (PSIA)	MEASURED LEAKAGE RATE
815 538.667 41.9436 0.030 830 538.665 41.9433 0.030 845 538.660 41.9429 0.029 900 538.658 41.9431 0.027 915 538.656 41.9417 0.033 930 538.651 41.9420 0.028 945 538.650 41.9419 0.028	900 500 275	at Gaas	0.029
830 538.665 41.9433 0.030 845 538.660 41.9429 0.029 900 538.658 41.9431 0.027 915 538.656 41.9417 0.033 930 538.651 41.9420 0.028 945 538.650 41.9419 0.028			
900 538.658 41.9431 0.027 915 538.656 41.9417 0.033 930 538.651 41.9420 0.028 945 538.650 41.9419 0.028			
915 538.656 41.9417 0.033 930 538.651 41.9420 0.028 945 538.650 41.9419 0.028	845 538.660	41.9429	0.029
930 538.651 41.9420 0.028 945 538.650 41.9419 0.028	900 538.658	41.9431	0.027
945 538.650 41.9419 0.028	915 538.656	41.9417	0.033
테이크 그 사람들이 아니는 그리고 아니다 아니다 아니라 아니라 아니는 아니는 아니는 아니라 아니다	930 538.651	41.9420	0.028
	945 538.650	41.9419	0.028
000 538.645 41.9415 0.027	000 538.645	41.9415	0.027
015 538.650 41.9407 0.033	015 538.650	41.9407	0.033
030 538.648 41.9412 0.029	030 538.648	41.9412	0.029
045 538.651 41.9408 0.031	045 538.651	41.9408	0.031
	EASURED LEAKAGE	PATES	_

MEAN OF MEASURED LEAKAGE RATES	=	0.028
STD. DEVIATION OF MEASURED LEAKAGE RATES		0.013
MAXIMUM ALLOWABLE LEAKAGE PATE	_	0.102
75 % OF MAXIMUM ALLOWABLE LEAKAGE RATE	=	0.077
THE UPPER 95% CONFIDENCE LIMIT	=	0.060
THE CALCULATED LEAKAGE RATE	=	0.034

### TURKEY POINT UNIT 3 ILPT

### LEAKAGE RATE (WEIGHT PERCENT/DAY) MASS-POINT ANALYSIS

TIME AND DATE AT START OF TEST: 2245 0319 ELAPSED TIME: 12.00 HOURS

TIME	TEMP (R)	PPESSURE (PS14)	CIMT. AIR MASS (LBM)	MASS LOSS (LBM)	TOT.AVG. MASS LOSS (LBM/HR)
2245	538.888	41.9658	325804		
2300	538.877	41.9647	325802	1.9	7.5
8315	538.868	41.9640	325802	-0.0	3.8
2330	538.851	41.9635	325909	-5.4	-6.0
2345	538.849	41.9685	325803	5.9	1.4
. 0	538.848	41.9619	325798	4.7	4.9
15	538.839	41.9618	325863	-4.7	1.0
3.0	538.828	41.9605	325799	3.4	2.8
45	538.823	41.9602	325800	-0.7	€.1
100	538.814	41.9592	325798	2.3	2.9
115	538.806	41.9584	325796	1.4	3.2
130	538.801	41.9578	385795	1.6	3.5
145	538.796	41.9569	325791	4.0	4.5
500	538.785	41.9568	325797	-5.9	2.3
215	538.787	41.9558	325788	9.0	4.7
230	538.781	41.9553	385787	0.2	4.5
245	538.776	41.9555	385798	-4.6	3.1
300	539.770	41.9544	325787	4.9	4.0
315	538.764	41.9538	325781	5.7	5.
330	538.758	41.9528	325782	-0.5	4.7
345	538.748	41.9524	325785	-2.9	3.9
400	538.746	41.9517	325781	4.2	4.5
415	538.737	41.9510	325781	-0.0	4.3
430	538.738	41.9510	325780	0.6	4.2
445	538.731	41.9507	325782	-1.9	3.7
500	538.730	41.9495	325773	8.7	5.0
515	538.723	41.9492	325775	-1.9	4.5
530	538.716	41.9490	325778	-2.7	3.9
545	538.707	41.9483	325778	-0.0	3.8
600	538.707	41.9474	325771	7.0	4.6
615	538.704	41.9475	325773	-2.6	4.1
630	538.695	41.9467	325773	0.8	4.1
645	538.695	41.9462	325769	3.9	4.4
700	538.690	41.9458	325769	0.1	4.3
715	538.687	41.9456	325769	-0.3	4.2
730	538.679	41.9450	325769	-0.2	4.0
745	538.679	41.9444	325764	4.7	4.4

### TABLE 5 (cont.)

### TURKEY POINT UNIT 3 ILET

### LEAKAGE RATE (MEIGHT PERCENT/DAY) MASS-POINT ANALYSIS

### TIME AND DATE AT START OF TEST: 2245 0319 ELAPSED TIME: 12.00 HOURS

TIME	TEMP (R)	PRESSURE (PSIA)	CTMT. AIR MASS (LBM)		TOT.AVG. MASS 6005 (CRM/HA)
800	538.675	41.9446	325768	-4.0	3.9
815	538.667	41.9436	325766	2.9	4.1
830	538.665	41.9433	325764	1.1	4.1
845	538.660	41.9429	325764	0.1	4.0
900	538.658	41.9431	325767	-8.8	3.6
915	538.656	41,9417	385757	9.7	4.5
930	538.651	41.9420	385763	-5.4	3.9
945	538.650	41.9419	325763	0.3	9.8
1000	538.645	41.9415	325763	0.1	3.7
1015	538.650	41.9407	325753	9.8	4.4
1030	539.648	41.9412	385758	-5.1	3.9
1045	538.651	41.9408	325753	4.9	4,2
	FREE AIR	VOLUME USET	0 (MILLIONS	OF CU. FT.)	= 1.550
	REGRESSI	The state of the s			
		EPT (LBM)			= 325806
	ZFORE	(LBM/HP)			= -4.2
		ALLOWABLE LE			= 0.106
	75 % OF 1	MAXIMUM ALL	JWABLE LEAKA	SE PATE	= 0.077
	THE UPPER	R 95% CONFII	DENCE LIMIT		= 0.033
	THE CALCI	JLATED LEAKE	AGE RATE		= 0.031

TURKEY POINT UNIT 3 VERIFICATION

LEAKAGE RATE (WEIGHT PERCENT/DAY)
TOTAL-TIME ANALYSIS

TIME AND DATE AT START OF TEST: 1845 0380 ELAPSED TIME: 5.50 HOURS

	TIME	TEMP.	(PSIA)			
	1245	538.638	41.9358			
		538.640	41.9355	0.104		
		538.642	41.9353	0.093		
	1330	The second of th	41.9346	0.000		
	1345	538.633	41.9333	0.121		
	1400	538.628	41.9326	0.111		
	1415	538.630	41.9321	0.117		
	1430	538.619	41.9312	0.102		
	1445	538.614	41.9309	0.087		
		538.615	41.9301	0.099		
	1515	538.616	41.9288	0.121		
	1530	538.611	41.9882			
	1545	538.613	41.9277	0.117		
	1600	538.610	41.9269	0.118		
	1615	538.606	41.9261	0.118		
	1630	538.600	41.9259	0.106		
	1645	538.600	41.9252	0.109		
	1700	538.599	41.9847	0.109		
	1715	538.598	41.9836	0.116		
	1730	538.595	41.9230	0.114		
	1745	538.595	41.9221	0.119		
	1800	538.589	41.9213	0.116		
	1815	538.586	41.9207	0.115		
						0.100
		RED LEAKAG			=	0.109
STD. I	EVIATIO	N OF MEASI	PED LEAKA	E KHIES	=	0.011
VERIFI	CATION	TEST LEAKE	AGE RATE UP	PER LIMIT	=	0.163
			AGE PATE LE			0.111
		D LEAKAGE			•	0.118

### TUPKEY POINT UNIT 3 VERIFICATION

### LEAKAGE PATE (MEIGHT PERCENT/DAY) MASS-POINT ANALYSIS

TIME AND DATE AT START OF TEST: 1245 0320 ELARSED TIME: 5.50 HOURS

TIME	TEMP (P)	PRESSURE (PSIA)	CTMT. AIR MASS (LBM)		TDT.AVG. MASS LDSS (LBM/AR)
1845	538.638	41.9358	325722		
1300	538.640	41.9355	325719	3.5	14.2
1315	538.648	41.9353	325716	2.8	12.6
1330	538.636	41.9346	325714	1.8	10.8
1345	538.633	41.9333	325706	8.3	16.4
1400	538.628	41.9326	325704	2.4	15.0
1415	538.630	41.9381	325699	5.1	15.9
1430	538.619	41.9312	325698	0.3	13.9
1445	538.614	41.9309	325699	-0.7	11.8
1500	538.615	41.9301	325692	6.8	13.5
1515	538.616	41.9288	325681	10.7	16.4
1530	538.611	41.9282	325680	1.6	15.5
1545	538.613	41.9277	325675	5.1	15.9
1600	538.610	41.9269	325670	4.4	16.1
1615	538.606	41.9861	325666	3.8	16.0
1630	538.600	41.9259	325669	-2.1	14.4
1645	538.600	41.9252	325663	5.4	14.8
1700	539.599	41.9847	325660	3.3	14.7
1715	538.598	41.9236	325652	7.9	15.7
1730	538.595	41.9230	325649	2.9	15.5
1745	538.595	41.9221	325642	7.0	16.1
1800	538.589	41.9213	325639	2.6	15.8
1815	538.586	41.9207	325637	2.9	15.6
	FREE AIR	VOLUME USED	(MILLIONS	OF CU. FT.>	= 1.550
	REGRESSI				
		EPT (LBM)			= 325724
	SLOPE	(LBM/HP)			= -15.9
	VERIFICA	TION TEST LE	AKAGE PATE	UPPER LIMIT	= 0.160
	VERIFICA	TION TEST LE	AKAGE PATE	LOWER LIMIT	= 0.108
	THE CALC	ULATED LEAKA	SE RATE		= 0.117

TABLE 8

TUPKEY POINT UNIT 3 STABILIZATION DATA

ľ	TIME	DATE	TEMP	PRESSURE
	1845	319	539.062	41.9828
1	1900	319	539.050	41.9813
1	1915	319	539.040	41.9798
1	1930	319	539.026	41.9788
	1945	319	539.016	41.9771
è	000	319	539.012	41.9765
è	:015	319	539.001	41.9753
-	2030	319	538.987	41.9748
è	2045	319	538.971	41.9734
è	2100	319	538.964	41.9721
1	2115	319	538.952	41.9710
0	2130	319	538.934	41.9701
è	2146	319	538.910	41.9686
	0055	319	538.918	41.9683
	2215	319	538.909	41.9685
è	2230	319	538.905	41.9661

### (TYPE B AND C TESTS)

The following routine local leak rate tests were performed during the reporting period on Unit 3; i.e., since the Unit 3, 1976 operational ILRT (Type A test).

### The following procedures were used:

Operating Procedure 13404.1 - Containment Boundary Isolation Valves Local Leak Rate Test

Operating Procedure 13514.1 - Personnel/Emergency Air Locks

Operating Procedure 13531.1 - Equipment Access Hatches Operating Procedure 13104.1 - Containment Purge Valves

Operating Procedure 13404.2 - Electrical Penetration Canisters

Operating Procedure 13404.1 - Containment Isolation Valves

Operating Procedure 16004.1 - Fuel Transfer Tube Flange

### Penetration Tested

### 1. Personnel Air Lock (entire air lock test)

	TEST DATE	"AS LEFT" LEAK RATE (cc/min)	TEST DATE	LEAK RATE (cc/min)
	12/19/75	0	7/27/77	10
	3/17/76	0	12/15/77	15
	7/13/76	0	1/29/78	30
	11/08/76	0	5/17/78	0
	3/30/77	0	8/31/78	5
	3/30///		3/02/79	40
2.	Emergency A	ir Lock (entire air lock te	st)	
	12/08/75	0	12/05/77	0
	3/18/76	10	1/23/78	0
	7/14/76	19.0	5/05/78	0
	11/09/76	0	8/29/78	20
	3/31/77	40	2/21/79	20
	7/25/77	0		
3.	Fuel Transf	er Flange		
	11/27/75	78.9	3/03/79	335
	1/10/77	80	3/07/79	100
	1/27/78	40		
4.	Equipment H	latch		
	12/11/75	0	2/06/78	0
	12/16/76	0	2/10/78	0
	1/13/77	20	8/05/73	0
	11/09/77	0	2/09/79	0
	1/03/78	60	3/13/79	0
	1/29/78	0	3/25/79	0

"AC TEET"

### FLORIDA POWER & LIGHT COMPANY TURKEY POINT UNIT #3 November 1976 to January 1977 #3 REFUELING

				AS FOUND		AS LEFT	
PEN	VALVE	DATE TESTED	PRESSURE P.S.I.A.	LEAK RATE CC/MIN	PRESSURE P.S.I.A.	LEAK RATE	
1	MOV-750/751	12/28/76	66	2,500		2,500	
2	MOV-744A & B, MOV-734	12/28/76	65.2	160		160	
3	MOV-716A MOV-716B CV-717	11/24/76 11/24/76 11/25/76	65.5 65.7 70	75.46 51.45 330		75.46 51.45 330	
4	MOV-730/732	11/25/76	68	13.72		13.72	
5	CV-516/552	11/19/76	72.3	0		0	
6	550 518	11/19/76 11/19/76	71.6 69.5	0		0	
7	CV-519A CV-522A, B, C	12/02/76	75.5	0		0	
8	CV-951/956A 989A	12/30/76 12/30/76	66 66	140 220		140 220	
9	989B CV-953, CV-956B	11/17/76 11/17/76	71 71	0		0	
10	CV-4658A, B CV-4657	11/20/76	72.7 66	0 110		0 110	
11	MOV-872	11/22/76	70.9	0		0	
12	737A 738	11/25/76 11/25/76	70 70	0		0	
13	737B 739	11/25/76 11/25/76	70 70	0		0	
14	CV-200A, B, C	11/30/76 12/29/76	66	8,000	67.7	100	
	CV-204	11/27/79	74.8	0		0	
15	HCV-121/333 CV-312C	11/27/76 11/27/76	74.75 75.2	10.29		10.29	
16	HV-3-1/2	11/15/76	67.1	0		0	
17	895V	11/16/76	67.6	37.33		37.33	
18	MOV-866A, B CV-869	11/16/76	64.8	102.9		102.9	
19A	CV-890A MOV-880A, 891A 883M	11/16/76 11/16/76	69.9 70.0	34.30		34.30 0	
19В	CV-890B 880B, 891B, 883N	11/16/76 11/16/76	68.0 70.0	68.6 0	23/1 n°	68.6	

#3 REFUELING, PTP UNIT #3 November 1976 to January 1977

			AS F	OUND	AS	LEFT
PEN	VALVE	DATE TESTED	PRESSURE P.S.I.A.	LEAK RATE CC/MIN	PRESSURE P.S.I.A.	LEAK RATE
20	989C CV-955A, B CV-956C	11/23/76 11/23/76	77.7 73.9	0 20		0 20
21/2	22 MOV-1417 MOV-1418	11/24/76	65.5	264		264
23	CV-2821, 2822	11/26/76	72.7	34.3		34.3
24A	297A 298A	11/15/76 11/17/76	71.2 70	0		0
24B	297B 298B	11/18/76 11/17/76	72.8 66	0		0
24C	297C 298C	11/18/76 11/17/76	70.7 69.0	0 17.2		0 17.2
25	MOV-3817, CV-307	11/17/76	72.9	0		0
28A	MOV-1410	11/19/76 12/17/76	66	12,000	72.0	0
28B	MOV-1411	11/19/76 12/17/76	66	21,000	69.6	50
28C	MOV-1412	11/19/76 12/17/76	66	31,000	71.5	35
29	CV-2803 CV-336	1/03/77 1/03/77	69 68.1	30 30		30 30
31	CV-4659A, B	11/20/76	71.7	0		0
32	CV "B" SV-2912	11/19/76 11/20/76	70 71	0		0
33	SV-2913 SV-2911	11/20/76 11/20/76	72 71.5	0		0
34	203, 205	11/26/76	68.9	51.45		51.45
35	2600, 2601	11/24/76	69.3	50		50
36	POV-2602, 2603	12/23/76	68.5	400		400
39	Trans Tub Flange	1/10/77	69.3	80		80
40	Equip Hatch	1/13/77 12/16/76	67.3 75	20		20
41	Pers Air Lock (out) (in)	11/08/76 3/30/77 11/08/76 3/30/77	67.0 65.9 70 71.8	0 0 0		0 0 0
42	CV-855	11/21/76	67.6	400		400
43	MOV-626 736	11/24/76 11/24/76	67.4 68.0	20.58		20.58 6.86
47	CV "A"	12/02/76	66.4	110		110

#3 REFUELING, PTP UNIT #3 November 1976 to January 1977

			AS F	AS FOUND		AS LEFT	
PEN	VALVE	DATE TESTED	PRESSURE P.S.I.A.	LEAK RATE CC/MIN	PRESSURE P.S.I.A.	LEAK RATE CC/MIN	
49	Emerg Air Lock Inner Out	11/09/76 3/31/77 11/09/76 3/31/77	70 69.2 68 66	0 0 0		0 0 0	
52	CV-4663A, B	11/23/76 1/11/77		>40,000	71.7	0	
53	H-V-3-3, 3-4	11/15/76	70	0		0	
54A	860A, 861A	11/20/76	70	0		0	
54B	MOV-860B, 861B	11/18/76	71.6	0		0	
55	CV-955C, D, E CV-956	12/30/76	70	5		5	
58	CV-873A	11/22/76	70	0		0	
59	CV-873B	11/22/76	68	65		65	
60	CV-873C	11/22/76	68	150		150	
58/59/60	MOV-843A, B	11/22/76	75.7	0		0	
61	Valve "C"	12/08/76	70	0		0	
63	CV-2819/2826	11/21/76 1/11/77	66	6,000	66	8,000	
64A	MOV-1425	12/08/76	70.4	30		30	
64B	MOV-1426	12/07/76	71.5	30		30	
64C	MOV-1427	12/07/76	67.8	50		50	
65A	Valve "E"	11/20/76	67.5	0		0	
65B	Valve "F"	1/11/76	66.9	1,000		1,000	
65C	Vaive "G"	11/22/76	68	0		0	
		TOTAL		>124,718.44		14,903	

All electrical canisters were tested and the "as found" leakage was "0" cc/min.

FLORIDA POWER & LIGHT COMPANY TURKEY POINT UNIT #3 November 1976 to February 1978 #4 REFUELING

			AS F	AS FOUND		AS LEFT	
PEN	VALVE	DATE TESTED	PRESSURE P.S.I.A.	LEAK RATE CC/MIN	PRESSURE P.S.I.A.	LEAK RATE CC/MIN	
1	MOV-750/751	1/15/78	66.1	730		730	
2	MOV-744A, B HCV-3-758 FCV-3-605	1/15/78	67.4	55		55	
3	CV-717 MOV-716B MOV-716A	12/09/77 12/05/77 12/05/77	70.81 74.4 74	0 0 58.8		0 0 58.8	
4	MOV-730, 732	12/06/77	69.5	0		0	
5	CV-516, 552	11/30/77	70.1	0		0	
6	CV-518	12/13/77	73.8	75		75	
7	CV-519A, B CV-552, A, B, C	12/01/77	69.9	5		5	
8	CV-951, 956A 989A	11/30/77 12/01/77	69.7 70.4	0		0	
9	CV-953, 956A 989B	12/01/77 12/01/77	70 69.2	0		0	
10	CV-4658A, B CV-4657	12/13/77 12/13/77	70 71.3	50 71		50 71	
11	MOV-872	12/05/77	70.1	0		0	
12	737A, CV-739	12/07/77	69.8	0		0	
13	737B, CV-738	12/07/77	68.4	0		0	
14	CV-200A, B, C	1/16/78	66	13,500	(0.0	250	
	CV-204	2/03/78 12/08/77 1/16/78	65.9	1,900	69.9	359	
15	CV-312C HCV-121, 333	12/07/77 12/07/77	69.62 71.08	15 28		15 28	
16	HV-3-1 & 2	11/29/77	69.5	0		0	
17	895V	12/02/77	/0.1	0		0	
18	MOV-866A, B CV-869	12/01/77	69.5	0		0	
19A	891A, CV-890A MOV-880A	11/30/77 11/30/77	67.6 69.7	60		60 0	
19A							

### #4 REFUELING, PTP UNIT #3 November 1976 to February 1978

			AS F	OUND	AS 1	LEFT
PEN	VALVE	DATE TESTED	PRESSURE P.S.I.A.	LEAK RATE CC/MIN	PRESSURE P.S.I.A.	LEAK RATE CC/MIN
19B	891B, CV-890B MOV-880B	11/30/77 11/30/77	69.7 69.9	0		0
20	955A, B, 956C 989C	11/30/77 11/30/77	69.95 69.7	0		0
21/22	MOV-1417, 1418	12/06/77	68.7	56		56
23	CV-2821, 2822	12/18/77	72.6	. 0		0
24A	298A	12/05/77	70.1	0		0
24B	298B	12/05/77	69.52	10		.0
24C	298C	12/05/77	69.7	. 0		0
25	MOV-381	12/01/77	70.2	0		0
28A	MOV-1410, 127 MOV-1410, 127	12/05/77 12/29/77	67.3	4,800	65.9	14
28B	MOV-1411, 327	12/05/77	67.6	0		0
28C	MOV-1412, 327	12/13/77	68.2	0		0
29	CV-336 CV-2803	1/24/77	68 76.8	30 30		30 30
31	CV-4659A, B	11/30/77	69.8	0		0
32	SV-2912 SV-2912 CV "B"	12/13/77 1/27/77 12/09/77	66.1 68.64	2,000	66.2	98
33	SV-29 <sub>1</sub> 1, 2913 SV-2913 & Iso Va	11/29/77	65.38 65.21	126 148		28 126 148
34	203, 205	12/22/77	69.5	85		85
35	PV-2600, 2601	12/12/77	67	210		210
36	PV-2602, 2603	1/24/78	66.1	9,423		9,423
42	PCV-846 CV-855	12/14/77 12/14/77	66.9 66.4	779 3,500		779
	CV-855	1/26/78			66	1,000
43	MOV-626, 736	12/07/77	70.3	0		0
47	CV "A"	12/01/77	67.9	59		59
52	CV-4668A, B	11/30/77	70.2	0		0
53	HV-3-3 & 4	11/29/77	69.1	23		23
54A	MOV-860A 861A	12/09/77	70.7	0		0
54B	MOV-860B 861B	12/09/77	70.5	0		0
55	CV-955C, D, E CV-956D	12/08/77	70.4	0		0

### #4 REFUELING, PTP UNIT #3 November 1976 to Febru y 1978

			AS F	OUND	AS	LIFT
PEN	VALVE	DATE TESTED	PRESSURE P.S.I.A.	LEAK RATE CC/MIN	PRESSURE P.S.I.A.	LEAK RATE
53	CV-873A	12/06/77	69.05	0		0
59	CV-873B	12/06/77	65	190		190
60	CV-873C	12/05/77	64.91	210		210
58/59/60	MOV-843A, B MOV-843A, B	12/02/77 1/26/78	66.4	2,100	66	1,600
61B	Test Valve "C"	11/28/77	66	0		0
64A	MOV-1425	12/02/77	68.8			10
64B	MOV-1426	12/02/77	70.5	0		0
64C	MOV-1427	12/02/77	69.2	6		6
65A	Valve "E"	1/27/78	69.6	0		0
65B	Valve "F"	1/04/78	69.5	0		0
65C	Valve "G"	1/04/78	69.7	G		0
63	CV-2819/2826 CV-2819/2826	1/24/78 1/27/78	66.7	6,200	66.2	3,538
- 29	Blind Flange	1/27/78	70.7	40		40
40	Inner Annulus	1/29/78 2/10/78	69.0 67.2	0		0
41	Inner Annulus Entire Air Lock	1/29/78 1/29/78	. 69.9 66.1	0 30		0 30
49	Inner Annulus Entire Air Lock	1/23/78 1/23/78	67.6 68.0	0		0
		TOTAL		46,580.8		19,249.8

All electrical canisters were leak rate tested all had "0" leakage except for

<sup>1)</sup> South 5KV "A" RCP electrical canister had a cracked insulator. "As found" leak rate was >50,000 cc/min. The insulator was replaced and the electrical canister was retested, the leakage was "0" cc/min.

<sup>2)</sup> North 5KV "A" RCP electrical canister had a leaking seal and a crack in it. "As found" leakage was 510 cc/min. The insulator was replaced and the electrical canister was retested, the leak rate was "O" cc/min.

# FLORIDA POUER & LIGHT COMPANY TURKEY POINT UNIT #3 1979 #5 REFUELING

			AS FO	DUND	AS 1	LEFT
PEN	VALVE	DATE TESTED	PRESSURE P.S.I.A.	LEAK RATE CC/MIN	PRESSURE P.S.I.A.	LEAK RATE CC/MIN
1	MOV-3-751	2/15/79	66.5	2,500		2,500
5	CV-3-516	1/05/79	68.4	0		0
6	Check Valve 518	1/24/79 2/15/79	66.5	820	66.5	620
7	CV-3-519A, B CV-3-522A, B, C	1/9/79	69.7	0		0
8	CV-3-951 CV-3-956A 989A	2/26/79 1/05/79 1/05/79 1/09/79	65.8 68.6 66.7	30 0 600	67.5	30 0 
9	CV-3-953 CV-3-956B 989B	2/26/79 1/05/79 1/05/79	67.0 68.9 68.6	0 0 0		0 0 0
10	CV-3-4658B PCV-3-1014	1/16/79 1/16/79	70.4 69.9	0		0
11	MOV-3-872	2/21/79	68.6	0		0
14	CV-3-200A, B, C	1/17/79 2/16/79 1/17/79	66.3	20,000	68.7	0 70
15	Check Valve 312C HCV-3-121, 333	2/12/79 2/08/79	68.7 68.8	0		0
16	HV-3-2	1/10/79	66.4	85		85
17	895V	1/11/79	70.2	0		. 0
19A	MOV-3-880A Check Valve 890A	1/03/79 1/03/79	69.2 67.7	15 220		15 220
19B	MOV-3-880B Check Valve 890B	1/03/79 1/03/79	70.7 72.5	0		0
20	CV-3-955A CV-3-955B CV-3-956C	2/26/79 2/26/79 1/11/79	67.9 67.0 70.7	30 0 0		30 0 0
23	CV-3-2821 CV-3-2822	1/15/79 1/12/79 3/07/79 3/09/79	66.2 72.0 66.0	8,000 0 51,000	66.5	8,000 0  0
24A	Check Valve 298A	1/11/79	69.0	0		0

### #5 REFUELING, PTP UNIT #3 1979

			AS F	OUND	AS	LEFT
PEN	VALVE	DATE TESTED	PRESSURE P.S.I.A.	LEAK RATE CC/MIN	PRESSURE P.S.I.A.	LEAK RATE CC/MIN
24B	Check Valve 298B	1/11/79	69.5	0		0
24C	Check Valve 298C	1/11/79	69.2	0		0
25	MOV-3-381	1/11/79	69.9	0		0
29	Check Valve 336 CV-3-2803	1/04/79	67.2 68.6	90 0		90
31	CV-3-4695B	1/12/79	69.4	0		0
32	Check Valve 11-003	1/19/79 2/27/79	69.0	>50,000	68.8	0
	SV-2912	1/18/79 2/26/79 2/26/79 3/11/73	66.0 66.7 66.7	>50,000 1,700 580	66.1	560
33	SV-2911 SV-2913	1/18/79 1/18/79	66.5 66.4	195 140		195 140
34	Check Valve 205	1/04/79 1/05/79 1/08/79 3/02/79	66.0 66.0 66.3	>50,000 16,000 11,000	66.1	10,000
	204	1/04/79	67.6	0		0
35	PV-2601, PV-2600 PV-2601, PV-2600	1/10/79 1/10/79	68.6	35	69.6	10
36	PV-2602, PV-2603	1/10/79 3/12/79	67.8	30	66.5	50
39	Fuel Trans Flange	3/03/79 3/07/79	67.0	335	67.2	100
40	Equip Hatch	2/09/79 3/13/79	84.8 81.8	0		0
41	Personnel Air Lock	3/02/79	66.3/71	.7 40/0		40/0
42	CV-3-855	1/16/79 2/09/79	66.5	>50,000	65.8	3,000
47	Check Valve 10-567	1/09/79	67.9	85		85
52	CV-3-4668B	1/12/79	69.8	0		0
53	HV-3-4	1/10/79	69.1	60		60
54A	MOV-3-861A	1/15/79	69.4	0		0
54B	MOV-3-861B	1/12/79	69.9	0		0
55	CV-3-955C CV-3-955D CV-3-955E CV-3-956D	2/27/79 2/27/79 2/27/79 1/12/79	69.0 68.0 67.0 69.7	0 0 0		0 0 0
61B	Valve "C"	1/19/79	69.2	0	2340	029°

### #5 REFUELING, PTP UNIT #3

		DATE TESTED	AS FOUND		AS LEFT	
PEN	VALVE		PRESSURE P.S.I.A.	LEAK RATE CC/MIN	PRESSURE P.S.I.A.	LEAK RATE CC/MIN
63	CV-3-2819	1/17/79 2/27/79	66.2	820	66.9	50
	CV-3-2826	1/17/79 2/28/79 3/06/79	66.0	>50,000 4,000	65.9	460
65A	Flange "E"	3/25/79	68.5	0		0
65B	Valve "F"	2/20/79 3/05/79 3/25/79 3/26/79	66.7 66.6 66.2	0 0 3,400	65.9	150
65C	Valve "G"	2/20/79 3/25/79 3/26/79	66.6 66.2	4,000	67.2	0
		TOTAL		>342,600		26,560

All electrical canisters were leak rate tested the as found leakage was "0" cc/min.

### APPENDIX A

FAILED TEST REPORT - TYPE A TEST

#### INTRODUCTION

Section V.B.3. of 10CFR50, Appendix J requires a summary report of Type A test leakage rate results that failed to meet test acceptance criteria, which includes an analysis and interpretation of test data, the instrumentation system error analysis and a description of containment conditions causing test failure. The following information is reported in response to this requirement.

### DISCUSSION

The initial Type A test failed because of excessive leakage at the Personnel Airlock equalizing valve shaft seal (inner door). This leak was repaired, and the Containment Leakage Rate Test was successfully conducted.

Prior to beginning the ILRT, the airlock had been local leakage rate tested and the leakage rate found to be essentially zero, i.e., approximately 0.0006%/day. After reaching ILRT test pressure, several hours of data yielded a leakage rate that was out of acceptable limits and was stable as indicated by the Trend Report (see attached Reports). Leak search teams found a leak at the airlock inner door equalizing valve shaft seal. The cavity in the shaft seal was then filled with grease and the leak stopped. A successful TLRT was then performed.

New components for the shaft seal have been ordered from the Pittsburgh-Des Moines Steel Co. (the airlock manufacturer) to effect permanent repairs. Appropriate local leakage rate tests will be performed.

The Type A test data and data analysis showing the excessive leakage rate prior to finding and stopping the leak follow.

The instrumentation system error analysis is based on the Instrumentation Selection Guide (ISG) formula from ANSI N274, Draft No. 2, Revision 3 - November 15, 1978 "Containment System Leakage Testing Requirements". The formula is

ISG = 
$$\frac{1}{2} \frac{2400}{t} \left[ 2 \left( \frac{e_p}{P} \right)^2 + 2 \left( \frac{e_T}{T} \right)^2 + 2 \left( \frac{e_{pV}}{P} \right)^2 \right]^{\frac{1}{2}}$$

The symbols are defined in Appendix G of ANSI N274. Based on the following test conditions:

Test duration:

Containment total pressure:

Containment water vapor pressure:

Containment temperature:

538°R

The error associated with the instrumentation system, ISG, is  $\pm 0.035\%$  per day.

ANSI N274 requires that the ISG shall not exceed 0.25 Lt, or 0.25 (0.1029), or 0.0257. While the ISG is greater than this value, the unacceptable leakage rate can be considered to be accurate based on the stability of the leakage rate as shown by the accompanying Trend Report. The ISG is dependent on test duration. Had the test been continued for three more hours as the final successful ILRT was, the ISG would have been satisfactory. However, this would have been strictly a data gathering exercise and would have served no useful purpose.

As stated in ANSI N274 the ISG formula is not based on a statistical analysis of the actual leakage rate data and is not added to the leakage rate value. The ISG value is used only for instrument selection and loss of sensor criteria. It is reported per the specific requirements of 10CFR50, Appendix J, Section V.B.3.

### SUMMARY DATA

TURKEY	POI	MT	UNIT	3	ILRT	
ALMAX	=	0.1	02			

VOL = 1550000.00

TIME	DATE	TEMP	PRESSURE	
1300	319	539.463	42.0219	
1315	319	539.443	42.0196	
1330	319	539.420	42.0175	
1345	319	539.396	42.0157	
1400	319	539.377	42.0130	
1415	319	539.347	42.0115	
1430	319	539.334	42.0096	
1445	319	539.315	42.0073	
1500	319	539.292	42.0061	
1515	319	539.273	42.0036	
1530		539.257	42.0023	
1545	319	539.239	42.0005	
1600	319	539.226	41.9990	
1615	319	539.213	41.9974	
1630	319	539.203	41.9959	
1645	319	539.180	41.9942	
1700	319	539.160	41.9923	
1715	319	539.153	41.9906	
1730	319	539.140	41.9896	
1745	319	539.131	41.9879	
1300		539.110	41.9366	
1315	319	539.096	41.9351	
1930	319	539.033	41.9840	
1345	319	539.062	41.9328	
1900	319	539.050	41.9913	
1915	319	539.040	41.9798	
1930		539.026	41.9738	
1945	319	539.016	41.9771	
2000		539.012	41.9765	
2015		539.001	41.9753	
	319		41.9742	
		538.971	41.9734	
		539.964	41.9721	
0	- 0	0.0	0.0	

### TURKEY POINT UNIT 3 ILRT

## TREND REPORT LEAKAGE RATES (WEIGHT PERCENT/DAY) TOTAL-TIME ANALYSIS

TIME AND DATE AT START OF TEST: 1300 0319 ELAPSED TIME: 8.00 HOURS

NO. VATA	ELAPSED Time	MEAN MEASURED LEAKAGE RATE	CALCULATED LEAKAGE RATE	CHG IN CALC LZR FROM LAST POINT	UPPER 95% CONF LEVEL
10	2.25	0.098	0.065		0.141
11	2.50	0.096	0.065	0.000	0.1 /
12	2.75	0.095	0.066	0.001	0.133
13	3.00	0.094	0.067	0.001	0.132
14	3.25	0.094	0.070	0.002	0.133
15	3.50	0.094	0.073	0.003	0.134
16	3.75	0.093	0.074	0.001	9.133
17	4.00	0.093	0.074	0.001	0.131
13	4.25	0.093	0.077	0.003	0.133
19	4.50	0.093	0.078	0.001	0.132
20	4.75	0.093	0.981	0.002	0.134
21	5.00	0.093	0.031	0.000	0.133
88	5.25	0.093	0.032	0.000	0.131
33	5.50	0.092	0.031	-0.000	9.130
24	5.75	0.098	0.080	-0.001	0.127
25	6.00	0.091	0.079	-0.001	0.125
36	6.25	0.091	0.079	-0.000	0.123
27	6.50	0.091	0.079	-0.001	0.121
28	6.75	0.090	0.078	0.000	0.121
29	7.00	0.090	0.078	-0.000	0.120
30	7.25	0.090	0.078	-0.000	0.119
31	7.50	0.090	0.073	-0.000	0.117
32	7.75	0.039	0.077	-0.001	0.116
33	8.00	0.089	0.076	-0.001	0.114

THE CALCULATED LEAKAGE RATE

0.076

TURKEY POINT UNIT 3 ILRT

LEAKAGE RATE (WEIGHT PERCENT/DAY) TOTAL-TIME ANALYSIS

TIME AND DATE AT START OF TEST: 1300 0319 ELAPSED TIME: 8.00 HOURS

TIME	TEMP.	PRESSURE (PSIA)	MEASURE LEAKAGE R	7	
1300		42.0219			
1315	The second secon				
1330					
1345	539.396		0.075		
1400	539.377		0.126		
1415	539.347	48.0115	0.062		
		42.0096			
		43.0078			
		#2.0061			
		42.0036			
		42.0023 42.0005			
		41.9990	0.085		
		41.9974	0.033		
			0.094		
		41.9948	0.086		
1700	539.160	41.9923	0.086		
1715	539.153	41,9906	0.096		
1730	539.140	41.9896	0.091		
1745	539.131	41.9879	0.098		
1300	539.110		0.039		
1915	539.096	41.9351	0.089		
1930	539.093	41.9840	0.086		
1345	539.062	41.9828	0.073		
1900	539.050	41.9813	0.030		
1915	539.040	41.9798	0.084		
1930	539.026	41.9788	0.030		
1945	539.016		0.095		
2000	539.012		0.034		
	539.091		0.034		
	539.987		0.081		
		41.9734	1.075		
2100	533.964	41.9721	073		
MEAN OF MEASUR	en Fakas	E PATES		=	0.089
STD. DEVIATION		CONTROL SUCCESSION OF STREET		= '	0.019
MAKIMUM ALLOW	ABLE LEAKA	GE RATE		=	0.102
75 % OF MAXIM	JM ALLOWAB	LE LEAKAGE	RATE	=	0.077
THE UPPER 95%	CONFIDENC	E LIMIT		=	0.114
THE CALCULATED	LEAKAGE	RATE		=	0.076

### TURKEY POINT UNIT 3 ILRT

### LEAKAGE RATE (WEIGHT PERCENT/DAY) MASS-POINT ANALYSIS

TIME AND DATE AT START OF TEST: 1300 0319 ELAPSED TIME: 3.00 HOURS

TIME	TEMP (R)	PRESSURE (PSIA)	CTMT. AIR MASS (LBM)	MASS LOSS		AVG. MASS
			mass (CDm)			, KEDIT HAD
1300	539.463	42.0219	325391			
1315	539.443	42.0196	325386	5.3		23.0
1330	539.420	42.0175	325994	3.4		16.3
1345	539.396	42.0157	325934	-0.5		10.2
1400	539.377	42.0130	335875	9.5		17.1
1415	539.347	43.0115	325331	-6.5		3.5
1430	539.334	42.0096	325 375	6.9		11.5
1445	539.315	42.0079	325972	2.5		11.4
1500	539.292	42.0061	385973	-0.7		9.6
1515	539.273	42.0036	325965	7.9		12.1
1530	539.257	42.0023	325864	0.4		11.0
1545	539.239	42.0005	325961	3.1		11.1
1600	539.226	41.9990	325858	3.8		11.5
1615	539.213	41.9974	325953	4.6		12.0
1630	539.203	41.9959	325347	5.6		12.7
1645	539.190	41.9943	335948	-0.7		11.7
1700	539.160	41.9923	335346	2.7		11.6
1715	539.153	41.9906	325337	9.0		13.1
1730	539.140	41.9996	325937	-0.1		12.3
1745	539.131	41.9379	325829	7.9		13.3
1300	539.110	41.9966	325832	-3.6		12.1
1915	539.096	41.9351	325323	3.2		12.1
1930	539.083	41.9840	325323	0.7		11.7
1345	539.062	41.9828	325831	-3.4		10.6
1900	539.050	41.9313	325327	4.4		10.9
1915	539.040	41.9793	325821	5.5		11.4
1930	539.026	41.9733	325833	-0.7		10.3
1945	539.016	41.9771	325915	7.1		11.5
2000	539.013	41.9765	325313	2.2		11.4
2015	539.001	41.9753	325310	2.7		11.4
2045	538.997		325810	0.1		11.0
2100	538.971	41.9734	325913 325907	-3.5		10.2
2100	533.964	41.9721	350307	5.9		10.6
	FREE HIR	VOLUME USEI	MILLIONS C	F CU. FT.	=	1.55.
	REGRESSI	ON LINE				
	INTERC	EPT (LBM)			= 3	25390
	SLOPE	(LBM/HR)			=	-10.9
		ALLOWABLE LE			=	0.102
			WABLE LEAKAG	E RATE	=	0.077
		95% CONFII			=	0.094
	THE CALC	JLATED LEAKE	HE PATE		=	0.030

Operating Procedure 13,100.1 #3 Integrated Leak Rate Test Master Copy

## Florida Power & Light Company Turkey Point Units 3 & 4

REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE REVIEW/OTSC 470

SEE INSTRUCTIONS ON REVERS	E SIDE.	Since the same of the same of	
Reason for Request:	отѕс     от	Request for Proc. Change	Periodic Proc. Review
2. Procedure Number 0P 1	3100.1	Date of procedure	
Procedure Title: ILR	г		
08 13100.1	shows it	mally closed d	uring an ILRT, ndex A, page 14, penetral
1. Heavan for Change Described A Value 14658 about 1 46		a trip zigna	V (Si) and thus
	,		2340 039
5 Submitted by Fred	& Bonne	<del>tt</del> .	Date 3/19/79
Approved by	Hage		Date 3/19/29
7. Approved by	15/		(SRO) Date 3/19/79
8. Would this change be a change in If yes, a Procedure Change Safe	n the procedures describe ty Evaluation such as in A	d in the FSAR? YesNo. Administrative Procedure 0109.	1 is required to be completed.
0. Completed by			Date
0. Reviewed by			Date
1. Change Reviewed by PNSC on	or F	NSC review not required	
2. Change Approved by		Plant Supt, Date	

# Florida Power & Light Company Turkey Point Units 3 & 4 REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE REVIEW/OTSC 075C NO. 469

1. Reason for Request:	€ OTSC	Request for Proc. Change	Periodic Proc. Review	
2. Procedure Number	3100,1	Date of procedure	MARCH 16, 1979	
			ST - TURKEY POINT	-77
		nended as a result of a periodic		
PAGE 4	SEC 4.5	DELETE PR	ZIDRTO ADD"ABO	OVZ
ENTE	PAKE SENTE Y IS REQUI	ENCE READ" RED ABOVE AL PERSONN	IF A CONTAINMEN 14.3 PSIG, EL BHALL BE	ł 7-
1. Reason for Change Descri	hed Ahove:		WRITTEN IS IN	
STAY TIME	ESTTOM TIME (ESTON)	AVY STANDARD	ING MANUAL, MAUSI DIVING THOLOS, ET IS MODERATI E CAN OPERATI	
SYMPTOMS	DEPTH WILL OFTHE BEN THE SERVE	DS OF NITE	PSIO NO MEDICA	14
SYMPTOMS	DEPTH WIN	L TO 17.7	Or Jerining	14
SYMPTOMS THIS DEPT COVERNOE !	DEPTH WIT OF THE ESK S NECESSAN W CLOSE	L TO 17.7	PSIO NO MEDICA E CIECUMSTANCE	14
AT THAT SYMPTOMS THIS DEPT COVERING  5. Submitted by	DEPTH WIT OF THE ESK S NECESSAN W CLOSE	DS OF NITH	POID NO INFORMATION ON BOOK 3-18-79	
5. Submitted by  7. Approved by	DEPTH WIT OF THE ESK IN ECESSAN WELLSON CH. Cho	DS OF NITH	Date 3-18-79  (SRO) Date 3-18-79  (SRO) Date 3-18-79	9
5. Submitted by  6. Approved by  8. Would this change be a change	DEPTH WIT OF THE ESK IN ECESSAN WELLSON CH. Cho	DS OF NITE	Date 3-18-79 (SRO) Date 3-18-79	9
5. Submitted by  6. Approved by  8. Would this change be a change of the second of the	DEPTH WIT OF THE ESK IN ECESSAN WELLSON CH. Cho	DS OF NITE	Date 3-18-79  (SRO) Date 3-18-79  (SRO) Date 3-18-79  (SRO) Date 3-18-79	9
5. Submitted by  6. Approved by  7. Approved by  8. Would this change be a change by  9. Completed by	OFTHE BEN SEQUAL S NECESSAN W CLOSS AN U CLOSS CA CLOS CA CLOS CA CAS Panage in the procedures describe Safety Evaluation such as in	DS OF NITE	Date 3-18-79  (SRO) Date 3-18-79  (SRO) Date 3-18-79  Date 3-18-79  Date 3-18-79  Date 3-18-79	9

FORM 5714 PEV. 1.74

## Florida Power & Light Company Turkey Point Units 3 & 4 REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE REVIEW

/OTSC	11	07
OTSC NO.	-1	01

NO.	10.	SEE INSTRUCTIONS ON REVERSE	SIDE.		STEET I OF J
	1.	Reason for Request:	□ ofsc	Request for Proc. Change	Periodic Proc. Review
	2.	Procedure Number OP 13	3100.1	Date of procedure _	MARCH9, 1979
		Procedure Title: INTEG	RATED LE	AK- PATE TES	T - TURKEY POINT UNIT 3
RIGINATOR	2	Pg. 24 PENS - ADD ADD	741E, ADD " "TC100; ADD " "TC100; ADD " "TE" 750A" = 75 "741D", ADD"	CLOSED", ADD SIGN CLOSED" ADD SIGN CLOSED" ADD SIGN CLOSED" ADD SIGN DELETE "75CA" ADD	-OFF LINEOFF LINE.  ED" FOR BOTH, DELETE SIGN-OFF LINE.  NO VLV. TC 100"
	Si	Reason for Change Described Ab Pi 13-PEN L - REFLE Pi 24 PEN I - REFLE Pi 13 PEN 5 - REFLE	CT "AS-15" COM	HFIGUENTION, COER.	2340 041
	5.	Submitted by Plubling			Date 3-16-79
-		Approved by	Dlane.	10	Date = 1/2-170,
	7.	Approved by	ulny		(SRO) Date 3-16-70
	8.	Would this change be a change in If yes, a Procedure Change Safety	the procedures described	d in the FSAR? YesNo_dministrative Procedure 0109.1	
DEP I.	9.	Completed by			Date
ان	)	Reviewed by			Date
1	11.	Change Reviewed by PNSC on	or P	NSC review not required	
	12.	Change Approved by		Plant Supt, Date	

Florida Power & Light Company
Turkey Point Units 3 & 4
REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE REVIEW/OTSC

SEE INSTRUCTIONS ON REVER	RSE SIDE.		SHEET 2 OF		
1. Reason for Request:	Отѕс	Request for Proc. Change	Periodic Proc. Review		
Procedure Number		Date of procedure			
Procedure Title:					
	- DELETE SIGN.	-OFF LINE FOR V	LV. 518 FD, DELETE SIGN-OFF LINE		
ADD "549", ADD "CLOSED", ADD SIGN-OFF LINE.  (E) P. 28, PEN 10 - DELETE VLV. TC-87, ADD CAP ON PIPESTUB  (F) P. 15 PEN 14 - CHANGE "201F" TO "201E"  (B) P. 15 PEN 15 - CV 3100" ADD "CV 310B", ADD CLOSED", ADD SIGN-OFF LINE  ADD "CV -311", ADD "CLOSED", ADD SIGN-OFF LINE  (G) P. 18 PEN 29 - ADD "VALVE", ADD CLOSED, ADD SIGN-OFF LINE.  4. Reason for Change Described Above:					
APX A PENG- NO	CORRECT OMIS	CONFIGURATION, CONFIGURATION SUCHS	CORPERT TYPING OMISSION		
5. Submitted by		^	Date		
Approved by ().	Olsone	se le	Date 3-16-79		
7. Approved by			(SRO) Date		
<ol> <li>Would this change be a change If yes, a Procedure Change Safe</li> </ol>	in the procedures described ety Evaluation such as in A	d in the FSAR? Yes No Administrative Procedure 0109.1	is required to be completed.		
9. Completed by Date					
). Reviewed by			Date		
Change Reviewed by PNSC on	or P	NSC review not required			
10. Reviewed by  11. Change Reviewed by PNSC on  12. Change Approved by	or P	NSC review not required  Plant Supt, Date	Date		

#### Florida Power & Light Company Turkey Point Units 3 & 4

REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE REVIEW

OTSC	1	1-	7
OTSC NO.	-+	U	

SEE INSTRUCTIONS ON REVERS	SE SIDE.		SHEET 3 CF J
1. Reason for Request:	Отѕс	Request for Proc. Change	Periodic Proc. Review
Procedure Number  Procedure Title:		Date of procedure	
Pg 37 PEN Pg 19 PEN Pg 20 PEN Pg 20 PEN	31 - CHANGE 32 - ADD"VAG 32 - ADD"VAG 34 - ADD" 20 36 - CHANGE 42 - ADD" 4619	"4 665 B" TO "A  LVE", ADD"CLOSED",  LVE"  "OPPOSITE" TO  L", ADD"CLOSED,  LVEV. TO HOUSED,	", HAD SKN-OFF-LINE
4. Reason for Change Described of Posts PEN31  (I) Posts PEN31  (I) Posts PEN32  (I) Posts PEN32	Above: - CERRELT - CORRECT - AORRECT - CORRECT - CORRECT - CORRECT - CORRECT	TYPO OMISSION OMISSION ERFOR OMISSIONS	2340 043
5. Submitted by			Date
. Approved by	J. Olso	nouse	Date 3-16-79
7. Approved by		<b>计图性系统</b>	(SRO) Date
Would this change be a change     If yes, a Procedure Change Safe	in the procedures describe ty Evaluation such as in A	d in the FSAR? Yes No. Administrative Procedure 0109.	o1 is required to be completed.
9. Completed by			Date
O. Reviewed by			Date
11. Change . viewed by PNSC on	or P	NSC review not required	
12. Change Approved by		Plant Supt, Date	

## Florida Power & Light Company Turkey Point Units 3 & 4

//OTSC	147
10100	21101
OTSC NO.	-1-1

	REQUEST FO	OR PROCEDURE CH	ANGE/PERIODIC PROCE	SHEET 4 OF	
	1. Reason for Request:	otsc	Request for Proc. Change	Periodic Proc. Review	
	Procedure Number  Procedure Title:		_ Date of procedure _		
HIGHNAIOH	(20) Py 22 PEN 65	B-CHANGE PER DELETE "VA B-CHANGE PE AUSELETE" SB-DELETE" ADD "FLANCE SC DELETE"	NETENTION # FROM  EVE P", DELETE"  ENETENTION # FEC  TILET A', DELETE  GE A", ADD" OPEN",  ILET B", DELETE		LINE
	4. Reason for Change Described A (18) Py ZI PENKIB (18) Py 43 PENKIB (20) Py Z-Z PENKSB (21) Py 22 PENKSB	- REFLECT "A - REFLECT "A - REFLECT"	AS-15' CONFIGURA	TICH	
	5. Submitted by			Date	
1	Approved by A	. Olson	whe a	Date 3-16-79	
	7. Approved by			(SRO) Date	
	Would this change be a change if If yes, a Procedure Change Safe     Completed by	in the procedures describe ty Evaluation such as in A	Administrative Procedure 0109.1	is required to be completed.	
	10. Reviewed by			Date	
				Date	
-	11. Change Reviewed by PNSC on	or F	PNSC review not required		
	12. Change Approved by		Plant Supt, Date		

### Florida Power & Light Company

Turkey Point Units 3 & 4

REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE REVIEW/OTSC

				OTSC NO. 4		
	1. Reason for Request:	SE SIDE.	Request for Proc. Change	Periodic Proc. Review		
	2. Procedure Number		Date of procedure			
	Procedure Title:					
ORIGINATOR	PR 44 PEN PS 21 PEN 25 13 PEN	65B - DELET 65C - DELET 60 - DELET 29 - ADD 31 ADD NOT	TE VALVE"ILET A TE VLV ESO", DE	", ADD WORDS FLANGE A ( OFFN)"  ", ADD WORDS" FLANGE B ( OFFN)"  LETE COSTO, DITTER SAN-OFF LANG		
	4. Fleason for Change Described (22) Pg 44 PEH. GS	REFLEC REFLEC REFLEC 9 - CORRECT	- omission			
	5. Submitted by		^	Date		
	Approved by	1. Olya	used	Date 2-16-79		
	7. Approved by			(SRO) Date		
	8. Would this change be a change in the procedures described in the FSAR? YesNo If yes, a Procedure Change Safety Evaluation such as in Administrative Procedure 0109.1 is required to be completed.					
DEPT.	9. Completed by			Date		
D. C.	10. Reviewed by			Date		
	11. Change Reviewed by PNSC on	or Pi	NSC review not required			
	12. Change Approved by		Plant Supt, Date			

1. Reason for Request:	[] orsc	Request for Proc. Change	Prioc Review				
2. Procedure Number/3/150	.1	Date of procedure _	MARCH 9, 1979				
Procedure Title: INTEGENEED LEAK RATE TEST - TURKEY POINT UNIT 3							
3. Describe Details of Change: (If no changes are recommended as a result of a periodic review, write none)  Pg. 2L - TEN L - DELETE VLV. AT TCBI. ADD NOTE "PEMOVE PLUG".  23. 30 PENIS - CHANGE VLV II FROM 2017 TO 120D							
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2. Change Approved by		Plant Supt, Date					

#### Florida Power & Light Company

#### Turkey Point Units 3 & 4

REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE RE- VOTSC

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Florida Power & Light Company
Turkey Point Units 3 & 4
REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE REVIEW/DTSC

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### Florida Power & Light Company

## Turkey Point Units 3 & 4 REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE REVIEW/OTSC OTSC NO

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# To: Dow Jones

10. Reviewed by

11. Change Faviewed by PNSC on

12. Change Approved by

#### Florida Power & Light Company Turkey Point Units 3 & 4

REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE REVIEW/OTSC TE: SEE INSTRUCTIONS ON REVERSE SIDE. Request for Periodic X orsc 1. Reason for Request: Proc. Change Proc. Review Date of procedure Procedure Title: INTEGRATED LEAK RATE TEST 3. Describe Details of Change: (If no changes are recommended as a result of a periodic review, write none) Delete (SPARE) on RTD #21 and RTD #22 Delete (SPARE) ON RAD #7 and RHD#8 ADD RHD # 9 and RHD # 10 ORIGINATOR 4. Reason for Change Described Above: Revised Data sheet to accomplishe 20 RTD's and 10 RAD. 5. Supmitted by 6. Approved by 7. Approved by (SRO) Date 8. Would this change be a change in the procedures described in the FSAR? Yes\_ No. If yes, a Procedure Change Safety Evaluation such as in Administrative Procedure 0109.1 is required to be completed. DEPT 9. Completed by Date

or PNSC review not required

Plant Supt, Date

FORM 5/14 Rt. V. 1/78

Date

## Florida Power & Light Company Turkey Point Units 3 & 4 REQUEST FOR PROCEDURE CHANGE/PERIODIC PROCEDURE REVIEW/O

OTSC	111	0
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1	Reason for Request:	<b>⊠</b> o⊤sc	Proc. Change	Periodic Proc. Review
2	Procedure Number/3/00  Procedure Title: #3 I I		Date of procedure	3/9/79
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FLORIDA POWER & LIGHT COMPANY
TURKEY POINT UNIT 3
OPERATING PROCEDURE 13100.1
MARCH 16, 1979

1.0 Title:

INTEGRATED LEAK RATE TEST

FOR DOCUMENT CONTROL USE ONLY
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#### 2.0 Approval and List of Effective Pages:

#### 2.1 Approval:

Change dated 3/16/79 Reviewed by PNSC March 16, 1979

Approved by States Plant Supt., March 16, 1979

2.2 List of Effective Pages:

Page	Date	Page	Date	Page	Date	Page	Date
1	3/16/79	17	2/15/79	33	2/15/79	49	3/16/79
2	2/15/79	18	2/15/79	34	2/15/79	50	3/16/79
3	3/16/79	19	2/15/79	35	2/15/79	51	3/16/79
4	2/15/79	20	2/15/79	36	2/15/79	52	3/16/79
5	2/15/79	21	2/15/79	37	2/15/79	53	3/16/79
6	3/16/79	22	2/15/79	38	2/15/79	54	3/16/79
7	2/15/79	23	2/15/79	39	2/15/79	55	3/16/79
8	3/9/79	24	2/15/79	40	2/15/79	56	3/16/79
9	2/15/79	25	2/15/79	41	2/15/79	57	3/16/79
10	3/16/79	26	2/15/79	42	2/15/79	58	3/16/79
11	2/15/79	27	2/15/79	43	2/15/79	59	3/16/79
12	2/15/79	28	2/15/79	44	2/-5/79	60	3/16/79
13	2/15/79	29	2/15/79	45	2/15/79	61	3/16/79
14	3/9/79	30	2/15/79	46	2/15/79	62	3/16/79
15	2/15/79	31	2/15/79	47	3/16/79	63	3/16/79
16	2/15/79	32	2/15/79	48	3/16/79	64	3/16/79
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						69	3/16/79

#### 3.0 Purpose:

The purpose of this test is to assure that leakage through the primary reactor containment, and systems and components penetrating the primary containment does not exceed the allowable leakage rate values as specified in Technical Specification, section 4.4.1 and 10CFR50, Appendix J.

#### 3.1 Method and Discussion of Test Techniques

The Integrated Leak Rate Test shall be performed by the absolute method by which the actual mass of contained air is calculated as a function of time.

#### 3.1.1 Corroboration of Measurement

Provisions shall be made within this test whereby the leak rate measurements shall be validated independently by the use of a Controlled Leakage Rate Test (CLRT). This validation shall be performed for a sufficient duration to accurately establish validation following the measurements at the test pressure. At the end of the overall test, a statistical analysis of the total time leak rate shall be performed.

#### 3.1.2 Test Computations

The equations used in this test procedure may be found in ORNL - NSIC - 26, "Testing of Containment Systems used with Light-Water-Cooled Power Reactors" (Frank C. Zapp) as well as in the proposed Standard for Leakage Rate Testing of Containment Structures," ANS Standards Committee, October 1970. Basically the leak rate of a volume may be computed by watching the test pressure decay, while at the same time, compensating for any changes in temperature and humidity. Thus the leak-rate (L) becomes:

LZ = 24 (1 - 
$$\frac{T_1}{T_2} [P_2 - W_2]$$
) (100). Where  $\frac{T_2}{T_2} [P_1 - W_1]$ )

T1 - Temperature (Rankine) at to, weighted average,

T2 - Temperature (Rankine) at t, weighted average,

P1 - Pressure, psia, at to,

P, = Pressure, psia, at t1,

W1 - Water vapor partial pressure at to, psia

W, - Water vapor partial pressure at t1, psia and

Delta  $t = (t_1 - t_0)$  hours of test duration

L (%) - Percent mass leak rate computed over the duration of the test

A sample sheet marked FOR INFORMATION ONLY may be used for manual calculations and is attached to this procedure. Refer to Appendix E.

Discrete temperature and humidity elements shall be placed throughout the containment, each placed spatially within a calculated fractional volume. The temperature, T, therefore, will be weighted average:

$$\overline{T} = n$$
  $\frac{v_1}{v_{\text{total}}}$ , where 2340 053

V, - Incremental volume at T, and

-Vtot - Total containment volume

#### OPERATING PROCEDURE 13100.1, PAGE 3 INTEGRATED LEAK RATE TEST

In practice it is usual to represent  $V_i$  as a fraction, so that  $V_{tot} = 1.000$ , though  $V_{tot}$  in net cubic feet = 1,550,000. Water vapor pressures shall be handled similarly.

The tabulated volume fractions for these sensors shall be as follows:

$$\begin{array}{c} T_1 \text{ and } T_{21} = 0.1600 \text{ each, where} & \frac{VT_1}{V_{tot}T} + \frac{VT_{21}}{V_{tot}T} = \frac{495,800}{1,550,000} = 0.320 \\ \hline T_2 \text{ and } T_{22} = 0.1810 \text{ each, where} & \frac{VT_2}{V_{tot}T} + \frac{VT_{22}}{V_{tot}T} = \frac{559,786}{1,550,000} = 0.362 \\ \hline T_3 \text{ thru } T_8 = 0.0200 \text{ each, where} & \frac{VT_3 \text{ thru } V_8}{V_{tot}T} = \frac{187,553}{1,550,000} = 0.120 \\ \hline T_9 \text{ thru } T_{20} = 0.0165 \text{ each, where} & \frac{VT_9 \text{ thru } VT_{20}}{V_{tot}T} = \frac{306,861}{1,550,000} = 0.198 \\ \hline \hline V_{Total} = 1.0000 \\ \hline VP_1 = 0.268, \text{ where} & \frac{V_{vpl}}{V_{tot}T} = \frac{415,400}{1,550,000} = 0.268 \\ \hline VP_2 \text{ and } VP_3 = 0.267 \text{ each, where} & \frac{V_{vp2} + V_{vp3}}{V_{tot}T} = \frac{827,739}{1,550,000} = 0.534 \\ \hline V_{Total} = 0.198, \text{ where} & \frac{V_{vp4}}{V_{tot}T} = \frac{306,861}{1,550,000} = 0.198 \\ \hline \end{array}$$

#### 3.1.3 Statistical Handling of Test Data

Least squares analysis of the leak rate calculations will provide the best linear regression fit to the data for the duration of the test period. The effect of instrument error on total-time leak rate and statistical leak rate shall be computed such that the resultant leak rate including this possible error shall have a confidence level of 952.

#### 4.0 Precautions and Limits:

4.1 The primary containment must be pressurized with air of such quality (oil and humidity) that it can be done safely with the least negative influence on the progress of the test. The air should be oil-free and should be cooled with an aftercooler to approximately 80° F to 85° F.

#### OPERATING PROCEDURE 13100.1, PAGE 4 INTEGRATED LEAK RATE TEST

4.2 The air in the containment should be circulated such that the presence of absolutely stagnant air can be prevented. Here it is important that the energy given to the circulating air is minimal. A few horsepower are all that are required, no more than three horsepower shall suffice. The reason for this is to maintain a nearly adiabatic condition of the containment environment once the test is started. The less energy introduced, therefore, the smaller the uncertainty in the resulting measurements. An uncontrolled increase in temperature (such as could be produced by large fans) masks the leak rate.

NOTE: Any fan placed in the containment must pump air of density up to approximately three times greater than standard conditions; modifications, either in supply voltage or blade size/pitch may be required.

- 4.3 Once the test pressure is achieved, approximately four (4) hours should be allotted for stabilization of temperature. Conditions would normally be considered stable when the average temperature does not vary by more than 1.0° F per hour for the last two (2) hours.
- 4.4 Access around the periphery of the containment should be limited to approximately 100 feet during periods of pressurization. These areas should be posted during these periods and limited to authorized personnel only as determined by the Lead Test Engineer. These areas do not include the Fuel Handling Building, Reactor Auxiliary Building (except electrical and mechanical penetration rooms), and any elevation above ground level.
- J4.5 If a containment entry is required prior to 14.3 psig, competent medical personnel shall be available. No personnel shall be allowed to enter the containment above 14.3 psig without conforming to U. S. Navy Diving Manual, NAVSHIPS 250-538, January 1959, stipulations.
- 4.6 All systems associated with the containment must be aligned as required by the Containment Isolation Signal (CIS). All boundary valves shall be closed. Any block valve which could prevent a containment isolation valve from being subjected to containment air pressure shall be left open. The position of the valves shall be per Appendix A. Closure of containment isolation valves shall be accomplished by normal operation and without any preliminary exercising or adjustments (e.g., no tightening of valves after closure by valve motor).
- V4.7 All pressure damageable equipment should be removed from the containment or vented. NOT included is any instrumentation associated with containment isolation or monitoring of accident conditions. Removed equipment shall be properly stored. Included would be the following:

#### EQUIPMENT

#### PROTECTION

Reactor	
Pressurizer	
Pressurizer Relief Tank	
Reactor Coolant Drain T	ank
Accumulators	

Vent	to	Containment
Vent	to	Containment
Vent.	to	Containment
Vent	to	Containment
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Refer to Appendix A

#### EQUIPMENT

Steam Generator Snubber
Oil Reservoir
Polar Crane Hydraulic Reservoir
and Gear Boxes
Manipulator Crane Gear Boxes

Nitrogen, Argon, Oxygen/
Acetylene, (etc) Bottles
Pire Extinguishers
Wooden Scaffolding

Refueling Machine Equipment
TV Monitor

Position Readout Units

Dillon Load Meters and Power Supply

. . . .

#### PROTECTION

Vent to Containment (if required) Vent to Containment (if required) Vent to Containment (if required) Remove from Containment

Remove from Containment Remove from Containment

Remove from Containment (if required) Remove from Containment (if required) Remove from Containment (if required)

- ✓ 4.7.1 All instruments located inside the containment should be checked and properly vented, if necessary, in order to prevent damage. Refer to Appendix F.
- 4.8 All wood platforms and wood scaffolding should be removed. The porous nature of wood will complicate the test and may abort it.
- 4.9 Any water standing on floors, in low spots, in open piping and in tankage should be removed as required and the areas left dry. The success of the test depends also on the changes in humidity during the test. These efforts will tend to stabilize the relative humidity.
- 4.10 Open vents or drains as shown in Appendix B to simulate those conditions that would be expected during a LOCA. All vented systems shall be drained of water to assure exposure of the containment isolation valves to containment air pressure.
  - 4.11 Check proper installation of pressurizing system and blowdown piping without opening inlet valve at penetration.
- 4.12 Check that the oil and moisture content of the air downstream of the filters and temperature are satisfactory. Air quality may be checked by discharging a quantity of air on a piece of white cloth or paper at a convenient vent or drain connection.
- 4.13 Check that installation and calibration of instrumentation for the ILRT is completed and properly documented.
- 4.14 Inspect, close, and seal personnel and emergency air lock inner and outer doors.

### OPERATING PROCEDURE 13100.1, PAGE 6 INTEGRATED LEAK RATE TEST

- 4.15 All electrical equipment should be de-energized within the containment except for those services required and power requirements for circulating fans. Refer to Appendix G.
- ✓ 4.16 A general inspection of the accessible interior and exterior surfaces of the containment structures and components has been satisfactorily performed with no evidence of structural deterioration that may affect containment structural integrity or leak-tightness.
- V4.17 A desk calculator or equivalent instrument shall be available in the unlikely event that the computers, phone connections or terminals are inoperable. Use the data sheet in Appendix E.
- 14.18 The Local Leak Rate Tests should be completed. DELETE OFSC 465 ON
  - 4.19 RCS leakage evaluation per Operating Procedure 0204.2, Schedule of Periodic Tests, Checks, Calibration and Operating Evolutions, Appendix B, cannot be performed during the TLRT. In lieu of this, the containment sump level shall be used to evaluate RCS leakage and this shall be so noted on the daily calculation sheet.

#### 5.0 Related System Status:

5.1 The following instrumentation or equivalent are required for the Integrated Leak Rate Test and are recently calibrated and properly documented:

#### 3.1.1 Temperature Monitoring & Indicating System

Consisting of 22 sensors, selector switches, constant current supply and digital indicator system accuracy of 0.2° F. Leeds & Northrup instrumentation utilizing 100 ohm copper thermohms, Catalog 8187-10-S. Catalog No. 900-9999-9999-1-S numatron numeric display.

#### 15.1.2 Flow Meter

Brooks Hi-accuracy full view rotameter, Model 1110.

RANGE: 0-12.4 scfm at 25 psig, 70° F OR 0-28 scfm at 5 psig, 70° F

### 5.1.3 Dew Point

E G & G Inc. Dew Point Hygrometers Model 660C1-S2, (4 each)

RANGE: -50° C to + 100° C, accuracy + 0.3° C, repeatability + 0.1° C.

### 5.1.4 Precision Pressure Gauge

 Readout unit, calibration accuracy of 0.015% of reading, resolution 0.001% full scale, readout 100,000 counts = full scale.

- 2. Absolute pressure capsule -
  - (1) Range 0-49 psi
  - (2) Range 0-100 psi

Texas Instrument Model 145

## 5.1.5 Pressure Gauge

Range 0-100 psia, graduation -0.1 psia, accuracy 0.1% full scale, sensitivity 0.01% full scale. Wallace & Tiernan Model #61A-1A-0100.

- V5.2 The data for this test shall be manually acquired from the ILRT cabinet containing the instrumentation listed above. These data shall be entered into the ILRT computer program utilizing a Texas Instrument 700 terminal or equivalent. The computer generated report and associated data shall be appended to and form a part of this procedure.
- 75.3 Throughout the test, temperatures, pressure and vapor pressure are monitored. These data are used to compute the leak rate from the perfect gas law, PV=nRT, using either the point-to-point method or the total-time method. Leak rate predictions and estimates of error are provided by first order linear regression over the test duration nominally of 24 hours. Further, the sensitivity to sensor inaccuracy is computed and the final NRC report should demonstrate that the test has met the minimum allowable NRC leakage rates within statistical error bounds.
- 5.4 Containment HVAC system should be available to maintain a temperature of not higher than 90° F or lower than 80° F within the containment. This temperature range should be maintained, if possible, for a matter of days before the beginning of the ILRT. A purge period may be performed whereby the initial volume of "moist" containment air is replaced with "drier" air prior to actual ILRT pressurization.
- 5.5 Shortly before the ILRT, the Containment HVAC system is to be shutdown and isolated from its electrical and cooling water supply.
- 5.6 The reactor shall be in a cold shutdown condition.
- 5.7 The following pressurization and support equipment or equivalent are required for the Integrated Leak Rate Test:

Equipment	Quantity	Capacity	Model No.
Aftercooler (American Std)	2	5000 SCFM/ea.	GT A200
Centrifugal Moisture Separator (Wright-Austin)	2	5000 SCFM/ea.	Туре Т
Centrifugal - Coalescent Oil Separator (General/Zurn)	2	6500 SCFM/ea.	S10 A30

#### OPERATING PROCEDURE 13100.1, PAGE 8 INTEGRATED LEAK RATE TEST

Equipment	Quantity	Capacity	Model No.
Refrigerated Air Drier	1	3200 SCFM	WC-3200
A. E. C. (General/Zurn)	1	4800 SCFM	R-960W
Air Filter (General/Zurn)	1	11,000 SCFM	77111
Air Compressors (Atlas-Copco)	8	900 SCFM/ea.	PIS-900
Blowers (Coppus)	6	1500 SCFM/ea.	HIT-3050-18

<sup>5.8</sup> Valve line-up, as delineated in Appendix A, shall be completed.

### /6.0 References:

The principal guides for the preparation of this test procedure were the 10 CFR part 50 and the American National Standard document outlining the methods for leak-rate testing. Others were consulted, in addition:

- 6.1 Leakage Rate Testing of Containment Structures for Nuclear Reactors, American National Standard ANSI N45.4 1972.
- 6.2 Primary Reactor Containment Leakage Testing for Water-Cooled Power Reactors, Appendix J. Title 10, CFR Part 50.
- 6.3 Testing Containment Systems used with Light-Water-Cooled Power Reactors, Frank Zapp, et al, ORNL NSIC 26 UC 80 Reactor Technology.
- 6.4 Turkey Point Plant Technical Specifications.
- 6.5 Bechtel Corporation preoperational test procedure and final report for Initial Integrated Leak Rate Test of the Reactor Containment Building.
- 6.6 Bechtel Corporation Testing Criteria BN-TOP-1, Revision 1, 11/1/72

#### 7.0 Records Required:

- 7.1 Current I & C calibration sheets for all instrumentation listed in Section 5.1.
- 7.2 A dated log of events and pertinent observations shall be maintained during the test.
- 7.3 Completed ILRT procedure, test log and data sheets constitute quality assurance records and, therefore, shall be routed to the Technical Supervisor for review and routing to the Quality Control Surveillance Technician in accordance with Administrative Procedure 0190.16, Scheduling and Surveillance of Periodic Tests and Checks Required by Technical Sepcifications, and shall be retained in accordance with Administrative Procedure 0190.14, Document Control and Quality Assurance Records.

<sup>5.9</sup> Steam generators are closed to the containment atmosphere; i.e., manways installed, vents and drains closed, level and flow instruments installed and/or root valves closed. Install Pressure gauge on steam side of each steam generator outside of containment.

## OPERATING PROCEDURE 13100.1, PAGE 9 INTEGRATED LEAK RATE TEST

0	Ins	t	r	uc	t	1	on	8	:
	-	-	-	-	-	_		-	_

8.6.3 Data Logger's name

Inst	uccions:
8.1	Precautions and Limits and Related System Status (sections 4.0 and 5.0, respectively) have been satisfactorily completed.
	Verified by H. Simamor Date 3/16/79
	Q. C. Accepted by Bull Bum H Date 3/16/79
8.2	Start pressurization and continue to pressurize until containment air pressure reaches 25.0 psig + 3 psig, -0 psig (alternately the test may be conducted at peak test pressure (Pp) of 50 psig + 5 psig, -0 pisg). Monitor every half hour physical parameters as outlined in "ILRT Data Sheet". Maximum pressurization rate should be 4 to 6 psi/hr. During pressurization:
	8.2.1 Maintain moisture and oil content as low as possible.
	8.2.2 Maintain containment temperature above 60° F and below 120° F.
	8.2.3 Check for leaks.
	NOTE: In any case the pressure should not fall below 25.0 psig (50 psig for the alternate test) for the duration of this test.
	Verified by Date
	. 4/
8.3	The following shall be monitored during the pressurization phase of the test.
	8.3.1 Containment intet air comperature
	Verified by Date
0 4	When desired pressure is achieved, isolate containment pressurizing system
0.4	and leak check the pressurizing system valves
	x. 6
	Verified by Date
8.5	Using ultrasonic leak detectors and/of soap solution check the condition of each suspect local exterior leak area. For form local leak test measurement
	for suspect leaks if required and record.
	Verified by Dave T
	Q. C. Accepted by Date
8.6	Record data as outlined below in Appendix D a minimum of once every one (1) hour. No repairs are allowed once the ILRT commences without returning to
	this point.
	8.6.1 Sample number : 2340 0
	Jampie Hamber
	8.6.2 Date and time

#### OPERATING PROCEDURE 13100.1, PAGE 10 INTEGRATED LEAK RATE TEST

	8.6.4 Containment temperature - 22		
	8.6.5 Containment dewpoint temperature - 4.		
	8.6.6 Containment pressure - 1		
	8.6.7 Outside atmospheric temperature - 1		
	8.6.8 Outside atmospheric pressure - 1		
8.7	7 From the data gathered on at least an hourly ba	sis, determine	that:
	8.7.1 The containment conditions are stablize Stabilization should take approximately		are predictable.
	Verified by	Date	Time
	8.7.2 Forecasted leak rate is significantly Perform local leak survey.	better than al	lowable limits.
	Verified by	Date	Time
8.8	8 Continue ILRT measurements until interpreted criterion is met for a minimum period of eigh Appendix C.	data indicates t (8) hours in	that the ILRT accordance with
	Verified by	Date	Time
	Q. C. Accepted by	Date	Time
3.9	Once predictable and allowable trends have bee results by superimposing a leakage approximatel alternate test). Test duration shall be app length to verify the ability to measure the lea	ly equivalent to proximately fou	verify the test Lt (La for the r (4) hours in
	Verified by	Date	Time
	The following additional data shall be recortest.	ded during thi	s phase of the
	8.9.1 Containment air flow (rotameter), SCFM.		
.10	O Compare the ILRT leak rate and verification 1 above indicated that the ILRT leak rate verification test (difference within 0.25 Lt, the ILRT leak rate and recheck. At the end repeat the verification test, if required.	is not substan	ntiated by the 5 La), continue
	Verified by	Date	Time
	0.0.1		

.2340 061

#### OPERATING PROCEDURE 13-100-1, PAGE 11 INTEGRATED LEAK RATE TEST

	Test Engineer, open blowdown valve and release	air from containment utilizing
	a maximum depressurization rate of approximate	Date 3/20/19 1840
	verified by A. O. Manager	Date of the state of the
8.12	When atmospheric pressure is achieved, consampled followed by containment entry and inspe	
	Verified by CA Ofesco	Date 3 -21-79 Time 1015
	Q. C. Accepted by Authorical	Date 3-21-79Time / :15Am
8.13	Inform Nuclear Plant Supervisor that ILRT is and equipment are turned-over to Operations De	
	Verified by / Hee	Date 3-21-79 Time 1015
	( //////	
8.14	Procedure completed by	Date 3-21-79

2340 063

#### OPERATING PROCEDURE 13100.1, PAGE 9 INTEGRATED LEAK RATE TEST

Inst	ructions:
8.1	Precautions and Limits and Related System Status (sections 4.0 and 5.0, respectively) have been satisfactorily completed.
	Verified by H. Sunnaman Date 3/15/79
	Q. C. Accepted by PW Klimoch Date 3-18-79
8.2	Start pressurization and continue to pressurize until containment air pressure reaches 25.0 psig + 3 psig, -0 psig (alternately the test may be conducted at peak test pressure (Pp) of 50 psig + 5 psig, -0 pisg). Monitor every half hour physical parameters as outlined in "ILRT Data Sheet". Maximum pressurization rate should be 4 to 6 psi/hr. During pressurization:
	8.2.1 Maintain moisture and oil content as low as possible.
	8.2.2 Maintain containment temperature above 60° F and below 120° F.
	8.2.3 Check for leaks.
	NOTE: In any case, the pressure should not fall below 25.0 psig (50 psig for the alternate test) for the duration of this test.
	Verified by Date 3-19-79
8.3	The following shall be monitored during the pressurization phase of the test.
	.8.3.1 Containment inlet air temperature.
	Verified by Date 9-19-79
8.4	When desired pressure is achieved, isolate containment pressurizing system and leak check the pressurizing system valves.
	Verified by Date 3-9-79
8.5	Using ultrasonic leak detectors and/or soap solution, check the condition of each suspect local exterior leak area. Perform local leak test measurement for suspect leaks if required and record.
	Verified by ACKE Date 3-19-79
	Q. C. Accepted by 0.4 11 11 12 Date 3-19-79
8.6	Record data as outlined below in Appendix D a minimum of once every one (1 hour. No repairs are allowed once the ILRT commences without returning to this point.
	8.6.1 Sample number

8.6.3 Data Logger's name

8.6.2 Date and time

#### OPERATING PROCEDURE 13100.1, PAGE 10 INTEGRATED LEAK RATE TEST

	8.6.4 Containment temperature - 22
	8.6.5 Containment dewpoint temperature - 4.
	8.6.6 Containment pressure - 1
	8.6.7 Outside atmospheric temperature - 1
	8.6.8 Outside atmospheric pressure - 1
8.7	From the data gathered on at least an hourly basis, determine that:
	8.7.1 The containment conditions are stablized and trends are predictable. Stabilization should take approximately four hours.
	Verified by 4 Simmen Date 3-9-79 Time /CCO
	8.7.2 Forecasted leak rate is significantly better than allowable limits.  Perform local leak survey.
	Verified by 4. Simmon Date 3-9-79 Time 2200
8.8	Continue ILRT measurements until interpreted data indicates that the ILRT criterion is met for a minimum period of eight (8) hours in accordance with Appendix C.
	Verified by 4. Surmanum Date 3/20/79 Time 10:55  Q. C. Accepted by Pluthyork Date 3-2077 Time 11:02
8.9	Once predictable and allowable trends have been established, verify the test results by superimposing a leakage approximately equivalent to $L_t$ ( $L_a$ for the alternate test). Test duration shall be approximately four (4) hours in length to verify the ability to measure the leak.
	Verified by / Someonica Date / Time
	The following additional data shall be recorded during this phase of the test.
	8.9.1 Containment air flow (rotameter), SCFM.
.10	Compare the ILRT leak rate and verification leak rates. If the comparison above indicated that the ILRT leak rate is not substantiated by the verification test (difference within 0.25 $L_t$ , alternately 0.25 $L_a$ ), continue the ILRT leak rate and recheck. At the end of the extended test period, repeat the verification test, if required.
	Verified by H Sunament Date 3/20/79 Time 18.75
	Q. C. Accepted by Paul H. Bonnett Date 3/30/2/rime 1835

#### OPERATING PROCEDURE 13100.1, PAGE 11 INTEGRATED LEAK RATE TEST

Test Engineer, open blowdown valve and release maximum depressurization rate of approxima	ase air from containment utilizing tely 4 to 6 psi/hr.
Verified by H )	Date 3/20/79 18 40
When atmospheric pressure is achieved, sampled followed by containment entry and in	containment atmosphere shall be spection.
Verified by CA Theory	Date 3 -21-79 Time 1015
Q. C. Accepted by Authorical	Date 3-21-79 Time 10:15 Am
Inform Nuclear Plant Supervisor that ILRT and equipment are turned-over to Operations	
Verified by Africe	Date 3-21-79 Time 1015
Procedure completed by	Date 3-21-79
Procedure reviewed by	
Technical Department Supv.	Date
	Test Engineer, open blowdown valve and release a maximum depressurization rate of approximate verified by  When atmospheric pressure is achieved, sampled followed by containment entry and in verified by  Q. C. Accepted by  Inform Nuclear Plant Supervisor that ILRT and equipment are turned-over to Operations  Verified by  Procedure completed by  Procedure reviewed by

APPENDIX A

VALVE LINE-UP

#### INTEGRATED LEAK RATE TEST

#### APPENDIX A

PEN. 0	FUNCTION	VALVE NO.	POSITION	REMARKS	VERIFIED BY/DATE
1	To RHR	MOV-750 MOV-751	NA NA Closed Closed CLOSED	System in service during ILRT	7HB 3:15:79
1	OTSCALL	7410	CLOSED		PHB 3-15-79
2	From RHR	MOV-744A MOV-744B FCV-605 HVC-758 734 734A	NA NA NA Closed Closed	System in service during ILRT	FWH 3-15.79
3	CCW to RCP's	716E MOV-716A MOV-716B 716D 718A 718B 718C	Closed Closed Closed Closed Closed Closed Closed	Not to be vented and/ or drained	04B 3-15-79 04B 3-15-79 04B 3-15-79 100 3-15-79 100 3-15-79 100 3-15-79
4	CCW from RCP's	MOV-730 730A 730B 727A 727B 727C	Closed Closed Closed Closed Closed Closed	Not to be vented and/ or drained	PHB 3-15-79  DE 3-15-79  PHB 3-15-79  PHB 3-15-79  PHB 3-15-79  PHB 3-15-79
5	PRT to Ga	517# CV-516 552 517B TC-2 TC-80 SV-4600M	Closed Open Open Closed Open Closed Open Closed	1150 467	173 3-16-19 PHB 3-16-11 YOU 3-15-79 VIHO 3-15-79 VIHO 3-15-79 PHB 3-15-79 146 3-15-79 146 3-15-79 146 3-15-79

#### INTEGRATED LEAK RATE TEST

PEN. J	FUNCTION	VALVE NO.	POSITION	REMARKS	VERIFIED BY/DATE
6	N2 to PRT	550 518 TC-3 TC=81	Closed NA Open Open	Check Valve	QHB 3-15-79
7	PW to Standpipes	CV-519A CV-519B CV-522A CV-552B CV-552C 10-532 10-531 10-543 10-563	Closed Closed Closed Closed Closed Open Closed Closed		PHB 3-15-79  (b) 3-15-79  (b) 3-15-79  (c) 3-15-79  (d) 3-15-79
8	Prz. Stm. Sample	CV-951 CV-956A 989A New TC 991 TC-5 New Iso.Vlv.	Closed Closed Closed Open Closed		120 3-15-79 13413 3-15-79 120 3-16-79 1413 3-15-79 1413 3-15-79 1413 3-15-79 120 3-15-79
9	Prz. Liquid Sample	CV-953 CV-956B 989B New TC 992 TC-6 New Iso.VIv.	Closed · Closed Closed Open Closed Open Closed Open Closed		200 3-15-99 PHB 3-15-79 200 3-16-79 RHB 3-15-79 RHB 3-13-79 RHB 3-13-79 DO 3-15-79
10	RCDT & PRT Vent; N <sub>2</sub> to RCDT	4608 CV-4658A CV-4658B 4666A TC-8 4653 4656	Closed Closed Closed Closed Closed Open Open	OTSC 470	PHB 3-15-79 1/HB 3-15-79 PHB 3-15-79 PHB 3-15-79 PHB 3-15-79 PHB 3-15-79 PHB 3-15-79
	075C 15/	4657 549	Bonnet Removed		एसंड ३-१५.ल

#### INTECRATED LEAK RATE TEST

PEN. #	FUNCTION	VALVE NO.	POSITION	REMARKS	VERIFIED BY/DATE
11	Alt. Lohead SIS	887 MOV-863A MOV-863B MOV-872, 940N 940L		Do Not Tag	(pe) 3-16-79 (pe) 3-16-79 (pe) 3-16-79 (pe) 3-15-79 (pe) 3-12-79
12	CCW to Excess LTDN. HX.	737A 737G	Closed Closed	Not to be vented and/ or drained	PHB 3-15-79 PHB 3-15-79
13	CCW from Excess LTDN. HX.	cv-379	Closed	Not to be vented and/ drained	PUB 3-15-79
14	Letdown to Regen HX	309D LCV-460 CV-200A CV-200B CV-200C CV-204 201A 201C 201 201P E 205A 205B	Closed Open Closed Closed Closed Open Closed Open Closed Open Closed Open Closed Open Closed Open		Onl 3-15-79 (h) 3-15-79
15	CVCS to Regen. HX	290 289 286 120B 312C HCV-121 333 120P , 200 202A 120A 202B CV-310A	Closed Closed Closed Closed NA Closed Closed Closed Open Open Open	Check Valve With Fuel in the vessel, 121 should be closed, but operable, 120A should be closed, one Ch. pp Disch. (290,289,or 286) should be open.	WHOL 3-16-79

#### INTEGRATED LEAK RATE TEST

PEN. 0	FUNCTION	VALVE NO.	POSITION	REMARKS	VERIFIED BY/DATE
16	PACVS	HV-3-1 HV-3-2 HV-3-8 HV-1 HV-2 HV-7 HV-9	Closed Closed Closed Closed Open Open	SIN AM FEET HU 7	2HB 3-15-79 2HB 3-15-79 2HB 3-15-71 WASH 3-16-79 WASH 3-16-79 WASH 3-16-79
17	SIS Test Line	850A 850B 850C 850C 850E 850F 837 895U 895K 895K 895P 849A 895V 940M 942E 942F	Closed Open Closed Open		12 3-16-79  57-2 3-16-79  57-2 3-16-79  57-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79  67-2 3-16-79
18	SIS .	MOV-866A MOV-866B MOV-869 942G 883R	Closed Closed Closed Closed Closed	Not to be vented and/ or drained	GTZ 2-/6-79 3-3 2-/6-79 2HD 3-15-79 DHB 3-15-79 ED 3-15-79
19A	Cont't. Spray A	890A MOV-880A 942W 896C 883M 883K 844A 891A 940U	NA Closed Closed Closed Closed Closed Closed Open Open	Check Valve	(CO) 3-11-79 1KDA 3-16-79 KDA 3-16-79 KDA 3-16-79 KDA 3-16-79 KDA 3-16-79 KDA 3-16-79 KDA 3-16-79 KDA 3-16-79

#### INTECRATED LEAK RATE TEST

PEN. Ø	FUNCTION	VALVE NO.	POSITION	REMARKS	VERIFIED BY/DATE
19В	Cont't. Spray B	890B MOV-880B 942V 896D 883N 883L 844B 891B 940T	NA Closed Closed Closed Closed Closed Closed Open	Check Valve	(10) 3-16-79 (10) 3-16-79 (10) 3-16-79 (10) 3-16-79 (10) 3-16-79 (10) 3-16-79 (10) 3-16-79 (10) 3-16-79
20	A&B Hot Leg Sample	CV-955A CV-955B CV-956C 989C New TC A New TC B 993 20 New Iso Vlv A New Iso Vlv B	Closed Closed Closed Closed Open Open Closed Open Closed Closed Closed		100 3-15-99 100 3-15-99 100 3-15-99 100 3-15-99 100 3-15-99 100 3-15-99 100 3-15-99 100 3-15-99 100 3-15-99
21	CCW to Cool rs	MOV-1417 10-871	Closed Closed	Not to be vented and/ or drained	Jap 3-16-79 Find 3-15-79
22	CCW from Coolers	MOV-1418 10-872	Closed Closed	Not to be vented and/ or drained	PHB 3-15-79 PHB 3-15-79
23	Cont't Sump	4671 CV-2821 CV-2822 TC-22 TC-102 4693A 4693B	Closed Closed Closed Closed Open Open Open		2110 3-15-71 2110 3-15-71 2110 3-15-71 9415 3-15-74 7615 3-15-74

#### INTEGRATED LEAK RATE TEST

#### APPENDIX A

PEN. 0	FUNCTION	VALVE NO.	POSITION	REMARKS	VERIFIED BY/DATE
24A	Seal Water to RCP-A	297A 298G 298A 285D 285A	Closed Closed NA Open Open	Check Valve	PHB 3-15-79  Den 3-15-79  PHB 3-15-79  PHB 3-15-79
24B	Seal Water to RCP-B	297B 298H 298B 285E 285E	Closed Closed NA Open Open	Check Valve	PHB 3-15-79 Pap 3-15-79 Pap 3-15-79 PHB 3-15-79
24C	Seal Water to RCP-C	297C -2981 - 2 ic j 298C 285F 285C	Closed Closed NA Open Open	Check Valve	PHB 3-15-79 CAD 3-15-79 WHB 3-15-79
25	RCP S.W. Return	318 380 CV-307 HCV-137 304B 304F 304K 306A 306B CV-389 MOV-381 384A 384B 306C	Closed Open Open		WAN 2-16-79 WHA 3-16-79  GRO 3-15-19  JOD 3-15-19
.29	Inst. Air Supply	336 CV-2803 TC-58 TC-59 TC-107 337A	NA Closed Open Closed Open Closed	Check Valve See Note on App. B, Page 36	pe 3-16-79 fal 3-16-79 fal 3-16-79

#### INTEGRATED LEAK RATE TEST

#### APPENDIX A

PEN. 0	FUNCTION	VALVE NO.	POSITION	REMARKS	VERIFIED BY/DATE
31	RCDT to GA	CV-4659A CV-4659B 4654 4667A 4667B SV-4600E 4655A 4655B	Open Closed Open Closed Open Closed Open Closed Open Open		PAR 3-15-79 PAR 3-15-79 PAR 3-15-79 PAR 3-15-79 PAR 3-15-79 PAR 3-16-79 PAR 3-16-79 PAR 3-16-79 PAR 3-16-79
32	Cont't. Air Sample Return	TC-30 11-003 11-002 TC-31 SV-2912 TC-109 SV-3713	Open NA Open Closed Closed Open Closed	Check Valve	20 3-15-79 (20 3-16-79 (20 3-16-79 (20 3-16-79 (20 3-16-79 (20 3-16-79 (20 3-16-79
33	Cont't. Air Sample	11-001 SV-2913 SV-2911 TC-32 TC-33 TC-110 SV-3709	Open Closed Closed Closed Closed Open Closed		20 3-11-79 100 3-16-79 100 3-16-79 100 3-16-79 100 3-16-79 100 3-16-79 100 3-16-79
34	Service Air :	204 205 203 TC-34A TC-34 216 204	Closed NA Closed Closed Open Open	Check Valve	#M 3-15-79 #M 3-15-79 *** 3-15-79 *** 3-15-79 *** 3-15-79
35	Cont't. Purge	PV-2601 PV-2600 -11-004-	Closed Closed Closed	,, P¥1601 IS 02+FFED	272 3-16-29 7-2-5-11-79 100 3-15-29
36	Cont't. Purge	PV-2603 PV-2602 11-005-71-004	Closed Closed Closed	Timeter t	Jr. 3-16-79 Jr. 3-16-74

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## INTECRATED LEAK RATE TEST

## APPENDIX A

PEN. 0	FUNCTION	VALVE NO.	POSITION	REMARKS	VERIFIED BY/DATE
	075C 4EL	40146	01000	<b> </b>	KD4 3:15:74
42	No to	4618 V	Closed		200 3-16-79
	Accum.	4618 X	Closed		TOOD 3-16-14
		847C	Closed		Jan 3-11-74
		HCV-936.	Closed		Jul 3-15-19
		CV-853A	Closed		1
		CV-853B	Closed		
		CV-853C	Closed		
	./	CV-855			april 3-15-79
	01524		Closed		K3 3-15 74
	+46 le	940R	Closed		KDA 3-15-79
		-TC-50	Open	PLO 4619MI AND_	1 / 1
	Post	FALL VALUE IL TO	1 open	Pc. 344	XD4 3.15.79
	*15¢ 467 -	NEC TRUE	OPEN		OPEN (013-15-0
43	CCW from	FCV-626	Closed	Not to be	15 3 3 15 TH
	RCP Thermal	626A	Closed	vented and/	204 3-10-79
		728A	Closed	venceu and	ace 3-15-77
		7288	Closed		
		728C	Closed		Andread Street, Street
		.200	Olosed		Span 3-15-79
47	Dadasan Haban	10.006			200 - 10
4/	Primary Water		Open		Jap 3-15-79
	to Wash	TC-40	Closed		KD2 3-15-79
	Header	10-567	NA	Check Valve	11.0.1 - 1. 20
		TC-113	Open		WX2 3-16-79
					1.1
52	From RCDT	4669	Closed		WH21 3-16-79
	Pumps	4671	Closed		WH2+ 3-16-79
		1101	Closed		Wy24 3-16-77
		CV-4668A	Open		17. CI-C +CI.
		CV-4668B	Closed		到 3-15-19
		4663A	Open		CED 3-15-79
		4663B	Open		Stell 3-15-19
		4668C	Closed		VIDA 3-15-71
		46680	Open		大XX 3-0-万
			The state of the s		
53	PACVS	HV-3-3	Closed	Refer to	10A 3-15-79
		HV-3-4	Closed	Pen #16	KNA 3-15-79
		HV-3-7	Closed	DESTRUCTION OF THE REAL PROPERTY.	KMA 3-15-79

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## INTEGRATED LEAK RATE TEST

## APPENDIX A

PEN. Ø	FUNCTION	VALVE NO.	POSITION	REMARKS	VERIFIED BY/DATE
54A 54B	Recirc. Sump	MOV-860A MOV-861A 899C MOV-860B MOV-861B 899E 899D 899F 898P 898N	Open Closed	Not to be vented and/ or drained	100 3-11-19 100 3-16-79 100 3-16-79 100 3-16-79 100 3-16-79
55	Accumulator	New TC A New TC B New TC C CV-955C CV-955D CV-955E CV-956D 994 989E TC-117 970A Valve E New Iso Vlv A New Iso Vlv B New Iso Vlv C	Open Open Open Closed Closed Closed Closed Open Open Open Closed Closed Closed Closed Closed Closed Closed Closed Closed		PWH 3-15 79  PWH 3-16-79  PWH 3-16-79  PWH 3-15-79  PWH 3-15-79  PWH 3-15-79  PWH 3-15-79  PWH 3-15-79  PWH 3-15-79  PWH 3-15-79
58 59 60	SIS	MOV-843A MOV-843B 941E 941F 941G 895T -836	Closed Closed Closed Closed Closed Closed	Not to be vented and/ or drained	100 3-16-79 100 3-16-79 100 3-16-77 20 3-15-77 200 3-16-79 WAN 3-16-79
37	Deadweight Tester	Valve C Valve P TC-51 TC-120	Closed Open OTS Closed Open	e	20 3-16-19 Cho 3-16-19 Cho 3-16-19

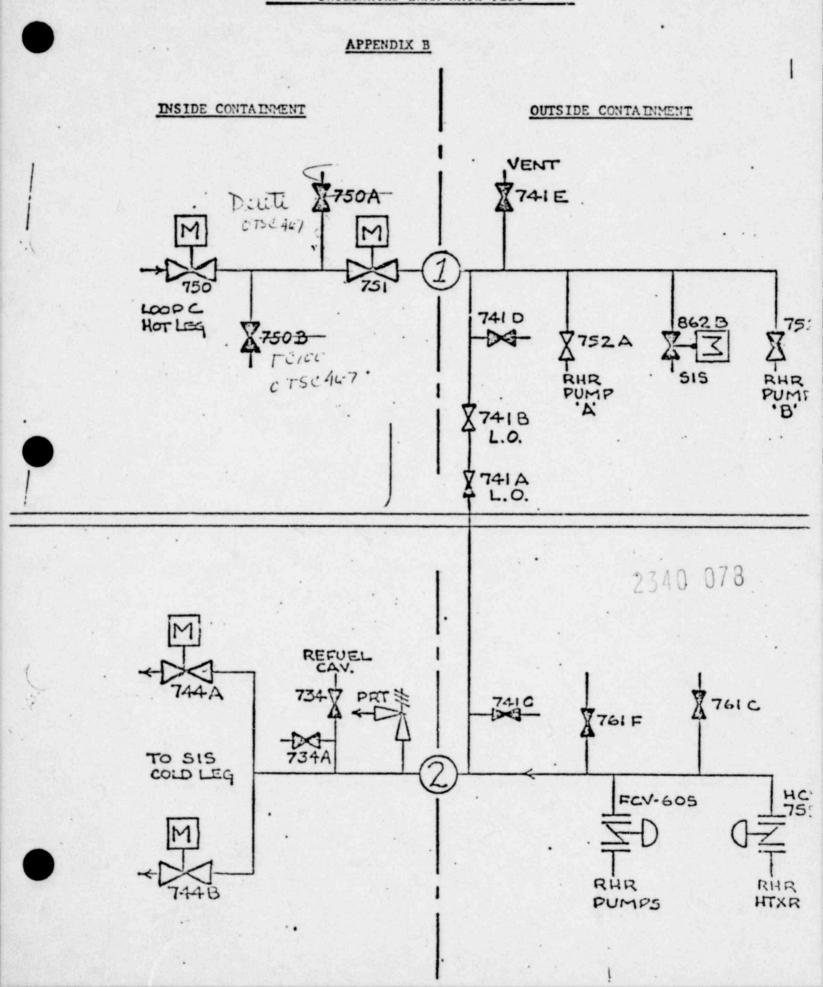
#### OPERATING PROCEDURE 13100.1, PAGE 22 INTEGRATED LEAK RATE TEST

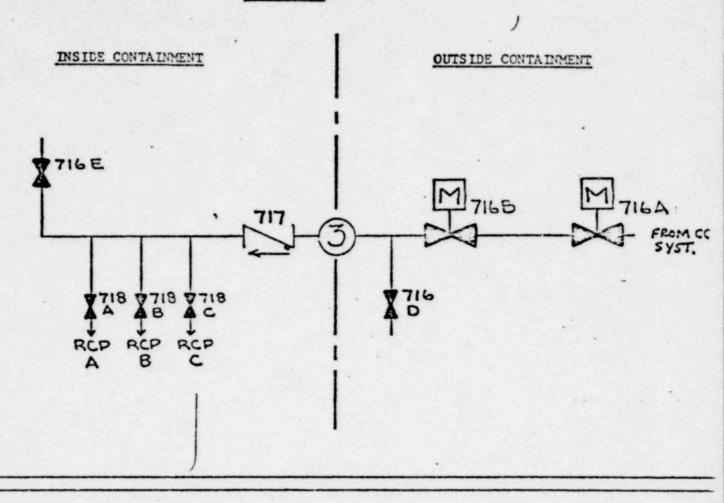
## INTEGRATED LEAK RATE TEST

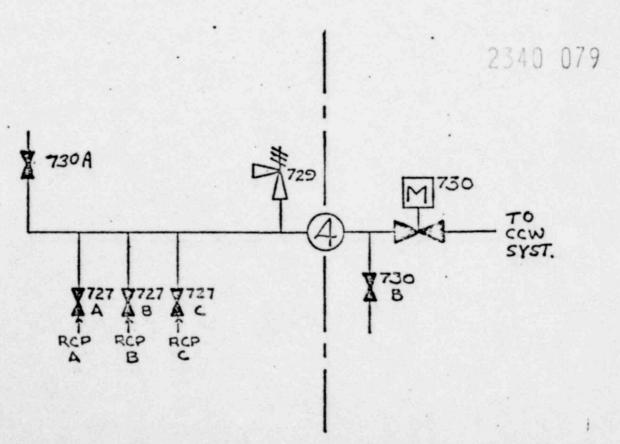
## APPENDIX A

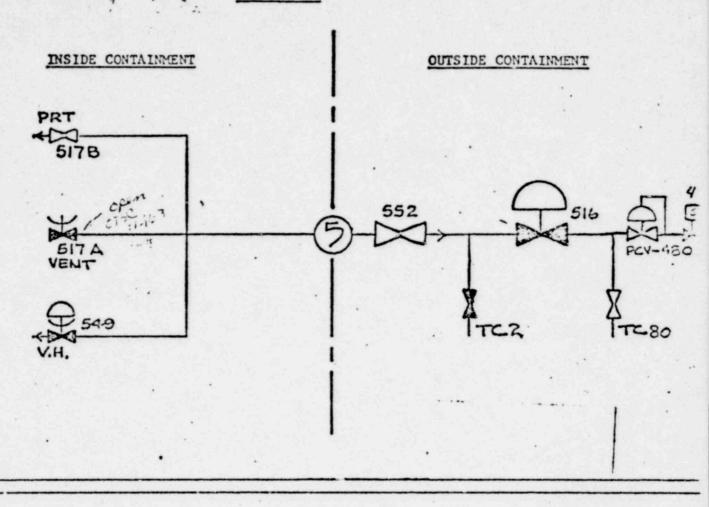
PEN. Ø	FUNCTION	VALVE NO.	POSITION	REMARKS	VERIFIED BY/DATE
65A	From ILRT Compressor	Valve E TC-55	Closed	As Required	Jan 3-16-19
65B	ILRT Press. Sensor Line	Valve F TC-56 FLANGE 'A'	Open Open Closed Crem	In service during ILRT & CLRT	ho 3-16-199 Vivon 3-16-199 Vivon 3-15-79
65C	CLRT Flow Line	TC-57 Valve G	Open CISC 46 Closed Open	In service during CLRT	100 3-16-79 100 3-1/-79
63	Instrument Air Bleed	CV-2819 11-006 CV-2826	Closed Closed Closed		672 376.70 32 3.15.79 323 3.15.71
NA	Reactor Vessel Vent	500	Open		H.S. 3-16-79
NA.	Pressurizer Vents	545 546 547	Open Open Open		H.S. 3-16-79 H.S. 3-16-79 H.S. 3-16-79 H.S. 3-16-79
NA	Accumulators Vents	883A 883D 883G	Open Open Open		H.S. 3-16-79 H.S. 3-16-79 H.S. 3-16-79

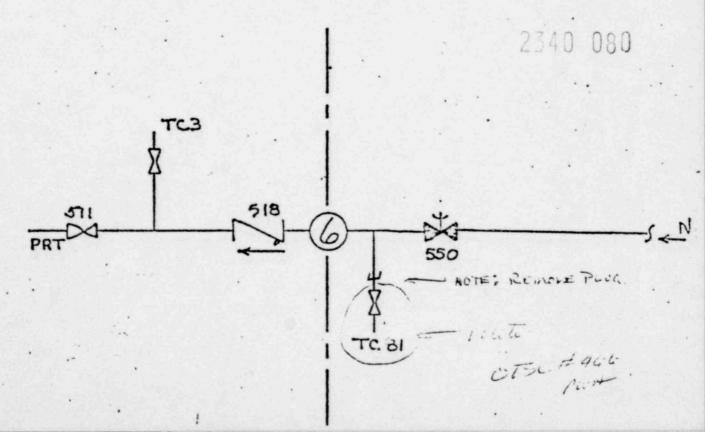
VALVE DRAWINGS

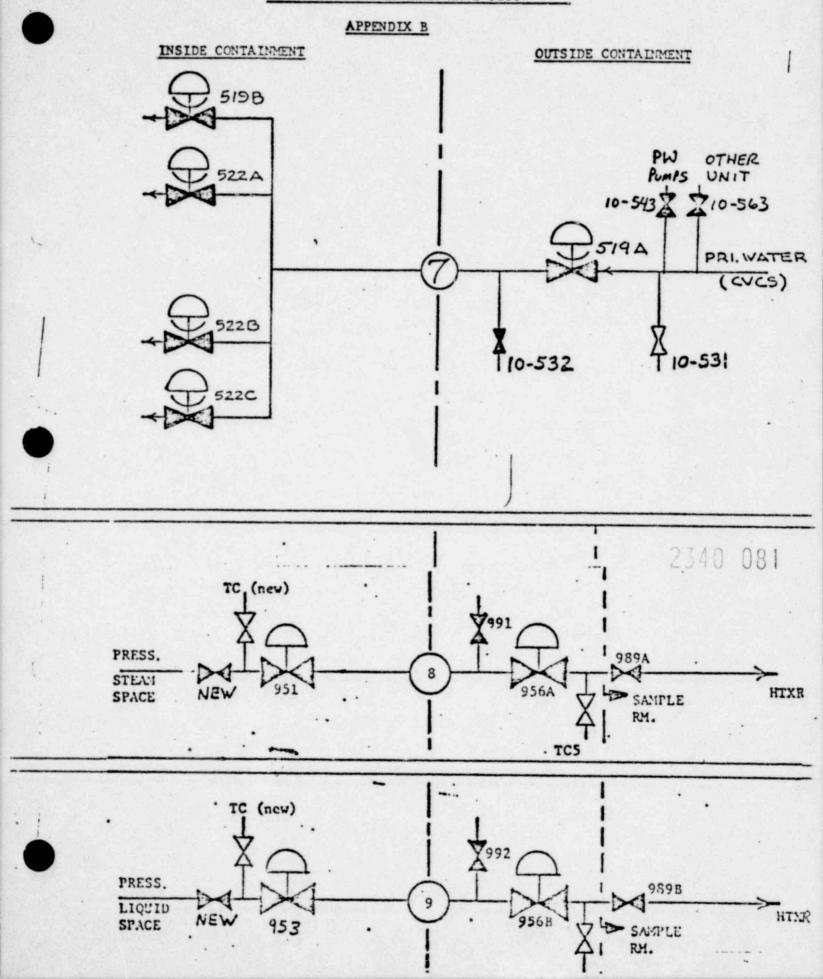


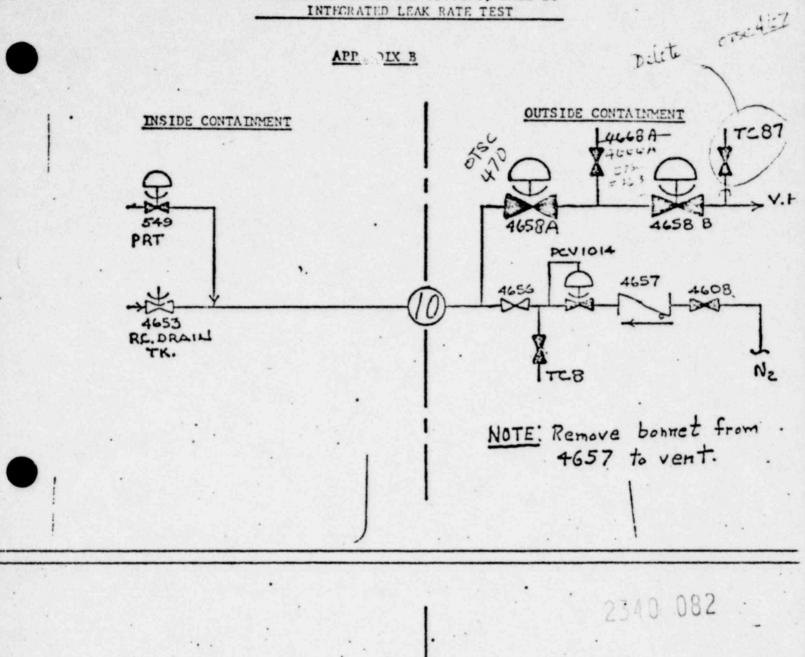


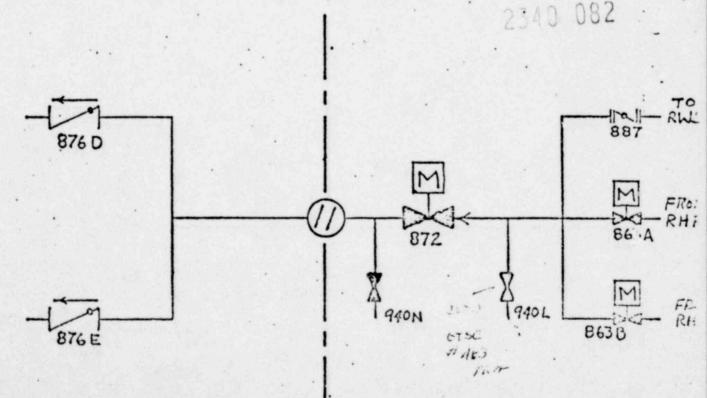


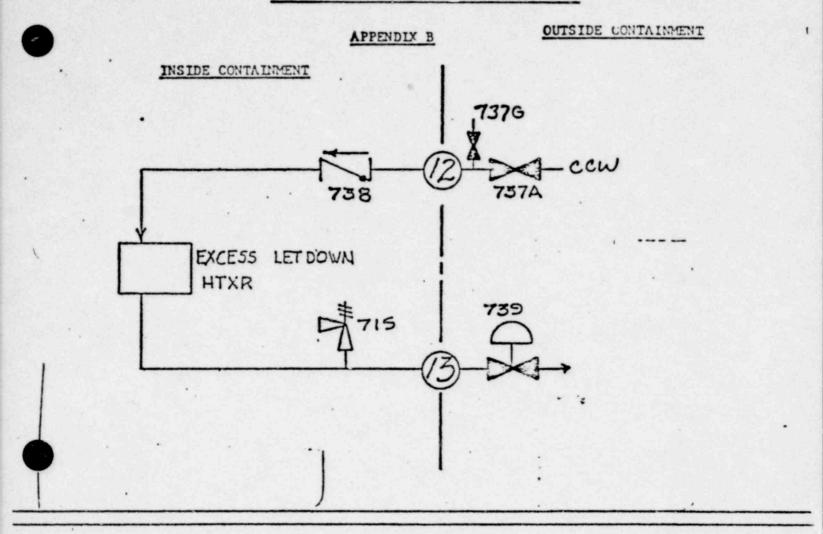


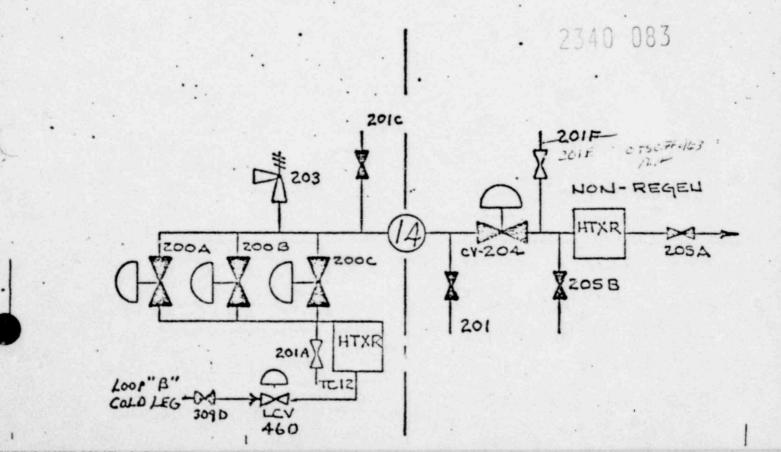


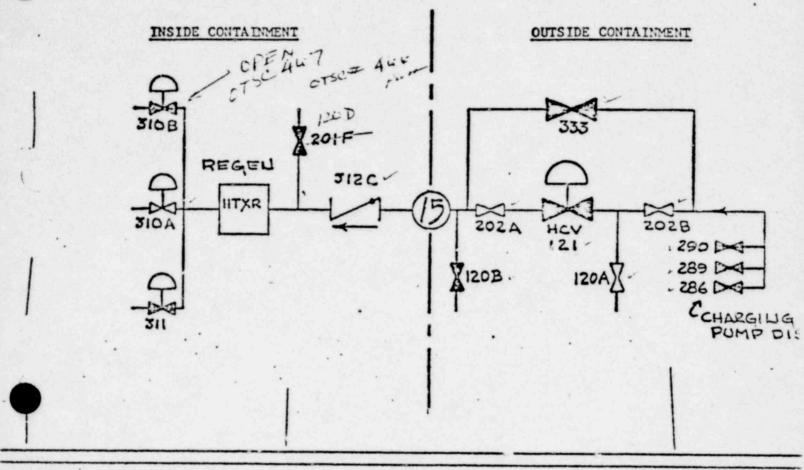


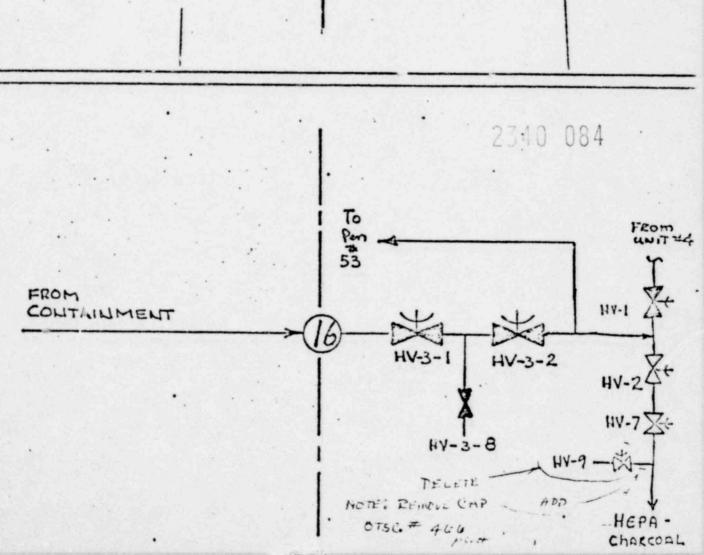


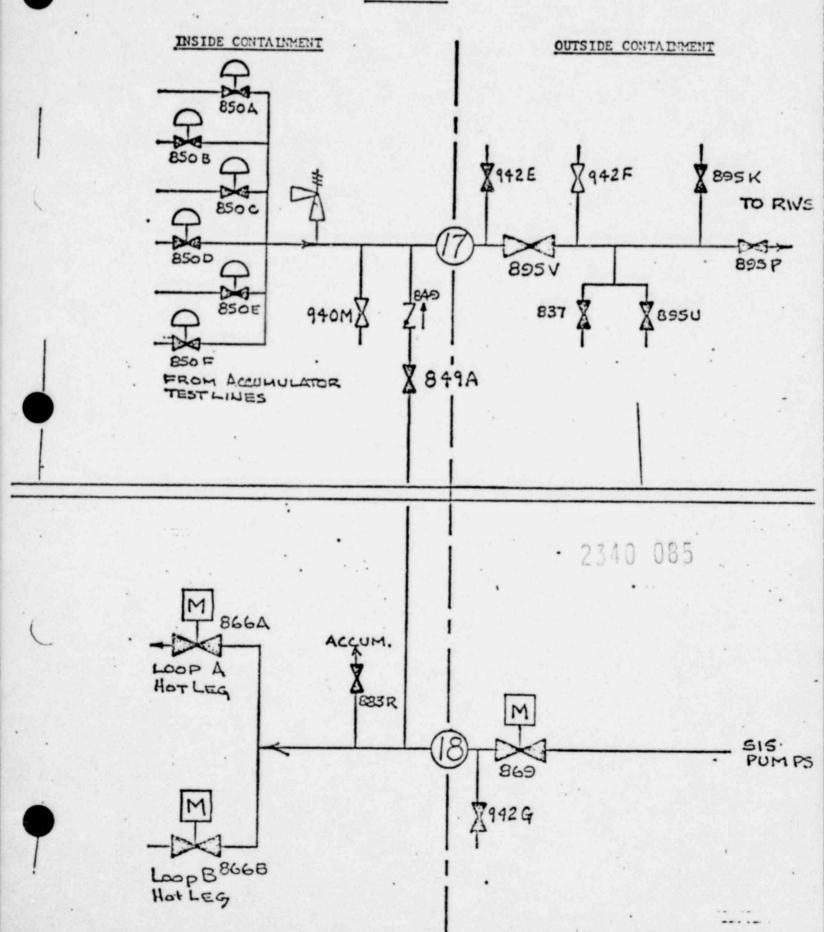


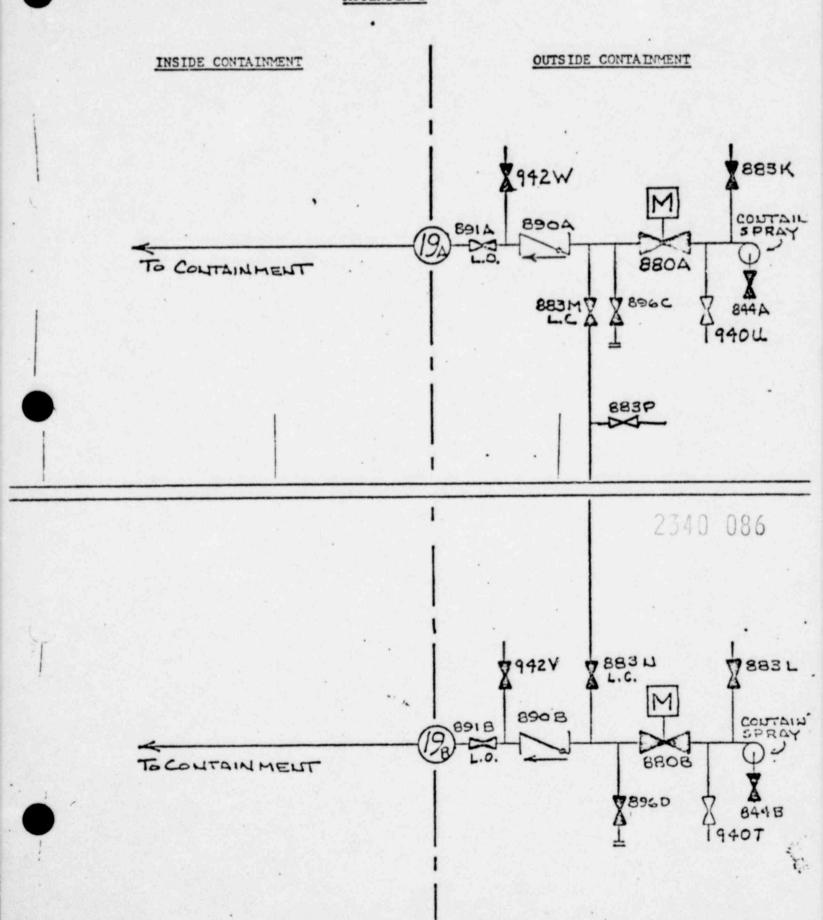


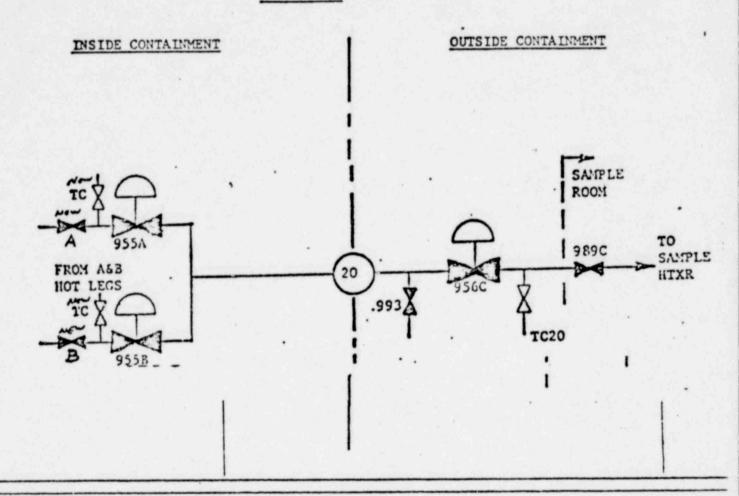


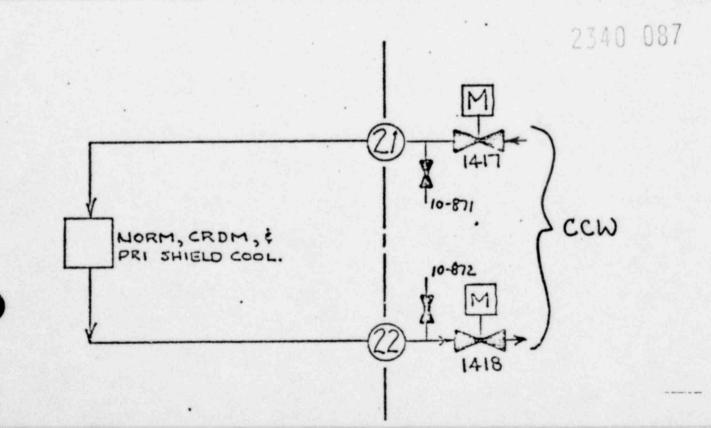




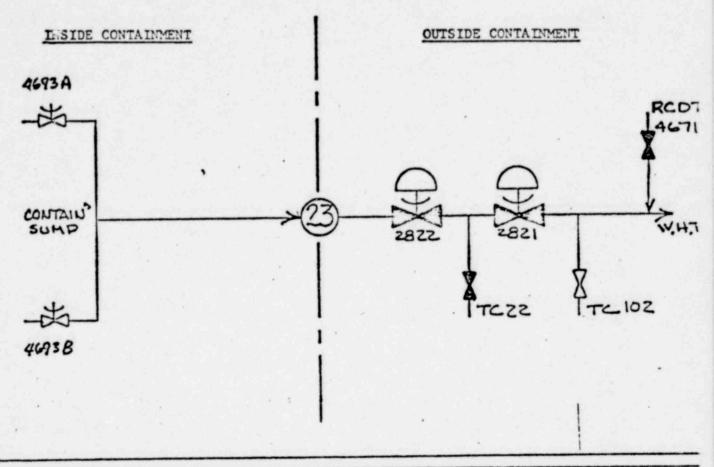


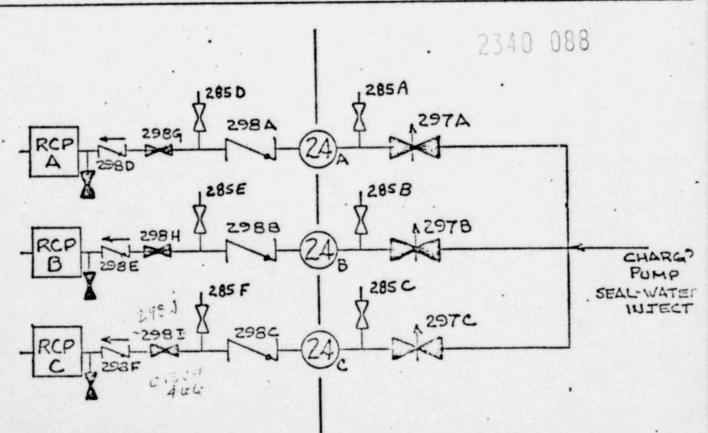


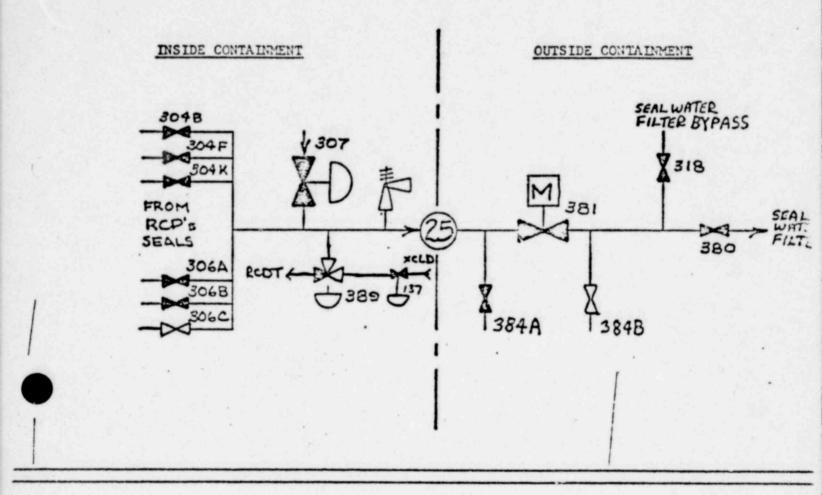


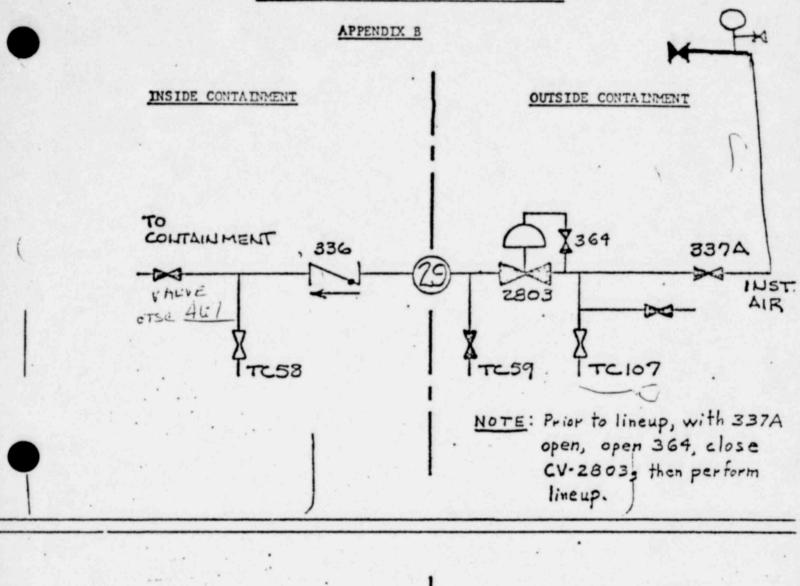


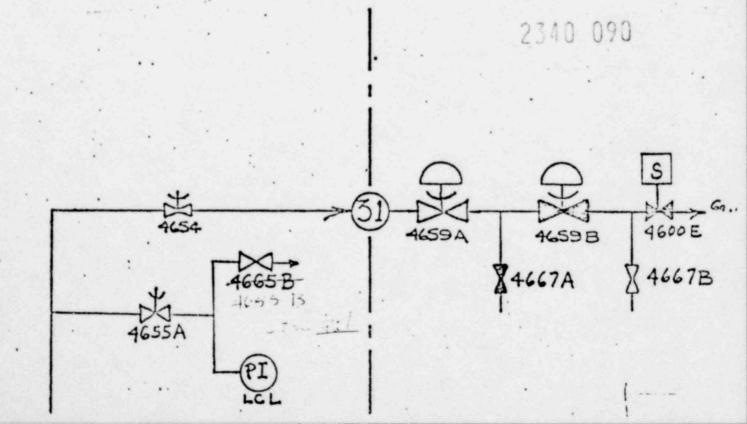
#### APPENDIX E

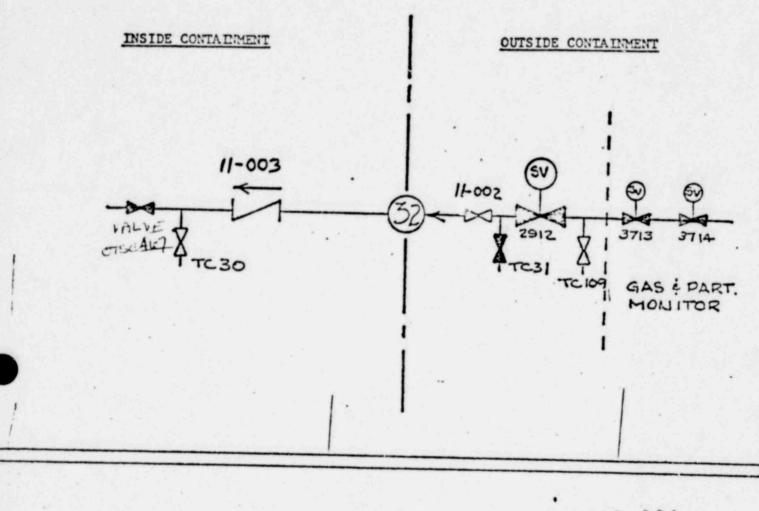


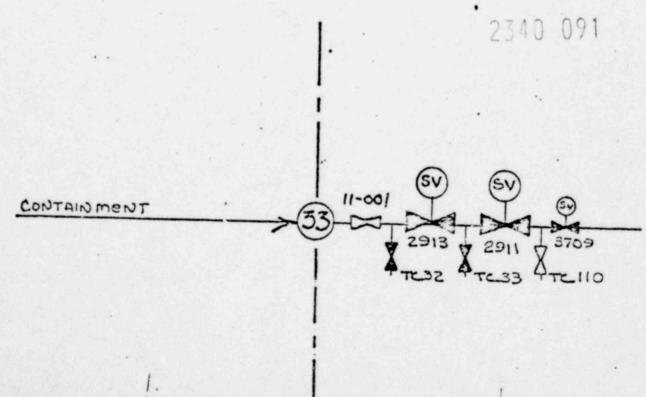


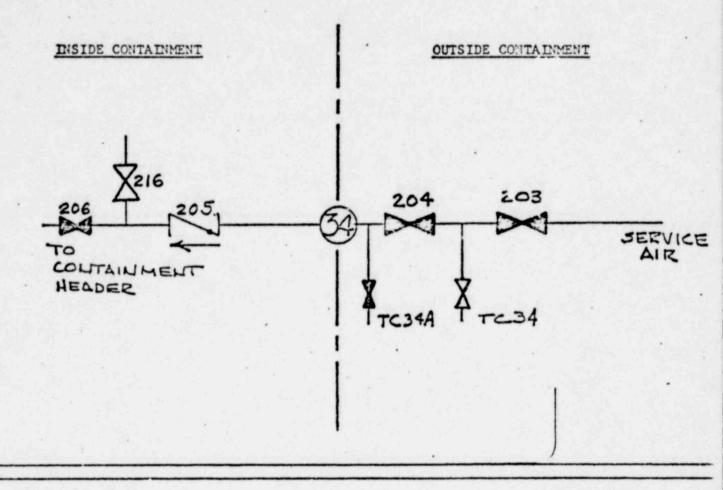


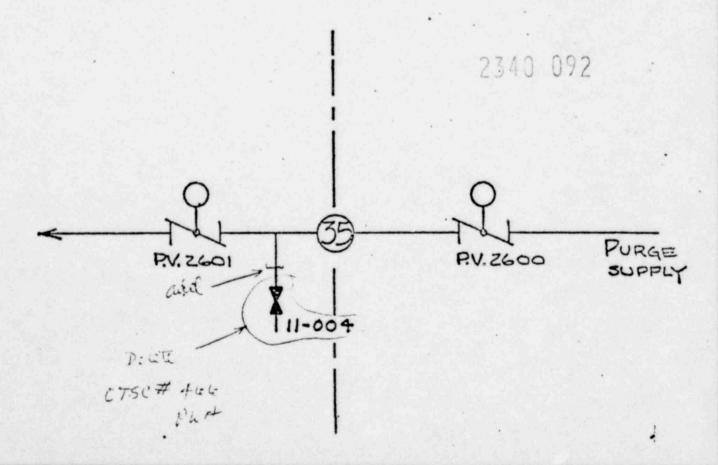


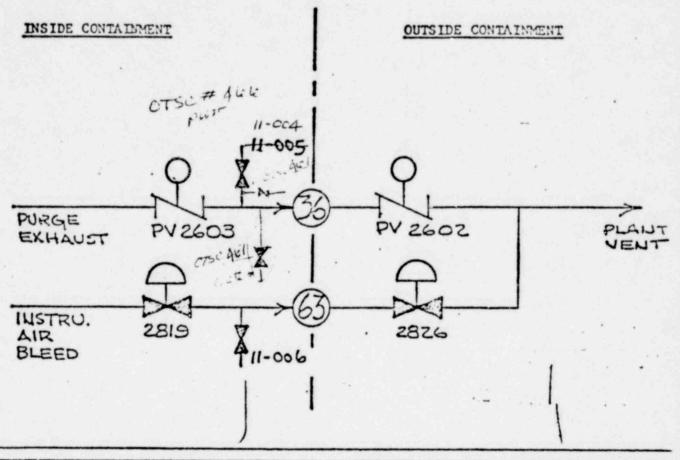


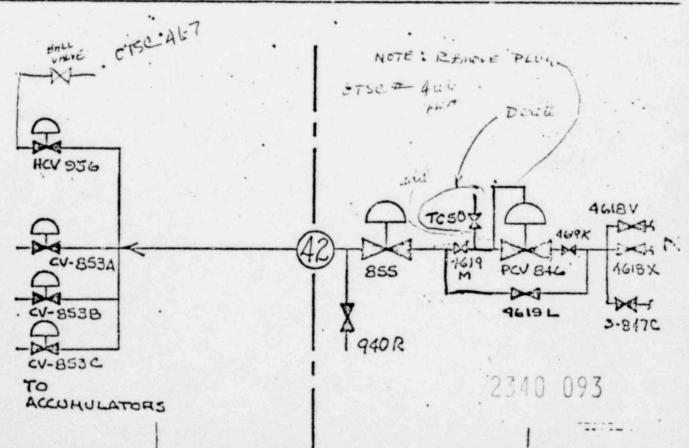


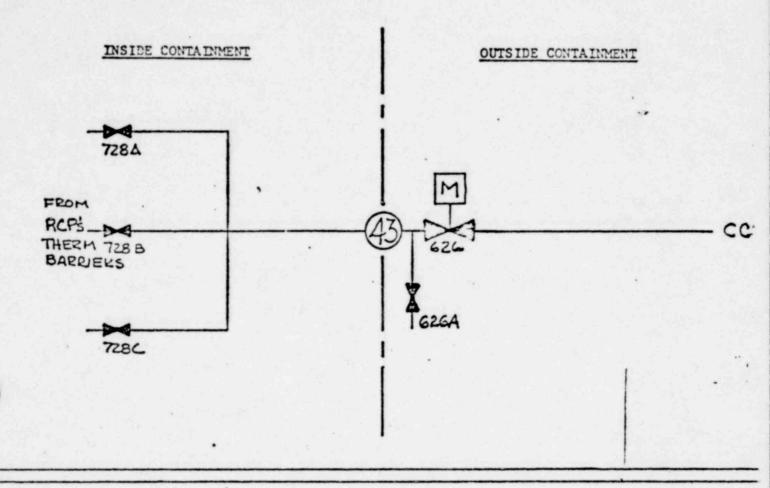


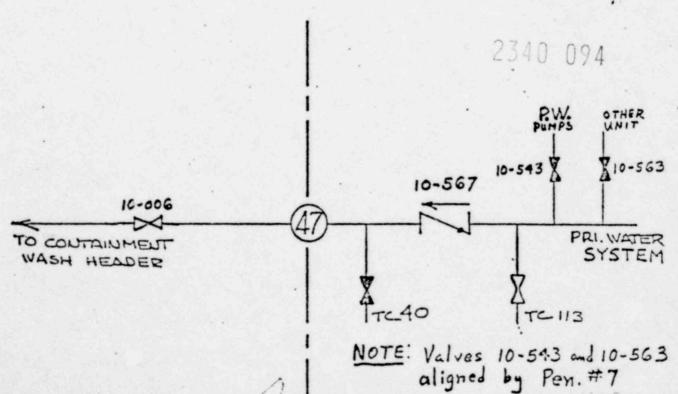


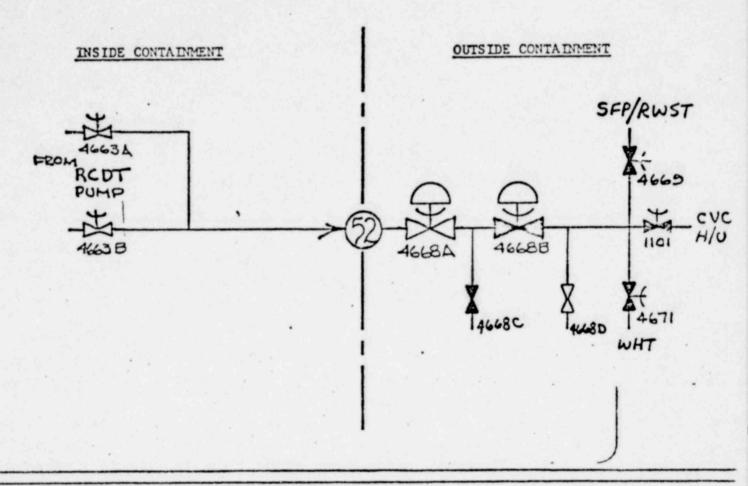


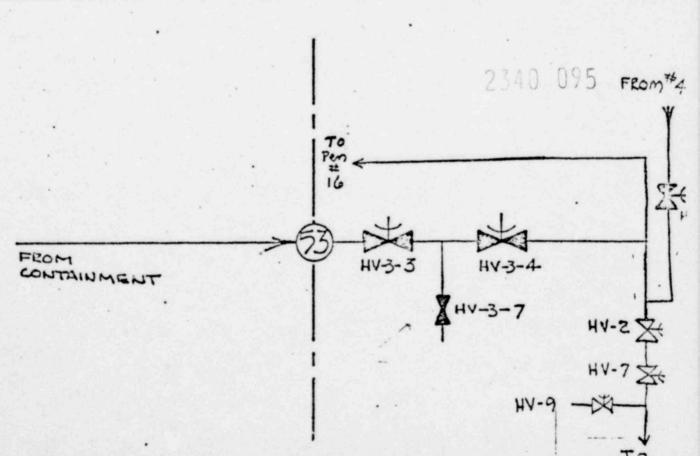


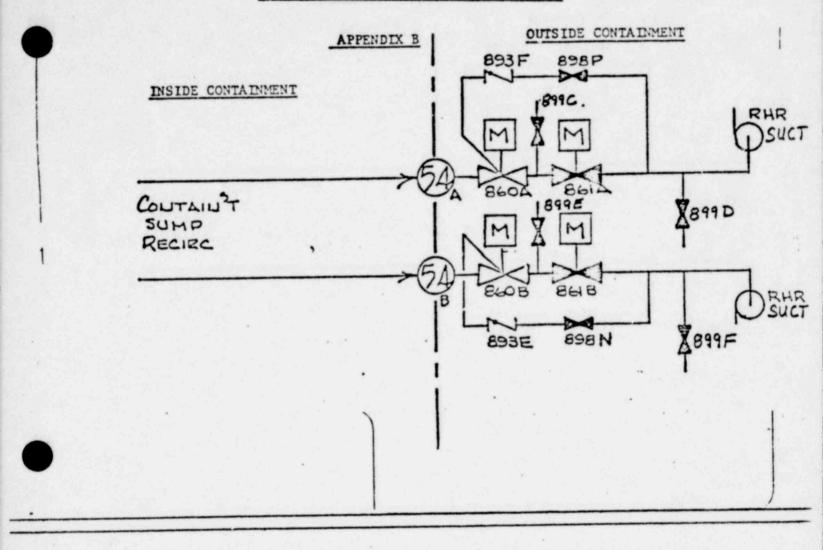


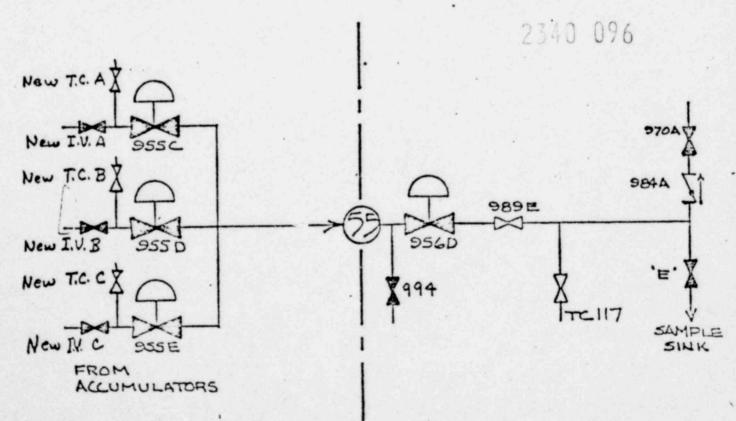


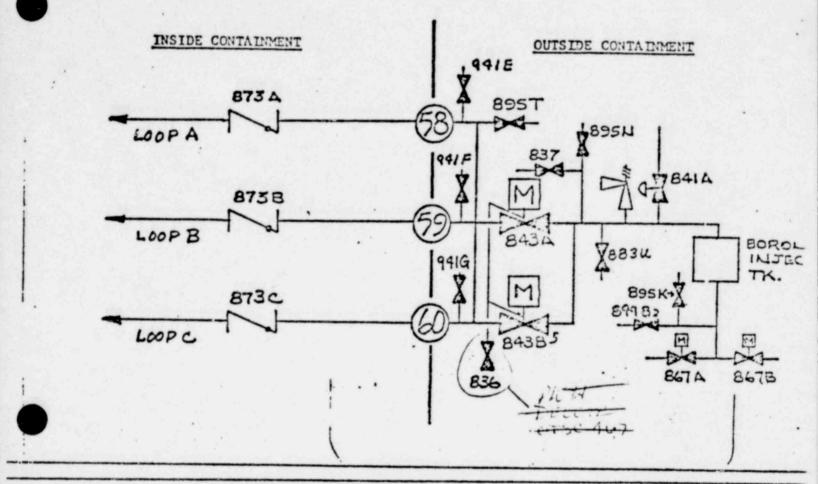


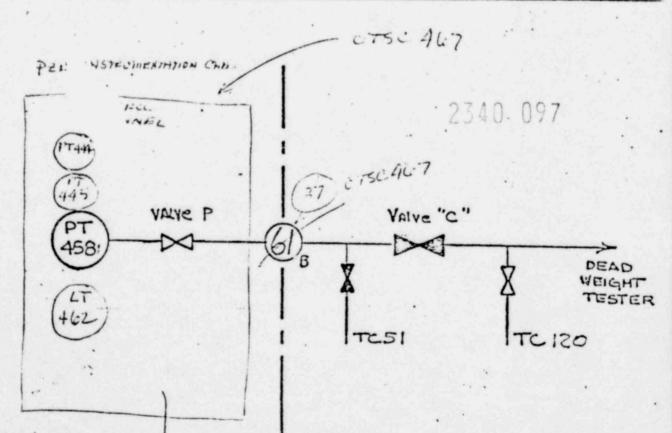


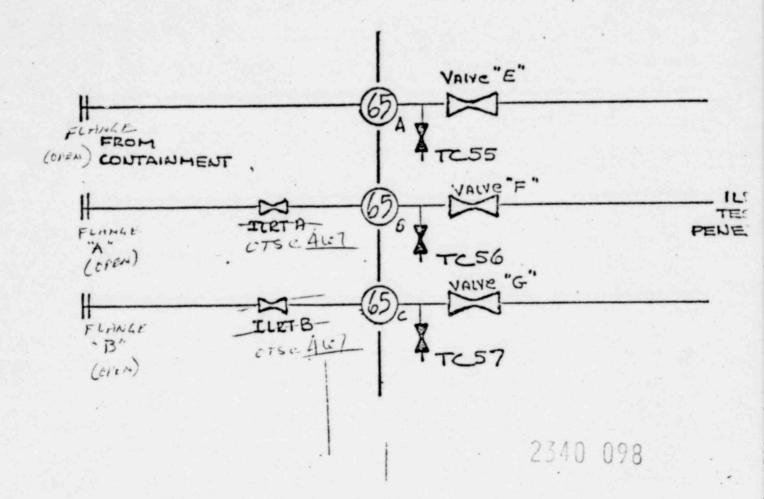


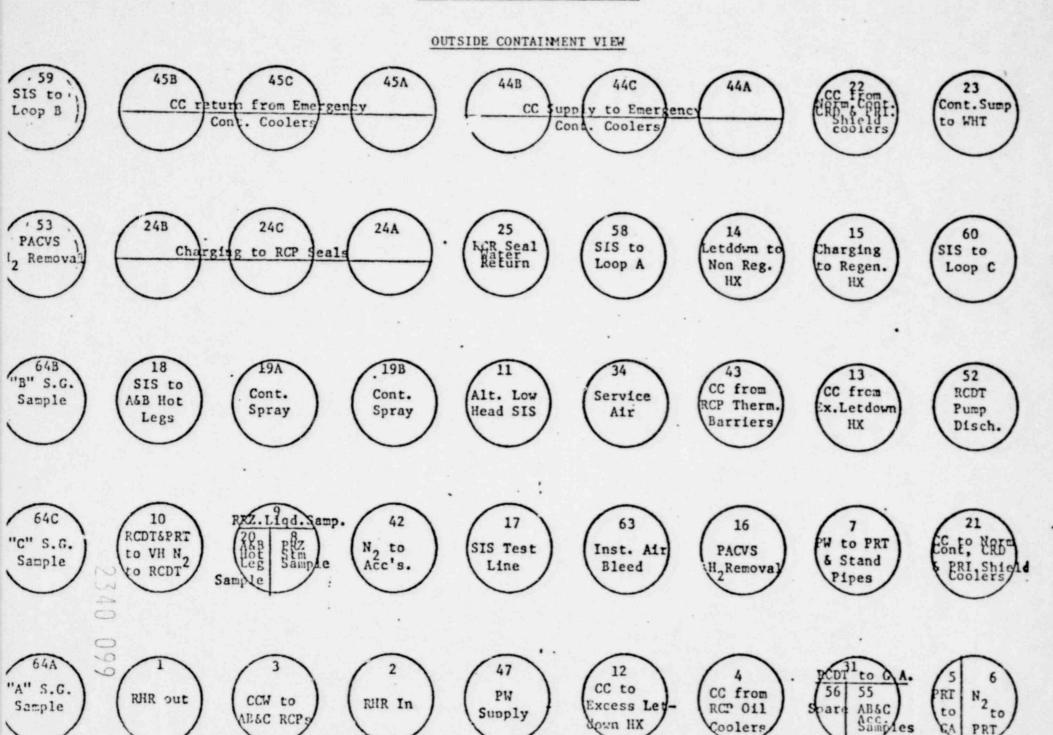


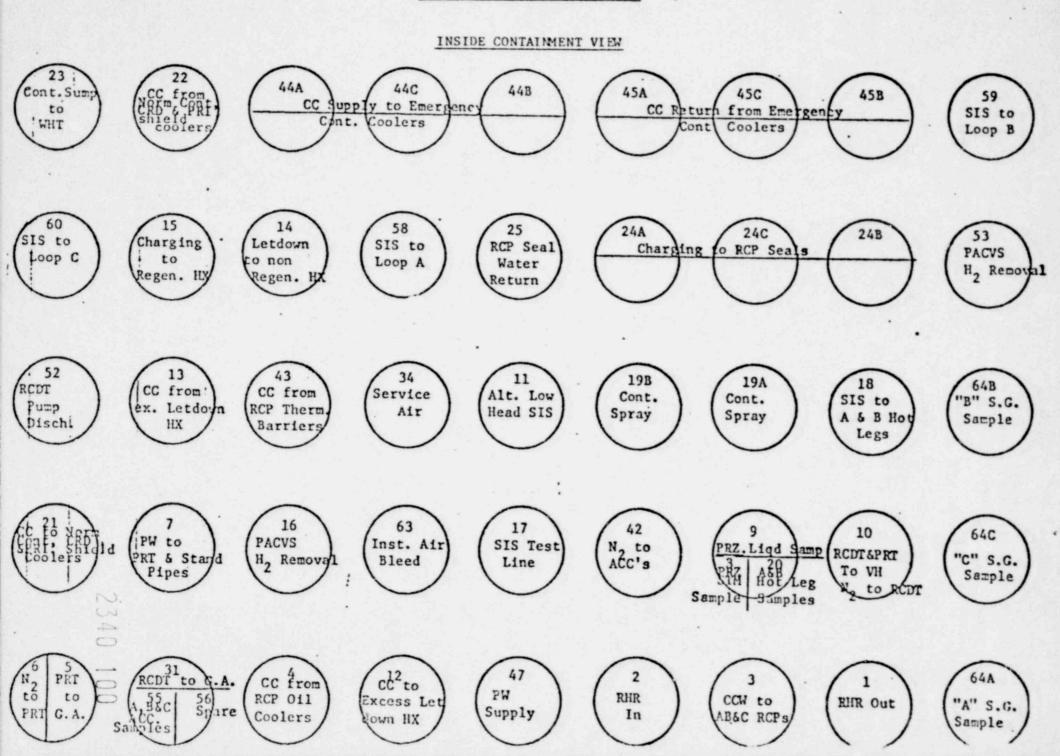












OPERATING FRO JRE, PAGE 47 INTEGRATED LAK RATE TEST

TOR CELL LOCATION	I. mod
2 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	RIO 21 SECTOR CELL LOCATION
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.0.2. 2.
2 De grande 12 05 09 08 09 05 05 05 05 05 05 05 05 05 05 05 05 05	// CEL.195.00'-
7. 22. 21	Riphon School
FL.6300' FL.6300' FL.6300' L. 12 CH. 56.00' L. 1	1000 2 12 21 21 22 22 22 22 22 22 22 22 22 2
(Roof)   Selver   Sel	- 6.63,00) 6 1 6 2 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
100TE:	£1.22,00,7
EL. 155.00' 014 :	11 12 14 KETO-7 STATE-FOR
- <u>@</u>	15 16 17 18
010 010	0.00
36' [M. "A" M.C.	,000
PLAUS	
A-RHO (CAL-1-DELACE)  A-RHO (CAL-1-DELACE)  C - DEW COLLS (4)	TUZZEY POINT PLANT

# APPENDIX C

DEFINITIONS AND ACCEPTANCE CRITERIA

#### APPENDIX C

## Definitions and Acceptance Criteria:

P. (50 psig)

The calculated peak containment internal pressure related to the design basis accident and specified in the Technical Specifications.

P. (> 25 psig)

The containment vessel reduced test pressure selected to measure the integrated leakage rate during periodic Type A tests.

Lam/Lrm (2/24 hrs.)

The total measured containment leakage rates by weight at Pa and P,, respectively, obtained from testing the containment with components and systems in the state as close as practical to that which would exist under design basis accident conditions (e.g., vented, drained, flooded or pressurized).

La (0.25 %/day)

The maximum allowable leakage rate by weight at P (50 psig) as specified for preoperational tests in the Technical Specificatin and as specified for periodic tests in the operating license.

L. (%/24 hrs.)

Maximum allowable test leakage rate by weight at P, (25 psig) derived from the preoperational test data as follows:

	Ltm			
$L_t \leq L_a$	Lam			
where,	La	- 0.2500	2340	103
	Ltm	= 0.0667		
	Lam	= 0.162		
therefore,	. Lt	≤ 0.2500	0.0667	
		≤ 0.2500	(0.4117)	
	Lt	≤ 0.1029		

Ltm - periodic test - For periodic Type A tests at Pt, Ltm shall be less than 0.75 Lt

 $L_{tm} \le 0.75 \quad (0.1029)$ 

Ltm < 0.0772 %/day by weight @ 25 psig

Lam - periodic test - For periodic Type A tests at Pa, Lam shall be less than 0.75 L

 $L_{am} < 0.75 (0.25)$ 

Lam < 0.1875%/day by weight @ 50 psig

The criteria listed below for either the short duration test or the twenty-four hour or longer duration test shall be met.

## SHORT DURATION TEST ACCEPTANCE CRITERIA:

The Trend Report (BN-TOP-1 Total Time Calculations) based on total-time calculations indicates that the magnitude of the calculated leakage rate is tending to stabilize at a value less than 75% of the maximum allowable leakage rate.

Note: The magnitude of the calculated leakage rate may be increasing slightly as it tends to stabilize. In this case, the average rate of increase of the calculated leakage rate shall be determined from the accumulated data over the last 5 hours or last 20 data points, whichever provides more points. Using this average rate, the calculated leakage rate is then linearly extrapolated to the 24th hour data point. This extrapolated value of the calculated leakage rate must be less than 75% of the maximum allowable leakage rate.

The calculated leakage rate based on total-time calculations is less than 75% of the maximum allowable leakage rate.

The end-of-test upper 95% confidence limit for the calculated leakage rate, based on total-time calculations is less than the maximum allowable leakage rate.

The mean of the measured leakage rates, based on total-time calculations over the last 5 hours of test or last 20 data points (whichever provides more data), is less than the maximum allowable leakage rate.

The calculated leakage rate at the 95% confidence level, based on mass-point calculations is less than 75% of the maximum allowable leakage rate.

Data has been recorded at approximately equal intervals and in no case at intervals greater than one hour.

At least 20 data points are provided for proper statistical analysis.

The minimum test for duration is 8 hours.

At least two-thirds of the drybulb temperature sensors and the dewpoint temperature sensors, and one absolute pressure gauge are fully operational. Additionally, the ISG (See ANSI N274) shall not exceed 0.25 La.

# TWENTY-FOUR-HOUR OR LONGER DURATION TEST ACCEPTANCE CRITERIA:

The calculated leakage rate and the end-of -test upper 95% confidence level, based on mass-point calculations (ANSI N274) is less than 75% of the maximum allowable leakage rate.

Data has been recorded at approximately equal intervals and in no case at intervals greater than one hour.

At least 20 data points are provided for proper statistical analysis.

the ISG (ANSI N274) does not exceed 0.25 La.

#### VERIFICATION TEST ACCEPTANCE CRITERIA

Imposed Leakage Rate Method

(Lo + Ltm - 0.25 lt) ≤ Lc ≤ (Lo + Ltm + 0.25 Lt)

where:

Lam = containment leakage rate calculated during presure ILRT.

Lt = maximum allowable leakage rate for reduced pressure ILRT.

Lc= containment leakage rate calculated during verification test.

Lo = leakage rate imposed on containment using flow measuring device.

Lo = (1 + 0.25) Lt

The verification test duration is at least four hours and at least 10 data points are used.

APPENDIX D

Data Sheets

# OPERATING PROCEDURE 13100.1, PAGE 52

INTEGRATED LEAK RATE TEST

0TSC 464

## APPENDIX D

AROMETRIC PRESSURE		DATE			
ROTAMETER FLOW		VERIFIED BY			
	ILRT DATA SHEET				
TIME/SAMPLE NO.	,	1 ,	,	1 ,	
KTD # 1					
RTD # 2	,				
RTD # 3					
RTD # 4		Into the same of			
RTD # 5					
RTD # 6					
RTD # 7			1		
RTD # 8					
RTD # 9					
RTD # 10					
RTD # 11					
RTD # 12					
RTD # 13			-		
RTD # 14			-		
RTD # 15			-		
RTD # 16 RTD # 17					
RTD # 18					
RTD # 19					
RTD # 20					
RTD # 21			<del> </del>		
RTD # 22					
KID V 22			-		
RHD # 1					
RHD # 2					
RHD # 3					
RHD # 4					
RHD # 5					
RHD # 6					
RHD # 7					
RHD # 8					
RHD # 9 RHD # 10					
			***************************************		
Pressure # 1					
Pressure # 2 (SPARE)				*	

RTD - Resistance Temperature Detector,

RHD - Relative Humidity Detector,

Pressure,

2340 107

Terminal Operator

### OPERATING PROCEDURE 13100.1, PAGE 53 INTEGRATED LEAK RATE TEST

## APPENDIX D

AROHETRIC PRESSURE 30,14			DATE 3-18		
OTAMETER FLOW			VERIFIED BY		
	ILRI	DATA SHEET		T . (	
TIME/SAMPLE NO.	1	()	20301	1 >	
RTD # 1			24.73	1	
RTD # 2	1		80.99	1	
RTD # 3			81.36	1	
RTD # 4	1		E=1.12.		
P.TD # 5		/	81.38	<del></del>	
RTD # 6	1 7	1	81.70	1	
RTD # 7	1 /	1	80.69	1	
RTD # 8			80.56		
RTD # 9			50.55	1.	
RTD # 10			00.00	1	
RTD # !1	1		75.79	1	
RTD # 12			80.32	<del>  / -</del>	
RTD # 13			79.62	1	
RTD # 14			100.52		
RTD # 15			20.04	<del> </del>	
RTD # 16		/	1 78.76	1	
RTD # 17	1	1	79.39	1	
RTD # 18	/	× 100	75 24		
RTD # 19	/	/	78.63		
RTD # 20		/	70.6/-	1	
RTD # 21 (SPARE)			1 845.03	1-7	
RTD # 22 (SPARE)			82.59	1	
				1 1	
D. Pt. 0 1	1	1	.911	1	
D. Pt. # 2			. 71-4		
D. Pt. # 3		7.00	1.795		
D. Pt. # 4		/ / /	1,830		
		/		1	
Pressure # 1			34410	T	
Pressure # 2 (SPARE)			1 54440		
D. Pt Dew Point		\			
				2711 1	
RHD - Relative Humidit	y Detector,	Latin AUCHOLINA		2340 1	
Pressure,					

## OPERATING PROCEDURE 13100.1, PAGE 53 INTEGRATED LEAK RATE TEST

AROMETRIC PRESSURE 30.145			DATE 3/18/	79
TAMETER FLOW			VERIFIED BY	Samte
	ILR	T DATA SHEET		
TME/SAMPLE NO.	121001 2	16	2730/ 3	)
T 0 1	86.96	1	87.99	-
TD # 2	63.09		84.45	/
TD # 3	81.55	1		
TD # 4	E-1 to 7	1	82.36	
TD # 5	8-1.71	1 7	151,87	
TD # 6	82.19	1	82.43	1
TD # 7	81.06		P1.29	1
TD # 8	65.73		81.35	
TD # 9	ENER		120.XU	
TD # 10	80.36		80.64	/
TD # 11	79.19	/	77.44	7
TD # 12	8°C 72		50,99	/
TD # 13	80.04		10.79	
TD # 14	78.70		10.45	
TD # 15	FC:51		80,50	
TD # 16	79.17		79.44	
TD # 17	79.76		180.09	\
TD # 18	79 63		77.91	
TD # 19	7920		79.43	
TD # 20	50.19	1	FE, 41	
TD # 21 (SPARE)	86.76	-	11.02	
TD # 22 (SPARE)	E 593	1-/	184.69	
D. A. 1	1 066	1		
• Pt. 0 1	.980	-	1.048	
• Pt • # 2	1500	-	. 566	
Pt. # 3	793	<del> </del>	. 795	\
. Pt. # 4	1 .826	1	1.806	
ressure # 1	35532-	1427 44	42744	
ressure # 2 (SPARE)	38600	\$2780	The second secon	
ressure : E (STARE)	7,000	1 + - 100	1 3220017	
· Pt Dew Point			1, 298947	ented T.
HD - Relative Humidit	v Detector		2-298513	+ 1

MBIENT TEMPERATURE	30.155		DATE 3/18/	79
DTAMETER FLOW			VERIFIED BY PR	Same
	1191	T DATA SHEET		
TIME/SAMPLE NO.	22001 4	11,	2230/ 5	. (
TD # 1	88.66	11	84-22	1
TD # 2	1554	1	86.25	<u> </u>
TD # 3	\$1.69		152.14	
TD # 4	12.31	1	22.49	7
TD # 5	F2,64		81.88	1
TD # 6	F2.53		82.42	1
TD # 7	81,46	/	81-57	
TD # 8	81.55	1 /	11.75	
TD # 9	F1.21		V1 - 12-4	1
TD # 10	80.76		X0+12	\
TD # 11	79.63		177.75	
TD # 12	181.07		81 31	
TD # 13	10,41		79,04	
TD # 14	81.19		81.40	
TD # 15	10.36621	43	80.13	1
TD # 16	79.62	111111111111111111111111111111111111111	79.71-	/
TD # 17	180.17		80.32	/
TD # 18	30,12	/ / / / / / / / / / / / / / / / / / / /	84 27	
TD # 19	79.60	/	79.71	
TD # 20	PO 55		82.61	
TD # 21 (SPARE)	184.78		43, 12	
TD # 22 (SPARE)	185.42	1	86.15	
. Pt. # 1	1.10%	1	1.156	
). Pt. # 2	1,945	<del></del>	1. 1.16	
Pt. # 3	1.404	1	8170	
. Pt. # 4	1815	7 10 10	-8140	
			70//0	/
ressure # 1	146845	1	51045	r (-
ressure # 2 (SPARE)	147025		51274	1 1 1 1 1 1 1 1
Pt Dew Point _				1
HD - Relative Humid	ity Detector,			/
			0.7	40 110

				_
	ILRT	DATA SHEET		
FIME/SAMPLE NO.	2300/6	1	23301 7	, )
RTD # 1	89.401		89.97	
RTD # 2	56.71	)	76.47	
RTD # 3	53.27	7	F1.36	
RTD # 4	1 31.66		122.76	
TD # 5	82.13	/	82,08	1
RTD # 6	1 52.43		12.55	
RTD # 7	81./4/		81.50	
RTD # 8	81.67		82,08	\
TD # 9	6144		\$1.51	
TD # 10	8100		91.16	
RTD # 12	79.45	<del> </del>	77.98	
TD # 13	3057		F1. 35	
TD # 14	8112		F1.13	
TD # 15	50.83	<del></del>	80,94	
TD # 16	70.55		79.99	<del></del>
TD # 17	78.00		FO.UR	1
TD # 18	50 35		10.49	
TD # 19	79:0		79,90	1
TD # 20	15:-7		12.73	
TD # 21 (SPARE)	29.15		86.99	
TD # 22 (SPARE)	1 54-7	<del></del>	186,99	
. Pt. 0 1	1 / 2		1	/
	1.207		11253	
Pt. # 2 Pt. # 3	1.143		1.173	
). Pt. # 4	1823		1839	-
				7
ressure # 1	55145	<del></del>	59300	
ressure # 2 (SPARE)	55430	59671	59620	

	IL	RT DATA SHEET		
TIME/SAMPLE NO.	000018	003019	01:5 9	0130/ //
RTD # 1	40,23	90.43	90.63	96.54
RTD 0 2	87.28	87.55	37 23	88 Cho
RTD # 3	1 43.41	77.43	22.53	\$2.55
RTD # 4	82.84	×2 ×3	32,93	82.97
RTD # 5	82.16	82,20	82.19	\$2.5027
RTD # 6	8.2.63	32.60	82.65	82,72
RTD # 7	82.01	32.01	82.37	82:37
RTD # 8	52.26	12.20	82.20	82.31
RTD # 9	81.59	31,60	51.73	31.75
RTD # 10	81.28	31.25	81.35	81.41
RTD # 11	80 68	77.35 3014	50.27	80.33
RTD # 12	81.40	250,12	8141	31.45
RTD # 13	86.15	2-21.02	80 82	20.36
RTD # 14	81.15	12:1.07 AT	81.11	11.12
RTD # 15	31.09	1.30.15 .	81.14	31.21
RTD # 16	80.08	2-304911	50.24	90 3 2
RTD # 17	80.56	2-80.61	80.57	30.58
RTD # 18	80.57	1 279.9.9 8	YE 13	30.71
RTD # 19	79.97	1-80.76	30 04	vn. 15
RTD # 20	Sc. 75	2-90.42	87,43	m 26.
RTD # 21 (SPARE)	1 40.33	18-87.56	90.67	190.54
RTD # 22 (SPARE)	1 87,32	- L	37.77	37.99
D. Pt. 0 1	1 / 250	1 / 2 7		1 ( )
	1.309	1.317	1.305	1.405
D. Pt. # 2 D. Pt. # 3	1:10.7	1.16.2	1314	1.235
D. Pt. # 4		. 478	. 47.7	, 9/7
D1 1C1 × 4	1 .856	1 .862	1383	1.900
Pressure # 1	153470	67515	72150	75675
Pressure # 2 (SPARE)	6 3870	67475	72660	76233

AROMETRIC PRESSURE	30.11		VERIFIED BY	19/79
OTABLIER FLOW			VERIFIED BY	Demo
	ILR	T DATA SHEET	, , , , , , , , , , , , , , , , , , , ,	
TIME/SAMPLE NO.	0200 / 12	02301 13	1030ch 14	0330 5
RTD # 1	41.65	91.23		
RTD # 2	89.31	59.52		1
RTD # 3	83.65	1 33.72		
RTD # 4	33.63	\$3.04	1	
RTD # 5	32.33	82.41		1 7
RTD # 6	82.79	\$2.91		
RTD 0 7	8.2.51	82.56	1	
TD # 8	82.42	32.49	1	
RTD # 9	81.75	57.50	1	1
RTD # 10	81.44	3151		
TD # 11	80,42	50,49		
RTD # 12	81.53	\$1.56		
TD # 13	80.91	80.94		
TD # 14	81.15	81.16-		1
TD # 15	81.26	81.33		
TD # 16	80.40	1 50.50		
TD # 17	80.61	80.61		1
TD # 18	1 80 87	30.95		
TD # 19	80.22	So. 28		
TD 0 20	QA 67	\$1.00		
KTD # 21 (SPARE)	91.07	91.24		
TD # 22 (SPARE)	88.15	55.47		1
				1
. Pt. # 1	1.4.24	1 1.455		1
0. Pt. # 2 0. Pt. # 3	1.330		1	1
The same of the sa	0.936	1.464		
. Pt. # 4	0.918	1 .956		
				7
Pressure # 1	79800	839+4		T- Comment
ressure # 2 (SPARE)	80 420	1 2-+	1	
D. Pt Dew Point		846254	+	\$
AB - Relative Humidit	y Detector.			
ressure,				340 113

BAROMETRIC PRESSURE	30.095		DATE 3	119/79
OTAMETER FLOW			VERIFIED BY	Bamo
	STAB	1112ATION		
		RT DATA SHEET		
TIME/SAMPLE NO.	03001 1	03151 2	0330/ 3	034514
RTD # 1	90,64	53.45	8706	56.15
RTD # 2	88,24	56.49	45.03	8463
RTD # 3	82.22	\$1.35	51.65	150.91
RTD # 4	32.57	51.69	51.79	21.09
RTD # 5	82.23	31.54	21.24	\$1.04
RTD # 6	32.38	81.53	51.11	80.75
RTD # 7	82.25	81.24	30.91	180.5%
RTD # 8	82.05	91.23	86.93	×6.76
RTD # 9	51.23	80 60	50.44	Y2.30
RTD # 10	81.14	80.46	56.22	301.11
RTD # 11	80.55	80.11	79.99	7112
RTD # 12	1 80.81	80.06	79.52	77.71
RTD # 13	80.34	79.81	79 64	79.53
RTD # 14	20.21	79.80	79.67	79.57
RTD # 15	20.72	80.13	50,00	74.93
RTD # 16	Vn.30	79.92	79.75	79.68
RTD # 17	80.05	79.59	79.40	79.32
RTD # 18	30,03	V1.25	86,12	82.00
RTD # 19	79.98	79.61	79.47	79 37
RTD # 20	Yn. 34	74.25	20.47	79.30
RTD # 21 (SPARZ)	1 411, 22	83.21	\$6.80	85.97
RTD # 22 (SPARE)	87.32	86.15	84.85	83.54
D. Pt. 0 1	1.501	1 1.461	1,450	1.451
D. Pt. # 2	1.445	11333	1, 332	1.200
D. Pt. # 3	. 959	- 943	. 944	1 953
D. Pt. # 4	1 1957	1 ,976	1 .985	11005
Pressure # 1	87063	56564	86659	86557
Pressure # 2 (SPARE)	8777.3	37569	1 47370 m	
D. Pt Dew Point				
RHD - Relative Humidit	y Detector,			
Pressure,				2340 11

30.095		DATE 3/	19/79
		VERIFIED BY	Bom
ILR	T DATA SHEET		
64001 5	64151 6	04301 7	C1451 S
	The second secon	A STATE OF THE PARTY OF THE PAR	54,05
1 47.29			52.66
81.74			50.45
86,45		32.72	50, 4.3
x3. x4	80.75	30.68	1 80,60
80.68	80.57	50.51	\$2.4.3
X0.45	80.34	80,24	80.15
×7.62	いたオラス・什	80.43	1 30,36
87.23		AC. 17	1 80.12
80.05	79.97	79,94	79.87
THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE OWNER	79.71	79 66	79.61
		71.50	79.45
		79.33	79.27
			79.42
			71.76
			79.47
the second secon		THE RESERVE THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TWIND TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN	74,00
			79 77
			79.22
The second secon		the second secon	79.19
			81,92
	1	22.72	1 01,14
1 1 1 1 1 1	1.453	1.441	1.971
1.431	1.356	1.378	1.217
1991	1.711	1.024	1,031
1 1.021	1 1.04.2	1.060	11.075
86481	177371 86421	853 73	863 33
87/8/	37122	37073	87031
	## E400 1 5 \$5.37 \$5.37 \$2.27 \$2.27 \$2.34 \$2.68 \$3.12 \$2.68 \$3.12	ILRT DATA SHEET	ILRT DATA SHEET     6400   5

OTAMETER FLOW			VERIFIED BY	
	ILR	T DATA SHEET	· · · · · · · · · · · · · · · · · · ·	
TIME/SAMPLE NO.	0500 19	05151 10	05301 11	C545 112
RTD # 1	83,77	83,52	53,27	83.03
RTD / 2	41.78	81.57	81,38	3/ 20
RTD # 3	23.32	100.34	80.24	30.24
RTD # 4	97.55	30.48	30.43	30 30
RTD # 5	30.53	50.46	80.41	80.35
RTD # 6	50.35	50.29	80.22	80.15
RTD # 7	50.09	80.07	80.00	79.97
RTD # 8	56.29	50,24	50.18	1 20.13
RTD # 9	50.04	50.05	80.01	180,00
RTD # 10	79.85	79.83	79.79	77 7/-
RTD @ 11	29.57	79.55	79.51	79.43
RTD # 12	29.43	79.40	77.36	77 31
RTJ # 13	79.24	79.19	79.16	79.13
RTD # 14	79.39	79.38	79.35	17.33
RTD # 15	79.73	79.70	79.68	79.66
RTD # 16	79.45	79.42	79.41	79.37
RTD # 17	19,05	79.01	78.99	78.96
RTD # 18	79.76	79.73	79.71	79.67
RTD # 19	79.18	79 17	79 14	77.11
RTD # 20	79.15	79.12	79.10	79.45
RTD # 21 (SPARE)	53.75	80.50	83.27	13303
RTD # 22 (SFARE)	1 81.66	81.45	81.26	81.09
D. Pt. # 1	1,940	1.432	1.436	1.429
0. Pt. # 2	1.314	1. 358	1.326	1.316
). Pt. # 3	1.551	1.080	1 597	11.112
D. Pt. # 4	1 1.699	1.118	1.135	11,152
Pressure # 1	86.2.44	01.312	1 9/3/1	1 37 373
Pressure # 2 (SPARE)	Vr 570,0997	86965	1 86241	36212
D. Pt Dew Point		1 30102	86733	86913

82.89 81.07	0615 1 14 32.72	C6301 15	T.,-,
82.59	-		
82.59	32.72		10195/ 16
		82.56	82.42
	80.95	80.85	80.76
80.20	50.17	80.13	80.11
80.33	80.28	80.24	80.20
80.30	80.25	80,20	50.17
80.11	80.07	80.02	7994
79.95	79.90	79.89	79.87
80.09	80.05	80.02	79.95
	30.01	00.01	3002
NAME AND ADDRESS OF THE OWNER, WHEN PERSON ASSESSMENT	79.72	79.70	79.70
	79.42		71.40
Control of the Contro			7726
	79.09		79.04
		79.30	79.29
		79.60	79.54
			79.34
CONTRACTOR OF THE PARTY OF THE			1 78.59
			79.65
79.01			79.06
			79.50
			52.43
30,70	30,33	50.77	80.70
1.429	1 1.425	1.422	1.422
	THE RESERVE THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER,	1.206	1 218
1.131			1:178
1.172	1.186	1 1,198	1,204
87.195	1 8/125	1 8/153	Toctal
	9/27/		868 37
	79.95 80.09 80.04 79.79 79.96 79.30 79.10 79.32 79.63 79.63 79.63 79.65 79.09 79.05 82.90 80.96	79.95 79.90 80.09 80.05 80.04 \$0.01 79.79 79.72 79.96 79.42 79.30 79.29 79.10 79.09 79.32 79.30 79.63 79.62 79.37 79.36 78.93 78.92 79.65 79.64 82.90 \$2.73 80.96 \$2.73 80.96 \$2.73 \$0.85	79.95     79.90     79.89       80.04     80.01     80.00       79.74     79.72     79.70       79.96     79.42     79.42       79.30     79.09     79.09       79.32     79.30     79.30       79.63     79.62     79.30       79.37     79.36     79.30       79.37     79.36     79.30       79.43     78.92     79.00       79.44     79.62     79.00       79.65     79.64     79.62       80.90     82.73     82.53       80.96     80.85     80.77       1.429     1.425     1.422       1.376     1.214     1.206       1.131     1.197     1.164       1.172     1.186     1.198       86195     86175     86157

TIME /CAMPIE NO	ILR	T DATA SHEET		
TIME /CAMPIE NO				
TIME/SAMPLE NO.	0700 / 17	0715 1 18	07301 19	0745126
RTD # 1	82.28	82.14	82.03	81.92
RTD # 2	80.66	50157	50.49	30.43
RTD # 3	50.07	80.04	80.02	30,00
RTD # 4	52.17	30.12	80.10	30.00
RTD # 5	80.12	80.09	80.05	80.03
RTD # 6	79.94	79.91	79.87	79.35
RTD # 7	75.54	79.83	79.82	79.80
RTD # 8	79.94	19.90	79.88	79.86
RTD # 9	50.02	79.90	80.01	79.97
RTD # 10	79.70	79.66	79.62	79.64
RTD # 11	79.37	74.36	79.34	75.33
RTD # 12	79.22	79.21	79.21	17.20
RTD # 13	79.03	72.02	79.00	75.57
RTD # 14	79.26	72.26	79.26	79 25
RTD # 15	79.57	79.57	19.55	79.54
RTD # 16	77.33	72.31	79.29	71.20
RTD # 17	79.87	78.95	75.84	75.59
RTD # 18	79.57	74.56	79.53	79.52
RTD # 19	75.04	79.02	79.02	79.01
TD # 20	79.00	78.99	78.97	78.97
RTD # 21 (SPARE)	52.29	82,16	82.05	81.95
TD # 22 (SPARE)	1 80.60	80.53	80.45	5034
D. Lt. # 1	1 1 1 1 2 2	1 1 2 2		
	1.420	1.418	1.415	1.414
). Pt. # 2 ). Pt. # 3	1.208	1,207	1.217	1.220
	11195	1.301	1.210	1.218
). Pt. # 4	1 1.221	1 1.228	1.236	11.242
ressure # 1	86125	1 86110.	86107	186083
A STATE OF THE LAND OF THE PARTY OF THE PART			1 10101	0000

ROTAMETER FLOW			VERIFIED BY	
	I IL	RT DATA SHEET		
TIME/SAMPLE NO.	0800 1 21	0815 1 22	08301 23	C8451 20
RTD # 1	81.81	81.71	81.101	81.53
RTD # 2	80:36	80.29	80.25	80 20
RTD # 3	79.98	79.97	79 94	79.93
RTD # 4	30.05	1. 80.01	79 99	79 91.
RTD # 5	80.00	79.45	79.94	79.91
RTD # 6	79.82	79.78	79.75	7972
RTD # 7	79.79	71.77	79 75	79.74
RTD 0 8	79.83	79.80	79.78	7976
RTD # 9	79.9.3	79.93	79.94	7452
RTD # 10	79.62	79.61	79.60	7960
RTD # 11 RTD # 12	79.31	79.29	19.24	79.26
RTD # 12	75.13	79.16	79.15	The second name of the second na
RTD # 14	73.99	78.97	78.97	78.95
RTD # 15	79.23	79.22	7921	19.41
RTD # 16	79.28	79.51	7951	79 50
RTD # 17	The second secon	79,27	79.24	79 25
RTD # 18	78.34	13.8.3	7002	75.51
RTD # 19	78.99	78.47	78.96	78.96
RTD # 20	78.95	78.95	78 94	70 04
RTD = 21 (SPARE)	31.54	31.74	81 65	E1.56
RTD # 22 (SPARE)	80.32	80.26	80.21	FC.116
D. Pt. 0 1	1,413	1 1 4.7	1 1 40 7	1
D. Pt. # 2		1.413	1 228	1.409
D. Pt. # 3	1.223	1.220	1.224	1.230
D. Pt. # 4	1.244	1.248	1-251	1.253
	- Liati	11.27/2	1	1.633
Pressure # 1	86073	86063	86052	86042
Pressure # 2 (SPARE)	136768	1 86757	1 56746	186736
RIID - Relative Humid			23/	10 119

'0°		HOUR NO.	
0.14		DATE 19 MAG	79
		VERIFIED BY	
ILR?	DATA SHEET		
0900/ 25	0915/26	09301 27	c9451 28
81.46	81.37	8130	21.22
90.16	1 80.13	80.08	80.00
79 91	79.89	79 88	19.87
79 94-	79 92	79 97	79 55
79 56	79.86	79.83	79.84
7970	79.68	79.66	79 103
	79.72	79.71	79 70
79.75	79.72	79.71	79.70
7992	7491		79.38
79.58	79.58		79 56
79.25	79.24		79.23
	77.13		79.12
The contract of the contract o	1896		75 95
19.21	79.22		79.21
	79 49		77.45
	79 24	79 23	7923
76.81	78.80	18.81	78.79
	7945	29.44	79.45
78.95			28 94
		The second secon	73.93
			5-1-27
80.12	80.09	1 20 U.S	80.02
1.407	1.405	1.4/:3	1,403
			1.242
THE RESERVE THE PERSON NAMED IN COLUMN 2 I			1.246
		The state of the same of the s	1.262
		1.23	1 1 2 5 6
66033	86025	86C17	80011
86726	86718	1 26710	2013
	1187 09001 25 51.46 80 16 79 91 79 94 79 96 79 70 79 74 79 75 79 92 79 75 79 14 75 96 79 25 79 14 75 96 79 25 78 81 79 45 78 95 78 93 81 48 80 12	ILRT DATA SHEET  0900/ 25	ILRT DATA SHEET   0900/ 25

OTAMETER FLOW			VERIFIED BY	
	ILR	T DATA SHEET		
TIME/SAMPLE NO.	1000 / 29	1015/ 30	1030/ 31	1c45/ 3
RTD # 1	81.16	3107	81.03	80.96
RTD # 2	80,03	79.99	79.97	79.94
RTD # 3	79 83	70 03	175.57	30.07
TD # 4	79.97	79 85	75.85	74 50
TD # 5	79.87 79.80	1 5 3 . 2 2	79 76	7-172
TD # 6	79 61	79.59	79.56	79 50
TD 0 7	79.70	79.70	79 68	79.60
TD # 8	79.68	1967	7965	746
TD # 9	79.91	79.87	79 82.	795
TD / 10	79.55	79 87 79 54	79.53	79 5
TD # 11	79.23	79 22	19.20	79.2
TD # 12	79.12	79.12	79.11	79.1
TD # 13	78.95	78 93	78.93	78.9
TD # 14	79,21	79 20	1520	29.1
TD # 15	79,48	79 47	19 47	79 1
TD # 16	79.23	79 23	79 23	747
TD # 17	78.81	78.81	18 01	16.1
TD # 18	79.43	79.42	7736	794
TD # 19	78.94	78 93	78.93	78.9
TD # 20	78.93	1 24.92	1842	75.4
TD # 21 (SPARE)	1 8120	51.14-	1 11.00	51.6
TD # 22 (SPARE)	79.99	79 94	7993	79.9
• Pt • 0 1	1.398	1 1400	1393	1.397
	1.248	1.247	1-249	
• Pt. # 2 • Pt. # 3	1 24 7	1246	1:252	1.250
• Pt • # 4	1.259	1.263	1.265	1.268
			1. 7:363	11.200
ressure # 1	86002	65995	65988	85980
ressure # 2 (SPARE)	1 86694	- 56668	5.4650	E 10 10 74

77.00	n night during		
ILK	T DATA SHEET		
1100/ 33	1115/34	1130/35	1145134
80.90	80.84	20,79	EC. 75
79 91	79. P.F.	7.89,86- Pat	74 55
79.79	79.78	784,77 ,00	79 77
79.83	79.82	724.81 10	79 82
19.72	79.70	79.69	79 69
79.52-	79 50	79.47	79 47
79.66	7965	79.64	7764
79.63	79 61		7960
79.83	79 80		74.46
79.51	79 49	THE RESIDENCE OF THE PARTY OF T	77.44
79.18	79.18		79 17
79.09	79.10	THE RESERVE OF THE PARTY OF THE	7910
78,93	78 94		79. 91.
A REAL PROPERTY OF THE PERSON NAMED IN COLUMN 2 ASSESSMENT ASSESSMENT OF THE PERSON NAMED IN COLUMN 2 ASSESSMEN	79.10		7971
		the same of the sa	79.40
79.20			70 11
18.80		-	7882
19.40			79.93
	THE RESERVE THE PARTY OF THE PA		77.91
75 92.	78.97		78 (1)
80.96	80.90		हरें हैं।
79.86	79.84	79.82	79 81
	1.38.7		1,365
1.6.2	1.240	1.262	1.2.43
		1.27!	1.270
1.272	1.2.74	1.277	1.279
85074	1 850/-0	85063	83958
1117	C / (6 /	86655	86650
	11001 33 80.90 79.91 29.79 79.83	1100   33   1115   34 80.90   80.64 79.91   79.86 79.72   79.76 79.83   79.82 79.64   79.65 79.63   79.65 79.63   79.61 79.83   79.80 79.18   79.18 79.18   79.18 79.18   79.16 79.93   78.94 79.46   79.46 79.46   79.41 79.46   79.41 78.92   78.91 80.96   79.84 1.390   1.36.7 1.264   1.260 1.272   1.274	100   33

BAROMETRIC PRESSURE	30,14		DATE 19 HAR	79
OTAMETER FLOW			VERIFIED BY	
	ILR	DATA SHEET		
TIME/SAMPLE NO.	1200/37	1215/ 38	1230/ 39	1245/40
RTD # I	80.70	80.65	80.57	¥0.55
RTD # 2	79 82	79.60	79.79	-976
RTD # 3	79.76	79.75	79.74	79.70
RTD # 4	79 81	79 81	79.75	70 -
RTD # 5	79 67	79 66	79,65	790
RTD # 6	79 45	79.43	79.41	74.41
RTD # 7	79.64	79.64	79.63	-ici 10
RTD # 8	7460	79.58	79.57	74=1
RTD # 9	79.82	79.8.4	79.82	70.00
RTD # 10	79 48	79.49	79.48	79.4
RTD # 11	79 17	79.17	79.15	79.1
RTD # 12	79 113	79.10	79.09	-9 cx
RTD # 13	78.96	78 95	79.19	-v G.
RTD # 14	79.19	79.19	79.18	79.15
RTD # 15	7941	79.46	74.45	74 4
RTD # 16	79 2c	79.20	79.70	7176
RTD # 17	78.81	78.61	70 01	70. 3
RTD # 18	79.43	7943	79.44	74.4
RTD # 19	78.92	78.91	78.91	70 G
RTD # 20	75 92	76.00	79 77	78 9 700
RTD # 21 (SPARE)	FC.71	80.71	80.67	ن ن نع
RTD # 22 (SPARE)	79.79	79.75	79.74	79.7
D. Pt. # 1	1.383	1.378	1.380	1.3.75
D. Pt. # 2	1.268	1.270	1.274	1. 772
D. Pt. # 3	1.267	1.277	1.274	1. 201
D. Pt. # 4	1 1 284	1.287	1.288	1, 290
Pressure # 1	1 35053	050.46	1-050-54	
Pressure # 2 (SPARE)	25953	85948	95944	F59 =9
	1 8 4 6 4 5	86640	86635	BU10 31
D. Pt Dew Point RND - Relative Humidit			2.7	10 123
Pressure,				10 173

ILR	DATA SHEET	,	
130141	13151 42	1330 43	1345144
80,50	80.47	80,42	80.38
79.74	74.72	79.70	79.10
74.72	79 71		74.70
1 79 7%	79.77		7-1.7
79.62			79.58
79.38	79,37		79.24
79.62	7961		791
74,55	79.54	74.53	74.5
79.78	79.80	747.747	77 7
T9.46	79.46	79.45	-19.4
79.15	74.13		74.10
79.09	79,02		79.67
TE 95	70.93		707.
79.17	79.10		7910
	79.45		74.4
79.19	74.20		1791.12
70,00	7001		7001
79,45	79.46		74.4
78.90			73.5
75,91			73,90
30,57			400
1 79.70	79,48	7966	79.6
1 ( 222			
1,514	1,312		1,349
1.350	1703	6.286	1. 2=4
The state of the last of the l	1.293		1. 292
1 1.694	1,294	1. 2649	1, 301
P59 35	959 31	85927	95924
	1 2 1 2 1	80618	011-
	13.0 1 41  80.50  79.74  79.72  79.72  79.62  79.62  79.78  79.78  79.78  79.79  79.15  79.90  79.17  79.45  79.90  79.45  79.70  1.374  1.290  1.294	20,50 80.47  79 74 79.72  79 74 79.72  79 75 79 71  79 75 79 91  79 78 77  79 62 79 61  79 78 78 78 37  79 62 79 54  79 78 78 79 54  79 78 79 79 79  79 78 79 79 79  79 79 79 79 79  79 79 79 79 79  79 79 79 79 79  79 79 79 79 79  79 79 79 79 79  79 80 79 79 79  79 80 79 79 79  79 80 79 79 79  79 80 79 79 79  79 80 79 79 79  79 80 79 79 79  79 80 79 79 79  79 80 79 79 79  79 80 79 79 79  79 80 79 79 79  79 79 79  79 79 79  79 79 79  79 79 79  1374 1372  1374 1372  1374 1372  1394 1,294	13.0   4    13.5   42   13.20   43     80.50

ROTAMETER FLOW			VERIFIED BY	
	ILRT	DATA SHEET		
TIME/SAMPLE NO.	1 45 / 1400	401 1415	47 / 1430	18 1 144
RTD # 1	861.34	90.29	80,26	80.27
RTD # 2	79.66	79.64	79.63	791.67
RTD # 3	79.69	79,07	79.48	79.67
RTD # 4	74.73	7-1.72	7-1,71	79.70
RTD # 5	79.57	79.56	79,55	79.55
RTD # 6	79,33	79,31	79,30	79.78
RTD # 7	79.60	79,59	79,59	74.40
RTD # 8	79.52	79.51	79.49	74.44
RTD # 9	79.82	7475	7-1.80	74,77
RTD # 10	79.45	79 44	FF 78 79.4	4 7443
RTD # 11	79.12	79.11	74,12	79.11
RTD # 12	79.00	79.04	79.06	74.04
RTD # 13	79.92	76 92	75.43	73.9.
RTD # 14	79.10	79.16	79.15	F1.15
RTD # 15	77.45	<u>79,43  </u>	79.44	77.43
RTD # 16	79.18	79.18	79,12	77.16
RTD # 17	72.79	78.80	79.79	75, 75
RTD # 18	79.47	79.47	79.49	79.48
RTD # 19	78.89	78.88	78.88	78 88
RTD # 20	7891	78 90 1	78.91	7796
RTD # 21 (SPARE)	80.41	EQ.35+		73.90
RTD # 22 (SPARE)	79.62	79.59	79.57	79,50
D. Pt. 0 1	1, 3,4	1.361	1, 359	1. 354
D. Pt. # 2 D. Pt. # 3	1,291	1.291	1.797	1790
D. Pt. # 3	1, 294	1.291	1.303	1. 302
D. Pt. # 4	1,300	1.307	1,310	1.311
Pressure # 1	85919	85916 A	85913	85909
Pressure # 2 (SPARE)	86609	86600	86603	E6-599

BAROMETRIC PRESSURE	30.095		DATE 19 M	AR 79
ROTAMETER FLOW			VERIFIED BY	
	ILR	T DATA SHEET		
TIME/SAMPLE NO.	15001 49	15151 50	1630 51	15451 52
RTD # 1	50.18	80.15	80.11	60.08
RTD # 2	7160	7759	74.57	79.50
RTD # 3	741.1.	1 79 65	79 64	79.53
RTD # 4	79.69	79 51	77.55	77.6
RTD # 5	79.53	79.52	79:51	79.50
RTD # 6	71.38	79.26	19-21.	79.21
RTD # 7	7958	74-57	79.57	7956
RTD # 8	79 48	71.47	1947	79.4
RTD # 9	29.00	79.71	7477	79.7-
RTD # 10	77.43	71.42	79.12	79.43
RTD # 11 RTD # 12	14.10	79.64	7-1-0-1	79.0
RTD # 13	27.05	79.05	77.00	79.00
RTD # 14	79.14	18.42	70.71	7571
RTD # 15	79.43	79.14	79.14	74.14
RTD # 16	1911.	1 39 15	79.41	79.4
RTD # 17	nenii	78.70	78.78	79.13
RTD # 18	199.49	74.49	79.50	
RTD # 19	25.58	18.86	78.87	79.50
RTD # 20		18.59	73:57	788
RTD # 21 (SPARE)	1 50.25	80.21	80.18	70,19
RTD # 22 (SPARE)	74.53	71.51	79.51	79.49
D. Pt. 0 1	17-354	1 1.353	1.351	1 250
D. Pt. # 2	11.301	1.308		1, 350
D. Pt. 6 3	1.304	1.308	1.30%	1 4 308
D. Pt. # 4	1.315	1-313	1.318	1, 321
			1.5010	1 34
Pressure # 1	85906	85962	85899	125676
Pressure # 2 (SPARE)	1 86596	186542	86589	156596

Terminal Operator\_

	ILRT	DATA SHEET		
TIME/SAMPLE NO.	16001 53	16151 54	1630 55	1145 5
RTD # 1	80.05	80.02	50,00	79.90
RTD # 2	79.55	79.54	7954	7951
RTD # 3	79.63	74.1.1	7162	74.1.0
RTD # 4	79.66	79.66	79-45	19.05
TD # 5	79.50	74.49	79.48	79.48
RTD # 6	19.25	79-24	74.23	77.21
RTD # 7	79.50	74.56	79.56	7955
RTD # 8	79.45	79.45	71.45	79.45
RTD # 10	79.79	79.77	71.75	79.79
CTD # 11	79.41		79 41	79.40
TD # 12	79.04	74.0£	79.08	77.07
TD # 13	78.90	78 AT	79.05	79.03
TD # 14	74.14	79.14 670	791.15	78.90
CTD # 15	79.41	71.41	79.41	74.40
TD # 16	79.15	79.16	74.13	79.70
TD # 17	78,79	15.78	78.78	78.77
TD # 18	79.51	71.50	70.51	70 40
TD # 19	78.87		78.87	78.67,
TD # 20	78.89	76.90	78.99	76 14
TD # 21 (SPARE)	80.12	30.09	30.06	80 112
TD # 22 (SPARE)	79.47	79.47	79.46	79.40
. Pt. # 1	1.346	1.3:45	1.338	1.338
. Pt. # 2	1. 314	1.300	1.3110	1.320
. Pt. # 3	1. 3.3	1.312	1.318	1.321
Pt. # 4	1,324	1.326	1.329	1-350
ressure # 1	85893	85559	85887	95984
ressure # 2 (SPARE)	86583	86550	86577	36574
. Pt Dew Point HD - Relative Humidit				2340 12

AD	DE	ND	IX	77
***	L	1411	10	11

BAROMETRIC PRESSURE	30.075	-	DATE 19 M	AR 17
ROTAMETER FLOW			VERIFIED BY	
	ILR	T DATA SHEET		
TIME/SAMPLE NO.	11001 57	17151 58	17301 59	17451 60
RTD # 1	79.93	79.90	79.48	74.54
RTD # 2	1951	79.49	79.49	141.47
RTD # 3	77.60	74.54	74.54	141.95
RTD # 4	79.64	79.44	7113	17:3
RTD # 5	74.47	74.46	19.45	2-1-45
RTD # 6	19.21	79.20	79.19	19919
RTD # 7	79.55	79.50	79.54	79 54
RTD # 8	79 43	79.42	79.41	1761.41
RTD # 9	79:71	29.78	21,00	2/12/2
RTD # 10	74.41	79.40	29.38	29,40
RTD # 11	20.06	77.0%	79.06	14.06
RTD # 12	79.64	79.03	101.02	11.62
RTD # 13	78.90	78.84	70,09	10(119
RTD # 14	29.14	7913	79 /3	199.12
RTD # 15	1 29 41	79.40	74.40	74.40
RTD # 16	77 07	7913	79.11	9.1
RTD # 17	19.77	72.77	78.77	10000
RTD # 18	7700	71.27	7741	79.47
RTD # 19	78.67	78.86	178.84	28.84
RTD # 20 RTD # 21 (SPARE)		75.59	78.57	1 21347
RTD # 22 (SPARE)	1974	79.97	77.74	29:11
KID V ZZ (SPARE)	1 77.44	71 +3	19.42	1 2112
D. Pt. 0 1	1 1.338	1 1.339	1.340	1.338
D. Pt. # 2	1.323	1.325	1.326	1.327
D. Pt. # 3	1.328	1.378	7 239	17.33/
D. Pt. # 4	1.332	1-336	1-336	1.338
Pressure # 1	85581	85978	55576	95473
Pressure # 2 (SPARE)	1 56572	86568	86566	156564
D. Pt Dew Point			0.2	340 128

APPENDIX	D
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	ILRT	DATA SHEET	······································	
TIME/SAMPLE NO.	18001 61	18151 62	18301 63	1847/4
RTD # 1	79.82	79.79	79.76	79 73
RTD # 2	79.46	79,45	79.44	79.40
RTD # 3	79.59	79.57	79.56	70 50
RTD # 4	79.61	79.62	74.60	179.60
RTD # 5	79.41	74.43	79.47	79.41
RTD # 6	79.17	79.18	74.16	79,15
RTD # 7	79.51	79,53	79.52	79,50
RTD # 8	79.41	79.40	79.39	79.31
RTD # 9	79.76	74 77	79.75	79.73
RTD # 10	79.39014	79.34	79.38	79.37
RTD # 11	79.06	79.05	74.04	79.02
RTD # 12	79.02	79.07	79.02	79.00
RTD # 13	78.55	7881	78.87	78.86
RTD # 14	74.12	79.12	79.11	179.11
RTD # 15	79.39	79.35	79.29	79.38
RTD # 16	71.11	79.11	79.04	79.09
RTD # 17	79.76	78.76.	18.75	18.74
RTD # 18	79.43	79.43	79.41	79.34
RTD # 19	76,83	78.83	78.83	79.52
RTD # 20 RTD # 21 (SPARE)	79.58	78.89	78.88	78.87
	71.53	79.85	79.83	79.80
RTD # 22 (SPARE)	1 74.40	79.39	79,34	74.31
D. Pt. 0 1	11,337	1, 335	11,335	1, 336
). Pt. # 2	1.337	1.334		
D. Pt. # 3	1.332	1.332	1.336	1. 333
D. Pt. # 4	1.345	1.348	1 210	1, 352
			05044	11.392
Pressure # 1	T 85271	85868	85866 1864 H	65566
Pressure # 2 (SPARE)	96562	86559	86551	SILEL

APPENDI	X	D
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MAROMETRIC PRESSURE	30,080		DATE 3/	19/79
OTAMETER FLOW			VERIFIED BY	
	ILR	T DATA SHEET		
TIME/SAMPLE NO.	1900 165	1915 166	1930/67	1945 / 68
RTD # 1	79,71	79.69	79.66	79,64
RTD # 2	79.41	179.40	79.39	79.35
RTD # 3	74.55	174.54	79.54	79.54
RTD # 4	79.58	79.59	79 50	71.50
RTD # 5	74.40	79,40	79.34	19.38
RTD # 6	19.14	79.13	79.12	79.12
RTD # 7	19.51	79.51	79.51	79:51
RTD # 8	79.36	77.26	79.34	79.33
RTD # 9	79.75	79.72	79.75	74.73
RTD # 10	79.37	79.37	79.35	79.36
RTD # 11	79.03	79.02	79.02	79.02
RTD # 12	79.00	78.99	7899	78.99
RTD # 13	78.85	18.84	78.83	78 84
RTD # 14	79.11	74.10 PHB		79.09
RTD # 15	79.38	1-78-3579.31		79.36
RTD # 16	79.07	79.09	79.09	79.68
RTD # 17 RTD # 18	78.74	78.74	78 73	18.73
RTD # 19	79.39	79.39	79.37	79.36
RTD # 20	78.8.1	78.80	78.76	7881
RTD # 21 (SPARE)	78.87	78 27	78 27	78.56
RTD # 22 (SPARE)	19.77	171.75	79.74	79.71
NIO F EZ (STAND)	1 19, 36	79.36	79.34	179.34
). Pt. # 1	11. 335	11.336	1, 3 360	1,335
). Pt. # 2	1. 339	1. 340	1.346	1.344
). Pt. # 3	1, 333	1, 344	1.331	11: 244
D. Pt. # 4	11. 352	1, 354	1.354	1.356
			11.22.7	11. 3.76
Pressure # 1	85861	85859	85851	185854
Pressure # 2 (SPARE)	86 557	86 550	86548	86 546
D. Pt Dew Point				340 130

AP	E	ND	IX	D	
-	-	-	-	-	

	1LR	T DATA SHEET	γ	
TIME/SAMPLE NO.	3000 1 69	205 1 70	20301 71	2045/72
RTD # 1	79.62	79.60	79.58	74.54
RTD # 2	79.39	79.37	79.36	79.35
RTD # 3	79.54	74.54	79.53	79.52
RTD # 4	79.58	79.54	79.55	70.55
RTD # 5	79,38	77.38	79.36	79.36
RTD # 6	79.12	79:12	79.11	79.07
RTD # 7	79.52	79,57	79.51	79.50
RTD # 8	79.33	79,30-	79.31	79.31
RTD # 9	79.73	79.74	79.71	79.71
RTD # 10	74.36	79.36	79,35	79.35
RTD # 11	79.02	70.03	72.01	7100
RTD # 12	79.00	74,00	78.49	7598
RTD # 13	78,83	78,82	78.50	78.81
RTD # 14	79.09	79.09	79.09	79.08
RTD # 15	79.31	19.37	79.37	79,36
RTD # 16	79.07	79.08	179.66.	79.07
RTD # 17	78.74	1 78 74	78.73	79 72
RTD # 18	79.34.	79.36	79.34	79.33
RTD # 19	78.50	78.80	78,80	75,79
RTD # 20	75.57	7887	78.86	78 66
RTD # 21 (SPARE)		79.67	79.65	179,62
RTD # 22 (SPARE)	1 79.34	79.34	79,33	79.32
D. Pt. 0 1	1 1 2 2 7	1 . 020	1 . 210	1. 2.00
D. Pt. # 2	1,337		1, 340	1344
D. Pt. # 3	1 3 47	1. 350	1.351	1.343
D. Pt. # 4	11.356		1. 344	1.352
D. 10. v 4	11.330	11.359	1, 358	11.346
Pressure # 1	85853	85851	85849	185847
Pressure # 2 (SPARE)	86544	86542	86540	86538

MAROMETRIC PRESSURE	30,095		DATE 3/	19/79
OTAMETER FLOW			VERIFIED BY	113
	ILI	RT DATA SHEET		
TIME/SAMPLE NO.	2100 1 73	21151 74	21301 75	2146 241
RTD # 1	79.57	74.50	79.46	79.42
RTD # 2	70 34	70.33	74, 32	75.21
RTD # 3	74 52	1 79.51	74.50	79.50
RTD # 4	70 24	19.54	79.53	79.63
RTD # 5	79.36	79,35	79.34	79.33
RTD # 6	79.09	79.09	74.08	79.07
RTD # 7	79.49	79.51	79.49	79,50
RTD # 8	K1.30	79,30	79. 78	79.29
RTD # 9	179.72	79.72	79.67	79.11
RTD # 10	79.35	19.35	79.35	77.34
RTD # 11	77.00	79.00	78.49	78.44
RTD # 12	78 99	78.98	128.97	78.9
RTD # 13	78.81	7081	78.81	78 %
RTD # 14	79.01	74,69	74.08	79.07
RTD # 15	79.36	74.36	79.35	79,34
RTD # 16	79.06	77.66	79,04	79,65
RTD # 17	78,72	70.71	7972	79.71
RTD # 18	79.34	79.33	79,3:1	19.31
RTD # 19	78,79	78.80	78.78	78.79
RTD # 20 RTD # 21 (SPARE)	78.86	78.87	76.86	78.86
RTD # 22 (SPARE)	79.61	74.59	79.56	79.48
KID F ZZ (STARE)	1 79.32	79.30	179,29	179,78
D. Pt. 0 1	11,337	11,346	11.344	11,352
D. Pt. # 2	1.352	1.357	1,356	11.359
D. Pt. # 3	1.349	1.350	1.350	1,352
D. Pt. # 4	1.358	1.360	1.362	1.363
				11.500
Pressure # 1	85045	E5844	85842	185840
Pressure # 2 (SPARE)	186537	86535	86534	86533
D. Pt Dew Point RHD - Relative Humidi				340 132

		RT STAR	1	
	ILR	T DATA SHEET	<del></del>	-
TIME/SAMPLE NO.	23001 77	122157 78	22301 79	22457 50
RTD # 1	199.41	79.33		79.32
RTD # 2	7931	7931	29.38	100. 311
RTD # 3	1 79.51	19.50	79-50	79.49
RTD # 4	1954	.70 52	27.52	.74 52
(TD # 5	79.34	79.33	74.32	74.33
RTD # 6	79.08	79.08	74.07	74.06
RTD / 7	79.50	79.51	79.50	1444
TD # 8	74.24	74.29	79.29	79.27
RTD # 9	74.1.1.	79 1.7	29.65	79.71
RTD # 10	79.35	79.34	79.34	79.51
TD # 11	78.98	79.78	78-49	78.99
TD # 12	28.98	78 98	25.95	73.91
TD # 13	78.80	78.80	78.80	79.79
TD # 14	79.07	79.08	79.07	79.07
TD # 15	71.36	79.35	79.36	79.35
TD # 16	79.05	20.01	79.03	79.03
TD # 17	78.71	78.7 with	74.72	78.77
TD # 18	74.31	79-32	74.31	79.30
TD # 20	28.28	7879	78.79	73.75
TD # 21 (SPARE)	29.52	75-16	1 23.87	74.36
TD # 22 (SPARE)		79.50	199.49	71.47
ID F EE (STAKE)	1 29.24	77.29	19.29	79.27
Dr. 4 1	1 1 2 1/			,
• Pt · # 1	1.34/	1.345	1 3.18	1-3:14
	1.359	1.341	1.300	1.361
Pt. # 3	1 2/1	1.333	1-36.3	1.350
, FL. F 4	1.364	1-365	1. 1. 30.8	1.369
ressure # 1	85839	1 9 5 0 2 5	1 8.500	
ressure # 2 (SPARE)		85839	95-637	22.232
Pt Dew Point	1 36530	1 86529	\$6528	36526

73001 87 79.29 79.29 79.49 79.52	2315-1 82 79.28 79.29	23501 53	23457
73001 87 79,29 79,29 79,49	79.28	The state of the s	
79,29	79.28	The state of the s	
79.29	74,24	1 / 1 / 1	79.2
79,49		79 28	70 14
THE RESERVE THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.	79.48	7418	7447
the state of the s	79.51	79.51	74.51
79.31	79.31	79.31	79-30
19,05	79.05	79.03	79.04
79.49	79.49	79.49	79.50
79,27	79.27		79.27
	79.63	71.65	7912
79.34	79.34	74.53	79.00
78,97	79.97	78 98	78.97
78.97	78,47	78.96	78:47
		79.79	73.97
		79.07	7909
79.35		74.35	79.35
	79.02	77.02	7101
	THE RESIDENCE OF THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER, THE PERS		72.71
	74.33		74.25
			73.75
NAME OF TAXABLE PARTY OF TAXABLE PARTY.	74.56		73.55
			79.40
77,21	19.26	14.25	79.26
1.352	1 1-363	1.21.1	1.361
1,366	1.362		1.301
1362	1.361		1-357
1.371	1.371	1.375	1.37.2
8583110,0	95933	95032	185830
	the state of the s	36.523	86522
	19, 27 19, 68 79, 34 78, 91 78, 91 78, 91 79, 07 79, 03 79, 03 78, 79 78, 79 78, 79 78, 86 79, 45 79, 27 1, 3, 66 79, 45 19, 27	79, 27 79, 68 79, 34 79, 34 79, 34 79, 97 78, 97 78, 97 78, 97 78, 97 79, 07 79, 07 79, 07 79, 07 79, 03 79, 03 79, 03 79, 03 79, 03 79, 03 79, 36 79	79, 27 79, 27 79, 27  79, 28 79, 34 79, 35  79, 34 79, 34 79, 35  78, 91 78, 91 78, 98  78, 91 78, 91 78, 98  78, 91 79, 71 78, 98  78, 91 79, 71 78, 98  78, 91 79, 71 78, 98  78, 91 79, 71 78, 98  79, 01 79, 01 79, 07  79, 01 79, 01 79, 07  79, 03 79, 02 79, 28  78, 72 78, 71 78, 71  79, 30 79, 28  78, 79 73, 78  78, 79 73, 78  78, 79 73, 78  78, 79 73, 78  79, 45 79, 43 79, 41  79, 21 79, 26 79, 28  1, 3, 66 1, 36, 2 1, 36, 4  1, 3, 62 1, 36, 2 1, 36, 4  1, 3, 62 1, 36, 1 1, 37, 5

MBIENT TEMPERATURE  MAROMETRIC PRESSURE	62°		DATE 20 M	3
OTAMETER FLOW	NA			as RA
THE PROPERTY			VERIFIED BY	ass jon
	ALR:	T DATA SHEET		
TIME/SAMPLE NO.	0000 1 85	0015 1 86	00301 37	00457 8
RTD # 1	79.24	79.20	79.17	77.17
RTD # 2	79.27	79.27	77 27	177.24
RTD # 3	79.47	1 79.47	79.46	79.45
RTD # 4	79.50	79.50	77.20	77.4
RTD # 5	79.30	79.30	79.28	79.28
RTD # 6	79.03	79.03	79.02	79.02
RTD # 7	79.49	79.50	79.47	79.48
RTD # 8	79.26	79.27	79.26	79.25
RTD # 9	72.65	79.44	79.4.2	7/59
RTD # 10	72.33	79.33	79.33	19.32
RTD # 11	78.97	78.97	73.95	75.94
RTD # 13	75.97	75.97	18.91	75.17
RTD # 14	79.07	75.77	73.77	75.30
RTD # 15	79.35	79.07	79.06	1907
grp # 16	79.01	19.01	77.35	79.34
RTD # 17	7971	78.71	75.70	75.71
TD # 18	79.28	79.27	79.25	79.25
RTD # 19	78.78	78,78	73.77	78.77
TD # 20	75.56	78.86	13.36	73.55
(TD # 21 (SPARE)	79.40	79.33	79.36	79.35
RTD # 22 (SPARE)	1 79.24	79.24	1 79.24	7924
). Pt. # 1	1.364	1 1.366	1.341	1 1 2/2
). Pt. # 2	1.365	1.367	1.371	1.363
). Pt. # 3	11.358	1.344	1,343	1.370
). Pt. # 4	1.374	1.377	1.378	1.379
Pressure # 1	85829	1 90000	1 32-3 3 3	1 9 30 57
Pressure # 2 (SPARE)	36520	85825	84518	35820
D. Pt Dew Point		1 20113	- 363 13	136517

Terminal Operator Sicium

		APPENDIX D		
AMBIENT TEMPERATURE	610		HOUR NO.	4
BAROMETRIC PRESSURE_	30.08 AA		DATE 20	march 29
ROTAMETER FLOW			VERIFIED BY	13 11/11/11
				/
	The second name of the second na	RT DATA SHEET		=
TIME/SAMPLE NO.	0100 1 89	0115 1 90	0130 / 17	0451 92
RTD # 1	79.15	79.15	79.13	79.13
RTD # 2	79.26	71.24	79.24	79.29
RTD # 3	79.45	79.45	79.44	77.44
RTD # 4	79.47	179.47	79.47	77.42
RTD # 5	79.28	79.27	79.27	79.27
RTD # 6	79.01	79.01	79.00	79.00
RTD # 7	79.48	79.48	77.48	79.418
RTD # 8	79.25	79.25	79.25	79.24
RTD # 9	79.59	79.56	29 53	74.56
RTD # 10	79.32	79.32	77.32	79.32
RTD # 11	78.96	73.95	78.94	75,94
RTD # 12	78.46	78.96	78,96	78:45
RTD # 13	79.77	78.77	25.78	73.73
RTD # 14	79.06	79.06	79.06	79.0%
RTD # 15	79.35	79.34	29.34	79.33
RTD # 16	79.01	79,00	72.00	79,00
RTD # 17	78.70	73.70	73.70	75.70
RTD # 18	79,25	79.25	77.24	79.24
RTD # 19	78.78	78.78	78.78	78.27
RTD # 20	78,53	73.46	78.85	
RTD # 21 (SPARE)	79.34	79.32	79.31	78.55
RTD # 22 (SPARE)	79.22	79.22	79.22	79.30
D. Pt. # 1	1.31.6	1 1,373	1.373	1,373
D. Pt. # 2	1.374	1.374	1.374	13-27_
D. Pt. # 3	1.362	1.362	1.364	1.370
D. Pt. # 4	1.380	1 1.331	1 1.337	17,384
Pressure # 1	858.25	85824	X5823	1 0000000
Pressure # 2 (SPARE)	84515	86514	865 13	9/5/2
D. Pt Dew Point RHD - Relative Humid				
Pressure,	· · · · · · · · · · · · · · · · · · ·		- 274	0 177
erminal Operator	- Lecher		239	0 136

	APPENDIX D		
61°		HOUR NO.	5
30.060		DATE 20 H	n - 1 79
		/	14 11
,,,,		VERIFIED BY	u arr
	T DATA SHEET		
	0215 / 97	102301 95	02451 96
79.11			79.10
79.23		the second section of the second section is a second section of	79.22
the state of the s		the same of the sa	79.42
79.45			79.45
1 79.26	79.26		79.26
1899	79.00	79.01 vit	78.99
79.47	79.47	79.47	79.47
79.23	and the same of th	79.22	79.23
79.56	79.56	79.56	79.57
79.31	79.32	79.31	79.31
78.94	78.95	7294	75.93
79.96	78.96	75.96	78,91
75.78	75.78	73.78	74.79
	74.66	79.06	79.06
		7733	74.34
the second name of the second name of the second name of		79.00	78.97
	the second secon	78.70	73.71
	The second secon		25.22
the same of the sa			78.77
			79.86
			79.26
1 79.79	14.20	19.19	79.19
1 1.368	1 1.375	1 1.372	1.374
1,377	1.380		1.379
1.366	1 365	the second name of the second name of the second name of	1.371
1 1.354	1.397	1.383	1,379
85821	85820	1 05019	858 19
1 22 3 41	1 900 20	85819	13117
	30.060  NA    11   12   12   13   14   15   15   15   15   15   15   15	30.060  NA  LRT DATA SHEET  0200 1 93 0215 1 94  79.11 79.11  79.23 79.24  79.45 79.45  79.26 79.26  79.47 79.47  79.23 79.23  79.56 79.56  79.31 79.32  79.56 79.56  79.31 79.32  78.99 78.96  79.31 79.32  78.99 78.96  79.25 79.28  79.26 79.26  79.27 78.99  78.78 78.79  78.78 78.79  78.78 78.79  78.78 78.79  78.78 78.79  78.78 78.79  78.79 78.70  79.29  79.19 79.20	

ROTAMETER FLOW	30.045 NA		VERIFIED BY	19 14/20
THETER FLOW	7011		VERIFIED BI	C. S. Cation
		T DATA SHEET	1	
TIME/SAMPLE NO.	0300 / 97	0315 / 98	0335 1 99	03451 100
RTD # 1	79,09	79.08	79.08	79.07
RTD # 2	79.21	79.21	79.20	70.19
RTD # 3	79.42	79.41	79.41	79.40
RTD # 4	79.45	74.45	79.44	79:42
RTD # 5	79.24	79.24	79.24	79.23
RTD # 6	79.00	79.00	78,99	75.98
RTD # 7	79.47	79.47	79.96	79.46
RTD # 8	79.22	79.21	79.21	179.20
RTD # 9	79.58	79.54	79.55	77.54
RTD # 10	79.30	77:30	79.30	79.30
RTD # 11 RTD # 12	73.93	18.73	78.7.3	73.92
RTD # 13	78,95	15.45	73.95	78.94
RTD # 14	70 05	75, 75	75.76	75.76
RTD # 15	79.05	79.05	79.06	79.64
RTD # 16	73.19	79.33	79.33	79.32
RTD # 17	78.70	7069	77.19	75.73
RTD # 18	79.21	72.21	79.21	77 20
RTD # 19	75.76	78.77	78.17	73:16
RTD # 20	78.85	1888	73.55	74.84
RTD # 21 (SPARE)	79.25	79.23	79.23	79.21
RTD # 22 (SPARE)	1 79.19	79.19	79.17	29.17
D. Pt. 0 1	1 1 227	1 1.350	1 ( 39/	1 7 505
D. Pt. # 2	1.377		1.256	1.382
D. Pt. # 3	1,352	1.333	1.3.73	1.353
D. Pt. # 4	1.386	1.376	1.377	1/3/2
	1. 30.6	-1 1:32/	1 1.3.70	1.39/
Pressure # 1	85818	1 85816	25314	8.5815
Pressure # 2 (SPARE)	36.508	36506	86506	86505
D. Pt Dew Point RHD - Relative Humid: Pressure,				. 2340 13

	APPENDIX D		
59°		HOUR NO	1
30.045		DATE 20	m rel 79
N/A		VERIFIED BY	A after
H.R	T DATA SHEET		
0400 / 101	04.5/102	24)	05001 104
A STATE OF THE PARTY OF THE PAR	and the same of th	Agreement nonemption statement	79.05
			70) (8
			121.38
		A REAL PROPERTY AND ADDRESS OF THE PERSON NAMED IN COLUMN TWO	71.10
			74.22
78.98			78.96
79.46			79.45
			179.19
79.55		The second secon	79.53
77.29			79.28.
7891	78.91		78.91
78.95	78.94	78.94	78 94
78.7%	75.74	78.75	78.73
79.05	79.05	79.03	79.03
79.33	79.31	74.32	7-1.32
79,00	78.98	78.99	28.96
	78.18	78.68	78.67
		77 19	79.19
		78.76	78.76
	75.54	78.84	74.83
		79.19	79.19
79.16	79.13	77.16	79.14
1.388	1 1,382	1.377	1.384
1.387			1.385
1,375			1379
1.390	1.393	1.375	1.394
85314	1 65073	1 0.50 / 2	1 (100 10
86504	56503	2:58/2	25812
	30.045  NA  NA  O400 1 101  79.07  79.31  79.42  79.46  79.19  79.55  79.46  79.75  79.75  79.75  79.75  79.75  79.75  79.75  79.75  79.75  79.75  79.75  79.75  79.75  79.76  79.75  79.76  79.75  79.76  79.76  79.76  79.77  79.85  79.16	## DATA SHEET (23) 0400   101   04.5   102 79.07   79.06 79.19   79.18 79.31   79.31 79.42   79.42 79.23   79.42 79.46   79.45 79.19   79.29 79.55   79.54 79.21   78.91 78.75   78.91 78.76   78.74 79.05   79.05 79.33   79.31 79.00   78.98 78.68   78.98 78.68   78.98 78.68   78.98 78.68   78.98 78.68   78.98 78.68   78.98 78.68   78.76 79.20   79.19 79.16   79.15	NA   VERIFIED BY

AMBIENT TEMPERATURE	580	A) ENDIX D	HOUR NO.	9
BAROMETRIC PRESSURE	30.050		DATE 20 HA	
ROTAMETER FLOW	NA		VERIFIED BY	11/11/11
		J DATA SHEET _		
TIME/SAMPLE NO.	0500 AT 20	051514 (27	05301 (28)	25
RTD # 1	79.05	79.04	79.03	79,03
RTD # 2	79.15	79.17	79.16	the second contract of the second contract of the second
RTD # 3	79.38	79.38	79.34	79.15
RTD # 4	22.42	11.40		79.36
RTD # 5	79.20	72.21	79.20	79.59
RTD # 6	78.95	78.95	78.96	79.19
RTD # 7	72.45	79.46	79.44	75:45
RTD # 8	72.18	79.18	79.17	the second second second second second second
RTD # 9	79.52	71.52	79.52	79.17
RTD # 10	79.27	79.28	79.27	79.26
RTD # 11	78.40	78.90	78.90	78.34
RTD # 12	7.7.44	78.93	75,92	78.92
RTD # 13	73.72	73.73	75.71	75.10
RTD # 14	79.03	79.02	79.02	79.02
RTD # 15	72.31	79.32	79.31	79.30
RTD # 16	78.48	78.97	78,95	
RTD # 17	78.66	75.67	78166	73.46
RTD # 18	77.18	79.13	79.18	79.18
RTD # 19	73.76	78.75	78.74	78.74
RTD # 20	78.83	78.83	75.82	78.82
RTD # 21 (SPARE)	1 79.18	79.17	79.16	79.14
RTD # 22 (SPARE)	79.15	79.14	7914	29.13
D. Pt. 0 1	1.385	1.387	1.358	1 1 3 27
D. Pt. # 2	1. 355	1.390		1.386
D. Pt. # 3	1 357	1.380	1.390	1.372
D. Pt. # 4	11.397	1.397	1.355	1 307
	1.1.211	1.1.377	1 1.397	1.397
Pressure # 1	85311	35810	85310	85804
Pressure # 2 (SPARE)	1 865 01	86999	36498	86498
D. Pt Dew Point RHD - Relative Humidi			. 23	40 140
Pressure,	- Annual Contraction of the Cont			
erminal Operator	benu	-eh		

VERIFIED BY  C6301 111  79.01  79.14  79.35  79.19  79.19  79.44  79.16  79.26  79.26  79.26  79.26  79.31  79.94	9 Horak 29 / 20 19.00 19.00 19.00 19.00 19.13 19.13 19.13 19.15 19.15 19.15 19.15 19.15 19.15 19.15 19.15 19.10 19.1
VERIFIED BY  C6301 111  79.01  79.14  79.35  79.19  79.19  79.44  79.16  79.26  79.26  79.26  79.26  79.31  79.94	79.00 79.00 79.00 79.14 29.36 79.18 79.18 79.18 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.17 79.18 79.18
VERIFIED BY  C6301 111  79.01  79.14  79.35  79.19  79.19  79.44  79.16  79.26  79.26  79.26  79.26  79.31  79.94	79.00 79.00 79.00 79.14 29.36 79.18 79.18 79.18 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.17 79.18 79.18
79.01 79.01 79.01 79.14 79.35 79.19 79.19 79.16 79.16 79.26 79.26 79.26 79.26 79.31 79.01 79.01 79.31 79.94	79.00 79.14 79.14 79.13 79.13 79.13 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15
79.01 79.01 79.01 79.14 79.35 79.19 79.19 79.44 79.16 79.26 79.26 79.26 79.26 79.26 79.26 79.31 79.01 79.31 79.94	79.00 79.14 79.14 79.13 79.13 79.13 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15
79.01 79.01 79.01 79.14 79.35 79.19 79.19 79.44 79.16 79.26 79.26 79.26 79.26 79.26 79.26 79.31 79.01 79.31 79.94	79.00 79.14 79.14 79.13 79.13 79.13 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15
79.01 79.01 79.01 79.14 79.35 79.19 79.19 79.44 79.16 79.26 79.26 79.26 79.26 79.26 79.26 79.31 79.01 79.31 79.94	79.00 79.14 79.14 79.13 79.13 79.13 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15
79.14 79.35 79.37 79.19 79.19 79.16 79.16 79.26 79.26 79.26 79.26 79.26 79.31 79.31 79.94	79.14 29.36 79.37 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.17 79.78 79.78 79.78 79.78
79.14 79.35 79.37 79.19 79.19 79.16 79.16 79.26 79.26 79.26 79.26 79.26 79.31 79.31 79.94	79.14 29.36 79.37 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.15 79.17 79.78 79.78 79.78 79.78
79.19 79.19 79.19 79.44 79.16 79.26 79.26 79.26 79.26 79.31 79.01 79.31 79.94	79.13 79.13 73.24 79.15 79.15 79.26 79.26 78.31 78.91 79.01
79.19 72.99 79.44 79.16 79.26 79.26 78.89 78.91 72.10 79.01 79.01	79.13 73.24 79.43 79.15 79.51 79.26 78.37 78.91 78.78 79.01
75,99 79,44 79,16 79,26 79,26 78,87 75,91 75,91 79,01 79,31	73.04 79.43 79.15 79.51 71.24 73.71 73.71 79.73 79.01
75,99 79,44 79,16 79,26 79,26 78,87 75,91 75,91 79,01 79,31	73.04 79.43 79.15 79.51 71.24 73.71 73.71 79.73 79.01
79.16 79.26 79.26 78.89 78.91 79.01 79.01 79.31	79.43 79.15 79.51 79.51 79.71 79.73 79.73
79.50 79.26 78.87 78.97 72.69 79.01 79.31 78.94	79.51 79.26 75.57 75.91 79.68 79.01
79.50 79.26 78.87 78.97 72.69 79.01 79.31 78.94	79.51 79.26 75.57 75.91 79.68 79.01
78.89 78.91 78.91 79.01 79.31 78.94	78.57 78.91 79.79 79.01
75.91 72.69 79.01 79.31 79.94	78.91
72.69 29.01 79.31 79.94	79.29
79.01 79.31 79.94	7901
79.31	Name of the Owner of Street, St
75.94	7930
THE RESIDENCE OF THE PARTY OF T	THE RESERVE AND ADDRESS OF THE PARTY AND ADDRESS.
	74.76
78.65	78.1.5
1 79.17	74.17
18.73	75.73
73.31	13.52
79.13	7912
79.11	2713
1 / 203	1 / 202
	1.393
	1.394
	1.405
1 11405	1 1.703
35807	1 45800
The second secon	186445
	79.13 79.11 1.393 1.395 1.389 1.465

90		HOUR NO.	10
		-	10
.09		DATE 20	nort 79
19		VERIFIED BY	1 2. Ut
(Ib)	PT DATA SHIFT	F14	
(34)		(36)	(37
rec 1 113	10715 1 114	0301 115	07451116
79.01	79.01	79.00	79.00
79.13	79.13	77.13	79.13
79.35	79.34	74.34	79.33
79.35	79.38	7137	79.35
79.15	29.18	79.17	79.15
78.92	78.43	74.43	78.92
79.94	72.43	79,43	77.42
79.14	79.14	79.15	1 79/3
79.49	7741	29.47	79.49
79.25	79.76	79.25	14.26
75.59	78:48	78.87	18.86
73.91	78.40	7=, =4	75.84
78.10	79.69	78,69	73.70
77.01	7900	79.00	79.00
79.24	77.29	79.29	79,28
75.94	75,72	73.93	78.42
78.65	73.65	73.64	78.64
79.17	79.16	79:16	79.15
	78.72	78.23	78.72
	78.50	73.31	175.51
	79.10	79.10	79.10
79.11	79.12	79.09	179.10
1. 396	1 1.392	1 1 420	1.395
1.395	The second secon		1.402
THE RESERVE AND PERSONS ASSESSED.			11,317
1.407	1.408	1.407	1.411
85811.	1 85805	25206	1 86864
56994	86994	36494	85504
	79.01 79.01 79.01 79.35 79.35 79.35 79.49 79.49 79.49 79.41 79.25 78.39 78.10 79.21 79.21 79.21 79.21 79.21 79.21 79.21 79.21 79.21 79.21 79.21 79.21 79.12 79.12 79.12 79.12 79.12 79.12 79.12 79.12 79.12	TERT DATA SHEET   34   35   79.01   79.01   79.01   79.01   79.01   79.01   79.35   79.35   79.35   79.35   79.35   79.18   78.92   78.92   78.93   79.14   79.14   79.14   79.14   79.15   78.53   78.90   78.10   78.90   78.10   78.90   78.10   78.90   78.10   78.90   78.10   78.90   78.90   78.10   78.90   78.10   78.90   78.12   78.00   78.12   78.12   78.12   78.12   78.12   79.10   79.11   79.12   79.10   79.11   79.12   79.10   79.11   79.12   79.10   79.11   79.12   79.12   79.11   79.12   79.12   79.11   79.12   79.12   79.11   79.12   79.12   79.12   79.12   79.11   79.12	Thrt Data Sheet   38   39   39   39   39   39   39   39

AROMETRIC PRESSURE	30.10		DATE 20	Marl 79
OTAMETER FLOW	NA		VERIFIED BY P	cheyer
			Continue and Labor	
	JL.	RT DATA SHEET		
TIME/SAMPLE NO.	0800 1117 35	0815/ 1/39	CS301 119	CS451 13
RTD # 1	79.00	70.98	78.98	78.9
RTD # 2	79.12	7911	2911	29.11
CTD # 3	79.33	79 33	7934	79 32
RTD # 4	79.35	79.36	79.30	79.55
TD # 5	7915	79.15	29.15	79.13
RTD # 6	75.92	78.93	78 90	7- 9
RTD # 7	79-42	7942	7942	79.4
RTD 0 8	79.12-	79.12	79.13	79 11
TD # 9	77.49	79 49	79 50	70 41
RTD # 10	79.25	79.24	1924	79 23
TD # 11	78.86	78.86	75 56	78.80
KTD # 12	78.89	78 69	78.56	78 50
RTD # 13	78.71	78.69	78.71	75 71
RTD # 14	78.99	78.99	79.00	74 00
RTD # 15	79,29	79.28	79.28	29.2
RTD # 16	78.92	78.92-	78-91	78.90
RTD # 17	78.64	28.64	78.65	78.00
TD # 18	79.15	7916	79.15	79 14
RTD # 19	78 72	78.72	78.72	74 71
TD # 20	78 72	78.82	75.01	76 51
TD # 21 (SPARE)	79.69	79.0%	79.08	74.07
RTD # 22 (SPARE)	1 79.10	79.09	79.08	79.68
). Pt. # 1	1 1.392			
). Pt. # 2	the state of the s	1.394	1 399	1.401
). Pt. # 3	1,403	1.403	1.404	1.42
). Pt. # 4		1,402	1 403	1.40
	11.412	1.413	1.415	1.410
ressure # 1	1 85804	E5'53	85603	85802
ressure # 2 (SPARE)	186492	E1:492	76491	86491

BAROMETRIC PRESSURE	30,11	-	DATE 20 M	ARCH 19	
ROTAMETER FLOW	NA	-	VERIFIED BY	Utleyer	
	LILRT DATA SHEET				
TIME/SAMPLE NO.	0900/121	04151 122	09301 123	0945/12	
RTD 0 1	78.97	78.96	70.96	70.9	
RTD # 2	79/15	79.10	79 69	7900	
RTD # 3	79 32.	79.31	7931	7430	
RTD # 4	75) 34-	79,34	79.34	29 35	
RTD # 5	77.14	79.14	19.14	74 /3	
RTD # 6	78.90	76.89	78.90	78.40	
RTD # 7	79.41	79.42	79,4-1	74) 42	
RTD # 8	79.11	19.12	79.11	29.10	
RTD # 9	79.49	19.49	29.50	7749	
RTD # 10	79.23	79.24-	79.23	79 23	
RTD # 11	75.85	18:80	78.85	76 6	
RTD # 12	70.84	78.89	78.18	1-1-8	
RTD # 13	78.72	78.74	78.74	19-78-76	
RTD # 14	78.49	78.99	78.99	7/6 (14)	
RTD # 15	74 28.	79.29	79.29	79.20	
RTD # 16	28.91	7849	78.91	70.91	
RTD # 17	78.64	78.1cle	78.66	78 44	
RTD # 18	1412	29.16	79.17	79.17	
RTD # 19	78.71	78.73	78,72	78.72	
RTD # 20	78.81	28.81	78.81	75.86	
RTD # 21 (SPARE)	7406	77.04	79.05	2900	
RTD # 22 (SPARE)	1 79 69	79.08	7907	79.00	
D. Pt. # 1	1 1 400	1 406	1.404	1,404	
D. Pt. # 2	1.404	1.408	1405	1,418	
D. Pt. # 3	1.399	1408	1.403		
D. Pt. # 4	1 411	1.415	1,415	1419	
Pressure # 1	85802	85801	eceri	25501	
Pressure # 2 (SPARE)	96490	86490	85801 86490	56990	

Terminal Operator\_\_\_

### APPENDIX D

AMBIENT TEMPERATURE 7	3	HOUR NO	13
BAROMETRIC PRESSURE 30.	10	DATE 20 MAIR	79
ROTAMETER FLOW NA		VERIFIED BY PROY	mett

	(ILBT DATA SHEET			
TIME/SAMPLE NO.	1000/125	1015/ 12/5	1030/ 121	1047 120
RTD # 1	78.95	74.95	78.95	7090
RTD # 2	70 67	79.64	167.00	79.10
RTD # 3	19.30	1 71 31	761.30	70131
RTD # 4	14.33	· K1 33	74.33	79.33
RTD # 5	79.13	74.13	79.13	79 13
RTD ∉ 6	28.59	28.41	78.90	78/11
RTD # 7	74,12	19.42	79.42	70,43
RTD 2 8	79.11	79.11	79.11	74.10
RTD # 9	1 1x152	27.51	79.50	79.51
RTD # 10	74.22	79.22	74.23	79 24
RTD # 11	18.54	28.85	79.24	74.86
RTD # 12	25.15	28.88	78,88	70,85
RTD # 13	13.15	98.75	78.76	14.77
RTD # 14	28.44	28,49	74-00	13:15
RTD # 15	19.19	199 20	74.20	79.23
RTD # 16	78.41	78.41	78.40	74.58
RTD # 17	78 65	28.19	79.16	7- 6.7
RTD # 18	79.18	11.19	71.21	74.21
RTD # 19	91 99	21,22	77.77	70, 73, 14
RTD # 20	7851	78.82.	78.33	77,95
RTD # 21 (SPARE)	79.63	1769 614	77.00	-10 01
RTD # 22 (SPARE)	19.07	79.08	79.07	7107

D. Pt. 0 1	1.408	1 1.418	1.349	1-408
D. Pt. # 2	1.412	1.1419	1.411	1.414
D. Pt. @ 3	1.464	1.41 DOM	1.409	1.467
D. Pt. # 4	1.418	1.420	1.420	1.420

Pressure # 1	85501	85800	85800 WYH	25500
Pressure # 2 (SPARE)	1 864867	41.449	56,419	5601641

D. Pt. - Dew Point

RHD - Relative Humidity Detector,\_\_\_\_

Pressure,\_\_\_\_

Terminal Operator fol 1. Musely

NOTE: 1045 END OF JURT.

2340 145

## OPERATING PROCEDURE 13100.1, PAGE 53

# INTEGRATED LEAK RATE TEST

AMBIENT TEMPERATURE	14		HOUR NO.	
BAROMETRIC PRESSURE 3	0.10		DATE 3-2	0-79
ROTAMETER FLOW 3	2		VERIFIED BY Dis	othyweh
	ILR	DATA SHEET		
TIME/SAMPLE NO.	1	1	11301	11451
RTD # 1			78.95	76 96
RTD # 2			79 00	77.11
RTD # 3			79 3 / 79 3 L	77.32
RTD # 4			79 32	74 32
RTD # 5			79.13	79.14
RTD # 6			78.90	75.91
RTD # 7			79.41	79.44
RTD @ 8			79.11	74.12
RTD # 9			79.52	79 54
RTD # 10			79.23	74.25
RTD # 11			78.86	75 67
RTD # 12		PAGE SPANISH	78.69	76 40
RTD # 13		Entric Co. 44	78.79	74.50
RTD # 14			78.99	79.01
RTD # 15			79.32	79.33
RTD # 16			72.91	78.92
RTD # 17			78.608	70.70
RTD # 18			1 79.28	79.29
RTD # 19		المناس والمراق	78.74	79.29 78.25
RTD # 20			77.54	75-11/2
RTD # 21 (SPARE)			79.04	79.05
RTD # 22 (SPARE)			79.07	14 79.0h
ROTAMETER FLOW			3.2 SCFM	3.2 SCF#
D. Pt. # 1			1.420	1,414
D. Pt. # 2			1.418	1.419
D. Pt. # 3			1411:	1 1-12
D. Pt. # 4			1422	1.424
				27 PSIG
Pressure # 1			85799	25797
Pressure # 2 (SPARE)		DECEMBER 1	86456	AGARS

# OPERATING PROCEDURE 13100.1, PAGE 53 CLRT

78.94 79.01 79.30 79.30	DATA SHEET  12151  78.95  79.06	12301 173.93	12451
78.94 79.01 79.30 79.30	78.95	73.93	Married Woman Company of the Company
78.94 79.01 79.30 79.52	7895 79.68	73.93	Married Woman or William Company of the Company of
78.94 79.01 79.30 79.52	7895 79.68	73.93	Married Woman or William Street, Stree
79.0° 79.3° 79.52	79.08		78.43
79.30 79.52		79 07	781.67
THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.	79 30	161 24	79.30
575 13	79 32	79,21	-/1 2
79.12	79.12	74.10	79.11
78.90	78.90	78.87	78.87
79.42	7942	79.41	79 40
79.10	79.11	77.04	79 10 0
			79.67
	The second control of		79.23
			70.65
MATERIAL PROPERTY OF THE PARTY			78-85
ACCORDING TO THE RESIDENCE OF THE PERSON OF		THE RESERVE AND THE PERSON NAMED IN	19.00 0
		78 90	73.00
	The second secon	78.48	70 / 8
		7150	79.31
	75.75		79.73
			42,85
79.03	79.03		7162
	7907	79.06	79.06
3,25cFm	3.25CFm	3.2	3.2
1.410	1.415		1.416
1.420	1.42.2		11,423
1.416	14110	1 4/3	1.420
1.425	1.425	1 427	1.428
27	27	27	27
5796	85795	85794	185793
26484	86483	86481	56490
	79.52 79.23 78.66 78.76 79.00 29.00 29.03 76.68 79.28 76.68 79.28 76.68 79.28 76.68 79.28 76.68 79.28 76.68 79.07 3.25cfm 1.425 1.425	79.52 79.56  79.23 79.24  78.86 78.66  78.78 78.86  79.00 79.00  79.00 79.00  79.32  78.91  78.68 78.69  79.28 79.28  76.73 75.75  78.65 79.03  79.03 79.03  79.07 79.07  3.25CFM 3.25CFM  1.410 1.415 1.425 1.425  77.27  27.27  27.27  27.27  27.27  27.27  27.27  27.27  27.27  27.27  27.27  27.27  27.27  27.27  27.27  27.27  27.27	79.52 79.56 79.52  79.23 79.24 79.23  28.86 78.66 78.37  78.78 78.86 78.97  79.00 79.00 78.09  29 79.32 79.32 79.31  78.68 78.69 78.68  79.28 79.31 79.68  79.28 79.31 79.68  79.28 79.31 79.68  79.28 79.28 79.31 79.68  79.03 78.68 78.69 79.73  78.65 79.65 79.73  78.65 79.65 79.73  79.07 79.07 79.06  3.25CFM 3.25CFM 3.2  1.410 1.415 1.422  1.425 1.425 1.423  1.425 1.425 1.427  27 27 27  57.96 85795 85796

#### CLRT

				Distigue
		RT DATA SHEET		
TIME/SAMPLE NO.	13001	1315/	1330/	13451
RTD # 1	78,42	79.42	78.92	78.92
RTD # 2	71.08	79.08	79.07	79.06
RTD # 3	70,29	71.30	79.24	79.28
RTD # 4	19.30	74.31	79.30	79.31
RTD # 5	79 12	78:85	79.10	79.10
RTD # 6	78.54	78.85	79.59	73.39
RTD # 7	79.42	79.41	79.44	1 79,43,000
RTD # 8 RTD # 9	79.10	79.10	79.10	79.09
RTD # 10	7954	1956	71.55	19.54
RTD # 11	79.22	79.24	79.24	79.22.
RTD # 12	75.56	78.86	78.85	78.05
RTD # 13	78.79	75.39	75.68	7847
RTD # 14	1 37.01	18.30	1800	101
RTD # 15	79.31	74.31	75.30	71.31
RTD # 16	75.91	78.92	78.91	70 90
RTD # 17	73.69	78/0	13.71	76 410
RTD # 18	7123	75.1.9	78.69	78.67
RTD # 19	75.74	13.75	78-75	75.75
RTD # 20	78.56	78.56	75.56	Trixis
RTD # 21 (SPARE)	11104	11162	1 79.01	74.61
RTD # 22 (SPARE)	79.c/p	79.06	79.05	79.05
ROTAMETER FLOW	3.2	3.2	3.2-	3.2
D. Pt. / 1	1.419	1.421	1.4 2%	
	1.424	1.426.	1.4.25	1.422
D. Pt. # 2 D. Pt. # 3	1-415	1.416	1.476	1.424
D. Pt. # 4	1.428	1.429	1.429	1.400
	27	27	27	27
Pressure # 1	55792	1 35742	1 55-791	185751
Pressure # 2 (SPARE)	156480	56479	36475	36472

	30.05		DATE 20 MAG	
DTAMETER FLOW 3		-	VERIFIED BY P	i Chywel
	IL	RT DATA SHEET		
TIME/SAMPLE NO.	14001	14151 74B	1430/	14451
RTD # 1	78.91	78.6318.90	78.90	78.90
RTD # 2	79.05	79.00人	79.05	74.04
R1'D # 3	79.29	79.16	79.27	74.47
RTD # 4	79.39	79.75	741.24	74.27
RTD # 5	74.10	79.08	71.64	14.04
RTD # 6	78.17	75.87	78.55	78 8/2
RTD # 7	79.41	79.42	79.41	74.40
RTD # 8	79.68	70.02	79 (8	74.07
RTD # 10	74.53	79.51	79.54	74.52
RTD # 10	74.12	79.21	7121	74.23
RTD # 12	78.54	75.54	78.5+	78.54
RTD # 13	78.74	The second line is the second line in the second line is the second li	7:57	78.87
RTD # 14	78.745	75.70	The second secon	78.80
RTD # 15	99.31	75 50	75.16	78.44
RTD # 16	78.90	75.89	78.91	78 41
RTD # 17	75.67	75.46	18.67	78.68
RTD # 18	79.33	7930	70.37	74 35
RTD # 19	75-14	75.73	78.73	79 14
RTD # 20	78-06	アン・ステ	78.81,	78.85
RTD # 21 (SPARE)	74.00	75.79	73.44	78.43
RTD # 22 (SPARE)	79.06	79.04	79.04	74.63
ROTAMETER FLOW	3.2	3.2.	3.2	3.2
D. Pt. # 1	1.423	1.422	white 4321.423	1.432-14.
D. Pt. # 2	1.429	1.430	. 4/2/12 1.432	44424143
D. Pt. # 3	1.426,	1.426	1-141-4-94 1.492	4451140
D. Pt. # 4	1,434	1.435	WAST -4 860 1.434	++++-11.44
	27	27	27	27
Pressure # 1	85788	85787	55756	45745
Pressure # 2 (SPARE)	1 66475	56.474	86473	52412

#### OPERATING PROCEDURE 13100.1, PAGE 53

# INTEGRATED LEAK RATE TEST

## APPENDIX D

AMBIENT TEMPERATURE	76	HOUR NO
BAROMETRIC PRESSURE	30.04	DATE 3/20/79
ROTAMETER FLOW	3.2	VERIFIED BY PB comitt

	ILR	T DATA SHEET		
TIME/SAMPLE NO.	15001	15151	15301	15451
RTD # 1	73.59	78.84	79.38	78.84
RTD # 2	79 04	74 04	74.03	74.04
KTD # 3	74.27	79.26	74.26	79 20
RTD # 4	7427	74 27	74.26	70 27
RTD # 5	74.08	79.08	74.08	74.08
RTD # 6	78.94	78.86	78.36	77 56
RTD # 7	79.41	79.41	74.40	74.40
RTD # 8	79.07	74 65	74.67	71.09
RTD # 9	79.55	74.55	79.55	70.5
RTD # 10	79.22	7422	79.22	79.21
RTD # 11	78.84	78.84	78 84	78.55
RTD # 12	78.87	78.87	78.57	75'57
RTD # 13	78.80	78 81	78 81	75.81
RTD # 14	78.44	78.44	78.48	78.44
RTD # 15	79.31	74.50	74.30	74.24
RTD # 16	78.91	78.90	78.89	79.90
RTD # 17	78.68	7869	78.69	78.68
RTD # 18	79.40	7939	79.34	79.41
RTD # 19	78.73	7874	75.74	78.75
RTD # 20	78 85	78.87	78 87	73' 38
RTD # 21 (SPARE)	15 93	75.43	13.43	78.43
RTD # 22 (SPARE)	79.04	74.04	74.04	7460
RETAMETER FLOW	3.2	3.2	3.2	3.2
D. Pt. 7 1	1,425	1.424	1.433	1,430
D. Pt. # 2	1.433	1.435	1.435	1.457
D. Pt. # 3	1.428	1.433	1.430	1.430
D. Pt. # 4	1,435	1.436	1.458	1.441

	27	27	27	27
Pressure # 1	\$5784	85782	85781	85180
Pressure # 2 (SPARE)	86474	86470	86464	56467

D. Pt.	Dew Point			
RHD - Re	lative Humidit	y Detecto	r,	
Pressure	,			
Terminal	Operator	or A.	111-26	

2340 150

AMBIENT TEMPERATURE	75°	HOUR NO.
BAROMETRIC PRESSURE	30.03	DATE 3/20/79
ROTAMETER FLOW	3,2	VERIFIED BY PE met

ILRT DATA SHEET				
TIME/SAMPLE NO.	1600,	1615,	16301	16451
RTD # 1	78.89	75.58	78.40	17887
RTD # 2	74.04	74.03	74.02	74.02
RTD # 3	74 24	79.26	74.20	7:1:26
RTD # 4	74.27	79.27	74.27	74.27
RTD # 5	1-1.07	7407	79.67	74.57
RTD # 6	78.84	1883	18.85	78.57
RTD # 7	74.40	79.41	74.34	74.54
RTD # 8	79.07	74.07	79.09	74.65
RTD # 9	74.55	74.53	74.55	74.52
RTD # 10	79.21	74.20	74.21	74.21
RTD # 11	ANT 78.85	78'54	78 54	75:54
RTD # 12	1 78.87	79.36	7480	75.50
RTD # 13	7881	78.81	78.81	78.57
RTD # 14	75.49	73.13	78.97	73 40
RTD # 15	7431	79.32	79.50	74.51
RTD # 16	7841	78.40	78 40	78.40
RTD # 17	75 64	78.69	7565	7364
RTD # 18	74.41	72.40	79.34	74.41
RTD # 19	73.74	78.75	78.74	78 75
RTD # 20	78.35	78.86	7830	78 87
RTD # 21 (SPARE)	78.47	75.47	78.41	78.40
RTD # 22 (SPARE)	79.02	74.02	79.02	79.02
POTAMETER FICE	3.2	3.2	3.2	3.2
). Pt. # 1	1.433	1.436	1.435	1.432
D. Pt. # 2	1.437	1.434	1.431	1.4.34
D. Pt. # 3	1 435	1.437	1.433	1.437
D. Pt. # 4	1.443	1.441	1.443	1.445
	27	. 27	27	27
Pressure # 1	85774	85778	85777	1 55774
			THE RESERVE AND ADDRESS OF THE PARTY OF THE	-

	27	27	27	27
Pressure # 1	85774	85778	85777	1 85776
Pressure # 2 (SPARE)	56466	96465	86464	56463

D. Pt Dew Point		
RHD - Relative Humi	dity Detector,	2712 1
Pressure,		2340 1
Terminal Operator	fol a war	

#### APPENDIX D

AMBIENT TEMPERATURE	73°	HOUR NO.
BAROMETRIC PRESSURE	30.02	DATE 3/20/79
ROTAMETER FLOW	3.2	VERIFIED BY PROMUM

	ILRT DATA SHEET					
TIME/SAMPLE NO.	17001	17151	17301	17451		
RTD # 1	78.87	78.57	78.87	78.86		
RTD # 2	79.63	79 62	79.02	7462		
RTD # 3	74.25	74.26	74.25	74.25		
RTD # 4	79.26	79.26	70 27	79.24		
RTD # 5	79.07	74.66	74.00	74.05		
RTD # 6	78.83	78 82	78.94	78.54		
RTD # 7	74.38	74.40	79.58	79.38		
RTD # 8	74.07	79.07	14.07	74.07		
RTD # 9	74.54	79.52	79.52	7453		
RTD # 10	14.21	74.21	79.21	79.21		
RTD # 11	7883	78.53	79.95	7833		
RTD # 12	7445	7880	78.55	73.35		
RTD # 13	75.80	79 81	78.75	7:779		
RTD # 14	7847	7847	78.47	78 95		
RTD # 15	74.00	74.30	74.30	701 30		
RTD # 16	78 59	78.90	78 96	73.34		
RTD # 17	78 64	7870	78 09	75.69		
RTD # 18	79 41	79 41	74.41	79.41		
RTD # 19	78.76	78 75	15.75	75 75		
RTD # 20	79 36	15 57	79.81	15.50		
RTD # 21 (SPARE)	78.44	78 16	18.45	Jiking 17		
RTD # 22 (SPARE)	74.01	79.01	74.61	74.01		
ROTAMETER FLOW	3.2	3.2	3.2	3.2		
D. Pt. # 1	1.433	1.441	1.440	1.430		
D. Pt. # 2	1.440	1.441	1.445	1.444		
D. Pt. # 3	1.435	1.439	1.443	1.4146		
D. Pt. # 4	1.446	1.447	1.446	1.449		
	27	27	27	27		
Prossure # 1	1 55775	1 66774		1 (620)		

Pressure # 1
Pressure # 2 (SPARE) 85774 85773 55771 56454

D.	Pt.	-	Dew	Point _		
RHI	- 0	Re:	lativ	e Humidi	ty Detector,	

Pressure,\_\_

Terminal Operator

2340 -152

AROMETRIC PRESSURE	30.02	기계시간 그 나가 나라가 하다	DATE 3/20	0/79
OTAMETER FLOW 3.3		-	VERIFIED BY	Demi
	ILI	RT DATA SHEET		
TIME/SAMPLE NO.	18001	100	,	1 ,
RTD # 1	73.86	78.86	(	(
RTD # 2	19.02	10,86 19.01/19.01		1
RTD # 3	19.25	74.24	)	1
RTD # 4	79.26	79 26		
TD # 5	74.05	74.05	\	1
RTD # 6	18.94	7854		(
TD # 7	74.38	79.37		
8 # DT	74.67	74.06	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	)
TD # 9	79.54	7452		
TD # 10	74.20	74.20		
TD # 11	78.83	7883		
TD # 12	75.85	19 84	Control A Lebes	
TD # 13	78.74	75 75		
TD # 14	78.45	78.45		`
TD # 16	79.30	74.30		1
	78 88	78.90		
TD # 17	78.68	7867		,
TD # 19	79 40	79.40		
TD # 20	75 86	79 95		
TD # 21 (SPARE)	78.94	78 94		
TTD # 22 (SPARE)	79.00	79.00		
		-		
Pt. # 1	1.440	1.442.		
Pt. # 2 Pt. # 3	1.446	1.445		
	1.442	1.241		
). Pt. # 4	1.450	1.454		
Pressure # 1	95770	85769		1
ressure # 2 (SPARE)	56458	84457		
RND - Relative Humidi	ty Detector,	1	2.	940 153

MBIENT TEMPERATURE			HOUR NO. /-	
AROMETRIC PRESSURE			DATE 3/2	0/79
OTAMETER FLOW			VERIFIED BY	Demit!
	ILRT	DATA SHEET		
TIME/SAMPLE NO.	11852	1 1930	12000	13030
RTD # 1	1	1 1/30	,,,,,	77.30
RTD # 2				-
RTD # 3				-
RTD ∅ 4				
RTD # 5				
RTD # 6				
RTD # 7				
RTD # 8				
RTD # 9				
RTD # 10				
RTD # 11	HARLES THE STATE OF			
RTD # 12		The transfer of the second		
RTD # 13 RTD # 14	-			
RTD # 15	-			
RTD # 16				
RTD # 17				
RTD # 18				
RTD # 19				-
RTD # 20	<del> </del>			-
RTD # 21 (SPARE)	-			-
RTD # 22 (SPARE)				-
PSIA	42 0			
D. Pt. # 1				
). Pt. # 2				
D. Pt. 1 3				
D. Pt. # 4			-	
Processo A 1	100000	0020		
Pressure # 1	65768	82820	-CC+ 70	78690
Pressure # 2 (SPARE)	186455	23550	81507	79300
D. Pt Dew Point				100 151
Pressure, PSIA 4	v Detector.		4.	340 154

Blow dawn

A	P	P	E	N	D	I	X	D
---	---	---	---	---	---	---	---	---

		AFTERNIA D					
MBIENT TEMPERATURE	HOUR NO.						
AROMETRIC PRESSURE			DATE 3/	20/79			
OTAMETED IT OU			VERIFIED BY 1	0.)			
OTAMETER FLOW			VERIFIED BY	100mc			
	I	LRT DATA SHEET	T DATA SHEET				
TIME/SAMPLE NO.	21001	21301	13001	2234			
RTD # 1	,						
RTD # 2							
RTD # 3							
RTD # 4							
RTD # 5							
RTD # 6							
RTD # 7				1			
RTD # 8				K			
RTD # 9							
RTD # 10				19			
RTD # 11		KIN KIND IN A HEL					
RTD # 12							
RTD # 13							
RTD # 14 RTD # 15							
RTD # 16							
RTD # 17 RTD # 18							
RTD # 19							
RTD # 20							
RTD # 21 (SPARE)							
RTD # 22 (SPARE)							
IBSCLUTE PRESS	36.7	2/1/					
	36.1	34.6	32.7	31.9			
D. Pt. # 1							
D. Pt. # 2 D. Pt. # 3							
D. Pt. # 4							
D	1 = 77 - 27	<b>A</b> 5.7771	1 777	1 30-5			
Pressure # 1	74610	70410	66490	62730			
Pressure # 2 (SPARE)	175/30	170880	166910.	63,00			
D. Pt Dew Point _			_ 2340	155			
RHD - Relative Humidi	ity Detector.						
Pressure, 36.7							
riessure,	-31/1	***************************************					
erminal Operator							

OPERATING.	PROCEDU	RE 1	3100.	1,	PAGE	53
INT	CRATED	LEAR	PATE	TI	ST	

Blow down

AMBIENT TEMPERATURE	HOUR NO.					
BAROMETRIC PRESSURE	DATE 3/20- 3/21/7					
ROTAMETER FLOW			VERIFIED BY			
		T DATA SHEET		T :		
TIME/SAMPLE NO.	23:01	23301	0001	00301		
RTD # 1	,					
RTD # 2						
RTD # 3						
RTD # 4						
RTD # 5						
RTD # 6	-					
RTD # 7						
RTD # 8 RTD # 9	-					
RTD # 10						
RTD # 11						
RTD # 12				-		
RTD # 13						
RTD # 14						
RTD # 15		<b></b>				
RTD # 16						
RTD # 17				-		
RTD # 18			1	1		
RTD # 19						
RTD # 20						
RTD # 21 (SPARE)						
RTD # 22 (SPARE)						
PSIA	29.15	27.50	26.12	24.65		
D. Pt. # 1						
D. Pt. # 2						
D. Pt. # 3	THE STATE OF THE S					
D. Pt. # 4						
P						
Pressure # 1	59180	55680	52755	19960		
Pressure # 2 (SPARE)	159480	55980	52990	50062		
D. Pt Dew Point				15/		
RHD - Relative Humidit	Trends and the second		2340	100		
Pressure, 29.15	HZIA					
'erminal Operator						

AP	D	27	×	173	*	v	n
MI	r	60	P	127	T	Λ	U

2/00 1	O/30/	02001	02301
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	The Part of the late of the la		701
Marin Service			
		Community of the first	
	P. P. P. B. B. B. B.		
	A Light Control of the Control		
		A Contract of the Contract of	
		A Label Constitution	
23.32	27.17	2120	10 9
47 -4	1 02.12	21.00	17.1
			-
47175	44690	1 42408	4032
47340	94820	4253	+6 to2
	47340	47175 44690	47175 44690 42408 47340 44820 4253

MBIENT TEMPERATURE	\		HOUR NO			
AROMETRIC PRESSURE			DATE 3/2	1/71		
			701/1			
OTAMETER FLOW			VERIFIED BY			
	ILI	RT DATA SHEET				
TIME/SAMPLE NO.	03001	03301	04001	04301		
RTD # 1						
RTD # 2						
RTD # 3						
RTD # 4						
RTD # 5						
RTD # 6						
RTD # 7						
RTD # 8						
RTD # 9						
RTD # 10			n de como de la composición de			
RTD # 11						
RTD # 12			The second second			
RTD # 13						
RTD # 14						
RTD # 15						
RTD # 16						
RTD # 17		100000 00000				
RTD # 18						
RTD # 19						
RTD # 20						
RTD # 21 (SPARE)						
RTD # 22 (SPARE)						
PSIA	18.98	13.18	17.45.47	16.30		
D. Pt. 6 1				DOMONE CONTRACTOR		
D. Pt. # 2						
D. Pt. # 3						
D. Pt. # 4		!				
Pressure # 1	38448	36764	35267	33961		
Pressure # 2 (SPARE)	33506	36800	35232	32761		
D. Pt Dew Point				72.3890		
RHD - Relative Humidit	y Detector,					
Pressure,			234	0 158		
'orminal Operator				130		
erminal Operator						

AMBIENT TEMPERATURE			HOUR NO.		
BAROMETRIC PRESSURE			DATE 3	DATE 3-21-79	
ROTAMETER FLOW		VERIFIED BY			
	ILE	ILRT DATA SHEET			
TIME/SAMPLE NO.	0500 1	10530 /	10000	06301	
RTD # 1	,				
RTD # 2	1				
RTD # 3					
RTD # 4					
RTD # 5					
RTD # 6					
RTD # 7					
RTD # 8					
RTD # 9					
RTD # 10					
RTD # 11					
RTD # 12					
RTD # 13					
RTD # 14					
RTD # 15					
RTD # 16					
RTD # 17					
RTD # 18					
RTD # 19					
RTD # 20 RTD # 21 (SPARE)	-				
	1 21	-			
PSIA	16.24	15,75	15.38	15.10	
D. Pt. # 1					
D. Pt. # 2					
D. Pt. # 3					
D. Pt. # 4					
Process A :	1 3 36 46	1000			
Pressure # 1	32840	31905.	31152	30575	
Pressure # 2 (SPARE)	1 32930	1 3/883.	131124	30539	
D. Pt Dew Point			- Aug Ten	p-73.32@ 05	
RHD - Relative Humidit	y Detector,				
Pressure,				2340 159	
erminal Operator					

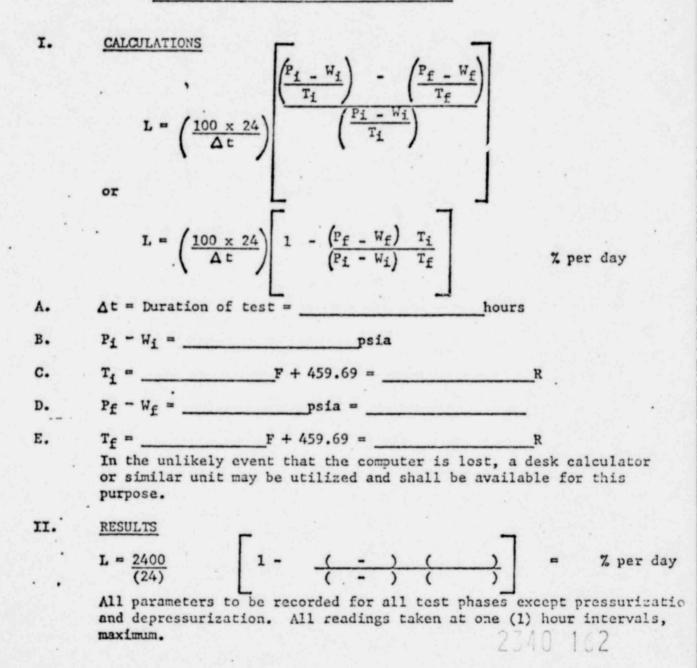
	IL	RT DATA SHEET		
TIME/SAMPLE NO.	0700 1	07301	- /	/
RTD # 1		75.18		
RTD # 2 RTD # 3		25.41		
RTD # 4	-	75.71		
RTD # 4		75.81		
RTD # 6		75:72		
RTD # 7		74,95		
RTD # 8	<del></del>	75.49		
RTD # 9		75.37		
FTD # 10	1			
RTD # 11		76.53		
RTD # 12		75.04		
RTD # 13		75.37		
RTD # 14		75.47		
RTD # 15		76.69		
RTD # 16		75.65		
RTD # 17		75.47		
RTD # 18		76.51		
RTD # 19		75.34	A LEWIS CO. LANCE	
RTD # 20	I Live a live re-	76.08		
RTD # 21 (SPARE)		9537 15.	39,50	
RTD # 22 (SPARE)		7.5.40		
PSIA	14.59	14.75		
D. Pt. # 1		1 . 378		
D. Pt. # 2		. 375		
D. Pt. # 3		1454		
D. Pt. # 4		, 468		
Pressure # 1	30166	29890		
Pressure # 2 (SPARE)	30124	29541		

#### APPENDIX E

Data Sheet for Manual Calculations

2340 161

# FOR INFORMATION ONLY INTEGRATED LEAK RATE TEST DATA SHEET



Verified by:

Date:

#### APPENDIX F

I & C Instrument List

2340 163

R. Cook Re Jose M. AMEZAGA

#### CONTAINMENT EQUIPMENT CHECK LIST

Fischer Porter/Hagan Transmitters - On all below listed transmitters, insure cover o-rings are installed and in good repair. Tighten cover hand-tight.

ransmitter #	Function	Performed By	Restored-QC
T-3-138	Excess Ltdn Line Press	3.15.79 Dung	2-26-19 CL
T-3-436	RC Flow Loop C	1 Sona	1 60
T-3-435	RC Flow Loop C	Due	l ec
T-3-932	Safety Inj. Line Flow Loop A	ana	ec.
T-3-933	Safety Inj. Line Flow Loop B	1 June	ec.
T-3-434	RC Flow Loop C	June 1	le le
T-3-424	RC Flow Loop B	2 ma	Re
T-3-425	RC Flow Loop B	me	ec.
T-3-426	RC Flow Loop B	2ma	ec
T-3-402	RCS Wide Range Press.	11 Sour	20
T-3-403	RCS N.R. Press.	11 June	RC
T-3-405	RCS W.R. Press.	) Dua	ec
T-3-416	RC Flow Loop A	1 Dua	· cc
T-3-415	RC Flow Loop A	1 ma	ec
T-3-414	RC Flow Loop A	ma	RC
T-3-1004	RCS Drain Tank Press.	11 Ema	Ec
T-3-155	RCP "B" Seal Delta P	11 France	EC
T-3-128	RCP "B" Thermal Barrier Delta P	1 Tour	RC
T-3-484	Stm Gen "B" N.R. Level Ch. 1	ma	
T-3-485	Stm Gen "B" N.R. Level Ch. 2	Burn	RC
T-3-486	Stm Gen "B" N.R. Level Ch. 3	11 one	ec.
T-3-487	Stm Gen "B" W.R. Level	1 Enua	20
T-3-455	Przr Press. Prot. Ch. I	11 &	rc ec
T-3-456	Przr Press. Prot. Ch. II	11. Dun	RC
T-3-457			ec.
T-3-445	Przr Press. Prot. Ch. III Przr Press. Control	Dur	80
T-3-462		22112	
T-3-444	Przr Level Control	mac	RC
T-3-458B	Przr Press. Control	2000	80
T-3-923	Przr Press. Cal.	Die	
	Acc. Tank A Press.	ipuc	ICC.
T-3-131 T-3-156	RCP C Thermal Barrier	pria	RC
	RCP A Seal Delta P	gma	RC
T-3-472	PRT Pressure	1 Some	. RC
T-3-474	Stm Gen A N.R. Level Ch. 1	But	EC.
T-3-475	Stm Gen A N.R. Level Ch. 2	1 men	EC
T-3-476	Stm Gen A N.R. Level Ch. 3	I ma	J.C.
T-3-477	Stm Gen A N.R. Level	22.10	ac ac
T-3-921	Acc A Press.	1 . Jone	I EC
T-3-925	Acc B Press.	1 mil	EC
T-3-927	Acc B Press.	1	EC
T-3-929	Acc C Press.	ma	rcc
T-3-494	Stm Gen C N.R. Level Ch. I	Gua	ec.
T-3-495	Stm Gen C N.R. Level Ch. II	1 grun	RC
T-3-496	Stm Gen C N.R. Level	1 come	RC
T-3-497	Stm Gen C W.R. Level	1 June	DC.
T-3-931	Acc C Press	Light	2.0
T-3-154	RCP 3C Seal Water Delta P	1000	14
T-3-125	RCP Loop C Shaft Seal Delta P	1 your	êc.
T-3-494	Stm Gen C Stm Flow Ch. I	1. When	V. Re
T-3-495			

Tosé M. Buezasa José M. Buezasa Druce

Transmitter #	Function	Performed By Restored-QC
FT-3-485	Stm Gen B Stm Flow Ch. II	Dana 3-26-71 ICC
FT-3-484	Stm Gen B Stm Flow Ch. I	gone cc
FT-3-474	Stm Gen A Stm Flow Ch. I	gua ec
'T-3-475	Stm Gen A Stm Flow Ch. II	Dua V CC

2. Barton Le 1 Transmitters - On all below listed transmitters, insure cover orings are installed and in good repair. Tighten covers.

Transmitter #	Function	Performed B	
LT-3-459	Press. Level Prot. Ch. I	Jun	2 10 11.046
LT-3-460	Press. Level Prot. Ch. II	Dur	1 72
LT-3-461	Press. Level Prot. Ch. III	Due	1 RC

3. Barton Flow Indicating Switches - Loosen the covers on all of the below listed equipment.

Transmitter #	Function	Performed By Res	stored-QC
FIC-3-490	RTD Bypass Flow A	Enia 3-2019	EC
FIC-3-491	RTD Bypass Flow B	Qua	ec
FIC-3-492	RTD Bypass Flow C	Due 1	CC

4. Brooks Flow Indicator/Transmitters - Loosen the covers on all of the below listed equipment.

Transmitter #	Function	Performed By Restored-00
FT-3-156A	RCP A Seal Leak Off (Hi)	3-15-14 Dece 6-20-19 EC
FT-3-156B	RCP A Seal Leak Off (Lo)	Dua CC
FT-3-155A	RCP B Seal Leak Off (Hi)	Dia CC
FT-3-155B	RCP B Seal Leak Off (Lo)	anne EC
FT-3-154A	RCP C Seal Leak Off (Hi)	2
FT-3-154B	RCP C Seal Leak Off (Lo)	put EC
FIC-3-154	Low Flow RCP C Seal Water	ina cc
FIC-3-635	RCP C Low Flow CCW	met La
FIC-3-629	RCP A Low Flow CCW	1 C
FIC-3-632	RCP B Low Flow CCW	Dut- EC
FIC-3-155	Low Flow RCP B Seal Water	Dut EC
FIC-3-156	Low Flow RCP A Seal Water	y me v ec

5. Pressurizer Instrument Cabinet Heaters - De-energize heaters by performing the following.

Transmitter #	Function	Performed By	Restored-QC
TC-3-440A	B/S switch to test (Rack 2)	3-15-79 Jan	3-26-79 RC
TC-3-44 LA	B/S switch to test (Rack 12)	3.15.19 gove	RC
TC-3-442A	B/S switch to test (Rack 15)	3-15-79 Dac	re
TC-3-443A	Remove output fuse (Rack 7)	3-15-79 Just	r ce

# OPERATING PROCEDURE 13100.1, PAGE 58

INTEGRATED LEAK RATE TEST

R. Cook RC JOSE M. AMERICA

Remove the following equipment from the Containment.

Equipment	Performed By	Restored-OC
Flux mapper Gas Bottles Containment Sump Floats M SEE OTSC # 465	3.15.74 Dec	3-26-17 RC
ARMS G.M. Tubes	3.15-79 Due	2-26-19 RC
Dillion Load meters (manipulator & polar crane)	3-15-29 Dea	3-26-79 KC

7. Install the following jumpers, with Temporary jumper tags.

Rack	Terminals	Performed By	Restored-QC
3Q R 51	Pl to 5	3.15.79 Qua	13-26-79 RC
3Q R 51	33 to 35	1 Dea	1 66
3Q R 51	23 to 25	Dun	80
3Q R 50	9 to 11	ma	86
3Q R 50	39 to 41	- One	I Re
3Q R 50	373 to 377	1 Done	1 80

Conduct inspection of all levels in Containment and ensure

	Performed By	Restored-QC
All Local Gauges (Pressure and Temp) faces are removed	3.5.14 Due	13-26-79 rcc
All Local flowrators have at least one glass face removed	3-15-24 Due	3-26-79 RC

System is operable M OTSC # 465 Menduta 3-15-79

NOTE: Pages 56, 57, 58 md 59 were filled out on or before 3/15/79 Using the 3/1/79 version of the procedure. On 3/15/79 the procedure was revised to reflect the use of demonstration instead & relative humiting betretors. This change precessitation renumbering of poss 47-69 of the precover. The only Change on good 56-59 was the good number & bate.

#### AIR OPERATED CONTAINMENT VALVE FAILURE MODE

VALVE	FAILURE MODE	
CV-3-200 A	3-15-79 Closed	
CV-3-200 B	Closed Dur	
CV-3-200 C	Closed pue	
CV-3-307	Closed Dux	
CV-3-310 A	Open &	
CV-3-310 B	Open Sur	
CV-3-311	Closed Sur	
CV-3-387	Closed gran	
CV-3-460	Open Dro-	
CV-3-455 A	Closed Sma	
CV-3-456 me	Closed Dan	SEE OTSC 465
CV-3-456 A DELE		SEE OTSC 465
CV-3-455 *Bom	Closed office	3EE 0/30 403
CV-3-455 C	Closed Dut	SEE OTSC 465
64 3 455 Dom OE	ETE Glosed M. (DELETE)	SEE 013C 403
CV-3-519 A	Closed Bran	
GV 3 522 ME DEL		3EE 015C 465
CV-3-519 B	Closed Die	
CV-3-522 A	Closed Disc	
CV-3-522 B	Closed Z	
CV-3-522 C	Closed Olic	
CV-3-523	Closed STAL	
CV-3-549	Closed Der	
CV-3-544 CV-3-389	Open Or	
CV-3-853 A	Divert Dr	
	Closed Tur	
CV-3-851 A CV-3-852 A	Closed Que	
CV-3-850 A	Closed Open	
CV-3-850 B	Closed Dist	
CV-3-853 B	Closed Due	
CV-3-851 B	Closed Drud	
CV-3-852 B	Closed Duck	
CV-3-850 C	Closed grid-	
CV-3-850 D	Closed June	
CV-3-850 E	Closed Die	
CV-3-850 F	Closed Duc	
CV-3-852 C	Closed III	
CV-3-853 C	Closed Are	
CV-3-851 C	Closed De-	
CV-3-936	Closed Are	
CV-3-951	Closed Om	2340 107
CV-3-953	Closed Duc	2090 10/
CV-3-955 B	Closed Duc-	
CV-3-955 C	Closed O	
CV-3-955 D	Closed Dea	
CV-3-955 E	Closed one	
LCV-3-1003 A	Closed 2	
LCV-3-1003 B	Closed We	

APPENDIX G

Breaker List

2340 168

# ELECTRICAL EQUIPMENT INSIDE UNIT #3 CONTAINMENT

## Canister No. T3C21

Containment Cooling Fan A	
MOV-3-865A Accumulator A Discharge to a Cold Leg	<b>3</b> B0518
RCP #3A 011 Lift Pump	380532
Containment Sump Pump 3A	3B0554
	360667
Canister No. T2C22	
Confirment Cooling Fan B	보니 레이지 보고 없었다면
Control Rod Drive Mechanisms Cooler 3A	3B0642
MOV-3-750 Loop C Hot Leg to RHR	3B0629
MOV-3-744B RHR Return to Cold Legs	3B0615
	380613
MOV-3-866B Delayed HH SI to Loop B Hot Leg	3B0621
MOV-3-865B Accumulator B Discharge to B Cold Leg	3B0631
MOV-3-535 Pressurizer Power Relief Isolation	
Reactor Coolant Pump 3B Oil Lift Pump	3B0605
Reactor Coolant Drain Tank Pump 3A Thermal Cut-Out	380679
	3B0662
Canister No. T3C13	
Containment Cooling Fan 3D	
	B0829
	2340 109
Canister No. T3C23	
Containment Cooling Fan 3C	
Control Rod Drive Mechani m 2 1 2 1 83B	3B0742
Reactor Coolant Pump 3C 011 Lift Pump	380727
	330762
NOV-3-865C Accumulator 3C Discharge to Loop C Cold Leg	3807€
MOV-3-536 Pressurizer Power Relief Valve Isolation	380713

#### OPERATING PROCEDURE 13100.1, PAGE 62 INTEGRATED LEAK RATE TEST

#### ELECTRICAL EQUIPMENT INSIDE UNIT #3 CONTAINMENT

#### Canister No. T3C21

	Containment Cooling Fan A	380518
	MOV-3-865A Accumulator A Discharge to a Cold Leg	380532
	RCP #3A Oil Lift Pump	3B0554
	Containment Sump Pump 3A	3B0667
,	Canister No. T3C22	
	Containment Cooling Fan B	3B0642
	Control Rod Drive Mechanisms Cooler 3A	3B0629
	MOV-3-750 Loop C Hot Leg to RHR	380615
	MOV-3-744B RHR Return to Cold Legs	3B0613
	MOV-3-866B Delayed HH SI to Loop B Hot Leg	3B0621
	MOV-3-865B Accumulator B Discharge to B Cold Leg	3B0631
	MOV-3-535 Pressurizer Power Relief Isolation	380600
	Reactor Coolant Pump 3B Oil Lift Pump	3B0679
	Reactor Coolant Drain Tank Pump 3A Thermal Cut-Out	3В0662
	Canister No. T3C13	
	Containment Cooling Fan 3D	B0829
		2340 170
	Canister No. T3C23	
	Containment Cooling Fan 3C	3B0742
	Control Rod Drive Mechanism Cooler Fan #3B	380727
	Reactor Coolant Pump 3C Oil Lift Pump	3B0762
	MOV-3-865C Accumulator scharge to Loop C Cold Leg	380733
	MOV-3-536 Pressurizer Power Relief Valve Isolation	380713

Canister No. T3C23 (con	ntinued)
MOV-3-751 Loop C Hot Leg to RHR Pump Suction	3B0731
MOV-3-744A RHR Return to Cold Legs	3B0722
MOV-3-866A Delayed High Head SI to Loop A Hot Leg	3B0732
Reactor Coolant Drain Tank Pump 3B Thermal Cut-Out	3B0787
Canister No. T3P1	<u>11</u>
Emergency Containment Filter Fan 3A	3B0611
Normal Containment Cooler Fan 3B	3B0642
Control Rod Drive Mechanisms Cooling Fan 3A	3B0629
Lighting Transformer 36	3B0658
Containment Elevator #3	3B0619
Canister No. T3P2	1
Reactor Crane 3	3B0104
Normal Contain .t Cooler Fan 3A	3B0518
Lighting Fa el D.C. Feed	3Y0605
Canister No. T3P3	2
480 Volt Receptacle #17 and #17A	380653
Reactor Coolant Drain Tank Pump 3A	380662

Canister No. T3P33

480 Volt Misc Containment Distribution Panel (3P11)

2340 171

3B0673

Canister No. T3P12	
Emergency Containment Filter Fan 3C	3B0719
Normal Containment Cooler Fan 3C	380742
Control Rod Drive Mcchanism Cooler Fan 3B	380727
Lighting Transformer #37 3X07 Containment Entrance	3B0768
Canister No. T3P22	
Emergency Containment Filter Fan 3B	в0806
Normal Containment Cooler Fan 3D	B0829
Canister No. T3P35	
480 Volt Misc Containment Distribution Panel #1 (3P10)	3B0771
Reactor Coolant Drain Tank Pump 3B	3B0787
Canister No. T3P41	
Pressurizer Heaters 2, 23, and 50	381101
Pressurizer Heaters 26, 53, and 54	3B1103
Pressurizer Heaters 7, 29, and 57	381105
Pressurizer Heaters 10, 32, and 60	3B1107
Pressurizer Heaters 12, 35, and 64	3B1102
Pressurizer Heaters 38, 67, and 68	3B1104
Pressurizer Heaters 17, 41, and 71	3B1106

Pressurizer Heaters 19, 44, and 75

Emergency Containment Cooler Fan 3A

3B1108

3B0650

#### Canister No. T3P51

Emergency Containment Cooler Fan 3B

Misc AC Instruments	3P0610
Space Heaters	<b>3</b> Y0439
Space Heaters	3Y0521
MOV-3-865B Accumulator B Discharge to B Cold Leg	380631
Reactor Coolant Pump 3B Oil Lift Pump	380679
MOV-3-866B Delayed HH SI to Loop B Hot Leg	-3B0621
MOV-3-535 Pressurizer Power Relief Isolation	3B0606
Containment Sump Pump 3A	3B0667
MOV-3-744B RHR Return to Cold Legs	3B0613
MOV-3-750 Loop C Hot Leg to RHR (IMB)	3B0615
Canister No. T3P42	
Pressurizer Heaters 21, 47, and 48	3B1201
Pressurizer Heaters 3, 24, and 51	3B1203
Pressurizer Heaters 5, 27, and 55	3B1205
Pressurizer Heaters 8, 30, and 58	3B1207
Pressurizer Heaters 33, 61, and 62	3B1209
Pressurizer Heaters 13, 36, and 65	3B1202
Pressurizer Heaters 15, 39, and 69	3B1204
Pressurizer Heaters 18, 42, and 72	3B1206
Pressurizer Heaters 20, 45, and 76	381208

B0820

## Canister No. T3P53

4	일을 보고 있다면 하는 다른 보다 이번 사람이 보니 아무지 않는데 <del>하는데 보고 있는데 하는데 하는데 하는데 하는데 하는데 하는데 하는데 하는데 하는데 하</del>	
	Space Heaters	3Y0467
	Space Heaters	3Y0501
	Space Heaters	3¥0502
	Space Heaters	3Y0504
	Space Heaters	3Y0503
	Space Heaters	3Y0505
	Space Heaters	3Y0506
	Space Heaters	3Y0507
	Space Heaters	<b>3Y0</b> 508
	Misc AC Instruments	3P0814
	MOV-3-865C Accumulator 3C Discharge to Loop C Cold Leg	3B0733
	Reactor Coolant Pump 3C 0il Lift Pump	3B0762
	MOV-3-866A Delayed high Head SI to Loop A Hot Leg	3B0732
	MOV-3-536 Pressurizer Power Relief Valve Isolation	3B0713
	MOV-3-744A RHR Return to Cold Legs	3B0722
	MOV-3-751 Loop C Hot Leg to RHR Pump Suction	3B0731
	Containment Sump Pump #3B	380778
	Fuel Tilting Winch Panel 3B (IC)	380763
	Canister No. T3P43	174
	Pressurizer Heaters 1, 22, and 49	
	Pressurizer Heaters 4, 25, and 52	3B1301
	Pressurizer Heaters 6, 28, and 56	3B1303
	Pressurizer Heaters 9, 31, and 59	3B1305
	Pressurizer Heaters 11, 34, and 63	3B1307
)	Pressurizer Heaters 14, 37, and 66	3B1309
	and ou	3B1302

Canister No. T3P43	(continued)
--------------------	-------------

A	(continued)	
	Pressurizer Heaters 16, 40, and 70	3B1304
	Pressurizer Heaters 43, 73, and 74	3B1306
	Pressurizer Heaters 46, 77, and 78	3B1308
	Emergency Containment Cooler Fan 3C	3B0729
	Canister No. T3P52	
	Misc AC Instruments	3P0917
	Space Heaters	<b>3</b> Y0439
	Space Heaters	3Y0521
	Misc A.C. Instruments	3P0714
	MOV-3-865A Accumulator A Discharge to a Cold Leg	<b>3</b> B0532
	RCP #3A Oil Lift Pump	<b>3</b> B0554
	Space Heaters	3Y0403
	Space Heaters	3Y0404
	Space Heaters	3Y0410
	Canister No. 5KV "A" RCP	
	Reactor Coolant Pump A	152-3AA01
	Canister No. 5KV "B" RCP	
	Reactor Coolant Pump B	152-3AB01
	Canister No. 5KV "C" RCP	
	Reactor Coolant Pump C	152-3AB06
		2343 175

#### MISC

RCP 3A Heater Breaker

3AA01

RCP 3B Heater Breaker

3AB01

RCP 3C Heater Breaker

3AB06

Canister No. T3C12

Fuel Tilting Wench

3FTS/3C08-T3C12/1

Fuel Tilting Wench

3FTS/3C08-T3C12/2

Code Call & Fire Alarm W6

Canister Wire ref. 26

Spare

Canister Wire ref. 6 & 8

Canister No. T3C31

Spare

Canister Wire ref. 7 & 12

Public Address Communication System

Canister Wire ref. 11

PAX Telephone W3

Canister Wire ref. 9

Canister No. T3C41

Spare

Canister Wire ref. 12

Telephone Circuit for Maintenance W7

Canister Wire ref. 11

Public Address Communication System

Canister Wire ref. 7

Canister No. T3C11

Spare

Canister Wire ref. 5, 6, 8,

18 & 22

Remote Control LP 37

Canister Wire ref. 2

Canister No. T3P31

Spare

Canister Wire ref. 25 & 26

2340 176