

1370-3

Combustion Engineering, Inc.	
Nuclear Power Systems	
QUALITY RECORD	
1/12/76	LSF
Date	Initials

TR-75-74

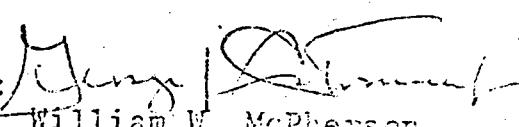
SEISMIC ANALYSIS
OF A
SHUTDOWN HEAT EXCHANGER, TYPE CEU
FOR THE
SOUTHERN CALIFORNIA EDISON COMPANY'S
SAN ONOFRE UNITS NO. 2 AND NO. 3 PLANTS
Revision #1
Prepared For:

Engineers and Fabricators, Company
P.O. Box 7395
Houston, Texas 77008

NUS Technical Report No. 1514

10 February, 1976

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William W. McPherson
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Engineers and Fabricators, Company
Purchase Order No. 64087-D

NUS Corporation
400 Totten Pond Road
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i 8103060 557

RECORD OF REVISIONS

Revision No.	Date	Page	Description	Author
1	2/10/76	Title Page Record of Revision Page A-1 - A-3	Addition of Addendum #1 - Foundation Loads	J. Wawzeniak

ADDENDUM #1
FOUNDATION LOADS

A-1

Rev. #1
2/10/76

SUMMARY OF SUPPORT AND SEISMIC LUG

REACTIONS

THE FOLLOWING IS A SUMMARY OF THE FOUNDATION LOADS AT THE SEISMIC LUGS AND SUPPORTS AS EXTRACTED FROM COMBINE OUTPUT, APPENDIX B. THE LOADS HAVE BEEN CONVERTED INTO THE GLOBAL COORDINATE SYSTEM FIGURE 1 PAGE 6.1-2

LOADING - EQ1 + DW + NOZZLE LOADS

● NODE FX1 FX2 FX3 MX1 MX2 MX3

SUPPORTS

13	1693	-7979	32224	-127330	-8552	4628
19	-959	7946	34587	204290	4826	9154
20	-7598	-1642	35268	-8283	203090	4882
25	7631	1010	31543	5095	-126080	8901

LUGS

32	-15635	-1267	0	-244	-76	-8152
34	1283	-14891	0	158	-116	-9568
40	-38391	-3336	0	-360	-179	-25432
42	7213	-41878	0	234	-275	-17038

DATE 6/1/70

SUBJECT.....

SHEET NO. OF

DATE 7/1/70

JOB NO.

EE-60-2

LOADING - EQ2 + DW + NOZZLE LOADS

NODE FX1 FX2 FX3 MX1 MX2 MX3

SUPPORTS

NODE	FX1	FX2	FX3	MX1	MX2	MX3
13	128	-7688	38144	-205640	-637	7597
19	-1430	7721	31459	164450	7190	747
20	-5120	-447	30099	-2192	150200	9503
25	5070	1816	36784	9119	-191390	1698

LUGS

NODE	FX1	FX2	FX3	MX1	MX2	MX3
31	-12133	-1094	0	-197	-43	-6149
33	1332	-11412	0	128	-67	-8098
39	-33164	-3250	0	-362	-178	-23005
41	7030	-36847	0	235	-274	-13928

TR-75-74

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REVIEWED BY: RJS 11-20-75
APPROVED BY: DPK 11-24-75

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Section 1.0
INTRODUCTION

The Engineering Mechanics Department of NUS Corporation received the Purchase Order No. 64087-D from Engineers and Fabricators, Co. to perform the seismic analysis of a Shutdown Heat Exchanger to be installed at the Southern California Edison Company's San Onofre Units No. 2 and No. 3 Plants. The above analysis is included herein and conforms to the requirements of the governing Combustion Engineering Specification, Reference 1.

Section 2.0

RESULTS AND CONCLUSIONS

This section presents a summary of the heat exchanger results as calculated in this report. The results include the effects of deadweight, seismic, nozzle and pressure loading on the supports and seismic lugs, support and seismic lug welds, support and seismic lug bolts, and local shell junctions. The analysis performed consisted of a worst case loading combination. When applicable, an upper bound for stress value was calculated.

The calculated natural frequency for the Shutdown Heat Exchanger was found to be:

48.5 Hz

The calculation of this natural frequency may be found in Section 8, beginning on Page 8.1-1. Flow induced vibrations are not a problem.

From a review of the summary of stress results, no failure areas were observed and, therefore, the heat exchanger meets the seismic and nozzle load requirements of the Combustion Engineering Specification, Reference 1.

2.0.2

<u>Location</u>	<u>Type of Stress</u>	<u>Loading</u>	<u>Maximum Stress Value</u>	<u>Allowable Stress Value</u>
Nozzles N ₁ ,N ₂	Primary Local Membrane	Nozzle Loads	9136 7220	28,000 (1) 26,730
Vessel Nozzle				
Tubeside	Primary Membrane	Seismic + Deadweight + Nozzle Loads + Pressure	12156 13043 13043	19,250 (2) 19,250 19,250
Plenum Outlet Inlet				
Shellside	Primary Membrane			
Inlet Plenum Inlet Nozzle Outlet Plenum Outlet Nozzle			6756 4651 6729 4987	19,250 (2) 16,500 19,250 16,500
Shell	Primary Membrane		6832	19,250 (2)
Support/Vessel Seismic Lug/Vessel	Primary Local Membrane		5630 5037	28,800 (1) 28,800
Support/Vessel Seismic Lug/Vessel	Primary + Secondary		7856 38078	52,500 (5) 52,500
Support	General Membrane General Membrane Plus Bending		1439 4639	17,500 (3) 26,250 (4)
Support Weld	Shear In Fillet Weld		2142	21,000 (7)
Support Bolts	Tension In Bolt		15848	40,000 (6)

<u>Location</u>	<u>Type of Stress</u>	<u>Loading</u>	<u>Maximum Stress Value</u>	<u>Allowable Stress Value</u>
Seismic Lug	General Membrane General Membrane Plus Bending	Seismic + Deadweight + Nozzle Loads + Pressure	3363 12546	17,500 (3) 26,250 (4)
Seismic Lug Weld	Shear In Fillet Weld		6784	21,000 (7)
Seismic Lug Bolts	Shear In Bolt		13911	15,390 (6) ^{qc}

2-0-5

MAXIMUM STRESS VALUES

NOTES:

- 1) Primary Local Membrane Stresses are compared to 1.65 S, Reference 1.
- 2) Primary Membrane Stresses are compared to 1.1 S, Reference 1.
- 3) General Membrane Stress are compared to 1.0 S, Reference 9.
- 4) General Membrane plus Bending Stresses are compared to 1.5 S, Reference 9.
- 5) Primary Membrane plus Secondary Stresses are compared to 3 S_m, Reference 1.
- 6) Bolt Stresses are compared to Limits of Para. XVII-2460, Reference 9.
- 7) Weld Stresses are compared to 21000 psi shear, Reference 9, Table NF-3292.1-1.

Section 3.0

ANALYTICAL METHODS

A finite element model of the type CEU heat exchanger was developed using Control Data Corporation's STARDYNE computer code, Reference 10. This model included the major load paths, flexibility members, and mass of the unit.

The frequency analysis was performed using the Householder-QR option of program STARDYNE. For this analysis the units weight was distributed among nine (9) node points as described in Section 6.3.

The nozzle load analysis, deadweight analysis, and seismic analysis were performed using the STATIC option of program STARDYNE. The deadweight and seismic analysis consisted of inputting concentrated forces at the mass points equal to the mass times the respective "g" loadings. The nozzle loads were applied to be consistent with the seismic loading per Reference (1), Paragraph 4.1.3.

The final total stresses on each component were determined by absolutely summing the effects of nozzle, seismic and deadweight loads. NUS Corporation's computer codes PRECOM and COMBINE were used in the summing of the stresses.

A local shell analysis of the nozzle to shell junctions and support, seismic lug to shell junctions was performed using the

Welding Research Council Bulletin, Reference 4, as coded in the SANSAR computer code.

Program abstracts of the NUS Corporation programs PRECOM, COMBINE, and SANSAR are presented in their respective appendices.

Standard engineering mechanics of materials formulae will be used to calculate support and support lug stresses.

Section 4.0

REFERENCES

1. Combustion Engineering Specification No. 1370-PE-301, Rev. 03-1/27/75, Project Specification for a Heat Exchanger.
2. EFCO Drawing No. CD-16645, Rev. D
3. XUS Corporation Proposal No. 7507041 (P-421).
4. K. R. Wichman, A. G. Hopper and J. L. Mershon, "Local Stresses in Spherical and Cylindrical Shells due to External Loading," Welding Research Council Bulletin, August 1965 and Revised Printing, December, 1968.
5. Telecon with D. Ringo of EFCO on 9/17/75.
6. Chi-Teh, Wang, Applied Elasticity, Mc Graw Hill, New York, New York, 1953.
7. Gere and Weaver, Analysis of Framed Structures, Van Nostrand Reinhold Company, New York, New York, 1965.
8. ASME Boiler and Pressure Vessel Code, Section II, 1974, American Society of Mechanical Engineers, New York, New York.
9. ASME Boiler and Pressure Vessel Code, Section III, 1974, American Society of Mechanical Engineers, New York, New York.
10. MRI/STARDYNE Structural Analysis System, Mechanics Research, Inc., Los Angeles, California, 1970.

Mr. JEC DATE 10/1/75
DRAWD BY ETS DATE 10/1/75

SUBJECT MATERIAL PROPERTIES

SHEET NO. OF
JOB NO. EFCO-2

SECTION 5.0

MATERIAL PROPERTIES

THE MODULUS OF ELASTICITY, AND ALLOWABLE STRESS VALUES WERE OBTAINED FROM REF(G).

TABLES I-6.0 P 105 & I-7.1 P 107 RESPECTIVELY FOR A-102-F809 TABLE I-7.2 P 118 FOR S.

COMPONENT	ASTM MATERIAL SPEC.	DESIGN TEMP. (OF)	MODULUS OF ELASTICITY E (PSI)	POLYMER RATIO	ALLOWABLE STRESS S (PSI)
ALL SHELLS, PLATES, AND SUPPORTS EXCEPT FLANGES	A-516-70 (carbon content <.3%)	400	27.0 x 10 ⁶	.3	17,500
NOZzLES	A-106 GRB	250	27.55 x 10 ⁶	.3	15,000
NOzzLES	A-182 F804	400	26.6 x 10 ⁶	.3	16,200
FLANGES	A-105 CARBON CONTENT ASSUME=.3)	250	27.65 x 10 ⁶	.3	17,500
FLANGES	A-105 CARBON CONTENT ASSUME=.3)	400	22.0 x 10 ⁶	.3	17,500

* CARBON CONTENT FROM REF(B)

Section 6.0

MODEL

Presented herein are the model CALCOMP plots, nodal coordinates, element connectivity, element flexibilities, and nodal weights for the mathematical model used in this analysis.

This finite element model was developed with the use of the Control Data Corporation CDC-6600 STARDYNE computer code, Reference 10.

Section 6.1

Plots

Presented herein are CALCOMP plots of the model together with sketches illustrating the node and element numbering schemes. Also shown on the sketches are the dynamic "principal" mass nodes.

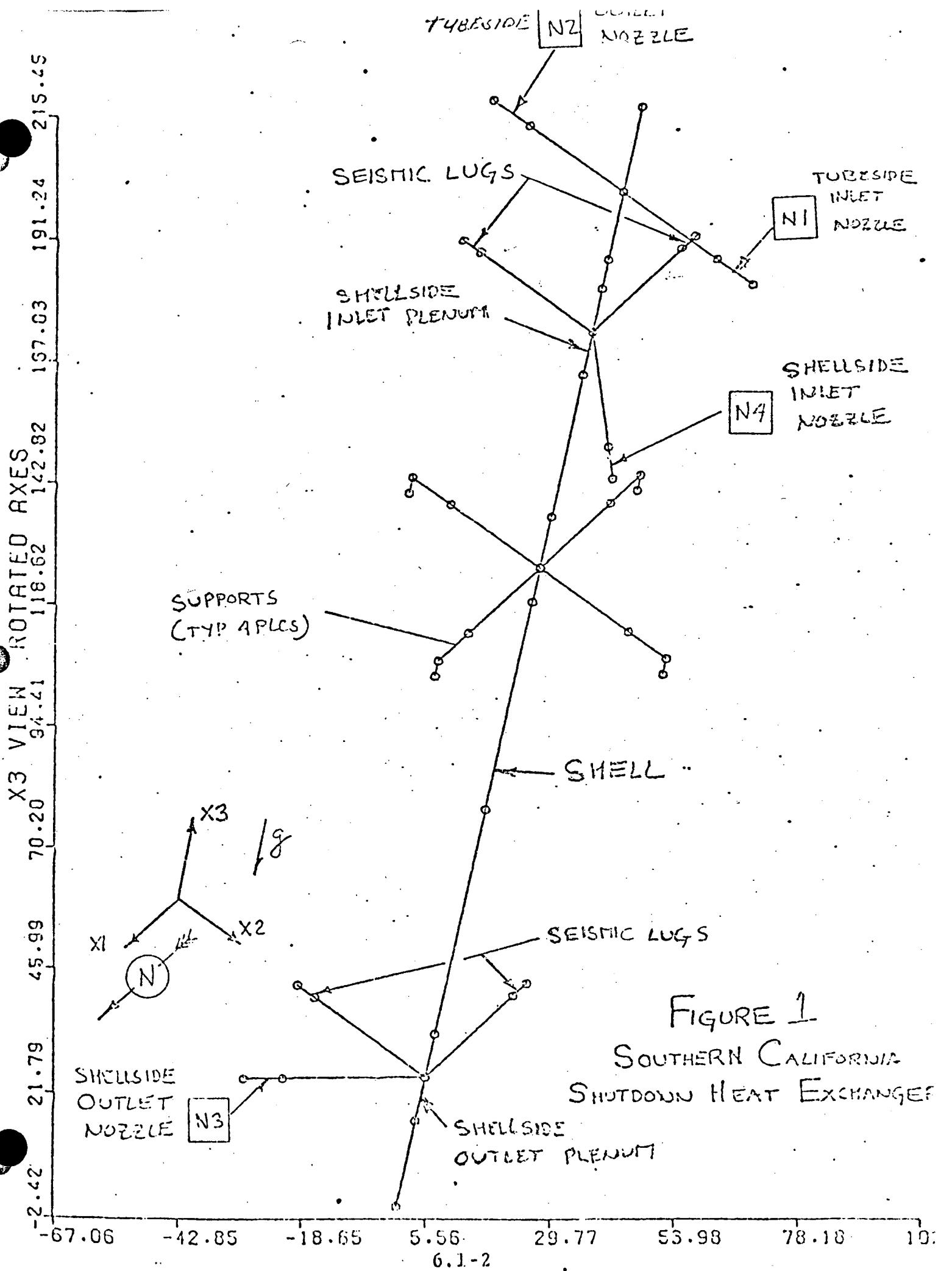


FIGURE 1
 SOUTHERN CALIFORNIA
 SHUTDOWN HEAT EXCHANGER

215.45
191.24
167.03
142.82
118.62
104.41
80.20
56.00
31.79
5.55
-18.65
-42.85
-57.06

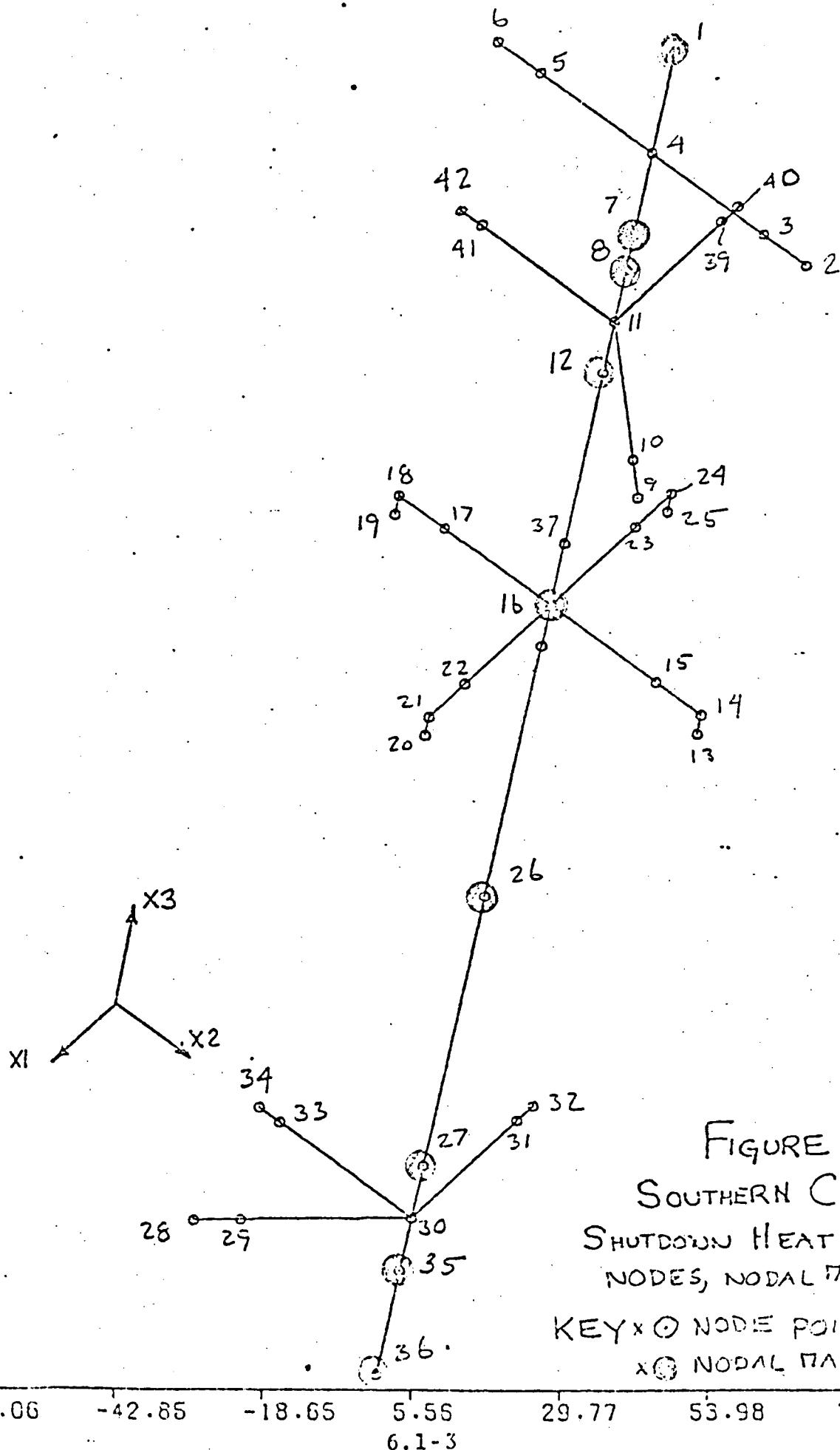
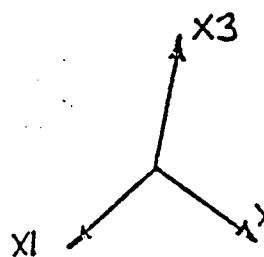


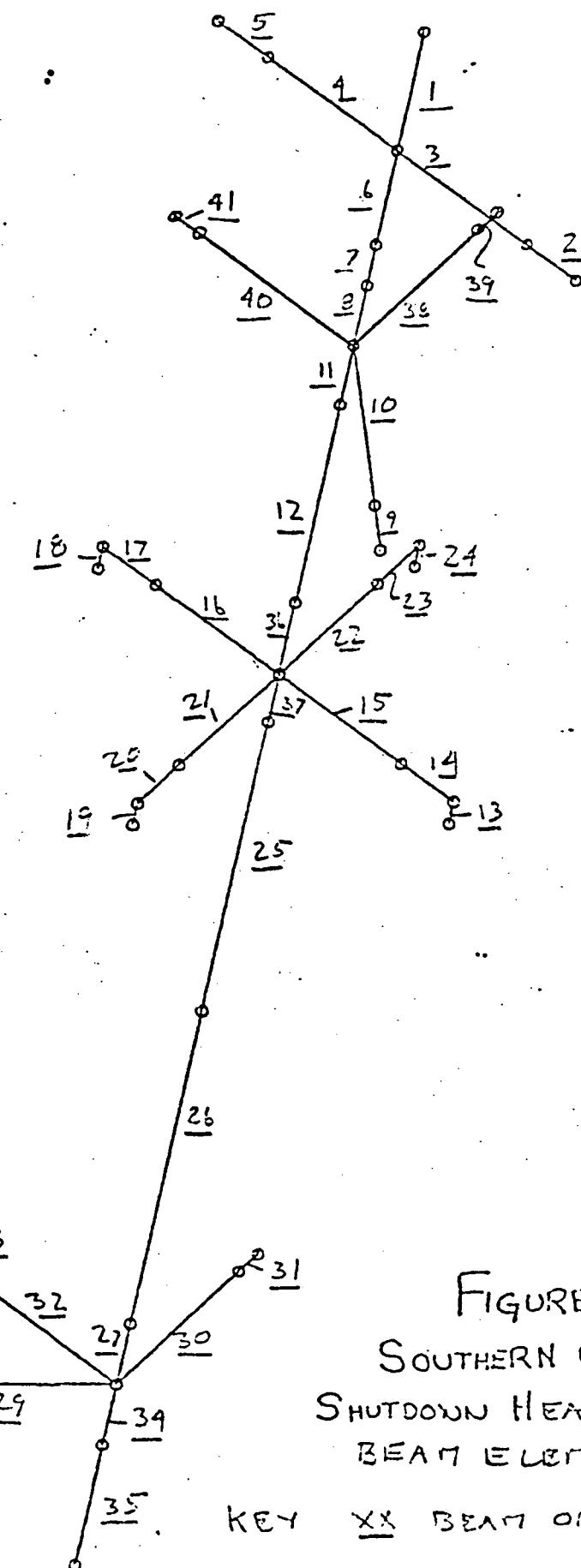
FIGURE 2
SOUTHERN CALIFORNIA
SHUTDOWN HEAT EXCHANGE:
NODES, NODAL MASS POINTS

57.06 -42.85 -18.65 5.55 29.77 53.98 78.18 100
-57.06 42.85 18.65 -5.55 -29.77 -53.98 -78.18 -100

215.45
211.24
191.03
167.03
142.62
110.62
84.51
64.51



-77.06 -42.85 -18.65 5.56 29.77 53.98 78.18 100
6.1-4



6.7 BEAM PROPERTIES

BPROP1 - 1 RIGID BEAMS

ASSUME THAT THE RIGID BEAMS HAVE PROPERTIES 5 TIMES THE PROPERTIES OF THE 86" O.D. DISTRIBUTORS. THIS SHELL WAS CHOSEN BECAUSE IT HAS THE LARGEST INERTIA PROPERTIES.

DISTRIBUTOR SHELL

$$O.D. = 56 \text{ IN} \quad t = .625 \text{ IN}$$

AREA, A

$$A = 2\pi R_{in} t = 2\pi(27.69).625 \\ = 108.7 \text{ IN}^2$$

POLAR MOMENT, J

$$J = 2\pi R_{in}^3 t = A R_{in}^2 = 108.7(27.69)^2 \\ = 83374 \text{ IN}^4$$

MOMENT OF INERTIA, I₂, I₃

$$I_2 = I_3 = \frac{J}{2} = 41697 \text{ IN}^4$$

SUMMARY OF RESULTS ($\approx 5x$ ABOVE PROPERTIES)

$$A = 500 \text{ IN}^2$$

$$J = 4 \times 10^5 \text{ IN}^4$$

$$I_2 = I_3 = 2 \times 10^5 \text{ IN}^4$$

$$\text{ASSUME } SF2 = SF3 = SSF2 = SSF3 = 1.0$$

BY J.W.C. DATE 10/15/67 SUBJECT BEAM PROPERTIES 2-6-7
CHKD. BY [initials] DATE 10/15/67 SHEET NO. OF
JOB NO. 100-2-2

BEAM PROPERTIES 2-6-7 ARE INPUT
AS "PIPE" BEAMS USING THE PROPERTIES
LISTED AS FOLLOWS:

BPROP3 NO.	DESCRIPTION	O.D.	t
2	CHANNEL SHELL	46.75	1.25
3	NOZZLES <input type="checkbox"/> <input checked="" type="checkbox"/>	12.75	.33
4	SHELLSIDE SHELL	45.	.50
5	DISTRIBUTORS	56.	.625
6	NOZZLES <input type="checkbox"/> <input checked="" type="checkbox"/>	16.	.50
9	SHELLSIDE SHELL PLUS PNO	45.	1.00

BY: JWC DATE 9/18/75 SUBJECT
 CHKD. BY DATE BEAR PROPERTY 7
 SHEET NO. OF
 JOB NO. EFCO - 1

AREA, A

$$A = 2A_1 + A_2$$

$$A = 2(.75)(14.11) + 15(.875)$$

$$A = 2(10.58) + 13.13$$

$$A = 34.29$$

CENTROID, \bar{x}

$$\bar{x} = (\sum A_i x_i) / A$$

$$\bar{x} = [2(10.58)7.93 + (13.13), 438] / 34.29$$

$$\bar{x} = 5.06$$

POLAR MOMENT OF INERTIA, I . REF(6) page 4.0.1

$$I = \sum \frac{1}{3} b_i t_i^3$$

$$I = 2 \left(\frac{1}{3}(14.11)(.75)^3 \right) + \frac{1}{3}(15)(.575)^3$$

$$I = 7.32 \text{ in}^4$$

MOMENT OF INERTIA, I_2

$$I_2 = \sum \left(\frac{1}{12} b_i h_i^3 + A_i \bar{x}_i^2 \right)$$

$$I_2 = 2 \left[\frac{1}{12}(14.11)(.75)^3 + 10.58(6.625)^2 \right] + \frac{1}{12}(15)(.575)^3$$

$$I_2 = 1176 \text{ in}^4$$

MOMENT OF INERTIA, I_3

$$I_3 = 2 \left[\frac{1}{12} (14.11)^3 (.75) + 10.56 (2.37)^2 \right]$$

$$+ \frac{1}{12} (.875)^3 (15) + (13.13)(4.62)^2$$

$$I_3 = 80.7 \text{ in}^4$$

SHEAR SHAPE FACTORS, SF2, SF3, REF 7 P459

$$SF2 \approx \frac{(15-.75)(.875)}{34.29} = .338$$

$$SF3 = 1 - SF2 = .662$$

TORSION STRESS FACTOR (CTORS) REF 6 P97

CTORS = GREATER THICKNESS

$$\therefore CTORS = .875 \text{ in}$$

SHEAR STRESS FACTORS

FOR PRIMARY MEMBRANE SHEAR STRESSES

$$SSF2 = SSF3 = 1.0$$

SUMMARY OF RESULTS, BPROP1, 7

$$A = 34.29 \text{ in}^2 \quad SF2 = .338$$

$$J = 7.32 \text{ in}^4 \quad SF3 = .662$$

$$I_2 = 1176 \text{ in}^4 \quad CTORS = .875 \text{ in}$$

$$I_3 = 807 \text{ in}^4$$

BY ALG DATE 7/18/85

SUBJECT BEAM PROPERTY 7

CHKD. BY TCK DATE

SHEET NO. OF

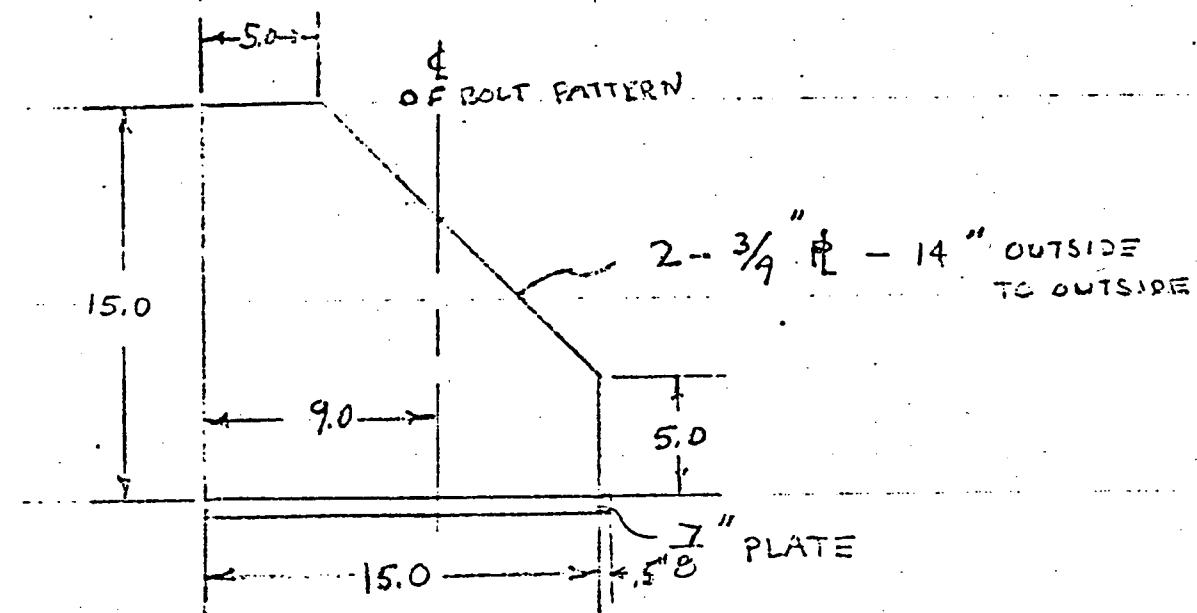
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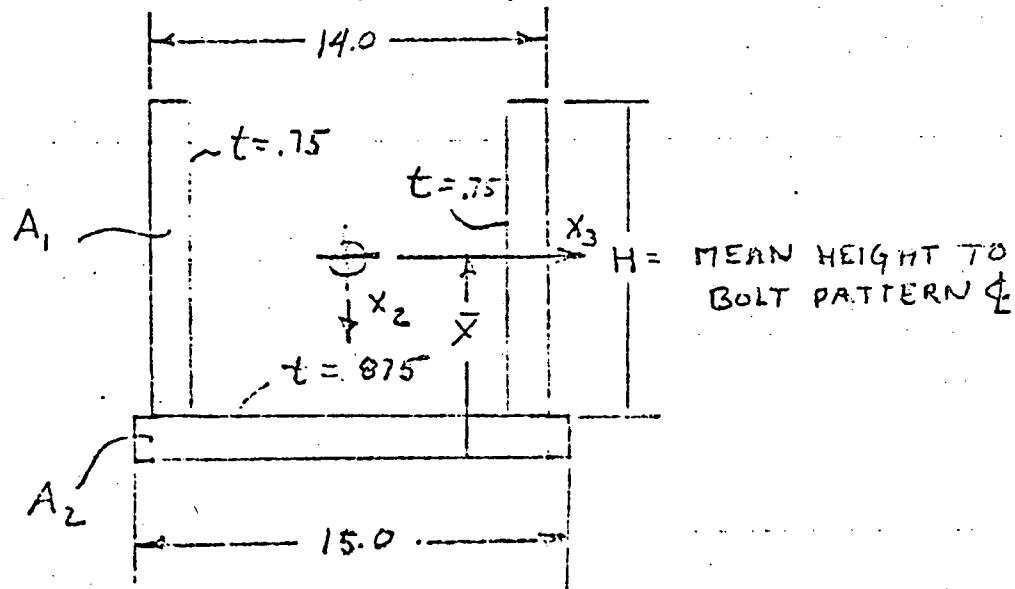
BPROP 1 - 7

SUPPORTS

ACTUAL GEOMETRY



ASSUMED GEOMETRY, AT VESSEL/SUPPORT JUNCTION



MEAN HEIGHT, H

$$H = \left[15(5) + \left(\frac{15+11}{2} \right) 4 \right] / 9 = 14.11 "$$

BY DATE 1/1/12 SUBJECT

CHKD. BY DATE 1/1/12

SHEET NO. OF

JOB NO.

F150-2

EPROP 1-3 SEISMIC LUGS

GEOMETRY

3/4" PLATE X 12" LONG

AREA, A

$$A = \frac{3}{4} \cdot 12 = 9 \text{ IN}^2$$

POLAR MOMENT OF INERTIA, I

$$I = \frac{1}{3} (12)(6.75)^3 = 1.688 \text{ IN}^4$$

MOMENT OF INERTIA, I₂

$$I_2 = \frac{1}{12} (12)^3 (6.75) = 108 \text{ IN}^4$$

MOMENT OF INERTIA, I₃

$$I_3 = \frac{1}{12} (12)(6.75)^3 = .422 \text{ IN}^4$$

SHEAR SHAPE FACTORS, REF 7 P 459

$$SF2 = 0 \quad SF3 = .833$$

TORSION STRESS FACTOR, CTORS

$$CTORS = .75 \text{ IN}$$

BY JWL DATE 7/1/71
CHKD. BY E. DATE 7/1/71

SUBJECT.....
..... NODAL WEIGHT
DISTRIBUTION

SHEET NO. OF ...
 JOB NO.
 E5C0-2

6.3 NODAL WEIGHT DISTRIBUTION

THE UNIT WEIGHT ABOVE & BELOW
THE CG OF THE UNIT WILL BE
EVENLY DISTRIBUTED ALONG THE LENGTH
OF THE UNIT. THE WEIGHT ABOVE
AND BELOW THE SUPPORTS WILL BE
DETERMINED BY RATIOING THE CG DISTANCE
ABOVE & BELOW THE SUPPORT AS SHOWN
ON REF ().

$$\text{TOTAL WEIGHT} = 61000 \text{ LBS}$$

$$w_{\text{BELOW}} = (w_{\text{TOTAL}}(8')) / 8' - 8'9''$$

$$w_{\text{BELOW}} = 61000 (.478)$$

$$w_{\text{BELOW}} = 29200 \text{ LBS} = w_B$$

$$\therefore w_{\text{ABOVE}} = w_A = 61000 - 29200 = 31800 \text{ LBS.}$$

RATIOING BY LENGTH THE DISTRIBUTED
MASS BECOMES:

$$w_1 = \frac{(361 - 310.5)(.5)}{361 - 204.5} w_A = .5 \left(\frac{50.5}{156.5} \right) 31,800$$

$$w_1 = 5131 \text{ LBS}$$

BY J.V. DATE 7/1/75
CHKD. BY DATE

SUBJECT

INTEGRAL WEIGHT
DIST. S. T. U. T. I. O. N

SHEET NO. OF
JOB NO.
E1820-2

$$w_7 = w_1 + w_A (.5) \frac{(310.5 - 300.88)}{156.5} = 6103 \text{ LBS}$$

$$w_8 = (.5) w_A \frac{(310.5 - 272.88)}{156.5} = 3922 \text{ LBS}$$

$$w_{12} = (.5) w_A \frac{(300.88 - 204.5)}{156.5} = 9792 \text{ LBS}$$

$$w_{16} = (.5) w_A \frac{(272.88 - 204.5)}{156.5} + .5 w_B \frac{(204.5 - 130.19)}{204.5} = 12252 \text{ LBS}$$

$$w_{26} = (.5) w_B \frac{(204.5 - 56.13)}{204.5} = 10593 \text{ LBS}$$

$$w_{27} = (.5) w_B \frac{(130.19 - 28.13)}{204.5} = 7286 \text{ LBS}$$

$$w_{35} = (.5) w_B \frac{(56.13 - 0)}{204.5} = 4007 \text{ LBS}$$

$$w_{36} = (.5) w_B \frac{(28.13)}{204.5} = 2008 \text{ LBS}$$

CHKD. BY J.M. DATE 4/1/65

NODAL WEIGHT
SUMMARY

JOB NO.

E170-2

NODAL WEIGHT SUMMARY

NODE NO	NODAL WEIGHT (LBS)
1	5131
7	6108
8	3822
12	9792
16	12252
26	10593
27	7286
35	4007
36	2008
TOTAL	60999 LBS.

Section 6.4
Support and Seismic Lug Details

SUPPORT DETAIL

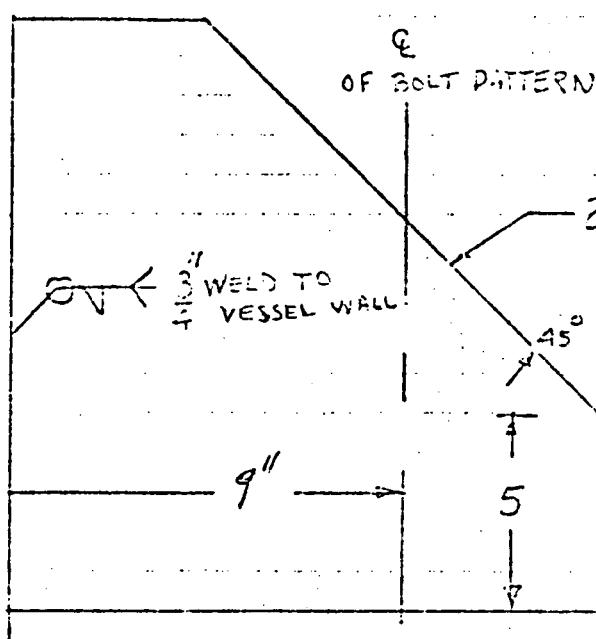
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4

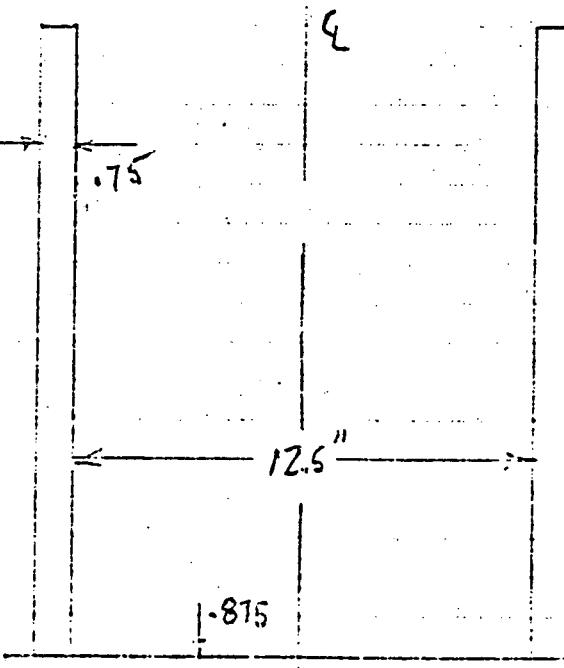
15

15

15



← 15 → ← .5" →



← 15 →

BY P.B. DATE 11/20/75 SUBJECT

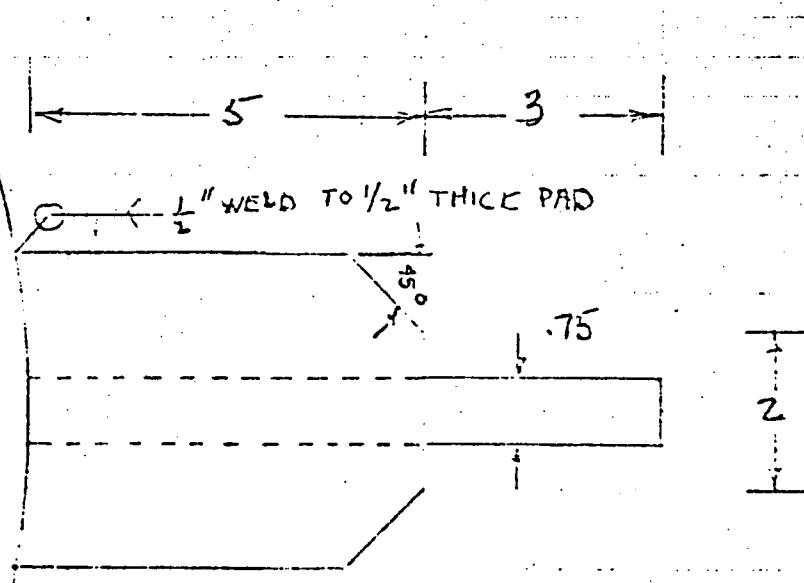
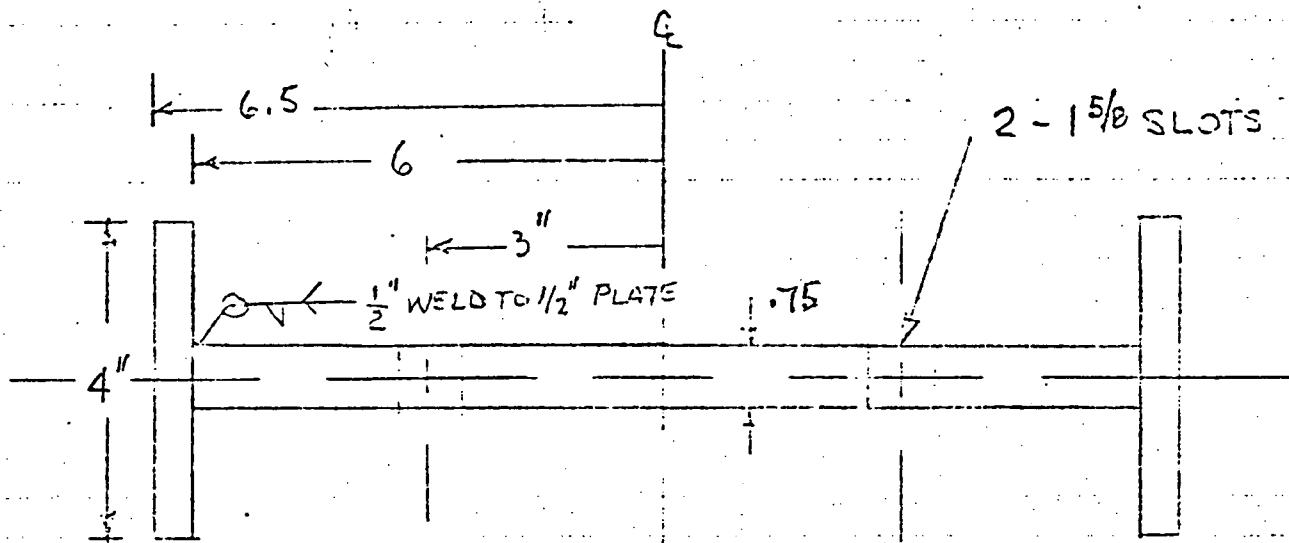
CHKD. BY J.S. DATE 10/20/75

SHEET NO. OF

JOB NO.

E1PC0-2

SEISMIC LUG DETAIL



BY J.W.C. DATE 11.11.13 SUBJECT.....
CHKD. BY K.W.C. DATE 11.11.13 JOB NO. 11-100-1

SUPPORT PAD LENGTH

LONG SHELL LENGTH FOR SUPPORT PAD, L

$$R_m = 22.5 \text{ " } \quad v = .3$$

$$t = 1.0 \text{ " } \quad L = \frac{3}{\lambda}$$

$$\lambda = \left(\frac{3(1-v^2)}{R_m^2 t^2} \right)^{1/4}$$

$$\lambda = \left(\frac{3(.91)}{225^2 (1)^2} \right)^{1/4} = .271$$

$$L = 11.1 \text{ "}$$

∴ SUPPORT SHOULD BE 12" LONG,

ON EACH SIDE OF SUPPORT CENTROID.

∴ USE 28" PAD $\frac{1}{2}$ " THICK

WITH 6.125" BELOW $\frac{7}{8}$ " RL

6 " ABOVE TOP OF SUPPORT

BY JPL DATE 10/11/75 SUBJECT.....
CHKD. BY JFB DATE 10/12/75 SECTION 7.1
SHEET NO. OF.....
JOB NO.
REF ID: E

7.1 NOZZLE AND DEADWEIGHT LOAD

ANALYSIS

DEADWEIGHT LOAD

THE DEADWEIGHT ANALYSIS WILL
BE PERFORMED BY INPUTTING A -1g
ACCELERATION FORCE ON THE NODAL MASSES
OR:

NODE	DEADWEIGHT FORCE, FX3
1	-5131
7	-6108
5	-3622
12	-9792
16	-12252
26	-10593
27	-7296
35	-4007
36	-2008

NOZZLE LOADS

THE NOZZLE LOADS WILL BE
APPLIED IN A DIRECTION THAT IS
ADDITIVE TO THE SEISMIC LOAD

DIRECTIONS OF SECTION 8.2 OF THIS REPORT (See
APPENDIX)

BY DATE 10/15/75 SUBJECT
CHKD. BY PFE DATE 10/31/75

SHEET NO. OF
JOB NO.
EFG-2

NOZZLE LOADS, (EARTHQUAKE 1)

NOZZLES **N1** & **N2**, NODES 2 & 6

LOAD (MAGNITUDE)	GLOBAL DIRECTION
------------------	------------------

F _A 2952	+ X2
---------------------	------

F _S 2952	- X1
---------------------	------

M _T 90300	- X2
----------------------	------

M _B 90300	- X1
----------------------	------

NOZZLE **N3**

NODE 28

F _A 5523	- .707 X1	+ .707 X2
---------------------	-----------	-----------

F _S 5523	+ X3	
---------------------	------	--

M _T 210300	- .707 X1	+ .707 X2
-----------------------	-----------	-----------

M _B 210300	- .707 X1	- .707 X2
-----------------------	-----------	-----------

NOZZLE

N4

NODE 9

F _A 5523	- .707 X1	- .707 X2
---------------------	-----------	-----------

F _S 5523	- .707 X1	+ .707 X2
---------------------	-----------	-----------

M _T 210300	- .707 X1	- .707 X2
-----------------------	-----------	-----------

M _B 210300	- .707 X1	+ .707 X2
-----------------------	-----------	-----------

FOR LOAD CASE 2 (EARTHQUAKE 2), THE LOADS WILL BE THE SAME EXCEPT THAT THE NOZZLE **N3**, NODE 28 SIGNS WILL BE OPPOSITE THOSE OF LOAD CASE 1

NOZZLE LOAD SUMMARY

LOAD CASE	NODE	F_{x1}	F_{x2}	F_{x3}	M_{x1}	M_{x2}
EQ1	2	-2952	+2952	0	-90300	-90300
	6	-2952	+2952	0	-90300	-90300
	28	-3905	+3905	5523	-297400	0
	9	0	+7810	0	-297400	0
EQ2	2	-2952	+2952	0	-90300	-90300
	6	-2952	+2952	0	-90300	-90300
	28	+3905	-3905	-5523	+297400	0
	9	0	+7810	0	-297400	0

A. THIRD NOZZLE LOAD CASE WILL
BE RUN THAT WILL PRODUCE A MAXIMUM
OVERTURNING MOMENT ABOUT THE SUPPORT
PLANE.

2	-2952	+2952	0	-90300	-90300
6	-2952	+2952	0	-90300	-90300
28	+3905	-3905	+5523	-297400	0
9	0	+7810	0	-297400	0

7.2 LOCAL STRESS ANALYSIS OF NOZZLE/ SHELL JUNCTIONS

PER REF(1) P2 THE FOLLOWING
NOZZLE LOADS WILL BE USED IN THIS
ANALYSIS.

12"	16"
NOZZLES	NOZZLES
<u>N1 & N2</u>	<u>N3 & N4</u>

AXIAL FORCE (LBS) 2952 5523

TRANSVERSE (LBS) 2952 5523

TORSIONAL MOMENT 7525 17,525
(ft/lbs)

BENDING MOMENT 7525 17,525
(ft/lbs)

THE PRESSURE AND TEMPERATURE
CONDITIONS TO BE USED ARE AS
FOLLOWS (FROM REF(2)):

NOZZLES	PRESSURE	TEMP.
P (PSI)	T (°F)	

N1 & N2 650 400°F

N3 & N4 150 250°F

NOZZLE / VESSEL JUNCTION PARAMETERS

NOZZLE	SV (ksi)	SN (ksi)	P (psi)	RIV ⁽¹⁾ (in)	TV ⁽¹⁾ (in)	RON ⁽¹⁾ (in)	TN ⁽¹⁾ (in)
N1 + N2	17.5	16.2	650	23.69	3.125	7.188	1.143
N3 + N4	17.5	15.0	150	28.25	1.5	9.0	.375

(1) NOTE: DIMENSIONS INCLUDE CORROSION ALLOWANCE WHERE APPLICABLE.

LOAD APPLICATION POINT

NOZZLE X Y H

N1 **N2** 0 9.06 0

2 2 0 7.75 0

SANSAR INPUT LOADS (IN SANSAR LOAD CONVENTION)

THESE LOADS ARE APPLIED TO MAXIMIZE STRESSES

IN THE NOZZLE VESSEL JUNCTION

$$F_x(10s) \quad F_y(10s) \quad F_z(10s) \quad M_x(100s) \quad M_y(100s) \quad M_z(100s)$$

CASE 1 - 2952 + 2952 0 0 90300 + 90300

CASE 2 0 + 2952. + 2952 + 90300 90300 0

CASE1 - 5523 + 5523 0 0 210300 + 210300

CASE 2 0 + 5523 + 5523 + 210300 210300 0

BY 11/3 DATE 11/2/75 SUBJECT LOCAL NOZZLE
CHKD BY EICD JOB NO. EICD-2

LOCAL NOZZLE STRESSES

THE FOLLOWING PRIMARY LOCAL
MEMBRANE STRESSES ARE EXTRACTED FROM
SANSAR OUTPUT, APPENDIX C.2

NOZZLE/ LOAD CASE	MAXIMUM PRINCIPLE STRESS (PSI)	MAXIMUM ALLOWABLE STRESS (1) (PSI)
----------------------	---	---

NOZZLES N1 & N2

LOAD CASE 1

VESSEL	9136	28,800
NOZZLE	7220	26,730

LOAD CASE 2

VESSEL	8908	28,800
NOZZLE	7220	26,730

NOZZLES N3 & N4

LOAD CASE 1

VESSEL	9168	28,800
NOZZLE	7378	24,750

LOAD CASE 2

VESSEL	7429	28,800
NOZZLE	7378	24,750

(1) NOTE: THE MAXIMUM ALLOWABLE STRESSES ARE
BASED ON NORMAL PLUS OBE LIMITS OF 1.65 S, REF(1) PAG. 45.
7.2-3

SECTION 8.1FREQUENCY ANALYSIS

THIS SECTION CONTAINS A SUMMARY OF THE SIGNIFICANT MODAL FREQUENCIES FROM THE FREQUENCY AND MODESHAPE ANALYSIS PRESENTED IN APPENDIX A.2.

THIS ANALYSIS REPRESENTS THE FREE VIBRATION RESULTS OF THE MATHEMATICAL MODEL PRESENTED IN SECTION 6.0.

THE FREQUENCIES AND MODESHAPES WERE EXTRACTED FROM $(K = \omega^2 m) \phi = 0$, BASED ON THE "CONDENSED" INERTIA MATRIX, BY THE HOUSEHOLDER QR TRANSFORMATION TECHNIQUE, HQR' OPTION OF "STARDYNE" REF 10.

MODE NO.	FREQUENCY (CPS)	NORMALIZED NODE (1)	DIRECTION (1)
1	48.5	1	-x1, +x2
2	50.5	1	+x1, +x2
3	62.2	26	-x1, -x2
4	62.3	26	+x1, +x2

(1) SEE MODEL PLOTS FOR NODE LOCATION
AND GLOBAL COORDINATE DIRECTION.

8.2 SEISMIC LOADING

PER REF(1) PARA 4.13 THE FOLLOWING
SEISMIC LOADS WILL BE USED IN THE
ANALYSIS

CONDITION	ACCELERATION (G's)	
	HORIZONTAL	VERTICAL
OBE	.55	$\pm .6$
DBE	1.2	± 1.1

THE HORIZONTAL ACCELERATION WILL
BE APPLIED TO THE UNIT COINCIDENT
WITH THE DIRECTION OF THE MODESHAPE
OF THE FIRST NATURAL FREQUENCY AS
EXTRACTED FROM THE HGR OUTPUT.
THIS DIRECTION IS THE MOST FLEXIBLE
PLANE OF THE UNIT.

THE UNIT WILL BE ANALYZED USING
DBE LOAD CONDITIONS AND STRESS
COMPARISONS MADE TO OBE STRESS
ALLOWABLES. FAILING THIS COMPARISON,
OBE AND DBE LOADINGS WILL BE ANALYZED
USING THEIR RESPECTIVE ALLOWABLES.

THE SEISMIC LOADING WILL BE INPUT AS NODAL FORCES ON THE NODAL WEIGHTS. PER REF(1) THE SEISMIC LOADS ARE TO BE APPLIED AS FOLLOWS:

1. HORIZONTAL ACCELERATIONS IN THE SAME DIRECTION ABOVE AND BELOW THE SUPPORT PLANE COMBINED WITH VERTICAL ACCELERATION.

2. HORIZONTAL ACCELERATIONS IN OPPOSITE DIRECTIONS ABOVE AND BELOW SUPPORT PLANE COMBINED WITH VERTICAL ACCELERATION.

FOR LOAD CASE 1, THE STATIC FORCE WILL BE APPLIED AS A CONSTANT FORCE ABOVE AND BELOW THE SUPPORT PLANE.

FOR LOAD CASE 2, THE STATIC FORCE WILL BE APPLIED AS A LINEARLY VARYING FORCE PROPORTIONAL TO THE DISTANCE FROM THE SUPPORT PLANE TO THE NODAL MASS,

BY Lee DATE 10/15/75 SUBJECT
CHKD. BY PJB DATE 10/21/75

SHEET NO. OF

JOB NO.

EFCO-7

LOAD CASE 1, EARTHQUAKE

RESOLVED IN ACCELERATION
(APPLIED IN DIRECTION OF FIRST FREQUENCY MODE SHAPE)

$$g_{x_1} = -\cos 45^\circ (1.2) = -.849 g$$

$$g_{x_2} = \sin 45^\circ (1.2) = +.849 g$$

$$g_{x_3} = -1.1 g$$

NODAL FORCE

NODE	WEIGHT	X1	X2	X3
		FORCE (LBS)	FORCE (LBS)	FORCE (LBS)(1)
1	5131	-4354	4354	-5644
7	6108	-5183	5163	-6719
8	3522	-3213	3243	-4204
12	9792	-8309	8309	-10771
16	12252	-10396	10396	-13477
26	10593	-8988	8988	-11652
27	7286	-6182	6182	-8015
35	4007	-3400	3400	-4408
36	2008	-1704	1704	-2209

(1) APPLIED IN A DIRECTION TO SUM WITH
THE DEADWEIGHT LOAD

LOAD CASE 2, EARTHQUAKE 2

NODES 1, 7, 8, 12, & 16 ARE ABOVE THE SUPPORT PLANE ($X_3 = 204.5"$) AND NODES 26, 27, 35 & 36 ARE BELOW THE SUPPORT PLANE.

NODAL FORCE (2)

NODE	FORCE MAGNITUDE BEFORE LINEARIZING	X3 LOCATION FROM PLANE	DISTANCE FROM PLANE	PROPORTION FACTOR(1)	FORCE	X1	X2	
					(LBS)	(LBS)	(-X1)	(+X2)
1	4354	361	156.5	+1	-4354	4354		
7	5183	310.5	106.0	+.677	-3509	3509		
8	3243	300.88	96.38	-.616	-1998	1998		
12	8309	272.88	68.38	+.437	-3631	3631		
16	10396	209.56	5.06	+.6323	-336	336		
26	8988	130.19	-74.31	-.363	+3263	-3263		
27	6182	56.13	-148.37	-.726	+4488	-4488		
35	5400	28.13	-176.37	-.862	+2931	-2931		
36	1704	0.0	-204.5	-1	+1704	-1704		

$$(1) F = \frac{D}{156.5} \text{ ABOVE PLANE}, F = \frac{D}{204.5} \text{ BELOW PLANE}$$

(2) THE X3 FORCES ARE THE SAME FOR LOAD CASE 2 AS FOR EARTHQUAKE 1.

SECTION 9.1

SUMMARY OF BEAM STRESSES

EXTRACTED FROM COMBINE OUTPUT APPENDIX B.2

BEAM NOS.	DESCRIPTION	EQ. 1 MAXIMUM STRESS INTENSITY (PSI)	EQ. 2 MAXIMUM STRESS INTENSITY (PSI)	ALLOWABLE STRESS (PSI) (1)
	TUBESIDE			
1, 6	PLENUM OUTLET	12156	12156	19250
5		13043	13043	17820
2	INLET	13043	13043	17820
	SHELLSIDE			
8, 11	INLET PLENUM	6756	6747	19250
9	INLET NOZZLE	4651	4651	16500
27, 34	OUTLET PLENUM	6729	6725	19250
28	OUTLET NOZZLE	4987	4987	16500
7, 12, 25, 26	SHELL	6817	6832	19250
35, 36, 37				
31, 33, 39, 41	SEISMIC LUG ⁽²⁾			19250
14, 17, 20, 23	SUPPORT ⁽²⁾			19250

(1) MEMBRANE STRESS LIMIT FOR NORMAL OPERATING OR UPSET, AND OBE 1.1 S

(2) REFINED SEISMIC LUG AND SUPPORT STRESS ANALYSIS IS PRESENTED IN SECTION 9.3

9.2 LOCAL STRESS ANALYSIS OF SUPPORT TO
 SHELL AND SEISMIC LUG TO SHELL JUNCTIONS

SUPPORT, LUG / VESSEL JUNCTION

PARAMETERS

JUNCTION	SMM (KSI)	P (PSI)	R _M ⁽¹⁾ (IN)	T ⁽¹⁾ (IN)	TRANSVERSE LENGTH TWOC1 (IN)	AXIAL LENGTH TWOC2 (IN)
SUPPORT/ VESSEL	17.5	150	22.56	.875	15.0	15.875
LUG/ VESSEL	17.5	150	28.00 ⁽²⁾	1.0 ⁽²⁾	4.0 ⁽²⁾	13.0 ⁽²⁾

(1) NOTE: DIMENSIONS INCLUDE CORROSION ALLOWANCE WHERE APPLICABLE AND PAD THICKNESS WERE APPLICABLE.

(2) NOTE: SEE SECTION

LOAD APPLICATION POINT

X Y Z
 FOR BOTH JUNCTIONS 0 0 0

THE FOLLOWING LOADS ARE THE MAXIMUM LOADS EXTRACTED FROM COMBINE OUTPUT, APPENDIX B FOR EACH OF THE TWO JUNCTION TYPES. THE MAXIMUM OF EACH INDIVIDUAL LOAD WILL BE USED TO PRODUCE.

A "WORST CASE" ANALYSIS.

JUNCTION	$F_1(P)$ (LBS)	$F_2(V_2)$ (LBS)	$F_3(V_3)$ (LBS)	M_1 (LBS)	M_2 (INCHES)	M_3 (INCHES)
SUPPORTS						
EQ1	7979	35268	1693	27	18653	170310
EQ2	7721	38144	1816	70.	15554	195490

SEISMIC LUGS

EQ1	41875	0	7213	360	26705	234
EQ2	36897	0	7030	362	25526	235

IN ORDER TO INPUT THESE LOADS INTO SANSAR,
THEY MUST BE CONVERTED TO SANSAR COORDINATES.
THE CONVERSION IS.

FOR BEAMS 31, 33, 34, 41, 14, 17, 20, 23, AT J_A END
 SEISMIC LUGS SUPPORTS

SANSAR FORCE STARDYNE FORCE

$$\begin{array}{ll}
 F_X & = 2 \\
 F_Y & = 1 \\
 F_E & = -F_3 \\
 M_X & = M_2 \\
 M_Y & = M_T \\
 M_Z & = -M_3
 \end{array}$$

o SUMMARY OF LOADS

	FX	FY	FE	MX	MY	MZ
SEISMIC WGS	0	41878	-7213	26705	362	-235
SUPPORT	38144	7979	-1816	18653	70	-195490

BY JWC DATE 1/7/73 SUBJECT.....
CHKD BY JFC DATE 1/21/73

SHEET NO. OF
JOB NO.
EFCO-2

LOCAL SUPPORT/LUG TO VESSEL STRESSES

THE FOLLOWING PRIMARY LOCAL
MEMBRANE STRESSES ARE EXTRACTED
FROM SANSAR OUTPUT, APPENDIX C.3.

JUNCTION	MAXIMUM PRINCIPLE STRESS (PSI)	MAXIMUM ALLOWABLE STRESS(1) (PSI)
SUPPORT/VESSEL	5630	28800
SEISMIC LUG/ VESSEL	-5037	28800

(1) NOTE: THE MAXIMUM ALLOWABLE STRESSES ARE BASED
ON NORMAL PLUS OBE LIMITS OF 1.65 S PER REF(1) PARA 4.5.

THE FOLLOWING PRIMARY PLUS SECONDARY
STRESSES ARE EXTRACTED FROM SANSAR
OUTPUT, APPENDIX C.3.

JUNCTION	MAXIMUM PRINCIPLE STRESS (PSI)	MAXIMUM ALLOWABLE STRESS(2) PSI
SUPPORT/VESSEL	-7586	52500
SEISMIC LUG/ VESSEL	-38078	52500

(2) NOTE: ALLOWABLE STRESS = 3.05 S PER
PARA 4.5.2 REF(1) ...

9.3 SUPPORT AND WELD STRESS EVALUATION

SUPPORT PROPERTIES

THE SUPPORTS ARE APPROXIMATED BY

ASSUMING THE FOLLOWING MINIMUM

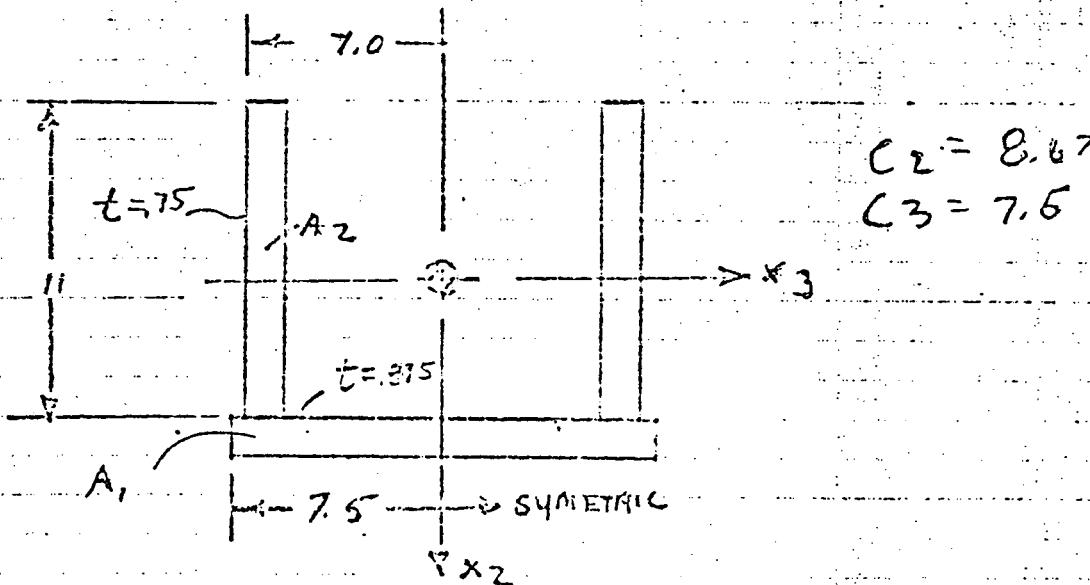
CROSS SECTION (AT THE BOLT CIRCLE &).

LOADS AT THE VESSEL/SUPPORT JUNCTION

WILL BE APPLIED TO THIS MINIMUM

CROSS SECTION TO PRODUCE CONSERVATIVE

STRESSES.



AREA

$$A = 2(A_1 + A_2)$$

$$A_1 = (.875)(7.5) = 6.56 \quad A_2 = (.75)(11) = 8.25$$

$$A = 29.62 \text{ in}^2$$

CENTROID, \bar{x}_2

$$\bar{x}_2 = (11 \cdot 75 + 1) / 4$$

$$\bar{x}_2 = (2) \left[6.56 \left(\frac{.875}{2} \right) + 8.25 \left(\frac{11}{2} + .875 \right) \right] / 29.62$$

$$\bar{x}_2 = 3.75 "$$

$$\therefore \bar{x}_{21} = 3.313 "$$

$$\bar{x}_{22} = 2.625$$

POLAR MOMENT OF INERTIA, J REF(6) PG 9

$$J = \sum \frac{1}{3} b_i t_i^3$$

$$J = 2 \left(\frac{1}{3} (11)(.75)^3 \right) + \frac{1}{3} (15)(.875)^3$$

$$J = 6.44 \text{ in}^4$$

MOMENT OF INERTIA, I_2

$$I_2 = - \frac{1}{12} (15)^3 (.875) + 2 \left[\frac{1}{12} (11)(.75)^3 + 8.25 (6.625)^2 \right]$$

$$I_2 = 971 \text{ in}^4$$

MOMENT OF INERTIA, I_3

$$I_3 = 2 \left[\frac{1}{12} (11)^3 (.75) + 8.25 (3.313)^2 \right]$$

$$+ \frac{1}{12} (.875)^3 (15) + (13.12)(2.625)^2$$

$$I_3 = 439 \text{ in}^4$$

THE FOLLOWING SUPPORT LOADS WERE EXTRACTED
FROM COMBINE OUTPUT (SEE SECTION 9.2).

P	V ₂	V ₃	M _T	M ₂	M ₃
(LBS)	(LBS)	(LBS)	(IN-LBS)	(IN-LBS)	(IN-LBS)
7979	38144	1816	70	18653	195490

GENERAL MEMBRANE STRESS SHEAR STRESS

$$\gamma = \frac{V_2}{A} + \frac{T_c}{J} \quad V = (V_2^2 + V_3^2)^{1/2}$$

$$\gamma = \frac{38147}{29.62} + \frac{70(.75)}{6.44} \quad A = 29.62$$

$$T_c = M_T = 70$$

$$\gamma = 1297 \text{ psi} \quad C = .75 \quad J = 6.44$$

NORMAL STRESS

$$\sigma_N = \frac{P}{A} \quad P = 7979$$

$$\sigma_N = 7979 / 29.62$$

$$\sigma_N = 269 \text{ psi}$$

CALCULATING σ_i

$$\sigma_i = +\frac{269}{2} + \left(\left(\frac{269}{2} \right)^2 + 1297^2 \right)^{1/2}$$

$$\sigma_i = 1439 \text{ psi} < 17500 \text{ KSI} = 1.0 \text{ S}^{(1)}$$

(1) ALLOWABLE STRENGTHS PER PARA NF 3321.1
D.3-3 REF (9)

GENERAL MEMBRANE PLUS BENDING

NORMAL STRESS DUE TO M_2

$$\sigma_{M_2} = \pm \frac{M_2 C_3}{I_2} = C_3 = 7.5$$

$$M_2 = 18653$$

$$\sigma_{M_2} = \pm 144 \text{ psi}$$

$$I_2 = 971$$

NORMAL STRESS DUE TO M_3

$$\sigma_{M_3} = \pm \frac{M_3 C_2}{I_3} = M_3 = 195490$$

$$C_2 = 8.67$$

$$I_3 = 439$$

$$\sigma_{M_3} = \pm 3861 \text{ psi}$$

COMBINING BENDING STRESSES AS THEY WILL ADD

$$\sigma_m = \pm 144 \pm 3861 = \pm 4005$$

$$\sigma = \sigma_m + \sigma_n$$

$$\sigma = 4005 + 269 = 4274 \text{ psi}$$

$$\tau = 1297 \text{ psi}$$

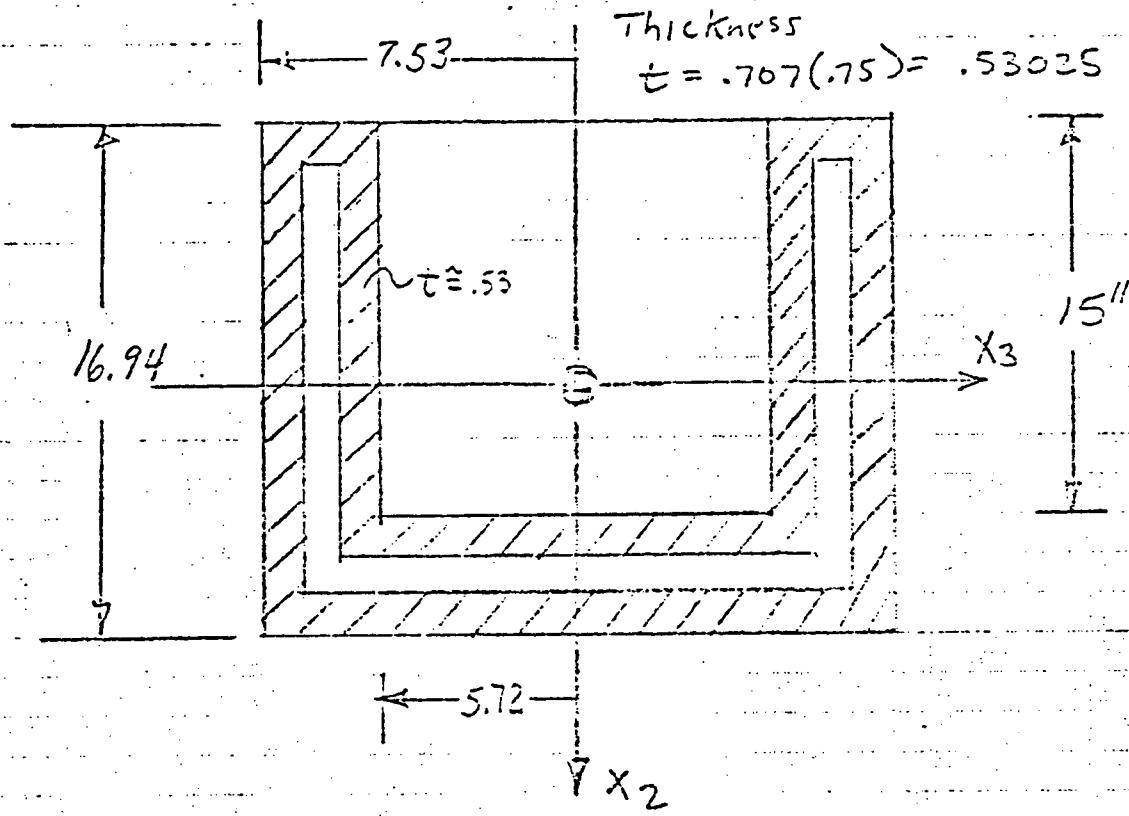
$$\therefore \sigma_i = \frac{4274}{2} + \left(\left(\frac{4274}{2} \right)^2 + 1297^2 \right)^{\frac{1}{2}}$$

$$\sigma_i = 4637 \text{ psi} < 26250 \text{ psi} = 1.5 S^{(1)}$$

(1) ALLOWABLE STRESS PER
PARA NF 3321.1 REF(7)

SUPPORT WELD PROPERTIES

The support weld configuration is approximated by the cross-hatched region shown below



Area

$$A_{WELD} = A_{TOTAL} - A_{SUPPORT} - 11.44(15)$$

$$= 16.94(15.06) - 2(15.815(.75) + 6.25(.875)) - 171.6$$

$$= 48.77 \text{ in}^2$$

Centroid, \bar{x}_2

$$\bar{x}_2 = \frac{\sum A_i x_i}{A}$$

$$\bar{x}_2 = \frac{(16.94(15.06)8.47 - 2(15.875)(.75)\left(\frac{15.875 + .53025}{2}\right) - 12.5(.875)\left(\frac{.875 + .53025}{2}\right)}{A} - 11.44(15)\left(\frac{15}{2} + 2(.53025) + .875\right)$$

$$\bar{x}_2 = \frac{255.12(8.47) - 23.81(8.47) - 10.94(.968) - 171.6(9.44)}{255.12 - 23.81 - 10.94 - 171.6}$$

$$\bar{x}_2 = 6.74$$

$$\bar{I}_3 = \frac{1}{12} 15.06(16.94)^3 + 255.12(1.73)^2 - \left(\frac{2(.75)15.875^3 + 23.81(1.73)^2}{12} \right) - \left(\frac{12.5(.875)^3 + 6.125(5.772)^2}{12} \right) - \left(\frac{1}{12} 11.44(15)^3 + 171.6(2.7)^2 \right)$$

$$\bar{I}_3 = 1620 \text{ in}^4$$

$$\bar{I}_2 = \frac{1}{12} 16.94(15.06)^3 - \left(\frac{2}{12}(15.875).75^3 + 23.81(6.625)^2 \right) - \frac{1}{12} (.875)12.5^3 - \frac{1}{12} 15(11.44)^3$$

$$\bar{I}_2 = 1762 \text{ in}^4$$

$$\text{Area} = \frac{48.77}{.707} = 68.98 \quad P_{\max} = 7979 \text{ lbs.}$$

$$\frac{P}{A} = \frac{7979}{68.98} = 116 \text{ psi} < 8750 \text{ psi} = .5 S$$

The stress on the effective throat of the fillet weld is required to meet the limits of Table NF-3292.1-1 of Ref. (9).

For SA-515 Gr 70 $S_{UT} = 70 \text{ ksi}$

$$\tau_{WELD MAX} = 21 \text{ ksi}$$

Taking all stresses as shear

$$\tau_{MAX(1)} = \left[\left(\frac{V_2}{A} \right)^2 + \left(\frac{M_2 C_3}{I_2} + \frac{P}{A} + \frac{M_3 C_2}{I_3} + \frac{V_3}{A} \right)^2 \right]^{1/2}$$

NOTE: M_T is negligible and neglected

$$\tau_{MAX(1)} = \left[\left(\frac{38144}{48.77} \right)^2 + \left(\frac{18653(7.53)}{1762} + \frac{7979}{48.77} + \frac{195490(9.26)}{1620} + \frac{1816}{48.77} \right)^2 \right]^{1/2}$$

$$\tau_{MAX(1)} = \left(782^2 + (80 + 163 + 1117 + 37) \right)^{1/2}$$

$$\tau_{MAX(1)} = 1601 \text{ psi}$$

$$\tau_{MAX(2)} = \left[\left(\frac{V_3}{A} \right)^2 + \left(\frac{M_2 C_3}{I_2} + \frac{P}{A} + \frac{M_3 C_2}{I_3} + \frac{V_2}{A} \right)^2 \right]^{1/2}$$

$$\tau_{MAX(2)} = \left(37^2 + (80 + 163 + 1117 + 782) \right)^{1/2}$$

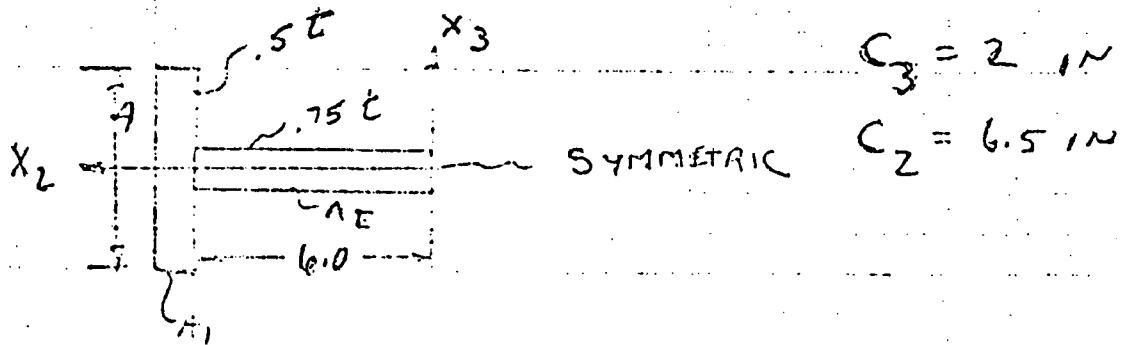
$$\tau_{MAX(2)} = 2142 \text{ psi} < 21,000 \text{ psi}$$

Therefore the support weld is OK

SEISMIC LUG STRESSES

THE SEISMIC LUG CONFIGURATION INPUT INTO "STARODYNE" WAS INCORRECTLY ORIENTED (X_2 AND X_3 DIRECTIONS WERE INVERTED). THE INVERTING OF AXES WILL HAVE LITTLE EFFECT ON THE REST OF THE STRUCTURE DUE TO THE REMOTENESS OF THE LUGS FROM THE SUPPORTS. THIS AXIS INVERSION WILL ALSO HAVE INSIGNIFICANT RESULTS ON THE FREQUENCY ANALYSIS. FOR PRIMARY LOCAL MEMBRANE PLUS BENDING CONSIDERATIONS, TWO END PLATES WERE ADDED TO THE SEISMIC LUGS, SEE SECTION(6.4). THIS NEW CROSS SECTION WILL BE ANALYZED FOR STRESSES USING THE LOADS FROM "COMBINE"

SECTION PROPERTIES



AREA

$$A = 2(A_1 + A_2)$$

$$A_1 = 4(6.5) = 26$$

$$A_2 = .75(6) = 4.5$$

$$A = 13 \text{ in}^2$$

POLAR MOMENT OF INERTIA, J

$$J = 2\left[\frac{1}{3}(0.5)(4)\right] + \frac{1}{3}(0.75)^3(12)$$

$$J = 2021 \text{ in}^4$$

MOMENT OF INERTIA, I_2

$$I_2 = 2 \cdot \frac{1}{12}(4)(0.5)^3 + \frac{1}{12}(0.75)^3(12)$$

$$I_2 = 5.755 \text{ in}^4$$

MOMENT OF INERTIA, I_3

$$I_3 = 2\left(\frac{1}{12}(4)(0.5)^3 + (6.25)^2(2)\right) + \frac{1}{12}(12)(0.75)^3$$

$$I_3 = 264 \text{ in}^4$$

THE MAXIMUM "COMBINE" LOADS ARE

P	V_2	V_3	M_T	M_2	M_3
41878	0	7213	362	26705	235

GENERAL MEMBRANE STRESS

SHEAR STRESS

$$\tau = \frac{V}{A} + \frac{TC}{J} \quad V = 7213$$

$$A = 13$$

$$\tau = \frac{7213}{13} + \frac{362(.75)}{2.021} \quad T = 362$$

$$\tau = 689 \text{ psi}$$

$$C = .75$$

$$J = 2.021$$

NORMAL STRESS

$$\sigma_p = \frac{P}{A} = \frac{41878}{13}$$

$$\sigma_p = 3221 \text{ psi}$$

CALCULATING σ_{max}

$$\sigma_{max} = \frac{3221}{2} + \left(\left(\frac{3221}{2} \right)^2 - (689)^2 \right)^{\frac{1}{2}}$$

$$\sigma_{max} = 3363 \text{ psi} < 17500 \text{ psi} = 1.05$$

GENERAL MEMBRANE PLUS BENDING

NORMAL STRESS DUE TO M_2

$$\sigma_{M_2} = \pm \frac{26705(2)}{5.755} = \pm 9281 \text{ psi}$$

NORMAL STRESS DUE TO M_3

$$\sigma_{M_3} = \pm \frac{235(6.5)}{264} = 6 \text{ psi}$$

COMBINE σ_n , σ_{n2} & σ_{n3}

$$\sigma = 3221 + 9281 - 6 = 12508 \text{ psi}$$

$$\tau = 689 \text{ psi}$$

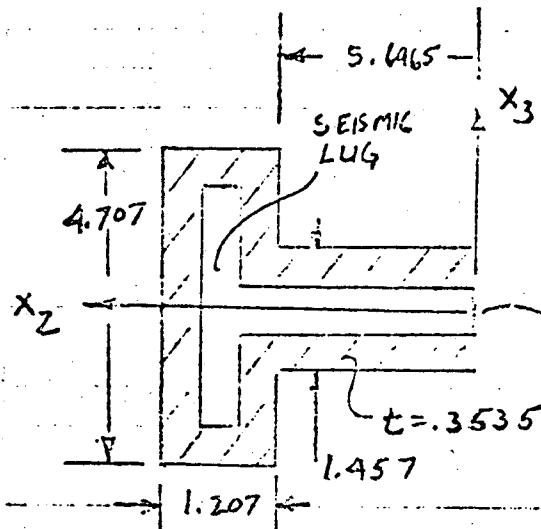
$$\sigma_{\max} = \frac{12508}{2} + \left(\left(\frac{12508}{2} \right)^2 + 689^2 \right)^{\frac{1}{2}}$$

$$\sigma_{\max} = 12546 \text{ psi} < 26250 \text{ psi} = 1.5 S$$

SEISMIC LUG WELD STRESS

SECTION PROPERTIES

THICKNESS



$$t = .707(.5) = .3535$$

$$C_2 = 6.8535$$

$$C_3 = 2.3535$$

SYMMETRIC

AREA

$$A = A_{\text{TOTAL}} - A_{\text{LUG}}$$

$$A_{\text{TOTAL}} = 2(4 + 2(.3535))(.5 + 2(.3535)) \\ + ((12 - 2(.3535))(.75 + 2(.3535))) = 27.82 \text{ m}^2$$

$$A = 27.82 - 13 = 14.82 \text{ m}^2$$

MOMENT OF INERTIA, I_2

$$I_2 = I_{2\text{TOTAL}} - I_{2\text{LUG}}$$

$$I_{2\text{TOTAL}} = 2 \cdot \frac{1}{12} (4.707)^3 (1.207) + \frac{1}{12} (1.457)^3 (11.293)$$

$$I_{2\text{TOTAL}} = 23.89 \text{ m}^4$$

$$I_2 = 23.89 - 5.76 = 18.13 \text{ m}^4$$

MOMENT OF INERTIA, I_3

$$I_3 = I_{3\text{TOTAL}} - I_{3\text{LUG}}$$

$$I_{3\text{TOTAL}} = 2 \left(\frac{1}{12} (4.707) (1.207)^3 + (6.25)^2 (5.68) \right) \\ + \frac{1}{12} (11.293)^3 (1.457)$$

$$I_{3\text{TOTAL}} = 620 \text{ in}^4$$

$$I_3 = 620 - 264 = 356.1 \text{ in}^4$$

THE STRESS ON THE THROUGH THICKNESS

OF THE AREA UNDER THE WELD IS

REQUIRED TO MEET .5 S PER PARA NF-3351.1

REF(9)

$$\text{so } \text{AREA} = \frac{14.82}{1.707} = 20.96 \text{ in}^2$$

$$P_{\text{MAX}} = 41878 \text{ LBS}$$

$$\frac{P}{A} = \frac{41878}{20.96} = 1998 \text{ psi} < 8750 = .5 S$$

THE STRESS ON THE EFFECTIVE THROAT OF
FILLET WELD IS REQUIRED TO MEET THE
LIMITS OF TABLE NF - 3292.1-1. REF(9)

so FOR SA 515 GR70 . SURF = 70 KSI

$$T_{\text{WELD MAX}} \leq 21 \text{ KSI}$$

8	5234.	-1148.	-650.
9	3056.	-11173.	-650.
10	3056.	-12523.	-650.
11	16552.	11305.	.
12	14954.	11297.	.
13	3062.	-11853.	-650.
14	3053.	-11845.	-650.
15	15773.	11282.	.
16	15738.	11316.	.

THE RESULTING STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	8225.	1415.	-9639.
2	8221.	1417.	-9638.
3	3605.	2773.	-6379.
4	2838.	5059.	-7897.
5	10716.	-1889.	-8827.
6	10713.	-1888.	-8825.
7	5401.	1544.	-6945.
8	6392.	-498.	-5884.
9	14229.	-10523.	-3706.
10	15579.	-11873.	-3706.
11	5246.	11305.	-16552.
12	3656.	11297.	-14954.
13	14915.	-11203.	-3712.
14	14398.	-11195.	-3703.
15	4491.	11282.	-15773.
16	4422.	11316.	-15738.

C.2-15

NOZZLES N3 + N4 LOAD CASE 2

KOPT	KTYPE	KBETA	KUEF				
3	1	*	*				
KEY1	KEY2	KEY3	KEY4	KEY5			
*	*	*	*	*			
SM1 17500.	SM2 15000.	P 150.	TN .3750	TV 1.5000	RN 8.0000	RMV 28.2500	
GAMMA 18.83	BETA .2478						
X .0000	Y 7.7500	Z .0000					
A1 .09495	A2 .07266	A3 .80504	A4 .08500	A5 .05920	A6 .03123		
B1 2.80574	B2 .04293	B3 1.39830	B4 .04346	B5 .77124	B6 .05169		

C-2-16

OPTION THREE OF PROGRAM NOZZLE

FOR THE FORCES(POUNDS) AND MOMENTS(POUND-INCHES)

	FX	FY	FZ	MX	MY	MZ
		5523.	5523.	210300.	210300.	

THE PRIMARY STRESSES IN THE VESSEL AND NOZZLE ARE

LOCATION	SX	SY	TGX	TGY	TGX
1	-125.	7396.	-75.	495.	
2	-125.	7396.	-75.	202.	
3	4884.	508.	-75.	349.	
4	7270.	1881.	-75.	349.	
5	-125.	7396.	-75.	495.	
6	-125.	7396.	-75.	202.	
7	4884.	508.	-75.	349.	
8	7270.	1881.	-75.	349.	
9	5380.	6309.	-75.	1461.	
10	-1655.	6309.	-75.	1461.	
11	5380.	6309.	-75.	1461.	
12	-1655.	6309.	-75.	1461.	
13	1863.	6309.	-75.	2062.	
14	1863.	6309.	-75.	861.	
15	1863.	6309.	-75.	2062.	
16	1863.	6309.	-75.	861.	

THE RESULTING PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	7429.	-158.	-75.
2	7402.	-131.	-75.
3	4911.	480.	-75.
4	7292.	1859.	-75.
5	7429.	-158.	-75.
6	7402.	-131.	-75.
7	4911.	480.	-75.
8	7292.	1859.	-75.

C.2-17

C-2-17

4	7292.	1859.	-75.
5	7429.	-158.	-75.
6	7402.	-131.	-75.
7	4911.	480.	-75.
8	7292.	1859.	-75.
9	7378.	4311.	-75.
10	6569.	-1915.	-75.
11	7378.	4311.	-75.
12	6569.	-1915.	-75.
13	7118.	1054.	-75.
14	6470.	1701.	-75.
15	7118.	1054.	-75.
16	6470.	1701.	-75.

THE RESULTING STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	7586.	-83.	-7504.
2	7532.	-56.	-7477.
3	4431.	555.	-4986.
4	5433.	1934.	-7367.
5	7586.	-83.	-7504.
6	7532.	-56.	-7477.
7	4431.	555.	-4986.
8	5433.	1934.	-7367.
9	3067.	4386.	-7453.
10	8484.	-1840.	-6644.
11	3067.	4386.	-7453.
12	8484.	-1840.	-6644.
13	6064.	1129.	-7193.
14	4769.	1776.	-6545.
15	6064.	1129.	-7193.
16	4769.	1776.	-6545.

C-2-18

THE TOTAL STRESSES IN THE VESSEL AND NOZZLE ARE

LOCATION	SX	SO	SY	TOX
1	1382.	8729.	.	495.
2	1382.	8729.	.	202.
3	1588.	-5743.	.	349.
4	12355.	12023.	.	349.
5	-1633.	6064.	-150.	495.
6	-1633.	6064.	-150.	202.
7	8179.	6758.	-150.	349.
8	2184.	-8250.	-150.	349.
9	-2708.	2108.	-150.	1426.
10	-15575.	2108.	-150.	1426.
11	19469.	10510.	.	1497.
12	12264.	10510.	.	1497.
13	-12141.	2108.	-150.	2026.
14	-12141.	2108.	-150.	826.
15	15866.	10510.	.	2097.
16	15866.	10510.	.	896.

THE RESULTING PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	8762.	1349.	.
2	8735.	1377.	.
3	1604.	-5759.	.
4	12575.	11803.	.
5	6095.	-1664.	-150.
6	6069.	-1638.	-150.
7	8260.	6677.	-150.
8	2196.	-8271.	-150.
9	2293.	-8893.	-150.
10	2223.	-15689.	-150.
11	19712.	10267.	.

C 2-19

1	7413.	1349.	-150.
2	7358.	1377.	-150.
3	7364.	-5759.	-1604.
4	773.	11803.	-12575.
5	7760.	-1514.	-6245.
6	7707.	-1489.	-6219.
7	1583.	6827.	-8410.
8	10467.	-8121.	-2346.
9	11186.	-8743.	-2443.
10	17912.	-15539.	-2373.
11	9445.	10267.	-19712.
12	3469.	9653.	-13122.
13	14815.	-12274.	-2541.
14	14345.	-12039.	-2306.
15	6802.	9787.	-16589.
16	5648.	10364.	-16012.

THE RESULTING STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	7413.	1349.	-8762.
2	7358.	1377.	-8735.
3	7364.	-5759.	-1604.
4	773.	11803.	-12575.
5	7760.	-1514.	-6245.
6	7707.	-1489.	-6219.
7	1583.	6827.	-8410.
8	10467.	-8121.	-2346.
9	11186.	-8743.	-2443.
10	17912.	-15539.	-2373.
11	9445.	10267.	-19712.
12	3469.	9653.	-13122.
13	14815.	-12274.	-2541.
14	14345.	-12039.	-2306.
15	6802.	9787.	-16589.
16	5648.	10364.	-16012.

Appendix C.3

LOCAL SUPPORT STRESS OUTPUT

SUPPORT/VESSEL JUNCTION

KOPT KTYPE KBETA KOEF

3 3 *

KEY1 KEY2 KEY3 KEY4 KEY5

SM P RM T TWOCl TWOc2

17500. 150. 22.5600 .8750 15.0000 15.8750

GAMMA BETA1 BETA2 BETA1/BETA2

25.78 .3024 .3518 .9449

X Y Z

-.0000 -.0000 -.0000

A1 A2 A3 A4 A5 A6

1.51182 .04062 1.06291 .06715 2.06837 .01814

B1 B2 B3 B4 B5 B6

2.94407 .01808 2.41481 .02949 1.02545 .03076

SHELL STRESSES DUE TO FORCES APPLIED TO A RECTANGULAR ATTACHMENT AND INTERNAL PRESSURE

THE TOTAL APPLIED LOADS ARE

FX	FY	FZ	MX	MY	MZ
38144.	7979.	-1816.	1d653.	70.	-195490.

VESSEL PRIMARY STRESSES

LOCATION	SX	SO	SY	TOX
1	2184.	5629.	-75.	-69.
2	2184.	5629.	-75.	-69.
3	-696.	884.	-75.	69.
4	-696.	884.	-75.	69.
5	1065.	3410.	-75.	-1373.
6	1065.	3410.	-75.	-1373.
7	423.	3103.	-75.	1373.
8	423.	3103.	-75.	1373.

THE RESULTING MEMBRANE PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	5630.	2182.	-75.
2	5630.	2182.	-75.
3	887.	-699.	-75.
4	887.	-699.	-75.
5	4043.	432.	-75.
6	4043.	432.	-75.
7	3682.	-156.	-75.
8	3682.	-156.	-75.

THE MEMBRANE STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	3448.	2257.	-5705.
2	3448.	2257.	-5705.

C.3-2

C.2

ACTION	S12	S23	S31
1	3448.	2257.	-5705.
2	3448.	2257.	-5705.
3	1587.	-624.	-962.
4	1587.	-624.	-962.
5	3611.	507.	-4118.
6	3611.	507.	-4118.
7	3837.	-81.	-3757.
8	3837.	-81.	-3757.

C.3-3

SHELL STRESSES DUE TO FORCES APPLIED TO A RECTANGULAR ATTACHMENT AND INTERNAL PRESSURE

PRIMARY PLUS SECONDARY VESSEL STRESSES

LOCATION	SX	SY	T0A
1	6809.	6824.	-69.
2	-2442.	4433.	-150.
3	-7583.	-5391.	69.
4	6191.	7159.	-150.
5	419.	2099.	-1373.
6	1710.	4721.	-150.
7	-1194.	-666.	1373.
8	2039.	5872.	-150.

THE RESULTING PRIMARY PLUS SECONDARY PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	6886.	6747.	•
2	4434.	-2442.	-150.
3	-5389.	-7586.	•
4	7164.	6186.	-150.
5	2868.	-350.	•
6	5253.	1178.	-150.
7	468.	-2328.	•
8	7235.	1676.	-150.

THE PRIMARY PLUS SECONDARY STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	139.	6747.	-6886.
2	6876.	-2292.	-4584.
3	2197.	-7586.	5389.
4	979.	6336.	-7314.
5	3219.	-350.	-2868.
6	4075.	1328.	-5403.

C 3-4

6	4974.	1324.	-5403.
7	2796.	-2328.	-468.
8	5558.	1826.	-7385.

1.5 SM = 26250. 3.0 SM = 52500.

SEISMIC LUG/ VESSEL JUNCTION

KOPT	KTYPE	KBETA	KOEF
3	3	*	*

KEY1	KEY2	KEY3	KEY4	KEY5
*	*	*	*	*

SM	P	R _M	T	TWOC1	TWOC2
17500.	150.	28.0000	1.0000	4.0000	13.0000

GAMMA	BETA1	BETA2	BETA1/BETA2
28.00	.0714	.2321	.3077

X	Y	Z
-.0000	-.0000	-.2000

A1	A2	A3	A4	A5	A6
3.42188	.13118	.78337	.09439	3.11599	.04217

B1	B2	B3	B4	B5	B6
4.63331	.06432	1.10778	.04494	1.00449	.05379

C 3-5

SWELL STRESSES DUE TO FORCES APPLIED TO A RECTANGULAR ATTACHMENT AND INTERNAL PRESSURE

THE TOTAL APPLIED LOADS ARE

FX	FY	FZ	MX	MY	MZ
41878.		-7213.	26705.	362.	-235.

VESSEL PRIMARY STRESSES

LOCATION	SX	SY	T0X
1	-4835.	-914.	-75.
2	-4835.	-914.	-75.
3	-4840.	-922.	-75.
4	-4840.	-922.	-75.
5	-4644.	-827.	-75.
6	-4644.	-827.	-75.
7	-5031.	-1009.	-75.
8	-5031.	-1009.	-75.

THE RESULTING MEMBRANE PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	-716.	-5032.	-75.
2	-716.	-5032.	-75.
3	-725.	-5037.	-75.
4	-725.	-5037.	-75.
5	-827.	-4644.	-75.
6	-827.	-4644.	-75.
7	-1009.	-5031.	-75.
8	-1009.	-5031.	-75.

THE MEMBRANE STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	4316.	-4957.	641.
2	4316.	-4957.	641.
3	4312.	-4962.	650.

C.3-6

	4316.	-4957.	641.
1	4316.	-4957.	641.
2	4316.	-4957.	641.
3	4312.	-4962.	650.
4	4312.	-4962.	650.
5	3817.	-4569.	752.
6	3817.	-4569.	752.
7	4022.	-4956.	934.
8	4022.	-4956.	934.

C.3-7

SHELL STRESSES DUE TO FORCES APPLIED TO A RECTANGULAR ATTACHMENT AND INTERNAL PRESSURE

PRIMARY PLUS SECONDARY VESSEL STRESSES

LOCATION	SX	SO	SY	T0A
1	-20981.	-33859.	.	-902.
2	11312.	32032.	-150.	-902.
3	-21015.	-33898.	.	902.
4	11336.	32053.	-150.	902.
5	-19361.	-29679.	.	-.
6	10074.	28026.	-150.	-.
7	-22636.	-38078.	.	-.
8	12574.	36060.	-150.	-.

THE RESULTING PRIMARY PLUS SECONDARY PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	-20919.	-33922.	.
2	32071.	11272.	-150.
3	-20953.	-33961.	.
4	32092.	11297.	-150.
5	-19361.	-29679.	.
6	28026.	10074.	-150.
7	-22636.	-38078.	.
8	36060.	12574.	-150.

THE PRIMARY PLUS SECONDARY STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	13003.	-33922.	20919.
2	20799.	11422.	-32221.
3	13008.	-33961.	20953.
4	20795.	11447.	-32242.
5	10318.	-29679.	19361.
6	17952.	10224.	-28176.

C 3-8

3	13008.	-33961.	20953.
4	20795.	11447.	-32242.
5	10318.	-29679.	19361.
6	17952.	10224.	-28176.
7	15442.	-38078.	22636.
8	23486.	12724.	-36210.

1.5 SM = 26250. 3.0 SM = 52500.

C 3-9

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EARTHQUAKE 2 • NOZZLE LOADS • DEADWEIGHT EFCU-2

HEAM ELEMENT LOADS

NOZZLE LOADS • EARTHQUAKE NO. 1 • DEADWEIGHT

BEAM	NODE	AXIAL V1	SHEAR V2	SHEAR V3	BENDING M2	BENDING M3	TORSION MT
1	1 JA	.10775E+05	-.3540E+04	.43540E+04	.0	.0	.0
1	4 JB	-.10775E+05	.3540E+04	-.43540E+04	.12300E+00	.12300E+00	.0
2	3 JA	.29520E+04	.0	-.29520E+04	.26745E+05	.90300E+05	.90300E+05
2	2 JB	-.29520E+04	.0	.29520E+04	.0	.90300E+05	.90300E+05
3	3 JA	.29520E+04	.0	-.29520E+04	.26745E+05	.90300E+05	.90300E+05
3	4 JB	-.29520E+04	.0	.29520E+04	.96675E+05	.90300E+05	.90300E+05
4	4 JA	.29520E+04	.0	-.29520E+04	.96675E+05	.90300E+05	.90300E+05
4	5 JB	-.29520E+04	.0	.29520E+04	.26745E+05	.90300E+05	.90300E+05
5	5 JA	.29520E+04	.0	-.29520E+04	.26745E+05	.90300E+05	.90300E+05
5	6 JB	-.29520E+04	.0	.29520E+04	.0	.90300E+05	.90300E+05
6	4 JA	.10775E+05	.10253E+05	-.10253E+05	.30360E+05	.30360E+05	.0
6	7 JB	-.10775E+05	.10253E+05	-.10253E+05	.53184E+06	.53184E+06	.0
7	7 JA	.23602E+05	.13767E+05	-.13767E+05	.53184E+06	.53184E+06	.0
7	8 JB	-.23602E+05	.13767E+05	-.13767E+05	.56428E+06	.66428E+06	.0
8	8 JA	.31620E+05	.15765E+05	-.15765E+05	.66428E+06	.66428E+06	.0
8	9 JB	-.31620E+05	.15765E+05	-.15765E+05	.88499E+06	.88499E+06	.0
9	10 JA	.55220E+04	.0	-.55220E+04	.43189E+05	.21029E+06	.21029E+06
9	11 JB	-.55220E+04	.0	.55220E+04	.0	.21029E+06	.21029E+06
10	10 JA	.55220E+04	.0	-.55220E+04	.43189E+05	.21029E+06	.21029E+06
10	11 JB	-.55220E+04	.0	.55220E+04	.19884E+06	.21029E+06	.21029E+06
11	11 JA	.31620E+05	.12777E+05	-.12777E+05	.16521E+05	.11670E+07	.87398E+06
11	12 JB	-.31620E+05	.12777E+05	-.12777E+05	.16521E+05	.93565E+06	.59510E+06
12	12 JA	.52191E+05	.91450E+04	-.91450E+04	.12890E+05	.93565E+06	.69510E+06
12	13 JB	-.52191E+05	.91450E+04	-.91450E+04	.12890E+05	.33624E+06	.26980E+06
13	13 JA	.38144E+05	.76890E+04	-.76890E+04	.12800E+03	.63700E+03	-.20564E+05
13	14 JB	-.38144E+05	.76890E+04	-.76890E+04	.12800E+03	.50000E+02	.15688E+06
14	15 JA	.76890E+04	.38144E+05	-.38144E+05	.12800E+03	.70100E+04	.19549E+06
14	14 JB	-.76890E+04	.38144E+05	-.38144E+05	.12800E+03	.75470E+04	.16688E+06
15	15 JA	.76890E+04	-.38144E+05	.38144E+05	.12800E+03	.70100E+04	.19549E+06
15	16 JB	-.76890E+04	-.38144E+05	.38144E+05	.12800E+03	.56200E+04	-.10537E+07
							.50000E+02

B, 2-9a

EARTHQUAKE

BEAM ELEMENT LOADS

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NOZZLE LOADS • EARTHQUAKE NO. 1 • DEADWEIGHT

BEAM NO	NODE	AXIAL P	SHEAR V2	SHEAR V3	BENDING M2	BENDING M3	TORSION MT
16	16 JA	.77210E+04	.31459E+05	.14300E+04	.45994E+05	.85620E+06	.50000E+02
16	17 JB	-.77210E+04	-.31459E+05	.14300E+04	.13801E+05	-.14838E+06	.50000E+02
17	17 JA	.77210E+04	.31459E+05	.14300E+04	.13801E+05	.14838E+06	.50000E+02
17	18 JB	-.77210E+04	-.31459E+05	.14300E+04	.74700E+03	.15989E+06	.50000E+02
18	19 JA	-.31459E+05	-.77210E+04	.14300E+04	.71900E+04	-.16445E+06	.74700E+03
18	18 JB	-.31459E+05	-.77210E+04	.14300E+04	.50000E+02	.15989E+06	.74700E+03
19	20 JA	.30099E+05	.51020E+04	.44700E+03	.21920E+04	-.15020E+06	.95030E+04
19	21 JB	-.30099E+05	-.51020E+04	.44700E+03	.70000E+02	.16089E+06	.95030E+04
20	22 JA	.51020E+04	.20099E+05	.44700E+03	.52570E+04	.13646E+06	.70000E+02
20	21 JB	-.51020E+04	-.20099E+05	.44700E+03	.95030E+04	.16089E+06	.70000E+02
21	22 JA	.51020E+04	-.30099E+05	.44700E+03	.52570E+04	.13646E+06	.70000E+02
21	15 JB	-.51020E+04	-.30099E+05	.44700E+03	.53400E+04	-.81366E+06	.70000E+02
22	16 JA	-.50700E+04	.36784E+05	.18160E+04	.56414E+05	.10112E+07	.70000E+02
22	23 JB	-.50700E+04	-.36784E+05	.18160E+04	.15554E+05	-.18356E+06	.70000E+02
23	23 JA	.50700E+04	.36784E+05	.18160E+04	.15554E+05	.18356E+06	.70000E+02
23	24 JB	-.50700E+04	-.36784E+05	.18160E+04	.16980E+04	.16588E+06	.70000E+02
24	25 JA	-.36784E+05	-.50700E+04	.18160E+04	.91190E+04	-.19139E+06	.16980E+04
24	24 JB	-.36784E+05	-.50700E+04	.18160E+04	.70000E+02	.16588E+06	.16980E+04
25	3d JA	-.55701E+05	.28270E+04	.50890E+04	.12011E+06	.63768E+05	.23106E+05
25	25 JB	.55701E+05	-.28270E+04	.50890E+04	.22690E+06	.12896E+06	.23106E+05
26	26 JA	-.33456E+05	.24560E+04	.47180E+04	.22690E+06	.12896E+06	.23106E+05
26	27 JB	.33456E+05	-.24560E+04	.47180E+04	.42104E+06	.15613E+06	.23106E+05
27	27 JA	-.18155E+05	.59440E+04	.92060E+04	.42164E+06	.15613E+06	.23106E+05
27	30 JB	.18155E+05	-.59440E+04	.92060E+04	.55053E+06	.25334E+06	.23106E+05
28	29 JA	.55220E+04	.55230E+04	.0	.0	.25349E+06	.21029E+06
28	29 JB	.55220E+04	-.55230E+04	.0	.0	.21029E+06	.21029E+06
29	29 JA	.55220E+04	.55230E+04	.0	.0	.25349E+06	.21029E+06
29	30 JB	.55220E+04	-.55230E+04	.0	.0	.40915E+06	.21029E+06
30	30 JA	.12133E+05	.0	.10940E+04	.28859E+05	.43000E+02	.19700E+03
30	31 JB	.12133E+05	.0	.10940E+04	.55960E+04	.43000E+02	.19700E+03

HEAM ELEMENT LOADS

NOZZLE LOADS - EARTHQUAKE NO. 1 + DEADWEIGHT

BEAM	NODE	AXIAL 10	SHEAR V2	SHEAR V3	BENDING M2	BENDING M3	TORSION MT
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31	31 JA	.1<133E+05	.0	.10940E+04	.55950E+04	.43000E+02	.19700E+03
31	32 JB	.1<133E+05	.0	.10940E+04	.61490E+04	.43000E+02	.19700E+03
32	30 JA	.11+12E+05	.0	.13320E+04	.34513E+05	.12800E+03	.67000E+02
32	33 JB	.11+12E+05	.0	.13320E+04	.46710E+04	.12800E+03	.67000E+02
33	33 JA	.11412E+05	.0	.13320E+04	.46710E+04	.12800E+03	.67000E+02
33	34 JB	.11412E+05	.0	.13320E+04	.80930E+04	.12800E+03	.67000E+02
34	36 JA	-12632E+05	.46350E+04	.46350E+04	.11282E+06	.11282E+06	.0
34	35 JB	-12632E+05	.46350E+04	.46350E+04	.47934E+05	.47934E+05	.0
35	35 JA	-42170E+04	.17040E+04	.17040E+04	.47934E+05	.47934E+05	.0
35	36 JB	.42170E+04	.17040E+04	.17040E+04	.0	.0	.0
36	37 JA	.52191E+05	.91460E+04	.12490E+05	.33624E+06	.26980E+06	.12633E+06
36	15 JB	.52191E+05	.91460E+04	.12490E+05	.11942E+06	.11595E+06	.12633E+06
37	16 JA	-55701E+05	.28270E+04	.50890E+04	.17701E+06	.95367E+05	.23106E+05
37	38 JB	.55701E+05	.28270E+04	.50890E+04	.12011E+06	.63768E+05	.23106E+05
38	11 JA	.33169E+05	.44300E+03	.32500E+04	.81009E+05	.12449E+05	.48200E+03
38	39 JB	.33169E+05	.44300E+03	.32500E+04	.89920E+04	.17800E+03	.48200E+03
39	39 JA	.33164E+05	.0	.32500E+04	.89980E+04	.17800E+03	.36200E+03
39	49 JB	.33164E+05	.0	.32500E+04	.23005E+05	.17800E+03	.36200E+03
40	11 JA	.36643E+05	.49200E+03	.70300E+04	.21105E+06	.13869E+05	.61500E+03
40	41 JB	.36643E+05	.49200E+03	.70300E+04	.25520E+05	.23500E+03	.61500E+03
41	41 JA	.36647E+05	.0	.70300E+04	.25526E+05	.23500E+03	.27400E+03
41	42 JB	.36647E+05	.0	.70300E+04	.13928E+05	.23500E+03	.27400E+03

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EARTHQUAKE 2 • NOZZLE LOADS • DEADWEIGHT EFCU-2

BEAM ELEMENT STRESSES

NOZZLE LOADS • EARTHQUAKE NO. 1 • DEADWEIGHT

SEG	NODE	AXIAL P/A	SHEAR V2/A	SHEAR V3/A	BENDING M2*C/12	BENDING M3*C/13	TORSION T*C/J
1	1 JA	.60297E+02	.24365E+02	.24365E+02	.0	.0	.0
1	4 JB	-.60297E+02	-.24365E+02	-.24365E+02	.62134E+02	.62134E+02	.0
2	3 JA	.22919E+03	.0	.22919E+03	.68625E+03	.23170E+04	.11545E+04
2	2 JB	.22919E+03	.0	.22919E+03	.0	.23170E+04	.11535E+04
3	3 JA	.59040E+01	.0	.59040E+01	.66862E-01	.22575E+00	.22575E+00
3	4 JB	-.59040E+01	-.0	-.59040E+01	-.24169E+00	-.22575E+00	-.22575E+00
4	4 JA	.59040E+01	.0	.59040E+01	.24169E+00	.22575E+00	.22575E+00
4	5 JB	.59040E+01	.0	.59040E+01	.66862E-01	.22575E+00	.22575E+00
5	5 JA	.22919E+03	.0	.22919E+03	.68625E+03	.23170E+04	.11545E+04
5	6 JB	-.22919E+03	-.0	-.22919E+03	-.0	-.23170E+04	-.11535E+04
6	4 JA	.60297E+02	.57403E+02	.57403E+02	.15336E+03	.15336E+03	.0
6	7 JB	-.60297E+02	-.57403E+02	-.57403E+02	.26866E+03	.26866E+03	.0
7	7 JA	.33765E+03	.19695E+03	.19695E+03	.69150E+03	.69150E+03	.0
7	8 JB	-.33765E+03	-.19695E+03	-.19695E+03	.86370E+03	.86370E+03	.0
8	8 JA	.29097E+03	-.14503E+03	-.14503E+03	.44624E+03	.44624E+03	.0
8	11 JB	-.29097E+03	-.14503E+03	-.14503E+03	.59451E+03	.59451E+03	.0
9	10 JA	.22673E+03	.0	.22632E+03	.47205E+03	.22985E+04	.11492E+04
9	9 JB	-.22673E+03	-.0	-.22632E+03	-.0	-.22985E+04	-.11492E+04
10	10 JA	.11044E+02	.0	.11046E+02	.10794E+00	.52573E+00	.52573E+00
10	11 JB	.11044E+02	.0	.11046E+02	.49711E+00	.52573E+00	.52573E+00
11	11 JA	.29097E+03	.11754E+03	.15199E+03	.78392E+03	.58711E+03	.42434E+02
11	12 JB	-.29097E+03	-.11754E+03	-.15199E+03	.62854E+03	.46694E+03	.42434E+02
12	12 JA	.74065E+03	.13984E+03	.18441E+03	.12165E+04	.90377E+03	.82132E+02
12	13 JB	-.74065E+03	-.13984E+03	-.18441E+03	.43715E+03	.35079E+03	.82132E+02
13	13 JA	.76288E+02	.15376E+02	.25600E+00	.15925E-02	-.51411E+00	.18992E-01
13	14 JB	-.76288E+02	-.15376E+02	-.25600E+00	.12500E-03	.41720E+00	.18992E-01
14	15 JA	.22421E+03	.11124E+04	.37329E+01	.22353E+02	.12021E+04	.59768E+01
14	14 JB	-.22421E+03	-.11124E+04	-.37329E+01	.24225E+02	.10262E+04	.59768E+01
15	15 JA	.15376E+02	-.76288E+02	-.25600E+00	.17525E-01	.48471E+00	.12500E-03
15	16 JB	-.15376E+02	-.76288E+02	-.25600E+00	.14050E-01	-.26343E+01	-.12500E-03

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BEAM ELEMENT STRESSES							
NOZZLE LOADS + EARTHQUAKE NO. 1 + DEADWEIGHT							
BEAM NO	NODE	AXIAL P/A	SHEAR V2/A	SHEAR V3/A	BENDING M2°C/12	BENDING M3°C/13	TORSION T°C/J
16	16 JA	.15442E+02	.02918E+02	.28600E+01	.11498E+00	.21405E+01	.12500E-03
16	17 JB	-.15442E+02	-.62918E+02	.28600E+01	.34502E-01	-.37095E+00	.12500E-03
17	17 JA	.22517E+03	.91744E+03	.41703E+02	.44008E+02	.91245E+03	.59768E+01
17	18 JB	-.22517E+03	-.91744E+03	.41703E+02	.23840E+01	.98322E+03	.59768E+01
18	19 JA	.62918E+02	.15442E+02	.28600E+01	.17975E-01	-.41113E+00	.18675E-02
18	18 JB	-.62918E+02	-.15442E+02	.28600E+01	.12500E-03	.39973E+00	.18675E-02
19	20 JA	.60198E+02	.10204E+02	.89400E+00	.54800E-02	-.37550E+00	.23757E-01
19	21 JB	-.60198E+02	-.10204E+02	.89400E+00	.17500E-03	.40223E+00	.23757E-01
20	22 JA	.14877E+03	.87778E+03	.13036E+02	.16763E+02	.83914E+03	.83675E+01
20	21 JB	-.14877E+03	-.87778E+03	.13036E+02	.30303E+02	.98934E+03	.83675E+01
21	22 JA	.10204E+02	-.50198E+02	.89400E+00	.13142E-01	.34115E+00	.17500E-03
21	16 JB	-.10204E+02	-.50198E+02	.89400E+00	.13350E-01	-.20342E+01	.17500E-03
22	16 JA	.10140E+02	.73568E+02	.36320E+01	.14103E+00	.25280E+01	.17500E-03
22	23 JB	-.10140E+02	-.73568E+02	.36320E+01	.38845E-01	-.45491E+00	.17500E-03
23	23 JA	.14780E+03	.10727E+04	.52960E+02	.49598E+02	.11288E+04	.83675E+01
23	24 JB	-.14780E+03	-.10727E+04	.52960E+02	.54165E+01	.10291E+04	.93675E+01
24	25 JA	.73565E+02	.19140E+02	.36320E+01	.22794E-01	-.47448E+00	.42450E-02
24	24 JB	-.73565E+02	-.19140E+02	.36320E+01	.17500E-03	.41470E+00	.42450E-02
25	38 JA	-.79687E+03	-.0443E+02	.72804E+02	.15617E+03	.82911E+02	.15022E+02
25	25 JB	-.79687E+03	-.0443E+02	.72804E+02	.29502E+03	.16768E+03	.15022E+02
26	26 JA	-.47635E+03	.35136E+02	.67496E+02	.29502E+03	.16768E+03	.15022E+02
26	27 JB	-.47635E+03	.35136E+02	.67496E+02	.54821E+03	.20300E+03	.15022E+02
27	27 JA	-.16702E+03	.03882E+02	.84692E+02	.28324E+03	.10488E+03	.77609E+01
27	30 JB	-.16702E+03	.03882E+02	.84692E+02	.36933E+03	.17019E+03	.77609E+01
28	29 JA	.22675E+03	.22562E+03	.0	.0	.27706E+04	.11492E+04
28	28 JB	.22675E+03	.22562E+03	.0	.0	.22995E+04	.11492E+04
29	24 JA	.11044E+02	.11046E+02	.0	.0	.63372E+00	.52573E+00
29	30 JB	.11044E+02	.11046E+02	.0	.0	.10229E+01	.52573E+00
30	30 JA	.24255E+02	.0	.21880E+01	.72147E-01	.10750E-03	.49250E-03
30	31 JB	.24255E+02	.0	.213d0E+01	.13990E-01	.10750E-03	.49250E-03

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BEAM ELEMENT STRESSES

NOZZLE LOADS + EARTHQUAKE NO. 1 + DEADWEIGHT

BEAM #	NODE	Axial P/A	Shear V2/A	Shear V3/A	Bending M2°C/12	Bending M3°C/13	Torsion T°C/J
31	31 JA	-13481E+04	0	.12156E+03	.97153E+01	.30564E+03	.87530E+02
31	32 JB	.13481E+04	0	.12156E+03	.19675E+02	.30564E+03	.87530E+02
32	30 JA	.22324E+02	0	.26640E+01	.86282E-01	.32000E-03	.16750E-03
32	33 JB	.22324E+02	0	.26640E+01	.11677E-01	.32000E-03	.16750E-03
33	33 JA	.12580E+04	0	.14800E+03	.81094E+01	.90995E+03	.29704E+02
33	34 JB	.12580E+04	0	.14800E+03	.14059E+02	.90995E+03	.29704E+02
34	30 JA	-.11621E+03	.42640E+02	.42640E+02	.75791E+02	.75791E+02	0
34	35 JB	-.11621E+03	.42640E+02	.42640E+02	.32201E+02	.32201E+02	0
35	35 JA	-.6032E+02	.24378E+02	.24378E+02	.62324E+02	.62324E+02	0
35	36 JB	.6032E+02	.24378E+02	.24378E+02	0	0	0
36	37 JA	.30910E+03	.64682E+02	.91160E+02	.21601E+03	.17332E+03	.40579E+02
36	38 JB	-.30910E+03	.64682E+02	.91160E+02	.76717E+02	.74495E+02	.40579E+02
37	16 JA	-.39393E+03	.19993E+02	.35990E+02	.11371E+03	.61266E+02	.74218E+01
37	38 JB	.39393E+03	.19993E+02	.35990E+02	.77164E+02	.40966E+02	.74218E+01
38	11 JA	.60320E+02	.65600E+00	.65600E+01	.20252E+00	.31122E-01	.12050E-02
38	39 JB	.60320E+02	.65600E+00	.65600E+01	.22480E-01	.44500E-03	.12050E-02
39	39 JA	.36049E+04	0	.36111E+03	.15622E+02	.12654E+04	.16084E+03
39	40 JB	.36049E+04	0	.36111E+03	.39939E+02	.12654E+04	.16084E+03
40	11 JA	.73056E+02	.98400E+00	.14060E+02	.52704E+00	.34672E-01	.15375E-02
40	41 JB	.73056E+02	.98400E+00	.14060E+02	.63600E-01	.58750E-03	.15375E-02
41	41 JA	.40941E+04	0	.78111E+03	.44316E+02	.16706E+04	.12174E+03
41	42 JB	.40941E+04	0	.78111E+03	.24161E+02	.16706E+04	.12174E+03

5.2.14

EARTHQUAKE 2 + NOZZLE LOADS + DEADWEIGHT EFCU-2

ELEMENT TOTAL STRESSES AND MAXIMUM STRESS INTENSITY

NOZZLE LOADS + DEADWEIGHT + EARTHQUAKE NO 1

BEAM	NODE	PRESSURE AXIAL	PRESSURE HOOP	PRESSURE RADIAL	TOTAL AXIAL	TOTAL SHEAR	TOTAL AXIAL	MAXIMUM INTENSITY
1	1	.57150E+04	.11830E+05	-.32500E+03	.5953E+04	.34457E+02	.5847E+04	.12155E+05
1	4	.57150E+04	.11830E+05	-.32500E+03	.60623E+04	.34457E+02	.57577E+04	.12155E+05
2	3	.61159E+04	.12232E+05	-.32500E+03	.87611E+04	.13877E+04	.34707E+04	.13043E+05
2	2	.61159E+04	.12232E+05	-.32500E+03	.86621E+04	.13877E+04	.35697E+04	.13033E+05
3	3	.0	.0	.0	.59040E+01	.61297E+01	-.59040E+01	.13607E+02
3	4	.0	.0	.0	.59040E+01	.61297E+01	-.59040E+01	.13607E+02
4	4	.0	.0	.0	.59040E+01	.61297E+01	-.59040E+01	.13607E+02
4	5	.0	.0	.0	.59040E+01	.61297E+01	-.59040E+01	.13607E+02
5	5	.61159E+04	.12232E+05	-.32500E+03	.87611E+04	.13877E+04	.34707E+04	.13043E+05
5	6	.61159E+04	.12232E+05	-.32500E+03	.86621E+04	.13877E+04	.35697E+04	.13033E+05
6	4	.57150E+04	.11830E+05	-.32500E+03	.61913E+04	.81181E+02	.56387E+04	.12156E+05
6	7	.57150E+04	.11830E+05	-.32500E+03	.63543E+04	.81181E+02	.54757E+04	.12156E+05
7	7	.43375E+04	.66750E+04	-.75000E+02	.46522E+04	.27853E+03	.20228E+04	.67877E+04
7	8	.43375E+04	.66750E+04	-.75000E+02	.48962E+04	.27853E+03	.17748E+04	.67926E+04
8	8	.43325E+04	.66450E+04	-.75000E+02	.42445E+04	.20511E+03	.24005E+04	.67374E+04
8	11	.43325E+04	.66450E+04	-.75000E+02	.44535E+04	.20511E+03	.21915E+04	.67390E+04
9	10	.11625E+04	.23250E+04	-.75000E+02	.37353E+04	.13750E+04	-.14103E+04	.46513E+04
9	9	.11625E+04	.23250E+04	-.75000E+02	.36873E+04	.13750E+04	-.13623E+04	.46165E+04
10	10	.0	.0	.0	.11044E+02	.11572E+02	-.11044E+02	.25644E+02
10	11	.0	.0	.0	.12044E+02	.11572E+02	-.12044E+02	.26090E+02
11	11	.43325E+04	.66450E+04	-.75000E+02	.45925E+04	.23457E+03	.20525E+04	.67465E+04
11	12	.43325E+04	.66450E+04	-.75000E+02	.43965E+04	.23457E+03	.22485E+04	.67442E+04
12	12	.43375E+04	.66750E+04	-.75000E+02	.55992E+04	.30824E+03	.10759E+04	.68321E+04
12	37	.43375E+04	.66750E+04	-.75000E+02	.46442E+04	.30824E+03	.20398E+04	.67954E+04
13	13	.0	.0	.0	.76288E+02	.15397E+02	-.76288E+02	.82269E+02
13	14	.0	.0	.0	.76288E+02	.15397E+02	-.76288E+02	.82269E+02
14	15	.0	.0	.0	.14432E+04	.11184E+04	-.14432E+04	.26647E+04
14	14	.0	.0	.0	.12742E+04	.11184E+04	-.12742E+04	.25742E+04
15	15	.0	.0	.0	.15376E+02	.75239E+02	-.15376E+02	.15335E+03
15	16	.0	.0	.0	.17376E+02	.76239E+02	-.17376E+02	.15356E+03

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EARTHQUAKE 2 + NOZZLE LOADS + DEADWEIGHT EFCU-2

ELEMENT TOTAL STRESSES AND MAXIMUM STRESS INTENSITY

NOZZLE LOADS + DEADWEIGHT + EARTHQUAKE NU 1

STAN	NODE	PRESSURE AXIAL	PRESSURE RADIAL	PRESSURE HOOP	TOTAL AXIAL	TOTAL SHEAR	TOTAL AXIAL	MAXIMUM INTENSITY
15	15	.0	.0	.0	.17442E+02	.62983E+02	-.17442E+02	.12717E+03
16	17	.0	.0	.0	.15442E+02	.62983E+02	-.15442E+02	.12691E+03
17	17	.0	.0	.0	.11612E+04	.92436E+03	-.11612E+04	.21934E+04
17	18	.0	.0	.0	.12102E+04	.92436E+03	-.12102E+04	.22096E+04
18	19	.0	.0	.0	.62918E+02	.15700E+02	-.62918E+02	.70324E+02
18	18	.0	.0	.0	.62918E+02	.15706E+02	-.62918E+02	.70324E+02
19	20	.0	.0	.0	.60198E+02	.10267E+02	-.60198E+02	.63604E+02
19	21	.0	.0	.0	.60198E+02	.10267E+02	-.60198E+02	.63604E+02
20	22	.0	.0	.0	.10036E+04	.88624E+03	-.10038E+04	.20370E+04
20	21	.0	.0	.0	.11678E+04	.88624E+03	-.11678E+04	.21226E+04
21	22	.0	.0	.0	.10204E+02	.60205E+02	-.10204E+02	.12084E+03
21	16	.0	.0	.0	.12204E+02	.60205E+02	-.12204E+02	.12103E+03
22	15	.0	.0	.0	.12140E+02	.73658E+02	-.12140E+02	.14781E+03
22	23	.0	.0	.0	.10140E+02	.73658E+02	-.10140E+02	.14765E+03
23	23	.0	.0	.0	.13259E+04	.10824E+04	-.13259E+04	.25345E+04
23	24	.0	.0	.0	.11729E+04	.10824E+04	-.11729E+04	.24621E+04
24	25	.0	.0	.0	.73568E+02	.10775E+02	-.73568E+02	.76659E+02
24	24	.0	.0	.0	.73568E+02	.10775E+02	-.73568E+02	.76659E+02
25	23	.33375E+04	.66750E+04	-.75000E+02	.43104E+04	.98305E+02	.23046E+04	.67541E+04
25	25	.33375E+04	.66750E+04	-.75000E+02	.44734E+04	.98305E+02	.22016E+04	.67544E+04
25	25	.33375E+04	.66750E+04	-.75000E+02	.41551E+04	.91116E+02	.25199E+04	.67533E+04
25	27	.33375E+04	.66750E+04	-.75000E+02	.44001E+04	.91116E+02	.22749E+04	.67535E+04
27	27	.33225E+04	.66450E+04	-.75000E+02	.37415E+04	.11384E+03	.28535E+04	.67245E+04
27	30	.33225E+04	.66450E+04	-.75000E+02	.38965E+04	.11384E+03	.27485E+04	.67247E+04
28	29	.11025E+04	.23250E+04	-.75000E+02	.41593E+04	.13760E+04	-.18343E+04	.49473E+04
28	28	.11025E+04	.23250E+04	-.75000E+02	.36873E+04	.13750E+04	-.13023E+04	.46165E+04
29	29	.0	.0	.0	.11644E+02	.11572E+02	-.11644E+02	.25644E+02
29	30	.0	.0	.0	.12044E+02	.11572E+02	-.12044E+02	.26040E+02
30	30	.0	.0	.0	.24266E+02	.21985E+01	-.24266E+02	.24658E+02
30	31	.0	.0	.0	.24266E+02	.21885E+01	-.24266E+02	.24658E+02

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EARTHQUAKE 2 + NOZZLE LOADS + DEADWEIGHT EFCU-2

ELEMENT TOTAL STRESSES AND MAXIMUM STRESS INTENSITY

NOZZLE LOADS + DEADWEIGHT + EARTHQUAKE NO 1

SEAM	NODE	PRESSURE	PRESSURE			TOTAL AXIAL	TOTAL SHEAR	TOTAL AXIAL	MAXIMUM INTENSITY
			HOOP	RADIAL					
31	31	.0	.0	.0		.16631E+04	.20904E+03	-.16631E+04	.17149E+04
31	32	.0	.0	.0		.16641E+04	.20904E+03	-.16641E+04	.17158E+04
32	30	.0	.0	.0		.22824E+02	.26642E+01	-.22824E+02	.23434E+02
32	33	.0	.0	.0		.22824E+02	.26642E+01	-.22824E+02	.23434E+02
33	33	.0	.0	.0		.21869E+04	.17777E+03	-.21869E+04	.22147E+04
33	34	.0	.0	.0		.21920E+04	.17777E+03	-.21920E+04	.22205E+04
34	39	.33225E+04	.66450E+04	-.75000E+02		.35457E+04	.60302E+02	.30993E+04	.67212E+04
34	35	.33225E+04	.66450E+04	-.75000E+02		.34837E+04	.60302E+02	.31613E+04	.67211E+04
35	35	.33375E+04	.66750E+04	-.75000E+02		.34858E+04	.34475E+02	.31692E+04	.67504E+04
35	35	.33375E+04	.66750E+04	-.75000E+02		.33976E+04	.34475E+02	.32772E+04	.67504E+04
36	37	.10075E+04	.33750E+04	-.75000E+02		.23326E+04	.15236E+03	.10424E+04	.34718E+04
36	16	.10075E+04	.33750E+04	-.75000E+02		.21626E+04	.15236E+03	.12124E+04	.34689E+04
37	16	.10075E+04	.33750E+04	-.75000E+02		.22104E+04	.48592E+02	.11546E+04	.34520E+04
37	38	.10075E+04	.33750E+04	-.75000E+02		.21684E+04	.48592E+02	.12066E+04	.34520E+04
38	11	.0	.0	.0		.66320E+02	.65613E+01	-.66320E+02	.67605E+02
38	39	.0	.0	.0		.66320E+02	.65613E+01	-.66320E+02	.67605E+02
39	39	.0	.0	.0		.49659E+04	.52195E+03	-.49659E+04	.50744E+04
39	40	.0	.0	.0		.49699E+04	.52195E+03	-.49699E+04	.50979E+04
40	11	.0	.0	.0		.73666E+02	.14096E+02	-.73666E+02	.78895E+02
40	41	.0	.0	.0		.73566E+02	.14096E+02	-.73566E+02	.78895E+02
41	41	.0	.0	.0		.58081E+04	.90245E+03	-.58081E+04	.60323E+04
41	42	.0	.0	.0		.57681E+04	.90285E+03	-.57681E+04	.60632E+04

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Appendix C

SANSAR OUTPUT

This section contains the following:

- C.1 SANSAR Abstract
- C.2 Local Nozzle Stress Output
- C.3 Local Support Stress Output

Appendix C.1
SANSAR ABSTRACT

SANSAR ABSTRACT

SANSAR is a multi-purpose computer program, written in Fortran IV, and used in the evaluation of seismic and nozzle load stresses. The program has been developed for various horizontal and vertical heat exchanger designs but can be applied to tanks as well.

SANSAR is divided into two segments, NOZZLE and SIZMIK.

NOZZLE performs nozzle to shell stress analysis based upon the combined effects of external mechanical pipe loads, (beam stresses in the nozzle and Bijlaard stresses in the shell), Johns and Orange pressure discontinuities influence, and pressure membrane effects.

SIZMIK performs static equivalent seismic analysis of vessel supports using "rigid" vessel and flexible support models. SIZMIK accounts for both seismic and external mechanical pipe load effects on the supports as well as considering internal pressure influence. In determining vessel stresses in SIZMIK, the methods of Welding Research Council Bulletin #107 are used.

For both NOZZLE and SIZMIK both principal stresses and stress intensities are calculated, thus stress comparisons can be made for Class 1, 2, 3 or NC nuclear equipment.

Nozzle Options

This segment of "SANSAR" is so written as to allow for the calculation of allowable forces and moments as well as the evaluation of stresses due to specified loadings. Due to the infinite possible loading combinations, the allowable forces and moments are found on an individual nozzle basis without regard to support geometries. The possible options available to the user are:

Option #1

The calculation of maximum allowable nozzle forces and moments, applied individually. (Since nozzle reactions do not occur as individual loads in one direction but simultaneously with loads in all directions, the results of Option #1 should be used for information only.)

Option #2

The calculation of maximum resultant forces and moments, arbitrarily oriented and applied together. (These results are presented as resultant force over resultant moment ratios and are based on the worst possible force/moment orientation.) The results of Option #2 should be used for information only.

Option #3

The calculation of stress intensities for specific load cases. (These specified loads are saved and reacted to the support locations to be included in the seismic evaluation.)

The effects of pressure are taken into account in all three options. The effects of shear stress are taken into account in Options #1 and #3 but are neglected in Option #2.

For Options #1 and #2, the size of the allowable loads is based on stresses calculated at eight (8) locations in the vessel and eight (8) locations in the nozzle at the nozzle-to-vessel junction. The stress intensity limit is $1.5 S_m$ in all calculations.

SANSAR Stress Output is presented in two subgroups: "Primary Stresses" and "Total Stresses".

"Primary Stresses" are primary local stress results whereas "Total Stresses" are primary plus secondary stress results.

For NOZZLE only analysis, a total of sixteen (16) positions are reviewed for stress state; eight (8) in the vessel and eight (8) in the nozzle.

positions 1 to 8 are located in the vessel and are identified using Welding Research Council Bulletin No. 107 nomenclature.

positions 1 to 8 are identified as A_{upper} , B_{upper} , C_{upper} , D_{upper} , A_{lower} , B_{lower} , C_{lower} , D_{lower} respectively.

positions 9 to 16 are located in the nozzle and although not necessarily aligned to the four vessel positions A, B, C, D, the nozzle locations represent locations at the inside and outside of

the nozzle -- i.e., a plane passing through the nozzle centerline and cutting through the nozzle thickness would contain position 9 on the inside and position 11 on the outside. The remaining related positions are 10 and 12, 13 and 15, 14 and 16. Since the positions at which the resultant stresses due to shear and bending moments do not necessarily coincide, eight (8) positions around the nozzle (four (4) inside and four (4) outside) must be examined.

For both the shell and the nozzle, "Total Stresses" are calculated first and then to establish primary stresses, common plane stresses are averaged across the thickness; i.e.,

$$\frac{A_{\text{upper}} + A_{\text{lower}}}{2}$$

or $\frac{"9" + "11"}{2}$ where stresses are added on a component basis.

For SIZMIK, eight (8) stress positions are reported for each support and "load case"*. These eight (8) stress positions are identical in definition to the first eight stress positions for NOZZLE. "Primary" and "Total" stresses are similarly identified.

*The "load cases" considered in SIZMIK are"

- 1) Pressure loading
- 2) Nozzle loading
- 3) Deadweight loading (special case nozzle loading)
- 4) Static equivalent seismic "G" loads

SIZMIK has the capability of combining the above specified load cases as follows:

- 1) Absolute summation of load cases 1, 2, 3, 4
- 2) Absolute summation of load cases 1, 2, and 3 plus SRSS of load case 4
- 3) Algebraic summation of load cases 1, 2, 3, 4
- 4) Algebraic summation of load cases 1, 2, and 3 plus SRSS or absolute summation of load case 4

Pressure stress effects for rectangular or square support attachments are based on "thin shell" pressure membrane stress theory.

References

Technical Report R-103 titled "Theoretical Elastic Stress Distributions Arising From Discontinuities and Edge Loads In Several Shell-Type Structures", by Robert H. Johns and Thomas W. Orange, Lewis Research Center, Cleveland, Ohio.

Welding Research Council Bulletin No. 107 titled "Local Stresses In Spherical and Cylindrical Shells Due to External Loadings".

Appendix C.2
LOCAL NOZZLE STRESS OUTPUT

NOZZLES N1 + N2 LOAD CASE 1

KOPT	KTYPE	KBETA	KOEF
3	1	*	*

KEY1	KEY2	KEY3	KEY4	KEY5
*	*	*	*	*

SM1	SM2	P	TN	TV	RN	RMV
17500.	16200.	650.	1:1430	3:1250	7:1880	23:6900

GAMMA	BETA
7.58	.2655

X	Y	Z
.0000	.90500	.0000

A1	A2	A3	A4	A5	A6
1.11050	.09807	.24391	.09464	.90938	.04378

B1	B2	B3	B4	B5	B6
1.28264	.07325	.45475	.05639	.24895	.06995

C_a=1

OPTION THREE OF PROGRAM NOZZLE

FOR THE FORCES (POUNDS) AND MOMENTS (POUND-INCHES)

FX	FY	FZ	HX	HY	MZ
-2952.	2952.	.	.	90300.	90300.

THE PRIMARY STRESSES IN THE VESSEL AND NOZZLE ARE

LOCATION	SX	SY	TOX
1	-623.	8678.	-325.
2	-498.	9135.	-325.
3	6449.	1897.	-325.
4	6449.	1897.	-325.
5	-623.	8678.	-325.
6	-498.	9135.	-325.
7	6449.	1897.	-325.
8	6449.	1897.	-325.
9	2683.	7188.	-325.
10	1204.	7188.	-325.
11	2683.	7188.	-325.
12	1204.	7188.	-325.
13	1943.	7188.	-325.
14	1943.	7188.	-325.
15	1943.	7188.	-325.
16	1943.	7188.	-325.

THE RESULTING PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	8678.	-524.	-325.
2	9136.	-499.	-325.
3	6450.	1896.	-325.
4	6453.	1893.	-325.
5	8678.	-624.	-325.
6	9136.	-499.	-325.
7	6450.	1896.	-325.

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			-325.
8	6453.	1893.	-325.
9	7206.	2665.	-325.
10	7201.	1191.	-325.
11	7206.	2665.	-325.
12	7201.	1191.	-325.
13	7193.	1939.	-325.
14	7220.	1912.	-325.
15	7193.	1939.	-325.
16	7220.	1912.	-325.

THE RESULTING STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	9302.	-299.	-9003.
2	9634.	-174.	-9461.
3	4554.	2221.	-6775.
4	4560.	2218.	-6778.
5	9302.	-299.	-9003.
6	9634.	-174.	-9461.
7	4554.	2221.	-6775.
8	4560.	2218.	-6778.
9	4541.	2990.	-7531.
10	6010.	1516.	-7526.
11	4541.	2990.	-7531.
12	6010.	1516.	-7526.
13	5254.	2264.	-7518.
14	5308.	2237.	-7545.
15	5254.	2264.	-7518.
16	5308.	2237.	-7545.

THE TOTAL STRESSES IN THE VESSEL AND NOZZLE ARE

LOCATION	SX	S0	SY	TOX
1	554.	8908.	.	89.
2	2279.	10366.	.	89.
3	7135.	3919.	.	47.
4	7135.	3919.	.	131.
5	-1800.	8447.	-650.	89.
6	-3275.	7903.	-650.	89.
7	5763.	-126.	-650.	47.
8	5763.	-126.	-650.	131.
9	-11168.	3052.	-650.	260.
10	-12519.	3052.	-650.	260.
11	16533.	11324.	.	310.
12	14927.	11324.	.	310.
13	-11843.	3052.	-650.	136.
14	-11843.	3052.	-650.	385.
15	15730.	11324.	.	185.
16	15730.	11324.	.	434.

THE RESULTING PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	8909.	554.	.
2	10367.	2278.	.
3	7136.	3918.	.
4	7141.	3913.	.
5	8448.	-1801.	-650.
6	7904.	-3276.	-650.
7	5764.	-126.	-650.
8	5766.	-129.	-650.
9	3056.	-11173.	-650.
10	3056.	-12523.	-650.
11	16552.	11305.	.

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8	5766.	-129.	-650.
9	3056.	-11173.	-650.
10	3056.	-12523.	-650.
11	16552.	11305.	.
12	14954.	11297.	.
13	3053.	-11845.	-650.
14	3062.	-11853.	-650.
15	15738.	11316.	.
16	15773.	11282.	.

THE RESULTING STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	8356.	554.	-8909.
2	8089.	2279.	-10367.
3	3218.	3918.	-7136.
4	3227.	3913.	-7141.
5	10249.	-1151.	-9098.
6	11179.	-2626.	-8554.
7	5890.	524.	-6414.
8	5895.	521.	-6416.
9	14229.	-10523.	-3705.
10	15579.	-11873.	-3706.
11	5246.	11305.	-16552.
12	3656.	11297.	-14954.
13	14898.	-11195.	-3703.
14	14915.	-11203.	-3712.
15	4422.	11316.	-15738.
16	4491.	11282.	-15773.

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NOZZLES N3 • N4 LOAD CASE 1

KOPT KTYPE KBETA KOEF

3

KEY1 KEY2 KEY3 KEY4 KEYS

SM1 S42 P TN TV RN RMV
17500. 15000. 150. .3750 1.5000 8.0000 28.2500

GAMMA BETA
19.83 .2478

X Y Z
.0000 7.7500 .0000

A1 A2 A3 A4 A5 A6
2.09495 .07266 .80504 .08500 2.05920 .03123

B1 B2 B3 B4 B5 B6
2.80674 .04293 1.39830 .04346 .77124 .05169

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OPTION THREE OF PROGRAM NOZZLE

FOR THE FORCES (POUNDS) AND MOMENTS (POUND-INCHES)

FX FY FZ MX MY MZ
-5523. 5523. . . 210300. 210300.

THE PRIMARY STRESSES IN THE VESSEL AND NOZZLE ARE

LOCATION	SX	SY	SY	TOX
1	-783.	5639.	-75.	349.
2	533.	9153.	-75.	349.
3	6077.	1195.	-75.	202.
4	6077.	1195.	-75.	495.
5	-783.	5639.	-75.	349.
6	533.	9153.	-75.	349.
7	6077.	1195.	-75.	202.
8	6077.	1195.	-75.	495.
9	5380.	6309.	-75.	1461.
10	-1655.	6309.	-75.	1461.
11	5380.	6309.	-75.	1461.
12	-1655.	6309.	-75.	1461.
13	1863.	6309.	-75.	861.
14	1863.	6309.	-75.	2062.
15	1863.	6309.	-75.	861.
16	1863.	6309.	-75.	2062.

THE RESULTING PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	5658.	-802.	-75.
2	9168.	519.	-75.
3	6085.	1186.	-75.
4	6126.	1145.	-75.
5	5658.	-802.	-75.
6	9168.	519.	-75.
7	6085.	1186.	-75.
8	6126.	1145.	-75.

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		217.	-75.
7	6085.	1186.	-75.
8	6126.	1145.	-75.
9	7378.	4311.	-75.
10	6569.	-1915.	-75.
11	7378.	4311.	-75.
12	6569.	-1915.	-75.
13	6470.	1701.	-75.
14	7118.	1054.	-75.
15	6470.	1701.	-75.
16	7118.	1054.	-75.

THE RESULTING STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	6460.	-727.	-5733.
2	8649.	594.	-9243.
3	4899.	1261.	-6160.
4	4981.	1220.	-6201.
5	6460.	-727.	-5733.
6	8649.	594.	-9243.
7	4899.	1261.	-6160.
8	4981.	1220.	-6201.
9	3067.	4386.	-7453.
10	8484.	-1840.	-6644.
11	3067.	4386.	-7453.
12	8484.	-1840.	-6644.
13	4769.	1776.	-6545.
14	6064.	1129.	-7193.
15	4769.	1776.	-6545.
16	6064.	1129.	-7193.

THE TOTAL STRESSES IN THE VESSEL AND NOZZLE ARE

LOCATION	SX	SO	SY	TOX
1	-4259.	3961.	•	349.
2	7024.	13497.	•	349.
3	6972.	3140.	•	202.
4	6972.	3140.	•	495.
5	2693.	7318.	-150.	349.
6	-5958.	4809.	-150.	349.
7	5182.	-751.	-150.	202.
8	5182.	-751.	-150.	495.
9	-8708.	2108.	-150.	1426.
10	-15575.	2108.	-150.	1426.
11	19469.	10510.	•	1497.
12	12264.	10510.	•	1497.
13	-12141.	2108.	-150.	826.
14	-12141.	2108.	-150.	2026.
15	15866.	10510.	•	896.
16	15866.	10510.	•	2097.

THE RESULTING PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	3976.	-4274.	•
2	13516.	7005.	•
3	6982.	3129.	•
4	7035.	3077.	•
5	7344.	2667.	-150.
6	4821.	-5969.	-150.
7	5189.	-758.	-150.
8	5223.	-792.	-150.
9	2293.	-8893.	-150.
10	2223.	-15689.	-150.
11	19712.	10267.	•

C.2-9

9	2693.	-3071.	-150.
10	2223.	-15689.	-150.
11	19712.	10267.	.
12	13122.	9653.	.
13	2156.	-12189.	-150.
14	2391.	-12424.	-150.
15	16012.	10364.	.
16	16589.	9787.	.

THE RESULTING STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	8250.	-4274.	-3976.
2	6511.	7005.	-13516.
3	3853.	3129.	-6982.
4	3957.	3077.	-7035.
5	4677.	2817.	-7494.
6	10790.	-5819.	-4971.
7	5946.	-608.	-5339.
8	6015.	-642.	-5373.
9	11186.	-8743.	-2443.
10	17912.	-15539.	-2373.
11	9445.	10267.	-19712.
12	3469.	9653.	-13122.
13	14345.	-12039.	-2306.
14	14815.	-12274.	-2541.
15	5648.	10364.	-16012.
16	6802.	9787.	-16589.

NOZZLES N1 + N2 LOAD CASE 2

KOPT KTYPE KBETA KUEF

3

KEY1 KEY2 KEY3 KEY4 KEYS

SM1 SM2 P TN TV RN RMV
17500 16200 650 1.1430 3.1250 7.1880 23.6900

GAMMA BETA
7.58 .2655

X Y Z
.0000 .90600 .0000

A1 A2 A3 A4 A5 A6
1.11050 .09807 .24391 .09464 .90938 .04378
B1 B2 B3 B4 B5 B6
1.28264 .07325 .45475 .05639 .24895 .06995

C2-11

OPTION THREE OF PROGRAM NOZZLE

FOR THE FORCES (POUNDS) AND MOMENTS (POUND-INCHES)

	FX	FY	FZ	MX	MY	MZ
	2952.	2952.	90300.	90300.		

THE PRIMARY STRESSES IN THE VESSEL AND NOZZLE ARE

LOCATION	SX	SY	TGX	
1	-560.	8906.	-325.	131.
2	-560.	8906.	-325.	47.
3	6335.	1835.	-325.	89.
4	6564.	1958.	-325.	89.
5	-560.	8906.	-325.	131.
6	-560.	8906.	-325.	47.
7	6335.	1835.	-325.	89.
8	6564.	1958.	-325.	89.
9	2683.	7188.	-325.	285.
10	1204.	7188.	-325.	285.
11	2683.	7188.	-325.	285.
12	1204.	7188.	-325.	285.
13	1943.	7188.	-325.	409.
14	1943.	7188.	-325.	161.
15	1943.	7188.	-325.	409.
16	1943.	7188.	-325.	161.

THE RESULTING PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	8908.	-562.	-325.
2	8906.	-561.	-325.
3	6337.	1833.	-325.
4	6565.	1955.	-325.
5	8908.	-562.	-325.
6	8906.	-561.	-325.
7	6337.	1833.	-325.

C.2-12

5	8908.	-562.	-325.
6	8908.	-561.	-325.
7	6337.	1833.	-325.
8	6565.	1956.	-325.
9	7206.	2665.	-325.
10	7201.	1191.	-325.
11	7206.	2665.	-325.
12	7201.	1191.	-325.
13	7220.	1912.	-325.
14	7193.	1939.	-325.
15	7220.	1912.	-325.
16	7193.	1939.	-325.

THE RESULTING STRESS INTENSITIES ARE

LOCATION	S12	S23	S31
1	9470.	-237.	-9233.
2	9467.	-236.	-9231.
3	4503.	2158.	-6662.
4	4609.	2281.	-6890.
5	9470.	-237.	-9233.
6	9467.	-236.	-9231.
7	4503.	2158.	-6662.
8	4609.	2281.	-6890.
9	4541.	2990.	-7531.
10	6010.	1516.	-7526.
11	4541.	2990.	-7531.
12	6010.	1516.	-7526.
13	5308.	2237.	-7545.
14	5254.	2264.	-7518.
15	5308.	2237.	-7545.
16	5254.	2264.	-7518.

THE TOTAL STRESSES IN THE VESSEL AND NOZZLE ARE

LOCATION	SX	SO	SY	TOX
1	1417.	9637.	.	131.
2	1417.	9637.	.	47.
3	6376.	2775.	.	89.
4	7895.	5062.	.	89.
5	-2538.	8175.	-650.	131.
6	-2538.	8175.	-650.	47.
7	6294.	895.	-650.	89.
8	5233.	-1146.	-650.	89.
9	-11168.	3052.	-650.	260.
10	-12519.	3052.	-650.	260.
11	16533.	11324.	.	310.
12	14927.	11324.	.	310.
13	-11843.	3052.	-650.	385.
14	-11843.	3052.	-650.	136.
15	15730.	11324.	.	434.
16	15730.	11324.	.	185.

THE RESULTING PRINCIPAL STRESSES ARE

LOCATION	S1	S2	S3
1	9639.	1415.	.
2	9638.	1417.	.
3	6379.	2773.	.
4	7897.	5059.	.
5	8177.	-2539.	-650.
6	8175.	-2538.	-650.
7	6295.	894.	-650.
8	5234.	-1148.	-650.
9	3056.	-11173.	-650.
10	3056.	-12523.	-650.
11	16552.	11305.	.

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EARTHQUAKE 2

MEAM STRESSES FOR OUTPUT VECTOR 6

BEAM	---	TRANSVERSE	---	TORSIONAL	-	STRESSES AT USER LOCATIONS -	MAXIMUM	MINIMUM	COMBINED	
NO.	LOAD-LOCATION,	SHEAR	SHEAR	(T/C/J)	A	B	C	(P/A-MC/I)	(P/A-MC/I)	SHEAR
	NU	---	---	---						
1	1 JA	0.0	-4.87E+01	-4.87E+01	0.	-3.159E+01	-3.159E+01	-3.159E+01	-3.1598E+01	1.59E+01 PIPEG
1	4 JB	100.0	-4.87E+01	-4.87E+01	0.	-3.159E+01	3.055E+01	3.055E+01	5.6293E+01	-1.1946E+02 2.81E+01
2	3 JA	0.0	-3.95E-11	-1.15E-10	-1.19E-11	1.447E-10	1.208E-10	6.177E-11	2.3093E-10	9.4392E-11 1.16E-10 PIPEG
2	2 JH	100.0	-3.95E-11	-1.15E-10	-1.19E-11	1.447E-10	1.984E-10	2.358E-10	2.5045E-10	3.8871E-11 1.26E-10
3	3 JA	0.0	-6.52E-12	2.63E-11	0.	-2.980E-11	-2.965E-11	-2.984E-11	-2.9616E-11	-2.9989E-11 1.48E-11 BEAMG
3	4 JD	100.0	-6.52E-12	2.63E-11	0.	-2.980E-11	-2.965E-11	-3.055E-11	-2.8908E-11	-3.0696E-11 1.45E-11
4	4 JA	0.0	-2.33E-11	1.68E-11	3.73E-13	-7.451E-11	-7.406E-11	-7.493E-11	-7.3630E-11	-7.5381E-11 3.68E-11 BEAMG
4	5 JH	100.0	-2.33E-11	1.68E-11	3.73E-13	-7.451E-11	-7.346E-11	-7.536E-11	-7.2606E-11	-7.6406E-11 3.63E-11
5	5 JA	0.0	1.24E-11	4.69E-11	8.96E-12	-1.808E-10	-1.510E-10	-1.987E-10	-1.4599E-10	-2.1566E-10 7.35E-11 PIPEG
5	6 JH	100.0	1.24E-11	4.69E-11	8.96E-12	-1.808E-10	-1.808E-10	-2.301E-10	-1.3154E-10	-2.3011E-10 6.64E-11
6	4 JA	0.0	-4.87E+01	-4.87E+01	4.0E-12	-3.159E+01	3.055E+01	3.055E+01	5.6293E+01	-1.1946E+02 2.81E+01 PIPEG
6	7 JB	100.0	-4.87E+01	-4.87E+01	4.70E-12	-3.159E+01	7.948E+01	7.948E+01	1.2549E+02	-1.8857E+02 6.27E+01
7	7 JA	0.0	-2.25E-02	-2.25E-02	2.30E-11	-1.769E+02	1.090E+02	1.090E+02	2.2744E+02	-5.8117E+02 1.14E+02 PIPEG
7	8 JB	100.0	-2.25E-02	-2.25E-02	2.30E-11	-1.769E+02	2.074E+02	2.074E+02	3.6653E+02	-7.2026E+02 1.03E+02
8	8 JA	0.0	-1.81E+02	-1.81E+02	7.51E-12	-1.524E+02	4.615E+01	4.015E+01	1.2838E+02	-4.3312E+02 6.42E+01 PIPEG
8	11 JB	100.0	-1.81E+02	-1.81E+02	7.51E-12	-1.524E+02	1.389E+02	1.389E+02	2.5454E+02	-5.6428E+02 1.30E+02
9	10 JA	0.0	-5.23E-11	-6.98E-11	-5.34E-11	-3.055E-11	-3.708E-12	-7.509E-11	2.1445E-11	-8.2555E-11 5.45E-11 PIPEG
9	10 JH	100.0	-5.23E-11	-6.98E-11	-5.34E-11	-3.055E-11	-4.146E-11	-2.562E-12	4.6713E-11	-1.0782E-10 5.43E-11
10	10 JA	0.0	1.27E-11	4.19E-12	2.24E-13	5.935E-12	5.531E-12	5.972E-12	6.3752E-12	5.4942E-12 3.20E-12 BEAMG
10	11 JH	100.0	1.27E-11	4.19E-12	2.24E-13	5.935E-12	5.061E-12	5.860E-12	6.8925E-12	4.9868E-12 3.45E-12
11	11 JA	0.0	1.43E+02	1.43E+02	1.93E+01	-1.524E+02	1.344E+02	1.344E+02	2.5314E+02	-5.5788E+02 1.28E+02 PIPEG
11	12 JH	100.0	1.43E+02	1.43E+02	1.93E+01	-1.524E+02	6.128E+01	6.128E+01	1.4977E+02	-4.5452E+02 7.73E+01
12	12 JA	0.0	1.18E+02	1.18E+02	3.74E+01	-3.911E+02	2.242E+01	2.242E+01	1.9371E+02	-9.7591E+02 1.04E+02 PIPEG
12	37 JH	100.0	1.18E+02	1.18E+02	3.74E+01	-3.911E+02	-2.279E+02	-2.279E+02	-1.6030E+02	-6.2190E+02 8.84E+01
13	13 JA	0.0	-4.67E+00	-1.89E-01	8.25E-03	-3.747E+01	-3.771E+01	-3.747E+01	-3.7233E+01	-3.7714E+01 1.86E+01 BEAMG
13	14 JB	100.0	-4.67E+00	-1.89E-01	8.25E-03	-3.747E+01	-3.768E+01	-3.747E+01	-3.7255E+01	-3.7682E+01 1.86E+01
14	15 JA	0.0	5.46E+02	-2.70E+00	3.43E+00	7.101E+01	6.521E+02	7.867E+01	6.5979E+02	-5.1776E+02 3.30E+02 BEAMG
14	14 JB	100.0	5.46E+02	-2.70E+00	3.43E+00	7.101E+01	-4.424E+02	6.153E+01	5.9499E+02	-4.5297E+02 2.98E+02
15	15 JA	0.0	-3.75E+01	-1.89E+01	7.18E-05	4.870E+00	5.106E+00	4.864E+00	5.1122E+00	4.6277E+00 2.56E+00 BEAMG
15	16 JB	100.0	-3.75E+01	-1.89E+01	7.18E-05	4.870E+00	6.160E+00	4.869E+00	6.1608E+00	3.5791E+00 3.08E+00
16	16 JA	0.0	2.46E+01	1.23E+00	-7.18E-05	-4.930E+00	-3.947E+00	-4.881E+00	-3.8973E+00	-5.9632E+00 1.95E+00 BEAMG
16	17 JB	100.0	2.46E+01	1.23E+00	-7.18E-05	-4.930E+00	-4.740E+00	-4.916E+00	-4.7657E+00	-5.0947E+00 2.38E+00
17	17 JA	0.0	4.32E+02	1.83E+01	-3.43E+00	-7.189E+01	2.978E+02	-5.377E+01	3.1596E+02	-4.5974E+02 1.58E+02 BEAMG
17	18 JB	100.0	4.32E+02	1.83E+01	-3.43E+00	-7.189E+01	-5.675E+02	-7.275E+01	6.2457E+02	-5.6835E+02 2.12E+02 A.3-25
18	19 JA	0.0	4.93E+00	1.25E+00	-6.72E-04	-2.963E+01	-2.980E+01	-2.962E+01	-2.9447E+01	-2.9804E+01 1.47E+01 BEAMG
18	19 JH	100.0	4.93E+00	1.25E+00	-6.72E-04	-2.963E+01	-2.983E+01	-2.963E+01	-2.9424E+01	-2.9827E+01 1.47E+01
19	20 JA	0.0	4.93E+00	-1.89E+01	8.25E-03	-2.963E+01	-2.980E+01	-2.963E+01	-2.9454E+01	-2.9797E+01 1.47E+01 BEAMG
19	21 JB	100.0	4.93E+00	-1.89E+01	8.25E-03	-2.963E+01	-2.983E+01	-2.963E+01	-2.9424E+01	-2.9827E+01 1.47E+01

17	17 JA	0.0	4.32E+02	1.89E+01	-3.43E+00	-7.189E+01	2.0E+02	-5.377E+01	3.1596E+02	-4.5974E+02	1.5AE+02	BEAMG
18	18 JH	100.0	4.32E+02	1.89E+01	-3.43E+00	-7.189E+01	-5.377E+02	-1.275E+01	4.2447E+02	-5.6934E+02	2.12E+02	
18	19 JA	0.0	4.32E+00	1.25E+00	-6.72E-04	-2.963E+01	-2.980E+01	-2.462E+01	-2.9447E+01	-2.9804E+01	1.47E+01	BEAMG
18	19 JH	100.0	4.32E+00	1.25E+00	-6.72E-04	-2.963E+01	-2.493E+01	-2.463E+01	-2.9424E+01	-2.9827E+01	1.47E+01	
19	20 JA	0.0	4.32E+00	-1.87E-01	8.25E-03	-2.963E+01	-2.980E+01	-2.463E+01	-2.9454E+01	-2.9797E+01	1.47E+01	BEAMG
19	21 JH	100.0	4.32E+00	-1.87E-01	8.25E-03	-2.963E+01	-2.983E+01	-2.463E+01	-2.9424E+01	-2.9827E+01	1.47E+01	
20	22 JA	0.0	4.32E+02	-2.70E+00	3.43E+00	-7.189E+01	2.978E+02	-6.424E+01	3.0550F+02	-4.4928E+02	1.53E+02	BEAMG
20	21 JH	100.0	4.32E+02	-2.70E+00	3.43E+00	-7.189E+01	-5.675E+02	-6.137E+01	4.3423F+02	-5.7801E+02	2.17E+02	
21	22 JA	0.0	-2.95E+01	-1.87E-01	7.1HE-05	-4.930E+00	-4.780E+00	-4.936E+00	-4.7739E+00	-5.0465E+00	2.39E+00	BEAMG
21	23 JH	100.0	-2.95E+01	-1.87E-01	7.1HE-05	-4.930E+00	-3.947E+00	-4.931E+00	-3.9460E+00	-5.9144E+00	1.47E+00	
22	16 JA	0.0	3.75E+01	1.25E+00	-7.1HE-05	4.870E+00	6.160E+00	4.919E+00	6.2096E+00	3.5303E+00	3.10E+00	BEAMG
22	23 JH	100.0	3.75E+01	1.25E+00	-7.1HE-05	4.870E+00	5.106E+00	4.884E+00	5.1204E+00	4.6195E+00	2.56E+00	
23	23 JA	0.0	5.46E+02	1.33E+01	-3.43E+00	7.101E+01	6.521E+02	8.913E+01	6.7025E+02	-5.2822E+02	3.35E+02	BEAMG
23	24 JH	100.0	5.46E+02	1.33E+01	-3.43E+00	7.101E+01	-6.424E+02	7.015E+01	5.8533E+02	-4.4339E+02	2.94E+02	
24	25 JA	0.0	-4.37E+00	1.25E+00	-6.72E-04	-3.747E+01	-3.771E+01	-3.747E+01	-3.7226E+01	-3.7721E+01	1.86E+01	BEAMG
24	24 JH	100.0	-4.37E+00	1.25E+00	-6.72E-04	-3.747E+01	-3.768E+01	-3.747E+01	-3.7265E+01	-3.7682E+01	1.86E+01	
25	39 JA	0.0	-5.20E+01	-5.20E+01	1.13E+01	3.760E+02	3.155E+02	3.155E+02	4.6159E+02	2.9045E+02	2.31E+02	PIPEG
25	26 JH	100.0	-5.20E+01	-5.20E+01	1.13E+01	3.760E+02	4.766E+02	4.766E+02	5.1826E+02	2.3378E+02	2.59E+02	
26	26 JA	0.0	4.14E+01	4.14E+01	1.13E+01	2.093E+02	3.099E+02	3.099E+02	3.5156E+02	6.7040E+01	1.76E+02	PIPEG
26	27 JH	100.0	4.14E+01	4.14E+01	1.13E+01	2.093E+02	1.706E+02	1.706E+02	2.6403E+02	1.5462E+02	1.33E+02	
27	27 JA	0.0	1.09E+02	1.09E+02	5.85E+00	6.086E+01	4.087E+01	4.087E+01	8.9122E+01	3.2594E+01	4.49E+01	PIPEG
27	28 JH	100.0	1.09E+02	1.09E+02	5.85E+00	6.086E+01	-1.494E+01	-1.494E+01	1.6805E+02	-4.6333E+01	8.42E+01	
28	29 JA	0.0	-2.43E-10	4.97E-11	7.93E-12	4.303E-11	-2.122E-11	9.202E-11	1.2383E-10	-3.7767E-11	6.24E-11	PIPEG
28	29 JH	100.0	-2.43E-10	4.97E-11	7.93E-12	4.303E-11	2.248E-10	4.049E-11	2.2484E-10	-1.3878E-10	1.13E-10	
29	29 JA	0.0	-2.25E-11	-5.12E-12	-2.92E-13	1.853E-12	1.518E-12	1.853E-12	2.2165E-12	1.5047E-12	1.15E-12	BEAMG
29	30 JH	100.0	-2.25E-11	-5.12E-12	-2.92E-13	1.863E-12	2.0335E-12	2.030E-12	2.5006E-12	1.2247E-12	1.28E-12	
30	30 JA	0.0	-2.35E-11	8.84E-01	9.07E-06	2.025E+01	2.025E+01	2.028E+01	2.0276E+01	2.0232E+01	1.01E+01	BEAMG
30	31 JH	100.0	-2.35E-11	8.84E-01	9.07E-06	2.025E+01	2.025E+01	2.025E+01	2.0263E+01	2.0245E+01	1.01E+01	
31	31 JA	0.0	-1.76E-11	4.91E+01	1.01E+00	1.125E+03	1.108E+03	1.119E+03	1.1481E+03	1.1024E+03	5.74E+02	BEAMG
31	32 JH	100.0	-1.76E-11	4.91E+01	1.01E+00	1.125E+03	1.109E+03	1.116E+03	1.1514E+03	1.0991E+03	5.76E+02	
32	30 JA	0.0	-4.65E-11	8.84E-01	9.07E-06	-2.025E+01	-2.025E+01	-2.023E+01	-2.0232E+01	-2.0276E+01	1.01E+01	BEAMG
32	33 JH	100.0	-4.65E-11	8.84E-01	9.07E-06	-2.025E+01	-2.025E+01	-2.026E+01	-2.0245E+01	-2.0263E+01	1.01E+01	
33	33 JA	0.0	-8.08E-12	4.91E+01	1.61E+00	-1.125E+03	-1.106E+03	-1.131E+03	-1.1024E+03	-1.1481E+03	5.51E+02	BEAMG
33	34 JH	100.0	-8.08E-12	4.91E+01	1.61E+00	-1.125E+03	-1.106E+03	-1.135E+03	-1.0941E+03	-1.1514E+03	5.50E+02	
34	30 JA	0.0	-8.52E+01	-8.52E+01	0.	6.086E+01	-1.493E+01	-1.493E+01	1.6804E+02	-4.6328E+01	8.40E+01	PIPEG
34	35 JH	100.0	-8.52E+01	-8.52E+01	0.	6.086E+01	2.866E+01	2.866E+01	1.0640E+02	1.5320E+01	5.32E+01	
35	35 JA	0.0	-4.87E+01	-4.87E+01	-3.03E-13	3.160E+01	-3.072E+01	-3.072E+01	1.1974E+02	-5.653HE+01	5.99E+01	PIPEG
35	36 JH	100.0	-4.87E+01	-4.87E+01	-3.03E-13	3.160E+01	3.160E+01	3.160E+01	3.1602E+01	3.1602E+01	1.58E+01	
36	37 JA	0.0	5.80E+01	5.80E+01	1.85E+01	-1.934E+02	-1.127E+02	-1.127E+02	-7.9344E+01	-3.0741E+02	4.38E+01	PIPEG
36	38 JH	100.0	5.80E+01	5.80E+01	1.85E+01	-1.934E+02	-1.575E+02	-1.575E+02	-1.4261E+02	-2.4414E+02	7.37E+01	
37	16 JA	0.0	-2.57E+01	-2.57E+01	5.01E+00	1.859E+02	1.430E+02	1.430E+02	2.4665E+02	1.2519E+02	1.23E+02	PIPEG
37	39 JH	100.0	-2.57E+01	-2.57E+01	5.01E+00	1.859E+02	1.560E+02	1.560E+02	2.2820E+02	1.4364E+02	1.14E+02	
38	11 JA	0.0	4.34E-01	-2.41E+00	-4.17E-04	-3.285E+01	-3.284E+01	-3.292E+01	-3.2766E+01	-3.2940E+01	1.64E+01	BEAMG
38	39 JH	100.0	4.34E-01	-2.41E+00	-4.17E-04	-3.285E+01	-3.285E+01	-3.284E+01	-3.2841E+01	-3.2865E+01	1.64E+01	
39	39 JA	0.0	-1.25E-11	-1.34E+02	-5.76E+01	-1.825E+03	-1.227E+03	-1.817E+03	-1.2187E+03	-2.4319E+03	6.12E+02	BEAMG
39	40 JH	100.0	-1.25E-11	-1.34E+02	-5.76E+01	-1.825E+03	-1.227E+03	-1.808E+03	-1.2097E+03	-2.4409E+03	6.08E+02	
40	11 JA	0.0	-4.33E-01	-2.41E+00	-4.17E-04	3.285E+01	3.284E+01	3.278E+01	3.2940E+01	3.2766E+01	1.65E+01	BEAMG
40	41 JH	100.0	-4.33E-01	-2.41E+00	-4.17E-04	3.285E+01	3.285E+01	3.286E+01	3.2845E+01	3.2841E+01	1.64E+01	
41	41 JA	0.0	9.70E-12	-1.34E+02	-5.76E+01	1.825E+03	1.227E+03	1.833E+03	2.4319E+03	1.2147E+03	1.22E+03	BEAMG
41	42 JH	100.0	9.70E-12	-1.34E+02	-5.76E+01	1.825E+03	1.227E+03	1.842E+03	2.4409E+03	1.2047E+03	1.22E+03	

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39	JA	0.0	-1.29E-11	-1.34E+02	-5.76E+01	-1.825E+03	-1.227E+03	-1.817E+03	-1.2187E+03	-2.4319E+03	6.12E+02	BEAMG	
40	JZ	100.0	-1.29E-11	-1.34E+02	-5.76E+01	-1.825E+03	-1.227E+03	-1.817E+03	-1.2097E+03	-2.4409E+03	5.09E+02		
40	11	JA	0.0	-4.39E-01	-2.41E+00	-4.77E-04	3.285E+01	3.284E+01	3.278E+01	3.2940E+01	3.2766E+01	1.65E+01	BEAMG
40	41	JR	100.0	-4.39E-01	-2.41E+00	-4.77E-04	3.285E+01	3.285E+01	3.286E+01	3.2865E+01	3.2841E+01	1.64E+01	
+1	41	JA	0.0	9.70E-12	-1.34E+02	-5.76E+01	1.825E+03	1.227E+03	1.833E+03	2.4319E+03	1.2187E+03	1.22E+03	BEAMG
+1	42	JR	100.0	9.70E-12	-1.34E+02	-5.76E+01	1.825E+03	1.227E+03	1.842E+03	2.4409E+03	1.2097E+03	1.22E+03	

EARTHQUAKE 2

MAXIMUM STRESS SUMMARY FOR

BEAM STRESSES **FOR OUTPUT VECTOR 6**
 --- TRANSVERSE --- TORSIONAL - STRESSES AT USER LOCATIONS - **MAXIMUM MINIMUM COMBINED**
 SHEAR SHEAR (T^oC/J) A B C (P/A+MC/I) (P/A-MC/I) STRESS
 (V2/K3^oA) (V3/K2^oA)

MAX. BEAM STRESSES = 5.46E+02 1.43E+02 3.74E+01 1.825E+03 1.227E+03 1.842E+03 2.4409E+03 1.2187E+03 1.22E+03
 BEAM NOS. = 14. 11. 12. 41. 41. 41. 41. 41. 41.

MIN. BEAM STRESSES = -2.25E+02 -2.25E+02 -5.76E+01 -1.825E+03 -1.227E+03 -1.817E+03 -1.2187E+03 -2.4409E+03 1.15E-12
 BEAM NOS. = 7. 7. 39. 39. 39. 39. 39. 39. 29.

A 3-27

B E G I N I N P U T L O A D C A S E N U . 1 T I T L E(N O Z Z L E L O A D C A S E 1

NODAL POINT APPLIED FORCES FOR LOAD CASE NO. 1

NODE	X1	X2	X3	X4	X5	X6
2	-2.452000E+03	-2.452000E+03	0.	-9.03000E+04	-9.03000E+04	0.
5	-2.452000E+03	-2.452000E+03	0.	-9.03000E+04	-9.03000E+04	0.
28	-3.403000E+03	-3.405000E+03	5.523000E+03	-2.974000E+05	0.	0.
9	0.	7.810000E+03	0.	-2.974000E+05	0.	0.

NODAL POINT APPLIED LOADS AND/OR DISPLACEMENTS FINAL SUMMARY FOR LOAD CASE NO. 1

NODE	X1	X2	X3	X4	X5	X6
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NOTE IF A FINAL SUMMARY OF APPLIED NODAL LOADS AND GENERATED LOADS IS DESIRED AT THIS POINT,
CODE A 1 IN COLUMN 20 OF THE STATIC CARD.

FORCE AND MOMENT SUMMATION
ABOUT AXES PARALLEL TO SYSTEM AXES
WITH ORIGIN AT POINT (0,0,0).
SUMMATION INCLUDES LOADS APPLIED TO RESTRAINED DOF.

FX1	=	-38090000000E+04
FX2	=	.1761900000E+05
FX3	=	.55230000000E+04
MX1	=	-52356226300E+07
MX2	=	-24502692300E+07
MX3	=	.19944260000E+06

B 3-28

NOZZLE LOAD CASE 1

		B E A M		E L E M E N T		L O A D S		FOR OUTPUT VECTOR		
BEAM		AXIAL	SHEAR	SHEAR	TORSION	HENDING	BENDING	M1	M2	M3
LOAD-LOCATION.	NO	P	V1	V2	V3	MT	M1	M2	M3	
NODE--PERCENT.										
1	1 JA	0.0	2.03727E-09	4.07454E-09	4.77303E-09	-3.72529E-09	5.96046E-08	7.45058E-09	PIPEG	
1	4 JA	100.0	-2.03727E-09	-4.07454E-09	-4.77303E-09	-3.72529E-09	-2.08616E-07	-8.94070E-08		
2	3 JA	0.0	-2.95200E+03	-1.45519E-10	-2.95200E+03	9.03000E+04	2.67451E+04	-9.03000E+04	PIPEG	
2	2 JB	100.0	2.95200E+03	-1.45519E-10	2.95200E+03	-9.03000E+04	2.44472E-09	9.03000E+04		
3	3 JA	0.0	-2.95200E+03	-4.65601E-09	-2.95200E+03	9.03000E+04	-2.67451E+04	-9.03000E+04	BEAMG	
3	4 JB	100.0	2.95200E+03	4.65601E-09	2.95200E+03	-9.03000E+04	9.66780E+04	9.03000E+04		
4	4 JA	0.0	2.95200E+03	-5.58794E-09	-2.95200E+03	-9.03000E+04	-9.66780E+04	9.03000E+04	BEAMG	
4	5 JB	100.0	-2.95200E+03	5.58794E-09	-2.95200E+03	9.03000E+04	2.67451E+04	-9.03000E+04		
5	5 JA	0.0	2.95200E+03	1.16415E-10	2.95200E+03	-9.03000E+04	-2.67451E+04	9.03000E+04	PIPEG	
5	6 JB	100.0	-2.95200E+03	-1.16415E-10	-2.95200E+03	9.03000E+04	-1.86265E-09	-9.03000E+04		
6	4 JA	0.0	-1.74623E-10	-5.90400E+03	-5.90400E+03	-3.35276E-08	-1.80500E+05	1.80500E+05	PIPEG	
6	7 JB	100.0	1.74623E-10	5.90400E+03	5.90400E+03	3.35276E-08	3.11964E+05	-3.11964E+05		
7	7 JA	0.0	-9.31323E-10	-5.90400E+03	-5.90400E+03	-4.84288E-08	-3.11964E+05	3.11964E+05	PIPEG	
7	8 JB	100.0	9.31323E-10	5.90400E+03	5.90400E+03	4.84288E-08	3.68760E+05	-3.68760E+05		
8	8 JA	0.0	-4.65661E-19	-5.90400E+03	-5.90400E+03	-4.09782E-08	-3.68760E+05	3.68760E+05	PIPEG	
8	11 JB	100.0	4.65661E-19	5.90400E+03	5.90400E+03	4.09782E-08	4.51416E+05	-4.51416E+05		
9	10 JA	0.0	-5.52250E+03	-4.94765E-10	-5.52250E+03	2.10294E+05	4.31893E+04	-2.10294E+05	PIPEG	
9	9 JB	100.0	5.52250E+03	4.94765E-10	5.52250E+03	-2.10294E+05	3.25963E-09	2.10294E+05		
10	10 JA	0.0	-5.52250E+03	1.39698E-09	-5.52250E+03	2.10294E+05	-4.31893E+04	-2.10294E+05	BEAMG	
10	11 JB	100.0	5.52250E+03	-1.39698E-09	5.52250E+03	-2.10294E+05	1.98433E+05	2.10294E+05		
11	11 JA	0.0	3.02680E-09	4.71507E+03	7.84757E+03	-6.64135E+04	-7.40462E+05	4.47252E+05	PIPEG	
11	12 JB	100.0	-3.02680E-09	-4.71507E+03	-7.84757E+03	6.64135E+04	6.30596E+05	-3.81241E+05		
12	12 JA	0.0	2.70566E-09	4.15070E+03	7.84757E+03	-6.64135E+04	-6.30596E+05	3.81241E+05	PIPEG	
12	37 JB	100.0	-2.70566E-09	-4.15070E+03	-7.84757E+03	6.64135E+04	2.05684E+05	-1.61991E+05		
13	13 JA	0.0	-1.66562E+03	-1.88795E+03	2.08045E+02	-3.59717E+03	-1.05849E+03	-2.57467E+03	BEAMG	
13	14 JB	100.0	1.66562E+03	1.88795E+03	-2.08045E+02	3.59717E+03	5.78821E+00	-6.97836E+03		
14	15 JA	0.0	-1.88795E+03	-1.66562E+03	2.08045E+02	-5.78821E+00	-5.57359E+03	-8.84503E+03	BEAMG	
14	14 JB	100.0	1.88795E+03	1.66562E+03	-2.08045E+02	5.78821E+00	3.59717E+03	-9.97836E+03		
15	15 JA	0.0	-1.88795E+03	1.66562E+03	2.08045E+02	-5.78821E+00	5.57359E+03	-8.84503E+03	BEAMG	
15	16 JB	100.0	1.88795E+03	-1.66562E+03	-2.08045E+02	5.78821E+00	-1.02546E+04	4.63215E+04		
16	17 JA	0.0	1.88547E+03	-1.09538E+03	6.60761E+02	5.80469E+00	-2.25006E+04	-2.85399E+04	BEAMG	
16	17 JB	100.0	-1.88547E+03	1.09538E+03	-6.60761E+02	-5.80469E+00	7.63351E+03	3.88258E+03		
17	17 JA	0.0	1.88547E+03	-1.09538E+03	6.60761E+02	5.80469E+00	-7.63351E+03	-3.88258E+03	BEAMG	
17	18 JB	100.0	-1.88547E+03	1.09538E+03	-6.60761E+02	-5.80469E+00	1.35628E+03	-6.52827E+03		A.3-39
18	19 JA	0.0	-1.39538E+03	1.85547E+03	6.60761E+02	-1.35628E+03	-3.33765E+03	1.60688E+04	BEAMG	
18	20 JB	100.0	1.39538E+03	-1.85547E+03	-6.60761E+02	1.35628E+03	-5.80469E+00	-6.52827E+03		
19	20 JA	0.0	-1.77651E+03	1.53734E+03	1.56842E+02	-3.85052E+03	-7.89460E+02	1.48185E+04	BEAMG	
19	21 JB	100.0	1.77651E+03	-1.53734E+03	-1.56842E+02	3.85052E+03	-6.16201E+00	-7.00202E+03		

13	13 JA	0.0	-1.3953E+03	1.3953E+03	-1.3953E+03	1.3953E+03	-7.0113E+03	-3.88258E+03	BEAMG	
14	13 JA	0.0	-1.3953E+03	1.3953E+03	-1.3953E+03	1.3953E+03	-7.0113E+03	-3.88258E+03	BEAMG	
15	13 JA	100.0	1.3953E+03	-1.3953E+03	-1.3953E+03	1.3953E+03	-3.33765E+03	1.60648E+04	BEAMG	
16	13 JA	0.0	-1.3953E+03	1.3953E+03	-1.3953E+03	1.3953E+03	-5.00446E+00	-5.52427E+03	BEAMG	
17	20 JA	0.0	-1.77551E+03	1.53734E+03	1.53734E+03	-1.53734E+03	-3.85052E+03	-7.89400E+02	1.68185E+04	BEAMG
18	21 JA	100.0	1.77551E+03	-1.53734E+03	-1.53734E+03	1.53734E+03	-4.16201E+00	-7.03957E+03	BEAMG	
19	22 JA	0.0	1.53734E+03	-1.77551E+03	1.53734E+03	-1.77551E+03	-4.16201E+00	-5.34002E+03	-9.83723E+03	BEAMG
20	21 JA	100.0	-1.53734E+03	1.77551E+03	-1.53734E+03	1.77551E+03	-4.16201E+00	3.85052E+03	-7.03957E+03	BEAMG
21	22 JA	0.0	1.53734E+03	-1.77551E+03	1.53734E+03	-1.77551E+03	-4.16201E+00	5.34002E+03	-9.83723E+03	BEAMG
22	15 JA	100.0	-1.53734E+03	1.77551E+03	-1.53734E+03	1.77551E+03	-4.16201E+00	-8.86957E+03	4.94985E+04	BEAMG
23	22 JA	0.0	-1.53992E+03	-9.44995E+02	7.11904E+02	-4.14553E+00	-2.38857E+04	-2.50528E+04	BEAMG	
24	23 JA	100.0	1.53992E+03	-9.44995E+02	-7.11904E+02	4.14553E+00	7.86648E+03	2.89039E+03	BEAMG	
25	23 JA	0.0	-1.53992E+03	-9.44995E+02	7.11904E+02	-4.14553E+00	-7.86648E+03	-2.89039E+03	BEAMG	
26	24 JA	100.0	1.53992E+03	-9.44995E+02	-7.11904E+02	4.14553E+00	1.10283E+03	-6.46707E+03	BEAMG	
27	25 JA	0.0	-9.34995E+02	-1.53942E+03	7.11904E+02	-1.10283E+03	-3.60608E+03	-1.32440E+03	BEAMG	
28	24 JB	100.0	9.34995E+02	1.53942E+03	-7.11904E+02	1.10283E+03	4.14553E+00	-6.46707E+03	BEAMG	
29	38 JA	0.0	5.52300E+03	1.18520E+03	3.51903E+03	-9.03013E+02	-1.12136E+05	4.46651E+04	PIPEG	
30	26 JB	100.0	-5.52300E+03	-1.18520E+03	-3.51903E+03	9.03013E+02	-1.27827E+05	3.61538E+04	PIPEG	
31	26 JA	0.0	5.52300E+03	1.18520E+03	3.51903E+03	-9.03013E+02	1.27827E+05	-3.61538E+04	PIPEG	
32	27 JB	100.0	-5.52300E+03	-1.18520E+03	-3.51903E+03	9.03013E+02	-3.88445E+05	1.23930E+05	PIPEG	
33	27 JA	0.0	5.52300E+03	1.18520E+03	3.51903E+03	-9.03013E+02	3.88445E+05	-1.23930E+05	PIPEG	
34	30 JB	100.0	-5.52300E+03	-1.18520E+03	-3.51903E+03	9.03013E+02	-4.37713E+05	1.40523E+05	PIPEG	
35	29 JA	0.0	5.52250E+03	5.52300E+03	-7.13953E-11	2.10294E+05	5.38421E-10	2.53487E+05	PIPEG	
36	29 JB	100.0	-5.52250E+03	-5.52300E+03	7.13953E-11	-2.10294E+05	0.	-2.10294E+05	PIPEG	
37	29 JA	0.0	5.52250E+03	-5.52300E+03	7.27596E-11	2.10294E+05	9.31323E-10	2.53487E+05	BEAMG	
38	30 JB	100.0	-5.52250E+03	5.52300E+03	-7.27596E-11	-2.10294E+05	-2.79397E-09	-4.09154E+05	BEAMG	
39	30 JA	0.0	1.91678E+03	-6.98492E-10	7.86995E+02	1.83652E+02	-2.41345E+04	3.65923E+01	BEAMG	
40	31 JB	100.0	-1.91678E+03	6.98492E-10	-7.86995E+02	-1.83652E+02	2.34294E+03	-3.65923E+01	BEAMG	
41	31 JA	0.0	1.91678E+03	-1.81899E-11	7.86995E+02	1.83652E+02	-2.34264E+03	3.65923E+01	BEAMG	
42	32 JB	100.0	-1.91678E+03	1.81899E-11	-7.86995E+02	-1.83652E+02	-1.04931E+03	-3.65923E+01	BEAMG	
43	32 JA	0.0	-1.17297E+03	4.19095E-09	-8.03020E+02	5.62951E+01	2.32315E+04	-1.19370E+02	BEAMG	
44	33 JB	100.0	1.17297E+03	-4.19095E-09	8.03020E+02	-5.62951E+01	-9.95889E+02	1.19376E+02	BEAMG	
45	33 JA	0.0	-1.17297E+03	5.82677E-11	-8.03020E+02	5.62951E+01	9.95889E+02	-1.19376E+02	BEAMG	
46	34 JB	100.0	1.17297E+03	-5.82677E-11	-8.03020E+02	-5.62951E+01	2.46513E+03	1.19376E+02	BEAMG	
47	34 JA	0.0	-9.31323E-10	1.30907E-10	6.98492E-10	0.	-4.47035E-08	0.	PIPEG	
48	35 JB	100.0	9.31323E-10	-1.30907E-10	-6.98492E-10	0.	2.98023E-08	7.45058E-09	PIPEG	
49	35 JA	0.0	-2.32831E-10	8.73115E-11	2.03727E-10	-1.16415E-10	-3.12529E-09	-2.79397E-09	PIPEG	
50	36 JB	100.0	2.32831E-10	-8.73115E-11	-2.03727E-10	1.16415E-10	0.	1.86265E-09	PIPEG	
51	37 JA	0.0	1.39693E-09	4.71507E+03	7.84757E+03	-6.64135E+04	-2.65684E+05	1.61991E+05	PIPEG	
52	16 JA	100.0	-1.39693E-09	-4.71507E+03	-7.84757E+03	6.64135E+04	1.33658E+05	-8.26831E+04	PIPEG	
53	38 JA	0.0	5.52300E+03	1.18520E+03	3.51903E+03	-9.03013E+02	-1.51478E+05	5.79157E+04	PIPEG	
54	39 JA	0.0	1.62831E+04	2.17579E+02	-1.78941E+03	2.91172E+02	4.48332E+04	0.11788E+03	BEAMG	
55	39 JB	100.0	-1.62831E+04	-2.17579E+02	1.78941E+03	-2.91172E+02	4.71990E+03	-9.25850E+01	BEAMG	
56	39 JA	0.0	1.62831E+04	-4.36597E-11	-1.78941E+03	2.24083E+02	-4.72337E+03	9.25850E+01	BEAMG	
57	40 JB	100.0	-1.62831E+04	4.36597E-11	1.78941E+03	-2.24083E+02	1.24357E+04	-9.25850E+01	BEAMG	
58	11 JA	0.0	1.62831E+04	2.17579E+02	-1.78941E+03	2.91172E+02	4.48332E+04	0.11788E+03	BEAMG	
59	39 JB	100.0	-1.62831E+04	-2.17579E+02	1.78941E+03	-2.91172E+02	4.71990E+03	-9.25850E+01	BEAMG	
60	39 JA	0.0	1.62831E+04	-4.36597E-11	-1.78941E+03	2.24083E+02	-4.72337E+03	9.25850E+01	BEAMG	
61	40 JB	100.0	-1.62831E+04	4.36597E-11	1.78941E+03	-2.24083E+02	1.24357E+04	-9.25850E+01	BEAMG	
62	11 JA	0.0	-1.47704E+04	-2.64176E+02	5.66552E+03	4.14755E+02	-1.77265E+05	-7.46391E+03	BEAMG	
63	41 JB	100.0	1.47704E+04	2.64176E+02	-5.66552E+03	-4.14755E+02	2.03726E+04	1.48211E+02	BEAMG	
64	41 JA	0.0	-1.97722E+04	5.82077E-11	5.66552E+03	1.42320E+02	-2.03726E+04	-1.48211E+02	BEAMG	

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+1	11	JA	0.0	1.67000E+03	-5.60000E-11	-1.70000E+03	2.20000E+02	-6.72337E+03	9.25950E+01	BEAMG
+1	40	JB	100.0	-1.67000E+03	4.60000E-11	1.70000E+03	-2.20000E+02	1.26357E+04	-9.25950E+01	
+0	11	JA	0.0	-1.97704E+04	-2.64176E+02	5.66552E+03	4.14755E+02	-1.7265E+05	-7.46741E+03	BEAMG
+0	41	JB	100.0	1.97704E+04	2.64176E+02	-5.66552E+03	-4.14755E+02	2.03726E+04	1.44211E+02	
+1	41	JA	0.0	-1.97722E+04	5.82077E-11	5.66552E+03	1.42220E+02	-2.03763E+04	-1.44211E+02	BEAMG
+1	42	JB	100.0	1.97722E+04	-5.82077E-11	-5.66552E+03	-1.42220E+02	-4.04205E+03	1.44211E+02	

NOZZLE LOAD CASE 1

MAXIMUM LOAD SUMMARY FOR

BEAM ELEMENT LOADS FOR OUTPUT VECTOR 1

AXIAL	SHEAR	SHEAR	TORSION	BENDING	BENDING
P	V2	V3	M1	M2	M3

MAXIMUM BEAM LOADS = 1.97722E+04 -5.90400E+03 -7.84757E+03 2.10294E+05 -6.30596E+05 -4.47252E+05
 BEAM NOS. = 41. 7. 36. 28. 11. 11.

MINIMUM BEAM LOADS = -1.62846E+04 -5.90400E+03 -7.84757E+03 -2.10294E+05 -7.40462E+05 -4.51416E+05
 BEAM NOS. = 39. 7. 36. 28. 11. 8.

NOZZLE LOAD CASE 1

BEAM	END-NODES--	BEAM	END	LOADS IN GLOBAL SYSTEM			FOR OUTPUT VECTOR	1
				FX1	FX2	FX3		
1	JA 1		JA	.407E+08	-.477E+08	-.204E+08	.596E+07	-.745E+08
	JB 4		JB	-.407E+08	-.477E+08	.204E+08	-.209E+06	-.994E+07
2	JA 3		JA	.295E+04	-.295E+04	-.140E+09	.903E+05	.903E+05
	JB 2		JB	-.295E+04	.295E+04	.140E+09	-.903E+05	-.903E+05
3	JA 3		JA	-.295E+04	.295E+04	.400E+08	-.903E+05	.903E+05
	JB 4		JB	.295E+04	-.295E+04	-.400E+08	.903E+05	-.903E+05
4	JA 4		JA	.295E+04	-.295E+04	.559E+08	.903E+05	.903E+05
	JB 5		JB	-.295E+04	.295E+04	-.559E+08	-.903E+05	-.903E+05
5	JA 5		JA	.295E+04	-.295E+04	-.116E+09	.903E+05	.903E+05
	JB 6		JB	-.295E+04	.295E+04	.116E+09	-.903E+05	-.903E+05
6	JA 4		JA	-.590E+04	.590E+04	.175E+09	-.312E+06	.312E+06
	JB 7		JB	.590E+04	-.590E+04	-.175E+09	.312E+06	-.335E+07
7	JA 7		JA	-.590E+04	.590E+04	.931E+09	-.312E+06	.312E+06
	JB 8		JB	.590E+04	-.590E+04	-.931E+09	.309E+06	-.359E+06
8	JA 8		JA	-.590E+04	.590E+04	.466E+09	-.369E+06	.359E+06
	JB 11		JB	.590E+04	-.590E+04	-.466E+09	.451E+06	-.410E+07
9	JA 10		JA	.611E+09	-.781E+04	.495E+09	.297E+05	.279E+08
	JB 9		JB	-.611E+09	.781E+04	-.495E+09	-.297E+06	-.745E+09
10	JA 10		JA	.735E+08	-.761E+04	-.140E+08	-.297E+06	.615E+07
	JB 11		JB	-.735E+08	.761E+04	.140E+08	.297E+06	-.829E+07
11	JA 11		JA	.472E+04	-.745E+04	.303E+08	-.740E+06	.447E+06
	JB 12		JB	-.472E+04	.745E+04	-.303E+08	.631E+06	.381E+06
12	JA 12		JA	-.472E+04	.785E+04	-.271E+08	-.631E+06	.381E+06
	JB 37		JB	-.472E+04	-.785E+04	.271E+08	.266E+06	.162E+06
13	JA 13		JA	.206E+03	.189E+04	-.16/E+04	-.257E+04	.105E+04
	JB 14		JB	-.206E+03	-.189E+04	.16/E+04	.698E+04	-.579E+01
14	JA 15		JA	.206E+03	-.189E+04	.16/E+04	.895E+04	-.579E+01
	JB 14		JB	.206E+03	.189E+04	-.16/E+04	.698E+04	.557E+04
15	JA 15		JA	.203E+03	.189E+04	-.16/E+04	-.405E+04	.579E+01
	JB 16		JB	-.203E+03	-.189E+04	.167E+04	.463E+05	-.579E+01
16	JA 16		JA	.661E+03	-.189E+04	.110E+04	-.285E+05	.540E+01
	JB 17		JB	.661E+03	.189E+04	-.110E+04	.380E+04	.540E+01
17	JA 17		JA	.661E+03	-.189E+04	.110E+04	-.388E+04	.540E+01
	JB 18		JB	.661E+03	.189E+04	-.110E+04	.653E+04	.580E+01
18	JA 19		JA	-.661E+03	.189E+04	-.110E+04	-.161E+05	.334E+04
	JB 18		JB	.661E+03	-.189E+04	.110E+04	.653E+04	-.580E+01
19	JA 20		JA	-.15+E+04	-.157E+03	-.178E+04	.789E+03	-.148E+05
	JB 21		JB	.154E+04	.157E+03	.178E+04	.416E+01	.704E+04
20	JA 22		JA	.154E+04	-.157E+03	.178E+04	.416E+01	-.984E+04
	JB 21		JB	-.154E+04	.157E+03	-.178E+04	.416E+01	.534E+04

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18	JA	19	-1.661E+03	-1.194E+04	-1.110E+01	-1.161E+05	-1.334E+04	-1.36E+04
	JB	18	-1.661E+03	-1.194E+04	-1.110E+01	-1.053E+04	-1.490E+01	-1.36E+04
19	JA	20	-1.154E+04	-1.157E+03	-1.178E+04	-1.789E+03	-1.148E+05	-1.385E+04
	JB	21	-1.154E+04	-1.157E+03	-1.178E+04	-1.416E+01	-1.704E+04	-1.355E+04
20	JA	22	-1.154E+04	-1.157E+03	-1.174E+04	-1.15E+01	-1.484E+04	-1.534E+04
	JB	21	-1.154E+04	-1.157E+03	-1.174E+04	-1.415E+01	-1.704E+04	-1.385E+04
21	JA	22	-1.154E+04	-1.157E+03	-1.174E+04	-1.416E+01	-1.934E+04	-1.534E+04
	JB	15	-1.154E+04	-1.157E+03	-1.178E+04	-1.416E+01	-1.494E+05	-1.487E+04
22	JA	16	-1.154E+04	-1.712E+03	-1.985E+03	-1.415E+01	-2.51E+05	-2.39E+05
	JB	23	-1.154E+04	-1.712E+03	-1.985E+03	-1.415E+01	-2.289E+04	-2.757E+04
23	JA	23	-1.154E+04	-1.712E+03	.985E+03	-1.415E+01	-2.89E+04	-7.87E+04
	JB	24	-1.154E+04	-1.712E+03	-1.985E+03	-1.415E+01	-1.547E+04	-1.110E+04
24	JA	25	-1.154E+04	-1.712E+03	-1.985E+03	-1.301E+04	-1.132E+04	-1.110E+04
	JB	24	-1.154E+04	-1.712E+03	-1.985E+03	-1.415E+01	-1.647E+04	-1.110E+04
25	JA	34	.119E+04	-1.352E+04	-1.552E+04	-1.128E+06	-1.447E+05	.903E+03
	JB	26	-1.119E+04	-1.352E+04	-1.552E+04	-1.128E+06	-1.362E+05	-1.903E+03
26	JA	26	-1.119E+04	-1.352E+04	-1.552E+04	-1.128E+06	-1.362E+05	-1.903E+03
	JB	27	-1.119E+04	-1.352E+04	-1.552E+04	-1.388E+06	-1.244E+05	-1.903E+03
27	JA	27	-1.119E+04	-1.352E+04	-1.552E+04	-1.388E+06	-1.244E+05	-1.903E+03
	JB	30	-1.119E+04	-1.352E+04	-1.552E+04	-1.438E+06	-1.141E+06	-1.903E+03
28	JA	29	-1.391E+04	-1.391E+04	-1.552E+04	-1.328E+06	-1.305E+05	-1.538E-09
	JB	28	-1.391E+04	-1.391E+04	-1.552E+04	-1.297E+06	-1.466E-08	0.
29	JA	29	-1.391E+04	-1.391E+04	-1.552E+04	-1.328E+06	-1.305E+05	-1.931E-09
	JB	30	-1.391E+04	-1.391E+04	-1.552E+04	-1.438E+06	-1.141E+06	-2.79E-08
30	JA	30	-1.192E+04	-1.747E+03	-1.694E-09	-1.164E+03	-1.366E+02	-2.41E+05
	JB	31	-1.192E+04	-1.747E+03	-1.694E-09	-1.184E+03	-1.366E+02	-2.34E+04
31	JA	31	-1.192E+04	-1.747E+03	.182E-10	-1.164E+03	-1.366E+02	.234E+04
	JB	32	-1.192E+04	-1.747E+03	-1.694E-09	-1.164E+03	-1.366E+02	.105E+04
32	JA	30	-1.803E+03	-1.117E+04	-1.419E-09	-1.119E+03	-1.563E+02	-2.325E+05
	JB	33	-1.403E+03	-1.117E+04	-1.419E-09	-1.119E+03	-1.563E+02	.996E+03
33	JA	33	-1.803E+03	-1.117E+04	-1.582E-10	-1.119E+03	-1.563E+02	-1.996E+03
	JB	34	-1.803E+03	-1.117E+04	-1.582E-10	-1.119E+03	-1.563E+02	-2.47E+04
34	JA	30	.131E-09	-1.698E-09	-1.931E-09	-1.447E-07	0.	0.
	JB	35	-1.31E-09	-1.698E-09	-1.931E-09	-1.298E-07	-1.745E-08	0.
35	JA	35	.873E-10	-2.04E-09	-1.233E-09	-1.373E-08	-1.279E-08	.116E-09
	JB	35	-1.973E-10	-2.04E-09	-1.233E-09	0.	-1.186E-08	-1.16E-09
36	JA	37	-1.472E+04	-1.785E+04	-1.140E-08	-1.266E+06	-1.162E+05	.664E+05
	JB	15	-1.472E+04	-1.785E+04	-1.140E-08	-1.144E+06	-1.827E+05	-1.664E+05
37	JA	16	.119E+04	-1.352E+04	-1.552E+04	-1.151E+06	-1.579E+05	.903E+03
	JB	38	-1.119E+04	-1.352E+04	-1.552E+04	-1.122E+06	-1.447E+05	-1.903E+03
38	JA	11	-1.163E+05	-1.179E+04	-1.147E-08	-1.490E+03	-1.612E+04	-1.448E+05
	JB	39	-1.163E+05	-1.179E+04	-1.147E-08	-1.228E+03	-1.926E+02	-1.472E+04
39	JA	19	-1.163E+05	-1.179E+04	.437E-10	-1.228E+03	-1.926E+02	.472E+04
	JB	40	-1.163E+05	-1.179E+04	-1.437E-10	-1.228E+03	-1.926E+02	-1.124E+05
40	JA	11	-1.567E+04	-1.194E+05	-1.375E-08	-1.745E+04	-1.195E+04	.177E+06
	JB	41	-1.567E+04	-1.194E+05	-1.375E-08	-1.145E+03	-1.143E+03	-2.04E+05
41	JA	41	-1.567E+04	-1.194E+05	-1.375E-08	-1.438E+03	-1.143E+03	.204E+05
	JB	42	-1.567E+04	-1.194E+05	-1.562E-10	-1.488E+03	-1.143E+03	-1.404E+04

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40	JA	42	$4.00E+03$	$-6.00E+04$	$-6.00E+10$	$+2.00E+03$	$-4.00E+02$	$-1.00E+05$
41	JA	41	$-5.67E+04$	$-1.00E+05$	$-5.67E+04$	$-7.00E+04$	$-1.00E+04$	$-2.04E+05$
	JH	42	$-5.67E+04$	$-1.00E+05$	$-5.67E+04$	$-5.67E+03$	$-1.00E+03$	$-4.04E+04$

NOZZLE LOAD CASE 1

BEAM STRESSES FOR OUTPUT VECTOR 1

BEAM --- TRANSVERSE --- TORSIONAL - STRESSES AT USER LOCATIONS - MAXIMUM MINIMUM COMBINED
 BEAM LOAD-LOCATION, SHEAR SHEAR (T²C/J) A B C (P/A+MC/I) (P/A-MC/I) SHEAR
 NO. NODE--PERCENT. (V2/K3°A) (V3/KK°A)

1	1	JA	0.0	$4.56E-11$	$5.34E-11$	$9.41E-13$	$-1.140E-11$	$-7.63E-12$	$-4.151E-11$	$1.8942E-11$	$-4.1745E-11$	$9.52E-12$
1	1	JH	100.0	$4.56E-11$	$5.34E-11$	$9.41E-13$	$-1.140E-11$	$-5.657E-11$	$-1.168E-10$	$1.0325E-10$	$-1.2605E-10$	$5.16E-11$
2	2	JA	0.0	$2.20E-11$	$-4.50E+02$	$-1.15E+03$	$2.293E+02$	$-2.088E+03$	$-4.570E+02$	$2.6457E+03$	$-2.1872E+03$	$1.76E+03$
2	2	JH	100.0	$2.20E-11$	$-4.50E+02$	$-1.15E+03$	$2.293E+02$	$-2.088E+03$	$2.293E+02$	$2.5462E+03$	$-2.0877E+03$	$1.72E+03$
3	3	JA	0.0	$-9.31E-12$	$-5.90E+00$	$-2.26E-01$	$5.904E+00$	$5.678E+00$	$5.971E+00$	$6.1966E+00$	$5.5114E+00$	$3.11E+00$
3	3	JH	100.0	$-9.31E-12$	$-5.90E+00$	$-2.26E-01$	$5.904E+00$	$5.678E+00$	$6.146E+00$	$6.3714E+00$	$5.4366E+00$	$3.19E+00$
4	4	JA	0.0	$-1.12E-11$	$5.90E+00$	$2.26E-01$	$-5.904E+00$	$-5.678E+00$	$-5.662E+00$	$-5.4366E+00$	$-6.3714E+00$	$2.73E+00$
4	4	JH	100.0	$-1.12E-11$	$5.90E+00$	$2.26E-01$	$-5.904E+00$	$-5.678E+00$	$-5.837E+00$	$-5.6114E+00$	$-6.1966E+00$	$2.81E+00$
5	5	JA	0.0	$1.01E-11$	$4.50E+02$	$1.16E+03$	$-2.293E+02$	$2.088E+03$	$4.570E+02$	$2.1872E+03$	$-2.6457E+03$	$1.54E+03$
5	5	JH	100.0	$1.01E-11$	$4.50E+02$	$1.16E+03$	$-2.293E+02$	$2.088E+03$	$-2.293E+02$	$2.0877E+03$	$-2.5462E+03$	$1.56E+03$
6	6	JA	0.0	$-6.01E+01$	$-5.61E+01$	$8.47E-12$	$9.773E-13$	$9.123E+01$	$9.123E+01$	$1.2902E+02$	$-1.2902E+02$	$6.45E+01$
6	6	JH	100.0	$-6.01E+01$	$-5.61E+01$	$8.47E-12$	$9.773E-13$	$1.576E+02$	$1.576E+02$	$2.2286E+02$	$-2.2286E+02$	$1.11E+02$
7	7	JA	0.0	$-1.69E+02$	$-1.69E+02$	$3.15E-11$	$1.332E-11$	$4.056E+02$	$4.056E+02$	$5.7364E+02$	$-5.7364E+02$	$2.87E+02$
7	7	JH	100.0	$-1.69E+02$	$-1.69E+02$	$3.15E-11$	$1.332E-11$	$4.795E+02$	$4.795E+02$	$6.7807E+02$	$-6.7807E+02$	$3.39E+02$
8	8	JA	0.0	$-1.09E+02$	$-1.09E+02$	$1.38E-11$	$4.283E-12$	$2.477E+02$	$2.477E+02$	$3.5033E+02$	$-3.5033E+02$	$1.75E+02$
8	8	JH	100.0	$-1.09E+02$	$-1.09E+02$	$1.38E-11$	$4.283E-12$	$3.032E+02$	$3.032E+02$	$4.2986E+02$	$-4.2986E+02$	$2.14E+02$
9	9	JA	0.0	$-4.06E-11$	$-4.53E+02$	$-1.15E+03$	$2.268E+02$	$-2.072E+03$	$-2.452E+02$	$2.5733E+03$	$-2.1196E+03$	$1.73E+03$
9	9	JH	100.0	$-4.06E-11$	$-4.53E+02$	$-1.15E+03$	$2.268E+02$	$-2.072E+03$	$-2.268E+02$	$2.5253E+03$	$-2.0717E+03$	$1.71E+03$
10	10	JA	0.0	$2.79E-12$	$-1.10E+01$	$-5.24E+01$	$1.105E+01$	$1.052E+01$	$1.115E+01$	$1.1679E+01$	$1.0411E+01$	$5.86E+00$
10	10	JH	100.0	$2.79E-12$	$-1.10E+01$	$-5.24E+01$	$1.105E+01$	$1.052E+01$	$1.154E+01$	$1.2058E+01$	$1.0022E+01$	$6.06E+00$
11	11	JA	0.0	$8.57E+01$	$1.44E+02$	$2.23E+01$	$-2.784E-11$	$3.005E+02$	$4.974E+02$	$5.8112E+02$	$-5.8112E+02$	$2.91E+02$
11	12	JH	100.0	$8.57E+01$	$1.44E+02$	$2.23E+01$	$-2.784E-11$	$2.561E+02$	$4.236E+02$	$4.9502E+02$	$-4.4502E+02$	$2.44E+02$
12	12	JA	0.0	$1.35E+02$	$2.25E+02$	$4.32E+01$	$-3.872E-11$	$4.957E+02$	$8.199E+02$	$9.5811E+02$	$-9.5811E+02$	$4.81E+02$
12	37	JH	100.0	$1.35E+02$	$2.25E+02$	$4.32E+01$	$-3.872E-11$	$2.105E+02$	$3.454E+02$	$4.0456E+02$	$-4.0460E+02$	$2.07E+02$
13	13	JA	0.0	$-3.75E+00$	$4.10E-01$	$8.99E-03$	$3.331E+00$	$3.325E+00$	$3.334E+00$	$3.3403E+00$	$3.3222E+00$	$1.67E+00$
13	14	JH	100.0	$-3.75E+00$	$4.10E-01$	$8.99E-03$	$3.331E+00$	$3.349E+00$	$3.331E+00$	$3.3487E+00$	$3.3138E+00$	$1.67E+00$
14	15	JA	0.0	$-4.46E+01$	$6.07E+00$	$6.92E-01$	$5.506E+01$	$6.674E+01$	$7.283E+01$	$1.2722E+02$	$-1.7106E+01$	$6.36E+01$
14	14	JH	100.0	$-4.46E+01$	$6.07E+00$	$6.92E-01$	$5.506E+01$	$9.797E+01$	$6.653E+01$	$1.0944E+02$	$6.7559E-01$	$5.47E+01$
15	15	JA	0.0	$3.33E+00$	$4.10E-01$	$1.045E-05$	$3.776E+00$	$3.754E+00$	$3.762E+00$	$3.8119E+00$	$3.7399E+00$	$1.91E+00$
15	16	JH	100.0	$3.33E+00$	$4.10E-01$	$1.045E-05$	$3.776E+00$	$3.660E+00$	$3.750E+00$	$3.9173E+00$	$3.6345E+00$	$1.96E+00$
16	16	JA	0.0	$-2.19E+00$	$1.32E+00$	$-1.45E-05$	$-3.771E+00$	$-3.842E+00$	$-3.715E+00$	$+3.6433E+00$	$-3.8985E+00$	$1.82E+00$
16	17	JH	100.0	$-2.19E+00$	$1.32E+00$	$-1.45E-05$	$-3.771E+00$	$-3.781E+00$	$-3.752E+00$	$-3.7421E+00$	$-3.7997E+00$	$1.87E+00$
17	17	JA	0.0	$-3.20E+01$	$1.93E+01$	$-6.94E-01$	$-5.499E+01$	$-7.486E+01$	$-3.064E+01$	$-6.7592E+00$	$-1.0320E+02$	$3.46E+00$
17	18	JH	100.0	$-3.20E+01$	$1.93E+01$	$-6.94E-01$	$-5.499E+01$	$-1.484E+01$	$-5.066E+01$	$-1.0517E+01$	$-9.9455E+01$	$5.30E+00$
18	19	JA	0.0	$3.77E+00$	$1.32E+00$	$3.39E-03$	$2.192E+00$	$2.232E+00$	$2.200E+00$	$2.2403E+00$	$2.1432E+00$	$1.12E+00$
18	19	JH	100.0	$3.77E+00$	$1.32E+00$	$3.39E-03$	$2.192E+00$	$2.204E+00$	$2.192E+00$	$2.2081E+00$	$2.1754E+00$	$1.10E+00$
19	20	JA	0.0	$3.07E+00$	$3.14E-01$	$9.43E-03$	$3.553E+00$	$3.590E+00$	$3.555E+00$	$3.5920E+00$	$3.5140E+00$	$1.80E+00$
19	21	JH	100.0	$3.07E+00$	$3.14E-01$	$9.63F-03$	$3.553E+00$	$3.571E+00$	$3.553E+00$	$3.5706E+00$	$3.5354E+00$	$1.79E+00$

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40	10 JA	0.0	-6.60E-12	1.13E+01	-1.04E-03	-1.809E+03	-1.009E+03	-1.009E+03	-1.009E+03	-1.009E+03	-1.009E+03	-1.009E+03	0.00E+02	BEAM0
40	40 JB	100.0	-6.60E-12	1.13E+01	-1.04E-03	-1.809E+03	-1.009E+03	-1.009E+03	-1.009E+03	-1.009E+03	-1.009E+03	-1.009E+03	0.74E+02	BEAM0
40	11 JA	0.0	-5.28E-01	1.13E+01	-1.04E-03	3.954E+01	3.952E+01	3.998E+01	4.0003E+01	3.9079E+01	2.00E+01	2.00E+01	BEAM0	
40	41 JB	100.0	-5.28E-01	1.13E+01	-1.04E-03	3.954E+01	3.954E+01	3.954E+01	3.954E+01	3.954E+01	3.9489E+01	1.98E+01	BEAM0	
41	41 JA	0.0	6.47E-12	6.30E+02	-6.30E+01	2.197E+03	1.143E+03	2.232E+03	3.2859E+03	1.1079E+03	1.64E+03	1.64E+03	BEAM0	
41	42 JB	100.0	6.47E-12	6.30E+02	-6.30E+01	2.197E+03	1.143E+03	2.190E+03	3.2576E+03	1.1363E+03	1.63E+03	1.63E+03	BEAM0	

NOZZLE LOAD CASE 1

MAXIMUM STRESS SUMMARY FOR

BEAM STRESSES FOR OUTPUT VECTOR 1						
--- TRANSVERSE --- TORSIONAL - STRESSES AT USER LOCATIONS -						
SHEAR (T ^o C/J)	A	B	C	MAXIMUM (P/A+MC/I)	MINIMUM (P/A-MC/I)	COMBINED STRESS
(V2/K3 ^o A) (V3/KC ^o A)						

MAX. BEAM STRESSES = 4.53E+02 6.30E+02 1.16E+03 2.197E+03 2.544E+03 2.232E+03 3.2859E+03 1.1363E+03 1.76E+03
 BEAM NOS. = 28. 41. 5. 41. 28. 41. 41. 41. 2.

MIN. BEAM STRESSES = -1.69E+02 -4.5dE+02 -1.16E+03 -1.809E+03 -2.088E+03 -1.801E+03 -1.1430E+03 -2.9974E+03 2.8RE-12
 BEAM NOS. = 7. 2. 2. 39. 2. 39. 39. 28. 35.

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B E G I N I N P U T L O A D C A S E N O . 2 T I T L E(N O Z Z L E L O A D C A S E 2

NODAL POINT APPLIED FORCES FOR LOAD CASE NO. 2

NODE	X1	X2	X3	X4	X5	X6
2	-2.952000E+03	-2.952000E+03	0.	-9.030000E+04	-9.030000E+04	0.
6	-2.952000E+03	-2.952000E+03	0.	-9.030000E+04	-9.030000E+04	0.
28	3.905000E+03	-3.905000E+03	-5.523000E+03	2.974000E+05	0.	0.
9	0.	7.810000E+03	0.	-2.974000E+05	0.	0.

NODAL POINT APPLIED LOADS AND/OR DISPLACEMENTS FINAL SUMMARY FOR LOAD CASE NO. 2

NODE	X1	X2	X3	X4	X5	X6
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NOTE IF A FINAL SUMMARY OF APPLIED NODAL LOADS AND GENERATED LOADS IS DESIRED AT THIS POINT,
CODE A 1. IN COLUMN 20 OF THE STATIC CARD.

FORCE AND MOMENT SUMMATION
ABOUT AXES PARALLEL TO SYSTEM AXES
WITH ORIGIN AT POINT (0,0,0)
SUMMATION INCLUDES LOADS APPLIED TO RESTRAINED DOF.

FX1	=	-1.9990000000E+04
FX2	=	.9909400000E+04
FX3	=	-.5523000000E+04
MX1	=	-.40805555700E+07
MX2	=	-.13400227700E+07
MX3	=	-.19234260000E+06

NOZZLE LOAD CASE 2

			H.E.A.M.	E.L.E.M.E.N.T.	L.O.A.D.S.	FOR OUTPUT VECTOR	2	
BEAM	LOAD-LOCATION.	NU	AXIAL	SHEAR	SHEAR	TORSION	BENDING	BENDING
			P	V2	V3	M1	M2	M3
1	1 JA	0.0	1.45519E-09	3.14321E-09	4.77303E-09	0.	4.47035E-08	7.45058E-09 PIPEG
1	4 JB	100.0	-1.45519E-09	-3.14321E-09	-4.77303E-09	0.	-1.93715E-07	5.96046E-08
2	3 JA	0.0	-2.95200E+03	-1.45519E-10	-2.95200E+03	9.03000E+04	2.67451E+04	-9.03000E+04 PIPEG
2	2 JB	100.0	2.95200E+03	-1.45519E-10	2.95200E+03	-9.03000E+04	2.79397E-09	9.03000E+04
3	3 JA	0.0	-2.95200E+03	-3.72529E-09	-2.95200E+03	9.03000E+04	-2.67451E+04	-9.03000E+04 BEAMG
3	4 JB	100.0	2.95200E+03	3.72529E-09	2.95200E+03	-9.03000E+04	9.66790E+04	9.03000E+04
4	4 JA	0.0	2.95200E+03	-2.79397E-09	2.95200E+03	-9.03000E+04	-9.66780E+04	9.03000E+04 BEAMG
5	5 JA	100.0	-2.95200E+03	2.79397E-09	-2.95200E+03	9.03000E+04	2.67451E+04	-9.03000E+04
5	6 JB	100.0	2.95200E+03	-1.16415E-10	-2.95200E+03	9.03000E+04	-2.29920E-09	9.03000E+04 PIPEG
6	4 JA	0.0	2.27010E-09	-5.90400E+03	-5.90400E+03	-3.72529E-08	-1.80600E+05	1.80500E+05 PIPEG
5	7 JB	100.0	-2.27010E-09	5.90400E+03	5.90400E+03	3.72529E-08	3.11964E+05	-3.11964E+05
7	7 JA	0.0	2.39651E-09	-5.90400E+03	-5.90400E+03	-5.51926E-08	-3.11964E+05	3.11964E+05 PIPEG
8	8 JB	100.0	-2.39651E-09	5.90400E+03	5.90400E+03	5.51926E-08	3.68760E+05	-3.68760E+05
9	2 JA	0.0	3.08501E-09	-5.90400E+03	-5.90400E+03	-2.98023E-08	-3.68760E+05	3.68760E+05 PIPEG
9	11 JB	100.0	-3.08501E-09	5.90400E+03	5.90400E+03	2.98023E-08	4.51416E+05	-4.51416E+05
9	10 JA	0.0	-5.52250E+03	-2.91038E-11	-5.52250E+03	2.10294E+05	4.31893E+04	-2.10294E+05 PIPEG
9	9 JB	100.0	5.52250E+03	2.91038E-11	5.52250E+03	-2.10294E+05	3.25963E-09	2.10294E+05
10	10 JA	0.0	-5.52250E+03	6.98472E-10	-5.52250E+03	2.10294E+05	-4.31893E+04	-2.10294E+05 BEAMG
10	11 JB	100.0	5.52250E+03	-6.98472E-10	5.52250E+03	-2.10294E+05	1.9843E+05	2.10294E+05
11	11 JA	0.0	5.93718E-09	5.00595E+03	8.75039E+03	-6.87952E+04	-7.40121E+05	4.47142E+05 PIPEG
11	12 JB	100.0	-5.93718E-09	-5.00595E+03	-8.75039E+03	6.87952E+04	6.17616E+05	-3.77059E+05
12	12 JA	0.0	6.37374E-09	-5.00595E+03	8.75039E+03	-6.87952E+04	-6.17616E+05	3.77059E+05 PIPEG
12	37 JB	100.0	-6.37374E-09	-5.00595E+03	-8.75039E+03	6.87952E+04	2.10723E+05	-1.44222E+05
13	13 JA	0.0	4.15744E+03	-5.23904E+03	3.29303E+01	-4.29669E+03	-1.87346E+02	-3.53065E+04 BEAMG
13	14 JB	100.0	-4.15744E+03	5.23904E+03	-3.29303E+01	4.29669E+03	2.07186E+01	8.79695E+03
14	15 JA	0.0	-5.23904E+03	4.15744E+03	3.29303E+01	-2.07186E+01	-4.60953E+03	3.06987E+04 BEAMG
14	14 JB	100.0	5.23904E+03	-4.15744E+03	-3.29303E+01	2.07186E+01	4.29669E+03	8.79695E+03
15	15 JA	0.0	-5.23904E+03	-4.15744E+03	3.29303E+01	-2.07186E+01	4.60953E+03	3.06987E+04 BEAMG
15	16 JB	100.0	5.23904E+03	4.15744E+03	-3.29303E+01	2.07186E+01	-5.35046E+03	-1.24241E+05
16	16 JA	0.0	5.24152E+03	-1.39594E+03	8.04466E+02	2.07344E+01	-2.62206E+04	-4.93797E+04 BEAMG
16	17 JB	100.0	-5.24152E+03	1.39594E+03	-8.04466E+02	-2.07344E+01	8.12010E+03	1.79711E+04
17	17 JA	0.0	5.24152E+03	-1.39594E+03	8.04466E+02	2.07344E+01	-8.12010E+03	-1.79711E+04 BEAMG
17	18 JB	100.0	-5.24152E+03	1.39594E+03	-8.04466E+02	-2.07344E+01	4.77677E+02	4.70968E+03
18	19 JA	0.0	-1.39594E+03	5.24152E+03	8.04466E+02	-4.77677E+02	-4.04986E+03	2.18124E+04 BEAMG
18	18 JB	100.0	1.39594E+03	-5.24152E+03	-8.04466E+02	4.77677E+02	-2.07344E+01	4.70968E+03
19	20 JA	0.0	-3.55634E+01	2.62323E+03	-3.52292E+02	-5.20349E+03	1.74197E+03	7.56297E+03 BEAMG
19	21 JB	100.0	3.55634E+01	-2.62323E+03	3.52292E+02	6.20349E+03	4.06265E+01	5.71058E+03

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17	17 JA	0.0	5.24152E+03	-1.39374E+03	8.04466E+01	2.07344E+01	-8.12010E+03	-1.79711E+04	BEAMG
17	18 JA	100.0	-5.24152E+03	1.39374E+03	-8.04466E+01	-2.07344E+01	4.77677E+02	4.70964E+03	
18	19 JA	0.0	-1.39374E+03	5.24152E+03	-8.04466E+02	-4.77677E+02	-4.04986E+03	2.18124E+04	BEAMG
18	18 JA	100.0	1.39374E+03	-5.24152E+03	-8.04466E+02	4.77677E+02	-2.07344E+01	4.70964E+03	
19	20 JA	0.0	-3.55834E+01	2.62323E+03	-3.52292E+02	-6.20349E+03	1.74197E+03	7.56297E+03	BEAMG
19	21 JA	100.0	3.55834E+01	-2.62323E+03	3.52292E+02	6.20349E+03	4.06265E+01	5.71058E+03	
20	22 JA	0.0	-2.62323E+03	-3.55834E+01	-3.52292E+02	-4.06265E+01	-2.85672E+03	-6.04862E+03	BEAMG
20	21 JA	100.0	2.62323E+03	3.55834E+01	3.52292E+02	4.06265E+01	6.20349E+03	5.71058E+03	
21	22 JA	0.0	2.62323E+03	3.55834E+01	-3.52292E+02	-4.06265E+01	2.85672E+03	-6.04862E+03	BEAMG
21	16 JA	100.0	-2.62323E+03	-3.55834E+01	-3.52292E+02	-4.06265E+01	5.06985E+03	6.84925E+03	
22	23 JA	0.0	-2.62075E+03	2.79708E+03	1.18909E+03	4.06424E+01	-3.66409E+04	8.17106E+04	BEAMG
22	23 JA	100.0	2.62075E+03	-2.79708E+03	-1.18909E+03	-4.06424E+01	9.87291E+03	-1.87762E+04	
23	23 JA	0.0	-2.62075E+03	2.79708E+03	1.18909E+03	4.06424E+01	-9.87291E+03	1.87762E+04	BEAMG
23	24 JA	100.0	2.62075E+03	-2.79708E+03	-1.18909E+03	-4.06424E+01	-1.42913E+03	7.79605E+03	
24	25 JA	0.0	2.79708E+03	-2.62075E+03	1.18909E+03	1.42913E+03	-5.97918E+03	-2.10571E+04	BEAMG
24	24 JA	100.0	-2.79708E+03	2.62075E+03	-1.18909E+03	-1.42913E+03	-4.06424E+01	7.79605E+03	
25	38 JA	0.0	-5.52300E+03	-1.00957E+03	-3.27216E+03	-5.65415E+03	7.35778E+04	-1.72325E+04	PIPEG
25	26 JA	100.0	5.52300E+03	1.00957E+03	3.27216E+03	5.65415E+03	-1.49551E+05	-5.16098E+04	
26	27 JA	0.0	-5.52300E+03	-1.00957E+03	-3.27216E+03	-5.65415E+03	-1.49551E+05	5.16098E+04	PIPEG
26	27 JA	100.0	5.52300E+03	1.00957E+03	3.27216E+03	5.65415E+03	3.91887E+05	-1.26378E+05	
27	27 JA	0.0	-5.52300E+03	-1.00957E+03	-3.27216E+03	-5.65415E+03	-3.91887E+05	1.26378E+05	PIPEG
27	30 JA	100.0	5.52300E+03	1.00957E+03	3.27216E+03	5.65415E+03	4.37697E+05	-1.40512E+05	
28	29 JA	0.0	-5.52250E+03	-5.52300E+03	8.23093E-11	-2.10294E+05	-6.11180E-10	-2.53487E+05	PIPEG
28	28 JA	100.0	5.52250E+03	5.52300E+03	-8.23093E-11	2.10294E+05	-1.45519E-11	2.10294E+05	
29	29 JA	0.0	-5.52250E+03	5.52300E+03	-1.45519E-10	-2.10294E+05	-1.86265E-09	-2.53487E+05	BEAMG
29	30 JA	100.0	5.52250E+03	-5.52300E+03	1.45519E-10	2.10294E+05	5.58794E-09	4.09154E+05	
30	30 JA	0.0	-2.00539E+03	-1.16415E-09	-6.51941E+02	-1.93086E+02	2.01331E+04	-4.07667E+01	BEAMG
30	31 JA	100.0	2.00539E+03	1.16415E-09	6.51941E+02	1.93086E+02	-2.08085E+03	4.07667E+01	
31	31 JA	0.0	-2.00539E+03	3.27418E-11	-6.51941E+02	-1.93086E+02	2.08085E+03	-4.07667E+01	BEAMG
31	32 JA	100.0	2.00539E+03	-3.27418E-11	6.51941E+02	1.93086E+02	7.29015E+02	4.07667E+01	
32	30 JA	0.0	1.28473E+03	-2.79397E-09	8.89544E+02	-6.2172E+01	-2.57872E+04	1.25508E+02	BEAMG
32	33 JA	100.0	-1.28473E+03	2.79397E-09	-8.89544E+02	6.2172E+01	1.15578E+03	-1.25508E+02	
33	33 JA	0.0	1.28473E+03	-2.91038E-11	8.89544E+02	-6.27172E+01	-1.15578E+03	1.25508E+02	BEAMG
33	34 JA	100.0	-1.28473E+03	2.91038E-11	-8.89544E+02	6.27172E+01	-2.57815E+03	-1.25508E+02	
34	30 JA	0.0	9.31323E-10	-1.16415E-10	-5.82077E-10	0.	2.98023E-08	7.45058E-09	PIPEG
34	35 JA	100.0	-9.31323E-10	1.16415E-10	5.82077E-10	0.	-4.47035E-08	0.	
35	35 JA	0.0	4.65661E-10	-7.27596E-11	-3.49246E-10	1.16415E-10	3.72529E-09	1.86265E-09	PIPEG
35	36 JA	100.0	-4.65661E-10	7.27596E-11	3.49246E-10	-1.16415E-10	0.	-1.86265E-09	
35	37 JA	0.0	7.45058E-09	5.00595E+03	8.75039E+03	-6.87962E+04	-2.10723E+05	1.44282E+05	PIPEG
36	16 JA	100.0	-7.45058E-09	-5.00595E+03	-8.75039E+03	6.87962E+04	6.35415E+04	-6.00819E+04	
37	16 JA	0.0	-5.52300E+03	-1.00957E+03	-3.27216E+03	-5.65415E+03	1.10161E+05	-2.85194E+04	PIPEG
37	32 JA	100.0	5.52300E+03	1.00957E+03	3.27216E+03	5.65415E+03	-7.35778E+04	1.72325E+04	
38	11 JA	0.0	1.67345E+04	2.23010E+02	-2.04577E+03	2.91377E+02	5.22350E+04	6.28596E+03	BEAMG
38	39 JA	100.0	-1.67345E+04	-2.23010E+02	2.04577E+03	-2.91377E+02	4.41742E+03	-9.36383E+01	
39	39 JA	0.0	1.67345E+04	-2.91038E-11	-2.04577E+03	2.32329E+02	-4.42042E+03	9.36383E+01	BEAMG
39	40 JA	100.0	-1.67345E+04	2.91038E-11	2.04577E+03	-2.32329E+02	1.32382E+04	-9.36383E+01	
40	11 JA	0.0	-2.04158E+04	-2.72814E+02	5.82606E+03	4.24033E+02	-1.82283E+05	-7.70585E+03	BEAMG
40	41 JA	100.0	2.04158E+04	2.72814E+02	-5.82606E+03	-4.24033E+02	2.09454E+04	1.50970E+02	
41	41 JA	0.0	-2.04158E+04	8.73115E-11	5.82606E+03	1.44142E+02	-2.09454E+04	-1.50970E+02	BEAMG
41	42 JA	100.0	2.04158E+04	-8.73115E-11	-5.82606E+03	-1.44142E+02	-6.15100E+02	1.50970E+02	

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41	34	0.0	-2.04105E+04	-2.72514E+02	5.82606E+03	4.24033E+02	-1.82283E+05	-7.70585E+03	BEAMG	
41	34	100.0	2.04105E+04	2.72514E+02	-5.82606E+03	-4.24033E+02	2.09454E+04	1.50970E+02		
+1	41	34	0.0	-2.04105E+04	5.73115E-11	5.82606E+03	1.44142E+02	-2.09492E+04	-1.50970E+02	BEAMG
+1	42	34	100.0	2.04105E+04	-8.73115E-11	-5.82606E+03	-1.44142E+02	-4.16109E+03	1.50970E+02	

NOZZLE LOAD CASE 2

MAXIMUM LOAD SUMMARY FOR

BEAM ELEMENT LOADS				FOR OUTPUT VECTOR 2	
AXIAL	SHEAR	SHEAR	TORSION	BENDING	BENDING
P	V2	V3	M1	M2	M3

MAXIMUM BEAM LOADS = 2.04105E+04 5.90400E+03 8.75039E+03 -2.10294E+05 -6.17616E+05 -4.47142E+05
 BEAM NOS. = 41. 34. 36. 28. 11. 11.

MINIMUM BEAM LOADS = -1.67350E+04 -5.90400E+03 -8.75039E+03 -2.10294E+05 -7.40121E+05 -4.51416E+05
 BEAM NOS. = 39. 34. 36. 28. 11. 8.

NOZZLE LOAD CASE 2

BEAM	--NODES--		BEAM			END LOADS IN GLOBAL SYSTEM			FOR OUTPUT VECTOR		
			FX1	FX2	FX3	MX1	MX2	MX3	2	2	2
1	JA	1	.314E+08	-6477E-08	-146E-08	.447E-07	.745E-08	0.	0.	0.	0.
	JB	4	-.314E+08	.4477E-08	.146E-08	-.194E-06	-.596E-07	0.			
2	JA	3	.295E+04	-.295E+04	-.295E+04	-.145E-09	.903E+05	.903E+05	-.267E+05	-.274E+08	0.
	JB	2	-.295E+04	.295E+04	.295E+04	.140E-09	-.903E+05	-.903E+05			
3	JA	3	-.295E+04	.295E+04	.295E+04	.373E-08	-.903E+05	-.903E+05	.267E+05	.274E+08	0.
	JB	4	.295E+04	-.295E+04	-.295E+04	-.373E-08	.903E+05	.903E+05			
4	JA	4	.295E+04	-.295E+04	-.295E+04	.274E-08	-.903E+05	-.903E+05	.967E+05	.967E+05	0.
	JB	5	-.295E+04	.295E+04	.295E+04	-.274E-08	.903E+05	.903E+05			
5	JA	5	.295E+04	-.295E+04	-.295E+04	-.116E-09	.903E+05	.903E+05	.267E+05	.274E+08	0.
	JB	6	-.295E+04	.295E+04	.295E+04	.116E-09	-.903E+05	-.903E+05			
6	JA	6	-.590E+04	.590E+04	.590E+04	-.227E-08	-.181E+06	-.181E+06	.373E-07	.373E-07	0.
	JB	7	.590E+04	-.590E+04	-.590E+04	.227E-08	.312E+06	.312E+06			
7	JA	7	-.590E+04	.590E+04	.590E+04	-.234E-08	-.312E+06	-.312E+06	.652E-07	.652E-07	0.
	JB	8	.590E+04	-.590E+04	-.590E+04	.234E-08	.369E+06	.369E+06			
8	JA	8	-.590E+04	.590E+04	.590E+04	-.304E-08	-.369E+06	-.369E+06	.298E-07	.298E-07	0.
	JB	11	.590E+04	-.590E+04	-.590E+04	.304E-08	.451E+06	.451E+06			
9	JA	10	.132E-08	-.781E+04	-.781E+04	.291E-10	.297E+06	.297E+06	.466E-08	.432E+05	0.
	JB	9	-.132E-08	.781E+04	.781E+04	-.291E-10	-.297E+06	-.297E+06			
10	JA	10	.803E-08	-.781E+04	-.781E+04	-.698E-09	-.237E+06	-.230E+06	.432E+05	.432E+05	0.
	JB	11	-.803E-08	.781E+04	.781E+04	.698E-09	.297E+06	.230E+06			
11	JA	11	.501E+04	-.875E+04	-.875E+04	-.594E-08	-.740E+06	-.447E+06	.688E+05	.688E+05	0.
	JB	12	-.501E+04	.875E+04	.875E+04	.594E-08	.618E+06	.377E+06			
12	JA	12	.501E+04	-.875E+04	-.875E+04	-.637E-08	-.618E+06	-.377E+06	.688E+05	.688E+05	0.
	JB	37	-.501E+04	.875E+04	.875E+04	.637E-08	.211E+06	.144E+06			
13	JA	13	.329E+02	.524E+04	.524E+04	.416E+04	-.353E+05	.187E+03	-.430E+04	-.430E+04	0.
	JB	14	-.329E+02	-.524E+04	-.524E+04	-.416E+04	.880E+04	-.207E+02			
14	JA	15	.329E+02	-.524E+04	-.524E+04	-.416E+04	-.416E+04	-.307E+05	.461E+04	.461E+04	0.
	JB	14	-.329E+02	.524E+04	.524E+04	.416E+04	-.880E+04	.207E+02			
15	JA	15	.329E+02	-.524E+04	-.524E+04	-.416E+04	-.416E+04	.307E+05	.207E+02	.461E+04	0.
	JB	16	-.329E+02	.524E+04	.524E+04	.416E+04	-.416E+04	-.124E+06			
16	JA	16	.804E+03	-.524E+04	-.524E+04	-.140E+04	-.494E+05	-.207E+02	.262E+05	.812E+04	0.
	JB	17	-.804E+03	.524E+04	.524E+04	.140E+04	-.180E+05	.207E+02			
17	JA	17	.604E+03	-.524E+04	-.524E+04	.140E+04	-.180E+05	-.207E+02	.812E+04	.478E+03	0.
	JB	18	-.604E+03	.524E+04	.524E+04	.140E+04	-.471E+04	.207E+02			
18	JA	19	-.604E+03	.524E+04	.524E+04	-.140E+04	-.218E+05	-.405E+04	.478E+03	.478E+03	0.
	JB	15	.604E+03	-.524E+04	-.524E+04	.140E+04	-.471E+04	.207E+02			
19	JA	20	-.252E+04	.352E+03	.352E+03	-.350E+02	-.174E+04	-.756E+04	.620E+04	.620E+04	0.
	JB	21	.252E+04	-.352E+03	-.352E+03	.350E+02	.406E+02	.571E+04			
20	JA	22	-.252E+04	.352E+03	.352E+03	-.356E+02	-.406E+02	-.605E+04	.286E+04	.620E+04	0.
	JB	21	.252E+04	-.352E+03	-.352E+03	.356E+02	.406E+02	.571E+04			

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	JA	18	-0.804E+03	.524E+04	-0.140E+04	.471E+04	.207E+02	-0.478E+03
	JA	19	-0.804E+03	.524E+04	-0.140E+04	-0.218E+05	-0.405E+04	-0.478E+03
19	JB	18	-0.804E+03	-0.524E+04	-0.140E+04	-0.471E+04	-0.207E+02	-0.478E+03
	JA	20	-0.252E+04	.352E+03	-0.350E+02	-0.174E+04	-0.756E+04	-0.620E+04
	JB	21	-0.252E+04	-0.352E+03	-0.350E+02	-0.405E+02	-0.571E+04	-0.620E+04
20	JA	22	-0.252E+04	-0.352E+03	-0.350E+02	-0.400E+02	-0.605E+04	-0.286E+04
	JB	21	-0.252E+04	-0.352E+03	-0.350E+02	-0.405E+02	-0.571E+04	-0.620E+04
21	JA	22	-0.262E+04	.352E+03	-0.350E+02	-0.405E+02	-0.605E+04	-0.286E+04
	JB	16	-0.262E+04	-0.352E+03	-0.350E+02	-0.405E+02	-0.605E+04	-0.507E+04
22	JA	16	-0.252E+04	-0.119E+04	-0.200E+04	-0.405E+02	-0.817E+05	-0.366E+05
	JB	23	-0.252E+04	-0.119E+04	-0.200E+04	-0.405E+02	-0.188E+05	-0.987E+04
23	JA	23	-0.262E+04	-0.119E+04	-0.200E+04	-0.405E+02	-0.198E+05	-0.987E+04
	JB	24	-0.262E+04	-0.119E+04	-0.200E+04	-0.405E+02	-0.780E+04	-0.143E+04
24	JA	25	-0.262E+04	-0.119E+04	-0.200E+04	-0.598E+04	-0.211E+05	-0.143E+04
	JB	24	-0.262E+04	-0.119E+04	-0.200E+04	-0.406E+02	-0.780E+04	-0.143E+04
25	JA	38	-0.101E+04	.327E+04	-0.552E+04	-0.735E+05	.172E+05	.565E+04
	JB	26	-0.101E+04	-0.327E+04	-0.552E+04	-0.150E+06	.516E+05	-0.565E+04
26	JA	26	-0.101E+04	.327E+04	-0.552E+04	-0.150E+06	-0.516E+05	.565E+04
	JB	27	-0.101E+04	-0.327E+04	-0.552E+04	-0.392E+05	.126E+06	-0.565E+04
27	JA	27	-0.101E+04	.327E+04	-0.552E+04	-0.392E+06	-0.125E+06	.565E+04
	JB	30	-0.101E+04	-0.327E+04	-0.552E+04	-0.418E+06	.141E+06	-0.565E+04
28	JA	29	-0.391E+04	.391E+04	-0.552E+04	-0.328E+06	-0.305E+05	.611E-09
	JB	28	-0.391E+04	-0.391E+04	-0.552E+04	-0.297E+06	-0.559E-08	.146E-10
29	JA	29	.391E+04	-0.391E+04	-0.552E+04	.328E+06	.305E+05	.186E-08
	JB	30	-0.391E+04	.391E+04	-0.552E+04	-0.438E+06	-0.141E+06	-0.559E-08
30	JA	30	-0.201E+04	.692E+03	-0.115E-08	-0.193E+03	-0.408E+02	-0.201E+05
	JB	31	-0.201E+04	-0.692E+03	-0.115E-08	-0.193E+03	-0.408E+02	-0.201E+04
31	JA	31	.201E+04	.692E+03	-0.327E-10	.193E+03	.408E+02	-0.208E+04
	JB	32	-0.201E+04	-0.692E+03	-0.327E-10	-0.193E+03	-0.408E+02	-0.729E+03
32	JA	30	.890E+03	-0.128E+04	-0.279E-08	-0.126E+03	-0.627E+02	-0.258E+05
	JB	33	-0.890E+03	.128E+04	-0.279E-08	-0.126E+03	-0.627E+02	-0.116E+04
33	JA	33	.890E+03	-0.128E+04	-0.291E-10	.126E+03	.627E+02	.116E+04
	JB	34	-0.890E+03	.128E+04	-0.291E-10	-0.126E+03	-0.627E+02	-0.268E+04
34	JA	30	-0.116E-09	.562E-09	-0.931E-09	-0.298E-07	-0.745E-08	0.
	JB	35	-0.116E-09	-0.562E-09	-0.931E-09	-0.447E-07	0.	0.
35	JA	35	-0.72dE-10	.349E-09	-0.466E-09	.373E-08	-0.186E-08	-0.116E-09
	JB	36	-0.72dE-10	-0.349E-09	-0.466E-09	0.	-0.186E-08	-0.116E-09
36	JA	37	.501E+04	-0.875E+04	-0.745E-08	-0.211E+06	-0.144E+06	.688E+05
	JB	16	-0.501E+04	.875E+04	.745E-08	.639E+05	.601E+05	-0.688E+05
37	JA	16	-0.101E+04	.327E+04	-0.552E+04	.110E+06	.295E+05	.565E+04
	JB	38	-0.101E+04	-0.327E+04	-0.552E+04	-0.735E+05	-0.172E+05	-0.565E+04
38	JA	11	-0.167E+05	.205E+04	-0.160E-08	-0.989E+03	-0.629E+04	-0.522E+05
	JB	39	.167E+05	-0.205E+04	.160E-08	.232E+03	.936E+02	-0.442E+04
39	JA	34	-0.167E+05	.205E+04	-0.291E-10	-0.232E+03	-0.936E+02	.442E+04
	JB	40	.167E+05	-0.205E+04	-0.291E-10	.232E+03	.936E+02	-0.132E+05
40	JA	11	.583E+04	.204E+05	-0.803E-08	-0.771E+04	.201E+04	.182E+06
	JB	41	-0.583E+04	-0.204E+05	-0.803E-08	.151E+03	.144E+03	-0.204E+05
41	JA	41	.583E+04	.204E+05	-0.873E-10	-0.151E+03	-0.144E+03	.209E+05
	JB	42	-0.583E+04	-0.204E+05	-0.873E-10	.151E+03	.144E+03	.416E+04

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29	40	.107E+05	.205E+04	.291E-10	.232E+03	.936E+02	.132E+05
JA	11	.583E+04	.204E+05	.803E-08	.771E+04	.201E+04	.142E+05
JH	41	-.583E+04	-.204E+05	-.803E-08	.131E+03	.144E+03	-.204E+05
-1	JA 41	.583E+04	.204E+05	-.873E-10	.151E+03	-.144E+03	.209E+05
32	42	-.583E+04	-.204E+05	.873E-10	.151E+03	.144E+03	.416E+04

NOZZLE LOAD CASE 2

B.E.A.M. S.T.R.E.S.S.E.S. FOR OUTPUT VECTOR 2
 BEAM --- TRANSVERSE --- TORSIONAL - STRESSES AT USER LOCATIONS - MAXIMUM MINIMUM COMBINED
 BEAM LOAD-LOCATION, SHEAR SHEAR (F²C/J) A B C (P/A+MC/I) (P/A-MC/I) SHEAR
 NO. NODE--PERCENT. (V2/K3⁰A) (V3/K2⁰A)

1	1 JA	0.0	3.52E-11	5.34E-11	0.	-8.144E-12	-4.381E-12	-3.073E-11	1.4749E-11	-3.1038E-11	7.37E-12	PIPEG
1	14 JH	100.0	3.52E-11	5.34E-11	0.	-8.144E-12	-3.825E-11	-1.060E-10	9.4238E-11	-1.1053E-10	4.71E-11	
2	3 JA	0.0	2.26E-11	4.5E+02	-1.16E+03	2.293E+02	-2.048E+03	-4.570E+02	2.6457E+03	-2.1872E+03	1.76E+03	PIPEG
2	2 JB	100.0	2.26E-11	4.5E+02	-1.16E+03	2.293E+02	-2.048E+03	2.293E+02	2.5462E+03	-2.0877E+03	1.72E+03	
3	3 JA	0.0	-7.45E-12	-5.90E+00	-2.26E-01	5.904E+00	5.678E+00	5.971E+00	6.1966E+00	5.6114E+00	3.11E+00	BEAMG
3	4 JB	100.0	-7.45E-12	-5.90E+00	-2.26E-01	5.904E+00	5.678E+00	5.146E+00	6.3714E+00	5.4366E+00	3.19E+00	
4	4 JA	0.0	-5.59E-12	5.90E+00	2.26E-01	-5.904E+00	-5.678E+00	-5.662E+00	-5.4356E+00	-6.3714E+00	2.73E+00	BEAMG
4	5 JH	100.0	-5.59E-12	5.90E+00	2.26E-01	-5.904E+00	-5.678E+00	-5.837E+00	-5.6114E+00	-6.1966E+00	2.81E+00	
5	5 JA	0.0	1.81E-11	4.5E+02	1.16E+03	-2.293E+02	2.048E+03	4.570E+02	2.1872E+03	-2.6457E+03	1.59E+03	PIPEG
5	6 JB	100.0	1.81E-11	4.5E+02	1.16E+03	-2.293E+02	2.048E+03	-2.293E+02	2.0877E+03	-2.5462E+03	1.56E+03	
6	4 JA	0.0	-6.61E+01	-6.61E+01	9.41E-12	-1.270E-11	9.123E+01	9.123E+01	1.2902E+02	-1.2902E+02	6.45E+01	PIPEG
6	7 JB	100.0	-6.61E+01	-6.61E+01	9.41E-12	-1.270E-11	1.576E+02	1.576E+02	2.2286E+02	-2.2286E+02	1.11E+02	
7	7 JA	0.0	-1.69E-02	-1.69E-02	4.24E-11	-3.414E-11	4.056E+02	4.056E+02	5.7364E+02	-5.7364E+02	2.87E+02	PIPEG
7	8 JB	100.0	-1.69E-02	-1.69E-02	4.24E-11	-3.414E-11	4.795E+02	4.795E+02	6.7807E+02	-6.7807E+02	3.39E+02	
8	8 JA	0.0	-1.09E+02	-1.09E+02	1.00E-11	-2.837E-11	2.477E+02	2.477E+02	3.5033E+02	-3.5033E+02	1.75E+02	PIPEG
8	11 JH	100.0	-1.09E+02	-1.09E+02	1.00E-11	-2.837E-11	3.032E+02	3.032E+02	4.2886E+02	-4.2886E+02	2.14E+02	
9	10 JA	0.0	-2.39E-12	-4.53E+02	-1.15E+03	2.268E+02	-2.072E+03	-2.452E+02	2.5733E+03	-2.1196E+03	1.73E+03	PIPEG
9	9 JB	100.0	-2.39E-12	-4.53E+02	-1.15E+03	2.268E+02	-2.072E+03	2.268E+02	2.5253E+03	-2.0717E+03	1.71E+03	
10	19 JA	0.0	1.40E-12	-1.10E+01	-5.26E-01	1.105E+01	1.052E+01	1.115E+01	1.1679E+01	1.0411E+01	5.46E+00	BEAMG
10	11 JH	100.0	1.40E-12	-1.10E+01	-5.26E-01	1.105E+01	1.052E+01	1.154E+01	1.2068E+01	1.0022E+01	6.06E+00	
11	11 JA	0.0	9.21E+01	1.61E+02	2.31E+01	-5.461E-11	3.004E+02	4.972E+02	5.8098E+02	-5.8088E+02	2.91E+02	PIPEG
11	12 JB	100.0	9.21E+01	1.61E+02	2.31E+01	-5.461E-11	2.533E+02	4.149E+02	4.8611E+02	-4.8611E+02	2.44E+02	
12	12 JA	0.0	1.43E+02	2.50E+02	4.47E+01	-9.118E-11	4.903E+02	8.030E+02	9.4086E+02	-9.4086E+02	4.73E+02	PIPEG
12	37 JB	100.0	1.43E+02	2.50E+02	4.47E+01	-9.118E-11	1.876E+02	2.740E+02	3.3206E+02	-3.3206E+02	1.72E+02	
13	13 JA	0.0	-1.05E+01	6.57E-02	1.07E-02	-8.315E+00	-8.403E+00	-8.314E+00	-8.2261E+00	-8.4036E+00	4.11E+00	BEAMG
13	14 JB	100.0	-1.05E+01	6.57E-02	1.07E-02	-8.315E+00	-8.337E+00	-8.315E+00	-8.2924E+00	-8.3369E+00	4.15E+00	
14	15 JA	0.0	1.21E+02	9.60E-01	2.48E+00	1.528E+02	3.416E+02	1.675E+02	3.5626E+02	-5.0689E+01	1.78E+02	BEAMG
14	14 JH	100.0	1.21E+02	9.60E-01	2.48E+00	1.528E+02	9.869E+01	1.665E+02	2.2058E+02	8.4990E+01	1.10E+02	
15	15 JA	0.0	-8.31E+00	6.57E-02	5.18E-05	1.048E+01	1.055E+01	1.047E+01	1.0566E+01	1.0390E+01	5.28E+00	BEAMG
15	16 JB	100.0	-8.31E+00	6.57E-02	5.18E-05	1.048E+01	1.079E+01	1.046E+01	1.0802E+01	1.0154E+01	5.40E+00	
16	16 JA	0.0	-2.19E+00	1.61E+00	-5.18E-05	-1.048E+01	-1.061E+01	-1.042E+01	-1.0294E+01	-1.0672E+01	5.15E+00	BEAMG
16	17 JB	100.0	-2.19E+00	1.61E+00	-5.18E-05	-1.048E+01	-1.053E+01	-1.046E+01	-1.0418E+01	-1.0548E+01	5.21E+00	
17	17 JA	0.0	-4.07E+01	2.33E+01	-2.49E+00	-1.529E+02	-2.634E+02	-1.270E+02	-1.5455E+01	-2.8926E+02	8.59E+00	BEAMG
17	18 JB	100.0	-4.07E+01	2.33E+01	-2.49E+00	-1.529E+02	-1.818E+02	-1.513E+02	-1.2237E+02	-1.8334E+02	6.12E+01	
18	19 JA	0.0	1.05E+01	1.61E+00	1.19E-03	2.792E+00	2.846E+00	2.802E+00	2.8565E+00	2.7212E+00	1.43E+00	BEAMG
18	19 JH	100.0	1.05E+01	1.61E+00	1.19E-03	2.792E+00	2.780E+00	2.792E+00	2.8037E+00	2.7800E+00	1.40E+00	
19	20 JA	0.0	5.22E+00	-7.05E-01	1.25E-02	7.117E-02	9.007E-02	6.681E-02	9.4429E-02	4.7904E-02	4.97E-02	BEAMG
19	21 JB	100.0	5.22E+00	-7.05E-01	1.25E-02	7.117E-02	6.649E-02	7.102E-02	8.5545E-02	5.4790E-02	4.97E-02	

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	11 JA	9.0 0	9.0E-12	1.1E+01	-1.05E-03	4.0H3E+01	4.0H1E+01	4.129E+01	4.1309E+01	4.0359E+01	2.07E+01	BEAMG
41	41 JA	100.0	9.0E-12	1.1E+01	-1.05E-03	4.0H3E+01	4.0H3E+01	4.0H2E+01	4.0H2E+01	4.07H1E+01	2.04E+01	
41	42 JB	100.0	9.0E-12	6.47E+02	-6.40E+01	2.269E+03	1.195E+03	2.305E+03	3.37H4E+03	1.1591E+03	1.69E+03	BEAMG
41	42 JB	100.0	9.0E-12	6.47E+02	-6.40E+01	2.269E+03	1.195E+03	2.252E+03	3.3492E+03	1.1883E+03	1.68E+03	

NOZZLE LOAD CASE 2

MAXIMUM STRESS SUMMARY FOR

BEAM STRESSES FOR OUTPUT VECTOR 2						
--- TRANSVERSE --- TORSIONAL - STRESSES AT USER LOCATIONS -						
SHEAR	SHEAR	COMBINED				
(T ⁰ C/J)	A	B	C	(P/A+MC/I)	(P/A-MC/I)	STRESS
(V2/K3 ⁰ A)	(V3/K2 ⁰ A)					

MAX. BEAM STRESSES = 1.43E+02 6.47E+02 1.16E+03 2.269E+03 2.0H8E+03 2.305E+03 3.37H4E+03 1.18H3E+03 1.69E+03
 BEAM NOS. = 12. 41. 5. 41. 5. 41. 41. 41. 28.

MIN. BEAM STRESSES = -4.03E+02 -4.50E+02 -1.15E+03 -1.860E+03 -2.544E+03 -1.852E+03 -1.1852E+03 -2.6457E+03 6.28E-13
 BEAM NOS. = 22. 6. 2. 39. 28. 39. 39. 5. 35.

B E G I N INPUT LOAD CASE NO. 3 TITLE(NUZZLE LOAD CASE 3- MAXIMUM OVERTURNING MOMENT

NODAL POINT APPLIED FORCES FOR LOAD CASE NO. 3

NODE	X1	X2	X3	X4	X5	X6
2	-2.952000E+03	2.952000E+03	0.	-9.030000E+04	-9.030000E+04	-0.
6	-2.952000E+03	2.952000E+03	0.	-9.030000E+04	-9.030000E+04	-0.
28	3.905000E+03	-3.905000E+03	5.523000E+03	-2.974000E+05	0.	-0.
9	0.	7.810000E+03	0.	-2.974000E+05	0.	-0.

NODAL POINT APPLIED LOADS AND/OR DISPLACEMENTS FINAL SUMMARY FOR LOAD CASE NO. 3

NODE	X1	X2	X3	X4	X5	X6
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NOTE* IF A FINAL SUMMARY OF APPLIED NODAL LOADS AND GENERATED LOADS IS DESIRED AT THIS POINT.
CODE A 1 IN COLUMN 20 OF THE STATIC CARD.

FORCE AND MOMENT SUMMATION
ABOUT AXES PARALLEL TO SYSTEM AXES
WITH ORIGIN AT POINT (0,0,0)

SUMMATION INCLUDES LOADS APPLIED TO RESTRAINED DOF.

$$FX1 = -1949000000E+04$$

$$FX2 = .9809000000E+04$$

$$FX3 = .5523000000E+04$$

$$MX1 = -49565567300E+07$$

$$MX2 = -.21212537300E+07$$

$$MX3 = -.1936426000E+06$$

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NOZZLE LOAD CASE 3- MAXIMUM OVERTURNING MOMENT

H E A M E L E M E N T L O A D S F O R O U T P U T V E C T O R 3

BEAM	LOAD-LOCATION	P	AXIAL NU	SHEAR NODE--PERCENT.	V2	SHEAR V3	TORSION M1	BENDING M2	BENDING M3	
1	1 JA	0.0	1.16415E-09	3.37604E-09	5.58794E-09	-1.86265E-09	4.47035E-08	2.98023E-08	2.98023E-08	PIPEG
1	4 JB	100.0	-1.16415E-09	-3.37604E-09	-5.58794E-09	1.86265E-09	-2.08616E-07	7.45058E-08		
2	3 JA	0.0	-2.95200E+03	3.49246E-10	-2.95200E+03	9.03000E+04	2.67451E+04	-9.03000E+04	9.03000E+04	PIPEG
2	2 JB	100.0	2.95200E+03	-3.49246E-10	2.95200E+03	-9.03000E+04	1.86265E-09	9.03000E+04		
3	3 JA	0.0	-2.95200E+03	-2.79397E-09	-2.95200E+03	9.03000E+04	-2.67451E+04	-9.03000E+04	9.03000E+04	BEAMG
3	4 JB	100.0	2.95200E+03	2.79397E-09	2.95200E+03	-9.03000E+04	9.66780E+04	9.03000E+04		
4	4 JA	0.0	-2.95200E+03	-1.86265E-09	2.95200E+03	-9.03000E+04	-9.66780E+04	9.03000E+04	9.03000E+04	BEAMG
4	5 JB	100.0	-2.95200E+03	1.86265E-09	-2.95200E+03	9.03000E+04	2.67451E+04	-9.03000E+04		
5	5 JA	0.0	2.95200E+03	5.82077E-11	2.95200E+03	-9.03000E+04	-2.67451E+04	9.03000E+04	9.03000E+04	PIPEG
5	6 JB	100.0	-2.95200E+03	-5.82077E-11	-2.95200E+03	9.03000E+04	-2.24099E-09	-9.03000E+04		
6	4 JA	0.0	-1.16415E-10	-5.90400E+03	-5.90400E+03	-3.35270E-08	-1.80600E+05	1.80500E+05	1.80500E+05	PIPEG
6	7 JB	100.0	1.16415E-10	5.90400E+03	5.90400E+03	3.35270E-08	3.11964E+05	-3.11964E+05		
7	7 JA	0.0	-1.57161E-09	-5.90400E+03	-5.90400E+03	-5.58794E-08	-3.11964E+05	3.11964E+05	3.11964E+05	PIPEG
7	8 JB	100.0	1.57161E-09	5.90400E+03	5.90400E+03	5.58794E-08	3.68760E+05	-3.58760E+05		
8	8 JA	0.0	-1.22235E-09	-5.90400E+03	-5.90400E+03	-3.35270E-08	-3.68760E+05	3.68760E+05	3.68760E+05	PIPEG
8	11 JB	100.0	1.22235E-09	5.90400E+03	5.90400E+03	3.35270E-08	4.51416E+05	-4.51416E+05		
9	10 JA	0.0	-5.52250E+03	2.91038E-11	-5.52250E+03	2.10294E+05	4.31893E+04	-2.10294E+05	2.10294E+05	PIPEG
9	9 JB	100.0	5.52250E+03	-2.91038E-11	5.52250E+03	-2.10294E+05	4.88944E-09	2.10294E+05		
10	10 JA	0.0	-5.52250E+03	2.09548E-09	-5.52250E+03	2.10294E+05	-4.31893E+04	-2.10294E+05	BEAMG	
10	11 JB	100.0	5.52250E+03	-2.09548E-09	5.52250E+03	-2.10294E+05	1.98843E+05	2.10294E+05		
11	11 JA	0.0	3.31704E-09	4.73776E+03	7.87026E+03	-6.76285E+04	-7.40454E+05	4.47244E+05	4.47244E+05	PIPEG
11	12 JB	100.0	-3.31704E-09	-4.73776E+03	-7.87026E+03	6.76285E+04	6.30270E+05	-3.80915E+05		
12	12 JA	0.0	2.92493E-09	4.73776E+03	7.87026E+03	-6.76285E+04	-6.30270E+05	3.80915E+05	3.80915E+05	PIPEG
12	37 JB	100.0	-2.92493E-09	-4.73776E+03	-7.87026E+03	6.76285E+04	2.64303E+05	-1.60609E+05		
13	13 JA	0.0	-1.59590E+03	-1.91380E+03	1.39807E+02	-3.24854E+03	-7.14233E+02	-2.75745E+03	BEAMG	
13	14 JB	100.0	1.59590E+03	1.91380E+03	-1.39807E+02	3.24854E+03	6.80903E+00	-6.92638E+03		
14	15 JA	0.0	-1.91380E+03	-1.59590E+03	1.39807E+02	-6.80903E+00	-4.57681E+03	-8.23470E+03	BEAMG	
14	14 JB	100.0	1.91380E+03	1.59590E+03	-1.39807E+02	6.80903E+00	3.24864E+03	-6.92638E+03		
15	15 JA	0.0	-1.41380E+03	1.59590E+03	1.39807E+02	-6.80903E+00	4.57681E+03	-8.23470E+03	BEAMG	
15	16 JB	100.0	1.41380E+03	-1.59590E+03	-1.39807E+02	6.80903E+00	-7.72246E+03	4.41425E+04		
15	16 JA	0.0	1.91132E+03	-1.1e500E+03	6.00132E+02	6.62307E+00	-2.01743E+04	-3.07188E+04	BEAMG	
15	17 JB	100.0	-1.91132E+03	1.1e500E+03	-6.00132E+02	-6.62307E+00	6.67134E+03	4.49292E+03		
17	17 JA	0.0	1.91132E+03	-1.1e500E+03	6.00132E+02	6.82307E+00	-6.67134E+03	-4.49292E+03	BEAMG	
17	18 JB	100.0	-1.91132E+03	1.1e500E+03	-6.00132E+02	-6.82307E+00	9.70082E+02	-6.58026E+03		A 3-47
18	19 JA	0.0	-1.1e500E+03	1.91132E+03	6.00132E+02	-9.70082E+02	-3.02985E+03	1.62515E+04	BEAMG	
18	19 JB	100.0	1.1e500E+03	-1.91132E+03	-6.00132E+02	9.70082E+02	-6.82307E+00	-6.58026E+03		
19	20 JA	0.0	-1.1e500E+03	1.91132E+03	6.00132E+02	-9.70082E+02	-3.02985E+03	1.62515E+04	BEAMG	

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40	40 JA	0.0	-1.62870E+04	BEAMG						
40	40 JB	100.0	-1.97745E+04	BEAMG						
41	41 JA	0.0	-1.97745E+04	-2.64209E+02	5.64523E+03	4.1419E+02	-1.76657E+05	-1.46484E+03	BEAMG	
41	41 JB	100.0	1.97745E+04	2.64209E+02	-5.64523E+03	-4.1419E+02	2.03268E+04	1.48246E+02		
42	42 JA	0.0	-1.97745E+04	5.82077E-11	5.64523E+03	1.42572E+02	-2.03305E+04	-1.48246E+02	BEAMG	
42	42 JB	100.0	1.97745E+04	-5.82077E-11	-5.64523E+03	-1.42572E+02	-4.00039E+03	1.48246E+02		

NOZZLE LOAD CASE 3- MAXIMUM OVERTURNING MOMENT

MAXIMUM LOAD SUMMARY FOR

AXIAL	BEAM	ELEMENT	LOADS	FOR OUTPUT VECTOR 3
A1	V1	V2	SHEAR	BENDING
A2	V2	V3	SHEAR	BENDING
A3	V3	MT	TORSION	BENDING

MAXIMUM BEAM LOADS = 1.97745E+04 -5.90400E+03 -7.87026E+03 -2.10294E+05 -6.30270E+05 4.47244E+05
 BEAM NOS. = 41. 8. 36. 28. 11. 11.

MINIMUM BEAM LOADS = -1.62870E+04 -5.90400E+03 -7.87026E+03 -2.10294E+05 -7.40454E+05 -4.51416E+05
 BEAM NOS. = 39. 8. 36. 28. 11. 8.

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NOZZLE LOAD CASE 3- MAXIMUM OVERTURNING MOMENT

BEA#	--NODES--	U D E A M I L E N D U M M L O A D S .			IN GLOBAL SYSTEM			FOR OUTPUT VECTOR . . . 3 . . .		
		FX1	FX2	FX3	MX1	MX2	MX3			
1	JA 1	.338E-08	-.559E-08	-.116E-08	.447E-07	-.298E-07	.186E-08			
	JB 4	-.338E-08	.559E-08	.116E-08	-.209E-06	-.745E-07	-.186E-08			
2	JA 3	.295E+04	-.295E+04	-.295E+04	-.349E-09	.903E+05	-.903E+05	.267E+05		
	JB 2	-.295E+04	.295E+04	.295E+04	.349E-09	-.903E+05	.903E+05	-.186E-08		
3	JA 3	-.295E+04	.295E+04	-.295E+04	.279E-08	-.903E+05	-.903E+05	.267E+05		
	JB 4	.295E+04	-.295E+04	.295E+04	-.279E-08	.903E+05	.903E+05	-.967E+05		
4	JA 4	.295E+04	-.295E+04	.295E+04	-.1M6E-08	.903E+05	-.903E+05	.967E+05		
	JB 5	-.295E+04	.295E+04	-.295E+04	.1M6E-08	-.903E+05	.903E+05	-.267E+05		
5	JA 5	.295E+04	-.295E+04	.295E+04	-.295E-10	.903E+05	-.903E+05	.267E+05		
	JB 6	-.295E+04	.295E+04	-.295E+04	.582E-10	-.903E+05	.903E+05	-.224E-03		
6	JA 4	-.590E+04	.590E+04	-.590E+04	.116E-09	-.181E+06	.181E+06	-.335E-07		
	JB 7	.590E+04	-.590E+04	.590E+04	-.116E-09	.312E+06	-.312E+06	-.335E-07		
7	JA 7	-.590E+04	.590E+04	-.590E+04	.157E-08	-.312E+06	.312E+06	.559E-07		
	JB 8	.590E+04	-.590E+04	.590E+04	-.157E-08	.369E+06	-.369E+06	-.559E-07		
8	JA 8	-.590E+04	.590E+04	-.590E+04	.590E+04	-.122E-08	.369E+06	-.369E+06	.335E-07	
	JB 11	.590E+04	-.590E+04	.590E+04	-.122E-08	.451E+06	-.451E+06	-.335E-07		
9	JA 10	.176E-03	-.781E+04	.781E+04	-.291E-10	.297E+06	-.652E-08	.432E+05		
	JB 9	-.176E-03	.781E+04	-.781E+04	.291E-10	-.297E+06	.652E-08	-.489E-08		
10	JA 10	.754E-08	-.781E+04	.781E+04	-.210E-08	-.297E+06	.240E-06	.432E+05		
	JB 11	-.754E-03	-.781E+04	.781E+04	.210E-08	.297E+06	-.262E-06	-.199E+06		
11	JA 11	.474E+04	-.137E+04	.137E+04	-.332E-08	-.740E+06	-.447E+05	.676E+05		
	JB 12	-.474E+04	.137E+04	-.137E+04	.332E-08	.630E+06	.381E+06	-.676E+05		
12	JA 12	-.474E+04	.137E+04	-.137E+04	-.242E-08	-.630E+06	-.391E+06	.676E+05		
	JB 37	.474E+04	-.137E+04	.137E+04	.242E-08	.264E+06	.161E+06	-.676E+05		
13	JA 13	.140E+03	.191E+04	-.191E+04	-.160E+04	-.276E+04	.714E+03	-.325E+04		
	JB 14	-.140E+03	-.191E+04	.191E+04	.160E+04	-.693E+04	-.681E+01	.325E+04		
14	JA 15	-.140E+03	.191E+04	-.191E+04	.160E+04	-.823E+04	.681E+01	.458E+04		
	JB 14	.140E+03	-.191E+04	.191E+04	-.160E+04	-.693E+04	.681E+01	-.325E+04		
15	JA 15	.140E+03	.191E+04	-.191E+04	.160E+04	-.823E+04	.6d1E+01	-.458E+04		
	JB 16	-.140E+03	-.191E+04	.191E+04	.160E+04	-.441E+05	-.681E+01	.772E+04		
16	JA 15	.500E+03	-.191E+04	.191E+04	-.117E+04	-.307E+05	-.682F+01	.202E+05		
	JB 17	-.500E+03	.191E+04	-.191E+04	.117E+04	-.449E+04	.682E+01	-.667E+04		
17	JA 17	.600E+03	-.191E+04	.191E+04	-.117E+04	-.449E+04	-.682E+01	.667E+04		
	JB 18	-.600E+03	.191E+04	-.191E+04	.117E+04	-.658E+04	.682E+01	-.970E+03		
18	JA 19	-.600E+03	.191E+04	-.191E+04	-.117E+04	-.163E+05	-.303E+04	.970E+03		
	JB 18	.600E+03	-.191E+04	.191E+04	.117E+04	-.658E+04	.682E+01	.970E+03		
19	JA 20	-.156E+04	-.885E+02	.885E+02	-.185E+04	-.445E+03	.150E+05	-.350E+04		
	JB 21	.156E+04	-.885E+02	.885E+02	.185E+04	.314E+01	-.709E+04	.350E+04		
20	JA 22	.156E+04	.885E+02	-.885E+02	.185E+04	.314E+01	-.104E+05	.434F+04		

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17	JA 20	-1.10E+04	-1.00E+04	-1.00E+04	-1.10E+04	-1.00E+04	-1.00E+04	-1.00E+04
	JB 21	-1.00E+04	-800E+02	-1.00E+04	-900E+01	-1.00E+01	-700E+04	-350E+04
20	JA 22	-1.50E+04	-800E+02	-1.80E+04	-314E+01	-1.04E+05	-434E+04	
	JB 21	-1.50E+04	-800E+02	-1.80E+04	-314E+01	-709E+04	-350E+04	
21	JA 22	-1.50E+04	-800E+02	-1.80E+04	-314E+01	-1.04E+05	-434E+04	
	JB 16	-1.50E+04	-800E+02	-1.80E+04	-314E+01	-520E+05	-634E+04	
22	JA 16	-1.57E+04	-651E+03	-915E+03	-313E+01	-229E+05	-216E+05	
	JB 23	-1.57E+04	-651E+03	-915E+03	-313E+01	-228E+04	-590E+04	
23	JA 23	-1.57E+04	-651E+03	-915E+03	-313E+01	-228E+04	-690E+04	
	JB 24	-1.57E+04	-651E+03	-915E+03	-313E+01	-642E+04	-717E+03	
24	JA 25	-1.57E+04	-651E+03	-915E+03	-313E+01	-151E+04	-717E+03	
	JB 24	-1.57E+04	-651E+03	-915E+03	-313E+01	-642E+04	-717E+03	
25	JA 28	-1.15E+04	-348E+04	-552E+04	-106E+06	-390E+05	-118E+05	
	JB 26	-1.15E+04	-348E+04	-552E+04	-131E+06	-394E+05	-118E+05	
26	JA 26	-1.15E+04	-348E+04	-552E+04	-131E+06	-394E+05	-118E+05	
	JB 27	-1.15E+04	-348E+04	-552E+04	-389E+06	-124E+06	-118E+05	
27	JA 27	-1.15E+04	-348E+04	-552E+04	-389E+06	-124E+06	-118E+05	
	JB 30	-1.15E+04	-348E+04	-552E+04	-438E+06	-141E+06	-118E+05	
28	JA 29	-391E+04	-391E+04	-552E+04	-323E+06	-305E+05	-221E+08	
	JB 24	-391E+04	-391E+04	-552E+04	-297E+06	-559E+04	-116E+09	
29	JA 29	-391E+04	-390E+04	-552E+04	-328E+06	-305E+05	-112E+07	
	JB 30	-391E+04	-390E+04	-552E+04	-438E+06	-141E+06	-224E+07	
30	JA 30	-556E+04	-108E+04	-931E-09	-189E+03	-396E+02	-296E+05	
	JB 31	-556E+04	-108E+04	-931E-09	-188E+03	-396E+02	-329E+03	
31	JA 31	-556E+04	-108E+04	-123E-10	-188E+03	-396E+02	-329E+03	
	JB 32	-556E+04	-108E+04	-123E-10	-188E+03	-396E+02	-499E+04	
32	JA 30	-509E+03	-631E+04	-652E-08	-122E+03	-610E+02	-178E+05	
	JB 33	-509E+03	-631E+04	-652E-08	-122E+03	-610E+02	-367E+04	
33	JA 33	-509E+03	-631E+04	-291E-10	-122E+03	-610E+02	-367F+04	
	JB 34	-509E+03	-631E+04	-291E-10	-122E+03	-610E+02	-147E+04	
34	JA 30	-146E-09	-502E-09	-456E-09	-596E-07	0.	0.	
	JB 35	-146E-09	-502E-09	-456E-09	-447E-07	0.	0.	
35	JA 35	.582E-10	-349E-09	.233E-09	-373E-08	.279E-08	0.	
	JB 36	-582E-10	-349E-09	-233E-09	0.	0.	0.	
36	JA 37	-474E+04	-787E+04	-192E-08	-264E+06	-161E+06	-676E+05	
	JB 16	-474E+04	-787E+04	-192E-08	-132E+06	-809E+05	-676E+05	
37	JA 16	.115E+04	-348E+04	-552E+04	-145E+06	-518E+05	-118E+05	
	JB 38	-115E+04	-348E+04	-552E+04	-106E+06	-390E+05	-118E+05	
38	JA 11	-163E+05	-1d1E+04	-146E+08	-898E+03	-612E+04	-454E+05	
	JB 39	-163E+05	-1d1E+04	-146E+08	-228E+03	-926E+02	-468E+04	
39	JA 39	-163E+05	-181E+04	-146E-10	-228E+03	-926E+02	-468E+04	
	JB 40	-163E+05	-181E+04	-146E-10	-228E+03	-926E+02	-125E+05	
40	JA 11	-565E+04	-194E+05	-698E+08	-746E+04	-195E+04	-177E+06	
	JB 41	-565E+04	-194E+05	-698E+08	-148E+03	-143E+03	-203E+05	
41	JA 41	-565E+04	-194E+05	-194E+05	-148E+03	-143E+03	-203E+05	
	JB 42	-565E+04	-194E+05	-194E+05	-148E+03	-143E+03	-409E+04	

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NOZZLE LOAD CASE 3 - MAXIMUM OVERTURNING MOMENT

BEAMS STREAMS USE FOR OUTPUT VECTOR 3

BEAM --- TRANSVERSE --- TORSIONAL - STRESSES AT USER LOCATIONS - MAXIMUM MINIMUM COMBINED
 DAD-LOCATION. SHEAR SHEAR (T+C/J) A B C (P/A+MC/I) (P/A-MC/I) SHEAR
 GOF---PERCENT. (V2/K2A) (V3/K3A)

1	1	JA	0.0	3.76E-11	6.25E-11	4.70E-13	-6.515E-12	8.539E-12	-2.910F-11	2.0625E-11	-3.3655E-11	1.03E-11	PIPEG
1	4	JB	100.0	3.76E-11	6.25E-11	4.70E-13	-6.515E-12	-4.415E-11	-1.119E-10	1.0539E-10	-1.1842E-10	5.27E-11	
2	3	JA	0.0	5.42E-11	-4.54E+02	-1.15E+03	2.293E+02	-2.088E+03	-4.570E+02	2.5457E+03	-2.1872E+03	1.76E+03	PIPEG
2	2	JB	100.0	5.42E-11	-4.54E+02	-1.15E+03	2.293E+02	-2.088E+03	2.293E+02	2.5462E+03	-2.0877E+03	1.72E+03	
3	3	JA	0.0	-5.59E-12	-5.40E+00	-2.26E-01	5.904E+00	5.674E+00	5.971E+00	6.1956E+00	5.6114E+00	3.11E+00	BEAMG
3	4	JB	100.0	-5.59E-12	-5.40E+00	-2.26E-01	5.904E+00	5.674E+00	6.146E+00	6.3714E+00	5.4366E+00	3.19E+00	
4	4	JA	0.0	-3.73E-12	5.90E+00	2.26E-01	-5.904E+00	-5.674E+00	-5.662E+00	-5.4356E+00	-6.3714E+00	2.73E+00	BEAMG
4	5	JB	100.0	-3.73E-12	5.90E+00	2.26E-01	-5.904E+00	-5.674E+00	-5.437E+00	-5.6114E+00	-6.1966E+00	2.81E+00	
5	5	JA	0.0	9.04E-12	4.53E+02	1.16E+03	-2.293E+02	2.088E+03	4.570E+02	2.1872E+03	-2.6457E+03	1.59E+03	PIPEG
5	6	JB	100.0	9.04E-12	4.53E+02	1.16E+03	-2.293E+02	2.088E+03	-2.293E+02	2.0877E+03	-2.5462E+03	1.55E+03	
6	4	JA	0.0	-6.61E+01	-5.61E+01	8.47E-12	6.515E-13	9.123E+01	9.123E+01	1.2902E+02	-1.2902E+02	6.45E+01	PIPEG
6	7	JH	100.0	-6.51E+01	-5.61E+01	8.47E-12	6.515E-13	1.576E+02	1.576E+02	2.2296E+02	-2.2296E+02	1.11E+02	
7	7	JA	0.0	-1.59E-02	-1.69E+02	3.63E-11	2.248E-11	4.056E+02	4.056E+02	5.7364E+02	-5.7364E+02	2.87E+02	PIPEG
7	8	JB	100.0	-1.69E-02	-1.69E+02	3.63E-11	2.248E-11	4.795E+02	4.795E+02	6.7807E+02	-6.7807E+02	3.39E+02	
8	8	JA	0.0	-1.09E-02	-1.09E+02	1.13E-11	1.124E-11	2.477E+02	2.477E+02	3.5033E+02	-3.5033E+02	1.75E+02	PIPEG
8	11	JB	100.0	-1.09E-02	-1.09E+02	1.13E-11	1.124E-11	3.032E+02	3.032E+02	4.2886E+02	-4.2886E+02	2.14E+02	
9	10	JA	0.0	2.39E-12	-4.53E+02	-1.15E+03	2.268E+02	-2.072E+03	-2.452E+02	2.5733E+03	-2.1196E+03	1.73E+03	PIPEG
9	9	JB	100.0	2.39E-12	-4.53E+02	-1.15E+03	2.268E+02	-2.072E+03	2.268E+02	2.5253E+03	-2.0717E+03	1.71E+03	
10	10	JA	0.0	4.19E-12	-1.10E+01	-5.26E-01	1.105E+01	1.052E+01	1.115E+01	1.1579E+01	1.0411E+01	5.86E+00	BEAMG
10	11	JB	100.0	4.19E-12	-1.10E+01	-5.26E-01	1.105E+01	1.052E+01	1.154E+01	1.2068E+01	1.0022E+01	6.06E+00	
11	11	JA	0.0	8.71E+01	1.45E+02	2.27E+01	-3.051E-11	3.004E+02	4.974E+02	5.8111E+02	-5.8111E+02	2.91E+02	PIPEG
11	12	JB	100.0	8.71E+01	1.45E+02	2.27E+01	-3.051E-11	2.554E+02	4.234E+02	4.9472E+02	-4.9472E+02	2.44E+02	
12	12	JA	0.0	1.35E+02	2.25E+02	4.40E+01	-4.184E-11	4.953E+02	8.195E+02	9.5753E+02	-9.5753E+02	4.41E+02	PIPEG
12	37	JB	100.0	1.35E+02	2.25E+02	4.40E+01	-4.184E-11	2.986E+02	3.337E+02	4.0213E+02	-4.0213E+02	2.06E+02	
13	13	JA	0.0	-3.63E+00	2.80E-01	8.12E-03	3.192E+00	3.185E+00	3.194E+00	3.2005E+00	3.1831E+00	1.60E+00	BEAMG
13	14	JB	100.0	-3.63E+00	2.80E-01	8.12E-03	3.192E+00	3.209E+00	3.192E+00	3.2091E+00	3.1745E+00	1.60E+00	
14	15	JA	0.0	-4.65E+01	4.05E+00	8.14E+01	5.581E+01	5.174E+00	7.041E+01	1.2104E+02	-9.4200E+00	6.05E+01	BEAMG
14	14	JB	100.0	-4.65E+01	4.05E+00	8.14E+01	5.581E+01	9.840E+01	6.617E+01	1.0876E+02	2.8605E+00	5.44E+01	
15	15	JA	0.0	3.19E+00	2.80E-01	1.70E-05	3.828E+00	3.807E+00	3.816E+00	3.8596E+00	3.7956E+00	1.93E+00	BEAMG
15	16	JB	100.0	3.19E+00	2.80E-01	1.70E-05	3.828E+00	3.807E+00	3.717E+00	3.9573E+00	3.6979E+00	1.98E+00	
16	16	JA	0.0	-2.33E+00	1.20E+00	-1.71E-05	-3.823E+00	-3.894E+00	-3.772E+00	-3.6954E+00	-3.9499E+00	1.85E+00	BEAMG
16	17	JB	100.0	-2.33E+00	1.20E+00	-1.71E-05	-3.823E+00	-3.894E+00	-3.800E+00	-3.7947E+00	-3.8505E+00	1.90E+00	
17	17	JA	0.0	-3.40E+01	1.75E+01	-8.16E+01	-5.574E+01	-8.337E+01	-3.447E+01	-6.8381E+00	-1.0464E+02	3.51E+00	BEAMG
17	18	JB	100.0	-3.40E+01	1.75E+01	-8.16E+01	-5.574E+01	-1.528E+01	-5.265E+01	-1.2182E+01	-9.9297E+01	6.15E+00	
18	19	JA	0.0	3.62E+00	1.20E+00	2.43E+03	2.331E+00	2.372E+00	2.339E+00	2.3794E+00	2.2930E+00	1.19E+00	BEAMG
18	19	JB	100.0	3.62E+00	1.20E+00	2.43E+03	2.331E+00	2.348E+00	2.331E+00	2.3477E+00	2.3147E+00	1.17E+00	
19	20	JA	0.0	3.19E+00	1.77E-01	8.75E-03	3.692E+00	3.730E+00	3.694E+00	3.7311E+00	3.6538E+00	1.87E+00	BEAMG
19	21	JH	100.0	3.19E+00	1.77E-01	8.75E-03	3.692E+00	3.710E+00	3.692E+00	3.7102E+00	3.6747E+00	1.86E+00	

17	JA	0.0	-3.40E+01	1.70E+01	-4.16E+01	-5.574E+01	-8.01	-3.447E+01	-6.834E+00	-1.0464E+02	3.51E+00	BEAMG	
18	JH	100.0	-3.40E+01	1.70E+01	-4.16E+01	-5.574E+01	-1.01	-5.264E+01	-1.2142E+01	-4.9297E+01	6.15E+00		
19	JA	0.0	3.62E+00	1.20E+00	2.43E+03	2.331E+00	2.37E+00	2.439E+00	2.3794E+00	2.2830E+00	1.19E+00	BEAMG	
19	JH	100.0	3.62E+00	1.20E+00	2.43E+03	2.331E+00	2.348E+00	2.431E+00	2.3477E+00	2.3147E+00	1.17E+00		
19	20	JA	0.0	3.13E+00	1.77E+01	3.76E+03	3.692E+00	3.730E+00	3.694E+00	3.7311E+00	3.6538E+00	1.87E+00	BEAMG
19	21	JH	100.0	3.13E+00	1.77E+01	3.76E+03	3.692E+00	3.710E+00	3.692E+00	3.7102E+00	3.6747E+00	1.86E+00	
20	22	JA	0.0	-5.39E+01	2.50E+00	-3.75E+01	-4.559E+01	-1.098E+02	-3.174E+01	3.2510E+01	-1.2368E+02	1.63E+01	BEAMG
20	21	JH	100.0	-5.39E+01	2.50E+00	-3.75E+01	-4.559E+01	-1.079E+00	-3.442E+01	9.1484E+00	-1.0036E+02	4.61E+00	
21	22	JA	0.0	3.69E+00	1.77E+01	-7.85E+06	-3.126E+00	-3.154E+00	-3.137E+00	-3.0894E+00	-3.1633E+00	1.54E+00	BEAMG
21	16	JH	100.0	3.69E+00	1.77E+01	-7.85E+06	-3.126E+00	-3.256E+00	-3.142E+00	-2.9406E+00	-3.2722E+00	1.49E+00	
22	15	JA	0.0	-1.63E+00	1.30E+00	7.32E+06	3.131E+00	3.074E+00	3.185E+00	3.2424E+00	3.0202E+00	1.62E+00	BEAMG
22	23	JH	100.0	-1.63E+00	1.30E+00	7.32E+06	3.131E+00	3.126E+00	3.149E+00	3.1543E+00	3.1084E+00	1.58E+00	
23	23	JA	0.0	-2.07E+01	1.90E+01	3.74E+01	4.566E+01	3.164E+01	6.768E+01	8.1697E+01	9.6225E+00	4.09E+01	BEAMG
23	24	JH	100.0	-2.07E+01	1.90E+01	3.74E+01	4.566E+01	8.511E+01	4.794E+01	8.7393E+01	3.9260E+00	4.37E+01	
24	25	JA	0.0	-3.13E+00	1.30E+00	1.74E+03	1.831E+00	1.827E+00	1.839E+00	1.8426E+00	1.8145E+00	9.21E+01	BEAMG
24	24	JH	100.0	-3.13E+00	1.30E+00	1.74E+03	1.831E+00	1.847E+00	1.831E+00	1.8466E+00	1.8145E+00	9.23E+01	
25	38	JA	0.0	3.29E+01	9.90E+01	7.04E+00	-7.901E+01	-2.837E+01	5.936E+01	6.8337E+01	-2.2636E+02	3.50E+01	PIPEG
25	26	JH	100.0	3.29E+01	9.90E+01	7.04E+00	-7.901E+01	-1.302E+02	-2.494E+02	9.8897E+01	-2.5642E+02	5.90E+01	
26	25	JA	0.0	3.29E+01	9.90E+01	7.04E+00	-7.901E+01	-1.302E+02	-2.494E+02	9.8897E+01	-2.5642E+02	5.90E+01	
25	27	JH	100.0	3.29E+01	9.90E+01	7.04E+00	-7.901E+01	-2.408E+02	-5.847E+02	4.5196E+02	-6.0994E+02	2.26E+02	
27	27	JA	0.0	2.11E+01	6.40E+01	3.28E+00	-5.080E+01	-1.344E+02	-3.121E+02	2.2354E+02	-3.2513E+02	1.12E+02	PIPEG
27	30	JH	100.0	2.11E+01	6.40E+01	3.28E+00	-5.080E+01	-1.452E+02	-3.448E+02	2.5802E+02	-3.5961E+02	1.29E+02	
28	29	JA	0.0	4.53E+02	2.52E+11	-1.15E+03	2.268E+02	2.997E+03	2.264E+02	2.9974E+03	-2.5437E+03	1.89E+03	PIPEG
28	28	JH	100.0	4.53E+02	2.52E+11	-1.15E+03	2.268E+02	2.525E+03	2.268E+02	2.5253E+03	-2.0717E+03	1.71E+03	
29	29	JA	0.0	-1.16E+01	-2.33E+12	-5.26E+01	1.105E+01	1.168E+01	1.105E+01	1.1679E+01	1.0411E+01	5.86E+00	BEAMG
29	30	JH	100.0	-1.16E+01	-2.33E+12	-5.26E+01	1.105E+01	1.207E+01	1.105E+01	1.2069E+01	1.0922E+01	6.06E+00	
30	30	JA	0.0	1.65E+12	2.10E+00	-4.71E+04	1.113E+01	1.113E+01	1.120E+01	1.1200E+01	1.1051E+01	5.50E+00	BEAMG
30	31	JH	100.0	1.65E+12	2.10E+00	-4.71E+04	1.113E+01	1.113E+01	1.112E+01	1.1126E+01	1.1125E+01	5.56E+00	
31	31	JA	0.0	-1.36E+12	1.20E+02	-8.37E+01	5.181E+02	8.997E+02	6.175E+02	9.0032E+02	3.3585E+02	4.58E+02	BEAMG
31	32	JH	100.0	-1.36E+12	1.20E+02	-8.37E+01	5.181E+02	8.997E+02	6.094E+02	9.0440E+02	3.2775E+02	4.52E+02	
32	30	JA	0.0	1.30E+11	-1.02E+00	-1.52E+04	-1.261E+01	-1.251E+01	-1.266E+01	-1.2558E+01	-1.2659E+01	6.28E+00	BEAMG
32	33	JH	100.0	1.30E+11	-1.02E+00	-1.52E+04	-1.261E+01	-1.261E+01	-1.262E+01	-1.2604E+01	-1.2623E+01	6.30E+00	
33	33	JA	0.0	3.23E+12	-5.60E+01	-2.71E+01	-7.007E+02	-1.571E+03	-7.071E+02	1.7581E+02	-1.5773E+03	9.20E+01	BEAMG
33	34	JH	100.0	3.23E+12	-5.60E+01	-2.71E+01	-7.007E+02	-1.571E+03	-7.033E+02	1.7200E+02	-1.5735E+03	9.02E+01	
34	30	JA	0.0	2.69E+12	1.07E+11	0.	4.283E+12	4.283E+12	4.432E+11	4.4323E+11	-3.5758E+11	2.22E+11	PIPEG
34	35	JH	100.0	2.69E+12	1.07E+11	0.	4.283E+12	4.283E+12	3.431E+11	3.4313E+11	-2.5749E+11	1.72E+11	
35	35	JA	0.0	1.07E+12	9.99E+12	0.	3.331E+12	-3.019E+13	8.175E+12	9.3455E+12	-2.7237E+12	4.59E+12	PIPEG
35	36	JH	100.0	1.07E+12	9.99E+12	0.	3.331E+12	3.331E+12	3.3309E+12	3.3309E+12	1.67E+12		
36	37	JA	0.0	6.70E+01	1.11E+02	2.17E+01	-1.359E+11	1.032E+02	1.698E+02	1.9868E+02	-1.9868E+02	1.02E+02	PIPEG
36	36	JH	100.0	6.70E+01	1.11E+02	2.17E+01	-1.359E+11	5.194E+01	8.475E+01	9.9424E+01	-9.9424E+01	5.43E+01	
37	16	JA	0.0	1.62E+01	4.92E+01	3.80E+00	-3.907E+01	-5.795E+00	5.431E+01	5.0062E+01	-1.3820E+02	3.03E+01	PIPEG
37	38	JH	100.0	1.62E+01	4.92E+01	3.80E+00	-3.907E+01	-1.404E+01	2.930E+01	3.3735E+01	-1.1187E+02	1.73E+01	
38	11	JA	0.0	4.35E+01	-3.62E+00	-7.27E+04	-1.257E+01	-3.256E+01	-3.268E+01	-3.2442E+01	-3.2700E+01	1.62E+01	BEAMG
38	39	JH	100.0	4.35E+01	-3.62E+00	-7.27E+04	-1.257E+01	-3.257E+01	-3.256E+01	-3.2559E+01	-3.2583E+01	1.63E+01	
39	39	JA	0.0	-1.52E+12	-2.01E+02	-1.01E+02	-1.810E+03	-1.151E+03	-1.892E+03	-1.1431E+03	-2.4762E+03	5.80E+02	BEAMG
39	40	JH	100.0	-1.52E+12	-2.01E+02	-1.01E+02	-1.810E+03	-1.151E+03	-1.788E+03	-1.1296E+03	-2.4998E+03	5.74E+02	
40	11	JA	0.0	-5.23E+01	1.13E+01	-1.04E+03	1.955E+01	3.953E+01	3.999E+01	4.0005E+01	3.9085E+01	2.00E+01	BEAMG
40	41	JH	100.0	-5.23E+01	1.13E+01	-1.04E+03	1.955E+01	3.955E+01	3.960E+01	3.9597E+01	3.9494E+01	1.94E+01	
41	41	JA	0.0	5.23E+01	6.27E+02	-6.33E+01	2.197E+03	1.143E+03	2.232E+03	3.2863E+03	1.1080E+03	1.64E+03	BEAMG
41	42	JH	100.0	5.23E+01	6.27E+02	-6.33E+01	2.197E+03	1.143E+03	2.199E+03	3.2580E+03	1.1364E+03	1.63E+03	

NOZZLE LOAD CASE 3- MAXIMUM OVERTURNING MOMENT
MAXIMUM STRESS SUMMARY FOR

--- TRANSVERSE --- TORSIONAL - STRESSES AT USER LOCATIONS - FOR OUTPUT VECTOR 3
SHEAR SHEAR (T_{P/C/J}) A B C MAXIMUM MINIMUM COMBINED
(V_{C/K^{3/4}A}) (V_{B/K^{3/4}A}) (P/A+MC/I) (P/A-MC/I) STRESS

MAX. BEAM STRESSES = 4.53E+02 6.27E+02 1.16E+03 2.197E+03 2.997E+03 2.232E+03 3.2863E+03 1.1364E+03 1.89E+03
BEAM NOS. = 25. 1. 5. 41. 28. 41. 41. 41. 28.

MIN. BEAM STRESSES = -1.69E+02 -4.53E+02 -1.16E+03 -1.810E+03 -2.088E+03 -1.802E+03 -1.1431E+03 -2.6457E+03 1.67E-12
BEAM NOS. = 7. 2. 39. 2. 39. 39. 5. 35.

Appendix B

COMBINE OUTPUT

This section contains the following:

B.1 COMBINE Abstract

B.2 COMBINE Output

Appendix B.1
COMBINE ABSTRACT

PROGRAM COMBINE

ABSTRACT

"COMBINE" is designed to take beam element loads from a STARDYNE model and combine these loads in the following manner:

- 1) Beam loads due to nozzle or external load cases are combined in a square root of the sum of the squares or absolute sum manner.
- 2) Beam loads due to earthquake and deadweight are used directly from tape.
- 3) The program calculates stresses due to the above loads separately and adds and subtracts the beam stresses from cylinder membrane stresses (if the beam is a pipe or elbow), calculates the maximum stress intensity for both cases and prints out the absolute maximum.
- 4) The program also adds the absolute sum or SRSS of the external loads from 1) with each earthquake and dead-weight and then adds in pressure stresses as in 3).

The primary use for the program is in making Section III comparisons for faulted and upset conditions. A key in the program allows the external and earthquake cases to be multiplied by factors, thus allowing, for example, upset conditions to be calculated from faulted conditions. The program also has a key which allows the input of beam properties different from those used in the STARDYNE analysis.

COMBINE is written in FORTRAN 4 for use on the CDC 6600 computer. Verification prepared by John C. Minichicello.

THEORY

The load and stress calculations for "COMBINE" are performed in the following manner.

- 1) Assume for beam N in a STARDYNE model we have external load cases which produce an axial force at node JB of:

Case 1, $P = M$

Case 2, $P = L$

Case 3, $P = Q$

then, in the external load analysis, the axial force used at JB of beam N is

$$P_{SRSS} = \sqrt{M^2 + L^2 + Q^2}$$

IF the beam has a cross-section of A, then the axial stress due to P_{SRSS} is

$$\sigma_{SRSS} = P_{SRSS}/A$$

Similar treatment is given to the shear loads V_2 and V_3 , the bending loads M_2 and M_3 , and the torsional load T with the following results:

$$\sigma(SRSS) = P(SRSS)/A$$

$$\tau_2(SRSS) = V_2(SRSS)/A$$

$$\tau_3(SRSS) = V_3(SRSS)/A$$

$$B_2(SRSS) = M_2(SRSS) C_3/I_2$$

$$B_3(SRSS) = M_3(SRSS) C_2/I_2$$

$$\tau_o(SRSS) = T(SRSS) CTORS/J$$

where:

- A = Cross-section area
- C₃ = Half beam width in "3" direction
- C₂ = Half beam width in "2" direction
- I₂ = Moment of inertia about "2" axis
- I₃ = Moment of inertia about "3" axis
- CTORS = Torsional multiplier
- J = Torsional constant

If beam N is a pipe or elbow, the pressure stresses are:

$$\sigma_{(AXIAL)}_p = pR/2t$$

$$\sigma_{(HOOP)}_p = pR/t$$

$$\sigma_{(RADIAL)}_p = -p/2$$

where:

p = pressure

R = mean radius

t = wall thickness

If beam N is a general or rectangular beam, pressure stresses are zero.

The SRSS stresses are combined with pressure thusly:

a) If the beam is a pipe or elbow

$$\sigma_{(AXIAL)}_{TOTAL} = \frac{pR}{2t} \pm (\sigma_{(SRSS)} + \sqrt{B_2(SRSS)^2 + B_3(SRSS)^2})$$

b) If the beam is rectangular or general

$$\sigma_{\text{AXIAL}}^{\text{TOTAL}} = \sigma_{\text{SRSS}} + B_2(\text{SRSS}) + B_3(\text{SRSS})$$

The shear stress on the axial plane in the hoop direction is found by

$$\tau_{\text{AX-HOOP}}^{\text{TOTAL}} = \tau_0(\text{SRSS}) + \sqrt{\tau_2(\text{SRSS})^2 + \tau_3(\text{SRSS})^2}$$

and the hoop and radial stress are as shown previously.

The maximum stress intensity for each total (pressure \pm SRSS) is now calculated

$$\sigma_1 = (\sigma_{\text{AXIAL}}^{\text{TOTAL}} + \sigma_{\text{HOOP}})_p / 2$$

$$+ \sqrt{\frac{(\sigma_{\text{AXIAL}}^{\text{TOTAL}} - \sigma_{\text{HOOP}})_p)^2}{4} + \tau_{\text{TOTAL}}^2}$$

$$\sigma_2 = (\sigma_{\text{AXIAL}}^{\text{TOTAL}} + \sigma_{\text{HOOP}})_p / 2 - \sqrt{\dots}$$

$$\sigma_3 = \sigma_{\text{RADIAL}}_p$$

Max stress intensity = absolute maximum of

$$((\sigma_1 - \sigma_2, \sigma_2 - \sigma_3, \sigma_3 - \sigma_1)_p + \text{SRSS}, (\sigma_1 - \sigma_2, \sigma_2 - \sigma_3, \sigma_3 - \sigma_1)_{p-\text{SRSS}})$$

Similar calculations are done if an absolute sum of the external load effects is desired. Referring to the previous discussion of beam N

$$P_{\text{ABS}} = |M| + |L| + |-Q|$$

The treatment for all remaining calculations is identical with ABS replacing SRSS as a subscript.

- 2) For loads due to a static or dynamic (DYNRE4) earthquake analysis, "COMBINE" reads the earthquake loads directly from each of the earthquake files. If earthquakes (for example, vertical plus north-south) are to be combined in an SRSS or absolute sum procedure, this must be done before input to "COMBINE". This is done internally in a DYNRE4 analysis. For static seismic earthquakes, program "PRECOM" does the required manipulations. The method used in "PRECOM" is identical to that used by "COMBINE" for external loads. The file output from "PRECOM" can then be used as input to "COMBINE".

Stresses due to the earthquake loads of each earthquake file input to "COMBINE" are now combined with pressure as in 1) and the maximum stress intensity calculated.

- 3) For beam loads due to deadweight and other external loads the sign and direction of which are known, "COMBINE" reads directly from the STARDYNE output file which contains the loads. The stresses due to these loads are then calculated and combined with pressure as in 1) and the maximum stress intensity calculated.

4) "COMBINE" now find the sum of the beam load due to the SRSS (or absolute sum) of the external loads (1) + earthquake (2) + deadweight and signed external loads (3) for each earthquake file. Since the SRSS (or absolute sum) loads and earthquake loads can be either positive or negative, the sum is made such that the sign of the deadweight run load is used, i.e., if for beam N at node JA we have

$$P(\text{SRSS})_{\text{AXIAL}} = +10$$

$$P(\text{EARTHQUAKE 1})_{\text{AXIAL}} = +20$$

$$P(\text{DEADWEIGHT})_{\text{AXIAL}} = -30$$

then

$$P(\text{TOTAL})_{\text{AXIAL}} = -60$$

Beam load stresses are now calculated for the total as in 1). These stresses are combined with pressure as in 1) with the following exceptions. If the axial and bending stresses due to total beam loads are negative because of deadweight and signed loads, the absolute value of the sum is added to and subtracted from the axial pressure stress to obtain the two possible load cases. If the torsional stress is negative for the same reason, it is made positive before addition to the transverse shear stress. The maximum intensity is now calculated as before.

Appendix B.2
COMBINE OUTPUT

EARTHQUAKE.1 • NOZZLE LOADS • DEADWEIGHT

BEAM ELEMENT LOADS

NOZZLE LOADS • EARTHQUAKE. N.O. 1 • DEADWEIGHT

BEAM	NODE	AXIAL	SHEAR V2	SHEAR V3	BENDING M2	BENDING M3	TORSION MT
1	1 JA	.10775E+05	.43540E+04	.43540E+04	.0	.0	.0
1	4 JB	-.10775E+05	-.43540E+04	-.43540E+04	-.12300E+06	-.12300E+06	.0
2	3 JA	.29520E+04	.0	.29520E+04	.26745E+05	.90300E+05	.90300E+05
2	2 JB	.29520E+04	.0	.29520E+04	.0	.90300E+05	.90300E+05
3	3 JA	.29520E+04	.0	.29520E+04	.26745E+05	.90300E+05	.90300E+05
3	4 JB	.29520E+04	.0	.29520E+04	-.96678E+05	.90300E+05	.90300E+05
4	4 JA	.29520E+04	.0	.29520E+04	.96678E+05	.90300E+05	.90300E+05
4	5 JB	.29520E+04	.0	.29520E+04	.26745E+05	.90300E+05	.90300E+05
5	5 JA	.29520E+04	.0	.29520E+04	.26745E+05	.90300E+05	.90300E+05
5	6 JB	.29520E+04	.0	.29520E+04	.0	.90300E+05	.90300E+05
6	6 JA	-.10775E+05	.10258E+05	.10258E+05	.30350E+06	.30360E+06	.0
6	7 JB	-.10775E+05	.10258E+05	.10258E+05	.53184E+06	.53184E+06	.0
7	7 JA	.23602E+05	.15441E+05	.15441E+05	.53184E+06	.53184E+06	.0
7	8 JB	.23602E+05	.15441E+05	.15441E+05	.68038E+06	.68038E+06	.0
8	8 JA	.31628E+05	.18684E+05	.18684E+05	.68038E+06	.68038E+06	.0
8	11 JB	-.31628E+05	.18684E+05	.18684E+05	.94195E+06	.94195E+06	.0
9	10 JA	.55220E+04	.0	.55230E+04	.43189E+05	.21029E+06	.21029E+06
9	11 JB	.55220E+04	.0	.55230E+04	.0	.21029E+06	.21029E+06
10	10 JA	.55220E+04	.0	.55230E+04	.43189E+05	.21029E+06	.21029E+06
10	11 JB	.55220E+04	.0	.55230E+04	.19884E+06	.21029E+06	.21029E+06
11	11 JA	.31628E+05	.15588E+05	.18721E+05	.12220E+07	.92882E+06	.13943E+06
11	12 JA	-.31628E+05	.15588E+05	.18721E+05	.95994E+06	.71059E+06	.13943E+06
12	12 JA	.52191E+05	.72790E+04	.10412E+05	.95994E+06	.71059E+06	.13943E+06
12	37 JB	-.52191E+05	.72790E+04	.10412E+05	.47578E+06	.37209E+06	.13943E+06
13	13 JA	.32224E+05	.79790E+04	.16930E+04	.85520E+04	-.12733E+06	.46280E+04
13	14 JB	.32224E+05	-.79790E+04	.16930E+04	.27000E+02	.16255E+06	.46280E+04
14	15 JA	.79790E+04	-.32224E+05	.16930E+04	.18653E+05	.14357E+06	.27000E+02
14	14 JB	-.79790E+04	-.32224E+05	.16930E+04	.45280E+04	.16255E+06	.27000E+02
15	15 JA	.79790E+04	-.32224E+05	.16930E+04	.18653E+05	.14357E+06	.27000E+02
15	16 JB	-.79790E+04	-.32224E+05	.16930E+04	.56753E+05	-.85850E+05	.27000E+02

3.2-1

B
EAM ELEMENT LOADS

NOZZLE LOADS + EARTHQUAKE NO. 1 + DEADWEIGHT

BEAM NO	NODE	AXIAL P	SHEAR V2	SHEAR V3	BENDING M2	BENDING M3	TORSION MT
15	16 JA	.79450E+04	.34587E+03	.95900E+03	.24251E+05	.94250E+06	.27000E+02
16	17 JB	-.79450E+04	-.34587E+03	.95900E+03	.12597E+05	-.16430E+06	.27000E+02
17	17 JA	.79450E+04	.34587E+03	.95900E+03	.12597E+05	.16436E+06	.27000E+02
17	18 JB	-.79450E+04	-.34587E+03	.95900E+03	.91540E+04	.16422E+06	.27000E+02
18	19 JA	.34587E+05	.79450E+04	.95900E+03	.48250E+04	-.20429E+06	.91540E+04
18	18 JB	-.34587E+05	-.79450E+04	.95900E+03	.27000E+02	.16422E+06	.91540E+04
19	20 JA	.39250E+05	.75940E+04	.16420E+04	.82830E+04	-.20304E+06	.48820E+04
19	21 JB	-.39250E+05	-.75940E+04	.16420E+04	.25000E+02	.16473E+06	.48820E+04
20	22 JA	.75940E+04	.35268E+05	.16420E+04	.18420E+05	.17031E+06	.25000E+02
20	21 JB	-.75940E+04	-.35268E+05	.16420E+04	.48820E+04	.16473E+06	.25000E+02
21	22 JA	.75940E+04	.35268E+05	.16420E+04	.18420E+05	.17031E+06	.25000E+02
21	15 JB	-.75940E+04	-.35268E+05	.16420E+04	.55368E+05	-.96383E+06	.25000E+02
22	15 JA	.70310E+04	.31543E+05	.10100E+04	.25630E+05	.84733E+06	.25000E+02
22	23 JB	-.70310E+04	-.31543E+05	.10100E+04	.12829E+05	-.13761E+06	.25000E+02
23	23 JA	.70310E+04	.31543E+05	.10100E+04	.12829E+05	.13761E+06	.25000E+02
23	24 JB	-.70310E+04	-.31543E+05	.10100E+04	.89010E+04	.16204E+06	.25000E+02
24	25 JA	.31543E+05	.76310E+04	.10100E+04	.50950E+04	-.12608E+06	.89010E+04
24	24 JB	-.31543E+05	-.76310E+04	.10100E+04	.25000E+02	.16204E+06	.89010E+04
25	35 JA	-.55701E+05	.72610E+04	.95950E+04	.30296E+06	.23549E+06	.17386E+05
25	26 JB	.55701E+05	.72610E+04	.95950E+04	.35132E+06	.25965E+06	.17386E+05
26	25 JA	-.33455E+05	.40970E+04	.64310E+04	.35132E+06	.25965E+06	.17386E+05
26	27 JB	.33455E+05	.40970E+04	.64310E+04	.39627E+06	.13176E+06	.17386E+05
27	27 JA	-.19155E+05	.10279E+05	.12613E+05	.39627E+06	.13176E+06	.17386E+05
27	30 JB	.19155E+05	.10279E+05	.12613E+05	.55720E+05	.26001E+06	.17386E+05
28	29 JA	.55220E+04	.55230E+04	.0	.0	.25349E+06	.21029E+06
28	28 JB	.55220E+04	.55230E+04	.0	.0	.21029E+06	.21029E+06
29	29 JA	.55220E+04	.55230E+04	.0	.0	.25349E+06	.21029E+06
29	30 JB	.55220E+04	.55230E+04	.0	.0	.40915E+06	.21029E+06
30	30 JA	.15035E+05	.0	.12670E+04	.32377E+05	.76000E+02	.24400E+03
30	31 JB	.15035E+05	.0	.12670E+04	.73800E+04	.76000E+02	.24400E+03

B.22

BEAM ELEMENT LOADS

NOZZLE LOADS - EARTHQUAKE NO. 1 + DEADWEIGHT

BEAM #0	NODE #0	AXIAL P	SHEAR V2	SHEAR V3	BENDING M2	BENDING M3	TORSION MT
		2.7					
31	31 JA	.15635E+05	.0	.12670E+04	.73800E+04	.76000E+02	.24400E+03
31	32 JB	.15635E+05	.0	.12570E+04	.81520E+04	.76000E+02	.24400E+03
32	33 JA	.14891E+05	.0	.12830E+04	.31474E+05	.15800E+03	.11600E+03
32	33 JB	.14891E+05	.0	.12830E+04	.60330E+04	.15800E+03	.11600E+03
33	33 JA	.14891E+05	.0	.12830E+04	.60330E+04	.15800E+03	.11600E+03
33	34 JB	.14891E+05	.0	.12830E+04	.95600E+04	.15800E+03	.11600E+03
34	30 JA	-.12632E+05	.0	.10400E+04	.51040E+04	.11939E+06	.0
34	35 JB	.12632E+05	.0	.51040E+04	.51040E+04	.47934E+05	.0
35	35 JA	-.42170E+04	.0	.17040E+04	.17040E+04	.47934E+05	.47934E+05
35	35 JB	.42170E+04	.0	.17040E+04	.0	.0	.0
36	37 JA	.52191E+05	.0	.72790E+04	.10412E+05	.47578E+06	.37209E+06
36	36 JB	.52191E+05	.0	.72790E+04	.10412E+05	.30060E+06	.24954E+05
37	16 JA	-.55701E+05	.0	.26100E+04	.95950E+04	.41023E+06	.31566E+06
37	38 JB	.55701E+05	.0	.26100E+04	.95950E+04	.30296E+05	.23549E+06
38	11 JA	.38357E+05	.0	.51300E+03	.33360E+04	.81346E+05	.14183E+05
38	39 JB	.38357E+05	.0	.51300E+03	.33360E+04	.11046E+05	.17900E+03
39	39 JA	.38357E+05	.0	.0	.33360E+04	.11052E+05	.17900E+03
39	40 JB	.38357E+05	.0	.0	.33360E+04	.25432E+05	.17900E+03
40	11 JA	.41874E+05	.0	.55900E+03	.72130E+04	.21378E+06	.15729E+05
40	41 JB	.41874E+05	.0	.55900E+03	.72130E+04	.26699E+05	.23400E+03
41	41 JA	.41874E+05	.0	.0	.72130E+04	.26705E+05	.23400E+03
41	42 JB	.41874E+05	.0	.0	.72130E+04	.17035E+05	.23400E+03

B2.3

EARTHQUAKE 1 + NOZZLE LOADS + DEADWEIGHT

BEAM ELEMENT STRESSES

NOZZLE LOADS + EARTHQUAKE NO. 1 + DEADWEIGHT

BEAM NO.	NODE	AXIAL PVA	SHEAR V2/A	SHEAR V3/A	BENDING M2*C/12	BENDING M3*C/13	TORSION T*C/J
1	1 JA	.60297E+02	.24365E+02	.24365E+02	.0	.0	.0
1	4 JB	-.60297E+02	-.24365E+02	-.24365E+02	.62134E+02	.62134E+02	.0
2	3 JA	.22919E+03	.0	.0	.22919E+03	.69625E+03	.23170E+04
2	2 JB	.22919E+03	.0	.0	.22919E+03	.0	.23170E+04
3	3 JA	.59040E+01	.0	.0	.59040E+01	.66802E+01	.22575E+00
3	4 JB	.59040E+01	.0	.0	.59040E+01	.24169E+00	.22575E+00
4	4 JA	.59040E+01	.0	.0	.39040E+01	.24169E+00	.22575E+00
4	5 JB	.59040E+01	.0	.0	.59040E+01	.66802E+01	.22575E+00
5	5 JA	.22919E+03	.0	.0	.22919E+03	.69625E+03	.23170E+04
5	6 JB	.22919E+03	.0	.0	.22919E+03	.0	.23170E+04
6	4 JA	.60297E+02	.57403E+02	.57403E+02	.15336E+03	.15336E+03	.0
6	7 JB	-.60297E+02	-.57403E+02	-.57403E+02	.26866E+03	.26866E+03	.0
7	7 JA	.33765E+03	.22090E+03	.22090E+03	.69150E+03	.69150E+03	.0
7	8 JB	.33765E+03	.42090E+03	.22090E+03	.88464E+03	.88464E+03	.0
8	8 JA	.29097E+03	.17189E+03	.17189E+03	.45706E+03	.45706E+03	.0
8	11 JB	-.29097E+03	-.17189E+03	-.17189E+03	.63278E+03	.63278E+03	.0
9	10 JA	.22675E+03	.0	.0	.22682E+03	.47205E+03	.22985E+04
9	9 JB	.22675E+03	.0	.0	.22682E+03	.0	.22985E+04
10	10 JA	.11044E+02	.0	.0	.11046E+02	.10797E+00	.52573E+00
10	11 JB	.11044E+02	.0	.0	.11046E+02	.49711E+00	.52573E+00
11	11 JA	.24047E+03	.14340E+03	.17223E+03	.82093E+03	.62396E+03	.46831E+02
11	12 JB	-.24047E+03	-.14340E+03	-.17223E+03	.64486E+03	.47735E+03	.46831E+02
12	12 JA	.74055E+03	.10413E+03	.14496E+03	.12431E+04	.92391E+03	.90644E+02
12	37 JB	-.74055E+03	-.10413E+03	-.14496E+03	.61861E+03	.48379E+03	.90644E+02
13	13 JA	.64444E+02	.15958E+02	.33460E+01	.21389E-01	-.31833E+00	.11570E-01
13	14 JB	-.64444E+02	-.15958E+02	-.33460E+01	.67500E-04	.40636E+00	.11570E-01
14	15 JA	.23269E+03	.73975E+03	.49373E+02	.59460E+02	.88286E+03	.32275E+01
14	14 JB	-.23269E+03	-.73975E+03	-.49373E+02	.14756E+02	.99959E+03	.32275E+01
15	15 JA	.15958E+02	-.64444E+02	.33460E+01	.46632E-01	.35892E+00	.67500E-04
15	16 JB	-.15958E+02	-.64444E+02	-.33460E+01	.14188E+00	-.21715E+01	.67500E-04

B.2-4

BEAM ELEMENT STRESSES

FOR EACH ELEMENT THE FOLLOWING ARE LISTED: ID, LENGTH, ELEMENT TYPE

ELM	NO	TYPE	X1/A	X2/A	SHEAR V3/A	BENDING M2°C/12	BENDING M3°C/13	TORSION T°C/J
16	16 JA	--	.15892E+02	.69174E+02	.19180E+01	.60527E-01	.23564E+01	.67500E-04
16	17 JB	--	.15892E+02	.69174E+02	.19180E+01	.31492E-01	.-41089E+00	.67500E-04
17	17 JA	--	.23173E+03	.10087E+04	.27967E+02	.40169E+02	.10107E+04	.32275E+01
17	18 JB	--	.23173E+03	.-10087E+04	.27967E+02	.29190E+02	.-10098E+04	.32275E+01
18	19 JA	--	.69174E+02	.15892E+02	.19180E+01	.12065E-01	.-51072E+00	.22845E-01
18	19 JB	--	.69174E+02	.-15892E+02	.19180E+01	.67500E-04	.41055E+00	.22845E-01
19	20 JA	--	.70535E+02	.15196E+02	.32440E+01	.20707E-01	.-50759E+00	.12205E-01
19	21 JB	--	.70535E+02	.-15196E+02	.32440E+01	.62500E-04	.41183E+00	.12205E-01
20	22 JA	--	.23158E+03	.10285E+04	.47845E+02	.58737E+02	.10473E+04	.29844E+01
20	21 JB	--	.23158E+03	.-10285E+04	.47845E+02	.15568E+02	.10130E+04	.29844E+01
21	22 JA	--	.15195E+02	.70536E+02	.32840E+01	.46050E-01	.42577E+00	.62500E-04
21	16 JB	--	.15195E+02	.-70536E+02	.32840E+01	.13842E+00	.-24096E+01	.62500E-04
22	15 JA	--	.15262E+02	.63086E+02	.20200E+01	.64090E-01	.-21183E+01	.62500E-04
22	23 JB	--	.15262E+02	.-63086E+02	.20200E+01	.32072E-01	.-34404E+00	.62500E-04
23	23 JA	--	.22254E+03	.-71969E+03	.29455E+02	.40409E+02	.-84624E+03	.29844E+01
23	24 JB	--	.22254E+03	.71969E+03	.29455E+02	.28303E+02	.99645E+03	.29844E+01
24	25 JA	--	.63086E+02	.15262E+02	.20200E+01	.12737E-01	.-31520E+00	.22252E-01
24	24 JB	--	.63086E+02	.-15262E+02	.20200E+01	.62500E-04	.40510E+00	.22252E-01
25	3d JA	--	.72567E+03	.10328E+03	.13727E+03	.39390E+03	.-30618E+03	.11303E+02
25	25 JB	--	.72567E+03	.-10328E+03	.13727E+03	.45679E+03	.33760E+03	.11303E+02
26	26 JA	--	.47603E+03	.28612E+02	.92003E+02	.45679E+03	.33760E+03	.11303E+02
26	27 JB	--	.47603E+03	.-28612E+02	.92003E+02	.51524E+03	.17131E+03	.11303E+02
27	27 JA	--	.16702E+03	.94563E+02	.11503E+03	.26621E+03	.88512E+02	.58397E+01
27	30 JB	--	.16702E+03	.-94563E+02	.11503E+03	.37431E+03	.17467E+03	.58397E+01
28	29 JA	--	.22674E+03	.22682E+03	.0	.0	.27705E+04	.11492E+04
28	29 JB	--	.22674E+03	.-22682E+03	.0	.0	.22985E+04	.11492E+04
29	29 JA	--	.11044E+02	.11046E+02	.0	.0	.63372E+00	.52573E+00
29	30 JB	--	.11044E+02	.-11046E+02	.0	.0	.10229E+01	.52573E+00
30	30 JA	--	.31270E+02	.0	.25340E+01	.80942E-01	.19000E-03	.61000E-03
30	31 JB	--	.31270E+02	.0	.25340E+01	.18450E-01	.19000E-03	.61000E-03

B.2.5

BEAM ELEMENT STRESSES

NUZZLE LOADS + EARTHQUAKE NO. 1 + DEADWEIGHT

BEAM NO	NODE	AXIAL P/A	SHEAR V2/A	SHEAR V3/A	BENDING M2*C/12	BENDING M3*C/13	TORSION T*C/J
31	31 JA	.17372E+04	.0	.14078E+03	.12812E+02	.54028E+03	.10841E+03
31	32 JB	.17372E+04	.0	.14078E+03	.14153E+02	.54028E+03	.10841E+03
32	30 JA	.27152E+02	.0	.25660E+01	.78665E-01	.39500E-03	.29000E-03
32	33 JB	.27152E+02	.0	.25660E+01	.15032E-01	.39500E-03	.24000E-03
33	33 JA	.15546E+04	.0	.14256E+03	.10474E+02	.11232E+04	.51540E+02
33	34 JB	.15546E+04	.0	.14256E+03	.16611E+02	.11232E+04	.51540E+02
34	30 JA	-.11621E+03	-.69455E+02	.46455E+02	.80202E+02	.80202E+02	.0
34	35 JB	-.11621E+03	-.69455E+02	.46455E+02	.32201E+02	.32201E+02	.0
35	35 JA	-.60324E+02	.24378E+02	.24378E+02	.62324E+02	.62324E+02	.0
35	36 JB	-.60324E+02	.24378E+02	.24378E+02	.0	.0	.0
35	37 JA	.30410E+03	.>1478E+02	.73635E+02	.30565E+03	.23904E+03	.44785E+02
35	16 JB	.30410E+03	.>1478E+02	.73635E+02	.19314E+03	.16038E+03	.44785E+02
37	15 JA	-.39393E+03	.>1351E+02	.67857E+02	.26354E+03	.20343E+03	.55845E+01
37	36 JB	-.39393E+03	.>1351E+02	.67857E+02	.19463E+03	.15128E+03	.55845E+01
38	11 JA	.70774E+02	.10250E+01	.66720E+01	.20330E+00	.35957E-01	.12700E-02
38	39 JB	.70774E+02	.10250E+01	.66720E+01	.27615E-01	.44750E-03	.12700E-02
39	39 JA	.42657E+04	.0	.37067E+03	.19187E+02	.12725E+04	.15995E+03
39	40 JB	.42657E+04	.0	.37067E+03	.44153E+02	.12725E+04	.15995E+03
40	11 JA	.83746E+02	.11180E+01	.14426E+02	.53444E+00	.39322E-01	.15800E-02
40	41 JB	.83746E+02	.11180E+01	.14426E+02	.66747E-01	.58500E-03	.15800E-02
41	41 JA	.46531E+04	.0	.80144E+03	.46363E+02	.16635E+04	.12214E+03
41	42 JB	.46531E+04	.0	.80144E+03	.29580E+02	.16635E+04	.12214E+03

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EARTHQUAKE 1 • NOZZLE LOADS • DEADWEIGHT

ELEMENT TOTAL STRESSES AND MAXIMUM STRESS INTENSITY

NOZZLE LOADS • DEADWEIGHT • EARTHQUAKE NO 1

BEAM	NODE	PRESSURE AXIAL	PRESSURE HOOP	PRESSURE RADIAL	TOTAL AXIAL	TOTAL SHEAR	TOTAL AXIAL	MAXIMUM INTENSITY
1	1	.59150E+04	.11630E+05	-.32500E+03	.59753E+04	.34457E+02	.58457E+04	.12155E+05
1	4	.59150E+04	.11630E+05	-.32500E+03	.60023E+04	.34457E+02	.57677E+04	.12155E+05
2	3	-.51159E+04	.12232E+05	-.32500E+03	.87611E+04	.13877E+04	.34707E+04	.13043E+05
2	2	.61159E+04	.12232E+05	-.32500E+03	.86021E+04	.13877E+04	.35697E+04	.13033E+05
3	3	.0	.0	.0	.59040E+01	.61297E+01	-.59040E+01	.13607E+02
3	4	.0	.0	.0	.59040E+01	.61297E+01	-.59040E+01	.13607E+02
4	5	.0	.0	.0	.59040E+01	.61297E+01	-.59040E+01	.13607E+02
5	5	.61159E+04	.12232E+05	-.32500E+03	.47611E+04	.13877E+04	.34707E+04	.13043E+05
5	6	.61159E+04	.12232E+05	-.32500E+03	.86021E+04	.13877E+04	.35697E+04	.13033E+05
6	4	-.57150E+04	.11830E+05	-.32500E+03	.61713E+04	.81141E+02	.56357E+04	.12155E+05
6	7	.57150E+04	.11830E+05	-.32500E+03	.63543E+04	.81141E+02	.54757E+04	.12155E+05
7	7	.33375E+04	.66750E+04	-.75000E+02	.46522E+04	.31240E+03	.29228E+04	.67971E+04
7	8	.33375E+04	.66750E+04	-.75000E+02	.49252E+04	.31240E+03	.17498E+04	.68041E+04
8	8	.33225E+04	.66450E+04	-.75000E+02	.42595E+04	.24308E+03	.23655E+04	.67445E+04
8	11	.33225E+04	.66450E+04	-.75000E+02	.45075E+04	.24308E+03	.21375E+04	.67473E+04
9	10	.11625E+04	.23250E+04	-.75000E+02	.37453E+04	.13760E+04	-.14103E+04	.46513E+04
9	9	.11625E+04	.23250E+04	-.75000E+02	.36673E+04	.13760E+04	-.13523E+04	.46165E+04
10	10	.0	.0	.0	.11044E+02	.11572E+02	-.11044E+02	.25644E+02
10	11	.0	.0	.0	.12044E+02	.11572E+02	-.12044E+02	.26090E+02
11	11	.33225E+04	.66450E+04	-.75000E+02	.46495E+04	.27094E+03	.20005E+04	.67560E+04
11	12	.33225E+04	.66450E+04	-.75000E+02	.44155E+04	.27094E+03	.22295E+04	.67525E+04
12	12	.33375E+04	.66750E+04	-.75000E+02	.56302E+04	.27239E+03	.10318E+04	.68171E+04
12	17	.33375E+04	.66750E+04	-.75000E+02	.48692E+04	.27239E+03	.18058E+04	.67902E+04
13	13	.0	.0	.0	.64445E+02	.16325E+02	-.64445E+02	.72246E+02
13	14	.0	.0	.0	.64445E+02	.16325E+02	-.64445E+02	.72246E+02
14	15	.0	.0	.0	.11747E+04	.94427E+03	-.11747E+04	.22241E+04
14	14	.0	.0	.0	.12467E+04	.94427E+03	-.12467E+04	.22629E+04
15	15	.0	.0	.0	.15958E+02	.64537E+02	-.15958E+02	.13005E+03
15	16	.0	.0	.0	.17958E+02	.64537E+02	-.17958E+02	.13032E+03

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EARTHQUAKE 1 • NOZZLE LOADS • DEADWEIGHT

ELEMENT TOTAL STRESSES AND MAXIMUM STRESS INTENSITY

NOZZLE LOADS + DEADWEIGHT + EARTHQUAKE NO 1

BEAM	NODE	PRESSURE	PRESSURE	PRESSURE	TOTAL	TOTAL	TOTAL	MAXIMUM
		Axial	Hoop	Radial	Axial	SHEAR	Axial	INTENSITY
16	16	.0	.0	.0	.17692E+02	.69201E+02	-.17692E+02	.13955E+03
16	17	.0	.0	.0	.15892E+02	.69201E+02	-.15892E+02	.13931E+03
17	17	.0	.0	.0	.12817E+04	.10123E+04	-.12817E+04	.23962E+04
17	19	.0	.0	.0	.12707E+04	.10123E+04	-.12707E+04	.23903E+04
18	19	.0	.0	.0	.69174E+02	.16030E+02	-.69174E+02	.76242E+02
18	18	.0	.0	.0	.59174E+02	.16030E+02	-.59174E+02	.76242E+02
19	20	.0	.0	.0	.70536E+02	.15559E+02	-.70536E+02	.77095E+02
19	21	.0	.0	.0	.70536E+02	.15559E+02	-.70536E+02	.77095E+02
20	22	.0	.0	.0	.13276E+04	.10326E+04	-.13276E+04	.24551E+04
20	21	.0	.0	.0	.12496E+04	.10326E+04	-.12496E+04	.24139E+04
21	22	.0	.0	.0	.15196E+02	.70612E+02	-.15196E+02	.14204E+03
21	15	.0	.0	.0	.17196E+02	.70612E+02	-.17196E+02	.14227E+03
22	16	.0	.0	.0	.17202E+02	.63116E+02	-.17202E+02	.12741E+03
22	23	.0	.0	.0	.15202E+02	.63118E+02	-.15202E+02	.12716E+03
23	23	.0	.0	.0	.11095E+04	.92335E+03	-.11095E+04	.21544E+04
23	24	.0	.0	.0	.12465E+04	.92335E+03	-.12465E+04	.22240E+04
24	25	.0	.0	.0	.63036E+02	.15417E+02	-.63036E+02	.70218E+02
24	24	.0	.0	.0	.63036E+02	.15417E+02	-.63036E+02	.70218E+02
25	38	.33375E+04	.66750E+04	-.75000E+02	.46324E+04	.18344E+03	.20426E+04	.67663E+04
25	26	.33375E+04	.66750E+04	-.75000E+02	.47024E+04	.18344E+03	.19726E+04	.67664E+04
26	26	.33375E+04	.66750E+04	-.75000E+02	.43841E+04	.12039E+03	.22909E+04	.67553E+04
25	27	.33375E+04	.66750E+04	-.75000E+02	.43581E+04	.12039E+03	.23169E+04	.67562E+04
27	27	.33225E+04	.66450E+04	-.75000E+02	.37675E+04	.15553E+03	.28755E+04	.67294E+04
27	30	.33225E+04	.66450E+04	-.75000E+02	.39065E+04	.15553E+03	.27425E+04	.67285E+04
28	29	.11025E+04	.23250E+04	-.75000E+02	.41593E+04	.13760E+04	-.18343E+04	.49873E+04
29	28	.11625E+04	.23250E+04	-.75000E+02	.36873E+04	.13760E+04	-.13623E+04	.46165E+04
29	29	.0	.0	.0	.11044E+02	.11572E+02	-.11044E+02	.25644E+02
29	30	.0	.0	.0	.12044E+02	.11572E+02	-.12044E+02	.26090E+02
30	30	.0	.0	.0	.31270E+02	.25345E+01	-.31270E+02	.31674E+02
30	31	.0	.0	.0	.31270E+02	.25345E+01	-.31270E+02	.31678E+02

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EARTHQUAKE 1 + NOZZLE LOADS + DEADWEIGHT

ELEMENT TOTAL STRESSES AND MAXIMUM STRESS INTENSITY

NOZZLE LOADS + DEADWEIGHT + EARTHQUAKE NO 1

BEAM	NODE	PRESSURE	PRESSURE	PRESSURE	TOTAL	TOTAL	TOTAL	MAXIMUM
		AXIAL	HOOPLA	RADIAL	AXIAL	SHEAR	AXIAL	INTENSITY
31	31	.0	.0	.0	.22902E+04	.24919E+03	-.22902E+04	.23438E+04
31	32	.0	.0	.0	.24912E+04	.24919E+03	-.22912E+04	.23448E+04
32	30	.0	.0	.0	.29782E+02	.25663E+01	-.29782E+02	.30221E+02
32	33	.0	.0	.0	.29752E+02	.25663E+01	-.29752E+02	.30221E+02
33	33	.0	.0	.0	.27876E+04	.19410E+03	-.27876E+04	.28145E+04
33	34	.0	.0	.0	.27936E+04	.19410E+03	-.27936E+04	.28204E+04
34	38	.33225E+04	.66450E+04	-.75000E+02	.35817E+04	.66494E+02	-.30933E+04	.67214E+04
34	35	.33225E+04	.66450E+04	-.75000E+02	.34637E+04	.66404E+02	.31613E+04	.67214E+04
35	35	.33375E+04	.66750E+04	-.75000E+02	.34658E+04	.34475E+02	.31892E+04	.67504E+04
35	35	.33375E+04	.66750E+04	-.75000E+02	.33978E+04	.34475E+02	.32712E+04	.67504E+04
35	37	.16675E+04	.33750E+04	-.75000E+02	.24445E+04	.13463E+03	.93040E+03	.34691E+04
35	16	.16675E+04	.33750E+04	-.75000E+02	.23076E+04	.13463E+03	.10674E+04	.34667E+04
37	16	.16675E+04	.33750E+04	-.75000E+02	.24134E+04	.90681E+02	.96157E+03	.34585E+04
37	38	.16675E+04	.33750E+04	-.75000E+02	.23274E+04	.90681E+02	.10476E+04	.34578E+04
38	11	.0	.0	.0	.76774E+02	.67517E+01	-.76774E+02	.77952E+02
38	39	.0	.0	.0	.76774E+02	.67517E+01	-.76774E+02	.77952E+02
39	39	.0	.0	.0	.55567E+04	.53062E+03	-.55567E+04	.56571E+04
39	40	.0	.0	.0	.55817E+04	.53062E+03	-.55817E+04	.56817E+04
40	11	.0	.0	.0	.83748E+02	.14471E+02	-.83748E+02	.88604E+02
40	41	.0	.0	.0	.83748E+02	.14471E+02	-.83748E+02	.88604E+02
41	41	.0	.0	.0	.63021E+04	.92363E+03	-.63021E+04	.66249E+04
41	42	.0	.0	.0	.63401E+04	.92363E+03	-.63401E+04	.65095E+04

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Appendix A.2
"HQR" OUTPUT

***** EIGENVALUE EXTRACTION HAS BEEN COMPLETED FOR 27 EIGENVALUES *****

NUMBER	EIGENVALUE (OMEGA**2.)	FREQUENCY(E)	FREQUENCY(F)
1	.9276525E+05	.4847460057E+02	48.4746
2	.10055122E+06	.5046773346E+02	50.4577
3	.15276881E+06	.6220674513E+02	62.2067
4	.15311241E+06	.6227666134E+02	62.2767
5	.21987183E+06	.7462853750E+02	74.6285
6	.38341193E+06	.9854917177E+02	98.5492
7	.52319630E+06	.1151204551E+03	115.1205
8	.60528181E+06	.1298223216E+03	123.8223
9	.67447620E+06	.1491712557E+03	149.1713
10	.12405265E+07	.1772650681E+03	177.2651
11	.12637533E+07	.1789172172E+03	178.9172
12	.16621877E+07	.2051918749E+03	205.1919
13	.16624394E+07	.2052074392E+03	205.2074
14	.16990310E+07	.2073924480E+03	207.3924
15	.19999466E+07	.2250760833E+03	225.0761
16	.40362071E+07	.3197472740E+03	319.7473
17	.47113024E+07	.3454543327E+03	345.4543
18	.50233039E+07	.3567273697E+03	356.7274
19	.58277930E+07	.3842131197E+03	384.2131
20	.59752203E+07	.3890425396E+03	389.0425
21	.59771318E+07	.3891047654E+03	389.1048
22	.83672706E+07	.4603753251E+03	460.3753
23	.87571483E+07	.4704802803E+03	470.9803
24	.10001512E+08	.5040844811E+03	504.0845
25	.13912804E+08	.5930458794E+03	593.6459
26	.26676794E+08	.8189413991E+03	818.9414
27	.43250312E+08	.1046681994E+04	1046.6820

*** ENTERING PHASE 7 *** RUN DATE = 10/14/75 TIME OF DAY 17.51.30 ***

***** POST-PROCESS FOR ELEMENT LOADS LINK *****

A.2-1

MODE SHAPE (EIGENVECTOR)

MODE NUMBER	1 . FREQUENCY	= 48.474601	, GENERALIZED WEIGHT	= 12270.700		
		MAXIMUM ROTATION IS AT NODE 1 *DOF = 4 VALUE = -.117683E-01				
		MAXIMUM TRANSLATION IS AT NODE 1 *DOF = 2 VALUE = .100000E+01				
NODE	X1	X2	X3	X4	X5	X6
1	-1.000000000	1.000000000	0.000000000	-.011374836	-.011374836	.001828604
2	-.644464218	.634577428	-.372525865	-.011374836	-.011374836	.001828604
3	-.677697064	.634577428	-.259469855	-.011374836	-.011374836	.001828604
4	-.634577428	.634577428	.000000000	-.011374836	-.011374836	.001828604
5	-.591257793	.634577428	.269469855	-.011374836	-.011374836	.001828604
6	-.574590638	.634577428	.372525865	-.011374836	-.011374836	.001828604
7	-.361307196	.361307196	.000000000	-.010511046	-.010511046	.001828604
8	-.220913870	.220913870	.000000000	-.009084803	-.009084803	.001828604
9	-.099977500	.099977500	.000000000	-.007952114	-.007952114	.001828604
10	-.089865518	.089865518	-.000000000	-.007952114	-.007952114	.001828604
11	-.053421235	.053421235	.000000000	-.007952114	-.007952114	.001828604
12	.021352597	.021352597	.000000000	-.006764658	-.006764658	.001671774
14	.000012633	.0000534137	-.000076427	.0000001428	.000000042	.000000905
15	.002495511	.006108798	-.007278965	-.000355869	-.000372862	.000176304
16	.007014259	.007014259	.000000000	-.000372878	-.000372878	.000197760
17	.010593802	.010593802	.007278965	-.000355869	-.000372862	.000195779
18	.0001323418	.000534137	.000076427	.0000001428	.0000000331	-.000000059
21	.000534137	-.000018633	.000076427	.000000042	.0000001428	.0000000905
22	.006108798	-.00495511	.007278965	-.000372862	-.000355869	.000195304
23	.006108798	-.010693802	-.007278965	-.000372862	-.000355869	.000185779
24	.000534137	-.000135418	.000076427	.000000331	.0000001428	-.000000059
26	.036287337	.036287337	.000000000	.0000001946	.0000007946	.000094449
27	.004276154	.004276154	.000000000	.000444102	.000444102	-.000009516
28	.000156620	.001058642	-.023158681	.000454805	.000454805	-.000017675
29	.000256364	.000460828	-.01128536	.000454805	.000454805	-.000017675
30	.003606031	-.003606031	.000000000	.000454805	.000454805	-.000017675
31	.000545543	-.000545543	.012593471	.000454793	.000454793	-.000018339
32	0.000000000	0.000000000	.013573563	0.000000000	0.000000000	0.000000000
33	0.00059512	-.000545543	-.012593471	.000454793	.000454793	-.000018339
34	0.000000000	0.000000000	-.013573563	0.000000000	0.000000000	0.000000000
35	-.005173406	.006173406	.000000000	.000459437	.000459437	-.000017675
36	-.019980554	.019980554	.000000000	.0004647431	.0004647431	-.000017575
37	.024429794	-.024429794	.000000000	-.000772427	-.000772427	.000417117
38	.011597537	-.011597537	.000000000	-.00365070	-.00365070	.000190174
39	-.050518540	.004430096	.220017765	-.007951688	-.007949304	.001838974
40	0.000000000	0.003000000	-.237148515	0.000000000	0.000000000	0.000000000
41	-.004430096	.050518540	.220017765	-.007949304	-.007951688	.001838974
42	0.000000000	0.000000000	.237148515	0.000000000	0.000000000	0.000000000

MODAL PARTICIPATION FACTOR (X1) = -6.1181022E-01 GEN.WT. TIMES MODAL PART. FACT. (X1) = -7.5073397E+03
 MODAL PARTICIPATION FACTOR (X2) = 6.1181022E-01 GEN.WT. TIMES MODAL PART. FACT. (X2) = 7.5073397E+03
 MODAL PARTICIPATION FACTOR (X3) = 5.7833388E-13 GEN.WT. TIMES MODAL PART. FACT. (X3) = 7.0965617E-09

B.2-2

MODE SHAPE (EIGENVECTOR)

MODE NUMBER 2 • FREQUENCY = 50.467733 • GENERALIZED WEIGHT = 12001.937

*MAXIMUM ROTATION IS AT NODE 1 *DOF = 5 VALUE = .122074E-01

*MAXIMUM TRANSLATION IS AT NODE 1 *DOF = 1 VALUE = .100000E+01

***** TRANSLATIONS ***** ***** ROTATIONS (RADIAN) *****

NODE	X1	X2	X3	X4	X5	X6
1	1.000000000	1.000000000	.000000000	-.012207433	.012207433	-.000000000
2	.619403938	.619403937	-.38527348	-.011780988	.011780988	-.000000000
3	.619403938	.619403937	-.279091599	-.011780988	.011780988	-.000000000
4	.619403938	.619403937	.000000000	-.011780988	.011780988	-.000000000
5	.619403938	.619403937	-.279091599	-.011780988	.011780988	-.000000000
6	.619403938	.619403937	.38527348	-.011780988	.011780988	-.000000000
7	.335403207	.335403207	.000000000	-.010844704	.010844704	-.000000000
8	.189552963	.189552963	.000000000	-.009302761	.009302761	-.000000000
9	.017335510	.017335510	-.411739891	-.008086015	.008086015	-.000000000
10	.017335510	.017335510	-.322308564	-.008086015	.008086015	-.000000000
11	.017335510	.017335510	.000000000	-.008086015	.008086015	-.000000000
12	-.056720451	-.056720451	.000000000	-.006814365	.006814365	-.000000000
14	-.000090031	-.000612226	-.000053330	.000001573	-.000000215	-.000000553
15	-.007560613	-.007560613	-.005081398	-.00248417	.00260280	-.000006033
16	-.008041589	-.008041589	.000000000	-.00260291	.00260291	-.000000000
17	-.007560613	-.007560613	.005081398	-.00248417	.00260280	-.000006033
18	-.000090031	-.000612226	-.000053330	.000001573	-.000000215	-.000000553
21	-.0060612226	-.0060612226	-.000053330	-.00000215	-.000001573	-.000000553
22	-.007003557	-.007560613	-.005081398	-.00260280	-.00248417	-.000006033
23	-.007003557	-.007560613	.005081398	-.00260280	.00248417	-.000006033
24	-.000612226	-.000612226	-.000053330	.000000215	-.000001573	-.000000553
25	-.033520297	-.033520297	.000000000	.000021252	-.000021252	-.000000000
27	-.007381214	-.007381214	-.000000000	.000419018	-.000419018	-.000000000
28	-.000207529	-.000207529	.000000000	.000429589	-.000429589	-.000000000
29	-.000207529	-.000207529	.000000000	.000429589	-.000429589	-.000000000
30	-.000207529	-.000207529	-.000000000	.000429589	-.000429589	-.000000000
31	-.000166017	-.000055246	-.011895233	.000429577	-.000429583	-.000001833
32	0.000000000	0.000000000	-.012820985	0.000000000	0.000000000	0.000000000
33	-.000005246	-.000186017	-.011895233	.000429583	-.000429577	-.000001833
34	0.000000000	0.000000000	-.012820985	0.000000000	0.000000000	0.000000000
35	.016244760	.016244760	-.000000000	.000434487	-.000434487	-.000000000
36	.019401637	.019401637	-.000000000	.000442901	-.000442901	-.000000000
37	-.031790438	-.031790438	.000000000	-.000603158	.000603158	-.000000000
38	-.011799769	-.011799769	.000000000	-.00263027	.00263027	-.000000000
39	.01821619	.005410937	.223837210	.008083808	.008084931	.000179545
40	0.000000000	0.000000000	.241260236	0.000000000	0.000000000	0.000000000
41	.005410937	.01821619	.223837209	.008084931	.008083908	.000179545
42	0.000000000	0.000000000	.241260236	0.000000000	0.000000000	0.000000000

MODAL PARTICIPATION FACTOR (X1) = 5.7535386E-01 GEN.WT. TIMES MODAL PART. FACT. (X1) = 6.9053607E+03

MODAL PARTICIPATION FACTOR (X2) = 5.7535386E-01 GEN.WT. TIMES MODAL PART. FACT. (X2) = 6.9053607E+03

MODAL PARTICIPATION FACTOR (X3) = 1.36260d1E-13 GEN.WT. TIMES MODAL PART. FACT. (X3) = 1.6353936E-09

A.2-3

MODE SHAPE (EIGENVECTOR)

MODE NUMBER 3 . FREQUENCY = 62.206745 • GENERALIZED WEIGHT = 240/4.945
 *MAXIMUM ROTATION IS AT NODE 36 *DOF = 5 VALUE = .143189E-01
 *MAXIMUM TRANSLATION IS AT NODE 26 *DOF = 1 VALUE = .100000E+01

***** TRANSLATIONS ***** ***** ROTATIONS (RADIAN) *****

NODE	X1	X2	X3	X4	X5	X6
1	.072289614	-.072289614	.000000000	.000891828	.000891828	.000058258
2	.041262614	-.041262614	.027673468	.000844991	.000844991	.000058258
3	.041790429	-.041790429	.020017846	.000844991	.000844991	.000058258
4	.043170555	-.043170555	.000000000	.000844991	.000844991	.000058258
5	.044550502	-.044550502	.020017846	.000944991	.000844991	.000058258
6	.045074497	-.045074497	.027673468	.000844991	.000844991	.000058258
7	.021967090	-.021967090	.000000000	.000742159	.000742159	.000058258
8	.010404955	-.010404955	.000000000	.000573341	.000573341	.000058258
9	-.003465487	.003465487	.000000000	.000441245	.000441245	.000058258
10	-.003143321	.003143321	.000000000	.000441245	.000441245	.000058258
11	-.001982244	.001982244	.000000000	.000441245	.000441245	.000058258
12	-.014731832	.014731832	.000000000	.000263161	.000263161	.000050837
14	.000221223	-.000221223	.000513331	.000004486	.000000515	.000001242
15	.018491824	-.018491824	-.042869682	-.002389362	-.002503435	-.000003825
16	.019251546	-.019251546	.000000000	-.002503543	-.002503543	-.000018910
17	.017707903	-.017707903	.044869682	-.002389362	-.002503435	-.000032710
18	.000209769	-.000209769	.000513331	.000004486	.000004487	-.000001363
21	.001467334	-.000221223	.000513331	.000000515	.000004486	.000001242
22	.015766551	-.010491824	.043369682	-.002503435	-.002389362	-.000003825
23	.016766551	-.017707903	-.042869682	-.002503435	-.002389362	-.000032710
24	.001457334	-.000209769	.000513331	.000000487	.000004486	-.000001363
26	1.000000000	-1.000000000	.000000000	-.000644736	-.000644736	-.000292862
27	.249427171	-.249427171	.000000000	.013200082	.013200082	.000568551
28	.002480837	-.032939171	-.695623203	.013661100	.013661100	-.000590187
29	.006150573	-.029075455	-.544531439	.013561100	.013661100	-.000590187
30	.017913004	-.017913004	.000000000	.013661100	.013661100	-.000590187
31	.016056619	-.001355708	.378273290	.013660729	.013660915	-.000591075
32	0.060000000	0.000000000	4.07712561	0.000000000	0.000000000	0.000000000
33	.001355708	-.016056219	-.378273290	.013660915	.013660729	-.000591075
34	0.000000000	0.000000000	-.407712561	0.000000000	0.000000000	0.000000000
35	-.176934458	-.176934458	.000000000	.013902355	.013902355	-.000590187
36	-.632013247	.632013247	.000000000	.014318755	.014318755	-.000590187
37	-.012495689	.012495689	.000000000	-.001971594	-.001971694	-.000006530
38	.190279183	-.190279183	.000000000	-.003674015	-.003674015	-.000039025
39	-.001630354	.001630354	.012223621	.000441242	.000441326	.000058794
40	0.000000000	0.000000000	.013174678	0.000000000	0.000000000	0.000000000
41	-.000147339	.000147339	-.012223621	.000441326	.000441242	.000058794
42	0.000000000	0.000000000	-.013174678	0.000000000	0.000000000	0.000000000

MOJAL PARTICIPATION FACTOR (X1) = 4.5676680E-01 GEN.WT. TIMES MOJAL PART. FACT. (X1) = 1.0996636E+04

MOJAL PARTICIPATION FACTOR (X2) = -4.5676680E-01 GEN.WT. TIMES MOJAL PART. FACT. (X2) = -1.0996636E+04

MOJAL PARTICIPATION FACTOR (X3) = 5.0056892E-12 GEN.WT. TIMES MOJAL PART. FACT. (X3) = 1.2051169E-07

A.2-4

A.2-4

MODE SHAPE (EIGENVECTOR)

NODE NUMBER 4 * FREQUENCY = 62.276661 , GENERALIZED WEIGHT = 24178.790

*MAXIMUM ROTATION IS AT NODE 36 *DOF = 4 VALUE = -.145669E-01

*MAXIMUM TRANSLATION IS AT NODE 26 *DOF = 2 VALUE = .100000E+01

***** TRANSLATIONS ***** ***** ROTATIONS (RADIAN) *****

NODE	X1	X2	X3	X4	X5	X6
1	.065815928	.066816928	.000000000	-.000810123	.000810123	.000000000
2	.040295017	.040295017	-.025110559	-.000766735	.000766735	.000000000
3	.040295017	.040295017	.040295017	-.018163943	-.000766735	.000000000
4	.040295017	.040295017	.040295017	.000000000	-.000766735	.000000000
5	.040295017	.040295017	.040295017	.018163943	-.000766735	.000000000
6	.040295017	.040295017	.040295017	.025110559	-.000766735	.000000000
7	.021009645	.021009645	.000000000	-.000671473	.000671473	.000000000
8	.010413456	.010413456	.000000000	-.000514919	.000514919	.000000000
9	-.000907300	-.000907300	-.000907300	-.019465732	-.000392100	.000000000
10	-.000907300	-.000907300	-.000907300	-.015529106	-.000392100	.000000000
11	-.000907300	-.000907300	-.000907300	.000000000	-.000392100	.000000000
12	-.013217307	-.013217307	.000000000	-.000223675	.000223675	.000000000
14	.009210940	.009210940	.001477422	.000512634	-.000004509	.000000505
15	.019224529	.019224529	.019224529	.019224529	.002386144	-.002500063
16	.019384143	.019384143	.019384143	.000000000	.002500172	-.002500172
17	.018224529	.018224529	.018224529	.016882030	.0048803883	-.002386144
18	.000210940	.000210940	.000210940	.001477422	.000512639	-.000004509
21	.001477422	.001477422	.001477422	.000216980	.000512639	-.000004509
22	.016882030	.016882030	.016882030	.016882030	.0048803883	-.002500063
23	.016882030	.016882030	.016882030	.016882030	.0048803883	-.002500063
24	.001477422	.001477422	.001477422	.000216980	.000512639	-.000004509
26	1.000000000	1.000000000	1.000000000	1.000000000	.000000000	.000000000
27	.239251418	.239251418	.239251418	.239251418	.000000000	-.013406696
28	.005459122	.005459122	.005459122	.005459122	.000000000	-.013880227
29	.005459122	.005459122	.005459122	.005459122	.000000000	-.013880227
30	.005459122	.005459122	.005459122	.005459122	.000000000	-.013880227
31	.004803253	.004803253	.004803253	.001453270	.384340890	-.013879851
32	0.000000000	0.000000000	0.000000000	.414252374	0.000000000	0.000000000
33	.001453270	.001453270	.001453270	.004493253	.384340890	-.013879851
34	0.000000000	0.000000000	0.000000000	.414252374	0.000000000	0.000000000
35	-.211728339	-.211728339	-.211728339	-.211728339	.000000000	-.014132896
36	-.65723554	-.65723554	-.65723554	-.65723554	.000000000	-.014566888
37	-.012013893	-.012013893	-.012013893	-.012013893	.000000000	.001968674
38	.100513151	.100513151	.100513151	.100513151	.000000000	.003669686
39	-.000683150	-.000683150	-.000683150	-.000683150	.010859539	-.000392131
40	0.000000000	0.000000000	0.000000000	0.000000000	.011704582	0.000000000
41	-.000202894	-.000202894	-.000202894	-.000202894	.010859539	-.000392131
42	0.000000000	0.000000000	0.000000000	0.000000000	.011704582	0.000000000

MODAL PARTICIPATION FACTOR (X1) = 4.4613880E-01 GEN.WT. TIMES MODAL PART. FACT. (X1) = 1.0787096E+04

MODAL PARTICIPATION FACTOR (X2) = 4.4613880E-01 GEN.WT. TIMES MODAL PART. FACT. (X2) = 1.0787096E+04

MODAL PARTICIPATION FACTOR (X3) = 3.1173005E-14 GEN.WT. TIMES MODAL PART. FACT. (X3) = 7.5374197E-10

A.2-5

MODE SHAPE (EIGENVECTOR)

MODE NUMBER 5 + FREQUENCY = 74.628537 + GENERALIZED WEIGHT = 22900.282
 *MAXIMUM ROTATION IS AT NODE 22 *DOF = 5 VALUE = .312944E-03
 *MAXIMUM TRANSLATION IS AT NODE 36 *DOF = 3 VALUE = .100000E-01

***** TRANSLATIONS ***** ***** ROTATIONS (RADIAN) *****

NODE	X1	X2	X3	X4	X5	X6
1	.000000000	-0.000000000	.482125480	.000000000	-0.000000000	-0.000000000
2	.000000000	-0.000000000	.473826219	.000000000	-0.000000000	-0.000000000
3	.000000000	-0.000000000	.473826219	.000000000	-0.000000000	-0.000000000
4	.000000000	-0.000000000	.473826219	.000000000	-0.000000000	-0.000000000
5	.000000000	-0.000000000	.473826219	.000000000	-0.000000000	-0.000000000
6	.000000000	-0.000000000	.473826219	.000000000	-0.000000000	-0.000000000
7	.000000000	-0.000000000	.467390454	.000000000	-0.000000000	-0.000000000
8	.000000000	-0.000000000	.452243694	.000000000	-0.000000000	-0.000000000
9	.000000000	-0.000000000	.433475588	.000000000	.000000000	-0.000000000
10	.000000000	-0.000000000	.433475588	.000000000	.000000000	-0.000000000
11	.000000000	-0.000000000	.433475588	.000000000	.000000000	-0.000000000
12	.000000000	-0.000000000	.414707481	.000000000	.000000000	-0.000000000
14	-.050000000	.000050735	.001775087	-.000021695	-0.000000000	-0.000000000
15	-.000000000	.000007089	.209752160	-.000312944	.000000000	-0.000000000
16	-.000000000	.000000000	.234627512	.000000000	.000000000	-0.000000000
17	-.030000000	-.000007089	.209752160	.000312944	.000000000	-0.000000000
18	-.000000000	-.000050735	.001775087	.000021695	-0.000000000	.000000000
21	.000050735	.000000000	.001775087	-.000000000	.000021695	-0.000000000
22	.000007089	.000000000	.209752160	.000000000	.000312944	-0.000000000
23	-.000007089	.000000000	.209752160	.000000000	-.000312944	-0.000000000
24	-.0000050735	.000000000	.001775087	-.000000000	.000021695	.000000000
26	-.000000000	.000000000	.669769993	.000000000	.000000000	.000000000
27	-.000000000	.000000000	.951671972	-.000000000	-.000000000	.000000000
28	-.000000000	.000000000	.967490830	-.000000000	-.000000000	.000000000
29	-.000000000	.000000000	.967490830	-.000000000	-.000000000	.000000000
30	-.000000000	.000000000	.967490830	-.000000000	-.000000000	.000000000
31	-.000000000	.000000000	.967490830	-.000000000	-.000000000	.000000000
32	0.000000000	0.000000000	.967490830	0.000000000	0.000000000	0.000000000
33	-.030000000	.000000000	.967490830	-.000000000	-.000000000	.000000000
34	0.000000000	0.000000000	.967490830	0.000000000	0.000000000	0.000000000
35	-.000000000	-.000000000	.983309689	-.000000000	-.000000000	.000000000
36	.000000000	-.000000000	1.000000000	-.000000000	-.000000000	.000000000
37	.000000000	-.000000000	.261948547	.000000000	-.000000000	-.000000000
38	-.600000000	.000000000	.267257574	.000000000	.000000000	-.000000000
39	-.000000000	-.000000000	.433475588	.000000000	.000000000	-.000000000
40	0.000000000	0.000000000	.433475588	0.000000000	0.000000000	0.000000000
41	-.000000000	-.000000000	.433475588	.000000000	-.000000000	-.000000000
42	0.000000000	0.000000000	.433475588	0.000000000	0.000000000	0.000000000

MODAL PARTICIPATION FACTOR (X1) = -1.5341782E-12 GEN.WT. TIMES MODAL PART. FACT. (X1) = -3.5133113E-08

MODAL PARTICIPATION FACTOR (X2) = 1.5134753E-12 GEN.WT. TIMES MODAL PART. FACT. (X2) = 3.4659011E-08

MODAL PARTICIPATION FACTOR (X3) = 1.4833630E+00 GEN.WT. TIMES MODAL PART. FACT. (X3) = 3.3969432E+04

A.2.6

D.6

MODE SHAPE (EIGENVECTOR)

NODE NUMBER 6 , FREQUENCY

98.549172

, GENERALIZED WEIGHT =

25786.370

*MAXIMUM ROTATION IS AT NODE 15 *DOF = 4 VALUE = -.193413E-03

*MAXIMUM TRANSLATION IS AT NODE 1 *DOF = 3 VALUE = .100000E+01

***** TRANSLATIONS *****

***** ROTATIONS (RADIAN) *****

NODE	X1	X2	X3	X4	X5	X6
1	-0.00000000	-0.00000000	1.00000000	-0.00000000	.00000000	.00000000
2	-0.00000000	-0.00000000	.970186429	-0.00000000	.00000000	.00000000
3	-0.00000000	-0.00000000	.970186429	-0.00000000	.00000000	.00000000
4	-0.00000000	-0.00000000	.970186429	-0.00000000	.00000000	.00000000
5	-0.00000000	-0.00000000	.970186429	-0.00000000	.00000000	.00000000
6	-0.00000000	-0.00000000	.970186429	-0.00000000	.00000000	.00000000
7	-0.00000000	-0.00000000	.970186429	-0.00000000	.00000000	.00000000
8	-0.00000000	-0.00000000	.946704944	-0.00000000	.00000000	.00000000
9	-0.00000000	-0.00000000	.892608942	-0.00000000	.00000000	.00000000
10	-0.00000000	-0.00000000	.826175497	-0.00000000	.00000000	.00000000
11	-0.00000000	-0.00000000	.826175497	-0.00000000	.00000000	.00000000
12	-0.00000000	-0.00000000	.826175497	-0.00000000	.00000000	.00000000
14	-0.00000000	-0.00000000	.759742052	-0.00000000	.00000000	.00000000
15	-0.00000000	-0.00000000	.001097080	-0.00013408	-0.00000000	-0.00000000
16	-0.00000000	-0.00000000	.129635882	-0.001193413	-0.00000000	-0.00000000
17	-0.00000000	-0.00000000	.129635882	-0.001193413	-0.00000000	-0.00000000
18	-0.00000000	-0.00000000	.001097080	-0.00013408	-0.00000000	-0.00000000
21	-0.000031356	-0.00000000	.001097080	-0.00000000	-0.00000000	-0.00000000
22	-0.000004381	-0.00000000	.129635882	-0.00000000	.000013408	-0.00000000
23	-0.000004381	-0.00000000	.129635882	-0.00000000	.0001919413	-0.00000000
24	-0.000031356	-0.00000000	.001097080	-0.00000000	-0.001193413	.00000000
26	-0.000000000	-0.00000000	.-291862752	-0.00000000	-0.000013408	.00000000
27	-0.000000000	-0.00000000	.-612782858	-0.00000000	-0.00000000	-0.00000000
28	-0.000000000	-0.00000000	.-631078449	-0.00000000	-0.00000000	-0.00000000
29	-0.000000000	-0.00000000	.-631078449	-0.00000000	.00000000	-0.00000000
30	-0.000000000	-0.00000000	.-631078449	-0.00000000	.00000000	-0.00000000
31	-0.000000000	-0.00000000	.-631078449	-0.00000000	.00000000	-0.00000000
32	0.000000000	0.000000000	.-631078449	0.030000000	0.000000000	-0.000000000
33	-0.000000000	-0.00000000	.-631078449	0.00000000	0.000000000	0.000000000
34	0.000000000	0.000000000	.-631078449	0.00000000	0.000000000	-0.000000000
35	-0.000000000	-0.00000000	.-649374040	0.00000000	0.000000000	-0.000000000
36	-0.000000000	-0.00000000	.-668490320	0.090000000	-0.000000000	-0.000000000
37	-0.000000000	-0.00000000	.-239274700	-0.00000000	-0.000000000	0.000000000
38	-0.000000000	-0.00000000	.-112250118	-0.00000000	-0.000000000	0.000000000
39	-0.000000000	-0.00000000	.-826175497	-0.00000000	-0.000000000	0.000000000
40	0.000000000	0.000000000	.-826175497	0.003000000	0.000000000	0.000000000
41	-0.000000000	-0.00000000	.-826175497	-0.00000000	-0.000000000	0.000000000
42	0.000000000	0.000000000	.-826175497	0.000000000	-0.000000000	0.000000000

MODAL PARTICIPATION FACTOR (X1) = 2.3030032E-13

GEN.WT. TIMES MODAL PART. FACT. (X1) = 5.9387639E-09

MODAL PARTICIPATION FACTOR (X2) = -3.395527E-13

GEN.WT. TIMES MODAL PART. FACT. (X2) = -8.7554334E-09

MODAL PARTICIPATION FACTOR (X3) = 4.6689605E-01

GEN.WT. TIMES MODAL PART. FACT. (X3) = 1.2039570E+04

A.2-7

Appendix A.3
"STATIC" OUTPUT

B E G I N INPUT LOAD CASE NO. 1 TITLE(DEADWEIGHT LOAD CASE

NODAL POINT APPLIED FORCES FOR LOAD CASE NO. 1

NODE	X1	X2	X3	X4	X5	X6
1	-0.	-0.	-5.131000E+03	-0.	-0.	-0.
7	-0.	-0.	-6.104000E+03	-0.	-0.	-0.
8	-0.	-0.	-3.822000E+03	-0.	-0.	-0.
12	-0.	-0.	-9.792000E+03	-0.	-0.	-0.
15	-0.	-0.	-1.225200E+04	-0.	-0.	-0.
25	-0.	-0.	-1.053000E+04	-0.	-0.	-0.
27	-0.	-0.	-7.246000E+03	-0.	-0.	-0.
35	-0.	-0.	-4.007000E+03	-0.	-0.	-0.
36	-0.	-0.	-2.008000E+03	-0.	-0.	-0.

NODAL POINT APPLIED LOADS AND/OR DISPLACEMENTS FINAL SUMMARY FOR LOAD CASE NO. 1

NOTE: IF A FINAL SUMMARY OF APPLIED NODAL LOADS AND GENERATED LOADS IS DESIRED AT THIS POINT,

CODE A 1 IN COLUMN 20 OF THE STATIC CARD.

FORCE AND MOMENT SUMMATION
ABOUT AXES PARALLEL TO SYSTEM AXES
WITH ORIGIN AT POINT (0,0,0)

SUMMATION INCLUDES LOADS APPLIED TO RESTRAINED DOF.

F_{X1} = 0.
F_{X2} = 0.
F_{X3} = -60999000000E+05
M_{X1} = 0.
M_{X2} = 0.
M_{X3} = 0.

DEADWEIGHT LOAD CASE

BEAM ELEMENT LOADS FOR OUTPUT VECTOR 1

BEAM	LOAD-LOCATION.	AXIAL	SHEAR	SHEAR	TORSION	BENDING	BENDING	
NU	NODE--PERCENT.	P	V2	V3	M1	M2	M3	
1	1 JA 0.0	5.13100E+03	-1.28931E-13	1.89514E-11	2.48506E-13	5.54025E-09	-5.38904E-12	PIPEG
1	4 JB 100.0	-5.13100E+03	1.28931E-13	-1.89514E-11	-2.48506E-13	-6.07562E-09	1.74673E-12	
2	3 JA 0.0	1.76572E-11	-2.89821E-11	-6.27414E-13	-4.45581E-13	-1.11372E-11	8.51986E-10	PIPEG
2	2 JH 100.0	-1.76572E-11	2.89821E-11	6.27414E-13	4.45581E-13	1.68216E-11	-1.61394E-09	
3	3 JA 0.0	7.88575E-13	-4.50417E-09	-1.50149E-12	3.78424E-11	1.49954E-10	-8.99911E-08	BEAMG
3	4 JB 100.0	-7.88575E-13	4.50417E-09	1.50149E-12	-3.78424E-11	-1.14384E-10	-3.72764E-08	
4	4 JA 0.0	1.336e0E-10	-1.68749E-09	-3.34743E-12	-1.88365E-11	-7.43143E-12	7.20169E-08	BEAMG
4	5 JB 100.0	-1.336e0E-10	1.68749E-09	3.34743E-12	1.88365E-11	8.67320E-11	-1.01600E-07	
5	5 JA 0.0	5.22584E-11	2.77203E-11	-1.15369E-12	3.54840E-12	-6.60378E-12	2.50833E-11	PIPEG
5	6 JB 100.0	-5.22584E-11	-2.77203E-11	1.15369E-12	-3.54840E-12	1.70612E-11	1.99177E-10	
6	4 JA 0.0	5.13100E+03	3.38327E-11	-1.35543E-10	9.92492E-11	-2.84972E-08	-1.44584E-09	PIPEG
6	7 JB 100.0	-5.13100E+03	-3.38327E-11	1.35543E-10	-9.92492E-11	3.15131E-08	2.19862E-09	
7	7 JA 0.0	1.12390E+04	-2.91581E-11	-1.17768E-10	6.50710E-11	-2.41580E-08	6.53934E-09	PIPEG
7	8 JB 100.0	-1.12390E+04	2.91581E-11	1.17768E-10	-6.50710E-11	2.52909E-08	-6.81984E-09	
8	8 JA 0.0	1.50510E+04	-1.87055E-11	-1.05366E-10	6.39042E-11	-3.44169E-08	-3.92603E-09	PIPEG
8	11 JB 100.0	-1.50510E+04	1.87055E-11	1.05366E-10	-6.39042E-11	3.58921E-08	3.66415E-09	
9	10 JA 0.0	-8.73308E-13	-4.90035E-10	6.41944E-12	3.20748E-10	-4.30168E-11	2.60274E-09	PIPEG
9	9 JB 100.0	0.73303E-13	4.90035E-10	-6.41944E-12	-3.20748E-10	-7.18713E-12	-5.71302E-09	
10	10 JA 0.0	2.29694E-10	4.85248E-09	3.26978E-11	2.57145E-08	-3.04730E-10	-3.08014E-08	BEAMG
10	11 JH 100.0	-2.29694E-10	-4.85248E-09	-3.26978E-11	-2.57145E-08	-6.16865E-10	1.76260E-07	
11	11 JA 0.0	1.50610E+04	-6.93373E-10	1.90322E-09	-2.16727E-09	-1.74384E-07	-6.24087E-08	PIPEG
11	12 JB 100.0	-1.50610E+04	6.93373E-10	-1.90322E-09	2.15727E-09	1.47749E-07	5.27015E-08	
12	12 JA 0.0	2.48530E+04	-6.93331E-10	1.90308E-09	-2.16727E-09	-1.47740E-07	-5.27003E-08	PIPEG
12	37 JB 100.0	-2.48530E+04	6.93331E-10	-1.90308E-09	2.16727E-09	5.92466E-08	2.04604E-08	
13	13 JA 0.0	1.52498E+04	1.36964E+01	5.26039E-11	1.59517E-10	-2.68342E-10	-7.45180E+04	BEAMG
13	14 JB 100.0	-1.52498E+04	-1.36964E+01	-5.26039E-11	-1.59517E-10	2.16628E-12	7.45873E+04	
14	15 JA 0.0	1.36964E+01	1.52498E+04	5.60204E-11	-1.23175E-12	-3.55797E-10	7.02853E+04	BEAMG
14	14 JB 100.0	-1.36964E+01	-1.52498E+04	-5.60204E-11	1.23175E-12	-1.76458E-10	7.45873E+04	
15	15 JA 0.0	1.36964E+01	-1.52498E+04	5.53906E-11	-5.73481E-09	3.57587E-10	7.02853E+04	BEAMG
15	16 JB 100.0	-1.36964E+01	1.52498E+04	-5.53906E-11	5.73481E-09	-1.60388E-09	-4.13405E+05	
16	16 JA 0.0	1.36964E+01	1.52498E+04	-3.76973E-11	9.13642E-10	9.10178E-10	4.13405E+05	BEAMG
16	17 JB 100.0	-1.36964E+01	-1.52498E+04	3.76973E-11	-9.13642E-10	-6.19881E-11	-7.02853E+04	
17	17 JA 0.0	1.36964E+01	1.52498E+04	-3.70139E-11	1.44107E-12	6.74558E-11	7.02853E+04	BEAMG
17	18 JB 100.0	-1.36964E+01	-1.52498E+04	3.70139E-11	-1.44107E-12	2.84176E-10	7.45873E+04	
18	19 JA 0.0	1.52498E+04	1.36964E+01	-3.36395E-11	-2.66985E-10	1.72267E-10	-7.45180E+04	BEAMG
18	18 JB 100.0	-1.52498E+04	-1.36964E+01	3.36395E-11	2.66985E-10	-2.05115E-12	7.45873E+04	
19	20 JA 0.0	1.52498E+04	1.36964E+01	-4.75815E-11	-3.36300E-10	2.46840E-10	-7.45180E+04	BEAMG
19	21 JB 100.0	-1.52498E+04	-1.36964E+01	4.75815E-11	3.36300E-10	-6.07742E-12	7.45873E+04	

A.3-2

17	17 JA	0.0	1.35964E+01	1.52498E+04	-3.70139E-11	-4.4107E-12	6.74558E-11	7.02853E+04	BEAMG
18	18 JB	100.0	-1.35964E+01	-1.52498E+04	3.70139E-11	1.44107E-12	2.84176E-10	7.45873E+04	
19	19 JA	0.0	1.35964E+01	1.52498E+04	-3.26385E-11	-2.66985E-12	1.72247E-11	-1.5141E-12	EE249
19	19 JB	100.0	-1.35964E+01	-1.52498E+04	3.26385E-11	2.66985E-12	-2.13155E-12	7.45873E-14	
20	20 JA	0.0	1.52498E+04	1.36704E+01	-4.75815E-11	-3.36300E-10	2.46840E-10	-7.45180E+04	BEAMG
20	20 JB	100.0	-1.52498E+04	-1.36704E+01	4.75815E-11	3.36300E-10	-6.07742E-12	7.45873E+04	
21	21 JA	0.0	1.35964E+01	1.52498E+04	-4.75177E-11	-6.08723E-12	1.15236E-10	7.02853E+04	BEAMG
21	21 JB	100.0	-1.35964E+01	-1.52498E+04	4.75177E-11	6.08723E-12	3.36181E-10	7.45873E+04	
21	22 JA	0.0	1.35964E+01	1.52498E+04	-5.83530E-11	-1.36168E-08	-1.47818E-12	7.02853E+04	BEAMG
21	22 JB	100.0	-1.35964E+01	-1.52498E+04	5.83530E-11	1.36168E-08	1.31442E-09	-4.13405E+05	
22	23 JA	0.0	1.36964E+01	1.52498E+04	-7.62975E-11	1.35574E-08	-2.01427E-09	4.13405E+05	BEAMG
22	23 JB	100.0	-1.36964E+01	-1.52498E+04	-7.62975E-11	-1.35574E-08	2.97576E-10	-7.02853E+04	
23	23 JA	0.0	1.36964E+01	1.52498E+04	6.65137E-11	-6.08430E-12	-4.03451E-10	7.02853E+04	BEAMG
23	24 JB	100.0	-1.36964E+01	-1.52498E+04	-6.65137E-11	6.08430E-12	-2.28429E-10	7.45873E+04	
24	25 JA	0.0	1.52498E+04	1.36964E+01	-6.65746E-11	2.28672E-10	-3.42942E-10	-7.45180E+04	BEAMG
24	25 JB	100.0	-1.52498E+04	-1.36964E+01	6.65746E-11	-2.28672E-10	6.07471E-12	7.45873E+04	
25	26 JA	0.0	-2.38940E+04	-3.82921E-11	9.72702E-10	-7.83951E-10	-2.70188E-08	-4.35391E-10	PIPEG
25	26 JB	100.0	2.38940E+04	3.82921E-11	-9.72702E-10	7.83951E-10	-3.93097E-08	-2.17575E-09	
25	26 JA	0.0	-1.33010E+04	-2.08608E-11	8.60882E-10	-7.31060E-10	3.97086E-08	2.10303E-09	PIPEG
25	27 JB	100.0	1.33010E+04	2.08608E-11	-8.60882E-10	7.31060E-10	-1.03466E-07	-3.64946E-09	
27	27 JA	0.0	-6.01500E+03	-2.38353E-11	8.75131E-10	-7.24234E-10	9.44396E-08	6.71194E-10	PIPEG
27	28 JB	100.0	6.01500E+03	2.38353E-11	-8.75131E-10	7.24234E-10	-1.06691E-07	-1.00448E-09	
28	29 JA	0.0	-4.41245E-11	-1.37356E-09	4.69226E-12	-1.43461E-09	-2.25073E-11	2.27471E-10	PIPEG
28	29 JB	100.0	4.41245E-11	1.37356E-09	-4.69226E-12	1.43461E-09	-1.41891E-11	-1.01635E-08	
29	29 JA	0.0	-4.57620E-11	-5.31974E-09	-8.21542E-13	8.10107E-08	-7.41878E-11	-5.53148E-08	BEAMG
29	30 JB	100.0	4.57620E-11	5.31974E-09	8.21542E-13	-8.10107E-08	9.73432E-11	-1.04694E-07	
30	30 JA	0.0	-3.39218E-10	-8.31367E-09	3.37374E-10	-6.41139E-08	-1.01870E-08	7.90805E-10	BEAMG
30	31 JB	100.0	3.39218E-10	8.31367E-09	-3.37374E-10	6.41139E-08	8.45146E-10	-2.55046E-07	
31	31 JA	0.0	-2.35308E-10	-1.30907E-10	3.32754E-10	5.22773E-11	-5.00391E-10	-2.61934E-10	BEAMG
31	32 JB	100.0	2.35308E-10	1.30907E-10	-3.32754E-10	-5.22773E-11	-9.33780E-10	-2.61934E-10	
32	30 JA	0.0	5.70242E-10	-1.78759E-08	-3.29406E-10	1.47724E-08	9.33927E-09	-1.98307E-07	BEAMG
32	33 JB	100.0	-5.70242E-10	1.78759E-08	3.29406E-10	-1.47724E-08	-2.18008E-10	-2.70241E-07	
33	33 JA	0.0	6.01510E-10	0.	-3.06775E-10	-2.02473E-12	8.42080E-10	-5.82077E-11	BEAMG
33	34 JB	100.0	-6.01510E-10	0.	3.06775E-10	-2.02473E-12	4.80121E-10	2.91038E-11	
34	30 JA	0.0	-6.01500E+03	-2.89513E-24	1.72054E-22	0.	-6.77626E-21	0.	PIPEG
34	35 JB	100.0	6.01500E+03	2.89513E-24	-1.72054E-22	0.	1.35525E-20	-2.11758E-22	
35	35 JA	0.0	-2.00800E+03	-1.65436E-24	7.94093E-23	2.64698E-23	-8.47033E-22	5.29396E-23	PIPEG
35	36 JB	100.0	2.00800E+03	1.65436E-24	-7.94093E-23	-2.64698E-23	0.	-5.29396E-23	
36	37 JA	0.0	2.48530E+04	-7.13971E-10	1.91679E-09	-2.16605E-09	-5.63757E-08	-1.32578E-08	PIPEG
36	36 JB	100.0	-2.48530E+04	7.13971E-10	-1.91679E-09	2.16606E-09	2.41353E-09	1.24881E-09	
37	16 JA	0.0	-2.38940E+04	-3.31750E-11	1.00646E-09	-7.73171E-10	-3.86366E-08	-9.50976E-10	PIPEG
37	32 JB	100.0	2.38940E+04	3.31750E-11	-1.00646E-09	7.73171E-10	2.73844E-08	5.80079E-10	
38	11 JA	0.0	2.91038E-10	-2.93091E-09	-1.16803E-09	-7.65184E-08	3.09821E-08	-4.62259E-08	BEAMG
38	39 JB	100.0	-2.91038E-10	2.93091E-09	1.16803E-09	7.65184E-08	1.36342E-09	-1.77458E-08	
39	39 JA	0.0	1.32153E-10	-8.73115E-11	-1.07821E-09	5.21648E-11	2.00019E-09	-2.32831E-10	BEAMG
39	40 JB	100.0	-1.32153E-10	8.73115E-11	1.07821E-09	-5.21648E-11	2.64689E-09	-2.03727E-10	
40	11 JA	0.0	-5.31323E-10	-9.08657E-09	9.91317E-10	-2.73397E-08	-2.94610E-08	-1.50118E-08	BEAMG
40	41 JB	100.0	9.31323E-10	9.08657E-09	-9.91317E-10	2.73397E-08	2.00866E-09	-2.14843E-07	
41	41 JA	0.0	-1.16473E-09	2.91038E-11	9.47173E-10	-1.67321E-11	-2.26558E-09	0.	BEAMG

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39	JA	0.0	-1.6719E-10	-2.8301E-09	1.16803E-09	-1.0044E-08	1.35342E-09	-1.1253E-08
40	JB	100.0	-1.32153E-10	-8.73115E-11	1.07041E-09	-1.71690E-11	-2.04669E-09	-2.03727E-10
40	11 JA	0.0	-9.31323E-10	-9.08657E-09	-9.91317E-10	-2.73897E-08	-2.94610E-08	-1.50118E-08
40	41 JB	100.0	9.31323E-10	9.08657E-09	-9.91317E-10	2.73897E-08	2.00896E-09	-2.14843E-07
41	41 JA	0.0	-1.10473E-09	2.91038E-11	9.47173E-10	-1.67321E-11	-2.25558E-09	0.
41	42 JB	100.0	1.10473E-09	-2.91038E-11	-9.47173E-10	1.67321E-11	-1.82674E-09	5.82077E-11

DEAD-EIGHT LOAD CASE

MAXIMUM LOAD SUMMARY FOR

AXIAL P	HEAM ELEMENT			LOADS			FOR OUTPUT VECTOR 1
	SHEAR V2	SHEAR V3	TORSION M1	BENDING M2	BENDING M3		

MAXIMUM BEAM LOADS = 2.38440E+04 1.52498E+04 1.91679E-09 8.10107E-08 1.47739E-07 4.13405E+05
 BEAM NOS. = 37. 10. 36. 29. 11. 16.

MINIMUM BEAM LOADS = -2.48530E+04 -1.52498E+04 -1.91679E-09 -8.10107E-08 -1.74384E-07 -4.13405E+05
 BEAM NOS. = 36. 10. 36. 29. 11. 15.

DEAWEIGHT LOAD CASE

BEAM	--NODES--	B E A M			E N D			L U O A D S			IN GLOBAL SYSTEM			FOR OUTPUT VECTOR		
		FX1	FX2	FX3	MX1	MX2	MX3	1	2	3	4	5	6	7	8	
1	JA 1	-.129E-12	-.190E-10	-.513E+04	.554E-08	.539E-11	-.249E-12									
	JB 4	.129E-12	.190E-10	.513E+04	-.608E-08	-.175E-11	.249E-12									
2	JA 3	-.52E-12	.177E-10	.290E-10	-.352E-09	-.446E-12	.111E-10									
	JB 2	-.527E-12	-.177E-10	-.290E-10	.161E-08	.446E-12	-.168E-10									
3	JA 3	-.150E-11	-.789E-12	.450E-08	-.900E-07	-.378E-10	-.150E-09									
	JB 4	.150E-11	.789E-12	.450E-08	-.378E-07	.378E-10	.114E-09									
4	JA 4	-.335E-11	-.134E-09	.164E-08	-.720E-07	-.189E-10	.743E-11									
	JB 5	.335E-11	.134E-09	-.164E-08	-.102E-06	-.189E-10	-.867E-10									
5	JA 5	-.115E-11	-.523E-10	-.277E-10	.251E-10	-.355E-11	.661E-11									
	JB 6	.115E-11	.523E-10	.277E-10	-.198E-09	.355E-11	-.171E-10									
6	JA 4	.33dE-10	.136E-09	-.513E+04	-.285E-07	.145E-08	-.992E-10									
	JB 7	-.33dE-10	-.136E-09	.513E+04	.315E-07	-.220E-08	.992E-10									
7	JA 7	-.292E-10	.118E-09	-.112E+05	-.242E-07	.654E-08	-.651E-10									
	JB 8	.292E-10	-.118E-09	.112E+05	.253E-07	.682E-08	.651E-10									
8	JA 8	-.187E-10	.105E-09	-.151E+05	-.344E-07	.393E-08	-.639E-10									
	JB 11	.187E-10	-.105E-09	.151E+05	.359E-07	-.366E-08	.639E-10									
9	JA 10	-.516E-11	.392E-11	.490E-09	-.161E-08	.207E-08	.430E-10									
	JB 9	.516E-11	-.392E-11	-.490E-09	.381E-08	-.427E-08	.719E-11									
10	JA 10	-.139E-09	-.105E-09	-.485E-08	-.400E-07	.360E-08	-.305E-09									
	JB 11	.139E-09	.105E-09	.485E-08	.143E-06	-.106E-06	.617E-09									
11	JA 11	-.693E-09	-.190E-08	-.151E+05	-.174E-06	.624E-07	.217E-08									
	JB 12	.693E-09	.190E-08	.151E+05	.148E-06	-.527E-07	-.217E-08									
12	JA 12	-.693E-09	-.190E-08	-.249E+05	-.148E-06	.527E-07	.217E-08									
	JB 37	.693E-09	.190E-08	.249E+05	.592E-07	-.205E-07	-.217E-08									
13	JA 13	.520E-10	-.137E+02	.152E+05	-.745E+05	.268E-09	.160E-09									
	JB 14	-.520E-10	.137E+02	-.152E+05	.746E+05	-.217E-11	-.160E-09									
14	JA 15	-.560E-10	-.137E+02	-.152E+05	-.703E+05	.123E-11	.356E-09									
	JB 14	.560E-10	-.137E+02	.152E+05	.740E+05	.123E-11	.176E-09									
15	JA 15	.554E-10	-.137E+02	.152E+05	.703E+05	.573E-08	-.358E-09									
	JB 15	-.554E-10	.137E+02	-.152E+05	-.703E+06	-.573E-08	.160E-08									
16	JA 16	-.317E-10	-.137E+02	-.152E+05	-.419E+06	-.914E-09	-.910E-09									
	JB 17	.317E-10	.137E+02	.152E+05	.703E+05	.914E-09	.620E-10									
17	JA 17	-.370E-10	-.137E+02	-.152E+05	.703E+05	-.144E-11	-.675E-10									
	JB 18	.370E-10	.137E+02	.152E+05	.740E+05	.144E-11	-.284E-09									
18	JA 19	-.335E-10	-.137E+02	-.152E+05	.740E+05	.172E-09	-.267E-09									
	JB 19	.335E-10	-.137E+02	-.152E+05	-.740E+05	-.205E-11	.267E-09									
19	JA 20	-.137E+02	.476E-10	.152E+05	-.247E-09	.745E+05	-.336E-09									
	JB 21	.137E+02	-.476E-10	-.152E+05	.608E-11	-.746E+05	.316E-09									
20	JA 22	.137E+02	-.476E-10	-.152E+05	.609E-11	.703E+05	-.115E-09									

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	JA 14	-1.170E-10	-1.170E-02	-1.152E+05	-1.152E+05	-1.144E-11	-1.675E-10
	JA 15	-1.130E-10	-1.130E-02	-1.152E+05	-1.152E+05	-1.172E-09	-2.267E-09
	JA 16	-1.130E-10	-1.130E-02	-1.152E+05	-1.152E+05	-1.205E-11	-2.267E-09
19	JA 20	-1.137E+02	-1.137E-10	-1.152E+05	-1.247E-09	-1.745E+05	-1.336E-09
	JB 21	.137E+02	-1.137E-10	-1.152E+05	.508E-11	-1.746E+05	.334E-09
20	JA 22	-1.137E+02	-1.137E-10	-1.152E+05	.509E-11	.703E+05	-1.115E-09
	JB 23	-1.137E+02	-1.137E-10	-1.152E+05	-1.509E-11	.746E+05	-1.334E-09
21	JA 22	-1.137E+02	.534E-10	-1.152E+05	.136E-07	-1.703E+05	.148E-11
	JB 16	-1.137E+02	-1.137E-10	-1.152E+05	-1.136E-07	.413E+06	-1.131E-08
22	JA 15	-1.137E+02	-1.703E-10	-1.152E+05	-1.135E-07	-1.413E+06	.201E-08
	JB 23	.137E+02	-1.703E-10	-1.152E+05	.135E-07	.703E+05	-2.294E-09
23	JA 23	-1.137E+02	-1.608E-10	-1.152E+05	.608E-11	-1.703E+05	.403E-09
	JB 24	.137E+02	.608E-10	-1.152E+05	-1.608E-11	-1.746E+05	.228E-09
24	JA 25	-1.137E+02	.606E-10	-1.152E+05	-1.493E-09	-1.745E+05	.229E-09
	JB 24	-1.137E+02	-1.606E-10	-1.152E+05	.607E-11	-1.746E+05	-1.229E-09
25	JA 38	-1.383E-10	-1.913E-09	.239E+05	-1.270E-07	.435E-09	.714E-09
	JB 26	.383E-10	.913E-09	.239E+05	-1.913E-07	.218E-08	-1.784E-09
26	JA 26	-1.209E-10	-1.801E-09	.133E+05	.391E-07	-1.210E-08	.731E-09
	JB 27	.209E-10	.801E-09	.133E+05	-1.103E-06	.365E-08	-1.731E-09
27	JA 27	-1.238E-10	-1.875E-09	.601E+04	.944E-07	-1.671E-09	.724E-09
	JB 30	.238E-10	.875E-09	.601E+04	-1.107E-06	.100E-08	-1.724E-09
28	JA 29	-1.279E-10	.345E-10	.137E-08	-1.856E-09	.114E-08	.225E-10
	JB 28	.279E-10	-1.345E-10	.137E-08	.617E-08	-1.920E-08	.142E-10
29	JA 29	.1330E-10	-1.345E-10	.532E-08	-1.102E-07	.964E-07	.742E-10
	JB 30	-1.330E-10	.345E-10	-1.532E-08	.131E-06	.167E-07	-1.973E-10
30	JA 30	-1.339E-09	-1.337E-09	.831E-08	.641E-07	-1.791E-09	.102E-07
	JB 31	.339E-09	.337E-09	.331E-08	-1.641E-07	.255E-06	-1.845E-09
31	JA 31	.285E-09	-1.333E-09	.131E-09	-1.523E-10	.262E-09	.500E-09
	JB 32	-1.285E-09	.333E-09	-1.131E-09	.523E-10	.262E-09	.934E-09
32	JA 30	-1.329E-09	-1.570E-09	.179E-07	-1.198E-06	-1.148E-07	-1.934E-08
	JB 33	.329E-09	.570E-09	-1.179E-07	-1.270E-06	.148E-07	.218E-09
33	JA 33	-1.307E-09	-1.602E-09	0.	-1.542E-10	.202E-11	-1.842E-09
	JB 34	.307E-09	.602E-09	0.	.241E-10	-1.202E-11	-1.480E-09
34	JA 30	-1.290E-23	-1.172E-21	.601E+04	-1.678E-20	0.	0.
	JB 35	.290E-23	.172E-21	-1.001E+04	.196E-19	.212E-21	0.
35	JA 35	-1.165E-23	-1.194E-22	.201E+04	-1.847E-21	-1.529E-22	-1.265E-22
	JB 35	.165E-23	.194E-22	-1.201E+04	0.	.529E-22	.265E-22
36	JA 37	-1.714E-09	-1.122E-08	-1.249E+05	-1.264E-07	.133E-07	.217E-08
	JB 16	.714E-09	.122E-08	.249E+05	.241E-07	-1.255E-08	-1.217E-08
37	JA 16	-1.332E-10	-1.101E-08	.239E+05	-1.386E-07	.951E-09	.773E-09
	JB 33	.332E-10	.101E-08	-1.239E+05	.274E-07	-1.580E-09	-1.73E-09
38	JA 11	-1.252E-09	.117E-08	-1.293E+04	-1.761E-07	.462E-07	-1.320E-07
	JB 39	.252E-09	-1.17E-08	.293E+04	-1.765E-07	.177E-07	-1.341E-09
39	JA 39	-1.132E-09	.103E-08	.873E-10	-1.522E-10	.233E-09	.200E-08
	JB 40	.132E-09	-1.03E-08	-1.873E-10	-1.522E-10	.204E-09	-1.265E-08
40	JA 11	.441E-09	.105E-08	.907E-04	-1.150E-07	.278E-07	.291E-07
	JB 41	-1.441E-09	-1.05E-08	-1.907E-04	-1.215E-06	-1.274E-07	-1.164E-08
41	JA 41	.947E-09	.110E-08	-1.291E-10	0.	.167E-10	.226E-08
	JB 42	-1.947E-09	-1.10E-08	.291E-10	.582E-10	-1.167E-10	.183E-08

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JA	11	.001E-09	.100E-08	-.200E-08	-.150E-07	.200E-07	.200E-08
JH	41	-.941E-09	-.100E-08	-.100E-08	-.215E-06	-.274E-07	-.164E-08
JA	41	.941E-09	.110E-08	-.291E-10	0.	.167E-10	.226E-08
JH	42	-.941E-09	-.110E-08	-.291E-10	.582E-10	-.167E-10	-.1d3E-08

DEADWEIGHT LOAD CASE

		BEAM		STRESSSES		FOR OUTPUT VECTOR					
BEAM	---	TRANSVERSE	TORSIONAL	- STRESSES AT USER LOCATIONS -	MAXIMUM	MINIMUM	COMBINED				
LOAD-LOCATION	SHEAR	SHEAR	(F/C/J)	A	B	C	(P/A+MC/I)	(P/A-MC/I)	SHEAR		
NU	NODE--PERCENT.	(V2/K3%A)	(V3/K2%A)								
1	1 JA	0.0	-1.44E-15	2.12E-13	-6.48E-17	-2.872E+01	-2.872E+01	-2.8716E+01	-2.8716E+01	1.44E+01 PIPEG	
1	4 JH	100.0	-1.44E-15	2.12E-13	-6.48E-17	-2.872E+01	-2.872E+01	-2.8716E+01	-2.8716E+01	1.44E+01	
2	3 JA	0.0	-4.50E-12	-9.74E-14	5.72E-15	-1.372E-12	2.049E-11	-1.086E-12	2.0491E-11	-2.3235E-11	1.02E-11 PIPEG
2	2 JH	100.0	-4.50E-12	-9.74E-14	5.72E-15	-1.372E-12	4.004E-11	-9.405E-13	4.0043E-11	-4.2787E-11	2.00E-11
3	3 JA	0.0	-9.01E-12	-3.00E-15	-9.46E-17	-1.577E-15	-2.266E-13	-1.952E-15	2.2378E-13	-2.2693E-13	1.12E-13 BEAMG
3	4 JH	100.0	-9.01E-12	-3.00E-15	-9.46E-17	-1.577E-15	-9.161E-14	-1.863E-15	-9.1899E-14	-9.5054E-14	4.59E-14
4	4 JA	0.0	-3.37E-12	-5.69E-15	4.72E-17	-2.674E-13	-8.732E-14	-2.673E-13	-8.7300E-14	-4.4742E-13	4.37E-14 BEAMG
4	5 JH	100.0	-3.37E-12	-5.69E-15	4.72E-17	-2.674E-13	-1.336E-14	-2.671E-13	-1.3144E-14	-5.2158E-13	6.57E-15
5	5 JA	0.0	4.30E-12	-1.79E-13	-4.55E-14	-4.059E-12	-3.415E-12	-3.889E-12	-3.3930E-12	-4.7241E-12	1.70E-12 PIPEG
5	6 JH	100.0	4.30E-12	-1.79E-13	-4.55E-14	-4.059E-12	-9.144E-12	-3.921E-12	-1.0452E-12	-9.1624E-12	5.25E-13
6	4 JA	0.0	3.78E-13	-1.52E-12	-2.51E-14	-2.872E+01	-2.872E+01	-2.8716E+01	-2.8716E+01	1.44E+01 PIPEG	
6	7 JH	100.0	3.78E-13	-1.52E-12	-2.51E-14	-2.872E+01	-2.872E+01	-2.8716E+01	-2.8716E+01	1.44E+01	
7	7 JA	0.0	-8.34E-13	-3.37E-12	-4.23E-14	-1.608E+02	-1.608E+02	-1.608E+02	-1.6079E+02	-1.6079E+02	8.04E+01 PIPEG
7	8 JH	100.0	-8.34E-13	-3.37E-12	-4.23E-14	-1.608E+02	-1.608E+02	-1.608E+02	-1.6079E+02	-1.6079E+02	8.04E+01
8	8 JA	0.0	-3.44E-13	-1.94E-12	-2.15E-14	-1.385E+02	-1.385E+02	-1.385E+02	-1.3852E+02	-1.3852E+02	6.93E+01 PIPEG
8	11 JH	100.0	-3.44E-13	-1.94E-12	-2.15E-14	-1.385E+02	-1.385E+02	-1.385E+02	-1.3852E+02	-1.3852E+02	6.93E+01
9	10 JA	0.0	-4.02E-11	5.2/E-13	-1.75E-12	3.587E-14	2.848E-11	5.060E-13	2.8487E-11	-2.8415E-11	1.44E-11 PIPEG
9	10 JH	100.0	-4.02E-11	5.27E-13	-1.75E-12	3.587E-14	6.248E-11	-4.269E-14	6.2478E-11	-6.2407E-11	3.13E-11
10	10 JA	0.0	9.70E-12	6.5/E-14	-6.43E-14	-4.594E-13	-5.364E-13	-4.586E-13	-3.8162E-13	-5.3715E-13	2.01E-13 BEAMG
10	11 JH	100.0	9.70E-12	6.54E-14	-6.43E-14	-4.594E-13	-9.000E-13	-4.609E-13	-1.7196E-14	-9.0158E-13	6.49E-14
11	11 JA	0.0	-1.20E-11	3.50E-11	7.2HE-13	-1.385E+02	-1.385E+02	-1.385E+02	-1.3852E+02	-1.3852E+02	6.93E+01 PIPEG
11	12 JH	100.0	-1.20E-11	3.50E-11	7.29E-13	-1.385E+02	-1.385E+02	-1.385E+02	-1.3852E+02	-1.3852E+02	6.93E+01
12	12 JA	0.0	-1.70E-11	5.44E-11	1.41E-12	-3.555E+02	-3.555E+02	-3.555E+02	-3.5555E+02	-3.5555E+02	1.78E+02 PIPEG
12	37 JH	100.0	-1.70E-11	5.44E-11	1.41E-12	-3.555E+02	-3.555E+02	-3.555E+02	-3.5555E+02	-3.5555E+02	1.78E+02
13	13 JA	0.0	2.7/E-02	1.00E-13	-3.99E-16	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01 BEAMG
13	14 JH	100.0	2.7/E-02	1.00E-13	-3.99E-16	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01
14	15 JA	0.0	4.45E+02	1.63E-12	1.47E-13	-3.994E-01	4.318E+02	-3.994E-01	4.3181E+02	-4.3261E+02	2.16E+02 BEAMG
14	14 JH	100.0	4.45E+02	1.63E-12	1.47E-13	-3.994E-01	-4.591E+02	-3.994E-01	4.5826E+02	-4.5906E+02	2.29E+02
15	15 JA	0.0	-3.05E+01	1.11E-13	1.43E-14	-2.739E-02	1.483E-01	-2.739E-02	1.4832E-01	-2.0311E-01	7.42E-02 BEAMG
15	15 JH	100.0	-3.05E+01	1.11E-13	1.43E-14	-2.739E-02	1.006E+00	-2.739E-02	1.0061E+00	-1.0604E+00	5.03E-01
16	16 JA	0.0	3.05E+01	-7.54E-14	-2.28E-15	2.739E-02	1.006E+00	-2.739E-02	1.0061E+00	-1.0604E+00	5.03E-01 BEAMG
16	17 JH	100.0	3.05E+01	-7.54E-14	-2.28E-15	2.739E-02	1.483E-01	-2.739E-02	1.4832E-01	-2.0311E-01	7.42E-02
17	17 JA	0.0	4.45E+02	-1.03E-12	1.72E-13	-3.994E-01	4.318E+02	-3.994E-01	4.3181E+02	-4.3261E+02	2.16E+02 BEAMG
17	18 JH	100.0	4.45E+02	-1.03E-12	1.72E-13	-3.994E-01	-4.591E+02	-3.994E-01	4.5826E+02	-4.5906E+02	2.29E+02
18	19 JA	0.0	2.7/E-02	-6.73E-14	6.67E-16	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01 BEAMG
18	18 JH	100.0	2.7/E-02	-6.73E-14	6.67E-16	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01
19	20 JA	0.0	2.7/E-02	-9.52E-14	8.41E-15	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01 BEAMG
19	21 JH	100.0	2.7/E-02	-9.52E-14	8.41E-16	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01

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17	JA	0.0	4.45E+02	-1.05E-12	-1.72E-13	-3.994E-01	4.31H1E+02	-3.994E-01	4.31H1E+02	-4.3261E+02	2.16E+02	BEAMG	
18	JB	100.0	4.45E+02	-1.05E-12	-1.72E-13	-3.994E-01	4.591E+02	-3.994E-01	4.5926E+02	-4.5905E+02	2.29E+02		
19	JA	0.0	2.74E-02	-6.73E-14	6.67E-16	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01	BEAMG	
18	JB	100.0	2.74E-02	-6.73E-14	6.67E-16	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01		
19	20	JA	0.0	2.74E-02	-9.52E-14	8.41E-15	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01	BEAMG
21	JB	100.0	2.74E-02	-9.52E-14	8.41E-15	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01		
20	22	JA	0.0	4.45E+02	-1.34E-12	-7.28E-13	-3.994E-01	4.31H1E+02	-3.994E-01	4.31H1E+02	-4.3261E+02	2.16E+02	BEAMG
21	JB	100.0	4.45E+02	-1.34E-12	-7.28E-13	-3.994E-01	4.591E+02	-3.994E-01	4.5926E+02	-4.5905E+02	2.29E+02		
21	22	JA	0.0	-3.05E+01	-1.17E-13	3.40E-14	-2.739E-02	1.483E-01	-2.739E-02	1.4832E-01	-2.0311E-01	7.42E-02	BEAMG
16	JB	100.0	-3.05E+01	-1.17E-13	3.40E-14	-2.739E-02	1.006E+00	-2.739E-02	1.0061E+00	-1.0609E+00	5.03E-01		
22	16	JA	0.0	3.05E+01	1.53E-13	-3.39E-14	-2.739E-02	1.006E+00	-2.739E-02	1.0061E+00	-1.0609E+00	5.03E-01	BEAMG
22	23	JB	100.0	3.05E+01	1.53E-13	-3.39E-14	-2.739E-02	1.483E-01	-2.739E-02	1.4832E-01	-2.0311E-01	7.42E-02	
23	23	JA	0.0	4.45E+02	1.94E-12	7.27E-13	-3.994E-01	4.318E+02	-3.994E-01	4.3181E+02	-4.3261E+02	2.16E+02	BEAMG
24	JB	100.0	4.45E+02	1.94E-12	7.27E-13	-3.994E-01	4.591E+02	-3.994E-01	4.5926E+02	-4.5905E+02	2.29E+02		
24	25	JA	0.0	2.74E-02	1.33E-13	-5.72E-16	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01	BEAMG
24	JB	100.0	2.74E-02	1.33E-13	-5.72E-16	-3.050E+01	-3.069E+01	-3.050E+01	-3.0313E+01	-3.0686E+01	1.52E+01		
25	38	JA	0.0	-1.10E-12	2.78E-11	5.10E-13	3.418E+02	3.418E+02	3.418E+02	3.4183E+02	3.4183E+02	1.71E+02	PIPEG
25	JB	100.0	-1.10E-12	2.78E-11	5.10E-13	3.418E+02	3.418E+02	3.418E+02	3.4183E+02	3.4183E+02	1.71E+02		
26	26	JA	0.0	-5.97E-13	2.40E-11	4.75E-13	1.903E+02	1.903E+02	1.903E+02	1.9028E+02	1.9028E+02	9.51E+01	PIPEG
26	JB	100.0	-5.97E-13	2.40E-11	4.75E-13	1.903E+02	1.903E+02	1.903E+02	1.9028E+02	1.9028E+02	9.51E+01		
27	27	JA	0.0	-4.38E-13	1.61E-11	2.3E-13	5.532E+01	5.532E+01	5.532E+01	5.5321E+01	5.5321E+01	2.77E+01	PIPEG
27	JB	100.0	-4.38E-13	1.61E-11	2.3E-13	5.532E+01	5.532E+01	5.532E+01	5.5321E+01	5.5321E+01	2.77E+01		
28	29	JA	0.0	-1.13E-10	3.8E-13	7.06E-12	1.812E-12	4.299E-12	2.058E-12	4.3107E-12	-6.8607E-13	8.15E-12	PIPEG
28	JB	100.0	-1.13E-10	3.8E-13	7.06E-12	1.812E-12	1.129E-10	1.657E-12	1.1290E-10	-1.0927E-10	5.70E-11		
29	29	JA	0.0	-1.06E-11	-1.64E-15	-2.03E-13	9.352E-14	-4.476E-14	9.371E-14	2.3200E-13	-4.4949E-14	2.33E-13	BEAMG
29	JB	100.0	-1.06E-11	-1.64E-15	-2.03E-13	9.352E-14	3.559E-13	9.377E-14	3.5590E-13	-1.646E-13	2.69E-13		
30	30	JA	0.0	-1.66E-11	6.79E-13	1.60E-13	6.784E-13	6.804E-13	7.039E-13	7.0588E-13	6.5099E-13	3.88E-13	BEAMG
30	JB	100.0	-1.66E-11	6.79E-13	1.60E-13	6.784E-13	1.316E-12	6.805E-13	1.3183E-12	3.8608E-14	6.78E-13		
31	31	JA	0.0	-1.46E-11	3.70E-11	-2.32E-11	3.17E-11	-1.830E-09	3.257E-11	1.8947E-09	-1.8313E-09	9.48E-10	BEAMG
31	JB	100.0	-1.46E-11	3.70E-11	-2.32E-11	3.17E-11	-1.830E-09	3.008E-11	1.8954E-09	-1.8320E-09	9.48E-10		
32	30	JA	0.0	-3.56E-11	-6.57E-13	-3.09E-14	-1.140E-12	-1.636E-12	-1.164E-12	-6.2137E-13	-1.6596E-12	3.13E-13	BEAMG
32	JB	100.0	-3.56E-11	-6.57E-13	-3.09E-14	-1.140E-12	-4.649E-13	-1.141E-12	-4.6424E-13	-1.8167E-12	2.35E-13		
33	33	JA	0.0	0.	-3.41E-11	9.00E-13	-6.683E-11	-4.906E-10	-6.830E-11	3.4843E-10	-4.8209E-10	1.74E-10	BEAMG
33	JB	100.0	0.	-3.41E-11	9.00E-13	-6.683E-11	-2.737E-10	-6.600E-11	1.4090E-10	-2.7457E-10	7.05E-11		
34	30	JA	0.0	-5.32E-26	3.10E-24	0.	5.532E+01	5.532E+01	5.532E+01	5.5321E+01	5.5321E+01	2.77E+01	PIPEG
34	35	JB	100.0	-5.32E-26	3.10E-24	0.	5.532E+01	5.532E+01	5.532E+01	5.5321E+01	5.5321E+01	2.77E+01	
35	35	JA	0.0	-4.73E-26	2.27E-24	-1.72E-26	2.873E+01	2.873E+01	2.873E+01	2.8727E+01	2.8727E+01	1.44E+01	PIPEG
35	JB	100.0	-4.73E-26	2.27E-24	-1.72E-26	2.873E+01	2.873E+01	2.873E+01	2.8727E+01	2.8727E+01	1.44E+01		
36	37	JA	0.0	-1.01E-11	2.71E-11	6.96E-13	-1.758E+02	-1.758E+02	-1.758E+02	-1.7580E+02	-1.7580E+02	8.79E+01	PIPEG
36	JB	100.0	-1.01E-11	2.71E-11	6.96E-13	-1.758E+02	-1.758E+02	-1.758E+02	-1.7580E+02	-1.7580E+02	8.79E+01		
37	16	JA	0.0	-4.09E-13	1.42E-11	2.48E-13	1.690E+02	1.690E+02	1.690E+02	1.6902E+02	1.6902E+02	8.45E+01	PIPEG
37	JB	100.0	-4.09E-13	1.42E-11	2.48E-13	1.690E+02	1.690E+02	1.690E+02	1.6902E+02	1.6902E+02	8.45E+01		
38	39	JA	0.0	-5.66E-12	-2.34E-12	1.91E-13	-5.821E-13	-6.976E-13	-6.595E-13	-3.8906E-13	-7.7510E-13	2.73E-13	BEAMG
38	JB	100.0	-5.66E-12	-2.34E-12	1.91E-13	-5.821E-13	-5.787E-13	-5.3430E-13	-6.2985E-13	-3.29E-13			
39	39	JA	0.0	-9.70E-12	-1.20E-10	-2.32E-11	-1.468E-11	-1.670E-09	-1.816E-11	1.6440E-09	-1.6734E-09	8.22E-10	BEAMG
39	JB	100.0	-9.70E-12	-1.20E-10	-2.32E-11	-1.468E-11	-1.434E-09	-1.009E-11	1.432E-09	-1.4676E-09	7.19E-10		
40	41	JA	0.0	-1.52E-11	1.93E-12	6.05E-14	1.863E-12	1.825E-12	1.935E-12	1.9738E-12	1.7515E-12	9.69E-13	BEAMG
40	41	JB	100.0	-1.52E-11	1.93E-12	6.05E-14	1.863E-12	2.400E-12	1.9468E-12	2.4048E-12	1.3205E-12	1.20E-12	
41	41	JA	0.0	3.23E-12	1.05E-10	7.43E-12	1.227E-10	1.227E-10	1.267E-10	1.2646E-10	1.1883E-10	6.39E-11	BEAMG
41	42	JB	100.0	3.23E-12	1.05E-10	7.43E-12	1.227E-10	1.227E-10	1.267E-10	1.2646E-10	1.1883E-10	6.39E-11	

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39	JA	0.0	-9.70E-14	-1.20E-10	-2.42E-11	-1.468E-11	-1.000E-09	-1.816E-11	1.6440E-09	-1.6734E-09	4.22E-10	BEAMS
40	J1	100.0	-9.70E-14	-1.20E-10	-2.42E-11	-1.468E-11	1.000E-09	-1.009E-11	1.4542E-09	-1.4676E-09	7.19E-10	
40	11 JA	0.0	-1.42E-11	1.90E-12	6.05E-14	1.863E-12	1.825E-12	1.936E-12	1.9738E-12	1.7515E-12	9.89E-13	BEAMS
40	41 J9	100.0	-1.42E-11	1.90E-12	6.05E-14	1.863E-12	2.400E-12	1.868E-12	2.4048E-12	1.3205E-12	1.20E-12	
41	41 JA	0.0	3.23E-12	1.05E-10	7.43E-12	1.227E-10	1.227E-10	1.267E-10	1.2665E-10	1.1883E-10	6.38E-11	BEAMS
41	42 J4	100.0	3.23E-12	1.05E-10	7.43E-12	1.227E-10	-2.911E-10	1.195E-10	5.3972E-10	-2.9422E-10	2.70E-10	

DEAD-WEIGHT LOAD CASE

MAXIMUM STRESS SUMMARY FOR

BEAM STRESSES FOR OUTPUT VECTOR 1		
--- TRANSVERSE --- TORSIONAL - STRESSES AT USER LOCATIONS -		
MAXIMUM	MINIMUM	COMBINED
SHEAR	SHEAR	(P/A+MC/I)
(V2/K3^A)	(V3/K2^A)	(P/A-MC/I)

MAX. BEAM STRESSES = 4.45E+02 1.05E-10 7.36E-12 3.418E+02 4.318E+02 3.418E+02 4.5826E+02 3.4183E+02 2.29E+02
 BEAM NOS. = 23. 41. 28. 25. 20. 25. 20. 25. 20.

MIN. BEAM STRESSES = -3.05E+01 -1.20E-10 -2.32E-11 -3.555E+02 -4.591E+02 -3.555E+02 -3.5555E+02 -4.5906E+02 6.57E-15
 BEAM NOS. = 15. 37. 31. 12. 23. 12. 12. 23. 4.

B E G I N I N P U T L O A D C A S E N U . 5 T I T L E(E A R T H Q U A K E 1

NODAL POINT APPLIED FORCES FOR LOAD CASE NO. 5

NODE	X1	X2	X3	X4	X5	X6
1	-4.35400E+03	-4.35400E+03	-5.64400E+03	-0.	-0.	-0.
7	-5.18300E+03	5.18300E+03	-6.719000E+03	-0.	-0.	-0.
8	-3.24300E+03	3.24300E+03	-4.204000E+03	-0.	-0.	-0.
12	-3.30400E+03	6.309000E+03	-1.077100E+04	-0.	-0.	-0.
15	-1.039400E+04	1.039600E+04	-1.347700E+04	-0.	-0.	-0.
26	-6.732600E+03	8.988000E+03	-1.165200E+04	-0.	-0.	-0.
27	-6.162000E+03	6.182000E+03	-8.015000E+03	-0.	-0.	-0.
35	-3.400000E+03	3.400000E+03	-4.408000E+03	-0.	-0.	-0.
36	-1.704000E+03	1.704000E+03	-2.209000E+03	-0.	-0.	-0.

NODAL POINT APPLIED LOADS AND/OR DISPLACEMENTS FINAL SUMMARY FOR LOAD CASE NO. 5

NODE X1 X2 X3 X4 X5 X6

ENVIRO. IF A FINAL SUMMARY OF APPLIED NODAL LOADS AND GENERATED LOADS IS DESIRED AT THIS POINT,
CODE A 1 IN COLUMN 20 OF THE STATIC CARD.

FORCE AND MOMENT SUMMATION
ABOUT AXES PARALLEL TO SYSTEM AXES
WITH ORIGIN AT POINT (0,0,0)
SUMMATION INCLUDES LOADS APPLIED TO RESTRAINED DOF.

FX1	=	-.51759000000E+05
FX2	=	.51759000000E+05
FX3	=	-.67099000000E+05
MX1	=	-.10215600400E+08
MX2	=	-.10215600400E+08
MX3	=	0.

EARTHQUAKE 1

BEAM NO.	LOAD-LOCATION NODE--PERCENT.	HEA.M. ELEMENT LOADS FOR OUTPUT VECTOR 5					
		AXIAL P	SHEAR V1	SHEAR V3	TORSION M1	BENDING M2	BENDING M3
1	1 JA 0.0	5.64400E+03	-4.35400E+03	-4.35400E+03	7.45050E-09	4.47035E-08	1.49012E-08 PIPEG
1	4 JB 100.0	-5.64400E+03	4.35400E+03	4.35400E+03	-7.45050E-09	1.23000E+05	-1.23000E+05
2	3 JA 0.0	-1.65255E-09	-2.47383E-10	-3.91083E-10	1.04774E-09	1.51340E-09	-6.98492E-10 PIPEG
2	2 JB 100.0	1.65255E-09	2.47383E-10	3.91083E-10	-1.04774E-09	1.68802E-09	-2.09548E-09
3	3 JA 0.0	0.	-4.65661E-10	5.12227E-09	-2.98023E-08	8.94070E-08	1.19209E-07 BEAMG
3	4 JB 100.0	0.	4.65661E-10	-5.12227E-09	2.98023E-08	-2.83122E-07	-5.96046E-08
4	4 JA 0.0	2.98023E-08	-1.25724E-08	4.19095E-09	-1.49012E-07	1.78814E-07	1.19209E-07 BEAMG
4	5 JB 100.0	-2.98023E-08	1.25724E-08	-4.19095E-09	1.49012E-07	-3.27826E-07	-4.17233E-07
5	5 JA 0.0	1.39693E-09	1.60071E-10	2.71029E-10	-5.82077E-10	-2.61934E-10	1.39693E-09 PIPEG
5	6 JB 100.0	-1.39693E-09	-1.60071E-10	-2.71029E-10	5.82077E-10	-1.51340E-09	4.65661E-10
6	4 JA 0.0	5.64400E+03	-4.35400E+03	-4.35400E+03	-5.21541E-08	-1.23001E+05	1.23001E+05 PIPEG
6	7 JB 100.0	-5.64400E+03	4.35400E+03	4.35400E+03	5.21541E-08	2.19877E+05	-2.19877E+05
7	7 JA 0.0	1.23610E+04	-9.53700E+03	-9.53700E+03	-7.82311E-08	-2.19877E+05	2.19877E+05 PIPEG
7	8 JB 100.0	-1.23610E+04	9.53700E+03	9.53700E+03	7.82311E-08	3.11623E+05	-3.11623E+05
8	8 JA 0.0	1.65670E+04	-1.27800E+04	-1.27800E+04	-5.21541E-08	-3.11623E+05	3.11623E+05 PIPEG
8	11 JB 100.0	-1.65670E+04	1.27800E+04	1.27800E+04	5.21541E-08	4.90543E+05	-4.90543E+05
9	10 JA 0.0	8.92719E-10	-8.05438E-10	-1.66619E-09	8.3d190E-09	6.98492E-09	1.14699E-09 PIPEG
9	9 JB 100.0	-8.92719E-10	8.05438E-10	1.66619E-09	-8.3d190E-09	5.35510E-09	-7.20618E-09
10	10 JA 0.0	-3.39125E-09	5.04261E-09	7.21775E-09	-5.96046E-08	-1.19209E-07	-7.85487E-08 BEAMG
10	11 JB 100.0	3.39125E-09	-5.04261E-09	-7.21775E-09	5.96046E-08	-7.45050E-08	2.68407E-07
11	11 JA 0.0	1.65670E+04	1.08735E+04	1.08735E+04	-7.30139E+04	-4.81573E+05	4.81573E+05 PIPEG
11	12 JB 100.0	-1.65670E+04	-1.08735E+04	-1.08735E+04	7.30139E+04	3.29345E+05	-3.29345E+05
12	12 JA 0.0	2.73380E+04	2.56447E+03	2.56447E+03	-7.30139E+04	-3.29345E+05	3.29345E+05 PIPEG
12	37 JB 100.0	-2.73380E+04	-2.56447E+03	-2.56447E+03	7.30139E+04	2.10097E+05	-2.10097E+05
13	13 JA 0.0	1.53082E+04	6.07696E+03	1.48529E+03	1.03092E+03	-7.49409E+03	-5.02382E+04 BEAMG
13	14 JB 100.0	-1.53082E+04	-6.07696E+03	-1.48529E+03	-1.03092E+03	-2.14939E+01	8.09876E+04
14	15 JA 0.0	6.07696E+03	1.53082E+04	1.48529E+03	2.14939E+01	-1.30794E+04	6.44399E+04 BEAMG
14	14 JB 100.0	-6.07696E+03	-1.53082E+04	-1.48529E+03	-2.14939E+01	-1.03092E+03	8.09876E+04
15	15 JA 0.0	0.07696E+03	-1.53082E+04	1.48529E+03	2.14939E+01	1.30794E+04	6.44399E+04 BEAMG
15	16 JA 0.0	-6.07696E+03	1.53082E+04	-1.48529E+03	-2.14939E+01	-6.64985E+04	-4.08874E+05
16	16 JA 0.0	-6.04683E+03	1.82413E+04	-2.98378E+02	-2.14714E+01	1.75004E+03	5.00618E+05 BEAMG
16	17 JB 100.0	6.04683E+03	-1.82413E+04	2.98378E+02	2.14714E+01	4.96346E+03	-9.01880E+04
17	17 JA 0.0	-6.04683E+03	1.82413E+04	-2.98378E+02	-2.14714E+01	-4.96346E+03	9.01880E+04 BEAMG
17	18 JB 100.0	6.04683E+03	-1.82413E+04	2.98378E+02	2.14714E+01	7.79405E+03	8.31047E+04
18	19 JA 0.0	1.42513E+04	-6.04683E+03	-2.98378E+02	-7.79405E+03	1.48832E+03	-1.13702E+05 BEAMG
18	18 JB 100.0	-1.42513E+04	6.04683E+03	2.98378E+02	7.79405E+03	2.14714E+01	8.31047E+04
19	20 JA 0.0	1.42413E+04	-6.04683E+03	1.48529E+03	1.03092E+03	-7.49409E+03	-1.13702E+05 BEAMG

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16	17 JA	100.0	6.04683E+03	-1.82413E+04	2.98378E+02	2.14714E+01	6.49634E+03	-9.01880E+04
17	17 JA	0.0	-6.04683E+03	1.82413E+04	-2.98378E+02	-2.14714E+01	-6.49634E+03	9.01880E+04 BEAMG
17	18 JB	100.0	-6.04683E+03	-1.82413E+04	-2.98378E+02	2.14714E+01	7.79805E+03	8.31047E+04
18	19 JA	0.0	1.82413E+04	-6.04683E+03	-2.98378E+02	-7.79805E+03	1.48832E+03	-1.13702E+05 BEAMG
19	18 JB	100.0	-1.82413E+04	6.04683E+03	2.98378E+02	7.79805E+03	2.14714E+01	8.31047E+04
19	20 JA	0.0	1.82413E+04	-6.04683E+03	1.48529E+03	1.03092E+03	-7.49499E+03	-1.13702E+05 BEAMG
20	21 JA	100.0	-1.82413E+04	6.04683E+03	-1.48529E+03	-1.03092E+03	-2.14939E+01	8.31047E+04
20	22 JA	0.0	-6.04683E+03	1.82413E+04	1.48529E+03	2.14939E+01	-1.30794E+04	9.01880E+04 BEAMG
21	21 JB	100.0	6.04683E+03	-1.82413E+04	-1.48529E+03	-2.14939E+01	-1.03092E+03	8.31047E+04
21	22 JA	0.0	-6.04683E+03	1.82413E+04	1.48529E+03	2.14939E+01	1.30794E+04	9.01880E+04 BEAMG
21	16 JB	100.0	6.04683E+03	-1.82413E+04	-1.48529E+03	-2.14939E+01	-4.64985E+04	-5.00618E+05
22	16 JA	0.0	6.07695E+03	1.53042E+04	-2.98378E+02	-2.14714E+01	1.75004E+03	4.08874E+05 BEAMG
22	23 JB	100.0	-6.07695E+03	-1.53042E+04	2.98378E+02	2.14714E+01	4.96346E+03	-6.44399E+04
23	23 JA	0.0	6.07695E+03	1.53042E+04	-2.98378E+02	-2.14714E+01	-4.96346E+03	6.44399E+04 BEAMG
23	24 JB	100.0	-6.07695E+03	-1.53042E+04	2.98378E+02	2.14714E+01	7.79805E+03	8.09876E+04
24	25 JA	0.0	1.53042E+04	6.07695E+03	-2.98378E+02	-7.79805E+03	1.48832E+03	-5.02382E+04 BEAMG
24	24 JB	100.0	-1.53042E+04	-6.07695E+03	2.98378E+02	7.79805E+03	2.14714E+01	8.09876E+04
25	38 JA	0.0	-2.62840E+04	6.07593E+03	6.07593E+03	1.64830E+04	-1.90821E+05	1.90821E+05 PIPEG
25	26 JB	100.0	2.62840E+04	-6.07593E+03	-6.07593E+03	-1.64830E+04	-2.23497E+05	2.23497E+05
26	26 JA	0.0	-1.46320E+04	-2.91207E+03	-2.91207E+03	1.64830E+04	2.23497E+05	-2.23497E+05 PIPEG
26	27 JB	100.0	1.46320E+04	2.91207E+03	2.91207E+03	-1.64830E+04	-7.82859E+03	7.82859E+03
27	27 JA	0.0	-6.61700E+03	-9.09407E+03	-9.09407E+03	1.64830E+04	7.82859E+03	-7.82859E+03 PIPEG
27	30 JB	100.0	6.61700E+03	9.09407E+03	-9.09407E+03	-1.64830E+04	1.19488E+05	-1.19488E+05
28	29 JA	0.0	8.14907E-10	-9.53150E-10	-6.69388E-10	-2.15043E-10	4.88944E-09	6.05360E-09 PIPEG
28	28 JB	100.0	-8.14907E-10	9.53150E-10	6.69388E-10	2.15043E-10	1.16415E-10	-1.30385E-08
29	29 JA	0.0	9.31323E-10	9.31323E-10	2.09548E-09	8.15204E-08	7.45058E-09	-2.98023E-08 BEAMG
29	30 JB	100.0	-9.31323E-10	-9.31323E-10	-2.09548E-09	-8.15204E-08	-7.45058E-09	0.
30	30 JA	0.0	1.37185E+04	-2.79397E-09	-4.79527E+02	5.99510E+01	8.24150E+03	3.89691E+01 BEAMG
30	31 JB	100.0	-1.37185E+04	2.79397E-09	4.79527E+02	-5.99510E+01	5.03659E+03	-3.89691E+01
31	31 JA	0.0	1.37185E+04	-2.61934E-10	-4.79527E+02	5.99510E+01	-5.03659E+03	3.89691E+01 BEAMG
31	32 JB	100.0	-1.37185E+04	2.61934E-10	-4.79527E+02	-5.99510E+01	7.10335E+03	-3.89691E+01
32	30 JA	0.0	-1.37185E+04	-2.04691E-08	-4.79527E+02	5.99510E+01	8.24150E+03	-3.89691E+01 BEAMG
32	33 JB	100.0	1.37185E+04	2.04691E-08	4.79527E+02	-5.99510E+01	5.03659E+03	3.89691E+01
33	33 JA	0.0	-1.37185E+04	-2.91038E-11	-4.79527E+02	5.99510E+01	-5.03659E+03	-3.89691E+01 BEAMG
33	34 JB	100.0	1.37185E+04	2.91038E-11	-4.79527E+02	-5.99510E+01	7.10335E+03	3.89691E+01
34	30 JA	0.0	-6.61700E+03	5.10400E+03	5.10400E+03	0.	-1.19390E+05	1.19390E+05 PIPEG
34	35 JB	100.0	6.61700E+03	-5.10400E+03	-5.10400E+03	0.	4.79335E+04	-4.79335E+04
35	35 JA	0.0	-2.20930E+03	1.70400E+03	1.70400E+03	-4.65661E-10	-4.79335E+04	4.79335E+04 PIPEG
35	36 JA	100.0	2.20930E+03	-1.70400E+03	-1.70400E+03	4.65661E-10	-9.31323E-10	0.
36	37 JA	0.0	2.73380E+04	2.56447E+03	2.56447E+03	-7.30139E+04	-2.10097E+05	2.10097E+05 PIPEG
36	16 JB	100.0	-2.73380E+04	-2.56447E+03	-2.56447E+03	7.30139E+04	1.66902E+05	-1.66962E+05
37	16 JA	0.0	-2.62840E+04	6.07593E+03	6.07593E+03	1.64830E+04	-2.58749E+05	2.58749E+05 PIPEG
37	38 JB	100.0	2.62840E+04	-6.07593E+03	-6.07593E+03	-1.64830E+04	1.90821E+05	-1.90821E+05
38	11 JA	0.0	2.21045E+04	2.95306E+02	-1.54697E+03	2.16655E+02	3.65131E+04	8.26523E+03 BEAMG
38	39 JB	100.0	-2.21045E+04	-2.45306E+02	1.54697E+03	-2.16655E+02	6.32638E+03	-8.58216E+01
39	39 JA	0.0	2.21045E+04	-2.03727E+02	-1.54697E+03	1.32110E+02	-6.32871E+03	8.58216E+01 BEAMG
39	40 JB	100.0	-2.21045E+04	2.03727E+02	1.54697E+03	-1.32110E+02	1.29996E+04	-8.58216E+01
40	11 JA	0.0	-2.21045E+04	-2.95306E+02	-1.54697E+03	2.16655E+02	3.65131E+04	8.26523E+03 BEAMG
40	41 JB	100.0	2.21045E+04	2.95306E+02	1.54697E+03	-2.16655E+02	6.32638E+03	8.58216E+01
41	41 JA	0.0	-2.21065E+04	9.45874E-11	-1.54697E+03	1.32110E+02	-6.32871E+03	-8.58216E+01 BEAMG

39	JA	0.0	-2.21065E+04	-2.03747E+10	-1.54697E+03	32110E+02	-6.32871E+03	8.58216E+01	BEAMG	
40	JH	100.0	-2.21065E+04	2.03747E+10	1.54697E+03	32110E+02	1.29962E+04	-8.58216E+01		
40	41	JA	0.0	-2.21045E+04	-2.95306E+02	-1.54697E+03	2.16650E+02	3.65131E+04	-8.26523E+03	BEAMG
41	42	JH	100.0	2.21045E+04	2.95306E+02	1.54697E+03	-2.16650E+02	6.32638E+03	8.58216E+01	
41	42	JA	0.0	-2.21065E+04	9.45874E-11	-1.54697E+03	1.32110E+02	-6.32871E+03	-8.58216E+01	BEAMG
41	42	JH	100.0	2.21065E+04	-9.45874E-11	1.54697E+03	-1.32110E+02	1.29962E+04	8.58216E+01	

EARTHQUAKE I

MAXIMUM LOAD SUMMARY FOR

AXIAL P	BEAM ELEMENT LOADS			FOR OUTPUT VECTOR 5		
	B V2	S V3	E V3	T M1	B M2	H M3

MAXIMUM BEAM LOADS = 2.62840E+04 1.82413E+04 1.27800E+04 7.30139E+04 4.90543E+05 5.00616E+05
 BEAM NOS. = 37. 20. 8. 36. 8. 16.

MINIMUM BEAM LOADS = -2.73380E+04 -1.82413E+04 -1.27800E+04 -7.30139E+04 -4.81573E+05 -5.00518E+05
 BEAM NOS. = 36. 20. 8. 36. 11. 21.

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EARTHQUAKE 1

BEAM			F E A M		E N D		L O A D S		IN GLOBAL SYSTEM		FOR OUTPUT VECTOR		5
	--NODES--		FX1	FX2	FX3	HX1	HX2	HX3					
1	JA	1	-435E+04	.435E+04	-.564E+04	.447E-07	-.149E-07	-.745E-08					
	JB	4	.435E+04	-.435E+04	.564E+04	.123E+06	.123E+06	.745E-08					
2	JA	3	.391E-09	-.166E-08	.247E-09	.698E-09	.105E-08	-.151E-08					
	JB	2	-.391E-09	.166E-08	-.247E-09	.210E-08	-.105E-08	.169E-08					
3	JA	3	-.512E-08	0.	.466E-09	.119E-06	.298E-07	-.894E-07					
	JB	4	.512E-08	0.	-.466E-09	-.596E-07	-.298E-07	.243E-06					
4	JA	4	.419E-08	-.298E-07	.120E-07	.119E-06	.149E-06	-.179E-06					
	JB	5	-.419E-08	.298E-07	-.120E-07	-.417E-06	-.149E-06	.329E-06					
5	JA	5	.271E-09	-.140E-08	-.160E-09	.140E-08	.582E-09	.262E-09					
	JB	6	-.271E-09	.140E-08	.160E-09	-.466E-09	-.582E-09	.151E-08					
6	JA	4	-.435E+04	.435E+04	-.564E+04	-.123E+06	-.123E+06	.522E-07					
	JB	7	.435E+04	-.435E+04	.564E+04	.220E+06	.220E+06	-.522E-07					
7	JA	7	-.954E+04	.954E+04	-.124E+05	-.220E+06	-.220E+06	.782E-07					
	JB	8	.954E+04	-.954E+04	.124E+05	.312E+06	.312E+06	-.782E-07					
8	JA	8	-.120E+05	.120E+05	-.166E+05	-.312E+06	-.312E+06	.522E-07					
	JB	11	.120E+05	-.120E+05	.166E+05	.491E+06	.491E+06	-.522E-07					
9	JA	10	.181E-08	-.547E-09	.805E-09	.512E-08	.674E-08	-.698E-08					
	JB	9	-.181E-08	.547E-09	-.805E-09	-.811E-09	-.110E-07	.536E-08					
10	JA	10	.750E-08	-.271E-08	-.504E-08	-.135E-07	.978E-07	.119E-06					
	JB	11	-.750E-08	.271E-08	.504E-08	.148E-06	-.232E-06	.745E-07					
11	JA	11	.109E+05	-.109E+05	-.166E+05	-.402E+06	-.482E+06	.730E+05					
	JB	12	-.109E+05	.109E+05	.166E+05	.329E+06	.329E+06	-.730E+05					
12	JA	12	-.256E+04	.256E+04	-.273E+05	-.329E+06	-.329E+06	.730E+05					
	JB	37	.256E+04	-.256E+04	.273E+05	.210E+06	.210E+06	-.730E+05					
13	JA	13	.149E+04	-.608E+04	.153E+05	-.302E+05	.749E+04	.103E+04					
	JB	14	-.149E+04	.608E+04	-.153E+05	.810E+05	.215E+02	-.103E+04					
14	JA	15	-.149E+04	.604E+04	-.153E+05	-.044E+05	.215E+02	.131E+05					
	JB	14	.149E+04	-.604E+04	.153E+05	-.810E+05	-.215E+02	.103E+04					
15	JA	15	.149E+04	-.608E+04	.153E+05	.644E+05	-.215E+02	.131E+05					
	JB	16	-.149E+04	.608E+04	-.153E+05	-.409E+06	.215E+02	.465E+05					
16	JA	16	-.298E+03	.005E+04	-.182E+05	.501E+06	.215E+02	-.175E+04					
	JB	17	.298E+03	-.005E+04	.182E+05	-.902E+05	-.215E+02	.496E+04					
17	JA	17	-.298E+03	.505E+04	-.182E+05	.902E+05	.215E+02	.496E+04					
	JB	18	.298E+03	-.505E+04	.182E+05	.831E+05	-.215E+02	.790E+04					
18	JA	19	-.298E+03	.605E+04	-.182E+05	.114E+05	.149E+04	.790E+04					
	JB	18	.298E+03	-.605E+04	.182E+05	-.831E+05	.215E+02	.780E+04					
19	JA	20	.603E+04	-.144E+04	.182E+05	.749E+04	.114E+06	.103E+04					
	JB	21	-.603E+04	.144E+04	-.182E+05	.215E+02	-.831E+05	-.103E+04					
20	JA	22	-.605E+04	.149E+04	-.182E+05	.415E+02	.902E+05	.131E+05					
	JB	22	.605E+04	-.149E+04	.182E+05	-.215E+02	.902E+05	-.103E+04					

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18	JA 19	-.170E+04	.170E+04	-.605E+04	.169E+05	.119E+05	-.121E+05	-.176E+04
19	JB 19	.170E+04	-.170E+04	.205E+04	-.205E+04	.119E+05	-.119E+05	-.176E+04
20	JA 20	.170E+04	-.170E+04	.170E+04	-.170E+04	.119E+05	-.119E+05	-.176E+04
21	JA 21	-.205E+04	.205E+04	-.149E+04	.149E+04	.182E+05	-.182E+05	.131E+05
22	JB 21	-.205E+04	.205E+04	-.149E+04	.149E+04	.182E+05	-.182E+05	.131E+05
23	JA 22	.505E+04	-.505E+04	.149E+04	-.149E+04	.182E+05	-.182E+05	.131E+05
24	JB 22	.505E+04	-.505E+04	.149E+04	-.149E+04	.182E+05	-.182E+05	.131E+05
25	JA 23	-.505E+04	.505E+04	.294E+03	-.294E+03	.153E+05	-.153E+05	.409E+06
26	JB 23	-.505E+04	.505E+04	.294E+03	-.294E+03	.153E+05	-.153E+05	.644E+05
27	JA 24	.605E+04	-.605E+04	.294E+03	-.294E+03	.153E+05	-.153E+05	.644E+05
28	JB 24	.605E+04	-.605E+04	.294E+03	-.294E+03	.153E+05	-.153E+05	.810E+05
29	JA 25	-.605E+04	.605E+04	.294E+03	-.294E+03	.153E+05	-.153E+05	.502E+05
30	JB 25	-.605E+04	.605E+04	.294E+03	-.294E+03	.153E+05	-.153E+05	.810E+05
31	JA 26	.605E+04	-.605E+04	.294E+03	-.294E+03	.153E+05	-.153E+05	.502E+05
32	JB 26	.605E+04	-.605E+04	.294E+03	-.294E+03	.153E+05	-.153E+05	.810E+05
33	JA 27	-.291E+04	.291E+04	-.291E+04	.291E+04	.149E+05	-.149E+05	.223E+06
34	JB 27	-.291E+04	.291E+04	-.291E+04	.291E+04	.149E+05	-.149E+05	.783E+04
35	JA 28	-.904E+04	.904E+04	-.904E+04	.904E+04	.52E+04	-.52E+04	.783E+04
36	JB 28	-.904E+04	.904E+04	-.904E+04	.904E+04	.52E+04	-.52E+04	.119E+06
37	JA 29	.904E+04	-.904E+04	.904E+04	-.904E+04	.52E+04	-.52E+04	.119E+06
38	JB 29	.904E+04	-.904E+04	.904E+04	-.904E+04	.52E+04	-.52E+04	.119E+06
39	JA 30	-.105E-09	.105E-09	-.105E-09	.105E-09	.953E-09	-.953E-09	.413E-08
40	JB 30	-.105E-09	.105E-09	-.105E-09	.105E-09	.953E-09	-.953E-09	.937E-08
41	JA 31	-.214E-08	.214E-08	-.214E-08	.214E-08	.823E-09	-.823E-09	.787E-07
42	JB 31	-.214E-08	.214E-08	-.214E-08	.214E-08	.823E-09	-.823E-09	.576E-07
43	JA 32	-.137E+05	.137E+05	-.137E+05	.137E+05	.480E+03	-.480E+03	.463E-08
44	JB 32	-.137E+05	.137E+05	-.137E+05	.137E+05	.480E+03	-.480E+03	.937E-08
45	JA 33	-.137E+05	.137E+05	-.137E+05	.137E+05	.480E+03	-.480E+03	.463E-08
46	JB 33	-.137E+05	.137E+05	-.137E+05	.137E+05	.480E+03	-.480E+03	.937E-08
47	JA 34	-.137E+05	.137E+05	-.137E+05	.137E+05	.480E+03	-.480E+03	.463E-08
48	JB 34	-.137E+05	.137E+05	-.137E+05	.137E+05	.480E+03	-.480E+03	.937E-08
49	JA 35	-.137E+05	.137E+05	-.137E+05	.137E+05	.480E+03	-.480E+03	.463E-08
50	JB 35	-.137E+05	.137E+05	-.137E+05	.137E+05	.480E+03	-.480E+03	.937E-08
51	JA 36	-.170E+04	.170E+04	-.170E+04	.170E+04	.221E+04	-.221E+04	.479E+05
52	JB 36	-.170E+04	.170E+04	-.170E+04	.170E+04	.221E+04	-.221E+04	.931E-09
53	JA 37	-.250E+04	.250E+04	-.250E+04	.250E+04	.273E+05	-.273E+05	.210E+06
54	JB 37	-.250E+04	.250E+04	-.250E+04	.250E+04	.273E+05	-.273E+05	.167E+06
55	JA 38	-.605E+04	.605E+04	-.605E+04	.605E+04	.263E+05	-.263E+05	.191E+06
56	JB 38	-.605E+04	.605E+04	-.605E+04	.605E+04	.263E+05	-.263E+05	.191E+06
57	JA 39	-.221E+05	.221E+05	-.221E+05	.221E+05	.195E+04	-.195E+04	.104E+03
58	JB 39	-.221E+05	.221E+05	-.221E+05	.221E+05	.195E+04	-.195E+04	.132E+03
59	JA 40	-.221E+05	.221E+05	-.221E+05	.221E+05	.195E+04	-.195E+04	.132E+03
60	JB 40	-.221E+05	.221E+05	-.221E+05	.221E+05	.195E+04	-.195E+04	.132E+03
61	JA 41	-.155E+04	.155E+04	-.155E+04	.155E+04	.221E+05	-.221E+05	.704E+03
62	JB 41	-.155E+04	.155E+04	-.155E+04	.155E+04	.221E+05	-.221E+05	.132E+03
63	JA 42	-.155E+04	.155E+04	-.155E+04	.155E+04	.221E+05	-.221E+05	.132E+03

B.3-15

JA	11	-1.00E+00						
JR	41	.155E+04	.221E+05	.940E-10	.950E+02	.132E+03	.633E+04	
JR	42	.155E+04	.221E+05	.940E-10	.950E+02	.132E+03	.130E+05	

EARTHQUAKE 1

B.E.A.M. S.T.R.E.S.S.E.S. FOR OUTPUT VECTOR 5

BEAM	--- TRANSVERSE ---	TORSIONAL	STRESSES AT USER LOCATIONS -	MAXIMUM	MINIMUM	COMBINED
LOAD-LOCATION	SHEAR	(T ² C/J)	A	B	C	(P/A+MC/I) (P/A-MC/I) SHEAR
NJ	NUDE--PERCENT.	(V ₂ /K ₃)A	(V ₃ /K ₂)A			

1	1 JA	0.0	-4.87E+01	-4.87E+01	-1.88E-12	-3.159E+01	-3.159E+01	-3.1588E+01	-3.1588E+01	1.5AE+01	PIPEG	
1	4 J3	100.0	-4.87E+01	-4.87E+01	-1.88E-12	-3.159E+01	-3.055E+01	-3.055E+01	-3.6283E+01	-1.1946E+02	2.81E+01	
2	2 J3	100.0	-3.64E+11	-6.07E+11	-1.34E+11	1.447E+10	1.267E+10	1.058E+10	1.8743E+10	1.0189E+10	9.47E+11	
2	2 JR	100.0	-3.64E+11	-6.07E+11	-1.34E+11	1.447E+10	1.984E+10	1.880E+10	2.1370E+10	7.5616E+11	1.08E+10	
3	3 JA	0.0	-9.31E-13	1.02E-11	7.45E-14	0.	2.980E-13	-2.235E-13	5.2154E-13	-5.2154E-13	2.71E-13	BEAMG
3	4 JR	100.0	-9.31E-13	1.02E-11	7.45E-14	0.	1.490E-13	-7.078E-13	8.5682F-13	-8.5682E-13	4.35E-13	
4	4 JA	0.0	-2.51E+11	8.38E+12	3.73E+13	-5.960E+11	-5.931E+11	-6.005E+11	-5.8860E+11	-6.0350E+11	2.94E+11	BEAMG
4	5 JR	100.0	-2.51E+11	8.38E+12	3.73E+13	-5.960E+11	-5.856E+11	-6.042E+11	-5.7742E+11	-6.1467E+11	2.89E+11	
5	5 JA	0.0	2.49E+11	4.21E+11	7.7E+12	-1.085E+10	-7.265E+11	-1.018E+10	-7.2025E+11	-1.4449E+10	3.68E+11	PIPEG
5	6 JR	100.0	2.49E+11	4.21E+11	7.47E+12	-1.085E+10	-1.204E+10	-1.473E+10	-6.7866E+11	-1.4912E+10	3.47E+11	
6	4 JA	0.0	-4.67E+01	-4.67E+01	1.32E+11	-3.159E+01	3.055E+01	3.055E+01	5.6243E+01	-1.1946E+02	2.81E+01	PIPEG
6	7 J3	100.0	-4.67E+01	-4.67E+01	1.32E+11	-3.159E+01	7.948E+01	7.948E+01	1.2549E+02	-1.6867E+02	6.27E+01	
7	7 JA	0.0	-2.73E+02	-2.73E+02	5.09E+11	-1.769E+02	1.090E+02	1.090E+02	2.2744E+02	-5.8117E+02	1.14E+02	PIPEG
7	8 JR	100.0	-2.73E+02	-2.73E+02	5.09E+11	-1.769E+02	2.203E+02	2.283E+02	3.9614E+02	-7.4988E+02	1.98E+02	
8	8 JA	0.0	-2.35E+02	-2.35E+02	1.75E+11	-1.524E+02	5.697E+01	5.697E+01	1.4368E+02	-4.4842E+02	7.18E+01	PIPEG
8	11 JR	100.0	-2.35E+02	-2.35E+02	1.75E+11	-1.524E+02	1.772E+02	1.772E+02	3.1366E+02	-6.1840E+02	1.57E+02	
9	10 JA	0.0	-6.01E+11	-1.37E+10	-4.58E+11	-3.667E+11	-2.413E+11	-1.130E+10	4.0700E+11	-1.1403E+10	5.01E+11	PIPEG
9	9 JR	100.0	-6.01E+11	-1.37E+10	-4.58E+11	-3.667E+11	-5.210E+11	-2.186E+11	-5.1463E+11	-1.3479E+10	5.52E+11	
10	10 JA	0.0	1.01E+11	1.44E+11	1.49E+13	6.782E+12	6.586E+12	7.081E+12	7.2771E+12	6.2874E+12	3.64E+12	BEAMG
10	11 JR	100.0	1.01E+11	1.44E+11	1.49E+13	6.782E+12	6.111E+12	6.596E+12	7.6398E+12	5.9252E+12	3.82E+12	
11	11 JA	0.0	2.00E+02	2.00E+02	2.45E+01	-1.524E+02	1.711E+02	1.711E+02	3.0514E+02	-6.0988E+02	1.55E+02	PIPEG
11	12 JR	100.0	2.00E+02	2.00E+02	2.45E+01	-1.524E+02	6.88E+01	6.88E+01	1.6052E+02	-4.6526E+02	8.39E+01	
12	12 JA	0.0	7.34E+01	7.34E+01	4.75E+01	-3.911E+02	3.712E+01	3.712E+01	2.1450E+02	-9.9670E+02	1.17E+02	PIPEG
12	37 JR	100.0	7.34E+01	7.34E+01	4.75E+01	-3.911E+02	-1.179E+02	-1.179E+02	-4.7749E+00	-7.7742E+02	4.75E+01	
13	13 JA	0.0	1.22E+01	2.97E+00	-2.59E+03	-3.062E+01	-3.074E+01	-3.060E+01	-3.0472E+01	-3.0761E+01	1.52E+01	BEAMG
13	14 JR	100.0	1.22E+01	2.97E+00	-2.59E+03	-3.062E+01	-3.082E+01	-3.062E+01	-3.0414E+01	-3.0819E+01	1.52E+01	
14	15 JA	0.0	4.46E+02	4.33E+01	-2.57E+00	-1.772E+02	2.190E+02	-1.355E+02	2.6075E+02	-6.1519E+02	1.30E+02	BEAMG
14	14 JR	100.0	4.46E+02	4.33E+01	-2.57E+00	-1.772E+02	-6.752E+02	-1.005E+02	3.2408E+02	-6.7853E+02	1.62E+02	
15	15 JA	0.0	-3.05E+01	2.97E+00	-5.37E+05	-1.215E+01	-1.199E+01	-1.219E+01	-1.1960E+01	-1.2348E+01	5.98E+00	BEAMG
15	16 JR	100.0	-3.05E+01	2.97E+00	-5.37E+05	-1.215E+01	-1.113E+01	-1.227E+01	-1.1015E+01	-1.3292E+01	5.51E+00	
15	16 JA	0.0	3.65E+01	-5.97E+01	5.37E+05	1.209E+01	1.335E+01	1.209E+01	1.3350E+01	1.0838E+01	6.67E+00	BEAMG
15	17 JR	100.0	3.65E+01	-5.97E+01	5.37E+05	1.209E+01	1.232E+01	1.211E+01	1.2332E+01	1.1856E+01	6.17E+00	
17	17 JA	0.0	5.32E+02	-8.70E+00	2.57E+00	1.763E+02	7.309E+02	1.922E+02	7.4677E+02	-3.9408E+02	3.73E+02	BEAMG
17	18 JR	100.0	5.32E+02	-8.70E+00	2.57E+00	1.763E+02	-3.347E+02	2.012E+02	7.1225E+02	-3.5456E+02	3.56E+02	
18	19 JA	0.0	-1.21E+01	-5.97E+01	1.95E+02	-3.64E+01	-3.677E+01	-3.649E+01	-3.6195E+01	-3.6771E+01	1.11E+01	BEAMG
18	19 JR	100.0	-1.21E+01	-5.97E+01	1.95E+02	-3.64E+01	-3.694E+01	-3.648E+01	-3.5275E+01	-3.6690E+01	1.41E+01	
19	20 JA	0.0	-1.21E+01	2.97E+00	-2.55E+03	-3.064E+01	-3.577E+01	-3.046E+01	-3.6180E+01	-3.5766E+01	1.81E+01	BEAMG
19	21 JR	100.0	-1.21E+01	2.97E+00	-2.55E+03	-3.064E+01	-3.669E+01	-3.648E+01	-3.5275E+01	-3.6690E+01	1.81E+01	

17	JA	0.0	5.32E+02	-4.70E+00	2.97E+00	1.763E+02	7.00E+02	1.422E+02	7.4677E+02	-3.9408E+02	3.73E+02	BEAMG	
18	JB	100.0	5.32E+02	-4.70E+00	2.97E+00	1.763E+02	-3.00E+02	2.012E+02	7.1225E+02	-3.5950E+02	3.56E+02		
19	JA	0.0	-1.21E+01	-5.97E+01	1.95E+02	-3.648E+01	-3.6577E+01	-3.649E+01	-3.6195E+01	-3.6771E+01	1.81E+01	BEAMG	
19	JB	100.0	-1.21E+01	-5.97E+01	1.95E+02	-3.648E+01	-3.659E+01	-3.648E+01	-3.6275E+01	-3.6690E+01	1.81E+01		
19	20	JA	0.0	-1.21E+01	2.97E+00	-2.58E+03	-3.648E+01	-3.677E+01	-3.646E+01	-3.6140E+01	-3.6786E+01	1.81E+01	BEAMG
19	21	JB	100.0	-1.21E+01	2.97E+00	-2.58E+03	-3.648E+01	-3.569E+01	-3.648E+01	-3.6275E+01	-3.6690E+01	1.81E+01	
20	22	JA	0.0	5.32E+02	4.33E+01	-2.57E+00	1.763E+02	7.303E+02	2.181E+02	7.7265E+02	-4.1996E+02	3.84E+02	BEAMG
20	21	JB	100.0	5.32E+02	4.33E+01	-2.57E+00	1.763E+02	7.347E+02	1.731E+02	6.9067E+02	-3.3744E+02	3.45E+02	
21	22	JA	0.0	-3.65E+01	2.97E+00	-5.37E+05	1.209E+01	1.232E+01	1.206E+01	1.2352E+01	1.1835E+01	6.18E+00	BEAMG
21	16	JB	100.0	-3.65E+01	2.97E+00	-5.37E+05	1.209E+01	1.335E+01	1.198E+01	1.3461E+01	1.0726E+01	6.73E+00	
22	23	JA	0.0	3.05E+01	-5.97E+01	5.37E+05	-1.215E+01	-1.113E+01	-1.216E+01	-1.1127E+01	-1.3160E+01	5.56E+00	BEAMG
22	23	JB	100.0	3.05E+01	-5.97E+01	5.37E+05	-1.215E+01	-1.199E+01	-1.214E+01	-1.1980E+01	-1.2327E+01	5.99E+00	
23	23	JA	0.0	4.46E+02	-8.70E+00	2.57E+00	-1.772E+02	2.190E+02	-1.614E+02	2.3487E+02	-5.8931E+02	1.17E+02	BEAMG
23	24	JB	100.0	4.46E+02	-8.70E+00	2.57E+00	-1.772E+02	-6.752E+02	-1.524E+02	3.4566E+02	-7.0011E+02	1.73E+02	
24	25	JA	0.0	1.22E+01	-5.97E+01	1.95E+02	-3.062E+01	-3.074E+01	-3.062E+01	-3.0487E+01	-3.0746E+01	1.52E+01	BEAMG
24	24	JB	100.0	1.22E+01	-5.97E+01	1.95E+02	-3.062E+01	-3.082E+01	-3.062E+01	-3.0414E+01	-3.0819E+01	1.52E+01	
25	23	JA	0.0	1.74E+02	1.7E+02	-1.07E+01	3.760E+02	6.241E+02	6.241E+02	7.2690E+02	2.5141E+01	3.64E+02	PIPEG
25	26	JB	100.0	1.74E+02	1.7E+02	-1.07E+01	3.760E+02	8.542E+01	8.542E+01	7.8694E+02	-3.4944E+01	3.94E+02	
26	25	JA	0.0	-8.33E+01	-8.33E+01	-1.07E+01	2.093E+02	-8.127E+01	-8.127E+01	6.2029E+02	-2.0164E+02	3.10E+02	PIPEG
26	27	JB	100.0	-8.33E+01	-8.33E+01	-1.07E+01	2.093E+02	1.991E+02	1.991E+02	2.2372E+02	1.9493E+02	1.12E+02	
27	27	JA	0.0	-1.67E+02	-1.67E+02	-5.54E+00	6.066E+01	5.560E+01	5.560E+01	6.8295E+01	5.3421E+01	3.46E+01	PIPEG
27	30	JB	100.0	-1.67E+02	-1.67E+02	-5.54E+00	6.066E+01	1.411E+02	1.411E+02	1.7430E+02	-5.2659E+01	8.74E+01	
28	29	JA	0.0	-7.02E-11	-5.49E-11	1.18E-12	-3.347E-11	3.269E-11	-8.691E-11	5.1581E-11	-1.1852E-10	2.58E-11	PIPEG
28	28	JB	100.0	-7.02E-11	-5.49E-11	1.18E-12	-3.347E-11	1.040E-10	-3.220E-11	1.0904E-10	-1.7598E-10	5.45E-11	
29	29	JA	0.0	1.06E-12	4.19E-12	-2.04E-13	-1.863E-12	-1.937E-12	-1.881E-12	-1.7695E-12	-1.9558E-12	9.08E-13	BEAMG
29	30	JB	100.0	1.06E-12	4.19E-12	-2.04E-13	-1.863E-12	-1.863E-12	-2.049E-12	-1.6764E-12	-2.0489E-12	8.63E-13	
30	30	JA	0.0	-5.59E-12	-9.59E-01	-1.50E-04	-2.744E+01	-2.744E+01	-2.746E+01	-2.7416E+01	-2.7459E+01	1.37E+01	BEAMG
30	31	JB	100.0	-5.59E-12	-9.59E-01	-1.50E-04	-2.744E+01	-2.744E+01	-2.742E+01	-2.7424E+01	-2.7450E+01	1.37E+01	
31	31	JA	0.0	-2.91E-11	-5.33E+01	-2.05E+01	-1.524E+03	-1.247E+03	-1.516E+03	-1.2385E+03	-1.8101E+03	6.20E+02	BEAMG
31	32	JB	100.0	-2.91E-11	-5.33E+01	-2.05E+01	-1.524E+03	-1.247E+03	-1.512E+03	-1.2349E+03	-1.8136E+03	6.18E+02	
32	30	JA	0.0	-4.10E-11	-4.57E-01	-1.50E-04	2.744E+01	2.744E+01	2.742E+01	2.7458E+01	2.7416E+01	1.37E+01	BEAMG
32	33	JB	100.0	-4.10E-11	-4.57E-01	-1.50E-04	2.744E+01	2.744E+01	2.745E+01	2.7450E+01	2.7424E+01	1.37E+01	
33	33	JA	0.0	-3.23E-12	-5.33E+01	-2.05E+01	1.524E+03	1.247E+03	1.533E+03	1.8101E+03	1.2385E+03	9.05E+02	BEAMG
33	34	JB	100.0	-3.23E-12	-5.33E+01	-2.05E+01	1.524E+03	1.247E+03	1.537E+03	1.8136E+03	1.2349E+03	9.07E+02	
34	30	JA	0.0	9.39E+01	9.39E+01	0.	6.086E+01	1.411E+02	1.411E+02	1.7428E+02	-5.2565E+01	8.71E+01	PIPEG
34	35	JB	100.0	9.39E+01	9.39E+01	0.	6.086E+01	9.305E+01	9.305E+01	1.0640E+02	1.5320E+01	5.32E+01	
35	35	JA	0.0	4.87E+01	4.87E+01	3.03E-13	3.160E+01	9.393E+01	9.393E+01	1.1974E+02	-5.6538E+01	5.99E+01	PIPEG
35	36	JB	100.0	4.87E+01	4.87E+01	3.03E-13	3.160E+01	3.160E+01	3.160E+01	3.1602E+01	3.1602E+01	1.59E+01	
36	37	JA	0.0	3.03E+01	3.63E+01	2.35E+01	-1.934E+02	-5.841E+01	-5.841E+01	-2.5013E+00	-3.8425E+02	2.35E+01	PIPEG
36	36	JB	100.0	3.03E+01	3.63E+01	2.35E+01	-1.934E+02	-8.612E+01	-8.612E+01	-4.1639E+01	-3.4506E+02	3.14E+01	
37	16	JA	0.0	8.59E+01	8.59E+01	-5.24E+00	1.859E+02	3.521E+02	3.521E+02	4.2100E+02	-4.9156E+01	2.11E+02	PIPEG
37	38	JB	100.0	8.59E+01	8.59E+01	-5.24E+00	1.859E+02	3.085E+02	3.085E+02	3.521E+02	-1.2558E+01	1.40E+02	
38	11	JA	0.0	5.91E-01	-3.09E+00	-5.42E+04	-4.421E+01	-4.414E+01	-4.430E+01	-4.4097E+01	-4.4321E+01	2.20E+01	BEAMG
38	39	JB	100.0	5.91E-01	-3.09E+00	-5.42E+04	-4.421E+01	-4.421E+01	-4.419E+01	-4.4193E+01	-4.4225E+01	2.21E+01	
39	39	JA	0.0	-2.26E-11	-1.72E+02	-5.87E+01	-2.456E+03	-1.846E+03	-2.445E+03	-1.8352E+03	-3.0774E+03	9.19E+02	BEAMG
39	40	JB	100.0	-2.26E-11	-1.72E+02	-5.87E+01	-2.456E+03	-1.846E+03	-2.434E+03	-1.8236E+03	-3.0889E+03	9.14E+02	A.3=17
40	11	JA	0.0	-5.91E-01	-3.09E+00	-5.42E+04	4.421E+01	4.414E+01	4.412E+01	4.4321E+01	4.4097E+01	2.22E+01	BEAMG
40	41	JB	100.0	-5.91E-01	-3.09E+00	-5.42L+04	4.421E+01	4.421E+01	4.422E+01	4.4225E+01	4.4193E+01	2.21E+01	
41	41	JA	0.0	1.05E-11	-1.72E+02	-5.87E+01	2.456E+03	1.846L+03	2.467E+03	3.0774E+03	1.8352E+03	1.54E+03	BEAMG
41	42	JB	100.0	1.05E-11	-1.72E+02	-5.87E+01	2.456E+03	1.846E+03	2.470E+03	3.0884E+03	1.8236E+03	1.55E+03	

+1	41 JA	0.0	1.05E-11	-1.72E+02	-5.87E+01	2.456E+03	1.846E+03	2.467E+03	3.0774E+03	1.8352E+03	1.54E+03	BEAM5	
+1	42 JB	100.0	1.05E-11	-1.72E+02	-5.87E+01	2.456E+03	1.846E+03	2.479E+03	3.0889E+03	1.8236E+03	1.55E+03	BEAM6	

EARTHQUAKE 1

MAXIMUM STRESS SUMMARY FOR

BEAM STRESSES FOR OUTPUT VECTOR 5
 --- TRANSVERSE --- TORSIONAL STRESSES AT USER LOCATIONS - MAXIMUM MINIMUM COMBINED
 SHEAR SHEAR ((P/C/J) A H C (P/A+MC/I) (P/A-MC/I) STRESS
 $(V2/K3*A)$ $(V3/K2*A)$

MAX. BEAM STRESSES = 5.32E+02 2.00E+02 4.75E+01 2.456E+03 1.846E+03 2.479E+03 3.0889E+03 1.8352E+03 1.55E+03
 BEAM NOS. = 16. 11. 12. 41. 41. 41. 41. 41. 41.

MIN. BEAM STRESSES = -2.73E+02 -2.73E+02 -5.87E+01 -2.456E+03 -1.846E+03 -2.445E+03 -1.8352E+03 -3.0889E+03 2.71E-13
 BEAM NOS. = 7. 7. 39. 39. 39. 39. 39. 39. 3.

BEGIN INPUT LOAD CASE NO. 6 TITLE: EARTHQUAKE 2

NODAL POINT APPLIED FORCES FOR LOAD CASE NO. 6

NODE	X1	X2	X3	X4	X5	X6
1	-4.354000E+03	4.354000E+03	-5.644000E+03	-0.	-0.	-0.
7	-3.504000E+03	3.504000E+03	-6.719000E+03	-0.	-0.	-0.
8	-1.998000E+03	1.998000E+03	-4.204000E+03	-0.	-0.	-0.
12	-3.631000E+03	3.631000E+03	-1.07100E+04	-0.	-0.	-0.
16	-3.350000E+02	3.350000E+02	-1.347700E+04	-0.	-0.	-0.
26	3.253000E+03	-3.263000E+03	-1.165200E+04	-0.	-0.	-0.
27	6.445000E+03	-4.483000E+03	-8.015000E+03	-0.	-0.	-0.
35	2.931000E+03	-2.931000E+03	-4.408000E+03	-0.	-0.	-0.
36	1.764000E+03	-1.764000E+03	-2.209000E+03	-0.	-0.	-0.

NODAL POINT APPLIED LOADS AND/OR DISPLACEMENTS FINAL SUMMARY FOR LOAD CASE NO. 6

NODE X1 X2 X3 X4 X5 X6

NOTE: IF A FINAL SUMMARY OF APPLIED NODAL LOADS AND GENERATED LOADS IS DESIRED AT THIS POINT,
CODE A 1 IN COLUMN 20 OF THE STATIC CARD.

FORCE AND MOMENT SUMMATION
ABOUT AXES PARALLEL TO SYSTEM AXES

WITH ORIGIN AT POINT (0,0,0)

SUMMATION INCLUDES LOADS APPLIED TO RESTRAINED DOF.

$$FX_1 = -1.442000000E+04$$

$$FX_2 = .1442000000E+04$$

$$FX_3 = -37099000000E+05$$

$$MX_1 = -35645557400E+07$$

$$MX_2 = -35645557400E+07$$

$$MX_3 = 0.$$

A.3-19

EARTHQUAKE 2

			DE A M	E L E M E N T	L O A D S	F O R _ O U T P U T	V E C T O R	.6
O	DEA1	LOAD-LOCATION.	AXIAL	SHEAR	SHEAR	TORSION	BENDING	BENDING
O	NO	NOOE--PERCENT.	J P	V2	V3	M1	M2	M3
O	1	1 JA 0.0	5.64400E+03	-4.35400E+03	-4.35400E+03	0.	3.72529E-08	2.98023E-08 PIPEG
O	1	4 JB 100.0	-5.64400E+03	4.35400E+03	4.35400E+03	0.	1.23000E+05	-1.23000E+05
O	2	3 JA 0.0	-1.86265E-09	-2.54659E-10	-7.43967E-10	9.31323E-10	3.23053E-09	-9.31323E-10 PIPEG
O	2	2 JB 100.0	1.86265E-09	2.54659E-10	7.43947E-10	-9.31323E-10	3.55067E-09	-2.0954HE-09
O	3	3 JA 0.0	1.49012E-08	-3.25963E-09	1.31549E-08	0.	1.49012E-08	5.96046E-08 BEAMG
O	3	4 JB 100.0	-1.49012E-08	3.25963E-09	-1.31549E-08	0.	-2.98023E-07	-5.96046E-08
O	4	4 JA 0.0	-3.72529E-08	-1.16415E-08	8.38190E-09	-1.49012E-07	1.71363E-07	1.78814E-07 BEAMG
O	4	5 JB 100.0	-3.72529E-08	1.16415E-08	-8.38190E-09	1.49012E-07	-3.42727E-07	-4.17233E-07
O	5	5 JA 0.0	2.32831E-09	8.00355E-11	3.01952E-10	-6.98492E-10	6.98492E-10	1.16415E-09 PIPEG
O	5	6 JB 100.0	-2.32831E-09	-8.00355E-11	-3.01952E-10	6.98492E-10	-1.92085E-09	0.
O	6	4 JA 0.0	5.64400E+03	-4.35400E+03	-4.35400E+03	-1.86265E-08	-1.23001E+05	1.23001E+05 PIPEG
O	6	7 JB 100.0	-5.64400E+03	4.35400E+03	4.35400E+03	1.86265E-08	2.19877E+05	-2.19877E+05
O	7	7 JA 0.0	1.23630E+04	-7.86300E+03	-7.86300E+03	-3.53903E-08	-2.19877E+05	2.19877E+05 PIPEG
O	7	8 JB 100.0	-1.23630E+04	7.86300E+03	7.86300E+03	3.53903E-08	2.95519E+05	-2.95519E+05
O	8	8 JA 0.0	1.65670E+04	-9.86100E+03	-9.86100E+03	-2.23517E-08	-2.95519E+05	2.95519E+05 PIPEG
O	8	11 JB 100.0	-1.65670E+04	9.86100E+03	9.86100E+03	2.23517E-08	4.33573E+05	-4.33573E+05
O	9	10 JA 0.0	7.43932E-10	-6.42706E-10	-8.47649E-10	9.77889E-09	4.07454E-09	2.45629E-09 PIPEG
O	9	14 JB 100.0	-7.43932E-10	6.42706E-10	8.47649E-10	-9.77889E-09	2.56114E-09	-6.58919E-09
O	10	10 JA 0.0	-2.96734E-09	6.34773E-09	2.09548E-09	-8.94070E-08	-1.49012E-08	-1.61289E-07 BEAMG
O	10	11 JB 100.0	2.96734E-09	-6.34773E-09	-2.09548E-09	8.94070E-08	-2.98023E-08	3.49341E-07
O	11	11 JA 0.0	1.55670E+04	7.77124E+03	7.77124E+03	-5.75376E+04	-4.26835E+05	4.26835E+05 PIPEG
O	11	12 JB 100.0	-1.55670E+04	-7.77124E+03	-7.77124E+03	5.75376E+04	3.18038E+05	-3.18038E+05
O	12	12 JA 0.0	2.73380E+04	4.14024E+03	4.14024E+03	-5.75376E+04	-3.18038E+05	3.18038E+05 PIPEG
O	12	37 JB 100.0	-2.73380E+04	-4.14024E+03	-4.14024E+03	5.75376E+04	1.25517E+05	-1.25517E+05
O	13	13 JA 0.0	1.87368E+04	-2.43498E+03	-9.46721E+01	-3.29985E+03	4.50340E+02	-9.58192E+04 BEAMG
O	13	14 JB 100.0	-1.87368E+04	2.43498E+03	9.46721E+01	3.29985E+03	2.87004E+01	8.34982E+04
O	14	15 JA 0.0	-2.43498E+03	1.87368E+04	-9.46721E+01	-2.87004E+01	-2.40047E+03	9.45016E+04 BEAMG
O	14	14 JB 100.0	2.43498E+03	-1.87368E+04	9.46721E+01	2.87004E+01	3.29985E+03	8.34982E+04
O	15	15 JA 0.0	-2.43498E+03	-1.87368E+04	-9.46721E+01	-2.87004E+01	2.40047E+03	9.45016E+04 BEAMG
O	15	16 JB 100.0	2.43498E+03	1.87368E+04	9.46721E+01	2.87004E+01	-2.70348E+02	-5.16080E+05
O	16	16 JA 0.0	2.46511E+03	1.48127E+04	6.26294E+02	2.87105E+01	-1.97726E+04	3.93412E+05 BEAMG
O	16	17 JB 100.0	-2.46511E+03	-1.48127E+04	-6.26294E+02	-2.87105E+01	5.68095E+03	-6.01263E+04
O	17	17 JA 0.0	2.46511E+03	1.48127E+04	6.26294E+02	2.87105E+01	-5.68095E+03	6.01263E+04 BEAMG
O	17	18 JB 100.0	-2.46511E+03	-1.48127E+04	-6.26294E+02	-2.87105E+01	-2.68844E+02	8.05941E+04
O	18	19 JA 0.0	1.48127E+04	2.46511E+03	6.26294E+02	2.68844E+02	-3.14034E+03	-6.81207E+04 BEAMG
O	18	18 JB 100.0	-1.48127E+04	-2.46511E+03	-6.26294E+02	-2.68844E+02	-2.87105E+01	8.05941E+04
O	19	20 JA 0.0	1.48127E+04	2.46511E+03	-9.46721E+01	-3.29985E+03	4.50340E+02	-6.81207E+04 BEAMG
O	19	21 JB 100.0	-1.48127E+04	-2.46511E+03	9.46721E+01	3.29985E+03	2.87004E+01	8.05941E+04

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17	17 JA	0.0	-2.46511E+03	1.48127E+04	6.26294E+02	-6.7105E+01	-5.68095E+03	6.01263E+04
18	18 JA	0.0	1.48127E+04	2.46511E+03	6.26294E+02	-2.68844E+02	-3.14034E+03	-6.81207E+04 BEAMG
18	18 JR	100.0	-1.48127E+04	-2.46511E+03	-6.26294E+02	-2.68844E+02	-2.87105E+01	8.05941E+04
19	19 JA	0.0	1.48127E+04	2.46511E+03	-9.46721E+01	-3.24995E+03	4.50340E+02	-6.81207E+04 BEAMG
19	19 JR	100.0	-1.48127E+04	-2.46511E+03	9.46721E+01	3.24995E+03	2.87004E+01	8.05941E+04
20	20 JA	0.0	2.46511E+03	1.48127E+04	-9.46721E+01	-2.87004E+01	-2.40047E+03	6.01263E+04 BEAMG
20	20 JR	100.0	-2.46511E+03	-1.48127E+04	9.46721E+01	2.87004E+01	3.24995E+03	8.05941E+04
21	21 JA	0.0	2.46511E+03	-1.48127E+04	-9.46721E+01	-2.87004E+01	2.40047E+03	6.01263E+04 BEAMG
21	21 JR	100.0	-2.46511E+03	1.48127E+04	9.46721E+01	2.87004E+01	-2.70349E+02	-3.93412E+05
22	22 JA	0.0	-2.43494E+03	1.87305E+04	6.26294E+02	2.87105E+01	-1.97726E+04	5.16080E+05 BEAMG
22	22 JR	100.0	2.43494E+03	-1.87305E+04	-6.26294E+02	-2.87105E+01	5.68095E+03	-8.45016E+04
23	23 JA	0.0	-2.43494E+03	1.87305E+04	6.26294E+02	2.87105E+01	-5.68095E+03	9.45016E+04 BEAMG
23	23 JR	100.0	2.43494E+03	-1.87305E+04	-6.26294E+02	-2.87105E+01	-2.68844E+02	8.34982E+04
24	24 JA	0.0	1.87305E+04	-2.43494E+03	6.26294E+02	2.68844E+02	-3.14034E+03	-9.58192E+04 BEAMG
24	24 JR	100.0	-1.87305E+04	2.43494E+03	-6.26294E+02	-2.68844E+02	-2.87105E+01	8.34982E+04
25	25 JA	0.0	-2.62840E+04	-1.81602E+03	-1.81602E+03	-1.74518E+04	4.65359E+04	-4.65359E+04 PIPEG
25	25 JR	100.0	2.62840E+04	1.81602E+03	1.81602E+03	1.74518E+04	-7.73531E+04	-7.73531E+04
26	26 JA	0.0	-1.46320E+04	1.44618E+03	1.44618E+03	-1.74518E+04	-7.73531E+04	7.73531E+04 PIPEG
26	26 JR	100.0	1.46320E+04	-1.44618E+03	-1.44618E+03	1.74518E+04	-2.97510E+04	2.97510E+04
27	27 JA	0.0	-6.61700E+03	5.93418E+03	5.93418E+03	-1.74518E+04	2.97510E+04	-2.97510E+04 PIPEG
27	27 JR	100.0	6.61700E+03	-5.93418E+03	-5.93418E+03	1.74518E+04	-1.12830E+05	1.12830E+05
28	28 JA	0.0	-1.04774E-09	-2.96632E-09	6.05723E-10	-1.45154E-09	-4.48199E-09	-5.87897E-09 PIPEG
28	28 JR	100.0	1.04774E-09	2.96632E-09	-6.05723E-10	1.45154E-09	-2.32831E-10	-1.66326E-08
29	29 JA	0.0	-9.31323E-10	-1.12032E-08	-2.56114E-09	1.16670E-07	3.72529E-09	-1.37836E-07 BEAMG
29	29 JR	100.0	9.31323E-10	1.12032E-08	2.56114E-09	-1.16670E-07	6.70552E-08	-1.88127E-07
30	30 JA	0.0	-1.01271E+04	-1.17579E-08	4.42057E+02	-3.62852E+00	-8.72588E+03	-2.35857E+00 BEAMG
30	30 JR	100.0	1.01271E+04	1.17579E-08	-4.42057E+02	3.62852E+00	-3.51408E+03	2.35857E+00
31	31 JA	0.0	-1.01271E+04	-1.60071E-10	4.42057E+02	-3.62852E+00	3.51468E+03	-2.35857E+00 BEAMG
31	31 JR	100.0	1.01271E+04	1.60071E-10	-4.42057E+02	3.62852E+00	-5.41994E+03	2.35857E+00
32	32 JA	0.0	1.01271E+04	-2.33142E-08	4.42057E+02	-3.62852E+00	-8.72588E+03	2.35857E+00 BEAMG
32	32 JR	100.0	-1.01271E+04	2.33142E-08	-4.42057E+02	3.62852E+00	-3.51468E+03	-2.35857E+00
33	33 JA	0.0	1.01271E+04	-7.27596E-11	4.42057E+02	-3.62852E+00	3.51468E+03	2.35857E+00 BEAMG
33	33 JR	100.0	-1.01271E+04	7.27596E-11	-4.42057E+02	3.62852E+00	-5.41994E+03	-2.35857E+00
34	34 JA	0.0	-6.61700E+03	-4.63500E+03	-4.63500E+03	0.	1.12824E+05	-1.12824E+05 PIPEG
34	34 JR	100.0	6.61700E+03	4.63500E+03	4.63500E+03	0.	-4.79335E+04	4.79335E+04
35	35 JA	0.0	-2.20900E+03	-1.70400E+03	-1.70400E+03	4.65661E-10	4.79335E+04	-4.79335E+04 PIPEG
35	35 JR	100.0	2.20900E+03	1.70400E+03	1.70400E+03	-4.65661E-10	4.65661E-10	0.
36	36 JA	0.0	2.73340E+04	4.14024E+03	4.14024E+03	-5.75376E+04	-1.25517E+05	1.25517E+05 PIPEG
36	36 JR	100.0	-2.73340E+04	-4.14024E+03	-4.14024E+03	5.75376E+04	5.58781E+04	-5.56781E+04
37	37 JA	0.0	-2.62840E+04	-1.81602E+03	-1.81602E+03	-1.74518E+04	6.68479E+04	-6.68479E+04 PIPEG
37	37 JR	100.0	2.62840E+04	1.81602E+03	1.81602E+03	1.74518E+04	-4.65359E+04	4.65359E+04
38	38 JA	0.0	1.64265E+04	2.19495E+02	-1.20425E+03	1.90751E+02	2.87739E+04	6.16257E+03 BEAMG
38	38 JR	100.0	-1.64265E+04	-2.19495E+02	1.20425E+03	-1.90751E+02	4.57471E+03	-8.42101E+01
39	39 JA	0.0	1.64265E+04	-1.16415E-10	-1.20425E+03	1.29611E+02	-4.57685E+03	8.42101E+01 BEAMG
39	39 JR	100.0	-1.64265E+04	1.16415E-10	1.20425E+03	-1.29611E+02	9.76716E+03	-8.42101E+01
40	41 JA	0.0	-1.64265E+04	-2.19495E+02	-1.20425E+03	1.90751E+02	2.87739E+04	-6.16257E+03 BEAMG
40	41 JR	100.0	1.64265E+04	2.19495E+02	1.20425E+03	-1.90751E+02	4.57471E+03	8.42101E+01
41	41 JA	0.0	-1.54230E+04	8.73115E-11	-1.20425E+03	1.29611E+02	-4.57685E+03	-8.42101E+01 BEAMG
41	41 JR	100.0	1.64265E+04	-8.73115E-11	1.20425E+03	-1.29611E+02	9.76716E+03	8.42101E+01

A.3.21

A.3.2

39	JA	0.0	1.64240E+04	-1.16415E+10	-1.20425E+03	29611E+02	-4.57685E+03	8.42101E+01	BEAMG	
40	JB	100.0	-1.64240E+04	1.16415E+10	1.20425E+03	29611E+02	9.76716E+03	-8.42101E+01		
-0	11	JA	0.0	-1.64255E+04	-2.19475E+02	-1.20425E+03	1.90751E+02	2.87739E+04	-6.16257E+03	BEAMG
-0	41	JB	100.0	1.64255E+04	2.19495E+02	1.20425E+03	-1.90751E+02	4.57471E+03	8.42101E+01	
-1	41	JA	0.0	-1.64280E+04	8.73115E-11	-1.20425E+03	1.24611E+02	-4.57685E+03	-8.42101E+01	BEAMG
-1	42	JB	100.0	1.64280E+04	-8.73115E-11	1.20425E+03	-1.24611E+02	9.76716E+03	8.42101E+01	

EARTHQUAKE 2

MAXIMUM LOAD SUMMARY FOR

AXIAL P	BEAM ELEMENT LOADS	FOR OUTPUT VECTOR 6		
SHEAR V2	SHEAR V3	TORSION M1	BENDING M2	BENDING M3

MAXIMUM BEAM LOADS = 2.62840E+04 1.87364E+04 9.86100E+03 5.75376E+04 4.33573E+05 5.16080E+05
 BEAM NOS. = 37. 15. 4. 36. 8. 22.

MINIMUM BEAM LOADS = -2.73380E+04 -1.87364E+04 -9.86100E+03 -5.75376E+04 -4.26835E+05 -5.16080E+05
 BEAM NOS. = 36. 15. 8. 36. 11. 15.

A.3-23

EARTHQUAKE 2

BE#1	--NODES--	B E A M	E N O	L O A D S	IN GLOBAL SYSTEM	FOR OUTPUT VECTOR	6
		FX1	FX2	FX3	MX1	MX2	MX3
1	JA 1	-435E+04	.435E+04	-.564E+04	.373E-07	-.298E-07	0.
	JB 4	.435E+04	-.435E+04	.564E+04	.123E+06	.123E+06	0.
2	JA 3	.764E-09	-.186E-08	.259E-09	.931E-09	.931E-09	-.323E-08
	JB 2	-.744E-09	.156E-08	-.259E-09	.210E-08	-.331E-09	-.355E-08
3	JA 3	.132E-07	-.149E-07	.320E-08	.596E-07	0.	-.149E-07
	JB 4	-.132E-07	.179E-07	-.320E-08	-.596E-07	0.	.298E-06
4	JA 4	.833E-09	-.373E-07	.116E-07	.179E-06	.149E-06	-.171E-06
	JB 5	-.833E-08	.373E-07	-.116E-07	-.417E-06	-.149E-06	.343E-06
5	JA 5	.302E-09	-.233E-08	-.800E-10	.116E-06	.698E-09	-.698E-09
	JB 6	-.302E-09	.233E-08	.800E-10	0.	-.698E-09	.192E-08
6	JA 4	-.435E+04	.435E+04	-.504E+04	-.123E+06	-.123E+06	.186E-07
	JB 7	.435E+04	-.435E+04	.504E+04	.220E+06	.220E+06	-.186E-07
7	JA 7	-.780E+04	.780E+04	-.124E+05	-.220E+06	-.220E+06	.354E-07
	JB 8	.780E+04	-.780E+04	.124E+05	.296E+06	.296E+06	-.354E-07
8	JA 8	-.980E+04	.980E+04	-.166E+05	-.296E+06	-.296E+06	.224E-07
	JB 11	.980E+04	-.980E+04	.166E+05	.434E+06	.434E+05	-.224E-07
9	JA 10	.113E-08	-.733E-10	.643E-09	.518E-08	.865E-08	-.497E-08
	JB 9	-.113E-08	.733E-10	-.643E-09	-.226E-08	-.116E-07	.256E-08
10	JA 10	.358E-08	-.617E-09	-.635E-08	-.508E-07	.177E-06	.149E-07
	JB 11	-.358E-08	.617E-09	.635E-08	.184E-06	-.310E-06	.298E-07
11	JA 11	.777E+04	-.777E+04	-.166E+05	-.427E+06	-.427E+06	.575E+05
	JB 12	-.777E+04	.777E+04	.166E+05	.318E+06	.318E+06	-.575E+05
12	JA 12	.414E+04	-.414E+04	-.273E+05	-.318E+06	-.318E+06	.575E+05
	JB 37	-.414E+04	.414E+04	.273E+05	.126E+06	.126E+06	-.575E+05
13	JA 13	-.947E+02	.243E+04	.187E+05	-.958E+05	-.450E+03	-.330E+04
	JB 14	.947E+02	-.243E+04	-.187E+05	.835E+05	-.287E+02	.330E+04
14	JA 15	.947E+02	-.243E+04	-.187E+05	-.945E+05	.237E+02	.240E+04
	JB 14	-.947E+02	.243E+04	.187E+05	.835E+05	.287E+02	-.330E+04
15	JA 15	-.947E+02	.243E+04	.187E+05	.945E+05	.287E+02	-.240E+04
	JB 16	.947E+02	-.243E+04	-.187E+05	-.510E+06	-.287E+02	.270E+03
16	JA 16	.626E+03	-.247E+04	-.146E+05	.193E+06	-.287E+02	.198E+05
	JB 17	-.626E+03	.247E+04	.146E+05	-.601E+05	.297E+02	-.568E+04
17	JA 17	.626E+03	-.247E+04	-.146E+05	.601E+05	-.287E+02	.568E+04
	JB 18	-.626E+03	.247E+04	.146E+05	-.806E+05	.287E+02	-.269E+03
18	JA 19	.626E+03	-.247E+04	-.146E+05	.601E+05	.314E+04	.269E+03
	JB 18	-.626E+03	.247E+04	.146E+05	-.806E+05	-.287E+02	-.269E+03
19	JA 20	-.247E+04	.947E+02	.146E+05	-.450E+03	.681E+05	-.330E+04
	JB 21	.247E+04	-.947E+02	-.146E+05	-.287E+02	-.806E+05	.330E+04
20	JA 22	.247E+04	-.947E+02	-.146E+05	-.287E+02	.601E+05	.240E+04

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	JA	14	-164E+03	.247E+04	.140E+05	.805E+05	.287E+02	.269E+03
	JA	15	-164E+03	.247E+04	.140E+05	.601E+05	-.314E+04	.269E+03
	JB	15	-164E+03	-.247E+04	-.140E+05	-.805E+05	-.287E+02	-.269E+03
19	JA	20	-.247E+04	.947E+02	.140E+05	.450E+03	.681E+05	-.330E+04
	JB	21	-.247E+04	-.947E+02	-.140E+05	-.207E+02	-.800E+05	-.330E+04
20	JA	22	.247E+04	-.947E+02	-.140E+05	-.287E+02	.601E+05	.240E+04
	JB	21	-.247E+04	.947E+02	.140E+05	.287E+02	.806E+05	-.330E+04
21	JA	22	-.247E+04	.947E+02	.148E+05	.287E+02	-.601E+05	.240E+04
	JB	16	.247E+04	-.947E+02	-.148E+05	-.287E+02	.393E+05	-.270E+03
22	JA	16	.243E+04	-.626E+03	-.187E+05	-.207E+02	.516E+06	.198E+05
	JB	23	-.243E+04	.626E+03	.187E+05	.207E+02	.945E+05	-.568E+04
23	JA	23	.243E+04	-.626E+03	-.187E+05	-.207E+02	-.445E+05	.568E+04
	JB	24	-.243E+04	.626E+03	.187E+05	.207E+02	.839E+05	.269E+03
24	JA	25	-.243E+04	.626E+03	.187E+05	.314E+04	.958E+05	.269E+03
	JB	24	.243E+04	-.626E+03	-.187E+05	-.287E+02	.815E+05	-.269E+03
25	JA	38	-.182E+04	.182E+04	.263E+05	.465E+05	.465E+05	.175E+05
	JB	26	.182E+04	-.182E+04	-.263E+05	.774E+05	.774E+05	-.175E+05
26	JA	26	-.145E+04	-.145E+04	-.145E+05	-.774E+05	-.774E+05	.175E+05
	JB	27	.145E+04	.145E+04	-.145E+05	-.298E+05	-.298E+05	-.175E+05
27	JA	27	.593E+04	-.593E+04	.662E+04	.298E+05	.298E+05	.175E+05
	JB	30	-.593E+04	.593E+04	-.662E+04	-.113E+06	-.113E+06	-.175E+05
28	JA	29	-.313E-09	-.117E-08	-.297E-08	-.518E-08	-.313E-08	.448E-08
	JB	28	.313E-09	-.117E-08	-.297E-08	-.107E-07	-.128E-07	.233E-09
29	JA	29	.247E-08	.115E-08	.115E-07	.150E-07	.180E-06	-.373E-08
	JB	30	-.247E-08	-.115E-08	-.115E-07	.216E-06	.505E-07	-.671E-07
30	JA	30	-.101E+05	-.442E+03	-.118E-07	.363E+01	.236E+01	.873E+04
	JB	31	.101E+05	.442E+03	-.118E-07	-.363E+01	-.236E+01	.351E+04
31	JA	31	.101E+05	-.442E+03	.160E-09	.363E+01	.236E+01	-.351E+04
	JB	32	-.101E+05	.442E+03	-.160E-09	-.363E+01	-.236E+01	.542E+04
32	JA	30	-.442E+03	-.101E+05	-.233E-07	.236E+01	.363E+01	.873E+04
	JB	33	.442E+03	.101E+05	-.233E-07	-.236E+01	-.363E+01	.351E+04
33	JA	33	.442E+03	-.101E+05	.728E-10	.236E+01	.363E+01	-.351E+04
	JB	34	-.442E+03	.101E+05	-.728E-10	-.236E+01	-.363E+01	.542E+04
34	JA	30	-.463E+04	.463E+04	.662E+04	.113E+06	.113E+06	0.
	JB	35	.463E+04	-.463E+04	-.662E+04	-.479E+05	-.479E+05	0.
35	JA	35	-.170E+04	.170E+04	.221E+04	.479E+05	.479E+05	-.466E-09
	JB	36	.170E+04	-.170E+04	-.221E+04	.406E-09	0.	.466E-09
36	JA	37	.414E+04	-.414E+04	-.273E+05	.126E+06	-.126E+06	.575E+05
	JB	16	-.414E+04	.414E+04	.273E+05	.559E+05	.559E+05	-.575E+05
37	JA	16	-.182E+04	.182E+04	.263E+05	.668E+05	.668E+05	.175E+05
	JB	38	.182E+04	-.182E+04	-.263E+05	-.405E+05	-.465E+05	-.175E+05
38	JA	11	-.164E+05	-.120E+04	-.638E-09	-.575E+03	.616E+04	.288E+05
	JB	39	.164E+05	.120E+04	.638E-09	.130E+03	.842E+02	-.458E+04
39	JA	39	-.164E+05	.120E+04	.116E-09	-.130E+03	-.842E+02	.458E+04
	JB	40	.164E+05	-.120E+04	-.116E-09	.130E+03	.842E+02	-.977E+04
40	JA	11	-.120E+04	.120E+05	.134E-07	-.616E+04	-.575E+03	.288E+05
	JB	41	.120E+04	-.120E+05	-.134E-07	.842E+02	.130E+03	.458E+04
+1	JA	41	-.120E+04	.120E+05	.104E+05	-.479E-10	-.42E+02	-.130E+03
	JB	42	.120E+04	-.120E+05	-.104E+05	-.873E-10	-.42E+02	-.130E+03

A.3-24

TAKING ALL STRESSES AS SHEAR

$$\tau = \frac{P}{A} + \frac{V_3}{A} + \frac{M_2 C_3}{I_2} + \frac{M_3 C_2}{I_3}$$

NOTE: M_T IS NEGLECTED DUE TO ITS SMALL VALUE

$$\tau = \frac{41878}{14.82} + \frac{7213}{14.82} + \frac{26705(23535)}{18.13} + \frac{235(66535)}{356}$$

$$\tau = 6784 < 21000 \text{ psi}$$

∴ WELD OK.

9.4 BOLT STRESS CALCULATION

SUPPORT BOLTS UNDER COMBINED LOADING

ARE SUBJECT TO THE FOLLOWING STRESS

LIMITS OF PARA XVII - 2460, REF(9)

$$\sigma_t \leq 50.0 - 1.6 \gamma \leq 40.0 \text{ ksi}$$

$$\left. \begin{array}{l} \gamma \leq .19 S_y \\ \sigma_t \leq .5 S_y \end{array} \right\} \begin{array}{l} \text{FOR } 1\frac{1}{4}'' \text{ A-325 BOLTS} \\ (\sigma_t \leq .44 S_y \text{ FOR } \frac{1}{8}'' \text{ BOLTS}) \end{array}$$

$$S_y = 81,000 \text{ psi} \quad \text{REF (9) P.128}$$

TABLE I-7.3

THE STRESSES ARE BASED ON THE

NOMINAL AREA OF THE BOLT.

1.25" BOLT

$$\text{AREA} = 1.227 \text{ in}^2$$

.875" BOLT

$$\text{AREA} = .601 \text{ in}^2$$

SUPPORT BOLT STRESSES

THE FOLLOWING LOADS WERE EXTRACTED
FROM "COMBINE" FOR THE BOLT BEAMS,

BAMS 13, 15, 19, 21 AT POINTS 13, 19, 20 & 25 RESPECTIVELY

	P	V ₂	V ₃	M _T	M ₂	M ₃
EQL	35268	7979	1693	9154	8552	204290
EQL	38149	7721	1816	9503	9119	205600

The maximum load of each category is used.

BOLT STRESSES

SHEAR STRESS

$$\gamma = \frac{(V_2^2 + V_3^2)^{\frac{1}{2}}}{4A} + \frac{M_r}{4RA}$$

$$R = \frac{1}{2} ((6)^2 + 5.5^2)^{\frac{1}{2}}$$

$$R = 4.67 \text{ in}$$

$$\gamma = \frac{(7979^2 + 1616^2)^{\frac{1}{2}}}{4(1.227)} + \frac{9503}{4(4.67)(1.227)}$$

$$\gamma = 2143 \text{ psi} < .19 S_y = 15390 \text{ psi}$$

OK

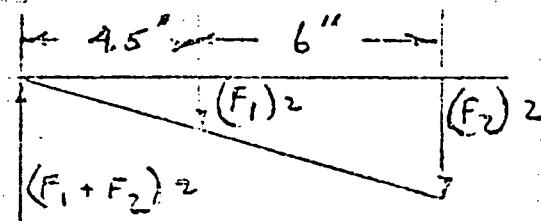
AXIAL STRESS

ASSUME P ACTS AS A TENSILE FORCE

$$\sigma_p = \frac{38194}{4A} = 7772 \text{ psi}$$

AXIAL TENSILE STRESS DUE TO M₂ASSUME THAT M₂ IS TAKEN OUT

BY THE TWO COUPLES AS SHOWN BELOW:



ASSUME LINEAR FORCE DISTRIBUTION

OR

$$F_1 = \frac{9.5}{10.5} F_2$$

$$M_2 = 2F_1(4.5) + 2F_2(10.5)$$

$$M_2 = \frac{2}{10} F_2 (9.5)^2 + 21(F_2) = 24.86 F_2$$

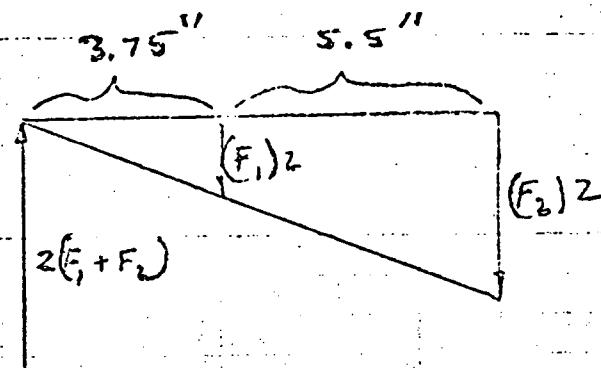
$$F_2 = \frac{9119}{24.86} = 366 \text{ LBS/BOLT}$$

$$\sigma_{M_2} = \frac{366}{1.227} = 298 \text{ psi}$$

AXIAL TENSILE STRESS DUE TO M_3

ASSUME THAT M_3 IS TAKEN OUT.

BY THE TWO COUPLES AS SHOWN BELOW:



ASSUME LINEAR
FORCE DISTRIBUTION

OR

$$F_1 = \frac{3.75}{9.25} F_2$$

$$\therefore M_3 = 2F_1(3.75) + 2F_2(9.25)$$

$$M_3 = 2F_2 \frac{(3.75)^2}{9.25} + 2F_2(9.25) = 21.54 F_2$$

$$\therefore F_2 = \frac{205600}{21.54} = 9545 \text{ LBS} \quad \sigma_{M_3} = 7779 \text{ psi}$$

\therefore TOTAL AXIAL STRESS.

$$\sigma_t = \sigma_p + \sigma_{M_2} + \sigma_{M_3} = 15848 \text{ psi}$$

$$\sigma_t = 15848 \text{ psi} < .5 S_y = 40500 \text{ psi}$$

\therefore OK

TOTAL COMPARISON

$$\sigma_t \leq 50.0 - 1.6 T \leq 40.0 \text{ ksi}$$

$$15848 \leq 40000 \text{ psi} \quad \therefore \text{BOLTS ARE ADEQUATE}$$

$$(40 \leq 50 - 1.6 T)$$

SEISMIC LUG BOLT STRESSES

THE FOLLOWING LOADS WERE EXTRACTED FROM "COMBINE" FOR THE SEISMIC LUG BOLTS, BEAMS 31, 33, 39 & 41, NODES 32, 34, 40, & 42 RESPECTIVELY. THE MOMENTS M_1 & M_2 WILL NOT BE CONSIDERED AS BOLT LOADS AS THEY WILL BE TAKEN OUT BY THE ATTACHMENT PLATES.

 Σ LOADS

	P	V_3	M_3
EQ1	41878	7213	235
EQ2	36847	7030	234

THE MAXIMUM LOADS ARE FROM EARTHQUAKE 1 Σ STRESSES

SHEAR STRESS

$$\tau = \frac{P}{2A} + \frac{V_3}{2A} + \frac{M_3}{bA}$$

M_3 TAKEN OUT AS MOMENT

$$\tau = \frac{41878}{2(.601)} + \frac{7213}{2(.601)} + \frac{235}{4(.601)}$$

$$\tau = 40906 \text{ psi} > 15390 \text{ psi } \text{LARGER BOLTS REQUIRED}$$

Σ TRY $1\frac{1}{2}$ " BOLTS AREA = 1.767 in^2

$$\therefore \tau = 40906 \frac{(601)}{(1.767)} = 13911 < 15390 \text{ psi.}$$

Appendix A

STARDYNE COMPUTER OUTPUT

This section contains the following output:

- A.1 Geometry
- A.2 "HQR" Output
- A.3 "STATIC" Output

Appendix A.1

GEOMETRY

*** STARDYNE 3.0 INPUT ***

CARD NO	CARD IMAGE								CARD TYPE
	1	4	8	12	16	20	24	28	
1
2	EFCO SHUTDOWN HEAT EXCHANGER TYPE.CEU								EF
3	MATLG	1CS	250	F	27.55	+6			MATLG
4		2SS	400	F	26.6	+6			MATLG
5		3 CS	400	F	27.0	+6			END
6	END								
7	NODE	1	0.0000		0.00000	361.00			NODE
8		2	0.0000		32.7500	332.75			NODE
9		3	0.0000		23.690	332.75			NODE
10		4	0.0000		0.00000	332.75			NODE
11		5	0.0000		-23.690	332.75			NODE
12		6	0.0000		-32.750	332.75			NODE
13		7	0.0000		0.00000	310.50			NODE
14		8	0.0000		0.00000	300.88			NODE
15		9	25.460		25.4600	286.88			NODE
16		10	19.93		19.93	296.88			NODE
17		11	0.0000		0.00000	286.88			NODE
18		12	0.0000		0.00000	272.88			NODE
19		13	0.0000		32.0000	204.50			NODE
20		14	0.0000		32.0000	209.56			NODE
21		15	0.0000		22.5000	209.56			NODE
22		16	0.0000		0.00000	209.56			NODE
23		17	0.0000		-22.500	209.56			NODE
24		18	0.0000		-32.000	209.56			NODE
25		19	0.0000		-32.000	204.50			NODE
26		20	32.000		0.00000	204.50			NODE
27		21	32.000		0.00000	209.56			NODE
28		22	22.500		0.00000	209.56			NODE
29		23	-22.50		0.00000	209.56			NODE
30		24	-32.00		0.00000	209.56			NODE
31		25	-32.00		0.00000	204.50			NODE
32		26	0.0000		0.00000	130.19			NODE
33		27	0.0000		0.00000	56.130			NODE
34		28	25.460		-25.460	42.130			NODE
35		29	19.930		-19.930	42.130			NODE
36		30	0.0000		0.00000	42.130			NODE
37		31	-27.69		0.00000	42.130			NODE
38		32	-32.00		0.00000	42.130			NODE
39		33	0.0000		-27.690	42.130			NODE
40		34	0.0000		-32.000	42.130			NODE
41		35	0.0000		0.00000	28.130			NODE
42		36	0.0000		0.00000	0.0000			NODE
43		37	0.0000		0.00000	226.38			NODE
44		38	0.0000		0.00000	198.38			NODE
45		39	-27.69		0.0000	287.25			NODE
46		40	-32.00		0.0000	287.25			NODE
47		41	0.0000		-27.69	287.25			NODE
48		42	0.0000		-32.00	287.25			END
49	END								
50	RESTG	13		111111					RESTG
51		19		111111					RESTG
52		20		111111					RESTG
53		25		111111					RESTG
54		32		11.1111					RESTG

A.1-1

51 17
 52 20 111111
 53 25 111111
 54 32 111111

RESTG
 RESTG
 RESTG

A.1-2

*** STARDYNE 3.0 INPUT ***

CARD IMAGE

	1	4	8	12	16	20	24	28	32	36	40	44	48	52	56	60	64	68	72	76	80	
CARD NO	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	CARD TYPE
55		34			11	1111																RESTG
56		40			11	1111																RESTG
57		42			11	1111																END
58	END																					WGHT
59	WGHT	1	5131.		5131.		5131.															WGHT
60		7	6108.		6108.		6108.															WGHT
61		8	3822.		3822.		3822.															WGHT
62		12	9792.		9792.		9792.															WGHT
63		16	12252.		12252.		12252.															WGHT
64		26	10593.		10593.		10593.															WGHT
65		27	7286.		7286.		7286.															WGHT
66		35	4007.		4007.		4007.															WGHT
67		36	2008.		2008.		2008.															END
68	END																					PIPEG
69	PIPEG	1		1	4		20	3	2													PIPEG
70		2		3	2		36	2	3													PIPEG
71	BEAMG	3		3	4		36	1	1													REAMG
72		4		5	5		36	1	1													BEAMG
73	PIPEG	5		5	6		36	2	3													PIPEG
74		6		4	7		20	3	2													PIPEG
75		7		7	8		20	1	4													PIPEG
76		8		8	11		20	1	5													PIPEG
77		9		10	9		36	1	6													BEAMG
78	BEAMG	10		10	11		36	1	1													PIPEG
79	PIPEG	11		11	12		20	1	5													PIPEG
80		12		12	37		20	1	4													PIPEG
81	BEAMG	13		13	14		36	1	1													BEAMG
82		14		15	14		36	1	7													BEAMG
83		15		15	16		36	1	1													BEAMG
84		16		16	17		36	1	1													BEAMG
85		17		17	18		36	1	7													BEAMG
86		18		19	18		36	1	1													BEAMG
87		19		20	21		36	1	1													BEAMG
88		20		22	21		36	1	7													BEAMG
89		21		22	16		36	1	1													BEAMG
90		22		16	23		36	1	1													BEAMG
91		23		23	24		36	1	7													HEAMG
92		24		25	24		36	1	1													PIPEG
93	PIPEG	25		38	26		20	1	4													PIPEG
94		26		26	27		20	1	4													PIPEG
95		27		27	30		20	1	5													PIPEG
96		28		29	28		36	1	6													BEAMG
97	BEAMG	29		29	30		36	1	1													BEAMG
98		30		30	31		36	1	1													BEAMG
99		31		31	32		36	1	8													BEAMG
100		32		30	33		36	1	1													BEAMG
101		33		33	34		36	1	8													BEAMG
102	PIPEG	34		30	35		20	1	5													PIPEG
103		35		35	30		20	1	4													PIPEG
104		36		37	10		20	1	9													PIPEG
105		37		16	38		20	1	9													PIPEG
106	BEAMG	38		11	39		36	1	1													BEAMG
107		39		39	40		36	1	8													BEAMG
108		40		11	41		36	1	1													BEAMG

A.1-2

105 37 10 3d 60 1 9
 106 BEAMG 38 11 39 36 1 1
 107 39 39 40 36 1 8
 108 40 11 41 36 1 1

PIPEG
 BEAMG
 BEAMG
 BEAMG

A.1.6

*** STARDYNE 3.0 INPUT ***

CARD IMAGE

1 4 8 12 16 20 24 28 32 36 40 44 48 52 56 60 64 68 72 76 80

CARD NO	CARD TYPE
109	BEAMG
110 END	END
111 BPROP1	BPROP
112 7 34.29	BPROP
113 8.9.0	BPROP
114 BPROP2	BPROP
115 7 9.925	BPROP
116 8 6.0	BPROP
117 BPROP3	BPROP
118 3 12.75	BPROP
119 4.45.	BPROP
120 5 55.	BPROP
121 6 16.	BPROP
122 9 46.	BPROP
123 END	END
124 ENGEOM	ENGE

A.1.3

TAPE2 CREATION DATE 10/16/75, TIME 16.15.41, STAR 3.0 VERSION AUGC28

EFCO SHUTDOWN HEAT EXCHANGER TYPE CEU

GEOMETRY PROCESSING OPTIONS---

GEOMETRY INPUT FILE (INFILE) = 0
ACCELERATION OF GRAVITY (G) = .3864000E+03
DOF PER NODE (JDOF) = 6
NODE REDRUE (IRENUM) = -0.0
GEOMETRY PLOTS (IGEOMP) = 0
DEFORMED PLOTS (IVECTP) = 0
PLOT VIEW SELECTOR (IPVIEW) = 0
PLUTTER TYPE (PLTYPE) =
PLOT SYMBOL (IPSYM) = 0
CALCOMP PLOT SIZE (IPSIZE) = 1.0

***** MATERIAL PROPERTY TABLE *****

---MATERIAL---		MODULUS OF ELASTICITY E1/E2	POISSONS RATIO PRI/PR2	SHEAR MODULUS G	DENSITY	COEFFICIENT OF THERMAL EXPANSION ALPH1/ALPH2	DAMPING COEFFICIENT
MATL	1 CS 250 F	2.755000E+07 2.755000E+07	3.000000E-01 3.000000E-01	1.059615E+07	-0.	-0. -0.	-0.
MATL	2 SS 400 F	2.660000E+07 2.660000E+07	3.000000E-01 3.000000E-01	1.023077E+07	-0.	-0. -0.	-0.
MATL	3 CS 400 F	2.700000E+07 2.700000E+07	3.000000E-01 3.000000E-01	1.038462E+07	-0.	-0. -0.	-0.

*** NODAL COORDINATE TABLE ***

	NODE	X1	X2	X3
	NUDES	1	0.	0.
	NUDES	2	0.	.3275000E+02
	NUDES	3	0.	.2369000E+02
	NUDES	4	0.	0.
	NUDES	5	0.	-.2369000E+02
	NUDES	6	0.	-.3275000E+02
	NUDES	7	0.	0.
	NUDES	8	0.	.3008800E+03
	NUDES	9	.2546000E+02	.2546000E+02
	NUDES	10	.1993000E+02	.1993000E+02
	NUDES	11	0.	0.
	NUDES	12	0.	.2728800E+03
	NUDES	13	0.	.3200000E+02
	NUDES	14	0.	.3200000E+02
	NUDES	15	0.	.2250000E+02
	NUDES	16	0.	0.
	NUDES	17	0.	-.2250000E+02
	NUDES	18	0.	-.3200000E+02
	NUDES	19	0.	-.3200000E+02
	NUDES	20	.3200000E+02	0.
	NUDES	21	.3200000E+02	0.
	NUDES	22	.2250000E+02	0.
	NUDES	23	-.2250000E+02	0.
	NUDES	24	-.3200000E+02	0.
	NUDES	25	-.3200000E+02	0.
	NUDES	26	0.	0.
	NUDES	27	0.	0.
	NUDES	28	.2546000E+02	-.2546000E+02
	NUDES	29	.1993000E+02	-.1993000E+02
	NUDES	30	0.	0.
	NUDES	31	-.2769000E+02	0.
	NUDES	32	-.3200000E+02	0.
	NUDES	33	0.	.2769000E+02
	NUDES	34	0.	-.3200000E+02
	NUDES	35	0.	0.
	NUDES	36	0.	0.
	NUDES	37	0.	0.
	NUDES	38	0.	.1983800E+03
	NUDES	39	-.2769000E+02	0.
	NUDES	40	-.3200000E+02	0.
	NUDES	41	0.	-.2769000E+02
	NUDES	42	0.	-.3200000E+02

--- MAXIMUM ALLOWABLE NODE NUMBER BY ANALYSIS TYPE ---

STAR STATIC	2500
STAR HLR	1606
STAR INVITER.	1300
STAR SUBSTRUCT.	2500
DYNRE 1	1606
DYNRE 2	1300
DYNRE 3	300
DYNRE 4	1606
DYNRE 5	1300

A.1-5

STAR SUBSTRUCT. 2500
DYNRE 1 1600
DYNRE 2 1300
DYNRE 3 300
DYNRE 4 1600
DYNRE 5 1300

LARGEST NODE NUMBER CODED IN THIS MODEL = 42

NEXT TABLE HEADER INESTG

A.1-6

*** NUDAL RESTRAINT TABLE ***

	NODE	X1	X2	X3	X4	X5	X6
RESTRAINTS	13	1	1	1	1	1	1
RESTRAINTS	19	1	1	1	1	1	1
RESTRAINTS	20	1	1	1	1	1	1
RESTRAINTS	25	1	1	1	1	1	1
RESTRAINTS	32	1	1	0	1	1	1
RESTRAINTS	34	1	1	0	1	1	1
RESTRAINTS	40	1	1	0	1	1	1
RESTRAINTS	42	1	1	0	1	1	1

NEXT TABLE HEADER (WHT)

A.1-7

*** INPUT NODAL WEIGHT TABLE ***

NODE	W1	W2	W3	W4	W5	W6
WEIGHTS 1	.51310E+04	.51310E+04	.51310E+04	0.	0.	0.
WEIGHTS 7	.61080E+04	.61080E+04	.61080E+04	0.	0.	0.
WEIGHTS 8	.38220E+04	.38220E+04	.38220E+04	0.	0.	0.
WEIGHTS 12	.97920E+04	.97920E+04	.97920E+04	0.	0.	0.
WEIGHTS 16	.12252E+05	.12252E+05	.12252E+05	0.	0.	0.
WEIGHTS 26	.10593E+05	.10593E+05	.10593E+05	0.	0.	0.
WEIGHTS 27	.72860E+04	.72860E+04	.72860E+04	0.	0.	0.
WEIGHTS 35	.40070E+04	.40070E+04	.40070E+04	0.	0.	0.
WEIGHTS 36	.20080E+04	.20080E+04	.20080E+04	0.	0.	0.
SUMMATION	.60999E+05	.60999E+05	.60999E+05	0.	0.	0.

NEXT TABLE HEADER (PIPEG)

A.1-8

*** BEAM SECTION PROPERTY TABLE ***

	BPROP1=	A	J	I2	I3	SF2	SF3	
	BPROP2=	H2	H3	CTORS	SSF2	SSF3	DIST	WGHT
	BPROP3=	CD	T	RADIUS	FLEX FLAG	L10 DENS	DIST	WGHT
	BPROP4=	XOFFA	YOFFA	ZOFFA	XOFFB	YOFFB	ZOFFB	
	BPROP5=	SYA	SZA	SYB	SZB	SYC	ZSC	
NUMBER								
1	BPROP1	5.000000E+02	4.000000E+05	2.000000E+05	2.000000E+05	1.000000E+00	1.000000E+00	
7	BPROP1	3.429000E+01	7.320000E+00	1.176000E+03	8.070000E+02	3.380000E-01	6.620000E-01	
8	BPROP1	9.000000E+00	1.688000E+00	1.080000E+02	4.220000E-01	0.	8.330000E-01	
1	BPROP2	1.000000E+00	1.000000E+00	1.000000E+00	1.000000E+00	1.000000E+00	-0.	
7	BPROP2	9.925000E+00	7.500000E+00	8.750000E-01	1.000000E+00	1.000000E+00	-0.	
8	BPROP2	6.000000E+00	3.750000E-01	7.500000E-01	1.000000E+00	1.000000E+00	-0.	
2	BPROP3	4.675000E+01	1.250000E+00	-0.	-0.	-0.	-0.	
3	BPROP3	1.275000E+01	3.300000E-01	-0.	-0.	-0.	-0.	
4	BPROP3	4.500000E+01	5.000000E-01	-0.	-0.	-0.	-0.	
5	BPROP3	5.600000E+01	6.250000E-01	-0.	-0.	-0.	-0.	
6	BPROP3	1.600000E+01	5.000000E-01	-0.	-0.	-0.	-0.	
9	BPROP3	4.600000E+01	1.000000E+00	-0.	-0.	-0.	-0.	

A.1-9

*** BEAM CONNECTIVITY TABLE ***

	NO	JA	JB	JC	MATL	BPRP	PIN	H2/ NO.	H3/ NO.	LENGTH OU	AREA T	J	I2	I3	SF2	SF3	
	PIPEG	1	1	4	20	3	2	000000	4.675E+01	1.250E+00	2.825E+01	1.787E+02	9.255E+04	4.627E+04	4.627E+04	.511	.511
	PIPEG	2	3	2	36	2	3	000000	1.275E+01	3.300E-01	9.060E+00	1.288E+01	4.969E+02	2.485E+02	2.485E+02	.511	.511
	BEAMG	3	3	4	36	1	1	000000	1.000E+00	1.000E+00	2.369E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	4	4	5	36	1	1	000000	1.000E+00	1.000E+00	2.369E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	PIPEG	5	5	6	36	2	3	000000	1.275E+01	3.300E+01	9.060E+00	1.288E+01	4.959E+02	2.485E+02	2.485E+02	.511	.511
	PIPEG	6	4	7	20	3	2	000000	4.675E+01	1.250E+00	2.225E+00	1.787E+02	9.255E+04	4.627E+04	4.627E+04	.511	.511
	PIPEG	7	7	8	20	1	4	000000	4.500E+01	5.000E+01	9.620E+00	6.990E+01	3.461E+04	1.730E+04	1.730E+04	.499	.499
	PIPEG	8	8	11	20	1	5	000000	5.600E+01	6.250E+01	1.400E+01	1.087E+02	8.336E+04	4.168E+04	4.168E+04	.499	.499
	PIPEG	9	10	9	36	1	6	000000	1.600E+01	5.000E+01	7.821E+00	2.435E+01	1.464E+03	7.319E+02	7.319E+02	.515	.515
	BEAMG	10	10	11	36	1	1	000000	1.000E+00	1.000E+00	2.819E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	PIPEG	11	11	12	20	1	5	000000	5.600E+01	6.250E+01	1.400E+01	1.087E+02	8.336E+04	4.168E+04	4.168E+04	.499	.499
	PIPEG	12	12	37	20	1	4	000000	4.500E+01	5.000E+01	4.650E+01	6.990E+01	3.461E+04	1.730E+04	1.730E+04	.499	.499
	BEAMG	13	13	14	36	1	1	000000	1.000E+00	1.000E+00	5.060E+00	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	14	15	14	36	1	7	000000	9.925E+00	7.500E+00	9.500E+00	3.429E+01	7.320E+00	1.176E+03	8.070E+02	.338	.562
	BEAMG	15	15	15	36	1	1	000000	1.000E+00	1.000E+00	2.250E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	16	16	17	36	1	1	000000	1.000E+00	1.000E+00	2.250E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	17	17	18	36	1	7	000000	9.925E+00	7.500E+00	9.500E+00	3.429E+01	7.320E+00	1.176E+03	8.070E+02	.338	.562
	BEAMG	18	19	18	36	1	1	000000	1.000E+00	1.000E+00	5.060E+00	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	19	20	21	36	1	1	000000	1.000E+00	1.000E+00	5.060E+00	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	20	22	21	36	1	7	000000	9.925E+00	7.500E+00	9.500E+00	3.429E+01	7.320E+00	1.176E+03	8.070E+02	.338	.562
	BEAMG	21	22	16	36	1	1	000000	1.000E+00	1.000E+00	2.250E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	22	16	23	36	1	1	000000	1.000E+00	1.000E+00	2.250E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	23	23	24	36	1	7	000000	9.925E+00	7.500E+00	9.500E+00	3.429E+01	7.320E+00	1.176E+03	8.070E+02	.338	.562
	BEAMG	24	25	24	36	1	1	000000	1.000E+00	1.000E+00	5.060E+00	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	PIPEG	25	38	26	20	1	4	000000	4.500E+01	5.000E+01	6.819E+01	6.990E+01	3.461E+04	1.730E+04	1.730E+04	.499	.499
	PIPEG	26	26	27	20	1	4	000000	4.500E+01	5.000E+01	7.406E+01	6.990E+01	3.461E+04	1.730E+04	1.730E+04	.499	.499
	PIPEG	27	27	30	20	1	5	000000	5.600E+01	6.250E+01	1.400E+01	1.087E+02	8.336E+04	4.168E+04	4.168E+04	.499	.499
	PIPEG	28	29	28	36	1	6	000000	1.600E+00	1.500E+00	2.812E+00	2.435E+01	1.464E+03	7.319E+02	7.319E+02	.515	.515
	BEAMG	29	29	30	36	1	1	000000	1.000E+00	1.000E+00	2.619E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	30	30	31	36	1	1	000000	1.000E+00	1.000E+00	2.769E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	31	31	32	36	1	8	000000	6.000E+00	3.750E+01	4.310E+00	9.000E+00	1.688E+00	1.080E+02	4.220E+01	0.000	.833
	BEAMG	32	30	33	36	1	1	000000	1.000E+00	1.000E+00	2.769E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	33	33	34	36	1	8	000000	6.000E+00	3.750E+01	4.310E+00	9.000E+00	1.688E+00	1.080E+02	4.220E+01	0.000	.833
	PIPEG	34	30	35	20	1	5	000000	5.600E+01	6.250E+01	1.400E+01	1.087E+02	8.336E+04	4.168E+04	4.168E+04	.499	.499
	PIPEG	35	35	36	20	1	4	000000	4.500E+01	5.000E+01	2.813E+01	6.990E+01	3.461E+04	1.730E+04	1.730E+04	.499	.499
	PIPEG	36	37	16	20	1	9	000000	4.600E+01	1.000E+00	1.626E+01	1.414E+02	7.160E+04	3.580E+04	3.580E+04	.507	.507
	PIPEG	37	16	38	20	1	9	000000	4.600E+01	1.000E+00	1.118E+01	1.414E+02	7.160E+04	3.580E+04	3.580E+04	.507	.507
	BEAMG	38	11	39	36	1	1	000000	1.000E+00	1.000E+00	2.769E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	39	39	40	36	1	8	000000	6.000E+00	3.750E+01	4.310E+00	9.000E+00	1.688E+00	1.080E+02	4.220E+01	0.000	.833
	BEAMG	40	11	41	36	1	1	000000	1.000E+00	1.000E+00	2.769E+01	5.000E+02	4.000E+05	2.000E+05	2.000E+05	1.000	1.000
	BEAMG	41	41	42	36	1	8	000000	6.000E+00	3.750E+01	4.310E+00	9.000E+00	1.688E+00	1.080E+02	4.220E+01	0.000	.833

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BEAM DATA TABLE 2

NO	WEIGHT	CTORS	SSF2	SSF3	ELBOW RADIUS	FLEXIBILITY FACTOR	ELBOW ANGLE	BEAM X2-DIR.COSINES		
								X1	X2	X3
PIPEG 1	0.	2.337E+01	1.999E+00	1.999E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 2	0.	6.375E+00	1.999E+00	1.999E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 3	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 4	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
PIPEG 5	0.	6.375E+00	1.999E+00	1.999E+00	0.	0.	0.	0.	0.	-1.000E+00
PIPEG 6	0.	2.337E+01	1.999E+00	1.999E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 7	0.	2.250E+01	2.000E+00	2.000E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 8	0.	2.400E+01	2.000E+00	2.000E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 9	0.	8.000E+00	1.999E+00	1.999E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 10	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
PIPEG 11	0.	2.600E+01	2.000E+00	2.000E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 12	0.	2.250E+01	2.000E+00	2.000E+00	0.	0.	0.	1.000E+00	0.	0.
BEAMG 13	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	-1.000E+00	0.
BEAMG 14	0.	8.750E-01	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 15	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 16	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 17	0.	8.750E-01	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 18	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	1.000E+00	0.
BEAMG 19	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	-1.000E+00	0.	0.
BEAMG 20	0.	8.750E-01	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 21	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 22	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 23	0.	8.750E-01	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 24	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 25	0.	2.250E+01	2.000E+00	2.000E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 26	0.	2.250E+01	2.000E+00	2.000E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 27	0.	2.800E+01	2.000E+00	2.000E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 28	0.	8.000E+00	1.999E+00	1.999E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 29	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 30	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 31	0.	7.500E-01	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 32	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 33	0.	7.500E-01	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
PIPEG 34	0.	2.800E+01	2.000E+00	2.000E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 35	0.	2.250E+01	2.000E+00	2.000E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 36	0.	2.300E+01	1.999E+00	1.999E+00	0.	0.	0.	1.000E+00	0.	0.
PIPEG 37	0.	2.300E+01	1.999E+00	1.999E+00	0.	0.	0.	1.000E+00	0.	0.
BEAMG 38	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	-1.335E-02	0.	-9.999E-01
BEAMG 39	0.	7.500E-01	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00
BEAMG 40	0.	1.000E+00	1.000E+00	1.000E+00	0.	0.	0.	0.	-1.335E-02	-9.999E-01
BEAMG 41	0.	7.500E-01	1.000E+00	1.000E+00	0.	0.	0.	0.	0.	-1.000E+00

NOTICE

- DEFAULT LOCATIONS FOR STRESS POINTS B AND C
- HAVE BEEN CHANGED FROM THOSE ON PAGE B1-120 TO
- (H2/2,0) FOR B AND (0,H3/2) FOR C. FOR PIPES,
- 00... IS USED INSTEAD OF H2 AND H3.

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BEAM DATA TABLE 3

BEAM C/L OFFSETS FROM NODES (GLOBAL)

USER SPECIFIED STRESS LOCATIONS (ELEMENT)

HEA4 NO	-- OFFSET AT A END -- X1	X2	X3	-- OFFSET AT B END -- X1	X2	X3	-- POINT A -- X1	X2	X3	-- POINT B -- X1	X2	X3	-- POINT C -- X1	X2	X3
PIPEG 1	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.337E+01	0.	0.	2.34E+01		
PIPEG 2	0.	0.	0.	0.	0.	0.	0.	0.	0.	6.375E+00	0.	0.	6.38E+00		
BEAMG 3	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 4	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
PIPEG 5	0.	0.	0.	0.	0.	0.	0.	0.	0.	6.375E+00	0.	0.	6.38E+00		
PIPEG 6	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.337E+01	0.	0.	2.34E+01		
PIPEG 7	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.250E+01	0.	0.	2.25E+01		
PIPEG 8	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.900E+01	0.	0.	2.80E+01		
PIPEG 9	0.	0.	0.	0.	0.	0.	0.	0.	0.	8.000E+00	0.	0.	8.00E+00		
BEAMG 10	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
PIPEG 11	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.800E+01	0.	0.	2.80E+01		
PIPEG 12	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.250E+01	0.	0.	2.25E+01		
BEAMG 13	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 14	0.	0.	0.	0.	0.	0.	0.	0.	0.	4.963E+00	0.	0.	3.75E+00		
BEAMG 15	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 16	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 17	0.	0.	0.	0.	0.	0.	0.	0.	0.	4.963E+00	0.	0.	3.75E+00		
BEAMG 18	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 19	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 20	0.	0.	0.	0.	0.	0.	0.	0.	0.	4.963E+00	0.	0.	3.75E+00		
BEAMG 21	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 22	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 23	0.	0.	0.	0.	0.	0.	0.	0.	0.	4.963E+00	0.	0.	3.75E+00		
BEAMG 24	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
PIPEG 25	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.250E+01	0.	0.	2.25E+01		
PIPEG 26	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.250E+01	0.	0.	2.25E+01		
PIPEG 27	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.800E+01	0.	0.	2.80E+01		
PIPEG 28	0.	0.	0.	0.	0.	0.	0.	0.	0.	8.000E+00	0.	0.	8.00E+00		
BEAMG 29	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 30	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 31	0.	0.	0.	0.	0.	0.	0.	0.	0.	3.000E+00	0.	0.	1.88E-01		
BEAMG 32	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 33	0.	0.	0.	0.	0.	0.	0.	0.	0.	3.000E+00	0.	0.	1.88E-01		
PIPEG 34	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.800E+01	0.	0.	2.80E+01		
PIPEG 35	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.250E+01	0.	0.	2.25E+01		
PIPEG 36	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.300E+01	0.	0.	2.30E+01		
PIPEG 37	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.300E+01	0.	0.	2.30E+01		
BEAMG 38	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 39	0.	0.	0.	0.	0.	0.	0.	0.	0.	3.000E+00	0.	0.	1.88E-01		
BEAMG 40	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.000E-01	0.	0.	5.00E-01		
BEAMG 41	0.	0.	0.	0.	0.	0.	0.	0.	0.	3.000E+00	0.	0.	1.88E-01		

*NEXT TABLE HEADER** (ENDMO)

XXXXXXXXXXXXXXXXXXXX END OF GEOMETRY DATA XXXXXXXXXXXXXXXXX

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*** FINAL WEIGHT SUMMARY ***
 (INCLUDES ELEMENT AND NODAL WEIGHTS)

NODE	W1	W2	W3	W4	W5	W6
WEIGHTS 1	.51310E+04	.51310E+04	.51310E+04	0.	0.	0.
WEIGHTS 7	.61080E+04	.61080E+04	.61080E+04	0.	0.	0.
WEIGHTS 8	.38220E+04	.38220E+04	.38220E+04	0.	0.	0.
WEIGHTS 12	.97920E+04	.97920E+04	.97920E+04	0.	0.	0.
WEIGHTS 16	.12252E+05	.12252E+05	.12252E+05	0.	0.	0.
WEIGHTS 26	.10593E+05	.10593E+05	.10593E+05	0.	0.	0.
WEIGHTS 27	.72860E+04	.72860E+04	.72860E+04	0.	0.	0.
WEIGHTS 35	.40070E+04	.40070E+04	.40070E+04	0.	0.	0.
WEIGHTS 36	.20080E+04	.20080E+04	.20080E+04	0.	0.	0.
SUMMATION	.60999E+05	.60999E+05	.60999E+05	0.	0.	0.

CENTER OF GRAVITY BASED ON X1 WEIGHTS ONLY.
 (WEIGHTS IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

$$\begin{aligned}X1 &= 0. \\X2 &= 0. \\X3 &= .197366206E+03\end{aligned}$$

CENTER OF GRAVITY BASED ON X2 WEIGHTS ONLY.
 (WEIGHTS IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

$$\begin{aligned}X1 &= 0. \\X2 &= 0. \\X3 &= .197366206E+03\end{aligned}$$

CENTER OF GRAVITY BASED ON X3 WEIGHTS ONLY.
 (WEIGHTS IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

$$\begin{aligned}X1 &= 0. \\X2 &= 0. \\X3 &= .197366206E+03\end{aligned}$$

A.1-13

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