

Calculation Cover Sheet

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1. Purpose

The purpose of this calculation is to document the Sequoyah Unit 2 pressurized water reactor (PWR) fuel depletion calculations performed as part of the commercial reactor critical (CRC) evaluation program. The CRC evaluations support the development and validation of the neutronics models used for criticality analyses involving commercial spent nuclear fuel in a geologic repository.

2. Method

The calculational method used to perform the Sequoyah Unit 2 fuel depletion calculations consisted of using the SAS2H control sequence of the SCALE, Version 4.3, code system (Ref. 7.1) to deplete the necessary fuel assemblies. The various fuel assemblies were depleted through their unique operating histories such that their modified fuel compositions would be available at specific exposure times corresponding to the times (statepoints) at which detailed core reactivity calculations would be performed. The fuel assembly depletion calculations were based on detailed core follow information for each assembly.

3. Assumptions

- 3.1** The inherent approximation of uniformly distributed non-fuel lattice cells in the Path B models of the SAS2H calculations as described in Section 5.4 was considered acceptable within the fidelity of these calculations. The basis for this assumption was provided in Section S2.2.3.1 of Volume 1, Rev. 5 in Reference 7.1. This assumption was used throughout all of the depletion calculations documented in Section 5.
- 3.2** With the utilization of one cross section update per irradiation time step in the SAS2H calculations, the maximum duration of any time step in any reactor cycle irradiation layout should have not exceeded 80 days. The basis for this assumption was that the 80 day irradiation time step limit ensured that the changing isotopic concentrations of the fuel in the system would not alter the neutron spectrum radically enough to cause a time step of the depletion calculation to be performed without the availability of cross sections which have been properly weighted with an updated neutron spectrum and spatial flux. This assumption was used throughout all of the depletion calculations documented in Section 5.
- 3.3** Distributing the spacer grid material uniformly in the moderator composition of the SAS2H Path A and Path B models was acceptable. The basis for this assumption was that the limited reactivity worth of the spacer grid materials would have a negligible impact on the neutron spectrum when homogeneously distributed in the moderator. This assumption was used throughout all of the depletion calculations documented in Section 5.

4. Use of Computer Software

4.1. Software Approved for QA Work

4.1.1. SAS2H

The SAS2H control module of the SCALE, Version 4.3, modular code system (Ref. 7.1) was used to perform the fuel assembly depletion calculations required for the Sequoyah Unit 2 CRC evaluations. The software specifications are as follow:

- Program Name: SAS2H of the SCALE Modular Code System
- Version/Revision Number: Version 4.3
- Computer Software Configuration Item (CSCI) Number: 30011 V4.3
- Computer Type: Hewlett Packard (HP) 9000 Series Workstations

The input and output files for the various SAS2H calculations were documented in the attachments to this calculation file as described in Section 5, such that an independent repetition of the software use could be performed. The SAS2H software used was: (a) appropriate for the application of commercial fuel assembly depletion, (b) used only within the range of validation as documented in References 7.1 and 7.2, (c) obtained from the Software Configuration Manager in accordance with appropriate procedures.

4.2. Software Routines

The description documentation for each of the software routines identified in this section, other than the acquired software routine Excel described in Section 4.2.1, contains the following information:

- Descriptions and equations of mathematical algorithms
- Description of software routine including execution environment
- Description of test cases
- Description of test results
- Range of input parameter values for which results were verified
- Identification of any limitations on software routine applications or validity
- Reference list of all documentation relevant to the qualification
- Directory listing of executable and data files
- Computer listing of source code
- Computer listing of test data input and output, identifying software routine name and version number.

4.2.1. Excel

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- **Version/Revision Number: Microsoft® Excel 97**

The Excel spreadsheet program was used for simple numeric calculations as documented in Section 5 of this calculation file. The user-defined formulas, inputs, and results were documented in sufficient detail in Section 5 to allow an independent repetition of the various computations.

4.2.2. CRAFT

- **Title: Commercial Reactor Assembly Follow Taskmaster (CRAFT)**
- **Version/Revision Number: Version 5**

The CRAFT software routine produced the input and directed the execution for the various SAS2H calculations required to deplete a commercial reactor fuel assembly to support a CRC evaluation. The input and output for the various CRAFT calculations were documented in Section 5, such that an independent repetition of the software routine use could be performed. The description of the CRAFT, Version 5, software routine was provided in Attachment I of Reference 7.6.

4.2.3. CRC Data Tabulizer

- **Title: CRC_DATA_TABULIZER**
- **Version/Revision Number: Version 3**

The CRC Data Tabulizer software routine produced tables containing the concentration results for a set of 29 isotopes and other relevant data at each CRC statepoint for a given fuel assembly. The CRC Data Tabulizer software routine is interactive, therefore, the input was not documented. However, the output contains all necessary information to verify that the input was provided correctly. The output from the CRC Data Tabulizer usage was provided in Attachment IV (the attachment tape has been moved to Reference 7.7). The information provided in this output and the information provided in the description of the CRC Data Tabulizer software routine, along with the CRAFT generated "*.cut" files, were sufficient such that an independent repetition of the software routine use could be performed. The description of the CRC Data Tabulizer, Version 3, software routine was provided in Attachment VI of Reference 7.6.

4.2.4. RLAYOUT

- **Title: RLAYOUT**
- **Version/Revision Number: Version 1**

The RLAYOUT software routine automated the development of irradiation time step layout inputs for depletion calculations involving rod insertion histories in which rod movements must be followed. The RLAYOUT code is mostly interactive, therefore, some of the input was not documented. The required boron letdown inputs and rod insertion history inputs for the required assemblies were presented in Sections 5.2.7 and 5.2.9, respectively. The output contained all necessary information to verify that the

entire input was provided correctly. The output from the RLAYOUT usage was presented in Section 5.5. The information provided in this output, the boron letdown input, and the rod insertion history input along with the information provided in the description of the RLAYOUT software routine, are sufficient such that an independent repetition of the software routine use could be performed. The description of the RLAYOUT, Version 1, software routine was provided in Attachment III of Reference 7.3.

5. Calculation

5.1. Sequoyah Unit 2 CRC Evaluation Description

The Sequoyah Unit 2 CRC evaluations were performed at three statepoints: Cycle 1 [0.0 Effective Full-Power Days (EFPD)], Cycle 3 [0.0, and 210.9 EFPD]. Each statepoint represented a specific time when the reactor was brought to the critical condition ($k_{eff} = 1$) and the corresponding reactor core conditions were measured. The CRC evaluations of each of these critical statepoints involved the use of SAS2H to deplete the various fuel assemblies and MCNP4B2 (Ref. 7.4) to model the reactor core such that the k_{eff} value at each of the critical statepoints could be predicted to demonstrate the ability of the dual code system. Hence, the objective of each CRC statepoint evaluation was to predict the reactor core k_{eff} as close to measurement as possible (the measurement is always $k_{eff} = 1$). The objective of the SAS2H depletion calculations documented in this calculation file was to provide the depleted fuel and burnable poison isotopic compositions to be used in the corresponding CRC reactivity calculations.

Fuel isotopic compositions were calculated with SAS2H for each depleted fuel assembly in each of the critical statepoint configurations to facilitate MCNP modeling. The Sequoyah Unit 2 statepoint calculations required the depletion of fuel assemblies from five fuel batches. Fuel assembly design characteristics may vary between each fuel batch. Section 5.2 presents the input parameters required to perform the various fuel assembly depletion calculations. Sections 5.3 through 5.7 describe how the parameters listed in Section 5.2 were utilized to perform the SAS2H depletion calculations relevant to the CRC statepoint evaluations. The CRAFT description and user information provided in Attachment I of Reference 7.6 is essential for understanding the SAS2H modeling techniques employed in the calculations. The information provided in Attachment I of Reference 7.6, the input parameters provided in Section 5.2, and the CRAFT input decks contained in Attachment I of this calculation file (the attachment tape has been moved to Reference 7.7) work together to provide a complete description of how all of SAS2H depletion calculations were performed.

5.2. Input Specifications for Depletion Calculations

The information documented in this section describes the design specifications and irradiation histories for the fuel assemblies required for the Sequoyah Unit 2 CRC evaluations. All of the input specifications presented in this section were obtained from Reference 7.5. The Sequoyah Unit 2 CRC reactivity evaluations included fuel assemblies from six fuel batches identified as follow: 1, 2, 3, 4, 5A, and 5B. Depletion calculations for fuel assemblies from batches 2, 3, 4, 5A, and 5B were required to perform k_{eff} calculations at the various statepoints. Fuel assemblies from fuel batch 1 were only used in

Table 5.2.1-1. Fuel Assembly Descriptions for the Sequoyah Unit 2 CRC Evaluations

Parameter	Fuel Batch Identifier					
	1	2	3	4	5A	5B
Assembly Pitch (cm)	21.50364	21.50364	21.50364	21.50364	21.50364	21.50364

¹ OD = Outer Diameter

² ID = Inner Diameter

³ The upper guide tube section is represented over nodes 1 through 13.

⁴ The lower guide tube section is represented over nodes 14 through 16.

⁵ Zr-4 = Zircaloy-4

5.2.2. Burnable Poison Rod Assembly (BPR) Descriptions Required for Depletion Calculations

Two types of annular burnable poison rods (BPRs) were used in the Sequoyah Unit 2 reactor from cycle 1 through cycle 3. The two BPR types were differentiated primarily by the type of absorber material utilized and the content of their annuli. One of the BPR types used $B_2O_3-SiO_2$ as the absorber material and had an empty annulus. This type is referred to as a Pyrex BPR in this calculation file. The other type of BPR used $B_4C-Al_2O_3$ as the absorber material and had a water filled annulus. This type is referred to as a WABA (Wet Annular Burnable Absorber) in this calculation file. Different numbers of either Pyrex or WABA BPRs were combined to form the various BPRAs utilized in the Sequoyah Unit 2 reactor. The number of BPRs in a given BPRa could vary from 1 to 24, depending on the number of guide tubes in which a BPR was inserted. The fuel assembly depletion calculations required to perform the CRC evaluations for Sequoyah Unit 2 utilized Pyrex BPRAs containing either 9, 10, or 20 BPRs and WABA BPRAs containing either 8, 12, 16, 20, or 24 BPRs. Knowing the geometric arrangement of the various BPRAs (referring to which guide tubes contain a BPR and which do not) was not required to perform the depletion calculations. Tables 5.2.2-1 and 5.2.2-2 contain descriptions of the Pyrex and WABA BPRAs, respectively, that were used in the fuel assembly depletion calculations. Table 5.2.2-3 presents the isotopic composition of the Pyrex absorber material.

Table 5.2.2-1. Pyrex BPRa Description for the Sequoyah Unit 2 Depletion Calculations

Parameter	Value
Burnable Poison Material	$B_2O_3-SiO_2$
Boron Loading	12.5 wt% B_2O_3 with 0.00624 g B-10/cm
Absorber OD (cm)	0.85344
Absorber ID (cm)	0.48260
Clad Material	Type 304 Stainless Steel (SS304)

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Table 5.2.2-1. Pyrex BPRA Description for the Sequoyah Unit 2 Depletion Calculations

Parameter	Value
Outer Clad OD (cm)	0.96774
Outer Clad ID (cm)	0.87376
Inner Clad OD (cm)	0.46101
Inner Clad ID (cm)	0.42799
Cross-Sectional Area (cm ²)	0.38913
Number of BPRs in BPRA	9, 10, or 20

Table 5.2.2-2. WABA BPRA Description for the Sequoyah Unit 2 Depletion Calculations

Parameter	Value
Burnable Poison Material	B ₄ C-Al ₂ O ₃
Boron Loading	14.0 wt% B ₄ C with 0.006165 g B-10/cm
Absorber OD (cm)	0.8077
Absorber ID (cm)	0.7061
Clad Material	Zircaloy-4
Outer Clad OD (cm)	0.96774
Outer Clad ID (cm)	0.83570
Inner Clad OD (cm)	0.67820
Inner Clad ID (cm)	0.57150
Cross-Sectional Area (cm ²)	0.12079
Number of BPRs in BPRA	8, 12, 16, 20, or 24

Table 5.2.2-3. Pyrex Absorber Material Composition (B₂O₃-SiO₂)

Isotope/Element	Weight Percent
Boron-10	0.6976
Boron-11	3.1866
Oxygen	55.2092
Silicon	40.9067

The CRAFT input required the density of the BPR absorber material to be provided in terms of grams per cubic centimeter (g/cc). The density in g/cc for both the Pyrex and WABA BPR absorber material had to be calculated using the boron loading information shown in Tables 5.2.2-1 and 5.2.2-2. The absorber material density results from these calculations were: 2.299 g/cc for the Pyrex BPR and 2.593 g/cc for the WABA BPR. Equations 5.2.2-1 through 5.2.2-7 show how the B₂O₃-SiO₂ and B₄C-Al₂O₃ densities were calculated.

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Equation 5.2.2-1. Calculation of B-10 grams per O gram in B_2O_3 of Pyrex BPR

$$\left(\frac{2 \text{ atoms B}}{3 \text{ atoms O}}\right) \left(\frac{0.194 \text{ atoms } B^{10}}{1 \text{ atoms B}}\right) \left(\frac{1 \text{ mol } B^{10}}{\text{Av.\# atoms } B^{10}}\right) \left(\frac{10.0129 \text{ g } B^{10}}{1 \text{ mol } B^{10}}\right) \left(\frac{\text{Av.\# atoms O}}{1 \text{ mol O}}\right) \left(\frac{1 \text{ mol O}}{15.9949 \text{ g O}}\right) =$$

$$= 0.0810 \frac{\text{g } B^{10}}{\text{g O}} \text{ in } B_2O_3, \text{ where, Av.\#} = 6.022136E23$$

Equation 5.2.2-2. Calculation of B-10 grams per B gram

$$\left(\frac{0.194 \text{ atoms } B^{10}}{1 \text{ atom B}}\right) \left(\frac{1 \text{ mol } B^{10}}{\text{Av.\# atoms } B^{10}}\right) \left(\frac{10.0129 \text{ g } B^{10}}{1 \text{ mol } B^{10}}\right) \left(\frac{\text{Av.\# atoms B}}{1 \text{ mol B}}\right) \left(\frac{1 \text{ mol B}}{10.8160 \text{ g B}}\right) = 0.1796 \frac{\text{g } B^{10}}{\text{g B}}$$

Equation 5.2.2-3. Calculation of B_2O_3 grams per cm in Pyrex BPR

$$\left(\frac{0.00624 \text{ g } B^{10}}{\text{cm}}\right) \left[\left(\frac{1}{0.1796 \frac{\text{g } B^{10}}{\text{g B}}}\right) + \left(\frac{1}{0.0810 \frac{\text{g } B^{10}}{\text{g O}} \text{ in } B_2O_3}\right) \right] = 0.1118 \frac{\text{g } B_2O_3}{\text{cm}}$$

Equation 5.2.2-4. Calculation of B_2O_3 - SiO_2 grams per cubic centimeter in Pyrex BPR

$$\left(\frac{0.1118 \text{ g } B_2O_3}{\text{cm}}\right) \left(\frac{100}{12.5 \text{ Wt\% } B_2O_3 \text{ in } B_2O_3 - SiO_2}\right) \left(\frac{1}{(\pi)(0.18209 \text{ cm}^2 - 0.05823 \text{ cm}^2)}\right) =$$

$$= 2.2985 \frac{\text{g } B_2O_3 - SiO_2}{\text{cm}^3}$$

Equation 5.2.2-5. Calculation of B-10 grams per C gram in B_4C of WABA BPR

$$\left(\frac{4 \text{ atoms B}}{1 \text{ atom C}}\right) \left(\frac{0.194 \text{ atoms } B^{10}}{1 \text{ atom B}}\right) \left(\frac{1 \text{ mol } B^{10}}{\text{Av.\# atoms } B^{10}}\right) \left(\frac{10.0129 \text{ g } B^{10}}{1 \text{ mol } B^{10}}\right) \left(\frac{\text{Av.\# atoms C}}{1 \text{ mol C}}\right) \left(\frac{1 \text{ mol C}}{12.0110 \text{ g C}}\right) =$$

$$= 0.6469 \frac{\text{g } B^{10}}{\text{g C}} \text{ in } B_4C$$

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Equation 5.2.2-6. Calculation of B_4C grams per cm in WABA BPR

$$\left(\frac{0.006165 \text{ g } B^{10}}{\text{cm}} \right) \left[\left(\frac{1}{0.1796 \frac{\text{g } B^{10}}{\text{g } B}} \right) + \left(\frac{1}{0.6469 \frac{\text{g } B^{10}}{\text{g } C} \ln B_4C} \right) \right] = 0.0439 \frac{\text{g } B_4C}{\text{cm}}$$

Equation 5.2.2-7. Calculation of $B_4C-Al_2O_3$ grams per cubic centimeter in WABA BPR

$$\left(\frac{0.0439 \text{ g } B_4C}{\text{cm}} \right) \left(\frac{100}{14.0 \text{ Wt\% } B_4C \text{ in } B_4C - Al_2O_3} \right) \left(\frac{1}{(\pi)(0.1631 \text{ cm}^2 - 0.1246 \text{ cm}^2)} \right) =$$

$$= 2.5925 \frac{\text{g } B_4C - Al_2O_3}{\text{cm}^3}$$

5.2.3. Rod Cluster Control Assembly (RCCA) Description Required for Depletion Calculations

The RCCA assemblies used in the Sequoyah Unit 2 reactor were composed of 24 control rods (CRs) arranged in a "cluster" such that each guide tube in the fuel assembly had a CR inserted from the top of the core to a uniform height in the assembly. Table 5.2.3-1 contains the description of the RCCAs utilized during the Sequoyah Unit 2 reactor operation relevant to the CRC evaluations documented in this calculation file.

Table 5.2.3-1. RCCA Description for the Sequoyah Unit 2 Depletion Calculations

Parameter	Value
Control Rod Neutron Absorbing Material	Ag-In-Cd (80 wt% Ag, 15 wt% In, 5 wt% Cd)
Ag-In-Cd Density (g/cc)	10.16
Absorber Pellet OD (cm)	0.86614
Control Rod Cladding Material	SS304
Control Rod Cladding OD (cm)	0.96774
Control Rod Cladding ID (cm)	0.87376
Number of Control Rods in RCCA	24

5.2.4. System Pressure

Sequoyah Unit 2 is a Westinghouse designed pressurized water reactor that operates at a constant pressure of 2250 psia (pounds per square inch absolute).

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5.2.5. Fuel Assembly Insertion, BPRA Type and Insertion, and RCCA Insertion Histories for the Sequoyah Unit 2 Depletion Calculations

The actual irradiation histories for the fuel assemblies from Sequoyah Unit 2 were used to perform the SAS2H depletion calculations relevant to the CRC evaluations. Table 5.2.5-1 identifies the following information:

- the cycles in which the various fuel assemblies were inserted
- the locations of the various fuel assemblies in each cycle corresponding to a one-eighth core location as shown in Figure 5.2.5-1
- the fuel batch to which each fuel assembly corresponds
- the cycles in which the various fuel assemblies contained either a BPRA or RCCA
- the types of BPRA inserted in the various fuel assemblies.

Table 5.2.5-1. Fuel Assembly Insertion Cycles, BPRA Insertion Cycles, and RCCA Insertion Cycles for the Sequoyah Unit 2 Depletion Calculations

Assembly Identifier / Fuel Batch	Fuel Assembly, BPRA, and RCCA Insertion Locations and Cycles		
	Cycle 1	Cycle 2	Cycle 3
A6/2	[20] ¹ / C8 ²	A8	{CD} ³ / D8
A8/3	[10] / A8	E8	F10
A15/3	A9	F9	D10
A21/3	[10] / A10	C8	B8
A21a/3	[10] / A10	G8	G13 ⁴
A25/2	[9] / B11	C12	{CD} / D12
A25a/2	[9] / B11	C12	B13
A26/3	A11	E10	{CD} / H8
A26a/3	A11	E10	C9
A29/3	B12	E9	E11
A29a/3	B12	E9	C14
A30/3	C13	{CD} / D12	G9
A31/3	[9] / B13	D11	B10
B14/4		[8] / B9	E9
B15/4		A9	D11
B19/4		[12] / C10	C11
B21/4		A10	C12
B25/4		[12] / B11	F9
B26/4		A11	B12
B29/4		B12	D9

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Table 5.2.5-1. Fuel Assembly Insertion Cycles, BPRA Insertion Cycles, and RCCA Insertion Cycles for the Sequoyah Unit 2 Depletion Calculations

Assembly Identifier / Fuel Batch	Fuel Assembly, BPRA, and RCCA Insertion Locations and Cycles		
	Cycle 1	Cycle 2	Cycle 3
B30 / 4		[8] / C13	F8
B31 / 4		B13	A11
C2 / 5B			[16] / G8
C4 / 5B			[24] / E8
C6 / 5B			[12] / C8
C8 / 5B			A8
C14 / 5A			[16] / B9
C15 / 5A			A9
C17 / 5B			[12] / E10
C19 / 5A			[20] / C10
C21 / 5A			A10
C25 / 5A			[8] / B11
C30 / 5B			C13

¹ Numbers appearing in bracket like [#] indicate that a BPRA was present in the assembly in that particular cycle. The number refers to the number of BPRs in the BPRA. Cycle 1 utilized Pyrex BPRAs, and cycles 2 and 3 utilized WABA BPRAs.

² The alphanumeric designations following the slash "/" identify the assembly position in the one-eighth symmetric core layout as shown in Figure 5.2.5-1.

³ Letters appearing in brackets like {xx} indicate that an RCCA corresponding to the letter symbol was present in the assembly during operation in that particular cycle.

⁴ For cycle 3, assemblies A21a and A26a are in 1/8th core symmetric locations, but do not have 1/8th core symmetric properties. Assemblies A25a and A29a are also in 1/8th core symmetric locations in cycle 3, but do not have 1/8th core symmetric properties.

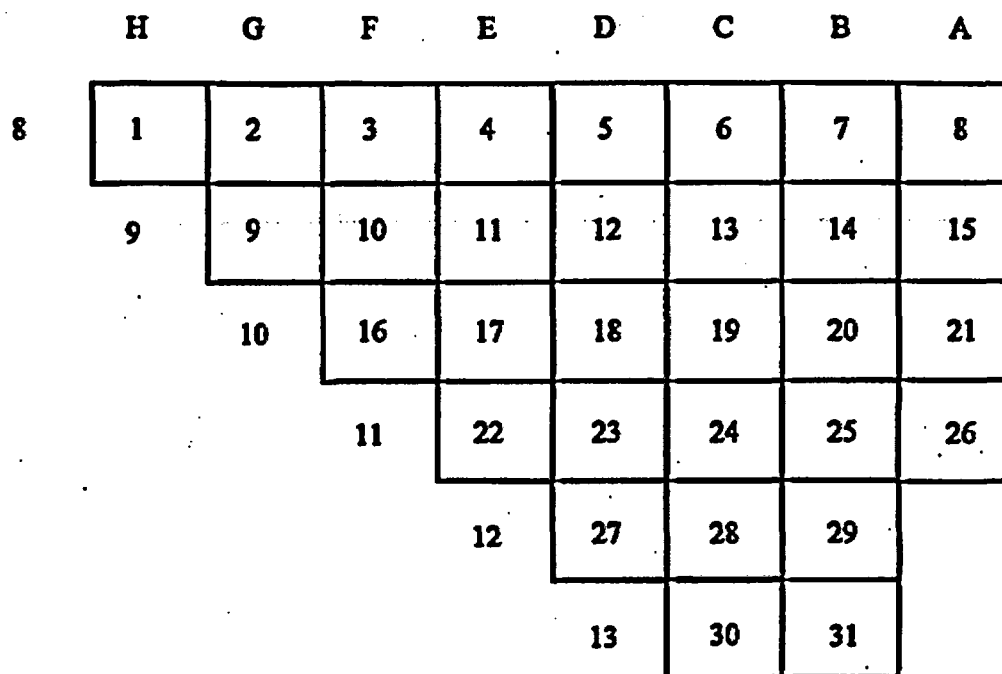


Figure 5.2.5-1. One-Eighth Symmetric Core Layout for Sequoyah Unit 2

5.2.6. Reactor Cycle History Specifications for Sequoyah Unit 2

This section contains the Sequoyah Unit 2 reactor cycle summary information relevant to the CRC evaluations documented in this calculation file. The calendar day duration between the various dates were determined using an Excel spreadsheet. Table 5.2.6-1 shows the cycle summary information. Table 5.2.6-2 shows the statepoint and datapoint summary information. The statepoints refer to times when the reactor was shutdown and restarted. MCNP reactivity calculations for the CRC evaluations were performed using the reactor startup conditions and appropriate depleted isotopics after each statepoint shutdown. The datapoints refer to times when the depletion calculations were halted to adjust various input parameters such as average fuel temperatures and average moderator specific volumes. The depletion calculations were continued after each datapoint halt without modeling any reactor downtime.

Table 5.2.6-1. Cycle Summary Information for Sequoyah Unit 2 Depletion Calculations

Cycle	Startup Date	Shutdown Date	Cycle Length (calendar days)	Cycle Length (EFPD)	Downtime at EOC ¹ (days)
1	11/05/81	07/18/83	620	389.3	86
2	10/12/83	09/28/84	352	297.0	81

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Table 5.2.6-1. Cycle Summary Information for Sequoyah Unit 2 Depletion Calculations

Cycle	Startup Date	Shutdown Date	Cycle Length (calendar days)	Cycle Length (EFPD)	Downtime at EOC ¹ (days)
3	12/18/84	01/18/89	1492	377.3	Not Required

¹ The letters EOC refer to end-of-cycle.

Table 5.2.6-2. Statepoint and Datapoint Summary Information for Sequoyah Unit 2 Depletion Calculations

Cycle	EFPD	Statepoint or Datapoint Identifier	Downtime at Statepoint or Datapoint (hours)
1	0.0	SP1 (36) ¹	0.0
1	187.06	DP1 ²	0.0
2	0.0	DP2	0.0
2	145.3	DP3	0.0
3	0.0	SP2 (37)	1943
3	210.9	SP3 (38)	23896

¹ The letters "SP" refer to a CRC statepoint. The number immediately following the "SP" refers to the relative statepoint for the Sequoyah Unit 2 CRC evaluations. The number in the parenthesis following the "SP#" refers to the statepoint number as identified in the global listing of statepoints in the CRC evaluation project.

² The letters "DP" refer to a CRC datapoint. The number immediately following the "DP" refers to the relative datapoint for the Sequoyah Unit 2 CRC evaluations.

5.2.7. Boron Letdown Data for Sequoyah Unit 2 Depletion Calculations

The boron letdown data for the Sequoyah Unit 2 reactor cycles relevant to CRC evaluations were obtained from linear regression fits of core operation data. Table 5.2.7-1 contains the coefficients from the linear regression fits of the core operation data for cycles 1 through 3.

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**Table 5.2.7-1. Linear Regression Fit Coefficients of
Boron Letdown for Sequoyah Unit 2 Depletion Calculations**

Regression Fit Description: Soluble Boron Concentration versus EFPD Regression Fit Equation: $\text{ppmB}^1 = A + B * \text{EFPD}$		
Cycle	A	B
1	1003.27	-2.47
2	986.95	-3.15
3	1180.18	-3.11

¹ "ppmB" refers to parts per million by mass of natural boron in moderator (water).

5.2.8. Burnup, Fuel Temperature, and Moderator Specific Volume Data

Burnup, fuel temperature, and moderator specific volume data were required for each node of each assembly in each SAS2H depletion calculation. A set of nodal burnup data at the beginning and end of each SAS2H depletion calculation was required. A set of nodal fuel temperature and moderator specific volume data representative of full-power operation during each depletion calculation of interest (between statepoints and/or datapoints) was required. Tables 5.2.8-1 through 5.2.8-33 contain the burnup, fuel temperature, and moderator specific volume data required to perform all depletion calculations for each of the fuel assemblies present in the Sequoyah Unit 2 CRC evaluations. The height of each fuel assembly axial node in Tables 5.2.8-1 through 5.2.8-33 is 22.86 cm. The top of node 1 begins at the top of the active fuel region. The burnup data is presented in units of gigawatt-days per metric ton of uranium (GWd/MTU). The fuel temperature data is presented in units of degrees Fahrenheit. The moderator specific volume data is presented in units of cubic feet per pound. Each set of fuel temperature and moderator specific volume data listed in the tables was applicable to the depletion calculation performed between the statepoints and/or datapoints identified above the particular data.

Table 5.2.8-1. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A6

Axial Node	SP36 to DP1			DP1 to DP2			DP2 to DP3		
	Burnup DP1	T-Fuel	Spec.Vol	Burnup DP2	T-Fuel	Spec.Vol	Burnup DP3	T-Fuel	Spec.Vol
1	2.324	835.5	0.0241	6.422	961.1	0.0242	8.558	820.0	0.0227
2	4.693	1048.9	0.0240	12.057	1159.7	0.0240	15.350	888.1	0.0226
3	6.555	1202.1	0.0238	15.680	1226.5	0.0238	19.358	890.8	0.0225
4	7.810	1296.5	0.0236	17.478	1232.9	0.0235	21.239	879.9	0.0224
5	8.631	1355.0	0.0234	18.293	1211.8	0.0233	22.045	872.0	0.0223
6	9.162	1390.3	0.0232	18.646	1185.6	0.0231	22.372	865.7	0.0222
7	9.503	1411.3	0.0229	18.801	1163.0	0.0229	22.508	861.2	0.0221
8	9.715	1424.1	0.0227	18.889	1146.9	0.0227	22.587	858.0	0.0220
9	9.831	1431.4	0.0225	18.971	1138.1	0.0225	22.665	855.4	0.0219
10	9.855	1433.7	0.0223	19.064	1137.4	0.0223	22.758	853.2	0.0218
11	9.759	1428.4	0.0220	19.146	1145.3	0.0221	22.842	851.3	0.0217
12	9.474	1409.7	0.0218	19.132	1162.1	0.0219	22.830	849.9	0.0216
13	8.875	1365.7	0.0216	18.797	1184.0	0.0217	22.485	848.8	0.0215
14	7.765	1277.6	0.0215	17.630	1194.3	0.0216	21.236	845.6	0.0214
15	5.879	1120.0	0.0213	14.571	1145.5	0.0214	17.834	837.2	0.0213
16	3.085	857.0	0.0213	8.321	963.9	0.0213	10.455	766.9	0.0213

Axial Node	DP3 to SP37			SP37 to SP38		
	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec.Vol
1	11.026	796.9	0.0228	14.243	831.8	0.0234
2	18.940	845.2	0.0227	24.922	962.8	0.0233
3	23.243	848.6	0.0226	30.319	988.5	0.0231
4	25.166	850.4	0.0225	32.671	983.2	0.0229
5	25.970	853.4	0.0224	33.655	977.0	0.0228
6	26.303	857.7	0.0223	34.032	970.9	0.0226
7	26.459	862.4	0.0222	34.184	964.9	0.0224
8	26.564	866.6	0.0221	34.258	958.9	0.0223
9	26.671	869.9	0.0220	34.309	952.7	0.0222
10	26.792	872.3	0.0219	34.352	946.1	0.0220
11	26.908	874.3	0.0218	34.368	939.0	0.0219
12	26.938	877.1	0.0217	34.276	931.3	0.0217
13	26.646	881.5	0.0216	33.839	922.8	0.0216
14	25.420	886.3	0.0215	32.417	912.7	0.0215
15	21.795	879.6	0.0214	28.340	897.8	0.0214
16	13.224	820.8	0.0213	17.965	838.0	0.0213

Datapoint
or

Statepoint	EFPD/Cycle
SP36	0.0 / Cy1
DP1	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ / lbm

Table 5.2.8-2. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A8

Axial Node	SP36 to DP1			DP1 to DP2			DP2 to DP3		
	Burnup DP1	T-Fuel	Spec.Vol	Burnup DP2	T-Fuel	Spec.Vol	Burnup DP3	T-Fuel	Spec.Vol
1	1.789	766.6	0.0230	4.866	859.8	0.0231	8.993	1060.0	0.0239
2	3.417	913.3	0.0230	8.617	1003.6	0.0230	14.892	1178.8	0.0237
3	4.631	1020.1	0.0229	10.864	1051.9	0.0228	17.695	1179.7	0.0235
4	5.456	1087.6	0.0228	12.017	1053.6	0.0227	18.731	1147.0	0.0233
5	5.995	1128.9	0.0226	12.560	1039.8	0.0226	19.025	1117.2	0.0231
6	6.343	1153.7	0.0225	12.802	1023.0	0.0224	19.058	1096.3	0.0229
7	6.565	1167.8	0.0223	12.913	1008.1	0.0223	19.024	1082.3	0.0227
8	6.704	1176.2	0.0222	12.980	997.5	0.0222	18.992	1072.5	0.0225
9	6.782	1181.1	0.0221	13.044	992.0	0.0220	18.983	1064.8	0.0223
10	6.799	1182.9	0.0219	13.114	992.1	0.0219	19.003	1058.4	0.0222
11	6.737	1179.8	0.0218	13.175	998.2	0.0218	19.044	1053.9	0.0220
12	6.550	1167.3	0.0216	13.163	1009.7	0.0217	19.065	1053.7	0.0218
13	6.151	1137.1	0.0215	12.917	1022.9	0.0216	18.923	1060.9	0.0217
14	5.405	1073.5	0.0214	12.082	1026.1	0.0214	18.195	1074.3	0.0215
15	4.125	956.6	0.0213	9.969	989.7	0.0213	15.790	1070.5	0.0214
16	2.179	767.1	0.0213	5.705	839.6	0.0213	9.674	959.8	0.0213

Axial Node	DP3 to SP37			SP37 to SP38		
	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec. Vol
1	12.975	890.7	0.0238	18.301	935.8	0.0237
2	20.594	949.6	0.0237	28.165	1011.8	0.0236
3	23.801	971.3	0.0236	32.131	1034.5	0.0234
4	24.847	998.6	0.0234	33.462	1038.2	0.0232
5	25.093	1017.5	0.0232	33.837	1035.8	0.0230
6	25.107	1030.6	0.0230	33.905	1031.1	0.0228
7	25.087	1041.4	0.0228	33.890	1025.4	0.0226
8	25.085	1049.8	0.0227	33.857	1019.3	0.0224
9	25.107	1055.8	0.0225	33.820	1012.9	0.0223
10	25.156	1059.9	0.0223	33.783	1006.2	0.0221
11	25.234	1063.1	0.0221	33.748	998.6	0.0220
12	25.327	1067.8	0.0219	33.694	989.7	0.0218
13	25.323	1077.5	0.0218	33.499	978.5	0.0217
14	24.773	1091.8	0.0216	32.665	962.5	0.0215
15	22.243	1094.8	0.0214	29.498	934.3	0.0214
16	14.378	1005.4	0.0213	19.522	853.5	0.0213

Datapoint or Statepoint

Datapoint or Statepoint	EFPD/Cycle
SP36	0.0 / Cy1
DP1	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ / lbm

Table 5.2.8-3. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A15

Axial Node	Burnup SP36 to DP1			Burnup DP1 to DP2			Burnup DP2 to DP3		
	DP1	T-Fuel	Spec.Vol	DP2	T-Fuel	Spec.Vol	DP3	T-Fuel	Spec.Vol
1	1.963	785.9	0.0232	5.273	878.0	0.0231	9.638	1060.9	0.0239
2	3.732	943.9	0.0232	9.221	1019.2	0.0230	15.669	1173.5	0.0237
3	5.032	1054.8	0.0230	11.529	1061.6	0.0229	18.434	1171.2	0.0235
4	5.912	1123.7	0.0229	12.708	1062.6	0.0228	19.458	1138.2	0.0232
5	6.486	1166.0	0.0228	13.264	1047.9	0.0226	19.748	1108.0	0.0230
6	6.857	1191.1	0.0226	13.515	1029.8	0.0225	19.777	1086.7	0.0228
7	7.095	1205.3	0.0225	13.633	1014.2	0.0223	19.740	1072.3	0.0227
8	7.246	1213.9	0.0223	13.708	1003.2	0.0222	19.706	1062.2	0.0225
9	7.333	1219.3	0.0221	13.780	997.5	0.0221	19.699	1054.1	0.0223
10	7.356	1221.8	0.0220	13.858	997.5	0.0220	19.722	1047.5	0.0222
11	7.296	1219.6	0.0218	13.927	1003.6	0.0218	19.768	1043.0	0.0220
12	7.104	1208.1	0.0217	13.921	1015.6	0.0217	19.798	1042.8	0.0218
13	6.687	1178.3	0.0215	13.680	1030.3	0.0216	19.663	1049.4	0.0217
14	5.898	1113.7	0.0214	12.837	1035.2	0.0215	18.930	1062.7	0.0215
15	4.529	993.5	0.0213	10.683	1002.1	0.0213	16.484	1059.5	0.0214
16	2.408	789.5	0.0213	6.206	858.2	0.0213	10.172	951.0	0.0213

Axial Node	Burnup DP3 to SP37			Burnup SP37 to SP38		
	SP37	T-Fuel	Spec.Vol	SP38	T-Fuel	Spec. Vol
1	13.826	915.1	0.0238	18.692	904.1	0.0236
2	21.492	976.0	0.0237	28.439	976.4	0.0235
3	24.566	988.1	0.0235	32.296	1001.5	0.0233
4	25.535	998.2	0.0234	33.610	1009.4	0.0231
5	25.754	1010.3	0.0232	34.002	1009.2	0.0229
6	25.760	1022.5	0.0230	34.094	1006.2	0.0227
7	25.736	1033.3	0.0228	34.102	1001.9	0.0226
8	25.732	1041.8	0.0226	34.092	997.1	0.0224
9	25.754	1047.9	0.0225	34.078	991.9	0.0222
10	25.804	1051.8	0.0223	34.066	986.2	0.0221
11	25.886	1054.9	0.0221	34.055	979.7	0.0219
12	25.984	1059.4	0.0219	34.021	971.5	0.0218
13	25.984	1068.7	0.0218	33.837	960.6	0.0216
14	25.427	1082.8	0.0216	32.995	944.7	0.0215
15	22.857	1086.0	0.0214	29.824	916.6	0.0214
16	14.833	997.3	0.0213	19.824	842.0	0.0213

Datapoint or Statepoint	EFPD / Cycle
SP36	0.0 / Cy1
DP1	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup - GWd/MTU
 T-Fuel - °F
 Spec. Vol - ft³ / lbm

Table 5.2.8-4. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A21

Axial Node	SP36 to DP1			DP1 to DP2			DP2 to DP3		
	Burnup DPI	T-Fuel	Spec.Vol	Burnup DP2	T-Fuel	Spec.Vol	Burnup DP3	T-Fuel	Spec.Vol
1	1.650	749.8	0.0229	4.496	838.3	0.0229	8.227	1038.4	0.0239
2	3.154	885.8	0.0228	7.975	975.6	0.0228	13.715	1157.3	0.0238
3	4.272	984.7	0.0227	10.057	1023.8	0.0227	16.425	1170.2	0.0235
4	5.031	1048.8	0.0226	11.126	1027.0	0.0226	17.520	1149.6	0.0233
5	5.526	1087.0	0.0225	11.628	1013.6	0.0224	17.903	1128.7	0.0231
6	5.844	1110.0	0.0224	11.849	997.4	0.0223	18.012	1113.6	0.0229
7	6.046	1123.5	0.0222	11.948	983.4	0.0222	18.037	1103.7	0.0227
8	6.172	1131.6	0.0221	12.008	973.5	0.0221	18.050	1097.0	0.0225
9	6.241	1136.2	0.0220	12.064	968.4	0.0220	18.077	1091.8	0.0224
10	6.255	1137.7	0.0219	12.126	968.5	0.0219	18.123	1087.4	0.0222
11	6.197	1134.6	0.0217	12.180	974.1	0.0218	18.174	1084.3	0.0220
12	6.023	1122.5	0.0216	12.165	984.5	0.0216	18.183	1083.9	0.0219
13	5.655	1093.1	0.0215	11.931	996.8	0.0215	18.000	1087.9	0.0217
14	4.967	1033.8	0.0214	11.148	1000.0	0.0214	17.225	1094.3	0.0215
15	3.788	924.0	0.0213	9.179	962.5	0.0213	14.871	1080.7	0.0214
16	1.999	749.2	0.0212	5.237	818.0	0.0213	9.082	964.0	0.0213

Axial Node	DP3 to SP37			SP37 to SP38		
	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec. Vol
1	12.145	905.0	0.0240	16.853	906.3	0.0237
2	19.408	975.1	0.0238	26.255	978.9	0.0236
3	22.617	1000.0	0.0237	30.355	1009.5	0.0234
4	23.794	1026.3	0.0235	31.982	1020.7	0.0232
5	24.173	1044.1	0.0233	32.617	1024.2	0.0230
6	24.287	1056.1	0.0231	32.892	1024.7	0.0228
7	24.343	1066.3	0.0229	33.052	1023.7	0.0227
8	24.400	1074.7	0.0227	33.177	1022.1	0.0225
9	24.473	1081.1	0.0225	33.291	1020.2	0.0223
10	24.564	1085.9	0.0223	33.396	1018.1	0.0221
11	24.668	1090.2	0.0222	33.481	1015.0	0.0220
12	24.758	1095.8	0.0220	33.501	1010.1	0.0218
13	24.701	1105.0	0.0218	33.289	1001.1	0.0217
14	24.055	1117.3	0.0216	32.313	984.5	0.0215
15	21.482	1115.6	0.0214	28.986	950.6	0.0214
16	13.842	1016.0	0.0213	19.102	863.9	0.0213

Datapoint or Statepoint	EFPD/Cycle
SP36	0.0/Cy1
DP1	187.06/Cy1
DP2	0.0/Cy2
DP3	145.3/Cy2
SP37	0.0/Cy3
SP38	210.9/Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ /lbm

Table 5.2.8-5. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A21a

Axial Node	SP36 to DP1			DP1 to DP2			DP2 to DP3		
	Burnup DP1	T-Fuel	Spec.Vol.	Burnup DP2	T-Fuel	Spec.Vol.	Burnup DP3	T-Fuel	Spec.Vol.
1	1.650	749.8	0.0229	4.496	838.3	0.0229	8.605	1059.4	0.0239
2	3.154	885.8	0.0228	7.975	975.6	0.0228	14.264	1180.8	0.0237
3	4.272	984.7	0.0227	10.057	1023.8	0.0227	16.936	1185.1	0.0235
4	5.031	1048.8	0.0226	11.126	1027.0	0.0226	17.890	1153.3	0.0232
5	5.526	1087.0	0.0225	11.628	1013.6	0.0224	18.127	1122.9	0.0230
6	5.844	1110.0	0.0224	11.849	997.4	0.0223	18.117	1101.0	0.0228
7	6.046	1123.5	0.0222	11.948	983.4	0.0222	18.051	1086.2	0.0226
8	6.172	1131.6	0.0221	12.008	973.5	0.0221	17.994	1075.7	0.0225
9	6.241	1136.2	0.0220	12.064	968.4	0.0220	17.966	1067.5	0.0223
10	6.255	1137.7	0.0219	12.126	968.5	0.0219	17.970	1060.7	0.0221
11	6.197	1134.6	0.0217	12.180	974.1	0.0218	18.000	1056.2	0.0220
12	6.023	1122.5	0.0216	12.165	984.5	0.0216	18.021	1056.3	0.0218
13	5.655	1093.1	0.0215	11.931	996.8	0.0215	17.896	1063.5	0.0217
14	4.967	1033.8	0.0214	11.148	1000.0	0.0214	17.215	1076.1	0.0215
15	3.788	924.0	0.0213	9.179	962.5	0.0213	14.929	1068.6	0.0214
16	1.999	749.2	0.0212	5.237	818.0	0.0213	9.125	955.5	0.0213

Axial Node	DP3 to SP37			SP37 to SP38		
	Burnup SP37	T-Fuel	Spec.Vol.	Burnup SP38	T-Fuel	Spec.Vol.
1	12.501	883.5	0.0238	17.313	911.9	0.0237
2	19.870	944.0	0.0237	26.753	982.0	0.0235
3	22.959	966.6	0.0235	30.658	1008.5	0.0233
4	23.934	994.0	0.0234	32.029	1016.6	0.0232
5	24.130	1014.4	0.0232	32.445	1018.3	0.0230
6	24.108	1029.1	0.0230	32.550	1017.3	0.0228
7	24.061	1041.2	0.0228	32.573	1015.0	0.0226
8	24.038	1050.7	0.0226	32.582	1012.1	0.0224
9	24.043	1057.4	0.0225	32.589	1008.6	0.0223
10	24.077	1061.9	0.0223	32.597	1004.6	0.0221
11	24.145	1065.1	0.0221	32.606	999.6	0.0220
12	24.238	1069.8	0.0219	32.593	992.6	0.0218
13	24.249	1079.2	0.0218	32.430	982.3	0.0217
14	23.737	1094.4	0.0216	31.621	966.6	0.0215
15	21.301	1096.4	0.0214	28.563	938.7	0.0214
16	13.737	1002.8	0.0213	18.959	862.6	0.0213

Datapoint
or

Statepoint	EFPD / Cycle
SP36	0.0 / Cy1
DP1	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ / lbm

Table 5.2.8-6. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A25

Axial Node	SP36 to DP1			DP1 to DP2			DP2 to DP3		
	Burnup DP1	T-Fuel	Spec.Vol	Burnup DP2	T-Fuel	Spec.Vol	Burnup DP3	T-Fuel	Spec.Vol
1	2.226	817.2	0.0236	5.991	922.0	0.0235	9.190	967.9	0.0238
2	4.267	998.1	0.0235	10.591	1082.1	0.0234	15.621	1076.7	0.0236
3	5.798	1126.9	0.0234	13.355	1127.3	0.0232	19.082	1089.9	0.0234
4	6.837	1204.1	0.0232	14.770	1127.0	0.0230	20.662	1076.2	0.0232
5	7.516	1250.9	0.0230	15.434	1110.6	0.0229	21.323	1061.8	0.0230
6	7.954	1278.6	0.0229	15.731	1090.4	0.0227	21.591	1052.2	0.0228
7	8.236	1295.0	0.0227	15.872	1072.8	0.0225	21.714	1045.9	0.0226
8	8.416	1305.1	0.0225	15.960	1060.3	0.0224	21.799	1041.6	0.0225
9	8.520	1311.5	0.0223	16.043	1053.6	0.0222	21.888	1038.4	0.0223
10	8.550	1314.7	0.0221	16.136	1053.3	0.0221	21.992	1035.7	0.0221
11	8.484	1312.7	0.0219	16.218	1059.8	0.0219	22.089	1033.5	0.0220
12	8.263	1300.1	0.0218	16.217	1073.0	0.0218	22.109	1032.6	0.0218
13	7.779	1266.9	0.0216	15.944	1089.2	0.0216	21.847	1033.0	0.0217
14	6.858	1195.9	0.0214	14.974	1095.2	0.0215	20.797	1033.7	0.0215
15	5.257	1062.0	0.0213	12.450	1062.5	0.0214	17.796	1019.9	0.0214
16	2.788	826.7	0.0213	7.202	903.2	0.0213	10.771	911.6	0.0213

Axial Node	DP3 to SP37			SP37 to SP38		
	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec.Vol
1	12.619	854.3	0.0237	15.316	783.2	0.0231
2	20.698	913.1	0.0236	25.918	903.8	0.0230
3	24.700	942.4	0.0234	30.980	930.1	0.0228
4	26.434	974.0	0.0233	33.131	926.7	0.0227
5	27.141	994.4	0.0231	34.013	921.3	0.0225
6	27.439	1007.3	0.0229	34.352	915.7	0.0224
7	27.604	1017.3	0.0228	34.508	909.8	0.0223
8	27.738	1025.1	0.0226	34.605	903.8	0.0221
9	27.876	1031.2	0.0224	34.685	897.9	0.0220
10	28.027	1035.7	0.0222	34.758	891.8	0.0219
11	28.178	1039.7	0.0221	34.811	885.3	0.0218
12	28.269	1044.5	0.0219	34.779	877.9	0.0217
13	28.103	1051.8	0.0217	34.457	869.1	0.0215
14	27.120	1059.3	0.0216	33.246	856.9	0.0214
15	23.847	1046.4	0.0214	29.437	837.6	0.0213
16	15.097	961.2	0.0213	18.981	777.2	0.0213

Datapoint or

Statenpoint	EFPD/Cycle
SP36	0.0 / Cy1
DP1	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ / lbm

Table 5.2.8-7. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A25a

Axial Node	SP36 to DP1			DP1 to DP2			DP2 to DP3		
	Burnup DPI	T-Fuel	Spec.Vol	Burnup DP2	T-Fuel	Spec.Vol	Burnup DP3	T-Fuel	Spec.Vol
1	2.226	817.2	0.0236	5.991	922.0	0.0235	9.190	967.9	0.0238
2	4.267	998.1	0.0235	10.591	1082.1	0.0234	15.621	1076.7	0.0236
3	5.798	1126.9	0.0234	13.355	1127.3	0.0232	19.082	1089.9	0.0234
4	6.837	1204.1	0.0232	14.770	1127.0	0.0230	20.662	1076.2	0.0232
5	7.516	1250.9	0.0230	15.434	1110.6	0.0229	21.323	1061.8	0.0230
6	7.954	1278.6	0.0229	15.731	1090.4	0.0227	21.591	1052.2	0.0228
7	8.236	1295.0	0.0227	15.872	1072.8	0.0225	21.714	1045.9	0.0226
8	8.416	1305.1	0.0225	15.960	1060.3	0.0224	21.799	1041.6	0.0225
9	8.520	1311.5	0.0223	16.043	1053.6	0.0222	21.888	1038.4	0.0223
10	8.550	1314.7	0.0221	16.136	1053.3	0.0221	21.992	1035.7	0.0221
11	8.484	1312.7	0.0219	16.218	1059.8	0.0219	22.089	1033.5	0.0220
12	8.263	1300.1	0.0218	16.217	1073.0	0.0218	22.109	1032.6	0.0218
13	7.779	1266.9	0.0216	15.944	1089.2	0.0216	21.847	1033.0	0.0217
14	6.858	1195.9	0.0214	14.974	1095.2	0.0215	20.797	1033.7	0.0215
15	5.257	1062.0	0.0213	12.450	1062.5	0.0214	17.796	1019.9	0.0214
16	2.788	826.7	0.0213	7.202	903.2	0.0213	10.771	911.6	0.0213

Axial Node	DP3 to SP37			SP37 to SP38		
	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec. Vol
1	12.621	854.3	0.0237	14.105	663.9	0.0219
2	20.701	913.1	0.0236	22.965	690.8	0.0219
3	24.703	942.4	0.0234	27.265	698.1	0.0218
4	26.437	974.0	0.0233	29.107	697.5	0.0218
5	27.144	994.4	0.0231	29.852	695.1	0.0217
6	27.443	1007.3	0.0229	30.161	692.4	0.0217
7	27.608	1017.3	0.0228	30.318	689.7	0.0216
8	27.742	1025.1	0.0226	30.435	687.2	0.0216
9	27.880	1031.2	0.0224	30.549	684.7	0.0215
10	28.032	1035.7	0.0222	30.669	682.1	0.0215
11	28.183	1039.7	0.0221	30.782	679.5	0.0214
12	28.273	1044.5	0.0219	30.823	676.6	0.0214
13	28.107	1051.8	0.0217	30.591	673.2	0.0214
14	27.124	1059.3	0.0216	29.499	668.7	0.0213
15	23.851	1046.4	0.0214	25.969	659.1	0.0213
16	15.100	961.2	0.0213	16.513	632.7	0.0212

Datapoint or Statepoint	EFPD / Cycle
SP36	0.0 / Cy1
DPI	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup - GWd/MTU
T-Fuel - °F
Spec. Vol - ft³ / lbm

Table 5.2.8-8. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A26

Axial Node	SP36 to DP1			DP1 to DP2			DP2 to DP3		
	Burnup DP1	T-Fuel	Spec.Vol	Burnup DP2	T-Fuel	Spec.Vol	Burnup DP3	T-Fuel	Spec.Vol
1	1.423	721.9	0.0226	3.843	795.8	0.0226	8.250	1093.6	0.0241
2	2.720	839.8	0.0226	6.783	913.1	0.0225	13.381	1223.2	0.0239
3	3.670	924.3	0.0225	8.500	953.7	0.0224	15.646	1231.2	0.0237
4	4.311	978.6	0.0224	9.373	956.3	0.0223	16.432	1204.6	0.0234
5	4.725	1011.4	0.0223	9.776	944.7	0.0222	16.621	1177.6	0.0232
6	4.989	1030.7	0.0222	9.949	930.5	0.0221	16.613	1158.2	0.0230
7	5.155	1041.7	0.0221	10.023	918.3	0.0220	16.563	1145.4	0.0228
8	5.258	1048.1	0.0220	10.065	909.6	0.0219	16.525	1136.7	0.0226
9	5.314	1051.8	0.0219	10.105	905.0	0.0218	16.510	1130.0	0.0224
10	5.324	1053.0	0.0218	10.151	904.9	0.0218	16.521	1124.6	0.0222
11	5.274	1050.4	0.0217	10.190	909.6	0.0217	16.552	1121.1	0.0221
12	5.129	1040.3	0.0215	10.174	918.5	0.0216	16.578	1121.5	0.0219
13	4.822	1015.8	0.0215	9.981	928.7	0.0215	16.487	1128.3	0.0217
14	4.245	965.1	0.0214	9.341	931.3	0.0214	15.929	1138.6	0.0216
15	3.252	871.9	0.0213	7.736	899.6	0.0213	13.950	1126.6	0.0214
16	1.722	721.6	0.0212	4.451	777.6	0.0213	8.632	996.5	0.0213

Axial Node	DP3 to SP37			SP37 to SP38		
	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec. Vol
1	12.568	938.8	0.0241	16.308	866.2	0.0238
2	19.465	1013.4	0.0239	26.257	1016.6	0.0236
3	22.122	1029.0	0.0237	30.177	1055.1	0.0234
4	22.897	1041.5	0.0235	31.479	1055.9	0.0232
5	23.041	1055.8	0.0233	31.846	1050.7	0.0230
6	23.026	1069.8	0.0231	31.888	1044.9	0.0228
7	23.003	1081.9	0.0229	31.862	1038.8	0.0226
8	23.006	1091.6	0.0227	31.826	1032.3	0.0225
9	23.034	1098.7	0.0226	31.787	1025.5	0.0223
10	23.085	1103.7	0.0224	31.749	1018.4	0.0221
11	23.165	1107.7	0.0222	31.714	1010.5	0.0220
12	23.271	1112.9	0.0220	31.674	1001.2	0.0218
13	23.319	1122.3	0.0218	31.533	989.6	0.0217
14	22.922	1136.3	0.0216	30.848	973.8	0.0215
15	20.755	1136.2	0.0214	28.096	946.3	0.0214
16	13.543	1029.9	0.0213	18.889	871.8	0.0213

Datapoint
or

Statepoint	EFPD / Cycle
SP36	0.0 / Cy1
DP1	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ / lbm

Table 5.2.8-9. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A26a

Axial Node	Burnup SP36 to DP1			Burnup DP1 to DP2			Burnup DP2 to DP3		
	DP1	T-Fuel	Spec.Vol	DP2	T-Fuel	Spec.Vol	DP3	T-Fuel	Spec.Vol
1	1.423	721.9	0.0226	3.843	795.8	0.0226	8.250	1093.6	0.0241
2	2.720	839.8	0.0226	6.783	913.1	0.0225	13.381	1223.2	0.0239
3	3.670	924.3	0.0225	8.500	953.7	0.0224	15.646	1231.2	0.0237
4	4.311	978.6	0.0224	9.373	956.3	0.0223	16.432	1204.6	0.0234
5	4.725	1011.4	0.0223	9.776	944.7	0.0222	16.621	1177.6	0.0232
6	4.989	1030.7	0.0222	9.949	930.5	0.0221	16.613	1158.2	0.0230
7	5.155	1041.7	0.0221	10.023	918.3	0.0220	16.563	1145.4	0.0228
8	5.258	1048.1	0.0220	10.065	909.6	0.0219	16.525	1136.7	0.0226
9	5.314	1051.8	0.0219	10.105	905.0	0.0218	16.510	1130.0	0.0224
10	5.324	1053.0	0.0218	10.151	904.9	0.0218	16.521	1124.6	0.0222
11	5.274	1050.4	0.0217	10.190	909.6	0.0217	16.552	1121.1	0.0221
12	5.129	1040.3	0.0215	10.174	918.5	0.0216	16.578	1121.5	0.0219
13	4.822	1015.8	0.0215	9.981	928.7	0.0215	16.487	1128.3	0.0217
14	4.245	965.1	0.0214	9.341	931.3	0.0214	15.929	1138.6	0.0216
15	3.252	871.9	0.0213	7.736	899.6	0.0213	13.950	1126.6	0.0214
16	1.722	721.6	0.0212	4.451	777.6	0.0213	8.632	996.5	0.0213

Axial Node	Burnup DP3 to SP37			Burnup SP37 to SP38		
	SP37	T-Fuel	Spec.Vol	SP38	T-Fuel	Spec. Vol
1	12.567	938.8	0.0241	17.360	911.0	0.0237
2	19.451	1013.4	0.0239	26.353	984.9	0.0236
3	22.096	1029.0	0.0237	29.863	1015.4	0.0234
4	22.867	1041.5	0.0235	31.057	1025.4	0.0232
5	23.008	1055.8	0.0233	31.428	1027.7	0.0230
6	22.992	1069.8	0.0231	31.540	1026.7	0.0228
7	22.969	1081.9	0.0229	31.586	1024.2	0.0226
8	22.971	1091.6	0.0227	31.617	1021.0	0.0225
9	22.998	1098.7	0.0226	31.643	1017.3	0.0223
10	23.048	1103.7	0.0224	31.665	1013.2	0.0221
11	23.128	1107.7	0.0222	31.683	1008.0	0.0220
12	23.233	1112.9	0.0220	31.680	1000.9	0.0218
13	23.281	1122.3	0.0218	31.548	990.1	0.0217
14	22.884	1136.3	0.0216	30.839	973.1	0.0215
15	20.722	1136.2	0.0214	28.023	942.7	0.0214
16	13.522	1029.9	0.0213	18.750	864.4	0.0213

Datapoint or Statepoint	EFFD / Cycle
SP36	0.0 / Cy1
DP1	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup - GWd/MTU
 T-Fuel - °F
 Spec. Vol. - ft³ / lbm

Table 5.2.8-10. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A29

Axial Node	SP36 to DP1			DP1 to DP2			DP2 to DP3		
	Burnup DP1	T-Fuel	Spec.Vol	Burnup DP2	T-Fuel	Spec.Vol	Burnup DP3	T-Fuel	Spec.Vol
1	2.092	799.5	0.0234	5.508	889.5	0.0233	9.743	1053.1	0.0239
2	4.020	969.2	0.0233	9.738	1036.2	0.0232	16.034	1163.7	0.0237
3	5.458	1088.2	0.0232	12.276	1080.2	0.0230	19.048	1159.0	0.0235
4	6.428	1161.5	0.0231	13.583	1081.0	0.0228	20.221	1126.4	0.0232
5	7.058	1205.0	0.0229	14.199	1064.9	0.0227	20.591	1097.7	0.0230
6	7.465	1230.5	0.0227	14.479	1045.6	0.0225	20.668	1077.3	0.0228
7	7.728	1245.6	0.0226	14.616	1029.1	0.0224	20.663	1063.7	0.0227
8	7.899	1255.2	0.0224	14.704	1017.6	0.0223	20.655	1054.1	0.0225
9	8.000	1261.6	0.0222	14.787	1011.5	0.0221	20.669	1046.4	0.0223
10	8.034	1265.2	0.0221	14.878	1011.2	0.0220	20.710	1040.1	0.0222
11	7.979	1264.2	0.0219	14.958	1017.2	0.0219	20.770	1035.7	0.0220
12	7.782	1253.7	0.0217	14.961	1029.4	0.0217	20.804	1035.2	0.0218
13	7.343	1224.4	0.0216	14.716	1044.9	0.0216	20.657	1041.1	0.0217
14	6.496	1159.9	0.0214	13.835	1052.4	0.0215	19.879	1052.8	0.0215
15	5.009	1034.3	0.0213	11.552	1020.8	0.0214	17.311	1050.7	0.0214
16	2.675	814.8	0.0213	6.745	876.5	0.0213	10.697	945.7	0.0213

Axial Node	DP3 to SP37			SP37 to SP38		
	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec.Vol
1	13.860	904.7	0.0238	18.660	899.5	0.0235
2	21.799	962.4	0.0237	28.700	972.2	0.0234
3	25.149	978.7	0.0235	32.822	996.0	0.0232
4	26.287	994.1	0.0234	34.276	1001.3	0.0230
5	26.595	1008.2	0.0232	34.730	999.3	0.0229
6	26.649	1020.2	0.0230	34.850	995.1	0.0227
7	26.656	1030.4	0.0228	34.874	990.0	0.0225
8	26.676	1038.4	0.0226	34.874	984.6	0.0224
9	26.719	1044.1	0.0225	34.870	978.9	0.0222
10	26.787	1047.9	0.0223	34.866	972.8	0.0221
11	26.881	1050.8	0.0221	34.861	966.0	0.0219
12	26.984	1055.3	0.0219	34.828	957.8	0.0218
13	26.970	1064.5	0.0218	34.635	947.3	0.0216
14	26.365	1078.7	0.0216	33.758	932.4	0.0215
15	23.679	1079.1	0.0214	30.477	904.2	0.0214
16	15.367	993.4	0.0213	20.208	830.4	0.0213

Datapoint or

Statepoint	EFPD/Cycle
SP36	0.0 / Cy1
DP1	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ /lbm

Table 5.2.8-11. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A29a

Axial Node	SP36 to DP1			DP1 to DP2			DP2 to DP3		
	Burnup DP1	T-Fuel	Spec.Vol	Burnup DP2	T-Fuel	Spec.Vol	Burnup DP3	T-Fuel	Spec.Vol
1	2.092	799.5	0.0234	5.508	889.5	0.0233	9.743	1053.1	0.0239
2	4.020	969.2	0.0233	9.738	1036.2	0.0232	16.034	1163.7	0.0237
3	5.458	1088.2	0.0232	12.276	1080.2	0.0230	19.048	1159.0	0.0235
4	6.428	1161.5	0.0231	13.583	1081.0	0.0228	20.221	1126.4	0.0232
5	7.058	1205.0	0.0229	14.199	1064.9	0.0227	20.591	1097.7	0.0230
6	7.465	1230.5	0.0227	14.479	1045.6	0.0225	20.668	1077.3	0.0228
7	7.728	1245.6	0.0226	14.616	1029.1	0.0224	20.663	1063.7	0.0227
8	7.899	1255.2	0.0224	14.704	1017.6	0.0223	20.655	1054.1	0.0225
9	8.000	1261.6	0.0222	14.787	1011.5	0.0221	20.669	1046.4	0.0223
10	8.034	1265.2	0.0221	14.878	1011.2	0.0220	20.710	1040.1	0.0222
11	7.979	1264.2	0.0219	14.958	1017.2	0.0219	20.770	1035.7	0.0220
12	7.782	1253.7	0.0217	14.961	1029.4	0.0217	20.804	1035.2	0.0218
13	7.343	1224.4	0.0216	14.716	1044.9	0.0216	20.657	1041.1	0.0217
14	6.496	1159.9	0.0214	13.835	1052.4	0.0215	19.879	1052.8	0.0215
15	5.009	1034.3	0.0213	11.552	1020.8	0.0214	17.311	1050.7	0.0214
16	2.675	814.8	0.0213	6.745	876.5	0.0213	10.697	945.7	0.0213

Axial Node	DP3 to SP37			SP37 to SP38		
	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec.Vol
1	13.860	904.7	0.0238	15.489	673.7	0.0220
2	21.808	962.4	0.0237	24.293	704.2	0.0219
3	25.166	978.7	0.0235	27.998	714.0	0.0219
4	26.309	994.1	0.0234	29.281	715.3	0.0218
5	26.619	1008.2	0.0232	29.651	714.1	0.0218
6	26.673	1020.2	0.0230	29.729	712.1	0.0217
7	26.682	1030.4	0.0228	29.739	709.9	0.0217
8	26.702	1038.4	0.0226	29.748	707.5	0.0216
9	26.745	1044.1	0.0225	29.771	705.1	0.0216
10	26.813	1047.9	0.0223	29.810	702.7	0.0215
11	26.908	1050.8	0.0221	29.867	700.0	0.0215
12	27.011	1055.3	0.0219	29.916	696.8	0.0214
13	26.997	1064.5	0.0218	29.824	692.7	0.0214
14	26.391	1078.7	0.0216	29.085	686.5	0.0213
15	23.702	1079.1	0.0214	26.095	674.2	0.0213
16	15.382	993.4	0.0213	16.974	643.5	0.0212

Datapoint or Statepoint	EFPD / Cycle
SP36	0.0 / Cy1
DP1	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ / lbm

Table 5.2.8-12. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A30

Axial Node	Burnup SP36 to DP1			Burnup DP1 to DP2			Burnup DP2 to DP3		
	DP1	T-Fuel	Spec.Vol.	DP2	T-Fuel	Spec.Vol.	DP3	T-Fuel	Spec.Vol.
1	2.420	836.7	0.0239	6.290	933.2	0.0237	9.164	980.5	0.0240
2	4.727	1036.3	0.0238	11.304	1096.2	0.0236	16.696	1130.1	0.0238
3	6.474	1174.0	0.0237	14.409	1144.3	0.0234	20.780	1130.0	0.0236
4	7.646	1256.2	0.0235	16.009	1146.6	0.0232	22.462	1106.7	0.0233
5	8.409	1305.5	0.0233	16.771	1129.4	0.0230	23.131	1088.0	0.0231
6	8.907	1335.2	0.0231	17.131	1108.4	0.0228	23.399	1074.2	0.0229
7	9.236	1353.7	0.0229	17.319	1090.3	0.0226	23.526	1064.9	0.0227
8	9.453	1365.8	0.0227	17.448	1077.4	0.0225	23.620	1058.3	0.0226
9	9.588	1374.3	0.0224	17.569	1070.6	0.0223	23.720	1053.1	0.0224
10	9.643	1379.9	0.0222	17.698	1070.3	0.0221	23.836	1048.6	0.0222
11	9.592	1380.4	0.0220	17.814	1077.3	0.0220	23.951	1045.1	0.0220
12	9.370	1370.3	0.0218	17.837	1091.4	0.0218	23.995	1043.8	0.0219
13	8.856	1338.3	0.0216	17.566	1109.3	0.0217	23.769	1046.0	0.0217
14	7.851	1266.7	0.0215	16.542	1117.7	0.0215	22.752	1049.4	0.0215
15	6.070	1126.1	0.0213	13.847	1083.7	0.0214	19.678	1041.2	0.0214
16	3.254	870.3	0.0213	8.132	932.5	0.0213	12.123	939.3	0.0213

Axial Node	Burnup DP3 to SP37			Burnup SP37 to SP38		
	SP37	T-Fuel	Spec.Vol.	SP38	T-Fuel	Spec. Vol.
1	11.965	774.7	0.0237	17.469	952.5	0.0236
2	21.752	799.9	0.0237	29.278	1006.6	0.0234
3	26.533	869.0	0.0236	34.621	1016.4	0.0232
4	28.569	979.8	0.0234	36.789	1013.4	0.0230
5	29.274	1011.0	0.0232	37.540	1006.8	0.0229
6	29.548	1024.3	0.0230	37.809	999.2	0.0227
7	29.700	1034.1	0.0229	37.922	991.5	0.0225
8	29.829	1041.6	0.0227	37.983	983.7	0.0224
9	29.965	1047.0	0.0225	38.029	975.7	0.0222
10	30.116	1050.7	0.0223	38.068	967.5	0.0220
11	30.272	1053.8	0.0221	38.093	958.8	0.0219
12	30.384	1058.2	0.0219	38.053	949.3	0.0218
13	30.272	1066.6	0.0218	37.768	938.6	0.0216
14	29.382	1078.3	0.0216	36.651	924.4	0.0215
15	26.131	1072.7	0.0214	32.902	896.9	0.0214
16	16.855	985.0	0.0213	21.794	827.2	0.0213

Datapoint or Statepoint	EFPD / Cycle
SP36	0.0 / Cy1
DP1	187.06 / Cy1
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ / lbm

Table 5.2.8-13. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly A31

Axial Node	SP36 to DP1			DP1 to DP2			DP2 to DP3		
	Burnup DP1	T-Fuel	Spec.Vol	Burnup DP2	T-Fuel	Spec.Vol	Burnup DP3	T-Fuel	Spec.Vol
1	1.271	703.5	0.0225	3.396	771.1	0.0225	7.475	1091.8	0.0243
2	2.465	811.4	0.0224	6.149	886.5	0.0224	12.476	1232.3	0.0241
3	3.371	891.8	0.0224	7.862	933.7	0.0224	14.916	1248.0	0.0238
4	3.985	944.9	0.0223	8.759	940.7	0.0223	15.859	1227.0	0.0236
5	4.384	977.1	0.0222	9.179	931.8	0.0222	16.160	1204.9	0.0233
6	4.638	996.2	0.0221	9.363	918.9	0.0221	16.231	1189.1	0.0231
7	4.801	1007.6	0.0220	9.446	907.4	0.0220	16.241	1178.9	0.0229
8	4.903	1014.5	0.0219	9.494	899.1	0.0219	16.248	1172.2	0.0227
9	4.960	1018.7	0.0218	9.539	894.7	0.0218	16.271	1167.2	0.0225
10	4.974	1020.4	0.0217	9.588	894.6	0.0217	16.311	1163.2	0.0223
11	4.931	1018.3	0.0216	9.630	899.1	0.0216	16.360	1160.6	0.0221
12	4.796	1008.7	0.0215	9.615	907.6	0.0216	16.386	1161.0	0.0219
13	4.507	985.1	0.0214	9.425	917.1	0.0215	16.269	1166.1	0.0218
14	3.964	937.1	0.0214	8.795	917.3	0.0214	15.664	1172.6	0.0216
15	3.027	848.4	0.0213	7.227	881.9	0.0213	13.649	1155.2	0.0214
16	1.599	708.7	0.0212	4.108	760.7	0.0213	8.406	1016.1	0.0213

Axial Node	DP3 to SP37			SP37 to SP38		
	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec. Vol
1	11.591	918.0	0.0242	16.153	898.0	0.0236
2	18.481	993.6	0.0240	25.154	969.4	0.0235
3	21.464	1022.9	0.0239	29.024	1000.5	0.0233
4	22.511	1055.8	0.0237	30.519	1012.3	0.0231
5	22.822	1079.1	0.0235	31.081	1016.0	0.0230
6	22.908	1094.7	0.0232	31.320	1016.2	0.0228
7	22.957	1107.1	0.0230	31.462	1014.7	0.0226
8	23.016	1116.9	0.0228	31.576	1012.6	0.0224
9	23.091	1124.3	0.0226	31.678	1010.3	0.0223
10	23.182	1129.8	0.0224	31.771	1007.6	0.0221
11	23.290	1134.4	0.0222	31.849	1004.1	0.0220
12	23.403	1140.2	0.0220	31.879	998.5	0.0218
13	23.421	1149.7	0.0218	31.723	988.6	0.0216
14	22.952	1162.3	0.0216	30.896	970.0	0.0215
15	20.700	1159.6	0.0214	27.860	933.8	0.0214
16	13.465	1046.1	0.0213	18.436	849.4	0.0213

Datapoint or Statpoint	FFPD/Cycle
SP36	0.0/Cy1
DP1	187.06/Cy1
DP2	0.0/Cy2
DP3	145.3/Cy2
SP37	0.0/Cy3
SP38	210.9/Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ /lbm

Table 5.2.8-14. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly B14

Axial Node	Burnup DP2 to DP3			Burnup DP3 to SP37			Burnup SP37 to SP38		
	Burnup DP3	T-Fuel	Spec.Vol	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec.Vol
1	4.030	1133.0	0.0247	8.416	1021.5	0.0248	14.230	1010.1	0.0244
2	6.098	1331.2	0.0245	12.502	1139.3	0.0246	21.148	1129.7	0.0242
3	7.010	1402.7	0.0242	14.182	1189.7	0.0244	23.957	1160.3	0.0239
4	7.309	1417.7	0.0239	14.724	1217.5	0.0241	24.976	1165.6	0.0237
5	7.373	1414.6	0.0236	14.890	1239.7	0.0239	25.361	1164.0	0.0234
6	7.380	1409.4	0.0234	14.985	1259.7	0.0236	25.552	1159.2	0.0232
7	7.391	1406.2	0.0231	15.096	1277.5	0.0234	25.687	1152.9	0.0230
8	7.418	1405.4	0.0229	15.232	1293.0	0.0231	25.801	1146.0	0.0227
9	7.458	1406.3	0.0227	15.384	1306.3	0.0229	25.895	1138.9	0.0225
10	7.507	1408.2	0.0224	15.545	1317.6	0.0226	25.968	1131.4	0.0223
11	7.563	1411.0	0.0222	15.720	1328.8	0.0224	26.022	1123.1	0.0221
12	7.618	1414.2	0.0220	15.911	1341.1	0.0221	26.050	1113.1	0.0219
13	7.633	1414.7	0.0218	16.064	1354.3	0.0219	25.979	1100.0	0.0217
14	7.453	1398.7	0.0216	15.904	1359.3	0.0217	25.455	1080.1	0.0216
15	6.674	1326.6	0.0214	14.558	1316.2	0.0215	23.265	1045.6	0.0214
16	4.476	1107.3	0.0213	9.998	1144.7	0.0213	15.987	932.5	0.0213

Table 5.2.8-15. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly B15

Axial Node	Burnup DP2 to DP3			Burnup DP3 to SP37			Burnup SP37 to SP38		
	Burnup DP3	T-Fuel	Spec.Vol	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec.Vol
1	2.762	966.7	0.0237	5.898	915.5	0.0238	10.916	983.4	0.0240
2	4.552	1158.4	0.0236	9.386	1036.4	0.0236	17.109	1108.6	0.0239
3	5.355	1227.7	0.0234	10.822	1076.5	0.0235	19.698	1146.7	0.0237
4	5.652	1246.0	0.0232	11.328	1096.5	0.0233	20.700	1152.4	0.0234
5	5.748	1247.5	0.0230	11.512	1112.0	0.0231	21.122	1149.3	0.0232
6	5.781	1245.3	0.0228	11.615	1126.3	0.0230	21.336	1143.7	0.0230
7	5.807	1243.8	0.0227	11.715	1139.3	0.0228	21.477	1137.4	0.0228
8	5.839	1243.8	0.0225	11.827	1150.7	0.0226	21.584	1130.8	0.0226
9	5.879	1245.0	0.0223	11.947	1160.4	0.0224	21.668	1124.3	0.0224
10	5.924	1247.0	0.0221	12.074	1168.6	0.0222	21.729	1117.6	0.0222
11	5.971	1249.4	0.0220	12.207	1176.1	0.0221	21.764	1110.4	0.0220
12	6.008	1251.4	0.0218	12.336	1183.6	0.0219	21.751	1101.9	0.0219
13	5.990	1249.3	0.0217	12.401	1190.9	0.0217	21.609	1090.9	0.0217
14	5.781	1230.6	0.0215	12.161	1191.4	0.0216	21.020	1075.2	0.0215
15	5.033	1159.5	0.0214	10.890	1157.2	0.0214	18.913	1041.4	0.0214
16	3.045	943.3	0.0213	6.888	997.2	0.0213	12.312	924.4	0.0213

Datapoint or

Statepoint	EFPD / Cycle
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ / lbm

Table 5.2.8-16. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly B19

Axial Node	Burnup DP2 to DP3			Burnup DP3 to SP37			Burnup SP37 to SP38		
	Burnup DP3	T-Fuel	Spec.Vol	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec.Vol
1	4.418	1172.9	0.0247	9.054	1024.4	0.0249	14.010	947.8	0.0241
2	6.370	1357.2	0.0244	12.974	1135.9	0.0247	20.566	1065.0	0.0239
3	7.170	1418.1	0.0241	14.497	1188.2	0.0244	23.258	1101.6	0.0237
4	7.366	1423.2	0.0239	14.896	1219.8	0.0242	24.217	1112.7	0.0235
5	7.347	1412.8	0.0236	14.950	1245.8	0.0239	24.565	1114.9	0.0232
6	7.295	1402.6	0.0233	14.966	1267.9	0.0237	24.738	1113.2	0.0230
7	7.263	1395.9	0.0231	15.019	1286.9	0.0234	24.870	1109.7	0.0228
8	7.254	1392.4	0.0229	15.108	1302.9	0.0232	24.989	1105.4	0.0226
9	7.263	1390.8	0.0226	15.217	1316.3	0.0229	25.094	1100.9	0.0224
10	7.283	1390.5	0.0224	15.338	1327.7	0.0227	25.181	1096.1	0.0222
11	7.317	1391.4	0.0222	15.481	1339.0	0.0224	25.254	1090.5	0.0220
12	7.366	1393.9	0.0220	15.661	1351.6	0.0222	25.307	1082.6	0.0219
13	7.406	1396.1	0.0218	15.853	1365.8	0.0219	25.276	1070.0	0.0217
14	7.307	1386.2	0.0216	15.816	1373.1	0.0217	24.820	1048.1	0.0215
15	6.698	1327.4	0.0214	14.722	1333.5	0.0215	22.776	1007.6	0.0214
16	4.770	1133.8	0.0213	10.570	1165.0	0.0213	15.942	890.5	0.0213

Table 5.2.8-17. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly B21

Axial Node	Burnup DP2 to DP3			Burnup DP3 to SP37			Burnup SP37 to SP38		
	Burnup DP3	T-Fuel	Spec.Vol	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec.Vol
1	2.756	967.8	0.0238	5.890	916.0	0.0238	10.185	930.1	0.0237
2	4.577	1163.3	0.0237	9.440	1039.1	0.0237	16.306	1053.8	0.0236
3	5.419	1236.3	0.0235	10.951	1081.0	0.0235	18.993	1094.3	0.0234
4	5.755	1258.0	0.0233	11.523	1102.8	0.0234	20.076	1101.0	0.0232
5	5.880	1261.8	0.0231	11.756	1119.4	0.0232	20.548	1098.0	0.0230
6	5.934	1261.1	0.0229	11.892	1134.5	0.0230	20.795	1092.5	0.0228
7	5.974	1260.7	0.0227	12.016	1148.2	0.0228	20.962	1086.4	0.0226
8	6.018	1261.7	0.0225	12.148	1160.0	0.0226	21.097	1080.3	0.0225
9	6.070	1263.7	0.0223	12.287	1170.1	0.0224	21.212	1074.3	0.0223
10	6.126	1266.5	0.0222	12.432	1178.7	0.0223	21.307	1068.5	0.0221
11	6.182	1269.6	0.0220	12.581	1186.6	0.0221	21.378	1062.4	0.0220
12	6.223	1271.9	0.0218	12.719	1194.4	0.0219	21.397	1055.2	0.0218
13	6.198	1269.2	0.0217	12.775	1201.5	0.0217	21.264	1045.5	0.0216
14	5.964	1248.4	0.0215	12.495	1201.3	0.0216	20.629	1030.2	0.0215
15	5.165	1173.2	0.0214	11.138	1164.4	0.0214	18.390	994.2	0.0214
16	3.101	950.0	0.0213	6.997	1001.8	0.0213	11.750	878.8	0.0213

Datapoint or Statepoint
 DP2 0.0 / Cy2
 DP3 145.3 / Cy2
 SP37 0.0 / Cy3
 SP38 210.9 / Cy3

Burnup - GWd/MTU
 T-Fuel - °F
 Spec. Vol. - ft³/lbm

Table 5.2.8-18. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly B25

Axial Node	Burnup DP2 to DP3			Burnup DP3 to SP37			Burnup SP37 to SP38		
	Burnup DP3	T-Fuel	Spec.Vol	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec.Vol
1	3.682	1091.8	0.0244	7.724	988.5	0.0246	13.720	1022.9	0.0243
2	5.486	1273.7	0.0242	11.382	1106.2	0.0244	20.261	1147.8	0.0241
3	6.380	1346.6	0.0240	13.067	1155.9	0.0242	22.966	1173.7	0.0239
4	6.734	1367.3	0.0237	13.717	1187.3	0.0240	23.985	1173.4	0.0236
5	6.850	1368.7	0.0235	13.969	1212.2	0.0237	24.391	1167.0	0.0234
6	6.894	1366.3	0.0232	14.118	1233.3	0.0235	24.596	1159.4	0.0231
7	6.929	1365.0	0.0230	14.261	1251.4	0.0233	24.735	1151.3	0.0229
8	6.973	1365.5	0.0228	14.418	1267.0	0.0230	24.845	1142.9	0.0227
9	7.026	1367.4	0.0226	14.585	1280.3	0.0228	24.934	1134.4	0.0225
10	7.084	1370.2	0.0224	14.759	1291.9	0.0226	25.001	1125.7	0.0223
11	7.145	1373.5	0.0222	14.942	1302.6	0.0223	25.047	1116.5	0.0221
12	7.195	1376.4	0.0220	15.122	1313.9	0.0221	25.057	1106.1	0.0219
13	7.186	1374.7	0.0218	15.231	1325.2	0.0219	24.947	1093.7	0.0217
14	6.960	1354.2	0.0216	14.979	1326.4	0.0217	24.360	1077.4	0.0216
15	6.179	1280.4	0.0214	13.586	1281.8	0.0215	22.146	1046.9	0.0214
16	4.238	1081.2	0.0213	9.459	1119.7	0.0213	15.267	925.7	0.0213

Table 5.2.8-19. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly B26

Axial Node	Burnup DP2 to DP3			Burnup DP3 to SP37			Burnup SP37 to SP38		
	Burnup DP3	T-Fuel	Spec.Vol	Burnup SP37	T-Fuel	Spec.Vol	Burnup SP38	T-Fuel	Spec.Vol
1	2.154	882.3	0.0232	4.642	847.7	0.0233	7.904	847.9	0.0230
2	3.590	1046.5	0.0231	7.506	960.1	0.0232	12.672	946.7	0.0229
3	4.280	1111.7	0.0229	8.776	1002.5	0.0230	14.790	980.5	0.0228
4	4.568	1132.6	0.0228	9.282	1023.6	0.0229	15.673	988.4	0.0227
5	4.677	1136.6	0.0227	9.489	1039.5	0.0228	16.057	987.8	0.0225
6	4.721	1136.2	0.0225	9.603	1053.5	0.0226	16.258	984.4	0.0224
7	4.752	1135.7	0.0224	9.700	1065.5	0.0225	16.394	980.2	0.0223
8	4.784	1136.1	0.0222	9.801	1075.8	0.0223	16.505	975.9	0.0221
9	4.821	1137.5	0.0221	9.907	1084.5	0.0222	16.601	971.8	0.0220
10	4.861	1139.4	0.0220	10.017	1092.0	0.0221	16.683	967.9	0.0219
11	4.901	1141.6	0.0218	10.129	1098.8	0.0219	16.745	963.6	0.0218
12	4.925	1142.8	0.0217	10.228	1105.4	0.0218	16.762	958.3	0.0216
13	4.891	1139.0	0.0216	10.248	1110.9	0.0216	16.638	950.7	0.0215
14	4.679	1118.6	0.0215	9.972	1108.5	0.0215	16.069	937.2	0.0214
15	4.025	1051.4	0.0213	8.818	1073.0	0.0214	14.195	903.8	0.0213
16	2.413	864.9	0.0213	5.497	921.3	0.0213	8.944	803.2	0.0213

Datapoint

Statepoint	EFPD / Cycle
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ / lbm

Table 5.2.8-20. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly B29

Axial Node	Burnup DP2 to DP3			Burnup DP3 to SP37			Burnup SP37 to SP38		
	DP3	T-Fuel	Spec.Vol	SP37	T-Fuel	Spec.Vol	SP38	T-Fuel	Spec.Vol
1	2.973	1005.0	0.0241	6.290	916.9	0.0240	11.627	1002.9	0.0242
2	4.921	1210.1	0.0239	10.066	1037.8	0.0239	18.158	1127.3	0.0240
3	5.848	1284.8	0.0237	11.729	1086.2	0.0237	20.954	1161.1	0.0238
4	6.225	1306.3	0.0235	12.386	1118.2	0.0235	22.091	1164.1	0.0235
5	6.364	1309.1	0.0233	12.655	1142.8	0.0233	22.588	1159.7	0.0233
6	6.423	1307.8	0.0230	12.808	1162.1	0.0231	22.845	1153.5	0.0231
7	6.468	1307.0	0.0228	12.942	1177.7	0.0229	23.015	1146.8	0.0229
8	6.516	1307.7	0.0226	13.082	1190.4	0.0227	23.148	1140.0	0.0227
9	6.572	1309.6	0.0224	13.229	1200.8	0.0225	23.255	1133.2	0.0225
10	6.632	1312.3	0.0223	13.381	1209.6	0.0224	23.337	1126.1	0.0223
11	6.692	1315.3	0.0221	13.537	1217.5	0.0222	23.391	1118.4	0.0221
12	6.737	1317.7	0.0219	13.686	1225.4	0.0220	23.396	1109.3	0.0219
13	6.716	1315.3	0.0217	13.754	1233.0	0.0218	23.263	1098.1	0.0217
14	6.477	1294.5	0.0215	13.475	1233.9	0.0216	22.660	1083.0	0.0216
15	5.645	1217.7	0.0214	12.071	1198.1	0.0214	20.481	1054.1	0.0214
16	3.440	988.1	0.0213	7.680	1033.8	0.0213	13.484	941.1	0.0213

Table 5.2.8-21. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly B30

Axial Node	Burnup DP2 to DP3			Burnup DP3 to SP37			Burnup SP37 to SP38		
	DP3	T-Fuel	Spec.Vol	SP37	T-Fuel	Spec.Vol	SP38	T-Fuel	Spec.Vol
1	3.347	1063.1	0.0244	7.013	935.6	0.0243	13.250	1047.4	0.0245
2	5.303	1262.3	0.0242	10.849	1050.3	0.0242	20.025	1173.4	0.0243
3	6.321	1339.8	0.0239	12.706	1105.6	0.0240	22.965	1200.1	0.0240
4	6.736	1361.5	0.0237	13.457	1150.5	0.0238	24.132	1199.9	0.0238
5	6.883	1363.5	0.0235	13.759	1183.1	0.0236	24.610	1193.3	0.0235
6	6.946	1361.7	0.0232	13.928	1206.0	0.0234	24.847	1185.4	0.0233
7	6.994	1360.8	0.0230	14.078	1223.8	0.0231	25.002	1177.2	0.0230
8	7.048	1361.7	0.0228	14.234	1238.2	0.0229	25.119	1169.2	0.0228
9	7.110	1363.8	0.0226	14.399	1250.1	0.0227	25.212	1161.2	0.0226
10	7.176	1366.8	0.0224	14.568	1260.2	0.0225	25.280	1152.9	0.0223
11	7.242	1370.3	0.0222	14.743	1269.5	0.0223	25.324	1144.0	0.0221
12	7.295	1373.1	0.0220	14.915	1278.8	0.0221	25.329	1133.8	0.0219
13	7.282	1371.3	0.0218	15.010	1288.0	0.0218	25.205	1121.4	0.0218
14	7.038	1350.2	0.0216	14.738	1289.2	0.0216	24.584	1104.3	0.0216
15	6.178	1272.0	0.0214	13.279	1250.3	0.0214	22.286	1074.2	0.0214
16	4.032	1055.8	0.0213	8.925	1090.8	0.0213	15.128	953.4	0.0213

Datapoint

or Statenpoint	EFPD/Cycle
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ /lbm

Table 5.2.8-22. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly B31

Axial Node	Burnup DP2 to DP3			Burnup DP3 to SP37			Burnup SP37 to SP38		
	DP3	T-Fuel	Spec.Vol	SP37	T-Fuel	Spec.Vol	SP38	T-Fuel	Spec.Vol
1	2.076	877.0	0.0232	4.446	822.3	0.0232	7.029	790.0	0.0227
2	3.535	1044.1	0.0231	7.317	929.3	0.0231	11.455	875.1	0.0226
3	4.272	1111.7	0.0229	8.654	975.4	0.0230	13.496	903.4	0.0225
4	4.588	1132.5	0.0228	9.207	1004.1	0.0229	14.378	912.6	0.0224
5	4.711	1136.3	0.0227	9.438	1025.6	0.0227	14.776	914.5	0.0223
6	4.763	1135.8	0.0225	9.561	1041.9	0.0226	14.991	913.6	0.0222
7	4.798	1135.3	0.0224	9.660	1054.5	0.0225	15.144	911.7	0.0221
8	4.833	1135.7	0.0222	9.760	1064.6	0.0223	15.273	909.5	0.0220
9	4.873	1137.0	0.0221	9.863	1072.8	0.0222	15.391	907.3	0.0219
10	4.915	1138.9	0.0220	9.970	1079.7	0.0220	15.497	905.2	0.0218
11	4.956	1141.0	0.0218	10.078	1085.9	0.0219	15.586	902.7	0.0217
12	4.982	1142.2	0.0217	10.173	1092.0	0.0218	15.630	899.1	0.0216
13	4.947	1138.4	0.0216	10.191	1097.3	0.0216	15.532	892.5	0.0215
14	4.729	1117.9	0.0214	9.912	1095.2	0.0215	14.989	878.9	0.0214
15	4.049	1049.7	0.0213	8.740	1061.0	0.0214	13.171	847.9	0.0213
16	2.398	860.9	0.0213	5.403	911.8	0.0213	8.189	759.5	0.0213

Table 5.2.8-23. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C2

Axial Node	Burnup SP37 to SP38		
	SP38	T-Fuel	Spec.Vol
1	6.214	1156.6	0.0246
2	8.843	1332.1	0.0244
3	10.110	1400.0	0.0241
4	10.639	1414.0	0.0239
5	10.862	1411.3	0.0236
6	10.955	1405.3	0.0233
7	10.980	1399.0	0.0231
8	10.962	1393.0	0.0228
9	10.912	1387.4	0.0226
10	10.833	1381.7	0.0224
11	10.724	1375.5	0.0222
12	10.579	1367.7	0.0220
13	10.372	1356.1	0.0218
14	9.989	1332.3	0.0216
15	9.076	1271.7	0.0214
16	6.672	1106.5	0.0213

Datapoint or Statepoint

Datapoint or Statepoint	FFPD / Cycle
DP2	0.0 / Cy2
DP3	145.3 / Cy2
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ /lbm

Table 5.2.8-24. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C4

Axial Node	Burnup		SP37 to SP38	
	SP38	T-Fuel	Spec.Vol	
1	6.152	1150.1	0.0245	
2	8.404	1302.2	0.0243	
3	9.706	1374.2	0.0241	
4	10.305	1394.0	0.0238	
5	10.573	1394.7	0.0235	
6	10.694	1390.6	0.0233	
7	10.738	1385.4	0.0230	
8	10.736	1380.0	0.0228	
9	10.699	1374.7	0.0226	
10	10.630	1369.3	0.0224	
11	10.529	1363.2	0.0222	
12	10.386	1355.2	0.0220	
13	10.177	1343.1	0.0218	
14	9.780	1318.1	0.0216	
15	8.878	1257.7	0.0214	
16	6.857	1117.8	0.0213	

Table 5.2.8-25. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C6

Axial Node	Burnup		SP37 to SP38	
	SP38	T-Fuel	Spec.Vol	
1	5.458	1102.6	0.0245	
2	8.083	1283.4	0.0243	
3	9.427	1357.8	0.0241	
4	10.086	1380.8	0.0238	
5	10.432	1385.8	0.0236	
6	10.630	1385.8	0.0233	
7	10.751	1384.5	0.0231	
8	10.825	1383.0	0.0228	
9	10.865	1381.6	0.0226	
10	10.871	1380.3	0.0224	
11	10.839	1378.2	0.0222	
12	10.751	1373.9	0.0220	
13	10.567	1364.3	0.0218	
14	10.163	1340.4	0.0216	
15	9.178	1276.6	0.0214	
16	6.542	1097.0	0.0213	

Datapoint

or
Statepoint EFPD / Cycle
 SP37 0.0 / Cy3
 SP38 210.9 / Cy3

Burnup - GWd/MTU
 T-Fuel - °F
 Spec. Vol. - ft³ / lbm

Table 5.2.8-26. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C8

Axial Node	Burnup SP38	T-Fuel	SP37 to SP38 Spec.Vol
1	4.078	969.8	0.0240
2	6.703	1160.2	0.0238
3	7.992	1235.8	0.0236
4	8.638	1264.4	0.0234
5	9.000	1274.4	0.0232
6	9.230	1277.9	0.0230
7	9.395	1279.4	0.0228
8	9.524	1280.9	0.0226
9	9.628	1283.0	0.0224
10	9.708	1285.6	0.0222
11	9.756	1288.2	0.0220
12	9.743	1289.0	0.0219
13	9.603	1283.4	0.0217
14	9.159	1260.1	0.0215
15	7.945	1185.7	0.0214
16	4.858	967.1	0.0213

Table 5.2.8-27. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C14

Axial Node	Burnup SP38	T-Fuel	SP37 to SP38 Spec.Vol
1	5.588	1104.8	0.0246
2	8.059	1270.1	0.0244
3	9.401	1347.0	0.0242
4	10.119	1378.6	0.0239
5	10.527	1390.2	0.0237
6	10.786	1394.5	0.0234
7	10.968	1396.4	0.0232
8	11.102	1397.9	0.0229
9	11.203	1399.6	0.0227
10	11.271	1401.5	0.0224
11	11.298	1402.8	0.0222
12	11.256	1401.5	0.0220
13	11.078	1393.1	0.0218
14	10.592	1365.6	0.0216
15	9.420	1292.0	0.0214
16	6.724	1109.5	0.0213

Datapoint or

Statepoint	EFPD / Cycle
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Burnup	- GWd/MTU
T-Fuel	- °F
Spec. Vol.	- ft ³ / lbm

Table 5.2.8-28. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C15

Axial Node	SP37 to SP38		
	Burnup SP38	T-Fuel	Spec.Vol
1	4.151	977.1	0.0240
2	6.801	1168.5	0.0239
3	8.113	1245.2	0.0237
4	8.776	1274.6	0.0235
5	9.147	1285.0	0.0233
6	9.384	1288.8	0.0230
7	9.554	1290.5	0.0228
8	9.686	1292.2	0.0226
9	9.794	1294.4	0.0224
10	9.878	1297.3	0.0223
11	9.928	1300.0	0.0221
12	9.917	1301.0	0.0219
13	9.774	1295.4	0.0217
14	9.318	1271.3	0.0215
15	8.083	1195.9	0.0214
16	4.963	975.5	0.0213

Table 5.2.8-29. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C17

Axial Node	SP37 to SP38		
	Burnup SP38	T-Fuel	Spec.Vol
1	6.131	1144.6	0.0247
2	8.880	1322.0	0.0245
3	10.162	1391.3	0.0242
4	10.735	1411.3	0.0239
5	11.013	1413.5	0.0236
6	11.160	1410.6	0.0234
7	11.233	1406.5	0.0231
8	11.258	1402.4	0.0229
9	11.245	1398.7	0.0226
10	11.200	1395.0	0.0224
11	11.117	1390.7	0.0222
12	10.986	1384.5	0.0220
13	10.773	1373.7	0.0218
14	10.355	1349.5	0.0216
15	9.323	1283.7	0.0214
16	6.587	1098.8	0.0213

Datapoint or Statepoint
 SP37 EFPD/Cycle
 SP38 0.0/Cy3
 210.9/Cy3

Burnup - GWd/MTU
 T-Fuel - °F
 Spec. Vol. - ft³/lbm

Table 5.2.8-30. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C19

Axial Node	SP37 to SP38		
	Burnup SP38	T-Fuel	Spec.Vol
1	5.776	1118.8	0.0245
2	8.035	1269.2	0.0243
3	9.266	1339.0	0.0240
4	9.907	1365.7	0.0238
5	10.251	1373.5	0.0235
6	10.453	1374.6	0.0233
7	10.575	1373.6	0.0230
8	10.647	1372.1	0.0228
9	10.683	1370.6	0.0226
10	10.686	1369.1	0.0224
11	10.648	1366.6	0.0222
12	10.548	1361.6	0.0220
13	10.339	1350.4	0.0218
14	9.885	1323.1	0.0216
15	8.883	1257.7	0.0214
16	6.634	1103.2	0.0213

Table 5.2.8-31. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C21

Axial Node	SP37 to SP38		
	Burnup SP38	T-Fuel	Spec.Vol
1	3.777	940.2	0.0237
2	6.202	1120.2	0.0235
3	7.370	1191.3	0.0234
4	7.943	1217.4	0.0232
5	8.257	1226.1	0.0230
6	8.449	1228.5	0.0228
7	8.582	1229.0	0.0226
8	8.680	1229.4	0.0225
9	8.754	1230.3	0.0223
10	8.807	1231.8	0.0221
11	8.829	1233.0	0.0220
12	8.797	1232.5	0.0218
13	8.650	1226.0	0.0216
14	8.233	1202.7	0.0215
15	7.130	1131.6	0.0214
16	4.352	926.7	0.0213

Datapoint or Statepoint
 SP37 EFPD/Cycle 0.0/Cy3
 SP38 210.9/Cy3

Burnup - GWd/MTU
 T-Fuel - °F
 Spec. Vol. - ft³/lbm

Table 5.2.8-32. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C25

Axial Node	SP37 to SP38		
	Burnup SP38	T-Fuel	Spec.Vol
1	4.848	1039.9	0.0242
2	7.436	1220.1	0.0240
3	8.750	1294.4	0.0238
4	9.408	1321.8	0.0236
5	9.761	1329.9	0.0234
6	9.970	1331.3	0.0231
7	10.105	1330.7	0.0229
8	10.194	1330.1	0.0227
9	10.253	1329.9	0.0225
10	10.283	1330.1	0.0223
11	10.276	1329.9	0.0221
12	10.209	1327.6	0.0219
13	10.020	1318.8	0.0217
14	9.549	1292.2	0.0216
15	8.385	1218.9	0.0214
16	5.567	1023.9	0.0213

Table 5.2.8-33. Burnup and Thermal Hydraulic Feedback Parameters by Axial Node for Assembly C30

Axial Node	SP37 to SP38		
	Burnup SP38	T-Fuel	Spec.Vol
1	3.747	943.3	0.0235
2	6.224	1130.9	0.0234
3	7.399	1197.6	0.0232
4	7.913	1214.2	0.0231
5	8.150	1214.5	0.0229
6	8.264	1210.7	0.0227
7	8.317	1206.4	0.0225
8	8.336	1202.6	0.0224
9	8.331	1199.4	0.0222
10	8.305	1196.8	0.0221
11	8.254	1194.1	0.0219
12	8.164	1190.2	0.0218
13	7.999	1182.3	0.0216
14	7.634	1161.6	0.0215
15	6.663	1098.4	0.0214
16	4.103	905.3	0.0213

Datapoint
or
Statepoint

EFPD / Cycle
SP37 0.0 / Cy3
SP38 210.9 / Cy3

Burnup - GWd/MTU
T-Fuel - °F
Spec. Vol. - ft³ / lbm

5.2.9. RCCA Insertion History Data for Sequoyah Unit 2 Depletion Calculations

The RCCA insertion time, duration, and position were required to perform the fuel assembly depletion calculations in which an RCCA was inserted. Hardening (locally increasing the average energy of the neutron population due to less local thermalization and increased local capture of neutrons at thermal energies) the neutron spectrum in a particular axial region of an assembly at a time during its irradiation history affects the isotopic composition of the depleted fuel. The CRC depletion calculations for fuel assemblies with an RCCA insertion history required the knowledge of the RCCA insertion time in terms of the number of EFPDs inserted in each axial node for each statepoint depletion calculation. Tables 5.2.9-1 through 5.2.9-4 present the RCCA insertion time data required for the fuel assembly depletion calculations relevant to the Sequoyah Unit 2 CRC evaluations. The height corresponding to the axial nodes presented in Tables 5.2.9-1 through 5.2.9-4 is 22.86 cm. The top of node 1 begins at the top of the active fuel region.

Table 5.2.9-1. Rod Insertion Time by Axial Node for Assembly A6

Axial Node	Time Rod Inserted (EFPD) SP37 to SP38
1	154.1
2	28.1
3	11.8
4	3.6
5	0.0
6	0.0
7	0.0
8	0.0
9	0.0
10	0.0
11	0.0
12	0.0
13	0.0
14	0.0
15	0.0
16	0.0

Statepoint	EFPD / Cycle
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Table 5.2.9-2. Rod Insertion Time by Axial Node for Assembly A25

Axial Node	Time Rod Inserted (EFPD) SP37 to SP38
1	153.8
2	28.0
3	12.0
4	3.7
5	0.0
6	0.0
7	0.0
8	0.0
9	0.0
10	0.0
11	0.0
12	0.0
13	0.0
14	0.0
15	0.0
16	0.0

Statepoint	EFPD / Cycle
SP37	0.0 / Cy3
SP38	210.9 / Cy3

Table 5.2.9-3. Rod Insertion Time by Axial Node for Assembly A26

Axial Node	Time Rod Inserted (EFPD) SP37 to SP38
1	154.5
2	28.1
3	11.9
4	3.5
5	0.0
6	0.0
7	0.0
8	0.0
9	0.0
10	0.0
11	0.0
12	0.0
13	0.0
14	0.0
15	0.0
16	0.0

Statepoint	EFPD / Cycle
DB2	0.0 / Cy2
DB3	145.3 / Cy2
SP37	0.0 / Cy2

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Table 5.2.9-4. Rod Insertion Time by Axial Node for Assembly A30

Axial Node	Time Rod Inserted (EFPD)	
	DB2 to DB3	DB3 to SP37
1	79.5	104.0
2	13.1	19.4
3	0.0	12.4
4	0.0	0.0
5	0.0	0.0
6	0.0	0.0
7	0.0	0.0
8	0.0	0.0
9	0.0	0.0
10	0.0	0.0
11	0.0	0.0
12	0.0	0.0
13	0.0	0.0
14	0.0	0.0
15	0.0	0.0
16	0.0	0.0

Statepoint	EFPD/Cycle
DB2	0.0/Cy2
DB3	145.3/Cy2
SP37	0.0/Cy3

5.3. Assembly Depletion Calculation Procedure

The procedure for performing the fuel assembly SAS2H depletion calculations documented in this analysis was based on the utilization of the CRAFT, Version 5, software routine. The CRAFT software routine is described generally in Sections 5.6 and 5.7. The complete detailed description of the CRAFT, Version 5, software routine is provided in Attachment I of Reference 7.6. The procedure for performing a fuel assembly depletion calculation with CRAFT, Version 5, consisted of the following steps:

- Create a CRAFT input deck for the assembly depletion calculation.
- Assure that the CRAFT executable file, the CRAFT input deck entitled "datain", and the "sedexecute" executable file are in the same directory. The "sedexecute" executable file is a script file which is used in conjunction with the CRAFT code to create the consolidated output files described in Section 5.7.
- Execute CRAFT.
- Check and analyze the CRAFT generated SAS2H input decks and the SAS2H isotopic results.

The various CRAFT generated and consolidated SAS2H output files contain unique filenames which specify the following information:

- reactor identifier
- one-eighth core symmetry assembly number in current reactor cycle

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- axial node number
- reactor cycle number in which the SAS2H calculation begins
- EFPD statepoint at which the SAS2H calculation begins
- reactor cycle number in which the SAS2H calculation ends
- EFPD statepoint at which the SAS2H calculation ends.

A complete detailed description of the filename content and format is provided in Attachment I of Reference 7.6.

5.4. Path B Model Development for the Sequoyah Unit 2 Depletion Calculations

The SAS2H control module used ORIGEN-S to perform a point depletion calculation for the fuel assembly or section of the fuel assembly described in the SAS2H input deck. The ORIGEN-S calculational module used cell-weighted cross sections based on one-dimensional (1-D) transport calculations performed by XSDRNPM. One-dimensional transport calculations were performed on two models, Path A and Path B, to calculate energy dependent spatial neutron flux distributions necessary to perform cross section cell-weighting calculations.

The Path A model was simply a unit cell of the fuel assembly lattice containing a fuel rod. In the Path A model, the fuel pellet, gap, and clad were modeled explicitly. The only modification required to develop the Path A model was the conversion of the fuel assembly's square lattice unit cell perimeter to a radial perimeter conserving moderator volume within the unit cell (exterior to the fuel rod cladding). This modification was performed automatically by the SAS2H control module. A 1-D transport calculation was performed on the Path A model for each energy group, and the spatial flux distributions for each energy group were used to calculate cell-weighted cross sections for the fuel.

The Path B model was a larger representation of the assembly than the Path A model. The Path B model approximated spectral effects due to heterogeneity within the fuel assembly such as water gaps, burnable poison rods, control rods, or axial power shaping rods. Typically, fuel assemblies contain a number of similar non-fuel lattice cells dispersed somewhat uniformly throughout the assembly lattice. The structure of the Path B model was based on a uniform distribution of these non-fuel lattice cells. In reality, most fuel assemblies do not have uniformly distributed non-fuel lattice cells, but the approximation of uniformly distributed non-fuel lattice cells was considered acceptable within the fidelity of these calculations as documented in Section S2.2.3.1 of Volume 1, Rev. 5 in Reference 7.1.

The basic structure of the Path B model for the fuel assembly depletion calculations performed in this analysis included an inner region composed of a representation of the non-fuel assembly lattice cell. A region containing the homogenization of the Path A model surrounded the inner region in the Path B model. A final region representing the moderator in the assembly-to-assembly spacing surrounded the homogenized region in the Path B model. The size of each radial region that surrounded the inner region in the Path B model was determined by conserving both the fuel-to-moderator mass ratio and the fuel-to-absorber (either burnable poison or RCCA poison) mass ratio in the corresponding section of the fuel assembly. The cell-weighted cross sections from the Path A model were applied to the homogenized region during the Path B model transport calculations. New cell-weighted cross sections

for each energy group were then developed using the unit cell spatial flux distribution results from the Path B model transport calculations. These cell-weighted cross sections were ultimately used in point depletion calculations performed by ORIGEN-S to calculate both the depleted fuel and the depleted burnable poison (if present) isotopic compositions in the corresponding section of the fuel assembly. A detailed description of the calculations used to produce time-dependent cross sections by SAS2H is documented in Section S2.2.4 of Volume 1, Rev. 5 in Reference 7.1.

The Path B models for the various fuel assembly configurations had to be provided to the SAS2H control module. The primary concern in the development of the Path B model for PWR assemblies was the conservation of the fuel-to-moderator and the fuel-to-absorber mass ratios in the corresponding section of the assembly.

The Path B model development calculations for the Sequoyah Unit 2 depletion calculations are presented in Tables 5.4-1 through 5.4-20 and contain the following information:

- the fuel assembly section characteristics for which the Path B model is developed
- the required Path B model development input parameters
- the parameters calculated to determine the final Path B model dimensions
- references to equations from Table 5.4-21 that were used to calculate parameters
- the final Path B model dimension results.

Table 5.4-21 contains a listing of the equations referenced and utilized in each of the Path B model development calculations presented in Tables 5.4-1 through 5.4-20.

**Table 5.4-1. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2:
STD Assembly Type, Upper Guide Tube Section, No Insertion Assembly****Input Parameters**

Number of unit cells in assembly: 289
Number of fuel rods in assembly: 264
Number of guide tubes in assembly: 24
Rod pitch in assembly (cm): 1.25984
Fuel pellet diameter (cm): 0.81915
Fuel cladding outer diameter (cm): 0.94996
Upper Region guide tube outer diameter (cm): 1.22428
Upper Region guide tube inner diameter (cm): 1.14300
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Unit Volume Ratio Calculation

Identifier of Equation Utilized: 5.4-1
Fuel-to-Moderator Unit Volume Ratio = 0.51951

Moderator Unit Volume in Central Region of Path B Model

Identifier of Equation Utilized: 5.4-2
Moderator Unit Volume in Central Region of Path B Model = 1.43608

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model)

Identifier of Equation Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model)

Identifier of Equation Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87844

**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Region of the Path B Model**

Identifier of Equation Utilized: 5.4-6
**Number of Fuel Rod Unit Cells that must be Represented in
the Homogenized Region of the Path B Model = 10.56000**

Path B Model Dimensions

	Region #	Outer Radius (cm)	Region Description
Inner	1	0.57150	Water filled gap
	2	0.61214	Guide tube
	3	0.71079	Guide tube unit cell moderator
	4	2.41668	Homogenized region
Outer	5	2.42643	Moderator in the inter-assembly spacing

Notes: The Region 4 outer radius is calculated using Equation 5.4-7.
 The Region 5 outer radius is calculated using Equation 5.4-8.

Table 5.4-2. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2: STD Assembly Type, Lower Guide Tube Section, No Insertion Assembly

Input Parameters

Number of unit cells in assembly: 289
 Number of fuel rods in assembly: 264
 Number of guide tubes in assembly: 24
 Rod pitch in assembly (cm): 1.25984
 Fuel pellet diameter (cm): 0.81915
 Fuel cladding outer diameter (cm): 0.94996
 Lower Region guide tube outer diameter (cm): 1.08966
 Lower Region guide tube inner diameter (cm): 1.00838
 Instrument tube outer diameter (cm): 1.22428
 Instrument tube inner diameter (cm): 1.14300
 Assembly pitch (cm): 21.50364

Fuel-to-Moderator Unit Volume Ratio Calculation

Identifier of Equation Utilized: 5.4-1
 Fuel-to-Moderator Unit Volume Ratio = 0.51871

Moderator Unit Volume in Central Region of Path B Model

Identifier of Equation Utilized: 5.4-2
 Moderator Unit Volume in Central Region of Path B Model = 1.45326

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model)

Identifier of Equation Utilized: 5.4-3
 Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model)

Identifier of Equation Utilized: 5.4-4
 Moderator Unit Volume in Fuel Rod Unit Cell = 0.87844

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**Number of Fuel Rod Unit Cells that must be Represented
 in the Homogenized Region of the Path B Model**

Identifier of Equation Utilized: 5A-6
**Number of Fuel Rod Unit Cells that must be Represented in
 the Homogenized Region of the Path B Model = 10.56500**

Path B Model Dimensions

	<u>Region #</u>	<u>Outer Radius (cm)</u>	<u>Region Description</u>
Inner	1	0.50419	Water filled gap
	2	0.54483	Guide tube
	3	0.71079	Guide tube unit cell moderator
	4	2.41720	Homogenized region
Outer	5	2.42695	Moderator in the inter-assembly spacing

Notes: The Region 4 outer radius is calculated using Equation 5A-7.
The Region 5 outer radius is calculated using Equation 5A-8.

**Table 5A-3. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2:
 STD Assembly Type, Upper Guide Tube Section, RCCA Insertion**

Input Parameters

Number of unit cells in assembly: 289
Number of fuel rods in assembly: 264
Number of guide tubes in assembly: 24
Number of CR's in assembly: 24
Rod pitch in assembly (cm): 1.25984
Fuel pellet diameter (cm): 0.81915
Fuel cladding outer diameter (cm): 0.94996
Upper Region guide tube outer diameter (cm): 1.22428
Upper Region guide tube inner diameter (cm): 1.14300
CR cladding outer diameter (cm): 0.96774
CR cladding inner diameter (cm): 0.87376
CR absorber material diameter (cm): 0.86614
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Unit Volume Ratio Calculation

Identifier of Equation Utilized: 5A-1
Fuel-to-Moderator Unit Volume Ratio = 0.55617

Moderator Unit Volume in Central Region of Path B Model

Identifier of Equation Utilized: 5A-2
Moderator Unit Volume in Central Region of Path B Model = 0.70054

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model)

Identifier of Equation Utilized: 5.4-3
 Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model)

Identifier of Equation Utilized: 5.4-4
 Moderator Unit Volume in Fuel Rod Unit Cell = 0.87844

Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Region of the Path B Model

Identifier of Equation Utilized: 5.4-6
 Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Region of the Path B Model = 10.13437

Required Area of Control Rod Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
 Area = 0.54284

Path B Model Dimensions

	<u>Region #</u>	<u>Outer Radius (cm)</u>	<u>Region Description</u>
Inner	1	0.41568	Neutron absorber material
	2	0.43688	Gap
	3	0.48387	Control rod cladding
	4	0.57150	Water filled gap
	5	0.61214	Guide tube
	6	0.71079	Guide tube unit cell moderator
	7	2.37177	Homogenized region
Outer	8	2.38134	Moderator in the inter-assembly spacing

Notes: The Region 1 outer radius is calculated using Equation 5.4-11.
 The Region 7 outer radius is calculated using Equation 5.4-7.
 The Region 8 outer radius is calculated using Equation 5.4-8.

Table 5.4-4. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2: STD Assembly Type, Lower Guide Tube Section, RCCA Insertion

Input Parameters

Number of unit cells in assembly: 289
 Number of fuel rods in assembly: 264
 Number of guide tubes in assembly: 24
 Number of CR's in assembly: 24
 Rod pitch in assembly (cm): 1.25984
 Fuel pellet diameter (cm): 0.81915

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Fuel cladding outer diameter (cm): 0.94996
Lower Region guide tube outer diameter (cm): 1.08966
Lower Region guide tube inner diameter (cm): 1.00838
CR cladding outer diameter (cm): 0.96774
CR cladding inner diameter (cm): 0.87376
CR absorber material diameter (cm): 0.86614
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation

Identifier of Equation Utilized: 5A-1
Fuel-to-Moderator Unit Volume Ratio = 0.55526

Moderator Unit Volume in Central Region of Path B Model

Identifier of Equation Utilized: 5A-2
Moderator Unit Volume in Central Region of Path B Model = 0.71772

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model)

Identifier of Equation Utilized: 5A-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model)

Identifier of Equation Utilized: 5A-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87844

Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Region of the Path B Model

Identifier of Equation Utilized: 5A-6
Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Region of the Path B Model = 10.15350

Required Area of Control Rod Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5A-10
Area = 0.54386

Path B Model Dimensions

	<u>Region #</u>	<u>Outer Radius (cm)</u>	<u>Region Description</u>
Inner	1	0.41604	Neutron absorber material
	2	0.43688	Gap
	3	0.48387	Control rod cladding
	4	0.50419	Water filled gap
	5	0.54483	Guide tube

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	6	0.71079	Guide tube unit cell moderator
	7	2.37381	Homogenized region
Outer	8	2.38338	Moderator in the inter-assembly spacing

Notes: The Region 1 outer radius is calculated using Equation 5.4-11.
 The Region 7 outer radius is calculated using Equation 5.4-7.
 The Region 8 outer radius is calculated using Equation 5.4-8.

**Table 5.4-5. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2:
 STD Assembly Type, Upper Guide Tube Section, Pyrex BPRA Insertion (9 BPRs)**

Input Parameters

Number of unit cells in assembly: 289
 Number of fuel rods in assembly: 264
 Number of guide tubes in assembly: 24
 Number of BPRs in assembly: 9
 Rod pitch in assembly (cm): 1.25984
 Fuel pellet diameter (cm): 0.81915
 Fuel cladding outer diameter (cm): 0.94996
 Upper Region guide tube outer diameter (cm): 1.22428
 Upper Region guide tube inner diameter (cm): 1.14300
 BPR outer cladding outer diameter (cm): 0.96774
 BPR outer cladding inner diameter (cm): 0.87376
 BPR inner cladding outer diameter (cm): 0.46101
 BPR inner cladding inner diameter (cm): 0.42799
 BPR absorber material outer diameter (cm): 0.85344
 BPR absorber material inner diameter (cm): 0.48260
 Instrument tube outer diameter (cm): 1.22428
 Instrument tube inner diameter (cm): 1.14300
 Assembly pitch (cm): 21.50364

Fuel-to-Moderator Unit Volume Ratio Calculation

Identifier of Equation Utilized: 5.4-1
 Fuel-to-Moderator Unit Volume Ratio = 0.53268

Moderator Unit Volume in Central Region of Path B Model

Identifier of Equation Utilized: 5.4-2
 Moderator Unit Volume in Central Region of Path B Model = 0.70054

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model)

Identifier of Equation Utilized: 5.4-3
 Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model)

Identifier of Equation Utilized: 5.4-4
 Moderator Unit Volume in Fuel Rod Unit Cell = 0.87844

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Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Region of the Path B Model

Identifier of Equation Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Region of the Path B Model = 6.31586

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
Area = 0.08379

Path B Model Dimensions

	<u>Region #</u>	<u>Outer Radius (cm)</u>	<u>Region Description</u>
Inner	1	0.21400	Gap
	2	0.23051	BPR inner cladding
	3	0.24130	Gap
	4	0.29137	Burnable poison
	5	0.43688	Gap
	6	0.48387	BPR outer cladding
	7	0.57150	Water
	8	0.61214	Guide tube
	9	0.71079	Water
	10	1.92253	Homogenized region
Outer	11	1.93028	Water in the inter-assembly spacing

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
 The Region 10 outer radius is calculated using Equation 5.4-7.
 The Region 11 outer radius is calculated using Equation 5.4-8.

Table 5.4-6. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2: STD Assembly Type, Lower Guide Tube Section, Pyrex BPRA Insertion (9 BPRs)

Input Parameters

Number of unit cells in assembly: 289
 Number of fuel rods in assembly: 264
 Number of guide tubes in assembly: 24
 Number of BPRs in assembly: 9
 Rod pitch in assembly (cm): 1.25984
 Fuel pellet diameter (cm): 0.81915
 Fuel cladding outer diameter (cm): 0.94996
 Lower Region guide tube outer diameter (cm): 1.08966
 Lower Region guide tube inner diameter (cm): 1.00838
 BPR outer cladding outer diameter (cm): 0.96774
 BPR outer cladding inner diameter (cm): 0.87376
 BPR inner cladding outer diameter (cm): 0.46101
 BPR inner cladding inner diameter (cm): 0.42799
 BPR absorber material outer diameter (cm): 0.85344

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BPR absorber material inner diameter (cm): 0.48260
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.53184

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.71772

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model:**

Identifier of Equation(s) Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model = 6.38093

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
Area = 0.08465

Path B Unit Cell Model Dimensions:

		Outer Radius	
	<u>Zone #</u>	<u>(cm)</u>	<u>Zone Description</u>
Inner	1	0.21400	Gap
	2	0.23051	BPR inner cladding
	3	0.24130	Gap
	4	0.29184	Burnable poison
	5	0.43688	Gap
	6	0.48387	BPR outer cladding
	7	0.50419	Water
	8	0.54483	Guide tube
	9	0.71079	Water
	10	1.93106	Homogenized region
Outer	11	1.93885	Water in the assembly-to-assembly gap

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Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
The Zone 10 outer radius is calculated using Equation 5.4-7.
The Zone 11 outer radius is calculated using Equation 5.4-8.

**Table 5.4-7. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2:
STD Assembly Type, Upper Guide Tube Section, Pyrex BPRs Insertion (10 BPRs)**

Input Parameters

Number of unit cells in assembly: 289
Number of fuel rods in assembly: 264
Number of guide tubes in assembly: 24
Number of BPRs in assembly: 10
Rod pitch in assembly (cm): 1.25984
Fuel pellet diameter (cm): 0.81915
Fuel cladding outer diameter (cm): 0.94996
Upper Region guide tube outer diameter (cm): 1.22428
Upper Region guide tube inner diameter (cm): 1.14300
BPR outer cladding outer diameter (cm): 0.96774
BPR outer cladding inner diameter (cm): 0.87376
BPR inner cladding outer diameter (cm): 0.46101
BPR inner cladding inner diameter (cm): 0.42799
BPR absorber material outer diameter (cm): 0.85344
BPR absorber material inner diameter (cm): 0.4826
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.53418

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.70053

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Zone of the Path B Model:

Identifier of Equation(s) Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Zone of the Path B Model = 6.47860

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
Area = 0.09549

Path B Unit Cell Model Dimensions:

	Zone #	Outer Radius (cm)	Zone Description
Inner	1	0.21400	Gap
	2	0.23051	BPR inner cladding
	3	0.24130	Gap
	4	0.29769	Burnable poison
	5	0.43688	Gap
	6	0.48387	BPR outer cladding
	7	0.57150	Water
	8	0.61214	Guide tube
	9	0.71079	Water
	10	1.94380	Homogenized region
Outer	11	1.95163	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
 The Zone 10 outer radius is calculated using Equation 5.4-7.
 The Zone 11 outer radius is calculated using Equation 5.4-8.

Table 5.4-8. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2: STD Assembly Type, Lower Guide Tube Section, Pyrex BPRA Insertion (10 BPRs)

Input Parameters

Number of unit cells in assembly: 289
Number of fuel rods in assembly: 264
Number of guide tubes in assembly: 24
Number of BPRs in assembly: 10
Rod pitch in assembly (cm): 1.25984
Fuel pellet diameter (cm): 0.81915
Fuel cladding outer diameter (cm): 0.94996
Lower Region guide tube outer diameter (cm): 1.08966
Lower Region guide tube inner diameter (cm): 1.00838
BPR outer cladding outer diameter (cm): 0.96774
BPR outer cladding inner diameter (cm): 0.87376
BPR inner cladding outer diameter (cm): 0.46101
BPR inner cladding inner diameter (cm): 0.42799
BPR absorber material outer diameter (cm): 0.85344

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BPR absorber material inner diameter (cm): 0.48260
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5A-1
Fuel-to-Moderator Volume Ratio = 0.53334

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5A-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.71772

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5A-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5A-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model:**

Identifier of Equation(s) Utilized: 5A-6
Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model = 6.54300

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5A-10
Area = 0.09644

Path B Unit Cell Model Dimensions:

		Outer Radius	
	<u>Zone #</u>	<u>(cm)</u>	<u>Zone Description</u>
Inner	1	0.21400	Gap
	2	0.23051	BPR inner cladding
	3	0.24130	Gap
	4	0.29820	Burnable poison
	5	0.43688	Gap
	6	0.48387	BPR outer cladding
	7	0.50419	Water
	8	0.54483	Guide tube
	9	0.71079	Water
	10	1.95215	Homogenized region
Outer	11	1.96002	Water in the assembly-to-assembly gap

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Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
The Zone 10 outer radius is calculated using Equation 5.4-7.
The Zone 11 outer radius is calculated using Equation 5.4-8.

**Table 5.4-9. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2:
STD Assembly Type, Upper Guide Tube Section, Pyrex BPRA Insertion (20 BPRs)**

Input Parameters

Number of unit cells in assembly: 289
Number of fuel rods in assembly: 264
Number of guide tubes in assembly: 24
Number of BPRs in assembly: 20
Rod pitch in assembly (cm): 1.25984
Fuel pellet diameter (cm): 0.81915
Fuel cladding outer diameter (cm): 0.94996
Upper Region guide tube outer diameter (cm): 1.22428
Upper Region guide tube inner diameter (cm): 1.14300
BPR outer cladding outer diameter (cm): 0.96774
BPR outer cladding inner diameter (cm): 0.87376
BPR inner cladding outer diameter (cm): 0.46101
BPR inner cladding inner diameter (cm): 0.42799
BPR absorber material outer diameter (cm): 0.85344
BPR absorber material inner diameter (cm): 0.48260
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.54971

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.70053

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model:**

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Identifier of Equation(s) Utilized: 5A-6
 Number of Fuel Rod Unit Cells that must be Represented
 in the Homogenized Zone of the Path B Model = 8.72731

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5A-10
 Area = 0.25728

Path B Unit Cell Model Dimensions:

	Zone #	Outer Radius (cm)	Zone Description
Inner	1	0.21400	Gap
	2	0.23051	BPR inner cladding
	3	0.24130	Gap
	4	0.37433	Burnable poison
	5	0.43688	Gap
	6	0.48387	BPR outer cladding
	7	0.57150	Water
	8	0.61214	Guide tube
	9	0.71079	Water
	10	2.21685	Homogenized region
Outer	11	2.22579	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5A-11.
 The Zone 10 outer radius is calculated using Equation 5A-7.
 The Zone 11 outer radius is calculated using Equation 5A-8.

Table 5A-10. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2: STD Assembly Type, Lower Guide Tube Section, Pyrex BPR Insertion (20 BPRs)

Input Parameters

- Number of unit cells in assembly: 289
- Number of fuel rods in assembly: 264
- Number of guide tubes in assembly: 24
- Number of BPRs in assembly: 20
- Rod pitch in assembly (cm): 1.25984
- Fuel pellet diameter (cm): 0.81915
- Fuel cladding outer diameter (cm): 0.94996
- Lower Region guide tube outer diameter (cm): 1.08966
- Lower Region guide tube inner diameter (cm): 1.00838
- BPR outer cladding outer diameter (cm): 0.96774
- BPR outer cladding inner diameter (cm): 0.87376
- BPR inner cladding outer diameter (cm): 0.46101
- BPR inner cladding inner diameter (cm): 0.42799
- BPR absorber material outer diameter (cm): 0.85344
- BPR absorber material inner diameter (cm): 0.48260
- Instrument tube outer diameter (cm): 1.22428
- Instrument tube inner diameter (cm): 1.14300

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Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.54881

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.71772

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Zone of the Path B Model:

Identifier of Equation(s) Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Zone of the Path B Model = 8.77071

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
Area = 0.25856

Path B Unit Cell Model Dimensions:

	<u>Zone #</u>	<u>Outer Radius (cm)</u>	<u>Zone Description</u>
Inner	1	0.21400	Gap
	2	0.23051	BPR inner cladding
	3	0.24130	Gap
	4	0.37487	Burnable poison
	5	0.43688	Gap
	6	0.48387	BPR outer cladding
	7	0.50419	Water
	8	0.54483	Guide tube
	9	0.71079	Water
	10	2.22179	Homogenized region
Outer	11	2.23075	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
The Zone 10 outer radius is calculated using Equation 5.4-7.

The Zone 11 outer radius is calculated using Equation 5.4-8.

**Table 5.4-11. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2:
STD Assembly Type, Upper Guide Tube Section, WABA BPRA Insertion (8 BPRs)**

Input Parameters

Number of unit cells in assembly: 289
Number of fuel rods in assembly: 264
Number of guide tubes in assembly: 24
Number of BPRs in assembly: 8
Rod pitch in assembly (cm): 1.25984
Fuel pellet diameter (cm): 0.81915
Fuel cladding outer diameter (cm): 0.94996
Upper Region guide tube outer diameter (cm): 1.22428
Upper Region guide tube inner diameter (cm): 1.14300
BPR outer cladding outer diameter (cm): 0.96774
BPR outer cladding inner diameter (cm): 0.83570
BPR inner cladding outer diameter (cm): 0.67820
BPR inner cladding inner diameter (cm): 0.57150
BPR absorber material outer diameter (cm): 0.80770
BPR absorber material inner diameter (cm): 0.70610
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.52705

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.95706

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model:**

Identifier of Equation(s) Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model = 7.87854

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
 Area = 0.02884

Path B Unit Cell Model Dimensions:

	Zone #	Outer Radius (cm)	Zone Description
Inner	1	0.28575	Water
	2	0.33910	BPR inner cladding
	3	0.35305	Gap
	4	0.36582	Burnable poison
	5	0.41785	Gap
	6	0.48387	BPR outer cladding
	7	0.57150	Water
	8	0.61214	Guide tube
	9	0.71079	Water
	10	2.11793	Homogenized region
Outer	11	2.12647	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
 The Zone 10 outer radius is calculated using Equation 5.4-7.
 The Zone 11 outer radius is calculated using Equation 5.4-8.

Table 5.4-12. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2: STD Assembly Type, Lower Guide Tube Section, WABA BPRA Insertion (8 BPRs)

Input Parameters

Number of unit cells in assembly: 289
 Number of fuel rods in assembly: 264
 Number of guide tubes in assembly: 24
 Number of BPRs in assembly: 8
 Rod pitch in assembly (cm): 1.25984
 Fuel pellet diameter (cm): 0.81915
 Fuel cladding outer diameter (cm): 0.94996
 Lower Region guide tube outer diameter (cm): 1.08966
 Lower Region guide tube inner diameter (cm): 1.00838
 BPR outer cladding outer diameter (cm): 0.96774
 BPR outer cladding inner diameter (cm): 0.83570
 BPR inner cladding outer diameter (cm): 0.67820
 BPR inner cladding inner diameter (cm): 0.57150
 BPR absorber material outer diameter (cm): 0.80770
 BPR absorber material inner diameter (cm): 0.70610
 Instrument tube outer diameter (cm): 1.22428
 Instrument tube inner diameter (cm): 1.14300
 Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
 Fuel-to-Moderator Volume Ratio = 0.52623

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
 Moderator Unit Volume in Central Unit Cell of Path B Model = 0.97424

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
 Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
 Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Zone of the Path B Model:

Identifier of Equation(s) Utilized: 5.4-6
 Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Zone of the Path B Model = 7.91818

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
 Area = 0.02898

Path B Unit Cell Model Dimensions:

	Zone #	Outer Radius (cm)	Zone Description
Inner	1	0.28575	Water
	2	0.33910	BPR inner cladding
	3	0.35305	Gap
	4	0.36588	Burnable poison
	5	0.41785	Gap
	6	0.48387	BPR outer cladding
	7	0.50419	Water
	8	0.54483	Guide tube
	9	0.71079	Water
	10	2.12265	Homogenized region
Outer	11	2.13121	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
 The Zone 10 outer radius is calculated using Equation 5.4-7.
 The Zone 11 outer radius is calculated using Equation 5.4-8.

**Table 5.4-13. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2:
STD Assembly Type, Upper Guide Tube Section, WABA BPR Insertion (12 BPRs)****Input Parameters**

Number of unit cells in assembly: 289
Number of fuel rods in assembly: 264
Number of guide tubes in assembly: 24
Number of BPRs in assembly: 12
Rod pitch in assembly (cm): 1.25984
Fuel pellet diameter (cm): 0.81915
Fuel cladding outer diameter (cm): 0.94996
Upper Region guide tube outer diameter (cm): 1.22428
Upper Region guide tube inner diameter (cm): 1.14300
BPR outer cladding outer diameter (cm): 0.96774
BPR outer cladding inner diameter (cm): 0.83570
BPR inner cladding outer diameter (cm): 0.67820
BPR inner cladding inner diameter (cm): 0.57150
BPR absorber material outer diameter (cm): 0.80770
BPR absorber material inner diameter (cm): 0.70610
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.53091

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.95706

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model:**

Identifier of Equation(s) Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model = 8.37917

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Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
 Area = 0.04601

Path B Unit Cell Model Dimensions:

	Zone #	Outer Radius (cm)	Zone Description
Inner	1	0.28575	Water
	2	0.33910	BPR inner cladding
	3	0.35305	Gap
	4	0.37321	Burnable poison
	5	0.41785	Gap
	6	0.48387	BPR outer cladding
	7	0.57150	Water
	8	0.61214	Guide tube
	9	0.71079	Water
	10	2.17682	Homogenized region
Outer	11	2.18560	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
 The Zone 10 outer radius is calculated using Equation 5.4-7.
 The Zone 11 outer radius is calculated using Equation 5.4-8.

Table 5.4-14. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2: STD Assembly Type, Lower Guide Tube Section, WABA BPRA Insertion (12 BPRs)

Input Parameters

- Number of unit cells in assembly: 289
- Number of fuel rods in assembly: 264
- Number of guide tubes in assembly: 24
- Number of BPRs in assembly: 12
- Rod pitch in assembly (cm): 1.25984
- Fuel pellet diameter (cm): 0.81915
- Fuel cladding outer diameter (cm): 0.94996
- Lower Region guide tube outer diameter (cm): 1.08966
- Lower Region guide tube inner diameter (cm): 1.00838
- BPR outer cladding outer diameter (cm): 0.96774
- BPR outer cladding inner diameter (cm): 0.83570
- BPR inner cladding outer diameter (cm): 0.67820
- BPR inner cladding inner diameter (cm): 0.57150
- BPR absorber material outer diameter (cm): 0.80770
- BPR absorber material inner diameter (cm): 0.70610
- Instrument tube outer diameter (cm): 1.22428
- Instrument tube inner diameter (cm): 1.14300
- Assembly pitch (cm): 21.50364

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Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.53007

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.97424

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Zone of the Path B Model:

Identifier of Equation(s) Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Zone of the Path B Model = 8.41454

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
Area = 0.04620

Path B Unit Cell Model Dimensions:

		Outer Radius	
	<u>Zone #</u>	<u>(cm)</u>	<u>Zone Description</u>
Inner	1	0.28575	Water
	2	0.33910	BPR inner cladding
	3	0.35305	Gap
	4	0.37330	Burnable poison
	5	0.41785	Gap
	6	0.48387	BPR outer cladding
	7	0.50419	Water
	8	0.54483	Guide tube
	9	0.71079	Water
	10	2.18092	Homogenized region
Outer	11	2.18972	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
 The Zone 10 outer radius is calculated using Equation 5.4-7.
 The Zone 11 outer radius is calculated using Equation 5.4-8.

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STD Assembly Type, Upper Guide Tube Section, WABA BPRA Insertion (16 BPRs)****Input Parameters**

Number of unit cells in assembly: 289
Number of fuel rods in assembly: 264
Number of guide tubes in assembly: 24
Number of BPRs in assembly: 16
Rod pitch in assembly (cm): 1.25984
Fuel pellet diameter (cm): 0.81915
Fuel cladding outer diameter (cm): 0.94996
Upper Region guide tube outer diameter (cm): 1.22428
Upper Region guide tube inner diameter (cm): 1.14300
BPR outer cladding outer diameter (cm): 0.96774
BPR outer cladding inner diameter (cm): 0.83570
BPR inner cladding outer diameter (cm): 0.67820
BPR inner cladding inner diameter (cm): 0.57150
BPR absorber material outer diameter (cm): 0.80770
BPR absorber material inner diameter (cm): 0.70610
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.53482

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.95706

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model:**

Identifier of Equation(s) Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model = 8.94775

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Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
Area = 0.06551

Path B Unit Cell Model Dimensions:

		Outer Radius	Zone Description
	Zone #	(cm)	
Inner	1	0.28575	Water
	2	0.33910	BPR inner cladding
	3	0.35305	Gap
	4	0.38144	Burnable poison
	5	0.41785	Gap
	6	0.48387	BPR outer cladding
	7	0.57150	Water
	8	0.61214	Guide tube
	9	0.71079	Water
	10	2.24183	Homogenized region
Outer	11	2.25087	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
 The Zone 10 outer radius is calculated using Equation 5.4-7.
 The Zone 11 outer radius is calculated using Equation 5.4-8.

Table 5.4-16. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2: STD Assembly Type, Lower Guide Tube Section, WABA BPRA Insertion (16 BPRs)

Input Parameters

- Number of unit cells in assembly: 289
- Number of fuel rods in assembly: 264
- Number of guide tubes in assembly: 24
- Number of BPRs in assembly: 16
- Rod pitch in assembly (cm): 1.25984
- Fuel pellet diameter (cm): 0.81915
- Fuel cladding outer diameter (cm): 0.94996
- Lower Region guide tube outer diameter (cm): 1.08966
- Lower Region guide tube inner diameter (cm): 1.00838
- BPR outer cladding outer diameter (cm): 0.96774
- BPR outer cladding inner diameter (cm): 0.83570
- BPR inner cladding outer diameter (cm): 0.67820
- BPR inner cladding inner diameter (cm): 0.57150
- BPR absorber material outer diameter (cm): 0.80770
- BPR absorber material inner diameter (cm): 0.70610
- Instrument tube outer diameter (cm): 1.22428
- Instrument tube inner diameter (cm): 1.14300
- Assembly pitch (cm): 21.50364

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Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.53397

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.97424

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model:**

Identifier of Equation(s) Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model = 8.97729

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
Area = 0.06572

Path B Unit Cell Model Dimensions:

		Outer Radius	
	<u>Zone #</u>	<u>(cm)</u>	<u>Zone Description</u>
Inner	1	0.28575	Water
	2	0.33910	BPR inner cladding
	3	0.35305	Gap
	4	0.38153	Burnable poison
	5	0.41785	Gap
	6	0.48387	BPR outer cladding
	7	0.50419	Water
	8	0.54483	Guide tube
	9	0.71079	Water
	10	2.24516	Homogenized region
Outer	11	2.25421	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
The Zone 10 outer radius is calculated using Equation 5.4-7.
The Zone 11 outer radius is calculated using Equation 5.4-8.

**Table 5.4-17. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2:
STD Assembly Type, Upper Guide Tube Section, WABA BPRA Insertion (20 BPRs)****Input Parameters**

Number of unit cells in assembly: 289
Number of fuel rods in assembly: 264
Number of guide tubes in assembly: 24
Number of BPRs in assembly: 20
Rod pitch in assembly (cm): 1.25984
Fuel pellet diameter (cm): 0.81915
Fuel cladding outer diameter (cm): 0.94996
Lower Region guide tube outer diameter (cm): 1.22428
Lower Region guide tube inner diameter (cm): 1.14300
BPR outer cladding outer diameter (cm): 0.96774
BPR outer cladding inner diameter (cm): 0.83570
BPR inner cladding outer diameter (cm): 0.67820
BPR inner cladding inner diameter (cm): 0.57150
BPR absorber material outer diameter (cm): 0.80770
BPR absorber material inner diameter (cm): 0.70610
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.53879

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.95706

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model:**

Identifier of Equation(s) Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model = 9.59910

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
 Area = 0.08784

Path B Unit Cell Model Dimensions:

	Zone #	Outer Radius (cm)	Zone Description
Inner	1	0.28575	Water
	2	0.33910	BPR inner cladding
	3	0.35305	Gap
	4	0.39065	Burnable poison
	5	0.41785	Gap
	6	0.48387	BPR outer cladding
	7	0.57150	Water
	8	0.61214	Guide tube
	9	0.71079	Water
	10	2.31406	Homogenized region
Outer	11	2.32339	Water in the assembly-to-assembly gap

- Notes:
- The Region 4 outer radius is calculated using Equation 5.4-11.
 - The Zone 10 outer radius is calculated using Equation 5.4-7.
 - The Zone 11 outer radius is calculated using Equation 5.4-8.

Table 5.4-18. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2: STD Assembly Type, Lower Guide Tube Section, WABA BPRA Insertion (20 BPRs)

Input Parameters

- Number of unit cells in assembly: 289
- Number of fuel rods in assembly: 264
- Number of guide tubes in assembly: 24
- Number of BPRs in assembly: 20
- Rod pitch in assembly (cm): 1.25984
- Fuel pellet diameter (cm): 0.81915
- Fuel cladding outer diameter (cm): 0.94996
- Lower Region guide tube outer diameter (cm): 1.08966
- Lower Region guide tube inner diameter (cm): 1.00838
- BPR outer cladding outer diameter (cm): 0.96774
- BPR outer cladding inner diameter (cm): 0.83570
- BPR inner cladding outer diameter (cm): 0.67820
- BPR inner cladding inner diameter (cm): 0.57150
- BPR absorber material outer diameter (cm): 0.80770
- BPR absorber material inner diameter (cm): 0.70610
- Instrument tube outer diameter (cm): 1.22428
- Instrument tube inner diameter (cm): 1.14300
- Assembly pitch (cm): 21.50364

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Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
 Fuel-to-Moderator Volume Ratio = 0.53793

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
 Moderator Unit Volume in Central Unit Cell of Path B Model = 0.97424

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
 Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
 Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Zone of the Path B Model:

Identifier of Equation(s) Utilized: 5.4-6
 Number of Fuel Rod Unit Cells that must be Represented in the Homogenized Zone of the Path B Model = 9.62072

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
 Area = 0.08804

Path B Unit Cell Model Dimensions:

	Zone #	Outer Radius (cm)	Zone Description
Inner	1	0.28575	Water
	2	0.33910	BPR inner cladding
	3	0.35305	Gap
	4	0.39073	Burnable poison
	5	0.41785	Gap
	6	0.48387	BPR outer cladding
	7	0.50419	Water
	8	0.54483	Guide tube
	9	0.71079	Water
	10	2.31642	Homogenized region
Outer	11	2.32576	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
 The Zone 10 outer radius is calculated using Equation 5.4-7.
 The Zone 11 outer radius is calculated using Equation 5.4-8.

Title: Sequoyah Unit 2 CRC Depletion Calculations**Document Identifier: B00000000-01717-0210-00005 REV 00****Page 72 of 91****Table 5.4-19. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2:
STD Assembly Type, Upper Guide Tube Section, WABA BPRA Insertion (24 BPRs)****Input Parameters**

Number of unit cells in assembly: 289
Number of fuel rods in assembly: 264
Number of guide tubes in assembly: 24
Number of BPRs in assembly: 24
Rod pitch in assembly (cm): 1.25984
Fuel pellet diameter (cm): 0.81915
Fuel cladding outer diameter (cm): 0.94996
Lower Region guide tube outer diameter (cm): 1.22428
Lower Region guide tube inner diameter (cm): 1.14300
BPR outer cladding outer diameter (cm): 0.96774
BPR outer cladding inner diameter (cm): 0.83570
BPR inner cladding outer diameter (cm): 0.67820
BPR inner cladding inner diameter (cm): 0.57150
BPR absorber material outer diameter (cm): 0.80770
BPR absorber material inner diameter (cm): 0.70610
Instrument tube outer diameter (cm): 1.22428
Instrument tube inner diameter (cm): 1.14300
Assembly pitch (cm): 21.50364

Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.54281

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.95706

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model:**

Identifier of Equation(s) Utilized: 5.4-6
**Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model = 10.35273**

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
Area = 0.11369

Path B Unit Cell Model Dimensions:

	Zone #	Outer Radius (cm)	Zone Description
Inner	1	0.28575	Water
	2	0.33910	BPR inner cladding
	3	0.35305	Gap
	4	0.40104	Burnable poison
	5	0.41785	Gap
	6	0.48387	BPR outer cladding
	7	0.57150	Water
	8	0.61214	Guide tube
	9	0.71079	Water
	10	2.39492	Homogenized region
Outer	11	2.40457	Water in the assembly-to-assembly gap

Notes:
 The Region 4 outer radius is calculated using Equation 5.4-11.
 The Zone 10 outer radius is calculated using Equation 5.4-7.
 The Zone 11 outer radius is calculated using Equation 5.4-8.

Table 5.4-20. SAS2H Path B Model Dimension Calculations for Sequoyah Unit 2: STD Assembly Type, Lower Guide Tube Section, WABA BPR Insertion (24 BPRs)

Input Parameters

- Number of unit cells in assembly: 289
- Number of fuel rods in assembly: 264
- Number of guide tubes in assembly: 24
- Number of BPRs in assembly: 24
- Rod pitch in assembly (cm): 1.25984
- Fuel pellet diameter (cm): 0.81915
- Fuel cladding outer diameter (cm): 0.94996
- Lower Region guide tube outer diameter (cm): 1.08966
- Lower Region guide tube inner diameter (cm): 1.00838
- BPR outer cladding outer diameter (cm): 0.96774
- BPR outer cladding inner diameter (cm): 0.83570
- BPR inner cladding outer diameter (cm): 0.67820
- BPR inner cladding inner diameter (cm): 0.57150
- BPR absorber material outer diameter (cm): 0.80770
- BPR absorber material inner diameter (cm): 0.70610
- Instrument tube outer diameter (cm): 1.22428
- Instrument tube inner diameter (cm): 1.14300
- Assembly pitch (cm): 21.50364

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Fuel-to-Moderator Volume Ratio Calculation:

Identifier of Equation(s) Utilized: 5.4-1
Fuel-to-Moderator Volume Ratio = 0.54194

Moderator Unit Volume in Central Unit Cell of Path B Model:

Identifier of Equation(s) Utilized: 5.4-2
Moderator Unit Volume in Central Unit Cell of Path B Model = 0.97424

Fuel Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-3
Fuel Unit Volume in Fuel Rod Unit Cell = 0.52701

Moderator Unit Volume in Fuel Rod Unit Cell (Path A Model):

Identifier of Equation(s) Utilized: 5.4-4
Moderator Unit Volume in Fuel Rod Unit Cell = 0.87843

Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model:

Identifier of Equation(s) Utilized: 5.4-6
Number of Fuel Rod Unit Cells that must be Represented
in the Homogenized Zone of the Path B Model = 10.36349

Required Area of BPR Absorber Material in Path B Model (cm²):

Identifier of Equation Utilized: 5.4-10
Area = 0.11381

Path B Unit Cell Model Dimensions:

	Zone #	Outer Radius (cm)	Zone Description
Inner	1	0.28575	Water
	2	0.33910	BPR inner cladding
	3	0.35305	Gap
	4	0.40109	Burnable poison
	5	0.41785	Gap
	6	0.48387	BPR outer cladding
	7	0.50419	Water
	8	0.54483	Guide tube
	9	0.71079	Water
	10	2.39605	Homogenized region
Outer	11	2.40571	Water in the assembly-to-assembly gap

Notes: The Region 4 outer radius is calculated using Equation 5.4-11.
The Zone 10 outer radius is calculated using Equation 5.4-7.
The Zone 11 outer radius is calculated using Equation 5.4-8.

**Table 5.4-21. Equations Used in the Path B Model
Development for the Sequoyah Unit 2 Depletion Calculations**

(The equations listed below were derived. All distance dimensions are in centimeters. All area dimensions are in square centimeters. All other parameters are dimensionless.)

Equation 5.4-1. Fuel-to-Moderator Unit Volume (Area) Ratio in Fuel Assembly Section

$$\frac{F}{M} \text{ Ratio} = \frac{(\# FR) \left(\frac{\pi}{4} \right) (FP \text{ Diameter})^2}{\left(\# FR \right) \left[P^2 - (FR \text{ Clad OD})^2 \left(\frac{\pi}{4} \right) \right] + \left(\# \text{ Empty GTs} \right) \left[P^2 - (GT \text{ OD})^2 \left(\frac{\pi}{4} \right) + (GT \text{ ID})^2 \left(\frac{\pi}{4} \right) \right] + \left(\# \text{ Rodded GTs} \right) \left[\left(P^2 - (GT \text{ OD})^2 \left(\frac{\pi}{4} \right) + (GT \text{ ID})^2 \left(\frac{\pi}{4} \right) - (Inserted Rod Outer Clad OD)^2 \left(\frac{\pi}{4} \right) + (Inserted Rod Inner Clad ID)^2 \left(\frac{\pi}{4} \right) \right] + \left[P^2 - (IT \text{ OD})^2 \left(\frac{\pi}{4} \right) + (IT \text{ ID})^2 \left(\frac{\pi}{4} \right) \right]}$$

where: F=Fuel, M=Moderator, #=Number, FR=Fuel Rod, FP=Fuel Pellet, P=Cell Pitch, OD=Outer Diameter, GT=Guide Tube, IT=Instrument Tube, ID=Inner Diameter. Equation 5.4-1 assumes that the instrument tube is filled with water and that there is no instrument inserted. A rodded GT is any GT that contains a rod from either an RCCA or BPRA. The inserted rod refers to either an RCCA or BPRA rod inserted into the GTs of the assembly.

Equation 5.4-2. Moderator Area in Central Region of Path B Model

$$CRMA = P^2 - \left(\frac{\pi}{4} \right) \left[(GT \text{ OD})^2 - (GT \text{ ID})^2 + (Inserted Rod Outer Clad OD)^2 - (Inserted Rod Inner Clad ID)^2 \right]$$

where: CRMA=Central Region Moderator Area

Equation 5.4-3. Fuel Pellet Cross-Sectional Area in Path A Model

$$FA = (Fuel \text{ Pellet OD})^2 \left(\frac{\pi}{4} \right) \text{ where: FA=Fuel Area}$$

Equation 5.4-4. Moderator Cross-Sectional Area in Path A Model

$$MA = P^2 - (FR \text{ Clad } OD)^2 \left(\frac{\pi}{4} \right) \text{ where: } MA = \text{Moderator Area}$$

Equation 5.4-5. Relationship Between Fuel-to-Moderator Unit Volume Ratio in the Explicit Assembly Section and the Path B Model

$$\frac{F}{M} \text{ Ratio} = \frac{x(FA)}{CRMA + x(MA)}$$

where: F/M Ratio is from Equation 5.4-1, FA is from Equation 5.4-3, CRMA is from Equation 5.4-2, MA is from Equation 5.4-4, and x refers to the number of assembly fuel pin lattice cells that must be represented in the Path B Model homogenized region to preserve the fuel-to-moderator unit volume ratio.

Equation 5.4-6. Number of Assembly Fuel Pin Lattice Cells Required in the Homogenized Region of the Path B Model

$$x = \frac{\left(\frac{F}{M} \text{ Ratio} \right) (CRMA)}{FA - \left(\frac{F}{M} \text{ Ratio} \right) (MA)}$$

Equation 5.4-7. Path B Model Homogenized Region Outer Radius

$$\text{Homogenized Region Outer Radius} = \sqrt{\frac{x(P)^2}{\pi} + (\text{Homogenized Region Inner Radius})^2}$$

where: x is from Equation 5.4-6 and the Homogenized Region Inner Radius always refers to the outer radius of the Path B model central region which is always the explicit perimeter of an assembly unit cell that has been converted to a radial perimeter by conserving area.

Equation 5.4-8. Inter-Assembly Spacing Moderator Region Outer Radius

$$IASMR \text{ Outer Radius} = \left\{ \left(\frac{(x+1)}{\# \text{ Assembly Lattice Unit Cells}} \right) \left[(\text{Assembly Pitch})^2 - (P)^2 (\# \text{ Assembly Lattice Unit Cells}) \right] \left(\frac{1}{\pi} \right) + \right\}^{1/2}$$

where: IASMR=Inter-Assembly Spacing Moderator Region

When developing the Path B model for an assembly section that has insertion rods in some or all of the guide tubes, the development should begin with an explicit representation of the insertion rod inserted in the guide tube in the central region of the Path B Model. The remaining dimensions of the Path B Model should then be determined by preserving the fuel-to-moderator unit volume ratio in the explicit assembly section. The neutron absorber unit volume or area in the Path B Model must then be adjusted to preserve the fuel-to-absorber unit volume ratio in the explicit assembly section. This adjustment is made by first determining the neutron absorber area that must exist in the Path B model to preserve the fuel-to-absorber ratio. The existing area of the neutron absorber material in the Path B Model is then adjusted by changing the outer radius dimension of the neutron absorber material. The inner radius dimension of the neutron absorber material (if applicable) is always fixed at its explicit value.

Equation 5.4-9. Fuel-to-Neutron Absorber Unit Volume Ratio (Area) in Fuel Assembly Section

$$\frac{F}{Abs} \text{ Ratio} = \frac{(\# FRs)(Fuel Pellet OD)^2 \left(\frac{\pi}{4}\right)}{(\# Insertion Rods) \left(\frac{\pi}{4}\right) [(Abs Pellet OD)^2 - (Abs Pellet ID)^2]}$$

where: F/Abs Ratio = Fuel-to-Neutron Absorber Ratio in the explicit fuel assembly section, Abs = Neutron Absorber Material, Insertion Rods = refers to the rods of either an RCCA or BPRA that are inserted into the guide tubes in the assembly section.

Equation 5.4-10. Relationship Between Fuel-to-Neutron Absorber Unit Volume Ratio in the Explicit Assembly Section and the Path B Model

$$RAA = \frac{x(Fuel Pellet OD)^2 \left(\frac{\pi}{4}\right)}{\frac{F}{Abs} \text{ Ratio}}$$

where: RAA = Required Absorber Area for Path B Model and F/Abs Ratio is from Equation 5.4-9

Equation 5.4-11. Adjusted Neutron Absorber Area Outer Diameter for Path B Model

$$\text{Adjusted Neutron Absorber Region OD} = \sqrt{\left(\frac{RAA}{(\pi/4)} + (Abs Pellet ID)^2\right)}$$

where: RAA is from Equation 5.4-10

5.5. Cycle Irradiation History Layouts for the Sequoyah Unit 2 Depletion Calculations

The RCCA insertion history for an assembly was modeled such that the appropriate axial nodes of the fuel assembly were depleted using the appropriate neutron flux and spectrum over the correct exposure duration. The isotopic inventory may be quite different between fuel assemblies with and without an RCCA insertion history. These isotopic inventory differences must be accounted for in the CRC depletion calculations to allow for correct prediction of core k_{eff} values in subsequent CRC reactivity calculations.

In SAS2H, the duration of a depletion calculation may be separated into a number of time steps of variable length. Typically, the length of a depletion calculation was the continuous irradiation time required to go from one CRC statepoint or datapoint to another. To follow the RCCA insertion histories, detailed intra-cycle variable irradiation time steps were required. This was due to the fact that the rods of the RCCA were only present in a given axial node of an assembly for a given period of exposure during a statepoint depletion calculation. A user-specified number of cross section library updates were performed during each time step of an irradiation interval. The CRC depletion calculations always used one cross section library update per time step. The boron letdown curve of the reactor cycle may also be followed by specifying, at each irradiation step, a fraction of the soluble boron concentration defined in the base moderator material specification. This boron concentration was applied uniformly over the irradiation time step. The boron concentration fraction at the mid-point of each irradiation time step was specified in the SAS2H depletion calculations of this analysis to appropriately follow boron letdown curves. Considering the cross section update frequency, the boron letdown data, and the absorber rod assembly insertion histories, the following requirements were applied to determining an appropriate reactor cycle irradiation layout for a fuel assembly:

- The duration of each time step was specified such that a maximum of 80 days of irradiation was not exceeded between cross section updates. The SAS2H calculations in this calculation utilized one cross section update per irradiation step. Therefore, the maximum duration of any time step in any reactor cycle irradiation layout of this calculation did not exceed 80 days. The 80 day limit was an arbitrary limit based on engineering judgement. The 80 day irradiation time step limit should assure that the changes in isotopic concentrations of the system (primarily fuel) did not alter the neutron spectrum radically enough to cause a time step of the depletion calculation to be performed without the availability of cross sections which have been properly weighted with an appropriate neutron spectrum and spatial flux.
- Any radical perturbations in the boron letdown curve were followed by defining irradiation time step duration such that the average boron concentration over each time step is representative of the actual boron letdown. Usually, the 80 day time step limit imposed for cross section update frequency is adequate to properly follow a reactor cycle's boron letdown curve.
- The duration of each time step was specified such that the insertion of an RCCA in a given assembly axial node could be modeled for the correct exposure time in terms of EFPD. In SAS2H, there is an option to vary the Path B model between irradiation steps as long as the number of radial zones in

the Path B models of a given SAS2H calculation remain the same. Therefore, an assembly axial node represented in a given SAS2H statepoint depletion calculation that has an RCCA insertion history for a specified period of exposure, that is less than the total exposure covered by the statepoint depletion calculation, was modeled by changing the Path B model from one representing the insertion of the RCCA to one representing the removal of the RCCA at the appropriate time step corresponding to the RCCA removal time.

The irradiation time step layout for a given statepoint depletion calculation was developed so that breakpoints existed between irradiation time steps that allowed for the appropriate removal or insertion of the RCCA to obtain the correct neutron spectrum for each axial node of the assembly. The complexity of the irradiation time step layout for a given statepoint calculation was proportional to the number of axial nodes being modeled and the frequency of RCCA movement during the assembly depletion. The time steps developed to model RCCA insertion histories were also designed to encompass the cross section update and boron letdown requirements. A software routine entitled "RLAYOUT" was written to automate the development of appropriate irradiation time step layouts for the statepoint depletion calculations of an assembly having an RCCA insertion history. The RLAYOUT software routine is described in Attachment III of Reference 7.3.

The RLAYOUT software routine was only utilized to determine the irradiation time step layouts for the CRC depletion calculations that contained an RCCA insertion history. A single assembly may have had a combination of CRC calculations that either required or did not require the RLAYOUT developed irradiation time step layouts. For the CRC depletion calculations that did not require the consideration of an RCCA insertion history, the irradiation time step layouts were developed by considering the cross section update frequency and the boron letdown data. Tables 5.5-1 through 5.5-3 contain the CRC depletion calculation time step layouts for each Sequoyah Unit 2 reactor cycle that was relevant to the CRC depletion calculations documented in this calculation file which did not have an RCCA insertion history. The mid-step boron concentrations presented in Tables 5.5-1 through 5.5-3 were obtained from the linear equations presented in Section 5.2.7.

The RLAYOUT developed irradiation time step layouts for the assemblies which had an RCCA insertion history are presented in Tables 5.5-4 through 5.5-7. The boron letdown data utilized by RLAYOUT in developing these irradiation layouts were obtained from the boron letdown linear regression fits presented in Table 5.2.7-1. The RCCA insertion times utilized by RLAYOUT in developing these irradiation layouts were obtained from Tables 5.2.9-1 through 5.2.9-4.

Table 5.5-1. Irradiation Layout for Cycle 1 of Sequoyah Unit 2

Depletion: BOC ¹ to 187.06 EFPD		Time Step Length: 62.353 days	Number of Time Steps: 3
Time Step	Mid-Step EFPD	Mid-Step ppmB	
1	31.177	926.263	
2	93.530	772.251	
3	155.883	618.239	
Depletion: 187.06 EFPD to EOC		Time Step Length: 67.413 days	Number of Time Steps: 3
Time Step	Mid-Step EFPD	Mid-Step ppmB	
1	220.766	457.978	
2	288.179	291.468	
3	355.592	124.958	

¹ Beginning of Cycle

Table 5.5-2. Irradiation Layout for Cycle 2 of Sequoyah Unit 2

Depletion: BOC to 145.3 EFPD		Time Step Length: 72.65 days	Number of Time Steps: 2
Time Step	Mid-Step EFPD	Mid-Step ppmB	
1	36.525	872.526	
2	108.975	643.679	
Depletion: 145.3 EFPD to EOC		Time Step Length: 75.85 days	Number of Time Steps: 2
Time Step	Mid-Step EFPD	Mid-Step ppmB	
1	183.225	409.791	
2	259.075	170.864	

Table 5.5-3. Irradiation Layout for Cycle 3 of Sequoyah Unit 2

Depletion: BOC to 210.9 EFPD		Time Step Length: 70.3 days	Number of Time Steps: 3
Time Step	Mid-Step EFPD	Mid-Step ppmB	
1	35.15	1070.864	
2	105.45	852.231	
3	175.75	633.598	
Depletion: 210.9 EFPD to EOC		Time Step Length: 166.4 days ²	Number of Time Steps: 1
Time Step	Mid-Step EFPD	Mid-Step ppmB	
1	294.1	265.529	

² Due to the last statepoint being at 210.9 EFPD in this calculation, the depleted fuel characteristics beyond this point are not necessary, so the 166.4 day step length is only for CRAFT to complete its run.

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Table 5.5-4. RLAYOUT Developed Irradiation Layout for Assembly A06 of Sequoyah Unit 2

IRRADIATION LAYOUT FOR ASSEMBLY: A06

Cycle-03, .0 EFPD to Cycle-03, 210.9 EFPD Statepoint Calculation

Irradiation Step Number	Step Duration (EFPD)	Exposure at End of Step (EFPD)	Mid-Step Boron Concentration (ppm)
1	3.60	3.60	1174.6
2	8.20	11.80	1156.2
3	16.30	28.10	1118.1
4	63.00	91.10	994.8
5	63.00	154.10	798.9
6	56.80	210.90	612.6

NODAL ROD ASSEMBLY INSERTION LAYOUT FOR FUEL ASSEMBLY: A06

COLUMN A: Cycle-03, .0 EFPD to Cycle-03, 210.9 EFPD Statepoint Calculation

X = Rod assembly inserted in corresponding node during the irradiation step

NODE #	A					
	1	2	3	4	5	6
1	X	X	X	X	X	X
2	X	X	X	X		
3	X	X				
4	X					
5						
6						
7						
8						
9						
10						
11						
12						
13						
14						
15						
16						

Table 5.5-5. RLAYOUT Developed Irradiation Layout for Assembly A25 of Sequoyah Unit 2

IRRADIATION LAYOUT FOR ASSEMBLY: A25
 Cycle-03, .0 EFPD to Cycle-03, 210.9 EFPD Statepoint Calculation

Irradiation Step Number	Step Duration (EFPD)	Exposure at End of Step (EFPD)	Mid-Step Boron Concentration (ppm)
1	3.70	3.70	1174.4
2	8.30	12.00	1155.8
3	16.00	28.00	1118.0
4	62.90	90.90	995.3
5	62.90	153.80	799.7
6	57.10	210.90	613.1

NODAL ROD ASSEMBLY INSERTION LAYOUT FOR FUEL ASSEMBLY: A25

COLUMN A: Cycle-03, .0 EFPD to Cycle-03, 210.9 EFPD Statepoint Calculation

X = Rod assembly inserted in corresponding node during the irradiation step

NODE #	A					
	1	2	3	4	5	6
1	X	X	X	X	X	X
2	X	X	X			
3	X	X				
4	X					
5						
6						
7						
8						
9						
10						
11						
12						
13						
14						
15						
16						

Table 5.5-6. RLAYOUT Developed Irradiation Layout for Assembly A26 of Sequoyah Unit 2

IRRADIATION LAYOUT FOR ASSEMBLY: A26
 Cycle-03, .0 EFPD to Cycle-03, 210.9 EFPD Statepoint Calculation

Irradiation Step Number	Step Duration (EFPD)	Exposure at End of Step (EFPD)	Mid-Step Boron Concentration (ppm)
1	3.50	3.50	1174.7
2	8.40	11.90	1156.2
3	16.20	28.10	1118.0
4	63.20	91.30	994.5
5	63.20	154.50	798.0
6	56.40	210.90	612.0

NODAL ROD ASSEMBLY INSERTION LAYOUT FOR FUEL ASSEMBLY: A26

COLUMN A: Cycle-03, .0 EFPD to Cycle-03, 210.9 EFPD Statepoint Calculation

X = Rod assembly inserted in corresponding node during the irradiation step

NODE #	A					
	1	2	3	4	5	6
1	X	X	X	X	X	X
2	X	X	X			
3	X	X				
4	X					
5						
6						
7						
8						
9						
10						
11						
12						
13						
14						
15						
16						

5.6. The Commercial Reactor Assembly Follow Taskmaster (CRAFT) Software Routine and Usage

The CRAFT software routine directed the performance of the assembly depletion and decay calculations relevant to CRC evaluations. The CRAFT software routine generated input decks for the SAS2H control module of the SCALE modular code system based on user-defined input which described the fuel assembly's specifications and irradiation history. Appropriate isotopic concentrations relevant to both the CRC evaluations containing the fuel assembly and subsequent depletion and decay calculations of the fuel assembly were extracted and stored by CRAFT as it generated and executed the SAS2H cases required to simulate the complete fuel assembly irradiation history.

The CRAFT software routine was developed with a high degree of flexibility to provide for the depletion and decay of fuel assemblies that have widely varying features under flexible core operating conditions. The following listing describes some of the capabilities and usage of CRAFT.

- The CRAFT software routine generates and executes appropriate SAS2H cases required to perform a prescribed depletion and decay sequence for a fuel assembly. The depletion and decay sequence is orchestrated from the BOC statepoint calculation of the initial prescribed insertion cycle through the final statepoint calculation of the last prescribed insertion cycle. The CRAFT software routine extracts and saves fuel and burnable poison isotopes at each statepoint, including BOC statepoints, during the fuel assembly's depletion and decay sequence. A certain number of the generated isotopes in the depleted fuel composition obtained from a SAS2H calculation are not used in the initial charge composition to the next SAS2H calculation due to a lack of cross section data in the specified SAS2H master cross section library. The CRAFT software routine provides a listing of the fuel isotopes from the output of a SAS2H calculation which are not used in the initial charge to the next SAS2H calculation. The isotopes left out of the initial charge are fission products whose reactivity worth is small relative to the isotopes retained in the initial charge composition. The listing of excluded initial charge isotopes allows for a determination of the impact upon the reactivity worth of the initial fuel composition in the subsequent depletion calculation.
- Any assembly design may be analyzed within the bounds of the SAS2H control module through the use of the CRAFT software routine.
- A spacer grid modeling technique is available with the CRAFT software routine. The modeling technique homogenizes the spacer grid material throughout the moderator of the fuel assembly by utilizing a user-defined spacer material and spacer material volume fraction in the moderator. The available spacer grid materials include the following -- ZIRC-4, INCONEL, SS316, SS316S, SS304, SS304S. Any volume fraction of spacer material in the moderator may be specified (including zero).
- The fuel cladding, burnable poison rod cladding, or control rod cladding in the CRAFT calculation may be designated as any of the following materials -- ZIRC-4, INCONEL, SS316, SS316S, SS304, SS304S.

- The insertion of a BPRA during the irradiation of the fuel assembly may be modeled in the CRAFT calculation. Up to 10 unique BPRA designs may be specified for use during the depletion of a fuel assembly. Any type of BPRA design may be specified. The default burnable poison (BP) material for use in CRAFT calculation is $Al_2O_3-B_4C$. However, any arbitrary BP material may be specified for use in a BPRA design. A maximum of 10 unique BP materials may be specified. A maximum of 20 unique elements or isotopes may be specified in any given BP material. A BPRA may be inserted in any reactor cycle specified in the CRAFT calculation. Only one BPRA design may be specified per cycle. The position of the BPRA in the fuel assembly is specified by identifying the top and bottom axial nodes of the BP material. The BPRA remains fixed during a given reactor cycle. The depletion of the BP material is tracked during the CRAFT calculation. The appropriate depleted BP material is utilized in the statepoint calculations for a given reactor cycle. Depleted BP material isotopic concentrations are also retained for use in subsequent mid-cycle CRC statepoint reactivity calculations.
- The insertion of an RCCA during the irradiation of the fuel assembly may be modeled in the CRAFT calculation. Up to 10 unique RCCA designs may be specified for use during the depletion of a fuel assembly. Any type of RCCA design may be specified. Any arbitrary control rod (CR) absorber material may be specified for use in an RCCA design. A maximum of 10 unique CR absorber materials may be specified. A maximum of 10 unique elements or isotopes may be specified in any given CR absorber material. An RCCA may be inserted in any reactor cycle specified in the CRAFT calculation. Multiple RCCA designs may be specified per cycle. The position of the RCCA in the fuel assembly is specified by identifying the top and bottom axial nodes of sections of the fuel assembly which contain the CR absorber material. The RCCA position may be changed between each irradiation step of a SAS2H calculation generated by CRAFT. The RCCA design may also be changed between any two CRC statepoint depletion calculations in a given reactor cycle.
- A fuel assembly may be inserted in a maximum of 10 reactor cycles during a CRAFT calculation.
- A maximum of 20 statepoints or datapoints (BOC is always considered a statepoint) may be specified in any given reactor cycle in a CRAFT calculation.
- A maximum of 23 irradiation steps of variable duration may be specified in any given SAS2H depletion calculation that is generated by CRAFT.
- A maximum of 50 axial assembly nodes may be specified for use in a CRAFT calculation. Each axial node may have a unique height.
- The CRAFT software routine utilizes a user-defined input format for fuel temperature, moderator specific volume, and burnup data. The input data must be specified for each axial node in a user-defined nodal format of up to 50 nodes of arbitrary height. The total assembly active fuel height for the input data descriptions may be different than that specified for use in the CRAFT generated SAS2H depletion calculations. Depending on the users needs, the fuel temperature, moderator specific volume, and burnup input data may be specified in a different nodal format each time a set of this input data is provided. Nominal fuel temperature input data representing full-power reactor

operation must be provided in units of degrees Fahrenheit for each node in each CRC statepoint depletion calculation that will be generated by CRAFT. Nominal moderator specific volume input data representing full-power reactor operation must be provided in units of cubic feet per pound for each node in each statepoint calculation that will be generated by CRAFT. The nodal average burnup input data must be provided in units of GWd/MTU for each node at each statepoint or datapoint including all BOC statepoints. All burnup input data that is specified must be cumulative from the initial insertion of the fuel assembly in the reactor.

- A continuation CRAFT calculation for an assembly may be initiated from any statepoint in any reactor cycle if all of the nodal consolidated output files ("*.cut" files) from the statepoint calculation immediately preceding the continuation calculation exist in the CRAFT execution directory.

Additional information on the CRAFT software routine is provided in the CRAFT user information in Attachment I of Reference 7.6. Instructions on how to develop CRAFT input decks and execute CRAFT calculations are also provided in Attachment I of Reference 7.6. This attachment also discusses specific modeling procedures and details relevant to the SAS2H fuel assembly depletion calculations which were generated by CRAFT.

5.7. Input and Output Filename Descriptions for CRAFT and SAS2H

The CRAFT code generated five types of files identified as either "*.input", "*.output", "*.cut", "*.msgs", or "*.notes", where the "*" is the base file set identifier for the statepoint depletion calculation of interest. The "*.cut" and "*.notes" files were the only files that had to be retained for CRC reactivity evaluations and documentation purposes. All files were generated in the working directory in which the CRAFT calculation was performed.

All CRAFT generated filenames utilized the following format -- "{Base File Set Identifier}.{suffix}", where the suffix corresponded to one of the five file types previously mentioned, and the base file set identifier was a 25 character name containing essential information necessary to uniquely identify each CRAFT generated SAS2H depletion calculation.

The base file set identifier for each statepoint depletion calculation contained the following information:

1. reactor identifier (three character)
2. one-eighth core symmetry assembly number in current reactor cycle (two digit)
3. axial node number (node 1 is always the top node) (two digit)
4. reactor cycle number in which the SAS2H calculation starts (two character)
5. EFPD statepoint at which the SAS2H calculation starts (three digit)
6. reactor cycle number in which the SAS2H calculation ends (two character)
7. EFPD statepoint at which the SAS2H calculation ends (three digit).

The format of the base file set identifier was as follows where the numbers identified as #{number} correspond to one of the seven items previously listed -- #1 A #2 N #3 DC #4 T #5 AC #6 T #7. The

letters contained in the base file set identifier were presented explicitly as shown in the previous format. The base file set identifier did not contain any spaces.

The "*.input" files each contained a CRAFT generated SAS2H input deck. The "*.output" files each contained a complete SAS2H depletion calculation output file. The "*.cut" files each contained the corresponding SAS2H input deck followed by an output extraction from the final ORIGEN-S pass of the SAS2H depletion calculation, which contained data relevant to subsequent CRC reactivity calculations. The "*.msgs" files each contained the standard run-time messages associated with the SAS2H calculations. The "*.notes" files each contained a listing of the isotopes and associated concentrations which were left behind in generating the initial charge fuel composition for the next continuation SAS2H calculation. The "*.notes" files were only created for CRAFT generated SAS2H calculations which were continuation depletion calculations. The "*.cut" and "*.notes" files contained all of the information required to perform CRC reactivity evaluations or repeat calculations as necessary for quality assurance purposes. The remainder of the CRAFT generated files were discarded once the "*.cut" and "*.notes" files were generated and retained.

6. Results

Depletion calculations for 33 fuel assemblies from Sequoyah Unit 2 were documented in this analysis. The depleted fuel and depleted burnable poison isotopics for these fuel assemblies had to be calculated at two statepoints in cycle 3 for use in subsequent CRC reactivity calculations. Table 5.2.6-2 identifies the CRC statepoint EFPD values for which isotopic compositions were required. Table 5.2.6-2 also identifies a number of datapoints at which the depletion calculations were interrupted to update input parameters. Even though the depleted isotopics available at each of the datapoints were not required for subsequent reactivity calculations, they were retained in this calculation file for completeness.

The CRAFT input decks for each assembly depletion were developed in accordance with the instructions presented in Sections 5 and 7 of Attachment I of Reference 7.6. The SAS2H modeling features incorporated in the depletion calculations are also described in Attachment I of Reference 7.6. The CRAFT input decks for the assembly depletions documented in this calculation file are provided in Attachment I (the attachment tape has been moved to Reference 7.7), as documented in Section 8.

Attachment II (the attachment tape has been moved to Reference 7.7) contains the CRAFT generated consolidated SAS2H output files for the depletion calculations documented in this analysis as identified in the attachment listing of Section 8. The consolidated output files contain the following information:

- time/date stamp for when the SAS2H depletion calculation was performed
- echo of the SAS2H input deck generated by CRAFT
- the output extraction of information pertinent to CRC evaluations from the final ORIGEN-S calculation of the SAS2H depletion calculation.

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Between CRC statepoints or datapoints in the depletion sequence for a fuel assembly axial region, a new SAS2H input deck had to be created using the fuel isotopic results from the previous calculation as the initial charge. Since the 44-group master cross section library utilized in the SAS2H depletion calculations of this analysis had a reduced isotopic inventory relative to the ORIGEN-S cross section library, a number of isotopes present in the ORIGEN-S output could not be transferred to the initial fuel charge of the subsequent SAS2H depletion calculation. The isotopic inventory in the ORIGEN-S output which could not be propagated to the continuation SAS2H depletion calculation did not significantly affect the integral reactivity or the energy dependent neutron spectrum, as documented in Section 4.9.1 of Attachment I of Reference 7.6. The non-propagated isotopic inventory was written to a file entitled "{depletion case identifier}.notes" to allow for subsequent analysis of the impact of excluding these isotopes in the initial charge to the continuation SAS2H depletion calculation. The "*.notes" files are contained in Attachment III (the attachment tape has been moved to Reference 7.7) as documented in Section 8.

Isotopic results for the set of 29 principal isotopes identified in Table 6-1 were tabulated for each axial node of each fuel assembly at each CRC statepoint other than beginning of life (BOC of first reactor cycle in which the assembly is inserted) statepoint. The program entitled "CRC_DATA_TABULIZER.exe" described in Attachment VI of Reference 7.6, was used to create the principal isotope result tables documented in this calculation file. Attachment IV (the attachment tape has been moved to Reference 7.7) contains the principal isotope tabulations for the assemblies documented in this calculation file.

Table 6-1. The Set of 29 Principal Isotopes

Mo-95	Tc-99	Ru-101	Rh-103	Ag-109
Nd-143	Nd-145	Sm-147	Sm-149	Sm-150
Sm-151	Sm-152	Eu-151	Eu-153	Gd-155
U-233	U-234	U-235	U-236	U-238
Np-237	Pu-238	Pu-239	Pu-240	Pu-241
Pu-242	Am-241	Am-242m	Am-243	---

7. References

- 7.1 *SCALE, Version 4.3: Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation.* User's Manual Volumes 0 through 3, Oak Ridge National Laboratory. Distributed by the Radiation Shielding Information Center, Oak Ridge National Laboratory, Document Number: CCC-545.
- 7.2 *Software Qualification Report for the SCALE Modular Code System Version 4.3.* SCALE Version 4.3 Computer Software Configuration Item (CSCI): 30011 V4.3, Document Identifier Number (DI#): 30011-2002 REV 00, Civilian Radioactive Waste Management System (CRWMS) Management and Operating Contractor (M&O).

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- 7.3 *CRC Depletion Calculations for the Rodded Assemblies in Batches 1, 2, 3, and IX of Crystal River Unit 3.* DI#: BBA000000-01717-0200-00040 REV 00, CRWMS M&O.
- 7.4 *MCNP, Version 4B2: Monte Carlo N-Particle Transport Code System. User's Manual, Los Alamos National Laboratory. Distributed by the Radiation Shielding Information Center, Oak Ridge National Laboratory, Document Number: LA-12625-M.*
- 7.5 *Summary Report of Commercial Reactor Criticality Data for Sequoyah Unit 2.* DI#: B00000000-01717-5705-00064 REV 01, CRWMS M&O.
- 7.6 *CRC Depletion Calculations for McGuire Unit 1.* DI#: B00000000-01717-0210-00003 REV 00, CRWMS M&O.
- 7.7 *Sequoyah Unit 2 CRC Depletion Calculations. (DI#: B00000000-01717-0210-00005 REV 00, CRWMS M&O) Attachments I through IV - 1 Data Cartridge. Batch Number: MOY-980416-03.*

8. Attachments

The attachments referenced throughout this calculation file are listed in Table 8-1 (the attachment tape has been moved to Reference 7.7). Attachment I contains the CRAFT input decks for the assembly depletion calculations. Attachment II contains the "*.cut" files for the assembly depletion calculations. Attachment III contains the "*.notes" files for the assembly depletion calculations. Attachment IV contains the principal isotope result tables for the assembly depletion calculations. Attachments I through IV were written in ASCII format to an attachment tape. This attachment tape was provided with REV 00A of this calculation file. After checking of the attachment tape in REV 00A, the tape was made a reference (Ref. 7.7). Detailed listings of the content of Attachments I through IV on the tape are provided in their corresponding hard-copy attachment locations in this calculation file. The listing of the content of Attachments I through IV contain the following information, as appropriate, for each of the files that were written to the tape:

- the directory and filename as taken from the HP workstation
- the corresponding filename on the attachment tape
- the date that the file was created on the HP workstation or personal computer
- the size of the file on the HP workstation or personal computer in bytes.

The tape containing Attachments I through IV was written using the HP Colorado Model T1000c External Parallel Port Backup System for personal computers.

Table 8-1. Attachment Listing

Attachment #	# of Pages	Creation Date	Description
I	1 (Hard-Copy Listing of Tape Content)	(Tape Written) 3/16/98	CRAFT Input Decks for the Sequoyah Unit 2 Depletion Calculations (attachment tape moved to Reference 7.7)
II	26 (Hard-Copy Listing of Tape Content)	(Tape Written) 3/16/98	"*.cut" Consolidated Output Files for the Sequoyah Unit 2 Depletion Calculations (attachment tape moved to Reference 7.7)
III	18 (Hard-Copy Listing of Tape Content)	(Tape Written) 3/16/98	"*.notes" Files for the Sequoyah Unit 2 Depletion Calculations (attachment tape moved to Reference 7.7)
IV	2 (Hard-Copy Listing of Tape Content)	(Tape Written) 3/16/98	Principal Isotope Tabulized Results for the Sequoyah Unit 2 Depletion Calculations. (attachment tape moved to Reference 7.7)

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This attachment contains the CRAFT input decks for the depletion calculations for Sequoyah Unit 2. The input decks are contained on an attachment tape of this calculation file (the attachment tape has been moved to Reference 7.7). The information contained in this hard-copy representation of Attachment I is a listing of the various CRAFT input deck files and their attributes. The file sizes listed in the following table are the file sizes as they appear on the Hewlett Packard (HP) Series 9000 workstation. The HP file sizes differ from the file sizes on the attachment tape due to the difference in the block sizes between the HP and the personal computer. The tape containing Attachment I was written using the Colorado Model T1000e External Parallel Port Backup System for personal computers.

Filename	File Type	File Size (Bytes)	Date File Copied to Tape
A06i.dat	ASCII	20,422	3/16/98
A08i.dat	ASCII	17,495	3/16/98
A15i.dat	ASCII	13,337	3/16/98
A21i.dat	ASCII	17,488	3/16/98
A21ai.dat	ASCII	17,493	3/16/98
A25i.dat	ASCII	17,487	3/16/98
A25ai.dat	ASCII	20,440	3/16/98
A26i.dat	ASCII	13,322	3/16/98
A26ai.dat	ASCII	16,517	3/16/98
A29i.dat	ASCII	13,334	3/16/98
A29ai.dat	ASCII	13,335	3/16/98
A30i.dat	ASCII	16,740	3/16/98
A31i.dat	ASCII	17,466	3/16/98
B14i.dat	ASCII	13,240	3/16/98
B15i.dat	ASCII	9,659	3/16/98
B19i.dat	ASCII	13,245	3/16/98
B21i.dat	ASCII	9,660	3/16/98
B25i.dat	ASCII	13,244	3/16/98
B26i.dat	ASCII	9,634	3/16/98
B29i.dat	ASCII	9,663	3/16/98
B30i.dat	ASCII	13,239	3/16/98
B31i.dat	ASCII	9,632	3/16/98
C02i.dat	ASCII	9,786	3/16/98
C04i.dat	ASCII	9,785	3/16/98
C06i.dat	ASCII	9,785	3/16/98
C08i.dat	ASCII	6,194	3/16/98
C14i.dat	ASCII	9,786	3/16/98
C15i.dat	ASCII	6,194	3/16/98
C17i.dat	ASCII	9,786	3/16/98
C19i.dat	ASCII	9,783	3/16/98

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Filename	File Type	File Size (Bytes)	Date File Copied to Tape
C21i.dat	ASCII	6,194	3/16/98
C25i.dat	ASCII	9,777	3/16/98
C30i.dat	ASCII	6,194	3/16/98

This attachment contains the consolidated SAS2H output files that were generated by CRAFT during the depletion calculations for Sequoyah Unit 2. These files are referred to as ".cut" files due to their ".cut" extension. The ".cut" files are contained on an attachment tape of this calculation file (the attachment tape has been moved to Reference 7.7). The information contained in this hard-copy representation of Attachment II is a listing of the various ".cut" files and their attributes. The file sizes listed in the following table are the file sizes as they appear on the Hewlett Packard (HP) Series 9000 workstation. The HP file sizes differ from the file sizes on the attachment tape due to the difference in the block sizes between the HP and the personal computer. The tape containing Attachment II was written using the Colorado Model T1000e External Parallel Port Backup System for personal computers.

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
A06/SQ2A05N01DC03T000AC03T210.cut	aI.I21	Feb 20 1997	144746	ASCII
A06/SQ2A05N02DC03T000AC03T210.cut	aI.I22	Feb 20 1997	146161	ASCII
A06/SQ2A05N03DC03T000AC03T210.cut	aI.I23	Feb 20 1997	146746	ASCII
A06/SQ2A05N04DC03T000AC03T210.cut	aI.I24	Feb 20 1997	146651	ASCII
A06/SQ2A05N05DC03T000AC03T210.cut	aI.I25	Feb 20 1997	142272	ASCII
A06/SQ2A05N06DC03T000AC03T210.cut	aI.I26	Feb 20 1997	142355	ASCII
A06/SQ2A05N07DC03T000AC03T210.cut	aI.I27	Feb 20 1997	142355	ASCII
A06/SQ2A05N08DC03T000AC03T210.cut	aI.I28	Feb 20 1997	142355	ASCII
A06/SQ2A05N09DC03T000AC03T210.cut	aI.I29	Feb 20 1997	142272	ASCII
A06/SQ2A05N10DC03T000AC03T210.cut	aII.F10	Feb 20 1997	142272	ASCII
A06/SQ2A05N11DC03T000AC03T210.cut	aII.F11	Feb 20 1997	142272	ASCII
A06/SQ2A05N12DC03T000AC03T210.cut	aII.F12	Feb 20 1997	142284	ASCII
A06/SQ2A05N13DC03T000AC03T210.cut	aII.F13	Feb 20 1997	142118	ASCII
A06/SQ2A05N14DC03T000AC03T210.cut	aII.F14	Feb 20 1997	142035	ASCII
A06/SQ2A05N15DC03T000AC03T210.cut	aII.F15	Feb 20 1997	141620	ASCII
A06/SQ2A05N16DC03T000AC03T210.cut	aII.F16	Feb 20 1997	140122	ASCII
A06/SQ2A06N01DC01T000AC01T187.cut	aII.F17	Feb 20 1997	288953	ASCII
A06/SQ2A06N01DC01T187AC02T000.cut	aII.F18	Feb 20 1997	143690	ASCII
A06/SQ2A06N02DC01T000AC01T187.cut	aII.F19	Feb 20 1997	295036	ASCII
A06/SQ2A06N02DC01T187AC02T000.cut	aII.F20	Feb 20 1997	146416	ASCII
A06/SQ2A06N03DC01T000AC01T187.cut	aII.F21	Feb 20 1997	297844	ASCII
A06/SQ2A06N03DC01T187AC02T000.cut	aII.F22	Feb 20 1997	147582	ASCII
A06/SQ2A06N04DC01T000AC01T187.cut	aII.F23	Feb 20 1997	300002	ASCII
A06/SQ2A06N04DC01T187AC02T000.cut	aII.F24	Feb 20 1997	147914	ASCII
A06/SQ2A06N05DC01T000AC01T187.cut	aII.F25	Feb 20 1997	300749	ASCII
A06/SQ2A06N05DC01T187AC02T000.cut	aII.F26	Feb 20 1997	148084	ASCII
A06/SQ2A06N06DC01T000AC01T187.cut	aII.F27	Feb 20 1997	301164	ASCII
A06/SQ2A06N06DC01T187AC02T000.cut	aII.F28	Feb 20 1997	148084	ASCII
A06/SQ2A06N07DC01T000AC01T187.cut	aII.F29	Feb 20 1997	301745	ASCII
A06/SQ2A06N07DC01T187AC02T000.cut	aII.F30	Feb 20 1997	148001	ASCII
A06/SQ2A06N08DC01T000AC01T187.cut	aII.F31	Feb 20 1997	301828	ASCII
A06/SQ2A06N08DC01T187AC02T000.cut	aII.F32	Feb 20 1997	147835	ASCII
A06/SQ2A06N09DC01T000AC01T187.cut	aII.F33	Feb 20 1997	301994	ASCII
A06/SQ2A06N09DC01T187AC02T000.cut	aII.F34	Feb 20 1997	147835	ASCII
A06/SQ2A06N10DC01T000AC01T187.cut	aII.F35	Feb 20 1997	301994	ASCII
A06/SQ2A06N10DC01T187AC02T000.cut	aII.F36	Feb 20 1997	147835	ASCII
A06/SQ2A06N11DC01T000AC01T187.cut	aII.F37	Feb 20 1997	301911	ASCII
A06/SQ2A06N11DC01T187AC02T000.cut	aII.F38	Feb 20 1997	147835	ASCII
A06/SQ2A06N12DC01T000AC01T187.cut	aII.F39	Feb 20 1997	301330	ASCII
A06/SQ2A06N12DC01T187AC02T000.cut	aII.F40	Feb 20 1997	148084	ASCII
A06/SQ2A06N13DC01T000AC01T187.cut	aII.F41	Feb 20 1997	300583	ASCII
A06/SQ2A06N13DC01T187AC02T000.cut	aII.F42	Feb 20 1997	148084	ASCII
A06/SQ2A06N14DC01T000AC01T187.cut	aII.F43	Feb 20 1997	299421	ASCII
A06/SQ2A06N14DC01T187AC02T000.cut	aII.F44	Feb 20 1997	147831	ASCII
A06/SQ2A06N15DC01T000AC01T187.cut	aII.F45	Feb 20 1997	296530	ASCII
A06/SQ2A06N15DC01T187AC02T000.cut	aII.F46	Feb 20 1997	147333	ASCII
A06/SQ2A06N16DC01T000AC01T187.cut	aII.F47	Feb 20 1997	285917	ASCII
A06/SQ2A06N16DC01T187AC02T000.cut	aII.F48	Feb 20 1997	141654	ASCII
A06/SQ2A08N01DC02T000AC02T145.cut	aII.F49	Feb 20 1997	290052	ASCII
A06/SQ2A08N01DC02T145AC03T000.cut	aII.F50	Feb 20 1997	139235	ASCII
A06/SQ2A08N02DC02T000AC02T145.cut	aII.F51	Feb 20 1997	295562	ASCII
A06/SQ2A08N02DC02T145AC03T000.cut	aII.F52	Feb 20 1997	140816	ASCII
A06/SQ2A08N03DC02T000AC02T145.cut	aII.F53	Feb 20 1997	297973	ASCII

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Document Identifier: B00000000-01717-0210-00005 REV 00

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A06/SQ2A08N03DC02T145AC03T000.cut	aII.f54	Feb 20 1997	142725	ASCII
A06/SQ2A08N04DC02T000AC02T145.cut	aII.f55	Feb 20 1997	298720	ASCII
A06/SQ2A08N04DC02T145AC03T000.cut	aII.f56	Feb 20 1997	142978	ASCII
A06/SQ2A08N05DC02T000AC02T145.cut	aII.f57	Feb 20 1997	298720	ASCII
A06/SQ2A08N05DC02T145AC03T000.cut	aII.f58	Feb 20 1997	143144	ASCII
A06/SQ2A08N06DC02T000AC02T145.cut	aII.f59	Feb 20 1997	298637	ASCII
A06/SQ2A08N06DC02T145AC03T000.cut	aII.f60	Feb 20 1997	143144	ASCII
A06/SQ2A08N07DC02T000AC02T145.cut	aII.f61	Feb 20 1997	298637	ASCII
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A06/SQ2A08N08DC02T000AC02T145.cut	aII.f63	Feb 20 1997	298637	ASCII
A06/SQ2A08N08DC02T145AC03T000.cut	aII.f64	Feb 20 1997	143144	ASCII
A06/SQ2A08N09DC02T000AC02T145.cut	aII.f65	Feb 20 1997	298637	ASCII
A06/SQ2A08N09DC02T145AC03T000.cut	aII.f66	Feb 20 1997	143227	ASCII
A06/SQ2A08N10DC02T000AC02T145.cut	aII.f67	Feb 20 1997	298886	ASCII
A06/SQ2A08N10DC02T145AC03T000.cut	aII.f68	Feb 20 1997	143310	ASCII
A06/SQ2A08N11DC02T000AC02T145.cut	aII.f69	Feb 20 1997	298886	ASCII
A06/SQ2A08N11DC02T145AC03T000.cut	aII.f70	Feb 20 1997	143393	ASCII
A06/SQ2A08N12DC02T000AC02T145.cut	aII.f71	Feb 20 1997	298886	ASCII
A06/SQ2A08N12DC02T145AC03T000.cut	aII.f72	Feb 20 1997	143393	ASCII
A06/SQ2A08N13DC02T000AC02T145.cut	aII.f73	Feb 20 1997	298637	ASCII
A06/SQ2A08N13DC02T145AC03T000.cut	aII.f74	Feb 20 1997	143393	ASCII
A06/SQ2A08N14DC02T000AC02T145.cut	aII.f75	Feb 20 1997	298471	ASCII
A06/SQ2A08N14DC02T145AC03T000.cut	aII.f76	Feb 20 1997	143223	ASCII
A06/SQ2A08N15DC02T000AC02T145.cut	aII.f77	Feb 20 1997	296060	ASCII
A06/SQ2A08N15DC02T145AC03T000.cut	aII.f78	Feb 20 1997	141978	ASCII
A06/SQ2A08N16DC02T000AC02T145.cut	aII.f79	Feb 20 1997	290720	ASCII
A06/SQ2A08N16DC02T145AC03T000.cut	aII.f80	Feb 20 1997	139484	ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
A08/SQ2A04N01DC02T000AC02T145.cut	aII.f81	Feb 20 1997	291404	ASCII
A08/SQ2A04N01DC02T145AC03T000.cut	aII.f82	Feb 20 1997	139733	ASCII
A08/SQ2A04N02DC02T000AC02T145.cut	aII.f83	Feb 20 1997	295876	ASCII
A08/SQ2A04N02DC02T145AC03T000.cut	aII.f84	Feb 20 1997	142127	ASCII
A08/SQ2A04N03DC02T000AC02T145.cut	aII.f85	Feb 20 1997	297540	ASCII
A08/SQ2A04N03DC02T145AC03T000.cut	aII.f86	Feb 20 1997	142874	ASCII
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Waste Package Operations

Engineering Calculation Attachment

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Engineering Calculation Attachment

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Engineering Calculation Attachment

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Engineering Calculation Attachment

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Waste Package Operations

Engineering Calculation Attachment

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Title: Sequoyah Unit 2 CRC Depletion Calculations

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Waste Package Operations

Engineering Calculation Attachment

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B29/SQ2A29N02DC02T000AC02T145.cut	aIIf1.347	Feb 20 1997	286423	ASCII
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B29/SQ2A29N06DC02T145AC03T000.cut	aIIf1.356	Feb 20 1997	140131	ASCII
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B29/SQ2A29N07DC02T145AC03T000.cut	aIIf1.358	Feb 20 1997	140131	ASCII
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B29/SQ2A29N08DC02T145AC03T000.cut	aIIf1.360	Feb 20 1997	140131	ASCII
B29/SQ2A29N09DC02T145AC03T000.cut	aIIf1.361	Feb 20 1997	288318	ASCII
B29/SQ2A29N09DC02T145AC03T000.cut	aIIf1.362	Feb 20 1997	140131	ASCII
B29/SQ2A29N10DC02T000AC02T145.cut	aIIf1.363	Feb 20 1997	288650	ASCII
B29/SQ2A29N10DC02T145AC03T000.cut	aIIf1.364	Feb 20 1997	140131	ASCII
B29/SQ2A29N11DC02T000AC02T145.cut	aIIf1.365	Feb 20 1997	288650	ASCII
B29/SQ2A29N11DC02T145AC03T000.cut	aIIf1.366	Feb 20 1997	140214	ASCII
B29/SQ2A29N12DC02T000AC02T145.cut	aIIf1.367	Feb 20 1997	288899	ASCII
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B29/SQ2A29N15DC02T145AC03T000.cut	aIIf1.374	Feb 20 1997	139463	ASCII
B29/SQ2A29N16DC02T000AC02T145.cut	aIIf1.375	Feb 20 1997	282581	ASCII
B29/SQ2A29N16DC02T145AC03T000.cut	aIIf1.376	Feb 20 1997	137571	ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
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B30/SQ2A03N03DC03T000AC03T210.cut	aIIf1.379	Feb 20 1997	131845	ASCII
B30/SQ2A03N04DC03T000AC03T210.cut	aIIf1.380	Feb 20 1997	132177	ASCII
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B30/SQ2A03N07DC03T000AC03T210.cut	aIIf1.383	Feb 20 1997	132177	ASCII
B30/SQ2A03N08DC03T000AC03T210.cut	aIIf1.384	Feb 20 1997	132260	ASCII
B30/SQ2A03N09DC03T000AC03T210.cut	aIIf1.385	Feb 20 1997	132177	ASCII
B30/SQ2A03N10DC03T000AC03T210.cut	aIIf1.386	Feb 20 1997	132177	ASCII
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B30/SQ2A03N13DC03T000AC03T210.cut	aIIf1.389	Feb 20 1997	132177	ASCII
B30/SQ2A03N14DC03T000AC03T210.cut	aIIf1.390	Feb 20 1997	132094	ASCII
B30/SQ2A03N15DC03T000AC03T210.cut	aIIf1.391	Feb 20 1997	131264	ASCII
B30/SQ2A03N16DC03T000AC03T210.cut	aIIf1.392	Feb 20 1997	130027	ASCII
B30/SQ2A30N01DC02T000AC02T145.cut	aIIf1.393	Feb 20 1997	286344	ASCII

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Engineering Calculation Attachment

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B30/SQ2A30N01DC02T145AC03T000.cut	aIIf1.394	Feb 20 1997	139354	ASCII
B30/SQ2A30N02DC02T000AC02T145.cut	aIIf1.395	Feb 20 1997	290421	ASCII
B30/SQ2A30N02DC02T145AC03T000.cut	aIIf1.396	Feb 20 1997	140831	ASCII
B30/SQ2A30N03DC02T000AC02T145.cut	aIIf1.397	Feb 20 1997	291913	ASCII
B30/SQ2A30N03DC02T145AC03T000.cut	aIIf1.398	Feb 20 1997	142080	ASCII
B30/SQ2A30N04DC02T000AC02T145.cut	aIIf1.399	Feb 20 1997	292413	ASCII
B30/SQ2A30N04DC02T145AC03T000.cut	aIIf1.400	Feb 20 1997	142080	ASCII
B30/SQ2A30N05DC02T000AC02T145.cut	aIIf1.401	Feb 20 1997	292579	ASCII
B30/SQ2A30N05DC02T145AC03T000.cut	aIIf1.402	Feb 20 1997	142246	ASCII
B30/SQ2A30N06DC02T000AC02T145.cut	aIIf1.403	Feb 20 1997	292662	ASCII
B30/SQ2A30N06DC02T145AC03T000.cut	aIIf1.404	Feb 20 1997	142329	ASCII
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B30/SQ2A30N08DC02T145AC03T000.cut	aIIf1.408	Feb 20 1997	142412	ASCII
B30/SQ2A30N09DC02T000AC02T145.cut	aIIf1.409	Feb 20 1997	292745	ASCII
B30/SQ2A30N09DC02T145AC03T000.cut	aIIf1.410	Feb 20 1997	142412	ASCII
B30/SQ2A30N10DC02T000AC02T145.cut	aIIf1.411	Feb 20 1997	292745	ASCII
B30/SQ2A30N10DC02T145AC03T000.cut	aIIf1.412	Feb 20 1997	142495	ASCII
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B30/SQ2A30N11DC02T145AC03T000.cut	aIIf1.414	Feb 20 1997	142495	ASCII
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B30/SQ2A30N13DC02T000AC02T145.cut	aIIf1.417	Feb 20 1997	292745	ASCII
B30/SQ2A30N13DC02T145AC03T000.cut	aIIf1.418	Feb 20 1997	142495	ASCII
B30/SQ2A30N14DC02T000AC02T145.cut	aIIf1.419	Feb 20 1997	292496	ASCII
B30/SQ2A30N14DC02T145AC03T000.cut	aIIf1.420	Feb 20 1997	142412	ASCII
B30/SQ2A30N15DC02T000AC02T145.cut	aIIf1.421	Feb 20 1997	291334	ASCII
B30/SQ2A30N15DC02T145AC03T000.cut	aIIf1.422	Feb 20 1997	141997	ASCII
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Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
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B31/SQ2A26N12DC03T000AC03T210.cut	aIIf1.436	Feb 20 1997	129948	ASCII
B31/SQ2A26N13DC03T000AC03T210.cut	aIIf1.437	Feb 20 1997	129948	ASCII
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B31/SQ2A31N02DC02T000AC02T145.cut	aIIf1.443	Feb 20 1997	282996	ASCII
B31/SQ2A31N02DC02T145AC03T000.cut	aIIf1.444	Feb 20 1997	137405	ASCII
B31/SQ2A31N03DC02T000AC02T145.cut	aIIf1.445	Feb 20 1997	285261	ASCII
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B31/SQ2A31N05DC02T000AC02T145.cut	aIIf1.449	Feb 20 1997	285842	ASCII
B31/SQ2A31N05DC02T145AC03T000.cut	aIIf1.450	Feb 20 1997	138318	ASCII
B31/SQ2A31N06DC02T000AC02T145.cut	aIIf1.451	Feb 20 1997	285842	ASCII
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B31/SQ2A31N07DC02T145AC03T000.cut	aIIf1.454	Feb 20 1997	138401	ASCII
B31/SQ2A31N08DC02T000AC02T145.cut	aIIf1.455	Feb 20 1997	286008	ASCII
B31/SQ2A31N08DC02T145AC03T000.cut	aIIf1.456	Feb 20 1997	138484	ASCII
B31/SQ2A31N09DC02T000AC02T145.cut	aIIf1.457	Feb 20 1997	286008	ASCII
B31/SQ2A31N09DC02T145AC03T000.cut	aIIf1.458	Feb 20 1997	138484	ASCII
B31/SQ2A31N10DC02T000AC02T145.cut	aIIf1.459	Feb 20 1997	286008	ASCII
B31/SQ2A31N10DC02T145AC03T000.cut	aIIf1.460	Feb 20 1997	138567	ASCII

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B31/SQ2A31N11DC02T000AC02T145.cut	aIIf1.461	Feb 20 1997	286091	ASCII
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B31/SQ2A31N12DC02T145AC03T000.cut	aIIf1.464	Feb 20 1997	138650	ASCII
B31/SQ2A31N13DC02T000AC02T145.cut	aIIf1.465	Feb 20 1997	286008	ASCII
B31/SQ2A31N13DC02T145AC03T000.cut	aIIf1.466	Feb 20 1997	138650	ASCII
B31/SQ2A31N14DC02T000AC02T145.cut	aIIf1.467	Feb 20 1997	285842	ASCII
B31/SQ2A31N14DC02T145AC03T000.cut	aIIf1.468	Feb 20 1997	138401	ASCII
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B31/SQ2A31N16DC02T000AC02T145.cut	aIIf1.471	Feb 20 1997	280257	ASCII
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Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
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C02/SQ2A02N04DC03T000AC03T210.cut	aIIf1.476	Feb 20 1997	129457	ASCII
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C02/SQ2A02N06DC03T000AC03T210.cut	aIIf1.478	Feb 20 1997	129457	ASCII
C02/SQ2A02N07DC03T000AC03T210.cut	aIIf1.479	Feb 20 1997	129457	ASCII
C02/SQ2A02N08DC03T000AC03T210.cut	aIIf1.480	Feb 20 1997	129374	ASCII
C02/SQ2A02N09DC03T000AC03T210.cut	aIIf1.481	Feb 20 1997	129374	ASCII
C02/SQ2A02N10DC03T000AC03T210.cut	aIIf1.482	Feb 20 1997	129374	ASCII
C02/SQ2A02N11DC03T000AC03T210.cut	aIIf1.483	Feb 20 1997	129374	ASCII
C02/SQ2A02N12DC03T000AC03T210.cut	aIIf1.484	Feb 20 1997	129291	ASCII
C02/SQ2A02N13DC03T000AC03T210.cut	aIIf1.485	Feb 20 1997	129042	ASCII
C02/SQ2A02N14DC03T000AC03T210.cut	aIIf1.486	Feb 20 1997	128876	ASCII
C02/SQ2A02N15DC03T000AC03T210.cut	aIIf1.487	Feb 20 1997	128544	ASCII
C02/SQ2A02N16DC03T000AC03T210.cut	aIIf1.488	Feb 20 1997	126038	ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
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C04/SQ2A04N03DC03T000AC03T210.cut	aIIf1.491	Feb 20 1997	129291	ASCII
C04/SQ2A04N04DC03T000AC03T210.cut	aIIf1.492	Feb 20 1997	129540	ASCII
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C04/SQ2A04N06DC03T000AC03T210.cut	aIIf1.494	Feb 20 1997	129540	ASCII
C04/SQ2A04N07DC03T000AC03T210.cut	aIIf1.495	Feb 20 1997	129540	ASCII
C04/SQ2A04N08DC03T000AC03T210.cut	aIIf1.496	Feb 20 1997	129540	ASCII
C04/SQ2A04N09DC03T000AC03T210.cut	aIIf1.497	Feb 20 1997	129540	ASCII
C04/SQ2A04N10DC03T000AC03T210.cut	aIIf1.498	Feb 20 1997	129540	ASCII
C04/SQ2A04N11DC03T000AC03T210.cut	aIIf1.499	Feb 20 1997	129540	ASCII
C04/SQ2A04N12DC03T000AC03T210.cut	aIIf1.500	Feb 20 1997	129540	ASCII
C04/SQ2A04N13DC03T000AC03T210.cut	aIIf1.501	Feb 20 1997	129291	ASCII
C04/SQ2A04N14DC03T000AC03T210.cut	aIIf1.502	Feb 20 1997	129125	ASCII
C04/SQ2A04N15DC03T000AC03T210.cut	aIIf1.503	Feb 20 1997	128793	ASCII
C04/SQ2A04N16DC03T000AC03T210.cut	aIIf1.504	Feb 20 1997	126287	ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
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C06/SQ2A06N02DC03T000AC03T210.cut	aIIf1.506	Feb 20 1997	128378	ASCII
C06/SQ2A06N03DC03T000AC03T210.cut	aIIf1.507	Feb 20 1997	128627	ASCII
C06/SQ2A06N04DC03T000AC03T210.cut	aIIf1.508	Feb 20 1997	128959	ASCII
C06/SQ2A06N05DC03T000AC03T210.cut	aIIf1.509	Feb 20 1997	129208	ASCII
C06/SQ2A06N06DC03T000AC03T210.cut	aIIf1.510	Feb 20 1997	129208	ASCII
C06/SQ2A06N07DC03T000AC03T210.cut	aIIf1.511	Feb 20 1997	129291	ASCII
C06/SQ2A06N08DC03T000AC03T210.cut	aIIf1.512	Feb 20 1997	129291	ASCII
C06/SQ2A06N09DC03T000AC03T210.cut	aIIf1.513	Feb 20 1997	129291	ASCII
C06/SQ2A06N10DC03T000AC03T210.cut	aIIf1.514	Feb 20 1997	129291	ASCII
C06/SQ2A06N11DC03T000AC03T210.cut	aIIf1.515	Feb 20 1997	129208	ASCII
C06/SQ2A06N12DC03T000AC03T210.cut	aIIf1.516	Feb 20 1997	129208	ASCII
C06/SQ2A06N13DC03T000AC03T210.cut	aIIf1.517	Feb 20 1997	129042	ASCII

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C06/SQ2A06N14DC03T000AC03T210.cut
 C06/SQ2A06N15DC03T000AC03T210.cut
 C06/SQ2A06N16DC03T000AC03T210.cut

aIIf1.518 Feb 20 1997
 aIIf1.519 Feb 20 1997
 aIIf1.520 Feb 20 1997

128793
 128544
 126038
 ASCII
 ASCII
 ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
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C08/SQ2A08N03DC03T000AC03T210.cut	aIIf1.523	Feb 20 1997	126524	ASCII
C08/SQ2A08N04DC03T000AC03T210.cut	aIIf1.524	Feb 20 1997	126607	ASCII
C08/SQ2A08N05DC03T000AC03T210.cut	aIIf1.525	Feb 20 1997	126690	ASCII
C08/SQ2A08N06DC03T000AC03T210.cut	aIIf1.526	Feb 20 1997	126773	ASCII
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C08/SQ2A08N08DC03T000AC03T210.cut	aIIf1.528	Feb 20 1997	126773	ASCII
C08/SQ2A08N09DC03T000AC03T210.cut	aIIf1.529	Feb 20 1997	126773	ASCII
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C08/SQ2A08N13DC03T000AC03T210.cut	aIIf1.533	Feb 20 1997	126773	ASCII
C08/SQ2A08N14DC03T000AC03T210.cut	aIIf1.534	Feb 20 1997	126690	ASCII
C08/SQ2A08N15DC03T000AC03T210.cut	aIIf1.535	Feb 20 1997	126524	ASCII
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Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
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C14/SQ2A14N03DC03T000AC03T210.cut	aIIf1.539	Feb 20 1997	128793	ASCII
C14/SQ2A14N04DC03T000AC03T210.cut	aIIf1.540	Feb 20 1997	129042	ASCII
C14/SQ2A14N05DC03T000AC03T210.cut	aIIf1.541	Feb 20 1997	129457	ASCII
C14/SQ2A14N06DC03T000AC03T210.cut	aIIf1.542	Feb 20 1997	129457	ASCII
C14/SQ2A14N07DC03T000AC03T210.cut	aIIf1.543	Feb 20 1997	129457	ASCII
C14/SQ2A14N08DC03T000AC03T210.cut	aIIf1.544	Feb 20 1997	129457	ASCII
C14/SQ2A14N09DC03T000AC03T210.cut	aIIf1.545	Feb 20 1997	129457	ASCII
C14/SQ2A14N10DC03T000AC03T210.cut	aIIf1.546	Feb 20 1997	129457	ASCII
C14/SQ2A14N11DC03T000AC03T210.cut	aIIf1.547	Feb 20 1997	129457	ASCII
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C14/SQ2A14N13DC03T000AC03T210.cut	aIIf1.549	Feb 20 1997	129374	ASCII
C14/SQ2A14N14DC03T000AC03T210.cut	aIIf1.550	Feb 20 1997	129042	ASCII
C14/SQ2A14N15DC03T000AC03T210.cut	aIIf1.551	Feb 20 1997	128344	ASCII
C14/SQ2A14N16DC03T000AC03T210.cut	aIIf1.552	Feb 20 1997	126121	ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
C15/SQ2A15N01DC03T000AC03T210.cut	aIIf1.553	Feb 20 1997	124022	ASCII
C15/SQ2A15N02DC03T000AC03T210.cut	aIIf1.554	Feb 20 1997	126287	ASCII
C15/SQ2A15N03DC03T000AC03T210.cut	aIIf1.555	Feb 20 1997	126524	ASCII
C15/SQ2A15N04DC03T000AC03T210.cut	aIIf1.556	Feb 20 1997	126690	ASCII
C15/SQ2A15N05DC03T000AC03T210.cut	aIIf1.557	Feb 20 1997	126773	ASCII
C15/SQ2A15N06DC03T000AC03T210.cut	aIIf1.558	Feb 20 1997	126773	ASCII
C15/SQ2A15N07DC03T000AC03T210.cut	aIIf1.559	Feb 20 1997	126773	ASCII
C15/SQ2A15N08DC03T000AC03T210.cut	aIIf1.560	Feb 20 1997	126773	ASCII
C15/SQ2A15N09DC03T000AC03T210.cut	aIIf1.561	Feb 20 1997	126773	ASCII
C15/SQ2A15N10DC03T000AC03T210.cut	aIIf1.562	Feb 20 1997	126773	ASCII
C15/SQ2A15N11DC03T000AC03T210.cut	aIIf1.563	Feb 20 1997	126773	ASCII
C15/SQ2A15N12DC03T000AC03T210.cut	aIIf1.564	Feb 20 1997	126773	ASCII
C15/SQ2A15N13DC03T000AC03T210.cut	aIIf1.565	Feb 20 1997	126773	ASCII
C15/SQ2A15N14DC03T000AC03T210.cut	aIIf1.566	Feb 20 1997	126690	ASCII
C15/SQ2A15N15DC03T000AC03T210.cut	aIIf1.567	Feb 20 1997	126441	ASCII
C15/SQ2A15N16DC03T000AC03T210.cut	aIIf1.568	Feb 20 1997	124520	ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
C17/SQ2A17N01DC03T000AC03T210.cut	aIIf1.569	Feb 20 1997	127975	ASCII

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C17/SQ2A17N02DC03T000AC03T210.cut	aIIf1.570	Feb 20 1997	128544	ASCII
C17/SQ2A17N03DC03T000AC03T210.cut	aIIf1.571	Feb 20 1997	129042	ASCII
C17/SQ2A17N04DC03T000AC03T210.cut	aIIf1.572	Feb 20 1997	129291	ASCII
C17/SQ2A17N05DC03T000AC03T210.cut	aIIf1.573	Feb 20 1997	129291	ASCII
C17/SQ2A17N06DC03T000AC03T210.cut	aIIf1.574	Feb 20 1997	129291	ASCII
C17/SQ2A17N07DC03T000AC03T210.cut	aIIf1.575	Feb 20 1997	129291	ASCII
C17/SQ2A17N08DC03T000AC03T210.cut	aIIf1.576	Feb 20 1997	129291	ASCII
C17/SQ2A17N09DC03T000AC03T210.cut	aIIf1.577	Feb 20 1997	129291	ASCII
C17/SQ2A17N10DC03T000AC03T210.cut	aIIf1.578	Feb 20 1997	129291	ASCII
C17/SQ2A17N11DC03T000AC03T210.cut	aIIf1.579	Feb 20 1997	129291	ASCII
C17/SQ2A17N12DC03T000AC03T210.cut	aIIf1.580	Feb 20 1997	129291	ASCII
C17/SQ2A17N13DC03T000AC03T210.cut	aIIf1.581	Feb 20 1997	129208	ASCII
C17/SQ2A17N14DC03T000AC03T210.cut	aIIf1.582	Feb 20 1997	128876	ASCII
C17/SQ2A17N15DC03T000AC03T210.cut	aIIf1.583	Feb 20 1997	128544	ASCII
C17/SQ2A17N16DC03T000AC03T210.cut	aIIf1.584	Feb 20 1997	126038	ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
C19/SQ2A19N01DC03T000AC03T210.cut	aIIf1.585	Feb 20 1997	127204	ASCII
C19/SQ2A19N02DC03T000AC03T210.cut	aIIf1.586	Feb 20 1997	128627	ASCII
C19/SQ2A19N03DC03T000AC03T210.cut	aIIf1.587	Feb 20 1997	128876	ASCII
C19/SQ2A19N04DC03T000AC03T210.cut	aIIf1.588	Feb 20 1997	129125	ASCII
C19/SQ2A19N05DC03T000AC03T210.cut	aIIf1.589	Feb 20 1997	129291	ASCII
C19/SQ2A19N06DC03T000AC03T210.cut	aIIf1.590	Feb 20 1997	129374	ASCII
C19/SQ2A19N07DC03T000AC03T210.cut	aIIf1.591	Feb 20 1997	129457	ASCII
C19/SQ2A19N08DC03T000AC03T210.cut	aIIf1.592	Feb 20 1997	129457	ASCII
C19/SQ2A19N09DC03T000AC03T210.cut	aIIf1.593	Feb 20 1997	129457	ASCII
C19/SQ2A19N10DC03T000AC03T210.cut	aIIf1.594	Feb 20 1997	129457	ASCII
C19/SQ2A19N11DC03T000AC03T210.cut	aIIf1.595	Feb 20 1997	129374	ASCII
C19/SQ2A19N12DC03T000AC03T210.cut	aIIf1.596	Feb 20 1997	129291	ASCII
C19/SQ2A19N13DC03T000AC03T210.cut	aIIf1.597	Feb 20 1997	129125	ASCII
C19/SQ2A19N14DC03T000AC03T210.cut	aIIf1.598	Feb 20 1997	128876	ASCII
C19/SQ2A19N15DC03T000AC03T210.cut	aIIf1.599	Feb 20 1997	128710	ASCII
C19/SQ2A19N16DC03T000AC03T210.cut	aIIf1.600	Feb 20 1997	126038	ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
C21/SQ2A21N01DC03T000AC03T210.cut	aIIf1.601	Feb 20 1997	123856	ASCII
C21/SQ2A21N02DC03T000AC03T210.cut	aIIf1.602	Feb 20 1997	125872	ASCII
C21/SQ2A21N03DC03T000AC03T210.cut	aIIf1.603	Feb 20 1997	126358	ASCII
C21/SQ2A21N04DC03T000AC03T210.cut	aIIf1.604	Feb 20 1997	126524	ASCII
C21/SQ2A21N05DC03T000AC03T210.cut	aIIf1.605	Feb 20 1997	126524	ASCII
C21/SQ2A21N06DC03T000AC03T210.cut	aIIf1.606	Feb 20 1997	126524	ASCII
C21/SQ2A21N07DC03T000AC03T210.cut	aIIf1.607	Feb 20 1997	126524	ASCII
C21/SQ2A21N08DC03T000AC03T210.cut	aIIf1.608	Feb 20 1997	126524	ASCII
C21/SQ2A21N09DC03T000AC03T210.cut	aIIf1.609	Feb 20 1997	126524	ASCII
C21/SQ2A21N10DC03T000AC03T210.cut	aIIf1.610	Feb 20 1997	126524	ASCII
C21/SQ2A21N11DC03T000AC03T210.cut	aIIf1.611	Feb 20 1997	126524	ASCII
C21/SQ2A21N12DC03T000AC03T210.cut	aIIf1.612	Feb 20 1997	126524	ASCII
C21/SQ2A21N13DC03T000AC03T210.cut	aIIf1.613	Feb 20 1997	126524	ASCII
C21/SQ2A21N14DC03T000AC03T210.cut	aIIf1.614	Feb 20 1997	126524	ASCII
C21/SQ2A21N15DC03T000AC03T210.cut	aIIf1.615	Feb 20 1997	126287	ASCII
C21/SQ2A21N16DC03T000AC03T210.cut	aIIf1.616	Feb 20 1997	124022	ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
C25/SQ2A25N01DC03T000AC03T210.cut	aIIf1.617	Feb 20 1997	126374	ASCII
C25/SQ2A25N02DC03T000AC03T210.cut	aIIf1.618	Feb 20 1997	128046	ASCII
C25/SQ2A25N03DC03T000AC03T210.cut	aIIf1.619	Feb 20 1997	128461	ASCII
C25/SQ2A25N04DC03T000AC03T210.cut	aIIf1.620	Feb 20 1997	128544	ASCII
C25/SQ2A25N05DC03T000AC03T210.cut	aIIf1.621	Feb 20 1997	128627	ASCII
C25/SQ2A25N06DC03T000AC03T210.cut	aIIf1.622	Feb 20 1997	128627	ASCII
C25/SQ2A25N07DC03T000AC03T210.cut	aIIf1.623	Feb 20 1997	128710	ASCII
C25/SQ2A25N08DC03T000AC03T210.cut	aIIf1.624	Feb 20 1997	128710	ASCII
C25/SQ2A25N09DC03T000AC03T210.cut	aIIf1.625	Feb 20 1997	128710	ASCII
C25/SQ2A25N10DC03T000AC03T210.cut	aIIf1.626	Feb 20 1997	128710	ASCII

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C25/SQ2A25N11DC03T000AC03T210.cut	aIIf1.627	Feb 20 1997	128710	ASCII
C25/SQ2A25N12DC03T000AC03T210.cut	aIIf1.628	Feb 20 1997	128627	ASCII
C25/SQ2A25N13DC03T000AC03T210.cut	aIIf1.629	Feb 20 1997	128627	ASCII
C25/SQ2A25N14DC03T000AC03T210.cut	aIIf1.630	Feb 20 1997	128544	ASCII
C25/SQ2A25N15DC03T000AC03T210.cut	aIIf1.631	Feb 20 1997	128212	ASCII
C25/SQ2A25N16DC03T000AC03T210.cut	aIIf1.632	Feb 20 1997	124935	ASCII

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
C30/SQ2A30N01DC03T000AC03T210.cut	aIIf1.633	Feb 20 1997	123856	ASCII
C30/SQ2A30N02DC03T000AC03T210.cut	aIIf1.634	Feb 20 1997	126038	ASCII
C30/SQ2A30N03DC03T000AC03T210.cut	aIIf1.635	Feb 20 1997	126358	ASCII
C30/SQ2A30N04DC03T000AC03T210.cut	aIIf1.636	Feb 20 1997	126524	ASCII
C30/SQ2A30N05DC03T000AC03T210.cut	aIIf1.637	Feb 20 1997	126524	ASCII
C30/SQ2A30N06DC03T000AC03T210.cut	aIIf1.638	Feb 20 1997	126524	ASCII
C30/SQ2A30N07DC03T000AC03T210.cut	aIIf1.639	Feb 20 1997	126524	ASCII
C30/SQ2A30N08DC03T000AC03T210.cut	aIIf1.640	Feb 20 1997	126524	ASCII
C30/SQ2A30N09DC03T000AC03T210.cut	aIIf1.641	Feb 20 1997	126524	ASCII
C30/SQ2A30N10DC03T000AC03T210.cut	aIIf1.642	Feb 20 1997	126524	ASCII
C30/SQ2A30N11DC03T000AC03T210.cut	aIIf1.643	Feb 20 1997	126524	ASCII
C30/SQ2A30N12DC03T000AC03T210.cut	aIIf1.644	Feb 20 1997	126524	ASCII
C30/SQ2A30N13DC03T000AC03T210.cut	aIIf1.645	Feb 20 1997	126524	ASCII
C30/SQ2A30N14DC03T000AC03T210.cut	aIIf1.646	Feb 20 1997	126358	ASCII
C30/SQ2A30N15DC03T000AC03T210.cut	aIIf1.647	Feb 20 1997	126038	ASCII
C30/SQ2A30N16DC03T000AC03T210.cut	aIIf1.648	Feb 20 1997	123856	ASCII

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This attachment contains the "*.notes" files that were generated by CRAFT during the depletion calculations for Sequoyah Unit 2. These files are referred to as "*.notes" files due to their ".notes" extension. The "*.notes" files are contained on an attachment tape of this calculation file (the attachment tape has been moved to Reference 7.7). The information contained in this hard-copy representation of Attachment III is a listing of the various "*.notes" files and their attributes. The file sizes listed in the following table are the file sizes as they appear on the Hewlett Packard (HP) Series 9000 workstation. The HP file sizes differ from the file sizes on the attachment tape due to the difference in the block sizes between the HP and the personal computer. The tape containing Attachment III was written using the Colorado Model T1000e External Parallel Port Backup System for personal computers.

Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
A06/SQ2A05N01DC03T000AC03T210.notes	aII.If1	Feb 20 1997	9147	ASCII
A06/SQ2A05N02DC03T000AC03T210.notes	aII.If2	Feb 20 1997	9140	ASCII
A06/SQ2A05N03DC03T000AC03T210.notes	aII.If3	Feb 20 1997	9437	ASCII
A06/SQ2A05N04DC03T000AC03T210.notes	aII.If4	Feb 20 1997	9395	ASCII
A06/SQ2A05N05DC03T000AC03T210.notes	aII.If5	Feb 20 1997	9458	ASCII
A06/SQ2A05N06DC03T000AC03T210.notes	aII.If6	Feb 20 1997	9440	ASCII
A06/SQ2A05N07DC03T000AC03T210.notes	aII.If7	Feb 20 1997	9440	ASCII
A06/SQ2A05N08DC03T000AC03T210.notes	aII.If8	Feb 20 1997	9444	ASCII
A06/SQ2A05N09DC03T000AC03T210.notes	aII.If9	Feb 20 1997	9446	ASCII
A06/SQ2A05N10DC03T000AC03T210.notes	aIII.f10	Feb 20 1997	9442	ASCII
A06/SQ2A05N11DC03T000AC03T210.notes	aIII.f11	Feb 20 1997	9450	ASCII
A06/SQ2A05N12DC03T000AC03T210.notes	aIII.f12	Feb 20 1997	9436	ASCII
A06/SQ2A05N13DC03T000AC03T210.notes	aIII.f13	Feb 20 1997	9452	ASCII
A06/SQ2A05N14DC03T000AC03T210.notes	aIII.f14	Feb 20 1997	9436	ASCII
A06/SQ2A05N15DC03T000AC03T210.notes	aIII.f15	Feb 20 1997	9477	ASCII
A06/SQ2A05N16DC03T000AC03T210.notes	aIII.f16	Feb 20 1997	9118	ASCII
A06/SQ2A06N01DC01T187AC02T000.notes	aIII.f17	Feb 20 1997	17308	ASCII
A06/SQ2A06N02DC01T187AC02T000.notes	aIII.f18	Feb 20 1997	18916	ASCII
A06/SQ2A06N03DC01T187AC02T000.notes	aIII.f19	Feb 20 1997	19443	ASCII
A06/SQ2A06N04DC01T187AC02T000.notes	aIII.f20	Feb 20 1997	19809	ASCII
A06/SQ2A06N05DC01T187AC02T000.notes	aIII.f21	Feb 20 1997	19872	ASCII
A06/SQ2A06N06DC01T187AC02T000.notes	aIII.f22	Feb 20 1997	19980	ASCII
A06/SQ2A06N07DC01T187AC02T000.notes	aIII.f23	Feb 20 1997	20221	ASCII
A06/SQ2A06N08DC01T187AC02T000.notes	aIII.f24	Feb 20 1997	20273	ASCII
A06/SQ2A06N09DC01T187AC02T000.notes	aIII.f25	Feb 20 1997	20323	ASCII
A06/SQ2A06N10DC01T187AC02T000.notes	aIII.f26	Feb 20 1997	20310	ASCII
A06/SQ2A06N11DC01T187AC02T000.notes	aIII.f27	Feb 20 1997	20271	ASCII
A06/SQ2A06N12DC01T187AC02T000.notes	aIII.f28	Feb 20 1997	20094	ASCII
A06/SQ2A06N13DC01T187AC02T000.notes	aIII.f29	Feb 20 1997	19882	ASCII
A06/SQ2A06N14DC01T187AC02T000.notes	aIII.f30	Feb 20 1997	19754	ASCII
A06/SQ2A06N15DC01T187AC02T000.notes	aIII.f31	Feb 20 1997	19325	ASCII
A06/SQ2A06N16DC01T187AC02T000.notes	aIII.f32	Feb 20 1997	17645	ASCII
A06/SQ2A08N01DC02T000AC02T145.notes	aIII.f33	Feb 20 1997	9054	ASCII
A06/SQ2A08N01DC02T145AC03T000.notes	aIII.f34	Feb 20 1997	18024	ASCII
A06/SQ2A08N02DC02T000AC02T145.notes	aIII.f35	Feb 20 1997	9359	ASCII
A06/SQ2A08N02DC02T145AC03T000.notes	aIII.f36	Feb 20 1997	19144	ASCII
A06/SQ2A08N03DC02T000AC02T145.notes	aIII.f37	Feb 20 1997	9445	ASCII
A06/SQ2A08N03DC02T145AC03T000.notes	aIII.f38	Feb 20 1997	19617	ASCII
A06/SQ2A08N04DC02T000AC02T145.notes	aIII.f39	Feb 20 1997	9537	ASCII
A06/SQ2A08N04DC02T145AC03T000.notes	aIII.f40	Feb 20 1997	19824	ASCII
A06/SQ2A08N05DC02T000AC02T145.notes	aIII.f41	Feb 20 1997	9600	ASCII
A06/SQ2A08N05DC02T145AC03T000.notes	aIII.f42	Feb 20 1997	19818	ASCII
A06/SQ2A08N06DC02T000AC02T145.notes	aIII.f43	Feb 20 1997	9574	ASCII
A06/SQ2A08N06DC02T145AC03T000.notes	aIII.f44	Feb 20 1997	19762	ASCII
A06/SQ2A08N07DC02T000AC02T145.notes	aIII.f45	Feb 20 1997	9576	ASCII
A06/SQ2A08N07DC02T145AC03T000.notes	aIII.f46	Feb 20 1997	19762	ASCII
A06/SQ2A08N08DC02T000AC02T145.notes	aIII.f47	Feb 20 1997	9570	ASCII
A06/SQ2A08N08DC02T145AC03T000.notes	aIII.f48	Feb 20 1997	19768	ASCII
A06/SQ2A08N09DC02T000AC02T145.notes	aIII.f49	Feb 20 1997	9584	ASCII
A06/SQ2A08N09DC02T145AC03T000.notes	aIII.f50	Feb 20 1997	19750	ASCII

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A06/SQ2A08N10DC02T000AC02T145.notes
 A06/SQ2A08N10DC02T145AC03T000.notes
 A06/SQ2A08N11DC02T000AC02T145.notes
 A06/SQ2A08N11DC02T145AC03T000.notes
 A06/SQ2A08N12DC02T000AC02T145.notes
 A06/SQ2A08N12DC02T145AC03T000.notes
 A06/SQ2A08N13DC02T000AC02T145.notes
 A06/SQ2A08N13DC02T145AC03T000.notes
 A06/SQ2A08N14DC02T000AC02T145.notes
 A06/SQ2A08N14DC02T145AC03T000.notes
 A06/SQ2A08N15DC02T000AC02T145.notes
 A06/SQ2A08N15DC02T145AC03T000.notes
 A06/SQ2A08N16DC02T000AC02T145.notes
 A06/SQ2A08N16DC02T145AC03T000.notes

aIII.f51
 aIII.f52
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 aIII.f64

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Computer File Name	Tape Backup File Name	File Date (Output)	File Size (Bytes)	File Type (Format)
A08/SQ2A04N01DC02T000AC02T145.notes	aIII.f65	Feb 20 1997	8950	ASCII
A08/SQ2A04N01DC02T145AC03T000.notes	aIII.f66	Feb 20 1997	19084	ASCII
A08/SQ2A04N02DC02T000AC02T145.notes	aIII.f67	Feb 20 1997	9213	ASCII
A08/SQ2A04N02DC02T145AC03T000.notes	aIII.f68	Feb 20 1997	20050	ASCII
A08/SQ2A04N03DC02T000AC02T145.notes	aIII.f69	Feb 20 1997	9379	ASCII
A08/SQ2A04N03DC02T145AC03T000.notes	aIII.f70	Feb 20 1997	20191	ASCII
A08/SQ2A04N04DC02T000AC02T145.notes	aIII.f71	Feb 20 1997	9413	ASCII
A08/SQ2A04N04DC02T145AC03T000.notes	aIII.f72	Feb 20 1997	20257	ASCII
A08/SQ2A04N05DC02T000AC02T145.notes	aIII.f73	Feb 20 1997	9395	ASCII
A08/SQ2A04N05DC02T145AC03T000.notes	aIII.f74	Feb 20 1997	20241	ASCII
A08/SQ2A04N06DC02T000AC02T145.notes	aIII.f75	Feb 20 1997	9363	ASCII
A08/SQ2A04N06DC02T145AC03T000.notes	aIII.f76	Feb 20 1997	20143	ASCII
A08/SQ2A04N07DC02T000AC02T145.notes	aIII.f77	Feb 20 1997	9349	ASCII
A08/SQ2A04N07DC02T145AC03T000.notes	aIII.f78	Feb 20 1997	20091	ASCII
A08/SQ2A04N08DC02T000AC02T145.notes	aIII.f79	Feb 20 1997	9345	ASCII
A08/SQ2A04N08DC02T145AC03T000.notes	aIII.f80	Feb 20 1997	20085	ASCII
A08/SQ2A04N09DC02T000AC02T145.notes	aIII.f81	Feb 20 1997	9351	ASCII
A08/SQ2A04N09DC02T145AC03T000.notes	aIII.f82	Feb 20 1997	20089	ASCII
A08/SQ2A04N10DC02T000AC02T145.notes	aIII.f83	Feb 20 1997	9321	ASCII
A08/SQ2A04N10DC02T145AC03T000.notes	aIII.f84	Feb 20 1997	20115	ASCII
A08/SQ2A04N11DC02T000AC02T145.notes	aIII.f85	Feb 20 1997	9333	ASCII
A08/SQ2A04N11DC02T145AC03T000.notes	aIII.f86	Feb 20 1997	20109	ASCII
A08/SQ2A04N12DC02T000AC02T145.notes	aIII.f87	Feb 20 1997	9323	ASCII
A08/SQ2A04N12DC02T145AC03T000.notes	aIII.f88	Feb 20 1997	20105	ASCII
A08/SQ2A04N13DC02T000AC02T145.notes	aIII.f89	Feb 20 1997	9335	ASCII
A08/SQ2A04N13DC02T145AC03T000.notes	aIII.f90	Feb 20 1997	20107	ASCII
A08/SQ2A04N14DC02T000AC02T145.notes	aIII.f91	Feb 20 1997	9359	ASCII
A08/SQ2A04N14DC02T145AC03T000.notes	aIII.f92	Feb 20 1997	20107	ASCII
A08/SQ2A04N15DC02T000AC02T145.notes	aIII.f93	Feb 20 1997	9287	ASCII
A08/SQ2A04N15DC02T145AC03T000.notes	aIII.f94	Feb 20 1997	19958	ASCII
A08/SQ2A04N16DC02T000AC02T145.notes	aIII.f95	Feb 20 1997	8972	ASCII
A08/SQ2A04N16DC02T145AC03T000.notes	aIII.f96	Feb 20 1997	19058	ASCII
A08/SQ2A08N01DC01T187AC02T000.notes	aIII.f97	Feb 20 1997	16706	ASCII
A08/SQ2A08N02DC01T187AC02T000.notes	aIII.f98	Feb 20 1997	17892	ASCII
A08/SQ2A08N03DC01T187AC02T000.notes	aIII.f99	Feb 20 1997	18675	ASCII
A08/SQ2A08N04DC01T187AC02T000.notes	aIII.f.100	Feb 20 1997	19031	ASCII
A08/SQ2A08N05DC01T187AC02T000.notes	aIII.f.101	Feb 20 1997	19264	ASCII
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A08/SQ2A16N06DC03T000AC03T210.notes	aIIIf.118	Feb 20 1997	9504	ASCII
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A15/SQ2A10N07DC02T000AC02T145.notes	aIIIf.141	Feb 20 1997	9355	ASCII
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A15/SQ2A18N08DC03T000AC03T210.notes	aIIIf.184	Feb 20 1997	9512	ASCII

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A15/SQ2A18N12DC03T000AC03T210.notes	aIIIf.188	Feb 20 1997	9514	ASCII
A15/SQ2A18N13DC03T000AC03T210.notes	aIIIf.189	Feb 20 1997	9570	ASCII
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A21a/SQ2A02N05DC02T145AC03T000.notes	aIIIf.266	Feb 20 1997	20199	ASCII
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Waste Package Operations

Engineering Calculation Attachment

Title: Sequoyah Unit 2 CRC Depletion Calculations

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A21a/SQ2A21N15DC01T187AC02T000.notes
A21a/SQ2A21N16DC01T187AC02T000.notes

aIIIf.319
aIIIf.320

Feb 20 1997
Feb 20 1997

17928
16732

ASCII
ASCII

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Engineering Calculation Attachment

Title: Sequoyah Unit 2 CRC Depletion Calculations

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Waste Package Operations

Engineering Calculation Attachment

Title: Sequoyah Unit 2 CRC Depletion Calculations

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Engineering Calculation Attachment

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Engineering Calculation Attachment

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Engineering Calculation Attachment

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B15/SQ2A15N05DC02T145AC03T000.notes	aIIIf.869	Feb 20 1997	19132	ASCII
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B15/SQ2A15N08DC02T145AC03T000.notes	aIIIf.872	Feb 20 1997	19128	ASCII
B15/SQ2A15N09DC02T145AC03T000.notes	aIIIf.873	Feb 20 1997	19170	ASCII
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B15/SQ2A23N13DC03T000AC03T210.notes	aIIIf.893	Feb 20 1997	9363	ASCII
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B19/SQ2A19N07DC02T145AC03T000.notes	aIIIf.903	Feb 20 1997	19797	ASCII
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B19/SQ2A19N09DC02T145AC03T000.notes	aIIIf.905	Feb 20 1997	19777	ASCII
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B19/SQ2A24N03DC03T000AC03T210.notes	aIIIf.915	Feb 20 1997	9367	ASCII
B19/SQ2A24N04DC03T000AC03T210.notes	aIIIf.916	Feb 20 1997	9369	ASCII
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B21/SQ2A21N04DC02T145AC03T000.notes	aIIIf.932	Feb 20 1997	19122	ASCII
B21/SQ2A21N05DC02T145AC03T000.notes	aIIIf.933	Feb 20 1997	19202	ASCII
B21/SQ2A21N06DC02T145AC03T000.notes	aIIIf.934	Feb 20 1997	19306	ASCII
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B25/SQ2A25N02DC02T145AC03T000.notes	aIIIf.978	Feb 20 1997	19127	ASCII
B25/SQ2A25N03DC02T145AC03T000.notes	aIIIf.979	Feb 20 1997	19519	ASCII
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B25/SQ2A25N05DC02T145AC03T000.notes	aIIIf.981	Feb 20 1997	19657	ASCII
B25/SQ2A25N06DC02T145AC03T000.notes	aIIIf.982	Feb 20 1997	19665	ASCII
B25/SQ2A25N07DC02T145AC03T000.notes	aIIIf.983	Feb 20 1997	19659	ASCII
B25/SQ2A25N08DC02T145AC03T000.notes	aIIIf.984	Feb 20 1997	19661	ASCII
B25/SQ2A25N09DC02T145AC03T000.notes	aIIIf.985	Feb 20 1997	19765	ASCII
B25/SQ2A25N10DC02T145AC03T000.notes	aIIIf.986	Feb 20 1997	19733	ASCII
B25/SQ2A25N11DC02T145AC03T000.notes	aIIIf.987	Feb 20 1997	19747	ASCII
B25/SQ2A25N12DC02T145AC03T000.notes	aIIIf.988	Feb 20 1997	19741	ASCII
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B25/SQ2A25N14DC02T145AC03T000.notes	aIIIf.990	Feb 20 1997	19649	ASCII
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B26/SQ2A26N03DC02T145AC03T000.notes	aIIIf.995	Feb 20 1997	18569	ASCII
B26/SQ2A26N04DC02T145AC03T000.notes	aIIIf.996	Feb 20 1997	18721	ASCII
B26/SQ2A26N05DC02T145AC03T000.notes	aIIIf.997	Feb 20 1997	18731	ASCII
B26/SQ2A26N06DC02T145AC03T000.notes	aIIIf.998	Feb 20 1997	18705	ASCII
B26/SQ2A26N07DC02T145AC03T000.notes	aIIIf.999	Feb 20 1997	18697	ASCII
B26/SQ2A26N08DC02T145AC03T000.notes	aIIIf1.000	Feb 20 1997	18693	ASCII
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B26/SQ2A26N10DC02T145AC03T000.notes	aIIIf1.002	Feb 20 1997	18796	ASCII
B26/SQ2A26N11DC02T145AC03T000.notes	aIIIf1.003	Feb 20 1997	18790	ASCII
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B26/SQ2A26N13DC02T145AC03T000.notes	aIIIf1.005	Feb 20 1997	18792	ASCII
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B26/SQ2A26N15DC02T145AC03T000.notes	aIIIf1.007	Feb 20 1997	18311	ASCII
B26/SQ2A26N16DC02T145AC03T000.notes	aIIIf1.008	Feb 20 1997	17299	ASCII
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B26/SQ2A29N02DC03T000AC03T210.notes	aIIIf1.010	Feb 20 1997	9046	ASCII
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B26/SQ2A29N08DC03T000AC03T210.notes	aIIIf1.016	Feb 20 1997	9207	ASCII
B26/SQ2A29N09DC03T000AC03T210.notes	aIIIf1.017	Feb 20 1997	9205	ASCII
B26/SQ2A29N10DC03T000AC03T210.notes	aIIIf1.018	Feb 20 1997	9258	ASCII
B26/SQ2A29N11DC03T000AC03T210.notes	aIIIf1.019	Feb 20 1997	9250	ASCII
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B29/SQ2A12N04DC03T000AC03T210.notes	aIIIf1.028	Feb 20 1997	9363	ASCII
B29/SQ2A12N05DC03T000AC03T210.notes	aIIIf1.029	Feb 20 1997	9355	ASCII
B29/SQ2A12N06DC03T000AC03T210.notes	aIIIf1.030	Feb 20 1997	9417	ASCII
B29/SQ2A12N07DC03T000AC03T210.notes	aIIIf1.031	Feb 20 1997	9413	ASCII
B29/SQ2A12N08DC03T000AC03T210.notes	aIIIf1.032	Feb 20 1997	9423	ASCII
B29/SQ2A12N09DC03T000AC03T210.notes	aIIIf1.033	Feb 20 1997	9407	ASCII
B29/SQ2A12N10DC03T000AC03T210.notes	aIIIf1.034	Feb 20 1997	9391	ASCII
B29/SQ2A12N11DC03T000AC03T210.notes	aIIIf1.035	Feb 20 1997	9403	ASCII

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B29/SQ2A12N12DC03T000AC03T210.notes	aIIIf1.036	Feb 20 1997	9385	ASCII
B29/SQ2A12N13DC03T000AC03T210.notes	aIIIf1.037	Feb 20 1997	9387	ASCII
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B29/SQ2A12N15DC03T000AC03T210.notes	aIIIf1.039	Feb 20 1997	9365	ASCII
B29/SQ2A12N16DC03T000AC03T210.notes	aIIIf1.040	Feb 20 1997	9056	ASCII
B29/SQ2A29N01DC02T145AC03T000.notes	aIIIf1.041	Feb 20 1997	17914	ASCII
B29/SQ2A29N02DC02T145AC03T000.notes	aIIIf1.042	Feb 20 1997	10840	ASCII
B29/SQ2A29N03DC02T145AC03T000.notes	aIIIf1.043	Feb 20 1997	19210	ASCII
B29/SQ2A29N04DC02T145AC03T000.notes	aIIIf1.044	Feb 20 1997	19480	ASCII
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B29/SQ2A29N06DC02T145AC03T000.notes	aIIIf1.046	Feb 20 1997	19478	ASCII
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B29/SQ2A29N11DC02T145AC03T000.notes	aIIIf1.051	Feb 20 1997	19554	ASCII
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B29/SQ2A29N14DC02T145AC03T000.notes	aIIIf1.054	Feb 20 1997	19460	ASCII
B29/SQ2A29N15DC02T145AC03T000.notes	aIIIf1.055	Feb 20 1997	19020	ASCII
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B30/SQ2A03N03DC03T000AC03T210.notes	aIIIf1.059	Feb 20 1997	9411	ASCII
B30/SQ2A03N04DC03T000AC03T210.notes	aIIIf1.060	Feb 20 1997	9359	ASCII
B30/SQ2A03N05DC03T000AC03T210.notes	aIIIf1.061	Feb 20 1997	9339	ASCII
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B30/SQ2A03N10DC03T000AC03T210.notes	aIIIf1.066	Feb 20 1997	9375	ASCII
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B30/SQ2A03N12DC03T000AC03T210.notes	aIIIf1.068	Feb 20 1997	9373	ASCII
B30/SQ2A03N13DC03T000AC03T210.notes	aIIIf1.069	Feb 20 1997	9363	ASCII
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B30/SQ2A30N12DC02T145AC03T000.notes	aIIIf1.084	Feb 20 1997	19779	ASCII
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B30/SQ2A30N14DC02T145AC03T000.notes	aIIIf1.086	Feb 20 1997	19761	ASCII
B30/SQ2A30N15DC02T145AC03T000.notes	aIIIf1.087	Feb 20 1997	19483	ASCII
B30/SQ2A30N16DC02T145AC03T000.notes	aIIIf1.088	Feb 20 1997	18317	ASCII

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B31/SQ2A26N03DC03T000AC03T210.notes	aIIIf1.091	Feb 20 1997	8231	ASCII
B31/SQ2A26N04DC03T000AC03T210.notes	aIIIf1.092	Feb 20 1997	9215	ASCII
B31/SQ2A26N05DC03T000AC03T210.notes	aIIIf1.093	Feb 20 1997	9205	ASCII
B31/SQ2A26N06DC03T000AC03T210.notes	aIIIf1.094	Feb 20 1997	9209	ASCII
B31/SQ2A26N07DC03T000AC03T210.notes	aIIIf1.095	Feb 20 1997	9207	ASCII
B31/SQ2A26N08DC03T000AC03T210.notes	aIIIf1.096	Feb 20 1997	9213	ASCII
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B31/SQ2A26N13DC03T000AC03T210.notes	aXXXX1.101	Feb 20 1997	9260	ASCII
B31/SQ2A26N14DC03T000AC03T210.notes	aXXXX1.102	Feb 20 1997	9201	ASCII
B31/SQ2A26N15DC03T000AC03T210.notes	aXXXX1.103	Feb 20 1997	9184	ASCII
B31/SQ2A26N16DC03T000AC03T210.notes	aXXXX1.104	Feb 20 1997	8997	ASCII
B31/SQ2A31N01DC02T145AC03T000.notes	aXXXX1.105	Feb 20 1997	17116	ASCII
B31/SQ2A31N02DC02T145AC03T000.notes	aXXXX1.106	Feb 20 1997	18225	ASCII
B31/SQ2A31N03DC02T145AC03T000.notes	aXXXX1.107	Feb 20 1997	18589	ASCII
B31/SQ2A31N04DC02T145AC03T000.notes	aXXXX1.108	Feb 20 1997	18731	ASCII
B31/SQ2A31N05DC02T145AC03T000.notes	aXXXX1.109	Feb 20 1997	18719	ASCII
B31/SQ2A31N06DC02T145AC03T000.notes	aXXXX1.110	Feb 20 1997	18687	ASCII
B31/SQ2A31N07DC02T145AC03T000.notes	aXXXX1.111	Feb 20 1997	18798	ASCII
B31/SQ2A31N08DC02T145AC03T000.notes	aXXXX1.112	Feb 20 1997	18788	ASCII
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B31/SQ2A31N12DC02T145AC03T000.notes	aXXXX1.116	Feb 20 1997	18798	ASCII
B31/SQ2A31N13DC02T145AC03T000.notes	aXXXX1.117	Feb 20 1997	18796	ASCII
B31/SQ2A31N14DC02T145AC03T000.notes	aXXXX1.118	Feb 20 1997	18697	ASCII
B31/SQ2A31N15DC02T145AC03T000.notes	aXXXX1.119	Feb 20 1997	18367	ASCII
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Attachment IV, Page 1 of 2

This attachment contains the results for the principle isotope concentrations in the depleted fuel of the Sequoyah Unit 2 fuel assemblies. The principle isotope concentration result tables are contained on an attachment tape of this calculation file (the attachment tape has been moved to Reference 7.7). The information contained in this hard-copy representation of Attachment IV is a listing of the various files containing the principle isotope concentration result tables that are contained on the attachment tape. Each file contains the results for a given fuel assembly. The filenames identify the fuel assembly to which they correspond. The file sizes listed in the following table are the file sizes as they appear on the Hewlett Packard (HP) Series 9000 workstation. The HP file sizes differ from the file sizes on the attachment tape due to the difference in the block sizes between the HP and the personal computer. The tape containing Attachment IV was written using the Colorado Model T1000e External Parallel Port Backup System for personal computers.

Filename	File Type	File Size (Bytes)	Date File Copied to Tape
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A21.results	ASCII	248,675	3/16/98
A21a.results	ASCII	248,675	3/16/98
A25.results	ASCII	248,675	3/16/98
A25a.results	ASCII	248,675	3/16/98
A26.results	ASCII	248,675	3/16/98
A26a.results	ASCII	248,675	3/16/98
A29.results	ASCII	248,675	3/16/98
A29a.results	ASCII	248,675	3/16/98
A30.results	ASCII	248,675	3/16/98
A31.results	ASCII	248,675	3/16/98
B14.results	ASCII	149,205	3/16/98
B15.results	ASCII	149,205	3/16/98
B19.results	ASCII	149,205	3/16/98
B21.results	ASCII	149,205	3/16/98
B25.results	ASCII	149,205	3/16/98
B26.results	ASCII	149,205	3/16/98
B29.results	ASCII	149,205	3/16/98
B30.results	ASCII	149,205	3/16/98
B31.results	ASCII	149,205	3/16/98
C02.results	ASCII	49,735	3/16/98
C04.results	ASCII	49,735	3/16/98
C06.results	ASCII	49,735	3/16/98
C08.results	ASCII	49,735	3/16/98

Waste Package Operations**Engineering Calculation Attachment****Title: Sequoyah Unit 2 CRC Depletion Calculations****Document Identifier: B00000000-01717-0210-00005 REV 00****Attachment IV, Page 2 of 2**

Filename	File Type	File Size (Bytes)	Date File Copied to Tape
C14.results	ASCII	49,735	3/16/98
C15.results	ASCII	49,735	3/16/98
C17.results	ASCII	49,735	3/16/98
C19.results	ASCII	49,735	3/16/98
C21.results	ASCII	49,735	3/16/98
C25.results	ASCII	49,735	3/16/98
C30.results	ASCII	49,735	3/16/98