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1. Purpose

The purpose of this design analysis is to determine the accuracy of the SAS2H module of SCALE 4.3 in predicting isotopic concentrations of spent fuel assemblies. The objective is to develop a methodology for modeling assemblies similar to those evaluated within this analysis and to establish the consistency of SAS2H predictions. The results of this analysis may then be applied to future depletion calculations using SAS2H in which no measurements are available.

2. Quality Assurance

The Quality Assurance (QA) program applies to this analysis. The work reported in this document is part of the Waste Package Design analysis that will eventually support the License Application Design phase. This activity, when appropriately confirmed, can impact the proper functioning of the Mined Geologic Disposal System (MGDS) waste package; the waste package has been identified as an MGDS Q-List item important to safety and waste isolation (pp. 4, 15, Reference 5.1). The waste package is on the Q-List by direct inclusion by the Department of Energy (DOE), without conducting a QAP-2-3 evaluation. The Waste Package Development Department (WPDD) responsible manager has evaluated this activity in accordance with QAP-2-0, *Conduct of Activities*. The *Perform Criticality, Thermal, Structural, and Shielding Analyses* (Reference 5.2) evaluation has determined the preparation and review of this design analysis is subject to *Quality Assurance Requirements and Description* (Reference 5.3) requirements. As specified in NLP-3-18, this activity is subject to QA controls.

The analysis described in this document supports development of the disposal criticality analysis methodology. No designs were analyzed in this document. This document will not directly support any construction, fabrication, or procurement activity and therefore is not required to be procedurally controlled as TBV (to be verified). The calculation design inputs or information used in this document come from data accepted by the Nuclear Regulatory Commission and by the scientific and engineering community as established fact. The specific references are listed in Section 5 and identified in Section 7. The information is therefore not treated as unqualified data.

3. Method

The analytical model employed for this analysis was the SAS2H module of the SCALE sequence. Based upon fuel design, power history, and operating data for specific assemblies in the Cooper boiling water reactor (BWR), a computational model was developed for use with the SAS2H module of SCALE. The SAS2H module is used to perform a fuel depletion analysis to predict the isotopic concentrations in localized areas of assembly pins (pellet samples) subsequent to irradiation and cooling time. The isotopic concentrations predicted by the SAS2H module are then compared with measured concentrations of the same localized areas (axial locations) of the assembly pins to determine the accuracy of the developed model. The measured isotopic concentrations used for comparisons in the analysis are obtained from a separate report (Reference 5.6).

4. Design Inputs

The sources for the design parameters are References 5.4 through 5.9. References 5.4 and 5.5 provide information on molar masses and half-lives; the assembly design, power history and operating parameters are obtained from References 5.6 and 5.7; the cladding composition from Reference 5.8; and a list of trace elements in the fuel is derived from Reference 5.9.

4.1 Design Parameters

The half-lives of selected isotopes and molar masses of selected elements are obtained from Reference 5.4, while molar masses for selected isotopes are obtained from Reference 5.5. The half-life and molar masses are provided below within three significant figures. Precision beyond three significant figures is not necessary since the calculated isotopic concentrations from SCALE are only to three significant figures. Also, the weight per mole of enriched uranium is approximated by the weight per mole of natural uranium since the weight percent of enrichment is small.

Mole of natural uranium = 238 g,
Half-Life of ^{99}Tc = 2.13×10^5 years,
Half-Life of ^{237}Np = 2.14×10^6 years,
Half-Life of ^{241}Am = 432.7 years,
 6.02×10^{23} atoms per mole. (Reference 5.4)
Mole of ^{99}Tc = 98.9 g,
Mole of ^{237}Np = 237 g,
Mole of ^{241}Am = 241 g. (Reference 5.5)

General spent fuel characteristics for each test sample are presented in Table 4-1 and include the initial ^{235}U enrichment, final burnup and the cooling time (p. 4.93, Figure 4.2, and Tables 4.17 and D.1; Reference 5.6). The initial enrichment for the type 1 fuel rod, which includes over half of the assembly's fuel rods, is 2.93 wt% ^{235}U and the burnup ranges from 17.84 to 33.94 GWd/MTU. The cooling time reflects the time after shutdown in which the burnup measurements were performed.

Assembly design parameters are presented in Table 4-2 (Table 4.1, Reference 5.6; Table 1 and 3, Reference 5.6). The assembly is a General Electric (GE) 7 x 7 and contains four types of fuel rods and three types of burnable poison rods. Assembly channel dimensions are obtained for Quad Cities, which also uses a GE 7 x 7 assembly (Table 1, Reference 5.7). A cross section of the assembly is presented in Figure 4-1 (Figure 4.2, Reference 5.6; Figure 8, Reference 5.7). The initial enrichments of ^{235}U and Gd_2O_3 for each type of fuel rod and burnable poison rod are included in Table 4-3. Power histories for each assembly during the three cycles of irradiation are presented in Table 4-4 in the form of Linear Heat Generation Rates (LHGRs) (Table A.2, Reference 5.6). The assemblies were irradiated for 5 cycles during cycles 1, 2, 3, 6 and 7. Both rods ADD2966 and ADD2974 are Type 1 fuel rods.

The composition of the channel, Zircaloy-4, is presented in Table 4-5, and has a density of 6.56 g/cm³ (Reference 5.8). A list of trace elements in the fuel used in updating cross sections during the depletion analysis is presented in Table 4-6 and developed with consideration of elements used in (Table 1, Reference 5.9).

The measured isotopic concentrations for plutonium and uranium isotopes are presented in Table 4-7, given in g/gUO₂ (Table 4.17, Reference 5.6). Also measured isotopic concentrations for ⁹⁹Tc, ²³⁷Np and ²⁴¹Am are presented in Table 4-8, given in Ci/gUO₂ (Table 4.17, Reference 5.6). The measurements were performed at the Materials Characterization Center at Pacific Northwest Laboratory for fuel pellets at three different axial positions in Rods ADD2974 and ADD2966, of Bundle CZ346.

Table 4-1. Spent Fuel Characteristic Parameters for Cooper BWR

Sample	Axial Location from Top, cm	Enrichment, wt % ²³⁵ U	Burnup, MWd/kgM	Cooling Time, years
ADD2966-B	55.107	2.93	18.96	5.35
ADD2966-K	218.869	2.93	33.07	5.35
ADD2966-T	274.777	2.93	33.94	5.35
ADD2974-B	55.723	2.93	17.84	5.28
ADD2974-J	115.042	2.93	29.23	5.28
ADD2974-U	291.087	2.93	31.04	5.28

Reference 5.6

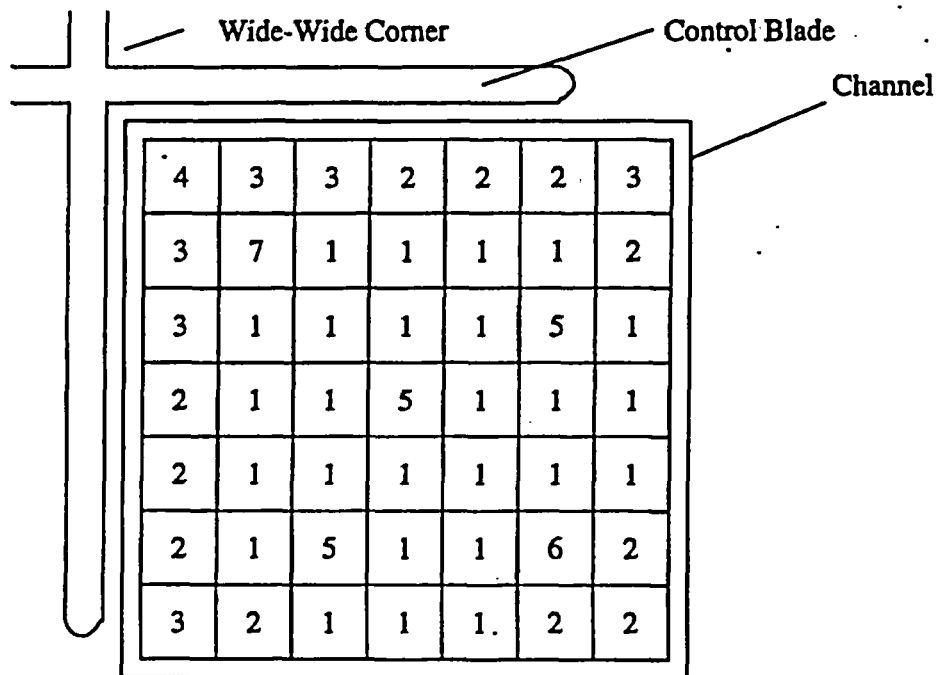
Table 4-2. Assembly Design Parameters for Cooper BWR

Parameter	Data
Assembly general data:	
Designer	General Electric
Lattice	7 x 7
Number of Fuel Rods	49
Assembly Pitch, in. (cm)	6.0 (15.24)
Channel	
Outside Dimension, in. (cm)	5.438 (13.813)
Thickness, in. (cm)	0.080 (0.203)
Material	Zircaloy-4
Fuel Rod Data:	
Type of Fuel Pellet	UO ₂
Pellet immersion density, g/cm ³	10.32
Rod Pitch, cm	1.87
Rod Outside Diameter (OD), cm	1.43
Cladding Thickness, cm	0.094
Pellet Diameter, cm	1.21
Active Fuel Length, cm	371
Clad Material	Zircaloy-2
Peripheral-Rod-to-Channel Spacing, in. (cm)	0.1435 (0.364)

Dimensions are converted from inches to centimeters by the following relationship: 1 in. = 2.54 cm.

Reference 5.6

Figure 4-1. Cross Section of Cooper BWR Assembly



Fuel Rod Location

See Table 4-3 for Rod Enrichments

References 5.6 and 5.7

Table 4-3. Rod Enrichments for Cooper BWR

Rod Type	Enrichment, wt % ²³⁵ U	wt % Gd ₂ O ₃	Number of Rods
1	2.93	0	26
2	1.94	0	11
3	1.69	0	6
4	1.33	0	1
5	2.93	3.0	3
6	2.93	4.0	1
7	1.94	4.0	1

Reference 5.6

Table 4-4. Power History for Bundle CZ346 from Cooper BWR

Elapsed Time, days	Time Interval, days	Power Density, MW/MTU	Cumulative Burnup, MWd/MTU	Average LHGR, kW/m
Cycle 1				
19	19	15.63	0.297	16.34
27	8	0	0.297	0
90	63	14.21	1.192	14.84
157	67	22.74	2.715	23.76
174	17	0	2.715	0
182	8	14.21	2.829	14.84
215	33	25.58	3.673	26.73
225	10	0	3.673	0
296	71	27.01	5.591	28.22
451	155	14.21	7.793	14.84
486	35	0	8.062	0
505	19	14.21	8.574	14.84

Table 4-4. Power History for Bundle CZ346 from Cooper BWR

Elapsed Time, days	Time Interval, days	Power Density, MW/MTU	Cumulative Burnup, MWd/MTU	Average LHGR, kW/m
525	20	25.58	8.574	26.73
532	7	0	9.074	0
554	22	22.74	9.074	23.76
566	12	0	10.325	0
621	55	22.74	11.379	23.76
674	53	19.89	11.379	20.79
693	19	0	11.876	0
718	25	19.89	11.876	20.79
807	89	22.74	13.900	23.76
Cycle 2				
866	59	0	13.900	0
880	14	15.46	14.116	16.15
904	24	20.98	14.620	21.92
919	15	11.04	14.785	11.53
945	26	20.99	15.331	21.93
953	8	0	15.331	0
996	43	20.99	16.234	21.93
1001	5	8.84	16.278	9.24
1017	16	20.99	16.614	21.93
1022	5	0	16.614	0
1044	22	19.88	17.051	20.77
1083	39	13.25	17.568	13.84
1172	89	17.67	19.140	18.46

Table 4-4. Power History for Bundle CZ346 from Cooper BWR

Elapsed Time, days	Time Interval, days	Power Density, MW/MTU	Cumulative Burnup, MWd/MTU	Average LHGR, kW/m
Cycle 3				
1203	31	0	19.140	0
1367	164	16.95	21.920	17.71
Cycle 6				
2166	799	0	21.920	0
2189	23	10.33	22.158	10.80
2214	25	11.48	22.445	12.00
2228	14	5.74	23.525	6.00
2326	98	10.91	23.594	11.40
2335	9	0	23.594	0
2377	42	10.91	24.052	11.40
2393	16	11.48	24.236	12.00
2452	59	10.91	24.880	11.40
2483	31	10.33	25.200	10.80
Cycle 7				
2531	48	0	25.200	0
2539	8	4.38	25.235	4.57
2548	9	8.75	25.314	9.14
2627	79	10.71	26.160	11.19
2688	61	0	26.160	0
2743	55	10.71	26.749	11.19
2817	74	10.39	27.518	10.86

Table 4-4. Power History for Bundle CZ346 from Cooper BWR

Elapsed Time, days	Time Interval, days	Power Density, MW/MTU	Cumulative Burnup, MWd/MTU	Average LHGR, kW/m
2822	5	0	27.518	0
2853	31	9.84	27.823	10.28
2879	26	8.75	28.050	9.14

Reference 5.6

Table 4-5. Composition of Zircaloy-4

Material	Weight Percent
O	0.12
Cr	0.10
Fe	0.20
Sn	1.40
Zr	98.18
Density = 6.56 g/cm ³	

Reference 5.8

Table 4-6. Nuclides Updated in SAS2H

⁸³ Kr	⁸⁵ Kr	⁸⁹ Y	⁹⁰ Sr	⁹⁵ Mo	⁹³ Zr
⁹⁴ Zr	⁹⁴ Nb	⁹⁵ Zr	⁹⁹ Tc	¹⁰¹ Ru	¹⁰³ Rh
¹⁰⁵ Rh	¹⁰⁶ Ru	¹⁰⁵ Pd	¹⁰⁸ Pd	¹⁰⁹ Ag	¹²⁴ Sb
¹³¹ Xe	¹³² Xe	¹³⁴ Cs	¹³⁵ Xe	¹³⁵ Cs	¹³⁶ Xe
¹³⁶ Ba	¹³⁷ Cs	¹³⁹ La	¹⁴¹ Pr	¹⁴³ Pr	¹⁴³ Nd
¹⁴⁴ Ce	¹⁴⁵ Nd	¹⁴⁷ Nd	¹⁴⁷ Pm	¹⁴⁷ Sm	¹⁴⁸ Pm
¹⁴⁹ Sm	¹⁵⁰ Sm	¹⁵¹ Sm	¹⁵² Sm	¹⁵³ Eu	¹⁵⁴ Eu
¹⁵⁵ Gd	¹⁵⁵ Eu				

Reference 5.9

Table 4-7. Measured Isotopic Concentrations (g/gUO₂)

Sample	ADD2966-B	ADD2966-K	ADD2966-T	ADD2974-B	ADD2974-J	ADD2974-U
Burnup, MWd/kgM	18.96	33.07	33.94	17.84	29.23	31.04
²³⁴ U	1.7E-4	1.35E-4	1.44E-4	1.74E-4	1.46E-4	1.54E-4
²³⁵ U	1.191E-2	5.34E-3	4.83E-3	1.30E-2	7.76E-3	6.28E-3
²³⁶ U	2.63E-3	3.53E-3	3.62E-3	2.48E-3	3.36E-3	3.48E-3
²³⁸ U	8.437E-1	8.346E-1	8.391E-1	8.545E-1	8.490E-1	8.455E-1
²³⁸ Pu	5.35E-5	1.743E-4	1.706E-4	5.21E-5	1.64E-4	1.389E-4
²³⁹ Pu	3.738E-3	3.579E-3	3.336E-3	4.056E-3	4.526E-3	3.668E-3
²⁴⁰ Pu	1.220E-3	2.216E-3	2.190E-3	1.184E-3	2.164E-3	2.082E-3
²⁴¹ Pu	3.403E-4	6.390E-4	6.201E-4	3.415E-4	6.649E-4	6.139E-4
²⁴² Pu	9.892E-5	4.407E-4	4.737E-4	8.742E-5	3.247E-4	3.823E-4

Reference 5.6

Table 4-8. Measure Isotopic Concentrations (Ci/gUO₂)

Sample	ADD2966-B	ADD2966-K	ADD2966-T	ADD2974-B	ADD2974-J	ADD2974-U
Burnup, MWd/kgM	18.96	33.07	33.94	17.84	29.23	31.04
⁹⁹ Tc	6.26E-6	1.03E-5	1.06E-5	6.17E-6	9.86E-6	1.00E-5
²³⁷ Np	1.11E-7	2.54E-7	2.46E-7	1.09E-7	2.35E-7	2.36E-7
²⁴¹ Am	5.18E-4	8.78E-4	8.38E-4	5.23E-4	9.46E-4	8.69E-4

Reference 5.6

4.2 Criteria

The design of the waste package will depend on waste package configuration criticality analyses performed using an acceptable disposal criticality analysis methodology. Criteria that relate to the development and design of repository and engineered barrier components are derived from the applicable requirements and planning documents. The Engineered Barrier Design Requirements Document (EBDRD, Reference 5.12) provides requirements for engineered barrier segment design. The Repository Design Requirements Document (RDRD, Reference 5.13) provides requirements for repository design. The Controlled Design Assumptions Document (Reference 5.14) provides guidance for requirements listed in the EBDRD and RDRD which have unqualified or unconfirmed data associated with the requirement.

This analysis supports the disposal criticality analysis methodology by providing input, in the form of fuel depletion results, to benchmark calculations which address the prediction of both spent fuel isotopic compositions and their associated reactivity. These benchmark calculations will contribute to the determination of bias values in the method of critical multiplication factor calculation that is implemented by the analytic tools to be used in the disposal criticality methodology. The requirements for utilizing the bias in the method of calculation of the critical multiplication factor for disposal configurations containing spent nuclear fuel are located in Section 3.2.2.5 of the RDRD and Section 3.2.2.6 of the EBRD. This analysis does not satisfy these requirements, but the results from this analysis will be used as input to subsequent analyses which will satisfy these requirements.

4.3 Assumptions

- 4.3.1 The average fuel temperature is unknown and assumed to be 840 K. The value for average fuel temperature is taken from an example depletion case on p. S2.6.12 of Reference 5.10. The basis for this assumption is that this is a representative value for the average fuel temperature in a BWR operating under normal conditions. Sensitivity analyses of fuel temperature changes are documented in Section 7.7 of this analysis. This assumption is used in Section 7.2.
- 4.3.2 The cladding temperature is unknown and assumed to be of 620 K. The value for the cladding temperature is taken from an example depletion case on p. S2.6.12 of Reference 5.10. The basis for this assumption is that this is a representative value for the cladding temperature in a BWR operating under normal conditions. Furthermore, it is expected that the cladding temperature will not significantly effect the resulting isotopic concentrations, since the composition contains no nuclides that are strong neutron absorbers. This assumption is used in Section 7.2.
- 4.3.3 The moderator temperature is unknown and assumed to be 557 K. The value for the moderator temperature in an example depletion case on p. S2.6.12 of Reference 5.10 is 558 K. The basis for this assumption is that this is a representative value for the cladding temperature in a BWR operating under normal conditions. This assumption is used in Section 7.2.
- 4.3.4 The moderator density profile is unknown and is assumed to be an inverse exponential function with an entrance density of 0.862 g/cm^3 and plateau density of 0.240 g/cm^3 . The basis for this assumption is that this is a representative function for the moderator density profile in a BWR operating under normal conditions. Additional supporting data for the moderator density profile is to be determined and will be included in revision(s) to this analysis. This assumption is used in Section 7.2.

4.4 Codes and Standards

There are no applicable codes or standards for this design analysis.

5. References

- 5.1 *Yucca Mountain Site Characterization Project Q-List*, YMP/90-55Q REV 04, Yucca Mountain Site Characterization Project.
- 5.2 *QAP-2-0 Activity Evaluations: ID #WP-20, Perform Criticality, Thermal, Structural, and Shielding Analyses*, Civilian Radioactive Waste Management System (CRWMS) Management and Operating Contractor (M&O), August 3, 1997.
- 5.3 *Quality Assurance Requirements and Description*, DOE/RW-0333P REV 07, U.S. Department of Energy (DOE) Office of Civilian Radioactive Waste Management (OCRWM).
- 5.4 *Nuclides and Isotopes*, General Electric Company, 14ed., 1989.
- 5.5 G. Audi and A. H. Wapstra, *Atomic Mass Adjustments: 'The 1995 Update to the Atomic Mass Evaluation'*, Nuclear Physics A595 Vol. 4, p. 409-480.
- 5.6 R. J. Guenther et. al., *Characterization of Spent Fuel Approved Testing Material - ATM-105*, PNL-5109-105, Pacific Northwest Laboratory, 1991.
- 5.7 *Core Design and Operating Data for Cycles 1 and 2 of Quad Cities 1*, EPRI NP-240, November 1976.
- 5.8 *Material Compositions and Number Densities for Neutronics Calculations*, Document Identifier Number (DI#): BBA000000-01717-0200-00002 REV 00, CRWMS M&O.
- 5.9 *SCALE-4 Analysis of Pressurized Water Reactor Critical Configurations: Volume 2- Sequoyah Unit 2 Cycle 3*, ORNL/TM-12294/V2, March 1995.
- 5.10 *SCALE 4.3, A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation for Workstations and Personal Computers*, NUREG/CR-0200 REV 05, ORNL/NUREG/CSD-2/R5, Volumes 1-3, Oak Ridge National Laboratory.
- 5.11 *Software Qualification Report for the SCALE Modular Code System*, DI#: 30011-2002 REV 01, CRWMS M&O.
- 5.12 *Engineered Barrier Design Requirements Document*, YMP/CM-0024, REV 00, ICN 01, DOE OCRWM.

- 5.13 *Repository Design Requirements Document*, YMP/CM-0023, REV 00, ICN 01, DOE OCRWM.
- 5.14 *Controlled Design Assumptions Document*, DI#: B00000000-01717-4600-00032 REV 04, ICN 01, CRWMS M&O.

6. Use of Computer Software

- A. Reference 5.10 describes the SAS2H module of SCALE 4.3 that is used with the 44GROUPNDF5 cross section library to calculate the isotopic concentrations for the specified burnup and cooling time. The computer code's spatially independent point depletion model is appropriate for comparison with pellet sample measurements, and is used within the range of validation, as described in Reference 5.11, in accordance with the QAP-SI series procedures. SCALE is obtained from the Software Configuration Management in accordance with appropriate procedures. SCALE's CSCI number is 30011 V4.3 and is installed on the WPDD HP 9000, 700 Workstation with CRWMS M&O tag number 110433.
- B. *Lotus 1-2-3 Release 5* for Windows 95 is an Acquired Software spreadsheet program as defined in QAP-SI-0. User defined formulas and/or algorithms, inputs and results, are documented in the appropriate sections.

7. Design Analysis

The SAS2H module of SCALE 4.3 is used to perform one-dimensional (1-D) neutron transport and point depletion analyses on the Cooper samples using the preferred 44GROUPNDF5 cross-section library. To properly model the neutron flux spectrum and the nuclide composition changes, it is necessary to define the compositions, temperatures, and geometry of the fuel assembly. This is accomplished with the use of data blocks in which similar parameters are grouped together.

7.1 SCALE Input Data Blocks 1, 2, and 3

Data blocks 1 through 3 define the SCALE module to be used, the title of the input file, the cross section library to be used, and the lattice type to be modeled. The module used is SAS2H and the cross sectional library is 44GROUPNDF5, abbreviated as 44GROUP. The 44GROUP cross section library is recommended by Oak Ridge National Laboratory. Since SAS2H is only to be used for isotopic depletion/generation, the 'parm=skipshipdata' option is used so that a shipping cask shielding analysis is not performed. The title is arbitrary and should contain information that is sample specific, while the lattice type is "latticecell" to reflect the array characteristic of the assembly.

7.2 SCALE Input Data Block 4

Data block 4 defines the material compositions present in the assembly. A unique mixture number is assigned to each composition, and follows the form of mixture 1 for fuel, mixture 2 for cladding and mixture 3 for moderator.

The fuel mixture is UO_2 with a density and isotopic weight percentages of the pellet on which the measurements are performed. This is to ensure that the proper amount of ^{235}U is present in the fuel region. The density is approximated as the pellet immersion density. Also, since only the ^{235}U enrichment is known, the enrichment of ^{234}U and ^{236}U are approximated by the following relationship with results for each rod type presented in Table 7-1: $\text{wt}\% ^{234}\text{U} = 0.0046 * \text{wt}\% ^{235}\text{U}$ and $\text{wt}\% ^{236}\text{U} = 0.0089 \text{ wt}\% ^{235}\text{U}$. The fuel temperature is unknown and assumed to be 840 K. The basis for this assumption is that this is a typical value for the average fuel temperature in a BWR. Isotopes which are selected as needing their cross sections updated during the depletion analysis are included in the fuel mixture. A standard list of trace fuel elements is given in Table 4-6 and defined in the fuel mixture to have a concentration of 10^{-20} atoms/barn-cm.

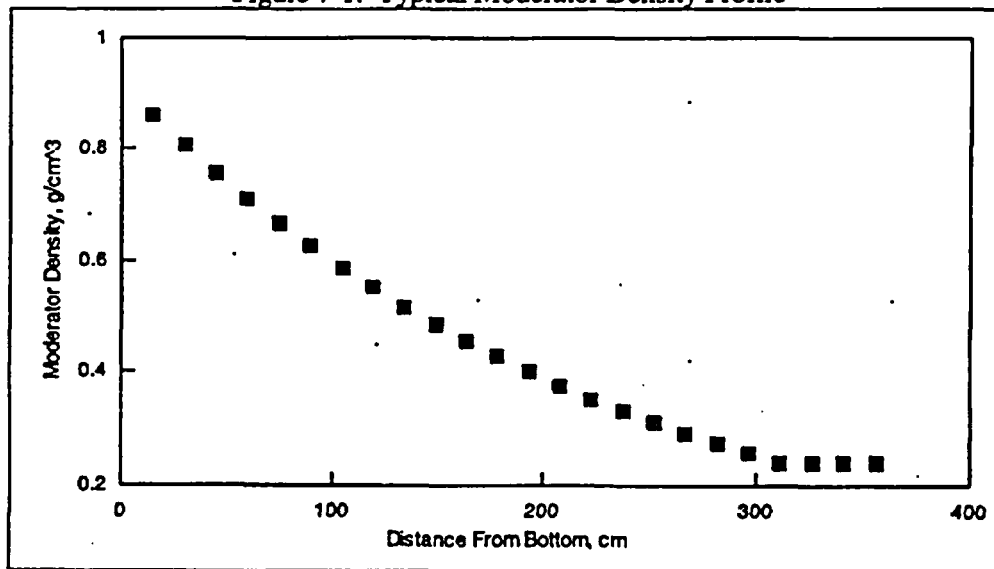
The cladding material is Zircaloy-2. The cladding temperature could not be obtained, therefore, a cladding temperature of 620 K is assumed for each sample. This value is consistent with the expectation that the cladding temperature is closer to the moderator temperature than the fuel temperature. Furthermore, it is expected that the cladding temperature will not significantly effect the resulting isotopic concentrations.

Table 7-1. Enrichment of Fuel Rods

Rod Type	wt% 236U	wt% 235U	wt% 234U	wt% 238U
1	0.013	2.93	0.026	97.031
2	0.009	1.94	0.017	98.034
3	0.008	1.69	0.015	98.287
4	0.006	1.33	0.011	98.663
5	0.013	2.93	0.026	97.031
6	0.013	2.93	0.026	97.031
7	0.009	1.94	0.017	98.034

The moderator temperature and density are unknown. Therefore, a moderator temperature of 557 K will be assumed. The basis for this assumption is that this is a typical value for the average moderator temperature in a BWR. The BWR moderator density profile used in this analysis is assumed to be an inverse exponential function with an average entrance density of 0.862 g/cm³ and plateau density of 0.240 g/cm³. Figure 7-1 shows a typical moderator density profile for a BWR.

Figure 7-1. Typical Moderator Density Profile



Several other material compositions must be specified. The material for the air between the fuel rod and cladding is nitrogen at 5×10^{-5} atoms/barn-cm, and the material for the channel is Zircaloy-4. The temperature for these materials is the same as the moderator temperature and the mixture numbers are 4 and 5, respectively. The average Gadolinium rod mixture is specified as mixture 6

and is an average of all 5 Gd rods. To obtain the average Gadolinium rod composition, the weight percentages for both Gd and ^{235}U are averaged by the number of rods. The resulting weight percents are 3.4 wt% Gd and 2.732 wt% ^{235}U ; resulting in 0.024 wt% ^{234}U , 0.013 wt% ^{236}U and 97.231 wt% ^{238}U from the method described previously. The moderator between assemblies does not behave in the same manner as the moderator within the assembly. Between assembly moderator must be defined as mixture 7 and has a density and temperature of the inlet conditions.

The channel material of Zircaloy-4 is not contained within the Standard Composition Library in SCALE 4.3 and must be defined as an arbitrary material. The channel is defined with a density and isotopic weight percentages from Table 4-5 and temperature given in Table 4-2.

7.3 SCALE Input Data Blocks 5 Through 7

The unit fuel rod cell geometry is defined in data block 5. The 'squarepitch' designation for the type of lattice is appropriate since the fuel assembly consists of a square array of fuel rods. Fuel rod, cladding and pitch dimensions are given in Table 4-2 with the mixture number for each composition defined in Section 7.2. The gap mixture is defined as 0.

Data block 6 allows the user to specify such parameters as the spatial mesh, angular quadrature and the convergence criteria. It is determined that the default values are sufficient and such options are not used in this design model.

In data block 7 the user defines general assembly data and determines the level of detail in which the assembly is to be modeled. The number of fuel rods per assembly is given in Table 4-2 and the length is calculated so that an assembly contains 1 Metric Ton of Uranium Dioxide (MTUO_2), using the following equation:

$$\text{Length} = \frac{1}{\frac{\pi}{4}(\text{POD})^2(\text{PDen})(\text{NFR})} \cdot \frac{10^6 \text{gUO}_2}{1 \text{MTUO}_2} \quad \text{Equation 7-1}$$

Where:

- Length = Length Required for an Assembly to Contain 1 MTUO_2 (cm)
- POD = Fuel Pellet Diameter (cm)
- PDen = Fuel Pellet Density (gUO_2/cm^3)
- NFR = Number of Fuel Rods

Since, measured isotopic concentrations are presented in grams of isotope per gram UO_2 and SCALE presents concentrations in grams of isotope per assembly, it is possible to alter the length so that the assembly contains 1 MTUO_2 . This is possible since the 1-D transport calculation is axially independent, consequently the length of the assembly does not impact the neutron flux spectrum nor the nuclide cross sections. The resulting calculated length for the Cooper assembly is 1719.74 cm.

Each assembly was irradiated for five cycles, which are divided into a total of 17 intervals so that

all periods of downtime may be modeled. It is determined that approximately 80 days per cross section library is sufficient to accurately model the change in nuclide cross sections with increasing burnup, without over-burdening the SAS2H code. Therefore, the number of libraries per cycle are specified as two. To obtain the concentrations of all interested nuclides, a print level of 5 is chosen, while an input level of 2 is defined so that a Path B model may be utilized. The number of light elements is zero, while the number of zones is eight which is determined by the Path B model described in Section 7.4.

7.4 SCALE Input Data Block 8

It should be noted that control blade insertion information could not be obtained for the pertinent cycles, even though such information is important in the modeling of BWR assemblies. Calculated concentrations obtained from a BWR model without control blade insertion information are not expected to agree closely with corresponding measurements.

The Path B model for Cooper is a centralized average Gadolinium rod unit cell surrounded by an homogenized fuel and moderator mixture that conserves the fuel to moderator volume ratio. Further surrounding the homogenized fuel and moderator mixture are the moderator between the fuel cells and channel, the channel, and the moderator between assemblies. The equation below is used to determine the number of fuel unit cells that surround the central guide tube. All of the following equations used to calculate the Path B model dimensions are derived. The results of the fuel-unit-cell calculations are presented in Table 7-2, and the resulting Path B model dimensions are presented in Table 7-3.

$$x = \frac{\left(\frac{F}{M}\right)(CUCMV)}{\left(FV\right) - \left(\frac{F}{M}\right)(MV)} \quad \text{Equation 7-2}$$

$$\frac{F}{M} = \frac{(NFR)\left(\frac{\pi}{4}\right)(POD)^2}{(NFR)\left[RP^2 - \left(\frac{\pi}{4}\right)(COD)^2\right] + (NGdR)\left[RP^2 - \left(\frac{\pi}{4}\right)(COD)^2\right]} \quad \text{Equation 7-3}$$

$$CUCMV = RP^2 - \left(\frac{\pi}{4}\right)(COD)^2 \quad \text{Equation 7-4}$$

$$FV = \left(\frac{\pi}{4}\right)(POD)^2 \quad \text{Equation 7-5}$$

$$MV = RP^2 - \left(\frac{\pi}{4}\right)(COD)^2 \quad \text{Equation 7-6}$$

Where:

- x = Number of Unit Fuel Cells
- F/M = Fuel to Moderator Volume Ratio
- NFR = Number of Fuel Rods
- POD = Fuel Pellet Outer Diameter
- RP = Rod Pitch
- COD = Cladding Outer Diameter
- NGdR = Number of Gadolinium Rods
- CUCMV = Central Unit Cell Moderator Volume
- FV = Fuel Volume of Fuel Unit Cell
- MV = Moderator Volume of Fuel Unit Cell

Once the number of fuel cells per central Gd rod is determined the geometry of the Path B model may be calculated. Since the Gd rod is centralized, the dimensions of the first three zones are the same as the Gd rod pellet radius, cladding inside radius and cladding outside radius.

The radius for the moderator surrounding the Gd rod, but still within the Gd rod unit cell, is calculated with the following equation:

$$R_s = \sqrt{\left(\frac{1}{\pi}\right)RP^2} \quad \text{Equation 7-7}$$

Where:

- R_s = Radius of Moderator Surrounding Gd Rod

The area of an annular region is calculated by the difference between the outer circular area and the inner circular area. Equation 7-8 is the basis for the Equations 7-9 and 7-10 which determine the radii of the homogenized fuel zone and the outer moderator zone.

$$ARA = \pi(ORAR^2 - IRAR^2) \quad \text{Equation 7-8}$$

Where:

- ARA = Annular Region Area
- ORAR = Outer Radius of Annular Region
- IRAR = Inner Radius of Annular Region

The area of the homogenized fuel zone surrounding the Gd rod unit cell is equal to the number of fuel unit cells surrounding the Gd rod multiplied by the area of a fuel unit cell. Consequently, the radius of the homogenized fuel zone is computed with the following equation:

$$R_3 = \sqrt{\left(\frac{x}{\pi}\right)RP^2 + R_4^2} \quad \text{Equation 7-9}$$

Where:

- R_3 = Radius of Homogenized Fuel and Moderator Zone

The mixture number of the homogenized fuel and moderator mixture must be specified as 500. The code then determines the composition of the region using cell averages or homogenized densities of the fuel-pin-cell.

The area of the moderator between the unit cells and the channel is determined by calculating the total moderator volume and multiplying by the fraction of unit cells surrounding the Gd rod in the Path B model. The volume is calculated by determining the distance from the unit cells and the channel using the following equation:

$$R_6 = \sqrt{\frac{(x+1)}{\pi \cdot N_{Cell}} \cdot 4 \left[(N_{CpR} \cdot RP + CC_{sp} - \frac{RP-POD}{2}) \cdot (CC_{sp} - \frac{RP-POD}{2}) \right] + R_5^2} \quad \text{Equation 7-10}$$

Where:

- R_6 = Radius of Moderator Between Unit Cell and Channel
- NCell = Number of Cells in Assembly
- N_{CpR} = Number of Cells per Row
- CC_{sp} = Cell to Channel Spacing

The area of the channel is calculated from the total channel volume and multiplying by the fraction of unit cells surrounding the Gd rod in the Path B model. The total channel volume of the assembly is calculated by the following equation:

$$R_7 = \sqrt{\frac{(x+1)}{\pi \cdot N_{Cell}} \cdot [4(CHOD - CH_{thick}) \cdot (CH_{thick})] + R_6^2} \quad \text{Equation 7-11}$$

Where:

- R₇ = Radius of Channel
- CHOD = Channel Outer Dimension
- CH_{thick} = Channel Thickness

The area of the moderator between assemblies is calculated from the total moderator between assemblies volume and multiplying by the fraction of unit cells surrounding the Gd rod in the Path B model. The total volume of the moderator between assemblies is calculated by the following equation:

$$R_8 = \sqrt{\frac{(x+1)}{\pi \cdot N_{Cell}} \cdot [2 \cdot (CHOD + W_w) \cdot (N_w) + 2 \cdot (CHOD + N_w) \cdot (W_w)] + R_7^2} \quad \text{Equation 7-12}$$

Where:

- R₈ = Radius of Moderator Between Assemblies
- W_w = Wide-Wide Half Dimension
- N_w = Narrow-Narrow Half Dimension

Table 7-2. Calculation of Fuel Unit Cell per Guide Tube Unit Cell

F/M	CUCMV, cm ²	FV, cm ²	MV, cm ²	x
0.5461	1.8908	1.1499	1.8908	8.8

Table 7-3. Path B Model Dimensions

	Radius, cm	Composition
R ₁	0.6050	Average Gd Rod
R ₂	0.6210	Air
R ₃	0.7150	Cladding
R ₄	1.0550	Moderator
R ₅	3.3028	Homogenized Fuel and Moderator
R ₆	3.3179	Moderator
R ₇	3.4223	Channel
R ₈	3.7883	Moderator

7.5 SCALE Input Data Blocks 9 Through 16

Data block 9 is used to describe the power history of the reactor. The specific power, fuel irradiation period, the length of downtime, the fraction of boron and moderator density, and the temperature during the cycle may all be defined. The specific power is in units of MW/MTUO₂, while the irradiation period and length of downtime are both defined in days. The specific power is determined from Table 4-4 by developing intervals that allow modeling of the downtime during and after each cycle. The power during the interval is determined by the cumulative burnup of that interval and the length of the interval. Tables 7-4 and 7-5 contain values for the specific powers and the interval lengths. The moderator density fractions and the individual cycle temperature options are not used in modeling the Cooper assemblies because data obtained were not in sufficient detail to determine cycle specific values.

Table 7-4. Approximated Power History for Samples from Rod ADD2966

Cycle	Time Interval, days		Specific Power, MW/MTUO ₂		
	Uptime	Downtime	Axial Level B	Axial Level K	Axial Level T
One	19	8	9.313	16.243	16.671
	130	17	11.086	19.336	19.845
	41	10	13.919	24.278	24.917
	226	35	10.863	18.947	19.445
	39	7	11.941	20.827	21.375
	22	12	13.549	23.632	24.254
	108	19	12.716	22.179	22.762
	114	59	13.177	22.983	23.587
Two	79	8	10.795	18.829	19.324
	64	5	11.941	20.827	21.375
	150	31	10.037	17.506	17.966
Three	164	799	10.099	17.615	18.078
Six	160	9	6.234	10.874	11.160
	148	48	6.465	11.276	11.573
Seven	96	61	5.958	10.391	10.664
	129	5	6.272	10.939	11.227
	57	See Table 4-1	5.567	9.709	9.965

Table 7-5. Approximated Power History for Samples from Rod ADD2974

Cycle	Time Interval, days		Specific Power, MW/MTUO ₂		
	Uptime	Downtime	Axial Level B	Axial Level J	Axial Level U
One	19	8	8.763	14.357	15.246
	130	17	10.431	17.091	18.149
	41	10	13.097	21.459	22.788
	226	35	10.221	16.747	17.784
	39	7	11.235	18.409	19.549
	22	12	12.749	20.888	22.182
	108	19	11.965	19.603	20.817
	114	59	12.398	20.314	21.572
Two	79	8	10.157	16.642	17.673
	64	5	11.235	18.409	19.549
	150	31	9.444	15.473	16.431
Three	164	799	9.503	15.570	16.534
Six	160	9	5.866	9.611	10.206
	148	48	6.083	9.967	10.584
Seven	96	61	5.606	9.184	9.753
	129	5	5.901	9.669	10.268
	57	See Table 4-1	5.238	8.582	9.113

Light elements and their effective weight, in kg per assembly, are entered in data block 10. However, information concerning the light elements could not be obtained and this option is not used.

Data blocks 11 through 15 describe parameters used in the radial shielding analysis of a shipping cask and are not necessary in performing the depletion analysis. Data block 16 denotes the end of the SCALE input.

7.6 Comparison of Calculated and Measured Concentrations

Comparisons of corresponding calculated and measured concentrations are performed on a percent difference basis. The difference between the measured and the calculated value is divided by the measured value to determine the accuracy of the SAS2H calculation. A positive percent difference represents an over-prediction by the code, while a negative percent difference represents an under-prediction by the code.

Measured concentrations presented in Table 4-7 have units of g of isotope per g of UO_2 , while calculated concentrations presented in Table 7-6 have units of g of isotope per Metric Ton of UO_2 . Therefore, the measured concentrations must be multiplied by 10^6 g UO_2 /MT UO_2 to obtain similar units.

Measured concentrations are presented in Table 4-8 with units of Curies per g UO_2 . The activity of a particular isotope per gram UO_2 is converted to grams of that isotope per gram UO_2 using the half-life and molar mass presented in Section 4.1 and the following equation:

$$\left(\frac{Y_g}{gUO_2}\right) = \left(\frac{XCi}{gUO_2}\right) \left(\frac{3.7 \times 10^{10} Bq}{Ci}\right) \left(\frac{1}{\lambda}\right) \left(\frac{3.16 \times 10^7 s}{1yr}\right) \left(\frac{1mole}{6.02 \times 10^{23} atoms}\right) \left(\frac{Mass}{1mole}\right) \quad \text{Equation 7-13}$$

Where:

Y = Measured Value Used in Comparison (g isotope/g UO_2)

X = Measured Value from SAS2H (Ci isotope/g UO_2)

$$\lambda = \frac{\ln(2)}{T_{1/2}} \quad (yr^{-1})$$

$T_{1/2}$ = Half-life of Isotope (yr)

Mass = Molar Mass of Isotope

Percent differences for the actinides and fission products are presented in Table 7-6.

In an attempt to determine the impact of the assumptions from Section 4.3 on the calculated isotopic concentrations, a sensitivity analysis is performed on the fuel temperature and moderator density. It is determined that the effect of the moderator temperature is not significant in the absorption of neutrons and the effect of up-scattering is not significant over the expected range of moderator temperatures. Also it is determined that the cladding temperature has no significant effect because it does not contribute significantly to either neutron absorption or scattering. Two samples representing low and high burnups, ADD2966-B and ADD2974-B, are used to observe the changes in isotopic concentrations for both: 1) a 100 K increase in fuel temperature, and 2) a 10 percent increase in moderator density for the sample taken near the bottom of the assembly and a 50 percent increase in moderator density for the sample taken near the top of the assembly. The results are reported in Tables 7-8 and 7-9.

7.7 Results

SAS2H predicted isotopic concentrations are presented in Table 7-6. The calculated concentrations are obtained through the methodology described in Sections 7.1 through 7.5, and with the input parameters defined in Section 4.1. Calculated concentrations are compared with measured concentrations as describe in Section 7.6 to determine the accuracy of the SAS2H module. Results of the comparison, in the form of percent differences, are presented in Table 7-6. Also the results of the sensitivity analysis are reported in Tables 7-8 and 7-9.

Table 7-6. Calculated concentrations (g/MTUO₂)

Sample	ADD2966-B	ADD2966-K	ADD2966-T	ADD2974-B	ADD2974-J	ADD2974-U
Burnup, MWd/kgM	18.96	33.07	33.94	17.84	29.23	31.04
⁹⁹ Tc	4.22E2	7.02E2	7.22E2	3.99E2	6.24E2	6.71E2
²³⁴ U	1.67E2	1.39E2	1.38E2	1.70E2	1.44E2	1.45E2
²³⁵ U	1.20E4	5.22E3	4.50E3	1.25E4	7.22E3	5.32E3
²³⁸ U	2.61E3	3.46E3	3.51E3	2.52E3	3.29E3	3.40E3
²³⁹ U	8.42E5	8.34E5	8.34E5	8.43E5	8.35E5	8.37E5
²³⁷ Np	2.00E2	3.44E2	3.32E2	1.85E2	3.29E2	2.93E2
²³⁹ Pu	5.93E1	1.60E2	1.54E2	5.15E1	1.44E2	1.25E2
²⁴⁰ Pu	4.41E3	3.95E3	3.57E3	4.32E3	4.61E3	3.47E3
²⁴¹ Pu	1.30E3	2.10E3	2.08E3	1.21E3	1.98E3	1.92E3
²⁴² Pu	4.28E2	6.87E2	6.44E2	3.93E2	6.93E2	5.82E2
²⁴³ Pu	1.22E2	4.60E2	4.91E2	1.05E2	3.42E2	3.98E2
²⁴¹ Am	2.08E2	3.06E2	2.83E2	1.92E2	3.19E2	2.60E2

Table 7-7. Percent Difference Between Measured and Calculated $[(C/M-1)*100]$

Sample	ADD2966-B	ADD2966-K	ADD2966-T	ADD2974-B	ADD2974-J	ADD2974-U
Burnup, MWd/kgM	18.96	33.07	33.94	17.84	29.23	31.04
⁹⁹ Tc	14.18	15.44	15.37	9.53	7.19	13.65
²³⁴ U	-1.76	2.96	-4.17	-2.30	-1.37	-5.84
²³⁵ U	0.76	-2.25	-6.83	-3.85	-6.96	-15.29
²³⁶ U	-0.76	-1.98	-3.04	1.61	-2.08	-2.30
²³⁸ U	-0.20	-0.07	-0.61	-1.35	-1.65	-1.01
²³⁷ Np	26.76	-4.72	-5.05	19.41	-1.51	-12.66
²³⁸ Pu	10.84	-8.20	-9.73	-1.15	-12.20	-10.01
²³⁹ Pu	17.98	10.37	7.01	6.51	1.86	-5.40
²⁴⁰ Pu	6.56	-5.23	-5.02	2.20	-8.50	-7.78
²⁴¹ Pu	25.77	7.51	3.85	15.08	4.23	-5.20
²⁴² Pu	23.33	4.38	3.65	20.11	5.33	4.11
²⁴¹ Am	37.39	19.25	15.55	25.61	15.38	2.37

Table 7-8. Sensitivity Analyses for Sample ADD2966-T

Case	Modeled Conditions	Fuel Temperature Increase of 100 K		Moderator Density Increase of 10%	
Isotope	Calculated Concentration, g/MTU	Calculated Concentration, g/MTU	% Change in Calculated	Calculated Concentration, g/MTU	% Change in Calculated
⁹⁹ Tc	7.22E2	7.22E2	0.00	7.24E2	0.28
²³⁴ U	1.38E2	1.38E2	0.00	1.38E2	0.00
²³⁵ U	4.50E3	4.54E3	0.89	4.31E3	-4.22
²³⁶ U	3.51E3	3.50E3	-0.28	3.52E3	0.28
²³⁸ U	8.34E5	8.34E5	0.00	8.35E5	0.12
²³⁷ Np	3.32E2	3.34E2	0.60	3.23E2	-2.71
²³⁸ Pu	1.54E2	1.55E2	0.65	1.48E2	-3.90
²³⁹ Pu	3.57E3	3.61E3	1.12	3.42E3	-4.20
²⁴⁰ Pu	2.08E3	2.08E3	0.00	2.06E3	-0.96
²⁴¹ Pu	6.44E2	6.50E2	0.93	6.21E2	-3.57
²⁴² Pu	4.91E2	4.92E2	0.20	4.92E2	0.20
²⁴¹ Am	2.83E2	2.86E2	1.06	2.71E2	-4.24

Table 7-9. Sensitivity Analyses for Sample ADD2974-B

Case	Modeled Conditions	Fuel Temperature Increase of 100 K		Moderator Density Increase of 50 %		
		Calculated Concentration, g/MTU	Calculated Concentration, g/MTU	% Change in Calculated	Calculated Concentration, g/MTU	% Change in Calculated
⁹⁹ Tc		3.99E2	3.99E2	0.00	4.02E2	0.75
²³⁴ U		1.70E2	1.70E2	0.00	1.72E2	1.18
²³⁵ U		1.25E4	1.26E4	0.80	1.22E4	-2.40
²³⁸ U		2.52E3	2.51E3	-0.40	2.51E3	-0.40
²³⁹ U		8.43E5	8.43E5	0.00	8.44E5	0.12
²³⁷ Np		1.85E2	1.86E2	0.54	1.69E2	-8.65
²³⁸ Pu		5.15E1	5.17E1	0.39	4.53E1	-12.04
²³⁹ Pu		4.32E3	4.36E3	0.93	3.93E3	-9.03
²⁴⁰ Pu		1.21E3	1.21E3	0.00	1.16E3	-4.13
²⁴¹ Pu		3.93E2	3.97E2	1.02	3.64E2	-7.38
²⁴² Pu		1.05E2	1.05E2	0.00	1.03E2	-1.90
²⁴¹ Am		1.92E2	1.94E2	1.04	1.77E2	-7.81

8. Conclusions

The accuracy with which the SAS2H module is able to predict isotopic concentrations is indicated by the percent differences presented in Table 7-7. Inspection of such results reveals that the code has a tendency to over-predict ^{99}Tc , ^{242}Pu and ^{241}Am while it tends to under-predict ^{238}U .

An analysis of the sensitivity of isotopic concentrations in relation to the fuel temperature reveals that for a 100 K increase in the fuel temperature, most of the plutonium isotopic concentrations increase by approximately 1%. For the sample at relatively low burnup, ADD2974-B, the isotopes of ^{235}U , ^{237}Np , ^{238}Pu , ^{239}Pu , ^{241}Pu and ^{241}Am increase by 1.04% or less; ^{236}U decreases by 0.4% and the remaining isotopes are unchanged. For the sample at relatively high burnup, ADD2966-T, the isotopes of ^{235}U , ^{237}Np , ^{238}Pu , ^{239}Pu , ^{241}Pu , ^{242}Pu and ^{241}Am all increase by 1.12% or less; ^{236}U decreases by 0.28% and the remaining isotopes remain unchanged. Since the actual fuel temperature is not expected to deviate more than 200 K from the temperature assumed, the assumption of a fuel temperature of 840 K does not significantly effect the calculated isotopic concentrations.

An analysis of the sensitivity of isotopic concentrations in relation to the moderator density reveals that for a 10 percent increase in the moderator density of sample ADD2966-T and a 50 percent change in sample ADD2974-B, the isotopic concentrations change significantly. For the sample at relatively low burnup, ADD2974-B, the isotopes of ^{235}U , ^{237}Np , ^{238}Pu , ^{239}Pu , ^{240}Pu , ^{241}Pu and ^{241}Am decrease between 2.4 to 12.04%, and the remaining isotopes change by less than 2%. For the sample at relatively high burnup, ADD2966-T, the isotopes of ^{235}U , ^{237}Np , ^{238}Pu , ^{239}Pu , ^{241}Pu and ^{241}Am decrease between 2.72 to 4.24% or less, and the remaining isotopes change by less than 2%. The moderator density is not expected to deviate more than 10 percent from the assumed value near the bottom of the assembly, or not more than 50 percent from the assumed value near the top of the assembly. Therefore, it may be concluded that an incorrect assumption of the moderator density would significantly effect the calculated isotopic concentrations.

The SAS2H code normally predicts isotopic concentrations as a radial assembly average; however, measurements are performed on individual pellet samples. Therefore, local pellet conditions are modeled as closely as possible in this analysis so that a more realistic pellet composition can be determined. However, it was necessary to approximate the fuel temperature and the moderator temperature as typical assembly average values. Furthermore, approximations made to obtain local pellet conditions will influence the calculated isotopic concentrations.

No final conclusions can be drawn from inspection of the measured to calculated ratios presented in this analysis. Although the assumptions for the fuel temperature and the moderator density do effect the resulting isotopic concentrations, the effect is not significant enough to account for all variation between the measured and calculated concentrations. More detailed operating data, especially data concerning control blade insertion, would be expected to improve the accuracy of the calculated concentrations in relation to the corresponding measurements. It is expected that future revision(s) to this analysis will incorporate more detailed operating data thereby providing more conclusive results.

9. Attachments

Attachment I includes ten pages and contains the input files used in the modeling of the Cooper samples. A description of the parameters contained within the input files is found in Sections 7.1 through 7.5.

Included in Attachment II is an extraction from each of the output files, containing the following information:

- echo of the SAS2H input deck,
- time/date stamp for when the SAS2H depletion calculation was performed,
- the output extraction of information pertinent to the Radiochemical Assay evaluations from the final ORIGEN calculation of the SAS2H depletion calculation.

coop2966b.input

wsas2h parm=skipshipdata

Cooper BWR Sample ADD2966-B, Height 55.107 cm from top, Aug 97

:

: mixtures of fuel-pin-unit-cell:

44group latticell

uo2 1 den=10.32 1 840

92234 0.026 92235 2.93 92236 0.013 92238 97.031 end

kr-83 1 0 1-20 840 end

kr-85 1 0 1-20 840 end

y-89 1 0 1-20 840 end

sr-90 1 0 1-20 840 end

zr-93 1 0 1-20 840 end

zr-94 1 0 1-20 840 end

zr-95 1 0 1-20 840 end

nb-94 1 0 1-20 840 end

mo-95 1 0 1-20 840 end

tc-99 1 0 1-20 840 end

ru-101 1 0 1-20 840 end

ru-106 1 0 1-20 840 end

rh-103 1 0 1-20 840 end

rh-105 1 0 1-20 840 end

pd-105 1 0 1-20 840 end

pd-108 1 0 1-20 840 end

ag-109 1 0 1-20 840 end

sb-124 1 0 1-20 840 end

xe-131 1 0 1-20 840 end

xe-132 1 0 1-20 840 end

xe-135 1 0 1-20 840 end

xe-136 1 0 1-20 840 end

cs-134 1 0 1-20 840 end

cs-135 1 0 1-20 840 end

cs-137 1 0 1-20 840 end

ba-136 1 0 1-20 840 end

la-139 1 0 1-20 840 end

pr-141 1 0 1-20 840 end

pr-143 1 0 1-20 840 end

ce-144 1 0 1-20 840 end

nd-143 1 0 1-20 840 end

nd-145 1 0 1-20 840 end

nd-147 1 0 1-20 840 end

pm-147 1 0 1-20 840 end

pm-148 1 0 1-20 840 end

sm-147 1 0 1-20 840 end

sm-149 1 0 1-20 840 end

sm-150 1 0 1-20 840 end

sm-151 1 0 1-20 840 end

sm-152 1 0 1-20 840 end

eu-153 1 0 1-20 840 end

eu-154 1 0 1-20 840 end

eu-155 1 0 1-20 840 end

gd-155 1 0 1-20 840 end

zirc2 2 1 620 end

:

h2o 3 den=0.240 1 557 end

n 4 0 5-5 557 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 5 1.0 557 end

uo2 6 den=10.32 1 840

92234 0.024 92235 2.732 92236 0.013 92238 97.231 end

arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end

h2o 7 den=0.862 1 557 end

end comp

:

fuel-pin-cell geometry:

squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end

:

assembly and cycle parameters:

npin/asm=49 fuelght=1719.74 ncycles=17 nlib/cyc=2

printlevel=5 inplevel=2 numztotal=8 end

6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5

3.4223 7 3.7883

power=9.313 burn=19 down=8 end

power=11.086 burn=130 down=17 end

power=13.919 burn=41 down=10 end

power=10.863 burn=226 down=35 end

power=11.941 burn=39 down=7 end

power=13.549 burn=22 down=12 end

power=12.716 burn=108 down=19 end

power=13.177 burn=114 down=59 end

power=10.795 burn=79 down=8 end

power=11.941 burn=64 down=5 end

power=10.037 burn=150 down=31 end

power=10.099 burn=164 down=799 end

power=6.234 burn=160 down=9 end

power=6.465 burn=148 down=48 end

power=5.958 burn=96 down=61 end

power=6.272 burn=129 down=5 end

power=5.567 burn=57 down=1954.09 end

:

end

coop2966k.input

==sas2h parm=skipshipdata
Cooper BWR Sample ADD2966-K, Height 218.869 cm from top, Aug 97

mixtures of fuel-pin-unit-cell:

```

44group latticecell
uo2 1 den=10.32 1 840
92234 0.026 92235 2.93 92236 0.013 92238 97.031 end
kr-83 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
zr-93 1 0 1-20 840 end
zr-94 1 0 1-20 840 end
zr-95 1 0 1-20 840 end
nb-94 1 0 1-20 840 end
mo-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-106 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
ag-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
xe-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
cs-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sm-147 1 0 1-20 840 end
sm-149 1 0 1-20 840 end
sm-150 1 0 1-20 840 end
sm-151 1 0 1-20 840 end
sm-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
gd-155 1 0 1-20 840 end

zirc2 2 1 620 end

.
.
.
h2o 3 den=0.478 1 557 end
n 4 0 5-5 557 end
.
arbm-zirc4 6.56 5 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 5 1.0 557 end
.
uo2 6 den=10.32 1 840
92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end

h2o 7 den=0.862 1 557 end

```

end comp

fuel-pin-cell geometry:

squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end

assembly and cycle parameters:

```

npin/assm=49 fuelnght=1719.74 ncycles=17 nlib/cyc=2
printlevel=5 inplevel=2 numztotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5
3.4223 7 3.7883
power=16.243 burn=19 down=8 end
power=19.336 burn=130 down=17 end
power=24.278 burn=41 down=10 end
power=18.947 burn=226 down=35 end
power=20.827 burn=39 down=7 end
power=23.632 burn=22 down=12 end
power=22.179 burn=108 down=19 end
power=22.983 burn=114 down=59 end
power=18.829 burn=79 down=8 end
power=20.827 burn=64 down=5 end
power=17.506 burn=150 down=31 end
power=17.615 burn=164 down=799 end
power=10.874 burn=160 down=9 end
power=11.276 burn=148 down=48 end
power=10.391 burn=96 down=61 end
power=10.939 burn=129 down=5 end
power=9.709 burn=57 down=1954.09 end

```

end

coop2966t.input

```

=as2h perm=skipshipdata
Cooper BWR Sample ADD2966-T, Height 274.777 cm from top, Aug 97

```

```

mixtures of fuel-pin-unit-cell:

```

```

44group latticecell
uo2 1 den=10.32 1 840
  92234 0.026 92235 2.93 92236 0.013 92238 97.031 end
kr-83 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
zr-93 1 0 1-20 840 end
zr-94 1 0 1-20 840 end
zr-95 1 0 1-20 840 end
nb-94 1 0 1-20 840 end
mo-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-106 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
ag-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
xe-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
cs-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sm-147 1 0 1-20 840 end
sm-149 1 0 1-20 840 end
sm-150 1 0 1-20 840 end
sm-151 1 0 1-20 840 end
sm-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
gd-155 1 0 1-20 840 end

zirc2 2 1 620 end

.
.
.
h2o 3 den=0.607 1 557 end

n 4 0 5-5 557 end

.
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 5 1 0 557 end

.
uo2 6 den=10.32 1 840
  92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end

.
h2o 7 den=0.862 1 557 end

```

```

.....
end comp

```

```

.....
fuel-pin-cell geometry:

```

```

squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end

```

```

.....
assembly and cycle parameters:

```

```

npin/assm=49 fuelight=1719.74 ncycles=17 alib/cyc=2
printlevel=5 inlevel=2 numztotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5
3.4223 7 3.7883
power=16.671 burn=19 down=8 end
power=19.845 burn=130 down=17 end
power=24.917 burn=41 down=10 end
power=19.445 burn=226 down=35 end
power=21.375 burn=39 down=7 end
power=24.254 burn=22 down=12 end
power=22.762 burn=108 down=19 end
power=23.587 burn=114 down=59 end
power=19.324 burn=79 down=8 end
power=21.375 burn=64 down=5 end
power=17.966 burn=150 down=31 end
power=18.078 burn=164 down=799 end
power=11.160 burn=160 down=9 end
power=11.573 burn=148 down=48 end
power=10.664 burn=96 down=61 end
power=11.227 burn=129 down=5 end
power=9.965 burn=57 down=1954.09 end

```

```

.....
end

```

coop2974b.input

=sas2h parm=skipshipdata

Cooper BWR Sample ADD2974-B, Height 55.723 cm from top. Aug 97

* mixtures of fuel-pin-unit-cell:

44group laricecell

uo2 1 den=10.32 1 840

92234 0.026 92235 2.93 92236 0.013 92238 97.031 end

kr-83 1 0 1-20 840 end

kr-85 1 0 1-20 840 end

y-89 1 0 1-20 840 end

sr-90 1 0 1-20 840 end

zr-93 1 0 1-20 840 end

zr-94 1 0 1-20 840 end

zr-95 1 0 1-20 840 end

nb-94 1 0 1-20 840 end

mo-95 1 0 1-20 840 end

tc-99 1 0 1-20 840 end

ru-101 1 0 1-20 840 end

ru-106 1 0 1-20 840 end

rh-103 1 0 1-20 840 end

rh-105 1 0 1-20 840 end

pd-105 1 0 1-20 840 end

pd-108 1 0 1-20 840 end

ag-109 1 0 1-20 840 end

sb-124 1 0 1-20 840 end

xe-131 1 0 1-20 840 end

xe-132 1 0 1-20 840 end

xe-135 1 0 1-20 840 end

xe-136 1 0 1-20 840 end

cs-134 1 0 1-20 840 end

cs-135 1 0 1-20 840 end

cs-137 1 0 1-20 840 end

ba-136 1 0 1-20 840 end

la-139 1 0 1-20 840 end

pr-141 1 0 1-20 840 end

pr-143 1 0 1-20 840 end

ce-144 1 0 1-20 840 end

nd-143 1 0 1-20 840 end

nd-145 1 0 1-20 840 end

nd-147 1 0 1-20 840 end

pm-147 1 0 1-20 840 end

pm-148 1 0 1-20 840 end

sm-147 1 0 1-20 840 end

sm-149 1 0 1-20 840 end

sm-150 1 0 1-20 840 end

sm-151 1 0 1-20 840 end

sm-152 1 0 1-20 840 end

eu-153 1 0 1-20 840 end

eu-154 1 0 1-20 840 end

eu-155 1 0 1-20 840 end

gd-155 1 0 1-20 840 end

zirc2 2 1 620 end

h2o 3 den=0.240 1 557 end

n 4 0 5-5 557 end

arbm-zirc4 6.56 5 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 5 1.0 557 end

uo2 6 den=10.32 1 840

92234 0.024 92235 2.732 92236 0.013 92238 97.231 end

arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end

h2o 7 den=0.862 1 557 end

end comp

* fuel-pin-cell geometry:

squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end

* assembly and cycle parameters:

npin/assm=49 fuelnght=1719.74 ncycles=17 plib/cyc=2

printlevel=5 inplevel=2 numztotal=8 end

6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5

3.4223 7 3.7883

power=8.763 burn=19 down=8 end

power=10.431 burn=130 down=17 end

power=13.097 burn=41 down=10 end

power=10.221 burn=226 down=35 end

power=11.235 burn=39 down=7 end

power=12.749 burn=22 down=12 end

power=11.965 burn=108 down=19 end

power=12.398 burn=114 down=59 end

power=10.157 burn=79 down=8 end

power=11.235 burn=64 down=5 end

power=9.444 burn=150 down=31 end

power=9.503 burn=164 down=799 end

power=5.866 burn=160 down=9 end

power=6.083 burn=148 down=48 end

power=5.606 burn=96 down=61 end

power=5.901 burn=129 down=5 end

power=5.238 burn=57 down=1954.09 end

end

coop2974j.input

*sas2h parm=skipshipdata

Cooper BWR Sample ADD2974-J, Height 115.042 cm from top, Aug 97

* mixtures of fuel-pin-unit-cell:

```
44group latticecell
uo2 1 den=10.32 1 840
92234 0.026 92235 2.93 92236 0.013 92238 97.031 end
```

kr-83 1 0 1-20 840 end

kr-85 1 0 1-20 840 end

y-89 1 0 1-20 840 end

sr-90 1 0 1-20 840 end

zr-93 1 0 1-20 840 end

zr-94 1 0 1-20 840 end

zr-95 1 0 1-20 840 end

nb-94 1 0 1-20 840 end

mo-95 1 0 1-20 840 end

tc-99 1 0 1-20 840 end

ru-101 1 0 1-20 840 end

ru-106 1 0 1-20 840 end

rh-103 1 0 1-20 840 end

rh-105 1 0 1-20 840 end

pd-105 1 0 1-20 840 end

pd-108 1 0 1-20 840 end

ag-109 1 0 1-20 840 end

sb-124 1 0 1-20 840 end

xe-131 1 0 1-20 840 end

xe-132 1 0 1-20 840 end

xe-135 1 0 1-20 840 end

xe-136 1 0 1-20 840 end

cs-134 1 0 1-20 840 end

cs-135 1 0 1-20 840 end

cs-137 1 0 1-20 840 end

ba-136 1 0 1-20 840 end

la-139 1 0 1-20 840 end

pr-141 1 0 1-20 840 end

pr-143 1 0 1-20 840 end

ce-144 1 0 1-20 840 end

nd-143 1 0 1-20 840 end

nd-145 1 0 1-20 840 end

nd-147 1 0 1-20 840 end

pm-147 1 0 1-20 840 end

pm-148 1 0 1-20 840 end

sm-147 1 0 1-20 840 end

sm-149 1 0 1-20 840 end

sm-150 1 0 1-20 840 end

sm-151 1 0 1-20 840 end

sm-152 1 0 1-20 840 end

eu-153 1 0 1-20 840 end

eu-154 1 0 1-20 840 end

eu-155 1 0 1-20 840 end

gd-155 1 0 1-20 840 end

zirc2 2 1 620 end

h2o 3 den=0.306 1 557 end

n 4 0 5-5 557 end

```
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 5 1.0 557 end
```

uo2 6 den=10.32 1 840

92234 0.024 92235 2.732 92236 0.013 92238 97.231 end

arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end

h2o 7 den=0.862 1 557 end

end comp

* fuel-pin-cell geometry:

squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end

* assembly and cycle parameters:

```
npin/assm=49 fuelight=1719.74 ncycles=17 nlib/cyc=2
printlevel=5 inplevel=2 numztotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5
3.4223 7 3.7883
```

power=14.357 burn=19 down=8 end

power=17.091 burn=130 down=17 end

power=21.459 burn=41 down=10 end

power=16.747 burn=226 down=35 end

power=18.409 burn=39 down=7 end

power=20.888 burn=22 down=12 end

power=19.603 burn=108 down=19 end

power=20.314 burn=114 down=59 end

power=16.642 burn=79 down=8 end

power=18.409 burn=64 down=5 end

power=15.473 burn=150 down=31 end

power=15.570 burn=164 down=799 end

power=9.611 burn=160 down=9 end

power=9.967 burn=148 down=48 end

power=9.184 burn=96 down=61 end

power=9.669 burn=129 down=5 end

power=8.582 burn=57 down=1954.09 end

end

coop2974u.input

=sas2h parm=skipshipdata

Cooper BWR Sample ADD2974-U, Height 291.087 cm from top, Aug 97

.

.

mixtures of fuel-pin-unit-cell:

44group latticecell

uo2 1 den=10.32 1 840

92234 0.026 92235 2.93 92236 0.013 92238 97.031 end

kr-83 1 0 1-20 840 end

kr-85 1 0 1-20 840 end

y-89 1 0 1-20 840 end

sr-90 1 0 1-20 840 end

zr-93 1 0 1-20 840 end

zr-94 1 0 1-20 840 end

zr-95 1 0 1-20 840 end

nb-94 1 0 1-20 840 end

mo-95 1 0 1-20 840 end

tc-99 1 0 1-20 840 end

ru-101 1 0 1-20 840 end

ru-106 1 0 1-20 840 end

rh-103 1 0 1-20 840 end

rh-105 1 0 1-20 840 end

pd-105 1 0 1-20 840 end

pd-108 1 0 1-20 840 end

ag-109 1 0 1-20 840 end

sb-124 1 0 1-20 840 end

xe-131 1 0 1-20 840 end

xe-132 1 0 1-20 840 end

xe-135 1 0 1-20 840 end

xe-136 1 0 1-20 840 end

cs-134 1 0 1-20 840 end

cs-135 1 0 1-20 840 end

cs-137 1 0 1-20 840 end

ba-136 1 0 1-20 840 end

la-139 1 0 1-20 840 end

pr-141 1 0 1-20 840 end

pr-143 1 0 1-20 840 end

ce-144 1 0 1-20 840 end

nd-143 1 0 1-20 840 end

nd-145 1 0 1-20 840 end

nd-147 1 0 1-20 840 end

pm-147 1 0 1-20 840 end

pm-148 1 0 1-20 840 end

sm-147 1 0 1-20 840 end

sm-149 1 0 1-20 840 end

sm-150 1 0 1-20 840 end

sm-151 1 0 1-20 840 end

sm-152 1 0 1-20 840 end

eu-153 1 0 1-20 840 end

eu-154 1 0 1-20 840 end

eu-155 1 0 1-20 840 end

gd-155 1 0 1-20 840 end

zirc2 2 1 620 end

.

.

h2o 3 den=0.652 1 557 end

.

n 4 0 5-5 557 end

.

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40

40000 98.18 5 1.0 557 end

.

uo2 6 den=10.32 1 840

92234 0.024 92235 2.732 92236 0.013 92238 97.231 end

arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end

.

h2o 7 den=0.862 1 557 end

end comp

.

fuel-pin-cell geometry:

squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end

.

assembly and cycle parameters:

npin/assm=49 fuelght=1719.74 ncycles=17 nlib/cyc=2

printlevel=5 inplevel=2 numztotal=8 end

6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5

3.4223 7 3.7883

power=15.246 burn=19 down=8 end

power=18.149 burn=130 down=17 end

power=22.788 burn=41 down=10 end

power=17.784 burn=226 down=35 end

power=19.549 burn=39 down=7 end

power=22.182 burn=22 down=12 end

power=20.817 burn=108 down=19 end

power=21.572 burn=114 down=59 end

power=17.673 burn=79 down=8 end

power=19.549 burn=64 down=5 end

power=16.431 burn=150 down=31 end

power=16.534 burn=164 down=799 end

power=10.206 burn=160 down=9 end

power=10.584 burn=148 down=48 end

power=9.753 burn=96 down=61 end

power=10.268 burn=129 down=5 end

power=9.113 burn=57 down=1954.09 end

.

.

end

2966tplus100deg.input

=as2h parm=skpshipdata

Cooper BWR Sample ADD2966-T, Height 274.777 cm from top, Aug 97

* 100 K increase in fuel temperature

* mixtures of fuel-pin-unit-cell:

44group latticecell

uo2 1 den=10.32 1 940

92234 0.026 92235 2.93 92236 0.013 92238 97.031 end

kr-83 1 0 1-20 940 end

kr-85 1 0 1-20 940 end

y-89 1 0 1-20 940 end

sr-90 1 0 1-20 940 end

zr-93 1 0 1-20 940 end

zr-94 1 0 1-20 940 end

zr-95 1 0 1-20 940 end

nb-94 1 0 1-20 940 end

mo-95 1 0 1-20 940 end

tc-99 1 0 1-20 940 end

ru-101 1 0 1-20 940 end

ru-106 1 0 1-20 940 end

rh-103 1 0 1-20 940 end

rh-105 1 0 1-20 940 end

pd-105 1 0 1-20 940 end

pd-108 1 0 1-20 940 end

ag-109 1 0 1-20 940 end

sb-124 1 0 1-20 940 end

xe-131 1 0 1-20 940 end

xe-132 1 0 1-20 940 end

xe-135 1 0 1-20 940 end

xe-136 1 0 1-20 940 end

cs-134 1 0 1-20 940 end

cs-135 1 0 1-20 940 end

cs-137 1 0 1-20 940 end

ba-136 1 0 1-20 940 end

la-139 1 0 1-20 940 end

pr-141 1 0 1-20 940 end

pr-143 1 0 1-20 940 end

cc-144 1 0 1-20 940 end

nd-143 1 0 1-20 940 end

nd-145 1 0 1-20 940 end

nd-147 1 0 1-20 940 end

pm-147 1 0 1-20 940 end

pm-148 1 0 1-20 940 end

sm-147 1 0 1-20 940 end

sm-149 1 0 1-20 940 end

sm-150 1 0 1-20 940 end

sm-151 1 0 1-20 940 end

sm-152 1 0 1-20 940 end

cu-153 1 0 1-20 940 end

cu-154 1 0 1-20 940 end

cu-155 1 0 1-20 940 end

gd-155 1 0 1-20 940 end

zirc2 2 1 620 end

h2o 3 den=0.607 1 557 end

n 4 0 5-5 557 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 5 1 0 557 end

uo2 6 den=10.32 1 940

92234 0.024 92235 2.732 92236 0.013 92238 97.231 end

arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 940 end

h2o 7 den=0.862 1 557 end

end comp

fuel-pin-cell geometry:

squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end

assembly and cycle parameters:

npin/asm=49 fuelight=1719.74 ncycles=17 alib/cyc=2

printlevel=5 inplevel=2 numxtotal=8 end

6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5

3.4223 7 3.7883

power=16.671 burn=19 down=8 end

power=19.845 burn=130 down=17 end

power=24.917 burn=41 down=10 end

power=19.445 burn=226 down=35 end

power=21.375 burn=39 down=7 end

power=24.254 burn=22 down=12 end

power=22.762 burn=108 down=19 end

power=23.587 burn=114 down=59 end

power=19.324 burn=79 down=8 end

power=21.375 burn=64 down=5 end

power=17.966 burn=150 down=31 end

power=18.078 burn=164 down=799 end

power=11.160 burn=160 down=9 end

power=11.573 burn=148 down=48 end

power=10.664 burn=96 down=61 end

power=11.227 burn=129 down=5 end

power=9.965 burn=57 down=1954.09 end

end

2966tplus10den.input

=sas2h parm=skipshipdata

Cooper BWR Sample ADD2966-T, Height 274.777 cm from top, Aug 97

* increase moderator density by 10%

* mixtures of fuel-pin-unit-cell:

```
44group latticecl
uo2 1 den=10.32 1 840
92234 0.026 92235 2.93 92236 0.013 92238 97.031 end
```

kr-83 1 0 1-20 840 end

kr-85 1 0 1-20 840 end

y-89 1 0 1-20 840 end

sr-90 1 0 1-20 840 end

zr-93 1 0 1-20 840 end

zr-94 1 0 1-20 840 end

zr-95 1 0 1-20 840 end

nb-94 1 0 1-20 840 end

mo-95 1 0 1-20 840 end

tc-99 1 0 1-20 840 end

ru-101 1 0 1-20 840 end

ru-106 1 0 1-20 840 end

rh-103 1 0 1-20 840 end

rh-105 1 0 1-20 840 end

pd-105 1 0 1-20 840 end

pd-108 1 0 1-20 840 end

ag-109 1 0 1-20 840 end

sb-124 1 0 1-20 840 end

xe-131 1 0 1-20 840 end

xe-132 1 0 1-20 840 end

xe-135 1 0 1-20 840 end

xe-136 1 0 1-20 840 end

cs-134 1 0 1-20 840 end

cs-135 1 0 1-20 840 end

cs-137 1 0 1-20 840 end

ba-136 1 0 1-20 840 end

la-139 1 0 1-20 840 end

pr-141 1 0 1-20 840 end

pr-143 1 0 1-20 840 end

ce-144 1 0 1-20 840 end

nd-143 1 0 1-20 840 end

nd-145 1 0 1-20 840 end

nd-147 1 0 1-20 840 end

pm-147 1 0 1-20 840 end

pm-148 1 0 1-20 840 end

sm-147 1 0 1-20 840 end

sm-149 1 0 1-20 840 end

sm-150 1 0 1-20 840 end

sm-151 1 0 1-20 840 end

sm-152 1 0 1-20 840 end

eu-153 1 0 1-20 840 end

eu-154 1 0 1-20 840 end

eu-155 1 0 1-20 840 end

gd-155 1 0 1-20 840 end

zirc2 2 1 620 end

h2o 3 den=0.668 1 557 end

n 4 0 5-5 557 end

```
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 5 1.0 557 end
```

uo2 6 den=10.32 1 840

92234 0.024 92235 2.732 92236 0.013 92238 97.231 end

arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end

h2o 7 den=0.862 1 557 end

end comp

fuel-pin-cell geometry:

squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end

assembly and cycle parameters:

```
npin/assm=49 fuelght=1719.74 acycles=17 nlib/cyc=2
printlevel=5 inplevel=2 numztotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5
3.4223 7 3.7883
```

power=16.671 burn=19 down=8 end

power=19.845 burn=130 down=17 end

power=24.917 burn=41 down=10 end

power=19.445 burn=226 down=35 end

power=21.375 burn=39 down=7 end

power=24.254 burn=22 down=12 end

power=22.762 burn=108 down=19 end

power=23.587 burn=114 down=59 end

power=19.324 burn=79 down=8 end

power=21.375 burn=64 down=5 end

power=17.966 burn=150 down=31 end

power=18.078 burn=164 down=799 end

power=11.160 burn=160 down=9 end

power=11.573 burn=148 down=48 end

power=10.664 burn=96 down=61 end

power=11.227 burn=129 down=5 end

power=9.965 burn=57 down=1954.09 end

end

2974bplus100deg.input

=sas2h parm=skipshipdata

Cooper BWR Sample ADD2974-B, Height 55.723 cm from top, Aug 97

increase fuel temperature 100 K

mixtures of fuel-pin-unit-cell:

44group latticecell

uo2 1 den=10.32 1 940

92234 0.026 92235 2.93 92236 0.013 92238 97.031 end

kr-83 1 0 1-20 940 end

kr-85 1 0 1-20 940 end

y-89 1 0 1-20 940 end

sr-90 1 0 1-20 940 end

zr-93 1 0 1-20 940 end

zr-94 1 0 1-20 940 end

zr-95 1 0 1-20 940 end

nb-94 1 0 1-20 940 end

mo-95 1 0 1-20 940 end

tc-99 1 0 1-20 940 end

ru-101 1 0 1-20 940 end

ru-106 1 0 1-20 940 end

rh-103 1 0 1-20 940 end

rh-105 1 0 1-20 940 end

pd-105 1 0 1-20 940 end

pd-108 1 0 1-20 940 end

ag-109 1 0 1-20 940 end

sb-124 1 0 1-20 940 end

xe-131 1 0 1-20 940 end

xe-132 1 0 1-20 940 end

xe-135 1 0 1-20 940 end

xe-136 1 0 1-20 940 end

cs-134 1 0 1-20 940 end

cs-135 1 0 1-20 940 end

cs-137 1 0 1-20 940 end

ba-136 1 0 1-20 940 end

la-139 1 0 1-20 940 end

pr-141 1 0 1-20 940 end

pr-143 1 0 1-20 940 end

ce-144 1 0 1-20 940 end

nd-143 1 0 1-20 940 end

nd-145 1 0 1-20 940 end

nd-147 1 0 1-20 940 end

pm-147 1 0 1-20 940 end

pm-148 1 0 1-20 940 end

sm-147 1 0 1-20 940 end

sm-149 1 0 1-20 940 end

sm-150 1 0 1-20 940 end

sm-151 1 0 1-20 940 end

sm-152 1 0 1-20 940 end

eu-153 1 0 1-20 940 end

eu-154 1 0 1-20 940 end

eu-155 1 0 1-20 940 end

gd-155 1 0 1-20 940 end

zirc2 2 1 620 end

h2o 3 den=0.240 1 557 end

n 4 0.5-5 557 end

arbm-zirc4 6.56 5 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 5 1.0 557 end

uo2 6 den=10.32 1 940

92234 0.024 92235 2.732 92236 0.013 92238 97.231 end

arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 940 end

h2o 7 den=0.862 1 557 end

end comp

fuel-pin-cell geometry:

squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end

assembly and cycle parameters:

npin/assm=49 fuelight=1719.74 acycles=17 nlib/cyc=2
printlevel=5 inplevel=2 numztotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5
3.4223 7 3.7883

power=8.763 burn=19 down=8 end

power=10.431 burn=130 down=17 end

power=13.097 burn=41 down=10 end

power=10.221 burn=226 down=35 end

power=11.235 burn=39 down=7 end

power=12.749 burn=22 down=12 end

power=11.965 burn=108 down=19 end

power=12.398 burn=114 down=59 end

power=10.157 burn=79 down=8 end

power=11.235 burn=64 down=5 end

power=9.444 burn=150 down=31 end

power=9.503 burn=164 down=799 end

power=5.866 burn=160 down=9 end

power=6.083 burn=148 down=48 end

power=5.606 burn=96 down=61 end

power=5.901 burn=129 down=5 end

power=5.238 burn=57 down=1954.09 end

end

2974bplus50den.input

=====
 =sas2h parm=skipshipdata
 Cooper BWR Sample ADD2974-B, Height 55.723 cm from top, Aug 97

increase moderator density by 50%

mixtures of fuel-pin-unit-cell:

```
44group latticecell
uo2 1 den=10.32 1 840
  92234 0.026 92235 2.93 92236 0.013 92238 97.031 end
kr-83 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
zr-93 1 0 1-20 840 end
zr-94 1 0 1-20 840 end
zr-95 1 0 1-20 840 end
nb-94 1 0 1-20 840 end
mo-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-106 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
ag-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
xe-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
cs-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sm-147 1 0 1-20 840 end
sm-149 1 0 1-20 840 end
sm-150 1 0 1-20 840 end
sm-151 1 0 1-20 840 end
sm-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
gd-155 1 0 1-20 840 end

zirc2 2 1 620 end

h2o 3 den=0.36 1 557 end

n 4 0.5-5 557 end

arbm-zirc4 6.56 5 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 5 1.0 557 end

uo2 6 den=10.32 1 840
  92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end

h2o 7 den=0.862 1 557 end
```

.....
 end comp

fuel-pin-cell geometry:

squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end

assembly and cycle parameters:

```
npin/assm=49 fuelght=1719.74 ncycles=17 .nlib/cyc=2
printlevel=5 inplevel=2 numxtotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5
3.4223 7 3.7883
power=8.763 burn=19 down=8 end
power=10.431 burn=130 down=17 end
power=13.097 burn=41 down=10 end
power=10.221 burn=226 down=35 end
power=11.235 burn=39 down=7 end
power=12.749 burn=22 down=12 end
power=11.965 burn=108 down=19 end
power=12.398 burn=114 down=59 end
power=10.157 burn=79 down=8 end
power=11.235 burn=64 down=5 end
power=9.444 burn=150 down=31 end
power=9.503 burn=164 down=799 end
power=5.866 burn=160 down=9 end
power=6.083 burn=148 down=48 end
power=5.606 burn=96 down=61 end
power=5.901 burn=129 down=5 end
power=5.238 burn=57 down=1954.09 end
```

.....
 end

coop2966b.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....
1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Cooper BMW Sample ADC2966-B, Weight 55.107 gm from top, Aug 97
  :
  :
  : mixtures of fuel-pin-unit-cell:
  44group latticecell
  uo2 1 den=10.32 1 840
    92236 0.026 92235 2.93 92236 0.013 92238 97.031 end
  kr-83 1 0 1-20 840 end
  kr-85 1 0 1-20 840 end
  yr-89 1 0 1-20 840 end
  sr-90 1 0 1-20 840 end
  sr-93 1 0 1-20 840 end
  sr-94 1 0 1-20 840 end
  sr-95 1 0 1-20 840 end
  nb-94 1 0 1-20 840 end
  mo-95 1 0 1-20 840 end
  tc-99 1 0 1-20 840 end
  ru-101 1 0 1-20 840 end
  ru-106 1 0 1-20 840 end
  rh-103 1 0 1-20 840 end
  rh-105 1 0 1-20 840 end
  pd-105 1 0 1-20 840 end
  pd-108 1 0 1-20 840 end
  ag-109 1 0 1-20 840 end
  ab-124 1 0 1-20 840 end
  xe-131 1 0 1-20 840 end
  xe-132 1 0 1-20 840 end
  xe-135 1 0 1-20 840 end
  xe-136 1 0 1-20 840 end
  cs-134 1 0 1-20 840 end
  cs-135 1 0 1-20 840 end
  cs-137 1 0 1-20 840 end
  ba-136 1 0 1-20 840 end
  la-139 1 0 1-20 840 end
  pr-141 1 0 1-20 840 end
  pr-143 1 0 1-20 840 end
  ce-144 1 0 1-20 840 end
  nd-143 1 0 1-20 840 end
  nd-145 1 0 1-20 840 end
  nd-147 1 0 1-20 840 end
  pm-147 1 0 1-20 840 end
  pm-148 1 0 1-20 840 end
  sm-147 1 0 1-20 840 end
  sm-149 1 0 1-20 840 end
  sm-150 1 0 1-20 840 end
  sm-151 1 0 1-20 840 end
  sm-152 1 0 1-20 840 end
  eu-153 1 0 1-20 840 end
  eu-154 1 0 1-20 840 end
  eu-155 1 0 1-20 840 end
  qd-155 1 0 1-20 840 end
  :
  sirc2 2 1 620 end
  :
  :
  h2o 3 den=0.240 1 557 end
  n 4 0 5-5 557 end
  :
  arbm=sirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
    40000 98.18 5 1.0 557 end
  :
  uo2 6 den=10.32 1 840
    92236 0.026 92235 2.732 92236 0.013 92238 97.231 end
  arbm=qdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end
  :
  h2o 7 den=0.862 1 557 end
  :
  -----
  end comp
  :
  :
  : fuel-pin-cell geometry:
  squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end
  :
  :
  : assembly and cycle parameters:
  npin/asmm=49 fuelwght=1719.74 ncycles=17 nlib/cyc=2
  printlevel=3 imdlev=1=2 namatotal=8 end
  6 0.6050 4 0.4210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5 3.4223 7 3.7883
  power=9.313 burn=19 down=8 end
  power=11.086 burn=130 down=17 end
  power=13.919 burn=41 down=10 end
  power=10.863 burn=226 down=35 end
  power=11.941 burn=19 down=7 end
  power=13.549 burn=22 down=12 end
  power=12.716 burn=108 down=19 end
  power=13.177 burn=114 down=39 end
  power=10.795 burn=79 down=8 end
  power=11.941 burn=64 down=5 end
  power=10.837 burn=150 down=31 end
  power=10.099 burn=144 down=799 end
  power=6.234 burn=160 down=9 end
  power=6.465 burn=148 down=48 end

```


coop2966k.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....
1 primary module access and input record | scale driver - 95/03/29 - 09:06:37 |
- module sas2h will be called
  Cooper BWR Sample ADD2966-K, Height 218.869 cm from top, Aug 97
.
.
. mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.32 1 840
  92234 0.024 92235 2.93 92236 0.013 92238 97.031 end
kr-83 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
sr-91 1 0 1-20 840 end
sr-94 1 0 1-20 840 end
sr-95 1 0 1-20 840 end
nb-94 1 0 1-20 840 end
mo-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-106 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
sg-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
xe-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
ca-134 1 0 1-20 840 end
ca-135 1 0 1-20 840 end
ca-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sa-147 1 0 1-20 840 end
sa-149 1 0 1-20 840 end
sa-150 1 0 1-20 840 end
sa-151 1 0 1-20 840 end
sa-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
gd-155 1 0 1-20 840 end
sirc2 2 1 620 end
.
.
h2o 3 den=0.478 1 557 end
n 4 0 3-5 557 end
arbm-sirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 24000 0.20 50000 1.40
  40000 98.18 5 1.0 557 end
uo2 6 den=10.32 1 840
  92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
arbm-odrod 10.32 2 0 1 0 8016 3 64000 2 4 0.034 840 end
h2o 7 den=0.862 1 557 end
.
.
. end comp
.
.
. fuel-pin-cell geometry:
squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end
.
.
. assembly and cycle parameters:
rpin/sasm=49 fuelight=1719.74 ncycles=17 nlib/cyc=2
printlevel=3 implevel=2 nasmtotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5 3.4223 7 3.7883
power=16.243 burn=19 down=8 end
power=19.336 burn=110 down=17 end
power=24.278 burn=41 down=10 end
power=18.947 burn=226 down=35 end
power=20.827 burn=39 down=7 end
power=21.632 burn=22 down=12 end
power=22.179 burn=108 down=19 end
power=22.983 burn=114 down=39 end
power=18.829 burn=79 down=8 end
power=20.827 burn=44 down=5 end
power=17.506 burn=150 down=31 end
power=17.615 burn=164 down=799 end
power=10.874 burn=160 down=9 end
power=11.276 burn=148 down=48 end

```

power=10.391 burn=96 down=61 and
power=10.939 burn=129 down=5 and
power=9.709 burn=57 down=1934.09 and

```
1 *****   *****   *****   2222222222   hh   hh  
*****   *****   *****   222222222222   hh   hh  
**   **   **   **   **   **   22   hh   hh  
**   **   **   **   **   **   22   hh   hh  
**   **   **   **   **   **   22   hh   hh  
*****   *****   *****   22   hhhhhhhhhhhh  
*****   *****   *****   22   hhhhhhhhhhhh  
**   **   **   **   **   **   22   hh   hh  
**   **   **   **   **   **   22   hh   hh  
**   **   **   **   **   **   22   hh   hh  
*****   **   **   *****   222222222222   hh   hh  
*****   **   **   *****   222222222222   hh   hh
```

```
0 run run   |iiiiiiiiiii|   ccccccccc   hh   hh   0000000000   11  
run run run   |iiiiiiiiiii|   ccccccccc   hh   hh   000000000000   11  
run run run   |ii|   cc   cc   hh   hh   oo   oo   00   11  
run run run   |ii|   cc   cc   hh   hh   oo   oo   00   11  
run run run   |ii|   cc   cc   hhhhhhhhhhhh   oo   oo   00   11  
run run run   |ii|   cc   cc   hhhhhhhhhhhh   oo   oo   00   11  
run run run   |ii|   cc   cc   hh   hh   oo   oo   00   11  
run run run   |ii|   cc   cc   hh   hh   oo   oo   00   11  
run run run   |ii|   cc   cc   hh   hh   oo   oo   00   11  
run run run   |iiiiiiiiiii|   ccccccccc   hh   hh   000000000000   111111111111  
run run run   |iiiiiiiiiii|   ccccccccc   hh   hh   000000000000   111111111111
```

```
0 0000000   0000000000   //   11   44   9999999999   7777777777  
0000000000   0000000000   //   111   444   999999999999   777777777777  
oo   oo   oo   oo   oo   oo   //   11   44   99   99   77  
oo   oo   oo   oo   oo   oo   //   11   44   99   99   77  
oo   oo   oo   oo   oo   oo   //   11   44   99   99   77  
oo   oo   oo   oo   oo   oo   //   11   44   99   99   77  
oo   oo   oo   oo   oo   oo   //   11   44   99   99   77  
oo   oo   oo   oo   oo   oo   //   11   44   99   99   77  
oo   oo   oo   oo   oo   oo   //   11   44   99   99   77  
oo   oo   oo   oo   oo   oo   //   11   44   99   99   77  
0000000000   0000000000   //   11111111   44   999999999999   77  
0000000000   0000000000   //   11111111   44   999999999999   77
```

```
11   0000000000   5555555555   9999999999   3333333333   11  
111   00000000000   555555555555   999999999999   333333333333   111  
1111   oo   oo   111   55   99   99   99   33   1111  
11   oo   oo   111   55   99   99   99   33   11  
11   oo   oo   111   55   99   99   99   33   11  
11   0000000000   5555555555   999999999999   333   11  
11   0000000000   555555555555   999999999999   333   11  
11   oo   oo   111   55   99   99   99   33   11  
11   oo   oo   111   55   99   99   99   33   11  
11   oo   oo   111   55   99   99   99   33   11  
1111111111   00000000000   555555555555   999999999999   333333333333   1111111111  
1111111111   00000000000   555555555555   999999999999   333333333333   1111111111
```

```
0 *****   cccccccccc   aaaaaaaaaa   11   0000000000  
**   **   cc   cc   cc   **   **   **   **   **   oo  
**   **   cc   cc   cc   **   **   **   **   **   oo  
**   **   cc   cc   cc   **   **   **   **   **   oo  
*****   cc   aaaaaaaaaa   11   ccccccccc  
**   **   cc   **   **   **   **   **   **   **   cc  
**   **   cc   cc   cc   **   **   **   **   **   cc  
*****   cc   cccccccccccc   aa   aa   111111111111   cccccccccccc  
*****   cccccccccc   aa   aa   111111111111   cccccccccccc
```

```
.....  
.....  
.....  
..... program verification information .....  
..... code system: scale version: 4.3 .....  
.....  
.....  
..... program: sas2 .....  
..... creation date: 03/07/97 .....  
..... library: /opt/neut/Scaled.3/bin .....  
..... this is not a scale configuration controlled code .....  
..... jobname: nichol .....  
..... date of execution: 08/14/97 .....  
..... time of execution: 18:59:32 .....  
.....  
.....
```

1
0
0
0
0

nucleide concentrations, grams

	initial	18-18 d	basis = single reactor assembly									
gd155	4.39E+02	4.39E+02										
total	1.97E+04	1.97E+04										
	initial		nuclide concentrations, grams									
	initial		basis = single reactor assembly									
u234	2.29E+02	2.29E+02										
u235	2.38E+04	2.38E+04										
u236	1.13E+02	1.13E+02										
u238	8.53E+05	8.53E+05										
total	8.81E+05	8.81E+05										
	initial		2.4 d		4.8 d		7.1 d		9.5 d		9.5 d	
	initial		2.4 d		4.8 d		7.1 d		9.5 d		9.5 d	
	initial		basis = single reactor assembly									
charge	2.4 d	4.8 d										
charge	2.4 d	4.8 d										
charge	2.4 d	4.8 d										
am147	0.0E+00	1.19E-22	4.47E-22	9.56E-22	1.61E-21	1.61E-21	9.81E-21	9.81E-21	9.81E-21	9.81E-21	9.81E-21	9.81E-21
am149	0.0E+00	3.33E-12	5.99E-12	9.12E-12	9.81E-12	9.81E-12	9.81E-12	9.81E-12	9.81E-12	9.81E-12	9.81E-12	9.81E-12
am150	0.0E+00	1.76E-11	3.59E-11	5.47E-11	7.40E-11	7.40E-11	7.40E-11	7.40E-11	7.40E-11	7.40E-11	7.40E-11	7.40E-11
am151	0.0E+00	3.55E-10	7.01E-10	1.04E-09	1.37E-09	1.37E-09	1.37E-09	1.37E-09	1.37E-09	1.37E-09	1.37E-09	1.37E-09
am152	0.0E+00	3.77E-10	7.59E-10	1.13E-09	1.54E-09	1.54E-09	1.54E-09	1.54E-09	1.54E-09	1.54E-09	1.54E-09	1.54E-09
eu151	0.0E+00	1.81E-12	3.60E-12	5.37E-12	7.11E-12	7.11E-12	7.11E-12	7.11E-12	7.11E-12	7.11E-12	7.11E-12	7.11E-12
eu153	0.0E+00	4.57E-08	1.62E-07	4.68E-07	7.21E-07	7.21E-07	7.21E-07	7.21E-07	7.21E-07	7.21E-07	7.21E-07	7.21E-07
gd155m	0.0E+00	6.85E-12	4.63E-12	4.63E-12	4.63E-12	4.63E-12	4.63E-12	4.63E-12	4.63E-12	4.63E-12	4.63E-12	4.63E-12
gd155	2.81E+00	2.82E+00	2.81E+00	2.80E+00	2.78E+00	2.78E+00	2.78E+00	2.78E+00	2.78E+00	2.78E+00	2.78E+00	2.78E+00
totals	6.35E+03	6.95E+03	6.95E+03	6.95E+03	6.95E+03	6.95E+03	6.95E+03	6.95E+03	6.95E+03	6.95E+03	6.95E+03	6.95E+03
	charge		2.4 d		4.8 d		7.1 d		9.5 d		9.5 d	
u233	0.0E+00	1.97E-08	3.93E-08	5.89E-08	7.84E-08	7.84E-08	7.84E-08	7.84E-08	7.84E-08	7.84E-08	7.84E-08	7.84E-08
u234	9.79E-01	9.79E-01	9.79E-01	9.79E-01	9.79E-01	9.79E-01	9.79E-01	9.79E-01	9.79E-01	9.79E-01	9.79E-01	9.79E-01
u235	1.10E+02	1.10E+02	1.09E+02	1.09E+02	1.09E+02	1.09E+02	1.09E+02	1.09E+02	1.09E+02	1.09E+02	1.09E+02	1.09E+02
u236	4.85E-01	3.21E-01	5.37E-01	5.93E-01	6.28E-01	6.28E-01	6.28E-01	6.28E-01	6.28E-01	6.28E-01	6.28E-01	6.28E-01
u238	3.59E+03	3.59E+03	3.59E+03	3.59E+03	3.59E+03	3.59E+03	3.59E+03	3.59E+03	3.59E+03	3.59E+03	3.59E+03	3.59E+03
np237	0.0E+00	7.22E-05	2.69E-04	5.65E-04	9.40E-04	9.40E-04	9.40E-04	9.40E-04	9.40E-04	9.40E-04	9.40E-04	9.40E-04
pu236	0.0E+00	3.71E-14	4.35E-13	1.70E-12	4.27E-12	4.27E-12	4.27E-12	4.27E-12	4.27E-12	4.27E-12	4.27E-12	4.27E-12
pu238	0.0E+00	5.22E-09	6.78E-08	2.88E-07	7.73E-07	7.73E-07	7.73E-07	7.73E-07	7.73E-07	7.73E-07	7.73E-07	7.73E-07
pu239	0.0E+00	5.22E-09	6.78E-08	2.88E-07	7.73E-07	7.73E-07	7.73E-07	7.73E-07	7.73E-07	7.73E-07	7.73E-07	7.73E-07
pu240	0.0E+00	2.65E-02	8.74E-02	1.65E-01	2.51E-01	2.51E-01	2.51E-01	2.51E-01	2.51E-01	2.51E-01	2.51E-01	2.51E-01
pu241	0.0E+00	4.65E-05	2.26E-04	5.73E-04	1.10E-03	1.10E-03	1.10E-03	1.10E-03	1.10E-03	1.10E-03	1.10E-03	1.10E-03
pu242	0.0E+00	1.13E-07	1.02E-06	4.06E-06	1.04E-05	1.04E-05	1.04E-05	1.04E-05	1.04E-05	1.04E-05	1.04E-05	1.04E-05
pu242	0.0E+00	3.95E-11	7.42E-10	4.18E-09	1.43E-08	1.43E-08	1.43E-08	1.43E-08	1.43E-08	1.43E-08	1.43E-08	1.43E-08
	charge		2.4 d		4.8 d		7.1 d		9.5 d		9.5 d	
am241	0.0E+00	8.45E-12	1.59E-10	8.94E-10	3.06E-09	3.06E-09	3.06E-09	3.06E-09	3.06E-09	3.06E-09	3.06E-09	3.06E-09
am242m	0.0E+00	1.02E-15	3.74E-14	3.13E-13	1.42E-12	1.42E-12	1.42E-12	1.42E-12	1.42E-12	1.42E-12	1.42E-12	1.42E-12
am243	0.0E+00	7.35E-15	2.84E-13	2.46E-12	1.14E-11	1.14E-11	1.14E-11	1.14E-11	1.14E-11	1.14E-11	1.14E-11	1.14E-11
totals	3.70E+03	3.70E+03	3.70E+03	3.70E+03	3.70E+03	3.70E+03	3.70E+03	3.70E+03	3.70E+03	3.70E+03	3.70E+03	3.70E+03
	decay data, including gamma and total energy, are from endf/b-vi											
	1697 total number of nuclides in library											
	initial		nuclide concentrations, grams									
	initial		basis = single reactor assembly									
am150	2.20E+04	3.20E+06	2.20E+06	2.20E+06	2.20E+06	2.20E+06	2.20E+06	2.20E+06	2.20E+06	2.20E+06	2.20E+06	2.20E+06
am152	1.34E+05	1.35E+05	1.35E+05	1.35E+05	1.35E+05	1.35E+05	1.35E+05	1.35E+05	1.35E+05	1.35E+05	1.35E+05	1.35E+05
eu153	7.80E+01	8.71E+01	9.06E+01	9.20E+01	9.26E+01	9.28E+01	9.28E+01	9.28E+01	9.28E+01	9.28E+01	9.28E+01	9.28E+01
	initial		nuclide concentrations, grams									
	initial		basis = single reactor assembly									
gd155	2.12E+01	2.16E+01	2.20E+01	2.23E+01	2.26E+01	2.28E+01	2.30E+01	2.30E+01	2.30E+01	2.30E+01	2.30E+01	2.30E+01
total	1.97E+04	1.97E+04	1.97E+04	1.97E+04	1.97E+04	1.97E+04	1.97E+04	1.97E+04	1.97E+04	1.97E+04	1.97E+04	1.97E+04
	initial		nuclide concentrations, grams									
	initial		basis = single reactor assembly									
u233	1.49E+03	1.40E+03	1.71E+03	1.81E+03	1.92E+03	1.93E+03	1.94E+03	1.94E+03	1.94E+03	1.94E+03	1.94E+03	1.94E+03
u234	1.32E+02	1.33E+02	1.34E+02	1.35E+02	1.37E+02	1.38E+02	1.38E+02	1.39E+02	1.39E+02	1.39E+02	1.39E+02	1.39E+02
u235	5.22E+03	5.22E+03	5.22E+03	5.22E+03	5.22E+03	5.22E+03	5.22E+03	5.22E+03	5.22E+03	5.22E+03	5.22E+03	5.22E+03
u236	3.46E+03	3.46E+03	3.46E+03	3.46E+03	3.46E+03	3.46E+03	3.46E+03	3.46E+03	3.46E+03	3.46E+03	3.46E+03	3.46E+03
u238	8.34E+05	8.34E+05	8.34E+05	8.34E+05	8.34E+05	8.34E+05	8.34E+05	8.34E+05	8.34E+05	8.34E+05	8.34E+05	8.34E+05
np237	3.40E+02	3.42E+02	3.42E+02	3.43E+02	3.43E+02	3.43E+02	3.43E+02	3.44E+02	3.44E+02	3.44E+02	3.44E+02	3.44E+02
pu236	3.30E+04	2.88E+04	2.16E+04	1.75E+04	1.41E+04	1.14E+04	9.22E+03	9.22E+03	9.22E+03	9.22E+03	9.22E+03	9.22E+03
pu238	1.30E+02	1.62E+02	1.64E+02	1.63E+02	1.62E+02	1.61E+02	1.60E+02	1.60E+02	1.60E+02	1.60E+02	1.60E+02	1.60E+02
pu239	1.50E+02	1.62E+02	1.64E+02	1.63E+02	1.62E+02	1.61E+02	1.60E+02	1.60E+02	1.60E+02	1.60E+02	1.60E+02	1.60E+02
pu239	3.93E+03	3.96E+03	3.96E+03	3.96E+03	3.96E+03	3.96E+03	3.96E+03	3.96E+03	3.96E+03	3.96E+03	3.96E+03	3.96E+03
pu240	2.09E+03	2.09E+03	2.09E+03	2.09E+03	2.10E+03	2.10E+03	2.10E+03	2.10E+03	2.10E+03	2.10E+03	2.10E+03	2.10E+03
pu241	8.90E+02	8.52E+02	8.16E+02	7.82E+02	7.49E+02	7.17E+02	6.87E+02	6.87E+02	6.87E+02	6.87E+02	6.87E+02	6.87E+02
pu242	4.60E+02	4.60E+02	4.60E+02	4.60E+02	4.60E+02	4.60E+02	4.60E+02	4.60E+02	4.60E+02	4.60E+02	4.60E+02	4.60E+02
am241	1.05E+02	1.43E+02	1.78E+02	2.13E+02	2.45E+02	2.76E+02	3.06E+02	3.06E+02	3.06E+02	3.06E+02	3.06E+02	3.06E+02
am242m	1.99E+00	1.98E+00	1.97E+00	1.96E+00	1.95E+00	1.94E+00	1.93E+00	1.93E+00	1.93E+00	1.93E+00	1.93E+00	1.93E+00
am243	9.47E+01	9.47E+01	9.47E+01	9.47E+01	9.47E+01	9.47E+01	9.47E+01	9.47E+01	9.47E+01	9.47E+01	9.47E+01	9.47E+01
total	8.51E+05	8.51E+05	8.51E+05	8.51E+05	8.51E+05	8.51E+05	8.51E+05	8.51E+05	8.51E+05	8.51E+05	8.51E+05	8.51E+05
	initial		nuclide concentrations, grams									
	initial		basis = single reactor assembly									
mo 95	6.38E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02
tc 99	7.02E+02	7.02E+02	7.02E+02	7.02E+02	7.02E+02	7.02E+02	7.02E+02	7.02E+02	7.02E+02	7.02E+02	7.02E+02	7.02E+02
	initial		nuclide concentrations, grams									
	initial		basis = single reactor assembly									
ru101	6.78E+02	6.78E+02	6.78E+02	6.78E+02	6.78E+02	6.78E+02	6.78E+02	6.78E+02	6.78E+02	6.78E+02	6.78E+02	6.78E+02
rh103	3.95E+02	4.08E+02	4.08E+02	4.08E+02	4.08E+02	4.08E+02	4.08E+02	4.08E+02	4.08E+02	4.08E+02	4.08E+02	4.08E+02
ag109	7.94E+01	7.94E+01	7.94E+01	7.94E+01	7.94E+01	7.94E+01	7.94E+01	7.94E+01	7.94E+01	7.94E+01	7.94E+01	7.94E+01
	initial		nuclide concentrations, grams									
	initial		basis = single reactor assembly									
nd143	6.36E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02	6.62E+02
nd145	5.89E+02	5.89E+02	5.89E+02	5.89E+02	5.89E+02	5.89E+02	5.89E+02	5.89E+02	5.89E+02	5.89E+02	5.89E+02	5.89E+02
am147	1.51E+02	1.70E+02	1.85E+02	1.96E+02	2.06E+02	2.13E+02	2.19E+02	2.19E+02	2.19E+02	2.19E+02	2.19E+02	2.19E+02
am149	2.18E+00	1.50E+00	1.50E+00	1.50E+00	1.50E+00	1.50E+00	1.50E+00	1.50E+00	1.50E+00	1.50E+00	1.50E+00	1.50E+00
am150	2.37E+02	2.37										

coop29661.sum

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.....
SCALR4.3 Bulletin Board
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Welcome to SCALR-4.3.
.....
1 primary module access and input record ( scale driver - 93/03/29 - 09:06:37 )
- module sas2h will be called
  Cooper BMR Sample ADC2966-T, Height 274.777 cm from top, Aug 97
  :
  :
  : mixtures of fuel-pin-unit-cell:
  :
  : $group latticecell
  : uo2 1 den=10.32 1 840
  : 92234 0.024 92235 2.93 92236 0.013 92238 97.031 end
  : hr-83 1 0 1-20 840 end
  : hr-85 1 0 1-20 840 end
  : y-89 1 0 1-20 840 end
  : sr-90 1 0 1-20 840 end
  : sr-93 1 0 1-20 840 end
  : sr-94 1 0 1-20 840 end
  : sr-95 1 0 1-20 840 end
  : nb-94 1 0 1-20 840 end
  : so-95 1 0 1-20 840 end
  : tc-99 1 0 1-20 840 end
  : ru-101 1 0 1-20 840 end
  : ru-106 1 0 1-20 840 end
  : rh-103 1 0 1-20 840 end
  : rh-105 1 0 1-20 840 end
  : pd-105 1 0 1-20 840 end
  : pd-108 1 0 1-20 840 end
  : ag-109 1 0 1-20 840 end
  : sb-124 1 0 1-20 840 end
  : xe-131 1 0 1-20 840 end
  : xe-132 1 0 1-20 840 end
  : xe-135 1 0 1-20 840 end
  : xe-136 1 0 1-20 840 end
  : cs-134 1 0 1-20 840 end
  : cs-135 1 0 1-20 840 end
  : cs-137 1 0 1-20 840 end
  : ba-136 1 0 1-20 840 end
  : la-139 1 0 1-20 840 end
  : pr-141 1 0 1-20 840 end
  : pr-143 1 0 1-20 840 end
  : ce-144 1 0 1-20 840 end
  : nd-143 1 0 1-20 840 end
  : nd-145 1 0 1-20 840 end
  : nd-147 1 0 1-20 840 end
  : pm-147 1 0 1-20 840 end
  : pm-148 1 0 1-20 840 end
  : sm-147 1 0 1-20 840 end
  : sm-149 1 0 1-20 840 end
  : sm-150 1 0 1-20 840 end
  : sm-151 1 0 1-20 840 end
  : sm-152 1 0 1-20 840 end
  : eu-153 1 0 1-20 840 end
  : eu-154 1 0 1-20 840 end
  : eu-155 1 0 1-20 840 end
  : gd-155 1 0 1-20 840 end
  :
  : rirc2 2 1 620 end
  :
  :
  : h2o 3 den=0.607 1 557 end
  :
  : n 4 0 5-5 557 end
  :
  : arbm-rirc4 6.56 5 0 0 0 8016 0.32 24000 0.10 26000 0.20 50000 1.40
  : 40000 99.18 5 1.0 557 end
  :
  : uo2 6 den=10.32 1 840
  : 92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
  : arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end
  :
  : h2o 7 den=0.862 1 557 end
  :
  : -----
  : end comp
  : -----
  :
  : fuel-pin-cell geometry:
  :
  : squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end
  :
  : -----
  :
  : assembly and cycle parameters:
  :
  : npin/asm=49 fuelght=1719.74 ncycles=17 nlib/cyc=3
  : printlevel=5 implevel=2 numtotal=8 end
  : 6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5 3.4223 7 3.7883
  : power=16.671 burn=19 down=8 end
  : power=19.845 burn=130 down=17 end
  : power=24.917 burn=41 down=10 end
  : power=19.445 burn=226 down=15 end
  : power=21.375 burn=39 down=7 end
  : power=24.254 burn=32 down=12 end
  : power=22.742 burn=108 down=19 end
  : power=23.587 burn=114 down=39 end
  : power=19.324 burn=79 down=8 end
  : power=21.375 burn=64 down=5 end
  : power=17.966 burn=150 down=31 end
  : power=18.078 burn=164 down=799 end
  : power=11.160 burn=160 down=9 end
  : power=11.573 burn=148 down=48 end

```

power=10.664 burn=96 down=61 and
power=11.227 burn=129 down=5 and
power=9.965 burn=37 down=1954.09 and

1 #####
2222222222 hh hh
2222222222 hh hh
ss aa aa ss 22 22 hh hh
ss aa aa ss 22 22 hh hh
ss aa aa ss 22 22 hh hh
22 hhhhhhhhhhhh
22 hhhhhhhhhhhh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
222222222222 hh hh
222222222222 hh hh

0
run run 1111111111 ccccccccc hh hh ooooooooo 11
run run 1111111111 ccccccccc hh hh ooooooooo 11
run run 11 cc hh hh oo oo 11
run run 11 cc hh hh oo oo 11
run run 11 cc hhhhhhhhhhhh oo oo 11
run run 11 cc hhhhhhhhhhhh oo oo 11
run run 11 cc hh hh oo oo 11
run run 11 cc hh hh oo oo 11
run run 11 cc hh hh oo oo 11
run run 1111111111 ccccccccc hh hh ooooooooo 111111111111
run run 1111111111 ccccccccc hh hh ooooooooo 111111111111

0
oooooo000000000000000000000000 44 9999999999 77777777777777
oo000000000000000000000000 111 444 99999999999999 777777777777
oo oo 00 ss 11 1111 4444 99 99 77 77
oo oo 00 ss 11 11 44 44 99 99 77 77
oo oo 00 ss 11 11 44 44 99 99 77 77
oo oo 00 ss 11 11 44 44 99 99 77 77
oo oo 00 ss 11 11 444444444444 99 99 77 77
oo oo 00 ss 11 11 444444444444 99 99 77 77
oo oo 00 ss 11 11 11111111 44 99999999999999 77 77
oo oo 00 ss 11 11 11111111 44 99999999999999 77 77

0
11 9999999999 44 6666666666 2222222222 44
111 999999999999 444 666666666666 222222222222 444
1111 99 99 111 4444 66 22 22 4444
11 99 99 111 44 44 66 22 22 44 44
11 99 99 111 44 44 66 22 22 44 44
11 99999999999999 44 44 666666666666 22 22 44 44
11 99999999999999 44 44 666666666666 22 22 44 44
11 44444444444444 66 66 111 22 444444444444
11 44444444444444 66 66 111 22 444444444444
11 11 66 66 111 22 44
11111111 999999999999 44 666666666666 222222222222 64
11111111 999999999999 44 666666666666 222222222222 64

0
ccccccccc aa 11
ccccccccc aa 11
ss ss cc aa aa 11
ss cc aa aa 11
ss cc aa aa 11
cc ##### 11
cc ##### 11
ss cc aa aa 11
ss cc aa aa 11
ccccccccc aa 111111111111
ccccccccc aa 111111111111

.....
program verification information
code system: scale version: 4.3
.....
Program: sas2
creation date: 03/07/97
library: /opt/nout/Scaled.3/bin
.....
this is not a scale configuration controlled code
jobname: nichol
date of execution: 08/14/97
time of execution: 19:46:24
.....

1
0
0
0
0

nuclide	initial	1E-18 d	basis =single reactor assembly			
gd155	4.39E+02	4.39E+02				
total	1.97E+04	1.97E+04				
nuclide concentrations, grams						
basis =single reactor assembly						
u234	2.29E+02	2.29E+02				
u235	2.58E+04	2.58E+04				
u238	1.15E+02	1.15E+02				
u238	8.55E+05	8.55E+05				
total	8.81E+05	8.81E+05				
basis =						
	initial	2.4 d	4.8 d	7.1 d	9.5 d	9.5 d
	initial	2.4 d	4.8 d	7.1 d	9.5 d	9.5 d
basis = single reactor assembly						
charge	2.4 d	4.8 d	7.1 d	9.5 d	9.5 d	
charge	2.4 d	4.8 d	7.1 d	9.5 d	9.5 d	
charge	2.4 d	4.8 d	7.1 d	9.5 d	9.5 d	
sa147	.00E+00	1.05E-22	3.94E-22	6.37E-22	1.42E-21	1.42E-21
sa149	.00E+00	3.08E-12	5.30E-12	7.40E-12	8.90E-12	8.90E-12
sa150	.00E+00	1.63E-11	3.37E-11	5.13E-11	6.94E-11	6.94E-11
sa151	.00E+00	3.31E-10	6.54E-10	9.67E-10	1.27E-09	1.27E-09
sa152	.00E+00	3.51E-10	7.07E-10	1.07E-09	1.44E-09	1.44E-09
eu151	.00E+00	1.71E-12	3.48E-12	5.04E-12	6.70E-12	6.70E-12
eu153	.00E+00	4.15E-08	1.67E-07	3.74E-07	6.42E-07	6.42E-07
gd155m	.00E+00	4.15E-12	4.10E-12	4.09E-12	4.07E-12	4.07E-12
gd155	2.83E+00	2.82E+00	2.81E+00	2.80E+00	2.78E+00	2.78E+00
totals	6.95E+03	6.95E+03	6.95E+03	6.95E+03	6.95E+03	6.95E+03
basis = single reactor assembly						
charge	2.4 d	4.8 d	7.1 d	9.5 d	9.5 d	
u233	.00E+00	1.88E-08	3.75E-08	5.62E-08	7.48E-08	7.48E-08
u234	9.79E-01	9.79E-01	9.79E-01	9.77E-01	9.77E-01	9.77E-01
u235	1.10E+02	1.10E+02	1.09E+02	1.09E+02	1.09E+02	1.09E+02
u236	4.85E-01	4.85E-01	4.84E-01	4.84E-01	4.80E-01	4.80E-01
u238	3.59E+03	3.59E+03	3.59E+03	3.59E+03	3.59E+03	3.59E+03
rp237	.00E+00	6.83E-05	2.54E-04	5.35E-04	8.90E-04	8.90E-04
pu236	.00E+00	3.34E-14	3.93E-13	1.53E-12	3.66E-12	3.66E-12
pu238	.00E+00	4.79E-09	6.22E-08	2.64E-07	7.09E-07	7.09E-07
pu239	.00E+00	4.79E-09	6.22E-08	2.64E-07	7.09E-07	7.09E-07
pu239	.00E+00	2.54E-02	8.38E-02	1.55E-01	2.41E-01	2.41E-01
pu240	.00E+00	4.30E-05	2.13E-04	5.43E-04	1.05E-03	1.05E-03
pu241	.00E+00	9.70E-08	9.40E-07	3.58E-06	9.24E-06	9.24E-06
pu242	.00E+00	3.48E-11	6.63E-10	3.77E-09	1.30E-08	1.30E-08
basis = single reactor assembly						
charge	2.4 d	4.8 d	7.1 d	9.5 d	9.5 d	
sa241	.00E+00	7.35E-12	1.38E-10	7.85E-10	2.70E-09	2.70E-09
sa242m	.00E+00	8.58E-16	3.20E-14	2.70E-13	1.23E-12	1.23E-12
sa243	.00E+00	6.15E-15	2.35E-13	2.05E-12	9.53E-12	9.54E-12
totals	3.70E+03	3.70E+03	3.70E+03	3.70E+03	3.70E+03	3.70E+03
decay data, including gamma and total energy, are from endf/b-vi						
1997 total number of nuclides in library						
nuclide concentrations, grams						
basis =single reactor assembly						
sa150	2.05E-06	2.06E-06	2.06E-06	2.06E-06	2.06E-06	2.06E-06
sa152	1.28E-05	1.28E-05	1.29E-05	1.29E-05	1.30E-05	1.31E-05
eu153	7.37E-01	8.25E-01	8.60E-01	8.74E-01	8.79E-01	8.81E-01
nuclide concentrations, grams						
basis =single reactor assembly						
gd155	1.86E+01	1.90E+01	1.93E+01	1.96E+01	1.99E+01	2.01E+01
total	1.97E+04	1.97E+04	1.97E+04	1.97E+04	1.97E+04	1.97E+04
nuclide concentrations, grams						
basis =single reactor assembly						
u233	1.36E-03	1.47E-03	1.57E-03	1.68E-03	1.78E-03	1.89E-03
u234	1.31E-02	1.32E-02	1.33E-02	1.35E-02	1.36E-02	1.37E-02
u235	4.49E+03	4.50E+03	4.50E+03	4.50E+03	4.50E+03	4.50E+03
u236	3.51E+03	3.51E+03	3.51E+03	3.51E+03	3.51E+03	3.51E+03
u238	8.34E+05	8.34E+05	8.34E+05	8.34E+05	8.34E+05	8.34E+05
rp237	3.28E+02	3.30E+02	3.31E+02	3.33E+02	3.35E+02	3.37E+02
pu236	3.08E-04	2.50E-04	2.02E-04	1.63E-04	1.33E-04	1.06E-04
pu238	1.44E-02	1.56E-02	1.58E-02	1.57E-02	1.56E-02	1.54E-02
pu239	1.44E-02	1.56E-02	1.58E-02	1.57E-02	1.56E-02	1.54E-02
pu239	3.54E+03	3.57E+03	3.57E+03	3.57E+03	3.57E+03	3.57E+03
pu240	2.08E+03	2.08E+03	2.08E+03	2.08E+03	2.08E+03	2.08E+03
pu241	8.34E-02	7.99E-02	7.65E-02	7.33E-02	7.02E-02	6.72E-02
pu242	4.91E-02	4.91E-02	4.91E-02	4.91E-02	4.91E-02	4.91E-02
sa241	9.43E-01	1.10E+02	1.63E+02	1.95E+02	2.26E+02	2.53E+02
sa242m	1.68E-00	1.67E+00	1.67E+00	1.66E+00	1.63E+00	1.64E+00
sa243	9.41E-01	9.62E+01	9.42E+01	9.62E+01	9.62E+01	9.61E+01
total	8.50E+05	8.50E+05	8.50E+05	8.50E+05	8.50E+05	8.50E+05
element concentrations, grams						
nuclide concentrations, grams						
basis =single reactor assembly						
mo 95	6.56E+02	6.64E+02	6.85E+02	6.85E+02	6.85E+02	6.85E+02
tc 95	7.21E+02	7.22E+02	7.22E+02	7.22E+02	7.22E+02	7.22E+02
nuclide concentrations, grams						
basis =single reactor assembly						
ru101	4.97E+02	4.97E+02	4.97E+02	4.97E+02	4.97E+02	4.97E+02
rh103	4.60E+02	4.13E+02	4.13E+02	4.13E+02	4.13E+02	4.13E+02
sg109	8.12E+01	8.12E+01	8.12E+01	8.12E+01	8.12E+01	8.12E+01
nuclide concentrations, grams						
basis =single reactor assembly						
rd143	6.44E+02	6.51E+02	6.51E+02	6.51E+02	6.51E+02	6.51E+02
rd145	6.05E+02	6.05E+02	6.05E+02	6.05E+02	6.05E+02	6.05E+02
sa147	1.57E+02	1.76E+02	1.91E+02	2.03E+02	2.12E+02	2.20E+02
sa149	1.01E+00	1.36E+00	2.16E+00	1.36E+00	1.36E+00	1.36E+00
sa150	2.41E+02	2.41E+02	2.41E+02	2.41E+02	2.41E+02	2.41E+02
sa151	8.81E+00	8.81E+00	8.77E+00	8.71E+00	8.65E+00	8.59E+00
eu151	2.25E+02	8.33E+02	1.44E+01	2.04E+01	2.63E+01	3.23E+01
sa152	1.22E+02	1.22E+02	1.22E+02	1.22E+02	1.22E+02	1.22E+02
eu153	1.05E+02	1.06E+02	1.06E+02	1.06E+02	1.06E+02	1.06E+02
nuclide concentrations, grams						
basis =single reactor assembly						
gd155	6.88E+02	6.51E+01	1.18E+00	1.61E+00	2.01E+00	2.35E+00
total	3.07E+04	3.07E+04	3.07E+04	3.07E+04	3.07E+04	3.07E+04

coop2974b.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....
1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Cooper BWR Sample ABB2974-B, Weight 55.723 gm from top, Aug 97
:
: mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.32 1 840
  92234 0.024 92235 2.93 92236 0.013 92238 97.031 end
kr-83 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-87 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
sr-93 1 0 1-20 840 end
sr-94 1 0 1-20 840 end
sr-95 1 0 1-20 840 end
nb-96 1 0 1-20 840 end
mo-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-104 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
ag-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
sr-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
cs-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sm-147 1 0 1-20 840 end
sm-149 1 0 1-20 840 end
sm-150 1 0 1-20 840 end
sm-151 1 0 1-20 840 end
sm-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
gd-155 1 0 1-20 840 end
:
: xirc2 2 1 620 end
:
:
h2o 3 den=0.240 1 557 end
n 4 0 3-5 557 end
:
arbm-xirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 30000 1.40
  40000 98.18 5 1.0 557 end
:
uo2 6 den=10.32 1 840
  92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
arbm-gdrod 10.32 2 0 1.0 8016 3 64000 3 6 0.034 840 end
:
h2o 7 den=0.862 1 557 end
:
-----
end comp
:
:
: fuel-pin-cell geometry:
squarespitch 1.87 1.21 1 3 1.43 2 1.242 0 end
:
:
: assembly and cycle parameters:
:
rpin/asm=49 fuelight=1719.74 nycycles=17 nlib/cyc=2
printlevel=5 implevel=2 sumtotal=8 end
6 0.4050 4 0.4210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5 3.4223 7 3.7883
power=8.763 burn=19 down=6 end
power=10.431 burn=130 down=17 end
power=13.097 burn=41 down=10 end
power=10.221 burn=226 down=35 end
power=11.235 burn=39 down=7 end
power=12.749 burn=22 down=12 end
power=11.965 burn=108 down=19 end
power=12.398 burn=116 down=39 end
power=10.137 burn=79 down=8 end
power=11.215 burn=64 down=5 end
power=9.444 burn=150 down=31 end
power=9.503 burn=164 down=799 end
power=5.866 burn=160 down=9 end
power=6.083 burn=148 down=48 end

```


coop2974j.sum

```

.....
:          SCALR4.J Bulletin Board
:          -----
:          Welcome to SCALR-4.J.
:          .....
1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Cooper BWR Sample ADD2974-J, Weight 115.042 gm from top, Aug 97
:
: mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.32 1 840
  92234 0.024 92235 2.93 92236 0.013 92238 97.031 end
kr-81 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
sr-93 1 0 1-20 840 end
sr-94 1 0 1-20 840 end
sr-95 1 0 1-20 840 end
nb-94 1 0 1-20 840 end
mo-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-106 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
sg-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
xe-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
cs-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
ia-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ca-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pa-147 1 0 1-20 840 end
pa-148 1 0 1-20 840 end
sm-147 1 0 1-20 840 end
sm-149 1 0 1-20 840 end
sm-150 1 0 1-20 840 end
sm-151 1 0 1-20 840 end
sm-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
pd-155 1 0 1-20 840 end
sirc2 2 1 620 end
:
:
h2o 3 den=0.306 1 557 end
n 4 0 5-5 557 end
arbm-sirc4 6.54 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 5 1.0 557 end
uo2 6 den=10.32 1 840
  92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end
h2o 7 den=0.842 1 557 end
:
: -----
: fuel-pin-cell geometry:
squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end
:
: -----
: assembly and cycle parameters:
rpin/sasm=49 fuelight=1719.74 nrcycles=17 nlib/cyc=2
printlevel=3 implevel=2 numtotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0530 500 3.3028 3 3.3179 5 3.4223 7 3.7883
power=14.257 burn=19 down=8 end
power=17.091 burn=130 down=17 end
power=21.459 burn=41 down=10 end
power=16.747 burn=226 down=15 end
power=18.409 burn=39 down=7 end
power=20.888 burn=22 down=12 end
power=19.603 burn=108 down=19 end
power=20.314 burn=114 down=59 end
power=18.642 burn=79 down=8 end
power=18.409 burn=64 down=5 end
power=15.473 burn=150 down=31 end
power=15.370 burn=164 down=799 end
power=9.611 burn=160 down=9 end
power=9.967 burn=148 down=48 end

```


power=9.184 burn=96 down=61 and
power=9.669 burn=129 down=3 and
power=8.582 burn=37 down=1934.09 and

```

1 00000000 00000000 00000000 2222222222 hh hh
00000000 00000000 00000000 2222222222 hh hh
ss ss aa aa ss ss 22 22 hh hh
ss ss aa aa ss ss 22 22 hh hh
ss ss aa aa ss ss 22 22 hh hh
00000000 00000000 00000000 22 hhhhhhhhhhh
00000000 00000000 00000000 22 hhhhhhhhhhh
ss ss aa aa ss ss 22 hh hh
ss ss aa aa ss ss 22 hh hh
ss ss aa aa ss ss 22 hh hh
00000000 00000000 00000000 2222222222 hh hh
00000000 00000000 00000000 2222222222 hh hh

run run 1111111111 eeeeeeeeee hh hh 0000000000 11
run run 1111111111 eeeeeeeeee hh hh 0000000000 11
run run 11 11 ee ee hh hh 00 00 11
run run 11 11 ee ee hh hh 00 00 11
run run 11 11 ee ee hh hh 00 00 11
run run 11 11 ee ee hhhhhhhhhhh 00 00 11
run run 11 11 ee ee hhhhhhhhhhh 00 00 11
run run 11 11 ee ee hh hh 00 00 11
run run 11 11 ee ee hh hh 00 00 11
run run 11 11 ee ee hh hh 00 00 11
run run 1111111111 eeeeeeeeee hh hh 0000000000 1111111111
run run 1111111111 eeeeeeeeee hh hh 0000000000 1111111111

00000000 00000000 11 44 9999999999 777777777777
00000000 00000000 111 444 9999999999 777777777777
00 00 88 88 111 4444 99 99 77 77
00 00 88 88 11 44 44 99 99 77 77
00 00 88 88 11 44 44 99 99 77 77
00 00 88 88 11 44 44 99 99 77 77
00 00 88 88 11 44 44 99 99 77 77
00 00 88 88 11 444444444444 99 99 77 77
00 00 88 88 11 444444444444 99 99 77 77
00000000 00000000 11111111 44 9999999999 77
00000000 00000000 11111111 44 9999999999 77

2222222222 11 2222222222 11 00000000 44
2222222222 111 2222222222 111 00000000 444
22 22 1111 111 22 1111 00 00 4444
22 22 11 11 22 11 00 00 44 44
22 22 11 11 22 11 00 00 44 44
22 22 11 11 22 11 00 00 44 44
22 22 11 11 22 11 00 00 44 44
22 22 11 11 22 11 00 00 44 44
22 22 11 11 22 11 00 00 444444444444
222222222222 11111111 222222222222 11111111 00000000 44
222222222222 11111111 222222222222 11111111 00000000 44

1 00000000 00000000 00000000 11 00000000
00000000 00000000 00000000 11 00000000
ss ss cc cc aa aa 11 00
ss ss cc cc aa aa 11 00
ss ss cc cc aa aa 11 00
ss ss cc cc aa aa 11 00
00000000 00000000 00000000 11 00000000
00000000 00000000 00000000 11 00000000
ss ss cc cc aa aa 1111111111 00000000
ss ss cc cc aa aa 1111111111 00000000

```

```

.....
.....
.....
program verification information
.....
code system: scale version: 4.3
.....
.....
program: sas2
creation date: 03/07/97
library: /opt/neut/Scale4.3/bin
.....
this is not a scale configuration controlled code
.....
jobname: nichol
.....
date of execution: 08/14/97
.....
time of execution: 21:21:04
.....
.....
.....

```

1
0
0
0
0

nuclide concentrations, grams

coop2974u.sum

```
.....
:
:           SCALE-1.3 Bulletin Board
:           -----
:           Welcome to SCALE-1.3.
:
:
:-----
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Cooper BWR Sample ADD2974-U, Height 291.087 cm from top, Aug 97
:
:
:   mixtures of fuel-pin-unit-cell:
:
44group latticecell
uo2 1 den=10.32 1 840
    92234 0.024 92235 2.93 92236 0.013 92238 97.031 end
kr-83 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
sr-93 1 0 1-20 840 end
sr-94 1 0 1-20 840 end
sr-95 1 0 1-20 840 end
sb-96 1 0 1-20 840 end
so-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-106 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
ag-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
xe-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
cs-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sa-147 1 0 1-20 840 end
sa-149 1 0 1-20 840 end
sa-150 1 0 1-20 840 end
sa-151 1 0 1-20 840 end
sa-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
gd-155 1 0 1-20 840 end

zirc2 2 1 620 end
:
:
h2o 3 den=0.652 1 557 end
n 4 0 5-5 557 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 30000 1.40
         40000 98.18 5 1.0 557 end
uo2 6 den=10.32 1 840
    92234 0.024 92235 2.732 92236 0.013 92238 97.211 end
arbm-gdrod 10.32 2 0 1.0 8016 3 64000 2 6 0.034 840 end
h2o 7 den=0.862 1 557 end
:
:-----
:   end comp
:
:-----
:   fuel-pin-cell geometry:
squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end
:
:-----
:   assembly and cycle parameters:
rpin/asm=49 fuelght=1719.74 ncycles=17 nlib/cyc=2
printlevel=5 implevel=2 numtotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5 3.4223 7 3.7883
power=15.246 burn=19 down=8 end
power=18.149 burn=130 down=17 end
power=22.788 burn=41 down=10 end
power=17.784 burn=226 down=15 end
power=19.549 burn=39 down=7 end
power=22.182 burn=22 down=12 end
power=20.817 burn=108 down=19 end
power=21.572 burn=114 down=59 end
power=17.673 burn=73 down=8 end
power=19.549 burn=64 down=5 end
power=16.411 burn=150 down=31 end
power=16.534 burn=164 down=799 end
power=10.206 burn=160 down=9 end
power=10.584 burn=148 down=48 end
```


2966tplus100deg.sum

```

.....
SCALE-4.3 Bulletin Board
.....
Welcome to SCALE-4.3.
.....
1 Primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
Cooper BWR Sample ADD2966-T, Weight 274.777 gm from top, Aug 97
.
. 100 X increase in fuel temperature
. mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.32 1 940
92234 0.026 92235 2.93 92236 0.013 92238 97.031 end
kr-83 1 0 1-20 940 end
kr-85 1 0 1-20 940 end
yr-89 1 0 1-20 940 end
sr-90 1 0 1-20 940 end
sr-93 1 0 1-20 940 end
sr-96 1 0 1-20 940 end
sr-95 1 0 1-20 940 end
nb-94 1 0 1-20 940 end
mo-95 1 0 1-20 940 end
tc-99 1 0 1-20 940 end
ru-101 1 0 1-20 940 end
ru-104 1 0 1-20 940 end
rh-103 1 0 1-20 940 end
rh-105 1 0 1-20 940 end
pd-105 1 0 1-20 940 end
pd-108 1 0 1-20 940 end
ag-109 1 0 1-20 940 end
sb-124 1 0 1-20 940 end
xe-131 1 0 1-20 940 end
xe-132 1 0 1-20 940 end
xe-135 1 0 1-20 940 end
xe-136 1 0 1-20 940 end
cs-134 1 0 1-20 940 end
cs-135 1 0 1-20 940 end
cs-137 1 0 1-20 940 end
ba-136 1 0 1-20 940 end
la-139 1 0 1-20 940 end
pr-141 1 0 1-20 940 end
pr-143 1 0 1-20 940 end
ce-144 1 0 1-20 940 end
nd-143 1 0 1-20 940 end
nd-145 1 0 1-20 940 end
nd-147 1 0 1-20 940 end
pm-147 1 0 1-20 940 end
pm-148 1 0 1-20 940 end
sm-147 1 0 1-20 940 end
sm-149 1 0 1-20 940 end
sm-150 1 0 1-20 940 end
sm-151 1 0 1-20 940 end
sm-152 1 0 1-20 940 end
eu-153 1 0 1-20 940 end
eu-154 1 0 1-20 940 end
eu-155 1 0 1-20 940 end
qd-155 1 0 1-20 940 end
zirc2 2 1 620 end
.
.
h2o 3 den=0.607 1 557 end
n 4 0 3-3 557 end
arbm-zirc4 6.56 5 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 5 1.0 557 end
uo2 6 den=10.32 1 940
92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
arbm-gdrod 10.32 2 0 1 0 8016 3 44000 2 4 0.034 940 end
h2o 7 den=0.862 1 557 end
.
.
end comp
.
.
fuel-pin-cell geometry:
squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end
.
.
assembly and cycle parameters:
spin/asam=49 fuelight=1719.74 ncycles=17 nlib/cycle=2
princlevel=3 implevel=2 sumtotal=8 end
6 0.4050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5 3.4223 7 3.7883
power=16.671 burn=19 down=8 end
power=19.845 burn=130 down=17 end
power=24.917 burn=41 down=10 end
power=19.445 burn=226 down=35 end
power=21.375 burn=39 down=7 end
power=24.254 burn=22 down=12 end
power=22.762 burn=108 down=19 end
power=22.587 burn=114 down=39 end
power=19.224 burn=79 down=8 end
power=21.375 burn=64 down=5 end
power=17.966 burn=150 down=31 end
power=18.078 burn=164 down=799 end
power=11.160 burn=160 down=9 end
power=11.573 burn=148 down=48 end

```


2966tplus10den.sum

```

.....
:          SCALE4.3 Bulletin Board
:          -----
:          Welcome to SCALE-4.3.
:          .....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
  Cooper BWR Sample AAD2966-T, Height 274.777 cm from top, Aug 97
:
:  increase moderator density by 10%
:  mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.32 1 840
  92234 0.024 92235 2.93 92236 0.013 92238 97.031 end
hr-83 1 0 1-20 840 end
hr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
sr-93 1 0 1-20 840 end
sr-94 1 0 1-20 840 end
sr-95 1 0 1-20 840 end
rb-94 1 0 1-20 840 end
so-95 1 0 1-20 840 end
sc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-104 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
sg-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
se-131 1 0 1-20 840 end
se-132 1 0 1-20 840 end
se-135 1 0 1-20 840 end
se-136 1 0 1-20 840 end
cs-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sm-147 1 0 1-20 840 end
sm-149 1 0 1-20 840 end
sm-150 1 0 1-20 840 end
sm-151 1 0 1-20 840 end
sm-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
gd-155 1 0 1-20 840 end
:
:  sirc2 2 1 620 end
:
:
h2o 3 den=0.668 1 557 end
n 4 0 5-5 557 end
arbm-sirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 5 1.0 557 end
uo2 6 den=10.32 1 840
  92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
arbm-gdrod 10.32 2 0 1 0 8016 3 64000 2 6 0.034 840 end
h2o 7 den=0.862 1 557 end
:
-----
:  end comp
:
:  fuel-pin-cell geometry:
squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end
:
-----
:  assembly and cycle parameters:
rpin/asm=49 fuelight=1719.74 ncycles=17 nlib/cyc=2
printlevel=5 implevel=2 sumtotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5 3.4223 7 3.7883
power=16.671 burn=19 down=8 end
power=19.845 burn=130 down=17 end
power=24.917 burn=41 down=10 end
power=19.445 burn=226 down=35 end
power=21.375 burn=39 down=7 end
power=24.234 burn=22 down=12 end
power=22.742 burn=108 down=19 end
power=23.587 burn=114 down=59 end
power=19.324 burn=79 down=8 end
power=21.375 burn=64 down=5 end
power=17.966 burn=130 down=31 end
power=18.078 burn=164 down=799 end
power=11.160 burn=160 down=9 end
power=11.573 burn=148 down=48 end

```


2974bplus100deg.sum

```

.....
SCALE4.3 Bulletin Board
.....
Welcome to SCALE-4.3.
.....
1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Cooper BWR Sample ADD2974-B, Weight 55.723 gm from top, Aug 97
  : increase fuel temperature 100 K
  : mixtures of fuel-pin-unit-cell:
44group latticecell
uo3 1 den=10.32 1 940
  92234 0.026 92235 2.93 92236 0.013 92238 97.031 end
xr-83 1 0 1-20 940 end
xr-85 1 0 1-20 940 end
yr-89 1 0 1-20 940 end
sr-90 1 0 1-20 940 end
sr-93 1 0 1-20 940 end
sr-94 1 0 1-20 940 end
sr-95 1 0 1-20 940 end
rb-94 1 0 1-20 940 end
mo-95 1 0 1-20 940 end
tc-95 1 0 1-20 940 end
ru-101 1 0 1-20 940 end
ru-104 1 0 1-20 940 end
rh-103 1 0 1-20 940 end
rh-105 1 0 1-20 940 end
pd-105 1 0 1-20 940 end
pd-108 1 0 1-20 940 end
ag-109 1 0 1-20 940 end
ab-124 1 0 1-20 940 end
xe-131 1 0 1-20 940 end
xe-132 1 0 1-20 940 end
xe-135 1 0 1-20 940 end
xe-136 1 0 1-20 940 end
ca-134 1 0 1-20 940 end
ca-135 1 0 1-20 940 end
ca-137 1 0 1-20 940 end
ba-136 1 0 1-20 940 end
la-139 1 0 1-20 940 end
pr-141 1 0 1-20 940 end
pr-143 1 0 1-20 940 end
ca-144 1 0 1-20 940 end
nd-143 1 0 1-20 940 end
nd-145 1 0 1-20 940 end
nd-147 1 0 1-20 940 end
pm-147 1 0 1-20 940 end
pm-148 1 0 1-20 940 end
am-147 1 0 1-20 940 end
am-149 1 0 1-20 940 end
am-150 1 0 1-20 940 end
am-151 1 0 1-20 940 end
am-152 1 0 1-20 940 end
eu-153 1 0 1-20 940 end
eu-154 1 0 1-20 940 end
eu-155 1 0 1-20 940 end
qd-155 1 0 1-20 940 end

zirc2 2 1 620 end
.
.
h2o 3 den=0.240 1 557 end
n 4 0 5-5 557 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 30000 1.40
  40000 98.18 5 1.0 557 end
uo2 6 den=10.32 1 940
  92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
arbm-gdred 10.32 2 0 1 0 8016 3 64000 2 6 0.034 940 end
h2o 7 den=0.862 1 557 end
.....
end comp
.....
fuel-pin-cell geometry:
squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end
.....
assembly and cycle parameters:
mpin/asm=49 fuelight=1919.74 nycycles=17 nlib/cyc=2
printlevel=5 implevel=2 numtotal=8 end
$ 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5 3.4223 7 3.7883
power=8.763 burn=19 down=1 end
power=10.431 burn=130 down=17 end
power=13.097 burn=41 down=10 end
power=10.221 burn=226 down=35 end
power=11.235 burn=39 down=7 end
power=12.749 burn=22 down=12 end
power=11.963 burn=108 down=19 end
power=12.398 burn=114 down=39 end
power=10.157 burn=79 down=8 end
power=11.235 burn=64 down=5 end
power=9.444 burn=150 down=31 end
power=9.503 burn=164 down=799 end
power=5.866 burn=160 down=9 end
power=6.083 burn=148 down=48 end

```


2974bplus50den.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....
1 primary module across and input record ( scale driver - 95/03/29 - 09:06:37 )
- module saszh will be called
Cooper SWR Sample ADC2974-B, Weight 55.733 gm from top, Aug 97
: increase moderator density by 50%
: mixtures of fuel-pin-unit-cell:
44group latticecell
uo3 1 den=10.32 1 840
92234 0.024 92235 2.93 92236 0.013 92238 97.031 end
kr-83 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
sr-93 1 0 1-20 840 end
sr-94 1 0 1-20 840 end
sr-95 1 0 1-20 840 end
rb-94 1 0 1-20 840 end
mo-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-106 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
eg-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
xe-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
ca-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-138 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sm-147 1 0 1-20 840 end
sm-149 1 0 1-20 840 end
sm-150 1 0 1-20 840 end
sm-151 1 0 1-20 840 end
sm-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
qd-155 1 0 1-20 840 end
sirc2 2 1 620 end
.
.
h2o 3 den=0.36 1 557 end
n 4 0 5-5 557 end
arbm-sirc4 6.56 5 0 0 0 8016 0.12 26000 0.10 26000 0.20 50000 1.40
40000 98.18 5 1.0 557 end
uo3 6 den=10.32 1 840
92234 0.024 92235 2.732 92236 0.013 92238 97.231 end
arbm-gdrod 10.32 2 0 1.0 8016 3 64000 2 6 0.034 840 end
h2o 7 den=0.862 1 557 end
.
.
end comp
.
.
fuel-pin-cell geometry:
squarepitch 1.87 1.21 1 3 1.43 2 1.242 0 end
.
.
assembly and cycle parameters:
rpin/asm=49 fuelght=1719.74 ncycles=17 nlib/cyc=2
printlevel=3 impllevel=2 numtotal=8 end
6 0.6050 4 0.6210 2 0.7150 3 1.0550 500 3.3028 3 3.3179 5 3.4223 7 3.7883
power=8.763 burn=19 down=8 end
power=10.431 burn=130 down=17 end
power=13.097 burn=41 down=10 end
power=10.221 burn=226 down=35 end
power=11.235 burn=39 down=7 end
power=12.749 burn=22 down=12 end
power=11.965 burn=108 down=19 end
power=12.398 burn=114 down=59 end
power=10.157 burn=79 down=8 end
power=11.235 burn=64 down=5 end
power=9.444 burn=150 down=31 end
power=9.503 burn=164 down=799 end
power=5.866 burn=160 down=9 end
power=6.083 burn=148 down=48 end

```


basis =single reactor assembly			
	initial	1E-18 d	
gd155	4.39E-02	4.39E-02	
total	1.97E-04	1.97E-04	
nuclide concentrations, grams			
basis =single reactor assembly			
	initial	1E-18 d	
u234	2.29E-02	2.29E-02	
u235	2.58E-04	2.58E-04	
u236	1.15E-02	1.15E-02	
u238	8.55E-05	8.55E-05	
total	8.81E-05	8.81E-05	
basis =			
	initial	2.4 d	4.8 d
	initial	2.4 d	4.8 d
basis = single reactor assembly			
	charge	2.4 d	4.8 d
	charge	2.4 d	4.8 d
	charge	2.4 d	4.8 d
sa147	.00E+00	4.22E-23	3.61E-22
sa149	.00E+00	2.09E-12	3.94E-12
sa150	.00E+00	1.03E-11	2.09E-11
sa151	.00E+00	2.11E-10	4.20E-10
sa152	.00E+00	2.22E-10	4.46E-10
su151	.00E+00	1.06E-12	2.13E-12
su153	.00E+00	2.75E-08	1.10E-07
gd155m	.00E+00	2.92E-12	2.92E-12
gd155	2.83E+00	2.83E+00	2.83E+00
totals	6.95E+03	6.95E+03	6.95E+03
basis = single reactor assembly			
	charge	2.4 d	4.8 d
	charge	2.4 d	4.8 d
	charge	2.4 d	4.8 d
u233	.00E+00	1.14E-08	2.28E-08
u234	9.79E-01	9.79E-01	9.78E-01
u235	1.30E-02	1.30E-02	1.30E-02
u236	4.85E-01	4.85E-01	4.84E-01
u238	3.59E-01	3.59E-01	3.59E-01
np237	.00E+00	4.20E-05	1.56E-04
pu236	.00E+00	1.25E-14	1.46E-13
pu238	.00E+00	1.74E-09	2.26E-08
pu239	.00E+00	1.74E-09	2.26E-08
pu239	.00E+00	1.52E-02	5.04E-02
pu240	.00E+00	1.55E-05	7.41E-05
pu241	.00E+00	2.22E-08	2.09E-07
pu242	.00E+00	4.22E-12	7.82E-11
basis = single reactor assembly			
	charge	2.4 d	4.8 d
	charge	2.4 d	4.8 d
	charge	2.4 d	4.8 d
am241	.00E+00	1.68E-12	3.11E-11
am242m	.00E+00	1.13E-16	4.12E-15
am243	.00E+00	4.81E-16	1.79E-14
totals	3.70E+03	3.70E+03	3.70E+03
decay data, including gamma and total energy, are from endf/b-vi			
1697 total number of nuclides in library			
nuclide concentrations, grams			
basis =single reactor assembly			
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
am150	1.34E-06	1.34E-06	1.34E-06
am152	1.22E-05	1.22E-05	1.22E-05
su153	6.06E-01	6.58E-01	6.78E-01
nuclide concentrations, grams			
basis =single reactor assembly			
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
gd155	3.00E-01	3.02E-01	3.04E-01
total	1.97E-04	1.97E-04	1.97E-04
nuclide concentrations, grams			
basis =single reactor assembly			
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
u233	1.30E-03	1.35E-03	1.41E-03
u234	1.70E-02	1.71E-02	1.71E-02
u235	1.22E-04	1.22E-04	1.22E-04
u236	2.51E-03	2.51E-03	2.51E-03
u238	8.44E-05	8.44E-05	8.44E-05
np237	1.67E-02	1.69E-02	1.69E-02
pu236	7.92E-05	6.41E-05	5.18E-05
pu238	4.24E-01	4.57E-01	4.63E-01
pu238	4.24E-01	4.57E-01	4.63E-01
pu239	3.93E-03	3.93E-03	3.93E-03
pu240	1.16E-03	1.16E-03	1.16E-03
pu241	4.71E-02	4.32E-02	4.32E-02
pu242	1.03E-02	1.03E-02	1.03E-02
am241	7.07E-01	9.05E-01	1.09E-02
am242m	1.28E-00	1.28E-00	1.27E-00
am243	1.27E-01	1.27E-01	1.27E-01
total	8.65E+05	8.65E+05	8.65E+05
nuclide concentrations, grams			
basis =single reactor assembly			
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
mo 95	3.68E-02	3.84E-02	3.85E-02
tc 99	4.02E-02	4.02E-02	4.02E-02
nuclide concentrations, grams			
basis =single reactor assembly			
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
ru101	3.69E-02	3.69E-02	3.69E-02
rh103	2.43E-02	2.43E-02	2.43E-02
ag109	3.37E-01	3.37E-01	3.37E-01
nuclide concentrations, grams			
basis =single reactor assembly			
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
nd143	4.37E-02	4.61E-02	4.61E-02
nd145	3.49E-02	3.49E-02	3.49E-02
sa147	1.09E-02	1.21E-02	1.31E-02
sa149	1.39E-00	1.54E-00	1.54E-00
sa150	1.22E-02	1.22E-02	1.22E-02
sa151	9.04E-00	9.04E-00	8.95E-00
su151	7.51E-02	1.37E-01	1.93E-01
sa152	6.62E-01	6.62E-01	6.62E-01
su153	4.39E-01	4.40E-01	4.40E-01
nuclide concentrations, grams			
basis =single reactor assembly			
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
	initial	325.7 d	651.4 d
gd155	4.67E-02	2.69E-01	4.66E-01
total	1.62E+04	1.62E+04	1.62E+04