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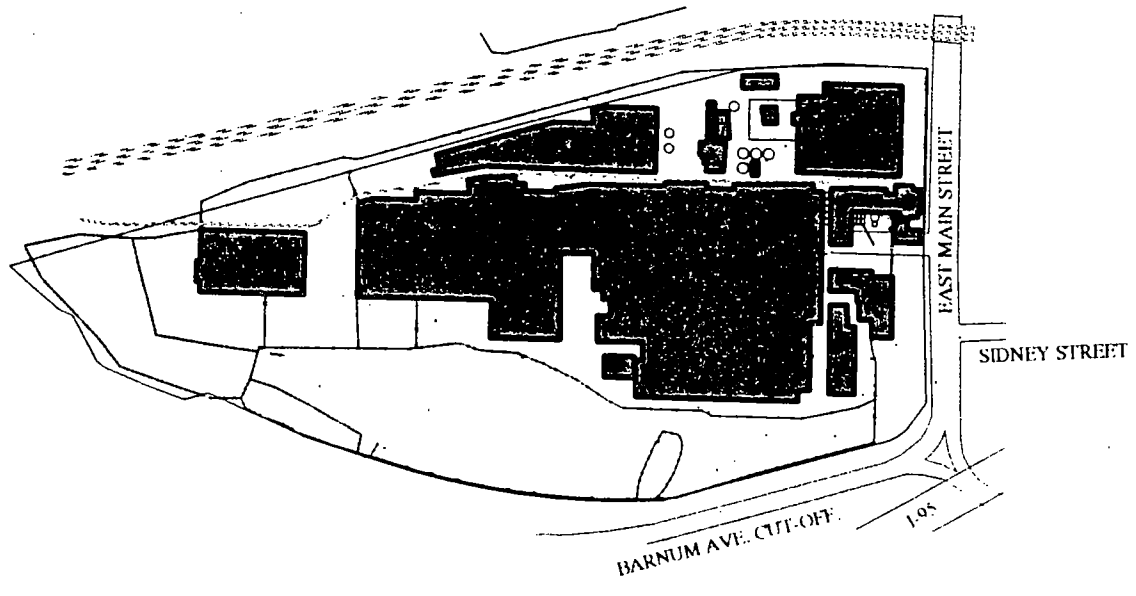
Submission to
U.S. Environmental Protection Agency
Region I
Boston, Massachusetts

RCRA SECTION 3013 ORDER
RAYMARK INDUSTRIES, INC.
Stratford, Connecticut
Docket No. 87-1057



SDMS DocID 464976

Volume III: Appendix E



February 10, 1995



ENVIRONMENTAL LABORATORIES, INC.

A member of The EICON Group, Inc.

142 Temple Street, New Haven, CT 06510 (203)789-1260

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ENVIRONMENTAL LABORATORIES, INC.

142 TEMPLE STREET
NEW HAVEN, CT 06510
(203) 789-1260
FAX (203) 789-8261

JOB NO. 91-595-19			
CLIENT/PROJECT Baymark Phase IIB			
SUBJECT/TITLE			
OBJECTIVE OF CALCULATION Determination of Hydraulic Conductivity; Confined solution.			
CALCULATION METHOD/ASSUMPTION Cooper - Bredehoeft - Papadopoulos Method:			
$H/H_0 = \frac{8\alpha}{\pi^2} \int_0^{\infty} \frac{e^{-\beta u^2/\alpha}}{u \cdot \{ [u J_0(u) - 2\alpha J_1(u)]^2 + [u Y_0 - 2\alpha Y_1(u)]^2 \}^{1/2}} du$ <p>see attached for definition of variables</p>			
SOURCES OF DATA/EQUATIONS <u>Aqtesolv</u> ; Garaghty + Miller software package; version 11, 1991			
CONCLUSIONS see software output			
CALC. BY	DATE	CHECKED BY	DATE

1045M

SLUG TEST FOR CONFINED AQUIFERS

REFERENCE: Cooper, H. H., J. D. Bredehoeft, and S. S. Papadopoulos, response of a finite-diameter well to an instantaneous charge of water, *Water Resources Research*, vol. 3, no. 1, pp. 263-269.

ASSUMPTIONS: aquifer has infinite areal extent
 aquifer is homogeneous, isotropic, and of uniform thickness
 aquifer potentiometric surface is initially horizontal
 a volume of water, V , is injected into or discharged from the well instantaneously
 pumping well is fully penetrating
 flow to pumping well is horizontal
 aquifer is confined
 flow is unsteady
 water is released instantaneously from storage with decline of hydraulic head
 diameter of pumping well is very small so that storage in the well can be neglected

SOLUTION:

Integral solution for dimensionless drawdown in well:

$$H/H_0 = \frac{8\alpha}{\pi^2} \int_0^{\infty} \frac{e^{-\beta u^2/\alpha}}{u \cdot \{[uJ_0(u) - 2\alpha J_1(u)]^2 + [uY_0 - 2\alpha Y_1(u)]^2\}} du$$

Laplace solution for response in well:

$$\bar{h} = \frac{r_w S H_0 K_0(rq)}{T q [r_w q K_0(r_w q) + 2\alpha K_1(r_w q)]}$$

$$q = (pS/T)^{1/2}$$

p = Laplace transform variable

where:

H = head in well at time t [L]

H_0 = initial head in well well due to slug injection or extraction [L]

α = $r_w^2 S / r_c^2$ [dimensionless]

SLUG TEST FOR CONFINED AQUIFERS
(continued)

r_w = effective radius of well [L]

r_c = internal radius of well casing [L]

β = Tt/r_c^2

J_0 = Bessel function of first kind, zero order

J_1 = Bessel function of first kind, first order

Y_0 = Bessel function of second kind, zero order

Y_1 = Bessel function of second kind, first order

K_0 = modified Bessel function of second kind, zero order

K_1 = modified Bessel function of second kind, first order

Response of a Finite-Diameter Well to an Instantaneous Charge of Water¹

HILTON H. COOPER, JR., JOHN D. BREDEHOEFT, AND
ISTAVROS S. PAPADOPULOS

Water Resources Division, U. S. Geological Survey, Washington, D. C.

Abstract. A solution is presented for the change in water level in a well of finite diameter after a known volume of water is suddenly injected or withdrawn. A set of type curves computed from this solution permits a determination of the transmissibility of the aquifer. (Key words: Aquifer tests; groundwater; hydraulics; permeability)

INTRODUCTION

Ferris and Knowles [1954] introduced a method for determining the transmissibility of an aquifer from observations of the water level in a well after a known volume of water is suddenly injected into the well. (See also *Ferris et al.* [1962]). They reasoned that for practical purposes the well may be approximated by an instantaneous line source in the infinite region, for which the residual head differences due to the injection are described by

$$h = (V/4\pi Tt)e^{-r^2 S/4Tt} \quad (1)$$

where

- h = change in head at distance r and time t due to the injection;
- r = distance from the line source or center of well;
- t = time since instantaneous injection;
- V = volume of water injected;
- T = transmissibility of aquifer;
- S = coefficient of storage of aquifer.

They reasoned further that the head H in the injected well would be described closely by (1) when r is set equal to the effective radius r_w [Jacob, 1947, p. 1049] of the screen or open well. Then, since r_w is small, the exponential approaches unity quickly, so that the equation approaches $H = V/4\pi Tt$, which can be written

$$T = V(1/t)/4\pi H \quad (2)$$

to the extent that the equation is valid for a

Publication authorized by the Director, U. S. Geological Survey.

well of finite diameter, a determination of the transmissibility can be obtained from the slope of a plot of head H versus the reciprocal of time ($1/t$).

Since the volume of water injected into the well is $\pi r_w^2 H_0$, where r_w is the radius of the casing in the interval over which the water level fluctuates and H_0 is the initial head increase in the well, equation 1 can be written

$$h/H_0 = (r_w^2/4Tt)e^{-r^2 S/4Tt} \quad (3)$$

and equation 2 can be written

$$H/H_0 = r_w^2/4Tt \quad (4)$$

Recently *Bredehoeft et al.* [1966] demonstrated by means of an electrical analog model of a well-aquifer system that equation 3 gives a satisfactory approximation of the head in an injected well only after the time t is large enough for the ratio H/H_0 to be very small (see Figure 1). The observed discrepancy appears to arise from the assumption that the injected well can be approximated by a line source.

We present here an exact solution for the head in and around a well of finite diameter after the well is instantaneously charged with a known volume of water.

ANALYSIS

Consider a nonflowing well cased to the top of a homogeneous isotropic artesian aquifer of uniform thickness, and screened (or open) throughout the thickness of the aquifer (Figure 2). Suppose that the well is instantaneously charged with a volume V of water. (We will consider

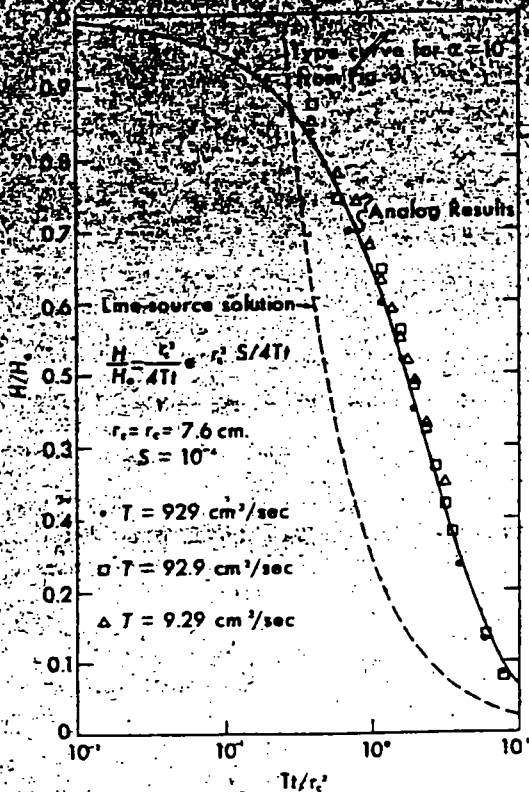


Fig. 1. Comparison of analog results with curve representing line-source solution.

an injection as a positive charge and a withdrawal as a negative one.) The water level in the well instantaneously moves to the height $H_0 = V/\pi r_w^2$ above or below its initial level and immediately begins to return to its initial level according to some function of time $H(t)$. Meanwhile the head in the surrounding aquifer varies according to $h(r, t)$. Our objective is to find a solution for $h(r, t)$ and $H(t)$. The inertia of the column of water in the well will be neglected. (See, in this connection, *Bredehoeft et al.* [1966]). Since the solution to be obtained can be superposed on any initial condition, we can simplify the problem without loss of generality by assuming that the head is initially uniform and constant.

The problem is described mathematically by

$$\frac{\partial^2 h}{\partial r^2} + \frac{1}{r} \frac{\partial h}{\partial r} = \frac{S}{T} \frac{\partial h}{\partial t} \quad (r > r_w) \quad (5)$$

$$h(r_w + 0, t) = H(t) \quad (t > 0) \quad (5a)$$

$$h(\infty, t) = 0 \quad (t > 0) \quad (5b)$$

$$\frac{\partial h}{\partial r}(r_w + 0, t) = 0 \quad (5c)$$

$$-\pi r_w^2 \frac{\partial H(t)}{\partial t} \quad (t > 0) \quad (5d)$$

$$h(r, 0) = 0 \quad (r > r_w) \quad (5e)$$

$$H(0) = H_0 = V/\pi r_w^2 \quad (5f)$$

Equation 5 is the differential equation governing nonsteady radial flow of confined groundwater. (See, for example, *Jacob*, 1950, p. 333.) Boundary condition 5a states that after the first instant the head in the aquifer at the face of the well is equal to that in the well. Boundary condition 5b states that as r approaches infinity the change in head approaches zero. Equation 5c expresses the fact that the rate of flow of water into (or out of) the aquifer is equal to the rate of decrease (or increase) in volume of water within the well. The conditions 5d and 5e state that initially the change in head is zero everywhere outside the well and equal to H_0 inside the well.

By applying the Laplace transform with respect to time the problem is reduced to

$$\frac{\partial^2 \bar{h}}{\partial r^2} + \frac{1}{r} \frac{\partial \bar{h}}{\partial r} = (S/T) (p\bar{h}) \quad (6)$$

$$\bar{h}(\infty, p) = 0 \quad (6a)$$

$$\begin{aligned} \frac{\partial \bar{h}(r_w + 0, p)}{\partial r} \\ = (r_w^2 / 2r_w T) [p\bar{h}(r_w + 0, p) - H_0] \end{aligned} \quad (6b)$$

for which the solution is

$$\bar{h}(r, p) = \frac{r_w S H_0 K_0(r/q)}{T q [r_w q K_0(r_w/q) + 2\alpha K_0(r_w/q)]} \quad (7)$$

where $q = (pS/T)^{1/2}$, and $\alpha = r_w^2 S/r_w^2$.

The solution $h(r, t)$ is the inverse transform which is available from the analogous problem in heat flow [*Carlaw and Jaeger*, 1959, p. 342]

$$\begin{aligned} h = \frac{2H_0}{\pi} \int_0^\infty e^{-\beta u^2 / \alpha} \{ J_0(u r / r_w) \\ \cdot [u Y_0(u) - 2\alpha Y_1(u)] - Y_0(u r / r_w) \\ \cdot [u J_0(u) - 2\alpha J_1(u)] \} \frac{du}{\Delta(u)} \end{aligned} \quad (8)$$

where $\beta = Tt/r_w^2$ and

$$\begin{aligned} \Delta(u) = [u J_0(u) - 2\alpha J_1(u)]^2 \\ + [u Y_0(u) - 2\alpha Y_1(u)]^2 \end{aligned}$$

Fig. 2. Idealized repre

The head $H(t)$ inside the well substituting $r = r_w$ in equation

$$H = (8H_0 \alpha / \pi^2) \int_0^\infty e^{-\beta u^2 / \alpha}$$

Values of H/H_0 computed by integrating equation 9 are given in Table 1. The values from Table 1 are a family of five curves of H/H_0 versus dimensionless time parameter Tt/r_w^2 . Also represented by the curves are the values computed from the line-source solution for each of five values of $\alpha = r_w^2 S/r_w^2$. Also represented by the curves are the values computed from the line-source solution for each of five values of $\alpha = r_w^2 S/r_w^2$. Also represented by the curves are the values computed from the line-source solution for each of five values of $\alpha = r_w^2 S/r_w^2$.

It is apparent from Table 1 and Figure 3 that the line-source solution proposed by *Ferris and Knowles* is a close approximation of the full solution for large values of Tt/r_w^2 . The approximation is acceptable for Tt/r_w^2 greater than 10 for H/H_0 less than about 0.1. At Speedway City, Indiana, *Knowles* to exemplify the results ranged from 0.01 to 0.001,

$$\partial h(r, + 0, t) / \partial r$$

$$\frac{\partial}{\partial t} (\partial H(t) / \partial t) \quad (t > 0) \quad (5c)$$

$$h(r, 0) = 0 \quad (r > r_w) \quad (5d)$$

$$H(0) = H_0 = V / \pi r_w^2 \quad (5e)$$

on 5 is the differential equation govern- nsteady radial flow of confined ground- (See, for example, *Jacob*, 1950, p. 333.) ary condition 5a states that after the first the head in the aquifer at the face of the equal to that in the well. Boundary con- 5b states that as r approaches infinity nge in head approaches zero. Equation resses the fact that the rate of flow of nto (or out of) the aquifer is equal to the decrease (or increase) in volume of water the well. The conditions 5d and 5e state itially the change in head is zero every- outside the well and equal to H_0 inside ll.

pplying the Laplace transform with re- o time the problem is reduced to

$$h / \partial r^2 + 1/r (\partial h / \partial r) = (S/T) (p\bar{h}) \quad (6)$$

$$h(\infty, p) = 0 \quad (6a)$$

$$+ 0 \quad p) / \partial r$$

$$r_w T [p\bar{h}(r_w, p) - H_0] \quad (6b)$$

ch the solution is

$$= \frac{r_w S H_0 K_0(r_w q)}{T q [r_w q K_0(r_w q) + 2\alpha K_0(r_w q)]} \quad (7)$$

$$q = (pS/T)^{1/2}, \text{ and } \alpha = r_w^2 S / r^2$$

olution $h(r, t)$ is the inverse transform is available from the analogous problem flow [*Carson and Jaeger*, 1959, p. 342]

$$\frac{H_0}{\pi} \int_0^\infty e^{-u^2/\alpha} (J_0(u/r_w))$$

$$Y_0(u) - 2\alpha Y_1(u) - Y_0(u/r_w)$$

$$J_0(u) - 2\alpha J_1(u) \frac{du}{\Delta(u)} \quad (8)$$

$$\beta = Tt/r_w^2 \text{ and}$$

$$[u J_0(u) - 2\alpha J_1(u)]$$

$$+ [u Y_0(u) - 2\alpha Y_1(u)]$$

Instantaneous Charge

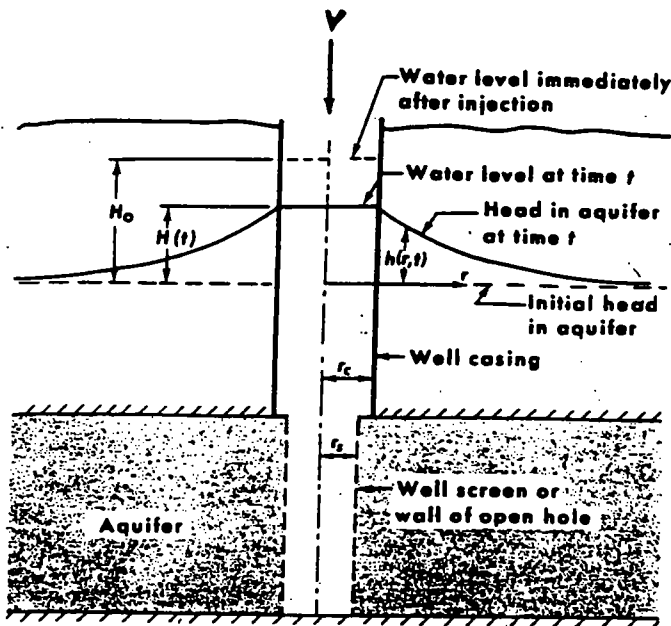


Fig. 2. Idealized representation of a well into which a volume V of water is suddenly injected.

The head $H(t)$ inside the well, obtained by substituting $r = r_w$ in equation 8, is

$$H = (8H_0\alpha/\pi^2) \int_0^\infty e^{-u^2/\alpha} du / (u \Delta(u)) \quad (9)$$

Values of H/H_0 computed by numerically integrating equation 9 are given in Table 1. Values computed from the line-source solutions, equations 3 and 4, are given in Table 2. In Figure 3 the values from Table 1 are represented as a family of five curves of H/H_0 versus the dimensionless time parameter $\beta = Tt/r_w^2$, one curve for each of five values of the parameter $\alpha = r_w^2 S / r^2$. Also represented, by a dashed curve, are the values computed from equation 4.

It is apparent from Tables 1 and 2 and from Figure 3 that the line-source solutions 3 and 4 proposed by Ferris and Knowles [1954] give a close approximation of the finite-source solution 9, only for large values of the time parameter Tt/r_w^2 . The approximation seems to be acceptable for Tt/r_w^2 greater than 100 (or, equivalently, for H/H_0 less than about 0.0025). (In the test at Speedway City, Indiana, used by Ferris and Knowles to exemplify their method, H/H_0 ranged from 0.01 to 0.001, and the value of

transmissibility determined from these data agreed fairly well with one obtained by another method.)

A family of type curves plotted on semilogarithmic paper, as in Figure 3, permits a determination of the transmissibility. The method is similar to the Theis graphical method [Wenzel, 1942]. A test on a well near Dawsonville, Georgia, will be used to demonstrate the method. This well is cased to 24 m with 15.2-cm (6-inch) casing and drilled as a 15.2-cm open hole to a depth of 122 m. Figure 4 is a reproduction of a chart showing the hydrograph of the well after the sudden withdrawal of a long weighted float from the well. The weight of the float was 10.16 kilograms, and hence by the principle of Archimedes it had displaced a volume of 0.01016 m³ of water when floating in the well. Its withdrawal was therefore equivalent to a negative charge of $V = 0.01016$ m³. From the relation $H_0 = V/\pi r_w^2$, the initial head change is found to be $H_0 = 0.560$ m.

The hydrograph in Figure 4 was recorded electrically from a pressure transducer, which was suspended below the water surface in the well. Table 3 lists data from this chart. To determine the aquifer constants, the data are

TABLE 1. Values of H/H_0 for a Well of Finite Diameter (computed from equation 9)

Tt/r_w^2	H/H_0				
	$\alpha = 10^{-1}$	$\alpha = 10^{-2}$	$\alpha = 10^{-3}$	$\alpha = 10^{-4}$	$\alpha = 10^{-5}$
1.00×10^{-3}	0.9771	0.9920	0.9969	0.9985	0.9992
2.15×10^{-3}	0.9658	0.9876	0.9949	0.9974	0.9985
4.64×10^{-3}	0.9490	0.9807	0.9914	0.9954	0.9970
1.00×10^{-2}	0.9238	0.9693	0.9853	0.9915	0.9942
2.15×10^{-2}	0.8860	0.9505	0.9744	0.9841	0.9888
4.64×10^{-2}	0.8293	0.9187	0.9545	0.9701	0.9781
1.00×10^{-1}	0.7480	0.8655	0.9183	0.9484	0.9672
2.15×10^{-1}	0.6238	0.7782	0.8538	0.8935	0.9167
4.64×10^{-1}	0.4782	0.6436	0.7436	0.8031	0.8410
1.00×10^0	0.3117	0.4598	0.5729	0.6520	0.7080
2.15×10^0	0.1865	0.2597	0.3543	0.4364	0.5038
4.64×10^0	0.07415	0.1088	0.1554	0.2082	0.2621
7.00×10^0	0.04625	0.06204	0.08519	0.1161	0.1521
1.00×10^1	0.03065	0.03780	0.04821	0.06355	0.08378
1.40×10^1	0.02092	0.02414	0.02844	0.03492	0.04426
2.15×10^1	0.01297	0.01414	0.01545	0.01723	0.01999
3.00×10^1	0.009070	0.009615	0.01016	0.01083	0.01169
4.64×10^1	0.005711	0.005919	0.006111	0.006319	0.006554
7.00×10^1	0.003722	0.003809	0.003884	0.003962	0.004046
1.00×10^2	0.002577	0.002618	0.002653	0.002688	0.002725
2.15×10^2	0.001179	0.001187	0.001194	0.001201	0.001208

plotted on semilogarithmic paper of the same scale as that of the type curves in Figure 3, and this plot is superposed on the type curves.

With the arithmetic axes coincident, the data plot is translated horizontally to a position where the data best fit the type curves, as

TABLE 2. Values of H/H_0 for Line-source Approximation of a Well

Tt/r_w^2	H/H_0 , from equation 3					H/H_0 , from eq. 4
	$\alpha = 10^{-1}$	$\alpha = 10^{-2}$	$\alpha = 10^{-3}$	$\alpha = 10^{-4}$	$\alpha = 10^{-5}$	
1.00×10^{-1}	0.000000	20.52	194.7	243.8	249.4	250.0
2.15×10^{-1}	0.001035	36.35	103.5	115.0	116.2	116.3
4.64×10^{-1}	0.2463	31.44	51.05	53.59	53.85	53.88
1.00×10^0	2.052	19.47	24.38	24.94	24.99	25.00
2.15×10^0	3.635	10.35	11.50	11.62	11.63	11.63
4.64×10^0	3.144	5.105	5.359	5.385	5.388	5.388
1.00×10^1	1.947	2.438	2.494	2.499	2.500	2.500
2.15×10^1	1.035	1.150	1.162	1.163		1.163
4.64×10^1	0.5105	0.5359	0.5385	0.5388		0.5388
1.00×10^2	0.2438	0.2494	0.2499	0.2500		0.2500
2.15×10^2	0.1150	0.1162	0.1163			0.1163
4.64×10^2	0.05359	0.05385	0.05388			0.05388
7.00×10^2	0.03558	0.03570	0.03571			0.03571
1.00×10^3	0.02494	0.02499	0.02500			0.02500
1.40×10^3	0.01783	0.01786				0.01786
2.15×10^3	0.01162	0.01163				0.01163
3.00×10^3	0.008326	0.008333				0.008333
4.64×10^3	0.005385	0.005388				0.005388
7.00×10^3	0.003570	0.003571				0.003571
1.00×10^4	0.002499	0.002500				0.002500
2.15×10^4	0.001183					0.001183

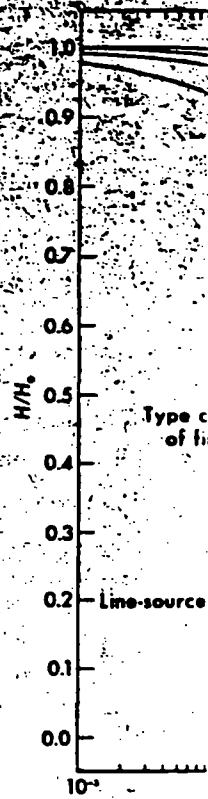


Fig. 3. Type curves

shown in Figure 5. In this plot $t = 11$ sec on the data coordinates overlie the value $Tt/r_w^2 = 1.0$ on the type curve coordinates. Hence the transmissivity S is computed to be

$$T = \frac{1.0 r_w^2}{t} = \frac{(1.0)(7.6)^2}{11} = 5.388 \text{ (11)}$$

In principle the coefficient of storage S is determined by interpolating from the type curves that lie on either side of the data plot in the matched position. In the example just described, the coefficient of storage would be $S = 10^{-4}$, since for this value of α the data plot would be slightly to the right of the type curve for $\alpha = 10^{-4}$. However, because of the shapes of the type curves, a determination of S by this method is not a particularly reliable one.

Finite Diameter

	$\alpha = 10^{-4}$	$\alpha = 10^{-5}$
	0.9985	0.9992
	0.9974	0.9985
	0.9954	0.9970
	0.9915	0.9942
	0.9841	0.9888
	0.9701	0.9781
	0.9434	0.9572
	0.8935	0.9167
	0.8031	0.8410
	0.6520	0.7080
	0.4364	0.5038
	0.2082	0.2620
	0.1161	0.1521
	0.06355	0.08378
	0.03492	0.04426
	0.01723	0.01999
	0.01083	0.01169
1	0.006319	0.006554
4	0.003962	0.004046
3	0.002688	0.002725
4	0.001201	0.001208

arithmetic axes coincident, the data translated horizontally to a position data best fit the type curves, as

ation of a Well

$\alpha = 10^{-4}$	$\alpha = 10^{-5}$	H/H_0 from eq. 4
243.8	249.4	250.0
115.0	116.2	116.3
53.59	53.85	53.88
24.94	24.99	25.00
11.62	11.63	11.63
5.385	5.388	5.388
2.499	2.500	2.500
1.163		1.163
0.5388		0.5388
0.2500		0.2500
		0.1163
		0.05388
		0.03571
		0.02500
		0.01786
		0.01163
		0.008333
		0.005388
		0.003571
		0.002500
		0.001163

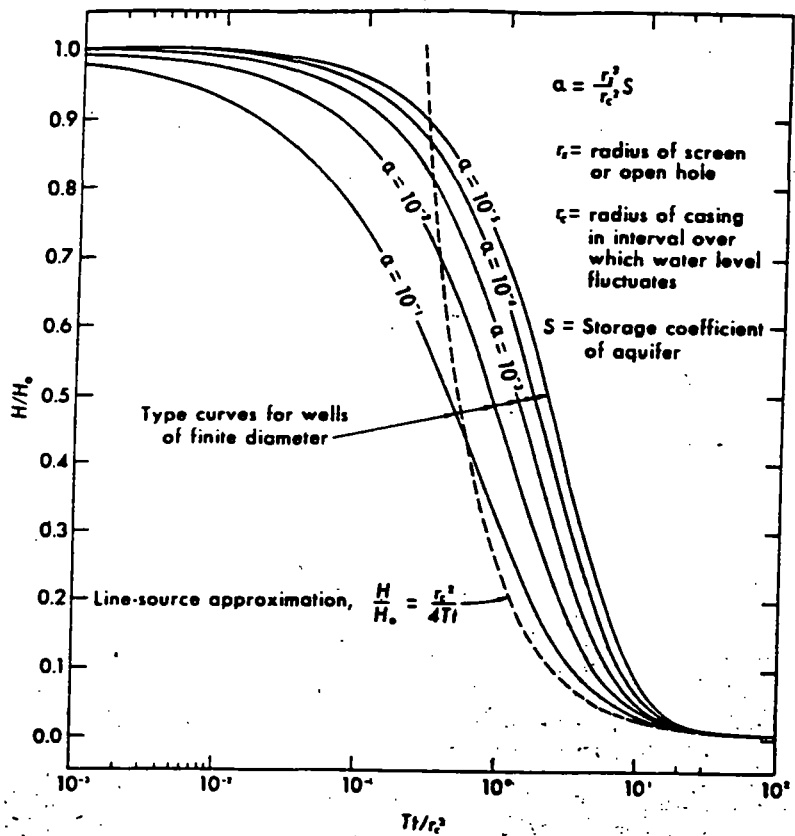


Fig. 3. Type curves for instantaneous charge in well of finite diameter.

shown in Figure 5. In this position the time $t = 11$ sec on the data coordinates is found to overlie the value $Tt/r_0^2 = 1.0$ on the type-curve coordinates. Hence the transmissibility is computed to be

$$T = \frac{1.0 r_0^2}{t} = \frac{(1.0)(7.6)^2}{(11)} = 5.3 \text{ cm}^2/\text{sec}$$

In principle the coefficient of storage can be determined by interpolating from its values for the curves that lie on either side of the data plot in the matched position. Thus, in the example just described, the coefficient of storage would be $S = 10^{-5}$, since for this well $r_0 = r_c$, so that $\alpha = S$, and the points fall on the curve for $\alpha = 10^{-5}$. However, because the matching of data plot to the type curves depends upon the shapes of the type curves, which differ only slightly when α differs by an order of magnitude, a determination of S by this method has questionable reliability.

The determination of T is not so sensitive to the choice of the curves to be matched. Whereas the determined value of S will change by an



Fig. 4. Hydrograph of well at Dawsonville, Georgia, showing response of water level to the sudden withdrawal of a weighted float.

TABLE 2. Rise of Water Level in Dawsonville Well after Instantaneous Withdrawal of Weighted Float

t (sec)	1/t	Head (m)	H (m)	H/H ₀
-1		0.896		
0		0.836	0.560	1.000
3	0.333	0.439	0.457	0.816
6	0.167	0.504	0.392	0.700
9	0.111	0.551	0.345	0.616
12	0.0833	0.588	0.308	0.550
15	0.0667	0.616	0.280	0.500
18	0.0556	0.644	0.252	0.450
21	0.0476	0.672	0.224	0.400
24	0.0417	0.691	0.205	0.366
27	0.0370	0.709	0.187	0.334
30	0.0333	0.728	0.168	0.300
33	0.0303	0.747	0.149	0.266
36	0.0278	0.756	0.140	0.250
39	0.0256	0.765	0.131	0.234
42	0.0238	0.784	0.112	0.200
45	0.0222	0.788	0.108	0.193
48	0.0208	0.803	0.093	0.166
51	0.0196	0.807	0.089	0.159
54	0.0185	0.814	0.082	0.146
57	0.0175	0.821	0.075	0.134
60	0.0167	0.825	0.071	0.127
63	0.0159	0.831	0.065	0.116

order of magnitude when the data plot is moved from one type curve to another, that of T will change much less. From a knowledge of the geologic conditions and other considerations one can ordinarily estimate S within an order of magnitude and thereby eliminate some of the doubt as to what value of α is to be used for matching the data plot.

Figure 6 shows the data from the test on the Dawsonville well plotted according to the Ferris-Knowles method. The points do not fall along a straight line as postulated in this method but, instead, fall along the trace of the type curve for $\alpha = 10^{-2}$, which has been transferred from Figure 5. Also shown is a straight line through the origin whose slope, when used according to the Ferris-Knowles method, will yield the transmissibility of $5.3 \text{ cm}^2/\text{sec}$ obtained by matching the data to the type curves.

CONCLUSION

The judgment of an experienced hydrologist is needed to decide the significance, if any, of a determination of T by the method of instantaneous

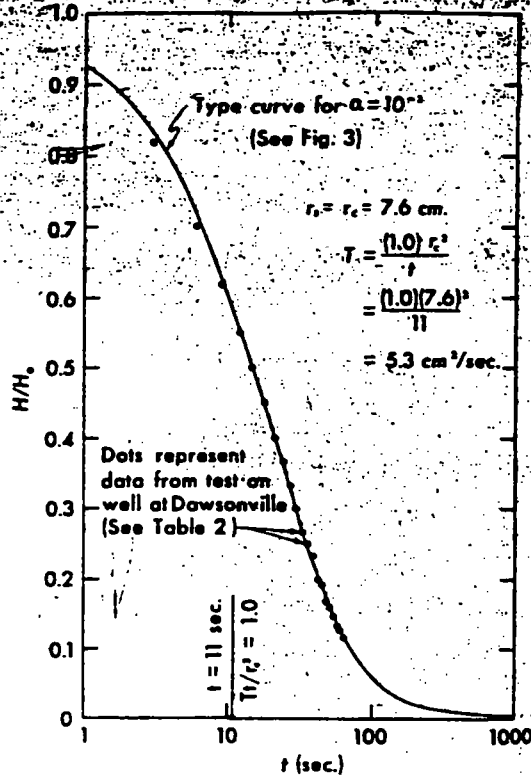


Fig. 5. Plot of data from test at Dawsonville, Georgia, superposed on type curve.

charge. As Ferris et al. [1962] properly warned

the duration of a 'slug' test is very short, hence the estimated transmissibility determined from the test will be representative only of the water-bearing material close to the well. Serious errors will be introduced unless the . . . well is fully developed and completely penetrates the aquifer.

Few wells completely penetrate an aquifer, but it is nevertheless possible under some circumstances for a hydrologist to derive useful information from a test on a partially penetrating well. Since the vertical permeabilities of most stratified aquifers are only small fractions of the horizontal permeabilities, the induced flow within the small radius of the cone that develops during the short period of observation is likely to be essentially 2-dimensional. Therefore, the determined value of T would represent approximately the transmissibility of that part

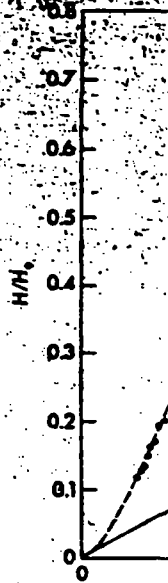
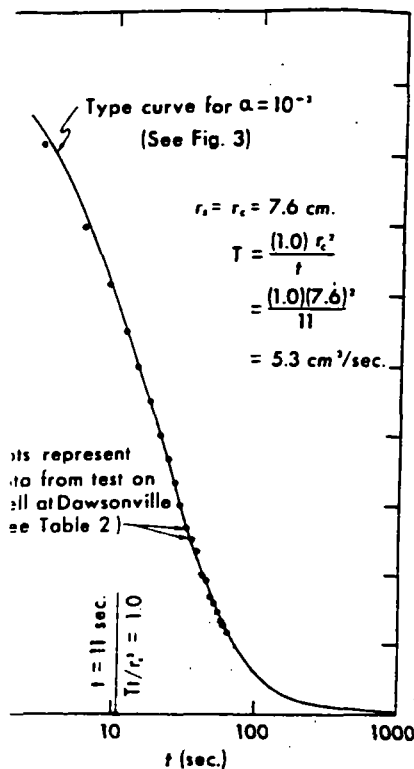


Fig. 6. Data from test

of the aquifer in which the open, provided that the aquifer is homogeneous and isotropic to the bedding and provides a radius r , can be estimated cl

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Carlaw, H. S., and J. C. Ja
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London, 1959.
Ferris, J. G., and D. B. Know



dots represent data from test on well at Dawsonville (See Table 2)

As Ferris et al. [1962] properly

tion of a 'slug' test is very short, the estimated transmissibility determined from the test will be representative of the water-bearing material close to the well. Large errors will be introduced unless the well is fully developed and completely penetrates the aquifer.

completely penetrate an aquifer, but nevertheless possible under some circumstances a hydrologist to derive useful information from a test on a partially penetrating well. The vertical permeabilities of most aquifers are only small fractions of their horizontal permeabilities, the induced flow from a small radius of the cone that develops during the short period of observation is essentially 2-dimensional. Therefore, the determined value of T would represent only the transmissibility of that part

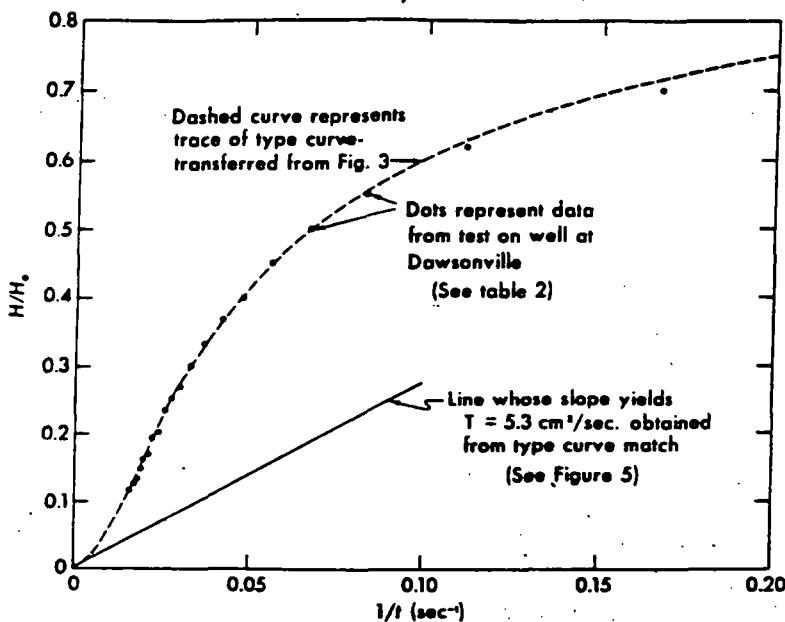


Fig. 6. Data from test on well of Dawsonville, Georgia, plotted according to the Ferris-Knowles method.

of the aquifer in which the well is screened or open, provided that the aquifer is reasonably homogeneous and isotropic in planes parallel to the bedding and provided that the effective radius r , can be estimated closely.

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ENVIRONMENTAL LABORATORIES, INC.

142 TEMPLE STREET
NEW HAVEN, CT 06510
(203) 789-1260
FAX (203) 789-8261

JOB NO. 91-545-19			
CLIENT/PROJECT Ranmark Phase II B			
SUBJECT/TITLE			
OBJECTIVE OF CALCULATION Determination of Hydraulic Conductivity; Unconfined solution.			
CALCULATION METHOD/ASSUMPTION Bever - Rice Method; $\ln S_0 - \ln S_t = \frac{2 K L t}{r_c^2 \ln(r_c/r_w)}$ see attached for definition of variables			
SOURCES OF DATA/EQUATIONS <u>Intesolv</u> ; Geoghty + Miller software package; version 1.1, 1991			
CONCLUSIONS See software output			
CALC. BY	DATE	CHECKED BY	DATE

1045M

629

SLUG TEST METHOD FOR UNCONFINED AQUIFERS

REFERENCE: Bouwer, H. and R. C. Rice, 1976. A slug test method for determining hydraulic conductivity of unconfined aquifers with completely or partially penetrating wells, *Water Resources Research*, vol. 12, no. 3, pp. 423-428.

SOLUTION:

$$\ln s_0 - \ln s_t = \frac{2 K L t}{r_c^2 \ln(r_0/r_w)}$$

where:

s_0 = initial drawdown in well due to instantaneous removal of water from well [L]

s_t = drawdown in well at time t [L]

L = length of well screen [L]

r_c = radius of well casing [L]

$\ln(r_0/r_w)$ = empirical "shape factor" determined from tables provided in Bouwer and Rice (1976)

r_0 = equivalent radius over which head loss occurs [L]

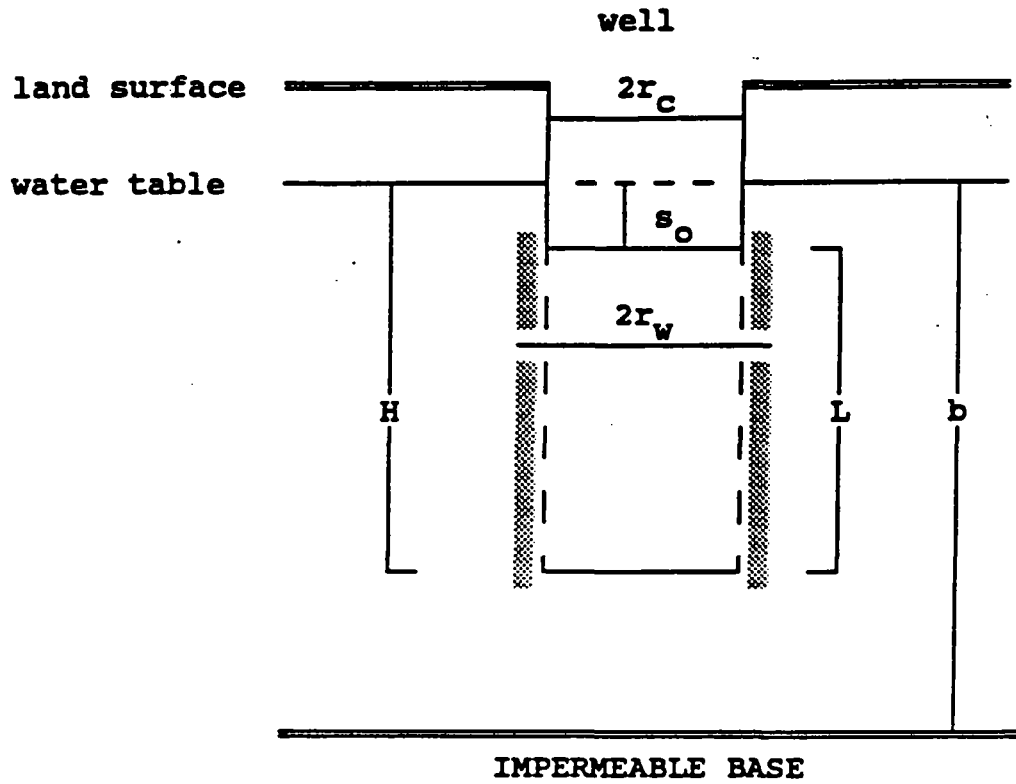
r_w = radius of well (including gravel pack) [L]

H = static height of water in well [L]

b = saturated thickness of aquifer

SLUG TEST METHOD FOR UNCONFINED AQUIFERS
(continued)

DEFINITION OF TERMS:



A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers With Completely or Partially Penetrating Wells

HERMAN BOUWER AND R. C. RICE

U.S. Water Conservation Laboratory, Agricultural Research Service, U.S. Department of Agriculture, Phoenix, Arizona 85040

A procedure is presented for calculating the hydraulic conductivity of an aquifer near a well from the rate of rise of the water level in the well after a certain volume of water is suddenly removed. The calculation is based on the Thiem equation of steady state flow to a well. The effective radius R_e , over which the head difference between the equilibrium water table in the aquifer and the water level in the well is dissipated was evaluated with a resistance network analog for a wide range of system geometries. An empirical equation relating R_e to the geometry of the well and aquifer was derived. The technique is applicable to completely or partially penetrating wells in unconfined aquifers. It can also be used for confined aquifers that receive water from the upper confining layer. The method's results are compatible with those obtained by other techniques for overlapping geometries.

With the slug test the hydraulic conductivity or transmissibility of an aquifer is determined from the rate of rise of the water level in a well after a certain volume or 'slug' of water is suddenly removed from the well. The slug test is simpler and quicker than the Theis pumping test because observation wells and pumping the well are not needed. With the slug test the portion of the aquifer 'sampled' for hydraulic conductivity is smaller than that for the pumping test even though with the latter, most of the head loss also occurs within a relatively small distance of the pumped well and the resulting transmissibility primarily reflects the aquifer conditions near the pumped well.

Essentially instantaneous lowering of the water level in a well can be achieved by quickly removing water with a bailer or by partially or completely submerging an object in the water, letting the water level reach equilibrium, and then quickly removing the object. If the aquifer is very permeable, the water level in the well may rise very rapidly. Such rapid rises can be measured with sensitive pressure transducers and fast-response strip chart recorders or x-y plotters. Also it may be possible to isolate portions of the perforated or screened portion of the well with special packers for the slug test. This not only reduces the inflow and hence the rate of rise of the water level in the well, but it also makes it possible to determine the vertical distribution of the hydraulic conductivity. Special packer techniques may have to be developed to obtain a good seal, especially for rough casings or perforations. Effecting a seal may be achieved with relatively long sections of inflatable stoppers or tubing. The use of long sections of these materials would also reduce leakage flow from the rest of the well to the isolated section between packers. This flow can occur through gravel envelopes or other permeable zones surrounding the casing. Sections of inflatable tubing may have to be long enough to block off the entire part of the well not used for the slug test. High inflation pressures should be used to minimize volume changes in the tubing due to changing water pressures in the isolated section when the head is lowered.

Until now, solutions for the slug test have been developed only for completely penetrating wells in confined aquifers. Cooper (1967) derived an equation for the rise or fall of the water level in a well after sudden lowering or raising, respectively. His equation was based on nonsteady flow to a pumped,

completely penetrating well, and the solution was expressed as a series of 'type curves' against which observed rates of water level rises were matched. Values for the transmissibility and storage coefficient were then evaluated from the curve parameter and horizontal-scale position of the type curve showing the best fit with the experimental data. Skibitzke [1958] developed an equation for calculating transmissibility from the recovery of the water level in a well that was repeatedly bailed. The technique is limited to wells in confined aquifers with sufficiently shallow water levels to permit short time intervals between bailing cycles [Lohman, 1972].

To use the slug test for partially penetrating or partially perforated wells in confined or unconfined aquifers, some solutions developed for the auger hole and piezometer techniques to measure soil hydraulic conductivity [Bouwer and Jackson, 1974] may be employed. However, the geometry of most groundwater wells is outside the range in geometry covered by the existing equations or tables for the auger hole or piezometer methods. For this reason, theory and equations are presented in this paper for slug tests on partially or completely penetrating wells in unconfined aquifers for a wide range of geometry conditions. The wells may be partially or completely perforated, screened, or otherwise open along their periphery. While the solutions are developed for unconfined aquifers, they may also be used for slug tests on wells in confined aquifers if water enters the aquifer from the upper confining layer through compression or leakage.

THEORY

Geometry and symbols of a well in an unconfined aquifer are shown in Figure 1. For the slug test the water level in the well is suddenly lowered, and the rate of rise of the water level is measured. The flow into the well at a particular value of y can be calculated by modifying the Thiem equation to

$$Q = 2\pi KL \frac{y}{\ln(R_e/r_w)} \quad (1)$$

where Q is the flow into the well (length³/time), K is the hydraulic conductivity of the aquifer (length/time), L is the height of the portion of well through which water enters (height of screen or perforated zone or of uncased portion of well), y is the vertical distance between water level in well and equilibrium water table in aquifer, R_e is the effective radius over which y is dissipated, and r_w is the horizontal distance

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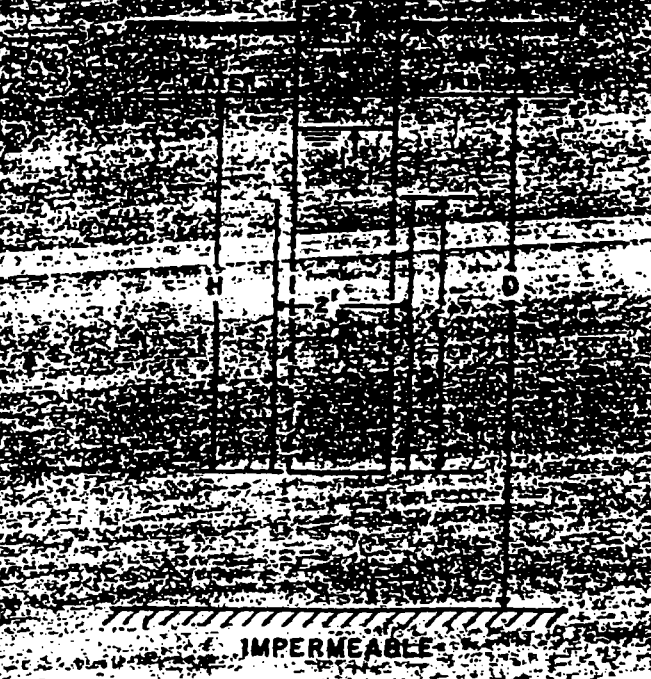


Fig. 1. Geometry and symbols of a partially penetrating, partially perforated well in unconfined aquifer with gravel pack or developed zone around perforated section.

from well center to original aquifer (well radius or radius of casing plus thickness of gravel envelope or developed zone).

The terms L , y , R_e , and r_w are all expressed in units of length. The effective radius R_e is the equivalent radial distance over which the head loss y is dissipated in the flow system. The value of R_e depends on the geometry of the flow system, and it was determined for different values of H , L , D , and r_w (Figure 1) with a resistance network analog, as will be discussed in the next section. Equation (1) is based on the assumptions that (1) drawdown of the water table around the well is negligible, (2) flow above the water table (in the capillary fringe) can be ignored, (3) head losses as water enters the well (well losses) are negligible, and (4) the aquifer is homogeneous and isotropic. These are the usual assumptions in the development of equations for pumped hole techniques [Bauer and Jackson, 1974, and references therein].

The value of r_w in (1) represents the radial distance between the undisturbed aquifer and the well center. Thus r_w should include gravel envelopes or 'developed' zones if they are much more permeable than the aquifer itself (Figure 1).

The rate of rise, dy/dt , of the water level in the well after suddenly removing a slug of water can be related to the inflow Q by the equation

$$dy/dt = - Q/\pi r_c^2 \quad (2)$$

where πr_c^2 is the cross-sectional area of the well where the water level is rising. The minus sign in (2) is introduced because y decreases as t increases.

The term r_c is the inside radius of the casing if the water level is above the perforated or otherwise open portion of the well. If the water level is rising in the perforated section of the well, allowance should be made for the porosity outside the well casing if the hydraulic conductivity of the gravel envelope or developed zone is much higher than that of the aquifer. In that case the (open) porosity in the permeable zone must be included in the cross-sectional area of the well. For example, if the radius of the perforated casing is 20 cm and the casing is

surrounded by a 10 cm permeable gravel envelope of 30% porosity, a total radius of 23 cm is used to obtain the cross-sectional area that relates Q to dy/dt . The value of r_w for this is 30 cm.

Combining (1) and (2) yields

$$\frac{1}{y} dy = \frac{2KL}{r_c^2 \ln(R_e/r_w)} dt$$

which can be integrated to

$$\ln y = \frac{2KL}{r_c^2 \ln(R_e/r_w)} t + \text{constant}$$

A straight line should be obtained when $\ln y$ is plotted against t and solving for K yields

$$K = \frac{r_c^2 \ln(R_e/r_w)}{2L} \frac{1}{t} \ln \frac{y_0}{y}$$

This equation enables K to be calculated from the rise in water level in the well after suddenly removing a slug from the well. Since K , r_c , r_w , R_e , and L in (5) are constant, $(1/t) \ln y_0/y$ must also be constant. Thus field data yield a straight line when they are plotted as $\ln y$ versus t . The value of $(1/t) \ln y_0/y$ in (5) is then obtained from the best straight line in a plot of $\ln y$ versus t (see the example). The value of $\ln R_e/r_w$ is dependent on H , D , L , and r_w and evaluated from the analog results presented in the next section. The transmissibility T of the aquifer is calculated by multiplying (5) by the thickness D of the aquifer or

$$T = \frac{Dr_c^2 \ln(R_e/r_w)}{2L} \frac{1}{t} \ln \frac{y_0}{y}$$

This equation is based on the assumption that the aquifer is uniform with depth.

Equations (5) and (6) are dimensionally correct. Thus K and T are expressed in the same units as the length and parameters in the equations.

EVALUATION OF R_e

Values of R_e , expressed as $\ln R_e/r_w$, were determined from an electrical resistance network analog for different values of r_w , L , H , and D (Figure 1), using the same assumption as those for (1). An axisymmetric sector of 1 rad was simulated by a network of electrical resistors. The vertical distance between the nodes was constant, but the radial distance between nodes increased with increasing distance from the center (Figure 2). This yielded a network with the highest node density near the well, where the head loss was greatest, and decreasing node density toward the outer reaches of the system. For a more detailed discussion of graded networks representing axisymmetric flow systems, see Liebmann [1955] and Bauer [1960].

The radial extent of the medium represented on the analog was more than 60,000 times the largest r_w value used in the analyses. Thus the radial extent of the analog system is essentially infinite, as evidenced by the fact that a reduction in radial extent by several nodes did not have a measurable effect on the observed value of R_e .

The value of R_e for an infinitely deep aquifer ($D = \infty$) is determined by simulating an impermeable and then a finite permeable layer at a certain value of D . If this value of D is taken to be sufficiently large, the flow in the system will be the same as in the

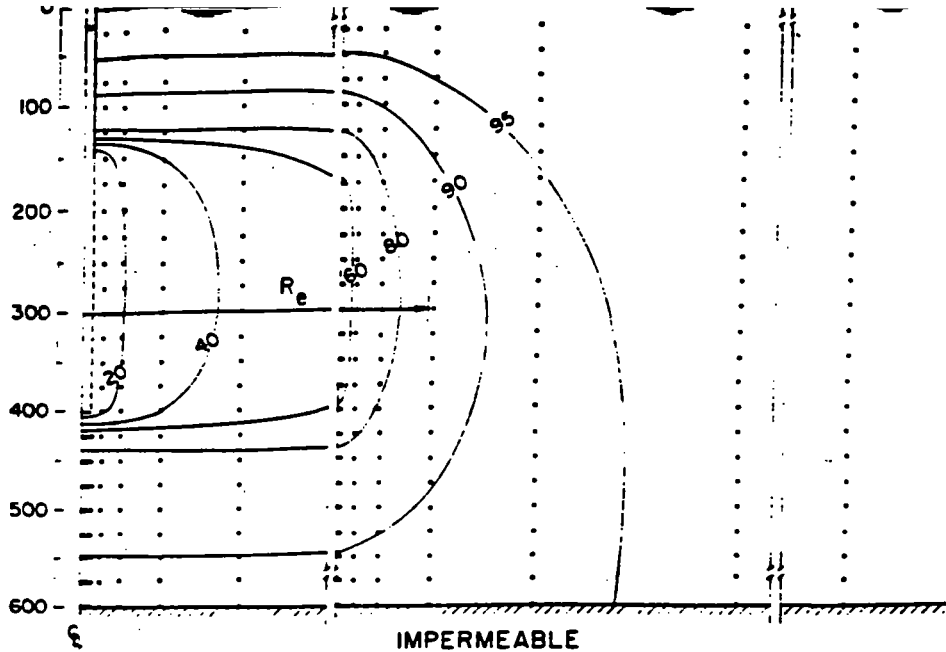


Fig. 2. Node arrangement (dots) for resistance network analog and potential distribution (indicated as percentages on equipotentials) for system with $L/r_w = 625$, $H/r_w = 1000$, and $D/r_w = 1500$. The numbers on the left and at the top of the figure are arbitrary length units (note breaks in horizontal scale).

less than the flow when the layer is taken as being infinitely permeable. The average of the two flows can then be taken as a good estimate of the flow that would occur if the aquifer were represented on the analog as being uniform to infinite depth [Bauer, 1967]. This average flow was used to calculate R_e for $D = \infty$.

The analog analyses were performed by simulating a system of certain values of r_w , H , and D . The electrical current entering the 'well' was then measured for different values of L , ranging from near H to near 0. This was repeated for other values of r_w , H , and D . The condition where $L = H$ could not be simulated on the analog because it would mean a short between the water table as the source and the well as the sink. The electrical current flow in the analog was converted to volume per day, and $\ln R_e/r_w$ was evaluated with (1) for each combination of r_w , H , L , and D used in the analog.

For a given geometry described by r_w , H , and D , the current flow Q_i into the simulated well varied essentially linearly with L and could be described by the equation

$$Q_i = mL - n \quad (7)$$

Because of the linearity between Q_i and L the results of the analyses could be extrapolated to the condition $L = H$. The values of m in (7) appeared to vary inversely with $\ln H/r_w$. The values of n varied approximately linearly with $\ln [(D - H)/r_w]$, the slope A and intercept B in these relations being a function of L/r_w . This enabled the derivation of the following empirical equation relating $\ln R_e/r_w$ to the geometry of the system:

$$\ln \frac{R_e}{r_w} = \left[\frac{1.1}{\ln (H/r_w)} + \frac{A + B \ln [(D - H)/r_w]}{L/r_w} \right]^{-1} \quad (8)$$

In this equation, A and B are dimensionless coefficients that are functions of L/r_w , as shown in Figure 3. If $D \gg H$, an increase in D has no measurable effect on $\ln R_e/r_w$. The analog

results indicated that the effective upper limit of $\ln [(D - H)/r_w]$ is 6. Thus if D is considered infinity or $(D - H)/r_w$ is so large that $\ln [(D - H)/r_w]$ is greater than 6, a value of 6 should still be used for the term $\ln [(D - H)/r_w]$ in (8).

If $D = H$, the term $\ln [(D - H)/r_w]$ in (8) cannot be used. The analog results indicated that for this condition, which is the case of a fully penetrating well, (8) should be modified to

$$\ln R_e/r_w = \left(\frac{1.1}{\ln (H/r_w)} + \frac{C}{L/r_w} \right)^{-1} \quad (9)$$

where C is a dimensionless parameter that is a function of L/r_w as shown in Figure 3.

Equations (8) and (9) yield values of $\ln R_e/r_w$ that are within 10% of the actual value as evaluated by analog if $L > 0.4H$ and within 25% if $L \ll H$ (for example, $L = 0.1H$).

The analog analyses were performed for wells that were closed at the bottom. Occasionally, however, wells with open bottoms were also simulated. The flow through the bottom appeared to be negligible for all values of r_w and L used in the analyses. If L is not much greater than r_w (for example, $L/r_w \ll 4$), the system geometry approaches that of a piezometer cavity [Bauer and Jackson, 1974], in which case the bottom flow can be significant. Equations (8) and (9) can also be used to evaluate $\ln R_e/r_w$ if a portion of the perforated or otherwise open part of the well is isolated with packers for the slug test.

Equipotentials for the flow system around a partially penetrating, partially perforated well in an unconfined aquifer after lowering the water level in the well are shown in Figure 2. The numbers along the symmetry axis and the water table represent arbitrary length units. The numbers on the equipotentials indicate the potential as a percentage of the total head difference between the water table (100%) and the open portion of the well (0%) shown as a dashed line.

The value of R_e for the case in Figure 2 is 96.7 length units. As shown in the figure, this corresponds approximately to the

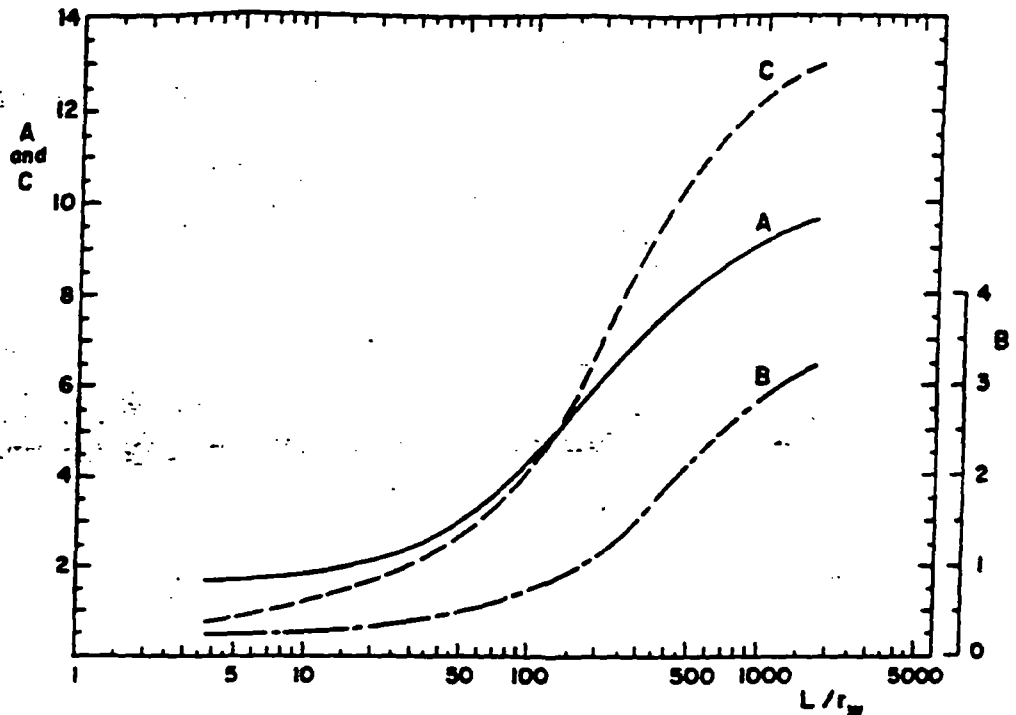


Fig. 3. Curves relating coefficients A, B, and C to L/r_w .

85% equipotential when R_e is laterally extended from the center of the open portion of the well. Thus most of the head loss in the flow system occurs in a cylinder with radius R_e , which is indicative of the horizontal extent of the portion of the aquifer sampled for K or T . The vertical extent is somewhat greater than L , as indicated by, for example, the 80% equipotential in Figure 2.

To estimate the rate of rise of the water level in a well after it is suddenly lowered, (5) can be written as

$$t = \frac{r_c^2}{2KL} \ln \frac{R_e}{r_w} \ln \frac{y_0}{y_t} \quad (10)$$

By taking $y_t = 0.9y_0$, (10) reduces to

$$t_{90\%} = 0.0527 \frac{r_c^2}{KL} \ln \frac{R_e}{r_w} \quad (11)$$

where $t_{90\%}$ is the time that it takes for the water level to rise 90% of the distance to the equilibrium level. By assuming a permeable aquifer with $K = 30$ m/day, a well with $r_c = 0.2$ m and $L = 10$ m, and $\ln(R_e/r_w) = 3$, (11) yields $t_{90\%} = 1.82$ s. Thus if y_0 is taken as 30 cm, it takes 1.8 s for the water level to rise 27 cm, another 1.8 s for the next 2.7 cm (90% of the remaining 3 cm), and another 1.8 s for the next 0.27 cm, or a total of 5.4 s for a rise of 29.97 cm. Measurement of this fast rise requires a sensitive and accurate transducer and a fast-response recorder. The rate of rise can be reduced by allowing groundwater to enter through only a portion of the open section of the well, as can be accomplished with packers.

For a moderately permeable aquifer with, for example, $K = 1$ m/day, a well with $r_c = 0.1$ m and $L = 20$ m, and $\ln(R_e/r_w) = 5$, (11) yields $t = 11.4$ s. In this case, it would take the water level 22.8 s to rise from 30 cm to 0.3 cm below static level.

EXAMPLE

A slug test was performed on a cased well in the alluvial deposits of the Salt River bed west of Phoenix, Arizona. The well, known as the east well, is located about 20 m east of six

rapid infiltration basins for groundwater recharge with effluent [Bouwer, 1970]. The static water table was at a depth of 3 m. $D = 80$ m, $H = 5.5$ m, $L = 4.56$ m, $r_c = 0.076$ m, $\ln[(D-H)/r_w]$ was taken as 0.12 m to allow for development of the aquifer around the perforated portion of the casing. A Sargent PM131TC pressure transducer was suspended about 1 m below the static water level in the well (when trade name company names are included, they are for the convenience of the reader and do not imply preferential endorsement of a particular product or company over others by the U.S. Department of Agriculture). A solid cylinder with a volume equivalent to a 0.32-m change in water level in the well was also placed below the water level. When the water level returned to equilibrium, the cylinder was quickly removed. The transducer output, recorded on a Sargent millivolt recorder, yielded the $y-t$ relationship shown in Figure 4 when plotted on a logarithmic scale. The straight-line portion is a valid part of the readings. The actual y_0 value of 0.2 m indicated by the straight line is close to the theoretical value of 0.32 m calculated from the displacement of the submerged cylinder.

Extending the straight line in Figure 4 shows that for an arbitrarily selected t value of 20 s, $y = 0.0025$ m. Thus $(1/y_0) \cdot y_t = 0.238 \text{ s}^{-1}$. The value of $L/r_w = 38$, for which Figure 3 yields $A = 2.6$ and $B = 0.42$. Substituting these values into (8) and using the maximum value of 6 for $\ln[(D-H)/r_w]$ (since $\ln[(D-H)/r_w]$ for the well exceeds 6) yield $\ln(R_e/r_w) = 2.2$. Equation (5) then gives $K = 0.00036 \text{ m/s} = 31 \text{ m/day}$. This value agrees with K values of 10 and 53 m/day obtained previously with the tube method on two nearby observation wells [Bouwer, 1970]. These K values were essentially pore measurements on the aquifer immediately around the well bottoms, which were at depths of 9.1 and 6.1 m, respectively.

COMPARISONS

Piezometer method. The geometry to which (8) and (9) apply overlaps the geometry of the coefficients in Figure 3 apply overlaps the geometry of

piezometer method at the lower values of L/r_w . With the piezometer method a cavity is augered out in the soil below a piezometer tube. The water level in the tube is abruptly lowered, and K of the soil around the cavity is calculated from the rate of rise of the water level in the tube [Bouwer and Jackson, 1974]. The equation for K is

$$K = \frac{\pi r_w^2}{A_Y t} \ln \frac{y_0}{y_1} \quad (12)$$

where A_Y is a geometry factor with dimension of length. Values of A_Y were evaluated with an electrolytic tank analog by Youngs [1968], whose results were expressed in tabular form as A_Y/r_w for different values of L/r_w (ranging between 0 and 8), $(H - L)/r_w$, and $(D - H)/r_w$.

Taking a hypothetical case where $L/r_w = 8$, $H/r_w = 12$, and $D/r_w = 16$, K calculated with (5) is 18% below K calculated with (12). This is more than the 10% error normally expected with (8) and (9) for the L/H value of 0.67 in this case. The larger discrepancy may be due to the difference in methodology, or to the fact that the L/r_w value is close to the lower limit of the range covered on the resistance network analog.

An approximate equation for calculating K with the piezometer method was presented by Hvorslev [1951]. The equation, which is based on the assumptions of an ellipsoidal cavity or well screen and infinite vertical extent (upward and downward) of the flow system, contains a term $[1 + (L/2r_w)^2]^{-1/2}$. For most well-slug-test geometries, $L/2r_w$ will be sufficiently large to permit replacement of this term by $L/2r_w$. In that case, however, Hvorslev's equation for Q yields $R_s = L$, which is not true. In reality, R_s is considerably less than L . For example, if $L = 40$ m, $r_w = 0.4$ m, $H = 80$ m, and $D = \infty$, (8) shows that $R_s = 11.9$ m, which is much less than the value of 40 m indicated by Hvorslev's equation. However, since the calculation of K is based on $\ln(R_s/r_w)$ as shown by (5), the error in K is less than the error in R_s (i.e., 36 and 236%, respectively, in this case).

For the above example, the top of the well screen or cavity had been taken at the same level as the water table ($H = 40$ m). R_s would have been 8.6 m and Hvorslev's equation would have yielded a K value that is 50% higher than K given by (5). The larger error is probably due to Hvorslev's assumption of infinite vertical (upward) extent of the flow system, which is not true when the cavity is immediately below the water table. Using Hvorslev's equation for cavities immediately below a confining layer would increase the error to 73%, but this, of course, is due to the fact that a water table is not a solid boundary. Hvorslev's equation for the confining layer case can be used to yield $R_s = 2L$.

Auger hole method. The analog analyses for (8) and (9) and (10) were performed for $L < H$, because short circuiting of the water table and the well prevented simulation of the case where $L = H$. If the analog results are extrapolated to $L = H$, however, the geometry of the system in Figure 1 becomes similar to that of the auger hole technique, for which a number of equations and graphs have been developed to calculate K from the rise of the water level in the well [Bouwer and Jackson, 1974]. Boast and Kirkham [1971], for example, developed the equation

$$K = C_{BK} \frac{\Delta y}{\Delta t} \quad (13)$$

where C_{BK} was determined mathematically and expressed in tabular form for various values of L/r_w , $(D - H)/r_w$, and $(H - L)/r_w$. The rate of rise of the water level in the hole after

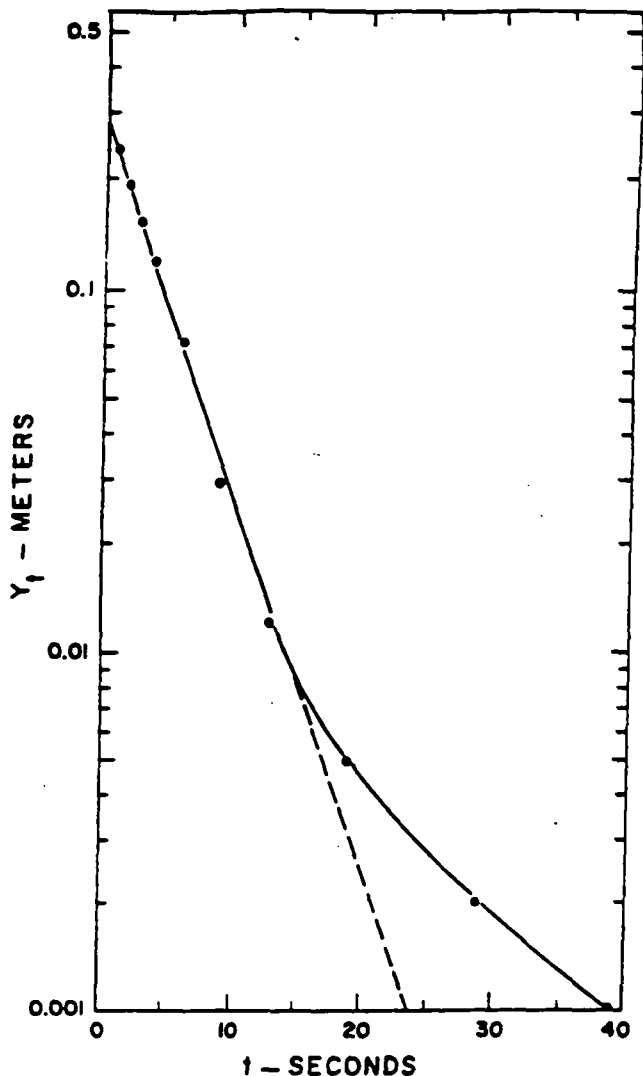


Fig. 4. Plot of y_1 versus t for slug test on east well.

the removal of a slug of water decreases with decreasing y_1 . $\Delta y/\Delta t$ is not a constant and the value of K obtained with this procedure depends on the magnitude of Δy used in the field measurements. The general rule is that Δy should be relatively small.

Taking a hypothetical case where $y_0 = 2.5$ m, $y_1 = 2.4$ m, $\Delta t = 10$ s, $L = H = 5$ m, $D = 6$ m, and $r_w = 0.1$ m, (5) yields a K value that is 36% lower than K calculated with (13). However, if y_1 is taken as 0.5 m, which should give $\Delta t = 394$ s according to the theory that $(1/t) \ln y_0/y_1$ is constant, the K value yielded by (5) is 26% higher than K obtained with (13). If y_1 is taken as 0.9 m, (5) and (13) give identical results.

Slug test on wells in confined aquifers. The confined aquifer for which the slug test by Cooper et al. [1967] was developed is an aquifer with an internal water source, for example, recharge through aquitards or compression of confining layers or other material. This situation is similar to that of the unconfined aquifer presented in this paper because the water table is considered horizontal, like the upper boundary of a confined aquifer, and the water table is a plane source. Thus K or T calculated with (5) or (6) should be of the same order as K calculated with the procedure of Cooper et al. [1967], which involves plotting the rise of the water level in the well and finding the best fit on a family of type curves. Cooper et al. [1967] presented an example of the calculation of T for a well

with $r_c = r_w = 0.076$ m and $L = 98$ m. The resulting value of T was 45.8 m²/day. Values of D and H for this well were not given. However, since the well was 122 m deep and completely penetrating (at least theoretically), D and H must have been between 98 and 122 m. Assuming that both D and H were 100 m, (6) yields $T = 62.8$ m²/day, which is compatible with T obtained by Cooper et al.

CONCLUSIONS

The hydraulic conductivity of an aquifer near a well can be calculated from the rise of the water level in the well after a slug of water is suddenly removed. The calculation is based on the Thiem equation, using an effective radius R_e for the distance over which the head difference between the equilibrium water table in the aquifer and the water level in the well is dissipated. Values of R_e were evaluated by electrical resistance network analog. An empirical equation was then developed to relate R_e to the geometry of the system. This equation is accurate to within 10–25%, depending on how much of the well below the water table is perforated or otherwise open. The technique is applicable to partially or completely penetrating wells in unconfined aquifers. It can also be used to estimate the hydraulic conductivity of confined aquifers that receive water from the upper confining layer through recharge or compression.

The vertical distance between the rising water level in the well and the equilibrium water table in the aquifer must yield a straight line when it is plotted on a logarithmic scale against time. This can be used to check the validity of field measurements and to obtain the best-fitting line for calculating the hydraulic conductivity. Permeable aquifers produce rapidly rising water levels that can be measured with fast-response pressure transducers and strip chart recorders or x-y plotters. The portion of the aquifer sampled for hydraulic conductivity with the slug test is approximately a cylinder with radius R_e and a height somewhat larger than the perforated or otherwise open section of the well.

Hydraulic conductivity values obtained with the slug test are compatible with those yielded by the auger and piezometer techniques where the geometries of the two overlap, and by a slug test for completely penetrating unconfined aquifers.

REFERENCES

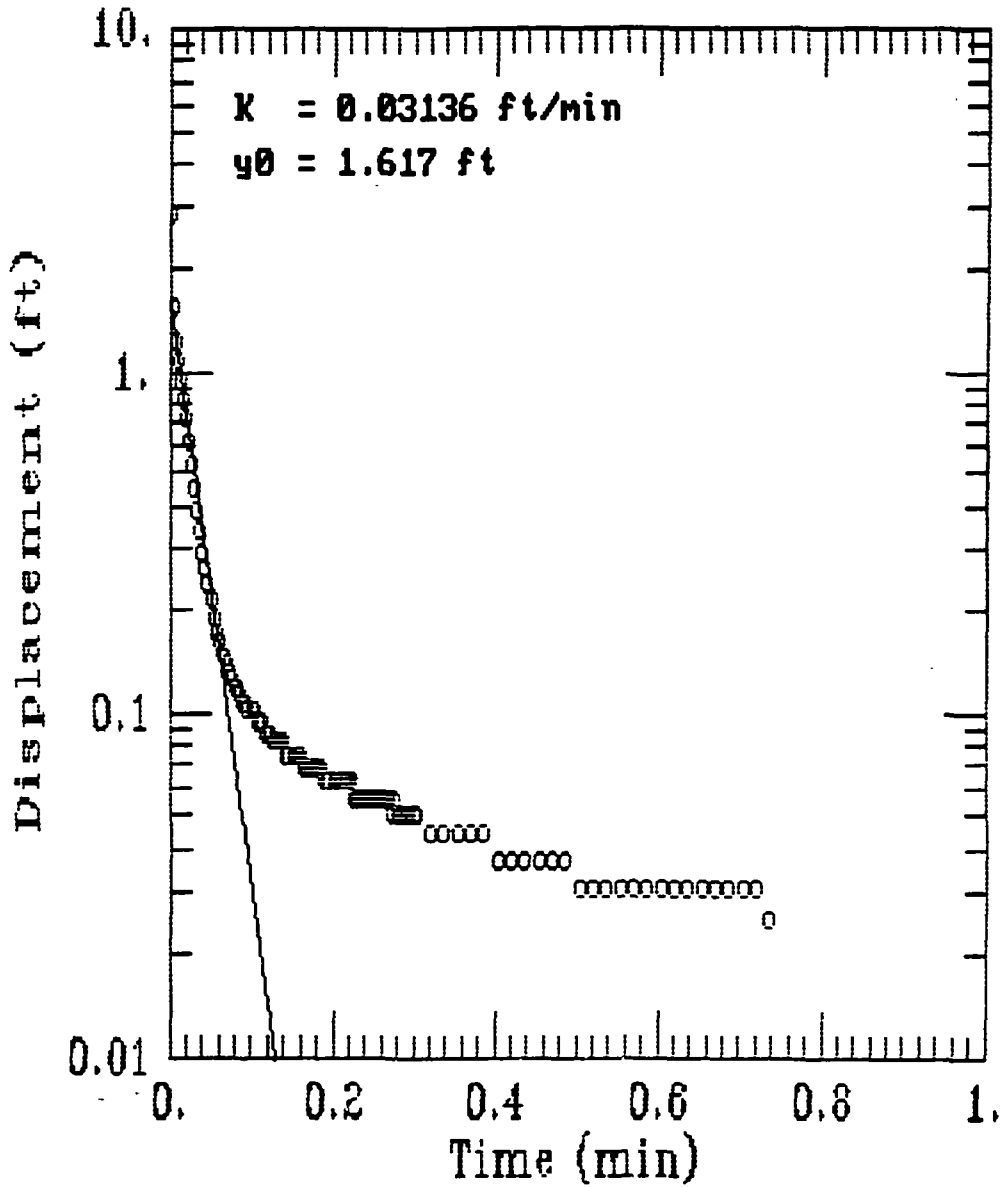
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revised January 19, 1976;
accepted January 23, 1976.)

WELL CLUSTER: A
WELL ID: A1-1
SCREENED INTERVAL: A-14

TEST METHOD: Farrar-Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 45.2 ft/day

A1-1-T2



0.0000 0.000
 0.0033 0.006
 0.0066 0.751
 0.0100 1.497
 0.0133 0.075
 0.0166 0.896
 0.0200 0.991
 0.0233 2.564
 0.0266 0.865
 0.0300 2.886
 0.0333 1.560
 0.0366 1.212
 0.0400 1.067
 0.0433 0.934
 0.0466 0.833
 0.0500 0.720
 0.0533 0.619
 0.0566 0.536
 0.0600 0.454
 0.0633 0.391
 0.0666 0.341
 0.0700 0.296
 0.0733 0.265
 0.0766 0.240
 0.0800 0.214
 0.0833 0.189
 0.0866 0.170
 0.0900 0.164
 0.0933 0.151
 0.0966 0.145
 0.1000 0.138
 0.1033 0.132
 0.1066 0.126
 0.1100 0.119
 0.1133 0.119
 0.1166 0.113
 0.1200 0.107
 0.1233 0.107
 0.1266 0.101
 0.1300 0.101
 0.1333 0.101
 0.1366 0.094
 0.1400 0.094
 0.1433 0.094
 0.1466 0.088
 0.1500 0.088
 0.1533 0.088
 0.1566 0.082
 0.1600 0.082
 0.1633 0.082
 0.1666 0.082
 0.1700 0.082
 0.1733 0.075
 0.1766 0.075
 0.1800 0.075
 0.1833 0.075
 0.1866 0.075
 0.1900 0.075
 0.1933 0.069
 0.1966 0.069

← H_0

$SH = 2.861$
 $\Delta t = 0.7366$

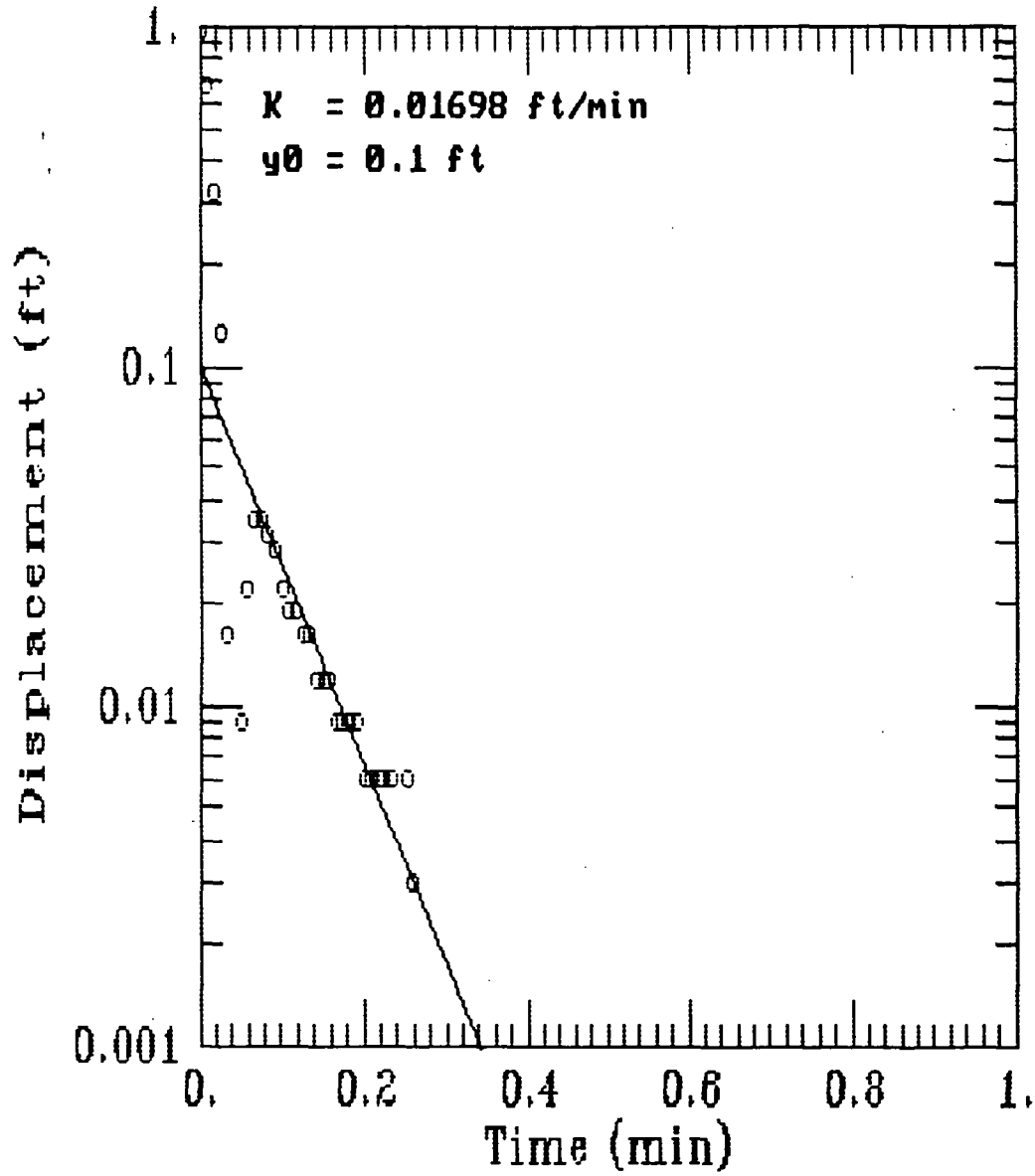
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Column 2:	<u>Head (ft)</u>	
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Column 3:	$t_0 = \underline{\quad}$	$t_1 = \underline{\quad}$

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0.2033	0.069
0.2066	0.069
0.2100	0.069
0.2133	0.069
0.2166	0.069
0.2200	0.063
0.2233	0.063
0.2266	0.063
0.2300	0.063
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0.2400	0.063
0.2433	0.063
0.2466	0.063
0.2500	0.063
0.2533	0.063
0.2566	0.056
0.2600	0.056
0.2633	0.056
0.2666	0.056
0.2700	0.056
0.2733	0.056
0.2766	0.056
0.2800	0.056
0.2833	0.056
0.2866	0.056
0.2900	0.056
0.2933	0.056
0.2966	0.056
0.3000	0.056
0.3033	0.050
0.3066	0.056
0.3100	0.050
0.3133	0.050
0.3166	0.050
0.3200	0.050
0.3233	0.050
0.3266	0.050
0.3300	0.050
0.3333	0.050
0.3500	0.044
0.3666	0.044
0.3833	0.044
0.4000	0.044
0.4166	0.044
0.4333	0.037
0.4500	0.037
0.4666	0.037
0.4833	0.037
0.5000	0.037
0.5166	0.037
0.5333	0.031
0.5500	0.031
0.5666	0.031
0.5833	0.031
0.6000	0.031
0.6166	0.031
0.6333	0.031
0.6500	0.031

0.6666	0.031
0.6833	0.031
0.7000	0.031
0.7166	0.031
0.7333	0.031
0.7500	0.031
0.7666	0.025 ← Hz
0.7833	0.031
0.8000	0.031
0.8166	0.031
0.8333	0.025
0.8500	0.025
0.8666	0.025
0.8833	0.025
0.9000	0.025
0.9166	0.025
0.9333	0.025
0.9500	0.025
0.9666	0.025
0.9833	0.025
1.0000	0.025
1.2000	0.025
1.4000	0.025
1.6000	0.025
1.8000	0.025
2.0000	0.025
2.2000	0.025
2.4000	0.025
2.6000	0.025
2.8000	0.025
3.0000	0.025
3.2000	0.025
3.4000	0.025
3.6000	0.025
3.8000	0.025
4.0000	0.025
4.2000	0.025
4.4000	0.025
4.6000	0.025
4.8000	0.025
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7.6000	0.025
7.8000	0.025
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8.2000	0.025
8.4000	0.031
8.6000	0.025
8.8000	0.025

9.0000	0.031
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10.0000	0.025

A2-T2 REVISION

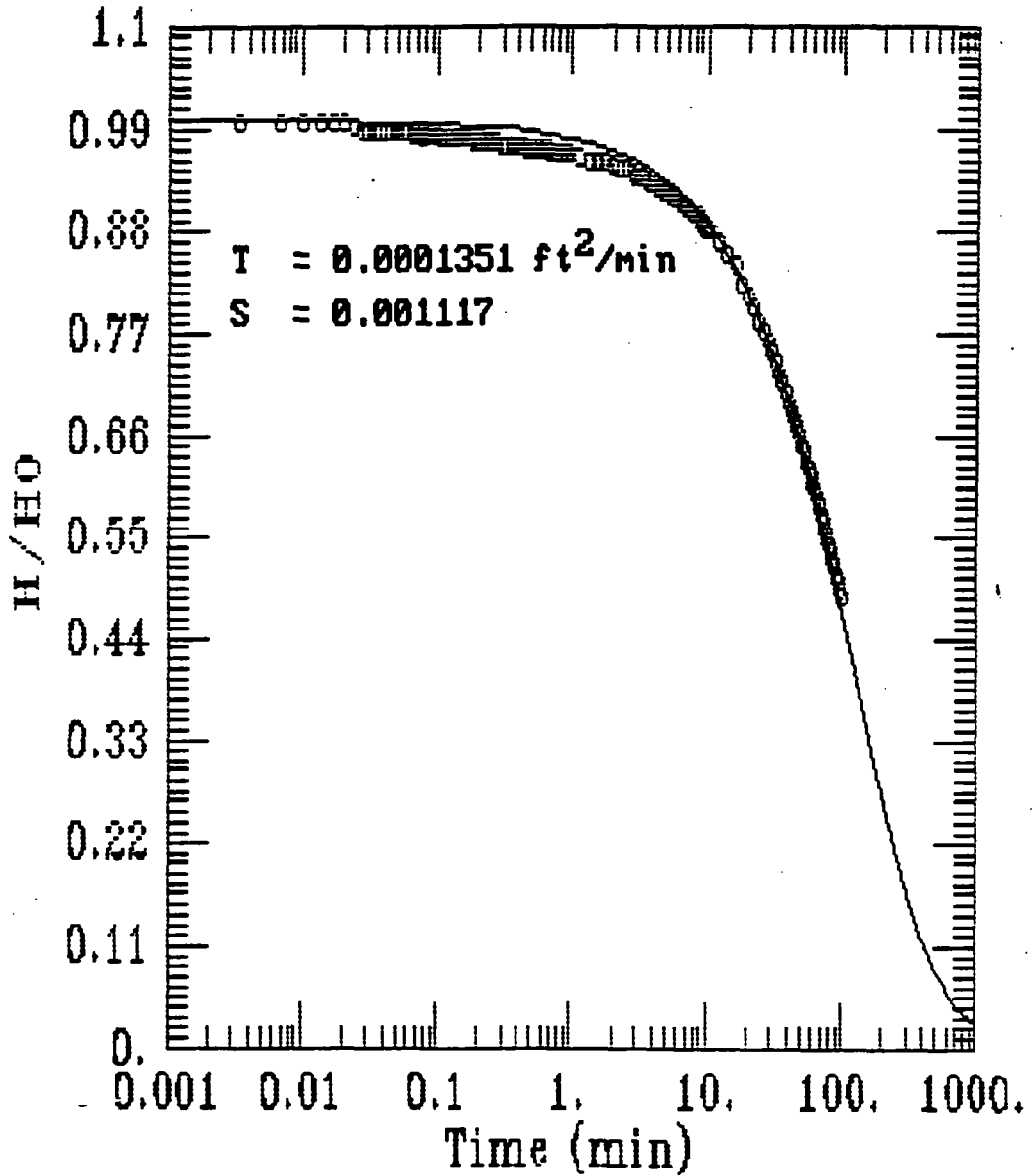


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0.4333	0.003
0.4500	0.003
0.4666	0.000
0.4833	0.003
0.5000	0.000
0.5166	0.000
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0.5666	0.000
0.5833	0.000
0.6000	0.000
0.6166	0.000
0.6333	0.000
0.6500	0.000
0.6666	0.000
0.6833	0.000
0.7000	0.000
0.7166	0.000
0.7333	0.000
0.7500	0.000
0.7666	0.000
0.7833	0.000
0.8000	0.000
0.8166	0.000
0.8333	0.000
0.8500	0.000
0.8666	0.000
0.8833	0.000
0.9000	0.000
0.9166	0.000
0.9333	0.000
0.9500	0.000
0.9666	0.000
0.9833	0.000
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1.0333	0.000
1.0500	0.000
1.0666	0.000
1.0833	0.000
1.1000	0.000
1.1166	0.000
1.1333	0.000
1.1500	0.000
1.1666	0.000
1.1833	0.000
1.2000	0.000
1.2166	0.000
1.2333	0.000
1.2500	0.000
1.2666	0.000
1.2833	0.000
1.3000	0.000
1.3166	0.000
1.3333	0.000
1.3500	0.000
1.3666	0.000
1.3833	0.000
1.4000	0.000
1.4166	0.000
1.4333	0.000
1.4500	0.000
1.4666	0.000
1.4833	0.000
1.5000	0.000
1.5166	0.000
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1.5666	0.000
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1.6500	0.000
1.6666	0.000
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1.7000	0.000
1.7166	0.000
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1.7666	0.000
1.7833	0.000
1.8000	0.000
1.8166	0.000
1.8333	0.000
1.8500	0.000
1.8666	0.000
1.8833	0.000
1.9000	0.000
1.9166	0.000
1.9333	0.000
1.9500	0.000
1.9666	0.000
1.9833	0.000
2.0000	0.000

WELL CLUSTER: A
WELL ID: A4-2
SCREENED INTERVAL: 36-41

TEST METHOD: Couper et al.
SLUG IN/SLUG OUT: Slug out
K-VALUE: 0.013 ft/day

A4-1-T2



0.0000	0.000
0.0033	0.063
0.0066	1.402
0.0100	1.212
0.0133	-0.581
0.0166	1.377
0.0200	0.713
0.0233	2.166
0.0266	0.625
0.0300	2.861
0.0333	1.118
0.0366	2.065
0.0400	1.768
0.0433	2.242
0.0466	2.507
0.0500	2.432
0.0533	2.406
0.0566	2.356
0.0600	2.280
0.0633	2.318
0.0666	2.318
0.0700	2.318
0.0733	2.305
0.0766	2.312
0.0800	2.299
0.0833	2.299
0.0866	2.299
0.0900	2.299
0.0933	2.299
0.0966	2.299
0.1000	2.293
0.1033	2.286
0.1066	2.290
0.1100	2.280
0.1133	2.280
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0.1200	2.280
0.1233	2.280
0.1266	2.280
0.1300	2.280
0.1333	2.280
0.1366	2.280
0.1400	2.274
0.1433	2.274
0.1466	2.274
0.1500	2.274
0.1533	2.267
0.1566	2.274
0.1600	2.274
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0.1666	2.274
0.1700	2.274
0.1733	2.274
0.1766	2.274
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0.1866	2.267
0.1900	2.267
0.1933	2.267
0.1966	2.267
0.2000	2.267
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0.2066	2.267
0.2100	2.267

① Corrected
start

② Stopped @ # 14

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	t = _____	t = _____

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0.2366	2.261
0.2400	2.261
0.2433	2.261
0.2466	2.261
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0.2533	2.261
0.2566	2.261
0.2600	2.255
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0.2666	2.261
0.2700	2.255
0.2733	2.255
0.2766	2.255
0.2800	2.261
0.2833	2.255
0.2866	2.255
0.2900	2.255
0.2933	2.255
0.2966	2.255
0.3000	2.255
0.3033	2.255
0.3066	2.255
0.3100	2.255
0.3133	2.255
0.3166	2.255
0.3200	2.255
0.3233	2.255
0.3266	2.255
0.3300	2.255
0.3333	2.255
0.3500	2.255
0.3666	2.248
0.3833	2.248
0.4000	2.248
0.4166	2.248
0.4333	2.242
0.4500	2.242
0.4666	2.242
0.4833	2.242
0.5000	2.242
0.5166	2.242
0.5333	2.236
0.5500	2.236
0.5666	2.236
0.5833	2.236
0.6000	2.236
0.6166	2.236
0.6333	2.236
0.6500	2.236
0.6666	2.236
0.6833	2.236
0.7000	2.236
0.7166	2.236
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0.7666	2.229
0.7833	2.229
0.8000	2.229
0.8166	2.229

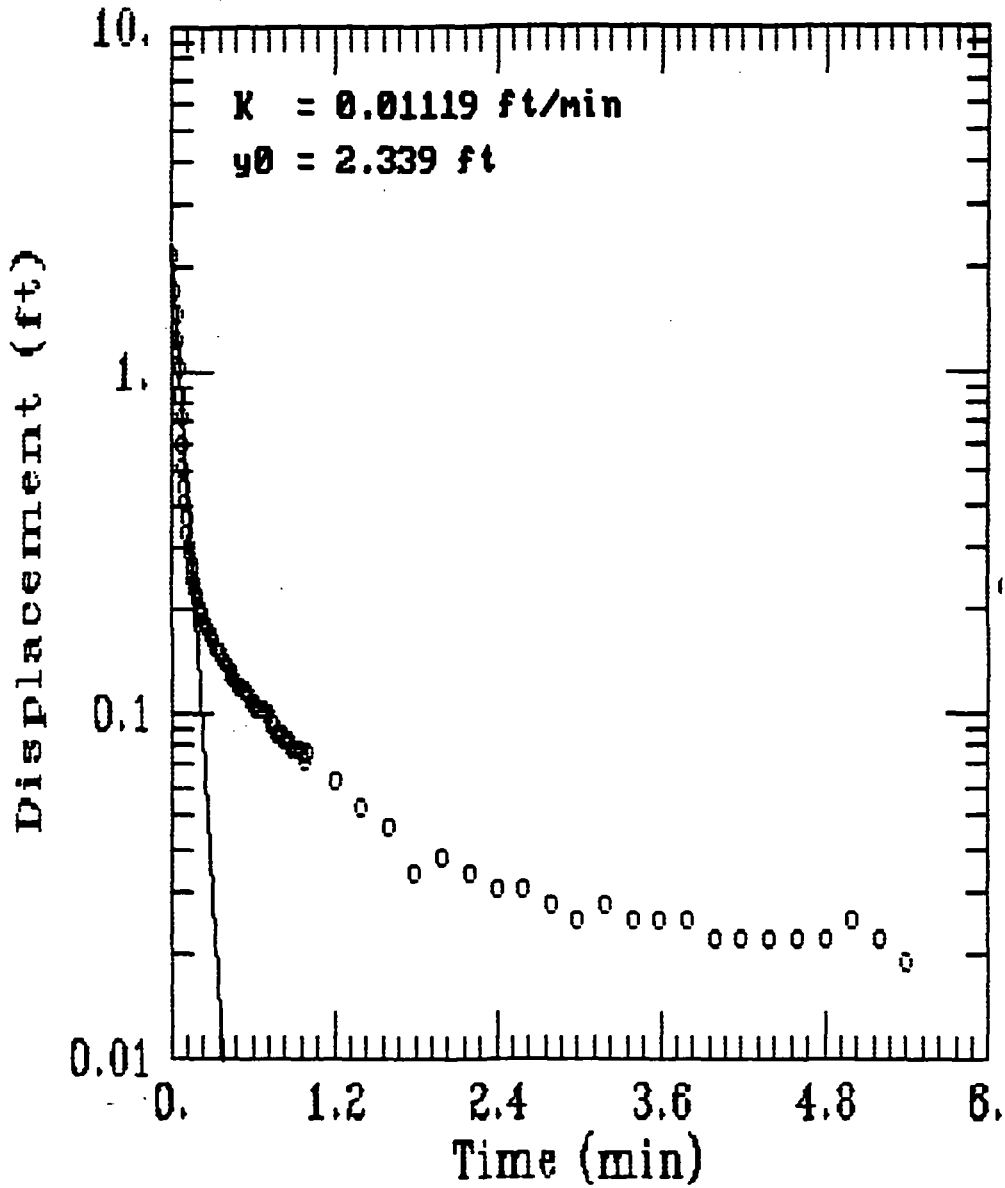
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0.9666	2.223
0.9833	2.223
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1.2000	2.217
1.4000	2.210
1.6000	2.204
1.8000	2.204
2.0000	2.198
2.2000	2.192
2.4000	2.192
2.6000	2.185
2.8000	2.179
3.0000	2.173
3.2000	2.173
3.4000	2.166
3.6000	2.160
3.8000	2.154
4.0000	2.154
4.2000	2.147
4.4000	2.141
4.6000	2.141
4.8000	2.135
5.0000	2.128
5.2000	2.128
5.4000	2.122
5.6000	2.122
5.8000	2.116
6.0000	2.116
6.2000	2.109
6.4000	2.103
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6.8000	2.097
7.0000	2.097
7.2000	2.090
7.4000	2.084
7.6000	2.084
7.8000	2.078
8.0000	2.078
8.2000	2.071
8.4000	2.071
8.6000	2.065
8.8000	2.059
9.0000	2.059
9.2000	2.053
9.4000	2.053
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9.8000	2.040
10.0000	2.040
12.0000	2.008
14.0000	1.977
16.0000	1.951
18.0000	1.907
20.0000	1.876
22.0000	1.844
24.0000	1.812
26.0000	1.787
28.0000	1.762
30.0000	1.737

38.0000	1.636
40.0000	1.610
42.0000	1.585
44.0000	1.566
46.0000	1.547
48.0000	1.528
50.0000	1.503
52.0000	1.490
54.0000	1.459
56.0000	1.446
58.0000	1.427
60.0000	1.408
62.0000	1.396
64.0000	1.377
66.0000	1.358
68.0000	1.345
70.0000	1.332
72.0000	1.313
74.0000	1.294
76.0000	1.282
78.0000	1.263
80.0000	1.250
82.0000	1.238
84.0000	1.219
86.0000	1.206
88.0000	1.200
90.0000	1.174
92.0000	1.168
94.0000	1.156
96.0000	1.137
98.0000	1.124
100.0000	1.118

WELL CLUSTER: B
WELL ID: B1-1
SCREENED INTERVAL: 7-17

TEST METHOD: Pressure Rise
SLUG IN/SLUG OUT: Slugs out
K-VALUE: 16.1 ft/day

B1-T2-1



0.0000	-0.003	0.006
0.0083	0.205	0.839
0.0166	<u>2.172</u>	1.405
0.0250	1.159	0.654
0.0333	1.716	1.633
0.0416	1.450	<u>1.869</u>
0.0500	1.219	1.843
0.0583	1.029	1.811
0.0666	0.858	1.799
0.0750	0.722	1.767
0.0833	0.611	1.754
0.0916	0.525	1.754
0.1000	0.459	1.722
0.1083	0.411	1.697
0.1166	0.367	1.684
0.1250	0.335	1.678
0.1333	0.313	1.665
0.1416	0.291	1.653
0.1500	0.275	1.640
0.1583	0.259	1.627
0.1666	0.247	1.614
0.1750	0.237	1.602
0.1833	0.228	1.589
0.1916	0.221	1.576
0.2000	0.215	1.564
0.2083	0.205	1.557
0.2166	0.202	1.544
0.2250	0.196	1.532
0.2333	0.193	1.525
0.2416	0.186	1.513
0.2500	0.183	1.506
0.2583	0.180	1.494
0.2666	0.174	1.487
0.2750	0.174	1.481
0.2833	0.171	1.468
0.2916	0.167	1.462
0.3000	0.164	1.455
0.3083	0.161	1.449
0.3166	0.161	1.436
0.3250	0.155	1.430
0.3333	0.152	1.424
0.3500	0.148	1.405
0.3666	0.148	1.392
0.3833	0.142	1.379
0.4000	0.139	1.366
0.4166	0.136	1.354
0.4333	0.133	1.335
0.4500	0.129	1.322
0.4666	0.126	1.309
0.4833	0.123	1.297
0.5000	0.120	1.284
0.5166	0.120	1.271
0.5333	0.117	1.258
0.5500	0.117	1.246
0.5666	0.114	1.239
0.5833	0.107	1.227
0.6000	0.107	1.214
0.6166	0.104	1.201
0.6333	0.101	1.189
0.6500	0.101	1.176

5107a
 Δt = 5.58
 Δt = 1.66
 Δt = 9.958

Test:	<u>RH, BA-2 Slug out</u>
File:	<u>RHBA2-TA.dat</u>
Round:	<u>KTEST2</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head R1-1 (ft)</u>
	<u>t = 0.0166 h = 5.40</u>
Column 3:	<u>Head BA-2 (ft)</u>
	<u>t = 0.0416 h = 12.6</u>

0.6666	0.101	1.169
0.6833	0.101	1.163
0.7000	0.098	1.150
0.7166	0.098	1.144
0.7333	0.095	1.131
0.7500	0.091	1.125
0.7666	0.091	1.112
0.7833	0.088	1.106
0.8000	0.088	1.093
0.8166	0.088	1.087
0.8333	0.082	1.074
0.8500	0.082	1.068
0.8666	0.082	1.061
0.8833	0.079	1.049
0.9000	0.079	1.042
0.9166	0.079	1.036
0.9333	0.079	1.023
0.9500	0.079	1.017
0.9666	0.076	1.011
0.9833	0.072	1.004
1.0000	0.076	0.991
1.2000	0.063	0.915
1.4000	0.053	0.839
1.6000	0.047	0.775
1.8000	0.034	0.712
2.0000	0.038	0.674
2.2000	0.034	0.635
2.4000	0.031	0.591
2.6000	0.031	0.565
2.8000	0.028	0.534
3.0000	0.025	0.508
3.2000	0.028	0.483
3.4000	0.025	0.464
3.6000	0.025	0.445
3.8000	0.025	0.426
4.0000	0.022	0.406
4.2000	0.022	0.394
4.4000	0.022	0.381
4.6000	0.022	0.368
4.8000	0.022	0.362
5.0000	0.025	0.349
5.2000	0.022	0.337
5.4000	0.019	0.330
5.6000	0.019	0.317
5.8000	0.015	0.311
6.0000	0.019	0.298
6.2000	0.019	0.292
6.4000	0.019	0.286
6.6000	0.019	0.279
6.8000	0.019	0.273
7.0000	0.022	0.273
7.2000	0.019	0.267
7.4000	0.015	0.254
7.6000	0.019	0.248
7.8000	0.019	0.248
8.0000	0.019	0.241
8.2000	0.015	0.241
8.4000	0.015	0.228
8.6000	0.015	0.228
8.8000	0.019	0.228

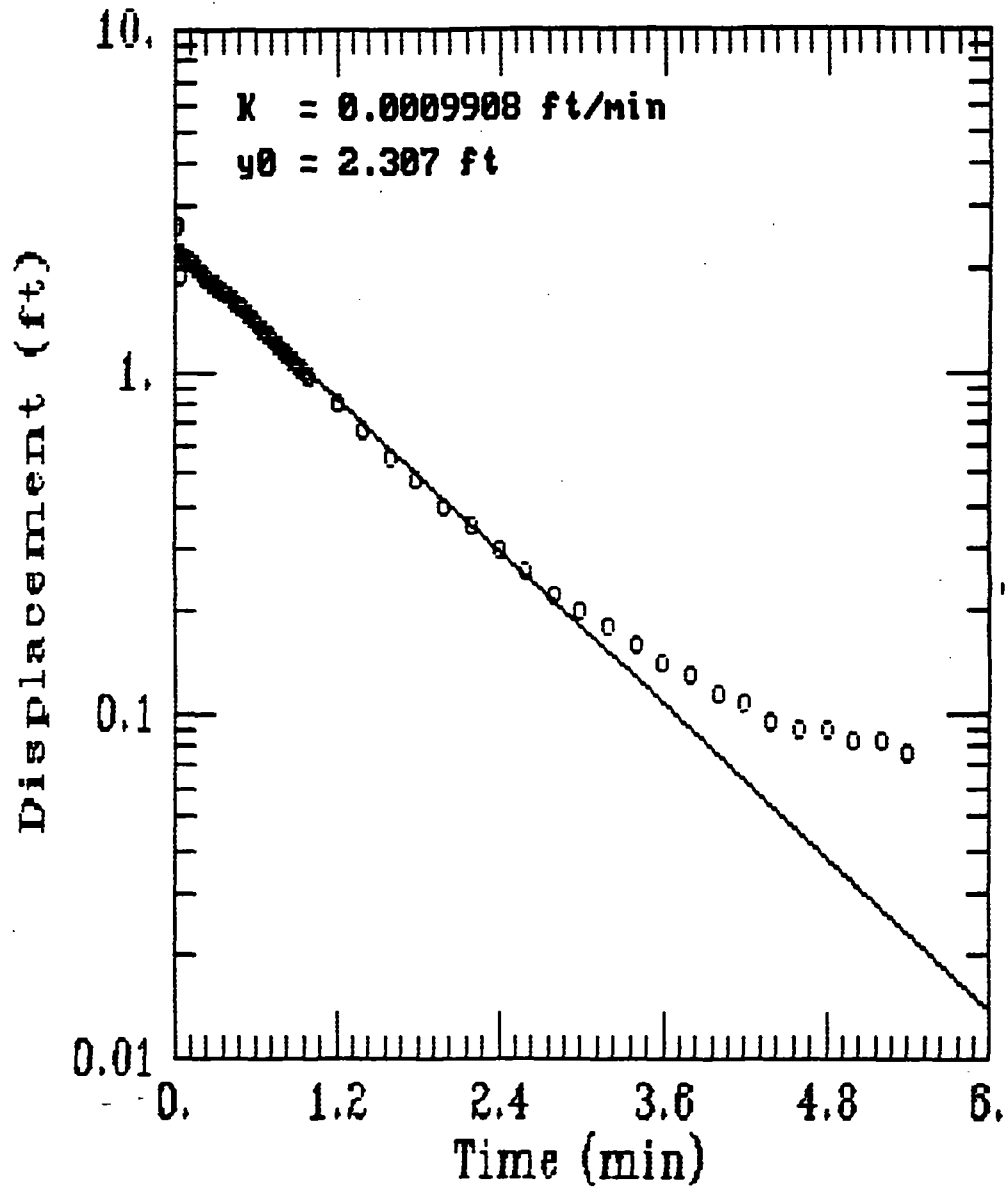
5.4
 ③ 0.019

9.0000	0.015	0.222
9.2000	0.019	0.222
9.4000	0.019	0.222
9.6000	0.019	0.216
9.8000	0.019	0.216
10.0000	0.019	0.209

WELL CLUSTER: B
WELL ID: B2-1
SCREENED INTERVAL: 29-39

TEST METHOD: Banner Rise
SLUG IN/SLUG OUT: Slu out
K-VALUE: 1.43 ft/day

B2-T2-1



0.0000	0.006
0.0083	0.597
0.0166	1.735
0.0250	1.881
0.0333	2.650
0.0416	1.913
0.0500	2.193
0.0583	2.174
0.0666	2.142
0.0750	2.136
0.0833	2.123
0.0916	2.116
0.1000	2.110
0.1083	2.097
0.1166	2.091
0.1250	2.078
0.1333	2.066
0.1416	2.053
0.1500	2.040
0.1583	2.028
0.1666	2.008
0.1750	1.996
0.1833	1.977
0.1916	1.964
0.2000	1.951
0.2083	1.932
0.2166	1.919
0.2250	1.900
0.2333	1.881
0.2416	1.869
0.2500	1.850
0.2583	1.837
0.2666	1.824
0.2750	1.811
0.2833	1.799
0.2916	1.786
0.3000	1.780
0.3083	1.767
0.3166	1.761
0.3250	1.748
0.3333	1.735
0.3500	1.716
0.3666	1.697
0.3833	1.678
0.4000	1.653
0.4166	1.633
0.4333	1.608
0.4500	1.589
0.4666	1.570
0.4833	1.544
0.5000	1.525
0.5166	1.506
0.5333	1.481
0.5500	1.455
0.5666	1.436
0.5833	1.417
0.6000	1.398
0.6166	1.373
0.6333	1.354
0.6500	1.335

$\Delta t = 5.3667$

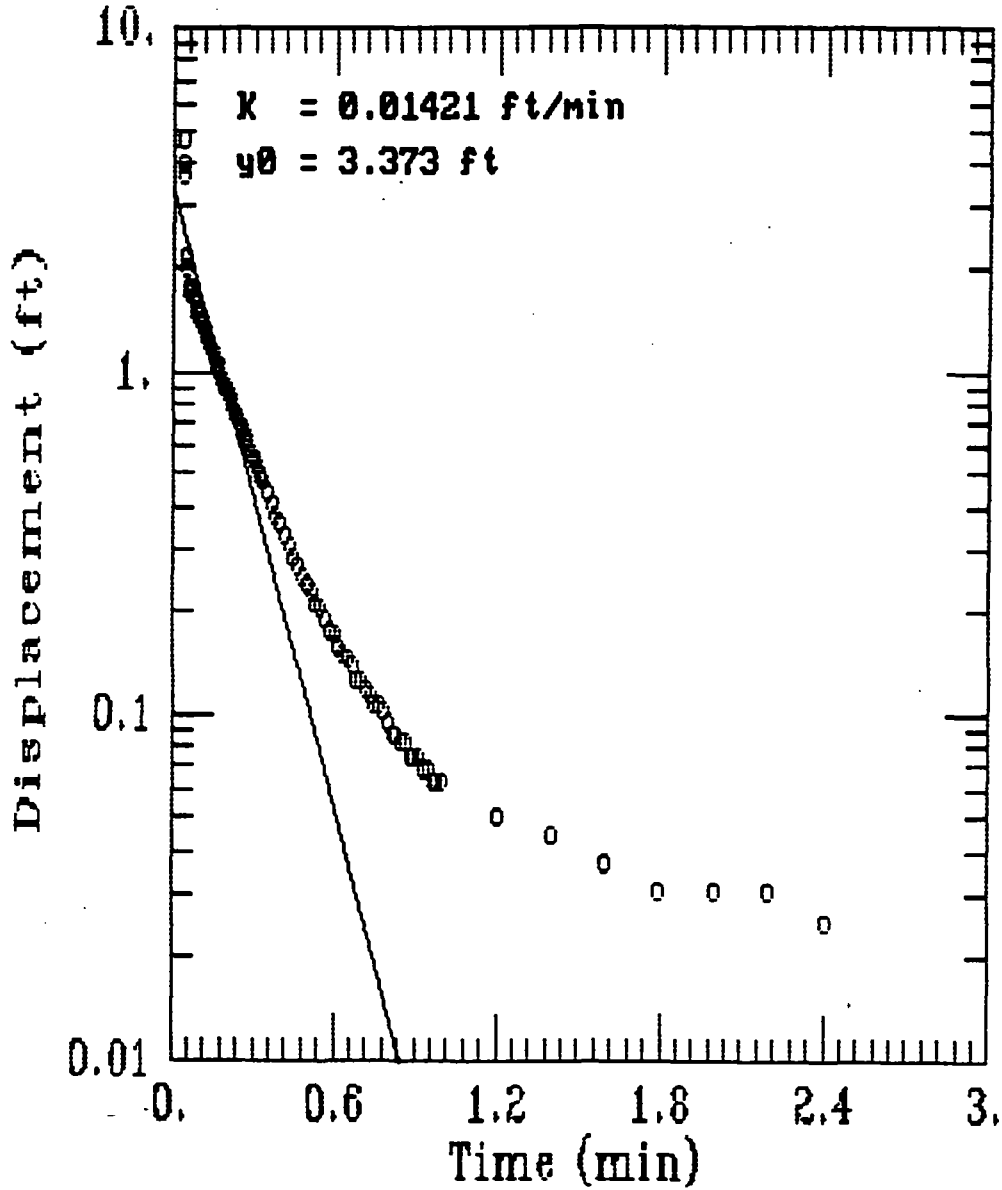
Test:	B2-1 Slg out
File:	B2-T2-1.Dat
Round:	KTEST 2
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	$t = 0.0333 \quad t = 5.40$
Column 3:	
	$t = \quad \quad t = \quad$

0.6666	1.316
0.6833	1.297
0.7000	1.271
0.7166	1.252
0.7333	1.233
0.7500	1.214
0.7666	1.195
0.7833	1.176
0.8000	1.157
0.8166	1.144
0.8333	1.125
0.8500	1.106
0.8666	1.087
0.8833	1.074
0.9000	1.061
0.9166	1.042
0.9333	1.023
0.9500	1.010
0.9666	0.991
0.9833	0.979
1.0000	0.966
1.2000	0.801
1.4000	0.667
1.6000	0.559
1.8000	0.476
2.0000	0.400
2.2000	0.349
2.4000	0.298
2.6000	0.260
2.8000	0.222
3.0000	0.197
3.2000	0.178
3.4000	0.158
3.6000	0.139
3.8000	0.127
4.0000	0.114
4.2000	0.108
4.4000	0.095
4.6000	0.089
4.8000	0.089
5.0000	0.082
5.2000	0.082
5.4000	0.076

WELL CLUSTER: E
WELL ID: B3
SCREENED INTERVAL: 32.75-43.75

TEST METHOD: Banner Rise
SLUG IN/SLUG OUT: Skat
K-VALUE: 20.5 ft/day

B3-T2



0.0000	0.000
0.0033	0.012
0.0066	0.871
0.0100	1.515
0.0133	-0.006
0.0166	-0.770
0.0200	1.717
0.0233	3.706
0.0266	2.279
0.0300	3.132
0.0333	2.942
0.0366	3.359
0.0400	4.754
0.0433	3.984
0.0466	3.694
0.0500	2.014
0.0533	2.140
0.0566	1.736
0.0600	1.742
0.0633	1.723
0.0666	1.742
0.0700	1.755
0.0733	1.717
0.0766	1.667
0.0800	1.673
0.0833	1.616
0.0866	1.629
0.0900	1.521
0.0933	1.465
0.0966	1.477
0.1000	1.477
0.1033	1.458
0.1066	1.408
0.1100	1.389
0.1133	1.376
0.1166	1.345
0.1200	1.319
0.1233	1.319
0.1266	1.281
0.1300	1.250
0.1333	1.231
0.1366	1.206
0.1400	1.187
0.1433	1.168
0.1466	1.149
0.1500	1.136
0.1533	1.111
0.1566	1.098
0.1600	1.073
0.1633	1.060
0.1666	1.041
0.1700	1.035
0.1733	1.010
0.1766	0.991
0.1800	0.972
0.1833	0.959
0.1866	0.953
0.1900	0.928
0.1933	0.915
0.1966	0.896

14 = 4.729

ΔC = 2.76

Test:	B3 Slug out
File:	B3-T2-2at
Round:	KTEST
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	t ₀ = 0.400 t ₁ = 2.40
Column 3:	
	t ₀ = _____ t ₁ = _____

0.2000	0.890
0.2033	0.871
0.2066	0.865
0.2100	0.839
0.2133	0.858
0.2166	0.827
0.2200	0.814
0.2233	0.795
0.2266	0.776
0.2300	0.770
0.2333	0.751
0.2366	0.745
0.2400	0.732
0.2433	0.719
0.2466	0.707
0.2500	0.700
0.2533	0.688
0.2566	0.675
0.2600	0.663
0.2633	0.656
0.2666	0.644
0.2700	0.637
0.2733	0.631
0.2766	0.618
0.2800	0.606
0.2833	0.599
0.2866	0.593
0.2900	0.580
0.2933	0.574
0.2966	0.568
0.3000	0.555
0.3033	0.549
0.3066	0.543
0.3100	0.530
0.3133	0.524
0.3166	0.517
0.3200	0.505
0.3233	0.505
0.3266	0.492
0.3300	0.486
0.3333	0.479
0.3500	0.448
0.3666	0.410
0.3833	0.385
0.4000	0.359
0.4166	0.334
0.4333	0.309
0.4500	0.290
0.4666	0.271
0.4833	0.252
0.5000	0.239
0.5166	0.227
0.5333	0.208
0.5500	0.202
0.5666	0.189
0.5833	0.176
0.6000	0.170
0.6166	0.157
0.6333	0.151
0.6500	0.145

0.6666	0.138
0.6833	0.126
0.7000	0.126
0.7166	0.119
0.7333	0.113
0.7500	0.107
0.7666	0.107
0.7833	0.101
0.8000	0.094
0.8166	0.088
0.8333	0.088
0.8500	0.082
0.8666	0.082
0.8833	0.075
0.9000	0.075
0.9166	0.075
0.9333	0.069
0.9500	0.069
0.9666	0.063
0.9833	0.063
1.0000	0.063
1.2000	0.050
1.4000	0.044
1.6000	0.037
1.8000	0.031
2.0000	0.031
2.2000	0.031
2.4000	0.025
2.6000	0.025
2.8000	0.025
3.0000	0.025
3.2000	0.025
3.4000	0.025
3.6000	0.025
3.8000	0.025
4.0000	0.025
4.2000	0.025
4.4000	0.018
4.6000	0.018
4.8000	0.018
5.0000	0.018
5.2000	0.018
5.4000	0.025
5.6000	0.018
5.8000	0.018
6.0000	0.018
6.2000	0.018
6.4000	0.018
6.6000	0.018
6.8000	0.018
7.0000	0.018
7.2000	0.018
7.4000	0.018
7.6000	0.018
7.8000	0.018
8.0000	0.018
8.2000	0.018
8.4000	0.018
8.6000	0.018
8.8000	0.018

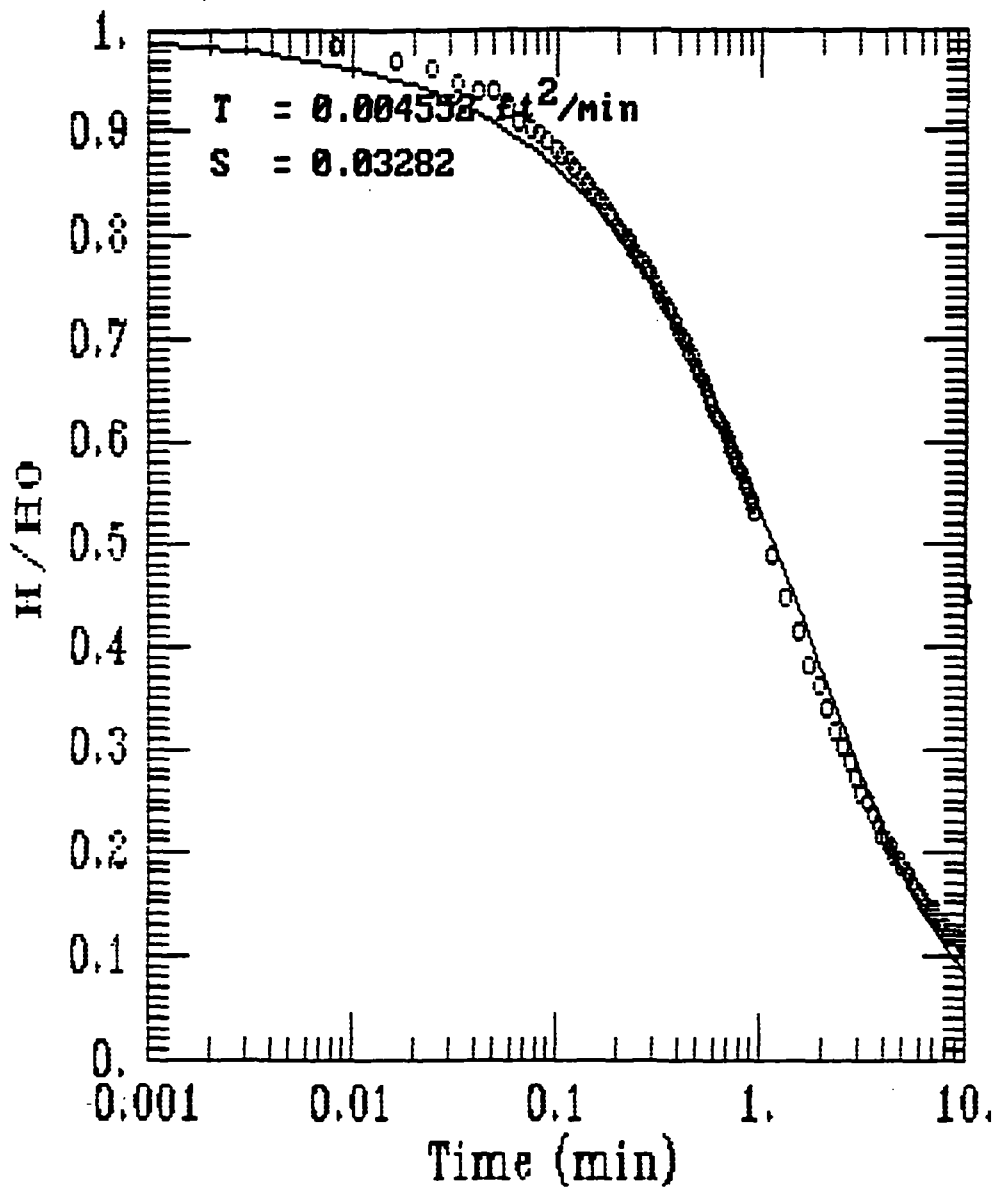
0.24

9.0000	0.018
9.2000	0.018
9.4000	0.018
9.6000	0.018
9.8000	0.018
10.0000	0.012

WELL CLUSTER: B
WELL ID: R4-2
SCREENED INTERVAL: 50.5-60.5

TEST METHOD: Cooper et al.
SLUG IN/SLUG OUT: Slut out
K-VALUE: 0.37 ft/day

B42-T2-1



0.0000	-0.003	0.006
0.0083	0.205	0.839
0.0166	2.172	1.405
0.0250	1.159	0.654
0.0333	1.716	1.633
0.0416	1.450	1.869
0.0500	1.219	1.843
0.0583	1.029	1.811
0.0666	0.858	1.799
0.0750	0.722	1.767
0.0833	0.611	1.754
0.0916	0.525	1.754
0.1000	0.459	1.722
0.1083	0.411	1.697
0.1166	0.367	1.684
0.1250	0.335	1.678
0.1333	0.313	1.665
0.1416	0.291	1.653
0.1500	0.275	1.640
0.1583	0.259	1.627
0.1666	0.247	1.614
0.1750	0.237	1.602
0.1833	0.228	1.589
0.1916	0.221	1.576
0.2000	0.215	1.564
0.2083	0.205	1.557
0.2166	0.202	1.544
0.2250	0.196	1.532
0.2333	0.193	1.525
0.2416	0.186	1.513
0.2500	0.183	1.506
0.2583	0.180	1.494
0.2666	0.174	1.487
0.2750	0.174	1.481
0.2833	0.171	1.468
0.2916	0.167	1.462
0.3000	0.164	1.455
0.3083	0.161	1.449
0.3166	0.161	1.436
0.3250	0.155	1.430
0.3333	0.152	1.424
0.3500	0.148	1.405
0.3666	0.148	1.392
0.3833	0.142	1.379
0.4000	0.139	1.366
0.4166	0.136	1.354
0.4333	0.133	1.335
0.4500	0.129	1.322
0.4666	0.126	1.309
0.4833	0.123	1.297
0.5000	0.120	1.284
0.5166	0.120	1.271
0.5333	0.117	1.258
0.5500	0.117	1.246
0.5666	0.114	1.239
0.5833	0.107	1.227
0.6000	0.107	1.214
0.6166	0.104	1.201
0.6333	0.101	1.189
0.6500	0.101	1.176

DATA

E1 $\Delta H = 2.172$

$\Delta t = 5.38$

E42 $\Delta H = 1.66$

$\Delta t = 9.958$

Test:	<u>RH, RA-2 slug out</u>
File:	<u>R1R42-TA.dat</u>
Round:	<u>KTEST2</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head R1-1 (ft)</u>
	$t = 0.0166 \quad h = 5.40$
Column 3:	<u>Head B4-2 (ft)</u>
	$t = 0.0416 \quad h = 10.0$

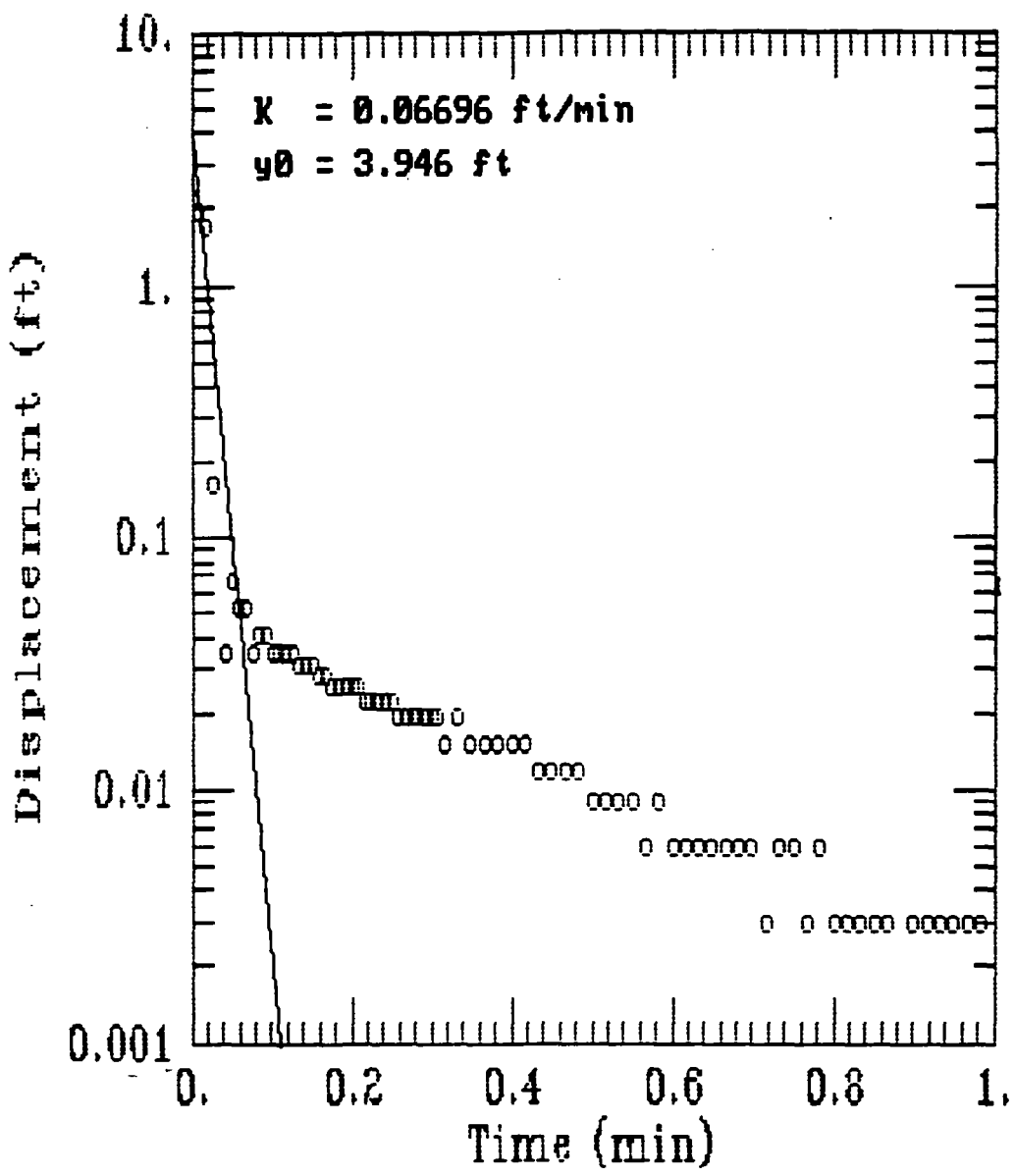
0.6666	0.101	1.169
0.6833	0.101	1.163
0.7000	0.098	1.150
0.7166	0.098	1.144
0.7333	0.095	1.131
0.7500	0.091	1.125
0.7666	0.091	1.112
0.7833	0.088	1.106
0.8000	0.088	1.093
0.8166	0.088	1.087
0.8333	0.082	1.074
0.8500	0.082	1.068
0.8666	0.082	1.061
0.8833	0.079	1.049
0.9000	0.079	1.042
0.9166	0.079	1.036
0.9333	0.079	1.023
0.9500	0.079	1.017
0.9666	0.076	1.011
0.9833	0.072	1.004
1.0000	0.076	0.991
1.2000	0.063	0.915
1.4000	0.053	0.839
1.6000	0.047	0.775
1.8000	0.034	0.712
2.0000	0.038	0.674
2.2000	0.034	0.635
2.4000	0.031	0.591
2.6000	0.031	0.565
2.8000	0.028	0.534
3.0000	0.025	0.508
3.2000	0.028	0.483
3.4000	0.025	0.464
3.6000	0.025	0.445
3.8000	0.025	0.426
4.0000	0.022	0.406
4.2000	0.022	0.394
4.4000	0.022	0.381
4.6000	0.022	0.368
4.8000	0.022	0.362
5.0000	0.025	0.349
5.2000	0.022	0.337
5.4000	0.019	0.330
5.6000	0.019	0.317
5.8000	0.015	0.311
6.0000	0.019	0.298
6.2000	0.019	0.292
6.4000	0.019	0.286
6.6000	0.019	0.279
6.8000	0.019	0.273
7.0000	0.022	0.273
7.2000	0.019	0.267
7.4000	0.015	0.254
7.6000	0.019	0.248
7.8000	0.019	0.248
8.0000	0.019	0.241
8.2000	0.015	0.241
8.4000	0.015	0.228
8.6000	0.015	0.228
8.8000	0.019	0.228

9.0000	0.015	0.222
9.2000	0.019	0.222
9.4000	0.019	0.222
9.6000	0.019	0.216
9.8000	0.019	0.216
10.0000	0.019	0.209

WELL CLUSTER: C
WELL ID: C1-1
SCREENED INTERVAL: 13.5-23.5

TEST METHOD: Flow-Back
SLUG IN/SLUG OUT: Slug out
K-VALUE: 96.4 ft/day

c11-t2-1



① C11-T2-1.dat

0.0000	0.000
0.0083	0.000
0.0166	2.182
0.0250	1.942
0.0333	1.688
0.0416	0.164
0.0500	-0.038
0.0583	0.034
0.0666	0.066
0.0750	0.053
0.0833	0.053
0.0916	0.034
0.1000	0.041
0.1083	0.041
0.1166	0.034
0.1250	0.034
0.1333	0.034
0.1416	0.034
0.1500	0.031
0.1583	0.031
0.1666	0.031
0.1750	0.028
0.1833	0.028
0.1916	0.025
0.2000	0.025
0.2083	0.025
0.2166	0.025
0.2250	0.025
0.2333	0.022
0.2416	0.022
0.2500	0.022
0.2583	0.022
0.2666	0.022
0.2750	0.019
0.2833	0.019
0.2916	0.019
0.3000	0.019
0.3083	0.019
0.3166	0.019
0.3250	0.019
0.3333	0.015
0.3500	0.019
0.3666	0.015
0.3833	0.015
0.4000	0.015
0.4166	0.015
0.4333	0.015
0.4500	0.012
0.4666	0.012
0.4833	0.012
0.5000	0.012
0.5166	0.009
0.5333	0.009
0.5500	0.009
0.5666	0.009
0.5833	0.006
0.6000	0.009
0.6166	0.006
0.6333	0.006
0.6500	0.006

$\Delta u = 2.7 = ?$
 $\Delta t = 1.966 = ?$

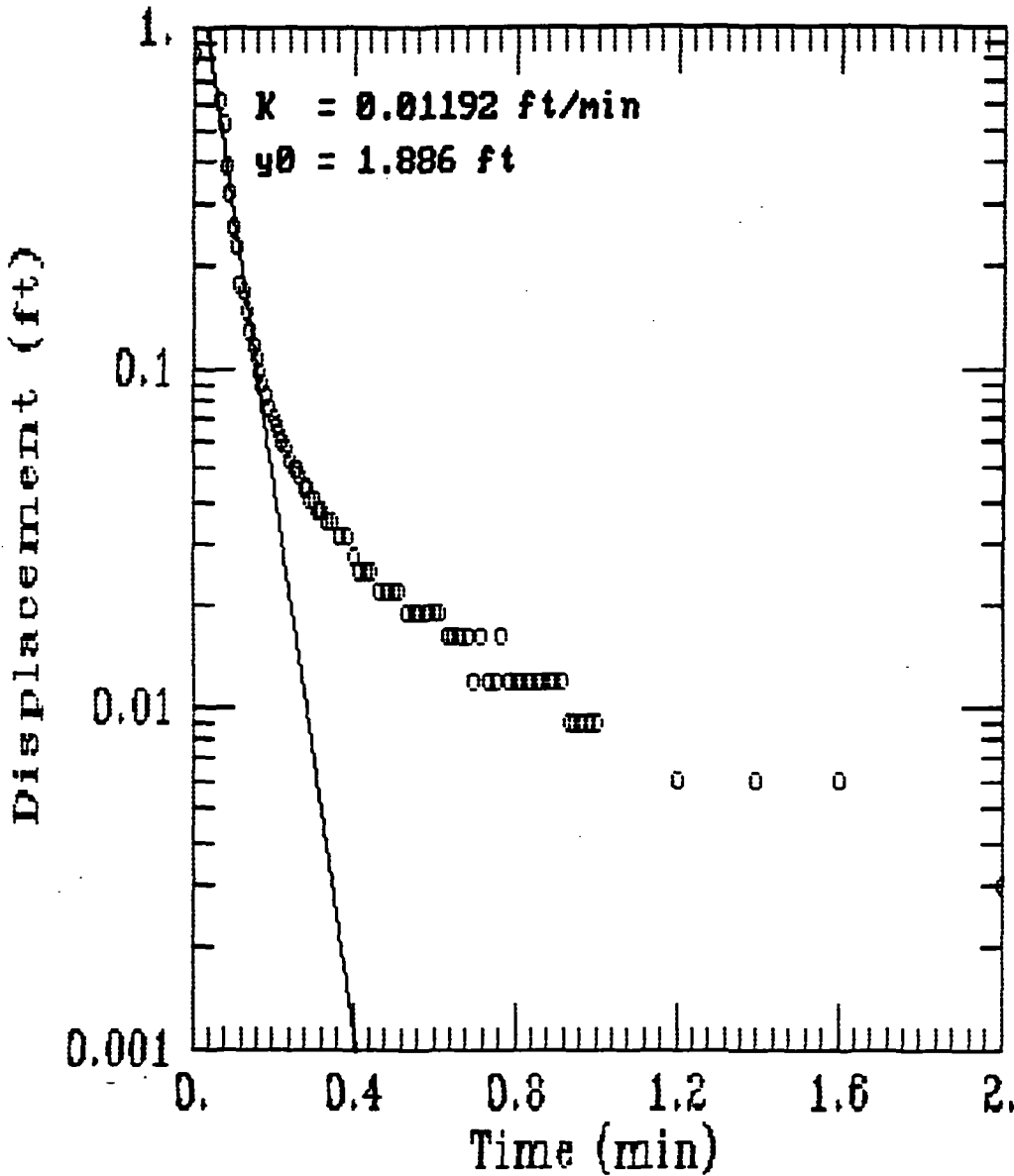
Test:	C1-1	slug out
File:	C11-T2-1	.dat
Round:	KTEST 2	
Column 1:	Elapsed time (min)	
Column 2:	Head (ft)	
	$t_b = 0.0166$	$t_c = 0.9233$
Column 3:		
	$t_b =$	$t_c =$

0.6666	0.006
0.6833	0.006
0.7000	0.006
0.7166	0.006
0.7333	0.003
0.7500	0.006
0.7666	0.006
0.7833	0.003
0.8000	0.006
0.8166	0.003
0.8333	0.003
0.8500	0.003
0.8666	0.003
0.8833	0.003
0.9000	0.000
0.9166	0.003
0.9333	0.003
0.9500	0.003
0.9666	0.003
0.9833	0.003
1.0000	0.003
1.2000	0.000
1.4000	0.000
1.6000	0.000
1.8000	0.000
2.0000	-0.003
2.2000	-0.003
2.4000	-0.006

WELL CLUSTER: D
WELL ID: D1-1
SCREENED INTERVAL: 9-24

TEST METHOD: Power Line
SLUG IN/SLUG OUT: Slug out
K-VALUE: 17.2 ft/day

D1-T2-1



D1-T2-1
slugt1
0.82
0.0833333
^ .260417
.ugt2

② D1-T2-1.dat

40
15
12.54
tsdata
0.0083 0.157 1
0.025 0.575 1
0.0333 0.82 1
0.0416 0.138 1
0.05 0.653 1
0.0583 0.392 1
0.0666 0.604 1
0.075 0.518 1
0.0833 0.395 1
0.0916 0.324 1
0.1 0.26 1
0.1083 0.228 1
0.1166 0.176 1
0.125 0.167 1
0.1333 0.148 1
0.1416 0.128 1
0.15 0.115 1
0.1583 0.106 1
0.1666 0.096 1
0.175 0.09 1
1833 0.083 1
.1916 0.077 1
0.2 0.07 1
0.2083 0.067 1
0.2166 0.064 1
0.225 0.061 1
0.2333 0.057 1
0.2416 0.054 1
0.25 0.051 1
0.2583 0.051 1
0.2666 0.048 1
0.275 0.045 1
0.2833 0.045 1
0.2916 0.041 1
0.3 0.041 1
0.3083 0.038 1
0.3166 0.038 1
0.325 0.038 1
0.3333 0.035 1
0.35 0.035 1
0.3666 0.032 1
0.3833 0.032 1
0.4 0.028 1
0.4166 0.025 1
0.4333 0.025 1
^ 45 0.025 1
4666 0.022 1
0.4833 0.022 1
0.5 0.022 1
0.5166 0.022 1

$\Delta H = 0.317$
 $\Delta t = 1.0662$

Test:	<u>D1 slug test</u>
File:	<u>D1-T2-1.dat</u>
Round:	<u>KTEST2</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head (ft)</u>
	<u>t₀ = 0.0333 t₁ = 2.0</u>
Column 3:	<u>t₀ = _____ t₁ = _____</u>

0.5333	0.019	1
0.55	0.019	1
0.5666	0.019	1
0.5833	0.019	1
6	0.019	1
.6166	0.019	1
0.6333	0.016	1
0.65	0.016	1
0.6666	0.016	1
0.6833	0.016	1
0.7	0.012	1
0.7166	0.016	1
0.7333	0.012	1
0.75	0.012	1
0.7666	0.016	1
0.7833	0.012	1
0.8	0.012	1
0.8166	0.012	1
0.8333	0.012	1
0.85	0.012	1
0.8666	0.012	1
0.8833	0.012	1
0.9	0.012	1
0.9166	0.012	1
0.9333	0.009	1
0.95	0.009	1
0.9666	0.009	1
0.9833	0.009	1
1	0.009	1
1.2	0.006	1
4	0.006	1
.6	0.006	1
2	0.003	1
2.2	0.003	1
2.4	0.003	1
2.6	0.003	1
2.8	0.003	1

0.0083

0.157

DH-72-1. PRN

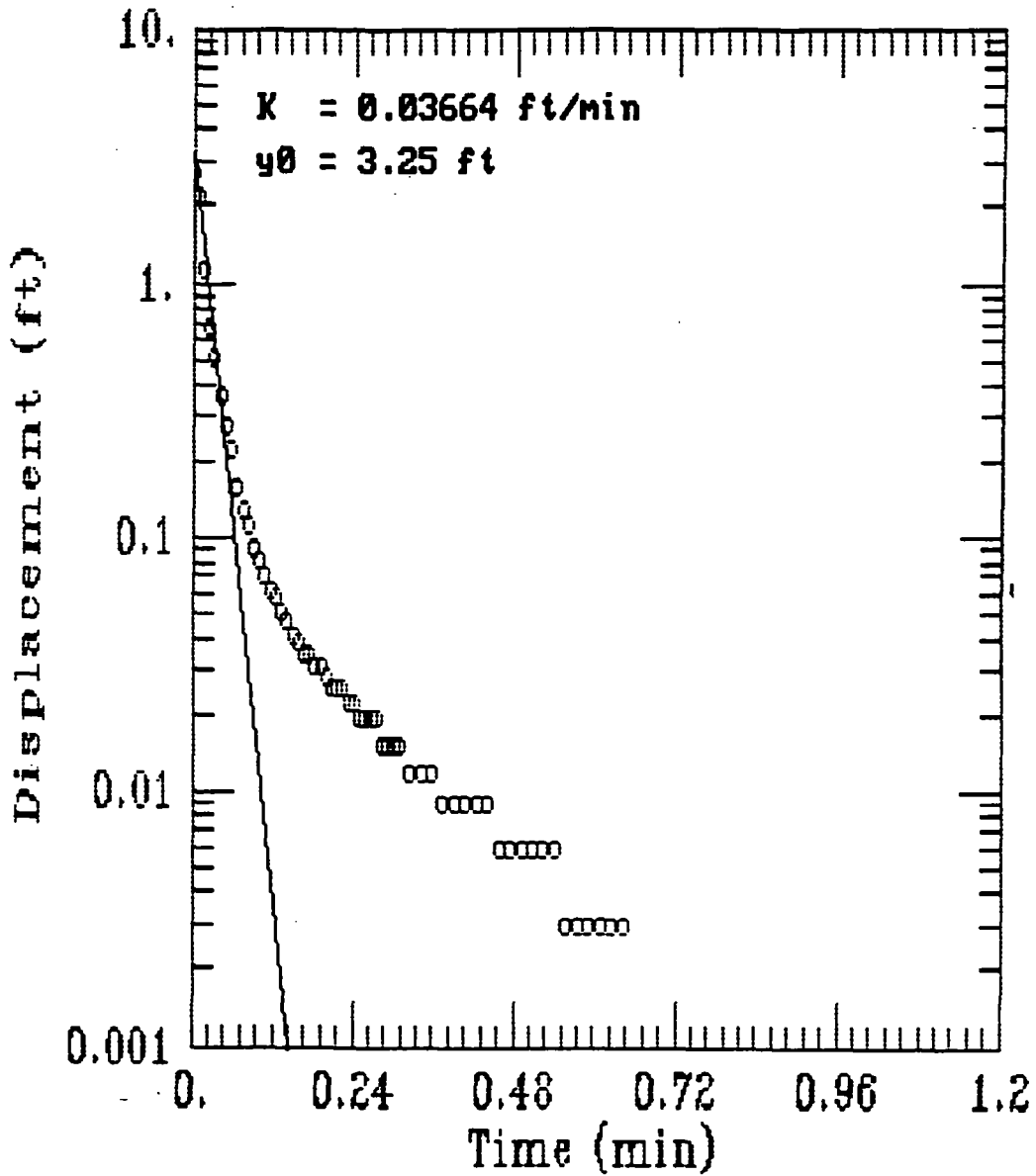
0.025	0.575
0.0333	0.82
0.0416	0.138
0.05	0.653
0.0583	0.392
0.0666	0.604
0.075	0.518
0.0833	0.395
0.0916	0.324
0.1	0.26
0.1083	0.228
0.1166	0.176
0.125	0.167
0.1333	0.148
0.1416	0.128
0.15	0.115
0.1583	0.106
0.1666	0.096
0.175	0.09
0.1833	0.083
0.1916	0.077
0.2	0.07
0.2083	0.067
0.2166	0.064
0.225	0.061
0.2333	0.057
0.2416	0.054
0.25	0.051
0.2583	0.051
0.2666	0.048
0.275	0.045
0.2833	0.045
0.2916	0.041
0.3	0.041
0.3083	0.038
0.3166	0.038
0.325	0.038
0.3333	0.035
0.35	0.035
0.3666	0.032
0.3833	0.032
0.4	0.028
0.4166	0.025
0.4333	0.025
0.45	0.025
0.4666	0.022
0.4833	0.022
0.5	0.022
0.5166	0.022
0.5333	0.019
0.55	0.019
0.5666	0.019
0.5833	0.019
0.6	0.019
0.6166	0.019
0.6333	0.016
0.65	0.016
0.6666	0.016
0.6833	0.016

0.7	0.012
0.7166	0.016
0.7333	0.012
0.75	0.012
0.7666	0.016
0.7833	0.012
0.8	0.012
0.8166	0.012
0.8333	0.012
0.85	0.012
0.8666	0.012
0.8833	0.012
0.9	0.012
0.9166	0.012
0.9333	0.009
0.95	0.009
0.9666	0.009
0.9833	0.009
1	0.009
1.2	0.006
1.4	0.006
1.6	0.006
2	0.003
2.2	0.003
2.4	0.003
2.6	0.003
2.8	0.003

WELL CLUSTER: E
WELL ID: E1-1
SCREENED INTERVAL: 9-24

TEST METHOD: Forsser Pipe
SLUG IN/SLUG OUT: Slug out
K-VALUE: 52.8 ft/day

e1-t2-1



	E1	E2
0.0000	0.000	0.000
0.0083	0.000	-0.003
0.0166	1.248	0.337
0.0250	2.699	0.495
0.0333	2.138	-0.019
0.0416	1.127	0.913
0.0500	0.662	1.006
0.0583	0.516	1.106
0.0666	0.367	1.241
0.0750	0.275	1.344
0.0833	0.221	1.312
0.0916	0.158	1.296
0.1000	0.129	1.261
0.1083	0.110	1.267
0.1166	0.091	1.245
0.1250	0.082	1.248
0.1333	0.072	1.212
0.1416	0.063	1.216
0.1500	0.057	1.154
0.1583	0.050	1.148
0.1666	0.047	1.161
0.1750	0.041	1.029
0.1833	0.038	1.129
0.1916	0.034	1.090
0.2000	0.034	1.080
0.2083	0.031	1.074
0.2166	0.031	1.055
0.2250	0.028	1.045
0.2333	0.025	1.032
0.2416	0.025	1.019
0.2500	0.025	1.006
0.2583	0.022	0.997
0.2666	0.022	0.984
0.2750	0.019	0.971
0.2833	0.019	0.958
0.2916	0.019	0.945
0.3000	0.019	0.936
0.3083	0.015	0.923
0.3166	0.015	0.913
0.3250	0.015	0.900
0.3333	0.015	0.891
0.3500	0.012	0.871
0.3666	0.012	0.849
0.3833	0.012	0.830
0.4000	0.009	0.810
0.4166	0.009	0.791
0.4333	0.009	0.772
0.4500	0.009	0.756
0.4666	0.009	0.736
0.4833	0.006	0.723
0.5000	0.006	0.704
0.5166	0.006	0.688
0.5333	0.006	0.672
0.5500	0.006	0.656
0.5666	0.006	0.643
0.5833	0.003	0.627
0.6000	0.003	0.614
0.6166	0.003	0.598
0.6333	0.003	0.585
0.6500	0.003	0.572

③ E1E3-T2- dat

E1 ΔH = 2.696
Δt = 5.3415

E3 ΔH = 1.341
Δt = 5.325

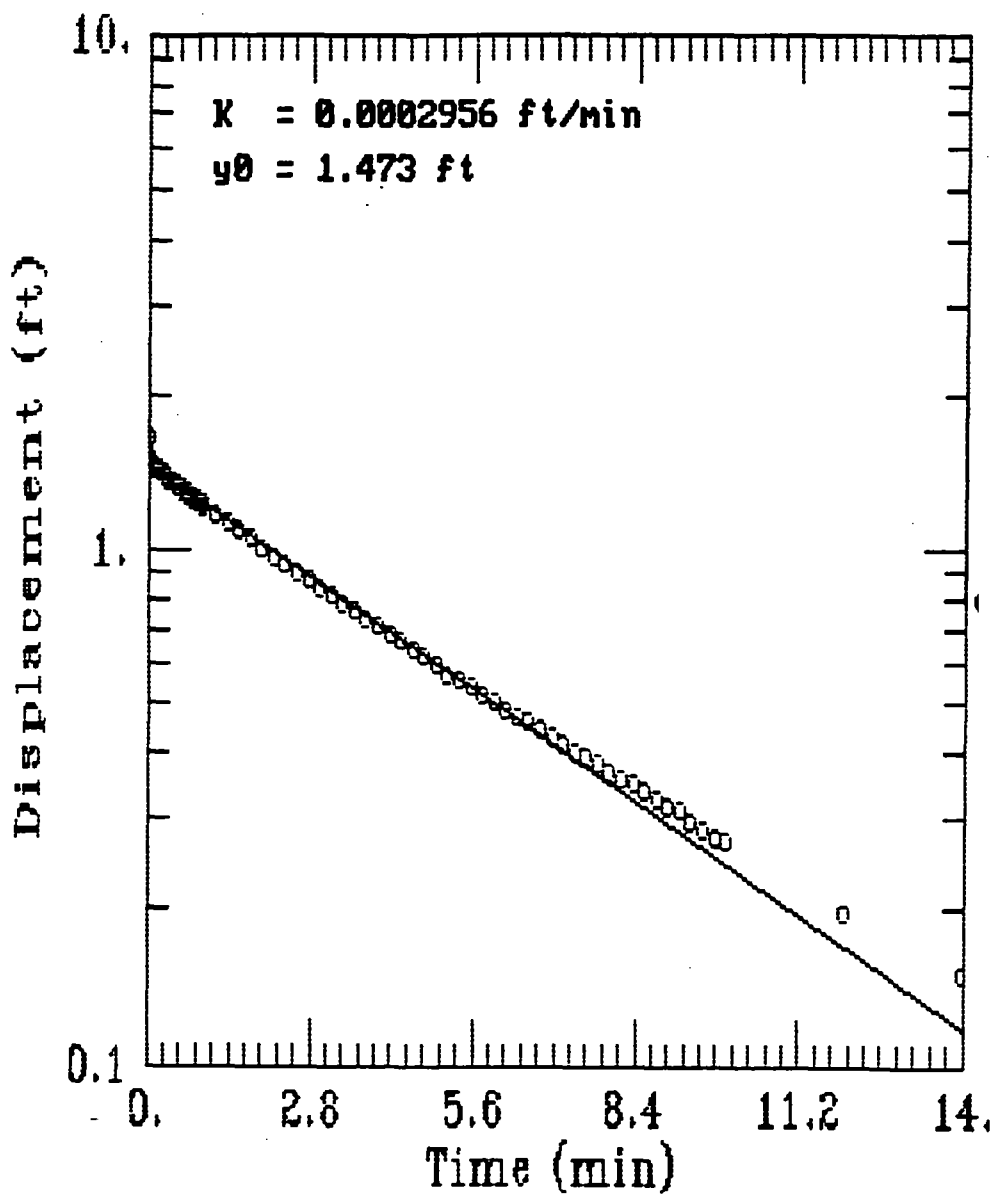
Test:	E1-1, E3 slug out
File:	E1E3-T2- dat
Round:	KTEST2
Column 1:	Elapsed time (min)
Column 2:	Head E1-1 (ft)
	t = 0.0250 t = 0.6666
Column 3:	Head E3 (ft)
	t = 0.0750 t = 5.10

0.6666	0.003	0.563
0.6833	0.000	0.550
0.7000	0.000	0.537
0.7166	0.000	0.524
0.7333	0.000	0.511
0.7500	0.000	0.498
0.7666	0.000	0.489
0.7833	0.000	0.479
0.8000	0.000	0.469
0.8166	0.000	0.460
0.8333	0.000	0.447
0.8500	0.000	0.437
0.8666	-0.003	0.431
0.8833	0.000	0.418
0.9000	0.000	0.411
0.9166	-0.003	0.402
0.9333	-0.003	0.392
0.9500	0.000	0.386
0.9666	-0.003	0.376
0.9833	-0.003	0.366
1.0000	-0.003	0.360
1.2000	-0.003	0.279
1.4000	-0.003	0.215
1.6000	-0.003	0.164
1.8000	0.000	0.128
2.0000	0.000	0.115
2.2000	0.000	0.080
2.4000	0.000	0.067
2.6000	0.000	0.054
2.8000	0.003	0.045
3.0000	0.003	0.035
3.2000	0.003	0.032
3.4000	0.003	0.025
3.6000	0.003	0.022
3.8000	0.003	0.016
4.0000	0.003	0.012
4.2000	0.003	0.009
4.4000	0.003	0.006
4.6000	0.003	0.006
4.8000	0.000	0.006
5.0000	0.003	0.003
5.2000	0.003	0.003
5.4000	0.003	0.003

WELL CLUSTER: E
WELL ID: E2
SCREENED INTERVAL: 39-44

TEST METHOD: Flowmeter
SLUG IN/SLUG OUT: Slug out
K-VALUE: 0.426 ft/day

E2-T2-1



0.0000	0.009	0.003
0.0083	0.009	0.000
0.0166	1.537	1.374
0.0250	-0.231	3.012
0.0333	1.084	2.480
0.0416	<u>1.643</u>	1.685
0.0500	1.508	<u>2.699</u>
0.0583	1.511	2.192
0.0666	1.498	2.065
0.0750	1.502	2.049
0.0833	1.489	2.043
0.0916	1.486	2.033
0.1000	1.486	2.024
0.1083	1.482	2.018
0.1166	1.476	2.011
0.1250	1.473	1.957
0.1333	1.473	1.976
0.1416	1.470	1.954
0.1500	1.453	1.976
0.1583	1.447	1.967
0.1666	1.460	1.961
0.1750	1.453	1.951
0.1833	1.450	1.945
0.1916	1.447	1.938
0.2000	1.444	1.932
0.2083	1.441	1.780
0.2166	1.437	1.919
0.2250	1.434	1.916
0.2333	1.431	1.910
0.2416	1.428	1.907
0.2500	1.424	1.900
0.2583	1.421	1.894
0.2666	1.421	1.888
0.2750	1.418	1.885
0.2833	1.415	1.878
0.2916	1.412	1.872
0.3000	1.408	1.866
0.3083	1.405	1.859
0.3166	1.402	1.856
0.3250	1.402	1.850
0.3333	1.399	1.847
0.3500	1.392	1.837
0.3666	1.386	1.824
0.3833	1.379	1.815
0.4000	1.376	1.805
0.4166	1.370	1.796
0.4333	1.367	1.786
0.4500	1.360	1.777
0.4666	1.357	1.767
0.4833	1.354	1.758
0.5000	1.347	1.751
0.5166	1.344	1.742
0.5333	1.338	1.732
0.5500	1.334	1.710
0.5666	1.331	1.704
0.5833	1.325	1.698
0.6000	1.322	1.691
0.6166	1.315	1.685
0.6333	1.312	1.675
0.6500	1.309	1.669

E2 $\Delta H = 1.492$

$\Delta t = 13.9584$

~~E6 $\Delta H = 2.984 = 2.671$~~

~~$\Delta t = 13.975 = 13.95$~~

Test:	<u>E2, E6 slugout</u>
File:	<u>E2E6-T2-dat</u>
Round:	<u>KTEST2</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head E2 (ft)</u>
	<u>t = 0.0416 t = 14.0</u>
Column 3:	<u>Head E6 (ft)</u>
	<u>t = 0.0500 t = 14.0</u>

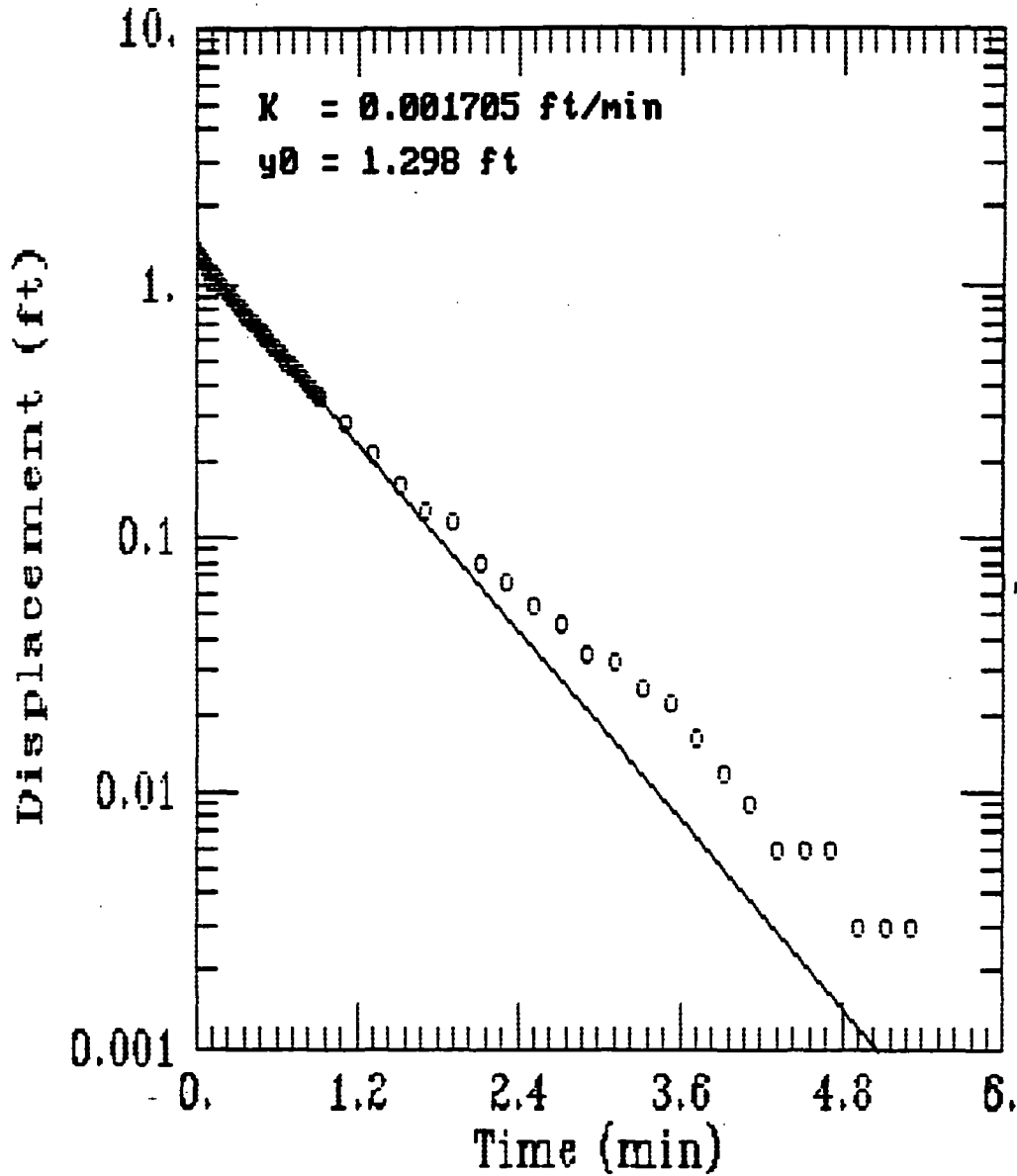
0.6666	1.302	1.663
0.6833	1.299	1.663
0.7000	1.296	1.666
0.7166	1.289	1.666
0.7333	1.283	1.660
0.7500	1.283	1.656
0.7666	1.277	1.647
0.7833	1.273	1.641
0.8000	1.267	1.634
0.8166	1.264	1.625
0.8333	1.260	1.618
0.8500	1.257	1.609
0.8666	1.254	1.603
0.8833	1.248	1.596
0.9000	1.244	1.587
0.9166	1.241	1.580
0.9333	1.235	1.574
0.9500	1.232	1.565
0.9666	1.228	1.558
0.9833	1.225	1.552
1.0000	1.222	1.546
1.2000	1.174	1.457
1.4000	1.132	1.378
1.6000	1.087	1.308
1.8000	1.048	1.235
2.0000	1.010	1.169
2.2000	0.974	1.108
2.4000	0.939	1.048
2.6000	0.903	0.994
2.8000	0.871	0.940
3.0000	0.842	0.893
3.2000	0.813	0.849
3.4000	0.784	0.804
3.6000	0.759	0.763
3.8000	0.733	0.722
4.0000	0.710	0.687
4.2000	0.685	0.649
4.4000	0.659	0.614
4.6000	0.636	0.582
4.8000	0.617	0.554
5.0000	0.595	0.525
5.2000	0.572	0.500
5.4000	0.556	0.475
5.6000	0.540	0.449
5.8000	0.524	0.427
6.0000	0.505	0.405
6.2000	0.489	0.383
6.4000	0.472	0.364
6.6000	0.460	0.345
6.8000	0.443	0.326
7.0000	0.434	0.310
7.2000	0.418	0.294
7.4000	0.405	0.278
7.6000	0.392	0.266
7.8000	0.382	0.253
8.0000	0.369	0.240
8.2000	0.357	0.224
8.4000	0.347	0.215
8.6000	0.337	0.202
8.8000	0.328	0.193

9.0000	0.318	0.183
9.2000	0.308	0.171
9.4000	0.295	0.158
9.6000	0.286	0.152
9.8000	0.276	0.142
10.0000	0.270	0.133
12.0000	0.199	0.069
14.0000	0.151	0.028

WELL CLUSTER: E
WELL ID: E3
SCREENED INTERVAL: 65-75

TEST METHOD: Bowen Rice
SLUG IN/SLUG OUT: Slug out
K-VALUE: 2.46 ft/day

e3-t2-1



0.0000	0.000	0.000
0.0083	0.000	-0.003
0.0166	1.248	0.337
0.0250	2.699	0.495
0.0333	2.138	-0.019
0.0416	1.127	0.913
0.0500	0.662	1.006
0.0583	0.516	1.106
0.0666	0.367	1.241
0.0750	0.275	1.344
0.0833	0.221	1.312
0.0916	0.158	1.296
0.1000	0.129	1.261
0.1083	0.110	1.267
0.1166	0.091	1.245
0.1250	0.082	1.248
0.1333	0.072	1.212
0.1416	0.063	1.216
0.1500	0.057	1.154
0.1583	0.050	1.148
0.1666	0.047	1.161
0.1750	0.041	1.029
0.1833	0.038	1.129
0.1916	0.034	1.090
0.2000	0.034	1.080
0.2083	0.031	1.074
0.2166	0.031	1.055
0.2250	0.028	1.045
0.2333	0.025	1.032
0.2416	0.025	1.019
0.2500	0.025	1.006
0.2583	0.022	0.997
0.2666	0.022	0.984
0.2750	0.019	0.971
0.2833	0.019	0.958
0.2916	0.019	0.945
0.3000	0.019	0.936
0.3083	0.015	0.923
0.3166	0.015	0.913
0.3250	0.015	0.900
0.3333	0.015	0.891
0.3500	0.012	0.871
0.3666	0.012	0.849
0.3833	0.012	0.830
0.4000	0.009	0.810
0.4166	0.009	0.791
0.4333	0.009	0.772
0.4500	0.009	0.756
0.4666	0.009	0.736
0.4833	0.006	0.723
0.5000	0.006	0.704
0.5166	0.006	0.688
0.5333	0.006	0.672
0.5500	0.006	0.656
0.5666	0.006	0.643
0.5833	0.003	0.627
0.6000	0.003	0.614
0.6166	0.003	0.598
0.6333	0.003	0.585
0.6500	0.003	0.572

③

E/E3-T2-dat

E1 $\Delta H = 2.696$
 $\Delta t = 0.6416$

E3 $\Delta H = 1.341$
 $\Delta t = 5.325$

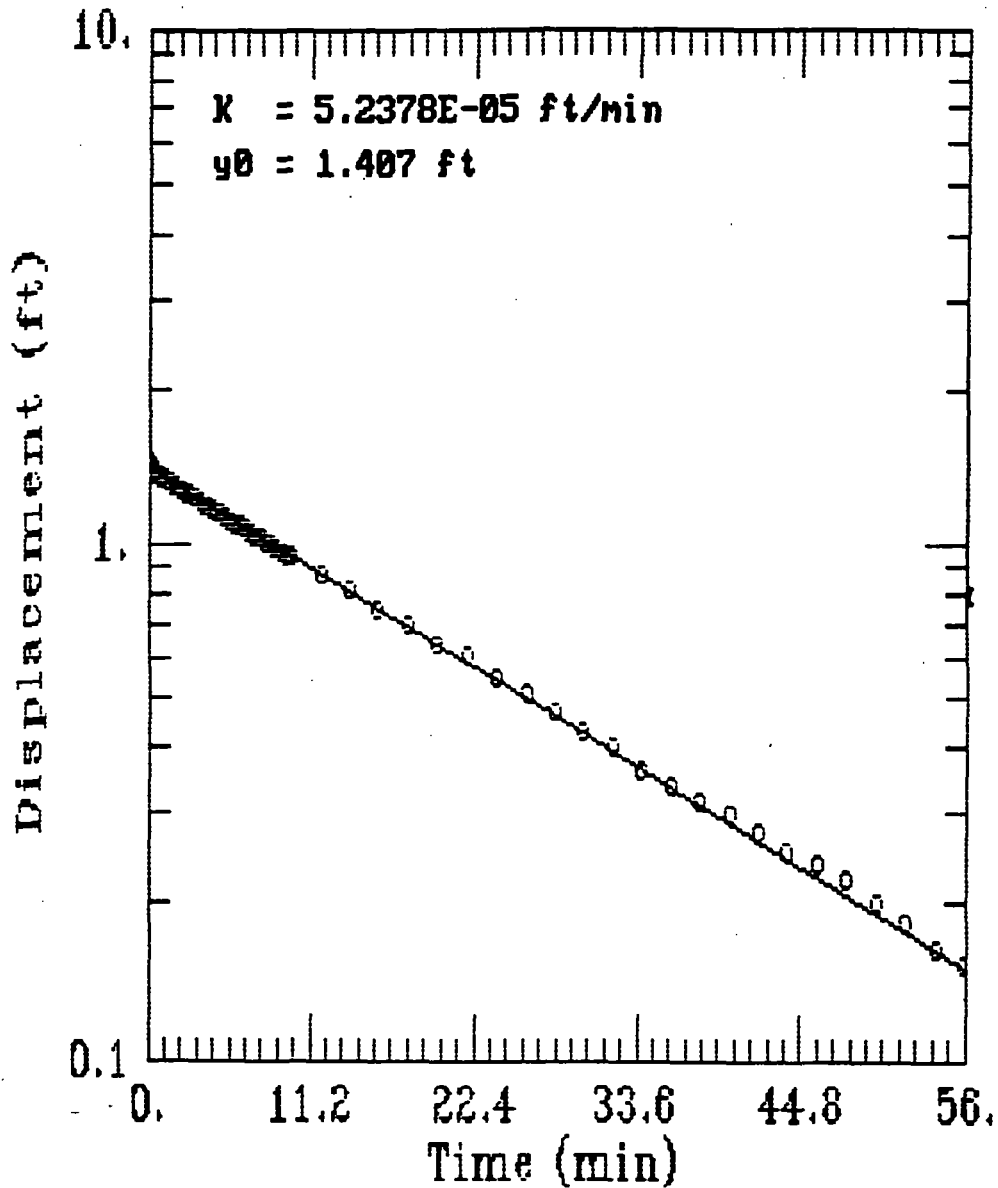
Test:	<u>E1, E3 slug out</u>
File:	<u>E/E3-T2-dat</u>
Round:	<u>KTEST2</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head E1 (ft)</u>
	<u>t = 0.0250 t = 0.6666</u>
Column 3:	<u>Head E3 (ft)</u>
	<u>t = 0.0750 t = 5.40</u>

0.6666	0.003	0.563
0.6833	0.000	0.550
0.7000	0.000	0.537
0.7166	0.000	0.524
0.7333	0.000	0.511
0.7500	0.000	0.498
0.7666	0.000	0.489
0.7833	0.000	0.479
0.8000	0.000	0.469
0.8166	0.000	0.460
0.8333	0.000	0.447
0.8500	0.000	0.437
0.8666	-0.003	0.431
0.8833	0.000	0.418
0.9000	0.000	0.411
0.9166	-0.003	0.402
0.9333	-0.003	0.392
0.9500	0.000	0.386
0.9666	-0.003	0.376
0.9833	-0.003	0.366
1.0000	-0.003	0.360
1.2000	-0.003	0.279
1.4000	-0.003	0.215
1.6000	-0.003	0.164
1.8000	0.000	0.128
2.0000	0.000	0.115
2.2000	0.000	0.080
2.4000	0.000	0.067
2.6000	0.000	0.054
2.8000	0.003	0.045
3.0000	0.003	0.035
3.2000	0.003	0.032
3.4000	0.003	0.025
3.6000	0.003	0.022
3.8000	0.003	0.016
4.0000	0.003	0.012
4.2000	0.003	0.009
4.4000	0.003	0.006
4.6000	0.003	0.006
4.8000	0.000	0.006
5.0000	0.003	0.003
5.2000	0.003	0.003
5.4000	0.003	0.003

WELL CLUSTER: A
WELL ID: E4-1
SCREENED INTERVAL: 79-89

TEST METHOD: Burner Pipe
SLUG IN/SLUG OUT: slug out
K-VALUE: 0.0754 ft/day

E41-T2-1



0.0000	7.631	-0.019
0.0083	7.631	-0.019
0.0166	7.631	-0.019
0.0250	7.650	0.896
0.0333	8.460	0.407
0.0416	10.141	0.706
0.0500	8.871	1.030
0.0583	8.213	1.348
0.0666	9.705	1.424
0.0750	9.655	1.437
0.0833	9.629	1.431
0.0916	9.585	1.443
0.1000	9.560	1.412
0.1083	9.541	1.412
0.1166	9.509	1.424
0.1250	9.490	1.424
0.1333	9.471	1.418
0.1416	9.440	1.418
0.1500	9.427	1.418
0.1583	9.408	1.412
0.1666	9.389	1.412
0.1750	9.364	1.412
0.1833	9.345	1.412
0.1916	9.326	1.412
0.2000	9.307	1.412
0.2083	9.294	1.412
0.2166	9.275	1.412
0.2250	9.250	1.405
0.2333	9.237	1.405
0.2416	9.225	1.405
0.2500	9.206	1.405
0.2583	9.187	1.405
0.2666	9.174	1.405
0.2750	9.155	1.405
0.2833	9.143	1.405
0.2916	9.124	1.399
0.3000	9.111	1.399
0.3083	9.098	1.399
0.3166	9.079	1.399
0.3250	9.067	1.399
0.3333	9.054	1.399
0.3500	9.022	1.399
0.3666	8.997	1.399
0.3833	8.972	1.393
0.4000	8.940	1.393
0.4166	8.915	1.393
0.4333	8.890	1.393
0.4500	8.864	1.393
0.4666	8.845	1.393
0.4833	8.814	1.386
0.5000	8.795	1.386
0.5166	8.769	1.386
0.5333	8.744	1.386
0.5500	8.725	1.380
0.5666	8.706	1.380
0.5833	8.687	1.380
0.6000	8.662	1.380
0.6166	8.643	1.380
0.6333	8.624	1.380
0.6500	8.605	1.380

E5 $\Delta H = 2.491$
 $\Delta t = 5.1584$
 E41 $\Delta H = 1.291$
 $\Delta t = 55.9$

Test:	E5, E41 slug test
File:	E5E41-T2.dat
Round:	KTEST2
Column 1:	Elapsed time (min)
Column 2:	Head E5 (ft)
	$t_0 = 0.0416$ $t_1 = 5.2$
Column 3:	Head E41 (ft)
	$t_0 = 0.1916$ $t_1 = 56.0$

0.6666	8.586	1.373
0.6833	8.567	1.373
0.7000	8.548	1.373
0.7166	8.536	1.373
0.7333	8.517	1.373
0.7500	8.498	1.367
0.7666	8.485	1.367
0.7833	8.466	1.367
0.8000	8.447	1.367
0.8166	8.434	1.367
0.8333	8.415	1.367
0.8500	8.403	1.361
0.8666	8.390	1.361
0.8833	8.371	1.361
0.9000	8.358	1.361
0.9166	8.346	1.361
0.9333	8.333	1.361
0.9500	8.321	1.354
0.9666	8.308	1.354
0.9833	8.295	1.354
1.0000	8.283	1.354
1.2000	8.150	1.342
1.4000	8.042	1.329
1.6000	7.960	1.316
1.8000	7.897	1.304
2.0000	7.846	1.297
2.2000	7.802	1.284
2.4000	7.770	1.272
2.6000	7.751	1.265
2.8000	7.732	1.253
3.0000	7.713	1.246
3.2000	7.701	1.234
3.4000	7.688	1.227
3.6000	7.682	1.214
3.8000	7.669	1.202
4.0000	7.669	1.195
4.2000	7.663	1.183
4.4000	7.656	1.176
4.6000	7.656	1.164
4.8000	7.650	1.157
5.0000	7.650	1.145
5.2000	7.650	1.138
5.4000	7.644	1.125
5.6000	7.644	1.113
5.8000	7.644	1.106
6.0000	7.644	1.100
6.2000	7.637	1.094
6.4000	7.637	1.087
6.6000	7.637	1.075
6.8000	7.644	1.068
7.0000	7.644	1.055
7.2000	7.637	1.049
7.4000	7.637	1.043
7.6000	7.644	1.036
7.8000	7.644	1.030
8.0000	7.644	1.017
8.2000	7.644	1.011
8.4000	7.644	1.005
8.6000	7.644	0.998
8.8000	7.644	0.992

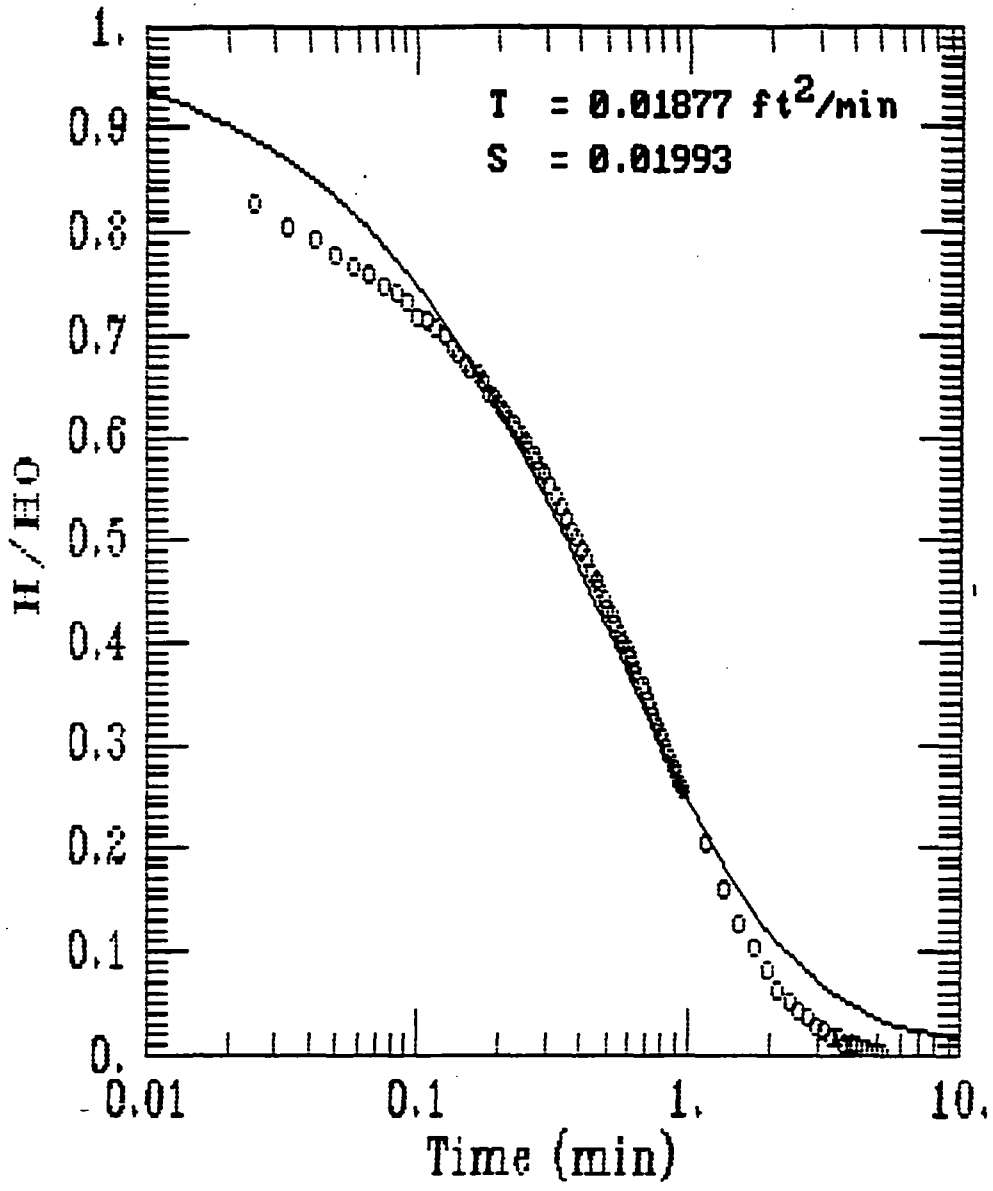
0.006

9.0000	7.644	0.979
9.2000	7.644	0.973
9.4000	7.644	0.966
9.6000	7.644	0.960
9.8000	7.644	0.954
10.0000	7.644	0.947
12.0000	7.637	0.871
14.0000	7.644	0.814
16.0000	7.644	0.750
18.0000	7.650	0.699
20.0000	7.650	0.642
22.0000	7.656	0.604
24.0000	7.644	0.547
26.0000	7.644	0.508
28.0000	7.644	0.470
30.0000	7.644	0.432
32.0000	7.644	0.400
34.0000	7.637	0.362
36.0000	7.637	0.337
38.0000	7.644	0.318
40.0000	7.650	0.299
42.0000	7.650	0.273
44.0000	7.650	0.254
46.0000	7.650	0.241
48.0000	7.650	0.222
50.0000	7.650	0.203
52.0000	7.644	0.184
54.0000	7.644	0.165
56.0000	7.644	0.152

WELL CLUSTER: E
WELL ID: E5
SCREENED INTERVAL: 94-104

TEST METHOD: Cooper et al.
SLUG IN/SLUG OUT: slug out
K-VALUE: 2.73 ft/day

E5-T2-1



0.0000	7.631	-0.019
0.0083	7.631	-0.019
0.0166	7.631	-0.019
0.0250	7.650	0.896
0.0333	8.460	0.407
0.0416	10.141	0.706
0.0500	8.871	1.030
0.0583	8.213	1.348
0.0666	9.705	1.424
0.0750	9.655	1.437
0.0833	9.629	1.431
0.0916	9.585	1.443
0.1000	9.560	1.412
0.1083	9.541	1.412
0.1166	9.509	1.424
0.1250	9.490	1.424
0.1333	9.471	1.418
0.1416	9.440	1.418
0.1500	9.427	1.418
0.1583	9.408	1.412
0.1666	9.389	1.412
0.1750	9.364	1.412
0.1833	9.345	1.412
0.1916	9.326	1.412
0.2000	9.307	1.412
0.2083	9.294	1.412
0.2166	9.275	1.412
0.2250	9.250	1.405
0.2333	9.237	1.405
0.2416	9.225	1.405
0.2500	9.206	1.405
0.2583	9.187	1.405
0.2666	9.174	1.405
0.2750	9.155	1.405
0.2833	9.143	1.405
0.2916	9.124	1.399
0.3000	9.111	1.399
0.3083	9.098	1.399
0.3166	9.079	1.399
0.3250	9.067	1.399
0.3333	9.054	1.399
0.3500	9.022	1.399
0.3666	8.997	1.399
0.3833	8.972	1.393
0.4000	8.940	1.393
0.4166	8.915	1.393
0.4333	8.890	1.393
0.4500	8.864	1.393
0.4666	8.845	1.393
0.4833	8.814	1.386
0.5000	8.795	1.386
0.5166	8.769	1.386
0.5333	8.744	1.386
0.5500	8.725	1.380
0.5666	8.706	1.380
0.5833	8.687	1.380
0.6000	8.662	1.380
0.6166	8.643	1.380
0.6333	8.624	1.380
0.6500	8.605	1.380

ES $\Delta H = 2.491$
 $\Delta T = 5.1584$
 EA1 $\Delta H = 1.291$
 $\Delta t = 63.9$

Test:	ES EA-1 slug cut
File:	ES EA-1-T2.dat
Round:	KTEST2
Column 1:	Elapsed time (min)
Column 2:	Head ES (ft)
	$t = 0.1416$ $h = 5.2$
Column 3:	Head EA-1 (ft)
	$t = 0.1916$ $h = 16.0$

0.6666	8.580	1.373
0.6833	8.567	1.373
0.7000	8.548	1.373
0.7166	8.536	1.373
0.7333	8.517	1.373
0.7500	8.498	1.367
0.7666	8.485	1.367
0.7833	8.466	1.367
0.8000	8.447	1.367
0.8166	8.434	1.367
0.8333	8.415	1.367
0.8500	8.403	1.361
0.8666	8.390	1.361
0.8833	8.371	1.361
0.9000	8.358	1.361
0.9166	8.346	1.361
0.9333	8.333	1.361
0.9500	8.321	1.354
0.9666	8.308	1.354
0.9833	8.295	1.354
1.0000	8.283	1.354
1.2000	8.150	1.342
1.4000	8.042	1.329
1.6000	7.960	1.316
1.8000	7.897	1.304
2.0000	7.846	1.297
2.2000	7.802	1.284
2.4000	7.770	1.272
2.6000	7.751	1.265
2.8000	7.732	1.253
3.0000	7.713	1.246
3.2000	7.701	1.234
3.4000	7.688	1.227
3.6000	7.682	1.214
3.8000	7.669	1.202
4.0000	7.669	1.195
4.2000	7.663	1.183
4.4000	7.656	1.176
4.6000	7.656	1.164
4.8000	7.650	1.157
5.0000	7.650	1.145
5.2000	7.650	1.138
5.4000	7.644	1.125
5.6000	7.644	1.113
5.8000	7.644	1.106
6.0000	7.644	1.100
6.2000	7.637	1.094
6.4000	7.637	1.087
6.6000	7.637	1.075
6.8000	7.644	1.068
7.0000	7.644	1.055
7.2000	7.637	1.049
7.4000	7.637	1.043
7.6000	7.644	1.036
7.8000	7.644	1.030
8.0000	7.644	1.017
8.2000	7.644	1.011
8.4000	7.644	1.005
8.6000	7.644	0.998
8.8000	7.644	0.992

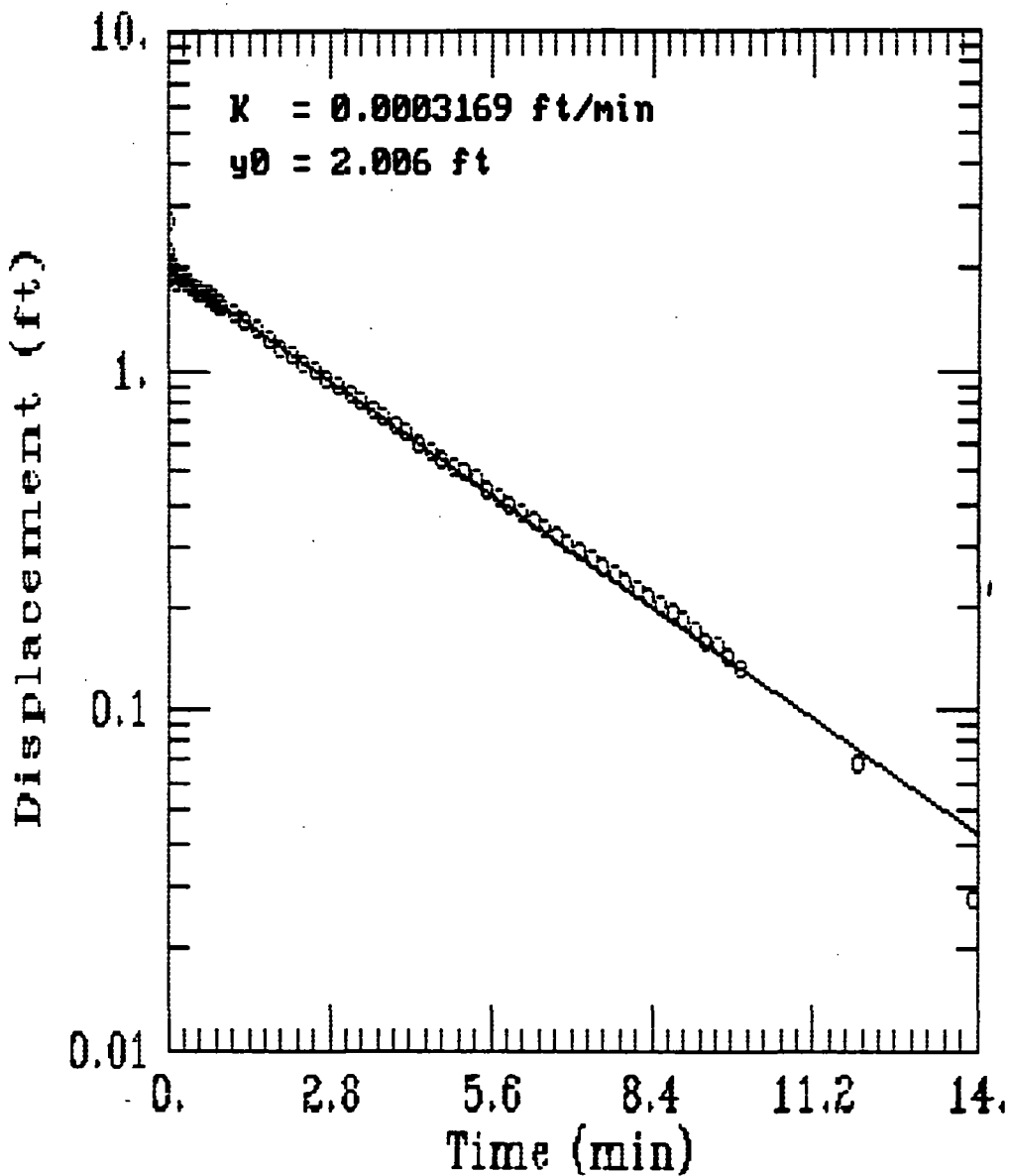
0.006

9.0000	7.644	0.979
9.2000	7.644	0.973
9.4000	7.644	0.966
9.6000	7.644	0.960
9.8000	7.644	0.954
10.0000	7.644	0.947
12.0000	7.637	0.871
14.0000	7.644	0.814
16.0000	7.644	0.750
18.0000	7.650	0.699
20.0000	7.650	0.642
22.0000	7.656	0.604
24.0000	7.644	0.547
26.0000	7.644	0.508
28.0000	7.644	0.470
30.0000	7.644	0.432
32.0000	7.644	0.400
34.0000	7.637	0.362
36.0000	7.637	0.337
38.0000	7.644	0.318
40.0000	7.650	0.299
42.0000	7.650	0.273
44.0000	7.650	0.254
46.0000	7.650	0.241
48.0000	7.650	0.222
50.0000	7.650	0.203
52.0000	7.644	0.184
54.0000	7.644	0.165
56.0000	7.644	0.152

WELL CLUSTER: E
WELL ID: E6
SCREENED INTERVAL: 54-64

TEST METHOD: Bauer Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 0.456 ft/day

E6-T2-1



0.0000	0.009	0.003
0.0083	-0.009	0.000
0.0166	1.537	1.374
0.0250	-0.231	3.012
0.0333	1.084	2.480
0.0416	<u>1.643</u>	1.685
0.0500	1.508	<u>2.699</u>
0.0583	1.511	2.192
0.0666	1.498	2.065
0.0750	1.502	2.049
0.0833	1.489	2.043
0.0916	1.486	2.033
0.1000	1.486	2.024
0.1083	1.482	2.018
0.1166	1.476	2.011
0.1250	1.473	1.957
0.1333	1.473	1.976
0.1416	1.470	1.954
0.1500	1.453	1.976
0.1583	1.447	1.967
0.1666	1.460	1.961
0.1750	1.453	1.951
0.1833	1.450	1.945
0.1916	1.447	1.938
0.2000	1.444	1.932
0.2083	1.441	1.780
0.2166	1.437	1.919
0.2250	1.434	1.916
0.2333	1.431	1.910
0.2416	1.428	1.907
0.2500	1.424	1.900
0.2583	1.421	1.894
0.2666	1.421	1.888
0.2750	1.418	1.885
0.2833	1.415	1.878
0.2916	1.412	1.872
0.3000	1.408	1.866
0.3083	1.405	1.859
0.3166	1.402	1.856
0.3250	1.402	1.850
0.3333	1.399	1.847
0.3500	1.392	1.837
0.3666	1.386	1.824
0.3833	1.379	1.815
0.4000	1.376	1.805
0.4166	1.370	1.796
0.4333	1.367	1.786
0.4500	1.360	1.777
0.4666	1.357	1.767
0.4833	1.354	1.758
0.5000	1.347	1.751
0.5166	1.344	1.742
0.5333	1.338	1.732
0.5500	1.334	1.710
0.5666	1.331	1.704
0.5833	1.325	1.698
0.6000	1.322	1.691
0.6166	1.315	1.685
0.6333	1.312	1.675
0.6500	1.309	1.669

E2 $\Delta H = 1.492$
 $\Delta t = 13.9584$

~~E6 $\Delta H = 2.984 = 2.671$
 $\Delta t = 13.975 = 13.95$~~

Test:	<u>E2, E6 slug out</u>
File:	<u>E2E6-T2-.dat</u>
Round:	<u>KTEST2</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>s Head E2 (ft)</u>
	<u>t = 0.0416 t = 14.0</u>
Column 3:	<u>s Head E6 (ft)</u>
	<u>t = 0.0500 t = 14.0</u>

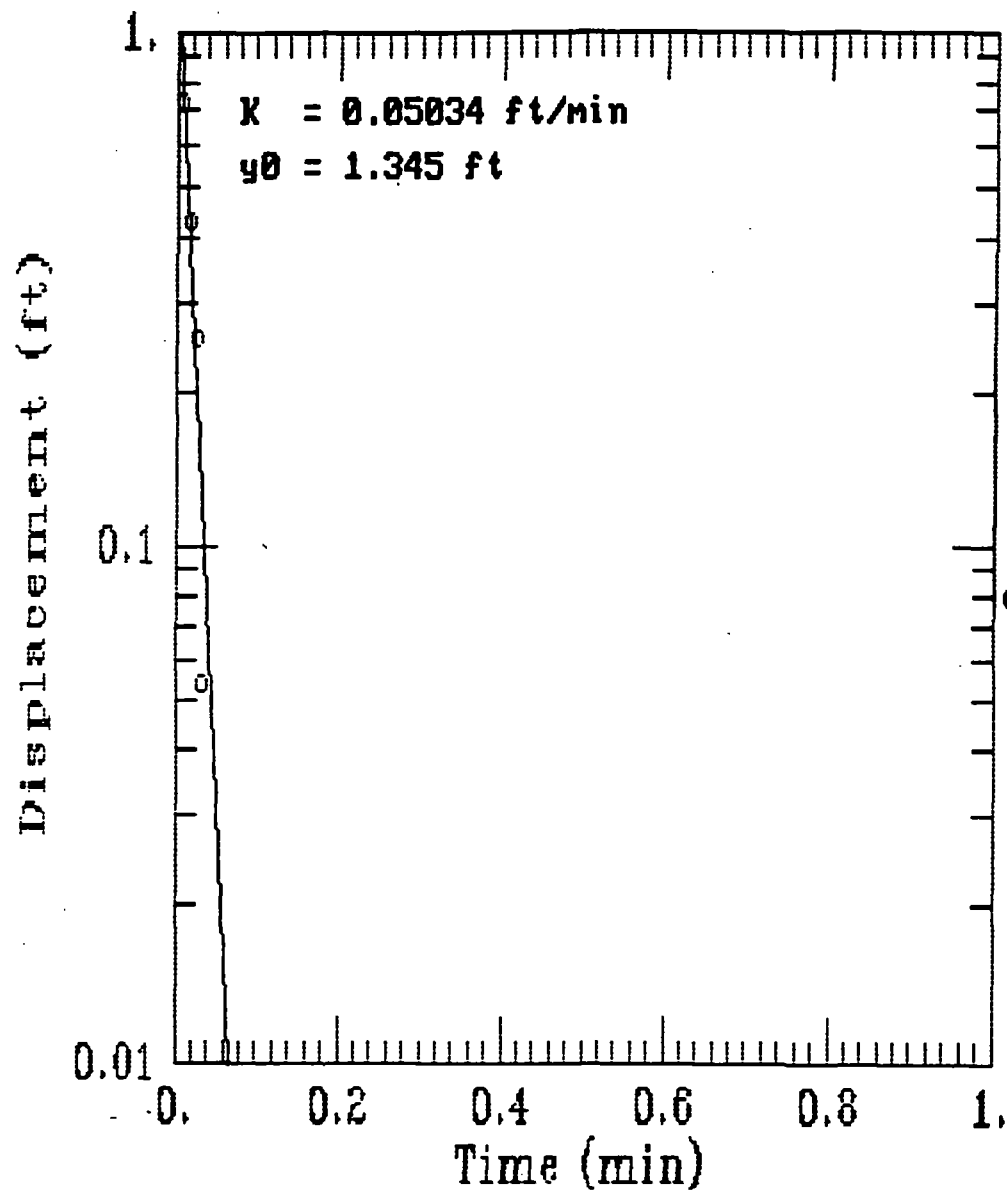
0.6666	1.302	1.663
0.6833	1.299	1.663
0.7000	1.296	1.666
0.7166	1.289	1.666
0.7333	1.283	1.660
0.7500	1.283	1.656
0.7666	1.277	1.647
0.7833	1.273	1.641
0.8000	1.267	1.634
0.8166	1.264	1.625
0.8333	1.260	1.618
0.8500	1.257	1.609
0.8666	1.254	1.603
0.8833	1.248	1.596
0.9000	1.244	1.587
0.9166	1.241	1.580
0.9333	1.235	1.574
0.9500	1.232	1.565
0.9666	1.228	1.558
0.9833	1.225	1.552
1.0000	1.222	1.546
1.2000	1.174	1.457
1.4000	1.132	1.378
1.6000	1.087	1.308
1.8000	1.048	1.235
2.0000	1.010	1.169
2.2000	0.974	1.108
2.4000	0.939	1.048
2.6000	0.903	0.994
2.8000	0.871	0.940
3.0000	0.842	0.893
3.2000	0.813	0.849
3.4000	0.784	0.804
3.6000	0.759	0.763
3.8000	0.733	0.722
4.0000	0.710	0.687
4.2000	0.685	0.649
4.4000	0.659	0.614
4.6000	0.636	0.582
4.8000	0.617	0.554
5.0000	0.595	0.525
5.2000	0.572	0.500
5.4000	0.556	0.475
5.6000	0.540	0.449
5.8000	0.524	0.427
6.0000	0.505	0.405
6.2000	0.489	0.383
6.4000	0.472	0.364
6.6000	0.460	0.345
6.8000	0.443	0.326
7.0000	0.434	0.310
7.2000	0.418	0.294
7.4000	0.405	0.278
7.6000	0.392	0.266
7.8000	0.382	0.253
8.0000	0.369	0.240
8.2000	0.357	0.224
8.4000	0.347	0.215
8.6000	0.337	0.202
8.8000	0.328	0.193

9.0000	0.318	0.183
9.2000	0.308	0.171
9.4000	0.295	0.158
9.6000	0.286	0.152
9.8000	0.276	0.142
10.0000	0.270	0.133
12.0000	0.199	0.069
14.0000	0.151	0.028

WELL CLUSTER: F
WELL ID: F1-1
SCREENED INTERVAL: 5-20

TEST METHOD: Forward Bore
SLUG IN/SLUG OUT: Slug out
K-VALUE: 72.5 ft/day

F1-1-T2b



SE2000
 Environmental Logger
 08/13 17:39

Unit# 22

Test 11

F11-T2B (retest)

PRN ✓

Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. 204363

Reference 0.000
 SG 1.000
 Linearity 0.038
 Scale factor 10.165
 Offset 0.010
 Delay mSEC 50.000

Step 0 08/18 14:39:17

Elapsed Time INPUT 1

0.0000	0.000
0.0083	-0.003
0.0166	-0.003
0.0250	0.920
0.0333	0.727
0.0416	0.425
0.0500	0.257
0.0583	0.054
0.0666	-0.051
0.0750	-0.041
0.0833	0.000
0.0916	0.009
0.1000	0.003
0.1083	-0.003
0.1166	-0.003
0.1250	-0.003
0.1333	-0.003
0.1416	0.000
0.1500	0.000
0.1583	0.000
0.1666	0.000
0.1750	-0.003
0.1833	-0.003
0.1916	-0.003
0.2000	-0.003
0.2083	-0.003
0.2166	-0.003
0.2250	-0.003
0.2333	-0.003
0.2416	-0.003
0.2500	-0.003
0.2583	-0.003
0.2666	-0.003
0.2750	-0.003
0.2833	-0.003
0.2916	-0.003
0.3000	-0.003
0.3083	-0.003
0.3166	-0.003
0.3250	-0.003
0.3333	-0.003
0.3416	-0.003
0.3500	-0.003
0.3583	-0.003
0.3666	-0.003
0.3750	-0.003
0.3833	-0.003
0.3916	-0.003
0.4000	-0.003
0.4083	-0.003
0.4166	-0.003
0.4250	-0.003
0.4333	-0.003
0.4416	-0.003
0.4500	-0.003
0.4583	-0.003
0.4666	-0.003
0.4750	-0.003
0.4833	-0.003
0.4916	-0.003
0.5000	-0.003
0.5083	-0.003
0.5166	-0.003
0.5250	-0.003
0.5333	-0.003
0.5416	-0.003
0.5500	-0.003
0.5583	-0.003
0.5666	-0.003
0.5750	-0.003
0.5833	-0.003
0.5916	-0.003
0.6000	-0.003
0.6083	-0.003
0.6166	-0.003
0.6250	-0.003
0.6333	-0.003
0.6416	-0.003
0.6500	-0.003
0.6583	-0.003
0.6666	-0.003
0.6750	-0.003
0.6833	-0.003
0.6916	-0.003
0.7000	-0.003
0.7083	-0.003
0.7166	-0.003
0.7250	-0.003
0.7333	-0.003
0.7416	-0.003
0.7500	-0.003
0.7583	-0.003
0.7666	-0.003
0.7750	-0.003
0.7833	-0.003
0.7916	-0.003
0.8000	-0.003
0.8083	-0.003
0.8166	-0.003
0.8250	-0.003
0.8333	-0.003
0.8416	-0.003
0.8500	-0.003
0.8583	-0.003
0.8666	-0.003
0.8750	-0.003
0.8833	-0.003
0.8916	-0.003
0.9000	-0.003
0.9083	-0.003
0.9166	-0.003
0.9250	-0.003
0.9333	-0.003
0.9416	-0.003
0.9500	-0.003
0.9583	-0.003
0.9666	-0.003
0.9750	-0.003
0.9833	-0.003
0.9916	-0.003
1.0000	-0.003

↑ INSE
 check to compare
 then plot K =

Test:	F1-1	slug out
File:	F11-T2B	
Round:	1	TEST3
Column 1:	Elapsed time (min)	
Column 2:	Head (ft)	
	t ₀ = 0.0250	t ₁ = 0.0583
Column 3:		
	t ₀ = _____	t ₁ = _____

0.3333	-0.003
0.3500	-0.003
0.3666	-0.003
0.3833	-0.003
0.4000	0.000
0.4166	-0.003
0.4333	-0.003
0.4500	-0.003
0.4666	-0.003
0.4833	-0.003
0.5000	-0.003
0.5166	-0.003
0.5333	-0.003
0.5500	-0.003
0.5666	-0.003
0.5833	-0.003
0.6000	-0.003
0.6166	0.000
0.6333	-0.003
0.6500	0.000
0.6666	-0.003
0.6833	0.000
0.7000	-0.003
0.7166	-0.003
0.7333	0.000
0.7500	0.000
0.7666	0.000
0.7833	0.000
0.8000	-0.003
0.8166	0.000
0.8333	-0.003
0.8500	0.000
0.8666	0.000
0.8833	0.000
0.9000	0.000
0.9166	0.000
0.9333	0.000
0.9500	0.000
0.9666	0.000
0.9833	0.000
1.0000	0.000
1.2000	0.000
1.4000	0.000
1.6000	0.000

SE2000
 Environmental Logger
 08/18 17:38

Unit# 22 Test 10

F11-T2 (see next; test 11)
 (retested)

 Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. 204363

Reference 0.000
 SS 1.000
 Linearity 0.038
 Scale factor 10.165
 Offset 0.010
 Delay mSEC 50.000

Step 0 08/18 14:33:51

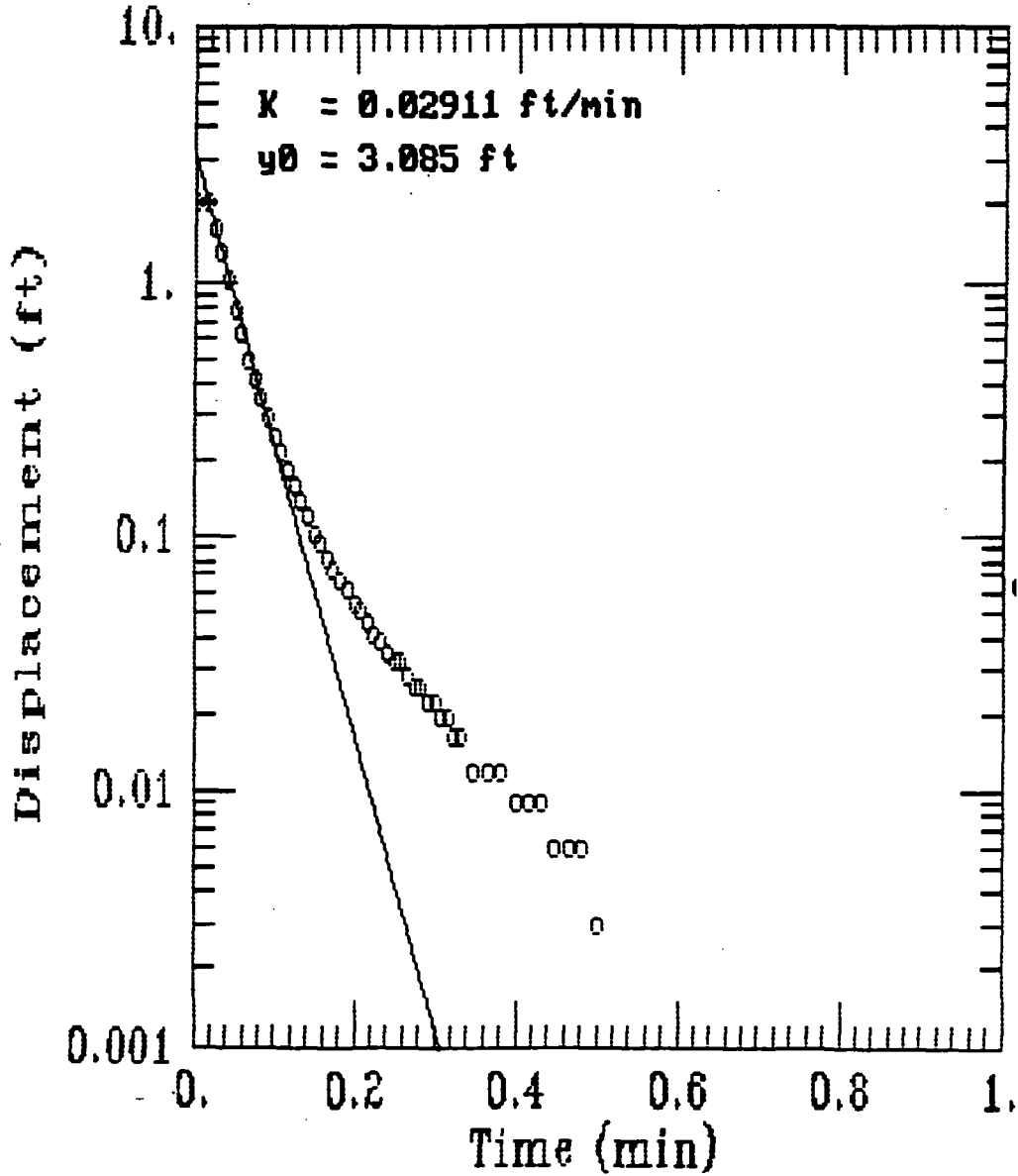
Elapsed Time	INPUT 1
0.0000	0.000
0.0083	0.000
0.0165	0.000
0.0250	0.000
0.0333	0.028
0.0416	0.557 ✓
0.0500	0.528
0.0583	0.325
0.0666	0.270
0.0750	0.173
0.0833	0.000 ✓
0.0916	-0.025
0.1000	-0.022
0.1083	0.003
0.1166	0.005
0.1250	0.003
0.1333	0.000
0.1416	-0.003
0.1500	0.000
0.1583	-0.003
0.1666	0.000
0.1750	-0.012
0.1833	0.006
0.1916	-0.000
0.2000	-0.003
0.2083	0.003
0.2166	-0.003
0.2250	-0.003
0.2333	0.000
0.2416	-0.016
0.2500	-0.006
0.2583	0.006
0.2666	0.013
0.2750	-0.016
0.2833	0.012
0.2916	-0.012
0.3000	0.005

0.3666	-0.006
0.3833	-0.003
0.4000	0.000
0.4166	-0.003
0.4333	-0.003
0.4500	-0.003
0.4666	-0.003
0.4833	0.000
0.5000	-0.003
0.5166	-0.003
0.5333	-0.003
0.5500	0.000
0.5666	-0.003
0.5833	0.000
0.6000	-0.003
0.6166	-0.003
0.6333	-0.003
0.6500	-0.003
0.6666	-0.003
0.6833	0.000
0.7000	-0.003
0.7166	0.000
0.7333	0.000
0.7500	0.000
0.7666	0.000
0.7833	0.000
0.8000	0.000
0.8166	-0.003
0.8333	0.000
0.8500	0.000
0.8666	0.000
0.8833	0.000
0.9000	0.000
0.9166	0.000
0.9333	0.000
0.9500	0.000
0.9666	0.000
0.9833	0.000
1.0000	0.000
1.2000	0.000
1.4000	0.000
1.6000	0.000

WELL CLUSTER: N
WELL ID: F2
SCREENED INTERVAL: 32-42

TEST METHOD: Packer Rise
SLUG IN/SLUG OUT: slug out
K-VALUE: 41.9 ft/day

F2-T2-1



fd-1d-1. Jul

0.6666	0.006
0.6833	0.003
0.7000	0.003
0.7166	0.003
0.7333	0.003
0.7500	0.003
0.7666	0.003
0.7833	0.003
0.8000	0.003
0.8166	0.003
0.8333	0.003
0.8500	0.003
0.8666	0.003
0.8833	0.003
0.9000	0.003
0.9166	0.003
0.9333	0.003
0.9500	0.006
0.9666	0.003
0.9833	0.006
1.0000	0.006
1.2000	0.006
1.4000	0.003

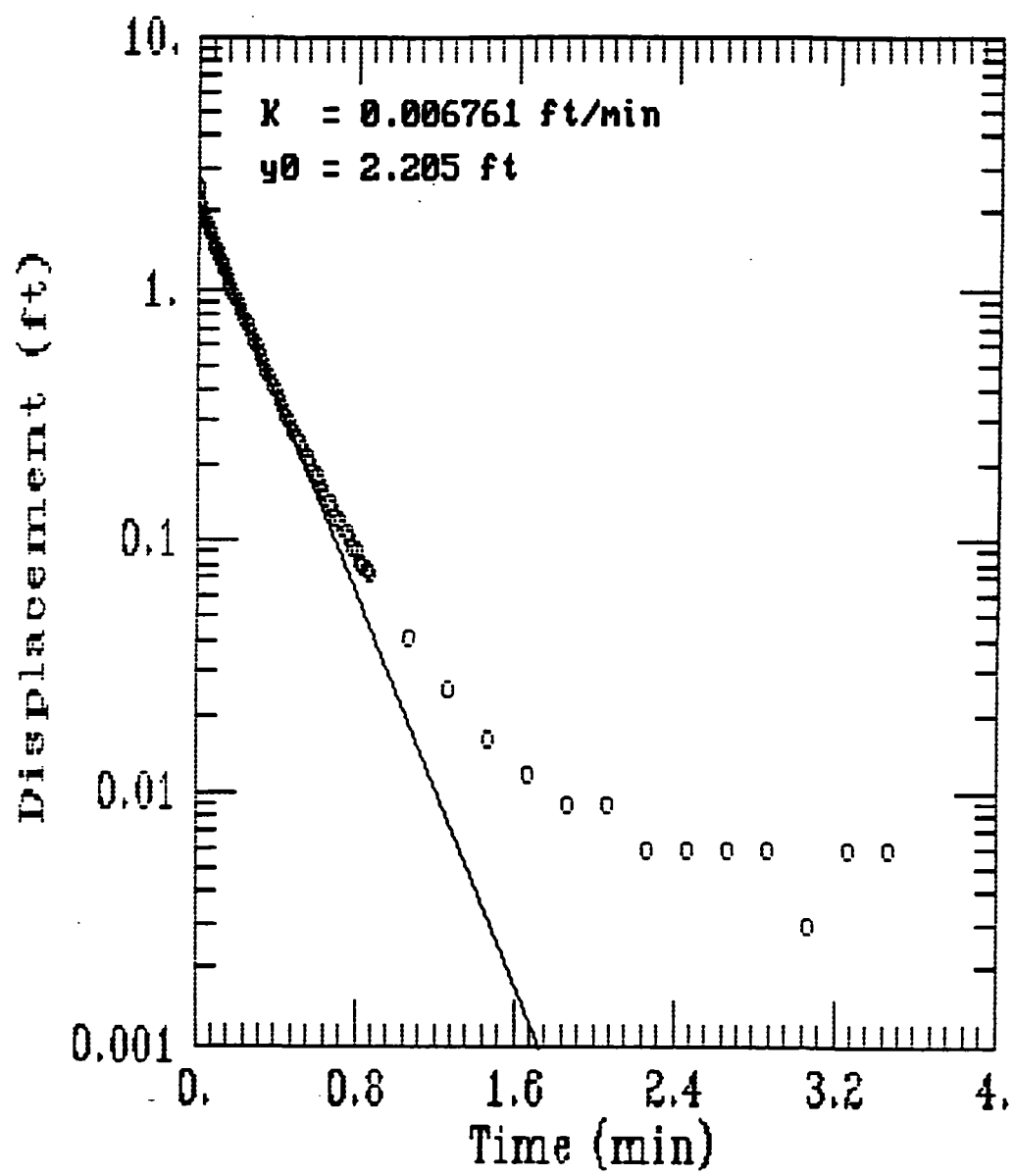
0	0.012
0.0083	0.209
0.0166	2.058
0.025	1.569
0.0333	1.312
0.0416	1.007
0.05	0.765
0.0583	0.627
0.0666	0.498
0.075	0.418
0.0833	0.35
0.0916	0.296
0.1	0.25
0.1083	0.212
0.1166	0.183
0.125	0.157
0.1333	0.135
0.1416	0.119
0.15	0.102
0.1583	0.093
0.1666	0.083
0.175	0.074
0.1833	0.067
0.1916	0.061
0.2	0.054
0.2083	0.051
0.2166	0.045
0.225	0.041
0.2333	0.038
0.2416	0.035
0.25	0.032
0.2583	0.032
0.2666	0.028
0.275	0.025
0.2833	0.025
0.2916	0.022
0.3	0.022
0.3083	0.019
0.3166	0.019
0.325	0.016
0.3333	0.016
0.35	0.012
0.3666	0.012
0.3833	0.012
0.4	0.009
0.4166	0.009
0.4333	0.009
0.45	0.006
0.4666	0.006
0.4833	0.006
0.5	0.003
0.5166	0.006
0.5333	0.006
0.55	0.006
0.5666	0.006
0.5833	0.006
0.6	0.006
0.6166	0.006
0.6333	0.006
0.65	0.003

0.5666	0.006
0.6833	0.003
0.7	0.003
0.7166	0.003
0.7333	0.003
0.75	0.003
0.7666	0.003
0.7833	0.003
0.8	0.003
0.8166	0.003
0.8333	0.003
0.85	0.003
0.8666	0.003
0.8833	0.003
0.9	0.003
0.9166	0.003
0.9333	0.003
0.95	0.006
0.9666	0.003
0.9833	0.006
1	0.006
1.2	0.006
1.4	0.003

WELL CLUSTER: 7
WELL ID: T3
SCREENED INTERVAL: 53-63

TEST METHOD: Banner Rise
SLUG IN/SLUG OUT: slug out
K-VALUE: 9.74 ft/day

F3-T2



SE2000
 Environmental Logger
 08/18 17:44

Unit# 22

Test 13

F3-T2

PRN ✓

 Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. 204363

Reference 0.000
 SG 1.000
 Linearity 0.038
 Scale factor 10.165
 Offset 0.010
 Delay μ SEC 50.000

Step 0 08/18 15:14:50

 Elapsed Time INPUT 1

0.0000	0.003
0.0083	0.000
0.0166	0.000
0.0250	-0.009
0.0333	0.003
0.0416	0.045
0.0500	-0.022
0.0583	0.012
0.0666	0.000
0.0750	0.003
0.0833	0.003
0.0916	0.025
0.1000	-0.070
0.1083	0.940
0.1166	1.997
0.1250	1.817
0.1333	2.483 ✓
0.1416	2.242
0.1500	2.084
0.1583	1.990
0.1666	1.916
0.1750	1.849
0.1833	1.759
0.1916	1.691
0.2000	1.623
0.2083	1.562
0.2166	1.501
0.2250	1.446
0.2333	1.391
0.2416	1.340
0.2500	1.288
0.2583	1.240
0.2666	1.195
0.2750	1.150
0.2833	1.108
0.2916	1.069
0.3000	1.031
0.3083	0.990

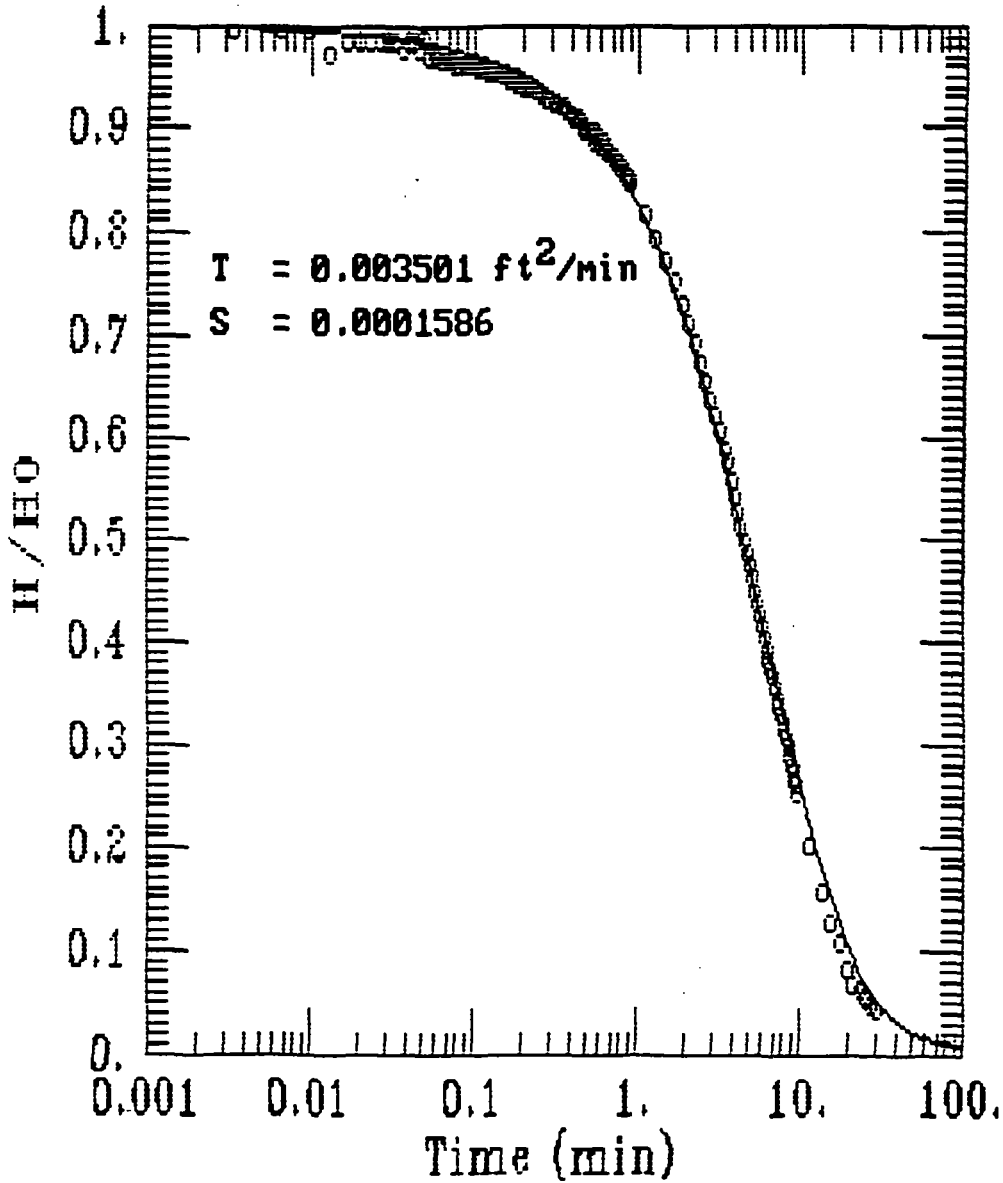
Test:	F3 - Slvg at
File:	F3-T2
Round:	KTEST3
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	t = 0.1333 t = 2.40
Column 3:	
	t = _____ t = _____

0.3333	0.889
0.3500	0.828
0.3666	0.770
0.3833	0.718
0.4000	0.670
0.4166	0.621
0.4333	0.583
0.4500	0.541
0.4666	0.505
0.4833	0.473
0.5000	0.441
0.5166	0.412
0.5333	0.386
0.5500	0.360
0.5666	0.338
0.5833	0.315
0.6000	0.293
0.6166	0.277
0.6333	0.257
0.6500	0.244
0.6666	0.228
0.6833	0.215
0.7000	0.203
0.7166	0.190
0.7333	0.180
0.7500	0.167
0.7666	0.157
0.7833	0.148
0.8000	0.141
0.8166	0.132
0.8333	0.125
0.8500	0.119
0.8666	0.112
0.8833	0.106
0.9000	0.099
0.9166	0.093
0.9333	0.090
0.9500	0.083
0.9666	0.080
0.9833	0.077
1.0000	0.074
1.2000	0.041
1.4000	0.025
1.6000	0.016
1.8000	0.012
2.0000	0.009
2.2000	0.009
2.4000	0.006 ✓
2.6000	0.006
2.8000	0.006
3.0000	0.006
3.2000	0.003
3.4000	0.006
3.6000	0.006

WELL CLUSTER: F
WELL ID: F4
SCREENED INTERVAL: 71-76

TEST METHOD: Cooper et al.
SLUG IN/SLUG OUT: slug out
K-VALUE: 0.327 Ft/day

F4-T2



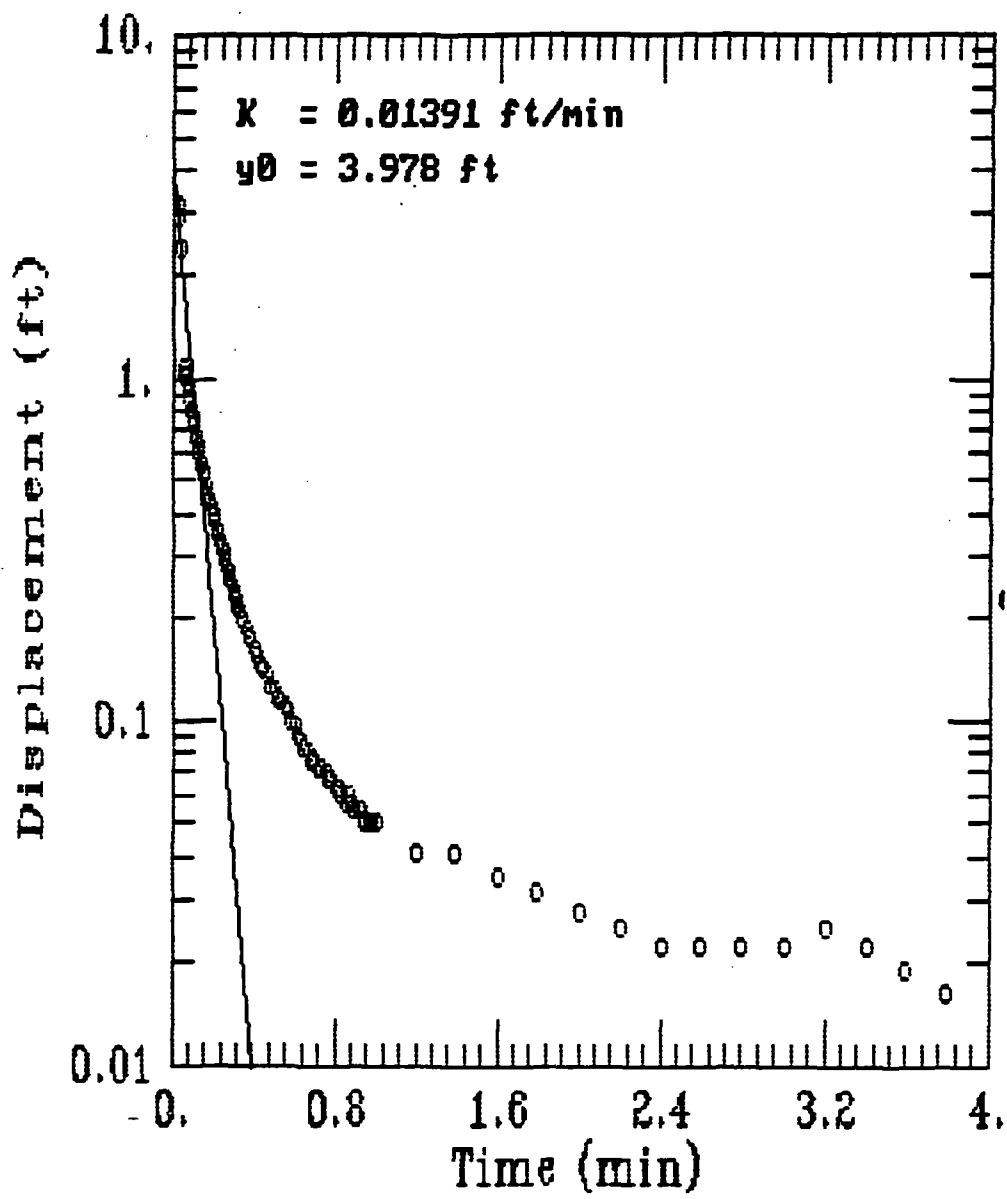
0.2200	2.147
0.2233	2.140
0.2266	2.140
0.2300	2.140
0.2333	2.140
0.2366	2.134
0.2400	2.134
0.2433	2.134
0.2466	2.134
0.2500	2.134
0.2533	2.134
0.2566	2.128
0.2600	2.128
0.2633	2.128
0.2666	2.128
0.2700	2.128
0.2733	2.121
0.2766	2.121
0.2800	2.121
0.2833	2.121
0.2866	2.121
0.2900	2.121
0.2933	2.115
0.2966	2.115
0.3000	2.115
0.3033	2.115
0.3066	2.115
0.3100	2.115
0.3133	2.109
0.3166	2.109
0.3200	2.109
0.3233	2.109
0.3266	2.109
0.3300	2.102
0.3333	2.102
0.3500	2.096
0.3666	2.090
0.3833	2.083
0.4000	2.083
0.4166	2.077
0.4333	2.071
0.4500	2.065
0.4666	2.058
0.4833	2.052
0.5000	2.052
0.5166	2.046
0.5333	2.039
0.5500	2.027
0.5666	2.027
0.5833	2.027
0.6000	2.014
0.6166	2.027
0.6333	1.995
0.6500	2.014
0.6666	1.989
0.6833	1.995
0.7000	2.001
0.7166	1.982
0.7333	1.976
0.7500	1.976
0.7666	1.970
0.7833	1.963
0.8000	1.963
0.8166	1.957

0.8833	1.938
0.9000	1.932
0.9166	1.926
0.9333	1.926
0.9500	1.919
0.9666	1.913
0.9833	1.913
1.0000	1.907
1.2000	1.837
1.4000	1.787
1.6000	1.736
1.8000	1.692
2.0000	1.641
2.2000	1.604
2.4000	1.559
2.6000	1.515
2.8000	1.477
3.0000	1.433
3.2000	1.395
3.4000	1.364
3.6000	1.326
3.8000	1.294
4.0000	1.256
4.2000	1.218
4.4000	1.187
4.6000	1.155
4.8000	1.124
5.0000	1.098
5.2000	1.067
5.4000	1.042
5.6000	1.010
5.8000	0.985
6.0000	0.959
6.2000	0.934
6.4000	0.909
6.6000	0.884
6.8000	0.858
7.0000	0.839
7.2000	0.821
7.4000	0.795
7.6000	0.776
7.8000	0.757
8.0000	0.738
8.2000	0.719
8.4000	0.707
8.6000	0.688
8.8000	0.669
9.0000	0.650
9.2000	0.631
9.4000	0.618
9.6000	0.599
9.8000	0.587
10.0000	0.574
12.0000	0.448
14.0000	0.353
16.0000	0.284
18.0000	0.239
20.0000	0.183
22.0000	0.151
24.0000	0.138
26.0000	0.120
28.0000	0.107
30.0000	0.094

WELL CLUSTER: G
WELL ID: G1-1
SCREENED INTERVAL: 2-10.5

TEST METHOD: Burser Rise
SLUG IN/SLUG OUT: Slug out
K-VALUE: 20.0 ft/day

G1-T2-1



0.0000	0.000	-0.006
0.0083	0.000	0.127
0.0166	0.000	0.298
0.0250	3.175	0.152
0.0333	2.985	5.768
0.0416	2.381	1.093
0.0500	1.009	0.375
0.0583	1.080	0.553
0.0666	1.015	0.184
0.0750	0.932	-0.057
0.0833	0.871	-0.235
0.0916	0.816	0.470
0.1000	0.761	0.050
0.1083	0.720	0.171
0.1166	0.671	0.343
0.1250	0.636	0.197
0.1333	0.601	0.146
0.1416	0.565	0.038
0.1500	0.536	-0.050
0.1583	0.514	-0.133
0.1666	0.485	-0.197
0.1750	0.462	-0.235
0.1833	0.443	-0.241
0.1916	0.424	-0.228
0.2000	0.401	-0.203
0.2083	0.382	-0.165
0.2166	0.366	-0.114
0.2250	0.350	-0.063
0.2333	0.334	-0.012
0.2416	0.321	0.038
0.2500	0.308	0.076
0.2583	0.295	0.101
0.2666	0.282	0.108
0.2750	0.273	0.108
0.2833	0.260	0.101
0.2916	0.253	0.082
0.3000	0.241	0.057
0.3083	0.234	0.031
0.3166	0.228	0.006
0.3250	0.218	-0.019
0.3333	0.212	-0.078
0.3500	0.199	-0.063
0.3666	0.186	-0.063
0.3833	0.176	-0.044
0.4000	0.163	-0.019
0.4166	0.154	0.006
0.4333	0.147	0.019
0.4500	0.141	0.025
0.4666	0.135	0.019
0.4833	0.125	0.006
0.5000	0.122	-0.006
0.5166	0.115	-0.019
0.5333	0.112	-0.019
0.5500	0.109	-0.012
0.5666	0.106	-0.012
0.5833	0.099	-0.006
0.6000	0.096	-0.006
0.6166	0.090	0.000
0.6333	0.086	0.000
0.6500	0.083	0.000

@ GIG5-T2-.dat

@ 0.0250

Note - G5 below peak
 had trouble with

0.0250
 0.0250
 0.0250

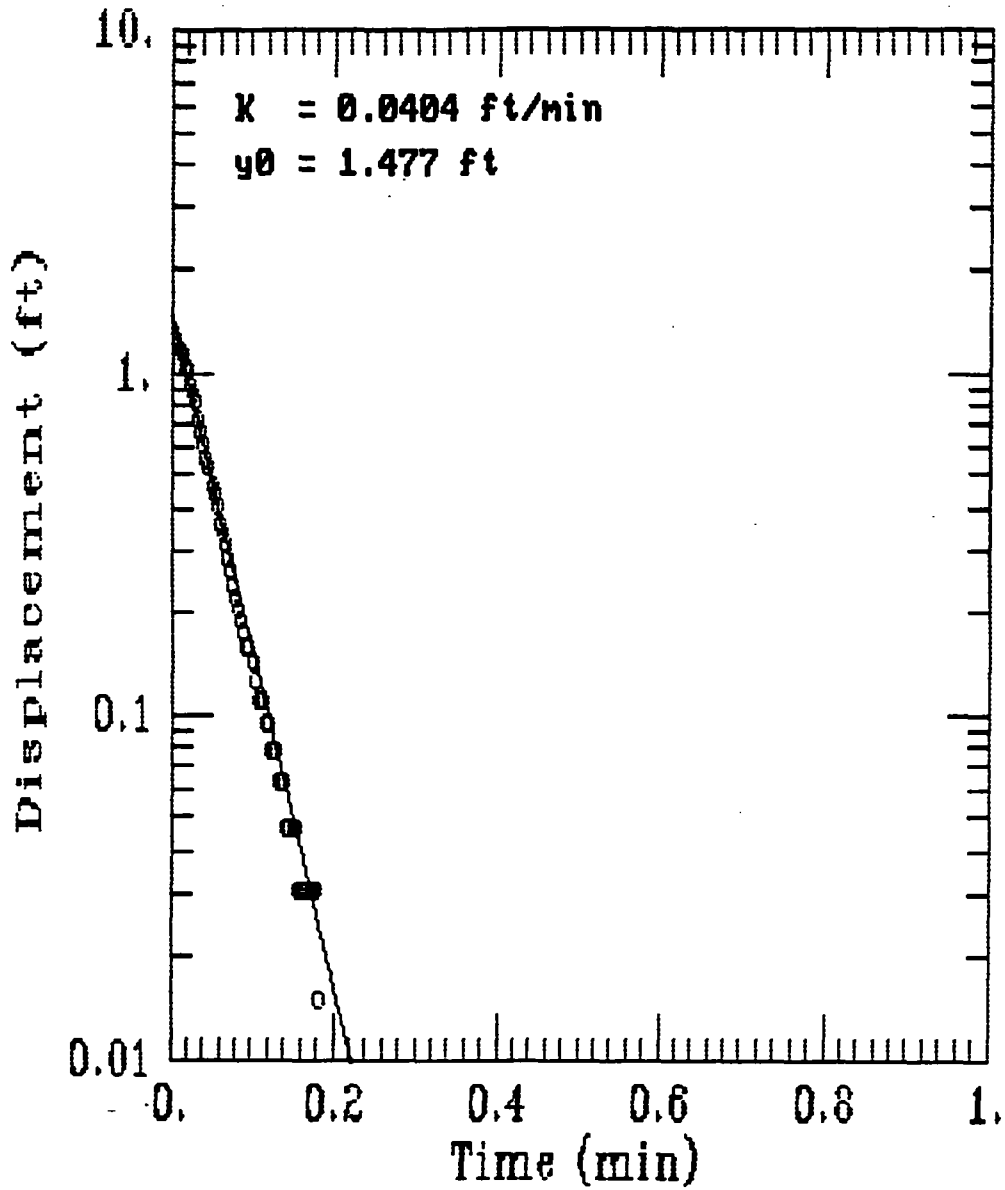
Test:	G1-1, G5 slug test
File:	GIG5-T2-.dat
Round:	KTEST2
Column 1:	Elapsed time (min)
Column 2:	Head G1-1 (ft)
	t ₁ = 0.0250 t ₂ = 3.80
Column 3:	
	t ₁ = _____ t ₂ = _____

0.6666	0.080	-0.006
0.6833	0.077	-0.006
0.7000	0.077	-0.006
0.7166	0.073	-0.006
0.7333	0.073	-0.006
0.7500	0.070	-0.006
0.7666	0.067	-0.006
0.7833	0.067	-0.012
0.8000	0.064	-0.006
0.8166	0.064	-0.012
0.8333	0.061	-0.006
0.8500	0.057	-0.012
0.8666	0.061	-0.012
0.8833	0.057	-0.006
0.9000	0.054	-0.006
0.9166	0.054	-0.006
0.9333	0.054	-0.012
0.9500	0.051	-0.006
0.9666	0.051	-0.006
0.9833	0.051	-0.006
1.0000	0.051	-0.006
1.2000	0.041	-0.012
1.4000	0.041	-0.019
1.6000	0.035	-0.012
1.8000	0.032	-0.006
2.0000	0.028	0.000
2.2000	0.025	0.006
2.4000	0.022	0.006
2.6000	0.022	0.006
2.8000	0.022	0.006
3.0000	0.022	0.000
3.2000	0.025	0.000
3.4000	0.022	0.006
3.6000	0.019	0.006
3.8000	0.016	0.012

WELL CLUSTER: G
WELL ID: G2
SCREENED INTERVAL: 63.5-68.5

TEST METHOD: Power Rice
SLUG IN/SLUG OUT: Slug out
K-VALUE: 58.2 ft/day

G2-T2



0.0000 0.094
 0.0033 0.726
 0.0066 0.300
 0.0100 0.568
 0.0133 0.632
 0.0166 0.189
 0.0200 0.458
 0.0233 -1.280
 0.0266 -0.410
 0.0300 0.505
 0.0333 0.679
 0.0366 0.458
 0.0400 0.268
 0.0433 0.284
 0.0466 0.284
 0.0500 0.158
 0.0533 0.410
 0.0566 0.347
 0.0600 0.268
 0.0633 0.600
 0.0666 0.742
 0.0700 0.853
 0.0733 0.948
 0.0766 1.169
 0.0800 1.295
 0.0833 1.311
 0.0866 1.279
 0.0900 1.264
 0.0933 1.200
 0.0966 1.169
 0.1000 1.121
 0.1033 1.042
 0.1066 1.027
 0.1100 0.916
 0.1133 0.869
 0.1166 0.821
 0.1200 0.726
 0.1233 0.679
 0.1266 0.616
 0.1300 0.568
 0.1333 0.537
 0.1366 0.474
 0.1400 0.442
 0.1433 0.410
 0.1466 0.363
 0.1500 0.347
 0.1533 0.316
 0.1566 0.284
 0.1600 0.268
 0.1633 0.236
 0.1666 0.221
 0.1700 0.205
 0.1733 0.189
 0.1766 0.174
 0.1800 0.158
 0.1833 0.158
 0.1866 0.142
 0.1900 0.126
 0.1933 0.110
 0.1966 0.110

3 52 1-
 t = 0

Test:	<u>Q2 Slug out</u>
File:	<u>Q2-T2.dat</u>
Round:	<u>KTEST</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head (ft)</u>
	<u>t₀ = 0.0833 t₁ = 0.2700</u>
Column 3:	<u>t₀ = _____ t₁ = _____</u>

Q2 = 1.296
 LT = 21867

0.2000	0.110
0.2033	0.094
0.2066	0.094
0.2100	0.078
0.2133	0.078
0.2166	0.078
0.2200	0.063
0.2233	0.063
0.2266	0.063
0.2300	0.047
0.2333	0.047
0.2366	0.047
0.2400	0.047
0.2433	0.031
0.2466	0.031
0.2500	0.031
0.2533	0.031
0.2566	0.031
0.2600	0.031
0.2633	0.031
0.2666	0.031
0.2700	0.015
0.2733	0.015
0.2766	0.015
0.2800	0.015
0.2833	0.015
0.2866	0.015
0.2900	0.015
0.2933	0.015
0.2966	0.015
0.3000	0.015
0.3033	0.015
0.3066	0.015
0.3100	0.015
0.3133	0.015
0.3166	0.000
0.3200	0.015
0.3233	0.000
0.3266	0.015
0.3300	0.000
0.3333	0.000
0.3500	0.000
0.3666	0.000
0.3833	0.000
0.4000	0.000
0.4166	0.000
0.4333	0.000
0.4500	0.000
0.4666	0.000
0.4833	0.000
0.5000	0.000
0.5166	0.000
0.5333	0.000
0.5500	0.000
0.5666	0.000
0.5833	0.000
0.6000	0.000
0.6166	0.000
0.6333	0.000
0.6500	0.000

0.6666	0.000
0.6833	0.000
0.7000	0.000
0.7166	0.000
0.7333	0.000
0.7500	0.000
0.7666	0.000
0.7833	0.000
0.8000	0.000
0.8166	0.000
0.8333	0.000
0.8500	0.000
0.8666	0.000
0.8833	0.000
0.9000	0.000
0.9166	0.000
0.9333	0.000
0.9500	0.000
0.9666	0.000
0.9833	0.000
1.0000	0.000
1.2000	0.000
1.4000	0.000
1.6000	-0.015
1.8000	-0.015
2.0000	-0.015
2.2000	-0.015
2.4000	-0.015
2.6000	-0.015
2.8000	-0.015
3.0000	-0.015
3.2000	-0.015
3.4000	-0.015
3.6000	-0.015
3.8000	-0.015
4.0000	-0.015
4.2000	-0.015
4.4000	-0.015
4.6000	-0.015
4.8000	-0.015
5.0000	-0.015
5.2000	-0.015
5.4000	-0.015
5.6000	-0.015
5.8000	-0.015
6.0000	-0.015
6.2000	-0.015
6.4000	-0.015
6.6000	-0.015
6.8000	-0.015
7.0000	-0.015
7.2000	-0.015
7.4000	-0.015
7.6000	-0.015
7.8000	-0.015
8.0000	-0.015
8.2000	-0.015
8.4000	-0.015
8.6000	-0.015
8.8000	-0.015

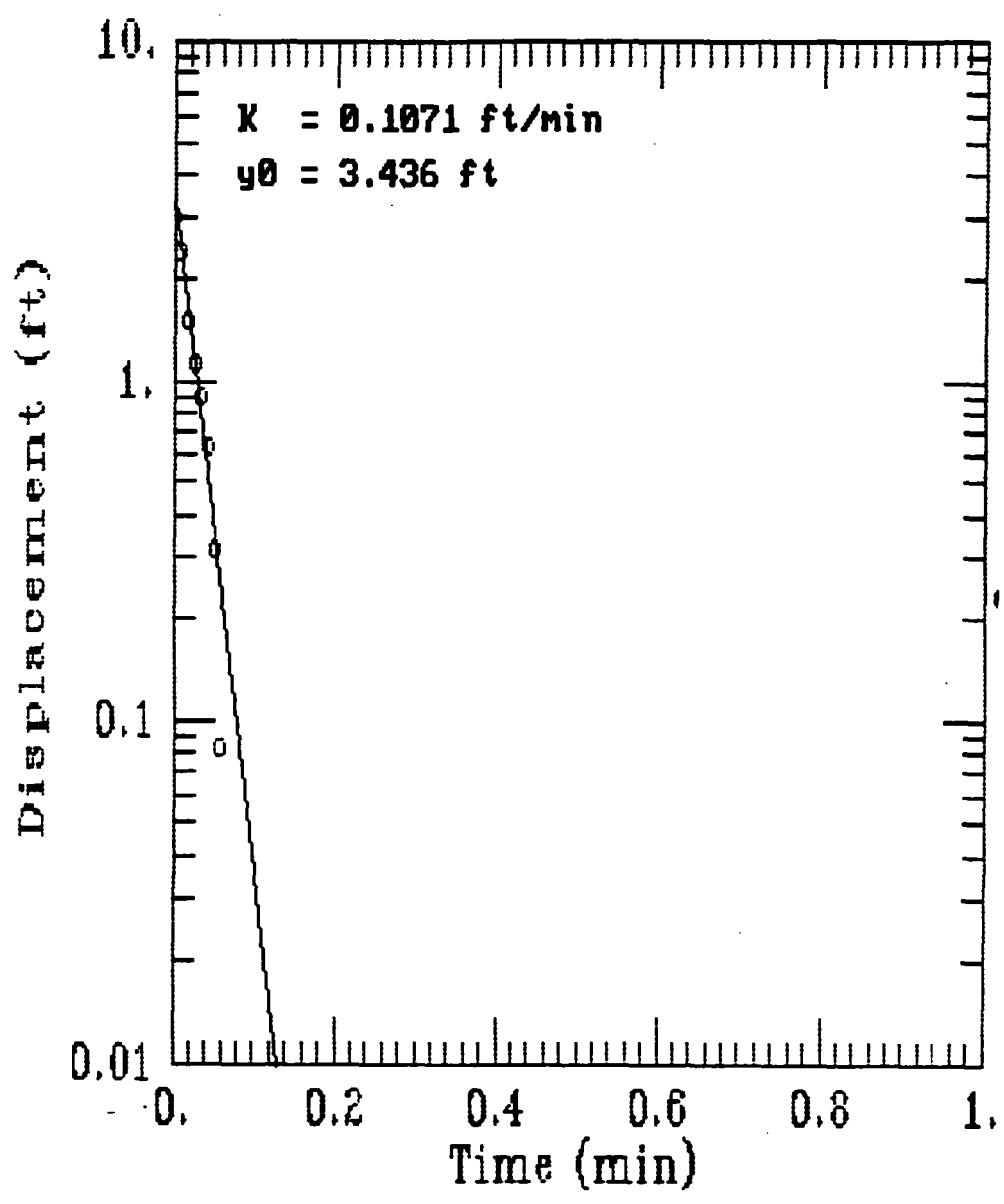
9.2000
9.4000
9.6000
9.8000
10.0000
12.0000

-0.015
-0.015
-0.015
-0.015
-0.015
-0.015
0.000

WELL CLUSTER: 6
WELL ID: 63
SCREENED INTERVAL: 96.5-101.5

TEST METHOD: Banner Rise
SLUG IN/SLUG OUT: Slug out
K-VALUE: 154 ft/day

GS-T2-1



0.0000	0.000	0.009
0.0083	0.553	0.012
0.0166	3.038	0.012
0.0250	2.402	0.655
0.0333	1.506	1.542
0.0416	1.144	1.634
0.0500	0.902	1.789
0.0583	0.642	1.900
0.0666	0.317	1.824
0.0750	0.082	1.815
0.0833	-0.101	1.812
0.0916	-0.241	1.789
0.1000	-0.330	1.780
0.1083	-0.362	1.774
0.1166	-0.368	1.758
0.1250	-0.343	1.745
0.1333	-0.298	1.736
0.1416	-0.241	1.726
0.1500	-0.171	1.717
0.1583	-0.101	1.707
0.1666	-0.044	1.698
0.1750	0.012	1.688
0.1833	0.063	1.685
0.1916	0.095	1.675
0.2000	0.114	1.663
0.2083	0.127	1.656
0.2166	0.133	1.647
0.2250	0.127	1.641
0.2333	0.114	1.634
0.2416	0.101	1.622
0.2500	0.089	1.609
0.2583	0.076	1.606
0.2666	0.057	1.599
0.2750	0.044	1.590
0.2833	0.031	1.584
0.2916	0.025	1.571
0.3000	0.019	1.565
0.3083	0.019	1.558
0.3166	0.012	1.555
0.3250	0.012	1.546
0.3333	0.019	1.536
0.3500	0.019	1.523
0.3666	0.025	1.508
0.3833	0.038	1.492
0.4000	0.038	1.476
0.4166	0.031	1.466
0.4333	0.038	1.451
0.4500	0.038	1.441
0.4666	0.038	1.425
0.4833	0.038	1.416
0.5000	0.038	1.400
0.5166	0.031	1.387
0.5333	0.031	1.374
0.5500	0.031	1.365
0.5666	0.031	1.352
0.5833	0.031	1.340
0.6000	0.038	1.327
0.6166	0.031	1.314
0.6333	0.031	1.305
0.6500	0.031	1.289

② G364-T2-dat

Trapped

63 2.956
- 0.0001

64 1.172
- 0.0001

Test:	<u>G3, G4 Slug out</u>
File:	<u>G364-T2-dat</u>
Round:	<u>KTEST2</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head G3 (ft)</u>
	<u>t₁ = 0.0166 t₂ = 0.750</u>
Column 3:	<u>Head G4 (ft)</u>
	<u>t₁ = 0.0583 t₂ = 4.80</u>

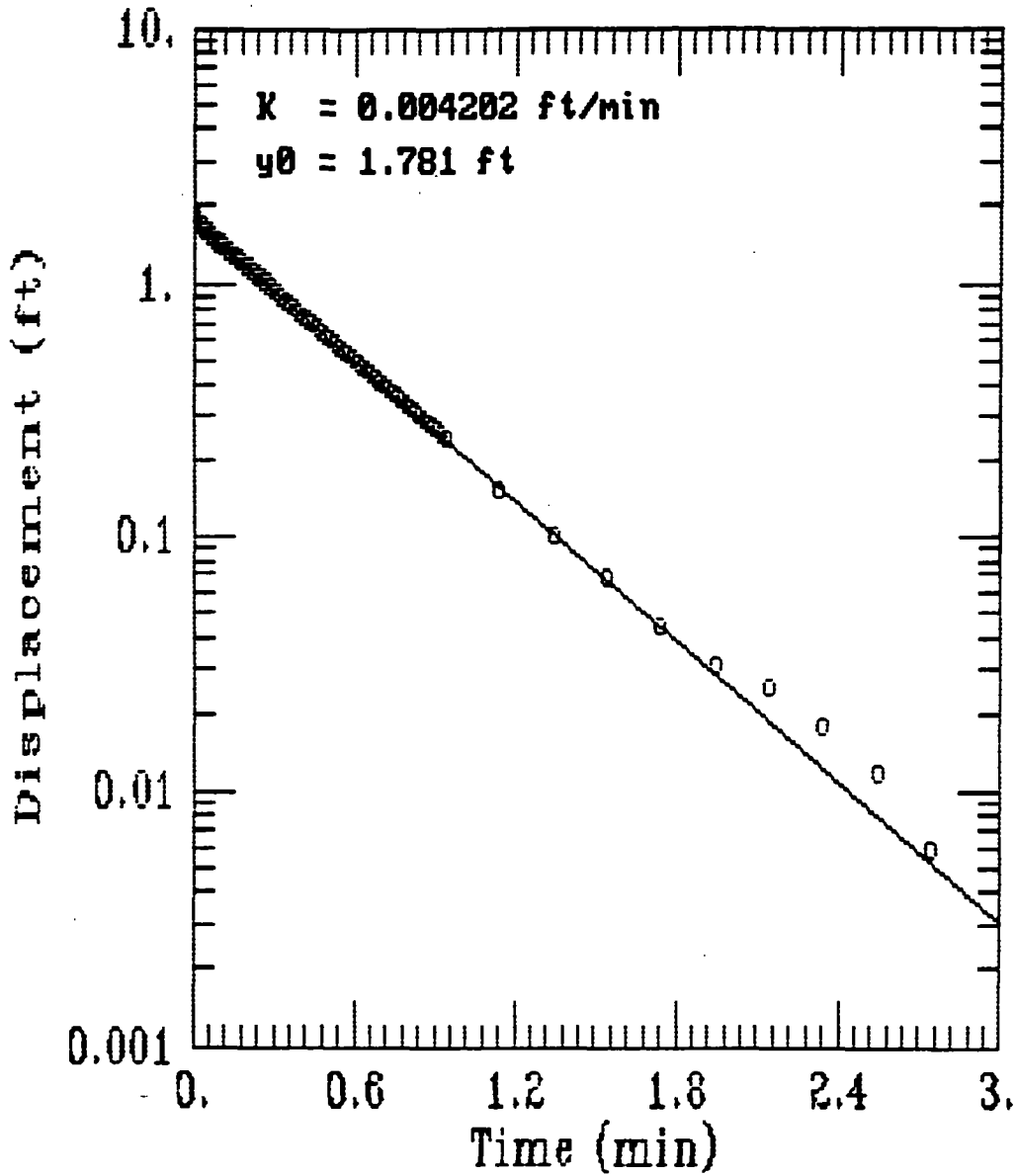
0.6666	0.038	1.283
0.6833	0.031	1.270
0.7000	0.031	1.260
0.7166	0.031	1.251
0.7333	0.031	1.235
0.7500	0.031	1.226
0.7666	0.031	1.213
0.7833	0.038	1.207
0.8000	0.038	1.194
0.8166	0.031	1.181
0.8333	0.031	1.172
0.8500	0.031	1.162
0.8666	0.031	1.150
0.8833	0.031	1.140
0.9000	0.031	1.131
0.9166	0.031	1.121
0.9333	0.031	1.112
0.9500	0.031	1.099
0.9666	0.031	1.093
0.9833	0.031	1.083
1.0000	0.038	1.070
1.2000	0.031	0.956
1.4000	0.031	0.849
1.6000	0.031	0.760
1.8000	0.031	0.674
2.0000	0.031	0.592
2.2000	0.031	0.522
2.4000	0.031	0.459
2.6000	0.031	0.402
2.8000	0.025	0.354
3.0000	0.025	0.307
3.2000	0.031	0.266
3.4000	0.031	0.228
3.6000	0.031	0.199
3.8000	0.031	0.171
4.0000	0.031	0.155
4.2000	0.025	0.129
4.4000	0.019	0.117
4.6000	0.031	0.101
4.8000	0.031	0.088

Proposed

WELL CLUSTER: I
WELL ID: I3
SCREENED INTERVAL: 48.2-53.2

TEST METHOD: Banner Pipe
SLUG IN/SLUG OUT: Slug out
K-VALUE: 6.45 ft/day

IS-T2



(13) I3-Td. dat

0.0000	1.415
0.0033	1.212
0.0066	1.459
0.0100	1.730
0.0133	0.151
0.0166	1.806
0.0200	1.174
0.0233	1.061
0.0266	0.998
0.0300	0.675
0.0333	0.827
0.0366	0.581
0.0400	0.833
0.0433	0.972
0.0466	1.478
0.0500	1.876
0.0533	1.876
0.0566	1.882
0.0600	1.857
0.0633	1.812
0.0666	1.775
0.0700	1.705
0.0733	1.737
0.0766	1.718
0.0800	1.705
0.0833	1.692
0.0866	1.680
0.0900	1.661
0.0933	1.648
0.0966	1.636
0.1000	1.623
0.1033	1.610
0.1066	1.598
0.1100	1.585
0.1133	1.572
0.1166	1.566
0.1200	1.554
0.1233	1.541
0.1266	1.528
0.1300	1.516
0.1333	1.503
0.1366	1.497
0.1400	1.484
0.1433	1.471
0.1466	1.459
0.1500	1.452
0.1533	1.440
0.1566	1.433
0.1600	1.421
0.1633	1.415
0.1666	1.402
0.1700	1.389
0.1733	1.383
0.1766	1.370
0.1800	1.364
0.1833	1.351
0.1866	1.345
0.1900	1.332
0.1933	1.326
0.1966	1.320

$\mu = 1.876$
 $\Delta t = 2.434$

Test:	I3 Slig cut
File:	I3-Td. dat
Round:	KTEST
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	$t_0 = 2.0506$ $t_1 = 2.80$
Column 3:	
	$t_0 = \underline{\hspace{2cm}}$ $t_1 = \underline{\hspace{2cm}}$

0.2000	1.307
0.2033	1.301
0.2066	1.288
0.2100	1.276
0.2133	1.276
0.2166	1.263
0.2200	1.257
0.2233	1.244
0.2266	1.238
0.2300	1.225
0.2333	1.219
0.2366	1.212
0.2400	1.206
0.2433	1.193
0.2466	1.187
0.2500	1.181
0.2533	1.174
0.2566	1.162
0.2600	1.156
0.2633	1.149
0.2666	1.143
0.2700	1.137
0.2733	1.124
0.2766	1.118
0.2800	1.111
0.2833	1.105
0.2866	1.092
0.2900	1.086
0.2933	1.080
0.2966	1.073
0.3000	1.067
0.3033	1.061
0.3066	1.054
0.3100	1.048
0.3133	1.035
0.3166	1.029
0.3200	1.023
0.3233	1.023
0.3266	1.010
0.3300	1.004
0.3333	0.998
0.3500	0.960
0.3666	0.928
0.3833	0.897
0.4000	0.865
0.4166	0.833
0.4333	0.802
0.4500	0.777
0.4666	0.751
0.4833	0.720
0.5000	0.694
0.5166	0.675
0.5333	0.650
0.5500	0.625
0.5666	0.606
0.5833	0.587
0.6000	0.568
0.6166	0.549
0.6333	0.530
0.6500	0.511

0.6666	0.492
0.6833	0.473
0.7000	0.461
0.7166	0.442
0.7333	0.429
0.7500	0.416
0.7666	0.397
0.7833	0.385
0.8000	0.372
0.8166	0.360
0.8333	0.347
0.8500	0.334
0.8666	0.328
0.8833	0.315
0.9000	0.303
0.9166	0.296
0.9333	0.284
0.9500	0.271
0.9666	0.265
0.9833	0.258
1.0000	0.246
1.2000	0.151
1.4000	0.101
1.6000	0.069
1.8000	0.044
2.0000	0.031
2.2000	0.025
2.4000	0.018
2.6000	0.012
2.8000	0.006
3.0000	0.006
3.2000	0.006
3.4000	0.006
3.6000	0.006
3.8000	0.000
4.0000	0.000
4.2000	0.000
4.4000	0.000
4.6000	0.000
4.8000	0.000
5.0000	0.000
5.2000	0.000
5.4000	0.000
5.6000	0.000
5.8000	0.000
6.0000	0.000
6.2000	0.000
6.4000	0.000
6.6000	0.000
6.8000	0.000
7.0000	0.000
7.2000	0.000
7.4000	0.000
7.6000	0.000
7.8000	0.000
8.0000	0.000
8.2000	0.000
8.4000	0.000
8.6000	0.000
8.8000	0.000

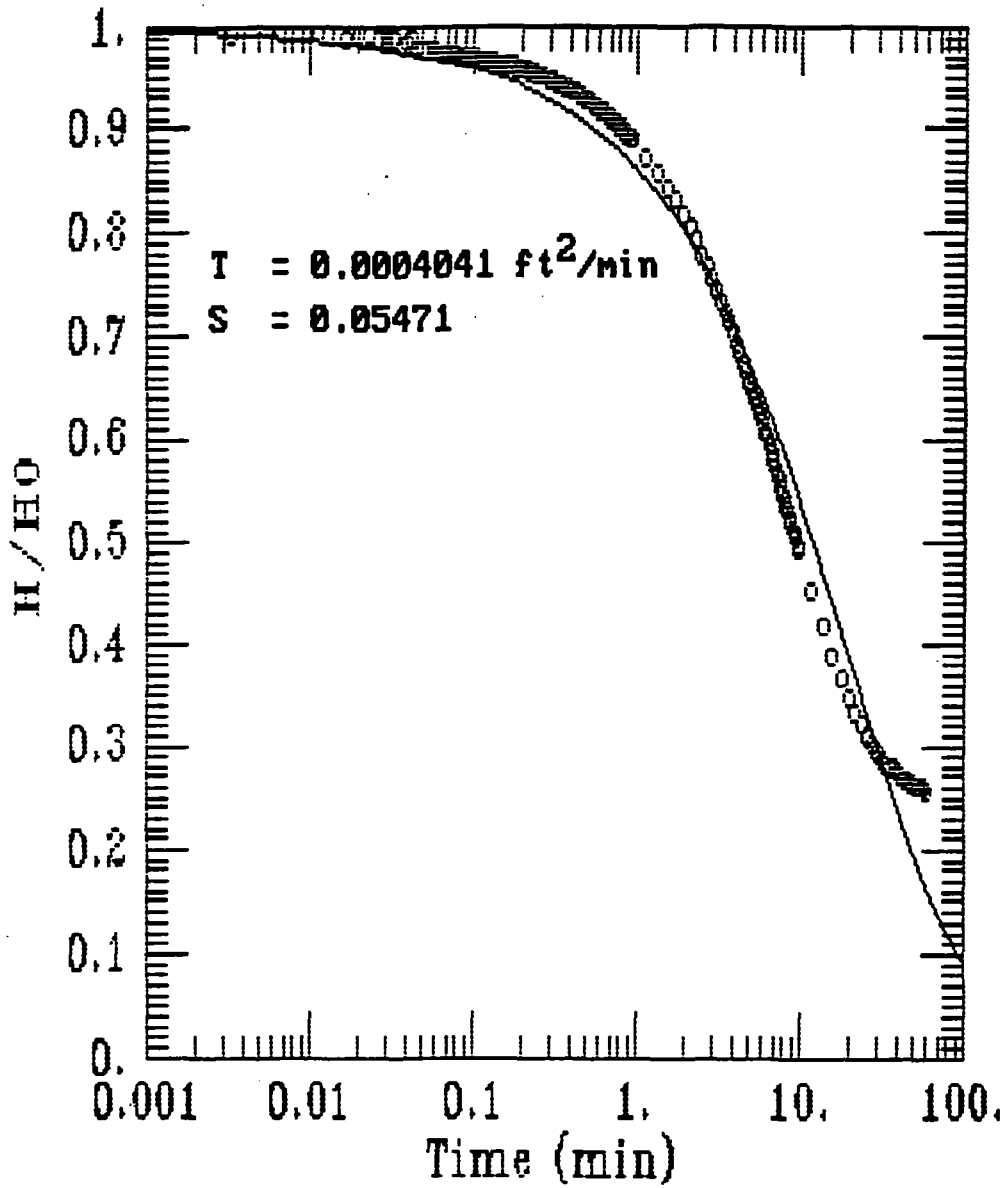
② 2.243

9.0000	0.000
9.2000	0.000
9.4000	0.000
9.6000	0.000
9.8000	0.000
10.0000	0.000

WELL CLUSTER: I
WELL ID: I4
SCREENED INTERVAL: 58.7-68.7

TEST METHOD: Couper et al.
SLUG IN/SLUG OUT: Slug out
K-VALUE: 0.042 ft/day

I4-T2



IA-10.00

IA-10

Stopped @
Rotation # 10

0.0000	1.020
0.0033	1.269
0.0066	1.528
0.0100	2.482
0.0133	2.735
0.0166	3.145
0.0200	3.322
0.0233	2.703
0.0266	1.686
0.0300	2.849
0.0333	3.537
0.0366	2.950
0.0400	3.518
0.0433	3.354
0.0466	3.253
0.0500	3.158
0.0533	3.392
0.0566	3.531
<u>0.0600</u>	<u>3.638</u>
0.0633	3.613
0.0666	3.619
0.0700	3.619
0.0733	3.613
0.0766	3.594
0.0800	3.607
0.0833	3.607
0.0866	3.600
0.0900	3.594
0.0933	3.588
0.0966	3.562
0.1000	3.581
0.1033	3.588
0.1066	3.550
0.1100	3.556
0.1133	3.556
0.1166	3.550
0.1200	3.550
0.1233	3.543
0.1266	3.543
0.1300	3.543
0.1333	3.537
0.1366	3.537
0.1400	3.537
0.1433	3.531
0.1466	3.531
0.1500	3.531
0.1533	3.531
0.1566	3.524
0.1600	3.524
0.1633	3.524
0.1666	3.524
0.1700	3.518
0.1733	3.518
0.1766	3.518
0.1800	3.518
0.1833	3.512
0.1866	3.512
0.1900	3.512
0.1933	3.512
0.1966	3.512
0.2000	3.505
0.2033	3.505
0.2066	3.505
0.2100	3.505

Start

Test:	IA Slug out
File:	IA-T2-dat
Round:	KTEST
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	$t_0 = 2.0400$ $t_1 = 60.0$
Column 3:	
	$t_0 =$ _____ $t_1 =$ _____

0.2200	3.477
0.2233	3.493
0.2266	3.499
0.2300	3.493
0.2333	3.493
0.2366	3.493
0.2400	3.493
0.2433	3.487
0.2466	3.487
0.2500	3.480
0.2533	3.487
0.2566	3.487
0.2600	3.487
0.2633	3.480
0.2666	3.480
0.2700	3.480
0.2733	3.480
0.2766	3.474
0.2800	3.474
0.2833	3.474
0.2866	3.474
0.2900	3.474
0.2933	3.468
0.2966	3.468
0.3000	3.468
0.3033	3.461
0.3066	3.461
0.3100	3.461
0.3133	3.461
0.3166	3.461
0.3200	3.461
0.3233	3.461
0.3266	3.455
0.3300	3.455
0.3333	3.455
0.3500	3.449
0.3566	3.442
0.3633	3.436
0.4000	3.430
0.4166	3.423
0.4333	3.417
0.4500	3.411
0.4666	3.404
0.4833	3.398
0.5000	3.392
0.5166	3.385
0.5333	3.379
0.5500	3.373
0.5666	3.373
0.5833	3.366
0.6000	3.360
0.6166	3.354
0.6333	3.348
0.6500	3.341
0.6666	3.335
0.6833	3.329
0.7000	3.329
0.7166	3.322
0.7333	3.316
0.7500	3.310
0.7666	3.310
0.7833	3.303
0.8000	3.297
0.8166	3.291

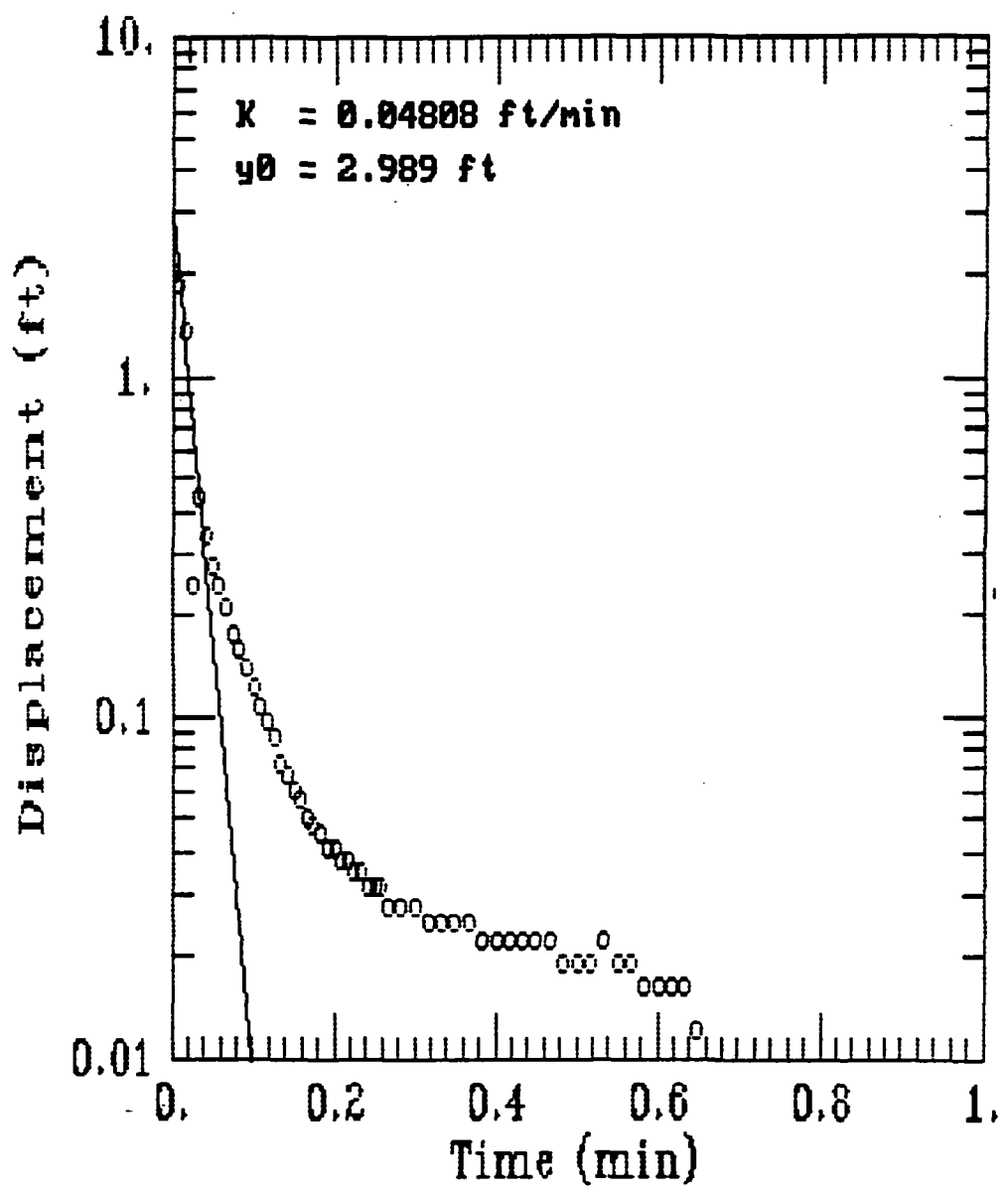
0.8833	3.272
0.9000	3.265
0.9166	3.259
0.9333	3.259
0.9500	3.253
0.9666	3.246
0.9833	3.246
1.0000	3.240
1.2000	3.171
1.4000	3.120
1.6000	3.063
1.8000	3.019
2.0000	2.969
2.2000	2.924
2.4000	2.880
2.6000	2.830
2.8000	2.792
3.0000	2.747
3.2000	2.710
3.4000	2.665
3.6000	2.627
3.8000	2.596
4.0000	2.558
4.2000	2.520
4.4000	2.488
4.6000	2.451
4.8000	2.419
5.0000	2.387
5.2000	2.356
5.4000	2.324
5.6000	2.299
5.8000	2.267
6.0000	2.242
6.2000	2.210
6.4000	2.185
6.6000	2.160
6.8000	2.135
7.0000	2.103
7.2000	2.084
7.4000	2.059
7.6000	2.034
7.8000	2.015
8.0000	1.989
8.2000	1.970
8.4000	1.945
8.6000	1.926
8.8000	1.907
9.0000	1.888
9.2000	1.869
9.4000	1.850
9.6000	1.832
9.8000	1.813
10.0000	1.794
12.0000	1.642
14.0000	1.516
16.0000	1.415
18.0000	1.332
20.0000	1.263
22.0000	1.206
24.0000	1.162
26.0000	1.124
28.0000	1.099
30.0000	1.067

40.0000	1.010
42.0000	0.998
44.0000	0.985
46.0000	0.979
48.0000	0.972
50.0000	0.966
52.0000	0.960
54.0000	0.953
56.0000	0.953
58.0000	0.947
60.0000	0.947
	0.941

WELL CLUSTER: J
WELL ID: J1-1
SCREENED INTERVAL: 10-20

TEST METHOD: Banner Pipe
SLUG IN/SLUG OUT: Slug out
K-VALUE: 69.2 ft/day

J1-T2-1



0.0000	0.003	0.000
0.0083	0.003	0.000
0.0166	0.003	0.000
0.0250	0.003	0.000
0.0333	0.003	0.000
0.0416	0.003	0.000
0.0500	0.003	0.000
0.0583	0.154	0.000
0.0666	1.980	0.006
0.0750	1.864	1.112
0.0833	1.359	0.322
0.0916	0.247	0.985
0.1000	0.440	1.301
0.1083	0.340	1.308
0.1166	0.276	1.257
0.1250	0.244	1.219
0.1333	0.208	1.169
0.1416	0.176	1.131
0.1500	0.157	1.106
0.1583	0.138	1.068
0.1666	0.122	1.023
0.1750	0.106	1.011
0.1833	0.096	0.979
0.1916	0.086	0.954
0.2000	0.073	0.935
0.2083	0.067	0.916
0.2166	0.061	0.884
0.2250	0.057	0.865
0.2333	0.051	0.853
0.2416	0.048	0.834
0.2500	0.045	0.821
0.2583	0.041	0.802
0.2666	0.041	0.790
0.2750	0.038	0.771
0.2833	0.038	0.752
0.2916	0.035	0.733
0.3000	0.035	0.720
0.3083	0.032	0.707
0.3166	0.032	0.688
0.3250	0.032	0.676
0.3333	0.028	0.663
0.3500	0.028	0.638
0.3666	0.028	0.613
0.3833	0.025	0.587
0.4000	0.025	0.562
0.4166	0.025	0.543
0.4333	0.025	0.524
0.4500	0.022	0.505
0.4666	0.022	0.486
0.4833	0.022	0.474
0.5000	0.022	0.461
0.5166	0.022	0.442
0.5333	0.022	0.429
0.5500	0.019	0.417
0.5666	0.019	0.404
0.5833	0.019	0.391
0.6000	0.022	0.385
0.6166	0.019	0.372
0.6333	0.019	0.360
0.6500	0.016	0.347

JKJ2-1d-2aT

J1 ΔH = 1.968

Δt = 0.65

J2 ΔH = 1.264

Δt = 4.492

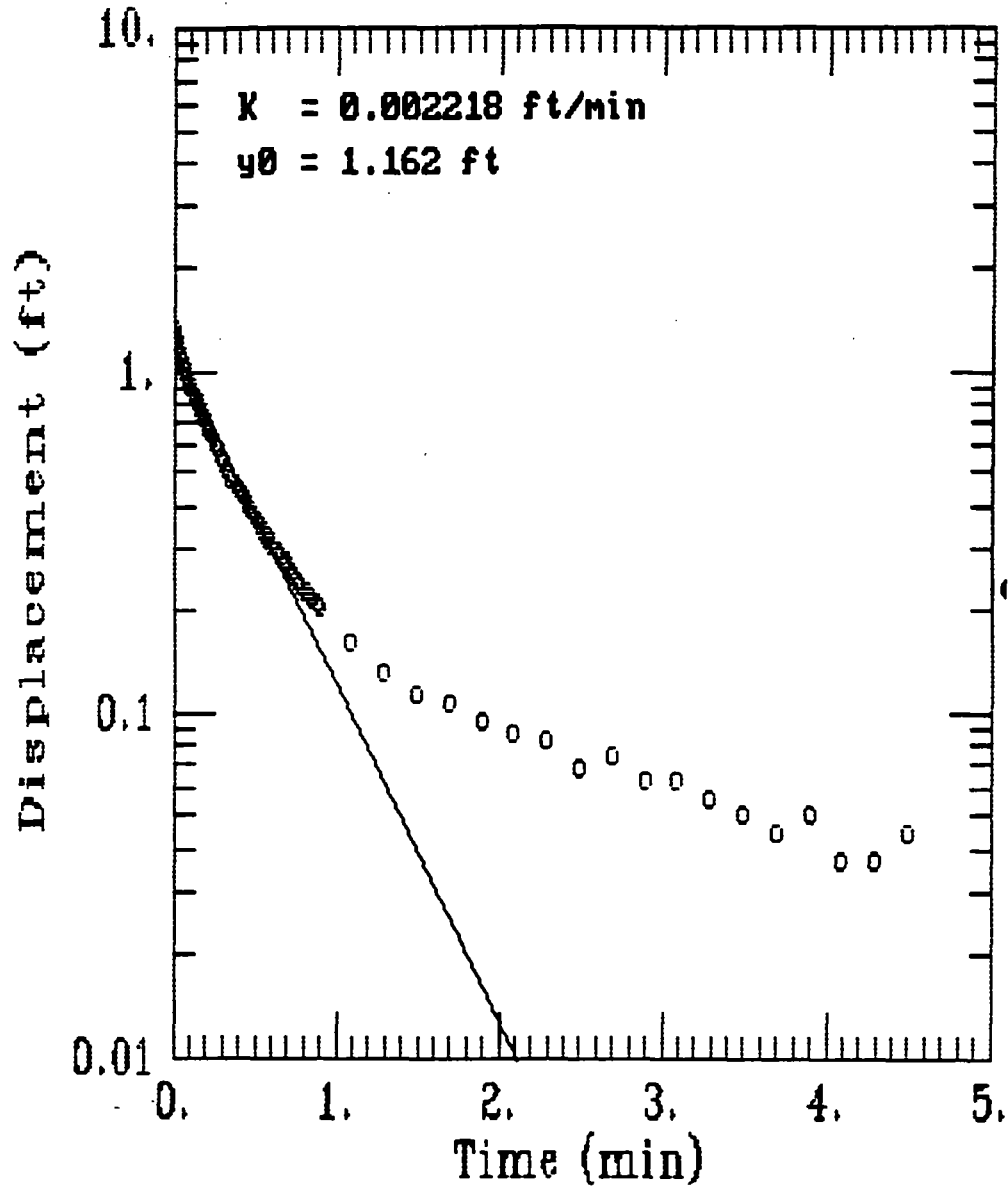
Test:	J1-1, J2-1	slug out
File:	JKJ2-T2-.dat	
Round:	KTEST2	
Column 1:	Elapsed time (min)	
Column 2:	Head J1-1 (ft)	
	t ₀ = 0.0666	t ₁ = 0.7166
Column 3:	Head J2-1 (ft)	
	t ₀ = 0.1083	t ₁ = 4.60

0.6666	0.016	0.341	
0.6833	0.016	0.328	@ 0.65
0.7000	0.016	0.322	
0.7166	0.012	0.309	
0.7333	0.012	0.303	
0.7500	0.012	0.297	
0.7666	0.016	0.290	
0.7833	0.012	0.278	
0.8000	0.016	0.278	
0.8166	0.012	0.265	
0.8333	0.012	0.259	
0.8500	0.009	0.252	
0.8666	0.009	0.246	
0.8833	0.009	0.240	
0.9000	0.009	0.233	
0.9166	0.009	0.227	
0.9333	0.009	0.227	
0.9500	0.006	0.221	
0.9666	0.006	0.214	
0.9833	0.006	0.208	
1.0000	0.003	0.202	
1.2000	0.003	0.164	
1.4000	0.000	0.132	
1.6000	0.003	0.113	
1.8000	0.003	0.107	
2.0000	0.006	0.094	
2.2000	0.006	0.088	
2.4000	0.006	0.082	
2.6000	0.003	0.069	
2.8000	0.006	0.075	
3.0000	0.000	0.063	
3.2000	0.003	0.063	
3.4000	0.000	0.056	
3.6000	0.000	0.050	
3.8000	-0.003	0.044	
4.0000	-0.006	0.050	
4.2000	-0.006	0.037	
4.4000	-0.003	0.037	
4.6000	0.000	0.044	@ 4 492

WELL CLUSTER: J
WELL ID: J2-1
SCREENED INTERVAL: 24-34

TEST METHOD: Bowser Pipe
SLUG IN/SLUG OUT: slug out
K-VALUE: 3.19 2/day

J2-T2-1



0.0000	0.003	0.000
0.0083	0.003	0.000
0.0166	0.003	0.000
0.0250	0.003	0.000
0.0333	0.003	0.000
0.0416	0.003	0.000
0.0500	0.003	0.000
0.0583	0.154	0.000
0.0666	1.980	0.006
0.0750	1.864	1.112
0.0833	1.359	0.322
0.0916	0.247	0.985
0.1000	0.440	1.301
0.1083	0.340	1.308
0.1166	0.276	1.257
0.1250	0.244	1.219
0.1333	0.208	1.169
0.1416	0.176	1.131
0.1500	0.157	1.106
0.1583	0.138	1.068
0.1666	0.122	1.023
0.1750	0.106	1.011
0.1833	0.096	0.979
0.1916	0.086	0.954
0.2000	0.073	0.935
0.2083	0.067	0.916
0.2166	0.061	0.884
0.2250	0.057	0.865
0.2333	0.051	0.853
0.2416	0.048	0.834
0.2500	0.045	0.821
0.2583	0.041	0.802
0.2666	0.041	0.790
0.2750	0.038	0.771
0.2833	0.038	0.752
0.2916	0.035	0.733
0.3000	0.035	0.720
0.3083	0.032	0.707
0.3166	0.032	0.688
0.3250	0.032	0.676
0.3333	0.028	0.663
0.3500	0.028	0.638
0.3666	0.028	0.613
0.3833	0.025	0.587
0.4000	0.025	0.562
0.4166	0.025	0.543
0.4333	0.025	0.524
0.4500	0.022	0.505
0.4666	0.022	0.486
0.4833	0.022	0.474
0.5000	0.022	0.461
0.5166	0.022	0.442
0.5333	0.022	0.429
0.5500	0.019	0.417
0.5666	0.019	0.404
0.5833	0.019	0.391
0.6000	0.022	0.385
0.6166	0.019	0.372
0.6333	0.019	0.360
0.6500	0.016	0.347

JKA-10-201

J1 $\Delta H = 1.968$

$\Delta t = 0.65$

J2 $\Delta H = 1.264$

$\Delta t = 4.492$

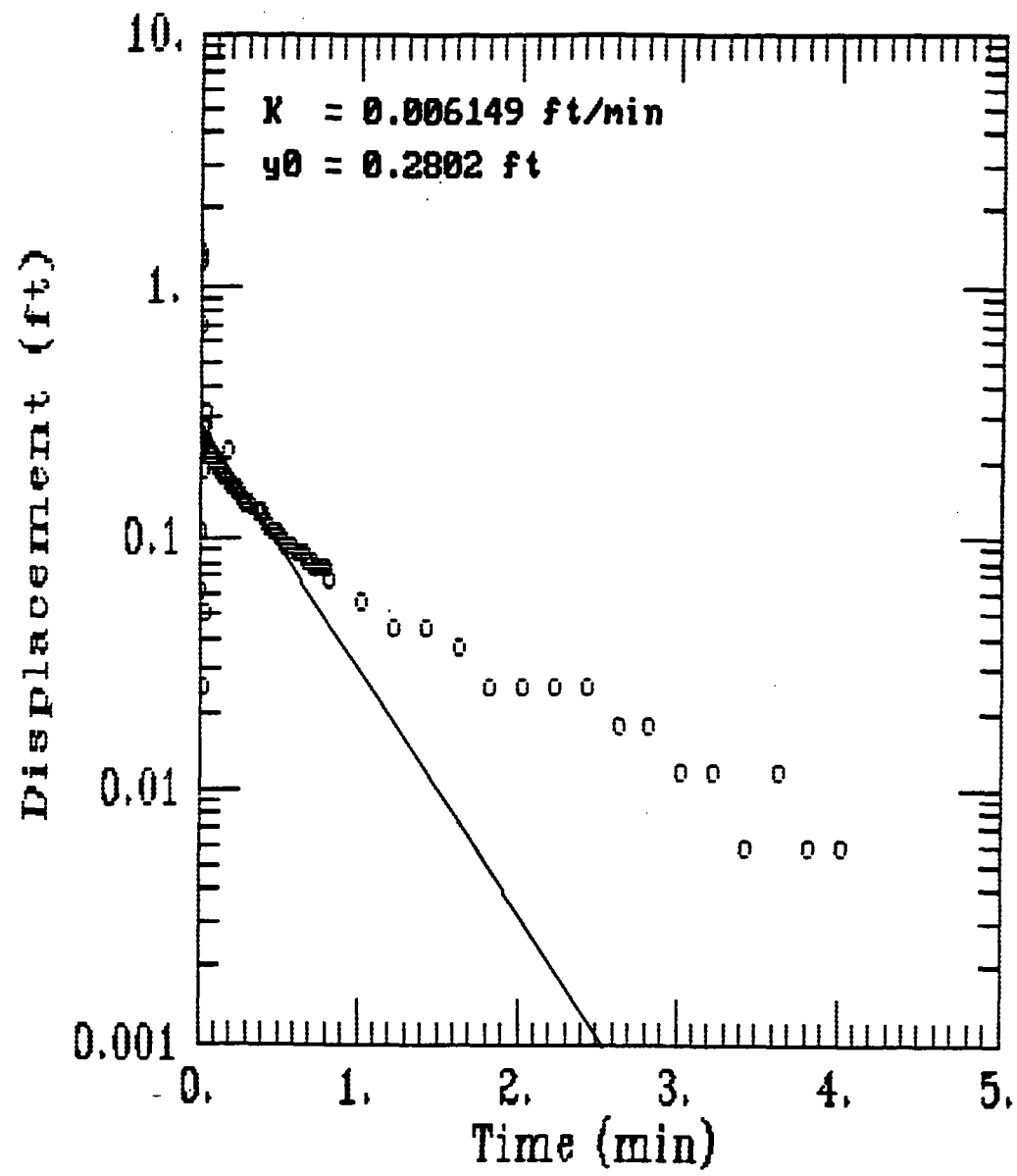
Test:	J1-1, J2-1	slug test
File:	J12-T2-dat	
Round:	KTEST2	
Column 1:	Elapsed time (min)	
Column 2:	Δ Head J1-1 (ft)	$b = 0.0666$ $l = 0.7166$
Column 3:	Δ Head J2-1 (ft)	$b = 0.1033$ $l = 4.60$

0.6666	0.016	0.341	
0.6833	0.016	0.328	@ 0.65
0.7000	0.016	0.322	
0.7166	0.012	0.309	
0.7333	0.012	0.303	
0.7500	0.012	0.297	
0.7666	0.016	0.290	
0.7833	0.012	0.278	
0.8000	0.016	0.278	
0.8166	0.012	0.265	
0.8333	0.012	0.259	
0.8500	0.009	0.252	
0.8666	0.009	0.246	
0.8833	0.009	0.240	
0.9000	0.009	0.233	
0.9166	0.009	0.227	
0.9333	0.009	0.227	
0.9500	0.006	0.221	
0.9666	0.006	0.214	
0.9833	0.006	0.208	
1.0000	0.003	0.202	
1.2000	0.003	0.164	
1.4000	0.000	0.132	
1.6000	0.003	0.113	
1.8000	0.003	0.107	
2.0000	0.006	0.094	
2.2000	0.006	0.088	
2.4000	0.006	0.082	
2.6000	0.003	0.069	
2.8000	0.006	0.075	
3.0000	0.000	0.063	
3.2000	0.003	0.063	
3.4000	0.000	0.056	
3.6000	0.000	0.050	
3.8000	-0.003	0.044	
4.0000	-0.006	0.050	
4.2000	-0.006	0.037	
4.4000	-0.003	0.037	
4.6000	0.000	0.044	@ 4 492

WELL CLUSTER: J
WELL ID: J3
SCREENED INTERVAL: 88.25-93.25

TEST METHOD: Boomer Pipe
SLUG IN/SLUG OUT: Slug out
K-VALUE: 2.25 ft/day

J3-T2



0.1000	-0.107
0.1033	-0.101
0.1066	0.897
0.1100	-0.025
0.1133	-0.966
0.1166	-0.581
0.1200	0.037
0.1233	-0.031
0.1266	-0.145
0.1300	-0.176
0.1333	-0.126
0.1366	0.461
0.1400	0.663
0.1433	-0.271
0.1466	-1.351
0.1500	-1.996
0.1533	-1.490
0.1566	-1.800
0.1600	-1.162
0.1633	-1.295
0.1666	-1.149
0.1700	-1.193
0.1733	-1.332
0.1766	-1.263
0.1800	-0.701
0.1833	-0.063
0.1866	-0.107
0.1900	-0.025
0.1933	-0.187
0.1966	-0.277
0.2000	-0.271
0.2033	-0.266
0.2066	-3.050
0.2100	-0.284
0.2133	-0.315
0.2166	-0.246
0.2200	-0.221
0.2233	-0.227
0.2266	-0.233
0.2300	-0.221
0.2333	-0.221
0.2366	-0.221
0.2400	-0.221
0.2433	-0.214
0.2466	-0.214
0.2500	-0.214
0.2533	-0.208
0.2566	-0.208
0.2600	-0.208
0.2633	-0.208
0.2666	-0.202
0.2700	-0.202
0.2733	-0.202
0.2766	-0.202
0.2800	-0.195
0.2833	-0.195
0.2866	-0.195
0.2900	-0.195
0.2933	-0.195
0.2966	-0.189
0.3000	-0.189
0.3033	-0.189
0.3066	-0.189

$$\Delta H = [1.326]$$

$$\Delta t = 4.0267$$

Test:	<u>J3 Slog out</u>
File:	<u>J3-T2.dat</u>
Round:	<u>KTEST</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head (ft)</u>
	<u>t = 0.1333 t = 4.20</u>
Column 3:	_____
	<u>t = _____ t = _____</u>

0.3166	-0.183
0.3200	-0.183
0.3233	-0.176
0.3266	-0.176
0.3300	-0.176
0.3333	-0.176
0.3500	-0.221
0.3666	-0.164
0.3833	-0.164
0.4000	-0.157
0.4166	-0.157
0.4333	-0.145
0.4500	-0.145
0.4666	-0.138
0.4833	-0.138
0.5000	-0.138
0.5166	-0.132
0.5333	-0.126
0.5500	-0.126
0.5666	-0.126
0.5833	-0.120
0.6000	-0.113
0.6166	-0.113
0.6333	-0.107
0.6500	-0.107
0.6666	-0.107
0.6833	-0.101
0.7000	-0.101
0.7166	-0.094
0.7333	-0.094
0.7500	-0.094
0.7666	-0.094
0.7833	-0.088
0.8000	-0.088
0.8166	-0.088
0.8333	-0.088
0.8500	-0.082
0.8666	-0.082
0.8833	-0.082
0.9000	-0.075
0.9166	-0.075
0.9333	-0.075
0.9500	-0.075
0.9666	-0.075
0.9833	-0.075
1.0000	-0.069
1.2000	-0.056
1.4000	-0.044
1.6000	-0.044
1.8000	-0.037
2.0000	-0.025
2.2000	-0.025
2.4000	-0.025
2.6000	-0.025
2.8000	-0.018
3.0000	-0.018
3.2000	-0.012
3.4000	-0.012
3.6000	-0.006
3.8000	-0.012
4.0000	-0.006
4.2000	-0.006
4.4000	0.000
4.6000	-0.006

5.4000	0.000
5.6000	-0.006
5.8000	0.000
6.0000	0.000
6.2000	-0.006
6.4000	0.000
6.6000	0.000
6.8000	0.000
7.0000	0.000
7.2000	-0.006
7.4000	-0.006
7.6000	0.000
7.8000	0.000
8.0000	0.000
8.2000	-0.006
8.4000	0.000
8.6000	-0.006
8.8000	0.000
9.0000	-0.006
9.2000	-0.006
9.4000	0.000
9.6000	0.000
9.8000	0.000
10.0000	-0.006
12.0000	0.000

MARKTEST

1201-1-T1

1./C1-1-T1 DAT

31pC1-1-T2 W

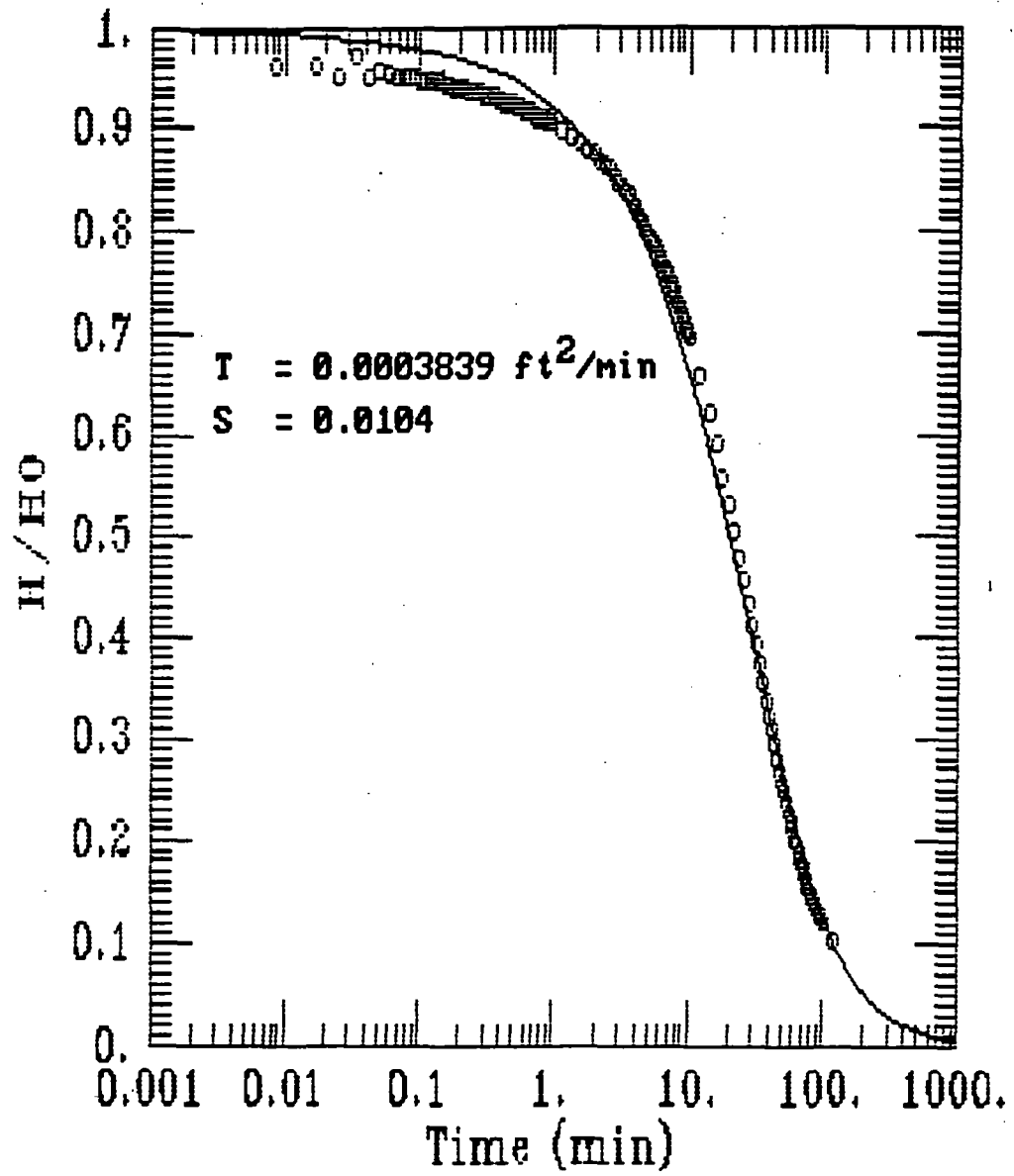
3PGC1-1-T2 DAT W

1-1-T1

WELL CLUSTER: J
WELL ID: J4
SCREENED INTERVAL: 101-111

TEST METHOD: Cooper et al.
SLUG IN/SLUG OUT: slug out
K-VALUE: 0.0268 ft/day

j4-t2



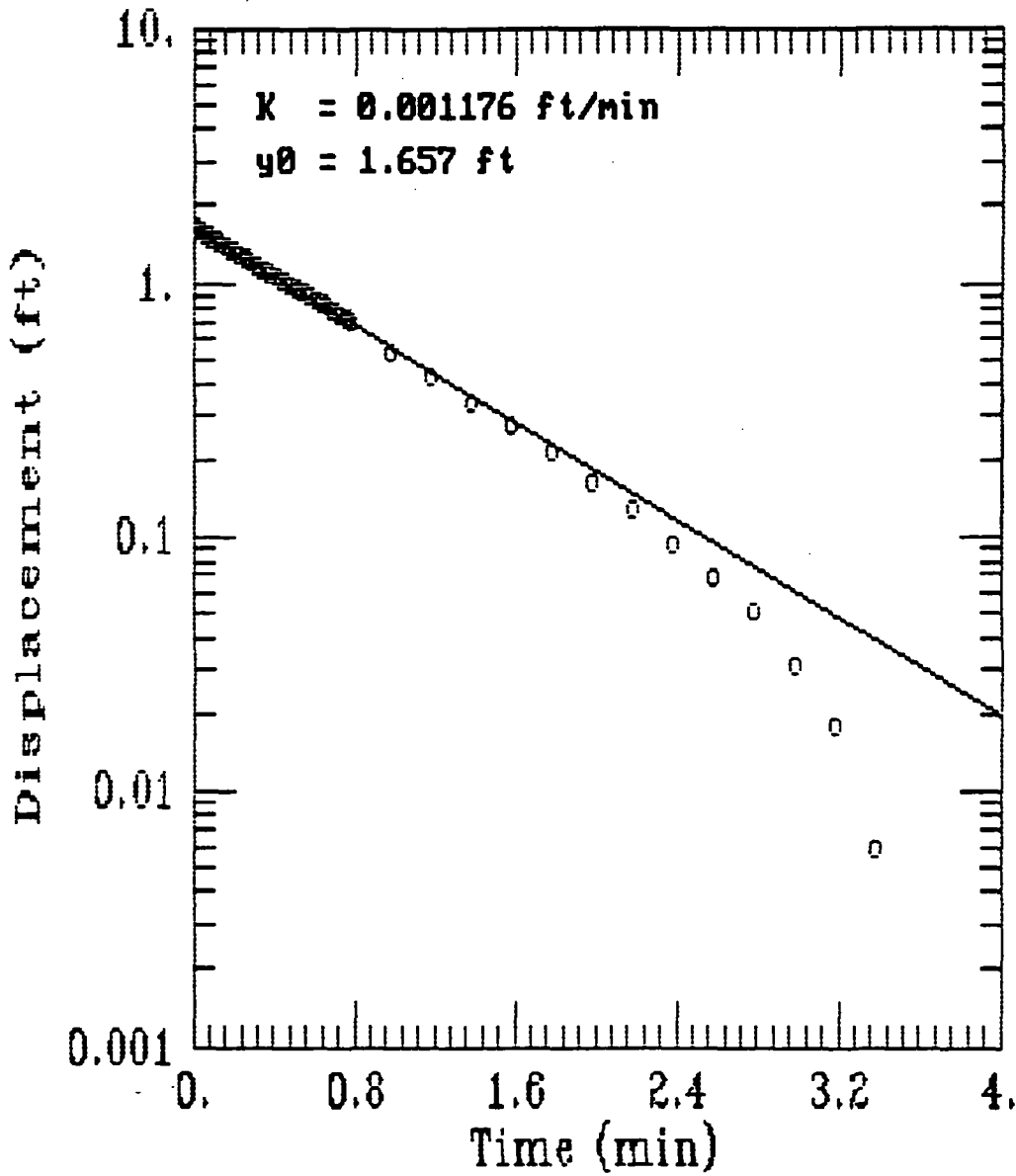
0.3333	2.720
0.3500	2.713
0.3666	2.707
0.3833	2.707
0.4000	2.707
0.4166	2.701
0.4333	2.701
0.4500	2.695
0.4666	2.695
0.4833	2.688
0.5000	2.688
0.5166	2.682
0.5333	2.682
0.5500	2.682
0.5666	2.682
0.5833	2.676
0.6000	2.676
0.6166	2.669
0.6333	2.669
0.6500	2.663
0.6666	2.663
0.6833	2.663
0.7000	2.657
0.7166	2.657
0.7333	2.657
0.7500	2.657
0.7666	2.650
0.7833	2.650
0.8000	2.644
0.8166	2.644
0.8333	2.644
0.8500	2.638
0.8666	2.644
0.8833	2.644
0.9000	2.644
0.9166	2.638
0.9333	2.638
0.9500	2.631
0.9666	2.631
0.9833	2.631
1.0000	2.625
1.2000	2.606
1.4000	2.587
1.6000	2.575
1.8000	2.556
2.0000	2.537
2.2000	2.518
2.4000	2.505
2.6000	2.493
2.8000	2.474
3.0000	2.455
3.2000	2.442
3.4000	2.430
3.6000	2.417
3.8000	2.398
4.0000	2.385
4.2000	2.373
4.4000	2.354
4.6000	2.342
4.8000	2.329
5.0000	2.316
5.2000	2.303
5.4000	2.291
5.6000	2.278

6.2000	2.234
6.4000	2.221
6.6000	2.215
6.8000	2.209
7.0000	2.196
7.2000	2.177
7.4000	2.171
7.6000	2.152
7.8000	2.146
8.0000	2.133
8.2000	2.120
8.4000	2.108
8.6000	2.095
8.8000	2.083
9.0000	2.070
9.2000	2.064
9.4000	2.045
9.6000	2.038
9.8000	2.026
10.0000	2.019
12.0000	1.906
14.0000	1.805
16.0000	1.710
18.0000	1.622
20.0000	1.540
22.0000	1.464
24.0000	1.388
26.0000	1.319
28.0000	1.256
30.0000	1.193
32.0000	1.136
34.0000	1.079
36.0000	1.029
38.0000	0.978
40.0000	0.934
42.0000	0.896
44.0000	0.852
46.0000	0.814
48.0000	0.782
50.0000	0.745
52.0000	0.719
54.0000	0.694
56.0000	0.662
58.0000	0.637
60.0000	0.612
62.0000	0.587
64.0000	0.568
66.0000	0.549
68.0000	0.530
70.0000	0.517
72.0000	0.505
74.0000	0.486
76.0000	0.473
78.0000	0.454
80.0000	0.441
82.0000	0.429
84.0000	0.416
86.0000	0.410
88.0000	0.397
90.0000	0.391
92.0000	0.385
94.0000	0.372
96.0000	0.366
98.0000	0.355

WELL CLUSTER: J
WELL ID: J5
SCREENED INTERVAL: 38-48

TEST METHOD: Bernier-Rice
SLUG IN/SLUG OUT: Slugs out
K-VALUE: 1.69 ft/day

J5-T2



START

0.2133	1.648
0.2166	1.648
0.2200	1.641
0.2233	1.635
0.2266	1.629
0.2300	1.623
0.2333	1.616
0.2366	1.610
0.2400	1.604
0.2433	1.597
0.2466	1.591
0.2500	1.585
0.2533	1.578
0.2566	1.578
0.2600	1.572
0.2633	1.566
0.2666	1.559
0.2700	1.553
0.2733	1.547
0.2766	1.540
0.2800	1.534
0.2833	1.534
0.2866	1.528

-- More --

0.2900	1.521
0.2933	1.515
0.2966	1.509
0.3000	1.503
0.3033	1.503
0.3066	1.496
0.3100	1.490
0.3133	1.484
0.3166	1.477
0.3200	1.471
0.3233	1.471
0.3266	1.465
0.3300	1.458
0.3333	1.452
0.3500	1.427
0.3666	1.401
0.3833	1.376
0.4000	1.351
0.4166	1.326
0.4333	1.300
0.4500	1.275
0.4666	1.250
0.4833	1.231

-- More --

0.5000	1.206
0.5166	1.187
0.5333	1.168
0.5500	1.143
0.5666	1.124
0.5833	1.105
0.6000	1.079
0.6166	1.060
0.6333	1.042

$\Delta H = 1.648$

$\Delta T = 3.5867$

Test:	J5 5ka out
File:	J5-TA.dat
Round:	KTEST
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	t = 0.2133 t = 3.80
Column 3:	
	t = _____ t = _____

0.7000	0.972
0.7166	0.953
0.7333	0.940
0.7500	0.922
0.7666	0.903
0.7833	0.890
0.8000	0.871
0.8166	0.858
0.8333	0.846
0.8500	0.827
0.8666	0.814

-- More --

0.8833	0.795
0.9000	0.783
0.9166	0.770
0.9333	0.757
0.9500	0.738
0.9666	0.726
0.9833	0.713
1.0000	0.701
1.2000	0.530
1.4000	0.423
1.6000	0.341
1.8000	0.271
2.0000	0.214
2.2000	0.164
2.4000	0.126
2.6000	0.094
2.8000	0.069
3.0000	0.050
3.2000	0.031
3.4000	0.018
3.6000	0.006
3.8000	0.000
4.0000	-0.012

-- More --

4.2000	-0.018
4.4000	-0.018
4.6000	-0.018
4.8000	-0.018
5.0000	-0.025
5.2000	-0.025
5.4000	-0.031
5.6000	-0.031
5.8000	-0.031
6.0000	-0.031
6.2000	-0.037
6.4000	-0.037
6.6000	-0.044
6.8000	-0.037
7.0000	-0.037
7.2000	-0.037
7.4000	-0.037
7.6000	-0.037
7.8000	-0.037
8.0000	-0.037
8.2000	-0.044
8.4000	-0.044
8.6000	-0.037

— END @ 3.387

7.4000	-0.037
7.6000	-0.037
7.8000	-0.037
8.0000	-0.037
8.2000	-0.044
8.4000	-0.044
8.6000	-0.037
-- More --	

8.8000	-0.044
9.0000	-0.044
9.2000	-0.044
9.4000	-0.044
9.6000	-0.050
9.8000	-0.050
10.0000	-0.044
12.0000	0.000
14.0000	0.006
16.0000	-0.075
18.0000	-0.075
20.0000	-0.082

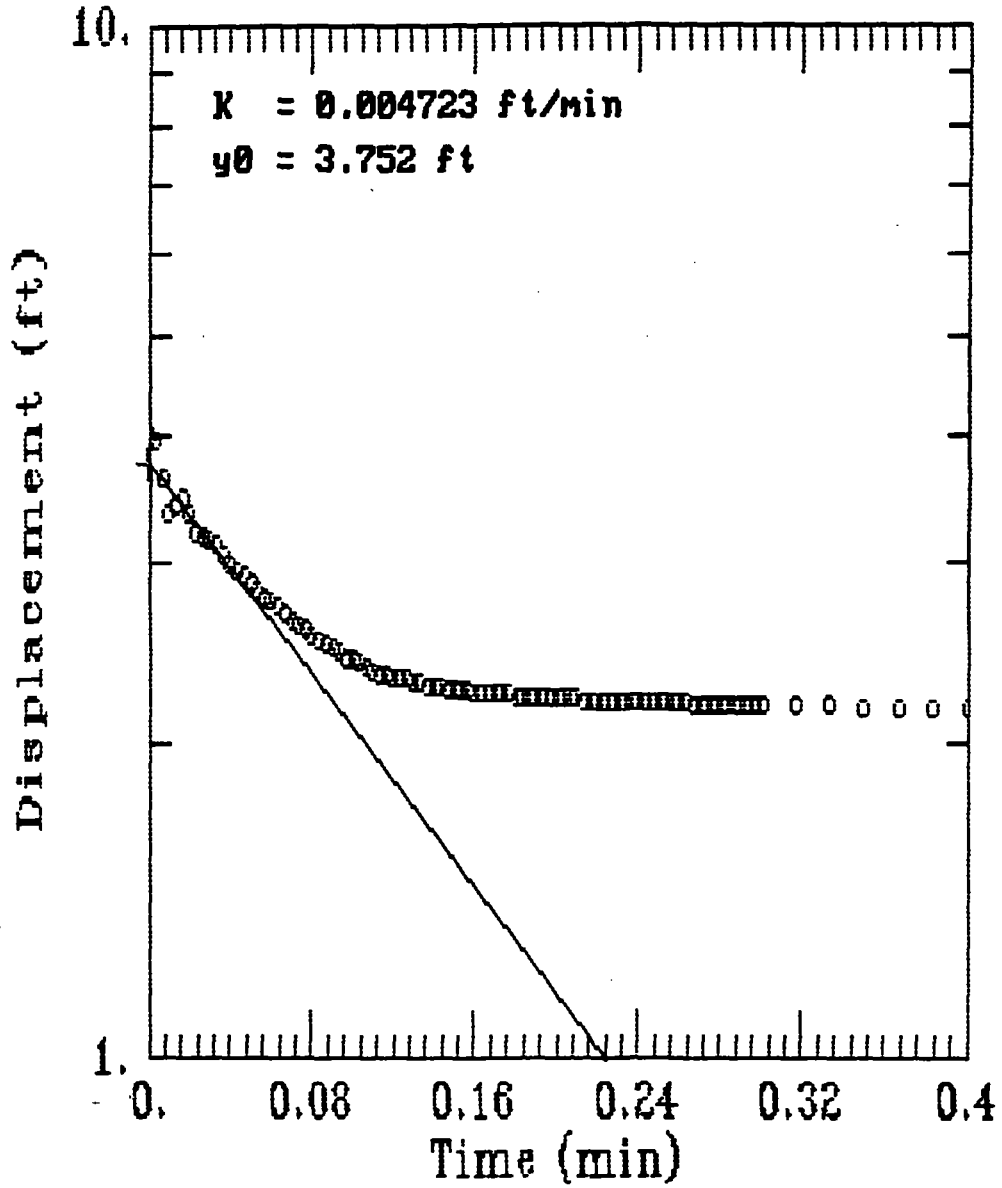
7

Type 'exit' to return to AQTESOLV.
C:\KTEST>

WELL CLUSTER: K
WELL ID: K1
SCREENED INTERVAL: 7-17

TEST METHOD: Bauer Pipe
SLUG IN/SLUG OUT: slug out
K-VALUE: 6.8 ft/day

K1-T2



(5)

KT-T2-dat

0.0000	1.907
0.0033	1.920
0.0066	1.977
0.0100	2.305
0.0133	2.924
0.0166	3.505
0.0200	3.903
0.0233	3.998
0.0266	3.821
0.0300	3.556
0.0333	3.966
0.0366	3.954
0.0400	3.651
0.0433	3.354
0.0466	3.411
0.0500	3.474
0.0533	3.373
0.0566	3.234
0.0600	3.183
0.0633	3.177
0.0666	3.145
0.0700	3.057
0.0733	2.994
0.0766	2.950
0.0800	2.931
0.0833	2.886
0.0866	2.823
0.0900	2.792
0.0933	2.760
0.0966	2.728
0.1000	2.678
0.1033	2.646
0.1066	2.621
0.1100	2.589
0.1133	2.552
0.1166	2.526
0.1200	2.501
0.1233	2.476
0.1266	2.457
0.1300	2.432
0.1333	2.413
0.1366	2.394
0.1400	2.381
0.1433	2.368
0.1466	2.349
0.1500	2.337
0.1533	2.330
0.1566	2.318
0.1600	2.312
0.1633	2.299
0.1666	2.293
0.1700	2.286
0.1733	2.280
0.1766	2.274
0.1800	2.267
0.1833	2.261
0.1866	2.261
0.1900	2.255
0.1933	2.248
0.1966	2.248

$\mu = 1.535$
 $\Delta t = 2.362$

Test:	KI Slug out
File:	KI-T2.dat
Round:	KTEST
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	$t_b = 0.0333$ $t_r = 7.40$
Column 3:	
	$t_b = \underline{\hspace{2cm}}$ $t_r = \underline{\hspace{2cm}}$

0.2000	2.242
0.2033	2.242
0.2066	2.242
0.2100	2.236
0.2133	2.229
0.2166	2.229
0.2200	2.229
0.2233	2.229
0.2266	2.223
0.2300	2.223
0.2333	2.223
0.2366	2.217
0.2400	2.217
0.2433	2.217
0.2466	2.210
0.2500	2.210
0.2533	2.210
0.2566	2.210
0.2600	2.204
0.2633	2.204
0.2666	2.204
0.2700	2.204
0.2733	2.198
0.2766	2.198
0.2800	2.198
0.2833	2.198
0.2866	2.198
0.2900	2.198
0.2933	2.198
0.2966	2.198
0.3000	2.192
0.3033	2.192
0.3066	2.192
0.3100	2.192
0.3133	2.192
0.3166	2.185
0.3200	2.185
0.3233	2.185
0.3266	2.185
0.3300	2.185
0.3333	2.185
0.3500	2.179
0.3666	2.179
0.3833	2.173
0.4000	2.173
0.4166	2.166
0.4333	2.166
0.4500	2.166
0.4666	2.160
0.4833	2.160
0.5000	2.160
0.5166	2.154
0.5333	2.154
0.5500	2.154
0.5666	2.154
0.5833	2.154
0.6000	2.147
0.6166	2.147
0.6333	2.147
0.6500	2.147

0.6666	2.147
0.6833	2.147
0.7000	2.141
0.7166	2.141
0.7333	2.141
0.7500	2.141
0.7666	2.141
0.7833	2.141
0.8000	2.141
0.8166	2.141
0.8333	2.135
0.8500	2.135
0.8666	2.135
0.8833	2.135
0.9000	2.135
0.9166	2.135
0.9333	2.135
0.9500	2.135
0.9666	2.128
0.9833	2.128
1.0000	2.128
1.2000	2.122
1.4000	2.122
1.6000	2.116
1.8000	2.109
2.0000	2.109
2.2000	2.109
2.4000	2.103
2.6000	2.103
2.8000	2.103
3.0000	2.103
3.2000	2.103
3.4000	2.097
3.6000	2.097
3.8000	2.097
4.0000	2.097
4.2000	2.090
4.4000	2.097
4.6000	2.090
4.8000	2.090
5.0000	2.090
5.2000	2.090
5.4000	2.090
5.6000	2.090
5.8000	2.090
6.0000	2.084
6.2000	2.084
6.4000	2.084
6.6000	2.084
6.8000	2.084
7.0000	2.084
7.2000	2.084
7.4000	2.078
7.6000	2.078
7.8000	2.078
8.0000	2.078
8.2000	2.078
8.4000	2.078
8.6000	2.078
8.8000	2.078

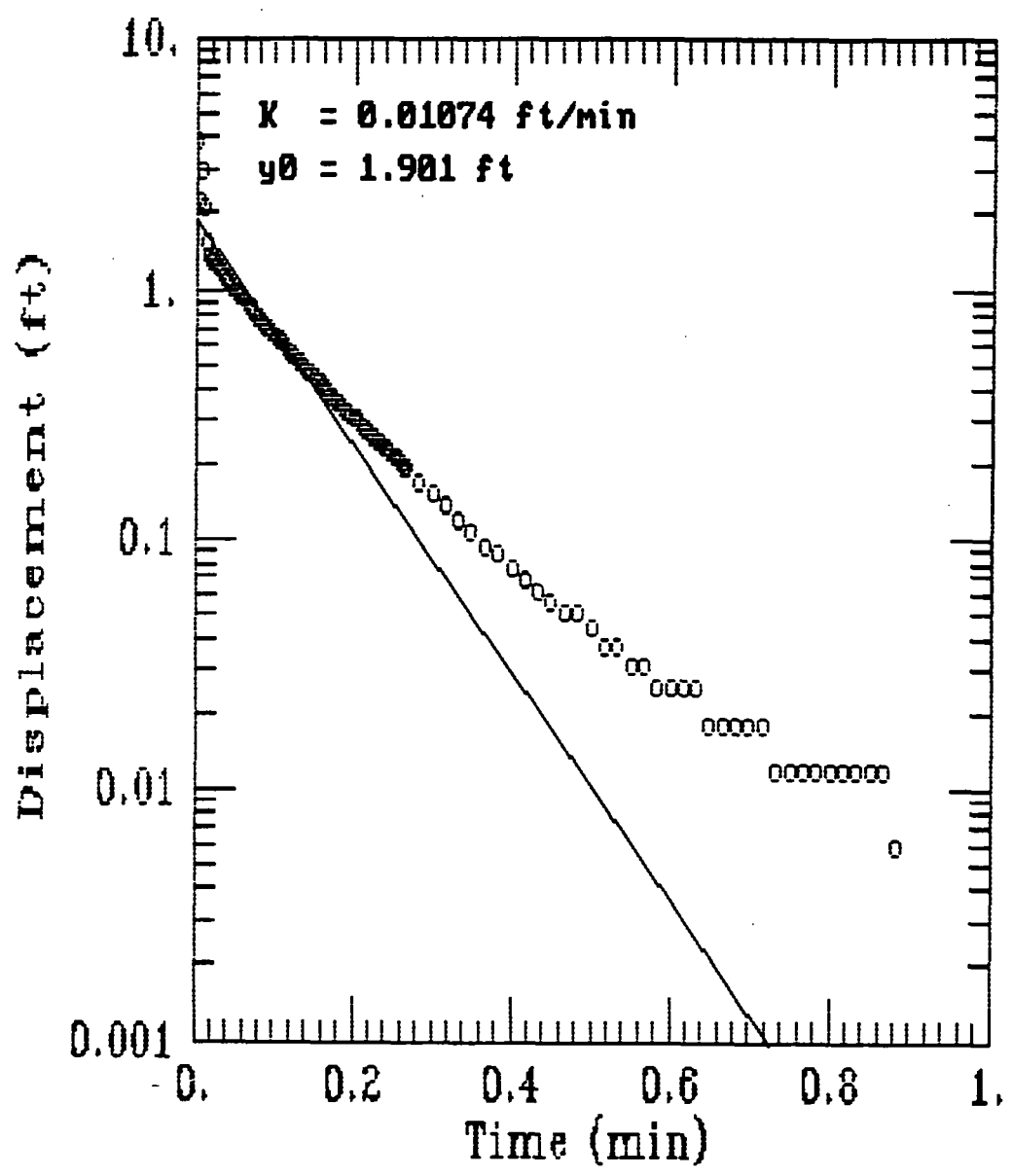
© 7.267

9.0000	2.078
9.2000	2.078
9.4000	2.071
9.6000	2.071
9.8000	2.071
10.0000	2.071
12.0000	2.065
14.0000	2.065

WELL CLUSTER: K
WELL ID: K2
SCREENED INTERVAL: 20.5-30.5

TEST METHOD: Barnes Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 15.5 ft/day

K2-T2



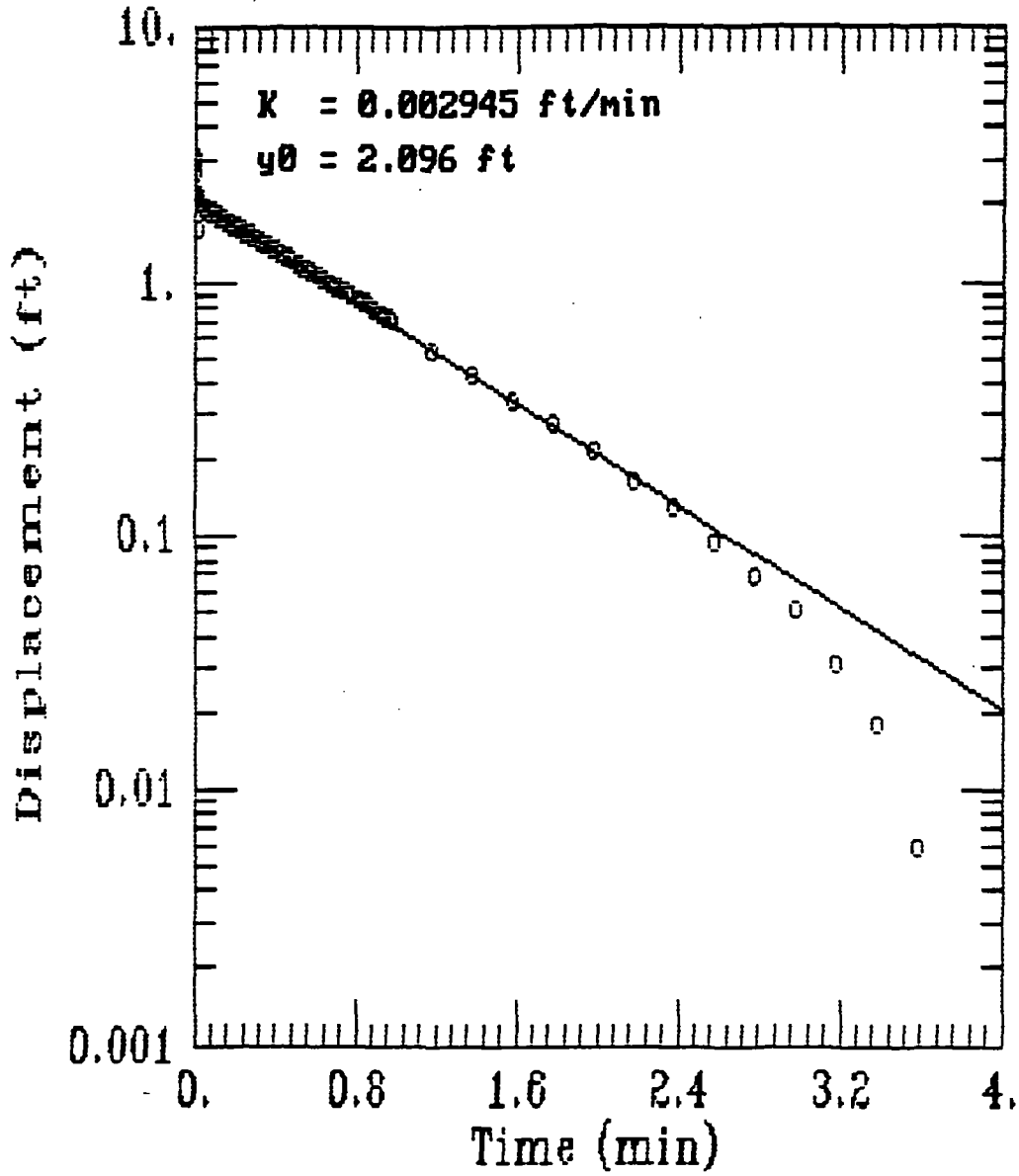
0.2200	0.433
0.2233	0.423
0.2266	0.410
0.2300	0.404
0.2333	0.391
0.2366	0.379
0.2400	0.372
0.2433	0.366
0.2466	0.353
0.2500	0.347
0.2533	0.341
0.2566	0.328
0.2600	0.322
0.2633	0.315
0.2666	0.309
0.2700	0.303
0.2733	0.290
0.2766	0.284
0.2800	0.277
0.2833	0.271
0.2866	0.265
0.2900	0.259
0.2933	0.252
0.2966	0.246
0.3000	0.246
0.3033	0.240
0.3066	0.233
0.3100	0.227
0.3133	0.221
0.3166	0.214
0.3200	0.214
0.3233	0.208
0.3266	0.202
0.3300	0.195
0.3333	0.195
0.3500	0.170
0.3666	0.151
0.3833	0.138
0.4000	0.120
0.4166	0.107
0.4333	0.094
0.4500	0.088
0.4666	0.075
0.4833	0.069
0.5000	0.063
0.5166	0.056
0.5333	0.050
0.5500	0.050
0.5666	0.044
0.5833	0.037
0.6000	0.037
0.6166	0.031
0.6333	0.031
0.6500	0.025
0.6666	0.025
0.6833	0.025
0.7000	0.025
0.7166	0.018
0.7333	0.018
0.7500	0.018
0.7666	0.018
0.7833	0.018
0.8000	0.012
0.8166	0.012

0.8833	0.012
0.9000	0.012
0.9166	0.012
0.9333	0.012
0.9500	0.006
0.9666	0.006
0.9833	0.006
1.0000	0.006
1.2000	0.006
1.4000	0.000
1.6000	0.000
1.8000	0.000
2.0000	0.000
2.2000	0.000
2.4000	-0.006
2.6000	0.000
2.8000	0.000
3.0000	0.000
3.2000	0.000
3.4000	0.000
3.6000	0.000
3.8000	-0.006
4.0000	0.000
4.2000	0.000
4.4000	-0.006
4.6000	0.000
4.8000	0.000
5.0000	-0.006
5.2000	0.000
5.4000	0.000
5.6000	0.000
5.8000	0.000
6.0000	0.000
6.2000	0.000
6.4000	0.000
6.6000	0.000
6.8000	0.000
7.0000	0.000
7.2000	-0.006
7.4000	0.006
7.6000	0.006
7.8000	0.006
8.0000	0.000
8.2000	0.000
8.4000	0.006
8.6000	-0.100
8.8000	-0.075
9.0000	-0.075
9.2000	-0.075
9.4000	-0.075
9.6000	-0.075
9.8000	-0.075
10.0000	-0.075
12.0000	-0.075
14.0000	-0.075
16.0000	-0.075
18.0000	-0.075
20.0000	-0.082

WELL CLUSTER: K
WELL ID: K3
SCREENED INTERVAL: 48.25-52.25

TEST METHOD: Banner Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 4.24 ft/day

K3-T2



0.2000	1.673
0.2033	1.667
0.2066	1.660
0.2100	1.654
0.2133	1.648
0.2166	1.648
0.2200	1.641
0.2233	1.635
0.2266	1.629
0.2300	1.623
0.2333	1.616
0.2366	1.610
0.2400	1.604
0.2433	1.597
0.2466	1.591
0.2500	1.585
0.2533	1.578
0.2566	1.578
0.2600	1.572
0.2633	1.566
0.2666	1.559
0.2700	1.553
0.2733	1.547
0.2766	1.540
0.2800	1.534
0.2833	1.534
0.2866	1.528
0.2900	1.521
0.2933	1.515
0.2966	1.509
0.3000	1.503
0.3033	1.503
0.3066	1.496
0.3100	1.490
0.3133	1.484
0.3166	1.477
0.3200	1.471
0.3233	1.471
0.3266	1.465
0.3300	1.458
0.3333	1.452
0.3500	1.427
0.3666	1.401
0.3833	1.376
0.4000	1.351
0.4166	1.326
0.4333	1.300
0.4500	1.275
0.4666	1.250
0.4833	1.231
0.5000	1.206
0.5166	1.187
0.5333	1.168
0.5500	1.143
0.5666	1.124
0.5833	1.105
0.6000	1.079
0.6166	1.060
0.6333	1.042
0.6500	1.023

0.6666	1.004
0.6833	0.991
0.7000	0.972
0.7166	0.953
0.7333	0.940
0.7500	0.922
0.7666	0.903
0.7833	0.890
0.8000	0.871
0.8166	0.858
0.8333	0.846
0.8500	0.827
0.8666	0.814
0.8833	0.795
0.9000	0.783
0.9166	0.770
0.9333	0.757
0.9500	0.738
0.9666	0.726
0.9833	0.713
1.0000	0.701
1.2000	0.530
1.4000	0.423
1.6000	0.341
1.8000	0.271
2.0000	0.214
2.2000	0.164
2.4000	0.126
2.6000	0.094
2.8000	0.069
3.0000	0.050
3.2000	0.031
3.4000	0.018
3.6000	0.006
3.8000	0.000
4.0000	-0.012
4.2000	-0.018
4.4000	-0.018
4.6000	-0.018
4.8000	-0.018
5.0000	-0.025
5.2000	-0.025
5.4000	-0.031
5.6000	-0.031
5.8000	-0.031
6.0000	-0.031
6.2000	-0.037
6.4000	-0.037
6.6000	-0.044
6.8000	-0.037
7.0000	-0.037
7.2000	-0.037
7.4000	-0.037
7.6000	-0.037
7.8000	-0.037
8.0000	-0.037
8.2000	-0.044
8.4000	-0.044
8.6000	-0.037
8.8000	-0.044

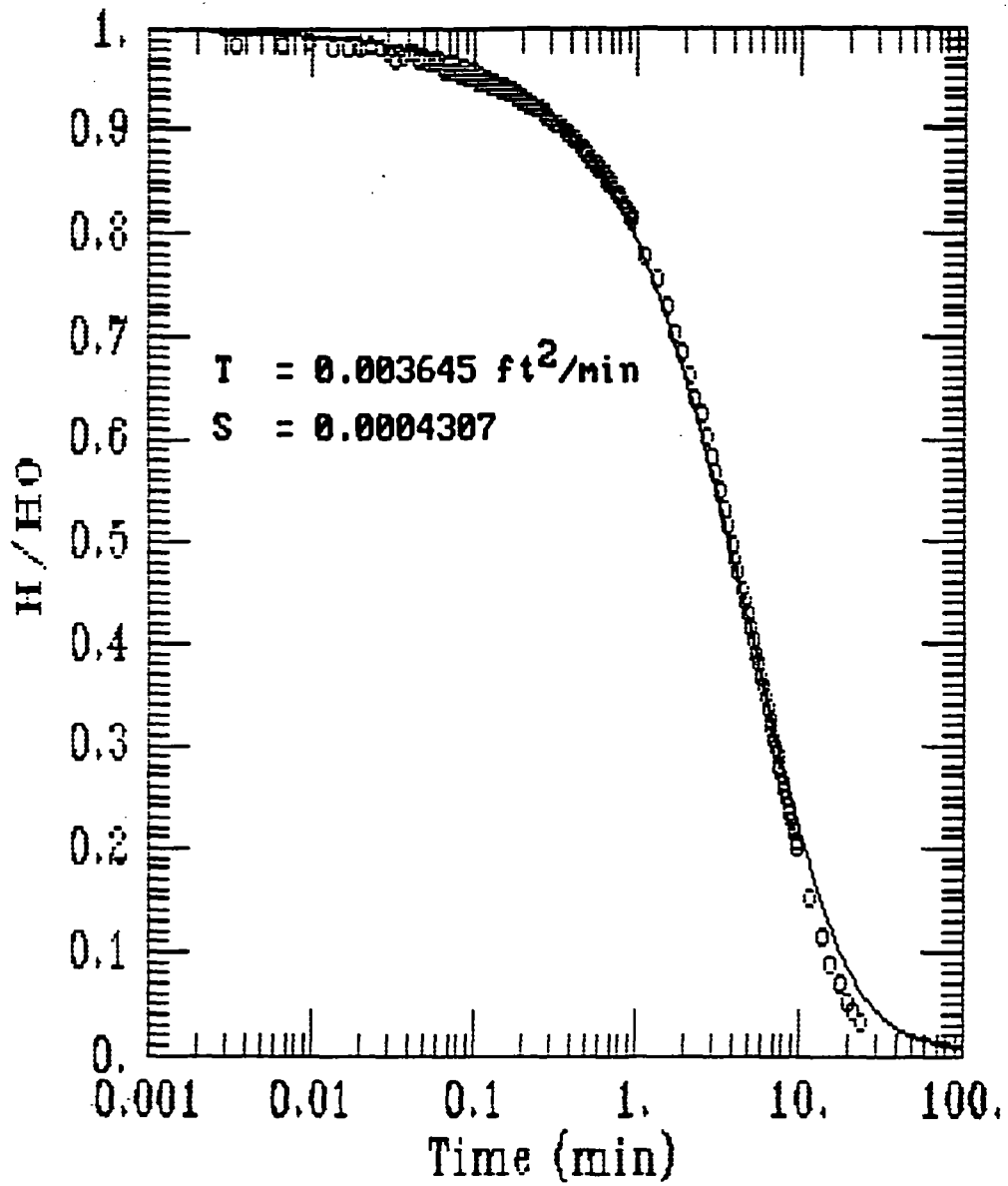
@ 3.523

9.0000	-0.044
9.2000	-0.044
9.4000	-0.044
9.6000	-0.050
9.8000	-0.050
10.0000	-0.044

WELL CLUSTER: K
WELL ID: K4
SCREENED INTERVAL: 57-67

TEST METHOD: Cooper et al.
SLUG IN/SLUG OUT: Slug out
K-VALUE: 0.287 ft/day

K4-T2



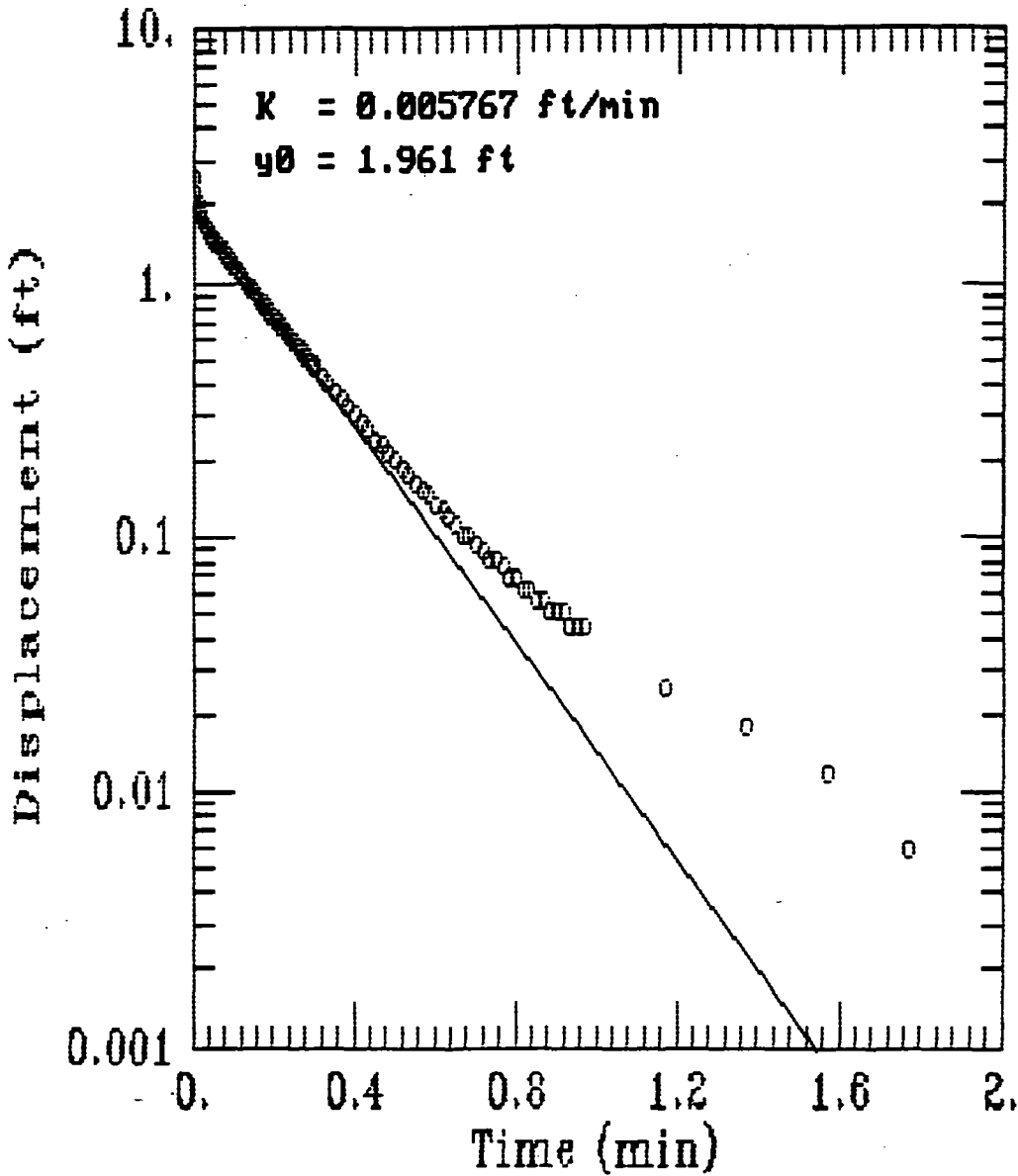
0.2233	2.614
0.2266	2.608
0.2300	2.608
0.2333	2.608
0.2366	2.608
0.2400	2.601
0.2433	2.601
0.2466	2.601
0.2500	2.595
0.2533	2.595
0.2566	2.595
0.2600	2.589
0.2633	2.595
0.2666	2.589
0.2700	2.589
0.2733	2.582
0.2766	2.582
0.2800	2.582
0.2833	2.582
0.2866	2.576
0.2900	2.576
0.2933	2.576
0.2966	2.576
0.3000	2.576
0.3033	2.570
0.3066	2.570
0.3100	2.570
0.3133	2.563
0.3166	2.563
0.3200	2.563
0.3233	2.563
0.3266	2.557
0.3300	2.557
0.3333	2.557
0.3500	2.544
0.3666	2.538
0.3833	2.532
0.4000	2.525
0.4166	2.513
0.4333	2.507
0.4500	2.500
0.4666	2.494
0.4833	2.488
0.5000	2.475
0.5166	2.469
0.5333	2.462
0.5500	2.456
0.5666	2.443
0.5833	2.437
0.6000	2.431
0.6166	2.424
0.6333	2.418
0.6500	2.412
0.6666	2.405
0.6833	2.393
0.7000	2.393
0.7166	2.380
0.7333	2.380
0.7500	2.374
0.7666	2.361
0.7833	2.355
0.8000	2.349
0.8166	2.342

0.8666	2.323
0.8833	2.317
0.9000	2.311
0.9166	2.298
0.9333	2.298
0.9500	2.292
0.9666	2.286
0.9833	2.279
1.0000	2.273
1.2000	2.178
1.4000	2.109
1.6000	2.039
1.8000	1.970
2.0000	1.913
2.2000	1.850
2.4000	1.793
2.6000	1.742
2.8000	1.686
3.0000	1.635
3.2000	1.585
3.4000	1.534
3.6000	1.484
3.8000	1.439
4.0000	1.395
4.2000	1.345
4.4000	1.313
4.6000	1.269
4.8000	1.231
5.0000	1.199
5.2000	1.155
5.4000	1.124
5.6000	1.086
5.8000	1.060
6.0000	1.023
6.2000	0.997
6.4000	0.966
6.6000	0.934
6.8000	0.909
7.0000	0.884
7.2000	0.858
7.4000	0.833
7.6000	0.808
7.8000	0.783
8.0000	0.764
8.2000	0.738
8.4000	0.719
8.6000	0.700
8.8000	0.675
9.0000	0.656
9.2000	0.637
9.4000	0.618
9.6000	0.599
9.8000	0.580
10.0000	0.562
12.0000	0.423
14.0000	0.322
16.0000	0.246
18.0000	0.195
20.0000	0.145
22.0000	0.119
24.0000	0.094

WELL CLUSTER: K
WELL ID: K5
SCREENED INTERVAL: 34-44

TEST METHOD: Bower Rice
SLUG IN/SLUG OUT: Slug out
K-VALUE: 2.30 ft/day

K5-T2



0.0000	0.000
0.0033	0.713
0.0066	1.206
0.0100	1.338
0.0133	2.153
0.0166	2.008
0.0200	2.393
0.0233	1.705
0.0266	2.216
0.0300	<u>2.557</u>
0.0333	2.222
0.0366	1.837
0.0400	1.995
0.0433	2.020
0.0466	1.856
0.0500	1.812
0.0533	1.755
0.0566	1.717
0.0600	1.686
0.0633	1.660
0.0666	1.622
0.0700	1.591
0.0733	1.559
0.0766	1.503
0.0800	1.439
0.0833	1.490
0.0866	1.458
0.0900	1.433
0.0933	1.408
0.0966	1.383
0.1000	1.364
0.1033	1.338
0.1066	1.319
0.1100	1.294
0.1133	1.275
0.1166	1.250
0.1200	1.231
0.1233	1.212
0.1266	1.187
0.1300	1.168
0.1333	1.149
0.1366	1.130
0.1400	1.111
0.1433	1.098
0.1466	1.079
0.1500	1.060
0.1533	1.042
0.1566	1.029
0.1600	1.010
0.1633	0.997
0.1666	0.978
0.1700	0.966
0.1733	0.953
0.1766	0.934
0.1800	0.922
0.1833	0.909
0.1866	0.890
0.1900	0.877
0.1933	0.865
0.1966	0.852

(17)

K5-T2.dat

$\Delta H = 2.557$

$\Delta E = 1.77$

Test:	<u>K5 Shg wt</u>
File:	<u>K5-T2.dat</u>
Round:	<u>KTEST</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head (ft)</u>
	$t_b = \underline{0.0300} \quad t_c = \underline{1.80}$
Column 3:	_____
	$t_b = \underline{\quad\quad\quad} \quad t_c = \underline{\quad\quad\quad}$

0.2000	0.839
0.2033	0.827
0.2066	0.814
0.2100	0.802
0.2133	0.789
0.2166	0.776
0.2200	0.764
0.2233	0.757
0.2266	0.745
0.2300	0.732
0.2333	0.719
0.2366	0.713
0.2400	0.701
0.2433	0.688
0.2466	0.682
0.2500	0.669
0.2533	0.663
0.2566	0.650
0.2600	0.644
0.2633	0.631
0.2666	0.625
0.2700	0.612
0.2733	0.606
0.2766	0.593
0.2800	0.587
0.2833	0.580
0.2866	0.568
0.2900	0.562
0.2933	0.555
0.2966	0.549
0.3000	0.543
0.3033	0.530
0.3066	0.524
0.3100	0.517
0.3133	0.511
0.3166	0.505
0.3200	0.492
0.3233	0.492
0.3266	0.479
0.3300	0.473
0.3333	0.467
0.3500	0.435
0.3666	0.404
0.3833	0.378
0.4000	0.347
0.4166	0.322
0.4333	0.303
0.4500	0.284
0.4666	0.265
0.4833	0.239
0.5000	0.227
0.5166	0.214
0.5333	0.202
0.5500	0.189
0.5666	0.176
0.5833	0.164
0.6000	0.151
0.6166	0.145
0.6333	0.132
0.6500	0.126

0.6666	0.119
0.6833	0.113
0.7000	0.101
0.7166	0.101
0.7333	0.094
0.7500	0.088
0.7666	0.082
0.7833	0.082
0.8000	0.075
0.8166	0.069
0.8333	0.069
0.8500	0.063
0.8666	0.063
0.8833	0.056
0.9000	0.056
0.9166	0.050
0.9333	0.050
0.9500	0.050
0.9666	0.044
0.9833	0.044
1.0000	0.044
1.2000	0.025
1.4000	0.018
1.6000	0.012
1.8000	0.006
2.0000	0.006
2.2000	0.006
2.4000	0.006
2.6000	0.006
2.8000	0.006
3.0000	0.006
3.2000	0.006
3.4000	0.006
3.6000	0.000
3.8000	0.000
4.0000	0.000
4.2000	0.000
4.4000	0.006
4.6000	0.006
4.8000	0.000
5.0000	0.000
5.2000	0.000
5.4000	0.000
5.6000	-0.006
5.8000	-0.006
6.0000	0.000
6.2000	0.000
6.4000	0.006
6.6000	-0.006
6.8000	0.000
7.0000	0.000
7.2000	-0.006
7.4000	-0.006
7.6000	0.000
7.8000	0.000
8.0000	0.000
8.2000	0.000
8.4000	0.000
8.6000	0.000
8.8000	0.000

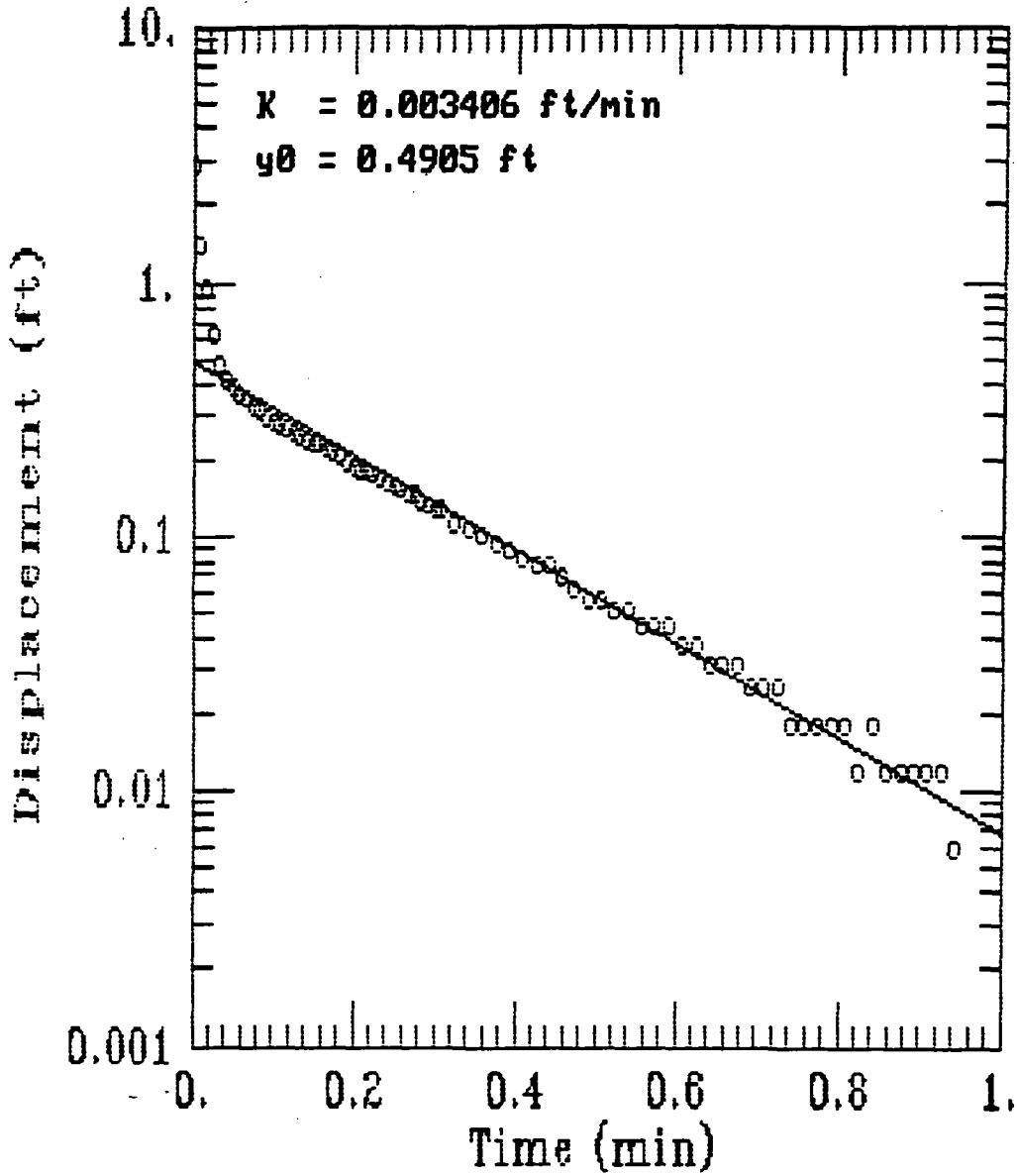
e 1.77

9.0000	0.000
9.2000	0.000
9.4000	0.000
9.6000	-0.006
9.8000	-0.006
10.0000	0.000
12.0000	0.000
14.0000	0.006

WELL CLUSTER: L
WELL ID: L1
SCREENED INTERVAL: 3-13

TEST METHOD: Bauer Pipe
SLUG IN/SLUG OUT: Slug out
K-VALUE: 4.90 ft/day

L1-T2



SE2000
 Environmental Logger
 08/23 09:38

L1-T2

PZN ✓

Unit# 22 Test 15

 Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. 204363

Reference 0.000
 SG 1.000
 Linearity 0.152
 Scale factor 19.970
 Offset 0.061
 Delay mSEC 50.000

Step 0 08/22 12:44:11

 Elapsed Time INPUT 1

0.0000	-0.006
0.0083	-0.006
0.0166	0.000
0.0250	2.819 ✓
0.0333	1.394
0.0416	0.959
0.0500	0.637
0.0583	0.473
0.0666	0.416
0.0750	0.384
0.0833	0.365
0.0916	0.347
0.1000	0.328
0.1083	0.315
0.1166	0.296
0.1250	0.283
0.1333	0.271
0.1416	0.265
0.1500	0.252
0.1583	0.246
0.1666	0.239
0.1750	0.233
0.1833	0.227
0.1916	-0.220
0.2000	0.214
0.2083	0.208
0.2166	0.195
0.2250	0.189
0.2333	0.183
0.2416	0.183
0.2500	0.176
0.2583	0.170
0.2666	0.164
0.2750	0.157
0.2833	0.151
0.2916	0.145
0.3000	0.145
0.3083	0.140

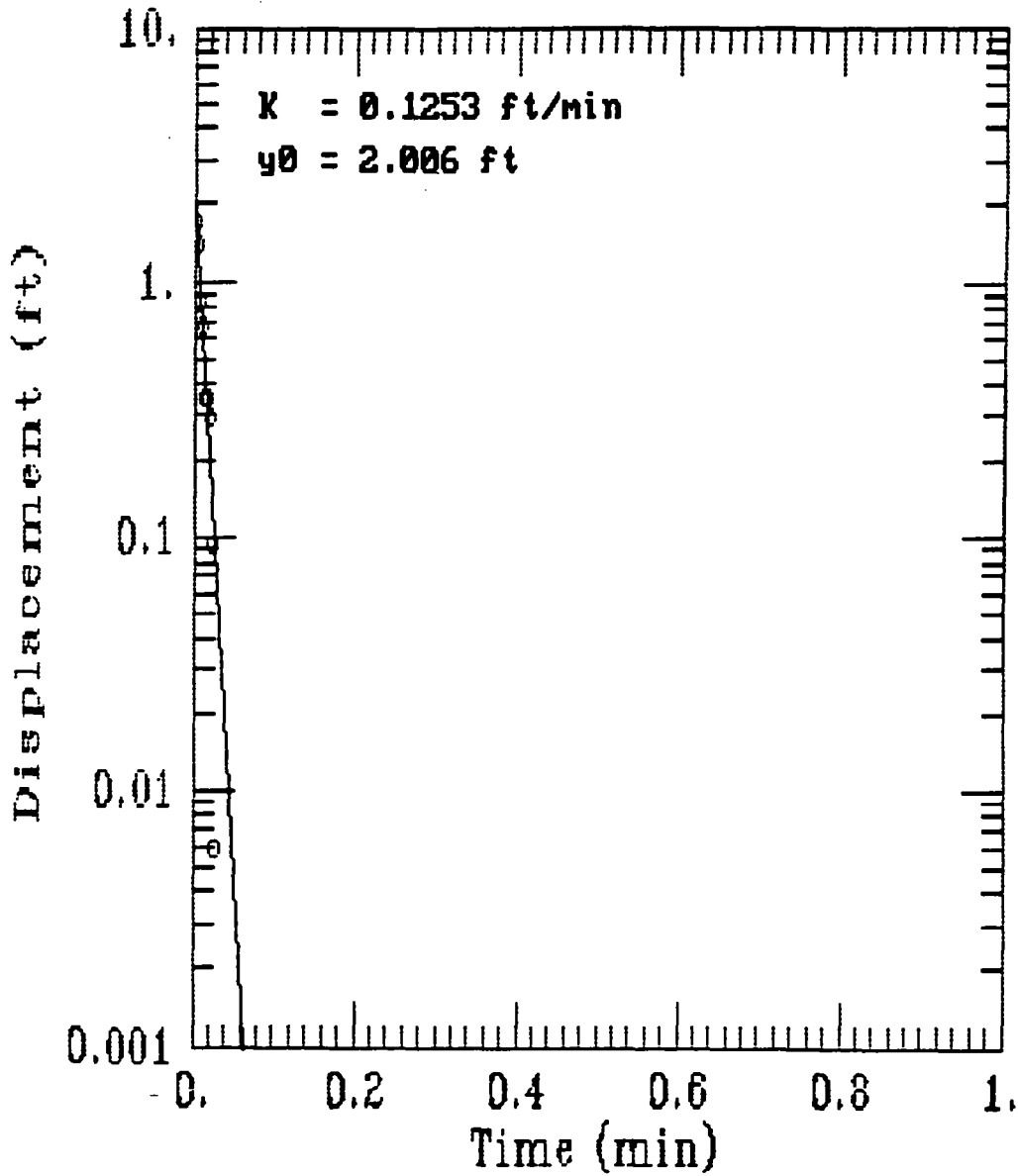
Test:	L1 Slvg out
File:	L1-T2
Round:	KTEST3
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	t ₀ = 0.0250 t ₁ = 0.9666
Column 3:	
	t ₀ = _____ t ₁ = _____

0.3333	0.126
0.3500	0.113
0.3666	0.107
0.3833	0.100
0.4000	0.094
0.4166	0.088
0.4333	0.082
0.4500	0.075
0.4666	0.075
0.4833	0.069
0.5000	0.063
0.5166	0.056
0.5333	0.056
0.5500	0.050
0.5666	0.050
0.5833	0.044
0.6000	0.044
0.6166	0.044
0.6333	0.037
0.6500	0.037
0.6666	0.031
0.6833	0.031
0.7000	0.031
0.7166	0.025
0.7333	0.025
0.7500	0.025
0.7666	0.018
0.7833	0.018
0.8000	0.018
0.8166	0.018
0.8333	0.018
0.8500	0.012
0.8666	0.018
0.8833	0.012
0.9000	0.012
0.9166	0.012
0.9333	0.012
0.9500	0.012
0.9666	0.006 ✓
0.9833	0.006
1.0000	0.006
1.2000	0.000
1.4000	0.000
1.6000	0.000
1.8000	-0.006
2.0000	-0.006
2.2000	0.000
2.4000	-0.006
2.6000	-0.006

WELL CLUSTER: L
WELL ID: L2
SCREENED INTERVAL: 19.5-29.5

TEST METHOD: Bowser Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 180 ft/day

L2-T2



0.2200	0.025
0.2233	0.025
0.2266	0.025
0.2300	0.018
0.2333	0.012
0.2366	0.012
0.2400	0.012
0.2433	0.006
0.2466	0.006
0.2500	0.006
0.2533	0.006
0.2566	0.006
0.2600	0.012
0.2633	0.012
0.2666	0.012
0.2700	0.012
0.2733	0.018
0.2766	0.018
0.2800	0.018
0.2833	0.018
0.2866	0.018
0.2900	0.025
0.2933	0.025
0.2966	0.025
0.3000	0.018
0.3033	0.018
0.3066	0.018
0.3100	0.025
0.3133	0.018
0.3166	0.018
0.3200	0.018
0.3233	0.018
0.3266	0.018
0.3300	0.018
0.3333	0.018
0.3500	0.012
0.3666	0.018
0.3833	0.018
0.4000	0.018
0.4166	0.018
0.4333	0.018
0.4500	0.012
0.4666	0.018
0.4833	0.012
0.5000	0.012
0.5166	0.012
0.5333	0.012
0.5500	0.012
0.5666	0.012
0.5833	0.012
0.6000	0.012
0.6166	0.012
0.6333	0.012
0.6500	0.012
0.6666	0.012
0.6833	0.012
0.7000	0.012
0.7166	0.012
0.7333	0.012
0.7500	0.012
0.7666	0.012
0.7833	0.012
0.8000	0.012
0.8166	0.012

0.8666	0.012
0.8833	0.006
0.9000	0.012
0.9166	0.012
0.9333	0.012
0.9500	0.012
0.9666	0.006
0.9833	0.012
1.0000	0.012
1.2000	0.012
1.4000	0.006
1.6000	0.012
1.8000	0.012
2.0000	0.006
2.2000	0.006
2.4000	0.012
2.6000	0.012
2.8000	0.012
3.0000	0.006
3.2000	0.006
3.4000	0.006
3.6000	0.006
3.8000	0.006
4.0000	0.006
4.2000	0.006
4.4000	0.006
4.6000	0.006
4.8000	0.006
5.0000	0.006
5.2000	0.000
5.4000	0.006
5.6000	0.006
5.8000	0.006
6.0000	0.006
6.2000	0.006
6.4000	0.006
6.6000	0.006
6.8000	0.006
7.0000	0.006
7.2000	0.012
7.4000	0.012
7.6000	0.012
7.8000	0.012
8.0000	0.006
8.2000	0.006
8.4000	0.006
8.6000	0.006
8.8000	0.012
9.0000	0.006
9.2000	0.006
9.4000	0.006
9.6000	0.006
9.8000	0.006
10.0000	0.012

WELL CLUSTER: L

TEST METHOD: Bowyer Rice

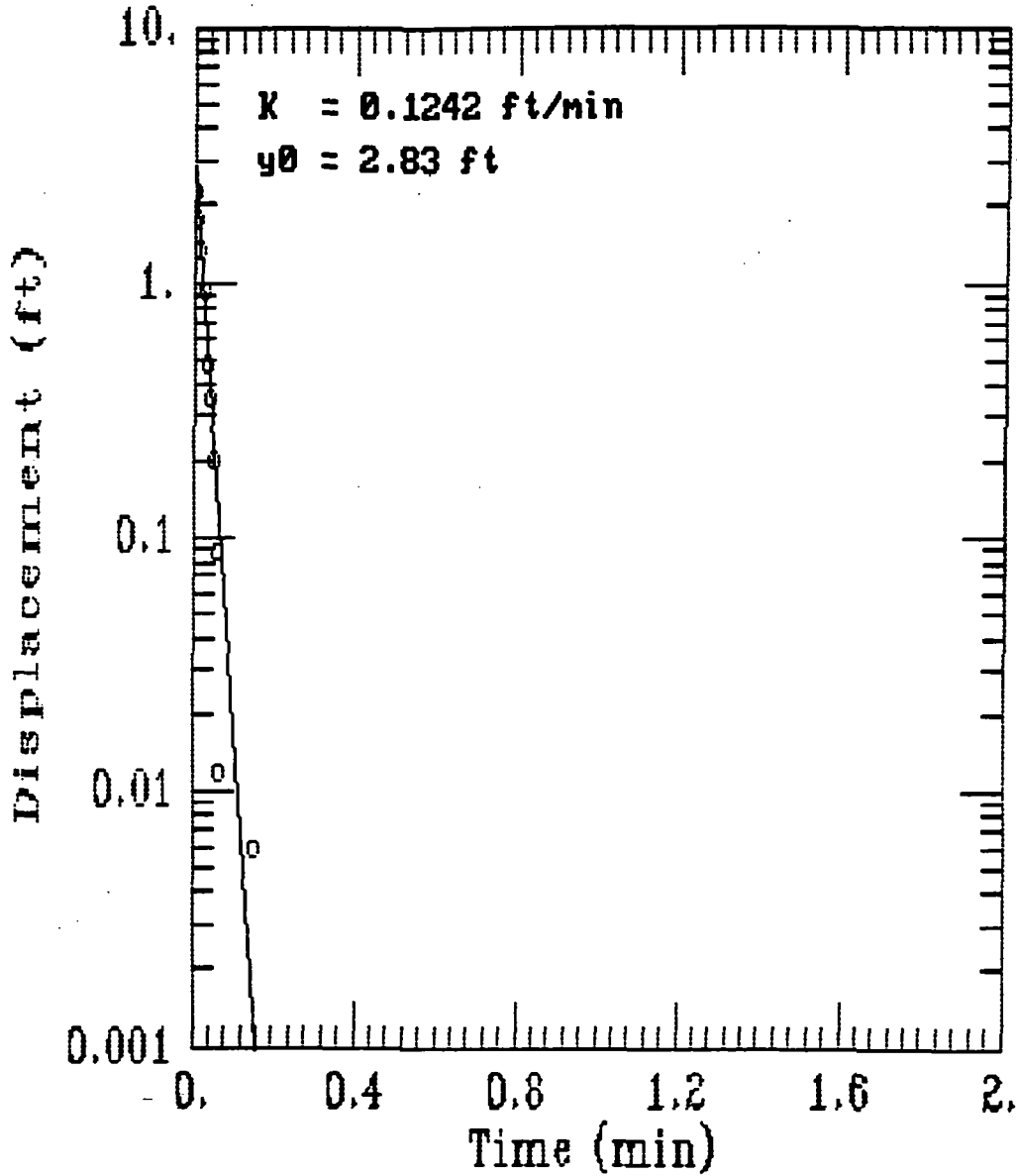
WELL ID: L3-1

SLUG IN/SLUG OUT: Slug out

SCREENED INTERVAL: 41.25-46.25

K-VALUE: 179. A/Day

L31-T2



SE2000
 Environmental Logger
 08/23 08:10

Unit# 22 Test 1

L31-T2

PRN ✓

 Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. 204363
 Reference 0.000
 SG 1.000
 Linearity 0.152
 Scale factor 19.970
 Offset 0.061
 Delay mSEC 50.000

Step 0 08/22 07:52:04

 Elapsed Time INPUT 1

 0.0000 0.000
 0.0083 0.006
 0.0166 0.000
 0.0250 0.006
 0.0333 0.725
 0.0416 2.233 ✓
 0.0500 1.785
 0.0583 1.363
 0.0566 0.921
 0.0750 0.473
 0.0833 0.353
 0.0916 0.201
 0.1000 0.088
 0.1083 0.012 ✓
 0.1166 -0.012
 0.1250 -0.031
 0.1333 -0.037
 0.1416 -0.037
 0.1500 -0.025
 0.1583 -0.018
 0.1666 -0.012
 0.1750 -0.006
 0.1833 0.000
 0.1916 -0.006
 0.2000 0.006
 0.2083 0.006
 0.2166 0.006
 0.2250 0.006
 0.2333 0.006
 0.2416 0.006
 0.2500 0.006
 0.2583 0.006
 0.2666 0.000
 0.2750 0.000
 0.2833 0.000
 0.2916 0.000
 0.3000 0.000
 0.3083 0.000

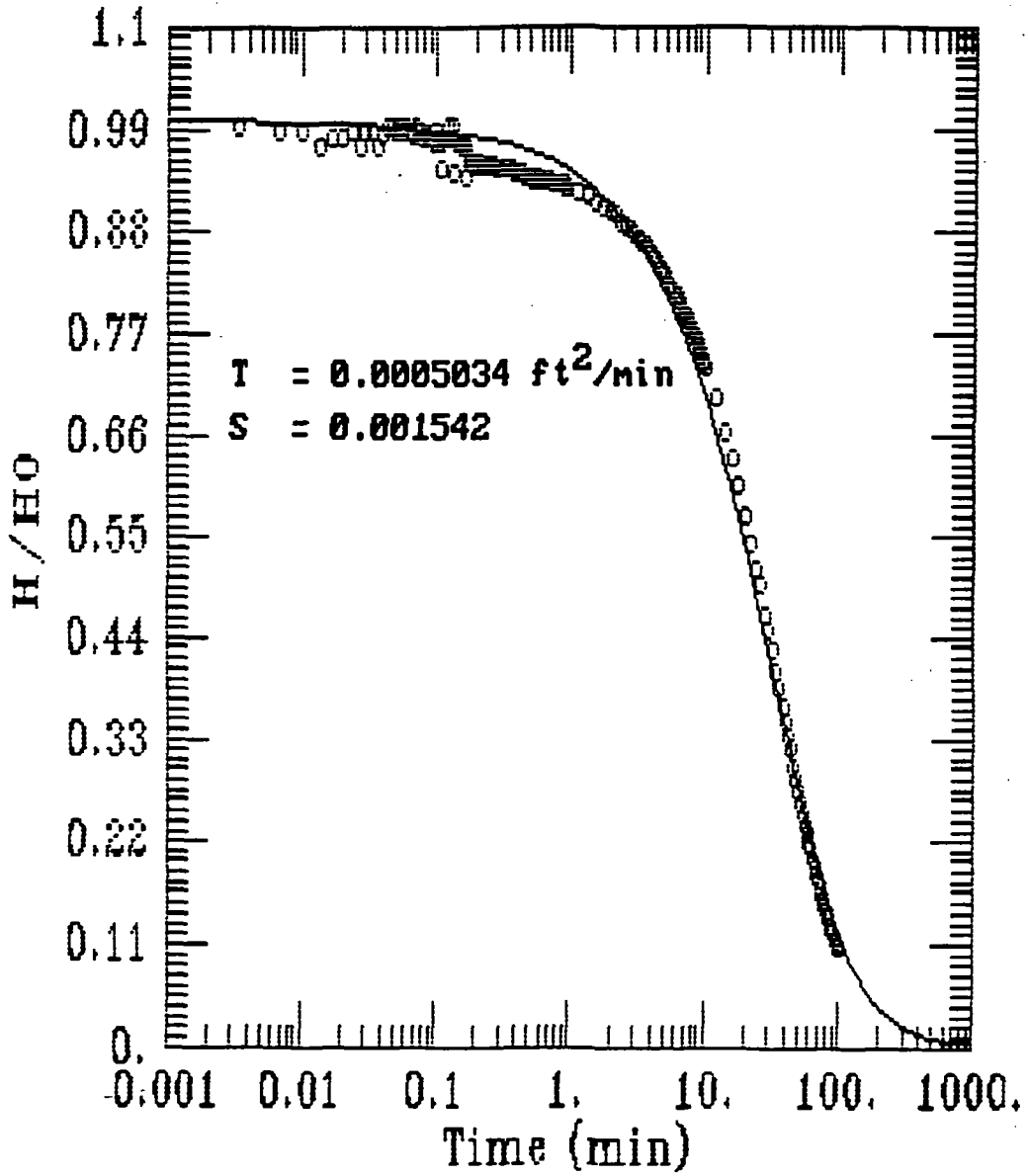
Test:	<u>L3-1 Slug out</u>
File:	<u>L31-T2</u>
Round:	<u>KTEST 3</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head (ft)</u>
	<u>t₀ = 0.0416 t₁ = 0.1683</u>
Column 3:	<u>_____</u>
	<u>t₀ = _____ t₁ = _____</u>

0.3333	0.000
0.3500	0.000
0.3666	0.000
0.3833	0.006
0.4000	0.006
0.4166	0.006
0.4333	0.000
0.4500	0.000
0.4666	0.006
0.4833	0.006
0.5000	0.006
0.5166	0.006
0.5333	0.006
0.5500	0.006
0.5666	0.006
0.5833	0.006
0.6000	0.006
0.6166	0.000
0.6333	0.006
0.6500	0.006
0.6666	0.006
0.6833	0.006
0.7000	0.006
0.7166	0.006
0.7333	0.006
0.7500	0.006
0.7666	0.006
0.7833	0.006
0.8000	0.006
0.8166	0.006
0.8333	0.006
0.8500	0.006
0.8666	0.006
0.8833	0.006
0.9000	0.006
0.9166	0.006
0.9333	0.006
0.9500	0.006
0.9666	0.006
0.9833	0.006
1.0000	0.006
1.2000	0.006
1.4000	0.006

WELL CLUSTER: L
WELL ID: L4
SCREENED INTERVAL: 48-58

TEST METHOD: Cooper et al
SLUG IN/SLUG OUT: Slug out
K-VALUE: 0.0489 ft/day

L4-T2



0.2200	2.703
0.2233	2.703
0.2266	2.710
0.2300	2.697
0.2333	2.703
0.2366	2.608
0.2400	2.659
0.2433	2.665
0.2466	2.646
0.2500	2.653
0.2533	2.653
0.2566	2.653
0.2600	2.653
0.2633	2.653
0.2666	2.653
0.2700	2.653
0.2733	2.646
0.2766	2.646
0.2800	2.646
0.2833	2.646
0.2866	2.646
0.2900	2.646
0.2933	2.646
0.2966	2.646
0.3000	2.640
0.3033	2.640
0.3066	2.646
0.3100	2.646
0.3133	2.640
0.3166	2.640
0.3200	2.640
0.3233	2.640
0.3266	2.640
0.3300	2.640
0.3333	2.640
0.3366	2.640
0.3400	2.634
0.3433	2.627
0.3466	2.627
0.3500	2.627
0.3533	2.627
0.3566	2.627
0.3600	2.621
0.3633	2.621
0.3666	2.621
0.3700	2.615
0.3733	2.608
0.3766	2.608
0.3800	2.608
0.3833	2.608
0.3866	2.608
0.3900	2.602
0.3933	2.608
0.3966	2.608
0.4000	2.602
0.4033	2.602
0.4066	2.602
0.4100	2.602
0.4133	2.602
0.4166	2.602
0.4200	2.602
0.4233	2.602
0.4266	2.602
0.4300	2.602
0.4333	2.602
0.4366	2.602
0.4400	2.602
0.4433	2.602
0.4466	2.602
0.4500	2.602
0.4533	2.602
0.4566	2.602
0.4600	2.602
0.4633	2.602
0.4666	2.602
0.4700	2.602
0.4733	2.602
0.4766	2.602
0.4800	2.602
0.4833	2.602
0.4866	2.602
0.4900	2.602
0.4933	2.602
0.4966	2.602
0.5000	2.602
0.5033	2.602
0.5066	2.602
0.5100	2.602
0.5133	2.602
0.5166	2.602
0.5200	2.602
0.5233	2.602
0.5266	2.602
0.5300	2.602
0.5333	2.602
0.5366	2.602
0.5400	2.602
0.5433	2.602
0.5466	2.602
0.5500	2.602
0.5533	2.602
0.5566	2.602
0.5600	2.602
0.5633	2.602
0.5666	2.602
0.5700	2.602
0.5733	2.602
0.5766	2.602
0.5800	2.602
0.5833	2.602
0.5866	2.602
0.5900	2.602
0.5933	2.602
0.5966	2.602
0.6000	2.602
0.6033	2.602
0.6066	2.602
0.6100	2.602
0.6133	2.602
0.6166	2.602
0.6200	2.602
0.6233	2.602
0.6266	2.602
0.6300	2.602
0.6333	2.602
0.6366	2.602
0.6400	2.602
0.6433	2.602
0.6466	2.602
0.6500	2.602
0.6533	2.602
0.6566	2.602
0.6600	2.602
0.6633	2.602
0.6666	2.602
0.6700	2.602
0.6733	2.602
0.6766	2.602
0.6800	2.602
0.6833	2.602
0.6866	2.602
0.6900	2.602
0.6933	2.602
0.6966	2.602
0.7000	2.602
0.7033	2.602
0.7066	2.602
0.7100	2.602
0.7133	2.602
0.7166	2.602
0.7200	2.602
0.7233	2.602
0.7266	2.602
0.7300	2.602
0.7333	2.602
0.7366	2.602
0.7400	2.602
0.7433	2.602
0.7466	2.602
0.7500	2.602
0.7533	2.602
0.7566	2.602
0.7600	2.602
0.7633	2.602
0.7666	2.602
0.7700	2.602
0.7733	2.602
0.7766	2.602
0.7800	2.602
0.7833	2.602
0.7866	2.602
0.7900	2.602
0.7933	2.602
0.7966	2.602
0.8000	2.602
0.8033	2.602
0.8066	2.602
0.8100	2.602
0.8133	2.602
0.8166	2.602
0.8200	2.602
0.8233	2.602
0.8266	2.602
0.8300	2.602
0.8333	2.602
0.8366	2.602
0.8400	2.602
0.8433	2.602
0.8466	2.602
0.8500	2.602
0.8533	2.602
0.8566	2.602
0.8600	2.602
0.8633	2.602
0.8666	2.602
0.8700	2.602
0.8733	2.602
0.8766	2.602
0.8800	2.602
0.8833	2.602
0.8866	2.602
0.8900	2.602
0.8933	2.602
0.8966	2.602
0.9000	2.602
0.9033	2.602
0.9066	2.602
0.9100	2.602
0.9133	2.602
0.9166	2.602
0.9200	2.602
0.9233	2.602
0.9266	2.602
0.9300	2.602
0.9333	2.602
0.9366	2.602
0.9400	2.602
0.9433	2.602
0.9466	2.602
0.9500	2.602
0.9533	2.602
0.9566	2.602
0.9600	2.602
0.9633	2.602
0.9666	2.602
0.9700	2.602
0.9733	2.602
0.9766	2.602
0.9800	2.602
0.9833	2.602
0.9866	2.602
0.9900	2.602
0.9933	2.602
0.9966	2.602
1.0000	2.602

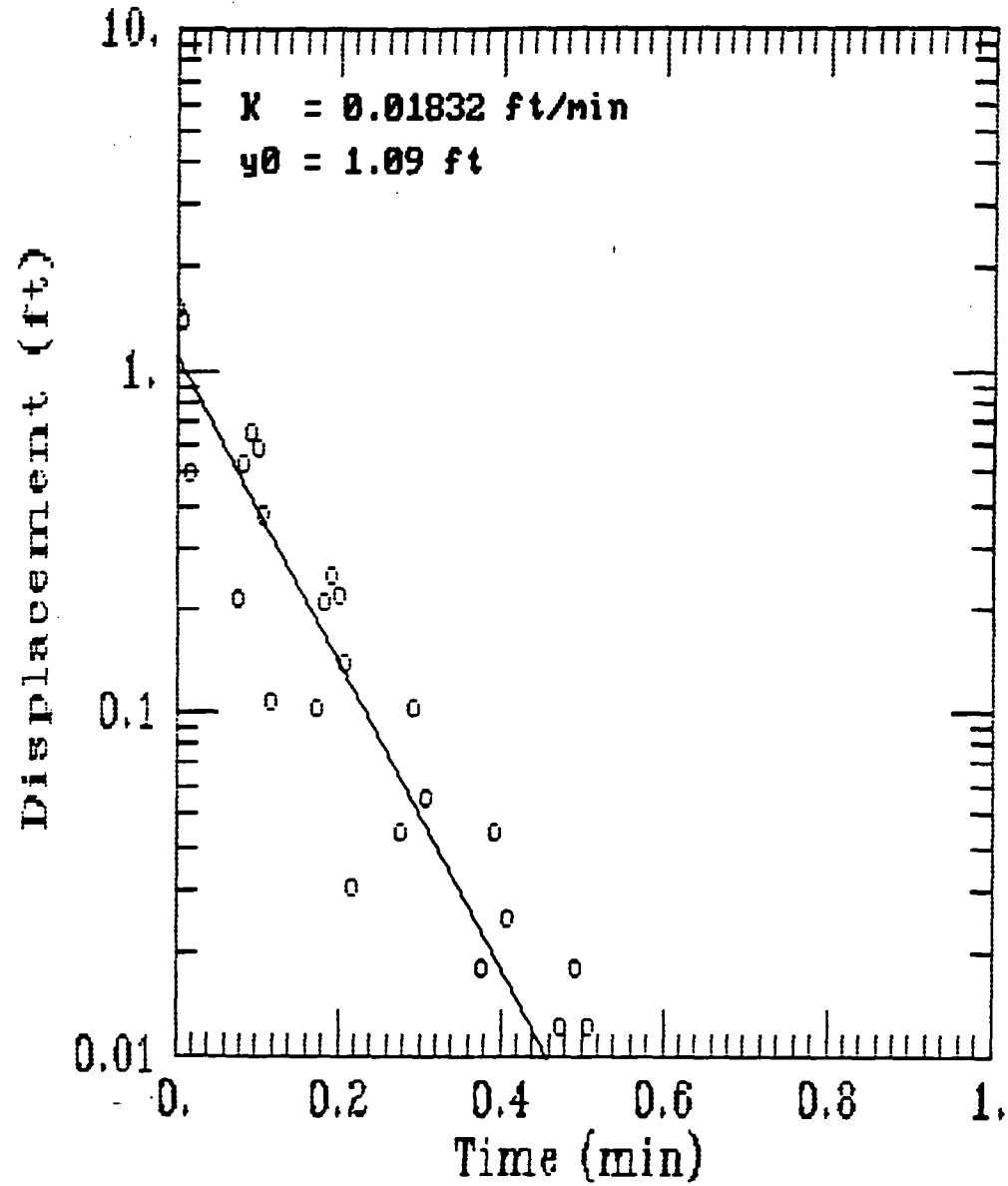
0.8833	2.583
0.9000	2.583
0.9166	2.583
0.9333	2.583
0.9500	2.583
0.9666	2.577
0.9833	2.577
1.0000	2.577
1.2000	2.558
1.4000	2.545
1.6000	2.526
1.8000	2.514
2.0000	2.501
2.2000	2.488
2.4000	2.469
2.6000	2.457
2.8000	2.444
3.0000	2.438
3.2000	2.419
3.4000	2.413
3.6000	2.400
3.8000	2.387
4.0000	2.375
4.2000	2.368
4.4000	2.356
4.6000	2.337
4.8000	2.324
5.0000	2.318
5.2000	2.305
5.4000	2.286
5.6000	2.274
5.8000	2.267
6.0000	2.255
6.2000	2.248
6.4000	2.236
6.6000	2.229
6.8000	2.211
7.0000	2.198
7.2000	2.192
7.4000	2.179
7.6000	2.173
7.8000	2.160
8.0000	2.147
8.2000	2.135
8.4000	2.128
8.6000	2.116
8.8000	2.109
9.0000	2.097
9.2000	2.084
9.4000	2.065
9.6000	2.053
9.8000	2.046
10.0000	2.040
12.0000	1.945
14.0000	1.844
16.0000	1.756
18.0000	1.674
20.0000	1.591
22.0000	1.509
24.0000	1.427
26.0000	1.377
28.0000	1.295
30.0000	1.244

36.0000	1.087
38.0000	1.017
40.0000	0.966
42.0000	0.928
44.0000	0.884
46.0000	0.833
48.0000	0.795
50.0000	0.758
52.0000	0.726
54.0000	0.694
56.0000	0.656
58.0000	0.638
60.0000	0.606
62.0000	0.587
64.0000	0.555
66.0000	0.530
68.0000	0.511
70.0000	0.499
72.0000	0.480
74.0000	0.454
76.0000	0.442
78.0000	0.423
80.0000	0.410
82.0000	0.391
84.0000	0.379
86.0000	0.366
88.0000	0.353
90.0000	0.341
92.0000	0.334
94.0000	0.322
96.0000	0.315
98.0000	0.303
100.000	0.296

WELL CLUSTER: L
WELL ID: L5
SCREENED INTERVAL: 31.5-36.5

TEST METHOD: Bowser Rice
SLUG IN/SLUG OUT: Slug out
K-VALUE: 26.4 ft/day

L5-RT2



Unit# 22 Test 5

L5-RT2 (re-test) PRN ✓

 Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. 204363

Reference 0.000
 SG 1.000
 Linearity 0.152
 Scale factor 19.970
 Offset 0.061
 Delay mSEC 50.000

Step 0 08/22 08:26:12

 Elapsed Time INPUT 1

0.0000	0.000
0.0083	0.012
0.0166	0.006
0.0250	0.000
0.0333	0.138
0.0416	-0.164
0.0500	1.281
0.0583	1.489 ✓
0.0666	1.375
0.0750	0.504
0.0833	-0.290
0.0916	-0.833
0.1000	-1.029
0.1083	-0.959
0.1166	-0.656
0.1250	-0.220
0.1333	0.214
0.1416	0.530
0.1500	0.656
0.1583	0.593
0.1666	0.378
0.1750	0.107
0.1833	-0.151
0.1916	-0.321
0.2000	-0.391
0.2083	-0.347
0.2166	-0.220
0.2250	-0.056
0.2333	0.101
0.2416	0.208
0.2500	0.252
0.2583	0.220
0.2666	0.138
0.2750	0.031
0.2833	-0.063
0.2916	-0.132
0.3000	-0.157

Same flux

Test:	L5 slug out
File:	L5-RT2
Round:	KTEST3
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	t = 0.5833 t = 0.5833
Column 3:	
	t = _____ t = _____

① re-do but stop test @ 0.5833

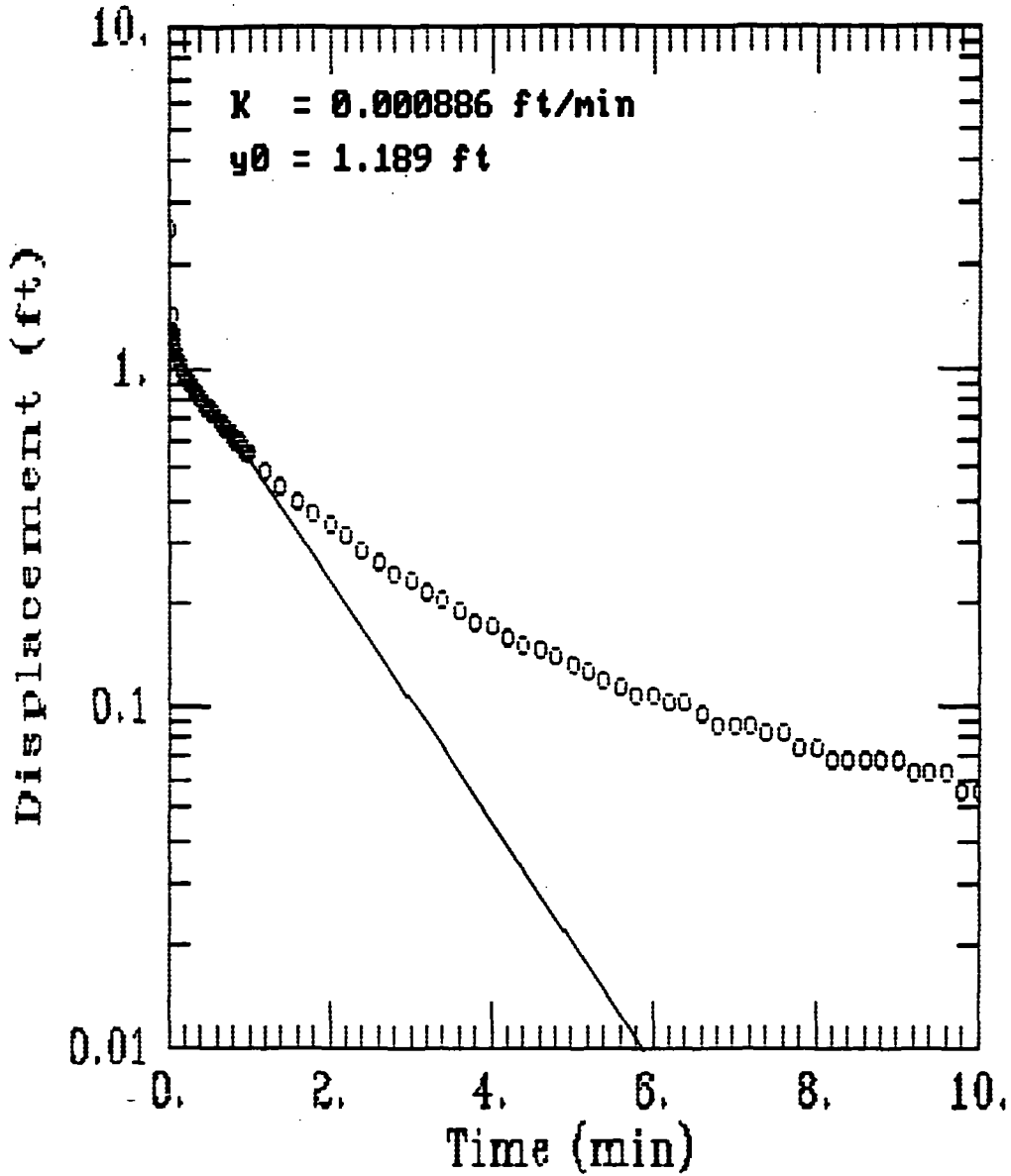
② analyze

0.3333	0.044
0.3500	0.101
0.3666	0.056
0.3833	-0.025
0.4000	-0.056
0.4166	-0.031
0.4333	0.018
0.4500	0.044
0.4666	0.025
0.4833	-0.012
0.5000	-0.025
0.5166	-0.012
0.5333	0.012
0.5500	0.018
0.5666	0.012
0.5833	0.000 — step
0.6000	-0.006
0.6166	0.000
0.6333	0.006
0.6500	0.006
0.6666	0.006
0.6833	0.000
0.7000	0.000
0.7166	0.000
0.7333	0.006
0.7500	0.006
0.7666	0.006
0.7833	0.000
0.8000	0.000
0.8166	0.000
0.8333	0.006
0.8500	0.006
0.8666	0.006
0.8833	0.000
0.9000	0.006
0.9166	0.006
0.9333	0.006
0.9500	0.006
0.9666	0.006
0.9833	0.006
1.0000	0.000
1.2000	0.006
1.4000	0.006
1.6000	0.006

WELL CLUSTER: M
WELL ID: M1
SCREENED INTERVAL: 2-8.5

TEST METHOD: Bowmer Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 1.28 ft/day

M1-T2



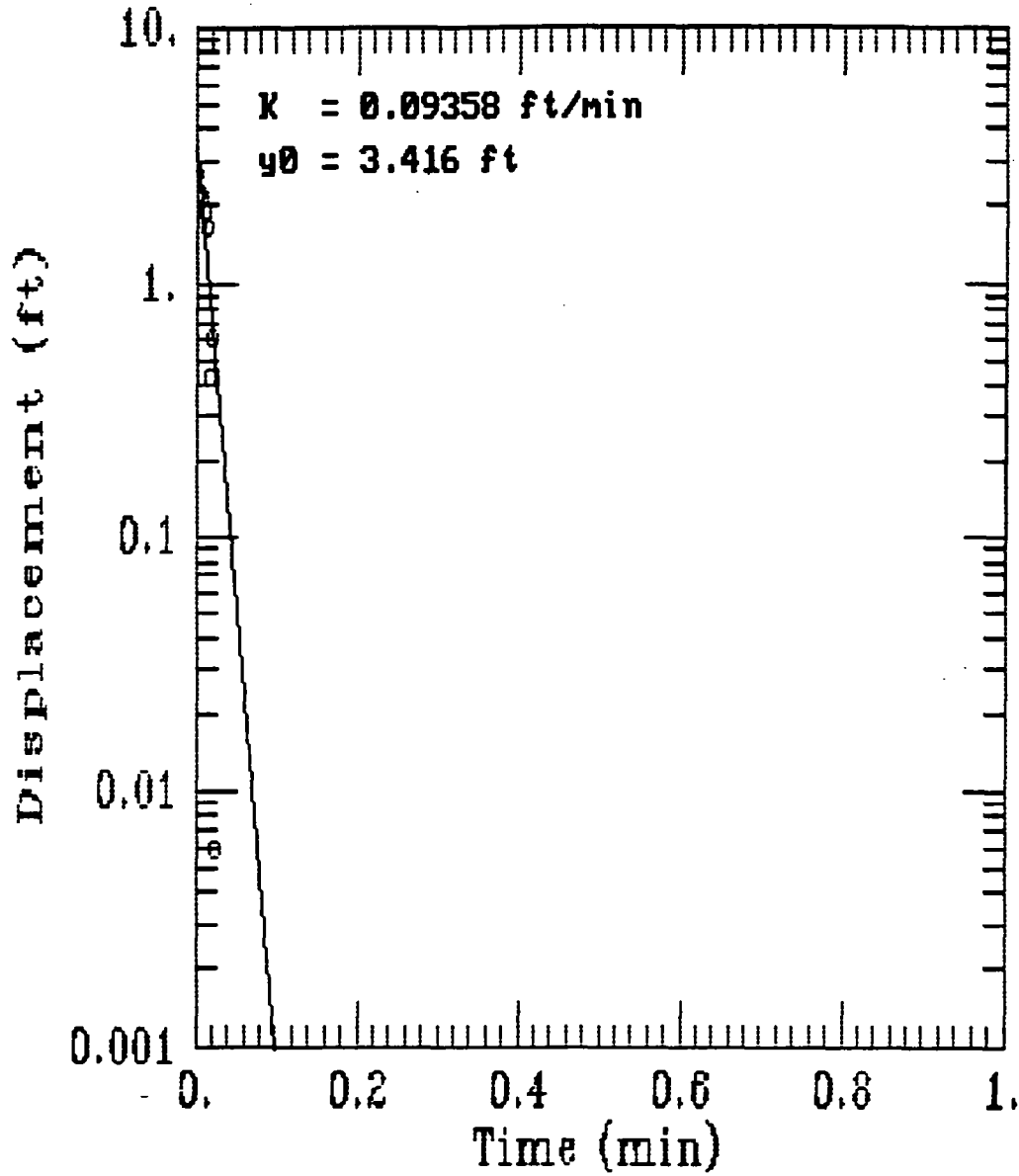
0.2200	0.947
0.2233	0.947
0.2266	0.941
0.2300	0.941
0.2333	0.934
0.2366	0.934
0.2400	0.928
0.2433	0.928
0.2466	0.928
0.2500	0.922
0.2533	0.915
0.2566	0.915
0.2600	0.915
0.2633	0.909
0.2666	0.909
0.2700	0.903
0.2733	0.903
0.2766	0.903
0.2800	0.897
0.2833	0.897
0.2866	0.890
0.2900	0.890
0.2933	0.890
0.2966	0.884
0.3000	0.884
0.3033	0.884
0.3066	0.878
0.3100	0.878
0.3133	0.871
0.3166	0.871
0.3200	0.865
0.3233	0.865
0.3266	0.865
0.3300	0.865
0.3333	0.859
0.3500	0.846
0.3666	0.833
0.3833	0.821
0.4000	0.814
0.4166	0.802
0.4333	0.795
0.4500	0.783
0.4666	0.776
0.4833	0.764
0.5000	0.758
0.5166	0.751
0.5333	0.739
0.5500	0.732
0.5666	0.726
0.5833	0.720
0.6000	0.707
0.6166	0.701
0.6333	0.694
0.6500	0.688
0.6666	0.682
0.6833	0.675
0.7000	0.669
0.7166	0.663
0.7333	0.656
0.7500	0.644
0.7666	0.638
0.7833	0.631
0.8000	0.625
0.8166	0.613

0.8666	0.606
0.8833	0.600
0.9000	0.593
0.9166	0.587
0.9333	0.581
0.9500	0.574
0.9666	0.568
0.9833	0.562
1.0000	0.562
1.2000	0.492
1.4000	0.442
1.6000	0.404
1.8000	0.372
2.0000	0.341
2.2000	0.315
2.4000	0.284
2.6000	0.265
2.8000	0.246
3.0000	0.233
3.2000	0.214
3.4000	0.202
3.6000	0.189
3.8000	0.176
4.0000	0.170
4.2000	0.157
4.4000	0.151
4.6000	0.145
4.8000	0.138
5.0000	0.132
5.2000	0.126
5.4000	0.120
5.6000	0.113
5.8000	0.107
6.0000	0.107
6.2000	0.101
6.4000	0.101
6.6000	0.094
6.8000	0.088
7.0000	0.088
7.2000	0.088
7.4000	0.082
7.6000	0.082
7.8000	0.075
8.0000	0.075
8.2000	0.069
8.4000	0.069
8.6000	0.069
8.8000	0.069
9.0000	0.069
9.2000	0.063
9.4000	0.063
9.6000	0.063
9.8000	0.056
10.0000	0.056

WELL CLUSTER: M
WELL ID: M2
SCREENED INTERVAL: 34-44

TEST METHOD: Barrier Piece
SLUG IN/SLUG OUT: <slug out
K-VALUE: 135 ft/day

M2-T2



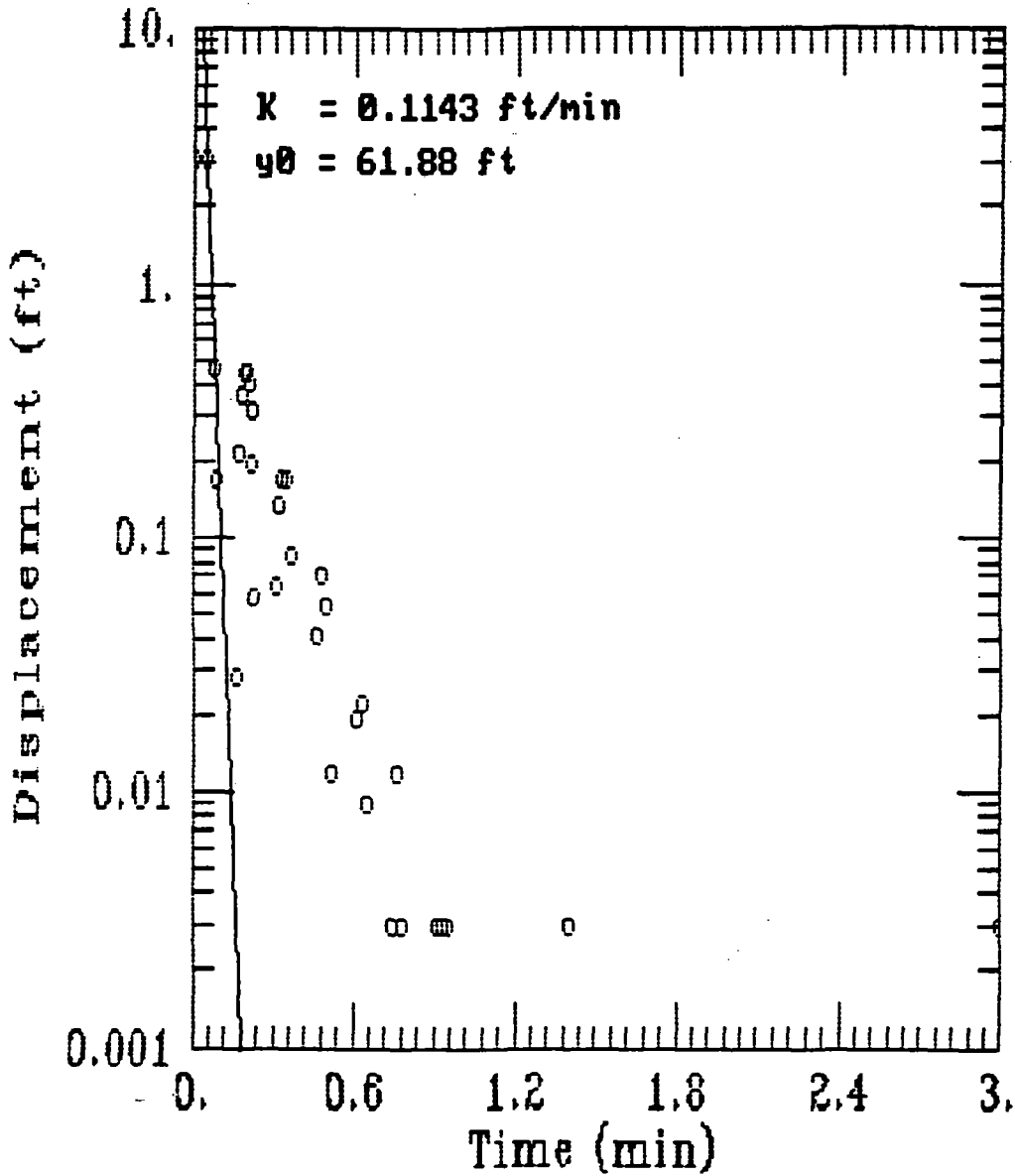
0.2200	-0.083
0.2233	-0.056
0.2266	-0.050
0.2300	-0.050
0.2333	-0.044
0.2366	-0.044
0.2400	-0.037
0.2433	-0.037
0.2466	-0.031
0.2500	-0.025
0.2533	-0.018
0.2566	-0.018
0.2600	-0.012
0.2633	-0.012
0.2666	-0.012
0.2700	-0.006
0.2733	0.000
0.2766	0.000
0.2800	0.006
0.2833	0.006
0.2866	0.012
0.2900	0.019
0.2933	0.019
0.2966	0.019
0.3000	0.025
0.3033	0.025
0.3066	0.025
0.3100	0.031
0.3133	0.031
0.3166	0.037
0.3200	0.037
0.3233	0.037
0.3266	0.044
0.3300	0.044
0.3333	0.044
0.3500	0.050
0.3666	0.056
0.3833	0.056
0.4000	0.056
0.4166	0.056
0.4333	0.050
0.4500	0.050
0.4666	0.044
0.4833	0.037
0.5000	0.031
0.5166	0.025
0.5333	0.019
0.5500	0.012
0.5666	0.012
0.5833	0.006
0.6000	0.006
0.6166	0.000
0.6333	0.000
0.6500	0.000
0.6666	0.000
0.6833	0.006
0.7000	0.006
0.7166	0.006
0.7333	0.006
0.7500	0.006
0.7666	0.006
0.7833	0.012
0.8000	0.012
0.8166	0.012

0.8888	0.017
0.8833	0.019
0.9000	0.019
0.9166	0.019
0.9333	0.012
0.9500	0.012
0.9666	0.012
0.9833	0.012
1.0000	0.012
1.2000	0.006
1.4000	0.000
1.6000	-0.006
1.8000	0.000
2.0000	0.000
2.2000	0.006
2.4000	0.006
2.6000	0.000
2.8000	0.000
3.0000	0.012
3.2000	0.006
3.4000	0.006
3.6000	0.006
3.8000	0.006
4.0000	0.006
4.2000	0.006
4.4000	0.006
4.6000	0.000
4.8000	0.000
5.0000	0.000
5.2000	0.000
5.4000	0.000
5.6000	0.006
5.8000	0.006
6.0000	0.006
6.2000	0.006
6.4000	0.000
6.6000	0.000
6.8000	0.000
7.0000	0.000
7.2000	0.000
7.4000	0.000
7.6000	0.000
7.8000	0.006
8.0000	0.000
8.2000	0.000
8.4000	0.000
8.6000	0.006
8.8000	0.000
9.0000	0.000
9.2000	0.006
9.4000	0.006
9.6000	0.000
9.8000	0.000
10.0000	0.000

WELL CLUSTER: M
WELL ID: M3
SCREENED INTERVAL: 57-63

TEST METHOD: Bowser Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 165 ft/day

M3-T2

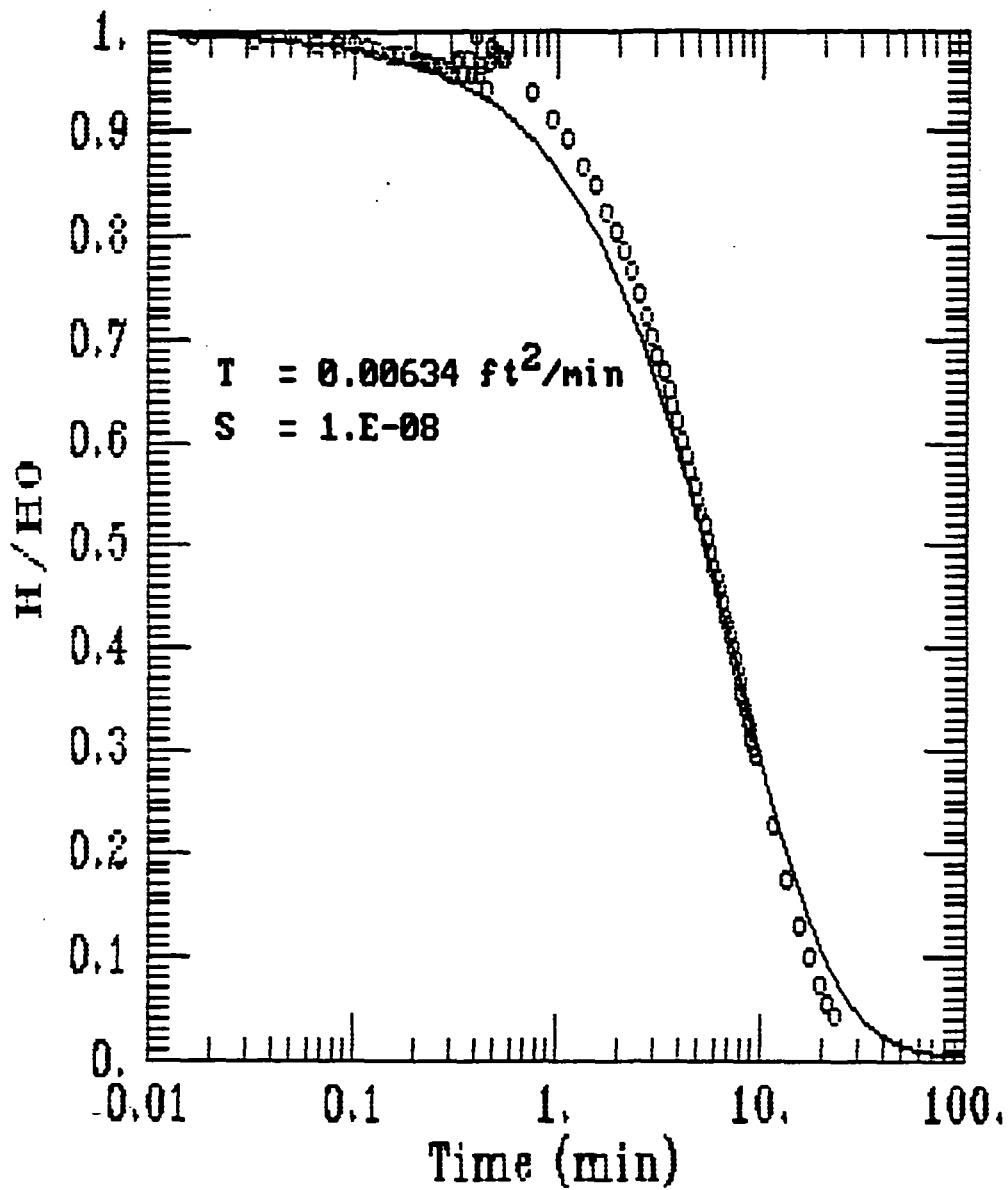


0.3333	0.170
0.3500	0.167
0.3666	0.086
0.3833	-0.022
0.4000	-0.103
0.4166	-0.125
0.4333	-0.086
0.4500	-0.016
0.4666	0.041
0.4833	0.070
0.5000	0.054
0.5166	0.012
0.5333	-0.028
0.5500	-0.051
0.5666	-0.054
0.5833	-0.035
0.6000	-0.003
0.6166	0.019
0.6333	0.022
0.6500	0.009
0.6666	-0.006
0.6833	-0.019
0.7000	-0.028
0.7166	-0.022
0.7333	-0.012
0.7500	0.003
0.7666	0.012
0.7833	0.003
0.8000	0.000
0.8166	-0.006
0.8333	-0.012
0.8500	-0.012
0.8666	-0.012
0.8833	-0.009
0.9000	0.000
0.9166	0.003
0.9333	0.003
0.9500	0.003
0.9666	-0.003
0.9833	-0.009
1.0000	-0.006
1.2000	-0.003
1.4000	0.003
1.6000	0.000
1.8000	-0.006
2.0000	0.000
2.2000	-0.003
2.4000	-0.012
2.6000	-0.006
2.8000	-0.000
3.0000	0.003

WELL CLUSTER: M
WELL ID: M4
SCREENED INTERVAL: 69-79

TEST METHOD: Cooper et al.
SLUG IN/SLUG OUT: slug out
K-VALUE: 0.609 ft/den

M4-T2



0.2200	2.788
0.2233	2.754
0.2266	2.741
0.2300	2.728
0.2333	2.880
0.2366	2.924
0.2400	3.070
0.2433	3.183
0.2466	3.183
0.2500	3.171
0.2533	3.171
0.2566	3.164
0.2600	3.164
0.2633	3.152
0.2666	3.139
0.2700	3.145
0.2733	3.133
0.2766	3.120
0.2800	3.114
0.2833	3.114
0.2866	3.114
0.2900	3.101
0.2933	3.095
0.2966	3.089
0.3000	3.082
0.3033	3.076
0.3066	3.070
0.3100	3.063
0.3133	3.057
0.3166	3.051
0.3200	3.038
0.3233	3.032
0.3266	3.025
0.3300	3.057
0.3333	3.063
0.3500	3.341
0.3666	3.341
0.3833	3.322
0.4000	3.335
0.4166	3.348 ^①
0.4333	3.089
0.4500	2.375 ^②
0.4666	2.368
0.4833	2.356
0.5000	2.362
0.5166	2.350
0.5333	2.350
0.5500	2.343
0.5666	2.337
0.5833	2.331
0.6000	2.324
0.6166	2.324
0.6333	2.318
0.6500	2.312
0.6666	2.305
0.6833	2.299
0.7000	2.293
0.7166	2.293
0.7333	2.286
0.7500	2.274
0.7666	2.305
0.7833	2.312
0.8000	2.280
0.8166	2.312

Start

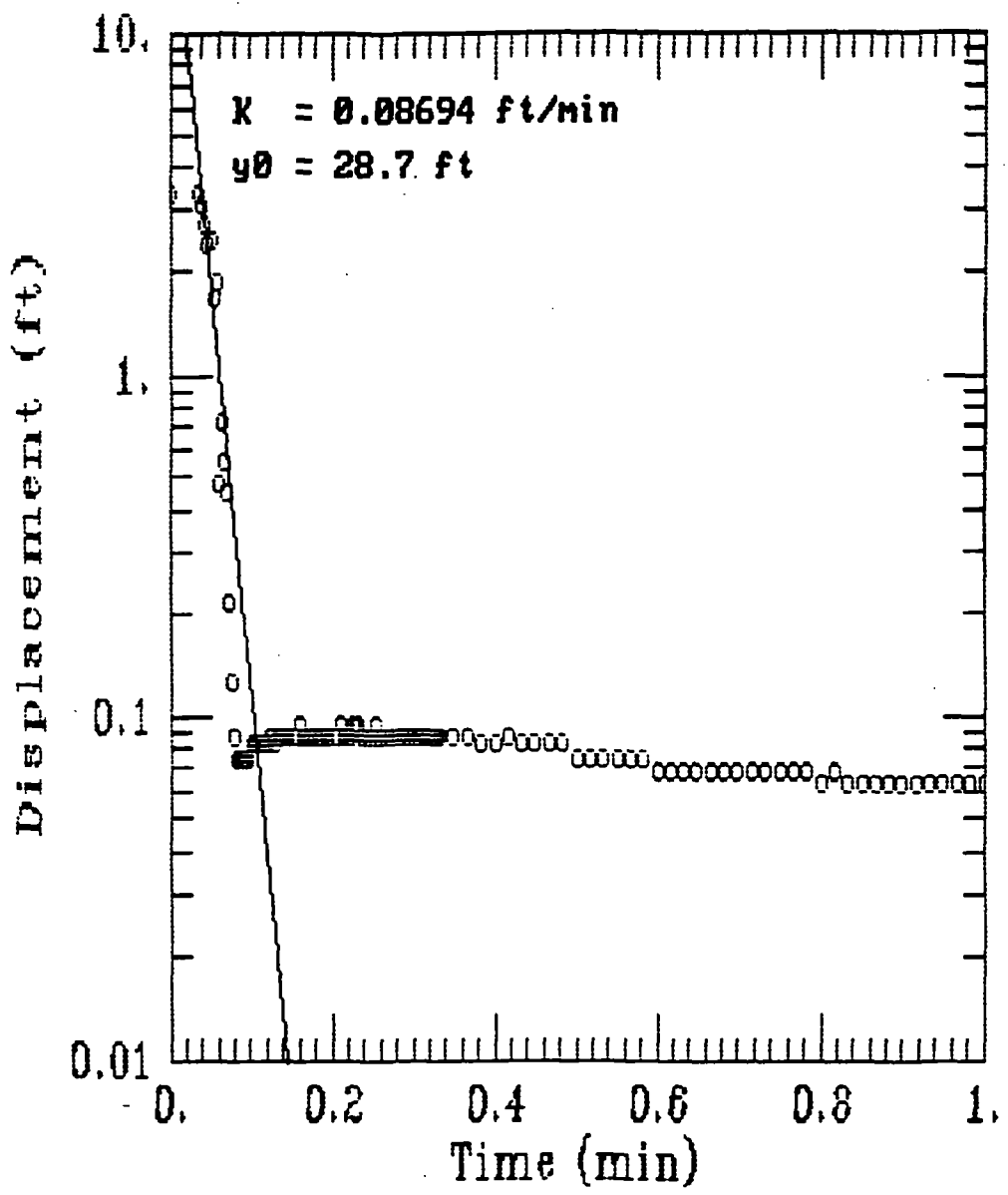
0.8000	2.280
0.8833	2.293
0.9000	2.236
0.9166	2.299
0.9333	2.337
0.9500	2.324
0.9666	2.318
0.9833	2.312
1.0000	2.312
1.2000	2.229
1.4000	2.173
1.6000	2.122
1.8000	2.065
2.0000	2.015
2.2000	1.958
2.4000	1.907
2.6000	1.863
2.8000	1.819
3.0000	1.768
3.2000	1.718
3.4000	1.674
3.6000	1.629
3.8000	1.591
4.0000	1.547
4.2000	1.509
4.4000	1.471
4.6000	1.427
4.8000	1.396
5.0000	1.358
5.2000	1.326
5.4000	1.288
5.6000	1.257
5.8000	1.231
6.0000	1.200
6.2000	1.168
6.4000	1.137
6.6000	1.111
6.8000	1.080
7.0000	1.055
7.2000	1.023
7.4000	0.998
7.6000	0.972
7.8000	0.947
8.0000	0.922
8.2000	0.897
8.4000	0.871
8.6000	0.846
8.8000	0.827
9.0000	0.802
9.2000	0.783
9.4000	0.764
9.6000	0.739
9.8000	0.720
10.0000	0.701
12.0000	0.536
14.0000	0.410
16.0000	0.309
18.0000	0.240
20.0000	0.176
22.0000	0.126
24.0000	0.101

- to Plot (a)

WELL CLUSTER: M
WELL ID: M5
SCREENED INTERVAL: 16-21

TEST METHOD: Blower Pipe
SLUG IN/SLUG OUT: slug out
K-VALUE: 125 ft/day

M5-T2



0.2200	0.088
0.2233	0.089
0.2266	0.094
0.2300	0.094
0.2333	0.094
0.2366	0.089
0.2400	0.089
0.2433	0.088
0.2466	0.088
0.2500	0.088
0.2533	0.094
0.2566	0.088
0.2600	0.088
0.2633	0.088
0.2666	0.088
0.2700	0.088
0.2733	0.088
0.2766	0.088
0.2800	0.088
0.2833	0.088
0.2866	0.088
0.2900	0.088
0.2933	0.088
0.2966	0.088
0.3000	0.088
0.3033	0.088
0.3066	0.088
0.3100	0.088
0.3133	0.088
0.3166	0.089
0.3200	0.088
0.3233	0.088
0.3266	0.088
0.3300	0.088
0.3333	0.088
0.3500	0.088
0.3666	0.088
0.3833	0.082
0.4000	0.082
0.4166	0.086
0.4333	0.082
0.4500	0.082
0.4666	0.082
0.4833	0.082
0.5000	0.075
0.5166	0.075
0.5333	0.075
0.5500	0.075
0.5666	0.075
0.5833	0.075
0.6000	0.069
0.6166	0.069
0.6333	0.069
0.6500	0.069
0.6666	0.069
0.6833	0.069
0.7000	0.069
0.7166	0.069
0.7333	0.069
0.7500	0.069
0.7666	0.069
0.7833	0.069
0.8000	0.063
0.8166	0.069

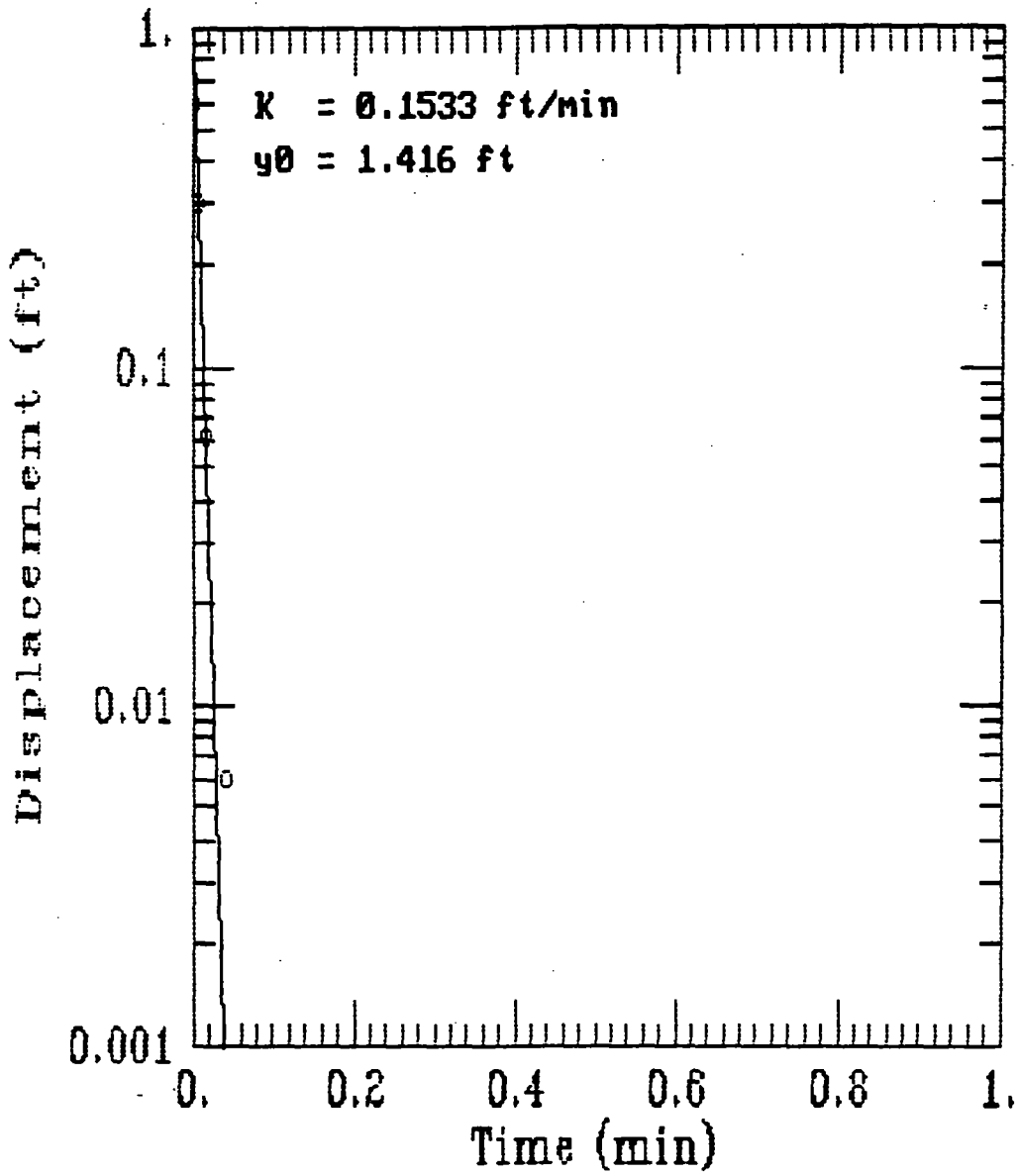
0.8833	0.063
0.9000	0.063
0.9166	0.063
0.9333	0.063
0.9500	0.063
0.9666	0.063
0.9833	0.063
1.0000	0.063
1.2000	0.056
1.4000	0.050
1.6000	0.044
1.8000	0.037
2.0000	0.037
2.2000	0.031
2.4000	0.025
2.6000	0.025
2.8000	0.018
3.0000	0.018
3.2000	0.018
3.4000	0.012
3.6000	0.012
3.8000	0.012
4.0000	0.012
4.2000	0.012
4.4000	0.012
4.6000	0.012
4.8000	0.012
5.0000	0.006
5.2000	0.012
5.4000	0.006
5.6000	0.006
5.8000	0.006
6.0000	0.006
6.2000	0.006
6.4000	0.006
6.6000	0.006
6.8000	0.006
7.0000	0.006
7.2000	0.000
7.4000	0.000
7.6000	0.006
7.8000	0.006
8.0000	0.006
8.2000	0.006
8.4000	0.006
8.6000	0.000
8.8000	0.000
9.0000	0.000
9.2000	0.006
9.4000	0.000
9.6000	0.000
9.8000	0.000
10.0000	0.006

tc

WELL CLUSTER: N
WELL ID: N1
SCREENED INTERVAL: 7-17

TEST METHOD: Packer Rise
SLUG IN/SLUG OUT: Slug out
K-VALUE: 221 ft/day

N1-T2

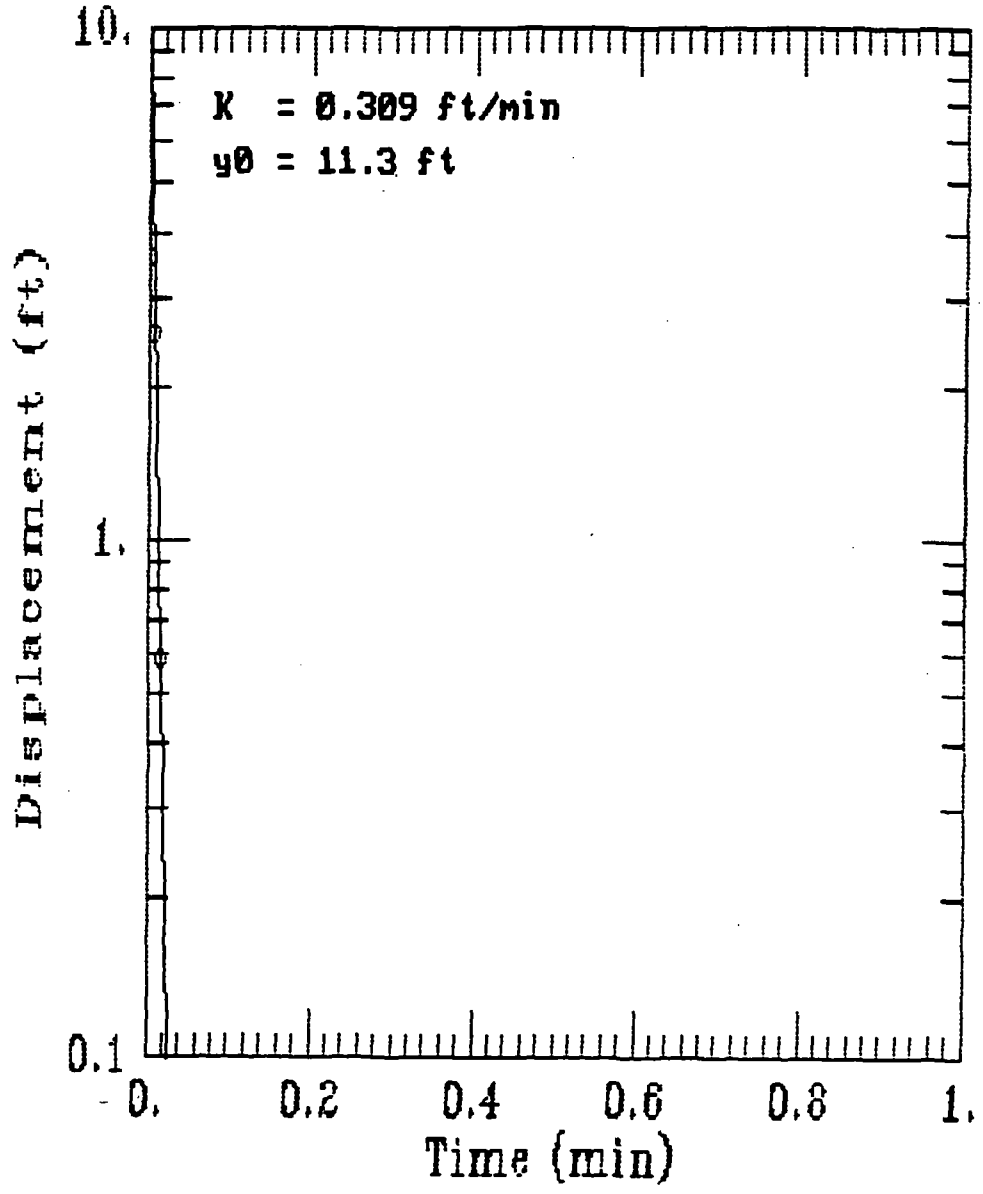


0.3333	-0.006
0.3500	-0.006
0.3666	-0.006
0.3833	-0.006
0.4000	-0.006
0.4166	-0.006
0.4333	-0.006
0.4500	-0.006
0.4666	-0.006
0.4833	-0.006
0.5000	-0.006
0.5166	-0.006
0.5333	-0.006
0.5500	-0.006
0.5666	-0.006
0.5833	-0.006
0.6000	-0.006
0.6166	-0.006
0.6333	-0.006
0.6500	-0.006
0.6666	-0.006
0.6833	-0.006
0.7000	-0.006
0.7166	-0.006
0.7333	-0.006
0.7500	-0.006
0.7666	-0.006
0.7833	-0.006
0.8000	-0.006
0.8166	-0.006
0.8333	-0.006
0.8500	-0.006
0.8666	-0.006
0.8833	-0.006
0.9000	-0.006
0.9166	-0.006
0.9333	-0.006
0.9500	-0.006
0.9666	-0.006
0.9833	-0.006
1.0000	-0.006
1.2000	-0.006
1.4000	-0.006
1.6000	-0.006
1.8000	-0.006
2.0000	-0.006
2.2000	-0.006
2.4000	0.000
2.5000	0.000

WELL CLUSTER: N
WELL ID: N13
SCREENED INTERVAL: 22-27

TEST METHOD: Banner Pipe
SLUG IN/SLUG OUT: Slug out
K-VALUE: 445 ft/day

N3-T2

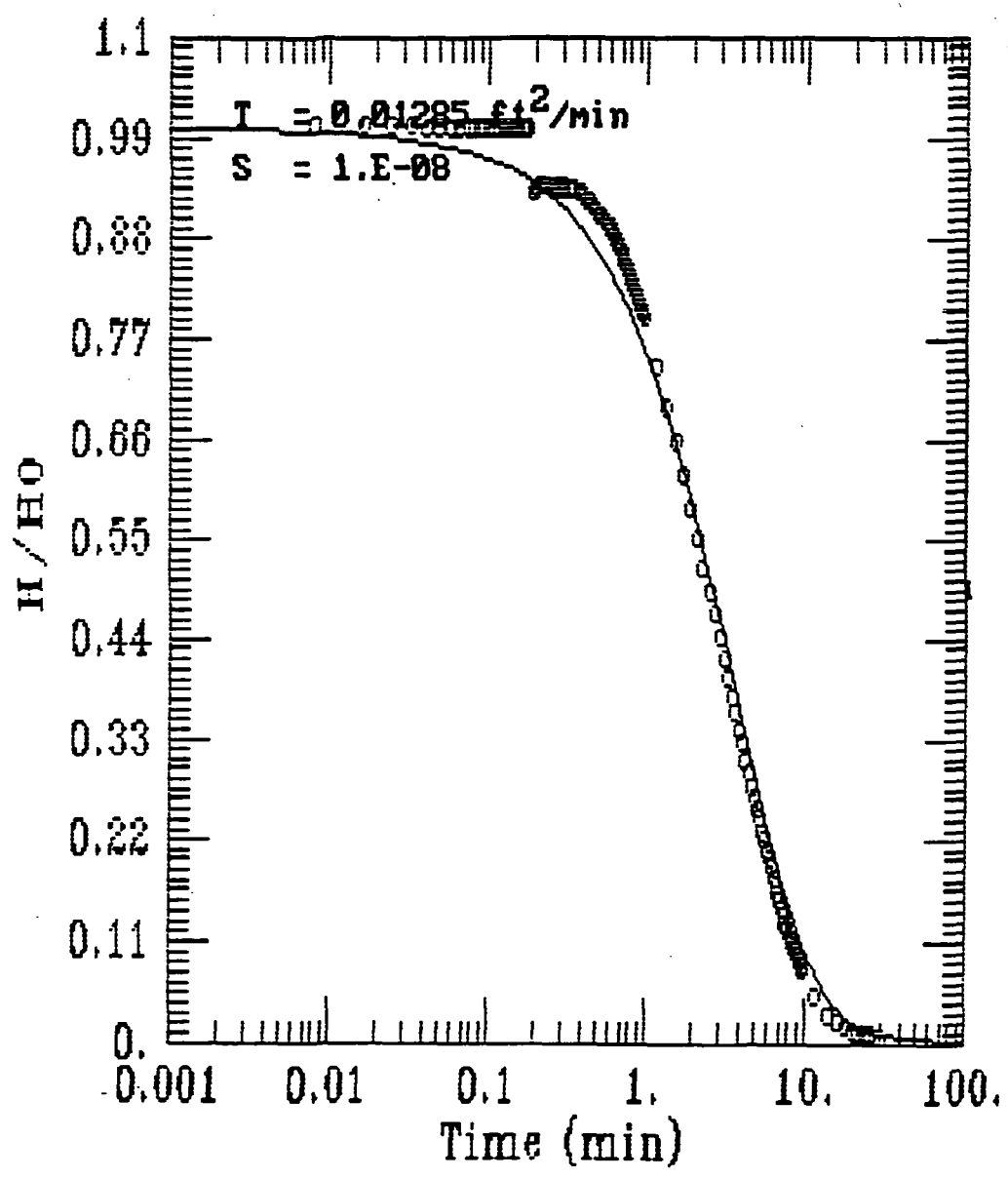


0.3333	-0.006
0.3500	-0.006
0.3666	-0.006
0.3833	-0.006
0.4000	-0.006
0.4166	-0.006
0.4333	-0.006
0.4500	-0.006
0.4666	0.000
0.4833	-0.006
0.5000	-0.006
0.5166	-0.006
0.5333	-0.006
0.5500	-0.006
0.5666	0.000
0.5833	-0.006
0.6000	-0.006
0.6166	0.000
0.6333	0.000
0.6500	-0.006
0.6666	0.000
0.6833	0.000
0.7000	0.000
0.7166	-0.006
0.7333	-0.006
0.7500	0.000
0.7666	0.000
0.7833	0.000
0.8000	-0.006
0.8166	0.000
0.8333	-0.006
0.8500	0.000
0.8666	-0.006
0.8833	-0.006
0.9000	-0.006
0.9166	-0.006
0.9333	-0.006
0.9500	-0.006
0.9666	0.000
0.9833	0.000
1.0000	-0.006
1.2000	-0.006
1.4000	-0.006
1.6000	0.000
1.8000	-0.006
2.0000	-0.006
2.2000	-0.006

WELL CLUSTER: N
WELL ID: N4-1
SCREENED INTERVAL: 32-42

TEST METHOD: Cooper et al.
SLUG IN/SLUG OUT: Slug out
K-VALUE: 1.34 ft/day

N41-T2-1



N41-1a-1.dat

0.0000	0.487
0.0083	5.794
0.0166	5.038
0.0250	2.847
0.0333	3.000
0.0416	3.012
0.0500	3.012
0.0583	3.012
0.0666	3.012
0.0750	3.006
0.0833	3.006
0.0916	3.006
0.1000	3.006
0.1083	3.006
0.1166	3.006
0.1250	3.006
0.1333	3.006
0.1416	3.006
0.1500	3.006
0.1583	3.006
0.1666	3.006
0.1750	3.000
0.1833	3.000
0.1916	3.000
0.2000	3.000
0.2083	3.000
0.2166	3.000
0.2250	2.796
0.2333	2.809
0.2416	2.815
0.2500	2.815
0.2583	2.815
0.2666	2.815
0.2750	2.815
0.2833	2.809
0.2916	2.815
0.3000	2.809
0.3083	2.809
0.3166	2.815
0.3250	2.809
0.3333	2.815
0.3500	2.809
0.3666	2.809
0.3833	2.809
0.4000	2.796
0.4166	2.790
0.4333	2.784
0.4500	2.771
0.4666	2.765
0.4833	2.752
0.5000	2.746
0.5166	2.733
0.5333	2.720
0.5500	2.714
0.5666	2.701
0.5833	2.695
0.6000	2.682
0.6166	2.676
0.6333	2.663
0.6500	2.650
0.6666	2.631
0.6833	2.625
0.7000	2.612
0.7166	2.599

to ①

Stopped @ # 5

Test:	<u>N4-1</u>	<u>Slug cut</u>
File:	<u>N41-T2-1.dat</u>	
Round:	<u>KTEST2</u>	
Column 1:	<u>Elapsed time (min)</u>	
Column 2:	<u>Head (ft)</u>	
	<u>t = 0.0333</u>	<u>t = 30.0</u>
Column 3:	<u> </u>	<u> </u>
	<u>t = _____</u>	<u>t = _____</u>

to ②

Stopped @ # 8

0.7833	2.549
0.8000	2.536
0.8166	2.523
0.8333	2.510
0.8500	2.498
0.8666	2.485
0.8833	2.466
0.9000	2.453
0.9166	2.441
0.9333	2.428
0.9500	2.415
0.9666	2.402
0.9833	2.390
1.0000	2.377
1.2000	2.225
1.4000	2.091
1.6000	1.977
1.8000	1.862
2.0000	1.754
2.2000	1.653
2.4000	1.557
2.6000	1.475
2.8000	1.405
3.0000	1.328
3.2000	1.258
3.4000	1.195
3.6000	1.138
3.8000	1.080
4.0000	1.023
4.2000	0.979
4.4000	0.928
4.6000	0.883
4.8000	0.839
5.0000	0.801
5.2000	0.763
5.4000	0.731
5.6000	0.693
5.8000	0.661
6.0000	0.629
6.2000	0.604
6.4000	0.572
6.6000	0.540
6.8000	0.515
7.0000	0.489
7.2000	0.464
7.4000	0.438
7.6000	0.413
7.8000	0.394
8.0000	0.375
8.2000	0.356
8.4000	0.343
8.6000	0.330
8.8000	0.317
9.0000	0.305
9.2000	0.292
9.4000	0.279
9.6000	0.267
9.8000	0.254
10.0000	0.241
12.0000	0.158
14.0000	0.095
16.0000	0.069
18.0000	0.050

24.0000
26.0000
28.0000
30.0000

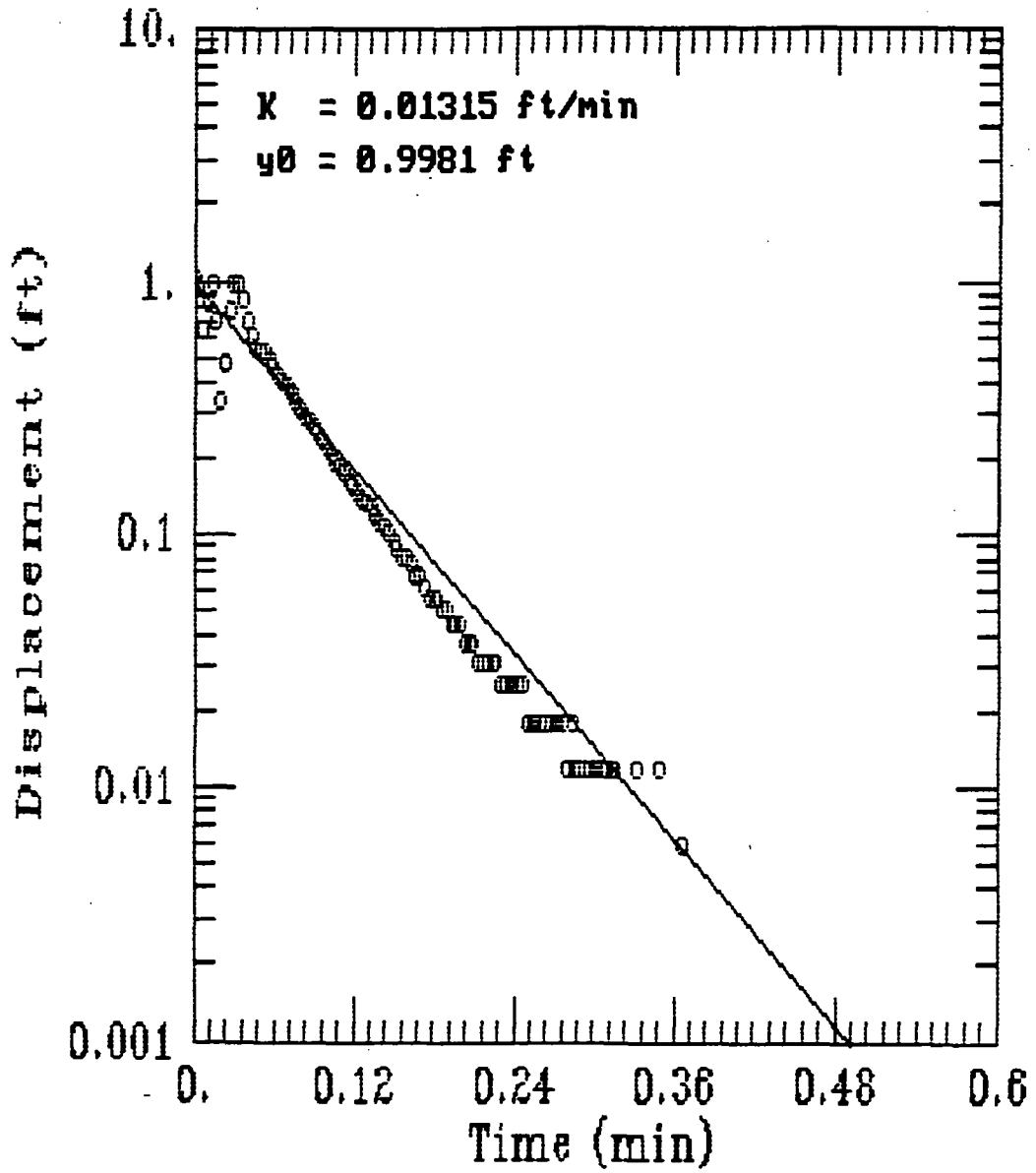
0.031
0.025
0.019
0.019

t_e

WELL CLUSTER: 0
WELL ID: 01
SCREENED INTERVAL: 11-21

TEST METHOD: Bowser-Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 18.9 ft/day

01-T2



0.0000 0.000
 0.0033 0.000
 0.0066 0.069
 0.0100 0.410
 0.0133 0.770
 0.0166 1.004
 0.0200 0.947
 0.0233 0.644
 0.0266 0.821
 0.0300 0.972
 0.0333 0.707
 0.0366 0.341
 0.0400 0.473
 0.0433 0.764
 0.0466 0.991
 0.0500 0.985
 0.0533 0.852
 0.0566 0.701
 0.0600 0.600
 0.0633 0.555
 0.0666 0.536
 0.0700 0.524
 0.0733 0.492
 0.0766 0.454
 0.0800 0.423
 0.0833 0.397
 0.0866 0.385
 0.0900 0.360
 0.0933 0.334
 0.0966 0.315
 0.1000 0.290
 0.1033 0.284
 0.1066 0.265
 0.1100 0.252
 0.1133 0.240
 0.1166 0.221
 0.1200 0.208
 0.1233 0.195
 0.1266 0.189
 0.1300 0.176
 0.1333 0.164
 0.1366 0.157
 0.1400 0.145
 0.1433 0.138
 0.1466 0.132
 0.1500 0.126
 0.1533 0.119
 0.1566 0.113
 0.1600 0.107
 0.1633 0.101
 0.1666 0.094
 0.1700 0.088
 0.1733 0.082
 0.1766 0.082
 0.1800 0.075
 0.1833 0.069
 0.1866 0.069
 0.1900 0.063
 0.1933 0.056
 0.1966 0.056
 0.2000 0.056
 0.2033 0.050
 0.2066 0.050

⑥ 01-T2-001
 to

$\Delta H = 0.998$
 $\Delta t = 0.3667$

Test:	01 Slug cut	
File:	01-T2-dat	
Round:	KTEST	
Column 1:	Elapsed time (min)	
Column 2:	Head (ft)	
	$t_b = 0.0166$	$t_c = 0.3833$
Column 3:	$t_b = \underline{\hspace{2cm}}$	$t_c = \underline{\hspace{2cm}}$

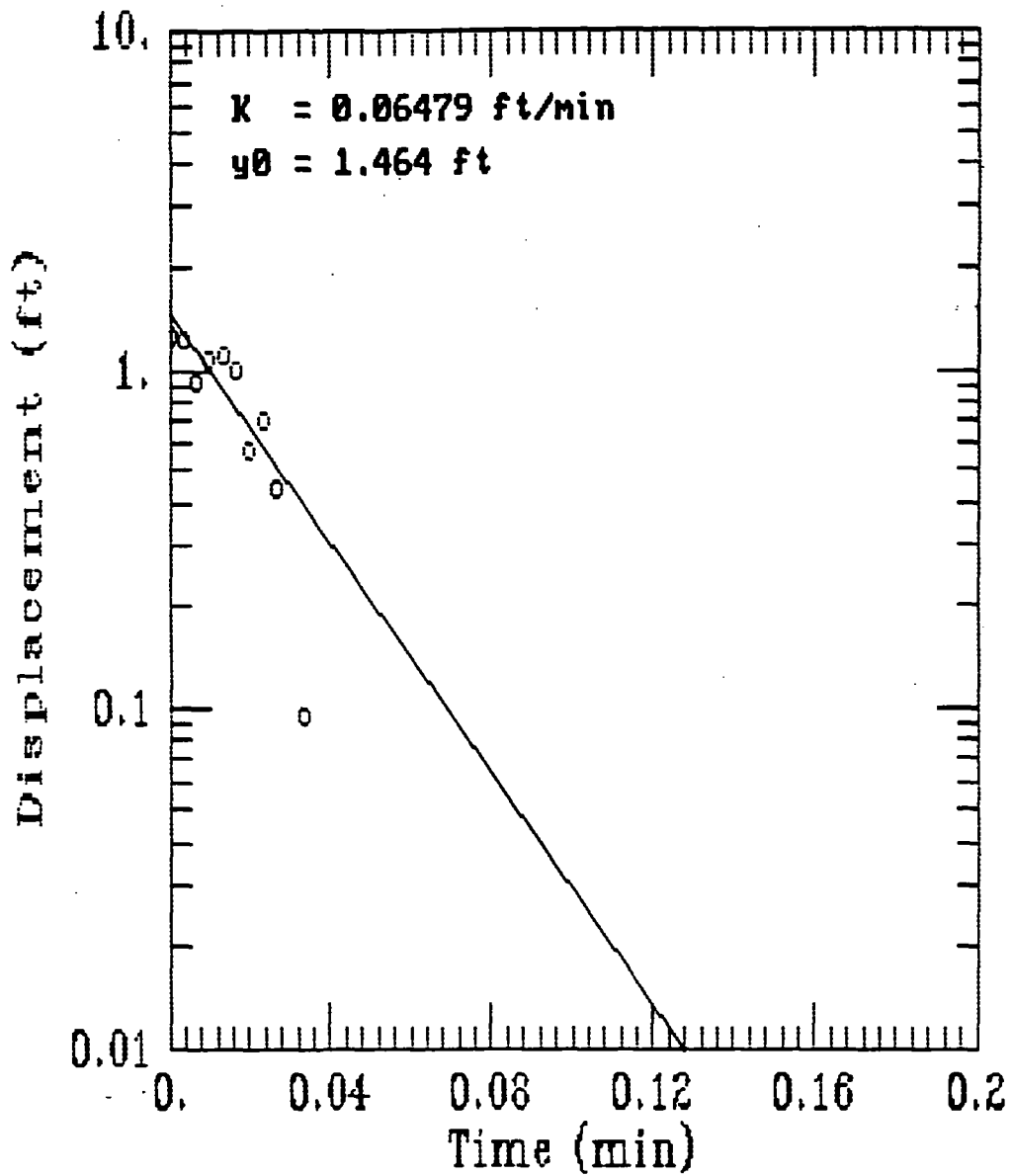
0.2200	0.037
0.2233	0.037
0.2266	0.037
0.2300	0.031
0.2333	0.031
0.2366	0.031
0.2400	0.031
0.2433	0.031
0.2466	0.025
0.2500	0.025
0.2533	0.025
0.2566	0.025
0.2600	0.025
0.2633	0.025
0.2666	0.018
0.2700	0.018
0.2733	0.018
0.2766	0.018
0.2800	0.018
0.2833	0.018
0.2866	0.018
0.2900	0.018
0.2933	0.018
0.2966	0.012
0.3000	0.018
0.3033	0.012
0.3066	0.012
0.3100	0.012
0.3133	0.012
0.3166	0.012
0.3200	0.012
0.3233	0.012
0.3266	0.012
0.3300	0.012
0.3333	0.012
0.3366	0.012
0.3400	0.012
0.3433	0.012
0.3466	0.012
0.3500	0.012
0.3533	0.012
0.3566	0.012
0.3600	0.006
0.3633	0.006
0.3666	0.006
0.3700	0.006
0.3733	0.006
0.3766	0.006
0.3800	0.006
0.3833	0.006
0.3866	0.006
0.3900	0.006
0.3933	0.006
0.3966	0.006
0.4000	0.006
0.4033	0.006
0.4066	0.006
0.4100	0.006
0.4133	0.006
0.4166	0.006
0.4200	0.006
0.4233	0.006
0.4266	0.006
0.4300	0.006
0.4333	0.006
0.4366	0.006
0.4400	0.006
0.4433	0.006
0.4466	0.006
0.4500	0.006
0.4533	0.006
0.4566	0.006
0.4600	0.006
0.4633	0.006
0.4666	0.006
0.4700	0.006
0.4733	0.006
0.4766	0.006
0.4800	0.006
0.4833	0.006
0.4866	0.006
0.4900	0.006
0.4933	0.006
0.4966	0.006
0.5000	0.006
0.5033	0.006
0.5066	0.006
0.5100	0.006
0.5133	0.006
0.5166	0.006
0.5200	0.006
0.5233	0.006
0.5266	0.006
0.5300	0.006
0.5333	0.006
0.5366	0.006
0.5400	0.006
0.5433	0.006
0.5466	0.006
0.5500	0.006
0.5533	0.006
0.5566	0.006
0.5600	0.006
0.5633	0.006
0.5666	0.006
0.5700	0.006
0.5733	0.006
0.5766	0.006
0.5800	0.006
0.5833	0.006
0.5866	0.006
0.5900	0.006
0.5933	0.006
0.5966	0.006
0.6000	0.006
0.6033	0.006
0.6066	0.006
0.6100	0.006
0.6133	0.006
0.6166	0.006
0.6200	0.006
0.6233	0.006
0.6266	0.006
0.6300	0.006
0.6333	0.006
0.6366	0.006
0.6400	0.006
0.6433	0.006
0.6466	0.006
0.6500	0.006
0.6533	0.006
0.6566	0.006
0.6600	0.006
0.6633	0.006
0.6666	0.006
0.6700	0.006
0.6733	0.006
0.6766	0.006
0.6800	0.006
0.6833	0.006
0.6866	0.006
0.6900	0.006
0.6933	0.006
0.6966	0.006
0.7000	0.006
0.7033	0.006
0.7066	0.006
0.7100	0.006
0.7133	0.006
0.7166	0.006
0.7200	0.006
0.7233	0.006
0.7266	0.006
0.7300	0.006
0.7333	0.006
0.7366	0.006
0.7400	0.006
0.7433	0.006
0.7466	0.006
0.7500	0.006
0.7533	0.006
0.7566	0.006
0.7600	0.006
0.7633	0.006
0.7666	0.006
0.7700	0.006
0.7733	0.006
0.7766	0.006
0.7800	0.006
0.7833	0.006
0.7866	0.006
0.7900	0.006
0.7933	0.006
0.7966	0.006
0.8000	0.006
0.8033	0.006
0.8066	0.006
0.8100	0.006
0.8133	0.006
0.8166	0.006
0.8200	0.006
0.8233	0.006
0.8266	0.006
0.8300	0.006
0.8333	0.006
0.8366	0.006
0.8400	0.006
0.8433	0.006
0.8466	0.006
0.8500	0.006
0.8533	0.006
0.8566	0.006
0.8600	0.006
0.8633	0.006
0.8666	0.006
0.8700	0.006
0.8733	0.006
0.8766	0.006
0.8800	0.006
0.8833	0.006
0.8866	0.006
0.8900	0.006
0.8933	0.006
0.8966	0.006
0.9000	0.006
0.9033	0.006
0.9066	0.006
0.9100	0.006
0.9133	0.006
0.9166	0.006
0.9200	0.006
0.9233	0.006
0.9266	0.006
0.9300	0.006
0.9333	0.006
0.9366	0.006
0.9400	0.006
0.9433	0.006
0.9466	0.006
0.9500	0.006
0.9533	0.006
0.9566	0.006
0.9600	0.006
0.9633	0.006
0.9666	0.006
0.9700	0.006
0.9733	0.006
0.9766	0.006
0.9800	0.006
0.9833	0.006
0.9866	0.006
0.9900	0.006
0.9933	0.006
0.9966	0.006
1.0000	0.006

0.8666	0.006
0.8833	0.006
0.9000	0.006
0.9166	0.006
0.9333	0.006
0.9500	0.006
0.9666	0.006
0.9833	0.006
1.0000	0.006
1.2000	0.006
1.4000	0.000
1.6000	0.000
1.8000	0.000
2.0000	0.000
2.2000	0.000
2.4000	0.000
2.6000	0.000
2.8000	0.000
3.0000	0.000
3.2000	0.000
3.4000	0.000
3.6000	0.000
3.8000	0.006
4.0000	0.006
4.2000	0.006
4.4000	0.000
4.6000	0.000
4.8000	0.000
5.0000	0.006
5.2000	0.000
5.4000	0.000
5.6000	0.000
5.8000	0.000
6.0000	0.000
6.2000	0.000
6.4000	0.000
6.6000	0.000
6.8000	0.006
7.0000	0.012
7.2000	0.012
7.4000	0.012
7.6000	0.012
7.8000	0.012
8.0000	0.012
8.2000	0.012
8.4000	0.012
8.6000	0.012
8.8000	0.012
9.0000	0.006
9.2000	0.006
9.4000	0.012
9.6000	0.012
9.8000	0.012
10.0000	0.012

WELL CLUSTER: 0
WELL ID: 02
SCREENED INTERVAL: 24-29

TEST METHOD: Runner Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 93.3 ft/day

02-T2



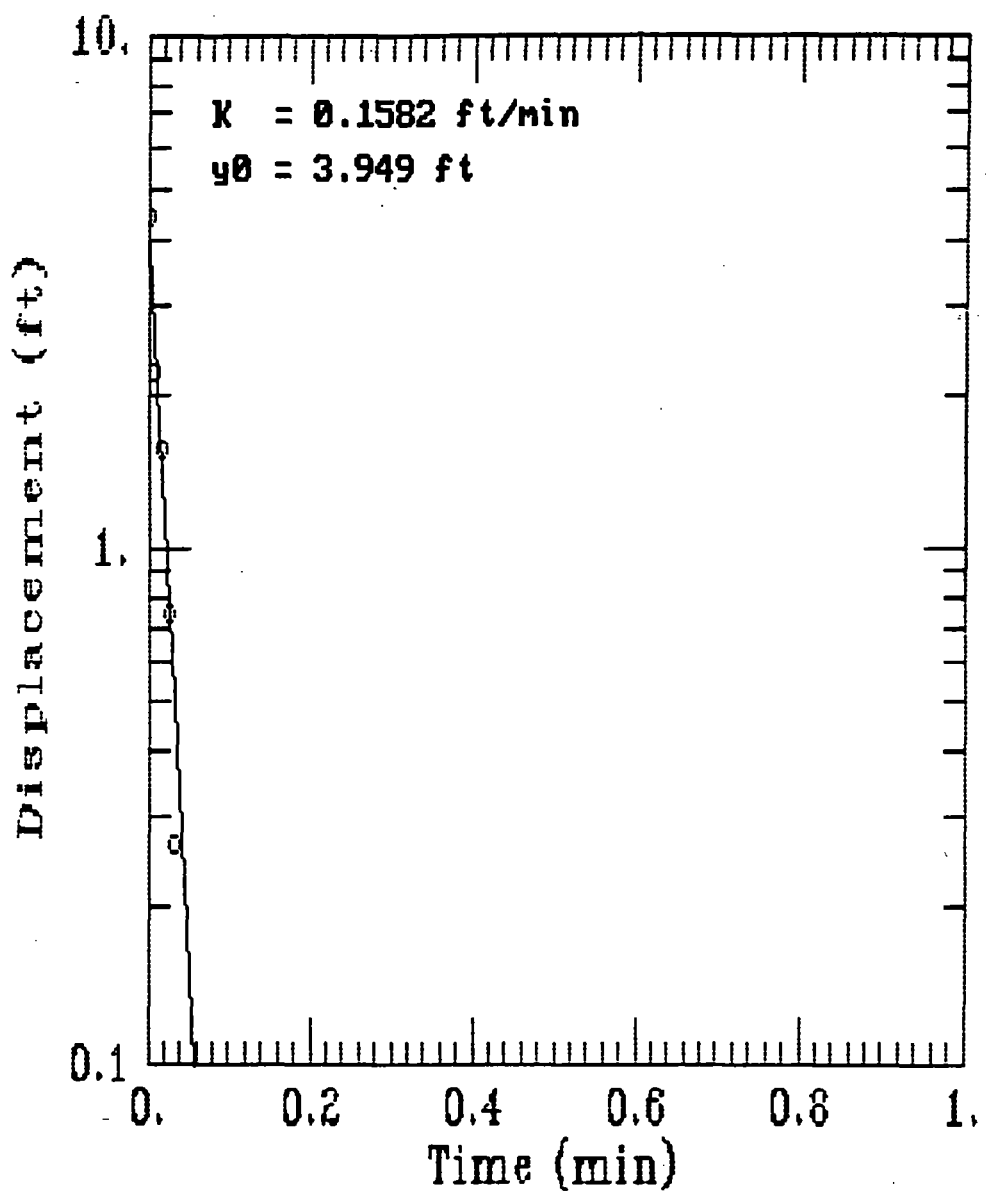
0.2200	0.037
0.2233	0.031
0.2266	0.025
0.2300	0.018
0.2333	0.012
0.2366	0.006
0.2400	0.006
0.2433	0.006
0.2466	0.006
0.2500	0.006
0.2533	0.006
0.2566	0.006
0.2600	0.006
0.2633	0.012
0.2666	0.012
0.2700	0.018
0.2733	0.018
0.2766	0.025
0.2800	0.025
0.2833	0.025
0.2866	0.031
0.2900	0.031
0.2933	0.031
0.2966	0.031
0.3000	0.031
0.3033	0.031
0.3066	0.031
0.3100	0.025
0.3133	0.025
0.3166	0.025
0.3200	0.025
0.3233	0.018
0.3266	0.018
0.3300	0.018
0.3333	0.018
0.3500	0.018
0.3666	0.018
0.3833	0.018
0.4000	0.018
0.4166	0.018
0.4333	0.018
0.4500	0.018
0.4666	0.018
0.4833	0.018
0.5000	0.018
0.5166	0.018
0.5333	0.012
0.5500	0.012
0.5666	0.018
0.5833	0.018
0.6000	0.018
0.6166	0.018
0.6333	0.018
0.6500	0.012
0.6666	0.018
0.6833	0.018
0.7000	0.012
0.7166	0.018
0.7333	0.018
0.7500	0.018
0.7666	0.012
0.7833	0.018
0.8000	0.012
0.8166	0.018

0.8833	0.018
0.9000	0.018
0.9166	0.018
0.9333	0.018
0.9500	0.012
0.9666	0.012
0.9833	0.012
1.0000	0.012
1.2000	0.012
1.4000	0.012
1.6000	0.012
1.8000	0.012
2.0000	0.006
2.2000	0.006
2.4000	0.012
2.6000	0.012
2.8000	0.006
3.0000	0.006
3.2000	0.012
3.4000	0.012
3.6000	0.012
3.8000	0.006
4.0000	0.006
4.2000	0.012
4.4000	0.006
4.6000	0.012
4.8000	0.012
5.0000	0.012
5.2000	0.006
5.4000	0.000
5.6000	0.000
5.8000	0.000
6.0000	0.006
6.2000	0.012
6.4000	0.012
6.6000	0.012
6.8000	0.012
7.0000	0.012
7.2000	0.012
7.4000	0.012
7.6000	0.006
7.8000	0.006
8.0000	0.006
8.2000	0.006
8.4000	0.006
8.6000	0.012
8.8000	0.012
9.0000	0.006
9.2000	0.006
9.4000	0.012
9.6000	0.006
9.8000	0.012
10.0000	0.006

WELL CLUSTER: 0
WELL ID: 03-1
SCREENED INTERVAL: 36.75-41.75

TEST METHOD: Bunker Rice
SLUG IN/SLUG OUT: Slug out
K-VALUE: 228 ft/day

03-T2



SE2000
 Environmental Logger
 08/23 08:36

PTN ✓

03-T2

Unit# 22 Test 13

Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. 204363

 Reference 0.000
 SB 1.000
 Linearity 0.152
 Scale factor 19.970
 Offset 0.061
 Delay mSEC 50.000

Step 0 08/22 11:10:03

Elapsed Time	INPUT 1
0.0000	-0.006
0.0083	0.000
0.0166	-0.006
0.0250	-0.006
0.0333	0.000
0.0416	0.000
0.0500	-0.006
0.0583	-0.006
0.0666	0.176
0.0750	4.427 ✓
0.0833	2.217
0.0916	1.573
0.1000	0.745
0.1083	0.265 ✓
0.1166	-0.012 ✓
0.1250	-0.164
0.1333	-0.233
0.1416	-0.126
0.1500	-0.107
0.1583	-0.088
0.1666	-0.056
0.1750	-0.031
0.1833	-0.012
0.1916	-0.006
0.2000	0.000
0.2083	0.000
0.2166	0.000
0.2250	-0.006
0.2333	-0.012
0.2416	-0.012
0.2500	-0.012
0.2583	-0.012
0.2666	-0.012
0.2750	-0.006
0.2833	-0.012
0.2916	-0.012
0.3000	-0.012
0.3083	-0.006

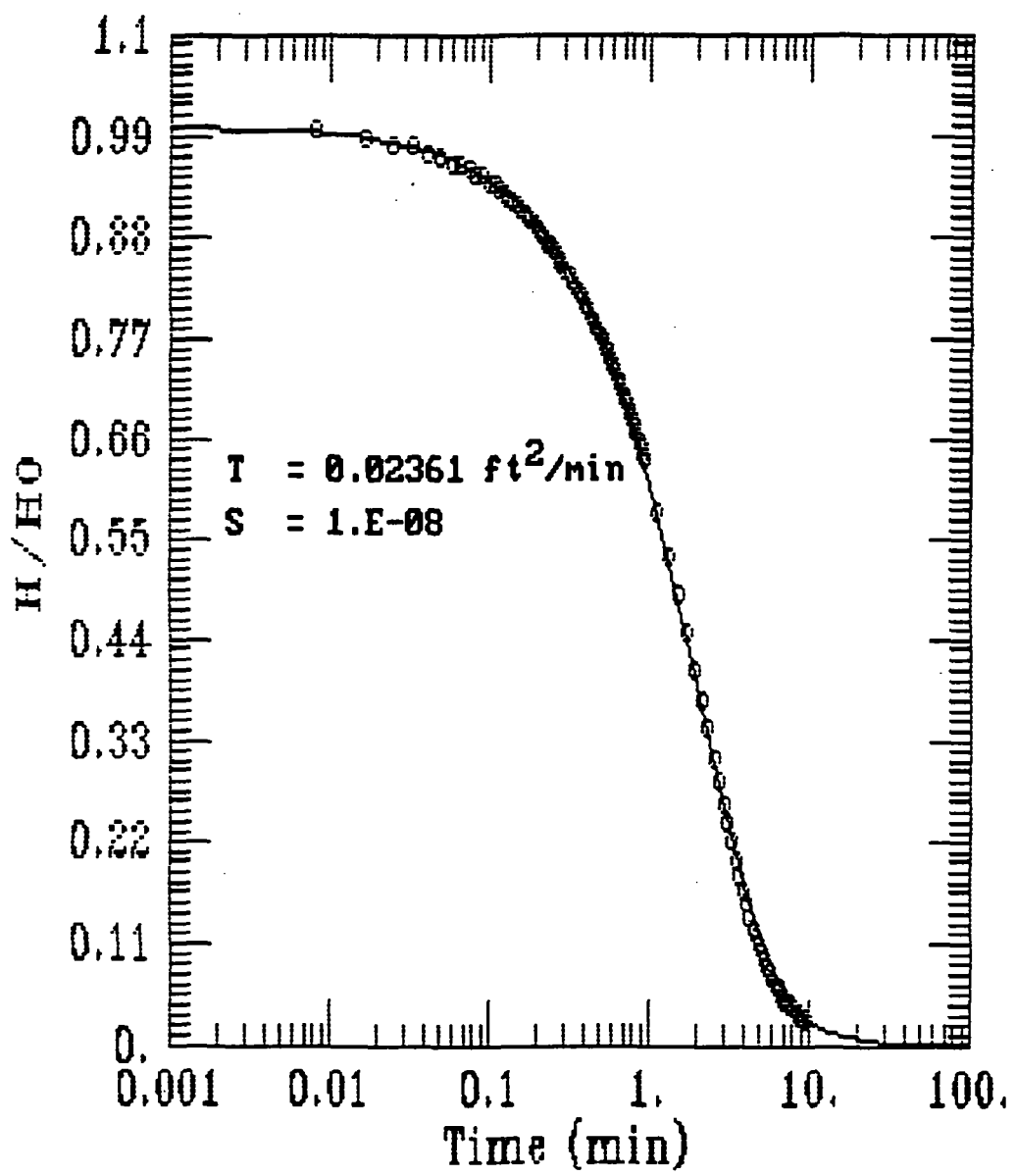
Test:	<u>02-1 Slug out</u>
File:	<u>03-T2</u>
Round:	<u>KTEST3</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head (ft)</u>
	<u>t₀ = 0.0750 t₁ = 0.1166</u>
Column 3:	<u>_____</u>
	<u>t₀ = _____ t₁ = _____</u>

0.3333	-0.006
0.3500	-0.006
0.3666	-0.012
0.3833	-0.006
0.4000	-0.006
0.4166	-0.006
0.4333	-0.012
0.4500	-0.006
0.4666	-0.006
0.4833	-0.006
0.5000	-0.006
0.5166	-0.006
0.5333	-0.006
0.5500	-0.006
0.5666	-0.006
0.5833	-0.006
0.6000	-0.006
0.6166	-0.006
0.6333	-0.006
0.6500	-0.006
0.6666	-0.006
0.6833	-0.006
0.7000	-0.006
0.7166	-0.006
0.7333	-0.006
0.7500	-0.006
0.7666	-0.006
0.7833	-0.006
0.8000	-0.006
0.8166	-0.006
0.8333	-0.006
0.8500	-0.006
0.8666	-0.006
0.8833	-0.012
0.9000	-0.006
0.9166	-0.006
0.9333	-0.006
0.9500	-0.006
0.9666	-0.006
0.9833	-0.006
1.0000	-0.006
1.2000	-0.006
1.4000	-0.006

WELL CLUSTER: 0
WELL ID: 04-1
SCREENED INTERVAL: 46-56

TEST METHOD: Cooper et al.
SLUG IN/SLUG OUT: Slug out
K-VALUE: 2-20 ft/day

04-T2-1



0.0083	0.006	0.804
0.0166	0.000	0.991
0.0250	0.000	0.399
0.0333	0.922	0.836
0.0416	2.638	1.656
0.0500	-0.273	1.840
0.0583	4.137	1.831
0.0666	2.530	1.818
0.0750	0.616	1.805
0.0833	0.108	1.799
0.0916	-0.152	1.786
0.1000	-0.254	1.783
0.1083	-0.235	1.764
0.1166	-0.216	1.761
0.1250	-0.178	1.758
0.1333	-0.082	1.745
0.1416	-0.025	1.739
0.1500	0.006	1.729
0.1583	0.044	1.723
0.1666	0.038	1.713
0.1750	0.050	1.704
0.1833	0.050	1.694
0.1916	0.076	1.691
0.2000	0.057	1.682
0.2083	0.000	1.675
0.2166	0.000	1.666
0.2250	-0.006	1.660
0.2333	0.000	1.650
0.2416	0.000	1.644
0.2500	0.000	1.637
0.2583	0.000	1.628
0.2666	0.000	1.622
0.2750	0.000	1.615
0.2833	0.006	1.609
0.2916	0.006	1.603
0.3000	0.006	1.596
0.3083	0.006	1.587
0.3166	0.006	1.580
0.3250	0.006	1.577
0.3333	0.006	1.568
0.3500	0.006	1.555
0.3666	0.006	1.542
0.3833	0.006	1.533
0.4000	0.006	1.520
0.4166	0.006	1.508
0.4333	0.006	1.498
0.4500	0.006	1.485
0.4666	0.006	1.476
0.4833	0.006	1.463
0.5000	0.006	1.451
0.5166	0.006	1.441
0.5333	0.006	1.432
0.5500	0.006	1.422
0.5666	0.006	1.412
0.5833	0.006	1.403
0.6000	0.006	1.390
0.6166	0.006	1.381
0.6333	0.006	1.371
0.6500	0.006	1.362
0.6666	0.006	1.352
0.6833	0.006	1.343
0.7000	0.006	1.330
0.7166	0.006	1.321

0.307
 Hopped @ # 11

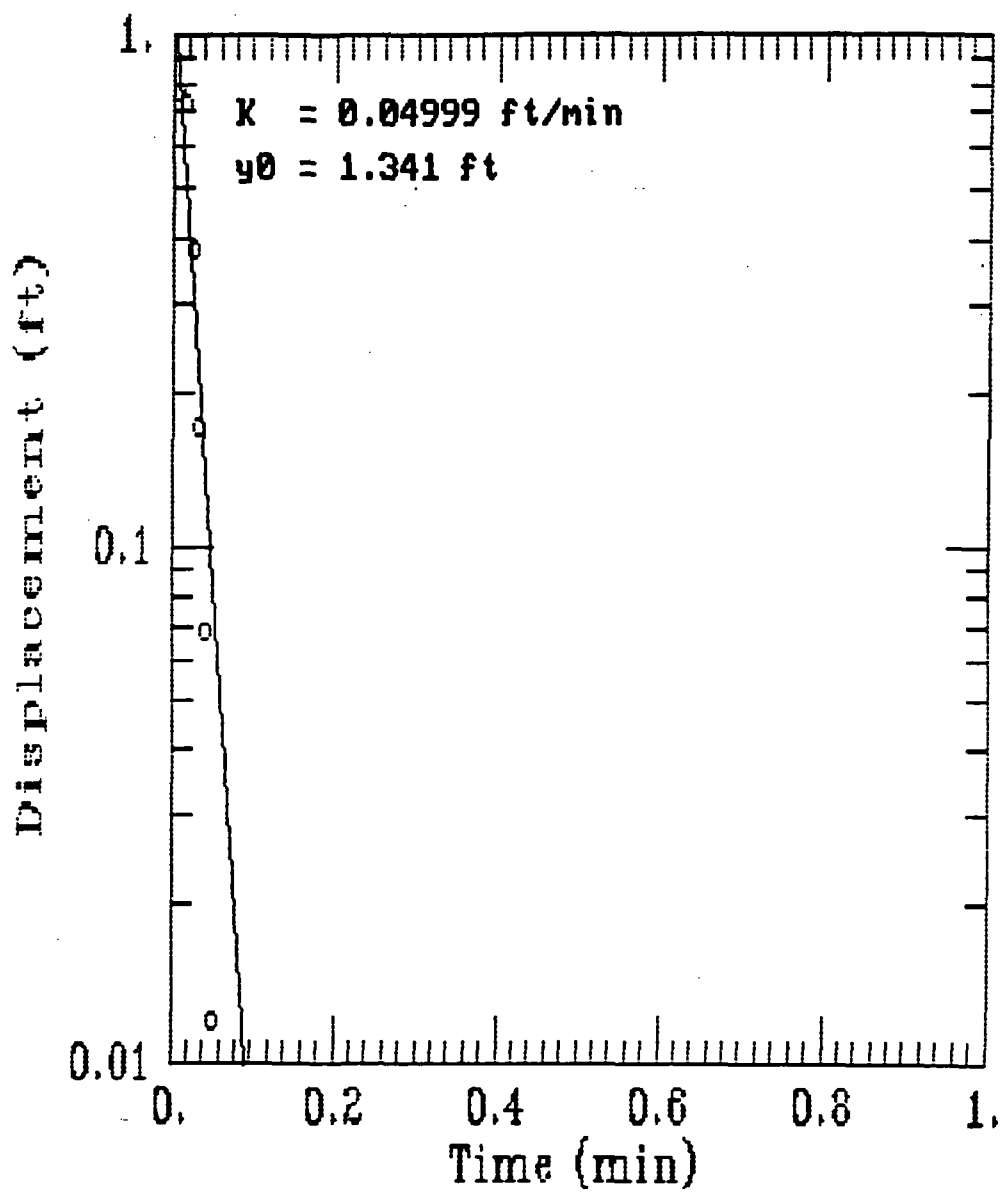
Test:	<u>03-1.04-1 Slug out</u>
File:	<u>0304-T2-dat</u>
Round:	<u>KTEST2</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head (ft) C3-1</u>
	<u>t = N/A t = N/A</u>
Column 3:	<u>Head (ft) C4-1</u>
	<u>t = 0.0500 t = 9.8</u>

0.7888	0.006	1.272
0.7833	0.006	1.283
0.8000	0.006	1.273
0.8166	0.006	1.264
0.8333	0.006	1.254
0.8500	0.006	1.245
0.8666	0.006	1.238
0.8833	0.006	1.229
0.9000	0.006	1.219
0.9166	0.006	1.210
0.9333	0.006	1.203
0.9500	0.006	1.194
0.9666	0.006	1.184
0.9833	0.006	1.175
1.0000	0.006	1.169
1.2000	0.006	1.070
1.4000	0.006	0.978
1.6000	0.006	0.896
1.8000	0.006	0.820
2.0000	0.006	0.750
2.2000	0.006	0.687
2.4000	0.006	0.630
2.6000	0.006	0.576
2.8000	0.006	0.529
3.0000	0.006	0.484
3.2000	0.006	0.443
3.4000	0.012	0.405
3.6000	0.006	0.370
3.8000	0.006	0.339
4.0000	0.006	0.310
4.2000	0.006	0.281
4.4000	0.006	0.256
4.6000	0.006	0.234
4.8000	0.006	0.215
5.0000	0.006	0.199
5.2000	0.006	0.183
5.4000	0.006	0.171
5.6000	0.012	0.158
5.8000	0.012	0.148
6.0000	0.012	0.136
6.2000	0.012	0.129
6.4000	0.012	0.120
6.6000	0.012	0.114
6.8000	0.012	0.104
7.0000	0.012	0.098
7.2000	0.012	0.091
7.4000	0.012	0.088
7.6000	0.012	0.085
7.8000	0.012	0.082
8.0000	0.012	0.076
8.2000	0.012	0.072
8.4000	0.012	0.069
8.6000	0.012	0.066
8.8000	0.012	0.063
9.0000	0.012	0.060
9.2000	0.012	0.060
9.4000	0.019	0.060
9.6000	0.012	0.057
9.8000	0.012	0.053

WELL CLUSTER: P
WELL ID: D1
SCREENED INTERVAL: 7-17

TEST METHOD: Bowser Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 72.0 ft/day

P1-T2



PRN ✓

P1-T2

Unit# 22 Test 11

 Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. 204363
 Reference 0.000
 SG 1.000
 Linearity 0.152
 Scale factor 19.970
 Offset -0.061
 Delay mSEC 50.000

Test:	P1	Slug out
File:	P1-T2	
Round:	KTEST3	
Column 1:	Elapsed time (min)	
Column 2:	Head (ft)	
	t = 0.0583	t = 2.1166
Column 3:		
	t =	t =

Step 0 08/22 10:39:37

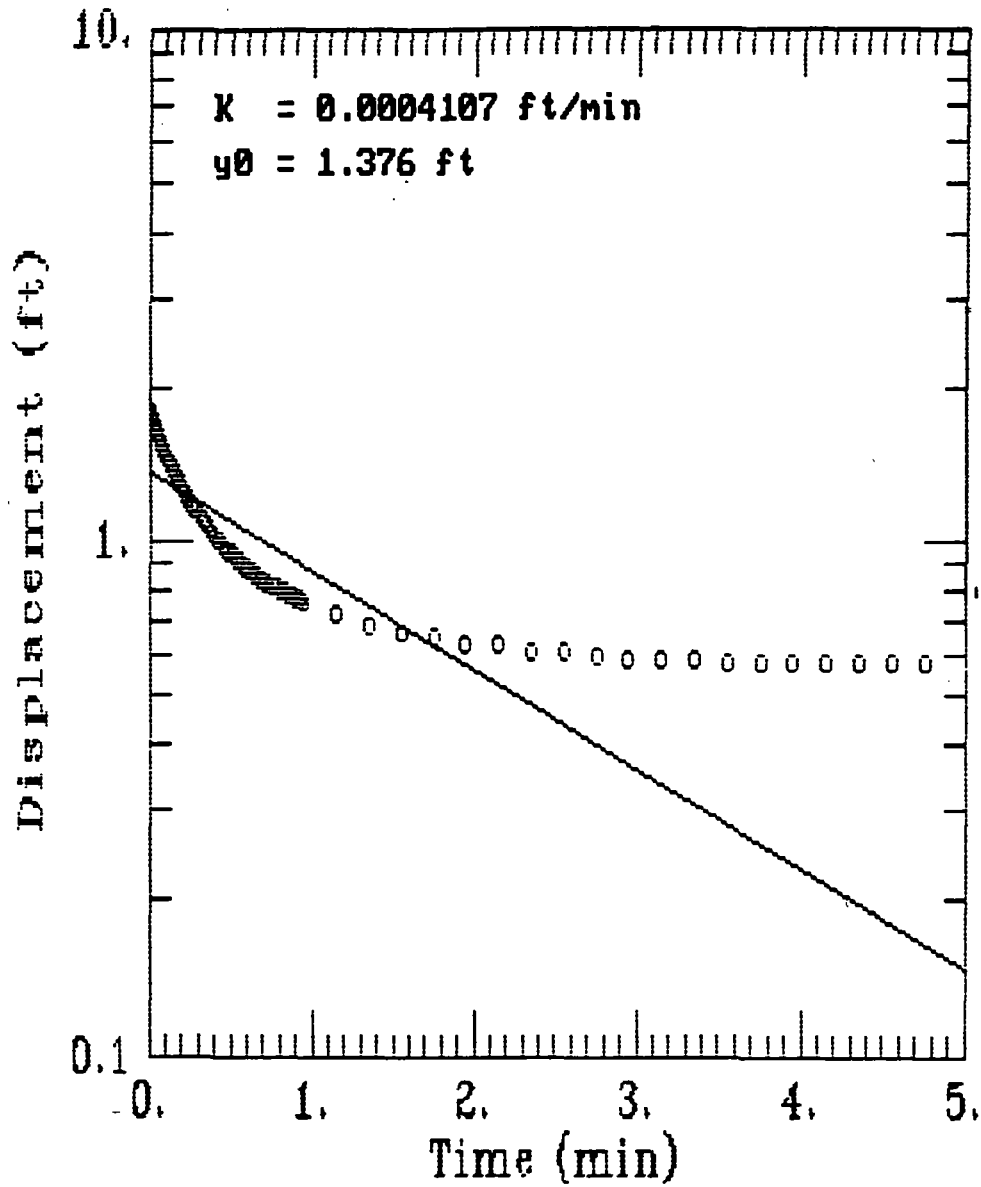
Elapsed Time	INPUT 1
0.0000	0.000
0.0083	0.000
0.0166	0.000
0.0250	0.000
0.0333	0.000
0.0416	0.000
0.0500	1.547
0.0583	1.642 ✓
0.0666	0.770
0.0750	0.732
0.0833	0.379
0.0916	0.170
0.1000	0.069
0.1083	0.012
0.1166	-0.006 ✓ @ 0.000
0.1250	-0.018
0.1333	-0.012
0.1416	-0.012
0.1500	-0.006
0.1583	-0.006
0.1666	-0.012
0.1750	-0.012
0.1833	-0.006
0.1916	-0.006
0.2000	-0.006
0.2083	-0.006
0.2166	-0.006
0.2250	-0.006
0.2333	-0.006
0.2416	-0.006
0.2500	-0.006
0.2583	-0.006
0.2666	-0.006
0.2750	-0.006
0.2833	-0.006
0.2916	-0.006
0.3000	-0.006

0.3333	-0.006
0.3500	-0.006
0.3666	-0.006
0.3833	-0.006
0.4000	-0.006
0.4166	-0.006
0.4333	-0.006
0.4500	-0.006
0.4666	-0.006
0.4833	0.000
0.5000	-0.006
0.5166	-0.006
0.5333	0.000
0.5500	-0.006
0.5666	0.000
0.5833	-0.006
0.6000	-0.006
0.6166	0.000
0.6333	0.000
0.6500	0.000
0.6666	-0.006
0.6833	-0.006
0.7000	-0.006
0.7166	0.000
0.7333	0.000
0.7500	-0.006
0.7666	0.000
0.7833	0.000
0.8000	0.000
0.8166	0.000
0.8333	0.000
0.8500	0.000
0.8666	0.000
0.8833	0.000
0.9000	0.000
0.9166	0.000
0.9333	0.000
0.9500	0.000
0.9666	0.000
0.9833	0.000
1.0000	0.000
1.2000	0.000
1.4000	0.000
1.6000	-0.006
1.8000	-0.006

WELL CLUSTER: Q
WELL ID: Q1
SCREENED INTERVAL: 17-27

TEST METHOD: Bauer Rice
SLUG IN/SLUG OUT: slug ext
K-VALUE: 0.591 ft/day

Q1-T2-1



0.0083	0.003	-0.006
0.0166	0.925	2.874
0.0250	1.083	3.008
0.0333	0.893	1.743
0.0416	1.698	2.506
0.0500	1.812	1.857
0.0583	1.767	1.863
0.0666	1.729	1.768
0.0750	1.701	1.673
0.0833	1.688	1.603
0.0916	1.644	1.539
0.1000	1.618	1.463
0.1083	1.593	1.399
0.1166	1.568	1.348
0.1250	1.542	1.291
0.1333	1.520	1.240
0.1416	1.498	1.189
0.1500	1.476	1.145
0.1583	1.457	1.100
0.1666	1.438	1.056
0.1750	1.419	1.018
0.1833	1.400	0.979
0.1916	1.381	0.941
0.2000	1.365	0.903
0.2083	1.346	0.871
0.2166	1.333	0.839
0.2250	1.317	0.808
0.2333	1.302	0.782
0.2416	1.286	0.750
0.2500	1.273	0.725
0.2583	1.260	0.699
0.2666	1.248	0.674
0.2750	1.232	0.649
0.2833	1.219	0.623
0.2916	1.207	0.604
0.3000	1.194	0.585
0.3083	1.181	0.566
0.3166	1.172	0.540
0.3250	1.159	0.521
0.3333	1.150	0.509
0.3500	1.127	0.470
0.3666	1.108	0.445
0.3833	1.093	0.413
0.4000	1.074	0.388
0.4166	1.055	0.362
0.4333	1.039	0.337
0.4500	1.023	0.318
0.4666	1.010	0.299
0.4833	0.998	0.279
0.5000	0.982	0.260
0.5166	0.969	0.248
0.5333	0.956	0.235
0.5500	0.947	0.216
0.5666	0.934	0.203
0.5833	0.925	0.190
0.6000	0.915	0.178
0.6166	0.902	0.171
0.6333	0.896	0.165
0.6500	0.887	0.152
0.6666	0.877	0.146
0.6833	0.871	0.133
0.7000	0.861	0.127
0.7166	0.855	0.121

(8) Q1 Q2 - T2 - det

Q1 $\Delta H = 1.122$
 $\Delta t = 1.35$

Q2 $\Delta H = 2.5$
 $\Delta t = 1.9584$

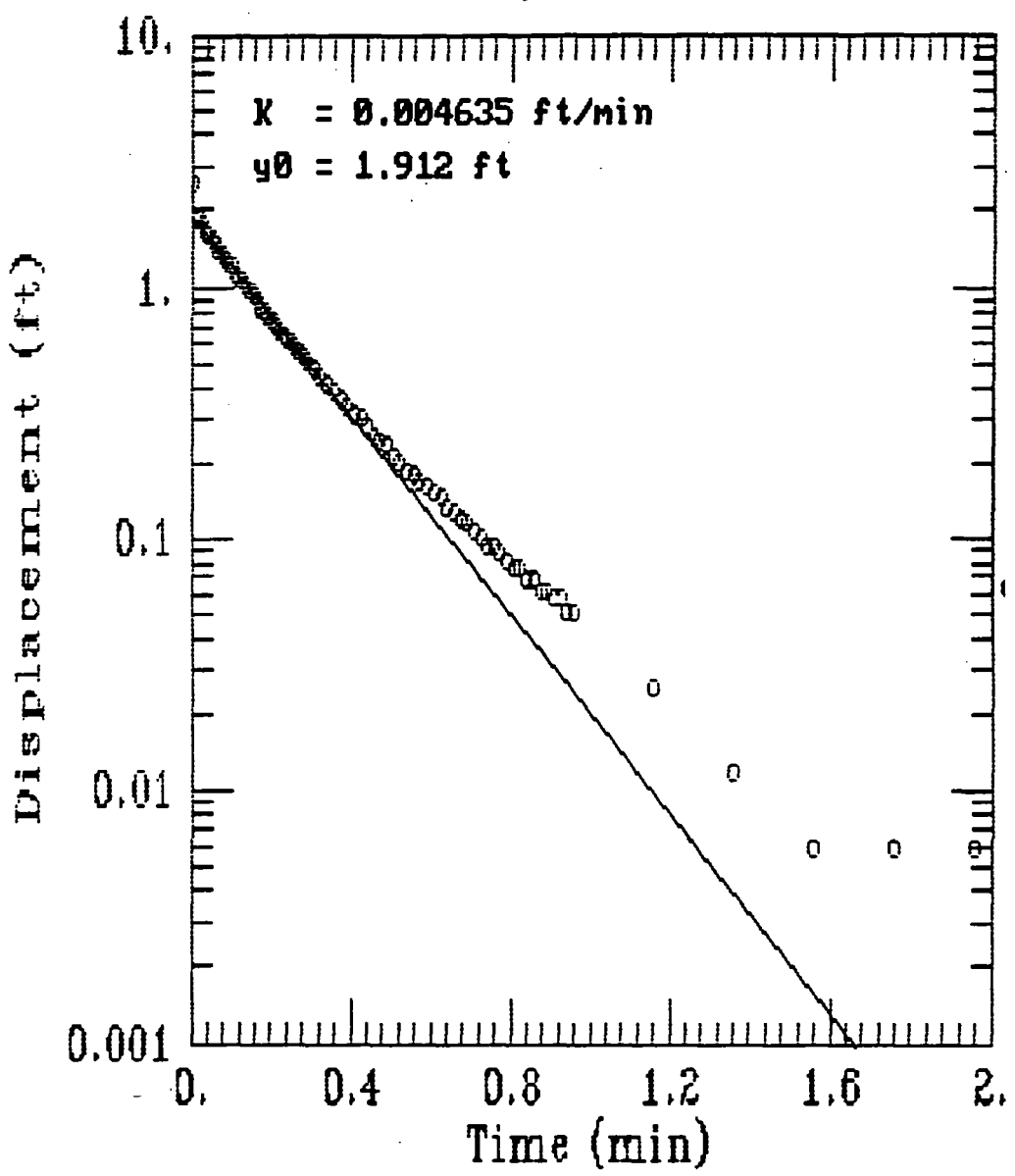
Test:	<u>Q1 Q2 Slug out</u>
File:	<u>Q1 Q2 - T2 - det</u>
Round:	<u>KTEST2</u>
Column 1:	<u>Elapsed time (min)</u>
Column 2:	<u>Head Q1 (ft)</u>
	$t = \underline{0.0500} \quad t = \underline{1.40}$
Column 3:	<u>Head Q2 (ft)</u>
	$t = \underline{0.0416} \quad t = \underline{2.00}$

0.7666	0.833	0.101
0.7833	0.826	0.095
0.8000	0.820	0.095
0.8166	0.817	0.089
0.8333	0.811	0.082
0.8500	0.804	0.076
0.8666	0.801	0.076
0.8833	0.795	0.069
0.9000	0.788	0.069
0.9166	0.785	0.063
0.9333	0.782	0.063
0.9500	0.776	0.057
0.9666	0.773	0.057
0.9833	0.769	0.050
1.0000	0.763	0.050
1.2000	0.722	0.025
1.4000	0.690	0.012
1.6000	0.665	0.006
1.8000	0.646	0.006
2.0000	0.633	0.006
2.2000	0.624	0.000
2.4000	0.611	0.000
2.6000	0.605	0.000
2.8000	0.598	-0.006
3.0000	0.589	-0.006
3.2000	0.589	-0.006
3.4000	0.586	-0.006
3.6000	0.579	-0.006
3.8000	0.579	-0.006
4.0000	0.576	-0.006
4.2000	0.576	-0.006
4.4000	0.573	-0.006
4.6000	0.573	-0.006
4.8000	0.573	-0.006
5.0000	0.570	-0.006
5.2000	0.567	-0.012
5.4000	0.567	-0.006
5.6000	0.567	-0.006
5.8000	0.567	-0.012
6.0000	0.567	-0.012
6.2000	0.563	-0.006
6.4000	0.563	-0.006
6.6000	0.563	-0.012
6.8000	0.563	-0.012
7.0000	0.563	-0.012
7.2000	0.563	-0.006
7.4000	0.563	-0.006
7.6000	0.563	-0.006
7.8000	0.563	-0.006
8.0000	-0.563	-0.006
8.2000	0.563	-0.006
8.4000	0.563	-0.006
8.6000	0.563	-0.006
8.8000	0.570	-0.012
9.0000	0.563	-0.006
9.2000	0.563	-0.006
9.4000	0.563	-0.006
9.6000	0.563	-0.006
9.8000	0.560	-0.006
10.0000	0.563	-0.006
12.0000	0.560	-0.006
14.0000	0.560	-0.006
16.0000	0.560	-0.006
17.0000	0.560	-0.006

WELL CLUSTER: Q
WELL ID: Q2
SCREENED INTERVAL: 17-27

TEST METHOD: Bowser Rice
SLUG IN/SLUG OUT: Slug out
K-VALUE: 6.67 ft/day

Q2-T2-1



Q1 Q2 - T2 - det

0.0083	0.003	-0.006
0.0166	0.925	2.874
0.0250	1.083	3.008
0.0333	0.893	1.743
0.0416	1.698	2.506
0.0500	1.812	1.857
0.0583	1.767	1.863
0.0666	1.729	1.768
0.0750	1.701	1.673
0.0833	1.688	1.603
0.0916	1.644	1.539
0.1000	1.618	1.463
0.1083	1.593	1.399
0.1166	1.568	1.348
0.1250	1.542	1.291
0.1333	1.520	1.240
0.1416	1.498	1.189
0.1500	1.476	1.145
0.1583	1.457	1.100
0.1666	1.438	1.056
0.1750	1.419	1.018
0.1833	1.400	0.979
0.1916	1.381	0.941
0.2000	1.365	0.903
0.2083	1.346	0.871
0.2166	1.333	0.839
0.2250	1.317	0.808
0.2333	1.302	0.782
0.2416	1.286	0.750
0.2500	1.273	0.725
0.2583	1.260	0.699
0.2666	1.248	0.674
0.2750	1.232	0.649
0.2833	1.219	0.623
0.2916	1.207	0.604
0.3000	1.194	0.585
0.3083	1.181	0.566
0.3166	1.172	0.540
0.3250	1.159	0.521
0.3333	1.150	0.509
0.3500	1.127	0.470
0.3666	1.108	0.445
0.3833	1.093	0.413
0.4000	1.074	0.388
0.4166	1.055	0.362
0.4333	1.039	0.337
0.4500	1.023	0.318
0.4666	1.010	0.299
0.4833	0.998	0.279
0.5000	0.982	0.260
0.5166	0.969	0.248
0.5333	0.956	0.235
0.5500	0.947	0.216
0.5666	0.934	0.203
0.5833	0.925	0.190
0.6000	0.915	0.178
0.6166	0.902	0.171
0.6333	0.896	0.165
0.6500	0.887	0.152
0.6666	0.877	0.146
0.6833	0.871	0.133
0.7000	0.861	0.127
0.7166	0.855	0.120

t₀

Q1 ΔH = 1.122

Δt = 1.35

Q2 ΔH = 2.5

Δt = 1.9584

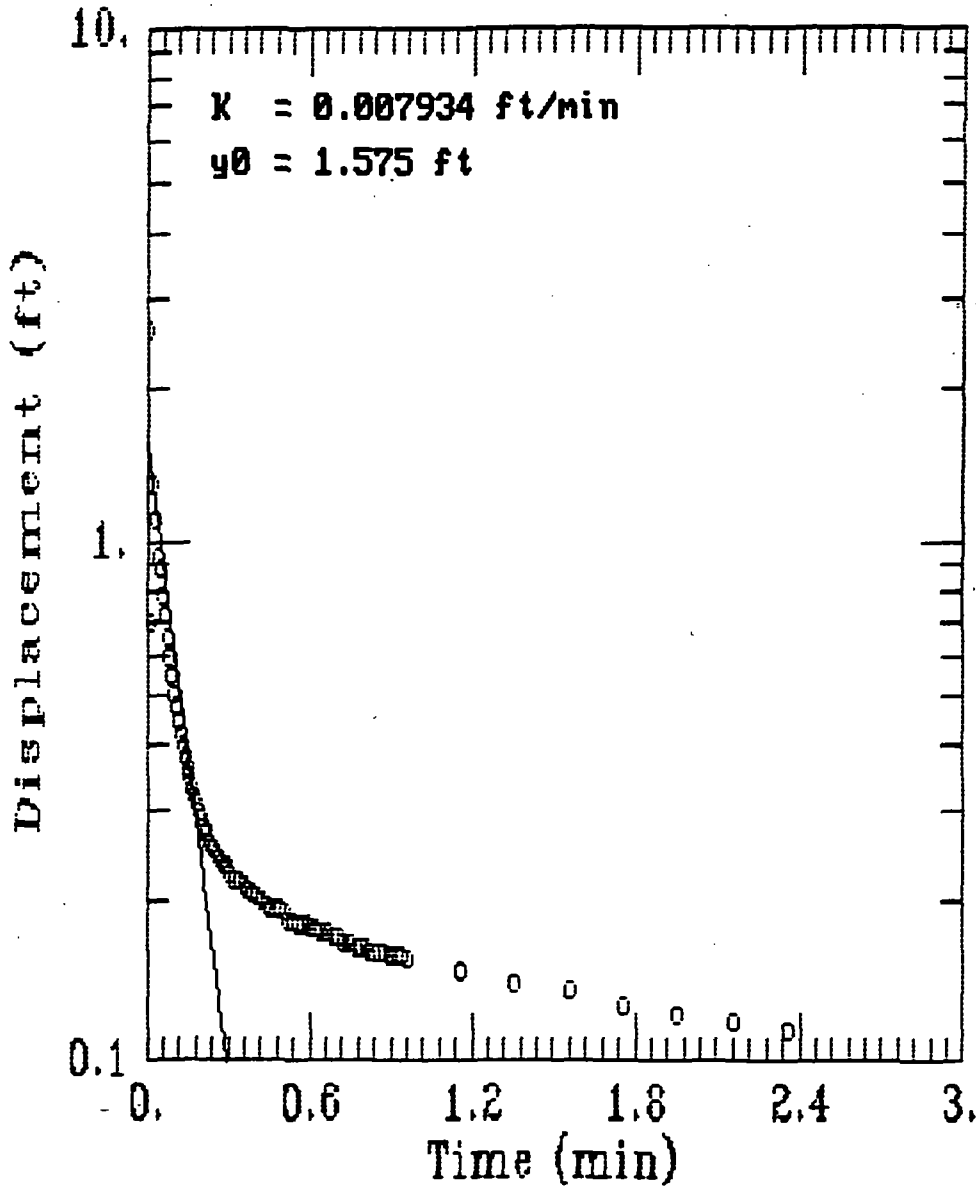
Test:	Q1 Q2 Slug out
File:	Q1 Q2 - T2 - det
Round:	KTEST2
Column 1:	Elapsed time (min)
Column 2:	Head Q1 (ft)
	t ₀ = 0.0500 t ₁ = 1.40
Column 3:	Head Q2 (ft)
	t ₀ = 0.0416 t ₁ = 2.00

0.7833	0.826	0.095
0.8000	0.820	0.095
0.8166	0.817	0.089
0.8333	0.811	0.082
0.8500	0.804	0.076
0.8666	0.801	0.076
0.8833	0.795	0.069
0.9000	0.788	0.069
0.9166	0.785	0.063
0.9333	0.782	0.063
0.9500	0.776	0.057
0.9666	0.773	0.057
0.9833	0.769	0.050
1.0000	0.763	0.050
1.2000	0.722	0.025
1.4000	0.690	0.012
1.6000	0.665	0.006
1.8000	0.646	0.006
2.0000	0.633	0.000
2.2000	0.624	0.000
2.4000	0.611	0.000
2.6000	0.605	0.000
2.8000	0.598	-0.006
3.0000	0.589	-0.006
3.2000	0.589	-0.006
3.4000	0.586	-0.006
3.6000	0.579	-0.006
3.8000	0.579	-0.006
4.0000	0.576	-0.006
4.2000	0.576	-0.006
4.4000	0.573	-0.006
4.6000	0.573	-0.006
4.8000	0.573	-0.006
5.0000	0.570	-0.006
5.2000	0.567	-0.012
5.4000	0.567	-0.006
5.6000	0.567	-0.006
5.8000	0.567	-0.012
6.0000	0.567	-0.012
6.2000	0.563	-0.006
6.4000	0.563	-0.006
6.6000	0.563	-0.012
6.8000	0.563	-0.012
7.0000	0.563	-0.012
7.2000	0.563	-0.006
7.4000	0.563	-0.006
7.6000	0.563	-0.006
7.8000	0.563	-0.006
8.0000	0.563	-0.006
8.2000	0.563	-0.006
8.4000	0.563	-0.006
8.6000	0.563	-0.006
8.8000	0.570	-0.012
9.0000	0.563	-0.006
9.2000	0.563	-0.006
9.4000	0.563	-0.006
9.6000	0.563	-0.006
9.8000	0.560	-0.006
10.0000	0.563	-0.006
12.0000	0.560	-0.006
14.0000	0.560	-0.006
16.0000	0.560	-0.006
17.0000	0.560	-0.006

WELL CLUSTER: ✓
WELL ID: V1
SCREENED INTERVAL: 2.5-13.5

TEST METHOD: Runner Pipe
SLUG IN/SLUG OUT: slug out
K-VALUE: 11.4 ft/den

V1-T2-1

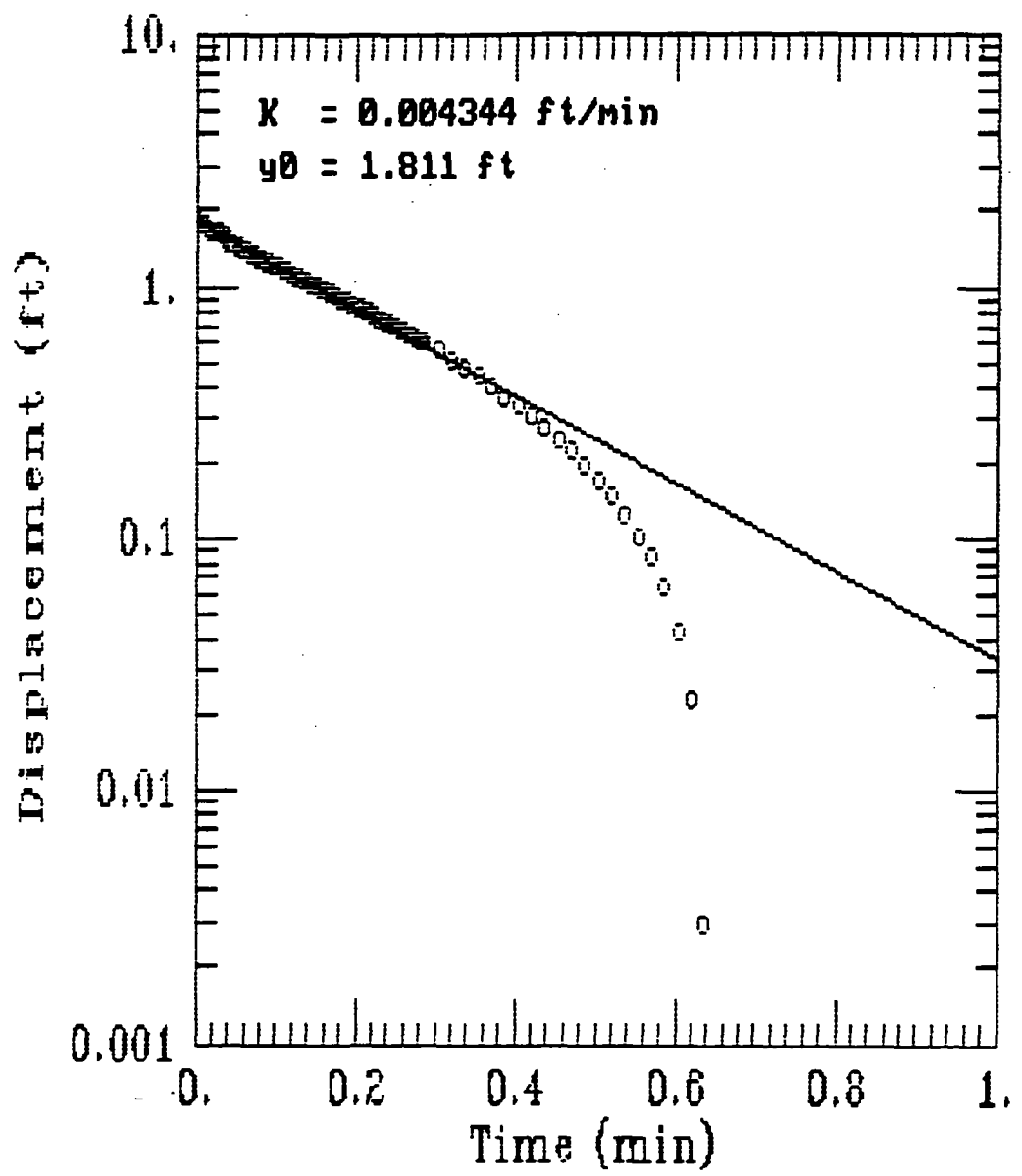


0.7833	0.167	-0.006
0.8000	0.167	-0.006
0.8166	0.164	-0.006
0.8333	0.164	-0.006
0.8500	0.164	-0.006
0.8666	0.161	-0.006
0.8833	0.161	-0.006
0.9000	0.161	-0.006
0.9166	0.161	-0.006
0.9333	0.158	-0.006
0.9500	0.158	-0.006
0.9666	0.158	-0.006
0.9833	0.158	-0.006
1.0000	0.155	-0.006
1.2000	0.148	-0.006
1.4000	0.139	-0.006
1.6000	0.136	-0.006
1.8000	0.126	-0.006
2.0000	0.123	-0.006
2.2000	0.117	-0.012
2.4000	0.114	-0.006

WELL CLUSTER: V
WELL ID: V2
SCREENED INTERVAL: 21-34

TEST METHOD: Brunner Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 6.26 FT/day

V2-T2



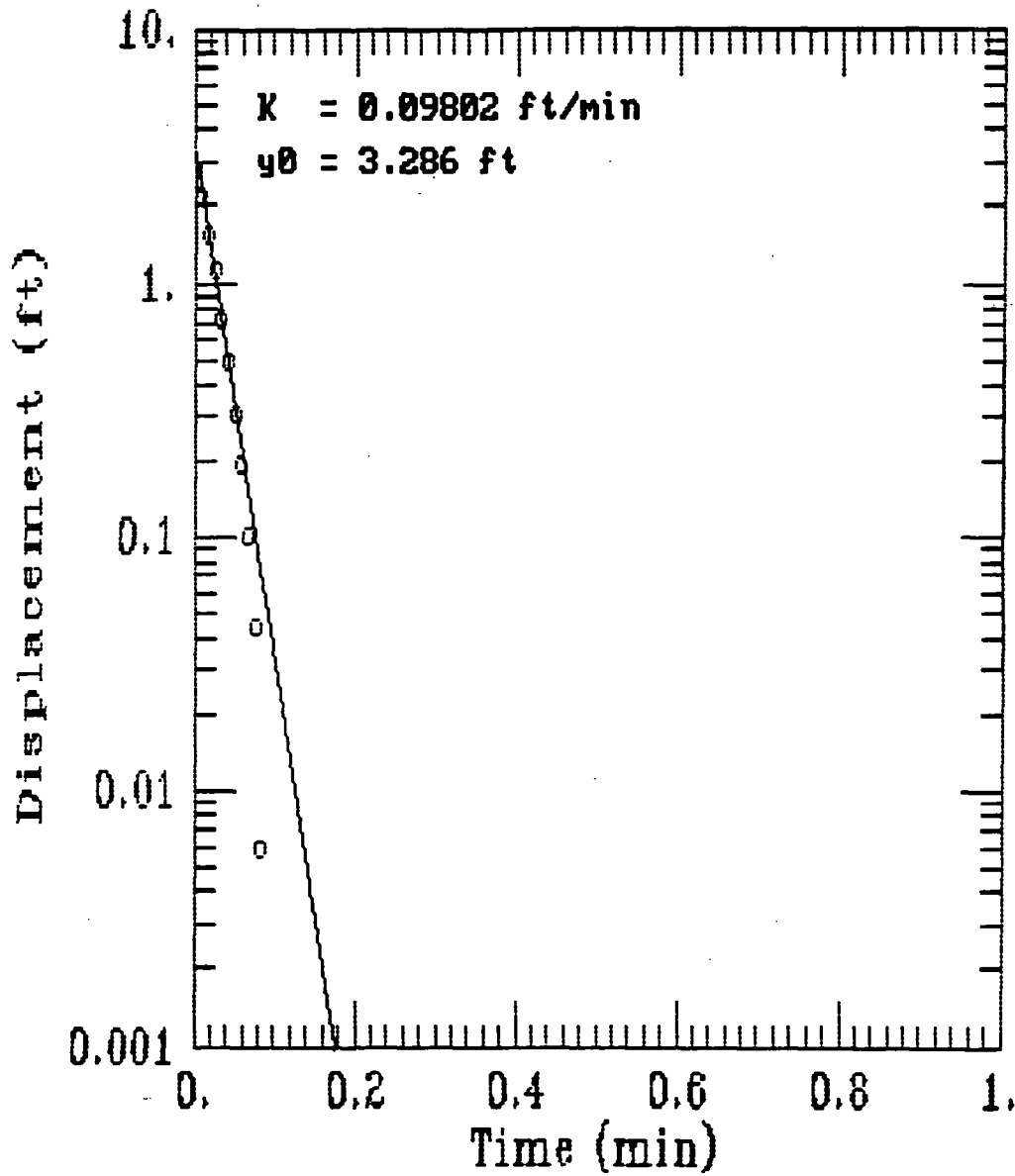
0.2200	0.925
0.2233	0.915
0.2266	0.901
0.2300	0.891
0.2333	0.881
0.2366	0.871
0.2400	0.858
0.2433	0.848
0.2466	0.838
0.2500	0.828
0.2533	0.818
0.2566	0.808
0.2600	0.797
0.2633	0.787
0.2666	0.777
0.2700	0.767
0.2733	0.757
0.2766	0.750
0.2800	0.740
0.2833	0.730
0.2866	0.720
0.2900	0.710
0.2933	0.700
0.2966	0.693
0.3000	0.683
0.3033	0.673
0.3066	0.666
0.3100	0.656
0.3133	0.650
0.3166	0.640
0.3200	0.633
0.3233	0.623
0.3266	0.616
0.3300	0.606
0.3333	0.599
0.3500	0.556
0.3666	0.515
0.3833	0.475
0.4000	0.438
0.4166	0.401
0.4333	0.367
0.4500	0.333
0.4666	0.303
0.4833	0.276
0.5000	0.246
0.5166	0.219
0.5333	0.195
0.5500	0.168
0.5666	0.145
0.5833	-0.124
0.6000	0.101
0.6166	0.084
0.6333	0.064
0.6500	0.043
0.6666	0.023
0.6833	0.003
0.7000	-0.013
0.7166	-0.033
0.7333	-0.047
0.7500	-0.064
0.7666	-0.081
0.7833	-0.094
0.8000	-0.104
0.8166	-0.116

0.8666	-0.152
0.8833	-0.162
0.9000	-0.172
0.9166	-0.179
0.9333	-0.189
0.9500	-0.199
0.9666	-0.206
0.9833	-0.212
1.0000	-0.223
1.2000	-0.300
1.4000	-0.327
1.6000	-0.344
1.8000	-0.351
2.0000	-0.358
2.2000	-0.365
2.4000	-0.365
2.6000	-0.368
2.8000	-0.368
3.0000	-0.371
3.2000	-0.371
3.4000	-0.371
3.6000	-0.371
3.8000	-0.371
4.0000	-0.371
4.2000	-0.371
4.4000	-0.371
4.6000	-0.371
4.8000	-0.371
5.0000	-0.371
5.2000	-0.371
5.4000	-0.368
5.6000	-0.368
5.8000	-0.368
6.0000	-0.368
6.2000	-0.371
6.4000	-0.371
6.6000	-0.371
6.8000	-0.371
7.0000	-0.371
7.2000	-0.371
7.4000	-0.371
7.6000	-0.368
7.8000	-0.368
8.0000	-0.368
8.2000	-0.368
8.4000	-0.371
8.6000	-0.368
8.8000	-0.368
9.0000	-0.368
9.2000	-0.368
9.4000	-0.365
9.6000	-0.365
9.8000	-0.365
10.0000	-0.365

WELL CLUSTER: V
WELL ID: V3
SCREENED INTERVAL: 53-58

TEST METHOD: Dunker Pipe
SLUG IN/SLUG OUT: Slug out
K-VALUE: 141. ft/day

V3-T2



SE2000
 Environmental Logger
 08/23 08:41

Unit# 22 Test 17

V3-T2

PRN ✓

 Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. 204363

Reference 0.000
 SG 1.000
 Linearity 0.152
 Scale factor 19.970
 Offset 0.061
 Delay mSEC 50.000

Step 0 08/22 13:37:37

Elapsed Time	INPUT 1
0.0000	0.000
0.0083	0.006
0.0166	0.000
0.0250	0.006
0.0333	0.000
0.0416	0.006
0.0500	0.000
0.0583	0.006
0.0666	0.126
0.0750	-0.012
0.0833	-0.012
0.0916	2.633
0.1000	2.771
0.1083	2.210
0.1166	1.541
0.1250	1.130
0.1333	0.732
0.1416	0.492
0.1500	0.303
0.1583	0.195
0.1666	0.101
0.1750	0.044
0.1833	0.006
0.1916	-0.012
0.2000	-0.025
0.2083	-0.025
0.2166	-0.025
0.2250	-0.025
0.2333	-0.025
0.2416	-0.018
0.2500	-0.018
0.2583	-0.012
0.2666	-0.012
0.2750	-0.012
0.2833	-0.012
0.2916	-0.012
0.3000	-0.006

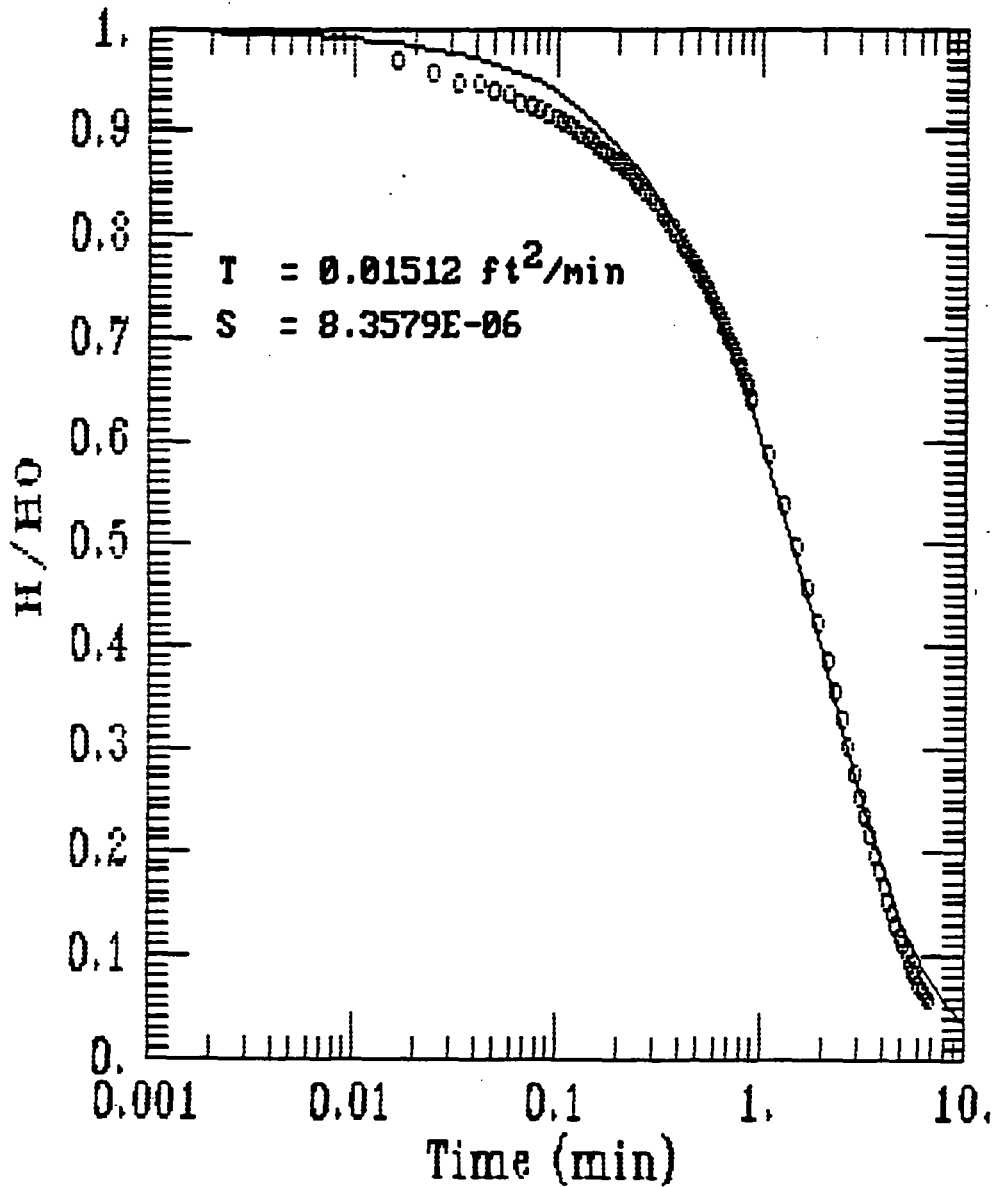
Test:	V3 Slug out
File:	V3-T2
Round:	KTEST3
Column 1:	Elapsed time (min)
Column 2:	head (ft)
	t ₀ = 0.100 t ₁ = 0.1833
Column 3:	
	t ₀ = _____ t ₁ = _____

0.3333	-0.012
0.3500	-0.012
0.3666	-0.012
0.3833	-0.012
0.4000	-0.018
0.4166	-0.012
0.4333	-0.012
0.4500	-0.012
0.4666	-0.012
0.4833	-0.012
0.5000	-0.012
0.5166	-0.012
0.5333	-0.012
0.5500	-0.012
0.5666	-0.012
0.5833	-0.012
0.6000	-0.012
0.6166	-0.012
0.6333	-0.012
0.6500	-0.012
0.6666	-0.012
0.6833	-0.012
0.7000	-0.012
0.7166	-0.012
0.7333	-0.012
0.7500	-0.012
0.7666	-0.012
0.7833	-0.012
0.8000	-0.012
0.8166	-0.012
0.8333	-0.012
0.8500	-0.012
0.8666	-0.012
0.8833	-0.012
0.9000	-0.012
0.9166	-0.012
0.9333	-0.012
0.9500	-0.012
0.9666	-0.012
0.9833	-0.012
1.0000	-0.012
1.2000	-0.006
1.4000	-0.006
1.6000	-0.006

WELL CLUSTER: V
WELL ID: V4
SCREENED INTERVAL: 69-79

TEST METHOD: Casper et al.
SLUG IN/SLUG OUT: slug out
K-VALUE: 1.05 ft/day

V4-T2-1

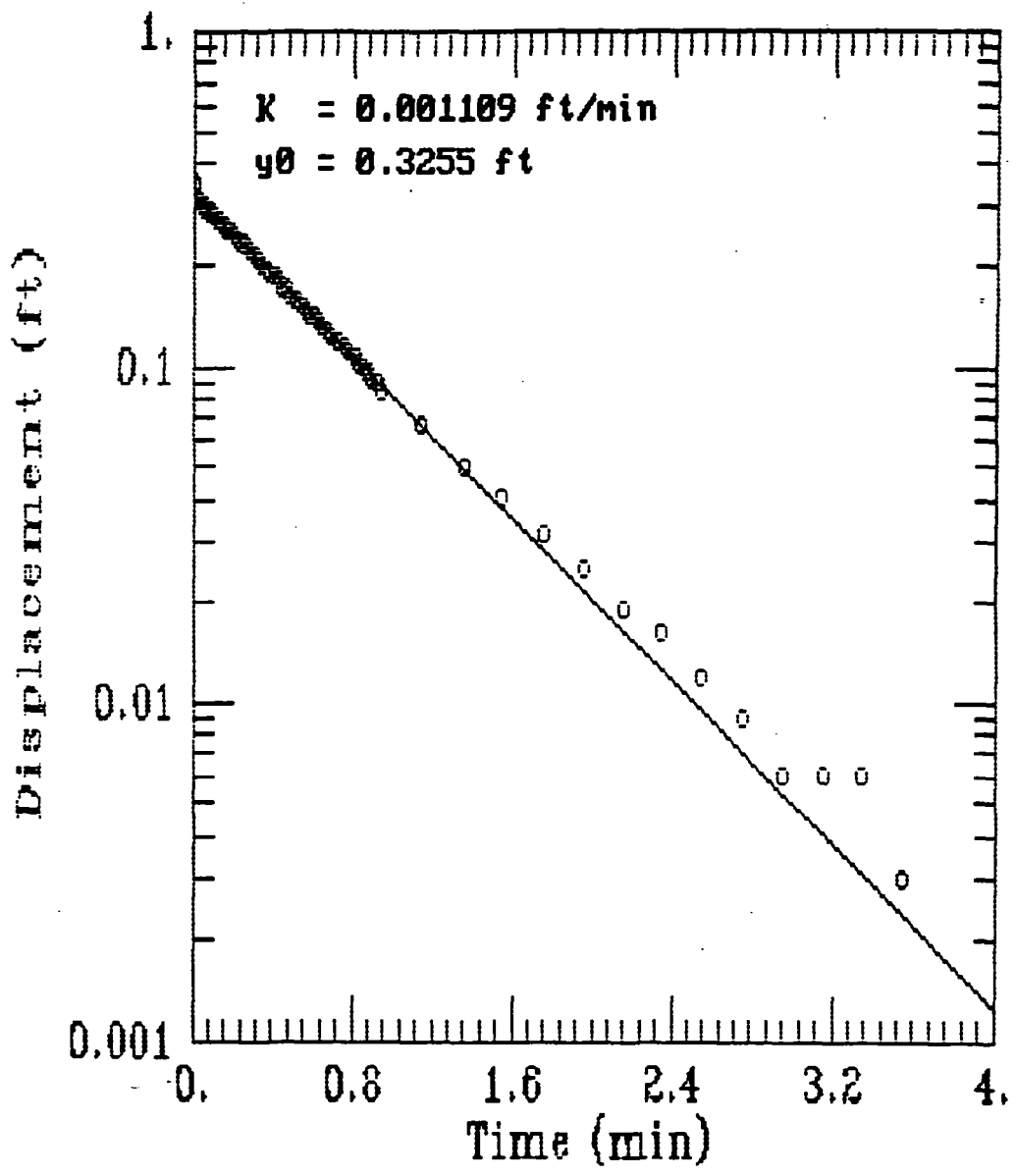


0.7000	1.972
0.7833	1.959
0.8000	1.946
0.8166	1.930
0.8333	1.917
0.8500	1.904
0.8666	1.892
0.8833	1.879
0.9000	1.866
0.9166	1.853
0.9333	1.840
0.9500	1.827
0.9666	1.814
0.9833	1.798
1.0000	1.789
1.2000	1.637
1.4000	1.509
1.6000	1.387
1.8000	1.277
2.0000	1.174
2.2000	1.078
2.4000	0.994
2.6000	0.914
2.8000	0.840
3.0000	0.772
3.2000	0.711
3.4000	0.650
3.6000	0.598
3.8000	0.550
4.0000	0.505
4.2000	0.463
4.4000	0.428
4.6000	0.392
4.8000	0.360
5.0000	0.331
5.2000	0.305
5.4000	0.283
5.6000	0.260
5.8000	0.241
6.0000	0.222
6.2000	0.202
6.4000	0.186
6.6000	0.170
6.8000	0.160

WELL CLUSTER: W
WELL ID: W1
SCREENED INTERVAL: 6-16

TEST METHOD: Bowser Rise
SLUG IN/SLUG OUT: Slug out
K-VALUE: 1.60 ft/day

W1-T2

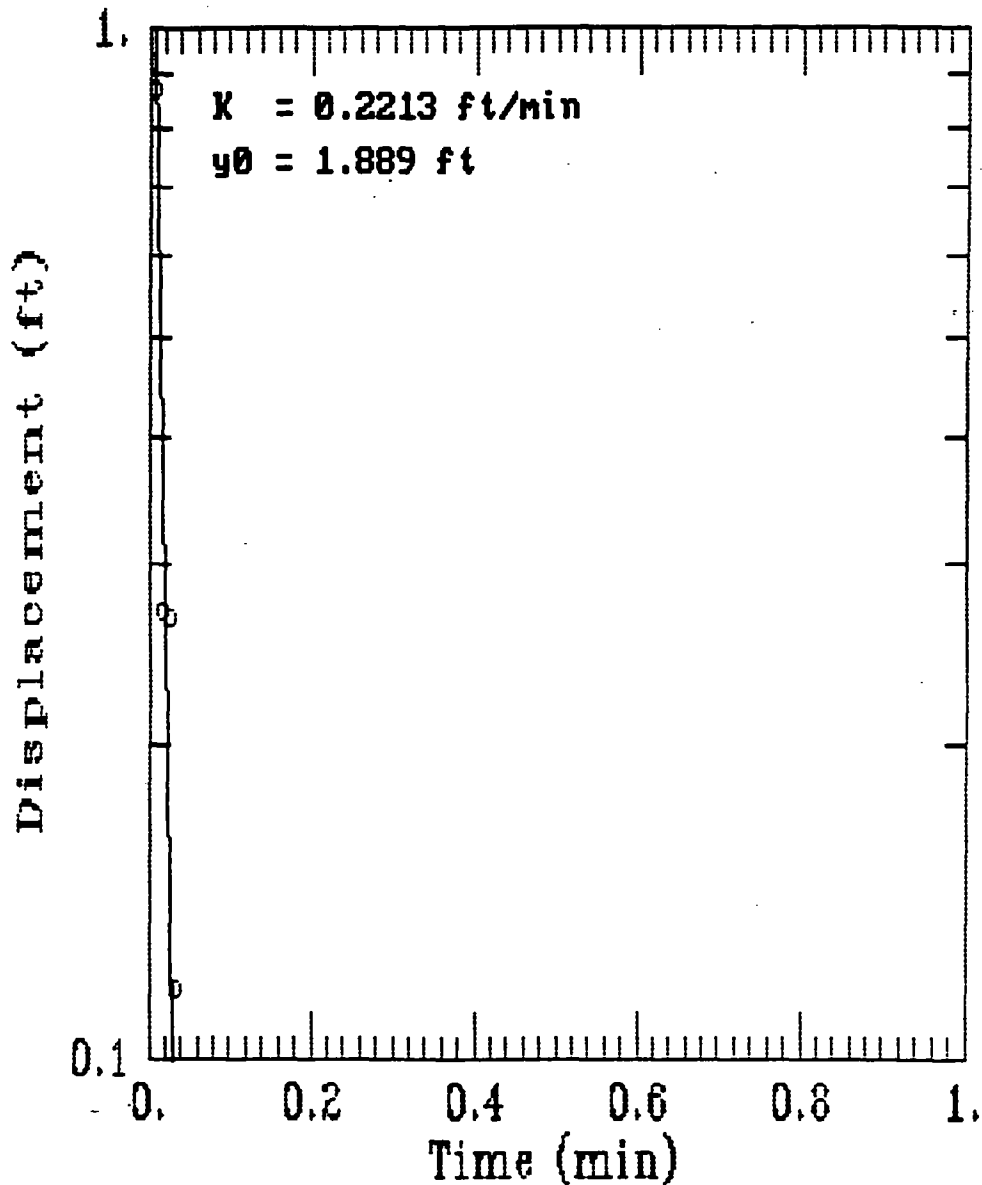


0.3333	0.221
0.3500	0.215
0.3666	0.208
0.3833	0.205
0.4000	0.202
0.4166	0.196
0.4333	0.189
0.4500	0.186
0.4666	0.183
0.4833	0.180
0.5000	0.173
0.5166	0.170
0.5333	0.163
0.5500	0.160
0.5666	0.157
0.5833	0.154
0.6000	0.151
0.6166	0.147
0.6333	0.144
0.6500	0.141
0.6666	0.138
0.6833	0.135
0.7000	0.131
0.7166	0.128
0.7333	0.125
0.7500	0.122
0.7666	0.118
0.7833	0.118
0.8000	0.115
0.8166	0.112
0.8333	0.109
0.8500	0.106
0.8666	0.106
0.8833	0.102
0.9000	0.099
0.9166	0.096
0.9333	0.096
0.9500	0.093
0.9666	0.090
0.9833	0.090
1.0000	0.086
1.2000	0.067
1.4000	0.051
1.6000	0.041
1.8000	0.032
2.0000	0.025
2.2000	0.019
2.4000	0.016
2.6000	0.012
2.8000	-0.009
3.0000	0.006
3.2000	0.006
3.4000	0.006
3.6000	0.003 ✓

WELL CLUSTER: W
WELL ID: W3
SCREENED INTERVAL: 28.75-33.75

TEST METHOD: Summer Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 319 ft/day

W3-T2



SE2000
 Environmental Logger
 08/18 17:32

Unit# 22 Test 6 W3-T2

 Setups: INPUT 1

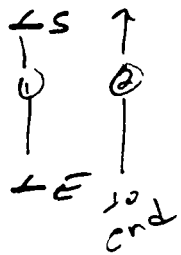
 Type Level (F)
 Mode TOC
 I.D. 204363

 Reference 0.000
 SG 1.000
 Linearity 0.038
 Scale factor 10.165
 Offset 0.010
 Delay mSEC 50.000

Step 0 08/18 12:59:14

 Elapsed Time INPUT 1

 0.0000 0.000
 0.0083 0.000
 0.0166 0.000
 0.0250 -0.003
 0.0333 0.745
 0.0416 0.922
 0.0500 0.870
 0.0583 0.270
 0.0666 0.267
 0.0750 0.116
 0.0833 -0.054
 0.0916 -0.167
 0.1000 -0.180
 0.1083 -0.154
 0.1166 -0.080
 0.1250 0.006
 0.1333 0.077
 0.1416 0.116
 0.1500 0.116
 0.1583 0.080
 0.1666 0.032
 0.1750 -0.022
 0.1833 -0.058
 0.1916 -0.070
 0.2000 -0.061
 0.2083 -0.032
 0.2166 -0.003
 0.2250 0.025
 0.2333 0.038
 0.2416 0.041
 0.2500 0.032
 0.2583 0.012
 0.2666 -0.006
 0.2750 -0.022
 0.2833 -0.025
 0.2916 -0.025
 0.3000 -0.016
 0.3083 -0.004



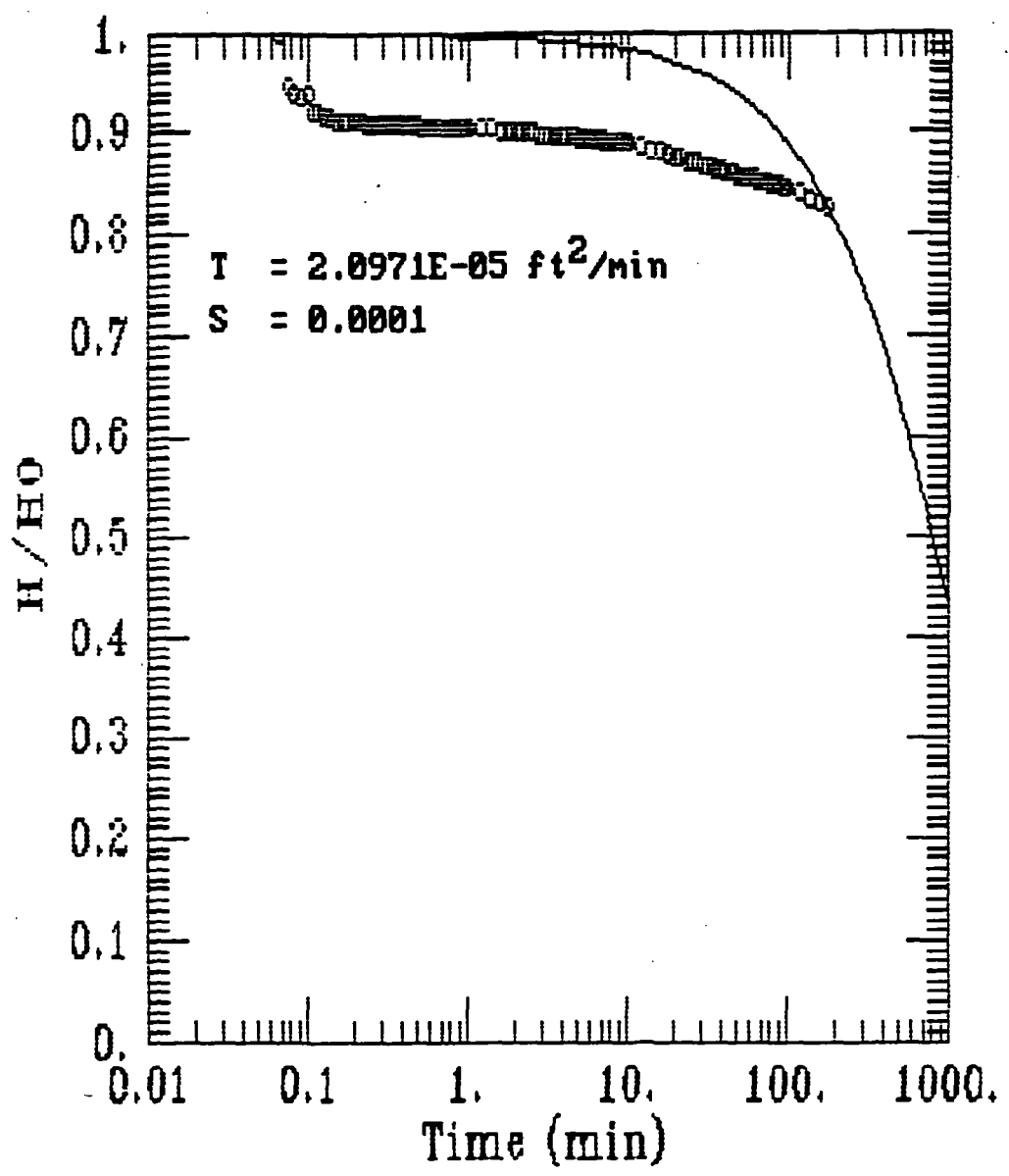
Test:	W3	Slug out
File:	W3-T2	
Round:	KTEST3	
Column 1:	Elapsed time (min)	
Column 2:	Head (ft)	
	t = 0.0416	t = 0.0833
Column 3:		
	t = _____	t = _____

0.3333	0.016
0.3500	0.003
0.3666	-0.009
0.3833	-0.009
0.4000	-0.003
0.4166	0.006
0.4333	0.003
0.4500	-0.003
0.4666	-0.006
0.4833	-0.003
0.5000	0.000
0.5166	0.003
0.5333	0.000
0.5500	0.000
0.5666	-0.003
0.5833	0.000
0.6000	0.000
0.6166	0.000
0.6333	0.000
0.6500	0.000
0.6666	0.000
0.6833	0.000
0.7000	0.000
0.7166	0.000
0.7333	0.000
0.7500	0.000
0.7666	0.000
0.7833	0.000
0.8000	0.000
0.8166	0.000
0.8333	0.000
0.8500	0.000
0.8666	0.000
0.8833	0.000
0.9000	0.000
0.9166	0.000
0.9333	0.003
0.9500	0.000
0.9666	0.000
0.9833	0.000
1.0000	0.000
1.2000	0.003
1.4000	0.000
1.6000	0.000
1.8000	0.000
2.0000	0.000

WELL CLUSTER: W
WELL ID: W4-1
SCREENED INTERVAL: 37-47

TEST METHOD: Casper et al.
SLUG IN/SLUG OUT: slug in T
K-VALUE: 2.022 ft/day

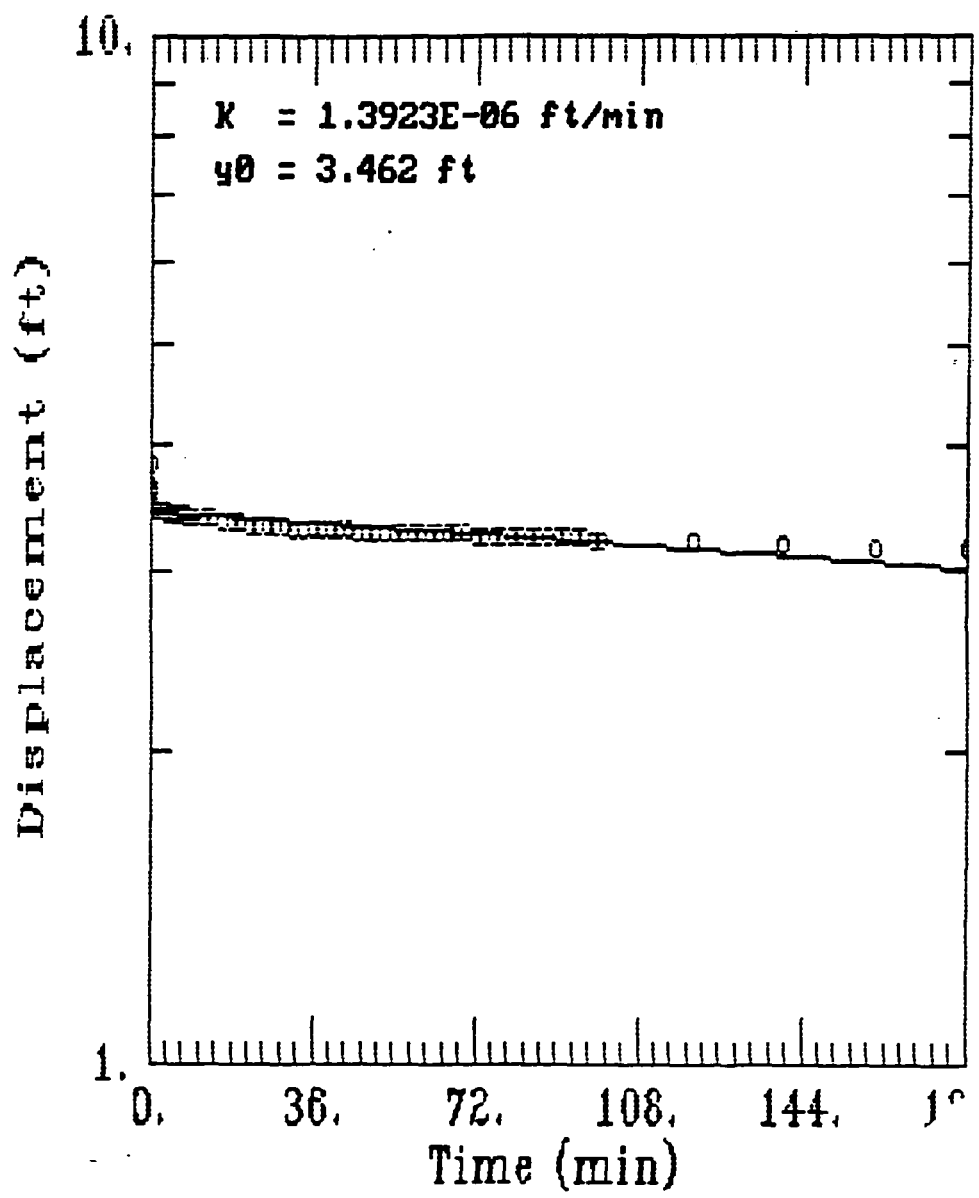
W4-T2



WELL CLUSTER: W)
WELL ID: W4-1
SCREENED INTERVAL: 27-47

TEST METHOD: Cooper et al.
SLUG IN/SLUG OUT: slug out
K-VALUE: 0.002 ft/day

W4-T2



SE2000
 Environmental Logger
 08/22 06:03

prn ✓
 Ant ✓

Unit# 22 Test 1

W4-T2

 Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. 204363

Reference 0.000
 SG 1.000
 Linearity 0.038
 Scale factor 10.165
 Offset 0.010
 Delay mSEC 50.000

Step 0 08/19 11:05:21

 Elapsed Time INPUT 1

0.0000	0.003
0.0083	0.003
0.0166	0.003
0.0250	2.391
0.0333	5.815
0.0416	7.166
0.0500	8.382
0.0583	5.403
0.0666	3.825
0.0750	3.625
0.0833	3.590
0.0916	3.574
0.1000	3.590
0.1083	3.522
0.1166	3.516
0.1250	3.512
0.1333	3.503
0.1416	3.500
0.1500	3.496
0.1583	3.493
0.1666	3.493
0.1750	3.490
0.1833	3.490
0.1916	3.490
0.2000	3.487
0.2083	3.487
0.2166	3.487
0.2250	3.487
0.2333	3.483
0.2416	3.483
0.2500	3.483
0.2583	3.483
0.2666	3.483
0.2750	3.480
0.2833	3.480
0.2916	3.480
0.3000	3.480

to end

① do slug in vs out.
 Bow/Rice

Test:	W4	slug out
File:	W4-T2	
Round:	KTEST3	
Column 1:	Elapsed time (min)	
Column 2:	Head (ft)	
	t = 0.0500	t = 0.0666
Column 3:		
	t = _____	t = _____

0.3333	3.480
0.3500	3.477
0.3666	3.477
0.3833	3.477
0.4000	3.477
0.4166	3.474
0.4333	3.474
0.4500	3.474
0.4666	3.474
0.4833	3.474
0.5000	3.474
0.5166	3.471
0.5333	3.471
0.5500	3.471
0.5666	3.471
0.5833	3.471
0.6000	3.471
0.6166	3.471
0.6333	3.471
0.6500	3.467
0.6666	3.467
0.6833	3.467
0.7000	3.467
0.7166	3.467
0.7333	3.467
0.7500	3.467
0.7666	3.464
0.7833	3.467
0.8000	3.464
0.8166	3.464
0.8333	3.464
0.8500	3.464
0.8666	3.464
0.8833	3.464
0.9000	3.461
0.9166	3.464
0.9333	3.464
0.9500	3.461
0.9666	3.461
0.9833	3.461
1.0000	3.461
1.2000	3.458
1.4000	3.458
1.6000	3.454
1.8000	3.451
2.0000	3.451
2.2000	3.448
2.4000	3.445
2.6000	3.445
2.8000	3.442
3.0000	3.442
3.2000	3.438
3.4000	3.438
3.6000	3.438
3.8000	3.435
4.0000	3.435
4.2000	3.432
4.4000	3.432
4.6000	3.432
4.8000	3.429
5.0000	3.425
5.2000	3.425
5.4000	3.425
5.6000	3.425

6.2000	3.419
6.4000	3.419
6.6000	3.416
6.8000	3.416
7.0000	3.413
7.2000	3.416
7.4000	3.413
7.6000	3.409
7.8000	3.409
8.0000	3.409
8.2000	3.409
8.4000	3.406
8.6000	3.406
8.8000	3.403
9.0000	3.403
9.2000	3.403
9.4000	3.400
9.6000	3.400
9.8000	3.400
10.0000	3.400
12.0000	3.390
14.0000	3.380
16.0000	3.371
18.0000	3.361
20.0000	3.355
22.0000	3.348
24.0000	3.342
26.0000	3.335
28.0000	3.329
30.0000	3.326
32.0000	3.319
34.0000	3.316
36.0000	3.309
38.0000	3.306
40.0000	3.303
42.0000	3.297
44.0000	3.293
46.0000	3.290
48.0000	3.287
50.0000	3.284
52.0000	3.284
54.0000	3.280
56.0000	3.277
58.0000	3.277
60.0000	3.274
62.0000	3.271
64.0000	3.271
66.0000	3.268
68.0000	3.264
70.0000	3.264
72.0000	3.261
74.0000	3.261
76.0000	3.258
78.0000	3.255
80.0000	3.255
82.0000	3.248
84.0000	3.248
86.0000	3.248
88.0000	3.245
90.0000	3.242
92.0000	3.242
94.0000	3.239
96.0000	3.239
98.0000	3.235

140.000
160.000
180.000

3.197
3.177
3.161 ✓

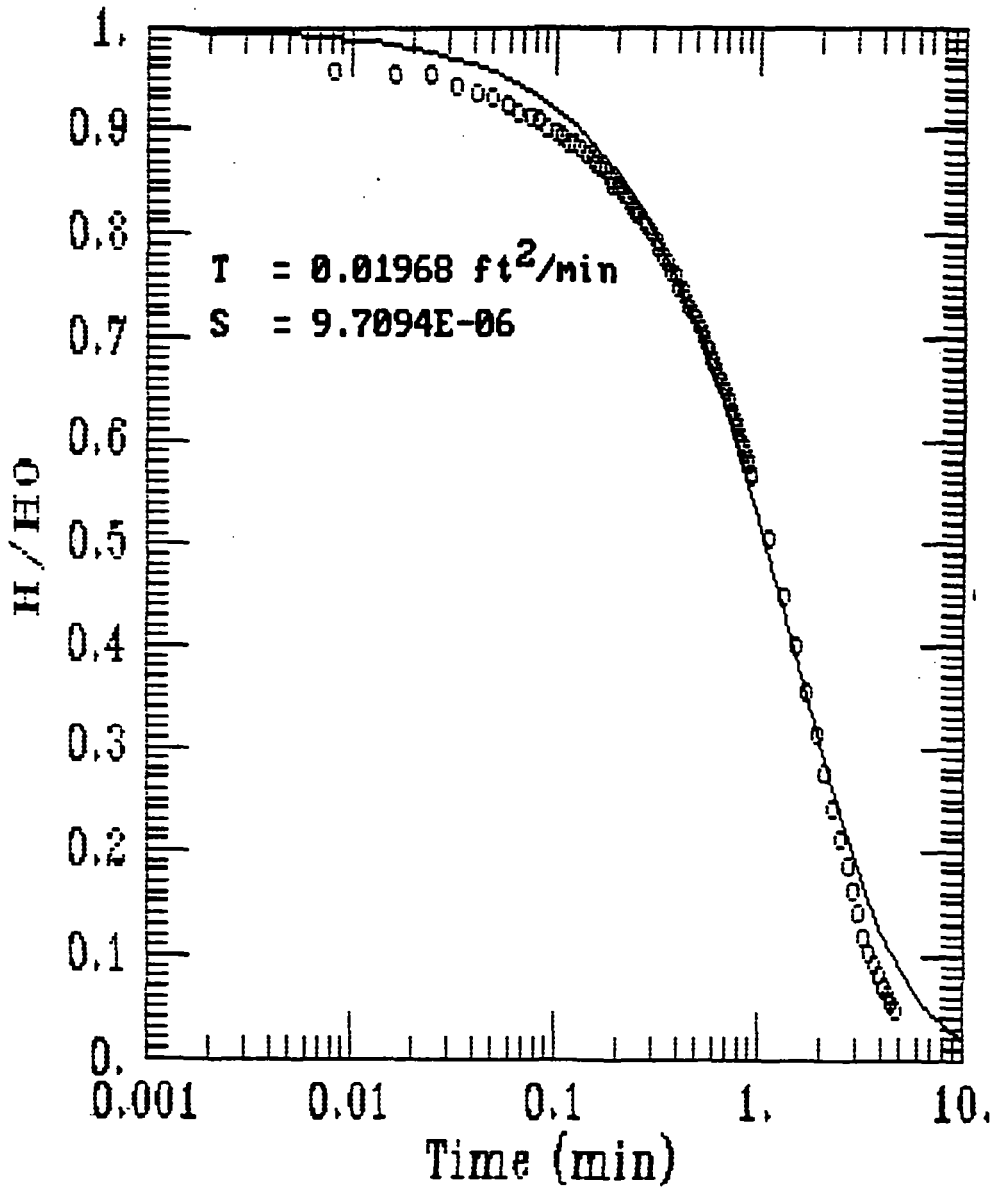
G4 COMPARISON OF CALCULATED K

FIELD TEST VS LOW FLOW SAMPLING DATA

WELL CLUSTER: G
WELL ID: 24
SCREENED INTERVAL: 106-116

TEST METHOD: Cooper et al.
SLUG IN/SLUG OUT: slug out
K-VALUE: 1.93 ft/day

G4-T2-1



0.0000	0.000	0.009
0.0083	0.553	0.012
0.0166	3.038	0.012
0.0250	2.402	0.655
0.0333	1.506	1.542
0.0416	1.144	1.634
0.0500	0.902	1.789
0.0583	0.642	1.900
0.0666	0.317	1.824
0.0750	0.082	1.815
0.0833	-0.101	1.812
0.0916	-0.241	1.789
0.1000	-0.330	1.780
0.1083	-0.362	1.774
0.1166	-0.368	1.758
0.1250	-0.343	1.745
0.1333	-0.298	1.736
0.1416	-0.241	1.726
0.1500	-0.171	1.717
0.1583	-0.101	1.707
0.1666	-0.044	1.698
0.1750	0.012	1.688
0.1833	0.063	1.685
0.1916	0.095	1.675
0.2000	0.114	1.663
0.2083	0.127	1.656
0.2166	0.133	1.647
0.2250	0.127	1.641
0.2333	0.114	1.634
0.2416	0.101	1.622
0.2500	0.089	1.609
0.2583	0.076	1.606
0.2666	0.057	1.599
0.2750	0.044	1.590
0.2833	0.031	1.584
0.2916	0.025	1.571
0.3000	0.019	1.565
0.3083	0.019	1.558
0.3166	0.012	1.555
0.3250	0.012	1.546
0.3333	0.019	1.536
0.3500	0.019	1.523
0.3666	0.025	1.508
0.3833	0.038	1.492
0.4000	0.038	1.476
0.4166	0.031	1.466
0.4333	0.038	1.451
0.4500	0.038	1.441
0.4666	0.038	1.425
0.4833	0.038	1.416
0.5000	0.038	1.400
0.5166	0.031	1.387
0.5333	0.031	1.374
0.5500	0.031	1.365
0.5666	0.031	1.352
0.5833	0.031	1.340
0.6000	0.038	1.327
0.6166	0.031	1.314
0.6333	0.031	1.305
0.6500	0.031	1.289

② G364-T2-dat

Proposed

G3 $\Delta H = 2.956$
 $\Delta t = 0.0524$

G4 $\Delta H = 1.812$
 $\Delta t = 1.2 = 4$

Test:	G3, G4 Slug out
File:	G364-T2-dat
Round:	KTEST2
Column 1:	Elapsed time (min)
Column 2:	Head G3 (ft)
	$t_0 = 0.0166$ $t_1 = 0.750$
Column 3:	Head G4 (ft)
	$t_0 = 0.0523$ $t_1 = 4.80$

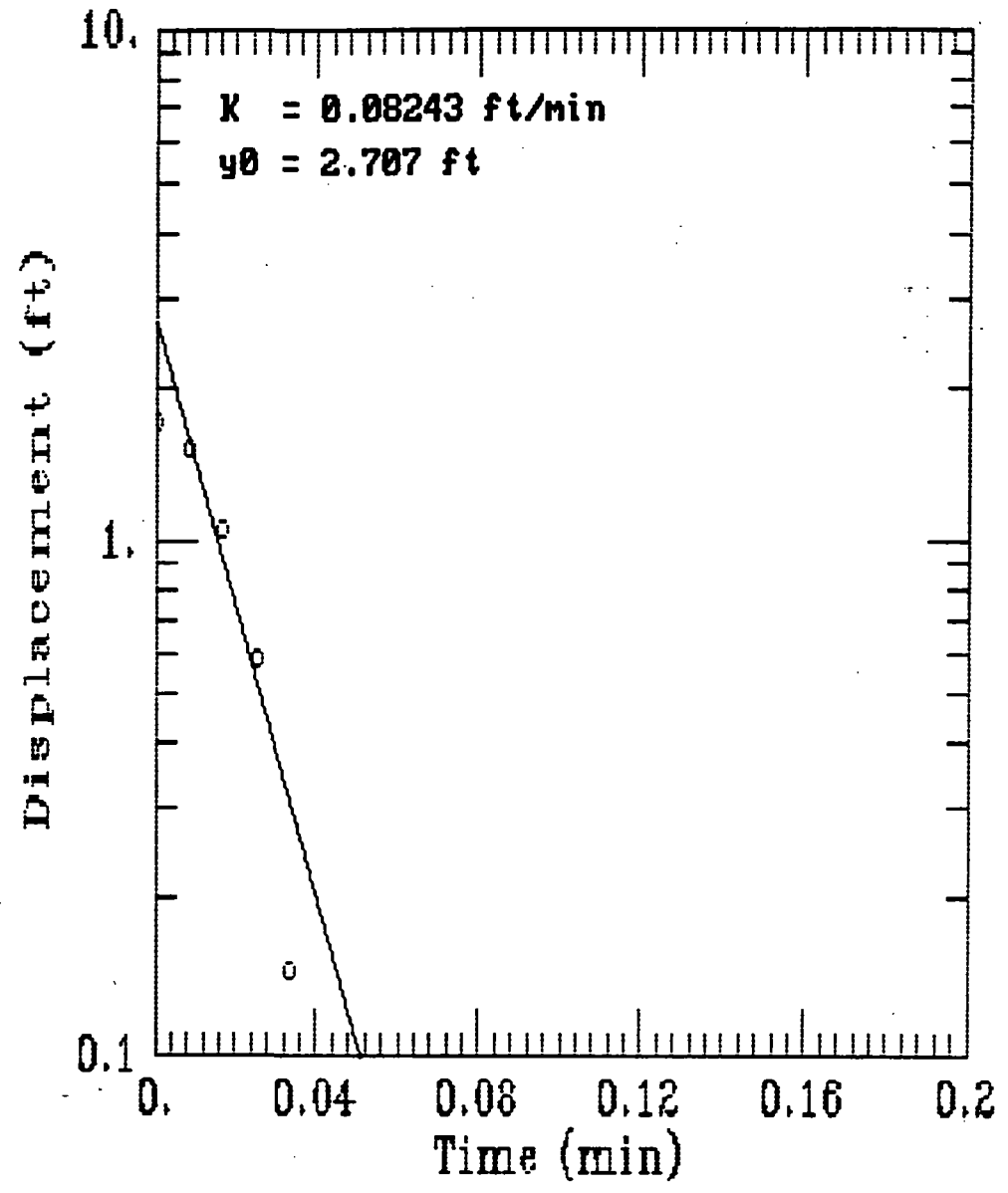
0.7000	0.031	1.283
0.7166	0.031	1.260
0.7333	0.031	1.251
0.7500	0.031	1.235
0.7666	0.031	1.226
0.7833	0.031	1.213
0.8000	0.038	1.207
0.8166	0.038	1.194
0.8333	0.031	1.181
0.8500	0.031	1.172
0.8666	0.031	1.162
0.8833	0.031	1.150
0.9000	0.031	1.140
0.9166	0.031	1.131
0.9333	0.031	1.121
0.9500	0.031	1.112
0.9666	0.031	1.099
0.9833	0.031	1.093
1.0000	0.031	1.083
1.2000	0.038	1.070
1.4000	0.031	0.956
1.6000	0.031	0.849
1.8000	0.031	0.760
2.0000	0.031	0.674
2.2000	0.031	0.592
2.4000	0.031	0.522
2.6000	0.031	0.459
2.8000	0.031	0.402
3.0000	0.025	0.354
3.2000	0.025	0.307
3.4000	0.031	0.266
3.6000	0.031	0.228
3.8000	0.031	0.199
4.0000	0.031	0.171
4.2000	0.031	0.155
4.4000	0.025	0.129
4.6000	0.019	0.117
4.8000	0.031	0.101
	0.031	0.088

Proposed

WELL CLUSTER: 6
WELL ID: 65
SCREENED INTERVAL: 30-90

TEST METHOD: Banner Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 119 ft/day

G5-T2B



Unit# 22 Test 15

65-T2B

PRN ✓

Setups: INPUT 1

Type Level (F)
Mode TOC
I.D. 204363

Plot ✓

Reference 0.000
SG 1.000
Linearity 0.038
Scale factor 10.165
Offset 0.010
Delay mSEC 50.000

ⓐ This round [- due slug in
- compare in/cut

ⓑ old round

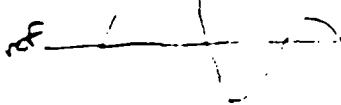
Step 0 08/18 15:55:27

Elapsed Time INPUT 1

0.0000	-0.003
0.0083	0.000
0.0166	-0.003
0.0250	0.003
0.0333	0.335
0.0416	0.831
0.0500	0.821
0.0583	1.133
0.0666	1.700
0.0750	1.526
0.0833	1.063
0.0916	0.592
0.1000	0.144
0.1083	-0.270
0.1166	-0.589
0.1250	-0.812
0.1333	-0.931
0.1416	-0.957
0.1500	-0.889
0.1583	-0.750
0.1666	-0.560
0.1750	-0.341
0.1833	-0.115
0.1916	-0.096
0.2000	0.273
0.2083	0.409
0.2166	0.492
0.2250	0.525
0.2333	0.509
0.2416	0.451
0.2500	0.360
0.2583	0.254
0.2666	0.135
0.2750	0.025
0.2833	-0.074
0.2916	-0.143
0.3000	-0.206
0.3083	-0.271

↳ start

↳ end

FW of 

Test:	65 Slug out
File:	65-T2B
Round:	KTEST3
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	b = 0.0666 t = 0.1083
Column 3:	
	b = _____ t = _____

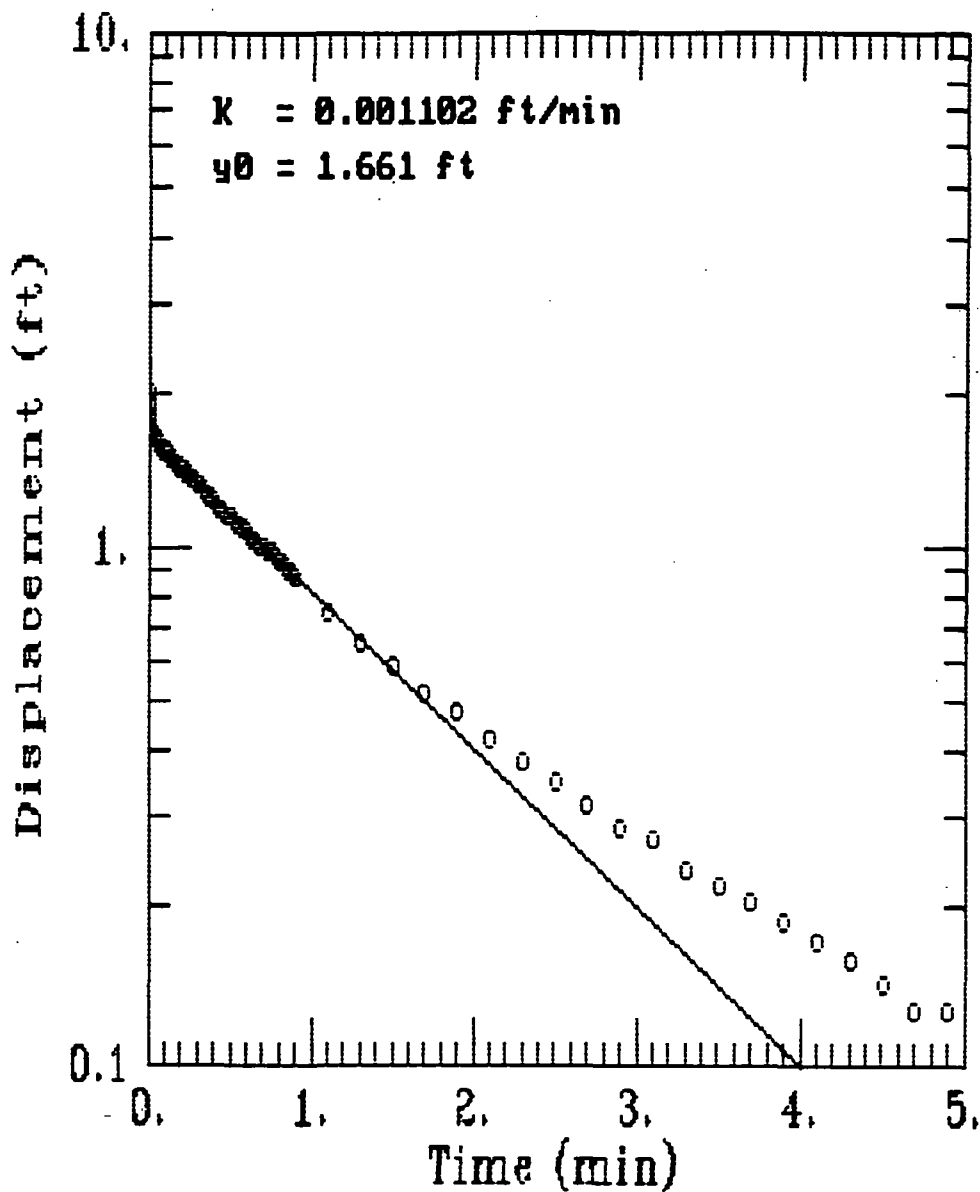
- line

0.3333	-0.173
0.3500	-0.064
0.3666	0.045
0.3833	0.122
0.4000	0.148
0.4166	0.125
0.4333	0.074
0.4500	0.019
0.4666	-0.025
0.4833	-0.045
0.5000	-0.038
0.5166	-0.016
0.5333	0.012
0.5500	0.038
0.5666	0.048
0.5833	0.045
0.6000	0.035
0.6166	0.022
0.6333	0.006
0.6500	0.000
0.6666	0.000
0.6833	0.003
0.7000	0.009
0.7166	0.019
0.7333	0.022
0.7500	0.022
0.7666	0.022
0.7833	0.019
0.8000	0.016
0.8166	0.012
0.8333	0.012
0.8500	0.012
0.8666	0.016
0.8833	0.012
0.9000	0.016
0.9166	0.016
0.9333	0.016
0.9500	0.019
0.9666	0.012
0.9833	0.012
1.0000	0.012
1.2000	0.022
1.4000	0.025
1.6000	0.025
1.8000	0.028
2.0000	0.025
2.2000	0.022
2.4000	0.022

WELL CLUSTER: G
WELL ID: G6
SCREENED INTERVAL: 21-26

TEST METHOD: Flowmeter
SLUG IN/SLUG OUT: slug out
K-VALUE: 1.59 ft/day

G6-T2



0.2000	1.548
0.2033	1.532
0.2066	1.532
0.2100	1.532
0.2133	1.532
0.2166	1.516
0.2200	1.516
0.2233	1.516
0.2266	1.516
0.2300	1.501
0.2333	1.501
0.2366	1.501
0.2400	1.501
0.2433	1.485
0.2466	1.485
0.2500	1.485
0.2533	1.485
0.2566	1.469
0.2600	1.469
0.2633	1.469
0.2666	1.469
0.2700	1.469
0.2733	1.453
0.2766	1.453
0.2800	1.453
0.2833	1.453
0.2866	1.438
0.2900	1.438
0.2933	1.438
0.2966	1.438
0.3000	1.422
0.3033	1.422
0.3066	1.422
0.3100	1.422
0.3133	1.422
0.3166	1.406
0.3200	1.406
0.3233	1.406
0.3266	1.406
0.3300	1.390
0.3333	1.390
0.3500	1.374
0.3666	1.358
0.3833	1.343
0.4000	1.327
0.4166	1.311
0.4333	1.295
0.4500	1.280
0.4666	1.264
0.4833	1.248
0.5000	1.232
0.5166	1.216
0.5333	1.201
0.5500	1.185
0.5666	1.169
0.5833	1.153
0.6000	1.153
0.6166	1.137
0.6333	1.122
0.6500	1.106

0.6666	1.090
0.6833	1.090
0.7000	1.074
0.7166	1.058
0.7333	1.043
0.7500	1.043
0.7666	1.027
0.7833	1.011
0.8000	0.995
0.8166	0.995
0.8333	0.979
0.8500	0.979
0.8666	0.964
0.8833	0.948
0.9000	0.932
0.9166	0.932
0.9333	0.916
0.9500	0.900
0.9666	0.900
0.9833	0.885
1.0000	0.869
1.2000	0.742
1.4000	0.647
1.6000	0.584
1.8000	0.521
2.0000	0.474
2.2000	0.426
2.4000	0.379
2.6000	0.347
2.8000	0.316
3.0000	0.284
3.2000	0.268
3.4000	0.237
3.6000	0.221
3.8000	0.205
4.0000	0.189
4.2000	0.173
4.4000	0.158
4.6000	0.142
4.8000	0.126
5.0000	0.126
5.2000	0.110
5.4000	0.110
5.6000	0.095
5.8000	0.095
6.0000	0.079
6.2000	0.079
6.4000	0.079
6.6000	0.063
6.8000	0.063
7.0000	0.063
7.2000	0.063
7.4000	0.047
7.6000	0.047
7.8000	0.047
8.0000	0.047
8.2000	0.047
8.4000	0.031
8.6000	0.031
8.8000	0.031

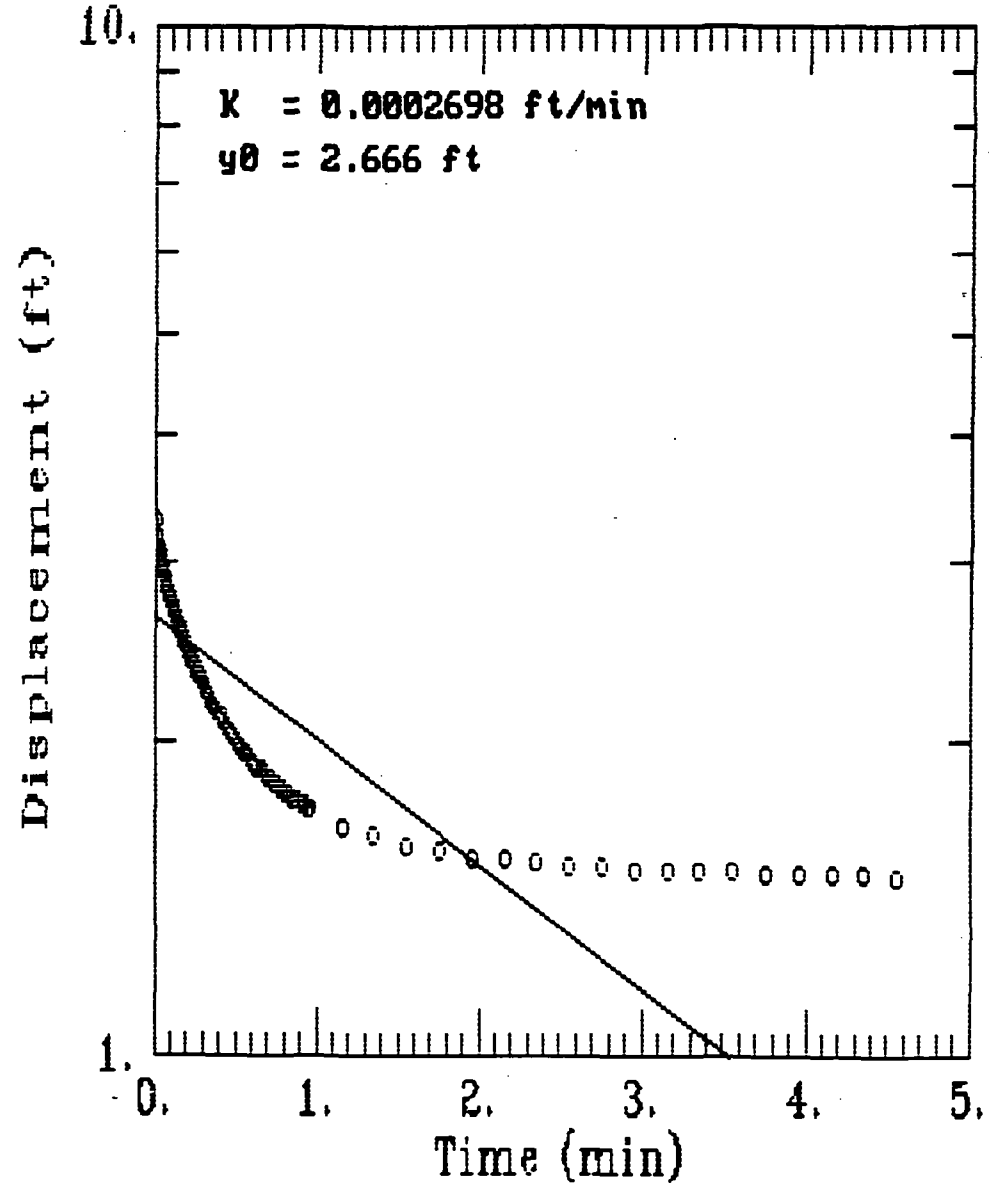
Handwritten scribble or signature

9.0000	0.031
9.2000	0.031
9.4000	0.031
9.6000	0.031
9.8000	0.031
10.0000	0.031

WELL CLUSTER: H
WELL ID: H1-1
SCREENED INTERVAL: 11-21

TEST METHOD: Banner Rice
SLUG IN/SLUG OUT: Silver Nit
K-VALUE: 0.389 ft/day

H1-T2



0.0000	1.471
0.0033	1.465
0.0066	1.471
0.0100	1.825
0.0133	3.031
0.0166	3.928
0.0200	4.218
0.0233	4.256
0.0266	3.239
0.0300	2.279
0.0333	3.062
0.0366	3.321
0.0400	3.309
0.0433	3.214
0.0466	3.195
0.0500	3.189
0.0533	3.157
0.0566	3.126
0.0600	3.113
0.0633	3.094
0.0666	3.094
0.0700	3.062
0.0733	3.062
0.0766	3.050
0.0800	3.031
0.0833	3.018
0.0866	2.999
0.0900	2.987
0.0933	2.968
0.0966	2.955
0.1000	2.949
0.1033	2.924
0.1066	2.905
0.1100	2.892
0.1133	2.873
0.1166	2.860
0.1200	2.822
0.1233	2.835
0.1266	2.810
0.1300	2.816
0.1333	2.791
0.1366	2.785
0.1400	2.772
0.1433	2.759
0.1466	2.747
0.1500	2.734
0.1533	2.728
0.1566	2.715
0.1600	2.702
0.1633	2.696
0.1666	2.684
0.1700	2.671
0.1733	2.665
0.1766	2.652
0.1800	2.646
0.1833	2.633
0.1866	2.627
0.1900	2.614
0.1933	2.608
0.1966	2.595
0.2000	2.589
0.2033	2.576
0.2066	2.570
0.2100	2.564

$$\Delta H = 1.825$$

$$\Delta t = 4.56$$

Test:	H1-1 Slug out
File:	H1-T2.dat
Round:	KTEST
Column 1:	Elapsed time (min)
Column 2:	Head (ft)
	$t_b = 0.1400$ $t_e = 4.60$
Column 3:	
	$t_b =$ _____ $t_e =$ _____

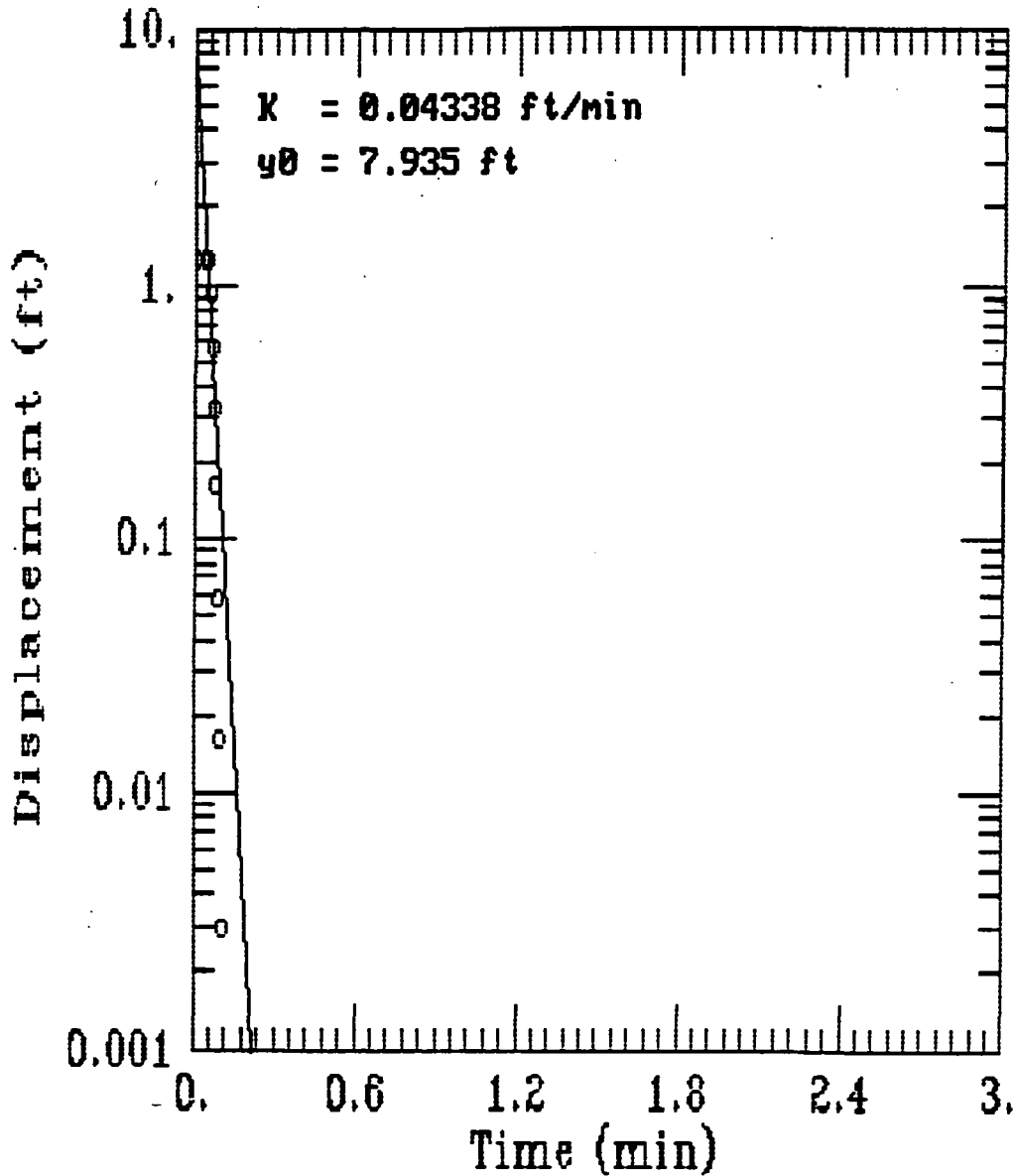
0.2233	2.532
0.2266	2.519
0.2300	2.513
0.2333	2.507
0.2366	2.494
.2400	2.488
0.2433	2.481
0.2466	2.475
0.2500	2.469
0.2533	2.462
0.2566	2.450
0.2600	2.444
0.2633	2.437
0.2666	2.431
0.2700	2.425
0.2733	2.418
0.2766	2.412
0.2800	2.399
0.2833	2.393
0.2866	2.387
0.2900	2.380
0.2933	2.374
0.2966	2.368
0.3000	2.361
0.3033	2.355
0.3066	2.349
0.3100	2.343
0.3133	2.336
0.3166	2.330
0.3200	2.330
0.3233	2.317
.3266	2.317
0.3300	2.311
0.3333	2.305
0.3366	2.273
0.3400	2.241
0.3433	2.216
0.4000	2.191
0.4166	2.166
0.4333	2.140
0.4500	2.122
0.4666	2.096
0.4833	2.077
0.5000	2.058
0.5166	2.039
0.5333	2.020
0.5500	2.008
0.5666	1.989
0.5833	1.976
0.6000	1.957
0.6166	1.945
0.6333	1.932
0.6500	1.913
0.6666	1.900
0.6833	1.894
0.7000	1.882
.7166	1.869
0.7333	1.856
0.7500	1.850
0.7666	1.837
0.7833	1.825
0.8000	1.818
0.8166	1.812

0.8888	1.787
0.8833	1.780
0.9000	1.768
0.9166	1.762
0.9333	1.755
0.9500	1.749
.9666	1.743
0.9833	1.736
1.0000	1.730
1.2000	1.660
1.4000	1.623
1.6000	1.591
1.8000	1.572
2.0000	1.553
2.2000	1.540
2.4000	1.528
2.6000	1.522
2.8000	1.515
3.0000	1.509
3.2000	1.509
3.4000	1.503
3.6000	1.503
3.8000	1.496
4.0000	1.496
4.2000	1.490
4.4000	1.490
4.6000	1.484
4.8000	1.484
5.0000	1.484
5.2000	1.484
5.4000	1.484
5.6000	1.477
.8000	1.477
6.0000	1.477
6.2000	1.477
6.4000	1.477
6.6000	1.477
6.8000	1.477
7.0000	1.477
7.2000	1.471
7.4000	1.471
7.6000	1.471
7.8000	1.477
8.0000	1.477
8.2000	1.477
8.4000	1.477
8.6000	1.477
8.8000	1.477
9.0000	1.477
9.2000	1.484
9.4000	1.484
9.6000	1.484
9.8000	1.484
10.0000	1.484

WELL CLUSTER: H
WELL ID: H2-1
SCREENED INTERVAL: 25-35

TEST METHOD: Banner Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 62.5 ft/day

H2-T2

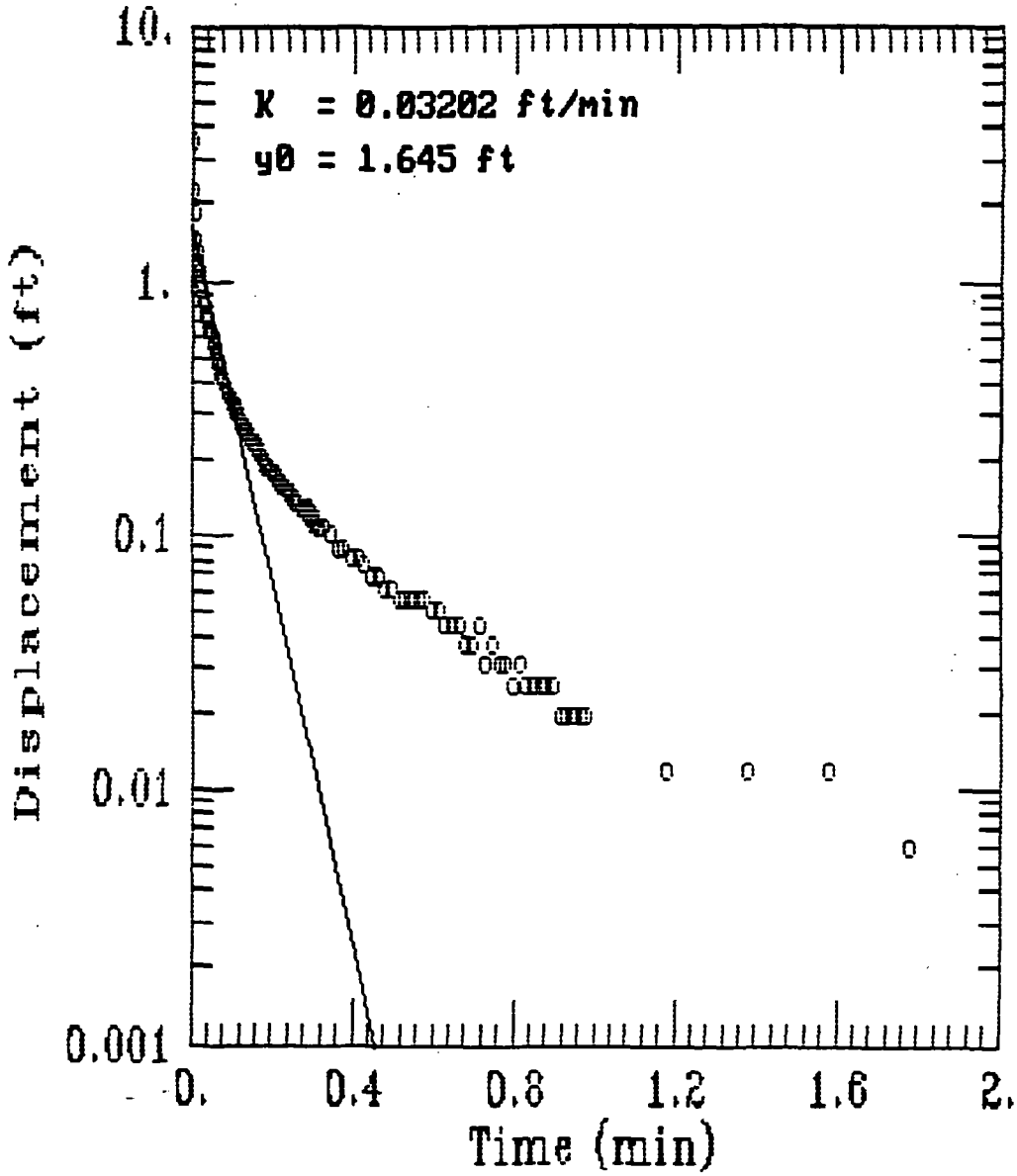


0.3333	0.009
0.3500	0.009
0.3666	0.006
0.3833	0.009
0.4000	0.006
0.4166	0.006
0.4333	0.006
0.4500	0.006
0.4666	0.006
0.4833	0.006
0.5000	0.006
0.5166	0.006
0.5333	0.006
0.5500	0.006
0.5666	0.006
0.5833	0.006
0.6000	0.006
0.6166	0.006
0.6333	0.006
0.6500	0.006
0.6666	0.006
0.6833	0.006
0.7000	0.006
0.7166	0.006
0.7333	0.003
0.7500	0.006
0.7666	0.003
0.7833	0.003
0.8000	0.003
0.8166	0.006
0.8333	0.003
0.8500	0.003
0.8666	0.003
0.8833	0.003
0.9000	0.003
0.9166	0.003
0.9333	0.003
0.9500	0.003
0.9666	0.003
0.9833	0.003
1.0000	0.003
1.2000	0.003
1.4000	0.003
1.6000	0.003
1.8000	0.003
2.0000	0.006
2.2000	0.006

WELL CLUSTER: H
WELL ID: 43
SCREENED INTERVAL: 49.1-54.1

TEST METHOD: Turner Rice
SLUG IN/SLUG OUT: Slug out
K-VALUE: 46.1 ft/Day

H3-T2



0.0000 -0.006
 0.0033 -0.006
 0.0066 0.296
 0.0100 3.215
 0.0133 4.251
 0.0166 1.042
 0.0200 3.480 ←
 0.0233 2.280
 0.0266 1.825
 0.0300 1.434
 0.0333 1.307
 0.0366 1.162
 0.0400 1.073
 0.0433 0.985
 0.0466 0.903
 0.0500 0.846
 0.0533 0.795
 0.0566 0.726
 0.0600 0.694
 0.0633 0.650
 0.0666 0.625
 0.0700 0.587
 0.0733 0.562
 0.0766 0.530
 0.0800 0.517
 0.0833 0.492
 0.0866 0.473
 0.0900 0.454
 0.0933 0.435
 0.0966 0.416
 0.1000 0.410
 0.1033 0.391
 0.1066 0.385
 0.1100 0.366
 0.1133 0.360
 0.1166 0.347
 0.1200 0.341
 0.1233 0.328
 0.1266 0.322
 0.1300 0.309
 0.1333 0.303
 0.1366 0.290
 0.1400 0.284
 0.1433 0.277
 0.1466 0.277
 0.1500 0.265
 0.1533 0.265
 0.1566 0.259
 0.1600 0.252
 0.1633 0.246
 0.1666 0.240
 0.1700 0.233
 0.1733 0.233
 0.1766 0.227
 0.1800 0.221
 0.1833 0.221
 0.1866 0.214
 0.1900 0.208
 0.1933 0.208
 0.1966 0.202

~~2.64~~ 3.480
~~1.78~~

Test:	H3 Slug test	
File:	H3-1a.dat	
Round:	KTEST	
Column 1:	Elapsed time (min)	
Column 2:	Head (ft)	
	$t_0 = 0.0340$	$t_1 = 1.70$
Column 3:	$t_0 =$	$t_1 =$

0.2000	0.202
0.2033	0.195
0.2066	0.189
0.2100	0.189
0.2133	0.189
0.2166	0.183
0.2200	0.176
0.2233	0.176
0.2266	0.176
0.2300	0.170
0.2333	0.164
0.2366	0.164
0.2400	0.164
0.2433	0.157
0.2466	0.157
0.2500	0.157
0.2533	0.151
0.2566	0.151
0.2600	0.145
0.2633	0.145
0.2666	0.145
0.2700	0.139
0.2733	0.139
0.2766	0.139
0.2800	0.132
0.2833	0.132
0.2866	0.132
0.2900	0.126
0.2933	0.126
0.2966	0.126
0.3000	0.126
0.3033	0.126
0.3066	0.126
0.3100	0.126
0.3133	0.120
0.3166	0.120
0.3200	0.120
0.3233	0.113
0.3266	0.113
0.3300	0.113
0.3333	0.107
0.3500	0.107
0.3666	0.101
0.3833	0.088
0.4000	0.088
0.4166	0.082
0.4333	0.082
0.4500	0.075
0.4666	0.069
0.4833	0.069
0.5000	0.063
0.5166	0.063
0.5333	0.056
0.5500	0.056
0.5666	0.056
0.5833	0.056
0.6000	0.056
0.6166	0.050
0.6333	0.050
0.6500	0.044

0.6666	0.044
0.6833	0.044
0.7000	0.037
0.7166	0.037
0.7333	0.044
0.7500	0.031
0.7666	0.037
0.7833	0.031
0.8000	0.031
0.8166	0.025
0.8333	0.031
0.8500	0.025
0.8666	0.025
0.8833	0.025
0.9000	0.025
0.9166	0.025
0.9333	0.019
0.9500	0.019
0.9666	0.019
0.9833	0.019
1.0000	0.019
1.2000	0.012
1.4000	0.012
1.6000	0.012
1.8000	0.006
2.0000	0.006
2.2000	0.006
2.4000	0.006
2.6000	0.012
2.8000	0.000
3.0000	0.000
3.2000	-0.006
3.4000	-0.006
3.6000	-0.006
3.8000	-0.006
4.0000	-0.006
4.2000	-0.006
4.4000	-0.006
4.6000	-0.006
4.8000	0.000
5.0000	0.000
5.2000	-0.006
5.4000	-0.006
5.6000	-0.006
5.8000	-0.006
6.0000	-0.012
6.2000	-0.012
6.4000	-0.006
6.6000	0.000
6.8000	0.000
7.0000	0.000
7.2000	-0.006
7.4000	-0.006
7.6000	0.000
7.8000	0.000
8.0000	0.006
8.2000	0.006
8.4000	0.006
8.6000	0.000
8.8000	0.000

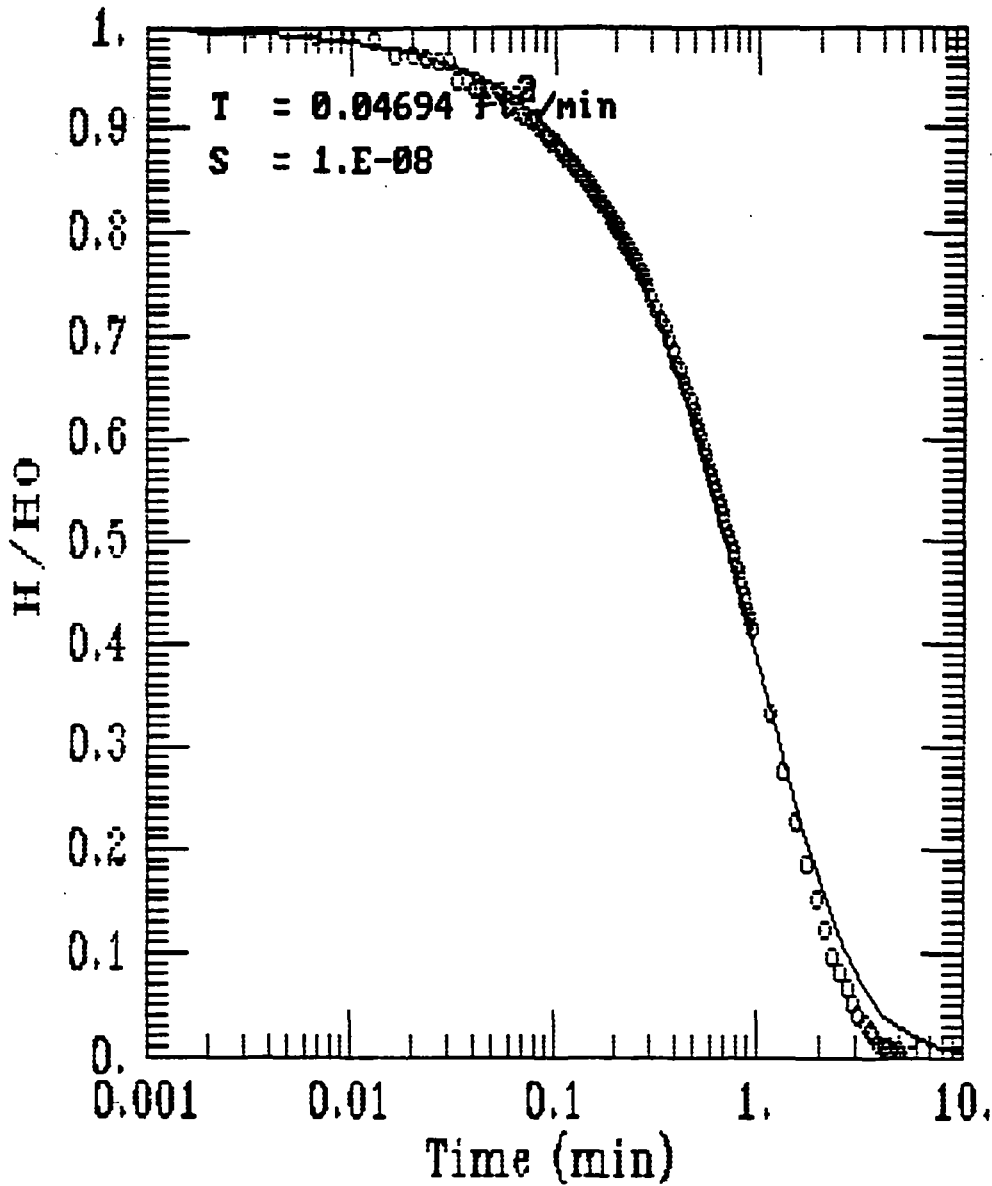
9.0000	0.000
9.2000	0.000
9.4000	0.000
9.6000	0.000
9.8000	0.000
10.0000	-0.006

FIELD TEST VS LOW FLOW SAMPLING DATA

WELL CLUSTER: H
 WELL ID: H4
 SCREENED INTERVAL: 62-72

TEST METHOD: Casper et al.
 SLUG IN/SLUG OUT: slug out
 K-VALUE: 5.72 ft/day

H4-T2



0.0000 0.0000
 0.0033 0.221
 0.0066 0.239
 0.0100 2.424
 0.0133 3.668
 0.0166 4.735
 0.0200 5.575
 0.0233 5.909
 0.0266 3.100
 0.0300 4.117
 0.0333 3.186
 0.0366 2.898
 0.0400 2.500
 0.0433 2.532
 0.0466 2.532
 0.0500 2.513
 0.0533 2.519
 0.0566 2.500
 0.0600 2.462
 0.0633 2.462
 0.0666 2.450
 0.0700 2.443
 0.0733 2.443
 0.0766 2.399
 0.0800 2.399
 0.0833 2.374
 0.0866 2.374
 0.0900 2.374
 0.0933 2.361
 0.0966 2.353
 0.1000 2.345
 0.1033 2.370
 0.1066 2.355
 0.1100 2.320
 0.1133 2.311
 0.1166 2.368
 0.1200 2.292
 0.1233 2.246
 0.1266 2.273
 0.1300 2.273
 0.1333 2.267
 0.1366 2.254
 0.1400 2.249
 0.1433 2.241
 0.1466 2.235
 0.1500 2.229
 0.1533 2.216
 0.1566 2.210
 0.1600 2.203
 0.1633 2.197
 0.1666 2.191
 0.1700 2.184
 0.1733 2.178
 0.1766 2.172
 0.1800 2.166
 0.1833 2.159
 0.1866 2.153
 0.1900 2.147
 0.1933 2.140
 0.1966 2.128
 0.2000 2.128
 0.2033 2.115
 0.2066 2.115
 0.2100 2.109

Start

←

$\Delta H = 2.532$
 $\Delta T = 9.9567$

44-12-191
 Stopped e
 Iteration # 10
 w/derivative success
 Stopped 5
 w/derivative success

Test:	HA	Skj cut
File:	HA-Ta.dat	
Round:	KTEST	
Column 1:	Elapsed time (min)	
Column 2:	Head (ft)	
	$t_0 = 0.0433$	$t_1 = 10.0$
Column 3:		
	$t_0 =$	$t_1 =$

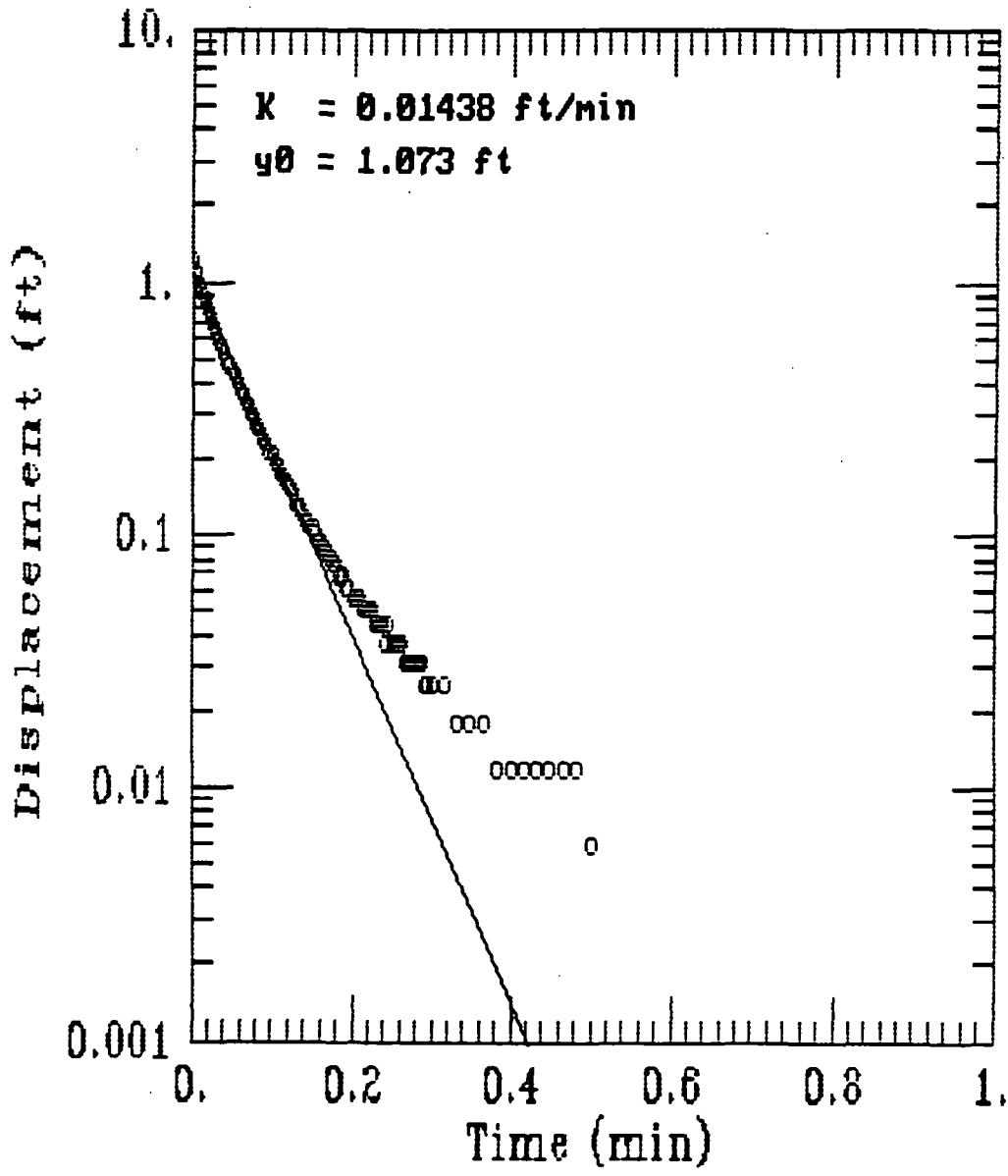
0.2200	2.090
0.2233	2.083
0.2266	2.077
0.2300	2.071
0.2333	2.064
0.2366	2.058
0.2400	2.052
0.2433	2.046
0.2466	2.039
0.2500	2.033
0.2533	2.027
0.2566	2.020
0.2600	2.014
0.2633	2.008
0.2666	2.001
0.2700	2.001
0.2733	1.995
0.2766	1.989
0.2800	1.982
0.2833	1.976
0.2866	1.970
0.2900	1.963
0.2933	1.957
0.2966	1.957
0.3000	1.951
0.3033	1.945
0.3066	1.938
0.3100	1.932
0.3133	1.926
0.3166	1.926
0.3200	1.919
0.3233	1.913
0.3266	1.907
0.3300	1.900
0.3333	1.900
0.3500	1.869
0.3666	1.837
0.3833	1.812
0.4000	1.787
0.4166	1.761
0.4333	1.730
0.4500	1.705
0.4666	1.686
0.4833	1.660
0.5000	1.635
0.5166	1.610
0.5333	1.591
0.5500	1.566
0.5666	1.547
0.5833	1.521
0.6000	1.496
0.6166	1.477
0.6333	1.452
0.6500	1.433
0.6666	1.414
0.6833	1.389
0.7000	1.370
0.7166	1.351
0.7333	1.332
0.7500	1.313
0.7666	1.294
0.7833	1.275
0.8000	1.256
0.8166	1.237

0.8833	1.168
0.9000	1.149
0.9166	1.130
0.9333	1.111
0.9500	1.098
0.9666	1.079
0.9833	1.067
1.0000	1.048
1.2000	0.839
1.4000	0.694
1.6000	0.574
1.8000	0.473
2.0000	0.385
2.2000	0.309
2.4000	0.246
2.6000	0.202
2.8000	0.164
3.0000	0.126
3.2000	0.101
3.4000	0.082
3.6000	0.063
3.8000	0.050
4.0000	0.037
4.2000	0.025
4.4000	0.025
4.6000	0.018
4.8000	0.018
5.0000	0.012
5.2000	0.006
5.4000	0.000
5.6000	0.000
5.8000	0.006
6.0000	0.000
6.2000	0.000
6.4000	0.000
6.6000	0.000
6.8000	0.000
7.0000	0.000
7.2000	0.000
7.4000	0.000
7.6000	0.000
7.8000	0.000
8.0000	0.000
8.2000	0.000
8.4000	0.000
8.6000	0.000
8.8000	0.000
9.0000	0.000
9.2000	0.000
9.4000	0.000
9.6000	-0.006
9.8000	0.000
10.0000	0.000

WELL CLUSTER: I
WELL ID: I1
SCREENED INTERVAL: 2.5-13.5

TEST METHOD: Burton Rice
SLUG IN/SLUG OUT: slug out
K-VALUE: 20.7 ft/day

I1-T2



0.2000	0.088
0.2033	0.082
0.2066	0.082
0.2100	0.075
0.2133	0.075
0.2166	0.069
0.2200	0.069
0.2233	0.069
0.2266	0.063
0.2300	0.063
0.2333	0.056
0.2366	0.056
0.2400	0.056
0.2433	0.056
0.2466	0.050
0.2500	0.050
0.2533	0.050
0.2566	0.050
0.2600	0.050
0.2633	0.044
0.2666	0.044
0.2700	0.044
0.2733	0.044
0.2766	0.037
0.2800	0.044
0.2833	0.037
0.2866	0.037
0.2900	0.037
0.2933	0.037
0.2966	0.037
0.3000	0.031
0.3033	0.031
0.3066	0.031
0.3100	0.031
0.3133	0.031
0.3166	0.031
0.3200	0.031
0.3233	0.031
0.3266	0.025
0.3300	0.025
0.3333	0.025
0.3500	0.025
0.3666	0.018
0.3833	0.018
0.4000	0.018
0.4166	0.012
0.4333	0.012
0.4500	0.012
0.4666	0.012
0.4833	0.012
0.5000	0.012
0.5166	0.012
0.5333	0.006
0.5500	0.006
0.5666	0.006
0.5833	0.006
0.6000	0.006
0.6166	0.006
0.6333	0.006
0.6500	0.006

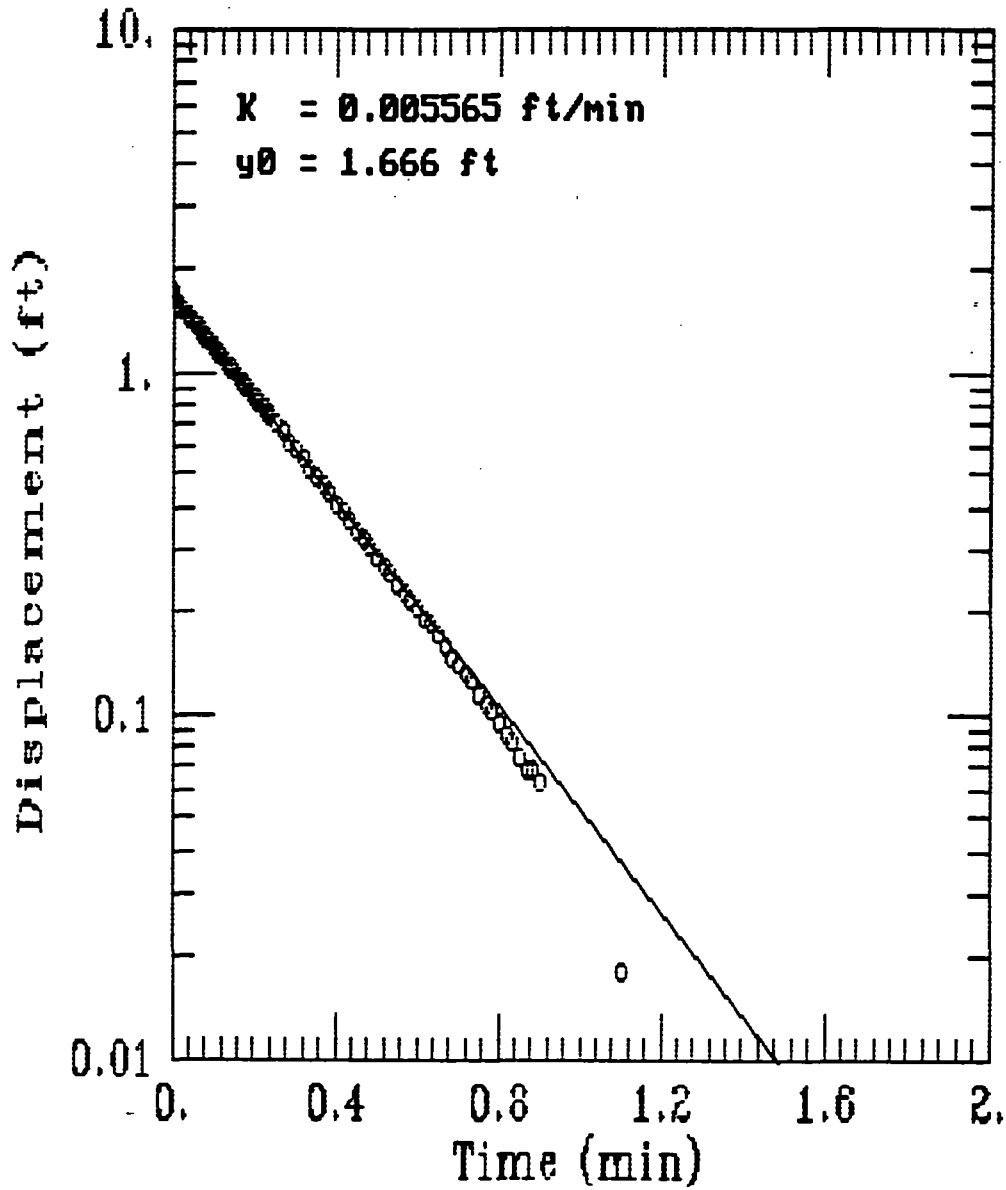
0.6666	0.006
0.6833	0.006
0.7000	0.006
0.7166	0.006
0.7333	0.006
0.7500	0.006
0.7666	0.006
0.7833	0.000
0.8000	0.006
0.8166	0.000
0.8333	0.000
0.8500	0.000
0.8666	0.000
0.8833	0.000
0.9000	0.000
0.9166	0.000
0.9333	0.000
0.9500	0.000
0.9666	0.000
0.9833	0.000
1.0000	0.000
1.2000	0.000
1.4000	-0.006
1.6000	-0.006
1.8000	-0.006
2.0000	-0.006
2.2000	-0.006
2.4000	-0.006
2.6000	-0.006
2.8000	-0.006
3.0000	-0.006
3.2000	-0.012
3.4000	-0.006
3.6000	-0.006
3.8000	-0.012
4.0000	-0.012
4.2000	-0.012
4.4000	-0.012
4.6000	-0.012
4.8000	-0.012
5.0000	-0.012
5.2000	-0.012
5.4000	-0.012
5.6000	-0.012
5.8000	-0.012
6.0000	-0.012
6.2000	-0.012
6.4000	-0.012
6.6000	-0.012
6.8000	-0.012
7.0000	-0.012
7.2000	-0.012
7.4000	-0.012
7.6000	-0.012
7.8000	-0.012
8.0000	-0.012
8.2000	-0.012
8.4000	-0.012
8.6000	-0.012
8.8000	-0.012

9.0000	-0.012
9.2000	-0.012
9.4000	-0.012
9.6000	-0.012
9.8000	-0.006
10.0000	-0.012

WELL CLUSTER: I
WELL ID: I2
SCREENED INTERVAL: 20-25

TEST METHOD: Burner Rise
SLUG IN/SLUG OUT: slug out
K-VALUE: 2.01 ft/day

I2-T2



0.0000 -0.037
 0.0033 -0.025
 0.0066 -0.018
 0.0100 0.031
 0.0133 0.644
 0.0166 0.871
 0.0200 1.010
 0.0233 1.099
 0.0266 1.187
 0.0300 0.814
 0.0333 0.094
 0.0366 0.094
 0.0400 0.846
 0.0433 0.890
 0.0466 0.694
 0.0500 0.821
 0.0533 1.156
 0.0566 1.149
 0.0600 1.061
 0.0633 0.953
 0.0666 0.985
 0.0700 0.966
 0.0733 0.840
 0.0766 0.865
 0.0800 1.187
 0.0833 1.061
 0.0866 1.137
 0.0900 1.389
 0.0933 1.610
 0.0966 1.705
 0.1000 1.680
 0.1033 1.623
 0.1066 1.591
 0.1100 1.579
 0.1133 1.560
 0.1166 1.547
 0.1200 1.522
 0.1233 1.509
 0.1266 1.497
 0.1300 1.471
 0.1333 1.471
 0.1366 1.459
 0.1400 1.434
 0.1433 1.415
 0.1466 1.402
 0.1500 1.389
 0.1533 1.370
 0.1566 1.358
 0.1600 1.339
 0.1633 1.326
 0.1666 1.307
 0.1700 1.295
 0.1733 1.276
 0.1766 1.263
 0.1800 1.250
 0.1833 1.238
 0.1866 1.225
 0.1900 1.212
 0.1933 1.193
 0.1966 1.181

(2) *Id-10.001*

Test:	<u>I2</u>	<u>Slig cut</u>
File:	<u>I2-I2.dat</u>	
Round:	<u>KTEST</u>	
Column 1:	<u>Elapsed time (min)</u>	
Column 2:	<u>Head (ft)</u>	
	<u>t₀ = 0.0966</u>	<u>t₁ = 1.200</u>
Column 3:	_____	
	<u>t₀ = _____</u>	<u>t₁ = _____</u>

$\Delta H = 0.682$
 $\Delta t = 0.00$

@ 1.103

0.2000	1.168
0.2033	1.156
0.2066	1.143
0.2100	1.130
0.2133	1.118
0.2166	1.105
0.2200	1.092
0.2233	1.080
0.2266	1.067
0.2300	1.054
0.2333	1.042
0.2366	1.036
0.2400	1.023
0.2433	1.010
0.2466	0.998
0.2500	0.985
0.2533	0.972
0.2566	0.966
0.2600	0.953
0.2633	0.947
0.2666	0.934
0.2700	0.922
0.2733	0.916
0.2766	0.903
0.2800	0.890
0.2833	0.884
0.2866	0.878
0.2900	0.865
0.2933	0.859
0.2966	0.846
0.3000	0.840
0.3033	0.827
0.3066	0.814
0.3100	0.808
0.3133	0.802
0.3166	0.795
0.3200	0.783
0.3233	0.777
0.3266	0.764
0.3300	0.758
0.3333	0.751
0.3500	0.707
0.3666	0.669
0.3833	0.625
0.4000	0.593
0.4166	0.555
0.4333	0.524
0.4500	0.492
0.4666	0.467
0.4833	0.442
0.5000	0.416
0.5166	0.391
0.5333	0.372
0.5500	0.347
0.5666	0.328
0.5833	0.309
0.6000	0.290
0.6166	0.271
0.6333	0.259
0.6500	0.240

0.6666	0.227
0.6833	0.214
0.7000	0.202
0.7166	0.189
0.7333	0.183
0.7500	0.170
0.7666	0.157
0.7833	0.145
0.8000	0.138
0.8166	0.132
0.8333	0.126
0.8500	0.113
0.8666	0.107
0.8833	0.101
0.9000	0.094
0.9166	0.088
0.9333	0.082
0.9500	0.075
0.9666	0.069
0.9833	0.069
1.0000	0.063
1.2000	0.018
1.4000	0.000
1.6000	-0.012
1.8000	-0.018
2.0000	-0.018
2.2000	-0.025
2.4000	-0.018
2.6000	-0.025
2.8000	-0.025
3.0000	-0.025
3.2000	-0.025
3.4000	-0.025
3.6000	-0.025
3.8000	-0.031
4.0000	-0.031
4.2000	-0.031
4.4000	-0.031
4.6000	-0.031
4.8000	-0.031
5.0000	-0.031
5.2000	-0.031
5.4000	-0.031
5.6000	-0.031
5.8000	-0.031
6.0000	-0.031
6.2000	-0.031
6.4000	-0.031
6.6000	-0.031
6.8000	-0.031
7.0000	-0.031
7.2000	-0.031
7.4000	-0.031
7.6000	-0.031
7.8000	-0.031
8.0000	-0.031
8.2000	-0.031
8.4000	-0.031
8.6000	-0.031
8.8000	-0.025

9.0000	-0.031
9.2000	-0.025
9.4000	-0.031
9.6000	-0.031
9.8000	-0.031
10.0000	-0.025
12.0000	-0.025
14.0000	-0.025
16.0000	-0.025

RAYMARK INDUSTRIES, INC.
STRATFORD, CONNECTICUT
RCRA SECTION 3013 ORDER
DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
0	3.67	4.82	4.94	4.38	4.76	4.52	8173.29	15.78	2224.66	16.35
15	3.66	4.82	4.97	4.40	4.76	4.51	8188.79	15.78	2229.62	16.35
30	3.67	4.83	4.97	4.41	4.77	4.51	8195.68	15.77	2234.25	16.35
45	3.67	4.83	4.97	4.41	4.76	4.51	8202.57	15.78	2236.57	16.34
60	3.67	4.85	4.99	4.43	4.76	4.51	8209.46	15.78	2239.54	16.35
75	3.67	4.85	4.99	4.43	4.76	4.52	8212.40	15.77	2242.52	16.35
90	3.67	4.85	4.99	4.43	4.76	4.52	8215.84	15.77	2242.85	16.36
105	3.67	4.85	4.99	4.43	4.76	4.52	8219.79	15.77	2244.50	16.35
120	3.67	4.85	4.99	4.43	4.74	4.52	8224.46	15.77	2247.81	16.35
135	3.67	4.85	4.99	4.43	4.76	4.52	8227.90	15.77	2249.80	16.34
150	3.67	4.85	4.99	4.45	4.76	4.52	8230.12	15.77	2250.78	16.35
165	3.67	4.85	4.99	4.43	4.76	4.53	8233.07	15.77	2252.77	16.35
180	3.68	4.86	4.99	4.45	4.76	4.53	8234.79	15.77	2252.77	16.36
195	3.68	4.86	4.99	4.45	4.76	4.54	8235.29	15.77	2255.74	16.35
210	3.67	4.86	4.99	4.45	4.76	4.53	8238.73	15.77	2255.74	16.35
225	3.67	4.86	4.99	4.43	4.76	4.53	8238.73	15.77	2257.39	16.35
240	3.67	4.85	4.99	4.43	4.76	4.53	8240.46	15.77	2259.38	16.35
255	3.68	4.86	4.99	4.43	4.77	4.54	8242.18	15.78	2261.04	16.35
270	3.67	4.86	4.97	4.43	4.76	4.53	8243.90	15.77	2263.02	16.35
285	3.67	4.86	4.99	4.45	4.76	4.54	8245.62	15.77	2267.31	16.35
300	3.68	4.86	4.99	4.43	4.76	4.54	8247.34	15.77	2267.31	16.35
315	3.67	4.86	4.99	4.43	4.76	4.53	8247.34	15.77	2267.31	16.35
330	3.67	4.86	4.99	4.43	4.76	4.53	8245.62	15.77	2268.97	16.35
345	3.67	4.86	4.99	4.45	4.76	4.53	8249.07	15.77	2268.97	16.35
360	3.66	4.86	4.99	4.45	4.76	4.53	8252.02	15.77	2270.62	16.35
375	3.66	4.86	4.99	4.45	4.76	4.53	8250.79	15.77	2271.29	16.35
390	3.66	4.88	4.99	4.45	4.76	4.52	8255.46	15.77	2272.61	16.36
405	3.66	4.88	4.99	4.45	4.76	4.51	8253.74	15.77	2274.26	16.35
420	3.65	4.88	4.99	4.45	4.74	4.51	8255.46	15.76	2274.26	16.35
435	3.66	4.88	4.99	4.46	4.74	4.50	8256.69	15.77	2274.26	16.35
450	3.66	4.89	4.99	4.46	4.74	4.50	8255.46	15.76	2276.25	16.35
465	3.66	4.89	5.00	4.48	4.74	4.51	8260.63	15.77	2276.25	16.35
480	3.66	4.89	5.00	4.48	4.74	4.50	8258.91	15.77	2276.25	16.35
495	3.65	4.89	5.00	4.48	4.73	4.49	8261.86	15.76	2276.25	16.35
510	3.65	4.89	5.00	4.48	4.73	4.49	8263.58	15.76	2276.25	16.35
525	3.66	4.91	5.00	4.48	4.73	4.49	8265.80	15.77	2274.60	16.34
540	3.65	4.91	5.00	4.48	4.73	4.49	8265.80	15.77	2274.60	16.35
555	3.66	4.91	5.00	4.48	4.73	4.49	8267.02	15.76	2274.60	16.35
570	3.65	4.91	5.02	4.49	4.73	4.48	8268.75	15.76	2272.95	16.35
585	3.66	4.91	5.00	4.49	4.73	4.48	8270.47	15.76	2272.95	16.34
600	3.65	4.91	5.02	4.49	4.73	4.49	8270.96	15.77	2271.29	16.35
615	3.66	4.91	5.02	4.49	4.73	4.49	8274.41	15.77	2271.29	16.35
630	3.66	4.91	5.00	4.49	4.73	4.49	8274.41	15.77	2271.29	16.34
645	3.66	4.93	5.00	4.49	4.73	4.48	8274.41	15.77	2271.29	16.35
660	3.65	4.91	5.00	4.49	4.73	4.48	8274.41	15.77	2269.98	16.36
675	3.66	4.93	5.02	4.49	4.73	4.48	8276.13	15.77	2267.99	16.35
690	3.66	4.93	5.02	4.49	4.73	4.49	8277.85	15.77	2266.33	16.35
705	3.66	4.93	5.02	4.49	4.73	4.48	8277.36	15.76	2266.33	16.34
720	3.66	4.93	5.02	4.49	4.73	4.48	8277.85	15.77	2266.33	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
735	3.66	4.93	5.02	4.51	4.73	4.48	8277.85	15.77	2266.33	16.34
750	3.66	4.93	5.02	4.51	4.73	4.49	8279.08	15.76	2266.67	16.36
765	3.66	4.93	5.02	4.51	4.73	4.49	8280.81	15.76	2265.01	16.34
780	3.67	4.94	5.02	4.51	4.73	4.50	8281.30	15.77	2265.01	16.34
795	3.67	4.94	5.02	4.51	4.73	4.50	8283.02	15.77	2265.01	16.36
810	3.67	4.94	5.02	4.51	4.73	4.50	8284.74	15.77	2266.33	16.36
825	3.67	4.94	5.02	4.51	4.73	4.51	8284.74	15.77	2265.01	16.36
840	3.67	4.94	5.02	4.51	4.73	4.50	8286.46	15.77	2264.68	16.34
855	3.66	4.94	5.02	4.51	4.73	4.49	8286.46	15.77	2265.01	16.36
870	3.66	4.94	5.02	4.51	4.73	4.50	8288.19	15.77	2265.01	16.34
885	3.66	4.94	5.02	4.51	4.73	4.50	8289.91	15.77	2266.67	16.36
900	3.66	4.94	5.02	4.51	4.73	4.49	8291.63	15.77	2267.99	16.35
915	3.66	4.94	5.02	4.51	4.73	4.50	8291.63	15.77	2267.99	16.36
930	3.67	4.94	5.02	4.51	4.74	4.51	8291.63	15.77	2267.99	16.36
945	3.68	4.94	5.02	4.52	4.74	4.52	8292.86	15.76	2266.67	16.34
960	3.68	4.94	5.02	4.51	4.74	4.53	8295.08	15.77	2266.67	16.34
975	3.67	4.94	5.02	4.51	4.73	4.53	8295.08	15.77	2266.33	16.35
990	3.67	4.96	5.02	4.51	4.74	4.53	8296.80	15.77	2268.32	16.36
1005	3.67	4.94	5.02	4.51	4.74	4.53	8297.54	15.77	2267.99	16.35
1020	3.66	4.94	5.02	4.51	4.73	4.53	8298.52	15.77	2271.63	16.34
1035	3.66	4.94	5.02	4.51	4.74	4.53	8298.52	15.77	2271.63	16.36
1050	3.67	4.94	5.02	4.51	4.74	4.54	8300.24	15.77	2272.61	16.36
1065	3.67	4.94	5.02	4.51	4.74	4.53	8299.76	15.76	2272.95	16.34
1080	3.67	4.96	5.02	4.51	4.74	4.53	8301.48	15.76	2274.94	16.34
1095	3.67	4.94	5.02	4.51	4.74	4.54	8301.48	15.76	2276.25	16.34
1110	3.66	4.94	5.02	4.51	4.74	4.53	8303.69	15.77	2277.91	16.35
1125	3.67	4.96	5.03	4.51	4.74	4.53	8305.41	15.77	2278.25	16.36
1140	3.66	4.94	5.03	4.51	4.74	4.53	8307.13	15.77	2279.90	16.36
1155	3.65	4.94	5.03	4.51	4.73	4.53	8304.92	15.76	2279.90	16.34
1170	3.66	4.96	5.03	4.51	4.74	4.53	8303.69	15.77	2277.91	16.35
1185	3.66	4.96	5.02	4.51	4.73	4.53	8305.41	15.77	2281.55	16.36
1200	3.68	4.96	5.03	4.52	4.74	4.54	8306.65	15.76	2279.56	16.34
1215	3.68	4.97	5.03	4.52	4.74	4.55	8306.65	15.76	2279.56	16.34
1230	3.69	4.97	5.03	4.52	4.74	4.56	8308.37	15.76	2277.91	16.35
1245	3.69	4.96	5.02	4.51	4.74	4.57	8308.86	15.77	2278.25	16.36
1260	3.68	4.96	5.03	4.52	4.76	4.56	8310.09	15.76	2277.91	16.34
1275	3.69	4.96	5.03	4.52	4.74	4.57	8312.30	15.77	2277.91	16.35
1290	3.69	4.96	5.02	4.52	4.74	4.57	8312.30	15.77	2278.25	16.36
1305	3.70	4.96	5.02	4.52	4.74	4.57	8310.58	15.77	2277.91	16.35
1320	3.71	4.96	5.02	4.51	4.74	4.57	8312.30	15.77	2272.95	16.34
1335	3.72	4.96	5.02	4.51	4.74	4.57	8312.30	15.77	2267.99	16.35
1350	3.75	4.97	5.03	4.52	4.76	4.58	8314.02	15.77	2264.68	16.35
1365	3.75	4.97	5.03	4.52	4.76	4.59	8314.02	15.77	2263.02	16.35
1380	3.77	4.97	5.03	4.52	4.76	4.60	8315.26	15.76	2256.41	16.34
1395	3.76	4.97	5.03	4.52	4.76	4.60	8315.75	15.77	2254.76	16.35
1410	3.77	4.97	5.03	4.52	4.76	4.62	8315.75	15.77	2253.10	16.35
1425	3.77	4.97	5.03	4.52	4.76	4.63	8315.75	15.77	2249.80	16.35
1440	3.77	4.99	5.03	4.52	4.76	4.63	8314.02	15.77	2249.80	16.35
1455	3.79	4.99	5.03	4.52	4.77	4.64	8314.02	15.77	2246.49	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
1470	3.81	4.99	5.03	4.54	4.77	4.67	8315.75	15.77	2244.84	16.35
1485	3.82	4.99	5.05	4.54	4.77	4.68	8315.75	15.77	2243.18	16.35
1500	3.80	4.99	5.03	4.54	4.77	4.67	8315.75	15.77	2243.18	16.34
1515	3.82	4.99	5.03	4.54	4.77	4.68	8316.98	15.76	2243.18	16.35
1530	3.89	5.01	5.05	4.54	4.79	4.70	8317.47	15.77	2243.51	16.36
1545	3.99	5.02	5.06	4.56	4.80	4.77	8315.75	15.77	2241.53	16.35
1560	3.93	4.99	5.03	4.54	4.77	4.73	8319.19	15.77	2241.53	16.35
1575	3.92	5.01	5.03	4.54	4.79	4.72	8320.43	15.76	2239.87	16.35
1590	3.90	5.01	5.05	4.54	4.77	4.72	8320.91	15.77	2238.22	16.35
1605	3.90	5.02	5.05	4.56	4.79	4.73	8322.15	15.76	2233.26	16.35
1620	3.92	5.01	5.05	4.54	4.79	4.75	8322.15	15.76	2220.03	16.35
1635	4.00	5.02	5.05	4.56	4.79	4.75	8324.36	15.77	2200.19	16.35
1650	4.01	5.02	5.03	4.56	4.79	4.75	8323.87	15.76	2178.69	16.35
1665	4.06	5.02	5.05	4.56	4.79	4.76	8323.87	15.76	2160.50	16.35
1680	4.13	5.04	5.05	4.56	4.80	4.76	8325.60	15.76	2142.31	16.35
1695	4.20	5.04	5.05	4.56	4.80	4.76	8326.08	15.77	2115.85	16.35
1710	4.23	5.04	5.06	4.56	4.80	4.77	8324.36	15.77	2089.40	16.35
1725	4.24	5.04	5.05	4.56	4.80	4.76	8325.60	15.76	2069.55	16.36
1740	4.26	5.04	5.05	4.57	4.82	4.76	8326.08	15.77	2054.67	16.35
1755	4.28	5.05	5.06	4.57	4.82	4.77	8327.80	15.77	2046.40	16.35
1770	4.30	5.05	5.06	4.57	4.82	4.77	8327.80	15.78	2036.48	16.35
1785	4.31	5.05	5.08	4.59	4.84	4.79	8327.32	15.76	2029.86	16.35
1800	4.28	5.05	5.08	4.57	4.84	4.79	8327.32	15.76	2029.86	16.35
1815	4.25	5.05	5.08	4.59	4.84	4.79	8327.80	15.77	2036.48	16.35
1830	4.20	5.05	5.10	4.59	4.84	4.79	8329.52	15.77	2046.40	16.35
1845	4.13	5.05	5.08	4.59	4.85	4.79	8326.08	15.77	2053.02	16.35
1860	4.09	5.07	5.08	4.59	4.85	4.79	8327.80	15.76	2064.59	16.35
1875	4.05	5.07	5.08	4.60	4.85	4.79	8327.32	15.77	2081.13	16.35
1890	4.03	5.07	5.08	4.60	4.87	4.80	8327.80	15.77	2147.27	16.35
1905	4.00	5.07	5.10	4.60	4.87	4.79	8327.32	15.76	2193.57	16.35
1920	3.97	5.07	5.10	4.62	4.87	4.80	8325.60	15.76	2258.06	16.35
1935	3.95	5.07	5.10	4.62	4.87	4.79	8327.32	15.76	2320.90	16.35
1950	3.92	5.07	5.10	4.62	4.87	4.79	8329.52	15.77	2416.81	16.35
1965	3.90	5.07	5.11	4.62	4.87	4.78	8330.76	15.76	2477.99	16.35
1980	3.88	5.07	5.11	4.62	4.87	4.78	8332.49	15.76	2504.45	16.35
1995	3.87	5.07	5.11	4.64	4.88	4.77	8331.25	15.77	2522.64	16.35
2010	3.86	5.08	5.11	4.64	4.88	4.78	8330.76	15.76	2529.26	16.34
2025	3.85	5.08	5.13	4.64	4.88	4.76	8331.25	15.78	2527.60	16.35
2040	3.85	5.08	5.13	4.65	4.90	4.78	8332.49	15.76	2524.30	16.34
2055	3.84	5.08	5.13	4.65	4.90	4.78	8331.73	15.77	2522.64	16.34
2070	3.82	5.08	5.13	4.65	4.88	4.78	8334.21	15.77	2529.26	16.35
2085	3.81	5.08	5.13	4.65	4.90	4.77	8334.21	15.76	2545.79	16.34
2100	3.80	5.08	5.13	4.65	4.90	4.76	8334.21	15.76	2563.98	16.34
2115	3.80	5.08	5.13	4.65	4.90	4.77	8332.49	15.77	2573.90	16.34
2130	3.80	5.08	5.14	4.65	4.90	4.77	8334.69	15.77	2582.17	16.35
2145	3.80	5.10	5.14	4.67	4.92	4.78	8334.69	15.77	2593.75	16.34
2160	3.80	5.10	5.14	4.67	4.92	4.78	8332.97	15.76	2605.32	16.34
2175	3.80	5.10	5.14	4.67	4.92	4.79	8334.69	15.76	2618.55	16.34
2190	3.78	5.10	5.14	4.67	4.92	4.78	8336.41	15.77	2631.78	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
2205	3.79	5.12	5.16	4.67	4.92	4.80	8336.41	15.77	2641.70	16.35
2220	3.78	5.12	5.16	4.68	4.92	4.79	8335.93	15.76	2648.71	16.34
2235	3.78	5.12	5.14	4.68	4.92	4.79	8334.69	15.76	2653.28	16.34
2250	3.78	5.12	5.16	4.68	4.92	4.79	8338.14	15.77	2659.50	16.35
2265	3.78	5.12	5.16	4.68	4.92	4.79	8339.38	15.76	2663.59	16.34
2280	3.80	5.13	5.16	4.68	4.93	4.79	8338.62	15.77	2664.85	16.34
2295	3.82	5.13	5.16	4.68	4.93	4.80	8341.10	15.76	2666.51	16.34
2310	3.83	5.13	5.16	4.68	4.93	4.81	8341.58	15.77	2669.81	16.34
2325	3.83	5.13	5.16	4.68	4.93	4.81	8341.10	15.76	2669.81	16.34
2340	3.83	5.13	5.16	4.68	4.93	4.81	8343.30	15.77	2669.81	16.34
2355	3.82	5.15	5.16	4.68	4.93	4.80	8343.30	15.77	2668.16	16.34
2370	3.83	5.15	5.16	4.68	4.93	4.81	8343.30	15.77	2668.16	16.34
2385	3.83	5.15	5.16	4.68	4.93	4.80	8341.10	15.76	2668.16	16.34
2400	3.85	5.15	5.18	4.70	4.93	4.81	8341.58	15.77	2664.85	16.34
2415	3.86	5.15	5.18	4.70	4.93	4.82	8341.10	15.76	2663.20	16.34
2430	3.87	5.15	5.18	4.70	4.95	4.82	8341.58	15.77	2659.89	16.34
2445	3.88	5.16	5.18	4.70	4.95	4.82	8339.38	15.76	2656.58	16.34
2460	3.89	5.16	5.18	4.70	4.95	4.82	8341.58	15.77	2654.93	16.34
2475	3.90	5.16	5.18	4.70	4.95	4.83	8343.30	15.77	2651.62	16.34
2490	3.91	5.16	5.19	4.70	4.95	4.84	8341.10	15.76	2649.58	16.35
2505	3.90	5.16	5.18	4.70	4.95	4.83	8342.82	15.77	2648.32	16.34
2520	3.90	5.16	5.18	4.70	4.95	4.84	8343.30	15.77	2648.32	16.34
2535	3.88	5.16	5.18	4.70	4.95	4.83	8344.54	15.76	2648.32	16.34
2550	3.87	5.16	5.18	4.70	4.95	4.83	8343.30	15.76	2648.32	16.34
2565	3.85	5.16	5.18	4.70	4.95	4.82	8345.03	15.77	2651.62	16.34
2580	3.83	5.16	5.18	4.70	4.95	4.81	8345.03	15.77	2653.28	16.35
2595	3.82	5.16	5.18	4.70	4.95	4.80	8346.27	15.76	2653.28	16.34
2610	3.83	5.18	5.18	4.70	4.95	4.80	8346.27	15.76	2652.88	16.35
2625	3.82	5.18	5.18	4.70	4.95	4.80	8346.27	15.76	2649.97	16.34
2640	3.84	5.18	5.19	4.70	4.95	4.81	8345.03	15.76	2646.66	16.35
2655	3.84	5.18	5.18	4.68	4.95	4.81	8346.27	15.76	2643.36	16.34
2670	3.83	5.18	5.19	4.70	4.95	4.80	8346.75	15.76	2640.05	16.34
2685	3.82	5.18	5.18	4.70	4.95	4.81	8349.71	15.76	2636.74	16.34
2700	3.81	5.18	5.18	4.70	4.95	4.80	8349.71	15.76	2635.09	16.34
2715	3.81	5.18	5.18	4.70	4.95	4.80	8346.75	15.76	2630.13	16.34
2730	3.80	5.18	5.18	4.70	4.95	4.80	8350.19	15.78	2628.47	16.34
2745	3.81	5.18	5.18	4.70	4.95	4.80	8351.43	15.76	2625.17	16.34
2760	3.82	5.18	5.18	4.70	4.95	4.79	8349.71	15.76	2623.51	16.34
2775	3.80	5.18	5.18	4.70	4.95	4.77	8348.47	15.76	2618.55	16.34
2790	3.79	5.18	5.16	4.70	4.95	4.77	8351.43	15.76	2616.90	16.35
2805	3.81	5.20	5.18	4.70	4.96	4.78	8351.43	15.77	2613.59	16.35
2820	3.80	5.18	5.16	4.70	4.95	4.77	8352.40	15.77	2610.28	16.34
2835	3.81	5.20	5.18	4.70	4.96	4.79	8351.43	15.76	2606.98	16.34
2850	3.79	5.20	5.18	4.70	4.96	4.77	8351.92	15.77	2605.32	16.35
2865	3.79	5.20	5.18	4.70	4.96	4.77	8351.43	15.76	2602.02	16.34
2880	3.78	5.20	5.18	4.71	4.96	4.77	8350.19	15.77	2602.02	16.35
2895	3.77	5.20	5.16	4.70	4.95	4.77	8351.92	15.77	2600.36	16.34
2910	3.76	5.20	5.18	4.70	4.95	4.76	8351.92	15.77	2595.40	16.34
2925	3.77	5.20	5.18	4.70	4.96	4.76	8351.92	15.76	2593.75	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
2940	3.76	5.20	5.18	4.70	4.96	4.76	8351.92	15.77	2590.44	16.34
2955	3.76	5.20	5.16	4.70	4.96	4.75	8353.64	15.77	2587.13	16.34
2970	3.76	5.20	5.16	4.70	4.95	4.75	8354.88	15.77	2587.13	16.34
2985	3.78	5.20	5.18	4.70	4.96	4.75	8353.64	15.76	2583.83	16.34
3000	3.79	5.20	5.18	4.71	4.96	4.78	8357.08	15.78	2580.52	16.34
3015	3.75	5.20	5.16	4.70	4.96	4.74	8353.64	15.77	2578.48	16.34
3030	3.78	5.21	5.18	4.70	4.96	4.77	8353.64	15.77	2577.21	16.34
3045	3.77	5.20	5.18	4.70	4.96	4.76	8353.64	15.76	2575.56	16.34
3060	3.79	5.21	5.18	4.71	4.96	4.76	8353.64	15.77	2573.90	16.34
3075	3.80	5.21	5.18	4.70	4.96	4.76	8353.64	15.77	2572.25	16.34
3090	3.80	5.20	5.16	4.70	4.96	4.74	8355.36	15.77	2568.94	16.34
3105	3.84	5.21	5.18	4.71	4.96	4.74	8355.36	15.76	2563.98	16.34
3120	3.85	5.21	5.18	4.71	4.96	4.75	8353.64	15.76	2560.68	16.34
3135	3.83	5.20	5.18	4.70	4.95	4.74	8355.84	15.77	2557.37	16.34
3150	3.83	5.21	5.18	4.71	4.96	4.74	8354.88	15.76	2555.71	16.34
3165	3.84	5.23	5.19	4.71	4.98	4.76	8355.36	15.77	2554.06	16.34
3180	3.84	5.23	5.18	4.71	4.96	4.77	8355.36	15.77	2554.06	16.34
3195	3.83	5.21	5.18	4.71	4.96	4.75	8344.54	15.77	2554.06	16.34
3210	3.83	5.21	5.18	4.71	4.96	4.75	8357.56	15.78	2552.41	16.34
3225	3.80	5.21	5.16	4.70	4.96	4.73	8350.19	15.77	2552.41	16.34
3240	3.83	5.23	5.19	4.73	4.96	4.74	8351.92	15.77	2550.75	16.34
3255	3.80	5.21	5.18	4.71	4.96	4.73	8351.92	15.76	2549.10	16.34
3270	3.78	5.21	5.19	4.71	4.95	4.71	8346.27	15.77	2547.45	16.34
3285	3.79	5.21	5.19	4.71	4.96	4.71	8351.92	15.77	2547.45	16.34
3300	3.80	5.23	5.18	4.71	4.96	4.72	8354.88	15.76	2547.45	16.34
3315	3.80	5.23	5.19	4.73	4.96	4.72	8357.08	15.78	2544.14	16.34
3330	3.78	5.21	5.18	4.71	4.96	4.70	8354.88	15.76	2544.14	16.34
3345	3.77	5.21	5.19	4.73	4.96	4.69	8357.08	15.77	2542.49	16.34
3360	3.78	5.23	5.19	4.73	4.96	4.70	8355.36	15.76	2542.49	16.34
3375	3.77	5.23	5.19	4.73	4.96	4.70	8358.33	15.76	2540.83	16.34
3390	3.79	5.23	5.19	4.73	4.96	4.71	8356.60	15.76	2539.18	16.34
3405	3.78	5.23	5.19	4.73	4.96	4.70	8358.33	15.77	2535.87	16.35
3420	3.80	5.24	5.19	4.75	4.96	4.72	8357.08	15.76	2535.87	16.34
3435	3.77	5.21	5.19	4.71	4.95	4.70	8355.36	15.76	2535.87	16.35
3450	3.78	5.23	5.19	4.73	4.96	4.69	8360.05	15.76	2532.56	16.34
3465	3.79	5.23	5.19	4.73	4.96	4.71	8357.08	15.76	2532.19	16.35
3480	3.76	5.23	5.19	4.73	4.96	4.68	8360.05	15.76	2530.91	16.34
3495	3.76	5.23	5.19	4.73	4.96	4.68	8358.33	15.76	2527.60	16.34
3510	3.76	5.23	5.19	4.73	4.96	4.68	8356.60	15.77	2525.95	16.34
3525	3.76	5.23	5.19	4.73	4.96	4.69	8358.33	15.76	2524.67	16.34
3540	3.76	5.23	5.19	4.73	4.96	4.68	8360.53	15.77	2522.64	16.34
3555	3.75	5.23	5.19	4.75	4.96	4.67	8360.05	15.76	2520.99	16.34
3570	3.77	5.24	5.21	4.75	4.96	4.69	8360.53	15.77	2517.68	16.34
3585	3.77	5.24	5.19	4.75	4.96	4.69	8356.60	15.76	2517.68	16.34
3600	3.76	5.24	5.19	4.75	4.96	4.69	8358.33	15.76	2516.03	16.35
3615	3.77	5.24	5.19	4.75	4.96	4.69	8358.33	15.76	2512.72	16.34
3630	3.78	5.24	5.21	4.75	4.96	4.70	8360.53	15.77	2512.72	16.35
3645	3.78	5.24	5.19	4.75	4.96	4.70	8361.77	15.76	2507.76	16.34
3660	3.79	5.24	5.21	4.75	4.98	4.70	8360.53	15.77	2506.11	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
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 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
3675	3.78	5.24	5.19	4.75	4.96	4.70	8361.77	15.76	2504.82	16.34
3690	3.78	5.24	5.19	4.75	4.96	4.69	8360.53	15.77	2501.52	16.34
3705	3.79	5.26	5.21	4.75	4.96	4.70	8360.05	15.76	2501.15	16.34
3720	3.80	5.24	5.21	4.75	4.96	4.70	8360.53	15.77	2501.52	16.34
3735	3.78	5.24	5.21	4.75	4.96	4.70	8361.77	15.76	2499.49	16.34
3750	3.78	5.24	5.21	4.76	4.96	4.70	8360.53	15.77	2498.21	16.34
3765	3.78	5.26	5.21	4.76	4.96	4.70	8361.77	15.76	2496.18	16.34
3780	3.80	5.26	5.22	4.76	4.98	4.73	8361.77	15.76	2497.84	16.34
3795	3.79	5.26	5.21	4.76	4.98	4.73	8361.77	15.76	2496.56	16.34
3810	3.77	5.26	5.21	4.76	4.98	4.72	8360.05	15.76	2499.49	16.34
3825	3.76	5.24	5.21	4.75	4.96	4.71	8361.77	15.76	2499.49	16.34
3840	3.75	5.26	5.21	4.76	4.96	4.71	8363.97	15.77	2501.52	16.34
3855	3.74	5.24	5.21	4.75	4.96	4.70	8361.77	15.76	2500.77	16.35
3870	3.76	5.24	5.21	4.75	4.96	4.71	8363.49	15.76	2497.84	16.34
3885	3.77	5.26	5.21	4.75	4.96	4.70	8361.77	15.76	2494.90	16.34
3900	3.79	5.26	5.21	4.76	4.98	4.71	8362.25	15.77	2491.59	16.34
3915	3.80	5.26	5.21	4.76	4.96	4.70	8363.49	15.76	2488.29	16.34
3930	3.81	5.26	5.21	4.76	4.96	4.70	8363.97	15.77	2486.63	16.34
3945	3.84	5.26	5.22	4.76	4.98	4.71	8363.97	15.77	2481.30	16.34
3960	3.85	5.26	5.22	4.76	4.98	4.71	8361.77	15.76	2477.99	16.35
3975	3.85	5.26	5.21	4.76	4.96	4.70	8361.77	15.76	2473.40	16.34
3990	3.86	5.26	5.22	4.76	4.98	4.71	8361.77	15.76	2466.42	16.34
4005	3.87	5.26	5.22	4.76	4.98	4.71	8363.97	15.77	2463.11	16.34
4020	3.88	5.27	5.22	4.76	4.98	4.71	8363.49	15.76	2456.86	16.34
4035	3.90	5.26	5.22	4.76	4.98	4.72	8363.97	15.77	2449.88	16.34
4050	3.91	5.27	5.22	4.78	4.98	4.72	8365.69	15.77	2443.27	16.34
4065	3.92	5.27	5.22	4.78	4.98	4.73	8365.69	15.77	2436.65	16.34
4080	3.90	5.27	5.22	4.76	4.98	4.73	8365.69	15.77	2432.05	16.34
4095	3.91	5.27	5.22	4.78	4.98	4.73	8367.42	15.77	2426.73	16.35
4110	3.90	5.27	5.22	4.78	4.98	4.73	8367.42	15.77	2423.79	16.34
4125	3.90	5.27	5.22	4.78	4.99	4.74	8363.49	15.76	2421.77	16.34
4140	3.91	5.27	5.22	4.78	4.99	4.75	8365.69	15.77	2422.13	16.34
4155	3.90	5.27	5.22	4.78	4.98	4.74	8367.42	15.77	2423.79	16.34
4170	3.90	5.27	5.22	4.78	4.99	4.74	8367.42	15.77	2430.04	16.34
4185	3.90	5.27	5.22	4.78	4.98	4.74	8369.14	15.77	2433.71	16.34
4200	3.89	5.27	5.22	4.78	4.98	4.74	8363.49	15.76	2439.60	16.35
4215	3.90	5.27	5.22	4.79	4.99	4.73	8365.22	15.76	2445.29	16.34
4230	3.92	5.29	5.24	4.79	4.99	4.76	8365.69	15.77	2446.94	16.34
4245	3.93	5.27	5.24	4.79	4.99	4.75	8365.22	15.76	2446.58	16.34
4260	3.93	5.27	5.24	4.79	4.99	4.75	8365.69	15.77	2444.92	16.34
4275	3.93	5.29	5.24	4.79	4.99	4.74	8365.69	15.77	2443.27	16.34
4290	3.95	5.29	5.24	4.79	4.99	4.76	8367.42	15.77	2441.62	16.35
4305	3.94	5.29	5.24	4.79	4.99	4.76	8367.42	15.77	2436.29	16.35
4320	3.94	5.29	5.24	4.79	4.99	4.76	8367.42	15.77	2431.69	16.34
4335	3.92	5.29	5.24	4.79	4.99	4.77	8367.42	15.77	2432.05	16.34
4350	3.91	5.29	5.24	4.81	5.01	4.77	8368.66	15.76	2433.71	16.34
4365	3.90	5.29	5.24	4.79	4.99	4.77	8369.14	15.77	2438.67	16.34
4380	3.89	5.29	5.25	4.81	5.01	4.77	8370.86	15.77	2446.94	16.34
4395	3.87	5.29	5.24	4.79	5.01	4.76	8369.14	15.77	2456.50	16.34

**RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057**

**TIDAL STUDY FIELD DATA
 G CLUSTER WELLS**

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
4410	3.86	5.29	5.24	4.79	5.01	4.76	8367.42	15.77	2465.13	16.34
4425	3.86	5.29	5.25	4.79	5.01	4.76	8369.14	15.77	2468.07	16.34
4440	3.87	5.29	5.24	4.79	5.01	4.76	8369.14	15.77	2468.07	16.34
4455	3.87	5.29	5.24	4.79	5.01	4.75	8370.86	15.77	2466.42	16.34
4470	3.88	5.29	5.25	4.79	5.01	4.75	8370.38	15.76	2463.48	16.34
4485	3.88	5.29	5.25	4.81	5.01	4.75	8367.42	15.77	2461.82	16.34
4500	3.88	5.29	5.25	4.81	5.01	4.74	8367.42	15.77	2461.46	16.34
4515	3.87	5.29	5.25	4.81	5.01	4.74	8370.38	15.76	2459.81	16.34
4530	3.86	5.29	5.25	4.81	5.01	4.74	8367.42	15.77	2458.15	16.34
4545	3.86	5.29	5.25	4.81	5.01	4.74	8369.14	15.77	2458.15	16.34
4560	3.84	5.29	5.25	4.81	5.03	4.73	8370.38	15.76	2459.81	16.34
4575	3.84	5.29	5.25	4.81	5.03	4.74	8369.14	15.77	2461.82	16.34
4590	3.83	5.29	5.25	4.81	5.01	4.74	8369.14	15.77	2463.48	16.34
4605	3.83	5.29	5.25	4.81	5.03	4.74	8370.86	15.77	2463.48	16.34
4620	3.82	5.29	5.25	4.81	5.03	4.73	8370.86	15.77	2463.11	16.34
4635	3.82	5.29	5.25	4.81	5.03	4.73	8370.86	15.77	2463.11	16.34
4650	3.81	5.29	5.25	4.81	5.03	4.73	8372.58	15.77	2461.46	16.34
4665	3.81	5.29	5.25	4.82	5.03	4.73	8370.86	15.77	2459.81	16.34
4680	3.81	5.29	5.25	4.82	5.03	4.73	8370.38	15.76	2460.17	16.34
4695	3.80	5.29	5.25	4.82	5.03	4.72	8368.66	15.76	2460.17	16.34
4710	3.79	5.29	5.25	4.82	5.03	4.72	8370.38	15.76	2459.81	16.34
4725	3.78	5.29	5.25	4.81	5.03	4.72	8374.31	15.77	2460.17	16.34
4740	3.77	5.29	5.25	4.82	5.03	4.72	8374.31	15.77	2458.15	16.34
4755	3.78	5.29	5.27	4.82	5.03	4.72	8374.31	15.77	2458.15	16.34
4770	3.77	5.29	5.25	4.82	5.03	4.71	8373.83	15.76	2456.50	16.34
4785	3.76	5.29	5.25	4.82	5.03	4.70	8376.03	15.77	2455.21	16.34
4800	3.76	5.29	5.27	4.82	5.03	4.70	8372.58	15.77	2455.21	16.34
4815	3.75	5.29	5.25	4.82	5.03	4.69	8372.58	15.77	2453.55	16.34
4830	3.76	5.31	5.27	4.82	5.03	4.69	8374.31	15.77	2451.90	16.34
4845	3.76	5.31	5.27	4.84	5.03	4.70	8373.83	15.76	2450.25	16.34
4860	3.75	5.31	5.27	4.82	5.03	4.69	8373.83	15.76	2449.88	16.35
4875	3.75	5.31	5.27	4.84	5.03	4.69	8376.03	15.77	2450.25	16.33
4890	3.75	5.31	5.27	4.84	5.03	4.69	8376.03	15.77	2446.94	16.34
4905	3.74	5.31	5.27	4.82	5.03	4.69	8377.75	15.77	2446.94	16.34
4920	3.74	5.31	5.27	4.84	5.03	4.69	8379.47	15.77	2446.94	16.34
4935	3.74	5.31	5.27	4.84	5.03	4.68	8376.03	15.77	2448.59	16.34
4950	3.74	5.31	5.29	4.84	5.03	4.69	8374.31	15.77	2445.29	16.33
4965	3.75	5.32	5.29	4.84	5.03	4.69	8372.58	15.77	2443.63	16.33
4980	3.74	5.31	5.29	4.84	5.03	4.68	8376.03	15.77	2441.98	16.33
4995	3.74	5.32	5.29	4.84	5.03	4.68	8374.31	15.77	2441.98	16.33
5010	3.74	5.32	5.29	4.84	5.03	4.69	8373.83	15.76	2439.96	16.35
5025	3.73	5.31	5.29	4.86	5.03	4.69	8376.03	15.77	2438.31	16.34
5040	3.73	5.31	5.29	4.84	5.03	4.68	8379.00	15.76	2435.36	16.34
5055	3.73	5.32	5.29	4.86	5.03	4.68	8374.31	15.77	2437.02	16.34
5070	3.73	5.32	5.29	4.86	5.03	4.68	8375.55	15.76	2433.71	16.34
5085	3.72	5.32	5.29	4.84	5.03	4.68	8377.75	15.77	2433.71	16.34
5100	3.73	5.32	5.29	4.84	5.03	4.67	8377.75	15.77	2428.75	16.33
5115	3.73	5.32	5.29	4.86	5.03	4.67	8376.03	15.77	2428.75	16.34
5130	3.72	5.32	5.29	4.86	5.03	4.67	8379.47	15.77	2425.44	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
5145	3.73	5.32	5.27	4.86	5.03	4.67	8381.20	15.76	2426.73	16.34
5160	3.73	5.32	5.29	4.86	5.03	4.69	8379.47	15.77	2423.79	16.34
5175	3.73	5.32	5.29	4.86	5.03	4.69	8379.47	15.77	2423.79	16.34
5190	3.73	5.32	5.29	4.86	5.03	4.68	8379.47	15.77	2420.48	16.33
5205	3.73	5.32	5.29	4.86	5.03	4.69	8379.47	15.77	2421.77	16.34
5220	3.73	5.32	5.29	4.86	5.04	4.69	8379.00	15.76	2418.82	16.33
5235	3.73	5.32	5.29	4.86	5.03	4.69	8379.47	15.77	2418.82	16.34
5250	3.72	5.32	5.29	4.86	5.03	4.69	8381.20	15.77	2416.81	16.34
5265	3.73	5.32	5.29	4.86	5.03	4.69	8381.20	15.77	2415.52	16.34
5280	3.72	5.32	5.29	4.86	5.03	4.70	8382.92	15.77	2413.86	16.33
5295	3.72	5.32	5.29	4.86	5.03	4.70	8383.69	15.77	2415.52	16.33
5310	3.72	5.32	5.29	4.86	5.03	4.69	8385.89	15.77	2412.21	16.33
5325	3.72	5.32	5.29	4.86	5.03	4.69	8381.20	15.77	2411.85	16.34
5340	3.72	5.32	5.29	4.86	5.04	4.69	8382.92	15.77	2408.90	16.34
5355	3.72	5.32	5.29	4.86	5.04	4.69	8379.47	15.77	2412.21	16.33
5370	3.71	5.32	5.29	4.86	5.03	4.69	8382.44	15.77	2408.90	16.33
5385	3.72	5.32	5.29	4.86	5.03	4.69	8380.72	15.76	2407.25	16.33
5400	3.71	5.32	5.29	4.86	5.03	4.68	8382.92	15.77	2405.59	16.33
5415	3.71	5.32	5.29	4.86	5.03	4.68	8382.92	15.77	2405.59	16.33
5430	3.71	5.32	5.29	4.86	5.03	4.68	8384.64	15.77	2405.59	16.33
5445	3.71	5.32	5.29	4.86	5.04	4.67	8382.92	15.77	2405.59	16.33
5460	3.71	5.32	5.29	4.86	5.03	4.67	8384.64	15.77	2402.29	16.34
5475	3.71	5.32	5.29	4.86	5.03	4.67	8384.16	15.76	2402.29	16.34
5490	3.71	5.32	5.29	4.86	5.03	4.67	8384.16	15.76	2403.94	16.33
5505	3.71	5.32	5.29	4.86	5.03	4.67	8382.92	15.77	2403.94	16.34
5520	3.71	5.32	5.29	4.86	5.03	4.67	8384.16	15.77	2403.94	16.33
5535	3.71	5.32	5.27	4.86	5.03	4.67	8384.64	15.77	2403.94	16.34
5550	3.71	5.32	5.27	4.84	5.04	4.67	8384.64	15.77	2400.63	16.33
5565	3.71	5.31	5.27	4.84	5.03	4.67	8385.89	15.76	2403.94	16.34
5580	3.71	5.31	5.27	4.86	5.03	4.67	8382.44	15.76	2402.29	16.33
5595	3.72	5.31	5.27	4.84	5.04	4.68	8384.64	15.77	2405.24	16.34
5610	3.71	5.31	5.25	4.84	5.04	4.67	8384.64	15.77	2403.94	16.34
5625	3.71	5.31	5.25	4.84	5.04	4.68	8386.36	15.77	2405.24	16.34
5640	3.71	5.31	5.25	4.84	5.04	4.68	8388.08	15.77	2405.59	16.33
5655	3.72	5.31	5.25	4.84	5.04	4.67	8387.61	15.76	2405.24	16.34
5670	3.73	5.31	5.25	4.84	5.04	4.69	8389.81	15.77	2403.58	16.34
5685	3.73	5.31	5.25	4.84	5.04	4.69	8384.64	15.76	2401.93	16.34
5700	3.73	5.31	5.25	4.84	5.04	4.69	8386.36	15.77	2401.93	16.34
5715	3.72	5.29	5.24	4.82	5.04	4.68	8387.61	15.76	2398.62	16.33
5730	3.72	5.29	5.24	4.82	5.04	4.69	8388.08	15.77	2400.27	16.34
5745	3.71	5.29	5.24	4.82	5.04	4.69	8385.89	15.76	2401.93	16.34
5760	3.72	5.29	5.24	4.82	5.06	4.69	8386.36	15.76	2400.27	16.34
5775	3.71	5.27	5.24	4.82	5.04	4.69	8385.89	15.76	2401.93	16.34
5790	3.72	5.29	5.24	4.82	5.06	4.70	8389.33	15.76	2400.27	16.34
5805	3.72	5.27	5.22	4.81	5.06	4.69	8387.61	15.76	2398.62	16.34
5820	3.73	5.27	5.22	4.79	5.04	4.70	8388.08	15.76	2400.27	16.34
5835	3.73	5.27	5.24	4.81	5.06	4.71	8389.81	15.76	2398.27	16.34
5850	3.73	5.29	5.24	4.81	5.06	4.71	8389.81	15.77	2395.31	16.34
5865	3.72	5.27	5.22	4.81	5.06	4.70	8389.81	15.77	2398.62	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
5880	3.71	5.27	5.22	4.81	5.04	4.70	8386.36	15.76	2400.27	16.34
5895	3.73	5.27	5.24	4.81	5.06	4.71	8388.08	15.77	2398.62	16.34
5910	3.71	5.27	5.22	4.81	5.04	4.70	8388.08	15.77	2400.27	16.34
5925	3.72	5.29	5.24	4.81	5.06	4.71	8388.08	15.77	2398.62	16.34
5940	3.72	5.27	5.24	4.81	5.06	4.71	8388.56	15.78	2396.97	16.34
5955	3.71	5.27	5.22	4.82	5.06	4.71	8389.81	15.77	2396.97	16.34
5970	3.71	5.27	5.22	4.81	5.06	4.71	8391.53	15.76	2396.61	16.34
5985	3.72	5.27	5.24	4.82	5.06	4.71	8391.53	15.76	2393.31	16.34
6000	3.72	5.27	5.24	4.81	5.06	4.72	8391.53	15.77	2394.96	16.34
6015	3.72	5.27	5.22	4.81	5.06	4.71	8393.25	15.77	2396.97	16.34
6030	3.71	5.27	5.24	4.82	5.06	4.71	8391.53	15.77	2396.97	16.34
6045	3.71	5.29	5.24	4.82	5.06	4.71	8391.53	15.76	2396.97	16.34
6060	3.71	5.27	5.24	4.82	5.06	4.72	8391.53	15.76	2393.66	16.34
6075	3.71	5.27	5.24	4.82	5.06	4.71	8393.25	15.76	2393.31	16.34
6090	3.71	5.27	5.24	4.82	5.06	4.71	8391.53	15.76	2392.01	16.34
6105	3.71	5.27	5.24	4.82	5.06	4.71	8391.53	15.77	2393.66	16.34
6120	3.71	5.27	5.24	4.82	5.06	4.70	8389.81	15.76	2393.66	16.34
6135	3.71	5.27	5.24	4.82	5.06	4.70	8388.08	15.77	2393.66	16.34
6150	3.70	5.27	5.22	4.82	5.06	4.70	8393.25	15.77	2395.31	16.34
6165	3.70	5.27	5.24	4.82	5.06	4.70	8394.97	15.76	2395.31	16.34
6180	3.70	5.27	5.24	4.82	5.06	4.69	8393.25	15.76	2396.97	16.34
6195	3.70	5.27	5.24	4.82	5.06	4.69	8394.97	15.76	2395.31	16.34
6210	3.70	5.27	5.24	4.82	5.04	4.69	8394.97	15.76	2392.01	16.34
6225	3.70	5.29	5.24	4.82	5.04	4.68	8393.25	15.76	2393.66	16.34
6240	3.70	5.27	5.24	4.82	5.04	4.68	8396.22	15.76	2392.01	16.34
6255	3.69	5.29	5.24	4.82	5.04	4.67	8393.25	15.76	2390.35	16.34
6270	3.69	5.29	5.25	4.84	5.04	4.66	8396.70	15.76	2388.70	16.34
6285	3.69	5.29	5.25	4.84	5.04	4.66	8392.00	15.77	2392.01	16.34
6300	3.70	5.29	5.25	4.84	5.04	4.66	8396.22	15.76	2392.01	16.34
6315	3.70	5.29	5.25	4.84	5.04	4.66	8398.42	15.77	2390.71	16.34
6330	3.70	5.29	5.25	4.84	5.04	4.66	8394.97	15.77	2392.01	16.34
6345	3.70	5.29	5.27	4.86	5.03	4.66	8396.70	15.77	2393.31	16.34
6360	3.70	5.31	5.27	4.86	5.04	4.66	8397.94	15.76	2394.02	16.34
6375	3.70	5.31	5.27	4.86	5.03	4.66	8393.25	15.77	2392.36	16.34
6390	3.70	5.31	5.27	4.86	5.03	4.66	8394.97	15.77	2392.36	16.34
6405	3.70	5.31	5.27	4.86	5.03	4.66	8396.70	15.77	2394.96	16.34
6420	3.70	5.31	5.27	4.87	5.03	4.66	8398.42	15.77	2394.02	16.34
6435	3.70	5.31	5.27	4.87	5.03	4.66	8398.42	15.77	2390.71	16.34
6450	3.70	5.32	5.27	4.86	5.03	4.66	8396.70	15.77	2394.02	16.34
6465	3.70	5.32	5.29	4.87	5.03	4.66	8398.42	15.76	2393.66	16.34
6480	3.70	5.31	5.29	4.87	5.03	4.67	8396.22	15.77	2394.02	16.34
6495	3.71	5.31	5.29	4.87	5.03	4.67	8394.97	15.77	2390.71	16.34
6510	3.71	5.32	5.29	4.87	5.03	4.67	8399.67	15.77	2392.36	16.34
6525	3.71	5.32	5.29	4.87	5.03	4.68	8397.94	15.77	2392.01	16.34
6540	3.71	5.32	5.29	4.87	5.03	4.68	8399.67	15.77	2390.71	16.34
6555	3.71	5.32	5.29	4.87	5.04	4.68	8399.67	15.77	2392.01	16.34
6570	3.71	5.32	5.29	4.89	5.03	4.69	8399.67	15.77	2395.31	16.34
6585	3.71	5.32	5.29	4.89	5.03	4.69	8399.67	15.76	2393.66	16.34
6600	3.70	5.32	5.29	4.87	5.03	4.68	8401.39	15.76	2392.36	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
6615	3.71	5.32	5.29	4.89	5.03	4.69	8399.67	15.77	2390.71	16.33
6630	3.71	5.32	5.29	4.89	5.03	4.70	8399.67	15.77	2390.71	16.33
6645	3.71	5.32	5.29	4.89	5.04	4.70	8401.39	15.76	2389.05	16.33
6660	3.71	5.32	5.29	4.89	5.03	4.71	8401.39	15.77	2390.71	16.33
6675	3.71	5.32	5.29	4.89	5.03	4.71	8401.39	15.77	2392.36	16.33
6690	3.71	5.32	5.29	4.89	5.03	4.71	8401.39	15.76	2392.36	16.33
6705	3.71	5.32	5.29	4.89	5.04	4.71	8401.39	15.77	2392.36	16.33
6720	3.70	5.32	5.29	4.89	5.03	4.71	8401.39	15.76	2395.31	16.34
6735	3.70	5.32	5.29	4.89	5.03	4.71	8399.67	15.77	2394.02	16.33
6750	3.70	5.32	5.29	4.89	5.03	4.71	8403.11	15.76	2393.66	16.34
6765	3.70	5.32	5.29	4.89	5.03	4.71	8399.67	15.76	2392.36	16.33
6780	3.70	5.32	5.29	4.89	5.03	4.71	8401.39	15.76	2392.01	16.34
6795	3.70	5.32	5.29	4.89	5.03	4.71	8401.39	15.77	2393.66	16.34
6810	3.70	5.32	5.29	4.89	5.03	4.71	8401.39	15.77	2394.02	16.33
6825	3.70	5.32	5.29	4.89	5.03	4.71	8401.39	15.76	2395.67	16.33
6840	3.70	5.32	5.29	4.87	5.03	4.71	8403.11	15.76	2394.02	16.33
6855	3.70	5.32	5.29	4.89	5.03	4.70	8401.39	15.77	2394.02	16.33
6870	3.69	5.32	5.29	4.87	5.03	4.70	8399.67	15.77	2392.36	16.33
6885	3.69	5.31	5.29	4.89	5.03	4.69	8401.39	15.77	2392.36	16.33
6900	3.69	5.31	5.29	4.89	5.03	4.69	8401.39	15.76	2396.97	16.34
6915	3.70	5.31	5.29	4.87	5.03	4.70	8399.67	15.77	2398.62	16.34
6930	3.70	5.31	5.27	4.87	5.03	4.70	8401.39	15.77	2398.62	16.34
6945	3.69	5.31	5.27	4.87	5.03	4.70	8401.39	15.77	2398.62	16.34
6960	3.69	5.31	5.27	4.87	5.03	4.70	8401.39	15.77	2400.63	16.33
6975	3.70	5.31	5.25	4.86	5.03	4.70	8401.39	15.77	2400.27	16.34
6990	3.69	5.29	5.25	4.86	5.03	4.71	8401.39	15.77	2397.32	16.34
7005	3.70	5.29	5.25	4.86	5.03	4.70	8401.86	15.77	2398.62	16.35
7020	3.70	5.29	5.25	4.84	5.03	4.70	8400.14	15.77	2398.98	16.33
7035	3.70	5.29	5.24	4.86	5.03	4.71	8403.11	15.77	2398.98	16.34
7050	3.70	5.29	5.24	4.84	5.04	4.71	8401.86	15.77	2398.98	16.33
7065	3.70	5.29	5.24	4.86	5.04	4.71	8401.86	15.77	2398.98	16.34
7080	3.70	5.27	5.24	4.84	5.04	4.71	8403.59	15.77	2400.27	16.34
7095	3.70	5.27	5.24	4.84	5.04	4.72	8403.11	15.76	2398.98	16.33
7110	3.70	5.27	5.22	4.84	5.04	4.72	8403.11	15.76	2400.27	16.34
7125	3.71	5.27	5.22	4.84	5.04	4.73	8403.11	15.76	2400.27	16.34
7140	3.71	5.27	5.22	4.84	5.06	4.73	8404.84	15.76	2401.93	16.34
7155	3.71	5.27	5.22	4.84	5.04	4.73	8403.59	15.76	2400.27	16.34
7170	3.71	5.27	5.22	4.84	5.06	4.74	8403.59	15.77	2400.27	16.34
7185	3.71	5.27	5.22	4.84	5.06	4.75	8404.84	15.76	2401.93	16.34
7200	3.72	5.27	5.22	4.84	5.06	4.76	8403.59	15.76	2400.27	16.34
7215	3.72	5.27	5.22	4.84	5.06	4.76	8401.86	15.77	2401.93	16.34
7230	3.72	5.26	5.22	4.82	5.06	4.77	8403.59	15.77	2401.93	16.34
7245	3.71	5.24	5.19	4.81	5.06	4.77	8404.84	15.76	2401.93	16.34
7260	3.71	5.24	5.19	4.79	5.06	4.78	8403.59	15.77	2401.57	16.34
7275	3.72	5.24	5.19	4.81	5.07	4.79	8402.34	15.77	2403.23	16.35
7290	3.71	5.24	5.19	4.81	5.07	4.78	8402.34	15.77	2401.57	16.32
7305	3.72	5.24	5.21	4.81	5.07	4.79	8402.34	15.77	2401.57	16.35
7320	3.72	5.24	5.21	4.81	5.07	4.79	8402.34	15.77	2403.23	16.35
7335	3.72	5.24	5.21	4.81	5.07	4.80	8402.34	15.77	2401.57	16.34

**RAYMARK INDUSTRIES, INC.
STRATFORD, CONNECTICUT
RCRA SECTION 3013 ORDER
DOCKET NO. I-87-1057**

**TIDAL STUDY FIELD DATA
G CLUSTER WELLS**

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
7350	3.72	5.26	5.21	4.81	5.07	4.80	8404.06	15.77	2401.93	16.34
7365	3.72	5.24	5.21	4.81	5.07	4.81	8404.06	15.77	2404.88	16.34
7380	3.72	5.24	5.21	4.81	5.07	4.82	8402.34	15.77	2401.57	16.35
7395	3.72	5.24	5.21	4.81	5.07	4.82	8402.34	15.77	2401.57	16.35
7410	3.72	5.24	5.21	4.82	5.07	4.82	8402.34	15.77	2402.87	16.33
7425	3.72	5.24	5.21	4.81	5.07	4.83	8404.06	15.77	2405.24	16.34
7440	3.72	5.26	5.21	4.82	5.09	4.83	8404.06	15.77	2402.87	16.34
7455	3.71	5.24	5.21	4.81	5.07	4.83	8405.78	15.77	2403.23	16.35
7470	3.72	5.26	5.21	4.81	5.07	4.84	8404.06	15.77	2402.87	16.34
7485	3.71	5.24	5.21	4.82	5.07	4.83	8404.06	15.77	2404.88	16.34
7500	3.71	5.24	5.21	4.82	5.07	4.83	8405.78	15.77	2404.88	16.35
7515	3.71	5.24	5.21	4.82	5.07	4.83	8405.31	15.77	2404.88	16.35
7530	3.71	5.26	5.21	4.82	5.07	4.84	8405.78	15.77	2403.23	16.35
7545	3.71	5.26	5.21	4.82	5.07	4.83	8405.31	15.77	2401.57	16.34
7560	3.71	5.26	5.22	4.84	5.07	4.84	8405.78	15.77	2401.57	16.34
7575	3.71	5.26	5.22	4.84	5.07	4.84	8405.78	15.77	2401.57	16.34
7590	3.71	5.26	5.22	4.84	5.07	4.84	8403.59	15.76	2403.58	16.34
7605	3.71	5.26	5.22	4.84	5.07	4.84	8405.31	15.77	2403.23	16.35
7620	3.71	5.26	5.22	4.84	5.07	4.84	8405.31	15.76	2405.24	16.34
7635	3.71	5.26	5.24	4.84	5.06	4.84	8407.03	15.76	2404.88	16.34
7650	3.71	5.26	5.24	4.84	5.06	4.84	8407.03	15.76	2404.88	16.34
7665	3.70	5.26	5.24	4.84	5.06	4.84	8407.50	15.77	2403.58	16.34
7680	3.70	5.26	5.24	4.84	5.06	4.84	8408.75	15.77	2405.24	16.33
7695	3.70	5.26	5.24	4.84	5.06	4.83	8407.03	15.76	2403.58	16.34
7710	3.70	5.27	5.24	4.86	5.06	4.84	8404.06	15.77	2401.93	16.34
7725	3.70	5.26	5.24	4.84	5.06	4.84	8406.56	15.76	2401.93	16.34
7740	3.70	5.27	5.24	4.86	5.06	4.84	8404.06	15.77	2403.58	16.34
7755	3.70	5.27	5.24	4.86	5.06	4.83	8404.84	15.76	2405.24	16.34
7770	3.70	5.27	5.24	4.86	5.06	4.83	8406.56	15.76	2406.89	16.34
7785	3.70	5.27	5.24	4.86	5.06	4.83	8407.03	15.77	2408.54	16.34
7800	3.70	5.27	5.24	4.86	5.04	4.83	8408.28	15.76	2405.59	16.34
7815	3.70	5.27	5.24	4.86	5.06	4.83	8408.28	15.76	2403.58	16.34
7830	3.70	5.27	5.24	4.86	5.06	4.84	8408.28	15.76	2405.59	16.34
7845	3.70	5.27	5.24	4.86	5.04	4.84	8407.03	15.77	2405.24	16.34
7860	3.70	5.27	5.24	4.86	5.06	4.84	8408.75	15.77	2405.24	16.33
7875	3.70	5.27	5.24	4.86	5.06	4.84	8408.28	15.76	2405.24	16.34
7890	3.70	5.27	5.24	4.86	5.06	4.84	8408.28	15.76	2405.24	16.34
7905	3.71	5.27	5.24	4.86	5.06	4.85	8410.47	15.77	2406.89	16.34
7920	3.71	5.27	5.24	4.86	5.06	4.86	8407.03	15.77	2405.24	16.34
7935	3.71	5.27	5.25	4.86	5.06	4.86	8407.03	15.77	2405.59	16.34
7950	3.71	5.27	5.24	4.86	5.06	4.86	8408.75	15.77	2405.24	16.33
7965	3.71	5.27	5.24	4.86	5.06	4.87	8408.75	15.77	2405.24	16.33
7980	3.71	5.27	5.24	4.86	5.06	4.87	8408.75	15.77	2405.24	16.34
7995	3.71	5.27	5.24	4.86	5.06	4.87	8407.03	15.77	2405.24	16.34
8010	3.72	5.27	5.24	4.86	5.06	4.88	8406.56	15.76	2406.89	16.33
8025	3.71	5.27	5.25	4.86	5.06	4.89	8408.28	15.76	2406.89	16.34
8040	3.71	5.27	5.24	4.87	5.06	4.89	8408.28	15.76	2405.24	16.33
8055	3.71	5.27	5.25	4.87	5.06	4.89	8408.75	15.77	2406.89	16.34
8070	3.71	5.27	5.24	4.86	5.06	4.89	8408.28	15.76	2408.90	16.34

**RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057**

**TIDAL STUDY FIELD DATA
 G CLUSTER WELLS**

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
8085	3.71	5.27	5.25	4.86	5.06	4.89	8408.28	15.76	2406.89	16.34
8100	3.71	5.27	5.24	4.87	5.06	4.89	8408.28	15.76	2406.89	16.34
8115	3.71	5.27	5.25	4.86	5.06	4.90	8408.28	15.76	2406.89	16.34
8130	3.71	5.27	5.25	4.87	5.06	4.90	8410.00	15.76	2406.89	16.34
8145	3.71	5.27	5.24	4.87	5.06	4.91	8407.03	15.77	2405.24	16.34
8160	3.71	5.27	5.24	4.87	5.06	4.91	8408.75	15.77	2408.54	16.33
8175	3.71	5.27	5.25	4.87	5.06	4.91	8408.75	15.77	2410.20	16.33
8190	3.71	5.27	5.24	4.87	5.06	4.91	8408.75	15.77	2408.90	16.34
8205	3.71	5.26	5.25	4.87	5.06	4.92	8407.03	15.77	2406.89	16.34
8220	3.71	5.27	5.25	4.87	5.06	4.92	8406.56	15.76	2408.54	16.34
8235	3.71	5.26	5.24	4.87	5.06	4.92	8408.75	15.77	2408.54	16.34
8250	3.70	5.27	5.24	4.87	5.06	4.92	8408.75	15.77	2410.20	16.34
8265	3.70	5.26	5.24	4.86	5.06	4.91	8407.03	15.77	2410.55	16.33
8280	3.70	5.26	5.24	4.87	5.06	4.91	8408.75	15.77	2408.54	16.34
8295	3.70	5.26	5.24	4.86	5.06	4.90	8408.28	15.76	2406.89	16.34
8310	3.70	5.26	5.24	4.87	5.06	4.90	8408.75	15.77	2406.89	16.34
8325	3.70	5.26	5.24	4.86	5.06	4.90	8408.75	15.77	2410.20	16.34
8340	3.70	5.26	5.24	4.86	5.04	4.90	8410.00	15.76	2413.86	16.33
8355	3.70	5.26	5.24	4.86	5.04	4.90	8406.56	15.76	2413.50	16.33
8370	3.70	5.27	5.25	4.87	5.06	4.89	8408.75	15.77	2412.21	16.34
8385	3.70	5.26	5.24	4.86	5.04	4.90	8408.75	15.77	2412.21	16.34
8400	3.70	5.26	5.24	4.86	5.06	4.89	8410.00	15.76	2410.20	16.34
8415	3.70	5.26	5.24	4.86	5.04	4.89	8410.47	15.77	2413.86	16.34
8430	3.70	5.26	5.24	4.86	5.06	4.89	8410.00	15.76	2413.50	16.34
8445	3.70	5.26	5.24	4.86	5.06	4.90	8410.00	15.76	2413.50	16.34
8460	3.70	5.24	5.22	4.86	5.04	4.90	8410.00	15.76	2411.85	16.34
8475	3.70	5.26	5.24	4.86	5.06	4.89	8410.00	15.76	2413.50	16.34
8490	3.70	5.24	5.22	4.86	5.06	4.89	8410.00	15.76	2413.50	16.34
8505	3.70	5.26	5.24	4.86	5.07	4.91	8410.00	15.76	2413.50	16.34
8520	3.70	5.24	5.22	4.84	5.06	4.90	8410.00	15.76	2415.16	16.34
8535	3.70	5.24	5.21	4.84	5.06	4.90	8410.00	15.76	2418.46	16.34
8550	3.70	5.24	5.21	4.84	5.06	4.91	8410.00	15.76	2416.45	16.34
8565	3.71	5.24	5.22	4.84	5.07	4.92	8408.75	15.76	2415.16	16.34
8580	3.71	5.24	5.21	4.84	5.06	4.92	8408.75	15.76	2415.16	16.34
8595	3.71	5.24	5.21	4.84	5.07	4.92	8410.47	15.76	2416.45	16.34
8610	3.72	5.24	5.21	4.84	5.07	4.92	8410.47	15.77	2418.46	16.34
8625	3.71	5.23	5.19	4.82	5.07	4.92	8410.47	15.76	2419.76	16.35
8640	3.71	5.23	5.19	4.82	5.07	4.93	8409.22	15.75	2418.11	16.34
8655	3.71	5.23	5.19	4.84	5.07	4.93	8410.95	15.75	2419.76	16.34
8670	3.71	5.23	5.21	4.82	5.07	4.92	8410.95	15.77	2419.76	16.34
8685	3.71	5.23	5.19	4.82	5.07	4.93	8410.95	15.75	2418.11	16.35
8700	3.71	5.21	5.19	4.82	5.07	4.93	8412.67	15.77	2421.41	16.34
8715	3.71	5.21	5.19	4.82	5.07	4.93	8412.67	15.77	2421.41	16.34
8730	3.71	5.21	5.19	4.82	5.07	4.93	8412.67	15.77	2419.76	16.35
8745	3.72	5.21	5.19	4.82	5.09	4.94	8412.67	15.77	2418.11	16.35
8760	3.71	5.21	5.19	4.81	5.07	4.94	8412.67	15.77	2418.11	16.34
8775	3.71	5.21	5.19	4.81	5.09	4.94	8412.67	15.77	2419.76	16.35
8790	3.71	5.21	5.19	4.81	5.09	4.94	8409.22	15.77	2419.40	16.34
8805	3.71	5.21	5.18	4.81	5.07	4.94	8410.95	15.77	2420.12	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
8820	3.71	5.20	5.18	4.81	5.09	4.94	8410.95	15.77	2416.45	16.34
8835	3.71	5.20	5.18	4.81	5.09	4.94	8411.42	15.76	2416.45	16.34
8850	3.71	5.20	5.18	4.81	5.09	4.94	8409.70	15.76	2419.40	16.34
8865	3.71	5.20	5.18	4.81	5.09	4.95	8409.70	15.76	2418.11	16.34
8880	3.71	5.20	5.18	4.81	5.09	4.95	8409.70	15.76	2419.76	16.34
8895	3.70	5.20	5.18	4.81	5.09	4.94	8411.42	15.76	2418.11	16.34
8910	3.70	5.20	5.18	4.81	5.09	4.94	8411.42	15.76	2419.40	16.34
8925	3.70	5.20	5.18	4.81	5.09	4.94	8414.86	15.76	2420.69	16.34
8940	3.70	5.20	5.18	4.81	5.09	4.94	8411.42	15.76	2419.40	16.34
8955	3.70	5.20	5.18	4.81	5.09	4.94	8411.42	15.76	2418.11	16.34
8970	3.70	5.20	5.18	4.81	5.09	4.94	8414.39	15.77	2416.45	16.34
8985	3.70	5.20	5.18	4.81	5.09	4.94	8411.42	15.77	2416.45	16.34
9000	3.70	5.20	5.16	4.81	5.09	4.93	8414.39	15.77	2417.39	16.34
9015	3.70	5.18	5.18	4.81	5.09	4.93	8411.42	15.76	2417.39	16.34
9030	3.69	5.20	5.18	4.81	5.09	4.92	8414.39	15.77	2416.45	16.34
9045	3.69	5.20	5.16	4.81	5.09	4.92	8414.39	15.77	2417.75	16.34
9060	3.69	5.20	5.18	4.81	5.07	4.91	8414.39	15.77	2417.75	16.34
9075	3.69	5.20	5.18	4.81	5.07	4.91	8414.39	15.77	2416.45	16.34
9090	3.69	5.20	5.18	4.81	5.07	4.90	8412.67	15.77	2414.80	16.34
9105	3.69	5.20	5.18	4.81	5.06	4.89	8410.95	15.75	2416.45	16.35
9120	3.69	5.20	5.19	4.82	5.06	4.89	8414.39	15.77	2418.11	16.34
9135	3.69	5.20	5.19	4.82	5.06	4.88	8414.39	15.75	2414.80	16.34
9150	3.68	5.20	5.19	4.82	5.06	4.88	8415.64	15.77	2416.45	16.34
9165	3.68	5.20	5.19	4.82	5.06	4.88	8413.92	15.77	2418.46	16.34
9180	3.68	5.20	5.19	4.82	5.04	4.86	8415.64	15.76	2416.81	16.34
9195	3.68	5.20	5.19	4.82	5.04	4.86	8413.92	15.76	2416.81	16.34
9210	3.68	5.20	5.19	4.82	5.04	4.86	8415.64	15.76	2416.81	16.34
9225	3.68	5.21	5.21	4.82	5.04	4.85	8415.64	15.76	2415.16	16.34
9240	3.68	5.21	5.21	4.82	5.04	4.85	8416.11	15.77	2415.16	16.34
9255	3.68	5.21	5.21	4.82	5.04	4.84	8416.11	15.77	2416.81	16.34
9270	3.68	5.21	5.21	4.84	5.04	4.85	8415.64	15.76	2416.81	16.34
9285	3.68	5.21	5.21	4.84	5.04	4.84	8417.84	15.77	2415.16	16.34
9300	3.68	5.21	5.21	4.84	5.03	4.84	8415.64	15.77	2416.81	16.34
9315	3.68	5.21	5.21	4.84	5.03	4.84	8417.36	15.77	2416.81	16.34
9330	3.68	5.21	5.21	4.84	5.03	4.84	8416.11	15.77	2418.46	16.34
9345	3.68	5.21	5.21	4.84	5.03	4.83	8416.89	15.76	2420.12	16.34
9360	3.68	5.20	5.21	4.82	5.03	4.82	8415.17	15.76	2420.12	16.34
9375	3.67	5.20	5.19	4.82	5.03	4.82	8416.89	15.76	2418.46	16.34
9390	3.68	5.20	5.21	4.82	5.03	4.82	8417.36	15.77	2418.46	16.34
9405	3.68	5.20	5.19	4.84	5.03	4.81	8417.36	15.77	2418.82	16.34
9420	3.68	5.20	5.19	4.82	5.03	4.81	8417.36	15.77	2420.12	16.34
9435	3.68	5.20	5.19	4.82	5.03	4.81	8417.36	15.77	2418.46	16.34
9450	3.68	5.20	5.19	4.82	5.03	4.80	8416.89	15.76	2418.46	16.34
9465	3.68	5.20	5.19	4.82	5.03	4.80	8418.62	15.76	2418.46	16.34
9480	3.68	5.20	5.19	4.82	5.01	4.80	8418.62	15.76	2416.81	16.33
9495	3.68	5.20	5.19	4.82	5.03	4.80	8420.81	15.77	2416.81	16.34
9510	3.68	5.20	5.19	4.82	5.03	4.80	8419.09	15.77	2418.46	16.34
9525	3.68	5.20	5.19	4.82	5.01	4.80	8417.36	15.77	2420.12	16.34
9540	3.68	5.20	5.19	4.84	5.03	4.80	8416.89	15.76	2418.46	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
9555	3.68	5.20	5.19	4.84	5.03	4.80	8418.62	15.76	2420.12	16.3
9570	3.67	5.20	5.19	4.82	5.01	4.79	8419.09	15.77	2420.48	16.3
9585	3.68	5.20	5.19	4.82	5.03	4.79	8417.36	15.77	2420.48	16.3
9600	3.68	5.20	5.19	4.82	5.01	4.78	8416.89	15.76	2420.12	16.3
9615	3.67	5.20	5.19	4.82	5.01	4.78	8418.62	15.76	2420.12	16.3
9630	3.67	5.18	5.19	4.82	5.01	4.77	8419.09	15.77	2423.79	16.3
9645	3.67	5.18	5.19	4.82	5.01	4.77	8419.09	15.77	2423.43	16.3
9660	3.67	5.18	5.19	4.82	5.01	4.77	8416.89	15.76	2420.12	16.3
9675	3.67	5.18	5.19	4.82	5.01	4.76	8417.36	15.77	2417.17	16.3
9690	3.67	5.18	5.19	4.82	5.01	4.76	8417.36	15.77	2416.81	16.3
9705	3.67	5.18	5.18	4.82	5.01	4.76	8419.09	15.77	2420.12	16.3
9720	3.67	5.18	5.18	4.82	5.01	4.75	8419.09	15.77	2423.43	16.3
9735	3.67	5.18	5.18	4.82	4.99	4.74	8419.09	15.77	2425.08	16.3
9750	3.67	5.18	5.18	4.82	4.99	4.74	8419.09	15.77	2427.09	16.3
9765	3.67	5.18	5.18	4.82	5.01	4.74	8415.64	15.77	2427.09	16.3
9780	3.67	5.18	5.18	4.82	5.01	4.74	8416.89	15.76	2425.44	16.3
9795	3.66	5.18	5.18	4.82	4.99	4.72	8415.64	15.77	2426.73	16.3
9810	3.66	5.18	5.18	4.82	4.99	4.72	8419.09	15.77	2425.08	16.3
9825	3.67	5.18	5.18	4.82	4.99	4.72	8417.36	15.77	2425.44	16.3
9840	3.67	5.16	5.18	4.81	4.99	4.71	8419.09	15.77	2423.43	16.3
9855	3.66	5.18	5.18	4.82	4.99	4.71	8419.09	15.77	2423.79	16.3
9870	3.67	5.16	5.18	4.81	4.99	4.71	8419.09	15.77	2425.44	16.3
9885	3.67	5.16	5.16	4.81	4.99	4.71	8418.62	15.76	2425.08	16.3
9900	3.67	5.16	5.16	4.81	4.99	4.71	8419.09	15.77	2428.39	16.3
9915	3.67	5.16	5.16	4.81	4.99	4.71	8418.62	15.76	2430.04	16.3
9930	3.67	5.16	5.16	4.79	4.99	4.71	8420.81	15.77	2431.69	16.3
9945	3.68	5.16	5.16	4.81	4.99	4.71	8420.34	15.76	2431.69	16.3
9960	3.68	5.16	5.16	4.81	4.99	4.71	8418.62	15.76	2431.69	16.3
9975	3.67	5.15	5.16	4.79	4.99	4.71	8418.62	15.76	2430.04	16.3
9990	3.67	5.15	5.14	4.79	4.99	4.70	8416.89	15.76	2431.69	16.3
10005	3.67	5.15	5.14	4.79	4.99	4.70	8417.36	15.77	2431.69	16.3
10020	3.68	5.15	5.14	4.79	4.99	4.70	8418.62	15.76	2431.69	16.3
10035	3.68	5.15	5.14	4.79	4.99	4.70	8415.64	15.76	2430.04	16.3
10050	3.68	5.15	5.14	4.79	4.99	4.70	8419.09	15.77	2430.04	16.3
10065	3.69	5.15	5.14	4.79	5.01	4.71	8417.36	15.76	2430.04	16.3
10080	3.69	5.15	5.14	4.79	4.99	4.71	8418.62	15.76	2430.04	16.3
10095	3.70	5.15	5.14	4.79	5.01	4.72	8417.36	15.76	2431.69	16.3
10110	3.69	5.15	5.14	4.79	5.01	4.71	8417.36	15.76	2433.35	16.3
10125	3.70	5.15	5.14	4.79	5.01	4.72	8417.84	15.78	2435.00	16.3
10140	3.69	5.13	5.13	4.78	5.01	4.72	8419.56	15.77	2435.00	16.3
10155	3.70	5.15	5.14	4.79	5.01	4.72	8417.84	15.77	2435.00	16.3
10170	3.69	5.15	5.14	4.79	5.01	4.72	8419.09	15.76	2436.65	16.3
10185	3.70	5.13	5.13	4.78	5.01	4.73	8417.36	15.76	2436.65	16.3
10200	3.70	5.13	5.14	4.78	5.01	4.73	8419.09	15.76	2434.64	16.3
10215	3.69	5.13	5.13	4.78	5.01	4.74	8419.09	15.77	2435.00	16.3
10230	3.70	5.13	5.13	4.78	5.01	4.74	8419.09	15.76	2434.64	16.3
10245	3.69	5.13	5.13	4.78	5.03	4.74	8417.84	15.75	2435.00	16.3
10260	3.70	5.13	5.14	4.79	5.03	4.74	8419.09	15.77	2434.64	16.3
10275	3.70	5.13	5.13	4.79	5.03	4.75	8419.09	15.77	2436.29	16.3

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
10290	3.70	5.13	5.13	4.78	5.01	4.75	8419.09	15.76	2434.64	16.3
10305	3.70	5.13	5.13	4.78	5.01	4.75	8419.09	15.77	2434.64	16.3
10320	3.69	5.13	5.13	4.78	5.03	4.76	8420.81	15.77	2436.65	16.3
10335	3.70	5.13	5.13	4.78	5.03	4.75	8420.81	15.77	2436.29	16.3
10350	3.70	5.13	5.14	4.78	5.03	4.75	8419.09	15.77	2436.29	16.3
10365	3.70	5.13	5.13	4.79	5.03	4.76	8419.09	15.77	2434.64	16.3
10380	3.70	5.13	5.14	4.79	5.01	4.76	8419.09	15.77	2435.00	16.3
10395	3.70	5.13	5.14	4.79	5.01	4.77	8420.81	15.76	2438.31	16.3
10410	3.70	5.15	5.14	4.79	5.01	4.76	8417.36	15.76	2438.31	16.3
10425	3.70	5.15	5.14	4.79	5.01	4.77	8417.36	15.76	2436.65	16.3
10440	3.70	5.15	5.14	4.79	5.01	4.77	8417.36	15.77	2436.65	16.3
10455	3.70	5.15	5.16	4.81	5.01	4.77	8419.56	15.77	2436.65	16.3
10470	3.70	5.15	5.14	4.81	5.01	4.76	8417.36	15.76	2435.00	16.3
10485	3.70	5.15	5.16	4.81	5.01	4.77	8419.09	15.76	2433.35	16.3
10500	3.69	5.16	5.16	4.81	5.01	4.76	8419.09	15.76	2431.69	16.3
10515	3.70	5.15	5.16	4.81	5.01	4.77	8420.34	15.76	2430.04	16.3
10530	3.70	5.16	5.16	4.81	5.01	4.77	8420.34	15.76	2433.35	16.3
10545	3.69	5.16	5.16	4.81	5.01	4.77	8420.81	15.77	2433.35	16.3
10560	3.69	5.16	5.16	4.81	5.01	4.77	8420.81	15.77	2435.36	16.3
10575	3.69	5.15	5.16	4.82	5.01	4.77	8420.34	15.76	2433.35	16.3
10590	3.69	5.16	5.16	4.81	5.01	4.77	8422.06	15.76	2433.35	16.3
10605	3.69	5.16	5.16	4.81	5.01	4.77	8423.78	15.76	2435.00	16.3
10620	3.69	5.16	5.16	4.82	5.01	4.77	8424.25	15.77	2433.35	16.3
10635	3.70	5.16	5.16	4.82	5.01	4.78	8424.25	15.77	2433.35	16.3
10650	3.70	5.16	5.18	4.82	5.01	4.79	8424.25	15.77	2435.00	16.3
10665	3.70	5.16	5.18	4.82	5.01	4.79	8423.78	15.76	2435.00	16.3
10680	3.69	5.16	5.16	4.82	5.01	4.78	8422.53	15.77	2437.02	16.3
10695	3.70	5.16	5.16	4.82	5.01	4.79	8422.06	15.76	2435.00	16.3
10710	3.70	5.16	5.18	4.82	5.01	4.80	8422.06	15.76	2433.71	16.3
10725	3.70	5.16	5.16	4.82	4.99	4.80	8422.06	15.76	2433.71	16.3
10740	3.70	5.16	5.18	4.82	5.01	4.80	8422.53	15.77	2435.00	16.3
10755	3.70	5.16	5.18	4.82	5.01	4.81	8422.53	15.77	2435.00	16.3
10770	3.70	5.16	5.18	4.82	5.01	4.82	8422.53	15.77	2435.36	16.3
10785	3.70	5.16	5.18	4.82	5.01	4.82	8422.06	15.76	2433.71	16.3
10800	3.70	5.16	5.18	4.82	5.01	4.82	8422.06	15.76	2435.36	16.3
10815	3.70	5.16	5.18	4.82	5.01	4.82	8424.25	15.77	2438.67	16.3
10830	3.70	5.16	5.18	4.82	5.01	4.82	8424.25	15.77	2437.02	16.3
10845	3.70	5.16	5.18	4.82	5.01	4.83	8423.78	15.76	2437.02	16.3
10860	3.70	5.16	5.18	4.84	5.01	4.83	8422.53	15.77	2438.67	16.3
10875	3.70	5.16	5.18	4.82	5.01	4.82	8422.53	15.77	2435.36	16.3
10890	3.70	5.16	5.18	4.82	5.01	4.83	8422.53	15.77	2433.71	16.3
10905	3.70	5.16	5.18	4.82	5.01	4.83	8424.25	15.77	2435.36	16.3
10920	3.70	5.16	5.18	4.84	5.01	4.84	8423.78	15.76	2437.02	16.3
10935	3.70	5.16	5.18	4.84	5.01	4.84	8422.53	15.77	2435.36	16.3
10950	3.71	5.18	5.18	4.84	5.01	4.85	8422.53	15.77	2435.36	16.3
10965	3.71	5.18	5.18	4.84	5.01	4.86	8422.53	15.77	2435.36	16.3
10980	3.71	5.16	5.18	4.84	5.01	4.86	8422.53	15.77	2435.36	16.3
10995	3.71	5.16	5.18	4.84	5.01	4.86	8424.25	15.77	2435.36	16.3
11010	3.70	5.16	5.18	4.84	5.03	4.86	8424.25	15.77	2438.67	16.3

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
11025	3.71	5.16	5.19	4.84	5.03	4.87	8423.78	15.76	2440.32	16.34
11040	3.71	5.18	5.18	4.84	5.01	4.88	8424.25	15.77	2438.67	16.33
11055	3.71	5.18	5.19	4.84	5.01	4.87	8422.06	15.76	2437.02	16.33
11070	3.71	5.18	5.19	4.84	5.03	4.88	8422.53	15.77	2435.36	16.34
11085	3.71	5.18	5.19	4.84	5.03	4.89	8422.53	15.77	2435.00	16.35
11100	3.70	5.18	5.19	4.84	5.03	4.89	8424.25	15.77	2432.05	16.33
11115	3.70	5.18	5.19	4.84	5.01	4.89	8424.25	15.77	2435.36	16.34
11130	3.70	5.18	5.19	4.84	5.01	4.89	8424.25	15.77	2435.36	16.33
11145	3.70	5.18	5.18	4.84	5.01	4.89	8424.25	15.77	2436.65	16.35
11160	3.70	5.18	5.19	4.84	5.01	4.89	8425.51	15.77	2438.31	16.34
11175	3.70	5.18	5.19	4.84	5.01	4.89	8424.25	15.77	2439.60	16.34
11190	3.70	5.18	5.19	4.86	5.01	4.89	8423.78	15.76	2438.67	16.33
11205	3.70	5.16	5.19	4.84	5.01	4.89	8423.78	15.76	2438.67	16.33
11220	3.70	5.18	5.19	4.84	5.01	4.90	8424.25	15.77	2438.67	16.34
11235	3.70	5.18	5.19	4.84	5.01	4.89	8424.25	15.77	2438.67	16.34
11250	3.70	5.16	5.18	4.84	5.01	4.89	8424.25	15.77	2443.63	16.33
11265	3.70	5.16	5.18	4.84	5.01	4.89	8422.53	15.77	2443.63	16.33
11280	3.70	5.16	5.18	4.84	5.01	4.90	8423.78	15.76	2443.63	16.34
11295	3.70	5.16	5.18	4.82	5.01	4.89	8424.25	15.77	2443.63	16.33
11310	3.70	5.16	5.16	4.82	5.03	4.90	8422.53	15.77	2446.58	16.34
11325	3.70	5.15	5.16	4.82	5.03	4.90	8421.28	15.77	2444.92	16.34
11340	3.70	5.16	5.16	4.82	5.03	4.91	8422.06	15.76	2444.92	16.34
11355	3.70	5.15	5.14	4.81	5.03	4.91	8420.81	15.77	2443.27	16.34
11370	3.70	5.15	5.14	4.81	5.03	4.91	8419.09	15.76	2444.92	16.34
11385	3.70	5.15	5.16	4.81	5.03	4.91	8420.34	15.76	2446.58	16.34
11400	3.70	5.15	5.14	4.81	5.04	4.91	8419.09	15.76	2446.58	16.34
11415	3.70	5.15	5.14	4.81	5.03	4.91	8420.81	15.76	2448.23	16.34
11430	3.70	5.13	5.14	4.81	5.03	4.91	8420.81	15.76	2451.54	16.34
11445	3.71	5.15	5.14	4.81	5.04	4.92	8419.09	15.76	2449.88	16.34
11460	3.71	5.15	5.14	4.81	5.04	4.92	8419.09	15.77	2449.88	16.34
11475	3.71	5.13	5.14	4.81	5.04	4.93	8419.09	15.76	2449.52	16.34
11490	3.71	5.13	5.14	4.81	5.04	4.93	8419.56	15.78	2449.52	16.34
11505	3.70	5.13	5.14	4.81	5.04	4.93	8420.81	15.77	2449.88	16.34
11520	3.72	5.13	5.14	4.81	5.04	4.94	8420.81	15.76	2449.52	16.34
11535	3.71	5.13	5.14	4.81	5.04	4.94	8420.81	15.76	2446.21	16.34
11550	3.72	5.15	5.14	4.81	5.04	4.95	8419.09	15.76	2444.56	16.34
11565	3.71	5.13	5.14	4.81	5.04	4.95	8419.09	15.76	2444.92	16.34
11580	3.71	5.15	5.14	4.81	5.04	4.96	8417.36	15.76	2448.23	16.34
11595	3.71	5.13	5.14	4.81	5.04	4.96	8419.09	15.76	2451.54	16.34
11610	3.70	5.13	5.13	4.79	5.04	4.95	8417.36	15.76	2449.52	16.34
11625	3.71	5.13	5.13	4.81	5.04	4.96	8417.36	15.77	2449.52	16.34
11640	3.71	5.13	5.14	4.81	5.06	4.97	8414.39	15.75	2451.17	16.34
11655	3.71	5.13	5.14	4.81	5.04	4.97	8416.11	15.75	2449.52	16.34
11670	3.71	5.13	5.14	4.81	5.04	4.96	8415.64	15.77	2452.83	16.34
11685	3.72	5.13	5.13	4.81	5.06	4.97	8416.11	15.77	2449.52	16.35
11700	3.70	5.13	5.14	4.81	5.04	4.96	8417.84	15.77	2449.52	16.34
11715	3.71	5.13	5.14	4.81	5.04	4.97	8419.09	15.76	2447.87	16.34
11730	3.71	5.13	5.14	4.81	5.04	4.97	8419.09	15.77	2446.21	16.34
11745	3.71	5.13	5.14	4.81	5.04	4.97	8419.09	15.76	2444.56	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
11760	3.71	5.13	5.14	4.81	5.04	4.97	8420.81	15.77	2441.62	16.34
11775	3.71	5.13	5.14	4.81	5.04	4.97	8419.56	15.78	2443.27	16.34
11790	3.71	5.15	5.14	4.81	5.04	4.97	8419.09	15.76	2442.91	16.34
11805	3.72	5.13	5.14	4.81	5.04	4.98	8419.09	15.76	2443.27	16.34
11820	3.71	5.13	5.14	4.81	5.04	4.99	8420.81	15.77	2444.56	16.34
11835	3.72	5.15	5.14	4.81	5.04	4.99	8420.81	15.76	2446.21	16.34
11850	3.71	5.13	5.14	4.81	5.04	4.99	8420.81	15.76	2448.23	16.34
11865	3.70	5.13	5.14	4.81	5.04	4.98	8422.53	15.76	2449.52	16.34
11880	3.71	5.13	5.14	4.81	5.04	4.98	8422.53	15.76	2447.87	16.34
11895	3.70	5.13	5.14	4.81	5.04	4.97	8424.25	15.76	2446.21	16.34
11910	3.70	5.13	5.14	4.81	5.03	4.97	8425.98	15.76	2446.21	16.34
11925	3.70	5.13	5.14	4.81	5.04	4.97	8425.98	15.76	2443.27	16.34
11940	3.70	5.13	5.14	4.81	5.03	4.97	8425.98	15.76	2441.62	16.34
11955	3.70	5.13	5.14	4.81	5.04	4.97	8425.98	15.76	2444.92	16.34
11970	3.70	5.13	5.14	4.81	5.04	4.97	8426.45	15.77	2443.27	16.34
11985	3.70	5.13	5.14	4.82	5.04	4.98	8425.98	15.76	2444.92	16.34
12000	3.70	5.13	5.14	4.81	5.03	4.97	8426.45	15.77	2441.25	16.34
12015	3.69	5.13	5.14	4.81	5.03	4.96	8424.72	15.77	2441.62	16.34
12030	3.69	5.13	5.14	4.81	5.03	4.96	8425.98	15.76	2441.62	16.34
12045	3.69	5.13	5.14	4.81	5.03	4.96	8424.25	15.76	2443.27	16.34
12060	3.69	5.13	5.14	4.81	5.03	4.96	8424.72	15.77	2441.62	16.34
12075	3.68	5.13	5.13	4.81	5.03	4.95	8422.53	15.76	2441.62	16.34
12090	3.67	5.12	5.13	4.79	5.01	4.93	8425.98	15.76	2443.27	16.34
12105	3.69	5.13	5.14	4.81	5.03	4.93	8425.98	15.76	2441.62	16.34
12120	3.69	5.13	5.14	4.81	5.03	4.94	8425.98	15.76	2438.31	16.34
12135	3.69	5.13	5.14	4.81	5.01	4.93	8425.98	15.76	2435.00	16.34
12150	3.69	5.13	5.14	4.81	5.01	4.93	8425.98	15.76	2436.65	16.34
12165	3.70	5.13	5.14	4.81	5.03	4.93	8423.00	15.77	2438.31	16.34
12180	3.71	5.13	5.14	4.81	5.03	4.95	8423.00	15.77	2438.31	16.34
12195	3.68	5.12	5.13	4.81	5.01	4.93	8424.25	15.76	2436.65	16.34
12210	3.69	5.12	5.14	4.81	5.01	4.92	8425.98	15.76	2439.96	16.34
12225	3.71	5.13	5.14	4.81	5.03	4.94	8425.98	15.77	2441.62	16.34
12240	3.70	5.13	5.14	4.81	5.01	4.94	8424.25	15.76	2436.65	16.34
12255	3.70	5.13	5.14	4.81	5.01	4.93	8425.98	15.76	2439.96	16.34
12270	3.70	5.13	5.13	4.81	5.01	4.93	8424.25	15.76	2441.62	16.34
12285	3.71	5.13	5.14	4.81	5.01	4.94	8425.98	15.77	2436.65	16.34
12300	3.70	5.13	5.13	4.81	5.03	4.94	8427.70	15.77	2433.35	16.34
12315	3.71	5.13	5.14	4.81	5.01	4.94	8424.25	15.76	2430.04	16.34
12330	3.71	5.13	5.14	4.81	5.01	4.94	8425.51	15.76	2431.69	16.34
12345	3.71	5.12	5.14	4.81	5.01	4.94	8425.98	15.76	2431.69	16.34
12360	3.71	5.13	5.14	4.81	5.01	4.94	8424.25	15.76	2433.35	16.34
12375	3.71	5.13	5.14	4.81	5.03	4.94	8424.25	15.76	2435.00	16.34
12390	3.71	5.13	5.14	4.79	5.01	4.95	8425.98	15.76	2438.31	16.34
12405	3.70	5.13	5.14	4.81	5.01	4.94	8425.51	15.76	2436.65	16.34
12420	3.70	5.13	5.14	4.81	5.01	4.94	8425.98	15.76	2436.65	16.34
12435	3.70	5.13	5.14	4.81	5.01	4.94	8427.23	15.76	2438.31	16.34
12450	3.70	5.13	5.13	4.81	5.01	4.94	8426.45	15.77	2441.62	16.34
12465	3.70	5.13	5.14	4.81	5.01	4.93	8425.98	15.77	2446.58	16.34
12480	3.69	5.13	5.13	4.81	5.01	4.92	8425.51	15.76	2451.54	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
12495	3.70	5.12	5.14	4.81	5.01	4.92	8423.78	15.76	2453.19	16.34
12510	3.69	5.13	5.13	4.81	5.01	4.92	8427.70	15.77	2451.90	16.34
12525	3.69	5.12	5.13	4.81	5.01	4.91	8425.98	15.77	2452.83	16.34
12540	3.69	5.12	5.14	4.81	4.99	4.92	8427.23	15.76	2449.88	16.34
12555	3.69	5.13	5.13	4.81	4.99	4.91	8425.51	15.76	2449.88	16.34
12570	3.69	5.12	5.13	4.81	4.99	4.91	8424.25	15.77	2449.88	16.34
12585	3.68	5.12	5.14	4.81	4.99	4.89	8424.25	15.77	2448.23	16.34
12600	3.68	5.12	5.14	4.81	4.99	4.89	8425.51	15.76	2444.92	16.34
12615	3.68	5.12	5.13	4.81	4.99	4.88	8424.25	15.77	2444.92	16.34
12630	3.68	5.12	5.14	4.79	4.99	4.88	8425.98	15.77	2444.92	16.34
12645	3.68	5.12	5.13	4.81	4.98	4.87	8425.51	15.76	2444.56	16.34
12660	3.68	5.12	5.14	4.81	4.98	4.87	8427.70	15.77	2441.62	16.34
12675	3.68	5.12	5.13	4.81	4.98	4.87	8425.98	15.76	2439.96	16.34
12690	3.68	5.12	5.13	4.79	4.98	4.87	8424.25	15.76	2441.25	16.34
12705	3.68	5.12	5.13	4.81	4.98	4.86	8425.51	15.76	2440.32	16.34
12720	3.68	5.12	5.13	4.81	4.98	4.86	8425.98	15.76	2439.96	16.34
12735	3.68	5.12	5.13	4.81	4.98	4.86	8425.98	15.77	2441.98	16.34
12750	3.68	5.12	5.13	4.79	4.98	4.85	8423.78	15.76	2441.98	16.34
12765	3.68	5.10	5.11	4.79	4.96	4.85	8425.04	15.77	2440.32	16.34
12780	3.69	5.10	5.11	4.78	4.98	4.85	8423.78	15.75	2441.98	16.34
12795	3.69	5.10	5.11	4.78	4.98	4.86	8423.78	15.76	2441.98	16.34
12810	3.68	5.08	5.10	4.78	4.98	4.85	8425.04	15.77	2440.32	16.34
12825	3.68	5.10	5.11	4.78	4.98	4.86	8424.25	15.77	2439.96	16.34
12840	3.68	5.10	5.11	4.79	4.98	4.85	8423.78	15.76	2439.96	16.34
12855	3.69	5.10	5.11	4.79	4.98	4.85	8423.78	15.76	2441.62	16.34
12870	3.69	5.10	5.11	4.79	4.98	4.85	8424.25	15.77	2443.27	16.34
12885	3.68	5.10	5.10	4.78	4.98	4.85	8423.78	15.76	2443.27	16.34
12900	3.69	5.10	5.11	4.78	4.98	4.85	8422.06	15.76	2439.96	16.34
12915	3.69	5.08	5.10	4.78	4.98	4.85	8422.06	15.76	2441.62	16.34
12930	3.69	5.08	5.10	4.76	4.98	4.85	8420.81	15.76	2438.31	16.34
12945	3.69	5.08	5.08	4.76	4.98	4.85	8422.06	15.76	2439.96	16.34
12960	3.69	5.08	5.10	4.78	4.99	4.86	8419.09	15.77	2438.31	16.34
12975	3.69	5.08	5.08	4.76	4.99	4.86	8419.09	15.76	2439.96	16.34
12990	3.69	5.08	5.08	4.76	4.99	4.86	8419.09	15.76	2441.62	16.34
13005	3.70	5.08	5.08	4.76	4.99	4.86	8417.36	15.77	2438.31	16.34
13020	3.70	5.07	5.08	4.76	4.99	4.86	8419.09	15.77	2439.60	16.34
13035	3.70	5.07	5.08	4.75	4.99	4.86	8416.11	15.75	2441.25	16.34
13050	3.70	5.07	5.06	4.76	5.01	4.87	8416.11	15.77	2441.25	16.35
13065	3.70	5.07	5.06	4.75	5.01	4.87	8416.11	15.75	2441.25	16.34
13080	3.70	5.07	5.06	4.76	5.01	4.88	8416.11	15.77	2441.25	16.35
13095	3.70	5.07	5.06	4.75	5.01	4.87	8416.11	15.77	2439.60	16.35
13110	3.70	5.07	5.06	4.75	5.01	4.87	8416.11	15.77	2439.60	16.35
13125	3.70	5.05	5.06	4.75	5.01	4.88	8416.11	15.77	2439.60	16.34
13140	3.70	5.07	5.06	4.75	5.01	4.88	8416.11	15.77	2442.54	16.34
13155	3.70	5.07	5.06	4.75	5.01	4.89	8414.86	15.76	2442.54	16.34
13170	3.70	5.05	5.06	4.75	5.01	4.88	8414.86	15.76	2441.25	16.34
13185	3.70	5.07	5.05	4.75	5.01	4.89	8414.86	15.76	2442.54	16.34
13200	3.70	5.05	5.05	4.75	5.01	4.89	8414.86	15.76	2441.25	16.34
13215	3.70	5.05	5.05	4.73	5.03	4.89	8414.86	15.76	2442.54	16.34

**RAYMARK INDUSTRIES, INC.
STRATFORD, CONNECTICUT
RCRA SECTION 3013 ORDER
DOCKET NO. I-87-1057**

**TIDAL STUDY FIELD DATA
G CLUSTER WELLS**

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
13230	3.70	5.05	5.05	4.73	5.01	4.89	8414.86	15.76	2442.54	16.34
13245	3.70	5.05	5.05	4.75	5.03	4.89	8414.86	15.76	2437.95	16.34
13260	3.70	5.05	5.05	4.73	5.03	4.89	8416.58	15.76	2437.58	16.33
13275	3.70	5.05	5.05	4.73	5.03	4.89	8420.03	15.76	2435.93	16.34
13290	3.70	5.05	5.05	4.73	5.03	4.89	8420.03	15.76	2437.95	16.34
13305	3.70	5.05	5.05	4.73	5.01	4.89	8421.75	15.76	2437.95	16.34
13320	3.70	5.05	5.05	4.73	5.01	4.88	8425.19	15.76	2439.24	16.34
13335	3.70	5.05	5.05	4.73	5.01	4.88	8426.45	15.77	2439.24	16.34
13350	3.70	5.05	5.06	4.73	5.01	4.88	8426.91	15.76	2437.58	16.34
13365	3.70	5.05	5.06	4.75	5.01	4.88	8426.45	15.77	2437.58	16.34
13380	3.70	5.07	5.06	4.75	5.01	4.88	8424.72	15.77	2437.58	16.34
13395	3.70	5.07	5.06	4.75	4.99	4.88	8426.45	15.77	2436.29	16.35
13410	3.70	5.07	5.08	4.76	4.99	4.88	8424.72	15.77	2434.64	16.35
13425	3.70	5.07	5.08	4.76	4.99	4.87	8425.98	15.77	2431.33	16.35
13440	3.69	5.07	5.08	4.76	4.99	4.87	8427.70	15.76	2430.04	16.34
13455	3.69	5.08	5.08	4.76	4.98	4.87	8428.17	15.77	2430.04	16.35
13470	3.69	5.08	5.08	4.76	4.98	4.87	8427.70	15.77	2430.04	16.35
13485	3.68	5.07	5.08	4.76	4.98	4.86	8429.42	15.77	2429.68	16.35
13500	3.68	5.08	5.10	4.76	4.99	4.85	8429.42	15.76	2430.04	16.34
13515	3.68	5.08	5.08	4.78	4.98	4.84	8429.42	15.76	2428.39	16.34
13530	3.68	5.08	5.10	4.78	4.98	4.84	8425.98	15.76	2426.73	16.34
13545	3.68	5.08	5.10	4.78	4.96	4.83	8427.70	15.76	2425.08	16.34
13560	3.69	5.08	5.10	4.78	4.98	4.83	8427.70	15.76	2423.43	16.34
13575	3.69	5.08	5.10	4.78	4.96	4.84	8427.70	15.76	2421.77	16.34
13590	3.69	5.08	5.10	4.78	4.96	4.84	8427.70	15.76	2420.12	16.34
13605	3.69	5.08	5.10	4.78	4.96	4.84	8429.42	15.77	2418.46	16.34
13620	3.69	5.08	5.10	4.78	4.96	4.84	8427.70	15.76	2415.16	16.34
13635	3.69	5.08	5.11	4.78	4.96	4.84	8427.70	15.76	2415.16	16.34
13650	3.69	5.10	5.10	4.78	4.96	4.84	8427.70	15.77	2413.86	16.34
13665	3.69	5.08	5.10	4.78	4.96	4.84	8427.70	15.77	2415.16	16.34
13680	3.69	5.08	5.10	4.79	4.96	4.84	8427.23	15.76	2415.16	16.34
13695	3.69	5.10	5.10	4.78	4.96	4.84	8425.98	15.76	2416.81	16.34
13710	3.69	5.10	5.11	4.79	4.96	4.83	8427.23	15.76	2417.17	16.34
13725	3.69	5.10	5.10	4.79	4.96	4.83	8427.70	15.76	2417.17	16.34
13740	3.69	5.10	5.11	4.79	4.96	4.84	8427.23	15.76	2416.81	16.34
13755	3.69	5.10	5.11	4.79	4.96	4.83	8427.23	15.76	2413.86	16.34
13770	3.69	5.10	5.11	4.79	4.96	4.83	8427.23	15.76	2415.16	16.34
13785	3.69	5.10	5.11	4.79	4.96	4.84	8427.23	15.76	2413.86	16.34
13800	3.69	5.10	5.11	4.79	4.96	4.84	8427.70	15.77	2411.85	16.34
13815	3.70	5.10	5.11	4.79	4.96	4.84	8427.23	15.76	2413.86	16.34
13830	3.70	5.10	5.11	4.79	4.96	4.84	8427.23	15.76	2412.21	16.34
13845	3.70	5.10	5.11	4.79	4.96	4.84	8427.23	15.76	2415.52	16.34
13860	3.69	5.10	5.11	4.79	4.95	4.84	8427.70	15.77	2415.52	16.34
13875	3.70	5.10	5.11	4.79	4.96	4.84	8427.70	15.77	2415.52	16.34
13890	3.69	5.10	5.11	4.79	4.96	4.84	8429.42	15.77	2418.82	16.34
13905	3.70	5.10	5.11	4.79	4.95	4.85	8427.70	15.76	2417.17	16.33
13920	3.69	5.10	5.11	4.79	4.95	4.84	8427.70	15.77	2416.81	16.35
13935	3.69	5.10	5.11	4.79	4.95	4.84	8429.42	15.77	2415.52	16.33
13950	3.69	5.10	5.11	4.79	4.95	4.84	8429.42	15.77	2413.86	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
13965	3.69	5.10	5.11	4.79	4.95	4.84	8429.42	15.77	2413.86	16.34
13980	3.70	5.10	5.11	4.81	4.95	4.84	8429.42	15.77	2415.16	16.35
13995	3.69	5.10	5.11	4.79	4.95	4.84	8429.42	15.76	2412.21	16.33
14010	3.69	5.10	5.11	4.79	4.95	4.84	8427.70	15.76	2412.21	16.33
14025	3.69	5.10	5.11	4.79	4.96	4.84	8430.67	15.76	2412.21	16.33
14040	3.69	5.10	5.11	4.79	4.95	4.83	8427.70	15.77	2412.21	16.34
14055	3.69	5.10	5.11	4.79	4.95	4.83	8428.95	15.76	2412.21	16.34
14070	3.69	5.10	5.11	4.79	4.95	4.83	8428.95	15.76	2415.16	16.34
14085	3.69	5.10	5.11	4.79	4.95	4.82	8427.23	15.77	2413.86	16.33
14100	3.68	5.10	5.11	4.79	4.95	4.82	8428.48	15.75	2413.86	16.34
14115	3.68	5.10	5.11	4.78	4.95	4.82	8427.70	15.77	2413.50	16.34
14130	3.68	5.10	5.11	4.79	4.95	4.81	8427.70	15.77	2410.55	16.34
14145	3.68	5.08	5.10	4.79	4.95	4.82	8428.95	15.76	2407.25	16.34
14160	3.68	5.08	5.10	4.79	4.95	4.81	8428.95	15.77	2405.59	16.34
14175	3.69	5.08	5.10	4.79	4.95	4.82	8427.23	15.76	2403.94	16.33
14190	3.69	5.10	5.08	4.78	4.95	4.82	8425.51	15.76	2402.29	16.34
14205	3.70	5.10	5.10	4.78	4.96	4.82	8423.78	15.76	2402.29	16.34
14220	3.69	5.08	5.08	4.78	4.95	4.82	8422.53	15.77	2401.93	16.35
14235	3.69	5.07	5.08	4.76	4.95	4.82	8420.81	15.77	2398.98	16.34
14250	3.69	5.07	5.06	4.76	4.95	4.82	8422.53	15.77	2398.98	16.34
14265	3.69	5.07	5.06	4.76	4.95	4.82	8422.53	15.77	2398.62	16.34
14280	3.69	5.07	5.06	4.76	4.95	4.82	8420.81	15.77	2398.62	16.34
14295	3.69	5.07	5.06	4.75	4.96	4.82	8420.34	15.76	2398.62	16.34
14310	3.70	5.07	5.06	4.75	4.96	4.83	8419.09	15.76	2398.62	16.34
14325	3.69	5.05	5.05	4.75	4.96	4.82	8419.09	15.76	2396.97	16.34
14340	3.70	5.05	5.05	4.75	4.96	4.83	8418.62	15.77	2396.97	16.34
14355	3.70	5.05	5.05	4.73	4.96	4.83	8415.64	15.76	2393.66	16.34
14370	3.70	5.05	5.03	4.73	4.96	4.83	8413.92	15.76	2392.01	16.34
14385	3.70	5.05	5.03	4.73	4.96	4.84	8413.92	15.76	2390.35	16.33
14400	3.70	5.04	5.03	4.73	4.98	4.84	8413.92	15.76	2388.35	16.35
14415	3.70	5.04	5.03	4.73	4.98	4.85	8413.92	15.77	2390.00	16.35
14430	3.70	5.04	5.03	4.73	4.98	4.85	8413.92	15.76	2393.31	16.35
14445	3.71	5.04	5.03	4.73	4.98	4.85	8410.95	15.77	2396.61	16.35
14460	3.70	5.04	5.03	4.71	4.98	4.85	8412.67	15.77	2397.91	16.34
14475	3.70	5.04	5.02	4.71	4.99	4.86	8412.67	15.77	2394.96	16.34
14490	3.71	5.04	5.02	4.71	4.99	4.86	8410.95	15.77	2395.31	16.35
14505	3.71	5.04	5.02	4.71	4.99	4.86	8411.42	15.76	2394.96	16.34
14520	3.70	5.02	5.00	4.70	4.98	4.86	8409.70	15.76	2394.96	16.35
14535	3.71	5.02	5.02	4.71	4.99	4.87	8407.50	15.75	2394.96	16.34
14550	3.71	5.02	5.02	4.70	4.99	4.87	8406.25	15.76	2396.61	16.34
14565	3.71	5.02	5.00	4.70	4.99	4.88	8406.25	15.76	2396.61	16.34
14580	3.71	5.02	5.02	4.70	4.99	4.88	8406.25	15.76	2396.61	16.34
14595	3.71	5.02	5.02	4.70	5.01	4.89	8406.25	15.77	2397.91	16.34
14610	3.71	5.02	5.02	4.71	4.99	4.89	8406.25	15.76	2398.27	16.35
14625	3.71	5.02	5.02	4.71	4.99	4.89	8406.25	15.76	2401.57	16.35
14640	3.71	5.02	5.02	4.71	4.99	4.90	8404.53	15.77	2402.87	16.34
14655	3.71	5.02	5.02	4.71	4.99	4.90	8406.25	15.76	2402.87	16.34
14670	3.71	5.02	5.02	4.71	4.99	4.89	8406.25	15.76	2402.87	16.34
14685	3.70	5.02	5.02	4.71	4.99	4.89	8404.53	15.76	2401.22	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
14700	3.70	5.02	5.02	4.71	4.99	4.89	8406.25	15.76	2401.22	16.34
14715	3.70	5.02	5.02	4.70	4.99	4.89	8404.53	15.76	2401.57	16.34
14730	3.70	5.02	5.02	4.70	4.99	4.89	8406.25	15.76	2399.92	16.34
14745	3.70	5.02	5.02	4.70	4.99	4.88	8407.98	15.77	2399.56	16.34
14760	3.70	5.02	5.02	4.70	4.99	4.88	8409.70	15.76	2398.27	16.35
14775	3.70	5.02	5.02	4.71	4.99	4.88	8409.70	15.76	2394.96	16.34
14790	3.70	5.02	5.02	4.70	4.98	4.88	8412.67	15.77	2391.65	16.34
14805	3.70	5.02	5.02	4.71	4.98	4.88	8414.39	15.77	2387.99	16.34
14820	3.70	5.04	5.02	4.71	4.98	4.88	8417.84	15.77	2386.69	16.35
14835	3.69	5.02	5.02	4.71	4.98	4.87	8420.03	15.76	2383.38	16.34
14850	3.70	5.04	5.03	4.71	4.98	4.87	8421.28	15.77	2385.04	16.35
14865	3.69	5.04	5.03	4.73	4.98	4.87	8421.28	15.75	2381.73	16.35
14880	3.69	5.04	5.03	4.73	4.96	4.86	8423.00	15.75	2381.73	16.35
14895	3.69	5.04	5.03	4.73	4.96	4.86	8424.25	15.76	2380.08	16.35
14910	3.69	5.04	5.03	4.73	4.96	4.86	8424.25	15.76	2380.08	16.34
14925	3.69	5.05	5.05	4.73	4.96	4.85	8424.25	15.77	2380.43	16.35
14940	3.69	5.04	5.05	4.73	4.95	4.85	8422.53	15.76	2382.09	16.34
14955	3.69	5.05	5.05	4.75	4.95	4.84	8424.72	15.77	2380.43	16.34
14970	3.69	5.05	5.05	4.75	4.95	4.84	8422.53	15.76	2378.78	16.34
14985	3.69	5.05	5.05	4.75	4.95	4.84	8420.81	15.76	2377.12	16.34
15000	3.70	5.05	5.05	4.75	4.95	4.85	8420.81	15.76	2377.12	16.34
15015	3.70	5.05	5.05	4.75	4.95	4.86	8421.28	15.77	2375.47	16.34
15030	3.70	5.05	5.06	4.75	4.95	4.86	8420.81	15.76	2373.82	16.34
15045	3.70	5.05	5.05	4.75	4.95	4.85	8420.81	15.76	2373.82	16.34
15060	3.70	5.05	5.05	4.75	4.95	4.86	8421.28	15.77	2375.47	16.34
15075	3.70	5.05	5.05	4.75	4.95	4.86	8419.09	15.76	2373.82	16.34
15090	3.70	5.05	5.06	4.75	4.95	4.86	8420.81	15.77	2373.82	16.34
15105	3.70	5.07	5.05	4.75	4.95	4.86	8417.36	15.76	2375.47	16.34
15120	3.70	5.05	5.06	4.75	4.95	4.86	8419.09	15.76	2375.47	16.34
15135	3.69	5.05	5.05	4.76	4.95	4.85	8420.34	15.76	2378.78	16.34
15150	3.70	5.05	5.05	4.76	4.95	4.86	8419.09	15.77	2380.43	16.34
15165	3.70	5.05	5.06	4.76	4.95	4.86	8418.62	15.76	2378.78	16.34
15180	3.69	5.05	5.05	4.75	4.95	4.86	8419.09	15.76	2378.78	16.34
15195	3.70	5.05	5.05	4.75	4.95	4.85	8419.09	15.77	2378.78	16.34
15210	3.70	5.05	5.05	4.76	4.95	4.85	8420.81	15.77	2379.13	16.34
15225	3.70	5.05	5.06	4.76	4.95	4.86	8419.09	15.77	2377.12	16.34
15240	3.70	5.07	5.06	4.76	4.95	4.87	8419.09	15.77	2375.47	16.34
15255	3.70	5.05	5.06	4.76	4.95	4.87	8416.11	15.77	2373.82	16.34
15270	3.70	5.07	5.06	4.76	4.95	4.87	8417.36	15.77	2372.16	16.34
15285	3.70	5.07	5.06	4.76	4.95	4.87	8416.89	15.76	2373.82	16.34
15300	3.70	5.07	5.05	4.76	4.95	4.87	8416.89	15.76	2375.47	16.34
15315	3.70	5.05	5.06	4.76	4.95	4.88	8415.17	15.76	2378.78	16.34
15330	3.70	5.05	5.05	4.75	4.95	4.87	8415.64	15.77	2382.44	16.34
15345	3.70	5.05	5.05	4.75	4.95	4.87	8415.17	15.76	2383.74	16.34
15360	3.70	5.05	5.05	4.76	4.95	4.88	8415.64	15.77	2384.09	16.34
15375	3.70	5.05	5.05	4.76	4.95	4.88	8413.92	15.77	2382.09	16.34
15390	3.71	5.07	5.06	4.76	4.95	4.88	8413.45	15.76	2382.09	16.34
15405	3.70	5.05	5.06	4.76	4.95	4.88	8411.73	15.76	2383.74	16.34
15420	3.70	5.07	5.06	4.76	4.95	4.88	8411.73	15.76	2382.09	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
15435	3.71	5.07	5.06	4.76	4.95	4.89	8410.47	15.76	2384.09	16.34
15450	3.70	5.05	5.06	4.75	4.95	4.89	8410.47	15.77	2382.09	16.34
15465	3.70	5.07	5.05	4.75	4.95	4.89	8412.20	15.77	2382.09	16.34
15480	3.70	5.05	5.05	4.75	4.95	4.89	8410.00	15.76	2383.74	16.34
15495	3.70	5.05	5.05	4.75	4.95	4.88	8408.75	15.76	2383.74	16.34
15510	3.70	5.05	5.05	4.75	4.95	4.89	8410.00	15.76	2382.09	16.34
15525	3.70	5.05	5.05	4.75	4.95	4.88	8410.00	15.76	2383.74	16.34
15540	3.70	5.05	5.05	4.75	4.95	4.88	8410.00	15.76	2383.74	16.34
15555	3.70	5.05	5.05	4.75	4.95	4.88	8407.03	15.76	2383.74	16.34
15570	3.70	5.05	5.05	4.75	4.93	4.89	8407.03	15.76	2385.39	16.34
15585	3.70	5.05	5.05	4.75	4.95	4.89	8407.03	15.76	2387.05	16.34
15600	3.69	5.05	5.05	4.75	4.95	4.88	8408.28	15.76	2388.70	16.34
15615	3.69	5.05	5.05	4.75	4.93	4.88	8407.03	15.77	2390.35	16.34
15630	3.70	5.05	5.03	4.75	4.93	4.88	8407.03	15.76	2388.70	16.34
15645	3.70	5.05	5.05	4.75	4.95	4.88	8407.03	15.76	2385.39	16.35
15660	3.70	5.05	5.05	4.75	4.93	4.88	8407.03	15.76	2383.74	16.34
15675	3.70	5.05	5.05	4.75	4.95	4.88	8406.56	15.76	2382.09	16.34
15690	3.70	5.05	5.05	4.75	4.95	4.88	8405.31	15.76	2380.43	16.34
15705	3.70	5.05	5.05	4.75	4.95	4.89	8405.31	15.76	2377.12	16.34
15720	3.70	5.05	5.03	4.75	4.95	4.90	8403.59	15.76	2377.12	16.35
15735	3.70	5.05	5.03	4.73	4.95	4.89	8403.59	15.76	2377.12	16.34
15750	3.70	5.05	5.03	4.71	4.95	4.89	8403.59	15.76	2378.78	16.34
15765	3.70	5.04	5.03	4.73	4.95	4.89	8403.59	15.76	2382.09	16.34
15780	3.70	5.04	5.03	4.73	4.95	4.90	8403.59	15.76	2382.09	16.34
15795	3.70	5.04	5.03	4.73	4.95	4.90	8401.86	15.77	2382.09	16.34
15810	3.71	5.05	5.03	4.73	4.95	4.90	8401.86	15.76	2380.43	16.35
15825	3.70	5.04	5.03	4.73	4.95	4.90	8401.86	15.76	2378.78	16.34
15840	3.71	5.04	5.03	4.73	4.95	4.90	8400.14	15.76	2376.77	16.34
15855	3.71	5.05	5.03	4.73	4.95	4.91	8401.86	15.77	2377.12	16.35
15870	3.71	5.05	5.03	4.73	4.95	4.91	8400.14	15.76	2377.12	16.34
15885	3.73	5.04	5.03	4.73	4.95	4.92	8398.42	15.76	2373.82	16.34
15900	3.75	5.05	5.03	4.73	4.95	4.92	8400.14	15.76	2367.20	16.34
15915	3.77	5.05	5.03	4.73	4.96	4.93	8398.42	15.76	2358.93	16.34
15930	3.78	5.05	5.03	4.73	4.96	4.93	8398.42	15.76	2347.36	16.35
15945	3.78	5.05	5.03	4.73	4.96	4.94	8396.70	15.76	2340.74	16.34
15960	3.79	5.05	5.03	4.73	4.96	4.94	8396.70	15.77	2334.13	16.35
15975	3.79	5.05	5.03	4.75	4.96	4.95	8394.97	15.76	2329.17	16.35
15990	3.80	5.05	5.03	4.73	4.96	4.94	8394.97	15.76	2319.25	16.35
16005	3.80	5.05	5.03	4.75	4.96	4.95	8394.97	15.76	2310.98	16.34
16020	3.81	5.07	5.03	4.75	4.96	4.95	8394.97	15.76	2302.37	16.35
16035	3.83	5.07	5.03	4.73	4.96	4.95	8394.97	15.77	2294.10	16.35
16050	3.87	5.07	5.03	4.75	4.96	4.96	8393.25	15.76	2289.48	16.35
16065	3.88	5.07	5.03	4.75	4.96	4.96	8393.25	15.76	2282.87	16.35
16080	3.88	5.07	5.03	4.75	4.96	4.97	8393.25	15.76	2274.60	16.35
16095	3.87	5.08	5.03	4.75	4.98	4.98	8391.53	15.76	2267.99	16.34
16110	3.84	5.07	5.05	4.75	4.96	4.98	8394.50	15.76	2263.02	16.35
16125	3.83	5.07	5.05	4.75	4.98	4.98	8393.25	15.76	2257.73	16.34
16140	3.81	5.07	5.03	4.75	4.96	4.97	8393.25	15.76	2254.42	16.35
16155	3.80	5.07	5.03	4.75	4.96	4.97	8391.53	15.76	2253.10	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
16170	3.80	5.07	5.05	4.75	4.96	4.97	8393.25	15.76	2249.80	16.35
16185	3.78	5.07	5.03	4.75	4.96	4.97	8393.25	15.76	2253.10	16.35
16200	3.76	5.07	5.03	4.75	4.96	4.95	8394.97	15.76	2258.06	16.35
16215	3.76	5.07	5.03	4.75	4.96	4.94	8396.70	15.77	2274.60	16.35
16230	3.75	5.07	5.03	4.73	4.96	4.94	8398.42	15.77	2294.44	16.35
16245	3.76	5.07	5.03	4.73	4.96	4.94	8398.42	15.76	2309.33	16.35
16260	3.78	5.07	5.03	4.75	4.96	4.95	8398.89	15.78	2319.59	16.34
16275	3.79	5.08	5.03	4.73	4.98	4.95	8398.42	15.76	2327.52	16.35
16290	3.77	5.07	5.03	4.73	4.96	4.95	8398.42	15.76	2332.48	16.35
16305	3.77	5.07	5.03	4.73	4.96	4.94	8398.42	15.77	2338.74	16.35
16320	3.77	5.07	5.03	4.75	4.96	4.94	8398.42	15.77	2344.40	16.34
16335	3.77	5.08	5.03	4.73	4.96	4.94	8398.42	15.77	2350.67	16.35
16350	3.76	5.07	5.03	4.75	4.96	4.94	8396.70	15.76	2355.63	16.35
16365	3.76	5.08	5.03	4.73	4.96	4.94	8398.42	15.77	2362.24	16.35
16380	3.75	5.07	5.03	4.73	4.96	4.93	8398.42	15.77	2367.20	16.35
16395	3.75	5.08	5.03	4.75	4.96	4.94	8398.42	15.77	2372.16	16.35
16410	3.75	5.08	5.03	4.73	4.96	4.95	8398.42	15.76	2378.78	16.35
16425	3.75	5.08	5.03	4.75	4.96	4.95	8398.42	15.76	2383.74	16.35
16440	3.75	5.08	5.03	4.75	4.96	4.94	8396.70	15.77	2392.01	16.35
16455	3.74	5.08	5.03	4.75	4.96	4.94	8396.70	15.76	2400.27	16.35
16470	3.74	5.08	5.03	4.75	4.96	4.95	8396.70	15.76	2411.85	16.35
16485	3.75	5.10	5.05	4.75	4.96	4.96	8396.70	15.77	2420.12	16.34
16500	3.74	5.10	5.03	4.75	4.98	4.96	8396.70	15.76	2425.08	16.35
16515	3.75	5.10	5.03	4.75	4.98	4.97	8396.70	15.76	2431.69	16.35
16530	3.73	5.10	5.05	4.75	4.96	4.97	8396.70	15.77	2436.65	16.35
16545	3.74	5.10	5.05	4.75	4.96	4.96	8394.97	15.77	2444.92	16.35
16560	3.73	5.10	5.05	4.75	4.96	4.97	8395.45	15.77	2449.88	16.35
16575	3.73	5.10	5.05	4.75	4.96	4.96	8394.97	15.76	2449.88	16.34
16590	3.73	5.10	5.05	4.75	4.96	4.96	8394.97	15.76	2449.88	16.35
16605	3.72	5.10	5.03	4.75	4.96	4.96	8394.97	15.76	2448.23	16.34
16620	3.73	5.10	5.05	4.75	4.96	4.96	8394.97	15.76	2448.23	16.35
16635	3.72	5.10	5.05	4.75	4.96	4.97	8394.97	15.76	2448.23	16.35
16650	3.73	5.10	5.05	4.75	4.96	4.97	8394.97	15.76	2451.54	16.35
16665	3.72	5.10	5.05	4.75	4.96	4.97	8394.97	15.77	2454.84	16.34
16680	3.72	5.10	5.05	4.75	4.96	4.97	8394.97	15.76	2459.81	16.34
16695	3.73	5.12	5.05	4.75	4.98	4.98	8394.97	15.76	2459.81	16.34
16710	3.73	5.12	5.05	4.76	4.96	4.99	8394.97	15.76	2456.50	16.35
16725	3.73	5.12	5.05	4.75	4.96	4.98	8395.45	15.77	2456.13	16.35
16740	3.73	5.12	5.05	4.75	4.96	4.99	8393.25	15.76	2458.15	16.34
16755	3.73	5.12	5.05	4.75	4.98	4.99	8394.97	15.76	2459.81	16.35
16770	3.74	5.12	5.05	4.76	4.98	5.00	8393.25	15.76	2458.15	16.34
16785	3.74	5.12	5.06	4.76	4.98	5.02	8393.25	15.76	2454.84	16.35
16800	3.73	5.12	5.05	4.76	4.98	5.02	8392.78	15.76	2449.88	16.34
16815	3.73	5.12	5.06	4.75	4.98	5.02	8391.53	15.76	2448.23	16.34
16830	3.74	5.12	5.06	4.76	4.98	5.02	8391.53	15.76	2449.88	16.34
16845	3.70	5.10	5.03	4.76	4.96	5.00	8390.28	15.77	2449.88	16.34
16860	3.78	5.12	5.06	4.76	4.98	5.03	8393.25	15.76	2446.58	16.34
16875	3.90	5.12	5.06	4.76	4.98	5.02	8392.78	15.76	2425.08	16.35
16890	3.95	5.12	5.06	4.76	4.98	5.02	8391.53	15.76	2411.85	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
16905	4.00	5.12	5.06	4.76	4.98	5.02	8391.53	15.76	2403.58	16.35
16920	4.04	5.13	5.06	4.76	4.98	5.03	8392.00	15.77	2387.05	16.34
16935	4.06	5.13	5.06	4.78	4.98	5.02	8391.53	15.76	2377.12	16.35
16950	4.05	5.13	5.06	4.78	4.99	5.03	8391.53	15.76	2367.20	16.35
16965	4.04	5.13	5.06	4.78	4.99	5.03	8390.28	15.77	2358.93	16.35
16980	4.00	5.13	5.06	4.76	4.98	5.00	8393.73	15.77	2350.67	16.35
16995	3.99	5.13	5.06	4.78	4.98	5.00	8393.25	15.76	2342.40	16.34
17010	3.98	5.13	5.08	4.78	4.99	5.00	8393.73	15.77	2335.78	16.34
17025	3.96	5.13	5.06	4.78	4.99	5.01	8391.53	15.76	2329.17	16.34
17040	3.93	5.13	5.06	4.78	4.99	5.00	8393.25	15.76	2324.21	16.35
17055	3.92	5.13	5.06	4.78	4.99	4.98	8394.97	15.76	2324.21	16.35
17070	3.91	5.13	5.06	4.78	4.99	4.97	8394.97	15.76	2325.86	16.35
17085	3.91	5.13	5.06	4.78	5.01	4.99	8394.97	15.76	2330.82	16.34
17100	3.89	5.13	5.08	4.79	5.01	4.99	8393.25	15.76	2339.09	16.35
17115	3.87	5.13	5.08	4.79	5.01	4.99	8394.97	15.76	2360.59	16.34
17130	3.86	5.15	5.08	4.79	5.01	4.99	8394.97	15.76	2388.70	16.34
17145	3.83	5.13	5.08	4.79	5.01	4.99	8393.25	15.76	2401.93	16.35
17160	3.82	5.13	5.08	4.78	5.01	4.98	8394.97	15.76	2410.20	16.35
17175	3.80	5.13	5.06	4.78	5.01	4.96	8393.25	15.76	2411.85	16.34
17190	3.80	5.13	5.06	4.78	5.01	4.96	8395.45	15.78	2418.11	16.35
17205	3.78	5.13	5.06	4.78	5.01	4.96	8394.97	15.76	2421.77	16.35
17220	3.78	5.13	5.06	4.78	5.01	4.95	8396.70	15.76	2428.39	16.34
17235	3.77	5.13	5.06	4.78	5.01	4.95	8398.42	15.77	2448.23	16.34
17250	3.77	5.13	5.06	4.78	5.01	4.95	8398.42	15.76	2469.73	16.35
17265	3.77	5.13	5.08	4.78	5.01	4.94	8400.14	15.76	2484.61	16.34
17280	3.76	5.13	5.06	4.78	5.01	4.95	8401.86	15.76	2496.18	16.34
17295	3.76	5.13	5.08	4.78	5.01	4.94	8401.86	15.76	2499.49	16.34
17310	3.75	5.13	5.08	4.78	5.01	4.94	8401.86	15.76	2499.12	16.34
17325	3.74	5.13	5.08	4.78	5.01	4.94	8401.86	15.76	2497.84	16.34
17340	3.74	5.13	5.08	4.78	5.01	4.93	8403.59	15.76	2492.88	16.34
17355	3.73	5.13	5.08	4.78	5.01	4.92	8401.86	15.77	2487.92	16.34
17370	3.73	5.15	5.06	4.78	5.01	4.92	8401.86	15.76	2481.30	16.34
17385	3.72	5.12	5.06	4.78	5.01	4.92	8401.86	15.76	2474.69	16.34
17400	3.73	5.13	5.06	4.78	5.01	4.92	8401.86	15.76	2471.38	16.34
17415	3.73	5.13	5.06	4.78	5.01	4.91	8401.86	15.76	2466.05	16.34
17430	3.72	5.13	5.06	4.78	5.01	4.91	8400.14	15.77	2467.71	16.35
17445	3.73	5.13	5.06	4.78	5.01	4.91	8401.86	15.77	2466.05	16.35
17460	3.72	5.12	5.06	4.78	5.01	4.90	8405.31	15.76	2464.40	16.35
17475	3.72	5.13	5.06	4.78	5.01	4.89	8407.03	15.76	2464.40	16.34
17490	3.72	5.12	5.06	4.78	5.01	4.88	8407.03	15.76	2462.75	16.35
17505	3.71	5.12	5.05	4.78	4.99	4.87	8405.31	15.76	2461.09	16.34
17520	3.71	5.12	5.06	4.76	4.99	4.87	8407.03	15.76	2456.50	16.34
17535	3.71	5.12	5.06	4.78	4.99	4.87	8405.31	15.76	2454.84	16.34
17550	3.71	5.13	5.06	4.78	4.99	4.86	8407.03	15.76	2454.84	16.34
17565	3.70	5.12	5.06	4.78	4.99	4.86	8407.03	15.76	2452.83	16.35
17580	3.70	5.13	5.06	4.78	4.99	4.84	8407.03	15.76	2453.19	16.35
17595	3.70	5.12	5.06	4.76	4.99	4.84	8408.75	15.76	2451.17	16.34
17610	3.70	5.12	5.06	4.76	4.99	4.83	8407.03	15.76	2451.54	16.35
17625	3.69	5.12	5.06	4.78	4.98	4.82	8407.03	15.77	2451.17	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
17640	3.70	5.12	5.06	4.76	4.99	4.82	8407.03	15.76	2449.88	16.35
17655	3.70	5.12	5.05	4.76	4.99	4.82	8407.03	15.77	2449.88	16.34
17670	3.70	5.12	5.05	4.76	4.99	4.82	8407.03	15.77	2451.54	16.34
17685	3.70	5.12	5.05	4.76	4.98	4.81	8407.03	15.76	2449.88	16.34
17700	3.69	5.12	5.06	4.76	4.98	4.80	8407.03	15.76	2451.54	16.34
17715	3.69	5.12	5.05	4.76	4.98	4.80	8407.03	15.76	2449.88	16.34
17730	3.69	5.12	5.05	4.76	4.98	4.80	8407.03	15.77	2448.23	16.34
17745	3.69	5.12	5.05	4.76	4.98	4.79	8408.28	15.76	2446.58	16.34
17760	3.69	5.12	5.05	4.76	4.98	4.78	8405.31	15.76	2444.92	16.34
17775	3.68	5.12	5.06	4.76	4.98	4.77	8407.03	15.77	2443.27	16.34
17790	3.68	5.12	5.05	4.76	4.96	4.76	8405.31	15.76	2441.62	16.34
17805	3.68	5.12	5.05	4.76	4.96	4.76	8405.31	15.76	2446.58	16.35
17820	3.68	5.12	5.05	4.76	4.96	4.75	8405.31	15.76	2446.58	16.34
17835	3.68	5.10	5.05	4.76	4.96	4.74	8405.31	15.76	2448.23	16.34
17850	3.68	5.10	5.05	4.76	4.96	4.74	8404.84	15.76	2443.27	16.34
17865	3.67	5.10	5.05	4.76	4.96	4.73	8406.56	15.76	2439.96	16.34
17880	3.68	5.10	5.05	4.76	4.96	4.72	8407.03	15.77	2438.31	16.34
17895	3.68	5.10	5.05	4.76	4.96	4.72	8406.56	15.76	2435.00	16.34
17910	3.67	5.10	5.05	4.76	4.95	4.72	8405.31	15.77	2433.35	16.34
17925	3.68	5.10	5.05	4.76	4.95	4.71	8404.84	15.76	2430.40	16.34
17940	3.68	5.10	5.05	4.78	4.96	4.71	8407.03	15.77	2428.75	16.34
17955	3.68	5.10	5.05	4.76	4.95	4.71	8407.03	15.76	2426.73	16.34
17970	3.68	5.10	5.05	4.76	4.95	4.70	8404.84	15.75	2425.44	16.34
17985	3.68	5.10	5.05	4.76	4.95	4.70	8407.03	15.77	2422.13	16.34
18000	3.68	5.10	5.06	4.78	4.95	4.70	8406.56	15.76	2422.13	16.34
18015	3.68	5.10	5.05	4.76	4.95	4.69	8406.56	15.76	2420.48	16.34
18030	3.68	5.10	5.06	4.76	4.95	4.69	8404.84	15.76	2418.82	16.34
18045	3.68	5.10	5.06	4.76	4.95	4.69	8406.56	15.76	2418.82	16.34
18060	3.68	5.10	5.06	4.78	4.95	4.69	8407.03	15.76	2417.17	16.34
18075	3.68	5.10	5.06	4.78	4.95	4.68	8404.84	15.76	2413.86	16.34
18090	3.68	5.10	5.06	4.78	4.95	4.68	8407.03	15.77	2413.86	16.34
18105	3.68	5.10	5.06	4.78	4.95	4.68	8404.84	15.75	2415.52	16.34
18120	3.68	5.10	5.06	4.78	4.95	4.68	8404.84	15.76	2415.52	16.33
18135	3.68	5.10	5.06	4.78	4.95	4.68	8405.31	15.76	2415.52	16.34
18150	3.69	5.10	5.06	4.78	4.93	4.68	8404.84	15.76	2413.86	16.33
18165	3.69	5.10	5.06	4.78	4.95	4.68	8406.09	15.75	2415.16	16.35
18180	3.68	5.10	5.06	4.78	4.93	4.68	8405.31	15.76	2416.81	16.35
18195	3.68	5.10	5.06	4.78	4.93	4.68	8405.31	15.77	2415.52	16.34
18210	3.68	5.10	5.06	4.78	4.93	4.68	8403.59	15.77	2418.82	16.34
18225	3.68	5.10	5.06	4.78	4.93	4.67	8404.84	15.76	2420.48	16.34
18240	3.68	5.10	5.06	4.78	4.93	4.68	8406.09	15.77	2418.82	16.34
18255	3.68	5.10	5.06	4.78	4.93	4.67	8405.31	15.77	2418.82	16.33
18270	3.68	5.10	5.06	4.78	4.93	4.67	8404.84	15.75	2418.82	16.34
18285	3.68	5.08	5.06	4.78	4.93	4.67	8405.31	15.77	2420.48	16.34
18300	3.68	5.10	5.06	4.78	4.93	4.66	8406.56	15.77	2418.82	16.34
18315	3.68	5.08	5.06	4.78	4.93	4.66	8403.11	15.76	2415.52	16.33
18330	3.68	5.08	5.06	4.78	4.93	4.66	8405.31	15.77	2417.17	16.34
18345	3.68	5.08	5.06	4.78	4.93	4.66	8406.56	15.76	2415.52	16.34
18360	3.68	5.08	5.06	4.78	4.93	4.66	8405.31	15.77	2416.81	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
18375	3.67	5.08	5.06	4.78	4.93	4.65	8405.31	15.77	2417.17	16.34
18390	3.67	5.08	5.06	4.78	4.93	4.65	8403.11	15.75	2420.48	16.34
18405	3.67	5.08	5.06	4.78	4.93	4.64	8406.09	15.77	2423.79	16.33
18420	3.67	5.08	5.06	4.78	4.92	4.64	8405.31	15.77	2423.79	16.34
18435	3.66	5.08	5.05	4.78	4.92	4.63	8406.56	15.77	2425.08	16.35
18450	3.67	5.07	5.05	4.76	4.92	4.63	8403.59	15.77	2422.13	16.34
18465	3.67	5.07	5.05	4.78	4.92	4.62	8406.56	15.77	2422.13	16.34
18480	3.66	5.07	5.05	4.76	4.92	4.62	8404.84	15.75	2420.48	16.34
18495	3.67	5.07	5.05	4.76	4.92	4.62	8405.31	15.77	2418.46	16.35
18510	3.67	5.07	5.03	4.75	4.93	4.61	8404.84	15.76	2417.17	16.34
18525	3.67	5.05	5.03	4.76	4.92	4.61	8404.84	15.76	2415.52	16.34
18540	3.67	5.05	5.03	4.75	4.93	4.61	8404.84	15.76	2412.21	16.34
18555	3.67	5.05	5.02	4.75	4.92	4.61	8404.84	15.75	2412.21	16.34
18570	3.68	5.05	5.03	4.75	4.92	4.62	8404.84	15.76	2408.90	16.34
18585	3.68	5.05	5.02	4.75	4.92	4.62	8407.03	15.77	2406.89	16.34
18600	3.67	5.04	5.02	4.73	4.93	4.62	8404.84	15.76	2407.25	16.34
18615	3.67	5.04	5.02	4.73	4.93	4.62	8404.84	15.76	2408.90	16.34
18630	3.67	5.04	5.02	4.73	4.93	4.62	8406.56	15.76	2410.55	16.34
18645	3.68	5.04	5.02	4.73	4.93	4.62	8404.84	15.76	2411.85	16.34
18660	3.68	5.02	5.00	4.73	4.93	4.62	8404.84	15.76	2411.85	16.34
18675	3.68	5.04	5.00	4.73	4.93	4.63	8405.31	15.76	2412.21	16.34
18690	3.69	5.02	5.00	4.73	4.93	4.63	8404.84	15.76	2410.20	16.34
18705	3.69	5.02	5.00	4.71	4.93	4.64	8404.84	15.76	2410.20	16.34
18720	3.69	5.04	5.00	4.71	4.95	4.64	8403.59	15.76	2410.20	16.34
18735	3.69	5.02	5.00	4.71	4.93	4.64	8405.31	15.77	2411.85	16.35
18750	3.69	5.02	4.99	4.71	4.93	4.64	8405.31	15.76	2411.85	16.34
18765	3.69	5.02	4.99	4.70	4.93	4.65	8403.59	15.77	2408.90	16.34
18780	3.69	5.01	4.99	4.71	4.95	4.65	8403.59	15.77	2411.49	16.35
18795	3.69	5.01	4.99	4.70	4.95	4.65	8401.86	15.76	2411.49	16.35
18810	3.69	5.01	4.97	4.70	4.95	4.65	8402.34	15.77	2411.49	16.35
18825	3.69	5.01	4.97	4.70	4.95	4.66	8400.61	15.77	2413.15	16.35
18840	3.69	5.01	4.97	4.70	4.96	4.66	8400.61	15.77	2411.49	16.35
18855	3.69	5.01	4.99	4.70	4.96	4.66	8398.89	15.77	2413.15	16.35
18870	3.69	4.99	4.97	4.68	4.95	4.67	8398.89	15.77	2411.49	16.35
18885	3.69	4.99	4.97	4.70	4.96	4.67	8397.17	15.77	2414.80	16.35
18900	3.69	4.99	4.97	4.68	4.96	4.67	8397.17	15.77	2413.50	16.34
18915	3.69	4.99	4.97	4.68	4.96	4.67	8397.17	15.77	2413.50	16.34
18930	3.69	4.99	4.97	4.68	4.96	4.68	8397.17	15.77	2411.49	16.34
18945	3.69	4.99	4.95	4.68	4.96	4.68	8395.92	15.76	2411.49	16.34
18960	3.69	4.99	4.95	4.68	4.96	4.68	8397.17	15.77	2411.49	16.34
18975	3.69	4.99	4.97	4.68	4.96	4.69	8397.17	15.77	2411.49	16.34
18990	3.69	4.99	4.95	4.68	4.96	4.69	8395.92	15.76	2409.84	16.35
19005	3.69	4.99	4.95	4.68	4.96	4.69	8395.92	15.76	2411.49	16.35
19020	3.69	4.99	4.95	4.68	4.96	4.70	8395.92	15.76	2408.19	16.34
19035	3.69	4.97	4.95	4.68	4.96	4.69	8395.92	15.76	2408.19	16.35
19050	3.69	4.97	4.95	4.68	4.96	4.69	8395.45	15.75	2406.53	16.34
19065	3.69	4.97	4.95	4.68	4.96	4.69	8395.92	15.76	2406.53	16.35
19080	3.68	4.97	4.95	4.68	4.96	4.69	8395.45	15.75	2408.19	16.34
19095	3.68	4.99	4.95	4.68	4.96	4.69	8395.92	15.76	2406.53	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
19110	3.68	4.99	4.95	4.68	4.96	4.69	8397.64	15.77	2404.88	16.3
19125	3.68	4.99	4.95	4.67	4.95	4.69	8402.34	15.77	2404.88	16.3
19140	3.68	4.97	4.95	4.68	4.96	4.68	8404.06	15.77	2406.17	16.3
19155	3.68	4.97	4.97	4.68	4.95	4.68	8405.78	15.77	2401.57	16.3
19170	3.68	4.99	4.97	4.68	4.95	4.68	8405.78	15.77	2403.23	16.3
19185	3.68	4.99	4.97	4.68	4.95	4.68	8405.78	15.77	2400.27	16.3
19200	3.68	4.99	4.97	4.70	4.95	4.68	8405.78	15.77	2399.92	16.3
19215	3.68	4.99	4.97	4.70	4.95	4.68	8407.03	15.77	2397.32	16.3
19230	3.68	4.99	4.99	4.70	4.93	4.68	8407.03	15.77	2395.67	16.3
19245	3.68	5.01	4.99	4.70	4.93	4.68	8407.03	15.76	2396.61	16.3
19260	3.68	5.01	4.99	4.71	4.93	4.67	8405.31	15.77	2393.31	16.3
19275	3.67	5.01	4.99	4.71	4.93	4.67	8405.31	15.76	2392.01	16.3
19290	3.67	5.01	4.99	4.71	4.92	4.66	8405.31	15.76	2390.35	16.3
19305	3.67	5.01	5.00	4.71	4.92	4.67	8405.31	15.76	2392.01	16.3
19320	3.68	5.01	5.00	4.71	4.93	4.66	8405.31	15.76	2392.01	16.3
19335	3.67	5.01	4.99	4.73	4.92	4.65	8405.31	15.76	2390.35	16.3
19350	3.68	5.01	5.00	4.71	4.92	4.66	8403.59	15.76	2390.35	16.3
19365	3.68	5.01	5.00	4.71	4.92	4.66	8404.84	15.76	2388.70	16.3
19380	3.68	5.01	5.00	4.71	4.92	4.66	8406.56	15.76	2387.05	16.3
19395	3.68	5.02	5.00	4.71	4.92	4.66	8405.78	15.77	2387.05	16.3
19410	3.68	5.01	5.00	4.71	4.92	4.66	8405.31	15.76	2383.74	16.3
19425	3.68	5.02	5.00	4.71	4.92	4.67	8405.31	15.76	2382.09	16.3
19440	3.68	5.01	5.00	4.71	4.92	4.67	8406.56	15.76	2382.09	16.3
19455	3.68	5.02	5.00	4.71	4.92	4.67	8407.03	15.77	2382.44	16.3
19470	3.68	5.02	5.00	4.73	4.92	4.66	8406.56	15.76	2382.09	16.3
19485	3.67	5.02	5.00	4.73	4.92	4.66	8404.84	15.76	2382.09	16.3
19500	3.67	5.02	5.00	4.73	4.92	4.66	8405.31	15.77	2384.09	16.3
19515	3.68	5.02	5.00	4.73	4.90	4.66	8404.84	15.76	2382.44	16.3
19530	3.68	5.02	5.00	4.73	4.92	4.66	8404.84	15.76	2380.79	16.3
19545	3.68	5.02	5.00	4.73	4.90	4.66	8404.84	15.76	2380.79	16.3
19560	3.68	5.02	5.02	4.73	4.90	4.67	8406.56	15.76	2380.79	16.3
19575	3.68	5.02	5.02	4.73	4.90	4.66	8404.84	15.76	2380.79	16.3
19590	3.68	5.02	5.02	4.73	4.90	4.66	8404.84	15.75	2380.79	16.3
19605	3.68	5.02	5.02	4.73	4.90	4.66	8404.84	15.76	2382.44	16.3
19620	3.68	5.02	5.00	4.73	4.90	4.66	8403.11	15.76	2382.44	16.3
19635	3.67	5.02	5.02	4.73	4.90	4.66	8404.84	15.76	2382.44	16.3
19650	3.67	5.02	5.02	4.73	4.90	4.66	8405.31	15.77	2379.13	16.3
19665	3.68	5.02	5.02	4.73	4.90	4.66	8404.84	15.76	2379.13	16.3
19680	3.68	5.02	5.02	4.73	4.90	4.66	8405.31	15.77	2380.79	16.3
19695	3.68	5.04	5.02	4.73	4.90	4.67	8404.84	15.76	2384.09	16.3
19710	3.69	5.04	5.02	4.73	4.90	4.67	8405.31	15.77	2382.44	16.3
19725	3.69	5.02	5.02	4.75	4.90	4.68	8405.31	15.77	2382.44	16.3
19740	3.68	5.02	5.02	4.73	4.90	4.68	8403.59	15.77	2384.09	16.3
19755	3.68	5.02	5.02	4.73	4.90	4.67	8405.31	15.76	2385.75	16.3
19770	3.68	5.02	5.02	4.73	4.90	4.67	8405.31	15.77	2387.40	16.3
19785	3.67	5.02	5.02	4.75	4.90	4.67	8404.84	15.76	2390.71	16.3
19800	3.68	5.02	5.02	4.73	4.90	4.67	8405.31	15.76	2392.36	16.3
19815	3.68	5.02	5.02	4.75	4.90	4.67	8406.56	15.77	2392.36	16.3
19830	3.68	5.02	5.02	4.73	4.90	4.67	8404.84	15.75	2395.67	16.3

**RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057**

**TIDAL STUDY FIELD DATA
 G CLUSTER WELLS**

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
19845	3.67	5.02	5.02	4.73	4.90	4.67	8405.31	15.76	2397.32	16.34
19860	3.67	5.02	5.02	4.73	4.88	4.66	8405.31	15.77	2400.27	16.35
19875	3.67	5.02	5.00	4.73	4.90	4.66	8404.84	15.75	2397.32	16.34
19890	3.67	5.02	5.00	4.73	4.88	4.66	8404.84	15.76	2395.67	16.33
19905	3.67	5.02	5.00	4.73	4.90	4.66	8403.11	15.76	2394.02	16.34
19920	3.67	5.02	5.00	4.73	4.88	4.66	8404.84	15.76	2390.71	16.34
19935	3.67	5.02	5.00	4.71	4.88	4.66	8404.84	15.75	2387.40	16.34
19950	3.68	5.02	5.00	4.71	4.90	4.67	8404.84	15.76	2385.75	16.34
19965	3.68	5.02	4.99	4.71	4.90	4.67	8405.31	15.77	2382.44	16.34
19980	3.68	5.01	4.99	4.71	4.88	4.66	8403.11	15.76	2379.13	16.34
19995	3.68	5.01	4.97	4.71	4.90	4.67	8403.59	15.77	2380.79	16.34
20010	3.68	5.01	4.97	4.70	4.90	4.67	8401.86	15.77	2380.79	16.34
20025	3.68	5.01	4.97	4.70	4.90	4.68	8399.67	15.76	2382.09	16.34
20040	3.68	4.99	4.97	4.70	4.90	4.67	8399.67	15.76	2385.39	16.34
20055	3.69	4.99	4.97	4.70	4.90	4.68	8397.17	15.77	2387.05	16.34
20070	3.69	4.99	4.95	4.68	4.92	4.69	8396.70	15.77	2388.70	16.34
20085	3.68	4.99	4.95	4.68	4.90	4.68	8396.22	15.76	2390.35	16.34
20100	3.69	4.99	4.95	4.68	4.90	4.69	8393.25	15.76	2390.35	16.35
20115	3.69	4.99	4.95	4.68	4.92	4.69	8391.53	15.76	2390.35	16.34
20130	3.69	4.99	4.95	4.68	4.92	4.70	8393.25	15.77	2388.70	16.35
20145	3.69	4.99	4.95	4.68	4.92	4.71	8392.78	15.76	2390.35	16.35
20160	3.70	4.99	4.95	4.68	4.93	4.72	8391.53	15.76	2391.65	16.35
20175	3.70	4.99	4.95	4.68	4.92	4.72	8392.00	15.77	2396.97	16.35
20190	3.69	4.99	4.94	4.67	4.92	4.72	8392.00	15.77	2406.53	16.35
20205	3.70	4.99	4.94	4.67	4.93	4.73	8393.73	15.77	2409.84	16.35
20220	3.70	4.99	4.94	4.68	4.93	4.73	8393.73	15.77	2411.85	16.34
20235	3.70	4.99	4.94	4.67	4.93	4.74	8393.73	15.77	2411.49	16.35
20250	3.70	4.99	4.94	4.67	4.93	4.74	8393.73	15.77	2411.49	16.35
20265	3.70	4.97	4.94	4.67	4.93	4.73	8393.73	15.77	2409.84	16.35
20280	3.69	4.97	4.92	4.67	4.93	4.73	8393.73	15.77	2409.84	16.35
20295	3.70	4.99	4.94	4.67	4.93	4.74	8393.73	15.77	2411.49	16.35
20310	3.70	4.99	4.94	4.67	4.93	4.75	8392.00	15.77	2409.84	16.35
20325	3.70	4.99	4.94	4.67	4.93	4.76	8393.73	15.77	2413.15	16.35
20340	3.70	4.99	4.94	4.67	4.93	4.75	8393.73	15.77	2418.11	16.35
20355	3.70	4.99	4.95	4.67	4.93	4.76	8393.73	15.77	2419.76	16.35
20370	3.71	4.99	4.94	4.67	4.93	4.77	8392.00	15.75	2416.81	16.34
20385	3.71	5.01	4.94	4.68	4.93	4.78	8392.00	15.77	2416.45	16.35
20400	3.70	5.01	4.95	4.68	4.93	4.78	8393.73	15.77	2414.80	16.35
20415	3.70	5.01	4.95	4.68	4.93	4.78	8393.73	15.77	2414.80	16.35
20430	3.70	5.01	4.95	4.67	4.93	4.78	8392.00	15.77	2418.11	16.35
20445	3.70	5.01	4.95	4.68	4.93	4.78	8392.00	15.77	2421.77	16.35
20460	3.70	5.01	4.95	4.68	4.93	4.79	8392.00	15.77	2421.41	16.35
20475	3.70	5.01	4.95	4.68	4.93	4.79	8392.00	15.77	2420.12	16.35
20490	3.70	5.01	4.95	4.68	4.93	4.79	8390.28	15.77	2418.11	16.35
20505	3.70	5.01	4.95	4.68	4.93	4.79	8393.25	15.77	2418.11	16.35
20520	3.70	5.01	4.95	4.68	4.93	4.80	8392.00	15.75	2418.46	16.35
20535	3.70	5.01	4.95	4.68	4.93	4.80	8392.00	15.77	2416.81	16.34
20550	3.70	5.01	4.95	4.68	4.93	4.80	8392.00	15.75	2419.76	16.35
20565	3.70	5.01	4.95	4.68	4.92	4.80	8392.00	15.77	2421.77	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
20580	3.70	5.01	4.95	4.68	4.92	4.80	8393.73	15.77	2423.07	16.35
20595	3.70	5.02	4.95	4.68	4.93	4.81	8393.25	15.77	2420.12	16.34
20610	3.70	5.02	4.95	4.68	4.93	4.81	8393.73	15.77	2420.12	16.35
20625	3.70	5.02	4.95	4.68	4.92	4.81	8393.25	15.77	2414.80	16.35
20640	3.70	5.02	4.95	4.68	4.92	4.82	8393.25	15.77	2415.16	16.35
20655	3.70	5.02	4.97	4.68	4.93	4.82	8393.25	15.76	2416.81	16.35
20670	3.70	5.02	4.95	4.68	4.92	4.82	8393.25	15.76	2418.46	16.35
20685	3.70	5.02	4.97	4.70	4.93	4.82	8393.25	15.76	2420.12	16.35
20700	3.70	5.02	4.95	4.70	4.92	4.82	8393.25	15.76	2420.12	16.34
20715	3.70	5.02	4.97	4.68	4.92	4.82	8393.25	15.76	2420.12	16.35
20730	3.70	5.02	4.95	4.68	4.92	4.82	8393.25	15.76	2418.46	16.35
20745	3.70	5.04	4.97	4.70	4.92	4.82	8393.73	15.77	2416.81	16.34
20760	3.70	5.04	4.97	4.70	4.92	4.82	8391.53	15.76	2416.81	16.34
20775	3.69	5.02	4.97	4.70	4.92	4.82	8393.25	15.76	2418.46	16.35
20790	3.69	5.02	4.95	4.70	4.92	4.82	8391.53	15.76	2416.81	16.34
20805	3.70	5.04	4.97	4.68	4.92	4.82	8391.53	15.76	2415.16	16.35
20820	3.69	5.04	4.97	4.68	4.92	4.82	8391.53	15.76	2415.16	16.34
20835	3.69	5.04	4.95	4.70	4.92	4.82	8393.25	15.76	2415.16	16.35
20850	3.69	5.04	4.97	4.68	4.92	4.82	8393.25	15.76	2415.16	16.34
20865	3.69	5.02	4.95	4.68	4.92	4.82	8393.25	15.76	2415.16	16.35
20880	3.69	5.04	4.97	4.68	4.92	4.82	8393.25	15.77	2415.16	16.35
20895	3.69	5.04	4.95	4.68	4.92	4.82	8391.53	15.76	2416.81	16.35
20910	3.70	5.02	4.95	4.68	4.92	4.82	8391.53	15.76	2415.16	16.34
20925	3.69	5.04	4.95	4.70	4.92	4.82	8391.53	15.76	2413.50	16.34
20940	3.70	5.04	4.97	4.68	4.92	4.82	8391.53	15.76	2415.16	16.35
20955	3.70	5.04	4.97	4.68	4.92	4.83	8391.53	15.76	2415.16	16.34
20970	3.70	5.04	4.97	4.70	4.92	4.84	8389.81	15.76	2415.16	16.34
20985	3.70	5.04	4.95	4.70	4.92	4.85	8391.53	15.76	2416.81	16.34
21000	3.70	5.04	4.97	4.70	4.92	4.84	8391.53	15.76	2415.16	16.34
21015	3.70	5.04	4.97	4.70	4.92	4.85	8392.00	15.77	2416.81	16.35
21030	3.70	5.04	4.97	4.70	4.92	4.86	8391.53	15.76	2416.81	16.35
21045	3.70	5.04	4.97	4.70	4.92	4.86	8391.53	15.76	2420.12	16.35
21060	3.70	5.04	4.97	4.70	4.92	4.87	8389.81	15.76	2421.77	16.35
21075	3.70	5.04	4.97	4.70	4.92	4.87	8389.81	15.76	2425.08	16.34
21090	3.70	5.04	4.97	4.70	4.92	4.87	8389.81	15.76	2428.39	16.35
21105	3.71	5.05	4.97	4.70	4.92	4.88	8389.81	15.76	2433.35	16.35
21120	3.70	5.05	4.97	4.70	4.92	4.88	8389.81	15.76	2431.69	16.35
21135	3.71	5.05	4.97	4.70	4.92	4.88	8388.08	15.76	2431.69	16.35
21150	3.70	5.05	4.97	4.70	4.92	4.89	8389.81	15.76	2430.04	16.34
21165	3.70	5.05	4.97	4.70	4.92	4.88	8389.81	15.76	2433.35	16.35
21180	3.70	5.04	4.97	4.70	4.92	4.89	8389.81	15.76	2438.31	16.34
21195	3.70	5.05	4.97	4.70	4.92	4.89	8388.08	15.76	2443.27	16.35
21210	3.70	5.05	4.97	4.70	4.92	4.89	8389.81	15.76	2443.27	16.35
21225	3.70	5.05	4.97	4.70	4.92	4.89	8389.81	15.76	2439.96	16.34
21240	3.70	5.05	4.97	4.70	4.92	4.89	8389.81	15.76	2435.00	16.35
21255	3.70	5.05	4.97	4.70	4.92	4.89	8389.81	15.76	2435.00	16.35
21270	3.69	5.05	4.97	4.70	4.92	4.88	8389.81	15.76	2433.35	16.35
21285	3.70	5.04	4.97	4.70	4.92	4.88	8389.81	15.76	2435.00	16.34
21300	3.70	5.05	4.97	4.70	4.92	4.88	8389.81	15.76	2435.00	16.35

RAYMARK INDUSTRIES, INC.
STRATFORD, CONNECTICUT
RCRA SECTION 3013 ORDER
DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
21315	3.69	5.04	4.95	4.68	4.92	4.88	8393.25	15.76	2435.00	16.3
21330	3.69	5.05	4.97	4.68	4.90	4.88	8391.53	15.76	2436.65	16.3
21345	3.70	5.04	4.95	4.68	4.92	4.88	8393.25	15.76	2436.65	16.3
21360	3.70	5.04	4.95	4.68	4.92	4.88	8391.53	15.76	2433.35	16.3
21375	3.69	5.04	4.95	4.70	4.92	4.89	8389.81	15.76	2431.69	16.3
21390	3.70	5.05	4.95	4.68	4.92	4.88	8389.81	15.76	2430.04	16.3
21405	3.70	5.05	4.95	4.68	4.92	4.88	8391.53	15.77	2426.73	16.3
21420	3.71	5.05	4.95	4.68	4.92	4.89	8389.81	15.76	2423.43	16.3
21435	3.71	5.05	4.95	4.68	4.92	4.89	8388.08	15.76	2420.12	16.3
21450	3.71	5.05	4.95	4.68	4.92	4.90	8391.53	15.76	2421.77	16.3
21465	3.71	5.05	4.95	4.68	4.92	4.90	8389.81	15.76	2420.12	16.3
21480	3.71	5.05	4.95	4.68	4.92	4.90	8391.53	15.77	2420.12	16.3
21495	3.72	5.05	4.95	4.68	4.92	4.91	8393.25	15.76	2420.12	16.3
21510	3.71	5.05	4.94	4.68	4.92	4.90	8392.00	15.75	2420.12	16.3
21525	3.71	5.04	4.95	4.68	4.92	4.92	8391.53	15.77	2419.76	16.3
21540	3.71	5.04	4.94	4.67	4.92	4.91	8391.53	15.77	2421.77	16.3
21555	3.71	5.04	4.94	4.67	4.93	4.92	8390.28	15.77	2421.41	16.3
21570	3.71	5.04	4.94	4.67	4.93	4.92	8390.28	15.77	2421.77	16.3
21585	3.71	5.04	4.94	4.67	4.93	4.92	8390.28	15.77	2423.07	16.3
21600	3.71	5.04	4.94	4.67	4.93	4.92	8390.28	15.77	2425.08	16.3
21615	3.71	5.04	4.94	4.67	4.92	4.92	8391.53	15.76	2424.72	16.3
21630	3.71	5.04	4.94	4.67	4.93	4.92	8391.53	15.77	2428.39	16.3
21645	3.72	5.04	4.94	4.67	4.93	4.93	8393.73	15.77	2429.68	16.3
21660	3.72	5.04	4.94	4.68	4.93	4.94	8392.00	15.77	2431.33	16.3
21675	3.72	5.05	4.94	4.68	4.93	4.94	8392.00	15.77	2433.35	16.3
21690	3.72	5.04	4.94	4.67	4.93	4.94	8390.28	15.77	2436.29	16.3
21705	3.71	5.04	4.94	4.67	4.93	4.94	8390.28	15.77	2437.95	16.3
21720	3.71	5.04	4.94	4.67	4.93	4.94	8390.28	15.77	2441.25	16.3
21735	3.72	5.04	4.94	4.68	4.93	4.95	8390.28	15.77	2442.91	16.3
21750	3.71	5.04	4.94	4.67	4.93	4.95	8388.56	15.77	2441.62	16.3
21765	3.72	5.05	4.94	4.67	4.93	4.95	8390.28	15.77	2444.56	16.3
21780	3.72	5.05	4.94	4.67	4.93	4.96	8388.56	15.75	2442.91	16.3
21795	3.71	5.05	4.94	4.67	4.93	4.95	8388.56	15.75	2439.96	16.3
21810	3.71	5.05	4.94	4.68	4.93	4.95	8388.56	15.77	2441.25	16.3
21825	3.72	5.05	4.94	4.67	4.93	4.95	8389.81	15.77	2439.96	16.3
21840	3.74	5.05	4.94	4.68	4.92	4.95	8390.28	15.77	2439.60	16.3
21855	3.78	5.05	4.94	4.68	4.93	4.95	8391.53	15.77	2431.33	16.3
21870	3.82	5.07	4.95	4.68	4.92	4.96	8389.81	15.77	2421.41	16.3
21885	3.84	5.07	4.95	4.68	4.93	4.97	8391.53	15.76	2410.20	16.3
21900	3.84	5.07	4.95	4.68	4.93	4.97	8390.28	15.75	2401.93	16.3
21915	3.84	5.07	4.95	4.68	4.93	4.97	8391.53	15.77	2396.61	16.3
21930	3.83	5.07	4.95	4.68	4.93	4.96	8391.53	15.76	2386.69	16.3
21945	3.83	5.07	4.95	4.68	4.92	4.96	8390.28	15.75	2380.08	16.3
21960	3.83	5.07	4.95	4.68	4.93	4.96	8390.28	15.77	2373.46	16.3
21975	3.83	5.07	4.95	4.68	4.92	4.95	8390.28	15.75	2363.54	16.3
21990	3.82	5.07	4.95	4.68	4.92	4.95	8391.53	15.76	2355.63	16.3
22005	3.81	5.07	4.94	4.68	4.92	4.95	8391.53	15.76	2349.01	16.3
22020	3.80	5.07	4.95	4.68	4.92	4.94	8391.53	15.76	2342.40	16.3
22035	3.79	5.07	4.94	4.67	4.92	4.93	8390.28	15.77	2337.09	16.3

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
22050	3.80	5.07	4.94	4.68	4.92	4.92	8391.53	15.76	2330.48	16.35
22065	3.81	5.07	4.94	4.67	4.92	4.90	8391.53	15.76	2323.86	16.35
22080	3.82	5.07	4.94	4.67	4.92	4.90	8393.25	15.76	2317.25	16.35
22095	3.83	5.07	4.94	4.67	4.92	4.91	8392.00	15.77	2309.33	16.34
22110	3.82	5.07	4.94	4.68	4.92	4.90	8393.25	15.77	2305.68	16.35
22125	3.80	5.07	4.95	4.68	4.92	4.90	8393.25	15.76	2299.40	16.35
22140	3.79	5.07	4.94	4.67	4.90	4.89	8393.25	15.77	2297.41	16.35
22155	3.77	5.07	4.94	4.67	4.92	4.88	8394.97	15.76	2294.44	16.35
22170	3.77	5.07	4.94	4.67	4.92	4.88	8394.97	15.76	2294.44	16.35
22185	3.76	5.07	4.94	4.67	4.90	4.87	8394.97	15.76	2296.10	16.35
22200	3.76	5.07	4.94	4.68	4.90	4.87	8394.97	15.77	2299.40	16.35
22215	3.76	5.07	4.94	4.67	4.90	4.86	8396.70	15.76	2302.71	16.35
22230	3.74	5.07	4.94	4.67	4.90	4.85	8398.42	15.76	2307.67	16.35
22245	3.74	5.07	4.94	4.67	4.90	4.85	8400.14	15.76	2315.94	16.35
22260	3.73	5.07	4.94	4.67	4.90	4.84	8400.14	15.77	2322.21	16.35
22275	3.72	5.07	4.94	4.67	4.90	4.83	8398.42	15.77	2330.82	16.35
22290	3.72	5.07	4.94	4.67	4.90	4.82	8400.14	15.76	2339.09	16.35
22305	3.72	5.07	4.94	4.67	4.90	4.82	8400.14	15.76	2344.05	16.35
22320	3.72	5.07	4.92	4.67	4.90	4.82	8401.86	15.76	2349.01	16.35
22335	3.72	5.07	4.94	4.67	4.90	4.81	8400.14	15.76	2353.97	16.35
22350	3.71	5.07	4.94	4.67	4.90	4.81	8401.86	15.76	2360.59	16.35
22365	3.71	5.07	4.94	4.67	4.88	4.80	8401.86	15.76	2370.51	16.35
22380	3.71	5.07	4.94	4.68	4.88	4.80	8401.86	15.76	2378.78	16.35
22395	3.71	5.07	4.94	4.67	4.88	4.79	8400.14	15.76	2388.70	16.35
22410	3.70	5.07	4.94	4.67	4.88	4.79	8402.34	15.77	2396.97	16.35
22425	3.70	5.07	4.94	4.67	4.88	4.79	8400.14	15.76	2405.24	16.35
22440	3.70	5.07	4.94	4.67	4.88	4.79	8401.86	15.76	2411.85	16.35
22455	3.70	5.07	4.94	4.68	4.88	4.79	8401.39	15.76	2418.46	16.35
22470	3.70	5.08	4.94	4.67	4.88	4.78	8401.39	15.76	2425.08	16.35
22485	3.70	5.07	4.94	4.68	4.88	4.78	8401.39	15.76	2432.05	16.34
22500	3.70	5.08	4.94	4.68	4.88	4.77	8401.39	15.76	2436.65	16.35
22515	3.70	5.08	4.95	4.68	4.88	4.77	8401.39	15.76	2441.62	16.35
22530	3.70	5.08	4.95	4.68	4.87	4.76	8401.39	15.76	2446.58	16.35
22545	3.70	5.07	4.95	4.68	4.87	4.76	8403.59	15.77	2451.54	16.35
22560	3.69	5.07	4.94	4.68	4.87	4.76	8401.39	15.76	2455.21	16.36
22575	3.69	5.08	4.94	4.68	4.87	4.75	8401.39	15.76	2460.17	16.34
22590	3.69	5.08	4.95	4.68	4.87	4.75	8401.39	15.76	2461.82	16.34
22605	3.70	5.08	4.94	4.68	4.87	4.75	8401.39	15.76	2465.13	16.36
22620	3.69	5.08	4.94	4.67	4.87	4.74	8401.86	15.77	2465.13	16.36
22635	3.69	5.08	4.94	4.68	4.87	4.74	8401.39	15.76	2470.09	16.34
22650	3.69	5.08	4.94	4.67	4.87	4.73	8400.14	15.76	2469.73	16.34
22665	3.68	5.07	4.94	4.67	4.87	4.72	8401.39	15.76	2471.75	16.34
22680	3.68	5.08	4.94	4.67	4.87	4.72	8401.39	15.76	2475.06	16.34
22695	3.68	5.07	4.94	4.67	4.87	4.72	8401.39	15.76	2476.34	16.35
22710	3.68	5.07	4.94	4.67	4.87	4.71	8401.39	15.76	2478.36	16.34
22725	3.68	5.08	4.94	4.67	4.87	4.71	8401.39	15.76	2480.02	16.34
22740	3.68	5.07	4.94	4.67	4.87	4.71	8401.39	15.76	2479.65	16.34
22755	3.69	5.08	4.94	4.67	4.87	4.71	8401.39	15.76	2479.65	16.35
22770	3.68	5.07	4.92	4.67	4.87	4.69	8401.86	15.77	2477.99	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
22785	3.68	5.08	4.92	4.65	4.87	4.70	8401.39	15.76	2479.65	16.34
22800	3.68	5.08	4.92	4.67	4.87	4.69	8401.39	15.76	2480.02	16.34
22815	3.68	5.07	4.92	4.65	4.85	4.69	8401.39	15.76	2478.36	16.36
22830	3.68	5.07	4.92	4.65	4.87	4.68	8401.39	15.76	2479.65	16.35
22845	3.68	5.07	4.91	4.65	4.85	4.68	8401.39	15.76	2479.65	16.34
22860	3.68	5.07	4.92	4.65	4.87	4.68	8401.39	15.76	2480.02	16.36
22875	3.68	5.07	4.91	4.65	4.87	4.68	8400.14	15.76	2479.65	16.35
22890	3.67	5.07	4.91	4.64	4.87	4.67	8400.14	15.76	2477.99	16.35
22905	3.68	5.07	4.91	4.64	4.87	4.67	8400.14	15.76	2477.99	16.35
22920	3.68	5.07	4.91	4.64	4.87	4.68	8400.14	15.76	2477.99	16.35
22935	3.68	5.07	4.91	4.64	4.87	4.68	8400.14	15.76	2477.99	16.35
22950	3.69	5.07	4.91	4.64	4.87	4.68	8400.14	15.76	2476.34	16.35
22965	3.68	5.05	4.89	4.64	4.87	4.67	8398.42	15.76	2476.34	16.35
22980	3.68	5.07	4.89	4.64	4.87	4.67	8400.14	15.76	2476.34	16.35
22995	3.68	5.05	4.89	4.64	4.87	4.67	8400.14	15.77	2476.34	16.35
23010	3.68	5.07	4.89	4.62	4.87	4.67	8400.14	15.77	2477.99	16.35
23025	3.69	5.07	4.89	4.64	4.87	4.67	8400.14	15.76	2477.63	16.35
23040	3.69	5.05	4.88	4.62	4.87	4.67	8397.17	15.75	2476.71	16.34
23055	3.69	5.05	4.88	4.64	4.87	4.68	8398.89	15.77	2477.99	16.35
23070	3.70	5.05	4.89	4.62	4.88	4.67	8398.89	15.77	2475.97	16.35
23085	3.70	5.05	4.89	4.62	4.87	4.69	8397.17	15.77	2474.69	16.36
23100	3.70	5.05	4.88	4.60	4.88	4.68	8397.17	15.77	2472.67	16.35
23115	3.69	5.05	4.88	4.60	4.87	4.68	8397.17	15.77	2471.38	16.34
23130	3.70	5.05	4.88	4.62	4.88	4.69	8397.17	15.77	2471.38	16.34
23145	3.70	5.05	4.88	4.62	4.88	4.69	8397.17	15.77	2469.73	16.34
23160	3.69	5.05	4.88	4.62	4.88	4.69	8397.17	15.77	2471.38	16.34
23175	3.69	5.05	4.86	4.60	4.88	4.69	8395.45	15.77	2471.38	16.35
23190	3.69	5.04	4.86	4.60	4.88	4.69	8397.17	15.77	2473.03	16.35
23205	3.70	5.05	4.86	4.60	4.88	4.70	8395.45	15.77	2475.97	16.35
23220	3.70	5.05	4.86	4.59	4.88	4.69	8394.20	15.76	2475.97	16.34
23235	3.70	5.05	4.86	4.59	4.90	4.70	8394.20	15.76	2475.97	16.35
23250	3.70	5.05	4.86	4.60	4.88	4.70	8394.20	15.76	2475.97	16.35
23265	3.70	5.05	4.86	4.59	4.90	4.70	8394.20	15.76	2475.97	16.35
23280	3.70	5.05	4.86	4.60	4.90	4.70	8395.92	15.76	2478.91	16.35
23295	3.70	5.04	4.84	4.59	4.90	4.70	8395.45	15.75	2479.28	16.35
23310	3.70	5.04	4.84	4.59	4.88	4.70	8395.92	15.76	2479.28	16.35
23325	3.70	5.04	4.84	4.59	4.90	4.71	8395.92	15.77	2482.59	16.35
23340	3.70	5.04	4.84	4.59	4.90	4.71	8394.20	15.76	2480.93	16.35
23355	3.69	5.04	4.84	4.59	4.90	4.70	8395.92	15.76	2482.22	16.34
23370	3.69	5.04	4.84	4.59	4.90	4.70	8395.92	15.76	2484.24	16.35
23385	3.69	5.04	4.84	4.59	4.90	4.70	8395.92	15.76	2487.55	16.35
23400	3.68	5.04	4.84	4.59	4.88	4.69	8397.17	15.75	2487.55	16.35
23415	3.69	5.05	4.86	4.59	4.88	4.69	8397.64	15.76	2490.48	16.35
23430	3.68	5.05	4.86	4.59	4.88	4.68	8399.37	15.76	2490.85	16.35
23445	3.68	5.05	4.86	4.60	4.88	4.68	8400.61	15.77	2492.51	16.35
23460	3.68	5.05	4.86	4.60	4.88	4.67	8400.61	15.77	2489.20	16.34
23475	3.68	5.05	4.86	4.60	4.87	4.67	8400.61	15.77	2489.20	16.35
23490	3.69	5.07	4.88	4.60	4.88	4.67	8400.61	15.77	2487.92	16.34
23505	3.68	5.07	4.88	4.60	4.87	4.67	8398.89	15.75	2485.89	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
23520	3.69	5.07	4.88	4.60	4.87	4.67	8400.61	15.75	2485.89	16.35
23535	3.68	5.07	4.88	4.60	4.87	4.66	8400.14	15.76	2484.24	16.35
23550	3.68	5.07	4.88	4.60	4.87	4.66	8398.89	15.75	2482.59	16.35
23565	3.68	5.07	4.88	4.60	4.87	4.66	8400.61	15.77	2482.59	16.35
23580	3.68	5.07	4.88	4.62	4.87	4.66	8400.14	15.77	2480.93	16.35
23595	3.69	5.07	4.88	4.62	4.87	4.66	8401.86	15.77	2479.28	16.35
23610	3.68	5.07	4.88	4.62	4.87	4.66	8401.86	15.77	2477.63	16.35
23625	3.68	5.08	4.88	4.62	4.87	4.65	8401.86	15.77	2479.65	16.35
23640	3.69	5.08	4.89	4.62	4.87	4.66	8401.86	15.76	2475.97	16.35
23655	3.69	5.08	4.89	4.62	4.87	4.67	8400.61	15.77	2473.03	16.35
23670	3.69	5.08	4.89	4.62	4.85	4.67	8401.86	15.76	2471.01	16.35
23685	3.69	5.08	4.89	4.62	4.87	4.67	8400.14	15.76	2471.38	16.35
23700	3.69	5.08	4.89	4.62	4.85	4.67	8400.14	15.76	2471.38	16.35
23715	3.69	5.08	4.89	4.62	4.85	4.67	8400.14	15.76	2471.38	16.35
23730	3.69	5.08	4.89	4.62	4.85	4.67	8400.14	15.76	2471.38	16.35
23745	3.69	5.08	4.89	4.62	4.85	4.67	8400.14	15.76	2471.38	16.35
23760	3.69	5.10	4.89	4.64	4.85	4.68	8400.14	15.76	2473.03	16.35
23775	3.69	5.08	4.89	4.64	4.85	4.67	8400.14	15.76	2471.38	16.35
23790	3.69	5.10	4.89	4.64	4.85	4.67	8400.14	15.76	2473.03	16.35
23805	3.69	5.10	4.89	4.64	4.85	4.67	8400.14	15.76	2471.38	16.35
23820	3.69	5.10	4.89	4.64	4.85	4.67	8400.14	15.76	2471.38	16.35
23835	3.69	5.10	4.89	4.64	4.85	4.68	8400.14	15.77	2471.38	16.35
23850	3.69	5.10	4.89	4.62	4.85	4.68	8400.14	15.76	2473.03	16.35
23865	3.69	5.10	4.89	4.62	4.85	4.68	8400.14	15.76	2471.38	16.35
23880	3.69	5.10	4.89	4.64	4.85	4.68	8400.14	15.76	2471.38	16.35
23895	3.69	5.10	4.89	4.62	4.85	4.68	8398.42	15.76	2473.03	16.35
23910	3.69	5.10	4.89	4.64	4.84	4.68	8400.14	15.76	2473.03	16.35
23925	3.70	5.10	4.89	4.64	4.85	4.69	8400.14	15.76	2469.73	16.34
23940	3.70	5.10	4.89	4.64	4.85	4.69	8398.42	15.76	2469.73	16.35
23955	3.70	5.10	4.89	4.64	4.84	4.69	8400.14	15.76	2469.73	16.35
23970	3.70	5.10	4.89	4.64	4.85	4.69	8398.42	15.76	2469.73	16.35
23985	3.70	5.10	4.89	4.64	4.85	4.69	8400.14	15.76	2469.73	16.35
24000	3.69	5.10	4.89	4.64	4.85	4.69	8400.14	15.76	2471.38	16.35
24015	3.70	5.10	4.89	4.64	4.85	4.70	8400.14	15.76	2471.38	16.35
24030	3.69	5.10	4.89	4.64	4.85	4.69	8400.14	15.76	2471.38	16.35
24045	3.70	5.10	4.89	4.64	4.85	4.70	8400.14	15.76	2469.73	16.35
24060	3.70	5.10	4.89	4.64	4.85	4.70	8398.42	15.76	2469.73	16.35
24075	3.69	5.12	4.89	4.64	4.85	4.70	8400.14	15.76	2469.73	16.35
24090	3.69	5.10	4.89	4.64	4.85	4.70	8400.14	15.76	2471.38	16.35
24105	3.69	5.12	4.89	4.64	4.85	4.70	8400.14	15.76	2471.38	16.35
24120	3.69	5.10	4.89	4.64	4.85	4.70	8400.14	15.76	2470.09	16.36
24135	3.69	5.12	4.89	4.62	4.84	4.70	8398.42	15.76	2471.38	16.35
24150	3.69	5.12	4.89	4.64	4.85	4.70	8401.39	15.76	2469.73	16.35
24165	3.69	5.10	4.89	4.64	4.84	4.70	8401.39	15.76	2469.73	16.35
24180	3.70	5.12	4.89	4.62	4.85	4.70	8398.42	15.76	2469.73	16.35
24195	3.68	5.10	4.88	4.62	4.84	4.69	8398.42	15.76	2469.73	16.35
24210	3.69	5.10	4.88	4.62	4.84	4.69	8400.14	15.76	2470.09	16.36
24225	3.69	5.12	4.89	4.64	4.85	4.69	8400.14	15.76	2469.73	16.35
24240	3.68	5.10	4.89	4.62	4.84	4.69	8399.67	15.76	2469.73	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
24255	3.69	5.10	4.88	4.62	4.84	4.69	8400.14	15.76	2469.73	16.39
24270	3.68	5.10	4.89	4.62	4.84	4.68	8398.42	15.76	2469.73	16.39
24285	3.68	5.10	4.89	4.62	4.84	4.68	8400.14	15.76	2471.38	16.39
24300	3.69	5.10	4.88	4.62	4.84	4.68	8400.14	15.76	2469.73	16.39
24315	3.69	5.10	4.88	4.62	4.84	4.69	8398.42	15.76	2471.38	16.39
24330	3.70	5.10	4.88	4.62	4.84	4.69	8398.89	15.77	2471.38	16.39
24345	3.69	5.10	4.88	4.62	4.85	4.69	8398.42	15.76	2471.38	16.39
24360	3.70	5.10	4.88	4.62	4.85	4.69	8398.42	15.76	2469.73	16.39
24375	3.69	5.10	4.88	4.62	4.84	4.70	8398.42	15.76	2468.07	16.39
24390	3.69	5.10	4.88	4.62	4.85	4.69	8398.42	15.76	2469.73	16.39
24405	3.68	5.10	4.88	4.60	4.84	4.69	8398.42	15.76	2469.73	16.39
24420	3.68	5.10	4.88	4.62	4.84	4.68	8398.42	15.76	2471.38	16.39
24435	3.68	5.08	4.86	4.60	4.84	4.68	8398.42	15.76	2471.38	16.39
24450	3.69	5.08	4.86	4.60	4.84	4.68	8398.42	15.76	2471.38	16.39
24465	3.69	5.10	4.86	4.60	4.84	4.67	8398.42	15.76	2471.38	16.39
24480	3.69	5.10	4.88	4.60	4.84	4.67	8398.42	15.76	2469.73	16.39
24495	3.69	5.10	4.88	4.62	4.84	4.68	8398.42	15.77	2469.73	16.39
24510	3.70	5.10	4.86	4.60	4.84	4.68	8398.42	15.76	2469.73	16.39
24525	3.72	5.10	4.86	4.60	4.84	4.68	8398.42	15.76	2471.38	16.39
24540	3.74	5.10	4.88	4.60	4.84	4.69	8398.42	15.76	2471.38	16.39
24555	3.77	5.10	4.88	4.62	4.84	4.69	8398.42	15.76	2469.73	16.39
24570	3.79	5.12	4.88	4.62	4.84	4.70	8398.42	15.76	2469.73	16.39
24585	3.82	5.12	4.88	4.62	4.84	4.71	8396.70	15.76	2466.42	16.39
24600	3.83	5.12	4.88	4.62	4.85	4.71	8396.70	15.76	2464.77	16.39
24615	3.83	5.12	4.88	4.62	4.85	4.71	8396.70	15.76	2466.42	16.39
24630	3.84	5.12	4.88	4.62	4.85	4.71	8396.70	15.76	2464.77	16.39
24645	3.84	5.12	4.88	4.62	4.85	4.72	8394.97	15.76	2464.77	16.39
24660	3.84	5.12	4.88	4.62	4.85	4.72	8394.97	15.76	2463.11	16.39
24675	3.85	5.13	4.88	4.62	4.85	4.73	8394.97	15.76	2464.77	16.39
24690	3.85	5.13	4.88	4.62	4.85	4.73	8393.25	15.76	2463.11	16.39
24705	3.86	5.13	4.88	4.62	4.85	4.74	8393.25	15.76	2463.11	16.39
24720	3.85	5.13	4.89	4.62	4.85	4.74	8393.25	15.76	2463.11	16.39
24735	3.85	5.13	4.89	4.64	4.85	4.74	8394.97	15.76	2463.11	16.39
24750	3.84	5.13	4.89	4.64	4.85	4.75	8393.25	15.76	2461.46	16.39
24765	3.83	5.13	4.89	4.64	4.85	4.75	8393.25	15.76	2464.77	16.39
24780	3.83	5.13	4.89	4.64	4.85	4.76	8393.25	15.76	2466.42	16.39
24795	3.83	5.13	4.89	4.64	4.85	4.76	8393.25	15.76	2468.07	16.39
24810	3.83	5.13	4.89	4.64	4.85	4.76	8391.53	15.76	2469.73	16.39
24825	3.84	5.13	4.89	4.64	4.85	4.75	8393.25	15.76	2469.73	16.39
24840	3.85	5.13	4.91	4.64	4.87	4.76	8391.53	15.76	2471.38	16.39
24855	3.86	5.13	4.89	4.64	4.85	4.76	8391.53	15.76	2471.38	16.39
24870	3.87	5.13	4.89	4.64	4.87	4.76	8393.25	15.76	2471.38	16.39
24885	3.89	5.13	4.91	4.64	4.87	4.76	8393.25	15.76	2471.75	16.39
24900	3.90	5.15	4.91	4.65	4.85	4.77	8393.25	15.76	2471.38	16.39
24915	3.90	5.15	4.91	4.64	4.87	4.77	8393.25	15.76	2471.38	16.39
24930	3.92	5.15	4.91	4.65	4.87	4.78	8393.25	15.76	2469.73	16.39
24945	3.93	5.15	4.91	4.65	4.87	4.78	8394.97	15.76	2468.07	16.39
24960	3.92	5.15	4.91	4.65	4.87	4.78	8393.25	15.76	2466.42	16.39
24975	3.91	5.15	4.91	4.65	4.87	4.78	8393.25	15.76	2466.42	16.39

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
24990	3.90	5.15	4.91	4.65	4.87	4.78	8392.78	15.76	2466.42	16.35
25005	3.89	5.15	4.91	4.64	4.87	4.78	8393.25	15.76	2469.73	16.35
25020	3.89	5.15	4.91	4.65	4.87	4.78	8393.25	15.76	2471.38	16.34
25035	3.87	5.15	4.91	4.65	4.87	4.78	8391.53	15.76	2473.03	16.35
25050	3.86	5.15	4.92	4.65	4.87	4.78	8393.25	15.76	2476.34	16.35
25065	3.85	5.15	4.91	4.67	4.87	4.79	8393.25	15.76	2481.30	16.35
25080	3.85	5.15	4.91	4.65	4.87	4.79	8393.25	15.76	2484.61	16.35
25095	3.84	5.15	4.92	4.67	4.87	4.80	8391.53	15.76	2487.92	16.35
25110	3.83	5.15	4.92	4.67	4.88	4.80	8391.53	15.76	2491.22	16.35
25125	3.83	5.15	4.92	4.67	4.88	4.80	8391.53	15.76	2492.88	16.35
25140	3.82	5.15	4.92	4.67	4.88	4.80	8393.25	15.76	2498.21	16.36
25155	3.81	5.15	4.92	4.67	4.88	4.81	8391.53	15.76	2501.15	16.35
25170	3.81	5.15	4.92	4.67	4.88	4.82	8392.78	15.76	2504.45	16.35
25185	3.80	5.15	4.92	4.67	4.88	4.81	8391.05	15.76	2507.76	16.35
25200	3.81	5.15	4.92	4.68	4.88	4.82	8392.78	15.76	2511.07	16.35
25215	3.80	5.15	4.92	4.67	4.88	4.83	8392.78	15.76	2514.37	16.35
25230	3.80	5.15	4.94	4.68	4.88	4.83	8393.25	15.76	2518.06	16.36
25245	3.78	5.15	4.94	4.68	4.88	4.83	8392.78	15.76	2523.02	16.36
25260	3.79	5.16	4.94	4.68	4.90	4.84	8393.25	15.76	2526.32	16.36
25275	3.78	5.15	4.94	4.68	4.88	4.84	8392.78	15.76	2530.91	16.35
25290	3.77	5.15	4.94	4.68	4.88	4.84	8392.78	15.76	2534.59	16.36
25305	3.77	5.15	4.94	4.68	4.88	4.84	8391.53	15.76	2539.18	16.35
25320	3.78	5.15	4.94	4.68	4.90	4.84	8394.50	15.76	2544.52	16.36
25335	3.77	5.15	4.94	4.68	4.88	4.85	8391.53	15.76	2549.48	16.36
25350	3.77	5.15	4.94	4.67	4.90	4.85	8393.25	15.76	2554.06	16.35
25365	3.77	5.15	4.94	4.68	4.88	4.85	8391.53	15.76	2559.02	16.35
25380	3.76	5.15	4.94	4.68	4.90	4.85	8391.53	15.76	2563.98	16.35
25395	3.77	5.16	4.94	4.68	4.90	4.86	8391.53	15.76	2569.32	16.36
25410	3.78	5.16	4.94	4.68	4.90	4.87	8393.25	15.76	2574.29	16.36
25425	3.77	5.15	4.94	4.68	4.90	4.88	8391.53	15.76	2575.56	16.35
25440	3.76	5.16	4.94	4.68	4.90	4.88	8393.25	15.76	2575.94	16.36
25455	3.76	5.15	4.94	4.68	4.90	4.87	8392.00	15.77	2577.21	16.35
25470	3.76	5.16	4.94	4.68	4.90	4.88	8391.53	15.76	2580.52	16.35
25485	3.76	5.16	4.94	4.68	4.90	4.88	8393.25	15.76	2582.17	16.35
25500	3.76	5.16	4.95	4.68	4.90	4.89	8394.97	15.76	2583.83	16.35
25515	3.76	5.16	4.94	4.68	4.90	4.89	8393.25	15.76	2583.83	16.35
25530	3.75	5.16	4.95	4.70	4.90	4.89	8394.97	15.76	2588.79	16.35
25545	3.75	5.16	4.95	4.70	4.90	4.90	8393.25	15.76	2593.75	16.35
25560	3.75	5.16	4.94	4.70	4.90	4.90	8393.25	15.76	2597.05	16.35
25575	3.75	5.16	4.94	4.70	4.90	4.90	8392.78	15.76	2600.75	16.36
25590	3.75	5.16	4.94	4.68	4.90	4.90	8393.25	15.77	2605.32	16.35
25605	3.74	5.16	4.94	4.68	4.90	4.90	8392.78	15.76	2609.02	16.36
25620	3.74	5.16	4.95	4.70	4.90	4.90	8391.53	15.76	2613.98	16.36
25635	3.75	5.16	4.95	4.70	4.92	4.91	8392.78	15.76	2617.29	16.36
25650	3.74	5.16	4.94	4.70	4.90	4.90	8392.78	15.76	2620.21	16.35
25665	3.74	5.16	4.95	4.68	4.90	4.90	8393.25	15.76	2622.25	16.36
25680	3.74	5.16	4.94	4.68	4.90	4.90	8392.78	15.76	2625.17	16.35
25695	3.74	5.16	4.95	4.70	4.92	4.91	8391.53	15.76	2628.86	16.36
25710	3.75	5.16	4.95	4.70	4.90	4.91	8394.97	15.76	2630.52	16.36

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
25725	3.74	5.16	4.95	4.70	4.92	4.91	8393.25	15.76	2635.09	16.30
25740	3.74	5.16	4.94	4.70	4.90	4.91	8393.25	15.76	2638.79	16.30
25755	3.74	5.16	4.94	4.68	4.90	4.92	8393.25	15.76	2643.75	16.30
25770	3.75	5.18	4.95	4.70	4.92	4.92	8394.50	15.76	2645.01	16.30
25785	3.74	5.16	4.95	4.68	4.92	4.92	8393.25	15.76	2645.01	16.30
25800	3.74	5.16	4.95	4.70	4.92	4.92	8392.78	15.76	2645.40	16.30
25815	3.74	5.18	4.94	4.70	4.92	4.92	8391.53	15.76	2643.36	16.30
25830	3.74	5.18	4.95	4.70	4.92	4.92	8391.53	15.76	2643.36	16.30
25845	3.74	5.18	4.94	4.70	4.92	4.94	8393.25	15.76	2643.75	16.30
25860	3.75	5.18	4.95	4.70	4.92	4.93	8394.50	15.76	2643.36	16.30
25875	3.75	5.18	4.94	4.70	4.92	4.94	8393.25	15.76	2645.01	16.30
25890	3.75	5.18	4.95	4.70	4.92	4.94	8391.53	15.76	2647.06	16.30
25905	3.75	5.18	4.95	4.70	4.92	4.95	8391.53	15.76	2647.06	16.30
25920	3.75	5.18	4.95	4.70	4.92	4.96	8388.08	15.76	2648.32	16.30
25935	3.75	5.18	4.95	4.70	4.92	4.95	8388.08	15.76	2649.97	16.30
25950	3.75	5.18	4.95	4.70	4.92	4.96	8391.53	15.76	2650.36	16.30
25965	3.75	5.18	4.95	4.70	4.92	4.97	8391.53	15.76	2651.62	16.30
25980	3.75	5.18	4.95	4.70	4.92	4.97	8389.81	15.76	2652.02	16.30
25995	3.75	5.18	4.95	4.70	4.92	4.97	8389.81	15.76	2653.67	16.30
26010	3.75	5.18	4.95	4.70	4.92	4.97	8391.53	15.76	2653.28	16.30
26025	3.75	5.20	4.97	4.70	4.93	4.99	8393.25	15.76	2653.28	16.30
26040	3.75	5.20	4.95	4.70	4.92	4.99	8391.53	15.76	2654.93	16.30
26055	3.75	5.20	4.95	4.70	4.93	4.99	8391.53	15.76	2656.58	16.30
26070	3.75	5.20	4.95	4.70	4.93	4.99	8391.53	15.76	2656.58	16.30
26085	3.75	5.20	4.95	4.70	4.93	5.00	8391.53	15.76	2656.58	16.30
26100	3.76	5.20	4.95	4.70	4.93	5.01	8389.81	15.76	2654.93	16.30
26115	3.77	5.20	4.95	4.70	4.93	5.02	8393.25	15.76	2653.28	16.30
26130	3.79	5.20	4.95	4.70	4.93	5.03	8391.53	15.76	2649.97	16.30
26145	3.81	5.20	4.95	4.70	4.93	5.04	8393.25	15.76	2643.36	16.30
26160	3.82	5.21	4.95	4.70	4.95	5.04	8391.53	15.76	2636.74	16.30
26175	3.83	5.20	4.95	4.70	4.95	5.04	8391.53	15.76	2626.82	16.30
26190	3.92	5.21	4.95	4.71	4.95	5.05	8391.53	15.76	2610.28	16.30
26205	4.00	5.21	4.97	4.71	4.95	5.07	8391.53	15.77	2590.44	16.30
26220	4.07	5.23	4.97	4.71	4.95	5.08	8391.53	15.76	2573.90	16.30
26235	4.18	5.24	4.97	4.71	4.96	5.10	8391.53	15.77	2563.98	16.30
26250	4.28	5.24	4.99	4.73	4.96	5.11	8391.53	15.76	2557.37	16.30
26265	4.28	5.24	4.99	4.73	4.98	5.10	8391.53	15.76	2552.41	16.30
26280	4.25	5.24	4.99	4.73	4.96	5.09	8391.53	15.76	2545.79	16.30
26295	4.23	5.26	4.99	4.73	4.98	5.09	8389.81	15.76	2544.14	16.30
26310	4.22	5.26	4.99	4.73	4.98	5.10	8389.81	15.76	2542.49	16.30
26325	4.21	5.26	5.00	4.75	4.99	5.10	8389.81	15.76	2539.18	16.30
26340	4.17	5.26	5.00	4.75	4.99	5.10	8389.81	15.76	2537.52	16.30
26355	4.12	5.26	5.00	4.75	4.99	5.10	8388.08	15.76	2537.15	16.30
26370	4.08	5.27	5.00	4.75	5.01	5.10	8386.84	15.75	2540.83	16.30
26385	4.05	5.27	5.02	4.76	5.01	5.10	8389.81	15.76	2545.79	16.30
26400	4.03	5.27	5.02	4.76	5.01	5.11	8388.08	15.76	2550.75	16.30
26415	4.01	5.27	5.02	4.78	5.03	5.11	8388.56	15.77	2559.02	16.30
26430	3.97	5.27	5.02	4.76	5.01	5.10	8391.53	15.76	2580.52	16.30
26445	3.95	5.27	5.02	4.78	5.03	5.11	8388.56	15.77	2646.66	16.30

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
26460	3.94	5.29	5.03	4.78	5.03	5.10	8388.56	15.75	2688.00	16.35
26475	3.91	5.29	5.03	4.78	5.03	5.10	8389.81	15.76	2688.00	16.35
26490	3.90	5.29	5.03	4.78	5.03	5.09	8390.28	15.77	2683.04	16.35
26505	3.88	5.29	5.05	4.79	5.04	5.09	8393.25	15.76	2671.47	16.35
26520	3.87	5.29	5.05	4.79	5.04	5.08	8393.25	15.76	2666.51	16.35
26535	3.86	5.29	5.05	4.79	5.04	5.08	8393.25	15.76	2663.20	16.35
26550	3.83	5.29	5.03	4.78	5.04	5.07	8392.00	15.77	2676.03	16.34
26565	3.84	5.29	5.05	4.79	5.04	5.08	8393.25	15.76	2679.74	16.35
26580	3.83	5.29	5.05	4.79	5.04	5.08	8393.25	15.76	2684.70	16.34
26595	3.85	5.29	5.05	4.79	5.06	5.07	8392.00	15.77	2692.96	16.35
26610	3.85	5.29	5.05	4.79	5.06	5.08	8393.25	15.76	2696.27	16.34
26625	3.84	5.29	5.05	4.79	5.04	5.07	8392.00	15.75	2698.33	16.34
26640	3.83	5.29	5.05	4.79	5.06	5.06	8393.25	15.76	2696.27	16.35
26655	3.83	5.29	5.05	4.79	5.06	5.06	8393.25	15.76	2692.96	16.35
26670	3.82	5.31	5.05	4.81	5.06	5.05	8393.25	15.77	2684.70	16.35
26685	3.82	5.31	5.05	4.79	5.06	5.05	8392.00	15.75	2678.08	16.34
26700	3.83	5.31	5.06	4.81	5.06	5.06	8393.25	15.76	2671.47	16.34
26715	3.82	5.31	5.06	4.81	5.06	5.06	8392.00	15.75	2663.20	16.35
26730	3.81	5.32	5.06	4.81	5.06	5.06	8393.25	15.76	2657.84	16.34
26745	3.81	5.31	5.06	4.81	5.06	5.06	8393.25	15.77	2653.28	16.35
26760	3.80	5.32	5.06	4.81	5.06	5.06	8392.00	15.75	2648.32	16.34
26775	3.80	5.32	5.06	4.81	5.06	5.06	8393.25	15.76	2641.70	16.34
26790	3.79	5.32	5.06	4.81	5.06	5.05	8393.25	15.76	2638.40	16.34
26805	3.78	5.32	5.06	4.81	5.06	5.04	8393.25	15.76	2636.74	16.34
26820	3.77	5.32	5.06	4.81	5.06	5.03	8393.25	15.76	2636.74	16.34
26835	3.77	5.32	5.06	4.81	5.06	5.02	8393.25	15.76	2636.74	16.34
26850	3.77	5.32	5.06	4.81	5.04	5.02	8393.25	15.76	2633.43	16.34
26865	3.76	5.32	5.06	4.81	5.04	5.02	8393.25	15.76	2628.47	16.34
26880	3.76	5.32	5.06	4.81	5.06	5.01	8393.25	15.76	2626.82	16.34
26895	3.76	5.34	5.06	4.81	5.04	5.01	8393.25	15.76	2625.56	16.33
26910	3.76	5.34	5.06	4.81	5.04	5.00	8394.97	15.76	2621.86	16.34
26925	3.76	5.32	5.06	4.81	5.04	5.01	8394.97	15.77	2616.90	16.34
26940	3.76	5.34	5.06	4.81	5.06	5.00	8394.97	15.76	2613.59	16.34
26955	3.76	5.34	5.06	4.81	5.06	5.00	8394.97	15.76	2613.59	16.35
26970	3.76	5.34	5.06	4.81	5.06	5.01	8394.97	15.76	2610.28	16.34
26985	3.76	5.34	5.06	4.81	5.06	5.00	8394.97	15.76	2606.98	16.34
27000	3.76	5.34	5.06	4.81	5.06	5.00	8396.70	15.76	2606.98	16.34
27015	3.76	5.34	5.06	4.81	5.04	5.00	8394.97	15.76	2605.32	16.34
27030	3.75	5.34	5.06	4.81	5.04	4.99	8394.97	15.76	2603.67	16.34
27045	3.74	5.34	5.06	4.81	5.04	4.98	8396.70	15.76	2602.02	16.34
27060	3.74	5.34	5.06	4.81	5.04	4.97	8396.70	15.76	2598.71	16.34
27075	3.74	5.34	5.06	4.81	5.04	4.97	8396.70	15.76	2595.40	16.34
27090	3.74	5.32	5.06	4.81	5.04	4.96	8396.70	15.76	2592.09	16.34
27105	3.73	5.32	5.05	4.81	5.04	4.96	8394.97	15.76	2588.79	16.34
27120	3.74	5.34	5.05	4.81	5.04	4.95	8396.70	15.76	2585.48	16.34
27135	3.74	5.32	5.06	4.81	5.04	4.95	8396.70	15.76	2580.52	16.34
27150	3.73	5.32	5.05	4.79	5.04	4.94	8396.70	15.76	2578.87	16.34
27165	3.74	5.32	5.06	4.79	5.04	4.95	8394.97	15.76	2575.56	16.34
27180	3.74	5.32	5.05	4.79	5.04	4.94	8396.70	15.76	2572.25	16.35

**RAYMARK INDUSTRIES, INC.
STRATFORD, CONNECTICUT
RCRA SECTION 3013 ORDER
DOCKET NO. I-87-1057**

**TIDAL STUDY FIELD DATA
G CLUSTER WELLS**

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
27195	3.73	5.31	5.03	4.79	5.04	4.94	8396.70	15.76	2568.94	16.35
27210	3.74	5.31	5.05	4.79	5.04	4.95	8393.73	15.75	2567.29	16.34
27225	3.73	5.31	5.03	4.78	5.04	4.94	8394.97	15.76	2565.64	16.34
27240	3.74	5.31	5.03	4.78	5.04	4.94	8394.97	15.76	2567.29	16.34
27255	3.75	5.31	5.05	4.79	5.06	4.95	8394.97	15.76	2565.64	16.35
27270	3.74	5.31	5.03	4.79	5.04	4.94	8393.73	15.75	2561.06	16.33
27285	3.74	5.31	5.03	4.78	5.04	4.94	8396.70	15.77	2560.30	16.34
27300	3.75	5.31	5.03	4.79	5.06	4.95	8393.73	15.77	2560.30	16.35
27315	3.73	5.29	5.02	4.78	5.04	4.93	8393.73	15.75	2558.64	16.35
27330	3.74	5.29	5.03	4.78	5.04	4.94	8395.45	15.75	2554.06	16.33
27345	3.74	5.29	5.03	4.76	5.04	4.93	8393.73	15.77	2552.03	16.35
27360	3.76	5.31	5.03	4.78	5.06	4.95	8393.73	15.75	2552.03	16.35
27375	3.73	5.27	5.02	4.76	5.04	4.92	8392.00	15.77	2552.03	16.35
27390	3.73	5.27	5.02	4.76	5.04	4.93	8395.45	15.77	2550.75	16.34
27405	3.74	5.27	5.02	4.76	5.06	4.94	8393.73	15.77	2552.03	16.35
27420	3.74	5.27	5.02	4.76	5.04	4.93	8392.48	15.76	2547.45	16.34
27435	3.73	5.26	5.00	4.75	5.04	4.92	8393.73	15.75	2545.41	16.35
27450	3.75	5.26	5.00	4.75	5.06	4.94	8393.25	15.76	2545.79	16.34
27465	3.74	5.24	4.97	4.73	5.06	4.94	8393.73	15.75	2543.76	16.34
27480	3.74	5.23	4.97	4.71	5.06	4.94	8393.73	15.75	2545.41	16.34
27495	3.75	5.24	5.00	4.75	5.07	4.94	8394.20	15.76	2545.04	16.33
27510	3.74	5.24	4.99	4.75	5.07	4.94	8395.92	15.76	2543.76	16.34
27525	3.74	5.24	4.99	4.75	5.07	4.94	8394.20	15.76	2543.76	16.34
27540	3.74	5.24	5.00	4.75	5.06	4.94	8394.20	15.76	2543.76	16.34
27555	3.75	5.26	5.00	4.75	5.07	4.95	8394.20	15.76	2543.76	16.35
27570	3.74	5.24	5.00	4.75	5.06	4.94	8394.20	15.76	2543.76	16.34
27585	3.74	5.24	5.00	4.75	5.06	4.94	8394.20	15.76	2543.76	16.34
27600	3.74	5.24	5.00	4.75	5.07	4.94	8394.20	15.76	2542.11	16.34
27615	3.74	5.24	5.00	4.76	5.06	4.95	8394.20	15.76	2541.73	16.33
27630	3.74	5.23	5.00	4.75	5.06	4.94	8394.20	15.76	2538.80	16.34
27645	3.74	5.23	4.99	4.75	5.06	4.94	8394.20	15.76	2536.77	16.33
27660	3.74	5.23	4.99	4.75	5.06	4.94	8394.20	15.76	2535.49	16.35
27675	3.74	5.23	5.00	4.75	5.06	4.94	8394.20	15.76	2537.15	16.34
27690	3.74	5.23	5.00	4.75	5.07	4.94	8394.20	15.76	2535.12	16.33
27705	3.74	5.23	5.00	4.75	5.06	4.94	8394.20	15.76	2533.84	16.34
27720	3.73	5.23	4.99	4.75	5.06	4.94	8394.20	15.76	2530.53	16.35
27735	3.73	5.23	5.00	4.75	5.06	4.93	8393.73	15.75	2531.81	16.34
27750	3.73	5.21	5.00	4.75	5.06	4.93	8394.20	15.76	2533.47	16.34
27765	3.73	5.21	5.00	4.75	5.06	4.93	8394.20	15.76	2532.19	16.34
27780	3.73	5.21	5.00	4.75	5.06	4.93	8394.20	15.76	2531.81	16.34
27795	3.73	5.21	5.00	4.75	5.06	4.92	8393.73	15.75	2527.23	16.34
27810	3.73	5.21	5.00	4.75	5.04	4.92	8393.73	15.75	2528.51	16.34
27825	3.73	5.21	5.00	4.75	5.04	4.92	8395.45	15.77	2525.20	16.34
27840	3.72	5.21	5.00	4.75	5.06	4.92	8395.45	15.77	2520.61	16.34
27855	3.72	5.21	5.00	4.75	5.04	4.91	8394.20	15.76	2520.61	16.34
27870	3.72	5.21	5.00	4.75	5.04	4.90	8395.45	15.75	2522.27	16.35
27885	3.72	5.21	5.00	4.75	5.04	4.90	8393.73	15.75	2522.27	16.35
27900	3.72	5.21	5.00	4.76	5.04	4.90	8396.70	15.76	2520.61	16.35
27915	3.71	5.21	5.02	4.76	5.03	4.89	8393.73	15.75	2520.61	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
27930	3.71	5.21	5.02	4.76	5.03	4.89	8393.73	15.75	2518.96	16.34
27945	3.71	5.21	5.02	4.76	5.03	4.88	8393.73	15.75	2515.65	16.34
27960	3.71	5.21	5.02	4.76	5.03	4.87	8394.97	15.76	2515.65	16.34
27975	3.72	5.21	5.02	4.76	5.03	4.88	8394.97	15.76	2512.72	16.34
27990	3.71	5.21	5.02	4.76	5.03	4.87	8394.97	15.76	2512.35	16.34
28005	3.71	5.20	5.02	4.76	5.03	4.87	8394.97	15.76	2512.72	16.34
28020	3.72	5.21	5.02	4.76	5.01	4.87	8394.97	15.76	2512.72	16.34
28035	3.71	5.20	5.02	4.76	5.01	4.87	8394.97	15.76	2511.07	16.34
28050	3.72	5.20	5.02	4.76	5.01	4.87	8394.97	15.76	2511.07	16.34
28065	3.72	5.20	5.02	4.76	5.01	4.86	8394.97	15.76	2509.41	16.34
28080	3.72	5.20	5.02	4.78	5.01	4.87	8394.97	15.76	2506.11	16.34
28095	3.72	5.20	5.02	4.76	5.01	4.86	8393.25	15.76	2506.11	16.34
28110	3.72	5.20	5.02	4.76	5.01	4.86	8394.97	15.76	2506.11	16.34
28125	3.71	5.20	5.02	4.78	5.01	4.86	8394.97	15.76	2507.76	16.34
28140	3.72	5.20	5.02	4.76	5.01	4.86	8393.25	15.76	2507.76	16.34
28155	3.71	5.20	5.02	4.78	5.01	4.85	8394.50	15.76	2507.76	16.34
28170	3.72	5.20	5.02	4.76	5.01	4.86	8395.45	15.77	2506.11	16.34
28185	3.72	5.20	5.02	4.78	5.01	4.86	8393.25	15.76	2504.45	16.34
28200	3.72	5.20	5.02	4.78	5.01	4.86	8393.25	15.76	2502.80	16.34
28215	3.72	5.20	5.02	4.76	5.01	4.86	8394.97	15.76	2502.80	16.34
28230	3.72	5.20	5.02	4.78	5.01	4.87	8394.97	15.76	2502.80	16.34
28245	3.72	5.20	5.02	4.78	5.01	4.87	8393.25	15.76	2502.80	16.34
28260	3.72	5.18	5.02	4.78	5.01	4.87	8393.73	15.77	2502.80	16.34
28275	3.72	5.18	5.02	4.78	5.01	4.86	8393.25	15.76	2504.45	16.34
28290	3.72	5.18	5.02	4.78	5.01	4.87	8396.70	15.77	2506.11	16.34
28305	3.72	5.18	5.02	4.78	5.01	4.87	8394.97	15.76	2504.45	16.34
28320	3.72	5.18	5.02	4.78	5.01	4.86	8393.25	15.76	2502.80	16.34
28335	3.72	5.18	5.02	4.78	4.99	4.87	8393.73	15.77	2502.80	16.34
28350	3.71	5.18	5.02	4.78	4.99	4.87	8393.25	15.76	2504.45	16.34
28365	3.72	5.18	5.03	4.78	5.01	4.86	8393.25	15.76	2504.45	16.34
28380	3.72	5.18	5.02	4.78	5.01	4.87	8394.50	15.76	2504.45	16.34
28395	3.72	5.18	5.02	4.78	5.01	4.87	8393.25	15.76	2501.15	16.34
28410	3.72	5.18	5.02	4.78	5.01	4.87	8393.73	15.75	2497.84	16.34
28425	3.71	5.18	5.02	4.78	4.99	4.87	8393.73	15.77	2497.84	16.34
28440	3.72	5.18	5.02	4.78	4.99	4.86	8393.25	15.76	2501.15	16.34
28455	3.71	5.16	5.02	4.78	4.99	4.86	8393.25	15.76	2501.15	16.34
28470	3.71	5.16	5.02	4.78	4.99	4.85	8394.50	15.76	2502.80	16.34
28485	3.71	5.16	5.02	4.78	4.99	4.85	8394.50	15.75	2506.11	16.34
28500	3.71	5.16	5.02	4.76	4.99	4.85	8394.50	15.76	2509.79	16.34
28515	3.70	5.16	5.02	4.76	4.99	4.84	8394.50	15.76	2507.76	16.34
28530	3.70	5.16	5.02	4.76	4.99	4.84	8394.50	15.76	2508.13	16.34
28545	3.70	5.16	5.02	4.76	4.99	4.84	8394.50	15.76	2507.76	16.34
28560	3.70	5.15	5.02	4.76	4.98	4.83	8394.50	15.76	2506.11	16.34
28575	3.70	5.15	5.00	4.76	4.99	4.83	8393.25	15.76	2504.45	16.34
28590	3.71	5.15	5.00	4.76	4.99	4.83	8394.50	15.76	2504.45	16.34
28605	3.71	5.15	5.00	4.76	4.98	4.84	8394.50	15.76	2502.80	16.34
28620	3.71	5.13	5.00	4.75	4.99	4.83	8394.97	15.76	2501.15	16.34
28635	3.71	5.13	4.99	4.75	4.99	4.83	8394.97	15.76	2499.49	16.34
28650	3.71	5.13	4.99	4.73	4.99	4.83	8393.25	15.76	2497.84	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
28665	3.71	5.13	4.99	4.75	4.99	4.83	8394.97	15.76	2496.18	16.34
28680	3.71	5.12	4.99	4.73	4.99	4.83	8394.97	15.76	2494.16	16.34
28695	3.70	5.12	4.97	4.73	4.99	4.82	8394.97	15.76	2492.51	16.35
28710	3.70	5.12	4.97	4.71	4.99	4.82	8393.73	15.75	2494.16	16.34
28725	3.71	5.12	4.95	4.73	4.99	4.82	8393.73	15.75	2492.51	16.35
28740	3.71	5.10	4.95	4.71	5.01	4.83	8393.73	15.75	2490.85	16.35
28755	3.72	5.10	4.97	4.71	5.01	4.84	8392.00	15.77	2489.20	16.35
28770	3.71	5.10	4.95	4.71	5.01	4.83	8392.00	15.75	2488.83	16.34
28785	3.71	5.10	4.95	4.71	5.01	4.82	8392.00	15.75	2489.20	16.35
28800	3.72	5.10	4.95	4.71	5.01	4.83	8392.00	15.77	2487.55	16.35
28815	3.72	5.08	4.95	4.71	5.01	4.83	8392.00	15.75	2487.55	16.35
28830	3.72	5.08	4.95	4.71	5.01	4.83	8392.00	15.77	2487.55	16.35
28845	3.73	5.08	4.95	4.71	5.01	4.84	8392.48	15.76	2484.24	16.34
28860	3.73	5.08	4.95	4.71	5.03	4.85	8390.76	15.76	2485.52	16.35
28875	3.72	5.08	4.95	4.70	5.03	4.85	8392.48	15.76	2485.52	16.35
28890	3.72	5.08	4.94	4.70	5.01	4.85	8390.76	15.76	2482.59	16.34
28905	3.72	5.08	4.95	4.70	5.03	4.85	8390.76	15.76	2480.93	16.34
28920	3.72	5.07	4.94	4.68	5.03	4.85	8390.76	15.76	2480.57	16.33
28935	3.73	5.07	4.94	4.70	5.03	4.86	8392.48	15.76	2482.59	16.35
28950	3.72	5.07	4.94	4.68	5.03	4.86	8391.23	15.77	2482.59	16.35
28965	3.73	5.07	4.94	4.70	5.03	4.87	8391.23	15.76	2482.22	16.34
28980	3.73	5.07	4.94	4.70	5.03	4.87	8391.23	15.76	2482.22	16.34
28995	3.73	5.07	4.94	4.70	5.04	4.88	8390.76	15.75	2482.22	16.34
29010	3.73	5.07	4.94	4.70	5.04	4.88	8391.23	15.77	2478.91	16.34
29025	3.73	5.05	4.94	4.70	5.04	4.88	8390.76	15.75	2478.91	16.34
29040	3.73	5.07	4.94	4.68	5.04	4.88	8390.76	15.76	2482.22	16.34
29055	3.73	5.07	4.94	4.70	5.04	4.89	8391.23	15.76	2480.20	16.34
29070	3.73	5.05	4.94	4.68	5.04	4.89	8391.23	15.77	2482.22	16.34
29085	3.73	5.05	4.94	4.70	5.04	4.90	8391.23	15.77	2480.57	16.34
29100	3.72	5.05	4.94	4.68	5.04	4.90	8391.23	15.77	2482.22	16.34
29115	3.72	5.05	4.94	4.68	5.04	4.90	8391.23	15.77	2480.20	16.34
29130	3.72	5.05	4.94	4.68	5.04	4.89	8392.48	15.76	2478.54	16.34
29145	3.72	5.05	4.94	4.68	5.04	4.89	8390.76	15.76	2477.26	16.34
29160	3.72	5.05	4.94	4.68	5.04	4.89	8389.99	15.77	2475.61	16.34
29175	3.72	5.05	4.94	4.68	5.04	4.89	8391.23	15.77	2473.95	16.34
29190	3.72	5.05	4.94	4.70	5.04	4.89	8390.76	15.76	2472.30	16.34
29205	3.72	5.05	4.94	4.68	5.03	4.89	8390.76	15.76	2470.65	16.34
29220	3.72	5.05	4.94	4.68	5.03	4.89	8390.76	15.76	2468.99	16.34
29235	3.72	5.05	4.94	4.70	5.04	4.90	8391.23	15.76	2465.69	16.34
29250	3.72	5.05	4.94	4.70	5.03	4.90	8394.20	15.76	2464.03	16.34
29265	3.72	5.07	4.95	4.70	5.03	4.90	8392.48	15.76	2460.73	16.34
29280	3.72	5.07	4.95	4.71	5.03	4.90	8392.48	15.76	2460.73	16.35
29295	3.72	5.07	4.95	4.71	5.03	4.90	8392.48	15.76	2457.79	16.34
29310	3.72	5.07	4.97	4.71	5.01	4.89	8392.00	15.77	2459.07	16.34
29325	3.72	5.08	4.95	4.71	5.01	4.89	8393.73	15.77	2457.79	16.35
29340	3.72	5.07	4.97	4.73	5.01	4.89	8392.00	15.75	2456.13	16.35
29355	3.71	5.07	4.97	4.71	5.01	4.89	8392.00	15.77	2456.13	16.35
29370	3.71	5.08	4.97	4.73	4.99	4.89	8392.00	15.75	2456.13	16.35
29385	3.71	5.07	4.99	4.73	4.99	4.89	8393.25	15.76	2456.13	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
29400	3.71	5.08	4.97	4.73	4.99	4.89	8391.53	15.76	2454.48	16.3
29415	3.71	5.07	4.99	4.73	4.99	4.88	8391.53	15.76	2452.83	16.3
29430	3.71	5.08	4.99	4.73	4.99	4.88	8391.53	15.76	2452.83	16.3
29445	3.71	5.08	4.99	4.73	4.99	4.88	8393.25	15.76	2451.17	16.3
29460	3.72	5.08	4.99	4.73	4.99	4.88	8391.53	15.76	2449.88	16.3
29475	3.72	5.08	4.99	4.73	4.99	4.89	8391.53	15.76	2449.52	16.3
29490	3.72	5.08	4.99	4.75	4.99	4.90	8391.53	15.76	2448.23	16.3
29505	3.72	5.08	4.99	4.73	4.99	4.90	8391.53	15.76	2446.58	16.3
29520	3.72	5.08	4.99	4.75	4.98	4.90	8391.53	15.76	2446.58	16.3
29535	3.72	5.08	4.99	4.75	4.98	4.89	8391.53	15.76	2446.21	16.3
29550	3.71	5.08	4.99	4.75	4.98	4.89	8391.53	15.76	2446.58	16.3
29565	3.72	5.08	4.99	4.75	4.98	4.89	8391.53	15.76	2446.58	16.3
29580	3.72	5.08	4.99	4.75	4.99	4.90	8391.53	15.76	2444.92	16.3
29595	3.72	5.10	4.99	4.75	4.99	4.90	8391.53	15.76	2443.27	16.3
29610	3.73	5.10	5.00	4.75	4.98	4.91	8392.00	15.77	2441.62	16.3
29625	3.73	5.10	5.00	4.75	4.99	4.92	8391.53	15.76	2441.62	16.3
29640	3.73	5.10	5.00	4.75	4.99	4.92	8391.53	15.76	2443.27	16.3
29655	3.74	5.10	5.00	4.75	4.99	4.94	8389.81	15.76	2446.58	16.3
29670	3.73	5.10	5.00	4.76	4.99	4.94	8392.00	15.77	2449.88	16.3
29685	3.73	5.10	5.00	4.76	4.99	4.94	8389.81	15.76	2453.19	16.3
29700	3.73	5.10	5.00	4.76	4.99	4.94	8391.53	15.76	2456.50	16.3
29715	3.72	5.10	5.00	4.76	4.98	4.94	8389.81	15.76	2459.81	16.3
29730	3.73	5.10	5.00	4.75	4.99	4.95	8391.05	15.76	2461.46	16.3
29745	3.73	5.10	5.00	4.75	4.99	4.95	8389.81	15.76	2463.11	16.3
29760	3.73	5.10	5.00	4.75	4.99	4.95	8389.81	15.76	2463.11	16.3
29775	3.73	5.10	5.00	4.75	4.99	4.95	8389.81	15.76	2463.11	16.3
29790	3.73	5.10	4.99	4.75	4.99	4.96	8389.81	15.76	2461.46	16.3
29805	3.73	5.10	5.00	4.75	4.99	4.96	8389.81	15.76	2461.46	16.3
29820	3.73	5.10	5.00	4.75	4.99	4.97	8389.81	15.76	2459.81	16.3
29835	3.74	5.10	4.99	4.75	4.99	4.97	8389.81	15.76	2459.81	16.3
29850	3.73	5.08	4.99	4.75	4.99	4.97	8389.81	15.76	2458.15	16.3
29865	3.74	5.10	5.00	4.75	4.99	4.98	8389.81	15.76	2459.81	16.3
29880	3.73	5.10	4.99	4.75	4.99	4.98	8391.05	15.76	2463.11	16.3
29895	3.73	5.10	5.00	4.75	4.99	4.98	8388.56	15.77	2462.75	16.3
29910	3.73	5.10	4.99	4.75	4.99	4.98	8388.08	15.76	2463.11	16.3
29925	3.73	5.10	4.99	4.75	4.99	4.99	8389.81	15.76	2464.77	16.3
29940	3.73	5.10	4.99	4.75	4.99	5.00	8389.81	15.76	2466.42	16.3
29955	3.73	5.10	4.99	4.75	4.99	4.99	8388.08	15.76	2464.77	16.3
29970	3.73	5.10	5.00	4.75	4.99	5.00	8388.08	15.76	2462.75	16.3
29985	3.73	5.10	4.99	4.75	4.99	4.99	8388.08	15.76	2461.46	16.3
30000	3.73	5.10	4.99	4.75	4.99	5.00	8388.08	15.76	2461.46	16.3
30015	3.73	5.08	4.99	4.75	4.99	5.00	8388.08	15.76	2461.09	16.3
30030	3.74	5.08	4.99	4.75	4.99	5.01	8388.08	15.76	2463.11	16.3
30045	3.74	5.10	4.99	4.75	5.01	5.01	8388.08	15.76	2466.42	16.3
30060	3.74	5.10	4.99	4.75	5.01	5.02	8388.08	15.76	2469.36	16.3
30075	3.75	5.10	5.00	4.75	5.01	5.03	8385.12	15.75	2469.36	16.3
30090	3.75	5.10	4.99	4.75	5.01	5.03	8386.36	15.76	2471.01	16.3
30105	3.75	5.10	4.99	4.75	5.01	5.04	8385.12	15.75	2471.01	16.3
30120	3.74	5.10	4.99	4.73	5.01	5.04	8386.36	15.77	2471.01	16.3

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
30135	3.75	5.10	4.99	4.75	5.01	5.05	8386.36	15.76	2471.01	16.35
30150	3.75	5.10	4.99	4.75	5.01	5.05	8386.36	15.76	2472.67	16.35
30165	3.76	5.10	5.00	4.75	5.01	5.07	8386.36	15.76	2472.67	16.35
30180	3.82	5.10	5.00	4.76	5.03	5.09	8384.64	15.76	2471.01	16.35
30195	4.07	5.13	5.00	4.76	5.03	5.10	8386.36	15.76	2457.79	16.35
30210	4.08	5.12	5.00	4.76	5.03	5.11	8386.36	15.76	2442.91	16.35
30225	4.07	5.12	5.00	4.75	5.03	5.09	8384.64	15.76	2431.33	16.35
30240	4.09	5.12	5.00	4.75	5.03	5.08	8385.12	15.75	2414.80	16.35
30255	4.12	5.12	5.00	4.75	5.03	5.06	8384.64	15.77	2393.66	16.35
30270	4.13	5.12	5.00	4.76	5.03	5.05	8384.64	15.76	2375.12	16.35
30285	4.12	5.13	5.00	4.76	5.03	5.04	8384.64	15.76	2367.20	16.35
30300	4.08	5.13	5.02	4.76	5.03	5.04	8384.64	15.76	2356.93	16.35
30315	4.04	5.13	5.02	4.76	5.04	5.04	8384.64	15.76	2347.36	16.35
30330	4.02	5.13	5.02	4.78	5.04	5.05	8384.64	15.76	2340.74	16.35
30345	3.99	5.13	5.02	4.78	5.04	5.05	8384.64	15.76	2337.09	16.35
30360	3.97	5.15	5.03	4.78	5.04	5.08	8384.64	15.76	2340.40	16.35
30375	3.93	5.15	5.03	4.78	5.06	5.06	8383.39	15.75	2347.01	16.35
30390	3.91	5.15	5.03	4.79	5.06	5.06	8384.64	15.76	2360.24	16.35
30405	3.88	5.13	5.03	4.78	5.06	5.04	8383.39	15.75	2401.57	16.35
30420	3.86	5.13	5.03	4.79	5.06	5.04	8383.39	15.75	2436.29	16.35
30435	3.85	5.15	5.03	4.79	5.06	5.03	8384.64	15.76	2447.87	16.35
30450	3.84	5.15	5.03	4.79	5.06	5.03	8383.39	15.75	2447.87	16.35
30465	3.83	5.15	5.03	4.79	5.06	5.02	8384.64	15.76	2449.88	16.35
30480	3.82	5.15	5.05	4.79	5.06	5.02	8384.64	15.76	2454.48	16.35
30495	3.82	5.15	5.05	4.81	5.06	5.03	8386.36	15.76	2487.92	16.34
30510	3.82	5.16	5.05	4.81	5.07	5.04	8386.36	15.76	2527.23	16.35
30525	3.79	5.13	5.03	4.79	5.06	5.02	8386.36	15.76	2547.07	16.34
30540	3.79	5.15	5.05	4.81	5.07	5.02	8386.36	15.76	2558.64	16.34
30555	3.79	5.15	5.05	4.79	5.07	5.03	8385.12	15.75	2565.26	16.35
30570	3.78	5.15	5.03	4.79	5.07	5.03	8385.12	15.77	2561.95	16.34
30585	3.77	5.15	5.03	4.79	5.07	5.03	8385.12	15.75	2556.99	16.34
30600	3.77	5.15	5.03	4.79	5.07	5.03	8386.84	15.77	2553.68	16.35
30615	3.77	5.15	5.03	4.79	5.09	5.03	8385.59	15.76	2550.37	16.35
30630	3.77	5.13	5.03	4.79	5.09	5.03	8386.84	15.77	2545.41	16.34
30645	3.76	5.15	5.03	4.79	5.09	5.02	8386.84	15.77	2540.45	16.35
30660	3.75	5.13	5.03	4.79	5.07	5.02	8386.84	15.75	2537.52	16.34
30675	3.75	5.13	5.03	4.79	5.07	5.02	8386.84	15.77	2533.84	16.35
30690	3.75	5.13	5.03	4.79	5.09	5.02	8385.59	15.75	2534.22	16.34
30705	3.74	5.13	5.03	4.78	5.07	5.01	8385.59	15.76	2535.87	16.34
30720	3.74	5.13	5.03	4.79	5.07	5.00	8386.84	15.77	2539.18	16.34
30735	3.74	5.13	5.03	4.79	5.07	5.00	8386.84	15.75	2543.76	16.35
30750	3.74	5.13	5.03	4.79	5.07	5.00	8386.84	15.75	2535.49	16.35
30765	3.73	5.15	5.03	4.79	5.07	4.99	8386.84	15.75	2532.19	16.34
30780	3.73	5.15	5.03	4.79	5.07	4.98	8385.12	15.75	2530.53	16.34
30795	3.73	5.13	5.03	4.79	5.06	4.98	8386.36	15.76	2527.23	16.35
30810	3.72	5.15	5.05	4.79	5.07	4.98	8388.08	15.76	2525.57	16.35
30825	3.73	5.15	5.05	4.79	5.06	4.97	8386.36	15.76	2522.27	16.34
30840	3.73	5.15	5.05	4.81	5.06	4.97	8388.08	15.76	2518.96	16.34
30855	3.73	5.15	5.05	4.81	5.06	4.97	8388.08	15.76	2518.96	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
30870	3.72	5.15	5.03	4.79	5.06	4.97	8388.08	15.76	2520.99	16.34
30885	3.72	5.15	5.05	4.79	5.06	4.96	8388.08	15.76	2522.64	16.34
30900	3.72	5.15	5.05	4.81	5.06	4.96	8386.84	15.75	2522.64	16.34
30915	3.73	5.15	5.05	4.81	5.06	4.97	8386.36	15.76	2520.99	16.34
30930	3.72	5.15	5.05	4.81	5.06	4.96	8386.36	15.76	2519.34	16.34
30945	3.72	5.15	5.05	4.79	5.06	4.96	8386.36	15.76	2519.34	16.34
30960	3.72	5.15	5.05	4.79	5.06	4.96	8386.36	15.76	2516.03	16.34
30975	3.72	5.15	5.05	4.79	5.06	4.96	8386.36	15.76	2512.72	16.34
30990	3.72	5.15	5.05	4.81	5.06	4.96	8386.36	15.76	2512.72	16.34
31005	3.72	5.15	5.05	4.79	5.06	4.95	8386.36	15.76	2514.37	16.34
31020	3.72	5.15	5.05	4.81	5.06	4.95	8386.36	15.76	2512.72	16.34
31035	3.72	5.13	5.05	4.79	5.06	4.95	8386.36	15.76	2511.07	16.34
31050	3.72	5.13	5.05	4.79	5.06	4.95	8386.36	15.76	2509.41	16.34
31065	3.72	5.15	5.05	4.79	5.04	4.95	8386.36	15.76	2509.41	16.34
31080	3.72	5.15	5.05	4.81	5.06	4.95	8388.08	15.76	2506.11	16.34
31095	3.71	5.15	5.05	4.79	5.04	4.94	8386.36	15.76	2502.80	16.34
31110	3.72	5.15	5.05	4.79	5.04	4.94	8386.36	15.76	2502.80	16.34
31125	3.72	5.13	5.05	4.81	5.04	4.94	8386.84	15.77	2501.15	16.34
31140	3.71	5.13	5.05	4.79	5.04	4.94	8386.36	15.76	2499.49	16.34
31155	3.71	5.13	5.05	4.79	5.04	4.94	8386.36	15.76	2497.84	16.34
31170	3.71	5.15	5.05	4.79	5.04	4.94	8388.08	15.76	2501.15	16.34
31185	3.71	5.13	5.05	4.79	5.04	4.94	8386.36	15.76	2501.15	16.34
31200	3.71	5.13	5.05	4.79	5.04	4.94	8386.84	15.77	2501.15	16.34
31215	3.71	5.13	5.05	4.79	5.04	4.93	8386.36	15.76	2502.80	16.34
31230	3.71	5.13	5.05	4.79	5.04	4.93	8386.36	15.76	2502.80	16.34
31245	3.71	5.13	5.05	4.79	5.04	4.93	8387.61	15.76	2506.11	16.34
31260	3.71	5.13	5.03	4.81	5.04	4.92	8386.36	15.76	2502.80	16.34
31275	3.71	5.13	5.05	4.79	5.04	4.92	8386.36	15.76	2501.15	16.34
31290	3.71	5.13	5.05	4.79	5.04	4.92	8388.08	15.77	2499.49	16.34
31305	3.71	5.13	5.05	4.79	5.03	4.92	8386.36	15.76	2501.15	16.34
31320	3.71	5.13	5.05	4.79	5.04	4.92	8386.36	15.76	2502.80	16.34
31335	3.71	5.13	5.05	4.79	5.03	4.92	8386.36	15.76	2502.80	16.34
31350	3.71	5.13	5.05	4.79	5.03	4.92	8386.84	15.77	2497.84	16.34
31365	3.71	5.13	5.05	4.79	5.04	4.92	8386.36	15.76	2496.18	16.34
31380	3.71	5.13	5.05	4.81	5.03	4.92	8388.08	15.77	2492.88	16.34
31395	3.70	5.13	5.05	4.79	5.03	4.92	8386.36	15.76	2491.59	16.34
31410	3.70	5.13	5.05	4.79	5.03	4.92	8387.61	15.76	2492.88	16.34
31425	3.70	5.13	5.03	4.79	5.03	4.91	8387.61	15.76	2499.49	16.34
31440	3.70	5.13	5.03	4.79	5.03	4.91	8388.08	15.77	2502.80	16.34
31455	3.71	5.13	5.03	4.79	5.03	4.91	8387.61	15.76	2506.11	16.34
31470	3.71	5.13	5.03	4.79	5.03	4.92	8386.84	15.77	2509.41	16.34
31485	3.70	5.12	5.03	4.79	5.03	4.91	8387.61	15.76	2511.07	16.34
31500	3.70	5.13	5.03	4.79	5.03	4.91	8386.36	15.76	2511.07	16.34
31515	3.70	5.13	5.03	4.79	5.03	4.91	8386.36	15.76	2511.07	16.34
31530	3.71	5.12	5.03	4.78	5.03	4.91	8386.36	15.76	2512.72	16.34
31545	3.71	5.12	5.03	4.78	5.03	4.91	8388.08	15.77	2514.37	16.34
31560	3.71	5.12	5.02	4.78	5.03	4.91	8386.36	15.76	2514.37	16.34
31575	3.72	5.13	5.02	4.78	5.03	4.92	8386.36	15.76	2516.03	16.34
31590	3.71	5.12	5.02	4.78	5.03	4.92	8386.36	15.76	2516.03	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
31605	3.72	5.12	5.02	4.78	5.03	4.92	8386.36	15.76	2517.68	16.34
31620	3.71	5.10	5.02	4.78	5.03	4.92	8386.36	15.76	2517.31	16.34
31635	3.72	5.12	5.02	4.78	5.04	4.93	8386.36	15.76	2519.34	16.34
31650	3.71	5.10	5.02	4.78	5.03	4.92	8386.36	15.76	2517.31	16.35
31665	3.73	5.12	5.02	4.78	5.04	4.94	8386.36	15.76	2517.68	16.35
31680	3.73	5.10	5.02	4.78	5.04	4.93	8386.36	15.76	2516.03	16.34
31695	3.74	5.12	5.02	4.78	5.04	4.96	8385.12	15.75	2518.96	16.34
31710	3.72	5.10	5.00	4.78	5.04	4.93	8386.36	15.76	2518.96	16.34
31725	3.72	5.10	5.02	4.78	5.04	4.94	8386.36	15.76	2517.68	16.34
31740	3.74	5.12	5.02	4.78	5.06	4.96	8386.36	15.76	2520.61	16.35
31755	3.73	5.10	5.00	4.76	5.04	4.94	8385.12	15.75	2520.99	16.34
31770	3.74	5.12	5.02	4.78	5.06	4.96	8385.12	15.75	2520.61	16.35
31785	3.75	5.12	5.02	4.78	5.06	4.97	8385.12	15.75	2520.61	16.35
31800	3.73	5.10	5.02	4.76	5.04	4.96	8385.12	15.75	2520.61	16.35
31815	3.71	5.10	5.00	4.76	5.04	4.94	8386.36	15.77	2522.27	16.35
31830	3.73	5.10	5.02	4.76	5.06	4.96	8386.36	15.77	2525.57	16.35
31845	3.71	5.10	5.00	4.76	5.04	4.95	8385.12	15.75	2523.92	16.34
31860	3.72	5.10	5.02	4.76	5.04	4.96	8385.12	15.75	2522.27	16.35
31875	3.72	5.10	5.00	4.76	5.06	4.96	8385.12	15.75	2518.96	16.35
31890	3.71	5.10	5.00	4.76	5.04	4.95	8385.12	15.77	2516.03	16.34
31905	3.72	5.10	5.00	4.76	5.04	4.95	8385.12	15.75	2517.31	16.35
31920	3.73	5.10	5.00	4.76	5.04	4.96	8385.12	15.75	2520.61	16.35
31935	3.72	5.10	5.00	4.76	5.04	4.96	8385.12	15.75	2522.27	16.35
31950	3.72	5.10	5.00	4.76	5.04	4.95	8386.36	15.76	2520.61	16.35
31965	3.72	5.10	5.00	4.78	5.04	4.95	8385.12	15.77	2520.61	16.34
31980	3.72	5.10	5.00	4.76	5.04	4.96	8385.12	15.75	2518.96	16.35
31995	3.73	5.10	5.00	4.76	5.04	4.96	8385.12	15.77	2517.31	16.35
32010	3.72	5.10	5.00	4.76	5.04	4.96	8385.12	15.75	2514.37	16.34
32025	3.72	5.08	5.00	4.76	5.04	4.96	8385.12	15.75	2514.00	16.35
32040	3.72	5.08	5.00	4.76	5.04	4.96	8385.12	15.77	2517.31	16.35
32055	3.72	5.08	5.00	4.76	5.04	4.96	8385.12	15.77	2520.61	16.35
32070	3.71	5.08	4.99	4.76	5.04	4.96	8385.12	15.75	2517.31	16.35
32085	3.71	5.08	5.00	4.75	5.04	4.95	8383.87	15.75	2516.93	16.34
32100	3.71	5.08	5.00	4.76	5.04	4.95	8385.12	15.77	2517.68	16.34
32115	3.71	5.08	4.99	4.75	5.04	4.95	8385.12	15.75	2517.68	16.34
32130	3.71	5.08	4.99	4.75	5.04	4.95	8385.12	15.77	2514.37	16.34
32145	3.71	5.08	5.00	4.75	5.04	4.95	8385.12	15.77	2512.72	16.34
32160	3.71	5.08	4.99	4.75	5.04	4.94	8385.12	15.77	2514.00	16.35
32175	3.70	5.08	5.00	4.76	5.04	4.93	8385.12	15.75	2514.00	16.35
32190	3.71	5.08	5.00	4.76	5.03	4.93	8385.12	15.75	2512.35	16.34
32205	3.71	5.08	5.00	4.76	5.03	4.93	8385.12	15.75	2510.69	16.35
32220	3.70	5.08	5.00	4.76	5.03	4.93	8385.12	15.75	2507.39	16.34
32235	3.70	5.08	5.00	4.76	5.03	4.92	8385.12	15.75	2504.45	16.35
32250	3.70	5.08	5.00	4.76	5.03	4.92	8383.39	15.75	2504.08	16.35
32265	3.70	5.08	5.00	4.76	5.03	4.91	8383.39	15.75	2502.80	16.34
32280	3.70	5.08	5.00	4.76	5.01	4.91	8386.36	15.76	2502.80	16.34
32295	3.70	5.08	5.00	4.76	5.01	4.90	8384.64	15.76	2501.15	16.34
32310	3.70	5.08	5.00	4.76	5.01	4.90	8386.36	15.76	2501.15	16.34
32325	3.70	5.10	5.00	4.76	5.01	4.90	8384.64	15.76	2499.49	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
32340	3.70	5.10	5.00	4.76	5.01	4.90	8384.64	15.76	2496.18	16.34
32355	3.70	5.10	5.02	4.76	5.01	4.90	8384.64	15.76	2494.53	16.34
32370	3.70	5.10	5.02	4.78	5.01	4.90	8384.64	15.76	2492.88	16.34
32385	3.70	5.10	5.02	4.76	5.01	4.89	8384.64	15.76	2492.88	16.34
32400	3.70	5.10	5.02	4.76	4.99	4.89	8384.16	15.76	2492.88	16.34
32415	3.70	5.10	5.02	4.78	4.99	4.89	8384.64	15.75	2491.22	16.34
32430	3.70	5.10	5.02	4.76	4.99	4.88	8385.89	15.76	2492.88	16.34
32445	3.70	5.10	5.02	4.76	5.01	4.88	8385.89	15.76	2494.53	16.34
32460	3.70	5.08	5.02	4.76	5.01	4.88	8385.89	15.75	2492.88	16.34
32475	3.70	5.08	5.02	4.76	5.01	4.88	8384.64	15.76	2491.22	16.34
32490	3.70	5.08	5.02	4.76	5.01	4.88	8385.89	15.76	2489.57	16.34
32505	3.70	5.10	5.00	4.78	4.99	4.88	8385.89	15.76	2486.63	16.34
32520	3.70	5.08	5.02	4.78	4.99	4.88	8384.64	15.76	2486.26	16.34
32535	3.70	5.10	5.00	4.78	4.99	4.88	8384.64	15.76	2486.26	16.34
32550	3.70	5.08	5.02	4.78	4.99	4.87	8384.64	15.76	2486.26	16.34
32565	3.70	5.10	5.02	4.76	4.99	4.87	8386.36	15.77	2484.61	16.34
32580	3.70	5.10	5.02	4.78	4.99	4.87	8382.92	15.75	2484.61	16.34
32595	3.70	5.10	5.02	4.78	4.99	4.87	8384.16	15.75	2483.32	16.34
32610	3.70	5.10	5.02	4.78	4.99	4.87	8384.16	15.76	2482.96	16.34
32625	3.70	5.10	5.00	4.78	4.99	4.87	8384.64	15.76	2486.63	16.34
32640	3.70	5.08	5.02	4.78	4.99	4.87	8384.16	15.76	2489.94	16.34
32655	3.70	5.08	5.00	4.76	4.99	4.86	8384.16	15.76	2487.92	16.34
32670	3.70	5.08	5.00	4.76	4.99	4.87	8386.36	15.76	2488.29	16.34
32685	3.70	5.08	5.00	4.76	4.99	4.87	8384.16	15.75	2486.26	16.34
32700	3.70	5.08	5.02	4.78	4.99	4.87	8383.39	15.77	2486.26	16.34
32715	3.70	5.08	5.00	4.76	4.99	4.86	8385.89	15.75	2484.98	16.34
32730	3.70	5.08	5.00	4.76	4.99	4.87	8384.64	15.77	2482.96	16.34
32745	3.70	5.08	5.00	4.76	4.98	4.86	8384.64	15.76	2483.32	16.34
32760	3.70	5.08	5.00	4.78	4.99	4.86	8384.16	15.75	2481.67	16.34
32775	3.70	5.08	5.00	4.76	4.98	4.85	8384.64	15.77	2479.65	16.34
32790	3.70	5.08	5.00	4.76	4.99	4.85	8384.16	15.76	2477.99	16.34
32805	3.70	5.08	5.00	4.76	4.98	4.85	8384.16	15.75	2479.65	16.34
32820	3.70	5.08	5.00	4.76	4.98	4.84	8384.16	15.76	2480.02	16.34
32835	3.69	5.08	5.00	4.76	4.98	4.84	8384.16	15.76	2480.02	16.34
32850	3.69	5.08	5.00	4.76	4.98	4.83	8384.16	15.76	2480.02	16.34
32865	3.70	5.08	5.00	4.76	4.98	4.83	8384.16	15.75	2479.65	16.34
32880	3.69	5.07	4.99	4.76	4.98	4.83	8384.16	15.76	2477.99	16.34
32895	3.69	5.07	4.99	4.75	4.98	4.83	8384.16	15.76	2474.69	16.34
32910	3.69	5.07	4.99	4.75	4.98	4.83	8382.92	15.76	2473.40	16.34
32925	3.69	5.07	4.99	4.75	4.98	4.82	8383.39	15.77	2471.38	16.34
32940	3.69	5.07	4.99	4.73	4.98	4.82	8382.92	15.76	2469.73	16.34
32955	3.70	5.07	4.97	4.75	4.98	4.82	8382.92	15.76	2469.73	16.34
32970	3.69	5.07	4.97	4.75	4.98	4.82	8385.89	15.76	2469.73	16.34
32985	3.70	5.07	4.97	4.73	4.98	4.82	8384.64	15.76	2469.73	16.34
33000	3.70	5.05	4.97	4.73	4.98	4.82	8385.89	15.75	2469.73	16.34
33015	3.70	5.05	4.97	4.73	4.98	4.82	8384.64	15.76	2468.07	16.34
33030	3.70	5.05	4.97	4.73	4.98	4.82	8382.92	15.76	2466.42	16.34
33045	3.70	5.05	4.95	4.73	4.98	4.82	8382.92	15.76	2466.42	16.34
33060	3.70	5.05	4.97	4.73	4.98	4.82	8382.92	15.76	2466.42	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
33075	3.70	5.05	4.97	4.73	4.98	4.82	8384.64	15.76	2466.42	16.34
33090	3.70	5.05	4.95	4.73	4.98	4.82	8384.64	15.76	2464.77	16.34
33105	3.70	5.05	4.97	4.71	4.98	4.82	8384.64	15.76	2464.77	16.34
33120	3.71	5.05	4.95	4.71	4.98	4.82	8382.92	15.76	2464.77	16.34
33135	3.70	5.04	4.95	4.71	4.98	4.82	8384.64	15.76	2464.40	16.34
33150	3.71	5.04	4.95	4.71	4.98	4.83	8384.64	15.76	2464.40	16.34
33165	3.71	5.04	4.95	4.71	4.98	4.83	8384.64	15.76	2464.40	16.34
33180	3.71	5.04	4.95	4.71	4.99	4.84	8384.64	15.76	2463.11	16.34
33195	3.71	5.04	4.95	4.71	4.99	4.84	8383.39	15.75	2462.75	16.34
33210	3.71	5.04	4.95	4.71	4.99	4.84	8383.39	15.75	2464.40	16.34
33225	3.71	5.04	4.94	4.71	4.99	4.85	8383.39	15.75	2466.05	16.34
33240	3.72	5.04	4.94	4.70	4.99	4.85	8383.39	15.75	2469.36	16.34
33255	3.71	5.04	4.94	4.70	4.99	4.85	8383.39	15.77	2471.01	16.34
33270	3.72	5.04	4.94	4.70	4.99	4.86	8383.39	15.75	2471.38	16.34
33285	3.71	5.02	4.94	4.70	4.99	4.85	8383.39	15.75	2472.67	16.34
33300	3.71	5.02	4.94	4.68	4.99	4.85	8382.15	15.76	2471.01	16.34
33315	3.71	5.02	4.92	4.70	4.99	4.86	8382.15	15.76	2473.95	16.34
33330	3.72	5.02	4.94	4.70	4.99	4.86	8382.15	15.76	2472.67	16.34
33345	3.72	5.02	4.94	4.70	4.99	4.87	8383.39	15.77	2472.67	16.34
33360	3.71	5.02	4.92	4.70	5.01	4.87	8382.15	15.76	2475.61	16.34
33375	3.71	5.02	4.92	4.68	5.01	4.87	8383.87	15.76	2475.61	16.34
33390	3.71	5.01	4.92	4.68	5.01	4.87	8382.15	15.76	2477.26	16.34
33405	3.71	5.02	4.92	4.68	5.01	4.87	8382.15	15.76	2475.61	16.34
33420	3.71	5.02	4.92	4.68	5.01	4.87	8383.87	15.76	2473.95	16.34
33435	3.71	5.02	4.92	4.68	5.01	4.87	8383.87	15.76	2474.32	16.34
33450	3.71	5.01	4.92	4.68	5.01	4.87	8383.87	15.76	2476.89	16.34
33465	3.71	5.02	4.92	4.68	5.01	4.87	8383.87	15.76	2478.91	16.34
33480	3.71	5.02	4.92	4.68	5.01	4.87	8383.87	15.76	2480.57	16.34
33495	3.71	5.01	4.92	4.68	5.01	4.87	8383.87	15.76	2482.22	16.34
33510	3.71	5.01	4.92	4.68	5.01	4.87	8383.87	15.76	2479.28	16.34
33525	3.70	5.01	4.92	4.68	5.01	4.87	8382.15	15.76	2478.91	16.34
33540	3.71	5.01	4.92	4.68	4.99	4.87	8382.15	15.76	2475.97	16.34
33555	3.71	5.02	4.92	4.68	4.99	4.87	8382.15	15.76	2474.32	16.34
33570	3.70	5.02	4.92	4.70	4.99	4.86	8382.15	15.76	2471.01	16.34
33585	3.70	5.02	4.92	4.68	4.99	4.86	8382.15	15.75	2471.01	16.34
33600	3.70	5.02	4.94	4.70	4.99	4.86	8382.15	15.76	2472.30	16.34
33615	3.70	5.02	4.92	4.70	4.99	4.85	8383.39	15.75	2470.65	16.34
33630	3.70	5.02	4.94	4.70	4.99	4.85	8383.39	15.77	2470.65	16.34
33645	3.70	5.02	4.94	4.70	4.99	4.85	8383.39	15.77	2468.99	16.34
33660	3.70	5.02	4.94	4.70	4.98	4.85	8383.39	15.77	2469.36	16.35
33675	3.70	5.02	4.94	4.70	4.98	4.84	8383.39	15.75	2469.36	16.35
33690	3.70	5.02	4.94	4.70	4.98	4.84	8383.39	15.75	2466.05	16.35
33705	3.70	5.02	4.94	4.70	4.98	4.84	8382.92	15.76	2466.05	16.35
33720	3.70	5.02	4.95	4.70	4.98	4.84	8382.92	15.76	2466.05	16.34
33735	3.70	5.02	4.94	4.70	4.98	4.84	8381.67	15.75	2466.05	16.35
33750	3.70	5.04	4.95	4.71	4.98	4.84	8381.67	15.75	2464.40	16.34
33765	3.70	5.04	4.95	4.71	4.96	4.83	8382.92	15.76	2462.75	16.34
33780	3.70	5.04	4.95	4.71	4.96	4.84	8382.92	15.76	2461.46	16.34
33795	3.70	5.04	4.95	4.71	4.96	4.84	8382.92	15.76	2461.09	16.34

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
33810	3.70	5.04	4.95	4.71	4.96	4.84	8382.92	15.76	2461.46	16.35
33825	3.71	5.04	4.95	4.71	4.96	4.84	8382.92	15.76	2463.11	16.34
33840	3.70	5.04	4.95	4.71	4.96	4.84	8383.39	15.77	2464.77	16.34
33855	3.70	5.04	4.95	4.71	4.96	4.85	8382.92	15.76	2464.40	16.34
33870	3.71	5.04	4.95	4.71	4.96	4.84	8382.92	15.76	2464.77	16.34
33885	3.70	5.04	4.95	4.71	4.96	4.85	8382.92	15.76	2464.77	16.34
33900	3.70	5.05	4.95	4.71	4.96	4.84	8382.92	15.76	2464.77	16.34
33915	3.70	5.04	4.97	4.71	4.96	4.84	8382.92	15.76	2466.42	16.34
33930	3.70	5.04	4.95	4.71	4.95	4.84	8382.92	15.75	2468.07	16.34
33945	3.70	5.05	4.95	4.71	4.96	4.84	8383.39	15.77	2473.03	16.34
33960	3.71	5.05	4.95	4.71	4.96	4.85	8384.64	15.77	2474.69	16.34
33975	3.71	5.05	4.95	4.71	4.96	4.85	8384.16	15.75	2473.03	16.34
33990	3.71	5.05	4.95	4.73	4.96	4.85	8384.64	15.77	2473.03	16.34
34005	3.71	5.05	4.95	4.71	4.96	4.86	8383.39	15.77	2471.38	16.34
34020	3.71	5.05	4.97	4.71	4.96	4.86	8381.67	15.77	2471.38	16.34
34035	3.71	5.05	4.95	4.71	4.96	4.86	8382.92	15.76	2473.03	16.34
34050	3.71	5.05	4.95	4.71	4.96	4.86	8382.92	15.76	2474.69	16.34
34065	3.71	5.05	4.95	4.71	4.96	4.86	8381.20	15.76	2477.99	16.34
34080	3.71	5.05	4.95	4.71	4.96	4.87	8382.92	15.76	2482.96	16.34
34095	3.70	5.04	4.95	4.71	4.96	4.86	8382.92	15.76	2481.30	16.34
34110	3.71	5.05	4.95	4.71	4.96	4.87	8383.39	15.77	2481.30	16.34
34125	3.73	5.05	4.95	4.73	4.96	4.88	8381.20	15.76	2479.65	16.34
34140	3.74	5.05	4.95	4.73	4.96	4.89	8381.20	15.76	2479.65	16.34
34155	3.74	5.05	4.97	4.73	4.96	4.89	8382.92	15.76	2476.34	16.34
34170	3.74	5.05	4.97	4.73	4.96	4.89	8383.39	15.77	2471.38	16.34
34185	3.74	5.07	4.97	4.73	4.96	4.90	8381.20	15.76	2466.42	16.35
34200	3.73	5.05	4.97	4.73	4.96	4.90	8382.92	15.76	2464.77	16.34
34215	3.74	5.05	4.97	4.71	4.96	4.90	8381.20	15.76	2464.77	16.34
34230	3.74	5.05	4.97	4.73	4.96	4.91	8381.20	15.76	2463.11	16.34
34245	3.73	5.05	4.97	4.73	4.96	4.91	8381.20	15.76	2464.77	16.34
34260	3.73	5.05	4.95	4.73	4.96	4.91	8381.20	15.76	2471.38	16.34
34275	3.73	5.05	4.97	4.73	4.96	4.92	8382.92	15.76	2474.69	16.34
34290	3.73	5.05	4.95	4.73	4.96	4.91	8382.92	15.76	2477.99	16.34
34305	3.73	5.05	4.97	4.73	4.96	4.92	8381.20	15.76	2482.96	16.35
34320	3.73	5.05	4.95	4.73	4.96	4.92	8382.92	15.75	2484.61	16.35
34335	3.73	5.05	4.97	4.71	4.96	4.92	8382.44	15.76	2487.92	16.34
34350	3.72	5.05	4.95	4.71	4.96	4.92	8382.92	15.76	2489.57	16.34
34365	3.72	5.05	4.95	4.71	4.98	4.92	8381.20	15.75	2491.22	16.34
34380	3.72	5.05	4.95	4.71	4.96	4.92	8381.20	15.75	2492.88	16.34
34395	3.72	5.05	4.95	4.70	4.96	4.92	8381.20	15.76	2496.18	16.34
34410	3.73	5.05	4.95	4.71	4.98	4.93	8382.92	15.76	2497.84	16.35
34425	3.73	5.05	4.95	4.71	4.98	4.94	8382.92	15.76	2497.47	16.34
34440	3.72	5.05	4.95	4.71	4.98	4.94	8381.20	15.76	2499.49	16.35
34455	3.72	5.05	4.95	4.70	4.98	4.94	8381.20	15.76	2504.45	16.34
34470	3.72	5.05	4.94	4.71	4.98	4.94	8383.39	15.77	2507.39	16.35
34485	3.72	5.04	4.94	4.70	4.98	4.94	8381.67	15.75	2509.41	16.35
34500	3.73	5.04	4.94	4.70	4.98	4.95	8381.67	15.75	2509.04	16.34
34515	3.73	5.04	4.94	4.70	4.98	4.95	8381.67	15.75	2509.04	16.35
34530	3.72	5.04	4.94	4.70	4.98	4.95	8381.67	15.75	2507.39	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
34545	3.71	5.04	4.92	4.70	4.98	4.94	8381.67	15.77	2505.73	16.35
34560	3.72	5.04	4.92	4.70	4.98	4.95	8381.67	15.75	2505.73	16.35
34575	3.73	5.04	4.92	4.68	4.99	4.96	8381.67	15.75	2505.73	16.35
34590	3.72	5.02	4.92	4.70	4.99	4.95	8381.67	15.77	2505.36	16.34
34605	3.74	5.04	4.92	4.70	5.01	4.97	8381.67	15.77	2504.08	16.35
34620	3.73	5.02	4.92	4.70	4.99	4.98	8383.39	15.77	2500.77	16.34
34635	3.72	5.02	4.91	4.68	4.99	4.96	8382.15	15.75	2502.06	16.34
34650	3.72	5.02	4.91	4.68	4.99	4.97	8382.15	15.76	2502.43	16.34
34665	3.72	5.02	4.91	4.68	4.99	4.97	8382.15	15.76	2508.67	16.34
34680	3.72	5.02	4.91	4.67	4.99	4.97	8382.15	15.76	2512.35	16.34
34695	3.72	5.02	4.91	4.68	4.99	4.97	8382.15	15.76	2517.31	16.35
34710	3.74	5.02	4.92	4.68	5.01	4.98	8382.15	15.76	2518.96	16.35
34725	3.73	5.02	4.91	4.68	5.01	4.99	8382.15	15.76	2517.31	16.35
34740	3.72	5.02	4.91	4.67	4.99	4.98	8380.90	15.76	2515.65	16.35
34755	3.72	5.02	4.91	4.67	4.99	4.98	8382.15	15.76	2516.93	16.34
34770	3.72	5.02	4.91	4.67	5.01	4.98	8382.15	15.76	2514.00	16.34
34785	3.73	5.02	4.91	4.68	5.01	4.99	8380.90	15.76	2514.00	16.35
34800	3.72	5.02	4.91	4.67	5.01	4.99	8380.90	15.76	2511.97	16.34
34815	3.71	5.01	4.89	4.67	4.99	4.98	8380.90	15.76	2510.69	16.35
34830	3.73	5.02	4.91	4.67	5.01	4.99	8380.43	15.75	2508.67	16.34
34845	3.74	5.02	4.91	4.67	5.01	5.01	8382.62	15.76	2507.02	16.34
34860	3.73	5.01	4.91	4.67	5.01	5.00	8382.62	15.77	2505.36	16.34
34875	3.72	5.01	4.91	4.67	5.01	5.00	8382.15	15.75	2507.02	16.34
34890	3.72	5.01	4.89	4.67	5.01	4.99	8382.15	15.75	2508.67	16.34
34905	3.71	5.01	4.89	4.65	5.01	4.99	8380.43	15.75	2511.97	16.34
34920	3.72	5.02	4.91	4.67	5.01	4.99	8380.90	15.76	2511.97	16.34
34935	3.72	5.02	4.91	4.67	4.99	4.99	8380.90	15.76	2511.97	16.34
34950	3.72	5.02	4.91	4.67	4.99	4.99	8380.90	15.76	2508.67	16.34
34965	3.70	5.02	4.91	4.67	4.99	4.98	8382.15	15.76	2505.36	16.34
34980	3.70	5.02	4.91	4.67	4.99	4.95	8382.15	15.76	2505.73	16.35
34995	3.71	5.02	4.91	4.67	4.99	4.95	8382.15	15.76	2505.73	16.35
35010	3.75	5.04	4.92	4.68	4.99	4.98	8382.15	15.76	2500.77	16.34
35025	3.77	5.04	4.92	4.68	4.99	4.99	8380.43	15.76	2494.16	16.34
35040	3.77	5.04	4.92	4.68	4.98	4.98	8380.43	15.75	2487.92	16.34
35055	3.76	5.04	4.92	4.70	4.98	4.98	8381.67	15.77	2481.30	16.34
35070	3.76	5.04	4.94	4.68	4.98	4.97	8381.67	15.77	2476.34	16.34
35085	3.75	5.04	4.92	4.68	4.98	4.97	8381.67	15.75	2472.67	16.35
35100	3.74	5.04	4.92	4.68	4.98	4.96	8381.67	15.75	2467.71	16.35
35115	3.74	5.04	4.92	4.70	4.98	4.96	8381.67	15.75	2462.75	16.35
35130	3.74	5.05	4.92	4.70	4.98	4.96	8381.67	15.75	2461.09	16.35
35145	3.74	5.05	4.92	4.70	4.98	4.96	8381.67	15.75	2459.44	16.35
35160	3.73	5.04	4.92	4.68	4.96	4.96	8381.67	15.75	2457.79	16.35
35175	3.72	5.04	4.92	4.70	4.96	4.95	8382.92	15.76	2456.13	16.35
35190	3.73	5.05	4.94	4.70	4.98	4.95	8382.92	15.76	2454.48	16.35
35205	3.72	5.05	4.92	4.68	4.96	4.94	8381.67	15.75	2456.13	16.35
35220	3.70	5.04	4.92	4.68	4.96	4.93	8382.92	15.76	2457.79	16.35
35235	3.72	5.04	4.92	4.68	4.96	4.93	8379.95	15.75	2462.75	16.35
35250	3.73	5.05	4.94	4.68	4.96	4.94	8381.67	15.75	2468.07	16.35
35265	3.73	5.05	4.94	4.68	4.96	4.94	8379.95	15.75	2472.67	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
35280	3.73	5.05	4.92	4.70	4.96	4.95	8379.95	15.75	2477.99	16.35
35295	3.73	5.05	4.94	4.70	4.96	4.95	8381.20	15.76	2484.24	16.35
35310	3.72	5.05	4.92	4.70	4.96	4.94	8381.67	15.75	2489.20	16.35
35325	3.71	5.04	4.92	4.70	4.96	4.93	8381.20	15.76	2492.88	16.34
35340	3.71	5.05	4.92	4.68	4.96	4.93	8381.20	15.76	2492.51	16.35
35355	3.70	5.04	4.92	4.68	4.96	4.92	8379.95	15.75	2492.51	16.35
35370	3.70	5.04	4.92	4.68	4.95	4.92	8381.20	15.76	2494.16	16.35
35385	3.71	5.05	4.92	4.68	4.95	4.91	8379.95	15.75	2495.81	16.35
35400	3.71	5.04	4.92	4.68	4.95	4.92	8382.92	15.76	2499.12	16.35
35415	3.71	5.04	4.92	4.68	4.95	4.92	8381.20	15.76	2500.77	16.35
35430	3.71	5.05	4.92	4.68	4.95	4.91	8381.20	15.76	2504.08	16.35
35445	3.71	5.04	4.92	4.68	4.95	4.91	8381.20	15.76	2507.39	16.35
35460	3.71	5.04	4.92	4.68	4.95	4.91	8381.20	15.76	2507.76	16.35
35475	3.71	5.05	4.92	4.70	4.95	4.91	8381.20	15.76	2509.41	16.35
35490	3.71	5.05	4.92	4.68	4.95	4.90	8381.20	15.76	2509.41	16.35
35505	3.71	5.05	4.92	4.68	4.95	4.91	8381.20	15.76	2509.41	16.35
35520	3.71	5.05	4.92	4.68	4.95	4.92	8381.20	15.76	2507.76	16.35
35535	3.71	5.05	4.92	4.70	4.95	4.91	8381.20	15.76	2509.41	16.35
35550	3.71	5.05	4.94	4.68	4.95	4.91	8381.20	15.76	2507.76	16.35
35565	3.71	5.05	4.92	4.70	4.95	4.91	8381.20	15.76	2509.41	16.35
35580	3.71	5.05	4.94	4.70	4.95	4.91	8381.20	15.76	2509.41	16.35
35595	3.70	5.05	4.92	4.68	4.93	4.90	8381.20	15.76	2509.41	16.35
35610	3.70	5.05	4.94	4.68	4.93	4.89	8381.20	15.76	2512.72	16.34
35625	3.70	5.05	4.94	4.70	4.93	4.89	8381.67	15.77	2514.37	16.35
35640	3.70	5.07	4.94	4.70	4.93	4.89	8381.20	15.75	2517.68	16.34
35655	3.70	5.05	4.94	4.70	4.93	4.88	8382.92	15.77	2519.34	16.34
35670	3.70	5.07	4.94	4.70	4.93	4.89	8381.20	15.76	2519.34	16.34
35685	3.70	5.07	4.94	4.70	4.93	4.87	8381.20	15.75	2519.34	16.34
35700	3.70	5.07	4.94	4.70	4.93	4.87	8381.20	15.76	2522.64	16.35
35715	3.70	5.07	4.94	4.70	4.92	4.87	8382.44	15.76	2524.30	16.34
35730	3.70	5.05	4.94	4.70	4.92	4.86	8382.44	15.76	2524.30	16.35
35745	3.70	5.07	4.94	4.68	4.92	4.86	8382.44	15.75	2526.32	16.36
35760	3.70	5.07	4.92	4.70	4.92	4.86	8381.67	15.77	2525.95	16.35
35775	3.70	5.05	4.92	4.68	4.92	4.86	8381.20	15.75	2524.30	16.34
35790	3.70	5.07	4.92	4.68	4.93	4.85	8381.20	15.76	2522.64	16.34
35805	3.70	5.05	4.92	4.68	4.93	4.85	8381.20	15.76	2522.64	16.34
35820	3.70	5.05	4.92	4.68	4.93	4.86	8381.20	15.76	2522.64	16.35
35835	3.70	5.05	4.91	4.68	4.93	4.85	8381.20	15.76	2520.99	16.35
35850	3.70	5.05	4.91	4.67	4.93	4.86	8381.20	15.76	2520.99	16.35
35865	3.70	5.05	4.91	4.67	4.93	4.86	8382.92	15.76	2520.99	16.35
35880	3.70	5.05	4.89	4.67	4.93	4.86	8382.92	15.76	2522.27	16.35
35895	3.70	5.04	4.89	4.65	4.93	4.85	8381.20	15.76	2522.64	16.35
35910	3.70	5.04	4.91	4.67	4.93	4.85	8382.92	15.76	2524.30	16.35
35925	3.70	5.04	4.89	4.65	4.93	4.85	8381.67	15.77	2525.95	16.35
35940	3.70	5.04	4.89	4.65	4.93	4.85	8381.67	15.75	2525.95	16.35
35955	3.70	5.04	4.89	4.67	4.93	4.85	8381.67	15.75	2525.57	16.35
35970	3.70	5.04	4.89	4.65	4.93	4.85	8381.67	15.75	2525.57	16.35
35985	3.70	5.04	4.89	4.65	4.93	4.85	8382.92	15.76	2525.57	16.35
36000	3.71	5.04	4.88	4.65	4.93	4.85	8379.95	15.75	2523.92	16.35

RAYMARK INDUSTRIES, INC.
STRATFORD, CONNECTICUT
RCRA SECTION 3013 ORDER
DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
36015	3.70	5.04	4.89	4.65	4.93	4.85	8381.67	15.75	2523.92	16.35
36030	3.71	5.04	4.89	4.65	4.93	4.86	8381.67	15.75	2522.27	16.35
36045	3.71	5.04	4.89	4.65	4.93	4.85	8381.67	15.75	2520.61	16.35
36060	3.73	5.05	4.89	4.65	4.95	4.87	8381.67	15.75	2518.96	16.35
36075	3.72	5.04	4.89	4.65	4.93	4.86	8381.67	15.75	2517.31	16.35
36090	3.73	5.05	4.89	4.65	4.95	4.87	8381.67	15.75	2518.96	16.35
36105	3.71	5.04	4.88	4.65	4.93	4.87	8381.67	15.77	2518.96	16.35
36120	3.72	5.04	4.88	4.65	4.95	4.87	8381.67	15.77	2518.96	16.35
36135	3.73	5.04	4.89	4.65	4.95	4.87	8381.67	15.75	2518.96	16.35
36150	3.71	5.02	4.88	4.64	4.95	4.86	8381.67	15.75	2517.68	16.34
36165	3.71	5.04	4.88	4.64	4.93	4.86	8381.67	15.75	2520.61	16.35
36180	3.71	5.04	4.88	4.62	4.93	4.86	8381.67	15.75	2520.61	16.36
36195	3.71	5.02	4.86	4.64	4.93	4.86	8382.15	15.76	2521.89	16.35
36210	3.71	5.04	4.88	4.64	4.93	4.86	8380.43	15.75	2520.61	16.34
36225	3.70	5.02	4.86	4.64	4.93	4.85	8381.67	15.77	2523.92	16.35
36240	3.71	5.04	4.88	4.64	4.95	4.86	8380.43	15.76	2523.92	16.35
36255	3.71	5.02	4.88	4.64	4.95	4.86	8381.67	15.77	2525.95	16.34
36270	3.72	5.04	4.88	4.64	4.95	4.86	8380.43	15.76	2528.51	16.35
36285	3.71	5.04	4.86	4.62	4.93	4.86	8380.43	15.76	2528.88	16.35
36300	3.71	5.04	4.86	4.62	4.95	4.86	8380.43	15.76	2530.53	16.36
36315	3.71	5.04	4.86	4.64	4.95	4.86	8380.43	15.75	2533.47	16.35
36330	3.70	5.04	4.86	4.64	4.93	4.86	8380.43	15.76	2533.84	16.35
36345	3.71	5.02	4.86	4.62	4.93	4.86	8380.43	15.76	2535.12	16.35
36360	3.71	5.02	4.86	4.62	4.93	4.86	8380.43	15.76	2533.84	16.34
36375	3.70	5.04	4.86	4.64	4.93	4.85	8380.43	15.76	2535.12	16.34
36390	3.70	5.02	4.86	4.62	4.93	4.85	8383.39	15.77	2533.84	16.35
36405	3.70	5.04	4.86	4.62	4.93	4.85	8380.43	15.76	2535.49	16.35
36420	3.70	5.04	4.86	4.64	4.95	4.84	8380.43	15.76	2535.49	16.34
36435	3.70	5.04	4.86	4.62	4.93	4.84	8381.67	15.77	2535.49	16.35
36450	3.70	5.04	4.86	4.62	4.93	4.83	8381.67	15.77	2535.49	16.34
36465	3.70	5.04	4.86	4.64	4.93	4.83	8381.67	15.77	2536.77	16.34
36480	3.69	5.04	4.86	4.62	4.92	4.82	8381.67	15.75	2535.87	16.34
36495	3.70	5.04	4.86	4.64	4.93	4.82	8381.67	15.75	2537.15	16.35
36510	3.70	5.04	4.88	4.64	4.92	4.82	8381.67	15.75	2534.22	16.34
36525	3.70	5.04	4.88	4.64	4.92	4.81	8379.95	15.75	2535.49	16.35
36540	3.70	5.05	4.88	4.64	4.92	4.82	8382.92	15.76	2533.84	16.35
36555	3.70	5.05	4.88	4.64	4.92	4.81	8379.95	15.75	2532.19	16.35
36570	3.69	5.05	4.88	4.64	4.92	4.80	8381.20	15.76	2528.88	16.35
36585	3.69	5.05	4.88	4.64	4.90	4.80	8381.20	15.76	2528.88	16.35
36600	3.69	5.05	4.88	4.65	4.90	4.79	8381.20	15.76	2525.95	16.35
36615	3.69	5.05	4.89	4.65	4.90	4.79	8381.20	15.76	2525.57	16.35
36630	3.69	5.05	4.88	4.65	4.90	4.79	8381.20	15.76	2524.30	16.35
36645	3.70	5.05	4.88	4.65	4.90	4.79	8381.20	15.76	2522.64	16.35
36660	3.70	5.05	4.88	4.65	4.90	4.79	8381.20	15.76	2520.99	16.35
36675	3.70	5.05	4.89	4.65	4.90	4.79	8381.20	15.76	2519.34	16.34
36690	3.70	5.07	4.89	4.65	4.90	4.79	8381.20	15.76	2517.68	16.35
36705	3.70	5.07	4.89	4.65	4.90	4.78	8381.20	15.76	2516.03	16.35
36720	3.70	5.07	4.89	4.65	4.90	4.78	8381.20	15.76	2514.37	16.34
36735	3.70	5.07	4.89	4.65	4.88	4.78	8381.67	15.75	2512.72	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
36750	3.70	5.07	4.89	4.65	4.88	4.78	8381.20	15.76	2511.07	16.3
36765	3.70	5.07	4.89	4.65	4.88	4.78	8381.20	15.75	2511.07	16.3
36780	3.70	5.07	4.89	4.65	4.90	4.78	8382.44	15.76	2509.41	16.3
36795	3.70	5.07	4.89	4.65	4.88	4.77	8381.20	15.75	2509.79	16.3
36810	3.70	5.07	4.89	4.67	4.88	4.77	8382.44	15.75	2509.41	16.3
36825	3.70	5.07	4.89	4.67	4.88	4.78	8382.92	15.77	2509.79	16.3
36840	3.70	5.07	4.91	4.67	4.88	4.77	8380.72	15.75	2509.79	16.3
36855	3.70	5.07	4.91	4.67	4.88	4.77	8382.44	15.75	2509.41	16.3
36870	3.70	5.08	4.91	4.67	4.88	4.77	8382.92	15.76	2508.13	16.3
36885	3.70	5.08	4.91	4.67	4.88	4.78	8381.20	15.76	2508.13	16.3
36900	3.71	5.07	4.91	4.67	4.88	4.78	8382.92	15.76	2506.11	16.3
36915	3.71	5.08	4.91	4.67	4.88	4.79	8380.72	15.75	2504.45	16.3
36930	3.71	5.08	4.91	4.67	4.88	4.78	8382.44	15.75	2504.82	16.3
36945	3.70	5.08	4.91	4.67	4.88	4.79	8382.92	15.76	2504.82	16.3
36960	3.70	5.08	4.91	4.67	4.88	4.79	8382.44	15.76	2504.82	16.3
36975	3.71	5.08	4.91	4.67	4.87	4.79	8380.72	15.75	2504.82	16.3
36990	3.71	5.08	4.91	4.67	4.88	4.79	8381.20	15.76	2506.11	16.3
37005	3.71	5.08	4.91	4.67	4.88	4.79	8381.20	15.76	2503.17	16.3
37020	3.71	5.08	4.91	4.67	4.88	4.80	8382.44	15.75	2501.52	16.3
37035	3.71	5.08	4.91	4.67	4.88	4.80	8380.72	15.75	2501.52	16.3
37050	3.71	5.08	4.91	4.67	4.87	4.80	8380.72	15.75	2501.52	16.3
37065	3.70	5.08	4.89	4.67	4.88	4.79	8381.20	15.77	2501.52	16.3
37080	3.70	5.08	4.89	4.67	4.88	4.79	8381.20	15.76	2503.17	16.3
37095	3.71	5.08	4.91	4.67	4.88	4.79	8380.72	15.75	2503.17	16.3
37110	3.70	5.08	4.91	4.67	4.88	4.79	8382.44	15.75	2503.17	16.3
37125	3.70	5.08	4.91	4.67	4.88	4.79	8380.72	15.75	2503.17	16.3
37140	3.70	5.08	4.91	4.67	4.87	4.79	8381.20	15.76	2504.82	16.3
37155	3.70	5.08	4.91	4.67	4.87	4.78	8380.72	15.75	2504.82	16.3
37170	3.70	5.08	4.89	4.67	4.87	4.78	8380.72	15.75	2505.73	16.3
37185	3.70	5.08	4.89	4.67	4.87	4.78	8380.72	15.75	2504.82	16.3
37200	3.70	5.08	4.89	4.65	4.87	4.78	8381.20	15.76	2504.82	16.3
37215	3.70	5.08	4.89	4.67	4.87	4.77	8381.20	15.76	2504.45	16.3
37230	3.70	5.07	4.89	4.65	4.87	4.77	8381.20	15.76	2504.45	16.3
37245	3.70	5.07	4.88	4.65	4.87	4.77	8382.44	15.76	2504.82	16.3
37260	3.70	5.07	4.88	4.65	4.87	4.77	8382.44	15.76	2504.82	16.3
37275	3.70	5.07	4.88	4.65	4.87	4.77	8381.20	15.76	2506.11	16.3
37290	3.70	5.07	4.88	4.64	4.88	4.77	8382.44	15.76	2506.11	16.3
37305	3.70	5.07	4.86	4.64	4.87	4.78	8381.20	15.76	2508.13	16.3
37320	3.70	5.07	4.86	4.64	4.87	4.77	8381.20	15.76	2507.76	16.3
37335	3.70	5.05	4.86	4.62	4.87	4.77	8381.20	15.76	2507.76	16.3
37350	3.71	5.05	4.86	4.64	4.88	4.78	8382.44	15.76	2509.41	16.3
37365	3.71	5.07	4.86	4.62	4.88	4.79	8381.20	15.76	2509.41	16.3
37380	3.70	5.05	4.86	4.64	4.88	4.78	8381.20	15.76	2509.41	16.3
37395	3.71	5.07	4.86	4.62	4.88	4.78	8381.20	15.76	2509.41	16.3
37410	3.71	5.05	4.84	4.62	4.88	4.78	8381.20	15.76	2509.41	16.3
37425	3.71	5.05	4.86	4.62	4.88	4.78	8381.20	15.76	2511.07	16.3
37440	3.72	5.05	4.84	4.62	4.88	4.79	8379.95	15.75	2511.07	16.3
37455	3.71	5.05	4.84	4.60	4.88	4.79	8380.43	15.76	2511.07	16.3
37470	3.72	5.05	4.84	4.62	4.88	4.80	8381.20	15.76	2512.35	16.3

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
37485	3.72	5.05	4.84	4.62	4.88	4.81	8381.67	15.75	2514.00	16.35
37500	3.73	5.05	4.84	4.60	4.90	4.82	8381.67	15.75	2516.03	16.35
37515	3.72	5.04	4.84	4.60	4.90	4.81	8381.67	15.75	2517.31	16.35
37530	3.74	5.05	4.86	4.62	4.92	4.83	8381.67	15.75	2520.61	16.35
37545	3.74	5.05	4.84	4.62	4.92	4.84	8381.67	15.75	2520.99	16.35
37560	3.71	5.04	4.83	4.60	4.90	4.82	8381.67	15.75	2525.57	16.35
37575	3.73	5.05	4.84	4.62	4.90	4.83	8381.67	15.75	2527.23	16.35
37590	3.73	5.05	4.84	4.62	4.92	4.83	8381.67	15.77	2528.88	16.35
37605	3.72	5.04	4.83	4.59	4.90	4.82	8381.67	15.75	2530.53	16.35
37620	3.73	5.05	4.84	4.60	4.92	4.84	8381.67	15.75	2530.91	16.35
37635	3.73	5.04	4.84	4.60	4.90	4.84	8381.67	15.77	2533.84	16.35
37650	3.73	5.04	4.83	4.60	4.90	4.84	8380.43	15.75	2534.22	16.35
37665	3.72	5.04	4.83	4.60	4.90	4.84	8380.43	15.76	2537.15	16.35
37680	3.72	5.04	4.83	4.60	4.90	4.84	8381.67	15.77	2540.45	16.35
37695	3.74	5.05	4.84	4.60	4.92	4.87	8379.95	15.75	2542.11	16.35
37710	3.72	5.04	4.83	4.59	4.92	4.85	8380.43	15.76	2542.11	16.35
37725	3.73	5.04	4.83	4.60	4.92	4.86	8382.15	15.76	2543.76	16.35
37740	3.73	5.04	4.83	4.60	4.92	4.87	8381.67	15.75	2545.41	16.35
37755	3.73	5.05	4.84	4.60	4.92	4.87	8380.43	15.76	2548.34	16.35
37770	3.72	5.04	4.83	4.60	4.92	4.87	8380.43	15.76	2548.72	16.35
37785	3.72	5.05	4.83	4.60	4.90	4.86	8380.43	15.75	2550.37	16.35
37800	3.72	5.05	4.84	4.60	4.92	4.86	8381.67	15.77	2552.03	16.35
37815	3.72	5.05	4.84	4.60	4.90	4.86	8381.67	15.75	2553.68	16.35
37830	3.72	5.05	4.84	4.60	4.90	4.86	8381.67	15.77	2555.34	16.35
37845	3.71	5.05	4.84	4.62	4.88	4.85	8381.67	15.75	2554.06	16.35
37860	3.71	5.05	4.84	4.62	4.88	4.85	8381.67	15.75	2556.99	16.35
37875	3.71	5.05	4.84	4.62	4.88	4.84	8381.67	15.75	2558.64	16.35
37890	3.71	5.05	4.84	4.62	4.88	4.85	8379.95	15.75	2558.64	16.35
37905	3.71	5.05	4.84	4.62	4.90	4.85	8381.67	15.75	2557.37	16.34
37920	3.71	5.05	4.84	4.60	4.88	4.84	8381.67	15.75	2558.64	16.35
37935	3.71	5.05	4.84	4.60	4.88	4.84	8379.95	15.75	2560.30	16.35
37950	3.71	5.05	4.84	4.60	4.88	4.84	8381.67	15.75	2562.33	16.35
37965	3.71	5.05	4.84	4.60	4.88	4.83	8379.95	15.75	2562.33	16.35
37980	3.71	5.05	4.84	4.62	4.88	4.83	8381.20	15.76	2565.26	16.35
37995	3.70	5.05	4.86	4.62	4.88	4.82	8381.20	15.76	2565.64	16.35
38010	3.70	5.07	4.84	4.62	4.87	4.82	8381.20	15.76	2567.29	16.35
38025	3.70	5.05	4.86	4.62	4.87	4.82	8381.20	15.76	2568.94	16.35
38040	3.70	5.07	4.86	4.62	4.88	4.82	8381.20	15.76	2568.94	16.35
38055	3.70	5.07	4.86	4.62	4.87	4.81	8381.20	15.76	2568.94	16.35
38070	3.70	5.07	4.86	4.62	4.87	4.81	8381.20	15.76	2570.60	16.35
38085	3.70	5.07	4.86	4.62	4.87	4.80	8381.20	15.76	2570.60	16.35
38100	3.70	5.07	4.86	4.62	4.87	4.80	8382.44	15.75	2570.60	16.35
38115	3.70	5.07	4.86	4.62	4.87	4.80	8381.20	15.76	2570.98	16.35
38130	3.70	5.07	4.86	4.62	4.87	4.80	8382.44	15.76	2572.25	16.35
38145	3.70	5.07	4.86	4.64	4.87	4.80	8381.20	15.75	2572.25	16.34
38160	3.70	5.07	4.88	4.62	4.87	4.79	8382.44	15.75	2572.63	16.35
38175	3.70	5.07	4.86	4.64	4.85	4.79	8382.44	15.76	2572.63	16.35
38190	3.70	5.07	4.86	4.64	4.87	4.79	8382.92	15.76	2572.63	16.35
38205	3.70	5.07	4.86	4.64	4.85	4.79	8380.72	15.75	2573.90	16.35

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 G CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
38220	3.70	5.07	4.86	4.64	4.85	4.79	8382.92	15.76	2575.56	16.35
38235	3.70	5.07	4.86	4.62	4.85	4.79	8380.72	15.75	2577.59	16.36
38250	3.70	5.07	4.86	4.64	4.85	4.79	8382.44	15.75	2579.25	16.36
38265	3.70	5.07	4.86	4.64	4.85	4.79	8382.44	15.76	2579.25	16.36
38280	3.70	5.07	4.86	4.62	4.85	4.79	8381.20	15.76	2578.87	16.34
38295	3.70	5.07	4.86	4.64	4.85	4.78	8381.67	15.75	2580.52	16.35
38310	3.70	5.07	4.86	4.64	4.85	4.78	8382.44	15.75	2582.17	16.35
38325	3.70	5.08	4.86	4.64	4.85	4.79	8382.44	15.75	2582.56	16.36
38340	3.71	5.07	4.86	4.64	4.85	4.78	8381.20	15.76	2582.17	16.35
38355	3.71	5.08	4.88	4.64	4.85	4.79	8381.20	15.77	2583.83	16.35
38370	3.71	5.08	4.88	4.64	4.85	4.79	8380.72	15.75	2584.21	16.36
38385	3.71	5.08	4.88	4.64	4.85	4.79	8380.72	15.75	2585.86	16.34
38400	3.71	5.08	4.88	4.64	4.85	4.79	8382.92	15.77	2585.48	16.34
38415	3.71	5.08	4.88	4.64	4.85	4.79	8382.44	15.75	2589.17	16.36
38430	3.71	5.08	4.88	4.64	4.85	4.78	8381.20	15.76	2590.44	16.35
38445	3.71	5.08	4.88	4.64	4.85	4.79	8380.72	15.75	2590.82	16.34
38460	3.71	5.08	4.88	4.64	4.85	4.79	8381.20	15.76	2590.82	16.34
38475	3.71	5.08	4.88	4.65	4.84	4.79	8381.20	15.76	2592.48	16.34
38490	3.71	5.08	4.88	4.65	4.84	4.79	8380.72	15.75	2592.48	16.34
38505	3.71	5.08	4.88	4.64	4.84	4.79	8381.20	15.76	2594.13	16.34
38520	3.71	5.08	4.88	4.65	4.84	4.79	8380.72	15.75	2594.13	16.34
38535	3.71	5.08	4.89	4.65	4.84	4.79	8380.72	15.75	2597.44	16.36
38550	3.71	5.08	4.88	4.65	4.84	4.79	8381.20	15.76	2599.09	16.34
38565	3.71	5.08	4.89	4.65	4.84	4.78	8381.20	15.76	2599.09	16.34
38580	3.71	5.08	4.88	4.64	4.84	4.79	8380.72	15.75	2600.75	16.34
38595	3.70	5.08	4.88	4.65	4.84	4.78	8381.20	15.76	2600.75	16.34
38610	3.70	5.08	4.89	4.64	4.84	4.78	8381.20	15.76	2600.75	16.34
38625	3.70	5.08	4.88	4.64	4.84	4.78	8380.72	15.75	2602.40	16.34
38640	3.70	5.08	4.88	4.64	4.84	4.77	8380.72	15.75	2604.06	16.36
38655	3.70	5.08	4.88	4.64	4.84	4.77	8381.20	15.76	2605.71	16.34
38670	3.70	5.08	4.88	4.64	4.84	4.77	8381.20	15.76	2607.36	16.36
38685	3.70	5.08	4.86	4.64	4.84	4.77	8381.20	15.76	2607.36	16.34
38700	3.71	5.08	4.86	4.64	4.84	4.77	8381.20	15.76	2609.02	16.36
38715	3.71	5.07	4.86	4.62	4.84	4.78	8380.72	15.75	2610.67	16.34
38730	3.71	5.07	4.84	4.62	4.84	4.78	8380.72	15.75	2610.67	16.34
38745	3.71	5.07	4.84	4.62	4.84	4.78	8382.44	15.76	2612.33	16.34
38760	3.71	5.07	4.84	4.60	4.84	4.78	8380.72	15.76	2613.59	16.35
38775	3.71	5.07	4.84	4.60	4.85	4.79	8379.47	15.76	2615.63	16.36
38790	3.71	5.07	4.84	4.60	4.85	4.79	8382.44	15.75	2615.24	16.35
38805	3.71	5.05	4.83	4.60	4.85	4.79	8381.20	15.76	2617.29	16.36
38820	3.71	5.05	4.83	4.60	4.84	4.78	8381.20	15.76	2618.55	16.35
38835	3.72	5.05	4.83	4.60	4.85	4.79	8381.20	15.76	2618.55	16.35
38850	3.73	5.07	4.84	4.60	4.85	4.80	8382.92	15.77	2620.21	16.35
38865	3.72	5.05	4.83	4.60	4.85	4.79	8381.20	15.75	2621.86	16.35
38880	3.72	5.05	4.83	4.60	4.85	4.79	8381.20	15.76	2623.51	16.35
38895	3.72	5.05	4.83	4.59	4.85	4.79	8381.20	15.76	2623.12	16.35
38910	3.72	5.05	4.81	4.59	4.85	4.80	8381.20	15.76	2625.17	16.35
38925	3.72	5.04	4.81	4.59	4.85	4.80	8381.20	15.76	2626.82	16.35
38940	3.73	5.05	4.81	4.59	4.85	4.81	8381.20	15.76	2628.47	16.35

**RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
 RCRA SECTION 3013 ORDER
 DOCKET NO. I-87-1057**

**TIDAL STUDY FIELD DATA
 G CLUSTER WELLS**

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)						WELL G3		WELL G2	
	G1-1	G2	G3	G4	G5	G6	SP CON	TEMP	SP CON	TEMP
38955	3.74	5.05	4.83	4.59	4.87	4.82	8381.20	15.76	2631.39	16.35
38970	3.73	5.05	4.83	4.59	4.87	4.81	8381.67	15.75	2633.04	16.35
38985	3.74	5.05	4.81	4.59	4.87	4.82	8379.95	15.75	2634.70	16.36
39000	3.72	5.04	4.80	4.59	4.85	4.81	8381.67	15.75	2636.35	16.35
39015	3.73	5.04	4.80	4.57	4.87	4.82	8381.67	15.75	2638.00	16.36
39030	3.73	5.05	4.81	4.59	4.87	4.83	8381.67	15.77	2639.66	16.36

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
0	7.86	7.77	7.73	7.65	7.60
15	7.86	7.78	7.73	7.67	7.31
30	7.86	7.78	7.73	7.67	7.61
45	7.88	7.79	7.73	7.67	7.33
60	7.87	7.79	7.73	7.67	7.32
75	7.86	7.79	7.73	7.67	7.62
90	7.86	7.78	7.73	7.67	7.34
105	7.86	7.77	7.73	7.67	7.34
120	7.87	7.78	7.73	7.68	7.34
135	7.86	7.78	7.73	7.68	7.34
150	7.86	7.78	7.73	7.68	7.34
165	7.87	7.79	7.73	7.67	8.44
180	7.86	7.78	7.73	7.68	7.34
195	7.86	7.78	7.73	7.67	8.25
210	7.86	7.77	7.73	7.67	7.62
225	7.86	7.77	7.73	7.67	7.61
240	7.85	7.77	7.73	7.68	7.61
255	7.85	7.77	7.73	7.67	7.61
270	7.84	7.76	7.73	7.67	7.60
285	7.83	7.75	7.73	7.67	7.60
300	7.83	7.75	7.73	7.67	7.32
315	7.83	7.75	7.73	7.67	7.59
330	7.84	7.75	7.73	7.67	7.59
345	7.84	7.75	7.73	7.65	7.60
360	7.84	7.75	7.73	7.65	7.32
375	7.83	7.74	7.73	7.65	7.31
390	7.84	7.75	7.73	7.65	7.60
405	7.83	7.74	7.73	7.65	7.32
420	7.83	7.74	7.73	7.67	7.32
435	7.83	7.74	7.73	7.67	7.31
450	7.83	7.75	7.73	7.65	7.32
465	7.83	7.75	7.73	7.65	7.32
480	7.84	7.75	7.73	7.65	7.32
495	7.84	7.75	7.75	7.67	7.32
510	7.84	7.76	7.75	7.67	7.32
525	7.83	7.75	7.73	7.67	7.32
540	7.83	7.75	7.75	7.67	7.32
555	7.84	7.76	7.75	7.67	7.32
570	7.84	7.76	7.75	7.67	7.33
585	7.84	7.75	7.75	7.67	7.32
600	7.85	7.76	7.75	7.67	7.33
615	7.85	7.77	7.77	7.67	7.33
630	7.85	7.77	7.77	7.67	7.34
645	7.86	7.78	7.77	7.67	7.34
660	7.87	7.79	7.77	7.68	7.35
675	7.87	7.79	7.77	7.68	7.36
690	7.87	7.79	7.78	7.68	7.36
705	7.86	7.79	7.77	7.68	7.36
720	7.86	7.78	7.77	7.70	7.35
735	7.86	7.78	7.77	7.68	7.35
750	7.86	7.78	7.77	7.68	7.35

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
765	7.85	7.77	7.77	7.68	7.35
780	7.85	7.77	7.77	7.68	7.34
795	7.87	7.79	7.78	7.68	7.36
810	7.89	7.81	7.78	7.68	7.37
825	7.90	7.82	7.80	7.70	7.38
840	7.89	7.82	7.80	7.70	7.39
855	7.90	7.83	7.80	7.70	7.39
870	7.89	7.81	7.78	7.70	7.38
885	7.89	7.81	7.80	7.70	7.38
900	7.88	7.81	7.78	7.70	7.37
915	7.89	7.81	7.78	7.70	7.37
930	7.89	7.82	7.80	7.70	7.38
945	7.89	7.81	7.80	7.70	7.38
960	7.89	7.82	7.80	7.70	7.38
975	7.89	7.81	7.80	7.70	7.38
990	7.89	7.81	7.78	7.70	7.37
1005	7.89	7.82	7.80	7.70	7.38
1020	7.87	7.80	7.78	7.70	7.37
1035	7.87	7.80	7.78	7.68	7.37
1050	7.87	7.79	7.77	7.68	7.36
1065	7.89	7.81	7.78	7.68	7.37
1080	7.91	7.83	7.80	7.68	7.39
1095	7.92	7.85	7.80	7.70	7.40
1110	7.91	7.84	7.80	7.70	7.41
1125	7.91	7.84	7.80	7.70	7.41
1140	7.92	7.84	7.81	7.70	7.41
1155	7.90	7.83	7.80	7.70	7.41
1170	7.90	7.83	7.81	7.70	7.41
1185	7.90	7.83	7.80	7.70	7.40
1200	7.89	7.82	7.80	7.70	7.39
1215	7.91	7.83	7.81	7.70	7.39
1230	7.93	7.85	7.81	7.70	7.41
1245	7.94	7.86	7.81	7.70	7.42
1260	7.94	7.87	7.83	7.70	7.43
1275	7.95	7.88	7.83	7.71	7.44
1290	7.95	7.89	7.85	7.71	7.45
1305	7.95	7.88	7.85	7.73	7.44
1320	7.97	7.91	7.85	7.73	7.74
1335	7.99	7.93	7.86	7.73	7.48
1350	7.99	7.93	7.86	7.74	7.49
1365	7.96	7.91	7.86	7.74	7.48
1380	7.96	7.91	7.86	7.74	7.47
1395	8.00	7.93	7.88	7.76	7.50
1410	8.08	8.01	7.91	7.76	7.55
1425	8.01	7.96	7.91	7.79	7.53
1440	7.99	7.93	7.89	7.78	7.51
1455	7.98	7.93	7.89	7.78	7.50
1470	7.98	7.93	7.88	7.78	7.76
1485	8.00	7.94	7.89	7.78	7.78
1500	8.00	7.93	7.89	7.78	7.51
1515	8.00	7.94	7.89	7.78	7.51

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
1530	7.99	7.93	7.89	7.78	7.50
1545	7.98	7.92	7.89	7.78	7.77
1560	7.98	7.92	7.89	7.78	7.50
1575	7.99	7.93	7.89	7.78	7.77
1590	7.97	7.91	7.89	7.78	7.49
1605	7.97	7.91	7.89	7.78	7.76
1620	7.98	7.91	7.89	7.78	7.48
1635	7.99	7.92	7.89	7.78	7.49
1650	8.00	7.94	7.91	7.78	7.77
1665	8.00	7.94	7.91	7.78	7.78
1680	8.01	7.94	7.91	7.79	7.78
1695	8.01	7.94	7.91	7.79	7.78
1710	8.01	7.94	7.91	7.79	7.78
1725	8.01	7.94	7.91	7.79	7.78
1740	8.02	7.95	7.92	7.79	7.78
1755	8.02	7.95	7.92	7.79	7.51
1770	8.02	7.95	7.92	7.79	7.78
1785	8.03	7.96	7.92	7.79	7.79
1800	8.02	7.95	7.92	7.79	7.78
1815	8.02	7.94	7.92	7.81	7.50
1830	8.01	7.94	7.92	7.79	7.77
1845	8.00	7.93	7.92	7.79	7.77
1860	8.00	7.93	7.91	7.79	7.76
1875	8.01	7.93	7.92	7.79	7.76
1890	8.00	7.92	7.91	7.79	7.48
1905	8.03	7.94	7.92	7.79	7.76
1920	8.04	7.96	7.92	7.81	7.78
1935	8.03	7.95	7.92	7.81	7.78
1950	8.01	7.93	7.91	7.81	7.48
1965	8.01	7.93	7.92	7.81	7.48
1980	8.02	7.94	7.92	7.81	7.76
1995	8.03	7.95	7.92	7.81	7.78
2010	8.04	7.95	7.94	7.81	7.78
2025	8.05	7.97	7.94	7.81	7.79
2040	8.06	7.98	7.96	7.82	7.53
2055	8.05	7.97	7.94	7.82	7.79
2070	8.06	7.99	7.96	7.82	7.81
2085	8.06	7.98	7.96	7.82	7.81
2100	8.05	7.98	7.96	7.82	7.53
2115	8.05	7.98	7.96	7.82	7.52
2130	8.06	7.98	7.96	7.82	7.80
2145	8.06	7.99	7.96	7.84	7.53
2160	8.07	7.99	7.97	7.84	7.53
2175	8.08	8.00	7.97	7.84	7.82
2190	8.08	8.01	7.97	7.84	7.55
2205	8.07	8.00	7.97	7.86	7.55
2220	8.06	7.99	7.97	7.86	7.55
2235	8.07	7.99	7.97	7.86	7.83
2250	8.06	7.99	7.97	7.86	7.54
2265	8.08	8.00	7.97	7.86	7.55
2280	8.09	8.01	7.97	7.86	7.56

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
2295	8.09	8.01	7.99	7.86	7.56
2310	8.09	8.02	7.99	7.86	7.84
2325	8.09	8.01	7.99	7.86	7.83
2340	8.10	8.02	7.99	7.87	7.85
2355	8.10	8.03	7.99	7.87	7.57
2370	8.09	8.02	7.99	7.87	7.84
2385	8.10	8.02	7.99	7.87	7.85
2400	8.09	8.02	7.99	7.87	7.84
2415	8.09	8.01	7.99	7.87	7.84
2430	8.07	8.00	7.97	7.86	7.83
2445	8.06	7.98	7.97	7.87	7.81
2460	8.05	7.96	7.96	7.86	7.79
2475	8.06	7.98	7.97	7.86	7.80
2490	8.06	7.98	7.97	7.86	7.53
2505	8.08	8.00	7.97	7.86	7.54
2520	8.08	8.00	7.99	7.86	7.82
2535	8.07	7.99	7.97	7.86	7.81
2550	8.08	7.99	7.97	7.86	7.81
2565	8.07	7.99	7.97	7.86	7.81
2580	8.08	8.00	7.97	7.86	7.82
2595	8.07	7.99	7.97	7.86	7.81
2610	8.08	8.00	7.97	7.86	7.82
2625	8.07	7.99	7.97	7.86	7.81
2640	8.05	7.97	7.96	7.86	7.79
2655	8.04	7.95	7.96	7.86	7.78
2670	8.06	7.97	7.96	7.84	7.79
2685	8.08	7.99	7.97	7.84	7.80
2700	8.09	8.00	7.97	7.86	7.54
2715	8.07	7.99	7.97	7.86	7.80
2730	8.07	7.99	7.97	7.86	7.81
2745	8.08	7.99	7.97	7.86	7.80
2760	8.07	7.99	7.97	7.86	7.80
2775	8.06	7.97	7.97	7.86	7.79
2790	8.08	7.99	7.97	7.86	7.80
2805	8.07	7.98	7.97	7.86	7.80
2820	8.07	7.98	7.97	7.86	7.79
2835	8.06	7.98	7.97	7.86	7.79
2850	8.10	8.01	7.99	7.86	7.81
2865	8.12	8.03	8.00	7.87	7.83
2880	8.07	7.99	7.97	7.87	7.80
2895	8.11	8.02	8.00	7.87	7.83
2910	8.09	8.00	8.00	7.87	7.83
2925	8.11	8.02	8.00	7.87	7.55
2940	8.09	8.01	8.00	7.89	7.83
2955	8.05	7.97	7.97	7.87	7.80
2970	8.08	7.99	7.99	7.87	7.81
2985	8.11	8.02	8.00	7.89	7.83
3000	8.09	8.00	7.99	7.89	7.81
3015	8.09	8.00	7.99	7.89	7.81
3030	8.11	8.03	8.00	7.89	7.83
3045	8.14	8.05	8.02	7.89	7.85

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
3060	8.11	8.02	8.02	7.90	7.84
3075	8.09	8.00	7.99	7.90	7.83
3090	8.06	7.98	7.99	7.89	7.81
3105	8.10	8.01	8.00	7.89	7.55
3120	8.07	7.99	7.99	7.89	7.53
3135	8.05	7.96	7.99	7.89	7.79
3150	8.05	7.96	7.97	7.87	7.79
3165	8.09	7.99	7.99	7.87	7.81
3180	8.09	8.00	7.99	7.87	7.81
3195	8.07	7.98	7.99	7.87	7.80
3210	8.06	7.97	7.99	7.87	7.79
3225	8.09	7.99	7.99	7.87	7.80
3240	8.07	7.98	7.99	7.87	7.80
3255	8.11	8.02	8.00	7.87	7.55
3270	8.10	8.00	8.00	7.89	7.82
3285	8.13	8.03	8.00	7.89	7.56
3300	8.09	8.00	8.00	7.89	7.55
3315	8.09	8.00	7.99	7.89	7.82
3330	8.10	8.01	8.00	7.89	7.55
3345	8.08	7.99	7.99	7.89	7.80
3360	8.08	7.99	7.99	7.89	7.81
3375	8.08	7.99	7.99	7.89	7.81
3390	8.09	8.00	8.00	7.89	7.81
3405	8.09	8.00	8.00	7.89	7.81
3420	8.09	8.00	8.00	7.89	7.53
3435	8.11	8.02	8.00	7.89	7.83
3450	8.13	8.04	8.02	7.90	7.57
3465	8.12	8.03	8.00	7.90	7.57
3480	8.15	8.06	8.02	7.90	7.85
3495	8.13	8.04	8.02	7.90	7.58
3510	8.13	8.04	8.02	7.92	7.57
3525	8.14	8.05	8.02	7.92	7.59
3540	8.13	8.04	8.02	7.92	7.58
3555	8.11	8.03	8.02	7.92	7.85
3570	8.13	8.04	8.02	7.92	7.85
3585	8.16	8.07	8.04	7.92	7.86
3600	8.15	8.06	8.04	7.92	7.59
3615	8.15	8.06	8.04	7.93	7.59
3630	8.16	8.07	8.04	7.93	7.88
3645	8.19	8.11	8.07	7.95	7.63
3660	8.18	8.10	8.07	7.95	7.64
3675	8.16	8.08	8.07	7.95	7.62
3690	8.16	8.07	8.05	7.95	7.61
3705	8.15	8.07	8.05	7.95	7.60
3720	8.13	8.05	8.04	7.95	7.59
3735	8.14	8.05	8.05	7.95	7.59
3750	8.15	8.06	8.05	7.95	7.60
3765	8.15	8.07	8.05	7.95	7.60
3780	8.14	8.06	8.05	7.95	7.59
3795	8.15	8.06	8.05	7.95	7.59
3810	8.16	8.07	8.05	7.95	7.60

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
3825	8.16	8.07	8.05	7.95	7.60
3840	8.14	8.05	8.05	7.95	7.60
3855	8.15	8.07	8.05	7.95	7.60
3870	8.16	8.07	8.07	7.95	7.61
3885	8.16	8.07	8.05	7.95	7.88
3900	8.17	8.08	8.07	7.97	7.62
3915	8.18	8.09	8.07	7.95	7.63
3930	8.19	8.11	8.08	7.97	7.64
3945	8.18	8.10	8.07	7.97	7.64
3960	8.19	8.11	8.07	7.97	7.64
3975	8.18	8.10	8.07	7.97	7.63
3990	8.20	8.12	8.08	7.98	7.65
4005	8.21	8.13	8.08	7.98	7.93
4020	8.20	8.12	8.08	7.98	7.64
4035	8.19	8.11	8.08	7.98	7.65
4050	8.20	8.12	8.08	7.98	7.64
4065	8.19	8.11	8.08	7.98	7.64
4080	8.19	8.11	8.08	7.98	7.64
4095	8.20	8.12	8.08	7.98	7.64
4110	8.21	8.12	8.08	7.98	7.65
4125	8.21	8.13	8.10	7.98	7.65
4140	8.20	8.12	8.08	7.98	7.65
4155	8.23	8.14	8.10	8.00	7.67
4170	8.23	8.14	8.10	8.00	7.67
4185	8.24	8.15	8.12	8.00	7.68
4200	8.24	8.15	8.12	8.00	7.68
4215	8.24	8.16	8.12	8.01	7.68
4230	8.23	8.15	8.12	8.01	7.69
4245	8.23	8.14	8.12	8.01	7.95
4260	8.22	8.14	8.10	8.01	7.67
4275	8.22	8.13	8.12	8.01	7.67
4290	8.22	8.14	8.12	8.01	7.67
4305	8.22	8.13	8.10	8.01	7.67
4320	8.21	8.13	8.10	8.01	7.93
4335	8.22	8.13	8.12	8.01	7.66
4350	8.21	8.12	8.10	8.01	7.65
4365	8.22	8.13	8.12	8.01	7.67
4380	8.22	8.13	8.12	8.01	7.65
4395	8.22	8.13	8.12	8.01	7.66
4410	8.23	8.13	8.12	8.01	7.65
4425	8.23	8.13	8.12	8.01	7.67
4440	8.23	8.14	8.13	8.03	7.67
4455	8.24	8.14	8.13	8.03	7.67
4470	8.24	8.14	8.12	8.03	7.93
4485	8.23	8.14	8.12	8.03	7.94
4500	8.23	8.13	8.12	8.03	7.67
4515	8.23	8.13	8.12	8.03	7.66
4530	8.24	8.14	8.13	8.03	7.66
4545	8.24	8.14	8.13	8.03	7.66
4560	8.24	8.14	8.13	8.03	7.66
4575	8.25	8.14	8.13	8.05	7.95

RAYMARK INDUSTRIES, INC
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
4590	8.24	8.14	8.13	8.03	7.66
4605	8.23	8.13	8.13	8.03	7.66
4620	8.24	8.14	8.13	8.03	7.66
4635	8.23	8.13	8.13	8.03	7.65
4650	8.23	8.12	8.12	8.03	7.65
4665	8.23	8.13	8.12	8.03	7.65
4680	8.23	8.13	8.12	8.03	7.92
4695	8.24	8.14	8.13	8.03	7.65
4710	8.25	8.15	8.13	8.03	7.67
4725	8.24	8.13	8.13	8.05	7.66
4740	8.25	8.15	8.13	8.03	7.66
4755	8.25	8.15	8.13	8.05	7.67
4770	8.25	8.14	8.13	8.05	7.66
4785	8.25	8.15	8.13	8.05	7.67
4800	8.25	8.15	8.13	8.05	7.67
4815	8.26	8.16	8.15	8.05	7.67
4830	8.27	8.16	8.15	8.05	7.68
4845	8.26	8.16	8.15	8.05	7.68
4860	8.28	8.17	8.15	8.05	7.69
4875	8.27	8.17	8.15	8.06	7.69
4890	8.27	8.17	8.15	8.06	7.69
4905	8.26	8.16	8.15	8.06	7.69
4920	8.26	8.16	8.15	8.06	7.69
4935	8.27	8.17	8.15	8.06	7.69
4950	8.26	8.16	8.15	8.06	7.68
4965	8.26	8.17	8.15	8.06	7.69
4980	8.26	8.16	8.15	8.06	7.68
4995	8.27	8.17	8.16	8.06	7.68
5010	8.28	8.18	8.16	8.06	7.69
5025	8.29	8.19	8.18	8.08	7.70
5040	8.29	8.19	8.18	8.08	7.71
5055	8.29	8.20	8.18	8.08	7.71
5070	8.29	8.20	8.18	8.08	7.71
5085	8.30	8.20	8.18	8.09	7.72
5100	8.30	8.20	8.20	8.09	7.72
5115	8.29	8.20	8.20	8.09	7.72
5130	8.30	8.20	8.18	8.09	7.72
5145	8.30	8.21	8.20	8.09	7.72
5160	8.30	8.20	8.20	8.09	7.72
5175	8.30	8.20	8.20	8.09	7.72
5190	8.30	8.20	8.20	8.11	7.73
5205	8.29	8.20	8.18	8.11	7.72
5220	8.29	8.20	8.20	8.11	7.72
5235	8.29	8.20	8.20	8.11	7.72
5250	8.29	8.20	8.20	8.11	7.72
5265	8.28	8.19	8.18	8.11	7.72
5280	8.28	8.19	8.18	8.11	7.71
5295	8.28	8.19	8.18	8.11	7.71
5310	8.28	8.19	8.20	8.11	7.71
5325	8.28	8.19	8.18	8.11	7.71
5340	8.28	8.18	8.18	8.11	7.71

RAYMARK INDUSTRIES, INC
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS
 PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
5355	8.28	8.19	8.18	8.11	7.71
5370	8.28	8.19	8.18	8.11	7.71
5385	8.28	8.19	8.20	8.11	7.71
5400	8.28	8.19	8.20	8.11	7.71
5415	8.28	8.19	8.20	8.11	7.71
5430	8.29	8.19	8.20	8.11	7.71
5445	8.29	8.20	8.20	8.11	7.72
5460	8.29	8.20	8.20	8.11	8.00
5475	8.30	8.20	8.20	8.11	8.00
5490	8.29	8.20	8.20	8.11	8.00
5505	8.29	8.20	8.20	8.11	7.72
5520	8.30	8.20	8.20	8.11	8.00
5535	8.30	8.21	8.20	8.11	8.00
5550	8.31	8.22	8.21	8.11	8.01
5565	8.31	8.22	8.21	8.12	8.02
5580	8.31	8.22	8.21	8.12	8.02
5595	8.32	8.22	8.21	8.12	8.02
5610	8.32	8.22	8.21	8.12	8.02
5625	8.32	8.22	8.21	8.12	8.02
5640	8.31	8.22	8.21	8.12	8.02
5655	8.32	8.23	8.21	8.12	8.02
5670	8.32	8.23	8.21	8.12	8.02
5685	8.33	8.23	8.21	8.14	8.03
5700	8.33	8.24	8.23	8.14	7.76
5715	8.33	8.24	8.23	8.14	8.04
5730	8.33	8.24	8.23	8.14	8.04
5745	8.33	8.24	8.23	8.14	8.04
5760	8.33	8.24	8.23	8.14	8.04
5775	8.33	8.24	8.23	8.16	8.04
5790	8.33	8.24	8.23	8.14	8.04
5805	8.34	8.24	8.23	8.16	8.04
5820	8.33	8.24	8.23	8.16	7.76
5835	8.33	8.24	8.23	8.16	8.04
5850	8.33	8.24	8.23	8.16	8.04
5865	8.33	8.24	8.24	8.16	8.04
5880	8.33	8.24	8.24	8.17	8.04
5895	8.33	8.24	8.24	8.17	8.04
5910	8.33	8.24	8.24	8.17	8.05
5925	8.33	8.24	8.24	8.17	8.04
5940	8.33	8.24	8.24	8.17	8.04
5955	8.32	8.23	8.24	8.17	8.04
5970	8.32	8.23	8.24	8.17	8.04
5985	8.32	8.23	8.24	8.17	8.04
6000	8.32	8.23	8.24	8.17	7.76
6015	8.31	8.22	8.24	8.17	8.03
6030	8.31	8.22	8.24	8.17	7.75
6045	8.31	8.22	8.24	8.17	8.03
6060	8.31	8.21	8.24	8.17	7.75
6075	8.30	8.21	8.24	8.17	8.02
6090	8.30	8.20	8.24	8.17	7.74
6105	8.29	8.20	8.23	8.17	7.74

RAYMARK INDUSTRIES, INC
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
6120	8.28	8.19	8.23	8.16	7.72
6135	8.29	8.19	8.23	8.16	8.01
6150	8.28	8.19	8.24	8.16	7.72
6165	8.28	8.19	8.23	8.16	7.73
6180	8.28	8.19	8.23	8.16	7.73
6195	8.29	8.19	8.23	8.17	8.00
6210	8.29	8.20	8.24	8.16	7.73
6225	8.30	8.20	8.24	8.16	7.74
6240	8.30	8.20	8.24	8.17	7.74
6255	8.31	8.21	8.24	8.17	7.74
6270	8.31	8.22	8.24	8.17	7.75
6285	8.32	8.22	8.26	8.17	7.76
6300	8.32	8.22	8.26	8.17	7.76
6315	8.33	8.23	8.26	8.19	7.76
6330	8.33	8.23	8.26	8.17	7.76
6345	8.33	8.24	8.26	8.17	7.77
6360	8.33	8.24	8.26	8.19	7.78
6375	8.34	8.25	8.26	8.19	7.78
6390	8.34	8.26	8.27	8.19	7.79
6405	8.34	8.25	8.27	8.19	7.79
6420	8.34	8.26	8.27	8.20	7.79
6435	8.34	8.26	8.27	8.20	7.79
6450	8.34	8.26	8.27	8.20	7.79
6465	8.35	8.26	8.27	8.20	7.79
6480	8.35	8.27	8.27	8.20	7.80
6495	8.36	8.27	8.27	8.20	7.80
6510	8.36	8.28	8.29	8.20	7.81
6525	8.37	8.28	8.29	8.22	7.81
6540	8.37	8.28	8.29	8.22	7.82
6555	8.37	8.28	8.29	8.22	7.82
6570	8.37	8.28	8.29	8.22	7.83
6585	8.36	8.28	8.29	8.24	7.81
6600	8.36	8.27	8.29	8.22	7.81
6615	8.35	8.27	8.29	8.24	7.81
6630	8.35	8.27	8.29	8.22	7.81
6645	8.35	8.27	8.29	8.22	7.81
6660	8.35	8.27	8.29	8.24	7.81
6675	8.35	8.26	8.29	8.22	7.81
6690	8.34	8.26	8.29	8.22	7.80
6705	8.34	8.26	8.29	8.22	7.80
6720	8.34	8.25	8.27	8.22	7.80
6735	8.33	8.25	8.27	8.22	7.79
6750	8.33	8.25	8.27	8.22	7.79
6765	8.34	8.25	8.27	8.22	7.79
6780	8.34	8.26	8.27	8.22	7.80
6795	8.34	8.25	8.27	8.22	7.79
6810	8.34	8.25	8.27	8.22	7.79
6825	8.34	8.26	8.27	8.22	7.79
6840	8.34	8.26	8.27	8.22	7.79
6855	8.34	8.26	8.27	8.22	7.79
6870	8.35	8.26	8.29	8.22	7.80

RAYMARK INDUSTRIES, INC
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
6885	8.35	8.26	8.29	8.22	7.80
6900	8.35	8.27	8.29	8.22	7.81
6915	8.35	8.27	8.29	8.22	8.09
6930	8.36	8.27	8.29	8.22	7.81
6945	8.36	8.27	8.29	8.22	7.81
6960	8.36	8.28	8.29	8.22	8.09
6975	8.37	8.29	8.29	8.22	8.10
6990	8.38	8.30	8.29	8.22	8.83
7005	8.38	8.30	8.31	8.22	8.11
7020	8.38	8.30	8.29	8.24	8.11
7035	8.39	8.31	8.31	8.24	8.12
7050	8.40	8.32	8.31	8.24	8.13
7065	8.40	8.32	8.31	8.24	8.13
7080	8.40	8.33	8.31	8.25	8.14
7095	8.40	8.33	8.32	8.25	8.14
7110	8.40	8.33	8.32	8.25	8.15
7125	8.41	8.33	8.31	8.25	8.14
7140	8.41	8.33	8.32	8.25	8.15
7155	8.41	8.34	8.32	8.25	8.15
7170	8.42	8.34	8.32	8.25	8.15
7185	8.42	8.34	8.32	8.27	8.16
7200	8.42	8.34	8.32	8.25	8.16
7215	8.42	8.35	8.32	8.27	8.16
7230	8.43	8.36	8.34	8.27	8.17
7245	8.43	8.35	8.34	8.27	8.17
7260	8.43	8.36	8.34	8.27	7.88
7275	8.44	8.36	8.34	8.28	8.18
7290	8.43	8.35	8.34	8.28	8.18
7305	8.42	8.35	8.34	8.28	8.17
7320	8.43	8.35	8.34	8.28	8.17
7335	8.43	8.35	8.34	8.28	8.18
7350	8.42	8.35	8.34	8.28	8.17
7365	8.42	8.34	8.34	8.28	8.16
7380	8.42	8.34	8.35	8.28	8.17
7395	8.42	8.34	8.34	8.28	8.17
7410	8.42	8.34	8.34	8.28	8.16
7425	8.42	8.34	8.34	8.28	8.16
7440	8.42	8.34	8.34	8.28	8.16
7455	8.42	8.34	8.34	8.28	8.16
7470	8.42	8.34	8.34	8.28	8.16
7485	8.42	8.34	8.34	8.28	8.16
7500	8.42	8.34	8.34	8.28	8.16
7515	8.41	8.33	8.34	8.28	8.16
7530	8.41	8.33	8.34	8.30	8.16
7545	8.41	8.33	8.34	8.28	7.88
7560	8.41	8.33	8.34	8.28	7.87
7575	8.41	8.33	8.34	8.28	8.15
7590	8.41	8.33	8.35	8.28	7.87
7605	8.41	8.33	8.34	8.28	7.88
7620	8.40	8.32	8.34	8.28	7.88
7635	8.40	8.32	8.34	8.28	7.86

RAYMARK INDUSTRIES, INC
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
7650	8.41	8.33	8.34	8.28	7.87
7665	8.41	8.33	8.34	8.28	7.88
7680	8.41	8.33	8.34	8.30	7.88
7695	8.41	8.33	8.34	8.28	8.16
7710	8.42	8.34	8.34	8.28	7.88
7725	8.42	8.34	8.34	8.28	7.88
7740	8.42	8.34	8.34	8.28	7.90
7755	8.43	8.35	8.34	8.30	8.17
7770	8.44	8.36	8.35	8.30	7.90
7785	8.44	8.36	8.35	8.30	7.90
7800	8.45	8.37	8.35	8.30	7.91
7815	8.45	8.37	8.35	8.31	8.20
7830	8.45	8.37	8.35	8.30	7.92
7845	8.45	8.38	8.35	8.30	7.92
7860	8.45	8.38	8.35	8.31	8.20
7875	8.45	8.38	8.35	8.31	7.92
7890	8.45	8.38	8.35	8.31	7.92
7905	8.45	8.38	8.37	8.31	8.21
7920	8.45	8.38	8.37	8.31	7.93
7935	8.45	8.38	8.37	8.31	7.92
7950	8.46	8.38	8.37	8.31	7.93
7965	8.46	8.38	8.37	8.31	8.21
7980	8.46	8.39	8.37	8.31	8.22
7995	8.47	8.39	8.37	8.33	7.93
8010	8.46	8.39	8.37	8.33	7.94
8025	8.46	8.39	8.37	8.33	7.93
8040	8.46	8.39	8.37	8.33	8.22
8055	8.46	8.39	8.37	8.33	7.95
8070	8.46	8.39	8.37	8.33	7.93
8085	8.45	8.38	8.37	8.33	8.21
8100	8.45	8.38	8.35	8.31	8.21
8115	8.45	8.37	8.35	8.33	7.92
8130	8.44	8.37	8.35	8.31	7.92
8145	8.43	8.36	8.35	8.31	7.91
8160	8.43	8.36	8.35	8.31	7.92
8175	8.43	8.35	8.35	8.31	7.90
8190	8.42	8.34	8.34	8.31	7.90
8205	8.42	8.34	8.34	8.31	7.90
8220	8.42	8.34	8.34	8.31	8.19
8235	8.42	8.34	8.34	8.30	7.90
8250	8.42	8.34	8.34	8.30	7.90
8265	8.42	8.35	8.34	8.30	7.90
8280	8.43	8.35	8.34	8.30	7.90
8295	8.43	8.35	8.34	8.30	7.90
8310	8.43	8.36	8.34	8.30	7.90
8325	8.43	8.35	8.34	8.30	8.19
8340	8.43	8.35	8.34	8.30	8.18
8355	8.44	8.36	8.34	8.30	8.19
8370	8.44	8.37	8.34	8.30	8.19
8385	8.44	8.37	8.34	8.31	8.19
8400	8.44	8.37	8.34	8.30	8.20

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
8415	8.45	8.38	8.34	8.31	8.20
8430	8.45	8.37	8.34	8.31	8.97
8445	8.45	8.38	8.34	8.31	9.05
8460	8.45	8.38	8.34	8.31	7.92
8475	8.46	8.38	8.34	8.31	7.90
8490	8.46	8.38	8.34	8.31	8.21
8505	8.45	8.38	8.34	8.31	7.92
8520	8.46	8.38	8.35	8.31	7.92
8535	8.46	8.38	8.34	8.31	8.21
8550	8.46	8.39	8.34	8.31	9.05
8565	8.46	8.39	8.34	8.31	8.92
8580	8.46	8.39	8.34	8.31	9.09
8595	8.47	8.39	8.35	8.31	9.08
8610	8.47	8.39	8.34	8.31	8.98
8625	8.47	8.40	8.35	8.31	7.93
8640	8.47	8.39	8.35	8.31	8.90
8655	8.47	8.39	8.34	8.31	8.22
8670	8.46	8.39	8.34	8.31	8.22
8685	8.46	8.39	8.34	8.31	8.22
8700	8.46	8.39	8.34	8.31	8.22
8715	8.46	8.39	8.34	8.31	8.22
8730	8.46	8.39	8.34	8.31	8.22
8745	8.46	8.39	8.34	8.31	8.22
8760	8.46	8.38	8.34	8.31	8.22
8775	8.46	8.39	8.35	8.31	8.23
8790	8.46	8.38	8.34	8.31	8.21
8805	8.45	8.38	8.32	8.31	8.21
8820	8.45	8.37	8.34	8.31	8.21
8835	8.45	8.37	8.34	8.31	8.20
8850	8.45	8.36	8.32	8.30	8.20
8865	8.44	8.36	8.32	8.30	8.20
8880	8.43	8.35	8.32	8.30	8.19
8895	8.43	8.35	8.32	8.30	9.08
8910	8.42	8.34	8.32	8.30	8.97
8925	8.41	8.33	8.31	8.28	8.17
8940	8.41	8.33	8.31	8.28	8.17
8955	8.41	8.33	8.31	8.28	8.16
8970	8.41	8.32	8.31	8.28	8.16
8985	8.40	8.32	8.31	8.27	8.16
9000	8.40	8.32	8.31	8.28	8.16
9015	8.39	8.31	8.29	8.28	7.87
9030	8.39	8.30	8.29	8.27	8.15
9045	8.39	8.30	8.29	8.27	8.15
9060	8.39	8.30	8.29	8.27	8.15
9075	8.39	8.30	8.29	8.27	8.15
9090	8.39	8.30	8.29	8.27	8.15
9105	8.39	8.30	8.27	8.27	8.15
9120	8.39	8.30	8.27	8.27	7.86
9135	8.39	8.30	8.27	8.27	7.86
9150	8.39	8.30	8.27	8.25	7.86
9165	8.39	8.30	8.27	8.25	8.15

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
9180	8.39	8.30	8.27	8.25	7.87
9195	8.39	8.30	8.27	8.25	7.86
9210	8.38	8.30	8.26	8.25	8.15
9225	8.37	8.29	8.27	8.24	7.86
9240	8.37	8.29	8.26	8.25	7.86
9255	8.37	8.28	8.26	8.24	7.85
9270	8.37	8.29	8.26	8.24	7.85
9285	8.37	8.28	8.26	8.24	8.13
9300	8.37	8.28	8.26	8.24	8.13
9315	8.37	8.28	8.26	8.24	8.13
9330	8.37	8.29	8.26	8.24	7.85
9345	8.38	8.29	8.26	8.24	7.86
9360	8.38	8.30	8.26	8.24	8.13
9375	8.38	8.30	8.26	8.24	7.86
9390	8.38	8.29	8.26	8.24	8.14
9405	8.38	8.30	8.26	8.24	7.85
9420	8.37	8.29	8.26	8.24	7.86
9435	8.38	8.29	8.24	8.24	8.13
9450	8.37	8.29	8.24	8.24	7.85
9465	8.37	8.28	8.24	8.24	8.13
9480	8.36	8.28	8.24	8.22	8.13
9495	8.36	8.27	8.24	8.22	7.84
9510	8.36	8.27	8.24	8.22	7.85
9525	8.36	8.27	8.24	8.22	8.12
9540	8.35	8.27	8.23	8.22	7.84
9555	8.35	8.27	8.24	8.22	8.11
9570	8.35	8.26	8.23	8.22	7.83
9585	8.35	8.26	8.24	8.22	8.11
9600	8.34	8.26	8.23	8.22	7.83
9615	8.34	8.26	8.23	8.22	7.83
9630	8.34	8.26	8.23	8.22	8.10
9645	8.33	8.25	8.23	8.20	7.82
9660	8.33	8.24	8.21	8.20	8.09
9675	8.34	8.25	8.21	8.20	8.10
9690	8.34	8.25	8.21	8.20	7.82
9705	8.33	8.25	8.21	8.20	7.81
9720	8.33	8.25	8.21	8.20	8.09
9735	8.34	8.25	8.21	8.20	7.81
9750	8.33	8.25	8.21	8.20	7.81
9765	8.33	8.25	8.21	8.20	7.81
9780	8.33	8.25	8.21	8.20	7.81
9795	8.34	8.26	8.21	8.20	8.09
9810	8.34	8.26	8.21	8.20	8.10
9825	8.34	8.25	8.21	8.20	8.09
9840	8.34	8.25	8.21	8.19	8.09
9855	8.34	8.25	8.21	8.19	8.09
9870	8.34	8.26	8.21	8.19	8.09
9885	8.34	8.26	8.21	8.20	7.82
9900	8.34	8.26	8.21	8.19	8.10
9915	8.35	8.27	8.21	8.20	8.11
9930	8.36	8.28	8.23	8.19	8.11

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
9945	8.37	8.29	8.21	8.20	8.12
9960	8.38	8.30	8.23	8.20	8.13
9975	8.38	8.30	8.23	8.20	8.13
9990	8.39	8.31	8.23	8.20	8.13
10005	8.39	8.31	8.23	8.20	8.14
10020	8.39	8.31	8.23	8.20	8.15
10035	8.40	8.32	8.23	8.22	8.15
10050	8.40	8.32	8.23	8.20	8.15
10065	8.40	8.32	8.23	8.22	8.15
10080	8.40	8.33	8.23	8.22	8.15
10095	8.40	8.33	8.23	8.22	8.16
10110	8.41	8.33	8.23	8.22	8.16
10125	8.41	8.33	8.23	8.22	8.16
10140	8.41	8.34	8.23	8.22	8.16
10155	8.41	8.34	8.23	8.22	8.16
10170	8.41	8.34	8.23	8.22	8.16
10185	8.42	8.34	8.23	8.22	8.16
10200	8.42	8.34	8.23	8.22	8.17
10215	8.42	8.34	8.24	8.22	8.18
10230	8.42	8.35	8.24	8.22	8.18
10245	8.42	8.34	8.24	8.22	8.18
10260	8.42	8.35	8.24	8.22	8.18
10275	8.42	8.35	8.24	8.22	7.90
10290	8.42	8.35	8.24	8.22	7.90
10305	8.43	8.35	8.23	8.22	7.90
10320	8.43	8.35	8.24	8.24	8.18
10335	8.43	8.35	8.24	8.22	8.18
10350	8.43	8.35	8.23	8.24	7.90
10365	8.43	8.35	8.24	8.22	7.90
10380	8.43	8.35	8.24	8.24	7.91
10395	8.42	8.35	8.24	8.24	7.90
10410	8.42	8.35	8.23	8.24	7.90
10425	8.43	8.35	8.23	8.22	7.90
10440	8.42	8.34	8.23	8.24	8.18
10455	8.42	8.34	8.23	8.22	7.90
10470	8.42	8.35	8.23	8.22	8.18
10485	8.43	8.36	8.24	8.22	7.91
10500	8.44	8.36	8.24	8.24	7.91
10515	8.44	8.36	8.24	8.24	7.92
10530	8.44	8.36	8.24	8.24	7.91
10545	8.44	8.37	8.24	8.24	7.92
10560	8.45	8.37	8.24	8.24	7.92
10575	8.45	8.38	8.24	8.24	8.20
10590	8.46	8.38	8.24	8.24	7.93
10605	8.46	8.39	8.26	8.24	7.94
10620	8.46	8.39	8.26	8.24	8.22
10635	8.46	8.39	8.26	8.25	8.22
10650	8.47	8.39	8.26	8.25	7.94
10665	8.46	8.39	8.24	8.25	7.93
10680	8.46	8.39	8.26	8.25	7.94
10695	8.46	8.39	8.24	8.25	7.94

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
10710	8.46	8.39	8.26	8.25	7.94
10725	8.46	8.39	8.26	8.25	7.94
10740	8.46	8.39	8.24	8.24	8.22
10755	8.46	8.39	8.24	8.24	8.22
10770	8.47	8.40	8.26	8.25	7.94
10785	8.48	8.40	8.26	8.24	8.23
10800	8.48	8.41	8.26	8.25	7.95
10815	8.49	8.42	8.26	8.25	7.97
10830	8.49	8.41	8.26	8.25	8.24
10845	8.49	8.42	8.26	8.25	7.97
10860	8.48	8.41	8.26	8.25	7.96
10875	8.49	8.42	8.26	8.25	7.96
10890	8.50	8.42	8.26	8.25	7.97
10905	8.50	8.43	8.26	8.27	7.97
10920	8.50	8.43	8.27	8.25	7.97
10935	8.50	8.43	8.26	8.27	7.97
10950	8.49	8.42	8.26	8.27	7.97
10965	8.49	8.42	8.27	8.27	7.97
10980	8.49	8.42	8.26	8.27	7.97
10995	8.49	8.42	8.26	8.27	7.97
11010	8.49	8.41	8.26	8.25	7.96
11025	8.48	8.41	8.26	8.25	7.97
11040	8.49	8.41	8.26	8.25	7.97
11055	8.48	8.41	8.26	8.25	7.96
11070	8.49	8.41	8.26	8.25	8.25
11085	8.49	8.42	8.26	8.27	7.96
11100	8.47	8.40	8.24	8.25	7.95
11115	8.48	8.41	8.24	8.25	7.96
11130	8.47	8.40	8.26	8.25	7.95
11145	8.47	8.40	8.24	8.25	8.23
11160	8.48	8.41	8.24	8.25	7.96
11175	8.48	8.41	8.24	8.25	7.96
11190	8.49	8.42	8.24	8.25	8.25
11205	8.48	8.41	8.24	8.25	8.24
11220	8.48	8.41	8.26	8.25	8.24
11235	8.49	8.41	8.24	8.25	7.95
11250	8.48	8.41	8.24	8.25	8.23
11265	8.48	8.40	8.24	8.25	8.23
11280	8.48	8.41	8.24	8.24	8.23
11295	8.49	8.42	8.24	8.25	8.24
11310	8.49	8.42	8.24	8.25	8.24
11325	8.48	8.41	8.24	8.25	8.24
11340	8.48	8.41	8.24	8.25	8.24
11355	8.50	8.42	8.24	8.25	8.99
11370	8.51	8.43	8.26	8.25	8.25
11385	8.51	8.44	8.26	8.25	8.25
11400	8.52	8.45	8.26	8.25	8.27
11415	8.51	8.44	8.26	8.25	8.27
11430	8.51	8.44	8.26	8.25	8.27
11445	8.51	8.44	8.26	8.25	8.26
11460	8.51	8.44	8.26	8.25	8.26

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
11475	8.51	8.44	8.26	8.25	8.27
11490	8.51	8.44	8.26	8.25	9.04
11505	8.51	8.44	8.26	8.27	7.98
11520	8.51	8.44	8.26	8.25	8.27
11535	8.51	8.44	8.26	8.27	7.98
11550	8.50	8.43	8.24	8.25	7.97
11565	8.51	8.44	8.24	8.25	8.26
11580	8.51	8.43	8.24	8.25	8.26
11595	8.51	8.43	8.24	8.25	8.26
11610	8.51	8.43	8.24	8.25	8.26
11625	8.51	8.43	8.24	8.25	8.26
11640	8.53	8.45	8.24	8.25	8.27
11655	8.53	8.46	8.26	8.25	8.28
11670	8.51	8.44	8.24	8.25	8.27
11685	8.52	8.45	8.26	8.27	8.28
11700	8.50	8.43	8.24	8.25	8.27
11715	8.50	8.43	8.24	8.25	8.26
11730	8.50	8.42	8.24	8.25	8.25
11745	8.49	8.41	8.23	8.25	8.25
11760	8.49	8.41	8.23	8.24	8.24
11775	8.50	8.42	8.23	8.24	7.97
11790	8.49	8.42	8.23	8.24	8.25
11805	8.49	8.41	8.23	8.24	8.25
11820	8.49	8.41	8.23	8.24	8.25
11835	8.49	8.41	8.23	8.25	8.25
11850	8.49	8.41	8.23	8.24	8.25
11865	8.47	8.39	8.21	8.24	8.23
11880	8.46	8.39	8.21	8.24	8.23
11895	8.47	8.40	8.23	8.24	8.23
11910	8.46	8.39	8.21	8.24	8.22
11925	8.44	8.36	8.20	8.22	8.21
11940	8.44	8.36	8.20	8.22	8.20
11955	8.45	8.37	8.20	8.22	8.20
11970	8.45	8.37	8.20	8.22	8.21
11985	8.45	8.37	8.20	8.22	8.20
12000	8.44	8.36	8.20	8.22	8.20
12015	8.46	8.38	8.21	8.22	8.22
12030	8.46	8.39	8.21	8.22	8.22
12045	8.43	8.35	8.20	8.20	8.19
12060	8.46	8.38	8.20	8.20	8.20
12075	8.47	8.39	8.21	8.22	8.22
12090	8.45	8.37	8.20	8.22	8.22
12105	8.46	8.38	8.21	8.22	8.22
12120	8.46	8.38	8.21	8.22	8.22
12135	8.47	8.39	8.21	8.22	8.22
12150	8.46	8.39	8.20	8.22	8.22
12165	8.47	8.39	8.21	8.22	8.22
12180	8.47	8.39	8.21	8.22	8.23
12195	8.48	8.40	8.21	8.22	8.23
12210	8.47	8.40	8.21	8.22	8.23
12225	8.48	8.40	8.21	8.22	8.23

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
12240	8.47	8.40	8.21	8.22	8.23
12255	8.47	8.40	8.21	8.22	8.23
12270	8.47	8.39	8.20	8.22	8.22
12285	8.45	8.38	8.20	8.22	8.22
12300	8.45	8.37	8.20	8.20	8.21
12315	8.45	8.37	8.18	8.20	8.20
12330	8.44	8.36	8.18	8.20	8.20
12345	8.45	8.37	8.18	8.20	8.20
12360	8.44	8.36	8.18	8.20	8.20
12375	8.43	8.35	8.18	8.19	8.19
12390	8.43	8.35	8.18	8.19	8.20
12405	8.43	8.34	8.18	8.19	8.18
12420	8.41	8.33	8.16	8.19	8.18
12435	8.41	8.33	8.16	8.19	8.17
12450	8.41	8.33	8.16	8.17	8.17
12465	8.40	8.32	8.15	8.19	8.16
12480	8.40	8.32	8.15	8.17	8.16
12495	8.40	8.31	8.15	8.17	8.16
12510	8.40	8.32	8.15	8.17	8.16
12525	8.40	8.32	8.15	8.17	8.16
12540	8.40	8.31	8.15	8.17	8.15
12555	8.40	8.32	8.15	8.17	8.16
12570	8.40	8.32	8.15	8.17	8.16
12585	8.39	8.31	8.15	8.17	8.16
12600	8.39	8.31	8.15	8.16	8.16
12615	8.40	8.31	8.15	8.17	8.15
12630	8.40	8.33	8.15	8.17	8.16
12645	8.40	8.32	8.15	8.17	8.16
12660	8.40	8.32	8.15	8.17	8.16
12675	8.40	8.32	8.15	8.16	8.15
12690	8.40	8.32	8.15	8.16	7.88
12705	8.40	8.32	8.15	8.16	8.15
12720	8.40	8.32	8.15	8.16	8.15
12735	8.40	8.32	8.13	8.16	8.15
12750	8.40	8.33	8.15	8.17	8.16
12765	8.40	8.33	8.13	8.16	8.16
12780	8.41	8.33	8.15	8.16	9.01
12795	8.41	8.33	8.15	8.17	7.88
12810	8.42	8.34	8.15	8.17	7.88
12825	8.42	8.34	8.15	8.17	8.87
12840	8.42	8.34	8.15	8.17	7.88
12855	8.42	8.34	8.13	8.17	8.17
12870	8.42	8.34	8.15	8.17	8.18
12885	8.42	8.35	8.15	8.17	8.18
12900	8.43	8.35	8.15	8.17	8.18
12915	8.43	8.35	8.16	8.16	9.09
12930	8.43	8.35	8.15	8.17	8.18
12945	8.43	8.36	8.15	8.17	8.18
12960	8.43	8.36	8.15	8.17	8.18
12975	8.44	8.36	8.15	8.17	8.18
12990	8.44	8.37	8.15	8.17	8.19

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
13005	8.44	8.37	8.16	8.17	8.20
13020	8.44	8.36	8.15	8.17	8.19
13035	8.44	8.36	8.15	8.17	8.19
13050	8.44	8.36	8.16	8.17	8.19
13065	8.44	8.37	8.15	8.17	8.20
13080	8.44	8.37	8.16	8.17	8.20
13095	8.44	8.36	8.15	8.17	8.18
13110	8.44	8.36	8.15	8.17	8.18
13125	8.44	8.36	8.15	8.17	8.18
13140	8.44	8.36	8.13	8.17	8.18
13155	8.43	8.35	8.15	8.17	7.89
13170	8.43	8.35	8.13	8.17	9.05
13185	8.43	8.35	8.13	8.17	8.91
13200	8.43	8.35	8.13	8.16	8.18
13215	8.43	8.35	8.15	8.16	8.18
13230	8.43	8.35	8.13	8.17	8.18
13245	8.43	8.35	8.13	8.17	8.18
13260	8.43	8.35	8.13	8.16	8.18
13275	8.42	8.34	8.13	8.16	8.18
13290	8.42	8.34	8.13	8.17	8.17
13305	8.41	8.33	8.13	8.16	7.88
13320	8.40	8.32	8.12	8.16	8.16
13335	8.40	8.32	8.12	8.16	8.15
13350	8.39	8.31	8.12	8.16	8.15
13365	8.39	8.31	8.12	8.16	7.87
13380	8.39	8.31	8.12	8.16	8.15
13395	8.39	8.31	8.12	8.14	8.15
13410	8.39	8.31	8.12	8.14	7.86
13425	8.40	8.32	8.12	8.14	7.88
13440	8.40	8.32	8.12	8.16	8.16
13455	8.40	8.32	8.12	8.16	7.88
13470	8.40	8.32	8.12	8.16	7.87
13485	8.40	8.32	8.12	8.16	7.87
13500	8.40	8.32	8.13	8.16	8.15
13515	8.40	8.33	8.12	8.16	7.87
13530	8.40	8.32	8.12	8.16	7.88
13545	8.39	8.31	8.12	8.16	7.87
13560	8.40	8.32	8.12	8.16	7.88
13575	8.40	8.32	8.13	8.16	7.87
13590	8.40	8.32	8.12	8.16	7.87
13605	8.40	8.32	8.12	8.16	7.87
13620	8.41	8.33	8.12	8.16	7.88
13635	8.40	8.33	8.12	8.16	7.88
13650	8.41	8.33	8.13	8.16	7.88
13665	8.42	8.34	8.13	8.16	7.90
13680	8.42	8.34	8.12	8.16	7.89
13695	8.41	8.34	8.13	8.16	7.89
13710	8.41	8.34	8.13	8.16	7.89
13725	8.41	8.33	8.12	8.16	7.89
13740	8.41	8.34	8.12	8.16	7.88
13755	8.41	8.33	8.13	8.16	7.90

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
13770	8.41	8.33	8.12	8.16	7.88
13785	8.40	8.33	8.12	8.16	7.88
13800	8.41	8.33	8.12	8.16	7.88
13815	8.41	8.34	8.13	8.16	7.90
13830	8.41	8.33	8.12	8.16	7.88
13845	8.41	8.33	8.12	8.16	7.88
13860	8.40	8.33	8.12	8.16	7.88
13875	8.40	8.32	8.12	8.16	7.88
13890	8.39	8.32	8.10	8.14	7.87
13905	8.39	8.31	8.10	8.14	7.87
13920	8.39	8.31	8.10	8.14	7.86
13935	8.38	8.30	8.10	8.14	7.86
13950	8.38	8.30	8.10	8.14	7.86
13965	8.38	8.30	8.10	8.14	7.86
13980	8.37	8.30	8.08	8.12	7.86
13995	8.37	8.30	8.08	8.12	7.85
14010	8.38	8.30	8.08	8.12	7.85
14025	8.38	8.31	8.10	8.12	7.86
14040	8.39	8.32	8.10	8.14	7.86
14055	8.39	8.32	8.10	8.12	8.15
14070	8.39	8.31	8.10	8.12	8.15
14085	8.38	8.31	8.08	8.12	8.14
14100	8.38	8.31	8.08	8.12	8.14
14115	8.38	8.31	8.08	8.12	8.14
14130	8.38	8.30	8.08	8.12	7.85
14145	8.38	8.31	8.08	8.12	8.14
14160	8.38	8.31	8.10	8.12	8.14
14175	8.39	8.31	8.08	8.12	7.85
14190	8.39	8.32	8.10	8.12	7.86
14205	8.40	8.33	8.10	8.14	9.05
14220	8.40	8.33	8.10	8.14	8.16
14235	8.40	8.33	8.10	8.14	7.87
14250	8.40	8.33	8.10	8.14	8.15
14265	8.41	8.33	8.10	8.14	7.87
14280	8.41	8.34	8.10	8.14	7.87
14295	8.41	8.34	8.10	8.14	7.88
14310	8.42	8.34	8.10	8.14	8.16
14325	8.42	8.35	8.10	8.14	8.17
14340	8.42	8.34	8.10	8.14	8.17
14355	8.42	8.34	8.10	8.14	7.88
14370	8.43	8.35	8.10	8.14	8.87
14385	8.42	8.35	8.10	8.14	7.88
14400	8.43	8.36	8.10	8.16	8.18
14415	8.44	8.37	8.12	8.16	7.90
14430	8.44	8.37	8.12	8.16	7.90
14445	8.44	8.37	8.12	8.16	7.90
14460	8.44	8.37	8.10	8.16	8.95
14475	8.44	8.37	8.12	8.16	8.19
14490	8.44	8.37	8.12	8.16	8.19
14505	8.44	8.37	8.12	8.16	8.87
14520	8.44	8.36	8.12	8.16	7.90

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
14535	8.43	8.36	8.10	8.16	7.89
14550	8.43	8.36	8.10	8.16	7.89
14565	8.42	8.35	8.10	8.16	8.17
14580	8.41	8.34	8.10	8.14	9.03
14595	8.41	8.33	8.08	8.14	8.16
14610	8.41	8.33	8.08	8.14	8.87
14625	8.41	8.33	8.08	8.14	7.88
14640	8.41	8.33	8.08	8.12	8.16
14655	8.41	8.33	8.08	8.12	8.16
14670	8.40	8.32	8.08	8.12	8.15
14685	8.40	8.33	8.08	8.12	8.15
14700	8.40	8.32	8.08	8.12	8.15
14715	8.39	8.32	8.08	8.12	8.15
14730	8.39	8.31	8.08	8.12	8.15
14745	8.38	8.30	8.07	8.12	8.14
14760	8.38	8.31	8.07	8.12	8.14
14775	8.37	8.30	8.07	8.12	8.13
14790	8.37	8.29	8.07	8.11	8.13
14805	8.38	8.30	8.07	8.11	8.13
14820	8.38	8.30	8.08	8.12	8.13
14835	8.39	8.31	8.08	8.12	8.14
14850	8.40	8.32	8.08	8.12	8.15
14865	8.40	8.32	8.08	8.12	8.15
14880	8.39	8.32	8.08	8.12	7.86
14895	8.40	8.32	8.08	8.12	7.87
14910	8.40	8.32	8.08	8.12	8.15
14925	8.40	8.33	8.08	8.12	7.88
14940	8.41	8.33	8.08	8.14	8.16
14955	8.40	8.33	8.08	8.12	8.16
14970	8.39	8.32	8.08	8.12	8.15
14985	8.40	8.32	8.08	8.12	8.15
15000	8.40	8.32	8.08	8.12	8.16
15015	8.39	8.31	8.07	8.12	7.86
15030	8.39	8.32	8.08	8.12	7.86
15045	8.39	8.32	8.08	8.12	7.87
15060	8.40	8.33	8.08	8.12	7.87
15075	8.41	8.33	8.08	8.12	8.16
15090	8.42	8.34	8.08	8.14	7.89
15105	8.41	8.34	8.08	8.14	7.89
15120	8.41	8.34	8.08	8.14	7.89
15135	8.41	8.34	8.08	8.14	7.90
15150	8.41	8.34	8.08	8.14	7.89
15165	8.40	8.33	8.08	8.14	7.88
15180	8.40	8.33	8.08	8.12	8.16
15195	8.41	8.34	8.08	8.12	7.89
15210	8.41	8.34	8.08	8.12	7.89
15225	8.42	8.34	8.08	8.12	7.90
15240	8.41	8.34	8.08	8.12	8.18
15255	8.41	8.34	8.08	8.12	7.89
15270	8.42	8.35	8.08	8.12	7.89
15285	8.42	8.35	8.08	8.12	7.89

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
15300	8.41	8.34	8.07	8.12	7.89
15315	8.41	8.34	8.07	8.12	8.17
15330	8.41	8.34	8.08	8.12	8.16
15345	8.41	8.33	8.07	8.12	8.17
15360	8.40	8.33	8.07	8.12	7.88
15375	8.40	8.33	8.07	8.12	8.16
15390	8.41	8.33	8.07	8.12	7.88
15405	8.41	8.33	8.07	8.12	7.89
15420	8.40	8.33	8.07	8.12	8.16
15435	8.39	8.32	8.07	8.12	8.15
15450	8.39	8.32	8.05	8.12	7.87
15465	8.39	8.32	8.05	8.11	8.15
15480	8.39	8.32	8.05	8.11	8.15
15495	8.39	8.32	8.05	8.11	7.87
15510	8.40	8.32	8.05	8.11	8.15
15525	8.40	8.33	8.07	8.11	8.16
15540	8.41	8.33	8.07	8.11	8.16
15555	8.41	8.34	8.07	8.11	7.89
15570	8.40	8.33	8.07	8.12	8.16
15585	8.40	8.33	8.07	8.11	7.88
15600	8.40	8.33	8.07	8.11	8.16
15615	8.40	8.33	8.07	8.11	7.88
15630	8.41	8.34	8.07	8.12	8.17
15645	8.41	8.34	8.07	8.11	8.16
15660	8.40	8.33	8.07	8.12	8.16
15675	8.41	8.34	8.07	8.12	8.17
15690	8.41	8.34	8.07	8.12	7.89
15705	8.42	8.35	8.08	8.12	8.18
15720	8.43	8.35	8.08	8.12	8.18
15735	8.43	8.36	8.10	8.12	8.20
15750	8.44	8.37	8.08	8.14	8.20
15765	8.44	8.37	8.08	8.12	8.19
15780	8.44	8.37	8.10	8.14	8.20
15795	8.45	8.38	8.10	8.14	8.20
15810	8.44	8.37	8.10	8.14	8.20
15825	8.44	8.37	8.08	8.14	8.20
15840	8.44	8.37	8.10	8.14	8.20
15855	8.44	8.37	8.10	8.14	8.20
15870	8.44	8.37	8.10	8.14	8.20
15885	8.45	8.38	8.10	8.14	8.20
15900	8.45	8.38	8.10	8.14	8.20
15915	8.46	8.40	8.10	8.16	8.21
15930	8.48	8.41	8.12	8.16	8.22
15945	8.46	8.40	8.10	8.16	8.22
15960	8.45	8.39	8.10	8.16	8.22
15975	8.45	8.39	8.12	8.16	8.22
15990	8.44	8.37	8.10	8.16	8.20
16005	8.44	8.37	8.10	8.16	8.20
16020	8.43	8.36	8.08	8.14	8.20
16035	8.41	8.34	8.08	8.14	8.18
16050	8.40	8.33	8.07	8.14	8.16

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
16065	8.40	8.32	8.07	8.14	8.16
16080	8.41	8.33	8.08	8.14	8.16
16095	8.42	8.34	8.08	8.12	8.17
16110	8.42	8.35	8.08	8.12	8.18
16125	8.41	8.34	8.08	8.12	8.17
16140	8.41	8.33	8.08	8.12	8.17
16155	8.40	8.33	8.07	8.14	8.16
16170	8.41	8.34	8.08	8.14	8.17
16185	8.41	8.34	8.08	8.14	7.89
16200	8.40	8.33	8.08	8.12	8.16
16215	8.41	8.33	8.08	8.12	8.17
16230	8.42	8.34	8.08	8.14	8.17
16245	8.42	8.34	8.08	8.12	8.17
16260	8.42	8.35	8.08	8.14	8.18
16275	8.42	8.34	8.08	8.14	8.18
16290	8.42	8.35	8.08	8.14	8.18
16305	8.43	8.35	8.08	8.14	8.18
16320	8.45	8.37	8.10	8.14	8.20
16335	8.45	8.37	8.10	8.16	8.20
16350	8.45	8.38	8.10	8.16	8.20
16365	8.44	8.37	8.10	8.16	8.20
16380	8.45	8.37	8.10	8.16	8.20
16395	8.44	8.37	8.10	8.16	8.20
16410	8.44	8.37	8.10	8.16	8.20
16425	8.44	8.36	8.10	8.16	8.20
16440	8.43	8.36	8.10	8.16	8.19
16455	8.44	8.37	8.10	8.16	8.20
16470	8.44	8.37	8.10	8.16	8.20
16485	8.44	8.37	8.10	8.16	7.92
16500	8.44	8.36	8.10	8.16	8.20
16515	8.44	8.37	8.10	8.16	8.20
16530	8.45	8.38	8.10	8.16	8.21
16545	8.45	8.38	8.10	8.16	8.21
16560	8.46	8.39	8.12	8.16	8.22
16575	8.47	8.40	8.10	8.16	8.22
16590	8.47	8.40	8.12	8.17	8.22
16605	8.50	8.42	8.12	8.17	8.23
16620	8.50	8.43	8.13	8.17	8.25
16635	8.49	8.42	8.13	8.17	8.24
16650	8.49	8.42	8.13	8.17	8.24
16665	8.50	8.43	8.13	8.17	8.25
16680	8.50	8.42	8.13	8.17	8.25
16695	8.49	8.42	8.13	8.19	8.25
16710	8.48	8.40	8.12	8.19	8.24
16725	8.46	8.39	8.12	8.17	8.23
16740	8.46	8.39	8.12	8.17	7.94
16755	8.47	8.40	8.12	8.17	8.23
16770	8.46	8.39	8.12	8.17	8.23
16785	8.47	8.40	8.12	8.17	8.23
16800	8.45	8.38	8.12	8.17	8.22
16815	8.42	8.35	8.10	8.17	8.20

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
16830	8.42	8.35	8.10	8.16	7.90
16845	8.43	8.35	8.10	8.16	7.91
16860	8.45	8.37	8.10	8.16	8.20
16875	8.42	8.34	8.10	8.16	8.18
16890	8.41	8.33	8.08	8.14	7.90
16905	8.41	8.33	8.08	8.14	8.17
16920	8.43	8.35	8.10	8.16	8.18
16935	8.44	8.36	8.10	8.16	7.91
16950	8.43	8.35	8.10	8.16	8.18
16965	8.45	8.37	8.10	8.16	8.20
16980	8.42	8.35	8.10	8.16	8.18
16995	8.40	8.33	8.08	8.16	8.18
17010	8.40	8.33	8.08	8.16	8.16
17025	8.40	8.32	8.08	8.14	8.16
17040	8.40	8.32	8.08	8.14	8.16
17055	8.40	8.32	8.10	8.14	8.16
17070	8.41	8.33	8.08	8.14	7.87
17085	8.41	8.33	8.08	8.14	8.16
17100	8.41	8.32	8.08	8.14	7.85
17115	8.41	8.33	8.08	8.14	8.16
17130	8.41	8.33	8.08	8.14	8.16
17145	8.41	8.33	8.08	8.16	8.16
17160	8.40	8.32	8.08	8.14	8.16
17175	8.40	8.32	8.08	8.14	8.16
17190	8.40	8.31	8.07	8.14	8.15
17205	8.40	8.31	8.08	8.14	8.15
17220	8.39	8.31	8.07	8.14	8.15
17235	8.39	8.30	8.07	8.14	8.14
17250	8.39	8.31	8.07	8.14	8.14
17265	8.39	8.30	8.07	8.14	8.14
17280	8.39	8.30	8.07	8.14	8.13
17295	8.38	8.29	8.07	8.12	8.13
17310	8.37	8.29	8.07	8.12	8.13
17325	8.37	8.28	8.05	8.12	8.12
17340	8.37	8.28	8.07	8.12	8.12
17355	8.37	8.28	8.07	8.12	8.12
17370	8.36	8.28	8.05	8.12	8.11
17385	8.36	8.27	8.05	8.12	8.11
17400	8.35	8.26	8.05	8.12	8.10
17415	8.35	8.26	8.04	8.11	8.10
17430	8.34	8.26	8.04	8.11	8.09
17445	8.34	8.25	8.04	8.11	8.09
17460	8.34	8.25	8.04	8.11	8.09
17475	8.34	8.25	8.04	8.11	8.09
17490	8.34	8.25	8.04	8.11	8.09
17505	8.34	8.25	8.04	8.09	8.09
17520	8.33	8.25	8.04	8.09	8.08
17535	8.33	8.24	8.04	8.09	8.08
17550	8.33	8.24	8.02	8.09	8.07
17565	8.32	8.23	8.02	8.09	7.79
17580	8.32	8.23	8.02	8.09	8.07

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS
 PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
17595	8.31	8.22	8.02	8.09	8.07
17610	8.31	8.21	8.00	8.09	8.06
17625	8.30	8.21	8.00	8.08	7.78
17640	8.29	8.20	8.00	8.08	7.78
17655	8.29	8.20	8.00	8.08	8.04
17670	8.29	8.20	8.00	8.08	8.04
17685	8.28	8.19	8.00	8.08	7.76
17700	8.28	8.19	8.00	8.08	7.75
17715	8.28	8.19	8.00	8.06	7.76
17730	8.28	8.19	7.99	8.08	7.76
17745	8.28	8.19	8.00	8.06	7.76
17760	8.28	8.19	8.00	8.06	7.76
17775	8.28	8.19	8.00	8.08	7.76
17790	8.28	8.19	8.00	8.06	7.76
17805	8.29	8.20	8.00	8.06	7.77
17820	8.29	8.20	8.00	8.08	7.76
17835	8.29	8.20	8.00	8.08	7.76
17850	8.29	8.20	8.00	8.08	7.76
17865	8.28	8.20	8.00	8.08	7.76
17880	8.28	8.20	8.00	8.08	7.76
17895	8.28	8.20	8.00	8.08	7.76
17910	8.28	8.20	8.00	8.08	7.76
17925	8.28	8.20	8.00	8.08	7.76
17940	8.29	8.20	8.00	8.08	7.76
17955	8.29	8.20	8.00	8.08	7.76
17970	8.30	8.21	8.02	8.08	7.77
17985	8.30	8.21	8.00	8.08	7.78
18000	8.30	8.21	8.02	8.08	7.78
18015	8.30	8.21	8.02	8.08	7.78
18030	8.30	8.21	8.02	8.08	7.78
18045	8.30	8.21	8.02	8.08	7.78
18060	8.30	8.21	8.00	8.08	7.78
18075	8.30	8.21	8.00	8.08	7.78
18090	8.30	8.21	8.00	8.09	7.78
18105	8.29	8.21	8.00	8.08	7.77
18120	8.29	8.20	8.00	8.08	7.77
18135	8.29	8.20	8.00	8.08	7.76
18150	8.29	8.20	8.00	8.08	7.77
18165	8.30	8.21	8.00	8.08	7.78
18180	8.29	8.20	8.02	8.08	7.78
18195	8.29	8.20	8.00	8.08	7.77
18210	8.28	8.20	7.99	8.08	7.76
18225	8.28	8.19	8.00	8.08	7.76
18240	8.28	8.19	7.99	8.06	7.76
18255	8.27	8.18	7.99	8.06	7.75
18270	8.26	8.18	7.99	8.06	7.74
18285	8.26	8.17	8.00	8.05	7.74
18300	8.26	8.17	7.97	8.06	7.74
18315	8.26	8.17	7.97	8.05	7.74
18330	8.25	8.17	7.97	8.05	7.74
18345	8.26	8.17	7.97	8.05	8.01

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
18360	8.25	8.17	7.99	8.05	7.73
18375	8.26	8.17	7.97	8.05	8.01
18390	8.26	8.18	7.97	8.05	8.02
18405	8.28	8.19	7.97	8.05	7.74
18420	8.28	8.19	7.97	8.05	8.02
18435	8.28	8.19	7.97	8.05	8.02
18450	8.27	8.19	7.97	8.05	8.02
18465	8.28	8.19	7.97	8.05	8.02
18480	8.28	8.20	7.99	8.05	8.88
18495	8.29	8.20	7.97	8.05	7.76
18510	8.29	8.21	7.99	8.06	7.75
18525	8.30	8.21	7.99	8.06	7.76
18540	8.30	8.21	7.99	8.06	7.76
18555	8.31	8.22	7.99	8.06	8.85
18570	8.31	8.22	7.99	8.06	7.77
18585	8.31	8.23	7.99	8.06	7.78
18600	8.32	8.23	8.00	8.08	7.78
18615	8.32	8.23	8.00	8.08	7.78
18630	8.33	8.24	8.00	8.06	7.78
18645	8.33	8.24	8.00	8.08	7.79
18660	8.33	8.25	8.00	8.08	7.79
18675	8.33	8.25	8.00	8.08	7.79
18690	8.33	8.25	8.00	8.08	7.79
18705	8.34	8.26	8.00	8.09	8.09
18720	8.34	8.26	8.00	8.09	8.84
18735	8.34	8.26	8.02	8.09	8.09
18750	8.34	8.26	8.00	8.09	8.09
18765	8.34	8.26	8.00	8.09	8.08
18780	8.34	8.26	8.02	8.09	8.78
18795	8.34	8.26	8.02	8.09	8.81
18810	8.34	8.26	8.02	8.09	8.09
18825	8.35	8.27	8.00	8.09	8.09
18840	8.35	8.27	8.02	8.09	8.09
18855	8.35	8.27	8.02	8.09	8.09
18870	8.35	8.26	8.00	8.11	7.80
18885	8.34	8.26	8.00	8.09	8.09
18900	8.34	8.26	8.00	8.09	7.79
18915	8.34	8.25	8.00	8.09	8.09
18930	8.34	8.25	8.00	8.09	8.99
18945	8.33	8.25	8.00	8.09	7.79
18960	8.34	8.25	8.00	8.09	8.08
18975	8.33	8.25	8.00	8.08	8.08
18990	8.33	8.24	8.00	8.08	8.08
19005	8.33	8.25	8.00	8.08	8.07
19020	8.33	8.24	8.00	8.08	8.07
19035	8.34	8.25	8.00	8.08	8.08
19050	8.33	8.24	8.00	8.08	7.80
19065	8.33	8.24	8.00	8.08	8.07
19080	8.33	8.24	7.99	8.08	8.07
19095	8.32	8.23	7.99	8.08	8.07
19110	8.32	8.23	7.99	8.08	8.07

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
19125	8.31	8.22	7.99	8.08	8.06
19140	8.32	8.23	7.99	8.08	7.78
19155	8.31	8.22	7.99	8.08	7.78
19170	8.31	8.22	7.99	8.06	7.79
19185	8.32	8.23	7.99	8.08	7.79
19200	8.32	8.23	8.00	8.08	7.79
19215	8.32	8.23	8.00	8.08	7.79
19230	8.32	8.23	7.99	8.08	8.07
19245	8.32	8.24	8.00	8.08	7.80
19260	8.33	8.24	8.00	8.08	7.79
19275	8.33	8.24	8.00	8.08	7.80
19290	8.33	8.24	8.00	8.08	7.80
19305	8.32	8.24	8.00	8.08	7.79
19320	8.32	8.23	8.00	8.08	7.79
19335	8.33	8.24	8.00	8.08	7.79
19350	8.32	8.24	7.99	8.08	8.07
19365	8.33	8.24	8.00	8.08	7.79
19380	8.33	8.24	8.00	8.08	7.80
19395	8.33	8.24	8.00	8.08	7.80
19410	8.33	8.24	7.99	8.08	7.79
19425	8.32	8.23	7.99	8.08	7.79
19440	8.32	8.24	7.99	8.08	7.80
19455	8.32	8.23	7.99	8.08	7.79
19470	8.32	8.23	7.99	8.08	7.79
19485	8.32	8.23	7.99	8.08	7.79
19500	8.33	8.24	7.99	8.08	7.79
19515	8.33	8.24	7.99	8.08	7.80
19530	8.34	8.25	8.00	8.08	7.81
19545	8.34	8.26	8.00	8.08	7.81
19560	8.34	8.26	8.00	8.09	7.81
19575	8.34	8.26	8.00	8.08	7.81
19590	8.33	8.25	7.99	8.09	7.81
19605	8.33	8.24	7.99	8.08	7.81
19620	8.33	8.24	7.99	8.08	7.81
19635	8.33	8.24	7.99	8.08	7.81
19650	8.33	8.24	7.99	8.08	7.80
19665	8.32	8.24	7.99	8.08	7.79
19680	8.32	8.23	7.97	8.08	7.79
19695	8.31	8.23	7.97	8.06	7.79
19710	8.32	8.23	7.97	8.06	7.79
19725	8.32	8.23	7.97	8.06	7.79
19740	8.31	8.23	7.97	8.06	7.79
19755	8.31	8.23	7.97	8.06	7.79
19770	8.32	8.24	7.97	8.06	7.79
19785	8.32	8.24	7.97	8.06	8.07
19800	8.32	8.24	7.97	8.05	7.79
19815	8.32	8.24	7.97	8.06	7.79
19830	8.33	8.24	7.97	8.06	7.79
19845	8.33	8.24	7.97	8.06	8.07
19860	8.33	8.25	7.97	8.06	8.07
19875	8.34	8.25	7.97	8.06	8.08

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
19890	8.34	8.25	7.97	8.06	8.08
19905	8.34	8.26	7.97	8.06	8.08
19920	8.34	8.26	7.97	8.06	8.09
19935	8.35	8.26	7.97	8.06	7.80
19950	8.35	8.27	7.97	8.06	7.81
19965	8.36	8.27	7.97	8.08	8.91
19980	8.37	8.28	7.99	8.08	8.99
19995	8.37	8.29	7.99	8.08	8.86
20010	8.37	8.28	7.99	8.08	7.83
20025	8.37	8.29	7.99	8.08	7.83
20040	8.38	8.29	7.99	8.08	8.97
20055	8.38	8.30	8.00	8.08	7.83
20070	8.38	8.29	8.00	8.09	8.92
20085	8.37	8.29	7.99	8.08	7.83
20100	8.37	8.29	7.99	8.09	8.87
20115	8.39	8.30	8.00	8.09	7.84
20130	8.40	8.31	7.99	8.09	7.85
20145	8.40	8.31	8.00	8.09	7.85
20160	8.38	8.30	8.00	8.09	7.84
20175	8.40	8.32	8.00	8.09	7.85
20190	8.41	8.32	8.00	8.11	7.86
20205	8.42	8.33	8.02	8.11	8.15
20220	8.41	8.33	8.02	8.11	8.15
20235	8.40	8.33	8.02	8.11	8.15
20250	8.40	8.32	8.02	8.11	8.15
20265	8.40	8.32	8.02	8.11	8.15
20280	8.40	8.32	8.02	8.11	8.15
20295	8.40	8.32	8.02	8.11	8.15
20310	8.40	8.32	8.02	8.11	8.15
20325	8.41	8.33	8.02	8.11	8.15
20340	8.41	8.33	8.02	8.11	8.15
20355	8.41	8.32	8.02	8.11	8.15
20370	8.40	8.32	8.02	8.11	8.15
20385	8.40	8.32	8.02	8.11	8.15
20400	8.40	8.32	8.02	8.11	8.15
20415	8.42	8.33	8.02	8.11	8.16
20430	8.42	8.34	8.02	8.12	8.16
20445	8.42	8.33	8.02	8.12	8.16
20460	8.42	8.33	8.04	8.12	8.16
20475	8.43	8.34	8.04	8.12	8.17
20490	8.42	8.34	8.04	8.12	8.16
20505	8.42	8.33	8.02	8.12	8.16
20520	8.42	8.33	8.04	8.11	8.17
20535	8.42	8.33	8.02	8.12	8.16
20550	8.42	8.33	8.02	8.11	8.16
20565	8.42	8.33	8.02	8.12	8.16
20580	8.41	8.33	8.02	8.11	8.16
20595	8.41	8.33	8.02	8.11	7.88
20610	8.41	8.33	8.02	8.11	7.88
20625	8.42	8.33	8.02	8.11	7.88
20640	8.41	8.32	8.02	8.11	8.16

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
20655	8.40	8.32	8.02	8.11	7.88
20670	8.40	8.32	8.02	8.11	8.15
20685	8.40	8.32	8.00	8.11	7.87
20700	8.40	8.32	8.00	8.11	8.15
20715	8.40	8.32	8.00	8.11	8.15
20730	8.41	8.32	8.02	8.11	8.15
20745	8.41	8.32	8.00	8.11	8.16
20760	8.41	8.32	8.02	8.11	8.16
20775	8.42	8.33	8.02	8.11	8.16
20790	8.43	8.34	8.02	8.11	8.16
20805	8.43	8.34	8.02	8.11	7.89
20820	8.43	8.34	8.02	8.11	8.18
20835	8.43	8.35	8.02	8.11	7.90
20850	8.44	8.36	8.04	8.12	7.90
20865	8.44	8.35	8.04	8.12	8.19
20880	8.44	8.36	8.02	8.12	8.19
20895	8.44	8.36	8.04	8.12	8.19
20910	8.44	8.36	8.04	8.12	7.91
20925	8.45	8.36	8.04	8.12	7.92
20940	8.45	8.37	8.04	8.12	8.20
20955	8.46	8.37	8.04	8.12	8.20
20970	8.46	8.38	8.04	8.12	7.92
20985	8.45	8.36	8.04	8.12	8.20
21000	8.45	8.37	8.04	8.12	8.20
21015	8.45	8.37	8.02	8.12	8.20
21030	8.45	8.36	8.02	8.12	7.92
21045	8.44	8.36	8.02	8.12	7.91
21060	8.44	8.36	8.02	8.12	8.19
21075	8.44	8.35	8.02	8.12	8.18
21090	8.43	8.34	8.02	8.11	8.18
21105	8.43	8.34	8.00	8.11	8.18
21120	8.42	8.33	8.00	8.11	7.90
21135	8.42	8.33	8.00	8.11	8.17
21150	8.42	8.33	8.00	8.11	8.17
21165	8.42	8.33	8.00	8.09	8.17
21180	8.43	8.34	8.00	8.09	7.89
21195	8.43	8.34	8.00	8.09	8.17
21210	8.42	8.33	8.00	8.09	7.89
21225	8.43	8.33	8.00	8.09	8.17
21240	8.43	8.34	8.00	8.09	8.18
21255	8.43	8.34	8.00	8.09	8.18
21270	8.44	8.35	8.00	8.09	7.90
21285	8.44	8.35	8.00	8.09	8.18
21300	8.44	8.36	8.00	8.09	8.18
21315	8.44	8.35	8.00	8.09	8.18
21330	8.44	8.35	8.00	8.09	8.18
21345	8.45	8.36	8.00	8.09	8.18
21360	8.45	8.36	8.00	8.09	8.19
21375	8.44	8.35	8.00	8.11	8.18
21390	8.44	8.35	8.00	8.09	8.18
21405	8.44	8.35	8.00	8.09	7.90

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
21420	8.44	8.35	8.00	8.09	7.90
21435	8.44	8.35	8.00	8.09	7.90
21450	8.45	8.36	8.00	8.09	8.18
21465	8.45	8.37	8.00	8.09	8.20
21480	8.46	8.38	8.00	8.11	7.91
21495	8.46	8.38	8.00	8.11	7.92
21510	8.47	8.38	8.00	8.11	7.92
21525	8.46	8.38	8.00	8.11	9.01
21540	8.45	8.37	8.00	8.11	8.95
21555	8.46	8.38	8.00	8.11	9.05
21570	8.46	8.37	8.00	8.11	8.92
21585	8.46	8.38	8.00	8.11	7.92
21600	8.47	8.38	8.00	8.11	7.92
21615	8.46	8.37	8.00	8.11	7.92
21630	8.45	8.37	8.00	8.11	7.91
21645	8.45	8.36	8.00	8.11	8.19
21660	8.44	8.36	8.00	8.09	8.19
21675	8.45	8.36	8.00	8.09	8.19
21690	8.45	8.37	8.00	8.09	8.20
21705	8.46	8.37	8.02	8.11	8.20
21720	8.47	8.38	8.02	8.11	8.21
21735	8.46	8.37	8.02	8.11	8.20
21750	8.45	8.36	8.00	8.11	8.20
21765	8.44	8.35	8.00	8.11	8.19
21780	8.44	8.35	8.00	8.11	8.18
21795	8.44	8.35	7.99	8.09	8.18
21810	8.43	8.34	7.99	8.09	8.17
21825	8.42	8.33	7.99	8.09	8.17
21840	8.41	8.33	7.99	8.08	8.16
21855	8.40	8.31	7.97	8.08	7.87
21870	8.38	8.29	7.97	8.08	8.14
21885	8.37	8.27	7.96	8.06	8.12
21900	8.37	8.27	7.96	8.06	8.11
21915	8.37	8.27	7.96	8.06	8.11
21930	8.38	8.28	7.96	8.05	8.11
21945	8.37	8.27	7.96	8.05	8.11
21960	8.36	8.26	7.96	8.05	8.11
21975	8.35	8.26	7.94	8.05	8.10
21990	8.35	8.25	7.94	8.05	8.09
22005	8.35	8.25	7.94	8.03	8.09
22020	8.35	8.25	7.94	8.03	8.09
22035	8.34	8.25	7.94	8.03	8.09
22050	8.34	8.24	7.94	8.03	8.08
22065	8.33	8.23	7.92	8.03	8.07
22080	8.32	8.22	7.92	8.03	8.07
22095	8.31	8.22	7.92	8.01	8.07
22110	8.31	8.21	7.92	8.01	8.06
22125	8.31	8.21	7.92	8.01	7.78
22140	8.31	8.20	7.91	8.01	7.78
22155	8.31	8.21	7.91	8.01	8.05
22170	8.30	8.20	7.91	8.01	8.05

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
22185	8.30	8.20	7.91	8.01	7.77
22200	8.30	8.20	7.91	8.01	7.77
22215	8.30	8.20	7.91	8.00	7.76
22230	8.30	8.20	7.91	8.00	7.76
22245	8.30	8.20	7.91	8.01	8.04
22260	8.30	8.20	7.91	8.01	7.76
22275	8.30	8.20	7.91	8.00	7.76
22290	8.29	8.20	7.91	8.00	7.76
22305	8.30	8.20	7.91	8.00	7.76
22320	8.29	8.20	7.91	8.00	7.76
22335	8.29	8.20	7.91	8.00	7.76
22350	8.29	8.20	7.91	8.00	7.76
22365	8.28	8.19	7.89	8.00	7.76
22380	8.28	8.19	7.89	8.00	8.04
22395	8.28	8.18	7.89	8.00	7.75
22410	8.28	8.18	7.89	8.00	7.75
22425	8.28	8.18	7.89	8.00	7.75
22440	8.28	8.18	7.89	7.98	7.74
22455	8.27	8.17	7.89	8.00	8.02
22470	8.27	8.17	7.89	7.98	7.74
22485	8.26	8.16	7.89	7.98	7.73
22500	8.26	8.16	7.89	7.98	7.73
22515	8.25	8.15	7.88	7.98	7.72
22530	8.25	8.15	7.88	7.97	7.72
22545	8.25	8.15	7.88	7.98	7.72
22560	8.25	8.15	7.88	7.97	7.72
22575	8.26	8.15	7.88	7.97	7.72
22590	8.25	8.15	7.88	7.97	7.72
22605	8.25	8.15	7.88	7.97	7.72
22620	8.24	8.14	7.86	7.97	7.71
22635	8.24	8.14	7.86	7.97	7.71
22650	8.24	8.14	7.86	7.95	7.71
22665	8.24	8.14	7.86	7.97	7.71
22680	8.24	8.14	7.86	7.97	7.99
22695	8.24	8.15	7.85	7.95	7.99
22710	8.24	8.14	7.86	7.97	7.99
22725	8.24	8.14	7.86	7.95	7.99
22740	8.24	8.14	7.86	7.97	7.71
22755	8.24	8.15	7.85	7.95	8.69
22770	8.25	8.15	7.86	7.95	7.71
22785	8.25	8.15	7.85	7.95	8.86
22800	8.24	8.15	7.86	7.97	8.71
22815	8.24	8.14	7.85	7.95	7.98
22830	8.24	8.14	7.85	7.95	7.70
22845	8.26	8.16	7.86	7.95	7.71
22860	8.25	8.15	7.85	7.95	7.99
22875	8.25	8.15	7.85	7.95	7.71
22890	8.26	8.16	7.86	7.95	8.00
22905	8.28	8.17	7.86	7.97	8.00
22920	8.28	8.18	7.86	7.97	8.71
22935	8.27	8.18	7.88	7.97	8.85

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
22950	8.28	8.18	7.86	7.97	7.72
22965	8.28	8.18	7.86	7.97	7.72
22980	8.28	8.18	7.86	7.97	8.01
22995	8.28	8.19	7.86	7.97	8.02
23010	8.28	8.18	7.86	7.97	8.02
23025	8.28	8.19	7.86	7.98	8.02
23040	8.28	8.19	7.86	7.98	8.02
23055	8.29	8.19	7.86	7.98	8.02
23070	8.29	8.19	7.88	7.98	7.72
23085	8.29	8.20	7.88	7.98	8.03
23100	8.28	8.19	7.86	7.98	8.02
23115	8.29	8.20	7.88	7.98	8.02
23130	8.29	8.19	7.88	7.98	8.02
23145	8.29	8.19	7.86	7.98	7.72
23160	8.29	8.20	7.88	7.98	8.03
23175	8.29	8.19	7.88	7.98	8.02
23190	8.28	8.19	7.88	7.98	8.02
23205	8.28	8.18	7.86	7.98	8.01
23220	8.27	8.17	7.86	7.97	8.00
23235	8.26	8.17	7.86	7.98	8.00
23250	8.26	8.16	7.85	7.97	7.99
23265	8.25	8.15	7.85	7.97	8.75
23280	8.25	8.15	7.85	7.97	8.88
23295	8.25	8.15	7.85	7.97	7.71
23310	8.25	8.15	7.85	7.97	8.86
23325	8.25	8.15	7.85	7.97	7.71
23340	8.25	8.15	7.85	7.97	7.99
23355	8.25	8.15	7.85	7.97	7.99
23370	8.25	8.15	7.85	7.95	7.99
23385	8.25	8.15	7.85	7.95	7.99
23400	8.25	8.15	7.85	7.97	7.99
23415	8.25	8.15	7.85	7.97	7.99
23430	8.25	8.15	7.85	7.95	7.99
23445	8.25	8.15	7.85	7.95	7.99
23460	8.26	8.16	7.85	7.95	7.99
23475	8.26	8.16	7.85	7.95	7.99
23490	8.27	8.17	7.86	7.97	8.00
23505	8.27	8.17	7.86	7.97	7.72
23520	8.27	8.17	7.86	7.97	8.00
23535	8.27	8.17	7.86	7.97	8.00
23550	8.27	8.17	7.86	7.97	8.01
23565	8.27	8.17	7.86	7.97	7.73
23580	8.28	8.18	7.86	7.97	7.73
23595	8.27	8.17	7.86	7.97	7.73
23610	8.27	8.17	7.86	7.97	8.00
23625	8.27	8.17	7.86	7.97	7.73
23640	8.27	8.17	7.86	7.97	7.73
23655	8.28	8.18	7.86	7.97	8.01
23670	8.27	8.17	7.86	7.97	8.01
23685	8.27	8.18	7.86	7.97	7.74
23700	8.28	8.18	7.86	7.97	8.02

RAYMARK INDUSTRIES, INC
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
23715	8.28	8.19	7.86	7.97	7.74
23730	8.28	8.18	7.86	7.97	8.02
23745	8.28	8.19	7.86	7.98	8.02
23760	8.29	8.19	7.88	7.98	8.03
23775	8.29	8.19	7.86	7.97	8.02
23790	8.29	8.20	7.86	7.98	8.03
23805	8.29	8.20	7.88	7.98	7.76
23820	8.29	8.19	7.86	7.98	7.74
23835	8.29	8.20	7.86	7.98	8.03
23850	8.29	8.19	7.86	7.98	8.02
23865	8.29	8.20	7.86	7.98	8.04
23880	8.29	8.20	7.86	7.98	7.76
23895	8.29	8.19	7.86	7.98	7.75
23910	8.29	8.19	7.86	7.97	7.75
23925	8.29	8.19	7.86	7.98	8.02
23940	8.28	8.19	7.86	7.98	8.03
23955	8.28	8.19	7.86	7.97	7.74
23970	8.28	8.19	7.86	7.97	7.75
23985	8.27	8.18	7.85	7.97	8.02
24000	8.28	8.19	7.86	7.97	8.02
24015	8.27	8.17	7.85	7.97	8.00
24030	8.27	8.17	7.85	7.97	8.01
24045	8.28	8.18	7.85	7.97	8.01
24060	8.26	8.17	7.85	7.97	8.01
24075	8.26	8.17	7.85	7.95	8.00
24090	8.26	8.16	7.85	7.95	8.00
24105	8.26	8.16	7.85	7.95	7.72
24120	8.26	8.16	7.83	7.95	8.00
24135	8.26	8.17	7.85	7.95	7.72
24150	8.27	8.17	7.85	7.95	8.00
24165	8.27	8.18	7.85	7.95	8.01
24180	8.28	8.18	7.85	7.95	7.74
24195	8.27	8.18	7.85	7.95	8.01
24210	8.27	8.17	7.83	7.95	8.00
24225	8.25	8.16	7.83	7.95	8.00
24240	8.25	8.15	7.83	7.95	7.71
24255	8.24	8.14	7.81	7.95	7.99
24270	8.24	8.14	7.81	7.93	7.99
24285	8.24	8.14	7.83	7.93	7.71
24300	8.24	8.14	7.81	7.93	7.99
24315	8.25	8.15	7.83	7.93	7.99
24330	8.26	8.16	7.85	7.93	8.00
24345	8.26	8.16	7.83	7.93	7.99
24360	8.26	8.16	7.83	7.93	7.99
24375	8.27	8.17	7.85	7.95	8.00
24390	8.28	8.18	7.86	7.95	8.02
24405	8.28	8.19	7.85	7.95	8.02
24420	8.28	8.19	7.86	7.95	7.74
24435	8.28	8.19	7.85	7.95	8.02
24450	8.29	8.19	7.86	7.95	8.02
24465	8.29	8.20	7.85	7.97	8.02

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
24480	8.29	8.20	7.86	7.97	8.03
24495	8.30	8.21	7.86	7.97	8.04
24510	8.31	8.22	7.88	7.97	8.04
24525	8.32	8.22	7.88	7.98	8.05
24540	8.32	8.22	7.88	7.98	8.06
24555	8.33	8.23	7.88	7.98	8.06
24570	8.32	8.23	7.88	7.98	7.78
24585	8.33	8.23	7.88	7.98	8.07
24600	8.32	8.23	7.88	7.98	8.06
24615	8.32	8.23	7.88	7.98	8.06
24630	8.32	8.23	7.88	7.98	8.06
24645	8.31	8.22	7.88	7.98	8.05
24660	8.32	8.23	7.88	7.98	7.78
24675	8.32	8.22	7.88	7.98	8.06
24690	8.32	8.22	7.88	8.00	8.06
24705	8.31	8.22	7.89	7.98	7.78
24720	8.32	8.22	7.88	7.98	8.06
24735	8.32	8.23	7.88	7.98	7.78
24750	8.32	8.23	7.88	8.00	8.06
24765	8.33	8.23	7.88	8.00	7.78
24780	8.33	8.24	7.88	7.98	7.79
24795	8.33	8.23	7.89	7.98	7.78
24810	8.33	8.23	7.88	7.98	8.06
24825	8.32	8.23	7.88	7.98	7.78
24840	8.32	8.23	7.88	7.98	8.06
24855	8.32	8.23	7.88	7.98	7.78
24870	8.33	8.23	7.88	7.98	8.07
24885	8.33	8.23	7.88	7.98	7.78
24900	8.34	8.25	7.89	8.00	7.79
24915	8.34	8.25	7.89	8.00	7.80
24930	8.34	8.25	7.89	8.00	7.80
24945	8.35	8.26	7.89	8.00	7.80
24960	8.35	8.26	7.89	8.00	8.09
24975	8.35	8.26	7.89	8.00	7.81
24990	8.36	8.27	7.91	8.00	7.82
25005	8.36	8.27	7.89	8.00	7.82
25020	8.38	8.28	7.91	8.01	7.83
25035	8.37	8.28	7.91	8.01	8.11
25050	8.38	8.29	7.91	8.01	7.83
25065	8.38	8.28	7.91	8.01	7.83
25080	8.39	8.29	7.92	8.01	7.84
25095	8.38	8.29	7.91	8.01	7.83
25110	8.37	8.28	7.91	8.01	7.83
25125	8.37	8.28	7.91	8.01	8.11
25140	8.38	8.28	7.91	8.01	7.83
25155	8.38	8.29	7.92	8.01	7.83
25170	8.38	8.29	7.92	8.03	7.83
25185	8.38	8.28	7.91	8.01	7.83
25200	8.38	8.28	7.92	8.01	8.11
25215	8.39	8.30	7.92	8.03	7.84
25230	8.41	8.32	7.92	8.03	7.86

RAYMARK INDUSTRIES, INC
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
25245	8.40	8.31	7.92	8.03	7.86
25260	8.40	8.31	7.92	8.03	7.85
25275	8.40	8.31	7.92	8.05	7.86
25290	8.40	8.31	7.92	8.03	8.13
25305	8.41	8.31	7.92	8.03	8.14
25320	8.41	8.32	7.94	8.05	8.15
25335	8.41	8.32	7.94	8.05	8.15
25350	8.41	8.32	7.92	8.05	7.86
25365	8.41	8.31	7.92	8.05	8.14
25380	8.41	8.32	7.94	8.05	7.86
25395	8.41	8.32	7.94	8.05	7.86
25410	8.41	8.31	7.92	8.05	8.14
25425	8.40	8.31	7.92	8.05	8.14
25440	8.40	8.30	7.92	8.05	8.13
25455	8.40	8.30	7.92	8.03	8.13
25470	8.40	8.31	7.92	8.03	8.13
25485	8.40	8.30	7.92	8.03	7.85
25500	8.40	8.30	7.92	8.03	7.85
25515	8.40	8.31	7.92	8.03	8.13
25530	8.40	8.31	7.92	8.03	7.86
25545	8.41	8.31	7.92	8.03	7.86
25560	8.40	8.31	7.92	8.03	7.86
25575	8.41	8.31	7.92	8.03	7.86
25590	8.41	8.32	7.92	8.03	8.15
25605	8.41	8.31	7.92	8.03	7.86
25620	8.42	8.32	7.92	8.03	7.86
25635	8.41	8.32	7.92	8.03	7.86
25650	8.42	8.32	7.92	8.03	8.15
25665	8.42	8.33	7.94	8.03	8.16
25680	8.42	8.33	7.92	8.05	7.86
25695	8.42	8.33	7.94	8.05	8.16
25710	8.43	8.33	7.94	8.05	8.16
25725	8.45	8.35	7.94	8.05	7.89
25740	8.44	8.35	7.94	8.05	8.17
25755	8.44	8.34	7.94	8.05	8.16
25770	8.45	8.35	7.94	8.05	8.17
25785	8.45	8.35	7.94	8.05	8.18
25800	8.45	8.36	7.96	8.06	8.18
25815	8.45	8.36	7.96	8.06	7.90
25830	8.46	8.36	7.96	8.06	7.90
25845	8.46	8.37	7.97	8.06	8.20
25860	8.46	8.37	7.96	8.06	7.90
25875	8.45	8.36	7.96	8.06	8.18
25890	8.47	8.37	7.96	8.06	8.19
25905	8.47	8.38	7.96	8.08	8.19
25920	8.48	8.39	7.97	8.08	7.92
25935	8.49	8.40	7.97	8.08	8.21
25950	8.49	8.40	7.97	8.08	8.22
25965	8.50	8.40	7.99	8.09	7.95
25980	8.49	8.40	7.99	8.09	8.22
25995	8.49	8.40	7.99	8.09	8.22

RAYMARK INDUSTRIES, INC
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
26010	8.50	8.41	7.99	8.09	8.23
26025	8.51	8.42	8.00	8.11	8.24
26040	8.52	8.43	8.00	8.11	8.25
26055	8.54	8.45	8.02	8.12	8.27
26070	8.53	8.44	8.02	8.12	8.27
26085	8.51	8.42	8.02	8.12	8.25
26100	8.50	8.41	8.00	8.12	8.25
26115	8.50	8.41	8.00	8.12	8.24
26130	8.51	8.42	8.02	8.12	8.24
26145	8.52	8.42	8.02	8.12	8.25
26160	8.52	8.43	8.02	8.14	8.25
26175	8.52	8.42	8.02	8.14	8.25
26190	8.53	8.43	8.02	8.14	8.25
26205	8.53	8.43	8.04	8.14	8.25
26220	8.54	8.44	8.04	8.14	8.26
26235	8.54	8.44	8.04	8.14	8.26
26250	8.53	8.43	8.04	8.14	8.25
26265	8.53	8.43	8.04	8.14	8.25
26280	8.54	8.43	8.04	8.14	8.25
26295	8.53	8.43	8.04	8.14	8.25
26310	8.52	8.41	8.04	8.14	8.24
26325	8.50	8.40	8.02	8.14	8.23
26340	8.51	8.40	8.02	8.14	8.23
26355	8.52	8.41	8.02	8.14	8.23
26370	8.51	8.40	8.02	8.14	8.22
26385	8.52	8.40	8.02	8.14	8.23
26400	8.51	8.40	8.02	8.14	8.22
26415	8.52	8.41	8.02	8.14	8.23
26430	8.52	8.41	8.04	8.14	8.23
26445	8.51	8.40	8.04	8.14	8.23
26460	8.51	8.39	8.02	8.14	8.22
26475	8.51	8.39	8.02	8.14	8.22
26490	8.50	8.39	8.02	8.14	8.22
26505	8.50	8.39	8.02	8.14	8.22
26520	8.53	8.41	8.04	8.14	8.23
26535	8.53	8.41	8.04	8.14	8.23
26550	8.53	8.41	8.04	8.14	8.23
26565	8.52	8.41	8.04	8.14	8.23
26580	8.53	8.41	8.04	8.14	8.23
26595	8.53	8.42	8.04	8.16	8.24
26610	8.51	8.40	8.04	8.16	8.23
26625	8.50	8.39	8.04	8.14	8.22
26640	8.50	8.38	8.02	8.14	8.22
26655	8.50	8.38	8.02	8.14	8.21
26670	8.49	8.37	8.02	8.14	8.20
26685	8.48	8.36	8.02	8.14	8.20
26700	8.48	8.36	8.00	8.14	8.19
26715	8.48	8.36	8.02	8.12	8.19
26730	8.48	8.36	8.02	8.12	8.20
26745	8.48	8.36	8.02	8.12	8.19
26760	8.48	8.36	8.02	8.14	8.19

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
26775	8.49	8.37	8.02	8.12	8.20
26790	8.49	8.37	8.02	8.14	8.20
26805	8.49	8.37	8.02	8.14	8.20
26820	8.49	8.37	8.02	8.14	7.92
26835	8.49	8.37	8.02	8.14	8.20
26850	8.48	8.36	8.02	8.14	8.20
26865	8.47	8.36	8.02	8.14	8.19
26880	8.47	8.35	8.00	8.14	7.90
26895	8.46	8.34	8.02	8.12	8.18
26910	8.46	8.34	8.02	8.12	7.90
26925	8.46	8.34	8.00	8.12	8.17
26940	8.46	8.33	8.00	8.12	8.17
26955	8.46	8.34	8.00	8.12	8.17
26970	8.46	8.34	8.00	8.12	8.17
26985	8.46	8.34	8.00	8.12	8.17
27000	8.46	8.34	8.00	8.12	8.18
27015	8.46	8.34	8.00	8.12	8.17
27030	8.46	8.34	8.00	8.12	7.89
27045	8.46	8.34	8.00	8.12	7.89
27060	8.47	8.35	8.00	8.12	9.02
27075	8.47	8.35	8.00	8.12	8.18
27090	8.47	8.35	8.00	8.12	7.89
27105	8.47	8.35	8.02	8.12	8.18
27120	8.47	8.35	8.02	8.12	7.90
27135	8.47	8.35	8.02	8.12	8.88
27150	8.47	8.35	8.02	8.12	7.90
27165	8.48	8.36	8.02	8.12	7.90
27180	8.48	8.36	8.02	8.14	7.90
27195	8.48	8.36	8.02	8.14	8.98
27210	8.48	8.36	8.02	8.14	8.19
27225	8.49	8.37	8.02	8.14	8.20
27240	8.49	8.37	8.02	8.14	8.20
27255	8.49	8.37	8.04	8.14	8.20
27270	8.49	8.37	8.04	8.14	7.90
27285	8.49	8.37	8.02	8.14	8.20
27300	8.50	8.38	8.02	8.14	8.20
27315	8.50	8.38	8.04	8.16	7.90
27330	8.50	8.38	8.04	8.14	7.89
27345	8.50	8.38	8.04	8.16	8.20
27360	8.50	8.38	8.04	8.16	8.20
27375	8.51	8.39	8.04	8.16	8.21
27390	8.51	8.39	8.04	8.16	7.90
27405	8.51	8.39	8.04	8.16	8.22
27420	8.51	8.39	8.04	8.16	8.22
27435	8.51	8.40	8.05	8.17	8.22
27450	8.51	8.39	8.05	8.16	8.22
27465	8.51	8.39	8.05	8.17	8.22
27480	8.51	8.39	8.04	8.17	8.22
27495	8.51	8.39	8.05	8.17	8.22
27510	8.51	8.39	8.04	8.17	8.22
27525	8.50	8.39	8.05	8.17	8.22

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
27540	8.50	8.38	8.05	8.17	8.22
27555	8.50	8.37	8.04	8.17	8.21
27570	8.49	8.37	8.04	8.17	8.21
27585	8.49	8.37	8.05	8.17	8.20
27600	8.49	8.37	8.04	8.17	8.20
27615	8.49	8.37	8.04	8.17	8.20
27630	8.49	8.36	8.04	8.16	8.20
27645	8.49	8.36	8.04	8.16	8.20
27660	8.48	8.36	8.04	8.16	8.20
27675	8.47	8.35	8.04	8.16	8.88
27690	8.47	8.34	8.04	8.16	7.90
27705	8.46	8.34	8.04	8.16	7.90
27720	8.46	8.34	8.04	8.16	8.18
27735	8.46	8.33	8.02	8.16	8.18
27750	8.46	8.33	8.02	8.16	8.17
27765	8.46	8.33	8.02	8.16	8.17
27780	8.46	8.33	8.04	8.16	8.17
27795	8.45	8.33	8.02	8.14	8.17
27810	8.45	8.33	8.04	8.14	8.17
27825	8.46	8.33	8.04	8.14	8.18
27840	8.46	8.33	8.04	8.16	8.18
27855	8.46	8.34	8.04	8.16	8.18
27870	8.46	8.34	8.04	8.16	8.18
27885	8.47	8.34	8.04	8.16	8.18
27900	8.47	8.35	8.05	8.16	8.18
27915	8.46	8.34	8.04	8.16	8.18
27930	8.46	8.34	8.04	8.16	7.90
27945	8.46	8.34	8.04	8.16	8.18
27960	8.46	8.34	8.04	8.16	8.18
27975	8.47	8.34	8.04	8.16	7.90
27990	8.47	8.35	8.04	8.16	8.18
28005	8.48	8.36	8.05	8.16	7.92
28020	8.49	8.36	8.05	8.17	8.20
28035	8.49	8.36	8.05	8.17	8.20
28050	8.49	8.37	8.05	8.17	8.20
28065	8.49	8.37	8.05	8.17	7.93
28080	8.49	8.37	8.05	8.17	7.93
28095	8.48	8.36	8.05	8.17	8.20
28110	8.49	8.37	8.05	8.17	7.92
28125	8.49	8.36	8.05	8.17	7.92
28140	8.49	8.37	8.05	8.17	7.92
28155	8.48	8.36	8.05	8.17	8.20
28170	8.49	8.37	8.05	8.17	8.21
28185	8.49	8.37	8.05	8.17	8.21
28200	8.49	8.37	8.05	8.17	8.21
28215	8.49	8.37	8.05	8.17	8.22
28230	8.48	8.36	8.05	8.17	8.20
28245	8.49	8.37	8.05	8.17	7.92
28260	8.48	8.36	8.05	8.17	8.20
28275	8.47	8.35	8.05	8.17	7.92
28290	8.47	8.36	8.05	8.17	8.20

**RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057**

**TIDAL STUDY FIELD DATA
 J CLUSTER WELLS**

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
28305	8.47	8.35	8.04	8.17	8.20
28320	8.46	8.34	8.04	8.17	8.19
28335	8.46	8.34	8.04	8.17	8.18
28350	8.45	8.34	8.04	8.16	8.18
28365	8.45	8.33	8.04	8.16	7.90
28380	8.45	8.33	8.04	8.16	7.90
28395	8.45	8.33	8.04	8.16	7.90
28410	8.45	8.33	8.04	8.16	8.18
28425	8.46	8.34	8.04	8.16	8.18
28440	8.45	8.34	8.04	8.16	8.18
28455	8.46	8.34	8.04	8.16	8.18
28470	8.46	8.34	8.04	8.16	9.07
28485	8.46	8.34	8.04	8.16	8.18
28500	8.45	8.33	8.04	8.16	8.18
28515	8.45	8.33	8.02	8.16	8.18
28530	8.45	8.34	8.04	8.16	8.18
28545	8.46	8.34	8.04	8.16	9.11
28560	8.46	8.34	8.04	8.16	8.18
28575	8.46	8.34	8.04	8.16	8.18
28590	8.46	8.34	8.04	8.16	8.18
28605	8.46	8.34	8.04	8.16	8.18
28620	8.47	8.35	8.04	8.16	8.19
28635	8.47	8.35	8.04	8.16	8.19
28650	8.48	8.36	8.05	8.17	8.20
28665	8.49	8.37	8.05	8.17	8.20
28680	8.49	8.37	8.05	8.17	8.21
28695	8.49	8.37	8.05	8.17	8.21
28710	8.50	8.38	8.05	8.17	8.22
28725	8.50	8.38	8.05	8.17	8.22
28740	8.50	8.38	8.05	8.19	8.22
28755	8.50	8.39	8.07	8.19	8.22
28770	8.51	8.39	8.07	8.19	8.23
28785	8.51	8.40	8.07	8.19	8.23
28800	8.52	8.40	8.07	8.19	8.23
28815	8.52	8.40	8.07	8.20	8.23
28830	8.52	8.40	8.07	8.20	8.23
28845	8.52	8.41	8.08	8.20	8.25
28860	8.53	8.41	8.08	8.20	8.25
28875	8.53	8.41	8.08	8.20	8.25
28890	8.54	8.42	8.08	8.20	8.25
28905	8.53	8.41	8.08	8.22	8.25
28920	8.52	8.41	8.08	8.22	8.25
28935	8.52	8.40	8.08	8.22	8.25
28950	8.52	8.40	8.08	8.22	8.24
28965	8.52	8.40	8.08	8.22	8.24
28980	8.51	8.40	8.08	8.22	8.24
28995	8.51	8.40	8.08	8.20	8.23
29010	8.52	8.40	8.08	8.22	8.23
29025	8.52	8.40	8.08	8.22	8.24
29040	8.52	8.40	8.08	8.22	8.24
29055	8.53	8.41	8.08	8.22	8.25

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
29070	8.53	8.41	8.08	8.22	7.95
29085	8.52	8.40	8.08	8.22	8.25
29100	8.52	8.40	8.10	8.22	9.14
29115	8.52	8.40	8.10	8.22	8.99
29130	8.52	8.40	8.08	8.22	8.94
29145	8.52	8.40	8.08	8.22	7.95
29160	8.51	8.40	8.08	8.22	8.24
29175	8.51	8.40	8.08	8.22	8.24
29190	8.52	8.40	8.08	8.22	8.24
29205	8.51	8.39	8.08	8.22	8.23
29220	8.51	8.39	8.08	8.22	8.23
29235	8.51	8.39	8.08	8.20	7.95
29250	8.51	8.39	8.08	8.20	8.23
29265	8.51	8.39	8.08	8.20	7.95
29280	8.52	8.40	8.08	8.20	8.24
29295	8.53	8.41	8.10	8.22	8.25
29310	8.53	8.41	8.10	8.22	8.25
29325	8.53	8.41	8.10	8.22	7.97
29340	8.53	8.41	8.10	8.22	8.25
29355	8.52	8.41	8.10	8.22	7.97
29370	8.52	8.40	8.08	8.22	8.25
29385	8.53	8.41	8.10	8.22	8.25
29400	8.54	8.42	8.10	8.22	8.26
29415	8.55	8.43	8.10	8.22	7.99
29430	8.56	8.44	8.12	8.24	8.28
29445	8.56	8.45	8.12	8.24	8.00
29460	8.57	8.46	8.12	8.24	8.29
29475	8.58	8.46	8.12	8.24	8.02
29490	8.57	8.46	8.12	8.24	8.30
29505	8.57	8.46	8.12	8.24	8.02
29520	8.56	8.45	8.12	8.25	8.29
29535	8.57	8.46	8.12	8.25	8.30
29550	8.57	8.46	8.12	8.24	8.30
29565	8.57	8.46	8.12	8.25	8.30
29580	8.57	8.46	8.12	8.25	8.30
29595	8.57	8.46	8.12	8.25	8.30
29610	8.58	8.47	8.13	8.25	8.30
29625	8.58	8.46	8.13	8.25	8.30
29640	8.58	8.47	8.13	8.25	8.31
29655	8.57	8.46	8.13	8.25	8.30
29670	8.59	8.47	8.13	8.25	8.31
29685	8.59	8.47	8.13	8.25	8.31
29700	8.58	8.47	8.13	8.27	8.31
29715	8.58	8.47	8.13	8.25	8.30
29730	8.58	8.47	8.13	8.25	8.31
29745	8.59	8.47	8.13	8.25	8.31
29760	8.59	8.47	8.13	8.27	8.31
29775	8.59	8.47	8.13	8.25	8.31
29790	8.59	8.47	8.13	8.27	8.31
29805	8.58	8.47	8.13	8.25	8.31
29820	8.59	8.47	8.13	8.25	8.31

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
29835	8.59	8.47	8.13	8.25	8.32
29850	8.60	8.48	8.13	8.27	8.32
29865	8.60	8.49	8.13	8.27	8.32
29880	8.61	8.50	8.13	8.27	8.33
29895	8.62	8.50	8.13	8.27	8.34
29910	8.62	8.50	8.15	8.27	8.34
29925	8.62	8.50	8.15	8.28	8.34
29940	8.62	8.51	8.15	8.27	8.34
29955	8.63	8.51	8.15	8.28	8.35
29970	8.64	8.53	8.16	8.28	8.36
29985	8.64	8.53	8.18	8.28	8.37
30000	8.66	8.55	8.18	8.30	8.38
30015	8.65	8.54	8.18	8.30	8.09
30030	8.62	8.51	8.16	8.30	8.07
30045	8.59	8.48	8.15	8.28	8.04
30060	8.56	8.45	8.13	8.28	8.02
30075	8.56	8.45	8.13	8.27	8.30
30090	8.56	8.44	8.13	8.27	8.29
30105	8.55	8.43	8.12	8.25	8.29
30120	8.56	8.44	8.13	8.25	8.29
30135	8.59	8.46	8.15	8.25	8.30
30150	8.61	8.47	8.15	8.27	8.31
30165	8.63	8.50	8.15	8.27	8.33
30180	8.61	8.49	8.15	8.27	8.32
30195	8.61	8.49	8.15	8.27	8.32
30210	8.60	8.47	8.15	8.27	8.31
30225	8.58	8.46	8.15	8.27	8.30
30240	8.58	8.45	8.13	8.27	8.29
30255	8.58	8.45	8.13	8.27	8.29
30270	8.59	8.45	8.13	8.25	8.29
30285	8.60	8.46	8.13	8.27	8.30
30300	8.60	8.47	8.15	8.27	8.30
30315	8.61	8.48	8.15	8.27	8.31
30330	8.60	8.47	8.15	8.27	8.30
30345	8.60	8.47	8.15	8.27	8.30
30360	8.61	8.47	8.15	8.28	8.02
30375	8.61	8.48	8.15	8.27	9.16
30390	8.61	8.48	8.15	8.28	8.02
30405	8.61	8.48	8.15	8.28	9.08
30420	8.61	8.48	8.15	8.28	9.01
30435	8.62	8.48	8.15	8.28	8.31
30450	8.61	8.47	8.15	8.28	9.04
30465	8.60	8.47	8.15	8.28	8.02
30480	8.61	8.47	8.15	8.28	8.02
30495	8.60	8.47	8.15	8.28	8.01
30510	8.59	8.46	8.15	8.28	8.30
30525	8.58	8.46	8.15	8.28	8.29
30540	8.59	8.45	8.15	8.28	8.29
30555	8.58	8.46	8.15	8.27	8.29
30570	8.58	8.45	8.15	8.27	8.29
30585	8.57	8.44	8.13	8.27	8.28

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
30600	8.57	8.44	8.13	8.27	8.28
30615	8.57	8.43	8.13	8.27	8.27
30630	8.57	8.44	8.13	8.27	8.27
30645	8.57	8.43	8.13	8.25	8.27
30660	8.57	8.44	8.13	8.27	8.28
30675	8.57	8.44	8.13	8.27	8.28
30690	8.57	8.44	8.13	8.27	8.28
30705	8.57	8.44	8.13	8.27	8.28
30720	8.58	8.44	8.13	8.27	8.28
30735	8.58	8.45	8.13	8.27	8.29
30750	8.58	8.45	8.13	8.27	8.29
30765	8.58	8.45	8.13	8.27	8.29
30780	8.58	8.45	8.15	8.27	8.29
30795	8.58	8.45	8.13	8.27	8.01
30810	8.58	8.45	8.13	8.27	8.29
30825	8.58	8.44	8.13	8.25	8.29
30840	8.58	8.44	8.13	8.27	8.29
30855	8.58	8.45	8.13	8.27	8.29
30870	8.58	8.45	8.13	8.27	8.29
30885	8.58	8.45	8.13	8.27	8.29
30900	8.57	8.44	8.13	8.27	8.28
30915	8.57	8.44	8.13	8.27	8.28
30930	8.58	8.44	8.13	8.27	8.29
30945	8.57	8.44	8.13	8.25	8.28
30960	8.57	8.44	8.13	8.25	8.28
30975	8.57	8.44	8.13	8.27	8.00
30990	8.57	8.44	8.13	8.27	8.28
31005	8.57	8.44	8.13	8.25	8.00
31020	8.57	8.44	8.13	8.27	8.00
31035	8.57	8.44	8.13	8.27	8.28
31050	8.57	8.44	8.13	8.25	8.28
31065	8.57	8.44	8.13	8.27	8.00
31080	8.57	8.44	8.13	8.25	8.00
31095	8.57	8.44	8.13	8.27	8.00
31110	8.57	8.44	8.13	8.25	8.00
31125	8.57	8.44	8.13	8.25	8.28
31140	8.57	8.44	8.13	8.27	8.00
31155	8.58	8.44	8.13	8.27	8.00
31170	8.58	8.45	8.13	8.27	8.00
31185	8.58	8.44	8.13	8.27	8.00
31200	8.57	8.44	8.13	8.27	8.29
31215	8.57	8.44	8.13	8.27	8.00
31230	8.56	8.43	8.13	8.27	8.00
31245	8.56	8.43	8.12	8.25	8.27
31260	8.57	8.44	8.13	8.25	8.00
31275	8.57	8.44	8.13	8.25	8.00
31290	8.57	8.44	8.13	8.27	8.28
31305	8.57	8.44	8.12	8.27	8.28
31320	8.57	8.44	8.12	8.25	8.28
31335	8.57	8.44	8.13	8.27	8.28
31350	8.58	8.45	8.12	8.27	8.29

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
31365	8.58	8.45	8.13	8.27	8.00
31380	8.58	8.46	8.13	8.27	8.00
31395	8.59	8.46	8.13	8.27	8.30
31410	8.59	8.46	8.13	8.27	8.30
31425	8.59	8.46	8.13	8.27	8.00
31440	8.59	8.46	8.13	8.27	9.11
31455	8.60	8.47	8.13	8.27	8.01
31470	8.60	8.47	8.13	8.27	8.01
31485	8.61	8.48	8.15	8.27	8.02
31500	8.62	8.49	8.15	8.27	8.03
31515	8.62	8.49	8.15	8.27	8.32
31530	8.62	8.48	8.15	8.28	9.00
31545	8.62	8.49	8.15	8.28	9.09
31560	8.62	8.49	8.15	8.27	8.32
31575	8.63	8.50	8.15	8.28	8.04
31590	8.63	8.50	8.15	8.28	8.04
31605	8.63	8.50	8.15	8.28	9.20
31620	8.61	8.48	8.15	8.28	8.03
31635	8.62	8.49	8.15	8.28	8.03
31650	8.62	8.49	8.15	8.28	8.32
31665	8.62	8.49	8.15	8.28	9.06
31680	8.62	8.49	8.15	8.28	9.12
31695	8.61	8.48	8.15	8.28	8.03
31710	8.60	8.47	8.13	8.27	9.19
31725	8.62	8.49	8.15	8.28	8.32
31740	8.61	8.47	8.13	8.28	9.17
31755	8.61	8.48	8.13	8.27	8.02
31770	8.61	8.48	8.15	8.28	8.03
31785	8.61	8.48	8.15	8.27	9.11
31800	8.62	8.49	8.15	8.27	9.05
31815	8.62	8.49	8.15	8.28	9.01
31830	8.62	8.49	8.15	8.28	9.18
31845	8.61	8.48	8.15	8.27	8.03
31860	8.61	8.48	8.15	8.28	9.13
31875	8.60	8.47	8.13	8.27	8.02
31890	8.60	8.46	8.13	8.27	9.06
31905	8.59	8.46	8.13	8.27	9.03
31920	8.59	8.46	8.13	8.27	8.01
31935	8.60	8.47	8.13	8.27	8.02
31950	8.60	8.46	8.13	8.27	8.30
31965	8.59	8.46	8.13	8.27	8.30
31980	8.58	8.45	8.13	8.27	8.29
31995	8.58	8.45	8.13	8.27	8.29
32010	8.58	8.45	8.13	8.27	8.29
32025	8.57	8.44	8.12	8.27	8.29
32040	8.57	8.44	8.12	8.27	8.28
32055	8.56	8.43	8.12	8.25	8.27
32070	8.55	8.42	8.12	8.25	8.27
32085	8.55	8.42	8.12	8.25	8.27
32100	8.55	8.42	8.10	8.25	8.27
32115	8.55	8.42	8.10	8.24	7.99

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
32130	8.55	8.42	8.10	8.25	8.27
32145	8.55	8.41	8.10	8.25	7.98
32160	8.55	8.42	8.10	8.24	7.98
32175	8.55	8.41	8.10	8.24	8.26
32190	8.55	8.41	8.10	8.24	8.26
32205	8.55	8.41	8.10	8.24	8.27
32220	8.55	8.41	8.10	8.24	7.98
32235	8.54	8.41	8.10	8.24	7.98
32250	8.55	8.41	8.10	8.24	8.26
32265	8.55	8.41	8.10	8.24	8.26
32280	8.55	8.41	8.10	8.24	8.27
32295	8.55	8.42	8.10	8.24	8.26
32310	8.55	8.42	8.10	8.24	7.98
32325	8.55	8.42	8.10	8.24	7.98
32340	8.56	8.42	8.10	8.24	8.27
32355	8.55	8.42	8.10	8.24	7.99
32370	8.55	8.42	8.10	8.24	7.98
32385	8.55	8.42	8.10	8.24	7.99
32400	8.55	8.42	8.10	8.24	7.98
32415	8.55	8.42	8.10	8.24	7.99
32430	8.55	8.42	8.08	8.24	7.98
32445	8.55	8.42	8.10	8.24	7.99
32460	8.55	8.42	8.10	8.24	7.99
32475	8.55	8.42	8.08	8.24	7.98
32490	8.55	8.42	8.10	8.24	8.26
32505	8.55	8.42	8.08	8.22	7.98
32520	8.55	8.42	8.10	8.24	7.98
32535	8.55	8.42	8.10	8.24	8.27
32550	8.54	8.41	8.08	8.24	7.98
32565	8.54	8.41	8.10	8.22	7.98
32580	8.54	8.41	8.08	8.22	7.97
32595	8.54	8.40	8.08	8.22	7.97
32610	8.53	8.40	8.08	8.22	7.97
32625	8.52	8.39	8.08	8.22	7.95
32640	8.52	8.39	8.07	8.22	7.95
32655	8.52	8.39	8.07	8.22	7.96
32670	8.52	8.38	8.07	8.22	8.23
32685	8.51	8.38	8.07	8.20	7.95
32700	8.51	8.38	8.07	8.20	8.23
32715	8.51	8.38	8.07	8.20	8.23
32730	8.51	8.38	8.07	8.20	7.95
32745	8.51	8.38	8.07	8.20	8.23
32760	8.51	8.38	8.07	8.20	8.23
32775	8.51	8.38	8.05	8.20	7.93
32790	8.51	8.38	8.07	8.20	8.22
32805	8.51	8.38	8.07	8.20	7.95
32820	8.51	8.39	8.07	8.20	7.94
32835	8.52	8.39	8.07	8.20	8.97
32850	8.52	8.39	8.07	8.20	8.23
32865	8.52	8.39	8.07	8.20	8.23
32880	8.52	8.39	8.07	8.20	7.94

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
32895	8.52	8.39	8.07	8.20	9.06
32910	8.52	8.40	8.07	8.20	7.94
32925	8.53	8.40	8.07	8.20	7.94
32940	8.53	8.40	8.07	8.22	9.10
32955	8.53	8.40	8.07	8.20	8.24
32970	8.54	8.41	8.07	8.20	9.12
32985	8.55	8.42	8.08	8.22	8.26
33000	8.56	8.43	8.08	8.22	8.26
33015	8.55	8.42	8.08	8.22	8.27
33030	8.56	8.43	8.08	8.22	8.27
33045	8.56	8.43	8.08	8.22	8.27
33060	8.56	8.43	8.08	8.22	8.27
33075	8.56	8.43	8.08	8.22	8.27
33090	8.56	8.43	8.08	8.22	8.27
33105	8.56	8.44	8.10	8.22	8.27
33120	8.56	8.44	8.08	8.22	8.27
33135	8.56	8.44	8.08	8.22	8.27
33150	8.57	8.44	8.08	8.22	8.27
33165	8.57	8.44	8.10	8.22	8.28
33180	8.57	8.44	8.08	8.22	8.27
33195	8.58	8.45	8.08	8.24	8.28
33210	8.57	8.45	8.08	8.24	8.28
33225	8.57	8.44	8.10	8.24	8.28
33240	8.57	8.44	8.08	8.24	8.28
33255	8.56	8.44	8.08	8.24	8.28
33270	8.56	8.43	8.08	8.22	8.27
33285	8.56	8.44	8.08	8.24	8.27
33300	8.56	8.44	8.08	8.22	8.27
33315	8.56	8.43	8.08	8.24	8.27
33330	8.56	8.42	8.08	8.22	8.27
33345	8.55	8.42	8.08	8.22	8.26
33360	8.55	8.42	8.07	8.22	8.26
33375	8.55	8.42	8.08	8.22	8.26
33390	8.54	8.41	8.07	8.22	8.26
33405	8.54	8.41	8.07	8.22	7.96
33420	8.54	8.40	8.07	8.22	7.96
33435	8.54	8.40	8.07	8.22	9.09
33450	8.54	8.40	8.07	8.22	7.96
33465	8.53	8.40	8.07	8.20	7.95
33480	8.53	8.40	8.07	8.20	8.24
33495	8.53	8.40	8.07	8.20	8.24
33510	8.53	8.40	8.07	8.20	8.24
33525	8.53	8.40	8.07	8.20	8.24
33540	8.53	8.40	8.07	8.20	8.24
33555	8.53	8.40	8.07	8.20	8.24
33570	8.53	8.40	8.07	8.20	8.24
33585	8.53	8.40	8.07	8.20	8.24
33600	8.54	8.40	8.07	8.20	8.25
33615	8.54	8.41	8.07	8.22	8.25
33630	8.55	8.42	8.07	8.20	7.97
33645	8.54	8.41	8.07	8.22	7.97

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
33660	8.54	8.41	8.07	8.22	8.25
33675	8.55	8.41	8.07	8.22	8.26
33690	8.55	8.42	8.07	8.22	8.26
33705	8.54	8.41	8.07	8.22	8.25
33720	8.55	8.42	8.07	8.22	8.26
33735	8.55	8.41	8.07	8.22	8.26
33750	8.54	8.41	8.07	8.22	8.25
33765	8.55	8.42	8.07	8.20	7.98
33780	8.55	8.42	8.07	8.22	8.27
33795	8.56	8.43	8.08	8.22	8.27
33810	8.56	8.43	8.07	8.22	8.27
33825	8.56	8.43	8.08	8.22	8.27
33840	8.56	8.43	8.08	8.22	8.27
33855	8.56	8.43	8.07	8.22	8.27
33870	8.56	8.44	8.08	8.22	8.28
33885	8.56	8.43	8.07	8.22	8.27
33900	8.55	8.42	8.07	8.22	8.27
33915	8.56	8.43	8.08	8.22	8.27
33930	8.58	8.45	8.08	8.22	8.29
33945	8.59	8.46	8.10	8.22	8.29
33960	8.59	8.46	8.10	8.22	8.29
33975	8.59	8.46	8.10	8.24	8.30
33990	8.59	8.46	8.08	8.24	8.30
34005	8.59	8.46	8.10	8.24	8.01
34020	8.60	8.47	8.10	8.24	8.02
34035	8.60	8.47	8.10	8.24	8.31
34050	8.60	8.47	8.10	8.24	8.30
34065	8.60	8.47	8.08	8.24	8.30
34080	8.60	8.47	8.10	8.24	8.30
34095	8.59	8.46	8.10	8.24	8.30
34110	8.60	8.47	8.10	8.24	8.30
34125	8.60	8.47	8.10	8.24	8.30
34140	8.60	8.47	8.10	8.24	8.30
34155	8.60	8.47	8.10	8.24	8.30
34170	8.58	8.46	8.08	8.24	8.30
34185	8.59	8.46	8.10	8.24	8.30
34200	8.59	8.46	8.10	8.24	8.30
34215	8.60	8.47	8.10	8.24	8.98
34230	8.60	8.47	8.10	8.24	8.01
34245	8.59	8.46	8.10	8.24	9.19
34260	8.60	8.47	8.10	8.24	8.30
34275	8.60	8.47	8.10	8.24	8.30
34290	8.61	8.47	8.10	8.24	8.30
34305	8.60	8.47	8.10	8.25	8.30
34320	8.60	8.47	8.10	8.24	8.30
34335	8.60	8.47	8.10	8.24	8.30
34350	8.60	8.47	8.10	8.24	8.30
34365	8.60	8.47	8.10	8.24	8.30
34380	8.60	8.47	8.10	8.24	8.30
34395	8.61	8.48	8.10	8.24	8.30
34410	8.63	8.50	8.10	8.25	8.32

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
34425	8.61	8.48	8.10	8.25	8.32
34440	8.61	8.48	8.10	8.25	8.32
34455	8.61	8.48	8.10	8.25	8.32
34470	8.61	8.47	8.10	8.24	8.31
34485	8.61	8.48	8.10	8.25	8.31
34500	8.60	8.47	8.08	8.25	8.30
34515	8.62	8.49	8.10	8.24	8.32
34530	8.62	8.48	8.10	8.25	8.32
34545	8.62	8.48	8.10	8.24	8.32
34560	8.61	8.48	8.10	8.24	8.31
34575	8.61	8.47	8.08	8.24	8.31
34590	8.62	8.48	8.10	8.25	8.31
34605	8.60	8.47	8.10	8.24	8.30
34620	8.61	8.48	8.10	8.24	8.31
34635	8.62	8.49	8.10	8.24	8.32
34650	8.63	8.49	8.10	8.25	8.32
34665	8.63	8.49	8.10	8.25	8.32
34680	8.62	8.48	8.10	8.25	8.32
34695	8.61	8.47	8.10	8.25	8.31
34710	8.60	8.47	8.10	8.24	8.31
34725	8.60	8.47	8.10	8.24	8.30
34740	8.60	8.46	8.08	8.24	8.30
34755	8.60	8.46	8.10	8.24	8.30
34770	8.52	8.39	8.05	8.24	8.25
34785	8.54	8.40	8.07	8.22	8.25
34800	8.55	8.40	8.07	8.22	8.25
34815	8.58	8.44	8.08	8.22	9.22
34830	8.59	8.46	8.10	8.22	8.29
34845	8.59	8.45	8.08	8.22	8.29
34860	8.59	8.45	8.08	8.22	8.00
34875	8.58	8.44	8.08	8.22	9.05
34890	8.57	8.43	8.08	8.22	7.99
34905	8.55	8.42	8.07	8.22	9.12
34920	8.57	8.44	8.08	8.22	9.16
34935	8.57	8.44	8.08	8.22	9.17
34950	8.57	8.43	8.08	8.22	9.00
34965	8.56	8.42	8.08	8.22	7.98
34980	8.55	8.41	8.07	8.22	7.97
34995	8.54	8.40	8.07	8.22	7.97
35010	8.55	8.41	8.07	8.22	7.97
35025	8.53	8.39	8.05	8.20	7.95
35040	8.54	8.40	8.07	8.20	8.25
35055	8.56	8.42	8.08	8.20	8.26
35070	8.56	8.43	8.08	8.22	8.27
35085	8.57	8.43	8.08	8.22	8.27
35100	8.56	8.42	8.08	8.22	8.27
35115	8.55	8.41	8.07	8.22	8.26
35130	8.55	8.41	8.07	8.20	8.25
35145	8.53	8.40	8.07	8.20	8.25
35160	8.52	8.39	8.07	8.20	8.24
35175	8.52	8.38	8.05	8.20	8.23

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
35190	8.51	8.37	8.05	8.20	8.23
35205	8.52	8.38	8.05	8.19	8.23
35220	8.52	8.39	8.05	8.20	8.23
35235	8.53	8.39	8.05	8.20	8.23
35250	8.53	8.39	8.05	8.19	8.23
35265	8.53	8.39	8.05	8.19	8.23
35280	8.53	8.39	8.05	8.19	8.23
35295	8.53	8.39	8.05	8.19	7.95
35310	8.54	8.40	8.05	8.19	8.24
35325	8.54	8.40	8.05	8.19	8.25
35340	8.54	8.40	8.05	8.19	8.24
35355	8.54	8.40	8.05	8.19	8.24
35370	8.53	8.40	8.05	8.19	8.24
35385	8.52	8.39	8.05	8.19	7.96
35400	8.52	8.38	8.05	8.19	8.23
35415	8.51	8.38	8.05	8.19	8.23
35430	8.51	8.38	8.04	8.19	8.23
35445	8.51	8.37	8.04	8.17	7.94
35460	8.51	8.38	8.04	8.19	7.94
35475	8.51	8.37	8.04	8.17	8.23
35490	8.50	8.36	8.02	8.17	7.93
35505	8.49	8.36	8.02	8.17	8.20
35520	8.49	8.35	8.02	8.17	7.92
35535	8.48	8.35	8.02	8.17	8.20
35550	8.49	8.35	8.02	8.16	8.20
35565	8.48	8.34	8.02	8.17	7.92
35580	8.48	8.34	8.02	8.16	8.20
35595	8.49	8.35	8.02	8.16	8.20
35610	8.49	8.35	8.02	8.16	8.20
35625	8.49	8.35	8.02	8.16	7.91
35640	8.50	8.36	8.05	8.17	8.99
35655	8.50	8.36	8.02	8.17	8.21
35670	8.50	8.36	8.02	8.16	7.90
35685	8.49	8.35	8.02	8.17	8.20
35700	8.49	8.35	8.02	8.17	8.20
35715	8.49	8.35	8.02	8.17	8.20
35730	8.49	8.35	8.02	8.16	8.20
35745	8.50	8.36	8.02	8.17	8.21
35760	8.49	8.35	8.02	8.17	8.21
35775	8.49	8.35	8.00	8.16	8.20
35790	8.50	8.36	8.02	8.16	8.20
35805	8.49	8.36	8.02	8.16	8.20
35820	8.50	8.36	8.02	8.16	8.21
35835	8.50	8.37	8.02	8.17	8.22
35850	8.51	8.37	8.02	8.16	8.22
35865	8.51	8.38	8.02	8.17	8.22
35880	8.52	8.38	8.04	8.17	8.22
35895	8.52	8.39	8.02	8.17	8.23
35910	8.51	8.38	8.02	8.16	8.22
35925	8.51	8.38	8.02	8.17	8.22
35940	8.52	8.38	8.04	8.17	8.23

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
35955	8.51	8.38	8.02	8.17	8.23
35970	8.51	8.37	8.00	8.16	8.21
35985	8.50	8.37	8.02	8.16	8.22
36000	8.51	8.37	8.00	8.17	8.21
36015	8.51	8.37	8.02	8.16	8.22
36030	8.50	8.36	8.00	8.16	8.20
36045	8.51	8.37	8.00	8.16	8.21
36060	8.51	8.37	8.02	8.16	8.22
36075	8.51	8.38	8.02	8.16	8.22
36090	8.52	8.38	8.02	8.16	8.23
36105	8.51	8.37	8.00	8.16	8.21
36120	8.50	8.37	8.00	8.16	8.21
36135	8.51	8.37	8.00	8.16	8.22
36150	8.51	8.36	8.00	8.16	8.22
36165	8.50	8.36	8.00	8.16	8.21
36180	8.50	8.36	8.00	8.16	8.20
36195	8.49	8.35	8.00	8.16	8.20
36210	8.48	8.34	7.99	8.14	8.19
36225	8.48	8.34	7.99	8.14	8.19
36240	8.47	8.33	7.99	8.14	9.08
36255	8.47	8.33	7.99	8.14	9.08
36270	8.46	8.32	7.99	8.12	7.89
36285	8.46	8.32	7.99	8.12	7.88
36300	8.45	8.32	7.99	8.12	8.16
36315	8.46	8.32	7.99	8.12	8.16
36330	8.46	8.32	7.99	8.12	8.16
36345	8.46	8.32	7.99	8.12	8.16
36360	8.45	8.31	7.99	8.12	8.16
36375	8.45	8.31	7.97	8.12	8.16
36390	8.45	8.30	7.99	8.12	8.16
36405	8.44	8.30	7.99	8.12	8.15
36420	8.44	8.30	7.97	8.12	8.15
36435	8.44	8.30	7.99	8.12	8.15
36450	8.45	8.30	7.99	8.12	8.15
36465	8.45	8.31	7.99	8.12	8.16
36480	8.45	8.31	7.99	8.12	7.88
36495	8.45	8.31	7.99	8.12	7.88
36510	8.45	8.31	7.99	8.12	8.16
36525	8.45	8.31	7.99	8.12	7.88
36540	8.45	8.31	7.99	8.12	8.16
36555	8.45	8.31	7.99	8.12	7.88
36570	8.45	8.31	7.99	8.12	7.89
36585	8.45	8.31	7.99	8.14	7.88
36600	8.45	8.30	7.99	8.14	7.88
36615	8.45	8.31	7.99	8.12	7.88
36630	8.45	8.31	7.99	8.12	7.88
36645	8.45	8.31	7.99	8.12	7.88
36660	8.45	8.31	7.99	8.12	7.88
36675	8.45	8.31	7.99	8.12	7.89
36690	8.46	8.32	7.99	8.12	7.89
36705	8.46	8.33	7.99	8.14	7.89

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057.

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
36720	8.47	8.33	8.00	8.14	7.91
36735	8.47	8.33	7.99	8.14	7.90
36750	8.47	8.33	7.99	8.14	7.90
36765	8.47	8.33	7.99	8.14	7.90
36780	8.47	8.33	7.99	8.14	7.90
36795	8.48	8.34	7.99	8.14	7.90
36810	8.48	8.34	8.00	8.14	7.92
36825	8.49	8.35	7.99	8.14	8.19
36840	8.48	8.35	8.00	8.14	7.91
36855	8.48	8.34	7.99	8.14	7.92
36870	8.47	8.34	7.99	8.14	7.91
36885	8.47	8.33	7.99	8.14	7.90
36900	8.47	8.33	7.99	8.14	7.90
36915	8.47	8.33	7.99	8.14	7.91
36930	8.46	8.33	7.99	8.12	7.91
36945	8.46	8.33	7.99	8.14	7.90
36960	8.46	8.32	7.99	8.12	7.90
36975	8.45	8.32	7.97	8.12	7.89
36990	8.45	8.31	7.97	8.12	7.89
37005	8.44	8.31	7.97	8.12	7.88
37020	8.44	8.30	7.96	8.11	7.88
37035	8.44	8.30	7.97	8.11	7.88
37050	8.44	8.30	7.97	8.11	7.88
37065	8.44	8.31	7.96	8.11	8.16
37080	8.45	8.31	7.97	8.11	8.16
37095	8.45	8.31	7.96	8.11	8.16
37110	8.45	8.31	7.96	8.11	7.87
37125	8.45	8.31	7.97	8.11	8.97
37140	8.45	8.31	7.96	8.11	7.87
37155	8.45	8.31	7.97	8.11	8.16
37170	8.45	8.31	7.97	8.11	8.16
37185	8.45	8.32	7.97	8.11	8.16
37200	8.45	8.32	7.97	8.12	8.18
37215	8.46	8.33	7.97	8.11	8.17
37230	8.47	8.33	7.97	8.12	8.18
37245	8.47	8.34	7.97	8.12	8.18
37260	8.48	8.34	7.97	8.12	8.19
37275	8.48	8.35	7.99	8.12	8.20
37290	8.50	8.36	7.99	8.12	8.20
37305	8.50	8.36	7.99	8.14	8.20
37320	8.50	8.37	7.99	8.14	8.21
37335	8.50	8.37	7.99	8.14	8.21
37350	8.51	8.37	8.00	8.14	8.22
37365	8.50	8.37	7.99	8.14	8.21
37380	8.50	8.37	8.00	8.14	8.21
37395	8.50	8.36	8.00	8.14	8.22
37410	8.50	8.37	7.99	8.14	8.20
37425	8.51	8.37	7.99	8.14	8.21
37440	8.51	8.38	8.00	8.16	8.22
37455	8.52	8.38	8.00	8.16	8.22
37470	8.52	8.39	8.00	8.16	8.22

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
37485	8.52	8.39	8.00	8.16	8.23
37500	8.53	8.39	8.00	8.16	8.23
37515	8.53	8.39	8.02	8.16	8.23
37530	8.52	8.39	8.02	8.16	8.23
37545	8.53	8.39	8.02	8.16	8.23
37560	8.52	8.39	8.00	8.16	8.23
37575	8.51	8.38	8.02	8.16	8.23
37590	8.51	8.37	8.00	8.16	8.22
37605	8.50	8.37	8.00	8.16	7.93
37620	8.50	8.36	8.00	8.16	7.92
37635	8.50	8.36	8.00	8.14	7.92
37650	8.50	8.36	8.00	8.14	8.21
37665	8.49	8.35	8.00	8.14	8.20
37680	8.49	8.35	7.99	8.14	8.20
37695	8.48	8.35	7.99	8.14	8.20
37710	8.48	8.34	7.99	8.14	8.20
37725	8.48	8.34	7.99	8.14	8.19
37740	8.47	8.33	7.99	8.14	8.19
37755	8.47	8.33	7.99	8.12	8.18
37770	8.47	8.33	7.99	8.12	8.18
37785	8.46	8.33	7.99	8.12	8.18
37800	8.45	8.32	7.97	8.12	7.90
37815	8.45	8.31	7.97	8.12	8.17
37830	8.45	8.31	7.97	8.12	8.17
37845	8.45	8.31	7.97	8.12	8.16
37860	8.44	8.30	7.97	8.12	8.16
37875	8.44	8.30	7.97	8.11	7.88
37890	8.44	8.30	7.96	8.11	8.15
37905	8.44	8.30	7.96	8.11	8.16
37920	8.43	8.29	7.96	8.11	7.87
37935	8.44	8.30	7.96	8.11	7.88
37950	8.44	8.30	7.96	8.11	8.16
37965	8.44	8.29	7.96	8.11	8.15
37980	8.44	8.29	7.96	8.11	7.87
37995	8.43	8.29	7.96	8.11	7.87
38010	8.43	8.29	7.96	8.11	7.86
38025	8.44	8.30	7.96	8.11	8.15
38040	8.44	8.29	7.96	8.11	7.87
38055	8.43	8.29	7.96	8.11	7.86
38070	8.43	8.29	7.96	8.11	7.87
38085	8.44	8.29	7.96	8.11	7.88
38100	8.43	8.29	7.96	8.11	7.86
38115	8.43	8.29	7.96	8.09	7.87
38130	8.44	8.30	7.96	8.11	7.87
38145	8.45	8.31	7.96	8.11	7.88
38160	8.45	8.31	7.96	8.11	7.88
38175	8.45	8.31	7.97	8.11	7.89
38190	8.45	8.31	7.96	8.09	7.88
38205	8.45	8.31	7.96	8.11	7.88
38220	8.44	8.31	7.96	8.11	7.88
38235	8.45	8.31	7.97	8.11	7.88

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
38250	8.45	8.31	7.96	8.11	7.88
38265	8.45	8.31	7.96	8.09	7.88
38280	8.45	8.32	7.96	8.11	7.89
38295	8.45	8.31	7.96	8.11	7.88
38310	8.45	8.31	7.96	8.11	7.88
38325	8.45	8.31	7.96	8.09	7.88
38340	8.44	8.31	7.96	8.09	7.88
38355	8.44	8.30	7.96	8.09	7.88
38370	8.44	8.30	7.96	8.09	7.88
38385	8.43	8.29	7.94	8.09	7.87
38400	8.43	8.29	7.94	8.09	7.87
38415	8.43	8.29	7.94	8.08	7.86
38430	8.42	8.29	7.94	8.08	7.86
38445	8.42	8.29	7.94	8.08	7.86
38460	8.42	8.29	7.92	8.08	7.86
38475	8.42	8.29	7.92	8.08	7.86
38490	8.42	8.28	7.92	8.08	8.14
38505	8.42	8.29	7.92	8.08	8.14
38520	8.42	8.29	7.92	8.08	8.15
38535	8.42	8.29	7.92	8.08	8.15
38550	8.43	8.29	7.92	8.08	7.86
38565	8.43	8.29	7.92	8.08	7.86
38580	8.43	8.29	7.92	8.08	8.15
38595	8.43	8.29	7.92	8.08	7.85
38610	8.43	8.30	7.92	8.08	8.15
38625	8.43	8.30	7.94	8.08	8.15
38640	8.44	8.30	7.92	8.08	8.15
38655	8.44	8.30	7.92	8.08	8.15
38670	8.44	8.30	7.92	8.09	8.15
38685	8.44	8.31	7.94	8.08	8.16
38700	8.44	8.31	7.94	8.08	8.16
38715	8.45	8.32	7.94	8.09	8.16
38730	8.45	8.32	7.94	8.09	8.16
38745	8.45	8.32	7.94	8.09	8.17
38760	8.45	8.32	7.94	8.09	8.16
38775	8.46	8.33	7.94	8.09	8.17
38790	8.46	8.33	7.94	8.09	8.17
38805	8.46	8.33	7.94	8.09	8.17
38820	8.46	8.33	7.96	8.09	8.18
38835	8.46	8.33	7.94	8.09	8.17
38850	8.47	8.33	7.94	8.11	8.18
38865	8.47	8.33	7.94	8.09	8.18
38880	8.47	8.33	7.96	8.09	8.18
38895	8.47	8.34	7.96	8.11	8.18
38910	8.47	8.34	7.94	8.11	8.18
38925	8.48	8.34	7.96	8.11	8.18
38940	8.48	8.34	7.96	8.11	8.18
38955	8.47	8.34	7.96	8.11	8.19
38970	8.47	8.33	7.96	8.11	8.18
38985	8.47	8.34	7.96	8.11	8.18
39000	8.47	8.33	7.94	8.11	8.18

RAYMARK INDUSTRIES, INC.
 STRATFORD, CONNECTICUT
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 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
39015	8.47	8.33	7.96	8.09	8.18
39030	8.46	8.33	7.96	8.09	8.18
39045	8.46	8.33	7.94	8.11	8.18
39060	8.46	8.32	7.94	8.09	8.17
39075	8.43	8.31	7.94	8.09	8.16
39090	8.43	8.31	7.94	8.09	8.16
39105	8.43	8.31	7.94	8.08	8.16
39120	8.42	8.30	7.94	8.08	8.16
39135	8.42	8.30	7.92	8.08	7.86
39150	8.41	8.29	7.92	8.08	7.86
39165	8.40	8.28	7.92	8.08	8.14
39180	8.40	8.28	7.92	8.08	8.13
39195	8.40	8.27	7.92	8.06	8.13
39210	8.40	8.27	7.91	8.06	8.13
39225	8.39	8.26	7.92	8.06	8.13
39240	8.38	8.26	7.91	8.06	8.12
39255	8.38	8.25	7.91	8.06	8.11
39270	8.37	8.24	7.91	8.05	8.11
39285	8.36	8.23	7.89	8.05	7.82
39300	8.35	8.23	7.89	8.05	8.09
39315	8.35	8.23	7.89	8.05	7.81
39330	8.36	8.23	7.89	8.05	8.09
39345	8.36	8.23	7.89	8.05	7.81
39360	8.36	8.24	7.89	8.05	8.09
39375	8.36	8.24	7.89	8.05	7.82
39390	8.36	8.24	7.89	8.05	8.10
39405	8.36	8.24	7.89	8.05	7.81
39420	8.36	8.24	7.89	8.05	7.82
39435	8.37	8.24	7.89	8.05	7.82
39450	8.37	8.24	7.91	8.05	7.82
39465	8.37	8.25	7.89	8.05	7.83
39480	8.37	8.25	7.91	8.05	7.82
39495	8.37	8.25	7.91	8.05	7.82
39510	8.37	8.24	7.91	8.05	7.83
39525	8.37	8.25	7.91	8.05	7.83
39540	8.37	8.25	7.91	8.05	7.83
39555	8.38	8.26	7.91	8.05	7.83
39570	8.38	8.26	7.91	8.05	7.83
39585	8.38	8.26	7.91	8.05	7.84
39600	8.38	8.26	7.91	8.05	7.84
39615	8.38	8.26	7.92	8.05	7.85
39630	8.38	8.26	7.91	8.06	7.84
39645	8.38	8.26	7.91	8.06	7.83
39660	8.38	8.26	7.91	8.05	7.83
39675	8.38	8.26	7.91	8.05	7.84
39690	8.38	8.26	7.91	8.05	7.83
39705	8.37	8.25	7.91	8.05	7.83
39720	8.37	8.25	7.91	8.05	7.83
39735	8.37	8.25	7.91	8.05	7.83
39750	8.37	8.25	7.91	8.05	7.83
39765	8.37	8.25	7.91	8.05	7.83

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
39780	8.37	8.25	7.89	8.05	7.83
39795	8.36	8.24	7.89	8.05	7.83
39810	8.35	8.23	7.89	8.05	7.82
39825	8.34	8.23	7.89	8.03	7.81
39840	8.34	8.23	7.88	8.03	7.81
39855	8.34	8.22	7.88	8.03	7.80
39870	8.34	8.22	7.88	8.03	7.80
39885	8.33	8.21	7.88	8.03	7.79
39900	8.34	8.22	7.86	8.01	7.80
39915	8.33	8.21	7.86	8.01	8.07
39930	8.33	8.21	7.88	8.01	7.80
39945	8.33	8.21	7.86	8.01	8.07
39960	8.33	8.22	7.86	8.01	8.07
39975	8.34	8.22	7.86	8.01	7.78
39990	8.34	8.22	7.86	8.01	8.94
40005	8.34	8.22	7.86	8.01	8.07
40020	8.34	8.22	7.86	8.01	7.77
40035	8.34	8.22	7.86	8.01	8.97
40050	8.34	8.23	7.86	8.01	9.08
40065	8.35	8.23	7.86	8.01	8.08
40080	8.35	8.23	7.86	8.01	8.09
40095	8.35	8.24	7.86	8.01	8.09
40110	8.36	8.24	7.88	8.01	8.09
40125	8.36	8.24	7.86	8.03	8.09
40140	8.37	8.25	7.88	8.01	8.09
40155	8.37	8.25	7.88	8.03	8.11
40170	8.38	8.26	7.88	8.03	7.79
40185	8.39	8.27	7.89	8.03	8.11
40200	8.39	8.27	7.89	8.03	8.11
40215	8.40	8.28	7.89	8.05	8.13
40230	8.40	8.28	7.89	8.03	8.13
40245	8.40	8.29	7.89	8.03	8.13
40260	8.40	8.28	7.89	8.03	8.13
40275	8.40	8.29	7.89	8.03	8.13
40290	8.41	8.29	7.89	8.05	8.14
40305	8.41	8.30	7.89	8.05	8.14
40320	8.42	8.31	7.91	8.05	8.15
40335	8.42	8.31	7.91	8.05	8.15
40350	8.43	8.32	7.91	8.05	8.16
40365	8.44	8.32	7.91	8.06	8.16
40380	8.44	8.33	7.91	8.06	8.16
40395	8.45	8.33	7.91	8.06	8.17
40410	8.45	8.33	7.91	8.06	8.17
40425	8.44	8.33	7.91	8.06	8.17
40440	8.45	8.34	7.92	8.06	7.87
40455	8.44	8.33	7.91	8.06	8.17
40470	8.44	8.33	7.91	8.06	8.17
40485	8.44	8.33	7.91	8.06	7.86
40500	8.44	8.32	7.91	8.06	8.16
40515	8.43	8.32	7.91	8.06	8.16
40530	8.43	8.31	7.91	8.06	8.16

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
40545	8.42	8.31	7.89	8.05	8.86
40560	8.42	8.30	7.89	8.05	7.86
40575	8.42	8.30	7.89	8.05	8.15
40590	8.41	8.30	7.89	8.05	8.15
40605	8.41	8.29	7.89	8.05	8.14
40620	8.40	8.29	7.88	8.03	8.14
40635	8.40	8.28	7.88	8.03	8.13
40650	8.40	8.28	7.88	8.03	8.13
40665	8.40	8.28	7.88	8.03	8.13
40680	8.40	8.28	7.88	8.03	8.13
40695	8.40	8.28	7.88	8.03	8.13
40710	8.40	8.28	7.88	8.01	8.13
40725	8.39	8.27	7.88	8.03	7.85
40740	8.39	8.27	7.86	8.01	8.12
40755	8.39	8.27	7.88	8.01	8.12
40770	8.40	8.27	7.88	8.01	8.12
40785	8.40	8.27	7.88	8.01	8.13
40800	8.40	8.28	7.88	8.01	8.13
40815	8.40	8.28	7.88	8.01	8.13
40830	8.40	8.28	7.88	8.01	8.13
40845	8.40	8.28	7.88	8.01	8.13
40860	8.40	8.28	7.88	8.01	7.85
40875	8.41	8.29	7.88	8.03	7.86
40890	8.40	8.28	7.88	8.01	8.13
40905	8.40	8.28	7.88	8.01	7.85
40920	8.40	8.28	7.88	8.01	8.13
40935	8.40	8.28	7.88	8.01	8.13
40950	8.40	8.28	7.88	8.01	7.85
40965	8.40	8.28	7.88	8.03	8.13
40980	8.40	8.28	7.88	8.01	8.13
40995	8.40	8.28	7.88	8.01	8.14
41010	8.40	8.29	7.88	8.01	8.13
41025	8.40	8.28	7.88	8.01	7.85
41040	8.40	8.28	7.88	8.01	7.85
41055	8.41	8.29	7.88	8.03	7.85
41070	8.40	8.28	7.88	8.01	8.13
41085	8.40	8.28	7.88	8.01	7.85
41100	8.40	8.28	7.86	8.01	7.85
41115	8.39	8.27	7.86	8.01	7.85
41130	8.39	8.27	7.86	8.01	8.12
41145	8.39	8.27	7.86	8.01	7.85
41160	8.39	8.27	7.86	8.01	8.12
41175	8.39	8.27	7.86	8.01	8.12
41190	8.39	8.27	7.86	8.01	8.12
41205	8.40	8.28	7.86	8.00	7.85
41220	8.39	8.27	7.86	8.01	7.85
41235	8.40	8.28	7.86	8.00	8.13
41250	8.39	8.27	7.86	8.01	7.84
41265	8.39	8.27	7.85	8.00	8.12
41280	8.39	8.27	7.85	8.00	8.12
41295	8.38	8.26	7.85	8.00	8.11

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
41310	8.38	8.26	7.85	8.00	7.83
41325	8.38	8.26	7.85	8.00	7.83
41340	8.38	8.26	7.85	8.00	7.83
41355	8.38	8.26	7.85	7.98	8.11
41370	8.38	8.27	7.85	8.00	8.11
41385	8.38	8.26	7.85	7.98	8.11
41400	8.38	8.26	7.85	7.98	8.11
41415	8.38	8.27	7.85	7.98	7.83
41430	8.39	8.27	7.85	7.98	8.11
41445	8.40	8.28	7.85	8.00	8.12
41460	8.40	8.28	7.85	8.00	8.12
41475	8.40	8.28	7.85	8.00	8.13
41490	8.40	8.28	7.85	8.00	7.82
41505	8.41	8.29	7.85	8.00	8.13
41520	8.40	8.29	7.85	8.00	8.86
41535	8.41	8.29	7.85	8.00	7.83
41550	8.41	8.29	7.86	8.00	7.83
41565	8.41	8.30	7.86	8.00	8.13
41580	8.42	8.30	7.86	8.01	8.14
41595	8.42	8.31	7.86	8.00	8.15
41610	8.43	8.31	7.86	8.01	8.15
41625	8.42	8.31	7.86	8.01	8.15
41640	8.43	8.31	7.86	8.01	8.15
41655	8.43	8.31	7.86	8.01	8.15
41670	8.43	8.31	7.86	8.01	8.15
41685	8.43	8.32	7.86	8.01	8.16
41700	8.43	8.32	7.88	8.01	8.16
41715	8.44	8.32	7.88	8.03	8.16
41730	8.43	8.32	7.86	8.01	8.16
41745	8.43	8.32	7.86	8.01	8.16
41760	8.44	8.33	7.88	8.01	8.16
41775	8.44	8.33	7.88	8.01	8.17
41790	8.45	8.33	7.86	8.03	8.17
41805	8.45	8.33	7.88	8.03	8.18
41820	8.45	8.33	7.88	8.03	8.17
41835	8.44	8.33	7.88	8.01	8.17
41850	8.44	8.33	7.88	8.03	8.17
41865	8.44	8.32	7.86	8.03	8.16
41880	8.43	8.32	7.86	8.01	8.16
41895	8.43	8.32	7.86	8.01	8.16
41910	8.43	8.31	7.86	8.01	8.15
41925	8.43	8.31	7.86	8.01	8.16
41940	8.43	8.31	7.86	8.01	8.15
41955	8.42	8.31	7.86	8.01	8.15
41970	8.42	8.30	7.85	8.01	8.15
41985	8.41	8.30	7.85	8.00	8.15
42000	8.41	8.29	7.85	8.01	8.14
42015	8.41	8.29	7.85	8.00	8.14
42030	8.40	8.28	7.85	8.00	8.13
42045	8.40	8.28	7.85	8.00	8.13
42060	8.39	8.27	7.83	7.98	8.12

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
42075	8.38	8.26	7.83	7.98	8.11
42090	8.38	8.26	7.83	7.98	8.11
42105	8.37	8.26	7.83	7.98	8.10
42120	8.37	8.25	7.81	7.98	8.10
42135	8.36	8.24	7.81	7.98	8.09
42150	8.36	8.24	7.81	7.97	8.09
42165	8.36	8.23	7.81	7.97	8.09
42180	8.36	8.23	7.81	7.97	8.09
42195	8.36	8.24	7.81	7.97	8.09
42210	8.36	8.24	7.81	7.97	8.09
42225	8.36	8.24	7.81	7.97	7.80
42240	8.36	8.24	7.81	7.97	8.86
42255	8.35	8.23	7.81	7.95	8.98
42270	8.34	8.22	7.81	7.95	8.81
42285	8.34	8.22	7.80	7.95	7.79
42300	8.34	8.21	7.80	7.95	8.07
42315	8.34	8.21	7.80	7.95	8.07
42330	8.34	8.21	7.80	7.95	8.06
42345	8.33	8.21	7.80	7.95	8.06
42360	8.33	8.20	7.80	7.95	8.06
42375	8.33	8.20	7.80	7.95	8.06
42390	8.33	8.21	7.80	7.95	8.06
42405	8.33	8.21	7.80	7.95	8.06
42420	8.33	8.21	7.80	7.95	8.06
42435	8.33	8.20	7.80	7.95	8.06
42450	8.33	8.21	7.80	7.95	8.06
42465	8.33	8.20	7.80	7.95	8.06
42480	8.32	8.20	7.80	7.95	8.06
42495	8.33	8.20	7.80	7.95	8.06
42510	8.33	8.20	7.80	7.93	8.06
42525	8.33	8.20	7.78	7.93	8.06
42540	8.33	8.20	7.78	7.93	8.06
42555	8.33	8.21	7.80	7.95	8.07
42570	8.33	8.20	7.78	7.93	8.06
42585	8.33	8.20	7.78	7.93	8.06
42600	8.33	8.21	7.80	7.93	8.06
42615	8.33	8.21	7.80	7.93	7.78
42630	8.33	8.21	7.78	7.93	8.06
42645	8.33	8.20	7.78	7.93	8.06
42660	8.32	8.20	7.78	7.93	8.05
42675	8.31	8.19	7.78	7.93	8.04
42690	8.30	8.18	7.77	7.92	8.04
42705	8.29	8.17	7.77	7.92	7.75
42720	8.28	8.16	7.77	7.92	8.02
42735	8.28	8.16	7.75	7.92	7.74
42750	8.28	8.15	7.75	7.90	8.01
42765	8.27	8.15	7.75	7.90	8.01
42780	8.27	8.14	7.75	7.90	8.00
42795	8.27	8.14	7.75	7.90	8.00
42810	8.27	8.14	7.75	7.90	8.00
42825	8.27	8.14	7.75	7.90	8.00

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
42840	8.27	8.14	7.75	7.89	7.71
42855	8.27	8.14	7.75	7.89	7.71
42870	8.26	8.13	7.73	7.90	7.99
42885	8.25	8.13	7.73	7.89	7.99
42900	8.25	8.13	7.73	7.89	8.67
42915	8.25	8.13	7.73	7.89	7.68
42930	8.25	8.13	7.73	7.89	7.68
42945	8.25	8.12	7.73	7.87	7.98
42960	8.24	8.12	7.72	7.87	7.97
42975	8.24	8.12	7.72	7.87	7.69
42990	8.25	8.12	7.73	7.87	8.87
43005	8.25	8.12	7.72	7.87	7.69
43020	8.24	8.12	7.72	7.87	7.69
43035	8.24	8.11	7.72	7.87	7.69
43050	8.24	8.11	7.72	7.87	7.69
43065	8.24	8.12	7.72	7.87	8.71
43080	8.25	8.12	7.73	7.87	8.72
43095	8.25	8.12	7.73	7.87	7.69
43110	8.24	8.12	7.72	7.87	7.97
43125	8.25	8.12	7.72	7.87	8.72
43140	8.24	8.12	7.73	7.87	7.97
43155	8.24	8.12	7.73	7.87	7.70
43170	8.23	8.11	7.72	7.89	7.96
43185	8.23	8.11	7.73	7.87	7.97
43200	8.23	8.11	7.72	7.87	8.69
43215	8.23	8.11	7.73	7.87	8.77
43230	8.24	8.11	7.72	7.87	7.68
43245	8.24	8.12	7.72	7.87	7.97
43260	8.23	8.11	7.72	7.87	7.97
43275	8.22	8.10	7.70	7.87	7.96
43290	8.21	8.09	7.70	7.87	7.95
43305	8.20	8.08	7.70	7.87	7.67
43320	8.23	8.10	7.72	7.87	7.95
43335	8.22	8.10	7.72	7.86	7.95
43350	8.24	8.11	7.72	7.86	7.96
43365	8.26	8.13	7.72	7.87	7.97
43380	8.24	8.12	7.72	7.87	7.97
43395	8.23	8.11	7.72	7.87	7.97
43410	8.23	8.10	7.72	7.87	7.96
43425	8.23	8.11	7.72	7.86	7.96
43440	8.23	8.10	7.73	7.86	7.96
43455	8.22	8.10	7.70	7.87	7.95
43470	8.23	8.10	7.70	7.86	7.95
43485	8.23	8.10	7.72	7.86	7.96
43500	8.22	8.09	7.70	7.86	7.95
43515	8.22	8.09	7.70	7.86	7.95
43530	8.21	8.08	7.70	7.84	7.94
43545	8.19	8.07	7.69	7.84	7.93
43560	8.20	8.07	7.69	7.84	7.93
43575	8.20	8.07	7.69	7.84	7.93
43590	8.19	8.07	7.69	7.84	7.93

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
43605	8.19	8.07	7.69	7.84	7.92
43620	8.18	8.06	7.67	7.82	7.92
43635	8.18	8.06	7.67	7.82	7.92
43650	8.19	8.06	7.69	7.82	7.64
43665	8.20	8.07	7.69	7.82	7.92
43680	8.19	8.07	7.69	7.82	7.92
43695	8.20	8.08	7.69	7.82	7.93
43710	8.21	8.08	7.69	7.82	7.93
43725	8.22	8.09	7.69	7.84	7.67
43740	8.21	8.08	7.69	7.82	7.93
43755	8.20	8.08	7.69	7.84	7.93
43770	8.20	8.08	7.69	7.82	7.65
43785	8.20	8.08	7.69	7.84	7.65
43800	8.21	8.08	7.69	7.82	7.93
43815	8.20	8.08	7.69	7.82	7.93
43830	8.20	8.08	7.69	7.84	7.66
43845	8.20	8.08	7.69	7.82	7.65
43860	8.21	8.08	7.69	7.82	7.93
43875	8.22	8.09	7.69	7.84	7.94
43890	8.22	8.09	7.69	7.84	7.67
43905	8.21	8.09	7.69	7.84	7.95
43920	8.22	8.09	7.70	7.84	7.67
43935	8.21	8.09	7.69	7.84	7.66
43950	8.22	8.10	7.69	7.84	7.67
43965	8.21	8.09	7.69	7.84	7.94
43980	8.22	8.10	7.69	7.84	7.67
43995	8.22	8.10	7.70	7.84	7.96
44010	8.22	8.10	7.69	7.84	7.95
44025	8.21	8.09	7.69	7.84	7.67
44040	8.22	8.10	7.69	7.84	7.95
44055	8.21	8.09	7.69	7.84	7.67
44070	8.21	8.09	7.69	7.84	7.94
44085	8.21	8.09	7.69	7.84	7.95
44100	8.21	8.09	7.69	7.84	7.67
44115	8.20	8.08	7.69	7.84	7.66
44130	8.20	8.08	7.69	7.82	7.93
44145	8.20	8.08	7.67	7.82	7.65
44160	8.20	8.08	7.67	7.82	7.93
44175	8.20	8.08	7.67	7.82	7.93
44190	8.20	8.08	7.67	7.82	7.93
44205	8.20	8.08	7.67	7.82	7.65
44220	8.20	8.08	7.67	7.82	7.65
44235	8.20	8.08	7.67	7.82	7.65
44250	8.19	8.07	7.67	7.82	7.65
44265	8.19	8.07	7.67	7.82	7.93
44280	8.19	8.07	7.67	7.81	7.65
44295	8.19	8.07	7.67	7.82	7.93
44310	8.19	8.07	7.67	7.81	7.93
44325	8.19	8.07	7.67	7.81	7.65
44340	8.19	8.07	7.65	7.81	7.65
44355	8.19	8.07	7.65	7.81	7.92

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
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TIDAL STUDY FIELD DATA
 J CLUSTER WELLS

PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
44370	8.19	8.07	7.65	7.81	7.93
44385	8.19	8.07	7.65	7.81	7.65
44400	8.19	8.07	7.67	7.81	7.92
44415	8.19	8.07	7.65	7.81	7.65
44430	8.20	8.08	7.65	7.81	7.93
44445	8.19	8.08	7.65	7.81	7.93
44460	8.19	8.08	7.67	7.81	7.93
44475	8.20	8.08	7.65	7.81	7.92
44490	8.20	8.09	7.67	7.81	7.93
44505	8.20	8.09	7.67	7.81	7.65
44520	8.21	8.09	7.67	7.81	7.66
44535	8.21	8.09	7.67	7.81	7.94
44550	8.21	8.09	7.67	7.81	7.93
44565	8.21	8.09	7.65	7.81	7.93
44580	8.21	8.09	7.67	7.82	7.93
44595	8.21	8.09	7.67	7.81	7.94
44610	8.20	8.09	7.67	7.82	7.94
44625	8.20	8.08	7.65	7.82	7.93
44640	8.20	8.09	7.67	7.81	7.93
44655	8.21	8.09	7.67	7.82	7.93
44670	8.21	8.10	7.67	7.82	7.94
44685	8.22	8.10	7.67	7.82	7.94
44700	8.22	8.10	7.67	7.82	7.95
44715	8.22	8.10	7.67	7.82	7.95
44730	8.22	8.10	7.67	7.82	7.95
44745	8.22	8.10	7.69	7.82	7.95
44760	8.22	8.11	7.67	7.82	7.95
44775	8.22	8.10	7.67	7.82	7.95
44790	8.22	8.10	7.67	7.82	7.95
44805	8.22	8.10	7.67	7.82	7.95
44820	8.22	8.10	7.67	7.82	7.95
44835	8.22	8.10	7.67	7.82	7.95
44850	8.22	8.10	7.67	7.82	7.95
44865	8.21	8.10	7.67	7.82	7.95
44880	8.21	8.09	7.67	7.82	7.94
44895	8.20	8.09	7.67	7.81	7.93
44910	8.20	8.08	7.67	7.81	7.93
44925	8.20	8.08	7.65	7.81	7.93
44940	8.20	8.08	7.65	7.81	7.93
44955	8.19	8.08	7.65	7.81	7.93
44970	8.19	8.07	7.65	7.81	7.93
44985	8.19	8.07	7.65	7.81	7.92
45000	8.19	8.07	7.65	7.79	7.92
45015	8.18	8.06	7.65	7.79	7.92
45030	8.17	8.06	7.64	7.79	7.91
45045	8.17	8.06	7.64	7.79	7.90
45060	8.17	8.05	7.64	7.79	7.90
45075	8.16	8.05	7.64	7.79	7.90
45090	8.16	8.04	7.64	7.79	7.62
45105	8.16	8.05	7.64	7.78	7.90
45120	8.17	8.05	7.64	7.78	7.62

RAYMARK INDUSTRIES, INC
 STRATFORD, CONNECTICUT
 RACR SECTION 3013 ORDER
 DOCKET NO. I-87-1057

TIDAL STUDY FIELD DATA
 J CLUSTER WELLS
 PREPARED BY: ENVIRONMENTAL LABORATORIES, INC.

TIME (MIN)	GROUNDWATER ELEVATIONS (N.G.V.D. 1929)				
	J1-1	J2-1	J3	J4	J5
45135	8.17	8.06	7.64	7.78	7.90
45150	8.17	8.06	7.64	7.79	7.90
45165	8.17	8.06	7.64	7.78	7.91
45180	8.17	8.05	7.64	7.79	7.90
45195	8.17	8.05	7.64	7.78	7.90
45210	8.17	8.05	7.64	7.78	7.90
45225	8.17	8.06	7.64	7.78	7.90
45240	8.17	8.06	7.64	7.78	7.91
45255	8.18	8.07	7.64	7.78	7.64
45270	8.18	8.07	7.64	7.79	7.64
45285	8.18	8.07	7.64	7.79	7.91
45300	8.18	8.07	7.64	7.79	7.92
45315	8.19	8.08	7.64	7.79	7.92
45330	8.19	8.08	7.65	7.79	7.92
45345	8.19	8.08	7.65	7.79	7.93
45360	8.19	8.08	7.64	7.79	7.65
45375	8.19	8.08	7.65	7.79	7.93
45390	8.19	8.07	7.64	7.79	7.64
45405	8.18	8.07	7.65	7.79	7.92
45420	8.18	8.07	7.64	7.79	7.92
45435	8.20	8.08	7.65	7.79	7.93
45450	8.21	8.09	7.65	7.79	7.93
45465	8.21	8.10	7.65	7.79	7.94
45480	8.22	8.11	7.65	7.79	7.67
45495	8.21	8.10	7.65	7.81	7.94
45510	8.21	8.09	7.65	7.81	7.93
45525	8.18	8.07	7.64	7.79	7.92
45540	8.18	8.07	7.64	7.79	7.92
45555	8.19	8.07	7.64	7.79	7.92
45570	8.17	8.07	7.64	7.79	7.92
45585	8.17	8.06	7.64	7.79	7.64
45600	8.17	8.06	7.64	7.79	7.64
45615	8.17	8.05	7.64	7.78	7.91
45630	8.17	8.05	7.64	7.78	7.62