ECEN720: High-Speed Links Circuits and Systems Spring 2023

Lecture 3: Time-Domain Reflectometry & S-Parameter Channel Models

Sam Palermo
Analog & Mixed-Signal Center
Texas A&M University

Announcements

- Lab 1 report and Prelab 2 due Feb 6
- Reference Material Posted on Website
  - TDR theory application note
  - S-parameter notes

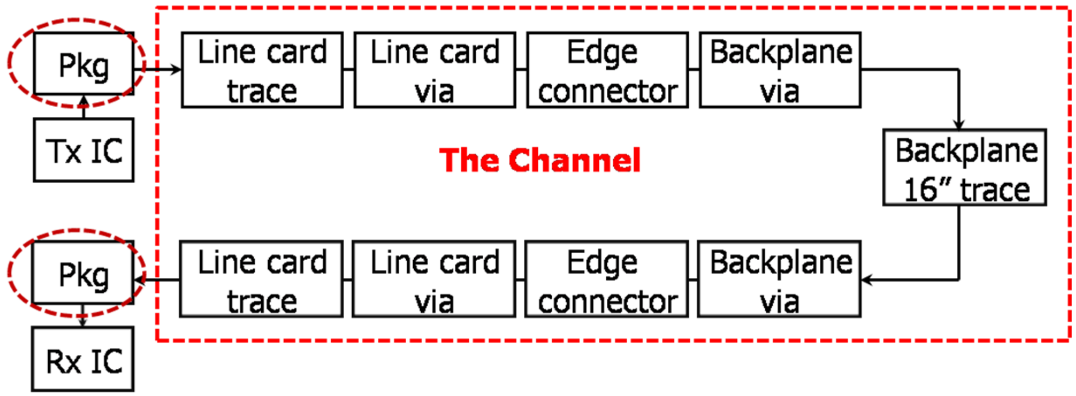
Agenda

- Interconnect measurement techniques
  - Time-domain reflectometry (TDR)
  - Network analyzer
- S-parameters
- Cascading S-parameter models
- Full S-parameter channel model
- Transient simulations
  - Impulse response generation
  - Eye diagrams
  - Inter-symbol interference

Lecture References

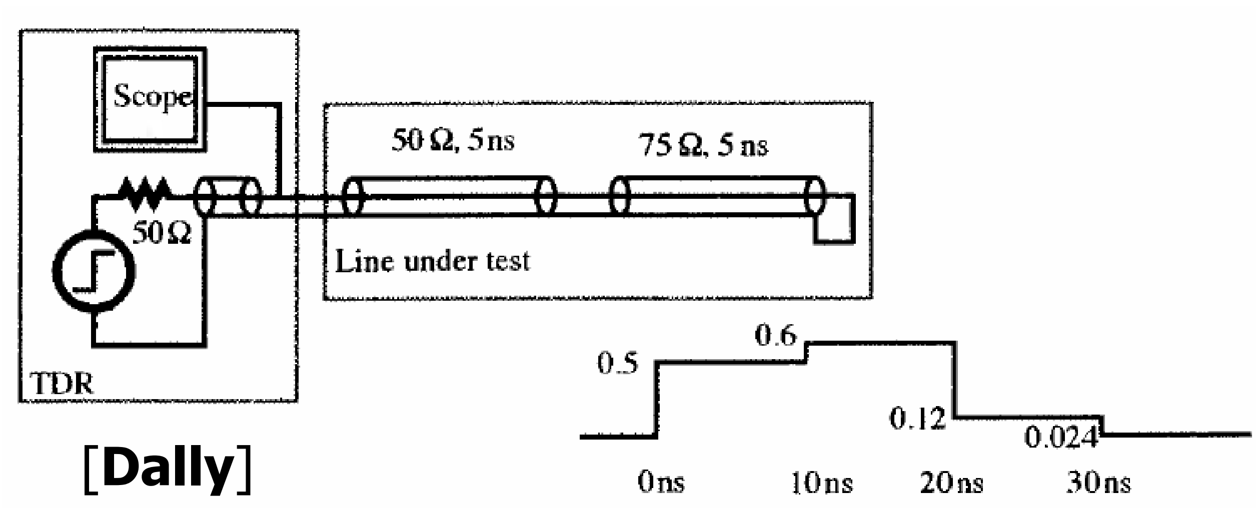
- Majority of TDR material from Dally Chapter 3.4, 3.6 - 3.7
- Majority of s-parameter material from Hall "Advanced Signal Integrity for High-Speed Digital Designs" Chapter 9

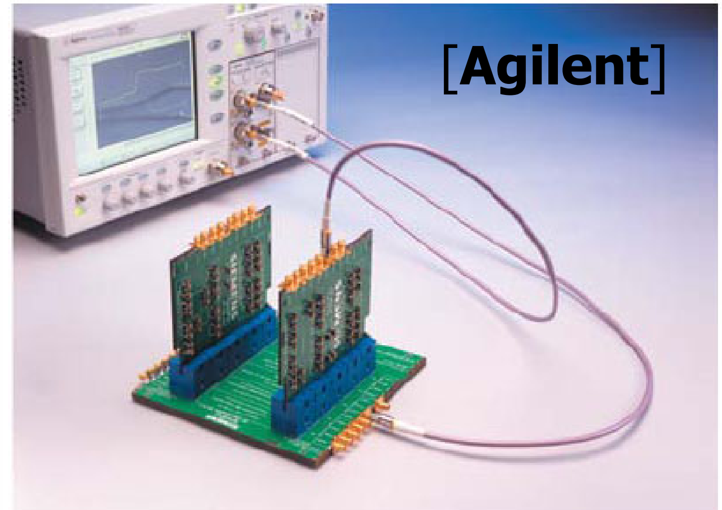
Interconnect Modeling



- Why do we need interconnect models?
  - Perform hand calculations and simulations (Spice, Matlab, etc…)
  - Locate performance bottlenecks and make design trade-offs
- Model generation methods
  - Electromagnetic CAD tools
  - Actual system measurements
- Measurement techniques
  - Time-Domain Reflectometer (TDR)
  - Network analyzer (frequency domain)

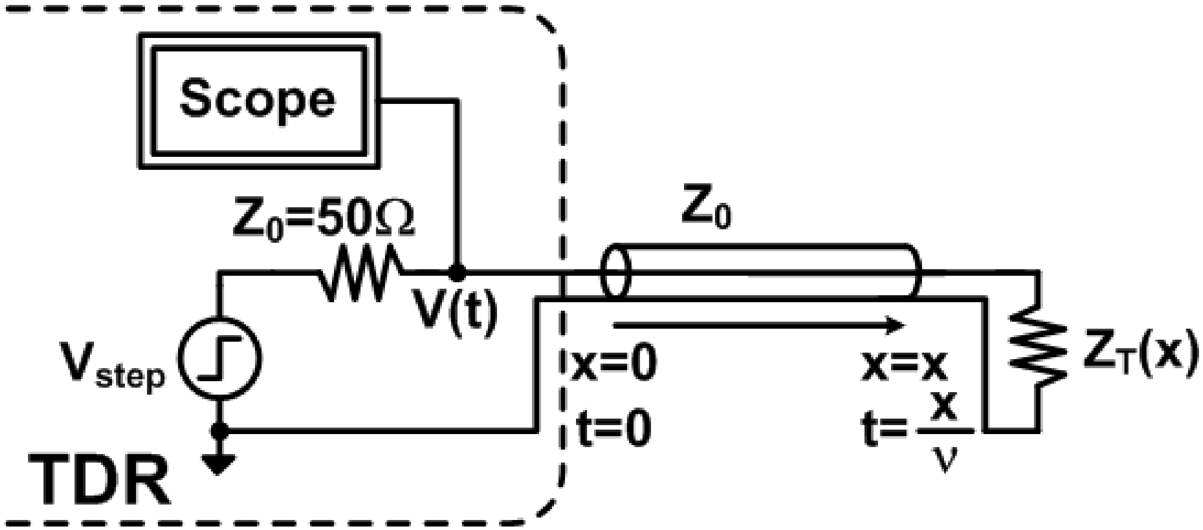
Time-Domain Reflectometer (TDR)





- TDR consists of a fast step generator and a high-speed oscilloscope
- TDR operation
  - Outputs fast voltage step onto channel
  - Observe voltage at source, which includes reflections
  - Voltage magnitude can be converted to impedance
  - Impedance discontinuity location can be determined by delay
- Only input port access to characterize channel

TDR Impedance Calculation



$$k_r(t) = \frac{V_r(t)}{V_i} = \frac{Z_T(t) - Z_0}{Z_T(t) + Z_0}$$

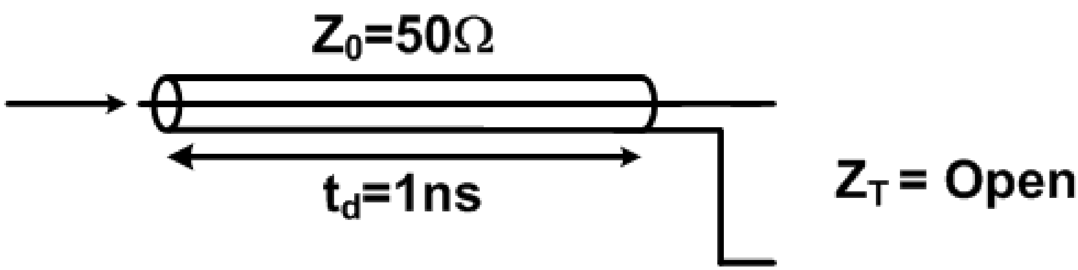
$$Z_T(t) = Z_0\left(\frac{1 + k_r(t)}{1 - k_r(t)}\right) = Z_0\left(\frac{V_i + V_r(t)}{V_i - V_r(t)}\right) = Z_0\left(\frac{V(t)}{2V_i - V(t)}\right)$$

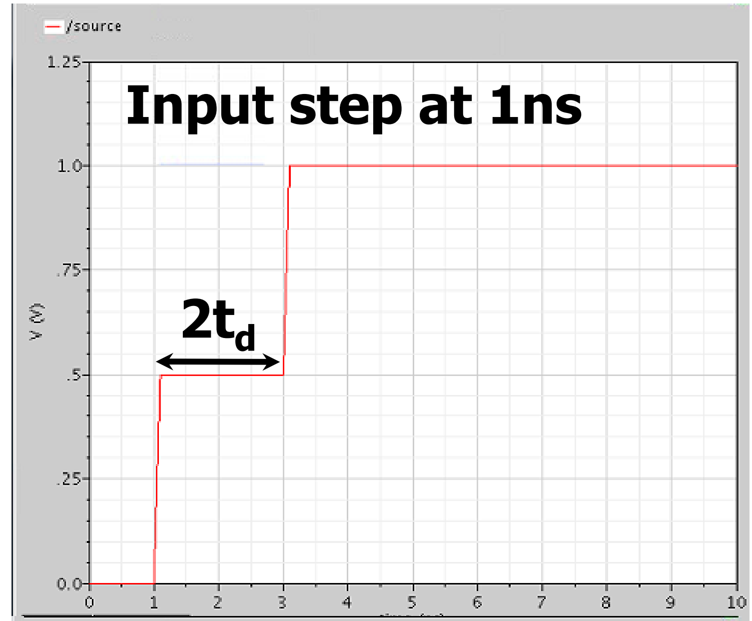
$$\text{If } V_{\text{STEP}} = 1V \Rightarrow V_i = 0.5\text{V}$$

$$Z_T(t) = Z_0\left(\frac{V(t)}{1V - V(t)}\right) \qquad Z_T(x) = Z_T\left(t = \frac{2x}{\upsilon}\right)$$

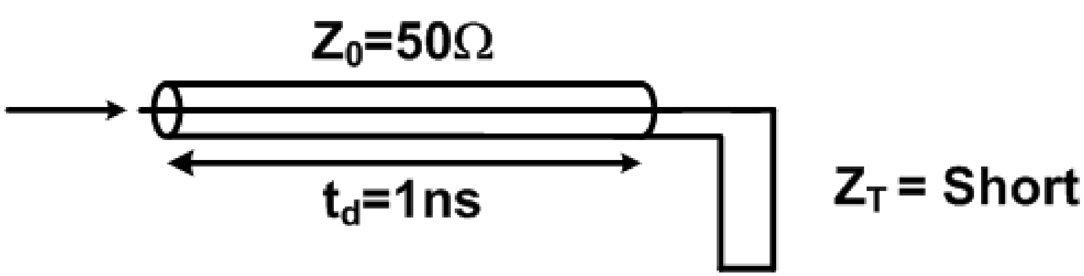
TDR Waveforms (Open & Short)

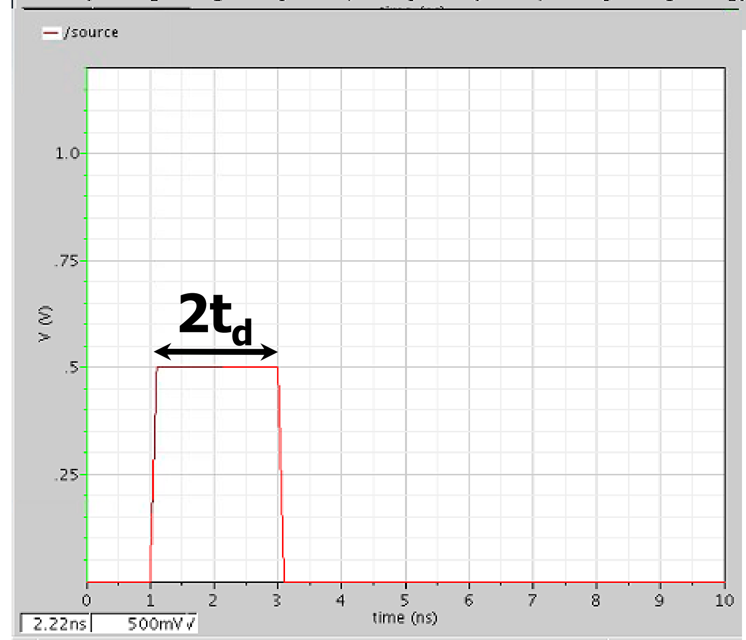
- Open termination





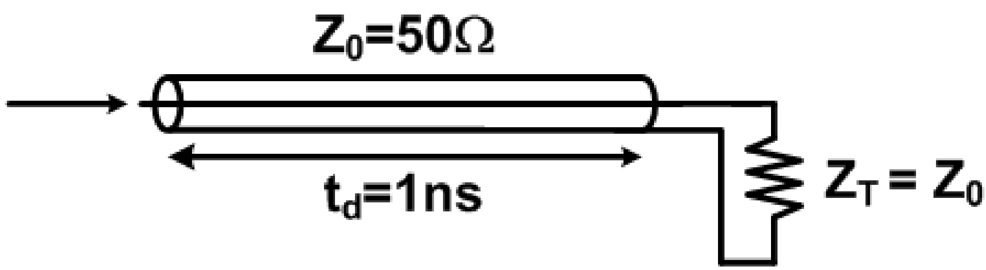
- Short termination

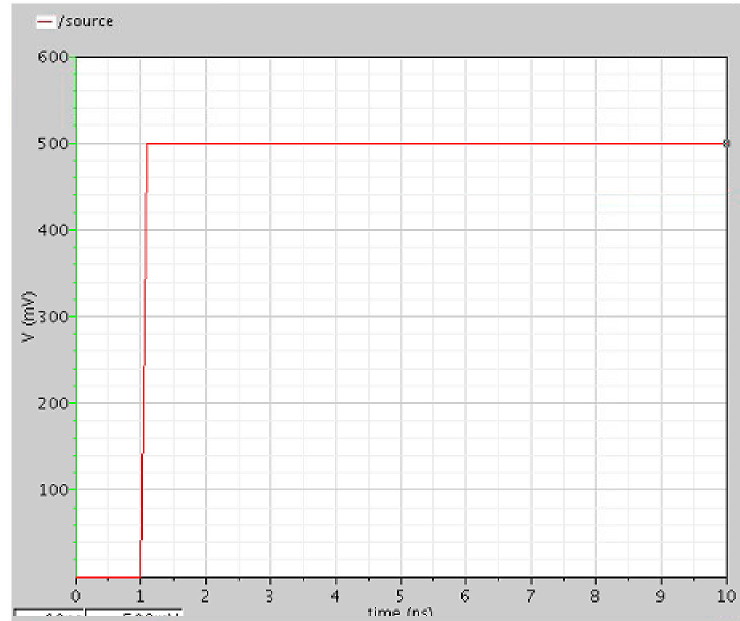




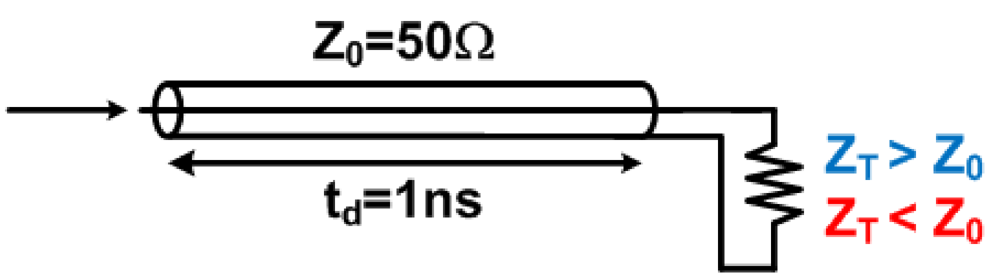
TDR Waveforms (Matched & Mismatched)

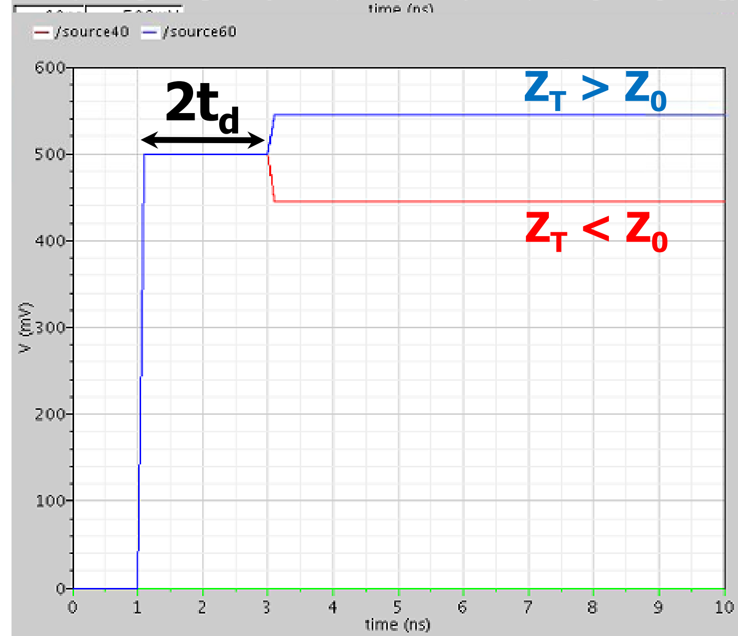
- Matched termination





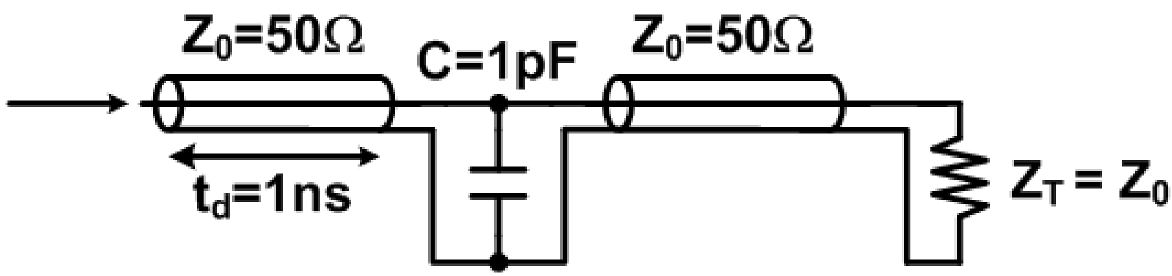
- Mismatched termination



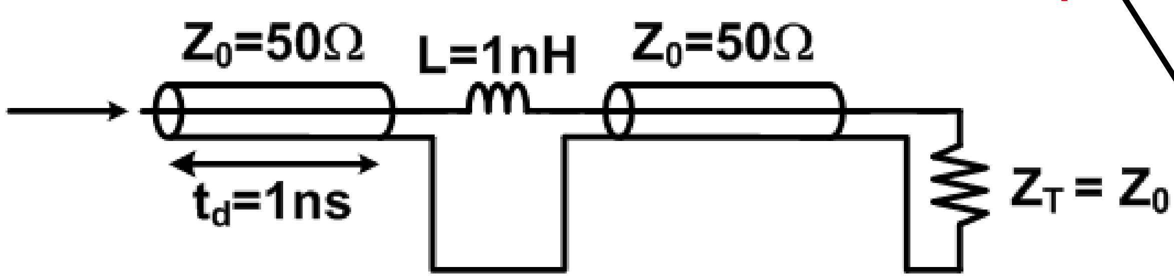


TDR Waveforms (C & L Discontinuity)

- Shunt C discontinuity

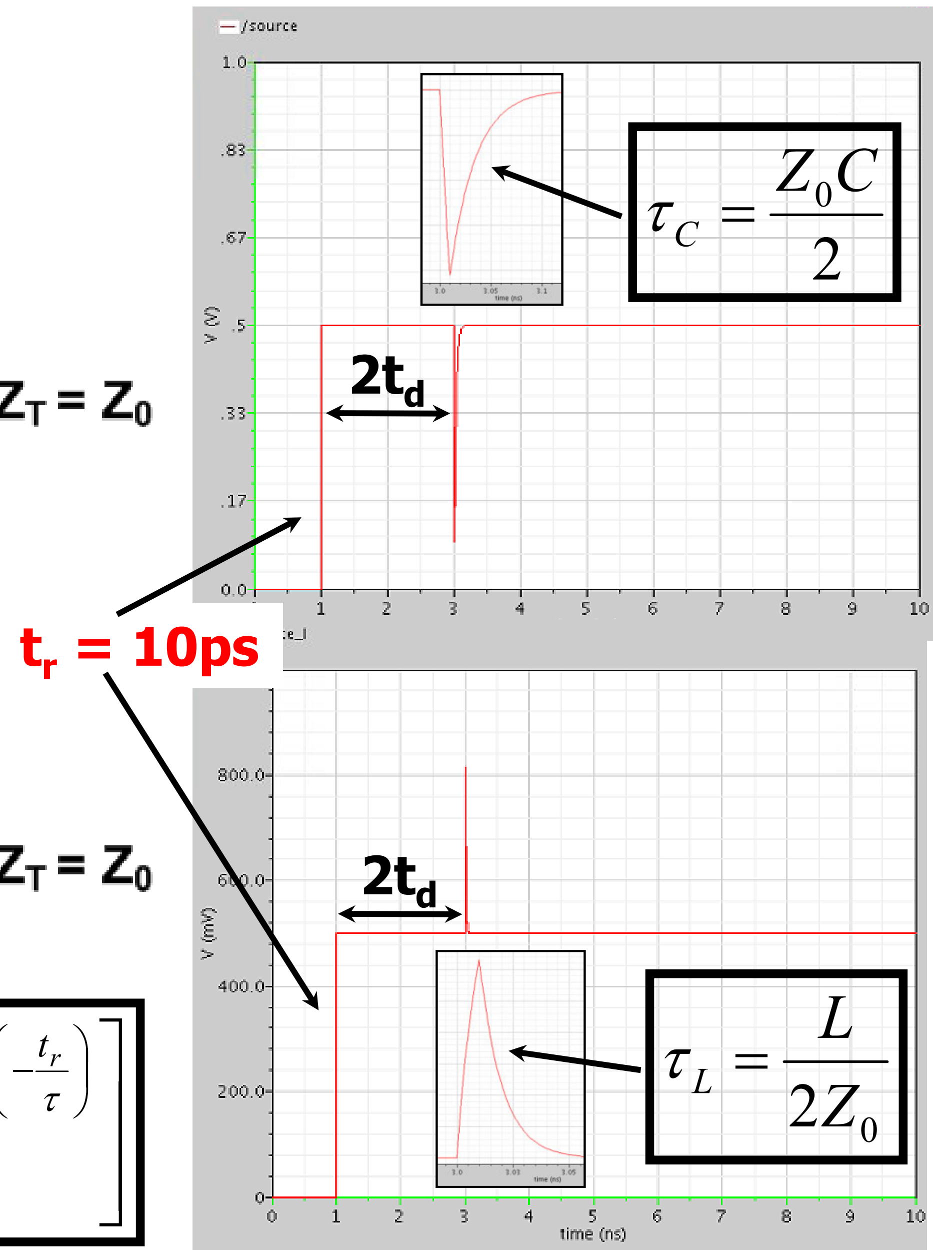


- Series L discontinuity



Peak voltage spike magnitude:

$$\frac{\Delta V}{V} = \left(\frac{\tau}{t_r}\right)\left[1 - e^{\left(-\frac{t_r}{\tau}\right)}\right]$$



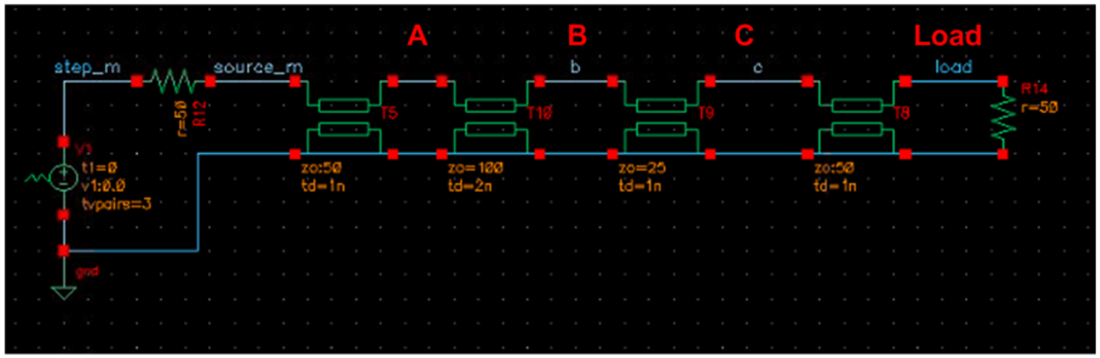
TDR Rise Time and Resolution

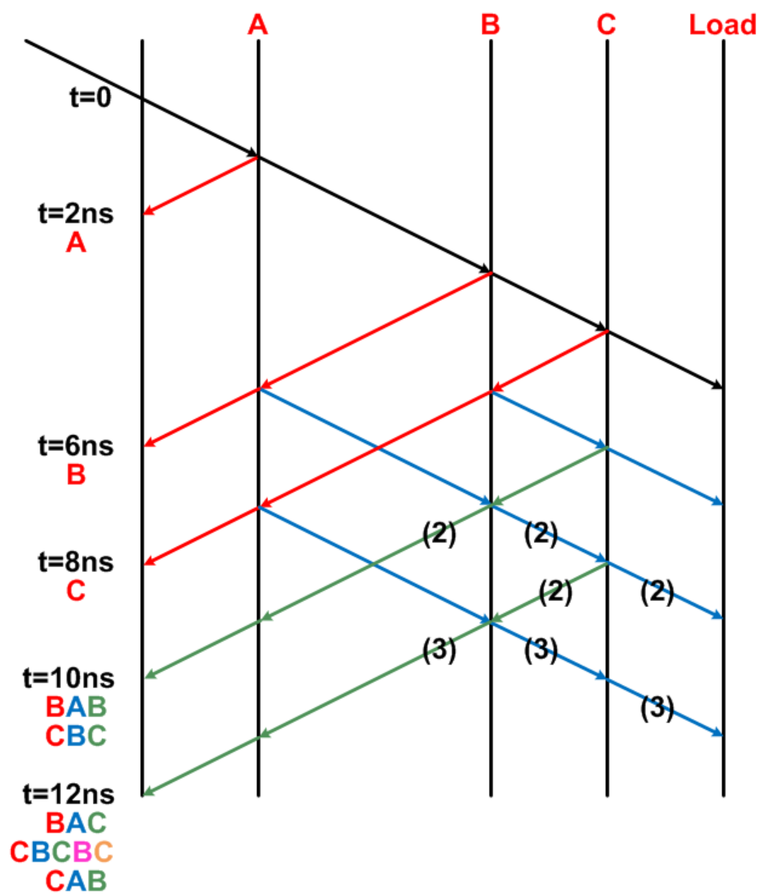
- TDR spatial resolution is set by step risetime

$$\boxed{\Delta x > t_r \upsilon}$$

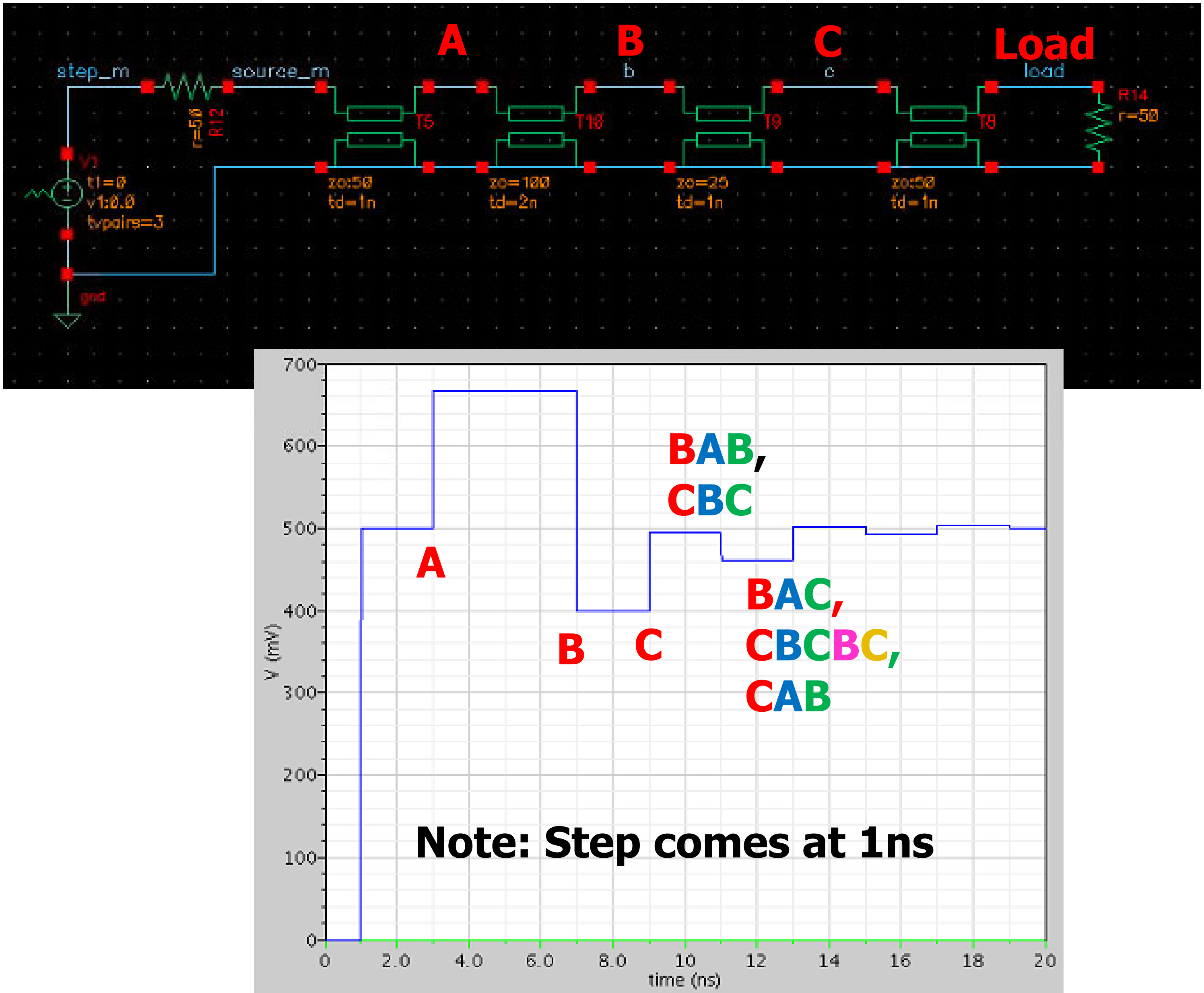
- Step risetime degrades with propagation through channel
  - Dispersion from skin-effect
  - Lump discontinuities low-pass filter the step
- Causes difficulty in estimating L & C values
- Channel filtering can actually compensate for lump discontinuity spikes ☺

TDR Multiple Reflections

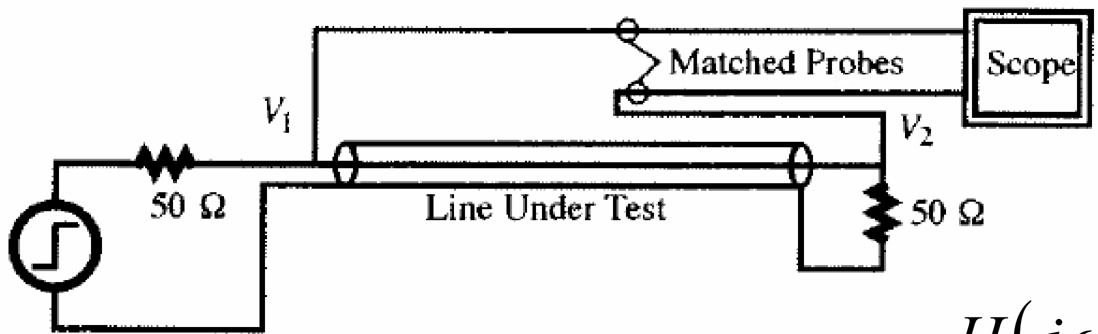




TDR Waveforms (Multiple Discontinuities)



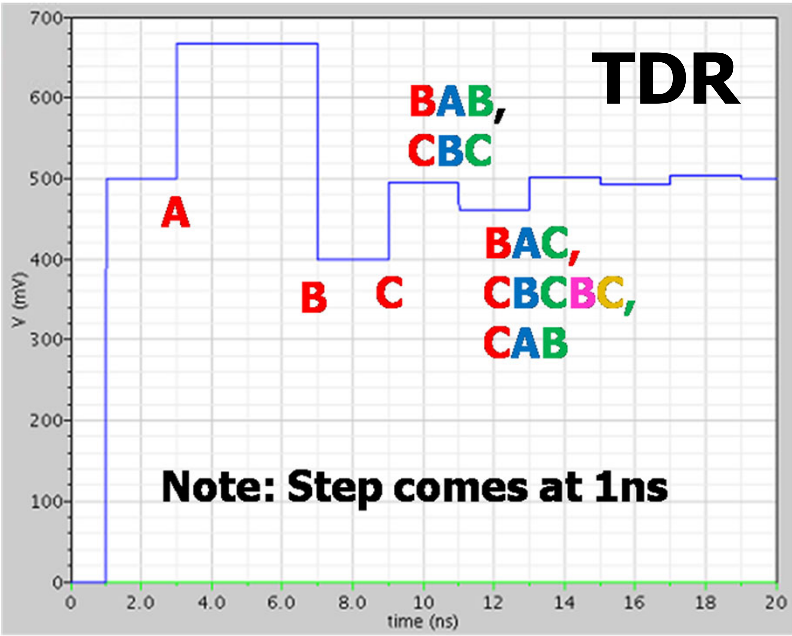
Time-Domain Transmission (TDT)

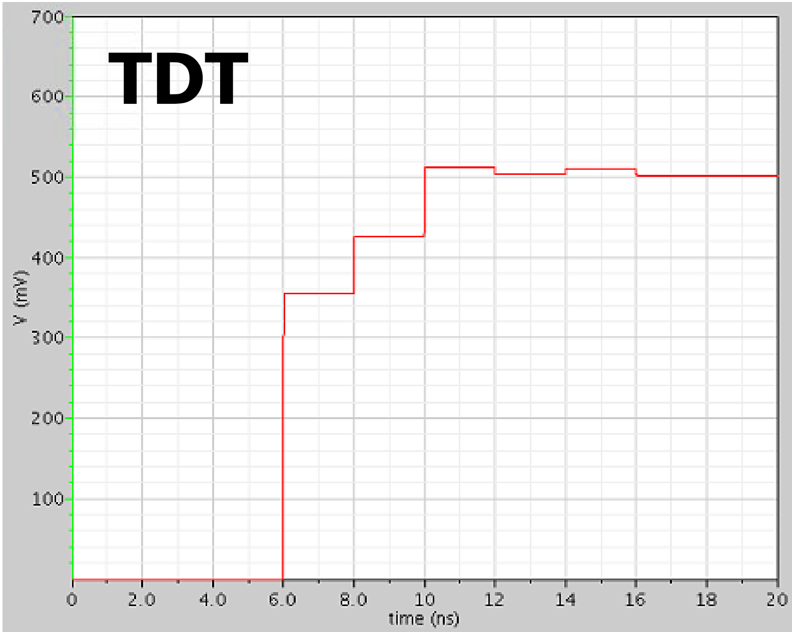


[Dally]

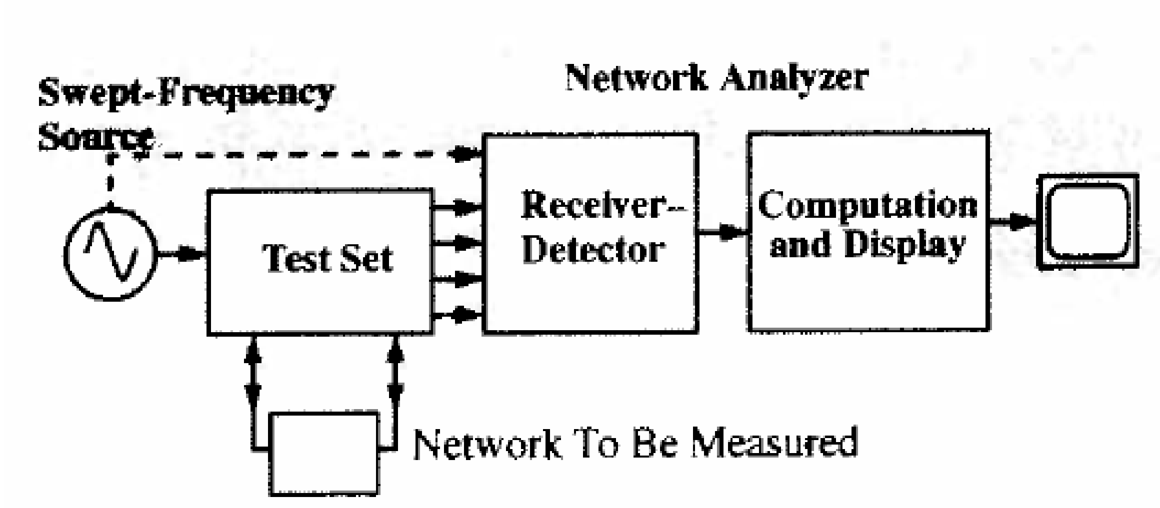
$$H(j\omega) = \frac{V_2(j\omega)}{V_1(j\omega)}$$

- Can measure channel transfer function
- Hard to isolate impedance discontinuities, as they are superimposed on a single rising edge





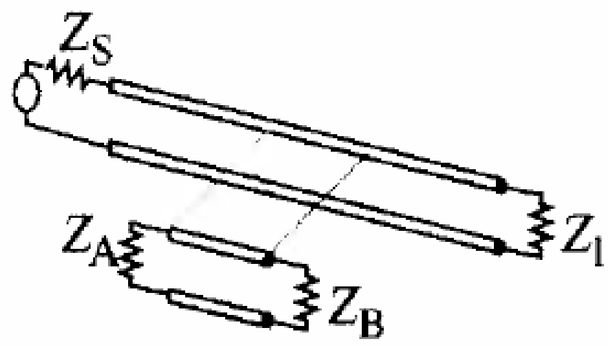
Network Analyzer



[Dally]

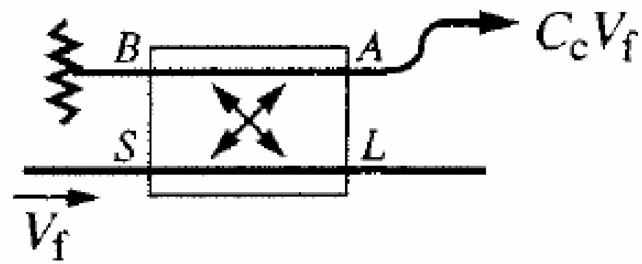
- Stimulates network with swept-frequency source
- Measures network response amplitude and phase
- Can measure transfer function, scattering matrices, impedance, …
- Test set is configured differently for each kind of measurement to be performed

Directional Coupler



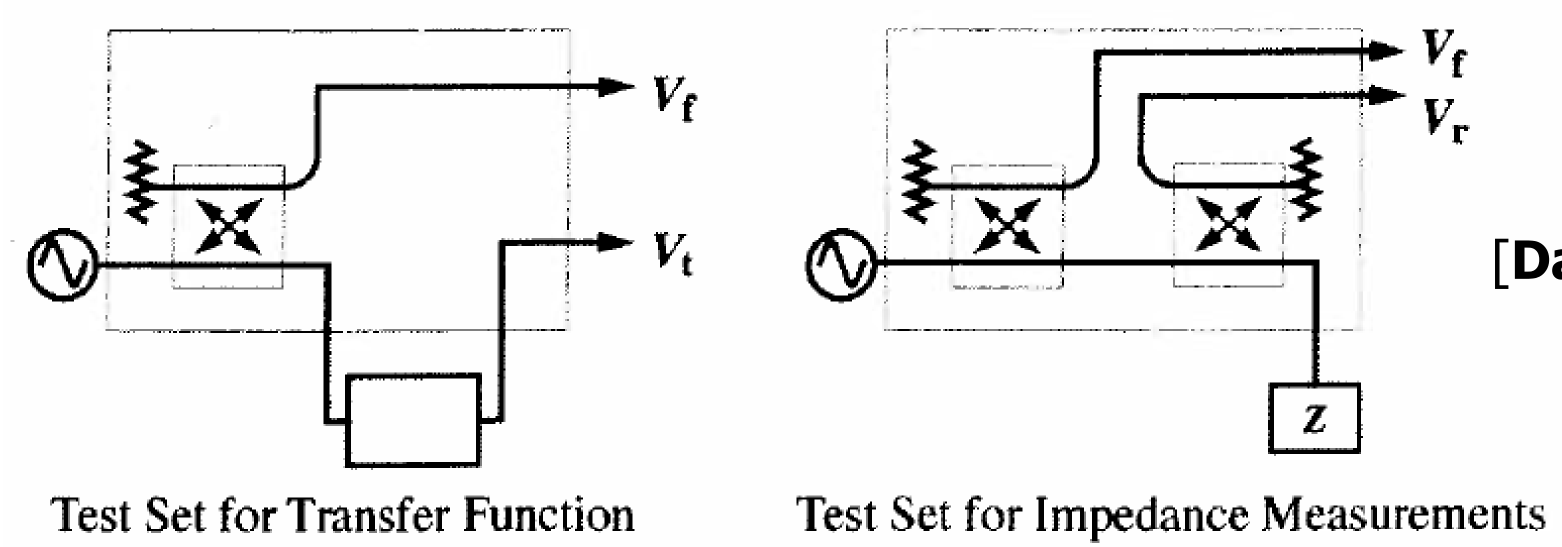
Direction Coupler

[**Dally**]



- Test sets in high-frequency network analyzers make use of directional couplers
- Directional couplers are two transmission lines coupled over a short distance
- If the short line is properly terminated, it allows for the voltage across Z_A to be proportional to the forward traveling wave and the voltage across Z_B to be proportional to any reflected wave

Transfer Function & Impedance Measurements



[Dally]

- Transfer function measurement
  - The input signal is from a directional coupler which samples the forward traveling wave
  - The network output serves as the output
- Impedance measurement
  - The input signal is from a directional coupler which samples the forward traveling wave
  - The reflected wave from the network is compared with this input to characterize the impedance over frequency

Scattering (S) Parameters

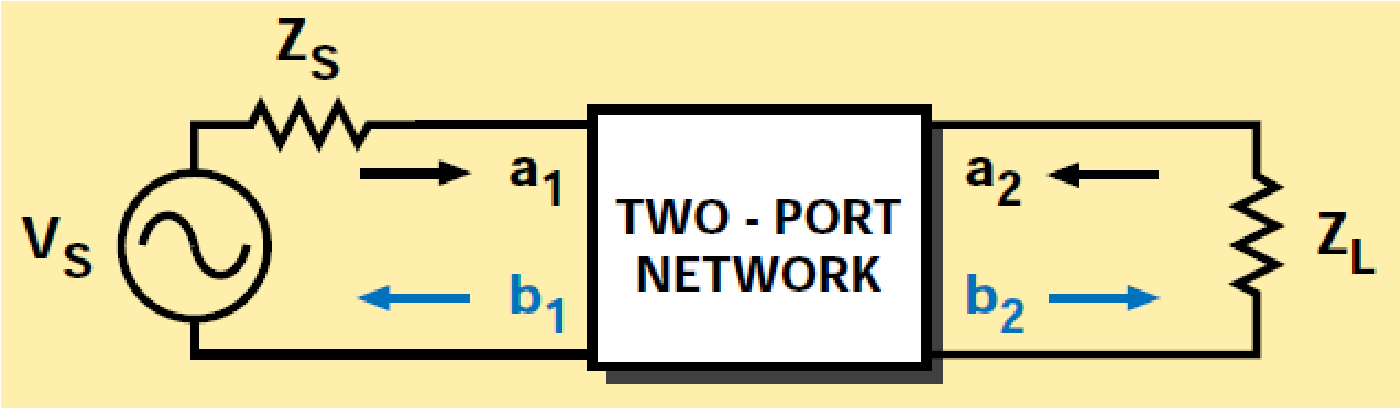
- Why S Parameters?
  - Easy to measure
  - Y, Z parameters need open and short conditions
  - S parameters are obtained with nominal termination
  - S parameters based on incident and reflected wave ratio

$$\begin{bmatrix} B_1 \\ B_2 \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} \cdot \begin{bmatrix} A_1 \\ A_2 \end{bmatrix}$$

S-matrix

[**Dally**]

Formal S-Parameter Definitions



[Agilent]

$$s_{11} = \left.\frac{b_1}{a_1}\right|_{a_2=0}$$ = Input reflection coefficient with the output port terminated by a matched load ($Z_L = Z_0$ sets $a_2 = 0$)

$$s_{22} = \left.\frac{b_2}{a_2}\right|_{a_1=0}$$ = Output reflection coefficient with the input terminated by a matched load ($Z_S = Z_0$ sets $V_s = 0$)

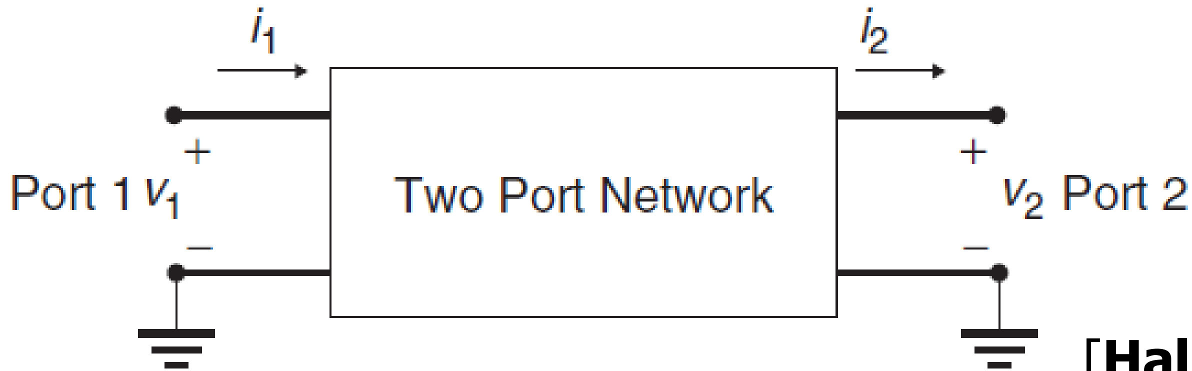
$$s_{21} = \left.\frac{b_2}{a_1}\right|_{a_2=0}$$ = Forward transmission (insertion) gain with the output port terminated in a matched load.

$$s_{12} = \left.\frac{b_1}{a_2}\right|_{a_1=0}$$ = Reverse transmission (insertion) gain with the input port terminated in a matched load.

Cascading S-Parameters

- Network analysis allows cascading of independently characterized structures
- However, can’t directly cascade s-parameter matrices and multiply
- Must first convert to an ABCD matrix (or T matrix)

ABCD Parameters



[Hall]

$$A = \left.\frac{v_1}{v_2}\right|_{i_{2=0}} \qquad B = \left.\frac{v_1}{i_2}\right|_{v_{2=0}} \qquad C = \left.\frac{i_1}{v_2}\right|_{i_{2=0}} \qquad D = \left.\frac{i_1}{i_2}\right|_{v_{2=0}}$$

$$\begin{vmatrix} v_1 \\ i_i \end{vmatrix} = \begin{vmatrix} A & B \\ C & D \end{vmatrix} \bullet \begin{vmatrix} v_2 \\ i_2 \end{vmatrix}$$

Converting Between S & ABCD Parameters

TABLE 9-3. Relationships Between Two-Port S and $ABCD$ Parameters[a]

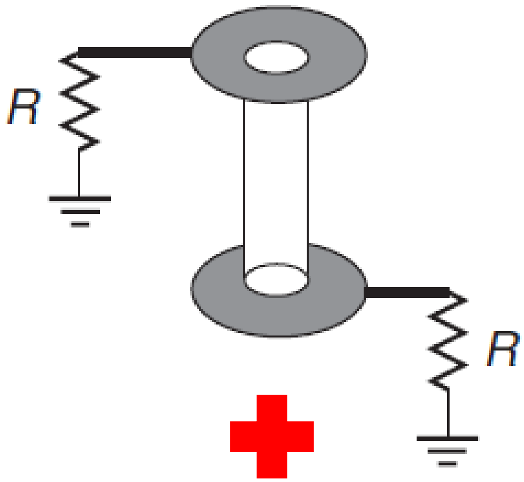
$$\begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} \qquad \begin{bmatrix} \dfrac{B - Z_n(D - A + CZ_n)}{B + Z_n(D + A + CZ_n)} & \dfrac{2Z_n(AD - BC)}{B + Z_n(D + A + CZ_n)} \\ \dfrac{2Z_n}{B + Z_n(D + A + CZ_n)} & \dfrac{B - Z_n(A - D + CZ_n)}{B + Z_n(D + A + CZ_n)} \end{bmatrix}$$

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} \qquad \begin{bmatrix} \dfrac{(1 + S_{11})(1 - S_{22}) + S_{12}S_{21}}{2S_{21}} & Z_n \dfrac{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}{2S_{21}} \\ \dfrac{1}{Z_n} \dfrac{(1 - S_{11})(1 - S_{22}) - S_{12}S_{21}}{2S_{21}} & \dfrac{(1 - S_{11})(1 + S_{22}) + S_{12}S_{21}}{2S_{21}} \end{bmatrix}$$

[a] Z_n is the termination impedance at the ports.

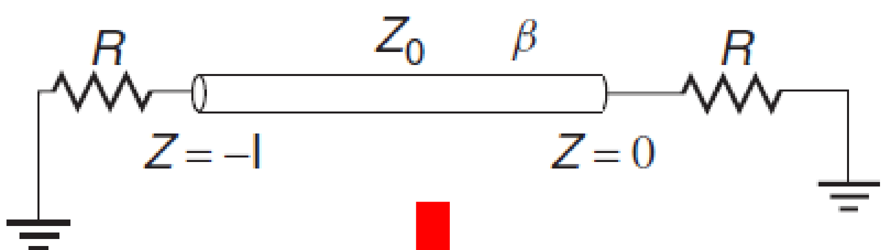
[Hall]

Example: Cascaded Via & Transmission Line



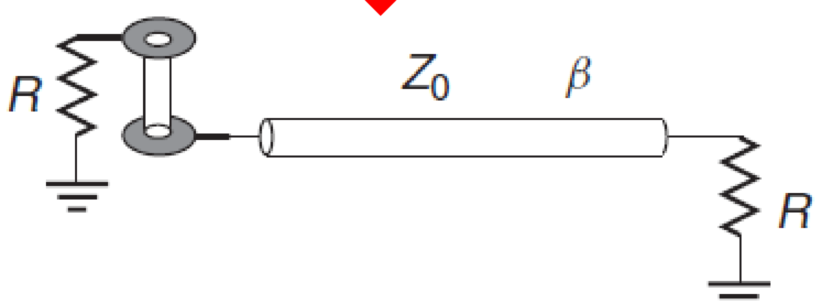
$$\begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix}_{\text{via}} = \begin{bmatrix} -0.1235 - j0.1516 & 0.7597 - j0.6190 \\ 0.7597 - j0.6190 & -0.1235 - j0.1516 \end{bmatrix}$$

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix}_{\text{via}} = \begin{bmatrix} 0.790 & j22.22 \\ j0.01686 & 0.790 \end{bmatrix}$$



$$\begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix}_{\text{t-line}} = \begin{bmatrix} 0.00325 - j0.00323 & -1.00 - j0.003 \\ -1.00 - j0.003 & 0.00325 - j0.00323 \end{bmatrix}$$

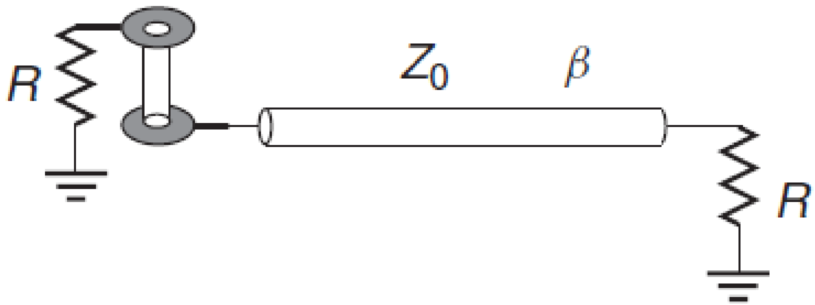
$$\begin{bmatrix} A & B \\ C & D \end{bmatrix}_{\text{t-line}} = \begin{bmatrix} -1 & j0.3228 \\ j0.000129 & -1 \end{bmatrix}$$



$$\begin{bmatrix} A & B \\ C & D \end{bmatrix}_{\text{cascade}} = \begin{bmatrix} A & B \\ C & D \end{bmatrix}_{\text{via}} \begin{bmatrix} A & B \\ C & D \end{bmatrix}_{\text{t-line}}$$

- Taken from "Advanced Signal Integrity for High-Speed Digital Designs" by Hall

Example: Cascaded Via & Transmission Line



$$\begin{bmatrix} A & B \\ C & D \end{bmatrix}_{\text{cascade}} = \begin{bmatrix} A & B \\ C & D \end{bmatrix}_{\text{via}} \begin{bmatrix} A & B \\ C & D \end{bmatrix}_{\text{t-line}}$$

$$= \begin{bmatrix} 0.790 & j22.22 \\ j0.01686 & 0.790 \end{bmatrix} \cdot \begin{bmatrix} -1 & j0.3228 \\ j0.000129 & -1 \end{bmatrix}$$

$$= \begin{bmatrix} -0.790 & -j21.965 \\ -j0.01686 & -0.795 \end{bmatrix}$$

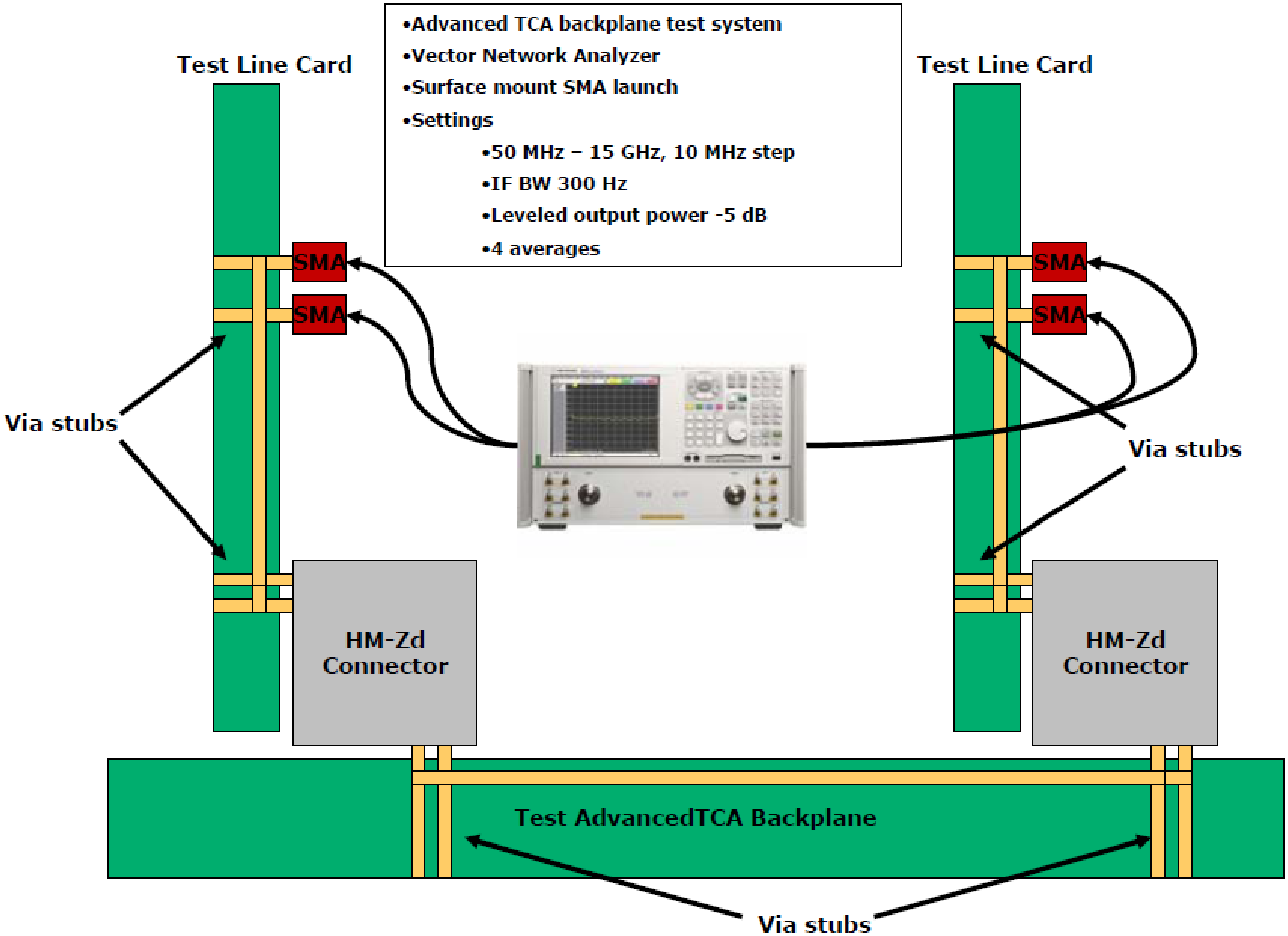
- Using conversion table:

$$\begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix}_{\text{cascade}} = \begin{bmatrix} -0.1259 - j0.1553 & -0.7635 + j0.6186 \\ -0.7645 + j0.6182 & -0.1200 - j0.1565 \end{bmatrix}$$

- Can also use T matrixes to cascade

- Taken from "Advanced Signal Integrity for High-Speed Digital Designs" by Hall

S-Parameter Channel Example



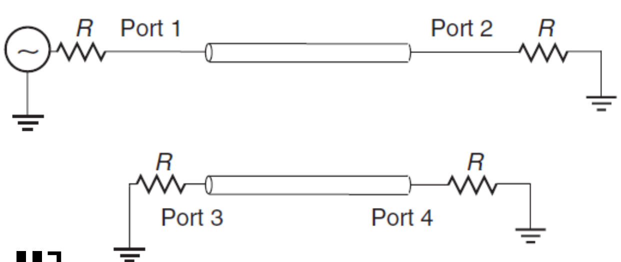
[**Peters, IEEE Backplane Ethernet Task Force**]

S-Parameter Channel Example (4-port differential)

```
! peters_01_0605_T20 channel thru response
#       HZ        S              RI           R       50
!
! FREQ                 S11                        S12                        S13                        S14
!                      S21                        S22                        S23                        S24
!                      S31                        S32                        S33                        S34
!                      S41                        S42                        S43                        S44
!                  REAL       IMAG            REAL       IMAG            REAL       IMAG            REAL       IMAG
5.00000000e+007  6.279266901548e-002 -5.256007502766e-002 -1.995363973143e-001 -9.018006169275e-001  7.405252014369e-002 -1.653914717779e-002  4.694410796534e-004  2.855671737566e-003
                -1.993592781969e-001 -9.017752677900e-001  6.847049395661e-002 -3.537762509466e-002  6.592975593456e-004  2.600733690373e-003  7.478976460177e-002 -1.488182269791e-002
                 7.438370524663e-002 -1.650568516548e-002  6.663957537997e-004  2.723661634513e-003  5.641343731365e-002 -5.693035832892e-002 -2.070369894915e-001 -8.986367167361e-001
                 3.380698172980e-004  2.715033111885e-003  7.497765935351e-002 -1.488546535615e-002 -2.063544808970e-001 -9.002700655374e-001  6.856095801756e-002 -3.019606086420e-002
6.00000000e+007  4.829977376755e-002 -6.288238652440e-002 -4.923832497425e-001 -7.721510464035e-001  6.298956599590e-002 -3.938489680891e-002  1.125377257145e-003  1.921732299021e-003
                -4.925547500023e-001 -7.726263821707e-001  6.163450406360e-002 -4.486265928179e-002  1.299644022342e-003  1.492436402394e-003  6.462146347807e-002 -3.736630924981e-002
                 6.308085276969e-002 -3.947655302643e-002  1.386741613180e-003  1.653454474207e-003  4.393874455850e-002 -6.448913049207e-002 -4.992743919180e-001 -7.660808533046e-001
                 1.280875740087e-003  1.936760526874e-003  6.482369657086e-002 -3.743006383763e-002 -4.995203164654e-001 -7.674804458241e-001  6.284893613667e-002 -4.132139739274e-002
```

Data from 50MHz to 15GHz in 10MHz steps

```
1.49900000e+010 -1.884123481138e-001  3.522933794755e-001  9.493645552321e-004  2.735890006358e-004  2.939002692375e-002 -8.676465491258e-003 -2.207496924854e-004  1.236065259912e-004
                 9.463443060684e-004  3.105615146344e-004 -1.742347383703e-001  4.813685271232e-002 -6.152705437030e-004  1.614752661571e-003  6.774475978813e-002  9.617239585695e-003
                 2.953403838205e-002 -8.707827389646e-003 -6.226849675423e-004  1.637610280621e-003 -1.595766021694e-001  3.757605914955e-001 -1.809501624148e-004 -7.061855554470e-004
                -2.613575703191e-004  1.368108929760e-004  6.788329666403e-002  9.551687705500e-003 -2.146293806886e-004 -7.363580847286e-004 -1.199804891859e-001  7.697336952293e-002
1.50000000e+010 -1.883176013184e-001  3.545614742110e-001  9.524680768441e-004 -5.404222971799e-005  2.935126165241e-002 -1.235086132268e-002 -1.616280086909e-004  2.347368458649e-004
                 1.039250921080e-003 -6.032017103742e-005 -1.649137634331e-001  4.966164587830e-002 -6.748937194262e-005  1.689652681670e-003  6.725041473699e-002  1.961009613152e-003
                 2.959693594806e-002 -1.251203706381e-002 -2.927441863297e-005  1.747754847916e-003 -1.531702433245e-001  3.773014940454e-001 -3.769459376261e-004 -5.671620228005e-004
                -2.089293612250e-004  2.303682313561e-004  6.740524959192e-002  1.672663579641e-003 -4.385850073691e-004 -5.810569604703e-004 -1.121319455376e-001  7.458173831411e-002
```



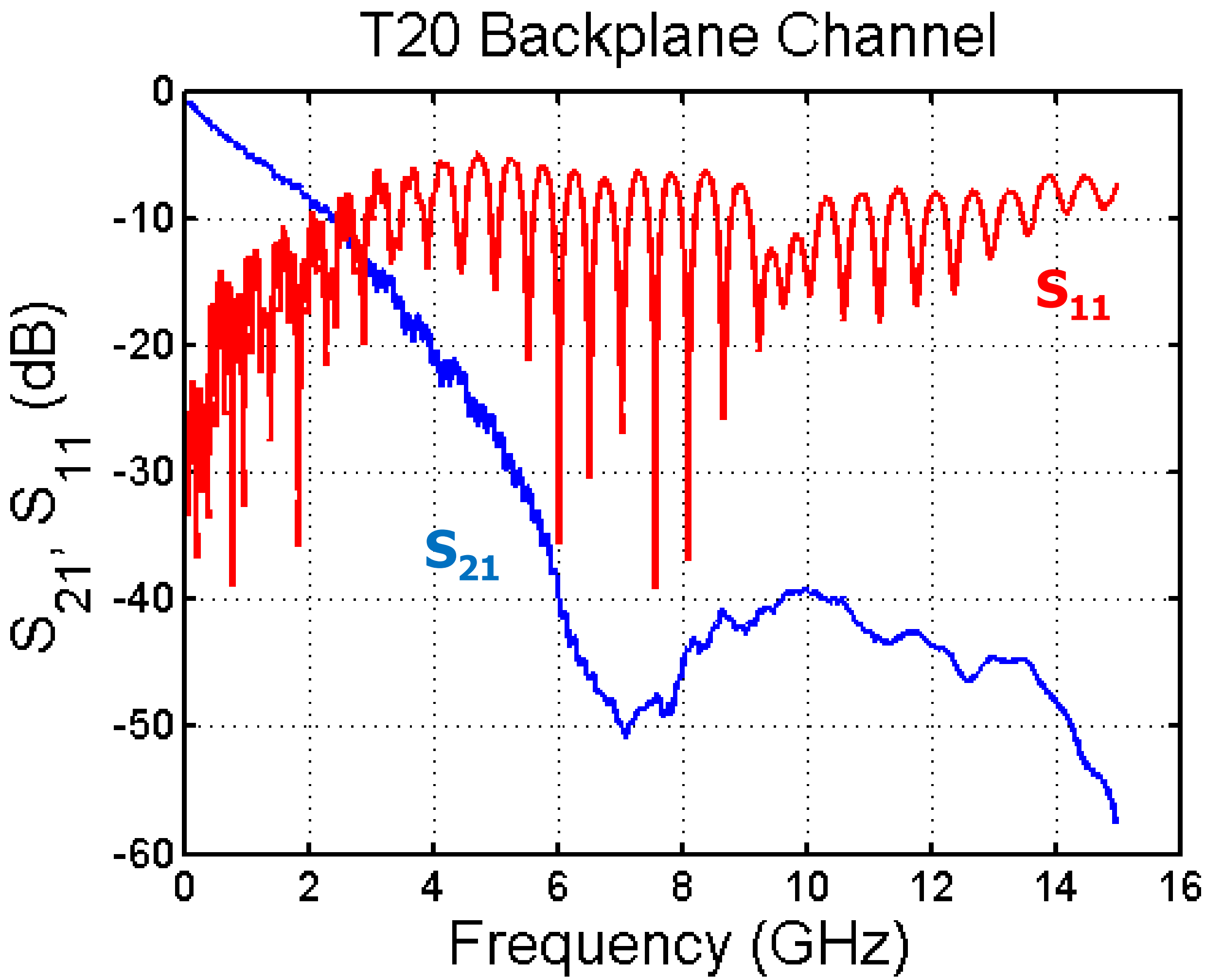
[Hall]

$$
\begin{bmatrix} b_1 \\ b_2 \\ b_3 \\ b_4 \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} & S_{13} & S_{14} \\ S_{21} & S_{22} & S_{23} & S_{24} \\ S_{31} & S_{32} & S_{33} & S_{34} \\ S_{41} & S_{42} & S_{43} & S_{44} \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} & S_{13} & S_{14} \\ S_{21} & S_{22} & S_{23} & S_{24} \\ S_{31} & S_{32} & S_{33} & S_{34} \\ S_{41} & S_{42} & S_{43} & S_{44} \end{bmatrix} \begin{bmatrix} v \\ 0 \\ -v \\ 0 \end{bmatrix}
$$

$$
S_{dd11} = \left. \frac{b_{d1}}{a_{d1}} \right|_{a_2 = a_4 = 0} = \frac{1}{2}\left(S_{11} + S_{33} - S_{13} - S_{31} \right)
$$

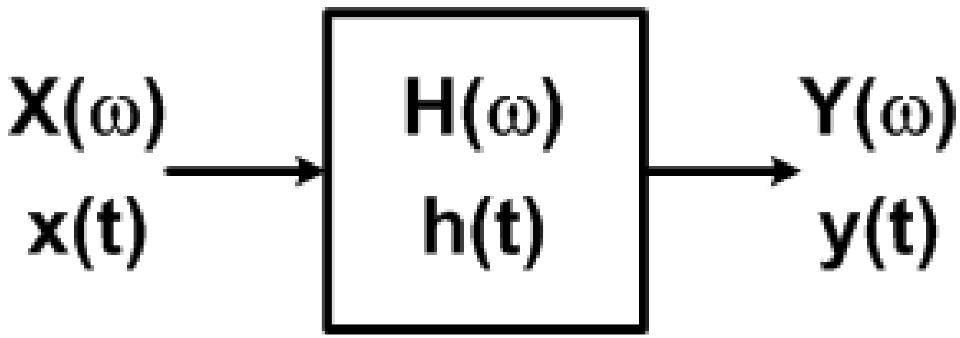
$$
S_{dd21} = \left. \frac{b_{d2}}{a_{d1}} \right|_{a_2 = a_4 = 0} = \frac{1}{2}\left(S_{21} + S_{43} - S_{23} - S_{41} \right)
$$

S-Parameter Channel Example



Impulse Response

- Channel impulse responses are used in
  - Time domain simulations
  - Link analysis tools



$$Y(\omega) = H(\omega)X(\omega)$$

$$y(t) = h(t) * x(t) = \int_{-\infty}^{\infty} h(t-\tau)x(\tau)$$

$$h(t) = F^{-1}\{H(w)\}$$

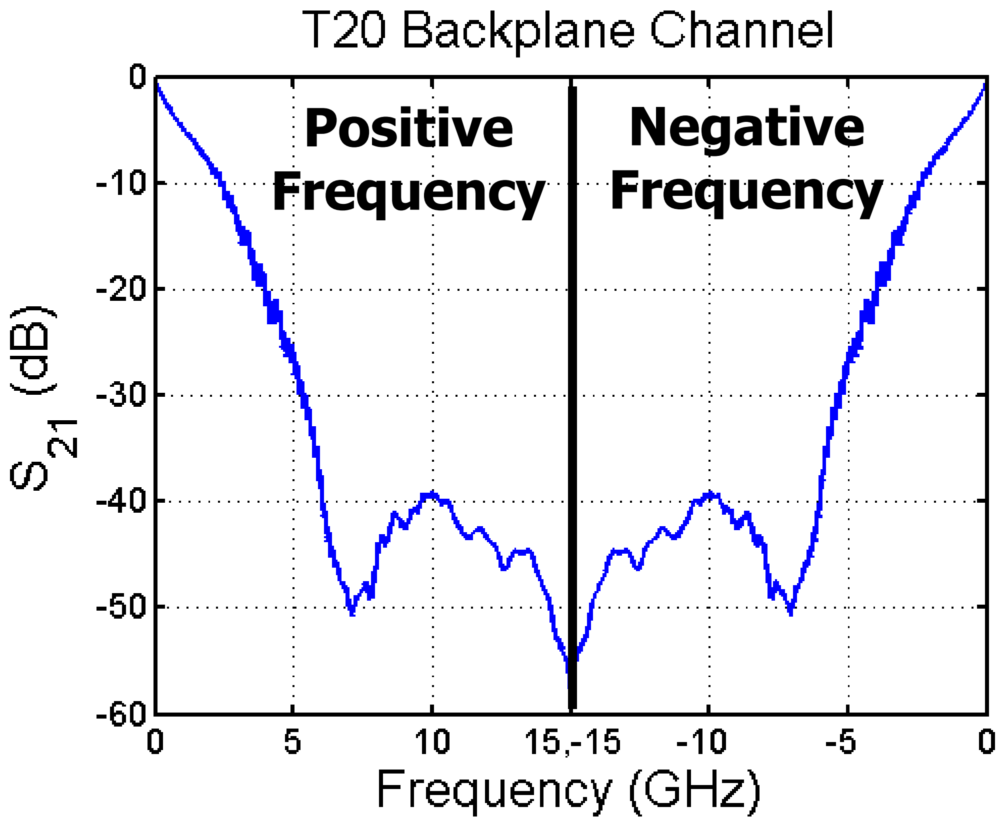
Generating an Impulse Response from S-Parameters

- Perform the inverse Fourier transform on the s-parameter of interest

$$h(t) = F^{-1}\{S(\omega)\}$$

- Step 1: For ifft, produce negative frequency values and append to s-parameter data in the following manner

$$S(-f) = S(f)^*$$



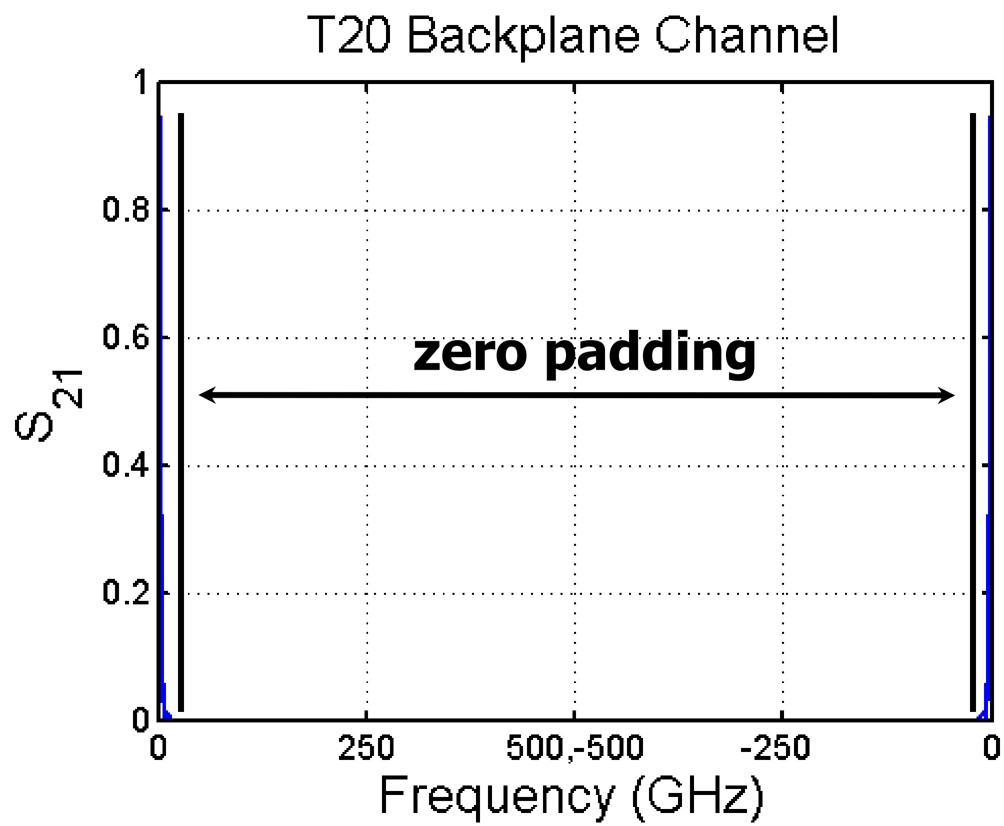
Increasing Impulse Response Resolution

- Could perform ifft now, but will get an impulse response with time resolution of

$$\frac{1}{2f_{\max}} = \frac{1}{2(15\text{GHz})} = 33.3\text{ps}$$

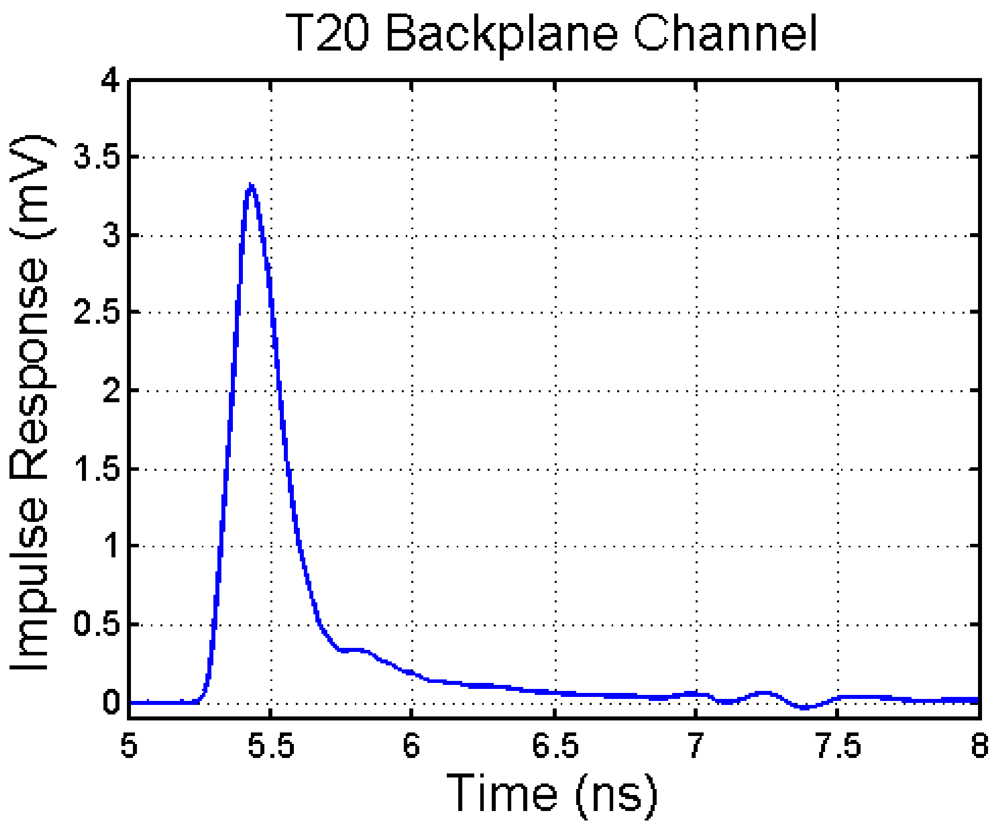
- To improve impulse response resolution expand frequency axis and "zero pad"

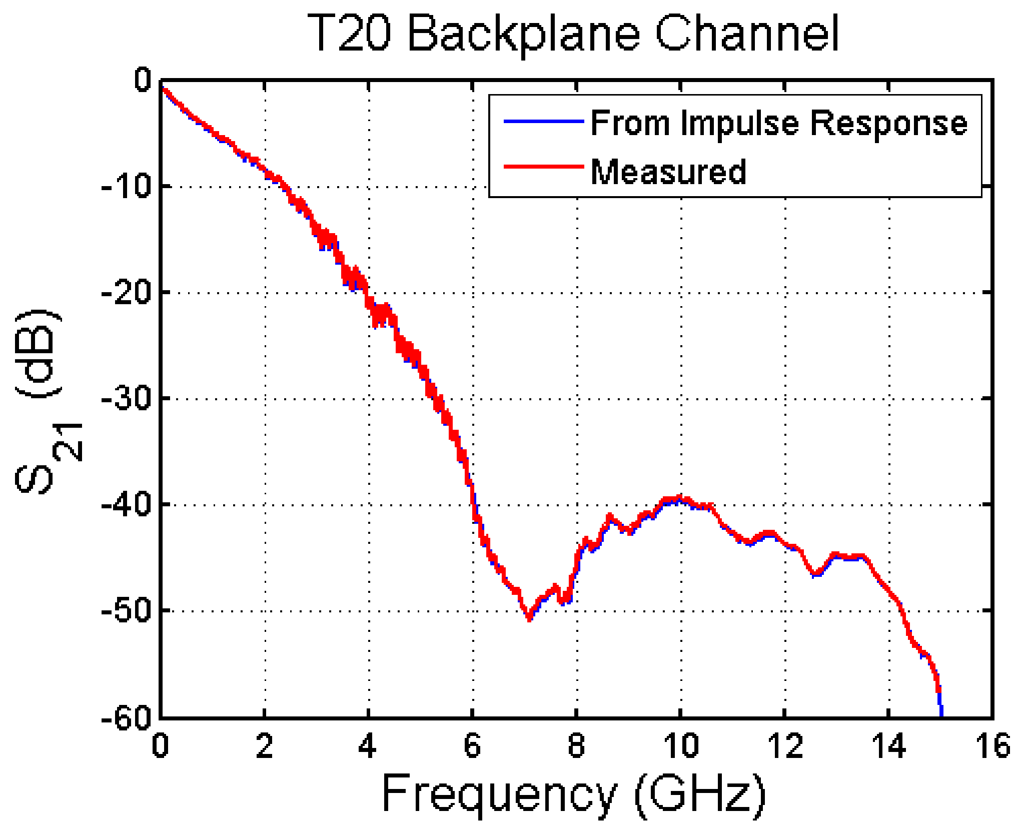
For 1ps resolution:
zero pad to +/-500GHz



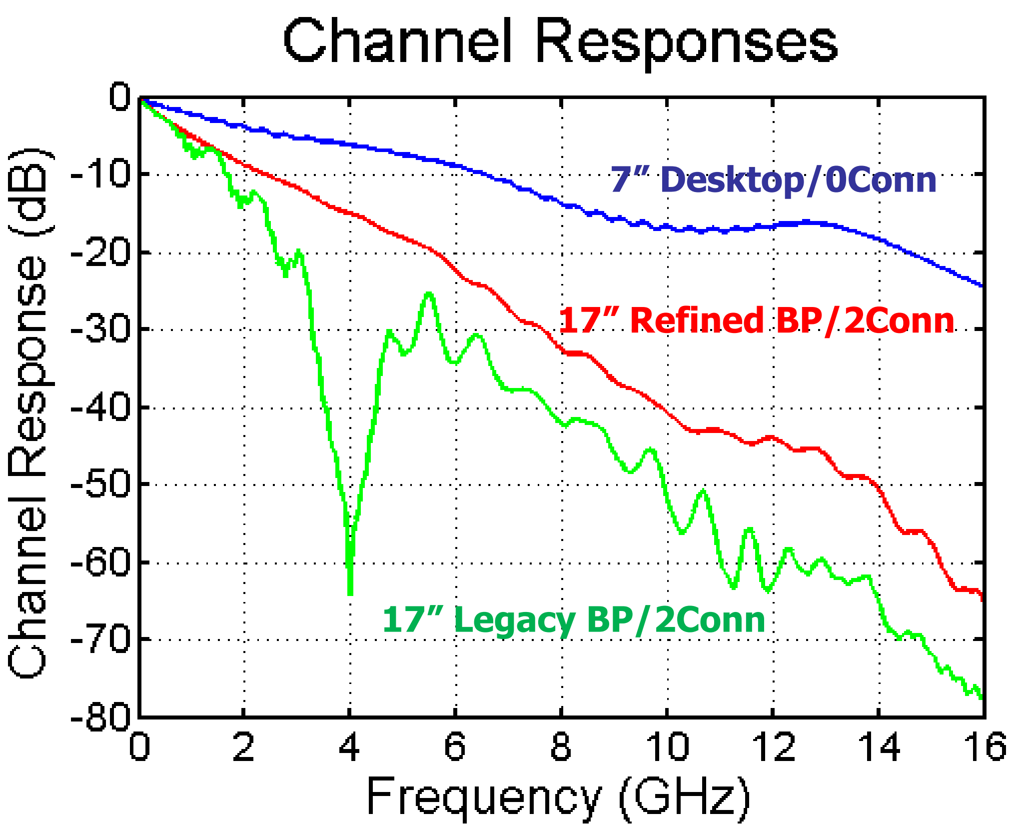
Channel Impulse Response

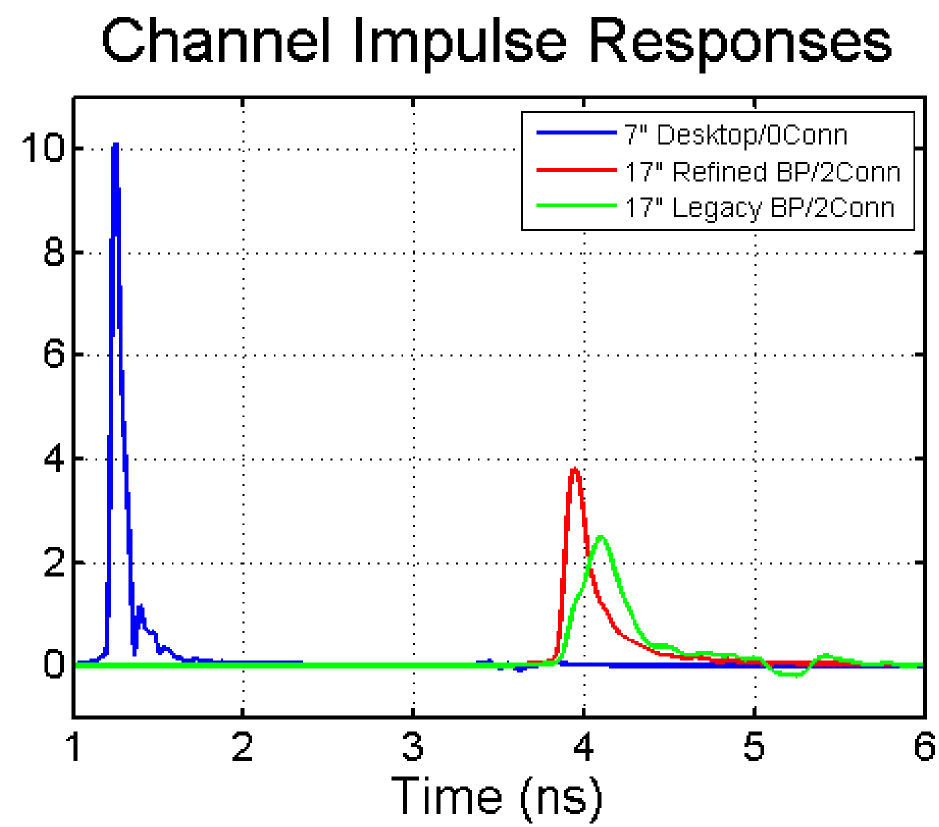
- Now perform ifft to produce impulse response
- Can sanity check by doing an fft on impulse response and comparing to measured data



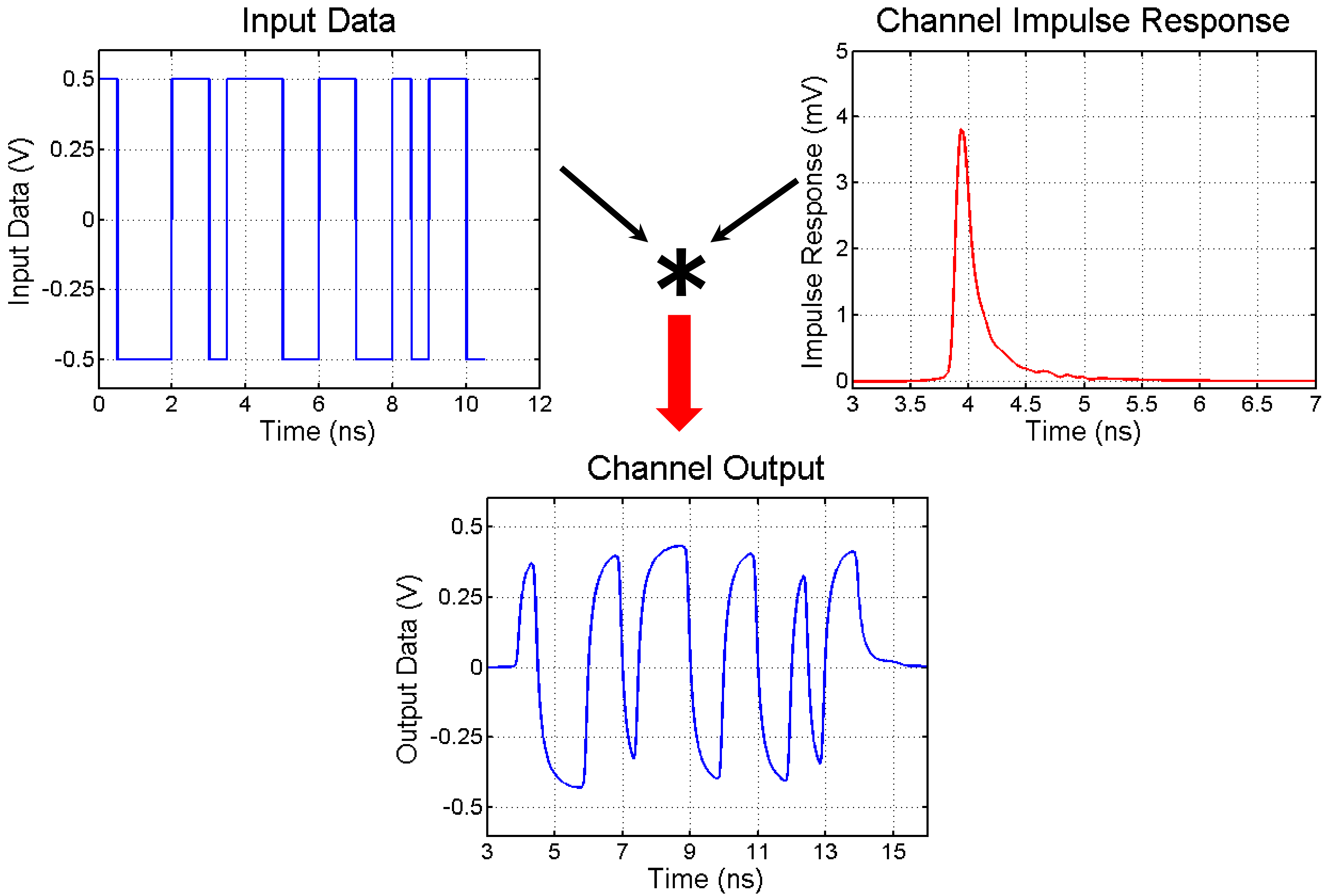


Impulse Response of Different Channels

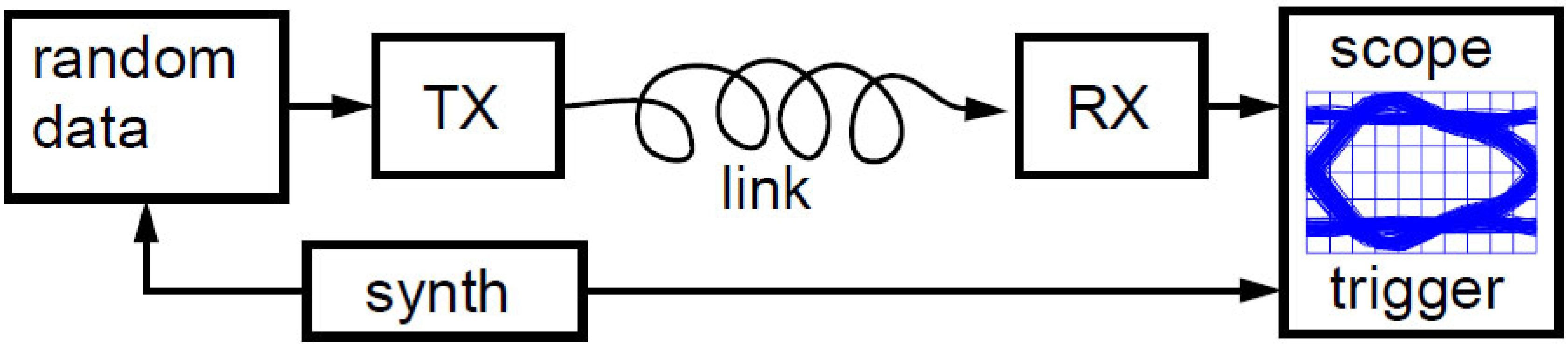


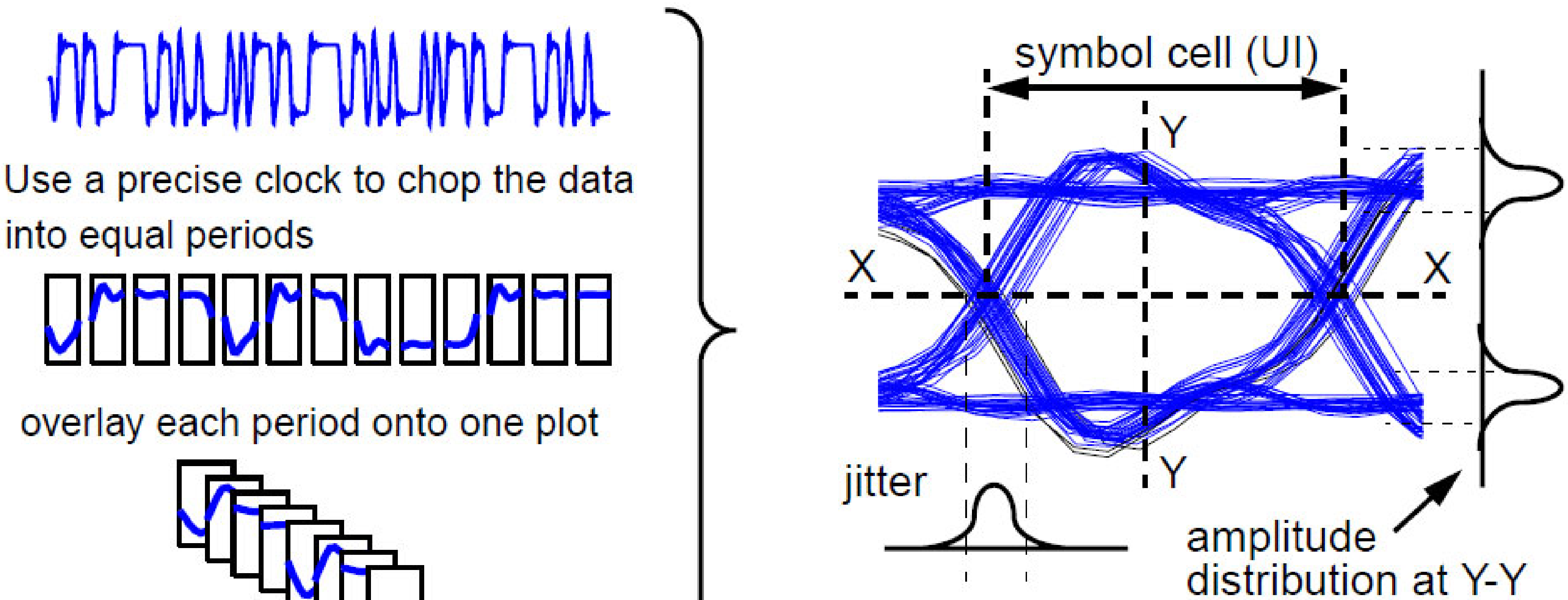


Channel Transient Response



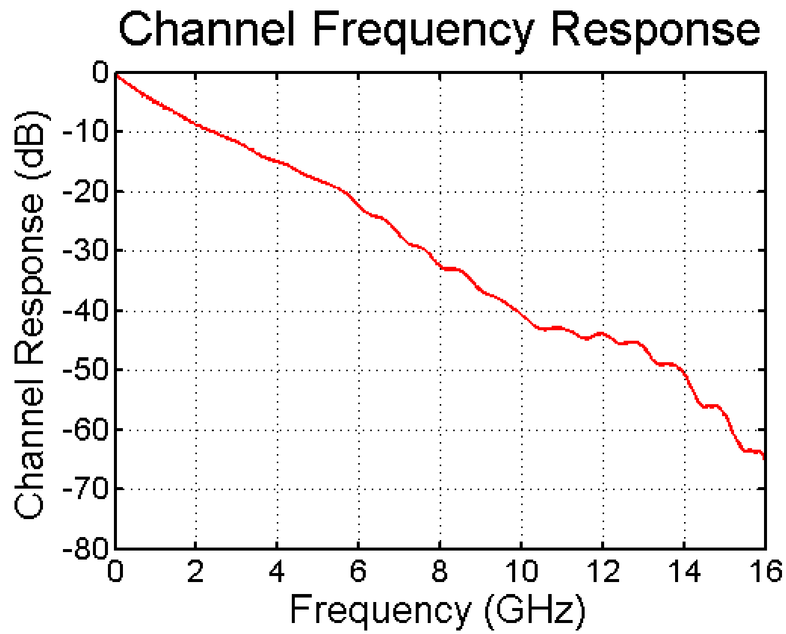
Eye Diagrams

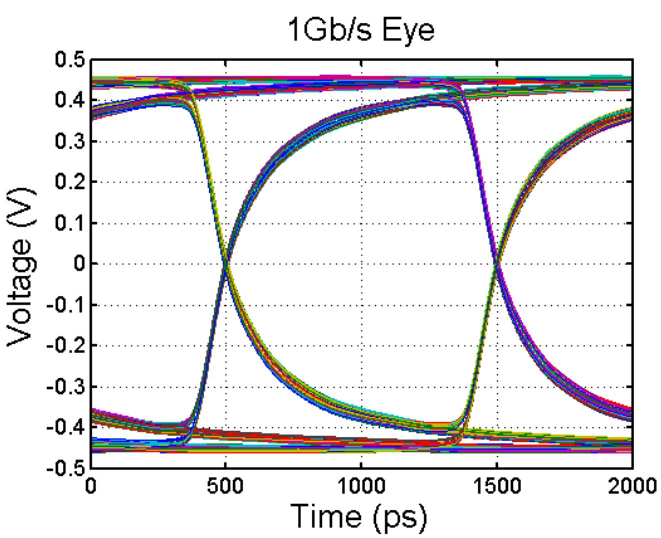


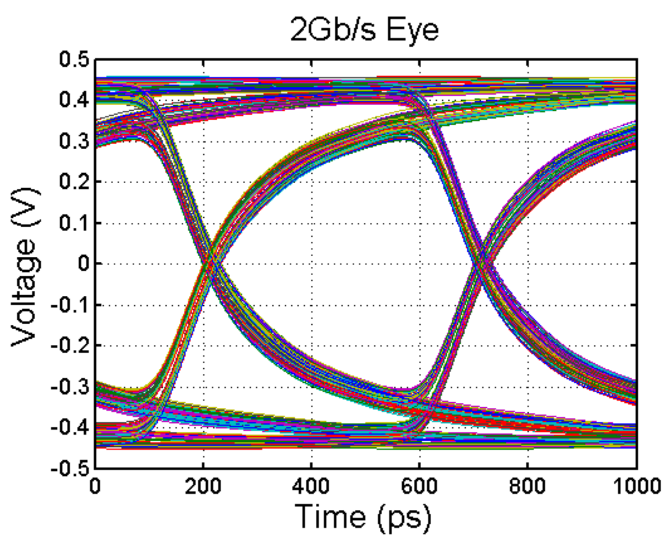


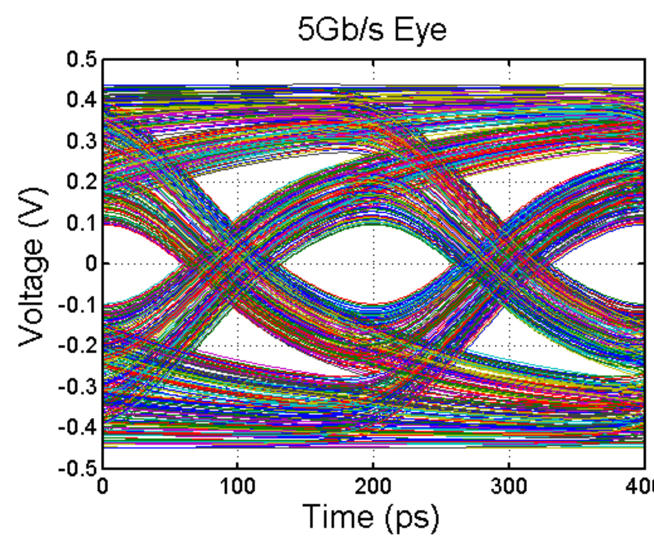
[**Walker**]

Eye Diagrams vs Data Rate

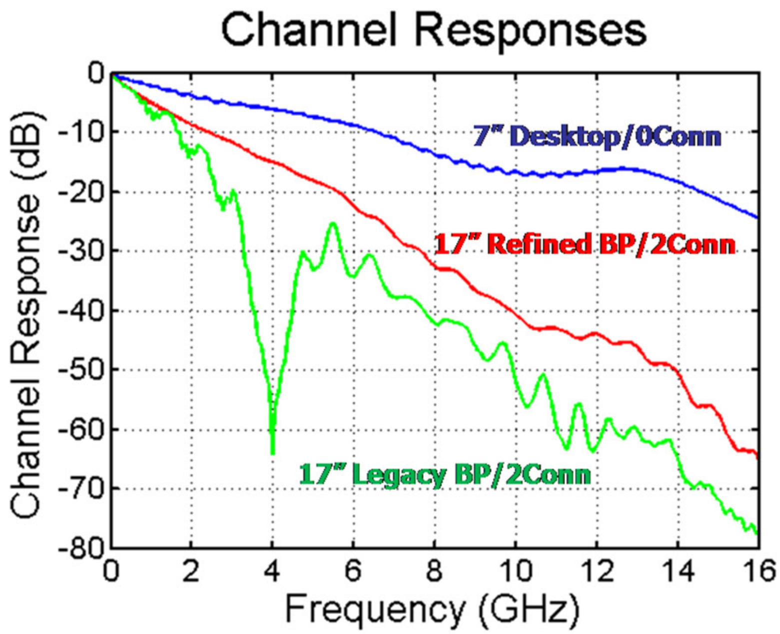


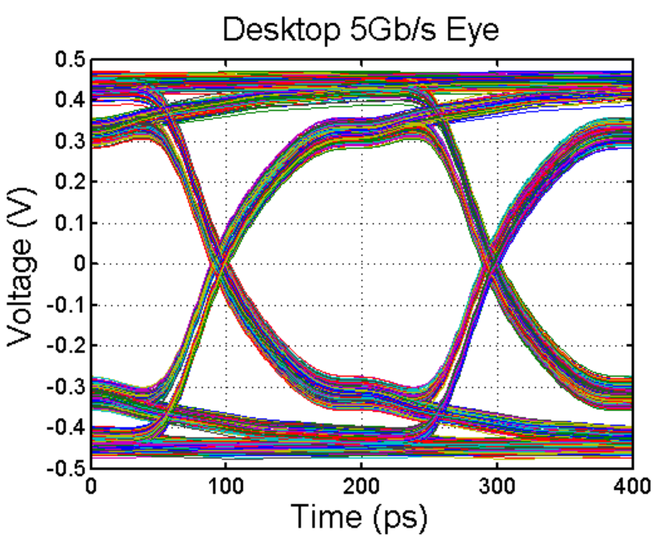


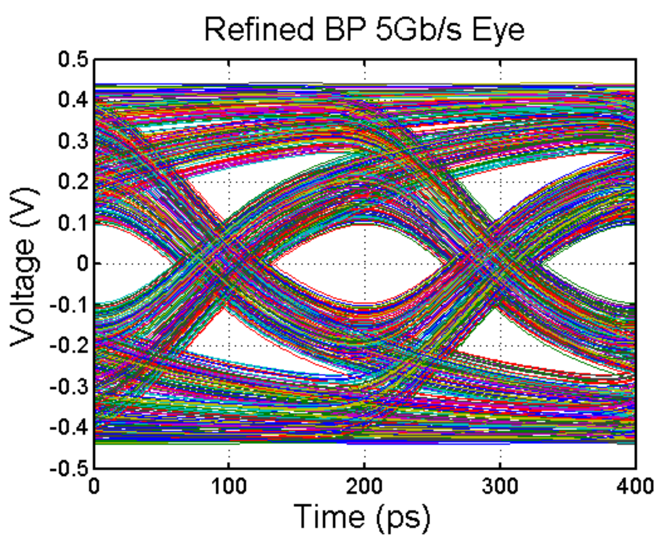


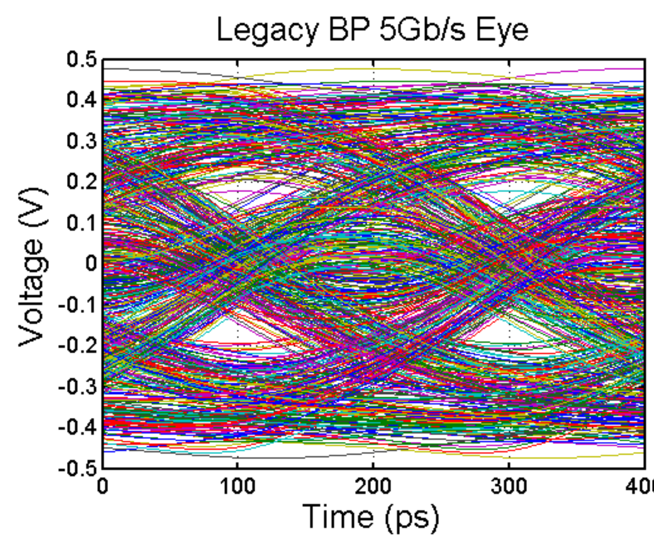


Eye Diagrams vs Channel



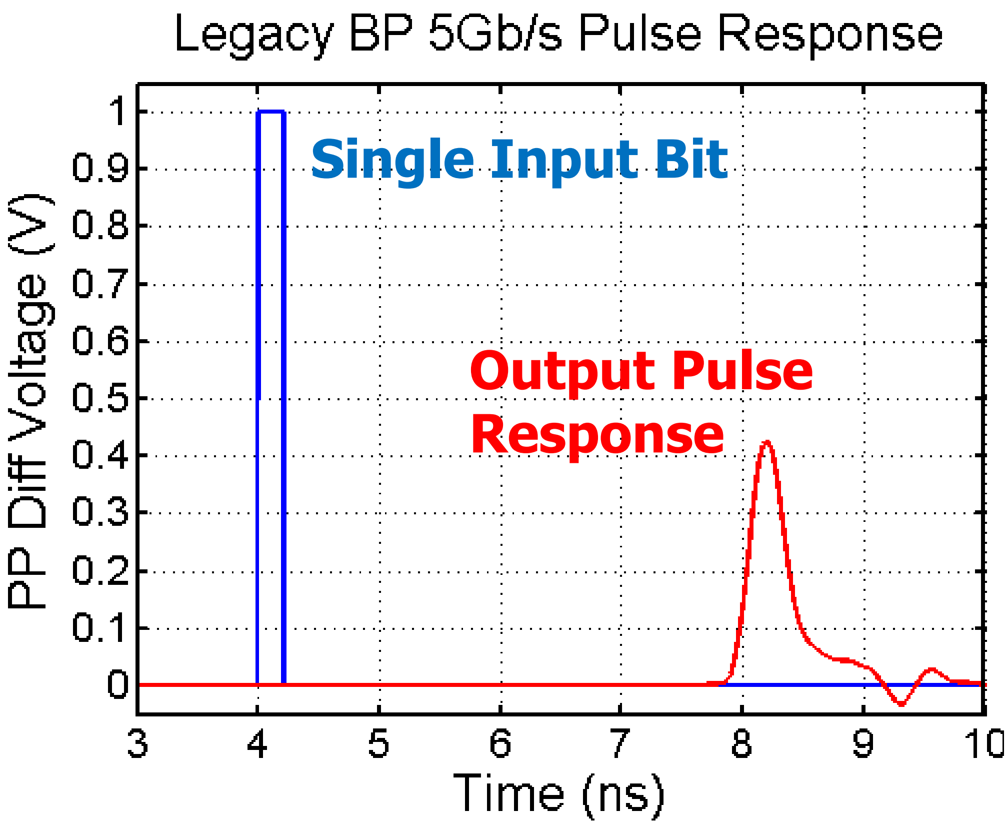


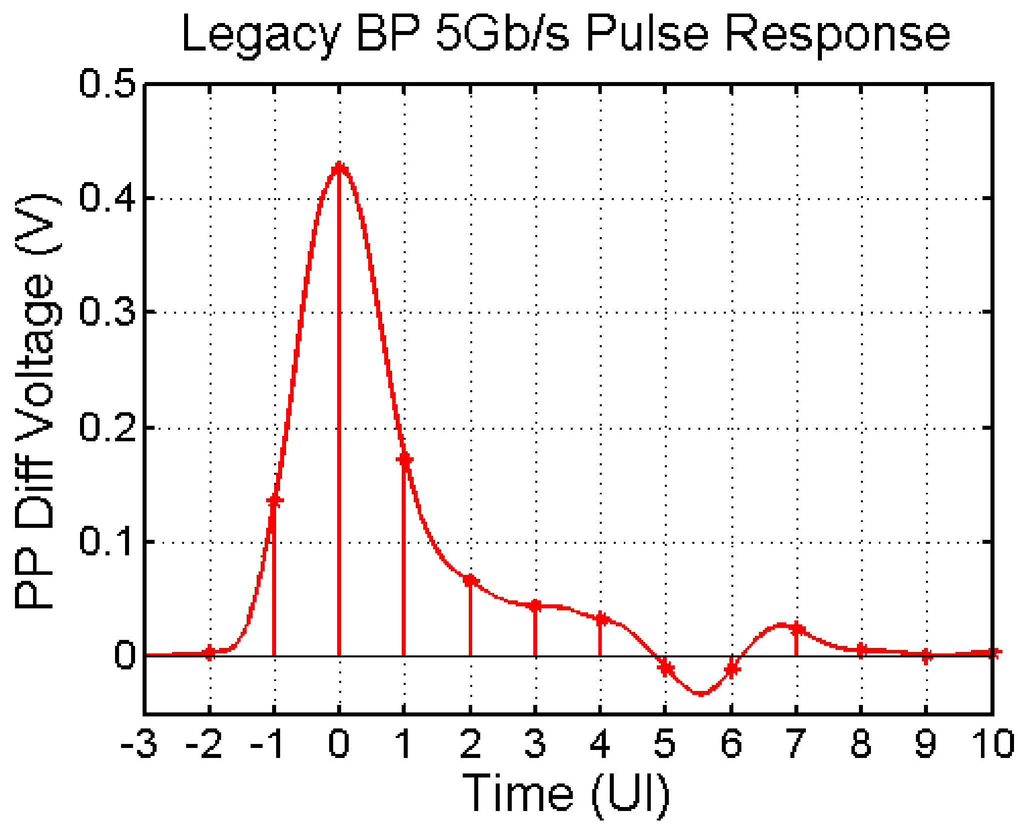




Inter-Symbol Interference (ISI)

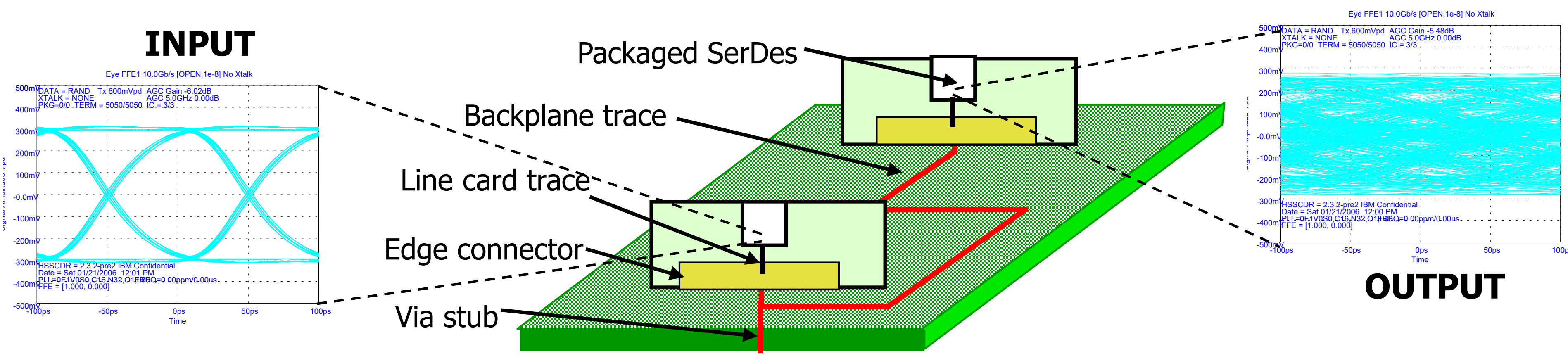
- Previous bits residual state can distort the current bit, resulting in inter-symbol interference (ISI)
- ISI is caused by
  - Reflections, Channel resonances, Channel loss (dispersion)





ISI Impact

- At channel input (TX output), eye diagram is wide open
- As data pulses propagate through channel, they experience dispersion and have significant ISI
  - Result is a closed eye at channel output (RX input)



[Meghelli (IBM) ISSCC 2006]

Next Time

- Channel pulse response model
- Modulation schemes