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NASA Contractor Report 3831

Development of a Turbomachinery
Design Optimization Procedure
Using a Multiple-Parameter
Nonlinear Perturbation Method



Stephen S. Stahara

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Design Optimization Procedure
Using a Multiple-Parameter
Nonlinear Perturbation Method

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SUMMARY

An investigation was carried out to complete the preliminary development of a combined perturbation/optimization procedure and associated computational code for designing optimized blade-to-blade profiles of turbomachinery blades. The overall purpose of the procedures developed in this study is to provide demonstration of a rapid nonlinear perturbation method for minimizing the computational requirements associated with parametric design studies of turbomachinery flows. The method reported here combines the multiple-parameter nonlinear perturbation method, successfully developed in previous phases of this study, with the NASA TSONIC blade-to-blade turbomachinery flow solver, and the COPES-CONMIN optimization procedure into a user's code for designing optimized blade-to-blade surface profiles of turbomachinery blades. Results of several design applications and a documented version of the code together with a user's manual are provided.

1. INTRODUCTION

The remarkable success of advanced computational methods for determining complex fluid dynamic phenomena has created a continuing demand both for increasing the accuracy and generality of these methods, as well as the desire to incorporate these methods into a routine use mode needed for design and parametric investigations. However, a major impediment to such routine use of many of these current and emerging computational codes is the high computational cost required in their direct application to situations requiring repetitive high-frequency use. Consequently, a real need exists for determining the means to reduce these costs while retaining the required accuracy in such nonlinear applications. While this need exists in virtually all engineering applications when relatively sophisticated numerical codes are employed, for turbomachinery applications it is particularly severe since both the underlying aerodynamic computation of the flow field is costly and also the number of flow and geometry parameters needed to be varied in design studies is large.

The ultimate objective of this investigation is to develop and demonstrate methods that would provide the means to reduce substantially the overall computational requirements necessary for turbomachinery design studies. It is conceived that these methods would be coupled with high run-time general turbomachinery computational flow field solvers and would be used in conjunction with them in applications where large numbers of related nonlinear turbomachinery solutions are required.

That such methods can be realized has been successfully demonstrated in the previous phases (Refs. 1-3) of this study. In the first of those investigations (Ref. 1), several candidate methods were studied and the most promising method was identified. Extensive development and testing of that method was then carried out in the subsequent phase (Ref. 2). This testing was performed for a wide variety of both flow and geometry parameters for turbomachinery flows past isolated blades and compressor cascades at both subcritical and supercritical conditions. Emphasis was placed in particular on strongly supercritical flows which exhibited large surface shock movements over the parametric range studied. Comparisons of the perturbation predictions with the corresponding exact nonlinear solutions indicated a remarkable accuracy and range of validity of the perturbation method. In the most recently completed phase (Ref. 3), the perturbation method was extended to treat simultaneous multiple-parameter perturbations. Extensive testing of the method has demonstrated remarkable accuracy and range of validity of the multiple-parameter perturbation procedure in direct correspondence with the previous results obtained for single-parameter perturbations. Additionally, initial applications of the multiple-parameter

perturbation method combined with an optimization procedure were made (Ref. 3) to several turbomachinery blade design problems. The results demonstrated the potential of the perturbation method for reducing the computational work in such applications by an order of magnitude with no degradation in accuracy.

The work reported here describes the continued development of the combined multiple-parameter perturbation method/ optimization procedure. The primary objective of this phase is on the development of that combined procedure into an operational method for designing optimized blade-to-blade profiles of turbomachinery compressor blades.

2. ANALYSIS

2.1 Perturbation Concept

The obvious method of carrying out a perturbation analysis, that is by establishing and solving a series of linear perturbation equations in the manner of Van Dyke (Ref. 4), appears to be an obvious choice for the current application. The initial phase of this study (Ref. 1) established that for sensitive flows, such as occur in turbomachinery, the basic linear variation assumption fundamental to the technique is sufficiently restrictive that the allowable range of parameter variation is so small as to be of little practical use. A novel alternative to the linear perturbation equation approach was then subsequently developed and successfully tested (Refs. 1-3) in which a correction method is used that employs two or more nonlinear solutions obtained from the basic nonlinear flow solver, rather than just one as in the linear perturbation equation approach. For this alternative method, the basic perturbation solution is determined simply by differencing two nonlinear flow solutions removed from one another by some nominal change of a particular flow or geometrical quantity. A unit perturbation solution is then obtained by dividing that result by the change in the perturbed quantity. Related solutions are determined by multiplying the unit perturbation by the desired parameter change and adding that result to the base flow solution. This simple procedure, however, only works directly for continuous flows for which the perturbation change does not alter the solution domain. For those perturbations which change the flow domain, coordinate stretching is necessary to ensure proper definition of the unit perturbation solution. For discontinuous flows, special coordinate straining is necessary to account for movement of discontinuities due to the perturbation.

At this point, the perturbation concept based on these ideas has both been implemented and thoroughly tested in a wide range of applications (Refs. 1-3, 5-11). These applications have purposely involved a number of different nonlinear flow field solvers to provide the base solutions necessary for the perturbation calculation. The most extensive and systematic of these studies are reported in References 2, 3, 9, and 11, where results are provided for case studies involving a variety of different flow and geometry parameter perturbations of nonlinear subsonic and transonic flows past isolated blade and compressor cascade geometries. For those applications, emphasis was placed in particular on strongly supercritical transonic flows which exhibit large surface shock movements over the parameter range studied. By extensive comparisons with the exact nonlinear solutions, these studies have established the accuracy, range of validity, and versatility of the perturbation method.

The underlying reason of the remarkable accuracy of the perturbation method developed in this study lies in the use of coordinate straining to define the unit perturbation. As shown in Figure 1, where the perturbation between two nonlinear solution states is displayed graphically as the shaded area between the base and the strained and unstrained calibration solution, coordinate straining provides the ability to account accurately for the displacement of a multiple number of discontinuities and maxima of high-gradient regions due to a parameter change. This enables the perturbation method to maintain very high accuracy in regions of high gradients where most perturbation methods commonly fail, and to maintain that accuracy over large parametric ranges.

In what follows, we provide a brief account of the theoretical essentials of the strained-coordinate perturbation concept as it configured and implemented in the present design application. This is to predict simultaneous multiple-parameter perturbation flow solutions for blade surface properties of turbomachinery blades for use in optimized blade design. The turbomachinery flow solutions thus considered can contain a total number N of discontinuities or high-gradient continuous regions. Complete details of the mathematical basis of the method, in particular, the application to flow field properties, may be found in Reference 3.

For the prediction of distributions of surface properties involving simultaneous multiple-parameter perturbations of aerodynamic flows where flow properties are required along some contour, the strained-coordinate, first-order, multiple-parameter perturbation approximation can be represented by

$$Q(x; \epsilon) = Q_0(s) + \sum_{j=1}^M \epsilon_j Q_{1j}(s) + \dots \quad (1)$$

$$x = s + \sum_{j=1}^M \epsilon_j x_{1j}(s) + \dots \quad (2)$$

where x is the independent variable measuring distance along the surface contour or some convenient projection of that distance, s is the strained coordinate, and ϵ_j a small parameter representing the change in one of M flow or geometrical variables which we wish to vary simultaneously.

In order to determine the first-order corrections $Q_{1j}(s)$, we require one base and M calibration solutions in which the calibration solutions are determined by varying each of the M

arbitrary independent parameters q_j by some nominal amount from the base flow value while keeping the others fixed at their base-line values.

In this way, the first-order corrections $Q_{1j}(s)$ can be determined as

$$Q_{1j}(s) = \frac{Q_{c_j}(\bar{x}_j) - Q_o(s)}{\bar{\epsilon}_j} \quad (3)$$

where Q_{c_j} is the calibration solution corresponding to changing the j th parameter to a new value q_{c_j} , \bar{x}_j is the strained coordinate pertaining to the Q_{c_j} calibration solution, and $\bar{\epsilon}_j = q_{c_j} - q_{o_j}$ represents the change in the q_j parameter from its base flow value. If we now desire to keep invariant during the perturbation process a total of N points corresponding to discontinuities or high-gradient maxima, we can represent the first-order solution by

$$Q(x, \epsilon_j) = Q_o(s) + \sum_{j=1}^M \epsilon_j Q_{1j}(s) \quad (4)$$

where $Q_{1j}(s)$ is given above and

$$\bar{x}_j = s + \sum_{i=1}^N \bar{\epsilon}_j \delta x_i x_{1_i}(s) \quad (5)$$

$$x = s + \sum_{i=1}^N \epsilon_j \delta x_i x_{1_i}(s) \quad (6)$$

$$\bar{\epsilon}_j = q_{c_j} - q_{o_j} \quad (7)$$

$$\epsilon_j = q_j - q_{o_j} \quad (8)$$

$$\bar{\epsilon}_j \delta x_i = \left(x_i^c - x_i^o \right)_j \quad (9)$$

$$\epsilon_j \delta x_i = \frac{\epsilon_j}{\bar{\epsilon}_j} \left(x_i^c - x_i^o \right)_j \quad (10)$$

Here $\bar{\epsilon}_j \delta x_i$ given in Equations (5) and (9) represent the displacement of the i th invariant point in the j th calibration solution from its base flow location due to the selected change $\bar{\epsilon}_j$ in the q_j parameter given by Equation (7), $\epsilon_j \delta x_i$ given in Equations (6) and (10) represents the predicted displacement of the i th invariant point from its base flow location due to the desired change ϵ_j in the q_j parameter given by Equation (8), and $x_{1_i}(s)$ is a unit-order straining function having the property that

$$x_{1_i} \left(x_k^o \right) = \begin{cases} 1 & k = i \\ 0 & k \neq i \end{cases} \quad (11)$$

which assures alignment of the i th invariant point between the base and calibration solutions.

In References 2 and 3, detailed studies were made of the effect of different straining functions on the accuracy of the perturbation result. In Reference 3, identification was made of a superior class of straining functions for use in general non-linear applications. This class turns out to be comprised of linear piecewise-continuous straining functions, and particular members of this class have proven effective in all case studies undertaken to date. It has been found that this type of straining function is able to maintain high accuracy of the perturbation predictive result in the vicinity of the invariant points, and furthermore, this class of straining function introduces no excessive straining in regions removed from those locations. Occurrence of the latter phenomenon has been found to be a common failure of certain other classes of straining functions (Refs. 2, 3).

The functional forms of the straining for linear piecewise-continuous straining functions can be compactly written. For example, the strained coordinate \bar{x}_j , in Equation (5) is given by

$$\bar{x}_j = s + \left\{ \frac{x_{i+1}^o - s}{x_{i+1}^o - x_i^o} \cdot \left(x_i^c - x_i^o \right)_j + \frac{s - x_i^o}{x_{i+1}^o - x_i^o} \cdot \left(x_{i+1}^c - x_{i+1}^o \right)_j \right\} H \left(x_{i+1} - s \right) \cdot H \left(s - x_i^o \right) \quad (12)$$

where H denotes the Heaviside step function. In addition to the points corresponding to discontinuities or high-gradient maxima, it is usually also necessary in coordinate straining to hold invariant both of the end points along the contour. Consequently, for the application developed here, the array of invariant points in the base and calibration solutions are taken as

$$\begin{aligned} x_i^o &= \{0, x_1^o, x_2^o, \dots, x_n^o, 1\} \\ x_{i_j}^c &= \{0, x_{1_j}^c, x_{2_j}^c, \dots, x_{n_j}^c, 1\} \end{aligned} \tag{13}$$

where the contour length has been normalized to unity and where n is the number of invariant points along the blade contour exclusive of the end points.

2.2 Combination of Perturbation Method with Optimization Procedures for Blade Design

One of the major objectives of the previous phase of this investigation (Ref. 3) was the demonstration of the capability of the perturbation method to work effectively in an important nonlinear design environment related to turbomachinery. The particular application selected was optimized turbomachinery blade design. Toward the above objective, the perturbation method, configured to treat simultaneous multiple-parameter changes, was combined with proven optimization procedures (Refs. 12, 13). Next, performance and design constraints characteristic of certain turbomachinery blade design problems were constructed. Finally, applications of the combined procedure to several case studies involving blade profile optimization were made. The objectives of these initial applications were to demonstrate the workability of the perturbation concept in a design environment, provide a benchmark of the potential for computational savings of the combined perturbation/optimization procedure for some typical design problems, and determine the accuracy of the perturbation-predicted results for these cases.

Two different types of optimization problems were considered. The first set of case studies involved isolated blades and were more fundamental in nature, while the second set involved a practical turbomachinery compressor blade design. For the first set of studies, the particular isolated blade design optimization problems selected for study involved the alteration of a baseline profile shape by adding to the baseline profile a set of shape functions according to the relation

$$Z(x) = Z_0(x) + \sum_{i=1}^M A_i F_i(x) \quad (14)$$

where Z_0 are the ordinates of the baseline profiles, F_i are the shape functions, and the coefficients A_i are the design variables whose values are determined by the optimization process as a result of a search through design-variable solution space to achieve a desired design improvement. The general class of geometric shape functions employed, which have been found to be successful in previous applications involving optimization of supercritical airfoil sections (Ref. 14), consisted of exponential decay functions and sine functions. These are of the general form $(1 - x) \cdot x^p / e^{qx}$ and $\sin(\pi x^r)^n$, where the exponents p , q , r , and n are selected to provide a desired ordinate maximum at a particular chordwise location. The exponential functions are generally employed to provide adjustments near the leading edge, while the sine functions are used to provide maximum ordinate changes at particular chordwise stations. Illustrations of the chordwise variation of typical members of these classes of shape functions are provided in Figure 2, and it can be seen that these functions smoothly concentrate ordinate thickness at selected locations. Consequently, they can be used effectively to add a series of smoothly blended bumps or scallops at selected locations along a baseline blade profile in order to control locally the flow characteristics at particular sections on the blade.

A strategy that has proven convenient for performing optimization studies involving aerodynamic performance parameters (Ref. 14) has been to recontour the profile shape so as to tailor the surface pressure distribution to conform to a desired distribution. This type of objective provides local control over the basic aerodynamic surface flow property of importance, and provides a means of attempting to achieve aft pressure gradients sufficiently weak to avoid separation. An important corollary advantage of using such an objective is that viscous separation can be minimized. This allows use of an inviscid aerodynamic flow solver in the optimization process rather than a much more computationally-expensive viscous solver, and assures that the optimization result thus obtained at the inviscid level is representative of the actual flow.

In such studies, the characteristics that are primarily sought after in the optimization process are the minimization of both the peaky behavior near the leading edge and the compressive gradient on the aft portion of the suction surface that typically exists on the baseline profiles considered. This is illustrated schematically in Figure 3. For two of the three series of case

studies undertaken for isolated blades, the objective function was taken as the minimization of the mean squared error between the predicted and desired surface pressure distribution, i.e.,

$$OBJ = \sum_{k=1}^K \left[C_{P_{\text{predicted}}}(x_k) - C_{P_{\text{desired}}}(x_k) \right]^2 \quad (15)$$

where K represents the number of chordwise locations x_k where desired and calculated surface pressures are compared. For the third series, the objective function was chosen to be the drag coefficient squared, a much more sensitive quantity. The optimization procedure employed was the now-standard CONMIN code (Ref. 12).

The detailed results presented in Reference 3 for the three case studies on isolated blades clearly established the ability of the perturbation method to work accurately in a highly non-linear multiple-parameter design environment. This was found to be true for both subcritical as well as strongly supercritical flow situations. The supercritical case study employing drag coefficient as the objective function demonstrated the advantages and accuracy benefits of multiple invariant point clustering in high-gradient regions as well as an explicit straining concept for determining the perturbation result. Finally, the potential for computational savings with the perturbation method in such optimization problems was benchmarked at an order of magnitude, and the possibility was demonstrated of even obtaining in some cases improved results in terms of a more global minima of the objective function with employing the perturbation method as compared to not using it.

The final set of case studies involved the optimization of realistic compressor blades and was directed toward laying the foundations of a practical turbomachinery blade design/optimization procedure coupled with the simultaneous multiple-parameter perturbation method. The combined code consisted of the TSONIC blade-to-blade flow solver (Ref. 15) with generalized circular-arc blade geometry routines BLADE (Ref. 16) to describe the blade profiles, and the more generalized COPES-CONMIN optimization procedure (Ref. 13). The combined PERTURB/TSONIC/BLADE/COPES-CONMIN procedure, called BLDOPT, was tested on several NASA designed case studies to demonstrate the accuracy and capability of the combined procedure on problems typical of practical turbomachinery blade design. These case studies involved, as design variables, selected geometry parameters related to the NASA/Lewis circular-arc blade profiles. The optimization objective usually chosen was the minimization of the peak suction surface velocity diffusion. Although that choice of objective is a somewhat sensitive selection since it represents a point

quantity in a high-gradient region, the combined procedure was able to demonstrate good results, with computational work savings comparable to those found in the previous case studies (Ref. 3).

In these case studies, however, because the design variables were selected as basic geometry parameters (blade curvature, maximum blade thickness, etc.) related to the circular-arc blade geometry, the optimization search problem itself becomes more sensitive. This occurs because these design variables by their very nature effect more global changes in the aerodynamic solution and therefore tend to interact more strongly with each other than would a corresponding optimization problem which employs, say, local shape functions as the design variables. For the latter case, the design variables generally effect only local changes in the aerodynamic solution and therefore tend to interact much more weakly with one another. Consequently, optimization problems posed with such design variables are usually much more stable and less sensitive to small changes in search direction.

However, the ability to employ basic blade geometry parameters as design variables is very attractive as it relates directly to the capability of performing the more general preliminary blade design problem where a wide universe of basic blade shapes is considered. This contrasts to the problem involving use of local shape functions as design variables which relates to a more specific refined-design problem where the basic blade profile has already been selected. The ability to treat both problems is important, with the former being the more general and more difficult to do.

3. RESULTS

Because the ultimate utility of the perturbation methods being developed under this investigation is in optimized turbomachinery design, the primary objective of the current study was to complete the development of the combined PERTURB/TSONIC/BLADE/COPES-CONMIN procedure (BLDOPT) for performing optimized turbomachinery blade-to-blade surface profile design, and to finalize the procedure into a user's code so as to make generally available such a procedure to facilitate future use and testing by the general turbomachinery community. Toward that end, we have completed the assembly and preliminary verification testing of the four component codes configured into a combined program and controlled under a user-friendly executive program.

A number of features have been incorporated into the current version of the BLDOPT program reported here, which were not available in the preliminary version reported in Reference 3. These features considerably enhance both the capability and generality of the method. An explicit straining procedure, which in essence specifies the points at which the final solution results are determined rather than allow these points to be determined implicitly from the straining of the base flow points as was done standardly in the past, has been implemented in the present BLDOPT code. The explicit procedure avoids a double interpolation of the perturbation result and has been found to yield significantly improved accuracy in high-gradient regions at only a very slight increase in computational work. In addition to the explicit straining procedure, the updated BLDOPT code has incorporated several new options available to the user when employing the perturbation method. These options, which are controlled by the parameter IOPT defined in Section A.4 of the user's manual, relate to the way the calibration solution matrix is defined. One of these options provides the user with a basically automatic hands-off procedure for using the perturbation method. Under this option, the user is not required to preselect and input the design variable values for the calibration solution matrix. Rather the matrix is determined completely by the program in the following way. For the first optimization cycle, the perturbation method is not used. Full nonlinear aerodynamic solutions are determined by the flow field code as required as input for the gradient and search optimization calculations. After the first search cycle is complete and a new design point determined, design variable values for the calibration solution matrix are then determined based on the direction that the first search cycle has taken. This results in an extremely good definition of the calibration solution matrix. The result is that the design variable solution space which is subsequently searched on the second and successive optimization searches usually requires only very reasonable interpolations/extrapolations within the design variable parameter range of the defined solution matrix.

This option (IOPT = 3) provides the automatic user-invisible procedure for defining the calibration solution matrix. An additional option (IOPT = 2) which requires user-input for defining the calibration solution matrix has also been incorporated into the code. Within this option, the calibration matrix definition can be accomplished by either individually specifying all the design variables (ICALB = 1) or alternatively (ICALB = 0) by employing a constant-value calibration stepsize which increments each design variable by this fractional change of its base flow value. The automatic IOPT = 3 option requires the additional cost of one optimization search cycle using full aerodynamic flow field solutions over that of the IOPT = 2 option which in contrast requires a user-input of the design variable values for the calibration solutions. Nevertheless, the IOPT = 3 option provides a highly accurate and basically hands-off means of employing the perturbation method and is recommended for use when no information is available on search direction from previous related calculations.

In terms of final design variable accuracy and potential computational time savings using this IOPT = 3 option, in Figures 4 and 5 we present comparisons of a severe test of this option for the optimization results for a 5 design variable supercritical pressure tailoring case study on an isolated blade using blade contour shape functions similar to those reported in Reference 3. Figure 4 provides a comparison of the perturbation-predicted final design variables and objective function (●) with results obtained with not using the perturbation method but employing full nonlinear full potential aerodynamic solutions throughout (⊙). These are the results after 5 optimization cycles. We note the essentially exact correspondence between the final design variable values. Corresponding comparison of the objective function, in fact, indicate a slightly better result obtained by the perturbation method (■). In Figure 5, the corresponding comparison of computational work in CPU seconds and objection function reduction per optimization search cycle is provided. Here we see that after the first cycle is complete, the perturbation procedure actually requires less time to define the calibration matrix solution and complete the second search than does the full nonlinear flow field method with the same reduction in objective. From that point on, the perturbation method requires essentially no time to complete searches 3 to 5, and then an additional increment to calculate the final design result using the nonlinear flow field solver. Time savings achieved with the perturbation method for this case is 58% of that required for the full nonlinear result. These and similar results obtained with the IOPT = 3 option confirm the utility of the automatic user option for defining the calibration solution matrix.

With regard to the particular optimization problem toward which the BLDOPT program has been configured, the following eight blade geometry parameters that are commonly used to characterize NASA circular-arc blade section profiles (Ref. 16) have been incorporated as design variables:

<u>Blade Geometry Parameter</u>	<u>Program Name</u>
Blade camber angle at inlet	KICR
Blade camber angle at outlet	KOCR
Transition location/chord	T
Maximum thickness location/chord	ZM
Inlet/outlet turning rate ratio	P
Blade maximum thickness/chord	TMX
Leading edge radius/chord	THLE
Trailing edge radius/chord	THTE

These geometry parameters are illustrated graphically in Figure 6. For more details about the geometry of these classes of blade shapes, we refer the reader to Reference 16. In the BLDOPT program, any arbitrary combination up to six of the above parameters may be used in the optimization analysis.

The sample optimization problem that has been examined to verify the combined procedure employs, as a design objective, the minimization of the velocity diffusion on the blade suction surface, i.e.,

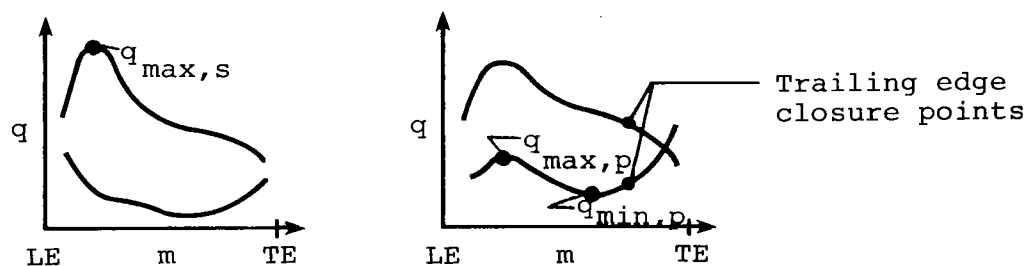
$$OBJ = \frac{q_{\max, \text{suction}}}{q_{\text{avg}, \text{exit}}} \quad (16)$$

where $q_{\max, \text{suction}}$ is the maximum surface velocity on the blade suction surface and $q_{\text{avg}, \text{exit}}$ is the average exit velocity in the freestream. Six of the eight design variables described above are employed: blade outlet camber angle, KOCR; transition location between fore and aft circular arc sections, T; maximum thickness location, ZM; inlet to outlet turning rate ratio, P; maximum thickness, TMX; and radius of the leading edge circle, THLE. During the optimization process, each of the design variables was constrained to remain within certain prescribed bounds in order to prevent a physically-unrealistic blade design from occurring. Furthermore, several active side constraints were additionally imposed both to insure design of a physically-realistic blade and also to achieve certain desirable flow

characteristics on the blade. The active side constraints employed were:

1. Maintenance of nonzero local blade thickness
2. Maintenance of low velocity diffusion on the blade pressure surface
3. Trailing edge closure via an effective Kutta condition

The basis of the first constraint is self-evident and is necessary since various combinations of the basic circular-arc blade geometry parameters can easily result in the upper and lower blade surface arcs crossing and thus lead to negative thickness. To understand the basis of the second and third constraints, it is helpful to examine the typical blade surface velocity plot as determined by the TSONIC solver. As sketched below in the plot on the left,



Baseline profile

During optimization

the baseline profile has a large peak suction velocity which is desired to be reduced. It is also desirable to maintain on the pressure surface as uniform a velocity distribution as possible and, furthermore, to avoid a large mismatch in the upper and lower surface velocities at the trailing edge. During the optimization process, it is sometimes found that the lower surface velocity can develop peaks, such as shown in the plot on the right, and that the velocity distributions may cross ahead of the trailing edge. The constraints constructed to alleviate these occurrences are as follows. In order to keep large differences between the pressure surface velocity maxima and minima from occurring, we enforce the condition

$$0.0 < \frac{q_{\max, \text{press}}}{q_{\min, \text{press}}} < 1.3$$

where $q_{\max, \text{pres}}$ is the maximum blade pressure surface velocity over the front half of the blade and $q_{\min, \text{press}}$ is the minimum blade pressure surface velocity over the last two-thirds of the blade. Restricting the maximum velocity considered to the front half of the blade and the minimum velocity to the rear of the blade prevents the maximum from moving rearward and the minimum from moving forward and thereby defeating the constraint. To maintain an effective Kutta condition at the rear of the blade, we enforce the condition

$$-1 < \frac{q_{\text{ITE-2, suction}} - q_{\text{ITE-2, press}}}{25} < 1$$

Here, $q_{\text{ITE-2, suction}}$ and $q_{\text{ITE-2, press}}$ are the third last surface velocities on the flow field grid near the trailing edge on the suction and pressure surfaces, respectively. Additional constraints, or constraints different from the above, can easily be implemented into the optimization analysis with the BLDOPT code. Details for carrying this out are provided in the user's manual.

We have successfully completed a verification series of calculations of the new combined PERTURB/TSONIC/BLADE/COPE-S-COMMIN procedure in which the accuracy and sensitivity of the perturbation method was tested as a function of choice of the initial calibration solution matrix. The initial or base values of the design variables for the baseline blade profile, and the upper and lower bounds of the design variables that were specified for this test problem were:

Design Variable Number	Description	Lower Bound	Upper Bound	Initial Value
1	Outlet blade camber angle - KOGR	-15.0°	0.0°	-10.0°
2	Transition location/chord - T	0.20	0.60	0.25
4	Maximum thickness location/ chord - ZM	0.20	0.55	0.45
5	Inlet/outlet turning/chord - P	0.50	4.00	1.50
6	Maximum thickness/chord - TMX	0.03	0.10	0.05
7	Leading edge radius/chord - THLE	0.003	0.012	0.005

The results of these calculations are summarized in Table 1. There we have provided comparisons of the final design variables and objective function predicted when employing full nonlinear TSONIC solutions throughout the optimization process with corresponding results when using the perturbation method. For the perturbation results, different choices of the calibration solution matrix were made and are noted in the table. All the results represent converged solutions, with each calculation employing 10 optimization search cycles or less if no change in objective function should occur in three successive iterations.

The result indicated for the case when the perturbation method is not employed and TSONIC solutions are used throughout (IOPT = 1) provide the benchmark solution for comparison with the perturbation results. We note that similar full nonlinear benchmark results reported in Reference 3 for a related problem demonstrated the sensitivity of this class of optimization problems to the choice of the maximum velocity diffusion as an objective function. Identical benchmark results were obtained on the Ames Research Center CDC 7600 and the Lewis Research Center IBM 3033. The differences between those two results, which were of the same order as the differences between the various perturbation results, were due solely to the number of significant figures maintained in the respective calculations, i.e., eight for the IBM 3033 and 14 for the CDC 7600. This illustrates a common characteristic of many nonlinear multiple-parameter optimization problems, i.e., the existence of many local minimums. Furthermore, it also emphasizes the sensitivity of certain classes of optimization problems to both choice of objective function and design variables.

We observe from the perturbation results indicated in Table 1 that, with the exception of only one design variable (T) in certain instances of a deliberately made poor choice of calibration solution matrix, the final design variables predicted by the perturbation method for both IOPT=2 or 3 options trend in the same direction from the baseline value as the full nonlinear (IOPT=1) result and consistently improve the objective function. Under the IOPT=2 option, case 1 displays the results for a choice of calibration solution matrix which is very close to the final design result reached using the full nonlinear IOPT=1 option. The final perturbation-predicted design result for case 1 is slightly removed from the nonlinear result, but the objective function is quite close to the nonlinear result, indicating the presence of nearby alternative local optimization minimums. For case 2, the calibration matrix was determined by using the option ICALB=0 and selecting a constant-value calibration stepsize for each design variable of PSTEP=0.10. This implies that the value for each design variable for the calibration solution matrix is found by incrementing by 10 percent its base value. This manner of selecting the calibration matrix design variables is

relatively crude since, on average, half of the perturbation flow solutions for the optimization searches will involve design variable interpolation and half will require extrapolation. Furthermore, a certain fixed percentage increment on some design variables may be far too much in range in that large solution interpolations may be required, while that same percentage increment may be far too small for other design variables which would then require large extrapolations. Nevertheless, in the face of no a priori information regarding the direction and range that the optimization search will proceed over, the use of the ICALB=0 option provides a convenient and inexpensive way of obtaining a preliminary optimization result. Additionally, as the results for case 2 indicate, the ICALB=0 results are often quite good. Analogous results using ICALB=0 and PSTEP=-0.10, which implies a decrement of 10 percent from the base design variable values for the calibration design variables, are given in case 3. As can be seen, these results are inferior to those of case 2, and illustrate the relative importance of choosing calibration matrix design variable values that result in modest interpolations/extrapolations, since for case 3 larger interpolations/extrapolations are required. The results of both cases 4 and 5 further illustrate this point. For case 4, the calibration design variables were chosen so as to result exclusively in modest perturbation solution extrapolations during the optimization searches. In case 5, similar choices were made so as to result exclusively in modest solution interpolations. Both results in terms of final design variable values and objective function are quite good. The final IOPT=2 result shown in case 6 illustrates the effect of an intentional bad selection for the calibration solution design variables in that large perturbation solution extrapolations/interpolations are required during optimization. Although the final design result for the objective function is the least satisfactory of the six IOPT=2 cases, the majority of the design variables have trended in the appropriate direction. Consequently, even in for this situation involving deliberate poor choices of the calibration matrix, the perturbation method does not break down and yield spurious results, but provides instead a reasonable preliminary result. The final perturbation result shown in Table 1 is for the IOPT=3 option. For a slightly higher computational cost, that result provides a very good comparison between the final IOPT 1 nonlinear result.

The computational time needed to obtain the perturbation results in cases 1 to 6 under the IOPT=2 option were 76-78 secs. of CDC 7600 CPU time per case. The corresponding time for the IOPT=3 option was 97 secs. The benchmark IOPT=1 full nonlinear CDC 7600 result shown in Table 1 required 644 secs. Thus, the perturbation method provides a savings of $(644 - 78)/644 = 88\%$ of the computational time for the IOPT=2 option and $(644 - 97)/644 = 85\%$ for the IOPT=3 option for this example.

The significant conclusions to be drawn from this study are that the perturbation method can work accurately in multiple-parameter design environments even for very sensitive optimization problems and provide both meaningful final design results and large computational savings over not using the method. The choice of objective function such as was made for this case study, namely a point quantity located in a high-gradient region, requires careful user attention to the initial calibration matrix choice if IOPT=2 is employed in order to avoid large extrapolations, whereas if the IOPT=3 option is employed and the program allowed to automatically determine the calibration matrix, no exceptional difficulties are observed.

Additional optimization computations were made to try to determine whether an alternative choice of objective function would remove the sensitivity observed in the current problem. For example, computations were made employing objective functions defined as:(1) the sum of the maximum surface velocity on the blade suction surface plus the surface velocities on either side of that point, and (2) the sum of the first five surface velocities near the leading edge on the blade suction surface. The design variables and side constraints were kept the same as those of the original problem. The hope was that by spreading the objective function over a wider region on the blade surface, that the extreme sensitivity of the problem would be reduced. The results of these calculations, however, were disappointing in that they provided uniformly inferior results to the original choice of the objective function as a point quantity [Eq. (16)]. Our conclusion with regard to improving the posing of this particular optimization problem is that two issues must be addressed that were beyond the scope of this investigation. The first concerns the definition of the flow solution in the vicinity of the peak suction pressure. A detailed examination should be made of the accuracy and reliability of the flow solver (TSONIC) in that region. The second issue concerns the reliability of the basic CONMIN optimizer itself. In many of the optimization calculations undertaken in this study, a notable characteristic of the CONMIN optimizer was its penchant to move to a shallow objective function minimum in the near vicinity of the baseline configuration and to remain there. Alteration of stepsizes, design variable scalings, and certain tolerances did not change this characteristic. This behavior of CONMIN has been noted by others (Ref. 18) who have concluded that the conjugate gradient algorithm has serious convergence deficiencies when applied to the class of aerodynamic optimization problems being considered in this study. An attractive alternative method based on a quasi-Newton algorithm has demonstrated significantly superior performance characteristics over COPES/CONMIN for these same classes of problems (Ref. 18). The CONMIN procedure was originally developed for structural design problems with large numbers of

variables and constraints, rather than for the relatively new aerodynamic optimization problem which involves a relatively limited number of design variables and constraints. Consequently, it is not surprising that superior procedures are now being discovered and developed. In future work, an investigation should be made of the desirability of replacing the COPES/CONMIN optimization procedure embodied in the present BLDOPT program developed here.

4. CONCLUSIONS AND RECOMMENDATIONS

An investigation was conducted to complete the preliminary development of a combined perturbation/optimization procedure and associated computational code for designing optimized blade-to-blade profiles of turbomachinery blades. The overall purpose of the procedures developed in this study is to provide demonstration of the utility of a rapid nonlinear perturbation method for minimizing the computational requirements associated with optimized design studies of turbomachinery flows. The nonlinear perturbation method employed has been successfully developed in previous phases of this study and employs coordinate straining concepts together with unit perturbations determined from a special calibration matrix of nonlinear base solutions to predict families of related nonlinear solutions without further need of the computational nonlinear flow field solver. The solutions predicted can be either continuous or discontinuous.

The results reported here relate to the combination of the perturbation method, configured to predict simultaneous multiple-parameter changes, with the NASA/Lewis Research Center TSONIC code for predicting blade-to-blade flow solutions, the NASA/Lewis Research Center BLADE code for generating NASA blade-to-blade double circular arc blade shapes, and the NASA COPES-CONMIN code for performing optimization searches in multiple-parameter design space. The combined PERTURB/TSONIC/BLADE/COPES-CONMIN code, called BLDOPT, has been configured to perform optimization studies employing one, all, or any combination of the following eight blade geometry parameters used to characterize NASA double circular arc blade profiles: inlet blade camber angle, outlet blade camber angle, transition location between the inlet and outlet circular arc sections, maximum thickness location, inlet to outlet turning rate ratio, blade maximum thickness, leading edge radius, and trailing edge radius. Redefinition of the objective function and active side constraints for other case studies have been made simple and straightforward by confining their definition to one subroutine. The sample objective function and constraint definitions included in the version of the code reported here employ the velocity diffusion on the blade suction surface as objective function and three active side constraints related to maintenance of nonzero local blade thickness, low velocity diffusion on the blade pressure surface, and an effective trailing edge Kutta condition. The combined BLDOPT code has been made user-friendly and has been documented in a user's manual included as part of this report. An option has been included to allow the user to bypass use of the perturbation method altogether and employ TSONIC solutions throughout the optimization process in order to establish selected benchmark calculations. Options are also available to allow the user to employ the perturbation method in an automatic hands-off fashion. This is accomplished at the modest computational expense of one additional nonlinear

TSONIC-solution only optimization cycle over the alternative option of employing the perturbation method with the user supplying information regarding the initial calibration solution matrix.

Results of a series of calculations of the combined BLDOPT code have verified the code, demonstrated the accuracy of the perturbation-predicted results, and established benchmark guidelines of the potential for computational savings of the method under the various options included in the code. In general, the perturbation method is capable of providing an order of magnitude reduction in computational work in these applications.

Based on these results, we conclude that perturbation methods formulated on these ideas are both accurate and extremely workable in design environments. They clearly can provide the means for substantially reducing the computational work required in such applications. We suggest the further testing of the perturbation method with the combined BLDOPT code in order to test the limits of the method in such important preliminary design applications. Furthermore, we recommend the combination of these same procedures with supercritical flow solvers so as to accomplish both subcritical and supercritical blade optimization design.

APPENDIX A

USER'S MANUAL FOR COMPUTER PROGRAM BLDOPT

A.1 INTRODUCTION

The purpose of this appendix is to describe the operation of the computer code that was developed in conjunction with the theoretical work presented in this report, and to provide sufficient detail to permit convenient use and change of the program. The program determines an optimized blade shape, with respect to certain blade surface geometry parameters (Ref. 16) and based on TSONIC blade-to-blade flow solutions (Ref. 15), by employing a modified version of the COPES-CONMIN optimization search program (Ref. 13). The typically large computational demands of such optimization procedures caused by the need for numerous blade-to-blade flow solutions during the optimum search process is substantially reduced by incorporation of a novel, recently-developed, rapid, nonlinear, strained-coordinate perturbation method (Refs. 2 and 3) as discussed in the main text.

A description of the general operating procedure of the combined program is given, together with complete description of both input and output. The program is written in FORTRAN IV and has been developed on the Ames Research Center CDC 7600 computer facility. Approximate program run times for an optimization problem involving six design variables and 10 optimization search cycles when not employing or employing the perturbation method under the various program options are:

<u>CPU Run Time</u>	<u>Program Option, IOPT</u>
800 secs.	1 (TSONIC solutions only)
100 secs.	2 (Perturbation method)
180 secs.	3 (1 TSONIC solutions only cycle followed by perturbation method)

The storage requirements are 141K₈ for small core memory and 77K₈ for large core memory.

A.2 PROGRAM DESCRIPTION

The combined blade optimization program BLDOPT consists of the following main elements:

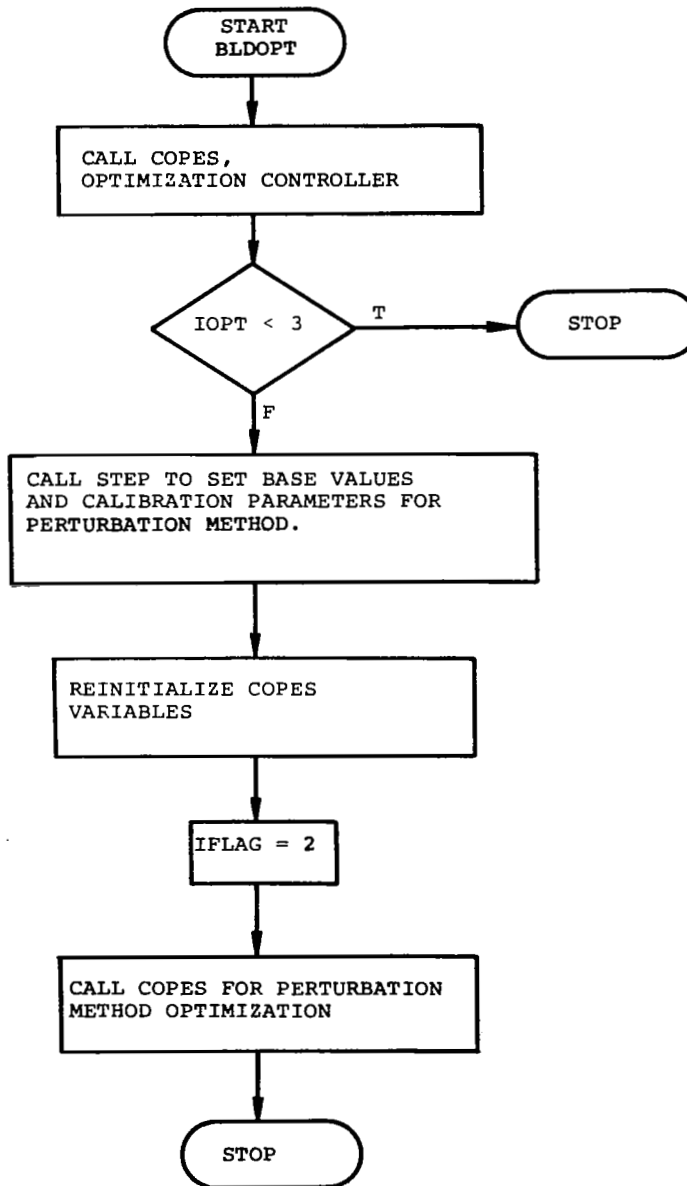
<u>Code Element</u>	<u>Function</u>
COPEP-CONMIN ¹³	Optimization procedure
TSONIC ¹⁵	Turbomachinery blade-to-blade flow solver
BLADE ¹⁶	Blade geometry description
PERTRB ³	Nonlinear perturbation method

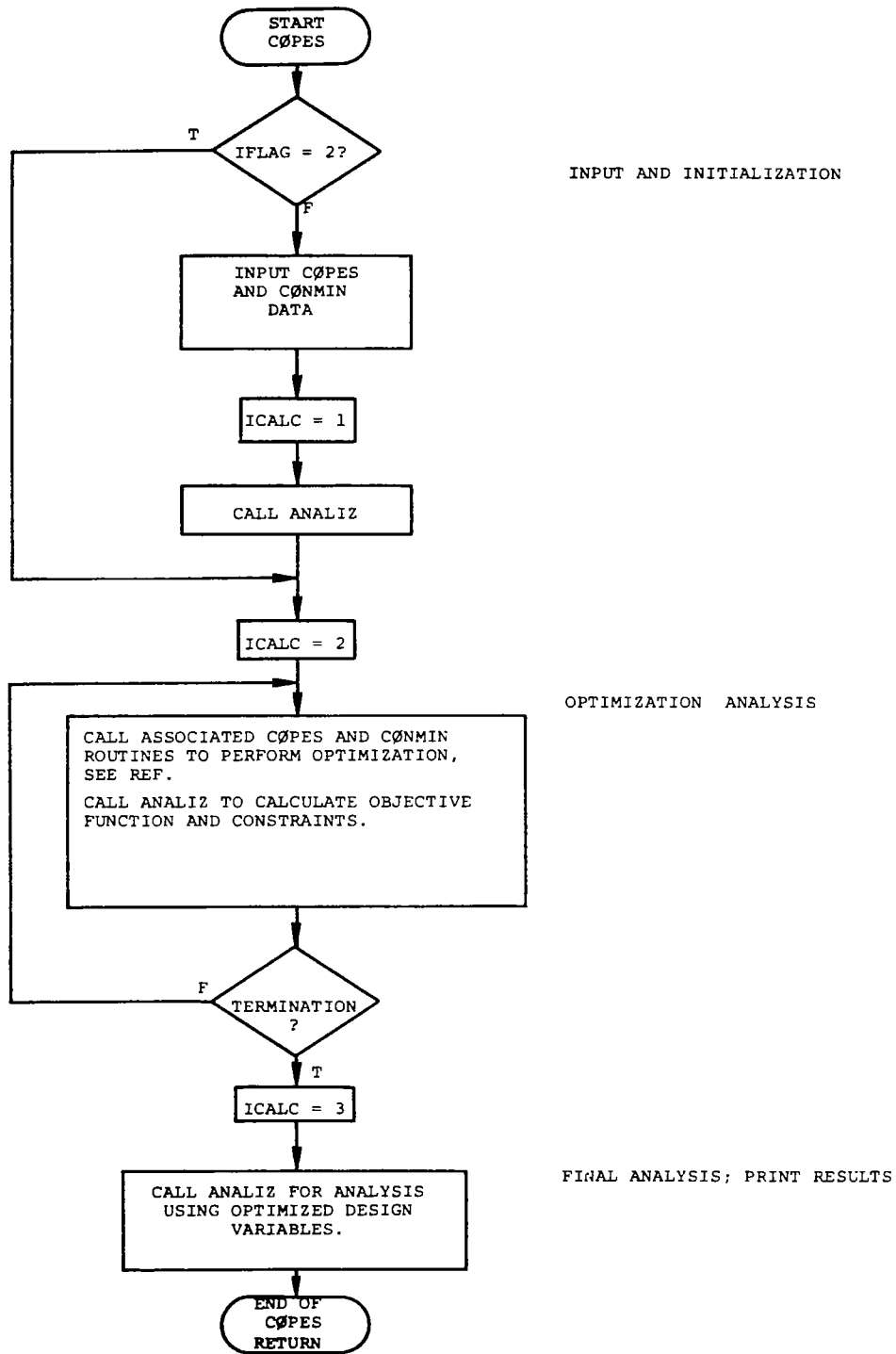
The program is configured to perform the optimization of a blade element as described geometrically in Reference 16. The optimization is based upon the following design variables which are geometric parameters describing the blade element:

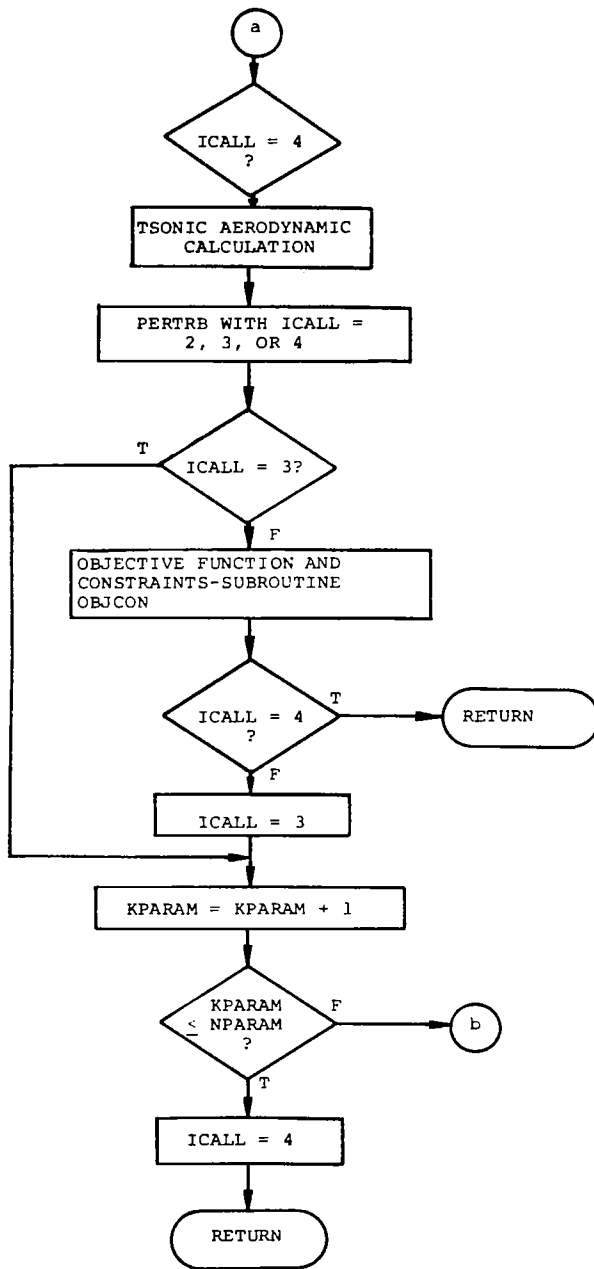
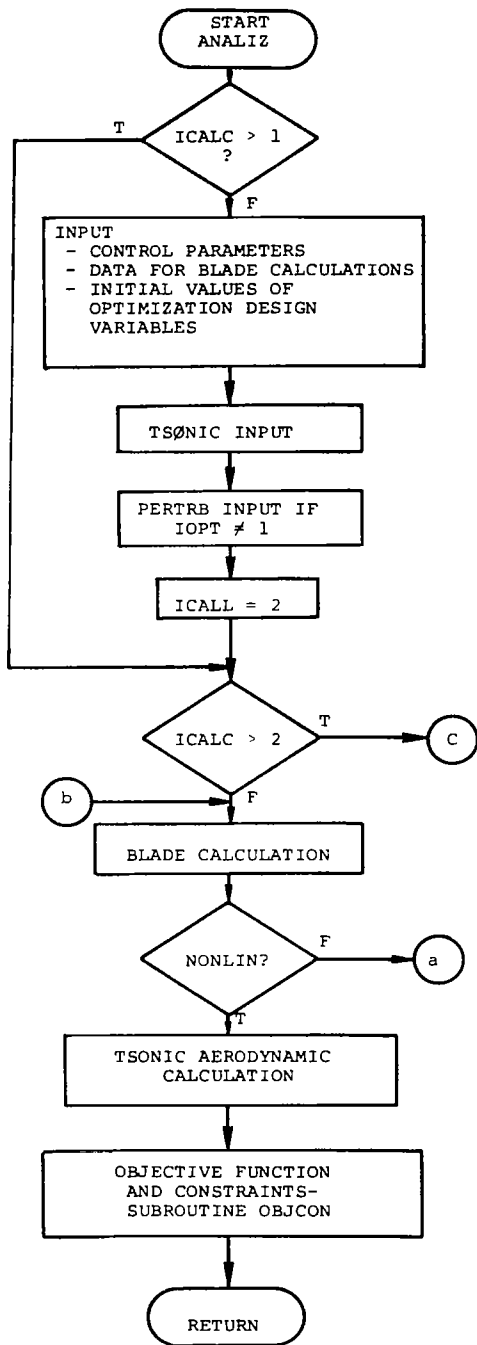
<u>Design Variable Number</u>	<u>Geometric Parameter</u>	<u>Program Name</u>
1	Blade camber angle at inlet	KICR
2	Blade camber angle at outlet	KOCR
3	Transition location/chord	T
4	Maximum thickness location/chord	ZM
5	Inlet/outlet turning rate ratio	P
6	Blade maximum thickness/chord	TMX
7	Leading edge radius/chord	THLE
8	Trailing edge radius/chord	THTE

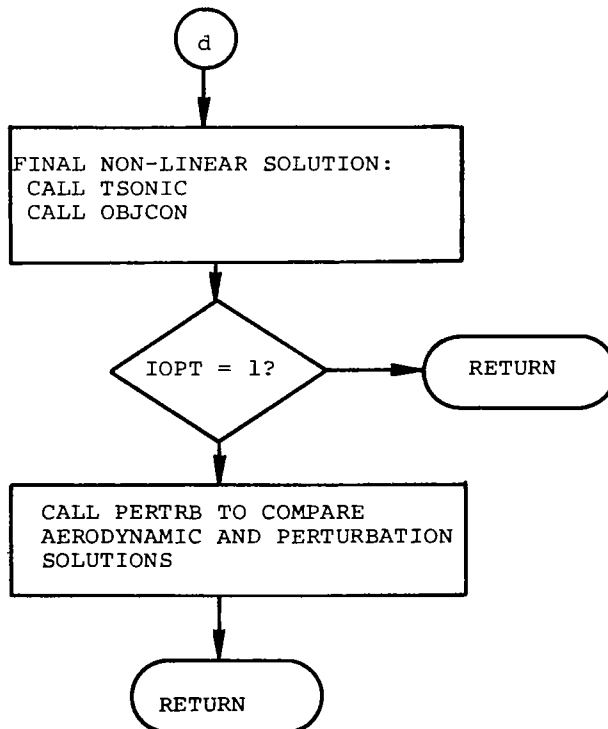
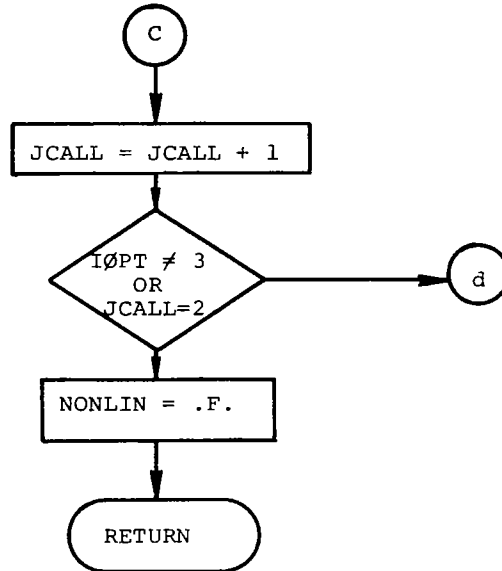
At the user's option, the optimization problem can be specified to employ any arbitrary combination up to six of the above design variables. Additionally, the user has the ability to construct readily particular objective functions and side constraints to be used in new optimization problems. Ease of definition and implementation of optimization problems with regard to objective function, side constraints, and design variable bounding were the primary reasons for selection of the COPES-CONMIN optimization driver. All information regarding definition of objective function and side constraints is contained in the subroutine OBJCON. In the program version listed here, the objective function is defined as the maximum velocity diffusion on the blade suction surface, and three side constraints are imposed to maintain (1) nonzero blade thickness, (2) low velocity diffusion on the blade pressure surface, and (3) trailing edge closure. Details of how these constraints are defined are provided in the main text, and their implementation in the code is straightforward and self-explanatory when viewing the program listing.

A.3 PROGRAM FLOW CHART









A.4 DICTIONARY OF INPUT VARIABLES

This section provides a dictionary of all input variables. The variables are divided into four sections corresponding to the four major parts of the program (see A.2).

A.4.1 Dictionary of Input Variables for Subroutine COPES (Ref. 13)

All COPES variables are defined in Section A.5.3.

A.4.2 Dictionary of Input Variables for Subroutine ANALIZ

ALP	Blade-element layout-cone half angle, degrees; see Reference 16.
DVCALB(I)	Array of dimension NDV, specifying the calibration parameters used in the perturbation method optimization
ICALB	Integer parameter which controls input of the array DVCALB: ICALB = 0, do not input DVCALB ICALB = 1, input DVCALB
IDV(I)	Array of integers, of dimension NDV, which is used to select a subset of variable blade parameters as design variables in the optimization. If IDV(I) = K, the Ith design variable is VV(K).
IOPT	Integer parameter which controls which method of analysis is to be used in optimization: IOPT = 1, nonlinear aerodynamic solution IOPT = 2, perturbation method IOPT = 3, nonlinear optimization for one iteration to predict calibration stepsizes, followed by perturbation method.
ITMAX3	Maximum number of optimization iterations allowed for the perturbation solution when IOPT = 3. Not used if IOPT = 1 or 2.
KICR	Centerline blade inlet angle on layout cone, degrees; see Reference 16.
KOCR	Centerline blade outlet angle on layout cone, degrees; see Reference 16.

NB Number of blades

NCN Number of constraint sets in the optimization problem; this value must be the same as that for NCONS in COPES input. $NCN \leq 5$.

NDV Number of independent design variables used in the optimization problem. This value must be the same as NDV in COPES input. $NDV \leq 8$.

P Ratio of inlet-segment turning ratio to outlet-segment turning rate for a blade element; see Reference 16.

PSTEP Constant-value calibration stepsize, which may be used in the perturbation method optimization. If ICALB = 0, the value of the K th calibration parameter $DV\text{CALB}(K) = (1.+PSTEP)*QO(K)$, where $QO(K)$ is the value of the K th base solution parameter.

R Inlet radius, length unit; see Reference 16.

SOLID Blade tip solidity (chord/circumferential spacing); see Reference 16.

T Blade centerline transition point location, made non-dimensional by the chord; see Reference 16.

THLE Blade-element leading-edge circle radius, made non-dimensional by the chord; see Reference 16.

THTE Blade-element trailing-edge circle radius, made non-dimensional by the chord; see Reference 16.

TMX Blade-element maximum thickness, made non-dimensional by the chord; see Reference 16.

VNAME(I) Array of dimension NDV, containing 10-character strings which identify, for printed output, the independent design variables used in optimization.

VV(I) Array of dimension 8 which is equivalent to the list of input variable blade parameters:

VV(1) = KICR	VV(5) = P
VV(2) = KOGR	VV(6) = TMX
VV(3) = T	VV(7) = THLE
VV(4) = ZM	VV(8) = THTE

ZM Blade centerline maximum thickness location, made non-dimensional by the chord; see Reference 16.

A.4.3 Dictionary of Input Variables for Subroutine TSONIC

This section presents definitions of the input variables required for the TSONIC flow analysis. For a complete description of the variables and their usage see Reference 15.

AR	Gas constant, J/(kg)(K)
BESP	Array of stream-channel normal thicknesses corresponding to the MR and RMSP arrays, meters, see Figure 12, Reference 15.
BETAI	Inlet flow angle β_{1e} along BG with respect to m-direction, deg, see Figure 11, Reference 15.
BETAO	Outlet flow angle β_{te} along CF with respect to m-direction, deg, see Figure 11, Reference 15.
DENTOL	Tolerance on density change per iteration for reduced weight flow (DENTOL may be left blank, and the value 0.01 will be used. If trouble is experienced in obtaining convergence (i.e., the maximum relative change in density (Item 14 of output, Ref. 15) does not get small enough, then a larger value of DENTOL may be used, or a smaller value of REDFAC may be used. (The value of 0.001 for DENTOL would be a tight tolerance, 0.01 is a medium tolerance, and 0.1 would be a loose tolerance.)
FSMI	m-coordinate corresponding to BETAI (it is assumed that $FSMI \leq 0$); if not specified, $FSMI = 0$.
FSMO	m-coordinate corresponding to BETAO (it is assumed that $FSMO \geq \text{chord}$); if not specified, $FSMO = \text{chord}$.
GAM	Specific heat ratio
LAMBDA	Upstream whirl, rV_{θ} , meters ² /sec.
LOPT	Integer variable which controls input of PLOSS array: LOPT = 0, PLOSS array is not given as input LOPT = 1, read in PLOSS array
LRVB	Integer variable which controls input: LRVB = 0, BETAI and BETAO are input LRVB = 1, LAMBDA and RVTHO are input
MBI	Number of vertical mesh lines from AH to BG inclusive, see Figure 13, Reference 15.

MBO Number of vertical mesh lines from AH to CF inclusive, see Figure 13, Reference 15.

MM Total number of vertical mesh lines in m-direction from AH to DE, maximum of 100, see Figure 13, Reference 15.

MOPT Integer control variable:
MOPT = 0, use only when REDFAC = 1, no correction is made to the BESP array for the reduced mass flow solution.
MOPT = 1, read in the WOWCR array to use for calculating the reduced mass flow BESP array.
MOPT = 2, the reduced BESP array will be calculated by the program using average blade angles and using SS1 and SS2 values to determine whether flow is subsonic or supersonic.

MR Array of m-coordinates of spline points for stream-channel radii and stream-channel thickness, meters, see Figure 12, Reference 15 (MR is measured from the leading edge of the blade. These coordinates should cover the entire distance from AH to DE, and may extend beyond these bounds. The total number of points is NRSP.).

NBBI Number of mesh spaces in θ -direction between AB and GH, maximum of 50, see Figure 13, Reference 15.

NBL Number of blades.

MRSP Number of spline points for stream-channel radius (RMSP) and thickness (BESP) coordinates, maximum of 50, see Figure 12, Reference 15.

OMEGA Rotational speed, ω , rad/sec (note that ω is negative if rotation is in the opposite direction of that shown in Fig. 12, Ref. 15).

ORF Value of overrelaxation factor to be used in the solution of the inner iteration simultaneous equations (if ORF = 0, the program calculates an estimated value for the overrelaxation factor. See page 25, Ref. 15 for discussion.).

PLOSS array of fractional total pressure loss, $1 - \frac{P'}{P'_{ideal}}$, corresponding to the MR, RMSP, and BESP arrays.

REDFAC Factor by which weight flow (WTFL) must be reduced
 in order to assure subsonic flow throughout passage
 (REDFAC is usually between 0.5 and 0.9).

RHOIP Inlet stagnation density, kg/meter³

RMSP Array of r-coordinates of spline points for the
 stream-channel radii, corresponding to the MR array,
 meters, see Figure 12, Reference 15.

RVTHO Downstream whirl, $(rV_r)_o$, meters²/sec.

SPLNO(1), Number of blade spline points given for each surface
 SPLNO(2) as input, maximum of 50 [these include the first and
 last points (dummies) that are tangent to the leading-
 and trailing-edge radii (Fig. 11, Ref. 15)].

SSM1 m-coordinate where supersonic solution is to start.

SSM2 m-coordinate where supersonic solution is to end.
 (Note: If SSM1 and SSM2 are both left blank, there
 will be no supersonic region).

TIP Inlet stagnation temperature, K

WOWCR Array of W/W_{cr} values at mid-channel, corresponding
 to the MR, RMSP, and BESP arrays. Used to calculate
 the reduced mass flow BESP array.

WTFL Mass flow per blade for stream channel, kg/sec.

The remaining variables, starting with BLDAT, are used to indicate what output is desired. A value of 0 for any of these variables will cause the output associated with that variable to be omitted. A value of 1 will cause the corresponding output to be printed for the final iteration only; 2, for the first and final iterations; and 3, for all iterations. Case should be used not to call for more output than is really useful. The following list gives the output associated with each of these variables:

BLDAT All geometrical information which does not change
 from iteration to iteration (i.e., coordinates and
 first and second derivatives of all blade surface
 spline points; blade coordinates, blade slopes, and
 blade curvatures where vertical mesh lines meet each
 blade surface; radii and stream-channel thickness
 corresponding to each vertical mesh line; m-coordinate,
 stream-channel radius and thickness, and blade surface
 angles and slopes where horizontal mesh lines inter-
 sect each blade; and ITV and IV arrays, internal
 variables describing the location of the blade sur-
 faces with respect to the finite difference grid).

AANDK	Coefficient array, constant vector, and indexes of all adjacent points for each point in finite-difference mesh (this information is needed for debugging the program only).
ERSOR	Maximum change in stream function at any point for each iteration of SOR equation [Eq. (A8), Ref. 17].
STRFN	Value of stream function at each unknown mesh point in region.
SLCRD	Streamline θ -coordinates at each vertical mesh line, and streamline plot.
INTVL	Velocity and flow angle at each interior mesh point for both reduced and actual weight flow.
SURVL	m-coordinate, surface velocity, flow angle, distance along surface, and W/W_{cr} based on meridional velocity components where each vertical mesh line meets each blade surface; m-coordinate, surface velocity, flow angle, distance along surface, and W/W_{cr} based on tangential velocity components where each horizontal mesh line meets each blade surface, plot of blade surface velocities against meridional streamline distance, meters.

A.4.4 Dictionary of Input Variables for Subroutine PERTRB

This section presents definitions of the input variables required for the perturbation method. For a complete description of the variables and their usage see Reference 3.

A	Scaling parameter in straining procedure. $A = -x(1)$, where $x(1)$ is x-location of first data point on lower surface (see PROGRAM DESCRIPTION, Ref. 3).
B	Scaling parameter in straining procedure. $B = -x(N)$, where $x(N)$ is location of last data point on upper surface (see PROGRAM DESCRIPTION, Ref. 3).
LPLOT	Specifies whether or not an additional plot by a peripheral device is to be made. Software must be supplied by user in subroutine DRVPLT. LPLOT = 0 ... no peripheral plot LPLOT = 1 ... peripheral plot

LSELECT(I) Array of length 6 of which NSELECT elements are read in; specifies nature of points to be held invariant according to the code:

- 1 ... minimum point held invariant
- 2 ... maximum point held invariant
- 3 ... 1st critical point held invariant
- 4 ... 2nd critical point held invariant
- 5 ... 3rd critical point held invariant
- 6 ... 4th critical point held invariant

Note that critical point ordering is determined from order of occurrence starting at the lower surface at the point furthest from the leading edge and proceeding clockwise around the surface (see PROGRAM DESCRIPTION, Ref. 3).

Note that the code numbers can be assigned in any order, e.g.,

LSELECT(1) = 1		LSELECT(1) = 4
LSELECT(2) = 3	and	LSELECT(2) = 1
LSELECT(3) = 4		LSELECT(3) = 3

Are equivalent, both corresponding to NSELECT = 3, with the minimum, and first and second critical points held invariant.

LUNIT Controls whether or not unit coordinate strainings and unit perturbation(s) are printed.

LUNIT = 0 ... no output
LUNIT = 1 ... output

NSELECT Number of points (in addition to end points) to be held invariant in straining; note: $1 \leq \text{NSELECT} \leq 6$.

PARNAM(K) Array of 8-character strings which identify the parameters varied. NPARAM element of the array are read in.

TITLE Character string of length 80; identifies job. First nine characters are used to identify peripheral plot.

VNAM Character string of length 2 which symbolizes dependent variables, e.g., "CP" for pressure coefficient.

A.5 PREPARATION OF INPUT DATA

This section describes the preparation of the card input data for the program. A description of each input item is presented, followed by a description of the card format.

A.5.1 Description of Input

The data are divided into four sections corresponding to the four major parts of the program.

A.5.1.1 COPES Input

Item 1.1 To end of COPES input. Input for the COPES optimization control subroutines is described in Section A.5.3. The user should take particular note of variable ITMAX in Block C and the array X in Block R. If IOPT = 3, ITMAX should be set equal to 1, and all values of the array X should be set to zero.

A.5.1.2 ANALIZ Input

- Item 2.1 One card, containing text which identifies the ANALIZ input block; may contain up to 80 characters.
- Item 2.2 One card, containing the control parameters IOPT, NDV, NCN, ITMAX3.
- Item 2.3 One card, containing the constant blade parameters NB, R, ALP, and SOLID.
- Item 2.4 One card, containing the variable blade parameters KICR, KOGR, T, ZM, P, TMX, THLE, THTE. The initial values of the design variables used in optimization are contained in this set.
- Item 2.5 One card, containing the character strings VNAME(I), I = 1, NDV.
- Item 2.6 One card, containing the integer array IDV(I), I = 1, NDV.
- Item 2.7 One card, containing parameters ICALB and PSTEP.
- Item 2.9 One card, optional, containing perturbation parameters. DVICALB(I), I = 1, NDV. Omit this item if ICALB = 0.

A.5.1.3 TSONIC Input

Item 3.1 One card, containing text identifying the TSONIC input block; may contain up to 80 characters.

- Item 3.2 One card, containing values for GAM, AR, TIP, RHOIP, WTFI, OMEGA, and ORF.
- Item 3.3 One card, containing values for geometric parameters BETAI, BETAO, FSMI, and FSMO.
Optional: LAMBDA and RVTHO may be specified instead of BETAI and BETAO. In this case, specify LRVB = 1. FSMI and FSMO are not needed.
- Item 3.4 One card, containing values for REDFAC, DENTOL, SSM1, SSM2.
- Item 3.5 One card, containing integral MBI, MBO, MM, NBBI, NBL, NRSP, MOPT, LOPT, LRVB.
- Item 3.6 One card, containing SPLNO(1).
- Item 3.7 One card, containing SPLNO(2).
- Item 3.8 Set of cards, eight values per card, containing array MR(I), I = 1, NRSP.
- Item 3.9 Set of cards, eight values per card, containing array RMSP(I), I = 1, NRSP.
- Item 3.10 Set of cards, eight values per card, containing array BESP(I), I = 1, NRSP.
- Item 3.11 Set of cards, optional, eight values per card, containing array WOWCR(I), I = 1, NRSP. This item is required only when MOPT = 1.
- Item 3.12 Set of cards, optional, eight values per card, containing array PLOSS(I), I = 1, MRSP. Omit this item if LOPT = 0.
- Item 3.13 One card, containing the integer print control variables BLDAT, AANDK, ERSOR, STRFN, SLCRD, INTVL, and survl.
- Item 3.14 One card, containing the character string \$END in columns 1-4. This identifies the end of TSONIC input.

A.5.1.4 PERTRB Input

- Item 4.1 One card of text, identifying the PERTRB input block. This item may contain up to 80 characters.
- Item 4.2 One card, containing TITLE for job identification. This item may contain up to 80 characters. The first 9 characters are used to identify peripheral plot, if LPLOT = 1.

- Item 4.3 One card, containing the integer control parameters NSELCT, LUNIT, and LPLOT.
- Item 4.4 One card, containing NSELCT values of the integer array LSELCT.
- Item 4.5 One card, containing the character string VNAM.
- Item 4.6 One card, containing the character strings PARNAM(I), I = 1, NDV.
- Item 4.7 One card, containing the scaling parameters A and B.

A.5.2 Format of Input Data

A.5.2. Format of Input Data

Item 1.1 - end of COPES input see Section A.5.3

Item no.2.1	1 card (8A10)			
Variable	Text			
Card column				80
Format type	A			

Item no.2.2	1 card (10I5)			
Variable	IOPT	NDV	NCN	ITMAX3
Card column	5	10	15	20
Format type	I	I	I	I

Item no.2.3	1 card (I10,3F10.6)			
Variable	NB	R	ALP	SOLID
Card column	10	20	30	40
Format type	I	F	F	F

Item no. 2.4	1 card (8F10.0)							
Variable	KICR	KOCR	T	ZM	P	TMX	THLE	THTE
Card column	10	20	30	40	50	60	70	80
Format type	F	F	F	F	F	F	F	F

Item no. 2.5	1 card (8A10)							
Variable	VNAME (1)	VNAME (2)	---	---	VNAME (NDV)			
Card column	10	20	30	40	50	60	70	80
Format type	A	A	A	A	A	A	A	A

Item no. 2.6	1 card (10I5)							
Variable	IDV (1)	IDV (2)	---	---	IDV (NDV)			
Card column	5	10	15	20	25	30	35	40
Format type	I	I	I	I	I	I	I	I

Item no. 2.7 1 card (I10, 3F10.6)

Variable	ICALB	PSTEP
Card column	10	20
Format type		

Item no. 2.8 1 card (8F10) Read only when ICALB not zero.

Variable	DVCALB(1)	DVCALB(2)	----	---	DVCALB(NDV)			
Card column	10	20	30	40	50	60	70	80
Format type	F	F	F	F	F	F	F	F

Item no. 3.1 1 card (8A10)

Variable	Text							
Card column								80
Format type	A							

Item no. 3.2 1 card (8F10.5)

Variable	GAM	AR	TIP	RHØIP	WTFI		ØMEGA	ØRF
Card column	10	20	30	40	50	60	70	80
Format type	F	F	F	F	F	F	F	F

Item no. 3.3 1 card (8F10.5)

Variable	BETA1	BETAØ			FSMI	FSMØ
Card column	10	20	30	40	50	60
Format type	F	F	F	K	F	F

Item no. 3.4 1 card (8F10.5)

Variable	REDFAC	DENTØL	SSM1	SSM2
Card column	10	20	30	
Format type	F	F	F	F

Item no. 3.5

1 card (16I5)

Variable

MBI	MBØ			MM	NBBI	NBL	NRSP	MØPT	LØPT	LRVB
5	10	15	20	25	30	35	40	45	50	55
I	I	I	I	I	I	I	I	I	I	I

Card column

Format type

Item no. 3.6

1 card (8F10.5)

Variable

				SPLNØ (1)
10	20	30	40	50
				F

Card column

Format type

Item no. 3.7

1 card (8F10.5)

Variable

				SPLNØ (2)
10	20	30	40	50
				F

Card column

Format type

Item no. 3.8

J cards, $J = \text{INT}((\text{NRSP}-1)/8) + 1$, 8 values per card (8F10.5)

Variable

MR(1)	MR(2)	---	---	MR(NRSP)			
10	20	30	40	50	60	70	80
F	F	F	F	F	F	F	F

Card column

Format type

Item no. 3.9

J cards, J as above, 8 values per card (8F10.5)

Variable

RMSP(1)	RMSP(2)	---	---	RMSP(NRSP)			
10	20	30	40	50	60	70	80
F	F	F	F	F	F	F	F

Card column

Format type

Item no. 3.10

J cards, J as above, 8 values per card (8F10.5)

Variable

BESP(1)	BESP(2)	---	---	BESP(NRSP)			
10	20	30	40	50	60	70	80
F	F	F	F	F	F	F	F

Card column

Format type

Item no.3.11 (If MØPT=1) J cards, J as above,8 values per card (8F10.5)

Variable	WØWCR(1)	WØWCR(2)	----	----	WØWCR(NRSP)		
Card column	10	20	30	40	50	60	70 80
Format type	F	F	F	F	F	F	F

Item no.3.12 (If LØPT=0) J cards, J as above,8 values per card (8F10.5)

Variable	PLØSS(1)	PLØSS(2)	---	---	PLØSS(NRSP)		
Card column	10	20	30	40	50	60	70 80
Format type	F	F	F	F	F	F	F

Item no.3.13 1 card (16I5)

Variable	BLDAT	AANDK	ERSØR	STRFN	SLCRD	INTVL	SURVL
Card column	5	10	15	20	25	30	35
Format type	I	I	I	I	I	I	I

Item no.3.14 1 card (8A10)

Variable	\$END
Card column	10
Format type	A

Item no. 4.1 1 card (8A10)

Variable	TEXT
Card column	80
Format type	A

Item no. 4.2 1 card (8A10)

Variable	TITLE
Card column	80
Format type	A

Item no. 4.3 1 card (16I5)

Variable	NSELCT	LUNIT	LPLØT
Card column	5	10	15
Format type	I	I	I

Item no. 4.4 1 card (16I5)

Variable	LSELCT(1)	LSELCT(2)	-----	-----	LSELCT(NSELCT)			
Card column	5	10	15	20	25	30	35	40
Format type	I	I	I	I	I	I	I	I

Item no. 4.5 1 card (2A1)

Variable	VNAM
Card column	2
Format type	A

Item no. 4.6 1 card (10A8)

Variable	PARNAM(1)	PARNAM(2)	---	----	PARNAM(NIV)			
Card column	8	16	24	32	40	48	56	64
Format type	A	A	A	A	A	A	A	A

Item no. 4.7 1 card (8F10.6)

Variable	A	B
Card column	10	20
Format type	F	F

A.5.3 Format of COPES Input Data.

DATA BLOCK ADESCRIPTION: Title card.FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
TITLE								20A4
CANTILEVERED BEAM DESIGN								

FIELDCONTENTS

1-8 Any 80 character title may be given on this card.

DATA BLOCK B

DESCRIPTION: Program Control Parameters.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7		FORMAT
NCALC	NDV	NSV	N2VAR	NXAPRX	IPNPUT	IPDBG		7I10
2	2	3	5	2	0	0		

FIELD

CONTENTS

- 1 NCALC: Calculation Control
- 0 - Read input and stop. Data of blocks A, B and V is required. Remaining data is optional.
 - 1 - One cycle through program. The same as executing ANALIZ stand-alone. Data of blocks A, B and V is required. Remaining data is optional.
 - 2 - Optimization. Data of blocks A-I and V is required. Remaining data is optional.
 - 3 - Sensitivity analysis. Data of blocks A, B, P, Q and V is required. Remaining data is optional.
 - 4 - Two variable function space. Data of blocks A, B, and R-V is required. Remaining data is optional.

FIELDCONTENTS

1 - cont. NCALC:

- 5 - Optimum Sensitivity. Data of blocks A-K and V is required. Remaining data is optional.
 - 6 - Optimization using approximation techniques. Data of blocks A-O and V is required. Remaining data is optional.
- 2 NDV: Number of independent design variables in optimization.
- 3 NSV: Number of variables on which sensitivity analysis will be performed.
- 4 NZVAR: Number of objective functions in a two variable function space study.
- 5 NXAPRX: Number of X-variables for approximate analysis/optimization.
- 6 IPNPUT: Input print control.
 - 0 - Print card images of data plus formatted print of input data.
 - 1 - Formatted print only of input data.
 - 2 - No print of input data.
- 7 IPDBG: Debug print control.

DATA BLOCK C OMIT IF NDV = 0 IN BLOCK B

DESCRIPTION: Integer optimization control parameters.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
IPRINT	ITMAX	ICNDIR	NSCAL	ITRM	LINOBJ	NACMX1	NFDG	8I10
5	0	0	0	0	0	0	0	

FIELD

CONTENTS

- 1 IPRINT: Print control used in the optimization program CONMIN.
- 0 - No print during optimization.
 - 1 - Print initial and final optimization information.
 - 2 - Print above plus objective function value and design variable values at each iteration.
 - 3 - Print above plus constraint values, direction vector and move parameter at each iteration.
 - 4 - Print above plus gradient information.
 - 5 - Print above plus each proposed design vector, objective function and constraint values during the one-dimensional search.

FIELDCONTENTS

- 2 ITMAX: Maximum number of optimization iterations allowed. DEFAULT = 20.
- 3 ICNDIR: Conjugate direction restart parameter. DEFAULT = NDV + 1.
- 4 NSCAL: Scaling parameter. GT.0 - Scale design variables to order of magnitude one every NSCAL iterations. LT.0 - Scal design variables according to user-input scaling values.
- 5 ITRM: Number of consecutive iterations which must satisfy relative or absolute convergence criterion before optimization process is terminated. DEFAULT = 3.
- 6 LINOBJ: Linear objective function identifier. If the optimization objective is known to be a linear function of the design variables, set LINOBJ = 1.
DEFAULT = Non-linear.
- 7 NACMX1; One plus the maximum number of active constraints anticipated. DEFAULT = NDV + 2.
- 8 NFDG: Finite difference gradient identifier.
- 0 - All gradient information is computed by finite difference within CONMIN.
 - 1 - All gradient information is computed analytically by the user-supplied code.
 - 2 - Gradient of objective is computed analytically. Gradients of constraints are computed by finite difference within CONMIN.

REMARKS

- 1) Currently NFDG must be zero in COPEs.

DATA BLOCK D OMIT IF NDV = 0 IN BLOCK B

DESCRIPTION: Floating point optimization program parameters.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7		FORMAT
FDCH	FDCHM	CT	CTMIN	CTL	CTLMIN	THETA		7F10
0.0	0.0	0.0	0.0	0.0	0.0	0.0		
DELFUN	DABFUN	ALPHAX	ABOBJ1					4F10
0.0	0.0	0.0	0.0					

NOTE: TWO CARDS ARE READ HERE.

FIELD

CONTENTS

- 1 FDCH: Relative change in design variables in calculating finite difference gradients. DEFAULT = 0.01.
- 2 FDCHM: Minimum absolute step in finite difference gradient calculations. DEFAULT = 0.001.

<u>FIELD</u>	<u>CONTENTS</u>
3	CT: Constraint thickness parameter. DEFAULT = -0.05.
4	CTMIN: Minimum absolute value of CT considered in the optimization process. DEFAULT = 0.004.
5	CTL: Constraint thickness parameter for linear constraints. DEFAULT = -0.01.
6	CTLMIN: Minimum absolute value of CTL considered in the optimization process. DEFAULT = 0.001.
7	THETA: Mean value of push-off factor in the method of feasible directions. DEFAULT = 1.0.
1	DELFUN: Minimum relative change in objective function to indicate convergence of the optimization process. DEFAULT = 0.001.
2	DABFUN: Minimum absolute change in objective function to indicate convergence of the optimization process. DEFAULT = 0.001 times the initial objective value.
3	ALPHAX: Maximum fractional change in any any design variable for first estimate of the step in the one-dimensional search. DEFAULT = 0.1.
4	ABOBJ1: Expected fractional change in the objective function for first estimate of the step in the one-dimensional search. DEFAULT = 0.1.

REMARKS

- 1) The DEFAULT values for these parameters usually work well.

DATA BLOCK E OMIT IF NDV = 0 IN BLOCK B

DESCRIPTION: Total number of design variables, design objective identification and sign.

FORMAT AND EXAMPLE

1	2	3	FORMAT
NDVTOT	IOBJ	SGNOPT	2I10,F10
0	3	-1.0	

FIELD

CONTENTS

- 1 NDVTOT: Total number of variables linked to the design variables. This option allows two or more parameters to be assigned to a single design variable. The value of each parameter is the value of the design variable times a multiplier, which may be different for each parameter. DEFAULT = NDV.
- 2 IOBJ: Global variable location associated with the objective function in optimization.
- 3 SGNOPT: Sign used to identify whether function is to be maximized or minimized. +1.0 indicates maximization. -1.0 indicates minimization. If SGNOPT is not unity in magnitude, it acts as a multiplier as well, to scale the magnitude of the objective.

DATA BLOCK F OMIT IF NDV = 0 IN BLOCK B

DESCRIPTION: Design variable bounds, initial values and scaling factors.

FORMAT AND EXAMPLE

1	2	3	4	FORMAT
VLB	VUB	X	SCAL	4F10
.5	5.	0.0	0.0	

NOTE: READ ONE CARD FOR EACH OF THE NDV INDEPENDENT DESIGN VARIABLES.

FIELD

CONTENTS

- | | | |
|---|-------|---|
| 1 | VLB: | Lower bound on the design variable. If VLB.LT.-1.0E+15, no lower bound. |
| 2 | VUB: | Upper bound on the design variable. If VUB.GT.10.E+15, no upper bound. |
| 3 | X: | Initial value of the design variable. If X is non-zero, this will supercede the value initialized by the user-supplied subroutine ANALIZ. |
| 4 | SCAL: | Design variable scale factor. Not used if NSCAL.GE.0 in BLOCK C. |

DATA BLOCK G OMIT IF NDV = 0 IN BLOCK B

DESCRIPTION: Design variable identification.

FORMAT AND EXAMPLE

1	2	3	FORMAT
NDSGN	IDSGN	AMULT	2I10,F10
1	1	1.0	

NOTE: READ ONE CARD FOR EACH OF THE NDVTOT DESIGN VARIABLES.

FIELD

CONTENTS

- 1 NDSGN: Design variable number associated with this variable.
- 2 IDSGN: Global variable number associated with this variable.
- 3 AMULT: Constant multiplier on this variable. The value of the variable will be the value of the design variable, NDSGN, times AMULT. DEFAULT = 1.0.

DATA BLOCK H OMIT IF NDV = 0 IN BLOCK B

DESCRIPTION: Number of constrained parameters.

FORMAT AND EXAMPLE

1		FORMAT
NCONS		I10
4		

FIELD

CONTENTS

1 NCONS: Number of constraint sets in the optimization problem.

REMARKS

- 1) If two or more adjacent parameters in the global common block have the same limits imposed, these are part of the same constraint set.

DATA BLOCK I OMIT IF NDV = 0 IN BLOCK B, OR NCONS = 0 IN BLOCK H

DESCRIPTION: Constraint identification and constraint bounds.

FORMAT AND EXAMPLE

1	2	3	4	FORMAT
ICON	JCON	LCON		3I10
4	0	0		
BL	SCAL1	BU	SCAL2	
-1.0 +20	0.0	20000.	0.0	

NOTE: READ TWO CARDS FOR EACH OF THE NCONS CONSTRAINT SETS.

FIELD

CONTENTS

- 1 ICON: First global number corresponding to the constraint set.
- 2 ICON: Last global number corresponding to the constraint set. DEFAULT = ICON.
- 3 LCON: Linear constraint identifier for this constraint set. LCON = 1 indicates
linear constraints.

<u>FIELD</u>	<u>CONTENTS</u>
1	BL: Lower bound on the constrained variables. If BL.LT.-1.OE+15, no lower bound.
2	SCAL1: Normalization factor on lower bound. DEFAULT = MAX of ABS(BL), 0.1.
3	BU: Upper bound on the constrained variables. If BU.GT.1.OE+15, no upper bound.
4	SCAL2: Normalization factor on upper bound. DEFAULT = MAX of ABS(BU), 0.1.

REMARKS

- 1) The normalization factor should usually be defaulted.
- 2) The constraint functions sent to CONMIN are of the form;
(BL - VALUE)/SCAL1 .LE. 0.0 and (VALUE - BU)/SCAL2 .LE. 0.0.
- 3) Each constrained parameter is converted to two constraints in CONMIN unless ABS(BL) or ABS(BU) exceeds 1.OE+15, in which case no constraint is created for that bound.

DATA BLOCK J OMIT IF NXAPRX = 0 IN BLOCK B

DESCRIPTION: Approximate analysis/optimization control parameters.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
NF	NXS	NXFS	NXA	INOM	ISCRX	ISCRXF	IPAPRX	8I10
5	1	1	1	0	0	0	1	
KMIN	KMAX	NPMAX	JNOM	INXLOC	INFLOC			6I10
0	0	0	0	0	0			

FIELD

CONTENTS

- 1 NF: Number of functions to be approximated. Default = number of optimization objective and constraint functions.
- 2 NXS: Number of X-vectors read as data.
- 3 NXFS: Number of X-F pairs read as data.
- 4 NXA: If non-zero, the design variables read by SUBROUTINE ANALIZ form an X-vector.
- 5 INOM: Nominal X-vector. Default = best available.

<u>FIELD</u>	<u>CONTENTS</u>
6	ISCRX: File from which NXS X-vectors are read. Default = 5.
7	ISCRXF: File from which NXFS X-F pairs of data are read. Default = 5.
1	KMIN: Minimum number of approximation iterations.
2	KMAX: Maximum number of approximation iterations.
3	NPMAX: Maximum number of designs retained for Tayler series expansion.
4	JNOM: Number of iterations after which the best design is picked as nominal.
5	INXLOC: X-variable global location identifier. If INXLOC = 0, the Tayler series expansion is on the design variables listed in BLOCK G.
6	INFLOC: Function global location identifier. If INFLOC = 0, the Objective and constraint functions identified in BLOCKS E and I are the functions on which the Tayler series expansion is performed.

REMARKS

- 1) If ISCRX and/or ISCRXF file number is other than 5, the data read from that file is assumed to be binary data.
- 2) If NXS = NXFS = 0, NXA is defaulted to NXA = 1, even is it is read as zero. Also, a second vector of design variables is automatically defined by COPEs to yield two independent designs to start the optimization.

DATA BLOCK K OMIT IF NDV = 0 IN BLOCK B, OR NXAPRX = 0 IN BLOCK B

DESCRIPTION: Bounds and multipliers for approximate optimization.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
DX1	DX2	DX3	DX4	DX5	8F10
.5	2.							
XFACT1	XFACT2							2F10
0.	0.							

NOTE: TWO OR MORE CARDS ARE READ HERE.

FIELD

CONTENTS

- 1-8 DXI: Allowable change (in magnitude) of the Ith design variable during each approximate optimization.
- 1 XFACT1: Multiplier on DXI when the diagonal elements of the H matrix are available. Default = 1.5.
- 2 XFACT2: Multiplier on DXI when all elements of the H matrix are available. Default = 2.0.

DATA BLOCK L OMIT IF NXAPRX = 0 IN BLOCK B OR INXLOC = 0 IN BLOCK J

DESCRIPTION: Global locations of approximating variables.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
LOCX1	LOCX2	LOCX3	LOCX4	8I10
1	2							

NOTE: MORE THAN ONE CARD MAY BE READ HERE.

FIELD

CONTENTS

1-8 LOCI: Global location of Ith approximating variable.

REMARKS

- 1) If INXLOC = 0 in BLOCK J, this data is not read. In this case, the data is defaulted to be the global locations of the design variables (IDSGN values in BLOCK G).

DATA BLOCK M OMIT IF NXAPRX = 0 IN BLOCK B OR INFLOC = 0 IN BLOCK J

DESCRIPTION: Global locations of functions to be approximated.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
LOCF1	LOCF2	LOCF3	LOCF4	8I10
3	5	6	4					

NOTE: MORE THAN ONE CARD MAY BE READ HERE.

FIELD

CONTENTS

1-8 LOCI: Global location of Ith function to be approximated.

REMARKS

- 1) If INFLOC = 0 in BLOCK J, this data is not read. In this case, the data is defaulted to be the global locations of the objective function (IOBJ in BLOCK E) followed by the global locations of the constrained parameters (ICON, JCON in BLOCK I).

DATA BLOCK N OMIT IF NXS = 0 IN BLOCK J

DESCRIPTION: X-Vectors for approximate optimization.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
XI1	XI2	XI3	XI4	8F10
4.	15.							

NOTE: NXS SETS OF DATA ARE READ HERE.

NOTE: MORE THAN ONE CARD MAY BE READ FOR EACH SET OF DATA.

FIELD

CONTENTS

1-8 XIJ: Jth value of Ith X-vector, J = 1, NXAPRX.

DATA BLOCK 0 OMIT IF NXFS = 0 IN BLOCK J

DESCRIPTION: X-F pairs of information for approximate optimization.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
X1	X2	X3	X4	8F10
2.	18.							
Y1	Y2	Y3	Y4	Y5	
7200.	416.667	.914495	18518.519					

NOTE: NXFS SETS OF DATA ARE READ HERE.

NOTE: MORE THAN ONE CARD MAY BE REQUIRED FOR XI OR YI.

NOTE: NXAPRX VALUES OF X AND NF VALUES OF Y ARE READ FOR EACH SET OF DATA.

FIELD

CONTENTS

1-8 XI: Ith value of X, I = 1,NXAPRX.

1-8 YI: Ith value of Y, I = 1,NF.

DATA BLOCK P OMIT IF NSV = 0 IN BLOCK B

DESCRIPTION: Sensitivity objectives.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
NSOBJ	IPSENS							2I10
5	0							
NSN1	NSN2	NSN3	NSN4	NSN5	8I10
3	4	5	6	7				

NOTE: TWO OR MORE CARDS ARE READ HERE.

FIELD

CONTENTS

- 1 NSOBJ: Number of separate objective functions to be calculated as functions of the sensitivity variables.
- 2 IPSENS: Print control. If IPSENS.GT.0, detailed print will be called at each step in the sensitivity analysis. DEFAULT = No print.
- 1-8 NSNI: Global variable number associated with the sensitivity objective functions.

REMARKS

- 1) More than eight sensitivity objectives are allowed. Add data cards as required to contain data.

DATA BLOCK Q OMIT IF NSV = 0 IN BLOCK B

DESCRIPTION: Sensitivity variables.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	--	FORMAT
ISENS	NSENS								2I10
9	4								
SNS1	SNS2	SNS3	SNS4		8F10
200.	100.	150.	250.						

NOTE: READ ONE SET OF DATA FOR EACH OF THE NSV SENSITIVITY VARIABLES.

NOTE: TWO OR MORE CARDS ARE READ FOR EACH SET OF DATA.

FIELD

CONTENTS

- 1 ISENS: Global variable number associated with the sensitivity variable.
- 2 NSENS: Number of values of this sensitivity variable to be read on the next card.
- 1-8 SENSI; Values of the sensitivity variable. I = 1, NSENS. I = 1 corresponds to the nominal value.

REMARKS

- 1) More than eight values of the sensitivity variable are allowed. Add data cards as required to contain the data.

DATA BLOCK R OMIT IF N2VAR = 0 IN BLOCK B

DESCRIPTION: Two variable function space control parameters.

FORMAT AND EXAMPLE

1	2	3	4	5		FORMAT
N2VX	M2VX	N2VY	M2VY	IP2VAR		5I10
1	4	2	5	0		

FIELD

CONTENTS

- 1 N2VX: Global location of the X-variable in the two variable function space.
- 2 M2VX: Number of values of X to be considered.
- 3 N2VY: Global location of the Y-variable in the two variable function space.
- 4 M2VY: Number of values of Y to be considered.
- 5 IP2VAR: Print control. If IP2VAR.GT.0, detailed print will be called at each step (each X-Y combination). DEFAULT = No print.

DATA BLOCK S OMIT IF N2VAR = 0 IN BLOCK B

DESCRIPTION: Objective functions of the two variable function space study.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
NZ1	NZ2	NZ3	NZ4	NZ5	8I10
3	4	5	6	7				

FIELD

CONTENTS

1-8 NZI: Global location corresponding to the Ith function of X and Y to be calculated. N2VAR values are read here.

REMARKS

1) More than eight objective functions are allowed. Add data cards as required to contain the data.

DATA BLOCK T OMIT IF N2VAR = 0 IN BLOCK B

DESCRIPTION: Values of the X-variable in a two variable function space study.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
X1	X2	X3	X4	8F10
0.5	1.0	1.5	2.0					

FIELD

CONTENTS

1-8 XI: Values of the X-variable in the two variable function space. M2VX values are read here.

REMARKS

1) More than eight values are allowed. Add data cards as required to contain the data.

DATA BLOCK U OMIT IF N2VAR = 0 IN BLOCK B

DESCRIPTION: Values of the Y-variable in a two variable function space study.

FORMAT AND EXAMPLE

1	2	3	4	5	6	7	8	FORMAT
Y1	Y2	Y3	Y4	Y5	8F10
4.0	8.0	12.0	16.0	20.0				

FIELD

CONTENTS

1-8 YI: Values of the Y-variable in the two variable function space. M2VY values are read here.

REMARKS

1) More than eight values are allowed. Add data cards as required to contain the data.

DATA BLOCK VDESCRIPTION: COPES data 'END' card.FORMAT AND EXAMPLE

1	FORMAT
END	3A1
END	

FIELDCONTENTS

1 The word 'END' in columns 1-3.

REMARKS

- 1) This card MUST appear at the end of the COPES data.
- 2) This ends the COPES input data.
- 3) Data for the user-supplied routine, ANALIZ, follows this.

A.6 DESCRIPTION OF OUTPUT

The first output item consists of a banner page related to the COPES control program and followed by card images of the COPES input data. The next output items contain COPES optimization information which will be employed by the optimization program. This is followed by a display of input information required by the ANALIZ subroutine and related to the control parameters, constant blade properties, variable blade properties, active design variables, and input information for the calibration solution matrix. Next, is a display of input information required by the TSONIC blade-to-blade flow solver. Finally, a display is provided of the input information needed by the perturbation method.

The next items of output are related to the TSONIC solution for the baseline blade profile. The first item consists of the input information on design variables and constant blade properties that is provided to the blade element program which then performs the computation necessary to determine blade property characteristics required as input to the TSONIC code. The next items are the input to the TSONIC code and the output generated by the code for the flow solution. This is followed by output from OBJCON related to the objective function and active constraints. The next item is the banner page of information that will initiate the CONMIN minimization procedure. The optimization search cycles are then begun. The output that follows depends upon which IOPT option was specified. However, regardless of the IOPT option selected, each time a TSONIC flow solution is required by the optimization package, the following segment of output is produced: the input information regarding design variables and constant blade properties that is provided to the blade element program is displayed, followed by the input to the TSONIC code, the output from TSONIC, and finally, output from OBJCON related to the current objective function and active side constraint values for the TSONIC solution just calculated. Consequently, for IOPT = 1, for which TSONIC solutions are used throughout the optimization process, the above segment of information is displayed for each TSONIC solution for the gradient and search calculations. At the end of each iteration cycle, CONMIN provides output regarding the ending values of the design variables and side constraints. This continues until the ITMAX limit is reached, or the objective function has not changed within the last three iterations, at which point the final optimization results are printed, followed by a final TSONIC calculation at the design point. For the IOPT = 2 option, after the base solution is computed, the calibration solution matrix is determined based on user-supplied information. The optimization cycles then proceed using perturbation-predicted solutions for the blade surface velocities. When the optimization process is complete, a final TSONIC solution is calculated at the design point and a printer plot provided exhibiting a comparison of the perturbation-predicted surface

velocity distribution with the TSONIC result. For the IOPT = 3 option, the optimization process is allowed to proceed with TSONIC solutions only as with IOPT = 1, but only for one search cycle. Then, based on the new base design point reached, design variable values for a calibration solution matrix are determined. Next, each of the TSONIC solutions for the new base and calibration solutions are separately determined, with output provided after each solution regarding number of critical points, and strained coordinate and surface pressure arrays. Following the final calibration solution, summary output is provided regarding the base coordinates, the strained coordinate arrays for each calibration solution, and the corresponding surface velocity arrays. Next, the CONMIN optimization search cycles are entered using the perturbation method to predict all flow solutions required in the gradient and search calculations. The search cycles are continued to the ITMAX3 limit or until the objective function does not change for three successive iterations, at which point the final optimization results are printed, followed by a final TSONIC calculation at the design point, and a printer plot illustrating comparisons between the perturbation method predicted surface velocities distribution and the nonlinear TSONIC result.

A.7 ERROR MESSAGES

NUMBER OF CRITICAL POINTS IN
BASE AND CALIBRATION SOLUTIONS
ARE UNEQUAL - CALCULATION ENDED

This message will be printed if critical points are specified in straining (LSPEC = 0) and the number of critical points in base and calibration solutions are unequal. The remedy is to avoid use of critical points in straining, or to use base and calibration solutions having equal numbers of critical points.

NUMBER OF CRITICAL POINTS
SELECTED EXCEEDS NUMBER
ACTUALLY LOCATED - CALCULATION
ENDED

This message will be printed if more critical points are specified in straining (LSPEC = 0) than the number located by the program. The remedy is to specify a number of points less than or equal to the actual number.

ORDER OF SPECIFIED POINTS IN
BASE AND CALIBRATION SOLUTIONS
DOES NOT CORRESPOND - CALCULATION
ENDED

This message will be printed if the fixed points specified (LSPEC = 0) occur in a different sequence in the base and calibration solutions. The remedy is to use base and calibration solutions having the same qualitative features.

A.8 SAMPLE CASE

The sample case presented in this section provides example results of the perturbation method for the blade design optimization problem described in Section 3 of the main text. The calculation is for the simultaneous six design variable (KOCR, T, ZM, P, TMX, THLE) optimization of full potential turbomachinery flows past compressor blades having NASA double circular arc blade profiles with the following initial values, lower, and upper bounds, respectively, of these parameters: (-10.0, 0.25, 0.45, 1.5, 0.05, 0.005), (-15.0, 0.20, 0.50, 0.03, 0.003), (0.00, 0.60, 0.55, 4.00, 0.10, 0.012).

The input data is tabulated in Figure A.1 with the COPES data appearing first, followed by the inputs for subroutine ANALIZ, subroutine TSONIC, and subroutine PERTURB. We note that in the input for subroutine PERTURB, the number of invariant points to be held invariant for this calculation were chosen to be one (NSELECT = 1), and that particular point was chosen as the maximum point (LSELECT(1) = 2, i.e.), the stagnation point, and that the dependent variable for print output will be symbolized by 'WM' denoting the surface speed. Examination of the sample input and comparison with the description of input data provided in Sections A.5.1 to A.5.3 provides a convenient, self-explanatory menu of how to prepare typical input data sets for future case studies.

Finally, Figure A.2 provides an abbreviated print output for this sample case. That output, together, with the information contained in Appendix A, provides a benchmark result that can be employed to completely verify the BLDOPT code on any user facility.

```

$---DATA BLOCK A
OPTIMIZATION TEST CASE 1 - MINIMIZE SUCTION SURFACE VELOCITY DIFFUSION
$---DATA BLOCK B
$   NCALC      NDV      NSV      N2VAR      NXAPRX      IPINPUT      IPDBG
      7          6
$---DATA BLOCK C
$   IPRINT     ITMAX     ICNDIR     NSCAL      ITRM      LINOBJ      NACMX1      NDFG
      5         1         -2         3         20
$---DATA BLOCK D
$ ALL DEFAULTS EXCEPT FOCH AND FDCHM
$   FDCH      FOCHM
      0.01     0.00100
$   DELFUN    DABFUN     ALPHAX     ABOBJI
      0.0      0.0       0.0       0.05
$---DATA BLOCK E
$   NDVTOT    IOBJ      SGNOPT
      1        -1.0
$---DATA BLOCK F
$   VLB      VUB      X      SCAL
$ OUTLET BLADE ANGLE - KOGR
      -15.0    0.0      0.0    -10.0
$ TRANSITION POINT LOCATION - T
      0.2     0.60    0.0    0.25
$ MAXIMUM THICKNESS LOCATION - ZM
      0.2     0.55    0.0    0.45
$ INLET/OUTLET TURNING RATE - P
      0.5     4.0     0.0    1.5
$ MAXIMUM THICKNESS - TMX
      0.03    0.10    0.0    0.05
$ LEADING EDGE RADIUS - THLE
      0.003   0.012   0.0    0.005
$---DATA BLOCK G
$   NDSGN     IDSGN     AMULT
$ OUTLET BLADE ANGLE - KOGR
      1        2        1.0
$ TRANSITION POINT LOCATION - T
      2        3        1.0
$ MAXIMUM THICKNESS LOCATION - ZM
      3        4        1.0
$ INLET/OUTLET TURNING RATE - P
      4        5        1.0
$ MAXIMUM THICKNESS - TMX
      5        6        1.0
$ LEADING EDGE RADIUS - THLE
      6        7        1.0
$---DATA BLOCK H
$   NCONS
      3
$---DATA BLOCK I
$   ICON      JCON      LCON
$   BL        SCAL1     BU        SCAL2
$ LOCAL BLADE THICKNESS CONSTRAINT - BLTKS
      8
      0.0     10.
$ PRESSURE SURFACE DIFFUSION - DIFFP
      9
      0.0     1.6
$ TRAILING EDGE CLOSURE - TECLSR
      10
      -1.     1.
$---DATA BLOCKS J-U NOT REQUIRED

```

Figure A.1.- Card input for sample case.


```

$---DATA BLOCK V
END
*** INPUT FOR SUBROUTINE ANALIZ ***
  3   6   3   6
 34  0.454  6.664  2.252
52.0 -10.0  0.25  0.45  1.5  0.05  0.005  0.005
KOCR  T      ZM  P      TMX  THLE
  2   3   4   5   6   7
  0   0.0
*** INPUT FOR SUBROUTINE TSONIC ***
1.400 1716.48 599.76 .00334586 .00570000 0.0 1.910
48.2  0.0  0.0  0.0  0.0  0.0
1.0  0.001 0.0  0.0
 24  56          72  15  34  13  0  1  0
          13.0
          13.0
-.13  -.005  .005  .02003  .04003  .08003  .10003  .12503
.15004 .17526 .18526 .22500 .27
.4540 .4540 .4540 .4540 .4540 .4540 .4540 .4540
.4540 .4540 .4540 .4540 .4540
.05 .05 .0499 .0496 .04925 .0485 .04815 .04770
.04720 .04675 .04661 .04661 .04661
0. 0. .0015 .0059 .0110 .0215 .0300 .0335
.0400 .0470 .048 .048 .048
  0  0  0  0  0  0  1
SEND
*** INPUT FOR SUBROUTINE PERTRB ***
OPTIMIZATION TEST CASE 1 - MINIMIZE SUCTION SURFACE VELOCITY DIFFUSION
  1  1  0
  2
WM
KOCR  T      ZM  P      TMX  THLE
-1.0  1.0

```

Figure A.1.- Concluded.

```

CCCCCC 000000  P P P P P  E E E E E  S S S S S
C      0      0  P   P  E       S
C      0      0  P   P  E       S
C      0      0  P P P P P  E E E E  S S S S S
C      0      0  P       E       S
C      0      0  P       E       S
CCCCCC 000000  P       E E E E E  S S S S S

```

```

      C O N T R O L   P R O G R A M
            F O R
    E N G I N E E R I N G   S Y N T H E S I S

```

```

      T I T L E
OPTIMIZATION TEST CASE 1 - MINIMIZE SUCTION SURFACE VELOCITY DIFFUSION

```

Figure A.2.- Abbreviated print output for sample case.

CARD IMAGES OF CONTROL DATA

CARD	IMAGE
1)	\$---DATA BLOCK A
2)	OPTIMIZATION TEST CASE 1 - MINIMIZE SUCTION SURFACE VELOCITY DIFFUSION
3)	\$---DATA BLOCK B
4)	\$ NCALC NDV NSV N2VAR NXAPRX IPNPUT IPDBG
5)	2 6
6)	\$---DATA BLOCK C
7)	\$ IPRINT ITMAX ICNDIR NSCAL ITRM LINOBJ NACHX1 NDFG
8)	5 1 -2 3 20
9)	\$---DATA BLOCK D
10)	\$ ALL DEFAULTS EXCEPT FDCH AND FDCHM
11)	\$ FDCH FDCHM
12)	0.01 0.00100
13)	\$ DELFUN DABFUN ALPHAX ABOBJ1
14)	0.0 0.0 0.0 0.05
15)	\$---DATA BLOCK E
16)	\$ NDVTOT IOBJ SGNOPT
17)	1 -1.0
18)	\$---DATA BLOCK F
19)	\$ VLB VUB X SCAL
20)	\$ OUTLET BLADE ANGLE - KOGR
21)	-15.0 0.0 0.0 -10.0
22)	\$ TRANSITION POINT LOCATION - T
23)	0.2 0.60 0.0 0.25
24)	\$ MAXIMUM THICKNESS LOCATION - ZM
25)	0.2 0.55 0.0 0.45
26)	\$ INLET/OUTLET TURNING RATE - P
27)	0.5 4.0 0.0 1.5
28)	\$ MAXIMUM THICKNESS - TMX
29)	0.03 0.10 0.0 0.05
30)	\$ LEADING EDGE RADIUS - THLE
31)	0.003 0.012 0.0 0.005
32)	\$---DATA BLOCK G
33)	\$ NDSGN IDSGN AMULT
34)	\$ OUTLET BLADE ANGLE - KOGR
35)	1 2 1.0
36)	\$ TRANSITION POINT LOCATION - T
37)	2 3 1.0
38)	\$ MAXIMUM THICKNESS LOCATION - ZM
39)	3 4 1.0
40)	\$ INLET/OUTLET TURNING RATE - P
41)	4 5 1.0
42)	\$ MAXIMUM THICKNESS - TMX
43)	5 6 1.0
44)	\$ LEADING EDGE RADIUS - THLE
45)	6 7 1.0
46)	\$---DATA BLOCK H
47)	\$ NCONS
48)	3
49)	\$---DATA BLOCK I
50)	\$ ICON JCON LCON
51)	\$ BL SCAL1 BU SCAL2
52)	\$ LOCAL BLADE THICKNESS CONSTRAINT - BLTKS
53)	H
54)	0.0 10.
55)	\$ PRESSURE SURFACE DIFFUSION - DIFFP
56)	0

```
57)      0.0      1.6
58) $ TRAILING EDGE CLOSURE - TECLSR
59)      10
60)      -1.      1.
61) $---DATA BLOCKS J-U NOT REQUIRED
62) $---DATA BLOCK V
63) END
```

Figure A.2.- Continued.

TITLE:
OPTIMIZATION TEST CASE 1 - MINIMIZE SUCTION SURFACE VELOCITY DIFFUSION

CONTROL PARAMETERS:
 CALCULATION CONTROL, NCALC = 2
 NUMBER OF GLOBAL DESIGN VARIABLES, NDV = 6
 NUMBER OF SENSITIVITY VARIABLES, NSV = 0
 NUMBER OF FUNCTIONS IN TWO-SPACE, N2VAR = 0
 NUMBER OF APPROXIMATING VAR, NXAPRX = 0
 INPUT INFORMATION PRINT CODE, IPNPUT = 0
 DEBUG PRINT CODE, IPDBG = 0

CALCULATION CONTROL, NCALC
 VALUE MEANING
 1 SINGLE ANALYSIS
 2 OPTIMIZATION
 3 SENSITIVITY
 4 TWO-VARIABLE FUNCTION SPACE
 5 OPTIMUM SENSITIVITY
 6 APPROXIMATE OPTIMIZATION

• • OPTIMIZATION INFORMATION

GLOBAL VARIABLE NUMBER OF OBJECTIVE = 1
 MULTIPLIER (NEGATIVE INDICATES MINIMIZATION) = -.1000E+01

CONMIN PARAMETERS (IF ZERO, CONMIN DEFAULT WILL OVER-RIDE)

IPRINT	ITMAX	ICNDR	NSCAL	ITRM	LINOBJ	NACMX1	NFDG
5	1	0	-2	3	0	20	0
FDCH		FDCHM		CT		CTMIN	
.10000E-01		.10000E-02		0.		0.	
CTL		CTLMIN		THETA		PHI	
0.		0.		0.		0.	
DELFUN		DARFUN		ALPHAX		ABOBJ1	
0.		0.		0.		.50000E-01	

DESIGN VARIABLE INFORMATION

D. V. NO.	LOWER BOUND	UPPER BOUND	INITIAL VALUE	SCALE
1	-.15000E+02	0.	0.	-.10000E+02
2	.20000E+00	.60000E+00	0.	.25000E+00
3	.20000E+00	.55000E+00	0.	.45000E+00
4	.50000E+00	.40000E+01	0.	.15000E+01
5	.30000E-01	.10000E+00	0.	.50000E-01
6	.30000E-02	.12000E-01	0.	.50000E-02

DESIGN VARIABLES

ID	D. V. NO.	GLOBAL VAR. NO.	MULTIPLYING FACTOR
1	1	2	.10000E+01

2	2	3	.10000E+01
3	3	4	.10000E+01
4	4	5	.10000E+01
5	5	6	.10000E+01
6	6	7	.10000E+01

CONSTRAINT INFORMATION

THERE ARE 3 CONSTRAINT SETS

ID	GLOBAL VAR. 1	GLOBAL VAR. 2	LINEAR ID	LOWER BOUND	NORMALIZATION FACTOR	UPPER BOUND	NORMALIZATION FACTOR
1	8	0	0	0.	.10000E+00	.10000E+02	.10000E+02
3	9	0	0	0.	.10000E+00	.16000E+01	.16000E+01
5	10	0	0	-.10000E+01	.10000E+01	.10000E+01	.10000E+01

TOTAL NUMBER OF CONSTRAINED PARAMETERS = 3

• • ESTIMATED DATA STORAGE REQUIREMENTS

INPUT	REAL EXECUTION	AVAILABLE	INPUT	INTEGER EXECUTION	AVAILABLE
57	779	5000	34	112	1000

Figure A.2.- Continued.

--- INPUT FOR CONTROL SUBROUTINE ANALIZ ---

CONTROL PARAMETERS

IOPT = 3 NDV = 6 NCN = 3 ITMAX3 = 6

CONSTANT BLADE PARAMETERS

NB	R	ALP	SOLID
34	.4540	6.6640	2.2520

VARIABLE BLADE PARAMETERS

KICR	KOCR	T	ZM	P	TMX	THLE	THTE
52.0000	-10.0000	.2500	.4500	1.5000	.0500	.0050	.0050

ACTIVE DESIGN VARIABLES

KOCR	T	ZM	P	TMX	THLE
-10.0000	.2500	.4500	1.5000	.0500	.0050

ICALB = 0 PSTEP = 0.000

Figure A.2.- Continued.

--- INPUT FOR TSONIC BLADE-TO-BLADE FLOW SOLVER ---

GAM	AR	TIP	RHOIP	WTFL	OMEGA	ORF				
1.400000	1716.480	599.7600	.3345860E-02	.5700000E-02	0.	1.910000				
BETAI	BETA0	CHORUF	STGRF	FSMI	FSMO					
48.20000	0.	0.	0.	0.	0.					
REDFAC	DENTOL	SSM1	SSM2							
1.000000	.1000000E-02	0.	0.							
MBI	MBO	MM	NBBI	NBL	NRSP	MOPT	LOPT	LRVB		
24	56	0	0	72	15	34	13	0	1	0
BLADE SURFACE 1 -- UPPER SURFACE										
RI1	RO1	BETI1	BET01	SPLN01						
0.	0.	0.	0.	13.00000						
MSP1	ARRAY									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
THSP1	ARRAY									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
BLADE SURFACE 2 -- LOWER SURFACE										
RI2	RO2	BETI2	BET02	SPLN02						
0.	0.	0.	0.	13.00000						
MSP2	ARRAY									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
THSP2	ARRAY									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
MR	ARRAY									
-.1300000	-.5000000E-02	.5000000E-02	.2003000E-01	.4003000E-01	.8003000E-01	.1000300	.1250300			
.1500400	.1752600	.1852600	.2250000	.2700000						
RMSP	ARRAY									
.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000			
.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000			
BESP	ARRAY									
.5000000E-01	.5000000E-01	.4990000E-01	.4960000E-01	.4925000E-01	.4850000E-01	.4815000E-01	.4770000E-01			
.4720000E-01	.4675000E-01	.4661000E-01	.4661000E-01	.4661000E-01						
PLOSS	ARRAY									
0.	0.	.1500000E-02	.5900000E-02	.1100000E-01	.2150000E-01	.3000000E-01	.3350000E-01			
.4000000E-01	.4700000E-01	.4800000E-01	.4800000E-01	.4800000E-01						
BLDAT	AANDK	ERSOR	STRFN	SLCRD	INTVL	SURVL				
0	0	0	0	0	0	1				

Figure A.2.- Continued.

--- INPUT FOR PERTURBATION METHOD ---

* OPTIMIZATION TEST CASE 1 - MINIMIZE SUCTION SURFACE VELOCITY DIFFUSION *

.....LIST OF INPUT PARAMETERS

N = 62
A = -1.0 B = 1.0
NPARAM = 6

.....STRAINING OPTIONS

NUMBER OF FIXED POINTS: 3
FIXED POINTS WILL BE AUTOMATICALLY DETERMINED
BY THE PROGRAM FOR ALL SOLUTIONS AS FOLLOWS:
TWO END POINTS
POINT OF MAXIMUM WM

Figure A.2.- Continued.

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX, THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-10.0000	.25000	.45000	1.50000	.05000	.00500	.00500

Figure A.2.- Continued.

--- INPUT FOR TSONIC BLADE-TO-BLADE FLOW SOLVER ---

GAM	AR	TIP	RHOIP	WTFLL	OMEGA	ORF		
1.400000	1716.480	599.7600	.3345860E-02	.5700000E-02	0.	1.910000		
BETA1	BETA0	CHORDF	STGRF	FSM1	FSM0			
48.20000	0.	.1834184	.1311528	0.	0.			
REDFAC	DENTOL	SSM1	SSM2					
1.000000	.1000000E-02	0.	0.					
MBI	MB0	MM	NBBI	NBL	NRSP	MOPT	LOPT	LRVB
24	56	0	0	72	15	34	13	0
BLADE SURFACE 1	-- UPPER SURFACE							
R11	R01	BET11	BET01	SPLN01				
.9668364E-03	.9668364E-03	57.62951	-13.13649	13.00000				
MSP1 ARRAY								
.1503113E-03	.5980107E-02	.1529854E-01	.2744253E-01	.4447412E-01	.6273379E-01	.8187670E-01	.1016760	
.1218970	.1423000	.1585911	.1727172	.1826858				
THSP1 ARRAY								
.1140045E-02	.1958139E-01	.4336945E-01	.6726818E-01	.9178661E-01	.1116067	.1269242	.1375985	
.1435478	.1447487	.1423112	.1377348	.1330935				
BLADE SURFACE 2	-- LOWER SURFACE							
R12	R02	BET12	BET02	SPLN02				
.9668364E-03	.9668364E-03	46.20771	-5.047831	13.00000				
MSP2 ARRAY								
.1664865E-02	.8669538E-02	.1911677E-01	.3189241E-01	.4893131E-01	.6676995E-01	.8523057E-01	.1041871	
.1235102	.1430679	.1587932	.1725519	.1823521				
THSP2 ARRAY								
-.1473028E-02	.1370723E-01	.3337744E-01	.5345856E-01	.7484201E-01	.9279699E-01	.1074271	.1186613	
.1264542	.1307850	.1317585	.1308042	.1290985				
MR ARRAY								
-.1300000	-.5000000E-02	.5000000E-02	.2003000E-01	.4003000E-01	.8003000E-01	.1000300	.1250300	
.1500400	.1752600	.1852600	.2250000	.2700000				
RMSP ARRAY								
.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	
.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	
BESP ARRAY								
.5000000E-01	.5000000E-01	.4990000E-01	.4960000E-01	.4925000E-01	.4850000E-01	.4815000E-01	.4770000E-01	
.4720000E-01	.4675000E-01	.4661000E-01	.4661000E-01	.4661000E-01				
PLOSS ARRAY								
0.	0.	.1500000E-02	.5900000E-02	.1100000E-01	.2150000E-01	.3000000E-01	.3350000E-01	
.4000000E-01	.4700000E-01	.4800000E-01	.4800000E-01	.4800000E-01				
BLDAT	AANDK	ERSOR	STRFN	SLCRD	INTVL	SURVL		
0	0	0	0	0	0	1		

Figure A.2.- Continued.

RELATIVE VELOCITY	MERIDIONAL VELOCITY	CRITICAL VELOCITY	REL. FLOW ANGLE
AT M = FSMI	AT M = FSMI	AT M = FSMI	AT UPSTREAM BDY.
745.90	497.17	1095.9	48.237
AT M = FSMO	AT M = FSMO	AT M = FSMO	AT DOWNSTREAM BDY.
499.45	499.45	1095.9	0.
FSMI = 0.			
FSMO = .18342			

CALCULATED PROGRAM CONSTANTS

PITCH	HT	HM1
.1847996	.1231997E-01	.5731826E-02
ITMIN	ITMAX	
0	25	
LAMBDA	DOWNSTREAM WHIRL (RVTHO)	
252.4466	0.	
REDUCED WEIGHT FLOW =	.5700000E-02	
NUMBER OF INTERIOR MESH POINTS =	1035	

CALCULATED VELOCITY DIAGRAM INFORMATION

	IM	W	W/WCR	BETA
UPSTREAM BOUNDARY	1	745.47	.68022	48.237
LEADING EDGE	24	745.90	.68061	48.200
TRAILING EDGE	56	499.45	.45573	0.
DOWNSTREAM BOUNDARY	72	500.06	.45629	0.

Figure A.2.- Continued.

ITERATION NO. 1
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3059 AT IM = 0, IT = 11, SURF = 1, M = .1779
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1105
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 86

ITERATION NO. 2
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2681 AT IM = 0, IT = 11, SURF = 1, M = .1779
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2909E-01
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 86

ITERATION NO. 3
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .4396 AT IM = 0, IT = 11, SURF = 1, M = .1779
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1291E-01
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 85

ITERATION NO. 4
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = 3.182 AT IM = 0, IT = 11, SURF = 1, M = .1779
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3816E-01
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 53
 DENSITY CALL NO. 9
 NER(1) = 1
 RHO*W IS 1.2430 TIMES THE MAXIMUM VALUE FOR RHO*W

ITERATION NO. 5
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .8418 AT IM = 0, IT = 11, SURF = 1, M = .1779
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1041E-01
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 22

ITERATION NO. 6
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3818 AT IM = 0, IT = 11, SURF = 1, M = .1779
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .4669E-02
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 12

ITERATION NO. 7
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = 1.655 AT IM = 0, IT = 11, SURF = 1, M = .1779
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1857E-01
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 8
 DENSITY CALL NO. 9
 NER(1) = 2
 RHO*W IS 1.2455 TIMES THE MAXIMUM VALUE FOR RHO*W

ITERATION NO. 8
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .7274 AT IM = 0, IT = 11, SURF = 1, M = .1779
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .8167E-02

NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1

ITERATION NO. 9

MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3803 AT IM = 0, IT = 11, SURF = 1, M = .1779
AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .4269E-02
NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1

ITERATION NO. 10

MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = 1.635 AT IM = 0, IT = 11, SURF = 1, M = .1779
AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1820E-01
NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1

DENSTY CALL NO. 9

NER(1) = 3

RHO*W IS 1.2472 TIMES THE MAXIMUM VALUE FOR RHO*W

ITERATION NO. 11

MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .7251 AT IM = 0, IT = 11, SURF = 1, M = .1779
AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .8072E-02
NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1

Figure A.2.- Continued.

SURFACE VELOCITIES BASED ON MERIDIONAL COMPONENTS - REDUCED WEIGHT FLOW									
M	VELOCITY	BLADF SURFACE 1			W/WCR	VELOCITY	BLADE SURFACE 2		
		ANGLE(DEG)	SURF. LENGTH	W/WCR			ANGLE(DEG)	SURF. LENGTH	W/WCR
0.	0.	90.00	0.	0.	0.	0.	-90.00	0.	0.
.5732E-02	* 871.6	52.87	.1030E-01	.7953	* 608.5	44.24	.6680E-02	.5552	*
.1146E-01	* 909.2	48.47	.1935E-01	.8296	* 579.5	41.58	.1451E-01	.5287	*
.1720E-01	* 919.0	44.47	.2767E-01	.8385	* 554.2	39.02	.2202E-01	.5057	*
.2293E-01	* 910.1	40.64	.3545E-01	.8304	* 536.5	36.57	.2927E-01	.4895	*
.2866E-01	* 884.7	36.99	.4281E-01	.8073	* 524.8	34.15	.3630E-01	.4789	*
.3439E-01	* 848.7	33.70	.4984E-01	.7744	* 515.5	31.78	.4313E-01	.4704	*
.4012E-01	* 811.1	30.94	.5661E-01	.7401	* 509.7	29.64	.4980E-01	.4651	*
.4585E-01	* 782.6	28.82	.6322E-01	.7141	* 506.7	27.78	.5633E-01	.4623	*
.5159E-01	* 760.0	26.89	.6971E-01	.6935	* 502.7	26.21	.6277E-01	.4587	*
.5732E-01	* 743.6	24.95	.7608E-01	.6785	* 498.7	24.68	.6911E-01	.4550	*
.6305E-01	* 727.9	23.02	.8235E-01	.6642	* 493.4	23.16	.7538E-01	.4502	*
.6878E-01	* 716.3	21.09	.8854E-01	.6536	* 489.6	21.65	.8158E-01	.4468	*
.7451E-01	* 705.9	19.20	.9464E-01	.6441	* 485.1	20.15	.8772E-01	.4426	*
.8025E-01	* 694.6	17.36	.1007	.6338	* 482.3	18.68	.9380E-01	.4401	*
.8598E-01	* 687.5	15.55	.1067	.6273	* 479.9	17.23	.9982E-01	.4379	*
.9171E-01	* 680.8	13.75	.1126	.6212	* 476.3	15.79	.1058	.4346	*
.9744E-01	* 672.8	11.97	.1185	.6139	* 474.2	14.37	.1117	.4327	*
.1032	* 666.8	10.22	.1243	.6085	* 471.9	12.96	.1176	.4306	*
.1089	* 660.3	8.47	.1301	.6025	* 469.8	11.56	.1235	.4287	*
.1146	* 653.6	6.73	.1359	.5964	* 466.0	10.17	.1293	.4252	*
.1204	* 646.4	5.01	.1417	.5898	* 465.3	8.80	.1351	.4246	*
.1261	* 639.3	3.30	.1474	.5834	* 464.7	7.45	.1409	.4241	*
.1318	* 632.1	1.60	.1531	.5768	* 464.7	6.09	.1467	.4240	*
.1376	* 624.4	-.09	.1589	.5698	* 465.8	4.72	.1525	.4250	*
.1433	* 616.1	-1.76	.1646	.5622	* 468.3	3.36	.1582	.4273	*
.1490	* 606.4	-3.45	.1703	.5534	* 472.3	2.02	.1640	.4310	*
.1548	* 594.3	-5.17	.1761	.5423	* 477.9	.75	.1697	.4360	*
.1605	* 578.3	-6.92	.1819	.5277	* 485.3	-.48	.1754	.4428	*
.1662	* 557.6	-8.56	.1876	.5088	* 496.7	-1.89	.1812	.4532	*
.1720	* 531.8	-10.05	.1934	.4853	* 521.7	-3.55	.1869	.4760	*
.1777	* 499.1	-11.58	.1993	.4554	* 600.4	-4.87	.1926	.5478	*
.1834	* 0.	-90.00	.2054	0.	* 0.	90.00	.1984	0.	*

Figure A.2.- Continued.

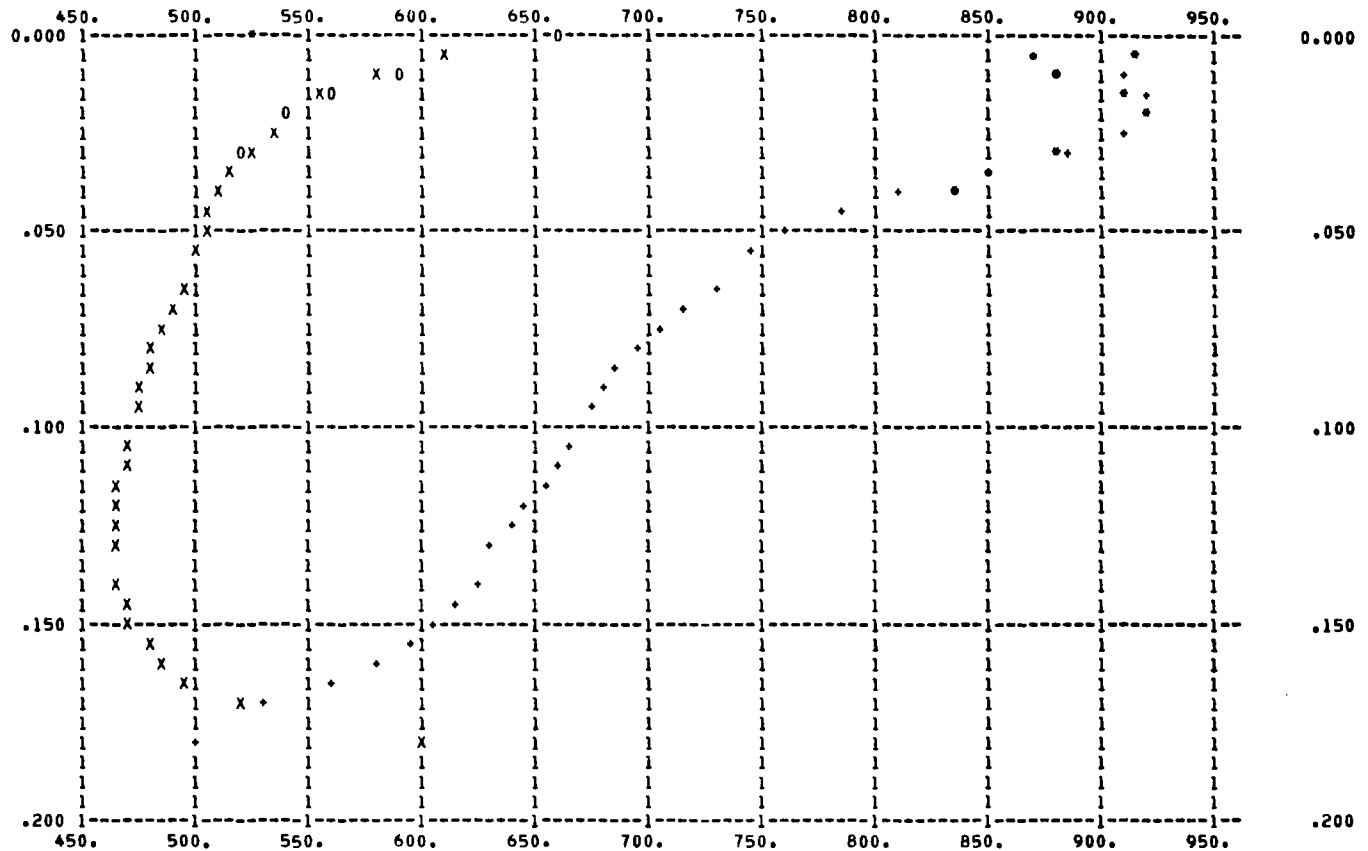
SURFACE VELOCITIES BASED ON TANGENTIAL COMPONENTS
REDUCED WEIGHT FLOW

M	BLADE SURFACE 1		W/WCR
	VELOCITY	ANGLE (DEG)	
0.	522.7	90.00	.4769
.3555E-02	914.3	54.65	.8343
.7776E-02	880.0	51.28	.8030
.1256E-01	911.6	47.67	.8318
.1800E-01	919.8	43.93	.8393
.2424E-01	909.4	39.79	.8298
.3152E-01	879.6	35.29	.8026
.4012E-01	833.8	30.94	.7608
.5018E-01	777.0	27.36	.7090
.6197E-01	743.7	23.38	.6786
.7657E-01	708.7	18.53	.6466
.9699E-01	694.0	12.11	.6333
.1779	1096.	-11.65	1.000

M	BLADE SURFACE 2		W/WCR
	VELOCITY	ANGLE (DEG)	
.2310E-02	660.1	45.89	.6023
.7995E-02	592.4	43.18	.5406
.1426E-01	560.6	40.32	.5115
.2122E-01	538.8	37.30	.4916
.2901E-01	517.8	34.00	.4725
.3790E-01	509.2	30.44	.4647
.4811E-01	502.4	27.13	.4585
.5979E-01	492.8	24.03	.4496
.7348E-01	484.4	20.42	.4420
.9043E-01	474.9	16.11	.4334
.1143	465.4	10.25	.4247

Figure A.2.- Continued.

BLADE SURFACE VELOCITIES FOR FULL WEIGHT FLOW



VELOCITY (W) VS. MERIDIONAL STREAMLINE DISTANCE (M) DOWN THE PAGE

- + - BLADE SURFACE 1, BASED ON MERIDIONAL COMPONENT
- - BLADE SURFACE 1, BASED ON TANGENTIAL COMPONENT
- x - BLADE SURFACE 2, BASED ON MERIDIONAL COMPONENT
- o - BLADE SURFACE 2, BASED ON TANGENTIAL COMPONENT

Figure A.2.- Continued.

BLADE SURFACE PRESSURES FOR FULL WEIGHT FLOW

IM	M	M/MC	P(1)/PT	P(2)/PT	CPT(1)	CPT(2)
24	0.	0.	.9994	.9994	-.6204E-03	-.6204E-03
25	.5732E-02	.3125E-01	.6760	.8301	-.3240	-.1699
26	.1146E-01	.6250E-01	.6507	.8435	-.3493	-.1565
27	.1720E-01	.9375E-01	.6432	.8543	-.3568	-.1457
28	.2293E-01	.1250	.6479	.8612	-.3521	-.1388
29	.2866E-01	.1563	.6631	.8652	-.3369	-.1348
30	.3439E-01	.1875	.6850	.8682	-.3150	-.1318
31	.4012E-01	.2188	.7074	.8697	-.2926	-.1303
32	.4585E-01	.2500	.7239	.8700	-.2761	-.1300
33	.5159E-01	.2813	.7365	.8707	-.2635	-.1293
34	.5732E-01	.3125	.7452	.8714	-.2548	-.1286
35	.6305E-01	.3438	.7533	.8725	-.2467	-.1275
36	.6878E-01	.3750	.7587	.8728	-.2413	-.1272
37	.7451E-01	.4063	.7631	.8731	-.2369	-.1269
38	.8025E-01	.4375	.7677	.8722	-.2323	-.1278
39	.8598E-01	.4688	.7696	.8710	-.2304	-.1290
40	.9171E-01	.5000	.7712	.8701	-.2288	-.1299
41	.9744E-01	.5313	.7736	.8689	-.2264	-.1311
42	.1032	.5625	.7755	.8684	-.2245	-.1316
43	.1089	.5938	.7782	.8683	-.2218	-.1317
44	.1146	.6250	.7813	.8693	-.2187	-.1307
45	.1204	.6563	.7846	.8691	-.2154	-.1309
46	.1261	.6875	.7877	.8687	-.2123	-.1313
47	.1318	.7188	.7906	.8677	-.2094	-.1323
48	.1376	.7500	.7933	.8660	-.2067	-.1340
49	.1433	.7813	.7961	.8635	-.2039	-.1365
50	.1490	.8125	.7995	.8602	-.2005	-.1398
51	.1548	.8438	.8039	.8563	-.1961	-.1437
52	.1605	.8750	.8101	.8516	-.1899	-.1484
53	.1662	.9063	.8184	.8453	-.1816	-.1547
54	.1720	.9375	.8289	.8334	-.1711	-.1666
55	.1777	.9688	.8423	.7961	-.1577	-.2039
56	.1834	1.000	.9521	.9521	-.4788E-01	-.4788E-01

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

600.354	521.669	496.727	485.325	477.873
472.312	468.339	465.802	464.706	464.733
465.289	466.016	469.834	471.882	474.222
476.253	479.869	482.344	485.093	489.643
493.390	498.688	502.725	506.666	509.703

Figure A.2.- Continued.

515.508	524.794	536.506	554.157	579.455
608.451	871.598	909.197	918.981	910.061
884.702	848.724	811.096	782.606	760.025
743.617	727.894	716.322	705.924	694.579
687.479	680.820	672.815	666.824	660.302
653.568	646.379	639.342	632.094	624.435
616.098	606.446	594.286	578.274	557.598
531.810	499.051			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.91898E+03
	WO	=	.49945E+03
	DIFFS/WO	=	.18400E+01
CONSTRAINT 1	BLTKS	=	.66765E+00
CONSTRAINT 2	YMAX	=	.60845E+03
	YMIN	=	.46471E+03
	DIFFP	=	.13093E+01
CONSTRAINT 3	WMB(MB0-2,1)	=	.53181E+03
	WMB(MB0-2,2)	=	.52167E+03
	TECLSR	=	.12677E+00

Figure A.2.- Continued.

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* * * * *
*           C O N M I N
*
*           FORTRAN PROGRAM FOR
*
*           CONSTRAINED FUNCTION MINIMIZATION
*
* * * * *

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CONSTRAINED FUNCTION MINIMIZATION

CONTROL PARAMETERS

IPRINT	NDV	ITMAX	NCON	NSIDE	ICNDIR	NSCAL	NFDG
5	6	1	6	1	7	-2	0
LINOBJ	ITRM	N1	N2	N3	N4	N5	
0	3	8	18	20	20	40	
CT	CTMIN	CTL	CTLMIN				
-.10000E+00	.40000E-02	-.10000E-01	.10000E-02				
THETA	PHI	DELFUN	DABFUN				
.10000E+01	.50000E+01	.10000E-03	.18400E-02				
FDCH	FDCHM	ALPHAX	ABOBJ1				
.10000E-01	.10000E-02	.10000E+00	.50000E-01				
LOWER BOUNDS ON DECISION VARIABLES (VLB)							
1)	-.15000E+01	.80000E+00	.44444E+00	.33333E+00	.60000E+00	.60000E+00	
UPPER BOUNDS ON DECISION VARIABLES (VUB)							
1)	0.	.24000E+01	.12222E+01	.26667E+01	.20000E+01	.24000E+01	
SCALING VECTOR (SCAL)							
	.1000E+02	.2500E+00	.4500E+00	.1500E+01	.5000E-01	.5000E-02	
ALL CONSTRAINTS ARE NON-LINEAR							
INITIAL FUNCTION INFORMATION							
OBJ =	.183998E+01						
DECISION VARIABLES (X-VECTOR)							
1)	-.10000E+02	.25000E+00	.45000E+00	.15000E+01	.50000E-01	.50000E-02	
CONSTRAINT VALUES (G-VECTOR)							
1)	-.66765E+01	-.93323E+00	-.13093E+02	-.18167E+00	-.11268E+01	-.87323E+00	

Figure A.2.- Continued.

BEGIN ITERATION NUMBER 1

CT = -.10000E+00 CTL = -.10000E-01 PHI = .50000E+01

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-9.9000	.25000	.45000	1.50000	.05000	.00500	.00500

Figure A.2.- Continued.

--- INPUT FOR TSONIC BLADE-TO-BLADE FLOW SOLVER ---

GAM	AR	TIP	RHOIP	WTFLL	OMEGA	ORF		
1.400000	1714.480	599.7600	.3345860E-02	.5700000E-02	0.	1.910000		
BETA1	BETA0	CHORDF	STGRF	FSMI	FSMO			
48.20000	0.	.1833593	.1315224	0.	0.			
REDFAC	DENTOL	SSM1	SSM2					
1.000000	.1000000E-02	0.	0.					
MBI	MBO	MM	NBBI	NBL	NRSP	MOPT	LOPT	LRVB
24	56	0	0	72	15	34	13	0
							1	0
BLADE SURFACE 1 -- UPPER SURFACE								
RI1	RO1	BETI1	BETO1	SPLN01				
.9668292E-03	.9668292E-03	57.63155	-13.03485	13.00000				
MSP1 ARRAY								
.1502917E-03	.5978272E-02	.1529266E-01	.2743032E-01	.4445239E-01	.6270190E-01	.8183494E-01	.1016254	
.1218393	.1422379	.1585276	.1726546	.1826251				
THSP1 ARRAY								
.1139973E-02	.1957908E-01	.4336726E-01	.6727171E-01	.9180706E-01	.1116533	.1270053	.1377225	
.1437228	.1449823	.1425966	.1380689	.1334640				
BLADE SURFACE 2 -- LOWER SURFACE								
RI2	RO2	BETI2	BETO2	SPLN02				
.9668292E-03	.9668292E-03	46.20589	-4.944609	13.00000				
MSP2 ARRAY								
.1664831E-02	.8668414E-02	.1911275E-01	.3188349E-01	.4891460E-01	.6674475E-01	.8519690E-01	.1041455	
.1234617	.1430141	.1587367	.1724944	.1822947				
THSP2 ARRAY								
-.1473066E-02	.1370572E-01	.3337749E-01	.5346616E-01	.7486838E-01	.9285030E-01	.1075148	.1187910	
.1266333	.1310207	.1320445	.1311376	.1294676				
MR ARRAY								
-.1300000	-.5000000E-02	.5000000E-02	.2003000E-01	.4003000E-01	.8003000E-01	.1000300	.1250300	
.1500400	.1752600	.1852600	.2250000	.2700000				
RMSR ARRAY								
.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	
.4540000	.4540000	.4540000	.4540000	.4540000				
BESP ARRAY								
.5000000E-01	.5000000E-01	.4990000E-01	.4960000E-01	.4925000E-01	.4850000E-01	.4815000E-01	.4770000E-01	
.4720000E-01	.4675000E-01	.4661000E-01	.4661000E-01	.4661000E-01				
PLOSS ARRAY								
0.	0.	.1500000E-02	.5900000E-02	.1100000E-01	.2150000E-01	.3000000E-01	.3350000E-01	
.4000000E-01	.4700000E-01	.4800000E-01	.4800000E-01	.4800000E-01				
BLDAT	AANDK	ERSOR	STRFN	SLCRD	INTVL	SURVL		
0	0	0	0	0	0	1		

Figure A.2.- Continued.

RELATIVE VELOCITY	MERIDIONAL VELOCITY	CRITICAL VELOCITY	REL. FLOW ANGLE
AT M = FSMI	AT M = FSMI	AT M = FSMI	AT UPSTREAM BDY.
745.90	497.17	1095.9	48.237
AT M = FSMO	AT M = FSMO	AT M = FSMO	AT DOWNSTREAM BDY.
499.44	499.44	1095.9	0.

FSMI = 0.
FSMO = .18336

CALCULATED PROGRAM CONSTANTS

PITCH	HT	HM1
.1847996	.1231997E-01	.5729979E-02
ITMIN	ITMAX	
0	25	
LAMBDA	DOWNSTREAM WHIRL (RVTHD)	
252.4466	0.	
REDUCED WEIGHT FLOW =	.5700000E-02	
NUMBER OF INTERIOR MESH POINTS =	1035	

CALCULATED VELOCITY DIAGRAM INFORMATION

	IM	W	W/WCR	BETA
UPSTREAM BOUNDARY	1	745.47	.68022	48.237
LEADING EDGE	24	745.90	.68061	48.200
TRAILING EDGE	56	499.44	.45572	0.
DOWNSTREAM BOUNDARY	72	500.06	.45629	0.

Figure A.2.- Continued.

ITERATION NO. 1
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3084 AT IM = 0, IT = 11, SURF = 1, M = .1786
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1106
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 86

ITERATION NO. 2
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2718 AT IM = 0, IT = 11, SURF = 1, M = .1786
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2915E-01
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 86

ITERATION NO. 3
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .4543 AT IM = 0, IT = 11, SURF = 1, M = .1786
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1308E-01
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 85

ITERATION NO. 4
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = 3.728 AT IM = 0, IT = 11, SURF = 1, M = .1786
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .4423E-01
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 53
 DENSITY CALL NO. 9
 NER(1) = 1
 RHO*W IS 1.2462 TIMES THE MAXIMUM VALUE FOR RHO*W

ITERATION NO. 5
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .8621 AT IM = 0, IT = 11, SURF = 1, M = .1786
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1063E-01
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 23

ITERATION NO. 6
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3878 AT IM = 0, IT = 11, SURF = 1, M = .1786
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .4736E-02
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 13

ITERATION NO. 7
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = 1.740 AT IM = 0, IT = 11, SURF = 1, M = .1786
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1951E-01
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 8
 DENSITY CALL NO. 9
 NER(1) = 2
 RHO*W IS 1.2487 TIMES THE MAXIMUM VALUE FOR RHO*W

ITERATION NO. 8
 MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .7370 AT IM = 0, IT = 11, SURF = 1, M = .1786
 AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .8272E-02

Figure A.2.- Continued.

NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1

ITERATION NO. 9
MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3891 AT IM = 0, IT = 11, SURF = 1, M = .1786
AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .4369E-02
NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1

ITERATION NO. 10
MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = 1.757 AT IM = 0, IT = 11, SURF = 1, M = .1786
AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1955E-01
NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1

DENSTY CALL NO. 9
NER(1) = 3
RHO*W IS 1.2486 TIMES THE MAXIMUM VALUE FOR RHO*W

ITERATION NO. 11
MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .7389 AT IM = 0, IT = 11, SURF = 1, M = .1786
AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .8235E-02
NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1

SURFACE VELOCITIES BASED ON MERIDIONAL COMPONENTS - REDUCED WEIGHT FLOW										
M	VELOCITY	BLADE SURFACE 1			W/WCR	VELOCITY	BLADE SURFACE 2			W/WCR
		ANGLE (DEG)	SURF. LENGTH				ANGLE (DEG)	SURF. LENGTH		
0.	0.	90.00	0.	0.	0.	-90.00	0.	0.	0.	0.
.5730E-02	* 871.3	52.88	.1030E-01	.7950	* 608.9	44.25	.6677E-02	.5556	*	*
.1146E-01	* 909.0	48.49	.1935E-01	.8294	* 579.9	41.59	.1450E-01	.5292	*	*
.1719E-01	* 918.8	44.49	.2767E-01	.8384	* 554.6	39.03	.2202E-01	.5061	*	*
.2292E-01	* 910.0	40.66	.3545E-01	.8304	* 537.0	36.59	.2927E-01	.4900	*	*
.2865E-01	* 884.7	37.02	.4281E-01	.8073	* 525.2	34.17	.3630E-01	.4793	*	*
.3438E-01	* 849.2	33.73	.4983E-01	.7749	* 516.0	31.81	.4313E-01	.4708	*	*
.4011E-01	* 811.3	30.97	.5661E-01	.7402	* 510.1	29.67	.4979E-01	.4655	*	*
.4584E-01	* 782.8	28.85	.6322E-01	.7143	* 507.1	27.82	.5633E-01	.4627	*	*
.5157E-01	* 760.2	26.93	.6970E-01	.6937	* 503.1	26.25	.6276E-01	.4591	*	*
.5730E-01	* 743.9	25.00	.7608E-01	.6787	* 499.1	24.73	.6911E-01	.4554	*	*
.6303E-01	* 728.1	23.06	.8235E-01	.6644	* 493.7	23.21	.7538E-01	.4505	*	*
.6876E-01	* 716.5	21.14	.8853E-01	.6538	* 490.0	21.70	.8158E-01	.4471	*	*
.7449E-01	* 706.1	19.25	.9464E-01	.6443	* 485.4	20.20	.8771E-01	.4429	*	*
.8022E-01	* 694.8	17.40	.1007	.6339	* 482.6	18.73	.9379E-01	.4404	*	*
.8595E-01	* 687.6	15.60	.1067	.6274	* 480.2	17.28	.9982E-01	.4382	*	*
.9168E-01	* 681.0	13.81	.1126	.6214	* 476.6	15.85	.1058	.4349	*	*
.9741E-01	* 672.9	12.03	.1185	.6140	* 474.4	14.43	.1117	.4329	*	*
.1031	* 666.9	10.27	.1243	.6085	* 472.2	13.02	.1176	.4309	*	*
.1089	* 660.5	8.53	.1301	.6027	* 470.0	11.62	.1235	.4288	*	*
.1146	* 653.6	6.80	.1359	.5964	* 467.2	10.24	.1293	.4263	*	*
.1203	* 646.5	5.07	.1416	.5899	* 465.4	8.87	.1351	.4247	*	*
.1261	* 639.3	3.37	.1474	.5834	* 464.7	7.52	.1409	.4240	*	*
.1318	* 632.2	1.67	.1531	.5769	* 464.8	6.16	.1467	.4241	*	*
.1375	* 624.6	-.01	.1589	.5699	* 465.9	4.80	.1525	.4252	*	*
.1432	* 616.2	-1.68	.1646	.5623	* 468.3	3.43	.1582	.4273	*	*
.1490	* 606.5	-3.37	.1703	.5534	* 472.3	2.10	.1639	.4310	*	*
.1547	* 594.4	-5.09	.1761	.5424	* 477.9	.83	.1697	.4361	*	*
.1604	* 578.6	-6.83	.1818	.5280	* 485.2	-.40	.1754	.4427	*	*
.1662	* 558.0	-8.47	.1876	.5091	* 496.4	-1.80	.1811	.4530	*	*
.1719	* 532.3	-9.97	.1934	.4857	* 521.3	-3.46	.1869	.4757	*	*
.1776	* 499.8	-11.49	.1992	.4561	* 598.6	-4.77	.1926	.5462	*	*
.1834	* 0.	-90.00	.2053	0.	* 0.	90.00	.1984	0.	*	*

Figure A.2.- Continued.

SURFACE VELOCITIES BASED ON TANGENTIAL COMPONENTS
REDUCED WEIGHT FLOW

M	BLADE SURFACE 1		W/WCR
	VELOCITY	ANGLE (DEG)	
0.	522.3	90.00	.4766
.3554E-02	913.9	54.66	.8339
.7774E-02	879.7	51.29	.8027
.1255E-01	911.4	47.68	.8316
.1799E-01	919.7	43.95	.8392
.2423E-01	909.4	39.81	.8298
.3150E-01	879.6	35.33	.8027
.4009E-01	833.0	30.98	.7601
.5013E-01	777.3	27.41	.7092
.6189E-01	744.0	23.44	.6788
.7644E-01	708.7	18.62	.6467
.9671E-01	693.5	12.25	.6328
.1786	1096.	-11.78	1.000

M	BLADE SURFACE 2		W/WCR
	VELOCITY	ANGLE (DEG)	
.2310E-02	660.6	45.89	.6028
.7994E-02	592.9	43.18	.5410
.1426E-01	561.1	40.33	.5120
.2121E-01	539.3	37.31	.4921
.2900E-01	518.3	34.02	.4729
.3788E-01	509.7	30.47	.4651
.4807E-01	502.8	27.18	.4588
.5973E-01	493.1	24.08	.4499
.7337E-01	484.7	20.49	.4423
.9024E-01	475.2	16.21	.4336
.1139	466.1	10.41	.4253

Figure A.2.- Continued.

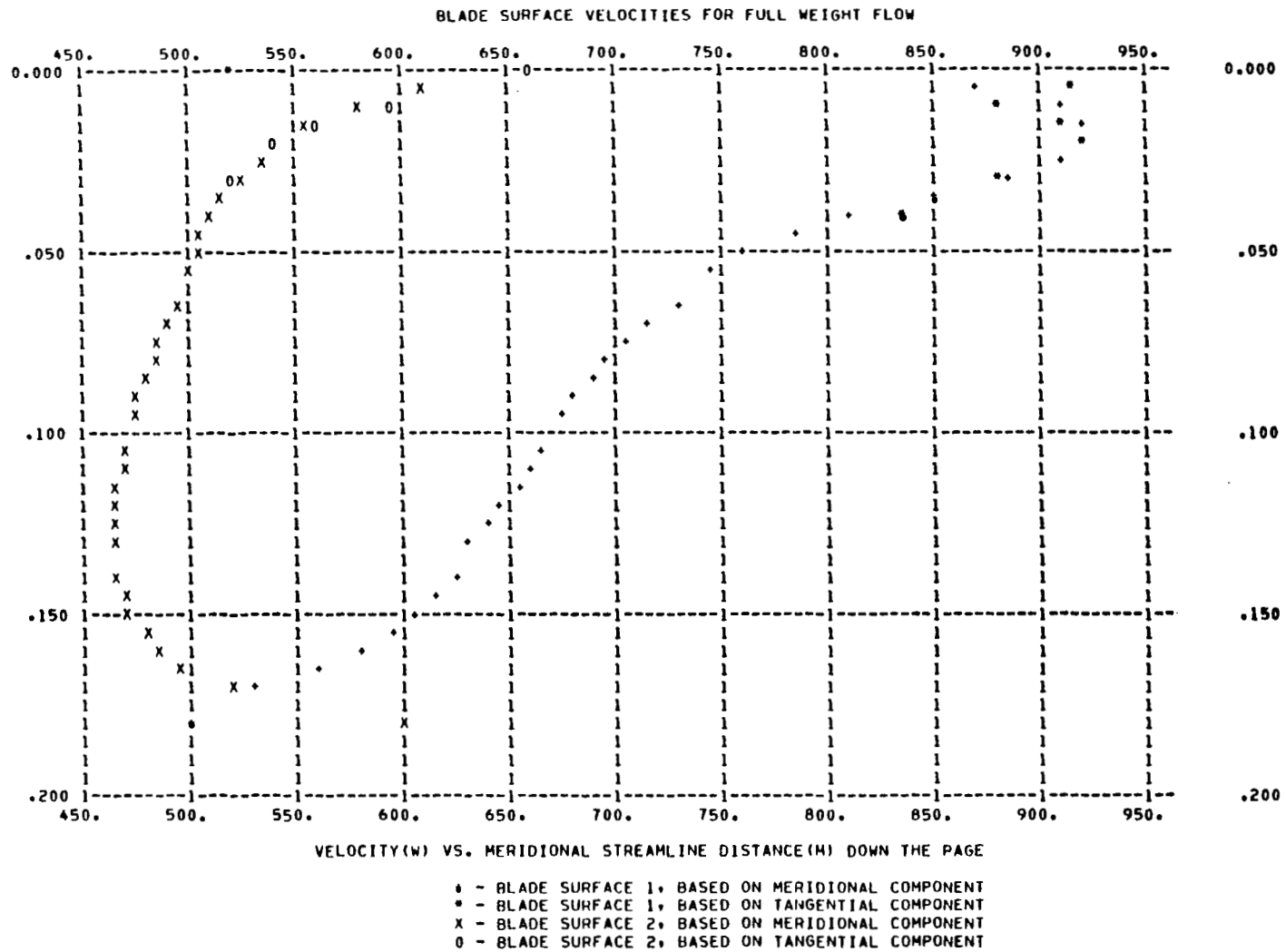


Figure A.2.- Continued.

BLADE SURFACE PRESSURES FOR FULL WEIGHT FLOW

IM	M	M/HC	PSI/PT	PI(2)PI	CPI(1)	CPT(2)
24	0.	0.	.9994	.9994	-.6204E-03	-.6204E-03
25	.5730E-02	.3125E-01	.6762	.8298	-.3238	-.1702
26	.1146E-01	.6250E-01	.6509	.8432	-.3491	-.1568
27	.1719E-01	.9375E-01	.6433	.8541	-.3567	-.1459
28	.2292E-01	.1250	.6479	.8610	-.3521	-.1390
29	.2865E-01	.1563	.6631	.8650	-.3369	-.1350
30	.3438E-01	.1875	.6847	.8680	-.3153	-.1320
31	.4011E-01	.2188	.7073	.8695	-.2927	-.1305
32	.4584E-01	.2500	.7238	.8699	-.2762	-.1301
33	.5157E-01	.2813	.7363	.8706	-.2637	-.1294
34	.5730E-01	.3125	.7450	.8713	-.2550	-.1287
35	.6303E-01	.3438	.7531	.8724	-.2469	-.1276
36	.6876E-01	.3750	.7585	.8726	-.2415	-.1274
37	.7449E-01	.4063	.7630	.8729	-.2370	-.1271
38	.8022E-01	.4375	.7676	.8721	-.2324	-.1279
39	.8595E-01	.4688	.7695	.8708	-.2305	-.1292
40	.9168E-01	.5000	.7711	.8700	-.2289	-.1300
41	.9741E-01	.5313	.7736	.8688	-.2264	-.1312
42	.1031	.5625	.7755	.8682	-.2245	-.1318
43	.1089	.5938	.7781	.8682	-.2219	-.1318
44	.1146	.6250	.7813	.8688	-.2187	-.1312
45	.1203	.6563	.7845	.8691	-.2155	-.1309
46	.1261	.6875	.7877	.8687	-.2123	-.1313
47	.1318	.7188	.7905	.8677	-.2095	-.1323
48	.1375	.7500	.7932	.8660	-.2068	-.1340
49	.1432	.7813	.7961	.8635	-.2039	-.1365
50	.1490	.8125	.7995	.8603	-.2005	-.1397
51	.1547	.8438	.8038	.8563	-.1962	-.1437
52	.1604	.8750	.8099	.8516	-.1901	-.1484
53	.1662	.9062	.8182	.8455	-.1818	-.1545
54	.1719	.9375	.8287	.8336	-.1713	-.1664
55	.1776	.9688	.8420	.7969	-.1580	-.2031
56	.1834	1.000	.9521	.9521	-.4788E-01	-.4788E-01

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

598.622	521.326	496.430	485.191	477.892
472.296	468.296	465.933	464.826	464.715
465.422	467.225	469.987	472.202	474.379
476.622	480.225	482.606	485.388	489.992
493.694	499.052	503.092	507.060	510.120

Figure A.2.- Continued.

515.956	525.246	536.981	554.624	579.933
608.917	871.309	908.986	918.846	910.016
884.741	849.202	811.259	782.794	760.231
743.855	728.095	716.532	706.124	694.759
687.633	680.982	672.940	666.912	660.502
653.560	646.538	639.326	632.201	624.598
616.196	606.488	594.393	578.629	557.971
532.289	499.834			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.91885E+03
	WO	=	.49944E+03
	DIFFS/WO	=	.18398E+01
CONSTRAINT 1	BLTKS	=	.66766E+00
CONSTRAINT 2	YMAX	=	.60892E+03
	YMIN	=	.46472E+03
	DIFFP	=	.13103E+01
CONSTRAINT 3	WMB(MBO-2.1)	=	.53229E+03
	WMB(MBO-2.2)	=	.52133E+03
	TECLSR	=	.13704E+00

FINAL OPTIMIZATION INFORMATION

OBJ = .170765E+01

DECISION VARIABLES (X-VECTOR)

1) -.93094E+01 .29650E+00 .55000E+00 .95806E+00 .32891E-01 .51525E-02

CONSTRAINT VALUES (G-VECTOR)

1) -.28002E+01 -.97200E+00 -.14455E+02 -.96575E-01 -.15965E+01 -.40346E+00

THERE ARE 1 ACTIVE CONSTRAINTS
CONSTRAINT NUMBERS ARE

4

THERE ARE 0 VIOLATED CONSTRAINTS

THERE ARE 1 ACTIVE SIDE CONSTRAINTS
DECISION VARIABLES AT LOWER OR UPPER BOUNDS (MINUS INDICATES LOWER BOUND)

3

TERMINATION CRITERION
ITER EQUALS ITMAX

NUMBER OF ITERATIONS = 1

OBJECTIVE FUNCTION WAS EVALUATED 12 TIMES

CONSTRAINT FUNCTIONS WERE EVALUATED 12 TIMES

OPTIMIZATION RESULTS

OBJECTIVE FUNCTION
 GLOBAL LOCATION 1 FUNCTION VALUE .17077E+01

DESIGN VARIABLES

ID	D. V. NO.	GLOBAL VAR. NO.	LOWER BOUND	VALUE	UPPER BOUND
1	1	2	-.15000E+02	-.93094E+01	0.
2	2	3	.20000E+00	.29650E+00	.60000E+00
3	3	4	.20000E+00	.55000E+00	.55000E+00
4	4	5	.50000E+00	.95806E+00	.40000E+01
5	5	6	.30000E-01	.32891E-01	.10000E+00
6	6	7	.30000E-02	.51525E-02	.12000E-01

DESIGN CONSTRAINTS

ID	GLOBAL VAR. NO.	LOWER BOUND	VALUE	UPPER BOUND
1	8	0.	.28002E+00	.10000E+02
3	9	0.	.14455E+01	.16000E+01
5	10	-.10000E+01	.59654E+00	.10000E+01

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-9.3094	.29650	.55000	.95806	.03289	.00515	.00500

Figure A.2.- Continued.

--- INPUT FOR TSONIC BLADE-TO-BLADE FLOW SOLVER ---

GAM	AR	TIP	RHOIP	WTFL	OMEGA	ORF		
1.400000	1716.480	599.7600	.3345860E-02	.5700000E-02	0.	1.910000		
BETAI	BETA0	CHORDF	STGRF	FSMI	FSMO			
48.20000	0.	.1795132	.1534563	0.	0.			
REDFAC	DENTOL	SSM1	SSM2					
1.000000	.1000000E-02	0.	0.					
MBI	MBO	MM	NBRI	NBL	NRSP	MOPT	LOPT	LRVB
24	56	0	0	72	15	34	13	0
							1	0
BLADE SURFACE 1 -- UPPER SURFACE								
R11	R01	BET11	BET01	SPLN01				
.9958413E-03	.9663591E-03	53.17187	-11.06885	13.00000				
MSP1 ARRAY								
.1988241E-03	.6491482E-02	.1596615E-01	.2768746E-01	.4356364E-01	.6073413E-01	.7906837E-01	.9830693E-01	
.1181776	.1383991	.1546368	.1687631	.1787495				
THSP1 ARRAY								
.1314862E-02	.1885167E-01	.4212224E-01	.6675356E-01	.9436997E-01	.1178990	.1367454	.1506814	
.1595550	.1632900	.1625744	.1592733	.1554091				
BLADE SURFACE 2 -- LOWER SURFACE								
R12	R02	BET12	BET02	SPLN02				
.9958413E-03	.9663591E-03	50.81841	-5.477123	13.00000				
MSP2 ARRAY								
.1767866E-02	.8225985E-02	.1791505E-01	.2985114E-01	.4593955E-01	.6312073E-01	.8117985E-01	.9994522E-01	
.1192385	.1388764	.1547094	.1685705	.1784377				
THSP2 ARRAY								
-.1385046E-02	.1513937E-01	.3691847E-01	.5973983E-01	.8493909E-01	.1063483	.1239432	.1375884	
.1471895	.1526932	.1541361	.1532488	.1513964				
MR ARRAY								
-.1300000	-.5000000E-02	.5000000E-02	.2003000E-01	.4003000E-01	.8003000E-01	.1000300	.1250300	
.1500400	.1752600	.1852600	.2250000	.2700000				
RMSP ARRAY								
.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	
.4540000	.4540000	.4540000	.4540000	.4540000				
BESP ARRAY								
.5000000E-01	.5000000E-01	.4990000E-01	.4960000E-01	.4925000E-01	.4850000E-01	.4815000E-01	.4770000E-01	
.4720000E-01	.4675000E-01	.4661000E-01	.4661000E-01	.4661000E-01				
PLOSS ARRAY								
0.	0.	.1500000E-02	.5900000E-02	.1100000E-01	.2150000E-01	.3000000E-01	.3350000E-01	
.4000000E-01	.4700000E-01	.4800000E-01	.4800000E-01	.4800000E-01				
BLDAT	AANDK	ERSOR	STRFN	SLCRD	INTVL	SURVL		
0	0	0	0	0	0	1		

Figure A.2.- Continued.

RELATIVE VELOCITY	MERIDIONAL VELOCITY	CRITICAL VELOCITY	REL. FLOW ANGLE
AT M = FSMI	AT M = FSMI	AT M = FSMI	AT UPSTREAM BDY.
745.90	497.17	1095.9	48.257
AT M = FSMO	AT M = FSMO	AT M = FSMO	AT DOWNSTREAM BDY.
498.55	498.55	1095.9	0.

FSMI = 0.
FSMO = .17951

CALCULATED PROGRAM CONSTANTS

PITCH	HT	HM1
.1847996	.1231997E-01	.5609788E-02
ITMIN	ITMAX	
0	27	
LAMBDA	DOWNSTREAM WHIRL (RVTHO)	
252.4466	0.	
REDUCED WEIGHT FLOW =	.5700000E-02	
NUMBER OF INTERIOR MESH POINTS =	1046	

CALCULATED VELOCITY DIAGRAM INFORMATION

	IM	W	W/WCR	BETA
UPSTREAM BOUNDARY	1	745.23	.68000	48.257
LEADING EDGE	24	745.90	.68061	48.200
TRAILING EDGE	56	498.55	.45491	0.
DOWNSTREAM BOUNDARY	72	499.77	.45602	0.

Figure A.2.- Continued.

ITERATION NO. 1	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1837	AT IM = 0,	IT = 4,	SURF = 1,	M = .1918E-01
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1045				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 90				
ITERATION NO. 2	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .7501E-01	AT IM = 0,	IT = 1,	SURF = 1,	M = .4069E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2483E-01				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 90				
ITERATION NO. 3	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3724E-01	AT IM = 0,	IT = 1,	SURF = 1,	M = .4069E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .7438E-02				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 89				
ITERATION NO. 4	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1933E-01	AT IM = 0,	IT = 1,	SURF = 1,	M = .4069E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2531E-02				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 49				
ITERATION NO. 5	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1019E-01	AT IM = 0,	IT = 1,	SURF = 1,	M = .4069E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .9376E-03				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 22				
ITERATION NO. 6	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .5275E-02	AT IM = 0,	IT = 1,	SURF = 1,	M = .4069E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3679E-03				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 14				
ITERATION NO. 7	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3104E-02	AT IM = 0,	IT = 1,	SURF = 1,	M = .4069E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1662E-03				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1				
ITERATION NO. 8	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1306E-02	AT IM = 0,	IT = 1,	SURF = 1,	M = .4069E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .5430E-04				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1				
ITERATION NO. 9	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .6819E-03	AT IM = 0,	IT = 1,	SURF = 1,	M = .4069E-02

Figure A.2.- Continued.

AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2643E-04
NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 0

ITERATION NO. 10
MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3138E-03 AT IM = 0, IT = 1, SURF = 1, M = .4069E-02
AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2102E-04
NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 0

SURFACE VELOCITIES BASED ON MERIDIONAL COMPONENTS - REDUCED WEIGHT FLOW																	
M	VELOCITY	BLADE SURFACE 1			W/WCR	VELOCITY	BLADE SURFACE 2			W/WCR							
		ANGLE (DEG)	SURF. LENGTH				ANGLE (DEG)	SURF. LENGTH									
0.	0.	90.00	0.	0.	0.	-90.00	0.	0.	0.	0.							
.5610E-02	* 836.7	50.59	.9360E-02	.7635	* 632.9	48.96	.6851E-02	.5775	* 848.1	48.08	.1797E-01	.7739	* 599.0	46.37	.1518E-01	.5466	
.1122E-01	* 851.3	45.66	.2618E-01	.7768	* 564.0	43.89	.2313E-01	.5147	* 1683E-01	43.35	.3404E-01	.7721	* 540.8	41.52	.3077E-01	.4935	
.2244E-01	* 846.2	41.16	.4162E-01	.7615	* 522.7	39.21	.3813E-01	.4769	* 2805E-01	39.02	.4895E-01	.7485	* 508.1	36.98	.4526E-01	.4636	
.3366E-01	* 820.3	36.85	.5607E-01	.7347	* 496.1	34.83	.5218E-01	.4527	* 3366E-01	36.85	.5607E-01	.7347	* 496.1	34.83	.5218E-01	.4527	
.3927E-01	* 805.2	34.68	.6298E-01	.7197	* 487.9	32.77	.5893E-01	.4452	* 4488E-01	34.68	.6298E-01	.7197	* 487.9	32.77	.5893E-01	.4452	
.4488E-01	* 770.7	32.50	.6972E-01	.7032	* 479.5	30.82	.6553E-01	.4375	* 5049E-01	32.50	.6972E-01	.7032	* 479.5	30.82	.6553E-01	.4375	
.5049E-01	* 754.2	30.30	.7629E-01	.6882	* 473.5	28.92	.7200E-01	.4320	* 5610E-01	30.30	.7629E-01	.6882	* 473.5	28.92	.7200E-01	.4320	
.5610E-01	* 739.3	28.11	.8272E-01	.6745	* 467.1	27.10	.7835E-01	.4263	* 6171E-01	28.11	.8272E-01	.6745	* 467.1	27.10	.7835E-01	.4263	
.6171E-01	* 723.5	25.94	.8901E-01	.6602	* 462.5	25.34	.8461E-01	.4220	* 6732E-01	25.94	.8901E-01	.6602	* 462.5	25.34	.8461E-01	.4220	
.6732E-01	* 710.8	23.83	.9520E-01	.6486	* 457.2	23.59	.9077E-01	.4172	* 7293E-01	23.83	.9520E-01	.6486	* 457.2	23.59	.9077E-01	.4172	
.7293E-01	* 697.6	21.78	.1013	.6365	* 453.8	21.87	.9685E-01	.4141	* 7854E-01	21.78	.1013	.6365	* 453.8	21.87	.9685E-01	.4141	
.7854E-01	* 688.8	19.78	.1073	.6285	* 449.7	20.17	.1029	.4104	* 8415E-01	19.78	.1073	.6285	* 449.7	20.17	.1029	.4104	
.8415E-01	* 680.9	17.80	.1132	.6213	* 447.5	18.48	.1088	.4083	* 8976E-01	17.80	.1132	.6213	* 447.5	18.48	.1088	.4083	
.8976E-01	* 671.6	15.84	.1191	.6128	* 445.6	16.82	.1147	.4066	* 9537E-01	15.84	.1191	.6128	* 445.6	16.82	.1147	.4066	
.9537E-01	* 665.3	13.91	.1249	.6070	* 442.6	15.19	.1205	.4039	* 1010	13.91	.1249	.6070	* 442.6	15.19	.1205	.4039	
.1010	* 658.7	12.00	.1306	.6011	* 441.0	13.57	.1263	.4024	* 1066	12.00	.1306	.6011	* 441.0	13.57	.1263	.4024	
.1066	* 652.0	10.10	.1363	.5949	* 439.8	11.97	.1321	.4013	* 1122	10.10	.1363	.5949	* 439.8	11.97	.1321	.4013	
.1122	* 645.0	8.23	.1420	.5885	* 439.2	10.39	.1378	.4007	* 1178	8.23	.1420	.5885	* 439.2	10.39	.1378	.4007	
.1178	* 635.7	6.38	.1477	.5801	* 437.8	8.82	.1435	.3995	* 1234	6.38	.1477	.5801	* 437.8	8.82	.1435	.3995	
.1234	* 629.3	4.54	.1533	.5742	* 438.7	7.25	.1491	.4003	* 1290	4.54	.1533	.5742	* 438.7	7.25	.1491	.4003	
.1290	* 622.6	2.71	.1589	.5681	* 440.7	5.69	.1548	.4021	* 1346	2.71	.1589	.5681	* 440.7	5.69	.1548	.4021	
.1346	* 615.5	.90	.1646	.5616	* 444.0	4.12	.1604	.4052	* 1402	.90	.1646	.5616	* 444.0	4.12	.1604	.4052	
.1402	* 607.4	-.92	.1702	.5542	* 449.0	2.60	.1660	.4097	* 1459	-.92	.1702	.5542	* 449.0	2.60	.1660	.4097	
.1459	* 597.2	-2.76	.1758	.5450	* 455.5	1.13	.1717	.4156	* 1515	-2.76	.1758	.5450	* 455.5	1.13	.1717	.4156	
.1515	* 584.1	-4.61	.1814	.5330	* 463.5	-.29	.1773	.4230	* 1571	-4.61	.1814	.5330	* 463.5	-.29	.1773	.4230	
.1571	* 567.1	-6.38	.1870	.5175	* 475.4	-1.92	.1829	.4338	* 1627	-6.38	.1870	.5175	* 475.4	-1.92	.1829	.4338	
.1627	* 548.2	-8.06	.1927	.5003	* 500.5	-3.80	.1885	.4567	* 1683	-8.06	.1927	.5003	* 500.5	-3.80	.1885	.4567	
.1683	* 533.5	-9.68	.1984	.4868	* 585.9	-5.24	.1941	.5347	* 1739	-9.68	.1984	.4868	* 585.9	-5.24	.1941	.5347	
.1739	* 0.	-90.00	.2043	0.	* 0.	90.00	.1998	0.	* 1795	0.	-90.00	.2043	* 0.	90.00	.1998	0.	
.1795																	

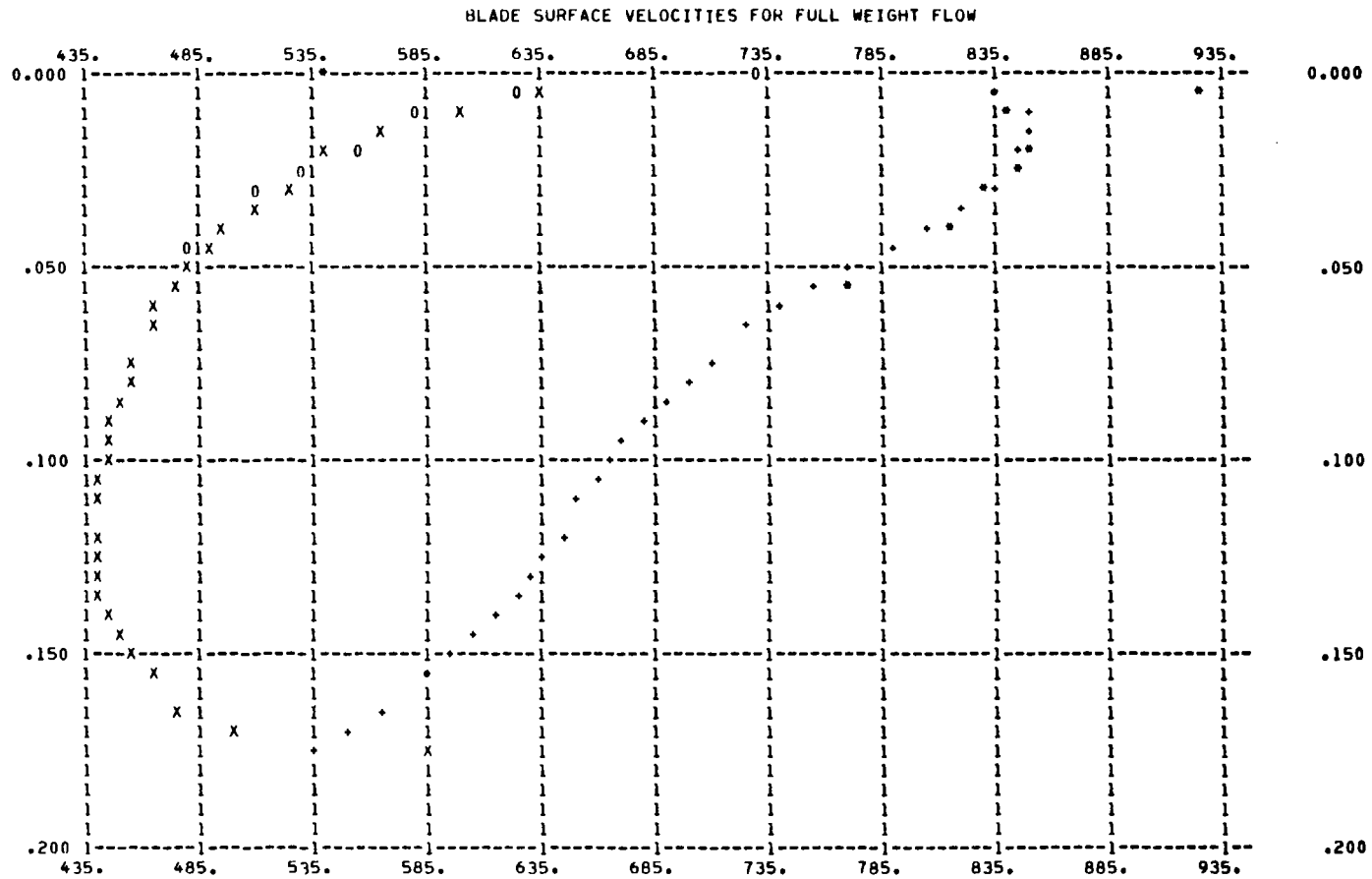
Figure A.2.- Continued.

SURFACE VELOCITIES BASED ON TANGENTIAL COMPONENTS
REDUCED WEIGHT FLOW

BLADE SURFACE 1			
M	VELOCITY	ANGLE (DEG)	W/WCR
0.	538.5	90.00	.4913
.4069E-02	923.1	51.31	.8423
.8721E-02	838.6	49.19	.7652
.1374E-01	850.8	46.98	.7763
.1918E-01	851.5	44.69	.7770
.2507E-01	844.3	42.31	.7704
.3149E-01	831.4	39.85	.7587
.3852E-01	815.4	37.15	.7440
.4631E-01	787.7	34.13	.7188
.5512E-01	768.0	30.68	.7008
.6534E-01	738.9	26.70	.6742
.7768E-01	713.0	22.08	.6506
.9369E-01	687.7	16.42	.6275
.1202	656.6	7.45	.5992
.1658	603.2	-7.33	.5504

BLADE SURFACE 2			
M	VELOCITY	ANGLE (DEG)	W/WCR
.2283E-02	729.0	50.57	.6652
.7074E-02	624.6	48.27	.5700
.1227E-01	581.7	45.90	.5308
.1793E-01	552.8	43.42	.5044
.2412E-01	530.1	40.82	.4837
.3092E-01	511.6	38.06	.4669
.3845E-01	496.7	35.13	.4532
.4688E-01	481.2	32.07	.4390
.5639E-01	467.9	28.82	.4270
.6734E-01	456.7	25.33	.4167
.8031E-01	447.8	21.33	.4086
.9666E-01	438.6	16.44	.4003
.1210	432.7	9.51	.3948

Figure A.2.- Continued.



VELOCITY (W) VS. MERIDIONAL STREAMLINE DISTANCE (M) DOWN THE PAGE

- - BLADE SURFACE 1, BASED ON MERIDIONAL COMPONENT
- - BLADE SURFACE 1, BASED ON TANGENTIAL COMPONENT
- X - BLADE SURFACE 2, BASED ON MERIDIONAL COMPONENT
- 0 - BLADE SURFACE 2, BASED ON TANGENTIAL COMPONENT

Figure A.2.- Continued.

BLADE SURFACE PRESSURES FOR FULL WEIGHT FLOW

IM	M	M/MC	P(1)/PT	P(2)/PT	CPT(1)	CPT(2)
24	0.	0.	.9994	.9994	-.6204E-03	-.6204E-03
25	.5610F-02	.3175E-01	.6981	.8173	-.3019	-.1827
26	.1122F-01	.6250E-01	.6899	.8337	-.3101	-.1663
27	.1683F-01	.9375E-01	.6867	.8496	-.3133	-.1504
28	.2244F-01	.1250	.6887	.8593	-.3113	-.1407
29	.2805E-01	.1563	.6949	.8663	-.3051	-.1337
30	.3366E-01	.1875	.7028	.8717	-.2972	-.1283
31	.3927E-01	.2188	.7111	.8759	-.2889	-.1241
32	.4488E-01	.2500	.7203	.8784	-.2797	-.1216
33	.5049E-01	.2813	.7303	.8810	-.2697	-.1190
34	.5610E-01	.3125	.7392	.8825	-.2608	-.1175
35	.6171E-01	.3438	.7469	.8839	-.2531	-.1161
36	.6732E-01	.3750	.7549	.8845	-.2451	-.1155
37	.7293F-01	.4063	.7608	.8851	-.2392	-.1149
38	.7854E-01	.4375	.7666	.8846	-.2334	-.1154
39	.8415E-01	.4688	.7695	.8840	-.2305	-.1160
40	.8976E-01	.5000	.7718	.8826	-.2282	-.1174
41	.9537E-01	.5313	.7749	.8811	-.2251	-.1189
42	.1010	.5625	.7768	.8806	-.2232	-.1194
43	.1066	.5938	.7793	.8801	-.2207	-.1199
44	.1122	.6250	.7823	.8799	-.2177	-.1201
45	.1178	.6563	.7855	.8797	-.2145	-.1203
46	.1234	.6875	.7899	.8797	-.2101	-.1203
47	.1290	.7188	.7925	.8785	-.2075	-.1215
48	.1346	.7500	.7949	.8766	-.2051	-.1234
49	.1402	.7813	.7972	.8740	-.2028	-.1260
50	.1459	.8125	.7999	.8705	-.2001	-.1295
51	.1515	.8437	.8033	.8663	-.1967	-.1337
52	.1571	.8750	.8082	.8614	-.1918	-.1386
53	.1627	.9062	.8148	.8551	-.1852	-.1449
54	.1683	.9375	.8222	.8433	-.1778	-.1567
55	.1739	.9687	.8278	.8035	-.1722	-.1965
56	.1795	1.000	.9525	.9525	-.4755E-01	-.4755E-01

Figure A.2.- Continued.

RESULTS OF COMPUTATIONS ON BASE SOLUTION:

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.....MACH NUMBER,
VALUES OF PERTURBATION PARAMETERS,
CRITICAL VALUE OF WM:

M0 = .1000
 Q0(1) = -9.3094 (KOCR)
 Q0(2) = .2965 (T)
 Q0(3) = .5500 (ZM)
 Q0(4) = .9581 (P)
 Q0(5) = .0329 (THX)
 Q0(6) = .0052 (THLE)
 WMCRT = -66.8587

.....LOCATIONS OF MIN., MAX., AND CRITICAL PTS.
(* DENOTES POINT ON LOWER SURFACE)

MINIMUM AT X = .6875* (POINT NO. 10)
 MAXIMUM AT X = .0937 (POINT NO. 34)

.....LOCATION OF FIXED POINTS
(* DENOTES POINT ON LOWER SURFACE)

XFIX(1) = 1.0000*
 XFIX(2) = .0937
 XFIX(3) = 1.0000

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

585.946	500.526	475.384	463.538	455.453
448.954	444.034	440.692	438.692	437.817

Figure A.2.- Continued.

439.170	439.833	441.032	442.598	445.557
447.463	449.745	453.791	457.230	462.531
467.147	473.460	479.521	487.914	496.105
508.106	522.699	540.850	564.034	599.017
632.856	836.747	848.134	851.345	846.151
834.503	820.308	805.229	788.747	770.703
754.190	739.256	723.486	710.818	697.563
688.798	680.850	671.634	665.267	658.725
651.996	644.996	635.734	629.278	622.630
615.503	607.355	597.245	584.097	567.118
548.249	533.506			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.85135E+03
	WO	=	.49855E+03
	DIFFS/WO	=	.17077E+01
CONSTRAINT 1	BLTKS	=	.28002E+00
CONSTRAINT 2	YMAX	=	.63286E+03
	YMIN	=	.43782E+03
	DIFFP	=	.14455E+01
CONSTRAINT 3	WMB(M80-2,1)	=	.54825E+03
	WMB(M80-2,2)	=	.50053E+03
	TECLSR	=	.59654E+00

UNIT PERTURBATION OF WM AND UNIT STRAINING OF XBASE
FOR CALIBRATION SOLUTIONS 1 THROUGH 5

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POINT	XBASE	* 1ST CALB SOLN *		* 2ND CALB SOLN *		* 3RD CALB SOLN *		* 4TH CALB SOLN *		* 5TH CALB SOLN *	
		XSTRUNIT	WMUNIT	XSTRUNIT	WMUNIT	XSTRUNIT	WMUNIT	XSTRUNIT	WMUNIT	XSTRUNIT	WMUNIT
1	.9687	.9687	-20.0835	.9687	-12.3557	.9687	.7336	.9679	49.8051	.9687	-134.3581
2	.9375	.9375	-2.0339	.9375	.3504	.9375	22.0747	.9357	31.4676	.9375	321.5647
3	.9062	.9062	-1.5704	.9062	-1.8310	.9062	32.2313	.9036	32.5262	.9062	553.3391
4	.8750	.8750	-1.1541	.8750	-2.8760	.8750	39.4171	.8714	33.1910	.8750	730.8362
5	.8437	.8437	-.5654	.8437	-3.2252	.8437	44.4573	.8393	33.0680	.8437	869.5636
6	.8125	.8125	-.0083	.8125	-3.2979	.8125	47.7861	.8071	32.3865	.8125	982.7536
7	.7813	.7813	.4519	.7813	-3.2944	.7813	49.9671	.7750	31.2294	.7813	1083.0267
8	.7500	.7500	.8409	.7500	-3.2652	.7500	51.3220	.7429	29.7367	.7500	1177.6278
9	.7188	.7188	1.1920	.7188	-3.1984	.7188	51.9009	.7107	27.8109	.7188	1266.5219
10	.6875	.6875	1.5444	.6875	-3.0260	.6875	51.5705	.6786	24.0298	.6875	1346.7744
11	.6563	.6563	1.7105	.6563	-2.7491	.6563	50.4412	.6464	22.6987	.6563	1436.6945
12	.6250	.6250	1.9518	.6250	-2.5167	.6250	48.7109	.6143	20.1833	.6250	1513.6100
13	.5938	.5938	2.1692	.5938	-2.2244	.5938	45.8657	.5821	17.5319	.5938	1584.0968
14	.5625	.5625	2.3808	.5625	-1.8467	.5625	41.5757	.5500	12.3536	.5625	1644.2614
15	.5313	.5313	2.4946	.5313	-1.4206	.5313	34.7531	.5179	9.6214	.5313	1711.4227
16	.5000	.5000	2.6598	.5000	-.9420	.5000	27.1473	.4857	4.7197	.5000	1760.2479
17	.4688	.4688	2.8328	.4688	-.3770	.4688	18.3364	.4536	-3.8576	.4688	1797.3748
18	.4375	.4375	2.9307	.4375	.3384	.4375	8.5195	.4214	-8.7994	.4375	1849.8007
19	.4063	.4063	2.8725	.4063	1.1044	.4063	-2.1194	.3893	-19.8105	.4063	1905.3349
20	.3750	.3750	-1.1870	.3750	1.6390	.3750	-18.8717	.3571	-28.8464	.3750	2411.8914
21	.3438	.3438	3.4304	.3438	1.2143	.3438	-42.9978	.3250	-49.4112	.3438	1914.4488
22	.3125	.3125	3.4417	.3125	-.2424	.3125	-82.2106	.2929	-73.9244	.3125	2377.3086
23	.2813	.2813	3.5360	.2813	1.7374	.2813	-121.3626	.2607	-100.9777	.2813	1799.7259
24	.2500	.2500	3.5962	.2500	11.6855	.2500	-170.1902	.2286	-129.5244	.2500	1750.2485
25	.2188	.2188	3.6615	.2188	28.8759	.2188	-213.2488	.1964	-168.5015	.2188	1673.8101
26	.1875	.1875	3.7119	.1875	49.8522	.1875	-259.9132	.1643	-199.0200	.1875	1603.4360
27	.1563	.1563	3.7645	.1563	63.6612	.1563	-294.5792	.1321	-227.0555	.1563	1542.7842
28	.1250	.1250	3.8190	.1250	67.6203	.1250	-314.5814	.1000	-256.8217	.1250	1493.5615
29	.0938	.0938	3.8704	.0938	67.8533	.0938	-323.8562	.0679	-313.1910	.0938	1439.4028
30	.0625	.0625	4.0452	.0625	64.1781	.0625	-318.0546	.0357	-301.6170	.0625	1395.2751
31	.0313	.0313	3.7273	.0313	59.1752	.0313	-306.1475	.0036	-390.5942	.0313	1315.1689
32	.0313	.0313	-2.0986	.0313	20.0463	.0313	38.5597	.0607	53.0857	.0313	-774.5666
33	.0625	.0625	-1.7847	.0625	59.1447	.0625	-147.0558	.0929	55.9563	.0625	-245.9485
34	.0937	.0937	-1.3110	.0937	75.5428	.0937	-243.1517	.1250	57.6540	.0937	128.3677
35	.1250	.1250	-.7343	.1250	86.0979	.1250	-298.0271	.1552	44.6364	.1250	439.0277
36	.1563	.1563	-.0684	.1563	76.0690	.1563	-316.0947	.1853	6.7466	.1563	734.5830
37	.1875	.1875	.5535	.1875	25.7422	.1875	-294.0541	.2155	-32.6152	.1875	1034.5656
38	.2188	.2188	1.0858	.2188	-37.4853	.2188	-251.8086	.2457	-67.3864	.2188	1319.4035
39	.2500	.2500	1.4408	.2500	-54.6629	.2500	-211.5466	.2759	-90.1078	.2500	1533.4164
40	.2813	.2813	1.6988	.2813	-40.9663	.2813	-164.2406	.3060	-107.1067	.2813	1716.9271
41	.3125	.3125	1.8322	.3125	-7.2238	.3125	-120.1525	.3362	-113.3012	.3125	1866.5859
42	.3438	.3438	1.8675	.3438	12.3028	.3438	-91.4976	.3664	-110.1136	.3438	1949.5734
43	.3750	.3750	1.8318	.3750	18.5201	.3750	-70.0210	.3966	-104.1926	.3750	1996.9997
44	.4063	.4063	1.7831	.4063	17.1651	.4063	-55.8055	.4267	-94.5723	.4063	2021.0725
45	.4375	.4375	1.6282	.4375	13.5137	.4375	-42.1093	.4569	-91.3018	.4375	2006.4598
46	.4688	.4688	1.4959	.4688	12.4504	.4688	-26.6607	.4871	-81.2246	.4688	2010.8281
47	.5000	.5000	1.4538	.5000	12.2531	.5000	-10.9074	.5172	-76.0135	.5000	2014.4030
48	.5313	.5313	1.2463	.5313	11.9896	.5313	4.2757	.5474	-72.4756	.5313	1961.1819
49	.5625	.5625	1.1544	.5625	11.4311	.5625	16.9513	.5776	-60.5096	.5625	1922.7421
50	.5938	.5938	1.0832	.5938	10.5534	.5938	27.4695	.6078	-54.5505	.5938	1865.9004
51	.6250	.6250	1.0269	.6250	9.3045	.6250	35.8149	.6379	-48.5193	.6250	1793.9780
52	.6563	.6563	1.4608	.6563	9.0808	.6563	43.1271	.6681	-40.0172	.6563	1744.0449
53	.6875	.6875	.9389	.6875	7.4211	.6875	45.2747	.6983	-39.3476	.6875	1578.7011
54	.7188	.7188	.9441	.7188	6.8230	.7188	48.1426	.7284	-35.3002	.7188	1464.1293

Figure A.2.- Continued.

55	.7500	.7500	1.0328	.7500	6.3076	.7500	49.1325	.7586	-31.5621	.7500	1334.1984
56	.7813	.7813	1.2671	.7813	5.8215	.7813	48.2877	.7888	-27.9952	.7813	1190.4777
57	.8125	.8125	1.6887	.8125	5.4206	.8125	45.5817	.8190	-24.4539	.8125	1030.4991
58	.8437	.8437	2.3181	.8437	5.0341	.8437	40.6758	.8491	-21.2165	.8437	846.5093
59	.8750	.8750	3.1611	.8750	4.5903	.8750	33.2001	.8793	-18.9875	.8750	630.1062
60	.9062	.9062	4.3495	.9062	3.9949	.9062	22.7723	.9095	-18.1252	.9062	376.1257
61	.9375	.9375	-0.8723	.9375	4.0444	.9375	9.3163	.9397	-13.9357	.9375	73.0336
62	.9687	.9687	24.4162	.9687	8.5940	.9687	-15.1745	.9698	-38.7317	.9687	-419.8816

Figure A.2.- Continued.

UNIT PERTURBATION OF WM AND UNIT STRAINING OF XBASE
FOR CALIBRATION SOLUTIONS 6 THROUGH 6

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POINT	XBASE	• 6TH CALB SOLN •	
		XSTRUNIT	WMUNIT
1	.9687	.9687	85.4341
2	.9375	.9375	-195.5425
3	.9062	.9062	-73.2089
4	.8750	.8750	-103.2774
5	.8437	.8437	-137.1931
6	.8125	.8125	-130.1613
7	.7813	.7813	-110.6727
8	.7500	.7500	-99.2898
9	.7188	.7188	-98.7822
10	.6875	.6875	-106.3977
11	.6563	.6563	-93.3852
12	.6250	.6250	-88.7640
13	.5938	.5938	-82.9426
14	.5625	.5625	-80.9244
15	.5313	.5313	-70.7242
16	.5000	.5000	-68.5586
17	.4688	.4688	-68.1042
18	.4375	.4375	-40.0619
19	.4063	.4063	-24.6671
20	.3750	.3750	-8.0421
21	.3438	.3438	-55.7364
22	.3125	.3125	-139.4742
23	.2813	.2813	-218.3122
24	.2500	.2500	-304.8216
25	.2188	.2188	-363.2004
26	.1875	.1875	-220.2327
27	.1563	.1563	179.5793
28	.1250	.1250	972.0918
29	.0938	.0938	2388.4336
30	.0625	.0625	6013.0030
31	.0313	.0313	10829.3858
32	.0313	.0313	4319.9999
33	.0625	.0625	974.4519
34	.0937	.0937	-336.1720
35	.1250	.1250	-849.5837
36	.1563	.1563	-863.6749
37	.1875	.1875	-370.0835
38	.2188	.2188	321.6473
39	.2500	.2500	678.9298
40	.2813	.2813	973.2190
41	.3125	.3125	1123.6623
42	.3438	.3438	1043.2128
43	.3750	.3750	941.1998
44	.4063	.4063	759.0115
45	.4375	.4375	621.9917
46	.4688	.4688	507.6942
47	.5000	.5000	403.4571
48	.5313	.5313	357.8155
49	.5625	.5625	304.2645
50	.5938	.5938	258.3880
51	.6250	.6250	218.0293
52	.6563	.6563	132.6033
53	.6875	.6875	150.2109
54	.7188	.7188	125.2795

Figure A.2.- Continued.

55	.7500	.7500	109.5129
56	.7813	.7813	108.1062
57	.8125	.8125	118.9669
58	.8437	.8437	116.0773
59	.8750	.8750	66.5779
60	.9062	.9062	1.4576
61	.9375	.9375	-18.1001
62	.9687	.9687	46.1274

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* * * * *
*           C O N M I N
*   FORTRAN PROGRAM FOR
*   CONSTRAINED FUNCTION MINIMIZATION
* * * * *

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CONSTRAINED FUNCTION MINIMIZATION

CONTROL PARAMETERS

IPRINT	NDV	ITMAX	NCON	NSIDE	ICNDR	NSCAL	NFDG		
5	6	6	6	1	7	-2	0		
LINOBJ	ITRM	N1	N2	N3	N4	N5			
0	3	8	18	20	20	40			
CT	CTMIN	CTL	CTLMIN						
-.10000E+00	.40000E-02	-.10000E-01	.10000E-02						
THETA	PHI	DELFUN	DABFUN						
.10000E+01	.50000E+01	.10000E-03	.17077E-02						
FDCH	FDCHM	ALPHAX	ABOBJ1						
.10000E-01	.10000E-02	.10000E+00	.50000E-01						
LOWER BOUNDS ON DECISION VARIABLES (VLB)									
1)	-.15000E+01	.80000E+00	.44444E+00	.33333E+00	.60000E+00	.60000E+00			
UPPER BOUNDS ON DECISION VARIABLES (VUB)									
1)	0.	.24000E+01	.12222E+01	.26667E+01	.20000E+01	.24000E+01			
SCALING VECTOR (SCAL)									
	.1000E+02	.2500E+00	.4500E+00	.1500E+01	.5000E-01	.5000E-02			
ALL CONSTRAINTS ARE NON-LINEAR									
INITIAL FUNCTION INFORMATION									
OBJ =	.170765E+01								
DECISION VARIABLES (X-VECTOR)									
1)	-.93094E+01	.29650E+00	.55000E+00	.95806E+00	.32891E-01	.51525E-02			
CONSTRAINT VALUES (G-VECTOR)									
1)	-.28002E+01	-.97200E+00	-.14455E+02	-.96575E-01	-.15965E+01	-.40346E+00			

Figure A.2.- Continued.

BEGIN ITERATION NUMBER 1
 CT = -.10000E+00 CTL = -.10000E-01 PHI = .50000E+01

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX. TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-9.2163	.29650	.55000	.95806	.03289	.00515	.00500

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

584.076	500.337	475.238	463.430	455.400
448.954	444.076	440.771	438.803	437.961
439.329	440.014	441.234	442.820	445.789
447.710	450.009	454.064	457.497	462.420
467.467	473.780	479.851	488.249	496.446
508.451	523.050	541.205	564.395	599.393
633.203	836.552	847.968	851.223	846.083
834.497	820.359	805.330	788.882	770.861
754.360	739.430	723.656	710.984	697.714
688.937	680.986	671.750	665.374	658.826
652.092	645.132	635.822	629.366	622.726
615.621	607.512	597.461	584.391	567.523
548.168	535.779			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.85122E+03
	WO	=	.49855E+03
	DIFFS/WO	=	.17074E+01
CONSTRAINT 1	BLTKS	=	.27996E+00
CONSTRAINT 2	YMAX	=	.63320E+03
	YMIN	=	.43796E+03
	DIFFP	=	.14458E+01
CONSTRAINT 3	WMB(MB0-2,1)	=	.54817E+03
	WMB(MB0-2,2)	=	.50034E+03

TECLSR = .59789E+00

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*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-9.3094	.29946	.55000	.95806	.03289	.00515	.00500

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

585.909	500.527	475.378	463.529	455.444
448.945	444.024	440.683	438.683	437.808
439.162	439.825	441.025	442.593	445.553
447.460	449.744	453.792	457.233	462.536
467.151	473.459	479.527	487.949	496.191
508.253	522.888	541.050	564.235	599.207
633.031	836.807	848.310	851.569	846.407
834.729	820.384	805.118	788.585	770.581
754.168	739.293	723.541	710.869	697.603
688.835	680.887	671.669	665.301	658.757
652.024	645.023	635.756	629.298	622.649
615.521	607.371	597.260	584.111	567.130
548.261	533.531			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION DIFFS = .85157E+03
 WO = .49855E+03
 DIFFS/WO = .17081E+01

CONSTRAINT 1 BLTKS = .28326E+00

CONSTRAINT 2 YMAX = .63303E+03
 YMIN = .43781E+03
 DIFFP = .14459E+01

CONSTRAINT 3 WMB(M80-2+1) = .54826E+03
 WMB(M80-2+2) = .50053E+03

Figure A.2.- Continued.

TECLSR = .59667E+00

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-9.3094	.29650	.54450	.95806	.03289	.00515	.00500
X ARRAY											
	.968750	.937500	.906250	.875000	.843750						
	.812500	.781250	.750000	.718750	.687500						
	.656250	.625000	.593750	.562500	.531250						
	.500000	.468750	.437500	.406250	.375000						
	.343750	.312500	.281250	.250000	.218750						
	.187500	.156250	.125000	.093750	.062500						
	.031250	.031250	.062500	.093750	.125000						
	.156250	.187500	.218750	.250000	.281250						
	.312500	.343750	.375000	.406250	.437500						
	.468750	.500000	.531250	.562500	.593750						
	.625000	.656250	.687500	.718750	.750000						
	.781250	.812500	.843750	.875000	.906250						
	.937500	.968750									
Y ARRAY											
	585.942	500.405	475.206	463.321	455.209						
	448.692	443.759	440.410	438.407	437.534						
	438.893	439.565	440.779	442.369	445.366						
	447.313	449.644	453.744	457.241	462.635						
	467.384	473.912	480.189	488.851	497.278						
	509.535	524.319	542.580	565.816	600.766						
	634.540	836.535	848.943	852.683	847.791						
	836.242	821.925	806.614	789.911	771.606						
	754.851	739.759	723.871	711.125	697.795						
	688.945	680.910	671.610	665.174	658.574						
	651.799	644.759	635.485	629.013	622.360						
	615.238	607.104	597.022	583.914	566.993						
	548.198	533.589									

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.85268E+03
	WO	=	.49855E+03
	DIFFS/WO	=	.17103E+01
CONSTRAINT 1	BLTKS	=	.30418E+00
CONSTRAINT 2	YMAX	=	.63454E+03
	YMIN	=	.43753E+03
	DIFFP	=	.14503E+01
CONSTRAINT 3	WMB(MBO-2+1)	=	.54820E+03
	WMB(MBO-2+2)	=	.50040E+03

Figure A.2.- Continued.

TECLSR = .59741E+00

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*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONF ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX. TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-9.3094	.29650	.55000	.96764	.03289	.00515	.00500

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

586.337	500.777	475.659	463.823	455.737
449.235	444.309	440.961	438.951	438.061
439.395	440.040	441.220	442.758	445.677
447.543	449.777	453.767	457.140	462.344
466.803	472.880	478.743	486.863	494.787
506.576	521.012	539.030	562.063	597.128
632.376	837.637	848.781	851.710	846.170
834.089	819.507	804.075	787.352	769.212
752.705	737.799	722.181	709.606	696.498
687.856	679.943	670.825	664.577	658.097
651.430	644.488	635.279	628.867	622.258
615.166	607.047	596.962	583.832	566.876
548.079	533.116			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.85171E+03
	WO	=	.49855E+03
	DIFFS/WO	=	.17084E+01
CONSTRAINT 1	BLTKS	=	.27981E+00
CONSTRAINT 2	YMAX	=	.63238E+03
	YMIN	=	.43806E+03
	DIFFP	=	.14436E+01
CONSTRAINT 3	WMB(MRO-2.1)	=	.54808E+03
	WMB(MRO-2.2)	=	.50078E+03

Figure A.2.- Continued.

TECLSR = .59128E+00

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-9.3094	.29650	.55000	.95806	.03389	.00515	.00500

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

585.812	500.848	475.937	464.269	456.323
449.937	445.117	441.870	439.959	439.164
440.607	441.346	442.616	444.242	447.268
449.223	451.543	455.641	459.135	464.943
469.062	475.837	481.321	489.665	497.779
509.709	524.242	542.343	565.474	600.412
634.171	835.973	847.888	851.474	846.590
835.238	821.342	806.548	790.281	772.420
756.056	741.206	725.483	712.839	699.569
690.809	682.865	673.595	667.190	660.591
653.790	646.740	637.313	630.742	623.964
616.694	608.385	598.092	584.727	567.494
548.322	533.086			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.85147E+03
	W0	=	.49855E+03
	DIFFS/W0	=	.17079E+01
CONSTRAINT 1	BLTKS	=	.29081E+00
CONSTRAINT 2	YMAX	=	.63417E+03
	YMIN	=	.43916E+03
	DIFFP	=	.14440E+01
CONSTRAINT 3	WMB(MB0-2,1)	=	.54832E+03
	WMB(MB0-2,2)	=	.50085E+03

Figure A.2.- Continued.

TECLSR = .593*3E+00

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*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-9.3094	.29650	.55000	.95806	.03289	.00615	.00500

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

586.031	500.331	475.311	463.435	455.316
448.824	443.923	440.593	438.594	437.711
439.077	439.744	440.949	442.517	445.486
447.394	449.677	453.751	457.205	462.523
467.092	473.320	479.303	487.610	495.742
507.885	522.879	541.822	566.423	605.030
643.685	841.067	849.109	851.009	845.302
833.639	819.938	805.551	789.426	771.676
755.314	740.299	724.427	711.577	698.185
689.306	681.254	671.991	665.571	658.984
652.214	645.128	635.885	629.403	622.739
615.612	607.474	597.362	584.164	567.120
548.231	533.552			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.85101E+03
	WO	=	.49855E+03
	DIFFS/WO	=	.17070E+01
CONSTRAINT 1	BLTKS	=	.42386E+00
CONSTRAINT 2	YMAX	=	.64369E+03
	YMIN	=	.43771E+03
	DIFFP	=	.14706E+01
CONSTRAINT 3	WMB (M80-2,1)	=	.54823E+03
	WMB (M80-2,2)	=	.50033E+03

Figure A.2.- Continued.

TECLSR = .59876E+00

THERE ARE 1 ACTIVE CONSTRAINTS
 CONSTRAINT NUMBERS ARE
 4

THERE ARE 0 VIOLATED CONSTRAINTS

THERE ARE 1 ACTIVE SIDE CONSTRAINTS
 DECISION VARIABLES AT LOWER OR UPPER BOUNDS (MINUS INDICATES LOWER BOUND)
 3

GRADIENT OF OBJ
 1) -.26392E-01 .37807E-01 -.21940E+00 .11434E+00 .12830E-01 -.33759E-02

GRADIENTS OF ACTIVE AND VIOLATED CONSTRAINTS
 CONSTRAINT NUMBER 4
 1) .21332E-01 .22680E-01 -.24471E+00 -.18588E+00 -.44941E-01 .78414E-01

SIDE CONSTRAINT ON VARIABLE 3
 1) 0. 0. .10000E+01 0. 0. 0.

PUSH-OFF FACTORS, (THETA(I), I=1,NAC)
 1) .11730E-02 0.

CONSTRAINT PARAMETER, BETA = .36299E+00

SEARCH DIRECTION (S-VECTOR)
 1) .32046E+00 -.10000E+01 .39056E-13 -.43887E+00 .19546E+00 -.72800E+00

ONE-DIMENSIONAL SEARCH
 INITIAL SLOPE = -.9148E-01 PROPOSED ALPHA = .1186E+00

• • CONSTRAINED ONE-DIMENSIONAL SEARCH INFORMATION • • •

PROPOSED DESIGN
 ALPHA = .11860E+00
 X-VECTOR
 -.8929E+01 .2668E+00 .5500E+00 .8800E+00 .3405E-01 .4721E-02

Figure A.2.- Continued.

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONF ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-8.9293	.26685	.55000	.87999	.03405	.00472	.00500

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

575.226	498.998	473.581	461.860	454.132
448.015	443.428	440.389	438.698	438.254
439.690	440.765	442.260	444.293	447.409
449.890	452.824	457.082	461.385	466.261
473.241	481.773	489.466	499.183	509.712
522.635	538.120	557.091	582.208	613.227
650.082	805.736	837.247	843.322	841.747
835.030	826.076	815.978	802.800	786.405
769.349	753.299	736.954	722.919	709.390
699.074	690.470	680.975	673.220	666.054
658.757	651.200	641.678	634.454	627.364
619.856	611.397	601.083	587.877	571.010
549.410	545.087			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.84332E+03
	WO	=	.49855E+03
	DIFFS/WO	=	.16916E+01
CONSTRAINT 1	BLTKS	=	.19679E+00
CONSTRAINT 2	YMAX	=	.65008E+03
	YMIN	=	.43825E+03
	DIFFP	=	.14833E+01
CONSTRAINT 3	WMB(M80-2.1)	=	.54941E+03
	WMB(M80-2.2)	=	.49900E+03

Figure A.2.- Continued.


```
TECLSR = .63015E+00
OBJ = .16916E+01
CONSTRAINT VALUES
-.1968E+01 -.9803E+00 -.1483E+02 -.7291E-01 -.1630E+01 -.3698E+00
TWO-POINT INTERPOLATION
PROPOSED DESIGN
ALPHA = .38598E+00
X-VECTOR
-.8072E+01 .2000E+00 .5500E+00 .7040E+00 .3666E-01 .3748E-02
```

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-8.0725	.20000	.55000	.70396	.03666	.00375	.00500

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

550.516	494.472	469.416	457.972	451.012
445.739	441.893	439.521	438.501	438.930
440.705	442.613	444.763	447.681	451.328
454.923	459.030	464.065	469.819	475.041
483.575	497.330	510.004	521.974	536.848
553.060	570.624	590.966	617.176	649.870
680.737	771.425	811.313	824.141	828.722
828.531	829.594	831.320	830.192	820.187
804.400	786.288	768.411	751.285	736.461
723.326	712.703	702.584	692.254	683.150
674.537	665.675	655.453	646.455	638.311
629.888	620.680	609.854	596.460	579.793
552.461	570.387			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.83132E+03
	WO	=	.49855E+03
	DIFFS/WO	=	.16675E+01
CONSTRAINT 1	BLTKS	=	-.15560E-01
CONSTRAINT 2	YMAX	=	.68074E+03
	YMIN	=	.43850E+03
	DIFFP	=	.15524E+01
CONSTRAINT 3	WMB(MBO-2.1)	=	.55246E+03
	WMB(MBO-2.2)	=	.49447E+03

TECLSR = .72486E+00
OBJ = .16675E+01
CONSTRAINT VALUES
.1556E+00 -.1002E+01 -.1552E+02 -.2974E-01 -.1725E+01 -.2751E+00
THREE-POINT INTERPOLATION
PROPOSED DESIGN
ALPHA = .34405E+00
X-VECTOR
-.8207E+01 .2105E+00 .5500E+00 .7316E+00 .3625E-01 .3900E-02

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-8.2069	.21048	.55000	.73157	.03625	.00390	.00500

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

554.440	495.278	470.079	458.591	451.514
446.110	442.149	439.674	438.551	438.852
440.560	442.346	444.394	447.189	450.736
454.173	458.122	463.009	468.580	473.631
482.259	495.175	506.951	518.634	532.909
548.497	565.728	585.899	612.229	643.711
676.661	773.620	815.504	827.247	831.057
830.276	829.937	829.753	826.301	815.041
798.820	780.988	763.374	746.734	732.177
719.420	709.164	699.143	689.165	680.415
672.011	663.358	653.257	644.542	636.568
628.294	619.208	608.467	595.108	578.415
551.941	566.495			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.83106E+03
	W0	=	.49855E+03
	DIFFS/W0	=	.16670E+01
CONSTRAINT 1	BLTKS	=	.20848E-01
CONSTRAINT 2	YMAX	=	.67666E+03
	YMIN	=	.43855E+03
	DIFFP	=	.15429E+01
CONSTRAINT 3	WMB(MB0-2,1)	=	.55194E+03
	WMB(MB0-2,2)	=	.49528E+03

Figure A.2.- Continued.

```

TECLSR = .70829E+00
OBJ = .16670E+01
CONSTRAINT VALUES
-.2085E+00 -.9979E+00 -.1543E+02 -.3566E-01 -.1708E+01 -.2917E+00
* * * END OF ONE-DIMENSIONAL SEARCH
CALCULATED ALPHA = .34405E+00
OBJ = .166695E+01
DECISION VARIABLES (X-VECTOR)
1) -.82069E+01 .21048E+00 .55000E+00 .73157E+00 .36253E-01 .39002E-02
CONSTRAINT VALUES (G-VECTOR)
1) -.20848E+00 -.99792E+00 -.15429E+02 -.35658E-01 -.17083E+01 -.29171E+00

BEGIN ITERATION NUMBER 2
CT = -.10000E+00 CTL = -.10000E-01 PHI = .50000E+01

```

Figure A.2.- Continued.

FINAL OPTIMIZATION INFORMATION

OBJ = .166529E+01

DECISION VARIABLES (X-VECTOR)

1) -.80297E+01 .20000E+00 .55000E+00 .73559E+00 .36263E-01 .39389E-02

CONSTRAINT VALUES (G-VECTOR)

1) -.44211E-01 -.99956E+00 -.15409E+02 -.36960E-01 -.17108E+01 -.28922E+00

THERE ARE 2 ACTIVE CONSTRAINTS

CONSTRAINT NUMBERS ARE

1 4

THERE ARE 0 VIOLATED CONSTRAINTS

THERE ARE 2 ACTIVE SIDE CONSTRAINTS

DECISION VARIABLES AT LOWER OR UPPER BOUNDS (MINUS INDICATES LOWER BOUND)

-2 3

TERMINATION CRITERION

ABS(OBJ(I))-OBJ(I-1)) LESS THAN DABFUN FOR 3 ITERATIONS

NUMBER OF ITERATIONS = 4

OBJECTIVE FUNCTION WAS EVALUATED 35 TIMES

CONSTRAINT FUNCTIONS WERE EVALUATED 35 TIMES

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONF ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX. TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-8.0297	.20000	.55000	.73559	.03626	.00394	.00500

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

Y ARRAY

551.119	494.850	469.915	458.527	451.557
446.251	442.372	439.964	438.901	439.254
440.997	442.810	444.888	447.705	451.267
454.707	458.662	463.548	469.088	473.693
482.427	495.670	507.322	518.886	532.924
548.211	565.190	585.230	611.560	642.955
676.287	773.752	815.380	826.614	830.225
829.402	829.251	829.606	826.571	815.313
798.841	780.729	762.982	746.369	731.856
719.154	708.939	698.905	688.952	680.241
671.864	663.297	653.173	644.471	636.534
628.317	619.321	608.705	595.505	579.029
551.713	570.457			

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.83023E+03
	WO	=	.49855E+03
	DIFFS/WO	=	.16653E+01
CONSTRAINT 1	BLTKS	=	.44211E-02
CONSTRAINT 2	YMAX	=	.67629E+03
	YMIN	=	.43890E+03
	DIFFP	=	.15409E+01
CONSTRAINT 3	WMB (MRO-2,1)	=	.55171E+03
	WMB (MRO-2,2)	=	.49485E+03

TECLSR = .71078E+00

OPTIMIZATION RESULTS

OBJECTIVE FUNCTION
 GLOBAL LOCATION 1 FUNCTION VALUE .16653E+01

DESIGN VARIABLES

ID	D. V. NO.	GLOBAL VAR. NO.	LOWER BOUND	VALUE	UPPER BOUND
1	1	2	-.15000E+02	-.80297E+01	0.
2	2	3	.20000E+00	.20000E+00	.60000E+00
3	3	4	.20000E+00	.55000E+00	.55000E+00
4	4	5	.50000E+00	.73559E+00	.40000E+01
5	5	6	.30000E-01	.36263E-01	.10000E+00
6	6	7	.30000E-02	.39389E-02	.12000E-01

DESIGN CONSTRAINTS

ID	GLOBAL VAR. NO.	LOWER BOUND	VALUE	UPPER BOUND
1	8	0.	.44211E-02	.10000E+02
3	9	0.	.15409E+01	.16000E+01
5	10	-.10000E+01	.71078E+00	.10000E+01

*** INPUT FOR BLADE ELEMENT PROGRAM ***

NO. BLADES	INLET RADIUS (L)	CONE ANGLE (DEG)	SOLIDITY	INLET BLADE ANGLE (DEG)	OUTLET BLADE ANGLE (DEG)	TRANS. LOC. /CHORD	MAX.TH. LOC. /CHORD	IN/OUT TURNING RATE	MAX. THICK. /CHORD	L.E. RAD. /CHORD	T.E. RAD. /CHORD
34	.45400	6.66400	2.25200	52.000	-8.0297	.20000	.55000	.73559	.03626	.00394	.00500

*** OUTPUT FROM BLADE ELEMENT PROGRAM ***

CHORD (L)	ELEMENT SETTING ANGLE (DEG)
.19322	23.5522

* MERID. LOC. FROM L.E. CENT. **				** THETA LOC. FROM L.E. CENT. **				***** BLADE ANGLES *****				SEGMENT LENGTHS		
*****				*****				(WITH RESPECT TO LOCAL CONIC RAY)				*****		
INLET (L)	OUTLET (L)	TRANS. (L)	MAX.TH. (L)	INLET (RAD)	OUTLET (RAD)	TRANS. (RAD)	MAX.TH. (RAD)	INLET (DEG)	OUTLET (DEG)	TRANS. (DEG)	MAX.TH. (DEG)	FIRST (L)	SECOND (L)	
SUCT.	-.00061	.17564	.02675	.08501	.00101	.16727	.06970	.15112	52.848	-11.222	44.807	20.661	.04159	.16190
CENT.	0.00000	.17546	.02807	.08624	0.00000	.16528	.06653	.14405	52.000	-8.030	42.376	20.661	.04136	.15935
PRES.	.00059	.17538	.02940	.08748	-.00105	.16325	.06334	.13699	51.166	-4.794	39.883	20.661	.04119	.15704

**** CONIC ANGLE COORD. - E ****				***** BLADE ANGLES *****				
** (FROM LEADING EDGE CENT.) **				(WITH RESPECT TO L.E. CENT. RAY)				
INLET (DEG)	OUTLET (DEG)	TRANS. (DEG)	MAX.TH. (DEG)	INLET (DEG)	OUTLET (DEG)	TRANS. (DEG)	MAX.TH. (DEG)	
SUCT.	.007	1.112	.463	1.005	52.855	-10.110	45.271	21.666
CENT.	0.000	1.099	.442	.958	52.000	-8.030	42.819	21.619
PRES.	-.007	1.085	.421	.911	51.159	-3.709	40.304	22.530

Figure A.2.- Continued.

*** OUTPUT THAT CAN BE PUNCHED FOR TSONIC INPUT ***

```

*****
*           CHORD      STGR           *
*           (L)       (RAD)          *
*           .17718    .165276        *
*           *           *           *
*****
*
*           *** SUCTION SURFACE ***   *
*           *           *           *
*           *****                 *
*           RI          RO          BETI  BETO  *
*           (L)        (L)        (DEG) (DEG) *
*           .00076    .00097    52.8551 -10.1097 *
*
*           ZMSP        THSP        *
*           (L)         (RAD)        *
*           .00015     .001012      *
*           .00644     .018624      *
*           .01569     .042414      *
*           .02688     .068304      *
*           .04209     .097782      *
*           .05884     .122866      *
*           .07687     .143206      *
*           .09593     .158534      *
*           .11571     .168663      *
*           .13592     .173491      *
*           .15219     .173520      *
*           .16637     .170770      *
*           .17641     .167241      *
*
*           *** PRESSURE SURFACE ***  *
*           *           *           *
*           *****                 *
*           RI          RO          BETI  BETO  *
*           (L)        (L)        (DEG) (DEG) *
*           .00076    .00097    51.1587 -3.7086 *
*
*           ZMSP        THSP        *
*           (L)         (RAD)        *
*           .00135     -.001051     *
*           .00775     .015605      *
*           .01729     .037720      *
*           .02898     .061165      *
*           .04470     .087489      *
*           .06153     .110221      *
*           .07931     .129167      *
*           .09786     .144173      *
*           .11700     .155129      *
*           .13656     .161966      *
*           .15237     .164450      *
*           .16624     .164451      *
*           .17614     .163216      *
*
*****

```

Figure A.2.- Continued.

*** PLOT OF BLADE SURFACE IN THETA - M COORDINATES ***

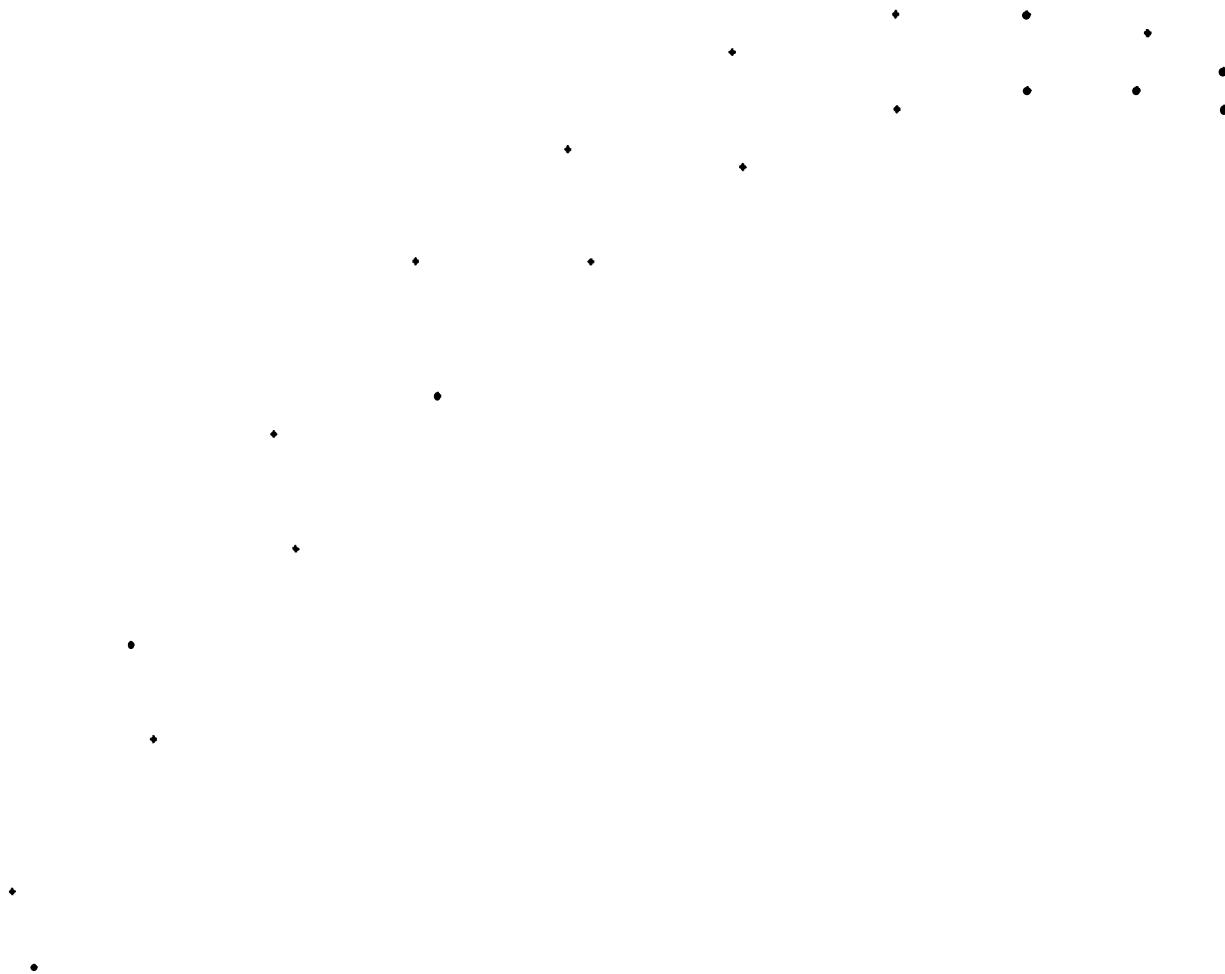


Figure A.2.- Continued.



Figure A.2.- Continued.

--- INPUT FOR TSONIC BLADE-TO-BLADE FLOW SOLVER ---

GAM	AR	TIP	RHOIP	WTFI	OMEGA	ORF				
1.400000	1716.480	599.7600	.3345860E-02	.5700000E-02	0.	1.910000				
BETA1	BETA0	CHORD	STGRF	FSMI	FSMO					
48.20000	0.	.1771834	.1652756	0.	0.					
REDFAC	DENTOL	SSM1	SSM2							
1.000000	.1000000E-02	0.	0.							
MBI	MBO	MM	NBRI	NBL	NRSP	MOPT	LOPT	LRVB		
24	56	0	0	72	15	34	13	0	1	0
BLADE SURFACE 1 -- UPPER SURFACE										
RI1	RO1	BET11	BET01	SPLN01						
.7610700E-03	.9660876E-03	52.85512	-10.10968	13.00000						
MSP1 ARRAY										
.1544666E-03	.6437113E-02	.1568635E-01	.2687976E-01	.4208902E-01	.5883798E-01	.7687469E-01	.9592700E-01			
.1157074	.1359176	.1521902	.1663708	.1764053						
THSP1 ARRAY										
.1012280E-02	.1862413E-01	.4241444E-01	.6830414E-01	.9778183E-01	.1228661	.1432064	.1585341			
.1686632	.1734907	.1735195	.1707699	.1672414						
BLADE SURFACE 2 -- LOWER SURFACE										
RI2	RO2	BET12	BET02	SPLN02						
.7610700E-03	.9660876E-03	51.15866	-3.708649	13.00000						
MSP2 ARRAY										
.1353915E-02	.7749708E-02	.1729088E-01	.2898442E-01	.4470456E-01	.6153388E-01	.7930961E-01	.9785967E-01			
.1170045	.1365588	.1523700	.1662433	.1761365						
THSP2 ARRAY										
.1050920E-02	.1560516E-01	.3771963E-01	.6116454E-01	.8748856E-01	.1102210	.1291670	.1441733			
.1551291	.1619659	.1644503	.1644505	.1632162						
MR ARRAY										
.1300000	.5000000E-02	.5000000E-02	.2003000E-01	.4003000E-01	.8003000E-01	.1000300	.1250300			
.1500400	.1752600	.1852600	.2250000	.2700000						
RMSP ARRAY										
.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000	.4540000			
.4540000	.4540000	.4540000	.4540000	.4540000						
BESP ARRAY										
.5000000E-01	.5000000E-01	.4990000E-01	.4960000E-01	.4925000E-01	.4850000E-01	.4815000E-01	.4770000E-01			
.4720000E-01	.4675000E-01	.4661000E-01	.4661000E-01	.4661000E-01						
PLOSS ARRAY										
0.	0.	.1500000E-02	.5900000E-02	.1100000E-01	.2150000E-01	.3000000E-01	.3350000E-01			
.4000000E-01	.4700000E-01	.4800000E-01	.4800000E-01	.4800000E-01						
BLDAT	AANDK	ERSOR	STRFN	SLCRD	INTVL	SURVL				
0	0	0	0	0	0	1				

Figure A.2.- Continued.

RELATIVE VELOCITY	MERIDIONAL VELOCITY	CRITICAL VELOCITY	REL. FLOW ANGLE
AT M = FSMI	AT M = FSMI	AT M = FSMI	AT UPSTREAM BDY.
745.90	497.17	1095.9	48.269
AT M = FSMO	AT M = FSMO	AT M = FSMO	AT DOWNSTREAM BDY.
497.92	497.92	1095.9	0.

FSMI = 0.
FSMO = .17718

CALCULATED PROGRAM CONSTANTS

PITCH	HT	HMI
.1847996	.1231997E-01	.5536980E-02
ITMIN	ITMAX	
0	28	
LAMBDA	DOWNSTREAM WHIRL (RVTHO)	
252.4466	0.	
REDUCED WEIGHT FLOW =	.5700000E-02	
NUMBER OF INTERIOR MESH POINTS =	1047	

CALCULATED VELOCITY DIAGRAM INFORMATION

	IM	W	W/WCR	BETA
UPSTREAM BOUNDARY	1	745.10	.67988	48.269
LEADING EDGE	24	745.90	.68061	48.200
TRAILING EDGE	56	497.92	.45433	0.
DOWNSTREAM BOUNDARY	72	499.62	.45589	0.

Figure A.2.- Continued.

ITERATION NO. 1	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1846	AT IM = 0,	IT = 7,	SURF = 1,	M = .3571E-01
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1074				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 92				
ITERATION NO. 2	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .6432E-01	AT IM = 0,	IT = 1,	SURF = 1,	M = .4135E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2615E-01				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 92				
ITERATION NO. 3	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2959E-01	AT IM = 0,	IT = 1,	SURF = 1,	M = .4135E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .8037E-02				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 91				
ITERATION NO. 4	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1410E-01	AT IM = 0,	IT = 1,	SURF = 1,	M = .4135E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2790E-02				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 55				
ITERATION NO. 5	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .6708E-02	AT IM = 0,	IT = 1,	SURF = 1,	M = .4135E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1041E-02				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 27				
ITERATION NO. 6	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .3285E-02	AT IM = 0,	IT = 1,	SURF = 1,	M = .4135E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .4003E-03				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 17				
ITERATION NO. 7	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1422E-02	AT IM = 0,	IT = 1,	SURF = 1,	M = .4135E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .1766E-03				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 1				
ITERATION NO. 8	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .7977E-03	AT IM = 0,	IT = 1,	SURF = 1,	M = .4135E-02
	AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .7674E-04				
	NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 0				
ITERATION NO. 9	MAXIMUM RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2963E-03	AT IM = 0,	IT = 15,	SURF = 2,	M = .1739E-02

Figure A.2.- Continued.

AVERAGE RELATIVE CHANGE IN DENSITY AT BLADE SURFACE POINTS = .2880E-04
 NUMBER OF UNCONVERGED BLADE SURFACE MESH POINTS = 0

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SURFACE VELOCITIES BASED ON MERIDIONAL COMPONENTS - REDUCED WEIGHT FLOW									
M	VELOCITY	BLADE SURFACE 1			W/WCR	VELOCITY	BLADE SURFACE 2		
		ANGLE (DEG)	SURF. LENGTH	W/WCR			ANGLE (DEG)	SURF. LENGTH	W/WCR
0.	0.	90.00	0.	0.	0.	0.	-90.00	0.	0.
.5537E-02	797.1	51.11	.9198E-02	.7273	659.3	49.33	.7168E-02	.6016	
.1107E-01	813.2	49.39	.1786E-01	.7420	631.7	47.02	.1547E-01	.5764	
.1661E-01	825.6	47.83	.2623E-01	.7533	596.0	44.79	.2343E-01	.5438	
.2215E-01	838.0	46.15	.3435E-01	.7646	571.5	42.65	.3109E-01	.5215	
.2768E-01	845.8	44.13	.4221E-01	.7718	551.4	40.56	.3849E-01	.5031	
.3322E-01	845.9	41.88	.4978E-01	.7719	534.4	38.52	.4567E-01	.4876	
.3876E-01	839.4	39.46	.5708E-01	.7659	519.7	36.50	.5265E-01	.4742	
.4430E-01	827.6	36.90	.6413E-01	.7551	507.1	34.53	.5946E-01	.4627	
.4983E-01	809.1	34.39	.7094E-01	.7383	497.9	32.60	.6610E-01	.4544	
.5537E-01	787.1	32.00	.7756E-01	.7182	488.4	30.71	.7261E-01	.4457	*
.6091E-01	767.5	29.79	.8401E-01	.7003	481.6	28.87	.7899E-01	.4394	*
.6644E-01	751.8	27.62	.9032E-01	.6860	474.2	27.07	.8526E-01	.4327	*
.7198E-01	735.6	25.47	.9651E-01	.6712	469.0	25.29	.9143E-01	.4279	*
.7752E-01	723.0	23.35	.1026	.6597	463.2	23.54	.9751E-01	.4227	*
.8305E-01	709.9	21.26	.1086	.6478	459.5	21.83	.1035	.4193	*
.8859E-01	700.7	19.21	.1145	.6394	454.9	20.14	.1094	.4151	*
.9413E-01	691.8	17.20	.1203	.6313	452.2	18.46	.1153	.4126	*
.9967E-01	681.5	15.23	.1261	.6219	449.7	16.82	.1211	.4103	*
.1052	673.9	13.28	.1318	.6149	446.0	15.19	.1269	.4069	*
.1107	666.0	11.34	.1375	.6077	444.0	13.58	.1326	.4052	*
.1163	658.1	9.43	.1431	.6005	442.6	12.00	.1383	.4038	*
.1218	650.4	7.53	.1487	.5935	441.7	10.43	.1439	.4030	*
.1274	642.7	5.65	.1543	.5865	441.7	8.85	.1495	.4030	*
.1329	632.3	3.79	.1598	.5770	441.3	7.28	.1551	.4027	*
.1384	624.6	1.94	.1654	.5699	443.7	5.71	.1607	.4049	*
.1440	615.9	.08	.1709	.5620	447.6	4.19	.1663	.4084	*
.1495	605.7	-1.78	.1764	.5527	452.8	2.74	.1718	.4132	*
.1550	593.0	-3.65	.1820	.5411	459.0	1.33	.1773	.4188	*
.1606	579.4	-5.46	.1875	.5287	468.2	-.33	.1829	.4272	*
.1661	561.2	-7.22	.1931	.5121	489.6	-2.27	.1884	.4467	*
.1716	549.8	-8.86	.1987	.5016	567.0	-3.66	.1940	.5173	*
.1772	0.	-90.00	.2045	0.	0.	90.00	.1995	0.	*

Figure A.2.- Continued.

SURFACE VELOCITIES BASED ON TANGENTIAL COMPONENTS
REDUCED WEIGHT FLOW

M	BLADE SURFACE 1		W/WCR
	VELOCITY	ANGLE (DEG)	
0.	493.5	90.00	.4503
.4135E-02	859.0	51.56	.7838
.8691E-02	801.6	50.11	.7314
.1349E-01	817.5	48.69	.7460
.1852E-01	829.3	47.29	.7567
.2384E-01	840.8	45.57	.7672
.2953E-01	847.4	43.40	.7732
.3571E-01	846.7	40.81	.7726
.4254E-01	838.8	37.72	.7654
.5026E-01	808.8	34.20	.7380
.5909E-01	783.6	30.50	.7150
.6940E-01	751.8	26.46	.6860
.8192E-01	726.3	21.69	.6627
.9848E-01	699.7	15.65	.6385
.1292	657.5	5.03	.5999
.1592	583.5	-5.01	.5324

M	BLADE SURFACE 2		W/WCR
	VELOCITY	ANGLE (DEG)	
.1739E-02	769.5	50.99	.7021
.6438E-02	661.6	48.95	.6037
.1149E-01	617.5	46.84	.5634
.1694E-01	587.2	44.66	.5358
.2283E-01	562.6	42.39	.5134
.2922E-01	541.6	39.99	.4942
.3620E-01	523.1	37.43	.4773
.4388E-01	507.4	34.68	.4630
.5243E-01	490.0	31.71	.4471
.6208E-01	475.2	28.48	.4336
.7321E-01	462.6	24.90	.4221
.8649E-01	453.6	20.78	.4139
.1035	444.2	15.70	.4053
.1300	433.7	8.09	.3958

Figure A.2.- Continued.

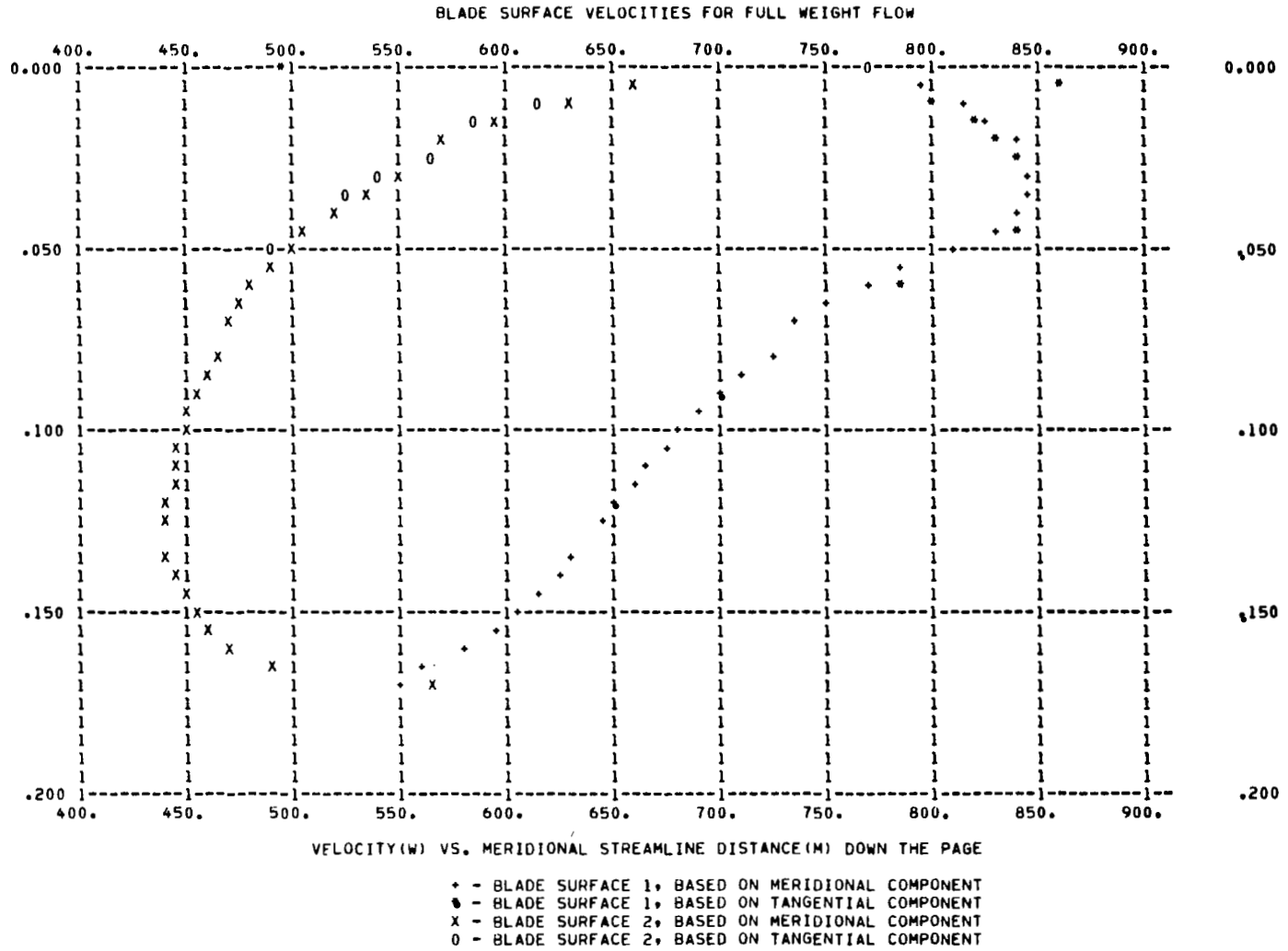


Figure A.2.- Continued.

BLADE SURFACE PRESSURES FOR FULL WEIGHT FLOW

IM	M	M/MC	P(1)/PT	P(2)/PT	CPT(1)	CPT(2)
24	0.	0.	.9994	.9994	-.6204E-03	-.6204E-03
25	.5537E-02	.3125E-01	.7228	.8030	-.2772	-.1970
26	.1107E-01	.6250E-01	.7118	.8167	-.2882	-.1833
27	.1661E-01	.9375E-01	.7029	.8338	-.2971	-.1662
28	.2215E-01	.1250	.6939	.8446	-.3061	-.1554
29	.2768E-01	.1563	.6879	.8530	-.3121	-.1470
30	.3322E-01	.1875	.6869	.8598	-.3131	-.1402
31	.3876E-01	.2188	.6901	.8655	-.3099	-.1345
32	.4430E-01	.2500	.6967	.8701	-.3033	-.1299
33	.4983E-01	.2813	.7072	.8732	-.2928	-.1268
34	.5537E-01	.3125	.7197	.8763	-.2803	-.1237
35	.6091E-01	.3438	.7305	.8781	-.2695	-.1219
36	.6644E-01	.3750	.7387	.8799	-.2613	-.1201
37	.7198E-01	.4063	.7469	.8806	-.2531	-.1194
38	.7752E-01	.4375	.7526	.8812	-.2474	-.1188
39	.8305E-01	.4688	.7582	.8806	-.2418	-.1194
40	.8859E-01	.5000	.7613	.8801	-.2387	-.1199
41	.9413E-01	.5313	.7643	.8790	-.2357	-.1210
42	.9967E-01	.5625	.7683	.8781	-.2317	-.1219
43	.1052	.5938	.7714	.8784	-.2286	-.1216
44	.1107	.6250	.7750	.8784	-.2250	-.1216
45	.1163	.6563	.7787	.8785	-.2213	-.1215
46	.1218	.6875	.7824	.8783	-.2176	-.1217
47	.1274	.7188	.7858	.8776	-.2142	-.1224
48	.1329	.7500	.7903	.8768	-.2097	-.1232
49	.1384	.7813	.7930	.8745	-.2070	-.1255
50	.1440	.8125	.7961	.8715	-.2039	-.1285
51	.1495	.8438	.7997	.8679	-.2003	-.1321
52	.1550	.8750	.8044	.8638	-.1956	-.1362
53	.1606	.9063	.8095	.8585	-.1905	-.1415
54	.1661	.9375	.8167	.8484	-.1833	-.1516
55	.1716	.9688	.8209	.8129	-.1791	-.1871
56	.1772	1.000	.9527	.9527	-.4728E-01	-.4728E-01

SURF 1		SURF 2	
XMSP	XTHSP	XMSP	XTHSP
.15447E-03	.10123E-02	.13539E-02	-.10509E-02
.64371E-02	.18624E-01	.77497E-02	.15605E-01
.15686E-01	.42414E-01	.17291E-01	.37720E-01
.26880E-01	.68304E-01	.28984E-01	.61165E-01
.42089E-01	.97782E-01	.44705E-01	.87489E-01
.58838E-01	.12287E+00	.61534E-01	.11022E+00
.76875E-01	.14321E+00	.79310E-01	.12917E+00
.95927E-01	.15853E+00	.97860E-01	.14417E+00
.11571E+00	.16866E+00	.11700E+00	.15513E+00
.13592E+00	.17349E+00	.13656E+00	.16197E+00
.15219E+00	.17352E+00	.15237E+00	.16445E+00
.16637E+00	.17077E+00	.16624E+00	.16445E+00
.17641E+00	.16724E+00	.17614E+00	.16322E+00

OUTPUT FROM OBJCON

OBJECTIVE FUNCTION	DIFFS	=	.84594E+03
	WO	=	.49792E+03
	DIFFS/WO	=	.16990E+01
CONSTRAINT 1	BLTKS	=	.44211E-02
CONSTRAINT 2	YMAX	=	.65929E+03
	YMIN	=	.44134E+03
	DIFFP	=	.14938E+01
CONSTRAINT 3	WMB(MB0-2,1)	=	.56124E+03
	WMB(MB0-2,2)	=	.48960E+03
	TECLSR	=	.89556E+00

FINAL OBJECTIVE COMPUTED BY TSONIC = 1.698965

FINAL CONSTRAINT VALUES
RLTKS DIFFP TECLSR
.44211E-02 .14938E+01 .89556E+00

X ARRAY

.968750	.937500	.906250	.875000	.843750
.812500	.781250	.750000	.718750	.687500
.656250	.625000	.593750	.562500	.531250
.500000	.468750	.437500	.406250	.375000
.343750	.312500	.281250	.250000	.218750
.187500	.156250	.125000	.093750	.062500
.031250	.031250	.062500	.093750	.125000
.156250	.187500	.218750	.250000	.281250
.312500	.343750	.375000	.406250	.437500
.468750	.500000	.531250	.562500	.593750
.625000	.656250	.687500	.718750	.750000
.781250	.812500	.843750	.875000	.906250
.937500	.968750			

LTRACE = 1

Y ARRAY BEFORE PERTRB CALL

566.953	489.596	468.231	459.001	452.816
447.620	443.724	441.341	441.690	441.695
442.577	444.037	445.975	449.688	452.173
454.893	459.487	463.246	468.972	474.208
481.593	488.443	497.947	507.051	519.736
534.387	551.407	571.509	596.015	631.744
659.289	797.094	813.197	825.572	837.975
845.829	845.941	839.362	827.555	809.126
787.101	767.508	751.752	735.601	722.997
709.946	700.748	691.827	681.542	673.904
666.048	658.146	650.419	642.711	632.308
624.559	615.941	605.686	592.951	579.399
561.240	549.767			

 * COMPARISON OF AERODYNAMIC AND PERTURBATION SOLUTIONS *

.....MACH NUMBER,
 VALUES OF PERTURBATION PARAMETERS,
 CRITICAL VALUE OF WM:

M2 = .1000
 Q2(1) = -8.0297 (KOCR)
 Q2(2) = .2000 (T)
 Q2(3) = .5500 (ZM)
 Q2(4) = .7356 (P)
 Q2(5) = .0363 (TMX)
 Q2(6) = .0039 (THLE)
 WMCRT = -66.8587

.....LOCATIONS OF MIN., MAX., AND CRITICAL PTS.
 (* DENOTES POINT ON LOWER SURFACE)

PERTURBATION SOLN:

MINIMUM AT X = .7122* (POINT NO. 9)
 MAXIMUM AT X = .1194 (POINT NO. 34)

AERODYNAMIC SOLN:

MINIMUM AT X = .7500* (POINT NO. 8)
 MAXIMUM AT X = .1875 (POINT NO. 37)

.....FINAL PRINTOUT AND GRAPHICAL DISPLAY OF WM

H = MAXIMUM VALUE OF WM = 845.9406
 L = MINIMUM VALUE OF WM = 438.9010
 * = CRITICAL VALUE OF WM = -66.8587
 P = VALUE OF WM PREDICTED BY PERTURBATION SOLUTION
 A = VALUE OF WM IN AERODYNAMIC SOLUTION
 \$ = AGREEMENT BETWEEN P AND A

PT	XBASE	WMBASE	XPERT	WMPERT	XAERO	WMAERO	WMPINT	H	
1	.9687585.9460		.9680549.7994		.9688566.9527551.1194				A P
2	.9375500.5262		.9360492.2104		.9375489.5955494.8503				PA
3	.9062475.3838		.9041468.2692		.9063468.2308469.9154				\$
4	.8750463.5379		.8721457.5440		.8750459.0015458.5273				\$
5	.8437455.4531		.8401450.7826		.8438452.8158451.5575				\$
6	.8125448.9545		.8081445.5287		.8125447.6203446.2512				\$
7	.7813444.0337		.7761441.7684		.7813443.7239442.3717				\$

Figure A.2.- Continued.

8	.7500440.6925	.7441439.5594	.7500441.3408439.9645
9	.7188438.6925	.7122438.7299	.7188441.6899438.9010
10	.6875437.8173	.6802439.4101	.6875441.6948439.2542
11	.6563439.1700	.6482441.5321	.6563442.5766440.9971
12	.6250439.8327	.6162443.2946	.6250444.0366442.8098
13	.5938441.0316	.5842445.5640	.5938445.9745444.8878
14	.5625442.5981	.5522448.7173	.5625449.6875447.7054
15	.5313445.5570	.5203452.6026	.5313452.1730451.2668
16	.5000447.4626	.4883455.9259	.5000454.8932454.7072
17	.4688449.7452	.4563460.4083	.4688459.4870458.6617
18	.4375453.7909	.4243465.7523	.4375463.2464463.5475
19	.4063457.2295	.3923471.6608	.4063468.9715469.0877
20	.3750462.5307	.3603475.4134	.3750474.2081473.6932
21	.3438467.1474	.3284488.9358	.3438481.5930482.4272
22	.3125473.4596	.2964502.5190	.3125488.4431495.6698
23	.2813479.5215	.2644512.6771	.2813497.9474507.3221
24	.2500487.9145	.2324526.4762	.2500507.0512518.8856
25	.2188496.1051	.2004541.5761	.2188519.7356532.9238
26	.1875508.1057	.1684557.9958	.1875534.3871548.2109
27	.1563522.6991	.1365576.8714	.1563551.4073565.1903
28	.1250540.8496	.1045600.2040	.1250571.5092585.2300
29	.0938564.0343	.0725634.0712	.0938596.0147611.5602
30	.0625599.0169	.0405662.5095	.0625631.7438642.9552
31	.0313632.8560	.0085710.1042	.0313659.2892676.2870
32	.0313836.7472	.0554812.4625	.0313797.0941773.7523
33	.0625848.1344	.0874825.6826	.0625813.1973815.3804
34	.0937851.3453	.1194830.3923	.0938825.5723826.6141
35	.1250846.1514	.1498829.4847	.1250837.9745830.2251
36	.1563834.5030	.1801829.0993	.1563845.8290829.4024
37	.1875820.3078	.2105829.7257	.1875845.9406829.2512
38	.2188805.2289	.2409829.2858	.2188839.3616829.6062
39	.2500788.7474	.2712820.2590	.2500827.5552826.5711
40	.2813770.7026	.3016805.2661	.2813809.1264815.3133
41	.3125754.1898	.3320787.3683	.3125787.1011798.8407
42	.3438739.2561	.3623770.2638	.3438767.5078780.7293
43	.3750723.4856	.3927752.8141	.3750751.7521762.9824
44	.4063710.8176	.4231738.3766	.4063735.6008746.3690
45	.4375697.5629	.4534724.6654	.4375722.9967731.8562
46	.4688688.7980	.4838713.7454	.4688709.9455719.1542
47	.5000680.8503	.5142704.7421	.5000700.7477708.9392
48	.5313671.6336	.5445694.3740	.5313691.8266698.9053
49	.5625665.2669	.5749685.2170	.5625681.5421688.9522
50	.5938658.7253	.6053677.2071	.5938673.9036680.2410
51	.6250651.9964	.6356668.9914	.6250666.0482671.8639
52	.6563644.9958	.6660660.6116	.6563658.1457663.2973
53	.6875635.7344	.6963650.1146	.6875650.4193653.1730
54	.7188629.2778	.7267642.4657	.7188642.7110644.4714
55	.7500622.6299	.7571634.7305	.7500632.3081636.5335
56	.7813615.5034	.7874626.6743	.7813624.5586628.3174
57	.8125607.3548	.8178617.7636	.8125615.9409619.3213
58	.8437597.2455	.8482607.1599	.8437605.6857608.7046
59	.8750584.0971	.8785593.9676	.8750592.9514595.5051
60	.9062567.1183	.9089577.5979	.9062579.3986579.0288
61	.9375548.2492	.9393550.1110	.9375561.2400551.7128
62	.9687533.5057	.9696571.0680	.9687549.7669570.4574

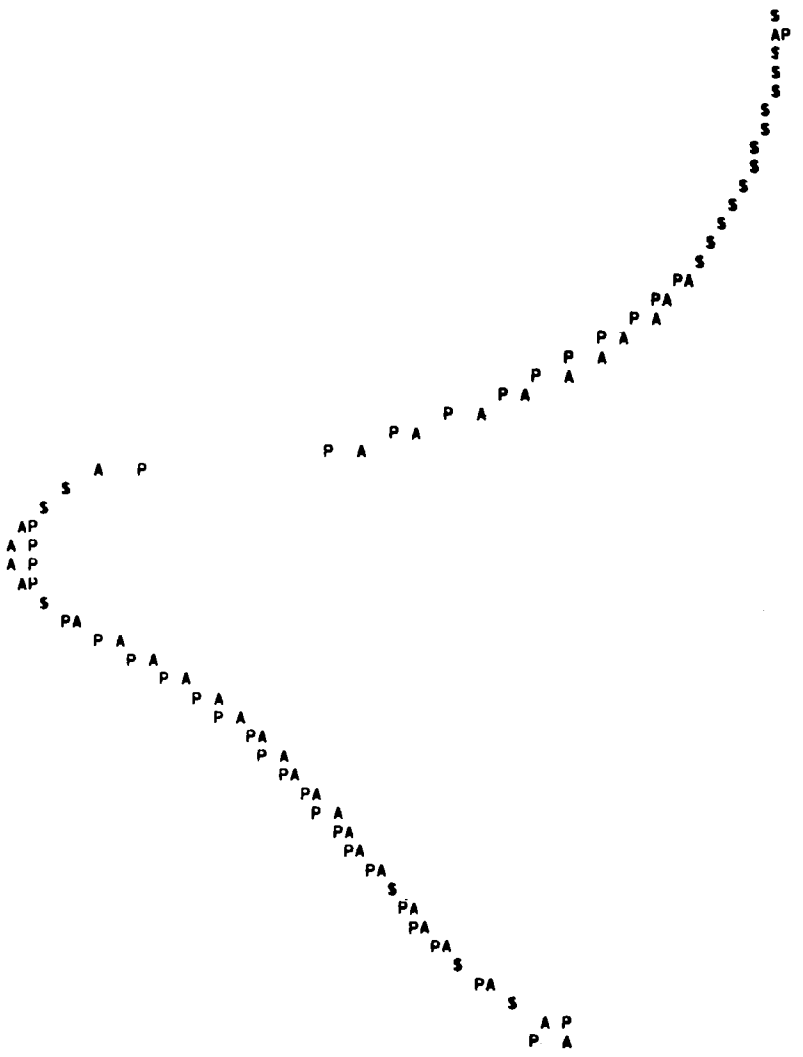


Figure A.2.- Concluded.

APPENDIX B
LISTING OF COMPUTER PROGRAM BLDOPT

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PROGRAM BLDOPT(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,
* TAPE1,TAPE7,TAPE9,TAPE10,TAPE11,TAPE12,TAPE13,TAPE14,
* TAPE20,TAPE40)
C
C DRIVER PROGRAM FOR COPE5 OPTIMIZATION STUDY WITH OPTIONS
C FOR PERTURBATION METHOD USE.
C THE RELATIONSHIP AMONG PROGRAM COMPONENTS IS
C DRIVER
C   - COPE5
C     - ANALIZ
C       - BLADE ROUTINES
C       - TSONIC ROUTINES
C       - PERTRB ROUTINE
C       - OBJCON
C
C PROGRAM OPTIONS
C   IOPT = 1 - OPTIMIZATION USING TSONIC SOLUTIONS ONLY -
C             PERTURBATION METHOD BYPASSED
C   2 - OPTIMIZATION WITH PERTURBATION METHOD EMPLOYING
C       USER-SPECIFIED CALIBRATION SOLUTION MATRIX
C   3 - OPTIMIZATION WITH 1 CYCLE EMPLOYING TSONIC SOLUTIONS
C       ONLY, FOLLOWED BY ITMAX CYCLES EMPLOYING
C       PERTURBATION METHOD
C
COMMON/CALB/ ICALB,DVCALB(6),PSTEP,IOPT,ITMAX3,VZERO(6)
COMMON/CNMN1/DUM(12),NDV,DUM(6),ITMAX,DUM2(7)
COMMON/COPE52/ RA(5000),IA(1000)
COMMON/COPE53/DUM3(16),LOCR(25),LOCI(25),DUM4(19)
COMMON/GLOBCH/ OBJ,V(6),C(5),EXTRA(1488)
C
C IFLAG=1
C CALL COPE5(IFLAG)
C IF(IOPT.LT.3) STOP
C
C IOPT=3 CALCULATE CALIBRATION STEPSIZES, THEN PERFORM
C OPTIMIZATION WITH PERTURBATION SOLUTIONS
C
C
C   NVLB=LOCR(2)
C   NVUB=LOCR(3)
C   CALL STEP(NDV,V,VZERO,DVCALB,RA(NVLB),RA(NVUB))
C   ICALB=1
C   ITMAX=ITMAX3
C   DO 10 I=1,NDV
10 RA(I)=0.0
C   IFLAG=2
C   CALL COPE5(IFLAG)
C   STOP
C   END
C   SUBROUTINE STEP(NDV,V,VZERO,DVCALB,VLB,VUB)
C
C ROUTINE TO CALCULATE CALIBRATION STEPSIZES FOR IOPT=3
C BASED ON DESIGN RESULTS AFTER 1 OPTIMIZATION CYCLE
C EMPLOYING TSONIC SOLUTIONS ONLY.
C
C   DIMENSION V(1),VZERO(1),DVCALB(1),VLB(1),VUB(1)
C   DO 20 I=1,NDV
C   P=V(I)-VZERO(I)
C   DVCALB(I)=V(I)*0.5*P
C   IF(DVCALB(I).LT.VLB(I)) DVCALB(I)=VLB(I)
C   IF(DVCALB(I).GT.VUB(I)) DVCALB(I)=VUB(I)
C
BLDOPT 2 IF(ABS(V(I)-VLB(I)).LT.1.E-6)
BLDOPT 3 * DVCALB(I)=0.9*(VLB(I)-VZERO(I))+VZERO(I)
BLDOPT 4 IF(ABS(V(I)-VUB(I)).LT.1.E-6)
BLDOPT 5 * DVCALB(I)=0.9*(VUB(I)-VZERO(I))+VZERO(I)
BLDOPT 6 20 CONTINUE
C
BLDOPT 7 RETURN
BLDOPT 8 END
BLDOPT 9 SUBROUTINE ANALIZ(ICALC)
C
C INITIALIZES, CALCULATES, AND OUTPUTS ALL DESIGN
C VARIABLES, OBJECTIVE FUNCTION, AND CONSTRAINTS FOR
C OPTIMIZATION WITH COPE5 DRIVER.
C
COMMON/GLOBCH/ OBJ,V(6),C(5),EXTRA(1488)
COMMON /PERT/ Q0(10),Q1,Q2(10),XM0,XM1,XM2,NPTS,KPARAM,NPARAM,
* LTRACE
COMMON /INPUTB/ ALP,KICR,KOCR,NB,P,R,SOLID,T,THLE,THTE,THX,ZH
COMMON /HBIMBO/ HBI,MBO
COMMON/INPUTA/ XHSP(50,2),XTHSP(50,2)
COMMON /CALB/ ICALB,DVCALB(6),PSTEP,IOPT,ITMAX3,VZERO(6)
DIMENSION X(200),Y(200),VV(8),IDV(6),VNAME(6)
REAL KICR,KOCR
LOGICAL NONLIN
DATA XM0/0.1/, XM1/0.1/, XM2/0.1/
IF (ICALC .GT. 1) GO TO 100
C
C ICALC = 1 READ INPUT AND INITIALIZE PARAMETERS
C
C READ(5,1025) COMENT
C READ(5,1005) IOPT,NDV,NCN,ITMAX3
C NPARAM=NDV
C READ(5,1010) NB,R,ALP,SOLID
C READ(5,1020) (VV(I),I=1,8)
C KICR=VV(1)
C KOCR=VV(2)
C T =VV(3)
C ZM =VV(4)
C P =VV(5)
C THX =VV(6)
C THLE=VV(7)
C THTE=VV(8)
C READ(5,1025) (VNAME(I),I=1,NDV)
C READ(5,1005) (IDV(I),I=1,NDV)
C DO 5 I=1,NDV
C J=IDV(I)
C V(I)=VV(J)
5 VZERO(I)=VV(J)
C READ(5,1010) ICALB,PSTEP
C IF(ICALB.EQ.0) GO TO 10
C READ(5,1020) (DVCALB(I),I=1,NDV)
10 CONTINUE
C
C WRITE(6,1000)
C WRITE(6,1055) IOPT,NDV,NCN,ITMAX3
C WRITE(6,1060) NB,R,ALP,SOLID
C WRITE(6,1065) (VV(I),I=1,8)
C WRITE(6,1070) (VNAME(I),I=1,NDV)
C WRITE(6,1072) (V(I),I=1,NDV)
C WRITE(6,1075) ICALB,PSTEP
STEP 14
STEP 15
STEP 16
STEP 17
STEP 18
STEP 19
STEP 20
STEP 21
ANALIZ 2
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IF(ICALB.EQ.0) GO TO 14
WRITE(6,1080) (I,I=1,NDV)
WRITE(6,1085) (DV(CALB(I),I=1,NDV)
14 CONTINUE
C
ICALL=1
JCALL=0
KPARAM=0
LTRACE=0
NONLIN=.T.
IF(IOPT.EQ.2) NONLIN=.F.
READ(5,1025) COMENT
CALL TSONIC
NPTS=2*(MBO-MBI-1)
IF(IOPT.EQ.1) GO TO 15
READ(5,1025) COMENT
CALL PERTRB(ICALL,X,Y)
15 CONTINUE
ICALL=2
RETURN
C
C ICALC = 2 PERFORM OPTIMIZATION CALCULATION
C
100 IF(ICALC.GT.2) GO TO 200
20 CALL DESVAR(VV,V,IOV,NDV,ICALL,KPARAM)
WRITE(6,2000) NB,R,ALP,SOLID,KICR,KOCR,T,ZM,P,TMX,THLE,THTE
CALL BLADE(0)
IF(.NOT.NONLIN) GO TO 22
C
EMPLOY TSONIC SOLUTIONS, IOPT=1 OR 3
C
CALL TSONIC
CALL XY(X,Y)
WRITE(6,2005) (X(I),I=1,NPTS)
WRITE(6,2010) (Y(I),I=1,NPTS)
CALL OBJCON(X,Y,OBJ,C)
RETURN
C
EMPLOY BASE/CALIBRATION/PERTURBATION SOLUTIONS, IOPT=2 OR 3
C
22 CONTINUE
IF(ICALL.EQ.4) GO TO 24
CALL TSONIC
CALL XY(X,Y)
24 CALL PERVAR(Q0,Q1,Q2,V,ICALL,KPARAM)
CALL PERTRB(ICALL,X,Y)
IF(ICALL.EQ.3) GO TO 26
WRITE(6,2005) (X(I),I=1,NPTS)
WRITE(6,2010) (Y(I),I=1,NPTS)
CALL OBJCON(X,Y,OBJ,C)
IF(ICALL.EQ.4) RETURN
ICALL=3
26 CONTINUE
KPARAM=KPARAM*1
IF(KPARAM.LE.NPARAM) GO TO 20
ICALL=4
RETURN
C
C ICALC = 3 CONMIN TERMINATION AND FINAL SOLUTION DETERMINATION
C

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200 CONTINUE
JCALL=JCALL*1
IF(IOPT.NE.3 .OR. JCALL.EQ.2) GO TO 30
NONLIN=.FALSE.
RETURN
30 CONTINUE
LTRACE=1
CALL DESVAR(VV,V,IOV,NDV,ICALL,KPARAM)
CALL BLADE(1)
CALL TSONIC
CALL XY(X,Y)
WRITE(6,1050) (XMSP(K,1),XTHSP(K,1),XMSP(K,2),XTHSP(K,2),K=1,13)
CALL OBJCON(X,Y,OBJ,C)
WRITE(6,1030) OBJ
WRITE(6,1035) (C(I),I=1,NCN)
IF(IOPT.EQ.1) RETURN
WRITE(6,2005) (X(I),I=1,NPTS)
WRITE(6,1040) LTRACE,(Y(I),I=1,NPTS)
CALL PERVAR(Q0,Q1,Q2,V,ICALL,KPARAM)
CALL PERTRB(ICALL,X,Y)
RETURN
C
1000 FORMAT(1H1,35X,43H--- INPUT FOR CONTROL SUBROUTINE ANALIZ ---)
1005 FORMAT(10I5)
1010 FORMAT (1I0,3F10.6)
1020 FORMAT(8F10.0)
1025 FORMAT(6A10)
1030 FORMAT (37H1FINAL OBJECTIVE COMPUTED BY TSONIC =,F10.6//)
1035 FORMAT(1H0,23HFINAL CONSTRAINT VALUES/10X,5HBLTK5,7X,5HDIFFP,
* 6X,6HTECLSR/5X,4E12.5)
1040 FORMAT(////* LTRACE =,I3//* Y ARRAY BEFORE PERTRB CALL*/
* (5X,5F12.3))
1045 FORMAT(////* LTRACE =,I3//* Y ARRAY AFTER PERTRB CALL*/
* (5X,5F12.3))
1050 FORMAT(////12X,*SURF 1*,29X,*SURF 2*/
* 5X,*XMSP*,11X,*XTHSP*,15X,*XMSP*,11X,*XTHSP*/
* (2E15.5,5X,2E15.5))
1055 FORMAT(//1H0,4X,18HCONTROL PARAMETERS/
* 1H0,9X,6HIOPT =,I3,10X,5HNDV =,I3,10X,5HNCN =,I3,
* 10X,8HITMAX3 =,I3)
1060 FORMAT(//1H0,4X,25HCONSTANT BLADE PARAMETERS/
* 1H0,9X,2HNB,7X,1HR,7X,3HALP,7X,5HSOLID/I12,3F10.4)
1065 FORMAT(//1H0,4X,25HVARIBLE BLADE PARAMETERS/
* 1H0,9X,4HKICR,6X,4HKOCR,8X,1HT,8X,2HZM,8X,1HP,9X,3HTMX,
* 6X,4HTLE,6X,4HTTE/5X,8F10.4)
1070 FORMAT(//1H0,4X,23HACTIVE DESIGN VARIABLES/1H0,9X,6A10)
1072 FORMAT(5X,6F10.4)
1075 FORMAT(//1H0,4X,7HCALB =,I2,6X,7HPSTEP =,F6.3)
1080 FORMAT(1H0,4X,6HDVCALB/6I12)
1085 FORMAT(3X,6F12.4)
2000 FORMAT(1H1,// 46X,39H*** INPUT FOR BLADE ELEMENT PROGRAM *** // ANALI164
*/ 49X,5HINLET,4X,6HOUTLET,4X,6HTRANS, 4X,7HMAX.TH, 3X,6HIN/OUT,5X, ANALI166
* 4HMAX, 6X,4HL.E, 6X,4HT.E. / 10X,3HND, 6X,5HINLET,5X,4HCOHE,4X, ANALI167
* 8HSOLIDITY,4X,5HBLADE,5X,5HBLADE,5X,4HLOC, 6X,4HLOC, 5X,7HTURNINGANALI168
* 3X,6HTHICK, 5X,4HRAD, 6X,4HRAD. / 8X,6HBLADES,4X,6HRADIUS,5X, ANALI169
* 5HANGLE, 15X,5HANGLE,5X,5HANGLE,4X,6H/CHORD,4X,6H/CHORD,5X,4HRATE, ANALI170
* 5X,6H/CHORD,4X,6H/CHORD,4X,6H/CHORD / 20X,3H(L),6X,5H(DEG),15X, ANALI171
* 5H(DEG),5X,5H(DEG) // 9X,I3,3X,3F10.5,F9.3,F10.4,6F10.5) ANALI172
2005 FORMAT(////* X ARRAY*/(5X,5F12.6)) ANALI173

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2010 FORMAT(1H0,* Y ARRAY*/(5X,5F12.3))
C
END
SUBROUTINE DESVAR(VV,V,NDV,NDV,ICALL,KPARAM)
C
C IDENTIFIES DESIGN VARIABLES
C
REAL KICR,KOCR
COMMON /CALB/ ICALB,DVCALB(6),PSTEP,IOPT,ITMAX3,VZERO(6)
COMMON /INPUTB/ ALP,KICR,KOCR,NB,P,R,SOLID,T,THLE,THTE,TMX,ZM
DIMENSION VV(12),V(1),IDV(1)
DO 10 I=1,NDV
J=IDV(I)
VV(J)=V(I)
10 CONTINUE
IF(ICALL.NE.3) GO TO 20
K=IDV(KPARAM)
IF(ICALB.EQ.0) VV(K)=(1.0*PSTEP)*VV(K)

IF(ICALB.EQ.0) VV(K)=(1.0*PSTEP)*VV(K)
IF(ICALB.GT.0) VV(K)=DVCALB(KPARAM)
20 CONTINUE
KICR=VV(1)
KOCR=VV(2)
T =VV(3)
ZM =VV(4)
P =VV(5)
TMX =VV(6)
THLE=VV(7)
THTE=VV(8)
RETURN
END
SUBROUTINE PERVAR(Q0,Q1,Q2,V,ICALL,KPARAM)
C
C SETS VALUES OF DESIGN VARIABLES FOR USE IN
C PERTURBATION SOLUTION CALCULATION.
C
DIMENSION Q0(1),Q2(1),V(1)
COMMON /CALB/ ICALB,DVCALB(6),PSTEP,IOPT,ITMAX3,VZERO(6)
IF (ICALL .GT. 2) GO TO 20
DO 10 I=1,6
10 Q0(I)=V(I)
RETURN
20 IF (ICALL .GT. 3) GO TO 30
IF(ICALB.EQ.0) Q1=(1. * PSTEP)*V(KPARAM)
IF(ICALB.GT.0) Q1=DVCALB(KPARAM)
RETURN
30 DO 40 I=1,6
4 Q2(I)=5(I)
RETURN
40 Q2(I)=V(I)
RETURN
END
SUBROUTINE XY(X,Y)
C
C DETERMINES SURFACE VELOCITY AND SURFACE COORDINATE ARRAYS
C
COMMON /VARCOM/ RDUH(400),WMB(100,2),SDUH(400),IDUH(100)
COMMON /MVIORH/ XMH(100)
COMMON /MBIMBO/ MBI,MBO
ANALI174 DIMENSION X(200),Y(200)
ANALI175 ND2=MBO-MBI-1
ANALI176 DO 10 I=1,ND2
DESVAR 2 X(I)=XMH*(MBO-I)
DESVAR 3 X(ND2+I)=XMH*(MBI+I)
DESVAR 4 Y(I)=WMB*(ND2-I,2)
DESVAR 5 10 Y(ND2+I)=WMB*(MBI+I,1)
DESVAR 6 RETUPH
DESVAR 7 END
DESVAR 8 SUBROUTINE OBJCOM(X,Y,DIFFS,C)
DESVAR 9 REAL KICR,KOCR
DESVAR 10 COMMON/INPUTA/ XHSP(50,2),XTHSP(50,2)
DESVAR 11 COMMON /INPUTB/ALP,KICR,KOCR,NB,P,R,SOLID,T,THLE,THTE,TMX,ZM
DESVAR 12 COMMON /MBIMBO/ MBI,MBO
DESVAR 13 COMMON/HIHO/WI,W0
DESVAR 14 COMMON/VARCOM/ADUM(400),WMB(100,2),BDUH(400),IDUH(100)
DESVAR 15 DIMENSION X(200),Y(200),C(5)
DESVAR 16
C
C CALCULATION OF OBJECTIVE FUNCTION
C
ND2=MBO-MBI-1
DIFFS=Y(ND2+1)
ND21=ND2-1
DO 10 I=1,ND21
10 IF(Y(ND2+I).GT.DIFFS) DIFFS=Y(ND2+I)
WRITE(6,1000) DIFFS,W0
DIFFS=DIFFS/W0
WRITE(6,1010) DIFFS
C
C CONSTRAINT NO. 1 - BLADE THICKNESS
C
BCHORD=2.*3.1415927*R*SOLID/FLOAT(NB)
TEDIAM=2.*THTE*BCHORD
DTHIN=1.E10
DO 20 I=2,12
DRTH=(XTHSP(I,1)-XTHSP(I,2))*R
DZ=XHSP(I,1)-XHSP(I,2)
DT=SQR(DRTH*DRTH+DZ*DZ)
TKODTE=(DT-TEDIAM)/TEDIAM
20 IF(TKODTE.LT.DTHIN) DTHIN=TKODTE
BLTKS=DTHIN
WRITE(6,1020) BLTKS
C(1)=BLTKS
C
C CONSTRAINT NO. 2 - PRESSURE SURFACE DIFFUSION
C
A=ND2/2
B=2.*ND2/3
N12=INT(A)
N23=INT(B)
YMAX=Y(ND2)
YMIN=YMAX
DO 30 I=N12,ND2
30 IF(Y(I).GT.YMAX) YMAX=Y(I)
DO 40 I=2,N23
40 IF(Y(I).LT.YMIN) YMIN=Y(I)
DIFFP=YMAX/YMIN
WRITE(6,1030) YMAX,YMIN,DIFFP
C(2)=DIFFP
C
XY 2
XY 3
XY 4
XY 5
XY 6
XY 7
XY 8
XY 9
XY 10
XY 11
XY 12
XY 13
XY 14
XY 15
XY 16
XY 17
OBJCON 2
OBJCON 3
OBJCON 4
OBJCON 5
OBJCON 6
OBJCON 7
OBJCON 8
OBJCON 9
OBJCON10
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C   CONSTRAINT NO. 3 - TRAILING EDGE CLOSURE
C
      NI=2*(MBO-MBI)-3
      TECLSR=(Y(NI)-Y(2))/80.
      WRITE (6,1040) Y(NI),Y(2),TECLSR
      C(3)=TECLSR
C
      RETURN
1000 FORMAT(////* OUTPUT FROM OBJCON*/1H0,3X,
*   * OBJECTIVE FUNCTION*,3X,*DIFFS   =*,E12.5/
*   * 25X,*MO   =*,E12.5)
1010 FORMAT (25X,*DIFFS/MO =*,E12.5)
1020 FORMAT(1H0,3X,*CONSTRAINT 1*, 9X,*BLTKS   =*,E12.5)
1030 FORMAT(1H0,3X,*CONSTRAINT 2*, 9X,*YMAX   =*,E12.5/
*   * 25X,*YMIN   =*,E12.5/
*   * 25X,*DIFFP   =*,E12.5)
1040 FORMAT(1H0,3X,*CONSTRAINT 3*, 5X,*MBO(MBO-2,1) =*,E12.5/
*   * 21X,*MBO(MBO-2,2) =*,E12.5/
*   * 25X,*TECLSR   =*,E12.5)
      END
      SUBROUTINE PERTRB (ICALL,X,Y)
C ***** SUBROUTINE PERTURB *****
C
C   ICALL=1 ... READ INPUT AND PRINT CONTROL PARAMETERS.
C
C   ICALL=2 ... PERFORM CALCULATIONS ON BASE SOLUTION.
C
C   ICALL=3 ... PERFORM CALCULATIONS ON CALIBRATION SOLUTION.
C
C   ICALL=4 ... RETURN PERTURBATION SOLUTION TO CALLING
      SUBROUTINE.
C *****
C
      DIMENSION XLOC0(6),XLOC1(6),XLOC2(6),XLOC3(6),XFIX0(8),XFIX1(8)
      DIMENSION LCR0(4),LCR1(4),LCR2(4),LCR3(4),ISEQ0(8),ISEQ1(8)
      DIMENSION HEAD0(5),HEAD1(5),HEAD2(5),HEAD3(5)
      DIMENSION XOUT(8),DEL1(10),ORD(10),X(200),Y(200)
      DIMENSION FLAG(8),STRING(100),STRUNI(100)
      REAL M0,M1,M2
      COMMON /COEFF/ C(10,7),D(10,7),DELX(200)
      COMMON /HEAD/ TITLE(8),JOBKEY
      COMMON /PARAM/ PARNAM(10),LSELECT(6),LUNIT,LPL0T,NSELECT,A,B,VNAM(2)
      COMMON /PERT/ Q0(10),Q1,Q2(10),M0,M1,M2,N,KPARAM,NPARAM,LTRACE
      COMMON /MINMAX/ YMIN,YMAX,YCR2
      COMMON /SAVE/ XCSAVE(10,200),YCSAVE(10,200)
      COMMON /XY/ XBASE(200),XCALB(200),XPERT(200),XAERO(200),
      X UNIT(200),YBASE(200),YCALB(200),YPERT(200),YAERO(200),
      YINTP(200),YPRTI(200),DUMMY(200)
      COMMON /XUYU/ XUSAVE(10,200),YUNIT(10,200)
      LEVEL 2, XCSAVE,YCSAVE,XUSAVE,YUNIT,C,D,DELX
      LEVEL 2, XBASE,XCALB,XPERT,XAERO,XUNIT,YBASE,YCALB,YPERT,YAERO,
      YINTP,YPRTI,DUMMY
      DATA LTERM/0/, L CORR/0/
      DATA HEAD0 /4HBASE,4H SOL,4HUTIO,4HN: 4H /,
      X HEAD1 /4HCALI,4HBRAT,4HION,4HSOLN,4H: /,
      X HEAD2 /4HPERT,4HURBA,4HTION,4H SOL,4HN: /,
      X HEAD3 /4HAERO,4HDYNA,4HHIC,4HSOLN,4H: /
      DATA ORD /5H 1ST ,5H 2ND ,5H 3RD ,5H 4TH ,
OBJCON53 Z 5H 5TH ,5H 6TH ,5H 7TH ,5H 8TH ,5H 9TH ,5H10TH /
OBJCON54 C
OBJCON55 C*****
OBJCON56 C
OBJCON57 C USER-SUPPLIED STATEMENT FUNCTION YCRIT(Z) DETERMINES CRITICAL
OBJCON58 C VALUES OF FLOW VARIABLE YCRIT AS FUNCTION OF FLOW PARAMETER Z.
OBJCON59 C IGRAD (+1 OR -1) IS THE USER-SUPPLIED ALGEBRAIC SIGN OF DYCRIT/DX
OBJCON60 C USED IN LOCATING THE CRITICAL POINT.
OBJCON61 C
OBJCON62 C IN THE PRESENT VERSION OF THE CODE, YCRIT REPRESENTS THE FULL-
OBJCON63 C POTENTIAL CRITICAL PRESSURE COEFFICIENT FOR AIR (GAMMA = 1.4), Z
OBJCON64 C IS THE FREE STREAM MACH NUMBER, AND IGRAD CORRESPONDS TO POSITIVE
OBJCON65 C PRESSURE GRADIENT (+1).
OBJCON66 C
OBJCON67 C YCRIT(Z)=2.0*((1.2+0.4*Z**2)/2.4)**(1.4/0.4)-1.0/(1.4*Z**2)
OBJCON68 C IGRAD=1
OBJCON69 C
OBJCON70 C*****
OBJCON71 C GO TO (501,502,503,504),ICALL
OBJCON72 C
PERTRB 2 C .....INPUT CONTROL, GEOMETRY, AND STRAINING PARAMETERS.
PERTRB 3 C
PERTRB 4 C 501 CALL INPUT (NPARAM)
PERTRB 5 C
PERTRB 6 C .....WRITE TITLE AND INPUT PARAMETERS.
PERTRB 7 C
PERTRB 8 C WRITE(6,1005)
PERTRB 9 C WRITE (6,1000) TITLE
PERTRB10 C WRITE (6,1010) N,A,B,NPARAM
PERTRB11 C
PERTRB12 C NFIX=NSELECT+2
PERTRB13 C NSEG=NFIX-1
PERTRB14 C
PERTRB15 C .....PRINT INFORMATION REGARDING STRAINING TO BE USED.
PERTRB16 C
PERTRB17 C WRITE (6,1020) NFIX
PERTRB18 C WRITE (6,1040)
PERTRB19 C DO 20 I=1,NSELECT
PERTRB20 C IF (LSELECT(I) .EQ. 1) WRITE (6,1050) VNAM
PERTRB21 C IF (LSELECT(I) .EQ. 2) WRITE (6,1060) VNAM
PERTRB22 C IF (LSELECT(I) .LE. 2) GO TO 20
PERTRB23 C L CORR=1
PERTRB24 C LPR=LSELECT(I)-2
PERTRB25 C WRITE (6,1070) VNAM,ORD(LPR)
PERTRB26 C 20 CONTINUE
PERTRB27 C RETURN
PERTRB28 C
PERTRB29 C .....BEGIN CALCULATIONS ON BASE SOLUTION.
PERTRB30 C
PERTRB31 C 502 YCR0=YCRIT(M0)
PERTRB32 C WRITE (6,1080) HEAD0
PERTRB33 C WRITE (6,1090) VNAM
PERTRB34 C WRITE (6,1100) M0
PERTRB35 C IF (NPARAM .EQ. 1) WRITE (6,1110) Q0(1),PARNAM(1)
PERTRB36 C IF (NPARAM .GT. 1) WRITE (6,1120) (K,Q0(K),PARNAM(K),K=1,NPARAM)
PERTRB37 C WRITE (6,1130) VNAM,YCR0
PERTRB38 C
PERTRB39 C .....NORMALIZE X COORDINATES AND LOCATE MINIMUM, MAXIMUM, AND CRITICAL
PERTRB40 C POINTS FOR BASE SOLUTION.
PERTRB41 C

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CALL COPY12 (N,X,XBASE)
CALL COPY12 (N,Y,YBASE)
CALL SCALE (N,XBASE,1,A,B)
CALL LOCATE (N,XBASE,YBASE,YCRO,IGRAD,LMNO,LMX0,NCRO,LCRO,XLOCO)
YBCHIN=YBASE(LMNO)
YBCHMAX=YBASE(LMX0)
WRITE (6,1140)
WRITE (6,1150)
CALL UPLOW (A,B,XLOCO,6,NCRO*2,XOUT,FLAG)
WRITE (6,1160) XOUT(1),FLAG(1),LMNO,XOUT(2),FLAG(2),LMX0
IF (NCRO .GT. 0) WRITE (6,1170) NCRO,
% (ORD(I),XOUT(I+2),FLAG(I+2),LCRO(I),I=1,NCRO)
C
C.....LOAD SELECTED STRAINING POINTS INTO FIXED-POINT ARRAY FOR BASE
C SOLUTION.
C
C
C XFIX0(1)=0.0
C XFIX0(NFIX)=1.0
C DO 50 I=1,NSELECT
C XFIX0(I+1)=XLOCO(LSELECT(I))
C 50 CONTINUE
C
C.....ARRANGE SELECTED FIXED POINTS IN A MONOTONE SEQUENCE.
C
C CALL SORT (NFIX,XFIX0,ISEQ0)
C WRITE (6,1200)
C WRITE (6,1150)
C CALL UPLOW (A,B,XFIX0,8,NFIX,XOUT,FLAG)
C WRITE (6,1210) (I,XOUT(I),FLAG(I),I=1,NFIX)
C RETURN
C
C.....BEGIN CALCULATIONS ON CALIBRATION SOLUTIONS.
C
C 503 K=KPARAM
C YCR1=YCPII(M1)
C DEL1(K)=Q1-Q0(K)
C CALL COPY12 (N,X,XCALB)
C CALL COPY12 (N,Y,YCALB)
C CALL COPYVA (1,N,K,XCALB,XCSAVE)
C CALL COPYVA (1,N,K,YCALB,YCSAVE)
C IF (NPARAM .EQ. 1) WRITE (6,1080) HEAD1
C IF (NPARAM .GT. 1) WRITE (6,1220) ORD(K),HEAD1
C WRITE (6,1090) VNAM
C WRITE (6,1230) M1
C IF (NPARAM .GT. 1) WRITE (6,1240)
C DO 60 KK=1,NPARAM
C IF (NPARAM .EQ. 1) WRITE (6,1250) Q1,PARNAM(1)
C IF (NPARAM .GT. 1 .AND. KK .EQ. K) WRITE (6,1260) KK,Q1,PARNAM(KK)
C IF (KK .NE. K) WRITE (6,1270) KK,Q0(KK),PARNAM(KK)
C 60 CONTINUE
C WRITE (6,1130) VNAM,YCR1
C
C.....NORMALIZE X COORDINATES AND LOCATE MINIMUM, MAXIMUM, AND CRITICAL
C POINTS FOR KTH CALIBRATION SOLUTION.
C
C CALL SCALE (N,XCALB,1,A,B)
C CALL LOCATE (N,XCALB,YCALB,YCR1,IGRAD,LMN1,LMX1,NCR1,LCR1,XLOCI)
C YTHIN=YCALB(LMN1)
C YTHMAX=YCALB(LMX1)
C IF (YTHIN .LT. YBCHIN) YBCHIN=YTHIN
PERTR102 IF (YTHMAX .GT. YBCHMAX) YBCHMAX=YTHMAX
PERTR103 WRITE (6,1140)
PERTR104 WRITE (6,1150)
PERTR105 CALL UPLOW (A,B,XLOCI,6,NCR1*2,XOUT,FLAG)
PERTR106 WRITE (6,1160) XOUT(1),FLAG(1),LMN1,XOUT(2),FLAG(2),LMX1
PERTR107 IF (NCR1 .GT. 0) WRITE (6,1170) NCR1,
PERTR108 % (ORD(I),XOUT(I+2),FLAG(I+2),LCR1(I),I=1,NCR1)
PERTR109
C
C.....CHECK FOR INVALID STRAINING SPECIFICATION.
C
C ICOUNT=0
C DO 70 I=1,NSELECT
C IF (LSELECT(I) .LE. 2) GO TO 70
C ICOUNT=ICOUNT+1
C IF (NCRO .NE. NCR1) LTERM=1
C 70 CONTINUE
C
C.....STOP EXECUTION IF CRITICAL POINTS ARE TO BE USED IN STRAINING AND
C NUMBER OF CRITICAL POINTS IN BASE AND CALIBRATION SOLUTIONS ARE
C UNEQUAL.
C
C IF (LTERM .EQ. 1) GO TO 900
C
C.....STOP EXECUTION IF NUMBER OF CRITICAL POINTS SELECTED EXCEEDS
C NUMBER ACTUALLY LOCATED.
C
C IF (ICOUNT .GT. NCRO) GO TO 905
C
C.....LOAD SELECTED STRAINING POINTS INTO FIXED-POINT ARRAY FOR KTH
C CALIBRATION SOLUTION.
C
C XFIX1(1)=0.0
C XFIX1(NFIX)=1.0
C DO 100 I=1,NSELECT
C XFIX1(I+1)=XLOCI(LSELECT(I))
C 100 CONTINUE
C
C.....ARRANGE SELECTED FIXED POINTS IN A MONOTONE SEQUENCE.
C
C CALL SORT (NFIX,XFIX1,ISEQ1)
C WRITE (6,1200)
C WRITE (6,1150)
C CALL UPLOW (A,B,XFIX1,8,NFIX,XOUT,FLAG)
C WRITE (6,1210) (I,XOUT(I),FLAG(I),I=1,NFIX)
C
C.....STOP EXECUTION IF ORDER OF OCCURRENCE OF CRITICAL POINTS IN BASE
C AND CALIBRATION SOLUTIONS DOES NOT CORRESPOND.
C
C DO 110 I=1,NFIX
C IF (ISEQ0(I) .NE. ISEQ1(I)) GO TO 910
C 110 CONTINUE
C
C.....COMPUTE COEFFICIENTS IN KTH UNIT STRAINING OF XBASE
C
C XSTR = C(K,I) + D(K,I)*XBASE, I=1,2, ... ,NSEG,
C
C WHERE NSEG IS THE NUMBER OF LINEAR SEGMENTS.
C
C DO 130 I=1,NSEG
C CUMI=XFIX1(I)*XFIX0(I+1)-XFIX1(I+1)*XFIX0(I)
PERTR162 PERTR162
PERTR163 PERTR163
PERTR164 PERTR164
PERTR165 PERTR165
PERTR166 PERTR166
PERTR167 PERTR167
PERTR168 PERTR168
PERTR169 PERTR169
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PERTR221 PERTR221

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<pre> DHUM=XFIX(I+1)-XFIX(I) DEHOM=XFIX0(I+1)-XFIX0(I) C(K,I)=CHUM/DEHOM D(K,I)=DNUM/DEHOM 130 CONTINUE C C.....DETERMINE KTH UNIT STRAINING OF XBASE. C CALL STRAIN (N,K,NSEG,XFIX0,XBASE,1,0) DO 140 I=1,N 140 XUNIT(I)=XBASE(I)*DELX(I) C C.....INTERPOLATE CALIBRATION SOLUTION TO BASE FLOW POINTS CORRESPONDING C TO UNIT STRAINING. C CALL INTERP (N,XCALB,YCALB,XUNIT,YINTP) C C.....CORRECT VALUES ON EITHER SIDE OF CRITICAL POINTS, IF THESE ARE C USED IN STRAINING. C IF (LCORR .EQ. 0) GO TO 160 DO 150 I=1,NCR1 YINTP(LCR0(I))=YCALB(LCR1(I)) YINTP(LCR0(I)+1)=YCALB(LCR1(I)+1) 150 CONTINUE 160 CONTINUE C C.....DETERMINE THE KTH UNIT PERTURBATION. C DO 170 I=1,N 170 YUNIT(K,I)=(YINTP(I)-YBASE(I))/DEL1(K) C C.....SAVE UNIT STRAINING IF REQUIRED FOR LATER PRINTOUT. C IF (LUNIT .EQ. 0) GO TO 180 CALL SCALE (N,XUNIT,2,A,B) CALL COPYVA (1,H,K,XUNIT,XUSAVE) 180 IF (KPARAM .LT. NPARAM) RETURN C C.....PRINT UNIT PERTURBATION(S) AND UNIT STRAINING(S) IF LUNIT .NE. 0. C IF (LUNIT .EQ. 0) RETURN CALL SCALE (N,XBASE,2,A,B) IRPT=0 IF (NPARAM .GT. 5) IRPT=1 KSTART=1 KSTOP=5 IF (KSTOP .GT. NPARAM) KSTOP=NPARAM GO TO 200 190 KSTART=6 KSTOP=NPARAM 200 CONTINUE WRITE (6,1280) VNAM IF (NPARAM .GT. 1) WRITE (6,1290) KSTART,KSTOP IF (NPARAM .EQ. 1) WRITE (6,1300) IF (NPARAM .EQ. 1) GO TO 210 NUM=KSTOP-KSTART+1 IF (NUM .EQ. 1) WRITE (6,1310) (ORD(K),K=KSTART,KSTOP) IF (NUM .EQ. 2) WRITE (6,1320) (ORD(K),K=KSTART,KSTOP) IF (NUM .EQ. 3) WRITE (6,1330) (ORD(K),K=KSTART,KSTOP) </pre>	<pre> PERTR222 IF (NUM .EQ. 4) WRITE (6,1340) (ORD(K),K=KSTART,KSTOP) PERTR223 IF (NUM .EQ. 5) WRITE (6,1345) (ORD(K),K=KSTART,KSTOP) PERTR224 210 CONTINUE PERTR225 CALL FILL (1,0,STPUNI) PERTR226 KLAST=20*(KSTOP-KSTART+1) PERTR227 WRITE (6,1350) (STRUH(I),K=1,KLAST) PERTR228 WRITE (6,1360) PERTR229 DO 220 I=1,N PERTR230 220 WRITE (6,1370) I,XBASE(I),(XUSAVE(K,I),YUNIT(K,I),K=KSTART,KSTOP) PERTR231 IF (IPPT .EQ. 0) GO TO 230 PERTR232 IRPT=0 PERTR233 GO TO 190 PERTR234 230 CALL SCALE (N,XBASE,1,A,B) PERTR235 RETURN PERTR236 C PERTR237 C.....CONSTRUCT PERTURBATION SOLUTIONS FOR REQUIRED CASES. PERTR238 C PERTR239 504 YCR2=YCRIT(M2) PERTR240 YCR3=YCR2 PERTR241 CALL COPY12 (N,X,XAERO) PERTR242 IF (LTRACE .EQ. 1) CALL COPY12 (N,Y,YAERO) PERTR243 C PERTR244 C.....INITIALIZE STRAINED COORDINATE AND PERTURBATION SOLUTION. PERTR245 C PERTR246 DO 250 I=1,N PERTR247 XPERT(I)=XBASE(I) PERTR248 250 YPERT(I)=YBASE(I) PERTR249 C PERTR250 C.....ADD IN CONTRIBUTIONS FROM ALL PERTURBATIONS. PERTR251 C PERTR252 DO 270 K=1,NPARAM PERTR253 DEL2=Q2(K)-Q0(K) PERTR254 DEL21=DEL2/DEL1(K) PERTR255 CALL STRAIN (N,K,NSEG,XFIX0,XBASE,DEL21) PERTR256 DO 260 I=1,N PERTR257 XPERT(I)=XPERT(I)+DELX(I) PERTR258 260 YPERT(I)=YPERT(I)+DEL2*YUNIT(K,I) PERTR259 270 CONTINUE PERTR260 C PERTR261 C.....ADJUST VALUES NEAR CRITICAL POINT FOR MONOTONE BEHAVIOR. PERTR262 C PERTR263 IF (LCORR .EQ. 1) CALL MONO (NCR0,LCR0,XPERT,YPERT) PERTR264 C PERTR265 C.....INTERPOLATE SOLUTION IN STRAINED COORDINATES TO BASE X VALUES. PERTR266 C PERTR267 CALL INTERP (N,XPERT,YPERT,XBASE,DUMMY) PERTR268 CALL COPY21 (N,DUMMY,Y) PERTR269 C PERTR270 IF (LTRACE.EQ.0) RETURN PERTR271 C PERTR272 C.....COMPARISON OF PERTURBATION AND AERODYNAMIC SOLUTIONS. PERTR273 C PERTR274 C.....LOCATE MINIMUM, MAXIMUM, AND CRITICAL POINTS IN PERTURBATION PERTR275 C SOLUTION. PERTR276 C PERTR277 C PERTR278 CALL SCALE (N,XPERT,2,A,B) PERTR279 CALL SCALE (N,XPERT,1,A,B) PERTR280 CALL LOCATE (N,XPERT,YPERT,YCR2,IGRAD,LMH2,LMX2,HC2,LCR2,XLOC2) PERTR281 YMH=YPERT(LMH2) </pre>	<pre> PERTR282 PERTR283 PERTR284 PERTR285 PERTR286 PERTR287 PERTR288 PERTR289 PERTR290 PERTR291 PERTR292 PERTR293 PERTR294 PERTR295 PERTR296 PERTR297 PERTR298 PERTR299 PERTR300 PERTR301 PERTR302 PERTR303 PERTR304 PERTR305 PERTR306 PERTR307 PERTR308 PERTR309 PERTR310 PERTR311 PERTR312 PERTR313 PERTR314 PERTR315 PERTR316 PERTR317 PERTR318 PERTR319 PERTR320 PERTR321 PERTR322 PERTR323 PERTR324 PERTR325 PERTR326 PERTR327 PERTR328 PERTR329 PERTR330 PERTR331 PERTR332 PERTR333 PERTR334 PERTR335 PERTR336 PERTR337 PERTR338 PERTR339 PERTR340 PERTR341 </pre>
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YMAX=YPERT(LMX2)
YPCMIN=YMIN
YPCMAX=YMAX
WRITE (6,1380)
WRITE (6,1090) VNAM
WRITE (6,1390) M2
IF (NPARAM .EQ. 1) WRITE (6,1400) Q2(1),PARNAM(1)
IF (NPARAM .GT. 1) WRITE (6,1410) (K,Q2(K),PARNAM(K),K=1,NPARAM)
WRITE (6,1130) VNAM,YCR2
WRITE (6,1140)
WRITE (6,1150)
CALL UPLOW (A,B,XLOC2,6,NCR2*2,XOUT,FLAG)
WRITE (6,1420) HEAD2,XOUT(1),FLAG(1),LMH2,XOUT(2),FLAG(2),LMX2
IF (NCR2 .GT. 0) WRITE (6,1430) NCR2,
% (ORD(I),XOUT(I+2),FLAG(I+2),LCR2(I),I=1,NCR2)
CALL SCALE (N,XBASE,2,A,B)
C
C.....LOCATE MINIMUM, MAXIMUM, AND CRITICAL POINTS IN AEROODYNAMIC
C SOLUTION.
C
CALL SCALE (N,XAERO,1,A,B)
CALL LOCATE (N,XAERO,YAERO,YCR3,IGRAD,LMN3,LMX3,NCR3,LCR3,XLOC3)
YMIN=YAERO(LMN3)
YMAX=YAERO(LMX3)
IF (YMIN .LT. YPCMIN) YPCMIN=YMIN
IF (YMAX .GT. YPCMAX) YPCMAX=YMAX
CALL UPLOW (A,B,XLOC3,6,NCR3*2,XOUT,FLAG)
WRITE (6,1420) HEAD3,XOUT(1),FLAG(1),LMN3,XOUT(2),FLAG(2),LMX3
IF (NCR3 .GT. 0) WRITE (6,1430) NCR3,
% (ORD(I),XOUT(I+2),FLAG(I+2),LCR3(I),I=1,NCR3)
CALL INTERP (N,XPERT,YPERT,XAERO,YPRTI)
CALL LOCATE (N,XAERO,YPRTI,YCR3,IGRAD,LMN3,LMX3,NCR3,LCR3,XLOC3)
YTHIN=YPRTI(LMN3)
YTHAX=YPRTI(LMX3)
IF (YTHIN .LT. YMIN) YMIN=YTHIN
IF (YTHAX .GT. YMAX) YMAX=YTHAX
CALL SCALE (N,XPERT,2,A,B)
CALL SCALE (N,XAERO,2,A,B)
CALL FILL (2,0,STRING)
WRITE (6,1440) VNAM
WRITE (6,1450) VNAM,YMAX,VNAM,YMIN,VNAM,YCR2,VNAM,VNAM
WRITE (6,1460) VNAM,VNAM,VNAM,VNAM,(STRING(I),I=1,72)
DO 280 I=1,N
CALL FILL (3,I,STRING)
280 WRITE (6,1470) I,XBASE(I),YBASE(I),XPERT(I),YPERT(I),
% XAERO(I),YAERO(I),YPRTI(I),(STRING(I),I=1,72)
C
C.....IF L PLOT .NE. 0 GENERATE PERIPHERAL PLOT OF PERTURBATION AND
C AEROODYNAMIC SOLUTIONS.
C
IF (L PLOT .EQ. 0) GO TO 320
YMIN=YBCHIN
YMAX=YBCHAX
IF (YPCMIN .LT. YMIN) YMIN=YPCMIN
IF (YPCMAX .GT. YMAX) YMAX=YPCMAX
CALL DRVPLT (N,NPARAM,YMIN,YMAX,YCR2)
320 CALL SCALE (N,XBASE,1,A,B)
RETURN
C
C.....ABNORMAL TERMINATION OF COMPUTATION.
PERTR342
PERTR343
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PERTR400
PERTR401
C
900 WRITE (6,9000)
GO TO 999
905 WRITE (6,9050)
GO TO 999
910 WRITE (6,9100)
C
999 WRITE (6,9500)
STOP
C
C.....I/O FORMAT STATEMENTS FOLLOW.
C
1000 FORMAT(1H0,132(1H*))
% 1X,1H*,25X,8A10,25X,1H*
% 1X,132(1H*)//)
1005 FORMAT(1H1,35X,37H--- INPUT FOR PERTURBATION METHOD ---//)
1010 FORMAT (1X,29H.....LIST OF INPUT PARAMETERS//
% 6X,3HN =,I4//
% 6X,3HA =,F5.1,4X,3HB =,F5.1//
% 6X,6HNPARAM =,I2//)
1020 FORMAT (1X,22H.....STRAINING OPTIONS//
% 6X,23HNUMBER OF FIXED POINTS:,I2//)
1040 FORMAT (6X,45HFIXED POINTS WILL BE AUTOMATICALLY DETERMINED//
% 6X,44HBY THE PROGRAM FOR ALL SOLUTIONS AS FOLLOWS://
% 11X,14HTWO END POINTS)
1050 FORMAT (11X,16HPOINT OF MINIMUM,1X,2A1)
1060 FORMAT (11X,16HPOINT OF MAXIMUM,1X,2A1)
1070 FORMAT (11X,2A1,6HCRT (,A5,6HPPOINT))
1080 FORMAT (1H1,26HRESULTS OF COMPUTATIONS ON,1X,5A4//)
1090 FORMAT (1X,17H.....MACH NUMBER,/
% 6X,34HVALUES OF PERTURBATION PARAMETERS,/
% 6X,17HCRTICAL VALUE OF,1X,2A1,1H://)
1100 FORMAT (11X,4HM0 =,F7.4//)
1110 FORMAT (11X,4HQ0 =,F10.4,5X,1H(,A8,1H)/)
1120 FORMAT (11X,3HQ0(,I1,3H) =,F10.4,5X,1H(,A8,1H)/)
1130 FORMAT (11X,2A1,6HCRT =,F8.4//)
1140 FORMAT (1X,47H.....LOCATIONS OF MIN., MAX., AND CRITICAL PTS.)
1150 FORMAT (3X,34H( * DENOTES POINT ON LOWER SURFACE)/)
1160 FORMAT (6X,14HMINIMUM AT X =,F7.4,A1,3X,10H(POINT NO.,I4,1H)/
% 6X,14HMAXIMUM AT X =,F7.4,A1,3X,10H(POINT NO.,I4,1H)/)
1170 FORMAT (6X,I1,1X,18HCRTICAL POINT(S)/
% (9X,A5,6HAT X =,1X,F6.4,A1,3X,
% 16H(AFTER POINT NO.,I4,1H))
1200 FORMAT (///1X,29H.....LOCATION OF FIXED POINTS)
1210 FORMAT (11X,5HXFIX(I1,3H) =,F7.4,A1)
1220 FOPHAT (1H1,26HRESULTS OF COMPUTATIONS ON,1X,A5,5A4//)
1230 FORMAT (11X,4HM1 =,F7.4//)
1240 FORMAT (2X,4H1( * DENOTES PERTURBATION FROM BASE VALUE)/)
1250 FORMAT (11X,4HQ1 =,F10.4,5X,1H(,A8,1H)/)
1260 FORMAT (9X,5H**Q1(,I1,3H) =,F10.4,5X,1H(,A8,1H)/)
1270 FORMAT (11X,3HQ1(,I1,3H) =,F10.4,5X,1H(,A8,1H)/)
1280 FORMAT (1H1,20HUNIT PERTURBATION OF,1X,2A1,1X,
% 27HAND UNIT STRAINING OF XBASE)
1290 FORMAT (26H FOR CALIBRATION SOLUTIONS,I2,1X,7HTHROUGH,I2)
1300 FORMAT (//1H )
1310 FORMAT (///19X,11H*,A5,11HCALB SOLN *,3X))
1320 FORMAT (///19X,2(1H*,A5,11HCALB SOLN *,3X))
1330 FORMAT (///19X,3(1H*,A5,11HCALB SOLN *,3X))
1340 FORMAT (///19X,4(1H*,A5,11HCALB SOLN *,3X))
1345 FOPHAT (///19X,5(1H*,A5,11HCALB SOLN *,3X))
PERTR402
PERTR403
PERTR404
PERTR405
PERTR406
PERTR407
PERTR408
PERTR409
PERTR410
PERTR411
PERTR412
PERTR413
PERTR414
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PERTR418
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PERTR420
PERTR421
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PERTR424
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PERTR458
PERTR459
PERTR460
PERTR461

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1350 FORMAT(1X,5HPOINT,4X,5HXBASE,4X,100A1)
1360 FORMAT (1X)
1370 FORMAT (1X,I4,1X,11F10.4)
1380 FORMAT (1H1,56(1H*)/1X,2H* ,
% 52HCOMPARISON OF AERODYNAMIC AND PERTURBATION SOLUTIONS,
% 2H */1X,56(1H*)//)
1390 FORMAT (11X,4HM2 =,F7.4/)
1400 FORMAT (11X,4HQ2 =,F7.4,5X,1H(,A8,1H)/)
1410 FORMAT (11X,3HQ2(I,1,3H) =,F7.4,5X,1H(,A8,1H)/)
1420 FORMAT (/6X,5A4//
% 11X,14HMINIMUM AT X =,F7.4,A1,3X,10H(POINT NO.,I4,1H)/
% 11X,14HMAXIMUM AT X =,F7.4,A1,3X,10H(POINT NO.,I4,1H))
1430 FORMAT (1H ,10X,I1,1X,18HCritical POINT(S):/
% (14X,A5,6HAT X =,F7.4,A1,3X,
% 16H(AFTER POINT NO.,I4,1H)))
1440 FORMAT (///1X,44H.....FINAL PRINTOUT AND GRAPHICAL DISPLAY OF,1X,
% 2A1)
1450 FORMAT (/72X,21HH = MAXIMUM VALUE OF,1X,2A1,1X,1H=,F8.4/
% 72X,21HL = MINIMUM VALUE OF,1X,2A1,1X,1H=,F8.4/
% 72X,21H* = CRITICAL VALUE OF,1X,2A1,1X,1H=,F8.4/
% 72X,12HP = VALUE OF,1X,2A1,1X,
% 34HPREDICTED BY PERTURBATION SOLUTION/
% 72X,12HA = VALUE OF,1X,2A1,1X,
% 23HIN AERODYNAMIC SOLUTION/
% 72X,29H# = AGREEMENT BETWEEN P AND A)
1460 FORMAT (/2X,2HPT,2X,5HXBASE,3X,2A1,4HBASE,2X,5HXPRT,3X,2A1,
% 4HPERT,2X,5HXAERO,3X,2A1,4HAERO,2X,2A1,4HPINT,1X,72A1)
1470 FORMAT (1X,I3,7F8.4,1X,72A1)
C
C.....ABNORMAL TERMINATION FORMATS FOLLOW.
C
9000 FORMAT (///1X,28HNUMBER OF CRITICAL POINTS IN/
% 1X,30HBASE AND CALIBRATION SOLUTIONS/
% 1X,31HARE UNEQUAL - CALCULATION ENDED)
9050 FORMAT (///1X,25HNUMBER OF CRITICAL POINTS/
% 1X,23HSELECTED EXCEEDS NUMBER/
% 1X,30HACTUALLY LOCATED - CALCULATION/
% 1X,5HENDED)
9100 FORMAT (///1X,28HORDER OF SPECIFIED POINTS IN/
% 1X,30HBASE AND CALIBRATION SOLUTIONS/
% 1X,39HDOES NOT CORRESPOND - CALCULATION ENDED)
9500 FORMAT (1H1)
END
SUBROUTINE COPY12 (N,XIN,XOUT)
C
C.....COPIES ELEMENTS OF VECTOR XIN (LEVEL 1) TO VECTOR XOUT (LEVEL 2).
C
DIMENSION XIN(200),XOUT(200)
LEVEL 2, XOUT
DO 10 I=1,N
10 XOUT(I)=XIN(I)
RETURN
END
SUBROUTINE COPY21 (N,XIN,XOUT)
C
C.....COPIES ELEMENTS OF VECTOR XIN (LEVEL 2) TO VECTOR XOUT (LEVEL 1).
C
DIMENSION XIN(200),XOUT(200)
LEVEL 2, XIN
DO 10 I=1,N
PERTR462 10 XOUT(I)=XIN(I)
PERTR463 RETURN
PERTR464 END
PERTR465 SUBROUTINE COPYVA (ICALL,N,K,VECTOR,ARRAY)
C
C.....COPIES ELEMENTS OF VECTOR INTO KTH ROW OF ARRAY.
C
DIMENSION VECTOR(200),ARRAY(10,200)
LEVEL 2, VECTOR,ARRAY
IF (ICALL .EQ. 2) GO TO 20
DO 10 I=1,N
10 ARRAY(K,I)=VECTOR(I)
RETURN
20 CONTINUE
DO 30 I=1,N
30 VECTOR(I)=ARRAY(K,I)
RETURN
END
SUBROUTINE DRVPLT (N,NPARAM,YMIN,YMAX,YCR2)
DIMENSION HLINE3(3),XPLOT(200),YPLT(200)
COMMON /HEAD/ ZTITLE(8),JOBKEY
COMMON /SAVE/ XCSAVE(10,200),YCSAVE(10,200)
COMMON /XY/ XBASE(200),XCALB(200),XPERT(200),XAERO(200),
% XUNIT(200),YBASE(200),YCALB(200),YPERT(200),YAERO(200),
% YINTP(200),YPRTI(200),DUMMY(200)
LEVEL 2, XCSAVE,YCSAVE
LEVEL 2, XBASE,XCALB,XPERT,XAERO,XUNIT,YBASE,YCALB,YPERT,YAERO,
% YINTP,YPRTI,DUMMY
DATA NPLT /0/
IF (NPLT .EQ. 0) CALL BETA
MIN=10.0*(YMIN-0.1)
MAX=10.0*(YMAX+0.1)
YMIN=0.1*MIN
YMAX=0.1*MAX
DO 20 K=1,NPARAM
NPLT=NPLT+1
ENCODE (22,1010,HLINE3) K,NPARAM
CALL BGNPL (-1)
CALL MIXALF ('L/CST')
CALL MX3ALF ('INSTR','%')
CALL SIMPLX
CALL TITLE (1H ,1,1HX,1,"ZE0.5JCZEX(P)%",100,6.0,8.0)
CALL HEADIN ("PLOT (OF) C%L0.25H0.7(P)%",100,3,3)
CALL HEADIN (JOBKEY,9,2,3)
CALL HEADIN (HLINE3,22,2,3)
CALL GRAF (0.0,"SCALE",1.0,YMAX,"SCALE",YMIN)
CALL FRAME
IF (YCR2 .GT. YMAX) GO TO 10
CALL RLVEC (0.0,YCR2,0.2,YCR2,0000)
CALL RLMESS ("C%L(P)%BE(*)%",100,0.21,YCR2)
10 CONTINUE
CALL DASH
CALL COPY21 (N,XBASE,XPLOT)
CALL COPY21 (N,YBASE,YPLT)
CALL CURVE (XPLOT,YPLT,N,0)
CALL RESET ("DASH")
CALL DOT
CALL COPYVA (2,N,K,XCALB,XCSAVE)
CALL COPYVA (2,N,K,YCALB,YCSAVE)
CALL COPY21 (N,XCALB,XPLOT)
COPY21 9
COPY21 10
COPY21 11
COPY21 2
COPY21 3
COPY21 4
COPY21 5
COPY21 6
COPY21 7
COPY21 8
COPY21 9
COPY21 10
COPY21 11
COPY21 12
COPY21 13
COPY21 14
COPY21 15
COPY21 16
COPY21 17
COPY21 18
COPY21 19
COPY21 20
COPY21 21
COPY21 22
COPY21 23
COPY21 24
COPY21 25
COPY21 26
COPY21 27
COPY21 28
COPY21 29
COPY21 30
COPY21 31
COPY21 32
COPY21 33
COPY21 34
COPY21 35
COPY21 36
COPY21 37
COPY21 38
COPY21 39
COPY21 40
COPY21 41
COPY21 42
COPY21 43

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CALL COPY21 (N,YCALB,YPLOT)
CALL CURVE (XPLOT,YPLOT,N,0)
CALL RESET ("DOT")
CALL MARKER (1)
CALL COPY21 (N,XPRT,XPLOT)
CALL COPY21 (N,YPERT,YPLOT)
CALL CURVE (XPLOT,YPLOT,N,-1)
CALL RESET ("MARKER")
CALL COPY21 (N,XAERO,XPLOT)
CALL COPY21 (N,YAERO,YPLOT)
CALL CURVE (XPLOT,YPLOT,N,0)
CALL ENDPL (NPLOT)
20 CONTINUE
1010 FORMAT (16HCALIBRATION NO. ,I1,4H OF ,I1)
RETURN
END
SUBROUTINE FILL (ICALL,I,STRING)
C
C.....FILLS ARRAY STRING WITH CHARACTERS FOR TABLE HEADINGS AND PRINTER
C PLOTS.
C
DIMENSION STRING(100),UNIT(20)
COMMON /PARAM/ PARNAM(10),LSELCT(6),LUNIT,LPLLOT,NSELCT,A,B,VNAM(2)
COMMON /MINMAX/ YMIN,YMAX,YCR2
COMMON /XY/ XBASE(200),XCALB(200),XPRT(200),XAERO(200),
X XUNIT(200),YBASE(200),YCALB(200),YPERT(200),YAERO(200),
X YINTP(200),YPRTI(200),DUMMY(200)
LEVEL 2, XBASE,XCALB,XPRT,XAERO,XUNIT,YBASE,YCALB,YPERT,YAERO,
X YINTP,YPRTI,DUMMY
DATA IENT /0/
DATA STAR/1H*/ , P/1HP/ , AA/1HA/ , DASH/1H-/ , H/1HH/ , EL/1HL/ ,
X BLANK/1H / , DOLLAR/1H$/
DATA UNIT /1HX,1HS,1HT,1HR,1HU,1HN,1HI,1HT,1H ,1H ,
X 1H ,1H ,1H ,1HU,1HN,1HI,1HT,1H ,1H ,1H /
GO TO (10,30,50), ICALL
10 IENT=IENT+1
IF (IENT.GT. 1) RETURN
UNIT(12)=VHAM(1)
UNIT(13)=VHAM(2)
DO 20 J=1,20
DO 20 K=1,5
II=J+20*(K-1)
20 STRING(II)=UNIT(J)
RETURN
30 RANGE=YMAX-YMIN
IFLAG=0
IF (YCR2.GT.YMAX .OR. YCR2.LT.YMIN) IFLAG=1
DO 40 II=1,72
40 STRING(II)=DASH
STRING(1)=H
STRING(72)=EL
IF (IFLAG.EQ.1) RETURN
NSTAR=1+(YMAX-YCR2)/RANGE*71
STRING(NSTAR)=STAR
RETURN
50 CONTINUE
DO 60 II=1,72
60 STRING(II)=BLANK
IF (IFLAG.EQ.0) STRING(NSTAR)=STAR
YP=YPRTI(I)
DRVPLT44 NPERT=1+(YMAX-YP)/RANGE*71
DRVPLT45 STRING(NPERT)=P
DRVPLT46 YC=YAERO(I)
DRVPLT47 NCHEK=1+(YMAX-YC)/RANGE*71
DRVPLT48 STRING(NCHEK)=AA
DRVPLT49 IF (NPERT .EQ. NCHEK) STRING(NPERT)=DOLLAR
DRVPLT50 RETURN
DRVPLT51 END
DRVPLT52 SUBROUTINE INPUT (NPARAM)
DRVPLT53
C INPUT FOR SUBROUTINE PERTURB IS REQUIRED IN THE FOLLOWING FORM.
C FOR DETAILS SEE ACCOMPANYING MANUAL.
C
C**** ITEM NO. 1 - ONE CARD (8A10) *****
C TITLE IDENTIFIES JOB - PRINTED AS HEADLINE ON FIRST PAGE
C OF OUTPUT. FIRST NINE CHARACTERS ARE USED TO
C IDENTIFY PERIPHERAL PLOT.
C**** ITEM NO. 2 - ONE CARD (16I5) *****
C NSELCT NUMBER OF POINTS (IN ADDITION TO END POINTS) TO BE
C HELD INVARIANT IN STRAINING.
C NOTE: 1 .LE. NSELCT .LE. 6.
C LUNIT CONTROLS WHETHER OR NOT UNIT COORDINATE STRAINING(S)
C AND UNIT PERTURBATION(S) ARE PRINTED.
C LUNIT = 0 ... NO OUTPUT
C LUNIT = 1 ... OUTPUT
C LPLLOT SPECIFIES WHETHER OR NOT AN ADDITIONAL PLOT BY A
C PERIPHERAL DEVICE IS TO BE MADE (SOFTWARE MUST BE
C SUPPLIED BY USER IN SUBROUTINE DRVPLT).
C LPLLOT = 0 ... NO PERIPHERAL PLOT
C LPLLOT = 1 ... PERIPHERAL PLOT
C**** ITEM NO. 3 - ONE CARD (16I5) *****
C LSELCT(I) ...
C ARRAY OF LENGTH 6 OF WHICH NSELCT ELEMENTS ARE READ
C IN. SPECIFIES NATURE OF POINTS TO BE HELD INVARIANT
C ACCORDING TO THE CODE
C 1 ... MINIMUM PT. HELD INVARIANT
C 2 ... MAXIMUM PT. HELD INVARIANT
C 3 ... 1ST CRITICAL PT. HELD INVARIANT
C 4 ... 2ND CRITICAL PT. HELD INVARIANT
C 5 ... 3RD CRITICAL PT. HELD INVARIANT
C 6 ... 4TH CRITICAL PT. HELD INVARIANT
C NOTE THAT THE CODE NUMBERS CAN BE ASSIGNED IN ANY
C ORDER, E.G.
C LSELCT(1) = 1
C LSELCT(2) = 3
C LSELCT(3) = 4
C IS EQUIVALENT TO

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C                                     INPUT 54
C                                     INPUT 55
C                                     INPUT 56
C                                     INPUT 57
C                                     INPUT 58
C                                     INPUT 59
C                                     INPUT 60
C                                     INPUT 61
C**** ITEM NO. 4 - ONE CARD (2A1) *****INPUT 62
C                                     INPUT 63
C      VNAM      CHARACTER STRING OF LENGTH 2 WHICH SYMBOLIZES
C                DEPENDENT VARIABLE, E.G. "CP" FOR PRESSURE
C                COEFFICIENT.
C                                     INPUT 65
C                                     INPUT 66
C                                     INPUT 67
C**** ITEM NO. 5 - ONE CARD (10A8) *****INPUT 68
C                                     INPUT 69
C      PARNAM(K) ...
C                ARRAY OF 8-CHARACTER STRINGS WHICH IDENTIFY THE
C                PARAMETERS VARIED. NPARAM ELEMENTS OF THE ARRAY
C                ARE READ IN.
C                                     INPUT 70
C                                     INPUT 71
C                                     INPUT 72
C                                     INPUT 73
C                                     INPUT 74
C**** ITEM NO. 6 - ONE CARD (8F10.6) *****INPUT 75
C                                     INPUT 76
C      A          SCALING PARAMETER (A = -X(1), WHERE X(1) IS FIRST
C                DATA POINT ON LOWER SURFACE ... SEE MANUAL).
C                                     INPUT 77
C                                     INPUT 78
C                                     INPUT 79
C      B          SCALING PARAMETER (B = X(N), WHERE X(N) IS LAST DATA
C                POINT ON UPPER SURFACE ... SEE MANUAL).
C                                     INPUT 80
C                                     INPUT 81
C                                     INPUT 82
C*****INPUT 83
C                                     INPUT 84
C                                     INPUT 85
C      COMMON /HEAD/ TITLE(8),JOBKEY
C      COMMON /PARAM/ PARNAM(10),LSELCT(6),LUNIT,LPLT,NSELCT,A,B,VNAM(2)INPUT 86
C      READ (5,900) TITLE
C      DECODE (9,950,TITLE(1)) JOBKEY
C      READ (5,1000) NSELCT,LUNIT,LPLT
C      READ (5,1000) (LSELCT(I),I=1,NSELCT)
C      READ (5,1010) VNAM
C      READ (5,1020) (PARNAM(I),I=1,NPARAM)
C      READ (5,1030) A,B
C      RETURN
C      900 FORMAT (8A10)
C      950 FORMAT (A9)
C      1000 FORMAT (16I5)
C      1010 FORMAT (2A1)
C      1020 FORMAT (10A8)
C      1030 FORMAT (8F10.6)
C      END
C      SUBROUTINE INTERP (N,X,Y,XI,YI)
C
C.....GIVEN THE SET OF POINTS X(I), Y(I), I=1,N, AND THE SET XI(J),
C      J=1,N, USES LINEAR INTERPOLATION TO COMPUTE THE SET YI(J), J=1,N.
C
C      DIMENSION X(200),Y(200),XI(200),YI(200)
C      LEVEL 2, X,Y,XI,YI
C      NM1=N-1
C      JSTART=1
C      DO 70 I=1,NM1
C      IF (XI(I) .LE. X(1)) GO TO 10
C      IF (XI(I) .GE. X(N)) GO TO 20
C                                     INPUT 87
C                                     INPUT 88
C                                     INPUT 89
C                                     INPUT 90
C                                     INPUT 91
C                                     INPUT 92
C                                     INPUT 93
C                                     INPUT 94
C                                     INPUT 95
C                                     INPUT 96
C                                     INPUT 97
C                                     INPUT 98
C                                     INPUT 99
C                                     INPUT100
C                                     INPUT101
C      INTERP 2
C      INTERP 3
C      INTERP 4
C      INTERP 5
C      INTERP 6
C      INTERP 7
C      INTERP 8
C      INTERP 9
C      INTERP10
C      INTERP11
C      INTERP12
C      INTERP13
C      GO TO 30
C      J=1
C      GO TO 60
C      J=N-1
C      GO TO 60
C      CONTINUE
C      DO 50 J=JSTART,NM1
C      IF (XI(I) .NE. X(J)) GO TO 40
C      YI(I)=Y(J)
C      GO TO 70
C      40 IF (XI(I) .GT. X(J) .AND. XI(I) .LT. X(J+1)) GO TO 60
C      50 CONTINUE
C      60 SLOPE=(Y(J+1)-Y(J))/(X(J+1)-X(J))
C      YI(I)=Y(J)+SLOPE*(XI(I)-X(J))
C      JSTART=J
C      70 CONTINUE
C      RETURN
C      END
C      SUBROUTINE LOCATE (N,X,Y,YCRIT,IGRAD,LMIN,LMAX,NCRIT,LCRIT,XLOC)
C.....OPERATES ON THE INPUT ARRAY Y, LOCATING MINIMUM AND MAXIMUM
C      VALUES, AND ALL CRITICAL POINTS (Y=YCRIT) FOR WHICH DY/DX (IN
C      PHYSICAL COORDINATES) HAS ALGEBRAIC SIGN GIVEN BY IGRAD. NCRIT
C      IS NUMBER OF CRITICAL POINTS. POINTS FOUND ARE STORED IN THE ARRAY
C      XLOC AS FOLLOWS
C
C      XLOC(1) = MINIMUM PT.
C      XLOC(2) = MAXIMUM PT.
C      XLOC(3) = CRITICAL PT. NO. 1
C      ... = ...
C      XLOC(6) = CRITICAL PT. NO. 4
C
C      DIMENSION X(200),Y(200),LCRIT(4),XCRIT(4),XLOC(6)
C      LEVEL 2, X,Y
C      COMMON /FLOREV/ IREV
C      IFLOW=-1
C      LMIN=1
C      LMAX=1
C      ISTART=2
C      IF (IREV .EQ. 0) GO TO 10
C      LMIN=2
C      LMAX=2
C      ISTART=3
C      10 CONTINUE
C      NCRIT=0
C      DO 30 I=ISTART,N
C      IF (IREV .NE. 0 .AND. I .EQ. N) GO TO 20
C      IF (Y(I) .GT. Y(LMAX)) LMAX=I
C      IF (Y(I) .LT. Y(LMIN)) LMIN=I
C      20 CONTINUE
C      IF ((Y(I) .GT. YCRIT .AND. Y(I-1) .GT. YCRIT) .OR.
C      % (Y(I) .LT. YCRIT .AND. Y(I-1) .LT. YCRIT)) GO TO 30
C      IF (I .GT. IREV) IFLOW=1
C      IF ((Y(I)-Y(I-1))*FLOAT(IFLOW*IGRAD) .LT. 0.0) GO TO 30
C      NCRIT=NCRIT+1
C      LCRIT(NCRIT)=I-1
C      SLOPE=(X(I)-X(I-1))/(Y(I)-Y(I-1))
C      XCRIT(NCRIT)=X(I-1)+SLOPE*(YCRIT-Y(I-1))
C      30 CONTINUE
C      XLOC(1)=X(LMIN)
C      INTERP14
C      INTERP15
C      INTERP16
C      INTERP17
C      INTERP18
C      INTERP19
C      INTERP20
C      INTERP21
C      INTERP22
C      INTERP23
C      INTERP24
C      INTERP25
C      INTERP26
C      INTERP27
C      INTERP28
C      INTERP29
C      INTERP30
C      INTERP31
C      LOCATE 2
C      LOCATE 3
C      LOCATE 4
C      LOCATE 5
C      LOCATE 6
C      LOCATE 7
C      LOCATE 8
C      LOCATE 9
C      LOCATE10
C      LOCATE11
C      LOCATE12
C      LOCATE13
C      LOCATE14
C      LOCATE15
C      LOCATE16
C      LOCATE17
C      LOCATE18
C      LOCATE19
C      LOCATE20
C      LOCATE21
C      LOCATE22
C      LOCATE23
C      LOCATE24
C      LOCATE25
C      LOCATE26
C      LOCATE27
C      LOCATE28
C      LOCATE29
C      LOCATE30
C      LOCATE31
C      LOCATE32
C      LOCATE33
C      LOCATE34
C      LOCATE35
C      LOCATE36
C      LOCATE37
C      LOCATE38
C      LOCATE39
C      LOCATE40
C      LOCATE41
C      LOCATE42
C      LOCATE43

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XLOC(2)=X(LMAX)
IF (NCRIT .EQ. 0) RETURN
DO 40 I=1,NCRIT
40 XLOC(I+2)=XCRIT(I)
RETURN
END
SUBROUTINE MONO (N,L,X,Y)
C
C.....CHECKS POINTS IN VICINITY OF A CRITICAL POINT FOR MONOTONE
C BEHAVIOR, AND ADJUSTS VALUES IF NECESSARY TO GIVE A LINEAR
C PROFILE.
C
DIMENSION L(4),X(200),Y(200)
LEVEL 2, X,Y
DO 10 I=1,N
LS=L(I)
Y1=Y(LS-1)
Y2=Y(LS)
Y3=Y(LS+1)
Y4=Y(LS+2)
IF ((Y1 .LT. Y2) .AND. (Y2 .LT. Y3) .AND. (Y3 .LT. Y4)) GO TO 10
IF ((Y1 .GT. Y2) .AND. (Y2 .GT. Y3) .AND. (Y3 .GT. Y4)) GO TO 10
X1=X(LS-1)
X2=X(LS)
X3=X(LS+1)
X4=X(LS+2)
SLOPE=(Y4-Y1)/(X4-X1)
Y(LS)=Y1+SLOPE*(X2-X1)
Y(LS+1)=Y1+SLOPE*(X3-X1)
10 CONTINUE
RETURN
END
SUBROUTINE SCALE (N,X,M,A,B)
C
C.....ENTRY WITH M = 1 CONVERTS FROM PHYSICAL X (0 TO -A ON LOWER
C SURFACE, 0 TO B ON UPPER SURFACE) TO NORMALIZED X (0 .LT. X .LT.
C 1) ENTRY WITH M=2 REVERSES THE PROCESS. NZ (DETERMINED WHEN M=1)
C CORRESPONDS TO POINT AT NOSE OF BLADE OR AIRFOIL.
C
COMMON /FLOREV/ NZ
DIMENSION X(200)
LEVEL 2, X
IF (M .EQ. 2) GO TO 30
CONTINUE
NZ=0
DO 10 I=2,N
IF (X(I) .LT. X(I-1)) NZ=I
10 CONTINUE
DO 20 I=1,N
IF (I .LE. NZ) T=-X(I)
IF (I .GT. NZ) T=X(I)
X(I)=(T-A)/(B-A)
20 CONTINUE
RETURN
30 DO 40 I=1,N
X(I)=ABS((B-A)*X(I)+A)
40 CONTINUE
RETURN
END
SUBROUTINE SORT (N,X,ISEQ)
LOCATE44 C
LOCATE45 C.....ARRANGES THE SET X(1), X(2), ... , X(N) IN A MONOTONE INCREASING
LOCATE46 C SEQUENCE. ISEQ GIVES ORDER OF SUBSCRIPTS IN REARRANGED SEQUENCE.
LOCATE47 C
LOCATE48 DIMENSION X(8),ISEQ(8)
LOCATE49 NM1=N-1
MONO 2 DO 10 I=1,N
MONO 3 10 ISEQ(I)=I
MONO 4 20 ITEST=0
MONO 5 DO 30 I=1,NM1
MONO 6 IF (X(I) .LE. X(I+1)) GO TO 30
MONO 7 XSAVE=X(I)
MONO 8 X(I)=X(I+1)
MONO 9 X(I+1)=XSAVE
MONO 10 ISAVE=ISEQ(I)
MONO 11 ISEQ(I)=ISEQ(I+1)
MONO 12 ISEQ(I+1)=ISAVE
MONO 13 ITEST=1
MONO 14 30 CONTINUE
MONO 15 IF (ITEST .EQ. 1) GO TO 20
MONO 16 RETURN
MONO 17 END
MONO 18 SUBROUTINE STRAIN (N,K,NSEG,XFIX,XIN,PARM)
MONO 19 C
MONO 20 C.....COMPUTES STRAINING INCREMENT DELX FROM INPUT ARRAY XIN, USING
MONO 21 C PIECEWISE LINEAR STRAINING WITH NSEG LINEAR SEGMENTS. FOR UNIT
MONO 22 C STRAINING, INPUT VALUE OF PARM IS 1.0; FOR GENERAL CASE,
MONO 23 C
MONO 24 C PARM = (Q2(K)-Q0(K))/(Q1-Q0(K)).
MONO 25 C
MONO 26 DIMENSION XFIX(8),XIN(200)
MONO 27 COMMON /COEFF/ C(10,7),D(10,7),DELX(200)
SCALE 2 LEVEL 2, C,D,DELX,XIN
SCALE 3 JSTART=1
SCALE 4 DO 30 I=1,N
SCALE 5 DO 10 J=JSTART,NSEG
SCALE 6 IF (XIN(I) .GE. XFIX(J) .AND. XIN(I) .LE. XFIX(J+1)) GO TO 20
SCALE 7 10 CONTINUE
SCALE 8 20 DELX(I)=PARM*(C(K,J)+D(K,J)-1.0)*XIN(I)
SCALE 9 JSTART=J
SCALE 10 30 CONTINUE
SCALE 11 RETURN
SCALE 12 END
SCALE 13 SUBROUTINE UPLW (A,B,XIN,K,N,XOUT,FLAG)
SCALE 14 C
SCALE 15 C.....CONVERTS NORMALIZED ARRAY XIN TO PHYSICAL ARRAY XOUT AND FLAGS
SCALE 16 C POINTS ON LOWER SURFACE WITH A "M".
SCALE 17 C
SCALE 18 DIMENSION XIN(K),XOUT(8)
SCALE 19 DIMENSION FLAG(8)
SCALE 20 DATA BLANK/1H /, STAR/1H*/
SCALE 21 XNOSE=-A/(B-A)
SCALE 22 DO 10 I=1,N
SCALE 23 FLAG(I)=BLANK
SCALE 24 IF (XIN(I) .LT. XNOSE) FLAG(I)=STAR
SCALE 25 XOUT(I)=ABS((B-A)*XIN(I)+A)
SCALE 26 10 CONTINUE
SCALE 27 RETURN
SCALE 28 END
SCALE 29 SUBROUTINE TSONIC
SORT 2 TSONIC 2

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COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
COMMON /INPUTT/ GAM,AR,TIP,RHOIP,WTFL,OMEGA,ORF,BETAI,BETA0,
1  LAMBDA,RVTHO,REDFAC,DENTOL,FSMI,FSHO,SSM1,SSM2,MBI,MBO,MM,
2  NDBI,NBL,NRSP,MOPT,LOPT,LRVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD,
3  INTVL,SURVL,CHORD(2),STGR(2),RI(2),ROI(2),BETI(2),BETO(2),
4  NSPI(2),TITLEI(20),MRI(50),RMSPI(50),BESPF(50),WOWCR(50),
5  PLOSSI(50),MSP(50,2),THSP(50,2)
COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIMI,MBIPI,MBOMI,MBOP1,MMH1,
1  HMI,HT,DTLR,DMLR,PITCH,CP,EXPON,TWH,CPTIP,TGROG,TBI,TBO,TWL,
2  WI,WMI,WCR1,ITMIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
3  THLE(2),RMI(2),RMO(2),BESPI(50),MVI(100),RM(100),BE(100),
4  BEF(100),DBDM(100),DBFDM(100),SALI(100),PLOSIMI(100),AAA(100),
5  BBB(100),IV(101),ITV(100,2),TV(100,2),DTHVI(100,2),
6  BETAVI(100,2),MH(100,2),DTHMI(100,2),BETAH(100,2),RMH(100,2),
7  BEH(100,2),PLOSMH(100,2)
COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500)
LEVEL 2, A,U,K,RHO
COMMON /HRBAAK/ H(4),R(4),B(4),KAK(4),KA(4),RZ,BZ,IH(4)
COMMON /VARCOM/ RHOHB(100,2),RHOVB(100,2),NMB(100,2),MTB(100,2),
1  NWCRM(100,2),LABEL(1,100)
COMMON /SLCDM/ USL(100,11),TSL(100,11)
LEVEL 2, USL,TSL
COMMON /BCDCOM/ INIT(2),EM(50,2),D2TDM2(100,2)
COMMON /PLTCOM/ TSLPT(1100),XDDMI(400),YACROS(400)
LEVEL 2, TSLPT,XDDMN,YACROS
INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,
1  UPPER,S1,ST
REAL K,KAK,LAMBDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVIMI
DATA ICALL/0/
ICALL=ICALL+1
IEND=-1
ITER = 0
INIT(1) = 0
INIT(2) = 0
CALL TINPUT
IF(ICALL.EQ.1) RETURN
IF (BLDAT.GE.2) CALL BLDPLT
CALL PRECAL
30 ITER = ITER+1
CALL COEF
CALL SOR
CALL VELMER
CALL VELTAN
CALL STRLIN
CALL OUTPUT
IF(NER(2).GT.0) RETURN
IF(IEND.LE.0) GO TO 30
IF(REDFAC.LT.1.) CALL TVELCY
RETURN
END
SUBROUTINE TINPUT
C
C INPUT READS AND PRINTS ALL INPUT DATA CARDS AND CALCULATES HORIZONTAL
C SPACING (MV ARRAY)
C
COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
COMMON /INPUTT/ GAM,AR,TIP,RHOIP,WTFL,OMEGA,ORF,BETAI,BETA0,
1  LAMBDA,RVTHO,REDFAC,DENTOL,FSMI,FSHO,SSM1,SSM2,MBI,MBO,MM,
2  NDBI,NBL,NRSP,MOPT,LOPT,LRVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD,
3  INTVL,SURVL,CHORD(2),STGR(2),RI(2),ROI(2),BETI(2),BETO(2),

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TSONIC 3
TSONIC 4
TSONIC 5
TSONIC 6
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TSONIC50
TSONIC51
TSONIC52
INPUU 2
INPUU 3
INPUU 4
INPUU 5
INPUU 6
INPUU 7
INPUU 8
INPUU 9
INPUU 10
INPUU 11

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4  NSPI(2),TITLEI(20),MR(50),RMSPI(50),BESPF(50),WOWCR(50),
5  PLOSSI(50),MSP(50,2),THSP(50,2)
COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIMI,MBIPI,MBOMI,MBOP1,MMH1,
1  HMI,HT,DTLR,DMLR,PITCH,CP,EXPON,TWH,CPTIP,TGROG,TBI,TBO,TWL,
2  WI,WMI,WCR1,ITMIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
3  THLE(2),RMI(2),RMO(2),BESPI(50),MVI(100),RM(100),BE(100),
4  BEF(100),DBDM(100),DBFDM(100),SALI(100),PLOSIMI(100),AAA(100),
5  BBB(100),IV(101),ITV(100,2),TV(100,2),DTHVI(100,2),
6  BETAVI(100,2),MH(100,2),DTHMI(100,2),BETAH(100,2),RMH(100,2),
7  BEH(100,2),PLOSMH(100,2)
COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500)
LEVEL 2, A,U,K,RHO
COMMON /MBIMBO/ MBIZ,MBOZ
COMMON /MHVORM/ XMVNI(100)
DIMENSION SPLND(2),CARD(8)
INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,
1  UPPER,S1,ST
REAL K,KAK,LAMBDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVIMI
DATA ICALL/0/, END/10H$END /
C
C READ AND PRINT ALL INPUT DATA
C
NREAD = 1
NWRIT = 6
ICALL=ICALL+1
IF (ICALL.GT.1) GO TO 2 -
1 READ (5,990) CARD
IF (CARD(1).EQ.END) GO TO 2
WRITE(1,990) CARD
GO TO 1
2 REWIND 1
WRITE(NWRIT,1000)
WRITE(NWRIT,1110)
READ (NREAD,1030) GAM,AR,TIP,RHOIP,WTFL,BLANK,OMEGA,ORF
WRITE(NWRIT,1040) GAM,AR,TIP,RHOIP,WTFL,BLANK,OMEGA,ORF
READ (NREAD,1030) BETAI,BETA0,BLANK,BLANK,FSMI,FSHO
READ (NREAD,1030) REDFAC,DENTOL,SSM1,SSM2
IF (DENTOL.LE.0.) DENTOL = .01
C -- MOPT = 0, NO CORRECTION TO THE BESP ARRAY (REDFAC MUST EQUAL 1.0)
C MOPT = 1, READ IN WOWCR ARRAY FOR CALCULATING REDUCED FLOW BESP
C MOPT = 2, REDUCED BESP ARRAY CALCULATED BY PROGRAM.
READ (NREAD,1010) MBI,MBO,BLANK,BLANK,MM,NDBI,NBL,NRSP,MOPT,LOPT,
1  LRVB
MBIZ=MBI
MBOZ=MBO
IF (LRVB.EQ.1) GO TO 6
WRITE(NWRIT,1120)
WRITE(NWRIT,1040)BETAI,BETA0,CHORD(1),STGR(1),FSMI,FSHO
GO TO 8
6 WRITE(NWRIT,1122)
LAMBDA = BETAI
RVTHO = BETAO
WRITE(NWRIT,1040) LAMBDA,RVTHO,CHORD(1),STGR(1)
8 WRITE(NWRIT,1125)
WRITE(NWRIT,1040) REDFAC,DENTOL,SSM1,SSM2
WRITE(NWRIT,1130)
WRITE(NWRIT,1020) MBI,MBO,BLANK,BLANK,MM,NDBI,NBL,NRSP,MOPT,LOPT,
1  LRVB
DO 10 J=1,2
IF (J.EQ.1) WRITE(NWRIT,1140)
INPUU 12
INPUU 13
INPUU 14
INPUU 15
INPUU 16
INPUU 17
INPUU 18
INPUU 19
INPUU 20
INPUU 21
INPUU 22
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INPUU 66
INPUU 67
INPUU 68
INPUU 69
INPUU 70
INPUU 71

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IF (J.EQ.2) WRITE(NWRIT,1150)
WRITE(NWRIT,1180) J,J,J,J,J
READ (NREAD,1030) BLANK,BLANK,BLANK,BLANK,SPLNO(J)
WRITE(NWRIT,1040) RI(J),RO(J),BETI(J),BETO(J),SPLNO(J)
NSPI(J) = SPLNO(J)
NSP = NSPI(J)
WRITE(NWRIT,1190) J
WRITE(NWRIT,1040) (MSP(I,J),I=1,NSP)
WRITE(NWRIT,1200) J
10 WRITE(NWRIT,1040) (THSP(I,J),I=1,NSP)
WRITE(NWRIT,1210)
READ (NREAD,1030) (MR(I),I=1,NRSP)
WRITE(NWRIT,1040) (MR(I),I=1,NRSP)
WRITE(NWRIT,1220)
READ (NREAD,1030) (RMSP(I),I=1,NRSP)
WRITE(NWRIT,1040) (RMSP(I),I=1,NRSP)
WRITE(NWRIT,1230)
READ (NREAD,1030) (BESPF(I),I=1,NRSP)
WRITE(NWRIT,1040) (BESPF(I),I=1,NRSP)
DO 20 I=1, NRSP
BESP(I) = BESPF(I)
20 PLOSS(I) = 0.
IF (MOPT.NE.1) GO TO 40
WRITE(NWRIT,1236)
READ (NREAD,1030) (WOWCR(I),I=1,NRSP)
WRITE(NWRIT,1040) (WOWCR(I),I=1,NRSP)
40 IF (LOPT.EQ.0) GO TO 60
WRITE(NWRIT,1237)
READ (NREAD,1030) (PLOSS(I),I=1,NRSP)
WRITE(NWRIT,1040) (PLOSS(I),I=1,NRSP)
60 WRITE(NWRIT,1240)
READ (NREAD,1010) BLDAT,AANDK,ERSOR,STRFN,SLCRD,INTVL,SURVL
WRITE(NWRIT,1020) BLDAT,AANDK,ERSOR,STRFN,SLCRD,INTVL,SURVL
IF(ICALL.EQ.1) RETURN
IF (MM.LE.100.AND.NBBI.LE.50.AND.NRSP.LE.50.AND.NSPI(1).LE.50
1 .AND.NSPI(2).LE.50) GO TO 70
WRITE(NWRIT,1250)
STOP
70 IF (REDFAC.EQ.1..OR.MOPT.NE.0) GO TO 75
WRITE(NWRIT,1260)
STOP
C
C CALCULATE MV ARRAY
C
75 HM1 = CHORD(1)/FLOAT(MBO-MBI)
DO 80 IM=1,MM
MV(IM) = FLOAT(IM-MBI)*HM1
XMVN(IM)=MV(IM)/CHORD(1)
IF (SSM1.EQ.SSM2) GO TO 80
IF (MV(IM).LT.SSM1) IMS1 = IM+1
IF (MV(IM).LE.SSM2) IMS2 = IM
80 CONTINUE
MV(MBO) = CHORD(1)
XMVN(MBO)=1.0
C
C CALCULATE MISCELLANEOUS CONSTANTS
C
HER(1) = 0
HER(2) = 0
INPUU 72
INPUU 73
INPUU 74
INPUU 75
INPUU 76
INPUU 77
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INPUU 79
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INPUU186
INPUU187
INPUU188
HER(1) = 0
HER(2) = 0
PITCH = 2.*3.1415927/FLOAT(NBL)
HT = PITCH/FLOAT(HBBI)
OTLR = HT/1000.
DMLR = HM1/1000.
BV(1) = 0.
BV(2) = 1.
MBIM1 = MBI-1
MBIP1 = MBI+1
MBOM1 = MBO-1
MBOP1 = MBO+1
MM1 = MM-1
CP = AR/(GAM-1.)*GAM
EXPON = 1./(GAM-1.)
THW = 2.*OMEGA/WTFL
CPTIP = 2.*CPTIP
TGROG = 2.*GAM*AR/(GAM+1.)
CALL SPLINT(MR,RMSP,NRSP,MV,MM,MM,SAL,AAA)
CALL SPLINT(MR,BESPF,NRSP,MV,MM,BEF,DBFDM,AAA)
CALL SPLINT(MR,BESP,NRSP,MV,MM,BE,DBDM,AAA)
CALL SPLINT(MR,PLOSS,NRSP,MV,MM,PLOSSIM,BBB,AAA)
C
C CALCULATE GEOMETRICAL CONSTANTS
C
CHORD(2) = CHORD(1)
STGR(2) = STGR(1)
MLE(1) = 0.
MLE(2) = 0.
THLE(1) = 0.
THLE(2) = PITCH
RMI(1) = RM(MBI)
RMI(2) = RM(MBI)
RMO(1) = RM(MBO)
RMO(2) = RM(MBO)
C
C INITIALIZE U AND K ARRAYS AND SURFACE DENSITY ARRAYS
C
DO 90 I=1,2500
U(I) = 1.
K(I) = 0.
90 RHO(I) = RHOIP
C
C INITIALIZE A ARRAY
C
DO 91 KDOM = 1,4
DO 91 I = 1,2500
91 A(I,KDOM) = 0.
NREAD=5
RETURN
C
C FORMAT STATEMENTS
C
990 FORMAT (8A10)
1000 FORMAT(1H1,35X,
* 5H--- INPUT FOR TSONIC BLADE-TO-BLADE FLOW SOLVER ---//)
1010 FORMAT (16I5)
1020 FORMAT (1X,16I7)
1030 FORMAT (8F10.5)
1040 FORMAT (1X,8G16.7)

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1100 FORMAT (20A4) INPUU189
1105 FORMAT (1X,20A4) INPUU190
1110 FORMAT (7X,3HGAM,14X,2HAR,13X,3HTIP,12X,5HRHOIP,12X,4HWTF,11X,6H INPUU191
1 ,10X,5HOMEGA,12X,3HORF) INPUU192
1120 FORMAT (6X,5HBETAI,11X,5HBETA0,11X,6HCHORDF,11X,5HSTGRF,12X,4HFSHI INPUU193
1 ,12X,4HFSHO) INPUU194
1122 FORMAT (6X,6HLAMBDA,10X,5HRVTHO,11X,6HCHORDF,10X,5HSTGRF) INPUU195
1125 FORMAT (6X,6HREDFAC,10X,6HDENTOL,11X,4HSSM1,12X,4HSSM2) INPUU196
1130 FORMAT(1H0,3X,3HMBI,4X,3HMBO,19X,2HMM,3X,4HNBBI,4X, INPUU197
* 3HNBL,3X,4HHRSP,3X,4HMOP,3X,4HLOPT,3X,4HLRVB) INPUU198
1140 FORMAT(39H0 BLADE SURFACE 1 -- UPPER SURFACE) INPUU199
1150 FORMAT(39H0 BLADE SURFACE 2 -- LOWER SURFACE) INPUU200
1180 FORMAT (7X,2HRI,1I,12X,2HRO,1I,12X,4HBETI,1I,11X,4HBETO,1I,11X,5HS INPUU201
1PLNO,1I) INPUU202
1190 FORMAT (7X,3HMSP,1I,2X,5HARRAY) INPUU203
1200 FORMAT (7X,4HTSP,1I,2X,5HARRAY) INPUU204
1210 FORMAT(16H0 MR ARRAY) INPUU205
1220 FORMAT (7X,11HRMSP ARRAY) INPUU206
1230 FORMAT (7X,11HBESP ARRAY) INPUU207
1235 FORMAT (7X,11HBESPF ARRAY) INPUU208
1236 FORMAT (7X,11HWOCR ARRAY) INPUU209
1237 FORMAT (7X,11HPLOSS ARRAY) INPUU210
1240 FORMAT(52H0 BLDAT AANDK ERSOR STRFN SLCRD INTVL SURVL) INPUU211
1250 FORMAT (41HI MM,NBBI,NRSP,OR SOME SPLNO IS TOO LARGE) INPUU212
1260 FORMAT (56HI WHEN REDFAC IS LESS THAN 1.0, MOPT MUST EQUAL 1 OR INPUU213
12) INPUU214
END INPUU215
SUBROUTINE PRECAL PRECAL 2
C PRECAL CALCULATES ALL REQUIRED FIXED CONSTANTS PRECAL 3
C PRECAL 4
COMMON NREAD,NWRIT,ITER,IEHD,LER(2),NER(2) PRECAL 5
COMMON /INPUT/ GAH,AR,TIP,RHOIP,WTF,OMEGA,ORF,BETAI,BETA0, PRECAL 6
1 LAMBDA,RVTHO,REDFAC,DENTOL,FSHI,FSHO,SSM1,SSM2,MBI,MBO,MM, PRECAL 7
2 NBBI,NBL,NRSP,MOPT,LOPT,LRVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD, PRECAL 8
3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),RO(2),BETI(2),BETO(2), PRECAL 9
4 NSPI(2),TITLEI(20),MR(50),RMSP(50),BESPF(50),WOCR(50), PRECAL 10
5 PLOSS(50),MSP(50,2),THSP(50,2) PRECAL 11
COMMON /CALCOM/ ACTWT,ACTOMG,ACTLAM,MBIM1,MBIP1,MBOM1,MBOP1,MMH1, PRECAL 13
1 HMI,HT,DTLR,DMLR,PITCH,CP,EXPON,TWN,CPTIP,TGROG,TBI,TBO,TWL, PRECAL 14
2 WI,WMI,WCRI,ITMIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2), PRECAL 15
3 THLE(2),RMI(2),RMD(2),BESP(50),MV(100),RMI(100),BE(100), PRECAL 16
4 BEF(100),OBDM(100),DBFDM(100),SAL(100),PLOSSIM(100),AAA(100), PRECAL 17
5 BBB(100),IV(101),ITV(100,2),TV(100,2),DTHV(100,2), PRECAL 18
6 BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RMH(100,2), PRECAL 19
7 BEH(100,2),PLOSSMH(100,2) PRECAL 20
COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500) PRECAL 21
LEVEL 2, A,U,K,RHO PRECAL 22
COMMON /VARCOM/ RHOHB(100,2),RHOVB(100,2),MMB(100,2),WTB(100,2), PRECAL 23
1 WOCR(100,2),LABEL(1,100) PRECAL 24
COMMON /BCDCOM/ INIT(2),EH(50,2),D2TDM2(100,2) PRECAL 25
COMMON /TBBC/ TBIBC,TBOBC PRECAL 26
COMMON /WIO/ WISV,WOSV PRECAL 27
DIMENSION CURV(100,2),ZMR(100),BEZMR(100),WIHOP(4),HWCR(4), PRECAL 28
1 BETAIM(4),IHOP(4) PRECAL 29
INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST, PRECAL 30
1 UPPER,S1,ST PRECAL 31
REAL K,KAK,LAMBDA,LMAX,MM,MLE,MR,MSL,MSP,MV,MVIM1 PRECAL 32
EXTERNAL BL1,BL2 PRECAL 33
DEGRAD = 180./3.1415927 PRECAL 34
NEGBE = 0
IEPROR = 0
C CALCULATE ITV, IV, TV, AND DTMV ARRAYS
C
ITMIN = 0
ITMAX = NBBI-1
C ITV UPSTREAM OF BLADE
FIRST = 0
LAST = NBBI-1
DO 10 IM=1,MBIM1
ITV(IM,1) = FIRST
10 ITV(IM,2) = LAST
C ITV, TV, AND DTMV ON BLADE
DO 20 IM=MBO,MBO
LER(2) = 1
C BLCD CALL NO. 1
CALL BL1(MV(IM),TV(IM,1),DTDMV(IM,1),INF)
ITV(IM,1) = INT((TV(IM,1)+DTLR)/HT)
IF (TV(IM,1).GT.-DTLR) ITV(IM,1)=ITV(IM,1)+1
ITMIN = MINO(ITMIN,ITV(IM,1))
LER(2) = 2
C BLCD CALL NO. 2
CALL BL2(MV(IM),TV(IM,2),DTDMV(IM,2),INF)
ITV(IM,2) = INT((TV(IM,2)+DTLR)/HT)
IF (TV(IM,2).LT.DTLR) ITV(IM,2)=ITV(IM,2)-1
20 ITMAX = MAXO(ITMAX,ITV(IM,2))
C ITV DOWNSTREAM OF BLADE
LAST = ITV(MBO,2)
FIRST = LAST+1-NBBI
DO 40 IM=MBOPI,MM
ITV(IM,1) = FIRST
40 ITV(IM,2) = LAST
ITMIN = MINO(ITMIN,ITV(MM,1))
C IV ARRAY
IV(1) = 1
DO 50 IM=1,MM
50 IV(IM+1) = IV(IM)+ITV(IM,2)-ITV(IM,1)+1
C CALCULATE BETAV AND CURV ARRAYS
C
DO 60 SURF=1,2
DO 60 IM=MBO,MBO
CURV(IM,SURF) = (RM(IM)*D2TDM2(IM,SURF)*SAL(IM)*DTDMV(IM,SURF)) /
1 (1.+(RM(IM)*DTDMV(IM,SURF)**2)**.5
60 BETAV(IM,SURF) = ATAN(DTDMV(IM,SURF)*RM(IM))*DEGRAD
NIP = IV(MM)*NBBI-1
IF(NIP.GT.2500) WRITE(NWRIT,1150)
C CALCULATE MH AND DTMH ARRAYS
C
ITO = ITV(1,1)
MRTS = 1
IMS(1) = 1
MH(1,1) = 0.
DTDMH(1,1) = 1.E10
LER(2) = 3
C BLCD AND POOT (VIA MHORIZ) CALL NO. 3
CALL MHORIZ(MV,ITV(1,1),BL1,MBI,MBO,ITO,HT,DTLR,0,IMS(1),MH(1,1),
1 DTMH(1,1),MRTS)
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IF (ITV(MBO,1)-ITV(MBO,2)*NBI.NE.2) GO TO 70
IMSL = IMS(1)+1
MH(IMSL,1) = MV(MBO)
DTOMH(IMSL,1) = -1.E10
IMS(1) = IMSL
70 IMS(2) = 0
MRTS = 1
LER(2) = 4
C BLCD AND ROOT (VIA MHORIZ) CALL NO. 4
CALL MHORIZ(MV,ITV(1,2),BL2,MBI,MBO,ITO,HT,OTLR,1,IMS(2),MH(1,2),
1 DTOMH(1,2),MRTS)
IMSMAX = MAX0(IMS(1),IMS(2))
IF (IMSMAX.GT.100) WRITE(NWRIT,1100) IMSMAX
C
C CALCULATE RMH ARRAY
C
DO 80 SURF=1,2
CALL SPLINT(MR,RMSP,NRSP,MH(1,SURF),IMS(SURF),RMH(1,SURF),AAA,BBB)
80 CALL SPLINT(MR,PLOSS,NRSP,MH(1,SURF),IMS(SURF),PLOSSMH(1,SURF),
1 AAA,BBB)
C
C CALCULATE LAMBDA WHEN BETA1 IS GIVEN AS INPUT
C
IF (LRVB.EQ.1) GO TO 130
BETA1 = BETA1/DEGRAD
BETA0 = BETA0/DEGRAD
IF (FSMI.NE.FSMO) GO TO 90
FSMI = 0.
FSMO = CHORD(1)
90 CALL SPLINT(MR,RMSP,NRSP,FSMI,1,RMFSMI,BLANK,AAA)
CALL SPLINT(MR,RMSP,NRSP,FSMO,1,RMFSMO,BLANK,AAA)
CALL SPLINT(MR,BESPF,NRSP,FSMI,1,BEFSMI,BLANK,AAA)
CALL SPLINT(MR,BESPF,NRSP,FSMO,1,BEFSMO,BLANK,AAA)
CALL SPLINT(MR,PLOSS,NRSP,FSMI,1,PLFSMI,BLANK,AAA)
CALL SPLINT(MR,PLOSS,NRSP,FSMO,1,PLFSMO,BLANK,AAA)
RHOVI = WTLF/BEFSMI/PITCH/COS(BETA1)/RMFSMI
WI = 0.
DELWMX = SQRT(TGROG*TIP)/10.
100 TTIP = 1.-(WI**2+2.*OMEGA*RMFSMI*WI*SIN(BETA1)+(OMEGA*RMFSMI)
1 **2)/CPTIP
IF (TTIP.LE.0.) GO TO 110
TEMP = TTIP**(EXPON-1.)
RHOIPL = RHOIP*(1.-PLFSMI)
RHOT = RHOIPL*TEMP*TTIP
FPRIME = RHOT-RHOIPL/GAM*WI/AR*(WI+OMEGA*RMFSMI*SIN(BETA1))/TIP
1 *TEMP
IF (FPRIME.LE.0.) GO TO 110
WINEW = WI*(RHOVI-RHOT*WI)/FPRIME
IF (WINEW-WI.GT.DELWMX) WINEW = WI+DELWMX
IF (ABS(WINEW-WI)/WINEW).LT..000005) GO TO 120
WI = WINEW
GO TO 100
110 WRITE(NWRIT,1020)
IERROR = 1
120 LAMBDA = RMFSMI*(WI*SIN(BETA1)+OMEGA*RMFSMI)
WMI = WI*COS(BETA1)
AA = (2.*OMEGA*LAMBDA-(OMEGA*RMFSMI)**2)/CPTIP
WCRI = SQRT(TGROG*TIP*(1.-AA))
C
C CALCULATE RVTHO WHEN BETA0 IS GIVEN AS INPUT
PRECAL95 C
PRECAL96 RHOVO = WTLF/BEFSMO/PITCH/COS(BETA0)/RMFSMO
PRECAL97 TWLMR = 2.*OMEGA*LAMBDA-(OMEGA*RMFSMO)**2
PRECAL98 TTIP = 1.-TWLMR/CPTIP
PRECAL99 RHOIPL = RHOIP*(1.-PLFSMO)
PRECAL100 RHOMB2 = RHOIPL*TTIP**EXPON
PRECAL101 LER(1) = 1
PRECAL102 C DENSTY CALL NO. 1
PRECAL103 NERT = NER(1)
PRECAL104 JZ = 1
PRECAL105 IF (FSMO.GE.SSM1.AND.FSMO.LE.SSM2) JZ=2
PRECAL106 CALL DENSTY(RHOVO,RHOMB2,W0,TWLMR,CPTIP,EXPON,RHOIPL,GAM,AR,TIP,
PRECAL107 1 JZ)
PRECAL108 IF (NERT.NE.NER(1)) WRITE(NWRIT,1022)
PRECAL109 RVTHO = RMFSMO*(W0*SIN(BETA0)+OMEGA*RMFSMO)
PRECAL110 WMO = W0*COS(BETA0)
PRECAL111 WCRO = SQRT(TGROG*TIP*(1.-TWLMR/CPTIP))
PRECAL112 130 TWL = 2.*OMEGA*LAMBDA
C
C INITIALIZE DENSITY WHERE HORIZONTAL MESH LINES INTERSECT BLADE
C AND CALCULATE BETAH ARRAY
C
DO 150 SURF=1,2
IMSS = IMS(SURF)
IF (IMSS.LT.1) GO TO 150
DO 140 IHS=1,IMSS
RHOHBI(IHS,SURF) = RHOIP*(1.-PLOSSMH(IHS,SURF))*(1.-(2.*OMEGA*
1 LAMBDA-(OMEGA*RMH(IHS,SURF))**2)/CPTIP)**EXPON
140 BETAHI(IHS,SURF) = ATAN(DTOMH(IHS,SURF)*RMH(IHS,SURF))*DEGRAD
150 CONTINUE
C
C INITIALIZE DENSITY WHERE VERTICAL MESH LINES INTERSECT BLADE
C AND AT INTERIOR POINTS
C
DO 170 IM=1,MM
TTIP = 1.-(TWL-(OMEGA*RM(IM))**2)/CPTIP
RHOT = RHOIP*(1.-PLOSIM(IM))*TTIP**EXPON
DO 160 SURF=1,2
160 RHOVB(IM,SURF) = RHOT
IPU = IV(IM)
IPL = IV(IM+1)-1
DO 170 IP=IPU,IPL
170 RHO(IP) = RHOT
C
C CALCULATE VELOCITY DIAGRAM INFORMATION, AND
C TAN BETA (TBI AND TBO) AT UPSTREAM AND DOWNSTREAM BOUNDARIES
C
IMOP(1) = 1
IMOP(2) = MBI
IMOP(3) = MBO
IMOP(4) = MM
WHIRL = LAMBDA
DELTWL = 0.
DO 220 I=1,4
IM = IMOP(I)
VTHIM = WHIRL/RM(IM)
VTHIM2 = VTHIM**2
WTHIM = VTHIM-OMEGA*RM(IM)
WTHIWL = VTHIM2*DELTWL
RHOIIM = WTLF/RM(IM)/PITCH/BEF(IM)
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RHOIM = RHOVB(IM,1)
RHOIPL = RHOIP*(1.-PLOSIM(IM))
LER(1) = 2
C DENSTY CALL NO. 2
NERT = NER(1)
JZ = 1
CALL DENSTY(RHOWIM,RHOIM,WMIM,WTHTML,CPTIP,EXPON,RHOIPL,GAM,AR,
1 TIP,JZ)
IF (NERT.NE.NER(1)) WRITE(NWRIT,1024) MV(IM),IM
TBETA = WTHIM/WMIM
BETA(IM) = ATAN(TBETA)*DEGRAD
AA = (TWL-(OMEGA*RM(IM)**2)/CPTIP
WCRIM = SQRT(TGROG*TIP*(1.-AA))
WIMOP(IM) = SQRT(WMIM**2+WTHIM**2)
WMCRI = WIMOP(IM)/WCRIM
IF (I.EQ.2) DELTIL = 2.*OMEGA*(LAMBDA-RVTHO)
IF (I.EQ.2) WHIRL = RVTHO
220 IF (I.EQ.1) TBI = TBETA
TBO = TBETA
BTAIN = ATAN(TBI)*DEGRAD
BTAOUT = ATAN(TBO)*DEGRAD
IF (LRVB.NE.1) GO TO 225
FSHI = MV(1)
FSHO = MV(MM)
RMFSHI = RM(1)
RMFSHO = RM(MM)
WI = WIMOP(1)
WMI = WI/SQRT(1.+TBI**2)
WCRI = WI/WMCRI(1)
WO = WIMOP(4)
WMO = WO/SQRT(1.+TBO**2)
WCRO = WO/WMCRI(4)
225 CONTINUE
C
C CALAULATE TAN BETA (TBIBC AND TBOBC) AT ONE-HALF MESH SPACE INSIDE
C UPSTREAM AND DOWNSTREAM BOUNDARIES
C
RMIM = (RM(1)+RM(2))/2.
VTHIM = LAMBDA/RMIM
WTHTML = VTHIM**2
WTHIM = VTHIM-OMEGA*RMIM
RHOWIM = WTFI/RMIM/PITCH/(BEF(1)+BEF(2))*2.
RHOIM = RHOVB(1,1)
RHOIPL = RHOIP*(1.-(PLOSIM(1)+PLOSIM(2))/2.)
LER(1) = 2
C--DENSTY CALL NO. 2-A
NERT = NER(1)
JZ = 1
CALL DENSTY(RHOWIM,RHOIM,WMIM,WTHTML,CPTIP,EXPON,RHOIPL,GAM,AR,
1 TIP,JZ)
IF (NERT.NE.NER(1)) WRITE(NWRIT,1026)
TBIBC = WTHIM/WMIM
RMIM = (RM(MM)+RM(MM-1))/2.
VTHIM = RVTHO/RMIM
WTHTML = VTHIM**2+2.*OMEGA*(LAMBDA-RVTHO)
WTHIM = VTHIM-OMEGA*RMIM
RHOWIM = WTFI/RMIM/PITCH/(BEF(MM)+BEF(MM-1))*2.
RHOIM = RHOVB(MM,1)
RHOIPL = RHOIP*(1.-(PLOSIM(MM)+PLOSIM(MM-1))/2.)
LER(1) = 2

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PRECA215 C--DENSTY C8LL NO. 2-B
PRECA216 NERT = NER(1)
PRECA217 JZ = 1
PRECA218 CALL DENSTY(RHOWIM,RHOIM,WMIM,WTHTML,CPTIP,EXPON,RHOIPL,GAM,AR,
PRECA219 1 TIP,JZ)
PRECA220 IF (NERT.NE.NER(1)) WRITE(NWRIT,1026)
PRECA221 TBOBC = WTHIM/WMIM
PRECA222
C
C CALCULATE REDUCED BESP WHEN REDFAC IS LESS THAN 1.0
C
IF (REDFAC.EQ.1.) GO TO 300
C
C CALCULATE REDUCED BESP WHEN W/WCR IS GIVEN AS INPUT
C
IF (MOPT.NE.1) GO TO 240
DO 230 I=1, NRSP
ZMR(I) = MR(I)
AA = (2.*OMEGA*LAMBDA-(OMEGA*RMSP(I)**2)/CPTIP
TPPRAT = (1.-AA)/(1.-REDFAC**2*AA)
AA = (GAM-1.)/(GAM+1.)*WMCRI(I)**2
AA = (TPPRAT*(1.-AA)/(1.-REDFAC**2*TPPRAT*AA))*EXPON
IF (BESPF(I).LE.0.) NEGBE = 1
230 BEZMR(I) = BESPF(I)*AA
NZMR = NRSP
IF (NEGBE.EQ.1) WRITE(NWRIT,1160)
GO TO 290
C
C CALCULATE REDUCED BESP WHEN W/WCR IS NOT GIVEN AS INPUT
C
C CALCULATE SOLIDITY AND FAIRING DISTANCE FROM L.E. AND T.E.
240 BLDCRD = SQRT(((RM(MBI)+RM(MBO))/2.*STGR(1))**2+CHORD(1)**2)
SOLDTY = BLDCRD/PITCH/RM(MBI)
DISTLE = AMINI(.5,AMAX(1./6.,(11.-4.*SOLDTY)/18.))*CHORD(1)
SOLDTY = BLDCRD/PITCH/RM(MBO)
DISTTE = AMINI(.5,AMAX(1./6.,(11.-4.*SOLDTY)/18.))*CHORD(1)
C CALCULATE REDUCED BESP UPSTREAM
RHOIM = RHOVB(1,1)
DO 250 IM=1,MBIM
ZMR(IM) = MV(IM)
VTH2IM = (LAMBDA/RM(IM))**2
RHOWM = WTFI/RM(IM)/PITCH/BEF(IM)
RHOIPL = RHOIP*(1.-PLOSIM(IM))
LER(1) = 3
C DENSTY CALL NO. 3
NERT = NER(1)
JZ = 1
CALL DENSTY(RHOWM,RHOIM,WMIM,VTH2IM,CPTIP,EXPON,RHOIPL,GAM,AR,TIP,
1 JZ)
IF (NERT.NE.NER(1)) WRITE(NWRIT,1024) MV(IM),IM
ENTHF = CPTIP-WMIM**2-VTH2IM
ENTHRE = CPTIP-(WMIM**2+VTH2IM)*REDFAC**2
250 BEZMR(IM) = BEF(IM)*(ENTHF/ENTHRE)**EXPON
C CALCULATE REDUCED BESP IN BLADE
IMLP = MBIM
IMI = MBI+INT((DISTLE/IMI)*1)
IML = MBI+INT((CHORD(1)-DISTTE)/IMI)
IF (IMI.GT.IML) GO TO 270
DO 260 IM=IMI,IML
IMLP = IMLP+1
ZMR(IMLP) = MV(IM)

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BETIM = (BETAV(IM,1)*BETAV(IM,2))/2./DEGRAD
RHOIM = WTFL/BEF(IM)/RMI(IM)/(TV(IM,2)-TV(IM,1))/COS(BETIM)
RHOIPL = RHOIP*(1.-PLOSIM(IM))
TWLMR = TWL-(OMEGA*RM(IM))*2
LER(1) = 4
C DENSTY CALL NO. 4
  NERT = NER(1)
  JZ = 1
  IF (IM.GE.IMS1.AND.IM.LE.IMS2) JZ=2
  CALL DENSTY(RHOWIM,RHOIM,WIM,TWLMR,CPTIP,EXPON,RHOIPL,GAM,AR,TIP,
1 JZ)
  IF (NERT.NE.NER(1)) WRITE(NWRIT,1024) MV(IM),IM
  ENTHF = CPTIP-WIM**2-TWLMR
  ENTHRE = CPTIP-(WIM**2+TWLMR)*REDFAC**2
260 BEZHR(IMLP) = BEF(IM)*(ENTHF/ENTHRE)**EXPON
270 CONTINUE
C CALCULATE REDUCED BESP DOWNSTREAM
  DO 280 IM=MBO1,MM
  IMLP = IMLP+1
  ZMRI(MLP) = MV(IM)
  WHTWL = (RVTHO/RM(IM))*2+2.*OMEGA*(LAMBDA-RVTHO)
  RHOWM = WTFL/RM(IM)/PITCH/BEF(IM)
  RHOIPL = RHOIP*(1.-PLOSIM(IM))
  LER(1) = 5
C DENSTY CALL NO. 5
  NERT = NER(1)
  JZ = 1
  CALL DENSTY(RHOWM,RHOIM,WIM,WHTWL,CPTIP,EXPON,RHOIPL,GAM,AR,TIP,
1 JZ)
  IF (NERT.NE.NER(1)) WRITE(NWRIT,1024) MV(IM),IM
  ENTHF = CPTIP-WIM**2-WHTWL
  ENTHRE = CPTIP-(WIM**2+WHTWL)*REDFAC**2
280 BEZHR(IMLP) = BEF(IM)*(ENTHF/ENTHRE)**EXPON
  NZMR = IMLP
290 CALL SPLINT(ZMR,BEZMR,NZMR,MV,MM,BE,DBDM,AAA)
C
C CALCULATE BEH ARRAY
C
300 DO 320 SURF=1,2
  IF (REDFAC.NE.1.) CALL SPLINT(ZMR,BEZMR,NZMR,MH(1,SURF),IMS(SURF),
1 BEH(1,SURF),AAA,BBB)
  IF (REDFAC.EQ.1.) CALL SPLINT(MR,BESP,NRSP,MH(1,SURF),IMS(SURF),
1 BEH(1,SURF),AAA,BBB)
  IMSS = IMS(SURF)
  IF (IMSS.LT.1) GO TO 320
  DO 310 IHS=1,IMSS
310 IF (BEH(IHS,SURF).LE.0.) NEGBE = 2
320 CONTINUE
C
C *****
C NOTE ** WTFL, OMEGA, AND LAMBDA ARE ALL REDUCED AT THIS POINT,
C AND REMAIN REDUCED FOR THE REST OF THE PROGRAM, EXCEPT THAT
C LAMBDA IS RESTORED TO FULL VALUE IN TVELCY
C
  ACTWT = WTFL
  ACTOMG = OMEGA
  ACTLAM = LAMBDA
  HTFL = REDFAC*WTFL
  OMEGA = REDFAC*OMEGA
  LAMBDA = REDFAC*LAMBDA
PRECA335 TWL = 2.*OMEGA*LAMBDA
PRECA336 THW = 2.*OMEGA/WTFL
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WRITE OUTPUT CALCULATED BY PRECAL
WRITE(NWRIT,1030) WI,WMI,WCRI,BTAIN,WD,WMO,WCR0,BTAOUT,FSMI,FSMO
WOSV=WO
WISV=WI
WRITE(NWRIT,1040) PITCH,HT,HM1
WRITE(NWRIT,1050) ITMIN,ITMAX,ACTLAM,RVTHO,WTFL,NIP
WRITE(NWRIT,1060) (IMOP(I),WIMOP(I),WNCRI(I),BETAIM(I),I=1,4)
GO TO 5000
WRITE(NWRIT,1070)
WRITE(NWRIT,1080) (MV(IM),RM(IM),TV(IM,1),DTDMV(IM,1),CURV(IM,1),
1 TV(IM,2),DTDMV(IM,2),CURV(IM,2),IM=MBI,MBO)
WRITE(NWRIT,1085) DISTLE,IM1,DISTTE,IML
WRITE(NWRIT,1090) (IM,MV(IM),RM(IM),SAL(IM),BE(IM),DBDM(IM),
1BEF(IM),DBFDM(IM),IM=1,MM)
WRITE(NWRIT,1120)
DO 330 SURF=1,2
IMSS = IMS(SURF)
330 WRITE(NWRIT,1130) SURF,(MH(IM,SURF),RHM(IM,SURF),BEH(IM,SURF),
1 BETAH(IM,SURF),DTDMH(IM,SURF),IM=1,IMSS)
WRITE(NWRIT,1110) (IM,IV(IM),(ITV(IM,SURF),SURF=1,2),IM=1,MM)
WRITE(NWRIT,1140)
5000 CONTINUE
IT = ITHIN
340 IF (IT.GT.ITMAX) GO TO 350
TH = FLOAT(IT)*HT
C WRITE(NWRIT,1010) IT,TH
IT = IT+1
GO TO 340
C
C STOP PROGRAM IF FATAL ERROR HAS OCCURRED IN PRECAL
C
350 IF(NIP.GT.2500) STOP
IF(IHSMAX.GT.100) STOP
IF(IZERROR.NE.0) STOP
IF(NER(1).NE.0) STOP
IF(NEGBE.NE.0) STOP
WRITE(NWRIT,1000)
RETURN
C
C FORMAT STATEMENTS
C
1000 FORMAT (1H1)
1010 FORMAT (4X,I4,G16.5)
1020 FORMAT(60H0INPUT WEIGHT FLOW (WTFL) IS TOO LARGE AT BLADE LEADING
1 EDGE)
1022 FORMAT(61H0INPUT WEIGHT FLOW (WTFL) IS TOO LARGE AT BLADE TRAILING
1 EDGE)
1024 FORMAT(45H0INPUT WEIGHT FLOW (WTFL) IS TOO LARGE AT M =,G15.5,7H
1M = ,I3,1H))
1026 FORMAT(97H0INPUT WEIGHT FLOW (WTFL) IS TOO LARGE ONE-HALF MESH SPAP
1CE INSIDE UPSTREAM OR DOWNSTREAM BOUNDARY)
1030 FORMAT(1H1,10X,8HRELATIVE,11X,10HMERIDIONAL,11X,8HCRITICAL,
1 11X,9HREL. FLOW/11X,3(8HVELOCITY,12X),6H ANGLE/
2 3(9X,11HAT M = FSHI),7X,16HAT UPSTREAM BDY./1X,4G20.5/
3 3(9X,11HAT M = FSHO),6X,18HAT DOWNSTREAM BDY./1X,4G20.5//
4 9X,6HFSHI =,G14.5/9X,6HFSHO =,G14.5)

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1040 FORMAT(//30H CALCULATED PROGRAM CONSTANTS//5X,5HPITCH,13X, PRECA455
1 2HHT,13X,3HHM1/1X,5G16.7) PRECA456
1050 FORMAT (/5X,5HITMIN,10X,5HITMAX/4X,15,10X,15//5X,6HLAMBDA,12X, PRECA457
1 29H DOWNSTREAM WHIRL (RVTHO) /1X,G16.7,12X,G16.7/26H0 REDPRECA458
2UCED HEIGHT FLOW =,G16.7/38H0 NUMBER OF INTERIOR MESH POINTS = PRECA459
3,15) PRECA460
1060 FORMAT(40H0CALCULATED VELOCITY DIAGRAM INFORMATION/24X,2HIM,9X,1HHPRECA461
1,17X,5HM/WCR,16X,4HBETA/1X,17HUPSTREAM BOUNDARY,5X,I3,3G20.5/1X, PRECA462
212HLEADING EDGE,10X,I3,3G20.5/1X,13HTRAILING EDGE,9X,I3,3G20.5/ PRECA463
31X,19HDDNSTREAM BOUNDARY,3X,I3,3G20.5) PRECA464
1070 FORMAT (1H1,6X,62HBLADE DATA AT INTERSECTIONS OF VERTICAL MESH LINPRECA465
1ES WITH BLADES) PRECA466
1080 FORMAT (1/37X,15HBLADE SURFACE 1,30X,15HBLADE SURFACE 2/7X,1HM,14X,PRECA467
1 1HR,14X,2HTV,11X,5HDTDMV,11X,4HCURV,12X,2HTV,11X,5HDTDMV,11X, PRECA468
2 4HCURV/(8G15.5)) PRECA469
1085 FORMAT(38H0FAIRING DISTANCE FROM LEADING EDGE IS,G20.5,8H (IM1 = ,PRECA470
1I3,1H)/39H FAIRING DISTANCE FROM TRAILING EDGE IS,G20.5,8H (IML = PRECA471
2,I3,1H)) PRECA472
1090 FORMAT (1H1,13X,44HSTREAM SHEET COORDINATES AND THICKNESS TABLE / PRECA473
1 2X,2HIM,7X,1HM,14X,1HR,13X,3HSAL,13X,1HB,12X,5HDB/DM,14X,2HBF, PRECA474
211X,6HDBF/DM/(1X,I3,7G15.5)) PRECA475
1100 FORMAT(34HLONE OF THE MH ARRAYS IS TOO LARGE/7H IT HAS,15, 8H POIPRECA476
1NTS) PRECA477
1110 FORMAT (4H1 IM,9X,8HIV ARRAY,25X,9HITV ARRAY/38X,5HBLADE/37X,7HSURPRECA478
1FACE,3X,1H1,5X,1H2/39X,3HNO./(1X,I3,5X,I10,25X,2(I4,2X))) PRECA479
1120 FORMAT (67H1M COORDINATES OF INTERSECTIONS OF HORIZONTAL MESH LINEPRECA480
1S WITH BLADE) PRECA481
1130 FORMAT (25H0MH ARRAY - BLADE SURFACE,I2//15X,2HMH,19X,3HRMH,19X, PRECA482
1 3HBEH,18X,5HBETAH,17X,5HDTDMH/(5G22.4)) PRECA483
1140 FORMAT (43H1THETA COORDINATES OF HORIZONTAL MESH LINES//6X,2HIT, PRECA484
15X,5H1THETA) PRECA485
1150 FORMAT(48H0THE NUMBER OF INTERIOR MESH POINTS EXCEEDS 2500) PRECA486
1160 FORMAT(80H0THE INPUT DESP ARRAY RESULTED IN A NEGATIVE VALUE OF BEPRECA487
1 AT A VERTICAL MESH LINE/5X,47HTHE PROGRAM WILL TERMINATE AT THE EPRECA488
2ND OF PRECAL) PRECA489
1170 FORMAT(82H0THE INPUT BEP ARRAY RESULTED IN A NEGATIVE VALUE OF BEPRECA490
1 AT A HORIZONTAL MESH LINE/5X,47HTHE PROGRAM WILL TERMINATE AT THEPRECA491
2 END OF PRECAL) PRECA492
END PRECA493

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SUBROUTINE PLOTER (KK1,KK2,KK3,KK4) PLOTER 2
ENTRY BLDPLT PLOTER 3
RETURN PLOTER 4
ENTRY VEPLOT PLOTER 5
RETURN PLOTER 6
ENTRY TVPLOT PLOTER 7
RETURN PLOTER 8
END PLOTER 9
SUBROUTINE COEF COEF 2
C COEF CALCULATES FINITE DIFFERENCE COEFFICIENTS, A, AND CONSTANTS, K, COEF 3
C AT ALL UNKNOWN MESH POINTS FOR THE ENTIRE REGION COEF 4
C COEF 5
C COEF 6
COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2) COEF 7
COMMON /INPUT/ GAM,AR,TIP,RHOIP,HTFL,OMEGA,DRF,BETA1,BETA0, COEF 8
1 LAMBDA,RVTHO,REFAC,DENTOL,FSMI,FSM0,SSM1,SSM2,MBI,MBO,MM, COEF 9
2 NBI,NBL,NRSP,MOPT,LOPT,LRVB,BLAT,AANDK,ERSOR,STRFN,SLCRD, COEF 10
3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),ROI(2),BETI(2),BETO(2), COEF 11
4 NSPI(2),TITLEI(20),MR(50),RHSP(50),BESPF(50),WOWCR(50), COEF 12
5 PLOSSI(50),MSP(50,2),THSP(50,2) COEF 13
COMMON /CALCON/ ACTWT,ACTONG,ACTLAM,MBIM1,MBIP1,MBOM1,MBOP1,MMH1, COEF 14
1 HMI,HT,DTLR,DMLR,PITCH,CP,EXPON,TMM,CPTIP,TGROG,TBI,TBO,TWL, COEF 15
2 MI,MMI,KCRI,ITHIN,ITMAX,NIP,IMS1,IMS2,IHS(2),BV(2),MLE(2), COEF 16
3 THLE(2),RMI(2),RMO(2),BESPI(50),MV(100),RM(100),BE(100), COEF 17
4 BEF(100),DBDM(100),DBFDM(100),SAL(100),PLOSIM(100),AAA(100), COEF 18
5 BBB(100),IV(101),ITV(100,2),TV(100,2),DTHMV(100,2), COEF 19
6 BETAV(100,2),MH(100,2),DTHMH(100,2),BETAH(100,2),RHM(100,2), COEF 20
7 BEH(100,2),PLOSSMH(100,2) COEF 21
COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500) COEF 22
LEVEL 2, A,U,K,RHO COEF 23
COMMON /HRBAAK/H(4),R(4),B(4),KAK(4),KA(4),RZ,BZ,IN(4) COEF 24
COMMON /TBBC/ TBIBC,TB09C COEF 25
INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AAEMP,SURF,FIRST, COEF 26
1 UPPER,S1,ST COEF 27
REAL K,KAK,LAMBDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVIM1 COEF 28
C INITIALIZE ARRAYS COEF 29
IH(1) = 1 COEF 30
IH(2) = 0 COEF 31
C INCOMPRESSIBLE CASE COEF 32
IF (GAM.NE.1.5.OR.AR.NE.1000..OR.TIP.NE.1.E6) GO TO 20 COEF 33
IEND = 1 COEF 34
GO TO 40 COEF 35
C ADJUSTMENT OF PRINTING CONTROL VARIABLES COEF 36
20 IF(ITER.NE.1.AND.ITER.NE.2) GO TO 30 COEF 37
AANDK = AANDK-1 COEF 38
ERSOR = ERSOR-1 COEF 39
STRFN = STRFN-1 COEF 40
SLCRD = SLCRD-1 COEF 41
INTVL = INTVL-1 COEF 42
SURVL = SURVL-1 COEF 43
30 IF(IEND.NE.0) GO TO 40 COEF 44
AANDK = AANDK+2 COEF 45
ERSOR = ERSOR+2 COEF 46
STRFN = STRFN+2 COEF 47
SLCRD = SLCRD+2 COEF 48
INTVL = INTVL+2 COEF 49
SURVL = SURVL+2 COEF 50
C FIRST VERTICAL MESH LINE COEF 51
C COEF 52
C COEF 53

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40 DO 50 IP=1,NBBI
  A(IP,1) = 0.
  A(IP,2) = 0.
  A(IP,3) = 0.
  A(IP,4) = 1.
50 K(IP) = HM1*TBIBC/PITCH*2./((RM(1)+RM(2)))
C
C UPSTREAM OF BLADE, EXCEPT FOR FIRST VERTICAL MESH LINE
C
  IF (2.GT.MBIM1) GO TO 70
  DO 60 IM=2,MBIM1
60 CALL COEFP(IM)
C
C BETWEEN BLADES
C
  70 DO 80 IM=MBI,MBO
  80 CALL COEFP(IM)
C
C DOWNSTREAM OF BLADES EXCEPT FOR FINAL MESH LINE
C
150 IF (MBO1.GT.MMM1) GO TO 170
  DO 160 IM=MBO1,MMM1
160 CALL COEFP(IM)
C
C FINAL VERTICAL MESH LINE
C
170 IVMM = IV(MM)
  DO 180 IP=IVMM,NIP
  A(IP,1) = 0.
  A(IP,2) = 0.
  A(IP,3) = 1.
  A(IP,4) = 0.
180 K(IP) = -HM1*TBIBC/PITCH*2./((RM(MM)+RM(MM-1)))
C
C TAKE CARE OF POINTS ADJACENT TO B, AND CASES WHEN POINTS J,C,E, OR F
C ARE GRID POINTS
C
C POINT B
  IP = IV(MBIM1)
  A(IP,4) = 0.
C POINT C
  IF (ITV(MBO,1)-ITV(MBO,2)+NBBI.NE.2) RETURN
  IT = ITV(MBO,1)-1
  IP = IPF(MBOP,IT)
  A(IP,3) = 0.
  RETURN
  END
  SUBROUTINE COSUB (IM)
C
C COSUB CALCULATES FINITE DIFFERENCE COEFFICIENTS, A, AND CONSTANTS, K
C ALONG ALL VERTICAL MESH LINES WHICH INTERSECT BLADES
C
  COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
  COMMON /INPUTT/ GAM,AR,TIP,RHOIP,WTFL,OMEGA,ORF,BETA1,BETA0,
1  LAMBDA,RVTHO,REDFAC,DENTOL,FSHI,FSHO,SSM1,SSM2,MBI,MBO,MM,
2  NBBI,NBL,NRSP,MOPT,LOPT,LRVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD,
3  INTVL,SURVL,CHORD(2),STGR(2),RI(2),RO(2),BETI(2),BETO(2),
4  NSPI(2),TITLEI(2),HR(50),RHSP(50),BESPF(50),HOWCR(50),
5  PLOSS(50),MSP(50,2),THSP(50,2)
  COMMON /CALCON/ ACTHT,ACTOMG,ACTLAM,MBIM1,MBIP1,MBOH1,MBOP1,MMH1,
COEF 54
COEF 55
COEF 56
COEF 57
COEF 58
COEF 59
COEF 60
COEF 61
COEF 62
COEF 63
COEF 64
COEF 65
COEF 66
COEF 67
COEF 68
COEF 69
COEF 70
COEF 71
COEF 72
COEF 73
COEF 74
COEF 75
COEF 76
COEF 77
COEF 78
COEF 79
COEF 80
COEF 81
COEF 82
COEF 83
COEF 84
COEF 85
COEF 86
COEF 87
COEF 88
COEF 89
COEF 90
COEF 91
COEF 92
COEF 93
COEF 94
COEF 95
COEF 96
COEF 97
COEF 98
COEF 99
COEF 100
COSUB 2
COSUB 3
COSUB 4
COSUB 5
COSUB 6
COSUB 7
COSUB 8
COSUB 9
COSUB 10
COSUB 11
COSUB 12
COSUB 13
COSUB 14
1  HM1,HT,DTLR,DMLR,PITCH,CP,EXPON,TWW,CPTIP,TGROG,TBI,TBO,TWL,
2  WJ,WMI,WCRI,ITHIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
3  THLE(2),RMI(2),RMO(2),BESP(50),MVI(100),RM(100),BE(100),
4  BEF(100),DBDM(100),DBFDM(100),SAL(100),PLOSSM(100),AAA(100),
5  BBB(100),IV(101),ITV(100,2),TV(100,2),DTDMV(100,2),
6  BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RHM(100,2),
7  BEH(100,2),PLOSSM(100,2)
  COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500)
  LEVEL 2, A,U,K,RHO
  COMMON /HRBAK/H(4),R(4),B(4),KAK(4),KA(4),RZ,BZ,IH(4)
  INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,
1  UPPER,S1,ST
  INTEGER DUMM
  REAL K,KAK,LAMBDA,LMAX,MH,HLE,MR,MSL,MSP,MV,MVIM1
  DATA IAOVER/0/
C
C COEFP CALCULATES FINITE DIFFERENCE COEFFICIENTS, A, AND CONSTANTS, K
C ALONG VERTICAL MESH LINES WHICH INTERSECT BLADES
C
  ENTRY COEFP
  IF (ITV(IM,1).GT.ITV(IM,2)) RETURN
  ITVU = ITV(IM,1)
  IT = ITVU - 1
  ITVL = ITV(IM,2)
  IPU = IPF(IM,ITVU)
  IPL = IPU+ITVL-ITVU
  DO 90 IP=IPU,IPL
  IT = IT+1
  CALL HRB (DUMM,IM,DUMM,IT,IP)
  DO 10 I=1,4
  KAK(I) = 0.
  10 KAK(I) = 0
C
C FIX HRB VALUES FOR CASES WHERE MESH LINES INTERSECT BLADES
60 IF (IT.EQ.ITV(IM,1)) CALL BDRY12(1,IM,DUMM,IT)
  IF (IT.EQ.ITV(IM,2)) CALL BDRY12(2,IM,DUMM,IT)
  ITVM1 = ITV(IM,1)
  ITVP1 = ITV(IM,1)
  IF (IT.LT.ITVM1) CALL BDRY34(3,IM,1)
  IF (IT.LT.ITVP1) CALL BDRY34(4,IM,1)
  IF (IT.GT.ITV(IM,2)) CALL BDRY34(3,IM,2)
  IF (IT.GT.ITV(IM,2)) CALL BDRY34(4,IM,2)
C
C COMPUTE A AND K COEFFICIENTS
80 CALL AAK (DUMM,IM,DUMM,DUMM,IP)
  DO 90 I=1,4
  K(IP) = K(IP)+KAK(I)*A(IP,I)
  IF (KAK(I).EQ.1) A(IP,I) = 0.
  IF (ABS(A(IP,I)).LE.1.) GO TO 90
  A(IP,I) = SIGN(1.,A(IP,I))
  IAOVER = IAOVER+1
  IF (IAOVER.LT.50) GO TO 90
  WRITE(NWRIT,1000)
  STOP
  90 CONTINUE
  RETURN
C
C COEFP CALCULATES FINITE DIFFERENCE COEFFICIENTS, A, AND CONSTANTS, K
C ALONG ALL VERTICAL MESH LINES WHICH DO NOT INTERSECT BLADES
C
  ENTRY COEFP
  ITVU = ITV(IM,1)
COSUB 15
COSUB 16
COSUB 17
COSUB 18
COSUB 19
COSUB 20
COSUB 21
COSUB 22
COSUB 23
COSUB 24
COSUB 25
COSUB 26
COSUB 27
COSUB 28
COSUB 29
COSUB 30
COSUB 31
COSUB 32
COSUB 33
COSUB 34
COSUB 35
COSUB 36
COSUB 37
COSUB 38
COSUB 39
COSUB 40
COSUB 41
COSUB 42
COSUB 43
COSUB 44
COSUB 45
COSUB 46
COSUB 47
COSUB 48
COSUB 49
COSUB 50
COSUB 51
COSUB 52
COSUB 53
COSUB 54
COSUB 55
COSUB 56
COSUB 57
COSUB 58
COSUB 59
COSUB 60
COSUB 61
COSUB 62
COSUB 63
COSUB 64
COSUB 65
COSUB 66
COSUB 67
COSUB 68
COSUB 69
COSUB 70
COSUB 71
COSUB 72
COSUB 73
COSUB 74

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IT  ITVU-1
ITVL = ITV(IM,2)
IPL = IV(IM+1)-1
IPU = IV(IM)
DO 100 IP=IPU,IPL
IT  IT+1
CALL HRB (DUMM,IM,DUMM,IT,IP)
IF (IT.EQ.ITVU) R(1) = RHO(IPL)
IF (IT.EQ.ITVL) R(2) = RHO(IPU)
CALL AAK (DUMM,IM,DUMM,DUMM,IP)
DO 100 I=1,4
IF (ABS(A(IP,I)).LE.1.) GO TO 100
A(IP,I) = SIGN(1.,A(IP,I))
IAOVER = IAOVER+1
IF (IAOVER.LT.50) GO TO 100
WRITE(NWRIT,1000)
STOP
100 CONTINUE
K(IPL) = K(IPL)+A(IPL,2)
K(IPU) = K(IPU)-A(IPU,1)
RETURN
1000 FORMAT (1H1,5X,81HPROGRAM HAS BEEN STOPPED BECAUSE 50 OF THE A
10EFFICIENTS ARE GREATER THAN 1.0./6X,62HLOCAL SUPERSONIC FLOW MAY
2BE THE CAUSE. TRY A SMALLER REDFAC.)
END
SUBROUTINE HRBAK (I,IM,SURF,IT,IP)
COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIMI,MBIPI,MBOM1,MBOP1,MMH1,
1 HM1,HT,DTLR,DMLR,PITCH,CP,EXPON,TWH,CPTIP,TGROG,TBI,TBO,TWL,
2 WI,MMI,WCRI,ITHIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
3 THLE(2),RMI(2),RMO(2),BESP(50),MV(100),RM(100),BE(100),
4 BEF(100),DBDH(100),DBFDM(100),SAL(100),PLOSIM(100),AAAI(100),
5 BBBI(100),IV(101),ITV(100,2),TV(100,2),DTDMV(100,2),
6 BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RMH(100,2),
7 BEH(100,2),PLOSSM(100,2)
COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500)
LEVEL 2, A,U,K,RHO
COMMON /HRBAK/H(4),R(4),B(4),KAK(4),KA(4),RZ,BZ,IH(4)
COMMON /VARCOM/ RHOMB(100,2),RHOVB(100,2),RMOB(100,2),MTB(100,2),
1 WHCRM(100,2),LABEL(1,100)
INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,
1 UPPER,S1,ST
REAL K,KAK,LAMBDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVIMI
C
C HRB CALCULATES MESH SPACING, H, DENSITIES, RZ AND R, AT GIVEN AND
C ADJACENT POINTS, AND STREAM SHEET THICKNESSES, BZ AND B, AT GIVEN
C AND ADJACENT POINTS
C
ENTRY HRB
H(1) = HT*RM(IM)
H(2) = HT*RM(IM)
H(3) = MV(IM) - MV(IM-1)
H(4) = MV(IM+1)-MV(IM)
RZ = RHO(IP)
IP3 = IPF(IM-1,IT)
IP4 = IPF(IM+1,IT)
R(1) = RHO(IP-1)
R(2) = RHO(IP+1)
R(3) = RHO(IP3)
R(4) = RHO(IP4)
BZ = BE(IM)
COSUB 75 B(3) = BE(IM-1)
COSUB 76 B(4) = BE(IM+1)
COSUB 77 RETURN
COSUB 78 C
COSUB 79 C AAK CALCULATES FINITE DIFFERENCE COEFFICIENTS, A, AND CONSTANT, K,
COSUB 80 C AT A SINGLE MESH POINT
COSUB 81 C
COSUB 82 ENTRY AAK
COSUB 83 A12 = 2./H(1)/H(2)
COSUB 84 A34 = 2./H(3)/H(4)
COSUB 85 AZ = A12+A34
COSUB 86 B12 = (R(2)-R(1))/RZ/(H(1)+H(2))
COSUB 87 B34 = (B(4)*R(4)-B(3)*R(3))/BZ/RZ/(H(3)+H(4))-SAL(IM)/RM(IM)
COSUB 88 A(IP,1) = (2./H(1)+B12)/AZ/(H(1)+H(2))
COSUB 89 A(IP,2) = A12/AZ-A(IP,1)
COSUB 90 A(IP,3) = (2./H(3)+B34)/AZ/(H(3)+H(4))
COSUB 91 A(IP,4) = A34/AZ-A(IP,3)
COSUB 92 K(IP) = -TWH*BZ*RZ*SAL(IM)/AZ
COSUB 93 RETURN
COSUB 94 C
COSUB 95 C BDRY12 CORRECTS VALUES COMPUTED BY HRB WHEN A VERTICAL MESH LINE
COSUB 96 C INTERSECTS A BLADE
COSUB 97 C
COSUB 98 ENTRY BDRY12
COSUB 99 H(I) = ABS(FLOAT(IT)*HT-TV(IM,I))*RM(IM)
HRBAK 2 R(I) = RHOVB(IM,I)
HRBAK 3 KAK(I) = BV(I)
HRBAK 4 KA(I) = 1
HRBAK 5 RETURN
HRBAK 6 C
HRBAK 7 C BDRY34 CORRECTS VALUES COMPUTED BY HRB WHEN A HORIZONTAL MESH LINE
HRBAK 8 C INTERSECTS A BLADE
HRBAK 9 C
HRBAK 10 ENTRY BDRY34
HRBAK 11 IH(SURF) = IH(SURF)+1
HRBAK 12 IHS = IH(SURF)
HRBAK 13 H(I) = ABS(MV(IM)-MH(IHS,SURF))
HRBAK 14 R(I) = RHOHB(IHS,SURF)
HRBAK 15 B(I) = BEH(IHS,SURF)
HRBAK 16 KAK(I) = BV(SURF)
HRBAK 17 KA(I) = 1
HRBAK 18 RETURN
HRBAK 19 END
HRBAK 20 SUBROUTINE SOR
HRBAK 21 C
HRBAK 22 C SOR SOLVES THE SET OF SIMULTANEOUS EQUATIONS FOR THE STREAM FUNCTION
HRBAK 23 C USING THE METHOD OF SUCCESSIVE OVER-RELAXATION
HRBAK 24 C
HRBAK 25 COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
HRBAK 26 COMMON /INPUT/ GAM,AR,TIP,RHOIP,WTFL,OMEGA,ORF,BETAI,BETAD,
HRBAK 27 1 LAMBDA,RVTHO,REDFAC,DENTOL,FSMI,FSMO,SSM1,SSM2,MBI,MBO,MM,
HRBAK 28 2 HBI,NBL,HRSP,MOPT,LOPT,LRVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD,
HRBAK 29 3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),RO(2),BETI(2),BETO(2),
HRBAK 30 4 NSPI(2),TITLEI(20),MR(50),RHSP(50),BESPF(50),WOWCR(50),
HRBAK 31 5 PLOSS(50),MSP(50,2),THSP(50,2)
HRBAK 32 COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIMI,MBIPI,MBOM1,MBOP1,MMH1,
HRBAK 33 1 HM1,HT,DTLR,DMLR,PITCH,CP,EXPON,TWH,CPTIP,TGROG,TBI,TBO,TWL,
HRBAK 34 2 WI,MMI,WCRI,ITHIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
HRBAK 35 3 THLE(2),RMI(2),RMO(2),BESP(50),MV(100),RM(100),BE(100),
HRBAK 36 4 BEF(100),DBDH(100),DBFDM(100),SAL(100),PLOSIM(100),AAAI(100),

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5 BBB(100),IV(101),ITV(100,2),TV(100,2),DTDMV(100,2),      SOR 19      IF (ICOUNT.EQ.(ICOUNT/1000)*1000) WRITE(NWRIT,1000) ORFOPT      SOR 79
6 BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RMH(100,2), SOR 20      IF (ORFTEM-ORFOPT.GT..00001.OR.ORFOPT.GT.1.99) GO TO 40      SOR 80
7 BEH(100,2),PLOSSH(100,2)      SOR 21      WRITE(NWRIT,1000) ORFOPT      SOR 81
COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500)      SOR 22      WRITE(NWRIT,1070) IT      SOR 82
LEVEL 2, A,U,K,RHO      SOR 23      ORF = ORFOPT      SOR 83
INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,      SOR 24      ICOUNT = 0      SOR 84
1 UPPER,S1,ST      SOR 25      GO TO 50      SOR 85
REAL K,KAK,LAMDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVIM1      SOR 26      130 IF (ERSOR.GT.0) WRITE(NWRIT,1040) ERROR      SOR 86
AATEMP = AANDK      SOR 27      IF (ICOUNT.EQ.(ICOUNT/1000)*1000) WRITE(NWRIT,1080) ERROR,ICOUNT      SOR 87
IF (ORF.GE.2.) ORF=0.      SOR 28      IF (ERROR.GT..00003) GO TO 50      SOR 88
ICOUNT = 0      SOR 29      IF (STRFN.LE.0) RETURN      SOR 89
IF (ORF.GT.1.) GO TO 50      SOR 30      C      SOR 90
ORF = 1.      SOR 31      C PRINT STREAM FUNCTION VALUES FOR THIS ITERATION      SOR 91
ORFOPT = 2.      SOR 32      C      SOR 92
40 ORFTEM = ORFOPT      SOR 33      IF (REDFAC.LT.1.) WRITE(NWRIT,1050)      SOR 93
LMAX = 0.      SOR 34      IF (REDFAC.EQ.1.) WRITE(NWRIT,1055)      SOR 94
50 IF (AATEMP.GT.0) WRITE(NWRIT,1010)      SOR 35      DO 140 IM=1,MM      SOR 95
ERROR = 0.      SOR 36      IPU = IV(IM)      SOR 96
ICOUNT = ICOUNT+1      SOR 37      IPL = IV(IM+1)-1      SOR 97
C      SOR 38      ITVU = ITV(IM,1)      SOR 98
C SOLVE MATRIX EQUATION BY SOR, OR CALCULATE OPTIMUM OVERRELAXATION      SOR 39      WRITE(NWRIT,1020) IM,ITVU      SOR 99
C FACTOR      SOR 40      140 WRITE(NWRIT,1060) (U(IP),IP=IPU,IPL)      SOR 100
C      SOR 41      RETURN      SOR 101
      SOR 42      C      SOR 102
      SOR 43      C FORMAT STATEMENTS      SOR 103
      SOR 44      C      SOR 104
      SOR 45      1000 FORMAT (24H ESTIMATED OPTIMUM ORF =,F9.6)      SOR 105
      SOR 46      1010 FORMAT (82H1 IT IP IP1 IP2 IP3 IP4 A(1) A(2)      SOR 106
      SOR 47      1 A(3) A(4) K)      SOR 107
      SOR 48      1020 FORMAT (5HKIM =,I4,6X,6HIT1 =,I4)      SOR 108
      SOR 49      1030 FORMAT (1X,I4,5I6.5F10.5)      SOR 109
      SOR 50      1040 FORMAT (8H ERROR =,F11.8)      SOR 110
      SOR 51      1050 FORMAT (1H1,10X,44HSTREAM FUNCTION VALUES FOR REDUCED MASS FLOW)      SOR 111
      SOR 52      1055 FORMAT (1H1,10X,41HSTREAM FUNCTION VALUES FOR FULL MASS FLOW)      SOR 112
      SOR 53      1060 FORMAT (2X,10F13.8)      SOR 113
      SOR 54      1070 FORMAT(1H,* IT = *,I6)      SOR 114
      SOR 55      1080 FORMAT (8H ERROR =,G14.4,7H AFTER ,I6,11H ITERATIONS)      SOR 115
      SOR 56      END      SOR 116
      SOR 57      SUBROUTINE VELMER      VELMER 2
      SOR 58      C      VELMER 3
      SOR 59      C VELMER CALLS VELPM AND VELBM TO CALCULATE RHO*W-SUB-M THROUGHOUT THE      VELMER 4
      SOR 60      C REGION AND ON THE BLADE SURFACES      VELMER 5
      SOR 61      C      VELMER 6
      SOR 62      COMMON /INPUTT/ GAM,AR,TIP,RHOIP,HTFL,OMEGA,ORF,BETAI,BETA0,      VELMER 7
      SOR 63      1 LAMBDA,RVTHO,REDFAC,DENTOL,FSMI,FSMO,SSH1,SSH2,MBI,MBO,MH,      VELMER 8
      SOR 64      2 NBBI,LBL,NRSP,MOPT,LOPT,LRVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD,      VELMER 9
      SOR 65      3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),ROI(2),BETI(2),BETO(2),      VELMER10
      SOR 66      4 NSPI(2),TITLEI(20),MR(50),RMSPI(50),BESPF(50),MOWCR(50),      VELMER11
      SOR 67      5 PLOSS(50),MSP(50,2),THSPI(50,2)      VELMER12
      SOR 68      COMMON /CALCON/ ACTWT,ACTOMS,ACTLAM,MBIH1,MBIP1,MBOH1,MBOP1,MMH1,      VELMER13
      SOR 69      1 HM1,HT,OTLR,OMLR,PITCH,CP,EXPON,TWH,CPTIP,TGROG,TBI,TBO,TWL,      VELMER14
      SOR 70      2 WI,WMI,MCRI,ITHIN,ITHAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),      VELMER15
      SOR 71      3 THLE(2),RMI(2),RMO(2),BESPI(50),HV(100),RMI(100),BEI(100),      VELMER16
      SOR 72      4 BEFI(100),DBDH(100),DBFDH(100),SAL(100),PLOSSH(100),AAA(100),      VELMER17
      SOR 73      5 BBB(100),IV(101),ITV(100,2),TV(100,2),DTDMV(100,2),      VELMER18
      SOR 74      6 BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RMH(100,2),      VELMER19
      SOR 75      7 BEH(100,2),PLOSSH(100,2)      VELMER20
      SOR 76      INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,      VELMER21
      SOR 77      1 UPPER,S1,ST      VELMER22
      SOR 78      REAL K,KAK,LAMDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVIM1      VELMER23

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C
C CALL VELPM AND VELBM THROUGHOUT THE REGION
C
      ITVU = ITV(1,1)
      ITVL = ITV(1,2)
      DO 10 IM=1,MBIM1
10 CALL VELPM(IM,ITVU,ITVL)
      DO 20 IM=MBI,MBO
      I = 0
20 CALL VELBM(IM)
      ITVU = ITV(MBOP1,1)
      ITVL = ITV(MBOP1,2)
      DO 30 IM=MBOP1,MM
30 CALL VELPM(IM,ITVU,ITVL)
      RETURN
      END
      SUBROUTINE VELSUB (IM,ITVU,ITVL)
C
C VELSUB CALCULATES RHO*W-SUB-M THROUGHOUT THE REGION AND ON THE BLADE
C SURFACES, AND CALCULATES THE STREAMLINE LOCATIONS
C
      COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
      COMMON /INPUT/ GAM,AR,TIP,RHOIP,WTF,OMEGA,ORF,BETA1,BETA0,
1 LAMBDA,RVTHO,REDFAC,DENTOL,FSM1,FSM0,SSM1,SSM2,MBI,MBO,MM,
2 NBB1,NBL,NRSP,MOPT,LOPT,LQVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD,
3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),RO(2),BET1(2),BET0(2),
4 NSPI(2),TITLE(20),HR(50),RHSP(50),BESPF(50),WOWCR(50),
5 PLOSS(50),MSP(50,2),THSP(50,2)
      COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIM1,MBIP1,MBOM1,MBOP1,MM1,
1 HM1,HT,DTLR,DMLR,PITCH,CP,EXPON,TWM,CPTIP,TGROG,TBI,TBO,TWL,
2 W1,WM1,WCR1,ITMIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
3 THLE(2),RMI(2),RMO(2),BESP(50),MV(100),RMI(100),BE(100),
4 BEF(100),DBDH(100),DBFDM(100),SAL(100),PLOSIM(100),AAA(100),
5 BBB(100),IV(101),ITV(100,2),TV(100,2),DTDMV(100,2),
6 BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RHH(100,2),
7 BEH(100,2),PLOSMH(100,2)
      COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500)
      LEVEL 2, A,U,K,RHO
      COMMON /VARCOM/ RHOHB(100,2),RHOVB(100,2),HMB(100,2),WTB(100,2),
1 WRCRM(100,2),LABEL(1,100)
      DIMENSION W(2500),BETA(2500),DUDT(2500),DUDTT(2500),AAP(2500),
1 BBP(2500)
      LEVEL 2, W,BETA,DUDT,DUDTT,AAP,BBP
      EQUIVALENCE (A,W),(A(1,2),BETA),(A(1,3),DUDT),(A(1,4),DUDTT),
1 (K,AAP),(RHO,BBP)
      COMMON /SLCOM/ USL(100,11),TSL(100,11)
      LEVEL 2, USL,TSL
      COMMON /PLTCOM/ TSLPT(1100),XDOWN(400),YACROS(400)
      LEVEL 2, TSLPT,XDOWN,YACROS
      DIMENSION TSP(51),USP(51),DDT(51),UINT(11),TINT(11)
      INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,
1 UPPER,S1,ST
      REAL K,KAK,LAMBDA,LMAX,MH,MLE,HR,MSL,MSP,MV,MVIM1
C
C VELPM CALCULATES ALONG VERTICAL MESH LINES WHICH DO NOT
C INTERSECT BLADES
C
      ENTRY VELPM
5 NSL = 5
      NSLM1 = NSL-1
      VELMER24
      VELMER25
      VELMER26
      VELMER27
      VELMER28
      VELMER29
      VELMER30
      VELMER31
      VELMER32
      VELMER33
      VELMER34
      VELMER35
      VELMER36
      VELMER37
      VELMER38
      VELMER39
      VELSUB 2
      VELSUB 3
      VELSUB 4
      VELSUB 5
      VELSUB 6
      VELSUB 7
      VELSUB 8
      VELSUB 9
      VELSUB10
      VELSUB11
      VELSUB12
      VELSUB13
      VELSUB14
      VELSUB15
      VELSUB16
      VELSUB17
      VELSUB18
      VELSUB19
      VELSUB20
      VELSUB21
      VELSUB22
      VELSUB23
      VELSUB24
      VELSUB25
      VELSUB26
      VELSUB27
      VELSUB28
      VELSUB29
      VELSUB30
      VELSUB31
      VELSUB32
      VELSUB33
      VELSUB34
      VELSUB35
      VELSUB36
      VELSUB37
      VELSUB38
      VELSUB39
      VELSUB40
      VELSUB41
      VELSUB42
      VELSUB43
      VELSUB44
      VELSUB45
      LOC = 0
      NSP = ITVL-ITVU+2
      IP = IV(IM)-1
      DO 10 IT=1,NSP
      IP = IP+1
      TSP(IT) = FLOAT(IT+ITVU-1)*HT
10 USP(IT) = U(IP)
      USP(NSP) = USP(1)*1.
      IP = IV(IM)
      INTU = INT(U(IP)*FLOAT(NSLM1))
      IF (U(IP).GT.0.) INTU=INTU+1
      DO 20 J=1,NSLM1
      UINT(J) = FLOAT(INTU)/FLOAT(NSLM1)
20 INTU = INTU+1
      UINT(NSL) = UINT(1)
      CALL SPLIPR(HT,USP,NBBI,DDT,AAA)
      GO TO 100
C
C VELBM CALCULATES ALONG VERTICAL MESH LINES WHICH INTERSECT BLADES
C
      ENTRY VELBM
      LOC = 1
      ITVUP1 = ITV(IM,1)
      ITVLM1 = ITV(IM,2)
      ITVU = ITVUP1-1
      ITVL = ITVLM1+1
      NSP = ITVL-ITVU+1
      TSP(1) = TV(IM,2)
      TSP(NSP) = TV(IM,1)
      USP(1) = BV(1)
      USP(NSP) = BV(2)
      IP = IV(IM)-1
      NSPM1 = NSP-1
      IF (.GT.NSPM1) GO TO 70
      DO 60 IT=2,NSPM1
      IP = IP+1
      TSP(IT) = FLOAT(IT+ITVU-1)*HT
60 USP(IT) = U(IP)
      DO 80 I=1,NSL
80 UINT(I) = FLOAT(I-1)/FLOAT(NSLM1)
      CALL SPLINE(TSP,USP,NSP,DDT,AAA)
C
C FOR VELPM AND VELBM, CALCULATE RHO*W-SUB-M IN THE REGION
C FOR VELBM, CALCULATE RHO*W AT VERTICAL MESH LINE INTERSECTIONS WITH
C BLADE SURFACES
C
100 CONTINUE
      IT = LOC
      IPU = IV(IM)
      IPL = IV(IM+1)-1
      DO 110 IP=IPU,IPL
      IT = IT+1
      DUDT(IP) = DDT(IT)
110 DUDTT(IP) = AAA(IT)
120 IF (LOC.EQ.0) GO TO 130
      WMB(IM,1) = DDT(1)*WTF/BE(IM)/RM(IM)
      WMB(IM,2) = DDT(NSP)*WTF/BE(IM)/RM(IM)
      RMDTU2 = (RMI(IM)*DTDMV(IM,1))*2
      RMDTL2 = (RMI(IM)*DTDMV(IM,2))*2
      IF (RMDTU2.GT.10000.) WND(IM,1) = 0.
      VELSUB46
      VELSUB47
      VELSUB48
      VELSUB49
      VELSUB50
      VELSUB51
      VELSUB52
      VELSUB53
      VELSUB54
      VELSUB55
      VELSUB56
      VELSUB57
      VELSUB58
      VELSUB59
      VELSUB60
      VELSUB61
      VELSUB62
      VELSUB63
      VELSUB64
      VELSUB65
      VELSUB66
      VELSUB67
      VELSUB68
      VELSUB69
      VELSUB70
      VELSUB71
      VELSUB72
      VELSUB73
      VELSUB74
      VELSUB75
      VELSUB76
      VELSUB77
      VELSUB78
      VELSUB79
      VELSUB80
      VELSUB81
      VELSUB82
      VELSUB83
      VELSUB84
      VELSUB85
      VELSUB86
      VELSUB87
      VELSUB88
      VELSUB89
      VELSUB90
      VELSUB91
      VELSUB92
      VELSUB93
      VELSUB94
      VELSUB95
      VELSUB96
      VELSUB97
      VELSUB98
      VELSUB99
      VELSUB100
      VELSUB101
      VELSUB102
      VELSUB103
      VELSUB104
      VELSUB105

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IF (RMDTL2.GT.10000.) WMB(IM,2) = 0.
WMB(IM,1) = WMB(IM,1)*SQRT(1.+RMDTU2)
WMB(IM,2) = WMB(IM,2)*SQRT(1.+RMDTL2)
130 IF (SLCPD.LE.0) RETURN
CALL SPLINT(USP,TSP,NSP,UINT,HSL,TINT,AAA,BBB)
DO 140 J=1,HSL
USL(IM,J) = UINT(J)
TSL(IM,J) = TINT(J)
L = (J-1)*MM*IM
140 TSLPT(L) = TINT(J)
RETURN
END
SUBROUTINE VELTAN
C
C VELTAN CALCULATES RHO*M-SUB-THETA AND THEN RHO*M THROUGHOUT THE
C REGION AND ON THE BLADE SURFACES, AND CALCULATES BETA
C THROUGHOUT THE REGION
C
COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
COMMON /INPUT/ GAM,AR,TIP,RHOIP,WFL,OMEGA,ORF,BETA1,BETA0,
1 LAMBDA,RVTHO,REFAC,DENTOL,FSMI,FSMO,SSM1,SSM2,MBI,MBO,MM,
2 NBI,NBL,NRSP,MOPT,LOPT,LRVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD,
3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),RO(2),BETI(2),BETO(2),
4 NSPI(2),TITLEI(20),MR(50),RMSPI(50),BESPI(50),WOWCR(50),
5 PLOSSI(50),HSP(50,2),THSP(50,2)
COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIM1,MBIP1,MBOM1,MBOP1,MMH1,
1 HM1,HT,DTLR,DHLR,PITCH,CP,EXPON,TMM,CPTIP,TGROG,TBI,TBO,TML,
2 WI,WMI,WCRI,ITMIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
3 THLE(2),RMI(2),RHO(2),BESPI(50),MV(100),RMI(100),BE(100),
4 BEF(100),DBDM(100),DBFDM(100),SAL(100),PLOSIM(100),AAA(100),
5 BBB(100),IV(101),ITV(100,2),TV(100,2),DTDMV(100,2),
6 BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RHH(100,2),
7 BEH(100,2),PLOSSMH(100,2)
COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500)
LEVEL 2, A,U,K,RHO
COMMON /VARCOM/ RHOHB(100,2),RHOVB(100,2),WMB(100,2),WTB(100,2),
1 WWCRI(100,2),LABEL(1,100)
DIMENSION W(2500),BETA(2500),DUOT(2500),DUOTT(2500),AAP(2500),
1 BBP(2500)
LEVEL 2, W,BETA,DUOT,DUOTT,AAP,BBP
EQUIVALENCE (A,W),(A(1,2),BETA),(A(1,3),DUOT),(A(1,4),DUOTT),
1 (K,AAP),(RHO,BBP)
DIMENSION SPM(100),USP(100),DDT(100),DUDM(100),DUDMH(100),
1 DUDTM(100),DWM(100),WIP(100)
INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,
1 UPPER,S1,ST
REAL K,KAK,LAMEDA,LMAX,MI,MLE,MR,MSL,HSP,MV,MVIM1
EXTERNAL BL1,BL2
C
C PERFORM CALCULATIONS ALONG ONE HORIZONTAL LINE AT A TIME
C
IT = ITMIN
10 IF (IT.GT.ITMAX) RETURN
S1 = 0
C
C ON THE GIVEN HORIZONTAL MESH LINE, FIND A FIRST POINT IN THE REGION
C
IF (IT.GE.0.AND.IT.LT.NBI) GO TO 60
IM = MBIM1
20 IM = IM+1
VELSU106
VELSU107
VELSU108
VELSU109
VELSU110
VELSU111
VELSU112
VELSU113
VELSU114
VELSU115
VELSU116
VELSU117
VELTAN 2
VELTAN 3
VELTAN 4
VELTAN 5
VELTAN 6
VELTAN 7
VELTAN 8
VELTAN 9
VELTAN10
VELTAN11
VELTAN12
VELTAN13
VELTAN14
VELTAN15
VELTAN16
VELTAN17
VELTAN18
VELTAN19
VELTAN20
VELTAN21
VELTAN22
VELTAN23
VELTAN24
VELTAN25
VELTAN26
VELTAN27
VELTAN28
VELTAN29
VELTAN30
VELTAN31
VELTAN32
VELTAN33
VELTAN34
VELTAN35
VELTAN36
VELTAN37
VELTAN38
VELTAN39
VELTAN40
VELTAN41
VELTAN42
VELTAN43
VELTAN44
VELTAN45
VELTAN46
VELTAN47
VELTAN48
VELTAN49
IF (IM.GT.MBOP1) GO TO 200
SURF = 1
IF (IT.GE.ITV(IM,1).AND.IT.LT.ITV(IM-1,1)) GO TO 70
IF (IM.EQ.MBOP1.AND.IT.EQ.ITV(MBO,1)-1.AND.ITV(MBO,1))-ITV(MBO,2)
1 +NBI.EQ.2) GO TO 70
SURF = 2
IF (IT.LE.ITV(IM,2).AND.IT.GT.ITV(IM-1,2)) GO TO 70
GO TO 20
C
C FIRST POINT IS ON BOUNDARY A-H
C
60 IM1 = 1
IM = 1
SPM(1) = MV(1)
USP(1) = U(IT+1)
GO TO 90
C
C FIRST POINT IS ON A BLADE SURFACE
C
70 S1 = SURF
IM1 = IM 1
IM2 = IM
TH = FLOAT(IT)*HT
MVIM1 = MV(IM1)
IF (IM.EQ.MBIP1) MVIM1 = MVIM1+(MV(IM2)-MVIM1)/1000.
LER(2) = 5
C
C BLCD (VIA ROOT) CALL NO. 5
IF (S1.EQ.1.AND.IM1.NE.MBO) CALL ROOT(MVIM1,MV(IM2),TH,BL1,DTLR,
1 ANS,AAA)
LER(2) = 6
C
C BLCD (VIA ROOT) CALL NO. 6
IF (S1.EQ.2) CALL ROOT(MVIM1,MV(IM2),TH,BL2,DTLR,ANS,AAA)
IF (S1.EQ.1.AND.IM1.EQ.MBO) ANS = MV(MBO)
SPM(IM1) = ANS
USP(IM1) = BV(S1)
C
C MOVE ALONG HORIZONTAL MESH LINE UNTIL MESH LINE INTERSECTS BOUNDARY
C
90 IF (IM.LT.MBI.OR.IM.GT.MBO) GO TO 120
SURF = 1
IF (IT.LT.ITV(IM,SURF).AND.IT.GE.ITV(IM-1,SURF)) GO TO 140
SURF = 2
IF (IT.GT.ITV(IM,SURF).AND.IT.LE.ITV(IM-1,SURF)) GO TO 140
120 SPM(IM) = MV(IM)
IP = IPF(IM,IT)
USP(IM) = U(IP)
IF (IM.EQ.MM) GO TO 130
IM = IM+1
GO TO 90
C
C FINAL POINT IS ON BOUNDARY D-E
C
130 IMT = MM
GO TO 150
C
C FINAL POINT IS ON A BLADE SURFACE
C
140 ST = SURF
IMT = IM
IMTH1 = IMT-1
VELTAN50
VELTAN51
VELTAN52
VELTAN53
VELTAN54
VELTAN55
VELTAN56
VELTAN57
VELTAN58
VELTAN59
VELTAN60
VELTAN61
VELTAN62
VELTAN63
VELTAN64
VELTAN65
VELTAN66
VELTAN67
VELTAN68
VELTAN69
VELTAN70
VELTAN71
VELTAN72
VELTAN73
VELTAN74
VELTAN75
VELTAN76
VELTAN77
VELTAN78
VELTAN79
VELTAN80
VELTAN81
VELTAN82
VELTAN83
VELTAN84
VELTAN85
VELTAN86
VELTAN87
VELTAN88
VELTAN89
VELTAN90
VELTAN91
VELTAN92
VELTAN93
VELTAN94
VELTAN95
VELTAN96
VELTAN97
VELTAN98
VELTAN99
VELTA100
VELTA101
VELTA102
VELTA103
VELTA104
VELTA105
VELTA106
VELTA107
VELTA108
VELTA109

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TH = FLOAT(IT)*HT
MVIMI = MV(IMTHI)
IF (IM.EQ.HBIP1) MVIMI = MVIMI+(MV(IMT)-MVIMI)/1000.
LER(2) = 7
C
BLCD (VIA ROOT) CALL NO. 7
IF (ST.EQ.1.AND.IMT.NE.MBI) CALL ROOT(MVIMI,MV(IMT),TH,BL1,
1 DTLR,ANS,AAA)
LER(2) = 8
C
BLCD (VIA ROOT) CALL NO. 8
IF (ST.EQ.2) CALL ROOT(MVIMI,MV(IMT),TH,BL2,DTLR,ANS,AAA)
IF (ST.EQ.1.AND.IMT.EQ.MBI) ANS=MV(MBI)
SPM(IMT) = ANS
USP(IMT) = BV(ST)
150 NSP = IMT-IMI*1
CALL SPLINE(SPM(IMI),USP(IMI),NSP,DUDM(IMI),DUDMH(IMI))
C
C CALCULATE RHO*W ON THE BLADE SURFACES
C
FIRST = 1
LAST = MM
IF (IMI.EQ.1) GO TO 160
FIRST = IM2
CALL SEARCH (SPM(IMI),S1,IHS)
ANS = DUDM(IMI)*MTFL/BEH(IHS,S1)
IF (S1.EQ.2) ANS=-ANS
MTB(IHS,S1) = ANS*SQRT(1.+1./(RHM(IHS,S1)*DUDMH(IHS,S1)**2)
DDT(IMI) = -DUDM(IMI)/DUDMH(IHS,S1)
WIP(IMI) = MTB(IHS,S1)/RHOHB(IHS,S1)
160 IF (IMT.EQ.MI) GO TO 170
LAST = IMTHI
CALL SEARCH (SPM(IMT),ST,IHS)
ANS = DUDM(IMT)*MTFL/BEH(IHS,ST)
IF (ST.EQ.1) ANS=-ANS
MTB(IHS,ST) = ANS*SQRT(1.+1./(RHM(IHS,ST)*DUDMH(IHS,ST)**2)
DDT(IMT) = -DUDM(IMT)/DUDMH(IHS,ST)
WIP(IMT) = MTB(IHS,ST)/RHOHB(IHS,ST)
C
C CALCULATE RHO*W-SUB-THETA AND THEN RHO*W AND BETA IN THE REGION
C
170 IF (FIRST.GT.LAST) GO TO 190
DO 180 I=FIRST, LAST
IP = IPFI,IT)
DDT(I) = DUOT(IP)
RHM = DDT(I)/RMI(I)
RHT = -DUDM(I)
WIP) = SQRT(RHT**2+RHM**2)/BE(I)*MTFL
TMLR = 2.*OMEGA*LAMBDA-(OMEGA*RMI(I))**2
RHOIPL = RHOIP*(1.-PLOSIM(I))
LER(1) = 6
C
DENSTY CALL NO. 6
RHOTEM=RHOIIP)
WTEM=W(IP)
CALL DENSTY(WTEM,RHOTEM,ANS,TMLR,CPTIP,EXPON,RHOIPL,GAM,AR,TIP,
1 J2)
RHOIIP)=RHOTEM
WIP)=WTEM
WIP) = ANS
WIP(I) = WIP)
BETA(IP) = ATAN2(RHT,RHM)*57.295779
180 CONTINUE

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VELTA110
VELTA111
VELTA112
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VELTA167
VELTA168
VELTA169

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IF (IEND.LT.0) GO TO 190
CALL SPLINE (SPM(IMI),DDT(IMI),NSP,DUDM(IMI),AAA(IMI))
CALL SPLINE (SPM(IMI),WIP(IMI),NSP,DUDM(IMI),AAA(IMI))
DO 185 I=FIRST, LAST
IP = IPFI,IT)
SBETA = SIN(BETA(IP)/57.295779)
CBETA = SQRT(1.-SBETA**2)
AAPIP) = SBETA**2*(2.*DUDM(I)/DUDM(I)-DUOT(IP)/DUDM(I)**2+
1 DUDM(I)-DUOT(IP)/DUOT(IP))*SAL(I)*SBETA/CBETA*(1.+CBETA**2)
BBPIP) = RMI(I)/CBETA*(2.*ACTOMG*SAL(I)+SBETA*DUDM(I)/REDFAC)
185 CONTINUE
190 CONTINUE
IF (IMT.NE.MM) GO TO 20
200 IT = IT+1
GO TO 10
END
SUBROUTINE SEARCH (DIST,SURF,IS)
C
C SEARCH LOCATES THE POSITION OF A GIVEN VALUE OF M IN THE MH ARRAY
C
COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIMI,MBIP1,MBOM1,MBOP1,MMH1,
1 MH1,HT,DTLR,DMLR,PITCH,CP,EXPON,TMW,CPTIP,TGROG,TBI,TBO,TWL,
2 MI,MMI,MCRI,ITHIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
3 THLE(2),RMI(2),RMO(2),BESPI(50),MVI(100),RMI(100),BE(100),
4 BEF(100),DBDM(100),DBFDM(100),SAL(100),PLOSIM(100),AAAL(100),
5 BBBI(100),IV(101),ITV(100,2),TV(100,2),DUDMH(100,2),
6 BETAV(100,2),MH(100,2),DUDMI(100,2),BETAH(100,2),RMI(100,2),
7 BEH(100,2),PLOSMH(100,2)
INTEGER BLDAT,AAANDK,ERSOR,STRFN,SLCRD,SURVL,AAATEMP,SURF,FIRST,
1 UPPER,S1,ST
REAL K,KAK,LAMBDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVIMI
DO 10 I=1,100
IF (ABS(MH(I),SURF)-DIST).GT.DMLR) GO TO 10
IS = I
RETURN
10 CONTINUE
WRITE(NWRIT,1000) DIST,SURF
STOP
1000 FORMAT (30H SEARCH CANNOT FIND M IN THE MH ARRAY/7H DIST =,G14.6,
110X,6HSURF =,G14.6)
END
SUBROUTINE STRLIN
C
C STRLIN CALCULATES, PRINTS, AND PLOTS THE STREAMLINE OUTPUT DATA
C
COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
COMMON /INPUT/ GAM,AR,TIP,RHOIP,MTFL,OMEGA,ORF,BETA1,BETA0,
1 LAMBDA,RVTHO,REDFAC,DENTOL,FSMI,FSMO,SSM1,SSM2,MBI,MO,MM,
2 NGBI,NBL,NRSP,HOPT,LOPT,LRVB,BLDAT,AAANDK,ERSOR,STRFN,SLCRD,
3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),RO(2),BETI(2),BETO(2),
4 NSPI(2),TITLEI(20),MR(50),RHSP(50),BESPF(50),MONCR(50),
5 PLOSSI(50),MSP(50,2),THSPI(50,2)
COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIMI,MBIP1,MBOM1,MBOP1,MMH1,
1 MH1,HT,DTLR,DMLR,PITCH,CP,EXPON,TMW,CPTIP,TGROG,TBI,TBO,TWL,
2 MI,MMI,MCRI,ITHIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
3 THLE(2),RMI(2),RMO(2),BESPI(50),MVI(100),RMI(100),BE(100),
4 BEF(100),DBDM(100),DBFDM(100),SAL(100),PLOSIM(100),AAA(100),
5 BBBI(100),IV(101),ITV(100,2),TV(100,2),DUDMH(100,2),
6 BETAV(100,2),MH(100,2),DUDMI(100,2),BETAH(100,2),RMI(100,2),

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7 BEH(100,2),PLOSMH(100,2)
COMMON /SLCOM/ USL(100,11),TSL(100,11)
LEVEL 2, USL,TSL
COMMON /PLTCOM/ TSLPT(1100),XDOWN(400),YACROS(400)
LEVEL 2, TSLPT,XDOWN,YACROS
COMMON /DUM1/ MSL(100)
LEVEL 2, MSL
DIMENSION DTDH(100),D2TDM2(100),KKK(24),P(11)
INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,
1 UPPER,S1,ST
REAL K,KAK,LAMBDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVIMI
DATA KKK(4)/1H*/,KKK(6)/1H*/,KKK(8)/1H*/,KKK(10)/1H*/,KKK(12)/1H*/,KKK(14)/1H*/,
1 KKK(16)/1H*/,KKK(18)/1H*/,KKK(20)/1H*/,
2 KKK(22)/1H*/,KKK(24)/1H*/
C
C CALCULATE AND PRINT STREAMLINE OUTPUT DATA
C
IF (SLCRD.LE.0) RETURN
NSL = 5
MML = MBO-MBI+1
RADDEG = 180./3.1415927
IF (REDFAC.LT.1.) WRITE(NWRIT,1000)
IF (REDFAC.EQ.1.) WRITE(NWRIT,1010)
DO 70 J=1,NSL
TSLTEM=TSL(MBI,J)
CALL SPLINE(MV(MBI),TSLTEM,MML,DTDH(MBI),D2TDM2(MBI))
TSL(MBI,J)=TSLTEM
WRITE(NWRIT,1020) J
DO 40 IM=1,MBIMI
40 WRITE(NWRIT,1030) IM,MV(IM),RM(IM),USL(IM,J),TSL(IM,J)
DO 50 IM=MBO
BETASL = ATAN(RM(IM)*DTDH(IM))*RADDEG
CURVSL = (RM(IM)*D2TDM2(IM)+SAL(IM)*DTDH(IM))/(1.+(RM(IM)*
1 DTDH(IM))*2)**1.5
IF (DTDH(IM).NE.0.) DTDH=-1./RM(IM)**2/DTDH(IM)
IF (DTDH(IM).EQ.0.) DTDH=1.E10
50 WRITE(NWRIT,1040) IM,MV(IM),RM(IM),USL(IM,J),TSL(IM,J),DTDH(IM),
1 DTDH,M,BETASL,CURVSL
DO 60 IM=MBOPI,MM
60 WRITE(NWRIT,1030) IM,MV(IM),RM(IM),USL(IM,J),TSL(IM,J)
70 CONTINUE
C
C PLOT STREAMLINES
C
KKK(1) = 7
KKK(2) = NSL
KKK(3) = MM
P(1) = 1.
P(3) = 0.
P(4) = 0.
DO 80 IM=1,MM
80 MSL(IM) = MV(IM)
IF (REDFAC.LT.1.) WRITE(NWRIT,1050)
IF (REDFAC.EQ.1.) WRITE(NWRIT,1060)
CALL PLOTHY(MSL,TSLPT,KKK,P)
WRITE(NWRIT,1070)
RETURN
C
C FORMAT STATEMENTS
C
STRLIN20 1000 FORMAT (1H1,2X,44HSTREAMLINE COORDINATES FOR REDUCED MASS FLOW)
STRLIN21 1010 FORMAT (1H1,2X,41HSTREAMLINE COORDINATES FOR FULL MASS FLOW)
STRLIN22 1020 FORMAT (////4X,14HSTREAMLINE NO.,I3,23H - WITHIN BLADE REGION//
STRLIN23 1 8X,2HIM,8X,1HM,14X,1HR,13X,3HUSL,12X,3HTSL,12X,4HODM,10X,
STRLIN24 2 5HODMH,10X,6HBETASL,9X,6HCURVSL)
STRLIN25 1030 FORMAT (7X,I3,2G15.5,3X,F7.3,5X,G15.5)
STRLIN26 1040 FORMAT (7X,I3,2G15.5,3X,F7.3,5X,G15.5,3X,F7.2,5X,G15.5)
STRLIN27 1050 FORMAT (1H1,50X,30HSTREAMLINE PLOTS FOR REDUCED MASS FLOW)
STRLIN28 1060 FORMAT (1H1,50X,35HSTREAMLINE PLOTS FOR FULL MASS FLOW)
STRLIN29 1070 FORMAT ( /40X,70HSTREAMLINES ARE PLOTTED WITH THETA ACROSS THE
STRLIN30 1PAGE AND M DOWN THE PAGE)
STRLIN31 END
STRLIN32 SUBROUTINE OUTPUT
STRLIN33 C
STRLIN34 C OUTPUT CALLS SUBROUTINES TO CALCULATE DENSITIES AND VELOCITIES
STRLIN35 C THROUGHOUT THE REGION AND ON THE BLADE SURFACES, AND IT PLOTS
STRLIN36 C THE SURFACE VELOCITIES
STRLIN37 C
STRLIN38 DIMENSION PRES(100,2),PRATIO(100,2),XVDIM(100),CPT(100,2)
STRLIN39 COMMON NREAD,NHRIT,ITER,IEHD,LER(2),NER(2)
STRLIN40 COMMON /IHPUTT/ GAM,AR,TIP,RHOIP,WTL,OMEGA,ORF,BETAI,BETAO,
STRLIN41 1 LAMBDA,RVTHO,REDFAC,DENTOL,FSMI,FSMO,SSM1,SSM2,MBI,MBO,MM,
STRLIN42 2 NBI,NBL,NRSP,MOPT,LOPT,LRVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD,
STRLIN43 3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),RO(2),BETI(2),BETO(2),
STRLIN44 4 NSPI(2),TITLEI(20),MR(50),RMSP(50),BESPF(50),HOWCR(50),
STRLIN45 5 PLOSS(50),MSP(50,2),THSPI(50,2)
STRLIN46 COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIMI,MBIP1,MBOH1,MBOPI,MMH1,
STRLIN47 1 HMI,HT,DYLR,DMLR,PITCH,CP,EXPN,TWH,CPTIP,TGROG,TBI,TBO,TWL,
STRLIN48 2 WI,WMI,WCRI,ITHIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
STRLIN49 3 THLE(2),RHII(2),RHOI(2),BESP(50),MV(100),RH(100),BE(100),
STRLIN50 4 BEF(100),DBDM(100),DBFDM(100),SAL(100),PLOSIM(100),AAA(100),
STRLIN51 5 BBB(100),IV(101),ITV(100,2),TV(100,2),DTDMV(100,2),
STRLIN52 6 BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RHM(100,2),
STRLIN53 7 BEH(100,2),PLOSMH(100,2)
STRLIN54 COMMON /VARCOM/ RHOHB(100,2),RHOVB(100,2),HMB(100,2),WTB(100,2),
STRLIN55 1 WHCRM(100,2),LABEL(1,100)
STRLIN56 COMMON /PLTCOM/ TSLPT(1100),XDOWN(400),YACROS(400)
STRLIN57 LEVEL 2, TSLPT,XDOWN,YACROS
STRLIN58 DIMENSION KKK(14)
STRLIN59 DIMENSION P(11)
STRLIN60 INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,
STRLIN61 1 UPPER,S1,ST
STRLIN62 REAL K,KAK,LAMBDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVIMI
STRLIN63 DATA KKK(4)/1H*/,KKK(6)/1H*/,KKK(8)/1H*/,KKK(10)/1H*/,
C
C CALL VELP, VELB, AND VELSUR THROUGHOUT THE REGION
C
IF (INTVL.GT.0) CALL VELP(1,MBIMI)
CALL VELB(MBI,MBO)
20 IF (INTVL.GT.0) CALL VELP(MBOPI,MM)
CALL VELSUR
C
C PREPARE INPUT ARRAYS FOR PLOT OF VELOCITIES
C
IF (SURVL.LE.0) RETURN
NP2 = 0
C
C TANGENTIAL COMPONENTS
DO 50 SURF=1,2
NPI = NP2
STRLIN78
STRLIN79
STRLIN80
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STRLIN176
STRLIN177
STRLIN178
STRLIN179

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IMSS = IMS(SURF)
IF (IMSS.LT.1) GO TO 40
DO 30 IMS=1,IMSS
IF (ABS(DTDMH(IHS,SURF)*RMH(IHS,SURF)).LT..57735) GO TO 30
NP1 = NP1+1
YACROS(NP1) = MTB(IHS,SURF)
XDDWN(NP1) = MH(IHS,SURF)
30 CONTINUE
40 KKK(2*SURF+1) = NP1-NP2
50 NP2 = NP1
C
C MERIDIONAL COMPONENTS
DO 80 SURF=1,2
NP1 = NP2
DO 60 IM=MBIP1,MBOH1
IF (ABS(DTDMV(IM,SURF)*RMH(IM)).GT.1.7321) GO TO 60
NP1 = NP1+1
YACROS(NP1) = MMB(IM,SURF)
XDDWN(NP1) = MV(IM)
60 CONTINUE
70 KKK(2*SURF+5) = NP1-NP2
80 NP2 = NP1
C
C PLOT VELOCITIES
KK1 = KKK(3)
KK2 = KKK(5)
KK3 = KKK(7)
KK4 = KKK(9)
IF (BLDAT.GE.2) CALL VEPL0T(KK1,KK2,KK3,KK4)
KKK(1) = 1
KKK(2) = 4
P(1) = 5.
IF (REDFAC.LT.1.) WRITE(NWRIT,1000)
IF (REDFAC.EQ.1.) WRITE(NWRIT,1020)
CALL PLOTMY(XDDWN,YACROS,KKK,P)
WRITE(NWRIT,1010)
PTOTAL = RHOIP*AR*TIP
DO 90 IS= 1,2
PRESIN = PTOTAL
DO 90 IM = MBI,MBO
XVDIM(IM)=MV(IM)/MV(MBO)
TWLMI = 2.*OMEGA*LAMBDA - (OMEGA*RMH(IM))*2
PRES(IM,IS) = PTOTAL*(1.-PLOSIM(IM))*(1.-(MMB(IM,IS))*2+TWLMI/
1 CPTIP)**(GAM/(GAM-1.))
PRATIO(IM,IS)=PRES(IM,IS)/PRESIN
CPT(IM,IS)=PRATIO(IM,IS)-1.
90 CONTINUE
IF (REDFAC.LT.1.) WRITE (NWRIT,998)
IF (REDFAC.EQ.1.) WRITE (NWRIT,999)
WRITE(6,1100)
DO 91 IM = MBI,MBO
WRITE (6,1001)IM,MV(IM),XVDIM(IM),PRATIO(IM,1),PRATIO(IM,2),CPT
1IM,1),CPT(IM,2)
91 CONTINUE
MB2=MBI+1
IND=MBI+MBO
IF (IEND.LE.0) RETURN
WRITE (9,1003) TITLEI
WRITE (9,1002) (XVDIM(IND-IM),IM=MBI,MBO), (XVDIM(IM),IM=MB2,MBO)

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WRITE (9,1002) ( CPT(IND-IM,2),IM=MBI,MBO), OUTPUT110
1 ( CPT(IM,1),IM=MB2,MBO) OUTPUT111
998 FORMAT (1H1,50X,47HBLADE SURFACE PRESSURES FOR REDUCED WEIGHT FLOW)OUTPUT112
1 /) OUTPUT113
999 FORMAT (1H1,50X,44HBLADE SURFACE PRESSURES FOR FULL WEIGHT FLOW /)OUTPUT114
1100 FORMAT (1H ,7X,3HIM ,8X,7H M ,8X,7H M/MC ,8X,7HP11)/PT, OUTPUT115
18X,7HP(2)/PT,8X,7HCPT(1) ,8X,7HCPT(2) ,/) OUTPUT116
1001 FORMAT(5X,I5,6(6X,G10.4)) OUTPUT117
1002 FORMAT (8F10.6) OUTPUT118
1003 FORMAT (20A4) OUTPUT119
RETURN OUTPUT120
C OUTPUT121
C FORMAT STATEMENTS OUTPUT122
C OUTPUT123
1000 FORMAT(1H1,50X,48HBLADE SURFACE VELOCITIES FOR REDUCED WEIGHT FLOW)OUTPUT124
1010 FORMAT ( 39X ,63HVELOCITY(M) VS. MERIDIONAL STREAMLINE DISTANCE)OUTPUT125
1(M) DOWN THE PAGE // OUTPUT126
2 52X,50H* - BLADE SURFACE 1, BASED ON MERIDIONAL COMPONENT/ OUTPUT127
3 52X,50H* - BLADE SURFACE 1, BASED ON TANGENTIAL COMPONENT/ OUTPUT128
4 52X,50HX - BLADE SURFACE 2, BASED ON MERIDIONAL COMPONENT/ OUTPUT129
5 52X,50H0 - BLADE SURFACE 2, BASED ON TANGENTIAL COMPONENT/ OUTPUT130
1020 FORMAT(1H1,50X,45HBLADE SURFACE VELOCITIES FOR FULL WEIGHT FLOW) OUTPUT131
END OUTPUT132
SUBROUTINE VEL (FIRST, LAST) VEL 2
VEL 3
C VEL CALCULATES DENSITIES AND VELOCITIES FROM THE PRODUCT OF VEL 4
C DENSITY TIMES VELOCITY VEL 5
C VEL 6
COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2) VEL 7
COMMON /INPUTT/ GAM,AR,TIP,RHOIP,WTFI,OMEGA,ORF,BETA1,BETA0, VEL 8
1 LAMBDA,RVTHD,REDFAC,DENTOL,FSHI,FSMO,SSM1,SSM2,MBI,MBO,MM, VEL 9
2 NBI,NBL,NRSP,MOPT,LOPT,LRVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD, VEL 10
3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),RO(2),BETI(2),BETO(2), VEL 11
4 NSPI(2),TITLEI(20),HR(50),RHSP(50),BESPF(50),H0WCR(50), VEL 12
5 PLOSS(50),MSP(50,2),THSP(50,2) VEL 13
COMMON /CALCOM/ ACTHT,ACTOMG,ACTLAM,MBIM1,MBIP1,MBOH1,MBDP1,MHM1, VEL 14
1 HMI,HT,DTLR,DHLR,PITCH,CP,EXPON,TMW,CPTIP,TGROG,TBI,TBD,TWL, VEL 15
2 WI,WHI,WCRI,ITIM,ITMAX,NIP,IMS1,IMS2,IMS(2),BY(2),MLE(2), VEL 16
3 THLE(2),RMI(2),RMO(2),BESP(50),MV(100),RM(100),BE(100), VEL 17
4 BEF(100),DBDM(100),DBFDM(100),SAL(100),PLOSIM(100),AAA(100), VEL 18
5 BBB(100),IVI(101),ITV(100,2),TV(100,2),DTDMV(100,2), VEL 19
6 BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RMH(100,2), VEL 20
7 BEH(100,2),PLOSHH(100,2) VEL 21
COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500) VEL 22
LEVEL 2, A,U,K,RHO VEL 23
COMMON /VARCOM/ RHOHBI(100,2),RHOVB(100,2),MMB(100,2),MTB(100,2), VEL 24
1 WRCRM(100,2),LABEL(1,100) VEL 25
DIMENSION W(2500),BETA(2500),DUDT(2500),DUDTT(2500),AAP(2500), VEL 26
1 BBP(2500) VEL 27
LEVEL 2, H,BETA,DUDT,DUDTT,AAP,BBP VEL 28
EQUIVALENCE (A,W),(A(1,2),BETA),(A(1,3),DUDT),(A(1,4),DUDTT), VEL 29
1 (K,AAP),(RHO,BBP) VEL 30
DIMENSION WRCRT(100,2),SURFL(100,2) VEL 31
C VEL 32
C VELD WRITES OUTPUT ALONG VERTICAL MESH LINES WHICH DO NOT VEL 33
C INTERSECT BLADES VEL 34
C VEL 35
INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST, VEL 36
1 UPPER,S1,ST VEL 37
REAL K,KAK,LAMBDA,LMAX,MH,MLE,HR,MSL,MSP,MV,MVZIM1 VEL 38

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DATA REDFUL/7HREDUCED/,FULL/6H FULL/
ENTRY VELP
IF (REDFAC.EQ.1) REDFUL=FULL
IF (FIRST.GT.LAST) RETURN
IF (FIRST.EQ.1) WRITE(NWRIT,1000) REDFUL
DO 20 IM=FIRST, LAST
IPU = IV(IM)
IPL = IPU+NBI-1
WRITE(NWRIT,1010) IM,(M(IP),BETA(IP),IP=IPU,IPL)
20 CONTINUE
RETURN
C
C VELB CALCULATES ALONG VERTICAL MESH LINES WHICH INTERSECT BLADES
C
ENTRY VELB
IF (FIRST.GT.LAST) RETURN
IF (FIRST.NE.MBI) GO TO 30
RELER = 0.
RELEA = 0.
ZMREL = 0.
IMREL = 0
ITREL = 0
ISREL = 0
ICOUNT = 0
SURFL(MBI,1) = 0.
SURFL(MBI,2) = 0.
30 DO 75 IM=FIRST, LAST
ITVU = ITV(IM,1)
ITVL = ITV(IM,2)
IPUP1 = IPF(IM,ITVU)
IPLM1 = IPF(IM,ITVL)
TWLMR = 2.*OMEGA*LAMBDA-(OMEGA*RMH(IM))**2
WCR = SQRT(TGROG*TIP*(1.-TWLMR/CPTIP))
IF (ITVL.LT.ITVU) GO TO 50
C ALONG THE LINE BETWEEN BLADES
IF (INTVL.LE.0) GO TO 50
WRITE(NWRIT,1010) IM,(M(IP),BETA(IP),IP=IPUP1,IPLM1)
C ON THE UPPER SURFACE
50 RHOB = RHOVB(IM,1)
RHOIPL = RHOIP*(1.-PLOSIM(IM))
LER(1) = 7
C
C DENSTY CALL NO. 7
CALL DENSTY(WMB(IM,1),RHOVB(IM,1),ANS,TWLMR,CPTIP,EXPON,RHOIPL,
1 GAM,AR,TIP,JZ)
WMB(IM,1) = ANS
WACRM(IM,1) = WMB(IM,1)/WCR
IF (IM.EQ.MBI) GO TO 60
DELTV = TV(IM-1,1)-TV(IM,1)
SURFL(IM,1) = SURFL(IM-1,1)+SQRT((MV(IM)-MV(IM-1))**2+
1 (DELTV*(RM(IM)+RM(IM-1))/2.)**2)
60 ERR = ABS((RHOB-RHOVB(IM,1))/RHOVB(IM,1))
RELER = AMAX1(RELER,ERR)
RELEA = RELEA+ERR
IF (RELER.NE.ERR) GO TO 65
IMREL = IM
ISREL = 1
ZMREL = MV(IM)
65 IF (ERR.GE.DENTOL) ICOUNT=ICOUNT+1
C ON THE LOWER SURFACE
RHOB = RHOVB(IM,2)
VEL 39
VEL 40
VEL 41
VEL 42
VEL 43
VEL 44
VEL 45
VEL 46
VEL 47
VEL 48
VEL 49
VEL 50
VEL 51
VEL 52
VEL 53
VEL 54
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VEL 85
VEL 86
VEL 87
VEL 88
VEL 89
VEL 90
VEL 91
VEL 92
VEL 93
VEL 94
VEL 95
VEL 96
VEL 97
VEL 98
RHOIPL = RHOIP*(1.-PLOSIM(IM))
LER(1) = 8
C DENSTY CALL NO. 8
CALL DENSTY(WMB(IM,2),RHOVB(IM,2),ANS,TWLMR,CPTIP,EXPON,RHOIPL,
1 GAM,AR,TIP,JZ)
WMB(IM,2) = ANS
WACRM(IM,2) = WMB(IM,2)/WCR
IF (IM.EQ.MBI) GO TO 70
DELTV = TV(IM-1,2)-TV(IM,2)
SURFL(IM,2) = SURFL(IM-1,2)+SQRT((MV(IM)-MV(IM-1))**2+
1 (DELTV*(RM(IM)+RM(IM-1))/2.)**2)
70 ERR = ABS((RHOB-RHOVB(IM,2))/RHOVB(IM,2))
RELER = AMAX1(RELER,ERR)
RELEA = RELEA+ERR
IF (RELER.NE.ERR) GO TO 75
IMREL = IM
ISREL = 2
ZMREL = MV(IM)
75 IF (ERR.GE.DENTOL) ICOUNT=ICOUNT+1
RETURN
C
C VELSUR CALCULATES WHERE HORIZONTAL MESH LINES INTERSECT THE BLADES
C
ENTRY VELSUR
ITERMX = 10
DO 90 SURF=1,2
IMSS = IMS(SURF)
IF (IMSS.EQ.0) GO TO 90
DO 80 IHS=1,IMSS
TWLMR = 2.*OMEGA*LAMBDA-(OMEGA*RMH(IHS,SURF))**2
WCR = SQRT(TGROG*TIP*(1.-TWLMR/CPTIP))
RHOB = RHOHB(IHS,SURF)
RHOIPL = RHOIP*(1.-PLOSIM(IHS,SURF))
LER(1) = 9
C DENSTY CALL NO. 9
CALL DENSTY(WTB(IHS,SURF),RHOHB(IHS,SURF),ANS,TWLMR,CPTIP,
1 EXPON,RHOIPL,GAM,AR,TIP,JZ)
WTB(IHS,SURF) = ANS
WACRT(IHS,SURF) = WTB(IHS,SURF)/WCR
ERR = ABS((RHOB-RHOHB(IHS,SURF))/RHOHB(IHS,SURF))
RELER = AMAX1(RELER,ERR)
RELEA = RELEA+ERR
IF (RELER.NE.ERR) GO TO 80
IMREL = 0
IF (SURF.EQ.1) CALL BL1(MH(IHS,SURF),THET,DTDM,INF)
IF (SURF.EQ.2) CALL BL2(MH(IHS,SURF),THET,DTDM,INF)
ITREL = THET/HT*SIGN(.1,THET)
ISREL = SURF
ZMREL = MH(IHS,SURF)
80 IF (ERR.GE.DENTOL) ICOUNT=ICOUNT+1
90 CONTINUE
IF (RELER.LT.DENTOL.OR.ITER.GE.ITERMX) IEND=IEND+1
RELEA = RELEA/FLOAT(2*(MBO-MBI+1)*IMS(1)*IMS(2))
WRITE(NWRIT,1080) ITER,RELER,IMREL,ITREL,ISREL,ZMREL,RELEA,ICOUNTVEL
VEL 99
VEL 100
VEL 101
VEL 102
VEL 103
VEL 104
VEL 105
VEL 106
VEL 107
VEL 108
VEL 109
VEL 110
VEL 111
VEL 112
VEL 113
VEL 114
VEL 115
VEL 116
VEL 117
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VEL 120
VEL 121
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VEL 140
VEL 141
VEL 142
VEL 143
VEL 144
VEL 145
VEL 146
VEL 147
VEL 148
VEL 149
VEL 150
VEL 151
VEL 152
VEL 153
VEL 154
VEL 155
VEL 156
VEL 157
VEL 158
WRITE ALL BLADE SURFACE VELOCITIES
C
IF (SURVL.LE.0) RETURN
WRITE (NWRIT,1020) REDFUL
WRITE(NWRIT,1040) (MV(IM),WMB(IM,1),BETAV(IM,1),SURFL(IM,1),

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1  WRCRM(IM,1),WMB(IM,2),BETA(IM,2),SURFL(IM,2),WRCRM(IM,2),    VEL 159
2  IM=MBI,MBO)                                                    VEL 160
WRITE (NHRIT,1050) REDFUL                                         VEL 161
DO 100 SURF=1,2                                                    VEL 162
IMSS = IMS(SURF)                                                  VEL 163
IF (IMSS.LT.1) GO TO 100                                          VEL 164
WRITE(NHRIT,1060) SURF                                            VEL 165
WRITE(NHRIT,1070) (MH(IHS,SURF),WTB(IHS,SURF),BETAH(IHS,SURF),  VEL 166
1  WRCRT(IHS,SURF), IHS=1,IMSS)                                   VEL 167
100 CONTINUE                                                       VEL 168
RETURN                                                             VEL 169
C                                                                    VEL 170
C                                                                    VEL 171
C  FORMAT STATEMENTS                                              VEL 172
C                                                                    VEL 173
1000 FORMAT(1H1/40X,34HVELOCITIES AT INTERIOR MESH POINTS/45X,   VEL 174
1  4HFOR ,A8,11HHEIGHT FLOW)                                       VEL 175
1010 FORMAT(1HL,3HIM=,I3,5(24H VELOCITY ANGLE( DEG )/            VEL 176
1(5X,5(G15.4,F9.2)))                                              VEL 177
1020 FORMAT(1H1/16X,1H*,18X,52HSURFACE VELOCITIES BASED ON MERIDIONAL CVEL 177
10MPONENTS - ,A8,11HHEIGHT FLOW,18X,1H*/16X,1H*,53X,1H*,53X,1H*/  VEL 178
2  16X,1H*,19X,15HBLADE SURFACE 1,19X,1H*,20X,15HBLADE SURFACE 2, VEL 179
3  18X,1H*/7X,1HM,8X,1H*,2(3X,8HVELOCITY,3X,23HANGLE( DEG ) SURF. LEVEL 180
4NGTH,5X,5HM/MCR,6X,1H*))                                         VEL 181
1040 FORMAT(1H ,G13.4,3H *,2(G12.4,F9.2,2G15.4,3H *)))          VEL 182
1050 FORMAT(1H1/3X,49HSURFACE VELOCITIES BASED ON TANGENTIAL COMPONENTSVEL 183
1  /18X,A8,11HHEIGHT FLOW)                                         VEL 184
1060 FORMAT(//22X,15HBLADE SURFACE ,I1/7X,1HM,10X,8HVELOCITY,3X,10HANGVEL 185
1LE( DEG ),3X,5HM/MCR)                                           VEL 186
1070 FORMAT(1H ,2G13.4,F9.2,G15.4)                                VEL 187
1080 FORMAT (//5X,14HITERATION NO. ,I4/5X,60HMAXIMUM RELATIVE CHANGE IVEL 188
1N DENSITY AT BLADE SURFACE POINTS =,G11.4,10H AT IM =,I3,      VEL 189
20H, IT =,I3,10H, SURF =,I2,7H, M =,G11.4/5X,60HAVERAGE RELATVEL 190
3IVE CHANGE IN DENSITY AT BLADE SURFACE POINTS =,G11.4/5X,49HNUMBERVEL 191
4 OF UNCONVERGED BLADE SURFACE MESH POINTS =,I4)                 VEL 192
END                                                                 VEL 193
SUBROUTINE TVELCY                                                 TVELCY 2
C                                                                    TVELCY 3
C  TVELCY SOLVES THE FULL MASS FLOW PROBLEM BY OBTAINING A      TVELCY 4
C  VELOCITY GRADIENT SOLUTION ALONG EACH VERTICAL MESH LINE     TVELCY 5
C                                                                    TVELCY 6
COMMON NREAD,NHRIT,ITER,IEND,LER(2),NER(2)                       TVELCY 7
COMMON /INPUT/ GAM,AR,TIP,RHOIP,WTF,OMEGA,ORF,BETA1,BETA2,      TVELCY 8
1  LAMBDA,RVTHO,REDFAC,DENTOL,F5MI,F5MO,SSM1,SSM2,MBI,MBO,MM,   TVELCY 9
2  NBBI,NBL,NRSP,HOPT,LOPT,LRYB,BLDAT,AANDK,ERSOR,STRFN,SLCRD,  TVELCY10
3  INTVL,SURVL,CHORD(2),STGR(2),RI(2),ROI(2),BETI(2),BETO(2),  TVELCY11
4  NSPI(2),TITLEI(20),MRI(50),RMSPI(50),BESPF(50),WOWCR(50),  TVELCY12
5  PLOSSI(50),MSP(50,2),THSP(50,2)                               TVELCY13
COMMON /CALCON/ ACTHT,ACTONG,ACTLAM,MBIH1,MBIP1,MBOH1,MBOPI,MMH1, TVELCY14
1  HMT,HT,OTLR,OMLR,PITCH,CP,EXPON,TMM,CPTIP,TGROG,TBI,TBO,TWL, TVELCY15
2  MI,WMI,MCRI,ITMIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),   TVELCY16
3  THLE(2),RMI(2),RMO(2),BESP(50),MV(100),RM(100),BE(100),     TVELCY17
4  BEF(100),OBDH(100),DBFDH(100),SAL(100),PLOSIM(100),AAA(100), TVELCY18
5  BBB(100),IV(101),ITV(100,2),TV(100,2),DTHV(100,2),         TVELCY19
6  BETA(100,2),MH(100,2),DTMH(100,2),BETAH(100,2),RMH(100,2),  TVELCY20
7  BEH(100,2),PLOSM(100,2)                                       TVELCY21
COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500)           TVELCY22
LEVEL 2, A,U,K,RHO                                               TVELCY23
COMMON /VARCOM/ RHOHB(100,2),RHOVB(100,2),WMB(100,2),WTB(100,2), TVELCY24
1  WRCRM(100,2),LABEL(1,100)                                       TVELCY25
COMMON /PLTCOM/ TSLPT(1100),XDOWN(400),YACROS(400)             TVELCY26
LEVEL 2, TSLPT,XDOWN,YACROS                                     TVELCY27
DIMENSION W(2500),BETA(2500),DUDT(2500),DUDTT(2500),AAP(2500),  TVELCY28
1  BDP(2500)                                                       TVELCY29
LEVEL 2, W,BETA,DUDT,DUDTT,AAP,BBP                             TVELCY30
EQUIVALENCE (A,W),(A(1,2),BETA),(A(1,3),DUDT),(A(1,4),DUDTT),  TVELCY31
1  (K,AAP),(RHO,BBP)                                             TVELCY32
DIMENSION KKK(14)                                              TVELCY33
DIMENSION P(11)                                               TVELCY34
INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,SURFBV,  TVELCY35
1FIRST,UPPER,UPPRBV,S1,ST                                     TVELCY36
REAL K,KAK,LAMBDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVM1              TVELCY37
C                                                                    TVELCY38
C  CALL VELGRP AND VELGRB THROUGHOUT THE SOLUTION REGION        TVELCY39
C                                                                    TVELCY40
LAMBDA = ACTLAM                                                 TVELCY41
IF (INTVL.GT.0) WRITE(NHRIT,1000)                               TVELCY42
IF (1.GT.MBIH1) GO TO 20                                        TVELCY43
DO 10 IM=1,MBIH1                                               TVELCY44
10 CALL VELGRPIH                                               TVELCY45
20 DO 30 IM=MBIP1,MBOH1                                         TVELCY46
30 CALL VELGRBIM                                               TVELCY47
IF (MBOPI.GT.MH) GO TO 50                                       TVELCY48
DO 40 IM=MBOPI,MH                                              TVELCY49
40 CALL VELGRPIM                                               TVELCY50
C                                                                    TVELCY51
C  FIX VELOCITIES ON LEADING AND TRAILING EDGE LINES           TVELCY52
C                                                                    TVELCY53
50 FIRST = IV(MBI)                                              TVELCY54
LAST = IV(MBIP1)-1                                             TVELCY55
DO 54 I=FIRST,LAST                                             TVELCY56
54 W(I) = W(I)/REDFAC                                          TVELCY57
FIRST = IV(MBO)                                               TVELCY58
LAST = IV(MBOP1)-1                                             TVELCY59
DO 56 I=FIRST,LAST                                             TVELCY60
56 W(I) = W(I)/REDFAC                                          TVELCY61
C                                                                    TVELCY62
C  WRITE SURFACE VELOCITIES                                     TVELCY63
C                                                                    TVELCY64
IF (SURVL.LE.0) RETURN                                         TVELCY65
WRITE(NHRIT,1010)                                              TVELCY66
WRITE(NHRIT,1020)(MV(IM),WMB(IM,1),WRCRM(IM,1),LABEL(1,IM),    TVELCY67
1  WMBI(IM,2),WRCRM(IM,2),LABEL(1,IM),IM=MBIP1,MBOH1)          TVELCY68
C                                                                    TVELCY69
C  PREPARE ARRAYS FOR PLOT OF SURFACE VELOCITIES               TVELCY70
C                                                                    TVELCY71
DO 60 IM=MBIP1,MBOH1                                           TVELCY72
I = IM-MBI                                                      TVELCY73
I2 = I+MBOH1-MBI                                               TVELCY74
XDOWN(I) = MV(IM)                                              TVELCY75
YACROS(I) = WMB(IM,1)                                          TVELCY76
60 YACROS(I2) = WMB(IM,2)                                       TVELCY77
KKK(1) = 0                                                       TVELCY78
KKK(2) = 2                                                       TVELCY79
KKK(3) = MBOH1-MBI                                             TVELCY80
P(1) = 1.                                                        TVELCY81
C                                                                    TVELCY82
C  PLOT SURFACE VELOCITIES                                     TVELCY83
C                                                                    TVELCY84
IF (BLDAT.GE.2) CALL TVPLOT                                    TVELCY85
WRITE(NHRIT,1030)                                              TVELCY86

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CALL PLOTMY (XDOWN,YACROS,KKK,P)
WRITE(NWRIT,1040)
RETURN
C
C
C  C  FORMAT STATEMENTS
1000 FORMAT(1H1/40X,34HVELOCITIES AT INTERIOR MESH POINTS/44X,
1 27H(BASED ON FULL WEIGHT FLOW))
1010 FORMAT(1H1/16X,1H*,13X,68HSURFACE VELOCITIES BASED ON MERIDIONAL CTVELOCITY95
10MPONENTS - FULL WEIGHT FLDW,30X,1H*/16X,1H*,55X,1H*,55X,1H*/16X,
21H*,20X,15HBLADE SURFACE 1,20X,1H*,20X,15HBLADE SURFACE 2,20X,1H*/VELCY97
37X,1H*,8X,1H*,2(3X,8HVELOCITY,6X,5HW/WCR,33X,1H*))
1020 FORMAT(1X,G13.4,3H *,2(2G13.4,A8,21X,1H*))
1030 FORMAT(1H1,51X,24HBLADE SURFACE VELOCITIES/51X,27H(BASED ON FULL WTVELC100
1EIGHT FLOW))
1040 FORMAT(39X,63HVELOCITY(W) VS. MERIDIONAL STREAMLINE DISTANCE(M) DOTVELC102
1WH THE PAGE//52X,19H* - BLADE SURFACE 1/52X,19H* - BLADE SURFACE 2VELC103
2)
END
SUBROUTINE VELGRA (IM)
COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
COMMON /INPUT/ GAM,AR,TIP,RHOIP,MTFL,OMEGA,DRF,BETA1,BETA0,
1 LAMBDA,RVTHO,REDFAC,DENTOL,FSH1,FSH0,SSH1,SSH2,MBI,MBO,MM,
2 NBB1,NBL,NRSP,HOPT,LOPT,LRVB,BLDA,AAAND,ERSOR,STRFN,SLCRD,
3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),RO(2),BETI(2),BETO(2),
4 NSPI(2),TITLEI(20),MR(50),RMSPI(50),BESPF(50),WOWCR(50),
5 PLOSSI(50),HSP(50,2),THSP(50,2)
COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIM1,MBIP1,MBOM1,MBOP1,MMH1,
1 MH1,HT,DTLR,DMLR,PITCH,CP,EXPON,TWH,CPTIP,TGROG,TBI,TBO,TWL,
2 HI,MMI,MCRI,ITMIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
3 THLE(2),RMI(2),RMO(2),BESP(50),MV(100),RMI(100),BE(100),
4 BEF(100),DBDH(100),DBFDM(100),SAL(100),PLOSIM(100),AAA(100),
5 BBB(100),IV(101),ITV(100,2),TV(100,2),DTDMV(100,2),
6 BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RMM(100,2),
7 BEH(100,2),PLOSSH(100,2)
COMMON /AUKRHO/ A(2500,4),U(2500),K(2500),RHO(2500)
LEVEL 2, A,U,K,RHO
COMMON /VARCOM/ RHOHB(100,2),RHOVB(100,2),HMB(100,2),WTB(100,2),
1 HRCRM(100,2),LABEL(1,100)
COMMON /BCDCOM/ INIT(2),EM(50,2),D2TDM2(100,2)
DIMENSION H(2500),BETA(2500),DUOT(2500),DUOTI(2500),AAP(2500),
1 BBPI(2500)
EQUIVALENCE (A,W),(A(1,2),BETA),(A(1,3),DUOT),(A(1,4),DUOTI),
1 (K,AAP),(RHO,BBP)
DIMENSION WGRAD(51),THETA(51),RWCB(51),CBETA(51),A2(51),B2(51)
INTEGER BLDA,AAAND,ERSOR,STRFN,SLCRD,SURVL,AAEMP,SURF,SURFDB,
1FIRST,UPPER,UPPRBV,S1,ST,CHOKED,BLANK
REAL K,KAK,LAMBDA,LMAX,HH,MLE,MR,MSL,HSP,MV,MVIMI
DATA CHOKED/6HCHOKED/,BLANK/1H /
C
C  C  VELGRP SOLVES IN THE PERIODIC REGION
C
C  ENTRY VELGRP
AORB = 1.
IP = IV(IM)
WGRAD(1) = W(IP)/REDFAC
ITI = ITV(IM,1)
IT = ITI
NSP = NBBI+1
GO TO 10
C
C  VELGRB SOLVES IN THE BLADE REGION
C
C  ENTRY VELGRB
IP = IV(IM)-1
WGRAD(1) = WMB(IM,1)/REDFAC
NSP = IV(IM+1)-IV(IM)+2
AORB = 2.
ITI = ITV(IM,1)
IT = ITI-1
10 NSPM1 = NSP-1
LABEL(1,IM) = BLANK
TORSAL = 2.*ACTOMG*RM(IM)*SAL(IM)
JZ = 1
IF (IM.GE.IMS1.AND.IM.LE.IMS2) JZ=2
TWLMR = 2.*ACTOMG*LAMBDA-(ACTOMG*RM(IM))*2
WCR = SQRT(TGROG*TIPI*(1.-TWLMR/CPTIP))
DELMAX = WCR/ 10.
TOLERC = WCR/ 100.
DO 20 I=1,NSPM1
CBETA(I) = COS(BETA(IP)/57.295779)
THETA(I) = HT*FLOAT(IT)
A2(I) = AAP(IP)
B2(I) = BBPI(IP)
IT = IT+1
20 IP = IP+1
CBETA(NSP) = CBETA(1)
A2(NSP) = A2(1)
B2(NSP) = B2(1)
THETA(NSP) = HT*FLOAT(IT)
IF (AORB.LE.1.) GO TO 30
CBETA(1) = 1./SQRT(1.+(RM(IM)*DTDMV(IM,1))*2)
SBETA1 = SQRT(1.-CBETA(1)**2)*SIGN(1.,DTDMV(IM,1))
A2(1) = (RM(IM)*CBETA(1)**2*DTDM2(IM,1)+SAL(IM)*SBETA1/
1 CBETA(1))*(1.+CBETA(1)**2)
B2(1) = B2(2)+TORSAL*(1./CBETA(1)-1./CBETA(2))
THETA(1) = TV(IM,1)
CBETA(NSP) = 1./SQRT(1.+(RM(IM)*DTDMV(IM,2))*2)
SBETAN = SQRT(1.-CBETA(NSP)**2)*SIGN(1.,DTDMV(IM,2))
A2(NSP) = (RM(IM)*CBETA(NSP)**2*DTDM2(IM,2)+SAL(IM)*SBETAN/
1 CBETA(NSP))*(1.+CBETA(NSP)**2)
B2(NSP) = B2(NSPM1)+TORSAL*(1./CBETA(NSP)-1./CBETA(NSPM1))
THETA(NSP) = TV(IM,2)
30 IHD = 1
40 CONTINUE
DO 50 I=2,NSP
WAS = WGRAD(I-1)+(A2(I-1)*WGRAD(I-1)+B2(I-1))*(THETA(I)-
1 THETA(I-1))
WASS = WGRAD(I-1)+(A2(I)*WAS+B2(I))*(THETA(I)-THETA(I-1))
50 WGRAD(I) = (WAS+WASS)/2.
DO 60 I=1,NSP
TIPI = 1.-(HGRAD(I)**2+TWLMR)/CPTIP
IF (TIPI.GE..0) GO TO 55
WRITE(NWRIT,1010) IM
IF (AORB.GT.1.) WGRAD(1) = 0.
IF (AORS.GT.1.) WGRAD(NSP) = 0.
GO TO 70
55 RHOT = RHOIP*(1.-PLOSIM(IM))*TIPI**EXPON
60 RWCB(I) = RHOT*WGRAD(I)*CBETA(I)
CALL INTGRL (THETA,RWCB,NSP,AAA)
VELGRA43
VELGRA44
VELGRA45
VELGRA46
VELGRA47
VELGRA48
VELGRA49
VELGRA50
VELGRA51
VELGRA52
VELGRA53
VELGRA54
VELGRA55
VELGRA56
VELGRA57
VELGRA58
VELGRA59
VELGRA60
VELGRA61
VELGRA62
VELGRA63
VELGRA64
VELGRA65
VELGRA66
VELGRA67
VELGRA68
VELGRA69
VELGRA70
VELGRA71
VELGRA72
VELGRA73
VELGRA74
VELGRA75
VELGRA76
VELGRA77
VELGRA78
VELGRA79
VELGRA80
VELGRA81
VELGRA82
VELGRA83
VELGRA84
VELGRA85
VELGRA86
VELGRA87
VELGRA88
VELGRA89
VELGRA90
VELGRA91
VELGRA92
VELGRA93
VELGRA94
VELGRA95
VELGRA96
VELGRA97
VELGRA98
VELGRA99
VELGR100
VELGR101
VELGR102

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WTFLES = BEF(IM)*RM(IM)*AAA(HSP)
IF (IND.GE.6.AND.ABS(ACHT-WTFLES).LE.ACTHT/1.E5) GO TO 70
CALL CONTIN (WGRAD(1),WTFLES,IND,JZ,ACTHT,DELMAX)
IF (IND.LT.10) GO TO 40
AA = WTFLES/ACTWT
IF (IND.EQ.10) WRITE(NWRIT,1030) IM,AA,IM
IF (IND.EQ.10) GO TO 65
WRITE(NWRIT,1020) IM
IF (AORB.GT.1.) WGRAD(1) = 0.
IF (AORB.GT.1.) WGRAD(NSP) = 0.
GO TO 70
65 LABEL(1,IM) = CHOKED
70 CONTINUE
FIRST = 1
IF (AORB.GT.1.) FIRST = 2
LAST = NSPM
IF (INTVL.GT.0) WRITE(NWRIT,1000) IM,ITI,(WGRAD(I),I=FIRST, LAST)
IP = IV(IM)-1
DO 80 I=FIRST, LAST
IP = IP+1
80 W(IP) = WGRAD(I)
IF (AORB.LE.1.) RETURN
WMB(IM,1) = WGRAD(1)
WMB(IM,2) = WGRAD(NSP)
WCMR(IM,1) = WMB(IM,1)/WCR
WCMR(IM,2) = WMB(IM,2)/WCR
RETURN
C
C FORMAT STATEMENTS
C
1000 FORMAT(5HKIM =,I3,10X,5HIT1 =,I3/(2X,10G13.4))
1010 FORMAT(73HK A VELOCITY GRADIENT SOLUTION CANNOT BE OBTAINED FOR
1VERTICAL LINE IM =,I3)
1020 FORMAT(92HK A VELOCITY GRADIENT SOLUTION COULD NOT BE OBTAINED IN
150 ITERATIONS FOR VERTICAL LINE IM =,I3)
1030 FORMAT(43HLACTWT EXCEEDS CHOKING WEIGHT FLOW FOR IM =,I3/22HKCHOKI
VLS
ING WEIGHT FLOW =,F6.3,3X,32H OF ACTUAL WEIGHT FLOW FOR IM =,I3)
END
SUBROUTINE BLCD (M,THETA,DTDM,INF)
C
C BLCD CALCULATES BLADE THETA COORDINATE AS A FUNCTION OF M
C
COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
COMMON /INPUT/ GAM,AR,TIP,RHOIP,WTFLE,OMEGA,ORF,BETA1,BETA0,
1 LAMBDA,RVTHO,REDFAC,DENTOL,FSMI,FSMO,SSH1,SSH2,MBI,MBO,MM,
2 NBSI,NBL,NRSP,MOPT,LOPT,LRVB,BLDAT,AANDK,ERSOR,STRFN,SLCRD,
3 INTVL,SURVL,CHORD(2),STGR(2),RI(2),RO(2),BETI(2),BETO(2),
4 NSPI(2),TITLEI(20),MR(50),RMSP(50),BESPF(50),WOWCR(50),
5 PLOSS(50),MSP(50,2),THSP(50,2)
COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIM1,MBIP1,MBOM1,MBOP1,MM1,
1 HM1,HT,D1LR,DMLR,PITCH,CP,EXPON,TMM,CPTIP,TGROG,TBI,TBO,TNL,
2 WI,WMI,WCRI,ITMIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
3 THLE(2),RMI(2),RMO(2),BESP(50),MV(100),RMI(100),BE(100),
4 BEF(100),DBDH(100),DBFDM(100),SAL(100),PLOSIM(100),AAA(100),
5 BBB(100),IVI(101),ITV(100,2),TV(100,2),DTDMV(100,2),
6 BETAV(100,2),MH(100,2),DTDMH(100,2),BETAH(100,2),RMH(100,2),
7 BEH(100,2),PLOSMH(100,2)
COMMON /BCDCOM/ INITI(2),EM(50,2),D2TDM2(100,2)
DIMENSION DTDHI(2),DTDMO(2)
VELGR103 C BL1 SOLVES FOR BLADE SURFACE 1
VELGR104 C
VELGR105 INTEGER BLDAT,AANDK,ERSOR,STRFN,SLCRD,SURVL,AATEMP,SURF,FIRST,
VELGR106 I UPPER,S1,ST
VELGR107 REAL K,KAK,LAMBDA,LMAX,IM,MLE,MR,MSL,MSP,MV,MVIM1
VELGR108 REAL M,MMLE,NSPMH,MMHSP
VELGR109 ENTRY BL1
VELGR110 SURF = 1
VELGR111 SIGN = 1.
VELGR112 GO TO 10
C
C BL2 SOLVES FOR BLADE SURFACE 2
C
ENTRY BL2
SURF = 2
SIGN = -1.
10 INF = 0
IM = 1
DO 15 I=MBI,MBO
15 IF (ABS(MV(I)-M).LE.DMLR) IM=I
MSP = NSPI(SURF)
IF (INITI(SURF).EQ.1) GO TO 30
INIT(SURF) = 1
C
C INITIAL CALCULATION OF FIRST AND LAST SPLINE POINTS ON BLADE
C
AA = BETI(SURF)/57.295779
AA = SIN(AA)
MSP(1,SURF) = RI(SURF)*(1.-SIGN*AA)
BB = SQRT(1.-AA**2)
THSP(1,SURF) = SIGN*BB*RI(SURF)/RMI(SURF)
DTDMI(SURF) = AA/BB/RMI(SURF)
AA = BETO(SURF)/57.295779
AA = SIN(AA)
MSP(NSP,SURF) = CHORD(SURF)-RO(SURF)*(1.+SIGN*AA)
BB = SQRT(1.-AA**2)
THSP(NSP,SURF) = STGR(SURF)*SIGN*BB*RO(SURF)/RMO(SURF)
DTDMO(SURF) = AA/BB/RMO(SURF)
DO 20 IA=1,NSP
MSP(IA,SURF) = MSP(IA,SURF)+MLE(SURF)
20 THSP(IA,SURF) = THSP(IA,SURF)+THLE(SURF)
CALL SPLIS(MSP(1,SURF),THSP(1,SURF),NSP,DTDMI(SURF),DTDMO(SURF),
1 AAA,EM(1,SURF))
IF (BLDAT.LE.0) GO TO 30
GO TO 5000
IF (SURF.EQ.1) WRITE(NWRIT,1000)
WRITE(NWRIT,1010) SURF
WRITE(NWRIT,1020) (MSP(IA,SURF),THSP(IA,SURF),AAA(IA),EM(IA,SURF)),
1 IA=1,NSP)
5000 CONTINUE
C
C BLADE COORDINATE CALCULATION
C
30 KK = 2
IF (M.GT.MSP(1,SURF)) GO TO 50
C
C AT LEADING EDGE RADIUS
C
MMLE = M-MLE(SURF)
IF (MMLE.LT.-D1LR) GO TO 90
BLCD 24
BLCD 25
BLCD 26
BLCD 27
BLCD 28
BLCD 29
BLCD 30
BLCD 31
BLCD 32
BLCD 33
BLCD 34
BLCD 35
BLCD 36
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BLCD 83

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MMLE = AMAX1(0.,MMLE)
THETA = SQRT(MMLE*(2.*RI(SURF)-MMLE))*SIGN
IF (THETA.EQ.0.) GO TO 40
RHM = RI(SURF)-MMLE
DTDM = RHM/THETA/PHI(SURF)
THETA = THETA/RHM(SURF)
D2TDM2(IM,SURF) = (-THETA-RHM*DTDM)/(RHM(SURF)*THETA)**2
THETA = THETA+THLE(SURF)
RETURN
40 INF = 1
DTDM = 1.E10*SIGN
THETA = THLE(SURF)
D2TDM2(IM,SURF) = 0.
RETURN
C
C ALONG SPLINE CURVE
C
50 IF (M.LE.MSP(KK,SURF)) GO TO 60
IF (KK.GE.NSP) GO TO 70
KK = KK+1
GO TO 50
60 S = MSP(KK,SURF)-MSP(KK-1,SURF)
EMKM1 = EM(KK-1,SURF)
EMK = EM(KK,SURF)
MSPMH = MSP(KK,SURF)-M
MMHSP = M-MSP(KK-1,SURF)
THK = THSP(KK,SURF)/S
THKM1 = THSP(KK-1,SURF)/S
THETA = EMKM1*MSPMH**3/6./S+EMK*MMHSP**3/6./S+(THK-EMK*S/6.)*
1 MMHSP + (THKM1-EMKM1*S/6.)*MSPMH
DTDM = -EMKM1*MSPMH**2/2./S+EMK*MMHSP**2/2./S+THK-THKM1-(EMK-
1 EMKM1)*S/6.
D2TDM2(IM,SURF) = EMKM1*MSPMH/S+EMK*MMHSP/S
RETURN
C
C AT TRAILING EDGE RADIUS
C
70 CMM = CHORD(SURF)+MLE(SURF)-M
IF (CMM.LT.-DHLE) GO TO 90
CMM = AMAX1(0.,CMM)
THETA = SQRT(CMM*(2.*RO(SURF)-CMM))*SIGN
IF (THETA.EQ.0.) GO TO 80
RHM = RO(SURF)-CMM
DTDM = -RHM/THETA/RMO(SURF)
THETA = THETA/RMO(SURF)
D2TDM2(IM,SURF) = (-THETA+RHM*DTDM)/(RMO(SURF)*THETA)**2
THETA = THETA+STGR(SURF)+THLE(SURF)
RETURN
80 INF = 1
DTDM = -1.E10*SIGN
THETA = THLE(SURF)+STGR(SURF)
D2TDM2(IM,SURF) = 0.
RETURN
C
C ERROR RETURN
C
90 WRITE(NWRIT,1030) LER(2),M,SURF
STOP
C
C FORMAT STATEMENTS
BLCD 84 C
BLCD 85 1000 FORMAT (1H1,13X,33HBLADE DATA AT INPUT SPLINE POINTS)
BLCD 86 1010 FORMAT(1H1,17X,16HBLADE SURFACE,I4)
BLCD 87 1020 FORMAT (7X ,1H1,10X,5HTHETA,10X,10HDERIVATIVE,5X,10H2ND DERIV. /
BLCD 88 1 (4G15.5) )
BLCD 89 1030 FORMAT (14HLBLCD CALL NO.,I3/33H M COORDINATE IS NOT WITHIN BLADE/BLCD 149
BLCD 90 14H M =,G14.6,10X,6HSURF =,G14.6)
BLCD 91 END
BLCD 92 SUBROUTINE MHORIZ(MV,ITV,BL,MBI,MBO,ITO,HT,DTLR,KODE,J,MH,DTDMH,
BLCD 93 1HRTS)
BLCD 94 C
BLCD 95 C MHORIZ CALCULATES M COORDINATES OF INTERSECTIONS OF ALL HORIZONTAL
BLCD 96 C MESH LINES WITH A BLADE SURFACE
BLCD 97 C KODE = 0 FOR UPPER BLADE SURFACE
BLCD 98 C KODE = 1 FOR LOWER BLADE SURFACE
BLCD 99 C
BLCD 100 COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
BLCD 101 DIMENSION MVI(100),ITV(100),MH(100),DTDMH(100)
BLCD 102 INTEGER BLDAT,AAHDK,ERSOR,STRFN,SLCRD,SURVL,AAEMP,SURF,FIRST,
BLCD 103 1 UPPER,S1,ST
BLCD 104 REAL K,KAK,LAMBDA,LMAX,MH,MLE,MR,MSL,MSP,MV,MVIM1,MVIM
BLCD 105 EXTERNAL BL
BLCD 106 IF (MBI.GE.MBO) RETURN
BLCD 107 IM = MBI
BLCD 108 10 ITIND = 0
BLCD 109 20 IF (ITV(IM+1)-ITV(IM)-ITIND) 30,40,50
BLCD 110 30 J = J+1
BLCD 111 TI = FLOAT(ITV(IM+1)-ITO-ITIND+KODE)*HT
BLCD 112 ITIND = ITIND-1
BLCD 113 MVIM = MV(IM)
BLCD 114 IF (MRTS.EQ.1) MVIM=MVIM*(MV(IM+1)-MVIM)/1000.
BLCD 115 CALL ROOT (MVIM,MV(IM+1),TI,BL,DTLR,MH(J),DTDMH(J))
BLCD 116 GO TO 20
BLCD 117 40 IM = IM+1
BLCD 118 MRTS = 0
BLCD 119 IF (IM.EQ.MBO) RETURN
BLCD 120 GO TO 10
BLCD 121 50 J = J+1
BLCD 122 TI = FLOAT(ITV(IM)-ITO+ITIND+KODE)*HT
BLCD 123 ITIND = ITIND+1
BLCD 124 MVIM = MV(IM)
BLCD 125 IF (MRTS.EQ.1) MVIM=MVIM*(MV(IM+1)-MVIM)/1000.
BLCD 126 CALL ROOT(MVIM,MV(IM+1),TI,BL,DTLR,MH(J),DTDMH(J))
BLCD 127 GO TO 20
BLCD 128 END
BLCD 129 SUBROUTINE ROOT(A,B,Y,FUNCT,TOLERY,X,DFX)
BLCD 130 C
BLCD 131 C ROOT FINDS A ROOT FOR (FUNCT MINUS Y) IN THE INTERVAL (A,B)
BLCD 132 C
BLCD 133 COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
BLCD 134 IERP = 0
BLCD 135 5 IF (IERP.EQ.1) WRITE(NWRIT,1010) A,B,Y,TOLERY
BLCD 136 X1 = A
BLCD 137 CALL FUNCT(X1,FX1,DFX,INF)
BLCD 138 FX1S = FX1
BLCD 139 DFXS = DFX
BLCD 140 IF (IERP.EQ.1) WRITE(NWRIT,1020) X1,FX1,DFX,INF
BLCD 141 X2 = B
BLCD 142 10 DO 30 I=1,20
BLCD 143 X = (X1+X2)/2.
BLCD 144
BLCD 145
BLCD 146
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CALL FUNCT(X,FX,DFX,INF)
IF (IERR.EQ.1) WRITE(NWRIT,1020) X,FX,DFX,INF
IF ((FX1-Y)*(FX-Y).GT.0.) GO TO 20
X2 = X
GO TO 30
20 X1 = X
FX1 = FX
30 CONTINUE
IF (ABS(Y-FX).LT.TOLERY) RETURN
IF (ABS(Y-FX1).GT.1.2*TOLERY) GO TO 40
X = A
DFX = DFXS
RETURN
40 X = B
CALL FUNCT(X,FX,DFX,INF)
IF (ABS(Y-FX).LE.1.2*TOLERY) RETURN
IF (IERR.EQ.1) RETURN
WRITE(NWRIT,1000)
IERR = 1
GO TO 5
C
C FORMAT STATEMENTS
C
1000 FORMAT(72H1ROOT HAS FAILED TO LOCATE A ROOT IN THE INTERVAL (A,B)
      1 IN 20 ITERATIONS)
1010 FORMAT(22H ROOT ARGUMENTS -- A =,G13.5,3X,3HB =,G13.5,3X,3HY =,
      1G13.5,3X,3HTOLERY =,G13.5/16X,1HX,17X,2HFX,15X,3HDFX,10X,3HINF)
1020 FORMAT(8X,G16.5,2G18.5,I6)
      END
      SUBROUTINE DENSTY(RHOW,RHO,VEL,TWLMR,CPTIP,EXPON,RHOIP,GAM,AR,TIP,
      1 JZ)
C
C DENSTY CALCULATES DENSITY AND VELOCITY FROM THE WEIGHT FLOW PARAMETER
C DENSITY TIMES VELOCITY
C
      COMMON NREAD,NWRIT,ITER,IEND,LER(2),NER(2)
      VEL = RHOW/RHO
      IF (VEL.NE.0.) GO TO 10
      RHO = RHOIP*(1.-TWLMR/CPTIP)**EXPON
10 TTIP = 1.-(VEL**2*TWLMR)/CPTIP
      IF (TTIP.LT.0.) GO TO 30
      IF (LER(1).GT.5) GO TO 25
      TEMP = TTIP*(EXPON-1.)
      RHOT = RHOIP*TEMP*TTIP
      RHOWP = -VEL**2/GAM*RHOIP/AR*TEMP/TIP*RHOT
      IF (JZ.EQ.1.AND.RHOWP.LE.0.) GO TO 30
      IF (JZ.EQ.2.AND.RHWP.GE.0.) GO TO 30
      VELNEW = VEL*(RHOW-RHOT*VEL)/RHWP
      VELNEW = ABS(VELNEW)
      IF (ABS(VELNEW-VEL)/VELNEW.LT..0001) GO TO 20
      VEL = VELNEW
      GO TO 10
20 VEL = VELNEW
      RHO = RHOW/VEL
      RETURN
25 RHO = RHOIP*TTIP**EXPON
      RETURN
30 TGROG = 2.*GAM*AR/(GAM+1.)
      VEL = SQRT(TGROG*TIP*(1.-TWLMR/CPTIP))
      RHO = RHOIP*(1.-(VEL**2*TWLMR)/CPTIP)**EXPON
      DENSTY 2
      DENSTY 3
      DENSTY 4
      DENSTY 5
      DENSTY 6
      DENSTY 7
      DENSTY 8
      DENSTY 9
      DENSTY10
      DENSTY11
      DENSTY12
      DENSTY13
      DENSTY14
      DENSTY15
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      DENSTY24
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      DENSTY26
      DENSTY27
      DENSTY28
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      DENSTY30
      DENSTY31
      DENSTY32
      DENSTY33
      DENSTY34
      DENSTY35
      DENSTY36
      DENSTY37
      DENSTY38
      DENSTY39
      DENSTY40
      DENSTY41
      DENSTY42
      DENSTY43
      DENSTY44
      DENSTY45
      IPF 2
      IPF 3
      IPF 4
      IPF 5
      IPF 6
      IPF 7
      IPF 8
      IPF 9
      IPF 10
      IPF 11
      IPF 12
      IPF 13
      CONTIN 2
      CONTIN 3
      CONTIN 4
      CONTIN 5
      CONTIN 6
      CONTIN 7
      CONTIN 8
      CONTIN 9
      CONTIN10
      CONTIN11
      CONTIN12
      CONTIN13
      CONTIN14
      CONTIN15
      CONTIN16
      CONTIN17
      CONTIN18
      CONTIN19
      CONTIN20
      CONTIN21
      CONTIN22
      CONTIN23
      CONTIN24
      CONTIN25
      CONTIN26
      CONTIN27
      CONTIN28
      CONTIN29
      CONTIN30
      CONTIN31
      CONTIN32
      CONTIN33
      CONTIN34
      CONTIN35
      CONTIN36
      CONTIN37
      RHMORH = RHOW/RHO/VEL
      IF (RHMORH.LT.1.) GO TO 40
      NER(1) = NER(1)+1
      WRITE(NWRIT,1000) LER(1),NER(1),RHMORH
      IF (NER(1).EQ.50) STOP
      RETURN
40 IF (JZ.EQ.1) VEL=0.
      IF (JZ.EQ.2) VEL=VEL*1.1
      GO TO 10
1000 FORMAT(16HLDENSTY CALL NO.,I3/9H NER(1) =,I3/10H RHOW IS ,F7.4,
      134H TIMES THE MAXIMUM VALUE FOR RHMORH)
      END
      FUNCTION IPF(IM,IT)
      COMMON /CALCON/ ACTWT,ACTOMG,ACTLAM,MBIM1,MBIP1,MBOM1,MBOP1,MMH1,
      1 HM1,HT,DTLR,DMLR,PITCH,CP,EXPON,TW, CPTIP,TGROG,TBI,TBO,TWL,
      2 WI,WMI,WCRI,ITMIN,ITMAX,NIP,IMS1,IMS2,IMS(2),BV(2),MLE(2),
      3 THLE(2),RHI(2),RMD(2),BESP(50),MV(100),RM(100),BE(100),
      4 BEF(100),DBDM(100),DBFDM(100),SAL(100),PLOSIM(100),AAA(100),
      5 BBB(100),IVI(101),ITVI(100,2),TV(100,2),DTHV(100,2),
      6 BETAV(100,2),MH(100,2),DTHM(100,2),BETAH(100,2),RHH(100,2),
      7 BEH(100,2),PLOSHH(100,2)
      IPF = IV(IM)*IT-ITV(IM,1)
      RETURN
      END
      SUBROUTINE CONTIN(XEST,YCALC,IND,JZ,YGIV,XDEL)
C
C--CONTIN CALCULATES AN ESTIMATE OF THE RELATIVE FLOW VELOCITY
C--FOR USE IN THE VELOCITY GRADIENT EQUATION
C
      DIMENSION X(3),Y(3)
      NCALL = NCALL+1
      IF (IND.NE.1.AND.NCALL.GT.100) GO TO 160
      GO TO (10,30,40,50,60,110,150),IND
C--FIRST CALL
10 NCALL = 1
      XORIG = XEST
      IF (YCALC.GT.YGIV.AND.JZ.EQ.1) GO TO 20
      IND = 2
      Y(1) = YCALC
      X(1) = 0.
      XEST = XEST+XDEL
      RETURN
20 IND = 3
      Y(3) = YCALC
      X(3) = 0.
      XEST = XEST-XDEL
      RETURN
C--SECOND CALL
30 IND = 4
      Y(2) = YCALC
      X(2) = XEST-XORIG
      XEST = XEST+XDEL
      RETURN
40 IND = 5
      Y(2) = YCALC
      X(2) = XEST-XORIG
      XEST = XEST-XDEL
      RETURN
C -- THIRD OR LATER CALL - FIND SUBSONIC OR SUPERSONIC SOLUTION
50 Y(3) = YCALC

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X(3) = XEST-XORIG
GO TO 70
60 Y(1) = YCALC
X(1) = XEST-XORIG
70 IF (YGIV.LT.AMINI(Y(1),Y(2),Y(3))) GO TO (120,130),JZ
80 IND = 6
CALL PABC(X,Y,APA,BPB,CPC)
DISCR = BPB**2-4.*APA*(CPC-YGIV)
IF (DISCR.LT.0.) GO TO 140
IF (ABS(400.*APA*(CPC-YGIV)).LE.BPB**2) GO TO 90
XEST = -BPB-SIGN(SQRT(DISCR),APA)
IF (JZ.EQ.1.AND.APA.GT.0..AND.Y(3).GT.Y(1)) XEST = -BPB+
ISQRT(DISCR)
IF (JZ.EQ.2.AND.APA.LT.0.) XEST = -BPB-SQRT(DISCR)
XEST = XEST/2./APA
GO TO 100
90 IF (JZ.EQ.2.AND.BPB.GT.0.) GO TO 130
ACB2 = APA/BPB*(CPC-YGIV)/BPB
IF (ABS(ACB2).LE.1.E-8) ACB2=0.
XEST = -(CPC-YGIV)/BPB*(1.+ACB2+2.*ACB2**2)
100 IF (XEST.GT.X(3)) GO TO 130
IF (XEST.LT.X(1)) GO TO 120
XEST = XEST+XORIG
RETURN
C--FOURTH OR LATER CALL - NOT CHOKED
110 IF(XEST-XORIG.GT.X(3)) GO TO 130
IF(XEST-XORIG.LT.X(1)) GO TO 120
Y(2) = YCALC
X(2) = XEST-XORIG
GO TO 70
C--THIRD OR LATER CALL - SOLUTION EXISTS,
C--BUT RIGHT OR LEFT SHIFT REQUIRED
120 IND = 5
C--LEFT SHIFT
XEST = X(1)-XDEL+XORIG
XOSHFT = XEST-XORIG
XORIG = XEST
Y(3) = Y(2)
X(3) = X(2)-XOSHFT
Y(2) = Y(1)
X(2) = X(1)-XOSHFT
RETURN
130 IND = 4
C--RIGHT SHIFT
XEST = X(3)+XDEL+XORIG
XOSHFT = XEST-XORIG
XORIG = XEST
Y(1) = Y(2)
X(1) = X(2)-XOSHFT
Y(2) = Y(3)
X(2) = X(3)-XOSHFT
RETURN
C--THIRD OR LATER CALL - APPEARS TO BE CHOKED
140 XEST = -BPB/2./APA
IND = 7
IF (XEST.LT.X(1)) GO TO 120
IF(XEST.GT.X(3)) GO TO 130
XEST = XEST+XORIG
RETURN
C--FOURTH OR LATER CALL - PROBABLY CHOKED
CONTIN38 150 IF (YCALC.GE.YGIV) GO TO 110
CONTIN39 IND = 10
CONTIN40 RETURN
CONTIN41 C--NO SOLUTION FOUND IN 100 ITERATIONS
CONTIN42 160 IND = 11
CONTIN43 RETURN
CONTIN44 END
CONTIN45 SUBROUTINE PABC(X,Y,A,B,C)
CONTIN46 C
CONTIN47 C--PABC CALCULATES COEFFICIENTS A,B,C OF THE PARABOLA
CONTIN48 C--Y=A*X**2+B*X+C, PASSING THROUGH THE GIVEN X,Y POINTS
CONTIN49 C
CONTIN50 DIMENSION X(3),Y(3)
CONTIN51 C1 = X(3)-X(1)
CONTIN52 C2 = (Y(2)-Y(1))/(X(2)-X(1))
CONTIN53 A = (C1*C2-Y(3)+Y(1))/C1/(X(2)-X(3))
CONTIN54 B = C2-(X(1)+X(2))*A
CONTIN55 C = Y(1)-X(1)*B-X(1)**2*A
CONTIN56 RETURN
CONTIN57 END
CONTIN58 SUBROUTINE SPLINE (X,Y,N,SLOPE,EM)
CONTIN59 C
CONTIN60 C--SPLINE CALCULATES FIRST AND SECONDD DERIVATIVES AT SPLINE POINTS
CONTIN61 C--END CONDITION - SECOND DERIVATIVES AT END POINTS ARE
CONTIN62 C--SDR1 AND SDRN TIMES SECONDD DERIVATIVES AT ADJACENT POINTS
CONTIN63 C
CONTIN64 COMMON NREAD,NWRIT
CONTIN65 DIMENSION X(N),Y(N),SLOPE(N),EM(N)
CONTIN66 DIMENSION G(101),SB(101)
CONTIN67 IERR = 0
CONTIN68 SDR1 = .5
CONTIN69 SDRN = .5
CONTIN70 C = X(2)-X(1)
CONTIN71 IF (C.EQ.0.) GO TO 50
CONTIN72 SB(1) = -SDR1
CONTIN73 G(1) = 0.
CONTIN74 NO = N-1
CONTIN75 IF (NO.LE.0) GO TO 60
CONTIN76 IF (NO.EQ.1) GO TO 20
CONTIN77 DO 10 I=2,NO
CONTIN78 A = C
CONTIN79 C = X(I+1)-X(I)
CONTIN80 IF (A*C.EQ.0.) GO TO 50
CONTIN81 IF (A*C.LT.0.) IERR = 1
CONTIN82 W = 2.*(A+C)-A*SB(I-1)
CONTIN83 SB(I) = C/W
CONTIN84 F = (Y(I+1)-Y(I))/C-(Y(I)-Y(I-1))/A
CONTIN85 G(I) = (6.*F-A*G(I-1))/W
CONTIN86 20 EM(N) = SDRN*G(N-1)/(1.+SDRN*SB(N-1))
CONTIN87 DO 30 I=2,N
CONTIN88 K = N+1-I
CONTIN89 EM(K) = G(K)-SB(K)*EM(K+1)
CONTIN90 SLOPE(1) = (X(1)-X(2))/6.*(2.*EM(1)+EM(2))*(Y(2)-Y(1))/(X(2)-X(1))
CONTIN91 DO 40 I=2,N
CONTIN92 40 SLOPE(I) = (X(I)-X(I-1))/6.*(2.*EM(I)+EM(I-1))*(Y(I)-Y(I-1))/
CONTIN93 (X(I)-X(I-1))
CONTIN94 IF (IERR.EQ.0) RETURN
CONTIN95 50 WRITE(NWRIT,1000)
CONTIN96 WRITE(NWRIT,1000) N,(X(I),Y(I),I=1,N)
CONTIN97 IF (IERR.EQ.0) STOP
CONTIN98
CONTIN99
CONTI100
CONTI101
CONTI102
CONTI103
CONTI104
PABC 2
PABC 3
PABC 4
PABC 5
PABC 6
PABC 7
PABC 8
PABC 9
PABC 10
PABC 11
PABC 12
PABC 13
PABC 14
SPLINE 2
SPLINE 3
SPLINE 4
SPLINE 5
SPLINE 6
SPLINE 7
SPLINE 8
SPLINE 9
SPLINE10
SPLINE11
SPLINE12
SPLINE13
SPLINE14
SPLINE15
SPLINE16
SPLINE17
SPLINE18
SPLINE19
SPLINE20
SPLINE21
SPLINE22
SPLINE23
SPLINE24
SPLINE25
SPLINE26
SPLINE27
SPLINE28
SPLINE29
SPLINE30
SPLINE31
SPLINE32
SPLINE33
SPLINE34
SPLINE35
SPLINE36
SPLINE37
SPLINE38
SPLINE39
SPLINE40
SPLINE41

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WRITE(NWRIT,1030)
RETURN
60 WRITE(NWRIT,1010)
WRITE(NWRIT,1020) N,(X(I),Y(I),I=1,N)
STOP
1000 FORMAT (1H1,10X,44HSPLINE ERROR -- ONE OF THREE POSSIBLE CAUSES/
117X,51H1. ADJACENT X POINTS ARE DUPLICATES OF EACH OTHER./
217X,30H2. SOME X POINTS ARE OUT OF SEQUENCE./
317X,32H3. SOME X POINTS ARE UNDEFINED.)
1010 FORMAT (1H1,10X,62HSPLINE ERROR -- NUMBER OF SPLINE POINTS GIVEN IS
1S LESS THAN TWO)
1020 FORMAT (//17X,10HNUMBER OF POINTS =,I4//17X,0HX ARRAY,6X,0HY ARR
1AY/(17X,2G13.5))
1030 FORMAT (1H1)
END
SUBROUTINE SPLINT (X,Y,N,Z,MAX,YINT,DYDX,D2YDX2)
C
C--SPLINT CALCULATES INTERPOLATED POINTS AND DERIVATIVES
C--FOR A SPLINE CURVE
C--END CONDITION - SECOND DERIVATIVES AT END POINTS ARE
C--SDR1 AND SDRN TIMES SECOND DERIVATIVES AT ADJACENT POINTS
C
COMMON NREAD,NWRIT
DIMENSION X(N),Y(N),Z(MAX),YINT(MAX),DYDX(MAX),D2YDX2(MAX)
DIMENSION G(101),SB(101),EM(101)
IERR = 0
SDR1 = .5
SDRN = .5
TOLER = ABS(X(N)-X(1))/FLOAT(N)*1.E-5
C = X(2)-X(1)
IF (C.EQ.0.) GO TO 130
SB(1) = -SDR1
G(1) = 0.
NO = N-1
IF (NO.LE.0) GO TO 140
IF (NO.EQ.1) GO TO 20
DO 10 I=2,NO
A = C
C = X(I+1)-X(I)
IF (A*C.EQ.0.) GO TO 130
IF (A*C.LT.0.) IERR = 1
W = 2.*(A*C)-A*SB(I-1)
SB(I) = C/W
F = (Y(I+1)-Y(I))/C-(Y(I)-Y(I-1))/A
10 G(I) = (6.*F-A*G(I-1))/W
20 EM(N) = SDR1*G(N-1)/(1.+SDRN*SB(N-1))
DO 30 I=2,N
K = N+1-I
30 EM(K) = G(K)-SB(K)*EM(K+1)
IF (MAX.LE.0) RETURN
C
ENTRY SPLINT
DO 120 I=1,MAX
K=2
IF (ABS(Z(I)-X(1)).LT.TOLER) GO TO 40
IF (Z(I).GT.2.0*X(1)-X(2)) GO TO 50
GO TO 80
40 YINT(I) = Y(1)
SK = X(K)-X(K-1)
GO TO 110
SPLINE42
SPLINE43
SPLINE44
SPLINE45
SPLINE46
SPLINE47
SPLINE48
SPLINE49
SPLINE50
SPLINE51
SPLINE52
SPLINE53
SPLINE54
SPLINE55
SPLINE56
SPLINT 2
SPLINT 3
SPLINT 4
SPLINT 5
SPLINT 6
SPLINT 7
SPLINT 8
SPLINT 9
SPLINT10
SPLINT11
SPLINT12
SPLINT13
SPLINT14
SPLINT15
SPLINT16
SPLINT17
SPLINT18
SPLINT19
SPLINT20
SPLINT21
SPLINT22
SPLINT23
SPLINT24
SPLINT25
SPLINT26
SPLINT27
SPLINT28
SPLINT29
SPLINT30
SPLINT31
SPLINT32
SPLINT33
SPLINT34
SPLINT35
SPLINT36
SPLINT37
SPLINT38
SPLINT39
SPLINT40
SPLINT41
SPLINT42
SPLINT43
SPLINT44
SPLINT45
SPLINT46
50 IF (ABS(Z(I)-X(K)).LT.TOLER) GO TO 60
IF (Z(I).GT.X(K)) GO TO 70
GO TO 100
60 YINT(I) = Y(K)
SK = X(K)-X(K-1)
GO TO 110
70 IF (K.GE.N) GO TO 90
K = K+1
GO TO 50
80 S2 = X(2)-X(1)
Y0 = EM(1)*S2**2+2.*Y(1)-Y(2)
DYDX(I) = (Y(2)-Y(1))/S2-7.*EM(1)/6.*S2
YINT(I) = Y0+DYDX(I)*(Z(I)-X(1))+S2)
D2YDX2(I) = 0.
GO TO 120
90 IF (Z(I).LT.2.*X(N)-X(N-1)) GO TO 100
SN = X(N)-X(N-1)
YNP1 = EM(N)*SN**2+2.*Y(N)-Y(N-1)
DYDX(I) = (Y(N)-Y(N-1))/SN+7.*EM(N)/6.*SN
YINT(I) = YNP1+DYDX(I)*(Z(I)-X(N)-SN)
D2YDX2(I) = 0.
GO TO 120
100 SK = X(K)-X(K-1)
YINT(I) = EM(K-1)*(X(K)-Z(I))**3/6./SK +EM(K)*(Z(I)-X(K-1))**3/6.
1 /SK*(Y(K)/SK -EM(K)*SK /6.)*(Z(I)-X(K-1))*(Y(K-1)/SK -EM(K-1))
2 *SK/6.)*(X(K)-Z(I))
110 DYDX(I) = -EM(K-1)*(X(K)-Z(I))**2/2.0/SK +EM(K)*(X(K-1)-Z(I))**2/2.
1 /SK*(Y(K)-Y(K-1))/SK -(EM(K)-EM(K-1))*SK/6.
D2YDX2(I) = EM(K)-(X(K)-Z(I))/SK*(EM(K)-EM(K-1))
120 CONTINUE
IF (IERR.EQ.0) RETURN
130 WRITE(NWRIT,1000)
WRITE(NWRIT,1020) N,(X(I),Y(I),I=1,N)
IF (IERR.EQ.0) STOP
WRITE(NWRIT,1030)
RETURN
140 WRITE(NWRIT,1010)
WRITE(NWRIT,1020) N,(X(I),Y(I),I=1,N)
STOP
1000 FORMAT (1H1,10X,44HSPLINT ERROR -- ONE OF THREE POSSIBLE CAUSES/
117X,51H1. ADJACENT X POINTS ARE DUPLICATES OF EACH OTHER./
217X,30H2. SOME X POINTS ARE OUT OF SEQUENCE./
317X,32H3. SOME X POINTS ARE UNDEFINED.)
1010 FORMAT (1H1,10X,62HSPLINT ERROR -- NUMBER OF SPLINE POINTS GIVEN IS
1S LESS THAN TWO)
1020 FORMAT (//17X,10HNUMBER OF POINTS =,I4//17X,0HX ARRAY,6X,0HY ARR
1AY/(17X,2G13.5))
1030 FORMAT (1H1)
END
SUBROUTINE SPLISL(X,Y,N,YIP,YNP,SLOPE,EM)
C
C--SPLISL CALCULATES FIRST AND SECOND DERIVATIVES AT SPLINE POINTS
C--END CONDITION - FIRST DERIVATIVES SPECIFIED AT END POINTS
C
COMMON NREAD,NWRIT
DIMENSION X(N),Y(N),SLOPE(N),EM(N)
IERR = 0
C = X(2)-X(1)
IF (C.EQ.0.) GO TO 50
SPLINT47
SPLINT48
SPLINT49
SPLINT50
SPLINT51
SPLINT52
SPLINT53
SPLINT54
SPLINT55
SPLINT56
SPLINT57
SPLINT58
SPLINT59
SPLINT60
SPLINT61
SPLINT62
SPLINT63
SPLINT64
SPLINT65
SPLINT66
SPLINT67
SPLINT68
SPLINT69
SPLINT70
SPLINT71
SPLINT72
SPLINT73
SPLINT74
SPLINT75
SPLINT76
SPLINT77
SPLINT78
SPLINT79
SPLINT80
SPLINT81
SPLINT82
SPLINT83
SPLINT84
SPLINT85
SPLINT86
SPLINT87
SPLINT88
SPLINT89
SPLINT90
SPLINT91
SPLINT92
SPLINT93
SPLINT94
SPLINT95
SPLISL 2
SPLISL 3
SPLISL 4
SPLISL 5
SPLISL 6
SPLISL 7
SPLISL 8
SPLISL 9
SPLISL10
SPLISL11
SPLISL12

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SB(I) = .5
F = (Y(2)-Y(1))/C-Y1P
G(1) = 3.*F/C
NO = N-1
IF (NO.LE.0) GO TO 60
IF (NO.EQ.1) GO TO 20
DO 10 I=2,NO
A = C
C = X(I+1)-X(I)
IF (A*C.EQ.0.) GO TO 50
IF (A*C.LT.0.) IERR = 1
W = 2.*(A+C)-A*SB(I-1)
SB(I) = C/W
F = (Y(I+1)-Y(I))/C-(Y(I)-Y(I-1))/A
10 G(I) = (6.*F-A*G(I-1))/W
20 W = C*(2.-SB(N-1))
F = YNP-(Y(N)-Y(N-1))/C
EM(N) = (6.*F-C*G(N-1))/W
DO 30 I=2,N
K = N+1-I
30 EM(K) = G(K)-SB(K)*EM(K+1)
SLOPE(1) = Y1P
DO 40 I=2,NO
40 SLOPE(I) = (X(I)-X(I-1))/6.*(2.*EM(I)+EM(I-1))+Y(I)-Y(I-1)/
1(X(I)-X(I-1))
SLOPE(N) = YNP
IF (IERR.EQ.0) RETURN
50 WRITE(NWRIT,1000)
WRITE(NWRIT,1020) N,(X(I),Y(I),I=1,N)
IF (IERR.EQ.0) STOP
WRITE(NWRIT,1030)
RETURN
60 WRITE(NWRIT,1010)
WRITE(NWRIT,1020) N,(X(I),Y(I),I=1,N)
STOP
1000 FORMAT (1H1,10X,44HSPLISL ERROR -- ONE OF THREE POSSIBLE CAUSES/
117X,51H1. ADJACENT X POINTS ARE DUPLICATES OF EACH OTHER./
217X,38H2. SOME X POINTS ARE OUT OF SEQUENCE./
317X,32H3. SOME X POINTS ARE UNDEFINED.)
1010 FORMAT (1H1,10X,62HSPLISL ERROR -- NUMBER OF SPLINE POINTS GIVEN
1S LESS THAN TWO)
1020 FORMAT (//17X,18HNUMBER OF POINTS =,I4//17X,8HX ARRAY,6X,8HY ARR
1AY/(17X,2G13.5))
1030 FORMAT (1H1)
END
SUBROUTINE SPLIPR(DX,Y,N,SLOPE,EM)
C
C--SPLIPR CALCULATES FIRST AND SECOND DERIVATIVES AT EQUALLY SPACED
C--SPLINE POINTS, USING SOR
C--END CONDITIONS - FIRST AND SECOND DERIVATIVES ARE PERIODIC, AND
C--Y INCREASES BY ONE IN THIS PERIOD
C
COMMON NREAD,NWRIT
DIMENSION Y(N),SLOPE(N),EM(N)
DIMENSION F(101)
IF (N.LT.2) GO TO 50
NO = N-1
DYP = 1.+Y(1)-Y(N)
CONST = 3./2./DX**2
DO 10 I=1,NO
SPLISL13 EM(I) = 0.
SPLISL14 DYM = DYP
SPLISL15 DYP = Y(I+1)-Y(I)
SPLISL16 10 F(I) = CONST*(DYP-DYM)
SPLISL17 EM(N) = 0.
SPLISL18 DYM = DYP
SPLISL19 DYP = 1.+Y(1)-Y(N)
SPLISL20 F(N) = CONST*(DYP-DYM)
SPLISL21 ORF = 2./(1.+SQRT(.75))
SPLISL22 DO 30 K=1,10
SPLISL23 EM(1) = EM(1)-ORF*(EM(N)+EM(2))/4.*EM(1)-F(1)
SPLISL24 IF (NO.EQ.1) GO TO 30
SPLISL25 DO 20 I=2,NO
SPLISL26 20 EM(I) = EM(I)-ORF*((EM(I-1)+EM(I+1))/4.*EM(I)-F(I))
SPLISL27 30 EM(N) = EM(N)-ORF*((EM(N-1)+EM(1))/4.*EM(N)-F(N))
SPLISL28 SLOPE(1) = -DX/6.*(2.*EM(1)+EM(2))+Y(2)-Y(1)/DX
SPLISL29 DO 40 I=2,N
SPLISL30 40 SLOPE(I) = DX/6.*(2.*EM(I)-EM(I-1))+Y(I)-Y(I-1)/DX
SPLISL31 RETURN
SPLISL32 50 WRITE(NWRIT,1000)
SPLISL33 STOP
SPLISL34 1000 FORMAT (1H1,10X,62HSPLIPR ERROR -- NUMBER OF SPLINE POINTS GIVEN
SPLISL35 1S LESS THAN TWO)
SPLISL36 END
SPLISL37 SUBROUTINE INTGRL(X,Y,N,SUM)
C
C--INTGRL CALCULATES THE INTEGRAL OF A SPLINE CURVE PASSING THROUGH
C--A GIVEN SET OF POINTS
C--END CONDITION - SECOND DERIVATIVES AT END POINTS ARE
C--SDR1 AND SDRN TIMES SECOND DERIVATIVES AT ADJACENT POINTS
C
COMMON NREAD,NWRIT
DIMENSION X(N),Y(N),SUM(N)
DIMENSION G(101),SB(101),EM(101)
IERR = 0
SDR1 = .5
SDRN = .5
C = X(2)-X(1)
IF (C.EQ.0.) GO TO 50
SB(1) = -SDR1
G(1) = 0.
NO = N-1
IF (NO.LE.0) GO TO 60
IF (NO.EQ.1) GO TO 20
DO 10 I=2,NO
A = C
C = X(I+1)-X(I)
IF (A*C.EQ.0.) GO TO 60
IF (A*C.LT.0.) IERR = 1
W = 2.*(A+C)-A*SB(I-1)
SB(I) = C/W
F = (Y(I+1)-Y(I))/C-(Y(I)-Y(I-1))/A
10 G(I) = (6.*F-A*G(I-1))/W
20 EM(N) = SDRN*G(N-1)/(1.+SDRN*SB(N-1))
DO 30 I=2,N
K = N+1-I
30 EM(K) = G(K)-SB(K)*EM(K+1)
SUM(1) = 0.
DO 40 I=2,N
40 SUM(I) = SUM(I-1)+(X(I)-X(I-1))*(Y(I)+Y(I-1))/2.-
(X(I)-X(I-1))**3
SPLIPR17
SPLIPR18
SPLIPR19
SPLIPR20
SPLIPR21
SPLIPR22
SPLIPR23
SPLIPR24
SPLIPR25
SPLIPR26
SPLIPR27
SPLIPR28
SPLIPR29
SPLIPR30
SPLIPR31
SPLIPR32
SPLIPR33
SPLIPR34
SPLIPR35
SPLIPR36
SPLIPR37
SPLIPR38
SPLIPR39
SPLIPR40
INTGRL 2
INTGRL 3
INTGRL 4
INTGRL 5
INTGRL 6
INTGRL 7
INTGRL 8
INTGRL 9
INTGRL 10
INTGRL 11
INTGRL 12
INTGRL 13
INTGRL 14
INTGRL 15
INTGRL 16
INTGRL 17
INTGRL 18
INTGRL 19
INTGRL 20
INTGRL 21
INTGRL 22
INTGRL 23
INTGRL 24
INTGRL 25
INTGRL 26
INTGRL 27
INTGRL 28
INTGRL 29
INTGRL 30
INTGRL 31
INTGRL 32
INTGRL 33
INTGRL 34
INTGRL 35
INTGRL 36
INTGRL 37

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1*(EM(I)*EM(I-1))/24.
IF (IERR.EQ.0) RETURN
50 WRITE(NWRIT,1000)
WRITE(NWRIT,1020) N,(X(I),Y(I),I=1,N)
IF (IERR.EQ.0) STOP
WRITE(NWRIT,1030)
RETURN
60 WRITE(NWRIT,1010)
WRITE(NWRIT,1020) N,(X(I),Y(I),I=1,N)
STOP
1000 FORMAT (1H1,10X,44HINTGRL ERROR -- ONE OF THREE POSSIBLE CAUSES/
117X,51H1. ADJACENT X POINTS ARE DUPLICATES OF EACH OTHER./
217X,30H2. SOME X POINTS ARE OUT OF SEQUENCE./
317X,32H3. SOME X POINTS ARE UNDEFINED.)
1010 FORMAT (1H1,10X,62HINTGRL ERROR -- NUMBER OF SPLINE POINTS GIVEN
15 LESS THAN TWO)
1020 FORMAT (//17X,10HNUMBER OF POINTS =,I4//17X,8HX ARRAY,6X,6HY ARR
1AY(17X,20I3.5))
1030 FORMAT (1H1)
END
SUBROUTINE PLOTMY(X,Y,K,P)
C--PLOTMY PLOTS MULTIPLE CURVES
COMMON NREAD,NWRIT
LOGICAL FORY,STUG,TONLY
DIMENSION YLABEL(11),A(104),KPCSTD(6),XLAB(8),YLAB(6),FKFD(6)
DIMENSION X(1),Y(1),P(1),K(1)
LEVEL 2, X,Y
COMMON /JOLD/ F,DX,TLINX,N,LABOUT,KFD,FORY,STUG,TONLY
EQUIVALENCE (KPC,TPC)
DATA BLANK,XGRID,YGRID,RMARK /1H ,1H-,1H1,1H=/
DATA KPCSTD /1H*,1H+,1H0,1HX,1H=,1H0 /
DATA XLAB/4H (1H,4H ,5,4HX, F,4H10.0,4H,104,4HA1,F,4H10.0,4H) /
DATA YLAB/4H (1H,4H , ,4H8X, ,4H 11F,4H10.0,4H) /
DATA FKFD/4H10.1,4H10.2,4H10.3,4H10.4,4H10.5,4H10.6/
C
100 WRITE(NWRIT,1000)
KODE = K(1)
KN = K(2)
NPTS = K(3)
LABOUT = 1
KTL = 1
FKFD0 = XLAB(4)
IF(P(1).GT.2.) GO TO 110
C--P(1) = 1. (DUPX)
KTL = KN
GO TO 130
110 IF(P(1).GT.4.) GO TO 140
C--P(1) = 3. (DUPY)
KTIMES = KN-1
DO 120 I=1,KTIMES
MM = I*NPTS
K(2*I+3) = NPTS
DO 120 II=1,NPTS
L = MM*II
120 Y(L) = Y(II)
C--P(1) = 1. OR 3. (DUPX OR DUPY)
130 NPTST = KN*NPTS
TLINX = 55*(1+NPTS/35)
GO TO 160
C--P(1) = 5. (NO DUP)
INTGRL38
INTGRL39
INTGRL40
INTGRL41
INTGRL42
INTGRL43
INTGRL44
INTGRL45
INTGRL46
INTGRL47
INTGRL48
INTGRL49
INTGRL50
INTGRL51
INTGRL52
INTGRL53
INTGRL54
INTGRL55
INTGRL56
INTGRL57
PLOTMY 2
PLOTMY 3
PLOTMY 4
PLOTMY 5
PLOTMY 6
PLOTMY 7
PLOTMY 8
PLOTMY 9
PLOTMY 10
PLOTMY 11
PLOTMY 12
PLOTMY 13
PLOTMY 14
PLOTMY 15
PLOTMY 16
PLOTMY 17
PLOTMY 18
PLOTMY 19
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PLOTMY 24
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PLOTMY 26
PLOTMY 27
PLOTMY 28
PLOTMY 29
PLOTMY 30
PLOTMY 31
PLOTMY 32
PLOTMY 33
PLOTMY 34
PLOTMY 35
PLOTMY 36
PLOTMY 37
PLOTMY 38
PLOTMY 39
PLOTMY 40
PLOTMY 41
140 NPTST = 0
DO 150 I=1,KN
150 NPTST = NPTST*K(2*I+1)
TLINX = 55*(1+NPTST/(35*KN))
160 IF(MOD(KODE,2).NE.0) GO TO 180
C--OPTION 1 NOT CHOSEN
DO 170 I=1,KN
170 K(2*I+2) = KPCSTD(I)
180 NX = 10
C--OPTION 2
IF(MOD(KODE/2,2).NE.0) NX = P(3)
IF (NX.EQ.0) NX = 1000
NY = 10
C--OPTION 4
IF(MOD(KODE/4,2).NE.0) NY = P(4)
IF(NY.EQ.0) NY = 100
C--OPTION 8 NOT AVAILABLE
IF(MOD(KODE/8,2).NE.0) WRITE(NWRIT,1080)
C--ALL OPTIONS
FORY = .TRUE.
STUG = .FALSE.
TONLY = .FALSE.
IF(MOD(KODE/32,2).EQ.0) GO TO 190
C--OPTION 32
STUG = .TRUE.
KSY = P(9)
PWR10Y = 10.** (KSY-6)
FY = P(10)*PWR10Y
F = FY
C--SPECIAL CASE OF OPTION 32
IF(P(5).GE.2.) GO TO 190
TONLY = .TRUE.
DY = P(11)*PWR10Y
DX = DY
C--ALL OPTIONS
190 N = NPTST
CALL PISTUG(Y)
IF(DX.EQ.0.) GO TO 510
FY = F
DY = DX
C--MODIFY Y LABEL FORMAT IF NECESSARY
IF(KFD.GT.0.AND.KFD.LE.6) YLAB(5) = FKFD(KFD)
C--SET LOGICAL VARIABLES
FORY = .FALSE.
STUG = .FALSE.
TONLY = .FALSE.
C--OPTION 16
IF(MOD(KODE/16,2).EQ.0) GO TO 200
STUG = .TRUE.
KSX = P(6)
PWR10X = 10.** (KSX-6)
FX = P(7)*PWR10X
F = FX
C--SPECIAL CASE OF OPTION 16
IF(MOD(IFIX(P(5)),2).EQ.1) GO TO 200
TONLY = .TRUE.
DX = P(8)*PWR10X
200 IF(P(1).LT.2.) N = NPTS
C--ALL OPTIONS
ILIM = N
PLOTMY42
PLOTMY43
PLOTMY44
PLOTMY45
PLOTMY46
PLOTMY47
PLOTMY48
PLOTMY49
PLOTMY50
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PLOTMY86
PLOTMY87
PLOTMY88
PLOTMY89
PLOTMY90
PLOTMY91
PLOTMY92
PLOTMY93
PLOTMY94
PLOTMY95
PLOTMY96
PLOTMY97
PLOTMY98
PLOTMY99
PLOTMY100
PLOTMY101

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CALL PISTUG(X)
IF(DX.EQ.0.) GO TO 510
FX = F
C--MODIFY X LABEL FORMAT IF NECESSARY
IF(KFD.GT.0.AND.KFD.LE.6) XLAB(4) = FKFD(KFD)
IF(KFD.GT.0.AND.KFD.LE.6) XLAB(7) = FKFD(KFD)
C--COMPUTE AND TEST Y LABELS
210 TDY = DY*10.
DO 220 I=1,11
TEMP = FY*FLOAT(I-1)*TDY
ATEMP = ABS(TEMP)
IF (ATEMP.LT.1.E-7) TEMP = 0.
IF (ATEMP.GE.1.E+7) LABOUT = 2
220 YLABEL(I) = TEMP
KSYLAB = 1
C--WRITE Y LABELS
230 WRITE(NWRIT,YLAB) YLABEL
IF(KSYLAB.EQ.2) GO TO 510
C--INITIALIZE VARIABLES FOR MAIN PLOT
KSYLAB = 2
LCTR = 0
NCTR = 1
KOUT = 1
KQUIT = 1
XMIN = FX-DX/2.
XMAX = FX+DX/2.
C--FILL THE A ARRAY FOR CURRENT LINE OF PLOT
C---FILL THE A ARRAY WITH BLANKS OR X-GRID MARKS, AS APPROPRIATE
240 AFILL = BLANK
IF(MOD(LCTR,NX).EQ.0) AFILL = XGRID
C--FILL IN LINE AND INSERT Y GRID MARKS
260 DO 270 I=2,104
270 A(I) = AFILL
DO 280 I=2,104,NY
280 A(I) = YGRID
A(1) = BLANK
IF(KOUT.EQ.2) GO TO 410
C--FIND INDEX OF NEXT X ON THE CURRENT LINE
IGON = 1
290 CONTINUE
IF(IGON.GT.ILIM) GO TO 420
DO 300 I=IGON,ILIM
IF(X(I).LE.XMIN.OR.X(I).GT.XMAX) GO TO 300
IMIN = I
GO TO 310
300 CONTINUE
C--IF NO MORE POINTS ON THE CURRENT LINE, WRITE IT OUT
GO TO 420
C--PLACE PLOTTING CHARACTER IN PROPER POSITION (KYL) IN THE A ARRAY
310 DO 390 IM=1,KTL
LL = IMIN+(IM-1)*NPTS
KY = (Y(LL)-FY)/DY+.5
IF(P(1).LT.2.) GO TO 340
C--DUPLY OR NODUP
IK = 0
KLAST = 2*KNT+1
DO 320 IL=3,KLAST,2
IK = IK+K(IL)
IF(IK.GE.IMIN) GO TO 330
320 CONTINUE

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PLOTM102 LABOUT = 5
PLOTM103 GO TO 510
PLOTM104 330 KPC = K(IL+1)
PLOTM105 GO TO 350
PLOTM106 C--DUPX
PLOTM107 340 KPC = K(2*IM+2)
PLOTM108 C--DEFINE KYL
PLOTM109 350 KYL = KY+2
PLOTM110 C--PLOT OUT RANGE Y AS
PLOTM111 IF(KY.LT.0) GO TO 360
PLOTM112 IF(KY.GT.101) GO TO 370
PLOTM113 GO TO 390
PLOTM114 360 KYL = 1
PLOTM115 GO TO 380
PLOTM116 370 KYL = 104
PLOTM117 380 TPC = RMARK
PLOTM118 390 A(KYL) = TPC
PLOTM119 C--ARE ALL POINTS DONE
PLOTM120 IF(NCTR.GE.ILIM) GO TO 400
PLOTM121 NCTR = NCTR+1
PLOTM122 IGON = IMIN+1
PLOTM123 GO TO 290
PLOTM124 C--ALL POINTS PLOTTED FOR ENTIRE PLOT
PLOTM125 400 KOUT = 2
PLOTM126 410 IF(MOD(LCTR,10).GT.5) NX = 10
PLOTM127 IF(MOD(LCTR,NX).EQ.0) KQUIT = 2
PLOTM128 C
PLOTM129 C--WRITE CURRENT LINE OF PLOT
PLOTM130 420 IF(MOD(LCTR,10).EQ.0) GO TO 430
PLOTM131 C--WRITE LINE WITHOUT XLABEL
PLOTM132 WRITE(NWRIT,1020) A
PLOTM133 GO TO 440
PLOTM134 430 XLABEL = FX+FLOAT(LCTR)*DX
PLOTM135 TEMP = ABS(XLABEL)
PLOTM136 IF(TEMP.GE.1.E+7) LABOUT = 2
PLOTM137 IF(TEMP.LT.1.E-7) XLABEL = 0.
PLOTM138 C--WRITE LINE WITH XLABEL
PLOTM139 WRITE(NWRIT,XLAB) XLABEL,A,XLABEL
PLOTM140 C--INCREMENT LINE COUNTER
PLOTM141 440 LCTR = LCTR+1
PLOTM142 XMIN = XMAX
PLOTM143 XMAX = DX*(FLOAT(LCTR)+.5)*FX
PLOTM144 C--DO NEXT LINE
PLOTM145 GO TO (240,230),KQUIT
PLOTM146 C
PLOTM147 C--PLOT COMPLETED - WRITE FINAL LINE OR ERROR MESSAGE
PLOTM148 510 GO TO (560,520,540,540,550),LABOUT
PLOTM149 520 WRITE(NWRIT,1040)
PLOTM150 GO TO 570
PLOTM151 540 WRITE(NWRIT,1050) (X(I),Y(I),I=1,2),(K(J),J=1,3),P(1)
PLOTM152 GO TO 570
PLOTM153 550 WRITE(NWRIT,1060)
PLOTM154 560 WRITE(NWRIT,1000)
PLOTM155 C--RESTORE INITIAL FORMATS BEFORE RETURN
PLOTM156 570 CONTINUE
PLOTM157 YLAB(5) = FKFD0
PLOTM158 XLAB(4) = FKFD0
PLOTM159 XLAB(7) = FKFD0
PLOTM160 RETURN
PLOTM161 C--FORMAT STATEMENTS

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PLOTM162
PLOTM163
PLOTM164
PLOTM165
PLOTM166
PLOTM167
PLOTM168
PLOTM169
PLOTM170
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PLOTM218
PLOTM219
PLOTM220
PLOTM221

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1000 FORMAT(1H )
1020 FORMAT(1H ,15X,104A1)
1040 FORMAT(1H ,3X,10HBAD LABELS)
1050 FORMAT(1H ,5H N.G.,4G20.8,3I7,F8.2)
1060 FORMAT(1H ,16HERROR IN K ARRAY)
1080 FORMAT(1H ,98X,28HOPTION 8 NO LONGER AVAILABLE)
END
SUBROUTINE PISTUG(ARRAY)
C--PISTUG CALCULATES DX, KFD, AND FX OR FY
LOGICAL FORY,STUG,TONLY
DIMENSION ARRAY(1)
LEVEL 2, ARRAY
COMMON /JOLO/ F,DX,TLINX,N,LABOUT,KFD,FORY,STUG,TONLY
KHAR(XMAX) = INT(10*LOG10(XMAX)+40.)-40
C--FIND X1, THE FIRST POINT TO BE PLOTTED
10 X1 = ARRAY(1)
IF(STUG) GO TO 110
DO 100 J=2,N
100 X1 = AMIN(X1,ARRAY(J))
110 IF(STUG) X1 = F
C--FIND XN, THE LAST POINT TO BE PLOTTED
DIFMAX = 0.
DO 120 J=1,N
DIF = ABS(X1-ARRAY(J))
IF(DIF.LE.DIFMAX) GO TO 120
DIFMAX = DIF
IHOLD = J
120 CONTINUE
IF(DIFMAX.EQ.0.) GO TO 300
XN = ARRAY(IHOLD)
IF(TONLY) GO TO 150
C--CALCULATE DX
TLIN = 101.
IF(.NOT.FORY) TLIN = TLINX
C5 = (XN-X1)/TLIN
K7 = KHAR(ABS(C5))
C9 = ABS(C5)/10.**K7
D = 2.
IF(C9.GT.2.) D = 2.5
IF(C9.GT.2.5) D = 5.
IF(C9.GT.5.) D = 10.
DX = SIGN(D*10.**K7,C5)
C--CALCULATE KFD
150 K7 = KHAR(ABS(DX))
IF(FLOAT(K7)+1.5.GT.5.6) LABOUT = 2
KFD = MAX(0,MIN(16,-K7))
IF(STUG) GO TO 200
C--CALCULATE F (FX OR FY)
KC12 = INT(ABS(X1/DX))
KC15 = KC12-MOD(KC12,10)
IF(DX*X1.LT.0.) KC15 = KC15+10
IF(X1.LT.0.) KC15 = -KC15
F = ABS(DX)*FLOAT(KC15)
IF(.NOT.FORY) GO TO 200
C--CALCULATE F DIFFERENTLY, IF NECESSARY, TO KEEP ALL POINTS ON PLOT
TEMP = F+100.*DX
IF(TEMP.GE.SIGN(XN,DX)) GO TO 200
IF(DX*X1.LT.0.) KC12 = KC12+1
IF(X1.LT.0.) KC12 = -KC12
F = ABS(DX)*FLOAT(KC12)

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PLOTM222
PLOTM223
PLOTM224
PLOTM225
PLOTM226
PLOTM227
PLOTM228
PISTUG 2
PISTUG 3
PISTUG 4
PISTUG 5
PISTUG 6
PISTUG 7
PISTUG 8
PISTUG 9
PISTUG 10
PISTUG 11
PISTUG 12
PISTUG 13
PISTUG 14
PISTUG 15
PISTUG 16
PISTUG 17
PISTUG 18
PISTUG 19
PISTUG 20
PISTUG 21
PISTUG 22
PISTUG 23
PISTUG 24
PISTUG 25
PISTUG 26
PISTUG 27
PISTUG 28
PISTUG 29
PISTUG 30
PISTUG 31
PISTUG 32
PISTUG 33
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PISTUG 36
PISTUG 37
PISTUG 38
PISTUG 39
PISTUG 40
PISTUG 41
PISTUG 42
PISTUG 43
PISTUG 44
PISTUG 45
PISTUG 46
PISTUG 47
PISTUG 48
PISTUG 49
PISTUG 50
PISTUG 51
PISTUG 52
PISTUG 53
PISTUG 54

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C--RETURN
200 RETURN
C--ERROR RETURN
300 DX = 0.
LABOUT = 3
GO TO 200
END
SUBROUTINE BLADE(IPLOTB)
C *** THE CENTRAL CONTROL ROUTINE
REAL KIC, KICR, KIP, KIS, KM, KOC, KOCR, KOP, KOS, KTC, KTP, KTS
COMMON /SCALR/
1 BLADES, CALP, CCC, CEPE, CKTC, CKTS, C1, C2, DRCE, DRCLP, DRCLSB, BLADE 6
2, DPCMT, DRCMT, DRCOI, DRCS, DRCT, DRCTEP, DRCTES, DRCTI, DRCTMP, BLADE 7
3 DRCTS, DRCTPI, DRCTSI, DSME, DSMT, DSOT, DSP, DSP1, DSP2, DSSE, BLADE 8
4 DSSI, DSS2, DST, DSTI, EMT, IR, IW, KIC, KIP, KIS, KM, KOC, KOP, BLADE 9
5 KOS, KTC, KTP, KTS, PI, RCI, RCHS, RCD, RCT, RCTP, RCTS, REE, BLADE 10
6 RELEP, PELES, REM, REMS, REHT, REOI, RES, RET, RETEP, RETES, RETIBL, BLADE 11
7, RETMP, RETMS, RETP, RETS, RIC, SGAM, SALP, SKTC, SKTS, TEPE, BLADE 12
8 THMAX, TKTN
COMMON /INPUTB/
1 ALP, KICR, KOCR, NB, P, R, SOLID, T, THLE, THTE, THX, ZM
COMMON /INPUTT/RDUM1(17),IDUM1(16),XCHORD(2),XSTGR(2),XRI(2),
1 XRO(2),XBETI(2),XBETO(2),IDUM2(2),RDUM2(270),XMS(50,2),
2 XTHSP(50,2)
COMMON /BLANK/
1 THSP1(13), THSP2(13), ZHSP1(13), ZHSP2(13), BETI1, BETI2, BETD1, BLADE 20
2 BETO2, CHORD, RI, RO, STGR
COMMON /INPUTA/ XXMSP(50,2),XXTHSP(50,2)
DIMENSION FSB(13)
DATA FSB/.0,.05,.12,.2,.3,.4,.5,.6,.7,.8,.88,.95,1.0/
IR = 5
IW = 6
PI = 3.1415927
RADIAN = 57.29578
IF(IPLOTB.NE.0)
*WRITE (IW,2000) NB, R, ALP, SOLID, KICR, KOCR, T, ZM, P, THX,
X THLE, THTE
C *** INPUT OPTIONS ARE IP = 1 OR 3 FOR PUNCH AND IP.GT.1 FOR PLOT
THMAX = TMX/2.0
KIC = KICR/RADIAN
KOC = KOCR/RADIAN
TALP = TAN(CALP/RADIAN)
SALP = TALP/SQRT(1.0 + TALP**2)
CALP = SQRT(1.0 - SALP**2)
BLADES = NB
GBL = (KIC + KOC)/2.0
SGAM = SIN(GBL)
CGAM = SORT(1.0 - SGAM**2)
CCC = 1.0 - THLE - THTE
C1 = T - THLE
C2 = 1.0 - T - THTE
THD = THLE - THTE
TEPE = THD/CCC
CEPE = 1.0/SQRT(1.0 + TEPE**2)
SEPE = TEPE*CEPE
CALL COHIC(CHD)
C *** BLADE ELEMENT SUCTION SURFACE Z AND THETA ARRAYS REFERENCED
C *** TO THE LOWEST Z POINT OF THE LEADING EDGE CIRCLE.
ZTRS = (DRCTSI + THLE)*CHD
RTC = RIC + (DRCTSI + THLE)*SALP
PISTUG55
PISTUG56
PISTUG57
PISTUG58
PISTUG59
PISTUG60
PISTUG61
BLADE 2
BLADE 3
BLADE 4
BLADE 5
BLADE 6
BLADE 7
BLADE 8
BLADE 9
BLADE 10
BLADE 11
BLADE 12
BLADE 13
BLADE 14
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BLADE 49
BLADE 50
BLADE 51
BLADE 52
BLADE 53
BLADE 54

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TTRS = RETS/RTC
FST = DSS1/(DSS1 + DSS2)
DO 50 K=1,13
FS = FSB(K) - FST
IF (FS.GT.0.0) GO TO 20
DSS = DSS1*FS/FST
DK = (KTS - KIS)*DSS/DSS1
GO TO 30
20 DSS = DSS2*FS/(1.0 - FST)
DK = (KOS - KTS)*DSS/DSS2
30 CALL EPSLON(KTS,DK,RCTS,DSS,DRCTS,RES)
ZMSP1(K) = ZTRS + DRCTS*CHD
50 THSP1(K) = TTRS + RES/(RTC + DRCTS*SALP)
C *** BLADE ELEMENT PRESSURE SURFACE Z AND THETA ARRAYS REFERENCED
C *** TO THE LOWEST Z POINT OF THE LEADING EDGE CIRCLE.
ZTRP = (DRCTPI + THLE)*CHD
RTC = RIC + (DRCTPI + THLE)*SALP
TTRP = RETP/RTC
FST = DSP1/DSP
DO 100 K=1,13
FS = FSB(K) - FST
IF (FS.GT.0.0) GO TO 70
DSS = DSP1*FS/FST
DK = (KTP - KIP)*DSS/DSP1
GO TO 80
70 DSS = DSP2*FS/(1.0 - FST)
DK = (KOP - KTP)*DSS/DSP2
80 CALL EPSLON(KTP,DK,RCTP,DSS,DRCTS,RES)
ZMSP2(K) = ZTRP + DRCTS*CHD
100 THSP2(K) = TTRP + RES/(RTC + DRCTS*SALP)
CHORD = (DRCOI + THLE + THTE)*CHD
RI = THLE*CHD
RO = THTE*CHD
BETI1 = KIS*RADIAN
BETO1 = KOS*RADIAN
BETI2 = KIP*RADIAN
BETO2 = KOP*RADIAN
GBL=RADIAN*ASIN(SGAM)
IF (IPLOTB.NE.0)
*WRITE (IW,2100) CHD, GBL
RTE = RIC + DRCOI*SALP
RM = RIC + (DRCTI + DRCHT)*SALP
REOI = REOI/RTE
STGR = REOI
RETI = RETI/(RIC + DRCTI*SALP)
REMT = RETI + REMT/RM
RELES = RELES/(RIC + DRCLCS*SALP)
RETES = REOI + RETES/(RTE + DRCTES*SALP)
RELEP = RELEP/(RIC + DRCLEP*SALP)
RETEP = REOI + RETEP/(RTE + DRCTEP*SALP)
REMS = REMT + REMS/(RIC + (DRCTSI - DRCTMS)*SALP)
REM = REMT + REM/(RIC + (DRCTPI - DRCTMP)*SALP)
RETHS = REMS + REHS/(RIC + DRCTSI*SALP)
RETHP = REM + REHP/(RIC + DRCTPI*SALP)
DRCHT = (DRCTI + DRCHT)*CHD
DRCTMS = (DRCTSI - DRCTMS)*CHD
DRCTMP = (DRCTPI - DRCTMP)*CHD
DRCTSI = DRCTSI*CHD
DRCTPI = DRCTPI*CHD
DRCTI = DRCTI*CHD
BLADE 55
BLADE 56
BLADE 57
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BLADE 64
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BLADE 66
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BLADE114
DRCTES = (DRCTES + DRCOI)*CHD
DRCTEP = (DRCTEP + DRCOI)*CHD
DRCOI = DRCOI*CHD
DRCLCS = DRCLCS*CHD
DRCLEP = DRCLEP*CHD
REF = 0.0
KTC = KTC*RADIAN
KTS = KTS*RADIAN
KTP = KTP*RADIAN
KM = KM*RADIAN
DSTI = DSTI*CHD
DSOT = DSOT*CHD
DSS1 = DSS1*CHD
DSS2 = DSS2*CHD
DSP1 = DSP1*CHD
DSP2 = DSP2*CHD
IF (IPLOTB.EQ.0) GO TO 110
WRITE (IW,2120) DRCLCS, DRCTES, DRCTSI, DRCTMS, RELES, RETES,
X REHMS, REMS, BETI1, BETO1, KTS, KM, DSS1, DSS2
WRITE (IW,2110) REF, DRCOI, DRCTI, DRCHT, REF, REOI, RETI, REMT,
X KICR, KOGR, KTC, KM, DSTI, DSOT
WRITE (IW,2130) DRCLEP, DRCTEP, DRCTPI, DRCTMP, RELEP, RETEP,
X REHMP, REM, BETI2, BETO2, KTP, KM, DSP1, DSP2
110 CONTINUE
RSALP = RADIAN*SALP
RELES = RSALP*RELES
RETES = RSALP*RETES
REHMS = RSALP*REHMS
REMS = RSALP*REMS
REOI = RSALP*REOI
RETI = RSALP*RETI
REMT = RSALP*REMT
RELEP = RSALP*RELEP
RETEP = RSALP*RETEP
REHMP = RSALP*REHMP
REM = RSALP*REM
BETI1 = BETI1 + RELES
BETO1 = BETO1 + RETES
KTS = KTS + REHMS
BMS = KM + REMS
KOCR = KOGR + REOI
KTC = KTC + RETI
KM = KM + REMT
BETI2 = BETI2 + RELEP
BETO2 = BETO2 + RETEP
KTP = KTP + REHMP
BMP = KM + REM
IF (IPLOTB.EQ.0) GO TO 125
WRITE (IW,2135)
WRITE (IW,2136) RELES, RETES, REHMS, REMS, BETI1, BETO1, KTS, BMS
WRITE (IW,2137) REF, REOI, RETI, REMT, KICR, KOGR, KTC, KM
WRITE (IW,2138) RELEP, RETEP, REHMP, REM, BETI2, BETO2, RTP, BMP
WRITE (IW,2140) CHORD, STGR, RI, RO, BETI1, BETO1, RI, RO, BETI2,
X BETO2
DO 120 K=1,13
120 WRITE (IW,2150) ZMSP1(K), THSP1(K), ZMSP2(K), THSP2(K)
WRITE (IW,2160)
125 CONTINUE
C *** ASSIGN VALUES TO BE PASSED TO TSONIC AND OPTIMIZATION PROGRAM
*CHORD(1)=CHORD
BLADE115
BLADE116
BLADE117
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BLADE120
BLADE121
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BLADE173
BLADE174

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XSTGR(1)=STGR
XRI(1)=RI
XRO(1)=RO
XBETI(1)=BETI1
XBETO(1)=BETO1
DO 130 K=1,13
  XMSP(K,1)=ZMSP1(K)
  XXHSP(K,1)=ZHSP1(K)
  XXTHSP(K,1)=THSP1(K)
130 XTHSP(K,1)=THSP1(K)
  XRI(2)=RI
  XRO(2)=RO
  XBETI(2)=BETI2
  XBETO(2)=BETO2
  DO 140 K=1,13
    XMSP(K,2)=ZMSP2(K)
    XXHSP(K,2)=ZHSP2(K)
    XXTHSP(K,2)=THSP2(K)
140 XTHSP(K,2)=THSP2(K)
  IF (IPLOTB.EQ.1) CALL EPLOTT
  RETURN
2000 FORMAT (1H1 // 46X,39H*** INPUT FOR BLADE ELEMENT PROGRAM *** //BLADE196
1 / 49X,5HINLET,4X,6HOUTLET,4X,6HTRANS.,4X,7HMAX.TH.,3X,6HIN/OUT,5X,BLADE197
2 4HMAX.,6X,4HL.E.,6X,4HT.E. / 10X,3HND.,6X,5HINLET,5X,4HCONE,4X, BLADE198
3 8HSOLIDITY,4X,5HBLADE,5X,5HBLADE,5X,4HLOC.,6X,4HLOC.,5X,7HTURNINGBLADE199
4 3X,6HTHICK.,5X,4HRAD.,6X,4HRAD. / 8X,6HBLADES,4X,6HRADIUS,5X, BLADE200
5 5HANGLE,15X,5HANGLE,5X,5HANGLE,4X,6H/CHORD,4X,6H/CHORD,5X,4HRATE,BLADE201
6 5X,6H/CHORD,4X,6H/CHORD,4X,6H/CHORD / 20X,3H(L),6X,5H(DEG),15X, BLADE202
7 5H(DEG),5X,5H(DEG) // 9X,I3,3X,3F10.5,F9.3,F10.4,6F10.5) BLADE203
2100 FORMAT (////// 45X,41H*** OUTPUT FROM BLADE ELEMENT PROGRAM *** BLADE204
1 // 69X,7HELEMENT / 69X,7HSETTING / 58X,5HCHORD,7X,5HANGLE / 59X, BLADE205
2 3H(L),8X,5H(DEG) // 52X,F12.5,F12.4 // 10X,32H MERID. LOC. FROMBLADE206
3 L.E. CENT. **,2X,32H THETA LOC. FROM L.E. CENT. **,2X,9(1H), BLADE207
4 14H BLADE ANGLES ,9(1H),3X,15HSEGMENT LENGTHS / 10X,8(4H****), BLADE208
5 2X,8(4H****),2X,33H(WITH RESPECT TO LOCAL CONIC RAY),2X,5(3H****) BLADE209
6 // 8X,3(4X,5HINLET,2X,6HOUTLET,2X,6HTRANS.,2X,7HMAX.TH.),4X, BLADE210
7 5HFIRST,2X,6HSECOND / 8X,4(5X,3H(L)),3X,4(3X,5H(RAD)),2X,4(3X, BLADE211
8 5H(DEG)),1X,2(5X,3H(L)) / ) BLADE212
2110 FORMAT (3X,5HCENT.,1X,4F8.5,2X,4F8.5,2X,4F8.3,3X,2F8.5 / ) BLADE213
2120 FORMAT (3X,5HSUCT.,1X,4F8.5,2X,4F8.5,2X,4F8.3,3X,2F8.5 / ) BLADE214
2130 FORMAT (3X,5HPRES.,1X,4F8.5,2X,4F8.5,2X,4F8.3,3X,2F8.5 / ) BLADE215
2135 FORMAT ( / 44X,32H*** CONIC ANGLE COORD. - C ****,2X,9(1H), BLADE216
1 14H BLADE ANGLES ,9(1H) / 1H+,69X,1H- / 44X,32H** (FROM LEADINGBLADE217
2 EDGE CENT.) ****,2X,32H(WITH RESPECT TO L.E. CENT. RAY) / 42X, BLADE218
3 2(4X,5HINLET,2X,6HOUTLET,2X,6HTRANS.,2X,7HMAX.TH.) / 43X, BLADE219
4 4(3X,5H(DEG)),2X,4(3X,5H(DEG)) / ) BLADE220
2136 FORMAT (37X,5HSUCT.,1X,4F8.3,2X,4F8.3 / ) BLADE221
2137 FORMAT (37X,5HCENT.,1X,4F8.3,2X,4F8.3 / ) BLADE222
2138 FORMAT (37X,5HPRES.,1X,4F8.3,2X,4F8.3 / ) BLADE223
2140 FORMAT (1H1 // 41X,51H*** OUTPUT THAT CAN BE PUNCHED FOR TSONICBLADE224
1 INPUT *** // 51X,10(3H****)/51X,1H*,28X,1H*/ 51X,1H*,6X,5HCHORD, BLADE225
2 6X,4HSTGR,7X,1H* / 51X,1H*,7X,3H(L),7X,5H(RAD),6X,1H* / 51X,1H*, BLADE226
3 28X,1H* / 51X,1H*,2X,F10.5,F11.6,5X,1H* / 51X,1H*,28X,1H* / 15X, BLADE227
4 103(1H*) / 15X,1H*,2(50X,1H*) / 15X,1H*,14X,23H*** SUCTION SURFACEBLADE228
5 **,13X,1H*,13X,24H*** PRESSURE SURFACE **,13X,1H* / 15X,1H*,2( BLADE229
6 50X,1H*) / 15X,1H*,8X,34(1H*),8X,1H*,8X,34(1H*),8X,1H* / 15X,1H*,BLADE230
7 2(50X,1H*) / 15X,2(1H*,8X,2HRI,9X,2HRO,8X,4HBETI,7X,4HDETO,6X), BLADE231
8 1H* / 15X,2(1H*,7X,3H(L),8X,3H(L),7X,5H(DEG),6X,5H(DEG),6X),1H* /BLADE232
9 15X,1H*,2(50X,1H*) / 15X,1H*,2(1X,2F11.5,2F11.4,5X,1H*) / 15X,1H*,BLADE233
.,2(50X,1H*) / 15X,1H*,2(50X,1H*) / 15X,1H*,2(15X,4HZMSP,12X,4HTHSP)BLADE234
BLADE175 1,15X,1H*) / 15X,1H*,2(16X,3H(L),12X,5H(RAD),14X,1H*) / 15X,1H*, BLADE235
BLADE176 2 2(50X,1H*) ) BLADE236
BLADE177 2150 FORMAT (15X,1H*,2(9X,F11.5,6X,F11.6,13X,1H*) ) BLADE237
BLADE178 2160 FORMAT (15X,1H*,2(50X,1H*)/ 15X,103(1H*) ) BLADE238
BLADE179 END BLADE239
BLADE180 SUBROUTINE CONIC(CHORD) CONIC 2
BLADE181 C *** THIS IS THE MAIN BLADE ELEMENT LAYOUT ROUTINE. BLADE ELEMENTS CONIC 3
BLADE182 C *** ARE LAID OUT ON A CONE SUCH THAT THE CIRCULAR ARC CHARACTERISTIC CONIC 4
BLADE183 C *** OF CONSTANT RATE OF ANGLE CHANGE WITH PATH DISTANCE IS MAINTAINED. CONIC 5
BLADE184 REAL KIC, KIP, KIS, KM, KOC, KOP, KOS, KTC, KTP, KTS CONIC 6
BLADE185 COMMON /SCALR/ CONIC 7
BLADE186 1 BLADES, CALP, CCC, CEPE, CKTC, CRKTS, C1, C2, DRCE, DRCLEP, DRCLSCONIC 8
BLADE187 2, DRCHST, DRCHT, DRCOI, DRCS, DRCT, DRCTEP, DRCTES, DRCTI, DRCTMP, CONIC 9
BLADE188 3 DRCTHS, DRCTPI, DRCTSI, DSME, DSMT, DSOT, DSP, DSP1, DSP2, DSSE, CONIC 10
BLADE189 4 DSS1, DSS2, DST, DSTI, EMT, IR, IM, KIC, KIP, KIS, KM, KOC, KOP, CONIC 11
BLADE190 5 KOS, KTC, KTP, KTS, RCI, RCHS, RCO, RCT, RCTP, RCTS, REC, CONIC 12
BLADE191 6 RELEP, RELES, REM, REHS, REMT, REOI, RES, RET, RETEP, RETES, RETICONIC 13
BLADE192 7, RETHP, REHS, RETP, RETS, RIC, SGAM, SALP, SKTC, SKTS, TEPE, CONIC 14
BLADE193 8 THMAX, TKTN CONIC 15
BLADE194 COMMON /INPUTB/ CONIC 16
BLADE195 1 ALP, KICR, KOCR, NB, P, R, SOLID, T, THLE, THTE, THX, ZM CONIC 17
C *** ESTABLISH BLADE ELEMENT CENTERLINE TO SATISFY CAMBER, CHORD CONIC 18
C *** AND TRANSITION POINT REQUIREMENTS. CONIC 19
PI2 = PI/2.0
CGAM = SQRT(1.0 - SGAM**2)
ICONV = 0
DKAPPA = KIC - KOC
ICL = 1
DK2 = DKAPPA/(1.0 + P*CI/CC2)
10 CHORD = 2.0*PI*RM*SOLID/(BLADES - PI*SOLID*CGAM*SALP)
RIC = R/CHORD
CCHORD = CALP*CHORD
IF (ICL.GT.1) GO TO 15
EPS = CCC*SGAM*SALP/(RIC + (THLE + CCC*CGAM)*SALP)
DPHI = DKAPPA - EPS
DPHI4 = DPHI/4.0
DPHIHS = DPHI*DPHI4
DSOI = CCC/(1.0 - DPHIHS/6.0*(1.0 - DPHIHS/20.0))
DSTI = CI/CCC*DSOI
DSOT = DSOI - DSTI
15 IF (ABS(SALP/RIC).LT.1.0E-08) GO TO 20
RCI = RIC/SALP + THLE
GO TO 30
20 RCI = 1.0E+08
30 DK1 = DKAPPA - DK2
CALL EPSLON(KIC,-DK1,RCI,DSTI, DRCTI, RETI)
KTC = KIC - DK1
RCT = RCI + DRCTI
35 CALL EPSLON(KTC,-DK2,RCT,DSOT,DRCOT,REOT)
RCO = RCT + DRCOT
REOI = RCO/RCT*RETI + REOT
DRCOI = DRCTI + DRCOT
CALL TANCAP(RCI,DRCOI,REOI,TANCCO)
TGBL = (TANCCO + TEPE)/(1.0 - TANCCO*TEPE)
CALL RPOINT(RCI,DRCTI,RETI,TGBL,DRCTP)
SECGDL = SQRT(1.0 + TGBL**2)
DC1 = DRCTP*SECGDL - CI
DC2 = DRCOI*SQRT(1.0 + TANCCO**2)*CEPE - CCC
IF (ICL.GT.1.AND.ABS(TGBL - TGBLL).LT.1.0E-04) GO TO 37
ICL = 2
CONIC 56

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TGBLL = TGBL
CGAM = 1.0/SQRT(1.0 + TGBL**2)
GO TO 38
37 ICONV = 1
38 IF (ABS(DC1).LT.1.0E-04) GO TO 40
DS1= DSTI*DC1/(C1 + DC1)
DSTI= DSTI - DS1
DSOT= DSOT - DSOI*DC2/(CCC + DC2) + DS1
DSOI = DSTI + DSOT
DK2 = DKAPPA/(1.0 + P*DSTI/DSOT)
IF (ICONV.LT.1) GO TO 10
GO TO 30
40 IF (ABS(DC2).LT.1.0E-05) GO TO 50
DSOT= DSOT - DSOI*DC2/(CCC + DC2)
DSOI = DSTI + DSOT
IF (ICONV.LT.1) GO TO 10
GO TO 35
C *** CONIC COORDINATES OF THE MAXIMUM THICKNESS POINT
50 SGAM=TGBL*CGAM
ZHT = ZH - T
IF (ABS(ZHT).GT.1.0E-07) GO TO 120
DRCHT= 0.0
REMT= 0.0
DK= 0.0
DSMT = 0.0
DSME= DSTI
DRCTMS = 0.0
RETHS = 0.0
DRCTHP = 0.0
RETHP = 0.0
GO TO 150
120 HKTC= KTC/2.0
SHKTC= HKTC*SR5(HKTC)
SHKTCQ= SHKTC**2
SKTC= 2.0*SHKTC*SQRT(1.0 - SHKTCQ)
IF (ABS(SKTC).LT.1.0E-07) SKTC = 1.0E-07
CKTC= 1.0 - 2.0*SHKTCQ
TKTH= -CKTC/SKTC
IF (ZHT.GT.0.0) GO TO 130
DSMT= DSTI*ZHT/C1
DKDS= DK1/DSOI
DSME= DSTI
GO TO 140
130 DSMT= DSOT*ZHT/C2
DKDS = DK2/DSOT
DSME= -DSOT
140 DK= -DSMT*DKDS
CALL EPSLON(KTC,DK,RCT,DSMT,DRCHT,REMT)
CALL RPOINT(RCT,DRCHT,REMT,TGBL,DRCMP)
ZHTCAL= DRCMP*SECGDL
IF (ABS(ZHTCAL - ZHT).LT.1.5E-05) GO TO 150
DSMT = DSMT*ZHT/ZHTCAL
GO TO 140
150 RCH= RCT + DRCHT
KH= KTC + DK
HKM= KH/2.0
SHKM= HKM*SR5(HKM)
SHKMQ= SHKM**2
CHKM= SQRT(1.0 - SHKMQ)
SKM= 2.0*SHKM*CIHKM
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CONIC113
CONIC114
CONIC115
CONIC116
CKM= 1.0 - 2.0*SHKMQ
DSME= DSME + DSMT
C *** DEFINITION OF SUCTION SURFACE MAX. THICKNESS POINT
CALL EPSLON(KH*PI2,0.0,RCH,THMAX,DRCH,REH)
REMS = REH
RCHS= RCH + DRCH
IF (ZHT.GT.1.0E-07) GO TO 180
REMI = (1.0 + DRCHT/RCT)*RETI + REMT
C *** DEFINITION OF SUCTION SURFACE CURVE FOR MAXIMUM THICKNESS
C *** POINT ON OR AHEAD OF THE TRANSITION POINT
DK= 2.0*(THMAX - THLE)/DSME
KIS = KIC + DK
KIP = KIC - DK
DRCIH= -DRCTI - DRCHT - DRCH
EMSI= REMI/RCH + REMT/RCHS
CALL SURF(KIS,KH,SKH,CKM,RCI,DRCIH,THLE,EMSI,DSSE)
DRCLIS = DRCE
RELES = REE
IF (ABS(ZHT).LT.1.0E-07) GO TO 160
DRCHST= DRCHT + DRCH
EMT= REM/RCHS + REMT/RCH
CALL TRAH(KIS,THLE,THMAX,KTS,RCTS,RETS,DSS1)
DRCTMS = DRCS
RETHS = RES
DHKT= (KTC - KTS)/2.0
DK= 2.0*(DST - THTE - DSOT*DHKT)/(DSOT + (DST - THTE)*DHKT)
DRCOTS= DRCOT - DRCT
EMSO= RET/RCTS - REOT/RCO
DRCTSI = DRCTI + DRCT
GO TO 170
160 RCTS= RCHS
KTS= KH
RETS = RCHS*EMSI
DSS1 = -DSSE
SKTS= SKH
CKTS= CKM
DK= 2.0*(THMAX - THTE)/DSOT
DRCOTS= DRCOT - DRCH
EMSO= REM/RCHS - REOT/RCO
DRCTSI = DRCTI + DRCH
170 KOS = KOC - DK
KOP = KOC + DK
CALL SURF(KOS,KTS,SKTS,CKTS,RCO,DRCOTS,THTE,EMSO,DSS2)
DRCTES = DRCE
RETES = REE
GO TO 190
C *** DEFINITION OF SUCTION SURFACE CURVE FOR MAXIMUM THICKNESS
C *** POINT BEHIND THE TRANSITION POINT
180 DK= 2.0*(THMAX - THTE)/DSME
KOS = KOC + DK
KOP = KOC - DK
DRCOM= DRCOT - DRCHT - DRCH
EMSO= REMT/RCH - REOT/RCO + REM/RCHS
CALL SURF(KOS,KH,SKH,CKM,RCO,DRCOM,THTE,EMSO,DSSE)
DRCTES = DRCE
RETES = REE
DRCHST= DRCHT + DRCH
EMT= REM/RCHS + REMT/RCH
CALL TRAH(KOS,THTE,THMAX,KTS,RCTS,RETS,DSS2)
DRCTMS = DRCS
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RETHS = RES
DHKT= (KTS- KTC)/2.0
DK= 2.0*(DST - THLE - DSTI)*DHKT/(DSTI + (DST - THLE)*DHKT)
KIS = KIC + DK
KIP = KIC - DK
DPCTSI = DRCTI + DRCT
EMSI = RETI/RCT + RET/RCTS
CALL SURF(KIS,KTS,SKTS,CKTS,RCI,-DRCTSI,THLE,EMSI,DSSE)
DRCLE = DRCE
RELES = REE
DSSI = -DSSE
C *** DEFINITION OF PRESSURE SURFACE MAXIMUM THICKNESS POINT
190 CALL EPSLON(KH*PI2,0.0,RCH,-THMAX,DRCH,REM)
RCHS= RCH + DRCH
IF (ZHT.GT.1.0E-07) GO TO 220
C *** DEFINITION OF PRESSURE SURFACE CURVE FOR MAXIMUM THICKNESS
C *** POINT ON OR AHEAD OF THE TRANSITION POINT
DRCIM= -DRCTI - DRCHT - DRCH
EMSI = REMI/RCH + REM/RCHS
CALL SURF(KIP,KH,SKH,CKH,RCI,DRCIM,-THLE,EMSI,DSSE)
DRCLEP = DRCE
RELEP = REE
IF (ABS(ZHT).LT.1.0E-07) GO TO 200
DRCHST= DRCHT + DRCH
EMT = REM/RCHS + REMT/RCH
CALL TRAN(KIP,-THLE,-THMAX,KTP,RCTP,RETP,DSPI)
DRCTMP = DRCS
RETMP = RES
DRCOTS= DRCOT - DRCT
EMSO = RET/RCTP - REOT/RCO
DRCTPI = DRCTI + DRCT
GO TO 210
200 RCTP = RCHS
KTP= KH
RETP= RCHS * EMSI
DSP1 = -DSSE
DRCOTS= DRCOT - DRCH
EMSO = REM/RCHS - REOT/RCO
DRCTPI = DRCTI + DRCH
210 CALL SURF(KOP,KTP,SKTS,CKTS,RCO,DRCOTS,-THTE,EMSO,DSP2)
DRCTEP = DRCE
RETEP = REE
GO TO 230
C *** DEFINITION OF PRESSURE SURFACE CURVE FOR THE MAXIMUM
C *** THICKNESS POINT BEHIND THE TRANSITION POINT
220 DRCOM= DRCOT - DRCHT - DRCH
EMSO = REMT/RCH - REOT/RCO + REM/RCHS
CALL SURF(KOP,KH,SKH,CKH,RCO,DRCOM,-THTE,EMSO,DSSE)
DRCTEP = DRCE
RETEP = REE
DRCHST= DRCHT + DRCH
EMT = REM/RCHS + REMT/RCH
CALL TRAN(KOP,-THTE,-THMAX,KTP,RCTP,RETP,DSP2)
DRCTMP = DRCS
RETMP = RES
DPCTPI = DRCTI + DRCT
EMSI = RETI/RCT + RET/RCTS
CALL SURF(KIP,KTP,SKTS,CKTS,RCI,-DRCTPI,-THLE,EMSI,DSSE)
DRCLEP = DRCE
RELEP = REE

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DSP1 = -DSSE
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EPL0T 43
EPL0T 44
EPL0T 45
EPL0T 46
EPL0T 47

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900 FORMAT (IH1//40X,
154H*** PLOT OF BLADE SURFACE IN THETA - M COORDINATES ***////)
1000 FORMAT (1H )
1010 FORMAT (1H+,132A1)
      END
      SUBROUTINE EPSLON(KO,DK,RO,DS,DR,RE)
C *** CALCULATION OF CONIC RADIAL AND CIRCUMFERENTIAL COMPONENTS OF
C *** A BLADE ELEMENT SEGMENT WITH GIVEN PATH DISTANCE AND END ANGLES
      REAL KO
      * IF (ABS(DS).LT.1.0E-08) GO TO 70
      HDK = DK/2.0
      IF (ABS(HDK).GT.0.78539816) GO TO 2
      SR = SRS(HDK)
      SHDK = HDK*SR
      SHDKQ = SHDK**2
      CHDK = SQRT(1.0 - SHDKQ)
      GO TO 6
2 IF (HDK.LT.0.0) GO TO 3
      HDK = 1.5707963 - HDK
      CHDK = HDK*SR*(HDK)
      SHDKQ = 1.0 - CHDK**2
      SHDK = SQRT(SHDKQ)
      GO TO 4
3 HDK = 1.5707963 + HDK
      CHDK = HDK*SR*(HDK)
      SHDKQ = 1.0 - CHDK**2
      SHDK = -SQRT(SHDKQ)
4 SR = ABS(SHDK)/HDK
6 HKO = KO/2.0
      IF (HKO.GT.0.78539816) GO TO 7
      SHKO = HKO*SR*(HKO)
      SHKOQ = SHKO**2
      CHKO = SQRT(1.0 - SHKOQ)
      SKO = 2.0*SHKO*CHKO
      CKO = 1.0 - 2.0*SHKOQ
      GO TO 8
7 HKO = 0.78539816 - HKO
      SHKO = HKO*SR*(HKO)
      SHKOQ = SHKO**2
      CHKO = SQRT(1.0 - SHKOQ)
      SKO = 1.0 - 2.0*SHKOQ
      CKO = 2.0*SHKO*CHKO
8 SKA = SHDK*CKO + SKO*CHDK
      CKA = CHDK*CKO - SKO*SHDK
C *** CONIC RADIAL COMPONENT OF THE PATH
      DR = DS*CKA*SR
      IF (ABS(DK).GT.0.00001) GO TO 10
      DRR = DR/RO
      IF (ABS(DRR).LT.0.01) GO TO 9
C *** CIRCUMFERENTIAL COMP. WHEN PATH ANGLE IS ESSENTIALLY CONSTANT
      RE = (RO + DR)*SKA/CKA*ALOG(1.0 + DRR)
      RETURN
9 RE = (1.0 * DRR)*DS*SR*SKA*(1.0 - DRR*(0.5 - DRR*(0.33333333 - DRRE
X /4.0)))
      RETURN
10 RS = RO/DS
      IF (ABS(RS).GT.10000.0) GO TO 60
      IF (RS**2/ABS(DK).GT.1.7E+09) GO TO 60
C *** CONIC CIRCUMFERENTIAL COMPONENT OF PATH BY GENERAL EQUATION
      RCK = RS*DK - SKO
      EPLOT 48
      EPLOT 49
      EPLOT 50
      EPLOT 51
      EPLOT 52
      EPLOT 52
      EPLOT 2
      EPLOT 4
      EPLOT 5
      EPLOT 6
      EPLOT 7
      EPLOT 8
      EPLOT 9
      EPLOT 10
      EPLOT 11
      EPLOT 12
      EPLOT 13
      EPLOT 14
      EPLOT 15
      EPLOT 16
      EPLOT 17
      EPLOT 18
      EPLOT 19
      EPLOT 20
      EPLOT 21
      EPLOT 22
      EPLOT 23
      EPLOT 24
      EPLOT 25
      EPLOT 26
      EPLOT 27
      EPLOT 28
      EPLOT 29
      EPLOT 30
      EPLOT 31
      EPLOT 32
      EPLOT 33
      EPLOT 34
      EPLOT 35
      EPLOT 36
      EPLOT 37
      EPLOT 38
      EPLOT 39
      EPLOT 40
      EPLOT 41
      EPLOT 42
      EPLOT 43
      EPLOT 44
      EPLOT 45
      EPLOT 46
      EPLOT 47
      EPLOT 48
      EPLOT 49
      EPLOT 50
      EPLOT 51
      EPLOT 52
      EPLOT 53
      EPLOT 54
      EPLOT 55
      EPLOT 56
      QDKS = HDK**2/4.0
      SES = 0.66666667*RCK*QDKS*(1.0 - 0.6*QDKS*(1.0 - 0.15873016*QDKS*
X (1.0 - 0.077777778*QDKS*(1.0 - 0.046753247*QDKS*(1.0 - .031339031
X *QDKS))))))
      DRR = DR/RO
      IF (ABS(DRR).GT.0.21) GO TO 20
      RRM = 0.5*DRR*(1.0 - 0.25*DRR*(1.0 - 0.5*DRR*(1.0 - 0.625*DRR*(1.0
X - 0.7*DRR*(1.0 - 0.75*DRR*(1.0 - 0.78571429*DRR*(1.0 - 0.8125*DRR
X *(1.0 - 0.83333333*DRR))))))
      RRQ = RRM + 1.0
      GO TO 30
20 RRQ = SQRT(1.0 + DRR)
      RRM = RRQ - 1.0
30 RM = RRQ*RS
      D = RCK*CHDK + SKA + DK*RM
      XS = SHDKQ*(1.0 - RCK**2)/D**2
      XSN = 35.0*ABS(XS)
      HXS = XSN
      N = 5 + HXS
      SXS = 0.0
      XPS = 1.0
      DKN = 1.0
      DO 40 KN=1,N
      IF (ABS(XPS).LT.1.0E-12.AND.KN.NE.1) GO TO 50
      XPS = XPS*XSN
      DKN = DKN + 2.0
40 SXS = SXS + XPS/DKN
50 RE = (RO + DR)*(DK*(SKO + SKA + DK*RS*RRM - SES) - 4.0*RCK*SHDK*
X SXS)/D
      RETURN
C *** CONIC CIRCUMFERENTIAL COMPONENT WHEN PATH DISTANCE IS A VERY
C *** SMALL FRACTION OF THE DISTANCE TO THE CONE VERTEX.
60 DRR = DR/RO
      RE = (1.0 + DRR)/(1.0 * 0.5*DRR*(1.0 - 0.25*DRR*(1.0 - 0.5*DRR*
X (1.0 - 0.625*DRR)))))*DS*SKA*SR
      RETURN
70 DR = 0.0
      RE = 0.0
      RETURN
      END
      SUBROUTINE RPOINT(RO,DR,RE,TK,DRP)
C *** THIS SUBROUTINE CALCULATES THE CONIC RADIAL COORDINATE AT THE POINT 3
C *** INTERSECTION OF PERPENDICULAR CONSTANT ANGLE LINES FROM TWO KNOWN
C *** POINTS ON A CONE. THE LINE THROUGH THE REFERENCE POINT HAS THE
C *** INPUT SLOPE TK.
      R = DR/RO
      CK = SQRT(1.0/(1.0 + TK**2))
      SK = TK*CK
      IF (ABS(R).LT.0.01) GO TO 20
      DRP = ROM*(EXP((RE*SK/(RO + DR) + ALOG(1.0 + R)*CK)*CK) - 1.0)
      RETURN
20 C = (RE*SK/(RO + DR) + R*(1.0 - 0.5*R*(1.0 - 0.66666667*R*(1.0 -
X 0.75*R)))*CK)*CK
      DRP = C
30 CS = DRP*(1.0 - 0.5*DRP*(1.0 - 0.66666667*DRP*(1.0 - 0.75*DRP)))
      IF (ABS((CS - C)/C).LT.1.0E-06) GO TO 40
      DRP = DRP*C/CS
      GO TO 30
40 DRP = DRP*RO
      RETURN
      RPOINT2
      RPOINT3
      RPOINT4
      RPOINT5
      RPOINT6
      RPOINT7
      RPOINT8
      RPOINT9
      RPOINT10
      RPOINT11
      RPOINT12
      RPOINT13
      RPOINT14
      RPOINT15
      RPOINT16
      RPOINT17
      RPOINT18
      RPOINT19
      RPOINT20
      RPOINT21

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      END                                RPOINT22
      FUNCTION SRS(ANG)                  SRS   2
C ***   SERIES FOR (SIN(ANG))/ANG WHEN THE MAGNITUDE OF ANG IS LESS SRS   3
C ***   THAN PI/4                       SRS   4
      IF (ABS(ANG).LT.1.0E-05) GO TO 10 SRS   5
      AQ = ANG**2                        SRS   6
      SRS = 1.0 - AQ/6.0*(1.0 - AQ/20.0*(1.0 - AQ/42.0*(1.0 - AQ/72.0))) SRS   7
      RETURN                              SRS   8
10 SRS = 1.0                            SRS   9
      RETURN                              SRS  10
      END                                SRS  11
      SUBROUTINE SURF(KE,KMM,SKM,CKM,RO,DR,TE,EMS,DSS) SURF  2
C ***   THIS SUBROUTINE CALCULATES THE BLADE ELEMENT SURFACE CURVE SURF  3
C ***   END POINT COORDINATES. THE SURFACE CURVE IS NORMAL TO THE END SURF  4
C ***   POINT THICKNESS PATH AND TANGENT TO A SURFACE REFERENCE POINT SURF  5
C ***   WHICH IS EITHER THE TRANSITION OR MAXIMUM THICKNESS POINT. SURF  6
      REAL KE,KE1,KIC,KIP,KIS,KM,KMM,KOC,KOP,KOS,KTC,KTP,KTSSURF  7
      COMMON /SCALR/ SURF  8
1 BLADES, CALP, CCC, CEPE, CKTC, CKTS, C1, C2, DRCE, DRCLP, DRCLLESSURF  9
2, DRCHST, DRCHT, DRCOI, DRCS, DRCT, DRCTEP, DRCTES, DRCTI, DRCTMP,SURF 10
3 DRCTMS, DRCTPI, DRCTSI, DSME, DSMT, DSOT, DSP, DSP1, DSP2, DSSE, SURF 11
4 DSS1, DSS2, DST, DSTI, EMT, IR, IW, KIC, KIP, KIS, KM, KOC, KOP, SURF 12
5 KOS, KTC, KTP, KTS, PI, RCI, RCMS, RCO, RCT, RCTP, RCTS, REE, SURF 13
6 RELEP, RELES, REM, REMS, REMT, REOI, RES, RET, RETEP, RETES, RETITRAN 14
7, RETHP, RETHS, RETP, RETS, RIC, SGAM, SALP, SKTC, SKTS, TEPE, SURF 15
8 THMAX, TKTN SURF 16
      RMS = RO - DRC SURF 17
      IT = 1 SURF 18
10 CALL EPSLON(KE + 1.5707963,0.0,RO,TE,DRCE,REE) SURF 19
      DRCS = DRC + DRCE SURF 20
      DK = KE - KMM SURF 21
      HDK = DK/2.0 SURF 22
      SR = SRS(HDK) SURF 23
      SHDK = HDK*SR SURF 24
      CHDK = SQRT(1.0 - SHDK**2) SURF 25
      DSS = DRCS/(SR*(CHDK*CKM - SHDK*SKM)) SURF 26
      CALL EPSLON(KMM,DK,RMS,DSS,DRCS,RES) SURF 27
      DRE = (RO + DRCE)*EMS + RES - REE SURF 28
      IF (ABS(DRE).LT.1.0E-05) RETURN SURF 29
      IF (IT.EQ.2) GO TO 20 SURF 30
      KE1 = KE SURF 31
      DRE1 = DRE SURF 32
      KE = KE - 2.0*DRE*(CKM*(1.0 - 2.0*SHDK**2) - 2.0*SKM*SHDK*CHDK)/DSS SURF 33
      IT = 2 SURF 34
      GO TO 10 SURF 35
20 KE = KE + (KE1 - KE)*DRE/(DRE - DRE1) SURF 36
      GO TO 10 SURF 37
      END SURF 38
      SUBROUTINE TANKAP(RO,DR,RE,TK) TANKAP 2
C ***   CALCULATION OF THE SLOPE OF THE CONSTANT ANGLE PATH BETWEEN TANKAP 3
C ***   TWO POINTS IN CONIC RADIUS AND EPSILON COORDINATES TANKAP 4
      R = DR/RO TANKAP 5
      IF (ABS(R).LT.0.1) GO TO 20 TANKAP 6
      TK = RE/((RO + DR)*ALOG(1.0 + R)) TANKAP 7
      RETURN TANKAP 8
20 SUM = 1.0 TANKAP 9
      IF (ABS(R).GT.1.0E-08) GO TO 25 TANKAP10
      IF (ABS(DR/RE).GT.1.0E-08) GO TO 35 TANKAP11
      TK = 1.0E+08 TANKAP12
      RETURN TANKAP13

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25 PROD = 1.0 TANKAP14
      DN = 8.0/(-ALOG10(ABS(R))) TANKAP15
      NT = DN TANKAP16
      DO 30 I=1,NT TANKAP17
      N = I + 1 TANKAP18
      DN = N TANKAP19
      PROD = -PROD*NR TANKAP20
30 SUM = SUM + PROD/DN TANKAP21
35 TK = RE/((RO + DR)*R*SUM) TANKAP22
      RETURN TANKAP23
      END TANKAP24
      SUBROUTINE TRAN(KE,TE,TH,KT,RT,RE,DS) TRAN 2
C ***   THIS SUBROUTINE CALCULATES THE BLADE ELEMENT SURFACE CURVE TRAN 3
C ***   TRANSITION POINT COORDINATES FROM THE INTERSECTION OF THE TRAN 4
C ***   ESTABLISHED SURFACE CURVE OVER THE MAXIMUM THICKNESS POINT WITH A TRAN 5
C ***   PATH PERPENDICULAR TO THE CENTERLINE AT THE TRANSITION POINT. TRAN 6
      REAL KE,KIC,KIP,KIS,KM,KOC,KOP,KOS,KT,KTC,KTP,KTS TRAN 7
      COMMON /SCALR/ TRAN 8
1 BLADES, CALP, CCC, CEPE, CKTC, CKTS, C1, C2, DRCE, DRCLP, DRCLSTRAN 9
2, DRCHST, DRCHT, DRCOI, DRCS, DRCT, DRCTEP, DRCTES, DRCTI, DRCTMP,TRAN 10
3 DRCTMS, DRCTPI, DRCTSI, DSME, DSMT, DSOT, DSP, DSP1, DSP2, DSSE, TRAN 11
4 DSS1, DSS2, DST, DSTI, EMT, IR, IW, KIC, KIP, KIS, KM, KOC, KOP, TRAN 12
5 KOS, KTC, KTP, KTS, PI, RCI, RCMS, RCO, RCT, RCTP, RCTS, REE, TRAN 13
6 RELEP, RELES, REM, REMS, REMT, REOI, RES, RET, RETEP, RETES, RETITRAN 14
7, RETHP, RETHS, RETP, RETS, RIC, SGAM, SALP, SKTC, SKTS, TEPE, TRAN 15
8 THMAX, TKTN TRAN 16
      DST = TH - (TH - TE)*(DSMT/DSME)**2 TRAN 17
      DSS = DST*(KM - KTC) - DSMT TRAN 18
      CS = (KE - KM)/DSSE TRAN 19
10 DK = CS*DSS TRAN 20
      CALL EPSLON(KM,DK,RCMS,DSS,DRCS,RES) TRAN 21
      DRCT = DRCHST + DRCS TRAN 22
      RT = RCMS + DRCS TRAN 23
      RET = RES + RT*EMT TRAN 24
      CALL TANKAP(RCT,DRCT,RET,TK) TRAN 25
      TKD = (TK - TKTN)/(1.0 + TK*TKTN) TRAN 26
      IF (ABS(DST*TKD).LT.1.0E-05) GO TO 20 TRAN 27
      DST = RET/(CKTC - SKTC*TKD) TRAN 28
      DSS = DSS + DST*TKD*SQRT(1.0 + TKD**2)/(1.0 - (DK + KM - KTC)**2/2.0)TRAN 29
      GO TO 10 TRAN 30
20 KT = KM + DK TRAN 31
      RE = RT*RETI/RCT + RET TRAN 32
      DS = DSS - DSSE TRAN 33
      IF (DSSE.GT.0.0) DS = -DS TRAN 34
      HKTS = KT/2.0 TRAN 35
      SHKTS = HKTS*SRS(HKTS) TRAN 36
      SHKTSQ = SHKTS**2 TRAN 37
      CHKTS = SQRT(1.0 - SHKTSQ) TRAN 38
      SKTS = 2.0*SHKTS*CHKTS TRAN 39
      CKTS = 1.0 - 2.0*SHKTSQ TRAN 40
      RETURN TRAN 41
      END TRAN 42

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FUNCTION YPC(DR,RE,EP)                                YPC 2
C *** Y PLOT COORDINATE FROM R AND EPSILON COORDINATES YPC 3 10
YPC = DR - RE*EP/2.0*(1.0 - EP**2/12.0*(1.0 - EP**2/30.0)) YPC 4 C
RETURN YPC 5
END YPC 6
SUBROUTINE COPE5(IFLAG)                                COPE5 2
C ***** COPE5 ***** COPE5 3 C
C COPE5 - CONTROL PROGRAM FOR ENGINEERING SYNTHESIS. COPE5 4 C
C ***** EXECUTION ***** COPE5 5 C
COMMON /CHMNI/ DELFUN,DABFUN,FOCH,FDCHM,CT,CTHIN,CTL,CTLMIN,ALPHAXCOPE5 6
1,ABOBJ1,THETA,OBJ,HDV,NCON,NSIDE,IPRINT,NFDG,NSCAL,LINDBJ,ITMAX,ITCOPE5 7
2RM,ICNDIR,IGOTO,NAC,INFO,INFOG,ITER COPE5 8
COMMON /COPE51/ TITLE(20) COPE5 9
COMMON /COPE52/ RA(5000),IA(1000) COPE5 10 C
COMMON /COPE53/ SGNOPT,NCALC,IOBJ,NSV,NSOBJ,NCONA,N2VX,M2VX,N2VY,MCOPE5 11 C
12VY,N2VAR,IPSENS,IP2VAR,IPDBG,NACMX1,NDVTOT,LOCR(25),LOCI(25),ISRCCOPE5 12 C
21,ISCR2,NXAPRX,NPS,NPFS,NPA,NF,INOM,IPAPRX,KMIN,KMAX,XFACT1,XFACT2COPE5 13 C
3,NAN2,NAN3,NPMAX,NPTOT,JNOM,MAXTRM COPE5 14
COMMON /GLOBCH/ ARRAY(1500) COPE5 15
C BY G. N. VANDERPLAATS OCT., 1974. COPE5 16 C
NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COPE5 17
C NCALC OPTIONS: COPE5 18
C 0. READ ALL INPUT AND STOP. COPE5 19
C 1. SINGLE PASS ANALYSIS. COPE5 20
C 2. OPTIMIZATION. COPE5 21
C 3. SENSITIVITY - Z = F(X). COPE5 22
C 4. TWO VARIABLE FUNCTION SPACE - Z = F(X,Y). COPE5 23
C 5. OPTIMUM SENSITIVITY. COPE5 24
C 6. ANALYSIS/OPTIMIZATION USING APPROXIMATION TECHNIQUES. COPE5 25
C NEAR,INC REVISION, JULY, 1982 COPE5 26 20
C - COPE5 CHANGED TO A SUBROUTINE CONTROLLED BY TSOPT DRIVER COPE5 28 30
C - CONTROL PARAMETER IFLAG ADDED COPE5 29 40
C IFLAG = 1, EXECUTE COPE5 FROM BEGINNING, READING ALL INPUT COPE5 30 C
C IFLAG = 2, SKIP INPUT AND INITIALIZATION COPE5 31
C ***** INPUT ***** COPE5 32
C ***** COPE5 33
C ***** COPE5 34
C ***** COPE5 35
C ***** COPE5 36
C ***** COPE5 37
NAN2=0 COPE5 38 50
NAN3=0 COPE5 39 60
IF(IFLAG.EQ.2) GO TO 15 COPE5 40
DIMENSIONS OF ARRAYS ARRAY, RA AND IA. COPE5 41 C
NARRAY=1500 COPE5 42 C
NDRA=5000 COPE5 43 C
NDIA=1000 COPE5 44
C READ GENERAL SYNTHESIS CONTROL INPUT. COPE5 45
C SCRATCH TAPE NUMBERS. COPE5 46
ISCR1=20 COPE5 47
ISCR2=40 COPE5 48
CALL COPE01 (RA,IA,NDRA,NDIA) COPE5 49
IF (NCALC.LT.0.OR.NCALC.GT.6) GO TO 340 COPE5 50
CHECK TO INSURE STORAGE REQUIREMENTS DO NOT EXCEED COPE5 51
DIMENSIONED SIZES OF ARRAYS RA AND IA. COPE5 52 .70
NDRA1=LOCR(25) COPE5 53 .80
NDIA1=LOCI(25) COPE5 54
IF (NDRA1.LE.NDRA.AND.NDIA1.LE.NDIA) GO TO 10 COPE5 55 C
WRITE (6,360) NDRA,NDRA1,NDIA,NDIA1 COPE5 56 C
GO TO 340 COPE5 57
CONTINUE COPE5 58
READ USER INPUT. COPE5 59
ICALC=1 COPE5 60
CALL ANALIZ (ICALC). COPE5 61
IF (NCALC.LT.1.OR.NCALC.GT.6) GO TO 340 COPE5 62
----- COPE5 63
***** EXECUTION ***** COPE5 64
----- COPE5 65
15 CONTINUE COPE5 66
ICALC=2 COPE5 67
JCALC=3 COPE5 68
IF (NCALC.NE.2.AND.NCALC.LT.5) GO TO 60 COPE5 69
----- COPE5 70
IF ABS(X(I)).GT.0 OVER-RIDE USER INPUT OF DECISION VARIABLES FOR COPE5 71
OPTIMIZATION. COPE5 72
----- COPE5 73
DO 40 I=1,NDV COPE5 74
XX=ARS(RA(I)) COPE5 75
OVER-RIDE ANALIZ INPUT. COPE5 76
N5=LOCR(5) COPE5 77
M2=LOCI(2) COPE5 78
DO 20 J=1,NDVTOT COPE5 79
NN1=IA(M2) COPE5 80
M2=M2+1 COPE5 81
IF (NN1.NE.I) GO TO 20 COPE5 82
NN1=IA(J) COPE5 83
IF (XX.LT.1.0E-10) GO TO 30 COPE5 84
ARRAY(NN1)=RA(I)*RA(N5) COPE5 85
N5=N5+1 COPE5 86
GO TO 40 COPE5 87
RA(I)=ARRAY(NN1)/RA(N5) COPE5 88
CONTINUE COPE5 89
TRANSFER DESIGN VARIABLES TO ARRAY. COPE5 90
M2=LOCI(2) COPE5 91
N5=LOCR(5) COPE5 92
DO 50 I=1,NDVTOT COPE5 93
N=IA(M2) COPE5 94
M=IA(I) COPE5 95
ARRAY(M)=RA(N)*RA(N5) COPE5 96
N5=N5+1 COPE5 97
M2=M2+1 COPE5 98
CONTINUE COPE5 99
IF (NCALC.NE.3.AND.NCALC.NE.5) GO TO 80 COPE5 100
----- COPE5 101
TRANSFER NOMINAL VALUES OF SENSITIVITY VARIABLES TO ARRAY. COPE5 102
----- COPE5 103
M16=LOCI(16) COPE5 104
M17=LOCI(17) COPE5 105
N15=LOCR(15) COPE5 106
DO 70 I=1,NSV COPE5 107
NN=IA(M16) COPE5 108
M16=M16+1 COPE5 109
ARRAY(NN)=RA(N15) COPE5 110
N15=N15+IA(M17) COPE5 111
M17=M17+1 COPE5 112
CONTINUE COPE5 113
IF (NCALC.LT.6) GO TO 290 COPE5 114
----- COPE5 115
INITIALIZATION FOR APPROXIMATE ANALYSIS/OPTIMIZATION COPE5 116

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C	-----	COPE5117	DX=RA(N23)-XX	COPE5177
	IF (NPA.EQ.0) GO TO 130	COPE5118	IF (ABS(DX).LT.1.0E-6) XX=1.001*RA(N23)	COPE5178
C	ANALIZ INPUT DEFINES AN X-VECTOR.	COPE5119	IF (ABS(XX).LT.1.0E-6) XX=.001	COPE5179
	M5=LOC1(5)	COPE5120	170 RA(NC4)=XX	COPE5180
	N23=LOCR(23)	COPE5121	N23=N23+1	COPE5181
	DO 120 I=1,NXAPRX	COPE5122	180 N24=NC4+1	COPE5182
	J=IA(M5)	COPE5123	190 CONTINUE	COPE5183
C	IS THIS A DESIGN VARIABLE.	COPE5124	REHIND ISCR2	COPE5184
	DO 90 K=1,NDVTOT	COPE5125	NPSA=NPS+NPA	COPE5185
	KK=K	COPE5126	IF (NPSA.EQ.0) GO TO 250	COPE5186
	IF (IA(K).EQ.J) GO TO 100	COPE5127	IF (NPS.EQ.0) GO TO 210	COPE5187
90	CONTINUE	COPE5128	C READ X-VECTORS.	COPE5188
C	NO.	COPE5129	NXI=LOCR(23)*NPA*HXAPRX	COPE5189
	AMULT=1.	COPE5130	DO 200 J=1,NPS	COPE5190
	GO TO 110	COPE5131	NYIJ=NXI+HXAPRX-1	COPE5191
C	YES.	COPE5132	READ (ISCR2) (RA(I),I=NXI,NXIJ)	COPE5192
100	K=LOCR(5)+KK-1	COPE5133	200 NXI=NXI+HXAPRX	COPE5193
	AMULT=RA(K)	COPE5134	210 CONTINUE	COPE5194
110	RA(N23)=ARRAY(J)/AMULT	COPE5135	IF (HPFS.LE.0) NPSA=NPTOT	COPE5195
	M5=M5+1	COPE5136	NXI=LOCR(23)	COPE5196
120	N23=N23+1	COPE5137	NY=NXI+HXAPRX*NPTOT	COPE5197
130	CONTINUE	COPE5138	DO 240 J=1,NPSA	COPE5198
	IF (NPS.GT.0.OR.NPFS.GT.0) GO TO 190	COPE5139	C TRANSFER X-VALUES.	COPE5199
C	ONLY ONE DESIGN VECTOR IS AVAILABLE. CREATE A SECOND X-VECTOR	COPE5140	M5=LOC1(5)	COPE5200
C	SO OPTIMIZATION CAN PROCEED.	COPE5141	I1=NXI	COPE5201
	N23=LOCR(23)	COPE5142	DO 220 I=1,NXAPRX	COPE5202
	N24=N23+NXAPRX	COPE5143	II=IA(M5)	COPE5203
	M5=LOC1(5)	COPE5144	ARRAY(II)=RA(II)	COPE5204
	DO 180 I=1,NXAPRX	COPE5145	M5=M5+1	COPE5205
C	GLOBAL LOCATION.	COPE5146	220 I1=I1+1	COPE5206
	IG=IA(M5)	COPE5147	C ANALYZE.	COPE5207
	M5=M5+1	COPE5148	NAH2=NAH2+1	COPE5208
C	PROPOSED X-VALUE.	COPE5149	CALL ANALIZ (ICALC)	COPE5209
	XX=1.1*RA(N23)	COPE5150	C PUT FUNCTION VALUES IN Y-ARRAY.	COPE5210
	IF (ABS(XX).LT.1.0E-10) XX=.1	COPE5151	M5=LOC1(6)	COPE5211
C	IS THIS A DESIGN VARIABLE.	COPE5152	I1=NY	COPE5212
	M5=LOCR(5)	COPE5153	DO 230 I=1,NF	COPE5213
	DO 140 J=1,NDVTOT	COPE5154	II=IA(M6)	COPE5214
	JJ=J	COPE5155	RA(II)=ARRAY(II)	COPE5215
	AMJ=RA(M5)	COPE5156	I1=I1+1	COPE5216
C	IF (IA(J).EQ.IG) GO TO 150	COPE5157	230 M6=M6+1	COPE5217
	NO.	COPE5158	NXI=NXI+HXAPRX	COPE5218
	M5=M5+1	COPE5159	NY=NY+NF	COPE5219
140	CONTINUE	COPE5160	240 CONTINUE	COPE5220
	GO TO 170	COPE5161	250 CONTINUE	COPE5221
150	CONTINUE	COPE5162	IF (HPFS.LE.0) GO TO 270	COPE5222
C	YES. WHICH DESIGN VARIABLE IS IT.	COPE5163	NXI=LOCR(23)*NPSA*HXAPRX	COPE5223
	ID=LOC1(2)+JJ-1	COPE5164	NY=LOCR(23)*NXAPRX*NPTOT*NF*NPSA	COPE5224
	ID=IA(ID)	COPE5165	C READ X AND Y VECTORS.	COPE5225
C	INSURE XX IS WITHIN BOUNDS.	COPE5166	DO 260 J=1,HPFS	COPE5226
	N2=LOCR(2)+ID-1	COPE5167	NXIJ=NXI+HXAPRX-1	COPE5227
	N3=LOCR(3)+ID-1	COPE5168	NYJ=NY+NF-1	COPE5228
	BL=RA(N2)*ABS(AMJ)	COPE5169	C X-VECTOR.	COPE5229
	BU=RA(N3)*ABS(AMJ)	COPE5170	READ (ISCR2) (RA(I),I=NXI,NXIJ)	COPE5230
	IF (BL.LE.BU) GO TO 160	COPE5171	C Y-VECTOR.	COPE5231
	SAV=BL	COPE5172	READ (ISCR2) (RA(I),I=NY,NYJ)	COPE5232
	BL=BU	COPE5173	NXI=NXI+HXAPRX	COPE5233
	BU=SAV	COPE5174	260 NY=NY+NF	COPE5234
160	IF (XX.LT.BL) XX=BL	COPE5175	270 CONTINUE	COPE5235
	IF (XX.GT.BU) XX=BU	COPE5176	C PUT X-F PAIRS BACK ON ISCR2.	COPE5236

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REWIND ISCR2                                COPE5237 C
NXI=LOCR(23)                                COPE5238 C
NY=NXI+NXAPRX*NPTOT                          COPE5239 C
DO 280 I=1,NPTOT                              COPE5240
NXIJ=NYI+NXAPRX-1                            COPE5241 C
NYJ=NY+NF-1                                  COPE5242
C X-VECTOR.                                  COPE5243
WRITE (ISCR2) (RA(J),J=NXI,NXIJ)            COPE5244 330
C Y-VECTOR.                                  COPE5245 C
WRITE (ISCR2) (RA(J),J=NY,NYJ)             COPE5246 C
NXI=NXIJ+1                                    COPE5247 C
280 NY=NYJ+1                                  COPE5248
290 CONTINUE                                  COPE5249 C
GO TO (300,300,310,320,310,330),NCALC      COPE5250
-----COPE5251
C ONE ANALYSIS                               COPE5252
C -----COPE5253
300 NAN2=NAN2+1                               COPE5254
CALL ANALIZ (ICALC)                          COPE5255
IF (NCALC.GT.1) GO TO 305                    COPE5256 340
NAN3=NAN3+1                                  COPE5257
CALL ANALIZ (JCALC)                          COPE5258
IF (NCALC.EQ.1) GO TO 340                   COPE5259
-----COPE5260
C OPTIIMIZATION                              COPE5261 C
C -----COPE5262
C OPTIIMIZATION.                             COPE5263 C
305 CONTINUE                                  COPE5264 350
CALL COPE02 (ARRAY,RA,IA,NARRAY,NDRA,NDIA) COPE5265
OUTPUT RESULTS.                              COPE5266 360
CALL COPE18 (IOBJ,NDVTOT,NCONA,RA,IA,LOCR,LOCI,ARRAY) COPE5267
NAN3=NAN3+1                                  COPE5268
CALL ANALIZ (JCALC)                          COPE5269
GO TO 340                                     COPE5270
-----COPE5271
C SENSITIVITY ANALYSIS                      COPE5272
C -----COPE5273
310 CONTINUE                                  COPE5274
C ARRAY STARTING LOCATIONS.                  COPE5275
C SENS.                                       COPE5276
N1=LOCR(15)                                  COPE5277
NN8=LOCR(16)-N1                              COPE5278
C NSENSZ.                                     COPE5279
N2=LOCI(15)                                  COPE5280
NN9=NSOBJ                                     COPE5281
C ISENS.                                     COPE5282 C
N3=LOCI(16)                                  COPE5283 C
NN10=NSV                                     COPE5284 C
C HSENS.                                     COPE5285 C
N4=LOCI(17)                                  COPE5286 C
C TEMP.                                       COPE5287 C
N5=LOCR(23)                                  COPE5288 C
CALL COPE04 (ARRAY,NARRAY,RA(N1),IA(N2),IA(N3),IA(N4),RA(N5),NN8,NCOPE5289
1N9,NN10,RA,IA,NDRA,NDIA)                   COPE5290 C
CALL COPE04 (ARRAY,NARRAY,RA(N1),IA(N2),IA(N3),IA(N4),RA(N5),NN8,NCOPE5289
1N9,NN10,RA,IA,NDRA,NDIA)                   COPE5290
C OUTPUT RESULTS.                             COPE5291
CALL COPE05 (RA,IA,NDRA,NDIA,ISCR1)         COPE5292
GO TO 340                                     COPE5293
320 CONTINUE                                  COPE5294

-----COPE5295
C TWO VARIABLE FUNCTION SPACE                COPE5296
-----COPE5297
CALL COPE06 (ARRAY,RA,IA,NARRAY,NDRA,NDIA) COPE5298
OUTPUT RESULTS.                              COPE5299
CALL COPE07 (RA,IA,NDRA,NDIA,ISCR1)         COPE5300
GO TO 340                                     COPE5301
CONTINUE                                     COPE5302
-----COPE5303
C APPROXIMATE ANALYSIS/OPTIMIZATION.         COPE5304
C -----COPE5305
CALL COPE09                                  COPE5306
OUTPUT RESULTS.                              COPE5307
CALL COPE14 (NXAPRX,NF,NPTOT,RA,IA,LOCR,LOCI,TITLE,INOM,NDV,IPAPRXCOPE5308
1,ISCR2,MAXTRM)                              COPE5309
IF (KMAX.LT.0) GO TO 340                     COPE5310
CALL COPE18 (IOBJ,NDVTOT,NCONA,RA,IA,LOCR,LOCI,ARRAY) COPE5311
NAN3=NAN3+1                                  COPE5312
CALL ANALIZ (JCALC)                          COPE5313
CONTINUE                                     COPE5314
WRITE (6,350) NAN2,NAN3                      COPE5315
REWIND ISCR1                                  COPE5316
REWIND ISCR2                                  COPE5317
RETURN                                         COPE5318
-----COPE5319
C FORMATS                                     COPE5320
C -----COPE5321
350 FORMAT (1H1,4X,23HPROGRAM CALLS TO ANALIZ//8X,5HICALC,3X,5HCALLS/1COPE5322
10X,1H1,7X,1H1/10X,1H2,18/10X,1H3,18)      COPE5323
360 FORMAT (//5X,60HREQUIRED STORAGE FOR ARRAY RA OR IA EXCEEDS DIMENSOCPE5324
1IONED SIZE/5X,5HARRAY,2X,9HDIMENSION,2X,8HPEQUIRED/7X,2HRA,18,6X,ICPE5325
25/7X,2HIA,18,6X,15//5X,22H * PROGRAM TERMINATED) COPE5326
EHD                                           COPE5327
SUBROUTINE COPE01 (RA,IA,NDRA,NDIA)         COPE5328
COMMON /CHM1/ DELFUN,DABFUN,FOCH,FOCHM,CT,CTHIN,CTL,CTLMIN,ALPHAXCOPE5329
1,ABOBJ1,THETA,OBJ,NDV,NCON,NSIDE,IPRINT,NFDG,NSCAL,LINOBJ,ITMAX,ITCOPE5330
2RM,ICNDIP,IGOTO,NAC,INFO,INFOG,ITER       COPE5331
COMMON /COPE51/ ATITLE(20)                  COPE5332
COMMON /COPE53/ SGNOPT,NCALC,IOBJ,NSV,NSOBJ,NCONA,N2VX,M2VX,N2VY,MCOPE5333
12VY,N2VAR,IPSENS,IPCVAR,IPDBG,NACMX1,NDVTOT,LOCR(25),LOCI(25),ISCRCOPE5334
21,ISCR2,NXAPRX,NPS,NPFS,NPA,NF,INOM,IPAPRX,KMIN,KMAX,XFACT1,XFACT2COPE5335
3,NAN2,NAN3,NHMAX,NPTOT,INOM,MAXTRM       COPE5336
DIMENSION RA(NDRA), IA(NDIA), TITLE(20)   COPE5337
DATA END1/1HE/,END2/1HN/,END3/1HD/       COPE5338
DATA COM/1H9/,BLANK/1H /                  COPE5339
*****COPE5340
ROUTINE TO READ CONTROL INPUT FOR COPE5.   COPE5341
*****COPE5342
BY G. N. VANDERPLAATS MAR., 1973.         COPE5343
NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COPE5344
-----COPE5345
READ CARD IMAGES AND STORE ON UNIT ISCR2. STORE ON UNIT ISCR1 COPE5346
WITHOUT COMMENT CARDS                      COPE5347
-----COPE5348
REWIND ISCR1                                  COPE5349
REWIND ISCR2                                  COPE5350
NCAPOS=0                                     COPE5351
LOCI(25)=0                                   COPE5352
NCOM=0                                       COPE5353
ICARD=0                                     COPE5354

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10	READ (5,580) (RA(I),I=1,80)	COPE335	DO 80 I=1,ICARD	COPE345
	ICARD=ICARD+1	COPE336	READ (ISCR2,590) NCARDS,(RA(J),J=1,80)	COPE346
	NCARDS=NCARDS+1	COPE337	WRITE (6,890) NCAPDS,(RA(J),J=1,80)	COPE347
	WRITE (ISCR2,590) NCARDS,(RA(I),I=1,80)	COPE338	REWIND ISCR2	COPE348
	IF (RA(1).EQ.COM) GO TO 10	COPE339	CONTINUE	COPE349
	IF (RA(1).EQ.END1.AND.(RA(2).EQ.END2.AND.RA(3).EQ.END3)) GO TO 20	COPE340	WRITE (6,1000) (ATITLE(I),I=1,20)	COPE350
	IF (NCOM.NE.0) GO TO 30	COPE341	WRITE (6,1010) NCALC,NDV,NSV,N2VAR,NXAPRX,IPNPUT,IPDBG	COPE351
C	TITLE OR END CARD.	COPE342	WRITE (6,910)	COPE352
20	WRITE (ISCR1,580) (RA(I),I=1,80)	COPE343	100 NACHX1=0	COPE353
	IF (NCOM.GT.0) GO TO 70	COPE344	NDVTOT=0	COPE354
C	IT WAS THE TITLE CARD.	COPE345	HCONA=0	COPE355
	NCOM=1	COPE346	NCON=0	COPE356
	GO TO 10	COPE347	IF (NDV.LE.0) GO TO 270	COPE357
30	CONTINUE	COPE348	-----	COPE358
C	FORMAT DATA AS REQUIRED.	COPE349	OPTIMIZATION INFORMATION	COPE359
	NA=1	COPE350	-----	COPE360
	NB=81	COPE351	OPTIMIZATION CONTROL VARIABLES. - COMMON DEPENDENT.	COPE361
	CALL COPE08 (RA(NA),RA(NB),IFORM,NFLD)	COPE352	DATA BLOCK C.	COPE362
C	DETERMINE NUMBER OF CARDS OF DATA AND ADD BLANKS TO FILL.	COPE353	READ (ISCR1,1200) IPRINT,ITMAX,ICNDIR,NSCAL,ITRM,LINOBJ,NACHX1,NFDC	COPE363
	NBC=(NFLD-1)/8+1	COPE354	1G	COPE364
	NB=80*NBC+80	COPE355	C --- DATA BLOCK D.	COPE365
	NA=10*NFLD+81	COPE356	READ (ISCR1,1210) FDCH,FDCHM,CT,CTMIN,CTL,CTLMIN,THETA,PHI,DELFUN,	COPE366
	IF (NA.GE.NB) GO TO 50	COPE357	1DASFUN,ALPHAX,ABOBJ1	COPE367
	DO 40 I=NA,NB	COPE358	C --- DATA BLOCK E.	COPE368
40	RA(I)=BLANK	COPE359	TOTAL NO. OF D. V., OBJECTIVE GLOBAL NUMBER, SIGN	COPE369
50	CONTINUE	COPE360	OR OPTIMIZATION OBJECTIVE.	COPE370
	WRITE (ISCR1,580) (RA(I),I=81,NB)	COPE361	READ (ISCR1,920) NDVTOT,IOBJ,SGNOPT	COPE371
	IF (IFORM.GT.0) GO TO 10	COPE362	IF (NDVTOT.LT.NDV) NDVTOT=NDV	COPE372
C	DATA WAS NOT PREVIOUSLY FORMATTED.	COPE363	IF (NCALC.EQ.6.AND.NACHX1.EQ.0) NACHX1=2*NDV+2	COPE373
	N1=1	COPE364	IF (NACHX1.LE.0) NACHX1=NDV+2	COPE374
	DO 60 II=1,NBC	COPE365	IF (IPNPUT.GE.2) GO TO 110	COPE375
	N1=N1+80	COPE366	IF (ABS(SGNOPT).LT.1.0E-10) SGNOPT=-1.	COPE376
	N2=N1+79	COPE367	WRITE (6,1070) IOBJ,SGNOPT	COPE377
	WRITE (ISCR2,590) NCARDS,(RA(I),I=N1,N2)	COPE368	WRITE (6,760) IPRINT,ITMAX,ICNDIR,NSCAL,ITRM,LINOBJ,NACHX1,NFDG	COPE378
60	ICARD=ICARD+1	COPE369	WRITE (6,770) FDCH,FDCHM,CT,CTMIN,CTL,CTLMIN,THETA,PHI,DELFUN,DABF	COPE379
	GO TO 10	COPE370	1UH,ALPHAX,ABOBJ1	COPE380
70	CONTINUE	COPE371	N2=NDV+3	COPE381
	REWIND ISCR1	COPE372	N3=N2+NDV+2	COPE382
	REWIND ISCR2	COPE373	H4=N3+NDV+2	COPE383
C	-----	COPE374	C --- DATA BLOCK F.	COPE384
C	GENERAL SYNTHESIS INFORMATION	COPE375	DESIGN VARIABLE INFORMATION, LB, UB, INITIAL VALUE, SCAL.	COPE385
C	-----	COPE376	IF (IPNPUT.LT.2) WRITE (6,1080)	COPE386
C	TITLE.	COPE377	N5=N4+NDV+2	COPE387
C ---	DATA BLOCK A.	COPE378	IF (NS.LE.NDRA) GO TO 120	COPE388
	READ (ISCR1,1190) (ATITLE(I),I=1,20)	COPE379	WRITE (6,780)	COPE389
C	CONTROL PARAMETERS.	COPE380	WRITE (6,790)	COPE390
C ---	DATA BLOCK B.	COPE381	LOC(25)=H5	COPE391
	READ (ISCR1,1200) NCALC,NDV,NSV,N2VAR,NXAPRX,IPNPUT,IPDBG	COPE382	GO TO 550	COPE392
	IF (NCALC.LT.0.OR.NCALC.GT.6) WRITE (6,1220) NCALC	COPE383	CONTINUE	COPE393
	IF (NCALC.LT.0.OR.NCALC.GT.6) RETURN	COPE384	H5IDE=0	COPE394
	IF (IPNPUT.GT.1) GO TO 100	COPE385	DO 130 I=1,NDV	COPE395
	WRITE (6,970)	COPE386	READ (ISCR1,1060) RA(N2),RA(N3),RA(I),RA(N4),(TITLE(J),J=1,5)	COPE396
	WRITE (6,980)	COPE387	IF (RA(N2).GT.-1.0E+15.OR.PA(N3).LT.1.0E+15) H5IDE=1	COPE397
	WRITE (6,990) (ATITLE(I),I=1,20)	COPE388	IF (RA(N2).LE.-1.0E+15) RA(N2)=-1.1E+15	COPE398
C	-----	COPE389	IF (RA(N3).GE.1.0E+15) PA(N3)=1.1E+15	COPE399
C	CARD IMAGE PRINT	COPE390	IF (IPNPUT.LT.2) WRITE (6,1090) I,RA(N2),RA(N3),RA(I),RA(N4),(TITL	COPE400
C	-----	COPE391	(J),J=1,5)	COPE401
C	IF (IPNPUT.GT.0) GO TO 90	COPE392	N2=N2+1	COPE402
	WRITE (6,870)	COPE393	N3=N3+1	COPE403
	WRITE (6,880)	COPE394	N4=N4+1	COPE404

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130 CONTINUE
C --- DATA BLOCK G.
D. V. NO., GLOBAL LOCATION, MULTIPLYING FACTOR.
IF (IPHPUT.LT.2) WRITE (6,930)
N5=4*NDV+9
M2=NDVTOT+1
N6=N5+NDVTOT
M3=M2+NDVTOT
IF (N6.LE.NDPA) GO TO 140
WRITE (6,780)
WRITE (6,800)
LOCP(25)=N5
GO TO 550
140 CONTINUE
IF (M3.LE.NDIA) GO TO 150
WRITE (6,810)
WRITE (6,800)
LOCI(25)=M3
GO TO 550
150 CONTINUE
DO 160 I=1,NDVTOT
READ (ISCR1,920) IA(M2),IA(I),RA(N5)
IF (ABS(RA(N5)).LT.1.0E-20) RA(N5)=1.0
IF (IPHPUT.LT.2) WRITE (6,940) I,IA(M2),IA(I),RA(N5)
M2=M2+1
N5=N5+1
160 CONTINUE
NCON=0
C --- DATA BLOCK H.
NUMBER OF CONSTRAINT SETS.
READ (ISCR1,920) NCONS
IF (IPHPUT.LT.2) WRITE (6,1110)
IF (IPHPUT.LT.2) WRITE (6,1120) NCONS
IF (NCONS.EQ.0) GO TO 270
IF (IPHPUT.LT.2) WRITE (6,1130)
N6=4*NDV+NDVTOT+9
M3=2*NDVTOT+1
M4=2*NDVTOT+NCONS
M4A=M4+1
L=1
C --- DATA BLOCK I.
DO 240 I=1,NCONS
NNH=N6+3
IF (NNH.GT.NDRA) GO TO 250
GLOBAL NO. 1, GLOBAL NO. 2, LINEAR CONSTRAINT ID.
READ (ISCR1,1200) ICONI,JCONI,LCONI
LB, NORM, UB, NORM.
READ (ISCR1,1210) (RA(J),J=N6,NNH)
IF (RA(N6).LE.-1.0E+15) RA(N6)=-1.1E+15
IF (RA(N6+2).GE.1.0E+15) RA(N6+2)=1.1E+15
IF (RA(N6+1).LT.1.0E-20) RA(N6+1)=ABS(RA(N6))
IF (RA(N6+1).LT.1.0E-20) RA(N6+1)=0.1
IF (RA(N6+3).LT.1.0E-20) RA(N6+3)=ABS(RA(N6+2))
IF (RA(N6+3).LT.1.0E-20) RA(N6+3)=0.1
NUMBER OF VARIABLES IN THIS SET.
NVAR=JCONI-ICONI+1
IF (NVAR.LT.1) NVAR=1
NCONA=NCONA+NVAR
HOW MANY CONSTRAINTS?
J1=0
COPE5475 IF (RA(N6).GE.-1.0E+15) J1=1
COPE5476 IF (RA(N6+2).LT.1.0E+15) J1=J1+1
COPE5477 NCONI=J1+NVAR
COPE5478 NCON=NCON+NCONI
COPE5479 IF (J1.EQ.0) GO TO 180
C ADD LINEAR CONSTRAINT IDENTIFIERS TO ISC.
COPE5480 DO 170 J=1,NCONI
COPE5481 M4=M4+1
COPE5482 MMM=M4
COPE5483 IF (MMM.GT.NDIA) GO TO 260
COPE5484 IA(M4)=LCONI
COPE5485 170 CONTINUE
COPE5486 180 ADD LB, UB AND SCAL TO BLU IF NVAR.GT.1.
C IF (NVAR.EQ.1) GO TO 200
COPE5487 NVAR1=NVAR-1
COPE5488 DO 190 J=1,NVAR1
COPE5489 NNN=N6+7
COPE5490 IF (NNN.GT.NDRA) GO TO 250
COPE5491 RA(N6+4)=RA(N6)
COPE5492 RA(N6+5)=RA(N6+1)
COPE5493 RA(N6+6)=RA(N6+2)
COPE5494 RA(N6+7)=RA(N6+3)
COPE5495 N6=N6+4
COPE5496 190 CONTINUE
COPE5497 200 CONTINUE
COPE5498 C ADD CONSTRAINED VARIABLE GLOBAL IDENTIFIERS TO ICON.
COPE5499 ICONI=ICONI
COPE5500 MMM=M4+NVAR-1
COPE5501 IF (MMM.GT.NDIA) GO TO 260
COPE5502 DO 230 J=1,NVAR
COPE5503 IF (J.EQ.1) GO TO 220
C SHIFT ISC VECTOR.
COPE5504 L1=M4+1
COPE5505 L2=M4
COPE5506 DO 210 K=M4A,M4
COPE5507 IA(L1)=IA(L2)
COPE5508 L1=L1-1
COPE5509 210 L2=L2-1
COPE5510 M4=M4+1
COPE5511 M4A=M4A+1
COPE5512 IA(M3)=ICONI
COPE5513 ICONI=ICONI+1
COPE5514 M3=M3+1
COPE5515 IF (IPHPUT.LT.2) WRITE (6,1100) L,ICONI,JCONI,LCONI,RA(N6),RA(N6+1),RA(N6+2),RA(N6+3)
COPE5516 N6=N6+4
COPE5517 L=NCON+1
COPE5518 CONTINUE
COPE5519 IF (IPHPUT.LT.2) WRITE (6,900) NCONA
COPE5520 GO TO 270
COPE5521 240 WRITE (6,780)
COPE5522 WRITE (6,820)
COPE5523 LOCP(25)=NNH
COPE5524 GO TO 550
COPE5525 250 WRITE (6,810)
COPE5526 WRITE (6,820)
COPE5527 LOCI(25)=MMM
COPE5528 GO TO 550
COPE5529 260 WRITE (6,810)
COPE5530 WRITE (6,820)
COPE5531 LOCI(25)=MMM
COPE5532 GO TO 550
COPE5533 270 CONTINUE
COPE5534 C STARTING LOCATIONS FOR APPROXIMATION INFORMATION.
COPE5535 COPE5536
COPE5537 COPE5538
COPE5539 COPE5540
COPE5541 COPE5542
COPE5543 COPE5544
COPE5545 COPE5546
COPE5547 COPE5548
COPE5549 COPE5550
COPE5551 COPE5552
COPE5553 COPE5554
COPE5555 COPE5556
COPE5557 COPE5558
COPE5559 COPE5560
COPE5561 COPE5562
COPE5563 COPE5564
COPE5565 COPE5566
COPE5567 COPE5568
COPE5569 COPE5570
COPE5571 COPE5572
COPE5573 COPE5574
COPE5575 COPE5576
COPE5577 COPE5578
COPE5579 COPE5580
COPE5581 COPE5582
COPE5583 COPE5584
COPE5585 COPE5586
COPE5587 COPE5588
COPE5589 COPE5590
COPE5591 COPE5592
COPE5593 COPE5594

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	NAPR=4*NDV+NDVTOT+4*NCONA+9	COPE5595	WRITE (6,630)	COPE5655
	NAPI=2*(NDV+NCONA)+2*NDVTOT+NCONA+1	COPE5596	LOC(25)=M5	COPE5656
	NF=0	COPE5597	GO TO 550	COPE5657
	KMAX=0	COPE5598	CONTINUE	COPE5658
	HPTOT=0	COPE5599	IF (INXLOC.EQ.0) GO TO 310	COPE5659
	MAXTRM=0	COPE5600	READ (ISCR1,1200) (IA(I),I=M5,MM5)	COPE5660
	IF (NXAPRX.LE.0) GO TO 450	COPE5601	GO TO 330	COPE5661
C	-----	COPE5602	310 CONTINUE	COPE5662
C	APPROXIMATE ANALYSIS/DESIGN	COPE5603	C X-LOCATIONS ARE DEFAULTED TO DESIGN VARIABLE LOCATIONS.	COPE5663
C	-----	COPE5604	DO 320 I=1,NXAPRX	COPE5664
C	DATA BLOCK J.	COPE5605	IA(M5)=IA(I)	COPE5665
C	CONTROL PARAMETERS.	COPE5606	320 M5=M5+1	COPE5666
	READ (ISCR1,1200) NF,NPS,NPFS,NPA,INOM,ISCRX,ISCRXF,IPAPRX	COPE5607	M5=NAPI	COPE5667
	IF (NPA.NE.0) NPA=1	COPE5608	330 CONTINUE	COPE5668
	IF (NPS.EQ.0.AND.NPFS.EQ.0) NPA=1	COPE5609	IF (IPNPUT.LT.2) WRITE (6,640)	COPE5669
	IF (ISCRX.EQ.0) ISCRX=5	COPE5610	IF (IPNPUT.LT.2) WRITE (6,1180) (IA(I),I=M5,MM5)	COPE5670
	IF (ISCRXF.EQ.0) ISCRXF=5	COPE5611	C --- DATA BLOCK M.	COPE5671
	IF (IPNPUT.LT.2) WRITE (6,600) NF,NPS,NPFS,NPA,INOM,ISCRX,ISCRXF,IPAPRX	COPE5612	C GLOBAL LOCATIONS OF FUNCTIONS.	COPE5672
	IPAPRX	COPE5613	M6=NAPI+NXAPRX	COPE5673
	NPSFS=NPS+NPFS	COPE5614	MM6=M6+MF-1	COPE5674
	IF (NPSFS.LT.2) NPA=1	COPE5615	IF (MM6.LE.NDIA) GO TO 340	COPE5675
	NPTOT=NPS+NPFS+NPA	COPE5616	WRITE (6,790)	COPE5676
	IF (NPTOT.LT.2) NPTOT=2	COPE5617	WRITE (6,650)	COPE5677
	READ (ISCR1,1200) KMIN,KMAX,NPMAX,JNOM,INXLOC,INFLOC,MAXTRM	COPE5618	LOC(25)=M6	COPE5678
	IF (INXLOC.EQ.0) NXAPRX=NDVTOT	COPE5619	GO TO 550	COPE5679
	M=NXAPRX+(NXAPRX*(NXAPRX+1))/2	COPE5620	340 CONTINUE	COPE5680
	IF (NPMAX.LE.0) NPMAX=2*M	COPE5621	IF (INFLOC.EQ.0) GO TO 350	COPE5681
	IF (KMAX.EQ.0) KMAX=3*M-NPTOT+1	COPE5622	READ (ISCR1,1200) (IA(I),I=M6,MM6)	COPE5682
	IF (KMIN.EQ.0) KMIN=2*NDV-NPTOT+1	COPE5623	GO TO 380	COPE5683
	IF (KMIN.LT.0) KMIN=0	COPE5624	350 CONTINUE	COPE5684
	IF (KMAX.GT.0.AND.KMAX.LT.KMIN) KMAX=KMIN	COPE5625	C FUNCTION LOCATIONS ARE DEFAULTED TO OBJECTIVE AND CONSTRAINT	COPE5685
	IF (JNOM.EQ.0) JNOM=2*M	COPE5626	C LOCATIONS.	COPE5686
	IF (MAXTRM.LT.1) MAXTRM=3	COPE5627	NF1=1	COPE5687
	IF (IPNPUT.LT.2) WRITE (6,610) KMIN,KMAX,NPMAX,JNOM,INXLOC,INFLOC,MAXTRM	COPE5628	M3=2*NDVTOT+1	COPE5688
	MAXTRM	COPE5629	IA(M6)=IOBJ	COPE5689
C	DATA BLOCK K, PART 1.	COPE5630	IF (NCOHA.EQ.0) GO TO 370	COPE5690
C	DELX BOUNDS ON APPROXIMATE OPTIMIZATION.	COPE5631	DO 360 I=1,NCOHA	COPE5691
	IF (NDV.LE.0) GO TO 290	COPE5632	IF (IA(M3).EQ.IOBJ) GO TO 360	COPE5692
	N7=NAPR	COPE5633	NF1=NF1+1	COPE5693
	NN7=N7+NDV-1	COPE5634	M6=M6+1	COPE5694
	IF (NN7.LE.NDRA) GO TO 280	COPE5635	IA(M6)=IA(M3)	COPE5695
	WRITE (6,780)	COPE5636	360 M3=M3+1	COPE5696
	WRITE (6,560)	COPE5637	370 NF=NF1	COPE5697
280	CONTINUE	COPE5638	380 M6=NAPI+NXAPRX	COPE5698
	READ (ISCR1,1210) (RA(I),I=N7,NN7)	COPE5639	MM6=M6+MF-1	COPE5699
	IF (IPNPUT.LT.2) WRITE (6,570)	COPE5640	IF (IPNPUT.LT.2) WRITE (6,660)	COPE5700
	IF (IPNPUT.LT.2) WRITE (6,1160) (RA(I),I=N7,NN7)	COPE5641	IF (IPNPUT.LT.2) WRITE (6,1180) (IA(I),I=M6,MM6)	COPE5701
C	DATA BLOCK K, PART 2.	COPE5642	C --- DATA BLOCK N.	COPE5702
C	MULTIPLIERS ON DELX.	COPE5643	C READ INPUT X-VECTORS AND STORE ON UNIT ISCR2.	COPE5703
	READ (ISCR1,1210) XFACT1,XFACT2	COPE5644	REWIND ISCR2	COPE5704
	IF (XFACT1.LT.1.0E-10) XFACT1=1.5	COPE5645	IF (NPS.EQ.0) GO TO 410	COPE5705
	IF (XFACT2.LT.1.0E-10) XFACT2=2.	COPE5646	N7=NAPR+NDV	COPE5706
	IF (IPNPUT.LT.2) WRITE (6,620) XFACT1,XFACT2	COPE5647	NN7=NN7+NXAPRX-1	COPE5707
290	CONTINUE	COPE5648	IF (NN7.LE.NDRA) GO TO 390	COPE5708
C	DATA BLOCK L.	COPE5649	WRITE (6,780)	COPE5709
C	GLOBAL LOCATIONS OF X-VARIABLES.	COPE5650	WRITE (6,670)	COPE5710
	M5=NAPI	COPE5651	LOC(25)=NN7	COPE5711
	MM5=M5+NXAPRX-1	COPE5652	GO TO 550	COPE5712
	IF (MM5.LE.NDIA) GO TO 300	COPE5653	390 CONTINUE	COPE5713
	WRITE (6,780)	COPE5654	IF (IPNPUT.LT.2) WRITE (6,680) ISCRX	COPE5714

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DO 400 I=1,NPS
C   BINARY READ IF ISCRX.NE.5.
   IF (ISCRX.NE.5) READ (ISCRX) (RA(J),J=N7,NN7)
C   FORMATTED READ IF ISCRX.EQ.5.
   IF (ISCRX.EQ.5) READ (ISCP1,1210) (RA(J),J=N7,NN7)
   WRITE (ISCR2) (RA(J),J=N7,NN7)
   IF (IPNPUT.LT.2) WRITE (6,710) I,I
   IF (IPNPUT.LT.2) WRITE (6,1160) (RA(J),J=N7,NN7)
400 CONTINUE
410 CONTINUE
C --- DATA BLOCK O.
C   READ INPUT X-F PAIRS AND STORE ON UNIT ISCR2.
   IF (NPFS.EQ.0) GO TO 440
   N7=NAPR+NDV
   NN7=N7+NXAPRX-1
   NN8=N7+NF-1
   IF (NN7.GT.NN8) NN8=NN7
   IF (NN8.LE.NDRA) GO TO 420
   WRITE (6,780)
   WRITE (6,690)
   LOCR(25)=NN8
   GO TO 550
420 CONTINUE
   NN8=N7+NF-1
   IF (IPNPUT.LT.2) WRITE (6,700) ISCRXF
   DO 430 I=1,NPFS
C   X-VECTOR.
C   BINARY READ IF ISCRXF.NE.5.
   IF (ISCRXF.NE.5) READ (ISCRXF) (RA(J),J=N7,NN7)
C   FORMATTED READ IF ISCRXF.EQ.5.
   IF (ISCRXF.EQ.5) READ (ISCR1,1210) (RA(J),J=N7,NN7)
   II=I+NPS
   IF (IPNPUT.LT.2) WRITE (6,710) I,II
   IF (IPNPUT.LT.2) WRITE (6,720)
   IF (IPNPUT.LT.2) WRITE (6,1160) (RA(J),J=N7,NN7)
   WRITE (ISCR2) (RA(J),J=N7,NN7)
C   FUNCTION VALUES.
C   BINARY READ IF ISCRXF.NE.5.
   IF (ISCRXF.NE.5) READ (ISCRXF) (RA(J),J=N7,NN8)
C   FORMATTED READ IF ISCRXF.EQ.5.
   IF (ISCRXF.EQ.5) READ (ISCR1,1210) (RA(J),J=N7,NN8)
   IF (IPNPUT.LT.2) WRITE (6,730)
   IF (IPNPUT.LT.2) WRITE (6,1160) (RA(J),J=N7,NN8)
   WRITE (ISCR2) (RA(J),J=N7,NN8)
430 CONTINUE
440 CONTINUE
450 CONTINUE
   NSOBJ=0
   NSVTOT=0
C   STARTING LOCATIONS FOR SENSITIVITY INFORMATION.
   NSVR=NAPR+NDV
   NSVI=NAPI+HXAPRX*NF
   IF (NSV.LE.0) GO TO 500
C -----
C   SENSITIVITY INFORMATION
C -----
   IF (IPNPUT.LT.2) WRITE (6,1020)
C --- DATA BLOCK P, PART 1.
C   NSOBJ, IPSENS
   READ (ISCR1,1200) NSOBJ,IPSENS
COPE5715 C --- DATA BLOCK P, PART 2.
COPE5716 C   HSEHSZ.
COPE5717   M15=NSVI
COPE5718   MM15=M15+NSOBJ-1
COPE5719   IF (MM15.LE.NDIA) GO TO 460
COPE5720   WRITE (6,810)
COPE5721   WRITE (6,830)
COPE5722   LOCI(25)=MM15
COPE5723   GO TO 550
COPE5724 460 CONTINUE
COPE5725   READ (ISCR1,1200) (IA(I),I=M15,MM15)
COPE5726   IF (IPNPUT.LT.2) WRITE (6,960) IPSENS,NSOBJ
COPE5727   IF (IPNPUT.LT.2) WRITE (6,950) (IA(I),I=M15,MM15)
COPE5728   IF (IPNPUT.LT.2) WRITE (6,1030)
COPE5729   N15=NSVR
COPE5730   M16=NSVI+NSOBJ
COPE5731   M17=M16+NSV
COPE5732   DO 490 I=1,NSV
C --- DATA BLOCK Q, PART 1.
COPE5733 C   ISENS, HSENS.
COPE5734 C   READ (ISCR1,1200) IA(M16),NN1
COPE5735   NN15=N15+NN1-1
COPE5736   IF (NN15.LE.NDRA) GO TO 470
COPE5737   WRITE (6,780)
COPE5738   WRITE (6,840)
COPE5739   LOCR(25)=NN15
COPE5740   GO TO 550
COPE5741 470 CONTINUE
COPE5742 C --- DATA BLOCK Q, PART 2.
COPE5743 C   SENS.
COPE5744 C   READ (ISCR1,1210) (RA(J),J=N15,NN15)
COPE5745   IF (IPNPUT.GE.2) GO TO 480
COPE5746   JJ=N15+5
COPE5747   IF (JJ.GT.NN15) JJ=NN15
COPE5748   WRITE (6,1040) I,IA(M16),(RA(J),J=N15,JJ)
COPE5749   JJ=JJ+1
COPE5750   IF (JJ.LE.NN15) WRITE (6,1050) (RA(J),J=JJ,NN15)
COPE5751 480 CONTINUE
COPE5752   NSVTOT=NSVTOT+NN1
COPE5753   IA(M17)=NN1
COPE5754   N15=NN15+1
COPE5755   M16=M16+1
COPE5756   M17=M17+1
COPE5757 490 CONTINUE
COPE5758 500 CONTINUE
COPE5759   M2VX=0
COPE5760   M2VY=0
COPE5761 C   STARTING LOCATIONS FOR TWO-VARIABLE FUNCTION SPACE INFORMATION.
COPE5762   N2VR=NSVR+NSVTOT
COPE5763   N2VI=NSVI+NSOBJ+2*NSV
COPE5764   IF (N2VAR.LE.0) GO TO 540
COPE5765 C -----
COPE5766 C   TWO-VARIABLE FUNCTION SPACE INFORMATION
COPE5767 C -----
COPE5768 C --- DATA BLOCK R.
COPE5769 C   VARIABLE NUMBERS AND NUMBER OF VALUES OF X AND Y.
COPE5770 C   READ (ISCR1,1200) N2VX,M2VX,N2VY,M2VY,IP2VAR
COPE5771   N20=N2VR
COPE5772   M20=N2VI
COPE5773   M120=M20+N2VAR-1
COPE5774
COPE5775 COPE5775
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IF (MM20.LE.HOIA) GO TO 510
WRITE (6,810)
WRITE (6,850)
LOCI(25)=MM20
GO TO 550
510 CONTINUE
C --- DATA BLOCK S.
C GLOBAL VARIABLE NUMBERS CORRESPONDING TO FUNCTIONS OF X AND Y.
READ (ISCR1,1200) (IA(I),I=M20,MM20)
IF (IPNPUT.LT.2) WRITE (6,1170) IP2VAR
IF (IPNPUT.LT.2) WRITE (6,1180) (IA(I),I=M20,MM20)
C --- DATA BLOCK T.
C VALUES OF X COMPONENTS.
NH20=N20*M2VX-1
IF (NH20.LE.NDRA) GO TO 520
WRITE (6,780)
WRITE (6,740)
LOCP(25)=NH20
GO TO 550
520 READ (ISCR1,1210) (RA(I),I=N20,NN20)
IF (IPNPUT.LT.2) WRITE (6,1140) N2VX
IF (IPNPUT.LT.2) WRITE (6,1160) (RA(I),I=N20,NN20)
C --- DATA BLOCK U.
C VALUES OF Y COMPONENTS.
N21=N20*M2VX
NN21=N21*M2VY-1
IF (NN21.LE.NDRA) GO TO 530
WRITE (6,780)
WRITE (6,750)
LOCR(25)=NN21
GO TO 550
530 CONTINUE
NH20=NH21
READ (ISCR1,1210) (RA(I),I=N21,NN21)
IF (IPNPUT.LT.2) WRITE (6,1150) N2VY
IF (IPNPUT.LT.2) WRITE (6,1160) (RA(I),I=N21,NN21)
540 CONTINUE
-----
C DYNAMIC STORAGE ALLOCATION
-----
NDV2=NDV*2
REAL VARIABLES.
X.
LOCR(1)=1
VLB.
LOCR(2)=NDV*3
VUB.
LOCR(3)=LOCR(2)+NDV2
SCAL.
LOCR(4)=LOCR(3)+NDV2
MULT.
LOCR(5)=LOCR(4)+NDV2
BLU.
LOCR(6)=LOCR(5)+NDVTOT
DELX.
LOCR(7)=LOCR(6)+4*HCONA
LOCR(8)=LOCR(7)+NDV
SENS.
LOCR(15)=LOCR(8)
XM2V.

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COPE5835 LOCR(20)=LOCR(15)+HSVTOT
COPE5836 YM2V.
COPE5837 C LOCR(21)=LOCR(20)*M2VX
COPE5838 LOCR(22)=LOCR(21)*M2VY
COPE5839 C START OF EXECUTION STORAGE.
COPE5840 LOCR(23)=LOCR(22)
COPE5841 C INTEGER VARIABLES.
COPE5842 C IDSGN.
COPE5843 LOCI(1)=1
COPE5844 C ND5GM.
COPE5845 LOCI(2)=NDVTOT+1
COPE5846 C ICCN.
COPE5847 LOCI(3)=LOCI(2)+NDVTOT
COPE5848 C ISC.
COPE5849 LOCI(4)=LOCI(3)+HCONA
COPE5850 C LOCX.
COPE5851 LOCI(5)=LOCI(4)+2*(NDV+HCONA)
COPE5852 C LOCF.
COPE5853 LOCI(6)=LOCI(5)+HXAPRX
COPE5854 LOCI(7)=LOCI(6)+NF
COPE5855 C NSENSZ.
COPE5856 LOCI(15)=LOCI(7)
COPE5857 C ISENS.
COPE5858 LOCI(16)=LOCI(15)+NSOBJ
COPE5859 C NSENS.
COPE5860 LOCI(17)=LOCI(16)+NSV
COPE5861 LOCI(18)=LOCI(17)+NSV
COPE5862 C H2VZ.
COPE5863 LOCI(20)=LOCI(18)
COPE5864 LOCI(21)=LOCI(20)+N2VAR
COPE5865 C START OF EXECUTION STORAGE.
COPE5866 LOCI(23)=LOCI(21)
COPE5867 C EXECUTION STORAGE REQUIREMENTS.
COPE5868 HRI=NDV
COPE5869 IF (HACHX1.GT.HRI) HRI=HACHX1
COPE5870 HR2=3+HCON+12*NDV+HACHX1*(NDV2+HACHX1)+3*HRI+12
COPE5871 NI2=HACHX1+2*HRI+2*NDV+HCON
COPE5872 NR3=NSV
COPE5873 IF (HSOBJ.GT.NR3) NR3=HSOBJ
COPE5874 HR4=H2VAR
COPE5875 HR5=NP2*NP3
COPE5876 NI5=NI2
COPE5877 M=HXAPRX+(HXAPRX*(HXAPRX+1))/2
COPE5878 IF (HMAXTRM.LT.3) M=HAXTFM*HXAPRX
COPE5879 HR6=3+HXAFBX*6*NDV+2*NF*M*NF
COPE5880 NI6=HCONA*HXAPRX
COPE5881 HRI=(HMAX+1-NPTOT)*(HXAPRX+NF+1)
COPE5882 IF (HRI.LT.NR2) HRI=NR2
COPE5883 IF (HMAX.LT.0) HRI=NPTOT*(HXAPRX+NF+1)
COPE5884 NP7=HR6+HRI
COPE5885 NI7=NI6*NI2
COPE5886 C START OF TEMPORARY STORAGE.
COPE5887 LOCR(24)=LOCR(23)
COPE5888 LOCI(24)=LOCI(23)
COPE5889 IF (HNCALC.EQ.2) LOCR(24)=LOCR(23)+HR2
COPE5890 IF (HNCALC.EQ.3) LOCR(24)=LOCR(23)+HR3
COPE5891 IF (HNCALC.EQ.4) LOCR(24)=LOCR(23)+HR4
COPE5892 IF (HNCALC.EQ.5) LOCR(24)=LOCP(23)+HR5
COPE5893 IF (HNCALC.EQ.6.AND.HMAX.LT.0) LOCR(24)=LOCR(23)+HR6
COPE5894 IF (HNCALC.EQ.6.AND.HMAX.GT.0) LOCR(24)=LOCR(23)+HR7

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COPE5895
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1ALIZATION,6X,5HUPPER,6X,13HNORMALIZATION/6X,2HID,3X,6HVAR. 1,2X,6HCOPE1075
2VAR. 2,4X,2HID,8X,5HBOUND,9X,6HFACTOR,10X,5HBOUND,9X,6HFACTOR) COPE1076 C
1140 FORMAT (/5X,49HGLOBAL VARIABLE NUMBER CORRESPONDING TO X, N2VX =,COPE1077
(15//5X,20HVALUES OF X-VARIABLE) COPE1078
1150 FOPHAT (/5X,49HGLOBAL VARIABLE NUMBER CORRESPONDING TO Y, N2VY =,COPE1079
115//5X,20HVALUES OF Y-VARIABLE) COPE1080
1160 FORNAT (3X,5E12.4) COPE1081
1170 FORNAT (/5X,51H* * TWO-VARIABLE FUNCTION SPACE MAPPING INFORMACOPE1082
110H//5X,23HPRINT CONTROL, IP2VAR =,15//5X,5CHGLOBAL VARIABLE NUMBECOPE1083
2RS ASSOCIATED WITH F(X,Y), MCVZ) COPE1084
1180 FORNAT (5X,10I5) COPE1085
1190 FORNAT (20A4) COPE1086 C
1200 FORNAT (8I10) COPE1087 C
1210 FORNAT (8F10.2) COPE1088 10
1220 FORNAT (/5X,26H* * * INPUT ERROR, HCALC =,I2,2X,41HIS LT.0 OR GTCOPE1089
1.6 PROGRAM TERMINATED * * *) COPE1090
END COPE1091
SUBROUTINE COPE02 (ARRAY,RA,IA,HARRAY,NDRA,NDIA) COPE1092 C
COMMON /CMMH1/ DELFUN,DABFUN,FDCH,FDCHM,CT,CTMIN,CTL,CTLMIN,ALPHAXCOPE1093
1,ABOBJ1,THETA,OBJ,NDV,NCON,NSIDE,IPRINT,NFDG,NSCAL,LINDBJ,ITMAX,ITCOPE1094
2RM,ICNDR,IGOTO,NAC,INFO,INFOG,ITER COPE1095
COMMON /COPE53/ SGNOPT,HCALC,IOBJ,NSV,NSCBJ,NCONA,N2VX,M2VX,N2VY,MCPE1096
12VY,N2VAR,IPSENS,IP2VAR,IPDBG,NACHX1,NDVTOT,LOCR(25),LOCI(25),ISRCOPE1097
21,ISCR2,NXAPRX,NPS,NPFS,NPA,NF,INOM,IPAPRX,KMIN,KMAX,XFACT1,XFACTCOPE1098
3,NAN2,NAN3,NPMAX,NPTOT,JHOM,MAXTRM COPE1099
DIMENSION ARRAY(HARRAY), RA(NDRA), IA(NDIA) COPE1100
***** COPE1101
ROUTINE TO CONTROL OPTIMIZATION. COPE1102 C
***** COPE1103
BY G. N. VANDERPLAATS MAR., 1973. COPE1104 C
NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COPE1105 C
***** COPE1106
ARRAY DIMENSIONS COPE1107 C
***** COPE1108
NN1=NDV*2 COPE1109 C
NN2=2*NDV*NCON COPE1110 C
NN3=NACHX1 COPE1111 C
NN4=NN3 COPE1112 C
IF (NDV.GT.NN4) NN4=NDV COPE1113 C
NN5=2*NN4 COPE1114 C
NN6=NDVTOT COPE1115 C
NN7=NCONA COPE1116 C
***** COPE1117
ARRAY STARTING LOCATIONS COPE1118 C
***** COPE1119
X, VLB, VUB, DF, A, S, G1, G2, C, B, SCAL, ISC, IC, M51 COPE1120 C
NX=1 COPE1121 C
NVLB=LOCR(2) COPE1122 C
NVUB=LOCR(3) COPE1123 C
NNSCAL=LOCR(4) COPE1124 C
NDF=LOCR(23) COPE1125 C
NG=NDF*NN1 COPE1126 C
NA=NG*NN2 COPE1127 C
NS=NA*NN1*NN3 COPE1128 C
NG1=NS*NN1 COPE1129 10
NG2=NG1*NN2 COPE1130 C
NC=NG2*NN2 COPE1131 C
NB=NC*NN4 COPE1132 C
NISC=LOCI(4) COPE1133 C
NIC=LOCI(23) COPE1134

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MNS1=NIC*NN3 COPE1135
AMULT, BLU, IDSGN, NSDGN, ICON COPE1136
NAMULT=LOCR(5) COPE1137
NBLU=LOCR(6) COPE1138
NIDSGN=1 COPE1139
NNSDGN=LOCI(2) COPE1140
NICCN=LOCI(3) COPE1141
----- COPE1142
OPTIMIZATION COPE1143
----- COPE1144
IGOTO=0 COPE1145
CALL COMMIN (X,VLB,VUB,G,SCAL,DF,A,S,G1,G2,B,C,ISC,IC,M51,NI,N2,N3COPE1146
*,N4,N5) COPE1147 C
CONTINUE COPE1148
CALL COMMIN (RA(NX),RA(NVLB),RA(NVUB),RA(NG),RA(NNSCAL),RA(NDF),RA(NDF1),RA(NDF2),RA(NDF3),RA(NDF4),RA(NDF5),RA(NDF6),RA(NDF7),RA(NDF8),RA(NDF9),RA(NDF10),RA(NDF11),RA(NDF12),RA(NDF13),RA(NDF14),RA(NDF15),RA(NDF16),RA(NDF17),RA(NDF18),RA(NDF19),RA(NDF20),RA(NDF21),RA(NDF22),RA(NDF23),RA(NDF24),RA(NDF25),RA(NDF26),RA(NDF27),RA(NDF28),RA(NDF29),RA(NDF30),RA(NDF31),RA(NDF32),RA(NDF33),RA(NDF34),RA(NDF35),RA(NDF36),RA(NDF37),RA(NDF38),RA(NDF39),RA(NDF40),RA(NDF41),RA(NDF42),RA(NDF43),RA(NDF44),RA(NDF45),RA(NDF46),RA(NDF47),RA(NDF48),RA(NDF49),RA(NDF50),RA(NDF51),RA(NDF52),RA(NDF53),RA(NDF54),RA(NDF55),RA(NDF56),RA(NDF57),RA(NDF58),RA(NDF59),RA(NDF60),RA(NDF61),RA(NDF62),RA(NDF63),RA(NDF64),RA(NDF65),RA(NDF66),RA(NDF67),RA(NDF68),RA(NDF69),RA(NDF70),RA(NDF71),RA(NDF72),RA(NDF73),RA(NDF74),RA(NDF75),RA(NDF76),RA(NDF77),RA(NDF78),RA(NDF79),RA(NDF80),RA(NDF81),RA(NDF82),RA(NDF83),RA(NDF84),RA(NDF85),RA(NDF86),RA(NDF87),RA(NDF88),RA(NDF89),RA(NDF90),RA(NDF91),RA(NDF92),RA(NDF93),RA(NDF94),RA(NDF95),RA(NDF96),RA(NDF97),RA(NDF98),RA(NDF99),RA(NDF100),RA(NDF101),RA(NDF102),RA(NDF103),RA(NDF104),RA(NDF105),RA(NDF106),RA(NDF107),RA(NDF108),RA(NDF109),RA(NDF110),RA(NDF111),RA(NDF112),RA(NDF113),RA(NDF114),RA(NDF115),RA(NDF116),RA(NDF117),RA(NDF118),RA(NDF119),RA(NDF120),RA(NDF121),RA(NDF122),RA(NDF123),RA(NDF124),RA(NDF125),RA(NDF126),RA(NDF127),RA(NDF128),RA(NDF129),RA(NDF130),RA(NDF131),RA(NDF132),RA(NDF133),RA(NDF134),RA(NDF135),RA(NDF136),RA(NDF137),RA(NDF138),RA(NDF139),RA(NDF140),RA(NDF141),RA(NDF142),RA(NDF143),RA(NDF144),RA(NDF145),RA(NDF146),RA(NDF147),RA(NDF148),RA(NDF149),RA(NDF150),RA(NDF151),RA(NDF152),RA(NDF153),RA(NDF154),RA(NDF155),RA(NDF156),RA(NDF157),RA(NDF158),RA(NDF159),RA(NDF160),RA(NDF161),RA(NDF162),RA(NDF163),RA(NDF164),RA(NDF165),RA(NDF166),RA(NDF167),RA(NDF168),RA(NDF169),RA(NDF170),RA(NDF171),RA(NDF172),RA(NDF173),RA(NDF174),RA(NDF175),RA(NDF176),RA(NDF177),RA(NDF178),RA(NDF179),RA(NDF180),RA(NDF181),RA(NDF182),RA(NDF183),RA(NDF184),RA(NDF185),RA(NDF186),RA(NDF187),RA(NDF188),RA(NDF189),RA(NDF190),RA(NDF191),RA(NDF192),RA(NDF193),RA(NDF194),RA(NDF195),RA(NDF196),RA(NDF197),RA(NDF198),RA(NDF199),RA(NDF200),RA(NDF201),RA(NDF202),RA(NDF203),RA(NDF204),RA(NDF205),RA(NDF206),RA(NDF207),RA(NDF208),RA(NDF209),RA(NDF210),RA(NDF211),RA(NDF212),RA(NDF213),RA(NDF214),RA(NDF215),RA(NDF216),RA(NDF217),RA(NDF218),RA(NDF219),RA(NDF220),RA(NDF221),RA(NDF222),RA(NDF223),RA(NDF224),RA(NDF225),RA(NDF226),RA(NDF227),RA(NDF228),RA(NDF229),RA(NDF230),RA(NDF231),RA(NDF232),RA(NDF233),RA(NDF234),RA(NDF235),RA(NDF236),RA(NDF237),RA(NDF238),RA(NDF239),RA(NDF240),RA(NDF241),RA(NDF242),RA(NDF243),RA(NDF244),RA(NDF245),RA(NDF246),RA(NDF247),RA(NDF248),RA(NDF249),RA(NDF250),RA(NDF251),RA(NDF252),RA(NDF253),RA(NDF254),RA(NDF255),RA(NDF256),RA(NDF257),RA(NDF258),RA(NDF259),RA(NDF260),RA(NDF261),RA(NDF262),RA(NDF263),RA(NDF264),RA(NDF265),RA(NDF266),RA(NDF267),RA(NDF268),RA(NDF269),RA(NDF270),RA(NDF271),RA(NDF272),RA(NDF273),RA(NDF274),RA(NDF275),RA(NDF276),RA(NDF277),RA(NDF278),RA(NDF279),RA(NDF280),RA(NDF281),RA(NDF282),RA(NDF283),RA(NDF284),RA(NDF285),RA(NDF286),RA(NDF287),RA(NDF288),RA(NDF289),RA(NDF290),RA(NDF291),RA(NDF292),RA(NDF293),RA(NDF294),RA(NDF295),RA(NDF296),RA(NDF297),RA(NDF298),RA(NDF299),RA(NDF300),RA(NDF301),RA(NDF302),RA(NDF303),RA(NDF304),RA(NDF305),RA(NDF306),RA(NDF307),RA(NDF308),RA(NDF309),RA(NDF310),RA(NDF311),RA(NDF312),RA(NDF313),RA(NDF314),RA(NDF315),RA(NDF316),RA(NDF317),RA(NDF318),RA(NDF319),RA(NDF320),RA(NDF321),RA(NDF322),RA(NDF323),RA(NDF324),RA(NDF325),RA(NDF326),RA(NDF327),RA(NDF328),RA(NDF329),RA(NDF330),RA(NDF331),RA(NDF332),RA(NDF333),RA(NDF334),RA(NDF335),RA(NDF336),RA(NDF337),RA(NDF338),RA(NDF339),RA(NDF340),RA(NDF341),RA(NDF342),RA(NDF343),RA(NDF344),RA(NDF345),RA(NDF346),RA(NDF347),RA(NDF348),RA(NDF349),RA(NDF350),RA(NDF351),RA(NDF352),RA(NDF353),RA(NDF354),RA(NDF355),RA(NDF356),RA(NDF357),RA(NDF358),RA(NDF359),RA(NDF360),RA(NDF361),RA(NDF362),RA(NDF363),RA(NDF364),RA(NDF365),RA(NDF366),RA(NDF367),RA(NDF368),RA(NDF369),RA(NDF370),RA(NDF371),RA(NDF372),RA(NDF373),RA(NDF374),RA(NDF375),RA(NDF376),RA(NDF377),RA(NDF378),RA(NDF379),RA(NDF380),RA(NDF381),RA(NDF382),RA(NDF383),RA(NDF384),RA(NDF385),RA(NDF386),RA(NDF387),RA(NDF388),RA(NDF389),RA(NDF390),RA(NDF391),RA(NDF392),RA(NDF393),RA(NDF394),RA(NDF395),RA(NDF396),RA(NDF397),RA(NDF398),RA(NDF399),RA(NDF400),RA(NDF401),RA(NDF402),RA(NDF403),RA(NDF404),RA(NDF405),RA(NDF406),RA(NDF407),RA(NDF408),RA(NDF409),RA(NDF410),RA(NDF411),RA(NDF412),RA(NDF413),RA(NDF414),RA(NDF415),RA(NDF416),RA(NDF417),RA(NDF418),RA(NDF419),RA(NDF420),RA(NDF421),RA(NDF422),RA(NDF423),RA(NDF424),RA(NDF425),RA(NDF426),RA(NDF427),RA(NDF428),RA(NDF429),RA(NDF430),RA(NDF431),RA(NDF432),RA(NDF433),RA(NDF434),RA(NDF435),RA(NDF436),RA(NDF437),RA(NDF438),RA(NDF439),RA(NDF440),RA(NDF441),RA(NDF442),RA(NDF443),RA(NDF444),RA(NDF445),RA(NDF446),RA(NDF447),RA(NDF448),RA(NDF449),RA(NDF450),RA(NDF451),RA(NDF452),RA(NDF453),RA(NDF454),RA(NDF455),RA(NDF456),RA(NDF457),RA(NDF458),RA(NDF459),RA(NDF4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	X(1)=XSAV2	COPE1195	SUBROUTINE COPE04 (ARRAY,HARRAY,SENS,NSENSZ,ISENS,HSENS,TEMP,NH8,HCOPE1255
20	CONTINUE	COPE1196	1N9,NH10,RA,IA,NDRA,NDTA) COPE1256
C	-----	COPE1197	COMMON /COPE51/ TITLE(20) COPE1257
C	TRANSFER DESIGN VARIABLES TO USER APRAY	COPE1198	COMMON /COPE53/ SGHOPT,NCALC,IOBJ,HSV,NSOBJ,HCONA,N2VX,H2VY,HCOPE1258
C	-----	COPE1199	12VY,H2VAR,IPSENS,IP2VAR,IPDBG,HACHX1,MDVTOT,LOCR(25),LOCI(25),ISCRCOPE1259
	N5=LOCR(5)	COPE1200	21,ISCP2,NXAPRX,NPS,NPFS,NPA,NF,INOM,IPAPRX,KMIN,KMAX,XFACT1,XFACT2COPE1260
	M2=LOCI(2)	COPE1201	3,NAH2,NAH3,NPMAX,NPTOT,JHOM,MAXTRM COPE1261
	DO 30 I=1,HDVTOT	COPE1202	COMMON /CHMN1/ DELFUN,DABFUN,FDCH,FDCHM,CT,CTHIN,CTL,CTLMIN,ALPHAXCOPE1262
	N=NDSGN(I)	COPE1203	1,ABOBJ1,THETA,OBJ,NOV,NCON,HSDIE,IPRINT,NFDG,HSCAL,LINOBJ,ITMAX,ITCOPE1263
	M=IDSGN(I)	COPE1204	2PH,ICHDIR,IGOTO,HAC,INFO,INFOG,ITER COPE1264
	IF (N.GT.0) ARRAY(M)=X(N)*AMULT(I)	COPE1205	DIMENSION ARRAY(HARRAY), SENS(NH8), NSENSZ(NH9), ISENS(NH10), NSENCOPE1265
30	CONTINUE	COPE1206	1S(NH10), TEMP(1), RA(NDRA), IA(NDIA) COPE1266
C	-----	COPE1207	*****COPE1267
C	ANALIZE	COPE1208	ROUTINE TO PROVIDE SENSITIVITY INFORMATION WITH RESPECT TO COPE1268
C	-----	COPE1209	A PRESCRIBED SET OF DESIGN VARIABLES. COPE1269
	ICALC=2	COPE1210	*****COPE1270
	NAH2=NAH2+1	COPE1211	BY G. N. VANDERPLAATS MAR., 1973. COPE1271
	CALL ANALIZ (ICALC)	COPE1212	STORE OUTPUT ON UNIT ISCR1. COPE1272
C	SAVE X(1).	COPE1213	REWIND ISCP1 COPE1273
	XSAV1=X(1)	COPE1214	IF (IPDBG.LT.1) IPRINT=0 COPE1274
C	-----	COPE1215	-----
C	OBJECTIVE	COPE1216	WRITE BASIC INFORMATION ON UNIT ISCR1 COPE1275
C	-----	COPE1217	-----
40	CONTINUE	COPE1218	TITLE. COPE1278
	OBJ=-SGHOPT*ARRAY(IOBJ)	COPE1219	WRITE (ISCR1,330) (TITLE(I),I=1,20) COPE1279
	IF (NCONA.EQ.0) RETURN	COPE1220	NCALC, HSV, NSOBJ COPE1280
C	-----	COPE1221	WRITE (ISCR1,340) NCALC,NSV,NSOBJ COPE1281
C	CONSTRAINT VALUES	COPE1222	ISENS(I),I=1,HSV. COPE1282
C	-----	COPE1223	WRITE (ISCR1,340) (ISENS(I),I=1,NSV) COPE1283
	J=1	COPE1224	NSENSZ(I),I=1,NSOBJ. COPE1284
	N=0	COPE1225	WRITE (ISCR1,340) (NSENSZ(I),I=1,NSOBJ) COPE1285
C	DO 60 I=1,NCONA	COPE1226	JCALC=3 COPE1286
	PARAMETER IDENTIFIER.	COPE1227	ICALC=2 COPE1287
	NH=ICON(I)	COPE1228	NDVSAV=HDV COPE1288
	CC=ARRAY(NH)	COPE1229	-----
C	LOWER BOUND.	COPE1230	***** NOMINAL *****COPE1290
	BB=BLU(1,I)	COPE1231	-----
	IF (BB.LT.-1.0E+15) GO TO 50	COPE1232	IF (NCALC.EQ.5) GO TO 10 COPE1292
C	NORMALIZATION FACTOR.	COPE1233	STANDARD SENSITIVITY. COPE1293
	C1=BLU(2,I)	COPE1234	NAH2=NAH2+1 COPE1294
C	CONSTRAINT VALUE.	COPE1235	CALL ANALIZ (ICALC) COPE1295
	N=N+1	COPE1236	IF (IPSENS.GT.0) NAH3=NAH3+1 COPE1296
	G(N)=(BB-CC)/C1	COPE1237	IF (IPSENS.GT.0) CALL ANALIZ (JCALC) COPE1297
C	UPPER BOUND.	COPE1238	GO TO 130 COPE1298
50	BB=BLU(3,I)	COPE1239	CONTINUE COPE1299
C	NORMALIZATION FACTOR.	COPE1240	OPTIMUM SENSITIVITY. COPE1300
	C1=BLU(4,I)	COPE1241	SAVE X, VLB, VUB AND SCAL IN TEMPORARY STORAGE. COPE1301
	J=J+4	COPE1242	N=4*HDV*8 COPE1302
	IF (BB.GT.1.0E+15) GO TO 60	COPE1243	L=LOCR(24) COPE1303
C	CONSTRAINT VALUE.	COPE1244	DO 20 I=1,N COPE1304
	N=N+1	COPE1245	RA(L)=RA(I) COPE1305
	G(N)=(CC-BB)/C1	COPE1246	L=L+1 COPE1306
60	CONTINUE	COPE1247	SAVE IDSGN AND HDGDN IN TEMPORARY STORAGE. COPE1307
	RETURN	COPE1248	N=2*HDVTOT COPE1308
C	-----	COPE1249	L=LOCI(24) COPE1309
C	FORMATS	COPE1250	DO 30 I=1,N COPE1310
C	-----	COPE1251	IA(L)=IA(I) COPE1311
	FORMAT (1H1)	COPE1252	L=L+1 COPE1312
70	END	COPE1253	SHIFT DESIGN VARIABLE INFORMATION IF ANY SENSITIVITY VARIABLE IS COPE1313
		COPE1254	ALSO A DESIGN VARIABLE. COPE1314


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NDV2=NDV+2
00 90 I=1,NSV
C GLOBAL SENSITIVITY VARIABLE LOCATION.
N=ISENS(I)
C IS THIS ALSO A DESIGN VARIABLE.
M2=LOCI(2)
DO 40 J=1,NDVTOT
L=IA(J)
IF (L.EQ.N) GO TO 50
40 M2=M2+1
C SENSITIVITY VARIABLE IS NOT A DESIGN VARIABLE.
GO TO 90
50 CONTINUE
C SENSITIVITY VARIABLE IS ALSO A DESIGN VARIABLE.
NDV=NDV+1
IDV=IA(M2)
C ELIMINATE THIS DESIGN VARIABLE AND REDUCE HIGHER NUMBER DESIGN
C VARIABLES BY ONE.
M2=LOCI(2)
DO 70 J=1,NDVTOT
IF (IA(M2).NE.IDV) GO TO 60
IA(M2)=0
C SET DESIGN VARIABLE VALUES TO SENSITIVITY VARIABLE VALUE.
K=IA(J)
M5=LOCR(5)+J-1
ARRAY(K)=ARRAY(N)*RA(M5)
60 CONTINUE
IF (IA(M2).GT.IDV) IA(M2)=IA(M2)-1
70 M2=M2+1
IF (IDV.EQ.NDV) GO TO 90
C SHIFT X, VLB, VUB AND SCAL.
DO 80 J=IDV,NDV
C X.
RA(J)=RA(J+1)
C VLB.
K=J+NDV2
RA(K)=RA(K+1)
C VUB.
K=K+NDV2
RA(K)=RA(K+1)
C SCAL.
K=K+NDV2
80 RA(K)=RA(K+1)
90 CONTINUE
NAN2=NAN2+1
CALL ANALIZ (ICALC)
IF (NDV.LE.0) GO TO 100
CALL COPE02 (ARRAY,RA,IA,NARRAY,NDRA,NDIA)
100 CONTINUE
IF (IPSENS.GT.0) NAN3=NAN3+1
IF (IPSENS.GT.0) CALL ANALIZ (JCALC)
C PUT X, VLB, VUB AND SCAL BACK.
L=LOCR(24)
M=4*NDVSAV*8
DO 110 I=1,N
RA(I)=RA(L)
110 L=L+1
C PUT IDSGN AND HDSGH BACK.
M=2*NDVTOT
L=LOCI(24)

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COPE1315 DO 120 I=1,N
COPE1316 JA(I)=IA(L)
COPE1317 L=L+1
COPE1318 120 CONTINUE
COPE1319 130
C -----
COPE1320 WRITE NOMINAL RESULTS ON UNIT ISCR1
COPE1321 C -----
COPE1322 SENS(I,1).
COPE1323 M=1
COPE1324 DO 140 I=1,NSV
COPE1325 TEMP(I)=SENS(M)
COPE1326 140 M=M+NSENS(I)
COPE1327 WRITE (ISCR1,350) (TEMP(I),I=1,NSV)
COPE1328 SENSITIVITY OBJECTIVES, OBJZ.
COPE1329 DO 150 I=1,NSOBJ
COPE1330 M=NSENSZ(I)
COPE1331 150 TEMP(I)=ARRAY(M)
COPE1332 WRITE (ISCR1,350) (TEMP(I),I=1,NSOBJ)
COPE1333 C -----
COPE1334 ***** SENSITIVITIES *****
COPE1335 C -----
COPE1336 NSVAL=0
COPE1337 DO 320 II=1,NSV
COPE1338 C GLOBAL LOCATION OF SENSITIVITY VARIABLE.
COPE1339 ISENSV=ISENS(II)
COPE1340 C NUMBER OF SENSITIVITY VARIABLES, HSENSV.
COPE1341 NSENSV=NSENS(II)
COPE1342 C WRITE ISEHSV AND HSENSV-1 ON UNIT ISCR1.
COPE1343 NSENSI=NSENSV-1
COPE1344 WRITE (ISCR1,340) ISENSV,NSENSI
COPE1345 IF (HSENSV.LE.1) GO TO 320
COPE1346 ID1=0
COPE1347 IF (HCALC.NE.5) GO TO 210
COPE1348 C IS THIS SENSITIVITY VARIABLE ALSO A DESIGN VARIABLE.
COPE1349 NDV=NDVSAV
COPE1350 DO 160 I=1,NDVTOT
COPE1351 JJ=I
COPE1352 IF (IA(I).EQ.ISEHSV) GO TO 170
COPE1353 160 CONTINUE
COPE1354 C ISEHSV IS NOT A DESIGN VARIABLE.
COPE1355 GO TO 210
COPE1356 170 CONTINUE
COPE1357 C ISENSV IS A DESIGN VARIABLE. MODIFY OPTIMIZATION INFORMATION.
COPE1358 HDV2=NDV+2
COPE1359 NDV=NDV-1
COPE1360 C SAVE X, VLB, VUB AND SCAL FOR THIS DESIGN VARIABLE AND SHIFT
COPE1361 C REMAINING VARIABLES.
COPE1362 C SAVE.
COPE1363 M2=LOCI(2)+JJ-1
COPE1364 ID1=IA(M2)
COPE1365 SAVX=RA(ID1)
COPE1366 K=ID1+NDV2
COPE1367 SAVL=RA(K)
COPE1368 K=K+NDV2
COPE1369 SAVU=RA(K)
COPE1370 K=K+NDV2
COPE1371 SAVS=RA(K)
COPE1372 C SHIFT
COPE1373 IF (ID1.GT.NDV) GO TO 190
COPE1374 DO 120 I=ID1,NDV
COPE1375
COPE1376
COPE1377
COPE1378
COPE1379
COPE1380
COPE1381
COPE1382
COPE1383
COPE1384
COPE1385
COPE1386
COPE1387
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COPE1432
COPE1433
COPE1434

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	RA(I)=RA(I+1)	COPE1435	WRITE (ISCR1,350) (TEMP(I),I=1,NSOBJ)	COPE1495
	K=I+NDV2	COPE1436	280 CONTINUE	COPE1496
	RA(K)=RA(K+1)	COPE1437	ARRAY (ISCR1,NSV)=SENS(NSVALN)	COPE1497
	K=K+NDV2	COPE1438	IF (NCALC.NE.5.OR.ID1.EQ.0) GO TO 320	COPE1498
	RA(K)=RA(K+1)	COPE1439	C RESTORE X, VLB, VUB AND SCAL.	COPE1499
	K=K+NDV2	COPE1440	NDV=NDVSAV	COPE1500
180	RA(K)=RA(K+1)	COPE1441	IF (ID1.EQ.NDV) GO TO 300	COPE1501
190	CONTINUE	COPE1442	L=NDV-1	COPE1502
C	MODIFY NDSGN.	COPE1443	L1=L	COPE1503
	M2=LOCII(2)	COPE1444	DO 290 I=ID1,L1	COPE1504
	DO 200 I=1,NDVTOT	COPE1445	RA(L+1)=RA(L)	COPE1505
	IF (IA(M2).EQ.ID1) IA(M2)=0	COPE1446	K=L+NDV2	COPE1506
	IF (IA(M2).GT.ID1) IA(M2)=IA(M2)-1	COPE1447	RA(K+1)=RA(K)	COPE1507
200	M2=M2+1	COPE1448	K=K+NDV2	COPE1508
210	CONTINUE	COPE1449	RA(K+1)=PA(K)	COPE1509
C	-----	COPE1450	K=K+NDV2	COPE1510
C	VARY THE VALUE OF THE SENSITIVITY PARAMETER	COPE1451	RA(K+1)=RA(K)	COPE1511
C	-----	COPE1452	290 L=L-1	COPE1512
	NSVAL1=NSVAL1+1	COPE1453	RA(ID1)=SAVX	COPE1513
	NSVALN=NSVAL1	COPE1454	K=ID1+NDV2	COPE1514
	DO 200 JJ=2,NSNSV	COPE1455	RA(K)=SAVL	COPE1515
	NSVAL1=NSVAL1+1	COPE1456	K=K+NDV2	COPE1516
	ARRAY (ISENSV)=SENS(NSVAL1)	COPE1457	RA(K)=SAVU	COPE1517
C	WRITE SENS(I,J) ON UNIT ISCR1.	COPE1458	K=K+NDV2	COPE1518
	WRITE (ISCR1,350) SENS(NSVAL1)	COPE1459	RA(K)=SAVS	COPE1519
C	ANALIZE.	COPE1460	300 CONTINUE	COPE1520
	IF (NCALC.EQ.5) GO TO 220	COPE1461	C RESTORE NDSGN.	COPE1521
C	STANDARD SENSITIVITY.	COPE1462	M2=LOCII(2)	COPE1522
	NAN2=NAN2+1	COPE1463	DO 310 I=1,NDVTOT	COPE1523
	CALL ANALIZ (ICALC)	COPE1464	IF (IA(M2).GE.ID1) IA(M2)=IA(M2)+1	COPE1524
	IF (IPSENS.GT.0) NAN3=NAN3+1	COPE1465	IF (IA(M2).EQ.0) IA(M2)=ID1	COPE1525
	IF (IPSENS.GT.0) CALL ANALIZ (JCALC)	COPE1466	310 M2=M2+1	COPE1526
	GO TO 260	COPE1467	320 CONTINUE	COPE1527
220	CONTINUE	COPE1468	RETURN	COPE1528
C	OPTIMUM SENSITIVITY.	COPE1469	-----	COPE1529
	IF (NDV.EQ.NDVSAV) GO TO 240	COPE1470	FORMATS	COPE1530
C	SET LINKED DESIGN VARIABLE VALUES TO PRESCRIBED VALUE.	COPE1471	-----	COPE1531
	M2=LOCII(2)	COPE1472	330 FORMAT (20A4)	COPE1532
	DO 230 I=1,NDVTOT	COPE1473	340 FORMAT (16I5)	COPE1533
	IF (IA(M2).NE.0) GO TO 230	COPE1474	350 FORMAT (5E15.8)	COPE1534
	L=IA(I)	COPE1475	END	COPE1535
	M5=LOCRI(5)+I-1	COPE1476	SUBROUTINE COPE05 (RA,IA,NDRA,NDIA,ISCR1)	COPE1536
	ARRAY (L)=ARRAY (ISENSV)*RA(M5)	COPE1477	DIMENSION RA(NDRA), IA(NDIA)	COPE1537
230	M2=M2+1	COPE1478	C *****	COPE1538
240	CONTINUE	COPE1479	C ROUTINE TO PRINT SENSITIVITY INFORMATION STORED ON UNIT ISCR1.	COPE1539
	NAN2=NAN2+1	COPE1480	C *****	COPE1540
	CALL ANALIZ (ICALC)	COPE1481	C BY G. N. VANDERPLAATS	COPE1541
	IF (NDV.LE.0) GO TO 250	COPE1482	C NASA-AMES RESEARCH CENTER, HOFFETT FIELD, CALIF.	COPE1542
	CALL COPE02 (ARRAY,RA,IA,NARRAY,NDRA,NDIA)	COPE1483	C REMIND ISCR1	COPE1543
250	CONTINUE	COPE1484	-----	COPE1544
	IF (IPSENS.GT.0) NAN3=NAN3+1	COPE1485	GENERAL INFORMATION	COPE1545
	IF (IPSENS.GT.0) CALL ANALIZ (JCALC)	COPE1486	-----	COPE1546
260	CONTINUE	COPE1487	C TITLE.	COPE1547
C	-----	COPE1488	READ (ISCR1,70) (RA(I),I=1,20)	COPE1548
C	WRITE SENSITIVITY RESULTS ON UNIT ISCR1	COPE1489	C NCALC, NSV, NSOBJ	COPE1549
C	-----	COPE1490	READ (ISCR1,80) NCALC,NSV,NSOBJ	COPE1550
-C	OBJZ.	COPE1491	IF (NCALC.NE.3.AND.NCALC.NE.5) RETURN	COPE1551
	DO 270 I=1,NSOBJ	COPE1492	IF (NCALC.EQ.3) WRITE (6,90)	COPE1552
	M=HSENSZ(I)	COPE1493	IF (NCALC.EQ.5) WRITE (6,50)	COPE1553
270	TEMP(I)=ARRAY(M)	COPE1494	WRITE (6,60) (PA(I),I=1,20)	COPE1554

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C WRITE (6,100) NSV,NSOBJ COPE1555 1ES) COPE1615
C ISENS(I),I=1,NSV. COPE1556 120 FORMAT (5X,1015) COPE1616
C READ (ISCR1,80) (IA(I),I=1,NSV) COPE1557 130 FORMAT (//5X,53HGLOBAL NUMBERS ASSOCIATED WITH SENSITIVITY OBJECTIVE COPE1617
C WRITE (6,110) COPE1558 COPE1558 COPE1618
C WRITE (6,120) (IA(I),I=1,NSV) COPE1559 140 FORMAT (5E15.8) COPE1619
C NSENSZ(I),I=1,NSOBJ. COPE1560 150 FORMAT (////5X,26HNOMINAL DESIGN INFORMATION//5X,31HVALUES OF SENSITIVITY COPE1620
C READ (ISCR1,80) (IA(I),I=1,NSOBJ) COPE1561 COPE1561 COPE1621
C WRITE (6,130) COPE1562 160 FORMAT (5X,5E13.5) COPE1622
C WRITE (6,120) (IA(I),I=1,NSOBJ) COPE1563 170 FORMAT (//5X,41HVALUES OF SENSITIVITY OBJECTIVE FUNCTIONS) COPE1623
C ----- COPE1564 180 FORMAT (////5X,28HSENSITIVITY ANALYSIS RESULTS) COPE1624
C NOMINAL INFORMATION COPE1565 190 FORMAT (//5X,15HGLOBAL VARIABLE,I5//10X,1HX,20X,4HF(X)) COPE1625
C ----- COPE1566 200 FORMAT (1/5X,35HTHE NOMINAL VALUE IS THE ONLY VALUE//5X,27HSPECIFIED COPE1626
C SENS(I),I=1,NSV. COPE1567 COPE1567 COPE1627
C READ (ISCR1,140) (RA(I),I=1,NSV) COPE1568 210 FORMAT (1/3X,E12.4,3X,4E13.4) COPE1628
C WRITE (6,150) COPE1569 220 FORMAT (18X,4E13.4) COPE1629
C WRITE (6,160) (RA(I),I=1,NSV) COPE1570 COPE1570 COPE1630
C OBJZ(I),I=1,NSOBJ. COPE1571 COPE1571 COPE1631
C READ (ISCR1,140) (RA(I),I=1,NSOBJ) COPE1572 COPE1572 COPE1632
C WRITE (6,170) COPE1573 COPE1573 COPE1633
C WRITE (6,160) (RA(I),I=1,NSOBJ) COPE1574 COPE1574 COPE1634
C ----- COPE1575 COPE1575 COPE1635
C ***** SENSITIVITY INFORMATION ***** COPE1576 COPE1576 COPE1636
C ----- COPE1577 COPE1577 COPE1637
C WRITE (6,180) COPE1578 C ***** COPE1638
C DO 40 ISENS=1,NSV COPE1579 C ROUTINE TO CALCULATE FUNCTIONS OF TWO DESIGN VARIABLES FOR ALL COPE1639
C ISENSI, NSENSI COPE1580 C COMBINATIONS OF A SET OF PRESCRIBED VALUES OF THESE VARIABLES. COPE1640
C READ (ISCR1,80) ISENSI,NSENSI COPE1581 C ***** COPE1641
C WRITE (6,190) ISENSI COPE1582 C WRITE OUTPUT INFORMATION ON SCRATCH UNIT ISCR1. COPE1642
C IF (NSENSI.EQ.0) WRITE (6,200) COPE1583 C BY G. N. VANDERPLAATS AUG., 1974. COPE1643
C IF (NSENSI.EQ.0) GO TO 40 COPE1584 C NASA-AMES RESEARCH CENTER, HOFFETT FIELD, CALIF. COPE1644
C DO 30 JJ=1,NSENSI COPE1585 C REWIHD ISCR1 COPE1645
C SENS(I,J). COPE1586 C ----- COPE1646
C READ (ISCR1,140) SENSIJ COPE1587 C UNIT ISCR1 WRITE COPE1647
C OBJZ(I),I=1,NSOBJ. COPE1588 C ----- COPE1648
C READ (ISCR1,140) (RA(I),I=1,NSOBJ) COPE1589 COPE1589 COPE1649
C N=MIN0(4,NSOBJ) COPE1590 COPE1590 COPE1650
C WRITE (6,210) SENSIJ,(RA(I),I=1,N) COPE1591 C NCVZ. COPE1651
C N=(NSOBJ-1)/4 COPE1592 COPE1592 COPE1652
C IF (N.LT.1) GO TO 20 COPE1593 COPE1593 COPE1653
C L1=5 COPE1594 COPE1594 COPE1654
C DO 10 I=1,N COPE1595 C ----- COPE1655
C L2=L1+3 COPE1596 C TWO-VARIABLE FUNCTION SPACE COPE1656
C L2=MIN0(L2,NSOBJ) COPE1597 C ----- COPE1657
C WRITE (6,220) (RA(J),J=L1,L2) COPE1598 COPE1598 COPE1658
C L1=L1+4 COPE1599 COPE1599 COPE1659
C 10 CONTINUE COPE1600 COPE1600 COPE1660
C 20 CONTINUE COPE1601 COPE1601 COPE1661
C 30 CONTINUE COPE1602 COPE1602 COPE1662
C 40 CONTINUE COPE1603 COPE1603 COPE1663
C RETURN COPE1604 COPE1604 COPE1664
C ----- COPE1605 COPE1605 COPE1665
C FORMATS COPE1606 COPE1606 COPE1666
C ----- COPE1607 COPE1607 COPE1667
C 50 FORMAT (1H1,4X,46HOPTIMUM SENSITIVITY ANALYSIS RESULTS (NCALC=5)) COPE1607 C ANALIZE. COPE1668
C 60 FORMAT (//5X,5HTITLE/5X,20A4) COPE1608 COPE1608 COPE1669
C 70 FORMAT (20A4) COPE1609 COPE1609 COPE1670
C 80 FORMAT (16I5) COPE1610 COPE1610 COPE1671
C 90 FORMAT (1H1,4X,47HSTANDARD SENSITIVITY ANALYSIS RESULTS (NCALC=3)) COPE1611 COPE1611 COPE1672
C 100 FORMAT (//5X,36HNUMBER OF SENSITIVITY VARIABLES, NSV,9X,1H=,I5/5X, COPE1612 COPE1612 COPE1673
C 139HNUMBER OF SENSITIVITY OBJECTIVES, NSOBJ,6X,1H=,I5) COPE1613 COPE1613 COPE1674
C 110 FORMAT (//5X,52HGLOBAL NUMBERS ASSOCIATED WITH SENSITIVITY VARIABLE COPE1614 C UNIT ISCR1 WRITE COPE1674

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C -----COPE1675
C WRITE X, Y. COPE1676
C WRITE (ISCR1,60) RA(N20),RA(N21) COPE1677
C F(X,Y) VALUES. COPE1678
N23=LOC(23) COPE1679
N24=N23 COPE1680
H20=LOCI(20) COPE1681
DO 10 K=1,N2VAR COPE1682
N=IA(N20) COPE1683
RA(N24)=ARRAY(N) COPE1684
N24=N24+1 COPE1685
N20=M20+1 COPE1686
10 CONTINUE COPE1687
N24=N23*N2VAR-1 COPE1688
WRITE (ISCR1,60) (RA(K),K=N23,N24) COPE1689
20 CONTINUE COPE1690
N21=N21+ISIGN COPE1691
N20=N20+1 COPE1692
ISIGN=-ISIGN COPE1693
30 CONTINUE COPE1694
RETURN COPE1695
C -----COPE1696
C FORMATS COPE1697
C -----COPE1698
C -----COPE1699
C -----COPE1700
C -----COPE1701
40 FORMAT (20A4) COPE1702
50 FORMAT (16I5) COPE1703
60 FORMAT (5E15.8) COPE1704
END COPE1705
SUBROUTINE COPE07 (RA,IA,NDRA,NDIA,ISCR1) COPE1706
DIMENSION RA(NDRA), IA(NDIA) COPE1707
*****COPE1708
ROUTINE TO PRINT TWO VARIABLE FUNCTION SPACE INFORMATION STORED ONCOPE1709
UNIT ISCR1. COPE1710
*****COPE1711
BY G. N. VANDERPLAATS AUG., 1974. COPE1712
NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COPE1713
REWIND ISCR1 COPE1714
C -----COPE1715
C GENERAL INFORMATION COPE1716
C -----COPE1717
C TITLE. COPE1718
C READ (ISCR1,60) (RA(I),I=1,20) COPE1719
C READ (ISCR1,70) NCALC,N2VAR,M2VX,M2VY,N2VY COPE1720
C IF (NCALC.NE.4.AND.NCALC.NE.6) RETURN COPE1721
C WRITE (6,50) COPE1722
C WRITE (6,40) (RA(I),I=1,20) COPE1723
C N2VZ(I),I=1,N2VAR. COPE1724
C READ (ISCR1,70) (IA(I),I=1,N2VAR) COPE1725
C N2VX, N2VY. COPE1726
C WRITE (6,120) N2VX,N2VY COPE1727
C N2VZ. COPE1728
C WRITE (6,130) COPE1729
C WRITE (6,80) (IA(I),I=1,N2VAR) COPE1730
C -----COPE1731
C TWO-VARIABLE FUNCTION SPACE INFORMATION COPE1732
C -----COPE1733
C DO 30 I=1,M2VX COPE1734
WRITE (6,140)
DO 30 J=1,M2VY
X, Y.
READ (ISCR1,150) XX,YY
F(X,Y).
READ (ISCR1,150) (RA(K),K=1,N2VAR)
N=4
IF (N2VAP.LT.4) N=N2VAR
IF (J.EQ.1) WRITE (6,100) XX,YY,(RA(K),K=1,N)
IF (J.GT.1) WRITE (6,90) YY,(RA(K),K=1,N)
IF (N.GE.N2VAR) GO TO 20
N=5
M=(N2VAR-1)/4
DO 10 K=1,M
L=N+3
IF (L.GT.N2VAR) L=N2VAR
WRITE (6,110) (RA(KK),KK=N,L)
N=L+1
CONTINUE
CONTINUE
RETURN
C -----COPE1756
C FORMATS COPE1757
C -----COPE1758
40 FORMAT (//5X,5HTITLE/5X,20A4) COPE1759
50 FORMAT (1H1,4X,35HTWO-VARIABLE FUNCTION SPACE RESULTS) COPE1760
60 FORMAT (20A4) COPE1761
70 FORMAT (16I5) COPE1762
80 FORMAT (5X,10I5) COPE1763
90 FORMAT (/15X,E12.4,3X,4E13.4) COPE1764
100 FORMAT (/3X,2E12.4,3X,4E13.4) COPE1765
110 FORMAT (30X,4E13.4) COPE1766
120 FORMAT (///5X,48HGLOBAL NUMBER ASSOCIATED WITH X-VARIABLE, N2VX =COPE1767
1,15//5X,48HGLOBAL NUMBER ASSOCIATED WITH Y-VARIABLE, N2VY =,15) COPE1768
130 FORMAT (//5X,37HGLOBAL NUMBERS ASSOCIATED WITH F(X,Y)) COPE1769
140 FORMAT (//10X,1HX,11X,1HY,20X,6HF(X,Y)) COPE1770
150 FORMAT (5E15.8) COPE1771
END COPE1772
SUBROUTINE COPE08 (A,B,IFORM,NFLD) COPE1773
DIMENSION A(1), B(1), C(10) COPE1774
DATA COMMA/1H,/,BLANK/1H / COPE1775
ROUTINE TO CONVERT UNFORMATTED DATA TO FORMATTED DATA IN FIELDS COPE1776
OF 10, EACH FIELD RIGHT JUSTIFIED. COPE1777
BY G. N. VANDERPLAATS AUG., 1978. COPE1778
NASA AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COPE1779
C --- INPUT. COPE1780
C A - ARRAY OF DATA SEPERATED BY COMMAS. MINIMUM DIMENSION OF COPE1781
IS A(80). COPE1782
C --- OUTPUT. COPE1783
C B - ARRAY OD DATA IN FIELDS OF 10 AND RIGHT JUSTIFIED. COPE1784
MINIMUM DIMENSION OF B IS 10*NFLD. COPE1785
C IFORM - 0 IF A WAS UNFORMATTED. COPE1786
1 IF A WAS ALLREADY FORMATTED. COPE1787
C NFLD - NUMBER OF FIELDS OF DATA. COPE1788
C --- NOTE. COPE1789
C 1) DATA IS ASSUMED TO BE REAL OR INTEGER DATA WITH NO EMBEDDED COPE1790
BLANKS WITHIN A GIVEN FIELD. COPE1791
C 2) DATA IS CONSIDERED UNFORMATTED IF COPE1792
A) A COMMA IS FOUND COPE1793
B) LAST NON-BLANK CHARACTER IS IN COLUMN 1-10 AND THERE IS COPE1794

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C          NO DECIMAL AND IT IS NOT RIGHT JUSTIFIED.
C
C          IFORM=0
C          SEARCH FOR LAST NON-BLANK CHARACTER AND SEARCH FOR COMMA.
C          CALCULATE NUMBER OF NON-BLANK SETS.
          INON=0
          KNON=0
          LST=0
          DO 10 I=1,80
          IF (A(I).EQ.COMMA) GO TO 20
          JNON=INON
          IF (A(I).EQ.BLANK) INON=0
          IF (A(I).NE.BLANK) INON=1
          IF (INON.GT.JNON) KNON=KNON+1
          IF (A(I).NE.BLANK) LST=I
10         CONTINUE
C          NO COMMA WAS FOUND. DATA MAY BE FORMATTED.
          IF (LST.GE.10) GO TO 90
C          IF MORE THAN ONE SETS OF CHARACTERS, DATA IS ASSUMED FORMATTED.
          IF (KNON.GT.1) GO TO 90
20         CONTINUE
C          DATA IS UNFORMATTED.
          K2=10
          NFLD=0
          I=0
30         CONTINUE
          I=I+1
          IF (I.GT.80) GO TO 110
C          IGNORE LEADING BLANKS.
          IF (A(I).EQ.BLANK) GO TO 30
C          CALCULATE NUMBER OF NON-BLANK CHARACTERS IN THIS FIELD.
          JJ=0
          DO 40 J=I,80
          IF (A(J).EQ.COMMA.OR.A(J).EQ.BLANK) GO TO 30
          JJ=JJ+1
40         C(JJ)=A(J)
50         NFLD=NFLD+1
          I=I+JJ
C          BLANK FIELD NFLD OF B.
          K1=K2-9
          DO 60 K=K1,K2
60         B(K)=BLANK
C          STORE C IN FIELD NFLD OF B, RIGHT JUSTIFIED.
          IF (JJ.EQ.0) GO TO 80
          J1=JJ
          K=K2
          DO 70 L=1,JJ
          B(K)=C(J1)
          K=K-1
70         J1=J1-1
80         K2=K2+10
          GO TO 30
90         CONTINUE
C          FORMATTED INPUT. STORE A DIRECTLY IN B.
          IFORM=1
          NFLD=8
          DO 100 I=1,80
100        B(I)=A(I)
110        CONTINUE
          RETURN

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END
SUBROUTINE COPE09
COMMON /CNMNI/ DELFUN,DABFUN,FOCH,FDCHM,CT,CTMIN,CTL,CTLMIN,ALPHAX
1,ABOBI,THETA,OBJ,NDV,NCON,NSIDE,IPRINT,NFDG,NSCAL,LINOBJ,ITHAX,ITCO
2RM,ICNDR,IGOTO,NAC,INFO,INFOG,ITER
COMMON /COPE52/ RA(5000),IA(1000)
COMMON /COPE53/ SGNOPT,NCALC,IOBJ,NSV,NSOBI,NCONA,N2VX,M2VY,N2VY,
12VY,N2VAR,IPSEHS,IP2VAR,IPDBG,NACHX1,NDVTOT,LOCR(25),LOCI(25),ISCR
21,ISCR2,NXAPRX,NPS,NPFS,NPA,NF,INOM,IPAPRX,KMIN,KMAX,XFACT1,XFACT2
3,NAN2,NAN3,NPMAX,NPTOT,JNOM,MAXTRM
COMMON /GLOBCH/ ARRAY(1500)
*****
ROUTINE TO DO APPROXIMATE OPTIMIZATION.
*****
BY G. N. VANDERPLAATS          JAN., 1979.
NASA AMES RESEARCH CENTER, MOFFETT FIELD, CALIF.
NFDGSV=NFDG
NFDG=1
IF (NFDGSV.LT.0) NFDG=0
CTMIN=ABS(CTMIN)
CTLMIN=ABS(CTLMIN)
IF (CTMIN.LE.0.) CTMIN=.0005
IF (CTLMIN.LE.0.) CTLMIN=.0001
IF (ABS(CT).LE.0.) CT=-.01
IF (ABS(CTLMIN).LE.0.) CTLMIN=-.0001
IF (DELFUN.LE.0.) DELFUN=.0001
IF (IPDBG.LT.1) IPRINT=0
IF (ITHAX.LT.50) ITHAX=50
NSIDE=1
KOUNT=0
-----
ARRAY STARTING LOCATIONS.
-----
NN1=NXAPRX*2
NXV=LOCR(23)
NVLB=NXV+NN1
NVUB=NVLB+NN1
NXNOM=NVUB+NN1
NDX=NXNOM+NXAPRX
NFNOM=NDX+NDV
NFNEM=NFNOM+NF
NBTAY=NFNEM+NF
NBR=NXAPRX*(NXAPRX*(NXAPRX+1))/2
IF (MAXTRM.LT.3) NBR=MAXTRM+NXAPRX
NTHP=NBTAY+NBR*NF
NBLU=LOCR(6)
NISC=LOCI(4)
NIGFN=LOCI(23)
NIDV=NIGFN+NCONA
IF (KMAX.LT.0) GO TO 160
COMMON ARRAYS.
DIMENSIONS.
NN1=NDV*2
NN2=2*NDV+NCON
NN3=NACHX1
NN4=NN3
IF (NDV.GT.NN4) NN4=NDV
NN5=2*NN4

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COPE1914

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C	SCAL, DF, G, A, S, G1, G2, C, B, ISC, IC, HSI.	COPE1915	C	THIS APPROXIMATING VARIABLE IS NOT A DESIGN VARIABLE.	COPE1975
	NNSCAL=LOC(4)	COPE1916		GO TO 90	COPE1976
	HDF=HIMP	COPE1917	80	CONTINUE	COPE1977
	HG=NDF*HN1	COPE1918	C	DESIGN VARIABLE NUMBER.	COPE1978
	HA=HG*HN2	COPE1919		IA(N3)=IA(H2)	COPE1979
	HS=HA*HN1*NN3	COPE1920	90	N3=N3+1	COPE1980
	HG1=NS*HN1	COPE1921	C	CHECK TO BE SUPE EACH INDEPENDENT DESIGN VARIABLE IS ALSO AN	COPE1981
	HG2=HG1*HN2	COPE1922	C	APPROXIMATING VARIABLE.	COPE1982
	NC=HG2*HN2	COPE1923		DO 120 I=1,NDV	COPE1983
	NB=NC*HN4	COPE1924		N1=LOC(I1)	COPE1984
	NISC=LOC(I4)	COPE1925		H2=LOC(I2)	COPE1985
	HIC=HIDV*HXAPRX	COPE1926		DO 110 J=1,NDVTOT	COPE1986
	HMS1=HIC*HN3	COPE1927	C	IS THIS DESIGN VARIABLE I.	COPE1987
C	-----	COPE1928	C	IF (IA(N2).NE.I) GO TO 110	COPE1988
C	DETERMINE IOBJA, ARRAYS IGFN AND IDV.	COPE1929	C	YES.	COPE1989
C	-----	COPE1930	C	GLOBAL VARIABLE NUMBER.	COPE1990
C	IOBJA.	COPE1931		IGLOB=IA(H1)	COPE1991
	M6=LOC(I6)	COPE1932		N1=N1+1	COPE1992
	DO 10 I=1,NF	COPE1933		N5=LOC(I5)	COPE1993
	J=IA(M6)	COPE1934		DO 100 K=1,HXAPRX	COPE1994
	IOBJA=I	COPE1935	C	IS THIS THE SAME AS IGLOB.	COPE1995
	IF (J.EQ.IOBJ) GO TO 20	COPE1936		IF (IA(N5).EQ.IGLOB) GO TO 120	COPE1996
10	M6=M6+1	COPE1937	C	NO.	COPE1997
C	ERROR - IOBJA NOT FOUND.	COPE1938	100	N5=N5+1	COPE1998
20	CONTINUE	COPE1939	110	N2=N2+1	COPE1999
	IF (NCONA.EQ.0) GO TO 60	COPE1940	C	ERROR - DESIGN VARIABLE IS NOT AN APPROXIMATING VARIABLE.	COPE2000
C	IGFN ARRAY.	COPE1941	120	CONTINUE	COPE2001
	M3=LOC(I3)	COPE1942	C	-----	COPE2002
	M23=LOC(I23)	COPE1943	C	BEGIN SEQUENTIAL APPROXIMATE OPTIMIZATION.	COPE2003
	DO 50 I=1,NCONA	COPE1944	C	-----	COPE2004
C	GLOBAL LOCATIONS OF CONSTRAINED PARAMETERS.	COPE1945		ICK1=0	COPE2005
	J=IA(M3)	COPE1946		ICK2=0	COPE2006
	M3=M3+1	COPE1947		ICK3=0	COPE2007
C	LOCAL VARIABLE, F, LOCATION.	COPE1948	130	CONTINUE	COPE2008
	M6=LOC(I6)	COPE1949		KOUNT=KOUNT+1	COPE2009
	DO 30 K=1,NF	COPE1950		IF (IPAPRX.LT.1.OR.IPAPRX.EQ.3) GO TO 160	COPE2010
	KK=K	COPE1951		IF (KMAX.LT.0) GO TO 160	COPE2011
	L=IA(M6)	COPE1952	C	PRINT INITIAL INFORMATION.	COPE2012
	IF (L.EQ.J) GO TO 40	COPE1953	C	TITLE.	COPE2013
30	M6=M6+1	COPE1954		IF (KOUNT.GT.1) GO TO 150	COPE2014
C	ERROR - CONSTRAINED VARIABLE IS NOT AN APPROXIMATE FUNCTION.	COPE1955		WRITE (6,670)	COPE2015
40	CONTINUE	COPE1956	C	OBJECTIVE FUNCTION.	COPE2016
	IA(M23)=KK	COPE1957		WRITE (6,550) IOBJA	COPE2017
50	M23=M23+1	COPE1958		IF (NCONA.EQ.0) GO TO 140	COPE2018
60	CONTINUE	COPE1959	C	CONSTRAINTS.	COPE2019
C	IDV ARRAY.	COPE1960		WRITE (6,560)	COPE2020
	H3=HIDV	COPE1961		N1=NIGFH	COPE2021
	N5=LOC(I5)	COPE1962		N2=N1+NCONA-1	COPE2022
	DO 90 I=1,HXAPRX	COPE1963		WRITE (6,570) (IA(I),I=N1,N2)	COPE2023
	IA(N3)=0	COPE1964	140	CONTINUE	COPE2024
C	GLOBAL LOCATION.	COPE1965	C	DESIGN VARIABLES.	COPE2025
	II=IA(N5)	COPE1966		WRITE (6,580)	COPE2026
	N5=N5+1	COPE1967		N1=HIDV	COPE2027
C	FIND CORRESPONDING DESIGN VARIABLE.	COPE1968		H2=N1*HXAPRX-1	COPE2028
	H1=LOC(I1)	COPE1969		WRITE (6,570) (IA(I),I=N1,N2)	COPE2029
	H2=LOC(I2)	COPE1970	150	CONTINUE	COPE2030
	DO 70 J=1,NDVTOT	COPE1971	C	ITERATION NUMBER.	COPE2031
	IF (IA(H1).EQ.II) GO TO 80	COPE1972		WRITE (6,680) KOUNT	COPE2032
	N1=N1+1	COPE1973	160	CONTINUE	COPE2033
70	N2=N2+1	COPE1974		NP=NPTOT-1	COPE2034

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C -----COPE2035
C          SET UP ARRAYS XNOM, FNOM, XI, Y.          COPE2036
C -----COPE2037
C          NXI=NTMP                                COPE2038
          NY=NXI*NXAPRX*NPTOT                       COPE2039
          HWGHT=NY*NF*NPTOT                         COPE2040
          IF (KMAX.LT.0.AND.INOM.LT.1) INOM=1       COPE2041
          CALL COPE10 (RA(NXI),RA(NY),RA(NXNOM),RA(NFNOM),NPTOT,KOUNT,RA(NBL)
          1U),IA(INIGFN),IOBJA,IA(NISC),NXAPRX,NF,NCONA,SGNOPT,CTMIN,ISCOPE2043
          2CR2,RA(NHWGHT),INOM,NPHAX,JNOM)          COPE2044
          IF (KMAX.LT.0) GO TO 170                  COPE2045
C          CURRENT OBJECTIVE.                      COPE2046
          N1=NFNOM*IOBJA-1                          COPE2047
          OBJSAV=-RA(N1)*SGNOPT                     COPE2048
          IF (KOUNT.LT.2.AND.DABFUN.LE.0.) DABFUN=.001*ABS(OBJSV) COPE2049
          IF (DABFUN.LT.1.0E-10) DABFUN=1.0E-10    COPE2050
          IF (IPAPRX.LT.1.OR.IPAPRX.EQ.3) GO TO 170 COPE2051
C          PRINT CURRENT NOMINAL.                  COPE2052
          WRITE (6,690) INOM                        COPE2053
          N2=NXNOM*NXAPRX-1                         COPE2054
          WRITE (6,700) (RA(I),I=NXNOM,N2)         COPE2055
          WRITE (6,710)                             COPE2056
          N2=NFNOM*NF-1                             COPE2057
          WRITE (6,700) (RA(I),I=NFNOM,N2)         COPE2058
170 CONTINUE                                       COPE2059
C -----COPE2060
C          LEAST SQUARES FIT FOR TAYLER SERIES EXPANSION. COPE2061
C -----COPE2062
          NX1=NXAPRX                                COPE2063
          M=NX1*(NX1*(NX1+1))/2                     COPE2064
          IF (M.GT.NP) M=NP                          COPE2065
          IF (NP.LT.NXAPRX) M=NXAPRX                COPE2066
          MMAX=NXAPRX*MAXTRM                         COPE2067
          IF (MAXTRM.GT.2) MMAX=M                   COPE2068
          IF (M.GT.MMAX) M=MMAX                     COPE2069
          NAA=HWGHT*NP                               COPE2070
          NFF=NAA*(M*(M+1))/2                       COPE2071
          NGG=NFF*M                                  COPE2072
          CALL COPE12 (RA(NXI),RA(NY),NX1,NP,NF,M,RA(NBTAY),RA(NAA),RA(NFF),
          1RA(NGG),NXAPRX,NF,NBR,RA(NHWGHT),NER)    COPE2073
          IF (NER.GT.0) WRITE (6,590)               COPE2074
          IF (KMAX.LT.0) GO TO 530                  COPE2075
          IF (IPAPRX.LT.2.AND.IPAPRX.NE.4) GO TO 190 COPE2076
          PRINT TAYLER SERIES COEFFICIENTS.         COPE2077
          WRITE (6,720)                             COPE2078
          N3=LOC(16)                                COPE2079
          N1=NBTAY                                   COPE2080
          DO 180 J=1,NF                              COPE2081
          N2=N1*M-1                                  COPE2082
          WRITE (6,600) J,IA(N3)                    COPE2083
          WRITE (6,700) (RA(I),I=N1,N2)            COPE2084
          N1=N1+NBR                                  COPE2085
          N3=N3+1                                    COPE2086
180 CONTINUE                                       COPE2087
190 CONTINUE                                       COPE2088
          IF (KOUNT.GT.KMAX) GO TO 470             COPE2089
C -----COPE2090
C          INITIALIZE XV, DX, VLB, VUB.           COPE2091
C -----COPE2092
          N1=HXV                                     COPE2093
          DO 200 I=1,NXAPRX                         COPE2094
          RA(H1)=0.                                  COPE2095
          N1=N1+1                                    COPE2096
          N2=NVLB                                    COPE2097
          N3=HVUB                                    COPE2098
          N4=HXNOM                                    COPE2099
          N5=LOCP(2)                                  COPE2100
          N6=LOCR(3)                                  COPE2101
          N7=LOCR(7)                                  COPE2102
          N8=NDX                                       COPE2103
          L1=M-NDV                                     COPE2104
          L2=L1-NDV                                    COPE2105
          ICK=ICK1+ICK2+ICK3                          COPE2106
          DO 210 I=1,NDV                               COPE2107
          RA(N8)=0.                                    COPE2108
          XFACT=1.                                     COPE2109
          IF (I.LE.L1) XFACT=XFACT1                  COPE2110
          L2=L2-NDV+I                                  COPE2111
          IF (L2.GE.0) XFACT=XFACT2                  COPE2112
          REDUCE BOUNDS IF ANY ICK.GT.0.             COPE2113
          IF (ICK.GT.0) XFACT=.5                      COPE2114
          DX=XFACT*PA(H7)                             COPE2115
          XX=RA(N4)                                    COPE2116
          DXL=XX-RA(N5)                               COPE2117
          IF (DXL.GT.DX) DXL=DX                      COPE2118
          DXU=RA(N6)-XX                               COPE2119
          IF (DXU.GT.DX) DXU=DX                       COPE2120
          RA(N2)=-DXL                                 COPE2121
          RA(N3)=-DXU                                 COPE2122
          N2=N2+1                                     COPE2123
          N3=N3+1                                     COPE2124
          N4=N4+1                                     COPE2125
          N5=N5+1                                     COPE2126
          N6=N6+1                                     COPE2127
          N7=N7+1                                     COPE2128
          N8=N8+1                                     COPE2129
          IF (IPAPRX.LT.2.AND.IPAPRX.NE.4) GO TO 220 COPE2130
          WRITE (6,610)                               COPE2131
          N1=NVLB+NDV-1                              COPE2132
          WRITE (6,700) (RA(I),I=NVLB,N1)           COPE2133
          WRITE (6,620)                               COPE2134
          N1=NVUB+NDV-1                              COPE2135
          WRITE (6,700) (RA(I),I=NVUB,N1)           COPE2136
          CONTINUE                                     COPE2137
          -----COPE2138
          OPTIMIZE APPROXIMATE FUNCTION.             COPE2139
          -----COPE2140
          OPTIMIZATION.                               COPE2141
          IGOTO=0                                     COPE2142
          CALL COMMIN (X,VLB,VUB,G,SCAL,DF,A,S,G1,G2,B,C,ISC,IC,MS1,N1,N2,N3) COPE2143
          *,N4,N5)                                    COPE2144
          CONTINUE                                     COPE2145
          CALL COMMIN (RA(NDX),RA(NVLB),RA(NVUB),RA(NG),RA(NHNSCAL),RA(NDF),
          1A(NA),RA(NS),RA(NG1),RA(NG2),RA(NB),RA(NC),IA(NISC),IA(NIC),IA(NHNS)
          21),HH1,HH2,HH3,HH4,HH5)                  COPE2146
          TRANSFER VARIABLES FROM DX TO XV.          COPE2147
          N1=NDV                                       COPE2148
          N2=HXV                                       COPE2149
          DO 240 I=1,NXAPRX                           COPE2150
          II=IA(N1)                                    COPE2151
          -----COPE2152
          -----COPE2153
          -----COPE2154

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	N4=NDX*II-1	COPE2155	C	MODIFY DELTA-X VECTOR.	COPE2215
	IF (II.GT.0.AND.II.LE.NDV) RA(N2)=RA(N4)	COPE2156		N6=NVUB	COPE2216
	N1=N1+1	COPE2157		N7=NXV	COPE2217
	N2=N2+1	COPE2158		N8=NVLB	COPE2218
240	N3=N3+1	COPE2159		N9=NXV*NDV-1	COPE2219
C	APPROXIMATE ANALYSIS.	COPE2160		IF (IPAPRX.LT.1.OR.IPAPRX.EQ.3) GO TO 310	COPE2220
	CALL COPE15 (RA(NXV),RA(NG),RA(NDF),RA(NA),IA(NISC),IA(NIC),NN1,RACOPE2161			WRITE (6,630)	COPE2221
	1(NBLU),HX1,IOBJA,M,RA(NFNOM),RA(NFNEW),RA(NBTAY),NBR,IA(NIGFN),CT,COPE2162			WRITE (6,740)	COPE2222
	2CTL,INFO,NAC,NCONA,NDV,NF,OBJ,SGNOPT)	COPE2163		WRITE (6,700) (RA(I),I=N7,N9)	COPE2223
	IF (IGOTO.GT.0) GO TO 230	COPE2164		WRITE (6,750)	COPE2224
C	IF DESIGN PRODUCED ZERO DELTA-X TWICE IN A ROW AND KOUNT.GE.KMIN,	COPE2165		N9=NTMP*HXAPRX-1	COPE2225
C	TERMINATE.	COPE2166		WRITE (6,700) (RA(I),I=NTMP,N9)	COPE2226
	ICK1=ICK1+1	COPE2167		WRITE (6,640)	COPE2227
	SUM=0.	COPE2168	310	CONTINUE	COPE2228
	N1=NXV	COPE2169		AMULT=.01*FLOAT(JJJ)	COPE2229
	DO 250 I=1,NDV	COPE2170		DO 320 I=1,NDV	COPE2230
	SUM=SUM*RA(N1)**2	COPE2171		BU=RA(N6)	COPE2231
250	N1=N1+1	COPE2172		BL=RA(N8)	COPE2232
	IF (SUM.GT.1.0E-10) ICK1=0	COPE2173		IF (BL.LT.-1.0E+15) BL=0.	COPE2233
	IF (IPAPRX.GT.0.AND.IPAPRX.NE.3) WRITE (6,730)	COPE2174		IF (BU.GT.1.0E+15) BU=0.	COPE2234
	IF (ICK1.GE.2.AND.KOUNT.GE.KMIN) GO TO 360	COPE2175		DB=ABS(BU-BL)	COPE2235
C	-----	COPE2176		IF (DB.LT.1.0E-6) DB=.1	COPE2236
C	INSURE NEW X-VECTOR IS INDEPENDENT	COPE2177		DX=RA(N7)*AMULT*DB	COPE2237
C	-----	COPE2178		IF (DX.GT.RA(N6)) DX=DX-2.*AMULT*DB	COPE2238
	JJJ=0	COPE2179		IF (DX.LT.RA(N8)) DX=DX+1.5*AMULT*DB	COPE2239
260	JJJ=JJJ+1	COPE2180		RA(N7)=DX	COPE2240
C	NOMINAL X-VECTOR.	COPE2181		N6=N6+1	COPE2241
	N1=NTMP	COPE2182		N7=N7+1	COPE2242
	N2=NXNOM	COPE2183		N8=N8+1	COPE2243
	N3=NXV	COPE2184	320	CONTINUE	COPE2244
	DO 270 I=1,NXAPRX	COPE2185		CALL COPE15 (RA(NXV),RA(NG),RA(NDF),RA(NA),IA(NISC),IA(NIC),NN1,RACOPE2245	
	RA(N1)=RA(N2)*RA(N3)	COPE2186		1(NBLU),HX1,IOBJA,M,RA(NFNOM),RA(NFNEW),RA(NBTAY),NBR,IA(NIGFN),CT,COPE2246	
	N1=N1+1	COPE2187		2CTL,INFO,NAC,NCONA,NDV,NF,OBJ,SGNOPT)	COPE2247
	N2=N2+1	COPE2188		IF (JJJ.LT.4) GO TO 260	COPE2248
270	N3=N3+1	COPE2189	C	FOUR TRIES HAVE FAILED TO PRODUCE A USABLE X-VECTOR.	COPE2249
C	READ X-VECTORS ONE AT A TIME AND COMPARE TO XNOM.	COPE2190	C	USE LATEST TRY.	COPE2250
	REWIND ISCR2	COPE2191	C	POSITION ISCR2 IF NEEDED.	COPE2251
	N1=NTMP*NXAPRX	COPE2192		IF (KK.EQ.NPTOT) GO TO 340	COPE2252
	N2=N1*NXAPRX-1	COPE2193		KK=KK+1	COPE2253
	N3=N2+1	COPE2194		DO 330 J=KK,NPTOT	COPE2254
	N4=N3*NF-1	COPE2195		READ (ISCR2) (RA(I),I=N1,N2)	COPE2255
	DO 290 J=1,NPTOT	COPE2196	330	READ (ISCR2) (RA(I),I=N3,N4)	COPE2256
	KK=J	COPE2197	340	CONTINUE	COPE2257
C	X-VECTOR.	COPE2198		IF (IPAPRX.LT.1.OR.IPAPRX.EQ.3) GO TO 350	COPE2258
	READ (ISCR2) (RA(I),I=N1,N2)	COPE2199		IF (JJJ.EQ.4) WRITE (6,650)	COPE2259
C	Y-VECTOR. NOT USED. READ TO POSITION ISCR2.	COPE2200	350	CONTINUE	COPE2260
	READ (ISCR2) (RA(I),I=N3,N4)	COPE2201	360	CONTINUE	COPE2261
C	COMPARE X WITH XNOM.	COPE2202	C	-----	COPE2262
	N5=N1	COPE2203	C	UPDATE ANALYSIS.	COPE2263
	N6=NTMP	COPE2204	C	-----	COPE2264
	SUM=0.	COPE2205	C	XNOM.	COPE2265
	DO 280 I=1,NXAPRX	COPE2206		N1=NXNOM	COPE2266
	SUM=SUM*(RA(N5)-RA(N6))**2	COPE2207		N2=NXV	COPE2267
	N5=N5+1	COPE2208		DO 370 I=1,NXAPRX	COPE2268
280	N6=N6+1	COPE2209		RA(N1)=RA(N1)*RA(N2)	COPE2269
	IF (SUM.LT.1.0E-10) GO TO 300	COPE2210		N1=N1+1	COPE2270
290	CONTINUE	COPE2211	370	N2=N2+1	COPE2271
	GO TO 360	COPE2212	C	GLOBAL VARIABLES.	COPE2272
300	CONTINUE	COPE2213		N3=NXNOM	COPE2273
C	THIS DESIGN IS SAME AS A PREVIOUS DESIGN.	COPE2214		N4=NDV	COPE2274

C	DO 410 I=1,NXAPRX	COPE2275	C	-----	COPE2335
	DESIGN VARIABLE NUMBER.	COPE2276	C	WRITE NEW X AND F VALUES ON ISCR2.	COPE2336
	II=IA(N4)	COPE2277	C	-----	COPE2337
	IF (II.EQ.0) GO TO 400	COPE2278	C	X-VECTOR.	COPE2338
C	DESIGN VARIABLE UPDATE.	COPE2279	C	N1=NXNHOM*NXAPRX-1	COPE2339
	N1=LOCI(1)	COPE2280	C	WRITE (ISCR2) (RA(I),I=NXNHOM,N1)	COPE2340
	N2=LOCI(2)	COPE2281	C	FUNCTIONS.	COPE2341
	N5=LOCR(5)	COPE2282	C	N1=NFNOM*NF-1	COPE2342
	DO 390 J=1,NDVTOT	COPE2283	C	WRITE (ISCR2) (RA(I),I=NFNOM,N1)	COPE2343
	IF (IA(N2).NE.II) GO TO 380	COPE2284	C	UPDATE PARAMETERS.	COPE2344
C	UPDATE VARIABLE J.	COPE2285	C	NPTOT=NPTOT*1	COPE2345
	JJ=IA(N1)	COPE2286	C	IF (JJJ.LT.2.OR.KOUNT.LT.KMIN) INOM=NPTOT	COPE2346
	ARRAY(JJ)=RA(N3)*RA(N5)	COPE2287	C	-----	COPE2347
380	N1=N1+1	COPE2288	C	CONVERGENCE CHECK.	COPE2348
	N2=N2+1	COPE2289	C	-----	COPE2349
	N5=N5+1	COPE2290	C	IF (KOUNT.LT.KMIN) GO TO 130	COPE2350
390	CONTINUE	COPE2291	C	ICK2=ICK2+1	COPE2351
400	N3=N3+1	COPE2292	C	ICK3=ICK3+1	COPE2352
410	N4=N4+1	COPE2293	C	DEL=ABS(OBJ)	COPE2353
	IF (IPAPRX.LT.1.OR.IPAPRX.EQ.3) GO TO 420	COPE2294	C	IF (DEL.LT.1.0E-6) DEL=1.0E-6	COPE2354
C	PRINT APPROXIMATE OPTIMIZATION INFORMATION.	COPE2295	C	DEL=(OBJ-OBJSAV)/DEL	COPE2355
	WRITE (6,740)	COPE2296	C	DEL=ABS(DEL)	COPE2356
	N2=NXV+NDV-1	COPE2297	C	DEL=(OBJ-OBJSAV)/DEL	COPE2357
	WRITE (6,700) (RA(I),I=NXV,N2)	COPE2298	C	DEL=ABS(DEL)	COPE2358
	WRITE (6,750)	COPE2299	C	IF (DEL.GT.DELFUN) ICK2=0	COPE2359
	N2=NXNHOM*NXAPRX-1	COPE2300	C	DEL=ABS(OBJ-OBJSAV)	COPE2360
	WRITE (6,700) (RA(I),I=NXNHOM,N2)	COPE2301	C	IF (DEL.GT.DABFUN) ICK3=0	COPE2361
	WRITE (6,760)	COPE2302	C	IF (ICK2.GE.2.OR.ICK3.GE.2) GO TO 460	COPE2362
	N2=NFNEW*NF-1	COPE2303	C	IF (KOUNT.LT.KMAX) GO TO 130	COPE2363
	WRITE (6,700) (RA(I),I=NFNEW,N2)	COPE2304	460	CONTINUE	COPE2364
420	CONTINUE	COPE2305	C	-----	COPE2365
	IF ((ICK1.GE.2.AND.KOUNT.GE.KMIN).AND.(IPAPRX.GT.0.AND.IPAPRX.NE.3	COPE2306	C	FINAL INFORMATION.	COPE2366
	1)) WRITE (6,540)	COPE2307	C	-----	COPE2367
	IF (ICK1.GE.2.AND.KOUNT.GE.KMIN) GO TO 460	COPE2308	C	IF (IPAPRX.GT.0.AND.IPAPRX.NE.3) WRITE (6,660)	COPE2368
	ICALC=2	COPE2309	C	GO BACK AND PICK BEST DESIGN.	COPE2369
	NAN2=NAN2+1	COPE2310	C	INOM=0	COPE2370
C	CALL ANALIZ (ICALC)	COPE2311	C	KOUNT=KMAX+1	COPE2371
	NEW FUNCTION VALUES.	COPE2312	C	IF (KOUNT.LT.JNHOM) KOUNT=JNHOM+1	COPE2372
	N1=NFNOM	COPE2313	C	CTSAV=CT	COPE2373
	M6=LOCI(6)	COPE2314	C	CTLSAV=CTL	COPE2374
	DO 430 I=1,NF	COPE2315	C	IF (ABS(CT).LT.1.0E-10) CT=-.004	COPE2375
	II=IA(M6)	COPE2316	C	IF (ABS(CTL).LT.1.0E-10) CTL=-.001	COPE2376
	M6=M6+1	COPE2317	C	GO TO 160	COPE2377
	RA(N1)=ARRAY(II)	COPE2318	470	CONTINUE	COPE2378
430	N1=N1+1	COPE2319	C	CT=CTSAV	COPE2379
	IF (IPDBG.LT.1) GO TO 440	COPE2320	C	CTL=CTLSAV	COPE2380
C	DEBUG OUTPUT.	COPE2321	C	STORE FINAL VALUES OF XNOM IN GLOBAL ARRAY.	COPE2381
	NAN3=NAN3+1	COPE2322	C	N3=NXNHOM	COPE2382
	ICALC=3	COPE2323	C	N4=NIDV	COPE2383
	CALL ANALIZ (ICALC)	COPE2324	C	DO 510 I=1,NXAPRX	COPE2384
440	CONTINUE	COPE2325	C	DESIGN VARIABLE NUMBER.	COPE2385
	IF (IPAPRX.LT.1.OR.IPAPRX.EQ.3) GO TO 450	COPE2326	C	II=IA(N4)	COPE2386
C	PRINT PRECISE FUNCTION VALUES.	COPE2327	C	IF (II.EQ.0) GO TO 500	COPE2387
	WRITE (6,770)	COPE2328	C	DESIGN VARIABLE UPDATE.	COPE2388
	N2=NFNOM*NF-1	COPE2329	C	N1=LOCI(1)	COPE2389
	WRITE (6,700) (RA(I),I=NFNOM,N2)	COPE2330	C	N2=LOCI(2)	COPE2390
450	CONTINUE	COPE2331	C	N5=LOCR(5)	COPE2391
C	NEW OBJECTIVE.	COPE2332	C	DO 490 J=1,NDVTOT	COPE2392
	N1=NFNOM*IOBJA-1	COPE2333	C	IF (IA(NC).NE.II) GO TO 480	COPE2393
	OBJ=-RA(N1)*SGHOPT	COPE2334	C	UPDATE VARIABLE J.	COPE2394

	JJ=IA(N1)	COPE2395	C	*****	COPE2455
	ARRAY(JJ)=RA(N3)*PA(N5)	COPE2396	C	ROUTINE TO SET UP ARRAYS FOR TAYLER SERIES EXPANSION.	COPE2456
480	N1=N1+1	COPE2397	C	*****	COPE2457
	N2=N2+1	COPE2398	C		COPE2458
	N5=N5+1	COPE2399	C	BY G. N. VANDERPLAATS	COPE2459
490	CONTINUE	COPE2400	C	NASA AMES RESEARCH CENTER, MOFFETT FIELD, CALIF.	COPE2460
500	N3=N3+1	COPE2401	C		COPE2461
510	N4=N4+1	COPE2402	C	REWIND ISCR2	COPE2462
C	STORE FINAL VALUES OF FNOM IN GLOBAL ARRAY.	COPE2403	C	DO 10 J=1,NPTOT	COPE2463
	M6=LOCI(6)	COPE2404	C	READ (ISCR2) (XI(I,J),I=1,NXAPRX)	COPE2464
	N1=NFNOM	COPE2405	10	READ (ISCR2) (Y(I,J),I=1,NF)	COPE2465
	DO 520 I=1,NF	COPE2406	C	-----	COPE2466
	II=IA(M6)	COPE2407	C	FIND BEST NOMINAL IF REQUIRED.	COPE2467
	M6=M6+1	COPE2408	C	-----	COPE2468
	ARRAY(II)=RA(N1)	COPE2409	C	IF (KOUNT.LE.1.AND.INOM.GT.0) GO TO 20	COPE2469
520	N1=N1+1	COPE2410	C	IF (KOUNT.GT.1.AND.KOUNT.LE.JNOM) GO TO 20	COPE2470
530	CONTINUE	COPE2411	C	CALL COPE11 (NPTOT,Y,NF,INOM,BLU,NCOHA,IGFN,IOBJA,SGNOPT,CTMIN,CTL	COPE2471
	RETURN	COPE2412	C	MIN,ISC)	COPE2472
C	-----	COPE2413	20	CONTINUE	COPE2473
C	FORMATS	COPE2414	C	-----	COPE2474
C	-----	COPE2415	C	CREATE XNOM AND FNOM.	COPE2475
540	FORMAT (//5X,71HTWO CONSECUTIVE APPROXIMATE OPTIMIZATIONS HAVE PRODUCED THE SAME DESIGN//5X,23HOPTIMIZATION TERMINATED)	COPE2416	C	-----	COPE2476
	1DUCE THE SAME DESIGN//5X,23HOPTIMIZATION TERMINATED)	COPE2417	C	DO 30 I=1,NXAPRX	COPE2477
550	FORMAT (/5X,22HAPPROXIMATING FUNCTION,I5,17H IS THE OBJECTIVE)	COPE2418	30	XNOM(I)=XI(I,INOM)	COPE2478
560	FORMAT (/5X,51HAPPROXIMATING FUNCTIONS ASSOCIATED WITH CONSTRAINTSCOPE2419	COPE2419	C	DO 40 I=1,NF	COPE2479
	1)	COPE2420	40	FNOM(I)=Y(I,INOM)	COPE2480
570	FORMAT (5X,10I5)	COPE2421	C	NP=NPTOT-1	COPE2481
580	FORMAT (//5X,63HDESIGN VARIABLE NUMBERS ASSOCIATED WITH APPROXIMATING VARIABLES)	COPE2422	C	IF (INOM.EQ.NPTOT) GO TO 80	COPE2482
	1ING VARIABLES)	COPE2423	C	-----	COPE2483
590	FORMAT (//5X,59H* * LEAST SQUARES FIT TO APPROXIMATION DATA IS SINCE	COPE2424	C	SHIFT XI AND Y.	COPE2484
	1GULAR * *//5X,26HRESULTS MAY NOT BE VALID)	COPE2425	C	-----	COPE2485
600	FORMAT (/5X,15HFUNCTION NUMBER,I5,25H GLOBAL VARIABLE NUMBER,I5,15X,12HCOEFFICIENTS)	COPE2426	C	DO 70 J=INOM,NP	COPE2486
	15X,12HCOEFFICIENTS)	COPE2427	C	DO 50 I=1,NXAPRX	COPE2487
610	FORMAT (/5X,44HSIDE CONSTRAINTS ON APPROXIMATE OPTIMIZATION//5X,12HLOWER BOUNDS)	COPE2428	50	XI(I,J)=XI(I,J+1)	COPE2488
	1HLOWER BOUNDS)	COPE2429	C	DO 60 I=1,NF	COPE2489
620	FORMAT (/5X,12HUPPER BOUNDS)	COPE2430	60	Y(I,J)=Y(I,J+1)	COPE2490
630	FORMAT (//5X,76HOPTIMIZATION HAS PRODUCED AN X-VECTOR WHICH IS THE	COPE2431	70	CONTINUE	COPE2491
	1 SAME AS A PREVIOUS DESIGN)	COPE2432	80	CONTINUE	COPE2492
640	FORMAT (/5X,51HTHE FOLLOWING DESIGN IS NOT THE APPROXIMATE OPTIMUM	COPE2433	C	-----	COPE2493
	1)	COPE2434	C	REPLACE XI BY DELTA-XI AND Y BY DELTA-Y.	COPE2494
650	FORMAT (/5X,60HFOUR ATTEMPTS HAVE FAILED TO PRODUCE AN INDEPENDENT	COPE2435	C	-----	COPE2495
	1 X-VECTOR/5X,52HOPTIMIZATION WILL CONTINUE WITH MOST RECENT X-VECT	COPE2436	C	DO 110 J=1,NP	COPE2496
	2OR)	COPE2437	C	DO 90 I=1,NXAPRX	COPE2497
660	FORMAT (1H1,4X,40HFINAL RESULT OF APPROXIMATE OPTIMIZATION)	COPE2438	90	XI(I,J)=XI(I,J)-XNOM(I)	COPE2498
670	FORMAT (1H1,4X,42HAPPROXIMATE OPTIMIZATION ITERATION HISTORY)	COPE2439	C	DO 100 I=1,NF	COPE2499
680	FORMAT (///5X,22HBEGIN ITERATION NUMBER,I5)	COPE2440	100	Y(I,J)=Y(I,J)-FNOM(I)	COPE2500
690	FORMAT (/5X,23HNOMINAL DESIGN NUMBER =,I5//5X,8HX-VECTOR)	COPE2441	110	CONTINUE	COPE2501
700	FORMAT (5X,5E13.5)	COPE2442	C	-----	COPE2502
710	FORMAT (/5X,15HFUNCTION VALUES)	COPE2443	C	WEIGHTING FACTORS.	COPE2503
720	FORMAT (/5X,26HTAYLOR SERIES COEFFICIENTS)	COPE2444	C	-----	COPE2504
730	FORMAT (/5X,35HRESULTS OF APPROXIMATE OPTIMIZATION)	COPE2445	C	SMAX=1.0E-10	COPE2505
740	FORMAT (/5X,14HDELTA-X VECTOR)	COPE2446	C	DO 130 J=1,NP	COPE2506
750	FORMAT (/5X,8HX-VECTOR)	COPE2447	C	SUM=0.	COPE2507
760	FORMAT (/5X,27HAPPROXIMATE FUNCTION VALUES)	COPE2448	C	DO 120 I=1,NXAPRX	COPE2508
770	FORMAT (/5X,23HPRECISE FUNCTION VALUES)	COPE2449	120	SUM=SUM+XI(I,J)**2	COPE2509
	END	COPE2450	C	IF (SUM.GT.SMAX) SMAX=SUM	COPE2510
	SUBROUTINE COPE10 (XI,Y,XNOM,FNOM,NPTOT,KOUNT,BLU,IGFN,IOBJA,ISC,N	COPE2451	130	WGHT(J)=SQRT(SUM)	COPE2511
	1XAPRX,NF,NCOHA,SGNOPT,CTMIN,CTLMIN,ISCR2,WGHT,INOM,NPMAX,JNOM)	COPE2452	C	SMAX=SQRT(SMAX)	COPE2512
	1DIMENSION XI(NXAPRX,1),Y(NF,1),XNOM(1),FNOM(1),BLU(4,1),IGFN(COPE2453	C	DO 140 I=1,NP	COPE2513
	11),ISC(1),WGHT(1)	COPE2454	140	WGHT(I)=2.-WGHT(I)/SMAX	COPE2514

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C      IF (NP.LE.NPMAX) RETURN                                COPE2515      I1=1                                COPE2575
C      -----                                                COPE2516      I2=0                                COPE2576
C      REDUCE THE NUMBER OF DESIGNS TO NPMAX.                COPE2517      DO 50 J=1,NPTOT                      COPE2577
C      -----                                                COPE2518      OBJECTIVE.                          COPE2578
C      NPMX1=NPMAX*1                                         COPE2519      OBJ=-Y(IOBJA,J)*SGNOPT              COPE2579
C      NPSAV=NP                                              COPE2520      CONSTRAINTS.                        COPE2580
C      DO 200 I1=NPMX1,NPSAV                                 COPE2521      ICON=0                               COPE2581
C      FIND DESIGN WITH MINIMUM WEIGHTING FACTOR.           COPE2522      G1=-1.                               COPE2582
C      WMIN=WGHT(I)                                          COPE2523      DO 30 I=1,NCONA                     COPE2583
C      IMN=1                                                 COPE2524      II=IGFN(I)                          COPE2584
C      DO 150 I=2,NP                                         COPE2525      GG=Y(II,J)                          COPE2585
C      IF (WGHT(I).GE.WMIN) GO TO 150                       COPE2526      LOWER BOUND.                        COPE2586
C      WMIN=WGHT(I)                                         COPE2527      IF (BLU(1,I).LT.-1.0E+15) GO TO 20  COPE2587
C      IMN=I                                                 COPE2528      ICON=ICON+1                         COPE2588
C      150 CONTINUE                                         COPE2529      CT=CT1                               COPE2589
C      IF (IMN.EQ.NP) GO TO 190                             COPE2530      IF (ISC(ICON).GT.0) CT=CTL1         COPE2590
C      SHIFT XI, Y AND WGHT.                                COPE2531      G=(BLU(1,I)-GG)/BLU(2,I)-CT        COPE2591
C      NPM1=NP-1                                             COPE2532      IF (G.GT.G1) G1=G                  COPE2592
C      DO 180 J=IMN,NPM1                                     COPE2533      UPPER BOUND.                       COPE2593
C      DO 160 I=1,NXAPRX                                    COPE2534      IF (BLU(3,I).GT.1.0E+15) GO TO 30  COPE2594
C      160 XI(I,J)=XI(I,J+1)                                COPE2535      ICON=ICON+1                         COPE2595
C      DO 170 I=1,NF                                         COPE2536      CT=CT1                               COPE2596
C      170 Y(I,J)=Y(I,J+1)                                  COPE2537      IF (ISC(ICON).GT.0) CT=CTL1         COPE2597
C      180 WGHT(I)=WGHT(I+1)                                COPE2538      G=(GG-BLU(3,I))/BLU(4,I)-CT        COPE2598
C      NP=NP-1                                              COPE2539      IF (G.GT.G1) G1=G                  COPE2599
C      200 CONTINUE                                         COPE2540      30 CONTINUE                        COPE2600
C      RETURN                                               COPE2541      IF (G1.LT.0..OR.G1.GT.GMAX) GO TO 40 COPE2601
C      END                                                  COPE2542      I1=J                                COPE2602
C      SUBROUTINE COPE11 (NPTOT,Y,NYR,INOM,BLU,NCONA,IGFN,IOBJA,SGNOPT,CT,COPE2543      GMAX=G1                            COPE2603
C      MIN,CTLMIN,ISC)                                       COPE2544      40 IF (OBJ.GT.OBJMAX.OR.G1.GT.0.) GO TO 50 COPE2604
C      DIMENSION Y(NYR,1), BLU(4,1), IGFN(1), ISC(1)        COPE2545      I2=J                                COPE2605
C      *****COPE2546                                       COPE2546      OBJMAX=OBJ                          COPE2606
C      ROUTINE TO DETERMINE NOMINAL DESIGN FOR APPROXIMATE OPTIMIZATION. COPE2547      CONTINUE                            COPE2607
C      *****COPE2548                                       COPE2548      INOM=I1                             COPE2608
C      *****COPE2549                                       COPE2549      IF (I2.GT.0) INOM=I2               COPE2609
C      BY G. N. VANDERPLAATS                                JAN., 1979. COPE2550      RETURN                               COPE2610
C      NASA AMES RESEARCH CENTER, MOFFETT FIELD, CALIF.    COPE2551      END                                  COPE2611
C      NOMINAL DESIGN IS THE ONE WITH LOWEST OBJECTIVE SATISFYING ALL COPE2552      SUBROUTINE COPE12                      COPE2612
C      CONSTRAINTS. IF ALL DESIGNS VIOLATE CONSTRAINTS, THE DESIGN WITH COPE2553      *****COPE2613
C      THE LEAST VIOLATION IS FOUND.                       COPE2554      ROUTINE TO PERFORM A LEAST SQUARES FIT OF AN ARBITRARY FUNCTION OF COPE2614
C      I1 IS DESIGN WITH LOWEST MAXIMUM CONSTRAINT VALUE.  COPE2555      NV VARIABLES.                        COPE2615
C      I2 IS THE DESIGN WITH THE LOWEST OBJECTIVE SATISFYING ALL COPE2556      Y = F(X1,X2,...,XNX) = B(1)*F(1) + B(2)*F(2) + ... + B(M)*F(M) COPE2616
C      CONSTRAINTS.                                         COPE2557      *****COPE2617
C      CT1=ABS(CTMIN)                                       COPE2558      COPE2618
C      IF (CT1.LT.0.004) CT1=0.004                         COPE2559      BY G. N. VANDERPLAATS                JAN., 1979. COPE2619
C      CT1=ABS(CTLMIN)                                       COPE2560      NASA AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COPE2620
C      IF (CT1.LT.0.001) CT1=0.001                         COPE2561      ARGUMENTS,                          COPE2621
C      -----                                                COPE2562      X,Y - INPUT ARRAYS OF OBSERVATIONS OF NP POINTS COPE2622
C      FIND MAXIMUM OBJECTIVE.                                COPE2563      X(NX,NP), Y(NF,NP)                  COPE2623
C      -----                                                COPE2564      NX - NUMBER OF INDEPENDENT VARIABLES OF WHICH Y IS A FUNCTION. COPE2624
C      OBJMAX=-Y(IOBJA,1)*SGNOPT                             COPE2565      NP - NUMBER OF OBSERVATION POINTS.   COPE2625
C      DO 10 J=2,NPTOT                                       COPE2566      NF - NUMBER OF SEPERATE CURVE FITS BEING DONE SIMULTANEOUSLY. COPE2626
C      OBJ=-Y(IOBJA,J)*SGNOPT                                COPE2567      THIS IS THE NUMBER OF SETS OF Y VALUES. COPE2627
C      IF (OBJ.GT.OBJMAX) OBJMAX=OBJ                         COPE2568      M - NUMBER OF COMPONENTS OF THE FUNCTIONS TO BE FITTED. COPE2628
C      10 CONTINUE                                          COPE2569      B - APRAY OF M COEFFICIENTS OF FUNCTIONAL FIT TO DATE. COPE2629
C      -----                                                COPE2570      A - M(M+1)/2 WORK VECTOR.           COPE2630
C      NOW FIND DESIGN VARIABLE WITH LOWEST OBJECTIVE SATISFYING ALL COPE2571      F - WORK VECTOR - F(M).             COPE2631
C      CONSTRAINTS AND DESIGN WITH LEAST CONSTRAINT VIOLATION. COPE2572      G - WORK VECTOR - G(MF).           COPE2632
C      -----                                                COPE2573      NXR - DIMENSIONED ROWS OF X.       COPE2633
C      GMAX=1.0E+20                                         COPE2574      NYR - DIMENSIONED ROWS OF Y.       COPE2634

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C   NBR - DIMENSIONED ROWS OF B.
C   Wght - ARRAY OF WEIGHTING FACTORS - Wght(NP1).
C   NER - ERROR FLAG. IF NER.GT.0, DIAGONAL ELEMENT NER OF A IS
C         LESS THAN 1.0E-10.
C
C   USER SUPPLIED SUBROUTINE, COPE13.
C   USAGE
C   CALL COPE13(XI,F,NX,M)
C   ROUTINE TO EVALUATE COMPONENTS F(1),...,F(M) WHICH ARE TO BE
C   FITTED TO DATA.
C   TO DATA. ROUTINE EVALUATES THE FUNCTIONS FOR A SINGLE VECTOR OF
C   XI AND STORES THE RESULTING VALUES IN VECTOR F.
C   ARGUMENTS.
C   XI - VECTOR OF INDEPENDENT VARIABLES AT WHICH FUNCTIONS ARE
C         TO BE EVALUATED.
C   F - VECTOR OF FUNCTION VALUES.
C   NX - NUMBER OF INDEPENDENT VARIABLES OF WHICH Y IS A FUNCTION.
C   M - NUMBER OF FUNCTION COMPONENTS, ALSO REQUIRED DIMENSION OF
C
SUBROUTINE COPE12 (X,Y,NX,NP,NF,M,B,A,F,G,NXR,NYR,NBR,Wght,NER)
DIMENSION X(NXR,1), Y(NYR,1), B(NBR,1), A(1), F(1), G(1)
DIMENSION Wght(1)
IF (NX.LE.NP) GO TO 50
SPECIAL CASE. FEWER OBSERVATIONS THAN DESIGN VARIABLES. USE
AVERAGE FINITE DIFFERENCE FOR FIRST ORDER EXPANSION.
NP1=NP+1
AP=FLOAT(NP)
DO 20 I=1,NX
X(I,NP1)=AP
DO 10 J=1,NP
IF (ABS(X(I,J)).GT.1.0E-10) GO TO 10
X(I,NP1)=X(I,NP1)-1.
X(I,J)=1.0E+20
CONTINUE
IF (X(I,NP1).LT.1.) X(I,NP1)=1.
CONTINUE
DO 40 I=1,NX
DO 40 J=1,NF
B(I,J)=0.
DO 30 K=1,NP
B(I,J)=B(I,J)+Y(J,K)/X(I,K)
40 B(I,J)=B(I,J)/X(I,NP1)
NER=0
RETURN
CONTINUE
C   GENERAL CASE. DO LEAST SQUARES FIT.
C   A=B=0.
DO 60 J=1,NF
DO 60 I=1,M
B(I,J)=0.
L=(M*(M+1))/2
DO 70 J=1,L
A(J)=0.
C   LOWER TRIANGLE OF A IN SYMMETRIC MODE.
DO 100 K=1,NP
WghtK=Wght(K)
CALL COPE13 (X(1,K),F,NX,M)
L=0
DO 80 J=1,M
DO 80 I=1,J
COPE2635 L=L+1
COPE2636 80 A(L)=A(L)+F(I)*F(J)*WghtK
COPE2637 C Y*F
COPE2638 DO 90 L=1,NF
COPE2639 YLK=Y(L,K)*WghtK
COPE2640 DO 90 I=1,M
COPE2641 90 B(I,L)=B(I,L)+YLK*F(I)
COPE2642 100 CONTINUE
COPE2643 C SOLVE FOR B.
COPE2644 IF (M.LE.1) GO TO 200
COPE2645 C LDU DECOMPOSITION.
COPE2646 MM1=M-1
COPE2647 KK=0
COPE2648 DO 110 K=1,MM1
COPE2649 NER=K
COPE2650 KK=KK+K
COPE2651 IF (ABS(A(KK)).LT.1.0E-20) GO TO 220
COPE2652 FACT=1./A(KK)
COPE2653 A(KK)=FACT
COPE2654 KP1=K+1
COPE2655 KJ=KK
COPE2656 DO 110 J=KP1,M
COPE2657 KJ=KJ+J-1
COPE2658 GG=A(KJ)*FACT
COPE2659 KI=KK
COPE2660 IJ=KJ
COPE2661 DO 110 I=KP1,J
COPE2662 IJ=IJ+1
COPE2663 KI=KI+I-1
COPE2664 A(IJ)=A(IJ)-A(KI)*GG
COPE2665 110 CONTINUE
COPE2666 KK=KK+M
COPE2667 NER=M
COPE2668 IF (ABS(A(YK)).LT.1.0E-20) GO TO 220
COPE2669 A(KK)=1./A(KK)
COPE2670 C FORWARD SUBSTITUTION
COPE2671 MP1=M+1
COPE2672 KK=0
COPE2673 DO 130 K=1,MM1
COPE2674 KP1=K+1
COPE2675 KK=KK+K
COPE2676 AKK=A(KK)
COPE2677 DO 120 L=1,NF
COPE2678 120 B(K,L)=B(K,L)*AKK
COPE2679 KI=KK
COPE2680 DO 130 I=KP1,M
COPE2681 KI=KI+I-1
COPE2682 AKI=A(KI)
COPE2683 DO 130 J=1,NF
COPE2684 B(I,J)=B(I,J)-AKI*B(K,J)
COPE2685 130 CONTINUE
COPE2686 KK=KK+M
COPE2687 AKK=A(KK)
COPE2688 DO 140 J=1,NF
COPE2689 140 B(M,J)=B(M,J)*AKK
COPE2690 C BACK SUBSTITUTION.
COPE2691 DO 190 I=2,M
COPE2692 J=MP1-I
COPE2693 JJ=J*(J+1)/2
COPE2694 JK=JJ
COPE2695
COPE2696
COPE2697
COPE2698
COPE2699
COPE2700
COPE2701
COPE2702
COPE2703
COPE2704
COPE2705
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COPE2751
COPE2752
COPE2753
COPE2754

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	JP1=J+1	COPE2755	30	F(II)=X(I)*X(J)	COPE2815	
	DO 150 L=1,NF	COPE2756	40	CONTINUE	COPE2816	
150	G(L)=0.	COPE2757		RETURN	COPE2817	
	DO 170 K=JP1,M	COPE2758		END	COPE2818	
	JK=JK+K-1	COPE2759		SUBROUTINE COPE14 (HXAPRX,NF,NPTOT,RA,IA,LOCR,LOCI,TITLE,INOM,NDV,	COPE2819	
	AJK=A(JK)	COPE2760		IPAPRX,ISCR2,MAXTRM)	COPE2820	
	DO 160 L=1,NF	COPE2761		DIMENSION RA(1), IA(1), LOCR(1), LOCI(1), TITLE(1)	COPE2821	
160	G(L)=G(L)+AJK*B(K,L)	COPE2762	C	*****	COPE2822	
170	CONTINUE	COPE2763	C	ROUTINE TO PRINT RESULTS OF APPROXIMATE ANALYSIS/OPTIMIZATION.	COPE2823	
	AJJ=A(JJ)	COPE2764	C	*****	COPE2824	
	DO 180 L=1,NF	COPE2765	C		COPE2825	
180	B(J,L)=B(J,L)-AJJ*G(L)	COPE2766	C	BY G. N. VANDERPLAATS	JAN., 1979.	COPE2826
190	CONTINUE	COPE2767	C	NASA AMES RESEARCH CENTER, MOFFETT FIELD, CALIF.	COPE2827	
	NER=0	COPE2768	C		COPE2828	
	RETURN	COPE2769	C	-----	COPE2829	
200	CONTINUE	COPE2770	C	TITLE.	COPE2830	
	AKK=A(1)	COPE2771	C	-----	COPE2831	
	NER=1	COPE2772	C	WRITE (6,90) (TITLE(I),I=1,20)	COPE2832	
	IF (ABS(AKK).LT.1.0E-20) GO TO 220	COPE2773	C	-----	COPE2833	
	AKK=1./AKK	COPE2774	C	GLOBAL LOCATION OF X AND F(X)	COPE2834	
	DO 210 J=1,NF	COPE2775	C	-----	COPE2835	
210	B(1,J)=B(1,J)*AKK	COPE2776	C	GLOBAL LOCATIONS OF X.	COPE2836	
	NER=0	COPE2777	C	M5=LOCI(5)	COPE2837	
	RETURN	COPE2778	C	M5=M5+HXAPRX-1	COPE2838	
220	CONTINUE	COPE2779	C	WRITE (6,100)	COPE2839	
	RETURN	COPE2780	C	WRITE (6,110) (IA(I),I=M5,MM5)	COPE2840	
	END	COPE2781	C	GLOBAL LOCATIONS OF F(X).	COPE2841	
	SUBROUTINE COPE13 (X,F,NX,M)	COPE2782	C	M6=LOCI(6)	COPE2842	
	DIMENSION X(1), F(1)	COPE2783	C	MM6=M6+NF-1	COPE2843	
C	*****	COPE2784	C	WRITE (6,140)	COPE2844	
C	ROUTINE TO CALCULATE F VALUES FOR LEAST SQUARES FIT TO QUADRATIC	COPE2785	C	WRITE (6,110) (IA(I),I=M6,MM6)	COPE2845	
C	Y-YO = DY-TRANSPOSE TIMES X + (1/2 X-TRANSPOSE TIMES H TIMES X.	COPE2786	C	-----	COPE2846	
C	*****	COPE2787	C	X-VALUES AND FUNCTIONS, F(X)	COPE2847	
C		COPE2788	C	-----	COPE2848	
C	BY G. N. VANDERPLAATS	COPE2789	C	X-VALUES.	COPE2849	
C	X CONTAINS X-X0.	COPE2790	C	N1=LOCR(23)+3*NXAPRX+6	COPE2850	
C	M = MAXIMUM NUMBER OF COEFFICIENTS TO BE CALCULATED.	COPE2791	C	N2=N1+NXAPRX-1	COPE2851	
C	M .LE. NX + (NX+1)/2.	COPE2792	C	WRITE (6,120) NPTOT,INOM	COPE2852	
C	DY COEF.	COPE2793	C	WRITE (6,130) (RA(I),I=N1,N2)	COPE2853	
C	DO 10 I=1,NX	COPE2794	C	F(X) VALUES.	COPE2854	
10	F(I)=X(I)	COPE2795	C	N1=N1+NXAPRX+NDV	COPE2855	
C	H COEF. = X1*X1, X2*X2, ... XN*XN, X1*X2... X1*XN...	COPE2796	C	N2=N1+NF-1	COPE2856	
	II=NX	COPE2797	C	WRITE (6,150)	COPE2857	
C	-----	COPE2798	C	WRITE (6,130) (RA(I),I=N1,N2)	COPE2858	
C	DIAGONAL ELEMENTS.	COPE2799	C	-----	COPE2859	
C	-----	COPE2800	C	TAYLER SERIES COEFFICIENTS.	COPE2860	
	DO 20 I=1,NX	COPE2801	C	-----	COPE2861	
	II=II+1	COPE2802	C	WRITE (6,170)	COPE2862	
	IF (II.GT.M) GO TO 40	COPE2803	C	NP=NPTOT-1	COPE2863	
20	F(II)=.5*(X(II)**2)	COPE2804	C	NBTAY=N1+2*NF	COPE2864	
	IF (NX.LT.2) RETURN	COPE2805	C	NBR=NXAPRX+(NXAPRX*(NXAPRX+1))/2	COPE2865	
C	-----	COPE2806	C	IF (MAXTRM.LT.3) NBR=1+MAXTRM*NXAPRX	COPE2866	
C	OFF-DIAGONAL ELEMENTS.	COPE2807	C	DO 30 JJ=1,NF	COPE2867	
C	-----	COPE2808	C	M6=LOCI(6)+JJ-1	COPE2868	
	NXM1=NX-1	COPE2809	C	M6=IA(M6)	COPE2869	
	DO 30 I=1,NXM1	COPE2810	C	WRITE (6,80) JJ,M6	COPE2870	
	IP1=I+1	COPE2811	C	LINEAR TERMS.	COPE2871	
	DO 30 J=IP1,NX	COPE2812	C	NC=NXAPRX	COPE2872	
	II=II+1	COPE2813	C	IF (NP.LT.H2) N2=NP	COPE2873	
	IF (II.GT.M) GO TO 40	COPE2814	C	N2=N2+NBTAY-1	COPE2874	

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WRITE (6,160)
WRITE (6,130) (RA(I),I=NBTAY,N2)
IF (NP.LE.NXAPRX) GO TO 20
IF (MAXTRM.LT.2) GO TO 20
C
NON-LINEAR TERMS.
C
N1 = LOCATION OF FIRST DIAGONAL ELEMENT.
N1=N2+1
C
N2 = LOCATION OF LAST DIAGONAL ELEMENT.
N2=NXAPRX
IF (N2.GT.NP) N2=NP
N2=N2*N1-1
C
N3=LOCATION OF FIRST OFF-DIAGONAL ELEMENT.
N3=N2+1
C
N4=LOCATION OF LAST OFF-DIAGONAL ELEMENT.
N4=NBR
IF (N4.GT.NP) N4=NP
N4=N4-2*NXAPRX+N3-1
C
LL = LOCATION OF LAST OFF-DIAGONAL ELEMENT - THIS ROW.
WRITE (6,190)
II=1
DO 10 I=N1,N2
WRITE (6,180) II
II=II+1
LL=N3+NXAPRX-II
IF (LL.GT.N4) LL=N4
IF (LL.LT.N3) WRITE (6,130) RA(I)
IF (LL.GE.N3) WRITE (6,130) RA(I),(RA(J),J=N3,LL)
10
20
CONTINUE
NBTAY=NBTAY+NBR
30
CONTINUE
IF (IPAPRX.LT.3) RETURN
REMINO ISCR2
WRITE (6,50)
DO 40 I=1,NPTOT
C
X-VECTOR.
READ (ISCR2) (RA(J),J=1,NXAPRX)
WRITE (6,60) I
WRITE (6,130) (RA(J),J=1,NXAPRX)
C
FUNCTION VALUES.
READ (ISCR2) (RA(J),J=1,NF)
WRITE (6,70)
WRITE (6,130) (RA(J),J=1,NF)
40
CONTINUE
RETURN
C
-----
C
FORMATS
C
-----
50
FORMAT (///5X,18HSUMMARY OF DESIGNS)
60
FORMAT (/5X,13HDESIGN NUMBER,15/5X,8HX-VECTOR)
70
FORMAT (/5X,15HFUNCTION VALUES)
80
FORMAT (///5X,9HPARAMETER,15,18H = GLOBAL VARIABLE,15)
90
FORMAT (1H1,4X,44HRESULTS OF APPROXIMATE ANALYSIS/OPTIMIZATION///5COPE2927
1X,5HTITLE/5X,20A4)
100
FORMAT (///5X,31HGLOBAL LOCATIONS OF X-VARIABLES)
110
FORMAT (5X,10I5)
120
FORMAT (///5X,25HAPPROXIMATION IS BASED ON,15,8H DESIGNS//5X,31HNONCOPE2931
FINAL DESIGN IS DESIGN NUMBER,15//5X,21HVALUES OF X-VARIABLES)
130
FORMAT (5X,5E13.4)
140
FORMAT (///5X,35HGLOBAL LOCATIONS OF FUNCTIONS, F(X))
COPE2875 150
FORMAT (///5X,25HVALUES OF FUNCTIONS, F(X))
COPE2876 160
FORMAT (/5X,19HLINEAR TERMS, DEL F)
COPE2877 170
FORMAT (///5X,39HCOEFFICIENTS OF TAYLOR SERIES EXPANSION)
COPE2878 180
FORMAT (/5X,31HROW,15)
COPE2879 190
FORMAT (///5X,51HNON-LINEAR TERMS, H, BEGINING WITH DIAGONAL ELEMENTCOPE2939
1T)
COPE2880
END
COPE2881
SUBROUTINE COPE15 (XV,G,DF,A,ISC,IC,NN1,BLU,NX1,IOBJA,M,FNOM,FNEW,COPE2942
1BTAY,NBR,IGFN,CT,CTL,INFO,HAC,NCONA,NDV,NF,OBJ,SGHOPT)
COPE2883
DIMENSION XV(1), FNOM(1), FNEW(1), A(NN1,1), BTAY(NBR,1), DF(1), ICOPE2943
1GFN(1), ISC(1), IC(1), G(1), BLU(4,1)
COPE2884
*****
COPE2885
FUNCTION EVALUATION FOR APPROXIMATE OPTIMIZATION.
COPE2886
*****
C
BY G. N. VANDERPLAATS
COPE2889
NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF.
COPE2890
COPE2891
COPE2892
COPE2893
COPE2894
C
-----
C
OBJECTIVE.
C
-----
CALL COPE16 (NX1,XV,NF,FNOM,FNEW,BTAY,NBR,M)
COPE2895
OBJ=-FNEW(IOBJA)*SGNOPT
COPE2896
IF (INFO.EQ.1) GO TO 20
COPE2897
GRADIENT OF OBJECTIVE.
COPE2898
CALL COPE17 (HX1,XV,IOBJA,BTAY,NBR,M,DF)
COPE2899
DO 10 I=1,NDV
COPE2900
DF(I)=-DF(I)*SGNOPT
COPE2901
CONTINUE
COPE2902
IF (NCONA.LE.0) GO TO 80
COPE2903
C
-----
C
CONSTRAINTS.
C
-----
IF (INFO.EQ.2) NAC=0
COPE2904
ICON=0
COPE2905
DO 70 I=1,NCONA
COPE2906
J=IGFN(I)
COPE2907
GG=FNEW(J)
COPE2908
LOWER BOUND.
COPE2909
IF (BLU(1,I).LT.-1.0E+15) GO TO 40
COPE2910
ICON=ICON+1
COPE2911
G(ICON)=(BLU(1,I)-GG)/BLU(2,I)
COPE2912
IF (INFO.EQ.1) GO TO 40
COPE2913
IS THIS CONSTRAINT ACTIVE OR VIOLATED.
COPE2914
CTI=CT
COPE2915
IF (ISC(ICON).GT.0) CTI=CTL
COPE2916
IF (G(ICON).LT.CTI) GO TO 40
COPE2917
ACTIVE CONSTRAINT. CALCULATE GRADIENT.
COPE2918
NAC=NAC+1
COPE2919
IC(HAC)=ICON
COPE2920
MM=M
COPE2921
IF (ISC(ICON).GT.0) MM=NDV
COPE2922
CALL COPE17 (NX1,XV,J,BTAY,NBR,M,A(1,NAC))
COPE2923
FF=1./BLU(2,I)
COPE2924
DO 30 K=1,NDV
COPE2925
A(K,NAC)=-A(K,NAC)*FF
COPE2926
IF (BLU(3,I).GT.1.0E+15) GO TO 60
COPE2927
ICON=ICON+1
COPE2928
G(ICON)=1GG-BLU(3,I)/BLU(4,I)
COPE2929
IF (INFO.EQ.1) GO TO 60
COPE2930
IS THIS CONSTRAINT ACTIVE OR VIOLATED.
COPE2931
COPE2932
COPE2933
COPE2934
COPE2935
COPE2936
COPE2937
COPE2938
COPE2939
COPE2940
COPE2941
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COPE2985
COPE2986
COPE2987
COPE2988
COPE2989
COPE2990
COPE2991
COPE2992
COPE2993
COPE2994

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CTI=CT          COPE2995
IF (ISC(ICON).GT.0) CTI=CTL      COPE2996
IF (G(ICON).LT.CTI) GO TO 60    COPE2997
C ACTIVE CONSTRAINT. CALCULATE GRADIENT. COPE2998 20
NAC=NAC+1          COPE2999 C
IC(NAC)=ICON      COPE3000 C
MM=M              COPE3001 C
IF (ISC(ICON).GT.0) MM=NDV      COPE3002
CALL COPE17 (NX1,XV,J,BTAY,NBR,MM,A(1,NAC)) COPE3003
FF=1./BLU(4,I)    COPE3004
DO 50 K=1,NDV     COPE3005
50 A(K,NAC)=A(K,NAC)*FF        COPE3006
60 CONTINUE        COPE3007
70 CONTINUE        COPE3008
80 CONTINUE        COPE3009
RETURN            COPE3010 30
END               COPE3011 40
SUBROUTINE COPE16 (NX,X,NF,FNOM,FNEW,B,NBR,M) COPE3012 50
*****COPE3013
C ROUTINE TO EVALUATE FUNCTIONS APPROXIMATED BY TAYLER SERIES COPE3014
C EXPANSION UP TO SECOND ORDER. COPE3015
C *****COPE3016 C
C BY G. N. VANDERPLAATS MAR., 1978. COPE3017 C
C NAVAL SHIP R AND D CENTER. COPE3018 C
C COPE3019 C
C F = F0 + DELF TIMES X + X-TRANPOSE TIMES DEL2F TIMES X. COPE3020 C
C ARGUEMENTS. COPE3021 C
C NX - NUMBER OF INDEPENDENT VARIABLES CONTAINED IN X. COPE3022 C
C X - VECTOR OF DELTA VARIABLES X-XNDM. DIMENSIONED X(NX) COPE3023 C
C NF - NUMBER OF FUNCTIONS TO BE EVALUATED. COPE3024 C
C FNOM - NOMINAL FUNCTION VALUES ABOUT WHICH TAYLER SERIES EXPANSION COPE3025 C
C WAS DONE. COPE3026 C
C FNEW - NEW APPROXIMATED VALUES. - OUTPUT. DIMENSIONED FNEW(NF) COPE3027 C
C B - MATRIX OF TAYLER SERIES COEFFICIENTS. COPE3028 C
C B(I,J) CONTAINS DEL F, I=1,NX. COPE3029 C
C B(NX+I,J) CONTAINS DEL2 TERMS, I = 1,NX*(NX+1)/2. COPE3030 C
C MINIMUM DIMENSIONS - B(M,NF). COPE3031 C
C NBR - DIMENSIONED ROWS OF B. COPE3032 C
C M - TOTAL NUMBER OF COEFFICIENTS CURRENTLY USED. COPE3033 C
C COPE3034 C
C DIMENSION X(1), FNOM(1), FNEW(1), B(NBR,1) COPE3035
C DO 50 J=1,NF COPE3036
C -----COPE3037 C
C CONSTANT TERM. COPE3038 C
C -----COPE3039 C
C F=FNOM(J) COPE3040
C -----COPE3041
C FIRST ORDER TERMS. COPE3042 10
C -----COPE3043 C
C DO 10 I=1,NX COPE3044 C
C IF (I.GT.M) GO TO 40 COPE3045 C
C F=F+B(I,J)*X(I) COPE3046
C -----COPE3047 C
C SECOND ORDER TERMS. COPE3048 C
C -----COPE3049 C
C -----COPE3050
C -----COPE3051
C DIAGONAL ELEMENTS. COPE3052
C -----COPE3053 20
C II=NX COPE3054 C

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DO 20 I=1,NX          COPE3055
II=II+1              COPE3056
IF (II.GT.M) GO TO 40 COPE3057
F=F+.5*B(II,J)*X(II)*X(II)**2) COPE3058
-----COPE3059
OFF-DIAGONAL ELEMENTS. COPE3060
-----COPE3061
IF (NX.LT.2) GO TO 40 COPE3062
NXM1=NX-1           COPE3063
DO 30 I=1,NXM1      COPE3064
IP1=I+1             COPE3065
XX=X(I)             COPE3066
DO 30 K=IP1,NX      COPE3067
II=II+1             COPE3068
IF (II.GT.M) GO TO 40 COPE3069
F=F*B(II,J)*XX*X(K) COPE3070
CONTINUE            COPE3071
FNEW(J)=F           COPE3072
RETURN              COPE3073
END                 COPE3074
SUBROUTINE COPE17 (NX,X,J,B,NBR,M,GRAD) COPE3075
*****COPE3076
C ROUTINE TO CALCULATE GRADIENT OF THE J-TH FUNCTION APPROXIMATED COPE3077
C BY TAYLER SERIES EXPANSION UP TO SECOND ORDER. COPE3078
C *****COPE3079
C BY G. N. VANDERPLAATS APRIL, 1978. COPE3080
C HASA AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COPE3081
C COPE3082
C F = F0 + DELF TIMES X + .5 X-TRANPOSE TIMES DEL2F TIMES X. COPE3083
C ARGUEMENTS. COPE3084
C NX - NUMBER OF INDEPENDENT VARIABLES CONTAINED IN X. COPE3085
C X - VECTOR OF DELTA VARIABLES X-XNDM. DIMENSIONED X(NX) COPE3086
C J - FUNCTION FOR WHICH GRADIENT INFORMATION IS CALCULATED. COPE3087
C B - MATRIX OF TAYLER SERIES COEFFICIENTS. COPE3088
C B(I,J) CONTAINS DELF, I = 1,NX. COPE3089
C B(NX+I,J) CONTAINS DEL2 TERMS, I = 1,NS*(NX+1)/2. COPE3090
C MINIMUM DIMENSIONS - B(M,NF). COPE3091
C NSR - DIMENSIONED POWS OF B. COPE3092
C M - TOTAL NUMBER OF COEFFICIENTS CURRENTLY USED. COPE3093
C GRAD - GRADIENT OF J-TH FUNCTION. OUTPUT. COPE3094
C COPE3095
C DIMENSION X(1), B(NBR,1), GRAD(1) COPE3096
C -----COPE3097
C FIRST ORDER TERMS. COPE3098
C -----COPE3099
DO 10 I=1,NX          COPE3100
IF (I.GT.M) GO TO 40 COPE3101
GRAD(I)=B(I,J)       COPE3102
-----COPE3103
SECOND ORDER TERMS. COPE3104
-----COPE3105
II=NX                COPE3106
-----COPE3107
DIAGONAL ELEMENTS. COPE3108
-----COPE3109
DO 20 I=1,NX          COPE3110
II=II+1              COPE3111
IF (II.GT.M) GO TO 40 COPE3112
GRAD(II)=GRAD(I)*B(II,J)*X(II) COPE3113
-----COPE3114

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SUBROUTINE COMMIN (X,VLB,VUB,G,SCAL,DF,A,S,G1,G2,B,C,ISC,IC,MS1,HC,COMMIN 2
1,N2,N3,N4,N5) COMMIN 3
COMMON /CNMIN/ DELFUN,DABFUN,FDCH,FDCHM,CT,CTMIN,CTL,CTLMIN,ALPHAX,COMMIN 4
1,ABOBJ,THETA,OBJ,NDV,NCON,NSIDE,IPRINT,NFDG,NSCAL,LINOBJ,ITMAX,ITCOMMIN 5
2RM,ICNDIR,IGOTO,HAC,INFO,INFO,ITER COMMIN 6
DIMENSION X(N1),VLB(N1),VUB(N1),G(N2),SCAL(N1),DF(N1),A(N1),NCOMMIN 7
13),S(N1),G1(N2),G2(N2),BIN3,N3),C(N4),ISC(N2),IC(N3),MS1,NCOMMIN 8
25) COMMIN 9
COMMON /CONSAV/ DM1,DM2,DM3,DM4,DM5,DM6,DM7,DM8,DM9,DM10,DM11,DM12,COMMIN10
1,DCT,DCTL,PHI,ABOBJ,CTA,CTAM,CTBM,OBJ1,SLOPE,DX,DX1,FI,XI,DF,DF1,ACOMMIN11
2LP,FFF,A1,A2,A3,A4,F1,F2,F3,F4,CV1,CV2,CV3,CV4,APP,ALPCA,ALPFES,ALCOMMIN12
3PLN,ALPHIN,ALPHC,ALPSAV,ALPSID,ALPTOT,RSRACE,IDM1,IDM2,IDM3,JDIR,ICOMMIN13
4OBJ,KOBJ,KCOUNT,NCAL(2),NFEAS,MSCAL,NCOBJ,NVC,KOUNT,ICOUNT,IGOOD1,COMMIN14
5IGOOD2,IGOOD3,IGOOD4,IBEST,III,NLNC,IGOTO,ISPACE(2) COMMIN15
ROUTINE TO SOLVE CONSTRAINED OR UNCONSTRAINED FUNCTION COMMIN16
MINIMIZATION. COMMIN17
BY G. N. VANDERPLAATS APRIL, 1972. COMMIN18
***** JUNE, 1979 VERSION ***** COMMIN19
NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COMMIN20
REFERENCE; COMMIN - A FORTRAN PROGRAM FOR CONSTRAINED FUNCTION COMMIN21
MINIMIZATION: USER'S MANUAL, BY G. N. VANDERPLAATS, COMMIN22
NASA TM X-62,282, AUGUST, 1973. COMMIN23
STORAGE REQUIREMENTS: COMMIN24
PROGRAM - 7000 DECIMAL WORDS (CDC COMPUTER) COMMIN25
ARRAYS - APPROX. 2*(NDV**2)*26*NDV*4*NCON, COMMIN26
WHERE N3 = NDV*2. COMMIN27
RE-SCALE VARIABLES IF REQUIRED. COMMIN28
IF (NSCAL.EQ.0.OR.IGOTO.EQ.0) GO TO 20 COMMIN29
DO 10 I=1,NDV COMMIN30
X(I)=C(I) COMMIN31
CONTINUE COMMIN32
CONSTANTS. COMMIN33
NDV1=NDV*1 COMMIN34
NDV2=NDV*2 COMMIN35
IF (IGOTO.EQ.0) GO TO 40 COMMIN36
-----
CHECK FOR UNBOUNDED SOLUTION COMMIN37
-----
STOP IF OBJ IS LESS THAN -1.0E+40 COMMIN38
IF (OBJ.GT.-1.0E+40) GO TO 30 COMMIN39
WRITE (6,980) COMMIN40
GO TO 810 COMMIN41
CONTINUE COMMIN42
GO TO (160,390,380,670,690),IGOTO COMMIN43
-----
SAVE INPUT CONTROL PARAMETERS COMMIN44
-----
CONTINUE COMMIN45
IF (IPRINT.GT.0) WRITE (6,1220) COMMIN46
IF (LINOBJ.EQ.0.OR.(NCON.GT.0.OR.NSIDE.GT.0)) GO TO 50 COMMIN47
TOTALLY UNCONSTRAINED FUNCTION WITH LINEAR OBJECTIVE. COMMIN48
SOLUTION IS UNBOUNDED. COMMIN49
WRITE (6,970) LINOBJ,NCON,NSIDE COMMIN50
RETURN COMMIN51
50 CONTINUE COMMIN52
IDM1=ITRM COMMIN53
IDM2=ITMAX COMMIN54
IDM3=ICNDIR COMMIN55
DM1=DELFUN COMMIN56
DM2=DABFUN COMMIN57

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DM3=CT COMMIN58
DM4=CTMIN COMMIN59
DM5=CTL COMMIN60
DM6=CTLMIN COMMIN61
DM7=THETA COMMIN62
DM8=PHI COMMIN63
DM9=FDCH COMMIN64
DM10=FDCHM COMMIN65
DM11=AEDEJI COMMIN66
DM12=ALPHAX COMMIN67
-----
DEFAULTS COMMIN68
-----
IF (ITRM.LE.0) ITRM=3 COMMIN69
IF (ITMAX.LE.0) ITMAX=20 COMMIN70
NDV1=NDV*1 COMMIN71
IF (ICNDIR.EQ.0) ICNDIR=NDV1 COMMIN72
IF (DELFUN.LE.0) DELFUN=.0001 COMMIN73
CT=-ABS(CT) COMMIN74
IF (CT.GE.0.) CT=-.1 COMMIN75
CTMIN=ABS(CTMIN) COMMIN76
IF (CTMIN.LE.0.) CTMIN=.004 COMMIN77
CTL=-ABS(CTL) COMMIN78
IF (CTL.GE.0.) CTL=-0.01 COMMIN79
CTLMIN=ABS(CTLMIN) COMMIN80
IF (CTLMIN.LE.0.) CTLMIN=.001 COMMIN81
IF (THETA.LE.0.) THETA=1. COMMIN82
IF (ABOBJ.LE.0.) ABOBJ=-1 COMMIN83
IF (ALPHAX.LE.0.) ALPHAX=.1 COMMIN84
IF (FDCH.LE.0.) FDCH=.01 COMMIN85
IF (FDCHM.LE.0.) FDCHM=.01 COMMIN86
-----
INITIALIZE INTERNAL PARAMETERS COMMIN87
-----
INFOG=0 COMMIN88
ITER=0 COMMIN89
JDIR=0 COMMIN90
IOBJ=0 COMMIN91
KOBJ=0 COMMIN92
NDV2=NDV*2 COMMIN93
KCOUNT=0 COMMIN94
NCAL(1)=0 COMMIN95
NCAL(2)=0 COMMIN96
NAC=0 COMMIN97
NFEAS=0 COMMIN98
MSCAL=MSCAL COMMIN99
CT1=ITRM COMMIN100
CT1=1./CT1 COMMIN101
DCT=(CTMIN/ABS(CT))*CT1 COMMIN102
DCTL=(CTLMIN/ABS(CTL))*CT1 COMMIN103
PHI=5. COMMIN104
ABOBJ=ABOBJ1 COMMIN105
NCOBJ=0 COMMIN106
CTAM=ABS(CTMIN) COMMIN107
CTPM=ABS(CTLMIN) COMMIN108
CALCULATE NUMBER OF LINEAR CONSTRAINTS, NLNC. COMMIN109
NLNC=0 COMMIN110
IF (NCON.EQ.0) GO TO 70 COMMIN111
DO 60 I=1,NCON COMMIN112
IF (ISC(I).GT.0) NLNC=NLNC+1 COMMIN113

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30 CONTINUE                                COMHI122 C ----- PRINT INITIAL DESIGN INFORMATION                                COMHI182
70 CONTINUE                                COMHI123 C ----- COMHI183
----- COMHI124 ----- COMHI184
CHECK TO BE SURE THAT SIDE CONSTRAINTS APE SATISFIED COMHI125 COMHI185
----- COMHI126 ----- COMHI186
IF (NSIDE.EQ.0) GO TO 110                  COMHI127 COMHI187
DO 100 I=1,NDV                             COMHI128 COMHI188
IF (VLBI).LE.VUB(I) GO TO 80              COMHI129 COMHI189
XX=-.5*(VLBI+VUB(I))                      COMHI130 COMHI190
X(I)=XX                                    COMHI131 COMHI191
VLBI=XX                                    COMHI132 COMHI192
VUB(I)=XX                                  COMHI133 COMHI193
WRITE (6,1120) I                          COMHI134 COMHI194
90 CONTINUE                                COMHI135 170 WRITE (6,1010) I,(VLBI(J),J=I,M1) COMHI195
XX=X(I)-VLBI(I)                          COMHI136 COMHI196
IF (XX.GE.0.) GO TO 90                    COMHI137 COMHI197
LOWER BOUND VIOLATED.                    COMHI138 COMHI198
WRITE (6,1130) X(I),VLBI(I),I           COMHI139 180 WRITE (6,1010) I,(VUB(J),J=I,M1) COMHI199
X(I)=VLBI(I)                             COMHI140 190 CONTINUE COMHI200
GO TO 100                                  COMHI141 COMHI201
90 CONTINUE                                COMHI142 COMHI202
XX=VUB(I)-X(I)                          COMHI143 COMHI203
IF (XX.GE.0.) GO TO 100                  COMHI144 200 CONTINUE COMHI204
WRITE (6,1140) X(I),VUB(I),I           COMHI145 COMHI205
X(I)=VUB(I)                              COMHI146 COMHI206
100 CONTINUE                              COMHI147 COMHI207
110 CONTINUE                              COMHI148 COMHI208
----- COMHI149 ----- COMHI209
INITIALIZE SCALING VECTOR, SCAL          COMHI150 210 WRITE (6,1030) I,(ISC(J),J=I,M1) COMHI210
----- COMHI151 ----- COMHI211
IF (NSCAL.EQ.0) GO TO 150                COMHI152 220 IF (NLNC.EQ.NCON) WRITE (6,1040) COMHI212
IF (NSCAL.LT.0) GO TO 130               COMHI153 COMHI213
DO 120 I=1,NDV                           COMHI154 230 CONTINUE COMHI214
120 SCAL(I)=1.                            COMHI155 WRITE (6,1440) OBJ COMHI215
GO TO 150                                 COMHI156 WRITE (6,1450) COMHI216
130 CONTINUE                              COMHI157 DO 240 I=1,NDV COMHI217
DO 140 I=1,NDV                           COMHI158 X1=1. COMHI218
SI=ABS(SCAL(I))                          COMHI159 IF (NSCAL.NE.0) X1=SCAL(I) COMHI219
IF (SI.LT.1.0E-20) SI=1.0E-5           COMHI160 240 G1(I)=X(I)*X1 COMHI220
SCAL(I)=SI                                COMHI161 DO 250 I=1,NDV,6 COMHI221
SI=1./SI                                  COMHI162 M1=MIN0(NDV,I+5) COMHI222
X(I)=X(I)*SI                             COMHI163 250 WRITE (6,1010) I,(G1(J),J=I,M1) COMHI223
IF (NSIDE.EQ.0) GO TO 140               COMHI164 IF (NCON.EQ.0) GO TO 270 COMHI224
VLBI)=VLBI)*SI                          COMHI165 WRITE (6,1470) COMHI225
VUB(I)=VUB(I)*SI                        COMHI166 DO 260 I=1,NCON,6 COMHI226
140 CONTINUE                              COMHI167 M1=MIN0(NCON,I+5) COMHI227
150 CONTINUE                              COMHI168 260 WRITE (6,1010) I,(G(J),J=I,M1) COMHI228
----- COMHI169 ----- COMHI229
***** CALCULATE INITIAL FUNCTION AND CONSTRAINT VALUES ***** COMHI170 270 CONTINUE COMHI230
----- COMHI171 ----- COMHI231
INFO=1                                    COMHI172 C ----- COMHI232
NSCAL(I)=1                                COMHI173 C ----- COMHI233
IGOTO=1                                   COMHI174 C ----- COMHI234
GO TO 950                                  COMHI175 280 CONTINUE COMHI235
160 CONTINUE                              COMHI176 ITER=ITER+1 COMHI236
OBJJ=OBJ                                  COMHI177 IF (ABOBJJ.LT..0001) ABOBJJ=.0001 COMHI237
IF (DABFUN.LE.0.) DABFUN=.001*ABS(OBJJ) COMHI178 IF (ABOBJJ.GT..2) ABOBJJ=.2 COMHI238
IF (DABFUN.LT.1.0E-10) DABFUN=1.0E-10 COMHI179 IF (ALPHAX.GT.1.) ALPHAX=1. COMHI239
IF (IPRINT.LE.0) GO TO 270              COMHI180 IF (ALPHAX.LT..001) ALPHAX=.001 COMHI240
----- COMHI181 ----- COMHI241
IF (IPRINT.GT.3.AND.NCON.GT.0) WRITE (6,1320) CT,CTL,PHI

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	CTA=ABS(CT)	COMMI242	IGOTO=2	COMMI302
	IF (NCOBJ.EQ.0) GO TO 340	COMMI243	GO TO 950	COMMI303
C	-----	COMMI244	370 CONTINUE	COMMI304
C	NO MOVE ON LAST ITERATION. DELETE CONSTRAINTS THAT ARE NO	COMMI245	JGOTO=0	COMMI305
C	LONGER ACTIVE.	COMMI246	380 CONTINUE	COMMI306
C	-----	COMMI247	CALL CHH01 (JGOTO,X,DF,G,ISC,IC,A,G1,VLB,VUB,SCAL,C,HCAL,DX,DX1,F	COMMI307
	NNAC=NAC	COMMI248	I1,X1,I11,H1,H2,H3,H4)	COMMI308
	DO 290 I=1,NNAC	COMMI249	IGOTO=3	COMMI309
	IF (IC(I).GT.NCON) NAC=NAC-1	COMMI250	IF (JGOTO.GT.0) GO TO 950	COMMI310
290	CONTINUE	COMMI251	390 CONTINUE	COMMI311
	IF (NAC.LE.0) GO TO 420	COMMI252	INFO=1	COMMI312
	NNAC=NAC	COMMI253	IF (NAC.GE.H3) GO TO 810	COMMI313
	DO 330 I=1,NNAC	COMMI254	IF (HCAL.EQ.0.OP.NFDG.EQ.0) GO TO 420	COMMI314
300	NIC=IC(I)	COMMI255	-----	COMMI315
	CT1=CT	COMMI256	C SCALE GRADIENTS	COMMI316
	IF (ISC(NIC).GT.0) CT1=CTL	COMMI257	-----	COMMI317
	IF (G(NIC).GT.CT1) GO TO 330	COMMI258	C SCALE GRADIENT OF OBJECTIVE FUNCTION.	COMMI318
	NAC=NAC-1	COMMI259	DO 400 I=1,NDV	COMMI319
	IF (I.GT.NAC) GO TO 420	COMMI260	400 DF(I)=DF(I)*SCAL(I)	COMMI320
	DO 320 K=1,NAC	COMMI261	IF (NFDG.EQ.2.OR.NAC.EQ.0) GO TO 420	COMMI321
	II=K+1	COMMI262	C SCALE GRADIENTS OF ACTIVE CONSTRAINTS.	COMMI322
	DO 310 J=1,NDV2	COMMI263	DO 410 J=1,NDV	COMMI323
310	A(J,K)=A(J,II)	COMMI264	SCJ=SCAL(J)	COMMI324
320	IC(K)=IC(II)	COMMI265	DO 410 I=1,NAC	COMMI325
	GO TO 300	COMMI266	410 A(J,I)=A(J,I)*SCJ	COMMI326
330	CONTINUE	COMMI267	420 CONTINUE	COMMI327
	GO TO 420	COMMI268	IF (IPPRINT.LT.3.OP.NCON.EQ.0) GO TO 470	COMMI328
340	CONTINUE	COMMI269	-----	COMMI329
	IF (MSCAL.LT.MSCAL.OP.MSCAL.EQ.0) GO TO 360	COMMI270	C PRINT	COMMI330
	IF (MSCAL.LT.0.AND.KCOUNT.LT.ICNDIR) GO TO 360	COMMI271	-----	COMMI331
	MSCAL=0	COMMI272	C PPINT ACTIVE AND VIOLATED CONSTRAINT NUMBERS.	COMMI332
	KCOUNT=0	COMMI273	M1=0	COMMI333
C	-----	COMMI274	M2=H3	COMMI334
C	SCALE VARIABLES	COMMI275	IF (NAC.EQ.0) GO TO 450	COMMI335
C	-----	COMMI276	DO 440 I=1,NAC	COMMI336
	DO 350 I=1,NDV	COMMI277	J=IC(I)	COMMI337
	SI=SCAL(I)	COMMI278	IF (J.GT.NCON) GO TO 440	COMMI338
	XI=SI*X(I)	COMMI279	GI=G(J)	COMMI339
	SIB=SI	COMMI280	C1=CTAH	COMMI340
	IF (MSCAL.GT.0) SI=ABS(XI)	COMMI281	IF (ISC(I).GT.0) C1=CTEM	COMMI341
	IF (SI.LT.1.0E-10) GO TO 350	COMMI282	GI=GI-C1	COMMI342
	SCAL(I)=SI	COMMI283	IF (GI.GT.0.) GO TO 430	COMMI343
	SI=1./SI	COMMI284	C ACTIVE CONSTRAINT.	COMMI344
	X(I)=XI*SI	COMMI285	M1=M1+1	COMMI345
	IF (NSIDE.EQ.0) GO TO 350	COMMI286	MS1(M1)=J	COMMI346
	VLB(I)=SIB*SI*VLB(I)	COMMI287	GO TO 440	COMMI347
	VUB(I)=SIB*SI*VUB(I)	COMMI288	430 M2=M2+1	COMMI348
350	CONTINUE	COMMI289	C VIOLATED CONSTRAINT.	COMMI349
	IF (IPRINT.LT.4.OP.(MSCAL.LT.0.AND.ITER.GT.1)) GO TO 360	COMMI290	MS1(M2)=J	COMMI350
	WRITE (6,1330)	COMMI291	440 CONTINUE	COMMI351
	WRITE (6,1460) (SCAL(I),I=1,NDV)	COMMI292	450 M3=M2-H3	COMMI352
360	CONTINUE	COMMI293	WRITE (6,1060) M1	COMMI353
	MSCAL=MSCAL*1	COMMI294	IF (M1.EQ.0) GO TO 460	COMMI354
	NAC=0	COMMI295	WRITE (6,1070)	COMMI355
C	-----	COMMI296	WRITE (6,1480) (MS1(I),I=1,M1)	COMMI356
C	OBTAIN GRADIENTS OF OBJECTIVE AND ACTIVE CONSTRAINTS	COMMI297	460 WRITE (6,1080) H3	COMMI357
C	-----	COMMI298	IF (H3.EQ.0) GO TO 470	COMMI358
	INFO=2	COMMI299	WRITE (6,1070)	COMMI359
	NCAL(2)=NCAL(2)+1	COMMI300	H3=H3*1	COMMI360
	IF (NFDG.NE.1) GO TO 370	COMMI301	WRITE (6,1460) (MS1(I),I=M3,M2)	COMMI361

470	CONTINUE	COHMI362	IF (NAC.EQ.0) GO TO 570	COHMI422
C	-----	COHMI363	WRITE (6,1350)	COHMI423
C	CALCULATE GRADIENTS OF ACTIVE SIDE CONSTRAINTS	COHMI364	DO 560 I=1,NAC	COHMI424
C	-----	COHMI365	M1=IC(I)	COHMI425
	IF (NSIDE.EQ.0) GO TO 530	COHMI366	M2=M1-NCON	COHMI426
	MCN1=NCON	COHMI367	M3=0	COHMI427
	M1=0	COHMI368	IF (M2.GT.0) M3=IABS(MS1(M2))	COHMI428
C	DO 510 I=1,NDV	COHMI369	IF (M2.LE.0) WRITE (6,990) M1	COHMI429
	LOWER BOUND.	COHMI370	IF (M2.GT.0) WRITE (6,1000) M3	COHMI430
	XI=X(I)	COHMI371	DO 550 K=1,NDV,6	COHMI431
	XID=VLB(I)	COHMI372	M1=MIN0(NDV,K+5)	COHMI432
	XI2=ABS(XID)	COHMI373	550 WRITE (6,1010) K,(A(J,I),J=K,M1)	COHMI433
	IF (XI2.LT.1.) XI2=1.	COHMI374	560 WRITE (6,1360)	COHMI434
	GI=(XID-XI)/XI2	COHMI375	570 CONTINUE	COHMI435
	IF (GI.LT.-1.0E-6) GO TO 490	COHMI376	-----	COHMI436
	M1=M1+1	COHMI377	***** DETERMINE SEARCH DIRECTION *****	COHMI437
	MS1(M1)=-I	COHMI378	-----	COHMI438
	NAC=NAC+1	COHMI379	ALP=1.0E+20	COHMI439
	IF (NAC.GE.N3) GO TO 810	COHMI380	IF (NAC.GT.0) GO TO 580	COHMI440
	MCN1=MCN1+1	COHMI381	-----	COHMI441
	DO 480 J=1,NDV	COHMI382	UNCONSTRAINED FUNCTION	COHMI442
480	A(J,NAC)=0.	COHMI383	-----	COHMI443
	A(I,NAC)=-1.	COHMI384	FIND DIRECTION OF STEEPEST DESCENT OR CONJUGATE DIRECTION.	COHMI444
	IC(NAC)=MCN1	COHMI385	NVC=0	COHMI445
	G(MCN1)=GI	COHMI386	NFEAS=0	COHMI446
	ISC(MCN1)=1	COHMI387	KCOUNT=KCOUNT+1	COHMI447
C	UPPER BOUND.	COHMI388	IF KCOUNT.GT.ICNDIR RESTART CONJUGATE DIRECTION ALGORITHM.	COHMI448
490	XID=VUB(I)	COHMI389	IF (KCOUNT.GT.ICNDIR.OR.IOBJ.EQ.2) KCOUNT=1	COHMI449
	XI2=ABS(XID)	COHMI390	IF (KCOUNT.EQ.1) JDIR=0	COHMI450
	IF (XI2.LT.1.) XI2=1.	COHMI391	IF JDIR = 0 FIND DIRECTION OF STEEPEST DESCENT.	COHMI451
	GI=(XI-XID)/XI2	COHMI392	CALL CMMH02 (JDIR,SLOPE,DFTDF1,DF,S,N1)	COHMI452
	IF (GI.LT.-1.0E-6) GO TO 510	COHMI393	GO TO 630	COHMI453
	M1=M1+1	COHMI394	580 CONTINUE	COHMI454
	MS1(M1)=I	COHMI395	-----	COHMI455
	NAC=NAC+1	COHMI396	CONSTRAINED FUNCTION	COHMI456
	IF (NAC.GE.N3) GO TO 810	COHMI397	-----	COHMI457
	MCN1=MCN1+1	COHMI398	FIND USABLE-FEASIBLE DIRECTION.	COHMI458
	DO 500 J=1,NDV	COHMI399	KCOUNT=0	COHMI459
500	A(J,NAC)=0.	COHMI400	JDIR=0	COHMI460
	A(I,NAC)=1.	COHMI401	PHI=10.*PHI	COHMI461
	IC(NAC)=MCN1	COHMI402	IF (PHI.GT.1000.) PHI=1000.	COHMI462
	G(MCN1)=GI	COHMI403	CALCULATE DIRECTION, S.	COHMI463
	ISC(MCN1)=1	COHMI404	CALL CMMH05 (G,DF,A,S,B,C,SLOPE,PHI,ISC,IC,MS1,NVC,N1,N2,N3,N4,N5)	COHMI464
510	CONTINUE	COHMI405	IF (IPRINT.LT.3) GO TO 600	COHMI465
C	-----	COHMI406	WRITE (6,1370)	COHMI466
C	PRINT	COHMI407	DO 590 I=1,NAC,6	COHMI467
C	-----	COHMI408	M1=MIN0(NAC,I+5)	COHMI468
	PRINT ACTIVE SIDE CONSTRAINT NUMBERS.	COHMI409	590 WRITE (6,1010) I,(A(NDV1,J),J=I,M1)	COHMI469
	IF (IPRINT.LT.3) GO TO 530	COHMI410	WRITE (6,1210) S(NDV1)	COHMI470
	WRITE (6,1090) M1	COHMI411	600 CONTINUE	COHMI471
	IF (M1.EQ.0) GO TO 530	COHMI412	-----	COHMI472
	WRITE (6,1100)	COHMI413	***** ONE-DIMENSIONAL SEARCH *****	COHMI473
	WRITE(6,1480) (MS1(J),J=1,M1)	COHMI414	-----	COHMI474
530	CONTINUE	COHMI415	IF (S(NDV1).LT.1.0E-6.AND.NVC.EQ.0) GO TO 710	COHMI475
C	PRINT GRADIENTS OF ACTIVE AND VIOLATED CONSTRAINTS.	COHMI416	-----	COHMI476
	IF (IPRINT.LT.4) GO TO 570	COHMI417	FIND ALPHA TO OBTAIN A FEASIBLE DESIGN	COHMI477
	WRITE (6,1340)	COHMI418	-----	COHMI478
	DO 540 I=1,NDV,6	COHMI419	IF (NVC.EQ.0) GO TO 630	COHMI479
	M1=MIN0(NDV,I+5)	COHMI420	ALP=-1.	COHMI480
540	WRITE (6,1010) I,(DF(J),J=I,M1)	COHMI421	DO 620 I=1,NAC	COHMI481

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NCI=IC(I)
C1=G(NCI)
CTC=CTAM
IF (ISC(NCI).GT.0) CTC=CTBM
IF (C1.LE.CTC) GO TO 620
ALP1=0.
DO 610 J=1,NDV
610 ALP1=ALP1+S(J)*A(J,I)
ALP1=ALP1*A(NDV2,I)
IF (ABS(ALP1).LT.1.0E-20) GO TO 620
ALP1=-C1/ALP1
IF (ALP1.GT.ALPH) ALP=ALP1
620 CONTINUE
630 CONTINUE
C -----
C LIMIT CHANCE TO ABOBJ1*OBJ
C -----
ALP1=1.0E+20
SI=ABS(OBJ)
IF (SI.LT..01) SI=.01
IF (ABS(SLOPE).GT.1.0E-20) ALP1=ABOBJ1*SI/SLOPE
ALP1=ABS(ALP1)
IF (NVC.GT.0) ALP1=10.*ALP1
IF (ALP1.LT.ALPH) ALP=ALP1
C -----
C LIMIT CHANGE IN VARIABLE TO ALPHAX
C -----
ALP11=1.0E+20
DO 640 I=1,NDV
SI=ABS(S(I))
XI=ABS(X(I))
IF (SI.LT.1.0E-10.OR.XI.LT.0.1) GO TO 640
ALP1=ALPHAX*SI/SI
IF (ALP1.LT.ALPH1) ALP11=ALP1
640 CONTINUE
IF (NVC.GT.0) ALP11=10.*ALP11
IF (ALP11.LT.ALPH) ALP=ALP11
IF (ALP.GT.1.0E+20) ALP=1.0E+20
IF (ALP.LE.1.0E-20) ALP=1.0E-20
IF (IPRINT.LT.3) GO TO 660
WRITE (6,1380)
DO 650 I=1,NDV,6
M1=MIN0(NDV,I+5)
650 WRITE (6,1010) I,(S(J),J=I,M1)
WRITE (6,1110) SLOPE,ALP
660 CONTINUE
IF (NCON.GT.0.OR.NSIDE.GT.0) GO TO 680
C -----
C DO ONE-DIMENSIONAL SEARCH FOR UNCONSTRAINED FUNCTION
C -----
JGOTO=0
670 CONTINUE
CALL CHH03 (X,S,SLOPE,ALP,FFF,A1,A2,A3,A4,F1,F2,F3,F4,APP,N1,NCAL,
1,KOUNT,JGOTO)
IGOTO=4
IF (JGOTO.GT.0) GO TO 950
JDIR=1
PROCEED TO CONVERGENCE CHECK.
GO TO 700
C -----
CONM1482 C SOLVE ONE-DIMENSIONAL SEARCH PROBLEM FOR CONSTRAINED FUNCTION CONM1542
CONM1483 C ----- CONM1543
CONM1484 680 CONTINUE CONM1544
CONM1485 JGOTO=0 CONM1545
CONM1486 690 CONTINUE CONM1546
CONM1487 CALL CHH06 (X,VLB,VUB,G,SCAL,DF,S,G1,G2,CTAM,CTBM,SLOPE,ALP,A2,A3,CONM1547
CONM1488 1,A4,F1,F2,F3,CV1,CV2,CV3,CV4,ALPCA,ALPFES,ALPLN,ALPHIN,ALPNC,ALPSA,CONM1548
CONM1489 2V,ALPSIO,ALPTOT,ISC,N1,HC,NCAL,NVC,ICOUNT,IGOOD1,IGOOD2,IGOOD3,IGOO,CONM1549
CONM1490 30D4,IBEST,III,HLIC,JGOTO) CONM1550
CONM1491 IGOTO=5 CONM1551
CONM1492 IF (JGOTO.GT.0) GO TO 950 CONM1552
CONM1493 IF (NAC.EQ.0) JDIR=1 CONM1553
C ----- CONM1554
C ***** UPDATE ALPHAX ***** CONM1555
C ----- CONM1556
CONM1497 700 CONTINUE CONM1557
CONM1498 710 CONTINUE CONM1558
CONM1499 IF (ALP.GT.1.0E+19) ALP=0. CONM1559
CONM1500 C UPDATE ALPHAX TO BE AVERAGE OF MAXIMUM CHANGE IN X(I) CONM1560
CONM1501 C AND ALPHAX. CONM1561
CONM1502 ALP11=0. CONM1562
CONM1503 DO 720 I=1,NDV CONM1563
CONM1504 SI=ABS(S(I)) CONM1564
CONM1505 XI=ABS(X(I)) CONM1565
CONM1506 IF (XI.LT.1.0E-10) GO TO 720 CONM1566
CONM1507 ALP1=ALP*SI/XI CONM1567
CONM1508 IF (ALP1.GT.ALPH1) ALP11=ALP1 CONM1568
CONM1509 720 CONTINUE CONM1569
CONM1510 ALP11=.5*(ALP11+ALPHAX) CONM1570
CONM1511 ALP12=.5*ALPHAX CONM1571
CONM1512 IF (ALP11.GT.ALPH1) ALP11=ALP12 CONM1572
CONM1513 ALPHAX=ALP11 CONM1573
CONM1514 NCOBJ=NCOBJ+1 CONM1574
CONM1515 C ABSOLUTE CHANGE IN OBJECTIVE. CONM1575
CONM1516 OBJD=OBJ1-OBJ CONM1576
CONM1517 OBJB=ABS(OBJD) CONM1577
CONM1518 IF (OBJB.LT.1.0E-10) OBJB=0. CONM1578
CONM1519 IF (NAC.EQ.0.OR.OBJB.GT.0.) NCOBJ=0 CONM1579
CONM1520 IF (NCOBJ.GT.1) NCOBJ=0 CONM1580
C ----- CONM1581
C PRINT CONM1582
C ----- CONM1583
C PRINT MOVE PARAMETER, NEW X-VECTOR AND CONSTRAINTS. CONM1584
CONM1521 IF (IPRINT.LT.3) GO TO 730 CONM1585
CONM1522 WRITE (6,1390) ALP CONM1586
CONM1523 730 IF (IPRINT.LT.2) GO TO 800 CONM1587
CONM1524 IF (OBJB.GT.0.) GO TO 740 CONM1588
CONM1525 IF (IPRINT.EQ.2) WRITE (6,1400) ITER,OBJ CONM1589
CONM1526 IF (IPRINT.GT.2) WRITE (6,1410) OBJ CONM1590
CONM1527 GO TO 760 CONM1591
CONM1528 740 IF (IPRINT.EQ.2) GO TO 750 CONM1592
CONM1529 WRITE (6,1420) OBJ CONM1593
CONM1530 GO TO 760 CONM1594
CONM1531 750 WRITE (6,1430) ITER,OBJ CONM1595
CONM1532 760 WRITE (6,1450) CONM1596
CONM1533 DO 770 I=1,NDV CONM1597
CONM1534 FF1=1. CONM1598
CONM1535 IF (NSCAL.NE.0) FF1=SCAL(I) CONM1599
CONM1536 G1(I)=FF1*X(I) CONM1600
CONM1537 770 DO 780 I=1,NDV,6 CONM1601

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780	M1=MIN0(NDV,I*5) WRITE (6,1010) I,(G(J),J=I,M1) IF (NCON.EQ.0) GO TO 800 WRITE (6,1470) DO 790 I=1,NCON,6 M1=MIN0(NCON,I*5)	CONMI602 CONMI603 CONMI604 CONMI605 CONMI606 CONMI607	C	UN-SCALE THE DESIGN VARIABLES. DO 820 I=1,NDV XI=SCAL(I) IF (INSIDE.EQ.0) GO TO 820 VLB(I)=XI*VLB(I) VUB(I)=XI*VUB(I) X(I)=XI*X(I)	CONMI662 CONMI663 CONMI664 CONMI665 CONMI666 CONMI667 CONMI668
790	WRITE (6,1010) I,(G(J),J=I,M1)	CONMI608	820		CONMI669
800	CONTINUE	CONMI609	C	----- PRINT FINAL RESULTS -----	CONMI670
C	----- CHECK FEASABILITY -----	CONMI610 CONMI611	C		CONMI671
C	IF(NCON.LE.0) GO TO 808 DO 804 I=1,NCON C1=CTAM IF(ISC(I).GT.0) C1=CTBM IF(G(I).LE.C1) GO TO 804 NFEAS=NFEAS+1 GO TO 806	CONMI612 CONMI613 CONMI614 CONMI615 CONMI616 CONMI617 CONMI618	830	IF (IPRINT.EQ.0.OR.NAC.GE.N3) GO TO 940 WRITE (6,1500) WRITE (6,1420) OBJ WRITE (6,1450) DO 840 I=1,NDV,6 M1=MIN0(NDV,I*5)	CONMI672 CONMI673 CONMI674 CONMI675 CONMI676 CONMI677
804	CONTINUE IF(NFEAS.GT.0) ABOBJ1=.05 NFEAS=0 PHI=5.	CONMI619 CONMI620 CONMI621 CONMI622	840	WRITE (6,1010) I,(X(J),J=I,M1) IF (NCON.EQ.0) GO TO 900 WRITE (6,1470) DO 850 I=1,NCON,6 M1=MIN0(NCON,I*5)	CONMI678 CONMI679 CONMI680 CONMI681 CONMI682
806	IF(NFEAS.GE.10) GO TO 810	CONMI623	850	WRITE (6,1010) I,(G(J),J=I,M1)	CONMI683
808	CONTINUE	CONMI624	C	DETERMINE WHICH CONSTRAINTS ARE ACTIVE AND PRINT. NAC=0 NVC=0 DO 870 I=1,NCON CTA=CTAM IF (ISC(I).GT.0) CTA=CTBM GI=G(I) IF (GI.GT.CTA) GO TO 860 IF (GI.LT.CT.AND.ISC(I).EQ.0) GO TO 870 IF (GI.LT.CTL.AND.ISC(I).GT.0) GO TO 870 NAC=NAC+1 IC(NAC)=I GO TO 870	CONMI684 CONMI685 CONMI686 CONMI687 CONMI688 CONMI689 CONMI690 CONMI691 CONMI692 CONMI693 CONMI694 CONMI695 CONMI696
C	----- CHECK CONVERGENCE -----	CONMI625 CONMI626 CONMI627		NVC=NVC+1 MS1(NVC)=I CONTINUE WRITE (6,1060) NAC IF (NAC.EQ.0) GO TO 880 WRITE (6,1070) WRITE (6,1480) (IC(J),J=1,NAC)	CONMI697 CONMI698 CONMI699 CONMI700 CONMI701 CONMI702 CONMI703
C	STOP IF ITER EQUALS ITHAX. IF (ITER.GE.ITHAX) GO TO 810	CONMI628 CONMI629 CONMI630	860	WRITE (6,1080) NVC IF (NVC.EQ.0) GO TO 890 WRITE (6,1070) WRITE (6,1480) (MS1(J),J=1,NVC)	CONMI704 CONMI705 CONMI706 CONMI707
C	----- ABSOLUTE CHANGE IN OBJECTIVE -----	CONMI631 CONMI632 CONMI633	870	CONTINUE WRITE (6,1060) NAC IF (NAC.EQ.0) GO TO 880 WRITE (6,1070) WRITE (6,1480) (IC(J),J=1,NAC)	CONMI708 CONMI709 CONMI710 CONMI711
C	OBJB=ABS(OBJD) KOBJ=KOBJ+1 IF (OBJB.GE.DABFUN.OR.NFEAS.GT.0) KOBJ=0	CONMI634 CONMI635 CONMI636		IF (NSIDE.EQ.0) GO TO 930 DETERMINE WHICH SIDE CONSTRAINTS ARE ACTIVE AND PRINT. NAC=0 DO 920 I=1,NDV XI=X(I) XID=VLB(I) X12=ABS(XID) IF (X12.LT.1.) X12=1. GI=(XID-XI)/X12 IF (GI.LT.-1.0E-6) GO TO 910 NAC=NAC+1 MS1(NAC)=-I	CONMI712 CONMI713 CONMI714 CONMI715 CONMI716 CONMI717 CONMI718 CONMI719 CONMI720 CONMI721
C	----- RELATIVE CHANGE IN OBJECTIVE -----	CONMI637 CONMI638 CONMI639	890		
C	IF (ABS(OBJ1).GT.1.0E-10) OBJD=OBJD/ABS(OBJ1) ABOJB1=.5*(ABS(ABOJB)+ABS(OBJD)) ABOJB=ABS(OBJD) IOBJ=IOBJ+1 IF(NFEAS.GT.0.OR.OBJD.GE.DELFUN) IOBJ=0 IF (IOBJ.GE.ITRM.OR.KOBJ.GE.ITRM) GO TO 810 OBJ1=OBJ	CONMI640 CONMI641 CONMI642 CONMI643 CONMI644 CONMI645 CONMI646	900		
C	----- REDUCE CT IF OBJECTIVE FUNCTION IS CHANGING SLOWLY -----	CONMI647 CONMI648 CONMI649			
C	IF (IOBJ.LT.1.OR.NAC.EQ.0) GO TO 280 CT=DCT*CT CTL=CTL*DCTL IF (ABS(CT).LT.CTMIN) CT=-CTMIN IF (ABS(CTL).LT.CTLMIN) CTL=-CTLMIN GO TO 280 CONTINUE	CONMI650 CONMI651 CONMI652 CONMI653 CONMI654 CONMI655 CONMI656			
810	IF (NAC.GE.N3) WRITE (6,1490)	CONMI657			
C	----- ***** FINAL FUNCTION INFORMATION ***** -----	CONMI658 CONMI659			
C	IF (NSCAL.EQ.0) GO TO 830	CONMI660 CONMI661			

910	XID=VUB(I) X12=ABS(XID) IF (X12.LT.1.) X12=1. GI=(X1-XID)/X12 IF (GI.LT.-1.0E-6) GO TO 920 NAC=NAC+1 MS1(NAC)=I CONTINUE	CONMI722 CONMI723 CONMI724 CONMI725 CONMI726 CONMI727 CONMI728 CONMI729 CONMI730 CONMI731 CONMI732 CONMI733 CONMI734 CONMI735 CONMI736 CONMI737 CONMI738 CONMI739 CONMI740 CONMI741 CONMI742 CONMI743 CONMI744	990	FORMAT (5X,17HCONSTRAINT NUMBER,15) 1000 FORMAT (5X,27HSIDE CONSTRAINT ON VARIABLE,15) 1010 FORMAT (3X,15,1H),2X,6E13.5) 1020 FORMAT (/5X,35HLINEAR CONSTPAINT IDENTIFIERS (ISC)/5X,36HNON-ZERO INDICATES LINEAR CONSTRAINT) 1030 FORMAT (3X,15,1H),2X,1515) 1040 FORMAT (/5X,26HALL CONSTRAINTS ARE LINEAR) 1050 FORMAT (/5X,30HALL CONSTRAINTS ARE NON-LINEAR) 1060 FORMAT (/5X,9HTHERE ARE,15,19H ACTIVE CONSTRAINTS) 1070 FORMAT (5X,22HCONSTRAINT NUMBERS ARE) 1080 FORMAT (/5X,9HTHERE ARE,15,21H VIOLATED CONSTRAINTS) 1090 FORMAT (/5X,9HTHERE ARE,15,24H ACTIVE SIDE CONSTRAINTS) 1100 FORMAT (5X,43HDECISION VARIABLES AT LOHER OR UPPER BOUNDS,30H (MIH IUS INDICATES LOWER BOUND)) 1110 FORMAT (/5X,22HONE-DIMENSIONAL SEARCH/5X,15HINITIAL SLOPE =,E12.4,COMMI796 12X,16HPPPOSED ALPHA =,E12.4) 1120 FORMAT (///5X,35H* * CONMIN DETECTS VLB(I).GT.VUB(I)/5X,57HFIX IS 1SET X(I)=VLB(I)=VUB(I) = .5*(VLB(I)+VUB(I) FOR I =,15) 1130 FORMAT (///5X,41H* * CONMIN DETECTS INITIAL X(I).LT.VLB(I)/5X,6HX(COMMI800 I) =,E12.4,2X,8HVUB(I) =,E12.4/5X,35HX(I) IS SET EQUAL TO VLB(I) FCOMMI801 2OR I =,15) 1140 FORMAT (///5X,41H* * CONMIN DETECTS INITIAL X(I).GT.VUB(I)/5X,6HX(COMMI803 I) =,E12.4,2X,8HVUB(I) =,E12.4/5X,35HX(I) IS SET EQUAL TO VUB(I) FCOMMI804 2OR I =,15) 1150 FORMAT (/5X,21HTERMINATION CRITERION) 1160 FORMAT (10X,17HITER EQUALS ITMAX) 1170 FORMAT (10X,62HTEN CONSECUTIVE ITERATIONS FAILED TO PRODUCE A FEASCOMMI808 IBLE DESIGN) 1180 FORMAT (10X,43HABS(1-OBJ(I-1)/OBJ(I)) LESS THAN DELFUN FOR,I3,11H COMMI810 1ITERATIONS) 1190 FORMAT (10X,43HABS(OBJ(I)-OBJ(I-1)) LESS THAN DABFUN FOR,I3,11H COMMI812 1ITERATIONS) 1200 FORMAT (/5X,22HNUMBER OF ITERATIONS =,15) 1210 FORMAT (/5X,28HCONSTRAINT PARAMETER, BETA =,E14.5) 1220 FORMAT (1H1,///12X,27(2H*)/12X,1H*,51X,1H*/12X,1H*,20X,11HC O N COMMI816 1H I N,20X,1H*/12X,1H*,51X,1H*/12X,1H*,15X,21H FORTRAN PROGRAM FOR COMMI817 2,15X,1H*/12X,1H*,51X,1H*/12X,1H*,9X,33HCONSTRAINED FUCTION MINIMICOMMI818 3ZATION,9X,1H*/12X,1H*,51X,1H*/12X,27(2H*) COMMI819 1230 FORMAT (///5X,33HCONSTRAINED FUNCTION MINIMIZATION//5X,18HCONTROLCOMMI820 1 PARAMETERS) 1240 FORMAT (/5X,60HPRINT HDV ITMAX NSIDE ICNDIR NSCCOMMI822 1AL NFDG/818//5X,12HLINEOBJ ITRM,5X,2HH1,6X,2HH2,6X,2HH3,6X,2HH4,COMMI823 26X,2HNS/818) 1250 FORMAT (/9X,4HFDCH,12X,5HFDCHM,11X,6HALPHAX,10X,6HABOBJ1/1X,4(2X,ECOMMI825 114.5)) 1260 FORMAT (/9X,2HCT,14X,5HCTHIN,11X,3HCTL,13X,6HCTLMIN/1X,4(2X,E14.5)COMMI827 1//9X,5HTHETA,11X,3HPHI,13X,6HDELFUN,10X,6HDABFUN/1X,4(2X,E14.5)) COMMI828 1270 FOPMAT (/5X,40HLOWER BOUNDS ON DECISION VARIABLES (VLB)) COMMI829 1280 FOPMAT (/5X,40HUPPER BOUNDS ON DECISION VAPIABLES (VUB)) COMMI830 1290 FOPMAT (///5X,35HUNCONSTRAINED FUCTION MINIMIZATION//5X,18HCONTRCOMMI831 1OL PARAMETERS) 1300 FORMAT (/5X,21HSCALING VECTOR (SCAL)) COMMI832 1310 FORMAT (///5X,22HBEGIN ITERATION NUMBER,15) 1320 FORMAT (/5X,4HCT =,E14.5,5X,5HCTL =,E14.5,5X,5HPHI =,E14.5) 1330 FORMAT (/5X,25HNEW SCALING VECTOR (SCAL)) COMMI836 1340 FOPMAT (/5X,15HGRADIENT OF OBJ) 1350 FOPMAT (/5X,44HGRADIENTS OF ACTIVE AND VIOLATED CONSTRAINTS) 1360 FOPMAT (1H) 1370 FOPMAT (/5X,37HPUSH-OFF FACTORS, (THETA(I), I=1,NAC)) 1380 FOPMAT (/5X,27HSEARCH DIRECTION (S-VECTOR))	CONMI722 CONMI723 CONMI724 CONMI725 CONMI726 CONMI727 CONMI728 CONMI729 CONMI730 CONMI731 CONMI732 CONMI733 CONMI734 CONMI735 CONMI736 CONMI737 CONMI738 CONMI739 CONMI740 CONMI741 CONMI742 CONMI743 CONMI744 CONMI745 CONMI746 CONMI747 CONMI748 CONMI749 CONMI750 CONMI751 CONMI752 CONMI753 CONMI754 CONMI755 CONMI756 CONMI757 CONMI758 CONMI759 CONMI760 CONMI761 CONMI762 CONMI763 CONMI764 CONMI765 CONMI766 CONMI767 CONMI768 CONMI769 CONMI770 CONMI771 CONMI772 CONMI773 CONMI774 CONMI775 CONMI776 CONMI777 CONMI778 CONMI779 CONMI780 CONMI781	CONMI782 CONMI783 CONMI784 CONMI785 CONMI786 CONMI787 CONMI788 CONMI789 CONMI790 CONMI791 CONMI792 CONMI793 CONMI794 CONMI795 CONMI796 CONMI797 CONMI798 CONMI799 COMMI800 COMMI801 COMMI802 COMMI803 COMMI804 COMMI805 COMMI806 COMMI807 COMMI808 COMMI810 COMMI811 COMMI812 COMMI813 COMMI814 COMMI815 COMMI816 COMMI817 COMMI818 COMMI819 COMMI820 COMMI821 COMMI822 COMMI823 COMMI824 COMMI825 COMMI826 COMMI827 COMMI828 COMMI829 COMMI830 COMMI831 COMMI832 COMMI833 COMMI834 COMMI835 COMMI836 COMMI837 COMMI838 COMMI839 COMMI840 COMMI841
C	-----	CONMI745				
C	RE-SET BASIC PARAMETERS TO INPUT VALUES	CONMI746				
C	-----	CONMI747				
C	-----	CONMI748				
940	ITRM=IDM1 ITMAX=IDM2 ICNDIR=IDM3 DELFUN=DM1 DABFUN=DM2 CT=DM3 CTHIN=DM4 CTL=DM5 CTLMIN=DM6 THETA=DM7 PHI=DM8 FDCH=DM9 FDCHM=DM10 ABOBJ1=DM11 ALPHAX=DM12 IGOTO=0 CONTINUE	CONMI748 CONMI749 CONMI750 CONMI751 CONMI752 CONMI753 CONMI754 CONMI755 CONMI756 CONMI757 CONMI758 CONMI759 CONMI760 CONMI761 CONMI762 CONMI763 CONMI764				
C	-----	CONMI765				
950	IF (NSCAL.EQ.0.OR.IGOTO.EQ.0) RETURN UN-SCALE VARIABLES. DO 960 I=1,NDV C(I)=X(I)	CONMI765 CONMI766 CONMI767 CONMI768 CONMI769				
C	-----	CONMI771				
C	FORMATS	CONMI772				
C	-----	CONMI773				
C	-----	CONMI774				
C	-----	CONMI775				
970	FORMAT (///5X,72HA COMPLETELY UNCONSTRAINED FUCTION WITH A LINEARCOMMI776 1 OBJECTIVE IS SPECIFIED//10X,8HLINEOBJ =,15/10X,8HNSCON =,15/10X,8COMMI777 2HNSIDE =,15//5X,35HCONTROL RETURNED TO CALLING PROGRAM) 980	CONMI776 CONMI777 CONMI778 CONMI779 CONMI780 CONMI781				
C	-----	CONMI781				

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1390 FORMAT (/5X,18HCALCULATED ALPHA =,E14.5)          CONMI842  C
1400 FORMAT (////5X,6HITER =,I5,5X,5HOBJ =,E14.5,5X,16HNO CHANGE IN OBJ CONMI843  C
1)                                                    CONMI844  C
1410 FORMAT (/5X,5HOBJ =,E15.6,5X,16HNO CHANGE ON OBJ) CONMI845  30
1420 FORMAT (/5X,5HOBJ =,E15.6)                      CONMI846  40
1430 FORMAT (////5X,6HITER =,I5,5X,5HOBJ =,E14.5)    CONMI847
1440 FORMAT (/5X,28HINITIAL FUNCTION INFORMATION//5X,5HOBJ =,E15.6) CONMI848
1450 FORMAT (/5X,29HDECISION VARIABLES (X-VECTOR))    CONMI849  C
1460 FORMAT (3X,7E13.4)                               CONMI850  C
1470 FORMAT (/5X,28HCONSTRAINT VALUES (G-VECTOR))   CONMI851  C
1480 FORMAT (5X,15I5)                                 CONMI852
1490 FORMAT (/5X,59HTHE NUMBER OF ACTIVE AND VIOLATED CONSTRAINTS EXCEE CONMI853
105 N3-1./5X,66HDIMENSIONED SIZE OF MATRICES A AND B AND VECTOR IC CONMI854
2IS INSUFFICIENT/5X,6HOPTIMIZATION TERMINATED AND CONTROL RETURNED CONMI855
3 TO MAIN PROGRAM.) CONMI856  50
1500 FORMAT (1H1,////4X,30HFINAL OPTIMIZATION INFORMATION) CONMI857
1510 FORMAT (/5X,32HOBJECTIVE FUNCTION WAS EVALUATED,8X,I5,2X,5HTIMES) CONMI858
1520 FORMAT (/5X,35HCONSTRAINT FUNCTIONS WERE EVALUATED,I10,2X,5HTIMES) CONMI859
1530 FORMAT (/5X,36HGRADIENT OF OBJECTIVE WAS CALCULATED,I9,2X,5HTIMES) CONMI860
1540 FORMAT (/5X,40HGRADIENTS OF CONSTRAINTS WERE CALCULATED,I5,2X,5HTI CONMI861
1MES) CONMI862
END CONMI863
SUBROUTINE CNMM01 (JGOTO,X,DF,G,ISC,IC,A,G1,VLB,VUB,SCAL,C,NCAL,DX CONMI864
1,DX1,FI,XI,III,N1,N2,N3,N4) CONMI865
COMMON /CNM01/ DELFUN,DABFUN,FDCH,FDCHM,CT,CTMIN,CTL,CTLMIN,ALPHAX CONMI866
1,ABOBJ1,THETA,OBJ,NDV,NCON,NSIDE,IPRINT,NFDG,NSCAL,LINOBJ,ITMAX,IT CONMI867
2RM,ICHDIR,IGOTO,NAC,INFO,INFOG,ITER CONMI868
DIMENSION X(N1), DF(N1), G(N2), ISC(N2), IC(N3), A(N1,N3), G1(N2) CONMI869
1 VLB(N1), VUB(N1), SCAL(N1), NCAL(2), C(N4) CONMI870
C ROUTINE TO CALCULATE GRADIENT INFORMATION BY FINITE DIFFERENCE. CONMI871
C BY G. N. VANDERPLAATS JUNE, 1972. CONMI872
C NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. CONMI873
C IF (JGOTO.EQ.1) GO TO 10 CONMI874
C IF (JGOTO.EQ.2) GO TO 70 CONMI875
INFOG=0 CONMI876
INF=INFO CONMI877
NAC=0 CONMI878
IF (LINOBJ.NE.0.AND.ITER.GT.1) GO TO 10 CONMI879
C ----- CONMI880
C GRADIENT OF LINEAR OBJECTIVE CONMI881
C ----- CONMI882
IF (NFDG.EQ.2) JGOTO=1 CONMI883
IF (NFDG.EQ.2) RETURN CONMI884
CONTINUE CONMI885
JGOTO=0 CONMI886
IF (NFDG.EQ.2.AND.NCON.EQ.0) RETURN CONMI887
IF (NCON.EQ.0) GO TO 40 CONMI888
C ----- CONMI889
C * * * DETERMINE WHICH CONSTRAINTS ARE ACTIVE OR VIOLATED * * * CONMI890
C ----- CONMI891
DO 20 I=1,NCON CONMI892
IF (G(I).LT.CT) GO TO 20 CONMI893
IF (ISC(I).GT.0.AND.G(I).LT.CT) GO TO 20 CONMI894
NAC=NAC+1 CONMI895
IF (NAC.GE.N3) RETURN CONMI896
IC(NAC)=I CONMI897
CONTINUE CONMI898
IF (NFDG.EQ.2.AND.NAC.EQ.0) RETURN CONMI899
IF ((LINOBJ.GT.0.AND.ITER.GT.1).AND.NAC.EQ.0) RETURN CONMI900
C ----- CONMI901
-----
STOPE VALUES OF CONSTRAINTS IN G1 CONMI902
-----
DO 30 I=1,NCON CONMI903
G1(I)=G(I) CONMI904
CONTINUE CONMI905
JGOTO=0 CONMI906
IF (NAC.EQ.0.AND.NFDG.EQ.2) RETURN CONMI907
C ----- CONMI908
C CALCULATE GRADIENTS CONMI909
C ----- CONMI910
INFOG=1 CONMI911
INFO=1 CONMI912
FI=OBJ CONMI913
III=0 CONMI914
III=III+1 CONMI915
XI=X(III) CONMI916
DX=FDCH*XI CONMI917
DX=ABS(DX) CONMI918
FDCH1=FDCHM CONMI919
IF (NSCAL.NE.0) FDCH1=FDCHM/SCAL(III) CONMI920
IF (DX.LT.FDCH1) DX=FDCH1 CONMI921
X1=XI+DX CONMI922
IF (NSIDE.EQ.0) GO TO 60 CONMI923
IF (X1.GT.VUB(III)) DX=-DX CONMI924
DX1=1./DX CONMI925
X(III)=X1+DX CONMI926
NCAL(1)=NCAL(1)+1 CONMI927
C ----- CONMI928
C FUNCTION EVALUATION CONMI929
C ----- CONMI930
JGOTO=2 CONMI931
RETURN CONMI932
CONTINUE CONMI933
X(III)=XI CONMI934
IF (NFDG.EQ.0) DF(III)=DX1*(OBJ-FI) CONMI935
IF (NAC.EQ.0) GO TO 90 CONMI936
C ----- CONMI937
C DETERMINE GRADIENT COMPONENTS OF ACTIVE CONSTRAINTS CONMI938
C ----- CONMI939
DO 80 J=1,NAC CONMI940
I1=IC(J) CONMI941
A(III,J)=DX1*(G(I1)-G1(I1)) CONMI942
CONTINUE CONMI943
IF (III.LT.NDV) GO TO 50 CONMI944
INFOG=0 CONMI945
INFO=INF CONMI946
JGOTO=0 CONMI947
OBJ=FI CONMI948
IF (NCON.EQ.0) RETURN CONMI949
C ----- CONMI950
C STORE CURRENT CONSTRAINT VALUES BACK IN G-VECTOR CONMI951
C ----- CONMI952
DO 100 I=1,NCON CONMI953
G1(I)=G(I) CONMI954
RETURN CONMI955
END CONMI956
SUBROUTINE CNMM02 (NCAL,SLOPE,DF,DF1,DF,S,N1) CONMI957
COMMON /CNM02/ DELFUN,DABFUN,FDCH,FDCHM,CT,CTMIN,CTL,CTLMIN,ALPHAX CONMI958
1,ABOBJ1,THETA,OBJ,NDV,NCON,NSIDE,IPRINT,NFDG,NSCAL,LINOBJ,ITMAX,IT CONMI959
2RM,ICHDIR,IGOTO,NAC,INFO,INFOG,ITER CONMI960
CONMI961

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DIMENSION DF(N1), S(N1)                                COH11962
ROUTINE TO DETERMINE CONJUGATE DIRECTION VECTOR OR DIPECTION COH11963
OF STEEPEST DESCENT FOR UNCONSTRAINED FUNCTION MINIMIZATION. COH11964
BY G. N. VANDERPLAATS                                APRIL, 1972. COH11965
NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COH11966
N1CALC = CALCULATION CONTROL. COH11967
N1CALC = 0, S = STEEPEST DESCENT. COH11968
N1CALC = 1, S = CONJUGATE DIRECTION. COH11969
CONJUGATE DIRECTION IS FOUND BY FLETCHER-REEVES ALGORITHM. COH11970
-----COH11971
CALCULATE NORM OF GRADIENT VECTOR COH11972
-----COH11973
DFTDF=0. COH11974
DO 10 I=1,NDV COH11975
DFI=DF(I) COH11976
DFTDF=DFTDF+DFI*DFI COH11977
-----COH11978
***** FIND DIRECTION S *****COH11979
-----COH11980
IF (N1CALC.NE.1) GO TO 30 COH11981
IF (DFTDF1.LT.1.0E-20) GO TO 30 COH11982
-----COH11983
FIND FLETCHER-REEVES CONJUGATE DIRECTION COH11984
-----COH11985
BETA=DFTDF/DFTDF1 COH11986
SLOPE=0. COH11987
DO 20 I=1,NDV COH11988
DFI=DF(I) COH11989
SI=BETA*S(I)-DFI COH11990
SLOPE=SLOPE+SI*DFI COH11991
20 S(I)=SI COH11992
GO TO 50 COH11993
30 CONTINUE COH11994
N1CALC=0 COH11995
-----COH11996
CALCULATE DIRECTION OF STEEPEST DESCENT COH11997
-----COH11998
DO 40 I=1,NDV COH11999
S(I)=-DF(I) COH12000
SLOPE=-DFTDF COH12001
50 CONTINUE COH12002
-----COH12003
NORMALIZE S TO MAX ABS VALUE OF UNITY COH12004
-----COH12005
S1=0. COH12006
DO 60 I=1,NDV COH12007
S2=ABS(S(I)) COH12008
IF (S2.GT.S1) S1=S2 COH12009
60 CONTINUE COH12010
IF (S1.LT.1.0E-20) S1=1.0E-20 COH12011
S1=1./S1 COH12012
DFTDF1=DFTDF*S1 COH12013
DO 70 I=1,NDV COH12014
S(I)=S1*S(I) COH12015
SLOPE=S1*SLOPE COH12016
RETURN COH12017
END COH12018
SUBROUTINE CNM03 (X,S,SLOPE,ALP,FFF,A1,A2,A3,A4,F1,F2,F3,F4,APP,NCOH12019
11,N1CALC,KOUNT,JGOTO) COH12020
COMMON /CNM03/ DELFUN,DABFUN,FDCH,FDCHM,CT,CTHIN,CTL,CTLMIN,ALPHAXCOH12021
1,ABOBJ1,THETA,OBJ,NDV,NCON,NSIDE,IPPINT,NFDG,HSCAL,LINOBJ,ITMAX,ITCOH12022
2RH,ICNDIR,JGOTO,HAC,INFO,INFOG,ITER COH12023
DIMENSION X(N1), S(N1), N1CAL(2) COH12024
ROUTINE TO SOLVE ONE-DIMENSIONAL SEARCH IN UNCONSTRAINED COH12025
MINIMIZATION USING 2-POINT QUADRATIC INTERPOLATION, 3-POINT COH12026
CUBIC INTERPOLATION AND 4-POINT CUBIC INTERPOLATION. COH12027
BY G. N. VANDERPLAATS                                APRIL, 1972. COH12028
NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COH12029
ALP = PROPOSED MOVE PARAMETER. COH12030
SLOPE = INITIAL FUNCTION SLOPE = S-TRANPOSE TIMES DF. COH12031
SLOPE MUST BE NEGATIVE. COH12032
OBJ = INITIAL FUNCTION VALUE. COH12033
ZRO=0. COH12034
IF (JGOTO.EQ.0) GO TO 10 COH12035
GO TO (50,80,110,140,180,220,270),JGOTO COH12036
-----COH12037
INITIAL INFORMATION (ALPHA=0) COH12038
-----COH12039
IF (SLOPE.LT.0.) GO TO 20 COH12040
ALP=0. COH12041
RETURN COH12042
20 CONTINUE COH12043
IF (IPPINT.GT.4) WRITE (6,360) COH12044
FFF=OBJ COH12045
API=0. COH12046
A1=0. COH12047
F1=OBJ COH12048
A2=ALP COH12049
A3=0. COH12050
F3=0. COH12051
AP=A2 COH12052
KOUNT=0 COH12053
-----COH12054
MOVE A DISTANCE AP*S AND UPDATE FUNCTION VALUE COH12055
-----COH12056
CONTINUE COH12057
KOUNT=KOUNT+1 COH12058
DO 40 I=1,NDV COH12059
X(I)=X(I)+AP*S(I) COH12060
IF (IPPINT.GT.4) WRITE (6,370) AP COH12061
IF (IPPINT.GT.4) WRITE (6,380) (X(I),I=1,NDV) COH12062
N1CAL(I)=N1CAL(I)+1 COH12063
JGOTO=1 COH12064
RETURN COH12065
50 CONTINUE COH12066
F2=OBJ COH12067
IF (IPPINT.GT.4) WRITE (6,390) F2 COH12068
IF (F2.LT.F1) GO TO 120 COH12069
-----COH12070
CHECK FOR ILL-CONDITIONING COH12071
-----COH12072
IF (KOUNT.GT.5) GO TO 60 COH12073
FF=2.*ABS(F1) COH12074
IF (F2.LT.FF) GO TO 90 COH12075
FF=5.*ABS(F1) COH12076
IF (F2.LT.FF) GO TO 60 COH12077
A2=5*A2 COH12078
AP=-A2 COH12079
ALP=A2 COH12080
GO TO 30 COH12081

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60	F3=F2	CONM1082	RETURN	CONM1142
	A3=A2	CONM1083	140 CONTINUE	CONM1143
	A2=.5*A2	CONM1084	F3=OBJ	CONM1144
C	-----	CONM1085	IF (IPRINT.GT.4) WRITE (6,390) F3	CONM1145
C	UPDATE DESIGN VECTOR AND FUNCTION VALUE	CONM1086	150 CONTINUE	CONM1146
C	-----	CONM1087	IF (F3.LT.F2) GO TO 190	CONM1147
	AP=A2-ALP	CONM1088	160 CONTINUE	CONM1148
	ALP=A2	CONM1089	C	CONM1149
	DO 70 I=1,NDV	CONM1090	C ***** 3-POINT CUBIC INTERPOLATION *****	CONM1150
70	X(I)=X(I)+AP*S(I)	CONM1091	-----	CONM1151
	IF (IPRINT.GT.4) WRITE (6,370) A2	CONM1092	II=3	CONM1152
	IF (IPRINT.GT.4) WRITE (6,380) (X(I),I=1,NDV)	CONM1093	CALL CNMN04 (II,APP,ZRO,A1,F1,SLOPE,A2,F2,A3,F3,ZRO,ZRO)	CONM1153
	NCAL(1)=NCAL(1)+1	CONM1094	IF (APP.LT.ZRO.OR.APP.GT.A3) GO TO 190	CONM1154
	JGOTO=2	CONM1095	C	CONM1155
	RETURN	CONM1096	C UPDATE DESIGN VECTOR AND FUNCTION VALUE.	CONM1156
80	CONTINUE	CONM1097	C	CONM1157
	F2=OBJ	CONM1098	API=APP	CONM1158
	IF (IPRINT.GT.4) WRITE (6,390) F2	CONM1099	AP=APP-ALP	CONM1159
C	PROCEED TO CUBIC INTERPOLATION.	CONM1100	ALP=APP	CONM1160
	GO TO 160	CONM1101	DO 170 I=1,NDV	CONM1161
90	CONTINUE	CONM1102	170 X(I)=X(I)+AP*S(I)	CONM1162
C	-----	CONM1103	IF (IPRINT.GT.4) WRITE (6,370) ALP	CONM1163
C	***** 2-POINT QUADRATIC INTERPOLATION *****	CONM1104	IF (IPRINT.GT.4) WRITE (6,380) (X(I),I=1,NDV)	CONM1164
C	-----	CONM1105	NCAL(1)=NCAL(1)+1	CONM1165
	JJ=1	CONM1106	JGOTO=5	CONM1166
	II=1	CONM1107	RETURN	CONM1167
	CALL CNMN04 (II,APP,ZRO,A1,F1,SLOPE,A2,F2,ZRO,ZRO,ZRO,ZRO)	CONM1108	180 CONTINUE	CONM1168
	IF (APP.LT.ZRO.OR.APP.GT.A2) GO TO 120	CONM1109	IF (IPRINT.GT.4) WRITE (6,390) OBJ	CONM1169
	F3=F2	CONM1110	C	CONM1170
	A3=A2	CONM1111	C	CONM1171
	A2=APP	CONM1112	C	CONM1172
	JJ=0	CONM1113	AA=1.-APP/A2	CONM1173
C	-----	CONM1114	AB2=ABS(F2)	CONM1174
C	UPDATE DESIGN VECTOR AND FUNCTION VALUE	CONM1115	AB3=ABS(OBJ)	CONM1175
C	-----	CONM1116	AB=AB2	CONM1176
	AP=A2-ALP	CONM1117	IF (AB3.GT.AB) AB=AB3	CONM1177
	ALP=A2	CONM1118	IF (AB.LT.1.0E-15) AB=1.0E-15	CONM1178
	DO 100 I=1,NDV	CONM1119	AB=(AB2-AB3)/AB	CONM1179
100	X(I)=X(I)+AP*S(I)	CONM1120	IF (ABS(AB).LT.1.0E-15.AND.ABS(AA).LT..001) GO TO 330	CONM1180
	IF (IPRINT.GT.4) WRITE (6,370) A2	CONM1121	A4=A3	CONM1181
	IF (IPRINT.GT.4) WRITE (6,380) (X(I),I=1,NDV)	CONM1122	F4=F3	CONM1182
	NCAL(1)=NCAL(1)+1	CONM1123	A3=APP	CONM1183
	JGOTO=3	CONM1124	F3=OBJ	CONM1184
	RETURN	CONM1125	IF (A3.GT.A2) GO TO 230	CONM1185
110	CONTINUE	CONM1126	A3=A2	CONM1186
	F2=OBJ	CONM1127	F3=F2	CONM1187
	IF (IPRINT.GT.4) WRITE (6,390) F2	CONM1128	A2=APP	CONM1188
	GO TO 150	CONM1129	F2=OBJ	CONM1189
120	A3=2.*A2	CONM1130	GO TO 230	CONM1190
C	-----	CONM1131	190 CONTINUE	CONM1191
C	UPDATE DESIGN VECTOR AND FUNCTION VALUE	CONM1132	C	CONM1192
C	-----	CONM1133	C ***** 4-POINT CUBIC INTERPOLATION *****	CONM1193
	AP=A3-ALP	CONM1134	-----	CONM1194
	ALP=A3	CONM1135	200 CONTINUE	CONM1195
	DO 130 I=1,NDV	CONM1136	A4=2.*A3	CONM1196
130	X(I)=X(I)+AP*S(I)	CONM1137	C UPDATE DESIGN VECTOR AND FUNCTION VALUE.	CONM1197
	IF (IPRINT.GT.4) WRITE (6,370) A3	CONM1138	AP=A4-ALP	CONM1198
	IF (IPRINT.GT.4) WRITE (6,380) (X(I),I=1,NDV)	CONM1139	ALP=A4	CONM1199
	NCAL(1)=NCAL(1)+1	CONM1140	DO 210 I=1,NDV	CONM1200
	JGOTO=4	CONM1141	210 X(I)=X(I)+AP*S(I)	CONM1201

	IF (IPRINT.GT.4) WRITE (6,370) ALP	COMH1202	310	CONTINUE	COMH1262
	IF (IPRINT.GT.4) WRITE (6,380) (X(I),I=1,NDV)	COMH1203	C	-----	COMH1263
	NCAL(1)=NCAL(1)+1	COMH1204	C	UPDATE DESIGN VECTOR	COMH1264
	JGOTO=6	COMH1205	C	-----	COMH1265
220	RETURN	COMH1206		DO 320 I=1,NDV	COMH1266
	CONTINUE	COMH1207	320	X(I)=X(I)+AP*S(I)	COMH1267
	F4=OBJ	COMH1208	330	CONTINUE	COMH1268
	IF (IPRINT.GT.4) WRITE (6,390) F4	COMH1209	C	-----	COMH1269
	IF (F4.GT.F3) GO TO 230	COMH1210	C	CHECK FOR MULTIPLE MINIMA	COMH1270
	A1=A2	COMH1211	C	-----	COMH1271
	F1=F2	COMH1212		IF (OBJ.LE.FFF) GO TO 350	COMH1272
	A2=A3	COMH1213	C	INITIAL FUNCTION IS MINIMUM.	COMH1273
	F2=F3	COMH1214		DO 340 I=1,NDV	COMH1274
	A3=A4	COMH1215	340	X(I)=X(I)-ALP*S(I)	COMH1275
	F3=F4	COMH1216		ALP=0.	COMH1276
	GO TO 200	COMH1217		OBJ=FFF	COMH1277
230	CONTINUE	COMH1218	350	CONTINUE	COMH1278
	II=4	COMH1219		JGOTO=0	COMH1279
	CALL CMMN04 (II,APP,A1,A1,F1,SLOPE,A2,F2,A3,F3,A4,F4)	COMH1220		RETURN	COMH1280
	IF (APP.GT.A1) GO TO 250	COMH1221	C	-----	COMH1281
	AP=A1-ALP	COMH1222	C	FORMATS	COMH1282
	ALP=A1	COMH1223	C	-----	COMH1283
	OBJ=F1	COMH1224	C		COMH1284
	DO 240 I=1,NDV	COMH1225	C		COMH1285
240	X(I)=X(I)+AP*S(I)	COMH1226	360	FORMAT (/////5X,60H* * * UNCONSTRAINED ONE-DIMENSIONAL SEARCH INFO	COMH1286
	GO TO 280	COMH1227		IRMATION * * *)	COMH1287
250	CONTINUE	COMH1228	370	FORMAT (/5X,7HALPHA =,E14.5/5X,8HX-VECTOR)	COMH1288
C	-----	COMH1229	380	FORMAT (5X,6E13.5)	COMH1289
C	UPDATE DESIGN VECTOR AND FUNCTION VALUE	COMH1230	390	FORMAT (/5X,5HOBJ =,E14.5)	COMH1290
C	-----	COMH1231		END	COMH1291
	AP=APP-ALP	COMH1232		SUBROUTINE CMMN04 (II,XBAR,EPS,X1,Y1,SLOPE,X2,Y2,X3,Y3,X4,Y4)	COMH1292
	ALP=APP	COMH1233	C	ROUTINE TO FIND FIRST XBAR.GE.EPS CORRESPONDING TO A MINIMUM	COMH1293
	DO 260 I=1,NDV	COMH1234	C	OF A ONE-DIMENSIONAL REAL FUNCTION BY POLYNOMIAL INTERPOLATION.	COMH1294
260	X(I)=X(I)+AP*S(I)	COMH1235	C	BY G. H. VANDERPLAATS APRIL, 1972.	COMH1295
	IF (IPRINT.GT.4) WRITE (6,370) ALP	COMH1236	C	MASA-AMES RESEAPCH CENTER, HOFFETT FIELD, CALIF.	COMH1296
	IF (IPRINT.GT.4) WRITE (6,380) (X(I),I=1,NDV)	COMH1237	C		COMH1297
	NCAL(1)=NCAL(1)+1	COMH1238	C	II = CALCULATION CONTROL.	COMH1298
	JGOTO=7	COMH1239	C	1: 2-POINT QUADRATIC INTERPOLATION, GIVEN X1, Y1, SLOPE,	COMH1299
	RETURN	COMH1240	C	X2 AND Y2.	COMH1300
270	CONTINUE	COMH1241	C	2: 3-POINT QUADRATIC INTERPOLATION, GIVEN X1, Y1, X2, Y2,	COMH1301
	IF (IPRINT.GT.4) WRITE (6,390) OBJ	COMH1242	C	X3 AND Y3.	COMH1302
280	CONTINUE	COMH1243	C	3: 3-POINT CUBIC INTERPOLATION, GIVEN X1, Y1, SLOPE, X2, Y2,	COMH1303
C	-----	COMH1244	C	X3 AND Y3.	COMH1304
C	CHECK FOR ILL-CONDITIONING	COMH1245	C	4: 4-POINT CUBIC INTERPOLATION, GIVEN X1, Y1, X2, Y2, X3,	COMH1305
C	-----	COMH1246	C	Y3, X4 AND Y4.	COMH1306
	IF (OBJ.GT.F2.OR.OBJ.GT.F3) GO TO 290	COMH1247	C	EPS MAY BE NEGATIVE.	COMH1307
	IF (OBJ.LE.F1) GO TO 330	COMH1248	C	IF REQUIRED MINIMUM ON Y DOES NOT EXITS. OR THE FUNCTION IS	COMH1308
	AP=A1-ALP	COMH1249	C	ILL-CONDITIONED, XBAR = EPS-1.0 WILL BE RETURNED AS AN ERROR	COMH1309
	ALP=A1	COMH1250	C	INDICATOR.	COMH1310
	OBJ=F1	COMH1251	C	IF DESIRED INTERPOLATION IS ILL-CONDITIONED, A LOWER ORDER	COMH1311
	GO TO 310	COMH1252	C	INTERPOLATION, CONSISTANT WITH INPUT DATA, WILL BE ATTEMPTED,	COMH1312
290	CONTINUE	COMH1253	C	AND II WILL BE CHANGED ACCORDINGLY.	COMH1313
	IF (F2.LT.F3) GO TO 300	COMH1254		XBAR1=EPS-1.	COMH1314
	OBJ=F3	COMH1255		XBAR=XBAR1	COMH1315
	AP=A3-ALP	COMH1256		X21=X2-X1	COMH1316
	ALP=A3	COMH1257		IF (ABS(X21).LT.(.10E-20) RETURN	COMH1317
	GO TO 310	COMH1258		NSLOP=NO(II,2)	COMH1318
300	OBJ=F2	COMH1259		GO TO (10,20,40,50),II	COMH1319
	AP=A2-ALP	COMH1260	10	CONTINUE	COMH1320
	ALP=A2	COMH1261	C	-----	COMH1321

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C ----- II=1: 2-POINT QUADRATIC INTERPOLATION ----- COH11322
C II=1 COH11323
C DX=X1-X2 COH11324
C IF (ABS(DX).LT.1.0E-20) RETURN COH11325
C AA=(SLOPE*(Y2-Y1)/DX)/DX COH11326
C IF (AA.LT.1.0E-20) RETURN COH11327
C BB=SLOPE-2.*AA*X1 COH11328
C XBAR=-.5*BB/AA COH11329
C IF (XBAR.LT.EPS) XBAR=XBAR1 COH11330
C RETURN COH11331
C CONTINUE COH11332
C ----- II=2: 3-POINT QUADRATIC INTERPOLATION ----- COH11333
C II=2 COH11334
C X21=X2-X1 COH11335
C X31=X3-X1 COH11336
C X32=X3-X2 COH11337
C QQ=X21*X31*X32 COH11338
C IF (ABS(QQ).LT.1.0E-20) RETURN COH11339
C AA=(Y1*X32-Y2*X31+Y3*X21)/QQ COH11340
C IF (AA.LT.1.0E-20) GO TO 30 COH11341
C BB=(Y2-Y1)/X21-AA*(X1*X2) COH11342
C XBAR=-.5*BB/AA COH11343
C IF (XBAR.LT.EPS) XBAR=XBAR1 COH11344
C RETURN COH11345
C CONTINUE COH11346
C IF (NSLOP.EQ.0) RETURN COH11347
C GO TO 10 COH11348
C CONTINUE COH11349
C ----- II=3: 3-POINT CUBIC INTERPOLATION ----- COH11350
C II=3 COH11351
C X21=X2-X1 COH11352
C X31=X3-X1 COH11353
C X32=X3-X2 COH11354
C QQ=X21*X31*X32 COH11355
C IF (ABS(QQ).LT.1.0E-20) RETURN COH11356
C X11=X1*X1 COH11357
C DNOM=X2*X2*X31-X11*X32-X3*X3*X21 COH11358
C IF (ABS(DNOM).LT.1.0E-20) GO TO 20 COH11359
C AA=((X31*X31*(Y2-Y1)-X21*X21*(Y3-Y1))/(X31*X21)-SLOPE*X32)/DNOM COH11360
C IF (ABS(AA).LT.1.0E-20) GO TO 20 COH11361
C BB=((Y2-Y1)/X21-SLOPE-AA*(X2*X2+X1*X2-2.*X11))/X21 COH11362
C CC=SLOPE-3.*AA*X11-2.*BB*X1 COH11363
C BAC=BB*BB-3.*AA*CC COH11364
C IF (BAC.LT.0.) GO TO 20 COH11365
C BAC=SQRT(BAC) COH11366
C XBAR=(BAC-BB)/(3.*AA) COH11367
C IF (XBAR.LT.EPS) XBAR=EPS COH11368
C RETURN COH11369
C CONTINUE COH11370
C ----- II=4: 4-POINT CUBIC INTERPOLATION ----- COH11371
C X21=X2-X1 COH11372
C X31=X3-X1 COH11373
C X41=X4-X1 COH11374
C X32=X3-X2 COH11375
C X42=X4-X2 COH11376
C X11=X1*X1 COH11377
C X22=X2*X2 COH11378
C Q2=X31*X21*X32 COH11379
C IF (ABS(Q2).LT.1.0E-30) RETURN COH11380
C Q1=X111*X32-X222*X31+X3*X33*X21 COH11381
C Q4=X111*X42-X222*X41+X4*X44*X21 COH11382
C Q5=X41*X21*X42 COH11383
C DNOM=Q2*Q4-Q1*Q5 COH11384
C IF (ABS(DNOM).LT.1.0E-30) GO TO 60 COH11385
C Q3=Y3*X21-Y2*X31+Y1*X32 COH11386
C Q6=Y4*X21-Y2*X41+Y1*X42 COH11387
C AA=(Q2*Q6-Q3*Q5)/DNOM COH11388
C BB=(Q3-Q1*AA)/Q2 COH11389
C CC=(Y2-Y1-AA*(X22-X111))/X21-BB*(X1*X2) COH11390
C BAC=BB*BB-3.*AA*CC COH11391
C IF (ABS(AA).LT.1.0E-20.OR.BAC.LT.0.) GO TO 60 COH11392
C BAC=SQRT(BAC) COH11393
C XBAR=(BAC-BB)/(3.*AA) COH11394
C IF (XBAR.LT.EPS) XBAR=XBAR1 COH11395
C RETURN COH11396
C CONTINUE COH11397
C IF (NSLOP.EQ.1) GO TO 40 COH11398
C GO TO 20 COH11399
C END COH11400
C SUBROUTINE CNM05 (G,DF,A,S,B,C,SLOPE,PHI,ISC,IC,MS1,NVC,M1,N2,N3, COH11401
C IN4,N5) COH11402
C COMMON /CNM05/ DELFUN,DABFUN,FDCH,FDCHM,CT,CTMIN,CTL,CTLMIN,ALPHACOH11403
C 1,ABOBJ1,THETA,OBJ,NOV,HCON,NSIDE,IPRINT,NFDG,NSCAL,LINOBJ,ITHAX,ITCOH11404
C 2RM,ICNDIR,IGOTO,NAC,INFO,INFOG,ITER COH11405
C DIMENSION DF(N1), G(N2), ISC(N2), IC(N3), A(N1,N3), S(N1), C(N4), COH11406
C IMS1(N5), B(N3,N3) COH11407
C ROUTINE TO SOLVE DIRECTION FINDING PROBLEM IN MODIFIED METHOD OF COH11408
C FEASIBLE DIRECTIONS. COH11409
C BY G. N. VANDERPLAATS MAY, 1972. COH11410
C NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. COH11411
C NORM OF S VECTOR USED HERE IS S-TRANSPPOSE TIMES S.LE.1. COH11412
C IF HVC = 0 FIND DIRECTION BY ZOUTENDIJK'S METHOD. OTHERWISE COH11413
C FIND MODIFIED DIRECTION. COH11414
C ----- COH11415
C *** NORMALIZE GRADIENTS, CALCULATE THETA'S AND DETERMINE NVC *** COH11416
C NDV1=NDV+1 COH11417
C NDV2=NDV+2 COH11418
C HAC1=HAC+1 COH11419
C NVC=0 COH11420
C THMAX=0. COH11421
C CTA=ABS(CT) COH11422
C CT1=1./CTA COH11423
C CTAH=ABS(CTMIN) COH11424
C CTB=ABS(CTL) COH11425
C CT2=1./CTB COH11426
C CTDH=ABS(CTLMIN) COH11427
C A1=1. COH11428
C DO 40 I=1,HAC COH11429

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C	CALCULATE THETA	CONM1442	NDB=NAC	CONM1502
	NCI=IC(I)	CONM1443	A(NDV1,NAC1)=-PHI	CONM1503
	NCJ=1	CONM1444	-----	CONM1504
	IF (NCI.LE.NCON) NCJ=ISC(NCI)	CONM1445	SCALE THETA'S SO THAT MAXIMUM THETA IS UNITY	CONM1505
	C1=G(NCI)	CONM1446	-----	CONM1506
	CTD=CT1	CONM1447	IF (THMAX.GT.0.00001) THMAX=1./THMAX	CONM1507
	CTC=CTAM	CONM1448	DO 90 I=1,NDB	CONM1508
	IF (NCJ.LE.0) GO TO 10	CONM1449	A(NDV1,I)=A(NDV1,I)*THMAX	CONM1509
	CTC=CTBM	CONM1450	90 CONTINUE	CONM1510
	CTD=CT2	CONM1451	DO 100 I=1,NDB	CONM1511
10	IF (C1.GT.CTC) NVC=NVC+1	CONM1452	C(I)=0.	CONM1512
	THT=0.	CONM1453	DO 100 J=1,NDV1	CONM1513
	GG=1.*CTD*C1	CONM1454	C(I)=C(I)+A(J,I)*A(J,NAC1)	CONM1514
	IF (NCJ.EQ.0.OR.C1.GT.CTC) THT=THETA*GG*GG	CONM1455	110 CONTINUE	CONM1515
	IF (THT.GT.50.) THT=50.	CONM1456	-----	CONM1516
	IF (THT.GT.THMAX) THMAX=THT	CONM1457	BUILD B MATRIX	CONM1517
	A(NDV1,I)=THT	CONM1458	-----	CONM1518
C	-----	CONM1459	DO 120 I=1,NDB	CONM1519
C	NORMALIZE GRADIENTS OF CONSTRAINTS	CONM1460	DO 120 J=1,NDB	CONM1520
C	-----	CONM1461	B(I,J)=0.	CONM1521
	A(NDV2,I)=1.	CONM1462	DO 120 K=1,NDV1	CONM1522
	IF (NCI.GT.NCON) GO TO 40	CONM1463	B(I,J)=B(I,J)-A(K,I)*A(K,J)	CONM1523
	A1=0.	CONM1464	-----	CONM1524
	DO 20 J=1,NDV	CONM1465	SOLVE SPECIAL L. P. PROBLEM	CONM1525
	A1=A1+A(J,I)**2	CONM1466	-----	CONM1526
20	CONTINUE	CONM1467	CALL CHRIN08 (NDB,HER.C,MS1,B,N3,N4,N5)	CONM1527
	IF (A1.LT.1.0E-20) A1=1.0E-20	CONM1468	IF (IFRINT.GT.1.AND.HER.GT.0) WRITE (6,180)	CONM1528
	A1=SQRT(A1)	CONM1469	CALCULATE RESULTING DIRECTION VECTOR, S.	CONM1529
	A(NDV2,I)=A1	CONM1470	SLOPE=0.	CONM1530
	A1=1./A1	CONM1471	-----	CONM1531
	DO 30 J=1,NDV	CONM1472	USABLE-FEASIBLE DIRECTION	CONM1532
30	A(J,I)=A1*A(J,I)	CONM1473	-----	CONM1533
40	CONTINUE	CONM1474	DO 140 I=1,NDV	CONM1534
C	-----	CONM1475	S1=0.	CONM1535
C	NORMALIZE GRADIENT OF OBJECTIVE FUNCTION AND STORE IN NAC+1	CONM1476	IF (NVC.GT.0) S1=-A(I,NAC1)	CONM1536
C	COLUMN OF A	CONM1477	DO 130 J=1,NDB	CONM1537
C	-----	CONM1478	S1=S1-A(I,J)*C(J)	CONM1538
	A1=0.	CONM1479	SLOPE=SLOPE+S1*DF(I)	CONM1539
	DO 50 I=1,NDV	CONM1480	S(I)=S1	CONM1540
	A1=A1+DF(I)**2	CONM1481	S(NDV1)=1.	CONM1541
50	CONTINUE	CONM1482	IF (NVC.GT.0) S(NDV1)=-A(NDV1,NAC1)	CONM1542
	IF (A1.LT.1.0E-20) A1=1.0E-20	CONM1483	DO 150 J=1,NDB	CONM1543
	A1=SQRT(A1)	CONM1484	S(NDV1)=S(NDV1)-A(NDV1,J)*C(J)	CONM1544
	A1=1./A1	CONM1485	-----	CONM1545
	DO 60 I=1,NDV	CONM1486	NORMALIZE S TO MAX ABS OF UNITY	CONM1546
60	A(I,NAC1)=A1*DF(I)	CONM1487	-----	CONM1547
C	BUILD C VECTOR.	CONM1488	S1=0.	CONM1548
C	IF (NVC.GT.0) GO TO 80	CONM1489	DO 160 I=1,NDV	CONM1549
C	-----	CONM1490	A1=ABS(S1)	CONM1550
C	BUILD C FOR CLASSICAL METHOD	CONM1491	IF (A1.GT.S1) S1=A1	CONM1551
C	-----	CONM1492	CONTINUE	CONM1552
	NDB=NAC1	CONM1493	IF (S1.LT.1.0E-10) RETURN	CONM1553
	A(NDV1,NDB)=1.	CONM1494	S1=1./S1	CONM1554
	DO 70 I=1,NDB	CONM1495	DO 170 I=1,NDV	CONM1555
70	C(I)=-A(NDV1,I)	CONM1496	S(I)=S1*S(I)	CONM1556
	GO TO 110	CONM1497	SLOPE=S1*SLOPE	CONM1557
80	CONTINUE	CONM1498	S(NDV1)=S1*S(NDV1)	CONM1558
C	-----	CONM1499	RETURN	CONM1559
C	BUILD C FOR MODIFIED METHOD	CONM1500	-----	CONM1560
C	-----	CONM1501	FORNATS	CONM1561

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C -----CONM1562
C CONM1563
C CONM1564
180 FORMAT (//5X,46H* * DIRECTION FINDING PROCESS DID NOT CONVERGE/5X,CONM1565
129H* * S-VECTOR MAY NOT BE VALID) CONM1566
END CONM1567
SUBROUTINE CMMN06 (X,VLB,VUB,G,SCAL,DF,S,G1,G2,CTAM,CTBM,SLOPE,ALP,CONM1568
1,A2,A3,A4,F1,F2,F3,CV1,CV2,CV3,CV4,ALPCA,ALPFES,ALPLN,ALPHIN,ALPNCCONM1569
2,ALPSAV,ALPSID,ALPTOT,ISC,N1,N2,NCAL,NVC,ICOUNT,IGOOD1,IGOOD2,IGOODCONM1570
3D3,IGOOD4,IBEST,III,MLNC,JGOTO) CONM1571
COMMON /CMMN1/ DELFUN,DABFUN,FDCH,FDCHM,CT,CTHIN,CTL,CTLMIN,ALPHAXCONM1572
1,ABOBJ1,THETA,OBJ,NDV,NCON,NSIDE,IPRINT,NFDG,NSCAL,LINOBJ,ITHAX,ITCONM1573
2RM,ICNDIR,IGOTO,NAC,INFO,INFOG,ITER CONM1574
DIMENSION X(N1), VLB(N1), VUB(N1), G(N2), SCAL(N1), DF(N1), S(N1),CONM1575
1 G1(N2), G2(N2), ISC(N2), NCAL(2) CONM1576
ROUTINE TO SOLVE ONE-DIMENSIONAL SEARCH PROBLEM FOR CONSTRAINED CONM1577
FUNCTION MINIMIZATION. CONM1578
BY G. N. VANDERPLAATS CONM1579
AUG., 1974. CONM1580
NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. CONM1581
OBJ = INITIAL AND FINAL FUNCTION VALUE. CONM1582
ALP = MOVE PARAMETER. CONM1583
SLOPE = INITIAL SLOPE. CONM1584
ALPSID = MOVE TO SIDE CONSTRAINT. CONM1585
ALPFES = MOVE TO FEASIBLE REGION. CONM1586
ALPNC = MOVE TO NEW NON-LINEAR CONSTRAINT. CONM1587
ALPLN = MOVE TO LINEAR CONSTRAINT. CONM1588
ALPCA = MOVE TO RE-ENCOUNTER CURRENTLY ACTIVE CONSTRAINT. CONM1589
ALPHIN = MOVE TO MINIMIZE FUNCTION. CONM1590
ALPTOT = TOTAL MOVE PARAMETER. CONM1591
ZRO=0. CONM1592
IF (JGOTO.EQ.0) GO TO 10 CONM1593
GO TO (140,310,520),JGOTO CONM1594
10 IF (IPRINT.GE.5) WRITE (6,730) CONM1595
ALPSAV=ALP CONM1596
ICOUNT=0 CONM1597
ALPTOT=0. CONM1598
C TOLERANCES. CONM1599
CTAM=ABS(CTHIN) CONM1600
CTBM=ABS(CTLMIN) CONM1601
C PROPOSED MOVE. CONM1602
20 CONTINUE CONM1603
C -----CONM1604
C ***** BEGIN SEARCH OR IMPOSE SIDE CONSTRAINT MODIFICATION ***** CONM1605
C -----CONM1606
A2=ALPSAV CONM1607
ICOUNT=ICOUNT+1 CONM1608
ALPSID=1.0E+20 CONM1609
C INITIAL ALPHA AND OBJ. CONM1610
ALP=0. CONM1611
F1=OBJ CONM1612
KSID=0 CONM1613
IF (NSIDE.EQ.0) GO TO 70 CONM1614
C -----CONM1615
C FIND MOVE TO SIDE CONSTRAINT AND INSURE AGAINST VIOLATION OF CONM1616
C SIDE CONSTRAINTS CONM1617
C -----CONM1618
DO 60 I=1,NDV CONM1619
SI=S(I) CONM1620
IF (ABS(SI).GT.1.0E-20) GO TO 30 CONM1621
C ITH COMPONENT OF S IS SMALL. SET TO ZERO. CONM1622
SI)=0. CONM1623
SLOPE=SLOPE-SI*DF(I) CONM1624
GO TO 60 CONM1625
CONTINUE CONM1626
XI=X(I) CONM1627
SI=1./SI CONM1628
IF (SI.GT.0.) GO TO 40 CONM1629
C LOWER BOUND. CONM1630
XI2=VLB(I) CONM1631
XI1=ABS(XI2) CONM1632
IF (XI1.LT.1.) XI1=1. CONM1633
C CONSTRAINT VALUE. CONM1634
GI=(XI2-XI)/XI1 CONM1635
IF (GI.GT.-1.0E-6) GO TO 50 CONM1636
C PROPOSED MOVE TO LOWER BOUND. CONM1637
ALPA=(XI2-XI)*SI CONM1638
IF (ALPA.LT.ALPSID) ALPSID=ALPA CONM1639
GO TO 60 CONM1640
40 CONTINUE CONM1641
C UPPER BOUND. CONM1642
XI2=VUB(I) CONM1643
XI1=ABS(XI2) CONM1644
IF (XI1.LT.1.) XI1=1. CONM1645
C CONSTRAINT VALUE. CONM1646
GI=(XI-XI2)/XI1 CONM1647
IF (GI.GT.-1.0E-6) GO TO 50 CONM1648
C PROPOSED MOVE TO UPPER BOUND. CONM1649
ALPA=(XI2-XI)*SI CONM1650
IF (ALPA.LT.ALPSID) ALPSID=ALPA CONM1651
GO TO 60 CONM1652
50 CONTINUE CONM1653
C MOVE WILL VIOLATE SIDE CONSTRAINT. SET S(I)=0. CONM1654
SLOPE=SLOPE-S(I)*DF(I) CONM1655
SI)=0. CONM1656
KSID=KSID+1 CONM1657
60 CONTINUE CONM1658
C ALPSID IS UPPER BOUND ON ALPHA. CONM1659
IF (A2.GT.ALPSID) A2=ALPSID CONM1660
70 CONTINUE CONM1661
C -----CONM1662
C CHECK ILL-CONDITIONING CONM1663
C -----CONM1664
IF (KSID.EQ.NDV.OR.ICOUNT.GT.10) GO TO 710 CONM1665
IF (NVC.EQ.0.AND.SLOPE.GT.0.) GO TO 710 CONM1666
ALPFES=-1. CONM1667
ALPHIN=-1. CONM1668
ALPLN=1.1*ALPSID CONM1669
ALPNC=ALPSID CONM1670
ALPCA=ALPSID CONM1671
IF (NCON.EQ.0) GO TO 90 CONM1672
C STORE CONSTRAINT VALUES IN G1. CONM1673
DO 80 I=1,NCON CONM1674
G1(I)=G(I) CONM1675
80 CONTINUE CONM1676
90 CONTINUE CONM1677
C -----CONM1678
C MOVE A DISTANCE A2*S CONM1679
ALPTOT=ALPTOT+A2 CONM1680
CONM1681

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	DO 100 I=1,NDV	COHM1682		IF (IGOOD1.EQ.0.AND.IGOOD2.EQ.0) GO TO 180	COHM1742
	X(I)=X(I)+A2*S(I)	COHM1683	C	VIOLATED CONSTRAINTS. PICK MINIMUM VIOLATION.	COHM1743
100	CONTINUE	COHM1684		IBEST=1	COHM1744
	IF (IPRINT.LT.5) GO TO 130	COHM1685		IF (CV1.GE.CV2) IBEST=2	COHM1745
	WRITE (6,740) A2	COHM1686		GO TO 190	COHM1746
	IF (NSCAL.EQ.0) GO TO 120	COHM1687	180	CONTINUE	COHM1747
	DO 110 I=1,NDV	COHM1688	C	NO CONSTRAINT VIOLATION. PICK MINIMUM F.	COHM1748
110	G(I)=SCAL(I)*X(I)	COHM1689		IBEST=1	COHM1749
	WRITE (6,750) (G(I),I=1,NDV)	COHM1690		IF (F2.LE.F1) IBEST=2	COHM1750
	GO TO 130	COHM1691	190	CONTINUE	COHM1751
120	WRITE (6,750) (X(I),I=1,NDV)	COHM1692		II=1	COHM1752
C	-----	COHM1693		IF (NCON.EQ.0) GO TO 230	COHM1753
C	UPDATE FUNCTION AND CONSTRAINT VALUES	COHM1694	C	-----	COHM1754
C	-----	COHM1695	C	***** 2 - POINT INTERPOLATION *****	COHM1755
130	NCAL(1)=NCAL(1)+1	COHM1696	C	-----	COHM1756
	JGOTO=1	COHM1697		III=0	COHM1757
	RETURN	COHM1698	200	III=III+1	COHM1758
140	CONTINUE	COHM1699		C1=G(III)	COHM1759
	F2=OBJ	COHM1700		C2=G(III)	COHM1760
	IF (IPRINT.GE.5) WRITE (6,760) F2	COHM1701		IF (ISC(III).EQ.0) GO TO 210	COHM1761
	IF (IPRINT.LT.5.OR.NCON.EQ.0) GO TO 150	COHM1702	C	-----	COHM1762
	WRITE (6,770)	COHM1703	C	LINEAR CONSTRAINT	COHM1763
	WRITE (6,750) (G(I),I=1,NCON)	COHM1704	C	-----	COHM1764
150	CONTINUE	COHM1705		IF (C1.GE.1.0E-5.AND.C1.LE.CTBM) GO TO 220	COHM1765
C	-----	COHM1706		CALL CHNH07 (II,ALP,ZRO,ZRO,C1,A2,C2,ZRO,ZRO)	COHM1766
C	IDENTIFY ACCAPTABILITY OF DESIGNS F1 AND F2	COHM1707		IF (ALP.LE.0.) GO TO 220	COHM1767
C	-----	COHM1708		IF (C1.GT.CTBM.AND.ALPH.GT.ALPHES) ALPHES=ALP	COHM1768
C	IGOOD = 0 IS ACCAPTABLE.	COHM1709		IF (C1.LT.CTL.AND.ALPH.LT.ALPLN) ALPLN=ALP	COHM1769
C	CV = MAXIMUM CONSTRAINT VIOLATION.	COHM1710		GO TO 220	COHM1770
	IGOOD1=0	COHM1711	210	CONTINUE	COHM1771
	IGOOD2=0	COHM1712	C	-----	COHM1772
	CV1=0.	COHM1713	C	NON-LINEAR CONSTRAINT	COHM1773
	CV2=0.	COHM1714	C	-----	COHM1774
	NVC1=0	COHM1715		IF (C1.GE.1.0E-5.AND.C1.LE.CTAM) GO TO 220	COHM1775
	IF (NCON.EQ.0) GO TO 170	COHM1716		CALL CHNH07 (II,ALP,ZRO,ZRO,C1,A2,C2,ZRO,ZRO)	COHM1776
	DO 160 I=1,NCON	COHM1717		IF (ALP.LE.0.) GO TO 220	COHM1777
	CC=CTAM	COHM1718		IF (C1.GT.CTAM.AND.ALPH.GT.ALPHES) ALPHES=ALP	COHM1778
	IF (ISC(I).GT.0) CC=CTBM	COHM1719		IF (C1.LT.CT.AND.ALPH.LT.ALPHNC) ALPHNC=ALP	COHM1779
	C1=G(I)-CC	COHM1720	220	CONTINUE	COHM1780
	C2=G(I)-CC	COHM1721		IF (III.LT.NCON) GO TO 200	COHM1781
	IF (C2.GT.0.) NVC1=NVC1+1	COHM1722	230	CONTINUE	COHM1782
	IF (C1.GT.CV1) CV1=C1	COHM1723		IF (LIMOBJ.GT.0.OR.SLOPE.GE.0.) GO TO 240	COHM1783
	IF (C2.GT.CV2) CV2=C2	COHM1724	C	CALCULATE ALPHA TO MINIMIZE FUNCTION.	COHM1784
160	CONTINUE	COHM1725		CALL CHNH04 (II,ALPHIN,ZRO,ZRO,F1,SLOPE,A2,F2,ZRO,ZRO,ZRO,ZRO)	COHM1785
	IF (CV1.GT.0.) IGOOD1=1	COHM1726	240	CONTINUE	COHM1786
	IF (CV2.GT.0.) IGOOD2=1	COHM1727	C	-----	COHM1787
170	CONTINUE	COHM1728	C	PROPOSED MOVE	COHM1788
	ALP=A2	COHM1729	C	-----	COHM1789
	OBJ=F2	COHM1730	C	MOVE AT LEAST FAR ENOUGH TO OVERCOME CONSTRAINT VIOLATIONS.	COHM1790
C	-----	COHM1731		A3=ALPHES	COHM1791
C	IF F2 VIOLATES FEWER CONSTRAINTS THAN F1 BUT STILL HAS CONSTRAINT	COHM1732	C	MOVE TO MINIMIZE FUNCTION.	COHM1792
C	VIOLATIONS RETURN	COHM1733		IF (ALPHIN.GT.A3) A3=ALPHIN	COHM1793
C	-----	COHM1734	C	IF A3.LE.0, SET A3 = ALPSID.	COHM1794
C	IF (NVC1.LT.NVC.AND.NVC1.GT.0) GO TO 710	COHM1735		IF (A3.LE.0.) A3=ALPSID	COHM1795
C	-----	COHM1736	C	LIMIT MOVE TO NEW CONSTRAINT ENCOUNTER.	COHM1796
C	IDENTIFY BEST OF DESIGNS F1 ANF F2	COHM1737		IF (A3.GT.ALPHNC) A3=ALPHC	COHM1797
C	-----	COHM1738	C	IF (A3.GT.ALPLN) A3=ALPLN	COHM1798
C	IBEST CORRESPONDS TO MINIMUM VALUE DESIGN.	COHM1739	C	MAKE A3 NON-ZEPO.	COHM1799
C	IF CONSTRAINTS ARE VIOLATED, IBEST CORRESPONDS TO MINIMUM	COHM1740		IF (A3.LE.1.0E-20) A3=1.0E-20	COHM1800
C	CONSTRAINT VIOLATION.	COHM1741	C	IF A3=AC=ALPSID AND F2 IS BEST, GO INVOKE SIDE CONSTRAINT	COHM1801

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C      MODIFICATION.
      ALPB=1.-A2/A3
      ALPA=1.-ALPSID/A3
      JBEST=0
      IF (ABS(ALPB).LT.1.0E-10.AND.ABS(ALPA).LT.1.0E-10) JBEST=1
      IF (JBEST.EQ.1.AND.IBEST.EQ.2) GO TO 20
C      SIDE CONSTRAINT CHECK NOT SATISFIED.
      IF (NCON.EQ.0) GO TO 260
C      STORE CONSTRAINT VALUES IN G2.
      DO 250 I=1,NCON
      G2(I)=G(I)
250    CONTINUE
260    CONTINUE
C      IF A3=A2, SET A3=.9*A2.
      IF (ABS(ALPB).LT.1.0E-10) A3=.9*A2
      MOVE AT LEAST .01*A2.
C      IF (A3.LT.(.01*A2)) A3=.01*A2
C      LIMIT MOVE TO 5.*A2.
      IF (A3.GT.(5.*A2)) A3=5.*A2
C      LIMIT MOVE TO ALPSID.
      IF (A3.GT.ALPSID) A3=ALPSID
C      MOVE A DISTANCE A3*5.
      ALP=A3-A2
      ALPTOT=ALPTOT+ALP
      DO 270 I=1,NDV
      X(I)=X(I)+ALP*(S(I)
270    CONTINUE
      IF (IPRINT.LT.5) GO TO 300
      WRITE (6,780)
      WRITE (6,740) A3
      IF (NSCAL.EQ.0) GO TO 290
      DO 280 I=1,NDV
280    G(I)=SCAL(I)*X(I)
      WRITE (6,750) (G(I),I=1,NDV)
      GO TO 300
290    WRITE (6,750) (X(I),I=1,NDV)
300    CONTINUE
C      -----
C      UPDATE FUNCTION AND CONSTRAINT VALUES
C      -----
      NCAL(1)=NCAL(1)+1
      JGOTO=2
      RETURN
310    CONTINUE
      F3=OBJ
      IF (IPRINT.GE.5) WRITE (6,760) F3
      IF (IPRINT.LT.5.OR.NCON.EQ.0) GO TO 320
      WRITE (6,770)
      WRITE (6,750) (G(I),I=1,NCON)
320    CONTINUE
C      -----
C      CALCULATE MAXIMUM CONSTRAINT VIOLATION AND PICK BEST DESIGN
C      -----
      CV3=0.
      IGOOD3=0
      NVC1=0
      IF (NCON.EQ.0) GO TO 340
      DO 330 I=1,NCON
      CC=CTAM
      IF (ISC(I).GT.0) CC=CTBM
      CONM1802
      CONM1803
      CONM1804
      CONM1805
      CONM1806
      CONM1807
      CONM1808
      CONM1809
      CONM1810
      CONM1811
      CONM1812
      CONM1813
      CONM1814
      CONM1815
      CONM1816
      CONM1817
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      CONM1854
      CONM1855
      CONM1856
      CONM1857
      CONM1858
      CONM1859
      CONM1860
      CONM1861
      C1=G(I)-CC
      IF (C1.GT.CV3) CV3=C1
      IF (C1.GT.0.) NVC1=NVC1+1
330    CONTINUE
      IF (CV3.GT.0.) IGOOD3=1
340    CONTINUE
C      DETERMINE BEST DESIGN.
      IF (IBEST.EQ.2) GO TO 360
      CHOOSE BETWEEN F1 AND F3.
C      IF (IGOOD1.EQ.0.AND.IGOOD3.EQ.0) GO TO 350
      IF (CV1.GE.CV3) IBEST=3
      GO TO 380
350    IF (F3.LE.F1) IBEST=3
      GO TO 380
360    CONTINUE
C      CHOOSE BETWEEN F2 AND F3.
      IF (IGOOD2.EQ.0.AND.IGOOD3.EQ.0) GO TO 370
      IF (CV2.GE.CV3) IBEST=3
      GO TO 380
370    IF (F3.LE.F2) IBEST=3
380    CONTINUE
      ALP=A3
      OBJ=F3
C      IF F3 VIOLATES FEWER CONSTRAINTS THAN F1 RETURN.
      IF (NVC1.LT.NVC) GO TO 710
C      IF OBJECTIVE AND ALL CONSTRAINTS ARE LINEAR, RETURN.
      IF (LINOBJ.NE.0.AND.NLNC.EQ.NCON) GO TO 710
C      IF A3 = ALPLN AND F3 IS BOTH GOOD AND BEST RETURN.
      ALPB=1.-ALPLN/A3
      IF (ABS(ALPB).LT.1.0E-20.AND.IBEST.EQ.3).AND.(IGOOD3.EQ.0) GO TO CONM1891
      710
C      IF A3 = ALPSID AND F3 IS BEST, GO INVOKE SIDE CONSTRAINT
      MODIFICATION.
      ALPA=1.-ALPSID/A3
      IF (ABS(ALPA).LT.1.0E-20.AND.IBEST.EQ.3) GO TO 20
C      -----
C      *****          3 - POINT INTERPOLATION          *****
C      -----
      ALPNC=ALPSID
      ALPCA=ALPSID
      ALPFES=-1.
      ALPHIN=-1.
      IF (NCON.EQ.0) GO TO 440
      III=0
390    III=III+1
      C1=G1(III)
      C2=G2(III)
      C3=G3(III)
      IF (ISC(III).EQ.0) GO TO 400
C      -----
C      LINEAR CONSTRAINT. FIND ALPFES ONLY. ALPLN SAME AS BEFORE.
C      -----
      IF (C1.LE.CTBM) GO TO 430
      II=1
      CALL CNM1807 (II,ALP,ZRO,ZRO,C1,A3,C3,ZRO,ZRO)
      IF (ALP.GT.ALPFES) ALPFES=ALP
      GO TO 430
400    CONTINUE
C      -----
C      NON-LINEAR CONSTRAINT
      CONM1862
      CONM1863
      CONM1864
      CONM1865
      CONM1866
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      CONM1917
      CONM1918
      CONM1919
      CONM1920
      CONM1921

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C	-----	CONH1922	IF (IPRINT.LT.5) GO TO 510	CONH1982
	II=2	CONH1923	WRITE (6,720)	CONH1983
	CALL CNM07 (II,ALP,ZRO,ZRO,C1,A2,C2,A3,C3)	CONH1924	WRITE (6,740) A4	CONH1984
	IF (ALP.LE.ZRO) GO TO 430	CONH1925	IF (NSCAL.EQ.0) GO TO 500	CONH1985
	IF (C1.GE.CT.AND.C1.LE.0.) GO TO 410	CONH1926	DO 490 I=1,NDV	CONH1986
	IF (C1.GT.CTAM.OR.C1.LT.0.) GO TO 420	CONH1927	G(I)=SCAL(I)*X(I)	CONH1987
C	ALP IS MINIMUM MOVE. UPDATE FOR NEXT CONSTRAINT ENCOUNTER.	CONH1928	WRITE (6,750) (G(I),I=1,NDV)	CONH1988
410	ALPA=ALP	CONH1929	GO TO 510	CONH1989
	CALL CNM07 (II,ALP,ALPA,ZRO,C1,A2,C2,A3,C3)	CONH1930	500 WRITE (6,750) (X(I),I=1,NDV)	CONH1990
	IF (ALP.LT.ALPCA.AND.ALP.GE.ALPA) ALPCA=ALP	CONH1931	510 CONTINUE	CONH1991
	GO TO 430	CONH1932	-----	CONH1992
420	CONTINUE	CONH1933	UPDATE FUNCTION AND CONSTRAINT VALUES	CONH1993
	IF (ALP.GT.ALPFES.AND.C1.GT.CTAM) ALPFES=ALP	CONH1934	-----	CONH1994
	IF (ALP.LT.ALPNC.AND.C1.LT.0.) ALPNC=ALP	CONH1935	NCAL(1)=NCAL(1)+1	CONH1995
430	CONTINUE	CONH1936	JGOTO=3	CONH1996
	IF (III.LT.NCON) GO TO 390	CONH1937	RETURN	CONH1997
440	CONTINUE	CONH1938	520 CONTINUE	CONH1998
	IF (LINOBJ.GT.0.OR.SLOPE.GT.0.) GO TO 450	CONH1939	F4=OBJ	CONH1999
C	-----	CONH1940	IF (IPRINT.GE.5) WRITE (6,760) F4	CONH2000
C	CALCULATE ALPHA TO MINIMIZE FUNCTION	CONH1941	IF (IPRINT.LT.5.OR.NCON.EQ.0) GO TO 530	CONH2001
C	-----	CONH1942	WRITE (6,770)	CONH2002
	II=3	CONH1943	WRITE (6,750) (G(I),I=1,NCON)	CONH2003
	IF (A2.GT.A3.AND.(IGOOD2.EQ.0.AND.IBEST.EQ.2)) II=2	CONH1944	CONTINUE	CONH2004
450	CALL CNM04 (II,ALPMIN,ZRO,ZRO,F1,SLOPE,A2,F2,A3,F3,ZRO,ZRO)	CONH1945	C DETERMINE ACCAPTABILITY OF F4.	CONH2005
	CONTINUE	CONH1946	IGOOD4=0	CONH2006
C	-----	CONH1947	CV4=0.	CONH2007
C	PROPOSED MOVE	CONH1948	IF (NCON.EQ.0) GO TO 550	CONH2008
C	-----	CONH1949	DO 540 I=1,NCON	CONH2009
C	MOVE AT LEAST ENOUGH TO OVERCOME CONSTRAINT VIOLATIONS.	CONH1950	CC=CTAM	CONH2010
	A4=ALPFES	CONH1951	IF (ISC(I).GT.0) CC=CTBM	CONH2011
C	MOVE TO MINIMIZE FUNCTION.	CONH1952	C1=G(I)-CC	CONH2012
	IF (ALPMIN.GT.A4) A4=ALPMIN	CONH1953	IF (C1.GT.CV4) CV4=C1	CONH2013
C	IF A4.LE.0, SET A4 = ALPSID.	CONH1954	540 CONTINUE	CONH2014
	IF (A4.LE.0.) A4=ALPSID	CONH1955	IF (CV4.GT.0.) IGODD4=1	CONH2015
C	LIMIT MOVE TO NEW CONSTRAINT ENCOUNTER.	CONH1956	550 CONTINUE	CONH2016
	IF (A4.GT.ALPLN) A4=ALPLN	CONH1957	ALP=A4	CONH2017
	IF (A4.GT.ALPNC) A4=ALPNC	CONH1958	OBJ=F4	CONH2018
C	LIMIT MOVE TO RE-ENCOUNTER CURRENTLY ACTIVE CONSTRAINT.	CONH1959	-----	CONH2019
	IF (A4.GT.ALPCA) A4=ALPCA	CONH1960	DETERMINE BEST DESIGN	CONH2020
C	LIMIT A4 TO 5.*A3.	CONH1961	-----	CONH2021
	IF (A4.GT.(5.*A3)) A4=5.*A3	CONH1962	GO TO (560,610,660),IBEST	CONH2022
C	UPDATE DESIGN.	CONH1963	CONTINUE	CONH2023
	IF (IBEST.NE.3.OR.NCON.EQ.0) GO TO 470	CONH1964	C CHOOSE BETWEEN F1 AND F4.	CONH2024
C	STORE CONSTRAINT VALUES IN G2. F3 IS BEST. F2 IS NOT.	CONH1965	IF (IGOOD1.EQ.0.AND.IGOOD4.EQ.0) GO TO 570	CONH2025
	DO 460 I=1,NCON	CONH1966	IF (CV1.GT.CV4) GO TO 710	CONH2026
	G2(I)=G(I)	CONH1967	GO TO 580	CONH2027
460	CONTINUE	CONH1968	CONTINUE	CONH2028
470	CONTINUE	CONH1969	570 IF (F4.LE.F1) GO TO 710	CONH2029
C	IF A4=A3 AND IGODD1=0 AND IGODD3=1, SET A4=.9*A3.	CONH1970	580 CONTINUE	CONH2030
	ALP=A4-A3	CONH1971	C F1 IS BEST.	CONH2031
	IF (IGOOD1.EQ.0.AND.IGOOD3.EQ.1).AND.ABS(ALP).LT.(1.0E-20) A4=.9*ALP	CONH1972	ALPTOT=ALPTOT-A4	CONH2032
	13	CONH1973	OBJ=F1	CONH2033
C	-----	CONH1974	DO 590 I=1,NDV	CONH2034
C	MOVE A DISTANCE A4*S	CONH1975	X(I)=X(I)-A4*S(I)	CONH2035
C	-----	CONH1976	590 CONTINUE	CONH2036
	ALP=A4-A3	CONH1977	IF (NCON.EQ.0) GO TO 710	CONH2037
	ALPTOT=ALPTOT+ALP	CONH1978	DO 600 I=1,NCON	CONH2038
	DO 480 I=1,NDV	CONH1979	G(I)=G(I)	CONH2039
	X(I)=X(I)+ALP*S(I)	CONH1980	600 CONTINUE	CONH2040
480	CONTINUE	CONH1981	GO TO 710	CONH2041

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610 CONTINUE                                CONM2042 :
C      CHOOSE BETWEEN F2 AND F4.           CONM2043 :
      IF (IGOOD2.EQ.0.AND.IGOOD4.EQ.0) GO TO 620 CONM2044 :
      IF (CV2.GT.CV4) GO TO 710            CONM2045 :
      GO TO 630                             CONM2046 :
620 CONTINUE                                CONM2047 C
      IF (F4.LE.F2) GO TO 710             CONM2048 C
630 CONTINUE                                CONM2049 C
C      F2 IS BEST.                         CONM2050 C
      OBJ=F2                                CONM2051 C
      A2=A4-A2                              CONM2052 C
      ALPTOT=ALPTOT-A2                     CONM2053 C
      DO 640 I=1,NDV                       CONM2054 C
      X(I)=X(I)-A2*(I)                     CONM2055 C
640 CONTINUE                                CONM2056 C
      IF (NCON.EQ.0) GO TO 710            CONM2057 C
      DO 650 I=1,NCON                      CONM2058 C
      G(I)=G2(I)                           CONM2059 C
650 CONTINUE                                CONM2060 C
      GO TO 710                             CONM2061 C
660 CONTINUE                                CONM2062 C
C      CHOOSE BETWEEN F3 AND F4.           CONM2063 C
      IF (IGOOD3.EQ.0.AND.IGOOD4.EQ.0) GO TO 670 CONM2064 C
      IF (CV3.GT.CV4) GO TO 710            CONM2065 C
      GO TO 680                             CONM2066 C
670 CONTINUE                                CONM2067 C
      IF (F4.LE.F3) GO TO 710             CONM2068 C
680 CONTINUE                                CONM2069 C
C      F3 IS BEST.                         CONM2070 C
      OBJ=F3                                CONM2071 C
      A3=A4-A3                              CONM2072 C
      ALPTOT=ALPTOT-A3                     CONM2073 C
      DO 690 I=1,NDV                       CONM2074 C
      X(I)=X(I)-A3*(I)                     CONM2075 C
690 CONTINUE                                CONM2076 C
      IF (NCON.EQ.0) GO TO 710            CONM2077 20
      DO 700 I=1,NCON                      CONM2078 C
      G(I)=G2(I)                           CONM2079 C
700 CONTINUE                                CONM2080 C
710 CONTINUE                                CONM2081 C
      ALP=ALPTOT                            CONM2082 C
      IF (IPRINT.GE.5) WRITE (6,790)      CONM2083 30
      JGOTO=0                                CONM2084 C
      RETURN                                CONM2085 C
C      -----CONM2086 C
C      FORMATS                             CONM2087 C
C      -----CONM2088 C
C      -----CONM2089 C
C      -----CONM2090 C
720 FORMAT (/5X,25HTHREE-POINT INTERPOLATION) CONM2091
730 FORMAT (////56H* * * CONstrained ONE-DIMENSIONAL SEARCH INFORMATION) CONM2092
10N * * *) CONM2093
740 FORMAT (/5X,15HPROPOSED DESIGN/5X,7HALPHA =,E12.5/5X,8HX-VECTOR) CONM2094
750 FORMAT (1X,8E12.4) CONM2095
760 FORMAT (1/5X,5HOBJ =,E13.5) CONM2096
770 FORMAT (/5X,17HCONSTRAINT VALUES) CONM2097
780 FORMAT (/5X,23HTWO-POINT INTERPOLATION) CONM2098
790 FORMAT (/5X,35H* * * END OF ONE-DIMENSIONAL SEARCH) CONM2099
      END CONM2100
      SUBROUTINE CNM07 (II,XBAR,EPS,X1,Y1,X2,Y2,X3,Y3) CONM2101
:
: ROUTINE TO FIND FIRST XBAR.GE.EPS CORRESPONDING TO A REAL ZERO CONM2102
: OF A ONE-DIMENSIONAL FUNCTION BY POLYNOMIAL INTERPOLATION. CONM2103
: BY G. N. VANDERPLAATS CONM2104
: APRIL, 1972. CONM2105
: NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF. CONM2106
: II = CALCULATION CONTROL. CONM2107
: 1: 2-POINT LINEAR INTERPOLATION, GIVEN X1, Y1, X2 AND Y2. CONM2108
: 2: 3-POINT QUADRATIC INTERPOLATION, GIVEN X1, Y1, X2, Y2, CONM2109
: X3 AND Y3. CONM2110
: EPS MAY BE NEGATIVE. CONM2111
: IF REQUIRED ZERO ON Y DOES NOT EXIST, OR THE FUNCTION IS CONM2112
: ILL-CONDITIONED, XBAR = EPS-1.0 WILL BE RETURNED AS AN ERROR CONM2113
: INDICATOR. CONM2114
: IF DESIRED INTERPOLATION IS ILL-CONDITIONED, A LOWER ORDER CONM2115
: INTERPOLATION, CONSISTANT WITH INPUT DATA, WILL BE ATTEMPTED AND CONM2116
: II WILL BE CHANGED ACCORDINGLY. CONM2117
: XBAR1=EPS-1. CONM2118
: XBAR=XBAR1 CONM2119
: JJ=0 CONM2120
: X21=X2-X1 CONM2121
: IF (ABS(X21).LT.1.0E-20) RETURN CONM2122
: IF (II.EQ.2) GO TO 30 CONM2123
:
: CONM2124
: -----CONM2125
: II=1: 2-POINT LINEAR INTERPOLATION CONM2126
: -----CONM2127
: II=1 CONM2128
: YY=Y1*Y2 CONM2129
: IF (JJ.EQ.0.OR.YY.LT.0.) GO TO 20 CONM2130
: INTERPOLATE BETWEEN X2 AND X3. CONM2131
: DY=Y3-Y2 CONM2132
: IF (ABS(DY).LT.1.0E-20) GO TO 20 CONM2133
: XBAR=X2+Y2*(X2-X3)/DY CONM2134
: IF (XBAR.LT.EPS) XBAR=XBAR1 CONM2135
: RETURN CONM2136
: 20 DY=Y2-Y1 CONM2137
: INTERPOLATE BETWEEN X1 AND X2. CONM2138
: IF (ABS(DY).LT.1.0E-20) RETURN CONM2139
: XBAR=X1+Y1*(X1-X2)/DY CONM2140
: IF (XBAR.LT.EPS) XBAR=XBAR1 CONM2141
: RETURN CONM2142
: 30 CONM2143
: CONM2144
: -----CONM2145
: II=2: 3-POINT QUADRATIC INTERPOLATION CONM2146
: -----CONM2147
: JJ=1 CONM2148
: X31=X3-X1 CONM2149
: X32=X3-X2 CONM2150
: QQ=X21*X31*X32 CONM2151
: IF (ABS(QQ).LT.1.0E-20) RETURN CONM2152
: AA=(Y1*X32-Y2*X31+Y3*X21)/QQ CONM2153
: IF (ABS(AA).LT.1.0E-20) GO TO 10 CONM2154
: BB=(Y2-Y1)/X21-AA*(X1+X2) CONM2155
: CC=Y1-X1*(AA*X1+BB) CONM2156
: BAC=BB*BB-4.*AA*CC CONM2157
: IF (BAC.LT.0.) GO TO 10 CONM2158
: BAC=SQRT(BAC) CONM2159
: AA=.5/AA CONM2160
: XBAR=AA*(BAC-BB) CONM2161
: XB2=-AA*(BAC+BB)

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	IF (XBAR.LT.EPS) XBAR=XB2	CONM12162		IF (ICHK.EQ.0) GO TO 70	CONM12222
	IF (XB2.LT.XBAR.AND.XB2.GT.EPS) XBAR=XB2	CONM12163	C	UPDATE VECTOR MS1.	CONM12223
	IF (XBAR.LT.EPS) XBAR=XBAR1	CONM12164		JJ=ICHK	CONM12224
	RETURN	CONM12165		IF (MS1(JJ).EQ.0) JJ=ICHK+NDB	CONM12225
	END	CONM12166		KK=JJ+NDB	CONM12226
	SUBROUTINE CNMNOB (NDB,NER,C,MS1,B,N3,N4,N5)	CONM12167		IF (KK.GT.M2) KK=JJ-NDB	CONM12227
	DIMENSION C(N4), B(N3,N3), MS1(N5)	CONM12168		MS1(KK)=ICHK	CONM12228
C	ROUTINE TO SOLVE SPECIAL LINEAR PROBLEM FOR IMPOSING S-TRANSPOSE	CONM12169		MS1(JJ)=0	CONM12229
C	TIMES S.LE.1 BOUNDS IN THE MODIFIED METHOD OF FEASIBLE DIRECTIONS.	CONM12170	C	-----	CONM12230
C	BY G. N. VANDERPLAATS	CONM12171	C	PIVOT OF B(ICHK,ICHK)	CONM12231
C	NASA-AMES RESEARCH CENTER, MOFFETT FIELD, CALIF.	CONM12172	C	-----	CONM12232
C	REF. 'STRUCTURAL OPTIMIZATION BY METHODS OF FEASIBLE DIRECTIONS'	CONM12173		BB=1./B(ICHK,ICHK)	CONM12233
C	G. N. VANDERPLAATS AND F. MOSES, JOURNAL OF COMPUTERS	CONM12174		DO 40 J=1,NDB	CONM12234
C	AND STRUCTURES, VOL 3, PP 739-755, 1973.	CONM12175		B(ICHK,J)=BB*B(ICHK,J)	CONM12235
C	FORM OF L. P. IS BX=C WHERE 1ST NDB COMPONENTS OF X CONTAIN VECTOR	CONM12176	40	C(ICHK)=CBMAX	CONM12236
C	U AND LAST NDB COMPONENTS CONTAIN VECTOR V. CONSTRAINTS ARE	CONM12177		B(ICHK,ICHK)=BB	CONM12237
C	U.GE.0, V.GE.0, AND U-TRANSPOSE TIMES V = 0.	CONM12178	C	ELIMINATE COEFFICIENTS ON VARIABLE ENTERING BASIS AND STORE	CONM12238
C	NER = ERROR FLAG. IF NER.NE.0 ON RETURN, PROCESS HAS NOT	CONM12179	C	COEFFICIENTS ON VARIABLE LEAVING BASIS IN THEIR PLACE.	CONM12239
C	CONVERGED IN 5*NDB ITERATIONS.	CONM12180		DO 60 I=1,NDB	CONM12240
C	VECTOR MS1 IDENTIFIES THE SET OF BASIC VARIABLES.	CONM12181		IF (I.EQ.ICHK) GO TO 60	CONM12241
C	-----	CONM12182		BB1=B(I,ICHK)	CONM12242
C	CHOOSE INITIAL BASIC VARIABLES AS V, AND INITIALIZE VECTOR MS1	CONM12183		B(I,ICHK)=0.	CONM12243
C	-----	CONM12184		DO 50 J=1,NDB	CONM12244
	NER=1	CONM12185	50	B(I,J)=B(I,J)-BB1*B(ICHK,J)	CONM12245
	M2=2*NDB	CONM12186		C(I)=C(I)-BB1*CBMAX	CONM12246
C	CALCULATE CBMIN AND EPS AND INITIALIZE MS1.	CONM12187	60	CONTINUE	CONM12247
	EPS=-1.0E+10	CONM12188		GO TO 20	CONM12248
	CBMIN=0.	CONM12189	70	CONTINUE	CONM12249
	DO 10 I=1,NDB	CONM12190		NER=0	CONM12250
	BI=B(I,I)	CONM12191	C	-----	CONM12251
	CBMAX=0.	CONM12192	C	STORE ONLY COMPONENTS OF U-VECTOR IN 'C'. USE B(I,1) FOR	CONM12252
	IF (BI.LT.-1.0E-6) CBMAX=C(I)/BI	CONM12193	C	TEMPORARY STORAGE	CONM12253
	IF (BI.GT.EPS) EPS=BI	CONM12194	C	-----	CONM12254
	IF (CBMAX.GT.CBMIN) CBMIN=CBMAX	CONM12195		DO 80 I=1,NDB	CONM12255
10	MS1(I)=0	CONM12196		B(I,1)=C(I)	CONM12256
	EPS=.0001*EPS	CONM12197	80	CONTINUE	CONM12257
	IF (EPS.LT.-1.0E-10) EPS=-1.0E-10	CONM12198		DO 90 I=1,NDB	CONM12258
	IF (EPS.GT.-.0001) EPS=-.0001	CONM12199		C(I)=0.	CONM12259
	CBMIN=CBMIN*1.0E-6	CONM12200		J=MS1(I)	CONM12260
	IF (CBMIN.LT.1.0E-10) CBMIN=1.0E-10	CONM12201		IF (J.GT.0) C(I)=B(J,1)	CONM12261
	ITER1=0	CONM12202		IF (C(I).LT.0.) C(I)=0.	CONM12262
	NMAX=5*NDB	CONM12203	90	CONTINUE	CONM12263
C	-----	CONM12204		RETURN	CONM12264
C	***** BEGIN NEW ITERATION *****	CONM12205		END	CONM12265
C	-----	CONM12206	00		
20	ITER1=ITER1+1	CONM12207	00		
	IF (ITER1.GT.NMAX) RETURN	CONM12208			
C	FIND MAX. C(I)/B(I,I) FOR I=1,NDB.	CONM12209			
	CBMAX=.9*CBMIN	CONM12210			
	ICHK=0	CONM12211			
	DO 30 I=1,NDB	CONM12212			
	C1=C(I)	CONM12213			
	BI=B(I,I)	CONM12214			
	IF (BI.GT.EPS.OR.C1.GT.0.) GO TO 30	CONM12215			
	CB=C1/BI	CONM12216			
	IF (CB.LE.CBMAX) GO TO 30	CONM12217			
	ICHK=I	CONM12218			
	CBMAX=CB	CONM12219			
30	CONTINUE	CONM12220			
	IF (CBMAX.LT.CBMIN) GO TO 70	CONM12221			

APPENDIX C

LIST OF SYMBOLS

A_i	design variable coefficient of profile shape function; Equation (14)
C	blade chord, meters
i	invariant point index; Equation (5); also, index for surface shape functions; Equation (14)
k	dummy index; Equation (11)
M	number of independent flow or geometrical variables to be perturbed; Equation (1)
n	total number of shock points and high-gradient maxima points; Equation (13)
N	total number of invariant points, equal to $n + 2$; Equation (5)
q_j	j th arbitrary geometric or flow parameter to be perturbed; Equation (8)
q_{c_j}	calibration flow value of q_j ; Equation (7)
q_{o_j}	base flow value of q_j ; Equation (7)
Q	approximate flow solution for arbitrary flow quantity; Equation (1)
Q_{c_j}	calibration flow solution for value q_{c_j} of arbitrary parameter; Equation (3)
Q_o	base flow solution for values q_{o_j} of arbitrary parameters; Equation (1)
Q_{1_j}	j th perturbation solution per unit change of perturbed parameter q_j ; Equation (3)
s	strained x coordinate; Equation (2)
x	nondimensional blade-fixed orthogonal coordinate; Equation (1), normalized by C
\bar{x}_j	nondimensional blade-fixed orthogonal coordinate related to j th calibration solution; Equation (3)

- x_1 straining function associated with x coordinate;
Equation (2)
- x_{1_i} straining function associated with i th invariant point;
Equation (5)
- δx_o unit displacement in x direction associated with i th
invariant point; Equations (6) and (10)
- ϵ_j desired perturbation change of j th geometric or flow
parameter; Equation (8)
- $\bar{\epsilon}_j$ perturbation change of j th geometric or flow parameter
between base and calibration flows; Equation (7)

Subscripts

- i denotes quantities associated with i th invariant point
- j denotes perturbation quantities

Superscripts

- o denotes base flow quantities
- c denotes quantities associated with calibration flows

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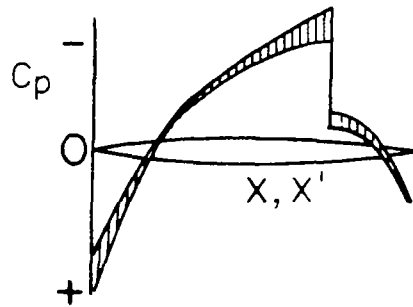
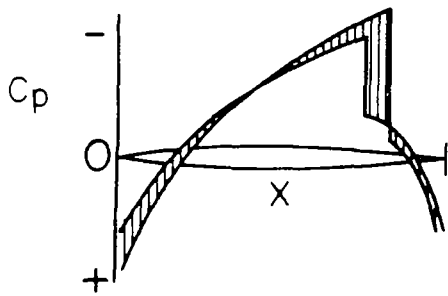
TABLE 1

COMPARISON OF FINAL DESIGN VARIABLES AND OBJECTIVE FUNCTION
 WHEN EMPLOYING FULL NONLINEAR TSONIC SOLUTIONS OR
 PERTURBATION METHOD FOR DIFFERENT CHOICES OF
 CALIBRATION SOLUTION MATRIX FOR SIX DESIGN
 VARIABLE SUBCRITICAL OPTIMIZATION CASE
 STUDY USING MAXIMUM SUCTION SURFACE
 VELOCITY DIFFUSION OBJECTIVE

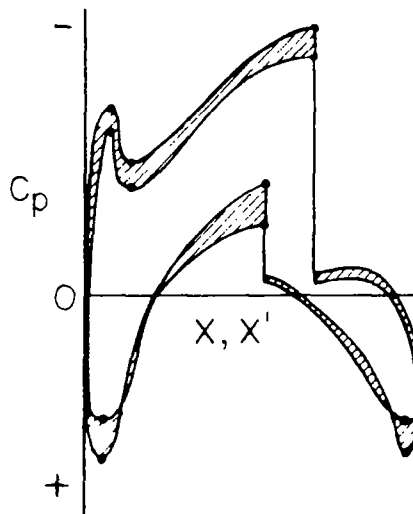
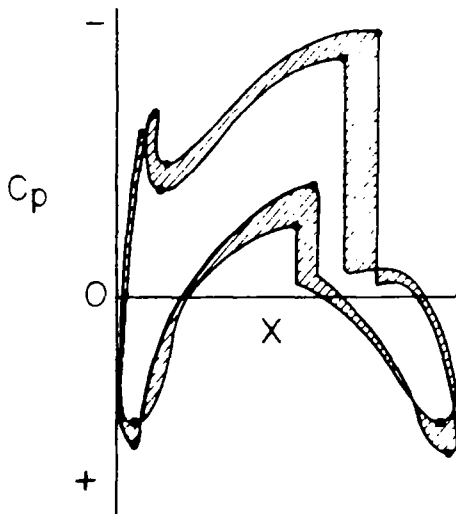
Design Variables							Objective Function
	KOCR	T	ZM	P	TMX	THLE	
<u>INITIAL</u>							
Baseline	-10.0000	0.2500	0.4500	1.50000	0.0500	0.0050	1.8400
Upper Bound	0.0000	0.6000	0.5500	4.0000	0.1000	0.0120	
Lower Bound	-15.0000	0.2000	0.2000	0.5000	0.0300	0.0030	
<u>FINAL</u>							
TSONIC SOLUTIONS ONLY RESULTS IOPT=1							
Final	-7.3854	0.2000	0.5500	0.9220	0.0300	0.0060	1.6764
PERTURBATION SOLUTION RESULTS IOPT=2							
<u>CASE 1</u>							
Calibration	-7.0000	0.2000	0.5500	0.9400	0.0300	0.0060	
Final	-9.1904	0.2342	0.5555	0.9371	0.0358	0.0052	1.6918
<u>CASE 2</u>							
Calibration	-9.0000	0.2350	0.4950	1.6500	0.0550	0.0055	
Final	-8.8994	0.3098	0.5500	0.7463	0.0300	0.0050	1.6829
<u>CASE 3</u>							
Calibration	-11.0000	0.2250	0.4050	1.3500	0.0450	0.0045	
Final	-9.7099	0.3162	0.5500	1.1332	0.0323	0.0055	1.7304
<u>CASE 4</u>							
Calibration	-8.0000	0.2300	0.5000	1.0000	0.0350	0.0058	
Final	-8.8860	0.2814	0.5500	0.9023	0.0370	0.0051	1.6986
<u>CASE 5</u>							
Calibration	-7.0000	0.2000	0.5500	0.9000	0.0300	0.0070	
Final	-9.1846	0.2314	0.5500	0.9397	0.0363	0.0053	1.6909
<u>CASE 6</u>							
Calibration	-11.0000	0.6000	0.2000	4.0000	0.1000	0.0120	
Final	-7.1492	0.3166	0.5500	1.2202	0.0300	0.0046	1.7332
IOPT=3							
Final	-8.0297	0.2000	0.5500	0.7356	0.0363	0.0039	1.6989

Perturbation for
calibration solution
in physical coordinates

Perturbation for
calibration solution
in strained coordinates



(a) Single shock



(b) Multiple shock and high-gradient locations.

Figure 1.- Illustration of perturbation solution
for calibration solution in physical and
strained coordinates

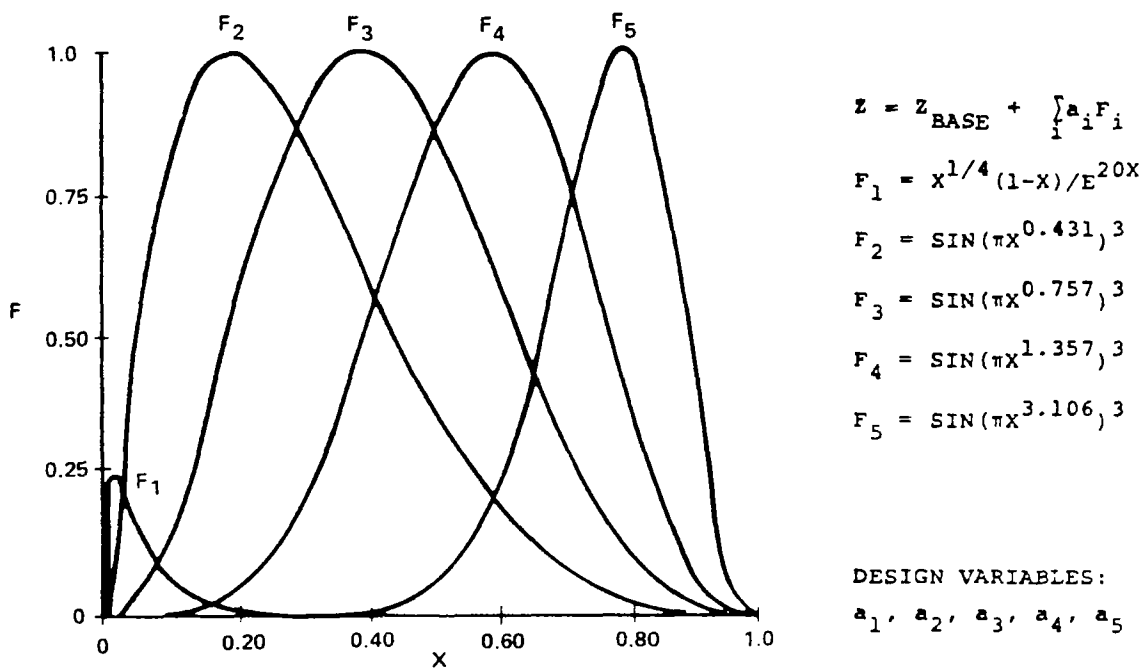


Figure 2.- Illustration of typical ordinate shape functions F_i employed in blade contour alteration optimization problems.

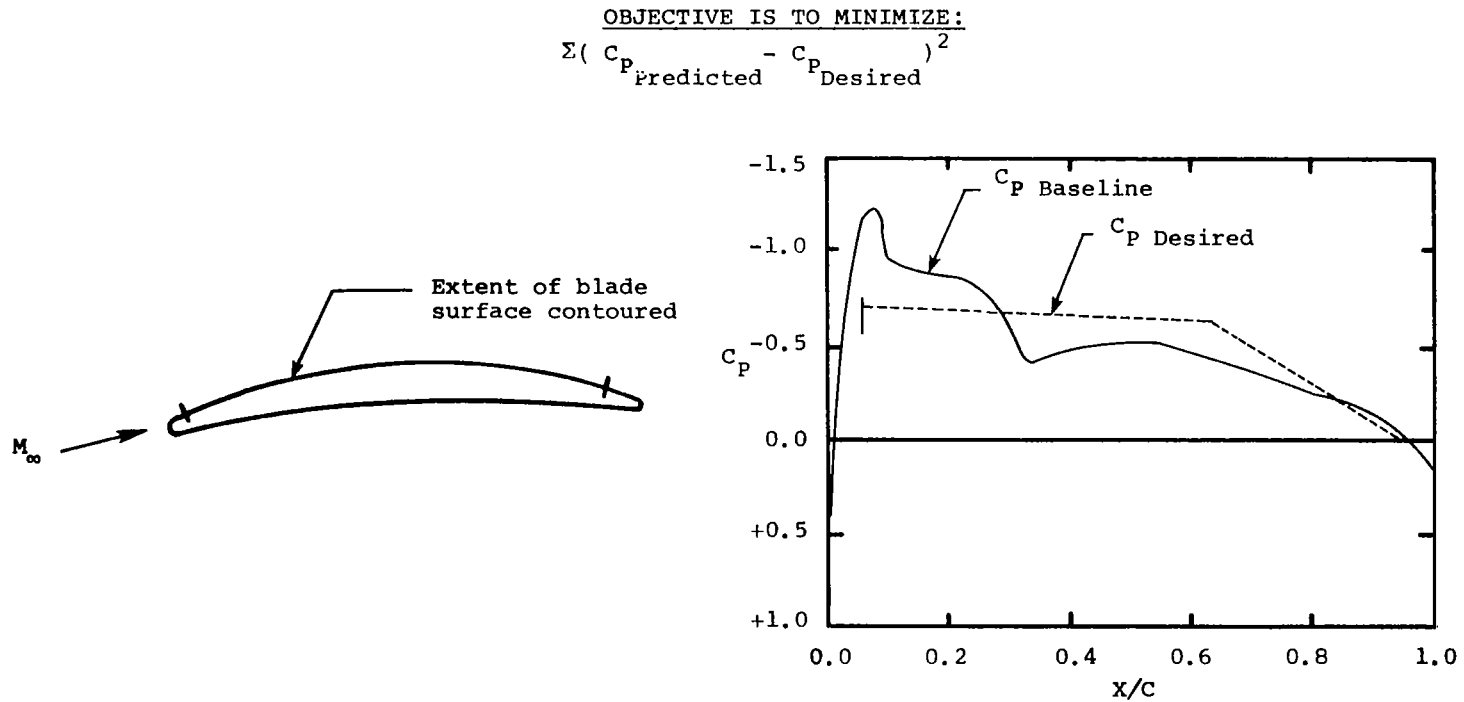


Figure 3.- Illustration of physical basis of optimization problem involving blade surface contouring to tailor the surface pressure distribution to a desired distribution.

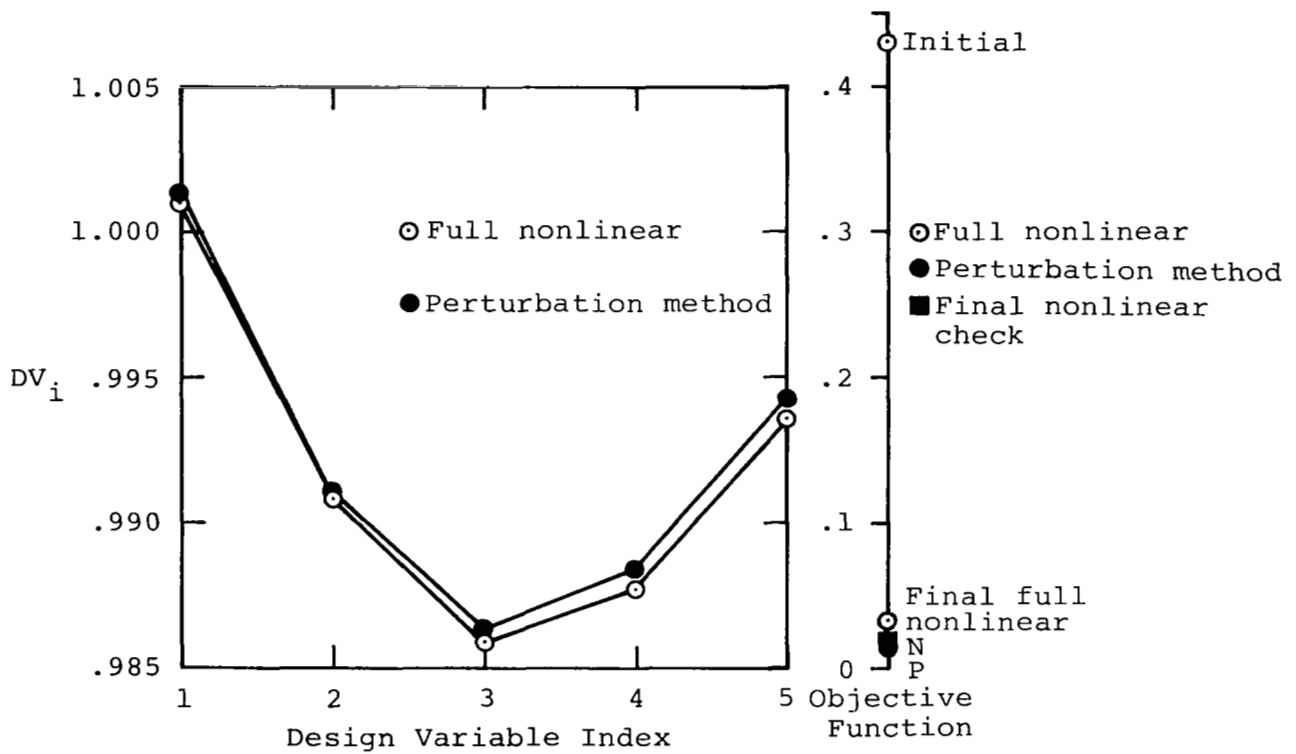


Figure 4.- Comparison of perturbation predicted and full nonlinear results for final design variables and objective function for 5 design variable supercritical case study with surface pressure tailoring objective.

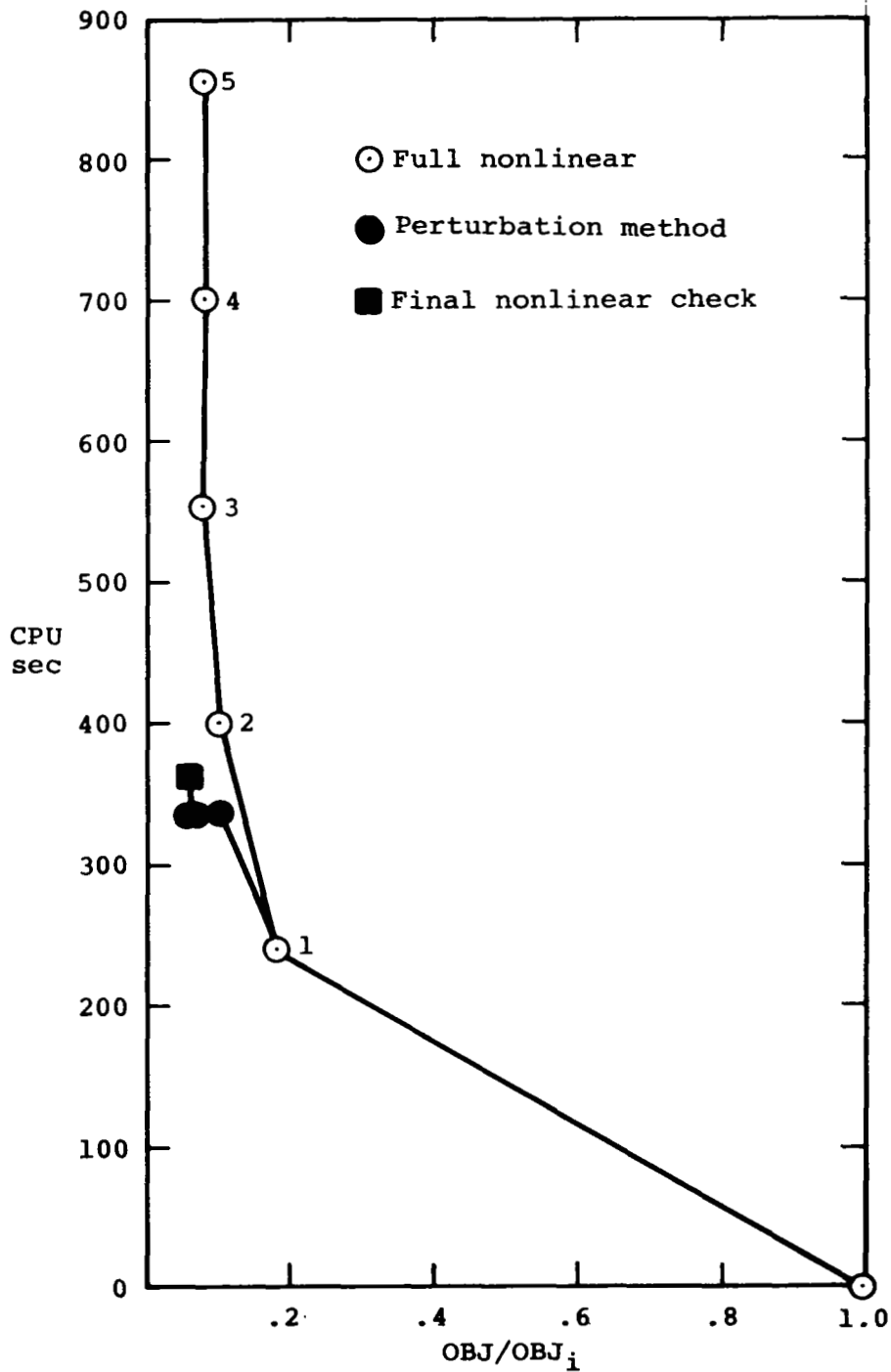


Figure 5.- Comparison of computational work and objective function reduction per optimization search cycle when employing perturbation method after first search cycle (●) or when using full nonlinear solutions (○) for a 5 design variable supercritical case study with surface pressure tailoring objective.

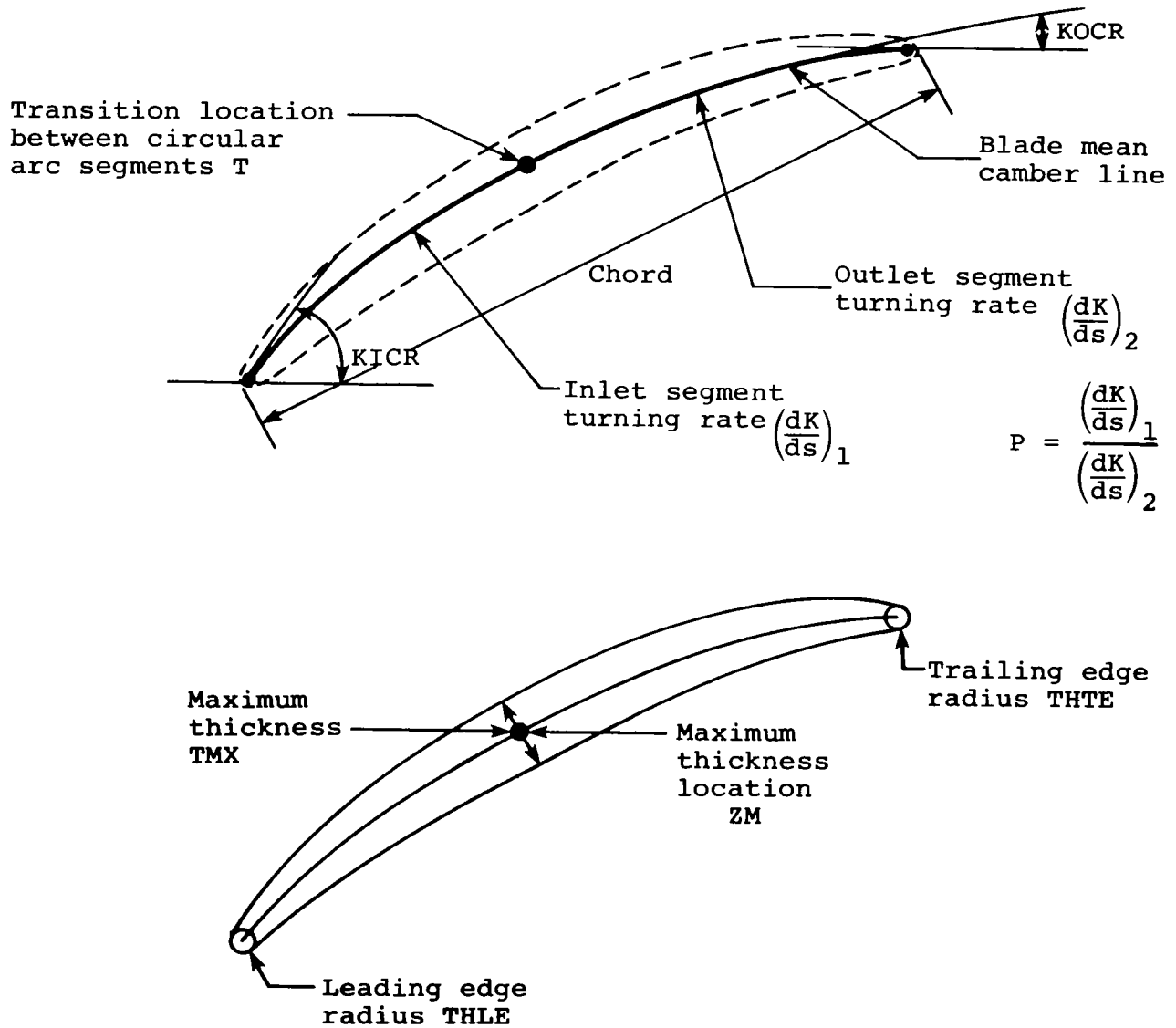


Figure 6.- NASA circular arc blade element layout parameters.

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16. Abstract An investigation was carried out to complete the preliminary development of a combined perturbation/optimization procedure and associated computational code for designing optimized blade-to-blade profiles of turbomachinery blades. The overall purpose of the procedures developed in this study is to provide demonstration of a rapid nonlinear perturbation method for minimizing the computational requirements associated with parametric design studies of turbomachinery flows. The method reported here combines the multiple-parameter nonlinear perturbation method, successfully developed in previous phases of this study, with the NASA TSONIC blade-to-blade turbomachinery flow solver, and the COPES-CONMIN optimization procedure into a user's code for designing optimized blade-to-blade surface profiles of turbomachinery blades. Results of several design applications and a documented version of the code together with a user's manual are provided.					
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