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TESTS WITH THREE-DIMENSIONAL ADJUSTMENTS IN THE RECTANGULAR
WORKING SECTION OF THE FRENCH T2 WIND TUNNEL, WITH AN
AS 07-TYPE SWEEPED-BACK WING MODEL

A. Blanchard, M. J. Payry, J. F. Breil

Translation of "Essais 'd'adaptation tridimensionnelle' de la
veine rectangulaire de la soufflerie T2, en presence d'une
maquette d'aile en fleche du type AS 07," Rapport Technique OA
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16. Abstract This report presents the results obtained on the AS 07 wing and the working section walls for three types of configurations. The first, called "non-adapted," corresponds to the divergent upper and lower rectilinear walls which compensate for limit layer thickening. It can serve as a basis for com- plete flow calculations. The second configuration corresponds to wall shapes determined from calculations which tend to minimize interference at the level of the fuselage. Finally, the third configuration, called "two-dimensional adapta- tion," uses the standard method for T2 profile tests. This case was tested to determine the influence of wall shape and error magnitude. These results are not sufficient to validate the three-dimensional adaptation; they must be coor- dinated with calculations or with unlimited atmosphere tests.			
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NOTATION

$\left. \begin{array}{l} X_p \\ Y_p \\ Z_p \end{array} \right\}$ Cartesian coordinates in the reference working section
 (porthole axis)

$\left. \begin{array}{l} X \\ Y \\ Z \end{array} \right\}$ Cartesian coordinates in the wing reference (leading
 edge to socket)

C Profile chord of the wing section considered

α Angle of the model (fuselage axis)

M_0 Infinite Mach upstream of the flow

M Local Mach (wing or wall)

$$K_p = \frac{p - p_0}{\frac{1}{2} \rho_0 V_0^2} \quad \text{Pressure coefficient}$$

C_z Local or complete-wing lift coefficient

$$\left\{ \begin{array}{l} C_{z \text{ local}} = \int_{\text{profil}} K_p \cdot d\left(\frac{x}{C_{\text{local}}}\right) \\ C_z = \frac{F_z}{\frac{1}{2} \rho_0 V_0^2 \cdot S_{\text{aile}}} \end{array} \right.$$

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1 - INTRODUCTION

/7*

This test series follows a study done in the T2 wind tunnel with the goal of defining a shape for the adaptable walls which would minimize their influence on three-dimensional objects placed in the center of the section or fastened on the side.

The present configuration of the working section does not allow obtaining a shape identical to that of the layer of current existing around a three-dimensional model in unlimited atmosphere (two completely rectilinear and parallel lateral walls, two flexible and bendable upper and lower walls). The planned solution thus consists of using the two bendable walls to minimize the influence of the walls on the model.

The method implemented uses solutions developed by "E. Wedemeyer and L. Lamarche" [5]. A first series of tests was done in cooperation with the University of Berlin on various existing models [6]:

- a C5 revolving body 166 mm long, 0.3% blockage;
- a civil F4 airplane model with 120-mm wingspan and three-component balance;
- a duck-type military airplane model with the same balance.

Another series of tests was then done on a bigger model [7]:

- a C5 body 400 mm long, 1.8% blockage.

*Numbers in the margin indicate pagination in the foreign text.

The results and calculations were compared.

The calculation method was optimized for revolving bodies placed in the center of the section; an extrapolation was tried which placed a half-wing at the wall. In this case, calculation is done as if the section were twice its actual width, using the Mach distribution at the wall measured near the plane of symmetry.

The results obtained on the "16/1000-scale" AS 07 are discussed in this report. They can be divided into two groups: control tests and systematic tests.

Included in the first group is control of wing angling by rotating the walls. The path of the jacks would not permit the displacements required by calculation for angling the model to +2°; we thus used this artificial method after having verified its validity.

The three-dimensional adaptation method supplies the optimal shape of the walls from the first calculation, whatever the initial position of the walls; this was verified in 8 several test configurations. Finally, an adaptation called "two-dimensional" was tested; it uses the normal method for T2 profile tests. This case, without theoretical justification, was tried to see the influence of the shape of the walls and the size of errors which can be made.

The second part of this study corresponds to systematic tests: four configurations were chosen which gave different lift coefficients, without making highly supersonic zones appear on the profiles. For each configuration, three wall positions were tested:

- The first, called "unadapted," corresponds to the upper and lower divergent rectilinear walls compensating for

thickening of the limit layers; it served as our basis for beginning three-dimensional adaptation calculations. These particularly simple limit conditions can also be used for complete calculation of the flow in the working section.

- The second wall shape comes from the three-dimensional adaptation calculation; the flexible sheets are positioned before the gust.

- Finally, the last case corresponds to "two-dimensional adaptation"; the iterative process converges on a single gust.

For each type of test, three gusts are necessary to obtain readings from the six rows of pressure recorders spread along the AS 07 wing.

The experimental results gathered during this series are not sufficient to validate the three-dimensional adaptation method used. Additional calculations must be made to estimate residual corrections. In these tests, a negligible influence of the walls is observed for low lift values or low Mach numbers; inversely, for 2 degrees of incidence or for Mach 0.8, the gaps become significant and can in part be interpreted as variations in aerodynamic incidence.

2 - ADAPTATION PRINCIPLE

The purpose of the adaptable walls is to create an unlimited flow around a model in a working section with finite dimensions; this can be done by controlling the wall conditions, either by their shape in the case of solid walls or by flows of mass through porous walls. The first solution has been chosen at T2, where flexible sheets moved by jacks form the upper and lower plates of the working section [3].

In the case of a three-dimensional body, it is necessary to bend the walls located around the model to arrive at a shape near the layer of current existing around the model in unlimited atmosphere. This solution is not at present possible at T2, but on the other hand it is possible to use the two flexible /9 walls to minimize residual corrections due to the influence of the walls on the object.

2.1 Two-dimensional adaptation

The details of the process will be found in [2] and [4]; it uses a coupling between the real flow in the working section (internal field) and a calculated virtual flow outside the wind tunnel (external field). Coupling occurs on a control surface near the walls through speed vector components. Adaptation is achieved by an iterative process acting on the shape of the walls: the components of the speed on the control surface become available at each iteration; they are extrapolated from the pressure measurements at the wall. The velocities needed on the control surface to achieve an unlimited external flow are calculated by the Green function following an inverse method. A method of optimized relaxation between the internal and external flows for the vertical velocity component, followed by an integration along each flexible wall, supplies the new shape of the wall. The real shape needed is obtained by adding the thickness displacement of the four wall limit layers.

2.2 Three-dimensional adaptation

For three-dimensional adaptation, the process is different [5]: it uses schematization of the model through distribution of sources and vortices in a narrow horseshoe placed on the section axis. This schematization gives a good representation of axisymmetrical bodies mounted in the middle of the working section.

The originality of the method lies in then doing a linear transformation, which permits passing directly from distribution of velocities at the walls to the adapted form without needing to determine the intensity of singularities. The optimized shape of the walls is thus theoretically obtained from the first calculation; this shape, which is not exactly "adapted," minimizes residual corrections on the model caused by the influence of the walls.

Using this method for a half-wing at the wall is abusive, because the base schematization does not represent a wingspan; it has nonetheless been tried here by replacing the lateral door by a plane of symmetry leading to a fictional double section width, and taking the Mach distribution of the flexible walls near the plane of symmetry as reference.

3 - EXPERIMENTAL EQUIPMENT

The T2 transonic wind tunnel is pressurizable and can function at low temperatures; only minimum-pressure and ambient-temperature tests were done during this series.

3.1 Working section equipment

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The working section has an almost square section of $0.39 \times 0.37 \text{ mm}^2$ at the entrance. Flexible sheets of Invar make up the upper and lower walls, equipped with three rows of pressure recorders whose coordinates are given in figures 7 and 8. The sheet-positioning mechanism is described in [2], [3], and [4].

The left lateral door has three portholes with pressure recorders placed along horizontal and vertical lines whose coordinates are shown in figures 7 and 9.

The pressure recorders are linked to the Scanivalves, each of whose head can observe 48 positions in 5 seconds.

The position of the wing in the working section is given in figure 6.

The Mach number of the flow is set by a second neck controlled by the computer which controls the gust.

No other equipment or wind tunnel measurement method was used.

3.2 Mounting the wing

The AS 07 wing model with a scale of "16/1000" is shown by the photographs in figure 5. The method of mounting the wing on the wall is shown (figure 6), the plane of the wing and its specifications are given (figures 10 and 11), and the shape of the profiles which compose it and the positions of the pressure recorders are indicated (figures 12 and 13).

There are six rows, each with 16 recorders on the inner and outer sections and one on the leading edge; they are placed across the wingspan so as to form lines with constant chord percentages. These recorders communicate with tubes placed in grooves along the wingspan; each tube communicates with three recorders (either on the external wing or on the internal wing). When one of the three rows of recorders is used to measure pressure, the other two are covered with thin (0.05-mm) adhesive strips. It is thus possible to simultaneously measure pressure on two sections of the wing (one internal and one external); measurement of velocities over the entire wing thus requires three different gusts.

The wing is mounted on a half-fuselage linked to a porthole, whose rotation ensures the angling of the wing-

fuselage assembly; the angular reference is the rectilinear part on the back of the fuselage [1].

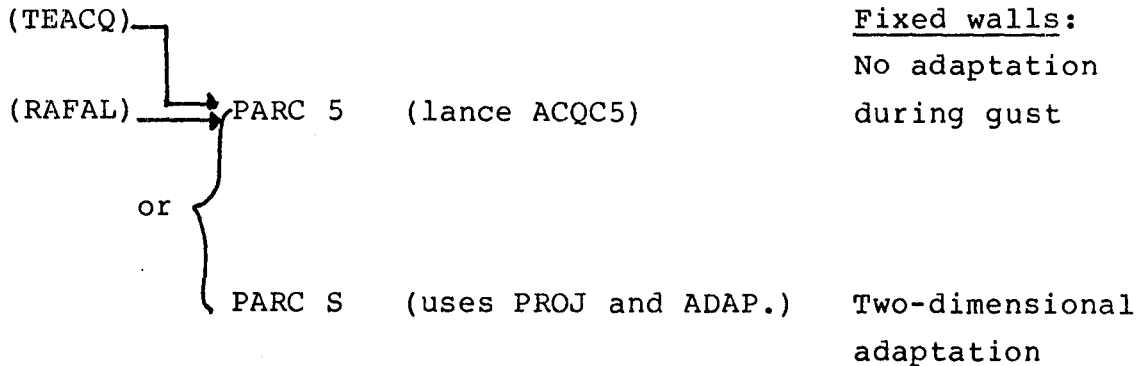
3.3 Acquisition and examination program

The T2 wind tunnel is linked to a team of two computers, one concerned with creating and regulating the gust and the other with obtaining data and storing measurements to disk at the end of the gust.

These tests are pursuant to the series done on the /11 C5 body and use its principal elements.

Disk cartridge LU 26, Program
 LU 34, Test files, calculation files

Acquisition program



Initialization of programs { with (TR,) RINC 5 (For PARC 5)
 { or (TR,) RINC S (For PARC S)

Test file

AD --- test number from AD 100 to AD 173

Wall positioning file

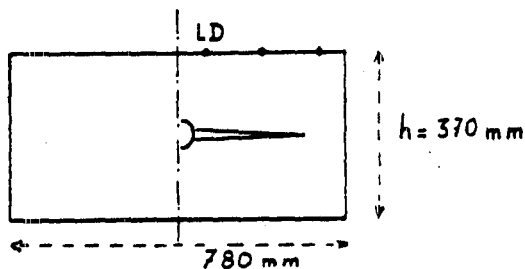
- any test file AD---
- or calculation file AD 9 ---
- or special file { AD 4: Divergent rectilinear walls of symmetrical limit layers.
AD 444: AD 4 + 10' rotation upward
AD 445: AD 4 + 30' rotation upward

Three-dimensional adaptation calculation

Calculation from a test file AD ---

VKJ 43 Calculation of wall shapes without rotation

VKI M Calculation of wall shapes with rotation



- section length 780 mm
- ratio $c = h/b = 2.1081$
- reference recorders:
right lateral RL
- weighting coefficients
file VKJ - R (cartridge
LU 43)

→ Filing to disk

File for new calculated wall shapes

AD 9 --- beginning test number for the calculation

Programs for examination of AD--- files

LTCS:

- graphs local profile Mach numbers
- graphs K_p
- lists AD file
- calculates C_z

LTC 51:

- graphs wall Mach numbers
- graphs wall shapes
- starts LTC 52 (does an RP, LTC 52)

LTC VK:

- graphs only wall shapes calculated by VKI 43 or VKIM (from AD 9---).

4 - SUMMARY OF TESTS PERFORMED

A previous study was done on the AS 07 wing [1]. We verified in one case that the same results would occur, although the working section was modified when the T2 wind tunnel was adapted for cryogenics.

The first control tests were done by measuring rows 2 and 5 of pressure recorders for the Mach numbers and incidences indicated below:

α	M_0		
	0,6	0,7	0,8
+2°	X	X	X
0	X	X	X
-2°	X	X	

Four configurations were selected for systematic tests: /13

α	M_0		
	0,6	0,7	0,8
+2°	X		
0°	X		X
-2°	X		

They correspond to a sampling of lift coefficients and to an infinite Mach effect upstream, while limiting the supersonic zones which appear on the profiles.

Figure 1 shows the list of tests in chronological order, and figures 2, 3, and 4 classify them by configuration.

We first showed that rotation of the upper and lower walls was equivalent to angling the model at the same angle. This artifice was made necessary because the path of the jacks did not permit the displacements required by calculation of three-dimensional adaptation for a model incidence of +2°.

- Divergent rectilinear walls

α gened.	α Display	Wall Start	M_0	
			0,6	0,8
+2°	+2°	AD 4	AD 120	
	+1,5°	AD 445	AD 122	
0°	0°	AD 4	AD 107 - AD 109	AD 108 - AD 132
	-0,5°	AD 445	AD 137	AD 139

M_0

$\alpha_{\text{aérod.}} = 0^\circ$	(α CALCUL	0,6	:	0,8
			:	
	(0° VKI 43	117	:	AD 119
	($-0,5^\circ$ VKI M	138	:	AD 141
			:	

The three-dimensional adaptation method theoretically supplies the optimal shape of the walls from the first calculation, whatever the initial position of the flexible sheets. Controls were done in this respect for the following configurations:

M_0

(α	0,7	:	0,8
(display		:	
($+1,5^\circ$:	AD 127 (1)
		:	AD 128 (2)
		:	AD 129 (3)
(0°	AD 115 (1)	:	AD 118 (1)
	AD 116 (2)	:	AD 119 (2)
($-0,5^\circ$:	AD 140 (1)
		:	AD 141 (2)
		:	

The figure in parentheses after the file number indicates the order of the iteration; the wall-positioning file thus results from calculation of the preceding test. (Iteration (0) is the test done with rectilinear walls.)

We also verified that the tests called "two-dimensional adaptation" converged rapidly, as is the case for the profile tests; it is sufficient for that to compare the wall position of

the 3rd and 4th iterations done during the same gust; the two positions are always close. In general, the beginning shape chosen is near the adapted shape, but we have tested this convergence in the two particular cases when the beginning shape was far from the adapted shape. The beginning file chosen was AD 4: rectilinear walls divergent from limit layers and symmetrical.

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Configuration: $Mo = 0.7$ $\alpha = +1.5^\circ$ File AD 130 (1)
Configuration: $Mo = 0.8$ $\alpha = 0^\circ$ File AD 133 (1)
followed by File AD 134 (2)

Comparisons were made between the various wall positions; they are noted:

- "Non," for divergent rectilinear walls
- "2D," for two-dimensional adaptation done with the PARCS program
- "3d," for positioning of the walls in the shape calculated by the VKI 43 or VKI M program

It was decided to do systematic tests for the three cases of "adaptation," the non-adapted case serving as a basis for three-dimensional calculation (any wall shape will work); this case can also serve as a basis for complete flow calculations, because here the limit conditions are particularly simple. The two-dimensional adaptation, a priori outside the subject of the study, was systematically tested to use as a comparison with the assumed optimal shape.

Finally, four configurations for three cases of adaptation, reproduced three times to have the velocity field on all of the wing, were tested; these 36 gusts make up the systematic tests listed in figure 26a.

5 - CONTROL TESTS

We will not present all the tests done, but only a selection of cases judged most interesting, since the goal of this series is not to evaluate the AS 07 wing.

5.1 Angling by wall rotation

Of the five configurations tested (paragraph 4), three are presented. The first corresponds to $M_0 = 0.6$ and $\alpha = +2^\circ$ for rectilinear walls (figure 14); this is the configuration which obliged us to use this artifice, as the three-dimensional case could not be tested.

Figure 15 shows the comparison of Mach numbers on the walls and on the wing, for an aerodynamic incidence equal to 0° and a Mach number equal to 0.8, in the case of rectilinear walls. Figure 16 presents the same configurations but for wall shapes coming respectively from calculations VKI 43 and VKI M.

The results of figures 14 and 15 show that the high Mach case is the most recordable, but the correspondence of the tests remains good. Figure 16 shows that the VKI M calculation makes perfect allowance for total rotation.

It is thus possible to display a model incidence /16 different from that desired and to compensate by rotating the walls.

5.2 Convergences of iterations

5.2.1 Three-dimensional adaptation

Several calculations for optimization of wall shape were connected for one configuration. The last test is always recalculated, leading to a wall shape which by definition

will not be used, but which will in fact constitute an additional iteration.

Of the four tested cases, two are presented in figures 17 and 18; the first ($Mo = 0.7$ and $\alpha = 0^\circ$) shows that the adapted shape is practically obtained from the first iteration; in the second case--much more difficult ($Mo = 0.8$ and $\alpha = +2^\circ$)--it is necessary to wait for the second calculation. This second case corresponds to a freely supersonic regime of the wing which will not be studied systematically herein.

5.2.2 Two-dimensional adaptation

In all tests done, the 3rd iteration is always identical to the 4th and last iteration of the gust, even when the upper and lower walls have been repositioned in a shape very different from the "adapted" shape. This is the case shown in figure 19 corresponding to $Mo = 0.8$ and $\alpha = 0^\circ$.

To confirm the validity of this statement, a second test was done, positioning the flexible sheets on the preceding shape; the values obtained can thus be considered to correspond to the 4th, 5th, 6th, and 7th iterations of the test; they are all identical (figure 20), which confirms that the convergence was well obtained.

5.3 Non/2-D/3-D comparison

Two cases are presented here, one of which is not part of the systematic tests:

- $Mo = 0.7$ $\alpha = 0^\circ$
- $Mo = 0.8$ $\alpha = 0^\circ$

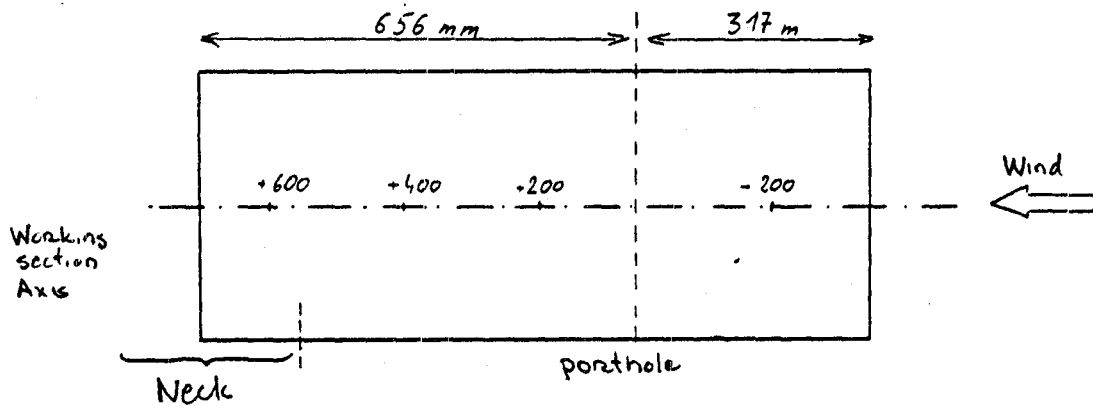
The gaps observed following the types of "adaptation" will become more significant as lift and Mach number upstream increase. The adaptation called "two-dimensional" gives results nearer to the non-adapted case; in fact, everything happens as if the aerodynamic incidence of the two-dimensional case were higher than that of the tests with a wall shape adapted in three dimensions. On the other hand, rectilinear walls lead to a higher effective Mach number upstream (blockage effect).

In the first case (figure 21), the gaps are moderate; they are more significant in the second case (figure 22). Observation of the direction of the walls leaving the convergent (figure 21) shows that effectively the direction of the flow upstream is no longer horizontal in the "2-D" case, unlike the "3-D" case; the angular reference was given by the "non-adapted" case. The effect produced is incontestable, because we /17 previously demonstrated that rotation of the wall assembly modified the aerodynamic incidence of the model; however, this is not sufficient to prove that the 2-D case is erroneous, because the direction of the current lines in unlimited atmosphere is not known. We note also the very different shapes of the walls downstream; they go downward for the "3-D" cases, which is logical allowing for the chosen schematization (horseshoe vortex) and the calculation made (in the plane of symmetry). But once more, that does not prove that the shape obtained is optimum.

Finally, one can observe on the last figure (23) that the effect produced by modifying the shape of the walls is not constant across the wingspan. This was predictable due to the working section geometry itself, allowing for twist of the wing and for three-dimensional effects.

5.4 Visualizations

For three configurations, oil visualizations were done on the left door of the working section, giving the direction of the current lines 55.4 mm from the end of the wing. Reference marks were made, making it possible to locate the positions relative to the current lines and to measure their deviations.



The end of the wing is located between the abscissas 91.06 mm and 135.86 mm from the porthole (figure 6) and very near to the section axis (function of the incidence).

The maximum deviations noticed are located on the section axis slightly behind the tip of the wing (figures 24, 25, and 26).

M_0	α	Walls	δ_{\max}
0,6	+2°	"Non-adapted" AD 4	(5°.....6°)
0,6	+2°	'Adapted 2-D	(5°.....6°)
0,6	-2°	"Non-adapted" AD 4	~ 0,5°

Figure 24

Figure 25

Figure 26

The photos taken from behind clearly show the deviations of the current lines.

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6 - SYSTEMATIC TESTS

For the 36 gusts that made up the systematic tests (paragraph 4 and figure 26a), the following information is given: wall shape (figures 27 and 28), Mach numbers of the three rows of recorders on the adaptable walls (figures 29, 30, 31, and 32), Mach numbers of the left lateral door (figures 33, 34, 35, and 36) following the horizontal axis or the three verticals, and finally spread of K_p on the AS 07 wing (figures 37 to 44).

Numerical values for these curves are given in the attached test listings. File numbers corresponding in chronological order to the experiments were kept in the interests of clarity.

Here will be found a systematic comparison of the three cases of adaptation--"Non/2-D/3-D"--and their influence on the speed distributions whose principal characteristics were seen in paragraph 5.3.

Finally, integration of K_p for each section supplies local lift coefficient C_z . The values are tabulated in figure 45; they were traced along the wingspan of the various configurations tested (figures 46 and 47). It is observed that the internal wing changes less rapidly than the external wing with incidence (figure 46) or Mach number upstream (figure 47).

On the other hand, the gap between the "non-adapted" and "adapted 3-D" cases increases with the lift.

Local C_z were multiplied by the chord of the profile in the section considered; the product $C_z \cdot C$ represents local /19 contribution to wing lift. The values obtained were traced in this representation (figures 48 and 49); this weighting modifies the appearance of the curves ("elliptic" distribution plane), but the observed tendencies are the same.

Finally, integration of the curves in this last representation supplies the overall lift coefficient of the wing, which was reported as a function of incidence (figure 50). We have also reported the lift measured during the preceding series [1], done between rectilinear walls for a Mach number upstream of 0.47. The effect of compressibility is felt more as supersonic zones develop on the wing.

7 - CONCLUSION

This series of tests on the AS 07 wing is registered as a study on three-dimensional adaptation of the T2 wind tunnel. It uses the two flexible walls to minimize residual corrections in the presence of a three-dimensional model. It implements the "E. Wedemeyer and L. Lamarche" method where schematization of the model by a distribution of singularities adequately represents an axisymmetrical body. Extrapolation of these methods in the case of a half-wing at the wall has no ultimate goal; it serves merely as a preliminary phase, to observe the influence of wall shape in various sections of the wing, to study the convergence of the method, and to make adjustments (rotation of walls, incidence, etc.).

On the other hand, these experiments can serve as a basis for calculating potential three-dimensional flow around the model. Then, a three-dimensional object placed in the section

could be more elaborately schematicized; it would lead to development, as for axisymmetrical bodies, of a method of adaptation minimizing the influence of the walls on the model.

At present, it is difficult to know if the shape called "adapted 3-D" is nearer to the values of unlimited atmosphere than the shape "adapted 2-D," but it is definitely not the optimum shape.

The tests will next be completed by directional limit layer readings on the lateral wall at the level of the end of the wing. The direction of the current lines in this area will be an important element in the reality-calculation comparison.

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Wall shape	
Wall Mach	
Profile Mach	14
- Second control ($\alpha = 0^\circ$, $Mo = 0.8$ Non-adaptable)	
Wall shape	
Wall Mach	
Profile Mach	15
- Third control ($\alpha = 0^\circ$, $Mo = 0.8$ 3-D)	
Wall shape	
Wall Mach	
Profile Mach	16
3.2 <u>Convergence of iterations</u>	
a - 3-D	
- First case ($\alpha = 0^\circ$, $Mo = 0.7$)	
Wall shape	
Profile Mach	17
- Second case ($\alpha = +2^\circ$, $Mo = 0.8$)	
Wall shape	
Profile Mach	18

b - 2-D ($\alpha = 0^\circ$, $Mo = 0.8$)

- Beginning of AD 4 (File AD 133)
Wall shape
Profile Mach 19
- Beginning of a similar shape: AD 133 (File AD 134)
Wall shape
Profile Mach 20

3.3 Non/2-D/3-D comparison

- ($\alpha = 0^\circ$, $Mo = 0.7$) Wall shape
Wall Mach 21
- ($\alpha = 0^\circ$, $Mo = 0.7$) Profile Mach (2)
Profile Mach (3) 21
- ($\alpha = 0^\circ$, $Mo = 0.8$) Wall shape
Wall Mach 22
- ($\alpha = 0^\circ$, $Mo = 0.8$) Profile Mach (2)
Profile Mach (3) 22
- ($\alpha = 0^\circ$, $Mo = 0.8$) Kp 23

4. Visualization, left lateral door

- ($\alpha = +2^\circ$, $Mo = 0.6$) Non - front
Visu (2) - back 24
- ($\alpha = +2^\circ$, $Mo = 0.6$) 2-D - front
Visu (1) - back 25
- ($\alpha = +2^\circ$, $Mo = 0.6$) Non - front
Visu (3) - back 26

5. Use in 4 base cases

5.1 Wall shape

- $\alpha = -2^\circ$ $Mo = 0.6$
- $\alpha = +2^\circ$ $Mo = 0.6$ 27
- $\alpha = 0^\circ$ $Mo = 0.6$
- $\alpha = 0^\circ$ $Mo = 0.8$ 28

5.2 Adaptable wall Mach

- ($\alpha = -2^\circ$ $Mo = 0.6$) - Non
- 2-D
- 3-D 29

- ($\alpha = 0^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	30
- ($\alpha = +2^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	31
- ($\alpha = 0^\circ$ Mo = 0.8)	- Non - 2-D - 3-D	32

5.3 Lateral wall Mach

- ($\alpha = -2^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	33
- ($\alpha = 0^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	34
- ($\alpha = +2^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	35
- ($\alpha = 0^\circ$ Mo = 0.8)	- Non - 2-D - 3-D	36

5.4 Kp

- ($\alpha = -2^\circ$ Mo = 0.6)	Non adaptable	37
- ($\alpha = -2^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	38
- ($\alpha = 0^\circ$ Mo = 0.6)	Non adaptable	39
- ($\alpha = 0^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	40
- ($\alpha = +2^\circ$ Mo = 0.6)	Non adaptable	41
- ($\alpha = +2^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	42
- ($\alpha = 0^\circ$ Mo = 0.8)	Non adaptable	43

- ($\alpha = 0^\circ$ Mo = 0.8)	- Non	
	- 2-D	
	- 3-D	44

5.5 Cz

- Cz recapitulative		45
- Cz Mo = 0.6 (3 inc.)		46
- Cz $\alpha = 0^\circ$ (2 Mach)		47
- Cz X chord Mo = 0.6 (3 inc.)		48
- Cz X chord $\alpha = 0^\circ$ (2 Mach)		49
- Cz (α)		50

TEST TABLES
FIGURES 1 TO 4

Figure 1

List of "AS 07 wing" tests

File AD4 : Divergent rectilinear walls
 AD445 : Idem + 30° rotation (upward)
 AD--- : Test file No. ---
 AD9---- : 3-D calculation of new wall position

A File	B	C	D	E
* A	INC.	RANGÉES	FICHER	ROT.
* FICHER	AFF.	DE PRISES	DE DEPART	PAROIS
* NB.	MACH	DE	ADAPT.	D'ITER.
* AD105	0	2 - 5	AD4	0
* AD107	0	"	"	0
* AD109	0	"	"	0
* AD110	-2	"	"	0
* AD115	0	"	AD9105	0
* AD116	0	"	AD9115	0
* AD117	0	"	AD9107	0
* AD118	0	"	AD9108	0
* AD119	0	"	AD9118	0
* AD120	+2	"	AD4	0
* AD122	+1.5	"	AD445	30'
* AD123	+1.5	"	AD9122	30'
* AD124	+1.5	"	AD445	30'
* AD125	+1.5	"	AD9124	30'
* AD126	+1.5	"	AD445	30'
* AD127	+1.5	"	AD9126	30'
* AD128	+1.5	"	AD9127	30'
* AD129	+1.5	"	AD9128	30'
* AD130	+1.5	"	AD4	0
* AD131	+1.5	"	AD130	0
* AD133	0	"	AD4	0
* AD134	0	"	AD133	0
* AD135	0	"	AD134	0
* AD136	0	"	AD135	0
* AD137	-0.5	"	AD445	30'
* AD138	-0.5	"	AD9137	30'
* AD139	-0.5	"	AD445	30'
* AD140	-0.5	"	AD9139	30'
* AD141	-0.5	"	AD9140	30'
* AD142	-2	"	AD4	0
* AD143	-2	"	AD9142	0
* AD144	-2	"	AD136	0
* AD145	+2	"	AD131	0
* AD146	+2	1 - 4	AD145	0
* AD147	+1.5	"	AD445	30'
* AD148	+1.5	"	AD9122	30'
* AD149	0	"	AD136	0
* AD150	0	"	AD4	0
* AD151	0	"	AD9107	0
* AD152	0	"	AD134	0
* AD153	0	"	AD4	0
* AD154	0	"	AD9118	0
* AD155	-2	"	AD144	0
* AD156	-2	"	AD4	0
* AD157	-2	"	AD9142	0
* AD158	-2	3 - 6	AD144	0
* AD159	-2	"	AD4	0
* AD160	-2	"	AD9142	0
* AD161	0	"	AD136	0
* AD162	0	"	AD4	0
* AD163	0	"	AD9107	0
* AD164	0	"	AD134	0
* AD165	0	"	AD4	0
* AD166	0	"	AD9118	0
* AD167	+1.5	"	AD445	30'
* AD168	+1.5	"	AD9122	30'
* AD169	+2	"	AD145	0

Figure 2

Rows of recorders : 1-4

NON ADAPTE				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+1.5	+2	147		
0	0	150		153
-2	-2	156		

ADAPTE 3-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+1.5	+2	148		
0	0	151		154
-2	-2	157		

ADAPTE 2-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+2	---	146		
0	---	149		152
-2	---	155		

Affichee = Displayed

Figure 3

Rows of recorders : 2-5

NON ADAPTE				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+2	+2.17	121		
	+2	120		
+1.5	+2	122	124	126
0	0	107 109	105	108 132
-0.5	0	137		139
-2	-2	142	110	

ADAPTE 3-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+1.5	+2	123	125	127(1) 128(2) 129(3)
0	0	117	115(1) 116(2)	118(1) 119(2)
-0.5	0	138		140(1) 141(2)
-2	-2	143		

ADAPTE 2-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+2	---	145		
+1.5	---	131	130	
0	---	136	135	134
-2	---	144		

Figure 4

Rows of recorders : 3-6

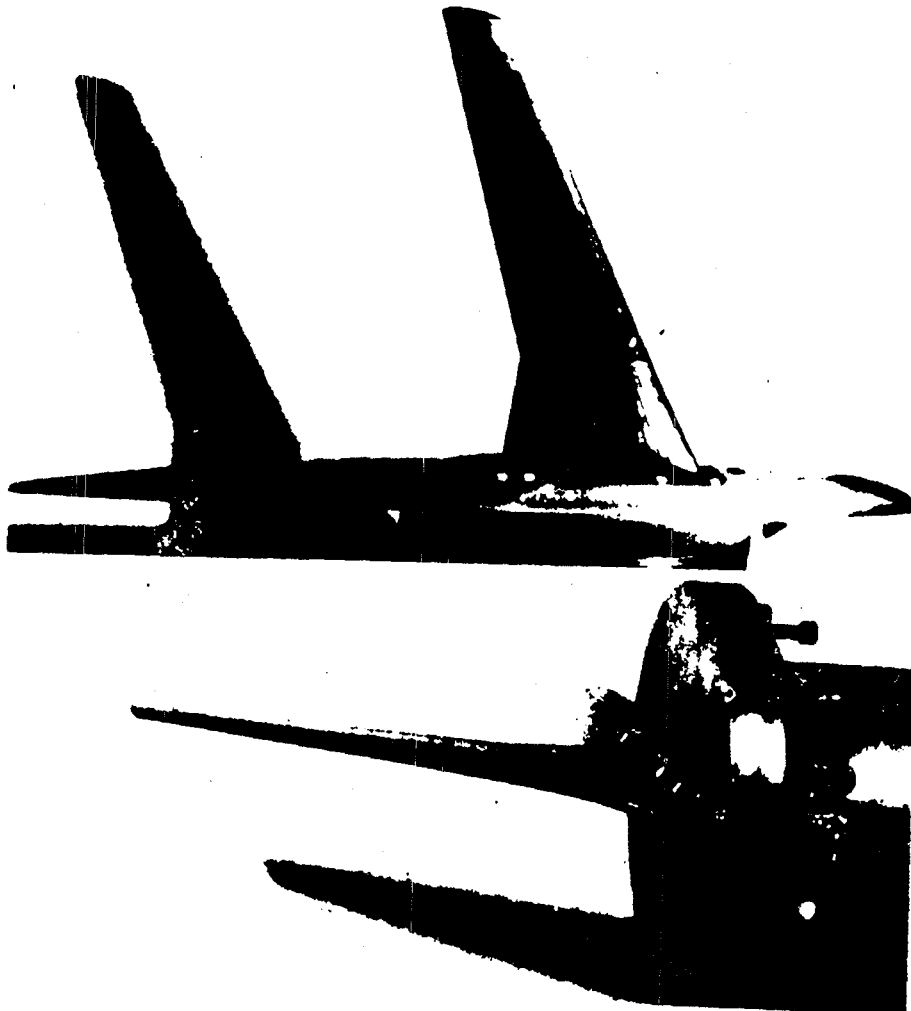
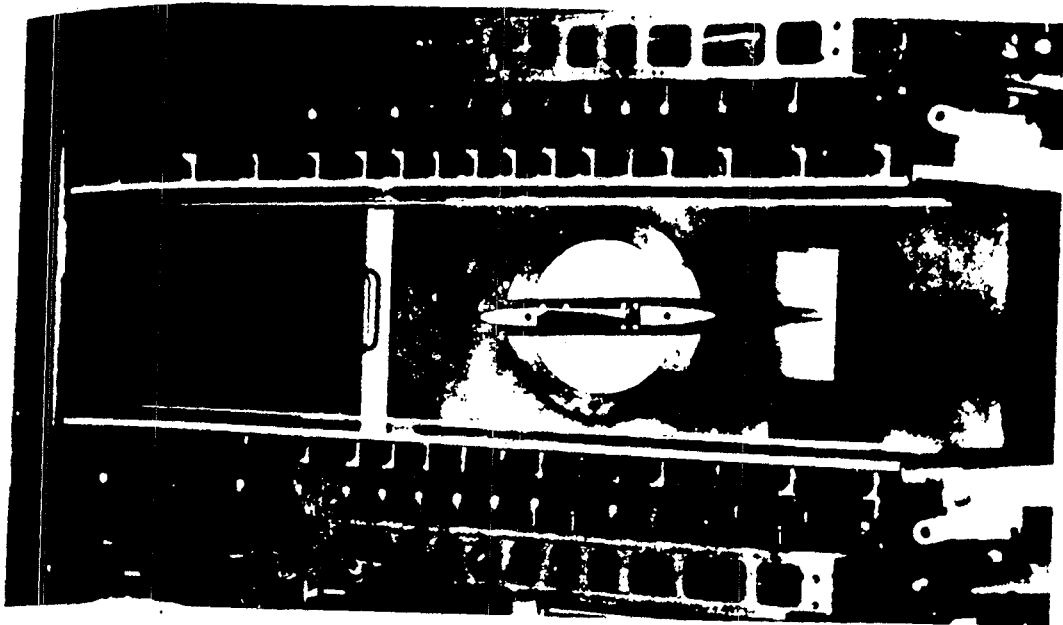
NON ADAPTE				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+1.5	+2	167		
0	0	162		165
-2	-2	159		

ADAPTE 3-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+1.5	+2	168		
0	0	163		166
-2	-2	160		

ADAPTE 2-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+2	---	169		
0	---	161		164
-2	---	158		

Affichee = Displayed

Presentation of mounting



WING MOUNTING

FIGURES 5 TO 13

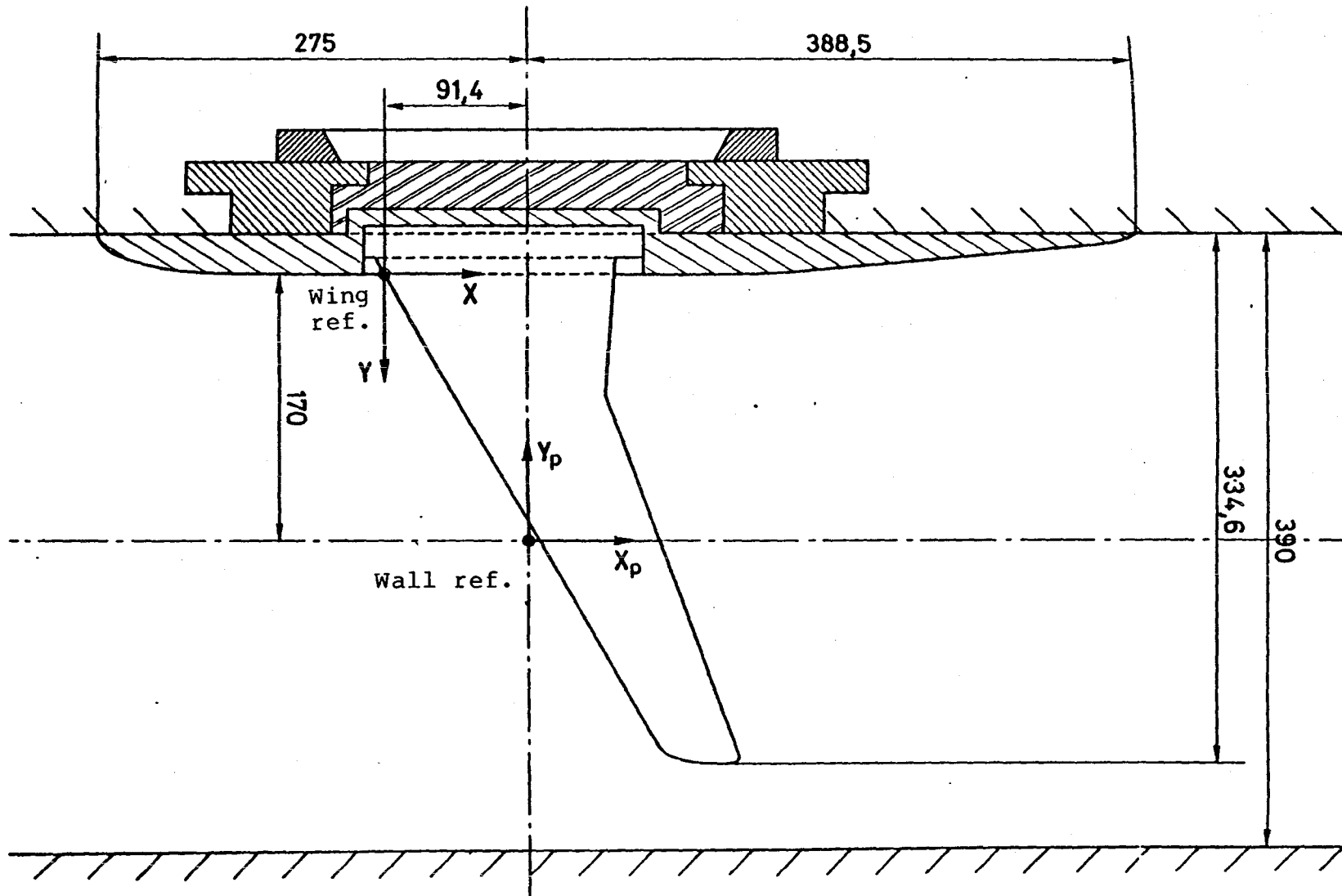


Diagram of wing mounting

Figure 6

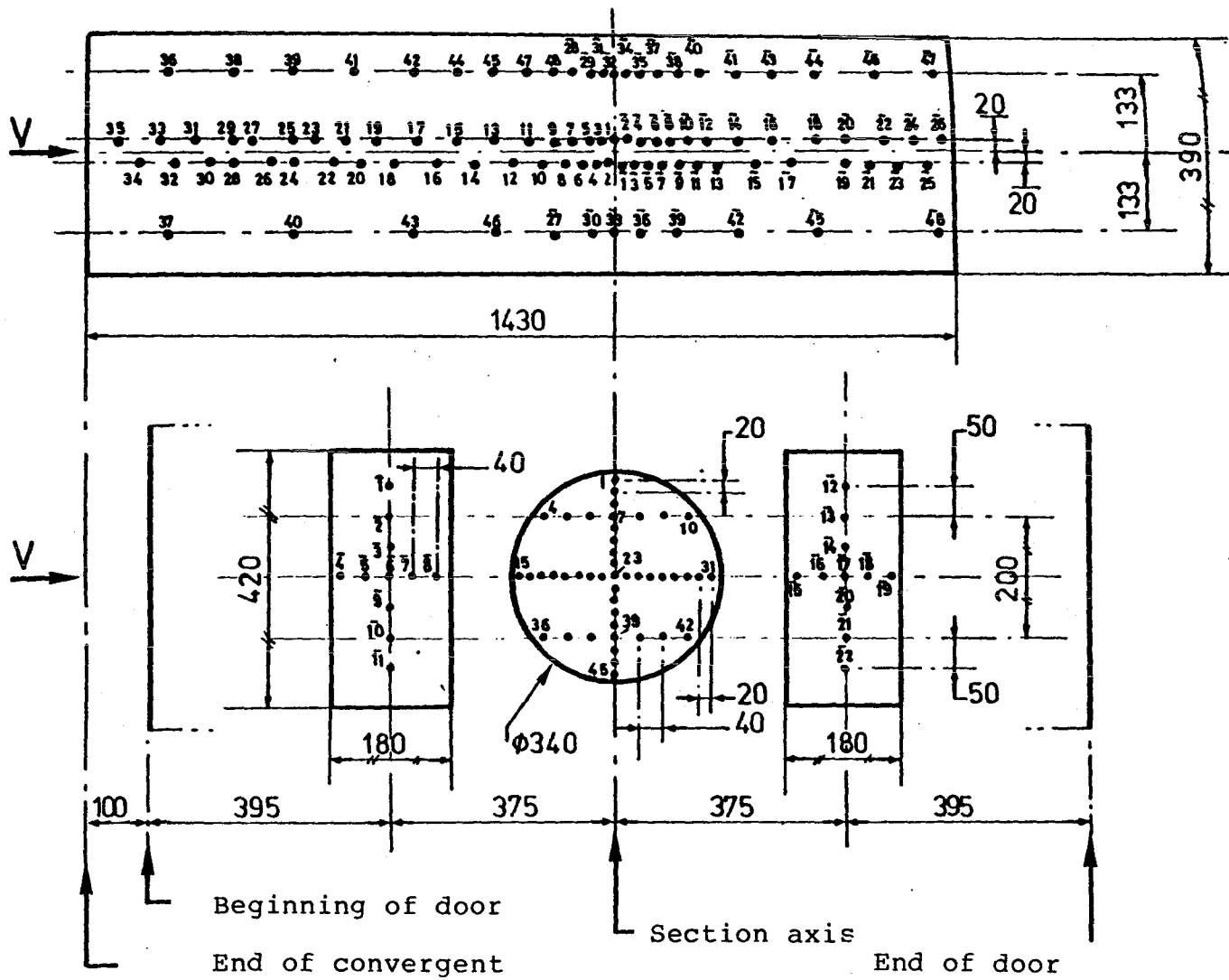


Diagram of wall pressure recorders

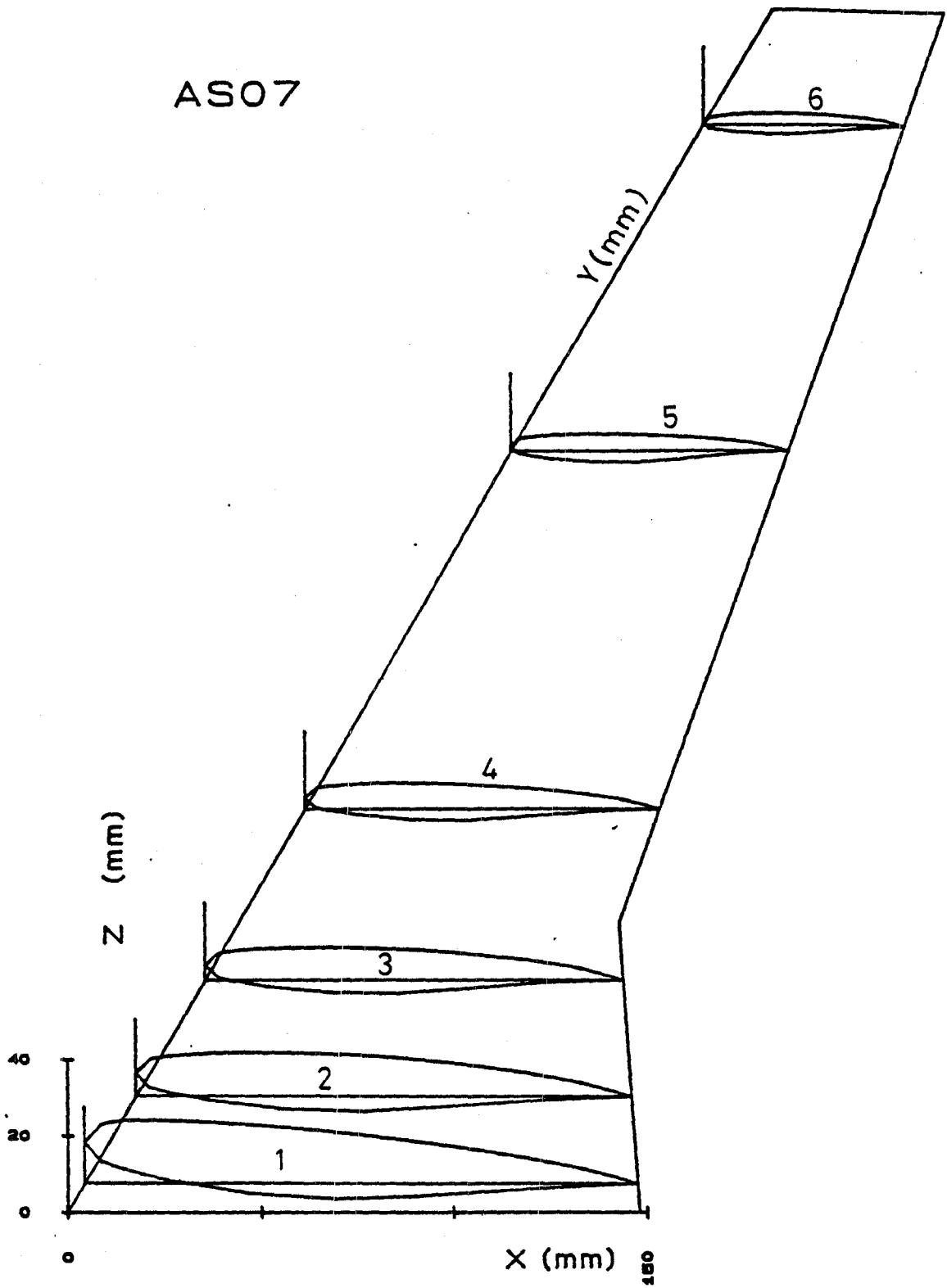
Figure 7

Figure 9

Pressure recorder specifications - lateral walls (mm)

upstream hole			central hole			downstream hole		
N	X	Z	N	X	Z	N	X	Z
1		+150	1		+160	1		+150
2	-375	+100	2	0	+140	2	+375	+100
3		+ 50	3		+120	3		+ 50
4	-455		4	-120		4	+295	
5	-410		5	- 80		5	+335	
6	-375	0	6	- 40		6	+375	0
7	-335		7	0	+100	7	+415	
8	-295		8	+ 40		8	+455	
9		- 50	9	+ 80		9		- 50
10	-375	-100	10	+120		10	+375	-100
11		-150	11		+ 80	11		-150
			12	0	+ 60			
			13		+ 40			
			14		+ 20			
			15	-160				
			16	-140				
			17	-120				
			18	-100				
			19	- 80				
			20	- 60				
			21	- 40				
			22	- 20				
			23	0	0			
			24	+ 20				
			25	+ 40				
			26	+ 60				
			27	+ 80				
			28	+100				
			29	+120				
			30	+140				
			31	+160				
			32		- 20			
			33	0	- 40			
			34		- 60			
			35		- 80			
			36	-120				
			37	- 80				
			38	- 40				
			39	0	-100			
			40	+ 40				
			41	+ 80				
			42	+120				
			43		-120			
			44	0	-140			
			45		-160			

Diagram of the wing



Specifications of the AS 07 wing

		A			
		Y	B.A. X	B.F. X	corde
B	Emplanture	0	0	148,112	148,112
C	rangee 1	7,56	4,46	147,62	143,16
	rangee 2	30,34	17,88	146,12	128,24
	rangee 3	60,40	35,6	144,15	108,55
	rupture	75,227	44,335	143,18	98,845
	rangee 4	104,301	61,47	153,61	92,14
	rangee 5	196,41	115,75	186,66	70,91
	rangee 6	279,87	164,94	216,60	51,66
D	Saumon	309,60	182,464	227,264	44,80

(mm)

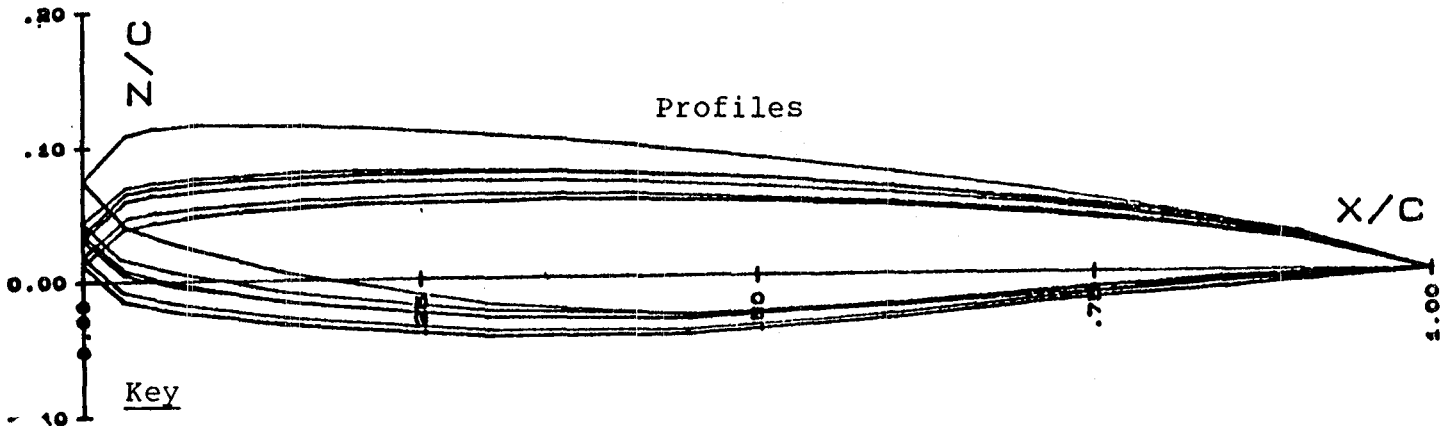
Key

- A - chord
- B - root
- C - row
- C - tip

Figure 12

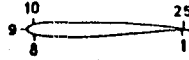
Position of pressure recorders for each section

A	B.A.	1 prise	0 %								
B	Extrados	16 prises	3	5	8	12	16	20	25	30 %	
			35	40	50	60	70	75	80	90 %	
C	Intrados	8 prises	3	7	15	30	45	60	75	85 %	



- A - B.A. 1 recorder
- B - Outer section 16 recorders
- C - Inner section 8 recorders

Specifications of pressure recorders on "Airbus" AS07 wing



A Aile Interne						B Aile Externe						
rangee 1		rangee 2		rangee 3		rangee 4		rangee 5		rangee 6		
Y = 7.560mm		Y = 30.340mm		Y = 60.400mm		Y = 104.301mm		Y = 198.410mm		Y = 279.870mm		
B.A. = 4.295mm		B.A. = 17.715mm		B.A. = 35.498mm		B.A. = 61.392mm		B.A. = 115.701mm		B.A. = 164.943mm		
B.F. = 147.620mm		B.F. = 146.120mm		B.F. = 144.150mm		B.F. = 153.610mm		B.F. = 166.660mm		B.F. = 216.600mm		
Corde 143.160mm		Corde 128.240mm		Corde 108.550mm		Corde 92.140mm		Corde 70.910mm		Corde 51.660mm		
X (mm)	Z (mm)	X (mm)	Z (mm)	X (mm)	Z (mm)	X (mm)	Z (mm)	X (mm)	Z (mm)	X (mm)	Z (mm)	
11	125.979	-1.060	126.753	-0.812	127.744	-0.477	139.796	-0.427	176.014	-0.529	208.802	-0.611
21	111.652	-2.030	113.946	-1.603	116.860	-1.104	130.546	-1.059	168.883	-1.062	203.655	-0.940
31	90.225	-3.393	94.643	-3.043	100.606	-2.349	116.608	-2.047	158.182	-2.085	195.877	-1.686
41	68.703	-4.100	75.476	-4.026	84.444	-3.416	102.910	-2.941	147.676	-2.836	188.110	-2.244
51	47.066	-2.670	56.069	-3.411	68.084	-3.155	89.086	-2.683	137.029	-2.739	180.378	-2.234
61	25.741	0.833	36.785	-1.156	51.753	-1.680	75.279	-1.404	126.444	-1.933	172.775	-1.685
71	14.624	3.784	26.560	0.924	43.091	-1.189	67.809	-0.344	120.661	-1.160	168.532	-1.158
81	8.751	5.783	21.249	2.395	38.873	0.869	64.174	0.458	117.768	-0.531	166.487	-0.742
91	4.295	10.800	17.715	6.327	35.498	3.823	61.392	2.909	115.701	1.302	164.943	0.631
101	8.723	15.493	21.770	9.986	38.940	7.078	64.267	5.467	117.973	3.323	166.547	2.025
111	11.585	16.199	24.358	10.487	41.105	7.486	66.108	5.843	119.417	3.598	167.634	2.203
121	15.846	16.647	28.129	10.923	44.283	7.849	68.897	6.110	121.501	3.835	169.065	2.442
131	21.618	16.604	33.252	11.253	48.640	8.184	72.644	6.408	124.422	4.057	171.278	2.676
141	27.277	16.489	38.412	11.529	52.991	8.315	76.313	6.598	127.290	4.257	173.375	2.808
151	32.911	16.259	43.567	11.634	57.393	8.490	80.039	6.745	129.993	4.320	175.430	2.922
161	40.345	15.832	50.130	11.621	62.771	8.539	84.700	6.784	133.473	4.440	177.931	2.954
171	47.378	15.325	56.415	11.552	68.203	8.599	89.220	6.730	137.156	4.498	180.642	2.974
181	54.600	14.779	62.367	11.373	73.628	8.559	93.797	6.674	140.619	4.442	183.036	3.024
191	61.817	14.109	69.275	11.123	79.051	8.330	98.353	6.557	144.214	4.438	185.851	2.985
201	76.080	12.593	81.970	10.477	89.905	7.886	107.621	6.118	151.250	4.116	190.836	2.862
211	90.393	10.871	94.843	9.268	100.707	7.162	116.809	5.564	158.243	3.824	196.000	2.648
221	104.729	8.981	107.703	7.823	111.669	6.098	126.168	4.814	165.501	3.331	201.100	2.312
231	111.839	7.869	114.070	6.961	117.001	5.560	130.641	4.311	168.927	3.009	203.841	2.056
241	119.020	6.701	120.482	5.980	122.467	4.846	135.204	3.747	172.367	2.629	206.349	1.850
251	133.269	3.920	133.311	3.626	133.304	3.071	144.355	2.427	179.552	1.684	211.614	1.181

Key

- A - Internal wing
- B - External wing
- C - Row
- D - B.A.
- E - B.F.
- F - Chord

CONTROL TESTS

Wall incidence and rotation: Figures 14 to 16
Convergence of iterations: Figures 17 to 20
Non/2-D/3-D comparison: Figures 21 to 23

Key to figures 14, 15, and 16

- A - Non-adapted
- B - Wall shapes
- C - Row
- D - Upper wall
- E - Lower wall
- F - Central rows of pressure recorders

$M=0,6$
 $\alpha=+2^\circ$

A non adapté

○ — AD120
 ♦ — AD122

Rotation: First control

C Rangée ⑤

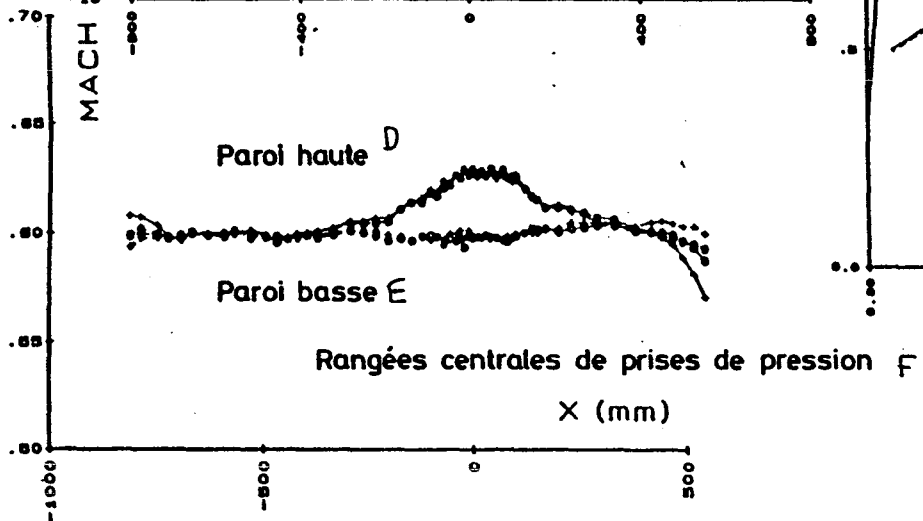
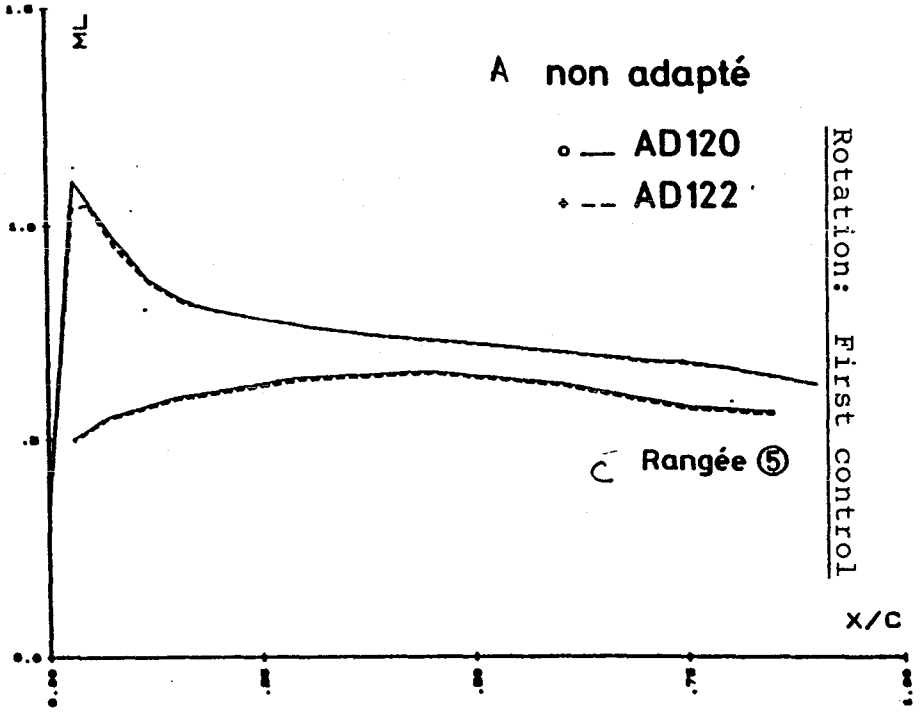
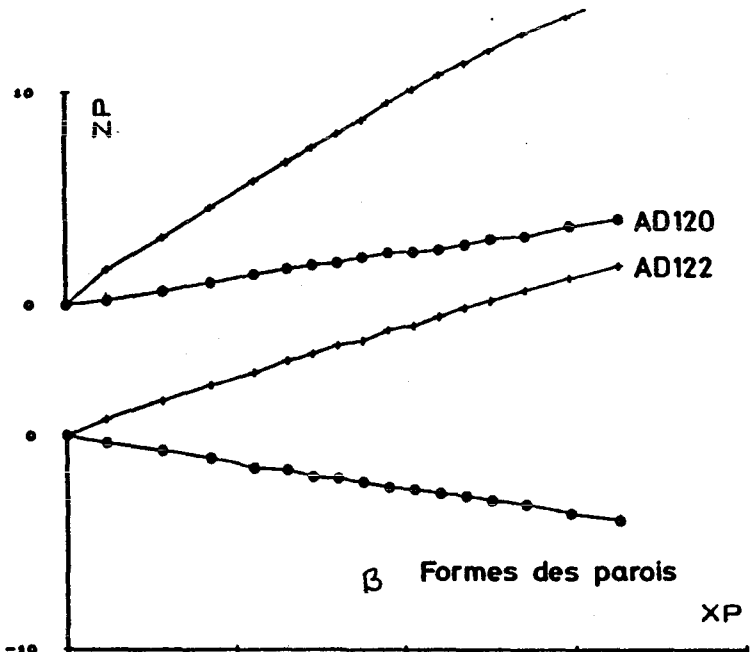


Figure 14

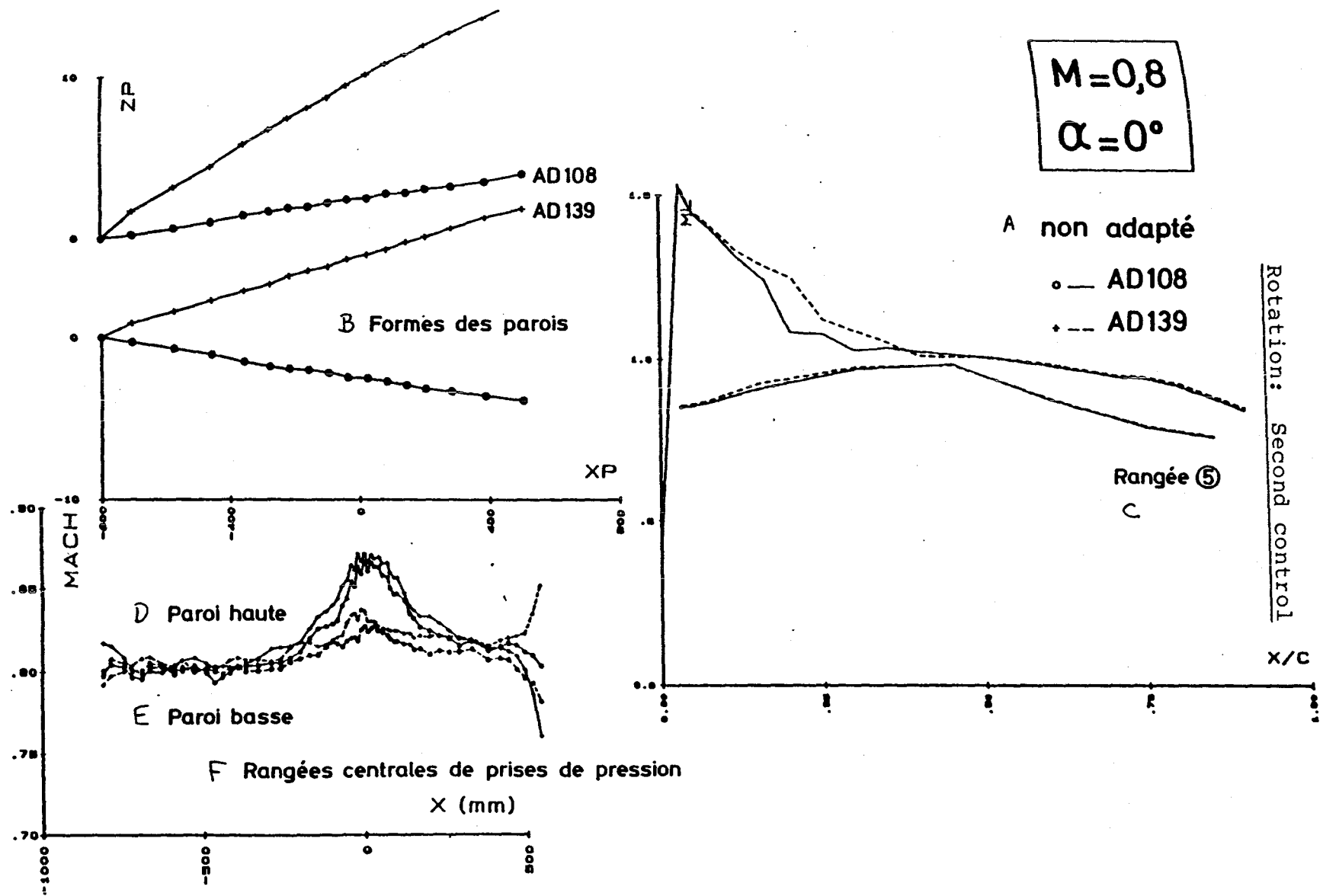


Figure 15

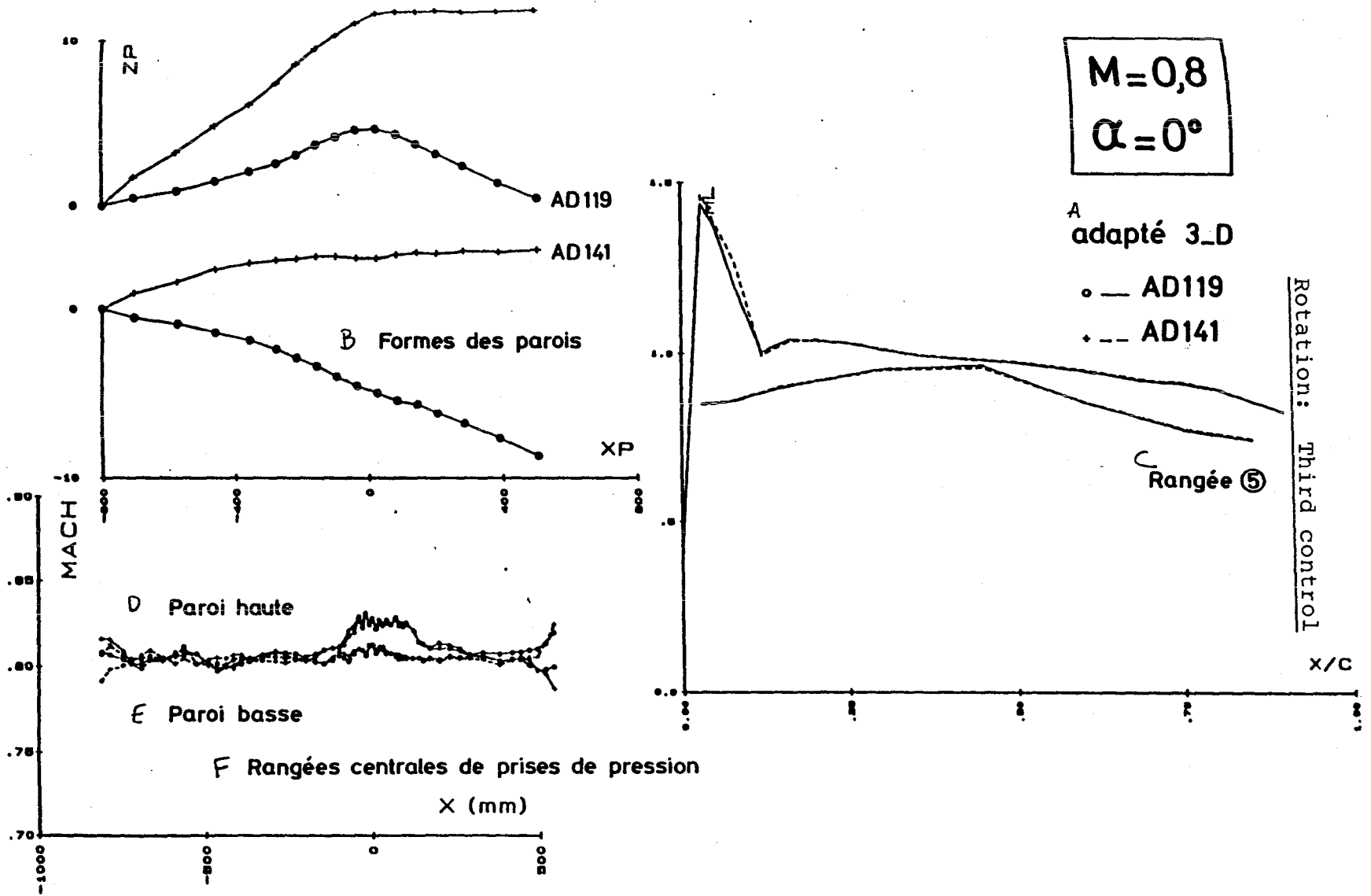
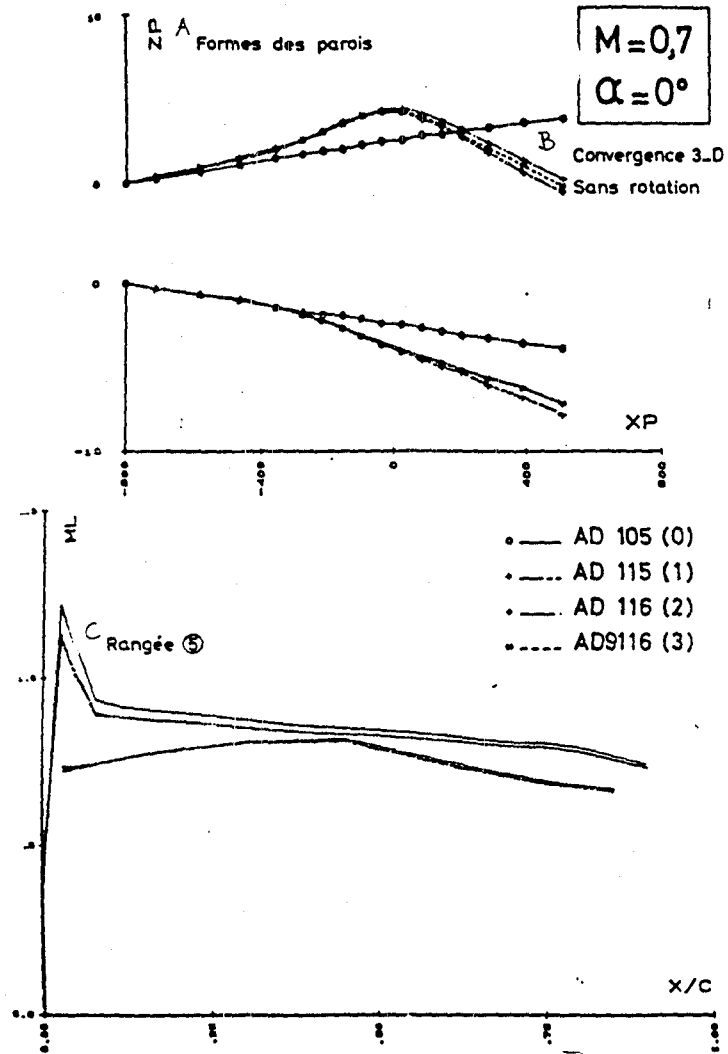


Figure 16

First case

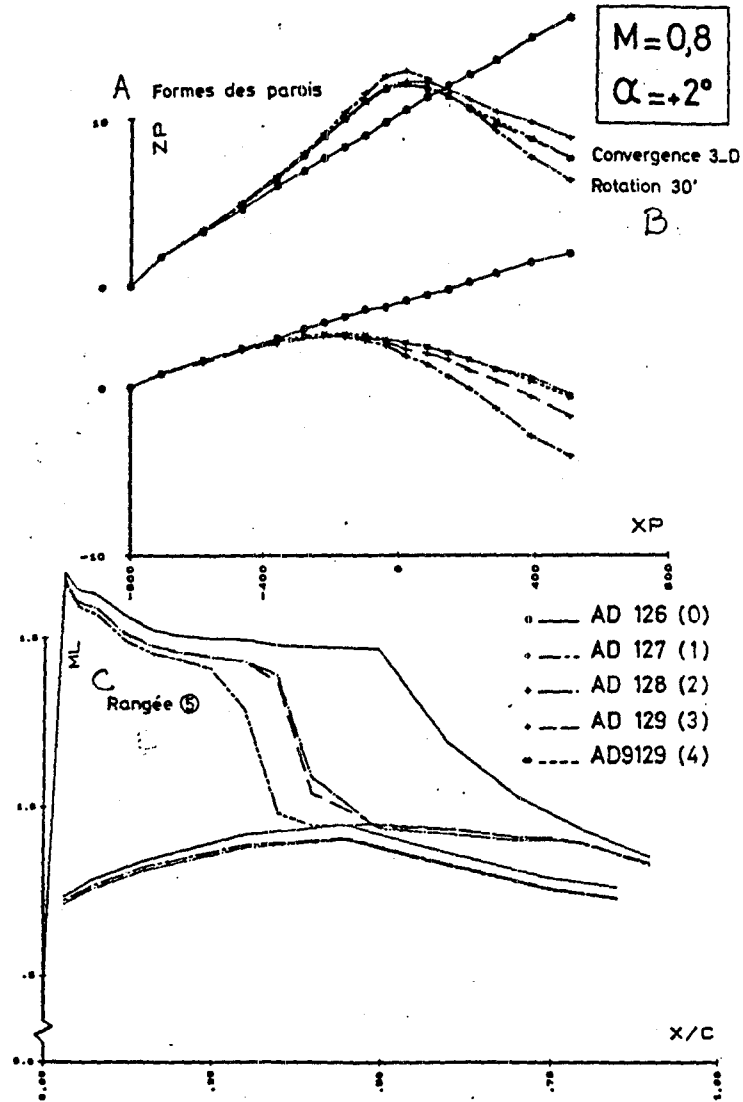


Key

- A - Wall shapes
- B - 3-D convergence, no rotation
- C - Row

Figure 18

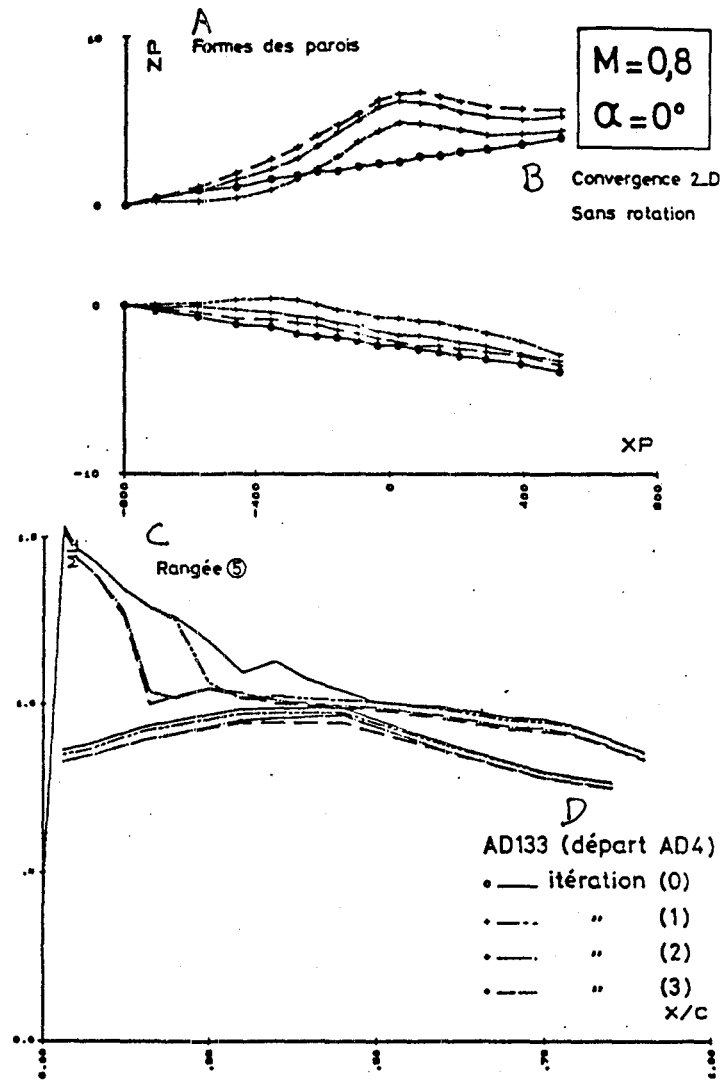
Second case



Key

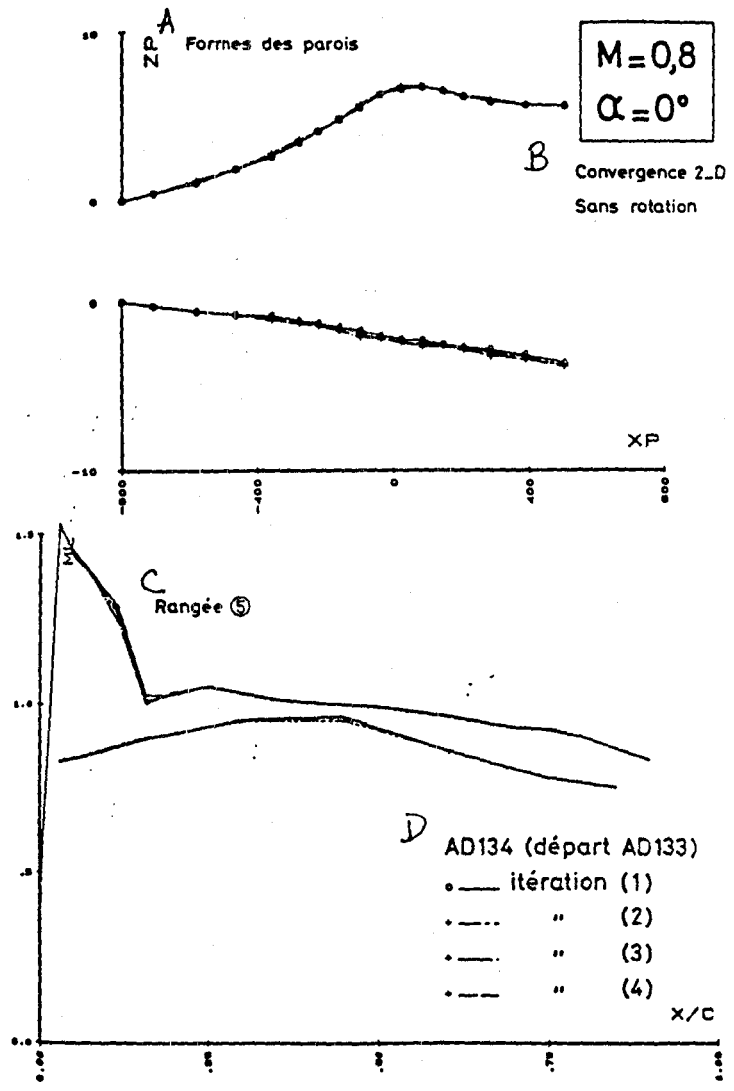
- A - Wall shapes
- B - Row

Figure 19



Key

- A - Wall shapes
- B - 2-D convergence, no rotation
- C - Row
- D - Beginning



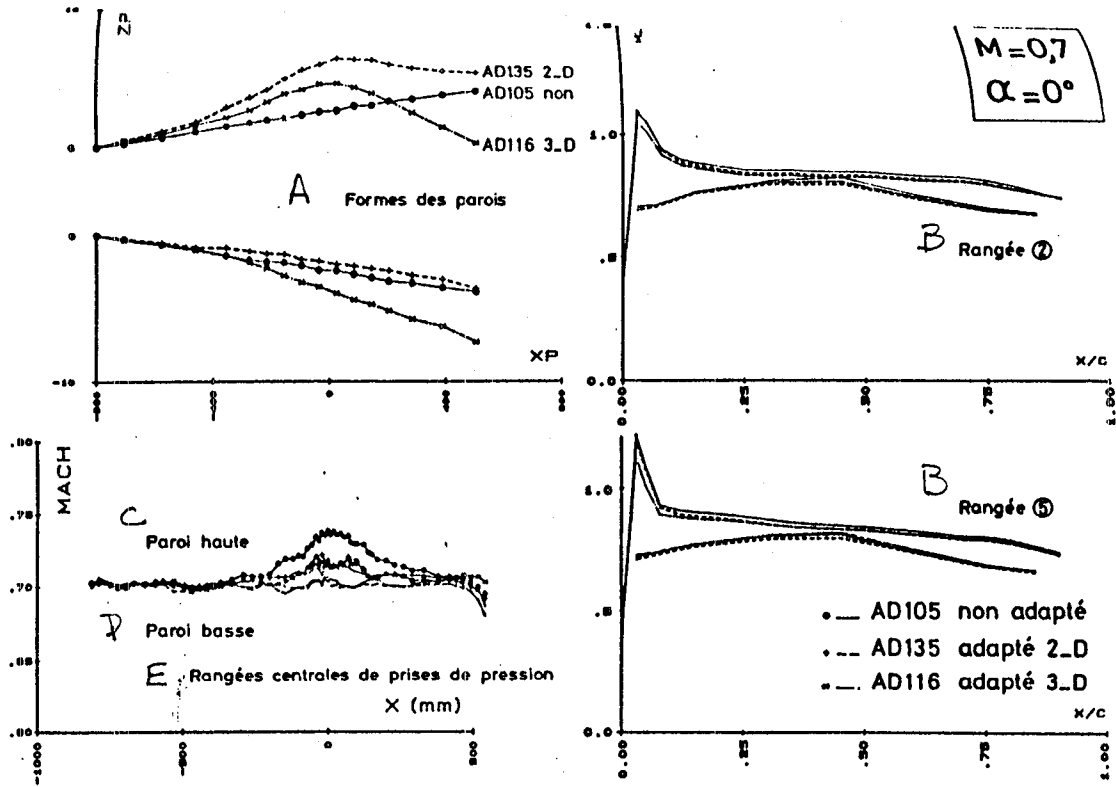
Key

- A - Wall shapes
- B - 2-D convergence, no rotation
- C - Row
- D - Beginning

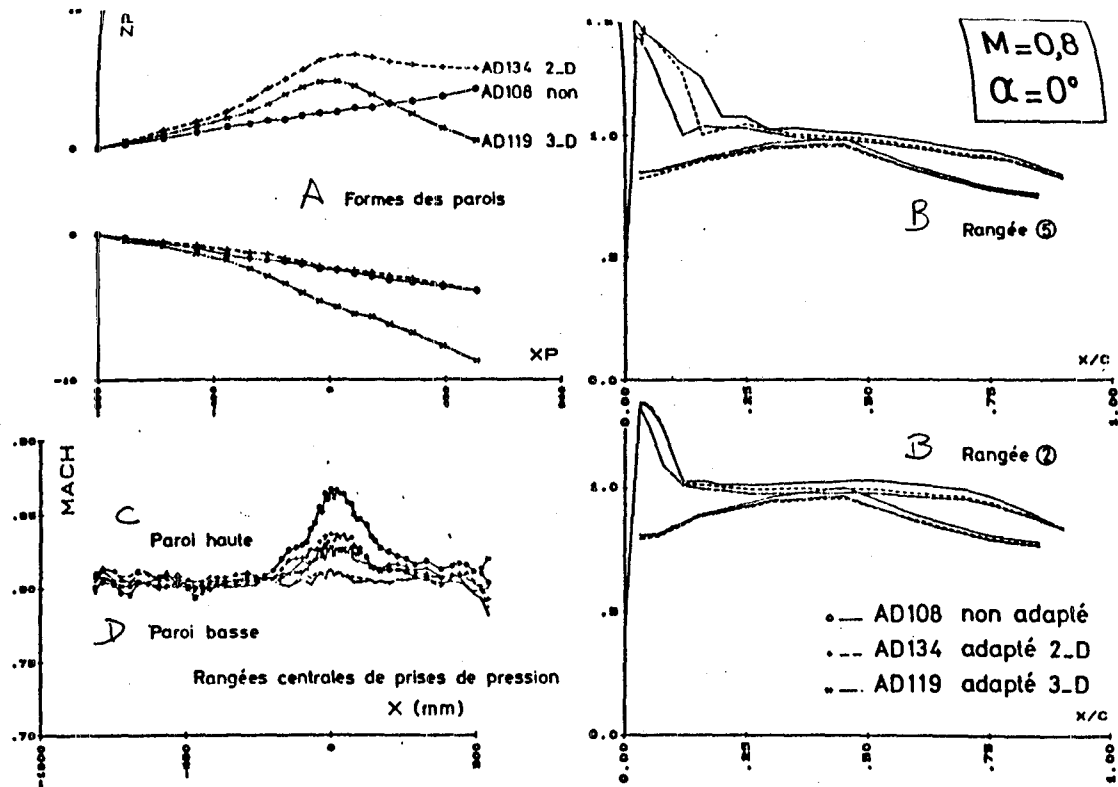
Key to figures 21 and 22

- A - Wall shapes
- B - Row
- C - Upper wall
- D - Lower wall
- E - Central rows of pressure recorders

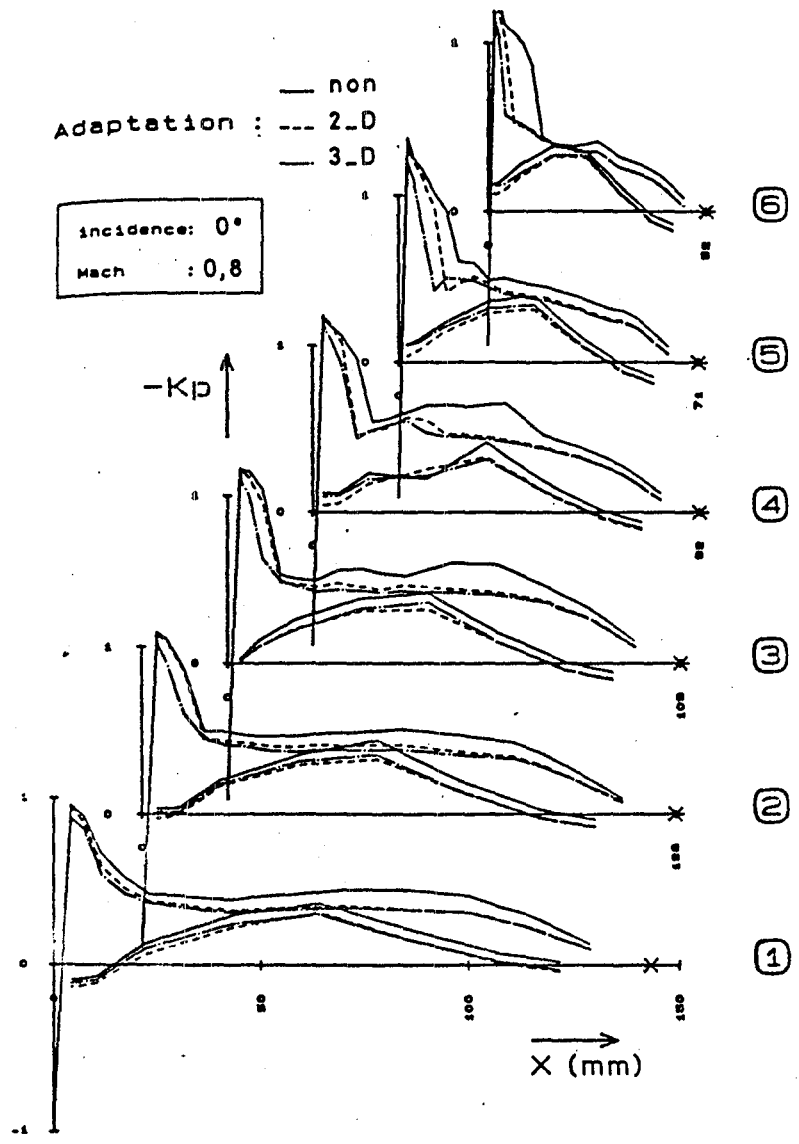
Non/2-D/3-D comparison



Non/2-D/3-D comparison



Non/2-D/3-D comparison

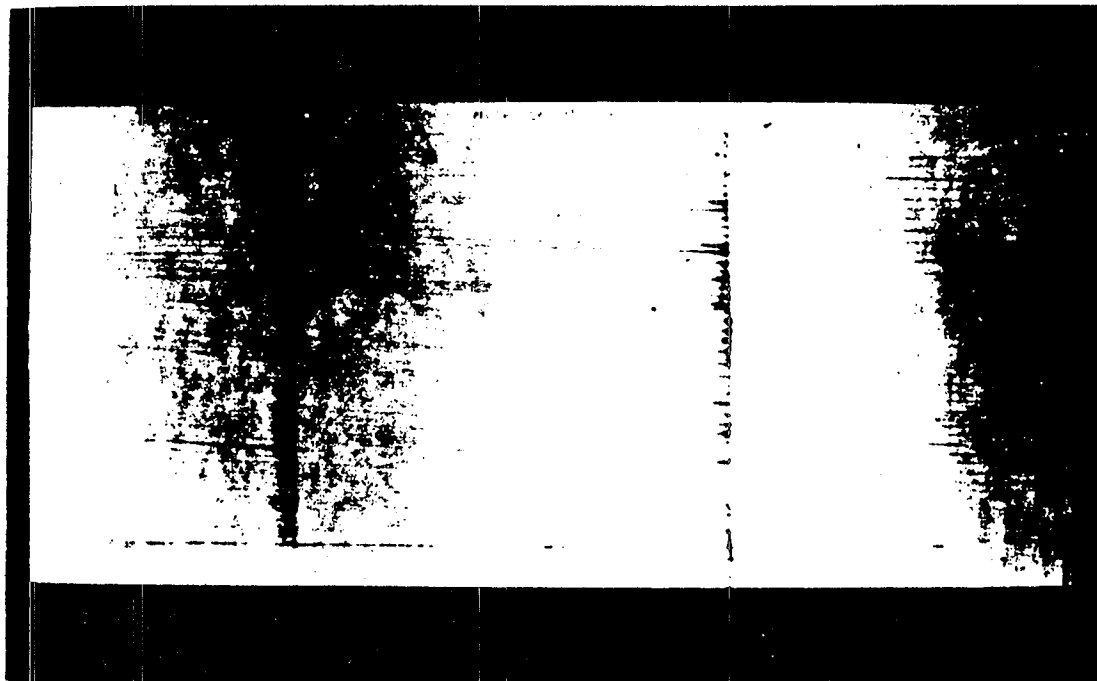
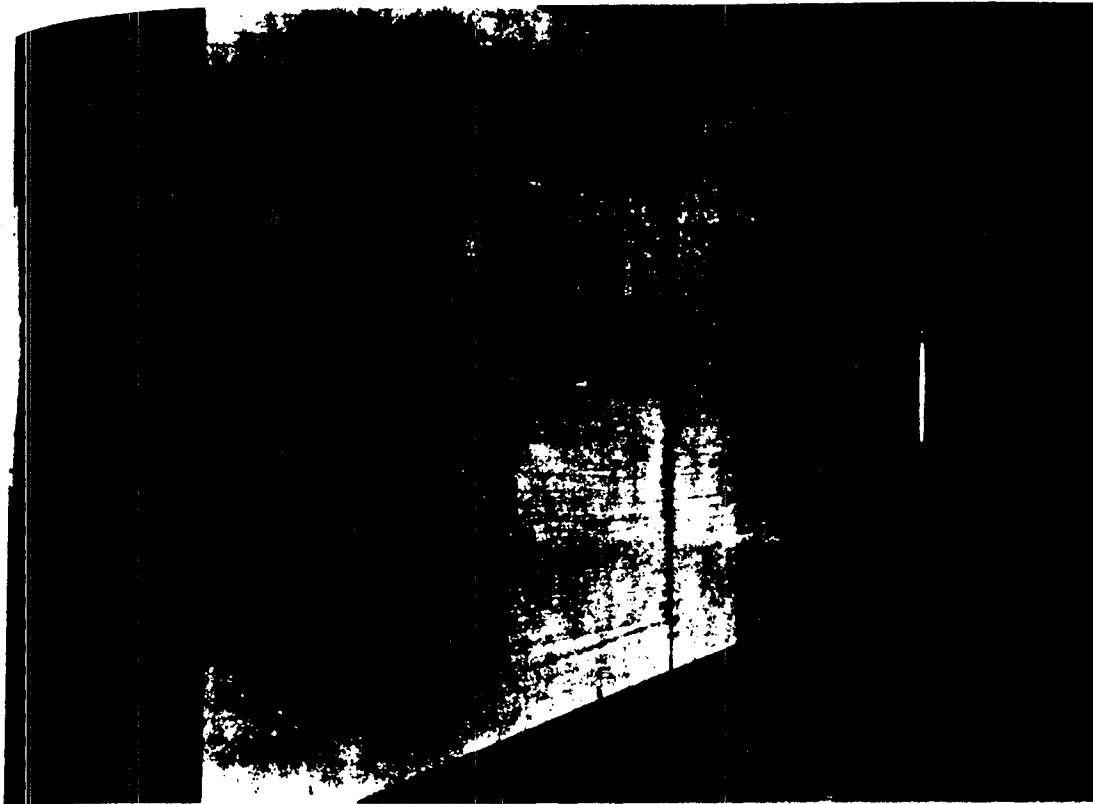


VISUALIZATION OF CURRENT LINES

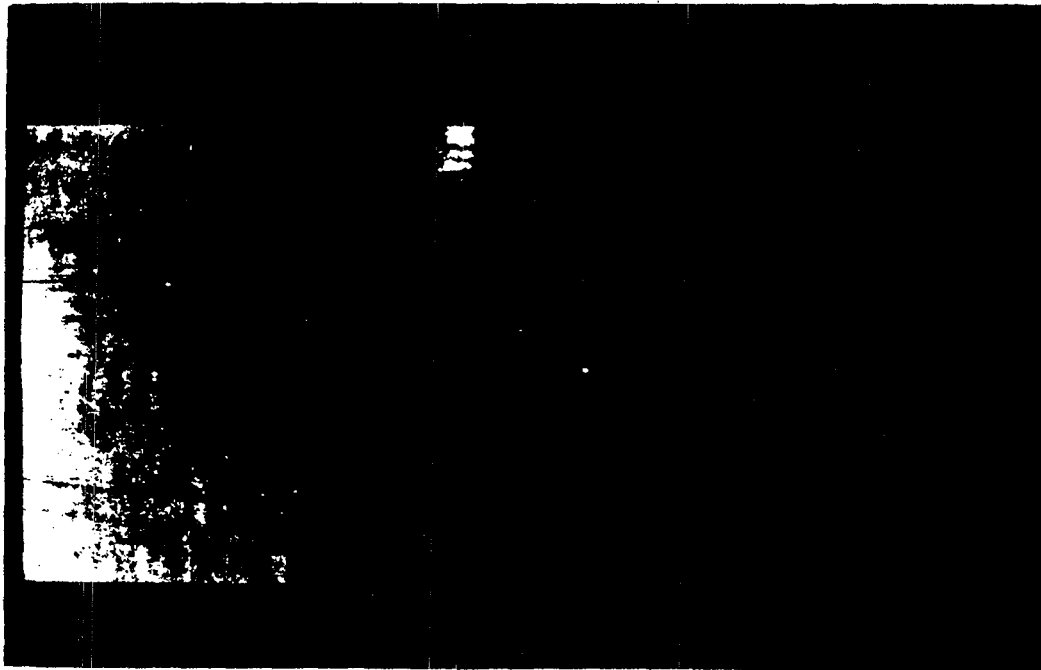
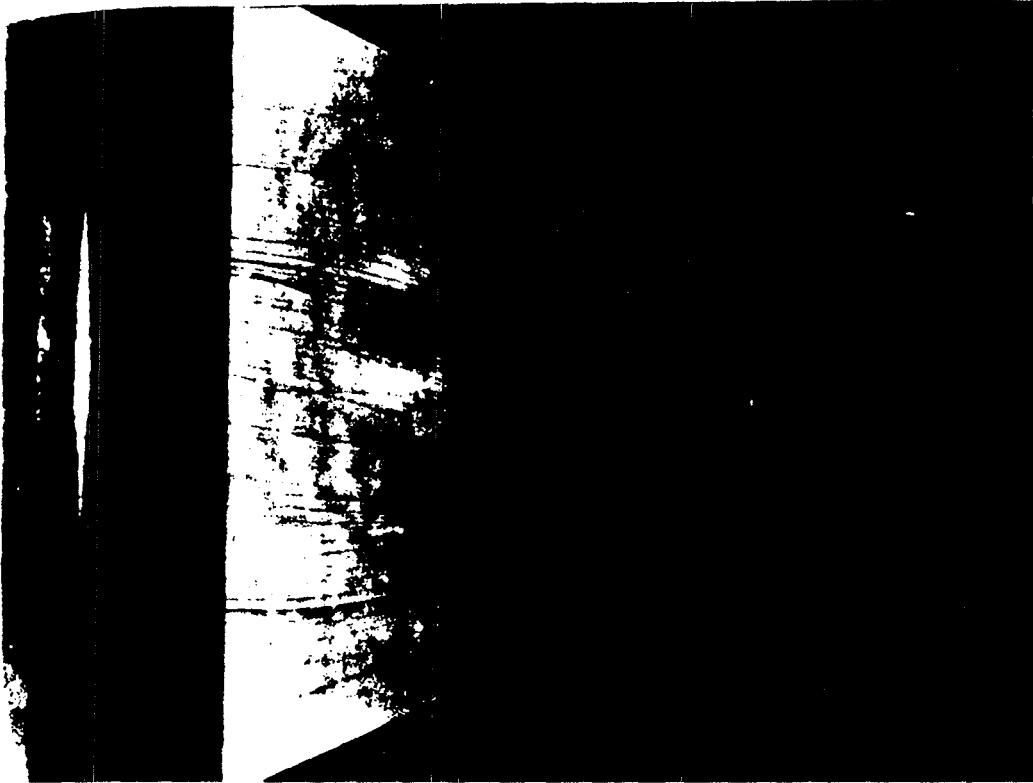
ON THE LEFT LATERAL WALL

$M_o = 0.6$	$\alpha = +2^\circ$	Non-adapted	Figure 24
$M_o = 0.6$	$\alpha = +2^\circ$	2-D	Figure 25
$M_o = 0.6$	$\alpha = -2^\circ$	Non-adapted	Figure 26

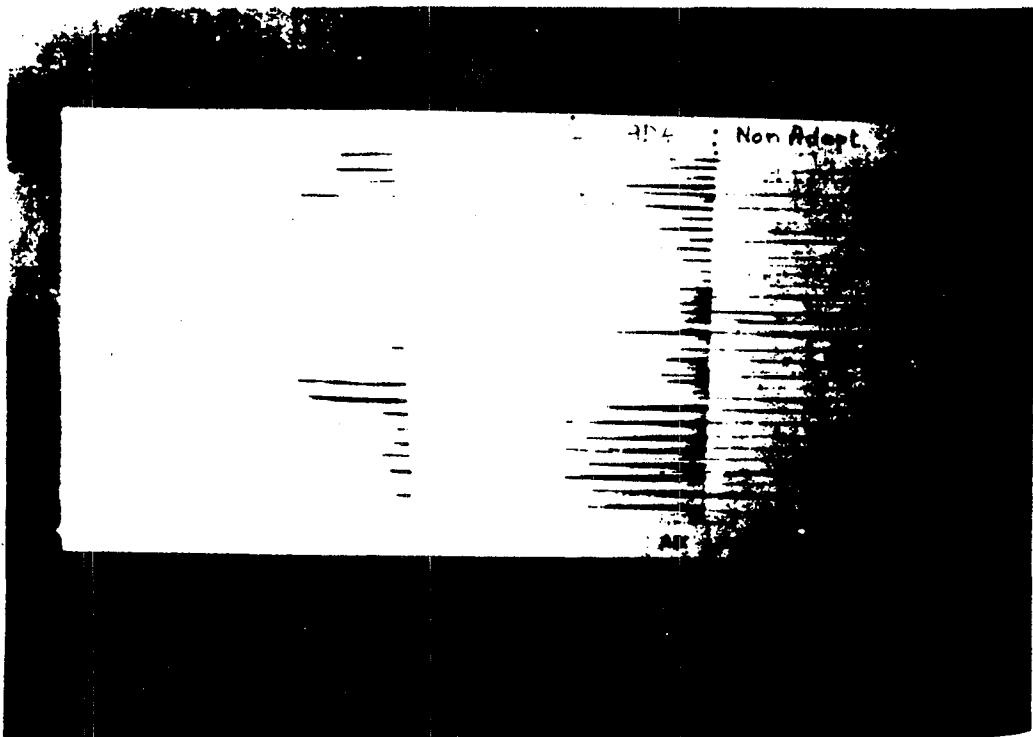
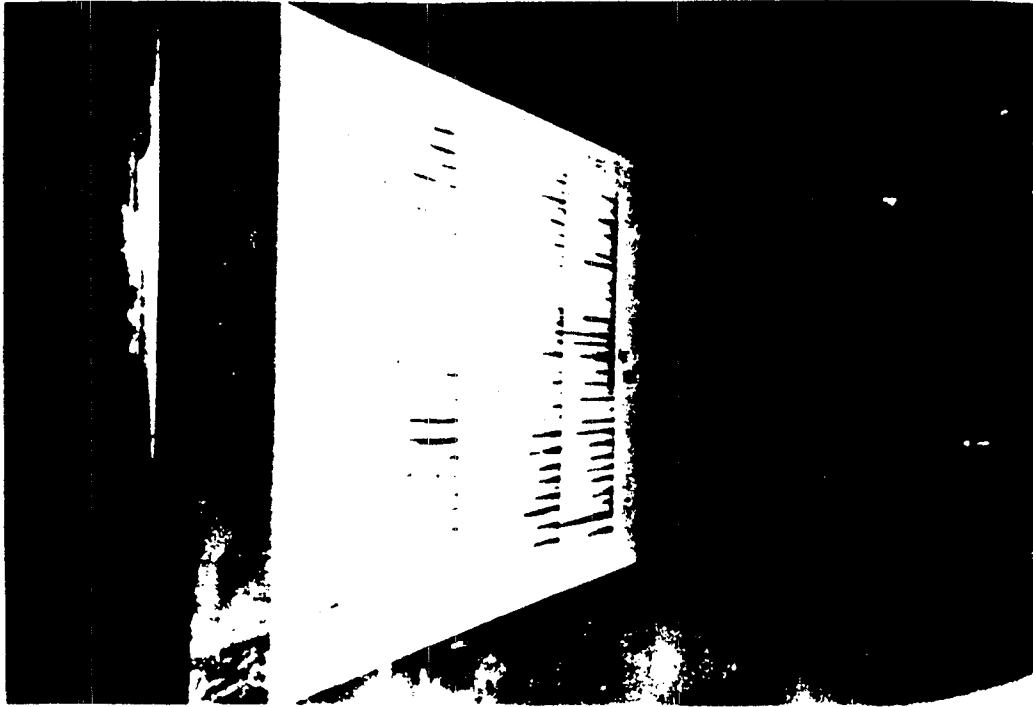
Left lateral door visualization $\alpha = +2^\circ$ $M = 0.6$ non-adapted



[illegible]



Left lateral door visualization $\alpha = -2^\circ$ $M = 0.6$ non-adapted



Use of four base cases

		M=0,6	0,8	NON ADAPTE
+2		147 (*)		(*) ranges 1-4 (**) ranges 2-5 (***) ranges 3-6
		122 (**)		
		167 (***)		
0		150 (*)	153 (*)	
		107 (**)	108 (**)	
		162 (***)	165 (***)	
-2		156 (*)		
		142 (**)		
		159 (***)		

		M=0,6	0,8	ADAPTE 2-D
+2		146 (*)		
		145 (**)		
		132 (***)		
0		149 (*)	152 (*)	
		136 (**)	134 (**)	
		161 (***)	164 (***)	
-2		155 (*)		
		144 (**)		
		158 (***)		

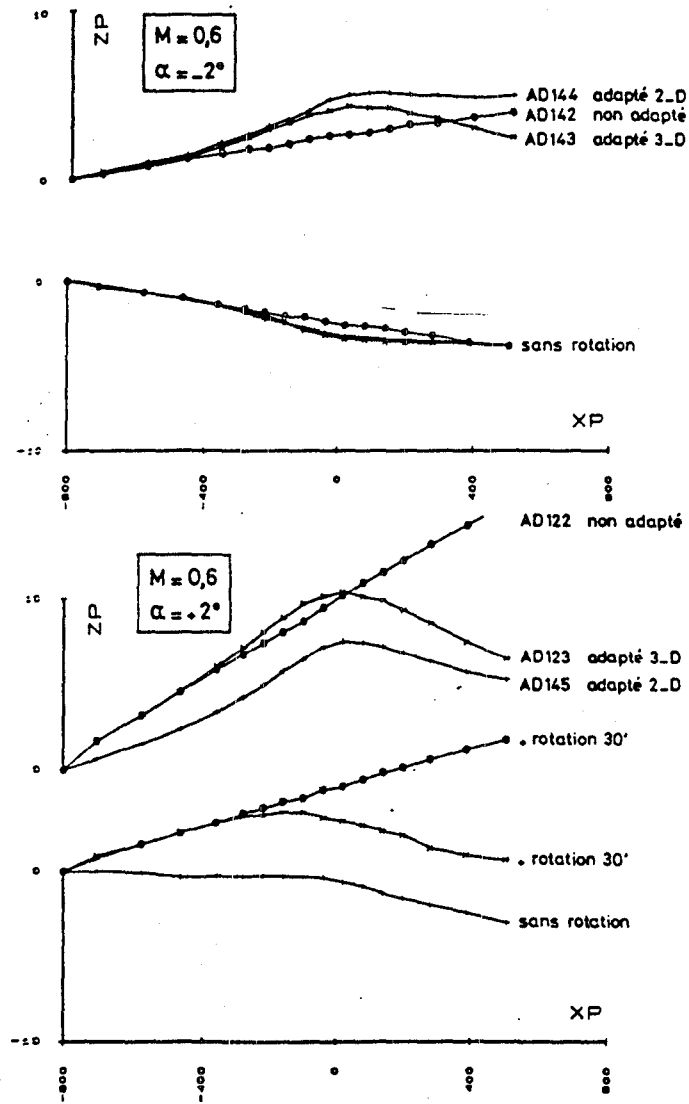
		M=0,6	0,8	ADAPTE 3-D
+2		148 (*)		
		123 (**)		
		182 (***)		
0		151 (*)	154 (*)	
		117 (**)	119 (**)	
		163 (***)	166 (***)	
-2		157 (*)		
		143 (**)		
		150 (***)		

Shape of walls
 Mach on adaptable walls
 Mach on lateral wall
 Kp distribution
 Lift coefficient

Figures 27-28
 Figures 29-32
 Figures 33-36
 Figures 37-44
 Figures 45-50

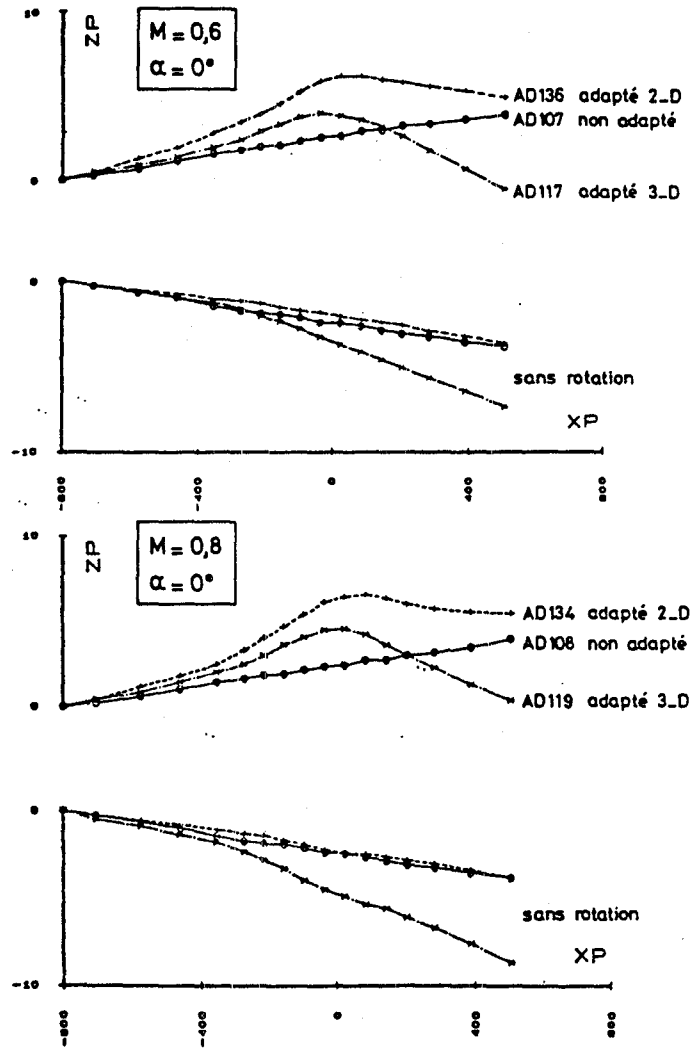
Figure 27

Use of the four base cases - Wall shape



"Sans rotation" = No rotation

Use of the four base cases - Wall shape



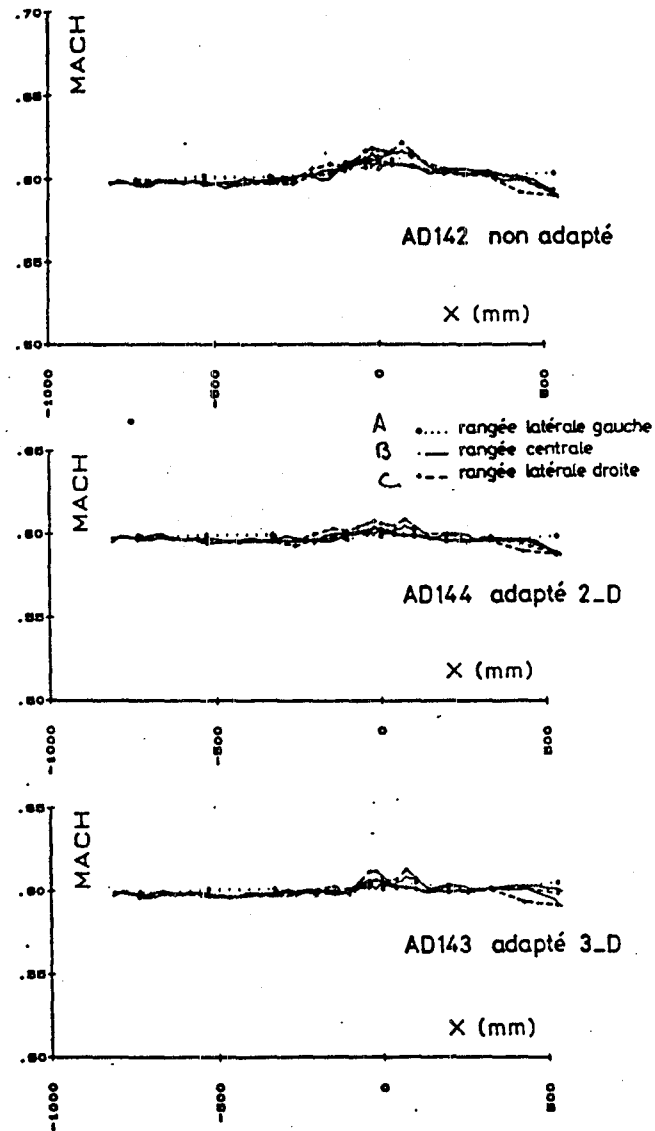
"Sans rotation" = No rotation

Key to Figures 29, 30, 31, and 32:

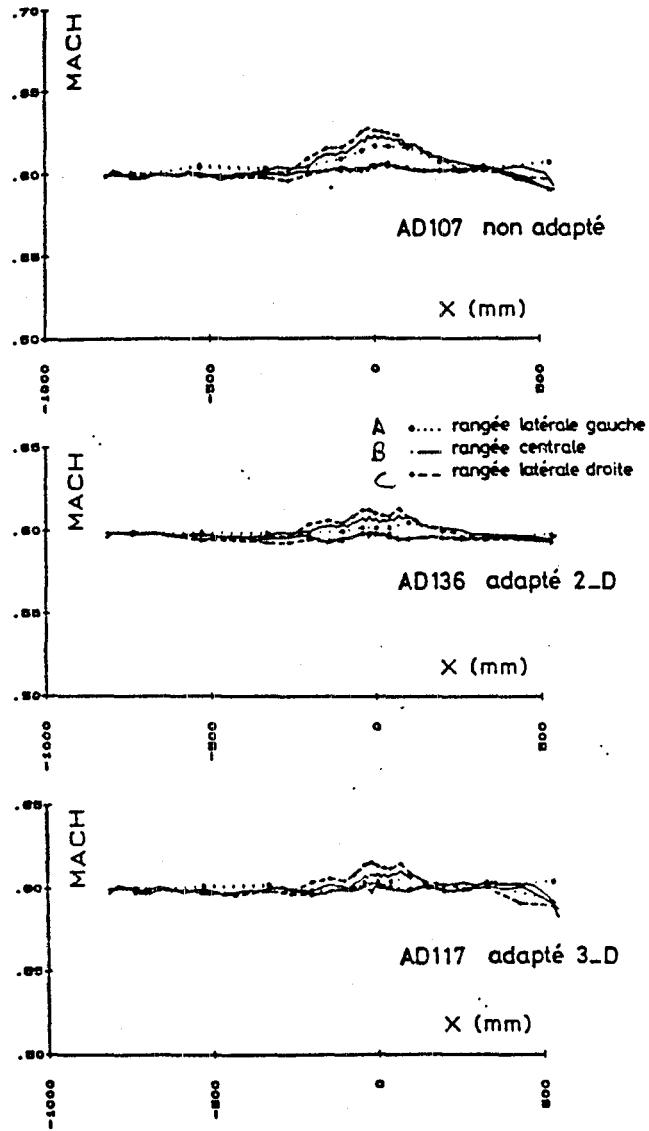
- A - Left lateral row
- B - Central row
- C - Right lateral row

Figure 29

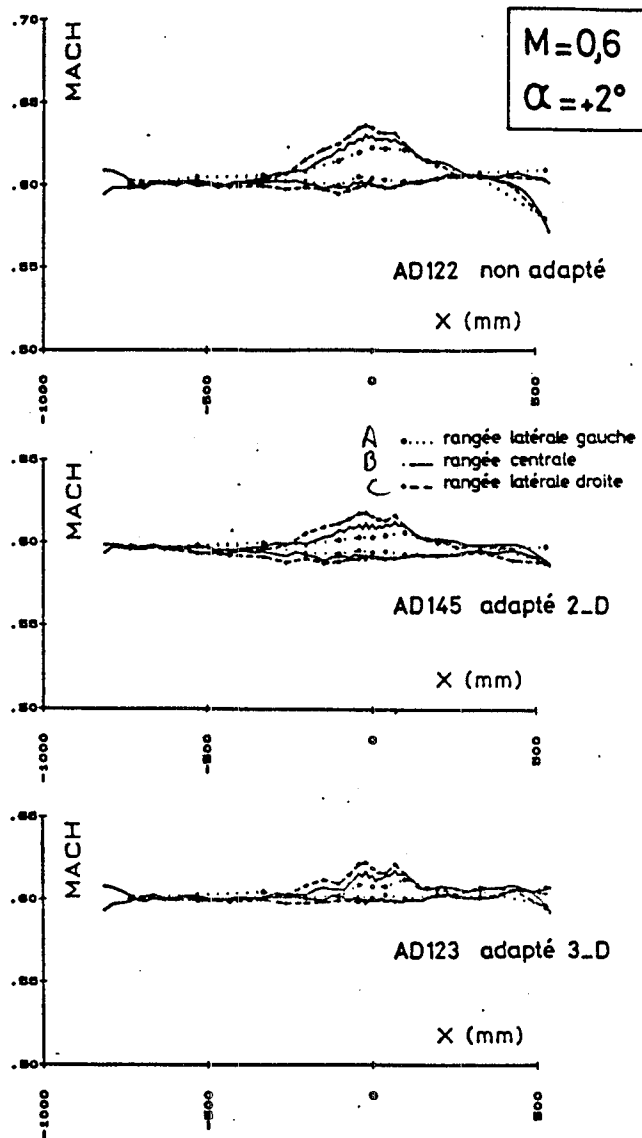
Use of the four base cases - Mach of adaptable walls



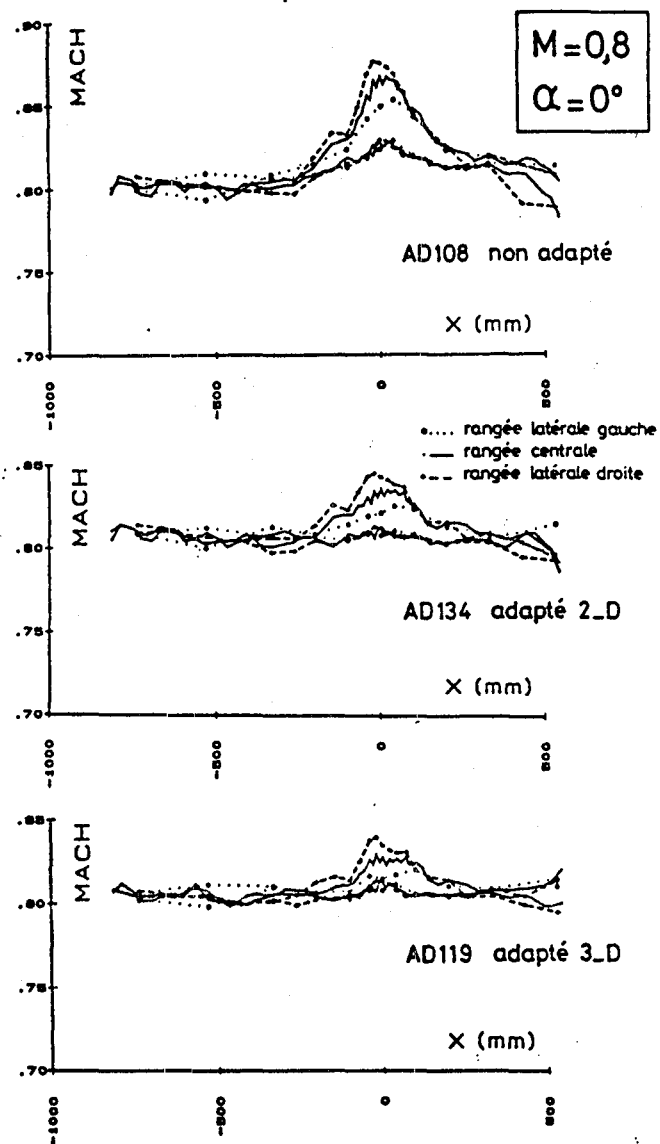
Use of the four base cases - Mach of adaptable walls



Use of the four base cases - Mach of adaptable walls



Use of the four base cases - Mach of adaptable walls



Key to Figures 33, 34, 35, and 36:

A - Vertical rows

° upstream
— middle
· downstream

B - Horizontal rows

° upper
— middle
· lower

Figure 33

Use of the four base cases - Mach of lateral walls

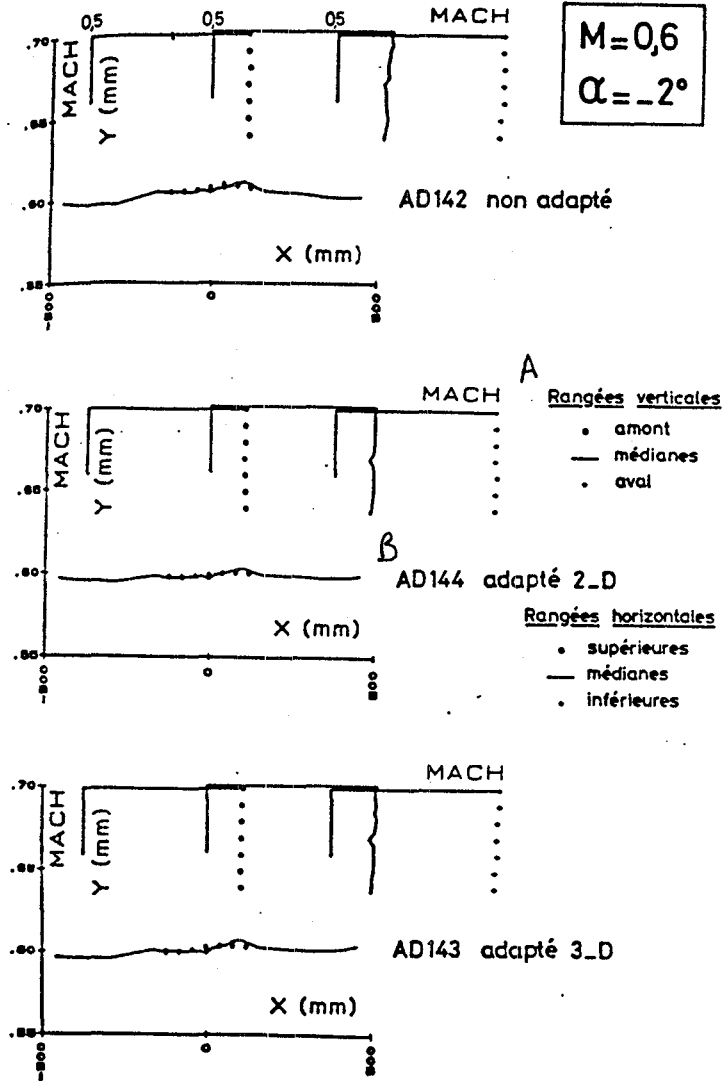


Figure 34

Use of the four base cases - Mach of lateral walls

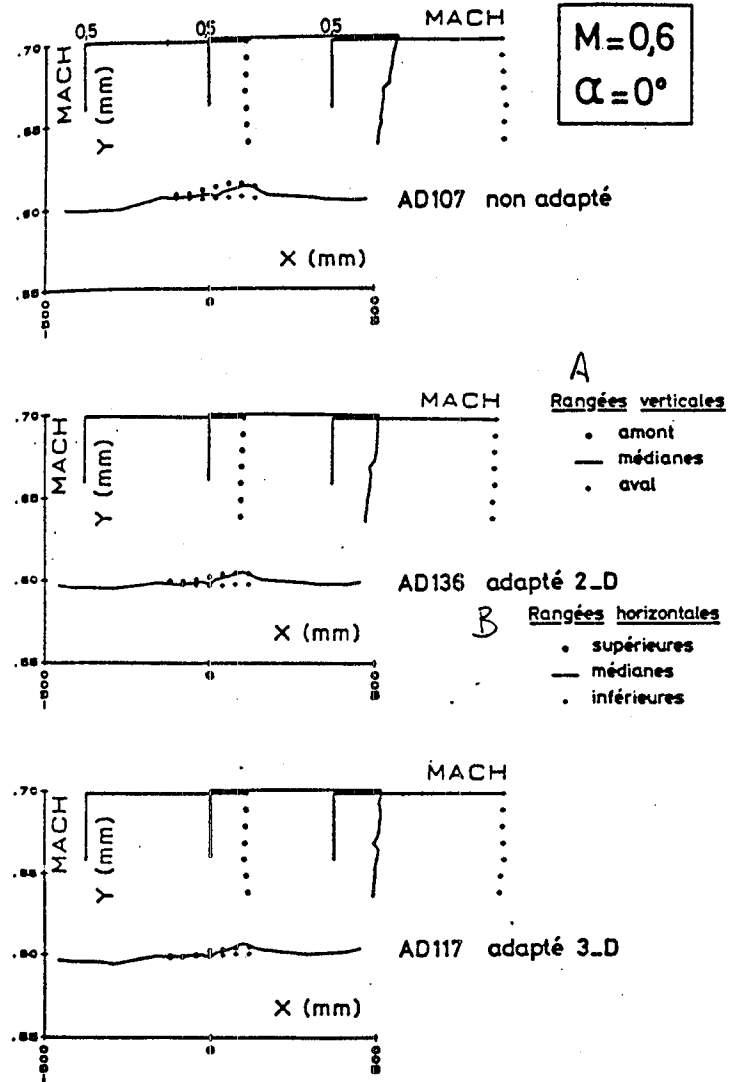


Figure 35

Use of the four base cases - Mach of lateral walls

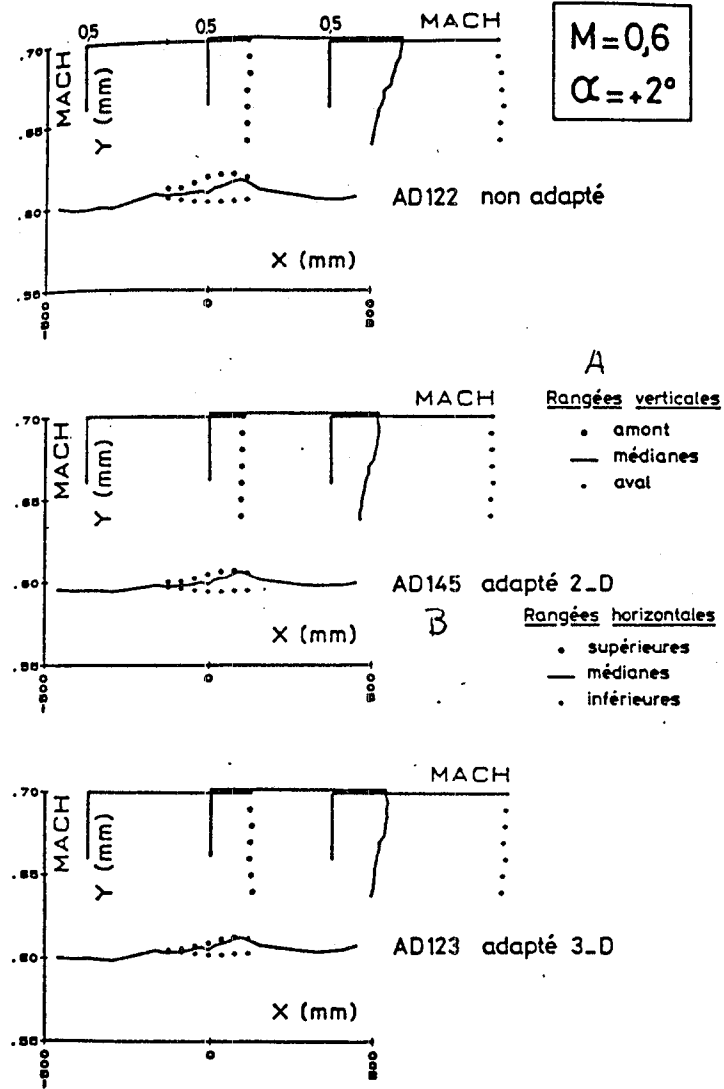


Figure 36

Use of the four base cases - Mach of lateral walls

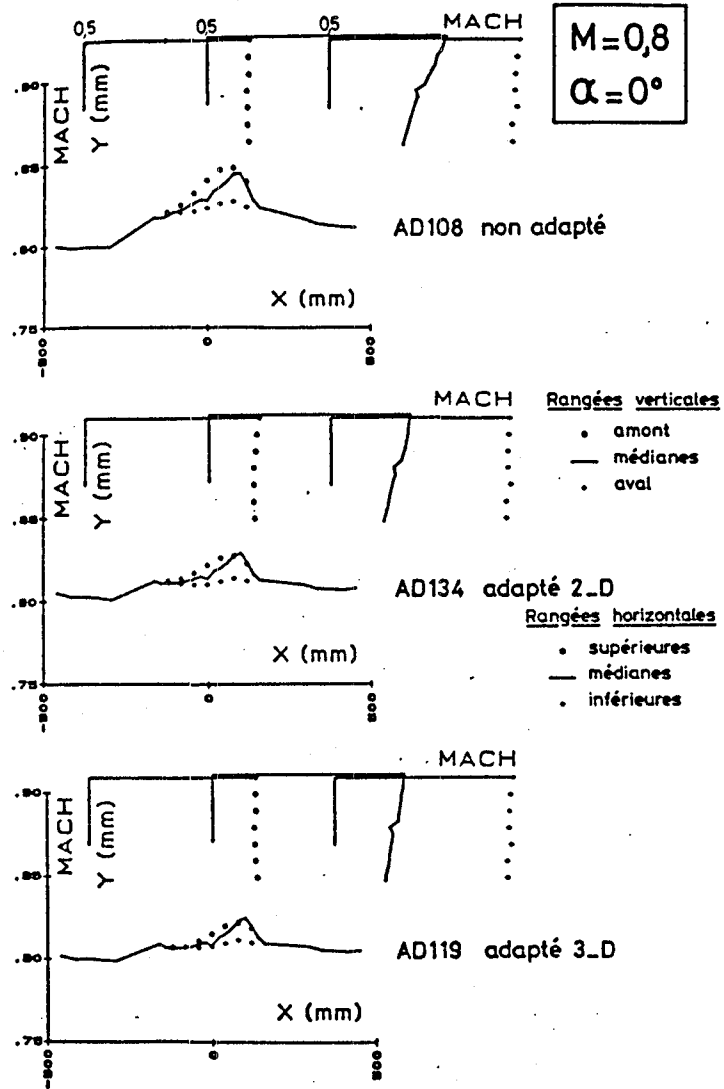


Figure 37

Use of the four base cases - Kp

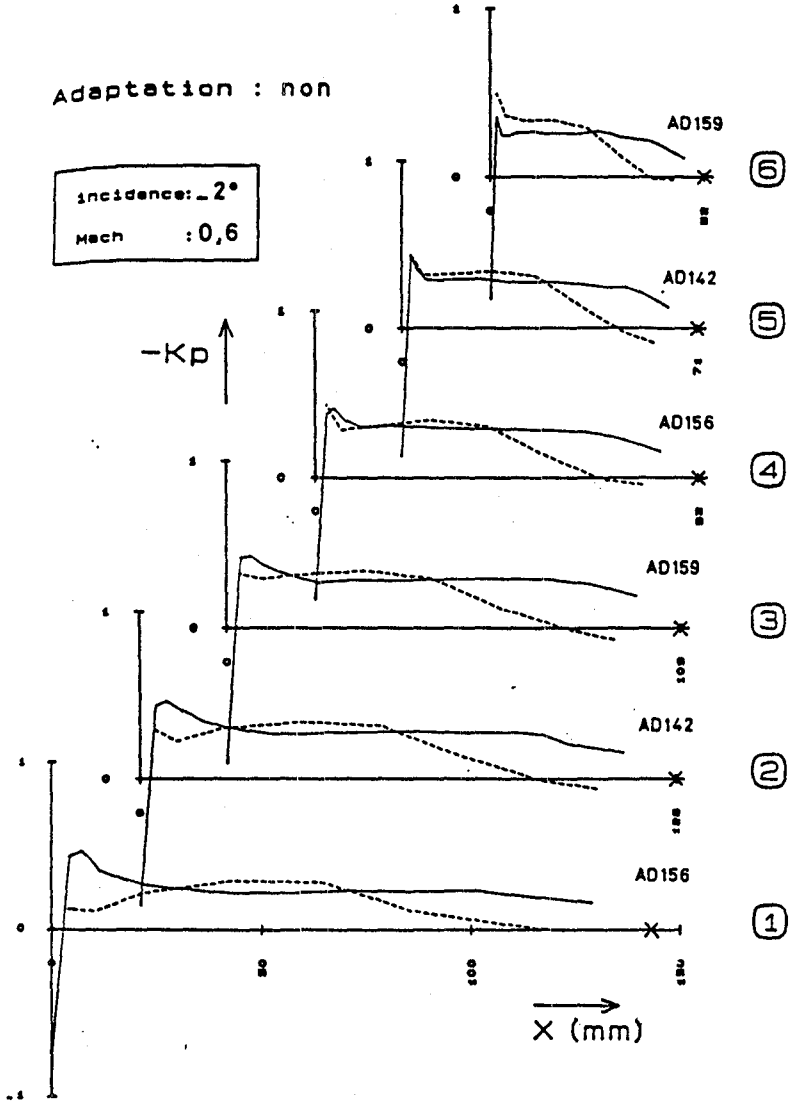


Figure 38

Use of the four base cases - Kp

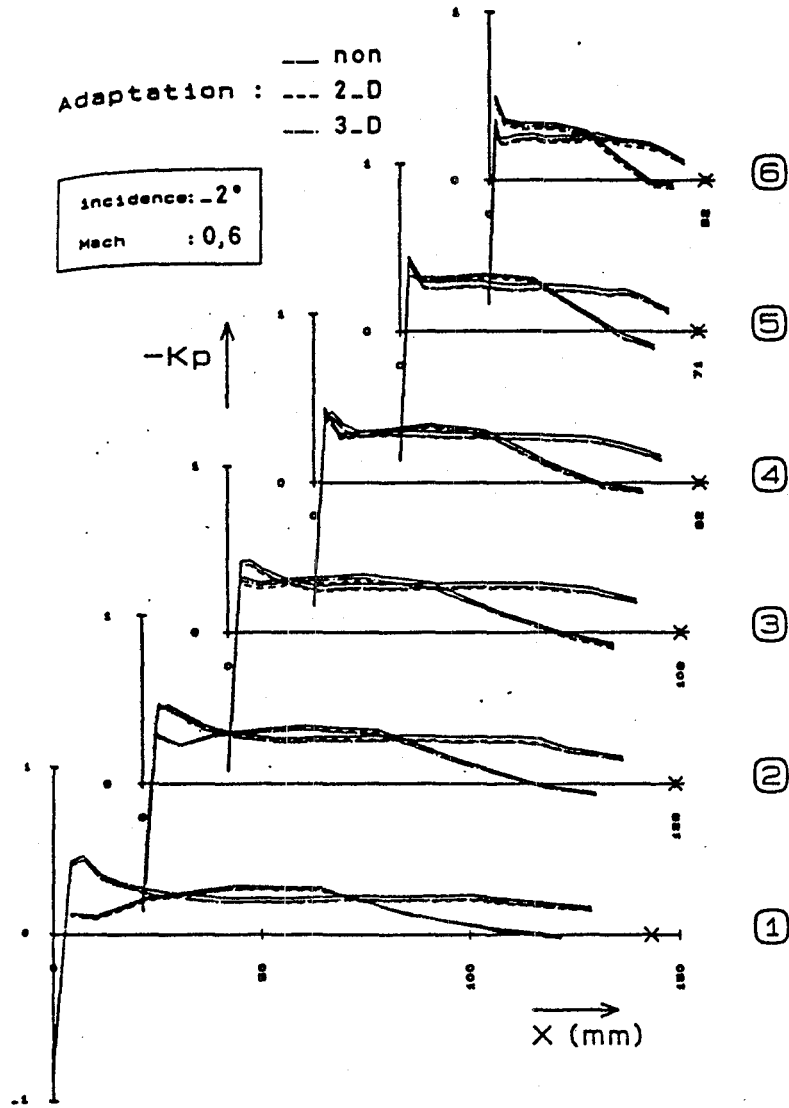


Figure 39

Use of the four base cases - Kp

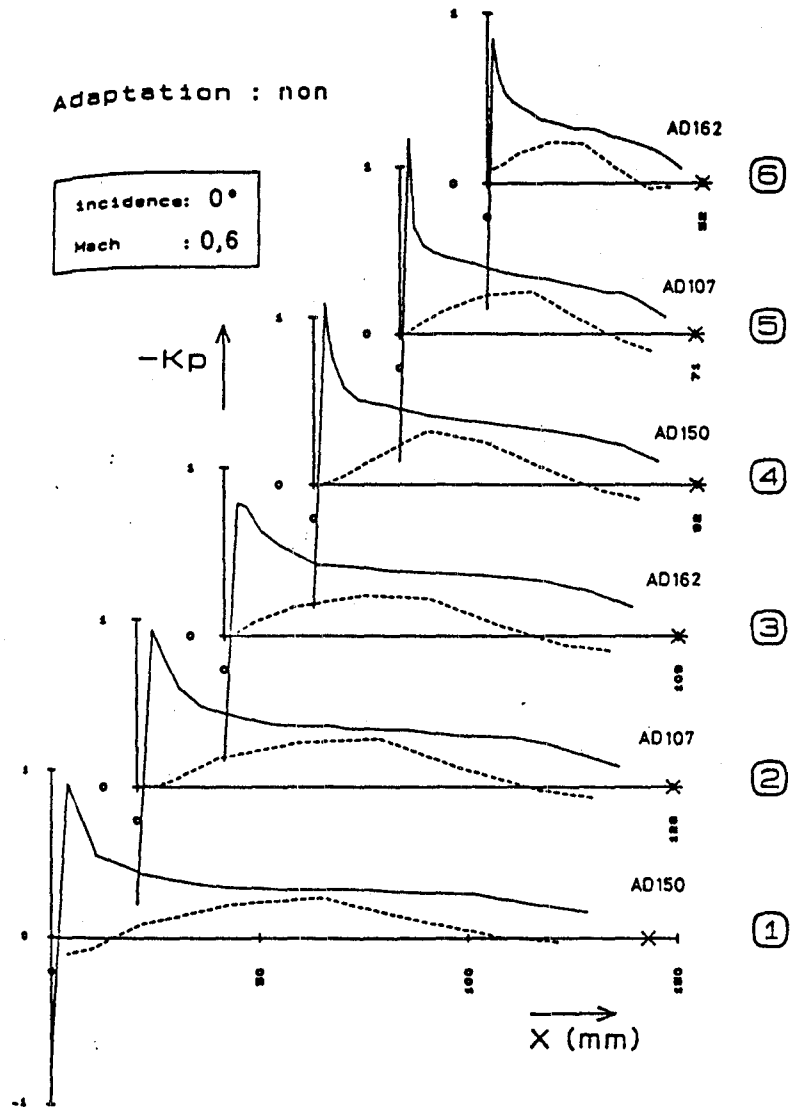


Figure 40

Use of the four base cases - Kp

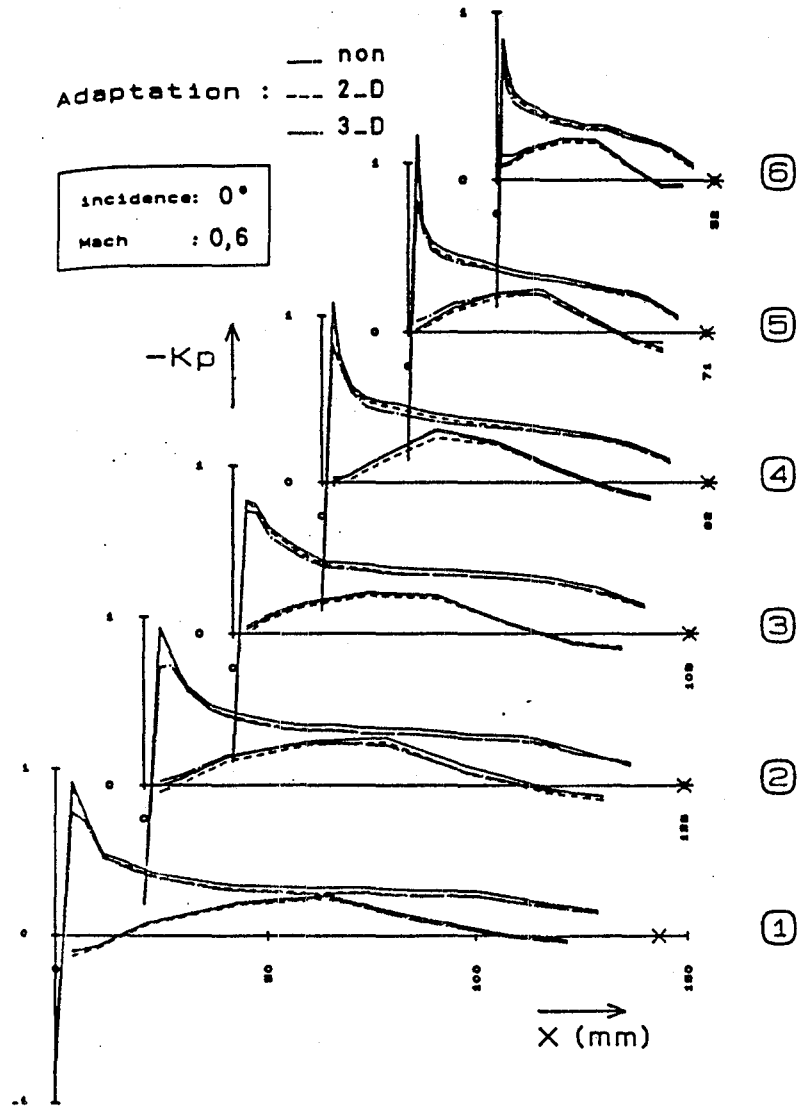


Figure 41

Use of the four base cases - Kp

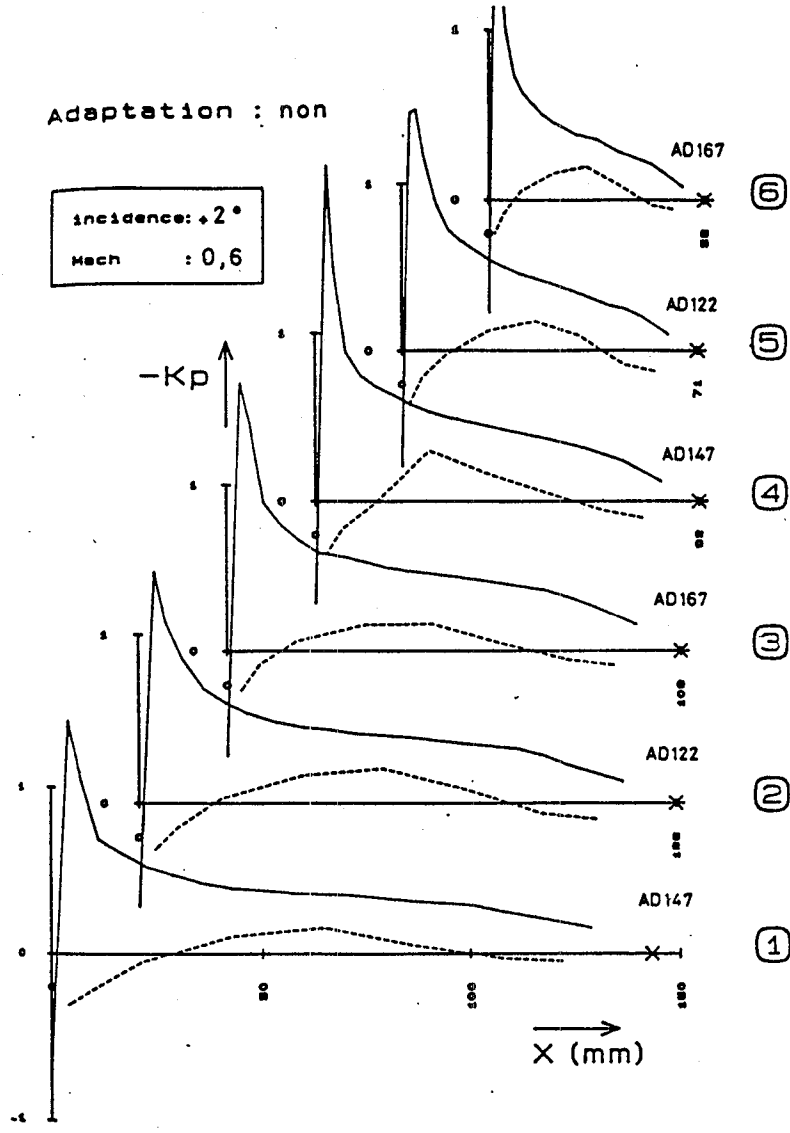


Figure 42

Use of the four base cases - Kp

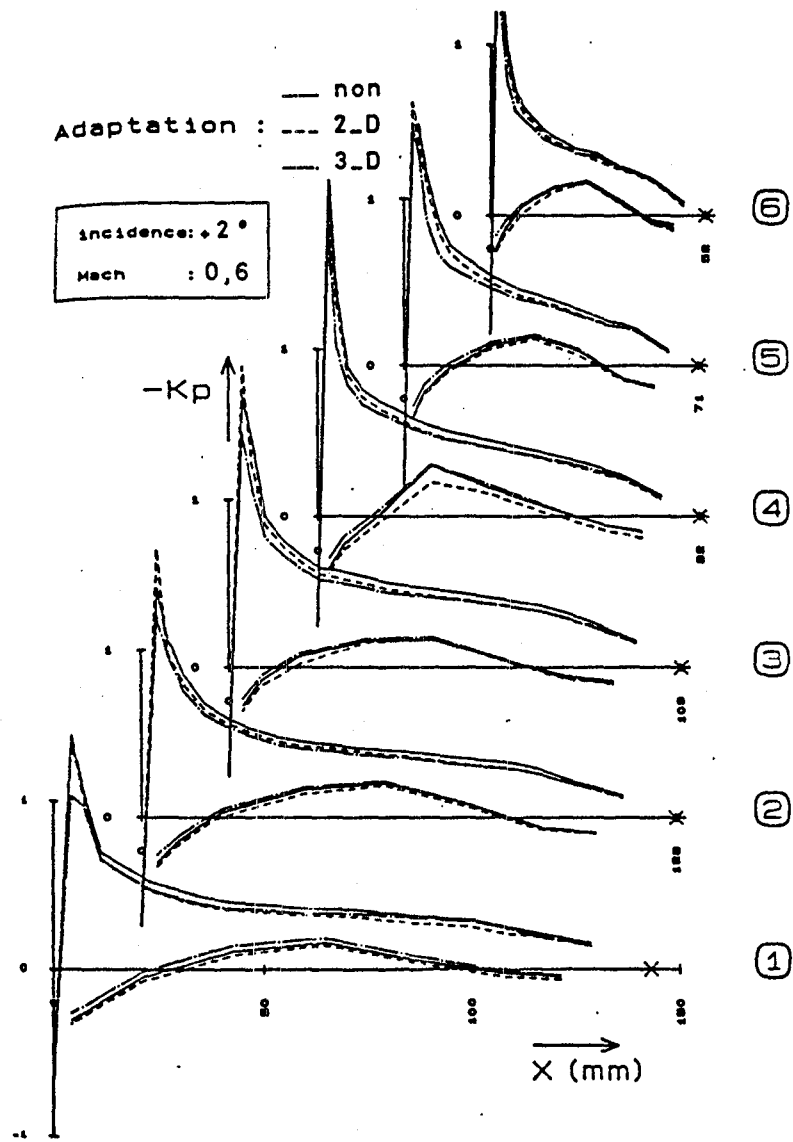


Figure 43

Use of the four base cases - Kp

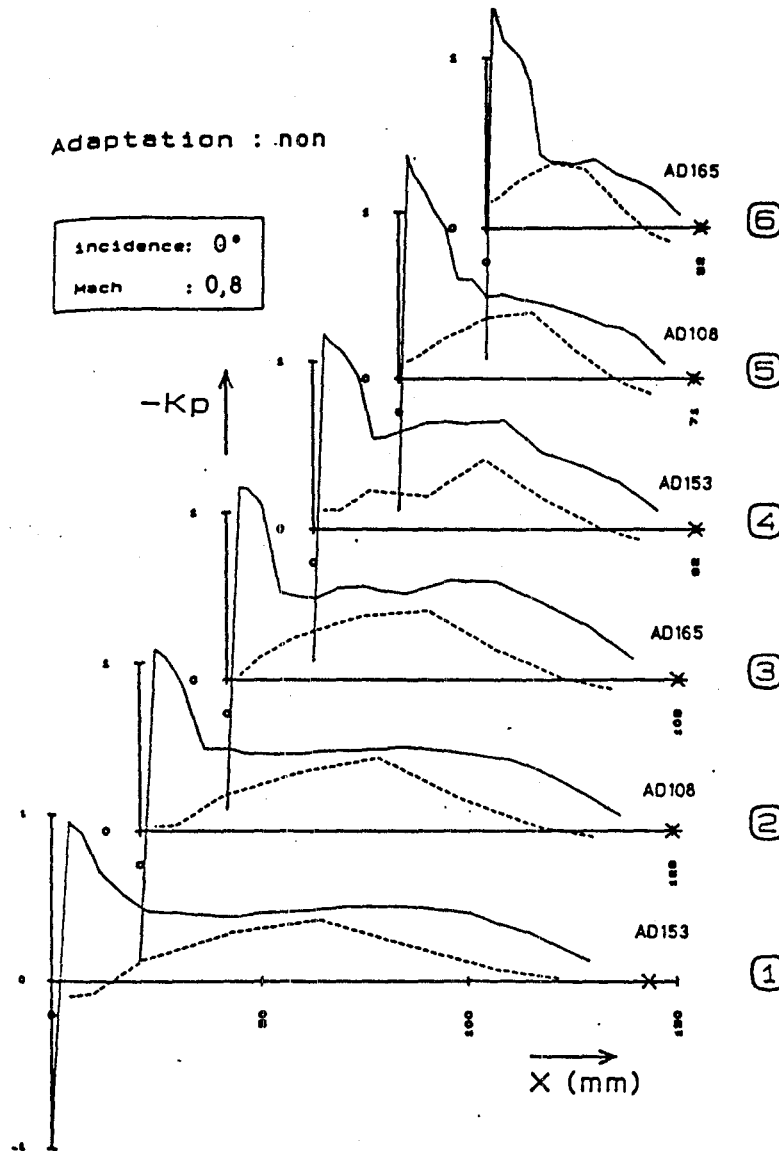
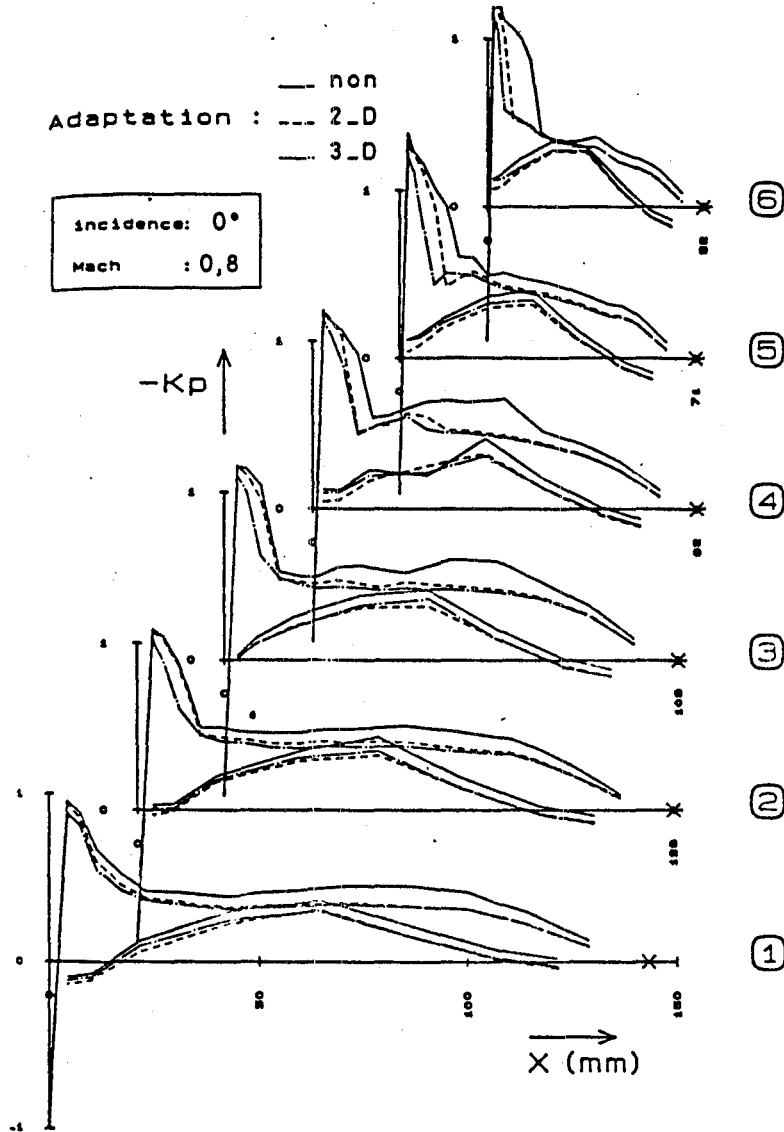


Figure 44

Use of the four base cases - Kp



Use of the four base cases - Cz
Cz recapitulative

Local lift coefficients

	NON ADAPTE	ADAPTE 2-D	ADAPTE 3-D
I = +2 M = 0.6	R 1 : 0.3600	R 1 : 0.3405	R 1 : 0.3027
	R 2 : 0.3726	R 2 : 0.3687	R 2 : 0.3229
	R 3 : 0.4388	R 3 : 0.4237	R 3 : 0.3752
	R 4 : 0.4740	R 4 : 0.4715	R 4 : 0.3861
	R 5 : 0.5091	R 5 : 0.4948	R 5 : 0.4127
	R 6 : 0.4348	R 6 : 0.4250	R 6 : 0.3658
	Aile : 0.448	Aile : 0.438	Aile : 0.371
I = 0 M = 0.6	R 1 : 0.2081	R 1 : 0.1995	R 1 : 0.1865
	R 2 : 0.2154	R 2 : 0.2198	R 2 : 0.1984
	R 3 : 0.2711	R 3 : 0.2537	R 3 : 0.2411
	R 4 : 0.2418	R 4 : 0.2419	R 4 : 0.2076
	R 5 : 0.2351	R 5 : 0.2337	R 5 : 0.1984
	R 6 : 0.1993	R 6 : 0.1926	R 6 : 0.1647
	Aile : 0.231	Aile : 0.227	Aile : 0.200
I = -2 M = 0.6	R 1 : 0.0798	R 1 : 0.0661	R 1 : 0.0687
	R 2 : 0.0888	R 2 : 0.0819	R 2 : 0.0799
	R 3 : 0.0989	R 3 : 0.0949	R 3 : 0.0945
	R 4 : 0.0665	R 4 : 0.0632	R 4 : 0.0607
	R 5 : 0.0561	R 5 : 0.0440	R 5 : 0.0486
	R 6 : 0.0232	R 6 : 0.0207	R 6 : 0.0174
	Aile : 0.066	Aile : 0.059	Aile : 0.052
I = 0 M = 0.8	R 1 : 0.2400	R 1 : 0.2253	R 1 : 0.2034
	R 2 : 0.2545	R 2 : 0.2509	R 2 : 0.2128
	R 3 : 0.3082	R 3 : 0.2842	R 3 : 0.2488
	R 4 : 0.3755	R 4 : 0.3341	R 4 : 0.3026
	R 5 : 0.4150	R 5 : 0.3825	R 5 : 0.2853
	R 6 : 0.4162	R 6 : 0.3193	R 6 : 0.2555
	Aile : 0.353	Aile : 0.315	Aile : 0.263

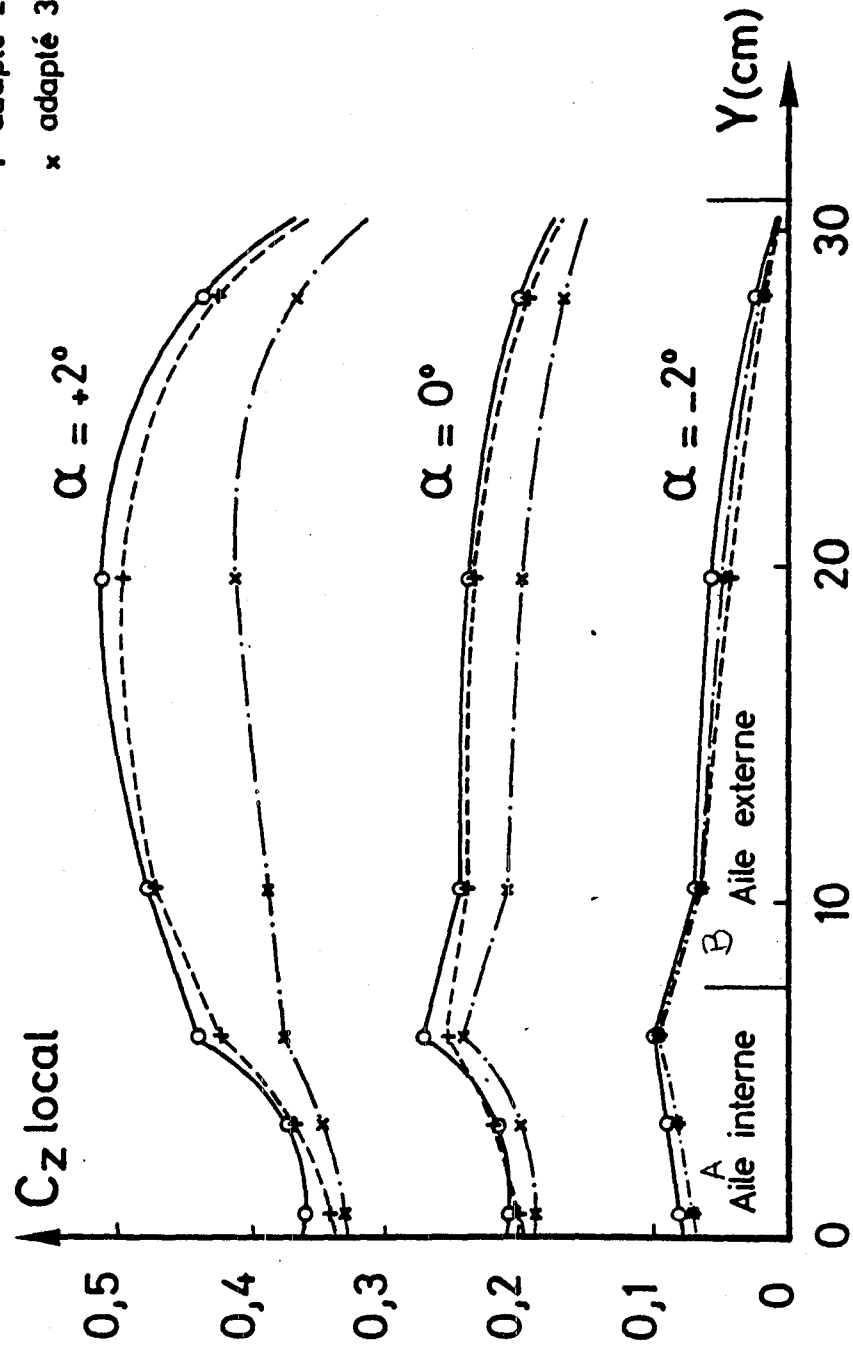
"Aile" = wing

Figure 46

Use of the four base cases - Cz

- o non adapté
- + adapté 2-D
- x adapté 3-D

$M = 0,6$



Key

- A - Internal wing
- B - External wing

Figure 47

Use of the four base cases - C_z

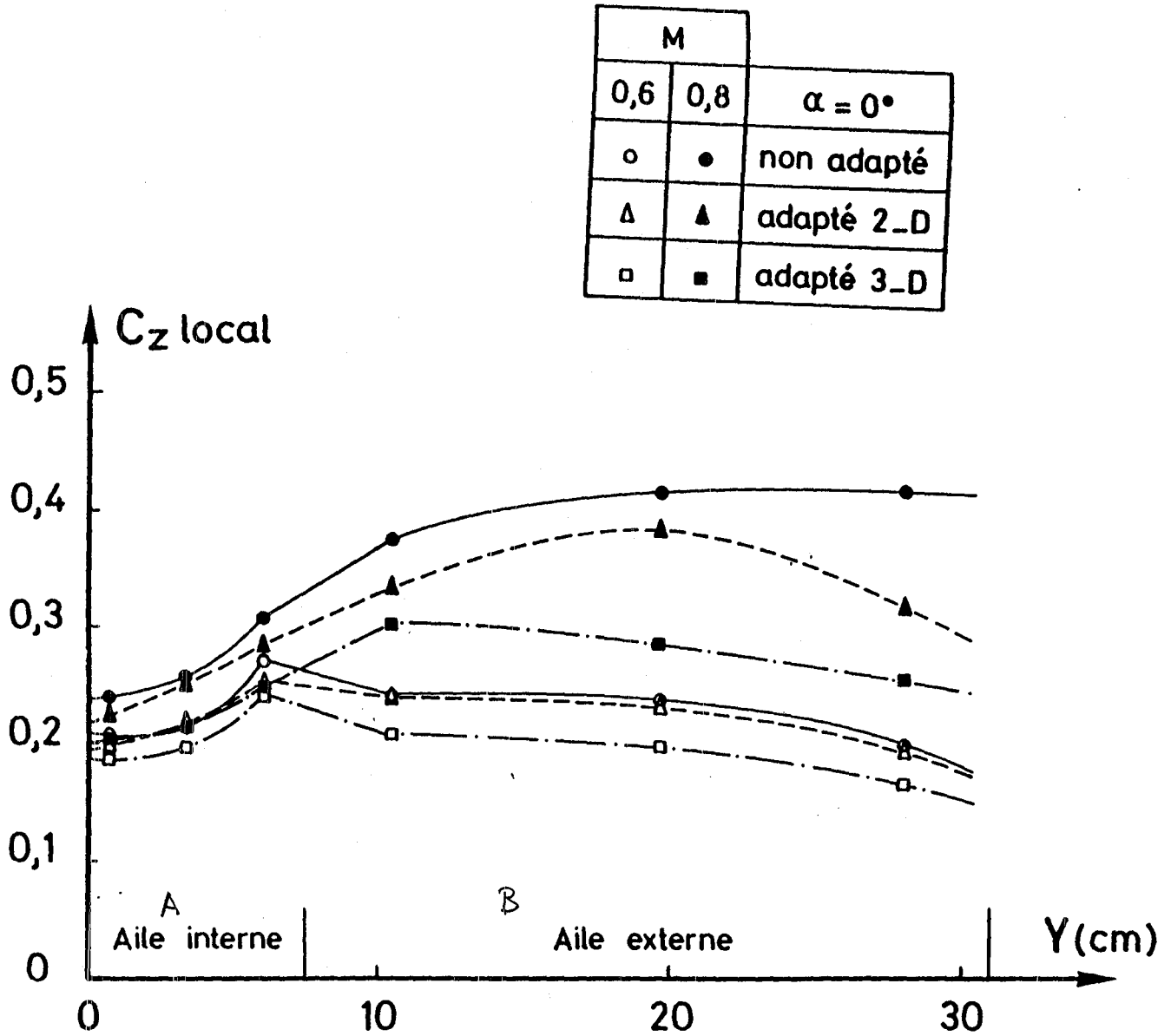
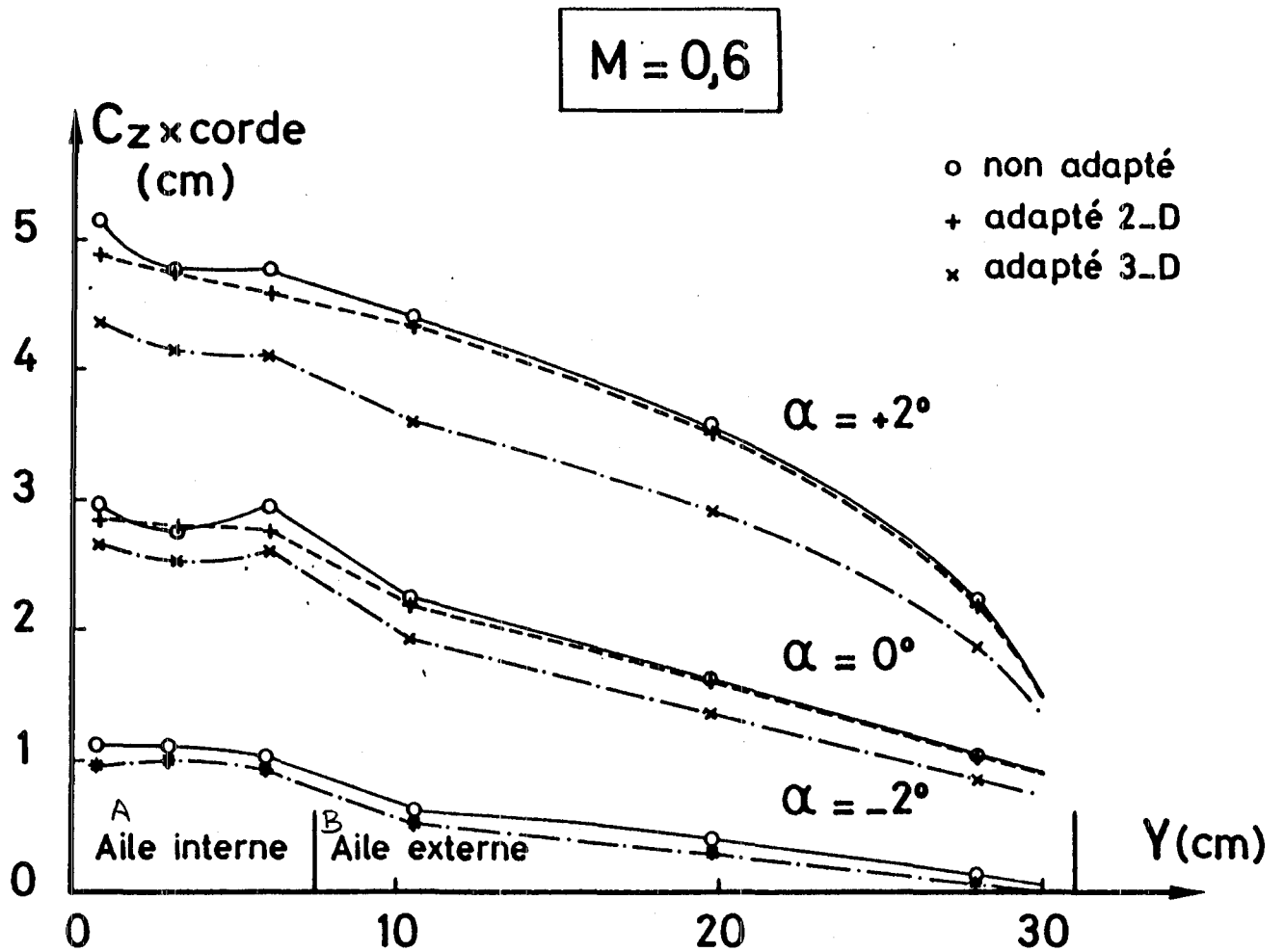


Figure 48

Use of the four base cases - Cz

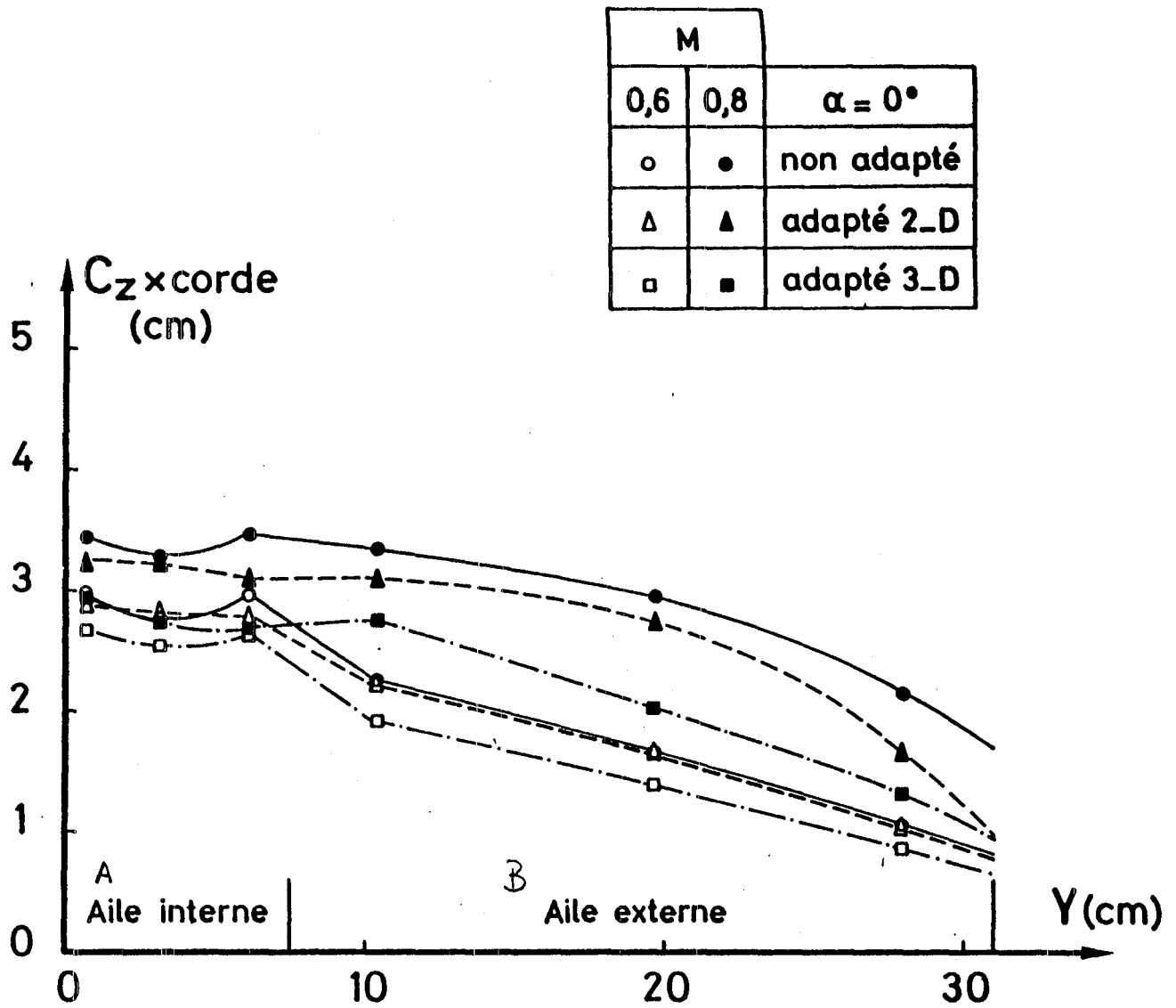


Key

- A - Internal wing
- B - External wing
- C - $C_z \times \text{chord}$

Figure 49

Use of the four base cases - Cz

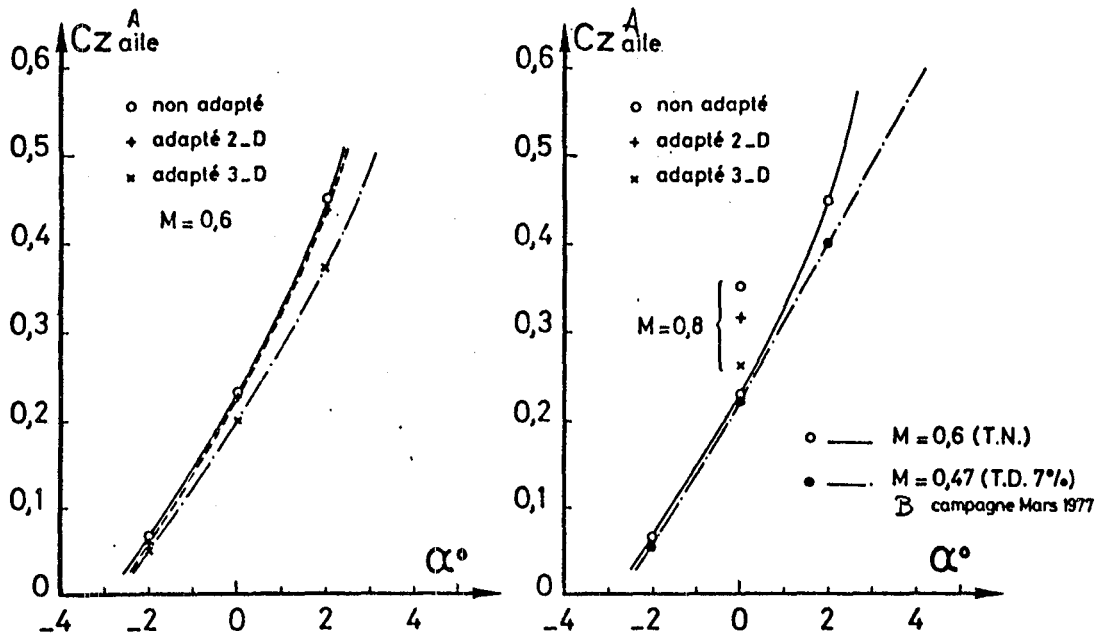


Key

- A ~ Internal wing
- B ~ External wing
- C ~ Cz x chord

Figure 50

Use of the four base cases - Cz



Key

- A - Wing
- B - March 1977 series

Listing of Cz

Key

Fichier = File
Rangee = Row
Corde = Chord

```
*****FICHIER : AD105 **** MACH = .702  INCIDENCE = 0.00  NON
* RANGE : 2      CZ= 2.310E-01  CORDE*CZ= 2.963E+01
* RANGE : 5      CZ= 2.790E-01  CORDE*CZ= 1.978E+01
*****

*****FICHIER : AD107 **** MACH = .599  INCIDENCE = 0.00  NON
* RANGE : 2      CZ= 2.154E-01  CORDE*CZ= 2.763E+01
* RANGE : 5      CZ= 2.351E-01  CORDE*CZ= 1.667E+01
*****

*****FICHIER : AD108 **** MACH = .801  INCIDENCE = 0.00  NON
* RANGE : 2      CZ= 2.545E-01  CORDE*CZ= 3.264E+01
* RANGE : 5      CZ= 4.150E-01  CORDE*CZ= 2.942E+01
*****

*****FICHIER : AD110 **** MACH = .697  INCIDENCE = -2.00  NON
* RANGE : 2      CZ= 6.918E-02  CORDE*CZ= 8.872E+00
* RANGE : 5      CZ= 3.999E-02  CORDE*CZ= 2.835E+00
*****

*****FICHIER : AD115 **** MACH = .702  INCIDENCE = 0.00  3D(1)
* RANGE : 2      CZ= 2.063E-01  CORDE*CZ= 2.645E+01
* RANGE : 5      CZ= 2.215E-01  CORDE*CZ= 1.570E+01
*****

*****FICHIER : AD116 **** MACH = .701  INCIDENCE = 0.00  3D(2)
* RANGE : 2      CZ= 2.050E-01  CORDE*CZ= 2.629E+01
* RANGE : 5      CZ= 2.270E-01  CORDE*CZ= 1.610E+01
*****

*****FICHIER : AD117 **** MACH = .598  INCIDENCE = 0.00  3D(1)
* RANGE : 2      CZ= 1.984E-01  CORDE*CZ= 2.545E+01
* RANGE : 5      CZ= 1.961E-01  CORDE*CZ= 1.390E+01
*****

*****FICHIER : AD118 **** MACH = .806  INCIDENCE = 0.00  3D(1)
* RANGE : 2      CZ= 2.070E-01  CORDE*CZ= 2.655E+01
* RANGE : 5      CZ= 2.732E-01  CORDE*CZ= 1.937E+01
*****

*****FICHIER : AD119 **** MACH = .805  INCIDENCE = 0.00  3D(2)
* RANGE : 2      CZ= 2.128E-01  CORDE*CZ= 2.729E+01
* RANGE : 5      CZ= 2.853E-01  CORDE*CZ= 2.023E+01
*****

*****FICHIER : AD120 **** MACH = .599  INCIDENCE = 2.00  NON
* RANGE : 2      CZ= 3.802E-01  CORDE*CZ= 4.876E+01
* RANGE : 5      CZ= 5.198E-01  CORDE*CZ= 3.685E+01
*****

*****FICHIER : AD122 **** MACH = .600  INCIDENCE = 2.00  NON
* RANGE : 2      CZ= 3.726E-01  CORDE*CZ= 4.779E+01
* RANGE : 5      CZ= 5.091E-01  CORDE*CZ= 3.609E+01
*****
```

*****FICHIER : AD123 **** MACH = .600 INCIDENCE = 2.00 3D(1)
* RANGE : 2 CZ= 3.229E-01 CORDE*CZ= 4.141E+01
* RANGE : 5 CZ= 4.127E-01 CORDE*CZ= 2.926E+01

*****FICHIER : AD124 **** MACH = .703 INCIDENCE = 2.00 NON
* RANGE : 2 CZ= 4.071E-01 CORDE*CZ= 5.221E+01
* RANGE : 5 CZ= 6.103E-01 CORDE*CZ= 4.327E+01

*****FICHIER : AD125 **** MACH = .703 INCIDENCE = 2.00 3D(1)
* RANGE : 2 CZ= 3.361E-01 CORDE*CZ= 4.310E+01
* RANGE : 5 CZ= 4.750E-01 CORDE*CZ= 3.368E+01

*****FICHIER : AD126 **** MACH = .806 INCIDENCE = 2.00 NON
* RANGE : 2 CZ= 5.214E-01 CORDE*CZ= 6.687E+01
* RANGE : 5 CZ= 7.394E-01 CORDE*CZ= 5.242E+01

*****FICHIER : AD127 **** MACH = .806 INCIDENCE = 2.00 3D(1)
* RANGE : 2 CZ= 3.792E-01 CORDE*CZ= 4.863E+01
* RANGE : 5 CZ= 7.103E-01 CORDE*CZ= 5.036E+01

*****FICHIER : AD128 **** MACH = .806 INCIDENCE = 2.00 3D(2)
* RANGE : 2 CZ= 4.116E-01 CORDE*CZ= 5.278E+01
* RANGE : 5 CZ= 7.521E-01 CORDE*CZ= 5.333E+01

*****FICHIER : AD129 **** MACH = .806 INCIDENCE = 2.00 3D(3)
* RANGE : 2 CZ= 3.977E-01 CORDE*CZ= 5.101E+01
* RANGE : 5 CZ= 7.435E-01 CORDE*CZ= 5.272E+01

*****FICHIER : AD130 **** MACH = .707 INCIDENCE = 1.50 2D
* RANGE : 2 CZ= 3.491E-01 CORDE*CZ= 4.477E+01
* RANGE : 5 CZ= 4.996E-01 CORDE*CZ= 3.542E+01

*****FICHIER : AD131 **** MACH = .602 INCIDENCE = 1.50 2D
* RANGE : 2 CZ= 3.210E-01 CORDE*CZ= 4.117E+01
* RANGE : 5 CZ= 4.168E-01 CORDE*CZ= 2.954E+01

*****FICHIER : AD134 **** MACH = .809 INCIDENCE = 0.00 2D
* RANGE : 2 CZ= 2.509E-01 CORDE*CZ= 3.217E+01
* RANGE : 5 CZ= 3.825E-01 CORDE*CZ= 2.712E+01

*****FICHIER : AD135 **** MACH = .702 INCIDENCE = 0.00 2D
* RANGE : 2 CZ= 2.384E-01 CORDE*CZ= 3.058E+01
* RANGE : 5 CZ= 2.758E-01 CORDE*CZ= 1.956E+01

```
*****FICHIER : AD136 **** MACH = .597  INCIDENCE = 0.00  2D
* RANGE : 2      CZ= 2.198E-01  CORDE*CZ= 2.819E+01
* RANGE : 5      CZ= 2.337E-01  CORDE*CZ= 1.657E+01
*****
*****FICHIER : AD137 **** MACH = .598  INCIDENCE = 0.00  NON
* RANGE : 2      CZ= 2.260E-01  CORDE*CZ= 2.898E+01
* RANGE : 5      CZ= 2.451E-01  CORDE*CZ= 1.738E+01
*****
*****FICHIER : AD138 **** MACH = .599  INCIDENCE = 0.00  3D(1)
* RANGE : 2      CZ= 2.004E-01  CORDE*CZ= 2.570E+01
* RANGE : 5      CZ= 1.968E-01  CORDE*CZ= 1.395E+01
*****
*****FICHIER : AD139 **** MACH = .804  INCIDENCE = 0.00  NON
* RANGE : 2      CZ= 2.686E-01  CORDE*CZ= 3.445E+01
* RANGE : 5      CZ= 4.513E-01  CORDE*CZ= 3.199E+01
*****
*****FICHIER : AD140 **** MACH = .804  INCIDENCE = 0.00  3D(1)
* RANGE : 2      CZ= 2.067E-01  CORDE*CZ= 2.651E+01
* RANGE : 5      CZ= 2.645E-01  CORDE*CZ= 1.876E+01
*****
*****FICHIER : AD141 **** MACH = .804  INCIDENCE = 0.00  3D(2)
* RANGE : 2      CZ= 2.222E-01  CORDE*CZ= 2.850E+01
* RANGE : 5      CZ= 2.991E-01  CORDE*CZ= 2.120E+01
*****
*****FICHIER : AD142 **** MACH = .598  INCIDENCE = -2.00  NON
* RANGE : 2      CZ= 8.875E-02  CORDE*CZ= 1.138E+01
* RANGE : 5      CZ= 5.611E-02  CORDE*CZ= 3.978E+00
*****
*****FICHIER : AD143 **** MACH = .598  INCIDENCE = -2.00  3D(1)
* RANGE : 2      CZ= 7.990E-02  CORDE*CZ= 1.025E+01
* RANGE : 5      CZ= 4.859E-02  CORDE*CZ= 3.445E+00
*****
*****FICHIER : AD144 **** MACH = .596  INCIDENCE = -2.00  2D
* RANGE : 2      CZ= 8.189E-02  CORDE*CZ= 1.050E+01
* RANGE : 5      CZ= 4.395E-02  CORDE*CZ= 3.116E+00
*****
*****FICHIER : AD145 **** MACH = .596  INCIDENCE = 2.00  2D
* RANGE : 2      CZ= 3.687E-01  CORDE*CZ= 4.729E+01
* RANGE : 5      CZ= 4.948E-01  CORDE*CZ= 3.508E+01
*****
*****FICHIER : AD146 **** MACH = .594  INCIDENCE = 2.00  2D
* RANGE : 1      CZ= 3.405E-01  CORDE*CZ= 4.872E+01
* RANGE : 4      CZ= 4.715E-01  CORDE*CZ= 4.344E+01
*****
```

```
*****FICHIER : AD147 **** MACH = .593  INCIDENCE = 2.00  NON
* RANGE : 1      CZ= 3.600E-01  CORDE*CZ= 5.151E+01
* RANGE : 4      CZ= 4.740E-01  CORDE*CZ= 4.367E+01
*****

*****FICHIER : AD148 **** MACH = .594  INCIDENCE = 2.00  3D(1)
* RANGE : 1      CZ= 3.027E-01  CORDE*CZ= 4.332E+01
* RANGE : 4      CZ= 3.861E-01  CORDE*CZ= 3.557E+01
*****

*****FICHIER : AD149 **** MACH = .594  INCIDENCE = 0.00  2D
* RANGE : 1      CZ= 1.995E-01  CORDE*CZ= 2.855E+01
* RANGE : 4      CZ= 2.419E-01  CORDE*CZ= 2.228E+01
*****

*****FICHIER : AD150 **** MACH = .595  INCIDENCE = 0.00  NON
* RANGE : 1      CZ= 2.081E-01  CORDE*CZ= 2.978E+01
* RANGE : 4      CZ= 2.418E-01  CORDE*CZ= 2.228E+01
*****

*****FICHIER : AD151 **** MACH = .594  INCIDENCE = 0.00  3D(1)
* RANGE : 1      CZ= 1.865E-01  CORDE*CZ= 2.669E+01
* RANGE : 4      CZ= 2.076E-01  CORDE*CZ= 1.913E+01
*****

*****FICHIER : AD152 **** MACH = .802  INCIDENCE = 0.00  2D
* RANGE : 1      CZ= 2.253E-01  CORDE*CZ= 3.225E+01
* RANGE : 4      CZ= 3.341E-01  CORDE*CZ= 3.078E+01
*****

*****FICHIER : AD153 **** MACH = .803  INCIDENCE = 0.00  NON
* RANGE : 1      CZ= 2.400E-01  CORDE*CZ= 3.434E+01
* RANGE : 4      CZ= 3.755E-01  CORDE*CZ= 3.460E+01
*****

*****FICHIER : AD154 **** MACH = .803  INCIDENCE = 0.00  3D(1)
* RANGE : 1      CZ= 2.034E-01  CORDE*CZ= 2.911E+01
* RANGE : 4      CZ= 3.026E-01  CORDE*CZ= 2.788E+01
*****

*****FICHIER : AD155 **** MACH = .595  INCIDENCE = -2.00  2D
* RANGE : 1      CZ= 6.814E-02  CORDE*CZ= 9.751E+00
* RANGE : 4      CZ= 6.321E-02  CORDE*CZ= 5.824E+00
*****

*****FICHIER : AD156 **** MACH = .596  INCIDENCE = -2.00  NON
* RANGE : 1      CZ= 7.980E-02  CORDE*CZ= 1.142E+01
* RANGE : 4      CZ= 6.654E-02  CORDE*CZ= 6.131E+00
*****

*****FICHIER : AD157 **** MACH = .596  INCIDENCE = -2.00  3D(1)
* RANGE : 1      CZ= 6.874E-02  CORDE*CZ= 9.836E+00
* RANGE : 4      CZ= 6.066E-02  CORDE*CZ= 5.589E+00
*****
```

```
****FICHER : AD158 **** MACH = .595  INCIDENCE =-2.00  2D
* RANGE : 3      CZ= 9.486E-02  CORDE*CZ= 1.030E+01
* RANGE : 6      CZ= 2.071E-02  CORDE*CZ= 1.070E+00
*****

****FICHER : AD159 **** MACH = .596  INCIDENCE =-2.00  NON
* RANGE : 3      CZ= 9.893E-02  CORDE*CZ= 1.074E+01
* RANGE : 6      CZ= 2.323E-02  CORDE*CZ= 1.200E+00
*****

****FICHER : AD160 **** MACH = .596  INCIDENCE =-2.00  3D(1)
* RANGE : 3      CZ= 9.454E-02  CORDE*CZ= 1.026E+01
* RANGE : 6      CZ= 1.742E-02  CORDE*CZ= 8.998E-01
*****

****FICHER : AD161 **** MACH = .597  INCIDENCE = 0.00  2D
* RANGE : 3      CZ= 2.537E-01  CORDE*CZ= 2.754E+01
* RANGE : 6      CZ= 1.926E-01  CORDE*CZ= 9.945E+00
*****

****FICHER : AD162 **** MACH = .598  INCIDENCE = 0.00  NON
* RANGE : 3      CZ= 2.711E-01  CORDE*CZ= 2.943E+01
* RANGE : 6      CZ= 1.993E-01  CORDE*CZ= 1.029E+01
*****

****FICHER : AD163 **** MACH = .598  INCIDENCE = 0.00  3D(1)
* RANGE : 3      CZ= 2.411E-01  CORDE*CZ= 2.617E+01
* RANGE : 6      CZ= 1.647E-01  CORDE*CZ= 8.506E+00
*****

****FICHER : AD164 **** MACH = .807  INCIDENCE = 0.00  2D
* RANGE : 3      CZ= 2.842E-01  CORDE*CZ= 3.085E+01
* RANGE : 6      CZ= 3.193E-01  CORDE*CZ= 1.649E+01
*****

****FICHER : AD165 **** MACH = .805  INCIDENCE = 0.00  NON
* RANGE : 3      CZ= 3.082E-01  CORDE*CZ= 3.346E+01
* RANGE : 6      CZ= 4.162E-01  CORDE*CZ= 2.150E+01
*****

****FICHER : AD166 **** MACH = .804  INCIDENCE = 0.00  3D(1)
* RANGE : 3      CZ= 2.488E-01  CORDE*CZ= 2.701E+01
* RANGE : 6      CZ= 2.555E-01  CORDE*CZ= 1.320E+01
*****

****FICHER : AD167 **** MACH = .599  INCIDENCE = 2.00  NON
* RANGE : 3      CZ= 4.388E-01  CORDE*CZ= 4.763E+01
* RANGE : 6      CZ= 4.348E-01  CORDE*CZ= 2.246E+01
*****

****FICHER : AD168 **** MACH = .599  INCIDENCE = 2.00  3D(1)
* RANGE : 3      CZ= 3.752E-01  CORDE*CZ= 4.074E+01
* RANGE : 6      CZ= 3.658E-01  CORDE*CZ= 1.889E+01
*****

****FICHER : AD169 **** MACH = .599  INCIDENCE = 2.00  2D
* RANGE : 3      CZ= 4.237E-01  CORDE*CZ= 4.600E+01
* RANGE : 6      CZ= 4.250E-01  CORDE*CZ= 2.195E+01
*****
```

Listing of Adaptable Wall Shapes

Listing of adaptable wall shapes (rows 2-5)

ADAPT.:	FORME	MACH	INCIDENCE
:	DEPART	0,6 : 0,8	:
NON	AD445	122	
2-D		145	+2
3-D	AD9122	123	
NON	AD4 AD4	107 : 108	
2-D		136 : 134	0
3-D	AD9107 AD9118	117 : 119	
NON	AD4	142	
2-D		144	-2
3-D	AD9142	143	

Forme depart = Beginning shape

File: AD136
Lines of current (mm)

File: AD134
Lines of current (mm)

N	Absc	12 L.C. Haut	12 L.C. Bas
1	-800.1	0.00	0.00
2	-784.7	.07	.04
3	-711.4	.14	.09
4	-670.0	.22	.14
5	-630.4	.30	.19
6	-582.6	.38	.23
7	-556.5	.48	.28
8	-522.0	.57	.32
9	-489.0	.67	.35
10	-457.6	.78	.38
11	-427.5	.90	.40
12	-398.7	1.04	.42
13	-371.2	1.19	.46
14	-345.0	1.32	.48
15	-319.9	1.46	.51
16	-295.9	1.59	.52
17	-273.0	1.72	.52
18	-251.2	1.84	.52
19	-230.3	1.99	.53
20	-210.3	2.11	.54
21	-191.2	2.26	.57
22	-174.4	2.40	.60
23	-159.3	2.52	.62
24	-145.6	2.63	.63
25	-132.8	2.72	.62
26	-120.9	2.81	.61
27	-109.7	2.89	.60
28	-99.08	2.97	.59
29	-89.09	3.05	.59
30	-79.09	3.13	.59
31	-69.60	3.20	.58
32	-60.39	3.27	.57
33	-51.39	3.34	.56
34	-42.57	3.39	.55
35	-33.99	3.43	.55
36	-25.33	3.47	.55
37	-16.94	3.49	.54
38	-8.41	3.51	.53
39	0.00	3.51	.52
40	8.41	3.51	.52
41	16.84	3.51	.52
42	25.43	3.51	.52
43	33.89	3.51	.52
44	42.57	3.50	.53
45	51.39	3.49	.53
46	60.39	3.49	.53
47	69.60	3.46	.54
48	79.09	3.43	.54
49	88.99	3.38	.54
50	99.08	3.33	.53
51	109.73	3.27	.53
52	120.94	3.18	.52
53	132.83	3.08	.52
54	145.56	2.97	.51
55	159.33	2.86	.49
56	174.43	2.75	.48
57	191.23	2.67	.47
58	210.31	2.57	.46
59	230.27	2.45	.45
60	251.17	2.31	.44
61	273.05	2.15	.44
62	295.94	1.99	.44
63	319.90	1.84	.43
64	344.99	1.70	.43
65	371.23	1.55	.43
66	398.70	1.40	.41
67	427.46	1.25	.38
68	457.55	1.11	.36
69	489.05	.99	.33
70	522.01	.87	.30

N	Absc	12 L.C. Haut	12 L.C. Bas
1	-800.1	0.00	0.00
2	-784.7	.06	.04
3	-711.4	.13	.07
4	-670.0	.20	.10
5	-630.4	.28	.14
6	-582.6	.36	.17
7	-556.5	.45	.20
8	-522.0	.54	.24
9	-489.0	.63	.28
10	-457.6	.74	.32
11	-427.5	.83	.36
12	-398.7	.97	.41
13	-371.2	1.11	.46
14	-345.0	1.27	.49
15	-319.9	1.43	.53
16	-295.9	1.60	.57
17	-273.0	1.76	.61
18	-251.2	1.91	.65
19	-230.3	2.07	.70
20	-210.3	2.24	.75
21	-191.2	2.42	.80
22	-174.4	2.60	.85
23	-159.3	2.75	.90
24	-145.6	2.89	.95
25	-132.8	3.00	.99
26	-120.9	3.09	.97
27	-109.7	3.18	.95
28	-99.08	3.27	.92
29	-89.09	3.37	.89
30	-79.09	3.48	.85
31	-69.60	3.59	.81
32	-60.39	3.68	.78
33	-51.39	3.78	.74
34	-42.57	3.86	.70
35	-33.99	3.92	.67
36	-25.33	3.99	.64
37	-16.94	4.02	.62
38	-8.41	4.05	.60
39	0.00	4.07	.59
40	8.41	4.09	.58
41	16.84	4.09	.57
42	25.43	4.09	.56
43	33.89	4.09	.55
44	42.57	4.09	.54
45	51.39	4.08	.53
46	60.39	4.06	.52
47	69.60	4.03	.51
48	79.09	3.99	.50
49	88.99	3.92	.49
50	99.08	3.85	.48
51	109.73	3.76	.47
52	120.94	3.65	.46
53	132.83	3.53	.45
54	145.56	3.41	.44
55	159.33	3.29	.43
56	174.43	3.19	.42
57	191.23	3.09	.41
58	210.31	2.97	.40
59	230.27	2.83	.39
60	251.17	2.66	.37
61	273.05	2.48	.35
62	295.94	2.31	.34
63	319.90	2.17	.33
64	344.99	2.03	.32
65	371.23	1.91	.31
66	398.70	1.81	.30
67	427.46	1.71	.29
68	457.55	1.60	.28
69	489.05	1.50	.27
70	522.01	1.40	.26

Key: Haut = high
Bas = low

File: AD144
Lines of current (mm)

File: AD145
Lines of current (mm)

N	Absc.	Z L.C. Haut	Z L.C. Bas
1	-900.1	0.00	0.00
2	-754.7	.02	0.00
3	-711.4	.05	.01
4	-670.0	.08	.01
5	-630.4	.11	.01
6	-592.6	.15	.01
7	-556.5	.19	.01
8	-522.0	.24	0.00
9	-489.0	.29	0.00
10	-457.6	.35	-.02
11	-427.5	.42	-.04
12	-398.7	.50	-.07
13	-371.2	.59	-.09
14	-345.0	.68	-.11
15	-319.9	.79	-.15
16	-295.9	.89	-.19
17	-273.0	.94	-.23
18	-251.2	1.05	-.27
19	-230.3	1.13	-.31
20	-210.3	1.21	-.35
21	-191.2	1.29	-.38
22	-174.4	1.40	-.40
23	-158.3	1.49	-.42
24	-145.6	1.58	-.45
25	-132.8	1.63	-.49
26	-120.9	1.68	-.53
27	-109.7	1.75	-.56
28	-99.08	1.81	-.60
29	-89.89	1.87	-.63
30	-79.09	1.94	-.65
31	-69.60	2.00	-.68
32	-60.39	2.07	-.71
33	-51.39	2.13	-.74
34	-42.57	2.18	-.77
35	-33.89	2.22	-.78
36	-25.33	2.26	-.78
37	-16.84	2.29	-.79
38	-8.41	2.30	-.80
39	0.00	2.31	-.80
40	8.41	2.32	-.79
41	16.84	2.32	-.78
42	25.33	2.33	-.76
43	33.89	2.34	-.75
44	42.57	2.35	-.73
45	51.39	2.35	-.71
46	60.39	2.35	-.68
47	69.60	2.35	-.66
48	79.09	2.33	-.63
49	89.89	2.31	-.60
50	99.08	2.28	-.58
51	109.73	2.24	-.55
52	120.94	2.19	-.51
53	132.83	2.11	-.48
54	145.56	2.02	-.44
55	159.33	1.94	-.41
56	174.43	1.87	-.37
57	191.23	1.80	-.34
58	210.31	1.73	-.31
59	230.27	1.65	-.28
60	251.17	1.56	-.25
61	273.05	1.49	-.21
62	295.94	1.39	-.16
63	319.90	1.31	-.11
64	344.98	1.22	-.03
65	371.23	1.12	.03
66	398.70	1.02	.09
67	427.46	.92	.13
68	457.55	.82	.17
69	489.05	.74	.20
70	522.01	.66	.23

N	Absc.	Z L.C. Haut	Z L.C. Bas
1	-900.1	0.00	0.00
2	-754.7	.12	.10
3	-711.4	.25	.21
4	-670.0	.38	.32
5	-630.4	.51	.42
6	-592.6	.65	.55
7	-556.5	.80	.69
8	-522.0	.95	.84
9	-489.0	1.10	.98
10	-457.6	1.27	1.12
11	-427.5	1.44	1.00
12	-398.7	1.61	1.06
13	-371.2	1.80	1.14
14	-345.0	1.99	1.22
15	-319.9	2.20	1.30
16	-295.9	2.42	1.48
17	-273.0	2.62	1.45
18	-251.2	2.80	1.51
19	-230.3	2.98	1.55
20	-210.3	3.17	1.64
21	-191.2	3.36	1.73
22	-174.4	3.57	1.81
23	-158.3	3.75	1.88
24	-145.6	3.89	1.94
25	-132.8	4.01	1.94
26	-120.9	4.11	1.94
27	-109.7	4.22	1.94
28	-99.08	4.32	1.95
29	-89.89	4.41	1.97
30	-79.09	4.51	1.99
31	-69.60	4.60	2.01
32	-60.39	4.69	2.03
33	-51.39	4.76	2.04
34	-42.57	4.83	2.05
35	-33.89	4.88	2.05
36	-25.33	4.93	2.07
37	-16.84	4.96	2.07
38	-8.41	4.98	2.06
39	0.00	5.00	2.05
40	8.41	5.00	2.05
41	16.84	5.00	2.04
42	25.33	5.00	2.03
43	33.89	5.00	2.02
44	42.57	5.00	2.02
45	51.39	4.99	2.01
46	60.39	4.97	2.00
47	69.60	4.94	1.99
48	79.09	4.90	1.98
49	89.89	4.83	1.94
50	99.08	4.76	1.91
51	109.73	4.67	1.88
52	120.94	4.55	1.84
53	132.93	4.41	1.80
54	145.56	4.27	1.76
55	159.33	4.13	1.72
56	174.43	3.99	1.66
57	191.23	3.85	1.61
58	210.31	3.70	1.55
59	230.27	3.53	1.53
60	251.17	3.34	1.49
61	273.05	3.13	1.43
62	295.94	2.91	1.36
63	319.90	2.69	1.29
64	344.98	2.47	1.24
65	371.23	2.24	1.19
66	398.70	2.02	1.14
67	427.46	1.81	1.09
68	457.55	1.60	1.03
69	489.05	1.41	.96
70	522.01	1.23	.88

Key: Haut = high
Bas = low

Fichier : AD142
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.24	-.34
2	-575.0	.66	-.72
3	-460.0	1.13	-1.00
4	-355.0	1.45	-1.42
5	-275.0	1.69	-1.70
6	-215.0	1.76	-1.87
7	-155.0	1.98	-2.11
8	-95.02	2.24	-2.13
9	-35.02	2.41	-2.40
10	24.99	2.46	-2.64
11	84.99	2.59	-2.69
12	144.99	2.82	-2.83
13	204.99	3.07	-3.05
14	284.99	3.16	-3.23
15	399.99	3.43	-3.62
16	504.99	3.79	-3.83

M = 0,6
 $\alpha = -2^\circ$

Non adapté

Fichier : AD144
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.37	-.21
2	-575.0	.97	-.70
3	-460.0	1.39	-1.11
4	-355.0	2.09	-1.48
5	-275.0	2.55	-1.94
6	-215.0	3.06	-2.29
7	-155.0	3.46	-2.52
8	-95.02	3.92	-2.77
9	-35.02	4.51	-3.06
10	24.99	4.79	-3.29
11	84.99	4.91	-3.35
12	144.99	4.91	-3.48
13	204.99	4.82	-3.49
14	284.99	4.78	-3.56
15	399.99	4.64	-3.59
16	504.99	4.77	-3.78

Fichier : AD143
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.45	-.40
2	-575.0	.83	-.70
3	-460.0	1.25	-1.00
4	-355.0	1.86	-1.43
5	-275.0	2.32	-1.71
6	-215.0	2.82	-2.07
7	-155.0	3.23	-2.49
8	-95.02	3.67	-2.95
9	-35.02	3.68	-3.23
10	24.99	4.12	-3.47
11	84.99	4.06	-3.53
12	144.99	4.05	-3.64
13	204.99	3.72	-3.68
14	284.99	3.48	-3.68
15	399.99	2.87	-3.72
16	504.99	2.34	-3.97

Key

Fichier = File
Cotes des parois =
Wall specifications
Haut = High
Bas = Low

Fichier : AD107
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.24	-.26
2	-575.0	.63	-.66
3	-460.0	1.05	-.98
4	-355.0	1.45	-1.45
5	-275.0	1.69	-1.73
6	-215.0	1.89	-1.88
7	-155.0	1.98	-1.94
8	-95.02	2.23	-2.13
9	-35.02	2.43	-2.41
10	24.98	2.50	-2.46
11	94.98	2.79	-2.56
12	144.98	2.83	-2.90
13	204.98	3.08	-3.11
14	294.93	3.23	-3.26
15	389.98	3.53	-3.55
16	504.98	3.89	-3.92

M
r

Non adapté

Fichier : AD136
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.19	-.21
2	-575.0	1.13	-.51
3	-460.0	1.92	-.72
4	-355.0	2.71	-1.03
5	-275.0	3.38	-1.12
6	-215.0	3.90	-1.29
7	-155.0	4.43	-1.50
8	-95.02	4.13	-1.79
9	-35.02	5.77	-1.51
10	24.98	6.04	-1.04
11	94.98	6.02	-2.27
12	144.98	5.89	-2.45
13	204.98	5.54	-3.60
14	294.93	5.40	-2.94
15	389.98	5.13	-3.21
16	504.98	4.82	-3.50

2-D

Fichier : AD117
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.44	-.29
2	-575.0	.84	-.66
3	-460.0	1.26	-1.00
4	-355.0	1.86	-1.25
5	-275.0	2.31	-1.56
6	-215.0	2.82	-2.07
7	-155.0	3.23	-2.36
8	-95.02	3.63	-2.77
9	-35.02	3.89	-3.24
10	24.98	3.74	-3.70
11	94.98	3.45	-4.14
12	144.98	3.03	-4.63
13	204.98	2.47	-5.11
14	294.93	1.85	-5.70
15	389.98	.56	-6.47
16	504.98	-.58	-7.38

3-D

Key

Fichier = File
Cotes des parois =
Wall specifications
Haut = High
Bas = Low

Fichier : AD122
Cotes des parois (mm)

N	Abac.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	1.67	1.76
2	-575.0	3.15	1.60
3	-460.0	4.55	2.30
4	-355.0	5.82	2.80
5	-275.0	6.70	3.43
6	-215.0	7.42	3.76
7	-155.0	8.05	4.11
8	-95.02	8.70	4.33
9	-35.02	9.52	4.83
10	24.98	10.22	5.03
11	84.98	10.96	5.44
12	144.98	11.58	5.87
13	204.98	12.28	6.13
14	264.98	13.25	6.66
15	329.98	14.37	7.21
16	504.98	15.71	7.73

M=0,6
 $\alpha = +2^\circ$

Non adapte

Fichier : AD145
Cotes des parois (mm)

N	Abac.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	1.55	1.01
2	-575.0	1.50	-1.18
3	-460.0	2.38	-1.28
4	-355.0	3.25	-1.23
5	-275.0	4.19	-1.28
6	-215.0	4.92	-1.23
7	-155.0	5.74	-1.27
8	-95.02	6.43	-1.17
9	-35.02	7.20	-1.34
10	24.98	7.42	-1.58
11	84.98	7.44	-1.51
12	144.98	7.21	-1.24
13	204.98	6.35	-1.53
14	264.98	6.37	-1.90
15	329.98	5.75	-2.36
16	504.98	5.30	-2.45

2-D

Fichier : AD123
Cotes des parois (mm)

N	Abac.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	1.58	1.95
2	-575.0	3.13	1.62
3	-460.0	4.54	2.32
4	-355.0	6.02	2.87
5	-275.0	7.12	3.23
6	-215.0	8.03	3.35
7	-155.0	8.89	3.50
8	-95.02	9.74	3.50
9	-35.02	10.16	3.20
10	24.98	10.41	2.99
11	84.98	10.16	2.76
12	144.98	9.93	2.43
13	204.98	9.33	2.17
14	264.98	8.62	1.42
15	329.98	7.50	1.02
16	504.98	6.55	1.75

3-D

Key

Fichier = File
Cotes des parois =
Wall specifications
Haut = High
Bas = Low

Fichier : AD108
Cotes des parois (mm)

N	Absc.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	.23	-.26
2	-575.0	.63	-.66
3	-460.0	1.04	-.99
4	-355.0	1.46	-1.45
5	-275.0	1.89	-1.74
6	-215.0	1.89	-1.88
7	-155.0	1.97	-1.94
8	-95.02	2.22	-2.13
9	-35.02	2.43	-2.40
10	24.98	2.50	-2.46
11	84.98	2.79	-2.67
12	144.98	2.82	-2.89
13	204.98	3.08	-3.11
14	264.98	3.23	-3.27
15	324.98	3.52	-3.55
16	504.98	4.00	-3.82

M = 0,8
α = 0°

Non adapté

Fichier : AD104
Cotes des parois (mm)

N	Absc.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	.42	-.26
2	-575.0	1.21	-.54
3	-460.0	1.33	-.77
4	-355.0	2.52	-1.09
5	-275.0	3.35	-1.30
6	-215.0	4.03	-1.44
7	-155.0	4.63	-1.49
8	-95.02	5.13	-1.91
9	-35.02	6.13	-2.19
10	24.98	6.44	-2.43
11	84.98	6.57	-2.48
12	144.98	6.34	-2.61
13	204.98	6.01	-2.84
14	264.98	5.74	-3.03
15	324.98	5.55	-3.40
16	504.98	5.47	-3.91

2-D

Fichier : AD119
Cotes des parois (mm)

N	Absc.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	.44	-.51
2	-575.0	.67	-.89
3	-460.0	1.47	-1.39
4	-355.0	2.06	-1.84
5	-275.0	2.53	-2.33
6	-215.0	3.03	-2.88
7	-155.0	3.64	-3.36
8	-95.02	4.11	-3.98
9	-35.02	4.51	-4.52
10	24.98	4.98	-4.93
11	84.98	4.25	-5.32
12	144.98	3.45	-5.60
13	204.98	3.08	-5.11
14	264.98	2.37	-6.71
15	324.98	1.26	-7.60
16	504.98	.45	-8.68

3-D

Key

Fichier = File
Cotes des parois =
Wall specifications
Haut = High
Bas = Low

Listing of Test Files

Key to Annex 3

Fichier = File
Parois rectilignes = Rectilinear walls
Symetriques = Symmetrical

Page format:

MACH HIGH AND LOW WALLS	MACH LATERAL WALLS	AS07 WING
I HIGH LOW	I HIGH LOW	I MACH
	DBL. RECORDERS	UPSTM PTHOLE

LFT. LAT. RECORDERS

DNSTRM PTHOLE RT. PTHOLE

RT. LAT. RECORDERS

LFT. PTHOLE

NECK RECORDERS

LISTE DES ESSAIS "AILE AS07"

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*****
* FICHER AD4 : PAROIS RECTILIGNES DIVERGENTES
* AD445 : IDEM + ROTATION DE 30° (VERS LE HAUT)
* AD___ : FICHER DE L'ESSAI N = ___
* AD9___ : CALCUL 3-D DE LA NOUVELLE POSITION DES PAROIS
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* FICHER	INC. AFF.	MACH	RANGÉES DE PRISES	FICHER DE DEPART	ROT. PAROIS	ADAPT.	NB. D'ITER.
* AD105	0	.7	2 - 5	AD4	0	NON	1
* AD107	0	.7	"	"	0	"	1
* AD108	0	.7	"	"	0	"	1
* AD110	-2	.7	"	"	0	"	1
* AD115	0	.7	"	AD9105	0	3-D (1)	1
* AD116	0	.7	"	AD9115	0	3-D (2)	1
* AD117	0	.6	"	AD9107	0	3-D	1
* AD118	0	.6	"	AD9108	0	3-D (1)	1
* AD119	0	.6	"	AD9118	0	3-D (2)	1
* AD120	+2	.5	"	AD4	0	NON	1
* AD122	+1.5	.6	"	AD445	30'	NON	1
* AD123	+1.5	.6	"	AD9122	30'	3-D	1
* AD124	+1.5	.7	"	AD445	30'	NON	1
* AD125	+1.5	.7	"	AD9124	30'	3-D	1
* AD126	+1.5	.6	"	AD445	30'	NON	1
* AD127	+1.5	.6	"	AD9126	30'	3-D (1)	1
* AD129	+1.5	.6	"	AD9127	30'	3-D (2)	1
* AD129	+1.5	.6	"	AD9128	30'	3-D (3)	1
* AD130	+1.5	.7	"	AD4	0	2-D	4
* AD131	+1.5	.6	"	AD130	0	2-D	4
* AD133	0	.6	"	AD4	0	2-D	4
* AD134	0	.6	"	AD133	0	2-D	4
* AD135	0	.6	"	AD134	0	2-D	4
* AD136	0	.6	"	AD135	0	2-D	4
* AD137	-0.5	.6	"	AD445	30'	NON	1
* AD138	-0.5	.6	"	AD9137	30'	3-D	1
* AD139	-0.5	.6	"	AD445	30'	NON	1
* AD140	-0.5	.6	"	AD9139	30'	3-D (1)	1
* AD141	-0.5	.6	"	AD9140	30'	3-D (2)	1
* AD142	-2	.6	"	AD4	0	NON	1
* AD143	-2	.6	"	AD9142	0	3-D	1
* AD144	-2	.6	"	AD136	0	2-D	4
* AD145	+2	.6	"	AD131	0	2-D	4

* AD146	+2	.6	1 - 4	AD145	0	2-D	4
* AD147	+1.5	.6	"	AD445	30'	NON	1
* AD148	+1.5	.6	"	AD9122	30'	3-D	1
* AD149	0	.6	"	AD136	0	2-D	4
* AD150	0	.6	"	AD4	0	NON	1
* AD151	0	.6	"	AD9107	0	3-D	1
* AD152	0	.6	"	AD134	0	2-D	4
* AD153	0	.6	"	AD4	0	NON	1
* AD154	0	.6	"	AD9118	0	3-D	1
* AD155	-2	.6	"	AD144	0	2-D	4
* AD156	-2	.6	"	AD4	0	NON	1
* AD157	-2	.6	"	AD9142	0	3-D	1

* AD158	-2	.6	3 - 6	AD144	0	2-D	4
* AD159	-2	.6	"	AD4	0	NON	1
* AD160	-2	.6	"	AD9142	0	3-D	1
* AD161	0	.6	"	AD136	0	2-D	4
* AD162	0	.6	"	AD4	0	NON	1
* AD163	0	.6	"	AD9107	0	3-D	1
* AD164	0	.6	"	AD134	0	2-D	4
* AD165	0	.6	"	AD4	0	NON	1
* AD166	0	.6	"	AD9118	0	3-D	1
* AD167	+1.5	.6	"	AD445	30'	NON	1
* AD168	+1.5	.6	"	AD9122	30'	3-D	1
* AD169	+2	.6	"	AD145	0	2-D	4

***** FICHER AD105 NOCITE= 1
 14/ 8/85 11H40 AS07 M=.7 I=0 R 2-5 NON ADAPTE AD105
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .7019 UINF= 231.103 M/S
 TIV=299.6 K PIV= 1557 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS4	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.702	.701	PRISES DOUBLES			HUB. AMONT	33	.715	1	.702	.702
2	.702	.705					34	.714	2	.702	.702
3	.701	.702	59	.701	.701	1	.702	35	.713	3	.702
4	.700	.701	60	.703	.704	2	.702	36	.712	4	.702
5	.700	.702	61	.706	.705	3	.701	37	.712	5	.702
6	.702	.703				4	.701	38	.712	6	.702
7	.702	.702	PRISES LAT. GAUCHES			5	.701	39	.713	7	.702
8	.704	.702				6	.701	40	.714	8	.702
9	.703	.705	62	.700	.703	7	.701	41	.715	9	.702
10	.703	.700	63	.701	.707	8	.701	42	.714	10	.702
11	.700	.701	64	.708	.707	9	.701	43	.712	11	.702
12	.698	.701	65	.709	.706	10	.701	44	.712	12	.702
13	.699	.700	66	.717	.709	11	.702	45	.711	13	.702
14	.700	.702	67	.725	.710					14	.702
15	.701	.703	68	.729	.713	HUB. AVAL		HUB. DROIT		15	.702
16	.703	.703	69	.730	.715	1	.703	1	.702	16	.702
17	.705	.703	70	.727	.711	2	.703	2	.702	17	.702
18	.703	.703	71	.715	.703	3	.703	3	.701	18	.702
19	.707	.703	72	.711	.709	4	.711	4	.702	19	.702
20	.707	.705	73	.698	.710	5	.703	5	.703	20	.702
21	.709	.705				6	.703	6	.703	21	.702
22	.716	.707	PRISES LAT. DROITES			7	.703	7	.702	22	.702
23	.719	.706				8	.703	8	.702	23	.702
24	.719	.709	74	.701	.704	9	.703	9	.702	24	.702
25	.721	.711	75	.701	.702	10	.703	10	.702	25	.702
26	.721	.710	76	.702	.701	11	.707	11	.702	26	.702
27	.726	.703	77	.700	.699					27	.702
28	.729	.711	78	.703	.700	HUB. GAUCHE		HUB. GAUCHE		28	.702
29	.734	.711	79	.705	.699	13	.703	13	.702	29	.702
30	.731	.711	80	.715	.704	14	.702	14	.702	30	.702
31	.737	.703	81	.724	.707	1	.723	1	.702	31	.702
32	.735	.713	82	.725	.710	2	.725	2	.702	32	.702
33	.733	.714	83	.732	.710	3	.724	3	.702	33	.702
34	.735	.713	84	.742	.710	4	.714	4	.702	34	.702
35	.733	.715	85	.745	.713	5	.715	5	.702	35	.702
36	.735	.715	86	.743	.715	6	.720	6	.702	36	.702
37	.736	.714	87	.742	.715	7	.723	7	.702	37	.702
38	.734	.714	88	.740	.714	8	.725	8	.702	38	.702
39	.735	.713	89	.736	.712	9	.725	9	.702	39	.702
40	.730	.712	90	.729	.711	10	.723	10	.702	40	.702
41	.739	.711	91	.725	.709	11	.722	11	.702	41	.702
42	.739	.710	92	.717	.703	12	.722	12	.702	42	.702
43	.729	.709	93	.709	.707	13	.720	13	.702	43	.702
44	.734	.703	94	.713	.705	14	.719	14	.703	44	.702
45	.722	.707	95	.705	.695	15	.713	15	.702	45	.702
46	.719	.703	96	.698	.692	16	.712	16	.703	46	.702
47	.713	.703				17	.712	17	.702	47	.702
48	.715	.709				18	.713	18	.702	48	.702
49	.714	.703				19	.713	19	.702	49	.702
50	.711	.703				20	.714	20	.702	50	.702
51	.712	.703				21	.715	21	.702		
52	.707	.705	PRISES COL			22	.715	22	.702		
53	.707	.705				23	.714	23	.702		
54	.707	.705		.764	1.155	24	.719	24	.702		
55	.705	.704		.813	1.250	25	.720	25	.702		
56	.703	.701		.874	.941	26	.722	26	.702		
57	.700	.698		.931	.795	27	.723	27	.702		
58	.695	.687		1.099	.738	28	.723	28	.702		
						29	.723	29	.702		
						30	.713	30	.702		
						31	.715	31	.702		
						32	.715	32	.702		

***** FICHER AD107 N0(17)= 1
 14 8 85 11H55 R307 M=.6 I=0 R 2-5 NON ADAPTE AD107
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

 MACH DE REFERENCE= .5983 UINF= 231.108 M/S
 TIV=296.8 K PIV= 1534 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE R307	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.599	.599	PRISES DOUBLES			HUB. AMONT	33	.605	1	.579	
2	.599	.602					34	.605	2	.593	
3	.599	.599	59	.598	.597	1	.598	35	.604	3	.605
4	.597	.597	60	.599	.600	2	.598	36	.604	4	.608
5	.597	.598	61	.599	.601	3	.598	37	.604	5	.602
6	.599	.600				4	.598	38	.604	6	.602
7	.599	.599	PRISES LAT. GAUCHES			5	.597	39	.604	7	.612
8	.599	.598				6	.597	40	.605	8	.599
9	.600	.601	62	.598	.600	7	.597	41	.605	9	.645
10	.600	.597	63	.604	.603	8	.597	42	.605	10	.605
11	.597	.598	64	.603	.601	9	.599	43	.603	11	.609
12	.596	.599	65	.603	.600	10	.598	44	.602	12	.719
13	.597	.598	66	.608	.601	11	.599	45	.602	13	.747
14	.598	.600	67	.613	.601					14	.735
15	.599	.600	68	.616	.603	HUB. AVANT		HUB. DROIT		15	.725
16	.600	.599	69	.616	.606	1	.602	1	.599	16	.714
17	.601	.599	70	.615	.603	2	.602	2	.599	17	.711
18	.603	.599	71	.605	.601	3	.603	3	.599	18	.711
19	.602	.599	72	.603	.602	4	.603	4	.599	19	.706
20	.603	.600	73	.590	.606	5	.605	5	.599	20	.704
21	.603	.600				6	.603	6	.599	21	.694
22	.608	.601	PRISES LAT. DROITES			7	.603	7	.599	22	.691
23	.611	.600				8	.603	8	.599	23	.682
24	.610	.602	74	.599	.600	9	.603	9	.599	24	.686
25	.612	.603	75	.599	.599	10	.604	10	.599	25	.682
26	.612	.603	76	.599	.598	11	.603	11	.599	26	.680
27	.614	.601	77	.597	.597					27	.673
28	.616	.603	78	.599	.597	HUB. GAUCHE				28	.644
29	.619	.603	79	.601	.595	13	.615	13	.599	29	.619
30	.618	.603	80	.608	.599	14	.614	14	.599	30	.603
31	.622	.601	81	.615	.601	15	.614	15	.599	31	.616
32	.620	.605	82	.615	.603	16	.612	16	.599	32	.616
33	.622	.605	83	.618	.601	17	.612	17	.599	33	.616
34	.620	.604	84	.624	.601	18	.606	18	.599	34	.716
35	.622	.605	85	.626	.602	19	.607	19	.599	35	.714
36	.620	.605	86	.625	.604	20	.609	20	.599	36	.714
37	.621	.604	87	.624	.605	21	.611	21	.599	37	.714
38	.619	.604	88	.623	.604	22	.613	22	.599	38	.713
39	.620	.604	89	.622	.603	23	.613	23	.599	39	.713
40	.617	.603	90	.616	.603	24	.612	24	.599	40	.712
41	.617	.603	91	.614	.601	25	.611	25	.599	41	.714
42	.617	.602	92	.608	.601	26	.610	26	.599	42	.703
43	.617	.601	93	.602	.600	27	.609	27	.599	43	.702
44	.613	.601	94	.604	.601	28	.609	28	.599	44	.690
45	.612	.600	95	.596	.598	29	.605	29	.599	45	.677
46	.609	.601	96	.590	.596	30	.604	30	.599	46	.668
47	.609	.601				31	.605	31	.599	47	.663
48	.607	.602				32	.605	32	.599	48	.666
49	.606	.602				33	.605	33	.599	49	.666
50	.604	.602				34	.606	34	.600	50	.661
51	.604	.602				35	.606	35	.600		
52	.601	.602	PRISES COL			36	.607	36	.599		
53	.599	.603				37	.605	37	.599		
54	.598	.603	1.066	1.064		38	.608	38	.599		
55	.596	.602	1.066	1.063		39	.609	39	.599		
56	.593	.600	1.000	.981		40	.610	40	.599		
57	.591	.599	1.066	.791		41	.611	41	.599		
58	.590	.593	1.027	.725		42	.612	42	.599		
						43	.610	43	.599		
						44	.608	44	.599		
						45	.606	45	.599		
						32	.606				

***** FICHER AD110 NOCIT)= 1
 14 3 35 15H50 AS07 M=7 I=-2 R 2-5 NON ADAPTE AD110
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

 MACH DE REFERENCE= .6974 UINF= 231.108 M/S
 TIV=299.3 K PIV= 1553 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.698	.697	PRISES DOUBLES			HUB. AMONT		33	.712	1	.681
2	.699	.702						34	.712	2	.706
3	.699	.699	59	.697	.697	1	.697	35	.712	3	.770
4	.696	.697	60	.699	.700	2	.697	36	.709	4	.649
5	.696	.699	61	.701	.700	3	.697	37	.710	5	.649
6	.699	.699	PRISES LAT. GAUCHES			4	.696	38	.711	6	.801
7	.697	.698				5	.695	39	.712	7	.779
8	.698	.697				6	.695	40	.714	8	.819
9	.699	.701	62	.696	.699	7	.696	41	.714	9	.869
10	.699	.695	63	.698	.704	8	.695	42	.712	10	.910
11	.696	.693	64	.702	.702	9	.696	43	.711	11	.873
12	.694	.698	65	.705	.701	10	.695	44	.711	12	.854
13	.695	.695	66	.708	.708	11	.696	45	.710	13	.826
14	.696	.698	67	.716	.711	HUB. AVAL		HUB. DROIT		14	.819
15	.697	.698	68	.718	.714	1	.703	1	.698	15	.811
16	.698	.696	69	.719	.713	2	.703	2	.699	16	.804
17	.698	.699	70	.717	.711	3	.702	3	.698	17	.805
18	.701	.702	71	.708	.707	4	.704	4	.698	18	.812
19	.700	.702	72	.705	.704	5	.702	5	.697	19	.810
20	.703	.702	73	.695	.705	6	.704	6	.698	20	.815
21	.704	.702	PRISES LAT. DROITES			7	.702	7	.697	21	.809
22	.703	.704				8	.701	8	.697	22	.812
23	.709	.705				9	.702	9	.697	23	.803
24	.709	.709	74	.698	.700	10	.703	10	.697	24	.804
25	.710	.712	75	.699	.699	11	.703	11	.697	25	.804
26	.710	.711	76	.698	.697	12	.701	12	.697	26	.811
27	.714	.711	77	.696	.695	13	.702	13	.697	27	.845
28	.716	.712	78	.697	.697	HUB. GAUCHE				28	.856
29	.720	.715	79	.699	.699	1	.710	1	.697	29	.841
30	.718	.714	80	.709	.702	2	.710	2	.697	30	.840
31	.723	.713	81	.713	.709	3	.715	3	.697	31	.803
32	.722	.718	82	.711	.714	4	.715	4	.697	32	.858
33	.724	.720	83	.717	.715	5	.715	5	.697	33	.894
34	.721	.717	84	.725	.717	6	.707	6	.697	34	.815
35	.724	.719	85	.728	.720	7	.708	7	.697	35	.811
36	.722	.719	86	.727	.721	8	.711	8	.697	36	.812
37	.723	.718	87	.727	.721	9	.714	9	.697	37	.814
38	.720	.716	88	.725	.713	10	.715	10	.697	38	.813
39	.721	.715	89	.725	.715	11	.715	11	.698	39	.819
40	.718	.713	90	.718	.712	12	.714	12	.697	40	.815
41	.718	.712	91	.718	.708	13	.713	13	.698	41	.811
42	.719	.711	92	.710	.707	14	.713	14	.698	42	.810
43	.718	.709	93	.703	.704	15	.713	15	.698	43	.812
44	.714	.703	94	.707	.702	16	.707	16	.698	44	.804
45	.714	.705	95	.700	.691	17	.707	17	.698	45	.804
46	.710	.707	96	.695	.689	18	.708	18	.698	46	.804
47	.710	.705				19	.708	19	.698	47	.807
48	.708	.705				20	.709	20	.698	48	.807
49	.707	.704				21	.709	21	.698	49	.807
50	.705	.703				22	.709	22	.698	50	.807
51	.706	.703				23	.711	23	.698		
52	.703	.701	PRISES COL			24	.709	24	.698		
53	.702	.701				25	.713	25	.698		
54	.702	.702		.757	1.149	26	.713	26	.698		
55	.692	.699		.816	1.279	27	.714	27	.698		
56	.699	.695		.871	.937	28	.715	28	.698		
57	.697	.693		.927	.793	29	.718	29	.698		
58	.692	.685		1.091	.730	30	.719	30	.698		
						31	.717	31	.697		
						32	.712	32	.697		
							.712				

***** FICHER AD115 NOÛT= 1
 20/ 8/85 11H15 AS07 M=.7 I=0 R 2-5 ADAPTE 3D L'ITE AD115
 DE AD9105 L'ITE.

MACH DE REFERENCE= .7013 UINF= 231.109 M/S
 TIV=298.7 K PIV= 1517 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.703	.701	*	PRISES DOUBLES		*	HUB. AMONT	33	.705	1		
2	.702	.705	+			+		34	.704	2		
3	.701	.702	+	59	.700	.699	1	.702	35	.704	3	
4	.699	.701	+	60	.703	.704	2	.701	36	.705	4	
5	.698	.701	+	61	.706	.704	3	.701	37	.704	5	
6	.701	.702	+				4	.701	38	.704	6	
7	.700	.700	+	PRISES LAT. GAUCHES		+	5	.699	39	.704	7	
8	.703	.700	+				6	.700	40	.705	8	
9	.704	.705	+	62	.699	.703	7	.699	41	.707	9	
10	.704	.701	+	63	.700	.707	8	.699	42	.706	10	
11	.702	.703	+	64	.707	.705	9	.700	43	.704	11	
12	.699	.704	+	65	.702	.701	10	.700	44	.703	12	
13	.701	.703	+	66	.703	.702	11	.701	45	.703	13	
14	.702	.703	+	67	.710	.704					14	
15	.703	.702	+	68	.708	.704					15	
16	.704	.701	+	69	.708	.706					16	
17	.704	.702	+	70	.715	.703	1	.707	1	.703	17	
18	.705	.704	+	71	.708	.704	2	.706	2	.703	18	
19	.702	.703	+	72	.707	.706	3	.706	3	.703	19	
20	.702	.701	+	73	.712	.710	4	.706	4	.703	20	
21	.702	.701	+				5	.705	5	.702	21	
22	.706	.702	+	PRISES LAT. DROITES		+	6	.705	6	.702	22	
23	.707	.703	+				7	.706	7	.702	23	
24	.707	.703	+	74	.700	.704	8	.707	8	.702	24	
25	.707	.704	+	75	.700	.701	9	.706	9	.703	25	
26	.707	.702	+	76	.702	.701	10	.704	10	.703	26	
27	.711	.701	+	77	.702	.701	11	.705	11	.702	27	
28	.713	.704	+	78	.702	.699					28	
29	.717	.705	+	79	.701	.699					29	
30	.715	.705	+	80	.708	.700					30	
31	.719	.703	+	81	.712	.704	1	.710	13	.702	31	
32	.715	.707	+	82	.710	.703	2	.710	14	.702	32	
33	.716	.707	+	83	.716	.703	3	.710	15	.702	33	
34	.712	.705	+	84	.724	.705	4	.705	16	.702	34	
35	.714	.706	+	85	.725	.707	5	.704	17	.702	35	
36	.713	.706	+	86	.730	.707	6	.707	18	.702	36	
37	.715	.704	+	87	.718	.706	7	.709	19	.702	37	
38	.716	.704	+	88	.718	.704	8	.712	20	.702	38	
39	.720	.703	+	89	.723	.702	9	.714	21	.702	39	
40	.717	.702	+	90	.717	.703	10	.712	22	.702	40	
41	.719	.703	+	91	.709	.705	11	.709	23	.702	41	
42	.719	.703	+	92	.712	.705	12	.709	24	.702	42	
43	.714	.704	+	93	.704	.702	13	.708	25	.702	43	
44	.708	.704	+	94	.707	.703	14	.707	26	.702	44	
45	.707	.704	+	95	.707	.693	15	.705	27	.702	45	
46	.707	.705	+	96	.711	.690	16	.704	28	.702	46	
47	.711	.704	+				17	.704	29	.702	47	
48	.710	.704	+				18	.704	30	.702	48	
49	.709	.703	+				19	.704	31	.702	49	
50	.705	.703	+				20	.705	32	.702	50	
51	.707	.704	+				21	.706	33	.702		
52	.707	.705	+				22	.706	34	.702		
53	.709	.706	+				23	.705	35	.702		
54	.710	.706	+				24	.709	36	.702		
55	.711	.702	+				25	.710	37	.702		
56	.710	.699	+				26	.711	38	.702		
57	.712	.695	+				27	.714	39	.702		
58	.713	.688	+				28	.715	40	.702		
				1.093	.710		29	.713	41	.702		
							30	.709	42	.702		
							31	.707	43	.702		
							32	.706	44	.702		
									45	.702		

***** FICHER AD115 NOCITE= 1
 20/ 8/85 11H30 A507 M=7 I=0 R 2-5 ADAPTE 3D 2'ITE. AD116
 DE AD115 1'ITE.

 MACH DE REFERENCE= .7014 UINF= 331.108 M/S
 TIV=300.2 K PIV= 1517 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				HILE A507	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.703	.701	PRISES DOUBLES			HUB. AMONT		33	.705	1	.675
2	.704	.705						34	.704	2	.690
3	.702	.703	59	.702	.701	1	.700	35	.703	3	.747
4	.699	.701	60	.704	.703	2	.699	36	.703	4	.810
5	.699	.701	61	.702	.703	3	.699	37	.703	5	.807
6	.702	.703				4	.699	38	.703	6	.770
7	.702	.702	PRISES LAT. GAUCHES			5	.697	39	.703	7	.714
8	.703	.700				6	.698	40	.704	8	.707
9	.703	.704	62	.700	.703	7	.698	41	.705	9	.884
10	.704	.700	63	.700	.706	8	.697	42	.705	10	1.055
11	.701	.701	64	.704	.705	9	.698	43	.703	11	1.009
12	.697	.701	65	.701	.701	10	.698	44	.702	12	.914
13	.698	.700	66	.705	.700	11	.699	45	.702	13	.875
14	.698	.701	67	.710	.705					14	.861
15	.699	.702	68	.708	.705	HUB. AVAL		HUB. DROIT		15	.849
16	.700	.701	69	.709	.705	1	.705	1	.702	16	.837
17	.701	.701	70	.712	.702	2	.705	2	.702	17	.833
18	.705	.700	71	.705	.701	3	.704	3	.702	18	.835
19	.704	.700	72	.706	.704	4	.705	4	.701	19	.831
20	.703	.702	73	.706	.708	5	.704	5	.701	20	.828
21	.702	.701				6	.704	6	.702	21	.816
22	.702	.699	PRISES LAT. DROITES			7	.704	7	.702	22	.812
23	.703	.696				8	.705	8	.702	23	.801
24	.706	.698	74	.700	.704	9	.705	9	.701	24	.657
25	.708	.700	75	.702	.701	10	.704	10	.701	25	.632
26	.708	.700	76	.702	.700	11	.703	11	.701	26	.741
27	.713	.701	77	.698	.699	12	.704	12	.701	27	.812
28	.713	.704	78	.699	.699	HUB. GAUCHE				28	.805
29	.715	.705	79	.702	.696	13	.702	13	.702	29	.777
30	.713	.705	80	.707	.699	14	.702	14	.702	30	.738
31	.717	.702	81	.709	.698	1	.710	15	.702	31	.729
32	.713	.707	82	.712	.699	2	.708	16	.702	32	.662
33	.716	.707	83	.713	.702	3	.708	17	.702	33	1.132
34	.712	.705	84	.704	.705	4	.703	18	.702	34	1.011
35	.714	.705	85	.725	.708	5	.703	19	.701	35	.893
36	.713	.704	86	.721	.708	6	.706	20	.701	36	.883
37	.715	.702	87	.719	.705	7	.709	21	.701	37	.875
38	.714	.701	88	.719	.703	8	.710	22	.702	38	.871
39	.718	.701	89	.721	.699	9	.712	23	.702	39	.854
40	.716	.700	90	.714	.701	10	.710	24	.702	40	.852
41	.715	.700	91	.708	.706	11	.707	25	.702	41	.844
42	.716	.701	92	.708	.702	12	.707	26	.702	42	.837
43	.712	.703	93	.702	.699	13	.708	27	.702	43	.829
44	.707	.704	94	.706	.702	14	.707	28	.702	44	.813
45	.706	.704	95	.705	.698	15	.704	29	.702	45	.795
46	.706	.705	96	.704	.696	16	.703	30	.702	46	.792
47	.708	.701				17	.703	31	.702	47	.781
48	.708	.701				18	.703	32	.702	48	.747
49	.707	.700				19	.702	33	.702	49	.737
50	.704	.701				20	.703	34	.702	50	.720
51	.705	.703				21	.704	35	.702		
52	.703	.704	PRISES COL			22	.705	36	.702		
53	.705	.705				23	.703	37	.701		
54	.707	.704				24	.707	38	.702		
55	.708	.700	.751	1.154		25	.709	39	.702		
56	.707	.696	.784	1.041		26	.710	40	.702		
57	.707	.691	.874	.861		27	.713	41	.702		
58	.703	.691	.900	.765		28	.714	42	.702		
			1.096	.711		29	.712	43	.702		
						30	.709	44	.702		
						31	.707	45	.702		
						32	.705				

***** FICHER AD117 N0(ITE)= 1
 20/ 8/85 11H50 AS07 M=.6 I=0 R 2-5 ADAPTE 30 1'ITE. AD117
 DE AD9107 1'ITE

MACH DE REFERENCE= .5983 UNF= 231.108 M/S
 TIV=300.1 K PIV= 1386 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILÉ
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I
1	.599	.597	PRISES DOUBLES			HUB. AMONT	33	.601		1
2	.600	.602					34	.600		2
3	.599	.600	59	.599	.599	1	.599	35	.599	3
4	.597	.599	60	.599	.598	2	.597	36	.599	4
5	.596	.600	61	.601	.599	3	.597	37	.599	5
6	.599	.601				4	.597	38	.599	6
7	.599	.600	PRISES LAT. GAUCHES			5	.596	39	.599	7
8	.599	.597				6	.596	40	.600	8
9	.598	.599	62	.597	.599	7	.596	41	.601	9
10	.600	.596	63	.601	.602	8	.595	42	.601	10
11	.598	.597	64	.601	.602	9	.596	43	.598	11
12	.595	.596	65	.599	.597	10	.597	44	.599	12
13	.597	.596	66	.599	.599	11	.598	45	.598	13
14	.598	.598	67	.604	.601					14
15	.599	.599	68	.604	.602	HUB. AVAL		HUB. DROIT		15
16	.598	.598	69	.604	.601					16
17	.599	.600	70	.607	.600	1	.602	1	.599	17
18	.601	.601	71	.601	.598	2	.601	2	.600	18
19	.599	.599	72	.602	.602	3	.601	3	.600	19
20	.599	.597	73	.598	.604	4	.600	4	.600	20
21	.598	.596				5	.601	5	.600	21
22	.601	.595	PRISES LAT. DROITES			6	.602	6	.600	22
23	.602	.597				7	.602	7	.600	23
24	.602	.599	74	.598	.601	8	.604	8	.600	24
25	.601	.599	75	.599	.599	9	.602	9	.600	25
26	.600	.598	76	.599	.597	10	.600	10	.599	26
27	.604	.599	77	.607	.595	11	.599	11	.599	27
28	.604	.600	78	.599	.599					28
29	.607	.601	79	.599	.595	HUB. GAUCHE				29
30	.605	.600	80	.604	.598	13	.600	13	.600	30
31	.603	.597	81	.606	.598	14	.604	14	.600	31
32	.607	.601	82	.604	.600	1	.604	15	.600	32
33	.609	.601	83	.608	.601	2	.602	16	.600	33
34	.606	.600	84	.614	.601	3	.599	17	.600	34
35	.608	.600	85	.615	.602	4	.599	18	.600	35
36	.607	.599	86	.613	.603	5	.601	19	.600	36
37	.609	.599	87	.612	.602	6	.603	20	.600	37
38	.608	.599	88	.611	.600	7	.604	21	.600	38
39	.610	.599	89	.614	.599	8	.605	22	.600	39
40	.608	.598	90	.609	.600	9	.605	23	.600	40
41	.607	.598	91	.604	.601	10	.605	24	.600	41
42	.608	.598	92	.602	.599	11	.603	25	.600	42
43	.606	.600	93	.599	.598	12	.602	26	.600	43
44	.604	.601	94	.604	.600	13	.602	27	.600	44
45	.602	.599	95	.601	.598	14	.601	28	.600	45
46	.601	.600	96	.599	.599	15	.599	29	.600	46
47	.602	.598				16	.599	30	.600	47
48	.602	.598				17	.600	31	.600	48
49	.603	.599				18	.599	32	.600	49
50	.602	.600				19	.600	33	.600	50
51	.603	.601				20	.600	34	.600	51
52	.602	.599				21	.601	35	.600	52
53	.603	.600				22	.600	36	.600	53
54	.602	.600				23	.599	37	.600	54
55	.601	.597				24	.602	38	.600	55
56	.598	.594				25	.603	39	.600	56
57	.594	.591				26	.604	40	.600	57
58	.583	.587				27	.606	41	.600	58
						28	.607	42	.600	59
						29	.606	43	.600	60
						30	.604	44	.600	
						31	.603	45	.600	
						32	.602			

***** FICHER AD113 NOCIT= 1
 20/3/85 14H35 AS07 M=3 I=0 R 2-5 ADAPTE 3D L'ITE. AD113
 DE AD9108 L'ITE.

MACH DE REFERENCE= .3059 UINFA 231.108 M/S
 TIV=300.9 K PIV= 1549 MB

MACH PAROIS HAUTE ET BASSE				MACH PAROIS LAT.ER.				FILE AS07					
I	HAUT	BAS	I	HAUT	SBS	I	MACH	I	MACH	I	MACH	I	MACH
1	.308	.305						33	.815	1	.815	1	.775
2	.306	.311						34	.815	2	.815	2	.799
3	.303	.305						35	.815	3	.815	3	.380
4	.300	.303						36	.814	4	.814	4	.389
5	.300	.303						37	.814	5	.814	5	.364
6	.304	.305						38	.813	6	.813	6	.302
7	.304	.304						39	.814	7	.814	7	.320
8	.309	.305						40	.817	8	.817	8	.320
9	.810	.813						41	.813	9	.813	9	.422
10	.311	.305						42	.817	10	.817	10	1.315
11	.307	.307						43	.814	11	.814	11	1.257
12	.303	.308						44	.813	12	.813	12	1.120
13	.305	.302						45	.813	13	.813	13	1.317
14	.305	.311						45	.812	14	.812	14	1.302
15	.307	.311								15		15	.327
16	.308	.309								16		16	.367
17	.309	.309								17		17	.365
18	.312	.309								18		18	.391
19	.310	.309								19		19	.389
20	.310	.309								20		20	.399
21	.311	.313								21		21	.379
22	.315	.311								22		22	.392
23	.313	.310								23		23	.349
24	.314	.312								24		24	.349
25	.312	.315								25		25	.377
26	.314	.314								26		26	.377
27	.321	.311								27		27	.373
28	.325	.313								28		28	.373
29	.334	.315								29		29	.373
30	.330	.315								30		30	.373
31	.337	.312								31		31	.373
32	.331	.319								32		32	.373
33	.329	.320								33		33	.373
34	.329	.320								34		34	.373
35	.329	.320								35		35	.373
36	.329	.320								36		36	.373
37	.332	.319								37		37	.373
38	.335	.317								38		38	.373
39	.331	.315								39		39	.373
40	.331	.314								40		40	.373
41	.325	.312								41		41	.373
42	.318	.311								42		42	.373
43	.317	.307								43		43	.373
44	.315	.308								44		44	.373
45	.320	.305								45		45	.373
46	.319	.308								46		46	.373
47	.320	.309								47		47	.373
48	.319	.308								48		48	.373
49	.319	.310								49		49	.373
50	.317	.315								50		50	.373
51	.315	.315								51		51	.373
52	.319	.321								52		52	.373
53	.319	.319								53		53	.373
54	.320	.317								54		54	.373
55	.318	.325								55		55	.373
56	.318	.325								56		56	.373
57	.320	.321								57		57	.373
58	.320	.321								58		58	.373
59	.320	.321								59		59	.373
60	.323	.323								60		60	.373

PRISES COL

34	1.209
35	1.117
36	.891
37	.860
38	.819
39	1.129

***** FICHER AD119 NOCIT)= I
 30/3/85 15H10 AS07 M=3 I=0 R 2-5 ADAPTE 30 2' ITR. AD119
 DE AD3118 Y'ITE.

MACH DE REFERENCE= 3049 UINF= 231.103 M/S
 TIV=301.4 K PIV= 1648 MB

MACH PAROIS HAUTE ET BASSE		MACH PAROIS LAT.		MACH PAROIS LAT.		MACH PAROIS LAT.		MACH PAROIS LAT.		MACH PAROIS LAT.	
I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS
1	.808	.807	*	PRISES DOUBLES	*	HUB. AMONT	33	.810	*	I	MACH
2	.807	.812	*		*		34	.809	*		
3	.804	.806	*	59	.803	*	35	.808	*	1	MACH
4	.801	.805	*	60	.806	*	36	.809	*	2	MACH
5	.802	.805	*	61	.805	*	37	.807	*	3	MACH
6	.805	.806	*	PRISES LAT. GAUCHES*	*	38	.807	*	4	MACH	
7	.804	.805	*		*	39	.808	*	5	MACH	
8	.808	.805	*	62	.805	*	40	.810	*	6	MACH
9	.809	.812	*	63	.798	*	41	.812	*	7	MACH
10	.807	.801	*	64	.809	*	42	.810	*	8	MACH
11	.802	.801	*	65	.806	*	43	.807	*	9	MACH
12	.799	.801	*	66	.804	*	44	.806	*	10	MACH
13	.800	.801	*	67	.803	*	45	.805	*	11	MACH
14	.799	.804	*	68	.808	*	HUB. RVAL				
15	.801	.805	*	69	.815	*	HUB. DROIT				
16	.803	.805	*	70	.817	*					
17	.805	.806	*	71	.820	*	1	.808	*	12	MACH
18	.808	.805	*	72	.810	*	2	.805	*	13	MACH
19	.808	.805	*	73	.809	*	3	.806	*	14	MACH
20	.807	.805	*	74	.814	*	4	.808	*	15	MACH
21	.806	.804	*	PRISES LAT. DROITES*	*	5	.806	*	16	MACH	
22	.807	.802	*		*	6	.805	*	17	MACH	
23	.810	.802	*	75	.804	*	7	.805	*	18	MACH
24	.811	.805	*	76	.805	*	8	.805	*	19	MACH
25	.813	.805	*	77	.808	*	9	.806	*	20	MACH
26	.813	.803	*	78	.808	*	10	.806	*	21	MACH
27	.820	.807	*	79	.801	*	11	.805	*	22	MACH
28	.827	.810	*	80	.805	*	HUB. GAUCHE			23	MACH
29	.832	.809	*	81	.813	*	1	.817	*	24	MACH
30	.830	.807	*	82	.816	*	2	.817	*	25	MACH
31	.824	.812	*	83	.814	*	3	.817	*	26	MACH
32	.828	.813	*	84	.815	*	4	.808	*	27	MACH
33	.823	.809	*	85	.810	*	5	.808	*	28	MACH
34	.827	.811	*	86	.813	*	6	.812	*	29	MACH
35	.825	.811	*	87	.818	*	7	.812	*	30	MACH
36	.824	.809	*	88	.822	*	8	.810	*	31	MACH
37	.829	.806	*	89	.804	*	9	.822	*	32	MACH
38	.823	.804	*	90	.813	*	10	.819	*	33	MACH
39	.824	.805	*	91	.816	*	11	.815	*	34	MACH
40	.821	.805	*	92	.814	*	12	.814	*	35	MACH
41	.813	.804	*	93	.804	*	13	.814	*	36	MACH
42	.811	.805	*	94	.804	*	14	.807	*	37	MACH
43	.813	.804	*	95	.804	*	15	.807	*	38	MACH
44	.811	.805	*	96	.813	*	16	.807	*	39	MACH
45	.814	.805	*	PRISES COL	*	17	.807	*	40	MACH	
46	.812	.805	*		*	18	.807	*	41	MACH	
47	.811	.805	*	845	1.133	*	19	.809	*	42	MACH
48	.809	.804	*	867	1.133	*	20	.809	*	43	MACH
49	.809	.804	*	888	.881	*	21	.809	*	44	MACH
50	.810	.799	*	910	.890	*	22	.805	*	45	MACH
51	.811	.799	*	918	.890	*	23	.805	*	46	MACH
52	.814	.800	*	1.108	.890	*	24	.805	*	47	MACH
53	.820	.800	*		*	25	.805	*	48	MACH	
54	.809	.809	*		*	26	.805	*	49	MACH	
55	.809	.809	*		*	27	.805	*	50	MACH	
56	.810	.809	*		*	28	.805	*			
57	.811	.809	*		*	29	.805	*			
58	.814	.800	*		*	30	.805	*			
59	.820	.800	*		*	31	.805	*			
60	.809	.809	*		*	32	.805	*			
61	.809	.809	*		*	33	.805	*			
62	.810	.809	*		*	34	.805	*			
63	.811	.809	*		*	35	.805	*			
64	.814	.800	*		*	36	.805	*			
65	.820	.800	*		*	37	.805	*			
66	.809	.809	*		*	38	.805	*			
67	.809	.809	*		*	39	.805	*			
68	.810	.809	*		*	40	.805	*			
69	.811	.809	*		*	41	.805	*			
70	.814	.800	*		*	42	.805	*			
71	.820	.800	*		*	43	.805	*			
72	.809	.809	*		*	44	.805	*			
73	.809	.809	*		*	45	.805	*			
74	.810	.809	*		*	46	.805	*			
75	.811	.809	*		*	47	.805	*			
76	.814	.800	*		*	48	.805	*			
77	.820	.800	*		*	49	.805	*			
78	.809	.809	*		*	50	.805	*			
79	.809	.809	*		*						
80	.810	.809	*		*						
81	.811	.809	*		*						
82	.814	.800	*		*						
83	.820	.800	*		*						
84	.809	.809	*		*						
85	.809	.809	*		*						
86	.810	.809	*		*						
87	.811	.809	*		*						
88	.814	.800	*		*						
89	.820	.800	*		*						
90	.809	.809	*		*						
91	.809	.809	*		*						
92	.810	.809	*		*						
93	.811	.809	*		*						
94	.814	.800	*		*						
95	.820	.800	*		*						
96	.809	.809	*		*						
97	.809	.809	*		*						
98	.810	.809	*		*						
99	.811	.809	*		*						
100	.814	.800	*		*						

***** FICHER AD120 NACIT= I
30/ 3/95 16H 0 HS07 M=15 I=+2 R 2-5 NON ADAPTE AD120
DE AD4 L'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .5993 UNF= 321.103 M/S
TIV=301.9 K PIV= 1395 MB

MACH PAROIS HAUTE ET BASSE				MACH PAROIS LAT. R.				MACH PAROIS LAT. L.											
I	HAUT	BAS	HAUT	BAS	I	MACH	HUB. AMONT	I	MACH	I	MACH	I	MACH	I	MACH	HAUT	BAS	HAUT	BAS
1	.500	.599	* PRISES DOUBLES	* PRISES LAT. GAUCHES	33	.505	33	33	.505	1	.504	1	.500	1	.572				
2	.500	.502	* PRISES DOUBLES	* PRISES LAT. GAUCHES	34	.505	34	34	.505	2	.504	2	.500	2	.573				
3	.599	.599	.599 .599	.599 .599	35	.503	35	35	.503	3	.504	3	.599	3	.580				
4	.599	.599	.501 .599	.501 .599	36	.504	36	36	.504	4	.599	4	.599	4	.585				
5	.599	.599	.501 .599	.501 .599	37	.503	37	37	.503	5	.599	5	.599	5	.585				
6	.599	.599	* PRISES LAT. GAUCHES	* PRISES LAT. GAUCHES	38	.503	38	38	.503	6	.503	6	.597	6	.589				
7	.500	.599	.599 .599	.599 .599	39	.503	39	39	.503	7	.597	7	.597	7	.593				
8	.500	.501	.599 .599	.599 .599	40	.504	40	40	.504	8	.597	8	.597	8	.593				
9	.500	.599	.599 .599	.599 .599	41	.504	41	41	.504	9	.597	9	.597	9	.593				
10	.599	.599	.604 .599	.604 .599	42	.502	42	42	.502	10	.597	10	.597	10	.593				
11	.599	.599	.605 .599	.605 .599	43	.502	43	43	.502	11	.597	11	.597	11	.593				
12	.596	.599	.612 .599	.612 .599	44	.501	44	44	.501	12	.593	12	.593	12	.593				
13	.598	.599	.619 .599	.619 .599	45	.501	45	45	.501	13	.593	13	.593	13	.593				
14	.599	.599	.621 .599	.621 .599	46	.501	46	46	.501	14	.593	14	.593	14	.593				
15	.501	.599	.623 .599	.623 .599	47	.503	47	47	.503	15	.593	15	.593	15	.593				
16	.502	.599	.623 .599	.623 .599	48	.503	48	48	.503	16	.593	16	.593	16	.593				
17	.505	.599	.623 .599	.623 .599	49	.504	49	49	.504	17	.593	17	.593	17	.593				
18	.505	.599	.623 .599	.623 .599	50	.504	50	50	.504	18	.593	18	.593	18	.593				
19	.505	.599	.623 .599	.623 .599	51	.504	51	51	.504	19	.593	19	.593	19	.593				
20	.506	.599	.623 .599	.623 .599	52	.504	52	52	.504	20	.593	20	.593	20	.593				
21	.611	.599	* PRISES LAT. DROITES	* PRISES LAT. DROITES	53	.504	53	53	.504	21	.593	21	.593	21	.593				
22	.614	.599	* PRISES LAT. DROITES	* PRISES LAT. DROITES	54	.504	54	54	.504	22	.593	22	.593	22	.593				
23	.614	.599	.599 .599	.599 .599	55	.504	55	55	.504	23	.593	23	.593	23	.593				
24	.610	.599	.599 .599	.599 .599	56	.503	56	56	.503	24	.593	24	.593	24	.593				
25	.611	.599	.597 .599	.597 .599	57	.501	57	57	.501	25	.593	25	.593	25	.593				
26	.622	.599	.597 .599	.597 .599	58	.501	58	58	.501	26	.593	26	.593	26	.593				
27	.622	.599	.597 .599	.597 .599	59	.504	59	59	.504	27	.593	27	.593	27	.593				
28	.625	.599	.597 .599	.597 .599	60	.504	60	60	.504	28	.593	28	.593	28	.593				
29	.627	.599	.597 .599	.597 .599	61	.504	61	61	.504	29	.593	29	.593	29	.593				
30	.627	.599	.597 .599	.597 .599	62	.504	62	62	.504	30	.593	30	.593	30	.593				
31	.627	.599	.597 .599	.597 .599	63	.504	63	63	.504	31	.593	31	.593	31	.593				
32	.627	.599	.597 .599	.597 .599	64	.504	64	64	.504	32	.593	32	.593	32	.593				
33	.627	.599	.597 .599	.597 .599	65	.504	65	65	.504	33	.593	33	.593	33	.593				
34	.627	.599	.597 .599	.597 .599	66	.504	66	66	.504	34	.593	34	.593	34	.593				
35	.627	.599	.597 .599	.597 .599	67	.504	67	67	.504	35	.593	35	.593	35	.593				
36	.627	.599	.597 .599	.597 .599	68	.504	68	68	.504	36	.593	36	.593	36	.593				
37	.627	.599	.597 .599	.597 .599	69	.504	69	69	.504	37	.593	37	.593	37	.593				
38	.627	.599	.597 .599	.597 .599	70	.504	70	70	.504	38	.593	38	.593	38	.593				
39	.627	.599	.597 .599	.597 .599	71	.504	71	71	.504	39	.593	39	.593	39	.593				
40	.627	.599	.597 .599	.597 .599	72	.504	72	72	.504	40	.593	40	.593	40	.593				
41	.627	.599	.597 .599	.597 .599	73	.593	73	73	.593	41	.593	41	.593	41	.593				
42	.627	.599	.597 .599	.597 .599	74	.593	74	74	.593	42	.593	42	.593	42	.593				
43	.627	.599	.597 .599	.597 .599	75	.593	75	75	.593	43	.593	43	.593	43	.593				
44	.627	.599	.597 .599	.597 .599	76	.593	76	76	.593	44	.593	44	.593	44	.593				
45	.627	.599	.597 .599	.597 .599	77	.593	77	77	.593	45	.593	45	.593	45	.593				
46	.627	.599	.597 .599	.597 .599	78	.593	78	78	.593	46	.593	46	.593	46	.593				
47	.627	.599	.597 .599	.597 .599	79	.593	79	79	.593	47	.593	47	.593	47	.593				
48	.627	.599	.597 .599	.597 .599	80	.593	80	80	.593	48	.593	48	.593	48	.593				
49	.627	.599	.597 .599	.597 .599	81	.593	81	81	.593	49	.593	49	.593	49	.593				
50	.627	.599	.597 .599	.597 .599	82	.593	82	82	.593	50	.593	50	.593	50	.593				
51	.627	.599	.597 .599	.597 .599	83	.593	83	83	.593	51	.593	51	.593	51	.593				
52	.627	.599	.597 .599	.597 .599	84	.593	84	84	.593	52	.593	52	.593	52	.593				
53	.627	.599	.597 .599	.597 .599	85	.593	85	85	.593	53	.593	53	.593	53	.593				
54	.627	.599	.597 .599	.597 .599	86	.593	86	86	.593	54	.593	54	.593	54	.593				
55	.627	.599	.597 .599	.597 .599	87	.593	87	87	.593	55	.593	55	.593	55	.593				
56	.627	.599	.597 .599	.597 .599	88	.593	88	88	.593	56	.593	56	.593	56	.593				
57	.627	.599	.597 .599	.597 .599	89	.593	89	89	.593	57	.593	57	.593	57	.593				
58	.627	.599	.597 .599	.597 .599	90	.593	90	90	.593	58	.593	58	.593	58	.593				

***** FICHER AD122 N0(1T)= 1
 20/ 3/85 16H50 AS07 M=.6 I=+2(+1.5+ROT.30') R 2-5 NON ADAPTE AD122
 DE AD445 1'ITE. PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .6002 UINF= 231.108 M/S
 TIV=302.0 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				MILE AS07				
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH			
1	.608	.594	*	PRISES DOUBLES		*	HUB. AMONT	33	.607	*	1	.579		
2	.608	.598	*			*		34	.605	*	2	.581		
3	.604	.598	*	59	.600	.599	*	35	.605	*	3	.629		
4	.599	.597	*	60	.601	.601	*	36	.605	*	4	.666		
5	.597	.598	*	61	.601	.603	*	37	.604	*	5	.653		
6	.600	.601	*				*	38	.604	*	6	.609		
7	.600	.600	*	PRISES LAT. GAUCHES		*	39	.603	*	7	.555			
8	.601	.598	*			*	40	.603	*	8	.510			
9	.600	.601	*	62	.601	.598	*	41	.604	*	9	.581		
10	.602	.598	*	63	.603	.604	*	42	.605	*	10	1.023		
11	.599	.599	*	64	.605	.603	*	43	.603	*	11	.538		
12	.597	.599	*	65	.607	.601	*	44	.602	*	12	.562		
13	.599	.598	*	66	.613	.599	*	45	.601	*	13	.509		
14	.600	.600	*	67	.619	.604	*			*	14	.754		
15	.601	.600	*	68	.621	.603	*	HUB. AVAL	HUB. DROIT	*	15	.765		
16	.601	.599	*	69	.621	.602	*	1	.602	*	16	.758		
17	.603	.600	*	70	.620	.601	*	2	.602	*	17	.741		
18	.606	.601	*	71	.611	.603	*	3	.604	*	18	.706		
19	.606	.601	*	72	.604	.606	*	4	.607	*	19	.723		
20	.607	.601	*	73	.579	.608	*	5	.605	*	20	.723		
21	.607	.599	*				*	6	.605	*	21	.711		
22	.611	.599	*	PRISES LAT. DROITES		*	7	.605	*	22	.792			
23	.615	.597	*			*	8	.605	*	23	.638			
24	.616	.598	*	74	.602	.600	*	9	.606	*	24	.568		
25	.620	.597	*	75	.601	.600	*	10	.606	*	25	.573		
26	.620	.598	*	76	.601	.609	*	11	.604	*	26	.623		
27	.624	.598	*	77	.599	.607	*	12	.604	*	27	.656		
28	.624	.600	*	78	.601	.608	*	13	.600	*	28	.609		
29	.627	.600	*	79	.605	.606	*	HUB. GAUCHE		*	29	.593		
30	.626	.602	*	80	.614	.597	*	14	.601	*	30	.549		
31	.630	.603	*	81	.620	.596	*	1	.600	*	31	.487		
32	.627	.602	*	82	.624	.594	*	2	.620	*	32	.549		
33	.629	.599	*	83	.628	.595	*	3	.619	*	33	1.042		
34	.626	.599	*	84	.633	.598	*	4	.611	*	34	1.045		
35	.627	.598	*	85	.635	.599	*	5	.611	*	35	.950		
36	.626	.599	*	86	.633	.599	*	6	.615	*	36	.863		
37	.627	.597	*	87	.631	.598	*	7	.613	*	37	.822		
38	.625	.597	*	88	.630	.597	*	8	.620	*	38	.804		
39	.627	.598	*	89	.631	.598	*	9	.620	*	39	.755		
40	.625	.599	*	90	.624	.600	*	10	.613	*	40	.767		
41	.624	.599	*	91	.617	.601	*	11	.615	*	41	.754		
42	.624	.600	*	92	.612	.603	*	12	.615	*	42	.741		
43	.620	.600	*	93	.605	.604	*	13	.614	*	43	.726		
44	.617	.600	*	94	.605	.603	*	14	.613	*	44	.706		
45	.615	.600	*	95	.598	.603	*	15	.608	*	45	.684		
46	.613	.602	*	96	.578	.602	*	16	.607	*	46	.579		
47	.613	.603	*				*	17	.607	*	47	.671		
48	.612	.605	*				*	18	.608	*	48	.642		
49	.609	.605	*				*	19	.608	*	49	.667		
50	.605	.605	*				*	20	.608	*	50	.638		
51	.604	.605	*				*	21	.609	*				
52	.602	.604	*	PRISES COL		*	22	.610	*	35	.601	*		
53	.600	.605	*			*	23	.608	*	36	.601	*		
54	.598	.606	*	.673	1.073	*	24	.612	*	37	.601	*		
55	.595	.605	*	.632	.896	*	25	.613	*	38	.600	*		
56	.589	.603	*	.806	.791	*	26	.614	*	39	.600	*		
57	.582	.603	*	.873	.692	*	27	.616	*	40	.600	*		
58	.571	.600	*	1.032	.632	*	28	.617	*	41	.600	*		
			*			*	29	.615	*	42	.600	*		
			*			*	30	.613	*	43	.600	*		
			*			*	31	.610	*	44	.600	*		
			*			*	32	.609	*	45	.600	*		

***** FICHER AD123 N0(1T)= 1
 20/8/85 17HIS AS07 M=.6 I=2(+1.5+ROT.30') R 2-5 ADAPTE 3D L'ITE. AD123
 DE AD9122 L'ITE.

MACH DE REFERENCE=.6002 UINF= 231.108 M/S
 TIV=001.9 K PIV= 1394 MB

MACH PAROIS HAUTE ET BASSE				MACH PAROIS LAT.ER.				MACH PAROIS LAT.ER.				MACH PAROIS LAT.ER.					
I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS
1	.608	.593															
2	.607	.597															
3	.603	.598															
4	.598	.599															
5	.600	.603															
6	.599	.600															
7	.601	.599															
8	.602	.602															
9	.600	.600															
10	.600	.600															
11	.598	.600															
12	.598	.600															
13	.600	.600															
14	.599	.601															
15	.600	.601															
16	.600	.600															
17	.604	.601															
18	.604	.601															
19	.603	.601															
20	.603	.601															
21	.603	.600															
22	.606	.602															
23	.605	.602															
24	.605	.601															
25	.605	.601															
26	.609	.599															
27	.612	.601															
28	.616	.600															
29	.613	.600															
30	.617	.597															
31	.613	.599															
32	.614	.599															
33	.611	.599															
34	.612	.599															
35	.612	.601															
36	.614	.599															
37	.613	.599															
38	.615	.598															
39	.615	.598															
40	.612	.599															
41	.613	.599															
42	.613	.599															
43	.608	.599															
44	.605	.599															
45	.605	.601															
46	.603	.602															
47	.607	.603															
48	.606	.601															
49	.606	.601															
50	.606	.601															
51	.606	.601															
52	.608	.605															
53	.608	.605															
54	.606	.605															
55	.603	.605															
56	.599	.605															
57	.592	.607															

MACH PAROIS HAUTE ET BASSE				MACH PAROIS LAT.ER.				MACH PAROIS LAT.ER.				MACH PAROIS LAT.ER.					
I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS
1	.608	.593															
2	.607	.597															
3	.603	.598															
4	.598	.599															
5	.600	.603															
6	.599	.600															
7	.601	.599															
8	.602	.602															
9	.600	.600															
10	.600	.600															
11	.598	.600															
12	.598	.600															
13	.600	.600															
14	.599	.601															
15	.600	.601															
16	.600	.600															
17	.604	.601															
18	.604	.601															
19	.603	.601															
20	.603	.601															
21	.603	.600															
22	.606	.602															
23	.605	.602															
24	.605	.601															
25	.605	.601															
26	.609	.599															
27	.612	.601															
28	.616	.600															
29	.613	.600															
30	.617	.597															
31	.613	.599															
32	.614	.599															
33	.611	.599															
34	.612	.599															
35	.612	.601															
36	.614	.599															
37	.613	.599															
38	.615	.598															
39	.615	.598															
40	.612	.599															
41	.613	.599															
42	.613	.599															
43	.608	.599															
44	.605	.599															
45	.605	.601															
46	.603	.602															
47	.607	.603															
48	.606	.601															
49	.606	.601															
50	.606	.601															
51	.606	.601															
52	.608	.605															
53	.608	.605															
54	.606	.605															
55	.603	.605															
56	.599	.605															
57	.592	.607															

***** FICHER AD124 MOXITE= 1
 21/3/95 9H35 AS07 M=7 I=2+1.5*ROT.30'> R 2-5 NON ADAPTE AD124
 DE AD+5 L'ITE. PARRIS RECTILIGNES + 30'

MACH DE REFERENCE= .7034 . VINP= 231.109 M/S
 TIV=302.4 K PIV= 1521 MB

MACH PARRIS HAUTE ET BASSE		MACH PARRIS LATERS.		AILLE #337				
I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.713	.695	+	33	+	.715	+	1
2	.712	.699	+	34	+	.714	+	2
3	.707	.700	+	35	+	.712	+	3
4	.702	.700	+	36	+	.712	+	4
5	.700	.703	+	37	+	.712	+	5
6	.702	.705	+	38	+	.711	+	6
7	.705	.703	+	39	+	.711	+	7
8	.705	.705	+	40	+	.712	+	8
9	.705	.701	+	41	+	.713	+	9
10	.701	.702	+	42	+	.713	+	10
11	.699	.702	+	43	+	.708	+	11
12	.701	.701	+	44	+	.708	+	12
13	.702	.705	+	45	+	.708	+	13
14	.704	.705	+	46	+	.708	+	14
15	.704	.705	+	47	+	.708	+	15
16	.705	.705	+	48	+	.708	+	16
17	.708	.705	+	49	+	.708	+	17
18	.712	.705	+	50	+	.708	+	18
19	.712	.705	+	51	+	.708	+	19
20	.713	.707	+	52	+	.704	+	20
21	.714	.705	+	53	+	.704	+	21
22	.711	.705	+	54	+	.704	+	22
23	.709	.702	+	55	+	.703	+	23
24	.709	.704	+	56	+	.703	+	24
25	.709	.705	+	57	+	.703	+	25
26	.704	.705	+	58	+	.703	+	26
27	.704	.705	+	59	+	.703	+	27
28	.704	.705	+	60	+	.703	+	28
29	.704	.705	+	61	+	.703	+	29
30	.704	.705	+	62	+	.703	+	30
31	.704	.705	+	63	+	.703	+	31
32	.704	.705	+	64	+	.703	+	32
33	.704	.705	+	65	+	.703	+	33
34	.704	.705	+	66	+	.703	+	34
35	.704	.705	+	67	+	.703	+	35
36	.704	.705	+	68	+	.703	+	36
37	.704	.705	+	69	+	.703	+	37
38	.704	.705	+	70	+	.703	+	38
39	.704	.705	+	71	+	.703	+	39
40	.704	.705	+	72	+	.703	+	40
41	.704	.705	+	73	+	.703	+	41
42	.704	.705	+	74	+	.703	+	42
43	.704	.705	+	75	+	.703	+	43
44	.704	.705	+	76	+	.703	+	44
45	.704	.705	+	77	+	.703	+	45
46	.704	.705	+	78	+	.703	+	46
47	.704	.705	+	79	+	.703	+	47
48	.704	.705	+	80	+	.703	+	48
49	.704	.705	+	81	+	.703	+	49
50	.704	.705	+	82	+	.703	+	50
51	.704	.705	+	83	+	.703	+	51
52	.704	.705	+	84	+	.703	+	52
53	.704	.705	+	85	+	.703	+	53
54	.704	.705	+	86	+	.703	+	54
55	.704	.705	+	87	+	.703	+	55
56	.704	.705	+	88	+	.703	+	56
57	.704	.705	+	89	+	.703	+	57
58	.704	.705	+	90	+	.703	+	58
59	.704	.705	+	91	+	.703	+	59
60	.704	.705	+	92	+	.703	+	60
61	.704	.705	+	93	+	.703	+	61
62	.704	.705	+	94	+	.703	+	62
63	.704	.705	+	95	+	.703	+	63
64	.704	.705	+	96	+	.703	+	64
65	.704	.705	+	97	+	.703	+	65
66	.704	.705	+	98	+	.703	+	66
67	.704	.705	+	99	+	.703	+	67
68	.704	.705	+	100	+	.703	+	68
69	.704	.705	+	101	+	.703	+	69
70	.704	.705	+	102	+	.703	+	70
71	.704	.705	+	103	+	.703	+	71
72	.704	.705	+	104	+	.703	+	72
73	.704	.705	+	105	+	.703	+	73
74	.704	.705	+	106	+	.703	+	74
75	.704	.705	+	107	+	.703	+	75
76	.704	.705	+	108	+	.703	+	76
77	.704	.705	+	109	+	.703	+	77
78	.704	.705	+	110	+	.703	+	78
79	.704	.705	+	111	+	.703	+	79
80	.704	.705	+	112	+	.703	+	80
81	.704	.705	+	113	+	.703	+	81
82	.704	.705	+	114	+	.703	+	82
83	.704	.705	+	115	+	.703	+	83
84	.704	.705	+	116	+	.703	+	84
85	.704	.705	+	117	+	.703	+	85
86	.704	.705	+	118	+	.703	+	86
87	.704	.705	+	119	+	.703	+	87
88	.704	.705	+	120	+	.703	+	88
89	.704	.705	+	121	+	.703	+	89
90	.704	.705	+	122	+	.703	+	90
91	.704	.705	+	123	+	.703	+	91
92	.704	.705	+	124	+	.703	+	92
93	.704	.705	+	125	+	.703	+	93
94	.704	.705	+	126	+	.703	+	94
95	.704	.705	+	127	+	.703	+	95
96	.704	.705	+	128	+	.703	+	96
97	.704	.705	+	129	+	.703	+	97
98	.704	.705	+	130	+	.703	+	98
99	.704	.705	+	131	+	.703	+	99
100	.704	.705	+	132	+	.703	+	100

***** FICHER AD125 NOCITE= 1
 85 9H50 AS07 M=.7 I=+3(+1.5+ROT.30') R 2-5 ADAPTE 3D 1'ITE. AD125
 9124 1'ITE.

 MACH DE REFERENCE= .7031 UINF= 331.103 M/S
 TIV=300.7 K PIV= 1522 MB

MACH PAROIS HAUTE ET BASSE					MACH PAROIS LATÉR.					FILE AS07		
HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH		
.713	.694	*	PRISES DOUBLES		*	HUB. AMONT	33	.705	*	1	.668	
.712	.699	**			**		34	.704	**	2	.683	
.707	.700	**	59	.701	.702	1	.702	.703	**	3	.701	
.702	.702	**	60	.705	.704	2	.701	.705	**	4	.708	
.700	.705	**	61	.706	.696	3	.701	.705	**	5	.707	
.702	.706	**			**	4	.702	.704	**	6	.707	
.702	.704	**	PRISES LAT. GAUCHES		**	5	.700	.703	**	7	.663	
.704	.702	**			**	6	.700	.703	**	8	.622	
.705	.705	**	62	.704	.702	7	.700	.704	**	9	.414	
.706	.700	**	63	.703	.706	8	.699	.704	**	10	1.391	
.703	.702	**	64	.707	.705	9	.700	.702	**	11	1.395	
.700	.702	**	65	.702	.702	10	.700	.702	**	12	.669	
.702	.702	**	66	.703	.702	11	.702	.701	**	13	.663	
.701	.704	**	67	.713	.706				**	14	.910	
.701	.704	**	68	.713	.704	HUB. AVAL		HUB. DROIT		15	.894	
.702	.702	**	69	.711	.704	1	.706	1	.704	15	.875	
.704	.702	**	70	.713	.701	2	.705	2	.704	17	.863	
.708	.703	**	71	.709	.703	3	.704	3	.703	18	.865	
.707	.702	**	72	.706	.701	4	.705	4	.703	19	.857	
.705	.703	**	73	.701	.703	5	.704	5	.703	20	.849	
.703	.702	**			**	6	.704	6	.703	21	.882	
.706	.702	**	PRISES LAT. DROITES		**	7	.704	7	.703	22	.831	
.703	.701	**			**	8	.703	8	.704	23	.806	
.706	.701	**	74	.705	.704	9	.704	9	.703	24	.875	
.703	.700	**	75	.702	.702	10	.704	10	.703	25	.871	
.703	.701	**	76	.704	.702	11	.700	11	.703	26	.879	
.715	.700	**	77	.701	.700				**	27	.731	
.716	.703	**	78	.702	.700	12	.699	12	.703	28	.756	
.723	.703	**	79	.705	.697	HUB. GAUCHE		13		.703	29	.716
.719	.704	**	80	.710	.699	1	.714	1	.703	30	.666	
.725	.700	**	81	.713	.699	2	.713	2	.703	31	.623	
.721	.704	**	82	.712	.697	3	.713	3	.703	32	.663	
.723	.703	**	83	.721	.699	4	.705	4	.703	33	1.166	
.719	.701	**	84	.731	.701	5	.705	5	.703	34	1.166	
.721	.700	**	85	.732	.703	6	.706	6	.703	35	1.108	
.713	.701	**	86	.733	.702	7	.709	7	.703	36	1.024	
.719	.699	**	87	.735	.701	8	.713	8	.703	37	.859	
.717	.699	**	88	.732	.699	9	.715	9	.703	38	.801	
.720	.699	**	89	.734	.698	10	.716	10	.703	39	.911	
.717	.700	**	90	.716	.699	11	.714	11	.703	40	.893	
.716	.699	**	91	.712	.699	12	.713	12	.703	41	.876	
.716	.699	**	92	.709	.703	13	.712	13	.704	42	.864	
.715	.698	**	93	.703	.702	14	.711	14	.704	43	.847	
.713	.699	**	94	.709	.698	15	.710	15	.704	44	.829	
.712	.699	**	95	.706	.695	16	.707	16	.703	45	.800	
.709	.701	**	96	.700	.692	17	.705	17	.703	46	.794	
.710	.703	**			**	18	.705	18	.703	47	.783	
.710	.705	**			**	19	.705	19	.703	48	.740	
.709	.704	**			**	20	.705	20	.703	49	.773	
.707	.702	**			**	21	.706	21	.703	50	.731	
.703	.700	**			**	22	.706	22	.703			
.707	.697	**	PRISES COL		**	23	.707	23	.703			
.703	.699	**			**	24	.706	24	.703			
.707	.701	**	.760	1.154	**	25	.710	25	.703			
.706	.700	**	.730	1.086	**	26	.712	26	.703			
.705	.699	**	.873	.862	**	27	.714	27	.703			
.703	.697	**	.929	.767	**	28	.717	28	.703			
.701	.691	*	1.096	.713	*	29	.718	29	.703			
						30	.715	30	.703			
						31	.711	31	.703			
						32	.709	32	.702			
							.707					

***** FICHER AD136 N0(1T)= 1
 21/ 3/85 10H 5 A307 M=.3 I=+2(+1.5+ROT.30') R 2-5 NON ADAPTE AD136
 DE AD445 1'ITE. PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .8060 UINF= 231.108 M/S
 TIV=300.3 K PIV= 1553 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE A307		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.819	.795	*	PRISES DOUBLES		HUB. AMONT	33	.839	*	1	.794	
2	.818	.800	*				34	.835	*	2	.811	
3	.811	.801	*	59	.801	.804	*	35	.832	*	3	.879
4	.804	.803	*	60	.810	.809	*	36	.827	*	4	.854
5	.800	.806	*	61	.820	.825	*	37	.823	*	5	.803
6	.802	.808	*				38	.820	*	6	.847	
7	.801	.806	*	PRISES LAT. GAUCHES			39	.831	*	7	.757	
8	.807	.806	*				40	.835	*	8	.713	
9	.809	.812	*	62	.806	.802	*	41	.849	*	9	.445
10	.811	.804	*	63	.801	.813	*	42	.840	*	10	1.458
11	.808	.806	*	64	.816	.815	*	43	.829	*	11	1.504
12	.805	.807	*	65	.824	.816	*	44	.827	*	12	1.483
13	.807	.806	*	66	.846	.824	*	45	.825	*	13	1.443
14	.806	.809	*	67	.871	.825	*			14	1.390	
15	.807	.809	*	68	.883	.825	*	HUB. AVANT	HUB. DROIT	15	1.123	
16	.808	.808	*	69	.897	.832	*			16	1.389	
17	.811	.809	*	70	.887	.831	*	1	.827	1	.805	
18	.817	.812	*	71	.847	.829	*	2	.827	2	.805	
19	.818	.813	*	72	.832	.835	*	3	.828	3	.807	
20	.820	.815	*	73	.788	.835	*	4	.835	4	.805	
21	.824	.815	*				5	.831	5	5	.805	
22	.833	.814	*	PRISES LAT. DROITES			6	.830	6	6	.805	
23	.842	.813	*				7	.828	7	7	.805	
24	.847	.819	*	74	.808	.804	*	8	.830	8	.805	
25	.853	.821	*	75	.802	.805	*	9	.832	9	.805	
26	.858	.821	*	76	.808	.805	*	10	.830	10	.805	
27	.872	.817	*	77	.807	.804	*	11	.830	11	.805	
28	.877	.821	*	78	.808	.806	*			12	.805	
29	.895	.820	*	79	.817	.805	*	HUB. GAUCHE	13	.805		
30	.891	.821	*	80	.833	.811	*			14	.805	
31	.911	.815	*	81	.851	.818	*	1	.830	15	.805	
32	.904	.824	*	82	.850	.815	*	2	.877	16	.805	
33	.920	.823	*	83	.888	.814	*	3	.874	17	.805	
34	.911	.822	*	84	.928	.815	*	4	.835	18	.805	
35	.934	.822	*	85	.934	.821	*	5	.844	19	.805	
36	.919	.825	*	86	.932	.823	*	6	.855	20	.805	
37	.932	.823	*	87	.929	.824	*	7	.871	21	.805	
38	.914	.825	*	88	.928	.822	*	8	.887	22	.805	
39	.908	.824	*	89	.902	.822	*	9	.895	23	.805	
40	.900	.824	*	90	.877	.825	*	10	.875	24	.805	
41	.898	.823	*	91	.858	.827	*	11	.867	25	.805	
42	.888	.824	*	92	.848	.830	*	12	.863	26	.805	
43	.871	.824	*	93	.831	.829	*	13	.858	27	.805	
44	.860	.827	*	94	.830	.829	*	14	.853	28	.805	
45	.855	.825	*	95	.818	.850	*	15	.828	29	.805	
46	.851	.828	*	96	.789	.848	*	16	.828	30	.805	
47	.848	.828	*				17	.830	31	.805		
48	.843	.831	*				18	.832	32	.805		
49	.838	.830	*				19	.834	33	.805		
50	.832	.831	*				20	.838	34	.805		
51	.830	.830	*				21	.841	35	.805		
52	.823	.827	*	PRISES COL			22	.845	36	.805		
53	.823	.829	*				23	.845	37	.805		
54	.822	.831	*	.881	1.233	*	24	.853	38	.805		
55	.820	.832	*	.873	.907	*	25	.859	39	.805		
56	.811	.833	*	.957	.862	*	26	.868	40	.805		
57	.798	.845	*	.999	.812	*	27	.882	41	.805		
58	.775	.864	*	1.157	.775	*	28	.891	42	.805		
			*				29	.874	43	.805		
			*				30	.856	44	.805		
			*				31	.848	45	.805		
			*				32	.843				

***** FICHER AD127 NOCIT= 1
 31/ 3/95 10H20 AS07 M=9 I=+2(+1.5+ROT.30') R 2-5 ADAPTE 3D 1'ITE. AD127
 DE AD9126 1'ITE.

MACH DE REFERENCE= .3056 UINF= 231.108 M=8
 TIV=299.9 K PIV= 1551 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07			
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH		
1	.320	.796	*	PRISES DOUBLES		*	HUB. AMONT	33	.305	*	1	.754	
2	.319	.801	+			+		34	.304	+	2	.775	
3	.312	.800	+	59	.301	.305	+	35	.302	+	3	.341	
4	.305	.803	+	60	.307	.307	+	36	.307	+	4	.313	
5	.301	.806	+	61	.304	.799	+	37	.305	+	5	.338	
6	.303	.808	+				+	38	.304	+	6	.336	
7	.301	.307	+	PRISES LAT. GAUCHES		+	39	.302	+	7	.749		
8	.306	.307	+			+	40	.302	+	8	.713		
9	.303	.812	+	62	.307	.302	+	41	.303	+	9	.438	
10	.303	.302	+	63	.799	.310	+	42	.303	+	10	1.456	
11	.305	.303	+	64	.311	.312	+	43	.301	+	11	1.474	
12	.302	.302	+	65	.307	.306	+	44	.301	+	12	1.433	
13	.304	.302	+	66	.306	.302	+	45	.300	+	13	1.365	
14	.304	.306	+	67	.310	.307	+			+	14	1.315	
15	.305	.303	+	68	.308	.302	+	HUB. AVAL	HUB. DROIT	+	15	1.315	
16	.306	.303	+	69	.312	.302	+	1	.304	+	16	1.307	
17	.307	.307	+	70	.313	.799	+	2	.302	+	17	1.313	
18	.309	.304	+	71	.307	.799	+	3	.301	+	18	1.321	
19	.309	.303	+	72	.304	.796	+	4	.302	+	19	1.313	
20	.309	.306	+	73	.309	.797	+	5	.300	+	20	1.303	
21	.307	.305	+				+	6	.306	+	21	.330	
22	.303	.302	+	PRISES LAT. DROITES		+	7	.300	+	22	.959		
23	.312	.799	+			+	8	.301	+	23	.934		
24	.312	.301	+	74	.310	.304	+	9	.300	+	24	.730	
25	.314	.303	+	75	.302	.307	+	10	.306	+	25	.733	
26	.313	.302	+	76	.306	.304	+	11	.796	+	26	.323	
27	.319	.799	+	77	.304	.300	+	12	.794	+	27	.303	
28	.313	.304	+	78	.303	.304	+	13	.306	+	28	.333	
29	.325	.305	+	79	.308	.797	+	HUB. GAUCHE	13	.306	+	29	.324
30	.319	.305	+	80	.316	.301	+	14	.306	+	30	.713	
31	.326	.799	+	81	.319	.793	+	1	.313	+	31	.723	
32	.320	.304	+	82	.313	.796	+	2	.312	+	32	.419	
33	.325	.303	+	83	.329	.793	+	3	.314	+	33	1.364	
34	.319	.799	+	84	.328	.302	+	4	.306	+	34	1.334	
35	.323	.799	+	85	.328	.304	+	5	.306	+	35	1.382	
36	.321	.793	+	86	.332	.303	+	6	.309	+	36	1.437	
37	.324	.796	+	87	.329	.300	+	7	.315	+	37	1.430	
38	.322	.796	+	88	.326	.795	+	8	.321	+	38	1.430	
39	.326	.794	+	89	.329	.793	+	9	.324	+	39	1.403	
40	.323	.794	+	90	.313	.794	+	10	.313	+	40	1.293	
41	.322	.794	+	91	.310	.797	+	11	.315	+	41	.332	
42	.323	.795	+	92	.309	.300	+	12	.314	+	42	.345	
43	.317	.795	+	93	.799	.799	+	13	.313	+	43	.330	
44	.310	.795	+	94	.306	.793	+	14	.311	+	44	.337	
45	.303	.795	+	95	.303	.796	+	15	.303	+	45	.312	
46	.306	.797	+	96	.308	.793	+	16	.306	+	46	.311	
47	.309	.799	+				+	17	.306	+	47	.332	
48	.303	.302	+				+	18	.306	+	48	.331	
49	.306	.300	+				+	19	.305	+	49	.331	
50	.304	.799	+				+	20	.306	+	50	.329	
51	.306	.795	+				+	21	.307	+			
52	.306	.790	+	PRISES COL		+	22	.303	+	35	.306		
53	.303	.792	+			+	23	.306	+	37	.305		
54	.307	.793	+	348	1.213	+	24	.311	+	38	.306		
55	.303	.793	+	363	1.213	+	25	.314	+	39	.306		
56	.303	.793	+	366	.327	+	26	.313	+	40	.306		
57	.313	.793	+	381	.321	+	27	.323	+	41	.306		
58	.315	.777	+	1.141	.730	+	28	.325	+	42	.306		
							29	.313	+	43	.306		
							30	.310	+	44	.306		
							31	.306	+	45	.306		
							32	.306	+				

***** FICHER AD123 NOCIT= 1
 21/ 8/85 10H35 AS07 M=.3 I=+2(+1.5+RDT.30') R 2-5 ADAPTE 3D 2'ITE. AD123
 DE AD9127 1'ITE.

MACH DE REFERENCE= .3053 UINF= 231.108 M/S
 TIV=299.3 K PIV= 1549 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				HAIE	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.319	.795	PRISES DOUBLES			HUB. AMONT	33	.309		1	
2	.313	.301					34	.307		2	
3	.311	.301	59	.305	.306	1	.302	35	.305	3	
4	.303	.302	60	.310	.308	2	.301	36	.307	4	
5	.300	.305	61	.303	.305	3	.301	37	.305	5	
6	.305	.309				4	.304	38	.304	6	
7	.305	.303	PRISES LAT. GAUCHES			5	.301	39	.303	7	
8	.309	.305				6	.301	40	.304	8	
9	.309	.309	62	.306	.301	7	.300	41	.307	9	
10	.311	.303	63	.301	.311	8	.799	42	.307	10	
11	.306	.304	64	.308	.310	9	.301	43	.303	11	
12	.300	.303	65	.308	.303	10	.301	44	.302	12	
13	.302	.302	66	.309	.300	11	.303	45	.300	13	
14	.302	.305	67	.322	.305					14	
15	.303	.307	68	.325	.304	HUB. AVAL		HUB. DROIT		15	
16	.303	.305	69	.331	.305	1	.303	1	.306	16	
17	.304	.305	70	.331	.302	2	.307	2	.306	17	
18	.306	.303	71	.314	.301	3	.307	3	.305	18	
19	.305	.300	72	.311	.309	4	.310	4	.305	19	
20	.307	.302	73	.305	.315	5	.309	5	.306	20	
21	.309	.302				6	.309	6	.305	21	
22	.313	.303	PRISES LAT. DROITES			7	.308	7	.305	22	
23	.317	.300				8	.309	8	.307	23	
24	.316	.300	74	.308	.304	9	.310	9	.306	24	
25	.317	.799	75	.305	.307	10	.307	10	.306	25	
26	.313	.799	76	.308	.304	11	.308	11	.305	26	
27	.326	.795	77	.302	.300					27	
28	.328	.301	78	.300	.301	HUB. GAUCHE				28	
29	.338	.301	79	.304	.794	13	.305	13	.305	29	
30	.333	.302	80	.317	.798	14	.306	14	.306	30	
31	.344	.797	81	.325	.798	1	.325	15	.305	31	
32	.338	.303	82	.322	.793	2	.325	16	.306	32	
33	.345	.302	83	.338	.794	3	.325	17	.307	33	
34	.339	.799	84	.354	.798	4	.310	18	.306	34	
35	.344	.799	85	.357	.302	5	.311	19	.306	35	
36	.342	.300	86	.353	.302	6	.317	20	.305	36	
37	.344	.793	87	.350	.300	7	.325	21	.305	37	
38	.341	.799	88	.347	.797	8	.333	22	.305	38	
39	.342	.799	89	.343	.797	9	.336	23	.305	39	
40	.337	.793	90	.329	.799	10	.328	24	.305	40	
41	.334	.793	91	.319	.301	11	.324	25	.305	41	
42	.334	.799	92	.316	.303	12	.322	26	.305	42	
43	.327	.300	93	.307	.301	13	.320	27	.305	43	
44	.319	.301	94	.310	.305	14	.317	28	.305	44	
45	.317	.300	95	.303	.305	15	.309	29	.305	45	
46	.315	.301	96	.304	.302	16	.308	30	.305	46	
47	.316	.301				17	.308	31	.305	47	
48	.316	.304				18	.308	32	.305	48	
49	.316	.303				19	.308	33	.305	49	
50	.312	.305				20	.309	34	.305	50	
51	.311	.307				21	.311	35	.305		
52	.305	.305	PRISES COL			22	.312	36	.305		
53	.307	.310				23	.312	37	.305		
54	.308	.310	.353	1.220		24	.317	38	.305		
55	.309	.303	.366	.989		25	.321	39	.305		
56	.307	.305	.342	.381		26	.325	40	.305		
57	.307	.305	.395	.319		27	.333	41	.305		
58	.305	.303	1.147	.777		28	.335	42	.305		
						29	.327	43	.305		
						30	.318	44	.305		
						31	.313	45	.305		
						32	.311				

***** FICHER AD129 N0(1T)= 1
 21/ 3/85 10450 AS07 M=.8 I=+2(+1.5+ROT.30') R 2-5 ADAPTE 3D 3'ITE. AD129
 DE AD9128 1'ITE.

MACH DE REFERENCE= .8059 UINF= 231.108 M/S
 TIV=299.3 K PIV= 1649 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				RILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.820	.797	*	PRISES DOUBLES		*	HUB. AMONT	33	.810	*	1	.763
2	.820	.803	*			*		34	.809	*	2	.781
3	.814	.803	*	59	.803	.805	*	1	.805	*	3	.845
4	.806	.804	*	60	.807	.808	*	2	.803	*	4	.832
5	.802	.806	*	61	.808	.805	*	3	.803	*	5	.800
6	.805	.810	*			*		4	.805	*	6	.827
7	.803	.806	*	PRISES LAT. GAUCHES		*		5	.802	*	7	.747
8	.805	.803	*			*		6	.802	*	8	.712
9	.806	.808	*	62	.809	.805	*	7	.801	*	9	.441
10	.808	.803	*	63	.799	.812	*	8	.800	*	10	1.475
11	.805	.806	*	64	.812	.809	*	9	.802	*	11	1.479
12	.801	.807	*	65	.807	.806	*	10	.802	*	12	1.434
13	.804	.805	*	66	.806	.805	*	11	.803	*	13	1.364
14	.805	.808	*	67	.824	.809	*			*	14	1.059
15	.807	.807	*	68	.824	.804	*	HUB. AVAL	HUB. DROIT	*	15	1.333
16	.807	.804	*	69	.829	.805	*			*	16	1.314
17	.807	.803	*	70	.832	.805	*	1	.811	*	17	1.824
18	.810	.805	*	71	.815	.802	*	2	.809	*	18	1.840
19	.808	.805	*	72	.812	.810	*	3	.809	*	19	1.839
20	.807	.807	*	73	.810	.814	*	4	.811	*	20	1.829
21	.808	.805	*			*		5	.809	*	21	1.801
22	.812	.802	*	PRISES LAT. DROITES		*		6	.809	*	22	.974
23	.816	.799	*			*		7	.809	*	23	.946
24	.813	.803	*	74	.811	.806	*	8	.810	*	24	.723
25	.814	.805	*	75	.804	.808	*	9	.811	*	25	.761
26	.815	.805	*	76	.806	.805	*	10	.807	*	26	.832
27	.825	.802	*	77	.804	.803	*	11	.807	*	27	.809
28	.828	.805	*	78	.805	.801	*			*	28	.809
29	.849	.805	*	79	.807	.798	*	HUB. GAUCHE		*	29	.823
30	.835	.805	*	80	.816	.801	*			*	30	.756
31	.845	.799	*	81	.824	.797	*	1	.825	*	31	.723
32	.838	.805	*	82	.819	.800	*	2	.825	*	32	.437
33	.844	.803	*	83	.826	.799	*	3	.825	*	33	1.576
34	.837	.800	*	84	.854	.801	*	4	.810	*	34	1.584
35	.841	.799	*	85	.857	.804	*	5	.812	*	35	1.581
36	.839	.800	*	86	.851	.803	*	6	.817	*	36	1.510
37	.842	.798	*	87	.847	.801	*	7	.825	*	37	1.474
38	.840	.800	*	88	.844	.798	*	8	.833	*	38	1.455
39	.843	.799	*	89	.845	.799	*	9	.835	*	39	1.440
40	.838	.800	*	90	.831	.802	*	10	.823	*	40	1.423
41	.835	.800	*	91	.817	.804	*	11	.824	*	41	1.383
42	.835	.801	*	92	.816	.803	*	12	.823	*	42	1.339
43	.826	.802	*	93	.807	.803	*	13	.820	*	43	.944
44	.817	.803	*	94	.813	.806	*	14	.818	*	44	.892
45	.815	.802	*	95	.808	.791	*	15	.810	*	45	.913
46	.813	.802	*	96	.808	.787	*	16	.808	*	46	.913
47	.816	.801	*			*		17	.809	*	47	.911
48	.817	.804	*			*		18	.810	*	48	.896
49	.815	.805	*			*		19	.810	*	49	.895
50	.812	.807	*			*		20	.811	*	50	.835
51	.813	.809	*			*		21	.812	*		
52	.811	.806	*	PRISES COL		*		22	.814	*		
53	.811	.809	*			*		23	.812	*		
54	.812	.810	*	.860	1.219	*		24	.818	*		
55	.813	.806	*	.868	.867	*		25	.822	*		
56	.811	.802	*	.843	.876	*		26	.827	*		
57	.811	.796	*	.895	.817	*		27	.833	*		
58	.811	.776	*	1.146	.777	*		28	.835	*		
			*			*		29	.827	*		
			*			*		30	.819	*		
			*			*		31	.814	*		
			*			*		32	.812	*		

***** FICHER AD130 NO(CIT)= 4
 21/3/85 12H20 AS07 M=7 I=1.5 R 2-5 ADAPTE 2D AD130
 DE AD4 L'ITE. PAROIS RECTILIGNES SYMETRIQUES

 MACH DE REFERENCE= .7071 UINF= 231.109 M/S
 TIV=294.0 K PIV= 1525 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.706	.702	PRISES DOUBLES			HUB. AMONT	33	.707	33	.707	1	.707
2	.707	.707					34	.706	34	.706	2	.706
3	.707	.705	59	.705	.704	1	.705	35	.705	3	.705	
4	.704	.704	60	.709	.703	2	.704	36	.706	4	.706	
5	.704	.705	61	.706	.703	3	.704	37	.706	5	.706	
6	.707	.707					4	.704	38	.705	6	.705
7	.706	.705	PRISES LAT. GAUCHES				5	.703	39	.704	7	.704
8	.705	.702					6	.703	40	.705	8	.705
9	.706	.705	62	.705	.705	7	.703	41	.705	9	.705	
10	.708	.700	63	.705	.709	8	.702	42	.706	10	.706	
11	.707	.701	64	.710	.709	9	.703	43	.704	11	.704	
12	.705	.703	65	.710	.704	10	.703	44	.703	12	.703	
13	.706	.705	66	.710	.701	11	.703	45	.703	13	.703	
14	.707	.709	67	.719	.706	HUB. AVAL		HUB. DROIT		14	.703	
15	.707	.711	68	.716	.705	1	.708	1	.705	15	.703	
16	.707	.706	69	.715	.705	2	.707	2	.705	16	.703	
17	.707	.704	70	.720	.703	3	.707	3	.705	17	.703	
18	.710	.704	71	.714	.703	4	.709	4	.706	18	.703	
19	.709	.703	72	.709	.707	5	.707	5	.705	19	.703	
20	.709	.704	73	.693	.710	6	.707	6	.705	20	.703	
21	.711	.703					7	.707	7	.705	21	.703
22	.715	.702	PRISES LAT. DROITES				8	.707	8	.706	22	.703
23	.713	.700					9	.707	9	.706	23	.703
24	.716	.701	74	.706	.707	10	.708	10	.706	24	.703	
25	.717	.701	75	.706	.705	11	.708	11	.706	25	.703	
26	.717	.701	76	.707	.699	12	.705	12	.706	26	.703	
27	.723	.700	77	.706	.703	13	.705	13	.705	27	.703	
28	.724	.703	78	.706	.699	HUB. GAUCHE				28	.705	
29	.730	.704	79	.707	.698	1	.713	1	.705	29	.705	
30	.726	.704	80	.713	.709	2	.713	2	.705	30	.705	
31	.731	.700	81	.725	.699	3	.713	3	.706	31	.705	
32	.726	.705	82	.722	.697	4	.713	4	.706	32	.705	
33	.728	.704	83	.730	.693	5	.711	5	.706	33	.705	
34	.723	.702	84	.730	.701	6	.711	6	.706	34	.705	
35	.725	.702	85	.739	.703	7	.711	7	.706	35	.705	
36	.733	.703	86	.733	.703	8	.714	8	.705	36	.705	
37	.735	.701	87	.729	.702	9	.717	9	.706	37	.705	
38	.724	.702	88	.722	.700	10	.720	10	.706	38	.705	
39	.727	.701	89	.731	.700	11	.721	11	.706	39	.705	
40	.724	.701	90	.724	.703	12	.719	12	.705	40	.705	
41	.724	.702	91	.713	.704	13	.717	13	.705	41	.705	
42	.724	.702	92	.715	.703	14	.716	14	.705	42	.705	
43	.721	.703	93	.706	.703	15	.715	15	.705	43	.705	
44	.718	.704	94	.707	.704	16	.713	16	.705	44	.705	
45	.717	.703	95	.705	.704	17	.713	17	.705	45	.705	
46	.715	.704	96	.691	.701	18	.708	18	.705	46	.705	
47	.716	.703					19	.708	19	.705	47	.705
48	.715	.705					20	.709	20	.705	48	.705
49	.713	.705					21	.708	21	.705	49	.705
50	.708	.706					22	.709	22	.705	50	.705
51	.709	.706					23	.710	23	.705	51	.705
52	.708	.704	PRISES COL				24	.711	24	.705	52	.705
53	.708	.706					25	.709	25	.705	53	.705
54	.708	.707	1.781	1.155		26	.713	26	.705	54	.705	
55	.707	.705	1.795	1.062		27	.714	27	.705	55	.705	
56	.702	.703	1.875	.983		28	.717	28	.705	56	.705	
57	.696	.703	1.931	.771		29	.719	29	.705	57	.705	
58	.685	.703	1.896	.713		30	.721	30	.705	58	.705	
						31	.718	31	.705			
						32	.714	32	.705			
						33	.711	33	.705			
						34	.709	34	.705			

***** FICHER AD131 NO(IT)= 4
 21/ 3/85 14H50 AS07 M=.6 I=1.5 R 2-5 ADAPTE 3D AD131
 DE AD130 4'ITE.

MACH DE REFERENCE= .6019 UINF= 231.108 M/S
 TIV=296.4 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.604	.600	PRISES DOUBLES			HUB.	AMONT	33	.603	1	.672	
2	.604	.603						34	.602	2	.681	
3	.603	.601	59	.602	.600	1	.602	35	.601	3	.628	
4	.601	.601	60	.604	.600	2	.601	36	.602	4	.669	
5	.601	.602	61	.602	.599	3	.601	37	.602	5	.658	
6	.603	.603				4	.601	38	.601	6	.617	
7	.602	.601	PRISES LAT. GAUCHES			5	.600	39	.600	7	.566	
8	.603	.601				6	.600	40	.601	8	.528	
9	.602	.602	62	.602	.602	7	.600	41	.601	9	.675	
10	.604	.598	63	.605	.604	8	.599	42	.601	10	1.021	
11	.602	.597	64	.603	.603	9	.600	43	.599	11	.886	
12	.601	.599	65	.605	.601	10	.599	44	.599	12	.828	
13	.602	.600	66	.606	.599	11	.600	45	.599	13	.784	
14	.601	.602	67	.609	.602					14	.755	
15	.602	.605	68	.609	.601	HUB.	AVAL	HUB.	DROIT	15	.750	
16	.602	.601	69	.609	.602	1	.604	1	.602	16	.735	
17	.601	.598	70	.612	.599	2	.603	2	.602	17	.728	
18	.603	.598	71	.607	.600	3	.604	3	.601	18	.726	
19	.603	.598	72	.604	.602	4	.604	4	.602	19	.719	
20	.605	.601	73	.596	.603	5	.603	5	.602	20	.711	
21	.605	.600				6	.603	6	.602	21	.699	
22	.607	.599	PRISES LAT. DROITES			7	.603	7	.602	22	.691	
23	.608	.597				8	.605	8	.601	23	.682	
24	.608	.597	74	.603	.603	9	.603	9	.602	24	.680	
25	.610	.597	75	.602	.602	10	.602	10	.602	25	.675	
26	.609	.597	76	.602	.597	11	.602	11	.602	26	.632	
27	.613	.596	77	.602	.603	12	.602	12	.602	27	.661	
28	.613	.599	78	.600	.595	13	.602	13	.602	28	.646	
29	.616	.599	79	.602	.594	HUB. GAUCHE			14	.601	29	.604
30	.614	.599	80	.612	.598	1	.610	15	.602	30	.566	
31	.617	.596	81	.613	.595	2	.609	16	.602	31	.621	
32	.614	.599	82	.614	.595	3	.609	17	.601	32	.640	
33	.616	.599	83	.618	.596	4	.605	18	.602	33	1.108	
34	.613	.599	84	.622	.597	5	.605	19	.602	34	.986	
35	.615	.598	85	.623	.599	6	.605	20	.601	35	.861	
36	.613	.599	86	.620	.599	7	.608	21	.602	36	.806	
37	.615	.598	87	.619	.599	8	.609	22	.602	37	.785	
38	.615	.598	88	.618	.598	9	.611	23	.602	38	.773	
39	.617	.598	89	.621	.598	10	.612	24	.602	39	.760	
40	.615	.598	90	.616	.599	11	.611	25	.602	40	.746	
41	.615	.598	91	.618	.600	12	.609	26	.602	41	.734	
42	.615	.599	92	.608	.599	13	.609	27	.601	42	.727	
43	.613	.599	93	.602	.599	14	.607	28	.602	43	.713	
44	.610	.599	94	.603	.600	15	.607	29	.601	44	.697	
45	.608	.599	95	.601	.595	16	.604	30	.601	45	.678	
46	.607	.599	96	.593	.593	17	.603	31	.602	46	.674	
47	.609	.599				18	.603	32	.602	47	.665	
48	.608	.600				19	.604	33	.602	48	.638	
49	.606	.600				20	.603	34	.602	49	.663	
50	.603	.600				21	.603	35	.602	50	.635	
51	.604	.601				22	.604	36	.602			
52	.603	.600	PRISES COL			23	.605	37	.602			
53	.604	.601				24	.603	38	.602			
54	.604	.601	.663	1.060		25	.607	39	.602			
55	.602	.599	.698	.912		26	.608	40	.601			
56	.608	.598	.799	.797		27	.608	41	.602			
57	.597	.596	.865	.694		28	.611	42	.602			
58	.593	.593	1.024	.634		29	.611	43	.602			
						30	.609	44	.601			
						31	.608	45	.601			
						32	.604		.602			

***** FICHER AD133 HAUT= 4
21/3x35 1SH55 AS07 M=3 I=0 R=25 ADAPTE 2D AD133
DE AD4 1.1TE. PAROIS RECTILICHES SYMETRIQUES

MACH DE REFERENCE= .8073 UINF= 231.102 M/S
TIV=295.2 K PIV= 1553 MB

MACH PAROIS HAUTE ET BASSE		MACH PAROIS LATÉR.			AILS AS07				
I	HAUT	BAS	I	HAUT	SBS	I	MACH	I	MACH
1	.809	.804	+	PRISES DOUBLES		+	.813	33	.813
1	.811	.812	+			+	.812	34	.812
2	.809	.805	+	59	.810	+	.811	35	.811
3	.804	.805	+	60	.810	+	.811	36	.811
4	.803	.807	+	61	.804	+	.811	37	.811
5	.810	.812	+			+	.811	38	.811
5	.810	.812	+	PRISES LAT. GAUCHES*		+	.811	39	.811
6	.809	.807	+	63	.805	+	.801	40	.812
6	.809	.809	+	63	.802	+	.801	41	.813
10	.811	.798	+	64	.812	+	.800	42	.812
11	.806	.797	+	64	.813	+	.801	43	.810
12	.800	.798	+	65	.811	+	.801	43	.809
12	.802	.803	+	66	.815	+	.801	44	.809
14	.803	.812	+	67	.821	+	.802	45	.808
15	.805	.819	+	68	.819	+			
15	.806	.808	+	68	.821	+			
17	.807	.802	+	70	.824	+			
18	.810	.802	+	71	.814	+			
19	.808	.802	+	72	.812	+			
19	.809	.807	+	73	.818	+			
20	.809	.806	+			+			
20	.813	.803	+	PRISES LAT. DROITES*		+			
20	.817	.801	+	74	.807	+			
21	.819	.805	+	75	.811	+			
21	.820	.809	+	76	.809	+			
21	.821	.807	+	77	.803	+			
21	.826	.807	+	78	.803	+			
22	.826	.810	+	79	.805	+			
22	.827	.811	+	80	.807	+			
22	.835	.809	+	81	.813	+			
23	.835	.814	+	82	.805	+			
23	.835	.814	+	83	.803	+			
23	.831	.810	+	84	.804	+			
23	.834	.811	+	85	.804	+			
23	.836	.805	+	86	.804	+			
23	.832	.808	+	87	.804	+			
23	.834	.806	+	88	.807	+			
24	.827	.804	+	89	.809	+			
24	.827	.804	+	91	.817	+			
24	.8215	.803	+	92	.809	+			
24	.816	.806	+	93	.803	+			
25	.810	.806	+	94	.805	+			
25	.811	.805	+	95	.807	+			
25	.806	.807	+	96	.805	+			
25	.809	.809	+	97	.805	+			
25	.810	.805	+	98	.805	+			
25	.812	.805	+	99	.804	+			
25	.816	.803	+	100	.804	+			
25	.810	.805	+	101	.804	+			
25	.810	.805	+	102	.805	+			
25	.816	.806	+	103	.804	+			
25	.816	.806	+	104	.804	+			
25	.816	.805	+	105	.804	+			
25	.812	.805	+	106	.804	+			
25	.810	.803	+	107	.804	+			
25	.816	.806	+	108	.804	+			
25	.816	.806	+	109	.804	+			
25	.816	.806	+	110	.804	+			
25	.816	.805	+	111	.804	+			
25	.807	.807	+	112	.803	+			
25	.809	.810	+	113	.803	+			
25	.804	.803	+	114	.803	+			
25	.804	.803	+	115	.803	+			
25	.804	.803	+	116	.803	+			
25	.804	.803	+	117	.803	+			
25	.804	.803	+	118	.803	+			
25	.804	.803	+	119	.803	+			
25	.804	.803	+	120	.803	+			
25	.804	.803	+	121	.803	+			
25	.804	.803	+	122	.803	+			
25	.804	.803	+	123	.803	+			
25	.804	.803	+	124	.803	+			
25	.804	.803	+	125	.803	+			
25	.804	.803	+	126	.803	+			
25	.804	.803	+	127	.803	+			
25	.804	.803	+	128	.803	+			
25	.804	.803	+	129	.803	+			
25	.804	.803	+	130	.803	+			
25	.804	.803	+	131	.803	+			
25	.804	.803	+	132	.803	+			
25	.804	.803	+	133	.803	+			
25	.804	.803	+	134	.803	+			
25	.804	.803	+	135	.803	+			
25	.804	.803	+	136	.803	+			
25	.804	.803	+	137	.803	+			
25	.804	.803	+	138	.803	+			
25	.804	.803	+	139	.803	+			
25	.804	.803	+	140	.803	+			
25	.804	.803	+	141	.803	+			
25	.804	.803	+	142	.803	+			
25	.804	.803	+	143	.803	+			
25	.804	.803	+	144	.803	+			
25	.804	.803	+	145	.803	+			
25	.804	.803	+	146	.803	+			
25	.804	.803	+	147	.803	+			
25	.804	.803	+	148	.803	+			
25	.804	.803	+	149	.803	+			
25	.804	.803	+	150	.803	+			
25	.804	.803	+	151	.803	+			
25	.804	.803	+	152	.803	+			
25	.804	.803	+	153	.803	+			
25	.804	.803	+	154	.803	+			
25	.804	.803	+	155	.803	+			
25	.804	.803	+	156	.803	+			
25	.804	.803	+	157	.803	+			
25	.804	.803	+	158	.803	+			
25	.804	.803	+	159	.803	+			
25	.804	.803	+	160	.803	+			
25	.804	.803	+	161	.803	+			
25	.804	.803	+	162	.803	+			
25	.804	.803	+	163	.803	+			
25	.804	.803	+	164	.803	+			
25	.804	.803	+	165	.803	+			
25	.804	.803	+	166	.803	+			
25	.804	.803	+	167	.803	+			
25	.804	.803	+	168	.803	+			
25	.804	.803	+	169	.803	+			
25	.804	.803	+	170	.803	+			
25	.804	.803	+	171	.803	+			
25	.804	.803	+	172	.803	+			
25	.804	.803	+	173	.803	+			
25	.804	.803	+	174	.803	+			
25	.804	.803	+	175	.803	+			
25	.804	.803	+	176	.803	+			
25	.804	.803	+	177	.803	+			
25	.804	.803	+	178	.803	+			
25	.804	.803	+	179	.803	+			
25	.804	.803	+	180	.803	+			
25	.804	.803	+	181	.803	+			
25	.804	.803	+	182	.803	+			
25	.804	.803	+	183	.803	+			
25	.804	.803	+	184	.803	+			
25	.804	.803	+	185	.803	+			
25	.804	.803	+	186	.803	+			
25	.804	.803	+	187	.803	+			
25	.804	.803	+	188	.803	+			
25	.804	.803	+	189	.803	+			
25	.804	.803	+	190	.803	+			
25	.804	.803	+	191	.803	+			
25	.804	.803	+	192	.803	+			
25	.804	.803	+	193	.803	+			
25	.804	.803	+	194	.803	+			
25	.804	.803	+	195	.803	+			
25	.804	.803	+	196	.803	+			
25	.804	.803	+	197	.803	+			
25	.804	.803	+	198	.803	+			
25	.804	.803	+	199	.803	+			
25	.804	.803	+	200	.803	+			
25	.804	.803	+	201	.803	+			
25	.804	.803	+	202	.803	+			
25	.804	.803	+	203	.803	+			
25	.804	.803	+	204	.803	+			
25	.804	.803	+	205	.803</				

***** FICHER AD134 NO(IT)= 4
 21/ 3/85 17H15 AS07 M=3 I=0 R 2-5 ADAPTE 2D AD134
 DE AD133 4'ITE

 MACH DE REFERENCE= .8085 UINF= 231.108 M/S
 TIV=297.1 K PIV= 1552 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07				
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH			
1	.811	.805	*	PRISES DOUBLES		*	HUB. AMONT	33	.813	*	1	.774		
2	.814	.814	*			*		34	.812	*	2	.797		
3	.812	.812	*	59	.809	.810	*	1	.806	*	3	.872		
4	.806	.808	*	50	.809	.807	*	2	.804	*	4	.950		
5	.805	.809	*	61	.804	.800	*	3	.803	*	5	.944		
6	.811	.813	*				*	4	.804	*	6	.885		
7	.809	.811	*	PRISES LAT. GAUCHES		*	5	.802	39	.810	*	7	.804	
8	.807	.804	*				*	6	.802	40	.812	*	8	.795
9	.806	.806	*	62	.809	.809	*	7	.802	41	.814	*	9	.424
10	.810	.802	*	63	.800	.812	*	8	.800	42	.812	*	10	1.359
11	.806	.805	*	64	.813	.807	*	9	.802	43	.809	*	11	1.332
12	.801	.805	*	65	.809	.807	*	10	.802	44	.808	*	12	1.233
13	.803	.805	*	66	.815	.806	*	11	.802	45	.807	*	13	1.019
14	.805	.809	*	67	.820	.809	*				*	14	1.012	
15	.807	.808	*	68	.822	.809	*	HUB. AVAL	HUB. DROIT	15	1.806			
16	.808	.802	*	69	.825	.811	*			16	.895			
17	.809	.801	*	70	.824	.809	*	1	.808	1	.808	*	17	.895
18	.811	.803	*	71	.814	.804	*	2	.808	2	.808	*	18	1.001
19	.808	.804	*	72	.810	.807	*	3	.807	3	.808	*	19	.998
20	.807	.808	*	73	.797	.815	*	4	.810	4	.808	*	20	1.000
21	.807	.807	*				*	5	.807	5	.808	*	21	.981
22	.814	.804	*	PRISES LAT. DROITES		*	6	.807	6	.808	*	22	.957	
23	.819	.801	*				*	7	.807	7	.808	*	23	.944
24	.820	.805	*	74	.810	.814	*	8	.808	8	.808	*	24	.749
25	.821	.809	*	75	.810	.811	*	9	.809	9	.808	*	25	.779
26	.821	.809	*	76	.807	.803	*	10	.806	10	.808	*	26	.860
27	.826	.807	*	77	.804	.805	*	11	.806	11	.808	*	27	.957
28	.826	.810	*	78	.807	.798	*			12	.808	*	28	.947
29	.832	.811	*	79	.806	.799	*	HUB. GAUCHE	13	.808	*	29	.891	
30	.827	.811	*	80	.814	.805	*		14	.808	*	30	.843	
31	.835	.807	*	81	.827	.802	*	1	.823	15	.808	*	31	.826
32	.831	.813	*	82	.824	.807	*	2	.823	16	.808	*	32	.410
33	.837	.813	*	83	.834	.807	*	3	.822	17	.808	*	33	1.523
34	.832	.809	*	84	.844	.810	*	4	.812	18	.808	*	34	1.454
35	.836	.809	*	85	.846	.814	*	5	.813	19	.808	*	35	1.380
36	.834	.810	*	86	.843	.813	*	6	.817	20	.808	*	36	1.266
37	.836	.808	*	87	.842	.810	*	7	.822	21	.808	*	37	1.005
38	.833	.809	*	88	.839	.808	*	8	.825	22	.808	*	38	1.029
39	.835	.809	*	89	.838	.807	*	9	.827	23	.808	*	39	1.050
40	.829	.808	*	90	.825	.808	*	10	.823	24	.808	*	40	1.029
41	.827	.808	*	91	.817	.807	*	11	.821	25	.808	*	41	1.008
42	.828	.807	*	92	.817	.804	*	12	.820	26	.808	*	42	1.000
43	.822	.807	*	93	.807	.805	*	13	.819	27	.808	*	43	.887
44	.816	.806	*	94	.810	.804	*	14	.818	28	.808	*	44	.959
45	.815	.804	*	95	.805	.796	*	15	.812	29	.808	*	45	.927
46	.813	.805	*	96	.795	.793	*	16	.810	30	.808	*	46	.921
47	.816	.803	*				*	17	.810	31	.808	*	47	.912
48	.816	.806	*				*	18	.811	32	.808	*	48	.840
49	.815	.806	*				*	19	.811	33	.808	*	49	.900
50	.810	.806	*				*	20	.812	34	.808	*	50	.830
51	.810	.805	*				*	21	.813	35	.808	*		
52	.806	.801	*	PRISES COL		*	22	.815	36	.808	*			
53	.809	.807	*				*	23	.813	37	.808	*		
54	.810	.810	*	.859	1.217		*	24	.818	38	.808	*		
55	.810	.807	*	.873	1.189		*	25	.820	39	.808	*		
56	.805	.803	*	.942	.895		*	26	.823	40	.808	*		
57	.801	.799	*	.985	.823		*	27	.827	41	.808	*		
58	.793	.797	*	1.144	.792		*	28	.829	42	.808	*		
			*				*	29	.824	43	.808	*		
			*				*	30	.816	44	.808	*		
			*				*	31	.812	45	.808	*		
			*				*	32	.814			*		

***** FICHER AD135 N0(1T)= 4
 22/ 8/85 9H30 AS07 M=.7 I=0 R 2-5 ADAPTE 2D AD135
 DE AD134 4'ITE

MACH DE REFERENCE= .7021 UINF= 231.108 M/S
 TIV=297.2 K PIV= 1521 MB

MACH PARDIS HAUTE ET BASSE						MACH PARDIS LAT.				FILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.703	.700	*	PRISES DOUBLES		*	HUB. AMONT	33	.704	*	1	.672
2	.704	.704	*			*		34	.703	*	2	.639
3	.703	.702	*	59	.700	.701	*	35	.702	*	3	.742
4	.700	.702	*	60	.703	.700	*	36	.703	*	4	.600
5	.699	.703	*	61	.702	.701	*	37	.702	*	5	.797
6	.702	.704	*				*	38	.702	*	6	.752
7	.701	.702	*	PRISES LAT. GAUCHES		*		39	.702	*	7	.707
8	.702	.700	*			*		40	.703	*	8	.691
9	.702	.702	*	62	.701	.703	*	41	.704	*	9	.696
10	.704	.697	*	63	.701	.704	*	42	.704	*	10	1.033
11	.702	.697	*	64	.704	.705	*	43	.702	*	11	1.054
12	.699	.698	*	65	.706	.701	*	44	.701	*	12	.935
13	.701	.698	*	66	.703	.696	*	45	.700	*	13	.897
14	.701	.700	*	67	.713	.702	*			*	14	.870
15	.701	.702	*	68	.710	.701	*	HUB. AVAIL	HUB. DROIT	*	15	.858
16	.701	.702	*	69	.710	.702	*			*	16	.845
17	.701	.702	*	70	.715	.702	*	1	.704	1	.702	.842
18	.704	.699	*	71	.707	.700	*	2	.703	2	.702	.843
19	.704	.698	*	72	.703	.702	*	3	.703	3	.702	.838
20	.707	.700	*	73	.695	.705	*	4	.704	4	.702	.835
21	.706	.701	*				*	5	.702	5	.702	.822
22	.707	.701	*	PRISES LAT. DROITES		*		6	.703	6	.702	.813
23	.707	.700	*			*		7	.702	7	.702	.803
24	.706	.699	*	74	.702	.704	*	8	.703	8	.702	.657
25	.708	.699	*	75	.701	.703	*	9	.704	9	.702	.690
26	.708	.699	*	76	.702	.697	*	10	.702	10	.702	.738
27	.714	.699	*	77	.701	.697	*	11	.702	11	.702	.795
28	.716	.703	*	78	.699	.698	*			12	.702	.792
29	.721	.704	*	79	.703	.695	*	HUB. GAUCHE		13	.702	.759
30	.718	.704	*	80	.712	.699	*			14	.702	.725
31	.722	.701	*	81	.712	.701	*	1	.711	15	.701	.707
32	.717	.704	*	82	.711	.698	*	2	.711	16	.702	.698
33	.719	.704	*	83	.719	.698	*	3	.710	17	.702	1.195
34	.714	.701	*	84	.723	.701	*	4	.704	18	.702	1.075
35	.715	.701	*	85	.723	.704	*	5	.705	19	.702	.922
36	.714	.701	*	86	.723	.703	*	6	.707	20	.702	.894
37	.717	.700	*	87	.720	.702	*	7	.710	21	.702	.886
38	.717	.700	*	88	.719	.700	*	8	.712	22	.702	.979
39	.721	.700	*	89	.725	.699	*	9	.713	23	.702	.869
40	.718	.700	*	90	.718	.701	*	10	.711	24	.702	.856
41	.718	.700	*	91	.708	.703	*	11	.710	25	.701	.844
42	.718	.700	*	92	.709	.701	*	12	.709	26	.701	.838
43	.713	.701	*	93	.702	.699	*	13	.708	27	.701	.829
44	.708	.702	*	94	.704	.700	*	14	.708	28	.701	.812
45	.706	.701	*	95	.701	.698	*	15	.704	29	.701	.793
46	.705	.702	*	96	.699	.695	*	16	.703	30	.701	.790
47	.709	.700	*				*	17	.704	31	.701	.781
48	.709	.701	*				*	18	.704	32	.702	.743
49	.708	.700	*				*	19	.704	33	.702	.777
50	.705	.700	*				*	20	.704	34	.702	.729
51	.704	.701	*				*	21	.705	35	.702	
52	.704	.701	*	PRISES COL		*		22	.705	36	.702	
53	.704	.702	*			*		23	.704	37	.702	
54	.703	.700	*	.753	1.148	*		24	.707	38	.702	
55	.703	.699	*	.739	1.098	*		25	.708	39	.702	
56	.700	.697	*	.869	.863	*		26	.710	40	.702	
57	.697	.696	*	.926	.767	*		27	.712	41	.702	
58	.692	.697	*	1.092	.711	*		28	.714	42	.702	
			*			*		29	.711	43	.702	
			*			*		30	.707	44	.702	
			*			*		31	.706	45	.702	
			*			*		32	.705			

***** FICHER AD136 NO(IT)= 4
 22/ 3/85 9H55 AS07 M=.6 I=0 R 2-5 ADAPTE 2D AD136
 DE AD135 4'ITE

MACH DE REFERENCE= .5972 UNF= 231.108 M/S
 TIV=295.8 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.598	.596	PRISES DOUBLES			HUB. AMONT	33	.598	1	.589	
2	.598	.599					34	.598	2	.583	
3	.599	.598	59	.597	.597	1	.596	35	.597	3	.589
4	.598	.598	60	.598	.597	2	.596	36	.598	4	.590
5	.598	.598	61	.596	.596	3	.596	37	.597	5	.573
6	.599	.599	PRISES LAT. GAUCHES			4	.596	38	.595	6	.542
7	.597	.597				5	.595	39	.595	7	.501
8	.597	.596				6	.595	40	.595	8	.584
9	.598	.597	62	.598	.598	7	.595	41	.597	9	.393
10	.598	.594	63	.598	.598	8	.594	42	.597	10	.381
11	.597	.596	64	.599	.597	9	.595	43	.596	11	.335
12	.596	.596	65	.599	.596	10	.595	44	.595	12	.183
13	.597	.596	66	.600	.595	11	.595	45	.595	13	.738
14	.596	.596	67	.602	.593	HUB. AVAL		HUB. DROIT		14	.7124
15	.596	.596	68	.602	.598	1	.598	1	.588	15	.715
16	.596	.594	69	.602	.593	2	.598	2	.598	16	.705
17	.597	.595	70	.605	.595	3	.598	3	.598	17	.701
18	.599	.595	71	.600	.595	4	.597	4	.598	18	.701
19	.598	.596	72	.597	.596	5	.598	5	.598	19	.696
20	.599	.597	73	.594	.598	6	.597	6	.598	20	.693
21	.600	.597	PRISES LAT. DROITES			7	.597	7	.598	21	.693
22	.602	.594				8	.597	8	.598	22	.680
23	.603	.593	74	.599	.599	9	.598	9	.598	23	.671
24	.602	.595	75	.597	.597	10	.598	10	.598	24	.659
25	.603	.596	76	.597	.594	11	.596	11	.598	25	.638
26	.602	.596	77	.596	.594	12	.598	12	.598	26	.624
27	.605	.596	78	.596	.592	HUB. GAUCHE				27	.610
28	.605	.598	79	.597	.592	1	.603	13	.598	28	.604
29	.608	.598	80	.604	.595	2	.602	14	.597	29	.595
30	.606	.598	81	.606	.593	3	.602	15	.597	30	.510
31	.608	.596	82	.605	.594	4	.602	16	.597	31	.395
32	.606	.599	83	.609	.594	5	.599	17	.597	32	.310
33	.607	.599	84	.612	.593	6	.599	18	.597	33	.799
34	.605	.597	85	.613	.599	7	.599	19	.597	34	.797
35	.606	.597	86	.610	.598	8	.600	20	.597	35	.750
36	.606	.598	87	.609	.598	9	.600	21	.597	36	.740
37	.607	.596	88	.609	.598	10	.602	22	.597	37	.732
38	.606	.596	89	.609	.596	11	.604	23	.597	38	.717
39	.610	.595	90	.614	.595	12	.604	24	.597	39	.711
40	.608	.595	91	.608	.595	13	.604	25	.597	40	.711
41	.608	.595	92	.604	.595	14	.602	26	.597	41	.703
42	.609	.595	93	.602	.595	15	.602	27	.597	42	.698
43	.607	.596	94	.607	.595	16	.601	28	.597	43	.692
44	.604	.596	95	.608	.598	17	.600	29	.598	44	.688
45	.603	.596	96	.605	.595	18	.598	30	.598	45	.683
46	.602	.597	97	.603	.593	19	.598	31	.597	46	.686
47	.602	.596				20	.597	32	.597	47	.688
48	.601	.596				21	.597	33	.598	48	.688
49	.600	.595				22	.597	34	.598	49	.691
50	.598	.595				23	.598	35	.598	50	.697
51	.598	.595				24	.598	36	.596		
52	.597	.596	PRISES COL			25	.599	37	.598		
53	.597	.596				26	.597	38	.598		
54	.597	.595				27	.600	39	.597		
55	.597	.594				28	.601	40	.597		
56	.596	.594				29	.602	41	.597		
57	.595	.594				30	.604	42	.597		
58	.597	.593				31	.605	43	.597		
			1.014		.632	32	.603	44	.597		
						33	.603	45	.597		
						34	.601				
						35	.602				
						36	.604				
						37	.605				
						38	.603				
						39	.601				
						40	.602				
						41	.604				
						42	.605				
						43	.603				
						44	.601				
						45	.600				
							.598				

***** FICHER AD137 N0(17)= 1
 22/ 3/85 10H25 ASOT M=1.5 I=0(-30'+ROT.30') R 2-5 NON ADAPTE AD137
 DE AD445 1'ITE PAROIS RECTILIGNES + 30'

 MACH DE REFERENCE= .5979 UINF= 331.100 M/S
 TIV=301.0 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE 930-	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.605	.591									
2	.604	.595				HUB. AMONT	33		.605	1	.571
3	.601	.595					34		.604	2	.608
4	.597	.595	59	.597	.598		35		.604	3	.605
5	.595	.597	60	.598	.597		36		.603	4	.604
6	.598	.599	61	.597	.601		37		.603	5	.601
7	.597	.597					38		.603	6	.604
8	.598	.597					39		.603	7	.597
9	.598	.598					40		.604	8	.601
10	.598	.598	62	.599	.597		41		.604	9	.603
11	.596	.595	63	.600	.601		42		.604	10	.603
12	.594	.595	64	.602	.602		43		.603	11	.603
13	.595	.595	65	.603	.600		44		.602	12	.713
14	.596	.597	66	.609	.599		45		.601	13	.714
15	.597	.598	67	.613	.606					14	.703
16	.598	.597	68	.614	.604	HUB. AVAL		HUB. DROIT		15	.723
17	.598	.597	69	.614	.604		1		.598	16	.712
18	.599	.598	70	.614	.603		2		.599	17	.708
19	.602	.599	71	.607	.602		3		.599	18	.708
20	.603	.600	72	.602	.604		4		.599	19	.703
21	.603	.600	73	.578	.605		5		.598	20	.701
22	.607	.600					6		.598	21	.691
23	.610	.599					7		.598	22	.687
24	.611	.600					8		.598	23	.678
25	.612	.599	74	.600	.599		9		.598	24	.663
26	.612	.599	75	.597	.598		10		.598	25	.652
27	.615	.600	76	.598	.597		11		.598	26	.629
28	.616	.603	77	.597	.595					27	.675
29	.618	.603	78	.599	.597					28	.669
30	.617	.605	79	.601	.597					29	.641
31	.621	.605	80	.608	.609	HUB. GAUCHE				30	.614
32	.618	.606	81	.614	.600		1		.612	31	.598
33	.619	.604	82	.615	.599		2		.612	32	.613
34	.617	.602	83	.613	.601		3		.612	33	.652
35	.619	.602	84	.623	.605		4		.606	34	.612
36	.618	.603	85	.624	.605		5		.606	35	.762
37	.619	.603	86	.623	.605		6		.608	36	.749
38	.617	.601	87	.621	.603		7		.610	37	.743
39	.619	.601	88	.621	.601		8		.612	38	.739
40	.616	.600	89	.623	.601		9		.612	39	.731
41	.616	.600	90	.617	.603		10		.611	40	.729
42	.616	.601	91	.611	.604		11		.610	41	.711
43	.614	.603	92	.609	.602		12		.610	42	.697
44	.611	.604	93	.601	.601		13		.609	43	.701
45	.610	.603	94	.602	.602		14		.608	44	.688
46	.609	.603	95	.595	.605		15		.604	45	.674
47	.609	.601	96	.577	.604		16		.603	46	.674
48	.606	.601					17		.603	47	.666
49	.604	.601					18		.604	48	.644
50	.601	.602					19		.604	49	.666
51	.601	.602					20		.605	50	.650
52	.601	.602					21		.605		
53	.601	.602					22		.605		
54	.601	.602					23		.604		
55	.601	.602					24		.607		
56	.601	.602					25		.608		
57	.601	.602					26		.609		
58	.601	.602					27		.611		
59	.601	.602					28		.611		
60	.601	.602					29		.610		
61	.601	.602					30		.608		
62	.601	.602					31		.606		
63	.601	.602					32		.606		

***** FICHER AD138 NOCIT= 1
 22/ 3/85 10H45 AS07 M=6 I=0(-30'+ROT.30') R 2-5 ADAPTE 3D AD138
 DE AD9137 L'ITE

MACH DE REFERENCE= .5985 UINF= 231.108 M/S
 TIV=300.6 K PIV= 1392 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.606	.591	*	PRISES DOUBLES		HUB. AMONT	33	.601	*	1	.570	
2	.605	.595	*				34	.601	*	2	.581	
3	.601	.595	*	59	.597	.599	1	.600	35	.601	* 3	.623
4	.597	.597	*	60	.600	.600	2	.599	36	.601	* 4	.631
5	.596	.599	*	61	.601	.599	3	.598	37	.601	* 5	.630
6	.597	.601	*				4	.598	38	.601	* 6	.651
7	.597	.599	*	PRISES LAT. GAUCHES		5	.598	39	.600			.611
8	.598	.599	*			6	.598	40	.601	*	8	.599
9	.599	.601	*	62	.598	.596	7	.598	41	.601	* 9	.600
10	.600	.597	*	63	.600	.602	8	.597	42	.601	* 10	.652
11	.598	.597	*	64	.602	.603	9	.598	43	.600	* 11	.622
12	.597	.597	*	65	.600	.599	10	.598	44	.600	* 12	.754
13	.599	.597	*	66	.602	.601	11	.599	45	.598	* 13	.732
14	.600	.599	*	67	.604	.601						.720
15	.600	.599	*	68	.603	.601	HUB. AVAL	HUB. DROIT			15	.712
16	.600	.599	*	69	.604	.602					16	.703
17	.599	.600	*	70	.606	.599	1	.602	1	.599	* 17	.699
18	.599	.600	*	71	.601	.601	2	.602	2	.599	* 18	.698
19	.599	.600	*	72	.602	.599	3	.602	3	.598	* 19	.693
20	.602	.602	*	73	.591	.604	4	.602	4	.598	* 20	.692
21	.601	.600	*				5	.601	5	.598	* 21	.682
22	.602	.597	*	PRISES LAT. DROITES		6	.601	6	.599	* 22	.680	
23	.602	.596	*			7	.602	7	.599	* 23	.672	
24	.603	.600	*	74	.600	.598	8	.604	8	.599	* 24	.651
25	.606	.603	*	75	.597	.599	9	.604	9	.599	* 25	.681
26	.605	.602	*	76	.598	.597	10	.602	10	.600	* 26	.627
27	.607	.602	*	77	.598	.596	11	.601	11	.599	* 27	.613
28	.607	.602	*	78	.598	.598					28	.672
29	.608	.601	*	79	.598	.597	HUB. GAUCHE				29	.649
30	.606	.601	*	80	.605	.598					30	.626
31	.609	.598	*	81	.605	.596	1	.605	13	.598	* 31	.617
32	.607	.602	*	82	.607	.601	2	.605	14	.598	* 32	.603
33	.608	.602	*	83	.610	.602	3	.604	15	.598	* 33	.699
34	.606	.601	*	84	.613	.601	4	.601	16	.598	* 34	.717
35	.607	.601	*	85	.614	.602	5	.601	17	.598	* 35	.740
36	.606	.601	*	86	.611	.603	6	.603	18	.599	* 36	.730
37	.607	.600	*	87	.610	.602	7	.605	19	.599	* 37	.724
38	.607	.600	*	88	.610	.601	8	.606	20	.599	* 38	.721
39	.610	.600	*	89	.614	.599	9	.607	21	.600	* 39	.716
40	.609	.600	*	90	.609	.599	10	.606	22	.599	* 40	.707
41	.609	.599	*	91	.604	.598	11	.604	23	.599	* 41	.699
42	.609	.599	*	92	.603	.600	12	.605	24	.599	* 42	.695
43	.607	.598	*	93	.600	.600	13	.604	25	.599	* 43	.690
44	.604	.598	*	94	.603	.598	14	.604	26	.599	* 44	.680
45	.603	.598	*	95	.598	.603	15	.602	27	.599	* 45	.687
46	.602	.599	*	96	.589	.601	16	.601	28	.599	* 46	.686
47	.604	.601	*				17	.601	29	.599	* 47	.660
48	.604	.602	*				18	.601	30	.599	* 48	.649
49	.604	.601	*				19	.601	31	.599	* 49	.660
50	.602	.600	*				20	.602	32	.599	* 50	.627
51	.602	.599	*				21	.602	33	.599		
52	.600	.598	*	PRISES COL		22	.593	34	.599			
53	.601	.601	*			23	.601	35	.599			
54	.600	.602	*	.656	1.064	24	.604	36	.599			
55	.600	.602	*	.632	.987	25	.604	37	.599			
56	.597	.602	*	.602	.795	26	.605	38	.598			
57	.594	.603	*	.668	.692	27	.607	39	.598			
58	.589	.605	*	1.028	.632	28	.608	40	.598			
			*			29	.606	41	.598			
			*			30	.604	42	.598			
			*			31	.604	43	.598			
			*			32	.602	44	.598			
			*					45	.598			

***** FICHER AD139 NOC(IT)= 1
 22/ 8/85 11H 0 AS07 M=3 I=0(-30'+ROT.30') R 2-5 NON ADAPTE AD139
 DE AD445 1'ITE PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .8043 UINF= 231.108 M/S
 TIV=301.2 K PIV= 1651 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LAT.				AILE AS0-	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.817	.792	PRISES DOUBLES			HUB. AMONT	33	.834		1	
2	.816	.798					34	.833		2	.790
3	.809	.800	59	.799	.805	1	.805	35	.832	3	.815
4	.802	.804	60	.807	.806	2	.805	36	.825	4	.803
5	.798	.808	61	.812	.815	3	.805	37	.827	5	.803
6	.800	.809				4	.805	38	.830	6	.808
7	.800	.805	PRISES LAT. GAUCHES			5	.803	39	.831	7	.807
8	.805	.803				6	.804	40	.833	8	.817
9	.807	.807	62	.804	.803	7	.805	41	.835	9	.823
10	.809	.800	63	.799	.809	8	.807	42	.832	10	1.062
11	.805	.802	64	.813	.813	9	.805	43	.830	11	1.044
12	.802	.804	65	.819	.818	10	.804	44	.829	12	1.056
13	.804	.804	66	.835	.817	11	.806	45	.827	13	1.026
14	.803	.807	67	.851	.832					14	1.036
15	.804	.809	68	.855	.831	HUB. AVAL		HUB. DROIT		15	1.016
16	.805	.808	69	.859	.832	1	.817	1	.804	16	1.022
17	.808	.808	70	.854	.827	2	.817	2	.805	17	1.035
18	.814	.807	71	.832	.821	3	.818	3	.805	18	1.035
19	.815	.808	72	.820	.823	4	.823	4	.805	19	1.044
20	.816	.815	73	.776	.827	5	.820	5	.804	20	1.036
21	.813	.813				6	.819	6	.804	21	1.044
22	.826	.819	PRISES LAT. DROITES			7	.817	7	.804	22	1.007
23	.833	.815				8	.818	8	.805	23	.875
24	.836	.817	74	.806	.805	9	.821	9	.805	24	.764
25	.841	.820	75	.800	.806	10	.820	10	.805	25	.794
26	.844	.821	76	.806	.802	11	.820	11	.805	26	.873
27	.852	.822	77	.804	.803					27	.883
28	.855	.830	78	.806	.804	HUB. GAUCHE				28	.877
29	.865	.834	79	.812	.801	13	.804	13	.804	29	.825
30	.862	.835	80	.826	.815	14	.804	14	.804	30	.870
31	.872	.831	81	.840	.816	1	.854	15	.805	31	.855
32	.867	.837	82	.842	.817	2	.852	16	.805	32	.840
33	.872	.837	83	.860	.823	3	.851	17	.805	33	1.532
34	.866	.830	84	.873	.834	4	.829	18	.804	34	1.451
35	.871	.831	85	.883	.839	5	.833	19	.804	35	1.493
36	.869	.830	86	.879	.838	6	.841	20	.804	36	1.326
37	.870	.828	87	.875	.833	7	.849	21	.804	37	1.283
38	.865	.826	88	.872	.828	8	.856	22	.804	38	1.250
39	.866	.825	89	.869	.825	9	.856	23	.804	39	1.122
40	.860	.825	90	.853	.825	10	.847	24	.805	40	1.087
41	.857	.825	91	.841	.823	11	.847	25	.804	41	1.053
42	.857	.825	92	.834	.823	12	.846	26	.805	42	1.010
43	.848	.823	93	.819	.819	13	.843	27	.805	43	1.008
44	.839	.823	94	.819	.818	14	.841	28	.804	44	.886
45	.837	.821	95	.809	.839	15	.825	29	.804	45	.852
46	.834	.822	96	.775	.836	16	.823	30	.804	46	.846
47	.833	.821				17	.825	31	.804	47	.838
48	.830	.823				18	.828	32	.804	48	.843
49	.825	.821				19	.829	33	.804	49	.823
50	.820	.821				20	.831	34	.804	50	.851
51	.819	.820				21	.834	35	.804		
52	.815	.816	PRISES COL			22	.836	36	.804		
53	.814	.819				23	.835	37	.804		
54	.813	.821	.869	1.221		24	.842	38	.804		
55	.810	.822	.868	.878		25	.845	39	.804		
56	.801	.823	.849	.881		26	.843	40	.805		
57	.786	.835	.842	.819		27	.853	41	.804		
58	.761	.852	1.150	.779		28	.854	42	.805		
						29	.846	43	.804		
						30	.836	44	.804		
						31	.831	45	.804		
						32	.836				

***** FICHER AD140 N0(17)= 1
 22/ 8/85 11H15 AS07 M=.8 I=0(-30' ROT.30') R 2-5 ADAPTE 3D 1' ITE. AD140
 DE AD9139 1' ITE

MACH DE REFERENCE= .8039 UINF= 231.109 M/S
 TIV=300.8 K PIV= 1649 MB

MACH PAROIS HAUTE ET BASSE									
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH
1	.817	.792	*	PRISES DOUBLES	*	HUB. AMONT	33	*	.809
2	.815	.793	*		*		34	*	.809
3	.810	.800	*	59	.805	1	.804	*	.808
4	.802	.804	*	60	.806	2	.802	*	.808
5	.799	.807	*	61	.793	3	.802	*	.807
6	.802	.809	*		*	4	.804	*	.807
7	.801	.805	*	PRISES LAT. GAUCHES*	*	5	.802	*	.807
8	.804	.802	*	62	.805	6	.801	*	.810
9	.806	.806	*	63	.797	7	.801	*	.811
10	.808	.801	*	64	.809	8	.800	*	.809
11	.800	.803	*	65	.806	9	.801	*	.807
12	.800	.804	*	66	.802	10	.802	*	.805
13	.804	.804	*	67	.814	11	.803	*	.805
14	.804	.806	*		*			*	
15	.807	.806	*	68	.810	HUB. AVAL	HUB. DROIT	*	
16	.807	.803	*	69	.813	1	.805	*	.804
17	.806	.804	*	70	.819	2	.805	*	.804
18	.804	.805	*	71	.806	3	.804	*	.804
19	.802	.805	*	72	.808	4	.805	*	.804
20	.804	.808	*	73	.797	5	.805	*	.804
21	.805	.807	*		*	6	.805	*	.804
22	.809	.805	*	PRISES LAT. DROITES*	*	7	.805	*	.804
23	.810	.803	*	74	.807	8	.804	*	.804
24	.808	.803	*	75	.801	9	.805	*	.804
25	.807	.806	*	76	.805	10	.805	*	.804
26	.808	.805	*	77	.804	11	.802	*	.804
27	.814	.804	*	78	.802			*	.804
28	.816	.808	*	79	.802	HUB. GAUCHE	HUB.	*	.804
29	.822	.810	*	80	.801	12	.804	*	.804
30	.813	.810	*	81	.813	13	.804	*	.804
31	.824	.807	*	82	.817	14	.804	*	.804
32	.813	.812	*	83	.809	15	.804	*	.804
33	.822	.815	*	84	.820	16	.804	*	.804
34	.817	.810	*	85	.833	17	.804	*	.804
35	.813	.812	*	86	.833	18	.804	*	.804
36	.822	.811	*	87	.824	19	.804	*	.804
37	.821	.810	*	88	.824	20	.804	*	.804
38	.827	.809	*	89	.821	21	.804	*	.804
39	.824	.807	*	90	.821	22	.804	*	.804
40	.823	.806	*	91	.809	23	.804	*	.804
41	.823	.805	*	92	.809	24	.805	*	.805
42	.816	.802	*	93	.802	25	.804	*	.804
43	.808	.801	*	94	.802	26	.804	*	.804
44	.805	.799	*	95	.803	27	.804	*	.804
45	.804	.801	*	96	.794	28	.804	*	.804
46	.808	.802	*		*	29	.804	*	.804
47	.810	.806	*		*	30	.804	*	.804
48	.810	.807	*		*	31	.804	*	.804
49	.809	.805	*		*	32	.804	*	.804
50	.809	.801	*		*	33	.804	*	.804
51	.807	.794	*	PRISES COL	*	34	.804	*	.804
52	.807	.797	*	.853	1.215	35	.804	*	.804
53	.807	.800	*	.855	1.195	36	.803	*	.803
54	.806	.802	*	.838	.895	37	.803	*	.803
55	.803	.805	*	.880	.823	38	.804	*	.804
56	.803	.812	*	1.143	.790	39	.804	*	.804
57	.803	.824	*		*	40	.804	*	.804
58	.795	.824	*		*	41	.804	*	.804
			*		*	42	.804	*	.804
			*		*	43	.804	*	.804
			*		*	44	.804	*	.804
			*		*	45	.804	*	.804
			*		*	46	.804	*	.804
			*		*	47	.804	*	.804
			*		*	48	.804	*	.804
			*		*	49	.804	*	.804
			*		*	50	.804	*	.804
			*		*	51	.804	*	.804
			*		*	52	.804	*	.804
			*		*	53	.804	*	.804
			*		*	54	.804	*	.804
			*		*	55	.804	*	.804
			*		*	56	.804	*	.804
			*		*	57	.804	*	.804
			*		*	58	.804	*	.804

***** FICHER AD141 NO(ITE)= 1
 22/ 8/85 11H35 A307 M=.3 I=0(-30)+ROT.30) R 2-5 ADAPTE 3D 2' ITE. AD141
 DE AD9140 1' ITE

MACH DE REFERENCE= .9043 UINF= 231.108 M/S
 TIV=229.3 K. PIV= 1551 MB

MACH PAROIS HAUTE ET BASSE			MACH PAROIS LAT.ER.			MILE ASB					
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.815	.792	*	PRISES HAUTES	*	HUB. AMONT	33	.309	.309	1	.309
2	.816	.793	*	PRISES DOUBLES	*	HUB. AMONT	34	.308	.308	2	.308
3	.809	.800	*	59	.803	.805	35	.308	.308	3	.308
4	.801	.803	*	60	.805	.805	36	.308	.308	4	.308
5	.799	.807	*	61	.800	.800	37	.307	.307	5	.307
6	.803	.810	*	PRISES LAT. GAUCHES*	*	HUB. AMONT	38	.307	.307	6	.307
7	.804	.805	*	62	.802	.801	39	.307	.307	7	.307
8	.806	.805	*	63	.804	.801	40	.810	.810	8	.810
9	.807	.805	*	64	.797	.810	41	.812	.812	9	.812
10	.807	.801	*	65	.797	.810	42	.810	.810	10	.810
11	.801	.804	*	66	.812	.809	43	.807	.807	11	.807
12	.777	.805	*	67	.804	.804	44	.806	.806	12	.806
13	.799	.805	*	68	.808	.805	45	.804	.804	13	.804
14	.801	.807	*	69	.819	.808	HUB. DROIT			14	.804
15	.804	.807	*	70	.815	.806	HUB. DROIT			15	.804
16	.805	.803	*	71	.817	.810	HUB. DROIT			16	.804
17	.807	.803	*	72	.821	.807	HUB. DROIT			17	.804
18	.809	.803	*	73	.809	.802	HUB. DROIT			18	.804
19	.807	.802	*	74	.808	.803	HUB. DROIT			19	.804
20	.804	.803	*	75	.803	.803	HUB. DROIT			20	.804
21	.803	.803	*	76	.792	.810	HUB. DROIT			21	.804
22	.806	.803	*	PRISES LAT. DROITES*	*	HUB. DROIT			22	.805	
23	.809	.802	*	77	.805	.805	HUB. DROIT			23	.805
24	.811	.805	*	78	.804	.805	HUB. DROIT			24	.805
25	.812	.808	*	79	.805	.805	HUB. DROIT			25	.805
26	.814	.808	*	80	.802	.804	HUB. DROIT			26	.804
27	.811	.805	*	81	.800	.804	HUB. DROIT			27	.804
28	.823	.809	*	82	.804	.800	HUB. DROIT			28	.804
29	.825	.810	*	83	.805	.795	HUB. DROIT			29	.804
30	.821	.809	*	84	.810	.802	HUB. DROIT			30	.805
31	.825	.812	*	85	.814	.805	HUB. DROIT			31	.805
32	.825	.812	*	86	.827	.805	HUB. DROIT			32	.805
33	.819	.807	*	87	.827	.810	HUB. DROIT			33	.805
34	.819	.807	*	88	.840	.810	HUB. DROIT			34	.804
35	.835	.809	*	89	.840	.814	HUB. DROIT			35	.804
36	.823	.807	*	90	.824	.813	HUB. DROIT			36	.804
37	.825	.807	*	91	.829	.810	HUB. DROIT			37	.804
38	.824	.807	*	92	.827	.805	HUB. DROIT			38	.805
39	.825	.807	*	93	.832	.804	HUB. DROIT			39	.805
40	.825	.807	*	94	.824	.806	HUB. DROIT			40	.804
41	.825	.805	*	95	.815	.805	HUB. DROIT			41	.804
42	.826	.805	*	96	.811	.805	HUB. DROIT			42	.804
43	.821	.805	*	PRISES COL			HUB. DROIT			43	.804
44	.814	.805	*	859	1.213		HUB. DROIT			44	.804
45	.821	.805	*	859	1.165		HUB. DROIT			45	.804
46	.810	.804	*	840	.928		HUB. DROIT			46	.804
47	.810	.804	*	935	.825		HUB. DROIT			47	.804
48	.810	.804	*	1.145	1.132		HUB. DROIT			48	.804
49	.809	.804	*				HUB. DROIT			49	.804
50	.805	.804	*				HUB. DROIT			50	.804
51	.807	.804	*				HUB. DROIT			51	.804
52	.809	.801	*				HUB. DROIT			52	.804
53	.804	.805	*				HUB. DROIT			53	.804
54	.804	.805	*				HUB. DROIT			54	.804
55	.804	.805	*				HUB. DROIT			55	.804
56	.803	.805	*				HUB. DROIT			56	.805
57	.805	.805	*				HUB. DROIT			57	.805
58	.805	.805	*				HUB. DROIT			58	.805
59	.805	.805	*				HUB. DROIT			59	.805
60	.805	.805	*				HUB. DROIT			60	.805
61	.805	.805	*				HUB. DROIT			61	.805
62	.805	.805	*				HUB. DROIT			62	.805
63	.805	.805	*				HUB. DROIT			63	.805
64	.805	.805	*				HUB. DROIT			64	.805
65	.805	.805	*				HUB. DROIT			65	.805
66	.805	.805	*				HUB. DROIT			66	.805
67	.805	.805	*				HUB. DROIT			67	.805
68	.805	.805	*				HUB. DROIT			68	.805
69	.805	.805	*				HUB. DROIT			69	.805
70	.805	.805	*				HUB. DROIT			70	.805

***** FICHER AD142 M8(17)= 1
 22/ 8.25 14H25 AS07 M=6 I=-2 R 2-5 NON ADAPTE AD142
 DE AD4 L'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .5976 UINF= 231.109 M/S
 TIV=02.5 K PIV= 1.990 MB

MACH PAROIS HAUTE ET BASSE			MACH PAROIS LAT. E.			MACH PAROIS LAT. O.			MACH PAROIS LAT. N.		
I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS
1	.597	.596									
2	.597	.593									
3	.597	.597									
4	.595	.597									
5	.595	.597									
6	.597	.599									
7	.598	.596									
8	.598	.598									
9	.598	.595									
10	.596	.597									
11	.594	.597									
12	.595	.597									
13	.595	.597									
14	.595	.599									
15	.597	.599									
16	.598	.599									
17	.598	.598									
18	.601	.598									
19	.600	.598									
20	.602	.602									
21	.601	.601									
22	.604	.599									
23	.605	.599									
24	.605	.602									
25	.605	.607									
26	.608	.608									
27	.609	.608									
28	.612	.609									
29	.611	.608									
30	.613	.608									
31	.611	.609									
32	.613	.608									
33	.613	.609									
34	.614	.607									
35	.613	.608									
36	.614	.607									
37	.614	.608									
38	.614	.607									
39	.616	.607									
40	.613	.606									
41	.617	.605									
42	.617	.605									
43	.617	.604									
44	.618	.604									
45	.618	.602									
46	.619	.603									
47	.615	.603									
48	.615	.602									
49	.615	.602									
50	.614	.602									
51	.604	.601									
52	.601	.598									
53	.601	.598									
54	.604	.598									
55	.604	.596									
56	.605	.594									
57	.603	.594									
58	.603	.593									
59	.603	.593									
60	.605	.593									
61	.605	.593									
62	.607	.593									
63	.607	.593									
64	.609	.593									
65	.609	.593									
66	.610	.593									
67	.610	.593									
68	.610	.593									
69	.610	.593									
70	.610	.593									
71	.610	.593									
72	.610	.593									
73	.610	.593									
74	.610	.593									
75	.610	.593									
76	.610	.593									
77	.610	.593									
78	.610	.593									
79	.610	.593									
80	.610	.593									
81	.610	.593									
82	.610	.593									
83	.610	.593									
84	.610	.593									
85	.610	.593									

***** FICHER AD143 NO(IT)= 1
 22/ 8/85 14H40 AS07 M=.6 I=-2 R 2-5 ADAPTE 3D AD143
 DE AD9142 1'ITE.

MACH DE REFERENCE= .5982 UNF= 231.109 M/S
 TIV=301.5 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.599	.597	PRISES DOUBLES			HUB. AMONT	33	.501	1	.575	
2	.599	.599						2	.592		
3	.598	.598	59	.598	.599	1	.597	35	.501	3	.536
4	.596	.598	60	.599	.599	2	.596	36	.501	4	.536
5	.595	.598	61	.602	.600	3	.596	37	.501	5	.536
6	.598	.600				4	.596	38	.501	6	.536
7	.598	.599	PRISES LAT. GAUCHES			5	.596	39	.501	7	.536
8	.599	.599				6	.595	40	.502	8	.536
9	.599	.599	62	.595	.598	7	.595	41	.503	9	.536
10	.599	.596	63	.600	.601	8	.595	42	.502	10	.536
11	.597	.596	64	.601	.601	9	.595	43	.501	11	.536
12	.595	.597	65	.598	.600	10	.595	44	.500	12	.536
13	.596	.597	66	.599	.598	11	.595	45	.500	13	.536
14	.597	.599	67	.605	.602					14	.536
15	.597	.599	68	.602	.601	HUB. AVANT		HUB. DROIT		15	.536
16	.598	.598	69	.602	.603					16	.536
17	.599	.599	70	.605	.601	1	.603	1	.599	17	.536
18	.601	.599	71	.602	.599	2	.602	2	.598	18	.536
19	.599	.600	72	.602	.602	3	.601	3	.598	19	.536
20	.599	.601	73	.600	.605	4	.601	4	.598	20	.536
21	.598	.601				5	.600	5	.599	21	.536
22	.601	.599	PRISES LAT. DROITES			6	.601	6	.599	22	.536
23	.600	.597				7	.601	7	.599	23	.536
24	.599	.598	74	.597	.600	8	.603	8	.599	24	.536
25	.600	.601	75	.597	.599	9	.601	9	.599	25	.536
26	.600	.600	76	.599	.595	10	.600	10	.598	26	.536
27	.603	.601	77	.597	.597	11	.599	11	.598	27	.536
28	.605	.603	78	.597	.595					28	.536
29	.607	.604	79	.598	.597	HUB. GAUCHE				29	.536
30	.606	.603	80	.601	.600					30	.536
31	.607	.601	81	.603	.600	1	.604	1	.599	31	.536
32	.606	.604	82	.600	.602	2	.602	2	.598	32	.536
33	.606	.605	83	.605	.605	3	.602	3	.598	33	.536
34	.604	.603	84	.612	.606	4	.603	4	.599	34	.536
35	.604	.603	85	.613	.606	5	.603	5	.599	35	.536
36	.603	.603	86	.609	.606	6	.601	6	.599	36	.536
37	.605	.602	87	.606	.605	7	.603	7	.599	37	.536
38	.606	.602	88	.607	.603	8	.603	8	.599	38	.536
39	.609	.602	89	.613	.602	9	.604	9	.599	39	.536
40	.607	.602	90	.608	.601	10	.603	10	.599	40	.536
41	.607	.602	91	.601	.600	11	.602	11	.599	41	.536
42	.608	.601	92	.604	.599	12	.603	12	.599	42	.536
43	.604	.599	93	.599	.599	13	.602	13	.599	43	.536
44	.600	.599	94	.602	.601	14	.602	14	.599	44	.536
45	.601	.599	95	.602	.599	15	.601	15	.599	45	.536
46	.601	.600	96	.599	.591	16	.600	16	.599	46	.536
47	.604	.599				17	.600	17	.599	47	.536
48	.603	.601				18	.600	18	.599	48	.536
49	.602	.600				19	.600	19	.599	49	.536
50	.600	.601				20	.599	20	.599	50	.536
51	.602	.601				21	.600	21	.599	51	.536
52	.603	.600	PRISES COL			22	.600	22	.599	52	.536
53	.603	.601				23	.598	23	.599	53	.536
54	.603	.601	.603	1.059		24	.602	24	.599	54	.536
55	.603	.599	.601	.917		25	.603	25	.599	55	.536
56	.602	.597	.799	.796		26	.604	26	.599	56	.536
57	.601	.595	.855	.692		27	.606	27	.599	57	.536
58	.599	.590	1.023	.631		28	.607	28	.599	58	.536
						29	.606	29	.599		
						30	.604	30	.599		
						31	.602	31	.599		
						32	.601	32	.599		

***** FICHER AD144 N0(1T)= 4
 22/ 8/85 15H10 AS07 M=1.6 I=-2 R 2-5 ADAPTE 2D AD144
 DE AD136 1'ITE.

MACH DE REFERENCE= .5964 UINF= 231.100 M/S
 TIV=296.8 K PIV= 1392 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	SAS	I	HAUT	SAS	I	MACH	I	MACH	I	MACH
1	.598	.595	PRISES DOUBLES			HUB. AMONT	33	.599	1	.575	
2	.599	.599				34	.599	2	.591		
3	.597	.598	59	.596	.597	35	.599	3	.639		
4	.596	.598	60	.597	.597	36	.599	4	.690		
5	.596	.599	61	.596	.595	37	.599	5	.697		
6	.598	.600	PRISES LAT. GAUCHES			38	.599	6	.686		
7	.597	.597				39	.599	7	.667		
8	.597	.596	62	.597	.598	40	.600	8	.681		
9	.597	.597	63	.597	.599	41	.600	9	.617		
10	.598	.594	64	.599	.600	42	.600	10	.737		
11	.597	.595	65	.596	.595	43	.598	11	.736		
12	.595	.596	66	.599	.597	44	.598	12	.718		
13	.595	.595	67	.600	.599	45	.597	13	.699		
14	.596	.597	68	.599	.598	HUB. AVAL HUB. DROIT		14	.687		
15	.599	.597	69	.601	.599	1	.598	15	.682		
16	.595	.595	70	.602	.598	2	.597	16	.676		
17	.596	.597	71	.599	.596	3	.598	17	.675		
18	.599	.595	72	.597	.597	4	.598	18	.678		
19	.597	.595	73	.589	.598	5	.598	19	.677		
20	.597	.595	PRISES LAT. DROITES			6	.597	20	.679		
21	.595	.595				7	.597	21	.675		
22	.599	.598	74	.597	.599	8	.597	22	.675		
23	.599	.598	75	.597	.597	9	.598	23	.670		
24	.599	.599	76	.597	.594	10	.598	24	.667		
25	.599	.599	77	.595	.595	11	.597	25	.678		
26	.599	.599	78	.595	.595	12	.597	26	.694		
27	.599	.599	79	.596	.593	HUB. GAUCHE		27	.686		
28	.599	.599	80	.600	.596	1	.600	28	.688		
29	.599	.599	81	.603	.598	14	.597	29	.688		
30	.599	.599	82	.602	.601	15	.597	30	.683		
31	.599	.599	83	.604	.601	16	.597	31	.683		
32	.599	.599	84	.606	.602	17	.597	32	.682		
33	.599	.599	85	.607	.604	18	.597	33	.685		
34	.599	.599	86	.606	.603	19	.597	34	.685		
35	.599	.599	87	.605	.602	20	.597	35	.685		
36	.599	.599	88	.605	.600	21	.597	36	.685		
37	.599	.599	89	.609	.599	22	.597	37	.685		
38	.599	.599	90	.604	.600	23	.597	38	.685		
39	.599	.599	91	.600	.598	24	.597	39	.685		
40	.599	.599	92	.600	.596	25	.597	40	.685		
41	.599	.599	93	.596	.595	26	.597	41	.685		
42	.599	.599	94	.599	.595	27	.597	42	.685		
43	.599	.599	95	.594	.598	28	.597	43	.685		
44	.599	.599	96	.587	.588	29	.597	44	.685		
45	.599	.599				30	.597	45	.685		
46	.599	.599				31	.597	46	.685		
47	.599	.599				32	.597	47	.685		
48	.599	.599				33	.597	48	.685		
49	.599	.599				34	.597	49	.685		
50	.599	.599				35	.597	50	.685		
51	.599	.599				36	.597				
52	.597	.595	PRISES COL			37	.597				
53	.597	.595				38	.597				
54	.596	.594	.658	1.053		39	.597				
55	.596	.592	.695	.925		40	.597				
56	.593	.592	.794	.801		41	.597				
57	.598	.599	.861	.693		42	.597				
58	.587	.598	1.019	.632		43	.597				
						44	.597				
						45	.597				

***** FICHER AD145 NO(ITE)= 4
 22/ 8/85 17H15 AS07 M=.6 I=+2 R 2-5 ADAPTE 2D AD145
 DE AD131 4'ITE.

MACH DE REFERENCE= .5959 UINF= 231.109 M/S
 TIV=297.1 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.598	.593	* PRISES DOUBLES *			HUB. AMONT	33		.597	1	.582
2	.599	.597				34		.595	2	.571	
3	.598	.596	59	.596	.596	35	.596	.595	3	.571	
4	.596	.596	60	.598	.596	36	.595	.596	4	.556	
5	.595	.597	61	.597	.595	37	.595	.596	5	.546	
6	.598	.598				38	.595	.595	6	.547	
7	.597	.596	* PRISES LAT. GAUCHES *			39	.595	.594	7	.544	
8	.597	.595				40	.595	.594	8	.489	
9	.597	.596	62	.596	.596	41	.595	.594	9	.384	
10	.598	.593	63	.599	.598	42	.594	.594	10	1.093	
11	.596	.594	64	.599	.597	43	.594	.594	11	.836	
12	.594	.594	65	.599	.594	44	.594	.592	12	.839	
13	.596	.593	66	.592	.593	45	.594	.593	13	.726	
14	.596	.594	67	.593	.595				14	.733	
15	.596	.595	68	.593	.594	HUB. AVAL		HUB. DROIT	15	.750	
16	.597	.594	69	.595	.595				16	.736	
17	.598	.594	70	.596	.593	1	.598	1	17	.728	
18	.600	.593	71	.599	.592	2	.597	2	18	.724	
19	.599	.592	72	.598	.596	3	.598	3	19	.718	
20	.600	.594	73	.599	.599	4	.598	4	20	.709	
21	.599	.593				5	.597	5	21	.696	
22	.601	.591	* PRISES LAT. DROITES *			6	.598	6	22	.686	
23	.603	.589				7	.598	7	23	.675	
24	.604	.591	74	.597	.598	8	.599	8	24	.662	
25	.608	.592	75	.597	.595	9	.598	9	25	.657	
26	.606	.592	76	.597	.593	10	.598	10	26	.645	
27	.609	.591	77	.595	.592	11	.597	11	27	.645	
28	.608	.593	78	.595	.591				28	.633	
29	.611	.592	79	.598	.593	HUB. GAUCHE			29	.620	
30	.608	.593	80	.596	.590	1	.605	1	30	.609	
31	.612	.589	81	.599	.593	2	.605	2	31	.469	
32	.608	.592	82	.612	.599	3	.604	3	32	.349	
33	.611	.592	83	.614	.599	4	.605	4	33	1.079	
34	.608	.591	84	.613	.598	5	.608	5	34	1.011	
35	.610	.590	85	.613	.592	6	.608	6	35	.924	
36	.609	.592	86	.616	.591	7	.602	7	36	.899	
37	.611	.590	87	.614	.591	8	.604	8	37	.891	
38	.610	.591	88	.613	.590	9	.606	9	38	.832	
39	.613	.591	89	.617	.591	10	.607	10	39	.755	
40	.610	.591	90	.610	.592	11	.606	11	40	.749	
41	.610	.591	91	.604	.593	12	.604	12	41	.735	
42	.610	.591	92	.602	.590	13	.603	13	42	.725	
43	.607	.592	93	.597	.593	14	.602	14	43	.711	
44	.604	.593	94	.598	.594	15	.601	15	44	.693	
45	.603	.592	95	.596	.599	16	.598	16	45	.671	
46	.601	.592	96	.597	.598	17	.597	17	46	.657	
47	.603	.592				18	.597	18	47	.660	
48	.602	.592				19	.597	19	48	.653	
49	.601	.593				20	.598	20	49	.647	
50	.599	.595				21	.599	21	50	.641	
51	.599	.595				22	.599	22	51	.634	
52	.599	.594				23	.599	23	52	.627	
53	.599	.595	* PRISES COL *			24	.600	24	53	.620	
54	.599	.595				25	.598	25	54	.616	
55	.598	.593	97	.598	.597	26	.601	26	55	.616	
56	.594	.593	98	.596	.597	27	.602	27	56	.616	
57	.591	.591	99	.596	.593	28	.603	28	57	.616	
58	.596	.598	100	.591	.591	29	.605	29	58	.616	
			101	.601	.601	30	.606	30			
						31	.605	31			
						32	.603	32			
						33	.601	33			
						34	.598	34			
						35	.598	35			
						36	.598	36			
						37	.598	37			
						38	.598	38			
						39	.598	39			
						40	.598	40			
						41	.598	41			
						42	.598	42			
						43	.598	43			
						44	.598	44			
						45	.598	45			

***** FICHER AD146 NOCIT= 4
23/ 3/85 9H50 AS07 M=6 I=+2 R 1-4 ADAPTE 2D AD146
DE AD145 4'ITE.

MACH DE REFERENCE= .5936 UINF= 231.109 M/S
TIV=297.0 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.595	.591	PRISES DOUBLES			HUB.	AMONT	33	.594	1	.573
2	.596	.595						34	.593	2	.573
3	.595	.593	59	.593	.593	1	.594	35	.592	3	.573
4	.593	.592	60	.596	.594	2	.594	36	.593	4	.577
5	.592	.593	61	.595	.590	3	.593	37	.593	5	.579
6	.594	.594				4	.593	38	.592	6	.571
7	.594	.593	PRISES LAT. GAUCHES			5	.592	39	.592	7	.566
8	.594	.593				6	.592	40	.591	8	.495
9	.594	.594	62	.594	.592	7	.592	41	.592	9	.328
10	.596	.591	63	.597	.596	8	.591	42	.593	10	1.010
11	.595	.591	64	.597	.593	9	.592	43	.591	11	.398
12	.593	.591	65	.596	.593	10	.592	44	.590	12	.799
13	.595	.591	66	.598	.593	11	.592	45	.590	13	.552
14	.594	.592	67	.603	.592					14	.735
15	.594	.592	68	.601	.591	HUB.	AVAL	HUB.	DROIT	15	.723
16	.594	.591	69	.601	.591	1	.596	1	.594	16	.709
17	.595	.591	70	.604	.590	2	.596	2	.594	17	.700
18	.597	.591	71	.600	.592	3	.596	3	.594	18	.697
19	.597	.591	72	.595	.593	4	.596	4	.594	19	.692
20	.598	.593	73	.587	.595	5	.595	5	.594	20	.689
21	.597	.592				6	.595	6	.594	21	.689
22	.599	.591	PRISES LAT. DROITES			7	.595	7	.594	22	.689
23	.601	.589				8	.595	8	.594	23	.689
24	.601	.589	74	.595	.595	9	.597	9	.594	24	.689
25	.604	.603	75	.594	.593	10	.596	10	.594	25	.689
26	.603	.603	76	.595	.591	11	.594	11	.594	26	.689
27	.607	.597	77	.594	.590					27	.689
28	.608	.599	78	.593	.593	HUB.	GAUCHE	12	.594	28	.689
29	.611	.599	79	.597	.588	13	.603	13	.594	29	.689
30	.608	.599	80	.603	.599	14	.602	14	.594	30	.689
31	.611	.586	81	.606	.597	15	.603	15	.594	31	.689
32	.608	.599	82	.608	.595	16	.602	16	.594	32	.689
33	.609	.589	83	.612	.596	17	.602	17	.594	33	1.013
34	.605	.588	84	.617	.597	18	.603	18	.594	34	.689
35	.607	.588	85	.617	.593	19	.603	19	.594	35	.689
36	.605	.588	86	.613	.593	20	.600	20	.594	36	.689
37	.607	.587	87	.610	.589	21	.602	21	.594	37	.689
38	.606	.587	88	.609	.586	22	.604	22	.594	38	.689
39	.609	.587	89	.613	.583	23	.604	23	.594	39	.689
40	.607	.587	90	.608	.589	24	.603	24	.594	40	.689
41	.607	.588	91	.601	.582	25	.602	25	.594	41	.689
42	.607	.588	92	.602	.583	26	.601	26	.594	42	.689
43	.604	.590	93	.595	.591	27	.600	27	.594	43	.689
44	.600	.591	94	.596	.591	28	.600	28	.594	44	.689
45	.600	.591	95	.594	.585	29	.600	29	.594	45	.689
46	.599	.593	96	.595	.583	30	.595	30	.593	46	.689
47	.602	.592				31	.595	31	.594	47	.689
48	.602	.593				32	.595	32	.594	48	.689
49	.599	.593				33	.595	33	.594	49	.689
50	.595	.592				34	.595	34	.594	50	.689
51	.595	.592				35	.595	35	.593	51	.689
52	.596	.593	PRISES COL			36	.597	36	.594	52	.689
53	.596	.593				37	.596	37	.594	53	.689
54	.596	.593	.593	1.048		38	.593	38	.594	54	.689
55	.595	.591	.593	.911		39	.599	39	.594	55	.689
56	.592	.589	.732	.933		40	.601	40	.594	56	.689
57	.589	.586	.659	.889		41	.602	41	.594	57	.689
58	.584	.582	1.015	.928		42	.604	42	.594	58	.689
						43	.602	43	.594		
						44	.600	44	.594		
						45	.599	45	.594		
						30	.595				

***** FICHER AD147 NO(IT)= 1
 23/ 8/ 85 10H25 AS07 M= 6 I=+2(+1.5+ROT.30') R 1-4 NON ADAPTE AD147
 DE AD445 1'ITE PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .5931 UINF= 231.108 M/S
 TIV=301.2 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.601	.597	*	PRISES DOUBLES			HUB. AMONT	33	.599	1	.599
2	.599	.599	*					34	.599	2	.599
3	.596	.591	*	59	.593	.593	1	.595	35	3	.597
4	.593	.593	*	60	.594	.593	2	.594	36	4	.598
5	.591	.594	*	61	.592	.597	3	.595	37	5	.597
6	.593	.595	*				4	.594	38	6	.596
7	.593	.593	*	PRISES LAT. GAUCHES			5	.593	39	7	.595
8	.594	.592	*				6	.593	40	8	.595
9	.594	.594	*	62	.594	.592	7	.594	41	9	.595
10	.594	.590	*	63	.595	.595	8	.594	42	10	.597
11	.591	.591	*	64	.599	.595	9	.593	43	11	.591
12	.590	.591	*	65	.599	.593	10	.593	44	12	.593
13	.591	.591	*	66	.600	.595	11	.593	45	13	.592
14	.592	.592	*	67	.612	.594				14	.591
15	.593	.593	*	68	.614	.594	HUB. AVANT	HUB. DROIT	15	15	.723
16	.594	.593	*	69	.614	.594	1	.597	1	16	.723
17	.596	.593	*	70	.613	.594	2	.597	2	17	.714
18	.599	.594	*	71	.604	.595	3	.597	3	18	.710
19	.599	.594	*	72	.598	.593	4	.598	4	19	.705
20	.599	.594	*	73	.574	.600	5	.600	5	20	.701
21	.601	.593	*				6	.600	6	21	.691
22	.605	.592	*	PRISES LAT. DROITES			7	.599	7	22	.693
23	.600	.590	*				8	.599	8	23	.692
24	.609	.590	*	74	.609	.604	9	.599	9	24	.682
25	.613	.593	*	75	.600	.593	10	.600	10	25	.675
26	.612	.593	*	76	.593	.591	11	.599	11	26	.666
27	.616	.591	*	77	.591	.590	12	.599	12	27	.657
28	.617	.592	*	78	.591	.590	HUB. GAUCHE	13	.599	13	.647
29	.620	.590	*	79	.599	.589	1	.613	14	14	.641
30	.619	.591	*	80	.605	.589	2	.611	15	15	.634
31	.623	.593	*	81	.613	.583	3	.611	16	16	.626
32	.619	.591	*	82	.615	.580	4	.604	17	17	.618
33	.621	.590	*	83	.620	.583	5	.608	18	18	.610
34	.618	.590	*	84	.625	.583	6	.608	19	19	.603
35	.620	.590	*	85	.628	.589	7	.610	20	20	.595
36	.619	.592	*	86	.634	.590	8	.612	21	21	.588
37	.621	.591	*	87	.639	.592	9	.613	22	22	.581
38	.618	.591	*	88	.643	.595	10	.610	23	23	.573
39	.620	.591	*	89	.644	.590	11	.610	24	24	.567
40	.617	.590	*	90	.647	.593	12	.609	25	25	.561
41	.617	.591	*	91	.649	.595	13	.608	26	26	.554
42	.616	.592	*	92	.655	.595	14	.606	27	27	.547
43	.613	.593	*	93	.659	.595	15	.601	28	28	.540
44	.610	.593	*	94	.667	.595	16	.600	29	29	.533
45	.609	.596	*	95	.669	.591	17	.599	30	30	.526
46	.607	.596	*	96	.673	.593	18	.600	31	31	.519
47	.607	.595	*				19	.600	32	32	.511
48	.605	.595	*				20	.600	33	33	.503
49	.602	.596	*				21	.601	34	34	.495
50	.600	.597	*				22	.602	35	35	.487
51	.597	.597	*				23	.603	36	36	.479
52	.593	.597	*	PRISES COL			24	.601	37	37	.471
53	.592	.599	*				25	.604	38	38	.463
54	.590	.590	*	.861	1.060		26	.605	39	39	.455
55	.587	.590	*	.892	.990		27	.607	40	40	.447
56	.584	.590	*	.797	.791		28	.609	41	41	.439
57	.579	.601	*	.865	.609		29	.610	42	42	.431
58	.570	.605	*	1.022	.629		30	.608	43	43	.423
			*				31	.606	44	44	.415
			*				32	.602	45	45	.407

***** FICHER AD148 NQ(IT)= 1
 23/ 8/95 10H40 AS07 M=.6 I=+2(1.5+ROT.30') R 1-4 ADAPTE 3D AD148
 DE AD9122 1'ITE.

MACH DE REFERENCE= .5936 UINF= 231.109 M/S
 TIV=300.6 K PIV= 1392 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.500	.586	PRISES DOUBLES			HUB. AMONT	33	.595	1	.582	
2	.599	.589				34	.595	2	.590		
3	.595	.590	59	.592	.592	1	.594	35	.594	3	.619
4	.592	.593	60	.595	.594	2	.593	36	.595	4	.651
5	.591	.594	61	.500	.592	3	.594	37	.595	5	.638
6	.593	.595				4	.594	38	.595	6	.589
7	.593	.592	PRISES LAT. GAUCHES			5	.593	39	.594	7	.595
8	.595	.592				6	.593	40	.594	8	.598
9	.596	.594	62	.593	.592	7	.593	41	.595	9	.595
10	.596	.591	63	.595	.595	8	.593	42	.595	10	.905
11	.594	.594	64	.597	.597	9	.593	43	.594	11	.896
12	.592	.595	65	.595	.594	10	.593	44	.594	12	.791
13	.593	.594	66	.595	.596	11	.594	45	.593	13	.752
14	.593	.595	67	.502	.593					14	.738
15	.593	.594	68	.500	.595	HUB. AVAL		HUB. DROIT		15	.724
16	.594	.593	69	.501	.593	1	.599	1	.594	16	.711
17	.595	.594	70	.505	.592	2	.599	2	.594	17	.703
18	.597	.595	71	.599	.595	3	.599	3	.595	18	.701
19	.596	.594	72	.500	.595	4	.598	4	.595	19	.696
20	.596	.594	73	.593	.597	5	.598	5	.595	20	.694
21	.596	.593				6	.598	6	.594	21	.688
22	.599	.592	PRISES LAT. DROITES			7	.598	7	.594	22	.681
23	.600	.592				8	.599	8	.594	23	.670
24	.599	.595	74	.594	.593	9	.599	9	.594	24	.674
25	.600	.595	75	.592	.592	10	.599	10	.594	25	.661
26	.599	.594	76	.594	.591	11	.597	11	.594	26	.654
27	.603	.591	77	.592	.592			12	.593	27	.652
28	.604	.592	78	.594	.592	HUB. GAUCHE		13	.593	28	.648
29	.608	.591	79	.596	.590	1	.602	13	.593	29	.643
30	.607	.592	80	.501	.590	2	.602	14	.593	30	.638
31	.610	.589	81	.605	.591	3	.602	15	.593	31	.633
32	.607	.593	82	.602	.592	4	.602	16	.593	32	.621
33	.608	.593	83	.608	.591	5	.602	17	.593	33	.614
34	.604	.594	84	.615	.590	6	.602	18	.594	34	.608
35	.606	.594	85	.615	.591	7	.602	19	.593	35	.600
36	.605	.596	86	.611	.592	8	.602	20	.594	36	.593
37	.607	.595	87	.609	.595	9	.602	21	.594	37	.588
38	.607	.594	88	.609	.594	10	.604	22	.594	38	.583
39	.610	.593	89	.614	.593	11	.604	23	.594	39	.578
40	.608	.592	90	.608	.592	12	.604	24	.594	40	.571
41	.609	.592	91	.601	.591	13	.602	25	.594	41	.564
42	.609	.592	92	.600	.594	14	.600	26	.594	42	.558
43	.605	.591	93	.596	.596	15	.601	27	.594	43	.553
44	.601	.592	94	.600	.593	16	.600	28	.594	44	.548
45	.599	.591	95	.598	.596	17	.597	29	.594	45	.543
46	.598	.593	96	.591	.595	18	.595	30	.594	46	.538
47	.600	.594				19	.595	31	.593	47	.533
48	.600	.596				20	.595	32	.593	48	.528
49	.600	.596				21	.595	33	.593	49	.523
50	.599	.596				22	.597	34	.593	50	.518
51	.600	.594				23	.598	35	.593		
52	.600	.592	PRISES COL			24	.599	36	.593		
53	.601	.594				25	.597	37	.593		
54	.600	.596	.659	1.059		26	.601	38	.593		
55	.600	.596	.631	.707		27	.601	39	.593		
56	.598	.595	.797	.746		28	.603	40	.593		
57	.595	.597	.364	.591		29	.604	41	.593		
58	.592	.599	1.021	.830		30	.604	42	.593		
						31	.602	43	.593		
						32	.597	44	.593		

***** FICHER ADI49 MACT)= 4
 23/8/85 11H10 AS07 M=6 I=0 R 1-4 ADAPTE 2D ADI49
 DE ADI36 4 ITE.

MACH DE REFERENCE= .5936 UINF= 231.108 M/S
 TIV=295.8 K PIV= 1394 MB

MACH PAROIS HAUTE ET BASSE		MACH PAROIS LATER.		ALLE AS07		
I	HAUT	BAS	I	MACH	I	MACH
1	.595	.592	33	.595	1	.593
2	.595	.595	34	.594	2	.591
3	.594	.594	35	.594	3	.591
4	.592	.594	36	.593	4	.596
5	.594	.594	37	.592	5	.591
6	.594	.596	38	.593	6	.592
7	.594	.593	39	.592	7	.595
8	.595	.592	40	.592	8	.595
9	.595	.593	41	.591	9	.597
10	.595	.590	42	.591	10	.597
11	.592	.592	43	.592	11	.594
12	.590	.592	44	.592	12	.595
13	.592	.591	45	.592	13	.595
14	.592	.591			14	.593
15	.594	.593			15	.595
16	.595	.592			16	.595
17	.594	.591			17	.597
18	.594	.591			18	.597
19	.594	.590			19	.594
20	.595	.592			20	.595
21	.595	.592			21	.595
22	.597	.591			22	.593
23	.598	.590			23	.595
24	.599	.590			24	.590
25	.601	.592			25	.590
26	.600	.592			26	.592
27	.602	.592			27	.592
28	.602	.594			28	.597
29	.604	.594			29	.592
30	.606	.594			30	.592
31	.603	.595			31	.591
32	.605	.595			32	.591
33	.602	.593			33	.595
34	.604	.594			34	.595
35	.604	.592			35	.594
36	.603	.594			36	.592
37	.603	.593			37	.595
38	.603	.592			38	.590
39	.603	.592			39	.590
40	.603	.591			40	.590
41	.603	.591			41	.590
42	.602	.591			42	.590
43	.602	.591			43	.590
44	.602	.591			44	.590
45	.602	.591			45	.590
46	.602	.591			46	.590
47	.602	.591			47	.590
48	.602	.591			48	.590
49	.602	.591			49	.590
50	.602	.591			50	.590
51	.602	.591			51	.590
52	.602	.591			52	.590
53	.602	.591			53	.590
54	.602	.591			54	.590
55	.602	.591			55	.590
56	.602	.591			56	.590
57	.602	.591			57	.590
58	.602	.591			58	.590
59	.602	.591			59	.590
60	.602	.591			60	.590
61	.602	.591			61	.590
62	.602	.591			62	.590

***** FICHER AD150 NOCIT= 1
33/ 3/85 11H25 AS07 M.F. I=0 R 1-4 NON ADAPTE AD150
DE AD4 L'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE .5947 UNF= 231.108 M/S
TIV=300.1 K PIV= 1331 MB

MACH PAROIS HAUTE ET BASSE		MACH PAROIS LAT. HUB. DROIT		MACH PAROIS LAT. HUB. GAUCHE		MACH PAROIS LAT. HUB. DROIT		MACH PAROIS LAT. HUB. GAUCHE									
I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS
1	.595	.594	1	.594	.595	1	.594	.595	1	.594	.595	1	.594	.595	1	.594	.595
2	.595	.597	2	.595	.596	2	.595	.596	2	.595	.596	2	.595	.596	2	.595	.596
3	.593	.595	3	.594	.595	3	.594	.595	3	.594	.595	3	.594	.595	3	.594	.595
4	.593	.595	4	.594	.595	4	.594	.595	4	.594	.595	4	.594	.595	4	.594	.595
5	.592	.595	5	.594	.595	5	.594	.595	5	.594	.595	5	.594	.595	5	.594	.595
6	.592	.595	6	.594	.595	6	.594	.595	6	.594	.595	6	.594	.595	6	.594	.595
7	.595	.594	7	.594	.595	7	.594	.595	7	.594	.595	7	.594	.595	7	.594	.595
8	.595	.594	8	.594	.595	8	.594	.595	8	.594	.595	8	.594	.595	8	.594	.595
9	.595	.594	9	.594	.595	9	.594	.595	9	.594	.595	9	.594	.595	9	.594	.595
10	.593	.593	10	.594	.595	10	.594	.595	10	.594	.595	10	.594	.595	10	.594	.595
11	.593	.593	11	.594	.595	11	.594	.595	11	.594	.595	11	.594	.595	11	.594	.595
12	.591	.594	12	.594	.595	12	.594	.595	12	.594	.595	12	.594	.595	12	.594	.595
13	.591	.594	13	.594	.595	13	.594	.595	13	.594	.595	13	.594	.595	13	.594	.595
14	.593	.595	14	.594	.595	14	.594	.595	14	.594	.595	14	.594	.595	14	.594	.595
15	.594	.596	15	.594	.595	15	.594	.595	15	.594	.595	15	.594	.595	15	.594	.595
16	.595	.594	16	.594	.595	16	.594	.595	16	.594	.595	16	.594	.595	16	.594	.595
17	.595	.594	17	.594	.595	17	.594	.595	17	.594	.595	17	.594	.595	17	.594	.595
18	.593	.593	18	.594	.595	18	.594	.595	18	.594	.595	18	.594	.595	18	.594	.595
19	.597	.594	19	.594	.595	19	.594	.595	19	.594	.595	19	.594	.595	19	.594	.595
20	.599	.595	20	.594	.595	20	.594	.595	20	.594	.595	20	.594	.595	20	.594	.595
21	.600	.595	21	.594	.595	21	.594	.595	21	.594	.595	21	.594	.595	21	.594	.595
22	.603	.595	22	.594	.595	22	.594	.595	22	.594	.595	22	.594	.595	22	.594	.595
23	.603	.597	23	.594	.595	23	.594	.595	23	.594	.595	23	.594	.595	23	.594	.595
24	.605	.597	24	.594	.595	24	.594	.595	24	.594	.595	24	.594	.595	24	.594	.595
25	.605	.597	25	.594	.595	25	.594	.595	25	.594	.595	25	.594	.595	25	.594	.595
26	.610	.597	26	.594	.595	26	.594	.595	26	.594	.595	26	.594	.595	26	.594	.595
27	.613	.598	27	.594	.595	27	.594	.595	27	.594	.595	27	.594	.595	27	.594	.595
28	.617	.598	28	.594	.595	28	.594	.595	28	.594	.595	28	.594	.595	28	.594	.595
29	.616	.598	29	.594	.595	29	.594	.595	29	.594	.595	29	.594	.595	29	.594	.595
30	.620	.598	30	.594	.595	30	.594	.595	30	.594	.595	30	.594	.595	30	.594	.595
31	.617	.598	31	.594	.595	31	.594	.595	31	.594	.595	31	.594	.595	31	.594	.595
32	.614	.599	32	.594	.595	32	.594	.595	32	.594	.595	32	.594	.595	32	.594	.595
33	.614	.599	33	.594	.595	33	.594	.595	33	.594	.595	33	.594	.595	33	.594	.595
34	.615	.599	34	.594	.595	34	.594	.595	34	.594	.595	34	.594	.595	34	.594	.595
35	.615	.599	35	.594	.595	35	.594	.595	35	.594	.595	35	.594	.595	35	.594	.595
36	.615	.599	36	.594	.595	36	.594	.595	36	.594	.595	36	.594	.595	36	.594	.595
37	.615	.599	37	.594	.595	37	.594	.595	37	.594	.595	37	.594	.595	37	.594	.595
38	.614	.599	38	.594	.595	38	.594	.595	38	.594	.595	38	.594	.595	38	.594	.595
39	.614	.599	39	.594	.595	39	.594	.595	39	.594	.595	39	.594	.595	39	.594	.595
40	.615	.599	40	.594	.595	40	.594	.595	40	.594	.595	40	.594	.595	40	.594	.595
41	.618	.599	41	.594	.595	41	.594	.595	41	.594	.595	41	.594	.595	41	.594	.595
42	.611	.599	42	.594	.595	42	.594	.595	42	.594	.595	42	.594	.595	42	.594	.595
43	.608	.599	43	.594	.595	43	.594	.595	43	.594	.595	43	.594	.595	43	.594	.595
44	.608	.599	44	.594	.595	44	.594	.595	44	.594	.595	44	.594	.595	44	.594	.595
45	.606	.599	45	.594	.595	45	.594	.595	45	.594	.595	45	.594	.595	45	.594	.595
46	.606	.599	46	.594	.595	46	.594	.595	46	.594	.595	46	.594	.595	46	.594	.595
47	.604	.599	47	.594	.595	47	.594	.595	47	.594	.595	47	.594	.595	47	.594	.595
48	.600	.599	48	.594	.595	48	.594	.595	48	.594	.595	48	.594	.595	48	.594	.595
49	.602	.599	49	.594	.595	49	.594	.595	49	.594	.595	49	.594	.595	49	.594	.595
50	.600	.599	50	.594	.595	50	.594	.595	50	.594	.595	50	.594	.595	50	.594	.595
51	.600	.599	51	.594	.595	51	.594	.595	51	.594	.595	51	.594	.595	51	.594	.595
52	.598	.599	52	.594	.595	52	.594	.595	52	.594	.595	52	.594	.595	52	.594	.595
53	.599	.599	53	.594	.595	53	.594	.595	53	.594	.595	53	.594	.595	53	.594	.595
54	.599	.599	54	.594	.595	54	.594	.595	54	.594	.595	54	.594	.595	54	.594	.595
55	.593	.599	55	.594	.595	55	.594	.595	55	.594	.595	55	.594	.595	55	.594	.595
56	.591	.599	56	.594	.595	56	.594	.595	56	.594	.595	56	.594	.595	56	.594	.595
57	.596	.599	57	.594	.595	57	.594	.595	57	.594	.595	57	.594	.595	57	.594	.595
58	.596	.599	58	.594	.595	58	.594	.595	58	.594	.595	58	.594	.595	58	.594	.595
59	.596	.599	59	.594	.595	59	.594	.595	59	.594	.595	59	.594	.595	59	.594	.595
60	.596	.599	60	.594	.595	60	.594	.595	60	.594	.595	60	.594	.595	60	.594	.595

PRISES COL

.557 1.052
.691 1.115
.795 1.195
.861 1.229
1.107 1.229

***** FICHER AD151 NO(IT)= 1
 23/ 3/85 11H40 AS07 M=6 I=0 R 1-4 ADAPTE 3D AD151
 DE AD9107 1'ITE.

MACH DE REFERENCE= .5943 UINF= 231.108 M/S
 TIV=300.0 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.595	.594	PRISES DOUBLES			HUB. AMONT	33	.597	1	.581	
2	.595	.597				34	.596	2	.592		
3	.594	.595	59	.594	.595	35	.596	3	.594		
4	.593	.594	60	.594	.594	36	.596	4	.585		
5	.593	.595	61	.599	.594	37	.596	5	.585		
6	.595	.596				38	.596	6	.579		
7	.594	.595	PRISES LAT. GAUCHES			39	.596	7	.574		
8	.595	.593				40	.596	8	.567		
9	.594	.594	62	.593	.595	41	.597	9	.560		
10	.595	.592	63	.596	.597	42	.597	10	.518		
11	.592	.592	64	.598	.599	43	.596	11	.503		
12	.590	.593	65	.595	.595	44	.595	12	.738		
13	.592	.593	66	.595	.594	45	.595	13	.717		
14	.592	.595	67	.599	.596	HUB. AVAL HUB. DROIT		14	.702		
15	.593	.595	68	.600	.597	1	.600	15	.694		
16	.594	.595	69	.601	.598	2	.594	16	.683		
17	.595	.595	70	.603	.598	3	.599	17	.677		
18	.597	.594	71	.607	.598	4	.599	18	.675		
19	.596	.593	72	.608	.599	5	.599	19	.672		
20	.596	.595	73	.606	.599	6	.598	20	.673		
21	.595	.595				7	.597	21	.663		
22	.595	.595	PRISES LAT. DROITES			8	.598	22	.663		
23	.599	.594				9	.598	23	.667		
24	.597	.595	74	.594	.597	10	.600	24	.669		
25	.597	.595	75	.596	.599	11	.598	25	.669		
26	.597	.595	76	.594	.599	12	.597	26	.661		
27	.600	.595	77	.592	.599	13	.595	27	.658		
28	.602	.597	78	.595	.599	HUB. GAUCHE		28	.659		
29	.604	.597	79	.595	.599	14	.600	29	.657		
30	.603	.597	80	.600	.599	15	.600	30	.651		
31	.603	.597	81	.603	.599	16	.600	31	.603		
32	.603	.597	82	.600	.599	17	.599	32	.610		
33	.605	.597	83	.604	.599	18	.599	33	.614		
34	.603	.596	84	.609	.599	19	.597	34	.605		
35	.605	.596	85	.611	.599	20	.597	35	.617		
36	.604	.597	86	.609	.599	21	.598	36	.618		
37	.606	.596	87	.609	.599	22	.599	37	.616		
38	.605	.597	88	.609	.599	23	.601	38	.613		
39	.608	.596	89	.611	.599	24	.602	39	.611		
40	.605	.596	90	.606	.599	25	.601	40	.607		
41	.604	.596	91	.601	.599	26	.600	41	.601		
42	.605	.594	92	.609	.599	27	.600	42	.609		
43	.603	.593	93	.597	.599	28	.600	43	.603		
44	.600	.593	94	.601	.599	29	.599	44	.606		
45	.600	.593	95	.609	.599	30	.597	45	.607		
46	.600	.594	96	.604	.599	31	.596	46	.607		
47	.600	.595				32	.596	47	.603		
48	.600	.595				33	.596	48	.603		
49	.600	.595				34	.596	49	.603		
50	.600	.594				35	.596	50	.603		
51	.600	.595				36	.596				
52	.600	.594	PRISES COL			37	.597				
53	.601	.596				38	.596				
54	.601	.596	.597	1.048		39	.599				
55	.600	.599	.600	.919		40	.600				
56	.603	.599	.605	.855		41	.600				
57	.607	.604	.601	.690		42	.602				
58	.604	.605	1.013	.609		43	.603				
						44	.602				
						45	.600				

***** FICHER AD152 NOC(IT)= 4
 23/ 8/85 11H55 AS07 M=.8 I=0 R 1-4 ADAPTE 2D AD152
 DE AD134 4'ITE.

MACH DE REFERENCE= .8022 UINF= 231.108 M/S
 TIV=295.3 K PIV= 1552 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.804	.800	PRISES DOUBLES			HUB. AMONT		32	.807	1	.784
2	.804	.806						34	.805	2	.808
3	.803	.802	59	.803	.802	1	.797	35	.805	3	.871
4	.799	.801	60	.805	.803	2	.796	36	.804	4	.944
5	.800	.802	61	.799	.796	3	.796	37	.804	5	.903
6	.804	.805						4	.798	38	.804
7	.803	.802	PRISES LAT. GAUCHES					5	.796	39	.804
8	.805	.801						5	.796	40	.805
9	.805	.804	62	.801	.801	7	.796	41	.808	8	.741
10	.806	.798	63	.796	.807	8	.796	42	.807	9	.834
11	.801	.799	64	.806	.804	9	.796	43	.803	10	1.213
12	.796	.799	65	.803	.801	10	.796	44	.802	11	1.078
13	.793	.799	66	.810	.800	11	.797	45	.801	12	1.010
14	.797	.801	67	.814	.804					14	.976
15	.799	.802	68	.816	.802	HUB. AVAL		HUB. DROIT		15	.969
16	.799	.799	69	.820	.805	1	.802	1	.802	16	.958
17	.802	.798	70	.813	.804	2	.802	2	.802	17	.951
18	.806	.797	71	.808	.799	3	.802	3	.802	18	.956
19	.804	.798	72	.805	.802	4	.801	4	.802	19	.955
20	.802	.802	73	.800	.807	5	.804	5	.802	20	.954
21	.801	.801	PRISES LAT. DROITES					6	.802	6	.802
22	.808	.797						7	.801	7	.802
23	.813	.796	74	.802	.805	8	.802	8	.802	8	.802
24	.814	.799	75	.804	.803	9	.802	9	.802	9	.754
25	.815	.803	76	.803	.799	10	.803	10	.802	10	.783
26	.815	.803	77	.803	.799	11	.800	11	.802	11	.859
27	.820	.801	78	.798	.798					12	.854
28	.820	.804	79	.799	.795					13	.819
29	.825	.805	80	.802	.792	HUB. GAUCHE				14	.879
30	.821	.804	81	.809	.799	1	.802	14	.803	15	.825
31	.823	.800	82	.821	.797	2	.815	15	.802	16	.821
32	.823	.805	83	.818	.801	3	.815	16	.802	17	.817
33	.823	.805	84	.829	.801	4	.815	17	.802	18	1.421
34	.824	.801	85	.837	.804	5	.806	18	.802	19	1.379
35	.828	.802	86	.839	.807	6	.807	19	.802	20	1.315
36	.827	.803	87	.836	.807	7	.811	20	.802	21	1.014
37	.830	.801	88	.835	.805	8	.815	21	.802	22	1.323
38	.826	.802	89	.833	.802	9	.820	22	.802	23	1.037
39	.828	.801	90	.832	.800	10	.821	23	.802	24	1.070
40	.823	.801	91	.821	.802	11	.817	24	.802	25	1.059
41	.821	.801	92	.811	.804	12	.815	25	.802	26	1.019
42	.821	.802	93	.812	.799	13	.814	26	.802	27	1.018
43	.816	.802	94	.802	.798	14	.813	27	.802	28	1.003
44	.810	.803	95	.804	.799	15	.812	28	.802	29	.961
45	.809	.801	96	.797	.799	16	.806	29	.802	30	.951
46	.807	.801						17	.805	31	.928
47	.812	.798						18	.804	32	.903
48	.810	.799						19	.805	33	.845
49	.809	.799						20	.806	34	.805
50	.805	.800						21	.806	35	.806
51	.804	.801						22	.808	36	.802
52	.802	.797	PRISES COL					23	.809	37	.802
53	.801	.800						24	.807	38	.802
54	.801	.801	849	1.211		25	.812	39	.802	39	.802
55	.802	.800	869	1.186		26	.814	40	.802	40	.802
56	.801	.798	886	.899		27	.817	41	.802	41	.802
57	.800	.799	881	.823		28	.821	42	.802	42	.802
58	.799	.797	1.140	.780		29	.823	43	.802	43	.802
						30	.813	44	.802	44	.802
						31	.811	45	.802	45	.802
						32	.807				
							.808				

***** FICHER AD153 NO(IT)= 1
 23/ 8/85 14H40 AS07 M=1.8 I=0 R 1-4 NON ADAPTE AD153
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .8029 UINF= 231.108 M/S
 TIV=302.4 K PIV= 1650 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.802	.801	PRISES DOUBLES			HUB. AMONT		33	.822	1	.811
2	.801	.805						34	.831	2	.833
3	.801	.802	59	.800	.801	1	.803	35	.829	3	.808
4	.800	.803	60	.803	.804	2	.802	36	.822	4	.872
5	.800	.804	61	.813	.811	3	.802	37	.825	5	.837
6	.802	.805				4	.801	38	.825	6	.859
7	.800	.801	PRISES LAT. GAUCHES			5	.801	39	.829	7	.771
8	.804	.802				6	.801	40	.832	8	.762
9	.805	.807	62	.800	.802	7	.801	41	.834	9	.827
10	.804	.799	63	.796	.809	8	.802	42	.830	10	1.277
11	.800	.801	64	.812	.810	9	.801	43	.829	11	1.238
12	.798	.802	65	.819	.814	10	.801	44	.827	12	1.115
13	.800	.803	66	.829	.821	11	.803	45	.825	13	1.043
14	.799	.805	67	.848	.824					14	.896
15	.802	.806	68	.855	.828	HUB. AVAL		HUB. DROIT		15	.994
16	.804	.804	69	.860	.834	1	.817	1	.803	16	.987
17	.805	.803	70	.851	.826	2	.816	2	.803	17	.880
18	.810	.805	71	.828	.819	3	.816	3	.803	18	.992
19	.812	.807	72	.821	.818	4	.820	4	.803	19	.997
20	.817	.813	73	.815	.823	5	.817	5	.804	20	1.012
21	.818	.813				6	.815	6	.804	21	1.011
22	.820	.809	PRISES LAT. DROITES			7	.813	7	.803	22	.993
23	.825	.809				8	.813	8	.803	23	.961
24	.829	.817	74	.801	.805	9	.816	9	.803	24	.779
25	.824	.824	75	.801	.803	10	.814	10	.803	25	.806
26	.838	.823	76	.802	.801	11	.815	11	.803	26	.887
27	.847	.821	77	.801	.802			12	.803	27	.996
28	.852	.825	78	.803	.801	HUB. GAUCHE		13	.803	28	.892
29	.853	.827	79	.819	.802	1	.854	13	.803	29	.809
30	.858	.826	80	.826	.811	2	.851	14	.803	30	.871
31	.871	.823	81	.832	.811	3	.849	15	.803	31	.855
32	.857	.831	82	.838	.822	4	.824	16	.803	32	.821
33	.875	.833	83	.855	.822	5	.820	17	.803	33	1.411
34	.869	.830	84	.876	.825	6	.808	18	.803	34	1.079
35	.875	.831	85	.883	.831	7	.808	19	.803	35	1.341
36	.871	.832	86	.883	.833	8	.847	20	.803	36	1.057
37	.871	.829	87	.881	.833	9	.853	21	.803	37	1.056
38	.866	.829	88	.874	.838	10	.845	22	.803	38	1.064
39	.854	.827	89	.866	.825	11	.846	23	.803	39	1.069
40	.858	.824	90	.859	.824	12	.843	24	.803	40	1.105
41	.853	.823	91	.841	.826	13	.841	25	.803	41	1.108
42	.854	.823	92	.832	.819	14	.839	26	.803	42	1.100
43	.847	.823	93	.819	.816	15	.832	27	.803	43	1.113
44	.840	.824	94	.820	.819	16	.821	28	.803	44	1.016
45	.837	.821	95	.812	.803	17	.821	29	.803	45	.879
46	.833	.822	96	.813	.799	18	.824	30	.803	46	.956
47	.830	.818				19	.824	31	.803	47	.807
48	.826	.818				20	.826	32	.803	48	.866
49	.824	.816				21	.831	33	.803	49	.938
50	.820	.815				22	.834	34	.803	50	.864
51	.819	.813				23	.833	35	.803		
52	.815	.811	PRISES COL			24	.833	36	.803		
53	.817	.815				25	.842	37	.803		
54	.816	.817	.855	1.211		26	.846	38	.804		
55	.816	.813	.866	1.036		27	.851	39	.804		
56	.814	.809	.838	.882		28	.852	40	.804		
57	.815	.805	.882	.816		29	.843	41	.804		
58	.818	.794	1.142	.775		30	.834	42	.804		
						31	.829	43	.804		
						32	.834	44	.804		

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***** FICHER AD154 NOCIT= 1
 23/ 8/85 14H50 AS07 M=13 I=0 R 1-4 ADAPTE 3D AD154
 DE ADP113 1'ITE.

MACH DE REFERENCE= .3025 UINF= 231.108 M/S
 TIV=301.5 K PIV= 1652 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.305	.303	PRISES DOUBLES			HUB. AMONT	33	.307	1	.787		
2	.302	.305					34	.305	2	.311		
3	.301	.304	59	.799	.302	1	.798	35	.305	3	.371	
4	.300	.305	60	.303	.302	2	.797	36	.305	4	.340	
5	.300	.307	61	.304	.799	3	.797	37	.305	5	.314	
6	.301	.305					4	.798	38	.305	6	.345
7	.300	.302	PRISES LAT. GAUCHES				5	.796	39	.305	7	.750
8	.305	.303					6	.796	40	.307	8	.752
9	.303	.303	62	.300	.304	7	.796	41	.309	9	.303	
10	.304	.795	63	.795	.305	8	.795	42	.308	10	1.232	
11	.799	.795	64	.307	.303	9	.797	43	.304	11	1.193	
12	.796	.798	65	.304	.300	10	.797	44	.303	12	1.353	
13	.797	.799	66	.305	.305	11	.799	45	.302	13	.394	
14	.795	.301	67	.314	.303	HUB. AVAL		HUB. DROIT		14	.369	
15	.798	.303	68	.312	.303	1	.305	1	.302	15	.351	
16	.300	.302	69	.314	.303	2	.303	2	.303	16	.350	
17	.302	.302	70	.313	.305	3	.303	3	.303	17	.345	
18	.305	.302	71	.308	.300	4	.305	4	.302	18	.349	
19	.304	.302	72	.305	.304	5	.303	5	.302	19	.350	
20	.304	.302	73	.313	.303	6	.303	6	.302	20	.357	
21	.303	.300	PRISES LAT. DROITES			7	.303	7	.302	21	.351	
22	.305	.798				8	.302	8	.302	22	.344	
23	.307	.303	74	.301	.307	9	.303	9	.302	23	.323	
24	.308	.303	75	.300	.303	10	.304	10	.303	24	.798	
25	.309	.305	76	.301	.793	11	.301	11	.303	25	.360	
26	.310	.303	77	.797	.798	HUB. GAUCHE				26	.347	
27	.315	.303	78	.799	.799	1	.314	1	.302	27	.301	
28	.317	.305	79	.799	.799	2	.314	2	.302	28	.345	
29	.324	.305	80	.301	.795	3	.314	3	.302	29	.392	
30	.319	.304	81	.311	.798	4	.313	4	.303	30	.345	
31	.327	.301	82	.314	.799	5	.313	5	.303	31	.345	
32	.322	.305	83	.312	.305	6	.314	6	.303	32	1.415	
33	.325	.307	84	.323	.305	7	.313	7	.302	33	1.382	
34	.320	.304	85	.305	.305	8	.304	8	.302	34	1.323	
35	.324	.306	86	.307	.309	9	.305	9	.302	35	1.231	
36	.322	.307	87	.302	.309	10	.309	10	.302	36	1.005	
37	.324	.305	88	.300	.309	11	.313	11	.302	37	1.000	
38	.321	.304	89	.307	.305	12	.317	12	.302	38	1.044	
39	.325	.304	90	.329	.303	13	.319	13	.302	39	1.059	
40	.321	.303	91	.319	.305	14	.315	14	.303	40	1.322	
41	.320	.303	92	.312	.306	15	.313	15	.303	41	1.312	
42	.321	.303	93	.311	.300	16	.312	16	.303	42	1.310	
43	.317	.303	94	.301	.301	17	.311	17	.303	43	.393	
44	.311	.303	95	.305	.302	18	.310	18	.303	44	.377	
45	.310	.301	96	.302	.797	19	.305	19	.303	45	.349	
46	.307	.301	97	.313	.734	20	.304	20	.302	46	.329	
47	.311	.799					21	.304	21	.303	47	.301
48	.308	.301					22	.304	22	.303	48	.344
49	.308	.302					23	.304	23	.303	49	.304
50	.305	.304					24	.304	24	.303	50	.305
51	.305	.303					25	.305	25	.303		
52	.306	.300	PRISES COL				26	.307	26	.303		
53	.307	.302					27	.306	27	.303		
54	.306	.302	344	1.207		28	.311	28	.303			
55	.309	.799	357	1.134		29	.314	29	.303			
56	.311	.795	332	.395		30	.317	30	.303			
57	.317	.792	377	.321		31	.321	31	.303			
58	.327	.792	1.135	.799		32	.322	32	.303			
						33	.317	33	.303			
						34	.310	34	.303			
						35	.307	35	.303			

***** FICHER AD155 N0KIT= 4
 23/ 3/85 15H20 AS07 M=6 I=-2 R 1-4 ADAPTE 20 AD155
 DE AD144 4'ITE

MACH DE REFERENCE= .5951 UINF= 231.108 M/S
 TIV=296.6 K PIV= 1394 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.596	.594	PRISES DOUBLES			HUB. AMONT	33		.597	1	.598
2	.596	.593					34		.597	2	.594
3	.595	.595	59	.594	.595	1	.594	35	.597	3	.595
4	.593	.594	60	.596	.595	2	.594	36	.597	4	.594
5	.593	.595	61	.594	.594	3	.594	37	.597	5	.595
6	.595	.597	PRISES LAT. GAUCHES			4	.595	38	.597	6	.596
7	.594	.595				5	.594	39	.597	7	.596
8	.595	.595				6	.593	40	.593	8	.597
9	.596	.597	62	.594	.595	7	.594	41	.593	9	.597
10	.597	.593	63	.597	.598	8	.593	42	.593	10	.598
11	.595	.593	64	.597	.597	9	.593	43	.597	11	.598
12	.593	.593	65	.594	.594	10	.593	44	.596	12	.598
13	.594	.593	66	.596	.595	11	.594	45	.596	13	.598
14	.594	.595	67	.599	.598	HUB. RVAL		HUB. DROIT		14	.598
15	.594	.595	68	.599	.599					15	.598
16	.593	.593	69	.598	.598	1	.596	1	.595	16	.598
17	.594	.594	70	.598	.598	2	.595	2	.595	17	.598
18	.597	.595	71	.597	.598	3	.595	3	.595	18	.598
19	.595	.595	72	.596	.598	4	.596	4	.595	19	.598
20	.595	.595	73	.596	.598	5	.596	5	.595	20	.598
21	.593	.595	PRISES LAT. DROITES			6	.596	6	.595	21	.598
22	.596	.595				7	.596	7	.595	22	.598
23	.597	.595	74	.595	.596	8	.597	8	.595	23	.598
24	.597	.595	75	.595	.596	9	.597	9	.595	24	.598
25	.597	.596	76	.594	.594	10	.597	10	.595	25	.598
26	.599	.597	77	.594	.594	11	.596	11	.595	26	.598
27	.601	.593	78	.593	.593	HUB. GAUCHE				27	.598
28	.602	.600	79	.593	.593	12	.599	12	.595	28	.598
29	.601	.599	80	.594	.594	13	.599	13	.595	29	.598
30	.603	.598	81	.598	.598	14	.599	14	.595	30	.598
31	.601	.600	82	.598	.598	1	.599	1	.595	31	.598
32	.602	.601	83	.601	.601	2	.598	2	.595	32	.598
33	.604	.600	84	.606	.602	3	.598	3	.595	33	.598
34	.601	.601	85	.607	.603	4	.598	4	.595	34	.598
35	.601	.600	86	.605	.603	5	.597	5	.595	35	.598
36	.601	.600	87	.603	.603	6	.598	6	.595	36	.598
37	.601	.600	88	.603	.603	7	.598	7	.595	37	.598
38	.601	.600	89	.603	.603	8	.598	8	.595	38	.598
39	.603	.600	90	.607	.603	9	.598	9	.595	39	.598
40	.601	.600	91	.603	.603	10	.598	10	.595	40	.598
41	.601	.600	92	.603	.603	11	.598	11	.595	41	.598
42	.602	.600	93	.604	.603	12	.598	12	.595	42	.598
43	.600	.600	94	.604	.603	13	.598	13	.595	43	.598
44	.600	.600	95	.604	.603	14	.598	14	.595	44	.598
45	.600	.600	96	.603	.603	1	.598	1	.595	45	.598
46	.600	.600	97	.603	.603	2	.598	2	.595	46	.598
47	.600	.600	98	.603	.603	3	.598	3	.595	47	.598
48	.600	.600	99	.603	.603	4	.598	4	.595	48	.598
49	.600	.600	100	.603	.603	5	.598	5	.595	49	.598
50	.600	.600	101	.603	.603	6	.598	6	.595	50	.598
51	.600	.600	102	.603	.603	7	.598	7	.595	51	.598
52	.600	.600	103	.603	.603	8	.598	8	.595	52	.598
53	.600	.600	104	.603	.603	9	.598	9	.595	53	.598
54	.600	.600	105	.603	.603	10	.598	10	.595	54	.598
55	.600	.600	106	.603	.603	11	.598	11	.595	55	.598
56	.600	.600	107	.603	.603	12	.598	12	.595	56	.598
57	.600	.600	108	.603	.603	13	.598	13	.595	57	.598
58	.601	.600	109	.603	.603	14	.598	14	.595	58	.598
59	.601	.600	PRISES COL			1	.598	1	.595	59	.598
60	.601	.600				2	.598	2	.595	60	.598
61	.601	.600	110	.604	.604	3	.598	3	.595	61	.598
62	.601	.600	111	.604	.604	4	.598	4	.595	62	.598
63	.601	.600	112	.604	.604	5	.598	5	.595	63	.598
64	.601	.600	113	.604	.604	6	.598	6	.595	64	.598
65	.601	.600	114	.604	.604	7	.598	7	.595	65	.598
66	.601	.600	115	.604	.604	8	.598	8	.595	66	.598
67	.601	.600	116	.604	.604	9	.598	9	.595	67	.598
68	.601	.600	117	.604	.604	10	.598	10	.595	68	.598
69	.601	.600	118	.604	.604	11	.598	11	.595	69	.598
70	.601	.600	119	.604	.604	12	.598	12	.595	70	.598

***** FICHER AD156 NOKIT= 1
 23/ 8-85 15H40 AS07 M=5 I=-3 R 1-4 NON ADAPTE AD156
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

 MACH DE REFERENCE= .5950 UINF= 231.109 M/S
 TIV=301.1 K PIV= 1395 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.596	.595	PRISES DOUBLES			HUB. AMONT	33	.604		1	.594
2	.596	.598					34	.604		2	.597
3	.596	.595	59	.596	.596	1	.596	35	.604	3	.592
4	.594	.595	60	.597	.598	2	.598	36	.602	4	.593
5	.594	.596	61	.599	.598	3	.596	37	.603	5	.597
6	.596	.598				4	.596	38	.603	6	.594
7	.596	.596	PRISES LAT. GAUCHES			5	.595	39	.604	7	.591
8	.597	.595				6	.595	40	.605	8	.595
9	.597	.598	62	.594	.595	7	.595	41	.605	9	.596
10	.597	.595	63	.597	.599	8	.596	42	.605	10	.731
11	.595	.596	64	.599	.599	9	.595	43	.604	11	.741
12	.593	.596	65	.600	.599	10	.596	44	.603	12	.705
13	.594	.595	66	.603	.601	11	.596	45	.603	13	.699
14	.594	.597	67	.607	.603					14	.613
15	.595	.597	68	.608	.605	HUB. AVANT		HUB. DROIT		15	.613
16	.595	.595	69	.609	.608	1	.599	1	.595	16	.601
17	.596	.596	70	.610	.603	2	.600	2	.596	17	.604
18	.598	.596	71	.602	.601	3	.599	3	.595	18	.604
19	.597	.597	72	.601	.600	4	.601	4	.595	19	.603
20	.599	.598	73	.588	.600	5	.599	5	.595	20	.603
21	.599	.600	PRISES LAT. DROITES			6	.599	6	.595	21	.605
22	.603	.600				7	.599	7	.595	22	.603
23	.603	.601	74	.595	.598	8	.600	8	.595	23	.603
24	.603	.603	75	.595	.596	9	.601	9	.595	24	.603
25	.604	.605	76	.595	.595	10	.601	10	.595	25	.603
26	.604	.604	77	.594	.594	11	.600	11	.595	26	.603
27	.605	.603	78	.595	.595					27	.603
28	.607	.604	79	.596	.594	HUB. GAUCHE				28	.603
29	.609	.605	80	.594	.599	13	.600	13	.595	29	.603
30	.608	.604	81	.604	.603	14	.600	14	.595	30	.603
31	.612	.604	91	.606	.603	15	.600	15	.595	31	.603
32	.610	.607	92	.604	.605	16	.607	16	.595	32	.603
33	.611	.608	93	.609	.606	17	.606	17	.595	33	.603
34	.609	.606	94	.614	.607	18	.601	18	.595	34	.603
35	.611	.608	95	.615	.608	19	.602	19	.595	35	.603
36	.611	.609	96	.614	.609	20	.604	20	.595	36	.603
37	.612	.606	97	.614	.610	21	.603	21	.595	37	.603
38	.611	.605	98	.613	.608	22	.607	22	.595	38	.603
39	.613	.604	99	.618	.604	23	.608	23	.595	39	.603
40	.611	.603	90	.613	.604	10	.607	10	.595	40	.603
41	.611	.603	91	.607	.604	11	.605	11	.595	41	.603
42	.613	.603	92	.604	.602	12	.605	12	.595	42	.603
43	.609	.603	93	.608	.609	13	.605	13	.595	43	.603
44	.606	.603	94	.601	.603	14	.605	14	.595	44	.603
45	.605	.602	95	.607	.606	15	.602	15	.595	45	.603
46	.603	.603	96	.606	.608	16	.601	16	.595	46	.603
47	.603	.601				17	.601	17	.595	47	.603
48	.602	.600				18	.601	18	.595	48	.603
49	.601	.598				19	.602	19	.595	49	.603
50	.599	.598				20	.603	20	.595	50	.603
51	.600	.599				21	.604	21	.595		
52	.599	.597	PRISES COL			22	.604	22	.595		
53	.600	.598				23	.605	23	.595		
54	.599	.598	.576	1.049		24	.605	24	.595		
55	.598	.595	.574	.925		25	.607	25	.595		
56	.594	.593	.594	.901		26	.606	26	.595		
57	.591	.592	.560	.894		27	.609	27	.595		
58	.586	.589	1.017	.833		28	.608	28	.595		
						29	.608	29	.595		
						30	.606	30	.595		
						31	.604	31	.595		
						32	.604	32	.595		

***** FICHER AD157 NOKIT= 1
 23/ 8/89 16H10 AS07 M#6 I=-2 R 1-4 ADAPTE 3D AD157
 DE AD9142 1'ITE.

 MACH DE REFERENCE= .5961 UINF= 231.108 M/S
 TIV=301.3 K PIV= 1395 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.597	.596	*	PRISES DOUBLES		HUB. AMONT	33	.599	*	1	.589
2	.597	.599	*				34	.599	*	2	.582
3	.597	.597	*	59	.595	.595	35	.599	*	3	.585
4	.595	.596	*	60	.597	.599	36	.599	*	4	.588
5	.594	.596	*	61	.598	.598	37	.599	*	5	.581
6	.596	.598	*				38	.598	*	6	.560
7	.596	.596	*	PRISES LAT. GAUCHES			39	.599	*	7	.527
8	.596	.595	*				40	.599	*	8	.533
9	.597	.598	*	62	.595	.595	41	.599	*	9	.578
10	.597	.595	*	63	.599	.599	42	.599	*	10	.724
11	.595	.596	*	64	.599	.599	43	.599	*	11	.703
12	.593	.595	*	65	.596	.597	44	.599	*	12	.698
13	.595	.595	*	66	.596	.596	45	.599	*	13	.633
14	.594	.596	*	67	.599	.599			*	14	.671
15	.594	.596	*	68	.591	.599	HUB. AVAL	HUB. DROIT	*	15	.655
16	.595	.595	*	69	.599	.591			*	16	.660
17	.596	.596	*	70	.599	.599	1	.599	*	17	.657
18	.599	.597	*	71	.599	.599	2	.599	*	18	.657
19	.596	.597	*	72	.599	.591	3	.599	*	19	.657
20	.596	.598	*	73	.598	.594	4	.599	*	20	.661
21	.595	.598	*				5	.599	*	21	.660
22	.598	.596	*	PRISES LAT. DROITES			6	.599	*	22	.662
23	.598	.596	*				7	.599	*	23	.657
24	.598	.597	*	74	.596	.599	8	.591	*	24	.677
25	.597	.599	*	75	.599	.599	9	.591	*	25	.687
26	.597	.598	*	76	.595	.595	10	.599	*	26	.691
27	.597	.599	*	77	.595	.595	11	.599	*	27	.684
28	.599	.599	*	78	.595	.595	12	.599	*	28	.682
29	.599	.599	*	79	.595	.595	13	.599	*	29	.702
30	.599	.599	*	80	.599	.599	HUB. GAUCHE		*	30	.685
31	.596	.599	*	81	.599	.599	1	.599	*	31	.689
32	.594	.599	*	82	.599	.599	2	.599	*	32	.726
33	.593	.599	*	83	.599	.599	3	.599	*	33	.689
34	.599	.599	*	84	.599	.599	4	.599	*	34	.705
35	.599	.599	*	85	.599	.599	5	.599	*	35	.717
36	.591	.599	*	86	.599	.599	6	.599	*	36	.694
37	.593	.599	*	87	.599	.599	7	.599	*	37	.683
38	.593	.599	*	88	.599	.599	8	.599	*	38	.683
39	.596	.599	*	89	.599	.599	9	.599	*	39	.685
40	.594	.599	*	90	.599	.599	10	.599	*	40	.684
41	.594	.599	*	91	.599	.599	11	.599	*	41	.680
42	.595	.599	*	92	.599	.599	12	.599	*	42	.680
43	.592	.599	*	93	.599	.599	13	.599	*	43	.678
44	.598	.599	*	94	.599	.599	14	.599	*	44	.675
45	.597	.599	*	95	.599	.599	15	.599	*	45	.673
46	.597	.599	*	96	.599	.599	16	.597	*	46	.669
47	.591	.599	*				17	.597	*	47	.651
48	.591	.598	*				18	.597	*	48	.641
49	.599	.599	*				19	.595	*	49	.659
50	.597	.598	*				20	.597	*	50	.640
51	.598	.599	*				21	.599	*		
52	.599	.598	*	PRISES COL			22	.599	*	22	.66
53	.591	.599	*				23	.597	*	23	.67
54	.599	.599	*	.558	1.054		24	.591	*	24	.68
55	.599	.599	*	.594	.928		25	.591	*	25	.69
56	.596	.598	*	.797	.802		26	.592	*	26	.697
57	.591	.599	*	.859	.594		27	.593	*	27	.695
58	.589	.599	*	1.028	.633		28	.594	*	28	.695
			*				29	.592	*	29	.695
			*				30	.591	*	30	.695
			*				31	.599	*	31	.695
			*				32	.599	*	32	.695

***** FICHER AD158 NOKIT= 4
 26/ 8/85 10H35 AS07 M=6 I=-2 R 3-5 ADAPTE 2D AD158
 DE AD144 4'ITE.

MACH DE REFERENCE= .5955 UINF= 331.109 M/S
 TIV=294.7 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	SAS	I	HAUT	SAS	I	MACH	I	MACH	I	MACH
1	.596	.594	PRISES DOUBLES			HUB. AMONT	33	.598	1	.564	
2	.596	.598					34	.598	2	.565	
3	.596	.597	59	.595	.595	1	.595	35	.598	3	.561
4	.595	.597	60	.596	.596	2	.595	36	.597	4	.560
5	.595	.598	61	.594	.594	3	.594	37	.598	5	.562
6	.595	.598	PRISES LAT. GAUCHES			4	.594	38	.598	6	.564
7	.595	.595	62	.595	.597	5	.594	39	.598	7	.565
8	.596	.594	63	.595	.597	6	.594	40	.599	8	.565
9	.596	.596	64	.597	.597	7	.594	41	.600	9	.569
10	.596	.593	65	.597	.597	8	.594	42	.600	10	.569
11	.595	.594	66	.597	.597	9	.594	43	.598	11	.560
12	.594	.595	67	.596	.594	10	.594	44	.597	12	.562
13	.595	.594	68	.596	.596	11	.594	45	.596	13	.563
14	.595	.595	69	.600	.596	HUB. AVANT		HUB. DROIT		14	.563
15	.596	.595	70	.599	.597	1	.595	1	.595	15	.567
16	.596	.594	71	.601	.597	2	.597	2	.595	16	.567
17	.595	.594	72	.598	.596	3	.597	3	.595	17	.565
18	.596	.595	73	.597	.595	4	.597	4	.595	18	.565
19	.594	.595	74	.600	.597	5	.597	5	.595	19	.565
20	.595	.598	PRISES LAT. DROITES			6	.597	6	.595	20	.567
21	.596	.593	75	.596	.599	7	.597	7	.595	21	.567
22	.600	.594	76	.595	.595	8	.598	8	.595	22	.566
23	.599	.593	77	.595	.594	9	.598	9	.595	23	.566
24	.598	.599	78	.595	.593	10	.597	10	.595	24	.566
25	.597	.598	79	.594	.593	11	.597	11	.595	25	.565
26	.599	.598	80	.594	.593	HUB. GAUCHE		12	.595	26	.565
27	.601	.599	81	.601	.598	1	.600	13	.595	27	.565
28	.602	.600	82	.602	.595	2	.600	14	.595	28	.565
29	.602	.600	83	.602	.600	3	.600	15	.595	29	.565
30	.604	.601	84	.601	.599	4	.599	16	.599	30	.565
31	.603	.601	85	.607	.600	5	.597	17	.599	31	.565
32	.603	.601	86	.608	.601	6	.597	18	.599	32	.565
33	.602	.599	87	.605	.601	7	.598	19	.599	33	.565
34	.602	.599	88	.605	.601	8	.598	20	.599	34	.565
35	.603	.598	89	.604	.600	9	.598	21	.599	35	.565
36	.604	.597	90	.604	.600	10	.598	22	.599	36	.565
37	.603	.597	91	.603	.598	11	.599	23	.599	37	.565
38	.603	.596	92	.605	.598	12	.599	24	.599	38	.565
39	.603	.596	93	.600	.596	13	.599	25	.599	39	.565
40	.601	.596	94	.597	.594	14	.599	26	.599	40	.565
41	.603	.595	95	.597	.594	15	.599	27	.599	41	.565
42	.603	.595	96	.593	.593	16	.599	28	.599	42	.565
43	.603	.595	97	.597	.593	17	.599	29	.599	43	.565
44	.603	.595	98	.597	.593	18	.599	30	.599	44	.565
45	.603	.595	99	.597	.593	19	.599	31	.599	45	.565
46	.600	.595	100	.597	.593	20	.599	32	.599	46	.565
47	.600	.595	PRISES COL			21	.599	33	.599	47	.565
48	.600	.595	1.013	.594	.594	22	.599	34	.599	48	.565
49	.600	.595	1.014	.594	.594	23	.599	35	.599	49	.565
50	.600	.595	1.014	.594	.594	24	.599	36	.599	50	.565
51	.600	.595	1.014	.594	.594	25	.599	37	.599	51	.565
52	.600	.595	1.014	.594	.594	26	.599	38	.599	52	.565
53	.600	.595	1.014	.594	.594	27	.599	39	.599	53	.565
54	.600	.595	1.014	.594	.594	28	.599	40	.599	54	.565
55	.600	.595	1.014	.594	.594	29	.599	41	.599	55	.565
56	.600	.595	1.014	.594	.594	30	.599	42	.599	56	.565
57	.600	.595	1.014	.594	.594	31	.599	43	.599	57	.565
58	.600	.595	1.014	.594	.594	32	.599	44	.599	58	.565
59	.600	.595	1.014	.594	.594	33	.599	45	.599	59	.565
60	.600	.595	1.014	.594	.594	34	.599	46	.599	60	.565

***** FICHER AD159 NOCIT= 1
 26/ 8/85 11H 0 AS07 M=6 I=-2 R 3-5 NON ADAPTE AD159
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .5958 UINF= 331.108 M/S
 TIV=398.9 K PIV= 1392 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				RILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.596	.595	PRISES DOUBLES			HUB. AMONT	33	.595	1	.574	
2	.597	.599				34	.594	2	.593		
3	.596	.596	59	.595	.595	35	.594	3	.594		
4	.595	.595	59	.597	.598	36	.592	4	.593		
5	.594	.595	61	.597	.595	37	.593	5	.704		
6	.596	.597				38	.593	6	.597		
7	.596	.595	PRISES LAT. GAUCHES			39	.594	7	.599		
8	.597	.599				40	.595	8	.599		
9	.597	.599	62	.595	.595	41	.595	9	.592		
10	.597	.595	63	.597	.599	42	.595	10	.598		
11	.595	.595	64	.599	.599	43	.594	11	.700		
12	.592	.595	65	.599	.599	44	.597	12	.713		
13	.593	.595	66	.592	.599	45	.593	13	.700		
14	.594	.595	67	.611	.601	HUB. AVAL		14	.599		
15	.595	.597	68	.610	.603	HUB. DROIT	15	.592			
16	.596	.595	69	.607	.605	1	.591	15	.599		
17	.597	.597	70	.610	.601	2	.590	17	.597		
18	.599	.597	71	.601	.599	3	.590	18	.595		
19	.598	.597	72	.601	.599	4	.592	19	.595		
20	.599	.599	73	.599	.599	5	.592	20	.598		
21	.599	.599				6	.591	21	.599		
22	.593	.599	PRISES LAT. DROITES			7	.590	22	.598		
23	.594	.592				8	.590	23	.593		
24	.593	.594	74	.596	.593	9	.590	24	.591		
25	.593	.595	75	.596	.595	10	.599	25	.593		
26	.593	.593	76	.595	.595	11	.599	26	.597		
27	.596	.594	77	.594	.594	HUB. GAUCHE		27	.701		
28	.590	.595	78	.595	.595	1	.598	28	.708		
29	.594	.595	79	.597	.595	2	.597	29	.703		
30	.592	.595	80	.594	.590	3	.596	30	.707		
31	.594	.594	81	.595	.593	4	.592	31	.597		
32	.592	.594	82	.594	.596	5	.593	32	.593		
33	.592	.593	83	.599	.593	6	.592	33	.597		
34	.590	.595	84	.597	.594	7	.595	34	.597		
35	.590	.595	85	.595	.596	8	.594	35	.597		
36	.590	.595	86	.595	.597	9	.595	36	.597		
37	.591	.595	87	.593	.593	10	.595	37	.597		
38	.591	.594	88	.593	.595	11	.595	38	.597		
39	.594	.594	89	.597	.592	12	.595	39	.597		
40	.591	.592	90	.593	.592	13	.595	40	.597		
41	.591	.592	91	.597	.592	14	.595	41	.597		
42	.592	.592	92	.599	.599	15	.592	42	.597		
43	.590	.593	93	.599	.597	16	.595	43	.597		
44	.597	.593	94	.591	.597	17	.595	44	.597		
45	.595	.591	95	.596	.599	18	.592	45	.597		
46	.593	.591	96	.597	.597	19	.592	46	.597		
47	.593	.593				20	.592	47	.597		
48	.593	.593				21	.592	48	.597		
49	.593	.593				22	.592	49	.597		
50	.592	.593				23	.593	50	.597		
51	.591	.593				24	.593				
52	.593	.595	PRISES COL			25	.594				
53	.593	.597				26	.593				
54	.593	.593	.554	1.045		27	.596				
55	.597	.595	.592	.925		28	.597				
56	.594	.593	.793	.801		29	.597				
57	.592	.591	.860	.922		30	.598				
58	.593	.599	1.015	.592		31	.594				
						32	.595				

***** FICHER AD160 NOCIT)= 1
 28/ 3/85 11H25 A907 M=6 I=-2 R 3-6 ADAPTE 3D AD160
 DE AD9142 1'ITE.

MACH DE REFERENCE= .5964 UNF= 231.103 M/S
 TIV=297.3 K PIV= 1390 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE A907	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
							HUB. AMONT				
1	.598	.596				33	.599			1	.570
2	.597	.599				34	.599			2	.589
3	.596	.597	59	.595	.595	35	.599			3	.600
4	.594	.597	60	.598	.599	36	.599			4	.601
5	.594	.597	61	.600	.597	37	.599			5	.600
6	.595	.598				38	.599			6	.600
7	.595	.598				39	.599			7	.600
8	.597	.598				40	.600			8	.600
9	.598	.598	62	.595	.597	41	.601			9	.600
10	.598	.598	63	.599	.601	42	.601			10	.600
11	.595	.597	64	.600	.599	43	.599			11	.600
12	.594	.598	65	.597	.598	44	.599			12	.600
13	.595	.597	66	.597	.595	45	.598			13	.600
14	.595	.597	67	.603	.598					14	.600
15	.596	.597	68	.601	.598	HUB. AVAL	HUB. DROIT			15	.675
16	.597	.597	69	.600	.599	1	.600	1	.597	16	.679
17	.598	.597	70	.604	.597	2	.600	2	.596	17	.680
18	.598	.598	71	.600	.597	3	.600	3	.598	18	.678
19	.598	.599	72	.601	.599	4	.600	4	.597	19	.679
20	.597	.598	73	.594	.602	5	.600	5	.597	20	.681
21	.596	.599				6	.599	6	.597	21	.682
22	.598	.599				7	.600	7	.597	22	.681
23	.598	.599				8	.601	8	.596	23	.685
24	.598	.599	74	.596	.599	9	.600	9	.596	24	.688
25	.598	.599	75	.596	.597	10	.599	10	.596	25	.685
26	.598	.599	76	.597	.596	11	.599	11	.596	26	.685
27	.598	.599	77	.595	.596			12	.597	27	.681
28	.598	.599	78	.595	.596			13	.596	28	.685
29	.598	.599	79	.596	.596			14	.597	29	.685
30	.598	.599	80	.600	.599	HUB. GAUCHE				30	.684
31	.596	.599	81	.601	.599	1	.601			31	.684
32	.594	.599	82	.599	.600	2	.600			32	.684
33	.594	.599	83	.603	.600	3	.600			33	.684
34	.591	.599	84	.609	.602	4	.598			34	.684
35	.592	.599	85	.610	.603	5	.598			35	.684
36	.592	.599	86	.607	.603	6	.599			36	.684
37	.593	.599	87	.605	.602	7	.600			37	.684
38	.593	.599	88	.605	.601	8	.601			38	.684
39	.595	.599	89	.610	.599	9	.602			39	.684
40	.594	.599	90	.607	.598	10	.602			40	.684
41	.594	.599	91	.603	.596	11	.600			41	.684
42	.595	.599	92	.602	.598	12	.600			42	.684
43	.594	.599	93	.597	.597	13	.600			43	.684
44	.592	.599	94	.601	.597	14	.600			44	.684
45	.591	.599	95	.600	.594	15	.599			45	.684
46	.590	.599	96	.592	.592	16	.598			46	.684
47	.592	.599				17	.598			47	.684
48	.591	.599				18	.598			48	.684
49	.590	.599				19	.598			49	.684
50	.599	.599				20	.598			50	.684
51	.590	.599				21	.598				
52	.591	.599				22	.598				
53	.591	.599				23	.597				
54	.591	.599				24	.600				
55	.590	.599				25	.601				
56	.590	.599				26	.603				
57	.596	.599				27	.604				
58	.592	.599				28	.604				
59	.590	.599				29	.604				
60	.590	.599				30	.602				
						31	.600				
						32	.599				

***** FICHER AD162 NOKIT= 1
 26/ 8/85 14H20 AS07 M=.5 I=0 R 3-6 NON ADAPTE AD162
 DE AD4 L'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .5979 UINF= 231.108 M/S
 TIV=299.4 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.597	.596	PRISES DOUBLES			HUB. AMONT		33	.604	1	.559
2	.597	.600						34	.604	2	.580
3	.597	.598	59	.597	.598	1	.598	35	.603	3	.620
4	.596	.597	60	.599	.599	2	.599	36	.602	4	.659
5	.596	.597	61	.602	.599	3	.599	37	.603	5	.674
6	.598	.599				4	.599	38	.602	6	.653
7	.598	.598	PRISES LAT. GAUCHES			5	.597	39	.603	7	.625
8	.598	.597				6	.597	40	.603	8	.606
9	.598	.599	62	.596	.597	7	.598	41	.605	9	.622
10	.599	.599	63	.600	.601	8	.598	42	.604	10	.640
11	.598	.598	64	.600	.601	9	.598	43	.603	11	.633
12	.596	.598	65	.603	.599	10	.598	44	.603	12	.7190
13	.598	.598	66	.607	.600	11	.598	45	.602	13	.7164
14	.598	.600	67	.611	.600					14	.7146
15	.599	.600	68	.613	.601	HUB. AVAL		HUB. DROIT		15	.7229
16	.598	.598	69	.614	.604	1	.602	1	.597	16	.7207
17	.599	.598	70	.615	.600	2	.603	2	.599	17	.724
18	.601	.593	71	.605	.600	3	.603	3	.599	18	.719
19	.600	.597	72	.602	.601	4	.603	4	.598	19	.717
20	.603	.599	73	.599	.603	5	.603	5	.598	20	.714
21	.604	.599				6	.603	6	.598	21	.709
22	.607	.599	PRISES LAT. DROITES			7	.603	7	.598	22	.701
23	.609	.599				8	.603	8	.598	23	.692
24	.609	.602	74	.597	.599	9	.604	9	.598	24	.690
25	.611	.602	75	.597	.598	10	.604	10	.598	25	.688
26	.610	.602	76	.597	.596	11	.602	11	.602	26	.627
27	.613	.603	77	.599	.597			12	.598	27	.673
28	.614	.601	78	.597	.596	HUB. GAUCHE		13	.598	28	.654
29	.617	.601	79	.600	.595	1	.613	13	.598	29	.654
30	.616	.601	80	.609	.598	2	.613	14	.598	30	.634
31	.620	.599	81	.612	.600	3	.612	15	.598	31	.626
32	.618	.603	82	.613	.602	4	.612	16	.598	32	.621
33	.619	.603	83	.617	.600	5	.612	17	.599	33	.655
34	.617	.602	84	.623	.600	6	.615	18	.599	34	.600
35	.620	.603	85	.625	.601	7	.615	19	.599	35	.7161
36	.619	.604	86	.623	.602	8	.611	20	.598	36	.7145
37	.620	.602	87	.622	.603	9	.611	21	.598	37	.7135
38	.619	.602	88	.621	.602	10	.613	22	.598	38	.7128
39	.621	.601	89	.624	.601	11	.613	23	.598	39	.7119
40	.618	.601	90	.619	.601	12	.612	24	.598	40	.709
41	.619	.601	91	.612	.600	13	.611	25	.598	41	.7086
42	.618	.601	92	.607	.599	14	.610	26	.598	42	.699
43	.615	.600	93	.601	.599	15	.609	27	.598	43	.697
44	.612	.600	94	.603	.600	16	.608	28	.598	44	.6882
45	.610	.599	95	.599	.591	17	.608	29	.598	45	.6771
46	.608	.600	96	.606	.588	18	.604	30	.598	46	.664
47	.607	.599				19	.605	31	.598	47	.6583
48	.606	.600				20	.605	32	.598	48	.6553
49	.605	.600				21	.605	33	.598	49	.6524
50	.604	.601				22	.605	34	.598	50	.6497
51	.604	.601				23	.606	35	.597		
52	.603	.600	PRISES OCL			24	.606	36	.597		
53	.602	.600				25	.605	37	.597		
54	.601	.600				26	.608	38	.597		
55	.599	.597				27	.609	39	.597		
56	.595	.595				28	.610	40	.598		
57	.591	.592				29	.611	41	.598		
58	.584	.597	1.319	.630		30	.612	42	.598		
						31	.610	43	.598		
						32	.608	44	.598		
								45	.598		

***** FICHER AD163 NO(IT)= 1
 26/ 3/85 14H40 AS07 M=.6 I=0 R 3-6 ADAPTE 3D AD163
 DE AD9107 1'ITE.

MACH DE REFERENCE= .5980 UNF= 231.108 M/S
 TIV=298.8 K PIV= 1390 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.599	.597	PRISES DOUBLES			HUB. AMONT		33	.601	1	.607
2	.599	.601						34	.600	2	.607
3	.598	.599	59	.598	.599	1	.599	35	.600	3	.617
4	.596	.598	60	.598	.598	2	.598	36	.600	4	.617
5	.596	.599	61	.603	.599	3	.598	37	.600	5	.617
6	.599	.600				4	.598	38	.600	6	.617
7	.598	.598	PRISES LAT. GAUCHES			5	.598	39	.600	7	.617
8	.599	.597	62	.597	.598	6	.598	40	.600	8	.612
9	.598	.598	63	.600	.601	7	.598	41	.601	9	.613
10	.599	.596	64	.601	.602	8	.597	42	.600	10	.621
11	.598	.597	65	.598	.597	9	.597	43	.599	11	.613
12	.596	.597	66	.599	.598	10	.597	44	.598	12	.613
13	.597	.597	67	.603	.601	11	.598	45	.598	13	.615
14	.598	.599	68	.604	.600	HUB. AVAL		HUB. DROIT		14	.613
15	.598	.600	69	.604	.602	1	.604	1	.598	15	.615
16	.599	.599	70	.606	.599	2	.604	2	.598	16	.615
17	.599	.600	71	.600	.597	3	.603	3	.598	17	.613
18	.602	.598	72	.603	.599	4	.603	4	.598	18	.608
19	.600	.597	73	.598	.602	5	.603	5	.598	19	.607
20	.599	.598				6	.602	6	.599	20	.604
21	.599	.598	PRISES LAT. DROITES			7	.603	7	.599	21	.608
22	.601	.598	74	.598	.600	8	.603	8	.599	22	.604
23	.602	.597	75	.598	.599	9	.605	9	.598	23	.605
24	.601	.599	76	.598	.596	10	.604	10	.598	24	.605
25	.602	.600	77	.597	.596	11	.602	11	.600	25	.605
26	.601	.599	78	.597	.597	12	.601	12	.600	26	.611
27	.604	.599	79	.598	.594	HUB. GAUCHE		13	.600	27	.605
28	.605	.601	80	.603	.596	14	.604	14	.600	28	.643
29	.608	.601	81	.605	.597	15	.604	15	.600	29	.643
30	.606	.600	82	.603	.599	16	.603	16	.600	30	.622
31	.609	.598	83	.608	.600	17	.603	17	.600	31	.622
32	.607	.601	84	.613	.600	18	.600	18	.600	32	.622
33	.609	.601	85	.615	.601	19	.600	19	.600	33	.622
34	.607	.599	86	.613	.601	20	.602	20	.600	34	.622
35	.608	.600	87	.612	.601	21	.604	21	.600	35	.622
36	.607	.600	88	.612	.600	22	.605	22	.600	36	.622
37	.609	.599	89	.615	.600	23	.605	23	.600	37	.622
38	.609	.600	90	.609	.600	24	.604	24	.600	38	.622
39	.611	.600	91	.605	.597	25	.603	25	.600	39	.622
40	.610	.599	92	.603	.598	26	.603	26	.600	40	.622
41	.609	.599	93	.609	.598	27	.603	27	.600	41	.622
42	.608	.598	94	.604	.597	28	.602	28	.600	42	.622
43	.606	.597	95	.602	.597	29	.601	29	.600	43	.622
44	.603	.597	96	.595	.584	30	.600	30	.600	44	.622
45	.602	.596				31	.600	31	.600	45	.622
46	.602	.597				32	.600	32	.600	46	.622
47	.603	.597				33	.600	33	.600	47	.622
48	.603	.599				34	.600	34	.600	48	.622
49	.603	.599				35	.600	35	.600	49	.622
50	.603	.600				36	.601	36	.600	50	.622
51	.605	.600				37	.601	37	.600	51	.622
52	.604	.600	PRISES COL			38	.601	38	.600	52	.622
53	.605	.600	1.020	1.024	.602	39	.602	39	.600	53	.622
54	.605	.600	1.021	1.026	.603	40	.604	40	.600	54	.622
55	.604	.597				41	.606	41	.600	55	.622
56	.601	.593				42	.606	42	.600	56	.622
57	.609	.609				43	.604	43	.600	57	.622
58	.605	.602	1.021	1.030	.606	44	.603	44	.600	58	.622
						45	.601	45	.600		

***** FICHER AD164 NOCIT= 4
 25/08/85 15H 5 A907 M=8 I=0 R 3-6 ADAPTE 2D AD164
 DE AD134 4'ITE.

MACH DE REFERENCE= .3067 UINF= 231.108 M/S
 TIV=294.0 K PIV= 1653 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE A907	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.306	.302	PRISES DOUBLES			HUB. AMONT	33	.311	1	.753	
2	.306	.303					34	.310	2	.789	
3	.307	.306	59	.304	.304	1	.304	35	.309	3	.865
4	.305	.306	60	.305	.305	2	.302	36	.308	4	.955
5	.305	.303	61	.307	.302	3	.301	37	.308	5	.950
6	.307	.303				4	.302	38	.307	6	.899
7	.304	.304	PRISES LAT. GAUCHES			5	.300	39	.308	7	.851
8	.305	.302				6	.300	40	.310	8	.817
9	.305	.306	62	.305	.306	7	.300	41	.312	9	.406
10	.306	.300	63	.797	.309	8	.799	42	.310	10	1.414
11	.303	.302	64	.310	.305	9	.300	43	.307	11	1.376
12	.300	.304	65	.311	.307	10	.300	44	.307	12	1.285
13	.303	.303	66	.311	.302	11	.300	45	.305	13	1.030
14	.303	.305	67	.323	.305					14	1.025
15	.305	.304	68	.319	.303	HUB. AVAL		HUB. DROIT		15	1.013
16	.306	.300	69	.321	.313					16	1.028
17	.306	.300	70	.325	.305	1	.308	1	.305	17	1.018
18	.306	.303	71	.310	.302	2	.307	2	.305	18	1.010
19	.306	.304	72	.303	.305	3	.306	3	.305	19	1.023
20	.310	.307	73	.305	.310	4	.307	4	.305	20	1.012
21	.311	.307				5	.306	5	.304	21	1.303
22	.312	.305	PRISES LAT. DROITES			6	.305	6	.305	22	.380
23	.314	.302				7	.305	7	.305	23	.355
24	.314	.303	74	.306	.309	8	.306	8	.305	24	.753
25	.315	.305	75	.304	.304	9	.307	9	.304	25	.719
26	.313	.303	76	.303	.300	10	.305	10	.305	26	.859
27	.325	.301	77	.302	.302	11	.305	11	.305	27	.956
28	.327	.305	78	.302	.795					28	.958
29	.335	.306	79	.304	.798	HUB. GAUCHE				29	.903
30	.330	.307	80	.313	.304					30	.963
31	.337	.304	81	.320	.303	1	.322	13	.305	31	.955
32	.331	.311	82	.319	.302	2	.321	14	.305	32	.416
33	.334	.313	83	.333	.303	3	.321	15	.305	33	1.512
34	.327	.310	84	.346	.306	4	.310	16	.305	34	1.433
35	.330	.312	85	.347	.310	5	.311	17	.305	35	1.334
36	.323	.313	86	.340	.313	6	.316	18	.305	36	1.051
37	.332	.310	87	.335	.313	7	.320	19	.305	37	1.043
38	.329	.309	88	.333	.310	8	.325	20	.305	38	1.034
39	.333	.307	89	.337	.304	9	.326	21	.305	39	1.005
40	.330	.305	90	.327	.304	10	.322	22	.305	40	.994
41	.329	.304	91	.317	.305	11	.320	23	.305	41	.986
42	.330	.304	92	.314	.303	12	.319	24	.305	42	.971
43	.324	.304	93	.303	.302	13	.318	25	.305	43	.970
44	.317	.304	94	.307	.303	14	.316	26	.305	44	.927
45	.317	.303	95	.306	.300	15	.310	27	.305	45	.906
46	.312	.304	96	.302	.797	16	.309	28	.305	46	.893
47	.313	.303				17	.309	29	.305	47	.831
48	.311	.304				18	.309	30	.305	48	.850
49	.313	.304				19	.310	31	.305	49	.875
50	.307	.305				20	.310	32	.304	50	.822
51	.303	.304				21	.312	33	.304		
52	.310	.303	PRISES COL			22	.313	34	.304		
53	.310	.305				23	.311	35	.304		
54	.309	.304	.352	1.213		24	.317	36	.304		
55	.309	.303	.371	1.213		25	.319	37	.304		
56	.306	.301	.307	.300		26	.322	38	.304		
57	.306	.302	.382	.325		27	.326	39	.304		
58	.306	.798	1.141	.793		28	.328	40	.304		
						29	.322	41	.304		
						30	.325	42	.304		
						31	.311	43	.304		
						32	.313	44	.304		
								45	.304		

***** FICHER AD155 NACITE 1
 26/ 8/85 15H35 AS07 M=8 I=0 R 3-5 NON ADAPTE AD155
 DE AD4 L'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .3046 UINF= 231.103 M/S
 TIV=299.1 K PIV= 1651 MB

MACH PAROIS HAUTE ET BASSE				MACH PAROIS LATER.				FILE AS07	
I	HAUT	BAS		I	HAUT	BAS		I	MACH
1	.303	.301	+	PRISES DOUBLES			HUB. AMONT	33	.302
2	.305	.309	+					34	.301
3	.304	.305	+	59	.305	.305	1	.303	.309
4	.300	.305	+	60	.305	.307	2	.303	.309
5	.300	.305	+	61	.316	.313	3	.302	.324
6	.305	.309	+	FRISES LAT. GAUCHES			4	.303	.327
7	.305	.306	+	52	.303	.305	5	.302	.319
8	.305	.306	+	63	.798	.311	6	.303	.323
9	.308	.305	+	64	.310	.310	7	.303	.323
10	.303	.305	+	65	.319	.313	8	.302	.327
11	.303	.305	+	66	.328	.318	9	.302	.326
12	.799	.305	+	67	.346	.323	10	.303	.324
13	.301	.304	+	68	.352	.327	11	.303	.324
14	.302	.307	+	69	.353	.323	HUB. AVAL		
15	.303	.306	+	70	.356	.323	12	.320	.305
16	.303	.303	+	71	.326	.316	13	.318	.305
17	.305	.304	+	72	.331	.320	14	.317	.304
18	.309	.305	+	73	.305	.323	15	.316	.305
19	.310	.306	+	FRISES LAT. DROITES			16	.315	.304
20	.315	.310	+	74	.303	.309	17	.315	.304
21	.313	.312	+	75	.306	.307	18	.316	.304
22	.324	.317	+	76	.305	.303	19	.317	.304
23	.329	.314	+	77	.302	.301	20	.316	.305
24	.330	.319	+	78	.303	.300	21	.316	.305
25	.333	.321	+	79	.303	.300	22	.317	.305
26	.335	.321	+	80	.309	.300	23	.316	.305
27	.345	.325	+	81	.326	.305	24	.316	.305
28	.349	.323	+	82	.325	.305	25	.317	.305
29	.361	.325	+	83	.323	.305	26	.317	.305
30	.356	.322	+	84	.323	.305	27	.317	.305
31	.364	.322	+	85	.323	.305	28	.317	.305
32	.367	.322	+	86	.323	.305	29	.317	.305
33	.372	.322	+	87	.323	.305	30	.317	.305
34	.366	.322	+	88	.323	.305	31	.317	.305
35	.371	.322	+	89	.323	.305	32	.317	.305
36	.363	.322	+	90	.323	.305	33	.317	.305
37	.363	.322	+	91	.323	.305	34	.317	.305
38	.363	.322	+	92	.323	.305	35	.317	.305
39	.363	.322	+	93	.323	.305	36	.317	.305
40	.363	.322	+	94	.323	.305	37	.317	.305
41	.363	.322	+	95	.323	.305	38	.317	.305
42	.363	.322	+	96	.323	.305	39	.317	.305
43	.363	.322	+	97	.323	.305	40	.317	.305
44	.363	.322	+	98	.323	.305	41	.317	.305
45	.363	.322	+	99	.323	.305	42	.317	.305
46	.363	.322	+	100	.323	.305	43	.317	.305
47	.363	.322	+	101	.323	.305	44	.317	.305
48	.363	.322	+	102	.323	.305	45	.317	.305
49	.363	.322	+	103	.323	.305	46	.317	.305
50	.363	.322	+	104	.323	.305	47	.317	.305
51	.363	.322	+	105	.323	.305	48	.317	.305
52	.363	.322	+	106	.323	.305	49	.317	.305
53	.363	.322	+	107	.323	.305	50	.317	.305
54	.363	.322	+	108	.323	.305	51	.317	.305
55	.363	.322	+	109	.323	.305	52	.317	.305
56	.363	.322	+	110	.323	.305	53	.317	.305
57	.363	.322	+	111	.323	.305	54	.317	.305
58	.363	.322	+	112	.323	.305	55	.317	.305
59	.363	.322	+	113	.323	.305	56	.317	.305
60	.363	.322	+	114	.323	.305	57	.317	.305
61	.363	.322	+	115	.323	.305	58	.317	.305
62	.363	.322	+	116	.323	.305	59	.317	.305
63	.363	.322	+	117	.323	.305	60	.317	.305
64	.363	.322	+	118	.323	.305	61	.317	.305
65	.363	.322	+	119	.323	.305	62	.317	.305
66	.363	.322	+	120	.323	.305	63	.317	.305
67	.363	.322	+	121	.323	.305	64	.317	.305
68	.363	.322	+	122	.323	.305	65	.317	.305
69	.363	.322	+	123	.323	.305	66	.317	.305
70	.363	.322	+	124	.323	.305	67	.317	.305
71	.363	.322	+	125	.323	.305	68	.317	.305
72	.363	.322	+	126	.323	.305	69	.317	.305
73	.363	.322	+	127	.323	.305	70	.317	.305
74	.363	.322	+	128	.323	.305	71	.317	.305
75	.363	.322	+	129	.323	.305	72	.317	.305
76	.363	.322	+	130	.323	.305	73	.317	.305
77	.363	.322	+	131	.323	.305	74	.317	.305
78	.363	.322	+	132	.323	.305	75	.317	.305
79	.363	.322	+	133	.323	.305	76	.317	.305
80	.363	.322	+	134	.323	.305	77	.317	.305
81	.363	.322	+	135	.323	.305	78	.317	.305
82	.363	.322	+	136	.323	.305	79	.317	.305
83	.363	.322	+	137	.323	.305	80	.317	.305
84	.363	.322	+	138	.323	.305	81	.317	.305
85	.363	.322	+	139	.323	.305	82	.317	.305
86	.363	.322	+	140	.323	.305	83	.317	.305
87	.363	.322	+	141	.323	.305	84	.317	.305
88	.363	.322	+	142	.323	.305	85	.317	.305
89	.363	.322	+	143	.323	.305	86	.317	.305
90	.363	.322	+	144	.323	.305	87	.317	.305
91	.363	.322	+	145	.323	.305	88	.317	.305
92	.363	.322	+	146	.323	.305	89	.317	.305
93	.363	.322	+	147	.323	.305	90	.317	.305
94	.363	.322	+	148	.323	.305	91	.317	.305
95	.363	.322	+	149	.323	.305	92	.317	.305
96	.363	.322	+	150	.323	.305	93	.317	.305
97	.363	.322	+	151	.323	.305	94	.317	.305
98	.363	.322	+	152	.323	.305	95	.317	.305
99	.363	.322	+	153	.323	.305	96	.317	.305
100	.363	.322	+	154	.323	.305	97	.317	.305
101	.363	.322	+	155	.323	.305	98	.317	.305
102	.363	.322	+	156	.323	.305	99	.317	.305
103	.363	.322	+	157	.323	.305	100	.317	.305
104	.363	.322	+	158	.323	.305	101	.317	.305
105	.363	.322	+	159	.323	.305	102	.317	.305
106	.363	.322	+	160	.323	.305	103	.317	.305
107	.363	.322	+	161	.323	.305	104	.317	.305
108	.363	.322	+	162	.323	.305	105	.317	.305
109	.363	.322	+	163	.323	.305	106	.317	.305
110	.363	.322	+	164	.323	.305	107	.317	.305
111	.363	.322	+	165	.323	.305	108	.317	.305
112	.363	.322	+	166	.323	.305	109	.317	.305
113	.363	.322	+	167	.323	.305	110	.317	.305
114	.363	.322	+	168	.323	.305	111	.317	.305
115	.363	.322	+	169	.323	.305	112	.317	.305
116	.363	.322	+	170	.323	.305	113	.317	.305
117	.363	.322	+	171	.323	.305	114	.317	.305
118	.363	.322	+	172	.323	.305	115	.317	.305
119	.363	.322	+	173	.323	.305	116	.317	.305
120	.363	.322	+	174	.323	.305	117	.317	.305
121	.363	.322	+	175	.323	.305	118	.317	.305
122	.363	.322	+	176	.323	.305	119	.317	.305
123	.363	.322	+	177	.323	.305	120	.317	.305
124	.363	.322	+	178	.323	.305	121	.317	.305
125	.363	.322	+	179	.323	.305	122	.317	.305
126	.363	.322	+	180	.323	.305	123	.317	.305
127	.363	.322	+	181	.323	.305	124	.317	.305
128	.363	.322	+	182	.323	.305	125	.317	.305
129	.363	.322	+	183	.323	.305	126	.317	.305
130	.363	.322	+	184	.323	.305	127	.317	.305
131	.363	.322	+	185	.3				

***** FICHER AD166 NO(IT)= 1
 26/ 3/95 15H45 AS07 M=.3 I=0 R 3-6 ADAPTE 3D AD166
 DE AD9118 1'ITE.

MACH DE REFERENCE= .3039 UINF= 231.109 M/S
 TIV=298.3 K PIV= 1649 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE A907	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.306	.303	PRISES DOUBLES			HUB. AMONT		33	.306	1	.758
2	.307	.311						34	.305	2	.786
3	.305	.307	59	.305	.305	1	.799	35	.305	3	.862
4	.300	.304	60	.306	.305	2	.798	36	.304	4	.973
5	.799	.305	61	.303	.301	3	.798	37	.303	5	.953
6	.304	.303				4	.300	38	.303	6	.892
7	.305	.306	PRISES LAT. GAUCHES			5	.798	39	.303	7	.849
8	.306	.303				6	.798	40	.305	8	.307
9	.306	.306	62	.302	.304	7	.797	41	.303	9	.425
10	.307	.300	63	.797	.303	8	.795	42	.307	10	1.375
11	.302	.301	64	.305	.306	9	.798	43	.303	11	1.301
12	.796	.300	65	.303	.300	10	.799	44	.302	12	1.097
13	.798	.300	66	.304	.798	11	.300	45	.301	13	1.030
14	.798	.303	67	.313	.303	HUB. AVAL		HUB. DROIT		14	1.015
15	.799	.304	68	.312	.303	1	.307	1	.304	15	1.001
16	.799	.301	69	.314	.307	2	.306	2	.304	16	1.006
17	.301	.302	70	.316	.306	3	.305	3	.304	17	1.003
18	.305	.302	71	.306	.797	4	.306	4	.304	18	.997
19	.304	.300	72	.303	.307	5	.305	5	.304	19	1.003
20	.304	.301	73	.306	.310	6	.305	6	.304	20	.998
21	.303	.301	PRISES LAT. DROITES			7	.305	7	.304	21	.991
22	.305	.799				8	.306	8	.304	22	.971
23	.307	.798	74	.303	.309	9	.306	9	.304	23	.948
24	.308	.799	75	.305	.306	10	.303	10	.304	24	.751
25	.308	.302	76	.304	.301	11	.304	11	.304	25	.777
26	.309	.300	77	.798	.799	12	.304	12	.304	26	.857
27	.315	.799	78	.797	.798	HUB. GAUCHE				27	.957
28	.317	.304	79	.302	.796	13	.304	13	.304	28	.959
29	.323	.305	80	.319	.798	14	.304	14	.304	29	.309
30	.319	.304	81	.313	.799	15	.314	15	.304	30	.373
31	.326	.301	82	.311	.300	16	.313	16	.304	31	.373
32	.321	.306	83	.311	.300	17	.312	17	.304	32	.416
33	.325	.307	84	.322	.301	18	.303	18	.304	33	1.403
34	.320	.303	85	.304	.305	19	.304	19	.304	34	1.336
35	.323	.304	86	.306	.308	20	.304	20	.304	35	1.373
36	.321	.305	87	.332	.303	21	.303	21	.304	36	1.356
37	.323	.303	88	.329	.307	22	.312	22	.304	37	1.343
38	.321	.305	89	.327	.304	23	.316	23	.304	38	1.326
39	.325	.305	90	.328	.303	24	.318	24	.304	39	1.000
40	.320	.305	91	.319	.305	25	.315	25	.304	40	.991
41	.319	.305	92	.311	.304	26	.312	26	.304	41	.302
42	.320	.305	93	.309	.797	27	.311	27	.304	42	.958
43	.317	.305	94	.301	.300	28	.311	28	.304	43	.956
44	.311	.304	95	.308	.305	29	.310	29	.304	44	.924
45	.311	.301	96	.304	.796	30	.304	30	.304	45	.904
46	.307	.301				31	.303	31	.304	46	.892
47	.309	.797				32	.303	32	.304	47	.925
48	.307	.799				33	.304	33	.304	48	.347
49	.308	.302				34	.304	34	.304	49	.370
50	.306	.305				35	.304	35	.304	50	.313
51	.308	.307				36	.305	36	.304		
52	.307	.302	PRISES COL			37	.307	37	.304		
53	.307	.303				38	.305	38	.304		
54	.308	.304	.343	1.210		39	.311	39	.304		
55	.310	.301	.355	1.123		40	.313	40	.304		
56	.308	.798	.336	.394		41	.315	41	.303		
57	.308	.798	.381	.319		42	.320	42	.303		
58	.304	.798	1.141	.780		43	.322	43	.303		
						44	.317	44	.303		
						45	.319	45	.304		
						46	.307				
						47	.307				

***** FICHER AD167 NO<IT>= 1
 26/ 3/85 16H15 AS07 M.=5 I=2(1.5+ROT.30) R 3-6 NON ADAPTE AD167
 DE AD45 1/ITE. PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .5991 UINF= 231.108 M/S
 TIV=398.7 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE		MACH PAROIS LAT. DROIT		MACH PAROIS LAT. GAUCHE		MACH PAROIS LAT. HUB.		MACH PAROIS LAT. HUB. DROIT		MACH PAROIS LAT. HUB. GAUCHE	
I	HAUT	BAS	I	HAUT	BAS	HUB.	AMONT	I	MACH	I	MACH
1	.597	.593						33	.595		.597
2	.595	.596						34	.594		.595
3	.593	.597						35	.593		.594
4	.599	.599		59	.599		1	.599	.593		.599
5	.597	.591		50	.590		2	.599	.593		.597
6	.593	.592		51	.593		3	.599	.592		.593
7	.598	.599		50	.590		4	.599	.592		.594
8	.599	.598		52	.599		5	.599	.591		.594
9	.599	.597		53	.599		6	.599	.591		.594
10	.598	.598		54	.594		7	.599	.592		.594
11	.598	.598		55	.596		8	.599	.591		.594
12	.596	.598		55	.596		9	.599	.591		.594
13	.598	.597		56	.594		10	.598	.590		.594
14	.598	.597		57	.599		11	.599	.599		.599
15	.599	.599		58	.599						
16	.599	.599		59	.599						
17	.599	.599		60	.599						
18	.595	.599		70	.599						
19	.595	.599		71	.599						
20	.595	.599		72	.594						
21	.595	.599		73	.599						
22	.597	.599									
23	.595	.599									
24	.595	.597									
25	.595	.595									
26	.595	.595									
27	.595	.595									
28	.595	.597									
29	.595	.597									
30	.595	.597									
31	.595	.597									
32	.595	.597									
33	.595	.597									
34	.595	.597									
35	.595	.597									
36	.595	.597									
37	.595	.597									
38	.595	.597									
39	.595	.597									
40	.595	.597									
41	.595	.597									
42	.595	.597									
43	.595	.597									
44	.595	.597									
45	.595	.597									
46	.595	.597									
47	.595	.597									
48	.595	.597									
49	.595	.597									
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51	.595	.597									
52	.595	.597									
53	.595	.597									
54	.595	.597									
55	.595	.597									
56	.595	.597									
57	.595	.597									
58	.595	.597									
59	.595	.597									
60	.595	.597									

PRISES COL
 .699 1.069
 .699 .892
 .699 .791
 .699 .699
 .699 .599
 .699 .499
 .699 .399
 .699 .299
 .699 .199
 .699 .099
 .699 .099

***** FICHER AD168 NO(IT)= 1
 26/ 8/85 16H25 AS07 M=6 I=+2(1.5+ROT.30') R 3-6 ADAPTE 3D AD168
 DE AD9122 1'ITE.

MACH DE REFERENCE= .5994 UINF= 231.109 M/S
 TIV=298.4 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
			PRISES DOUBLES			HUB.	AMONT	33	.602	1	.563
1	.607	.592						34	.601	2	.573
2	.606	.595						35	.600	3	.577
3	.603	.597	59	.598	.599	1	.599	36	.602	4	.583
4	.599	.598	60	.600	.600	2	.598	37	.601	5	.584
5	.597	.599	61	.604	.599	3	.598	38	.600	6	.585
6	.599	.601				4	.599	39	.600	7	.584
7	.598	.600	PRISES LAT. GAUCHES			5	.599	40	.600	8	.583
8	.599	.599	62	.600	.597	6	.598	41	.601	9	.583
9	.600	.601	63	.602	.603	7	.598	42	.601	10	1.004
10	.601	.597	64	.603	.604	8	.598	43	.599	11	.583
11	.599	.598	65	.601	.600	9	.598	44	.599	12	.587
12	.597	.598	66	.599	.601	10	.598	45	.598	13	.584
13	.598	.597	67	.607	.600	11	.599			14	.579
14	.598	.599	68	.606	.600	HUB. AVANT		HUB. DROIT		15	.761
15	.599	.600	69	.606	.601					16	.755
16	.599	.599	70	.611	.600	1	.603	1	.599	17	.747
17	.601	.600	71	.604	.599	2	.604	2	.599	18	.738
18	.603	.601	72	.605	.602	3	.604	3	.599	19	.733
19	.602	.600	73	.605	.605	4	.604	4	.600	20	.726
20	.602	.600				5	.604	5	.600	21	.716
21	.602	.599	PRISES LAT. DROITES			6	.604	6	.600	22	.714
22	.605	.599	74	.601	.599	7	.604	7	.600	23	.694
23	.605	.597	75	.600	.599	8	.605	8	.599	24	.693
24	.603	.600	76	.600	.599	9	.605	9	.599	25	.693
25	.604	.600	77	.600	.597	10	.603	10	.599	26	.693
26	.604	.600	78	.599	.598	11	.602	11	.599	27	.693
27	.608	.598	79	.602	.596	HUB. GAUCHE		12	.600	28	.693
28	.610	.599	80	.607	.597	13	.600	13	.600	29	.693
29	.614	.598	81	.611	.607	14	.600	14	.600	30	.693
30	.612	.598	82	.608	.598	15	.607	15	.600	31	.693
31	.615	.594	83	.613	.597	16	.607	16	.600	32	1.000
32	.612	.598	84	.620	.596	17	.607	17	.600	33	.693
33	.613	.597	85	.620	.597	18	.603	18	.599	34	.693
34	.609	.597	86	.617	.598	19	.603	19	.599	35	.693
35	.611	.597	87	.615	.599	20	.603	20	.599	36	.693
36	.609	.598	88	.614	.597	21	.603	21	.599	37	.693
37	.613	.597	89	.620	.597	22	.609	22	.599	38	.693
38	.613	.598	90	.618	.598	23	.610	23	.599	39	.693
39	.616	.598	91	.607	.598	24	.608	24	.599	40	.693
40	.614	.597	92	.606	.599	25	.607	25	.599	41	.693
41	.613	.597	93	.602	.600	26	.607	26	.599	42	.693
42	.613	.598	94	.606	.601	27	.606	27	.599	43	.693
43	.609	.597	95	.604	.599	28	.603	28	.599	44	.693
44	.606	.598	96	.594	.597	29	.602	29	.599	45	.693
45	.604	.598				30	.602	30	.599		
46	.606	.598				31	.602	31	.599		
47	.606	.601				32	.602	32	.599		
48	.606	.601									
49	.606	.601									
50	.604	.601									
51	.605	.601									
52	.605	.599	PRISES COL			33	.602	33	.600		
53	.606	.601				34	.602	34	.600		
54	.605	.602	371	1.072		35	.602	35	.600		
55	.604	.601	371	.901		36	.602	36	.600		
56	.601	.600	371	.793		37	.602	37	.600		
57	.598	.599	371	.691		38	.602	38	.600		
58	.591	.596	1.002	.633		39	.602	39	.600		
						40	.602	40	.600		
						41	.602	41	.600		
						42	.602	42	.600		
						43	.602	43	.600		
						44	.602	44	.600		
						45	.602	45	.600		

***** FICHER AD159 N00IT= 4
 25/ 8/85 16H50 AS07 M=6 I=+2 R 3-5 ADAPTE 2D AD159
 DE AD145 4'ITE.

MACH DE REFERENCE= .5991 UINF= 231.108 M/S
 TIV=294.2 K PIV= 1391 MB

MACH PAROIS-HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.601	.596	PRISES DOUBLES			HUB. AMONT	33	.599		1	.596
2	.601	.600					34	.598		2	.596
3	.600	.599	59	.600	.598	1	.600	35	.597	3	.596
4	.597	.599	60	.602	.599	2	.599	36	.598	4	.594
5	.597	.600	61	.600	.597	3	.599	37	.597	5	.596
6	.600	.601				4	.599	38	.597	6	.594
7	.600	.598	PRISES LAT. GAUCHES			5	.598	39	.596	7	.592
8	.601	.597				6	.598	40	.595	8	.592
9	.602	.599	62	.598	.599	7	.598	41	.597	9	.592
10	.602	.596	63	.602	.601	8	.597	42	.597	10	.594
11	.599	.598	64	.603	.599	9	.598	43	.596	11	.594
12	.596	.598	65	.602	.596	10	.597	44	.595	12	.594
13	.598	.597	66	.602	.595	11	.597	45	.595	13	.593
14	.599	.597	67	.606	.597					14	.593
15	.600	.597	68	.607	.596	HUB. AVAL		HUB. DROIT		15	.593
16	.600	.596	69	.607	.597	1	.601	1	.600	16	.593
17	.601	.596	70	.609	.595	2	.602	2	.600	17	.593
18	.603	.603	71	.604	.595	3	.601	3	.600	18	.594
19	.603	.597	72	.602	.596	4	.602	4	.600	19	.597
20	.604	.596	73	.592	.600	5	.601	5	.600	20	.597
21	.604	.595				6	.601	6	.600	21	.596
22	.606	.596	PRISES LAT. DROITES			7	.601	7	.600	22	.596
23	.608	.595				8	.601	8	.600	23	.599
24	.606	.595	74	.599	.601	9	.602	9	.600	24	.599
25	.608	.594	75	.600	.598	10	.599	10	.600	25	.599
26	.607	.594	76	.601	.597	11	.599	11	.600	26	.599
27	.611	.593	77	.598	.596					27	.599
28	.611	.595	78	.599	.594	HUB. GAUCHE				28	.599
29	.615	.595	79	.602	.593	12	.600	12	.600	29	.599
30	.613	.596	80	.609	.592	13	.600	13	.600	30	.599
31	.616	.593	81	.613	.594	14	.600	14	.600	31	.599
32	.613	.596	82	.611	.591	15	.597	15	.600	32	.599
33	.615	.595	83	.615	.591	16	.597	16	.600	33	.599
34	.612	.594	84	.621	.593	17	.597	17	.600	34	.599
35	.613	.594	85	.621	.593	18	.602	18	.600	35	.599
36	.613	.594	86	.619	.593	19	.603	19	.600	36	.599
37	.615	.593	87	.617	.593	20	.605	20	.600	37	.599
38	.615	.593	88	.615	.592	21	.609	21	.600	38	.599
39	.616	.593	89	.619	.592	22	.619	22	.600	39	.599
40	.614	.594	90	.614	.594	23	.619	23	.600	40	.599
41	.613	.594	91	.607	.593	24	.608	24	.600	41	.599
42	.613	.595	92	.605	.595	25	.608	25	.600	42	.599
43	.611	.595	93	.600	.596	26	.606	26	.600	43	.599
44	.603	.595	94	.602	.596	27	.604	27	.600	44	.599
45	.607	.595	95	.609	.596	28	.601	28	.600	45	.599
46	.604	.596	96	.601	.599	29	.600	29	.600	46	.599
47	.606	.596				30	.600	30	.600	47	.599
48	.605	.596				31	.600	31	.600	48	.599
49	.605	.597				32	.600	32	.600	49	.599
50	.602	.597				33	.600	33	.600	50	.599
51	.603	.598				34	.601	34	.600		
52	.601	.598	PRISES COL			35	.601	35	.600		
53	.601	.598				36	.601	36	.600		
54	.600	.597	1.061	1.057		37	.600	37	.600		
55	.600	.595	.794	.795		38	.603	38	.600		
56	.597	.593	.799	.794		39	.604	39	.600		
57	.594	.591	.865	.831		40	.606	40	.600		
58	.589	.600	1.023	.822		41	.607	41	.600		
						42	.608	42	.600		
						43	.607	43	.600		
						44	.605	44	.600		
						45	.603	45	.600		

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ADAPTATIONS
TESTS WITH THREE-DIMENSIONAL ADJUSTMENTS IN THE RECTANGULAR
WORKING SECTION OF THE FRENCH T2 WIND TUNNEL, WITH AN
TYPE AS 07-TYPE SWEPT-~~BACK~~ WING^{HALL} MODEL INSTALLED

A. Blanchard, M. J. Payry, J. F. Breil

Translation of "Essais 'd'adaptation tridimensionnelle' de la
veine rectangulaire de la soufflerie T2, en presence d'une
maquette d'aile en fleche du type AS 07," Rapport Technique OA
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TESTS WITH THREE-DIMENSIONAL ADJUSTMENTS IN THE
RECTANGULAR WORKING SECTION OF THE FRENCH T2
WIND TUNNEL WITH AN AS 07-TYPE SWEPT-BACK WING
MODEL

A. Blanchard, M. J. Payry, and J. F. Breil Jul. 1986 161 p
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The results obtained on the AS 07 wing and the working
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tions which tend to minimize interference at the level of the
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case was tested to determine the influence of wall shape and
error magnitude. These results are not sufficient to validate the
three-dimensional adaptation; they must be coordinated with
calculations or with unlimited atmosphere tests.

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NASA TM-88442

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ADAPTATIONS
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Adaptation

NOTATION

$\left. \begin{array}{l} X_p \\ Y_p \\ Z_p \end{array} \right\}$ Cartesian coordinates in the reference working section
 (porthole axis)

$\left. \begin{array}{l} X \\ Y \\ Z \end{array} \right\}$ Cartesian coordinates in the wing reference (leading
 edge to socket)

C Profile chord of the wing section considered

α Angle of the model (fuselage axis)

M_o ~~Infinite Mach~~ ^{Test} ~~upstream of the flow~~ ^{number} ~~number~~

M Local Mach (wing or wall)

$$K_p = \frac{p - p_o}{\frac{1}{2} \rho V_o^2} \quad \text{Pressure coefficient}$$

C_z Local or complete-wing lift coefficient

$$\left\{ \begin{array}{l} C_z \text{ local} = \int_{\text{profil}} K_p \cdot d\left(\frac{x}{C_{\text{local}}}\right) \\ C_z = \frac{F_z}{\frac{1}{2} \rho V_o^2 \cdot S_{\text{aile}}} \end{array} \right.$$

ADAPTATIONS
TESTS WITH THREE-DIMENSIONAL ADJUSTMENTS IN THE RECTANGULAR
WORKING SECTION OF THE FRENCH T2 WIND TUNNEL, WITH AN
TYPE AS 07 ~~TYPE~~ SWEEPED-BACK WING MODEL INSTALLED.

A. Blanchard, M. J. Payry, J. F. Breil

1 - INTRODUCTION

/7*

This test series follows a study done in the T2 wind tunnel with the goal of defining a shape for the adaptable walls which would minimize their influence on three-dimensional ~~objects~~ ^{models} placed in the center of the ^{test} section or fastened on the sidewall.

flow flow The present configuration of the working section does not allow obtaining a shape ^{to be set which are} identical to that of the ^{streamlines} ~~layer of the streamlines~~ ^{which} ~~current~~ existing around a three-dimensional model in unlimited ^{fixed} ~~atmosphere~~ ^{unconfined} atmosphere (two completely ~~rectilinear~~ and parallel lateral walls, two flexible and bendable upper and lower walls). The planned solution thus consists of using the two bendable walls to minimize the influence of the walls on the model.

The method implemented uses solutions developed by "E. Wedemeyer and L. Lamarche" [5]. A first series of tests was done in cooperation with the ^{technical} University of Berlin on various existing models [6]:

- a C5 revolving body 166 mm long, 0.3% blockage;
- a civil F4 airplane model with 120-mm wingspan and three-component balance;
- a duck-type military airplane model with the same balance.

Another series of tests was then done on a bigger model [7]:

- a C5 body 400 mm long, 1.8% blockage.

*Numbers in the margin indicate pagination in the foreign text.

The results and calculations were compared.

The calculation method was optimized for revolving bodies of revolution placed in the center of the ^{test} section; an extrapolation was tried which placed a half-wing at the wall. In this case, calculations are done as if the section were twice its actual width, using the Mach distribution at the wall measured near the plane of symmetry.

The results obtained on the "16/1000-scale" AS 07 are discussed in this report. They can be divided into two groups: control tests and systematic tests.

Included in the first group is control of wing angling by rotating the walls. The ^{power} path of the jacks would not permit the displacements ~~required by calculation~~ for ~~angling the model to~~ ^{flow angle} ^{low angle} ^{angle of attack of} $+2^\circ$; we thus used this "artificial" method after having ~~verified~~ ^{ed} its validity.

The three-dimensional adaptation method supplies the ^{own} optimal shape of the walls from the first calculation, whatever the initial position of the walls; this was verified in 18 several test configurations. Finally, an adaptation called ^{2D} "two-dimensional" was tested; it uses the normal method for ~~T2 2D~~ ^{model} profile tests. This case, without theoretical justification, was tried to see the influence of the ~~shape of the walls~~ ^{shapes} and the ~~size of errors which can be made.~~ ^{magnitude of the corresponding interferences}

The second part of this study corresponds to systematic tests: four configurations were chosen which gave different lift coefficients, without making highly supersonic zones appear on the profiles. For each configuration, three wall positions were tested:

- The first, called "unadapted," corresponds to the upper and lower divergent ~~rectilinear~~ walls compensating for

boundary
boundary

thickening of the limit layers; it served as our basis for beginning three-dimensional adaptation calculations. These particularly simple limit conditions can also be used for complete calculation of the flow in the working section.

- The second wall shape comes from the three-dimensional adaptation calculation; the flexible ^{walls} sheets are positioned before the ~~gust~~ tunnel is run.
- Finally, the last case corresponds to "two-dimensional adaptation"; the iterative process converges ⁱⁿ on a single gust. tunnel run.

For each type of test, three ^{tunnel runs} gusts are necessary to obtain readings from the six rows of pressure recorders spread along the AS 07 wing.

The experimental results gathered during this series are not sufficient to validate the three-dimensional adaptation method used. Additional calculations must be made to estimate residual corrections. In these tests, ^{the small} a negligible influence of the walls is observed for low lift values or low Mach numbers; inversely, for 2 degrees of incidence or for Mach 0.8, the ~~influence~~ become significant and can in part be interpreted as variations in aerodynamic incidence.

2 - ADAPTATION PRINCIPLE

^{unconfined} The purpose of the adaptable walls is to create an unlimited flow around a model, in a working section with finite dimensions; this can be done by controlling the wall conditions, either by their shape in the case of solid walls or by flows of mass through porous walls. The first solution has been chosen at T2, where flexible sheets moved by jacks form the upper and lower ^{walls} plates of the working section [3].

meaningful flow

In the case of a three-dimensional body, it is necessary to bend the walls located around the model to arrive at a shape *corresponding* near ~~the layer of current~~ ^{to a streamtube} existing around the model in ~~unlimited~~ ⁱⁿ atmosphere. This solution is not at present possible ~~at~~ ⁱⁿ T2, but on the other hand it is possible to use the two flexible 19 walls to minimize residual corrections due to the influence of the walls on the ~~object~~ ^{model}.

2.1 Two-dimensional adaptation

The details of the process will be found in [2] and [4]; it uses a coupling between the real flow in the working section (internal field) and a calculated ^{imaginary} virtual flow outside the wind tunnel (external field). Coupling occurs on a control surface near the walls through speed vector components. Adaptation is achieved by an iterative process acting on the shape of the walls: the components of ^{velocity at} the ~~speed~~ on the control surface ~~becomes~~ available at each iteration; they are extrapolated from the pressure measurements at the wall. The velocities needed on the control surface to achieve an unlimited external flow are calculated by the Green function following an inverse method. A method of optimized relaxation between the internal and external flows for the vertical velocity component, followed by an integration along each flexible wall, supplies the new shape of the wall. The real shape needed is obtained by adding the thickness displacement of the four wall limit layers.

2.2 Three-dimensional adaptation

For three-dimensional adaptation, the process is different [5]: it uses ^{a representation} ~~schematization~~ of the model through ^{by} a distribution of sources and vortices in a narrow horseshoe, placed on the ^{test} section axis. This ^{centerline} ~~schematization~~ ^{representation} ~~gives~~ ^{is} a good ^{approximation} ~~representation~~ of axisymmetrical bodies mounted in the middle of the working section.
centerline

The originality of the method lies in then doing a linear transformation, which permits passing directly from distribution of velocities at the walls to the adapted form without needing to determine the intensity of singularities. The optimized shape of the walls is thus theoretically obtained from the first calculation; this shape, which is not exactly "adapted," minimizes residual corrections on the model caused by the influence of the walls.

Using this method for a half-wing at the wall is ^{not quite} ~~correct~~ ^{abusive}, because the ~~base schematization~~ ^{basic representation} does not ~~represent~~ ^{rearrange} a wingspan; it has nonetheless been tried here by replacing the ~~one~~ ^{sidewall} lateral ~~door~~ by a plane of symmetry leading to a ~~fictional~~ ^{fictional} double section width, and taking the Mach distribution of the flexible walls near the plane of symmetry as reference. ^{fictional}

3 - EXPERIMENTAL EQUIPMENT

The T2 transonic wind tunnel ^{can be} ~~is~~ ^{ed} pressurizable and can function at low temperatures; only minimum-pressure and ambient-temperature tests were ~~done~~ ^{used} during this series.

3.1 Working section equipment

/10

The working section has an almost square section of $0.39 \times 0.37 \text{ mm}^2$ at the entrance. Flexible sheets of Invar make up the upper and lower walls, equipped with three rows of pressure recorders whose coordinates are given in figures 7 and 8. The ~~sheet~~ ^{wall}-positioning mechanism is described in [2], [3], and [4].

The left lateral ~~door~~ ^{sidewall} ~~sidewall~~ has three portholes with pressure recorders placed along horizontal and vertical lines whose coordinates are shown in Figures 7 and 9.

The pressure recorders are linked to ~~the~~ Scanivalves, each of ~~whose head~~ ^{which} can observe 48 positions in 5 seconds.

The position of the wing in the working section is given in figure 6.

The Mach number of the flow is set by a ~~second neck~~ ^{secondary throat} ~~throat~~ ^{secondary throat} controlled by the computer which controls the ~~gust~~ ^{gust} tunnel run.

No other equipment or wind tunnel measurement method ~~were~~ was used.

3.2 Mounting the wing

The AS 07 ^{half-} wing model with a scale of "16/1000" is shown by the photographs in figure 5. The method of mounting the wing on the wall is shown (figure 6), the plane of the wing and its specifications are given (figures 10 and 11), and the shape of the profiles ^{at different spanwise locations are shown} ~~which compose it~~, and the positions of the pressure recorders are indicated (figures 12 and 13).

^{at different spanwise locations are shown}

There are six rows, each with 16 recorders on the inner and outer sections and one on the leading edge; they are placed across the wingspan so as to form lines with constant chord percentages. These recorders communicate with tubes placed in grooves along the wingspan; each tube communicates with three recorders (either on the external wing or on the internal wing). When one of the three rows of recorders is used to measure pressure, the other two are covered with thin (0.05-mm) adhesive strips. It is thus possible to simultaneously measure pressure on two sections of the wing (one internal and one external); measurement of velocities over the entire wing thus requires three different ~~gusts~~ ^{runs} tunnel runs.

The wing is mounted on a half-fuselage linked to a porthole, whose rotation ~~ensures the angling of the wing-~~

^{which rotates} ~~ensures the angling of the wing-~~ ^{so to change the angle of attack of}

fuselage assembly; the angular reference is the ^{straight} ~~rectilinear~~ part on the back of the fuselage [1].

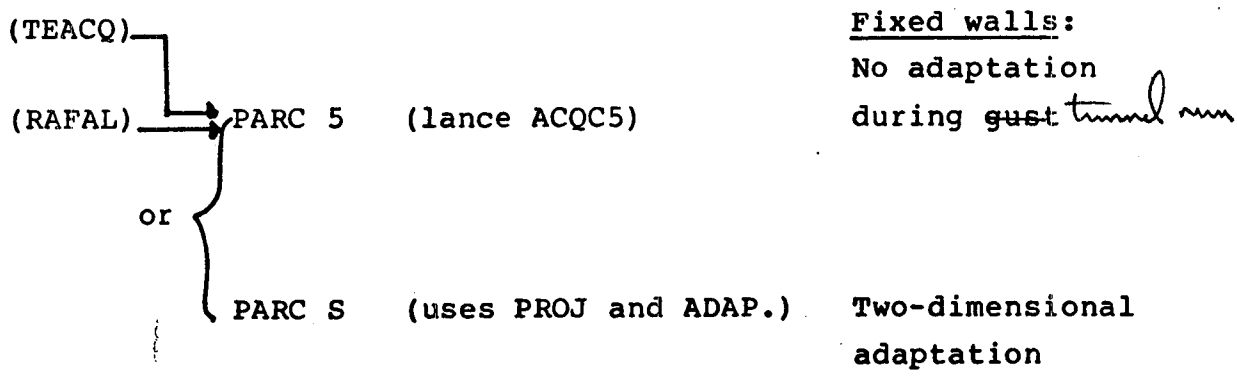
3.3 Acquisition and examination programs ^{graphics}

The T2 wind tunnel is linked to a team of two computers, one concerned with creating and ^{controlling} ~~regulating~~ the ^{tunnel run} ~~gust~~ and the other with obtaining data and storing measurements to disk at the end of ^{each} ~~the~~ ^{tunnel run} ~~gust~~.

These tests are ^{similar} ~~pursuant~~ to the series done on the /11 C5 body and use its principal elements.

Disk cartridge LU 26, Program
LU 34, Test files, calculation files

Acquisition program



Initialization of programs { with (TR,) RINC 5 (For PARC 5)
or (TR,) RINC S (For PARC S)

Test file

AD --- test number from AD 100 to AD 173

Wall positioning file

- any test file AD---
- or calculation file AD 9 ---
- or special file

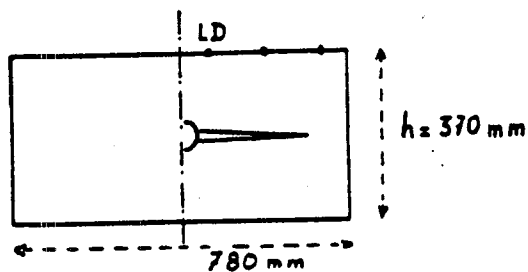
}	AD 4:	Divergent rectilinear walls of ^{with} int ^{boundary} layers ^{axis} symmetrical ^{limit} layers .
	AD 444:	AD 4 + 10' ^{axis} rotation upward
	AD 445:	AD 4 + 30' ^{axis} rotation upward

Three-dimensional adaptation calculation

Calculation from a test file AD ---

VKJ 43 Calculation of wall shapes without rotation

VKI M Calculation of wall shapes with rotation



- section length 780 mm
- ratio $c = h/b = 2.1081$
- reference recorders:
right lateral RL
- weighting coefficients
file VKJ - R (cartridge
LU 43)

→ Filing to disk

File for new calculated wall shapes

AD 9 --- beginning test number for the calculation

Programs for examination of AD--- files

LTCS:

- graphs local profile Mach numbers
- graphs K_p
- lists AD file
- calculates C_z

LTC 51:

- graphs wall Mach numbers
- graphs wall shapes
- starts LTC 52 (does an RP, LTC 52)

LTC VK:

- graphs only wall shapes calculated by VKI 43 or VKIM (from AD 9---).

4 - SUMMARY OF TESTS PERFORMED

A previous study was done on the AS 07 wing [1]. We verified in one case that the same results would occur, although the working section was modified when the T2 wind tunnel was *modified* adapted for cryogenics.

The first control tests were done by measuring rows 2 and 5 of pressure recorders for the Mach numbers and incidences indicated below:

α \ M_0	Mach number		
	0,6	0,7	0,8
+2°	X	X	X
0	X	X	X
-2°	X	X	

Four configurations were selected for systematic tests: /13

$\alpha \backslash M_0$	0,6	0,7	0,8
+2°	X		
0°	X		X
-2°	X		

They correspond to a sampling of lift coefficients and ~~to an~~ ^{numbers} infinite Mach effect ^{numbers} upstream, while limiting the supersonic zones which appear on the profiles.

Figure 1 shows the list of tests in chronological order, and figures 2, 3, and 4 classify them by configuration.

We first showed that rotation of the upper and lower walls was equivalent to ^{changing the angle of attack of} angling the model at the same ^{geometric} angle. This ^{technique} ~~artifice~~ was made necessary because the ^{power} path of the jacks did ^{power} not permit the displacements required by calculation of three-dimensional adaptation for a model incidence of +2°.

- Divergent rectilinear walls

α accid.			M_0	
	α Display	Wall Start	0,6	0,8
+2°	+2°	AD 4	AD 120	
	+1,5°	AD 445	AD 122	
0°	0°	AD 4	AD 107 - AD 109	AD 108 - AD 132
	-0,5°	AD 445	AD 137	AD 139

		M_0	
$\alpha_{aérod.} = 0^\circ$	α CALCUL	0,6	: 0,8
	0° VKI 43	117	: AD 119
	-0,5° VKI M	138	: AD 141

The three-dimensional adaptation method theoretically supplies the optimal ^{sum} shape of the walls from the first calculation, whatever the initial position of the flexible ^{walls} sheets. ^{Tests} Controls were done in this respect for the following configurations:

		M_0	
α <i>(display)</i>		0,7	: 0,8
+1,5°			: AD 127 (1) : AD 128 (2) : AD 129 (3)
0°	AD 115 (1) AD 116 (2)		: AD 118 (1) : AD 119 (2)
-0,5°			: AD 140 (1) : AD 141 (2)

The figure in parentheses after the file number indicates the order of the iteration; the wall-positioning file thus results from calculation of the preceding test. (Iteration (0) is the test done with ~~rectilinear~~ ^{straight} walls.)

We also verified that the tests called "two-dimensional ^{2D model} adaptation" converged rapidly, as is the case for the ~~profile~~ ^{2D Model} tests; it is sufficient ~~for that~~ to compare the wall positions of

the 3rd and 4th iterations, ^{performed} ~~done~~ during the same ~~gust~~; the two positions are always close. In general, the beginning shape chosen is near the adapted shape, but we have tested this convergence in the two particular cases when the beginning shape was far from the adapted shape. The beginning file chosen was AD 4: ~~rectilinear walls divergent from limit layers and symmetrical.~~ ^{straight} ~~symmetrical.~~ ^{performed} ~~symmetrically~~ ^{tunnel run} ~~tunnel run~~ ^{for boundary layers.} ~~for boundary layers.~~

/15

Configuration: $Mo = 0.7 \quad \alpha = +1.5^\circ$ File AD 130 (1)
Configuration: $Mo = 0.8 \quad \alpha = 0^\circ$ File AD 133 (1)
followed by File AD 134 (2)

Comparisons were made between the various wall positions; they are noted:

- "Non," for divergent ^{straight} rectilinear walls
- "2D," for two-dimensional adaptation done with the PARCS program
- "3d," for positioning of the walls in the shape calculated by the VKI 43 or VKI M program

It was decided to do systematic tests for the three cases of "adaptation," the non-adapted case serving as a basis for three-dimensional calculation (any wall shape will work); this case can also serve as a basis for complete flow calculations, because here the limit conditions are particularly simple. The two-dimensional adaptation, ^{beyond} ~~outside~~ the subject of the study, was systematically tested to use as a comparison with the assumed optimal ^{um} shape.

Finally, four configurations for three cases of adaptation, reproduced three times to have the velocity field on all of the wing, were tested; these 36 ^{tunnel runs.} gusts, make up the systematic tests listed in figure 26a.

5 - CONTROL TESTS

We will not present all the tests done, but only a selection of cases judged most interesting, since the goal of this series ^{was} ~~is~~ not to evaluate the AS 07 wing.

5.1 Angling by wall rotation *Change of flow angle* *change of flow angle*

Of the five configurations tested (^{section} paragraph 4), three are presented. The first corresponds to $Mo = 0.6$ and $\alpha = +2^\circ$ for ~~rectilinear~~ ^{straight} walls (figure 14); this is the configuration which obliged us to use this ^{technique} ~~artifice~~, as the three-dimensional case could not be tested.

Figure 15 shows the comparison of Mach numbers on the walls and on the wing, for an aerodynamic incidence equal to 0° and a Mach number equal to 0.8, in the case of ~~rectilinear~~ ^{straight} walls. Figure 16 presents the same configurations but for wall shapes coming respectively from ^{3D} ~~2D~~ calculations VKI 43 and VKI M.

The results of figures 14 and 15 show that the high Mach case is the most ^{interesting} ~~recordable~~, but the ^{quality} ~~correspondence~~ of the tests remains good. Figure 16 shows that the VKI M calculation makes perfect allowance for ^{axis} ~~total~~ rotation.

It is thus possible to ^{set} ~~display~~ a model incidence ^{/16} different from that desired and to compensate by rotating the walls.

5.2 Convergence of iterations *Adaptation*

5.2.1 Three-dimensional adaptation

Several calculations for optimization of wall shape were ^{made} ~~connected~~ for one configuration. The last test is always recalculated, leading to a wall shape which by definition

will not be used, but which will in fact constitute an additional iteration.

Of the four tested cases, two are presented in figures 17 and 18; the first ($M_o = 0.7$ and $\alpha = 0^\circ$) shows that the adapted shape is practically obtained from the first iteration; in the second case--much more difficult ($M_o = 0.8$ and $\alpha = +2^\circ$)--it is necessary to wait for the second calculation. This second case corresponds to a ~~freely~~ *influenced by the ?* supersonic regime of the wing which will not be studied systematically herein.

5.2.2 Two-dimensional adaptation

In all tests done, the 3rd iteration is always identical to the 4th and last iteration of the ~~test~~ *tunnel run*, even when the upper and lower walls have been prepositioned in a shape very different from the "adapted" shape. This is the case shown in figure 19 corresponding to $M_o = 0.8$ and $\alpha = 0^\circ$.

To confirm the validity of this statement, a second test was done, positioning the flexible ~~sheets on the~~ *walls* preceding shapes; the values obtained can thus be considered to correspond to the 4th, 5th, 6th, and 7th iterations of the test; they are all identical (figure 20), which confirms that the convergence was well obtained.

5.3 Non/2-D/3-D comparison

Two cases are presented here, one of which is not part of the systematic tests:

- $M_o = 0.7$ $\alpha = 0^\circ$
- $M_o = 0.8$ $\alpha = 0^\circ$

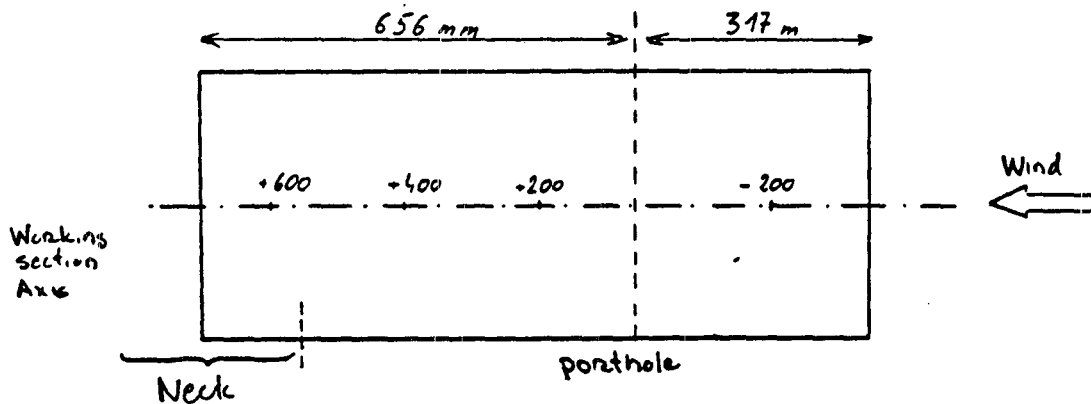
The ^{differences} gaps, observed following the ^{various} types of "adaptation" ~~will~~ become more significant as lift ^{and} Mach number ~~upstream~~ increase. The adaptation called "two-dimensional" gives results nearer to the non-adapted case; in fact, everything happens as if the aerodynamic incidence of the two-dimensional case were higher than that of the tests with a wall shape adapted in three dimensions. On the other hand, ^{straight} ~~rectilinear~~ walls lead to a higher effective Mach number upstream (blockage effect).

In the first case (figure 21), the ^{differences} gaps are moderate; they are more significant in the second case (figure 22). Observation of the ^{slope} ~~direction~~ of the walls leaving the ^{contraction} ~~convergent~~ (figure 21) shows that, effectively, the direction of the flow upstream is no longer horizontal in the "2-D" case, unlike the "3-D" case; the angular reference was given by the "non-adapted" case. The effect produced is ^{indisputable} ~~incontestable~~, because we /17 previously demonstrated that rotation of the walls ~~assembly~~ modified the aerodynamic incidence of the model; however, this is not sufficient to prove that the 2-D case is ^{in error} ~~erroneous~~, because the direction of the ^{stream} ~~current~~ lines in ~~unlimited~~ the ^{unconfined flow} ~~unconfined~~ atmosphere ^{are} ~~is~~ not known. We note also the very different shapes of the walls downstream; they go downward for the "3-D" cases, which is logical allowing for the chosen ^{schematization} ~~representation~~ (horseshoe vortex) and the calculation made (in the plane of symmetry). But once more, that does not prove that the shape obtained is optimum.

Finally, one can observe on the last figure (23) that the effect ^{at} ~~produced by~~ modifying the shape of the walls is not constant across the wingspan. This was predictable due to the working section geometry itself, allowing for twist of the wing and for three-dimensional effects.

5.4 Visualizations

For three configurations, oil visualizations were done on the left ^{sidewall} of the working section, giving the direction of the ^{flow} ~~current~~ ^{stream} lines 55.4 mm from the end of the wing. Reference marks were made, making it possible to locate the positions relative to the ^{stream} ~~current~~ lines and to measure their deviations.



The end of the wing is located between the abscissas 91.06 mm and 135.86 mm from the porthole (figure 6) and very near to the section axis (function of the incidence).

The maximum deviations noticed are located on the ^{test} section axis slightly behind the tip of the wing (figures 24, 25, and 26).

M_0	α	Walls	δ_{max}
0,6	+2°	"Non-adapted" AD 4	(5°.....6°)
0,6	+2°	'Adapted 2-D	(5°.....6°)
0,6	-2°	"Non-adapted" AD 4	~ 0,5°

Figure 24

Figure 25

Figure 26

The photos taken from behind clearly show the deviations of the ^{stream}current-lines.

/18

6 - SYSTEMATIC TESTS

For the 36 ^{tunnel runs} gusts that made up the systematic tests (paragraph 4 and figure 26a), the following information is given: wall shape (figures 27 and 28), Mach numbers of the three rows of recorders on the adaptable walls (figures 29, 30, 31, and 32), Mach numbers of the left lateral ^{side wall} door (figures 33, 34, 35, and 36) following the horizontal axis or the three verticals, and finally spread of Kp on the AS 07 wing (figures 37 to 44).

Numerical values for these curves are given in the attached test listings. File numbers corresponding in chronological order to the experiments were kept in the interests of clarity.

Here will be found a systematic comparison of the three cases of adaptation--"Non/2-D/3-D"--and their influence on the ^{velocity} ~~speed~~ distributions. ^{velocity} ~~speed~~ ^{whose} ~~whose~~ principal characteristics ^{of which} ~~of which~~ were seen in paragraph 5.3.

Finally, integration of Kp for each section supplies local lift coefficient Cz. The values are tabulated in figure 45; they were traced along the wingspan of the various configurations tested (figures 46 and 47). It is observed that the internal wing changes less rapidly than the external wing with incidence (figure 46) or ^{test} Mach number ^{upstream} (figure 47).

On the other hand, the ^{difference} ~~gap~~ between the "non-adapted" and adapted 3-D" cases increases with the lift.

Local C_z s were multiplied by the chord of the profile in the section considered; the product $C_z \cdot C$ represents local /19 contribution to wing lift. The values obtained were traced in this representation (figures 48 and 49); this weighting modifies the appearance of the curves ("elliptic" distribution plane), but the observed tendencies are the same.

Finally, integration of the curves in this last representation supplies the overall lift coefficient of the wing, which ^{is} was reported as a function of incidence (figure 50). We have also reported the lift measured during the preceding series [1], ^{performed} done between ^{straight} rectilinear walls for a Mach number upstream of 0.47. The effect of compressibility is felt more as supersonic zones develop on the wing.

- CONCLUSION

This series of tests on the AS 07 wing is ^{recorded} registered as a study on three-dimensional adaptation of the T2 wind tunnel. It uses the two flexible walls to minimize residual corrections in the presence of a three-dimensional model. It implements the "E. Wedemeyer and L. Lamarche" method where ^{the representation} ~~schematization~~ of the model by a distribution of singularities adequately represents an axisymmetrical body. Extrapolation of these methods in the case of a half-wing ^{model mounted on the sidewall} ~~at the wall~~ has no ultimate goal; it serves merely as a preliminary phase, to observe the influence of wall shape ^{on} in various sections of the wing, to study the convergence of the method, and to make adjustments ^{to} (rotation of walls, incidence, etc.).

On the other hand, these experiments can serve as a basis for calculating potential three-dimensional flow around the model. Then, a three-dimensional ^{test} ~~object~~ _{model} placed in the section

theoretically
theoretically represented
could be more elaborately ~~schematicized~~; it would lead to development, as for axisymmetrical bodies, of a method of adaptation minimizing the influence of the walls on the model.

At present, it is difficult to know if the shape called "adapted 3-D" is nearer to the values of ~~unlimited atmosphere~~ *unconfined flow* than the shape "adapted 2-D," but it is definitely not the optimum shape.

The tests will ~~next~~ *continue with* be completed by directional ~~limit~~ *boundary* layer ~~layer~~ *boundary* ~~readings~~ *measurements* on the lateral ~~wall~~ *side* at the level of ~~the end~~ *with* of the wing tip. The direction of the ~~current~~ *stream* lines in this area will be an important element in the reality-calculation comparisons

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PAPER 14

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- 2-D
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side

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