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AUXILIARY SUBPROGRAMS FOR CALCULATING THE NAVIGATIONAL  
PARAMETERS OF ARTIFICIAL EARTH SATELLITES. FORTRAN IV.

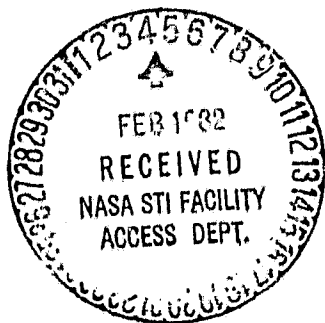
V. I. Prokhorenko

(NASA-TM-75684) AUXILIARY SUBPROGRAMS FOR  
CALCULATING THE NAVIGATIONAL PARAMETERS OF  
ARTIFICIAL EARTH SATELLITES. FORTRAN IV  
(National Aeronautics and Space  
Administration) 60 p HC A04/MF A01 CSCL 22B G3/15

N82-16140

Unclass  
07979

Translation of "Vspomogatel'nyye Podprogrammy dlya  
Rascheta Navigatsionnykh Parametrov Iskusst-  
vennykh Sputnikov Zemli. Fortran IV." Academy of Sciences  
USSR, Institute of Space Research, Moscow, Report PR-301,  
1976, pp 1-59



1. Report No. NASA TM-75684		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle AUXILIARY SUBPROGRAMS FOR CALCULATING THE NAVIGATIONAL PARAMETERS OF ARTIFICIAL EARTH SATELLITES. FORTRAN IV.				5. Report Date June 1981	
7. Author(s) V. I. Prokhorenko, Academy of Sciences USSR Institute of Space Research; Moscow				6. Performing Organization Code	
9. Performing Organization Name and Address Leo Kanner Associates, Redwood City, California 94063				8. Performing Organization Report No.	
				10. Work Unit No.	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration, Washington, DC 20546				11. Contract or Grant No. NASW-3199	
				13. Type of Report and Period Covered Translation	
15. Supplementary Notes Translation of "Vspomogatel'nyye podprogrammy dlya rascheta navigatsionnykh parametrov iskusstvennykh sputnikov zemli. Fortran IV." Academy of Sciences, USSR, Institute of Space Research, Moscow, Report PR-301, 1976, pp. 1-59				14. Sponsoring Agency Code	
16. Abstract The work contains a description of subprograms for trans- forming coordinates and time, for determining the position of the moon and sun, and for calculating the atmosphere and disturbances, which are specified by anomalies of the Earth's gravitational field. The subprograms are written in Fortran IV and form a major part of the package of applied programs for calculating the navigational parameters of artificial Earth satellites.					
17. Key Words (Selected by Author(s))			18. Distribution Statement Unclassified-Unlimited		
19. Security Classif. (of this report) Unclassified		20. Security Classif. (of this page) Unclassified		21. No. of Pages 54	22.

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FOREWORD

In the process of creating this packet of applied programs for calculating the navigational parameters of artificial Earth satellites (AES), the methods of use, whose possibilities and organization are described in Preprint [8], there arose a library of subprograms which have a sufficiently independent nature. The present work is devoted to a description of these subprograms. Because of the space limitation of a preprint, the description of the subprogram library has been divided into two parts. Included in the present preprint are the subprograms for transforming coordinates and time, for determining the position of the Moon and Sun, and for calculating atmospheric density on the basis of various models of the atmosphere and disturbances specified by anomalies of the Earth's gravitational field. In the library of subprograms of the packet mentioned above, these subprograms have indexes A-E.

The second part of the subprogram library (F-I) contains subprograms for the formation of the right parts of a system of differential equations for the motion of AES and for its integration by Adam's method, and subprograms for calculating the values of various functions from the parameters of the AES's motion.

The description of the master program and auxiliary subprograms, which guarantee the organization of information input, as well as the calculation and printing or recording on magnetic tape of an arbitrary set of navigational parameters (NP), makes up the content of an independent preprint.

There is a variant of the subprogram library for execution with binary precision of the calculations enumerated above.

When using the suggested library of subprograms or even one program of this library, one must keep in mind that all constants which are encountered in separate subprograms are located in a common region and values are assigned to them by a preliminary reference to the subprogram CONST(p. 2.1). Therefore, before turning to descriptions of actual subprograms, it is necessary to become familiar with points 1.2 and 2.1.

The systems of coordinates used and accepted when describing the subprogram library of designations are introduced in point 1.3.

The principle of the organization of the library of subprograms is described in p. I.1.

The remaining points contained in the description of actual subprograms can be used independently of one another.

The author of subprograms VKMA and DENS (DO2) is M.I. Vpyskovskiy, and of subprograms DEG2, DEG3, and DEG5 (EOI) it is Ye.Ye. Ryazanova.

The subprograms ADEN, AMBAR, GRAV, and TIOGAI are taken from [ 6 ] and are tested and modified for the Ye.Ye. Ryazanova's electronic computer (BESM-6). The remaining subprograms are those of the author of this work.

The author wishes to thank Ye.A. Chistyakova for help editing the tests of the programs for publication and I.V. Zaytseva and V.V. Smirnova for their help in preparing the manuscript.

# AUXILIARY SUBPROGRAMS FOR CALCULATING THE NAVIGATIONAL PARAMETERS OF ARTIFICIAL EARTH SATELLITES. FORTRAN IV.

V. I. Prokhorenko

## CHAPTER.I. THE ORGANIZATION OF THE SUBPROGRAM LIBRARY AND ITS FEATURES

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### 1.1 Organization of the Subprogram Library

At the base of the organizational procedure of the subprogram library are the principles of organizing a subprogram library which are accepted at this time, and which are used, for example in the joint Institute of Nuclear Research in Dubna.

To facilitate the review, the library is broken down into specific logical groups, each of which has its own index (A,B,C...). These indexes in a sense do not coincide with the indexes used in the joint Institute of Nuclear Research library but are used for the convenience of describing the library presented below.

The chapter names conform to the names of respective groups. Subprograms in each group are numbered (for example, AO1, AO2,...). Each individual subprogram is described in a separate point, and sometimes several subprograms which are linked to one another are described in one point. The names of points coincide with the names of subprograms. In such manner the indexing can be considered an inventory of subprograms which are grouped according to their meaning.

Besides this, in each section of the description of the subprogram library is a list of subprograms by their names in alphabetical order (together with indexes by which one can find a corresponding subprogram). In the last section is a full list of subprograms given by names.

When describing each individual subprogram the following format is used:

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1. Function
2. Structure  
Subprograms, subprogram-function, and the packet of subprograms

Identifier (identifiers) of the subprogram which is the input for the user.

Internal inputs (subprograms inaccessible to the user)  
Peripheral subprograms used (access to other subprograms of the library)

Peripheral devices (input and output devices)

Common units (COMMON)

---

\*Numbers in the margin indicate pagination in the foreign text.



3. Access
4. Input data
5. Results
6. Usage of the region COMMON
7. Limitations
8. Emergency outputs
9. Method or algorithm
10. References
11. Text

Information on all of the above points is not contained in each description, and numeration according to these points is not strictly adhered to.

In order to save space in the description of structure (p.2) replies of the type "Peripheral devices not in use" or "Access to internal subprograms unavailable" are omitted.

### 1.2 Constants, dimensional variables

The proposed subprogram library is a complex of subprograms which have been developed on the basis of several general principles.

All constants, dimensional and non-dimensional, which are used in various subprograms, are taken out of the common region (COMMON), and values are assigned to these constants by accessing the subprogram CONST (for the majority of constants, see Tables 2.1-2.4) and the subprogram CONGR (for coefficients of anomalies of the Earth's gravitational field, see Table 2.5). /7

All dimensional constants which are originally given in the system of units kg, m, and sec, can be subjected to multiplexing with the scale factors EM and ESEC, which are given as actual parameters of the subprograms CONST and CONGR.

The problem is that for various AES it may be necessary to conduct the calculations in various systems of units: kg, m, sec; 1000000 m, 1000 sec, and so forth. The system of units chosen for calculations can be fixed by two scale factors: EM, ESEC--the number of meters in the chosen unit of measuring distance and the number of seconds in the chosen unit of measuring time. In the case that the system of units is kg, m, and sec.--EM=1, ESEC=1.

Dimensional reference data, such as T, s, y, z, v,  $v_x$ ,  $v_y$ ,  $v_z$ , a, SB and so forth, should be translated into the system of units which are fixed by the scale factors EM, ESGC, for which the scale factors from corresponding units of COMMON can be used (see Table 2.3).

In these subprograms for which the descriptions do not contain indication of the system of units in which the dimensional reference data should be fixed and resulting in dimensional results, it is

implied that it is a system of units fixed by the scale factors EM and ESEC. The current moment of time is given by the date and Moscow time T, figured from that particular date. The date can be given as the calendar date or as the RJD, the relative Julian date (see p. 1.2).

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The time T is measured in seconds (or in units determined by the scale factor ESEC). Only in the subprograms HMSSEC (B03) and SECHMS (B04) is the time T always measured in seconds.

In several of the subprograms of the library (usually the subprograms of other authors, for example DENS (D02), ADEN (D03)) the dimensional reference data should be given in definite units. This is discussed in the descriptions of the corresponding subprograms.

### 1.3 Systems of Coordinates, Time and Designations

1. The following system of coordinates is used. Greenwich relative rectangular coordinate system  $O_{xyz}$ , coordinated with the rotating Earth:

the center O coincides with the Earth's center;

the axis  $O_z$  coincides with the rotational axis of the Earth and is oriented towards the North pole;

the axis  $O_x$  is oriented towards the point of intersection of the Earth's equator and the Greenwich meridian;

the axis  $O_y$  completes the system to the right

The absolute rectangular quadrangle (equatorial, stellar) systems of coordinates OXYZ:

the center O coincides with the center of the Earth;

the axis OZ coincides with the Earth's rotational axis oriented towards the North pole;

the axis OX is oriented towards the point of the vernal equinox (at the current moment);

the axis OY completes the system to the right.

Oscillating system of coordinates (elements of the orbit). The elements of this system of coordinates are:

- a -the semimajor axis of the orbit;
- e -eccentricity;
- i -inclination (the angle of incline of the plane of orbit and the equatorial plane);
- $\Omega$  -the longitude of the ascending vertex of the orbit (calculated along the equatorial arc

- from the direction towards the point of spring counterclockwise);
- $\omega$  -argument of perigee (angular distance from the ascending vertex to the perigee);
- $\tau$  -the time of passage through the perigee.

The position of the satellite in orbit is determined by the argument of latitude  $u$  (angular distance of the AES from the ascending orbital vertex).

2. In descriptions of the subprogram library, the following concepts are connected with the estimation of time [4].

- the Gregorian calendar (GU)--contemporary chronology
- the Julian computation of time--the system of continuous count of days from the beginning of the Julian period, year 4713 to the New era January 1, 12<sup>h</sup> according to the Gregorian calendar.
- JD--the Julian date, the number of days which have passed since the beginning of the Julian period.
- In many of the subprograms the relative Julian date (RJD) is used, the number of days which have passed since 1900, January 0.12<sup>h</sup> of ephemeris time.

$$RJD=JD-2415020.0$$

- The stellar local time [2] at the given meridian (S) is the time calculated from the moment of the upper culmination of the point of the vernal equinox to any other of its positions. Stellar time is numerically equal to the hour angle of the point of the vernal equinox.

3. For several of the quantities more frequently encountered in the subprogram descriptions we will introduce constant designations (identifiers of these quantities). /10

RJD-relative Julian date;

T,TR- Moscow time, calculated from a certain date in seconds (or in other units fixed by the scale factor ESEC);

SO-stellar time on the Greenwich meridian at midnight in Greenwich on the corresponding date;

ST-stellar time on the Greenwich meridian at the moment of time T;

YA-array containing  $X, Y, Z, V_x, V_y, V_z$   
(absolute systems of coordinates);  
YG-array containing  $x, y, z, v_x, v_y, v_z$   
(Greenwich coordinate system);

Y-array containing coordinates and  
constituents of a vector of velocity in an  
arbitrary system of coordinates;

XA-array containing only  $X, Y, Z$ ;

XG-array containing only  $x, y, z$ ;

X-array containing AES coordinates in a  
random system of coordinates;

A-array containing elements of orbit

$a, e, i, \Omega, \omega, u$  ;

SB-ballistic coefficient;

P-atmospheric density.

When the size of an array is mentioned in the descriptions,  
instead of the words "array Y is reserved for 6 real values,"  
it will be written "array Y<sub>6</sub>."

When the size of an area reserved in the COMMON/B/3 block  
is mentioned, the number 3 indicates the quantity of real values  
for which block B is reserved.

2.1 Basic Constants (A01-CONST)

1. Function. The subprogram CONST dispatches to the common area (COMMON) the values of dimensional and non-dimensional constants which are used in the system of subprograms for computing navigational information which characterizes the position of the AES, and translates the dimensional constants into any given system of units. In Tables 2.1-2.4 a list is introduced of corresponding constants, their standard designations, the values and dimensions in the units (kg, m, and sec). For an assignment of the needed system of units the following parameters are used:

EM-number of meters in the unit of measuring distance;

ESEC-number of seconds in the unit of measuring time.

For example, if for computations the chosen units are kg, m, and sec, then EM=1, and ESEC=1. In order to carry out computations in the systems of units, kg, 1000 km, 1000 sec then it is necessary to let EM=1,000,000, and ESEC=1000.

2. Structure. Subprogram CONST.

The Common Units

*/CAED/1, /CA00/2, /CA00A/2, /CA22/4, /COR/1, /CORL/1,  
/CGRS/2, /CGM/1, /CRE/1, /CRZ/1, /CAE/2, /CAEL/1, /CCLZ/1,  
/COMZ/1, /COMZP/2, /CSDAY/1, /CT3/1, /CKDM/13, /CDSJS/1,  
/CPI/3, /CDEGR/1, /CHRAD/1, /CE2/1, /CE3/1, /CE4/1, /CE6/1, /CC60/1,  
/CC3600/1, /BEM/2, /CEV/1, /CESB/1, /CELB/1, /CERO/1, /CHA/20.*

3. Access: Call CONST (EM, ESEC).

4. Raw data: EM, ESEC.

5. Results, use of the area COMMON.

The values of constants in accordance with Tables 2.1-2.4 are dispatched to the units of Common enumerated in p. 2.

6. Text

```

SUBROUTINE CONST(EH,ESEC)
DIMENSION A(70),K(13)
DATA A/1.E0,1.5E5,3.E5,6.E5,0.E5,1.4141E-7,2.173E-9,.4801E-11
      ,.0904E-13,.0407E-14,.1469E-6,.8004E-10,.7111E-11
      ,.1931E-11,0.,.1787E-3,.3734E-4,.1547E-4,.9275E-5,.954E-3/
DATA K/0.,31,50,70,120,151,181,212,243,273,304,334,365/
COMMON /CHA/HA(5),AA(5),Q1(5),Q2(5)
COMMON /CAR0/AR0
COMMON /CA00/AA00,AR0
COMMON /CA00A/A00A,AR0A
COMMON /CA22/AR22,AR22,AR30,AR40
COMMON /CGR/GR
COMMON /CGR1/GR1
COMMON /CGRS/GRS,DGRS
COMMON /CGH/GH
COMMON /GRE/RE
COMMON /CRZ/RZ
COMMON /CAE/AE,AL
COMMON /ZC/EC/ZEL
COMMON /COLZ/CLZ
COMMON /COMZ/OMZ
COMMON /COMZP/OMZP,OMZK
COMMON /SDAV/SDAV
COMMON /CT3/T3
COMMON /CK00/K00(13)
COMMON /DSJS/DSJS
COMMON /CPI/PI,PI02,PI2
COMMON /CDEGR/DEGR
COMMON /CHRAD/HRAD
COMMON /ER2/ER2

```

```

COMMON /CL0/ER0
COMMON /ER4/ER4
COMMON /ER6/ER6
COMMON /C000/C000
COMMON /C0000/C0000
COMMON /EM/EM1,ESEC1
COMMON /CEV/EV
COMMON /CER0/ER0
COMMON /CESB/ERB
COMMON /CELB/ELB
ER0=140600./E5/EM
C000=C0000/EM
ER012=C00012*ECOM2
ER02=C0002*ECOM2
AR22=-0.7886,473*ECOM2
A00A=-.025009349EM*ECOM2
AR0A=-.478913065EM*ECOM2
AR22=93.44706*ECOM2
ER22=-55.24096*ECOM2
AR30=150.7066*ECOM2
AR40=24.29772*ECOM2
ER2=149.5013E15*ECOM2/EM
ER1=149.5013E15*ECOM2/EM
GRS=.13217011*ECOM2/EM

```

```

OMZK=0.0002*OMZ
SDAV=86600./T3*E
T3=10000./ESEC
DO 1 J=1,13
K00(J)=K(J)
DSJS=36525.
PI02=1.57079633
PI=3.14159265
PI2=6.28318531
DEGR=57.2957795
HRAD=DEGR/15
ER=1ER
ER4=1ER4
ER6=1ER6
CAU=60.
C0000=3600.
EM1=EM
ESEC1=ESEC
EV=EM/ESEC
ESB=EV*EV*EM
ELB=EV/ESEC
ER0=ESB*EM

```

```

      BARS=1L10
      H1E=9.3106D
      H2E=0378388./EM
      H3E=0371900./EM
      H4E=0378140./EM
      A1E=3.35289137E-7
      A2E=AE*AL
      C1E=0033545B
      O1E=72921575E-4*ESFC
  
```

```

      E1Z=EM*EM
      M=E/12/L6DM2
      D3=0.5701D
      H3=0.5701D
      AA(J)=A(J+5)*M
      R1(J)=A(J+10)*EM
      R2(J)=A(J+15)*EM
      RETURN
      END
  
```

## 2.2 Coefficients of Expansion of the Earth's Gravitational Field in Spherical Functions (AOZ-CONGR)

1. Function: Subprogram CONGR dispatches the values of coefficients of expansion of the Earth's gravitational field in spherical functions (5) to the common region (COMMON) and translates these coefficients into the given system of units. Values of the coefficients are given in table 2.5. These coefficients are used only in subprograms for computing anomalies of the Earth's gravitational field.

2. Structure. Subprogram CONGR.

COMMON units: /BCONGR/546.

3. Access: CALL CONGR (EM, ESEC).

4. Raw Data: EM, ESEC

5. Results, use of the area COMMON.

In the unit COMMON/BCONGR/ANM (273), BNM (273), in accordance with table 2.5, the values of  $C_{nm}$  are dispatched to array ANM, and the values  $\beta_{nm}$  are dispatched to array BNM.

Table 2.1 Astronomical units, gravitational characteristics, parameters of the Earth's ellipsoid, angular velocity of the Earth's rotation.

Units	Identifiers	Type	Designation	Values (kg, m, sec.)	Dimensions	Contents
/CAED/	AEI		E.C.	149600 10 <sup>9</sup>	M	astronomical unit
/CAOD/	AOI		C <sub>100</sub>	62564230.6	M <sup>2</sup> /sec <sup>2</sup>	parameters of the Earth's normal gravitational field
/CAQDA/	AQA		C <sub>20</sub>	61883.873	M <sup>2</sup> /sec <sup>2</sup>	resolution ratio of the Earth's gravitational field
/CA22A/	AQA		C <sub>40</sub>	62564934.9	M <sup>2</sup> /sec <sup>2</sup>	Additional variant according to spherical functions
/CGR/	AQA		C <sub>20</sub>	67891.5965	M <sup>2</sup> /sec <sup>2</sup>	effect of the gravitational constant on masses accordingly
/CGRL/	AQA		C <sub>20</sub>	98.44753	M <sup>2</sup> /sec <sup>2</sup>	scale factors for the acceleration of the forces of gravity on the Earth's surface
/CGRS/	AQA		C <sub>20</sub>	160.7058	M <sup>2</sup> /sec <sup>2</sup>	equatorial radius of semi-major axis of the Earth's ellipsoid
/CGM/	AQA		C <sub>40</sub>	99.29772	M <sup>2</sup> /sec <sup>2</sup>	contraction of the Earth's ellipsoid
/CGRE/	GR	REAL	A	0.3986013 10 <sup>10</sup>	M <sup>3</sup> /sec <sup>3</sup>	
/CRZ/	GR		M <sub>0</sub>	0.49027779 10 <sup>15</sup>	M <sup>3</sup> /sec <sup>3</sup>	
/CAE/	GRS		M <sub>0</sub> 10 <sup>-10</sup>	0.132712517 10 <sup>11</sup>	M <sup>3</sup> /sec <sup>3</sup>	
/CAEL/	GRS		C	9.90665	M	
/CCLZ/	GM		C <sub>2</sub>	6378388	M	
/COMZ/	GM		R	6371000	M	
/CONZP/	GM		C <sub>4</sub>	6378140	M	
	GM		C <sub>6</sub>	0.00335289187	M	
	GM		C <sub>8</sub>	0.993305458	M	
	GM		(1-0 <sub>1</sub> ) <sup>4</sup>	0.729211575 10 <sup>-4</sup>	M	
	GM		ω <sub>0</sub>		I/sec.	angular velocity of the earths rotation.
	GM		2ω <sub>0</sub>		I/sec.	
	GM		ω <sub>0</sub> <sup>2</sup>		I <sup>2</sup> /sec <sup>2</sup>	

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Table 2.2 Constants used in the measurement of time.

1	2	3	4	5	6
Units COMMON	Identifiers	Type	Values	Content	
1 /CSDAY/	SDAY	REAL	86400	1 days in seconds	
2 /CT3/	T3	REAL	10800	3 hours in seconds	
3 /CKDM/	KDM	INTEGER ARRAY	0 3I 59 90 120 151 181 212 243 273 304 334 365	interval of time in days from Greenwich midnight, Jan 1, of the current year to Greenwich midnight on the first day of the corresponding month: number of days in the year	
4 /CDSJS/	DSTS	REAL	36525	Julian centuries in ephemeris days	

Table 2.3 Auxilliary constants, scale factors

1	2	3	4	5	6
I /CPI/	PI		3.14159265	$\pi$	
	PID2		1.57079633	$\pi/2$	
	PI2		6.28318531	$2\pi$	
2 /CDEGR/	DEGR		57.2957795	radian in degrees	
3 /CHRAD/	HRAD		DEGR/15.	radian in hours	
4 /CE2/	E2		100		
5 /CE3/	E3		1000		
6 /CE4/	E4		10000		
7 /CE6/	E6		1000000		
8 /CC60/	C60		60		
9 /CC3600/	C3600		3600		
10 /BEM/	EM ESEC	REAL	EM ESEC	distance times	
11 /CEV/	EV		EM/ESEC	velocity	
12 /CESB/	ESB		EM <sup>3</sup> /ESEC <sup>2</sup>	SB	
13 /CELB/	ELB		EM/ESEC <sup>2</sup>	B	
14 /CERO/	ERO		EM <sup>2</sup> /ESEC <sup>2</sup>	density	

Table 2.4. Characteristics of the standard five-layer model of the Earth's atmosphere:  $h_{i-}$  - layer boundaries by altitude,  $A_i, k_{1,i}, k_{2,i}$  - model coefficients ( $i = 1, 2, \dots, 5$ )

ID	Units COMMON	Identifiers	Specifications	Length of array	Designations	Values	Dimensions	
I	/CHA/20	HA	ARRAY	5	$h_{i-}$ ( $i=1\div 5$ )	100000	M	
						150000		M
						300000		M
						600000		M
						900000		M
		AA	ARRAY	5	$A_i$ ( $i=1\div 5$ )	0,4141 $10^{-7}$	$kg\text{cm}^2\text{M}^{-4}$	
						0,2173 $10^{-9}$		$kg\text{cm}^2\text{M}^{-4}$
						0,4861 $10^{-11}$		$kg\text{cm}^2\text{M}^{-4}$
						0,8904 $10^{-13}$		$kg\text{cm}^2\text{M}^{-4}$
						0,6497 $10^{-14}$		$kg\text{cm}^2\text{M}^{-4}$
		Q1	ARRAY	5	$k_{1,i}$ ( $i=1\div 5$ )	0,1469 $10^{-8}$	$\text{M}^{-2}$	
						0,8004 $10^{-10}$		$\text{M}^{-2}$
						0,7111 $10^{-11}$		$\text{M}^{-2}$
						0,1831 $10^{-11}$		$\text{M}^{-2}$
						0		$\text{M}^{-2}$
		Q2	ARRAY	5	$k_{2,i}$ ( $i=1\div 5$ )	0,1787 $10^{-3}$	$\text{M}^{-1}$	
						0,3734 $10^{-4}$		$\text{M}^{-1}$
						0,1547 $10^{-4}$		$\text{M}^{-1}$
						0,9275 $10^{-5}$		$\text{M}^{-1}$
						0,954 $10^{-5}$		$\text{M}^{-1}$

Table 2.5 Resolution ratios of the Earth's gravitational field by spherical function (unit COMMON/BCONGR/ANM (273), BNM (273)).

ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	ANM (sec)	
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4
5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5
6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7
8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9
10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11
12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12
13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13
14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
15	15	15	15	15	15	15	15	15	15	15	15	15	15	15	15	15	15	15	15	15
16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16
17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17
18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18
19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19
20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20
21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21
22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22
23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23
24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24
25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25
26	26	26	26	26	26	26	26	26	26	26	26	26	26	26	26	26	26	26	26	26
27	27	27	27	27	27	27	27	27	27	27	27	27	27	27	27	27	27	27	27	27
28	28	28	28	28	28	28	28	28	28	28	28	28	28	28	28	28	28	28	28	28
29	29	29	29	29	29	29	29	29	29	29	29	29	29	29	29	29	29	29	29	29
30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30
31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31
32	32	32	32	32	32	32	32	32	32	32	32	32	32	32	32	32	32	32	32	32
33	33	33	33	33	33	33	33	33	33	33	33	33	33	33	33	33	33	33	33	33
34	34	34	34	34	34	34	34	34	34	34	34	34	34	34	34	34	34	34	34	34
35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35
36	36	36	36	36	36	36	36	36	36	36	36	36	36	36	36	36	36	36	36	36
37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37
38	38	38	38	38	38	38	38	38	38	38	38	38	38	38	38	38	38	38	38	38
39	39	39	39	39	39	39	39	39	39	39	39	39	39	39	39	39	39	39	39	39
40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40
41	41	41	41	41	41	41	41	41	41	41	41	41	41	41	41	41	41	41	41	41
42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42
43	43	43	43	43	43	43	43	43	43	43	43	43	43	43	43	43	43	43	43	43
44	44	44	44	44	44	44	44	44	44	44	44	44	44	44	44	44	44	44	44	44
45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45
46	46	46	46	46	46	46	46	46	46	46	46	46	46	46	46	46	46	46	46	46
47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47
48	48	48	48	48	48	48	48	48	48	48	48	48	48	48	48	48	48	48	48	48
49	49	49	49	49	49	49	49	49	49	49	49	49	49	49	49	49	49	49	49	49
50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
51	51	51	51	51	51	51	51	51	51	51	51	51	51	51	51	51	51	51	51	51
52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52
53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53

Here ANM (1) =  $\alpha_{20} = 0$ , in so far as the corresponding member of the resolution is considered to be in the Earth's normal field (the value  $\alpha_{20}$  is from table 2.i).

Table 2.5 (continued)

80	12	4	0.72	10 <sup>-7</sup>	I12	I4	0	0.1	10 <sup>-7</sup>	-0.20	10 <sup>-10</sup>	0.213	10 <sup>-10</sup>	0.19	10 <sup>-7</sup>
81	12	5	0.34	10 <sup>-6</sup>	I13	I4	0	0.07	10 <sup>-6</sup>	-0.30	10 <sup>-10</sup>	0.20	10 <sup>-10</sup>	0	0.183
82	12	6	0.30	10 <sup>-6</sup>	I14	I4	10	0.07	10 <sup>-6</sup>	-0.19	10 <sup>-10</sup>	0.20	10 <sup>-10</sup>	0	0.183
83	12	7	0.17	10 <sup>-5</sup>	I15	I4	10	0.09	10 <sup>-5</sup>	-0.29	10 <sup>-10</sup>	0.21	10 <sup>-10</sup>	0.39	10 <sup>-7</sup>
84	12	8	0.42	10 <sup>-8</sup>	I16	I4	10	0.31	10 <sup>-5</sup>	-0.7	10 <sup>-10</sup>	0.22	10 <sup>-10</sup>	0.1	10 <sup>-7</sup>
85	12	9	0.57	10 <sup>-8</sup>	I17	I4	10	0.41	10 <sup>-5</sup>	-0.7	10 <sup>-10</sup>	0.23	10 <sup>-10</sup>	0.83	10 <sup>-7</sup>
86	12	10	0	10 <sup>-9</sup>	I18	I4	0	0	10 <sup>-5</sup>	0	10 <sup>-10</sup>	0.24	10 <sup>-10</sup>	0.83	10 <sup>-7</sup>
87	12	11	-0.14	10 <sup>-9</sup>	I19	I5	0	0.1	10 <sup>-4</sup>	0	10 <sup>-10</sup>	0.25	10 <sup>-10</sup>	0.13	10 <sup>-7</sup>
88	12	12	-0.24	10 <sup>-10</sup>	I20	I5	0	0.09	10 <sup>-4</sup>	0	10 <sup>-10</sup>	0.26	10 <sup>-10</sup>	0.13	10 <sup>-7</sup>
89	13	1	0	10 <sup>-10</sup>	I21	I5	2	0.31	10 <sup>-4</sup>	-0.44	10 <sup>-10</sup>	0.27	10 <sup>-10</sup>	0.43	10 <sup>-7</sup>
90	13	2	0.10	10 <sup>-10</sup>	I22	I5	3	0.14	10 <sup>-4</sup>	-0.64	10 <sup>-10</sup>	0.28	10 <sup>-10</sup>	0.43	10 <sup>-7</sup>
91	13	3	0.52	10 <sup>-10</sup>	I23	I5	4	0.91	10 <sup>-4</sup>	-0.57	10 <sup>-10</sup>	0.29	10 <sup>-10</sup>	0.90	10 <sup>-7</sup>
92	13	4	-0.53	10 <sup>-10</sup>	I24	I5	5	0.13	10 <sup>-4</sup>	0.507	10 <sup>-10</sup>	0.30	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
93	13	5	-0.89	10 <sup>-10</sup>	I25	I5	6	0.30	10 <sup>-4</sup>	-0.12	10 <sup>-10</sup>	0.31	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
94	13	6	-0.59	10 <sup>-10</sup>	I26	I5	7	0.36	10 <sup>-4</sup>	-0.88	10 <sup>-10</sup>	0.32	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
95	13	7	-0.57	10 <sup>-10</sup>	I27	I5	8	0.23	10 <sup>-4</sup>	-0.51	10 <sup>-10</sup>	0.33	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
96	13	8	0	10 <sup>-10</sup>	I28	I5	9	0.29	10 <sup>-4</sup>	0	10 <sup>-10</sup>	0.34	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
97	13	9	0.14	10 <sup>-7</sup>	I29	I5	10	0.27	10 <sup>-4</sup>	0	10 <sup>-10</sup>	0.34	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
98	13	10	0.75	10 <sup>-8</sup>	I30	I5	10	0.19	10 <sup>-4</sup>	0	10 <sup>-10</sup>	0.35	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
99	13	11	0.71	10 <sup>-9</sup>	I31	I5	11	0.19	10 <sup>-4</sup>	0	10 <sup>-10</sup>	0.36	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
100	13	12	0.50	10 <sup>-10</sup>	I32	I5	12	0.19	10 <sup>-4</sup>	0	10 <sup>-10</sup>	0.37	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
101	13	13	0.55	10 <sup>-10</sup>	I33	I5	13	0.19	10 <sup>-4</sup>	-0.51	10 <sup>-10</sup>	0.38	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
102	13	14	0.16	10 <sup>-11</sup>	I34	I5	14	0	10 <sup>-10</sup>	-0.31	10 <sup>-10</sup>	0.39	10 <sup>-10</sup>	0.27	10 <sup>-7</sup>
103	14	1	0.17	10 <sup>-10</sup>	I35	I6	0	0.31	10 <sup>-10</sup>	0.25	10 <sup>-10</sup>	0.41	10 <sup>-10</sup>	0.12	10 <sup>-7</sup>
104	14	2	-0.12	10 <sup>-10</sup>	I36	I6	1	0.31	10 <sup>-10</sup>	0.57	10 <sup>-10</sup>	0.42	10 <sup>-10</sup>	0.12	10 <sup>-7</sup>
105	14	3	0	10 <sup>-10</sup>	I37	I6	2	0.31	10 <sup>-10</sup>	0.35	10 <sup>-10</sup>	0.43	10 <sup>-10</sup>	0.12	10 <sup>-7</sup>
106	14	4	-0.46	10 <sup>-10</sup>	I38	I6	3	0.31	10 <sup>-10</sup>	0.27	10 <sup>-10</sup>	0.44	10 <sup>-10</sup>	0.12	10 <sup>-7</sup>
107	14	5	-0.17	10 <sup>-10</sup>	I39	I6	4	0.31	10 <sup>-10</sup>	0.14	10 <sup>-10</sup>	0.45	10 <sup>-10</sup>	0.12	10 <sup>-7</sup>
108	14	6	-0.37	10 <sup>-10</sup>	I40	I6	5	0.31	10 <sup>-10</sup>	-0.12	10 <sup>-10</sup>	0.46	10 <sup>-10</sup>	0.12	10 <sup>-7</sup>
109	14	7	-0.48	10 <sup>-10</sup>		I6	6	0	10 <sup>-10</sup>	-0.12	10 <sup>-10</sup>	0.47	10 <sup>-10</sup>	0.12	10 <sup>-7</sup>
110	14	8	0	10 <sup>-10</sup>		I6	6	0	10 <sup>-10</sup>	-0.12	10 <sup>-10</sup>	0.48	10 <sup>-10</sup>	0.12	10 <sup>-7</sup>



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NO. 10-1118X 2-  
ECOM2=ECOM2\*ECOM2  
10 1 1 1/2/3  
ANN(1)=A(1)\*ECOM2  
BN(1)=B(1)\*ECOM2  
RETURN  
END

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CHAPTER 3  
SUBPROGRAMS FOR THE TRANSFORMATION  
OF TIME AND COORDINATES  
(INDEX B)

3.1 Transition from GU, the Calendar Date,  
to RJD, Relative Julian Date (B01-  
DATDAY)

1. Function: the program determines the RJD, the relative Julian date, the number of days which have passed since the mean Greenwich midday, January 0, 1900 until the mean Greenwich mid-night of the given calendar date.

2. Structure. Subprogram: DATDAY.  
Common units: /CKDM/13, /CE2/1.

3. Access: CALL DATDAY (DTK, RJD).

4. Raw data: DTK-real variable containing the date GU which is given by the decimal fraction of the type:  $\emptyset$ . DDMMGG, where DO is the date, MM is the month's number and GG is the year's number minus 1900 (the two last numbers of the year).

5. Results: RJD-relative Julian date.

6. Use of the COMMON units. Constants are used from the units: /CKDM/13, /CEZ/1 (No. 3 Table 2.2., No. 4 Table 2.3).

7. Algorithm:  $RJD = 365GG + \lfloor (GG-1)/4 \rfloor - 0,5 + t$  where GG is the number of years minus 1900, the number of days passed since January 0 of the current year until the given date. [x] is the whole part of x.

/20

8. Text

<pre> SUBROUTINE DATDAY(DAT:DAY) COMMON/CEZ/ER COMMON/CKDM/CKDM(13) N=DAT*ER NDT=1 I=(1-NDT)*ER N=N+I N=(N-11)*ER N=N+.5                 </pre>	<pre> JG=0 KDTG=KDM(N1)+NDT1 KVG=(JG-1)/4 IF((KVG+1)*4-N1)2,1,2 1 IF(N1-2)2,2,3 3 KDTG=KDTG+1 2 DAY=JG*CKDM(13)+KVG+KDTG-.5 RETURN END                 </pre>
---	---

3.2 Transition from RJD (the relative Julian date) to GU, the  
Calendar Date (B02-DAYDAT)

1. Function. For the moment of time, given by RJD the relative Julian Date (see p. 1.3), the calendar date is determined.

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The moment of time can also be given in the form of RJD and the time T in seconds (or in units given by the scale factor ESEC, calculated from midnight of the RJD date (the interval of time T may contain any number of days). A result of the operation of subprogram DAYDAT, the interval which is a multiple for whole days is excluded from the time T; TR is obtained, and the days excluded from T are added to the date RJD and the RJDR is obtained. The calendar date is determined for the RJDR date.

2. Structure. Subprogram DAYDAT  
Common units: /CSDAY/1, /CKDM/13, /CCGO/1.

3. Access: CALL DAYDAT (RJD, T, RJDR, TR, ND, NM, NG)

4. Raw data: RJD-relative Julian date. T-time (in seconds), calculated from the RJD date.

5. Results: RJDR-relative Julian date; TR-time in seconds, calculated from the RJDR date: ND, NM, NG-whole variables containing the corresponding number, month and year (minus 1900), corresponding to the RJDR date.

6. Use of the area COMMON. Constants are used from the units COMMON/CSDAY/1, /CKDM/13, /CCGO/1 (No. 1.3 of table 2.2, No. 8<sup>21</sup> of table 2.3).

7. Algorithm. Let RJD be the reference Julian date, T the time in seconds calculated from midnight of the RJD date.

$$RJDR = RJD + [T/SDAY]; \quad TR = T - [T/SDAY] \cdot SDAY,$$

where SDAY is the number of seconds in the days, [x] is the whole part of x.

$$KVG = (RJDR - 365) / 1491; \quad K = RJDR - KVG; \quad N = K / 365,$$

where KVG is the number of leap years which have passed since 1900 to the given moment.

$$NG = \begin{cases} N, & \text{if } 4(KVG + 1) - k \geq 0 \\ N - 1, & \text{if } 4(KVG + 1) - k < 0. \end{cases}$$

The number of days, calculated from the beginning of the present year:

$$KDTG = K - 365NG + 1.$$

The month and day of an unknown date are determined with a comparison of KDTG with the array KDM<sub>i</sub> (i=1.13), in which the i element contains the number of days which have passed since the beginning of the present year (not a leap year) to the beginning of the i-month. In the case of a leap year, when KDTG ≥ 60 a correction is made.



8. Text.

```

S 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
C 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
D 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
E 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
F 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
G 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
H 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
I 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
J 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
K 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
L 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
M 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
N 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
O 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
P 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
Q 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
R 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
S 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
T 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
U 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
V 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
W 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
X 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
Y 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
Z 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25

```

```

2 KDTG=K-1-16*VDM(15)
  IF(IVS)5,3,6
3 IF(KDTG-CHU)6,4,5
4 HD=29
  NH=2
  GOTQ 10
5 KDTG=KDTG-1
6 DO 7 NH=1,15
  IF(KDTG-KON(TH))5,3,7
7 CONTINUE
8 NH=NH-1
  NH=KDTG-KON(TH)
9 RETURN
END

```

3.3 Conversion of Hours, Minutes and Seconds into Seconds  
(B03-HMSSEC)

/22

1. Function: Originating from the time given in hours, minutes, and seconds, the time is determined in seconds.
2. Structure. Subprogram HMSSEC  
Common units: /CE2/1,/CCG0/1,/CC3600/1.
3. Access: CALL HMSSEC (HMS, T).
4. Raw data: HMS-the real variable, containing the time given in hours, minutes and seconds in the following form:  
O. HHMMSSDS, where HH is the hours, MM the minutes, and SS the seconds with fractions.
5. Results: T-the time in seconds.
6. Use of the COMMON units. Constants are used from the units COMMON/CEZ/1,/CCG0/1,/CC3600/1 (Nos. 8 and 9 of Table 2.3).
7. Text.

```

S 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
C 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
D 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
E 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
F 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
G 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
H 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
I 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
J 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
K 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
L 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
M 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
N 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
O 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
P 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
Q 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
R 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
S 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
T 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
U 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
V 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
W 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
X 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
Y 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
Z 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25

```

3.4 Conversion of Seconds into Hours,  
Minutes, and Seconds  
(B04-SECHMS)

1. Function: Originating from the time given in seconds, the time is determined in hours, minutes, and seconds.
2. Structure: Subprogram SECHMS.  
Common units: /CCGØ/1, /CC 36ØØ/1.
3. Access: CALL SECHMS (T, KH, KM, SEC).
4. Raw data: T-time in seconds and fractions of seconds.
5. Results: KH-hours (whole variable), KM-minutes (whole variable), SEC-seconds and fractions of seconds (real variable). 23
6. Use of the area COMMON. Constants are used from the units COMMON/CCGØ/1, /CC36ØØ/1 (Nos. 8 and 9 of Table 2.3).
7. Text.

```

      COMMON /CCGØ/1, /CC36ØØ/1
      DIMENSION T(1), KH(1), KM(1), SEC(1)
      T(1) = T
      KH(1) = T / 3600
      KM(1) = (T / 60) - KH(1) * 60
      SEC(1) = T - KH(1) * 3600 - KM(1) * 60
      RETURN
      END

```

3.5 Stellar Time (B05-STTIME, STT)

1. Function: Subprogram STTIME determines the stellar time SO on the Greenwich meridian at Greenwich midnight of the given RJD date.

Subprogram STT according to the known SO determines stellar time ST on the Greenwich meridian at any moment of time T on the RJD date.

2. Structure: The independent subprogram STTIME and the subprogram-function STT.

Common units: /CSDJS/1, /CPI/3, /COMZ/1, /CT3/1, /BSO/3.

3. Description of the subprogram STTIME.  
Access: CALL STTIME (RJD, SO).  
Raw data: RJD-relative Julian date.  
Results: SO-stellar time on the Greenwich meridian in radians ( $SO \leq 2\pi$ ).

Use of the units COMMON. Constants are used from the units COMMON/CDSJS/<sub>1</sub>,/CPI/<sub>3</sub> (No. 4 of Table 2.2, No. 1 of Table 2.3).

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Algorithm:

$$SO = 6^h 38^m 45^s,836 + 8640184^s,542 T + 0^s,0929 T^2 + 0^s,061164 \Delta\psi,$$

$$\Delta\psi = -17,23 \sin \Omega,$$

$$\Omega = 259^{\circ} 10' 59'',79 - 1934^{\circ} 08' 31'',23 T + 7'',48 T^2 + 0'',0080 T^3,$$

$$T = RJD / 36525, RJD$$

4. Text.

```

SUBROUTINE STTIME(DAV,SO)
COMMON/CDSJS/CSJS
COMMON/CPI/PI,PI2,PI2
T=DAV/DSJS
SOM=SIN(((.387851E-7*T+.362640634E-4-.33.75714625)*T
+4.523601516))
W=625.33*T
N=N/PI2
W=W-N*PI2
SO=(6.755E-6*T+.19511E-2)*T+1.7399359-.766385E-4*SOM+W
N=SO/PI2
SO=SO-N*PI2
RETURN
END

```

5. Description of the subprogram-function STT.

Access: ST=STT(T).  
Raw data: T is the present moment in time in seconds, Moscow time.  
Results: ST-stellar time on the Greenwich meridian in radians.

Use of the region COMMON: in the unit COMMON/BSO/SO, TS, NS the following values should be initially placed:

SO-stellar time at Greenwich midnight on the date RJD,  
TS=0, NS=0, if T is calculated from the same RJD date.

In most cases the RJDI date and the locking of time T can be less than or equal to RJD. If  $RJDI < RJD$ , then TS and NS should contain (TS in seconds, and NS in days) the interval of time between the RJDI and RJD dates. /25

Constants are used from the units COMMON/COMZ/1, /CT3/1 (No. 14 of Table 2.1 and No. 2, Table 2.2).

Algorithm. Stellar time ST is calculated according to the following approximate formula:

$$ST = SO + \omega_3(T - TS, -10800^s)$$

where  $\omega_3$  is the absolute angular velocity of the Earth's rotation.

SO-is the stellar time at Greenwich midnight on the RJD date,

T- is the Moscow time, figured from the RJDI date, usually different from the RJD ( $RJDI \leq RJD$ ) date,

$TS=86400^s (RJD-RJDI)$ .

Text:

```
FUNCTION STT(T)
COMMON/BSO/SO,TS,NS
COMMON/CT3/CT3
COMMON/COMZ/COMZ
STT=SO+CT3*(T-TS-CT3)
RETURN
END
```

### 3.6 Transition from the Absolute System of Coordinates to the Greenwich and the Reverse: from the Greenwich System to the Absolute (B06-AGIGA,AGIGAC)

1. Function. According to the known values  $X, Y, Z, V_x, V_y, V_z$  in the absolute system of coordinates, the subprogram AGIGA determines the values of  $x, y, z, v_x, v_y, v_z$  in the Greenwich relative system of coordinates; the transition back is also possible:  $x, y, z, v_x, v_y, v_z \rightarrow X, Y, Z, V_x, V_y, V_z$ . The subprogram AGIGAC makes the same conversion possible only with the coordinates:  $X, Y, Z \rightarrow x, y, z$  and  $x, y, z \rightarrow X, Y, Z$ .

2. Structure. Subprograms: AGIGA, AGIGAX  
Common units: /COMZ/1, /CT3/1.

3. Access to AGIGA: CALL AGIGA (SO, T, Y1, 1, YR).  
Raw data: T-Moscow time (in seconds).

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SO--stellar time on the Greenwich meridian at Greenwich midnight; Y1<sub>6</sub>--array of reference values of coordinates and constituents of the velocity vector; I--indicator of the transition. I=1 during the transition from the absolute system of coordinates to the Greenwich, I=2 during the transition from the Greenwich system of coordinates to the absolute.

Results: YR<sub>6</sub>--array of values of coordinates and constituents of the velocity vector in the resulting system of coordinates.

4. Access to AGIGAC: CALL AGIAC(ST, X1, 1, XR).  
Raw data: St--stellar time on the Greenwich meridian at the present moment of time; x1<sub>3</sub>--array of base coordinate values; l--indicator of the coordinate transition (which both by its meaning and values conforms to the I parameter in subprogram AGIGA).

Results: XR--array of coordinate values in the resulting system of coordinates.

5. Use of the area COMMON: in subprogram AGIGA constants are used from the units COMMON/COMZ/1, /CT3/1 (No. 14, Table 2.1, No. 2, Table 2.2).

6. Algorithm: a) transition from X, Y, Z, V<sub>x</sub>, V<sub>y</sub>, V<sub>z</sub> to x, y, z, v<sub>x</sub>, v<sub>y</sub>, v<sub>z</sub> is conducted according to the formula:

$$\begin{aligned}x &= X \cos \beta + Y \sin \beta, & v_x &= V_x \cos \beta + V_y \sin \beta + \omega_3 Y, \\y &= -X \sin \beta + Y \cos \beta, & v_y &= -V_x \sin \beta + V_y \cos \beta - \omega_3 X, \\z &= Z, & v_z &= V_z\end{aligned}$$

where  $\beta = SO + \omega_3(T - 3^h)$ ,

SO--stellar time at Greenwich midnight.  
W3--angular velocity of the Earth's rotation,  
T--Moscow time

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b) transition back from x, y, z, v<sub>x</sub>, v<sub>y</sub>, v<sub>z</sub> to X, Y, Z, V<sub>x</sub>, V<sub>y</sub>, V<sub>z</sub> is conducted according to the formula:

$$\begin{aligned}X &= x \cos \beta - y \sin \beta, & V_x &= v_x \cos \beta - v_y \sin \beta - \omega_3 Y, \\Y &= x \sin \beta + y \cos \beta, & V_y &= v_x \sin \beta + v_y \cos \beta + \omega_3 X, \\Z &= z, & V_z &= v_z.\end{aligned}$$

In subprogram AGIGAC  $ST = \beta$

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```

COMMON /GGR/ A, YA
B=50+0.17*(Y-Y1)
U(1)=520*(B)
U(2)=GGRS(B)
U(3)=-U(1)
A=0.17
X=XI(1)
Z=XI(3)
GOTO(2,1),1
1 A=-A
U(3)=-U(3)
U(1)=-U(1)
2 DO 3 J=1,2
XR(J)=U(J-1)*Y+U(J)*XI(2)
3 XR(J+3)=U(J+1)-Z*U(J)*XI(3)
XR(4)=XR(4)+A*X(2)
XR(5)=XR(5)-A*X(1)
XR(3)=U(3)
XR(6)=U(6)
RETURN
END

```

```

SUBROUTINE ARIGAC( ST, XI, I, XR)
DIMENSION XI(3), XR(3)
CH=COS( ST)
SH=SIN( ST)
GOTO(2,1),1
2 SH=-SH
1 W=XI(1)*SH
XR(1)=XI(1)*CH-XI(2)*SH
XR(2)=XI(2)*CH+W
XR(3)=XI(3)
RETURN
END

```

3.7 Determination of Coordinates and Constituents of the Velocity Vector in the Absolute System of Coordinates According to the Elements of Orbit (BO7-3 ABS)

1. Function: according to the known elements of orbit:  $a, e, i, \Omega, \omega, u, X, Y, Z, V_x, V_y, V_z$  are determined.
2. Structure. Subprogram MIABS  
Common units: /GGR/1.
3. Access: CALL MIABS (A, YA).
4. Raw data: Array  $A_6$ , containing values of the orbital elements in the following order:  $a, e, i, \Omega, \omega, u$ . All angles should be given in radians. /28
5. Results: Array  $Y_6$ , containing values of  $X, Y, Z, V_x, V_y, V_z$  in the absolute system of coordinates.
6. Application of the area COMMON. Constants are used from the unit. /GGR/1 (No. 5 table 2.1).
7. Algorithm: The following correlations are used:
 
$$X = r (\cos \Omega \cos u - \sin \Omega \sin u \cos i),$$

$$Y = r (\sin \Omega \cos u + \cos \Omega \sin u \cos i),$$

$$Z = r \sin u \sin i,$$

$$V_x = V_r (\cos \Omega \cos u - \sin \Omega \sin u \cos i) - V_u (\cos \Omega \sin u + \sin \Omega \cos u \cos i),$$

$$V_y = V_r (\sin \Omega \cos u + \cos \Omega \sin u \cos i) - V_u (\sin \Omega \sin u - \cos \Omega \cos u \cos i),$$

$$V_z = V_r \sin u \sin i + V_u \cos u \sin i,$$

where

$$r = P / (1 + e \cos v), \quad v = u - \omega,$$

$$V_r = (\mu/P)^{1/2} e \sin v, \quad V_u = (\mu/P)^{1/2} (1 + \cos v), \quad P = a(1 - e^2),$$

$\mu$  - product of the gravitational constant into the Earth's mass.

8. Text.

```

SUBROUTINE ELABT(A,X)
DIMENSION A(4),Y(6),U(6)
COMMON/CGR/CP
P=A(1)*A(1)+A(2)*A(2)
A(2)=A(6)-A(3)
DO 1 J=1,4
U(J)=COS(A(J+2))
1 U(J+4)=SIN(A(J+2))
X(1)=U(4)*U(2)
X(2)=-U(4)*U(5)
U(1)=SQRT(CR/P)
UR=U(1)*A(2)*U(7)
R=1.+A(2)*U(3)
U(1)=V(1)
4 X=U/R
P=U(4)*U(1)
U(1)=U(4)*U(2)
U(2)=U(2)
U(3)=-U(3)
DO 2 J=1,2
X(J)=U(J+4)*U(4)-U(J+5)*P
2 X(J+3)=U(J+4)*U(5)+U(J+5)*U(1)
DO 3 J=1,3
X(J+3)=X(J)*UR-V(J+3)*U(1)
3 X(J)=X(J)*R
A(2)=A(6)-A(3)
RETURN
END

```

3.8 Determination of Orbital Elements and the Position of Points on the Orbit According to Known Coordinates and Constituents of the Velocity Vector in the Absolute System of Coordinates  
(BO8-ABSEL)

/29

1. Function: According to the known coordinates X, Y, Z and the constituents of the velocity vector  $V_x$ ,  $V_y$ ,  $V_z$  in the absolute system of coordinates, the elements of orbit  $a$ ,  $e$ ,  $i$ ,  $\Omega$ ,  $\omega$ , are determined as well as their position in the orbit  $u$ .

2. Structure. Subprogram ABSEL  
Common units: /CGR/1, /CP1/3.

Access: CALL ABSEL (YA, A).

4. Raw data:

Array YA<sub>6</sub>, containing the values of X, Y, Z, V<sub>x</sub>, V<sub>y</sub>, V<sub>z</sub>.

5. Results: Array A<sub>6</sub>, which contains the values of orbital elements in the following order: a, e, i, Ω, ω. The values of all angles are in radians.

6. Use of the area COMMON. Constants are used from units /CGR/1, /CPI/3 (No. 5 of Table 2.1, No. 1 of Table 2.3).

7. Algorithm.  $a = r/(2-k)$ ,  $k = rV^2/\mu$ ,  $V^2 = V_x^2 + V_y^2 + V_z^2$ ,  
 $r^2 = X^2 + Y^2 + Z^2$ ,  $e = \{1 - k(2-k)\cos^2 Q\}^{1/2}$ ,

$$\sin Q = (XV_x + YV_y + ZV_z)/rV,$$

$$i = \pi/2 - \arctg \frac{c_3}{\sqrt{c_1^2 + c_2^2}}, \quad 0 \leq i \leq \pi,$$

$$c_1 = YV_z - ZV_y, \quad c_2 = ZV_x - XV_z, \quad c_3 = XV_y - YV_x,$$

$$c = (c_1^2 + c_2^2 + c_3^2)^{1/2},$$

$$\Omega = \arctg \left( \frac{c_1}{-c_2} \right), \quad \nu = \arctg \frac{k \sin Q \cos Q}{k \cos^2 Q - 1},$$

$$u = \arctg \frac{Zc}{Yc_1 - Xc_2}, \quad \omega = u - \nu,$$

μ - product of the gravitational constant into the Earth's mass. /30



8. Text.

```

CURROUT:ME ABSEL(X,A)
DIMENSION X(6),A(6),C(4),S(4)
DIMENSION U(6)
COMMON/CGR/GR
COMMON/CE1/PI,P12,P12
I=0
I=0
V=0
DO 1J=1,3
E=X(J)*X(J)+P
V=X(J+3)+X(J+3)+V
YV=X(J)*Y(J+3)+XY
P=SQRT(P)
AE=(E/GR)*U
P=SQRT(P)
DO 12 J=1,3
U(1)=X(J)/R
U(2)=Y(J+3)/V
U(3)=V(2)*V(5)-V(3)*V(5)
U(4)=V(3)*V(4)-V(1)*V(6)
U(5)=V(1)*V(5)-V(2)*V(4)
CN=C(1)*C(1)+C(2)*C(2)+C(3)*C(3)
CN=SQRT(CN)
C(4)=P
IF(CN=1,E=0)14,14,14
13 C(4)=C(1)*X(2)/U(1)-C(2)*V(1)/U(1)
14 C(1)=SQRT(C(1)*C(1)+C(2)*C(2))
S(4)=X(3)
C(2)=C(1)
C(1)=C(3)
SL=XV/P/V
CR=1.-SQ(4)
V=P.-AV
Z(1)=R/V
C(3)=AK*GR-1.
Z(2)=SL*Z(1)-C(2)*GR
C(2)=AK*GR*Z(2)
C(2)=-C(2)
DO 2J=1,4
IF(C(J))4,7,4
3 Z(J+2)=SIGN(C(J),Z(J))
C(2)=9
4 Z(J+2)=ATAN (U(1)-Z(J))
IF(C(J))5,7,7
5 Z(J+2)=Z(J+2)+Z(J)
6 IF(A(J+2))7,7,7
7 Z(J+2)=Z(J+2)+Z(J)
8 CONTINUE
IF(A(5)=0)9,11,11
9 Z(3)=Z(3)-Z(1)
10 Z(5)=X(4)-Z(1)
11 Z(5)=Z(5)+Z(1)
12

```

3.9 Standard Array of Initial Conditions  
(BO9-TRDATO)

1. Function. Subprogram TRDATO extracts from the initial conditions, which are given in the standard form, information which is necessary for conducting navigational computations.

The initial conditions can be given in three forms: as the elements of orbit; as the coordinates and constituents of the velocity vector in the absolute (b) and Greenwich (c) system of coordinates. We will designate as PN the array which contains the initial conditions in the standard form. There are 12 elements in this array. In all three cases the first four elements and the second elements of that array contain the following parameters:

PN(1)-the number of AES and the launching date in the form of a decimal fraction, the first three numbers after the decimal point are the number of the AES, the following six numbers are the date (the year is indicated by the last two numbers);

PN(2)-the current date in the form: C.DDMMGG, where DD is the day, MM the month, and GG the year;

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PN(3)-the number of revolutions;

PN(4)-the present time in the form O.HHMMSSDS, where HH is the hour, MM the minutes, and SSDS the seconds and fractions of seconds ;

PN(11)-is the ballistic coefficient ( $m^3/kgsec^2$ ).

The rest of the elements of array PN are different for all three cases.

In the case a):PN(5) is the Draconian period in minutes,

PN(6)-the semimajor axis of orbit (m).

PN(7)-eccentricity,

PN(8)-angle of inclination of the orbit from the equator (degrees),

PN(9)-vertex of the orbit (degrees),

PN(10)-argument of perigee (degrees),

PN(12)-minimum altitude of the orbit (m).

In the case b):PN(5)-PN(10) contain respectively values X,Y,Z, $V_x$ , $V_y$ , $V_z$ ; PN(12)=2

In the case c):PN(5)-PN(10) contain values x,y,z, $v_x$ , $v_y$ , $v_z$ ; PN(12)=1.

In both cases the coordinates are given in meters, and the constituents of the velocity vector in m/sec.

In the work results of subprogram TRDATO the angles are translated into radians, the time into seconds, and the calendar date into the RJD. The stellar time is determined for Greenwich midnight on the current date, and the initial conditions are converted into all three systems of coordinates.

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Dimensional quantities are converted into the system of units given by the scale factors: EM, ESEC.

Note: If EM=1, then the initial conditions remain in meters and seconds.

2. Structure. Subprograms TRDATO.  
Access to the peripheral subprograms: DATDAY (BO1), HMSSEC(BO3), STTIME(BO5), AGIGA (BO6), ELABS (BO7), ABSEI (BO8).

Common units:/CDEGR/1, /CE3/1,/CC60/1.

3. Access:

CALL TRDATO (PN, NSP, DZ, RJD, NB, T, TD, SB, B, SO, A, YA, YG, EM, ESEC).

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4. Raw data: Array  $PN_{12}$ , which contains the initial conditions in one of the three forms described in p. 1;

EM, MSEC-scale factors.

In the case of a, it is necessary to make the value of  $A(6)-u$  (most often the initial conditions are given in the point of the ascending vertex of orbit, where  $u=0$ ).

5. Results: NSP-the number of the satellite;  
 DZ-the launching date in the form: O.DDMMGG;  
 RJD-the current date as the relative Julian date;  
 NB-the number of revolutions;  
 T-the current time in seconds;  
 TD-the period in minutes;  
 SB-the ballistic coefficient;  
 B-minimum altitude of the orbit;  
 SO-stellar time at Greenwich midnight on the current date;  
 Array  $A_6$ -which contains the elements of orbit  
 $a, e, i, \Omega, \omega, u$   
 (angles in radians);  
 Array  $YA_6$ -which contains  $X, Y, Z, V_x, V_y, V_z$ ;  
 Array  $YG_6$ -which contains  $x, y, z, v_x, v_y, v_z$ .

6. Use of the area COMMON: Constants are used from the units: /CDEGR/<sub>1</sub>, /CE3/<sub>1</sub>, /CGG0/<sub>1</sub> (Nos. 2, 5 and 8 of Table 2.3).

7. Text.

```

SUBROUTINE TPDATO(PN, NSP, DZ, DT, NB, T, TD, SB, B, SO, A, XA, XG,
*             EM, ESEC)
  DIMENSION PN(12), A(6), XA(6), XG(6)
  COMMON /CE3/ E3
  COMMON /CDEGR/ DEGR
  COMMON /CGG0/ CG0
  CALL DATDAY(PN(2), DT)
  CALL MSECSEC(PN(4), T)
  T = T/ESEC
  TR = PN(1) * E3
  NSP = TR
  BZ = (TR - NSP)
  V = E1/ESEC
  SB = PN(5) / V / V / EM
  NB = PN(3) - .1
  CALL STIME(57, SO)
  V = PN(12) - .1
  IF (NB - 1) 3, 1, 3
1 DO = J - 1, 3
  XA(J) = PN(J+4) / EM
2 XG(J-3) = PN(J+7) / V
  CALL AIGAL(SO, T, XG, 2, XA)
  GOTO 2
3 IF (NB - 2) 5, 2, 5
2 DO = J - 1, 3
  XA(J) = PN(J+4) / EM
5 XG(J-3) = PN(J+7) / V
  CALL AIGAL(SO, T, XG, 2, XA)
  RETURN
END
  
```

3.10 Altitude of the AES over the Earth's Surface, the Geographic Latitude and Longitude, the Geocentric Latitude of a Sub-Satellite Point.  
(BLO-GEOGRC, HEIGHT, GCLTIN)

1. Function. Using the known Greenwich coordinates  $x, y, z$ , of the AES, the subprogram GEOGRC determines  $h$ --the altitude of the AES above the surface of the Earth's ellipsoid and,  $\varphi, \lambda$  -- the geographical latitude and longitude of the sub-satellite point; subprogram HEIGHT determines only  $h$ ; subprogram GCLTIN determines  $\varphi_{oc}, \lambda$  the geocentric latitude and longitude of the sub-satellite point. For subprograms HEIGHT and GCLTIN,  $x, y$ , and  $z$  can also be given in the absolute system of coordinates; in this case there is the right ascension of the AES.

2. Structure. Independent subprograms:

GEOGRC, HEIGHT, GCLTIN.  
 Common units: /CAE/2, /CAEI/1, /CCIZ/1, /CPI/3.

3. Access:

CALL GEOGRC (X, HC, ALT, ALN, XNG),  
 CALL HEIGHT (X, HC),  
 CALL GCLTIN (X, ALTC, ALN).

4. Raw data: Array  $X_3$ , which contains the values of  $x, y, z$  /3/ (for GEOGRC only in the Greenwich frame of axes).

5. Results:

HC--the altitude of the AES above the surface of the Earth's ellipsoid; ALT, ALN--the geographic altitude and longitude of the sub-satellite point; array  $XNG_3$ , which contains the cosines of the peripheral standard which is directed towards the Earth's ellipsoid; ALTC--the geocentric latitude of the sub-satellite point.

6. Use of the area COMMON.

In subprogram HEIGHT constants are used from the units COMMON/CAE/2, /CAEI/1, /CCIZ/1, /CPI/3 (Nos. 11, 12 and 13 of Table 2.1 and No. 1 of Table 2.3), in subprogram HEIGHT constants are used from units: /CAE/2, /CAEI/1 and in subprogram GCLTIN from unit /CPI/3.

7. Algorithm

$$h = r - a_e + a_e \alpha z^2 / r^2,$$

$$\varphi = \arctg \{ z / r_1 (1 - \alpha)^2 \}, \quad -\pi/2 < \varphi < \pi/2,$$

$$\lambda = \text{Arct} \rho (y/x), \quad 0 < \lambda < 2\pi,$$

where  $r = (x^2 + y^2 + z^2)^{1/2}$ ,  $r_1 = (x^2 + y^2)^{1/2}$ ,

$\alpha_e, \alpha$  - is the semimajor axis and the contraction of the Earth's whole ellipsoid.

$\varphi_{oc} = \arccos(x/r_1)$  - the geocentric latitude.

$$x_N^0 = x(1-\alpha)^2/r_2, \quad y_N^0 = y(1-\alpha)^2/r_2, \quad z_N^0 = z/r_2,$$

where  $x_N^0, y_N^0, z_N^0$  the cosines of the peripheral standards directing towards the Earth's ellipsoid,

$$r_2 = \{r_1^2(1-\alpha)^4 + z^2\}^{1/2}.$$

### 8. Texts.

```

SUBROUTINE GEOTRC(X,HC,ALT,ALN,XE)
COMMON/CCCLZ/CLZ
COMMON/CAE/AE,AL
COMMON/CPI/PI,PID2,PI2
COMMON /CAEL/AEL
DIMENSION U(2),CU(2),X(6),XE(3)
R12=X(1)*X(1)+X(2)*X(2)
W=X(3)*X(3)
R2=R12+W
HC=SQRT(R2)-AE+AEL+W/R2
CU(1)=X(1)
CU(2)=CLZ*SQRT(R12)
W=SQRT(W+CU(2)*CU(2))
DO 1 J=1,2
  IF(CU(J))2,3,2
3 U(J)=SIGN(PID2,X(J+1))
  GOTO 4
2 U(J)=ATAN(X(J+1)/CU(J))
4 XE(J)=X(J)*CLZ/W
1 CONTINUE
XE(3)=X(3)/W
ALT=U(2)
ALN=U(1)
IF(CU(1))5,6,6
5 ALN=ALN*PI
6 IF(ALN)7,8,8
7 ALN=ALN+PI2
8 RETURN
END

```

```

SUBROUTINE HEIGHT(V,HC)
DIMENSION V(6)
COMMON /CAE/AE,AL
COMMON/CAEL/AEL
W=V(3)*V(3)
R2=W+V(1)*V(1)+V(2)*V(2)
HC=SQRT(R2)-AE+AEL+W/R2
RETURN
END

```

```

SUBROUTINE GOITLN(V,ALT,ALN)
COMMON /CPI/PI,PID2,PI2
DIMENSION V(3)
R1=SQRT(V(1)*V(1)+V(2)*V(2))
ALT=PID2
IF(R1)1,1,2
2 ALT=ATAN(V(3)/R1)
1 ALN=ATAN2(V(2),V(1))
IF(ALN)3,4,4
3 ALN=ALN+PI2
4 RETURN
END

```

CHAPTER 4  
POSITION OF THE MOON AND THE SUN  
(INDEX C)

36

4.1 Position of the Moon  
(COL-SELENA)

1. Function: The subprogram determines the position of the moon in the absolute geographical system of coordinates for the moment of time which is given by the relative Julian date and Moscow time in seconds.
2. Structure. Subprogram SELENA.  
Common units: /CRE/1, /CSDAY/1, /CT3/1, /CDSJS/1, /CPL/3.
3. Access: CALL SELENA (RJD, T, XS, RS).
4. Raw data: RJD-relative Julian date;  
T- Moscow time in seconds.
5. Results: Array XS<sub>3</sub>, which contains the direction cosines of the radius vector of the Moon in the absolute system of coordinates; RS--the module of the Moon's radius vector.
6. Use of the area COMMON. Constants are used from the units:  
/CRE/1, /CSDAY/1, /CT3/1, /CDSJS/1, /CPL/3 (No. 9 of Table 2.1, Nos. 1,2,4, of Table 2.2, No. 1 of Table 2.3).
7. Algorithm:

$$X_c^{\circ} = \cos \alpha_c \cos \delta_c = \cos \beta_{\varepsilon} \cos \lambda_{\varepsilon} ,$$

$$Y_c^{\circ} = \sin \alpha_c \cos \delta_c = \cos \beta_{\varepsilon} \sin \lambda_{\varepsilon} \cos \varepsilon - \sin \beta_{\varepsilon} \sin \varepsilon ,$$

$$Z_c^{\circ} = \sin \delta_c = \cos \beta_{\varepsilon} \sin \lambda_{\varepsilon} \sin \varepsilon + \sin \beta_{\varepsilon} \cos \varepsilon .$$

In accordance with Brown's theory of approximation, presented in [7], which guarantees a prediction of the Moon's position with an accuracy to 30", the following correlations are used:

$$\varepsilon = 23^{\circ} 27' 08",26 - 46",845 T - 0",0059 T^2 + 0",00181 T^3;$$

$$l = 296^{\circ} 06' 16",59 + 477198^{\circ} 50' 56",79 T + 33",09 T^2 + 0",0518 T^3;$$

$$l' = 358^{\circ} 28' 33",04 + 35999^{\circ} 02' 59",10 T - 0",54 T^2 - 0",0120 T^3;$$

$$F = 11^{\circ} 15' 03",20 + 483202^{\circ} 01' 30",54 T - 11",56 T^2 - 0",0012 T^3;$$

$$\begin{aligned}
 D &= 350^{\circ}44'14",95 + 445267^{\circ}06'51",18T - 5",17T^2 + 0.0068T^3; \\
 \lambda_{\epsilon} &= 270^{\circ}26'02",99 + 481267^{\circ}52'59",31T - 4",08T^2 + 0.0068T^3 + \\
 &+ 22639",58 \sin \ell - 4586",438 \sin(\ell - 2D) + 2369",899 \sin 2D + \\
 &+ 769",021 \sin 2\ell - 668",944 \sin \ell' - 411",614 \sin 2F - \\
 &- 211",658 \sin(2\ell - 2D) - 206",219 \sin(\ell + \ell' - 2D) + 191,954 \sin(\ell + 2D) \\
 &- 165",351 \sin(\ell' - 2D) + 147",878 \sin(\ell - \ell') - 124,785 \sin D - \\
 &- 109",804 \sin(\ell + \ell') - 55",174 \sin(2F - 2D) - 45",100 \sin(\ell + 2F) + \\
 &+ 39",532 \sin(\ell - 2F) - 38",428 \sin(\ell - 4D) + 36",124 \sin 3\ell - \\
 &- 30",773 \sin(2\ell - 4D) - 28",511 \sin(\ell - \ell' - 2D) - 24",451 \sin(\ell' + 2D); \\
 \beta_{\epsilon} &= 18461",480 \sin F + 1010",18 \sin(\ell + F) - 999",695 \sin(F - \ell) - \\
 &- 623",658 \sin(F - 2D) + 199",485 \sin(F + 2D - \ell) - 166",577 \sin(\ell + F - 2D) \\
 &+ 117",262 \sin(F + 2D) + 61",913 \sin(2\ell + F) - 33",359 \sin(F - 2D - \ell) -
 \end{aligned}$$

$$\begin{aligned}
 \pi_{\epsilon} &= 3427",7 + 186",5398 \cos \ell + 34",3117 \cos(\ell - 2D) + 28,2333 \cos 2D \\
 &+ 10",1657 \cos 2\ell + 3",0861 \cos(\ell + 2D) + 1",9202 \cos(\ell' - 2D) + \\
 &+ 1",4455 \cos(\ell + \ell' - 2D) + 1",1542 \cos(\ell - \ell') - 0",9752 \cos D - \\
 &- 0",9502 \cos(\ell + \ell') - 0",7136 \cos(\ell - 2F) + 0",6215 \cos 3\ell + \\
 &+ 0",6008 \cos(\ell - 4D);
 \end{aligned}$$

$$Z_{\epsilon} = 206264",81 R_{\oplus} / \pi_{\epsilon},$$

where  $R_{\oplus}$  is the equatorial radius of the Earth.

- T - RJD/36525,
- RJD - relative Julian date in days,
- T - the same interval of time in Julian centuries
- $\ell$  - the median anomaly of the Moon,
- $\ell'$  - the median anomaly of the Sun,
- F - the median argument of the Moon's latitude,
- D - the difference between the median longitudes of the Moon and Sun,
- $\ell$  - the Moon's longitude,
- $\beta_{\epsilon}$  - the Moon's declination,
- $\pi_{\epsilon}$  - the Moon's parallax

8. Text.

```

SUBROUTINE SELENA(DT,T,S,R)
DIMENSION S(3),A(32),B(17)
COMMON /CT3/T3
COMMON/CPI/PI,PID2,PI2
COMMON/CDSJS/DSJS
COMMON/CSDAV/SDAV
COMMON/CRE/RE
TR=DT/DSJS*(T-T3)/SDAV/DSJS
B(1)=((.877512763E-8*TR-.286040072E-7)*TR
+ .227110969E-3)*TR+.4093197553
W=B325.691*TR
N=W/PI2
W=W-4*PI2
A(4)=((.251133487E-6*TR+.160424847E-3)*TR
+ .20556971E-3)*TR+.168000347*W
W=028.301*TR
N=W/PI2
W=W-4*PI2
A(27)=((- .581776417E-7*TR-.261799388E-5)*TR
+ .045870201E-3)*TR+.6.256583776*W
W=B433.466*TR
N=W/PI2
W=W-4*PI2
A(17)=((- .581776417E-8*TR-.560444612E-4)*TR
+ .295097557E-3)*TR+.1963650549*W
W=7771.377*TR
N=W/PI2
W=W-4*PI2
A(2)=((.324673303E-7*TR-.250648673E-4)*TR
+ .1257089207E-3)*TR+.6.121523944*W
A(3)=2.*A(2)
A(4)=2.*A(4)
DO 1 J=4,7
1 A(J+2)=A(J)-A(3)
DO 2 J=4,6,2
2 A(J+7)=A(J)+A(27)
2 A(J+5)=A(J)-A(27)
DO 3 J=3,9
L=2*(J-1)+14
A(L)=A(17)*A(J)
3 A(L+1)=A(17)-A(J)
A(15)=A(27)-A(3)
A(11)=3*A(4)
A(24)=2*A(17)
A(25)=A(24)-A(3)
A(26)=A(4)+A(24)
A(10)=A(4)-A(24)
A(28)=A(15)+A(17)
A(29)=A(6)+A(17)
A(16)=A(4)+A(3)
A(30)=A(16)-A(4)
A(31)=A(27)+A(3)

```



```

A(32)=A(21)-A(3)
DO* J=1,10
4 B(J+1)=COS(A(J))
DCP: J=1,32
5 A(J)=SIN(A(J))
B(1)=-.29127606E-5*B(0)+.301311703E-5*B(2)
-.345963043E-5*B(11)+.46066998E-5*B(12)+.472760302E-5*B(13)
+.559571021E-5*B(14)+.700798174E-5*B(15)+.920092231E-5*B(16)
+.14061635E-4*B(17)+.492847044E-4*B(18)+.170878001E-5*B(19)
+.146347816E-5*B(7)+.904370671E-5*B(8)+.168977170E-5
H=0.99,704*TR
H=H/212
H=H-4*H/2
B(1)=-.112241793E-3*A(21)+.136222229E-3*A(16)
-.112241793E-3*A(19)+.175134694E-3*A(11)+.106300201E-3*A(8)
+.112241793E-3*A(20)+.21865597E-3*A(26)+.2674911E-3*A(25)
+.112241793E-3*A(11)+.607974752E-3*A(2)+.714932776E-3*A(12)
+.112241793E-3*A(12)+.930619253E-3*A(18)+.109077792E-3*A(13)
+.112241793E-3*A(17)+.199556099E-2*A(24)+.324312293E-2*A(27)
+.112241793E-3*A(15)+.114895044E-1*A(3)+.222356780E-1*A(6)
+.112241793E-3*A(4)+.11320673303E-7*TR+.197402682E-4*TR
+.1460643247E-3*TR+.4.7199665708*H

B(2)=-.163436534E-3*A(28)+.15399137E-3*A(23)
-.161725445E-3*A(32)+.300162694E-3*A(22)+.568502219E-3*A(18)
+.667575245E-3*A(29)+.967130572E-3*A(30)+.302357931E-2*A(19)
+.444665013E-2*A(21)+.489749084E-7*A(20)+.805037808E-1*A(17)
DCP: J=1,2
B(J+1)=COS(B(J))
H(J)=SIN(B(J))
S(0)=B(6)+*B(3)
S(2)=S(1)+B(1)+B(5)+B(2)
S(2)=S(1)+*B(1)+B(5)+B(2)
S(1)=B(4)+*B(5)
K=H/212
RETURN
END

```

4.2 Position of the Sun  
(C02-SUN)

1. Function. The subprogram determines the position of the sun in the absolute geographic frame of axes for the moment of time, which is given as the RJD and as Moscow time in seconds.

2. Structure. Subprogram SUN.

Common units: /CAED/1, /CSDAY/1, /CT3/1, /CDSJS/1, /CP1/3, /BIECL/2

3. Access: CALL SUN (RJD, T, RS, AS, BS, XS).

\$. Raw data: RJD-relative Julian date;  
T-Moscow time in seconds

5. Results: RS-the module of the Sun's radius vector; AS, BS-  
the corresponding right ascension and declination of the Sun; array 40  
XS<sub>3</sub>-directing cosines of the Sun's radius-vector.

6. Use of the area COMMON. Constants are used from the units:  
/CAED/1, /CSDAY/1, /CT3/1, /CDSJS/1, /CP1/3 (No. 1 of Table 2.1, Nos. 1, 2,  
4, of Table 2.2, No. 1 of Table 2.3). Into the unit COMMON/BIECL/2 are  
dispatched the values  $\cos \varepsilon$ ,  $\sin \varepsilon$ , which are defined below.

$$\begin{aligned}\Omega &= 2;9^{\circ} 10' 59''.79 - 1934^{\circ} 08' 31''.23T + 7''.48T^2 + 0''.008T^3; \\ \varepsilon &= 23^{\circ} 27' 08''.26 - 46''.845T - 0''.0059T^2 + 0''.00181T^3 + 9''.21 \cos \Omega; \\ e_{\odot} &= 0,01675104 - 0,0000418T - 0,000000126T^2,\end{aligned}$$

#### 7. Algorithm

$$\begin{aligned}\alpha_{\odot} &= \text{Arctg}(\sin \lambda_{\odot} \cos \varepsilon / \cos \lambda_{\odot}) (0,061164 \cdot 15 \Delta \psi)^{\circ} - 20'',496; \\ \delta_{\odot} &= \text{arctg}(\sin \lambda_{\odot} \sin \varepsilon / (\cos^2 \lambda_{\odot} + \sin^2 \lambda_{\odot} \cos^2 \varepsilon)^{1/2}) - 20'',496 \sin \varepsilon \cos \alpha_{\odot}; \\ \lambda_{\odot} &= \bar{\lambda} + 2e_{\odot} \sin(\bar{\lambda} - \bar{\pi}) + 5/4 e_{\odot}^2 \sin 2(\bar{\lambda} - \bar{\pi}); \\ r_{\odot} &= a_{\odot} \{1 - e_{\odot} \cos M_{\odot} + e_{\odot}^2 (1 - \cos 2M_{\odot})/2\}; \\ \bar{\pi} &= 281^{\circ} 13' 15'' + 6189'',03T + 1'',63T^2 + 0'',12T^3; \\ \Delta \psi &= -17,23 \sin \Omega; \quad a_{\odot} = 1,00000023 \text{ a.e.}; \quad 1 \text{ a.e.} = 149600000 \text{ km} \\ M &= \bar{\lambda} - \bar{\pi} \quad \bar{\lambda} = 279^{\circ} 41' 48'',04 + 129602768'',13T + 1'',089T^2\end{aligned}$$

where T=RJD/36525

RJD-relative Julian date in days,

T-the same interval of time in Julian centuries,

$$X_{\odot}^{\circ} = \cos \alpha_{\odot} \cos \delta_{\odot},$$

$$Y_{\odot}^{\circ} = \sin \alpha_{\odot} \cos \delta_{\odot},$$

$$Z_{\odot}^{\circ} = \sin \delta_{\odot}.$$

8. Text

```
S. SPONTANEOUS SUN(DT,T,RS,AS,BS,XS)
DIMENSION AS(3)
COMMON /CT3/T3
COMMON /CPI/P1,P12,P12
COMMON /CA10/CA10
COMMON /CDSJS/DSJS
COMMON /CSDAV/SDAV
COMMON /CEGL/CEGL,SEP
T1=DT/PSJS+(T-T3)/SDAV/DSJS
PR11,DS1775417E-7*T1+.7902465E-5+1
+.130852842E-11*T1+.4.90822946S
T1=25.33*T1
T1=DT/PSJS
T1=DT/PSJS
AL=1.00700000E-5*T1+.1051134E-2)*T1+4,881627935+W
T1=25.33*T1
T1=DT/PSJS
Q1=1.58700000E-7*T1+.362640634E-4)*T1
+.130852842E-11*T1+.4.90822946S
ES=1.00700000E-5*T1+.1051134E-2)*T1+.0167210E
AL=AL-P
ES=ES-P
AL=AL-2.0E-5*IN(AM)+1.25*ESK*SQ(2*AM)
SQ=1.25*ES*SQ(2*AM)
EP=1.00700000E-5*T1+.1051134E-2)*T1+.0167210E
+.227110909E-3)*T1+.4465134E-4)*T1+.009319755S
CL=EP*(AL)
SL=EP*(AL)
CE=EP*(EP)
SE=EP*(EP)
IF(SL*SEP
IF(CE)3,2
7 AS=SIGN(CE,AM)
GO TO 8
8 AS=ATAN(1/CL)
IF(CE)6,6,2
6 AS=PI+AS
5 IF(AS)12,12,11
10 AS=PI2-AS
12 AS=AC-SQ(1.993674121E-4
RESORT(CE*CL+PI*W)
AL=SL*SEP
IF(W)7,8,7
7 BS=SIGN(P12,P1)
```

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```
      GO TO 1
      BS=ATAN(1/1)
      BS=BS-CFP*COB(AE)*.993674121E-4
1     RS=1.-BS*COB(AE)+ESK*(1.-COB(2.*AE))/2.
      AS=(RS*.23E-4*BS)*AE
      XS(3)=SIN(AS)
      XS(2)=COS(AS)
      XS(1)=COS(AS)*XS(2)
      XS(2)=SIN(AS)*XS(2)
      RETURN
      END
```

CHAPTER 5  
MODELS OF THE EARTH'S ATMOSPHERE  
(INDEX D)

/42

5.1 The Standard Five-Layer Model of the  
Earth's Atmosphere  
(DCL-RO)

1. Function: Subprogram RO calculates values for the density of the Earth's atmosphere  $\rho$  at the point given by the altitude above the Earth's surface.

2. Structure. Subprogram RO.  
Common units: /CHA/20.

3. Access: RO (HC<sub>1</sub>P).

4. Raw data: HC-altitude above the Earth's surface.

5. Results: P-the atmospheric density.

6. Use of the area COMMON. Constants are used from the unit /CHA/20 (Table 2.4).

7. Algorithm

$$\rho = A_i \exp(k_{1i}(h-h_i)^2 - k_{2i}(h-h_i)),$$

where  $h$  is the altitude over the Earth's surface,  $A_i, k_{1i}, k_{2i}$  are the coefficients depending on the altitude  $h$  (Table 5.1).

TABLE 5.1 Values of the Coefficients  $A_i, k_{1i}, k_{2i}$ .

$i$	$h_i \leq h < h_{i+1} (M)$	$A_i (\text{kg} \cdot \text{m}^{-3})$	$k_{1i} (\text{m}^{-2})$	$k_{2i} (\text{m}^{-1})$
1	$100000 \leq h < 150000$	$0,4141 \cdot 10^{-7}$	$0,1469 \cdot 10^{-8}$	$0,1787 \cdot 10^{-3}$
2	$150000 \leq h < 300000$	$0,2173 \cdot 10^{-9}$	$0,8004 \cdot 10^{-10}$	$0,3734 \cdot 10^{-4}$
3	$300000 \leq h < 600000$	$0,4861 \cdot 10^{-11}$	$0,7111 \cdot 10^{-11}$	$0,1547 \cdot 10^{-4}$
4	$600000 \leq h < 900000$	$0,8904 \cdot 10^{-13}$	$0,1831 \cdot 10^{-11}$	$0,9275 \cdot 10^{-5}$
5	$900000 \leq h$	$0,6497 \cdot 10^{-14}$	0	$0,9540 \cdot 10^{-5}$

8. Text.

```
SUBROUTINE DENS(D)
COMMON/OKOA/A(5),AA(5),Q1(5),Q2(5)
I=1
DO2J=2,5
IF(OC-RA(J))3,1,1
1 I=I+1
2 CONTINUE
3 J=OC-RA(I)
P=AA(I)*EXP((Q1(I)*W-Q2(I))*W)
RETURN
```

5.2. Model of the Earth's Atmosphere, with a  
Calculation for the Influence of Solar  
Radio Emission at Wavelength 10.7 cm  
of Geomagnetic Disturbance, Daily and  
Semiannual Effects  
(DO2-VKMA, DENS)<sup>1</sup>

1. Function. According to the given positions of the point and Sun, and according to the values of the indexes  $F_{10.7}$  (the intensity of solar radio emission at wave 10.7 cm) and  $a_p$  (three hour indexes of the geomagnetic disturbance), the subprogram DENS determines the atmospheric density at the given moment of time.

Coefficients of the model of the atmosphere are chosen with the help of subprogram VKMA depending on  $F_0$ , the mean level of solar activity.

2. Structure. The packet of subprograms:

VKMA, DENS.  
Peripheral devices: printer  
Common units: /AKOEF/50, /SYEAR/38.

3. Access to VKMA: CALL VKMA (F).

Raw data: F-the mean value of solar activity.  
Possible values of F: 75, 100, 125, 150. If F differs from the indicated values, then a stop should occur, whereupon the printer reads: "F incorrectly given."

Results: Into the unit COMMON/OKOEF/A(50), are sent values of coefficients of the model according to Table 5.2, and into the unit COMMON/SYEAR/F<sub>38</sub> is the set of numerical corrections on the semiannual effect according to Table 5.3.

<sup>1</sup> Author of the subprogram M.I. Voyskovskiy.

4. Access to DENS:

CALL DENS (HC,X,Y,Z,SUN,AP,F10<sub>7</sub>,D,I,RO).

Raw data: HC-altitude above the Earth's surface in km; /44  
X,Y,Z,-directing cosines of the radius-vector in the  
absolute system of coordinates; the array SUN, which  
contains the values  $\alpha_0, \delta_0$  (right ascension and declina-  
tion of the sun in radians);

AP-the value  $\alpha_p$  at the moment of time  $t - \Delta\tau_p$ , where  
t is Moscow time (for isolating the calculation of the  
influence of geomagnetic disturbance it is sufficient  
to let  $AP < 0.5$ );

F10<sub>7</sub>-the  $F_{10.7}$ , at the moment of time  $t - \Delta\tau_f$  where  
t is Moscow time (for isolating the calculation of the  
influence of solar activity it is sufficient to let  $F_{10.7}$   
< 0.5);

D-the date and Moscow time in the form of the number  
of days from the beginning of the year (for isolating the  
calculation of the semiannual effect it is sufficient  
to let  $D < 0$ );

I-the parameter controlling the calculation of the  
daily effect (DE):

if  $I < 0$ , then DE is considered memberless with the  
coefficient  $C_6$ ;

if  $I = 0$ , then DE is not considered;

if  $I > 0$ , then DE is considered in its entirety.

Results: Array RO<sub>6</sub>, which contains values of five factors,  
each of which takes into consideration its effect in the modes  
of atmospheric density (see p. 6) and the value of the density:

$$RO(1) = k_4,$$

$$RO(2) = k_1, RO(3) = k_2, RO(4) = k_3, RO(5) = \rho_H, RO(6) = \rho_H k_1 k_2 k_3 k_4.$$

5. Use of the area COMMON:

In subprogram DENS coefficients of the atmosphere model and  
corrections for semiannual effects, whose values are assigned by  
a preliminary accessing to subprogram VKMA, are used from the com-  
mon units /QKOE/50 and /SYEAP/38.

6. Algorithm

The density p is calculated according to the formula:

$$p = \rho_H \cdot k_1 k_2 k_3 k_4, \quad \text{where } \rho_H \text{ is the nightly vertical } /45$$

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cross section of the atmospheric density.

$k_1$  - is the factor which allows for the influence of measurements of the intensity of solar radio emission  $F$  at wavelength 10.7 cm relative to certain mean levels of solar radio emission.

$k_2$  - the factor which allows for daily effects in the dispersion of the atmosphere,

$k_3$  - correction for the semiannual effect.

$k_4$  - the factor which allows for the correlation between changes in the atmospheric density and geomagnetic disturbances.

$$\hat{h} = \exp(a_1 - \hat{a}_2 (h - \hat{a}_3)^{1/2});$$

$$k_1 = 1 + (b_1 + b_2 h)(F - F_0)/F_0;$$

$$k_2 = 1 + (c_1 + c_2 h + c_3 \exp(-(h + c_4)^2/c_5^2))(\cos^{m_1} \psi_1/2 + c_6 \cos^{m_2} \psi_2/2);$$

$$k_3 = 1 + (A_1 + A_2 h)A(d); \quad k_4 = 1 + (e_1 + e_2 h) \ln(a_p/\hat{a}_p);$$

where

$$\cos \psi_1 = Z^c \sin \delta_0 + \cos \delta_0 (X^c \cos \gamma_1 + Y^c \sin \gamma_1),$$

$$\cos \psi_2 = -Z^c \sin \delta_0 + \cos \delta_0 (X^c \cos \gamma_2 + Y^c \sin \gamma_2);$$

$$\gamma_1 = \alpha_0 + \varphi_1, \quad \gamma_2 = \alpha_0 + \varphi_2,$$

$h$  - the altitude above the Earth's surface.

$X^c, Y^c, Z^c$  - the directing cosines of the radius-vector of a point in the absolute system of coordinates,

$\alpha_0, \delta_0$  - the right ascension and declination of the Sun.

$d$  - the date and time in the form of the number of days, counted from the beginning of the year,

$A(d)$  - correction for the semiannual effect (the volumes of are shown in Table 5.3, with 10 day increments of time, the intermediate moments of time  $A(d)$  exists as a linear interpolation),

$F$  - the intensity of solar radio emission at 10.7 cm,

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$a_p$  - the three hour index of geomagnetic disturbance.

The values  $F$  and  $a_p$  should be at the moment of time, respectively:  $t_F = t - \Delta\tau_F$  and  $t_{a_p} = t - \Delta\tau_{a_p}$  where  $t$  is Moscow time,  $\Delta\tau_F$  and  $\Delta\tau_{a_p}$  are the "time lags" of changes in the density of the atmosphere which correlate to a



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corresponding change of the quantities  $F$  and  $a_p$ . The values

$\Delta\tau_{a_p}$  and  $\Delta\tau_F$  are shown in Table 5.2, and also are  $\Delta t_F$ , and,  $\Delta t_{a_p}$ , the duration of intervals in the course of which the quantities  $F$  and  $a_p$  are maintained by the constants and tabular values which are equal to them.

In table 5.2 are also the coefficients of the model:  $a_1, a_2, a_3, b_1, b_2, \dots, \bar{a}_p$ , which depend on the mean level of solar radio emission  $F_0$ .

Table 5.2 Values of coefficients of the atmospheric model, depending on the mean level of solar radio emission  $F_0 \cdot 10^{22} \text{ W.m}^{-2}\text{Hz}^{-1}$  (units COMMON/QKOEf/Q50)).

i	Designations	Q(i)	Q(i)	Q(i)	Q(i)
I	$F_0$	75	100	125	150
2	$a_1$	-14,030	-15,095	-17,028	-16,072
3	$a_2$	0,9108	0,8229	0,7198	0,7155
4	$a_3$	59,77	68,92	93,36	70,33
5	$b_1$	-0,630	-0,750	-0,710	-0,765
6	$b_2$	0,00506	0,00560	0,00562	0,00571
7	$e_1$	0,130	0,172	-0,274	-0,247
8	$e_2$	0,00014	0,00217	0,00257	0,00199
9	$c_3$	3,733	3,784	4,048	4,698
10	$c_4$	-507,95	-566,11	-632,63	-707,58
11	$c_5$	189,85	200,97	230,76	278,35
12	$c_6$	-0,041	-0,047	-0,038	-0,012
13	$m_1$	4,2	4,1	4,4	5,2
14	$m_2$	6,0	6,0	5,9	5,9
15	$\varphi_1$	$37^\circ,4$	$34^\circ,2$	$34^\circ,5$	$33^\circ,8$
16	$\varphi_2$	$325^\circ,9$	$318^\circ,0$	$308^\circ,0$	$322^\circ,2$
17	$A_1$	-0,602	-0,526	-0,513	-0,607
18	$A_2$	0,00669	0,00636	0,00631	0,00670
19	$e_1$	-0,132	-0,130	-0,128	-0,115
20	$e_2$	0,00108	0,00104	0,00095	0,00089
21	$\Delta\tau_F$	$39^h$	$39^h$	$39^h$	$39^h$
22	$\Delta\tau_{a_p}$	$10^h,5$	$10^h,5$	$10^h,5$	$10^h,5$
23	$\delta t_F$	$4^h$	$4^h$	$4^h$	$4^h$
24	$\delta t_{a_p}$	$1^h$	$1^h$	$1^h$	$1^h$
25	$\bar{a}_p$	2	2	3	4

Table 5.3 Corrections for the semiannual effect in dependence on, d and the number of days since the beginning of the year (unit COMMON/SYEAR/P(38)).

$i$	$d$	$P(i) = A(d)$	$i$	$d$	$P(i) = A(d)$
1	0	-0,067	20	190	-0,172
2	10	-0,083	21	200	-0,180
3	20	-0,094	22	210	-0,183
4	30	-0,088	23	220	-0,179
5	40	-0,083	24	230	-0,163
6	50	-0,065	25	240	-0,133
7	60	0,039	26	250	-0,085
8	70	0,090	27	260	-0,018
9	80	0,123	28	270	0,059
10	90	0,133	29	280	0,123
11	100	0,126	30	290	0,161
12	110	0,099	31	300	0,170
13	120	0,059	32	310	0,156
14	130	0,017	33	320	0,119
15	140	-0,027	34	330	0,073
16	150	-0,065	35	340	0,027
17	160	-0,103	36	350	-0,023
18	170	-0,136	37	360	-0,055
19	180	-0,156	38	370	-0,078

7. Text.

```

SUBROUTINE VRMA (F)
COMMON/GRDEF/P(50)/SYEAR/P(38)
DIMENSION R(100),S(38)
DATA S/-.067,-.083,-.094,-.088,-.083,-.065,.039,.090,.123,
      .133,.126,.099,.059,.017,-.027,-.065,-.103,-.136,-.156,
      -.172,-.180,-.183,-.179,-.163,-.133,-.085,-.018,.059,.123,
      .161,.170,.156,.119,.073,.027,-.023,-.055,-.078/
DATA R/75,-14.000,5196,50.77,63,.00506,130,.00014,3.733,
      -207.45,130.13,-.341,4.216,.31,4.325,9,-.602,.00564,
      -.132,.00103,29.12,5.4,1.2,100,-15.092,.8299,08.92,
  
```

```

100217,3.784,-566,11,200.97,-.047,4.1,
100218,1.514,-.526,.00636,-.13,.00104,39.,10.5,4.,1.,2.,
5 100219,17.028,7198.93,36,-.715,00562,274,700257,4.048,
6 -532.63,230.76,-.035,4.4,5.9,34.5,308.,-.513,.00631,
7 -.128,.00095,39.,10.5,4.,1.,3.,150.,-16.074,.7155,70.33,
8 -.765,.00571,-.247,.00199,4.698,-707.58,278.35,-.012,5.2,
9 5.9,33.8,322.2,-.607,.0067,-.115,.00089,39.,10.5,4.,1.,4.7
1006 J=1,58
1 P(J)=S(J)
1003 I=1,100,25.
1 IF(ABS(R(I)-F)-.1) 2,3,3
3 CONTINUE
PRINT 4
STOP
FORMAT ('HEBEPHO 3AAAHO F')
2 L=I+24
1005 K=I,L
H=K-I+1
5 Q(N)=R(K)
RETURN
END

```

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```

SUBROUTINE DENS(H,X,Y,Z,SUN,AP,F107,D,ISUT,RO)
DIMENSION RO(6),V(5),SUN(2)
COMMON /RKOEF/R(30)/SVEAR/P(38)
C6=0.
PI=3.1415926/180.
1007 J=1,4
7 RO(J)=1.
RO(5)=EXP(Q(2)-R(3)*SQRT(H-R(4)))
IF (AP=.5) 2,2,1
1 RO(1)=1.+(R(10)+R(20)*H)*ALOG (AP/R(25))
2 IF (F107-.5) 3,3,4
4 RO(2)=1.+(R(5)+R(6)*H)*(-1+F107/R(1))
3 IF (D) 5,6,6
6 I=INT(D/10.)+1
RO(3)=AMOD (D,10.)/10.
RO(3)=P(I)+(P(I+1)-P(I))*H(3)
RO(3)=1.+RO(3)*(R(17)+R(18)*H)
5 ASSIGN 11 TO M
IF (ISUT) 8,9,10
10 ASSIGN 12 TO M
5 V(1)=SIN(SUN(2))
V(2)=COS(SUN(2))
RO(4)=R(7)+R(8)*H+R(9)*EXP(-((H+R(10))/R(11))*C6)
V(4)=SUN(1)+R(15)*PI
V(3)=SIN(V(4))
V(4)=COS(V(4))
V(5)=Z+V(1)+V(2)*(X+V(4)+Y+V(3))
V(5)=((1.+V(5))/2.)**(R(13)/2.)
GO TO 11,(11,12)
12 V(4)=SUN(1)+R(16)*PI
V(3)=SIN(V(4))
V(4)=COS(V(4))
C6=-Z+V(1)+V(2)*(X+V(4)+Y+V(3))
C6=((1.+C6)/2.)**(R(14)/2.)
C6=R(12)*C6
11 RO(4)=1.+RO(4)*(V(5)+C6)
9 RO(6)=RO(5)*RO(4)*RO(3)*RO(2)*RO(1)
RETURN
END

```

5.3 Yakkia-72 Model of the Earth's Atmosphere  
(DO3-ADEN, AMBAR, GRAV, TLOCAL)<sup>1</sup>

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1. Function. According to the given location of a point, of the Sun, the values of  $F_{107}$ ,  $k_p$  at a given moment in time determine the temperature at a given point, the exospheric temperature, the density of the atmosphere, the number of molecules of nitrogen, oxygen, argon, helium and hydrogen in a single volume, and also the mean molecular weight of constituents of the atmosphere (presuming that it consists only of the elements listed above).

2. Structure. Subprogram ADEN.  
Internal access: AMBAR, GRAV, TLOCAL.

3. Access:  
CALL ADEN (AMJD, SUN, SAT, GEO, TEMP, ALION, AMHW, RHO).

4. Raw data:  
AMJD-date & time in modified Julian days and fractions of days;

SUN-the array which consists of two elements:  
SUN(1)-the direct ascension of the Sun in radians,  
SUN(2)-the Sun's declination in radians;  
SAT-the array consisting of three elements:  
SAT(1)-the longitude of a point in radians.  
SAT(2)-geocentric latitude of a point in radians;  
SAT(3)-the altitude of the point in kilometers;  
GEO-an array consisting of three elements:  
GEO(1)-the value of the index  $F_{107}$  (the time lag-1.7 days),  
GEO(2)-the value of the geomagnetic index  $k_p$ ,  $\tau_{k_p}$  /50  
considering  
that  $3^- = 2.667$ ,  $3^+ = 3.333$  and so forth, the time delay  
=0.279 days.

5. Results: TEMP-an array consisting of two elements TEMP (1)--the exospheric temperature over a given point (in Kelvin degrees); TEMP (2)--the temperature at a given point (in Kelvin degrees).

ALION-an array consisting of six elements:  
ALION(1)-common logarithm of the number of nitrogen molecules in  $M^3$ ,  
ALION(2)-common logarithm of the number of oxygen molecules in  $M^3$ ;  
ALION(3)-common logarithm of the number of oxygen atoms in  $M^3$ ;

<sup>1</sup>The subprograms used are from [6] and were tested and modified for a high speed electronic computer BESM-6 by Ye.Ye. Ryazanova.

ALION(4)-common logarithm of the number of argon molecules  
in  $M^3$ ;  
ALION(5)-common logarithm of the number of helium  
molecules in  $M^3$ .  
ALION(6)-common logarithm of the number of hydrogen mole-  
cules in  $M^3$ ;  
AMHW-mean molecular weight;  
RHO-density (in  $Kg/m^3$ ).

6. Due to a lack of space there can be no description of  
the Yakkia-72 atmospheric model or of the texts of subprograms  
which were published in [6].

CHAPTER 6  
ANOMALIES OF THE EARTH'S GRAVITATIONAL FIELD  
(INDEX 7)

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6.1 The Acceleration Vector, Determined  
By the Influence of Anomalies of  
Earth's Gravitational Field  
(EO1-DEG2, DEG3, DEG4)<sup>1</sup>

1. Function. For a point in space fixed by the Greenwich coordinates:  $x, y, z$ , one determines the constituents  $\Delta g_r$ ,  $\Delta g_m$ , and  $\Delta g_l$  of the acceleration vector which is specified by the influence of anomalies of the Earth's gravitational field 1.2 :

$\Delta g_r$  --the radial constituent of vector  $\Delta g$  (project on the radius-vector of a point with a minus sign),  
the meridional constituent (the meridian directed to the north),

$\Delta g_l$  -the projection of  $\Delta g$  on the perpendicular to the plane of the meridian (directed to the east).

Subprogram DEG2 determines the acceleration vector which is determined by the influence only of zonal harmonics of anomalies of the Earth's gravitational field. Subprogram DEG3 determines the acceleration vector, allowing for the influence of zonal, tesseral and sectorial harmonics of the Earth's gravitational field. Subprogram DEG4 determines the acceleration vector allowing for the influence of only the harmonics 22, 30 and 40.

2. Structure. The packet of subprograms:  
DEG2, DEG3, DEG4.

Common units: /RAD/2, /GRZ/1, /BCONGR/546, /CAZZ/4.

3. Access: CALL DEG2 (X, DG, NM),  
CALL DEG3 (XG, DG, NM),  
CALL DEG 4 (XG, DG).

4. Raw data. Array XG<sub>3</sub>, which contains  $x, y, z$ --the Greenwich coordinates of a point;

NM--the number of harmonics considered (NM ≤ 22).

Note. When accessing subprogram DEG<sub>2</sub>, one may use coordinates of a point both in the Greenwich and absolute system of coordinates.

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5. Results. Array DG, which contains the components:

$\Delta g_r, \Delta g_m, \Delta g_l$  of the acceleration vector.

6. Use of the area COMMON:

Before accessing any of the subprograms it is necessary to put the values  $R = (x^2 + y^2 + z^2)^{\frac{1}{2}}$  and  $R_l = (x^2 + y^2)^{\frac{1}{2}}$  into the unit COMMON/RAD/R, R<sub>l</sub>.

<sup>1</sup>Author--Ye.Ye. Ryazanova.

In the unit COMMON/CRZ/RZ the value RZ should be fixed.  
(No. 10 of Table 2.1).

In order to secure the work of subprograms DEG2 and DEG3, the values of coefficients of the resolution ratio of the Earth's gravitational field (according to Table 2.5) by means of a preliminary accessing of subprogram CONGR(AO2). In subprogram DEG4 an additional variant of coefficient values of the Earth's gravitational field is used from unit COMMON/CAZZ/4 (No. 4 of Table 2.1).

7. Algorithm.

a) calculation of zonal harmonics

$$\Delta g_r = 1/r \sum_{n=0}^{n_{max}} (R/r)^{n+1} (n+1) \alpha_{n0} P_{n0}(\sin \psi);$$

$$\Delta g_m = 1/r \sum_{n=0}^{n_{max}} (R/r)^{n+1} \alpha_{n0} P_{n1}(\sin \psi); \quad \Delta g_l = 0.$$

b) calculation of zonal, tesseral, and sectoral harmonics:

$$\Delta g_r = 1/r \sum_{n=2}^{n_{max}} (R/r)^{n+1} (n+1) \sum_{m=0}^n (\alpha_{nm} \cos mL + \beta_{nm} \sin mL) P_{nm}(\sin \psi);$$

$$\Delta g_m = 1/r \sum_{n=2}^{n_{max}} (R/r)^{n+1} \sum_{m=0}^n (\alpha_{nm} \cos mL + \beta_{nm} \sin mL) (P_{n,m}(\sin \psi) - \int_0^\psi P_{nm}(\sin \psi) d\psi);$$

$$\Delta g_l = 1/r \sum_{n=2}^{n_{max}} (R/r)^{n+1} \sum_{m=0}^n (-\alpha_{nm} \sin mL + \beta_{nm} \cos mL) m P_{nm}(\sin \psi);$$

x, y, z - the Greenwich coordinates of a point,

$$r = (x^2 + y^2 + z^2)^{1/2}, \quad r_1 = (x^2 + y^2)^{1/2}, \quad R = 6371 \text{ km},$$

$\psi, L$  - the geocentric latitude and longitude of a point,

$$\sin L = y/r_1, \quad \cos L = x/r_1, \quad \sin \psi = z/r, \quad \cos \psi = r_1/r,$$

$P_{n,m}(\sin \psi)$  - Legendre's joined functions

$$P_{n+1,m} = (2n+1) \sin \psi P_{n,m} - (n+m) P_{n-1,m}, \quad \text{when } n > m,$$

$$P_{nn} = (2n-1) \cos \psi P_{n-1, n-1},$$

when  $n = m, P_{nm} = 0$

$$\sin mL = \sin(m-1)L \cos L + \cos(m-1)L \sin L,$$

$$\cos mL = -\sin(m-1)L \sin L + \cos(m-1)L \cos L,$$

$$P_{00} = 1, \quad P_{10} = \sin \psi = z/r, \quad P_{11} = \cos \psi = r_1/r, \quad P_{20} = (3 \sin^2 \psi - 1)/2,$$

$$P_{21} = 3 \sin \psi \cos \psi = 3z r_1 / r^2, \quad P_{22} = 3 \cos^2 \psi,$$

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$\alpha_{nm}$ ,  $\beta_{nm}$  - anomaly coefficients

$n_{max}$  - the greatest number of harmonics considered.

c) calculation of only the first four harmonics

$$\Delta g_r = \frac{1}{r} \left( \frac{R}{r} \right)^3 \left( 9 \frac{x^2 - y^2}{r^2} \alpha_{22} + 18 \frac{xy}{r^2} \beta_{22} + \right. \\ \left. + \frac{Rz}{r^2} \left( 10 \frac{z^2}{r^2} - 6 \right) \alpha_{30} + \left( \frac{R}{r} \right)^2 \left( \frac{175}{8} \frac{z^2}{r^2} - \frac{150}{8} \frac{z^2}{r^2} + \frac{15}{8} \right) \alpha_{40} \right);$$

$$\Delta g_m = \frac{1}{r} \left( \frac{R}{r} \right)^3 \frac{r_1}{r} \left( -6 \frac{z}{r} \frac{x^2 - y^2}{r_1^2} \alpha_{22} + 2 \frac{xy}{r_1^2} \beta_{22} \right. \\ \left. + \frac{3}{2} \frac{R}{r} \left( \frac{5z^2}{r^2} - 1 \right) \alpha_{30} + \frac{5}{2} \frac{R^2}{r^2} \frac{z}{r} \left( 7 \frac{z^2}{r^2} - 3 \right) \alpha_{40} \right);$$

$$\Delta g_l = \frac{1}{r} \left( \frac{R}{r} \right)^3 \frac{r_1}{r} \left( -12 \frac{xy}{r_1^2} \alpha_{22} + 6 \frac{x^2 - y^2}{r_1^2} \beta_{22} \right).$$



8. Texts.

```

SUBROUTINE DEG2(X,DG,NM)
DIMENSION X(3),DG(3),PH0(3),PH1(3),A(13)
COMMON/BCONGR/ANM(273),BNM(273)
COMMON/RAD/R1,R
COMMON/CR2/RE
A(1)=ANM(4)
A(2)=ANM(8)
A(3)=ANM(12)
A(4)=ANM(16)
A(5)=ANM(20)
A(6)=ANM(24)
A(7)=ANM(28)
A(8)=ANM(32)
A(9)=ANM(36)
A(10)=ANM(40)
A(11)=ANM(44)
A(12)=ANM(48)
A(13)=ANM(52)
A(14)=ANM(56)
A(15)=ANM(60)
A(16)=ANM(64)
A(17)=ANM(68)
A(18)=ANM(72)
A(19)=ANM(76)
C1=RE/R
C2=X(3)/R
PH0(1)=C2
PH0(2)=(3.0*C2*C2-1.0)/2.0
PH1(1)=R1
PH1(1)=PH1(1)/R
PH1(2)=3.0*C2*PH1(1)
DG(1)=0.0
DG(2)=0.0
U=0.0
DO 10,N=3,NM
U=N
C3=(2.0*U-1.0)*C2
PH0(3)=(C3*PH0(2)-(U-1.0)*PH0(1))/U
PH1(3)=(C3*PH1(2)-U*PH1(1))/(U-1.0)
C3=(C1*(N+1))*A(N-2)
DG(1)=DG(1)+C3*(U+1.0)*PH0(3)
DG(2)=DG(2)+C3*PH1(3)
PH0(1)=PH0(2)
PH0(2)=PH0(3)
PH1(1)=PH1(2)
PH1(2)=PH1(3)
10 CONTINUE
DG(1)=DG(1)/R
DG(2)=DG(2)/R
DG(3)=0.0
RETURN
END

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SUBROUTINE DFR3(X,DG,UN)
  DIMENSION X(3),DG(3),SG(3)
  DIMENSION P(23,24),SML(23),CML(23)
  COMMON/BCONSTR/AMH(273),BMH(273)
  COMMON/RAD/R1,R
  COMMON/GRZ/RF
  SFI=X(3)/R
  CFI=R1/R
  NH1=UN+1
  SML(1)=0.0
  SML(2)=X(2)/R1
  CML(1)=1.0
  CML(2)=X(1)/R1
  DO 1 I=3,NH1
    SML(I)=SML(I-1)*CML(2)+CML(I-1)*SML(2)
1  CML(I)=-SML(I-1)*SML(2)+CML(I-1)*CML(2)
  UN=0.0
  UM=0.0
  P(1,1)=1.0
  P(2,1)=SFI
  P(2,2)=CFI
  NH2=NH1+1
  DO 2 I=2,NH2
2  P(1,I)=0.0
  DO 3 J=3,NH2
3  P(2,J)=0.0
  DO 4 M=1,NH2
  UN=UN-1
  DO 4 N=3,NH1
  UM=UM-1
  J=(2.0*UM-1.0)
  IF(N-H)5,6,7
5  P(N,M)=0.0
  GO TO 4
6  P(N,M)=M*CFI*P(N-1,M-1)
  GO TO 4
7  P(N,M)=(P(N-1,M)+P(N-1,M-1)+UM+UN-1.0)*P(N-1,M-1)/(UM+UN)
4 CONTINUE
  RHOR=RE/R
  UN=0.0
  DO 8 I=1,3
8  DG(I)=0.0
  DO 9 H=3,NH1
  UN=N
  DO 10 I=1,3
10 SG(I)=0.0
  UM=0.0
  DO 11 M=1,N
  IS=0
  JS=N-3
  NAB=M
  IF(NS.LT.1)
  GO TO 13
  DO 12 JS=1,NS
12 NAB=NAB+JS+2
13 C1=AMH(NAB)*CML(H)+BMH(NAB)*SML(H)
  UM=M
  U=(UM-1.)*P(H,M)
  S1(1)=SG(1)+C1*P(H,M)
  S1(2)=SG(2)+C1*(P(H,M+1)-W*(X(3)/R1))
11 SG(3)=SG(3)+(-AMH(NAB)*SML(M)+BMH(NAB)*CML(M))*W
  C2=RHOR*UN
  DG(1)=DG(1)+C2*UN*SG(1)
  DG(2)=DG(2)+C2*SG(2)
  DG(3)=DG(3)+C2*SG(3)
  DG(1)=DG(1)/R
  DG(2)=DG(2)/R
  DG(3)=DG(3)/R1
  RETURN
  END

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SUBROUTINE DEG4(X,DG)
DIMENSION X(3),DG(3)
COMMON/RAD/R1,R
COMMON/CRZ/RE
COMMON/CA22/A22,B22,A30,A40
C1=PE/R
C2=C1*C1
C3=C2*C1/R
C4=C3*C1/R
U1=X(3)/R
U2=U1*U1
U3=X(1)*X(1)-X(2)*X(2)
R2=R*R
R12=R1*R1
U4=U3/R12
U5=X(1)*X(2)/R12
DG(1)=C3*(9.0*U3+A22/R2+14.0*X(1)*X(2)+B22/R2+C1*U1
      *(1.0,0*U2-6.0)*A30*(175.0*U2*U2-150.0*U2+15.0)*C2*A40/3.0)
DG(2)=C4*(-0.0*U1*(4*B22-2.0*U5*B22)+1.5*C1
      *(5.0*U2-1.0)*A30-2.5*C2*U1*(7.0*U2-3.0)*A40)
DG(3)=C4*6.0*(-7.0*U5*A22+U4*B22)
RETURN
END

```

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## REFERENCES

1. El'yasberg, P. Ye., Vvedeniye v teoriyu polyeta isskusstvennykh sputnikov Zemli [Introduction to the theory of flight of artificial Earth satellites], Moscow, Nauka Publ., 1965.
2. Narimanov, G.S., Ed., Osnovy teorii polyeta kosmicheskikh apparatov [Fundamentals of flight theory for spacecraft], Moscow, Mashinostroyeniye Publ., 1972.
3. El'yasberg, P. Ye., B. V. Kugayenko and V. M. Sinitsyn, Algoritmy raschyeta navigatsionnoy o polozhenii sputnika [Algorithms for calculating navigational information on satellite positions], Preprint IKI, No. 102, 1972.
4. Kugayenko, B. V., V. A. Kuz'minykh, G. A. Mersov, R. R. Nazriov, N. G. Khavenson, I. G. Khatskevich, N. A. Eismont and P. E. El'yasberg, Algoritmy raschyeta navigatsionnoy informatsii [Algorithms for calculating navigational information], Preprint IKI, No. 251, 1975.
5. El'yasberg, P. Ye., B. V. Kugayenko, V. M. Sinitsyn and V. E. Sokolov, Algoritmy raschyeta orientatsii sputnika. Znacheniya gravitatsionnykh postoyannykh [Algorithms for calculating the orientation of a satellite. Values of gravitational constants], Preprint IKI, No. 118, 1972.
6. CIRA-72, COSPAR International Reference Atmosphere, Akademie-Verlag, Berlin, 1972.
7. Eskobal, P., Metody astrodinamiki [Methods of astrodynamics], Mir Publ., 1971.
8. Prokhorenko, V. I., Opisaniye universalinoy programmy raschyeta navigatsionnoy informatsii o polozhenii iskusstvennogo sputnika Zemli [Description of general purpose programs for calculating navigational information on the position of an artificial Earth satellite], Preprint IKI, No. 263, 1976.