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JPL PUBLICATION 78-85

# Comet Tempel 2

## Orbit, Ephemerides and Error Analysis

D. K. Yeomans

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National Aeronautics and  
Space Administration

**Jet Propulsion Laboratory**  
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Pasadena, California



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by the Jet Propulsion Laboratory, California Institute of  
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Abstract

The dynamical behavior of comet Tempel 2 is investigated and the comet is found to be very well behaved and easily predictable. The nongravitational forces affecting the motion of this comet are the smallest of any comet that is affected by nongravitational forces. The sign and time history of these nongravitational forces imply (1) a direct rotation of the comet's nucleus and (2) the comet's ability to outgas has not changed substantially over its entire observational history. The well behaved dynamical motion of the comet, the well observed past apparitions, the small nongravitational forces and the excellent 1988 ground based observing conditions all contribute to relatively small position and velocity errors in 1988--the year of a proposed rendezvous space mission to this comet. To assist in planned ground based and earth orbital observations of this comet, ephemerides are given for the 1978-79, 1983-84 and 1988 apparitions.

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PERIODIC COMET TEMPTEL 2

Photographed by H. M. Jeffers at Lick Observatory  
Fall 1946

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## 1. Introduction

On July 3, 1873 Ernst Wilhelm Liebrecht Tempel, a German astronomer working at Arcetri Observatory, Italy, discovered a comet in Cetus. Upon discovery, the comet was approximately 9.5 magnitude, 2 arc minutes in diameter, somewhat elongated in shape with an eccentric condensation of light and a granular appearance. Orbit computations quickly established that the comet was short periodic and Tempel himself was the first to recover the comet on its next return to perihelion in 1878. Tempel had previously discovered two other short-period comets--one in 1867 (Tempel 1) and the other in 1869 (Tempel-Swift). Hence his 1873 comet is denoted Tempel 2 to show this was the second comet to have been discovered by Tempel alone. Within the time of six years and three months, Tempel had discovered three periodic comets--a record that will likely stand for some time. Since its discovery in 1873, comet Tempel 2 has been observed during 16 of its 21 returns to perihelion. Since 1946, every apparition has been observed.

Comet Tempel 2 has recently become of interest as the prime target for a first space rendezvous mission to a comet. NASA's Comet Science Working Group has recommended a rendezvous mission to comet Tempel 2 in 1988 with an en route flyby of comet Halley in late 1985 (Belton, 1978). As the primary objective of the first mission to a comet, the dynamical behavior of comet Tempel 2 is of great interest.

For the majority of short-period comets with three or more apparitions, obvious nongravitational perturbations are affecting their motions. By assuming that these nongravitational accelerations are due to the rocket effect of outgassing volatiles from an icy-conglomerate nucleus (Whipple 1950), the nongravitational accelerations have been successfully modeled

by Marsden et al. (1973). The mathematical form of these nongravitational terms represents an empirical fit to a theoretical plot of water-snow vaporization flux versus heliocentric distance. The cometary equations of motion are written

$$\frac{d^2\vec{r}}{dt^2} = -\mu \frac{\vec{r}}{r^3} + \frac{\partial R}{\partial \vec{r}} + A_1 g(r) \hat{r} + A_2 g(r) \hat{T},$$

where

$$g(r) = \alpha (r/r_0)^{-m} [1 + (r/r_0)^n]^{-k}.$$

The acceleration is given in astronomical units/(ephemeris day)<sup>2</sup>,  $\mu$  is the product of the gravitational constant and the solar mass, while  $R$  is the planetary disturbing function. The scale distance  $r_0$  is the heliocentric distance where reradiation of solar energy begins to dominate the use of this energy for vaporizing the comet's nuclear ices. For water ice  $r_0 = 2.808$  AU and the normalizing constant  $\alpha = 0.111262$ . The exponents  $m$ ,  $n$ , and  $k$  equal 2.15, 5.093, and 4.6142, respectively. The nongravitational acceleration is represented by a radial [ $A_1 g(r)$ ] and a transverse [ $A_2 g(r)$ ] term in the equations of motion. The radial unit vector ( $\hat{r}$ ) is defined outward along the radius vector while the transverse unit vector ( $\hat{T}$ ) is directed normal to  $\hat{r}$ , in the orbit plane and in the direction of the comet's motion. An acceleration component normal to the orbit plane has been found to have a negligible effect upon the orbital motion of short-period comets. The parameters  $A_1$  and  $A_2$ , as well as the six initial conditions, can be solved for in the least-squares differential correction procedure.

Integrated variational orbits were used to form the necessary partial derivatives and the employed numerical integrator was a ninth-order predictor-corrector scheme (summed ordinate form) running at a constant one-day step size. At each step, the required planetary coordinates, from all nine planets, have been read from magnetic tape. All computations were performed in double precision (18 significant figures) on the UNIVAC 1108 computers at the Jet Propulsion Laboratory.

## 2. Orbit Computations

Without solving for nongravitational parameters, Marsden (1968) linked five apparitions of Tempel 2 (1946-1967) with a mean residual of 1.8 arc seconds. Marsden and Sekanina (1971), solving for the nongravitational parameters  $A_1$  and  $A_2$ , managed to successfully link four different sets of apparitions from 1873 through 1967. These parameters, taken from Marsden, Sekanina and Yeomans (1973) are listed in Table 2.

The present orbital solutions are represented in Table 1. Orbit number 1 did not solve for the nongravitational parameters while orbits 2 and 3 solved for  $A_1$  and  $A_2$ . In Table 1 the second column gives the observational interval included in the solution, the third and fourth columns present the number of observations employed and the mean of the absolute values of the residuals. Columns 5 and 6 give the radial ( $A_1$ ) and transverse ( $A_2$ ) nongravitational parameters.

From Tables 1 and 2, the transverse nongravitational parameters are seen to be small and nearly constant in time. Because the transverse nongravitational acceleration directly affects the comet's orbital energy, this component is more accurately determined. If one assumes that the comet's spin axis is not precessing, the magnitude of  $A_1$  and  $A_2$  over a

period of time is a direct measure of a comet's ability to outgas.

From Table 2, we note that, within the associated errors,  $A_1$  and  $A_2$  have remained nearly constant and the comet's ability to outgas has not changed substantially over its entire observational history. The magnitude of this comet's nongravitational parameters is the smallest of any comet that is affected by nongravitational forces. The very slight secular deceleration ( $A_2 > 0$ ) implies that the comet's nucleus is rotating in a direct sense. The very small mean residual resulting from the 1956-1977 orbit (orbit #2, Table 1) implies that this comet is very well behaved and very easy to predict dynamically.

### 3. Ephemeris Computations

In order to generate accurate prediction ephemerides for the coming apparitions, orbit #2 of Table 1 was integrated forward taking into account nongravitational effects and perturbations from all planets. Ephemerides for the 1978-79, 1982-83 and 1988 apparitions are presented in Appendix A.

Sekanina, et al. (1978) have investigated the nuclear magnitude of comet Tempel 2 based upon Roemer's photographic observations in 1962, 1967 and 1972. They find the absolute nuclear magnitude to be  $15.0 \pm 0.5$  pre-perihelion and  $16.0 \pm 0.3$  post-perihelion. However the scatter is so large that an absolute nuclear magnitude of 15.5 was assumed for the present computations. For comet Tempel 2, the variation of total magnitude with heliocentric distance is quite asymmetric with respect to perihelion. This comet brightens very quickly about 80 days before perihelion and this dramatic increase in brightness before perihelion is followed by a less steep decline post-perihelion (see Figure 1). For prediction purposes, a Chebychev series was fit to the light curve of comet Tempel 2

(Figure 1) and total magnitude predictions were made by evaluating this series at appropriate times.

The osculating orbital elements, derived from orbit #2 of Table 1, are presented in Table 3 for the seven returns to perihelion 1957-1988.

#### 4. Error Analysis

A statistical covariance error analysis was undertaken to determine the evolution of comet Tempel 2's error ellipsoid during the 1988 apparition. The ORAN computer program took into account planetary perturbations and considered the errors inherent in the values for the nongravitational parameters and initial conditions. The partial derivatives utilized in the conditional equations matrices and the state transition matrices were computed numerically.

For the present analysis, the four returns to perihelion (1972-1988) are represented by eight observations from September 22, 1973 through April 17, 1977 and by 26 additional postulated observations from April 6, 1983 through September 16, 1988. The 1983 and 1988 recoveries of the comet were conservatively assumed to be April 6, 1983 and March 20, 1988 respectively. The error analysis was initialized in 1973 and the initial a priori covariance matrix was essentially infinite. Each set of observations was batch processed and the updated covariance was propagated forward in time via the state transition matrix to the date of selected observations. The time history of the comet's position and velocity errors is presented in Table 4. The first column represents the dates in 1988 on which one simulated ground based observation was made. The columns headed by  $r$ ,  $\Lambda$  and  $\theta$  represent the sun-comet distance in AU, the earth-comet distance in AU and the sun-earth-comet angle in degrees. The next six

columns represent the 1- $\sigma$  position (km) and velocity (m/s) errors for the radial sun-comet direction ( $R$ ), the direction normal to the comet's orbital plane ( $N$ ), and the transverse direction defined by the cross product of the first two unit vectors ( $T = N \times R$ ). The present analysis assumed a 1- $\sigma$  observational error of 2 arc seconds for both the right ascension and declination. The assumed error for each observation is the same value, and the observations themselves are assumed to be uncorrelated. This being the case, the covariance matrix is linear with respect to observational errors. For example, although the current analysis has been done using an observational error of 2 arc seconds, one only has to multiply the error component entries in Table 4 by 3/2 to obtain the results for  $\sigma=3$  arc seconds.

From Table 4 we see that the transverse position error ( $\sigma_T$ ) reaches a minimum in May when the conditions are excellent for observing the comet's along track error (see Figure 2). The radial position error reaches a minimum at perihelion (September 16) and this is due in part to the comet's radial velocity which reaches a minimum there. The comet's transverse velocity reaches a maximum at perihelion and this partially explains the growth of the transverse position error from May to September. For the present analysis, observations were assumed made every ten days in 1988 from March 20 to September 16. In Table 4, the improvement realized by making the 1988 observations at five day intervals is shown in parentheses for September 16.

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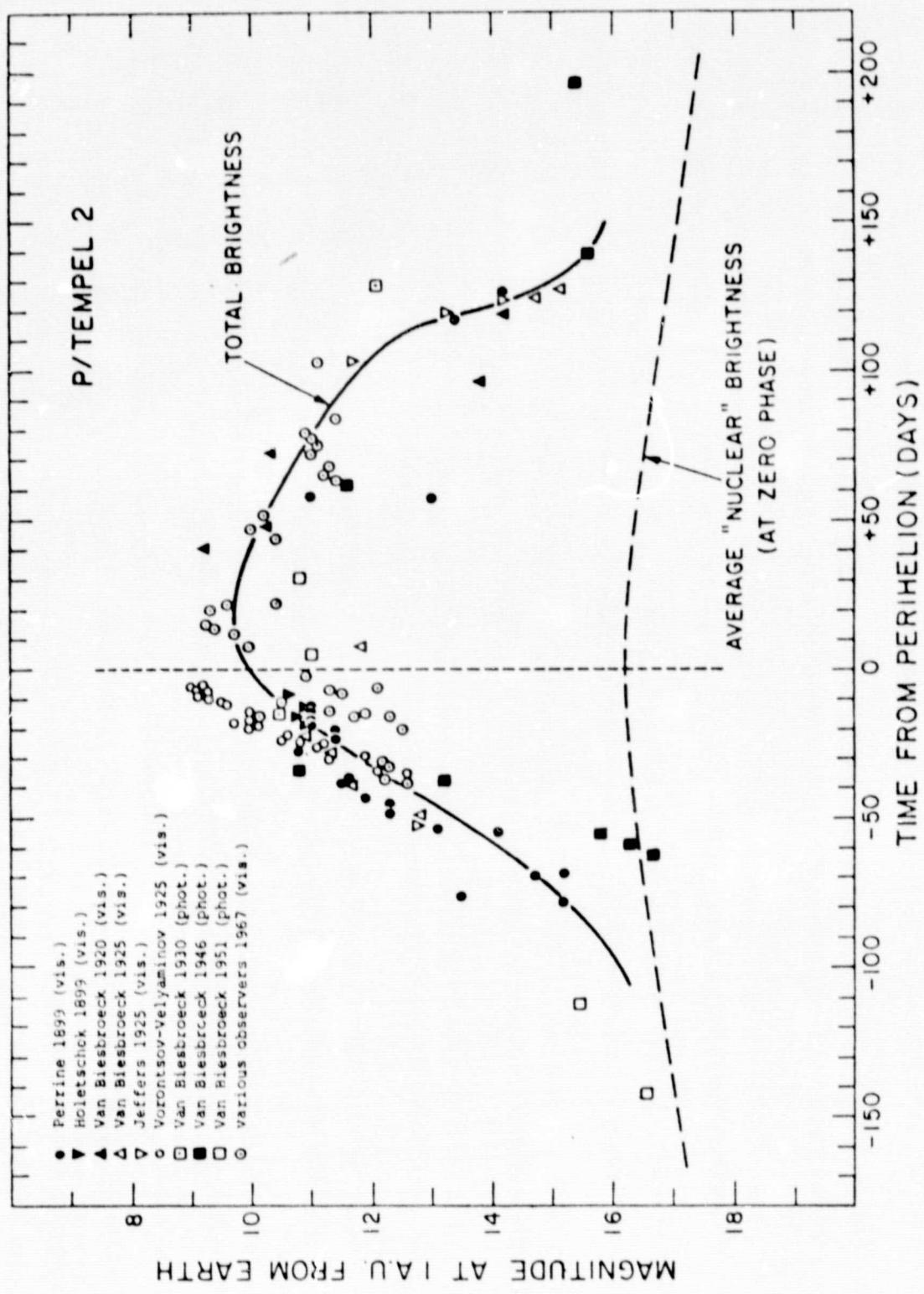
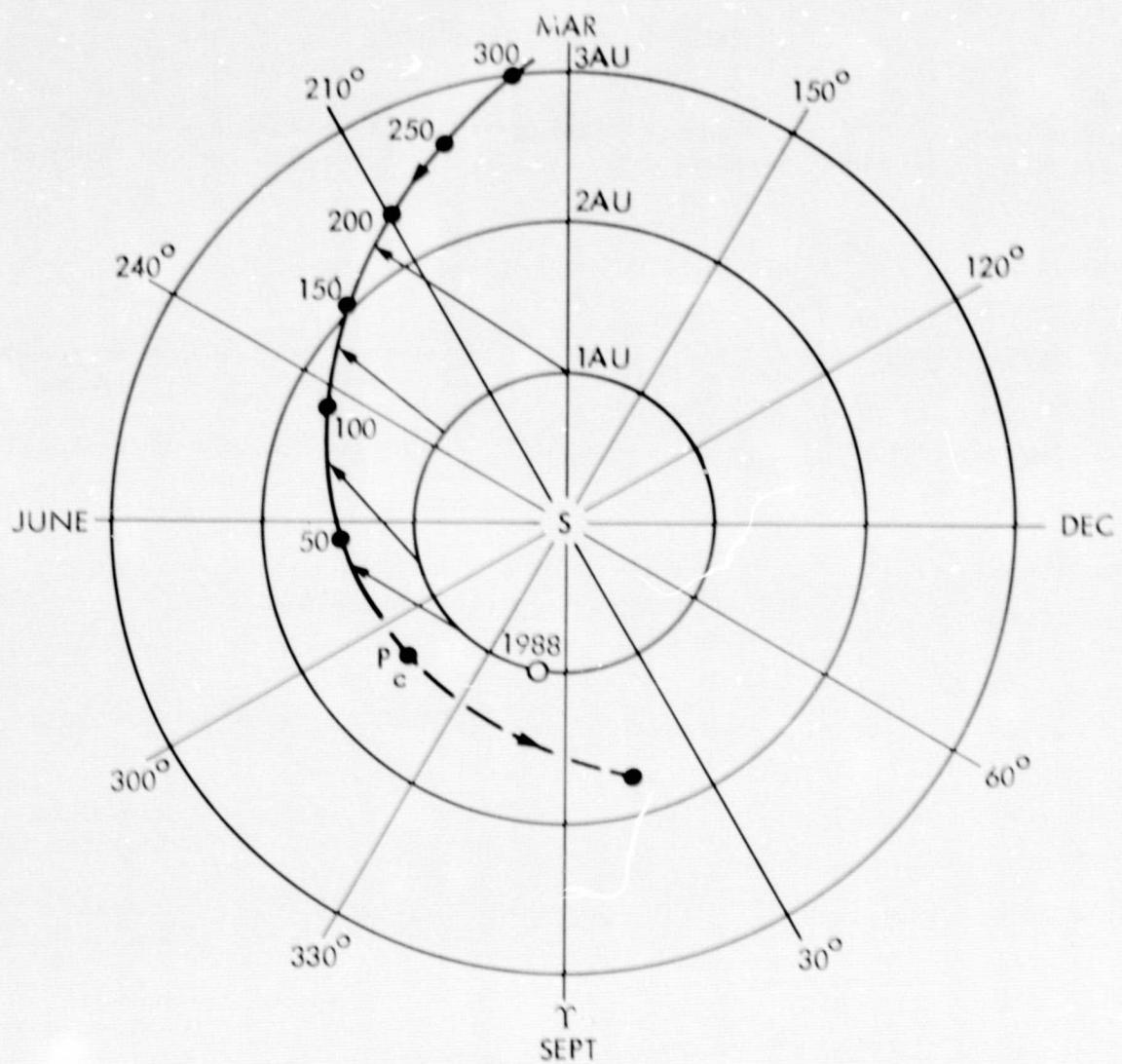


Figure 1. Light Curve for Comet Tempel 2



$P_c$  = PERIHELION OF COMET

● = POSITION OF COMET AT STATED NUMBER OF DAYS BEFORE PERIHELION

O = PREDICTED POSITIONS OF EARTH AT PERIHELION OF COMET

→ = LINE OF SIGHT VECTORS FROM EARTH TO COMET ON Mar 20, May 9, July 8, AND Aug 7

Figure 2. Comet Tempel 2 1988 Observing Conditions

TABLE 1 Orbit Solutions

Orbit	Observation Interval	No. Obs	Mean Residual	Nongravitational Parameters		Comments
				$A_1 \times 10^8$	$A_2 \times 10^8$	
1	1956-1977	91	1.42"	-----	-----	Residual trends to 6"
2	1956-1977	91	0.96"	+0.0815±0.0085	+0.00245±0.00028	No residual trends
3	1946-1977	128	1.36"	-0.0156±0.0053	+0.00245±0.00000	Residual trends to 6"

TABLE 2 Nongravitational Parameters

Perihelion Distance	Eccen.	Interval	Mean Residual	$A_1 \times 10^8$	$A_2 \times 10^8$	Source
1.4	0.6	1873-1915	1.40"	+0.1	+0.002	Marsden & Sekanina (1971)
1.3	0.6	1904-1946	2.31"	0.0	+0.002	Marsden & Sekanina (1971)
1.3	0.6	1915-1956	1.98"	0.0	+0.001	Marsden & Sekanina (1971)
1.4	0.6	1930-1967	1.41"	0.0	+0.001	Marsden & Sekanina (1971)
1.4	0.6	1956-1977	0.96"	0.0	+0.002	Yeomans

TABLE 3 Orbital Elements from Orbit No. 2

Epoch (E.T.)	Perihelion Passage (E.T.)		q (AU)	e	$\omega$ (degrees, 1950.0)	$\Omega$	i	p yrs
1988 Oct. 6.0	1988 Sept. 16.7369		1.383429	0.544428	191.0386	119.1182	12.4319	5.29
1983 May 26.0	1983 June 1.5372		1.381404	0.544893	190.9220	119.1579	12.4375	5.29
1978 Feb. 21.0	1978 Feb. 20.7295		1.369385	0.547833	190.9336	119.2429	12.4680	5.27
1972 Nov. 19.0	1972 Nov. 15.0380		1.364387	0.548887	190.8729	119.2699	12.4804	5.26
1967 Aug. 18.0	1967 Aug. 14.2501		1.366510	0.548395	190.9787	119.2716	12.4739	5.26
1962 May 16.0	1962 May 12.6907		1.363959	0.548987	191.0531	119.2767	12.4819	5.26
1957 Feb. 11.0	1957 Feb. 5.2012		1.369265	0.547682	191.0343	119.2810	12.4702	5.27

TABLE 4 Orbital Error Analysis

Date (1988)	r AU	$\Delta$ AU	$\theta$ Deg.	$\sigma_R$ Km	$\sigma_N$ Km	$\sigma_T$ Km	$\sigma_R^*$ m/s	$\sigma_N^*$ m/s	$\sigma_T^*$ m/s
Mar. 20	2.23	1.58	119	2872	1522	2338	0.128	0.076	0.166
30	2.17	1.43	126						
Apr. 9	2.11	1.28	134	2583	1108	1303	0.082	0.076	0.163
19	2.04	1.16	142						
29	1.98	1.05	149						
May 9	1.92	0.95	154	2403	789	694	0.070	0.080	0.158
19	1.85	0.88	156						
29	1.79	0.83	153						
Jun. 8	1.73	0.79	147	2250	602	914	0.084	0.088	0.146
18	1.68	0.78	138						
29	1.62	0.77	130						
Jul. 8	1.57	0.77	122	2015	448	1626	0.128	0.098	0.127
18	1.53	0.79	115						
28	1.49	0.80	109						
Aug. 7	1.45	0.82	104	1471	388	1993	0.174	0.100	0.093
17	1.42	0.85	99						
27	1.40	0.88	96	1069	431	1870	0.183	0.092	0.076
Sep. 6	1.39	0.91	92						
16	1.38	0.95	90	807	475	1638	0.176	0.079	0.073
				(755)	(396)	(1394)	(0.163)	(0.064)	(0.068)

APPENDIX A

EPHEMERIS (WITH PERTURBATIONS)  
FOR COMET TEMPEL-2

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PHENOMENA (WITH PERTURBATIONS) FOR COMET TEMPEL-2

DAY	HR	J.D.	R.A.	DEC.	DATE	DEC.	LONG	LAT	HEA	THETA	NAG	THETA	NAG	THETA	NAG
74	7 31	0 2445720.5	4 21.303	+10 29.50	4 22.075	+10 33.45	2.370	-2.100	25.51	42.31	25.51	42.31	25.51	42.31	25.51
1974	8 1	0 2443721.5	4 22.459	+10 30.94	4 24.031	+10 34.84	2.366	-2.07	19.75	62.87	25.59	42.87	25.59	42.87	25.59
1974	8 2	0 2443722.5	4 24.397	+10 32.28	4 25.07	+10 36.11	2.363	-2.013	19.75	63.43	25.43	42.33	25.43	42.33	40.41
1974	8 3	0 2443723.5	4 25.920	+10 33.50	4 27.493	+10 37.24	2.359	-2.020	19.76	64.00	25.44	42.22	25.44	42.22	40.45
1974	8 4	0 2443724.5	4 27.625	+10 34.62	4 29.000	+10 34.34	2.354	-2.024	19.76	64.57	25.53	42.02	25.53	42.02	40.48
1974	8 5	0 2443725.5	4 28.014	+10 35.62	4 31.049	+10 39.29	2.350	-2.033	19.77	65.15	25.57	42.22	25.57	42.22	41.41
1974	8 6	0 2443726.5	4 30.386	+10 36.53	4 31.961	+10 40.14	2.346	-2.037	19.77	65.73	25.61	42.42	25.61	42.42	41.44
1974	8 7	0 2443727.5	4 31.440	+10 37.32	4 33.046	+10 40.88	2.342	-2.046	19.78	66.32	25.65	42.47	25.65	42.47	41.47
1974	8 8	0 2443728.5	4 33.277	+10 38.01	4 34.854	+10 41.51	2.337	-2.052	19.78	66.91	25.68	42.42	25.68	42.42	42.41
1974	8 9	0 2443729.5	4 34.096	+10 38.60	4 36.274	+10 42.05	2.333	-2.059	19.78	67.51	25.72	42.42	25.72	42.42	42.44
1974	8 10	0 2443730.5	4 36.094	+10 39.09	4 37.676	+10 42.04	2.328	-2.065	19.79	68.11	25.75	42.42	25.75	42.42	42.47
1974	8 11	0 2443731.5	4 37.082	+10 39.48	4 39.060	+10 42.41	2.324	-2.072	19.79	68.71	25.78	42.41	25.78	42.41	43.00
1974	8 12	0 2443732.5	4 38.487	+10 39.75	4 40.426	+10 43.05	2.319	-2.074	19.79	69.32	25.80	42.46	25.80	42.46	43.01
1974	8 13	0 2443733.5	4 40.194	+10 39.75	4 41.771	+10 43.18	2.314	-2.085	19.79	69.94	25.84	42.41	25.84	42.41	43.06
1974	8 14	0 2443734.5	4 41.523	+10 40.05	4 43.003	+10 43.22	2.310	-2.091	19.80	70.55	25.85	42.41	25.85	42.41	43.09
1974	8 15	0 2443735.5	4 42.834	+10 40.04	4 44.013	+10 43.17	2.304	-2.096	19.80	71.14	25.86	42.41	25.86	42.41	44.02
1974	8 16	0 2443736.5	4 44.425	+10 39.94	4 45.705	+10 43.02	2.304	-2.104	19.80	71.14	25.86	42.41	25.86	42.41	44.05
1974	8 17	0 2443737.5	4 45.138	+10 39.75	4 46.074	+10 42.78	2.302	-2.109	19.80	71.14	25.86	42.41	25.86	42.41	44.06
1974	8 18	0 2443738.5	4 46.652	+10 39.47	4 48.232	+10 42.45	2.294	-2.217	19.80	71.14	25.86	42.41	25.86	42.41	45.01
1974	8 19	0 2443739.5	4 47.884	+10 39.10	4 49.667	+10 42.02	2.294	-2.223	19.81	71.72	25.91	42.41	25.91	42.41	45.04
1974	8 20	0 2443740.5	4 49.101	+10 38.63	4 50.643	+10 41.51	2.278	-2.230	19.81	71.72	25.91	42.41	25.91	42.41	45.07
1974	8 21	0 2443741.5	4 50.125	+10 38.04	4 51.704	+10 41.91	2.273	-2.234	19.81	71.72	25.91	42.41	25.91	42.41	46.00
1974	8 22	0 2443742.5	4 51.471	+10 37.04	4 53.074	+10 42.43	2.267	-2.243	19.81	71.72	25.91	42.41	25.91	42.41	46.03
1974	8 23	0 2443743.5	4 52.424	+10 36.72	4 54.210	+10 39.46	2.262	-2.249	19.81	71.72	25.91	42.41	25.91	42.41	46.05
1974	8 24	0 2443744.5	4 52.764	+10 35.91	4 55.364	+10 38.60	2.256	-2.250	19.81	71.72	25.91	42.41	25.91	42.41	46.09
1974	8 25	0 2443745.5	4 54.874	+10 35.01	4 56.461	+10 37.67	2.251	-2.262	19.81	71.72	25.91	42.41	25.91	42.41	46.13
1974	8 26	0 2443746.5	4 55.972	+10 30.04	4 57.555	+10 36.45	2.245	-2.266	19.81	71.72	25.91	42.41	25.91	42.41	47.55
1974	8 27	0 2443747.5	4 57.045	+10 32.98	4 58.624	+10 35.55	2.239	-2.275	19.81	71.72	25.91	42.41	25.91	42.41	47.77
1974	8 28	0 2443748.5	4 58.097	+10 31.85	4 59.679	+10 34.37	2.233	-2.281	19.81	71.72	25.91	42.41	25.91	42.41	48.00
1974	8 29	0 2443749.5	4 59.127	+10 31.63	4 59.709	+10 33.11	2.227	-2.284	19.81	71.72	25.91	42.41	25.91	42.41	48.33
1974	8 30	0 2443750.5	4 59.135	+10 29.34	4 59.717	+10 31.78	2.221	-2.294	19.81	71.72	25.91	42.41	25.91	42.41	48.66
1974	8 31	0 2443751.5	4 59.172	+10 27.98	4 59.755	+10 30.38	2.215	-2.301	19.81	71.72	25.91	42.41	25.91	42.41	48.99
1974	8 32	0 2443752.5	4 59.224	+10 26.54	4 59.867	+10 32.30	2.205	-2.307	19.81	71.72	25.91	42.41	25.91	42.41	49.32
1974	8 33	0 2443753.5	4 59.225	+10 25.02	4 59.808	+10 27.35	2.203	-2.313	19.81	71.72	25.91	42.41	25.91	42.41	49.44
1974	8 34	0 2443754.5	4 59.344	+10 23.44	4 59.256	+10 25.73	2.197	-2.320	19.81	71.72	25.91	42.41	25.91	42.41	49.47
1974	8 35	0 2443755.5	4 59.439	+10 21.79	4 59.421	+10 24.04	2.191	-2.326	19.81	71.72	25.91	42.41	25.91	42.41	50.00
1974	8 36	0 2443756.5	4 59.710	+10 20.07	4 59.243	+10 22.28	2.184	-2.332	19.81	71.72	25.91	42.41	25.91	42.41	50.24
1974	8 37	0 2443757.5	4 59.558	+10 18.28	4 59.141	+10 20.46	2.178	-2.339	19.81	71.72	25.91	42.41	25.91	42.41	50.55
1974	8 38	0 2443758.5	4 59.342	+10 16.43	4 58.965	+10 18.54	2.172	-2.345	19.81	71.72	25.91	42.41	25.91	42.41	50.88
1974	8 39	0 2443759.5	4 59.192	+10 14.52	4 59.765	+10 16.63	2.165	-2.352	19.81	71.72	25.91	42.41	25.91	42.41	51.00
1974	8 40	0 2443760.5	4 59.958	+10 12.54	4 59.540	+10 14.63	2.159	-2.358	19.81	71.72	25.91	42.41	25.91	42.41	51.33
1974	8 41	0 2443761.5	4 59.700	+10 10.51	4 59.129	+10 12.56	2.152	-2.364	19.81	71.72	25.91	42.41	25.91	42.41	51.55
1974	8 42	0 2443762.5	4 59.436	+10 8.41	4 58.667	+10 10.44	2.146	-2.371	19.81	71.72	25.91	42.41	25.91	42.41	51.78
1974	8 43	0 2443763.5	4 59.137	+10 6.27	4 58.719	+10 8.26	2.139	-2.377	19.81	71.72	25.91	42.41	25.91	42.41	52.11
1974	8 44	0 2443764.5	4 58.814	+10 4.06	4 58.195	+10 6.03	2.133	-2.383	19.81	71.72	25.91	42.41	25.91	42.41	52.33
1974	8 45	0 2443765.5	4 58.468	+10 1.81	4 54.046	+10 3.75	2.126	-2.390	19.81	71.72	25.91	42.41	25.91	42.41	52.66
1974	8 46	0 2443766.5	4 58.091	+10 59.50	4 54.671	+10 1.42	2.120	-2.396	19.81	71.72	25.91	42.41	25.91	42.41	52.88
1974	8 47	0 2443767.5	4 57.690	+10 57.15	4 55.040	+10 5.271	2.113	-2.402	19.81	71.72	25.91	42.41	25.91	42.41	53.11
1974	8 48	0 2443768.5	4 57.264	+10 56.74	4 55.844	+10 5.844	2.106	-2.409	19.81	71.72	25.91	42.41	25.91	42.41	53.44
1974	8 49	0 2443769.5	4 56.811	+10 52.30	4 54.191	+10 6.14	2.101	-2.415	19.81	71.72	25.91	42.41	25.91	42.41	53.66
1974	8 50	0 2443770.5	4 55.332	+10 49.91	4 51.613	+10 6.912	2.093	-2.421	19.81	71.72	25.91	42.41	25.91	42.41	53.88
1974	8 51	0 2443771.5	4 54.926	+10 47.27	4 49.048	+10 4.08	2.087	-2.428	19.81	71.72	25.91	42.41	25.91	42.41	54.11
1974	8 52	0 2443772.5	4 54.293	+10 44.70	4 46.048	+10 4.45	2.080	-2.434	19.81	71.72	25.91	42.41	25.91	42.41	54.33
1974	8 53	0 2443773.5	4 53.753	+10 42.08	4 43.845	+10 4.85	2.073	-2.440	19.81	71.72	25.91	42.41	25.91	42.41	54.66





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L.A. 1950.0 DEC.										
L.L.	J.D.	LL.	LL.	LL.	LL.	LL.	LL.	LL.	LL.	
240384.5	4	7.185	4	9.407	4	10.75	4	12.10	4	13.45
240384.5	5	7.166	5	9.455	5	10.50	5	11.55	5	12.65
240384.5	6	7.147	6	9.472	6	10.52	6	11.57	6	12.75
240384.5	7	7.128	7	9.493	7	10.54	7	11.59	7	12.85
240384.5	8	7.109	8	9.513	8	10.56	8	11.63	8	12.95
240384.5	9	7.090	9	9.534	9	10.58	9	11.67	9	13.05
240384.5	10	7.071	10	9.554	10	10.60	10	11.71	10	13.15
240384.5	11	7.052	11	9.574	11	10.62	11	11.75	11	13.25
240384.5	12	7.033	12	9.594	12	10.64	12	11.79	12	13.35
240384.5	13	7.014	13	9.614	13	10.66	13	11.83	13	13.45
240384.5	14	6.995	14	9.634	14	10.68	14	11.87	14	13.55
240384.5	15	6.976	15	9.654	15	10.70	15	11.91	15	13.65
240384.5	16	6.957	16	9.674	16	10.72	16	11.95	16	13.75
240384.5	17	6.938	17	9.694	17	10.74	17	11.99	17	13.85
240384.5	18	6.919	18	9.714	18	10.76	18	12.03	18	13.95
240384.5	19	6.899	19	9.734	19	10.78	19	12.07	19	14.05
240384.5	20	6.880	20	9.754	20	10.80	20	12.11	20	14.15
240384.5	21	6.861	21	9.774	21	10.82	21	12.15	21	14.25
240384.5	22	6.842	22	9.794	22	10.84	22	12.19	22	14.35
240384.5	23	6.823	23	9.814	23	10.86	23	12.23	23	14.45
240384.5	24	6.804	24	9.834	24	10.88	24	12.27	24	14.55
240384.5	25	6.785	25	9.854	25	10.90	25	12.31	25	14.65
240384.5	26	6.766	26	9.874	26	10.92	26	12.35	26	14.75
240384.5	27	6.747	27	9.894	27	10.94	27	12.39	27	14.85
240384.5	28	6.728	28	9.914	28	10.96	28	12.43	28	14.95
240384.5	29	6.709	29	9.934	29	10.98	29	12.47	29	15.05
240384.5	30	6.690	30	9.954	30	11.00	30	12.51	30	15.15
240384.5	31	6.671	31	9.974	31	11.02	31	12.55	31	15.25
240384.5	32	6.652	32	9.994	32	11.04	32	12.59	32	15.35
240384.5	33	6.633	33	10.014	33	11.06	33	12.63	33	15.45
240384.5	34	6.614	34	10.034	34	11.08	34	12.67	34	15.55
240384.5	35	6.595	35	10.054	35	11.10	35	12.71	35	15.65
240384.5	36	6.576	36	10.074	36	11.12	36	12.75	36	15.75
240384.5	37	6.557	37	10.094	37	11.14	37	12.79	37	15.85
240384.5	38	6.538	38	10.114	38	11.16	38	12.83	38	15.95
240384.5	39	6.519	39	10.134	39	11.18	39	12.87	39	16.05
240384.5	40	6.499	40	10.154	40	11.20	40	12.91	40	16.15
240384.5	41	6.480	41	10.174	41	11.22	41	12.95	41	16.25
240384.5	42	6.461	42	10.194	42	11.24	42	12.99	42	16.35
240384.5	43	6.442	43	10.214	43	11.26	43	13.03	43	16.45
240384.5	44	6.423	44	10.234	44	11.28	44	13.07	44	16.55
240384.5	45	6.404	45	10.254	45	11.30	45	13.11	45	16.65
240384.5	46	6.385	46	10.274	46	11.32	46	13.15	46	16.75
240384.5	47	6.366	47	10.294	47	11.34	47	13.19	47	16.85
240384.5	48	6.347	48	10.314	48	11.36	48	13.23	48	16.95
240384.5	49	6.328	49	10.334	49	11.38	49	13.27	49	17.05
240384.5	50	6.309	50	10.354	50	11.40	50	13.31	50	17.15
240384.5	51	6.290	51	10.374	51	11.42	51	13.35	51	17.25
240384.5	52	6.271	52	10.394	52	11.44	52	13.39	52	17.35
240384.5	53	6.252	53	10.414	53	11.46	53	13.43	53	17.45
240384.5	54	6.233	54	10.434	54	11.48	54	13.47	54	17.55
240384.5	55	6.214	55	10.454	55	11.50	55	13.51	55	17.65
240384.5	56	6.195	56	10.474	56	11.52	56	13.55	56	17.75
240384.5	57	6.176	57	10.494	57	11.54	57	13.59	57	17.85
240384.5	58	6.157	58	10.514	58	11.56	58	13.63	58	17.95
240384.5	59	6.138	59	10.534	59	11.58	59	13.67	59	18.05
240384.5	60	6.119	60	10.554	60	11.60	60	13.71	60	18.15
240384.5	61	6.100	61	10.574	61	11.62	61	13.75	61	18.25
240384.5	62	5.981	62	10.594	62	11.64	62	13.79	62	18.35
240384.5	63	5.962	63	10.614	63	11.66	63	13.83	63	18.45
240384.5	64	5.943	64	10.634	64	11.68	64	13.87	64	18.55
240384.5	65	5.924	65	10.654	65	11.70	65	13.91	65	18.65
240384.5	66	5.905	66	10.674	66	11.72	66	13.95	66	18.75
240384.5	67	5.886	67	10.694	67	11.74	67	14.00	67	18.85
240384.5	68	5.867	68	10.714	68	11.76	68	14.04	68	18.95
240384.5	69	5.848	69	10.734	69	11.78	69	14.08	69	19.05
240384.5	70	5.829	70	10.754	70	11.80	70	14.12	70	19.15
240384.5	71	5.810	71	10.774	71	11.82	71	14.16	71	19.25
240384.5	72	5.791	72	10.794	72	11.84	72	14.20	72	19.35
240384.5	73	5.772	73	10.814	73	11.86	73	14.24	73	19.45
240384.5	74	5.753	74	10.834	74	11.88	74	14.28	74	19.55
240384.5	75	5.734	75	10.854	75	11.90	75	14.32	75	19.65
240384.5	76	5.715	76	10.874	76	11.92	76	14.36	76	19.75
240384.5	77	5.696	77	10.894	77	11.94	77	14.40	77	19.85
240384.5	78	5.677	78	10.914	78	11.96	78	14.44	78	19.95
240384.5	79	5.658	79	10.934	79	11.98	79	14.48	79	20.05
240384.5	80	5.639	80	10.954	80	12.00	80	14.52	80	20.15
240384.5	81	5.620	81	10.974	81	12.02	81	14.56	81	20.25
240384.5	82	5.601	82	10.994	82	12.04	82	14.60	82	20.35
240384.5	83	5.582	83	11.014	83	12.06	83	14.64	83	20.45
240384.5	84	5.563	84	11.034	84	12.08	84	14.68	84	20.55
240384.5	85	5.544	85	11.054	85	12.10	85	14.72	85	20.65
240384.5	86	5.525	86	11.074	86	12.12	86	14.76	86	20.75
240384.5	87	5.506	87	11.094	87	12.14	87	14.80	87	20.85
240384.5	88	5.487	88	11.114	88	12.16	88	14.84	88	20.95
240384.5	89	5.468	89	11.134	89	12.18	89	14.88	89	21.05
240384.5	90	5.449	90	11.154	90	12.20	90	14.92	90	21.15
240384.5	91	5.430	91	11.174	91	12.22	91	14.96	91	21.25
240384.5	92	5.411	92	11.194	92	12.24	92	15.00	92	21.35
240384.5	93	5.392	93	11.214	93	12.26	93	15.04	93	21.45
240384.5	94	5.373	94	11.234	94	12.28	94	15.08	94	21.55
240384.5	95	5.354	95	11.254	95	12.30	95	15.12	95	21.65
240384.5	96	5.335	96	11.274	96	12.32	96	15.16	96	21.75
240384.5	97	5.316	97	11.294	97	12.34	97	15.20	97	21.85
240384.5	98	5.297	98	11.314	98	12.36	98	15.24	98	21.95
240384.5	99	5.278	99	11.334	99	12.38	99	15.28	99	22.05
240384.5	100	5.259	100	11.354	100	12.40	100	15.32	100	22.15
240384.5	101	5.240	101	11.374	101	12.42	101	15.36	101	22.25
240384.5	102	5.221	102	11.394	102	12.44	102	15.40	102	22.35
240384.5	103	5.202	103	11.414	103	12.46	103	15.44	103	22.45
240384.5	104	5.183	104	11.434	104	12.48	104	15.48	104	22.55
240384.5	105	5.164	105	11.454	105	12.50	105	15.52	105	22.65
240384.5	106	5.145	106	11.474	106	12.52	106	15.56	106	22.75
240384.5	107	5.126	107	11.494	107	12.54	107	15.60	107	22.85
240384.5	108	5.107	108	11.514	108	12.56	108	15.64	108	22.95
240384.5	109	5.088	109	11.534	109	12.58	109	15.68	109	23.05
240384.5	110	5.069	110	11.554	110	12.60	110	15.72	110	23.15
240384.5	111	5.050	111	11.574	111	12.62	111	15.76	111	23.25
240384.5	112	5.031	112	11.594	112	12.64	112	15.80	112	23.35
240384.5	113	5.012	113	11.614	113	12.66	113	15.84	113	23.45
240384.5	114	4.993	114	11.634	114	12.68	114	15.88	114	23.55
240384.5	115	4.974	115	11.654	115	12.70	115	15.92	115	23.65
240384.5	116	4.955	116	11.674	116	12.72	116	15.96	116	23.75
240384.5	117	4.936	117	11.694	117	12.74	117	16.00	117	23.85
240384.5	118	4.917	118	11.714	118	12.76	118	16.04	118	23.95
240384.5	119</td									

TR.	NO.	JUL.	ST.	J.D.	R.A.	1950.0	DEC.	R.A.	1950.0	DEC.	RA.	DEC.	MAG.	THET.	LAT.	LONG.
1979	3	13	0	2443945.5	4 27.143	+14 35.35	4 28.435	+14 39.16	3.491	3.392	0.0	21.36	76.10	16.52	-7.3	84.1
1979	3	14	0	2443946.5	4 27.074	+14 40.23	4 29.631	+14 44.01	3.510	3.397	.00	21.38	75.31	16.44	-7.2	84.2
1979	3	15	0	2443947.5	4 28.780	+14 05.09	4 30.438	+14 08.83	3.529	3.402	.00	21.39	74.53	16.36	-7.2	84.3
1979	3	16	0	2443948.5	4 29.610	+14 49.91	4 51.255	+14 53.63	3.548	3.406	.00	21.40	73.74	16.28	-7.2	84.4
1979	3	17	0	2443949.5	4 30.426	+14 54.71	4 32.083	+14 58.39	3.411	3.411	.00	21.41	72.96	16.19	-7.2	84.5

## EXPLANATION OF SYMBOLS

J.D. = JULIAN DATE  
 RA. AND DEC. = 1950.0 ARE RIGHT ASCENSION AND DECLINATION REFERRED TO MEAN EQUATOR AND EQUINOX OF 1950.0  
 RA. AND DEC. = DATE ARE RIGHT ASCENSION AND DECLINATION REFERRED TO MEAN EQUATOR AND EQUINOX OF DATE  
 DISTANCE GEOCENTRIC DISTANCE OF OBJECT IN A.U.  
 R = HELIOCENTRIC DISTANCE OF OBJECT IN A.U.

MAG = TOTAL MAGNITUDE, COMPUTED FROM EMPIRICAL EQUATION BASED UPON PAST OBSERVED BEHAVIOR  
 NAME = NUCLEAR MAGNITUDE = 15.5 + 5.00 \* LONGIT.(DELT.) + 5.00 DLOG10(R) + 3(BETA)  
 NOTE: IN CASES WHERE THET. AND/OR MAG ARE NOT COMPUTED, THE CORRESPONDING COLUMN(S) ARE FILLED WITH ZEROES (0.0).

THET = SUN-EARTH-OBJECT ANGLE IN DEGREES  
 RET = SUN-OBJECT-EARTH ANGLE IN DEGREES  
 LAT AND LONG ARE HELIOCENTRIC ECLIPITIC LATITUDE AND LONGITUDE IN DEG. REFERRED TO 1950.0

THE FOLLOWING OSCULATING ORBITAL ELEMENTS ARE CONSISTENT WITH THE ABOVE EPHEMERIS

PERIOD	2443940.50000	197A	2	21.00000
PERHELION PASSAGE	2443940.22946	197A	2	20.72446
PERHELION DISTANCE (IN A.U.)	1.3693453			
ECCENTRICITY	.5474224			
ANG. OF PERHELION	190.93361			
LONG. OF ASCENDING NODE	119.24287			
INCIDINATION	12.46601			

ANGLES ARE IN DEGREES AND ARE REFERRED TO THE ECLIPTIC AND EQUINOX OF 1950.0  
 CHART AND EPHEMERIS COMPUTATIONS BY  
 DR. D.K. REDWANS  
 JET PROPULSION LAB.  
 PASADENA, CALIF. 91103

REF

NTP

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				LAP	LONG
1983	10	3	2445610.5	3 9-473 - 7 8.71	3 11-133 - 7 1-10
1983	10	5	2445612.5	3 8-032 - 7 23.53	3 9-690 - 7 15.87
1983	10	7	2445614.5	3 6-455 - 7 37.64	3 6-111 - 7 43.08
1983	10	9	2445616.5	3 4-753 - 7 50.95	3 6-111 - 7 29.92
1983	10	11	2445618.5	3 2-938 - 8 3.38	3 4.592 - 8 5.3
1983	10	13	2445620.5	3 1-022 - 8 14.83	3 2.676 - 8 6.92
1983	10	15	2445622.5	2 59.018 - 8 25.24	3 1-017 - 8 17.25
1983	10	17	2445624.5	2 56.939 - 8 26.54	3 1-026 - 8 26.48
1983	10	19	2445626.5	2 54.798 - 8 42.67	2 56.450 - 8 34.54
1983	10	21	2445628.5	2 52.609 - 8 49.60	2 54.261 - 8 41.39
1983	10	23	2445630.5	2 50.384 - 8 55.26	2 52.037 - 8 46.98
1983	10	25	2445632.5	2 48.136 - 8 59.85	2 49.791 - 8 51.29
1983	10	27	2445634.5	2 45.883 - 8 73.73	2 47.517 - 8 54.30
1983	10	29	2445636.5	2 43.633 - 8 45.50	2 45.267 - 8 35.99
1983	10	31	2445638.5	2 41.399 - 8 4.94	2 43.055 - 8 56.35
1983	11	1	2445640.5	2 39.196 - 9 4.05	2 40.853 - 8 55.39
1983	11	3	2445642.5	2 37.035 - 9 1.84	2 38.693 - 8 53.11
1983	11	5	2445644.5	2 34.929 - 9 58.33	2 36.588 - 8 49.53
1983	11	7	2445646.5	2 32.887 - 8 53.53	2 34.549 - 8 44.68
1983	11	9	2445648.5	2 30.921 - 8 47.50	2 32.585 - 8 36.58
1983	11	11	2445650.5	2 29.039 - 8 40.26	2 30.705 - 8 31.28
1983	11	13	2445652.5	2 27.149 - 8 31.86	2 28.817 - 8 22.83
1983	11	15	2445654.5	2 25.557 - 8 22.37	2 27.227 - 8 13.29
1983	11	17	2445656.5	2 23.699 - 8 11.83	2 25.641 - 8 7.70
1983	11	19	2445658.5	2 22.089 - 8 3.30	2 24.163 - 8 1.27
1983	11	21	2445660.5	2 21.120 - 7 47.84	2 22.798 - 7 38.82
1983	11	23	2445662.5	2 19.865 - 7 34.51	2 21.544 - 7 25.26
1983	11	25	2445664.5	2 18.726 - 7 30.37	2 20.408 - 7 11.08
1983	11	27	2445666.5	2 17.705 - 7 5.47	2 19.389 - 7 6.34
1983	11	29	2445668.5	2 16.802 - 6 49.86	2 18.469 - 6 40.52
1983	11	31	2445670.5	2 16.019 - 6 33.60	2 17.709 - 6 24.23
1983	11	32	2445672.5	2 15.356 - 6 16.72	2 17.048 - 6 7.34
1983	11	34	2445674.5	2 14.812 - 5 59.30	2 16.503 - 5 49.89
1983	11	36	2445676.5	2 14.386 - 5 41.36	2 16.083 - 5 31.94
1983	11	38	2445678.5	2 14.077 - 5 22.97	2 15.777 - 5 13.54
1983	11	40	2445680.5	2 14.024 - 5 4.16	2 15.585 - 4 35.73
1983	11	42	2445682.5	2 13.883 - 5 4.16	2 15.506 - 4 35.55
1983	11	44	2445684.5	2 13.801 - 5 4.49	2 15.537 - 4 16.05
1983	11	46	2445686.5	2 13.829 - 4 4.50	2 15.675 - 3 56.27
1983	11	48	2445688.5	2 13.945 - 4 5.71	2 15.917 - 3 56.27
1983	11	50	2445690.5	2 14.204 - 3 45.66	2 15.917 - 3 36.24
1983	11	52	2445692.5	2 14.544 - 3 4.16	2 16.265 - 3 16.01
1983	11	54	2445694.5	2 14.982 - 3 5.03	2 16.700 - 3 55.59
1983	11	56	2445696.5	2 15.515 - 2 44.42	2 17.236 - 2 35.02
1983	11	58	2445698.5	2 16.140 - 2 23.70	2 17.864 - 2 14.32
1983	11	60	2445700.5	2 16.581 - 2 2.86	2 18.561 - 2 8.66
1983	11	62	2445702.5	2 17.657 - 2 1.14	2 19.366 - 2 1.32.63
1983	11	64	2445704.5	2 18.543 - 1 21.00	2 20.275 - 1 11.88
1983	11	66	2445706.5	2 19.511 - 0 59.98	2 21.246 - 0 30.89
1983	11	68	2445708.5	2 20.558 - 0 36.94	2 22.296 - 0 29.67
1983	11	70	2445710.5	2 21.681 - 0 17.89	2 23.422 - 0 8.66
1983	11	72	2445712.5	2 22.677 - 0 3.14	2 24.621 - 0 12.34
1983	11	74	2445714.5	2 23.143 - 0 24.14	2 25.890 - 0 21.19
1983	11	76	2445716.5	2 24.477 - 0 45.09	2 27.227 - 0 54.22
1983	11	78	2445718.5	2 26.875 - 1 5.98	2 28.629 - 1 15.07
1983	11	80	2445720.5	2 28.336 - 1 26.80	2 30.092 - 1 35.84
1983	11	82	2445722.5	2 29.856 - 1 47.52	2 31.615 - 1 56.53
1983	11	84	2445724.5	2 31.433 - 2 8.16	2 33.196 - 2 17.11
1984	1	1	2445610.5	3 9-473 - 7 8.71	3 11-133 - 7 1-10
1984	1	3	2445612.5	3 8-032 - 7 23.53	3 9-690 - 7 15.87
1984	1	5	2445614.5	3 6-455 - 7 37.64	3 6-111 - 7 43.08
1984	1	7	2445616.5	3 4-753 - 7 50.95	3 6-111 - 7 29.92
1984	1	9	2445618.5	3 2-938 - 8 3.38	3 4.592 - 8 5.3
1984	1	11	2445620.5	3 1-022 - 8 14.83	3 2.676 - 8 6.92
1984	1	13	2445622.5	2 59.018 - 8 25.24	3 1-017 - 8 17.25
1984	1	15	2445624.5	2 56.939 - 8 26.54	3 1-026 - 8 26.48
1984	1	17	2445626.5	2 54.798 - 8 42.67	3 1-052 - 8 34.54
1984	1	19	2445628.5	2 52.609 - 8 49.60	3 1-040 - 8 32.04
1984	1	21	2445630.5	2 50.384 - 8 55.26	3 1-050 - 8 41.41
1984	1	23	2445632.5	2 48.136 - 8 59.85	3 1-060 - 8 51.95
1984	1	25	2445634.5	2 45.883 - 8 73.73	3 1-071 - 8 55.9
1984	1	27	2445636.5	2 43.633 - 8 45.50	3 1-084 - 8 35.0
1984	1	29	2445638.5	2 41.399 - 8 4.94	2 43.055 - 8 56.35
1984	1	31	2445640.5	2 39.196 - 9 4.05	2 40.853 - 8 55.39
1984	1	33	2445642.5	2 37.035 - 9 1.84	2 40.693 - 8 53.11
1984	1	35	2445644.5	2 34.929 - 9 58.33	2 40.588 - 8 49.53
1984	1	37	2445646.5	2 32.887 - 8 53.53	2 40.480 - 8 44.68
1984	1	39	2445648.5	2 30.921 - 8 47.50	2 40.382 - 8 36.58
1984	1	41	2445650.5	2 29.039 - 8 40.26	2 40.285 - 8 31.28
1984	1	43	2445652.5	2 27.149 - 8 31.86	2 40.188 - 8 22.83
1984	1	45	2445654.5	2 25.557 - 8 22.37	2 40.091 - 8 13.29
1984	1	47	2445656.5	2 23.699 - 8 11.83	2 40.004 - 8 13.33
1984	1	49	2445658.5	2 21.602 - 8 1.83	2 40.007 - 8 1.83
1984	1	51	2445660.5	2 20.000 - 7 47.84	2 39.900 - 7 38.82
1984	1	53	2445662.5	2 19.865 - 7 34.51	2 39.705 - 7 25.26
1984	1	55	2445664.5	2 18.726 - 7 30.37	2 39.508 - 7 21.08
1984	1	57	2445666.5	2 17.705 - 7 5.47	2 39.311 - 7 1.08
1984	1	59	2445668.5	2 16.802 - 6 49.86	2 39.114 - 6 40.52
1984	1	61	2445670.5	2 16.019 - 6 33.60	2 39.017 - 6 24.23
1984	1	63	2445672.5	2 15.356 - 6 16.72	2 38.920 - 6 17.34
1984	1	65	2445674.5	2 14.812 - 5 59.30	2 38.823 - 6 17.85
1984	1	67	2445676.5	2 14.386 - 5 41.36	2 38.726 - 6 17.38
1984	1	69	2445678.5	2 14.077 - 5 22.97	2 38.629 - 6 17.76
1984	1	71	2445680.5	2 14.024 - 5 4.16	2 38.532 - 6 17.18
1984	1	73	2445682.5	2 13.883 - 5 4.16	2 38.435 - 6 17.60
1984	1	75	2445684.5	2 13.801 - 5 4.49	2 38.338 - 6 18.02
1984	1	77	2445686.5	2 13.829 - 4 4.50	2 38.241 - 6 18.44
1984	1	79	2445688.5	2 14.204 - 3 45.66	2 38.144 - 6 18.86
1984	1	81	2445690.5	2 14.544 - 3 4.16	2 38.047 - 6 19.28
1984	1	83	2445692.5	2 14.982 - 3 5.03	2 38.950 - 6 19.70
1984	1	85	2445694.5	2 15.515 - 2 44.42	2 40.893 - 6 20.19
1984	1	87	2445696.5	2 16.140 - 2 23.70	2 41.796 - 6 20.50
1984	1	89	2445698.5	2 16.581 - 2 2.86	2 42.699 - 6 21.00
1984	1	91	2445700.5	2 17.657 - 2 1.14	2 43.502 - 6 21.41
1984	1	93	2445702.5	2 18.543 - 1 21.00	2 44.305 - 6 21.82
1984	1	95	2445704.5	2 19.511 - 0 59.98	2 45.108 - 6 22.25
1984	1	97	2445706.5	2 20.558 - 0 36.94	2 46.001 - 6 22.34
1984	1	99	2445708.5	2 21.681 - 0 17.89	2 46.904 - 6 22.41
1984	1	101	2445710.5	2 22.677 - 0 3.14	2 47.807 - 6 22.46
1984	1	103	2445712.5	2 23.143 - 0 24.14	2 48.710 - 6 22.49
1984	1	105	2445714.5	2 24.477 - 0 45.09	2 49.613 - 6 22.50
1984	1	107	2445716.5	2 25.875 - 0 5.98	2 50.516 - 6 22.50
1984	1	109	2445718.5	2 26.875 - 1 5.98	2 51.419 - 6 22.50
1984	1	111	2445720.5	2 28.336 - 1 26.80	2 52.322 - 6 22.48
1984	1	113	2445722.5	2 30.092 - 1 27.52	2 53.225 - 6 22.44
1984	1	115	2445724.5	2 31.433 - 1 31.433	2 54.128 - 6 22.39
1984	1	117	2445726.5	2 32.336 - 1 31.433	2 55.031 - 6 22.39
1984	1	119	2445728.5	2 33.196 - 1 31.433	2 55.934 - 6 22.39
1984	1	121	2445730.5	2 34.133 - 1 31.433	2 56.837 - 6 22.39
1984	1	123	2445732.5	2 35.000 - 1 31.433	2 57.740 - 6 22.39

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TH	DT	DE	RA.	1950.0	DEC.	RA.	DEC.	RA.	1950.0	DEC.	RA.	DEC.
1954	5 18	+0	24 45 58 38.5	4 52.673	+16 15.71	0 54.686	+16 18.98	0.170	3.223	+0.0	21.31	18.07
1954	5 20	+0	24 45 58 40.5	4 55.617	+16 22.85	0 57.398	+16 26.00	4.188	3.253	+0.0	21.32	16.69
1954	5 22	+0	24 45 58 42.5	4 58.180	+16 29.73	0 58.140	+16 32.75	4.206	3.263	+0.0	21.32	15.72
1954	5 24	+0	24 45 58 44.5	5 1.699	+16 36.38	5 2.682	+16 39.24	4.224	3.253	+0.0	21.32	14.58
1954	5 26	+0	24 45 58 46.5	5 3.634	+16 42.72	5 5.620	+16 45.47	4.240	3.263	+0.0	21.33	13.91
1954	5 28	+0	24 45 58 48.5	5 6.368	+16 48.63	5 8.358	+16 51.45	4.256	3.273	+0.0	21.33	12.29
1954	5 30	+0	24 45 58 50.5	5 9.093	+16 54.69	5 11.083	+16 57.17	4.272	3.283	+0.0	21.34	11.19
1954	5 31	+0	24 45 58 52.5	5 11.814	+17 2.63	5 13.807	+17 2.63	4.286	3.293	+0.0	21.34	3.44

## EXPLANATION OF SYMBOLS

JD = JULIAN DATE  
 RA. AND DEC. = 1950.0 ARE RIGHT ASCENSION AND DECLINATION REFERRED TO MEAN EQUATOR AND EQUINOX OF 1950.0  
 RA. AND DEC. = DATE ARE RIGHT ASCENSION AND DECLINATION REFERRED TO MEAN EQUATOR AND EQUINOX OF DATE  
 DELTAR = GEOCENTRIC DISTANCE OF OBJECT IN AU.  
 RH = HELIOCENTRIC DISTANCE OF OBJECT IN AU.

MAG = TOTAL MAGNITUDE COMPUTED FROM EMPIRICAL EQUATION BASED UPON PAST OBSERVED BEHAVIOR  
 NMAG = NUCLEAR MAGNITUDE = 15.5 + 5.0 LOG(DIST(DELTA) \* S(OROLOGIC)1(B) \* S(OROLOGIC)2(B))  
 NOTE: IN CASES WHERE THAG AND/OR NMAG ARE NOT COMPUTED, THE CORRESPONDING COLUMN(B) ARE FILLED WITH ZEROES (0.0).

TETRA = SUN-EARTH-OBJECT-EARTH ANGLE IN DEGREES  
 BETAN = BUN-OBJECT-EARTH ANGLE IN DEGREES  
 LAT AND LONG = HELIOCENTRIC ECLIPSTIC LATITUDE AND LONGITUDE IN DEGREES REFERRED TO 1950.0

THE FOLLOWING OSCULATING ORBITAL ELEMENTS ARE CONSISTENT WITH THE ABOVE EPHEMERIS

EPPOCH	PERIMELION PASSAGE	1953	5 26.00000
	PERIMELION DISTANCE IN AU	1.3814043	6 1.93719
	ECCENTRICITY	.5446830	
	ARG. OF PERIMELION	190.92200	
	LONG. OF ASCENDING NODE	119.15793	
	INCLINATION	12.43750	

ANGLES ARE IN DEGREES AND ARE REFERRED TO THE ECLIPSTIC AND EQUINOX OF 1950.0  
 ORBIT AND EPHEMERIS COMPUTATIONS BY  
 DR. D.K. YEOMANS

JET PROPULSION LAB.  
 PASADENA, CALIF.  
 91103

SPIN

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EQUATIONS (WITH PERTURBATIONS) FOR COSET TEMPEL #2

DAY	HR	MIN	SEC	DEC.	DATE	DELT.	BETA	THETA	LON.
1	0	244220.5	15 44 38.7	+ 4	2 48 39.3	+ 4	9.54	19.50	163.81
2	0	244221.5	15 45 42.8	- 3	59.8	- 3	8.83	19.48	166.53
3	0	244222.5	15 46 45.8	- 3	57.0	- 3	9.9	19.45	165.24
4	0	244223.5	15 47 47.1	- 3	54.0	- 3	1.01	19.42	165.98
5	0	244224.5	15 48 47.3	- 3	51.0	- 3	57.81	19.39	166.68
6	0	244225.5	15 49 48.0	- 3	47.4	- 3	54.87	19.31	167.41
7	0	244226.5	15 50 43.3	- 3	44.5	- 3	51.30	19.28	167.92
8	0	244227.5	15 51 49.2	- 3	41.0	- 3	47.75	19.25	168.59
9	0	244228.5	15 52 33.6	- 3	37.4	- 3	44.15	19.22	169.26
10	0	244229.5	15 53 25.4	- 3	35.7	- 3	40.38	19.19	169.93
11	0	244230.5	15 54 17.8	- 3	32.8	- 3	38.48	19.16	170.50
12	0	244231.5	15 55 0.3	- 3	25.6	- 3	32.44	19.13	171.78
13	0	244232.5	15 55 55.3	- 3	21.9	- 3	28.27	19.10	172.27
14	0	244233.5	15 56 1.9	- 3	17.4	- 3	23.97	19.07	172.82
15	0	244234.5	15 56 59.1	- 3	13.9	- 3	19.53	19.04	173.37
16	0	244235.5	15 57 4.2	- 3	8.6	- 3	15.98	19.01	173.92
17	0	244236.5	15 57 52.0	- 3	5.1	- 3	12.44	18.98	174.47
18	0	244237.5	15 58 1.6	- 3	1.6	- 3	8.94	18.95	174.92
19	0	244238.5	15 58 56.9	- 3	59.1	- 3	5.48	18.92	175.37
20	0	244239.5	15 59 18.1	- 3	13.6	- 3	2.02	18.89	175.82
21	0	244240.5	15 59 58.1	- 3	59.1	- 3	1.60	18.86	176.27
22	0	244241.5	16 00 2.7	- 3	64.6	- 3	55.80	18.83	176.72
23	0	244242.5	16 00 59.3	- 3	69.7	- 3	51.98	18.80	177.17
24	0	244243.5	16 01 55.8	- 3	75.2	- 3	47.59	18.77	177.62
25	0	244244.5	16 02 52.3	- 3	81.7	- 3	43.38	18.74	178.07
26	0	244245.5	16 03 48.8	- 3	88.2	- 3	39.28	18.71	178.52
27	0	244246.5	16 04 45.3	- 3	94.7	- 3	35.28	18.68	178.97
28	0	244247.5	16 05 41.8	- 3	101.2	- 3	31.32	18.65	179.42
29	0	244248.5	16 06 38.3	- 3	107.7	- 3	27.47	18.62	179.87
30	0	244249.5	16 07 34.8	- 3	114.2	- 3	23.62	18.59	180.32
31	0	244250.5	16 08 31.3	- 3	120.7	- 3	19.77	18.56	180.77
32	0	244251.5	16 09 27.8	- 3	127.2	- 3	15.92	18.53	181.22
33	0	244252.5	16 10 24.3	- 3	133.7	- 3	12.07	18.50	181.67
34	0	244253.5	16 11 20.8	- 3	140.2	- 3	8.22	18.47	182.12
35	0	244254.5	16 12 17.3	- 3	146.7	- 3	4.37	18.44	182.57
36	0	244255.5	16 13 13.8	- 3	153.2	- 3	0.52	18.41	183.02
37	0	244256.5	16 14 8.3	- 3	159.7	- 3	1.67	18.38	183.47
38	0	244257.5	16 15 4.8	- 3	166.2	- 3	7.82	18.35	183.92
39	0	244258.5	16 16 0.3	- 3	172.7	- 3	13.97	18.32	184.37
40	0	244259.5	16 16 56.8	- 3	179.2	- 3	19.12	18.29	184.82
41	0	244260.5	16 17 53.3	- 3	185.7	- 3	25.27	18.26	185.27
42	0	244261.5	16 18 49.8	- 3	192.2	- 3	31.42	18.23	185.72
43	0	244262.5	16 19 46.3	- 3	198.7	- 3	37.57	18.20	186.17
44	0	244263.5	16 20 42.8	- 3	205.2	- 3	43.72	18.17	186.62
45	0	244264.5	16 21 39.3	- 3	211.7	- 3	49.87	18.14	187.07
46	0	244265.5	16 22 35.8	- 3	218.2	- 3	56.02	18.11	187.52
47	0	244266.5	16 23 32.3	- 3	224.7	- 3	62.17	18.08	187.97
48	0	244267.5	16 24 28.8	- 3	231.2	- 3	68.32	18.05	188.42
49	0	244268.5	16 25 25.3	- 3	237.7	- 3	74.47	18.02	188.87
50	0	244269.5	16 26 21.8	- 3	244.2	- 3	80.62	18.00	189.32
51	0	244270.5	16 27 18.3	- 3	250.7	- 3	86.77	18.07	189.77
52	0	244271.5	16 28 14.8	- 3	257.2	- 3	92.92	18.04	190.22
53	0	244272.5	16 29 11.3	- 3	263.7	- 3	99.07	18.01	190.67
54	0	244273.5	16 30 7.8	- 3	270.2	- 3	105.22	17.98	191.12
55	0	244274.5	16 31 4.3	- 3	276.7	- 3	111.37	17.95	191.57
56	0	244275.5	16 32 0.8	- 3	283.2	- 3	117.52	17.92	192.02
57	0	244276.5	16 32 25.3	- 3	289.7	- 3	123.67	17.89	192.47
58	0	244277.5	16 33 1.8	- 3	296.2	- 3	130.82	17.86	192.92
59	0	244278.5	16 33 28.3	- 3	302.7	- 3	137.97	17.83	193.37
60	0	244279.5	16 34 24.8	- 3	309.2	- 3	145.12	17.80	193.82
61	0	244280.5	16 35 21.3	- 3	315.7	- 3	152.27	17.77	194.27
62	0	244281.5	16 36 17.8	- 3	322.2	- 3	159.42	17.74	194.72
63	0	244282.5	16 37 14.3	- 3	328.7	- 3	166.57	17.71	195.17
64	0	244283.5	16 38 10.8	- 3	335.2	- 3	173.72	17.68	195.62
65	0	244284.5	16 39 6.3	- 3	341.7	- 3	180.87	17.65	196.07
66	0	244285.5	16 40 2.8	- 3	348.2	- 3	188.02	17.62	196.52
67	0	244286.5	16 41 8.3	- 3	354.7	- 3	195.17	17.59	196.97
68	0	244287.5	16 42 4.8	- 3	361.2	- 3	202.32	17.56	197.42
69	0	244288.5	16 43 10.3	- 3	367.7	- 3	209.47	17.53	197.87
70	0	244289.5	16 44 6.8	- 3	374.2	- 3	216.62	17.50	198.32
71	0	244290.5	16 45 2.3	- 3	380.7	- 3	223.77	17.47	198.77
72	0	244291.5	16 46 8.8	- 3	387.2	- 3	230.92	17.44	199.22
73	0	244292.5	16 47 4.3	- 3	393.7	- 3	238.07	17.41	199.67
74	0	244293.5	16 48 9.8	- 3	400.2	- 3	245.22	17.38	200.12
75	0	244294.5	16 49 5.3	- 3	406.7	- 3	252.37	17.35	200.57
76	0	244295.5	16 50 10.8	- 3	413.2	- 3	259.52	17.32	201.02
77	0	244296.5	16 51 6.3	- 3	419.7	- 3	266.67	17.29	201.47
78	0	244297.5	16 52 11.8	- 3	426.2	- 3	273.82	17.26	201.92
79	0	244298.5	16 53 7.3	- 3	432.7	- 3	280.97	17.23	202.37
80	0	244299.5	16 54 2.8	- 3	439.2	- 3	288.12	17.20	202.82
81	0	244300.5	16 55 8.3	- 3	445.7	- 3	295.27	17.17	203.27
82	0	244301.5	16 56 38.8	- 3	452.2	- 3	302.42	17.14	203.72
83	0	244302.5	16 57 24.3	- 3	458.7	- 3	309.57	17.11	204.17
84	0	244303.5	16 58 9.8	- 3	465.2	- 3	316.72	17.08	204.62
85	0	244304.5	16 59 5.3	- 3	471.7	- 3	323.87	17.05	205.07
86	0	244305.5	16 59 10.8	- 3	478.2	- 3	331.02	17.02	205.52
87	0	244306.5	16 59 16.3	- 3	484.7	- 3	338.17	17.00	205.97
88	0	244307.5	16 59 21.8	- 3	491.2	- 3	345.32	16.97	206.42
89	0	244308.5	16 59 27.3	- 3	497.7	- 3	352.47	16.95	206.87
90	0	244309.5	16 59 32.8	- 3	504.2	- 3	359.62	16.92	207.32
91	0	244310.5	16 59 38.3	- 3	510.7	- 3	366.77	16.90	207.77
92	0	244311.5	16 59 43.8	- 3	517.2	- 3	373.92	16.87	208.22
93	0	244312.5	16 59 49.3	- 3	523.7	- 3	381.07	16.85	208.67
94	0	244313.5	16 59 54.8	- 3	530.2	- 3	388.22	16.82	209.12
95	0	244314.5	16 59 59.3	- 3	536.7	- 3	395.37	16.80	209.57
96	0	244315.5	16 59 64.8	- 3	543.2	- 3	402.52	16.77	210.02
97	0	244316.5	16 59 69.3	- 3	549.7	- 3	409.67	16.75	210.47
98	0	244317.5	16 59 74.8	- 3	556.2	- 3	416.82	16.72	210.92
99	0	244318.5	16 59 79.3	- 3	562.7	- 3	423.97	16.70	211.37
100	0	244319.5	16 59 84.8	- 3	569.2	- 3	431.12	16.67	211.82
101	0	244320.5	16 59 89.3	- 3	575.7	- 3	438.27	16.65	212.27
102	0	244321.5	16 59 94.8	- 3	582.2	- 3	445.42	16.62	212.72
103	0	244322.5	16 59 99.3	- 3	588.7	- 3	452.57	16.60	213.17
104	0	244323.5	16 59 104.8	- 3	595.2	- 3	459.72	16.58	213.62
105	0	244324.5	16 59 109.3	- 3	601.7	- 3	466.87	16.55	214.07
106	0	244325.5	16 59 114.8	- 3	608.2	- 3	474.02	16.53	214.52
107	0	244326.5	16 59 119.3	- 3	614.7	- 3	481.17	16.50	214.97
108	0	244327.5	16 59 124.8	- 3	621.2	- 3	488.32	16.48	215.42
109	0	244328.5	16 59 129.3	- 3	627.7	- 3	495.47	16.45	215.87
110	0	244329.5	16 59 134.8	- 3	634.2	- 3	502.62	16.43	216.32
111	0	244330.5	16 59 139.3	- 3	640.7	-			



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T.M.D.		R.A.		1950.0 DEC.	
1988	6 15	0	24473886.5	16 3.315	+15 55.43
1988	6 16	0	2447384.5	16 2.78	+16 17.74
1988	6 17	0	2447390.5	16 5.287	+16 4.07
1988	6 18	0	2447394.5	16 7.287	+16 9.494
1988	6 19	0	2447394.5	16 9.341	+17 2.29
1988	6 20	0	2447392.5	16 1.441	+17 24.43
1988	6 21	0	2447393.5	16 1.585	+17 46.48
1988	6 22	0	2447394.5	16 15.775	+18 6.44
1988	6 23	0	2447395.5	16 18.008	+18 30.24
1988	6 24	0	2447396.5	16 20.286	+18 52.00
1988	6 25	0	2447397.5	16 22.608	+19 13.59
1988	6 26	0	2447398.5	16 24.973	+19 35.04
1988	6 27	0	2447399.5	16 27.348	+19 56.34
1988	6 28	0	2447400.5	16 29.833	+20 17.47
1988	6 29	0	2447401.5	16 32.327	+20 20.32
1988	6 30	0	2447402.5	16 34.863	+20 34.44
1988	6 31	0	2447403.5	16 37.442	+21 1.981
1988	6 32	0	2447404.5	16 40.062	+21 40.19
1988	6 33	0	2447405.5	16 42.724	+22 1.37
1988	6 34	0	2447406.5	16 45.428	+22 16.47
1988	6 35	0	2447407.5	16 48.172	+22 30.503
1988	6 36	0	2447408.5	16 50.958	+22 59.22
1988	6 37	0	2447409.5	16 53.784	+22 59.50
1988	6 38	0	2447410.5	16 56.612	+23 1.871
1988	6 39	0	2447411.5	16 58.450	+23 4.612
1988	6 40	0	2447412.5	16 59.558	+23 56.33
1988	6 41	0	2447413.5	17 5.487	+24 1.472
1988	6 42	0	2447414.5	17 6.510	+24 50.80
1988	6 43	0	2447414.5	17 6.510	+24 50.58
1988	6 44	0	2447415.5	17 11.572	+25 8.04
1988	6 45	0	2447415.5	17 14.671	+25 25.18
1988	6 46	0	2447417.5	17 17.808	+25 41.95
1988	6 47	0	2447418.5	17 20.979	+25 58.39
1988	6 48	0	2447419.5	17 24.187	+26 14.46
1988	6 49	0	2447420.5	17 27.430	+26 17.29
1988	6 50	0	2447421.5	17 30.707	+26 45.50
1988	6 51	0	2447422.5	17 34.017	+27 1.43
1988	6 52	0	2447423.5	17 37.380	+27 14.97
1988	6 53	0	2447424.5	17 40.735	+27 29.10
1988	6 54	0	2447425.5	17 44.141	+27 42.82
1988	6 55	0	2447426.5	17 47.576	+27 46.576
1988	6 56	0	2447427.5	17 51.040	+28 6.97
1988	6 57	0	2447428.5	17 54.532	+28 21.39
1988	6 58	0	2447429.5	17 58.051	+28 33.38
1988	6 59	0	2447430.5	18 1.598	+28 44.88
1988	6 60	0	2447431.5	18 5.165	+28 55.93
1988	6 61	0	2447432.5	18 8.759	+29 6.52
1988	6 62	0	2447433.5	18 12.375	+29 1.664
1988	6 63	0	2447434.5	18 16.013	+29 15.42
1988	6 64	0	2447435.5	18 19.672	+29 35.43
1988	6 65	0	2447436.5	18 23.350	+29 44.09
1988	6 66	0	2447437.5	18 27.097	+29 52.26
1988	6 67	0	2447438.5	18 30.762	+29 59.93
1988	6 68	0	2447439.5	18 34.493	+29 56.973
1988	6 69	0	2447440.5	18 38.240	+30 1.376
1988	6 70	0	2447441.5	18 42.000	+30 19.92
1988	6 71	0	2447442.5	18 45.779	+30 25.56
1988	6 72	0	2447443.5	18 49.559	+30 30.70
1988	6 73	0	2447444.5	18 53.355	+30 35.32
1988	6 74	0	2447445.5	18 56.837	+30 41.008
1988	6 75	0	2447446.5	18 59.837	+30 45.076
1988	6 76	0	2447447.5	18 62.840	+30 49.880
1988	6 77	0	2447448.5	18 65.837	+30 54.908
1988	6 78	0	2447449.5	18 68.837	+30 59.935
1988	6 79	0	2447450.5	18 71.837	+30 64.963
1988	6 80	0	2447451.5	18 74.837	+30 69.991
1988	6 81	0	2447452.5	18 77.837	+30 74.020
1988	6 82	0	2447453.5	18 80.837	+30 78.048
1988	6 83	0	2447454.5	18 83.837	+30 82.077
1988	6 84	0	2447455.5	18 86.837	+30 86.105
1988	6 85	0	2447456.5	18 89.837	+30 90.133
1988	6 86	0	2447457.5	18 92.837	+30 94.161
1988	6 87	0	2447458.5	18 95.837	+30 98.189
1988	6 88	0	2447459.5	18 98.837	+31 02.217
1988	6 89	0	2447460.5	19 1.837	+31 06.245
1988	6 90	0	2447461.5	19 4.837	+31 09.273
1988	6 91	0	2447462.5	19 7.837	+31 13.301
1988	6 92	0	2447463.5	19 10.837	+31 17.329
1988	6 93	0	2447464.5	19 13.837	+31 21.357
1988	6 94	0	2447465.5	19 16.837	+31 25.385
1988	6 95	0	2447466.5	19 19.837	+31 29.413
1988	6 96	0	2447467.5	19 22.837	+31 33.441
1988	6 97	0	2447468.5	19 25.837	+31 37.469
1988	6 98	0	2447469.5	19 28.837	+31 41.497
1988	6 99	0	2447470.5	19 31.837	+31 45.525
1988	6 100	0	2447471.5	19 34.837	+31 49.553
1988	6 101	0	2447472.5	19 37.837	+31 53.581
1988	6 102	0	2447473.5	19 40.837	+31 57.609
1988	6 103	0	2447474.5	19 43.837	+31 61.637
1988	6 104	0	2447475.5	19 46.837	+31 65.665
1988	6 105	0	2447476.5	19 49.837	+31 69.693
1988	6 106	0	2447477.5	19 52.837	+31 73.721
1988	6 107	0	2447478.5	19 55.837	+31 77.749
1988	6 108	0	2447479.5	19 58.837	+31 81.777
1988	6 109	0	2447480.5	19 61.837	+31 85.805
1988	6 110	0	2447481.5	19 64.837	+31 89.833
1988	6 111	0	2447482.5	19 67.837	+31 93.861
1988	6 112	0	2447483.5	19 70.837	+31 97.889
1988	6 113	0	2447484.5	19 73.837	+32 01.917
1988	6 114	0	2447485.5	19 76.837	+32 05.945
1988	6 115	0	2447486.5	19 79.837	+32 09.973
1988	6 116	0	2447487.5	19 82.837	+32 13.001
1988	6 117	0	2447488.5	19 85.837	+32 16.029
1988	6 118	0	2447489.5	19 88.837	+32 19.057
1988	6 119	0	2447490.5	19 91.837	+32 22.085
1988	6 120	0	2447491.5	19 94.837	+32 25.113
1988	6 121	0	2447492.5	19 97.837	+32 28.141
1988	6 122	0	2447493.5	20 0.837	+32 31.169
1988	6 123	0	2447494.5	20 3.837	+32 34.197
1988	6 124	0	2447495.5	20 6.837	+32 37.225
1988	6 125	0	2447496.5	20 9.837	+32 40.253
1988	6 126	0	2447497.5	21.237	+32 43.281
1988	6 127	0	2447498.5	21.547	+32 46.309
1988	6 128	0	2447499.5	21.857	+32 49.337
1988	6 129	0	2447500.5	22.167	+32 52.365
1988	6 130	0	2447501.5	22.477	+32 55.393
1988	6 131	0	2447502.5	22.787	+32 58.421
1988	6 132	0	2447503.5	23.097	+32 61.449
1988	6 133	0	2447504.5	23.407	+32 64.477
1988	6 134	0	2447505.5	23.717	+32 67.505
1988	6 135	0	2447506.5	24.027	+32 70.533
1988	6 136	0	2447507.5	24.337	+32 73.561
1988	6 137	0	2447508.5	24.647	+32 76.589
1988	6 138	0	2447509.5	24.957	+32 80.617
1988	6 139	0	2447510.5	25.267	+32 83.645
1988	6 140	0	2447511.5	25.577	+32 86.673
1988	6 141	0	2447512.5	25.887	+32 89.701
1988	6 142	0	2447513.5	26.197	+32 92.729
1988	6 143	0	2447514.5	26.507	+32 95.757
1988	6 144	0	2447515.5	26.817	+32 98.785
1988	6 145	0	2447516.5	27.127	+33 01.813
1988	6 146	0	2447517.5	27.437	+33 04.841
1988	6 147	0	2447518.5	27.747	+33 07.869
1988	6 148	0	2447519.5	28.057	+33 10.897
1988	6 149	0	2447520.5	28.367	+33 13.925
1988	6 150	0	2447521.5	28.677	+33 16.953
1988	6 151	0	2447522.5	29.087	+33 19.981
1988	6 152	0	2447523.5	29.497	+33 22.009
1988	6 153	0	2447524.5	29.807	+33 24.037
1988	6 154	0	2447525.5	30.217	+33 26.065
1988	6 155	0	2447526.5	30.627	+33 28.093
1988	6 156	0	2447527.5	31.037	+33 31.121
1988	6 157	0	2447528.5	31.447	+33 34.149
1988	6 158	0	2447529.5	31.857	+33 37.177
1988	6 159	0	2447530.5	32.267	+33 40.205
1988	6 160	0	2447531.5	32.677	+33 43.233
1988	6 161	0	2447532.5	33.087	+33 46.261
1988	6 162	0	2447533.5	33.497	+33 49.289
1988	6 163	0	2447534.5	33.907	+33 52.317
1988	6 164	0	2447535.5	34.317	+33 55.345
1988	6 165	0	2447536.5	34.727	+33 58.373
1988	6 166	0	2447537.5	35.137	+33 61.401
1988	6 167	0	2447538.5	35.547	+33 64.429
1988	6 168	0	2447539.5	35.957	+33 67.457
1988	6 169	0	2447540.5	36.367	+33 70.485
1988	6 170	0	2447541.5	36.777	+33 73.513
1988	6 171	0	2447542.5	37.187	+33 76.541
1988	6 172	0	2447543.5	37.597	+33 79.569
1988	6 173	0	2447544.5	38.007	+33 82.597
1988	6 174	0	2447545.5	38.417	+33 85.625
1988	6 175	0	2447546.5	38.82	

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Lotto									
Year	Month	Day	1	2	3	4	5	6	7
1988	10	11	24474455.5	14 57 - 160	-30 39 - 42	18 59 - 642	-30 36 - 16	1 - 082	1 - 408
1988	10	12	24474465.5	19 .973	-30 43 - 01	19 34 - 50	-30 39 - 54	1 - 089	1 - 410
1988	10	13	24474475.5	19 4 .793	-30 46 - 09	19 72 - 272	-30 42 - 41	1 - 095	1 - 412
1988	10	14	24474485.5	19 8 .619	-30 48 - 65	19 11 - 096	-30 44 - 77	1 - 101	1 - 414
1988	10	15	24474495.5	19 12 .448	-30 50 - 71	19 14 - 924	-30 46 - 61	1 - 108	1 - 416
1988	10	16	24474505.5	19 16 .281	-30 52 - 25	19 18 - 754	-30 47 - 95	1 - 115	1 - 419
1988	10	17	24474515.5	19 20 .115	-30 53 - 28	19 22 - 586	-30 48 - 77	1 - 122	1 - 421
1988	10	18	24474525.5	19 23 .085	-30 56 - 41	19 26 - 416	-30 49 - 27	1 - 128	1 - 424
1988	10	19	24474535.5	19 27 .783	-30 53 - 83	19 30 - 249	-30 49 - 10	1 - 135	1 - 426
1988	10	20	24474545.5	19 31 .615	-30 53 - 35	19 34 - 077	-30 48 - 24	1 - 142	1 - 429
1988	10	21	24474555.5	19 35 .443	-30 52 - 38	19 37 - 902	-30 47 - 07	1 - 150	1 - 431
1988	10	22	24474565.5	19 39 .267	-30 50 - 92	19 41 - 722	-30 45 - 41	1 - 157	1 - 434
1988	10	23	24474575.5	19 43 .085	-30 50 - 97	19 45 - 536	-30 43 - 27	1 - 164	1 - 437
1988	10	24	24474585.5	19 46 .897	-30 46 - 54	19 49 - 342	-30 40 - 65	1 - 170	1 - 440
1988	10	25	24474595.5	19 50 .700	-30 43 - 63	19 53 - 141	-30 37 - 55	1 - 179	1 - 443
1988	10	26	24474605.5	19 54 .495	-30 40 - 26	19 56 - 931	-30 33 - 99	1 - 187	1 - 446
1988	10	27	24474615.5	19 58 .279	-30 36 - 42	20 71 - 1	-30 29 - 96	1 - 194	1 - 449
1988	10	28	24474625.5	20 2 - 053	-30 40 - 0	20 47 - 79	-30 25 - 46	1 - 202	1 - 452
1988	10	29	24474635.5	20 5 - 816	-30 27 - 37	20 8 - 236	-30 20 - 55	1 - 210	1 - 456
1988	10	30	24474645.5	20 9 - 566	-30 22 - 18	20 11 - 980	-30 15 - 17	1 - 218	1 - 459
1988	10	31	24474655.5	20 13 - 303	-30 16 - 55	20 15 - 711	-30 19 - 36	1 - 226	1 - 462
1988	11	1	24474665.5	20 17 .088	-30 10 - 48	20 19 - 428	-30 13 - 13	1 - 235	1 - 466
1988	11	2	24474675.5	20 20 .734	-30 4 - 0	20 23 - 130	-29 56 - 47	1 - 243	1 - 469
1988	11	3	24474685.5	20 24 .426	-29 57 - 09	20 26 - 816	-29 49 - 39	1 - 251	1 - 473
1988	11	4	24474695.5	20 28 .103	-29 49 - 78	20 30 - 06	-29 41 - 91	1 - 260	1 - 476
1988	11	5	24474705.5	20 31 .764	-29 42 - 07	20 34 - 139	-29 34 - 04	1 - 269	1 - 480
1988	11	6	24474715.5	20 35 .406	-29 33 - 96	20 37 - 775	-29 25 - 77	1 - 277	1 - 484
1988	11	7	24474725.5	20 39 .031	-29 25 - 46	20 41 - 393	-29 17 - 13	1 - 286	1 - 488
1988	11	8	24474735.5	20 42 .637	-29 16 - 61	20 44 - 93	-29 8 - 11	1 - 295	1 - 491
1988	11	9	24474745.5	20 46 .225	-29 16 - 25	20 48 - 573	-28 56 - 73	1 - 304	1 - 495
1988	11	10	24474755.5	20 49 .793	-28 57 - 80	20 52 - 35	-28 48 - 99	1 - 313	1 - 499
1988	11	11	24474765.5	20 53 .342	-28 47 - 86	20 55 - 676	-26 38 - 91	1 - 323	1 - 503
1988	11	12	24474775.5	20 56 .870	-28 37 - 59	20 59 - 197	-28 27 - 1	1 - 332	1 - 507
1988	11	13	24474785.5	21 1 - 378	-26 26 - 98	21 2 - 697	-28 17 - 74	1 - 341	1 - 512
1988	11	14	24474795.5	21 3 - 864	-24 16 - 6	21 6 - 176	-28 6 - 66	1 - 351	1 - 516
1988	11	15	24474805.5	21 7 - 330	-26 4 - 82	21 9 - 634	-27 55 - 30	1 - 361	1 - 520
1988	11	16	24474815.5	21 10 - 773	-27 53 - 28	21 13 - 070	-27 43 - 63	1 - 370	1 - 524
1988	11	17	24474825.5	21 14 - 495	-27 41 - 44	21 16 - 484	-27 31 - 67	1 - 380	1 - 528
1988	11	18	24474835.5	21 17 - 594	-27 19 - 33	21 19 - 876	-27 19 - 42	1 - 393	1 - 533
1988	11	19	24474845.5	21 20 - 971	-27 16 - 94	21 23 - 246	-27 6 - 91	1 - 400	1 - 536
1988	11	20	24474855.5	21 24 - 489	-26 11 - 17	21 39 - 751	-26 5 - 58	1 - 452	1 - 542
1988	11	21	24474865.5	21 40 - 752	-27 4 - 28	21 56 - 953	-26 54 - 13	1 - 410	1 - 547
1988	11	22	24474875.5	21 47 - 161	-26 1 - 36	21 63 - 917	-26 21 - 60	1 - 421	1 - 547
1988	11	23	24474885.5	21 34 - 250	-26 38 - 0	21 53 - 218	-26 1 - 431	1 - 431	1 - 551
1988	11	24	24474895.5	21 37 - 513	-26 11 - 17	21 59 - 85	-26 1 - 506	1 - 452	1 - 560
1988	11	25	24474905.5	21 40 - 752	-27 4 - 28	21 61 - 92	-25 46 - 83	1 - 410	1 - 562
1988	11	26	24474915.5	21 43 - 908	-25 43 - 68	21 68 - 192	-25 32 - 45	1 - 421	1 - 567
1988	11	27	24474925.5	21 47 - 161	-25 28 - 98	21 74 - 378	-25 18 - 08	1 - 484	1 - 575
1988	11	28	24474935.5	21 50 - 332	-25 14 - 51	21 52 - 541	-25 3 - 51	1 - 495	1 - 580
1988	11	29	24474945.5	21 53 - 479	-24 59 - 85	21 55 - 682	-24 48 - 75	1 - 506	1 - 585
1988	11	30	24474955.5	21 56 - 604	-24 6 - 66	21 58 - 00	-24 33 - 82	1 - 517	1 - 591
1988	12	1	24474965.5	21 59 - 707	-24 9 - 66	22 1 - 99	-24 18 - 71	1 - 528	1 - 594
1988	12	2	24474975.5	22 2 - 787	-24 14 - 81	22 4 - 99	-24 3 - 44	1 - 539	1 - 600
1988	12	3	24474985.5	22 5 - 845	-24 8 - 021	22 8 - 01	-23 48 - 01	1 - 551	1 - 605
1988	12	4	24474995.5	22 6 - 881	-24 3 - 48	22 11 - 50	-23 32 - 43	1 - 562	1 - 610
1988	12	5	24475005.5	22 11 - 895	-24 1 - 48	22 14 - 508	-23 1 - 47	1 - 573	1 - 617
1988	12	6	24475015.5	22 14 - 087	-24 1 - 48	22 17 - 044	-23 1 - 47	1 - 585	1 - 620
1988	12	7	24475025.5	22 17 - 044	-24 1 - 48	22 21 - 044	-23 1 - 47	1 - 588	1 - 620



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EXPLANATION OF SYMBOLS

THE MAGNETIC TOTAL MAGNITUDE, COMPUTED FROM EMPIRICAL EQUATION BASED UPON PAST OBSERVED BEHAVIOR  
 IMAGE NUCLEAR MAGNITUDE = 15.5 + 5.00 LOG10(DELTA) + .03 BETA  
 IMAGE NUCLEAR MAGNITUDE = 15.5 + 5.00 LOG10(R) + .03 BETA  
 IN CASES WHERE TWAG AND/OR NMAG ARE NOT COMPUTED, THE CORRESPONDING COLUMN(S) ARE FILLED WITH ZEROS (0.0).

$\theta_{\text{HE}}$  = SUN-EARTH-OBJECT ANGLE IN DEGREES  
 $\beta_{\text{HE}}$  = SUN-OBJECT-EARTH ANGLE IN DEGREES  
LAT AND LONG ARE HELIOCENTRIC ECLIPTIC LATITUDE AND LONGITUDE IN DEG., REFERRED TO 1950.0

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P E R I H E L I O N P A S S A G E	2447440.50000	1988	10	6.00000
P E R I H E L I O N D I S T A N C E I N A U	2447421.23687	1988	9	16.73687
E C C E N T R I C I T Y	1.3834294			
E C C E N T R I C I T Y	* 5444427A			
O F P E R I M I L I O N	191.03860			
O N G . O F A S C E N D I N G N O D E	119.11816			
O N C E N T R I C I T Y	12.43190			

EQUATION OF STATE OF 1950-0

PARTIAL AND ELEMENTWISE COMPUTATIONS BY

DR. D.K. YEOMANS  
PROPULSION LAB.  
PASADENA, CALIF. 91103

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