

NASA CR-137553
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ASRL TR 174-2

(NASA-CR-137553) USER'S MANUAL FOR COMPUTER
PROGRAM ROTOR (Massachusetts Inst. of Tech.)
235 p HC \$7.50 CSCL 01B

N75-14725

UIC:148

33/ 2 8233

USER'S MANUAL FOR COMPUTER PROGRAM ROTOR

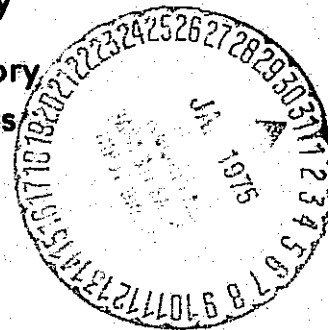
Masahiro Yasue

August 1974



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Prepared under Contract No. NAS2-7262 by
Aeroelastic and Structures Research Laboratory
Department of Aeronautics and Astronautics
Massachusetts Institute of Technology
Cambridge, Massachusetts 02139



for

AMES RESEARCH CENTER
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
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1. Report No. NASA CR-137553		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle USER'S MANUAL FOR COMPUTER PROGRAM ROTOR				5. Report Date August 1974	
				6. Performing Organization Code	
7. Author(s) Masahiro Yasue				8. Performing Organization Report No. ASRL TR 174-2	
9. Performing Organization Name and Address Massachusetts Institute of Technology Aeroelastic and Structures Research Laboratory Cambridge, Massachusetts 02139				10. Work Unit No.	
				11. Contract or Grant No. NAS2-7262	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Moffett Field, California 94035				13. Type of Report and Period Covered Contractor Report	
				14. Sponsoring Agency Code	
15. Supplementary Notes NASA Technical Monitors: J.P. Rabbott, Jr., and Wayne R. Johnson					
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17. Key Words (Suggested by Author(s)) Rotary Wing Dynamics Gust Response Proprotor Tilt-Rotor				18. Distribution Statement Unclassified, Unlimited	
19. Security Classif. (of this report) Unclassified		20. Security Classif. (of this page) Unclassified		21. No. of Pages 234	22. Price*

* For sale by the National Technical Information Service, Springfield, Virginia 22151

FOREWORD

This report has been prepared by the Aeroelastic and Structures Research Laboratory (ASRL), Department of Aeronautics and Astronautics, Massachusetts Institute of Technology, Cambridge, Massachusetts, under NASA Contract No. NAS2-7262 from the Ames Research Center, National Aeronautics and Space Administration, Moffett Field, California 94035. Mr. John Rabbott and Dr. Wayne Johnson of the Ames Research Center served as technical monitors. The valuable assistance and advice received from these individuals is gratefully acknowledged.

The research described in this report was supervised by Professor Norman D. Ham and Associate Professor Pin Tong. The author would like to express his deep appreciation and gratitude for their invaluable advice and guidance throughout this study. The author is also deeply indebted to Professor John Dugundji and to Dr. Wayne Johnson, who contributed various useful suggestions. Professor E.A. Witmer's advice and assistance in various phases of the work is acknowledged gratefully.

The computations were performed at the Information Processing Center of the Massachusetts Institute of Technology.

ABSTRACT

This report presents a detailed description of a computer program to calculate tilt-rotor aircraft dynamic characteristics. This program (named ROTOR) consists of two separate parts. In the first part, the natural frequencies and corresponding mode shapes of the rotor blade and wing are developed from structural data (mass distribution and stiffness distribution). The second part of the program deals with the frequency response (to gust and blade pitch control inputs) and eigenvalues of the tilt-rotor dynamic system, based on the natural frequencies and mode shapes derived beforehand. Sample problems are included to assist the user.

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SECTION 1

INTRODUCTION

1.1 Purpose and Scope

Program ROTOR is an in-core program written in FORTRAN IV language for analysis of the dynamic characteristics of the tilt-rotor aircraft.

The analytical model considered here consists of a cantilevered semispan wing with the engine-rotor system at the wing tip (see Fig. 1 of Ref. 1). The dynamic and aeroelastic characteristics of this aircraft are in many ways unique and complicated. The large flexible blades with a large amount of twist have significant coupling between flapping and lagging motion. The engines and gearboxes at the wing tip lead to low wing natural frequencies and possible resonances in the low frequency range.

The purpose of this program is the numerical analysis of the complicated dynamic and aeroelastic behavior of the tilt-rotor aircraft. The first step is the derivation of the equations of motion of the blade and the wing, including inertia forces, blade aerodynamic forces and wing aerodynamic forces. This formulation is described in detail in Ref. 1. Based on the equations of motion, the frequency response of the blade and wing motions to the gust input or blade pitch angle control input are derived. An eigenvalue analysis provides the system stability characteristics.

1.2 Program Outline and Limitations

Program ROTOR consists of two separate parts. One is called FREEVI (free vibration of the tilt-rotor aircraft), which produces the natural frequencies and mode shapes of the free vibration from the blade or from the wing structural characteristic data. The second part is named TILDYN (tilt-rotor dynamics)

which calculates the dynamic characteristics of the aircraft, including eigenvalues and frequency response to the gust and to the pitch-control inputs.

The reason for the separation of the program into two parts is that this system gives the user the opportunity to check the results for the natural frequencies and mode shapes without performing the entire calculation. In addition, the dynamic characteristics can be evaluated easily by changing the input natural frequencies or using different assumed modes without changing the structural characteristics, mass distribution, or stiffness distribution. The disadvantage is that the input data for TILDYN are the output data of FREEVI.

The free vibration problem of the wing and blade is solved as an eigenvalue problem in FREEVI by the finite element method. The wing has three degrees of freedom, vertical bending, chordwise bending and torsion. A large wing tip mass represents the rotor, engine, and gearbox.

Only flapping and lagging motions are considered for the blade. Torsion is neglected as a higher-order effect for the blade case. The rotor types treated here are the hingeless rotor and the gimbaled rotor. The maximum number of elements is limited to twenty.

With respect to the TILDYN program, it should be mentioned that the flight configuration is restricted to cruising flight only, with the rotor disk plane perpendicular to the free stream. Both powered and autorotation cases can be treated. Total degrees of freedom considered are nine or eighteen for powered flight. The nine degrees of freedom consist of blade flapping and lagging fundamental modes (each has a collective and two cyclic degrees of freedom) and wing vertical bending, chordwise bending, and torsion modes. The eighteen degrees of freedom include two additional blade modes and three additional wing modes. It should be noted

that description of the blade motion requires three independent degrees of freedom to reduce one equation with periodic coefficients in the rotating system to three equations with constant coefficients in the non-rotating system.

In the autorotation case, one more degree of freedom is added, the rigid body rotation of the rotor, and the total degrees of freedom become ten or nineteen. After the construction of the equations of motion for each case, the frequency response problem is solved. The excitation inputs consist of the following: vertical gust, lateral gust, longitudinal gust, collective-blade pitch control and two cyclic blade pitch controls. By appropriately specifying the excitation input components, the flight in a cross-wind gust can be considered.

The eigenvalue problem to be solved is the usual eigenvalue problem of a linear system of equations. The EISPACK subroutine developed by the Argonne Code Center is used to treat this problem (Refs. 2 and 3).

SECTION 2

DESCRIPTION OF THE PROGRAMS

2.1 Description of the FREEVI Program

This program consists of one main program and twelve sub-routines for the computation of the lowest few eigenvalues and eigenvectors of the proprotor dynamic system modelled by the finite-element method, as described in Ref. 1. The outline flow chart is shown in Fig. 1.

Input data include element-structural characteristics (mass distribution, stiffness distribution and angle of twist), rotational speed, and some instruction data for the computation. The boundary conditions are automatically chosen when the calculation case is selected appropriately. Boundary conditions and degrees of freedom are tabulated in Table 1 for the rotor and wing. Next, the element stiffness and mass matrices are assembled globally. From the input information, the boundary conditions are imposed on the global system. The subspace iteration method is applied to find the eigenvalues and eigenvectors of the system (Refs. 4 and 5). Consider the eigenvalue problem of the n-degree-of-freedom equations:

$$[K][u] = \lambda [M][u] \quad (2.1)$$

where $[K]$ and $[M]$ are square stiffness and mass matrices with order n , $[u]$ is a matrix of the mode shape and λ is an eigenvalue. When m eigenvalues and eigenvectors are required, the main steps of the subspace iteration method are as follows:

- (a) Assume mode shape matrix $[u_0]$; $n \times m$ matrix containing m vectors
- (b) $[M_R] = [u_0]^T [M] [u_0]$; $[K_R] = [u_0]^T [K] [u_0]$ where $[M_R]$ and $[K_R]$ are reduced square matrices with order m .

- (c) Find eigenvectors $[A]$ ($m \times m$ matrix) such that $[K_R][A] = [D][M_R][A]$, with $[D]$ denoting a diagonal matrix.
- (d) $[\bar{u}_0] = [u_0][A]$
- (e) $[u_1] = [K]^{-1}[M][\bar{u}_0]$
- (f) $[u_0] = [u_1]$ and go to step (b)

The eigenvalue analysis of the smaller system (order m) in step (c) is achieved by using the Jacobi method. The criterion of terminating the iteration is defined as

$$\left| \frac{\lambda_{i+1} - \lambda_i}{\lambda_i} \right| \leq e \quad (2.2)$$

Each eigenvalue must satisfy this criterion; the error threshold e can be defined by the user.

Output includes the input data, the eigenvalues, the eigenvectors, and, if required, punched-out cards of the eigenvectors. A built-in message as to whether convergence was achieved is also furnished.

A short description of each of the subroutines is given below:

MAIN	Defines dimensions
TEIGEN	Calculates the normal modes and frequencies
INPUT	Supplies input information
ELEMK	Controls the generation of element stiffness and mass matrices
MESH	Calculates mesh information for the finite element assemblage
ASBV	Applies boundary conditions
FAC	Triple matrix factorization
MTRTR	Matrix multiplication
MULTZ	Matrix multiplication
SOLZ	Forward and backward substitution
DNROOT	Eigen-analysis routine
EIGEN	Eigen-analysis routine needed in DNROOT
OUTPUT	Output routine

The listing is shown in Appendix A.

2.2 Description of the TILDYN Program

This program to solve the equations of motion of the tilt-rotor aircraft derived in Ref. 1, consists of one main program and twenty-four subroutine programs. The outline flow chart is shown in Fig. 2.

Input data are natural frequencies and corresponding mode shapes of the rotor and wing, aerodynamic coefficients, and flight conditions.

Based on such input data, the coefficients of the equations of motion are derived, using the numerical integration method. Finally, the equations of motion are formulated as a matrix:

$$[A] \{\ddot{x}\} + [B] \{\dot{x}\} + [C] \{x\} = [D] \{e\} \quad (2.3)$$

[A], [B], [C], and [D] are the coefficient matrices, including inertia terms and aerodynamic terms. The matrix {x} is a set of variables and {e} is an exciting force matrix including gust components and blade pitch-control components (see Ref. 1). These equations have nine or eighteen degrees of freedom in the powered flight case. In the autorotation flight case, ten or nineteen degrees of freedom are required, due to the addition of rigid-body rotation (see Table 2).

The dynamic characteristics of these equations are analyzed by two methods. One is the frequency-response analysis and the other is the eigenvalue analysis. In the frequency-response analysis, the accelerations and velocities of the equations are expressed in terms of a given frequency, and the differential equations are transformed into a set of linear algebraic equations. These linear equations are solved by the Gauss-Jordan reduction to obtain the response to the gust or blade pitch-control input.

The eigenvalue problem is formulated in the usual way. Equation 2.3 is rewritten

$$\begin{Bmatrix} \dot{x} \\ x \end{Bmatrix} = \begin{bmatrix} -A^{-1}B & -A^{-1}C \\ I & 0 \end{bmatrix} \begin{Bmatrix} \dot{x} \\ x \end{Bmatrix} \quad (2.4)$$

to obtain first-order differential equations. The real general matrix eigenvalue problem is solved by the EISPACK package, developed by Argonne National Laboratory to solve a standard matrix eigenvalue-eigenvector problem (Refs. 2 and 3).

A short description for each of the subroutines of the TILDYN program is given below:

MAIN	Defines the sequence of the program
BLOCK DATA	Initializes the coefficients of Gaussian quadrature
INITIL	Initialization of the matrices
COEFF	Defines the points and coefficients of the Gaussian quadrature
INPUT	Supplies input information
INTPL	Interpolation for the numerical integration by Gaussian quadrature
AERO	Defines the aerodynamic coefficients at the points of Gaussian quadrature
ORDINT	Defines the order of the numerical integration
INTEG	Numerical integration
F	Defines the integrand function
AINER	Defines the inertia coefficients of the equations in matrix form
AEROMT	Defines the aerodynamic coefficients of the equations in matrix form
EQMTX	Defines the coefficient matrices [A], [B], [C], and [D] in Eq. 2.3.
AUTO	In the autorotation case, another degree of freedom is added

GUSTCO	Defines gust and blade pitch control components
FRQRES	Calculates the frequency response
GAELI	The Gauss-Jordan reduction routine
EIGEN	Routine to form the eigenvalue problem and to call EIPACK subroutine
EIPACK	An eigensystem problem solver for the real general matrix consisting of EISPACK subroutine BALANC, ELMHES, ELTRAN, HQR2 and BALBAK
BALANC	Balances a real general matrix and isolates eigenvalues whenever possible
ELMHES	Obtains an upper Hessenberg matrix from a real general matrix
ELTRAN	Accumulates the elementary similarity transformations for the reduction to upper Hessenberg form
HQR2	Finds the eigenvalues and eigenvectors
BALBAK	Forms the eigenvectors by back-transforming those of the corresponding balanced matrix determined by BALANC
MINV	Inverses a matrix

The listing is shown in Appendix A.

SECTION 3
USER'S GUIDE FOR FREEVI PROGRAM

3.1 Input Data Requirements

The input and output of the computer code is a part of the built-in program with fixed format. This approach requires a minimum knowledge of the programs and programming.

The finite-element model for the input data is shown in Fig. 3. The structure is divided into several elements for application of the finite-element method. The mass distribution, bending and torsional stiffness, and angle of twist are the average values in the element. The unit system used should be consistent throughout the entire program.

This program calculates the natural frequencies and normal modes for five cases, including wing vibration and blade vibration with various boundary conditions (see Table 1). The parameter ICASE specifies the particular case in the program. The parameter IPUNCH specifies whether a punched card deck of the mode shapes is required for input to the program TILDYN.

Uncoupled mode shapes, instead of coupled mode shapes, can be generated, if necessary. The parameter IGUEST controls the initial assumed values for the purpose of generating the uncoupled mode shapes.

The value of M expresses the number of eigenvalues and mode shapes required by the user.

Parameters and variables are described in detail below:

DES A vector to express the test identifying information.
 The user can punch the run identification in the first column through the eightieth column of the first card. The format is 20A4.

ICASE A parameter to specify the calculation case:

ICASE=1; wing case with clamped boundary conditions at the root.

ICASE=2; blade case with boundary conditions clamped for the flapping motion and clamped for the lagging motion at the root.

ICASE=3; blade case, clamped for flapping and hinged for lagging.

ICASE=4; blade case, hinged for flapping and clamped for lagging.

ICASE=5; blade case, both hinged boundary conditions.

It is punched in the integer format as I1 in the first column of the second card.

IPUNCH A parameter to control whether the mode shapes are punched out in cards for input to the TILDYN program.

IPUNCH=0; no punched output

IPUNCH=1; punched output

The parameter is punched in the integer format as I1 in the first column of the third card.

IGUEST A parameter to control the mode-shape type coupled or uncoupled, both for the blade and the wing.

IGUEST=0; coupled

IGUEST=1; uncoupled vertical bending (w)

IGUEST=2; uncoupled chordwise bending (v)

IGUEST=3; uncoupled torsion (ϕ)

It should be noted that the terms PB, RAMDA, COL and THETAE related to coupled motion should be set to zero when uncoupled mode shapes are required. The parameter is punched in the integer format as I1 in the first column of the fourth card.

NET Total number of elements, maximum number is 20. It is punched out in the integer format as I5 in the first through fifth columns in the fifth card.

NITR The maximum number of iterations to be performed. If the number of iterations reaches NITR, yet the iteration is not converged, the program execution is terminated and a built-in message appears. Recommended value for NITR is 20. It is punched in the integer format as I5 in the 6th through the 10th columns of the fifth card.

M Number of vibration modes required by the user. Recommended value for M is less than 10. If $M = 10$ to 20, NITR is recommended to be 50.

ERR The error limit used to compare with $|(\lambda_{i+1} - \lambda_i)/\lambda_i|$, where λ_i is the eigenvalue calculated at the i th iteration cycle. The iteration terminates if the calculated value is smaller than ERR. Recommended values for ERR are 0.001 to 0.01. It is punched in the real value format (F10.6) at the first through 10th columns of the sixth card.

OMEG Rotational speed Ω in rad/sec, the direction of rotation is positive for the upward rotational vector when the aircraft configuration is in the helicopter mode. For the wing or non-rotating blade it is set to zero. It is punched in real value format (F10.6) in the first through the 10th columns of the seventh card.

RAMDA Inflow ratio λ is defined as $(V + v)/\Omega R$. It determines the collective pitch of the blade.

For the wing and non-rotating blade, it is set to zero. It is punched in real value format (F10.6) in the first through the 10th columns of the 8th card.

COL Collective pitch angle in radians (θ_D in Ref. 1). For the wing case it is set to zero. It is punched in real value format (F10.6) in the first through the 10th columns of the 9th card.

SPKB The flapwise spring constant at the root of the hinged rotor. If there is no spring, it is set to zero. It is punched in real value format (F10.6) in the 1st through the 10th columns of the 10th card.

SPKC The lagwise spring constant at the root of the hinged rotor. If there is no spring, it is set to zero. It is punched in real value format (F10.6) in the 11th through 20th columns of the 10th card.

ALPHAH The number is used to avoid a singularity of the stiffness matrix in the case of the hinged blade. The recommend value for ALPHAH is the squared value (λ^2) of the first non-zero eigenvalue. The value 5000.0 is appropriate for the first trial. It is punched in real value format (F10.6) in the first through the 10th columns of the 11th card.

EIBE A vector to express the vertical bending stiffness $(EI)_B$ of the element. The length of the vector equals NET. It is punched in the exponent format (E15.7) and five data items can be included per card. These data occupy the 12th card through card $[10+(NET/5)]$ if NET is a multiple of 5. Otherwise, up to card $[11+(NET/5)]$ is occupied.

EICE A vector to express the chordwise bending stiffness $(EI)_C$ of the element. The length of the vector is NET. It is punched in the exponent format (E15.7) and five data items can be included in a card. These data occupy $(NET/5)$ cards if NET is a multiple of 5, otherwise $[1+(NET/5)]$ cards.

THETAE A vector to express the angle of twist θ_{AT} in radians of the structure element, positive nose up. It should be the average angle of twist over the element. The length of the vector is NET. Eight data items can be punched in real value format (F10.6) in each card. These data occupy (NET/8) cards if NET is a multiple of 8, otherwise $[1+(NET/8)]$ cards.

AMASE A vector to describe the mass distribution (mass/unit length); its length is NET. It is punched in real value format (F10.6), 8 data items on one card. These data occupy (NET/8) cards if NET is a multiple of 8, otherwise $[1+(NET/8)]$ cards.

ESE A vector to define the size of the beam element of the blade or wing and its length is NET. It is punched in real value format (F10.6), 8 data items on a card. These data occupy (NET/8) cards if NET is a multiple of 8, otherwise $[1+(NET/8)]$ cards.

AMN The number to express the tip mass. In the case of the wing, it includes the nacelle and all blade mass as

$$AMN = M_N + NM_B$$

in the symbols of Ref. 1. If a tip mass exists in the blade, it is also appropriate to use AMN. It is punched in real value format (F10.6) in the first through the 10th columns of the card. The next four numbers PIR, PIY, PIP and PBW are punched on the same card with AMN.

PIR A number to express the rolling moment of inertia of the nacelle and blades at the wing tip:

$$PIR = I_{P_r} + NI_B$$

The format is (F10.6) and it is punched from the 11th to 20th columns.

PIY A number to express the yawing moment of inertia of the nacelle and blades at the wing tip:

$$PIY = I_{P_y} + \frac{N}{2} I_B + NM_B h^2$$

The format is (F10.6) and it is punched from the 21st to the 30th columns.

PIP A number to express the pitching moment of inertia of the nacelle and blades at the wing tip:

$$PIP = I_{P_p} + \frac{N}{2} I_B + NM_B h^2$$

The format is (F10.6) and it is punched from the 31st to the 40th columns.

PBW A number to express the mass coupling effect at the tip between the wing vertical bending and the torsion due to blade mass:

$$PBW = NM_B h$$

The format is (F10.6) and it is punched from the 41st to the 50th columns.

If the calculation case is the wing (ICASE=1), the next three data cards should be added:

GJ A vector to express the torsional rigidity: its length is NET. The format is (E15.7) and five data items can be included in a card. These data occupy (NET/5) cards if NET is a multiple of 5, otherwise [1+(NET/5)].

PI A vector to express wing mass moment of inertia about the elastic axis per unit length: its length is NET. The format is (E15.7) and five data items can be included in a card. These data occupy (NET/5) cards if NET is a multiple of 5, otherwise [1+(NET/5)].

PI12 A vector to express wing static mass moment of the segment to define the coupling motion between wing vertical bending and torsion. The vector length is NET and the format is (E15.7). Five data items can be included in a card and data occupy NET/5 cards if NET is a multiple of 5, otherwise $[1+(NET/5)]$.

The data deck setup is shown in Fig. 5 and the example problem data listing is in Appendix B.

A few remarks will now be stated to avoid misuse of the program:

- 1) A consistent unit system must be adopted.
- 2) The maximum element number (NET) is 20.
- 3) Appropriate rotor rotational direction must be chosen. If OMEG is negative, RAMDA (inflow ratio) should be negative. However, COL (the collective pitch) and THETAE (angle of twist) should be positive nose up.
- 4) If uncoupled mode shapes are required, the coupling terms such as RAMDA, COL, THETA, PBW and PI12 should be set to zero.
- 5) If there are several cases to be dealt with, the data may consist of several data sets. After the execution of the first case, the computer automatically returns to the beginning of the program and reads the second input data set. Therefore, at the end of the entire calculation, the computer notes the absence of data sets and generates an error message.

3.2 Output Features

All input data are printed out for checking. The built-in messages and outputs in the FREEVI program are as follows:

- (a) TENSION DUE TO CENTRIF. FORCE

This prints out the tension force at each nodal

(b) MASS = 0.XXXXXXXXX

This indicates the total mass of the blade or wing.

(c) MOMENT OF INERTIA AT ROOT = 0.XXXXXXXXX

This gives the mass moment of inertia of the blade or wing about the virtual hinge at the root.

(d) MAX. SIZE OF STF IS XXX SPECIFIED SIZE IS XXX

This prints out the specified value of the estimated length of the stiffness matrix and the actual required value for the stiffness matrix. If the specified value is smaller, the program stops. Check the input. If the required value is smaller, no remedy is needed.

(e) THE XXXXTH DIAG. AFTER FACT=0.0, INCOMPLETE FACT

This message appears when the factorization of the mass matrix is not complete. The program also stops. Check the input.

(f) NO. OF NEGATIVE DIAG. = XXXX, FACT COMPLETED

This prints out the number of negative diagonals of the factorized mass matrix. If the printed value is other than zero, the mass matrix is not positive definite. Check the input data.

(g) EIGENVALUES =

At each iteration, calculated eigenvalues are printed out. If eigenvalues satisfy the accuracy requirements, these results are printed out in eigenvalue format (the square value of the natural frequency), radian/second and Hertz.

(h) NO. OF ITERATION = XXXX CONVERGED WITHIN 0.XXXXXXXXX

This indicates that the subspace iteration is completed. The first value printed is the number of the

iteration and the second value is the error limit input by the user.

(i) NO. OF ITERATION = XXXX NOT CONVERGED

This appears instead of (h) message if the user specified maximum number of iterations (NITR) has been reached, yet the eigenvalues have not converged to within the error limit set by the user. The user should check the input for possible errors or change the error limit (ERR) because the previous error limit may be too small to be achieved, or increase the maximum number of iteration (NITR).

(j) REDUCED MASS MATRIX

The lower triangular part of the reduced mass matrix is printed out.

(k) REDUCED STIF MATRIX

The lower triangular part of the reduced stiffness matrix is printed out.

(l) ****BLADE MODE SHAPES**** or ****WING MODE SHAPES****

Mode shapes are printed out. Index I indicates the eigenvalue to which the mode shape corresponds and index J indicates the station number of the node. Symbols $W(I,J)$, $V(I,J)$, $PW(I,J)$, and $DV(I,J)$ are vertical bending (flapping motion), chordwise bending (lagging motion), slope of the vertical bending, and slope of the chordwise bending, for the case of blade vibration. In addition to those symbols, $\text{PHI}(I,J)$ and $\text{DPHI}(I,J)$ are used for the torsion and slope of the torsion for the wing vibration. The coordinate system is shown in Fig. 4.

(m) Punched Card Output

If IPUNCH is set equal to one, the punched card output is also performed. The format is E13.5 with six data items on a card. The order is $W(1,1)$ of the first mode to last $W(1,NET+1)$, punched on $[(NET+1)/6]$ cards if $(NET+1)$ is a multiple of 6, otherwise $[(NET+1)/6+1]$ cards. Next $V(1,J)$, $DW(1,J)$ and $DV(1,J)$ groups are punched. After the first mode shape the group of the second mode shape is punched and it continues to the Mth mode shape. In the case of the wing, the output data of $\Phi(I,J)$, $D\Phi(I,J)$ are added in the same fashion after the set of $DV(I,J)$.

3.3 Example Problems

Example problems cited here for the FREEVI program are taken from Ref. 1.

3.3.1 Application to the Wing

The free vibration of the Bell wing is considered in this report. Structural characteristics (mass distribution, bending stiffness and so on) are shown in Fig. 6. Mass moments of inertia of the nacelle and blades are tabulated in the "Bell" column of Table 3. The listing of both input and output are shown in Appendix B.

3.3.2 Application to the Blade

The hingeless rotor of the Boeing Vertol is studied here. It should be noted that the rotation direction is negative in this case. Structural characteristics are shown in Fig. 7. The listing of both input and output are shown in Appendix B.

SECTION 4

USER'S GUIDE FOR THE TILDYN PROGRAM

4.1 Input Data Requirements

This program has several parameters to designate the case being considered by the user. The first one is ITYPE, which specifies whether collective mode shapes of the blade different from the cyclic mode shapes are needed. If it is the gimballed rotor, the parameter instructs the computer to read more data for the collective mode shapes of the gimballed rotor. The parameter IPLT defines whether the case considered is powered flight or autorotation flight. The next parameter IDOF specifies the number of degrees of freedom. If it is nine, two blade modes (giving six degrees of freedom in the non-rotating system) and three wing modes are necessary. If IDOF is eighteen, two more modes for the blade and three more modes for the wing should be added to the nine degrees-of-freedom system. The parameter IRES specifies execution of the frequency response analysis. The user should decide whether the response based in terms of normal mode shapes or in terms of mode shapes normalized to unity at the blade tip. This is determined by the parameter IFRMAG. The last parameter IEIGEN specifies execution of the eigenvalue analysis.

Parameters and variables are described in input order below:

- DES A vector to express the test identifying information.
 The user can punch the run identification in the first
 column through the eightieth column of the first card.
 The format is 80A1.
- ITYPE A parameter to control the reading of input data depending
 upon the type of rotor.
- ITYPE=0; the hingeless rotor in powered flight
 ITYPE=1; the hingeless rotor in autorotational
 flight.
- the gimballed rotor both in powered and
 autorotational flight.

The format is (I1) and it is punched in the first column of the second card.

IFLT A parameter to determine the flight condition.

IFLT=0; powered flight

IFLT=1; autorotation flight

The format is (I1) and it is punched in the first column of the third card.

IDOF A parameter to define the number of basic elastic deformation degrees of freedom and how many mode shapes are needed. It should be noted that the same number IDOF is used for both powered flight and autorotation flight.

IDOF=9; In the powered flight case, nine equations are constructed and two mode shapes for the blade and three mode shapes for the wing are necessary. In the autorotation flight (IFLT=1), ten equations are constructed, due to the addition of the rigid-body rotation of the blades.

The same number of mode shapes as for the powered flight is necessary.

IDOF=18; In powered flight, eighteen equations are formulated. In autorotation flight they become nineteen. In total, four mode shapes are necessary for the blade and six for the wing.

The format is (I1) and it is punched in the first two columns of the fourth card.

IRES A parameter to control whether the frequency response analysis is carried out.

IRES=0; it is not carried out.

IRES=1; it is carried out.

The format is (I1) and it is punched in the first column of the fifth card.

IFRMAG A parameter to control the type of mode shapes used for the output results.

IFRMAG=0; the frequency response and eigenvector results are based on mode shapes as follows: the predominant components of the blade-coupled-mode shape are normalized to R (rotor radius) at the maximum deflection point. The wing-bending-mode shapes are normalized to L (wing semispan) at the the maximum deflection point, and the wing-torsion-mode shape is normalized to unity at the maximum deflection point. This type of normalization is for the purpose of obtaining results comparable with those described in Ref. 6.

IFRMAG=1; the frequency response and eigenvector results are based on the normal modes used as input data.

The format is (I1), and it is punched out in the first column of the sixth card.

IEIGEN A parameter to control whether the eigenvalue analysis is executed.

IEIGEN=0; it is not executed.

IEIGEN=1; it is executed.

The format is (I1) and it is punched in the first column of the seventh card.

NOBLD The blade number. The format is (I1) and it is punched in the first column of the eighth card.

ROH The air density. The format is (E10.0); the user can put a datum in either F format or E format in the first ten columns of the ninth card.

- OMEGA The rotor rotational speed (radian/sec). The format is E10.0; the user can choose either E or F type. The datum is put in the eleventh column through the twentieth column of the ninth card. OMEGA can take positive or negative values corresponding to the rotational direction. The sign definition is the same as that of the FREEVI program.
- RAMDA The inflow ratio. The sign should be consistent with the rotational direction of the rotor. The format is either in E or F type. The datum is put in the 21st through 30th column of the ninth card.
- VEL The cruising speed of the aircraft. The format is either E or F type. The datum is put in the 31st through the 40th column of the ninth card.
- R The blade radius. The format is either E or F type. It is punched in the first through the tenth column of the tenth card.
- AIB The blade flapping moment of inertia. The format is either E or F type. It is punched in the eleventh through the 20th column of the tenth card.
- CHOD The mean chord length of the blade. The format is either E or F type. It is punched in the 21st through the 30th column of the tenth card.
- CL The lift-curve slope of the blade. The format is either E or F type. It is punched in the 31st through the 40th column of the tenth card.
- CD The drag coefficient of the blade (C_{D_0}). The format is either E or F type. It is punched in the 41st through the 50th column of the tenth card.

- HMAST The mast height. The format is either E or F type. It is punched in the 51st through the 60th column of the tenth card.
- DEL3 The rotor blade pitch-flap coupling (δ_3). The unit is radians. The format is either E or F type. It is punched in the 61st through the 70th column of the tenth card.
- WL The wing semispan length. The format is either E or F type. It is punched in the first through the tenth column of the eleventh card.
- WCOD The mean wing chord length. The format is either E or F type. It is punched in the eleventh through the 20th column of the eleventh card.
- WCL The wing lift curve slope. The format is either E or F type. It is punched in the 21st through the 30th column of the eleventh card.
- WCD The wing drag coefficient (C_{D_0} of the wing). The format is either E or F type. It is punched in the 31st through the 40th column of the eleventh card.
- WCMO The wing pitching moment coefficient (C_{m_0}). The format is either E or F type. It is punched out in the 41st through the 50th column of the eleventh card.
- WCMA The wing pitching moment curve slope (C_{m_α}). The format is either E or F type. It is punched in the 51st through the 60th column of the eleventh card.
- EDIS The distance (nondimensionalized by the wing chord) between the elastic axis and the aerodynamic center of the wing (positive if the aerodynamic center is ahead of the elastic axis). The format is either E or F type. It is punched in the 61st through the 70th column of the 11th card.

WTHET The wing trim angle of attack in radians. The format is either E or F type. It is punched in the 71st through the 80th column of the eleventh card.

CGUST A vector to express the magnitudes of the exciting force components shown in Eq. 2.3 as {e}.

CGUST(1); vertical gust u_G/V

CGUST(2); lateral gust v_G/V

CGUST(3); longitudinal gust w_G/V

CGUST(4); collective pitch control θ_o

CGUST(5); cyclic cosine pitch control θ_{1c}

CGUST(6); cyclic sine pitch control θ_{1s}

If the user specifies 1.0 for one of these quantities, that gust or pitch control quantity becomes the exciting force. Each vector component has either E or F format and occupies ten columns each of the twelfth card.

BRAM A vector to express the blade eigenvalues and its length is 4. The values are the squared values of the natural frequencies ($\text{rad}^2/\text{sec}^2$). If IDOF is set equal to 9, the latter two eigenvalue columns may have blanks. If the calculation case is the gimballed rotor (ITYPE=1), BRAM should include the cyclic mode eigenvalues of the blade. The format is either E or F type and each component occupies ten columns in order of the 13th card.

WRAM A vector to express the wing eigenvalues and its length is 6. The values are the squared values of the natural frequencies ($\text{rad}^2/\text{sec}^2$). If IDOF is set equal to 9, the latter three eigenvalue columns may have blanks. The format is either E or F type and each component occupies ten columns in order of the 14th card.

NW A number to specify the wing element quantity. The format is (I2) and it is punched in the first two columns of the 15th card.

- EMSW A vector to describe the wing element size. The vector length is NW and the element size, nondimensionalized by the wing semispan, should be input. The format is either E or F type (E10.0). Each vector component occupies ten columns from the 16th card. The number of the card for EMSW is NW/8 if NW is a multiple of 8. Otherwise [(NW/8) + 1] cards.
- G A matrix to describe the wing vertical bending mode shape (γ in Ref. 1) at the nodes. The size of the matrix is $MW \times (NW+1)$, where MW is 3 if IDOF=9 and 6 if IDOF=18. The format is E or F type (E13.5) and G(1,1) expresses the vertical deflection at the root node of the first mode. G(1,NW+1) is the one at the tip node of the first mode (Fig. 4). The data should be punched in order from the root node to the tip node value. One card can include 6 data.
- Z A matrix to describe the wing chordwise bending mode shape (ζ in Ref. 1) at the node. Other comments are the same as for G.
- DG A matrix to describe the wing vertical bending slope ($d\gamma/dy$ in Ref. 1). Other comments are the same as for G.
- DZ A matrix to describe the wing chordwise bending slope ($d\zeta/dy$ in Ref. 1). Other comments are the same as for G.
- WPHI A matrix to describe the wing torsion deflection (ϕ in Ref. 1). Other comments are the same as for G.
- DWPHI A matrix to describe the wing torsion slope ($d\phi/dy$ in Ref. 1). Other comments are the same as for G.

The output of the FREEVI program automatically satisfies the deck setup for the TILDYN program, but for convenience the card setup for the wing mode shapes are repeated as follows:

1st card contains G(1,1), G(1,2)..... G(1,6)
 Next card contains G(1,7)G(1,NW+1)
 New card contains Z(1,1)..... Z(1,6)
 Z(1,7)..... Z(1,NW+1)
 New card contains DG(1,1).....
 DG(1,7).....
 New card contains DZ(1,1).....
 DZ(1,7).....
 New card contains WPHI(1,1).....
 WPHI(1,7).....
 New card contains DWPHI(1,1).....
 DWPHI(1,7).....
 New card contains G(2,1)..... G(2,6)
 G(2,7)
 Z(2,1)
 Z(2,7)
 .
 .
 New card contains DWPHI(MW,1).....
 Last card for the wing mode shape contains DWPHI(MW,7) ...
 DWPHI(MW,NW+1)

The wing mode shapes occupy N_w cards where

$$N_w = \begin{cases} 6MW[(NW+1)/6] & \text{if } (NW+1) \text{ is a multiple of } 6 \\ 6MW[(NW+1)/6+1] & \text{if } (NW+1) \text{ is not a multiple of } 6 \end{cases}$$

N A number to specify the blade element quantity. The format is (I2) and it is punched in the first two columns of the next card to the wing mode shapes.

EMS A vector to describe the blade element size. The vector length is N and the element size, nondimensionalized by the rotor radius, should be input. The format is either E or F type (E10.0). Each vector component occupies ten columns, and the card number is $N/8$ if the N is a multiple of 8. Otherwise $[N/8+1]$ cards.

AMASS A vector to describe the mass distribution of the blade. The vector length is $(N+1)$. The value should be the mass distribution (mass per unit length) expressed at the node. The format is either E or F type (E10.0). Each vector component occupies ten columns, and the card number is $(N+1)/8$ if $(N+1)$ is a multiple of 8. Otherwise $[(N+1)/8+1]$ cards.

THETN A vector to describe the angle of twist of the blade. The vector length is $(N+1)$. The value should be the angle of twist at the node and positive nose up. The format is either E or F type (E10.0). Each vector component occupies ten columns, and the card number is $(N+1)/8$ if $(N+1)$ is a multiple of 8. Otherwise, $[(N+1)/8+1]$ cards.

COL A number to express the collective pitch angle (θ_D in Ref. 1) defined from the performance (trim) calculation. The format is either E or F type (E10.0), and it occupies the first ten columns of the next card to THETN.

W A matrix to describe the blade out-of-plane bending mode shape (W_j in Ref. 1) at the node. The size of the matrix is $MB \times (N+1)$ where MB is 2 if $IDOF=9$ and 4 if $IDOF=18$. The format is E or F type (E13.5) and $W(1,1)$ expresses the out-of-plane deflection at the root node of the first mode. $W(1,N+1)$ is the one at the tip node of the first mode. The data should be punched in order from the root node to the tip node value. One card can include 6 data.

- V A matrix to describe the blade inplane bending mode shape (V_j in Ref. 1) at the node. Other comments are the same as those for W.
- DW A matrix to describe the blade out-of-plane bending mode shape slope (dW_j/dr in Ref. 1) at the node. Other comments are the same as those for W.
- DV A matrix to describe the blade inplane bending mode shape slope (dV_j/dr in Ref. 1) at the node. Other comments are the same as those for W.

If the calculation case is the gimbaled rotor (ITYPE=1), or autorotational flight (ITYPE=1 and IFLT=1), the above blade-mode shapes correspond to the cyclic mode shapes.

The output of the FREEVI program automatically satisfies the deck setup for the TILDYN program; however, for convenience, the card setup for blade mode shapes is repeated below:

```

1st card contains W(1,1), W(1,2), .....W(1,6)
Next card contains W(1,7).....W(1,N+1)
New card contains V(1,1).....
                   V(1,7).....
                   DW(1,1) .....
                   DW(1,7) .....
                   DV(1,1)           DV(1,6)
                   DV(1,7)..... DV(1,N+1)
                   W(2,1) .....
                   W(2,7) .....
                   V(2,1).....
                   V(2,7).....
                   .
                   .
                   .
                   .
                   .
                   DV(MB,1) .....
```

Last card contains DV(MB,7) DV(MB,N+1)

The blade mode shapes occupy n_B cards where

$$n_B = \begin{cases} 4MB[(N+1)/6] & \text{if } (N+1) \text{ is a multiple of } 6 \\ 4MB[(N+1)/6+1] & \text{if } (N+1) \text{ is not a multiple of } 6 \end{cases}$$

If the computer calculation case is the gimballed rotor (ITYPE=1) or autorotational flight (ITYPE=1 and IFLT=1), the next five data cards as for the collective mode shapes of the blade should be added.

BRAMO A vector to express the blade collective mode eigenvalues and its length is 4. The values are the squared values of the natural frequencies ($\text{rad}^2/\text{sec}^2$). If IDOF is set equal to 9, the latter two eigenvalue columns may have blanks. The format is either E or F type and each vector component occupies ten columns in order of the next card to the blade mode shapes.

WCOL A matrix to describe the blade collective out-of-plane bending mode shape (W_j^0 in Ref. 1) at the node. The size and other comments are the same as those for W.

VCOL A matrix to describe the blade collective inplane bending mode shape (V_j^0 in Ref. 1) at the node. Other comments are the same as those for W.

DWCOL A matrix to describe the blade collective out-of-plane mode shape slope (dW_j^0/dr in Ref. 1). Other comments are the same as those for W.

DVCOL A matrix to describe the blade collective inplane mode shape slope (dV_j^0/dr in Ref. 1). Other comments are the same as those for W.

The data deck setup is shown in Fig. 8, and an example problem data listing is given in Appendix B.

A few notes to supplement the input data definitions:

- a) The maximum element number (N or NW) is 20
- b) If rotor rotational direction is negative, RAMDA should be negative. However, THETN and COL are positive nose up as in the FREEVI program.
- c) The mode shapes used in the TILDYN program should be defined as normal modes. Those definitions appear in Eq. 4.7 for the blade and in Eq. 4.12 for the wing in Ref. 1. If modes are not normalized in this way, the calculation will give wrong answers.
- d) Output mode shapes from the FREEVI program sometimes include unnecessary mode shapes; for example, the rigid body mode for the collective mode shapes of the gimbaled rotor if the user uses the clamped boundary condition for the flapping motion and the hinged boundary condition for the lagging motion to derive the collective mode for autorotational flight.
- e) If there are several cases, the data may consist of several data sets. The computer execution continues until it finds the absence of data.

4.2 Output Features

In the output, the identifying title is printed first, as punched in by the user. All input data are printed out below.

After the mode shape listing, the matrices A, B, C, and D of the equations of motion in Eq. 2.3 are listed. When the degrees of freedom of the equations are 18 or 19, the first 9 columns of the coefficient matrix are printed out, followed by the latter 9 or 10 columns of the matrix.

If the user has chosen the frequency response analysis (IRES=1), the results of that calculation appear next. Each

response magnitude is showed corresponding to a nondimensional frequency. If IFRMAG is set equal to zero, the response magnitudes are based on the mode shapes normalized to rotor radius and wing semispan (refer to the explanation of IFRMAG in Section 4.1). In autorotation flight, the rigid-body rotation response is added to the basic form. It should be noted that the rigid-body rotation response is the rotational speed perturbation response, not the deflection response. Therefore, it is termed $D(NUR)/DT$ (to express \dot{v}_R).

The eigenvalue analysis consists of the eigenvalue and eigenvector listing. All eigenvalues of the system are printed in the form of complex values with damping ratios, including pairs of complex conjugate values. The eigenvectors corresponding to the eigenvalue are printed. The maximum absolute values of the eigenvector components are normalized to unity. Real parts and imaginary parts express the phase angle between each eigenvector component. If IFRMAG is set to zero, the eigenvectors are expressed based on the mode shapes normalized by rotor radius and wing semispan (refer to the explanation of IFRMAG in Subsection 4.1) as in the frequency response. On the other hand, if IFRMAG is set to unity, all are in length, except v_R (rigid-body rotation in autorotation flight). v_R is an angle, in radians. Therefore, some attention should be paid to comparing the role of each eigenvector.

Only one built-in message is furnished for this program. If an error occurs in the eigenvalue analysis, the message below is automatically printed out after the title "EIGENVALUES":

IERROR=XXXXX

The error code is shown as follows:

<u>Value of IERROR</u>	<u>Error Significance</u>
I	The calculation of the Ith eigenvalue failed to converge. Eigenvalues I+1 ... N should be correct.
-I	The calculation of one or more eigenvectors, including the Ith, failed to converge. All eigenvalues and non-zero eigenvectors are correct.

4.3 Example Problems

Sample problems are carried out here for the Bell and Boeing tilt rotor wings. The flight condition is normal level flight cruising (around 200 kt) at sea level. The detail data is shown in Table 3. The input data listing in Appendix B includes the autorotation flight case for the Bell model and the powered flight case for the Boeing model. However, the output listing of only the Bell autorotation flight case is shown as an example in Appendix B.

REFERENCES

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5. Rutishauser, H., "Computational Aspects of F.L. Bauer's Simultaneous Iteration Method", Numerical Method, Vol. 13, 1969, pp 4-13.
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TABLE 1 BOUNDARY CONDITIONS AND OUTPUT DEFLECTIONS OF THE ROTOR AND WING IN THE FREEVI PROGRAM

	BOUNDARY CONDITIONS			OUTPUT DEFLECTIONS
	ROOT		TIP	
Wing	Clamped for all Deflections		Lumped Mass with Mass and Mass Moment of Inertia	Vertical Bending Chordwise Bending Torsion
Blade				
Powered				
Hingeless Rotor	Clamped for all Deflections		Free or Tip Mass if Necessary	Out-of-Plane Bending Inplane Bending
Gimballed Rotor				
Collective Mode	Clamped for all Deflections		"	"
Cyclic Mode	Hinged for Flapping, Clamped for Lagging		"	"
Autorotation				
Hingeless Rotor				
Collective Mode	Clamped for Flapping, Hinged for Lagging		"	"
Cyclic Mode	Clamped for all Deflections		"	"
Gimballed Rotor				
Collective Mode	Clamped for Flapping, Hinged for Lagging		"	"
Cyclic Mode	Hinged for Flapping, Clamped for Lagging		"	"

TABLE 2 DESCRIPTION OF VARIABLES

(a) Description of {x} in Eq. 2.3

Total Degrees of Freedom				Description
Powered Flight		Autorotation Flight		
9 DOF	18DOF	10DOF	19DOF	
Q_{10}	Q_{10}	Q_{10}	Q_{10}	Blade Collective Motion of 1st Natural Frequency
Q_{1c}	Q_{1c}	Q_{1c}	Q_{1c}	Blade Cyclic Cosine Motion of 1st Natural Frequency
Q_{1s}	Q_{1s}	Q_{1s}	Q_{1s}	Blade Cyclic Sine Motion of 1st Natural Frequency
Q_{20}	Q_{20}	Q_{20}	Q_{20}	Blade Collective Motion of 2nd Natural Frequency
Q_{2c}	Q_{2c}	Q_{2c}	Q_{2c}	Blade Cyclic Cosine Motion of 2nd Natural Frequency
Q_{2s}	Q_{2s}	Q_{2s}	Q_{2s}	Blade Cyclic Sine Motion of 2nd Natural Frequency
	Q_{30}		Q_{30}	Blade Collective Motion of 3rd Natural Frequency
	Q_{3c}		Q_{3c}	Blade Cyclic Cosine Motion of 3rd Natural Frequency
	Q_{3s}		Q_{3s}	Blade Cyclic Sine Motion of 3rd Natural Frequency
	Q_{40}		Q_{40}	Blade Collective Motion of 4th Natural Frequency
	Q_{4c}		Q_{4c}	Blade Cyclic Cosine Motion of 4th Natural Frequency
	Q_{4s}		Q_{4s}	Blade Cyclic Sine Motion of 4th Natural Frequency
a_1	a_1	a_1	a_1	Wing Motion of 1st Natural Frequency
a_2	a_2	a_2	a_2	Wing Motion of 2nd Natural Frequency
a_3	a_3	a_3	a_3	Wing Motion of 3rd Natural Frequency
	a_4		a_4	Wing Motion of 4th Natural Frequency
	a_5		a_5	Wing Motion of 5th Natural Frequency
	a_6		a_6	Wing Motion of 6th Natural Frequency
		\bar{v}_R	v_R	Rotor Rigid-Body Rotation

TABLE 2 CONCLUDED

(b) Description of {e} in Eq. 2.3

Symbol	Description
u_G/V	Nondimensional Vertical Gust
v_G/V	Nondimensional Lateral Gust
w_G/V	Nondimensional Longitudinal Gust
θ_o	Collective Pitch Control
θ_{1c}	Lateral Cyclic Pitch Control
θ_{1s}	Longitudinal Cyclic Pitch Control

TABLE 3

DESCRIPTION OF THE BELL AND THE BOEING PROPROTOR DESIGNS
IN POWERED FLIGHT CONSIDERED IN THIS REPORT

ROTOR Type	<u>BELL</u>	<u>BOEING</u>
	gimballed, stiff inplane	cantilever, soft inplane
Number of blades, N	3	3
Radius, R	156 in.	150 in.
Chord, C_B	18.9 in.	14 in.
Lock number, γ	3.83	4.04
Solidity, σ	0.089	0.115
Pitch/flap coupling, δ_3	-15 deg.	0
Collective pitch, θ_D	1.25 deg.	1.0 deg.
Lift-curve slope, a	5.7	5.7
Drag Coefficient, C_{Do}	0.0065	0.0065
Rotor rotation direction, $\bar{\Omega}$	+1	-1
Inflow ratio,	0.7	-0.7
Rotational speed, $ \Omega $	458 RPM 48.9 rad/sec	386 RPM 40.4 rad/sec
Blade Natural Frequencies		
first, $\lambda_1/ \Omega $	1.02/rev (7.78Hz)	0.827/rev. (5.32Hz)
second, $\lambda_2/ \Omega $	1.34/rev (10.2Hz)	1.32/rev (8.49Hz)
third, $\lambda_3/ \Omega $	4.35/rev (33.2Hz)	3.40/rev (21.9Hz)

TABLE 3. CONTINUED

ROTOR(cont'd)	<u>BELL</u>	<u>BOEING</u>
fourth, $\lambda_4/ \Omega $	10.1/rev (77.1Hz)	6.77/rev (43.5Hz)
Collective Natural Frequency		
first, $\lambda_1^{(o)}/ \Omega $	1.31/rev (10.0Hz)	
second, $\lambda_2^{(o)}/ \Omega $	2.12/rev (16.2Hz)	
third, $\lambda_3^{(o)}/ \Omega $	4.93/rev (37.7Hz)	
fourth $\lambda_4^{(o)}/ \Omega $	10.6/rev (80.9Hz)	
Blade flapping inertia, I_B	105 slug-ft ²	150 slug-ft ²
One blade weight, M_B	133 lb	124 lb
WING		
Semispan, L	200 in.	200 in.
Chord, c_w	62.2 in.	62.2 in.
Mast height, h	51.3 in.	51.3 in.
Sweep	0	0
Dihedral	0	0
Lift-curve slope, a_w	5.7	5.7
Drag coefficient, C_{Dow}	0.004	0.004
Moment coefficient C_{mo}	-0.005	-0.005
Aerodynamic center, $\bar{e} = x_{A_w}/c_w$	0.01	0.01
Angle of attack, α_{wo}	2.0 deg	2.0 deg

TABLE 3. CONCLUDED

	<u>BELL</u>	<u>BOEING</u>
WING (cont'd)		
Natural Frequencies		
first, $\Lambda_1/ \Omega $	0.347/rev (2.65Hz)	0.365/rev (2.35Hz)
second, $\Lambda_2/ \Omega $	0.622/rev (4.75Hz)	0.653/rev (4.20Hz)
third, $\Lambda_3/ \Omega $	1.09/rev (8.32Hz)	1.11/rev (7.14Hz)
fourth, $\Lambda_4/ \Omega $	2.37/rev (18.1Hz)	2.47/rev (15.9Hz)
fifth, $\Lambda_5/ \Omega $	3.76/rev (28.7Hz)	3.95/rev (25.4Hz)
sixth, $\Lambda_6/ \Omega $	10.6/rev (80.9Hz)	12.5/rev (80.4Hz)
PYLON		
Weight, M_p	1420 lb	2000 lb
Yaw inertia, I_{py}	164.8 slug-ft ²	250.0 slug-ft ²
Pitch inertia, I_{pp}	190.0 slug-ft ²	250.0 slug-ft ²
Roll inertia, I_{pr}	42.4 slug-ft ²	30.0 slug-ft ²
FLIGHT CONDITION FOR CALCULATIONS, $\lambda = 0.7$		
Cruising speed, V	250 kt	218 kt
Cruising altitude	sea level	sea level

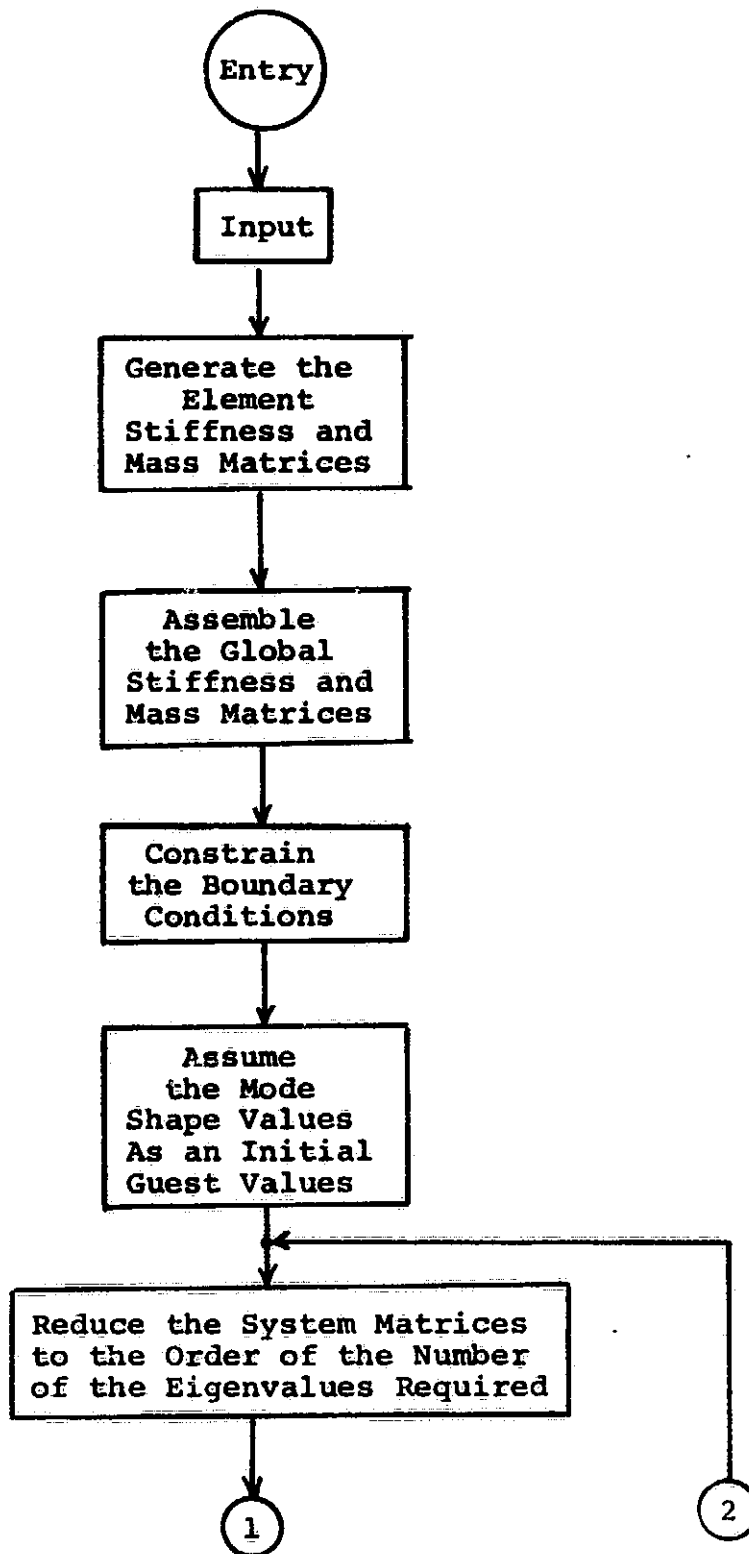


FIG. 1 FLOW CHART OF FREEVI PROGRAM FOR BLADE AND WING OF NATURAL FREQUENCIES AND MODE SHAPES

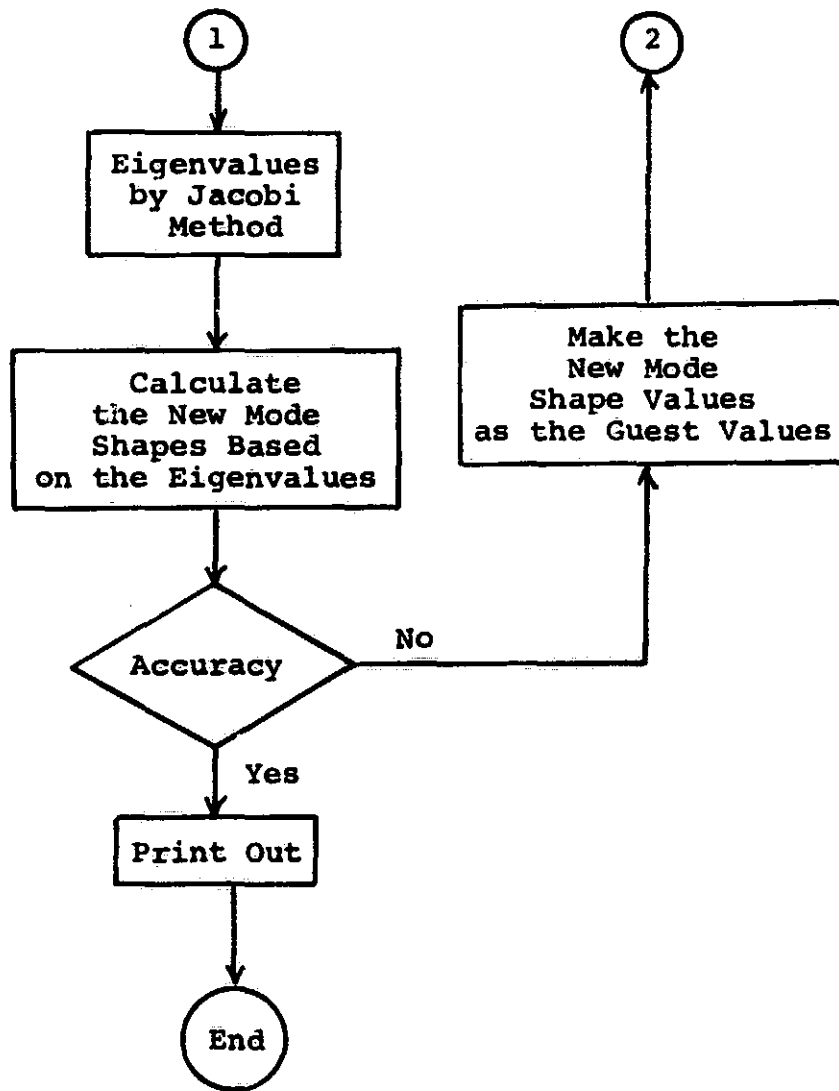


FIG. 1 CONCLUDED

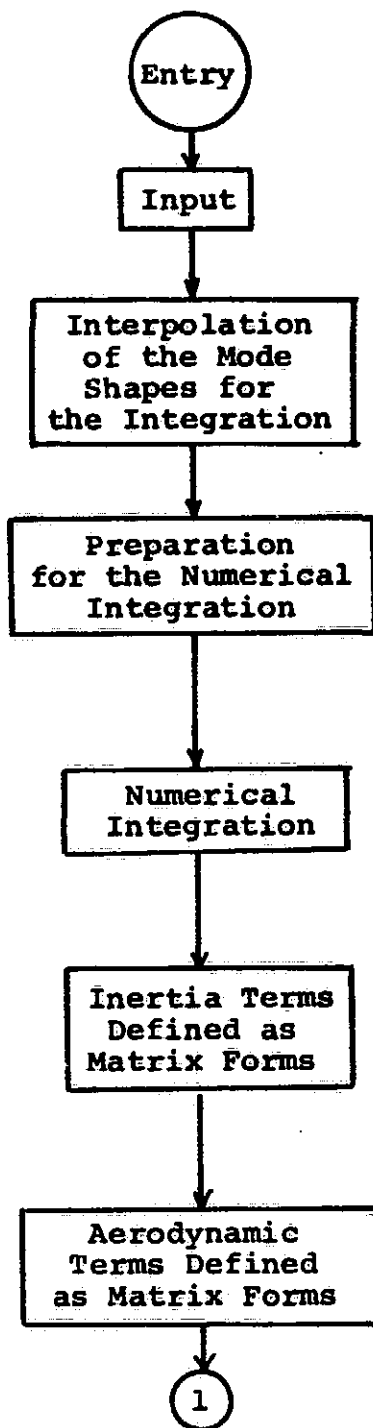


FIG. 2 FLOW CHART OF TILDYN PROGRAM FOR ANALYSIS OF TILT ROTOR AIRCRAFT DYNAMICS

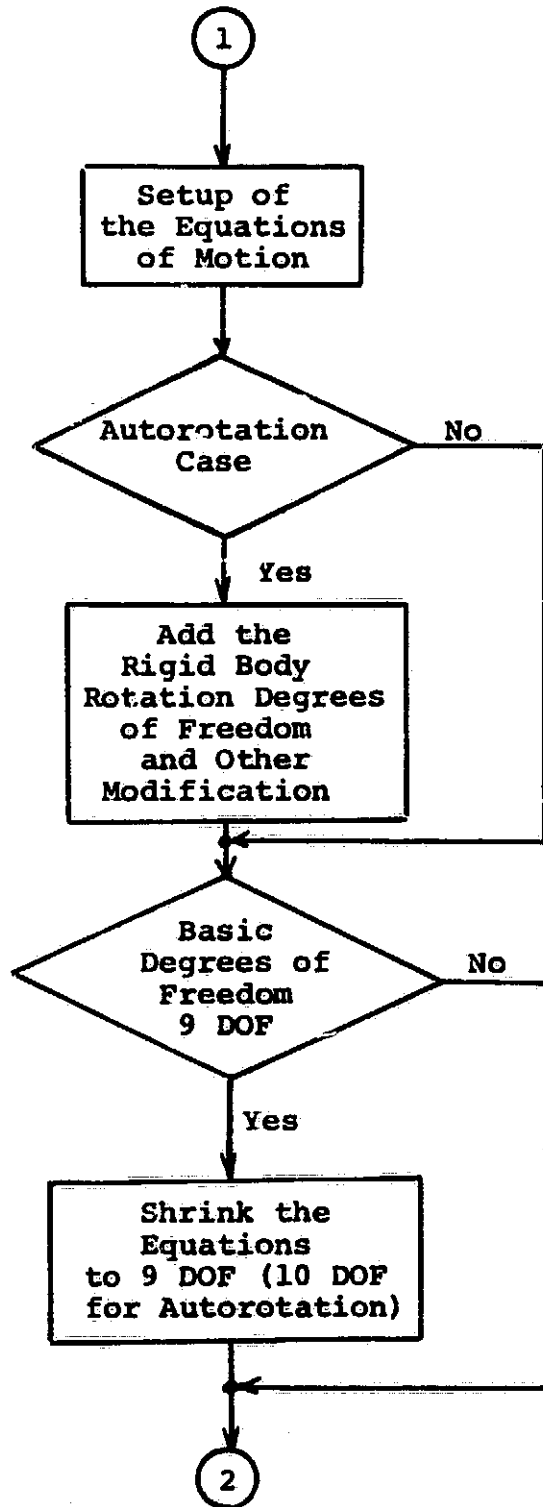


FIG. 2 CONTINUED

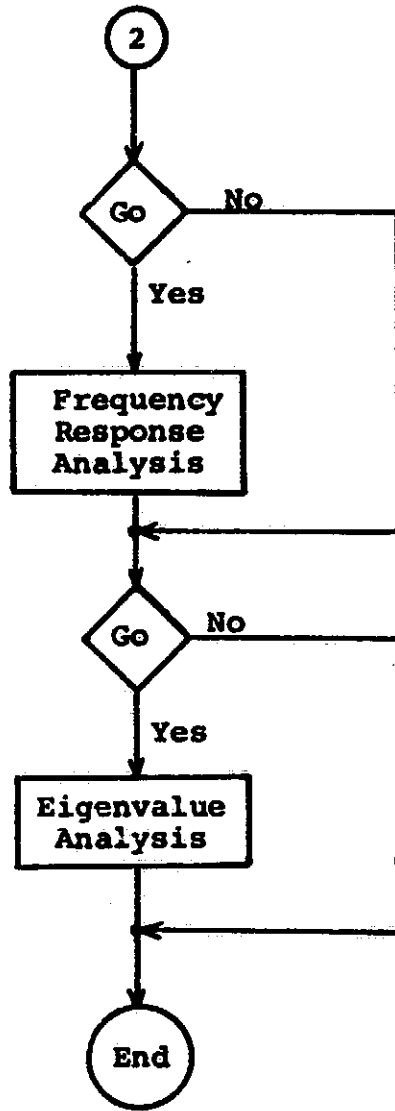


FIG. 2 CONCLUDED

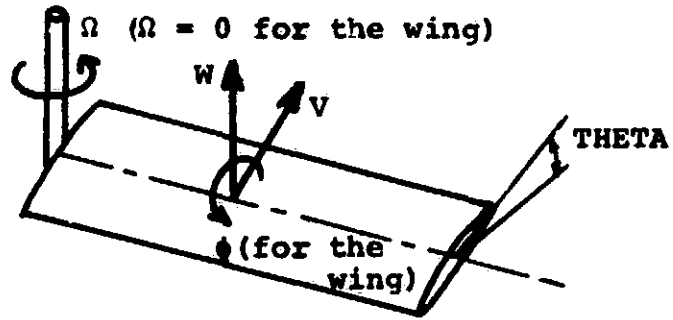


FIG. 3 COORDINATE SYSTEM FOR FREEVI PROGRAM

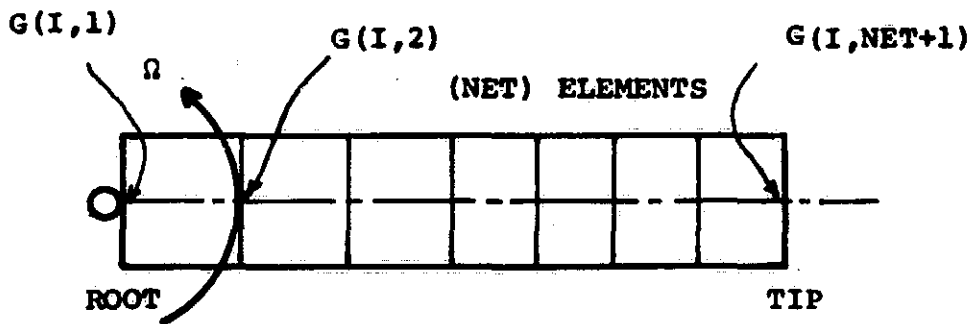


FIG. 4 FINITE ELEMENT REPRESENTATION WITH BEAM ELEMENTS

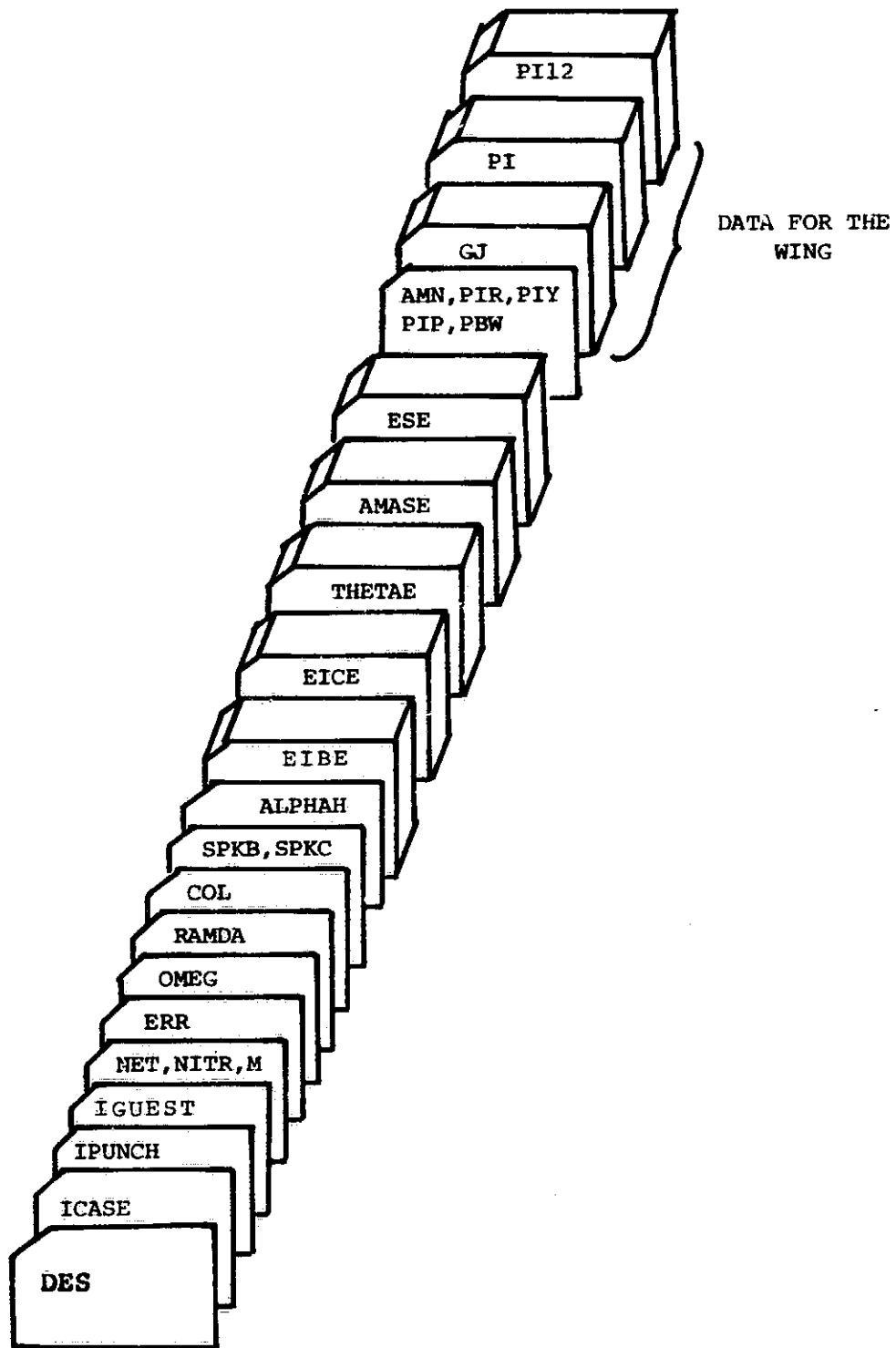
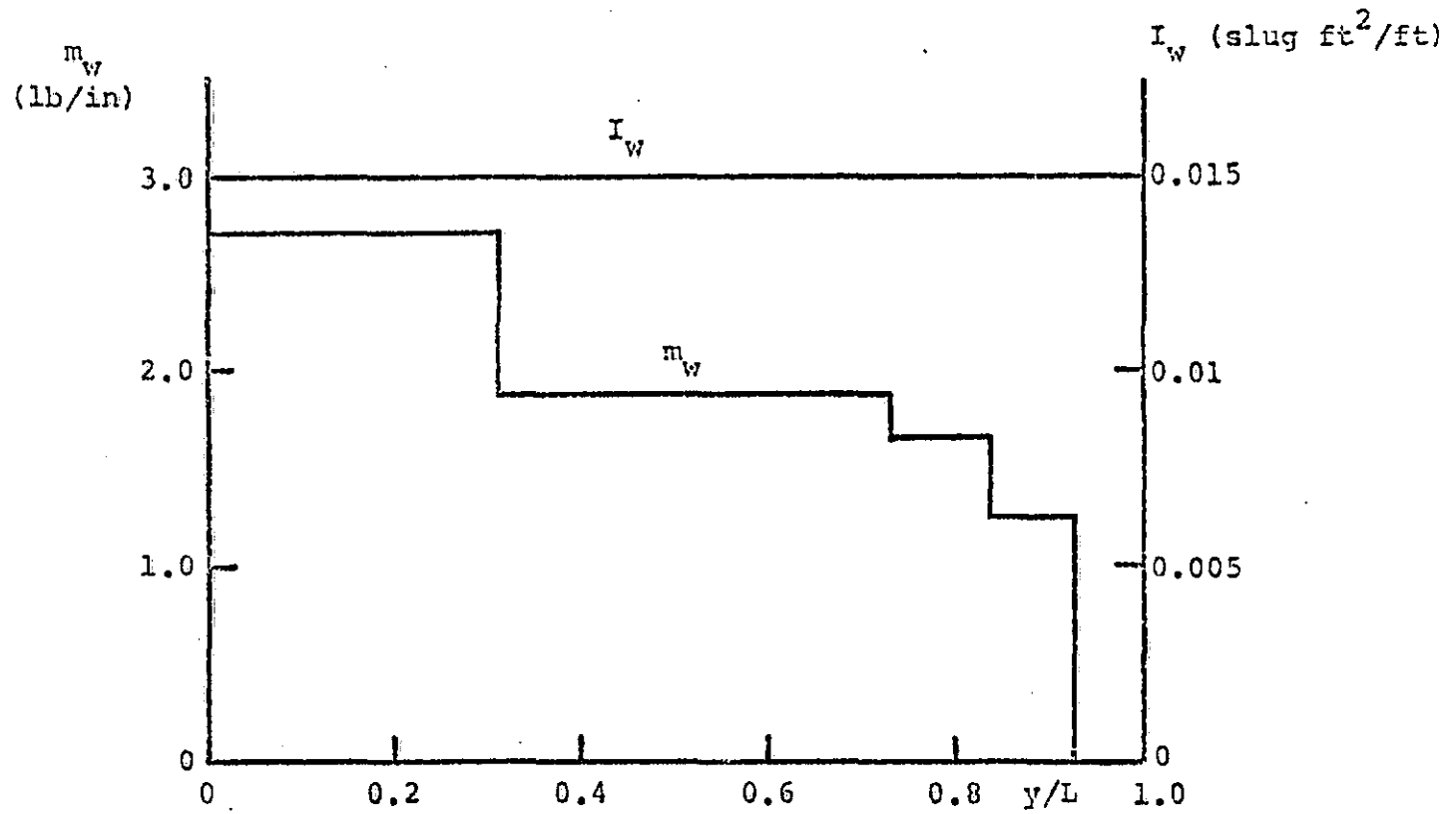
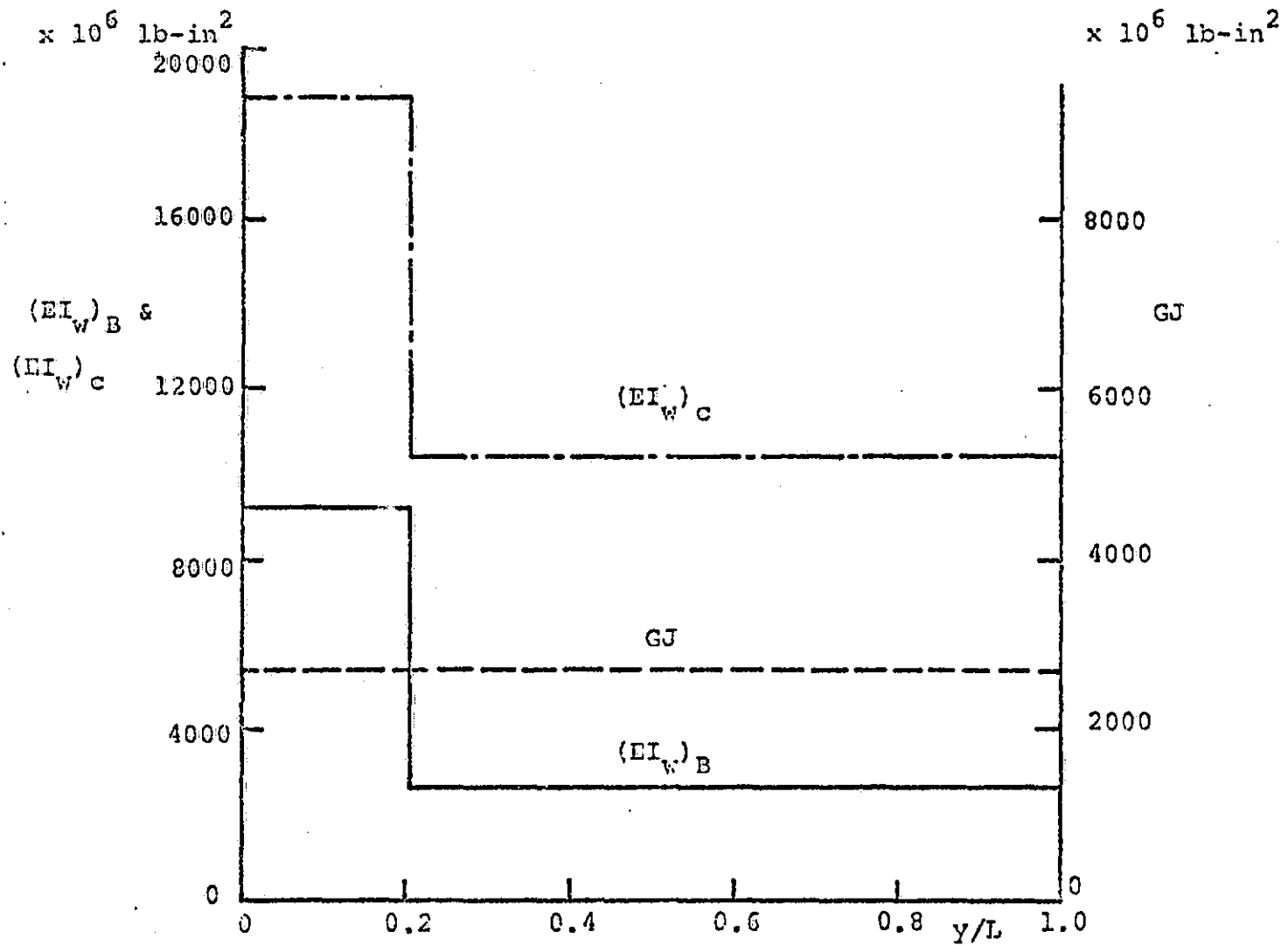


FIG. 5 DATA DECK SETUP FOR THE FREEVI PROGRAM



(a) Mass and Cross-Sectional Moment of Inertia Distribution

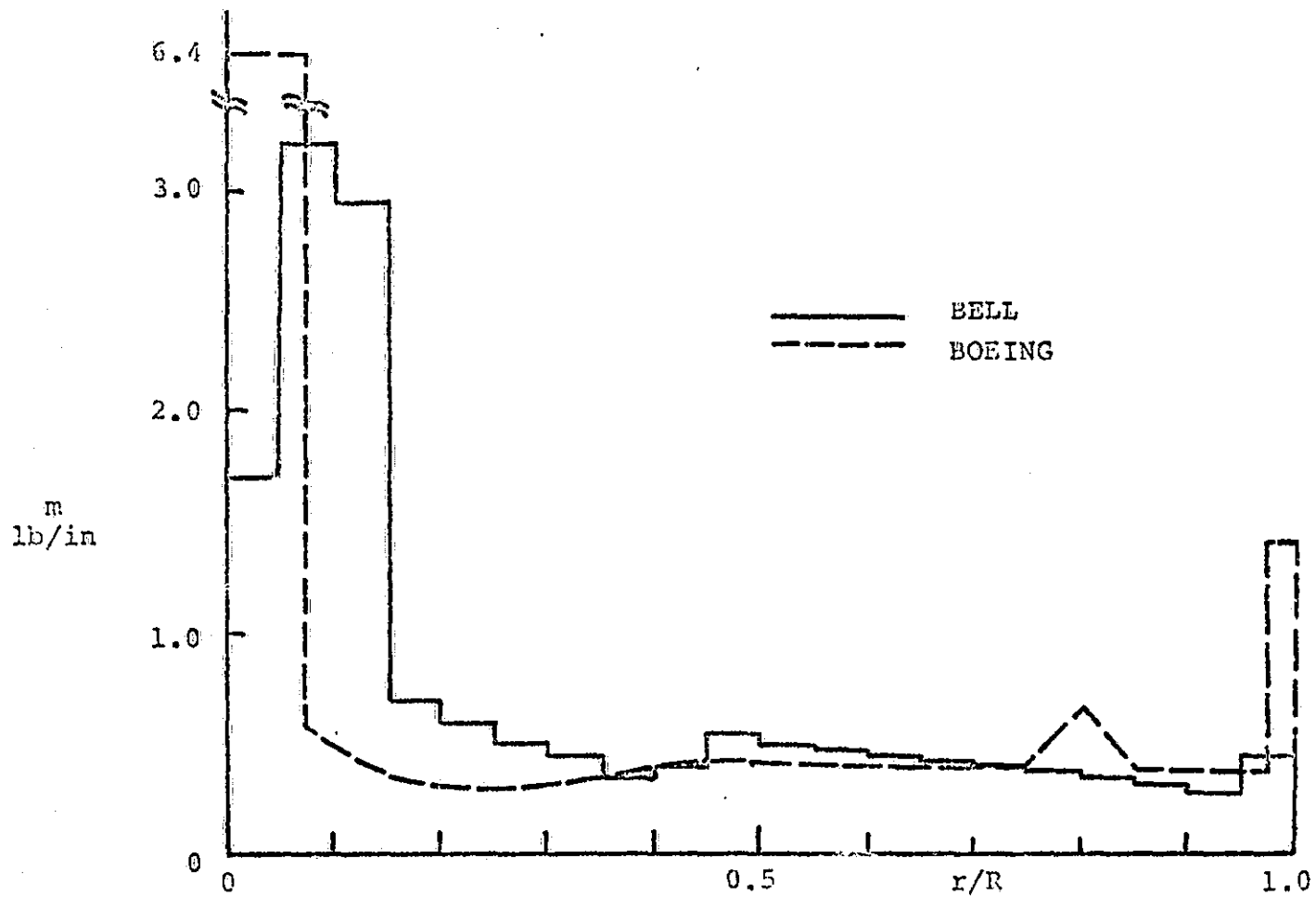
FIG. 6 STRUCTURAL CHARACTERISTICS OF THE WING



49

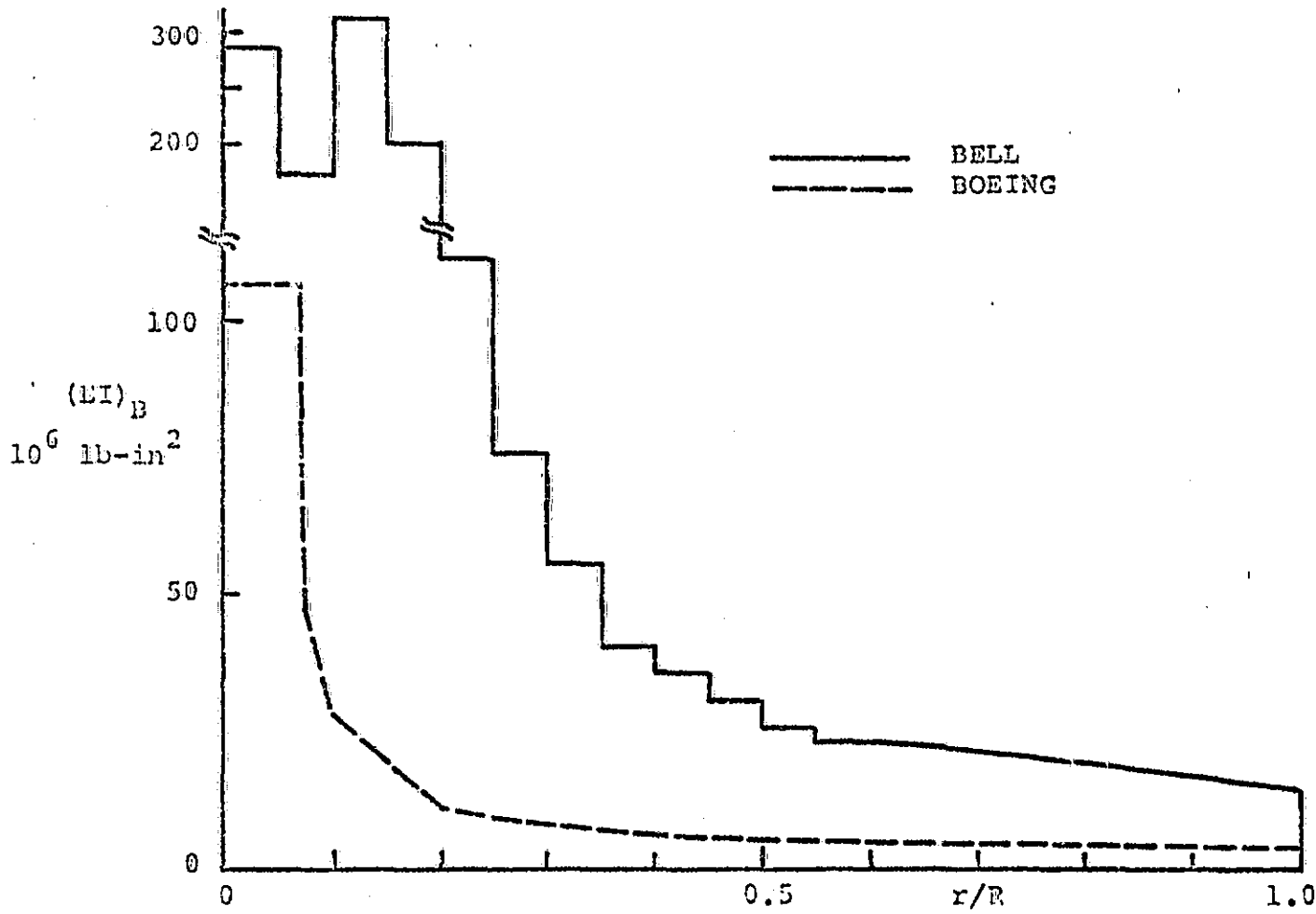
(b) Stiffness Distribution: Vertical Bending Stiffness $(EI_w)_B$, Chordwise Bending Stiffness $(EI_w)_c$, and Torsional Rigidity GJ

FIG. 6 CONCLUDED



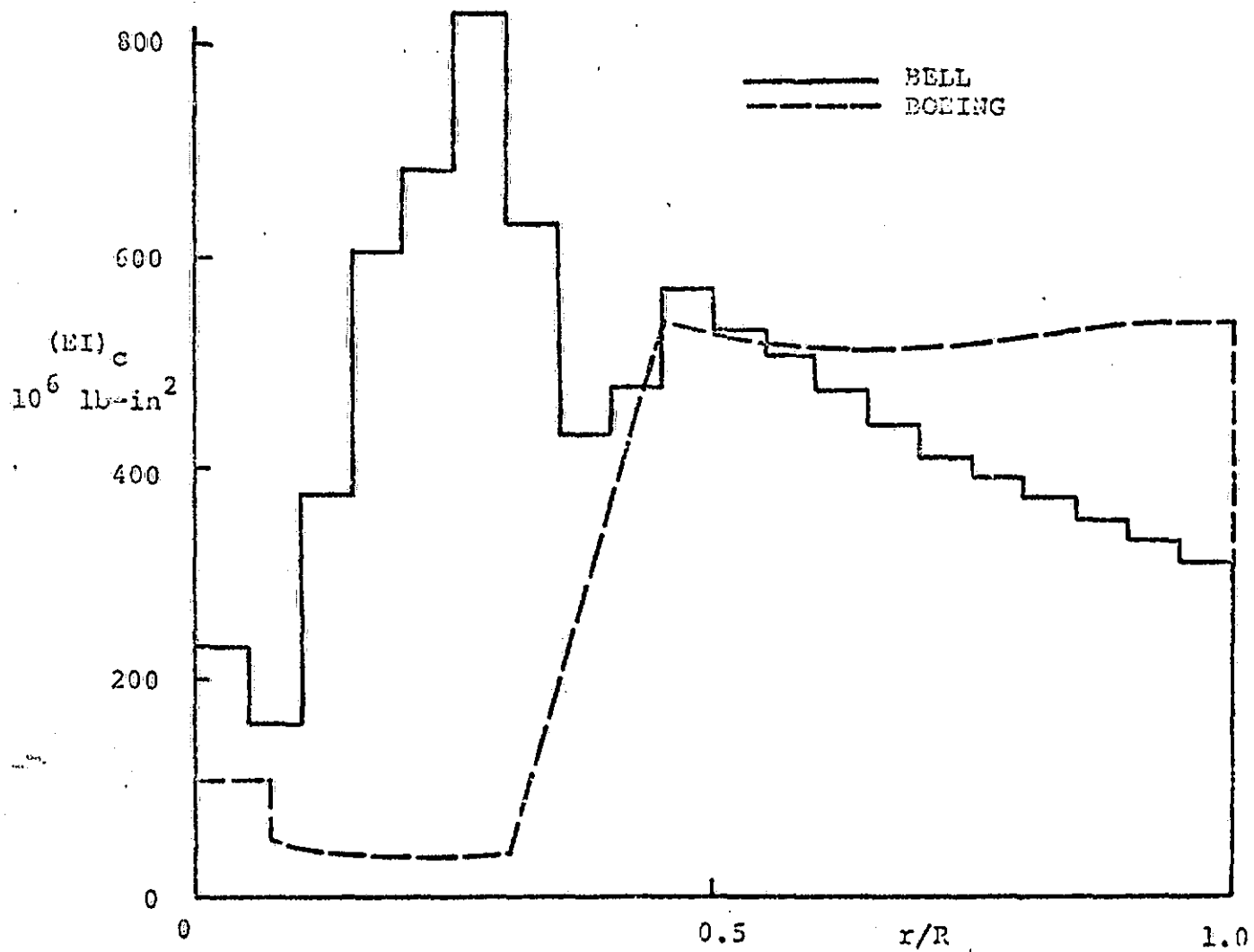
(a) Section Mass Distribution

FIG. 7 STRUCTURAL CHARACTERISTICS OF TWO PROPRTOR BLADES



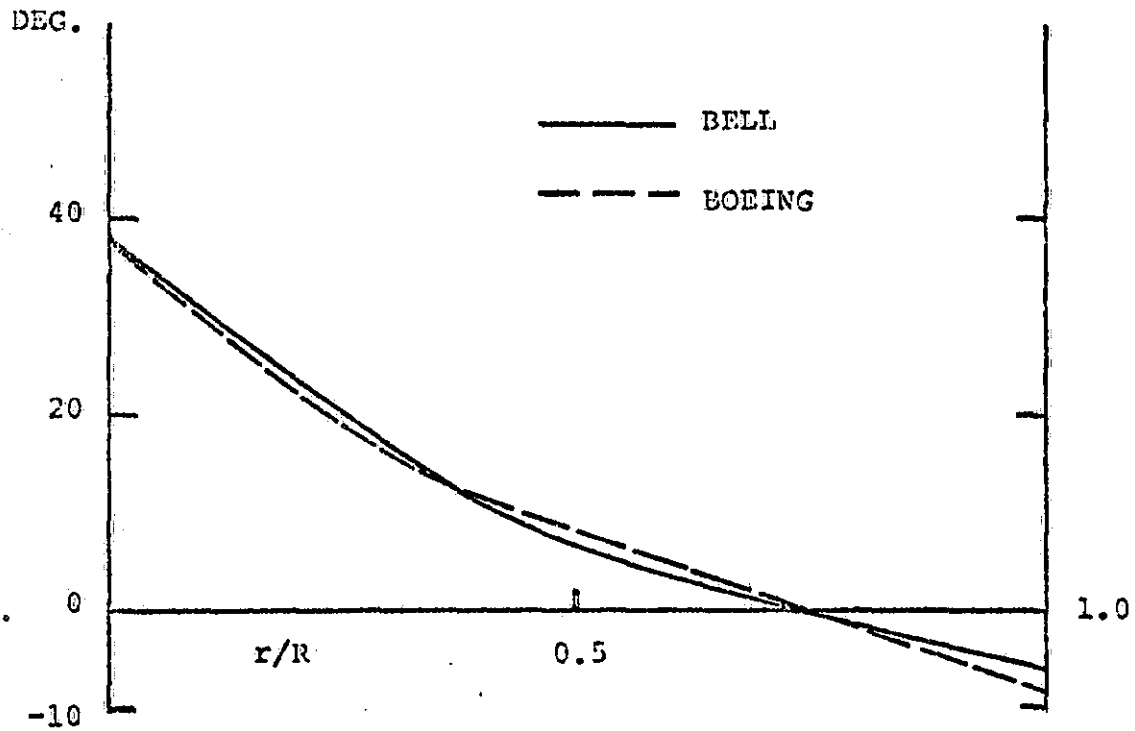
(b) Section Flapwise Bending Stiffness Distribution

FIG. 7 CONTINUED



(c) Section Chordwise Bending Stiffness Distribution

FIG. 7 CONTINUED



(d) Angle of Twist

FIG. 7 CONCLUDED

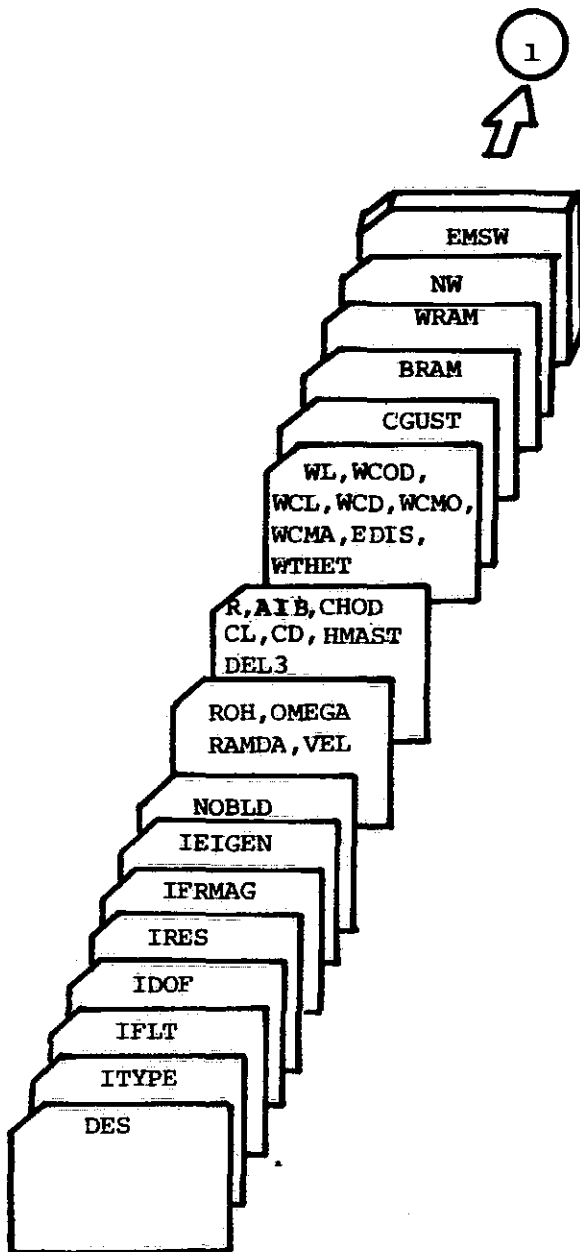


FIG. 8 DATA DECK SETUP FOR THE TILDYN PROGRAM

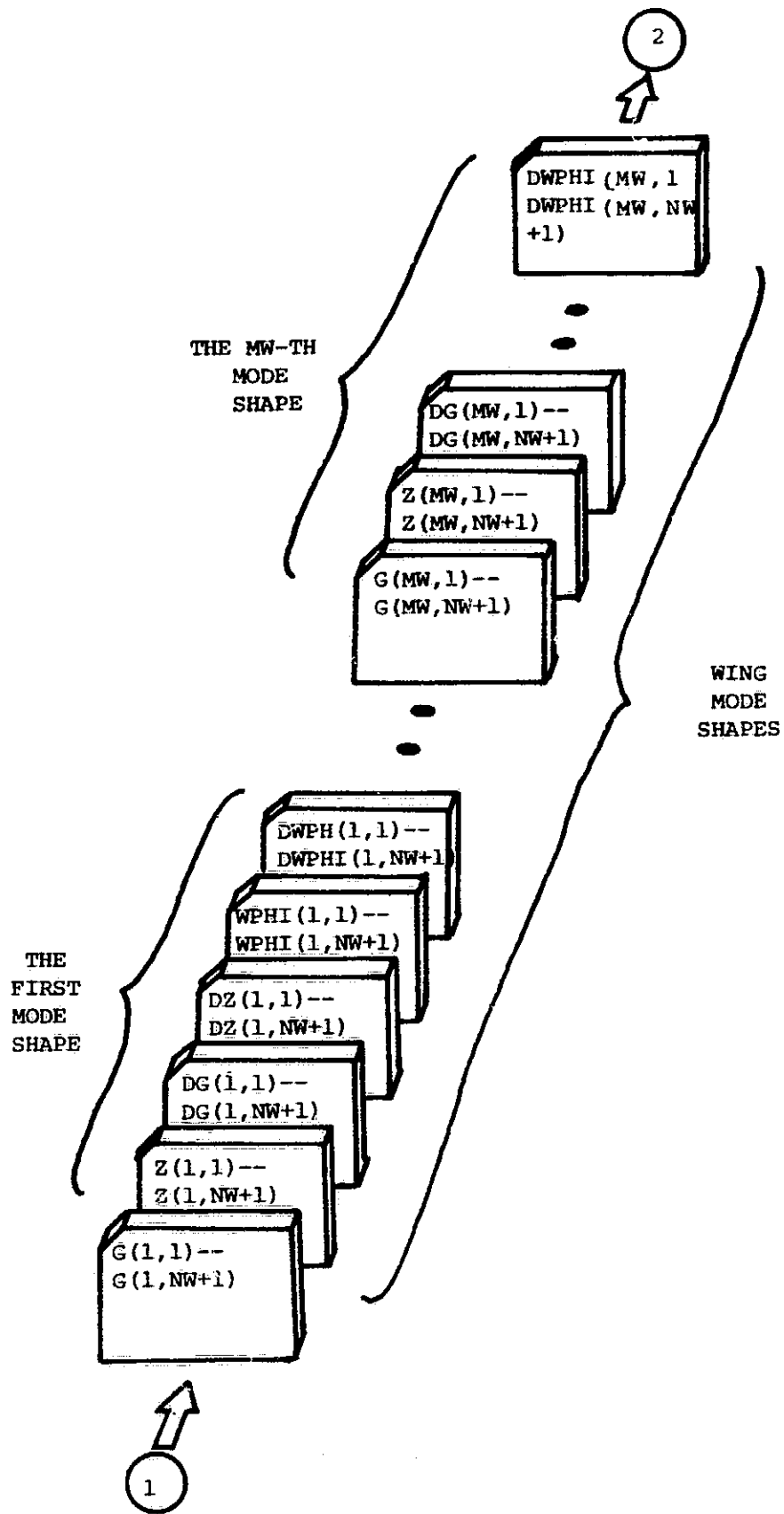


FIG. 8 CONTINUED

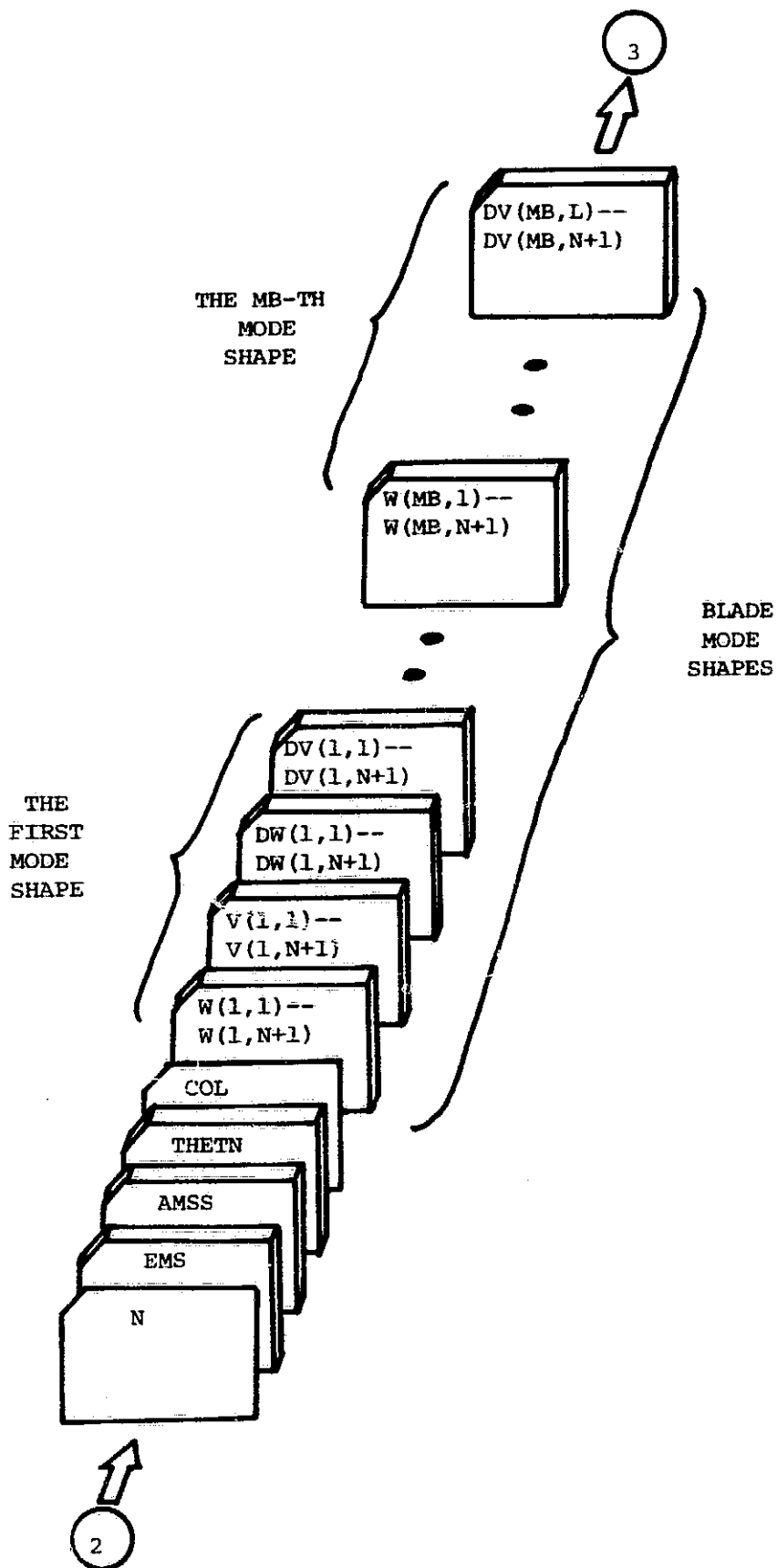
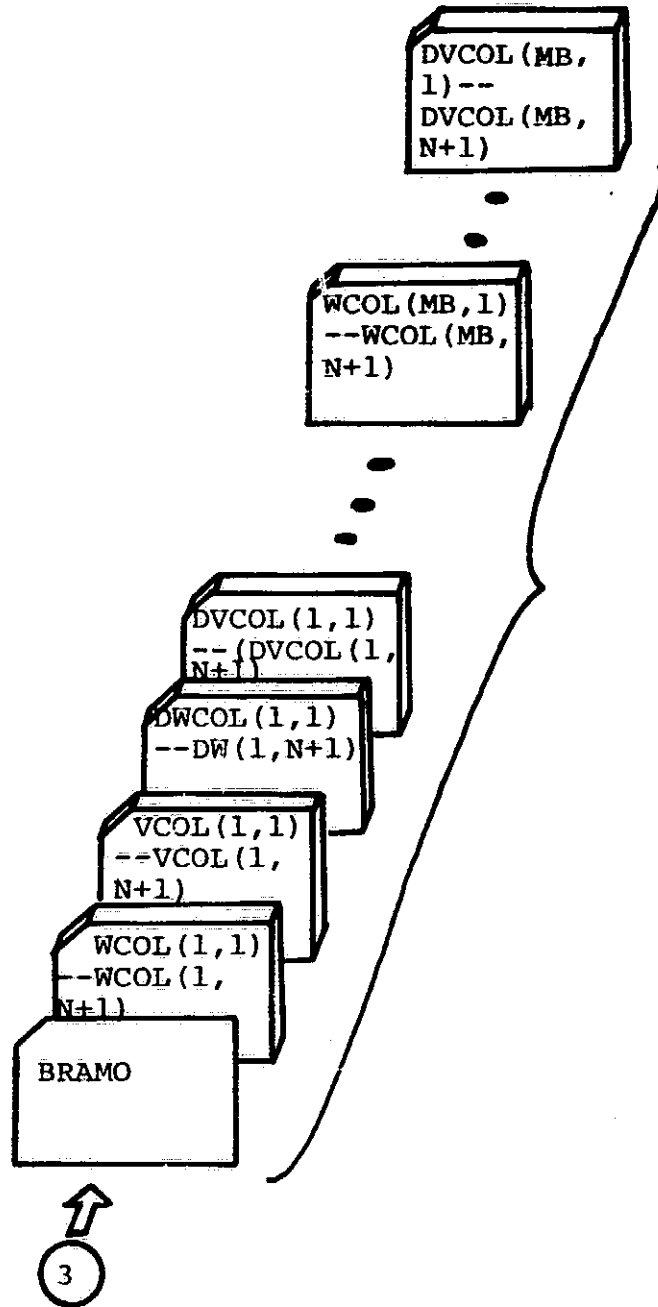


FIG. 8 CONTINUED



BLADE COLLECTIVE
MODE SHAPE DATA
IS FURNISHED IF
THE CASE IS AUTO-
ROTATION FLIGHT
(IFLT=1, ITYPE=1) OR
GIMBALLED ROTOR IN
POWERED FLIGHT (IFLT=0,
ITYPE=1)

FIG. 8 CONCLUDED

APPENDIX A
PROGRAM LISTING

A.1 The FREEVI Program Listing

PROGRAM ROTOR
PART 1 ; PROGRAM FREEVI

PURPOSE

TO OBTAIN THE NATURAL FREQUENCIES AND MODE SHAPES
OF THE ROTOR BLADE AND WING OF THE TILT-ROTOR AIRCRAFT

DEVELOPED BY MASAHIRO YASUE
OF AEROELASTIC AND STRUCTURES RESEARCH LABORATORY
AUGUST 1974
ADDRESS ; BLDG 41-211
MASSACHUSETTS INSTITUTE OF TECHNOLOGY
CAMBRIDGE, MASS. 02139

1 IMPLICIT REAL*8(A-H,O-Z)
DIMENSION NDPE(20), NNCDE(252), NOD(126), ICOL(126), INUM(126)
DIMENSION STK(1550), STM(1550), EK(78), EM(78), XLR(1200), X(1200)
DIMENSION Y(1200), U(126), EIG(9), LCH(9), RM(81), RK(81), RV(81)
DIMENSION SRM(81), SRK(81)
1 CALL TEIGEN(NDPE, NOD, NNODE, ICOL, INUM, STK, STM, EK, EM,
1 XLR, U, EIG, LCH, RM, RK, RV, SRM, SRK, X, Y)
GO TO 1
END

MAIN0001
MAIN0002
MAIN0003
MAIN0004
MAIN0005
MAIN0006
MAIN0007
MAIN0008
MAIN0009
MAIN0010
MAIN0011
MAIN0012
MAIN0013
MAIN0014
MAIN0015
MAIN0016
MAIN0017
MAIN0018
MAIN0019
MAIN0020
MAIN0021
MAIN0022
MAIN0023
MAIN0024
MAIN0025
MAIN0026
MAIN0027
MAIN0028
MAIN0029

C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C

SUBROUTINE TEIGEN(NDPE, NOD, NNODE, ICOL, INUM, STK, STM, EK
a, EM, XLR, U, EIG, LCH, RM, RK, RV, SRM, SRK, X, Y)

TO CALCULATE THE NORMAL MODES AND FREQUENCIES

IMPLICIT REAL*8(A-H, C-Z)
COMMON /BW/ ICASE , IGUEST
COMMON/HELP/ALPHAH
DIMENSION NDPE(1), NBCU(1), NOD(1), NNODE(1), ICOL(1)
DIMENSION INUM(1), STK(1), STM(1), EK(1), EM(1), XLR(1)
DIMENSION U(1), EIG(1), LCH(1)
DIMENSION RM(1), RK(1), RV(1), SRK(1), SRM(1), X(1)
DIMENSION Y(1)
DIMENSION SQU(20), CYC(20)
CALL INPUT(IEQ, NDPE, NET, NDT, MNC, NNODE, NBU, INUM, ERR, NITR, M)
CALL MESH(NDPE, NET, NDT, NCDT, MNC, MN, NOD, NNODE, ICOL, INUM, NBU
a , INDEX)
IF(INDEX .EQ. 0) GO TO 99
CALL ASBV(STK, STM, IEQ, EK, EM, NDPE, NDT, NCDT, NNODE, MN, NET, INUM)
MA=M
N=NCDT
M=M*N
MM=M*M
CALL FAC(STK, N, NNDG, ICOL, INUM, U)
IF(NNDG .LT. 0) GO TO 99
DO 3 I=1, M
3 EIG(I)= .0
DO 74 K=1, M
II=(K-1)*N
IY=K*2-1
DO 74 I=1, N
IX=IY
IY=IX*65539
IF(IY) 75, 76, 76
75 IY=IY+2147483647+1
76 YFL=IY

TEIG0001
TEIG0002
TEIG0003
TEIG0004
TEIG0005
TEIG0006
TEIG0007
TEIG0008
TEIG0009
TEIG0010
TEIG0011
TEIG0012
TEIG0013
TEIG0014
TEIG0015
TEIG0016
TEIG0017
TEIG0018
TEIG0019
TEIG0020
TEIG0021
TEIG0022
TEIG0023
TEIG0024
TEIG0025
TEIG0026
TEIG0027
TEIG0028
TEIG0029
TEIG0030
TEIG0031
TEIG0032
TEIG0033
TEIG0034
TEIG0035
TEIG0036

C
C
C

```

74 XLR(II+II)=YFL*0.4656613D-9-0.5D+00
   IF(IGUFST.EQ.0) GO TO 200
   GO TO (210,220,230,240,220),ICASE
210 GO TO (310,320,330),IGUEST
C-----W ONLY
310 IX=N/6
   DO 301 K=1,M
   II=NCDT*K-NCDT
   XLR(II+1)=0.0D+00
   DO 301 KK=1,IX
   JJ=KK*6-5
   XLR(II+JJ+2)=0.0D+00
   XLR(II+JJ+4)=0.0D+00
   XLR(II+JJ+5)=0.0D+00
301 XLR(II+JJ+6)=0.0D+00
   GO TO 200
C-----V ONLY
320 IX=N/6
   DO 302 K=1,M
   II=NCDT*K-NCCT
   XLR(II+1)=0.0D+00
   DO 302 KK=1,IX
   JJ=KK*6-5
   XLR(II+JJ+1)=0.0D+00
   XLR(II+JJ+3)=0.0D+00
   XLR(II+JJ+5)=0.0D+00
302 XLR(II+JJ+6)=0.0D+00
   GO TO 200
C-----PHI ONLY
330 IX=N/6
   DO 303 K=1,M
   II=NCDT*K-NCDT
   DO 303 KK=1,IX
   JJ=KK*6-5
   DO 303 KKK=1,4
303 XLR(II+JJ+KKK)=0.0D+00

```

```

TEIG0037
TEIG0038
TEIG0039
TEIG0040
TEIG0041
TEIG0042
TEIG0043
TEIG0044
TEIG0045
TEIG0046
TEIG0047
TEIG0048
TEIG0049
TEIG0050
TEIG0051
TEIG0052
TEIG0053
TEIG0054
TEIG0055
TEIG0056
TEIG0057
TEIG0058
TEIG0059
TEIG0060
TEIG0061
TEIG0062
TEIG0063
TEIG0064
TEIG0065
TEIG0066
TEIG0067
TEIG0068
TEIG0069
TEIG0070
TEIG0071
TEIG0072

```

```

GO TO 200
220 GO TO (221,222),IGUEST
C-----W ONLY
221 IX=N/2
    DO 201 K=1,M
    II=N*K-N
    DO 201 I=1,IX
201 XLR(II+2*I)=0.000
    GO TO 200
C-----V ONLY
222 IX=N/2
    DO 202 K=1,M
    II=K*N-N
    DO 202 I=1,IX
202 XLR(II+2*I-1)=0.000
    GO TO 200
230 GO TO (231,232),IGUEST
C-----W ONLY
231 IX=N/2
    DO 233 K=1,M
    II=N*K-N
    XLR(II+1)=0.000
    DO 233 KK=1,IX
233 XLR(II+2*KK+1)=0.000
    GO TO 200
C-----V ONLY
232 IX=N/2
    DO 234 K=1,M
    II=N*K-N
    DO 234 KK=1,IX
234 XLR(II+2*KK)=0.000
    GO TO 200
240 GO TO (241,242),IGUEST
C-----W ONLY
241 IX=N/2
    DO 243 K=1,M

```

```

TEIG0073
TEIG0074
TEIG0075
TEIG0076
TEIG0077
TEIG0078
TEIG0079
TEIG0080
TEIG0081
TEIG0082
TEIG0083
TEIG0084
TEIG0085
TEIG0086
TEIG0087
TEIG0088
TEIG0089
TEIG0090
TEIG0091
TEIG0092
TEIG0093
TEIG0094
TEIG0095
TEIG0096
TEIG0097
TEIG0098
TEIG0099
TEIG0100
TEIG0101
TEIG0102
TEIG0103
TEIG0104
TEIG0105
TEIG0106
TEIG0107
TEIG0108

```

```

        II=N*K-N
        DO 243 KK=1, IX
243    XLR(II+2*KK+1)=0.000
        GO TO 200
C-----V ONLY
242    IX=N/2
        DO 244 K=1, M
        II=N*K-N
        XLR(II+1)=0.000
        DO 244 KK=1, IX
244    XLR(II+2*KK)=0.000
200    CONTINUE
        IST=1
        DO 21 KKK=1, NITR
        IT=(IST-1)*N+1
        DO 1 I=IT, NM
1    Y(I)=XLR(II)
        CALL SOLZ(STK, Y, N, M-IST+1, ICOL, INUM, IST)
        DO 11 K=IST, M
        K1=K-1
        II=(K-1)*N
        XM=C.0
        LCH(K)=0
        DO 7 I=1, N
        U=DABS(Y(II+I))
        IF(D-XM)7, 7, 9
9    XP=D
        LCH(K)=I
7    CONTINUE
        IF(LCH(K) .EQ. 0) GO TO 99
        E=Y(II+LCH(K))
        E=1./E
        DO 11 I=1, N
        III=1+II
        Y(III)=Y(III)*E
11    XLR(III)=XLR(III)*E

```

```

TEIG0109
TEIG0110
TEIG0111
TEIG0112
TEIG0113
TEIG0114
TEIG0115
TEIG0116
TEIG0117
TEIG0118
TEIG0119
TEIG0120
TEIG0121
TEIG0122
TEIG0123
TEIG0124
TEIG0125
TEIG0126
TEIG0127
TEIG0128
TEIG0129
TEIG0130
TEIG0131
TEIG0132
TEIG0133
TEIG0134
TEIG0135
TEIG0136
TEIG0137
TEIG0138
TEIG0139
TEIG0140
TEIG0141
TEIG0142
TEIG0143
TEIG0144

```

```

CALL MTRTR(M,N,RK,Y,XLR,IST)
DO 31 I=1,NM
31 X(I)=Y(I)
CALL MLTZ(STM,X,U,N,M-IST+1,ICCL,INUM,IST)
CALL MTRTR(M,N,RM,Y,X,IST)
DO 39 I=1,MM
SRM(I)=RM(I)
39 SRK(I)=RK(I)
CALL DNROOT(M,RM,RK,U,RV)
DO 40 I=1,M
40 U(I)=1./U(I)-ALPHAH
WRITE(6,41) (U(I),I=1,M)
41 FORMAT(/2X,'EIGENVALLES=',/(2X,10D13.5))
DO 22 I=1,MA
IST=I
IF(DABS(EIG(I)/U(I)-1.0) .GT. ERR) GO TO 23
22 CONTINUE
DO 504 I=1,M
SQU(I)=ESQRT(DABS(U(I)))
CYC(I)=SQU(I)*0.500/3.14159200
504 CONTINUE
WRITE(6,505)(SQU(I),I=1,M)
505 FORMAT(/5X,'RADIAN/SEC',/(2X,10D13.5))
506 FORMAT(/5X,'HERTZ',/(2X,10D13.5))
WRITE(6,506)(CYC(I),I=1,M)
DO 10 I=1,NCDT
DO 10 J=1,M
JJ=(J-1)*NCDT
XLR(I+JJ)=0.0
DO 10 K=1,M
10 XLR(I+JJ)=XLR(I+JJ)+Y(I+(K-1)*N)*RV((J-1)*M+K)
DO 15 I=1,M
II=(I-1)*M
DO 15 J=1,M
JJ=(J-1)*M
IJ=JJ+I

```

```

TEIG0145
TEIG0146
TEIG0147
TEIG0148
TEIG0149
TEIG0150
TEIG0151
TEIG0152
TEIG0153
TEIG0154
TEIG0155
TEIG0156
TEIG0157
TEIG0158
TEIG0159
TEIG0160
TEIG0161
TEIG0162
TEIG0163
TEIG0164
TEIG0165
TEIG0166
TEIG0167
TEIG0168
TEIG0169
TEIG0170
TEIG0171
TEIG0172
TEIG0173
TEIG0174
TEIG0175
TEIG0176
TEIG0177
TEIG0178
TEIG0179
TEIG0180

```

```

PM(IJ)=0.0
RK(IJ)=0.0
DO 15 K=1,M
KK=(K-1)*M
RM(IJ)=RM(IJ)+SRM(KK+I)*RV(JJ+K)
15 RK(IJ)=RK(IJ)+SRK(KK+I)*RV(JJ+K)
CALL MTRTR(M,M,SRM,RV,RM,1)
CALL MTRTR(M,M,SRK,RV,RK,1)
DO 42 I=1,M
KK=M*I-M+I
Y(I)=1./DSQRT(SRM(KK))
II=I*NCDT-NCBT
DO 42 J=1,NCBT
42 XLR(II+J)=XLR(II+J)*Y(I)
DO 17 I=1,M
KK=I*M-M
DO 17 J=1,I
E=Y(I)*Y(J)
IJ=KK+J
SRM(IJ)=E*SRM(IJ)
17 SRK(IJ)=E*SRK(IJ)
CALL OUTPUT(KKK,M,NCBT,NDT,NOD,NODE,ERR,XLR,U,SRM,SRK)
GO TO 99
23 DO 25 I=1,M
25 EIG(I)=U(I)
IF(IST.EQ.1) GO TO 45
IQ=IST-1
DO 44 I=1,IQ
II=(I-1)*M
DO 44 J=1,IQ
IJI=II+J
RM(IJI)=SRM(IJI)
44 RK(IJI)=SRK(IJI)
45 CONTINUE
DO 34 I=1,N
DO 34 J=IST,M

```

```

TEIG0181
TEIG0182
TEIG0183
TEIG0184
TEIG0185
TEIG0186
TEIG0187
TEIG0188
TEIG0189
TEIG0190
TEIG0191
TEIG0192
TEIG0193
TEIG0194
TEIG0195
TEIG0196
TEIG0197
TEIG0198
TEIG0199
TEIG0200
TEIG0201
TEIG0202
TEIG0203
TEIG0204
TEIG0205
TEIG0206
TEIG0207
TEIG0208
TEIG0209
TEIG0210
TEIG0211
TEIG0212
TEIG0213
TEIG0214
TEIG0215
TEIG0216

```



```
JJ=(J-1)*N
XLR(I+JJ)=0.0
DO 34 K=1,M
34 XLR(I+JJ)=XLR(I+JJ)+X(I+(K-1)*N)*RV((J-1)*M+K)
21 CONTINUE
WRITE(6,26) KKK
26 FORMAT(/2X,'NO. OF ITERATION=',I4,2X,'NOT CONVERGED')
99 RETURN
END
```

```
TEIG0217
TEIG0218
TEIG0219
TEIG0220
TEIG0221
TEIG0222
TEIG0223
TEIG0224
TEIG0225
```

SUBROUTINE INPUT(IEQ,NDPE,NET,NDT,MNC,NODE,NBU,NBCU,ERR,NITR,M)

TO SUPPLY INPUT INFORMATION

DES COMMENTS AND DESCRIPTIONS

ICASE=1 WING
ICASE=2 BLADE B.C. CANTILEVER+CANTILEVER
ICASE=3 BLADE B.C. CANTILEVER+HINGE
ICASE=4 BLADE B.C. HINGE+CANTILEVER
ICASE=5 BLADE B.C. HINGE+HINGE

IPUNCH=0 NO PUNCH OUTPUT
IPUNCH=1 PUNCH OUTPUT

IGUEST=0 COUPLED MODE SHAPES GENERATED
IGUEST=1 W DEFLECTION ONLY
IGUEST=2 V DEFLECTION ONLY
IGUEST=3 PHI DEFLECTION ONLY

--CAUTION-- TO DERIVE UNCOUPLED MODES, COUPLING TERMS SHOULD BE
--CAUTION-- SET AT ZERO.
--CAUTION-- PR IN THE WING, RAMDA,COL,THETA IN THE BLADE

NET NO OF ELEMENTS
NITR = NO OF ITERATION ALLOWED
M= NO OF MODES WANTED

ERR ERROR TOLERANCE FOR ITERATION
OMEG ROTATION FREQ IN RAD / SEC
RAMDA=INFLOW RATIO
COL=COLLECTIVE PITCH ANGLE DETERMINED BY PERFORMANCE ANALYSIS
SPKB,SPKC =SPRING CONSTANT OF THE HINGED PLADE (BEAMWISE
& CHORDWISE)
ALPHAH=HELPER TO AVOID THE SINGULARITY OF THE STIFFNESS MATRIX
EIBE= EI FOR SPANWISE BENDING

INPU0001
INPU0002
INPU0003
INPU0004
INPU0005
INPU0006
INPU0007
INPU0008
INPU0009
INPU0010
INPU0011
INPU0012
INPU0013
INPU0014
INPU0015
INPU0016
INPU0017
INPU0018
INPU0019
INPU0020
INPU0021
INPU0022
INPU0023
INPU0024
INPU0025
INPU0026
INPU0027
INPU0028
INPU0029
INPU0030
INPU0031
INPU0032
INPU0033
INPU0034
INPU0035
INPU0036

EICE ET FOR CORDWISE BENDING
 THETA=ANGLE OF TWIST
 AMASE=MASS/UNIT LENGTH
 ESE=ELEMENT SIZE

AMN =MASS OF NACELLE AND ALL BLADES OR TIP MASS IN CASE OF BLADES
 PIP =ROLLING MOMENT OF INERTIA OF NACELLE
 PIY=YAWING MOMENT OF INERTIA OF NACELLE,
 HALF OF THAT OF ALL BLADES AND $(H**2)*MASS$ OF ALL BLADES
 PIP=PITCHING MOMENT OF INERTIA OF NACELLE,
 HALF OF THAT OF ALL BLADES AND $(H**2)*MASS$ OF ALL BLADES
 PRW=MASS COUPLING OF WING DUE TO BLADES $H*MASS$ OF BLADES

IF ICASE=1, NEXT THREE DATA GJ,PI, AND PI12 SHOULD BE ADDED.

GJ =TORSIONAL RIGIDITY
 PI=MOMENT OF INERTIA FOR TORSION
 PI12=MASS COUPLING BETWEEN TORSION AND SPANWISE BENDING
 POSITIVE IF C.G. IS AHEAD OF ELASTIC AXIS

NDPN= NO OF DEGREES OF FREEDOM PER NODE
 NDPN = 4 FOR BLADE MODE
 NDPN = 6 FOR WING MODE

COMMON /PUNCH/ IPUNCH
 COMMON /BW/ ICASE , IGUEST
 COMMON/SPRING/SPKR,SPKC
 COMMON/HELP/ALPHAH
 DOUBLE PRECISION ALPHAH
 DIMENSION NDPF(1),NODE(1),NRCU(1)
 DOUBLE PRECISION ERR
 DIMENSION FIRE(20),EICE(20), THETA(20),AMASE(20),ESE(20),TN(21)
 DIMENSION GJ(20) , PI(20) ,PI12 (20)
 COMMON /ELEMI/ OMEG,FIRE,EICE,THETA,AMASE,ESE,TN,GJ,PI, PI12,AMN,

INPU0037
 INPU0038
 INPU0039
 INPU0040
 INPU0041
 INPU0042
 INPU0043
 INPU0044
 INPU0045
 INPU0046
 INPU0047
 INPU0048
 INPU0049
 INPU0050
 INPU0051
 INPU0052
 INPU0053
 INPU0054
 INPU0055
 INPU0056
 INPU0057
 INPU0058
 INPU0059
 INPU0060
 INPU0061
 INPU0062
 INPU0063
 INPU0064
 INPU0065
 INPU0066
 INPU0067
 INPU0068
 INPU0069
 INPU0070
 INPU0071
 INPU0072

```

1 PIP,PIY,PIP,PBW,BM,BI,R,NETT
  DIMENSION DES(20)
10  FORMAT (16I5)
1   FORMAT (8F10.6)
4   FORMAT(5E15.7)
149  FORMAT(20A4)
150  FORMAT(I1)
    IEQ=0
    READ(5,149)(DES(I),I=1,20)
    READ(5,150)ICASE
    READ(5,150)IPUNCH
    READ(5,150)    IGUEST
    READ (5,10)    NET,NITR,M
    IF(ICASE.EQ.1) GO TO 192
    NDPN=4
    GO TO 193
192  NDPN=6
193  CONTINUE
    NETT=NET
    READ (5,1) ERR
    READ (5,1) OMEG
    READ(5,1) RAMDA
    READ(5,1) COL
    READ(5,1)SPKR,SPKC
    READ(5,1)    ALPHAH
    READ (5,4) ( SIRE(I),I=1,NET)
    READ (5,4) ( FICE(I),I=1,NET)
    READ (5,1) ( THETA(I),I=1,NET)
    READ (5,1) ( AMASE(I),I=1,NET)
    READ (5,1) ( ESE(I),I=1,NET)
    READ (5,1) AMN,PIP,PIY,PIP,PBW
    IF ( NDPN .EQ. 4) GO TO 100
    READ (5,4) (GJ(I),I=1,NET)
    READ (5,4) (PI(I),I=1,NET)
    READ (5,4) ( PI12(I),I=1,NET)
100 CONTINUE

```

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INPU0073
INPU0074
INPU0075
INPU0076
INPU0077
INPU0078
INPU0079
INPU0080
INPU0081
INPU0082
INPU0083
INPU0084
INPU0085
INPU0086
INPU0087
INPU0088
INPU0089
INPU0090
INPU0091
INPU0092
INPU0093
INPU0094
INPU0095
INPU0096
INPU0097
INPU0098
INPU0099
INPU0100
INPU0101
INPU0102
INPU0103
INPU0104
INPU0105
INPU0106
INPU0107
INPU0108

```

	WRITE(6,181)		INPU0109
191	FORMAT(///5X,45(1H*))		INPU0110
	GO TO (151,152,153,154,155),ICASE		INPU0111
151	WRITE(6,171)		INPU0112
171	FORMAT(9X,'WING')		INPU0113
	GO TO 180		INPU0114
152	WRITE(6,172)		INPU0115
172	FORMAT(9X,'BLADE',3X,'BEAM*CANTI',3X,'CHORD*CANTI')		INPU0116
	GO TO 180		INPU0117
153	WRITE(6,173)		INPU0118
173	FORMAT(9X,'BLADE',3X,'BEAM*CANTI',3X,'CHORD*HINGE')		INPU0119
	GO TO 180		INPU0120
154	WRITE(6,174)		INPU0121
174	FORMAT(9X,'BLADE',3X,'BEAM*HINGE',3X,'CHORD*CANTI')		INPU0122
	GO TO 180		INPU0123
155	WRITE(6,175)		INPU0124
175	FORMAT(9X,'BLADE',3X,'BEAM*HINGE',3X,'CHORD*HINGE')		INPU0125
180	CONTINUE		INPU0126
	WRITE(6,182)(DES(I),I=1,20)		INPU0127
182	FORMAT(/5X,45(1H*))///15X,20A4///)		INPU0128
	WRITE(6,9)		INPU0129
	WRITE(6,6(1))IPUNCH ,IGUEST		INPU0130
600	FORMAT(1X,'IPUNCH=',I1 ,5X,'IGUEST=',I1)		INPU0131
	WRITE(6,16) NDPN, NET, NITR, M, EPR		INPU0132
	WRITE(6,114) OMEG		INPU0133
114	FORMAT(6H OMEG=,F15.5)		INPU0134
	WRITE(6,300) RAMDA		INPU0135
300	FORMAT(8H LAMBDA=,F15.5)		INPU0136
	WRITE(6,301) COL		INPU0137
301	FORMAT(18H COLLECTIVE PITCH=,F15.5)		INPU0138
	WRITE(6,299) SPKR,SPKC		INPU0139
299	FORMAT(1X,'SPRING= ',F15.5,F15.5)		INPU0140
	WRITE(6,298) ALPHAH		INPU0141
298	FORMAT(1X,'ALPHAH=',F15.5)		INPU0142
	WRITE(6,183)		INPU0143
183	FORMAT(1X,'--FLAPPING BENDING STIFFNESS--')		INPU0144

	WRITE(6,105) (EIBE(I),I=1,NET)	INPU0145
	WRITE(6,184)	INPU0146
184	FORMAT(1X,'--CHORDWISE BENDING STIFFNESS--')	INPU0147
	WRITE(6,105) (EICE(I),I=1,NET)	INPU0148
	WRITE(6,185)	INPU0149
185	FORMAT(1X,'--ANGLE OF TWIST--')	INPU0150
	WRITE(6,104) (THETA(I),I=1,NET)	INPU0151
	THE=ATAN(RAMDA*4.0/3.0)+CDI.*SIGN(1.0,OMEG)	INPU0152
	DO 302 I=1,NET	INPU0153
302	THETA(I)=THETA(I)*SIGN(1.0,OMEG)+THE	INPU0154
	WRITE(6,186)	INPU0155
186	FORMAT(1X,'--MASS DISTRIBUTION--')	INPU0156
	WRITE(6,104) (AMASE(I),I=1,NET)	INPU0157
	WRITE(6,188)	INPU0158
188	FORMAT(1X,'--ELEMENT SIZE--')	INPU0159
	WRITE(6,104) (ESE(I),I=1,NET)	INPU0160
	WRITE(6,187)	INPU0161
187	FORMAT(8X,'TIP MASS',T19,'ROLL INERTIA',T34,'YAW INERTIA',	INPU0162
	8 T49,'PITCH INERTIA',T64,'MASS COUPLING')	INPU0163
	WRITE(6,104) AMN,PIR,PIY,PIP,PRW	INPU0164
	NN=NET+1	INPU0165
104	FORMAT(8F15.5)	INPU0166
105	FORMAT(5X,7E15 7)	INPU0167
	IF (NDPN .EQ. 4) GO TO 14	INPU0168
	WRITE(6,189)	INPU0169
189	FORMAT(1X,'--TORSIONAL RIGIDITY--')	INPU0170
	WRITE(6,105) (GJ(I),I=1,NET)	INPU0171
	WRITE(6,190)	INPU0172
190	FORMAT(1X,'--MOMENT OF INERTIA--')	INPU0173
	WRITE(6,105) (OI(I),I=1,NET)	INPU0174
	WRITE(6,191)	INPU0175
191	FORMAT(1X,'--MASS COUPLING ALONG SPAN--')	INPU0176
	WRITE(6,105) (PI12(I),I=1,NET)	INPU0177
9	FORMAT (/8H * * /12H INPUT DATA ///)	INPU0178
16	FORMAT (25H NO OF DEGRE PER NODE= , 13/	INPU0179
1	17H NO OF ELEMENTS=,13/24H NO OF MAX ITER ALLOEWD=,13	INPU0180

```

2 /14H NO OF MODES=, 13/ 6H ERR=, F15.5)
14 NDE=NDPN+NDPN
   NDT=NFT*NDPN+NDPN
   MNC=NDT*NDE-(NDE*NDE-NDE)/2
   DO 5 I=1,NFT
   NDPE(I)=NDE
   NII=NDE*I-NDE
   NDD=NDPN*I-NDPN
   NDDF(NII +1)=NDD+1
   NDDF(NII +5)=NDD+2
   NDDF(NII +2)=NDD+3
   NDDF(NII +6)=NDD+4
   NDDF(NII +3)=NDD+NDPN+1
   NDDF(NII +7)=NDD+NDPN+2
   NDDF(NII +4)=NDD+NDPN+3
   NDDF(NII +8)=NDD+NDPN+4
   IF (NDPN EQ 4) GO TO 5
   NDDF(NII +9)=NDD+5
   NDDF(NII +10)=NDD+6
   NDDF(NII +11)=NDD+NDPN+5
   NDDF(NII +12)=NDD+NDPN+6
5 CONTINUE
GO TO (501,502,503,504,505),ICASE
501 NBU=NDPN-1
   GO TO 506
502 NBU=4
506 DO 6 I=1,NBU
6 NBCU(I)=I
GO TO 507
503 NBU=3
   NBCU(1)=1
   NBCU(2)=2
   NBCU(3)=3
GO TO 507
504 NBU=3
   NBCU(1)=1

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INPU0181
INPU0182
INPU0183
INPU0184
INPU0185
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INPU0190
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INPU0192
INPU0193
INPU0194
INPU0195
INPU0196
INPU0197
INPU0198
INPU0199
INPU0200
INPU0201
INPU0202
INPU0203
INPU0204
INPU0205
INPU0206
INPU0207
INPU0208
INPU0209
INPU0210
INPU0211
INPU0212
INPU0213
INPU0214
INPU0215
INPU0216

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	NBCU(2)=2	INPU0217
	NBCU(3)=4	INPU0218
	GO TO 507	INPU0219
505	NBU=2	INPU0220
	NBCU(1)=1	INPU0221
	NBCU(2)=2	INPU0222
507	CONTINUE	INPU0223
	R=0	INPU0224
	DO 2 I=1,NET	INPU0225
2	R=R+ESE(I)	INPU0226
	TN(NET+1)=AMN*R*OMEG*OMEG	INPU0227
	DO 3 I=1,NET	INPU0228
	II=NET-I+1	INPU0229
	P=R-ESE(II)	INPU0230
3	TN(II)= TN(II+1) +AMASE(II)*(R+.5*ESE(II))*ESE(II)*OMEG*OMEG	INPU0231
	WRITE (6,15)	INPU0232
	WRITE(6,104) (TN(I),I=1,NN)	INPU0233
15	FORMAT(///' TENSION DUE TO CENTRIF FORCE')	INPU0234
	R=0.	INPU0235
	BI=0.	INPU0236
	BM=0	INPU0237
	DO 11 I=1,NET	INPU0238
	BM=BM+ AMASE(I)*ESE(I)	INPU0239
	RR=R+ESE(I)	INPU0240
	BI= BI+ AMASE(I)*(PR**3-R**3)*.33333333	INPU0241
11	R=RR	INPU0242
	BM=BM+AMN	INPU0243
	BI=BI+AMN*R*R	INPU0244
	WRITE (6,12) BM,BI,R	INPU0245
12	FORMAT('/' MASS =' ,E13.5/ ' MOMENT OF INERTIA AT ROOT=' ,F13.5/	INPU0246
	1 ' TOTAL LENGTH OF THE BEAM=' ,F13.5)	INPU0247
	RETURN	INPU0248
	END	INPU0249

SUBROUTINE ELEMK (EKT,EMT ,NDE,NE)

TO CONTROL THE GENERATION OF ELEMENT STIFFNESS AND MASS
MATRICES

NDF=8 FOR BLADE MODE
NDE=12 FOR WING MODE
COMMON/SPRING/SPKH,SPKC
COMMON/HELP/ALPHAH
DOUBLE PRECISION ALPHAH
DOUBLE PRECISION EKT,EMT
DIMENSION EKC(4,4),ETC(4,4) ,EMC(4,4),EKT(1),EMT(1)
DIMENSION EIBE(20),EICE(20), THETA(20),AMASE(20),ESE(20),TN(21)
DIMENSION GJ(20) , PI(20) ,PI12 (20)
COMMON /ELEM/ OMEG,EIBE,EICE,THETAE,AMASE,ESE,TN,GJ,PI, PI12,AMN,
1 PIR,PIY,PIP,PBW,BM,BI,R,NETT
NET=NETT
EIB=EIBE(NE)
EIC=EICE(NE)
THETA=THETA(NE)
AMAS=AMASE(NE)
ES=ESE(NE)
T= (TN(NE)+ TN(NE+1))*.5
ESS=ES*ES
IF (NDE .EQ.8) GO TO 9
GJE=GJ(NE)/ES
PIE=PI(NE) *ES
PI12E=PI12(NE) *ES
9 EKC(1,1)=12.
EKC(2,1)=6.*ES
EKC(3,1)=-12.
EKC(4,1)=6.*ES
EKC(2,2)=4.*ESS
EKC(3,2)=-6.*ES
EKC(4,2)=2.*ESS
EKC(3,3)=12.

ELEM0001
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ELEM0030
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ELEM0034
ELEM0035
ELEM0036

```

EKC(4,3)=-6.*ES
EKC(4,4)=4.*ESS
ETC(1,1)=1.2
ETC(2,1)=.1*ES
ETC(3,1)=-1.2
ETC(4,1)=.1*ES
ETC(2,2)=.13333333*ESS
ETC(3,2)=-.1*ES
ETC(4,2)=-.03333333*ESS
ETC(3,3)=1.2
ETC(4,3)=-.1*ES
ETC(4,4)=.13333333*ESS
EMC(1,1)=156./420.
EMC(2,1)=22./420.*FS
EMC(3,1)=54./420.
EMC(4,1)=-13./420.*ES
EMC(2,2)=4./420.*ESS
EMC(3,2)=-EMC(4,1)
EMC(4,2)=-3./420.*ESS
EMC(3,3)=EMC(1,1)
EMC(4,3)=-EMC(2,1)
EMC(4,4)=EMC(2,2)
DO 10 I=1,4
DO 10 J=1,4
EMC(J,I)=EMC(I,J)
EKC(J,I)=EKC(I,J)
ESSS=ESS*FS
SI=SIN(THETA)
CC=CCS(THETA)
B=(EIB*CC*CC +EIC*SI*SI)/ESSS
C=(EIC*CC*CC + EIB*SI*SI)/ESSS
BC=(EIC-EIB)*SI*CC/ESSS
TE=T/ES
AM=OMEG*OMEG*AMAS*ES
AMAE =AMAS*ES
DO 5 I=1,4

```

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ELEM0037
ELEM0038
ELEM0039
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ELEM0041
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ELEM0043
ELEM0044
ELEM0045
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ELEM0049
ELEM0050
ELEM0051
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ELEM0053
ELEM0054
ELEM0055
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ELEM0057
ELEM0058
ELEM0059
ELEM0060
ELEM0061
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ELEM0064
ELEM0065
ELEM0066
ELEM0067
ELEM0068
ELEM0069
ELEM0070
ELEM0071
ELEM0072

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	II=(I*I-I)/2	ELEM0073
	I4=(I+4)*(I+3)/2	ELEM0074
	DC 1 J=1, I	ELEM0075
	EKT(I1+J)= B*FKC(I,J)+TE*ETC(I,J)	ELEM0076
	EMT(I1+J)= AMAE*EMC(I,J)	ELEM0077
	EKT(I4+J+4)= C*EKC(I,J) + TE*ETC(I,J) -AM*EMC(I,J)	ELEM0078
1	EMT(I4+J+4)= AMAE*EMC(I,J)	ELEM0079
	DC 2 J=1,4	ELEM0080
	EMT(I4+J)=0.	ELEM0081
2	EKT(I4+J)=BC*EKC(I,J)	ELEM0082
	IF (NDE .EQ. 8) GO TO 5	ELEM0083
	I8=(I+8)*(I+7)/2	ELEM0084
	DC 3 J=1, I	ELEM0085
	EKT(I8+J+8)=GJE*ETC(I,J)	ELEM0086
3	EMT(I8+J+8)= PIE *EMC(I,J)	ELEM0087
	DC 4 J=1,4	ELEM0088
	EKT(I8+J)=0.	ELEM0089
	EKT(I8+J+4)=0.	ELEM0090
	EMT(I8+J+4)=0.	ELEM0091
4	EMT(I8+J)=PII2E*EMC(I,J)	ELEM0092
5	CONTINUE	ELEM0093
	IF(NE.LT.NET) GO TO 100	ELEM0094
	EMT(6)= EMT(6)+AMN	ELEM0095
	EMT(28) =EMT(28)+AMN	ELEM0096
	IF(NDE.EQ.8) GO TO 100	ELEM0097
	EMT(10) =EMT(10)+ PIR	ELEM0098
	EMT(36) =EMT(36)+ PIY	ELEM0099
	EMT(66)= EMT(66)+PIP	ELEM0100
	EMT(58)= EMT(58)+ PBW	ELEM0101
100	IF(NE.GT.1) GO TO 101	ELEM0102
	EKT(3)=EKT(3)+SPKB	ELEM0103
	EKT(21)=EKT(21)+SPKC	ELEM0104
101	DC 102 I=1,36	ELEM0105
102	EKT(I)=EKT(I)+EMT(I)*ALPHAH	ELEM0106
	RETURN	ELEM0107
	END	ELEM0108

SUBROUTINE MESH(NDPE,NET,NDT,NCOT,MNC,MN, NBD,NNODE,ICOL,INUM,
@NBU, INDEX)

C
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C

TO CALCULATE MESH INFORMATION OF THE FINITE ELEMENT

DIMENSION NOD(1),NNODE(1),ICOL(1),INUM(1), NDPE(1)
IF(NBU .GT. 0) GO TO 100
DO 99 I=1,NDT
99 NOD(I)=1
NCOT=NDT
GO TO 98
100 DO 22 I=1,NBU
IF (I .GE. NBU) GO TO 101
I1=I+1
DO 21 J=I1,NBU
IF (INUM(I).NE.INUM(J)) GO TO 21
IF (J.GE.NBU) GO TO 20
J1=J+1
DO 19 K=J1,NBU
19 INUM(K-1)= INUM(K)
20 NBU=NBU-1
J=J-1
21 CONTINUE
22 CONTINUE
101 DO 1 I=1,NDT
1 NOD(I)=1
DO 2 I=1,NBU
I1=INUM(I)
2 NOD(I1)=0
DO 3 I=2,NDT
3 NOD(I)=NOD(I)+NOD(I-1)
NCOT=NDT-NBU
DO 4 I=1,NBU
I1=INUM(I)
4 NOD(I1)=NCOT+I
98 CONTINUE

MESH0001
MESH0002
MESH0003
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MESH0014
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MESH0020
MESH0021
MESH0022
MESH0023
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MESH0025
MESH0026
MESH0027
MESH0028
MESH0029
MESH0030
MESH0031
MESH0032
MESH0033
MESH0034
MESH0035
MESH0036

```

      II=0
      DO 5 I=1,NET
      JJ=NDPE(I)
      DO 54 J=1,JJ
54  ICOL(J)=NNODE(J+II)
      DO 55 J=1,JJ
      J1=ICOL(J)
55  NNODE(J+II)=NJC(J1)
      5  II=II+JJ
      DO 6 I=1,NCDT
      6  ICOL(I)=I
      II=0
      DO 88 I=1,NET
      JJ=NDPE(I)
      IMIN=NDT
      DO 7 J=1,JJ
      IN=NNODE(J+II)
      7  IF(IN .LT. IMIN) IMIN=IN
      DO 8 J=1,JJ
      ID=NNODE(J+II)
      8  IF(ICOL(ID) .GT. IMIN) ICOL(ID)=IMIN
38  II=II+JJ
      INUM(1)=0
      DO 9 I=2,NCDT
      9  INUM(I)=INUM(I-1)+I-ICOL(I)
      MN=INUM(NCDT)+NCDT
      WRITE(6,10) MN,MNC
10  FORMAT(/2X,'MAX. SIZE OF STF IS ',I6,5X,'SPECIFIED SIZE IS ',I6)
      INDEX=1
      IF(MNC .LT. MN) INDEX=0
      RETURN
      END

```

```

MESH0037
MESH0038
MESH0039
MESH0040
MESH0041
MESH0042
MESH0043
MESH0044
MESH0045
MESH0046
MESH0047
MESH0048
MESH0049
MESH0050
MESH0051
MESH0052
MESH0053
MESH0054
MESH0055
MESH0056
MESH0057
MESH0058
MESH0059
MESH0060
MESH0061
MESH0062
MESH0063
MESH0064
MESH0065
MESH0066
MESH0067
MESH0068

```

SUBROUTINE ASBV(STK,STM,IEQ,EK,EM, NDPE,NDT,NCDT,NNODE,MN,NET,IN
NUM)

TO ASSEMBLE AND CONSTRAIN BOUNDARY CONDITIONS

IMPLICIT REAL*8(A-H,O-Z)
DIMENSION STK(1),STM(1),EK(1),EM(1), NDPE(1),NNODE(1),INUM(1)
ID=NCDT+1
DO 1 I=1,MN
STK(I)=0.0
1 STM(I)=0.0
II=0
DO 15 N=1,NET
JJ=NDPE(N)
IF(IEQ .EQ. 0) GO TO 3
IF(N .GT. 1) GO TO 8
3 CALL FLEMK(EK,EM,JJ,N)
8 DO 14 I=1,JJ
KI=(I+II-1)/2
KMA=NNODE(KI+1)
IF(KMA .GE. ID) GO TO 14
DO 13 J=1,I
KNA=NNODE(KI+J)
IF(KNA .GE. ID) GO TO 13
KA=INUM(KMA)+KNA
IF(KNA .GT. KMA) KA=INUM(KNA)+KMA
STK(KA)=STK(KA)+EK(KI+J)
STM(KA)=STM(KA)+EM(KI+J)
13 CONTINUE
14 CONTINUE
15 II=JJ+II
RETURN
END

ASBV0001
ASBV0002
ASBV0003
ASBV0004
ASBV0005
ASBV0006
ASBV0007
ASBV0008
ASBV0009
ASBV0010
ASBV0011
ASBV0012
ASBV0013
ASBV0014
ASBV0015
ASBV0016
ASBV0017
ASBV0018
ASBV0019
ASBV0020
ASBV0021
ASBV0022
ASBV0023
ASBV0024
ASBV0025
ASBV0026
ASBV0027
ASBV0028
ASBV0029
ASBV0030
ASBV0031
ASBV0032
ASBV0033

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C

C
C
C

SUBROUTINE FAC(STF,NDT,NNDG,ICOL,INUM,U)

FACTURING A SYSMETRIC MATRIX INTO LDL#

IMPLICIT REAL*8(A-F,D-Z)

DIMENSION STF(1),ICOL(1),INUM(1),U(1)

NNDG=C

IF(STF(1)) 2,1,3

1 IZR=1

99 WRITE(6,100) IZR

100 FORMAT(/2X,'THE',I4,'TH DIAG. AFTER FACT.=0.0,INCOMPLETE FACT.')

NNDG=-1

RETURN

2 NNDG=1

3 IF(NDT .LT. 2) GO TO 11

DO 10 IR=2,NDT

II=ICOL(IR)

IF(II .EQ. IR) GO TO 10

JR=INUM(IR)

IE=IR-1

DO 5 IC=II,IE

IMAX=II

IF(II .LT. ICOL(IC)) IMAX=ICOL(IC)

JE=IC-1

SUM=STF(JR+IC)

IF(JE .LT. IMAX) GO TO 55

JC=INUM(IC)

DO 4 J=IMAX,JE

4 SUM=SUM-U(J)*STF(JC+J)

55 U(IC)=SUM

5 STF(JR+IC)=SUM/STF(INUM(IC)+IC)

JJ=JR+IR

DO 6 J=II,IF

6 STF(JJ)=STF(JJ)-U(J)*STF(JR+J)

IF(STF(JJ)) 8,7,10

7 IZR=IR

08

FACT0001
FACT0002
FACT0003
FACT0004
FACT0005
FACT0006
FACT0007
FACT0008
FACT0009
FACT0010
FACT0011
FACT0012
FACT0013
FACT0014
FACT0015
FACT0016
FACT0017
FACT0018
FACT0019
FACT0020
FACT0021
FACT0022
FACT0023
FACT0024
FACT0025
FACT0026
FACT0027
FACT0028
FACT0029
FACT0030
FACT0031
FACT0032
FACT0033
FACT0034
FACT0035
FACT0036

```
GO TO 99
8 NNDG=NNDG+1
10 CONTINUE
11 WRITE(6,101) NNDG
101 FORMAT(/2X,'NO. OF NEGATIVE DIAGS.=' ,I4,5X,'FACT. COMPLETED')
RETURN
END
```

```
FACT0037
FACT0038
FACT0039
FACT0040
FACT0041
FACT0042
FACT0043
```


SUBROUTINE MTRTR(M,N,RP,XLR,X,IST)

MATRIX MULTIPLICATION

IMPLICIT REAL*8(A-H,O-Z)
DIMENSION RM(1),XLR(1),X(1)
DO 2 I=IST,M
II=(I-1)*N
IJ=(I-1)*M
DO 2 J=1,I
JJ=(J-1)*N
RM(IJ+J)=C.O
DO 2 K=1,N
2 RM(IJ+J)=RM(IJ+J)+XLR(II+K)*X(JJ+K)
DO 3 I=IST,M
JJ=(I-1)*M
DO 3 J=1,I
3 RM((J-1)*M+I)=RM(JJ+J)
RETURN
END

MTRT0001
MTRT0002
MTRT0003
MTRT0004
MTRT0005
MTRT0006
MTRT0007
MTRT0008
MTRT0009
MTRT0010
MTRT0011
MTRT0012
MTRT0013
MTRT0014
MTRT0015
MTRT0016
MTRT0017
MTRT0018
MTRT0019
MTRT0020

SUBROUTINE MULTZ(STF,X,Y,NDT,M,ICOL,INUM,MM)

C
C
C

MATRIX MULTIPLICATION

IMPLICIT REAL*8(A-H,O-Z)
DIMENSION STF(1),X(1),Y(1),ICOL(1),INUM(1)
DO 1 I=1,NDT
1 Y(I)=0.0
MM=MM+MM-1
DO 4 I=MM,MMM
II=(I-1)*NDT
DO 3 IR=1,NDT
IS=INUM(IR)
IC=ICOL(IR)
IF=IR-1
IF(IC.GT.IE) GO TO 3
DO 2 J=IC,IE
S=STF(IS+J)
Y(IR)=Y(IR)+S*X(II+J)
2 Y(J)=Y(J)+S*X(II+IR)
3 Y(IR)=Y(IR)+STF(IS+IR)*X(II+IR)
DO 4 J=1,NDT
X(II+J)=Y(J)
4 Y(J)=0.0
RETURN
END

MULT0001
MULT0002
MULT0003
MULT0004
MULT0005
MULT0006
MULT0007
MULT0008
MULT0009
MULT0010
MULT0011
MULT0012
MULT0013
MULT0014
MULT0015
MULT0016
MULT0017
MULT0018
MULT0019
MULT0020
MULT0021
MULT0022
MULT0023
MULT0024
MULT0025
MULT0026

C
C
C

```
SUBROUTINE SOLZ(STF,U,NDT,M,ICOL,INUM,MM)
SOLVE (LDL*)(U)=U FOR GIVEN U OF M VECTORS OF LENGTH NDT

IMPLICIT REAL*8(A-H,O-Z)
DIMENSION STF(1),U(1),ICOL(1),INUM(1)
MM=MM+MM-1
IF(NDT.LT.2) GO TO 3
DO 2 IR=2,NDT
JI=ICOL(IR)
JE=IR-1
IF(JI.GT.JE) GO TO 2
DO 1 I=MM,MMM
II=(I-1)*NDT
IS=II+IR
DO 1 J=JI,JE
1 U(IS)=U(IS)-STF(INUM(IR)+J)*U(II+J)
2 CONTINUE
3 DO 4 I=MM,MMM
II=(I-1)*NDT
DO 4 IR=1,NDT
4 U(II+IR)=U(II+IR)/STF(INUM(IR)+IR)
IF(NDT.LT.2) GO TO 7
DO 6 IK=2,NDT
IR=NDT-IK+2
JI=ICOL(IR)
JE=IR-1
IF(JI.GT.JE) GO TO 6
DO 5 I=MM,MMM
II=(I-1)*NDT
IS=II+IR
DO 5 J=JI,JE
5 U(II+J)=U(II+J)-STF(INUM(IR)+J)*U(IS)
6 CONTINUE
7 RETURN
END
```

SOLZ0001
SOLZ0002
SOLZ0003
SOLZ0004
SOLZ0005
SOLZ0006
SOLZ0007
SOLZ0008
SOLZ0009
SOLZ0010
SOLZ0011
SOLZ0012
SOLZ0013
SOLZ0014
SOLZ0015
SOLZ0016
SOLZ0017
SOLZ0018
SOLZ0019
SOLZ0020
SOLZ0021
SOLZ0022
SOLZ0023
SOLZ0024
SOLZ0025
SOLZ0026
SOLZ0027
SOLZ0028
SOLZ0029
SOLZ0030
SOLZ0031
SOLZ0032
SOLZ0033
SOLZ0034
SOLZ0035
SOLZ0036

C
C
C

SUBROUTINE DNRCOT(M,A,B,XL,X)

EIGENVALUE ANALYSIS ROUTINE

DIMENSION A(1),B(1),XL(1),X(1)

DOUBLE PRECISION A,B,XL,X,SUMV

K=1

DO 100 J=2,M

L=M*(J-1)

DO 100 I=1,J

L=L+1

K=K+1

100 B(K)=B(L)

MV=0

CALL EIGEN (B,X,M,MV)

L=0

DO 110 J=1,M

L=L+J

110 XL(J)=1.0/DSQRT(CABS(B(L)))

K=J

DO 115 J=1,M

DO 115 I=1,M

K=K+1

115 B(K)=X(K)*XL(J)

DO 120 I=1,M

N2=0

DO 120 J=1,M

N1=M*(I-1)

L=M*(J-1)+I

X(L)=0.0

DO 120 K=1,M

N1=N1+1

N2=N2+1

120 X(L)=X(L)+B(N1)*A(N2)

L=0

DO 130 J=1,M

DNRO0001

DNRO0002

DNRO0003

DNRO0004

DNRO0005

DNRO0006

DNRO0007

DNRO0008

DNRO0009

DNRO0010

DNRO0011

DNRO0012

DNRO0013

DNRO0014

DNRO0015

DNRO0016

DNRO0017

DNRO0018

DNRO0019

DNRO0020

DNRO0021

DNRO0022

DNRO0023

DNRO0024

DNRO0025

DNRO0026

DNRO0027

DNRO0028

DNRO0029

DNRO0030

DNRO0031

DNRO0032

DNRO0033

DNRO0034

DNRO0035

DNRO0036

85

```

DO 130 I=1,J
N1=I-M
N2=M*(J-1)
L=L+1
A(L)=0.0
DO 130 K=1,M
N1=N1+M
N2=N2+1
130 A(L)=A(L)+X(N1)*B(N2)
CALL EIGEN (A,X,M,MV)
L=0
DO 140 I=1,M
L=L+I
140 XL(I)=A(L)
DO 150 I=1,M
N2=0
DO 150 J=1,M
N1=I-M
L=M*(J-1)+I
A(L)=0.0
DO 150 K=1,M
N1=N1+M
N2=N2+1
150 A(L)=A(L)+B(N1)*X(N2)
L=0
K=0
DO 180 J=1,M
SUMV=0.0
DO 170 I=1,M
L=L+1
170 SUMV=SUMV+A(L)*A(L)
175 SUMV=DSQRT(SUMV)
DO 180 I=1,M
K=K+1
180 X(K)=A(K)/SUMV
RETURN
END

```

```

DNR00037
DNR00038
DNR00039
DNR00040
DNR00041
DNR00042
DNR00043
DNR00044
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DNR00065
DNR00066
DNR00067
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DNR00070
DNR00071
DNR00072
DNR00073

```

C C C	SUBROUTINE EIGEN(A,R,N,MV) EIGENVALUE ANALYSIS ROUTINE NEEDED IN DNROOT DIMENSION A(1),R(1) DOUBLE PRECISION A,R,ANORM,ANRMX,THR,X,Y,SINX,SINX2,CO SX, 1 COSX2,SINCS,RANGE 5 RANGE=1.0E-12 IF(MV-1) 10,25,10 10 IQ=-N DO 20 J=1,N IQ=IQ+N DO 20 I=1,N IJ=IQ+I R(IJ)=0.0 IF(I-J) 20,15,20 15 R(IJ)=1.0 20 CONTINUE 25 ANORM=0.0 DO 35 I=1,N DO 35 J=I,N IF(I-J) 30,35,30 30 IA=I+(J-J)/2 ANORM=ANORM+A(IA)*A(IA) 35 CONTINUE IF(ANORM) 165,165,40 40 ANCRM=1.414*DSQRT(ANORM) ANRMX=ANCRM*RANGE/FLOAT(N) IND=0 THR=ANCRM 45 THR=THR/FLOAT(N) 50 L=1 55 M=L+1 60 MQ=(M*M-M)/2 LQ=(L*L-L)/2 LM=L+MQ	EIGEO001 EIGEO002 EIGEO003 EIGEO004 EIGEO005 EIGEO006 EIGEO007 EIGEO008 EIGEO009 EIGEO010 EIGEO011 EIGEO012 EIGEO013 EIGEO014 EIGEO015 EIGEO016 EIGEO017 EIGEO018 EIGEO019 EIGEO020 EIGEO021 EIGEO022 EIGEO023 EIGEO024 EIGEO025 EIGEO026 EIGEO027 EIGEO028 EIGEO029 EIGEO030 EIGEO031 EIGEO032 EIGEO033 EIGEO034 EIGEO035 EIGEO036
-------------	--	--

62	IF (DABS(A(LM))-THR) 130,65,65	EIGEO037
65	IND=1	EIGEO038
	LL=L+LQ	EIGEO039
	MM=M+MQ	EIGEO040
	X=0.5*(A(LL)-A(MM))	EIGEO041
68	Y=-A(LM)/DSQRT(A(LM)*A(LM)+X*X)	EIGEO042
	IF (X) 70,75,75	EIGEO043
70	Y=-Y	EIGEO044
75	SINX=Y/DSQRT(2.0*(1.0+(DSQRT(1.0-Y*Y))))	EIGEO045
	SINX2=SINX*SINX	EIGEO046
78	COSX=DSQRT(1.0-SINX2)	EIGEO047
	COSX2=COSX*COSX	EIGEO048
	SINCS =SINX*COSX	EIGEO049
	ILQ=N*(L-1)	EIGEO050
	IMQ=N*(M-1)	EIGEO051
	DO 125 I=1,N	EIGEO052
	IQ=(I+1-1)/2	EIGEO053
	IF (I-L) 80,115,80	EIGEO054
80	IF (I-M) 85,115,90	EIGEO055
85	IM=I+MQ	EIGEO056
	GO TO 95	EIGEO057
90	IM=M+IQ	EIGEO058
95	IF (I-L) 100,105,105	EIGEO059
100	IL=I+LQ	EIGEO060
	GO TO 110	EIGEO061
105	IL=L+IQ	EIGEO062
110	X=A(IL)*COSX-A(IM)*SINX	EIGEO063
	A(IM)=A(IL)*SINX+A(IM)*COSX	EIGEO064
	A(IL)=X	EIGEO065
115	IF (MV-1) 120,125,120	EIGEO066
120	ILR=ILQ+I	EIGEO067
	IMR=IMQ+I	EIGEO068
	X=R(ILR)*COSX-R(IMR)*SINX	EIGEO069
	R(IMR)=R(ILR)*SINX+R(IMR)*COSX	EIGEO070
	R(ILR)=X	EIGEO071
125	CONTINUE	EIGEO072

```

X=2.0*A(LM)*SINCS
Y=A(LL)*COSX2+A(MM)*SINX2-X
X=A(LL)*SINX2+A(MM)*COSX2+X
A(LM)=(A(LL)-A(MM))*SINCS+A(LM)*(COSX2-SINX2)
A(LL)=Y
A(MM)=X
130 IF(M=N) 135,140,135
135 M=M+1
GO TO 60
140 IF(L=(N-1)) 145,150,145
145 L=L+1
GO TO 45
150 IF(I=ND-1) 160,155,160
155 I=ND
GO TO 50
160 IF(THP-ANRMX) 165,165,45
165 IQ=-N
DO 135 I=1,N
IQ=IQ+N
LL=I+(I-1)/2
JQ=N*(I-2)
DO 185 J=1,N
JQ=JQ+N
MM=J+(J-J)/2
IF(A(LL)-A(MM)) 170,185,185
170 X=A(LL)
A(LL)=A(MM)
A(MM)=X
IF(MV-1) 175,185,175
175 DO 180 K=1,N
ILR=IQ+K
IMR=JQ+K
X=R(ILR)
R(ILR)=R(IMR)
180 R(IMR)=X
185 CONTINUE
RETURN
END

```

```

EIGEO073
EIGEO074
EIGEO075
EIGEO076
EIGEO077
EIGEO078
EIGEO079
EIGEO080
EIGEO081
EIGEO082
EIGEO083
EIGEO084
EIGEO085
EIGEO086
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EIGEO105
EIGEO106
EIGEO107
EIGEO108
EIGEO109
EIGEO110

```


	SUBROUTINE OUTPUT(KKK,M,NCDT,NDT,NOD,NNODE,EPR,XLR,U,SRM,SRK)	OUTPG001
C	OUTPUT ROUTINE	OUTPG002
C	COMMON /PUNCH/ IPUNCH	OUTPG003
C	COMMON /BW/ ICASE , IGUEST	OUTPG004
	DOUBLE PRECISION XLR,SRM,SRK ,U ,ERR	OUTPG005
	DIMENSION XLR(1),U(1), SRM(1), SRK(1)	OUTPG006
	DIMENSION NOD(1),NNODE(1)	OUTPG007
	DIMENSION XXLF(15,120)	OUTPG008
	IDERUG=0	OUTPG009
	WRITE(6,24) KKK,ERR	OUTPG010
	24 FORMAT(/2X,'NO. OF ITERATION=',I4,2X,'CONVERGED WITHIN',D13.5)	OUTPG011
	IF(IDERUG.EQ.0) GO TO 15	OUTPG012
	WRITE(6,12)	OUTPG013
	12 FORMAT(/2X,'EIGENVECTORS=',/)	OUTPG014
	DO 14 I=1,M	OUTPG015
	II=(I-1)*NCDT	OUTPG016
	14 WRITE(6,13) (XLR(II+J),J=1,NCDT)	OUTPG017
	13 FORMAT(/,(2X,10D13.5))	OUTPG018
96	15 CONTINUE	OUTPG019
	WRITE(6,20)	OUTPG020
	DO 18 I=1,M	OUTPG021
	KK=I*M-M	OUTPG022
	18 WRITE (6,16) (SRM(J+KK) , J=1,I)	OUTPG023
	WRITE(6,21)	OUTPG024
	DO 19 I=1,M	OUTPG025
	KK=I*M-M	OUTPG026
	19 WRITE (6,16) (SRK(J+KK) ,J=1,I)	OUTPG027
	16 FORMAT (2X,10D13.5)	OUTPG028
	20 FORMAT (/ 23H REDUCED MASS MATRIX /)	OUTPG029
	21 FORMAT (/ 23H REDUCED STIF MATRIX /)	OUTPG030
	NBU=NDT-NCDT	OUTPG031
	GO TO (101,101,101,102,101),ICASE	OUTPG032
101	DO 100 I=1,M	OUTPG033
	DO 201 J=1,NBU	OUTPG034
		OUTPG035
		OUTPG036

```

201  XXLR(I,J)=0.0
CONTINUE
DO 202 J=1,NCDT
202  XXLR(I,NBU+J)=XLR((I-1)*NCDT+J)
100  CONTINUE
GO TO 205
102  DO 203 I=1,M
DO 206 J=1,NBU
206  XXLR(I,J)=0.0
XXLR(I,3)=XLR((I-1)*NCDT+1)
DO 204 J=2,NCDT
204  XXLR(I,J+NBU)=XLR((I-1)*NCDT+J)
203  CONTINUE
205  CONTINUE
IF(ICASE.EQ.1) GO TO 333
NOM=4
NODE=NDT/NOM
WRITE(6,350)
350  FORMAT(///1X,'**** BLADE MODE SHAPES ****')
DO 351 I=1,M
WRITE(6,450C)I
4500  FORMAT(///1X,'I=',I2//)
WRITE(6,490C)
4900  FORMAT(T5,'K',T12,'W(I,J)',T33,'V(I,J)', T53,'DW(I,J)', T73,
& 'DV(I,J)')
DO 351 K=1,NODE
WRITE(6,352) K,(XXLR(I,NOM*(K-1)+J),J=1,NOM)
352  FORMAT((1X,I4,6(5X,{15.7}))
351  CONTINUE
GO TO 360
333  CONTINUE
NOM=6
NODE=NDT/NOM
WRITE(6,353)
353  FORMAT(///1X,'**** WING MODE SHAPES ****')
DO 354 I=1,M

```

```

OUTPUT0037
OUTPUT0038
OUTPUT0039
OUTPUT0040
OUTPUT0041
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OUTPUT0069
OUTPUT0070
OUTPUT0071
OUTPUT0072

```

	WRITE(6,450) I	OUTP0073
	WRITE(6,4901)	OUTP0074
4901	FORMAT(T5,'K',T12,'W(I,J)',T33,'V(I,J)', T53,'DW(I,J)', T73,	OUTP0075
	& 'DV(I,J)',T53,'PHI(I,J)',T112,'DPHI(I,J)')	OUTP0076
	DO 355 K=1,NODE	OUTP0077
	WRITE(6,352) K,(XXLR(I,NOM*(K-1)+J),J=',NOM)	OUTP0078
355	CONTINUE	OUTP0079
354	CONTINUE	OUTP0080
360	CONTINUE	OUTP0081
	IF(IPUNCH.EQ.0) GO TO 370	OUTP0082
	DO 359 I=1,M	OUTP0083
	DO 358 K=1,NOM	OUTP0084
	WRITE(7,357)(XXLR(I,NOM*(J-1)+K),J=1,NODE)	OUTP0085
357	FORMAT(6E13.5)	OUTP0086
358	CONTINUE	OUTP0087
359	CONTINUE	OUTP0088
370	CONTINUE	OUTP0089
	WRITE(6,371)	OUTP0090
371	FORMAT(IH1)	OUTP0091
	RETURN	OUTP0092
	END	OUTP0093

A.2 The TILDYN Program Listing

MAIN0001
MAIN0002
MAIN0003
MAIN0004
MAIN0005
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PROGRAM ROTOR
PART 2 ; PROGRAM TILDYN

PURPOSE
TO ANALYZE THE TILT-ROTOR DYNAMIC SYSTEM BY MEANS
OF FREQUENCY RESPONSE AND EIGENVALUES IN POWERED
AND AUTOROTATION FLIGHT

DEVELOPED BY MASAHIRO YASUE
OF AERDYNAMIC AND STRUCTURES RESEARCH LABORATORY
AUGUST 1974
ADDRESS ; BLG 41-211
MASSACHUSETTS INSTITUTE OF TECHNOLOGY
CAMBRIDGE, MASS. 02139

.....

MAIN PROGRAM

TO DEFINE THE SEQUENCE OF THE PROGRAM

```
COMMON/DDF18/AAZ(19,19),BBY(19,19),CCY(19,19),LDY(19,6)
DIMENSION CGUST(6) ,DDZ(19)
COMMON /PARMT/ ITYPE ,IFLT
1 CONTINUE
5001 FORMAT(1F1)
CALL INITIL
CALL COEFF
CALL INPUT(CGUST,IDDZ,IRCS,IEIGEN)
CALL INTPL
WRITE(6,5001)
```

```

CALL AEROBT
CALL ORDINT
WRITE(6,5001)
CALL      AINER
CALL      AEROMT
CALL EQMTX(IDOF)
IF(IFLT.EQ.C) GO TO 400
CALL AUTO(IDOF)
400  CONTINUE
     IDIM=IDOF+IFLT
     IF (IPES.EQ.0) GO TO 200
     WRITE(6,5001)
     CALL GUSTCO(CGUST,DDY,IDIM,DDZ)
     CALL FRQRES(IDIM,AAY,BBY,CCY,DDZ,IFLT, IDOF)
200  CONTINUE
     IF (IEIGEN.EQ.0) GO TO 1000
     WRITE(6,5001)
     CALL EIGEN(IDIM,AAY,BBY,CCY,DDY, IDOF)
1000 CONTINUE
     WRITE(6,5001)
     GO TO 1
     END

```

```

MAIN0037
MAIN0038
MAIN0039
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MAIN0055
MAIN0056
MAIN0057
MAIN0058

```

BLOCK DATA

TO INITIALIZE THE COEFFICIENTS OF GAUSSIAN QUADRATURE

COMMON /AREA2/NPT,XXX(20),A(20)

DATA NPT/11/

DATA A(1),A(2),A(3),A(4),A(5),A(6)/0.055668,

0.125580 ,0.186290, 0.233193 ,0.262804 , 0.272925 /

END

BLOC0001
BLOC0002
BLOC0003
BLOC0004
BLOC0005
BLOC0006
BLOC0007
BLOC0008
BLOC0009

SUBROUTINE INITIL

INITIALIZATION OF THE MATRICES

COMMON/DOF18/AAY(19,19),BBY(19,19),CCY(19,19),DDY(19,6)
COMMON/INERTI/TTMT(4,6,3),TTCTJ(4,6,3),AMJT(4,3,6),CJT(4,3,6)
COMMON /ARR/WGUST(6,6),DAMX(6,6),AMX(6,6),DQ(4,6,3),Q(4,6,3)
@ ,DHMAX(4,3,6),HMAX(4,3,6)
COMMON/WINGAR/TSOS(20,6,6),TSAS(20,6,6),TSAG(20,6,3)
DO 10 I=1,4
DO 10 J=1,6
DO 10 K=1,3
TTMT(I,J,K)=0.0
TTCTJ(I,J,K)=0.0
AMJT(I,K,J)=0.0
CJT(I,K,J)=0.0
DQ(I,J,K)=0.0
Q(I,J,K)=0.0
DHMAX(I,K,J)=0.0
HMAX(I,K,J)=0.0
CONTINUE
DO 11 I=1,6
DO 11 J=1,6
WGUST(I,J)=0.0
DAMX(I,J)=0.0
AMX(I,J)=0.0
DO 11 K=1,20
TSOS(K,I,J)=0.0
TSAS(K,I,J)=0.0
CONTINUE
DO 12 I=1,20
DO 12 J=1,6
DO 12 K=1,3
TSAG(I,J,K)=0.0
CONTINUE
DO 13 I=1,19

INIT0001
INIT0002
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INIT0036


```
DO 14 J=1,15
  AAY(I,J)=0.0
  RBY(I,J)=0.0
  CCY(I,J)=0.0
14  CONTINUE
  DO 15 K=1,6
  DDY(I,K)=0.0
15  CONTINUE
13  CONTINUE
  RETURN
  END
```

```
INIT0037
INIT0038
INIT0039
INIT0040
INIT0041
INIT0042
INIT0043
INIT0044
INIT0045
INIT0046
INIT0047
```

```

SUBROUTINE COEFF
      TO DEFINE THE POINTS AND COEFFICIENTS OF GAUSSIAN QUADRATURE

      DIMENSION Y(20),YY(20)
      COMMON /AREA2/NPT,XXX(20),A(20)
      NPTH=NPT/2
      IF((FLOAT(NPTH)-NPT/2.0).NE.0.0)GO TO 100
      READ(5,5000)(Y(I),I=1,NPTH),(A(J),J=1,NPTH)
5000  FORMAT(8F10.5)
      DO 10 I=1,NPTH
      Y(NPTH+I)=-Y(NPTH-I+1)
      A(NPTH+I)=A(NPTH-I+1)
      10 CONTINUE
      GO TO 200
      100 NPTH1=NPTH+1
      DATA Y(1),Y(2),Y(3),Y(4),Y(5),Y(6)/0.978228,
      *      0.897002 , 0.730152 , 0.519096 , 0.269543 , 0.0 /
      DO 20 MM=1,NPTH
      A(NPTH+MM+1)=A(NPTH-MM+1)
      Y(NPTH+MM+1)=-Y(NPTH-MM+1)
      20 CONTINUE
      200 DO 50 KK=1,NPT
      YY(KK)=Y(KK)
      50 CONTINUE
      DO 60 IN=1,NPT
      Y(IN)=YY(NPT-IN+1)
      60 CONTINUE
      DO 30 JJJ=1,NPT
      XXX(JJJ)=(Y(JJJ)+1.0)/2.0
      30 CONTINUE
      RETURN
      END

```

```

COEF0001
COEF0002
COEF0003
COEF0004
COEF0005
COEF0006
COEF0007
COEF0008
COEF0009
COEF0010
COEF0011
COEF0012
COEF0013
COEF0014
COEF0015
COEF0016
COEF0017
COEF0018
COEF0019
COEF0020
COEF0021
COEF0022
COEF0023
COEF0024
COEF0025
COEF0026
COEF0027
COEF0028
COEF0029
COEF0030
COEF0031
COEF0032
COEF0033

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SUBROUTINE INPUT(CGUST, IDOF, IRES, IEIGEN)

C		INPU0001
C		INPU0002
C	TO SUPPLY INPUT INFORMATION	INPU0003
C		INPU0004
C		INPU0005
C	DES = IDENTIFYING INFORMATION	INPU0006
C	ITYPE=0:HINGELSS ROTOR IN POWERED FLIGHT	INPU0007
C	ITYPE=1:HINGELSS ROTOR IN AUTOROTATIONAL FLIGHT	INPU0008
C	GIMBALLED ROTOR IN BOTH FLIGHTS	INPU0009
C	IFLT =0 : POWERED FLIGHT IFLT=1 : AUTOROTATION FLIGHT	INPU0010
C	IDOF =9 : BASIC DEGREES OF FREEDOM IS 9 IDOF=18 : DOF IS 18	INPU0011
C	IRES =0 : FREQUENCY RESPONSE OFF IRES=1 : RESPONSE ON	INPU0012
C	IFRMAG=0 : MODE NORMALIZED ROTOR RADIUS AND WING SEMISPAN	INPU0013
C	IFRMAG=1 : NORMAL MODES	INPU0014
C	IEIGEN=0 : EIGENANALYSIS OFF IEIGEN=1 : EIGENANALYSIS ON	INPU0015
C		INPU0016
C	NOBLD= NUMBER OF BLADES	INPU0017
C	POH= AIR DENSITY	INPU0018
C	OMEGA= ROTATIONAL SPEED (RAD/SEC)	INPU0019
C	RAMDA= INFLOW RATIO	INPU0020
C	VEI= CRUISING FLIGHT SPEED	INPU0021
C	R= ROTOR RADIUS	INPU0022
C	AIB= BLADE FLAPPING MOMENT OF INERTIA	INPU0023
C	CHOD= BLADE CHORD	INPU0024
C	CL= BLADE LIFT CURVE SLOPE	INPU0025
C	CD= BLADE DRAG COEFFICIENT	INPU0026
C	HMAST= MAST HEIGHT	INPU0027
C	DFL3= PITCH-FLAP COUPLING COEFFICIENT (RADIAN)	INPU0028
C		INPU0029
C	WL= WING SEMISPAN	INPU0030
C	WCHD= WING CHORD	INPU0031
C	WCL= WING LIFT CURVE SLOPE	INPU0032
C	WCD= WING DRAG COEFFICIENT	INPU0033
C	WCMO= WING PITCHING MOMENT COEFFICIENT	INPU0034
C	WCMA= WING PITCHING MOMENT CURVE SLOPE	INPU0035
C	EDIS= DISTANCE BETWEEN AERODYNAMIC CENTER AND ELASTIC AXIS	INPU0036

C	(NONDIMENSIONALIZED BY WING CHORD, POSITIVE AERODYNAMIC	INPU0037
C	CENTER AHEAD)	INPU0038
C	WTHET= WING TRIM ANGLE OF ATTACK (RADIAN)	INPU0039
C		INPU0040
C	CGUST= EXCITING FORCE COMPONENTS	INPU0041
C		INPU0042
C	BRAM= (BLADE NATURAL FREQUENCY)**2 (RADIAN/SEC)**2	INPU0043
C	WRAM= (WING NATURAL FREQUENCY)**2 (RADIAN/SEC)**2	INPU0044
C		INPU0045
C	NW= WING ELEMENT NUMBER	INPU0046
C	EMSW= WING ELEMENT SIZE NORMALIZED BY THE SEMISPAN	INPU0047
C	G= VERTICAL BENDING MODE COMPONENT AT THE NODE OF THE WING	INPU0048
C	Z= CHORDWISE BENDING MODE COMPONENT AT THE NODE OF THE WING	INPU0049
C	DG= VERTICAL BENDING MODE SLOPE AT THE NODE OF THE WING	INPU0050
C	DZ= CHORDWISE BENDING MODE SLOPE AT THE NODE OF THE WING	INPU0051
C	WPHI= TORSION MODE COMPONENT AT THE NODE OF THE WING	INPU0052
C	DWPHI= TORSION MODE SLOPE AT THE NODE OF THE WING	INPU0053
C		INPU0054
C	N= BLADE ELEMENT NUMBER	INPU0055
C	EMS=BLADE ELEMENT SIZE NORMALIZED BY THE ROTOR RADIUS	INPU0056
C	AMASS= MASS DISTRIBUTION AT THE NODE OF THE BLADE	INPU0057
C	THTEN= ANGLE OF TWIST AT THE NODE OF THE BLADE	INPU0058
C	COL= COLLECTIVE PITCH ANGLE DETERMINED BY THE PERFORMANCE (RADIAN)	INPU0059
C	W=OUT-OF-PLANE MODE COMPONENT AT THE NODE OF THE WING	INPU0060
C	V= INPLANE MODE COMPONENT AT THE NODE OF THE BLADE	INPU0061
C	DW= OUT-OF- PLANE MODE SLOPE COMPONENT AT THE NODE OF THE BLADE	INPU0062
C	DV= INPLANE MODE SLOPE COMPONENT AT THE NODE OF THE BLADE	INPU0063
C		INPU0064
C	BRAM0= (COLLECTIVE MODE NATURAL FREQUENCY OF THE BLADE)**2	INPU0065
C	(RADIAN/SEC)**2	INPU0066
C	WCOL= OUT-OF-PLANE COMPONENT OF THE BLADE COLLECTIVE MODE AT THE NODE	INPU0067
C	VCOL= INPLANE COMPONENT OF THE BLADE COLLECTIVE MODE AT THE NODE	INPU0068
C	DWCOL= OUT-OF-PLANE SLOPE COMPONENT OF THE BLADE COLLECTIVE MODE	INPU0069
C	AT THE NODE	INPU0070
C	DVCOL=INPLANE SLOPE COMPONENT OF THE BLADE COLLECTIVE MODE AT THE NODE	INPU0071
C		INPU0072

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DIMENSION RMAX(4),BOMAX(4),WMAX(6),RIG(6)
DIMENSION CGUST(6) ,SRMO(4),SBM(4),SWG(6),DES(80)
COMMON /PARMT/ ITYPE ,IFLT
COMMON/AMATIC/TT(6,5),C(6,6) ,T(5,6)
COMMON /AREAL/OMEGA,R,VFL,CL,CD,PAMDA,SNOMEG
COMMON /AREAR/NORLD,ROH,CHOD,ATR,CK,HMAST ,ALOCK ,AND,HR
COMMON/AREAR/BLAM(4),WLAM(6),BRAM(4),WRAM(6),BLAMO(4),BRAMO(4)
COMMON/GIN/ V(4,21),W(4,21),DV(4,21),DW(4,21),THETA(21),
%FMS(20),AMASS (20),N,NDP
COMMON /GINO/ VCOL(4,21),WCOL(4,21),DVCOL(4,21),DWCOL(4,21)
COMMON/WING/ NW,NDPW,FMSW(20),G(6,21),DG(6,21),Z(6,21),DZ(6,21),
*WPHI(6,21),DWPHI(6,21)
COMMON/WICH/WL,WCOD,WCL,WCD,WCMO,WOMA,EDIS,WTHET,VV
COMMON /COMPL/ AKPC(4),AKPD(4)
COMMON/FRMAG/ FRB(4),FRBD(4),FRW(6) ,IFRMAG
COMMON/THET/THETN(21) ,MR,MW
IDFRUG=0
MR=2
MW=3
READ(5,5003)(DES(I),I=1,80)
PEAD(5,5001) ITYPE
READ(5,5001) IFLT
READ(5,2034)IDOF
IE(IDOF.EQ.9) GO TO 62
MR=4
MW=6
62 CONTINUE
READ(5,5001)IRES
PEAD(5,5001)IFRMAG
READ(5,5001)IETGEN
READ(5,5001)NORLD
READ(5,5000)ROH,OMEGA,PAMDA,VEL
READ(5,5000)R,ATR,CHOD,CL,CD,HMAST,DEL3
READ(5,5000)WL,WCOD,WCL,WCD,WCMO,WOMA,EDIS,WTHET
PEAD(5,5000)CGUST

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INPU0073
INPU0074
INPU0075
INPU0076
INPU0077
INPU0078
INPU0079
INPU0080
INPU0081
INPU0082
INPU0083
INPU0084
INPU0085
INPU0086
INPU0087
INPU0088
INPU0089
INPU0090
INPU0091
INPU0092
INPU0093
INPU0094
INPU0095
INPU0096
INPU0097
INPU0098
INPU0099
INPU0100
INPU0101
INPU0102
INPU0103
INPU0104
INPU0105
INPU0106
INPU0107
INPU0108

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READ(5,5000)PRAM
 READ(5,5000)WRAM
 READ(5,2034)NW
 NDPW=NW+1
 READ(5,5000)(EMSW(K),K=1,NW)
 DO 60 I=1,MW
 READ(5,1001)(G(I,J),J=1,NDPW)
 READ(5,1001)(Z(I,J),J=1,NDPW)
 READ(5,1001)(DG(I,J),J=1,NDPW)
 READ(5,1001)(DZ(I,J),J=1,NDPW)
 READ(5,1001)(WPHI(I,J),J=1,NDPW)
 READ(5,1001)(DWPHT(I,J),J=1,NDPW)
 CONTINUE
 60 READ(5,2034)N
 NDP=N+1
 READ(5,5000)(EMS(K),K=1,N)
 READ(5,5000)(AMASS(J),J=1,NDP)
 READ(5,5000)(THETN(J),J=1,NDP)
 READ(5,5000)COL
 DO 50 I=1,MR
 READ(5,1001)(W(I,J),J=1,NDP)
 READ(5,1001)(V(I,J),J=1,NDP)
 READ(5,1001)(DW(I,J),J=1,NDP)
 READ(5,1001)(DV(I,J),J=1,NDP)
 AKPC(I)=DW(I,1)*TAN(DEL3)*(-1.0)
 CONTINUE
 50 IF(IJTYPE.EQ.3) GO TO 100
 READ(5,5000)PRAMO
 DO 52 I=1,MR
 READ(5,1001)(WCOL(I,J),J=1,NDP)
 READ(5,1001)(VCOL(I,J),J=1,NDP)
 READ(5,1001)(DWCOL(I,J),J=1,NDP)
 READ(5,1001)(DVCOL(I,J),J=1,NDP)
 AKPD(I)=DWCOL(I,1)*TAN(DEL3)*(-1.0)
 CONTINUE
 52 DO 200 I=1,4

INPU0109
 INPU0110
 INPU0111
 INPU0112
 INPU0113
 INPU0114
 INPU0115
 INPU0116
 INPU0117
 INPU0118
 INPU0119
 INPU0120
 INPU0121
 INPU0122
 INPU0123
 INPU0124
 INPU0125
 INPU0126
 INPU0127
 INPU0128
 INPU0129
 INPU0130
 INPU0131
 INPU0132
 INPU0133
 INPU0134
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 INPU0136
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 INPU0138
 INPU0139
 INPU0140
 INPU0141
 INPU0142
 INPU0143
 INPU0144

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BLAMD(I)=BRAMD(I)/OMEGA**2
SRMD(I)=SQRT(BLAMQ(I))
200 CONTINUE
100 CONTINUE
IF(IDDF.EQ.18) GO TO 101
DO 305 I=4,6
DO 305 J=1,NDPW
G(I,J)=0.0
DG(I,J)=0.0
Z(I,J)=0.0
DZ(I,J)=0.0
WPHI(I,J)=0.0
DWPHI(I,J)=0.0
305 CONTINUE
DO 307 I=3,4
DO 306 J=1,NDP
W(I,J)=0.0
DW(I,J)=0.0
V(I,J)=0.0
306 DV(I,J)=0.0
307 AKPC(I)=0.0
IF(ITYPE.EQ.0) GO TO 101
DO 308 I=3,4
DO 309 J=1,NDP
WCOL(I,J)=0.0
DWCOL(I,J)=0.0
VCOL(I,J)=0.0
309 DVCOL(I,J)=0.0
308 AKPO(I)=0.0
101 CONTINUE
DO 22 I=1,NDP
THETA(I)=THETN(I)+COL
22 CONTINUE
DO 6 I=1,4
BLAM(I)=BRAM(I)/OMEGA**2
6 SBM(I)=SQRT(BLAM(I))

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INPU0145
INPU0146
INPU0147
INPU0148
INPU0149
INPU0150
INPU0151
INPU0152
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INPU0172
INPU0173
INPU0174
INPU0175
INPU0176
INPU0177
INPU0178
INPU0179
INPU0180

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DO 5 I=1,6
WLAM(I)=WRAM(I)/OMEGA**2
5 SWG(I)=SQRT(WLAM(I))
DO 30 I=1,6
TT(I,1)=G(I,NDPW)
TT(I,2)=Z(I,NDPW)
TT(I,3)=DZ(I,NDPW)
TT(I,4)=WPHT(I,NDPW)
TT(I,5)=-DG(I,NDPW)
30 CONTINUE
IF(IFLT.EQ.0) GO TO 23
DO 24 I=1,6
24 TT(I,5)=0.0
23 CONTINUE
DO 40 I=1,6
DO 40 J=1,6
40 C(I,J)=DZ(I,NDPW)*WPHT(J,NDPW)-DZ(J,NDPW)*WPHT(I,NDPW)
ALOCK=ROH*CL*CHOD*R**4/AIB
ANO=FLOAT(NOBLD)
HR=HMAST/R
SNOMEG=SIGN(1.0,OMEGA)
2034 FORMAT(I2)
5003 FORMAT(80A1)
5001 FORMAT(I1)
5000 FORMAT(8E10.0)
1001 FORMAT(6F13.5)
C ***** PRINT OUT OF INPUT DATA *****
WRITE(6,5002) (DEF(I),I=1,80)
5002 FORMAT(///10X,100(1H*),//20X,80A1,///10X,100(1H*)//)
WRITE(6,5004) ITYPE,IFLT, IDOF,IRFS,IEIGEN,IFRMAG
5004 FORMAT(///10X,'ITYPE=',I2,3X,'IFLT=',I2,3X,'IDOF=',
& I2,3X,'IRFS=',I2,3X,'IEIGEN=',I2,3X,'IFRMAG=',I2)
WRITE(6,1)NOBLD,ROH,CHOC,AIB,HMAST,ALOCK
1 FORMAT(/// T4,'NO OF BLADES',T25,'ROH',T41,'CHORD',T59,'IB'
$,T74,'HMAST',T94,'LOCK NO',
</// T7,I2,T18,5(1P15.7,2X))

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INPU0181
INPU0182
INPU0183
INPU0184
INPU0185
INPU0186
INPU0187
INPU0188
INPU0189
INPU0190
INPU0191
INPU0192
INPU0193
INPU0194
INPU0195
INPU0196
INPU0197
INPU0198
INPU0199
INPU0200
INPU0201
INPU0202
INPU0203
INPU0204
INPU0205
INPU0206
INPU0207
INPU0208
INPU0209
INPU0210
INPU0211
INPU0212
INPU0213
INPU0214
INPU0215
INPU0216

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	WRITE(6,2)OMEGA,P,VFL,CL,CD,RAMDA	INPU0217
2	FORMAT(/// T6,'OMEGA',T25,'P',T41,'VFL',T59,'CL',T74,'CD' #,T94,'RAMDA' //1X,6(1PE15.7,2X))	INPU0218
	WRITE(6,61) COL ,DFL3	INPU0219
61	FORMAT(///T6,'COLLECTIVE PITCH',T25,'DFL3' //1X,2(1PE15.7,2X))	INPU0220
	WRITE(6,3)WL,WCD,WCL,WCD,WCMD,WOMA	INPU0221
3	FORMAT(/// T6,'WING L',T25,'WING CHOD',T41,'WING CL',T59,'WING CD' %,T74,'WING CMD',T94,'WING CMA' *///1X,6(1PE15.7,2X))	INPU0222
	WRITE(6,4)EDIS,WTHET	INPU0223
4	FORMAT(/// T6,'DISTANCE AC FA',T25,'WING ALPHA' @///1X,2(1PE15.7,2X))	INPU0224
	WRITE(6,250)	INPU0225
250	FORMAT(///1X,35(1H-)/1X,'EIGENVALUES (NATURAL FREQUENCIES)' E //1X,35(1H-)//2X,'--(RAD/SEC)**2--')	INPU0226
	IF(ITYPE.EQ.0) GO TO 254	INPU0227
	WRITE(6,251)(BRAMO(I),I=1,MR)	INPU0228
251	FORMAT(/1X,' **BLADE COLLECTIVE**'/4X,4(F12.3,3X))	INPU0229
	WRITE(6,252)	INPU0230
252	FORMAT(/1X,' **BLADE CYCLIC**')	INPU0231
	GO TO 255	INPU0232
254	WRITE(6,253)	INPU0233
253	FORMAT(/1X,' **BLADE**')	INPU0234
255	WRITE(6,256)(BRAM(I),I=1,MR)	INPU0235
256	FORMAT(4X,4(F12.3,3X))	INPU0236
	WRITE(6,257)(WRAM(I),I=1,MW)	INPU0237
257	FORMAT(/1X,' **WING**'/4X,6(F12.3,3X))	INPU0238
	WRITE(6,408)	INPU0239
408	FORMAT(/2X,'-- RAD/SEC/OMEGA --')	INPU0240
	IF(ITYPE.EQ.0) GO TO 354	INPU0241
	WRITE(6,351)(SBMO(I),I=1,MR)	INPU0242
351	FORMAT(/1X,' **BLADE COLLECTIVE/OMEGA**'/4X,4(F12.3,3X))	INPU0243
	WRITE(6,352)	INPU0244
352	FORMAT(/1X,' **BLADE CYCLIC/OMEGA**')	INPU0245
	GO TO 355	INPU0246
354	WRITE(6,353)	INPU0247
		INPU0248
		INPU0249
		INPU0250
		INPU0251
		INPU0252

353	FORMAT(/1X,' **BLADE/OMEGA**')	INPU0253
355	WRITE(6,356)(SBM(I),I=1,MB)	INPU0254
356	FORMAT(4X,4(F12.3,3X))	INPU0255
	WRITE(6,357)(SWG(I),I=1,MW)	INPU0256
357	FORMAT(/1X,' **WING/OMEGA**'/4X,6(F12.3,3X))	INPU0257
	WRITE(6,409)	INPU0258
400	FORMAT(///1X,'EXCITING FORCE COMPONENTS')	INPU0259
	WRITE(6,358)CGUST	INPU0260
358	FORMAT(//T6,'U GUST',T25,'V GUST', T41,'W GUST', T59,	INPU0261
	'THETA 0',T74,'THETA 10', T94,'THETA 15',/ /1X,	INPU0262
	* 6(1PE15.7,2X))	INPU0263
	DO 430 I=1,MR	INPU0264
	DO 431 J=1,NDP	INPU0265
	RIG(I)=0.0	INPU0266
	PA=ABS(W(I,J))	INPU0267
	IF(PA -RIG(I)) 460,460,461	INPU0268
461	RIG(I)=PA	INPU0269
460	PA=ABS(V(I,J))	INPU0270
	IF(PA -RIG(I)) 431,431,462	INPU0271
462	RIG(I)=PA	INPU0272
431	CONTINUE	INPU0273
430	BMAX(I)=RIG(I)	INPU0274
	DO 435 I=1,MW	INPU0275
	DO 436 J=1,NDPW	INPU0276
	RIG(I)=0.0	INPU0277
	PA=ABS(G(I,J))	INPU0278
	IF(PA -RIG(I)) 465,465,466	INPU0279
466	RIG(I)=PA	INPU0280
465	PA=(Z(I,J))	INPU0281
	IF(PA -RIG(I)) 436,436,467	INPU0282
467	RIG(I)=PA	INPU0283
436	CONTINUE	INPU0284
435	WMAX(I)=RIG(I)	INPU0285
	IF(I TYPE.EQ.0) GO TO 480	INPU0286
	DO 440 I=1,MR	INPU0287
	DO 441 J=1,NDP	INPU0288

	RIG(I)=0.0	INPU0289
	PA=ABS(WCOL(I,J))	INPU0290
	IF(PA -RIG(I)) 470,470,471	INPU0291
471	BIG(I)=PA	INPU0292
470	PA=ABS(VCOL(I,J))	INPU0293
	IF(PA -RIG(I)) 441,441,472	INPU0294
472	BIG(I)=PA	INPU0295
441	CONTINUE	INPU0296
440	BOMAX(I)=RIG(I)	INPU0297
	GO TO 487	INPU0298
480	DO 481 I=1,MB	INPU0299
481	BOMAX(I)=BMAX(I)	INPU0300
487	CONTINUE	INPU0301
	DO 475 I=1,MB	INPU0302
	FRB(I)=BMAX(I) /R	INPU0303
	FRBO(I)=BOMAX(I) /R	INPU0304
475	CONTINUE	INPU0305
	DO 476 I=1,MW	INPU0306
	FRW(I)=WMAX(I) /WL	INPU0307
476	CONTINUE	INPU0308
	FRW(3)=ABS(WPHI(3,NDPW))	INPU0309
	IDERUG=0	INPU0310
	IF(IDERUG.EQ.0) GO TO 477	INPU0311
	WRITE(6,5005)(BMAX(I),I=1,MB),(BOMAX(I),I=1,MB),(WMAX(I),I=1,MW)	INPU0312
5005	FORMAT(///(10X,E15.7))	INPU0313
477	CONTINUE	INPU0314
	RETURN	INPU0315
	END	INPU0316

	SUBROUTINE INTPL	INTP0001
C		INTP0002
C	INTERPOLATION FOR THE NUMERICAL INTEGRATION	INTP0003
C		INTP0004
C	INTERPOLATION FUNCTION-----HERMIT INTERPOLATION(2 POINTS)	INTP0005
C	INTERPOLATION FUNCTION----LAGRANGIAN INTERPOLATION FOR THE ANGLE OF TWIST	INTP0006
	COMMON/THE/THETN(21) ,MB,MW	INTP0007
	COMMON /PARMT/ ITYPE ,IFLT	INTP0008
	COMMON /AREA1/OMEGA,R,VEL,CL,CD,RAMDA,SNOMFG	INTP0009
	COMMON/WICH/WL,WCDP,WCL,WCD,WCMO,WOMA,EDIS,WTHET,VV	INTP0010
	DIMENSION WX(21)	INTP0011
	COMMON/WING/ NW,NDPW,EMSW(20),G(6,21),DG(6,21),Z(6,21),DZ(6,21),	INTP0012
	*WPHI(6,21),DWPHI(6,21)	INTP0013
	DIMENSION GI(6,20),ZI(6,20),WPHI1(6,20)	INTP0014
	COMMON/WIMOD/STR(20,3,6),TSTP(20,6,3)	INTP0015
	DIMENSION XX(21)	INTP0016
	COMMON/GIN/ V(4,21),W(4,21),DV(4,21),DW(4,21),THETA(21),	INTP0017
	%EMS(20),AMASS (20),N,NDP	INTP0018
	COMMON /GINO/ VCOL(4,21),WCOL(4,21),DVCOL(4,21),DWCOL(4,21)	INTP0019
	COMMON /AREA3/VI(4,20),WI(4,20),THETA1(20) ,AMASS1(20)	INTP0020
	* ,VICOL(4,20),WICOL(4,20)	INTP0021
	COMMON /AREA2/NPT,XXX(20),A(20)	INTP0022
	IDEBUG=0	INTP0023
	WRITE(6,50)	INTP0024
50	FORMAT(///1X,'***** BLADE MODE SHAPES *****')	INTP0025
	XX(1)=0.0	INTP0026
	DO 8 I=1,N	INTP0027
	XX(I+1)=XX(I)+EMS(I)	INTP0028
80	CONTINUE	INTP0029
	IF(IATYPE.EQ.) GOTO 100	INTP0030
	WRITE(6,51)	INTP0031
51	FORMAT(/1X,'--- COLLECTIVE MODES ---')	INTP0032
	DO 36 I=1,MB	INTP0033
	WRITE(6,4900)I	INTP0034
	WRITE(6,4999)	INTP0035
	WRITE(6,3)(J,XX(J),VCOL(I,J),DVCOL(I,J),WCOL(I,J),DWCOL(I,J),	INTP0036

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*   J=1,NDP)
36  CONTINUE
    WRITE(6,52)
52  FORMAT(//IX,'---- CYCLIC MODES ----')
100  CONTINUE
    DO 35 I=1,MR
    WRITE(6,4500)I
4500 FORMAT(/// IX,'I=',I1)
    WRITE(6,4999)
4999 FORMAT(      T5,'J',T13,'XX(J)',T33,'V(I,J)',T53,'DV(I,J)',T73,'W(I
%,J)',T93,'DW(I,J)')
    WRITE(6,3)(J,XX(J),V(I,J),DV(I,J),W(I,J),DW(I,J),J=1,NDP)
3   FORMAT(IX,      I4,5(5X,E15.7)))
35  CONTINUE
    WRITE(6,5999)
5999 FORMAT(/// T5,'J',T13,'XX(J)',T33,'THETN(J)',T53,'AMASS(J)')
    WRITE(6,4)(J,XX(J),THETN(J),AMASS(J),J=1,NDP)
4   FORMAT(IX,      I4,3(5X,E15.7)))
    DO 70 II=1,NPT
    DO 60 I=1,NDP
    IF(XX(I).GE.XXX(II)) GO TO 110
60  CONTINUE
110  EA=XX(I)-XX(I-1)
    EB=XX(I)+XX(I-1)
    XKSI=2.0/EA*XXX(II)-EB/EA
    F1=(XKSI+2.0)*(XKSI-1.0)**2/4.0
    F2=(2.0-XKSI)*(XKSI+1.0)**2/4.0
    G1=(XKSI+1.0)*(XKSI-1.0)**2/4.0
    G2=(XKSI-1.0)*(XKSI+1.0)**2/4.0
    F1L=(1.0-XKSI)/2.0
    F2L=(1.0+XKSI)/2.0
    DO 90 JJ=1,4
    VI(JJ,II)=V(JJ,I-1)*F1+V(JJ,I)*F2+(DV(JJ,I-1)*G1+DV(JJ,I)*G2)
    a*EA/2.0*R
    WI(JJ,II)=W(JJ,I-1)*F1+W(JJ,I)*F2+(DW(JJ,I-1)*G1+DW(JJ,I)*G2)
    a*EA/2.0*R

```

```

INTP0037
INTP0038
INTP0039
INTP0040
INTP0041
INTP0042
INTP0043
INTP0044
INTP0045
INTP0046
INTP0047
INTP0048
INTP0049
INTP0050
INTP0051
INTP0052
INTP0053
INTP0054
INTP0055
INTP0056
INTP0057
INTP0058
INTP0059
INTP0060
INTP0061
INTP0062
INTP0063
INTP0064
INTP0065
INTP0066
INTP0067
INTP0068
INTP0069
INTP0070
INTP0071
INTP0072

```

	IF(IATYPE.EQ.0)GO TO 90	INTP0073
	VICOL(JJ,II)=VCOL(JJ,I-1)*F1+VCOL(JJ,I)*F2+(DVCOL(JJ,I-1)*G1	INTP0074
	* +DVCOL(JJ,I)*G2)*EA/2.0*R	INTP0075
	WICOL(JJ,II)=WCOL(JJ,I-1)*F1+WCOL(JJ,I)*F2+(DWCOL(JJ,I-1)*G1	INTP0076
	* +DWCOL(JJ,I)*G2)*EA/2.0*R	INTP0077
90	CONTINUE	INTP0078
	AMASSI(II)=AMASS(I-1)*F1L+AMASS(I)*F2L	INTP0079
	THETAI(II)=THETA(I-1)*F1L+THETA(I)*F2L	INTP0080
70	CONTINUE	INTP0081
	IF(IDEBUG.EQ.0) GO TO 400	INTP0082
	WRITE(6,5048)	INTP0083
5048	FORMAT(/// T5,'J',T13,'XXX(J)',T33,'VI(1,J)',T53,'WI(1,J)',T73,	INTP0084
	@'VI(2,J)',T93,'WI(2,J)')	INTP0085
	WRITE(6,3)(JJ,XXX(JJ),VI(1,JJ),WI(1,JJ),VI(2,JJ),WI(2,JJ),JJ=1,	INTP0086
	%NPT)	INTP0087
	WRITE(6,5047)	INTP0088
5047	FORMAT(/// T5,'J',T13,'XXX(J)',T33,'VI(3,J)',T53,'WI(3,J)',T73,	INTP0089
	@'VI(4,J)',T93,'WI(4,J)')	INTP0090
	WRITE(6,3)(JJ,XXX(JJ),VI(3,JJ),WI(3,JJ),VI(4,JJ),WI(4,JJ),JJ=1,	INTP0091
	%NPT)	INTP0092
	WRITE(6,5046)	INTP0093
5046	FORMAT(/// T5,'J',T13,'XXX(J)',T33,'AMASSI(J)',T53,'THETAI(J)')	INTP0094
	WRITE(6,4)(JJ,XXX(JJ),AMASSI(JJ),THETAI(JJ),JJ=1,NPT)	INTP0095
400	CONTINUE	INTP0096
	WRITE(6,53)	INTP0097
53	FORMAT(///1X,'***** WING MODE SHAPES *****')	INTP0098
	WX(1)=0.0	INTP0099
	DO 81 I=1,NW	INTP0100
	WX(I+1)=WX(I)+EMSW(I)	INTP0101
81	CONTINUE	INTP0102
	DO 38 II=1,MW	INTP0103
	WRITE(6,7000)II	INTP0104
7000	FORMAT(/// 1X,'II=',II)	INTP0105
	WRITE(6,7001)	INTP0106
7001	FORMAT(T5,'J',T9,'WX(J)',T25,'G(II,J)',T41,'DG(II,J)',T57,	INTP0107
	*'Z(II,J)',T73,'DZ(II,J)',T89,'WPHI(II,J)',T105,'DWPHI(II,J)')	INTP0108

```

WRITE(6,5)(J,WX(J),G(II,J),DG(II,J),Z(II,J),DZ(II,J),WPHI(II,J),
%DWPHI(II,J),J=1,NDPW)
5   FORMAT(1X,      14,7(1X,E15.7))
38   CONTINUE
    DO 10 II=1,NPT
    DO 20 I=1,NDPW
    IF(WX(I).GE.XXX(II)) GO TO 220
20   CONTINUE
220   WEA=WX(I)-WX(I-1)
    WEB=WX(I)+WX(I-1)
    XKSI=2.0/WEA*XXX(II)-WEB/WEA
    F1=(XKSI+2.0)*(XKSI-1.0)**2/4.0
    F2=(2.0-XKSI)*(XKSI+1.0)**2/4.0
    G1=(XKSI+1.0)*(XKSI-1.0)**2/4.0
    G2=(XKSI-1.0)*(XKSI+1.0)**2/4.0
    DO 37 IJ=1,6
    GI(IJ,II)=G(IJ,I-1)*F1+G(IJ,I)*F2+(DG(IJ,I-1)*G1+DG(IJ,I)*G2)*
*WEA/2.0 *WL
    ZI(IJ,II)=Z(IJ,I-1)*F1+Z(IJ,I)*F2+(DZ(IJ,I-1)*G1+DZ(IJ,I)*G2)*
*WEA/2.0 *WL
    WPHI(II,IJ)=WPHI(II,I-1)*F1+WPHI(II,I)*F2+(DWPHI(II,I-1)*G1+
%DWPHI(II,I)*G2)*WEA/2.0*WL
    STR(II,1,IJ)=GI(IJ,II)
    STR(II,2,IJ)=ZI(IJ,II)
    STR(II,3,IJ)=WPHI(II,IJ)
    TSTR(II,IJ,1)=GI(IJ,II)
    TSTR(II,IJ,2)=ZI(IJ,II)
    TSTR(II,IJ,3)=WPHI(II,IJ)
37   CONTINUE
10   CONTINUE
    IF(IDDEBUG.EQ.0) GO TO 401
    WRITE(6,7:03)
7003 FORMAT(/// T5,'J',T9,'XXX(J)',T25,'GI(1,J)',T41,'HI(1,J)',T57,
%'WPHI(1,J)',T73,'GI(2,J)',T89,'H(2,J)',T105,'WPHI(2,J)')
    WRITE(6,5)(J,XXX(J),GI(1,J),ZI(1,J),WPHI(1,J),GI(2,J),ZI(2,J),
%DWPHI(2,J),J=1,NPT)

```

```

INTP0109
INTP0110
INTP0111
INTP0112
INTP0113
INTP0114
INTP0115
INTP0116
INTP0117
INTP0118
INTP0119
INTP0120
INTP0121
INTP0122
INTP0123
INTP0124
INTP0125
INTP0126
INTP0127
INTP0128
INTP0129
INTP0130
INTP0131
INTP0132
INTP0133
INTP0134
INTP0135
INTP0136
INTP0137
INTP0138
INTP0139
INTP0140
INTP0141
INTP0142
INTP0143
INTP0144

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```

WRITE(6,7004)
7004  FORMAT(/// T5,'J',T9,'XXX(J)',T25,'GI(3,J)',T41,'HI(3,J)',T57,
      %'WPHII(3,J)',T73,'GI(4,J)',T89,'H(4,J)',T105,'WPHII(4,J)')
      WRITE(6,5)(J,XXX(J),GI(3,J),ZI(3,J),WPHII(3,J),GI(4,J),ZI(4,J),
      @WPHII(4,J),J=1,NPT)
      WRITE(6,7005)
7005  FORMAT(/// T5,'J',T9,'XXX(J)',T25,'GI(5,J)',T41,'HI(5,J)',T57,
      %'WPHII(5,J)',T73,'GI(6,J)',T89,'H(6,J)',T105,'WPHII(6,J)')
      WRITE(6,5)(J,XXX(J),GI(5,J),ZI(5,J),WPHII(5,J),GI(6,J),ZI(6,J),
      @WPHII(6,J),J=1,NPT)
401  CONTINUE
      RETURN
      END

```

```

INTP0145
INTP0146
INTP0147
INTP0148
INTP0149
INTP0150
INTP0151
INTP0152
INTP0153
INTP0154
INTP0155
INTP0156
INTP0157

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SUBROUTINE AERODT

TO DEFINE THE AERODYNAMIC COEFFICIENTS AT THE POINTS OF GAUSSIAN
QUADRATURE

```

COMMON /PARMT/ ITYPE ,IFLT
COMMON /AREA1/OMEGA,R,VEL,CL,CD,RAMDA,SNOMEG
COMMON /AREA6/NOBLD,RCH,CHOD,AIB,CK,FMAST ,ALOCK ,ANO,HR
COMMON /AREA2/NPT,XXX(20),A(20)
COMMON /AREA3/VI(4,20),WI(4,20),THETA1(20) ,AMASSI(20)
      ,VICOL(4,20),WICCL(4,20)
COMMON/ AREA4/F(4,4,20),HI(4,20),HII(4,20),HRZ(4,20),HNR(4,20),
%WD(4,20),VO(4,20),W1(4,20),V1(4,20)
@      ,OH(4,4,20),OWD(4,20),OV1(4,20),OHII(4,20),CHII(4,20)
@      ,CHV(4,20),OHIV(4,20)
COMMON/AKKH/FTOP1(20),FT1P0(20),FT1P2(20),FT2P1(20), FZ2P0(20),
/FZ0P0(20),FZ1P1(20),FZ2P2(20)
@      ,FT3P0(20),FT3P1(20),FZ3P0(20),FZ3P1(20)
COMMON/ADFE/HIII(4,20),FIV(4,20),HV(4,20),HVI(4,20),HVII(4,20)
COMMON/WIND/STR(20,3,6),TSTR(20,6,3)
COMMON/WICH/WL,WCD,WCL,WCD,WCMO,WOMA,EDIS,WTHET,VV
COMMON/WINGAR/TSCS(20,6,6),TSAS(20,6,6),TSAG(20,6,3)
DIMENSION DAWA(3,3),AWA(3,3),AWG(3,3)
DIMENSION TSCF(20,6,3),TSA(20,6,3)
DO 1 I=1,3
DO 1 J=1,3
DAWA(I,J)=0.0
AWA(I,J)=0.0
1 AWG(I,J)=0.0
DO 2 I=1,20
DO 2 J=1,6
DO 2 K=1,3
TSDA(I,J,K)=0.0
2 TSA(I,J,K)=0.0
CK=-0.5*ROH*CL*CHOD*R**4
CA=CD/CL

```

AER0001
AER0002
AER0003
AER0004
AER0005
AER0006
AER0007
AER0008
AER0009
AER0010
AER0011
AER0012
AER0013
AER0014
AER0015
AER0016
AER0017
AER0018
AER0019
AER0020
AER0021
AER0022
AER0023
AER0024
AER0025
AER0026
AER0027
AER0028
AER0029
AER0030
AER0031
AER0032
AER0033
AER0034
AER0035
AER0036

```

CA1=1.0+CA
CA2=1.0-CA
ARAMCA=RAMDA
RAMCA=ABS(RAMEA)
DO 11 JJ=1,NPT
XSQ=SQRT(RAMCA**2+XXX(JJ)**2)
TAU0=1.0/XSQ
TAU1=XXX(JJ)/XSQ
TAU2=XXX(JJ)**2/XSQ
TAU3=XXX(JJ)**3/XSQ
ALPHA=THETA(JJ)-ATAN(RAMCA/XXX(JJ))+ATAN(RAMDA*4.0/3.0)
FTH0=RAMDA**3-ALPHA*TAU0+RAMCA**2*CA*TAU1+RAMDA*ALPHA*TAU2
/+CA*TAU3
FTH1=RAMDA**2*CA1*TAU0+RAMCA*ALPHA*TAU1+2.0*CA*TAU2
FTH2=2.0*RAMDA**2*ALPHA*TAU0-RAMDA*CA2*TAU1+ALPHA*TAU2
FTH3=RAMDA**3*TAU0+RAMCA*TAU2
FTHC=-FTH0*SNOMEG
FTH1=-FTH1
FTH2=-FTH2*SNOMEG
FTH3=-FTH3*SNOMEG
FZ0=-RAMDA**3*CA*TAU0+RAMDA**2*ALPHA*TAU1--RAMDA*CA*TAU2
/+ALPHA*TAU3
FZ1=RAMDA**2*ALPHA*TAU0+RAMCA*CA2*TAU1+2.0*ALPHA*TAU2
FZ2=-2.0*RAMDA**2*CA*TAU0+RAMCA*ALPHA*TAU1-CA1*TAU2
FZ3=RAMDA**2*TAU1+TAU3
FZ1=FZ1*SNOMEG
DO 200 J=1,4
DO 100 I=1,4
H(J,I,JJ)=FTH1*VI(J,JJ)*VI(I,JJ)+FZ1*WI(J,JJ)*VI(I,JJ)+FTH2*
*VI(J,JJ)*WI(I,JJ)+FZ2*WI(J,JJ)*WI(I,JJ)
IF(I*TYPE.EQ.0) GO TO 100
EH(J,I,JJ)=FTH1*VICOL(J,JJ)*VICOL(I,JJ)+FZ1*WICOL(J,JJ)*
*VICOL(I,JJ)+FTH2*VICOL(J,JJ)*WICOL(I,JJ)+FZ2*WICOL
*(J,JJ)*WICOL(I,JJ)
100 CONTINUE
HI(J,JJ)=FTH1*VI(J,JJ)+FZ1*WI(J,JJ)

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AER00037
AER00038
AER00039
AER00040
AER00041
AER00042
AER00043
AER00044
AER00045
AER00046
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AER00048
AER00049
AER00050
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AER00069
AER00070
AER00071
AER00072

```

HII(J, JJ) = (FTH2*VI(J, JJ) + FZ2*WI(J, JJ))*XXX(JJ)
 HRZ(J, JJ) = FTH2*VI(J, JJ) + FZ2*WI(J, JJ)
 HNR(J, JJ) = (FTH1*VI(J, JJ) + FZ1*WI(J, JJ))*XXX(JJ)
 WO(J, JJ) = AMASSI(JJ)*WI(J, JJ)
 VO(J, JJ) = AMASSI(JJ)*VI(J, JJ)
 W1(J, JJ) = AMASSI(JJ)*WI(J, JJ)*XXX(JJ)
 V1(J, JJ) = AMASSI(JJ)*VI(J, JJ)*XXX(JJ)
 HIII(J, JJ) = FTH1*VI(J, JJ) + FTH2*WI(J, JJ)
 HIV(J, JJ) = HIII(J, JJ)*XXX(JJ)
 HV(J, JJ) = FZ1*VI(J, JJ) + FZ2*WI(J, JJ)
 HVI(J, JJ) = HV(J, JJ)*XXX(JJ)
 HVII(J, JJ) = FZ0*VI(J, JJ) - FTH0*WI(J, JJ)
 CHIII(J, JJ) = FZ3*WI(J, JJ) + FTH3*VI(J, JJ)
 IF(ITYPE.EQ.0) GO TO 200
 QWC(J, JJ) = AMASSI(JJ)*VICOL(J, JJ)
 QVI(J, JJ) = AMASSI(JJ)*VICOL(J, JJ)*XXX(JJ)
 HRZ(J, JJ) = FTH2*VICOL(J, JJ) + FZ2*WICOL(J, JJ)
 HNR(J, JJ) = (FTH1*VICOL(J, JJ) + FZ1*WICOL(J, JJ))*XXX(JJ)
 QHTII(J, JJ) = FZ3*WICOL(J, JJ) + FTH3*VICOL(J, JJ)
 QHV(J, JJ) = FZ1*VICOL(J, JJ) + FZ2*WICOL(J, JJ)
 QHIV(J, JJ) = (FTH1*VICOL(J, JJ) + FTH2*WICOL(J, JJ))*XXX(JJ)

200 CONTINUE

C AERC FOR WING DUE TO BLADES

FTDP1(JJ) = FTH0*XXX(JJ)
 FT1P0(JJ) = FTH1
 FT1P2(JJ) = FTH1*XXX(JJ)*2
 FT2P1(JJ) = FTH2*XXX(JJ)
 FZ3P0(JJ) = FZ3
 FZ1P1(JJ) = FZ1*XXX(JJ)
 FZ2P0(JJ) = FZ2
 FZ2P2(JJ) = FZ2*XXX(JJ)*2
 FT3P0(JJ) = FTH3
 FT3P1(JJ) = FTH3*XXX(JJ)
 FZ3P1(JJ) = FZ3
 FZ3P1(JJ) = FZ3*XXX(JJ)

11 CONTINUE

AER00073
 AER00074
 AER00075
 AER00076
 AER00077
 AER00078
 AER00079
 AFR00080
 AER00081
 AER00082
 AER00083
 AER00084
 AER00085
 AER00086
 AER00087
 AFR00088
 AER00089
 AFR00090
 AER00091
 AER00092
 AER00093
 AER00094
 AER00095
 AER00096
 AER00097
 AER00098
 AER00099
 AFR00100
 AER00101
 AER00102
 AFR00103
 AER00104
 AFR00105
 AER00106
 AER00107
 AER00108

```

C   AERO FOR WING DUE TO ITSELF
    RAMDA=ARAMDA
    RC=ROH*WCD
    DAWA(1,1)=-0.5*RC*VEL*(WCL+WCD)
    DAWA(1,2)=RC*WCL*WTHET*VEL
    DAWA(2,1)=-0.5*RC*WCL*WTHET*VEL
    DAWA(2,2)=-RC*WCD*VEL
    DAWA(3,1)=-0.5*RC*WCD*VEL*(WCL*EDIS+WMA)
    DAWA(3,2)=RC*WCD*(WCMO+WMA*WTHET+WCL*WTHET*EDIS)*VEL
    AWA(1,3)=0.5*RC*WCL*VEL**2
    AWA(3,3)=0.5*RC*WCD*VEL**2*(WMA+WCL*EDIS)
    AWG(1,1)=DAWA(1,1)*VEL
    AWG(1,3)=DAWA(1,2)*VEL
    AWG(2,1)=DAWA(2,1)*VEL
    AWG(2,3)=DAWA(2,2)*VEL
    AWG(3,1)=DAWA(3,1)*VEL
    AWG(3,3)=DAWA(3,2)*VEL
    DO 501 II=1,NPT
    DO 502 I=1,6
    DO 502 J=1,3
    DO 502 K=1,3
    TSDA(II,I,J)=TSTR(II,I,K)*DAWA(K,J)+TSDA(II,I,J)
    TSA(II,I,J)=TSTR(II,I,K)*AWA(K,J)+TSA(II,I,J)
    TSAG(II,I,J)=TSTR(II,I,K)*AWG(K,J)+TSAG(II,I,J)
502 CONTINUE
    DO 503 I=1,6
    DO 503 J=1,6
    DO 503 K=1,3
    TSDS(II,I,J)=TSDA(II,I,K)*STR(II,K,J)+TSDS(II,I,J)
    TSAS(II,I,J)=TSA(II,I,K)*STR(II,K,J)+TSAS(II,I,J)
503 CONTINUE
501 CONTINUE
    RETURN
    END
AERO0109
AERO0110
AERO0111
AERO0112
AERO0113
AERO0114
AERO0115
AERO0116
AERO0117
AERO0118
AERO0119
AERO0120
AERO0121
AERO0122
AERO0123
AERO0124
AERO0125
AERO0126
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AERO0131
AERO0132
AERO0133
AERO0134
AERO0135
AERO0136
AERO0137
AERO0138
AERO0139
AERO0140
AERO0141
AERO0142

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SUBROUTINE CRDINT

C
C
C

TO DEFINE THE ORDER OF NUMERICAL INTEGRATION

```

COMMON /PARMT/ ITYPE ,IFLT
COMMON /AREA1/OMEGA,R,VEL,CL,CD,RAMDA,SNOMEG
COMMON /AREA6/NOBLD,RDH,CHOD,AIB,CK,HMAST ,ALOCK ,AND,HR
COMMON/AREA5/AH(4,4),AHI(4),AHII(4),AHRZ(4),AHNR(4),AWC(4),AVO(4)
@,AWI(4),AVI(4),OAH(4,4),OAWO(4),OAVI(4),OAHIII(4),CAHIII(4)
@ ,OAHV(4),OAHIV(4)
COMMON/AERO/AFTOP1,AFT1P0,AFT1P2,AFT2P1,AFZOP0,AFZ1P1,AFZ2P0,
@AFZ2P2,AHIII(4),AHIV(4),AHV(4),AHVI(4),AHVII(4)
@ ,AFT3P0,AFT3P1,AFZ3P0,AFZ3P1
COMMON/WICH/WL,WCD0,WCL,WCD,WCM0,WCM1,EDIS,WTHET,VV
COMMON/ARWG/DARWA(6,6),ARWA(6,6),ARWG(6,3)
IDEBUG=0
NN=1
DO 100 JQ=1,4
DO 100 IQ=1,4
CALL INTEG(FSUM,NN,JQ,IQ)
AH(JQ,IQ)=CK*FSUM/R**2
100 CONTINUE
NK=NN
1000 NN=NN+1
DO 200 JQ=1,4
CALL INTEG(FSUM,NN,JQ,IQ)
FSUM=FSUM*CK/R
NM=NN-NK
GO TO (2,3,4,5),NM
2 AHI(JQ)=FSUM
GO TO 200
3 AHII(JQ)=FSUM
GO TO 200
4 AHRZ(JQ)=FSUM
GO TO 200
5 AHNR(JQ)=FSUM

```

```

ORDI0001
ORDI0002
ORDI0003
ORDI0004
ORDI0005
ORDI0006
ORDI0007
ORDI0008
ORDI0009
ORDI0010
ORDI0011
ORDI0012
ORDI0013
ORDI0014
ORDI0015
ORDI0016
ORDI0017
ORDI0018
ORDI0019
ORDI0020
ORDI0021
ORDI0022
ORDI0023
ORDI0024
ORDI0025
ORDI0026
ORDI0027
ORDI0028
ORDI0029
ORDI0030
ORDI0031
ORDI0032
ORDI0033
ORDI0034
ORDI0035
ORDI0036

```

200	CONTINUE	ORDI0037
	IF(NN.LT.5) GO TO 1000	ORDI0038
	NK=NN	ORDI0039
2000	NN=NN+1	ORDI0040
	DO 300 JQ=1,4	ORDI0041
	CALL INTEG(FSUM,NN,JQ,IQ)	ORDI0042
	FSUM=FSUM*R**2	ORDI0043
	NM=NN-NK	ORDI0044
	GO TO (6,7,8,9),NM	ORDI0045
6	AWO(JQ)=FSUM	ORDI0046
	GO TO 300	ORDI0047
7	AVO(JQ)=FSUM	ORDI0048
	GO TO 300	ORDI0049
8	AWI(JQ)=FSUM	ORDI0050
	GO TO 300	ORDI0051
9	AVI(JQ)=FSUM	ORDI0052
300	CONTINUE	ORDI0053
	IF(NN.LT.9) GO TO 2000	ORDI0054
	NK=NN	ORDI0055
3000	NN=NN+1	ORDI0056
	CALL INTEG(FSUM,NN,JQ,IQ)	ORDI0057
	FSUM=FSUM*CK*ANO	ORDI0058
	NM=NN-NK	ORDI0059
	GO TO (10,11,12,13,14,15,16,17),NM	ORDI0060
10	AFTOP1=FSUM	ORDI0061
	GO TO 400	ORDI0062
11	AFT1P1=FSUM	ORDI0063
	GO TO 400	ORDI0064
12	AFT1P2=FSUM	ORDI0065
	GO TO 400	ORDI0066
13	AFT2P1=FSUM	ORDI0067
	GO TO 400	ORDI0068
14	AFZOP0=FSUM	ORDI0069
	GO TO 400	ORDI0070
15	AFZ1P1=FSUM	ORDI0071
	GO TO 400	ORDI0072

```

16 AFZ2P0=FSUM
GO TO 400
17 AFZ2P2=FSUM
400 IF(NN.LT.17) GO TO 3000
NK=NN
4000 NN=NN+1
DO 500 JQ=1,4
CALL INTEG(FSUM,NN,JQ,IQ)
FSUM=FSUM/R*CK*AND
NM=NN-NK
GO TO ( 18,19,20,21,22),NM
18 AHIII(JQ)=FSUM
GO TO 500
19 AHIV(JQ)=FSUM
GO TO 500
20 AHV(JQ)=FSUM
GO TO 500
21 AHVI(JQ)=FSUM
GO TO 500
22 AHVII(JQ)=FSUM
500 CONTINUE
IF(NN.LT.22) GO TO 4000
NK=NN
5000 NN=NN+1
DO 600 JQ=1,6
DO 600 IQ=1,6
CALL INTEG(FSUM,NN,JQ,IQ)
NM=NN-NK
GO TO (23,24),NM
23 FSUM=FSUM*WL/ABS(OMEGA)
CARWA(JQ,IQ)=FSUM
GO TO 600
24 FSUM=FSUM*WL/OMEGA**2
ARWA(JQ,IQ)=FSUM
600 CONTINUE
IF(NN.LT.24) GO TO 5000

```

```

ORDI0073
ORDI0074
ORDI0075
ORDI0076
ORDI0077
ORDI0078
ORDI0079
ORDI0080
ORDI0081
ORDI0082
ORDI0083
ORDI0084
ORDI0085
ORDI0086
ORDI0087
ORDI0088
ORDI0089
ORDI0090
ORDI0091
ORDI0092
ORDI0093
ORDI0094
ORDI0095
ORDI0096
ORDI0097
ORDI0098
ORDI0099
ORDI0100
ORDI0101
ORDI0102
ORDI0103
ORDI0104
ORDI0105
ORDI0106
ORDI0107
ORDI0108

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```

NN=25
DO 700 JQ=1,6
DO 700 IQ=1,3
CALL INTEG(FSUM,NN,JQ,IQ)
FSUM=FSUM*WL/OMEGA**2
ARWG(JQ,IQ)=FSUM
700 CONTINUE
NN=28
DO 801 JQ=1,4
CALL INTEG(FSUM,NN,JQ,IQ)
FSUM=FSUM*CK/R
CAHIII(JQ)=FSUM
801 CONTINUE
NK=NN
2003 NN=NN+1
CALL INTEG(FSUM,NN,JQ,IQ)
FSUM=FSUM*CK*AND
NM=NN-NK
GOTO (27,28,29,30),NM
27 AFT3P0=FSUM
GO TO 2003
28 AFT3P1=FSUM
GO TO 2003
29 AFZ3P0=FSUM
GO TO 2003
30 AFZ3P1=FSUM
IF(IDEBUG.EQ.0) GO TO 450
WRITE(6,50)((AH(I,J),J=1,4),I=1,4)
50 FORMAT(////1X,2X,'AH',4(T10,4(E15.7,2X)/1X))
WRITE(6,51)AH1,AH2,AHRZ,AHNR,AHIII,AHIV,AHV,AHVI,AHVII,CAHIII
51 FORMAT(2X,'AH1',T10,4(E15.7,2X)
%      /2X,'AH2',      T10,4(E15.7,2X)
%      /2X,'AHRZ',     T10,4(E15.7,2X)
%      /2X,'AHNR',     T10,4(E15.7,2X)
*      /2X,'AHIII',    T10,4(E15.7,2X)
%      /2X,'AHIV',     T10,4(E15.7,2X)

```

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ORDI0109
ORDI0110
ORDI0111
ORDI0112
ORDI0113
ORDI0114
ORDI0115
ORDI0116
ORDI0117
ORDI0118
ORDI0119
ORDI0120
ORDI0121
ORDI0122
ORDI0123
ORDI0124
ORDI0125
ORDI0126
ORDI0127
ORDI0128
ORDI0129
ORDI0130
ORDI0131
ORDI0132
ORDI0133
ORDI0134
ORDI0135
ORDI0136
ORDI0137
ORDI0138
ORDI0139
ORDI0140
ORDI0141
ORDI0142
ORDI0143
ORDI0144

```


	@	/2X,'AHV',	T10,4(E15.7,2X)	ORDI0145
	*	/2X,'AHVI',	T10,4(E15.7,2X)	ORDI0146
	%	/2X,'AHVII',	T10,4(E15.7,2X)	ORDI0147
	@	/2X,'CAHIII',	T10,4(E15.7,2X)	ORDI0148
		WRITE(6,82)	AFT3P0,AFT3P1,AFZ3P0,AFZ3P1	ORDI0149
82		FORMAT(2X,'AFT3P0'	,T10,E15.7	ORDI0150
	*	/2X,'AFT3P1'	,T10,E15.7	ORDI0151
	*	/2X,'AFZ3P0'	,T10,E15.7	ORDI0152
	*	/2X,'AFZ3P1'	,T10,E15.7	ORDI0153
450		CONTINUE		ORDI0154
		IF(IITYPE.EQ.0) GO TO 851		ORDI0155
		NN=NN+1		ORDI0156
		DO 101 JQ=1,4		ORDI0157
		DO 101 IQ=1,4		ORDI0158
		CALL INTEG(FSUM,NN,JQ,IQ)		ORDI0159
		DAH(JQ,IQ)=CK*FSUM/R**2		ORDI0160
101		CONTINUE		ORDI0161
		NK=NN		ORDI0162
2001		NN=NN+1		ORDI0163
		DO 301 JQ=1,4		ORDI0164
		CALL INTEG(FSUM,NN,JQ,IQ)		ORDI0165
		FSUM=FSUM*R**2		ORDI0166
		NM=NN-NK		ORDI0167
		GO TO (32,33),NM		ORDI0168
32		DAW(JQ)=FSUM		ORDI0169
		GO TO 301		ORDI0170
33		OAV1(JQ)=FSUM		ORDI0171
301		CONTINUE		ORDI0172
		IF(NN.LT.33) GO TO 2001		ORDI0173
		NN=NN+1		ORDI0174
		DO 302 JQ=1,4		ORDI0175
		CALL INTEG(FSUM,NN,JQ,IQ)		ORDI0176
		FSUM=FSUM*CK/R		ORDI0177
		DAHIII(JQ)=FSUM		ORDI0178
302		CONTINUE		ORDI0179
		NN=NN+1		ORDI0180

	DO 780 JQ=1,4	ORDI0181
	CALL INTEG(FSUM,NN,JQ,IQ)	ORDI0182
	FSUM=FSUM*CK/R*AND	ORDI0183
	DAHV(JQ)=FSUM	ORDI0184
780	CONTINUE	ORDI0185
	NN=NN+1	ORDI0186
	DO 781 JQ=1,4	ORDI0187
	CALL INTEG(FSUM,NN,JQ,IQ)	ORDI0188
	FSUM=FSUM*CK/P*AND	ORDI0189
	DAHIV(JQ)=FSUM	ORDI0190
781	CONTINUE	ORDI0191
	IF (IDEBUG.EQ.0) GO TO 851	ORDI0192
	WRITE(6,80) ((DAH(I,J),J=1,4),I=1,4)	ORDI0193
80	FORMAT(2X,'DAH',4(T10,4(E15.7,2X)/1X))	ORDI0194
	WRITE(6,81) DAW0,DAV1,DAHIII,DAHV,DAHIV	ORDI0195
81	FORMAT(2X,'DAW0',T10,4(E15.7,2X)	ORDI0196
	* /2X,'DAV1',T10,4(E15.7,2X)	ORDI0197
	* /2X,'DAHIII',T10,4(E15.7,2X)	ORDI0198
	* /2X,'DAHV',T10,4(E15.7,2X)	ORDI0199
	* /2X,'DAHIV',T10,4(E15.7,2X)	ORDI0200
851	RETURN	ORDI0201
	END	ORDI0202

```
      SUBROUTINE INTEG(FSU*,NN,JQ,IQ)
C
C NUMERICAL INTEGRATION----GAUSSIAN QUADRATURE
C
      COMMON /AREA2/NPT,XXX(20),A(20)
      SUM=0.0
      DO 40 JJJ=1,NPT
      X=XXX(JJJ)
      SUM=SUM+A(JJJ)*F(X,NN,JJJ,JQ,IQ)
40 CONTINUE
      FSUM=0.5*SUM
      RETURN
      END
```

```
INTE0001
INTE0002
INTE0003
INTE0004
INTE0005
INTE0006
INTE0007
INTE0008
INTE0009
INTE0010
INTE0011
INTE0012
INTE0013
```

FUNCTION F(X,NN, JJJ, JQ, IC)

TO DEFINE THE INTEGRAND FUNCTIONS

COMMON/AREA4/H(4,4,20),HI(4,20),HII(4,20),HRZ(4,20),HNR(4,20),
%WO(4,20),VO(4,20),W1(4,20),V1(4,20)
@ ,DH(4,4,20),DWC(4,20),DVI(4,20),DHIII(4,20),CHIII(4,20)
@ ,OHV(4,20),OHIV(4,20)
COMMON/AKKH/FTOP1(20),FT1P0(20),FT1P2(20),FT2P1(20), FZ2P0(20),
/FZ0P0(20),FZ1P1(20),FZ2P2(20)
@ ,FT3P0(20),FT3P1(20),FZ3P0(20),FZ3P1(20)
COMMON/ADFB/HIII(4,20),HIV(4,20),HV(4,20),HVI(4,20),HVII(4,20)
COMMON/WINGAR/TSDS(20,6,6),TSAS(20,6,6),TSAG(20,6,3)
GC TO(1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,
@21,22,23,24,25,26,27,28,29,30,31,32,33,34,35,36),NN

1 F=H(JQ,IC, JJJ)

RETURN

2 F=HI(JQ, JJJ)

RETURN

3 F=HII(JQ, JJJ)

RETURN

4 F=HRZ(JQ, JJJ)

RETURN

5 F=HNR(JQ, JJJ)

RETURN

6 F= W0(JQ, JJJ)

RETURN

7 F= VO(JQ, JJJ)

RETURN

8 F= W1(JQ, JJJ)

RETURN

9 F= V1(JQ, JJJ)

RETURN

10 F=FTOP1(JJJ)

RETURN

11 F=FT1P0(JJJ)

F 0001
F 0002
F 0003
F 0004
F 0005
F 0006
F 0007
F 0008
F 0009
F 0010
F 0011
F 0012
F 0013
F 0014
F 0015
F 0016
F 0017
F 0018
F 0019
F 0020
F 0021
F 0022
F 0023
F 0024
F 0025
F 0026
F 0027
F 0028
F 0029
F 0030
F 0031
F 0032
F 0033
F 0034
F 0035
F 0036

	RETURN	F	0037
12	F=FT1P2(JJJ)	F	0038
	RETURN	F	0039
13	F=FT2P1(JJJ)	F	0040
	RETURN	F	0041
14	F=FZ0P0(JJJ)	F	0042
	RETURN	F	0043
15	F=FZ1P1(JJJ)	F	0044
	RETURN	F	0045
16	F=FZ2P0(JJJ)	F	0046
	RETURN	F	0047
17	F=FZ2P2(JJJ)	F	0048
	RETURN	F	0049
18	F=HIII(JQ, JJJ)	F	0050
	RETURN	F	0051
19	F=HIV(JQ, JJJ)	F	0052
	RETURN	F	0053
20	F=HV(JQ, JJJ)	F	0054
	RETURN	F	0055
21	F=HVI(JQ, JJJ)	F	0056
	RETURN	F	0057
22	F=HVII(JQ, JJJ)	F	0058
	RETURN	F	0059
23	F=TSDS(JJJ, JQ, IQ)	F	0060
	RETURN	F	0061
24	F=TSAS(JJJ, JQ, IQ)	F	0062
	RETURN	F	0063
25	F=TSAG(JJJ, JQ, IQ)	F	0064
	RETURN	F	0065
26	F=CHIII(JQ, JJJ)	F	0066
	RETURN	F	0067
27	F=FT3P0(JJJ)	F	0068
	RETURN	F	0069
28	F=FT3P1(JJJ)	F	0070
	RETURN	F	0071
29	F=FZ3P0(JJJ)	F	0072

	RETURN	F	0073
30	F=FZ3P1(JJJ)	F	0074
	RETURN	F	0075
31	F=OH(JQ,IC,JJJ)	F	0076
	RETURN	F	0077
32	F=OWO(JQ,JJJ)	F	0078
	RETURN	F	0079
33	F=OVI(JQ,JJJ)	F	0080
	RETURN	F	0081
34	F=OHIII(JQ,JJJ)	F	0082
	RETURN	F	0083
35	F=OHV(JQ,JJJ)	F	0084
	RETURN	F	0085
36	F=OHIV(JQ,JJJ)	F	0086
	RETURN	F	0087
	END	F	0088

SUBROUTINE AINER

C
C
C
CTO DEFINE THE EQUATION'S COEFFICIENTS IN MATRIX FORM RELATING TO
INERTIA TERMS

```

COMMON /PARMT/      ITYPE ,IFLT
COMMON /AREA1/OMEGA,R,VEL,CL,CD,RAMDA,SNOMEG
COMMON /AREA6/NOBLD,ROH,CHOD,AIB,CK,HMAST ,ALOCK ,ANO,HR
COMMON/AREA5/AH(4,4),AHI(4),AHII(4),AHRZ(4),AHNR(4),AWO(4),AVO(4)
a,AWI(4),AVI(4),OAH(4,4),OAWO(4),OAVI(4),OAHIII(4),CAHIII(4)
a ,OAHV(4),OAHIV(4)
COMMON/INERTI/TTMT(4,6,3),TTCTJ(4,6,3),AMJT(4,3,6),CJT(4,3,6)
COMMON/AMATIC/TT(6,5),C(6,6) ,T(5,6)
DIMENSION AMT(4,5,3),CJ(4,3,5),AM(4,3,5),TCJ(4,5,3)
DO 50 I=1,4
DO 50 J=1,5
DO 50 K=1,3
AMT(I,J,K)=0.0
50 CJ(I,K,J)=0.0
DO 210 NM=1,4
AMT(NM,1,3)=-AVO(NM)/R
AMT(NM,2,1)=AWO(NM)/R
AMT(NM,3,2)=-AVC(NM)*HR
AMT(NM,3,3)=AWI(NM)
AMT(NM,4,2)=-AWI(NM)
AMT(NM,4,3)=-AVO(NM)*HR
AMT(NM,5,1)=AVI(NM)
IF(ITYPE.EQ.0) GO TO 300
AMT(NM,2,1)=OAWO(NM)/R
AMT(NM,5,1)=OAVI(NM)
300 CONTINUE
DO 2 I=1,6
DO 2 J=1,3
DO 2 K=1,5
2 TTMT(NM,I,J)=TT(I,K)*AMT(NM,K,J)+TTMT(NM,I,J)
DO 3 I=1,6

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AINE0001
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 AINE0025
 AINE0026
 AINE0027
 AINE0028
 AINE0029
 AINE0030
 AINE0031
 AINE0032
 AINE0033
 AINE0034
 AINE0035
 AINE0036

	DO 3 J=2,3	AINEO037
3	TTMT(NM,I,J)=0.5*TTMT(NM,I,J)	AINEO038
	CJ(NM,2,3)=2.0*AW1(NM)	AINEO039
	CJ(NM,3,4)=2.0*AW1(NM)	AINEO040
	DO 5 I=1,5	AINEO041
	DO 5 J=1,3	AINEO042
5	TCJ(NM,I,J)=CJ(NM,J,I)	AINEO043
	DO 6 I=1,6	AINEO044
	DO 6 J=1,3	AINEO045
	DO 6 K=1,5	AINEO046
6	TTCTJ(NM,I,J)=TT(I,K)*TCJ(NM,K,J)+TTCTJ(NM,I,J)	AINEO047
	DO 100 I=1,6	AINEO048
	DO 100 J=2,3	AINEO049
100	TTCTJ(NM,I,J)=0.5*TTCTJ(NM,I,J)	AINEO050
	DO 7 I=1,5	AINEO051
	DO 7 J=1,6	AINEO052
7	T(I,J)=T(J,I)	AINEO053
	DO 8 I=1,3	AINEO054
	DO 8 J=1,5	AINEO055
8	AM(NM,I,J)=AMT(NM,J,I)	AINEO056
	DO 9 I=1,3	AINEO057
	DO 9 J=1,6	AINEO058
	DO 9 K=1,5	AINEO059
9	AMJT(NM,I,J)=AM(NM,I,K)*T(K,J)+AMJT(NM,I,J)	AINEO060
	DO 10 I=1,3	AINEO061
	DO 10 J=1,6	AINEO062
	DO 10 K=1,5	AINEO063
10	CJT(NM,I,J)=CJ(NM,I,K)*T(K,J)+CJT(NM,I,J)	AINEO064
210	CONTINUE	AINEO065
	RETURN	AINEO066
	END	AINEO067

SUBROUTINE AEROMT

TO DEFINE THE EQUATION'S COEFFICIENTS IN MATRIX FORM RELATING TO
AERODYNAMIC TERMS

```

COMMON /PARMT/      ITYPE ,IFLT
COMMON /AREA6/NOBLD,RCH,CHOD,AIB,CK,HMAST ,ALOCK ,AND,HR
COMMON/AREA5/AH(4,4),AHI(4),AHI1(4),AHRZ(4),AHNR(4),AWO(4),AVO(4)
@,AW1(4),AV1(4),OAH(4,4),CAWO(4),CAV1(4),OAHIII(4),CAHIII(4)
@
@,CAHV(4),OAHIV(4)
COMMON /AREA1/OMEGA,R,VEL,CL,CD,RAMDA,SNOMEG
COMMON/AERO/AFTOP1,AFT1FO,AFT1P2,AFT2P1,AFZOP0,AFZ1P1,AFZ2P0,
@AFZ2P2,AHIII(4),AHIV(4),AHV(4),AHVI(4),AHVII(4)
@
@,AFT3P0,AFT3P1,AFZ3P0,AFZ3P1
COMMON/AMATIC/TT(6,5),C(6,6) ,T(5,6)
COMMON /ARR/WGUST(6,6),CAMX(6,6),AMX(6,6),DQ(4,6,3),Q(4,6,3)
@
@,DHMAX(4,3,6),HMAX(4,3,6)
COMMON /COUPL/      AKPC(4),AKPD(4)
DIMENSION              CDHMX(4,3,5),CHMX(4,3,5)
DIMENSION GUST(5,6),CCAMX(5,5),CCDAMX(6,5),CAMX(5,5),CCAMX(6,5)
@,CDQ(4,5,3),CQ(4,5,3)
DC 100 I=1,4
DC 100 J=1,3
DC 100 K=1,5
CDHMX(I,J,K)=0.0
CHMX(I,J,K)=0.0
CDQ(I,K,J)=0.0
100 CQ(I,K,J)=0.0
DC 101 I=1,5
DC 102 J=1,5
CAMX(I,J)=0.0
102 CCDAMX(I,J)=0.0
DC 103 K=1,6
GUST(I,K)=0.0
CCDAMX(K,I)=0.0
103 CCAMX(K,I)=0.0

```

AER00001
AER00002
AER00003
AER00004
AER00005
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AER00009
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AER00035
AER00036

101	CONTINUE	AER00037
	DO 1 I=1,2	AER00038
	DO 1 J=1,6	AER00039
1	T(I,J)=T(I,J)/R	AER00040
	DO 2 I=1,6	AER00041
	DO 2 J=1,2	AER00042
2	TT(I,J)=TT(I,J)/R	AER00043
	GUST(1,1)=0.5*AFT1P0	AER00044
	GUST(2,3)=AFZ2P0	AER00045
	GUST(3,1)=-0.5*AFZ1P1	AER00046
	GUST(3,2)=-HR*AFT1P0 *0.5	AER00047
	GUST(4,1)=0.5*HR*AFT1P0	AER00048
	GUST(4,2)=-AFZ1P1 *0.5	AER00049
	GUST(5,3)=AFT2P1	AER00050
	GUST(1,6)=0.5*AFT3PJ	AER00051
	GUST(2,4)=AFZ3P0	AER00052
	GUST(3,5)=-0.5*HR*AFT3PC	AER00053
	GUST(3,6)=0.5*AFZ3P1	AER00054
	GUST(4,5)=-0.5*AFZ3P1	AER00055
	GUST(4,6)=-0.5*HR*AFT3PC	AER00056
	GUST(5,4)=AFT3P1	AER00057
	DO 5 I=1,6	AER00058
	DO 5 J=1,6	AER00059
	DO 5 K=1,5	AER00060
5	WGUST(I,J)=TT(I,K)*GUST(K,J)+WGUST(I,J)	AER00061
	DO 6 I=1,6	AER00062
	DO 6 J=1,3	AER00063
6	WGUST(I,J)=WGUST(I,J)*ABS(RAMDA)	AER00064
	CDAMX(1,1)=0.5*AFT1P0	AER00065
	CDAMX(1,3)=-0.5*AFT2P1	AER00066
	CDAMX(1,4)=0.5*HR*AFT1P0	AER00067
	CDAMX(2,2)=AFZ2P0	AER00068
	CDAMX(2,5)=AFZ1P1	AER00069
	CDAMX(3,1)=-0.5*AFZ1P1	AER00070
	CDAMX(3,3)=0.5*(HR**2*AFT1P0+AFZ2P2)	AER00071
	CDAMX(3,4)=0.5*HR*(AFT2P1-AFZ1P1)	AER00072

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CDAMX(4,1)=0.5*HR*AFT1P0
CDAMX(4,3)=HR*( -AFT2P1+AFZ1P1) *0.5
CCAMX(4,4)=0.5*(HR**2*AFT1P0+AFZ2P2)
CDAMX(5,2)=AFT2P1
CDAMX(5,5)=AFT1P2
  DO 9 I=1,6
  DO 9 J=1,5
  DO 9 K=1,5
9  CCDAMX(I,J)=TT(I,K)*CDAMX(K,J)+CCDAMX(I,J)
  DO 11 I=1,6
  DO 11 J=1,6
  DO 11 K=1,5
11 DAMX(I,J)=CCDAMX(I,K)*T(K,J)+DAMX(I,J)
  AMDA=ABS(RAMDA)
  CAMX(1,4)=-0.5*AMDA*AFT1P0+AFZ0P0
  CAMX(3,3)=HR*(AFZ0P0-0.5*AMDA*AFT1P0)
  CAMX(3,4)=0.5*AMDA*AFZ1P1+AFT0P1
  CAMX(4,3)=-0.5*AMDA*AFZ1P1
  CAMX(4,4)=HR*(-0.5*AMDA*AFT1P0+AFZ0P0)
  DO 12 I=1,6
  DO 12 J=1,5
  DO 12 K=1,5
12 CCAMX(I,J)=TT(I,K)*CAMX(K,J)+CCAMX(I,J)
  DO 13 I=1,6
  DO 13 J=1,6
  DO 13 K=1,5
13 AMX(I,J)=CCAMX(I,K)*T(K,J)+AMX(I,J)
  DO 40 NM=1,4
  CCQ(NM,1,3)=-0.5*AHIII(NM)
  CCQ(NM,2,1)=AHV(NM)
  CCQ(NM,3,2)=-0.5*HR*AHIII(NM)
  CCQ(NM,3,3)=0.5*AHVI(NM)
  CCQ(NM,4,2)=-0.5*AHVI(NM)
  CCQ(NM,4,3)=-0.5*HR*AHIII(NM)
  CCQ(NM,5,1)=AHIV(NM)
  CCQ(NM,1,2)=0.5*AHIII(NM)*SACMEG

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AER00107
AER00108

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```

CQ(NM,3,2)=0.5*(AHVII(NM)-AHVI(NM)*SNOMEG)
CQ(NM,3,3)=-0.5*HR*AHIII(NM)*SNOMEG
CQ(NM,4,2)=0.5*HR*AHIII(NM) *SNOMEG
CQ(NM,4,3)=0.5*(AHVII(NM)- AHVI(NM) *SNOMEG)
IF(ITYPE.EQ.0) GO TO 110
CDQ(NM,2,1)=0AHV(NM)
CDQ(NM,5,1)=0AHIV(NM)
CQ(NM,1,3)=0.5*AKPC(NM)*AFT3P0
CQ(NM,2,1)=AKPJ(NM)*AFZ3P0
CQ(NM,3,2)=CQ(NM,3,2)-0.5*HR*AKPC(NM)*AFT3P0
CQ(NM,3,3)=CQ(NM,3,3)+0.5*AKPC(NM)*AFZ3P1
CQ(NM,4,2)=CQ(NM,4,2)-0.5*AKPC(NM)*AFZ3P1
CQ(NM,4,3)=CQ(NM,4,3)-0.5*HR*AKPC(NM)*AFT3P0
CQ(NM,5,1)=AKPJ(NM)*AFT3P1
110 CONTINUE
DO 16 I=1,6
DO 16 J=1,3
DO 16 K=1,5
Q(NM,I,J)=TT(I,K)*CQ(NM,K,J)+Q(NM,I,J)
16 DQ(NM,I,J)=TT(I,K)*CDQ(NM,K,J)+DQ(NM,I,J)
C AERG FOR BLADES DUE TO WING MOTION
CDHMX(NM,1,2)=AHRZ(NM)
CDHMX(NM,1,5)=AHNR(NM)
CDHMX(NM,2,3)=-HR*AHI(NM)
CDHMX(NM,2,4)=-AHII(NM)
CDHMX(NM,3,1)=-AHI(NM)
CDHMX(NM,3,3)=AHII(NM)
CDHMX(NM,3,4)=-HR*AHI(NM)
CHMX(NM,2,3)=AMDA*AHI(NM)
CHMX(NM,3,4)=AMDA*AHI(NM)
DO 20 I=1,3
DO 20 J=1,6
DO 20 K=1,5
DHMAX(NM,I,J)=CDHMX(NM,I,K)*T(K,J)+DHMAX(NM,I,J)
20 HMAX(NM,I,J)=CHMX(NM,I,K)*T(K,J)+HMAX(NM,I,J)
40 CONTINUE

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AER00109
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AER00144

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133

RE TURN
END

AERO0145
AERO0146

134

SUBROUTINE EQMTX(IDOF)

TO DEFINE THE COEFFICIENT MATRICES A,B,C AND D IN EQ. 2.3

```
COMMON /PARMT/ ITYPE ,IFLT
COMMON/AREA8/BLAM(4),WLAM(6),BRAM(4),WRAM(6),BLAM0(4),BRAM0(4)
COMMON /AREA1/OMEGA,R,VEL,CL,CD,RAMDA,SNOMEG
COMMON /AREA6/NOBLD,RCH,CHOD,AIB,CK,FMAST ,ALOCK ,ANO,HR
COMMON/AMATIC/TT(6,5),C(6,6) ,T(5,6)
COMMON/AREA5/AH(4,4),AHI(4),AHII(4),AHRZ(4),AHNR(4),AWO(4),AVO(4)
a,AWI(4),AVI(4),CAH(4,4),DAWI(4),DAVI(4),CAHIII(4),CAHIII(4)
a ,CAHV(4),DAHIV(4)
COMMON/INERTI/TTMT(4,6,3),TTCTJ(4,6,3),AMJT(4,3,6),CJT(4,3,6)
COMMON /ARR/WGUST(6,6),DAMX(6,6),AMX(6,6),DQ(4,6,3),Q(4,6,3)
a ,DHMAX(4,3,6),FMAX(4,3,6)
COMMON/ARWNG/DARWA(6,6),ARWA(6,6),ARWG(6,3)
COMMON/DOF18/AAY(19,19),BBY(19,19),CCY(19,19),DDY(19,6)
COMMON /COUPL/ AKPC(4),AKPD(4)
WRITE(6,450)
450 FORMAT(///1X,75(1H-))//15X,44HEQUATIONS OF MOTION : A*X''+B*X'+C
&*X=D*E ,//1X,75(1H-))//)
DO 801 I=1,18
801 AAY(I,I)=1.0
DC 802 NM=1,4
DO 802 I=1,3
DC 802 J=1,6
AAY(3*(NM-1)+I,J+12)=AMJT(NM,I,J)
802 AAY(J+12,3*(NM-1)+I)=ANC*TTMT(NM,J,I)
DC 804 I=1,4
BBY(3*I-1,3*I)=2.0*SNOMEG
804 BBY(3*I,3*I-1)=-2.0*SNOMEG
DC 805 J=1,4
DC 805 I=1,4
DO 805 K=1,3
805 BBY(3*(J-1)+K,3*(I-1)+K)=AH(J,I)
DC 806 NM=1,4
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EQMT0026
EQMT0027
EQMT0028
EQMT0029
EQMT0030
EQMT0031
EQMT0032
EQMT0033
EQMT0034
EQMT0035
EQMT0036

	DC 806 I=1,3		EQMT0037
	DO 806 J=1,6		EQMT0038
	BBY(3*(NM-1)+I,J+12)=DHMAX(NM,I,J)+CJT(NM,I,J)*SNOMEG		EQMT0039
806	BBY(J+12,3*(NM-1)+I)=DC(NM,J,I)-AND*TTCTJ(NM,J,I)*SNOMEG		EQMT0040
	DC 808 I=1,6		EQMT0041
	DO 808 J=1,6		EQMT0042
808	BBY(I+12,J+12)=DAMX(I,J)+C(I,J)*SNOMEG-DARWA(I,J)		EQMT0043
	CC 809 I=1,4		EQMT0044
	CCY(3*(I-1)+1,3*(I-1)+1)=BLAM(I)		EQMT0045
	CCY(3*(I-1)+2,3*(I-1)+2)=BLAM(I)-1.0		EQMT0046
809	CCY(3*I,3*I)=BLAM(I)-1.0		EQMT0047
	DC 810 J=1,4		EQMT0048
	DO 810 I=1,4		EQMT0049
	CCY(3*J-1,3*I)=AH(J,I)*SNOMEG		EQMT0050
810	CCY(3*J,3*I-1)=-AH(J,I)*SNOMEG		EQMT0051
	DC 811 NM=1,4		EQMT0052
	DO 811 I=1,3		EQMT0053
	DO 811 J=1,6		EQMT0054
	CCY(3*(NM-1)+I,J+12)=HMAX(NM,I,J)		EQMT0055
811	CCY(J+12,3*(NM-1)+I)=G(NM,J,I)		EQMT0056
	DO 812 I=1,6		EQMT0057
	DO 812 J=1,6		EQMT0058
812	CCY(I+12,J+12)=AMX(I,J) -ARWA(I,J)		EQMT0059
	CC 813 I=1,6		EQMT0060
813	CCY(I+12,I+12)=CCY(I+12,I+12)+WLAM(I)		EQMT0061
	DC 814 NM=1,4		EQMT0062
	DDY(3*(NM-1)+1,4)=-CAHIII(NM)		EQMT0063
	DDY(3*(NM-1)+2,5)=-CAHIII(NM)		EQMT0064
	DDY(3*(NM-1)+3,6)=-CAHIII(NM)		EQMT0065
	DDY(3*NM-1,2)=AHI(NM)*ABS(RAMCA) *(-1.0)		EQMT0066
	DDY(3*NM-2,3)=AHRZ(NM)*ABS(RAMDA) *(-1.0)		EQMT0067
814	DDY(3*NM,1)=-AHI(NM)*ABS(RAMDA) *(-1.0)		EQMT0068
	CC 815 I=1,6		EQMT0069
	DO 816 J=1,3		EQMT0070
816	DDY(I+12,J)=-WGUST(I,J) +ARWG(I,J)		EQMT0071
	DC 817 J=4,6		EQMT0072

```

817  DDY(I+12,J)=-WGUST(I,J)
815  CCNTINUE
      IF(IITYPE.EQ.0)GO TO 300
      DO 500 J=1,4
      DO 500 I=1,4
500  BBY(3*(J-1)+1,3*(I-1)+1)=OAH(J,I)
      DO 550 I=1,4
      CCY(3*(I-1)+1,3*(I-1)+1)=BLAMO(I)
      CCY(3*(I-1)+2,3*(I-1)+2)=BLAM(I)-1.0
550  CCY(3*I,3*I)=BLAM(I)-1.0
      DO 502 J=1,4
      DO 502 I=1,4
      CCY(3*J-2,3*I-2)=CCY(3*J-2,3*I-2)+AKPD(I)*OAHIII(J)
      CCY(3*J-1,3*I-1)=CCY(3*J-1,3*I-1)+AKPC(I)*CAHIII(J)
5J2  CCY(3*J ,3*I )=CCY(3*J ,3*I )+AKPC(I)*CAHIII(J)
      DO 501 NM=1,4
501  DDY(3*(NM-1)+1,4)=-OAHIII(NM)
300  CCNTINUE
      IF(IDDF.EQ.9) GO TO 100
      IF(IFLT.NE.0) GO TO 205
      WRITE(6,451)
      WRITE(6,6)(( AAY(I,J),J=1,9),I=1,18)
      WRITE(6,6)((AAY(I,J),J=10,18),I=1,18)
      WRITE(6,5)
      WRITE(6,452)
      WRITE(6,6)(( BBY(I,J),J=1,9),I=1,18)
      WRITE(6,6)((BBY(I,J),J=10,18),I=1,18)
      WRITE(6,5)
      WRITE(6,453)
      WRITE(6,6)(( CCY(I,J),J=1,9),I=1,18)
      WRITE(6,6)((CCY(I,J),J=10,18),I=1,18)
      WRITE(6,5)
      WRITE(6,454)
      WRITE(6,7)((DDY(I,J),J=1,6),I=1,18)
5    FORMAT(1H1)
6    FORMAT(////1X,18(/1X,9(E12.5,1X)))

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EQMT0073
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EQMT0097
EQMT0098
EQMT0099
EQMT0100
EQMT0101
EQMT0102
EQMT0103
EQMT0104
EQMT0105
EQMT0106
EQMT0107
EQMT0108

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7      FORMAT(///1X,18(/1X,6(E12.5,1X)))
451    FORMAT(2CX,'A MATRIX=')
452    FURMAT(//20X,'B MATRIX=')
453    FORMAT(//20X,'C MATRIX=')
454    FORMAT(//20X,'D MATRIX=')
      RETURN
100    CCONTINUE
      DO 201 I=1,6
      DC 201 J=7,9
      AAY(I,J)=AAY(I,J+6)
      BBY(I,J)=BBY(I,J+6)
      CCY(I,J)=CCY(I,J+6)
      AAY(J,I)=AAY(J+6,I)
      BBY(J,I)=BBY(J+6,I)
201    CCY(J,I)=CCY(J+6,I)
      DO 202 I=7,9
      DO 202 J=7,9
      AAY(I,J)=AAY(I+6,J+6)
      BBY(I,J)=BBY(I+6,J+6)
202    CCY(I,J)=CCY(I+6,J+6)
      DO 204 I=7,9
      DC 204 J=1,6
204    DDY(I,J)=DDY(I+6,J)
      IF(IFLT.NE.0) GO TO 205
      WRITE(6,451)
      WRITE(6,850)((AAY(I,J),J=1,9),I=1,9)
      WRITE(6,452)
      WRITE(6,850)((BBY(I,J),J=1,9),I=1,9)
      WRITE(6,453)
      WRITE(6,850)((CCY(I,J),J=1,9),I=1,9)
      WRITE(6,454)
      WRITE(6,950)((DDY(I,J),J=1,6),I=1,9)
850    FURMAT(///1X,9(/1X,9(E12.5,1X)))
950    FORMAT(///1X,9(/1X,6(E12.5,1X)))
205    CONTINUE
      RETURN

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EQMT0109
EQMT0110
EQMT0111
EQMT0112
EQMT0113
EQMT0114
EQMT0115
EQMT0116
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EQMT0118
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EQMT0121
EQMT0122
EQMT0123
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EQMT0140
EQMT0141
EQMT0142
EQMT0143
EQMT0144

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END

EQMT0145

SUBROUTINE AUTO(IDDF)

IN AUTOROTION FLIGHT ANOTHER DEGREE OF FREEDOM IS ADDED

COMMON /PARMT/ ITYPE ,IFLT
COMMON/AMATIC/TT(6,5),C(6,6) ,T(5,6)
COMMON /AREA6/NOBLD,ROH,CHOD,AIB,CK,HMAST ,ALOCK ,ANG,HR
COMMON/AREA5/AH(4,4),AHI(4),AHII(4),AHRZ(4),AHNR(4),AWO(4),AVO(4)
@ ,AWI(4),AVI(4),OAH(4,4),CAWC(4),CAVI(4),CAHIII(4),CAHIII(4)
@ ,CAHV(4),OAHIV(4)
COMMON/DDF18/AAY(19,19),BBY(19,19),CCY(19,19),DDY(19,6)
COMMON /COUPL/ AKPC(4),AKPD(4)
COMMON/AERO/AFTOP1,AFT1P0,AFT1P2,AFT2P1,AFZOP0,AFZ1P1,AFZ2P0,
@AFZ2P2,AHIII(4),AHIV(4),AHV(4),AHVI(4),AHVII(4)
@ ,AFT3P0,AFT3P1,AFZ3P0,AFZ3P1
NB=4
N_h=6
NR=19
DO 11 I=1,NB
AAY(3*I-2,NR)=AVI(I)
AAY(NR,3*I-2)=AVI(I)*ANG
BBY(3*I-2,NR)=AHNR(I)
BBY(NR,3*I-2)=AHIV(I)
11 CONTINUE
DO 12 I=1,N_h
BBY(NR,3*NB+I)=AFT2P1*T(2,I)
BBY(3*NR+I,NR)=AFZ1P1*T(2,I)
12 CONTINUE
AAY(NR,NR)=AIB*ANG
BBY(NR,NR)=AFT1P2
CCY(NR,3)=-AFT2P1
DDY(NR,4)=-AFT3P1
IF(ITYPE.EQ.0) GO TO 13
DO 14 I=1,NB
AAY(3*I-2,NR)=CAVI(I)
AAY(NR,3*I-2)=CAVI(I)*ANG

AUTOJ001
AUTOJ002
AUTO0003
AUTOJ014
AUTOJ005
AUTO0006
AUTOJ007
AUTOJ008
AUTO0009
AUTO0010
AUTOJ011
AUTOJ012
AUTO0013
AUTO0014
AUTOJ015
AUTO0016
AUTO0017
AUTO0018
AUTO0019
AUTOJ020
AUTO0021
AUTO0022
AUTOJ023
AUTO0024
AUTOJ025
AUTO0026
AUTO0027
AUTOJ028
AUTO0029
AUTOJ030
AUTOJ031
AUTO0032
AUTO0033
AUTOJ034
AUTO0035
AUTOJ036

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BBY(NR,3*I-2)=DAHIV(I)
CCY(NR,3*I-2)=AKPO(I)*AFT3P1
14 CONTINUE
13 CONTINUE
IF(IDCF.EC.9) GO TO 100
WRITE(6,451)
WRITE(6,6)(( AAY(I,J),J=1,9),I=1,19)
WRITE(6,8)((AAY(I,J),J=10,19),I=1,19)
WRITE(6,5)
WRITE(6,452)
WRITE(6,6)(( BBY(I,J),J=1,9),I=1,19)
WRITE(6,8)((BBY(I,J),J=10,19),I=1,19)
WRITE(6,5)
WRITE(6,453)
WRITE(6,6)(( CCY(I,J),J=1,9),I=1,19)
WRITE(6,8)((CCY(I,J),J=10,19),I=1,19)
WRITE(6,5)
WRITE(6,454)
WRITE(6,7)((DDY(I,J),J=1,6),I=1,19)
5 FORMAT(1H1)
6 FORMAT(///1X,19(/1X,9(E12.5,1X)))
7 FORMAT(///1X,19(/1X,6(E12.5,1X)))
8 FORMAT(///1X,19(/1X,10(E12.5,1X)))
RETURN
100 CONTINUE
DC 15 I=1,6
AAY(I,10)=AAY(I,19)
BBY(I,10)=BBY(I,19)
CCY(I,10)=CCY(I,19)
AAY(10,I)=AAY(19,I)
BBY(10,I)=BBY(19,I)
CCY(10,I)=CCY(19,I)
DDY(10,I)=DDY(19,I)
15 CONTINUE
DO 16 I=1,3
AAY(I+6,10)=AAY(I+12,19)

```

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AUTO0037
AUTO0038
AUTO0039
AUTO0040
AUTO0041
AUTO0042
AUTO0043
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AUTO0045
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AUTO0070
AUTO0071
AUTO0072

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```

BBY(I+6,10)=BBY(I+12,19)
CCY(I+6,10)=CCY(I+12,19)
AAZ(I0,I+6)=AAZ(19,I+12)
BBY(10,I+6)=BBY(19,I+12)
CCY(10,I+6)=CCY(19,I+12)
16  CONTINUE
AAZ(10,10)=AAZ(19,19)
BBY(10,10)=BBY(19,19)
CCY(10,10)=CCY(19,19)
WRITE(6,451)
WRITE(6,850)((AAZ(I,J),J=1,10),I=1,10)
WRITE(6,452)
WRITE(6,850)((BBY(I,J),J=1,10),I=1,10)
WRITE(6,453)
WRITE(6,850)((CCY(I,J),J=1,10),I=1,10)
WRITE(6,454)
WRITE(6,850)((DDY(I,J),J=1,6),I=1,10)
451  FORMAT(20X,'A MATRIX=')
452  FORMAT(//20X,'B MATRIX=')
453  FORMAT(//20X,'C MATRIX=')
454  FORMAT(//20X,'D MATRIX=')
850  FORMAT(///1X,10(/1X,10(E12.5,1X)))
950  FORMAT(///1X,10(/1X,6(E12.5,1X)))
RETURN
END

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AUTO0073
AUTO0074
AUTO0075
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AUTO0097

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SUBROUTINE GUSTCC(CCLST,DBY,L,DDZ)
C
C      TO DEFINE GLST AND BLADE PITCH CONTROL COMPONENTS
C
      DIMENSION CCLST(6),EDY(19,6) ,DDZ(19)
      DO 1 I=1,L
      DDZ(I)=0.0
      DO 2 I=1,L
      DO 2 J=1,6
      DDZ(I)=EDY(I,J)*CCLST(J)+DDZ(I)
      RETURN
      END

```

```

GUST0001
GUST0002
GUST0003
GUST0004
GUST0005
GUST0006
GUST0007
GUST0008
GUST0009
GUST0010
GUST0011
GUST0012

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SUBROUTINE FRQRES(L,AAA,BBB,CCC,DDD,IFLT,IDCF)
C
C      TO CALCULATE THE FREQUENCY RESPONSE
C
      DIMENSION AAA(19,19),BBB(19,19),CCC(19,19),DDD(19)
      DOUBLE PRECISION FREQ,DPA(19,19),DPR(19,19),DPC(19,19),DPD(19)
      COMPLEX*16 CCMA(19,19),CCME(19),DCMPLX
      WRITE(6,1000)
1000  FORMAT(///10X,40(1H-),//20X,'FREQUENCY RESPONSE',//10X,40(1H-),
*      ///4X,'--FREQUENCY/OMEGA--')
      IF(IDCF.EQ.18) GO TO 1001
      WRITE(6,1002)
1002  FORMAT(//10X,'Q1C',T22,'Q1C',T34,'Q1S',T46,'Q2C',T58,'Q2C',T70,
*      'Q2S',T82,'WING 1',T94,'WING 2',T106,'WING 3')
      GO TO 1003
1001  WRITE(6,1004)
1004  FORMAT(//10X,'Q1C',T22,'Q1C',T34,'Q1S',T46,'Q2C',T58,'Q2C',T70,
*      'Q2S',T82,'Q3C',T94,'Q3C',T106,'Q3S'//10X,'Q4C',T22,
*      'Q4C',T34,'Q4S',T46,'WING 1',T58,'WING 2',T70,'WING 3',
*)      T82,'WING 4',T94,'WING 5',T106,'WING 6')
1003  CONTINUE
      IF(IFLT.EQ.0) GO TO 1007
      WRITE(6,1005)
1005  FORMAT(//10X,'D(NU R)/DT')
1007  CONTINUE
      DO 180 I=1,L
      DO 180 J=1,L
      DPA(I,J)=AAA(I,J)
      DPR(I,J)=BBB(I,J)
      DPC(I,J)=CCC(I,J)
180  CONTINUE
      DO 181 I=1,L
      DPD(I) =DDD(I)
181  CONTINUE
      IK=J
      FREQ=C.CDU

```

```

FRQR0001
FRQR0002
FRQR0003
FRQR0004
FRQR0005
FRQR0006
FRQR0007
FRQR0008
FRQR0009
FRQR0010
FRQR0011
FRQR0012
FRQR0013
FRQR0014
FRQR0015
FRQR0016
FRQR0017
FRQR0018
FRQR0019
FRQR0020
FRQR0021
FRQR0022
FRQR0023
FRQR0024
FRQR0025
FRQR0026
FRQR0027
FRQR0028
FRQR0029
FRQR0030
FRQR0031
FRQR0032
FRQR0033
FRQR0034
FRQR0035
FRQR0036

```

144

```

211  FREQ=FREQ+C.0100
      IK=IK+1
      GO TO 511
311  FREQ=FREQ+C.0200
      IK=IK+1
      GO TO 511
611  FREQ=FREQ+C.0500
      IK=IK+1
      GO TO 511
711  FREQ=FREQ+C.100
      IK=IK+1
      GO TO 511
811  FREQ=FREQ+C.500
      IK=IK+1
      GO TO 511
511  DO 100 I=1,L
      DO 100 J=1,L
100  CCMA(I,J)=DCMPLX(DPC(I,J)-FREQ**2* DPA(I,J),FREQ*DPH(I,J))
      DO 301 I=1,L
301  CCMD(I)=DCMPLX( EPC(I),C.CDC)
      CALL GAEL I(CCMA,CCMD,L ,FREQ,IDDF,IFLT)
      IF(IK.LT.10) GO TO 211
      IF(IK.LT.25) GO TO 311
      IF(IK.LT.37) GO TO 611
      IF(IK.LT.57) GO TO 711
      IF(IK.LT.71) GO TO 811
      RETRN
      END

```

```

FRQR0037
FRQR0038
FRQR0039
FRQR0040
FRQR0041
FRQR0042
FRQR0043
FRQR0044
FRQR0045
FRQR0046
FRQR0047
FRQR0048
FRQR0049
FRQR0050
FRQR0051
FRQR0052
FRQR0053
FRQR0054
FRQR0055
FRQR0056
FRQR0057
FRQR0058
FRQR0059
FRQR0060
FRQR0061
FRQR0062
FRQR0063
FRQR0064

```

145

SUBROUTINE GAELI(A,Y,N,FREQ,ICDF,IFLT)

THE GAUSS-JORDAN REDUCTION

COMPLEX*16 / (19,19),Y(19),X(19)

DOUBLE PRECISION FREQ ,CCABS

DIMENSION ARX(19)

COMMON/FRMAG/ FRB(4),FRBC(4),FRW(6),IFRMAG

M=N-1

DO 10 I=1,M

L=I+1

DO 10 J=L,N

IF(CCABS(A(I,J)).EQ.C(0D0))GO TO 10

DO 8 K=L,N

A(J,K)=A(J,K)-A(I,K)+A(J,I)/A(I,I)

CONTINUE

Y(J)=Y(J)-Y(I)*A(J,I)/A(I,I)

CONTINUE

X(N)=Y(N)/A(N,N)

DO 20 I=1,M

K=N-I

L=K+1

DO 20 J=L,N

Y(K)=Y(K)-X(J)*A(K,J)

X(K)=Y(K)/A(K,K)

DO 40 I=1,N

ARX(I)=CCABS(X(I))

IF(IFRMAG.EQ.1) GO TO 50

IF(ICDF.EQ.9) GO TO 51

LT=4

LTT=6

GO TO 54

LT=2

LTT=3

DO 52 I=1,LT

DO 52 J=1,3

GAEL0001

GAEL0002

GAEL0003

GAEL0004

GAEL0005

GAEL0006

GAEL0007

GAEL0008

GAEL0009

GAEL0010

GAEL0011

GAEL0012

GAEL0013

GAEL0014

GAEL0015

GAEL0016

GAEL0017

GAEL0018

GAEL0019

GAEL0020

GAEL0021

GAEL0022

GAEL0023

GAEL0024

GAEL0025

GAEL0026

GAEL0027

GAEL0028

GAEL0029

GAEL0030

GAEL0031

GAEL0032

GAEL0033

GAEL0034

GAEL0035

GAEL0036

```

52  ABX(3*(I-1)+J)=ABX(3*(I-1)+J)*FRB(I)
    DC 55 I=1,LT
55  ABX(3*(I-1)+1)=ABX(3*(I-1)+1)*FRBO(I)/FRB(I)
    DO 53 I=1,LT
53  ABX(I+3*LT)=ABX(I+3*LT)*FRW(I)
50  CONTINUE
    IF (IFLT.EQ.0) GO TO 56
    ABX(N)=FREQ*ABX(N)
56  CONTINUE
    WRITE(6,100) FREQ
100  FORMAT(/3X,'---',F 6.2,'---')
    WRITE(6,200)(ABX(I),I=1,N)
200  FORMAT(/(8X,9(E10.3,2X)/))
    RETURN
    END

```

```

GAEL0037
GAEL0038
GAEL0039
GAEL0040
GAEL0041
GAEL0042
GAEL0043
GAEL0044
GAEL0045
GAEL0046
GAEL0047
GAEL0048
GAEL0049
GAEL0050
GAEL0051

```

SUBROUTINE EIGEN(N,AAA,BBB,CCC,DDD,IDDF)

ROUTINE TO FORM AN EIGENVALUE PROBLEM AND TO CALL EIPACK SUBROUTINE

DIMENSION AAA(19,19),BBB(19,19),CCC(19,19),DDD(19,6)
DIMENSION A(361),L(19),M(19),ATNV(19,19)
DIMENSION AAN(19,19),BBN(19,19),CCN(19,19),DDN(19,6)
REAL*8 AFIG(38,38),WR(38),WI(38),ZP(38,38)
REAL*8 SCALE(38)
INTEGER INT(38)
DIMENSION RIG(25), ARMOD(25,25), DAMP(38)
COMPLEX AMOD(25,25), RIGCOM(25)
COMMON/ERMAG/ FRB(4),FRBD(4),FRW(6),TERMAG
IDEBUG=0
WRITE(6,153)
DO 3003 I=1,N
DO 3004 J=1,N
AAN(I,J)=0.0
BBN(I,J)=0.0
3004 CCN(I,J)=0.0
DO 3005 K=1,6
3005 DDN(I,K)=0.0
3003 CONTINUE
LI=0
DO 1000 J=1,N
DO 1000 I=1,N
LI=LI+1
1000 A(LL)=AAA(I,J)
CALL MINV(A,N,D,L,M)
LI=0
DO 2000 J=1,N
DO 2000 I=1,N
LL=LL+1
2000 ATNV(I,J)=A(LL)
DO 3000 I=1,N
DO 3001 J=1,N

EIGF0001
EIGF0002
EIGF0003
EIGF0004
EIGF0005
EIGF0006
EIGF0007
EIGF0008
EIGF0009
EIGF0010
EIGF0011
EIGF0012
EIGF0013
EIGF0014
EIGF0015
EIGF0016
EIGF0017
EIGF0018
EIGF0019
EIGF0020
EIGF0021
EIGF0022
EIGF0023
EIGF0024
EIGF0025
EIGF0026
EIGF0027
EIGF0028
EIGF0029
EIGF0030
EIGF0031
EIGF0032
EIGF0033
EIGF0034
EIGF0035
EIGF0036

148

	DO 3001 K=1,N	EIGF0037
	AAN(I,J)=AINV(I,K)*AAA(K,J)+AAN(I,J)	EIGF0038
	BRN(I,J)=AINV(I,K)*BBB(K,J)+BRN(I,J)	EIGF0039
3001	CCN(I,J)=AINV(I,K)*CCC(K,J)+CCN(I,J)	EIGF0040
	DO 3002 J=1,6	EIGF0041
	DO 3002 K=1,N	EIGF0042
3002	DDN(I,J)=AINV(I,K)*DDD(K,J)+DDN(I,J)	EIGF0043
3000	CONTINUE	EIGF0044
6000	N2=2*N	EIGF0045
	DO 300 I=1,N	EIGF0046
	DO 300 J=1,N	EIGF0047
	AEIG(I,J)=-BRN(I,J)	EIGF0048
300	AFIG(I,J+N)=-CCN(I,J)	EIGF0049
	DO 301 I=1,N	EIGF0050
	DO 301 J=1,N2	EIGF0051
301	AFIG(I+N,J)=0.000	EIGF0052
	DO 302 I=1,N	EIGF0053
302	AFIG(I+N,I)=1.000	EIGF0054
	CALL EIPACK(38,N2,AEIG,WR,WI,ZP,IERROR,SCALE,INT)	EIGF0055
	IF(IERROR.EQ.0) GO TO 152	EIGF0056
	WRITE(6,150)IERROR	EIGF0057
150	FORMAT(15X,'IERROR=',I5)	EIGF0058
152	CONTINUE	EIGF0059
	IF(IDRBUG.EQ.0) GO TO 61	EIGF0060
	WRITE(6,67)(WR(I),WI(I),I=1,N2)	EIGF0061
67	FORMAT(/10X,D15.7,2X,D15.7)	EIGF0062
	N3=N/3	EIGF0063
	DO 400 IL=1,N3	EIGF0064
	IJ=6*(IL-1)+1	EIGF0065
	KL=6*(IL-1)+6	EIGF0066
400	WRITE(6,251)((ZP(I,J),J=IJ,KL),I=1,N2)	EIGF0067
251	FORMAT(///1X,(/1X,(2D15.7,4X,2D15.7,4X,2D15.7)))	EIGF0068
	IF(3*N3.EQ.N) GO TO 61	EIGF0069
	K=2*(N-3*N3)	EIGF0070
	IJ=KL+1	EIGF0071
	KL=KL+K	EIGF0072

```

751 WRITE(6,751)((ZP(I,J),J=1J,KL),I=1,N2)
61 FORMAT(///1X,(/1X,(2D15,7)))
CONTINUE
DO 140 I=1,N2
XX=SNGL(WR(I)**2+WI(I)**2)
IF(XX.EQ.0.0) GO TO 141
DAMP(I)=-SNGL(WR(I))/SQRT(XX)
GO TO 140
141 DAMP(I)=0.0
140 CONTINUE
NI=N+1
LK=0
LKK=0
NTDT=0
I=1
64 CONTINUE
IF(I.GE.N2+1) GO TO 63
NTDT=NTDT+1
K=NTDT
IF(WI(I).EQ.0.000) GO TO 65
INT(I)=K
INT(I+1)=K
LK=LKK+1
LKK=LK+1
IF(IDRBUG.EQ.0) GO TO 68
WRITE(6,69)I,LK,LKK,K
69 FORMAT(1X,4I5)
68 CONTINUE
DO 50 J=N1,N2
IF(IDRBUG.EQ.0) GO TO 71
WRITE(6,72)ZP(J,LK),ZP(J,LKK)
72 FORMAT(1X,2D15,7)
71 CONTINUE
AMOD(K,J-N1+1)=CMPLX(SNGL(ZP(J,LK)),SNGL(ZP(J,LKK)))
50 CONTINUE
I=I+2

```

```

EIGF0073
EIGF0074
EIGF0075
EIGF0076
EIGF0077
EIGF0078
EIGF0079
EIGF0080
EIGF0081
EIGF0082
EIGF0083
EIGF0084
EIGF0085
EIGF0086
EIGF0087
EIGF0088
EIGF0089
EIGF0090
EIGF0091
EIGF0092
EIGF0093
EIGF0094
EIGF0095
EIGF0096
EIGF0097
EIGF0098
EIGF0099
EIGF0100
EIGF0101
EIGF0102
EIGF0103
EIGF0104
EIGF0105
EIGF0106
EIGF0107
EIGF0108

```

	GO TO 64	EIGF0109
65	CONTINUE	EIGF0110
	INT(I)=K	EIGF0111
	LK=LKK+1	EIGF0112
	LKK=LK	EIGF0113
	IF(IDFRUG.EQ.0) GO TO 73	EIGF0114
	WRITE(6,69)I,LK,LKK,K	EIGF0115
73	CONTINUE	EIGF0116
	DO 66 J=N1,N2	EIGF0117
	IF(IDFRUG.EQ.0) GO TO 74	EIGF0118
	WRITE(6,72)ZP(J,LK),ZP(J,LKK)	EIGF0119
74	CONTINUE	EIGF0120
	AMOD(K, J-N1+1)=CMPLX(SNGL(ZP(J,LK)),0.0)	EIGF0121
66	CONTINUE	EIGF0122
	I=I+1	EIGF0123
	GO TO 64	EIGF0124
63	CONTINUE	EIGF0125
	IF(IFRMAG.EQ.1) GO TO 130	EIGF0126
	IF(IDDF.EQ.9) GO TO 131	EIGF0127
	LT=4	EIGF0128
	LTT=6	EIGF0129
	GO TO 134	EIGF0130
131	LT=2	EIGF0131
	LTT=3	EIGF0132
134	CONTINUE	EIGF0133
	DO 136 IJ=1,NTOT	EIGF0134
	DO 132 I=1,LT	EIGF0135
	DO 132 J=1,3	EIGF0136
132	AMOD(IJ, 3*(I-1)+J)= AMOD(IJ, 3*(I-1)+J)*FRB(I)	EIGF0137
	DO 135 I=1,LT	EIGF0138
135	AMOD(IJ, 3*(I-1)+1)= AMOD(IJ, 3*(I-1)+1)*FRRO(I)/FRB(I)	EIGF0139
	DO 133 I=1,LTT	EIGF0140
133	AMOD(IJ, I+3*LT)=AMOD(IJ, I+3*LT)*FRW(I)	EIGF0141
136	CONTINUE	EIGF0142
130	CONTINUE	EIGF0143
	DO 51 I=1,NTOT	EIGF0144

	DO 51 J=1,N	EIGEO145
51	ARMOD(I,J)=CABS(AMOD(I,J))	EIGEO146
	DO 52 I=1,NTOT	EIGEO147
	BIG(I)=0.0	EIGEO148
	DO 53 J=1,N	EIGEO149
	IF(ABMOD(I,J) - BIG(I)) 53,53,54	EIGEO150
54	BIG(I)=ARMOD(I,J)	EIGEO151
	BIGCOM(I)=AMOD(I,J)	EIGEO152
53	CONTINUE	EIGEO153
52	CONTINUE	EIGEO154
	DO 60 I=1,NTOT	EIGEO155
	DO 60 J=1,N	EIGEO156
	ARMOD(I,J)=ARMOD(I,J)/BIG(I)	EIGEO157
	AMOD(I,J)=AMOD(I,J)/BIGCOM(I)	EIGEO158
60	CONTINUE	EIGEO159
153	FORMAT(///15X,20(1H*)//20X,'EIGENVALUES',//15X, 20(1H*),	EIGEO160
	& ///20X,'** REAL PART **', 3X,'** IMAGINARY PART **')	EIGEO161
	& ,10X,'** DAMPING RATIO **'/)	EIGEO162
	WRITE(6,151)(INT(I),WR(I),WI(I),DAMP(I),I=1,N2)	EIGEO163
151	FORMAT(/ 9X,'NO.',I2,5X,D15.7,5X,D15.7,15X,E15.7)	EIGEO164
	WRITE(6,59)	EIGEO165
59	FORMAT(1H1,///5X, 20 (1H*),//10X, 'EIGENVECTORS',//5X, 20(1H*))	EIGEO166
	IP=0	EIGEO167
	DO 55 I=1,NTOT	EIGEO168
	IP=IP+1	EIGEO169
	WRITE(6,154)I ,WR(IP),WI(IP)	EIGEO170
154	FORMAT(///2X,'-- CORRESPONDING TO NO.',I2,1X,'EIGENVALUE --',	EIGEO171
	& 5X,'(',,D10.3,')+IMAG(',D10.3,')',	EIGEO172
	& ///8X,'** ABSOLUTE VALUE **',20X,'** REAL PART **',2X,	EIGEO173
	& '** IMAGINARY PART **',//)	EIGEO174
	IF((IP+1).GT.N2) GO TO 752	EIGEO175
	IF(INT(IP).EQ.INT(IP+1)) IP=IP+1	EIGEO176
752	CONTINUE	EIGEO177
	DO 56 J=1,N	EIGEO178
	WRITE(6,57)ABMOD(I,J), AMOD(I,J)	EIGEO179
57	FORMAT(10X,E15.7,22X,E15.7,3X,E15.7)	EIGEO180

```
56 CONTINUE
WRITE(6,58)
58 FORMAT(///1X)
55 CONTINUE
RETURN
END
```

```
EIGF0181
EIGF0182
EIGF0183
EIGF0184
EIGF0185
EIGF0186
```

```
SUBROUTINE EIPACK( NM, N, A, WR, WI, Z, IERR, SCALE, INT )
```

```
AN EIGENSYSTEM PROBLEM SOLVER FOR THE GENERAL MATRIX
```

```
REAL*8 A(NM,N),Z(NM,N), WR(N), WI(N), SCALE(N)
INTEGER INT(N)
CALL BALANC(NM,N,A,LOW,IGH,SCALE)
CALL ELMHES(NM,N,LOW,IGH,A,INT)
CALL ELTRAN(NM,N,LOW,IGH,A,INT,Z)
CALL HQR2(NM,N,LOW,IGH,A,WR,WI,Z,IERR)
CALL BALPAK(NM,N,LOW,IGH,SCALE,N,Z)
RETURN
END
```

```
EIPA0001
EIPA0002
EIPA0003
EIPA0004
EIPA0005
EIPA0006
EIPA0007
EIPA0008
EIPA0009
EIPA0010
EIPA0011
EIPA0012
EIPA0013
```


C		69210001
C	-----	69210002
C		69210003
C	SUBROUTINE BALANC(NM,N,A,LOW,IGH,SCALE)	69210004
C		69210005
C	INTEGER I,J,K,L,M,N, JJ,NM,IGH,LOW,IEXC	69210006
C	REAL*8 A(NM,N),SCALE(N)	69210007
C	REAL*8 C,F,G,R,S,B2,RADIX	69210008
C	REAL*8 DABS	69210009
C	LOGICAL NOCONV	69210010
C		69210011
C	THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE BALANCE,	69210012
C	NUM. MATH. 13, 293-304(1969) BY PARLETT AND REINSCH.	69210013
C	HANDBOOK FOR AUTO. COMP., VOL.II-LINEAR ALGEBRA, 315-326(1971).	69210014
C		69210015
C	THIS SUBROUTINE BALANCES A REAL MATRIX AND ISOLATES	69210016
C	EIGENVALUES WHENEVER POSSIBLE.	69210017
C		69210018
C	ON INPUT:	69210019
C		69210020
C	NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL	69210021
C	ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM	69210022
C	DIMENSION STATEMENT;	69210023
C		69210024
C	N IS THE ORDER OF THE MATRIX;	69210025
C		69210026
C	A CONTAINS THE INPUT MATRIX TO BE BALANCED.	69210027
C		69210028
C	ON OUTPUT:	69210029
C		69210030
C	A CONTAINS THE BALANCED MATRIX;	69210031
C		69210032
C	LOW AND IGH ARE TWO INTEGERS SUCH THAT A(I,J)	69210033
C	IS EQUAL TO ZERO IF	69210034
C	(1) I IS GREATER THAN J AND	69210035
C	(2) J=1,...,LOW-I OR I=IGH+1,...,N;	69210036

```

C
C           SCALE CONTAINS INFORMATION DETERMINING THE
C           PERMUTATIONS AND SCALING FACTORS USED.
C
C           SUPPOSE THAT THE PRINCIPAL SUBMATRIX IN ROWS LCW THROUGH IGH
C           HAS BEEN BALANCED, THAT P(J) DENOTES THE INDEX INTERCHANGED
C           WITH J DURING THE PERMUTATION STEP, AND THAT THE ELEMENTS
C           OF THE DIAGONAL MATRIX USED ARE DENOTED BY C(I,J). THEN
C           SCALE(J) = P(J),    FOR J = 1,...,LCW-1
C                       = C(J,J),    J = LCW,...,IGH
C                       = P(J)    J = IGH+1,...,N.
C
C           THE ORDER IN WHICH THE INTERCHANGES ARE MADE IS N TO IGH+1,
C           THEN 1 TO LCW-1.
C
C           NOTE THAT 1 IS RETURNED FOR IGH IF IGH IS ZERO FORMALLY.
C
C           THE ALGOL PROCEDURE EXC CONTAINED IN BALANCE APPEARS IN
C           BALANC IN LINE. (NOTE THAT THE ALGOL ROLES OF IDENTIFIERS
C           K,L HAVE BEEN REVERSED.)
C
C           QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARROW,
C           APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY
C
C           -----
C           ::::::::::: RADIX IS A MACHINE DEPENDENT PARAMETER SPECIFYING
C           THE BASE OF THE MACHINE FLOATING POINT REPRESENTATION.
C           RADIX = 16.C00 FOR LONG FORM ARITHMETIC
C           ON S360 :::::::::::
C           DATA RADIX/Z421CCCCC0CCCC0CC0/
C
C           B2 = RADIX * RADIX
C           K = 1
C           L = N
C           GO TO 100
C           ::::::::::: IN-LINE PROCEDURE FOR ROW AND

```

```

69210037
69210038
69210039
69210040
69210041
69210042
69210043
69210044
69210045
69210046
69210047
69210048
69210049
69210050
69210051
69210052
69210053
69210054
69210055
69210056
69210057
69210058
69210059
69210060
69210061
69210062
69210063
69210064
69210065
69210066
69210067
69210068
69210069
69210070
69210071
69210072

```

C	COLLUM EXCHANGE ::::::::::	69210073
	20 SCALE(M) = J	69210074
	IF (J .EQ. M) GC TC 50	69210075
C		69210076
	DC 30 I = 1, L	69210077
	F = A(I,J)	69210078
	A(I,J) = A(I,M)	69210079
	A(I,M) = F	69210080
	30 CONTINUE	69210081
C		69210082
	DC 40 I = K, N	69210083
	F = A(J,I)	69210084
	A(J,I) = A(M,I)	69210085
	A(M,I) = F	69210086
	40 CONTINUE	69210087
C		69210088
	50 GC TC (80,130), IEXC	69210089
C	::::::::: SEARCH FOR ROWS ISOLATING AN EIGENVALLE	69210090
C	AND PUSH THEM DOWN :::::::::::	69210091
	80 IF (L .EQ. 1) GC TC 280	69210092
	L = L - 1	69210093
C	::::::::: FOR J=L STEP -1 UNTIL 1 DO -- :::::::::::	69210094
	100 DC 120 JJ = 1, L	69210095
	J = L + 1 - JJ	69210096
C		69210097
	DC 110 I = 1, L	69210098
	IF (I .EQ. J) GC TC 110	69210099
	IF (A(J,I) .NE. C.CDC) GC TC 120	69210100
	110 CONTINUE	69210101
C		69210102
	M = L	69210103
	IEXC = 1	69210104
	GC TC 20	69210105
	120 CONTINUE	69210106
C		69210107
	GC TC 140	69210108

C	::: SEARCH FOR COLUMNS ISOLATING AN EIGENVALUE	69210109
C	AND PUSH THEM LEFT :::	69210110
	130 K = K + 1	69210111
C		69210112
	140 DO 170 J = K, L	69210113
C		69210114
	DO 150 I = K, L	69210115
	IF (I .EQ. J) GO TO 150	69210116
	IF (A(I,J) .NE. 0.000) GO TO 170	69210117
	150 CONTINUE	69210118
C		69210119
	M = K	69210120
	IEXC = 2	69210121
	GO TO 20	69210122
	170 CONTINUE	69210123
C	::: NOW BALANCE THE SUBMATRIX IN ROWS K TO L :::	69210124
	DO 180 I = K, L	69210125
	180 SCALE(I) = 1.000	69210126
C	::: ITERATIVE LOOP FOR NORM REDUCTION :::	69210127
	190 NOCONV = .FALSE.	69210128
C		69210129
	DO 270 I = K, L	69210130
	C = 0.000	69210131
	R = 0.000	69210132
C		69210133
	DO 200 J = K, L	69210134
	IF (J .EQ. I) GO TO 200	69210135
	C = C + CABS(A(J,I))	69210136
	R = R + CABS(A(I,J))	69210137
	200 CONTINUE	69210138
C		69210139
	G = R / RADIX	69210140
	F = 1.000	69210141
	S = C + R	69210142
	210 IF (C .GE. G) GO TO 220	69210143
	F = F * RADIX	69210144

	C = C * P2	69210145
	GC TC 210	69210146
220	G = R * RADIX	69210147
230	IF (C .LT. G) GC TC 240	69210148
	F = F / RADIX	69210149
	C = C / P2	69210150
	GC TC 230	69210151
C	:::::::::: NOW BALANCE ::::::::::	69210152
240	IF ((C + R) / F .GE. 0.9500 * S) GC TC 270	69210153
	G = 1.000 / F	69210154
	SCALE(I) = SCALE(I) * F	69210155
	ACCENV = .TRUE.	69210156
C		69210157
	CC 250 J = K, N	69210158
250	A(I,J) = A(I,J) * G	69210159
C		69210160
	CC 260 J = 1, L	69210161
260	A(J,I) = A(J,I) * F	69210162
C		69210163
270	CONTINUE	69210164
C		69210165
	IF (ACCENV) GC TC 190	69210166
C		69210167
280	LOW = K	69210168
	IGH = L	69210169
	RETURN	69210170
C	:::::::::: LAST CARD OF BALANC ::::::::::	69210171
	END	69210172

C		73210001
C	-----	73210002
C		73210003
C	SUBROUTINE ELMHES(NP,N,LOW,IGH,A,INT)	73210004
C		73210005
C	INTEGER I,J,M,N,LA,NM,IGH,KP1,LOW,MPI,MPI	73210006
C	REAL*8 A(NP,N)	73210007
C	REAL*8 X,Y	73210008
C	REAL*8 DABS	73210009
C	INTEGER INT(IGH)	73210010
C		73210011
C	THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE ELMHES,	73210012
C	NUM. MATH. 12, 349-368(1968) BY MARTIN AND WILKINSON.	73210013
C	HANDBOOK FOR AUT. COMP., VOL.II-LINEAR ALGEBRA, 339-358(1971).	73210014
C		73210015
C	GIVEN A REAL GENERAL MATRIX, THIS SUBROUTINE	73210016
C	REDUCES A SUBMATRIX SITUATED IN ROWS AND COLUMNS	73210017
C	LOW THROUGH IGH TO UPPER HESSENBERG FORM BY	73210018
C	STABILIZED ELEMENTARY SIMILARITY TRANSFORMATIONS.	73210019
C		73210020
C	ON INPUT:	73210021
C		73210022
C	NP MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL	73210023
C	ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM	73210024
C	DIMENSION STATEMENT;	73210025
C		73210026
C	N IS THE ORDER OF THE MATRIX;	73210027
C		73210028
C	LOW AND IGH ARE INTEGERS DETERMINED BY THE BALANCING	73210029
C	SUBROUTINE BALANC. IF BALANC HAS NOT BEEN USED,	73210030
C	SET LOW=1, IGH=N;	73210031
C		73210032
C	A CONTAINS THE INPUT MATRIX.	73210033
C		73210034
C	ON OUTPUT:	73210035
C		73210036

C	A CONTAINS THE HESSENBERG MATRIX. THE MULTIPLIERS	73210037
C	WHICH WERE USED IN THE REDUCTION ARE STORED IN THE	73210038
C	REMAINING TRIANGLE UNDER THE HESSENBERG MATRIX;	73210039
C		73210040
C	INT CONTAINS INFORMATION ON THE ROWS AND COLUMNS	73210041
C	INTERCHANGED IN THE REDUCTION.	73210042
C	ONLY ELEMENTS LOW THROUGH IGH ARE USED.	73210043
C		73210044
C	QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBCW,	73210045
C	APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY	73210046
C		73210047
C	-----	73210048
C		73210049
C	LA = IGH - 1	73210050
C	KPI = LOW + 1	73210051
C	IF (LA .LT. KPI) GO TO 200	73210052
C		73210053
C	DC 180 M = KPI, LA	73210054
C	MM1 = M - 1	73210055
C	X = C.OOO	73210056
C	I = M	73210057
C		73210058
C	DC 100 J = M, IGH	73210059
C	IF (DABS(A(J,MM1)) .LE. DABS(X)) GO TO 100	73210060
C	X = A(J,MM1)	73210061
C	I = J	73210062
C	100 CONTINUE	73210063
C		73210064
C	INT(M) = I	73210065
C	IF (I .EQ. M) GO TO 130	73210066
C	:::::::::: INTERCHANGE ROWS AND COLUMNS OF A ::::::::::::	73210067
C	DC 110 J = MM1, M	73210068
C	Y = A(I,J)	73210069
C	A(I,J) = A(M,J)	73210070
C	A(M,J) = Y	73210071
C	110 CONTINUE	73210072

C	DC 120 J = 1, IGH	73210073
	Y = A(J,I)	73210074
	A(J,I) = A(J,M)	73210075
	A(J,M) = Y	73210076
120	CONTINUE	73210077
C	::::::::::::: END INTERCHANGE ::::::::::::::	73210078
130	IF (X .EQ. C.CDC) GO TO 180	73210079
	MP1 = M + 1	73210080
C		73210081
	DC 160 I = MP1, IGH	73210082
	Y = A(I,MP1)	73210083
	IF (Y .EQ. C.CDC) GO TO 160	73210084
	Y = Y / X	73210085
	A(I,MP1) = Y	73210086
C		73210087
	DC 140 J = M, N	73210088
140	A(I,J) = A(I,J) - Y * A(M,J)	73210089
C		73210090
	DC 150 J = 1, IGH	73210091
150	A(J,M) = A(J,M) + Y * A(J,I)	73210092
C		73210093
160	CONTINUE	73210094
C		73210095
180	CONTINUE	73210096
C		73210097
200	RETURN	73210098
C	::::::::::::: LAST CARD OF ELMFES ::::::::::::::	73210099
	END	73210100
		73210101

C		20210001
C	-----	20210002
C		20210003
C	SUBROUTINE ELTRAN(NM,N,LCW,IGH,A,INT,Z)	20210004
C		20210005
C	INTEGER I,J,N,KL,PM,PP,NM,IGH,LOW,MP1	20210006
C	REAL*8 A(NM,IGH),Z(NM,N)	20210007
C	INTEGER INT(IGH)	20210008
C		20210009
C	THIS SUBROUTINE IS A TRANSLATION OF THE ALGCL PROCEDURE ELMTRANS,	20210010
C	NUM. MATH. 16, 181-204(1970) BY PETERS AND WILKINSON.	20210011
C	HANDBOOK FOR AUTO. COMP., VOL.II-LINEAR ALGEBRA, 372-395(1971).	20210012
C		20210013
C	THIS SUBROUTINE ACCUMULATES THE STABILIZED ELEMENTARY	20210014
C	SIMILARITY TRANSFORMATIONS USED IN THE REDUCTION OF A	20210015
C	REAL GENERAL MATRIX TO UPPER HESSENBERG FORM BY ELMHES.	20210016
C		20210017
C	ON INPUT:	20210018
C		20210019
C	NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL	20210020
C	ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM	20210021
C	DIMENSION STATEMENT;	20210022
C		20210023
C	N IS THE ORDER OF THE MATRIX;	20210024
C		20210025
C	LOW AND IGH ARE INTEGERS DETERMINED BY THE BALANCING	20210026
C	SUBROUTINE BALANC. IF BALANC HAS NOT BEEN USED,	20210027
C	SET LOW=1, IGH=N;	20210028
C		20210029
C	A CONTAINS THE MULTIPLIERS WHICH WERE USED IN THE	20210030
C	REDUCTION BY ELMHES IN ITS LOWER TRIANGLE	20210031
C	BELOW THE SUBDIAGONAL;	20210032
C		20210033
C	INT CONTAINS INFORMATION ON THE ROWS AND COLUMNS	20210034
C	INTERCHANGED IN THE REDUCTION BY ELMHES.	20210035
C	ONLY ELEMENTS LOW THROUGH IGH ARE USED.	20210036

C		20210037
C	ON CLTPUT:	20210038
C		20210039
C	Z CONTAINS THE TRANSFORMATION MATRIX PRODUCED IN THE	20210040
C	REDUCTION BY ELPFES.	20210041
C		20210042
C	QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBCW,	20210043
C	APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABCRATCRY	20210044
C		20210045
C	-----	20210046
C		20210047
C	::::::::::: INITIALIZE Z TO IDENTITY MATRIX :::::::::::	20210048
C	DO 80 I = 1, N	20210049
C		20210050
C	DO 60 J = 1, N	20210051
C	60 Z(I,J) = 0.000	20210052
C		20210053
C	Z(I,I) = 1.000	20210054
C	80 CONTINUE	20210055
C		20210056
C	KL = IGH - LOW - 1	20210057
C	IF (KL .LT. 1) GO TO 200	20210058
C	::::::::::: FOR MP=IGH-1 STEP -1 UNTIL LOW+1 DO -- :::::::::::	20210059
C	DO 140 MM = 1, KL	20210060
C	MP = IGH - MM	20210061
C	MP1 = MP + 1	20210062
C		20210063
C	DO 100 I = MP1, IGH	20210064
C	100 Z(I,MP) = A(I,MP-1)	20210065
C		20210066
C	I = INT(MP)	20210067
C	IF (I .EQ. MP) GO TO 140	20210068
C		20210069
C	DO 130 J = MP, IGH	20210070
C	Z(MP,J) = Z(I,J)	20210071
C	Z(I,J) = 0.000	20210072

130 CONTINUE
C
Z(I,MP) = 1.000
140 CONTINUE
C
200 RETURN
C
:::::::::: LAST CARD OF ELTRAN ::::::::::::
END

20210073
20210074
20210075
20210076
20210077
20210078
20210079
20210080

C		87210001
C	-----	87210002
C		87210003
C	SUBROUTINE HQR2(NM,N,LCW,ICF,F,WR,WI,Z,IERR)	87210004
C		87210005
	INTEGER I,J,K,L,M,N,EN,II,JJ,LL,MM,NA,NM,NN,	87210006
X	ICF,ITS,LCW,MP2,ENM2,IERR	87210007
	REAL*8 F(NM,N),WR(N),WI(N),Z(NM,N)	87210008
	REAL*8 P,Q,R,S,T,h,X,Y,RA,SA,VI,VR,ZZ,NCRM,MACHEP	87210009
	REAL*8 CSCRT,CABS,CSIGN	87210010
	INTEGER MINC	87210011
	LOGICAL MCTLAS	87210012
	COMPLEX*16 Z3	87210013
	COMPLEX*16 DCMPLX	87210014
	REAL*8 T3(2)	87210015
	EQUIVALENCE (Z3,T3(1))	87210016
C		87210017
C	THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE HQR2,	87210018
C	NUM. MATH. 16, 181-204(1970) BY PETERS AND WILKINSON.	87210019
C	HANDBOOK FOR ALGOL COMP., VOL.II-LINEAR ALGEBRA, 372-395(1971).	87210020
C		87210021
C	THIS SUBROUTINE FINDS THE EIGENVALUES AND EIGENVECTORS	87210022
C	OF A REAL UPPER HESSENBERG MATRIX BY THE QR METHOD. THE	87210023
C	EIGENVECTORS OF A REAL GENERAL MATRIX CAN ALSO BE FOUND	87210024
C	IF ELMHES AND ELTRAN OR CRTHES AND CRTRAN HAVE	87210025
C	BEEN USED TO REDUCE THIS GENERAL MATRIX TO HESSENBERG FORM	87210026
C	AND TO ACCUMULATE THE SIMILARITY TRANSFORMATIONS.	87210027
C		87210028
C	ON INPUT:	87210029
C		87210030
C	NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL	87210031
C	ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM	87210032
C	DIMENSION STATEMENT;	87210033
C		87210034
C	N IS THE ORDER OF THE MATRIX;	87210035
C		87210036

C	LOW AND IGH ARE INTEGERS DETERMINED BY THE BALANCING	87210037
C	SUBROUTINE BALANC. IF BALANC HAS NOT BEEN USED,	87210038
C	SET LOW=1, IGH=N;	87210039
C		87210040
C	F CONTAINS THE UPPER HESSENBERG MATRIX;	87210041
C		87210042
C	Z CONTAINS THE TRANSFORMATION MATRIX PRODUCED BY ELTRAN	87210043
C	AFTER THE REDUCTION BY ELMHES, OR BY CRTRAN AFTER THE	87210044
C	REDUCTION BY CRTRES, IF PERFORMED. IF THE EIGENVECTORS	87210045
C	OF THE HESSENBERG MATRIX ARE DESIRED, Z MUST CONTAIN THE	87210046
C	IDENTITY MATRIX.	87210047
C		87210048
C	ON OUTPUT:	87210049
C		87210050
C	F HAS BEEN DESTROYED;	87210051
C		87210052
C	WR AND WI CONTAIN THE REAL AND IMAGINARY PARTS,	87210053
C	RESPECTIVELY, OF THE EIGENVALUES. THE EIGENVALUES	87210054
C	ARE UNORDERED EXCEPT THAT COMPLEX CONJUGATE PAIRS	87210055
C	OF VALUES APPEAR CONSECUTIVELY WITH THE EIGENVALUE	87210056
C	HAVING THE POSITIVE IMAGINARY PART FIRST. IF AN	87210057
C	ERROR EXIT IS MADE, THE EIGENVALUES SHOULD BE CORRECT	87210058
C	FOR INDICES IERR+1,....,N;	87210059
C		87210060
C	Z CONTAINS THE REAL AND IMAGINARY PARTS OF THE EIGENVECTORS.	87210061
C	IF THE I-TH EIGENVALUE IS REAL, THE I-TH COLUMN OF Z	87210062
C	CONTAINS ITS EIGENVECTOR. IF THE I-TH EIGENVALUE IS COMPLEX	87210063
C	WITH POSITIVE IMAGINARY PART, THE I-TH AND (I+1)-TH	87210064
C	COLUMNS OF Z CONTAIN THE REAL AND IMAGINARY PARTS OF ITS	87210065
C	EIGENVECTOR. THE EIGENVECTORS ARE UNNORMALIZED. IF AN	87210066
C	ERROR EXIT IS MADE, NONE OF THE EIGENVECTORS HAS BEEN FOUND;	87210067
C		87210068
C	IERR IS SET TO	87210069
C	ZERO FOR NORMAL RETURN,	87210070
C	J IF THE J-TH EIGENVALUE HAS NOT BEEN	87210071
C	DETERMINED AFTER 30 ITERATIONS.	87210072

C		87210073
C	ARITHMETIC IS REAL EXCEPT FOR THE REPLACEMENT OF THE ALGCL	87210074
C	PROCEDURE CDIV BY COMPLEX DIVISION.	87210075
C		87210076
C	QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBCW,	87210077
C	APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY	87210078
C		87210079
C	-----	87210080
C		87210081
C	:::~::~: MACHEP IS A MACHINE DEPENDENT PARAMETER SPECIFYING	87210082
C	THE RELATIVE PRECISION OF FLOATING POINT ARITHMETIC.	87210083
C	MACHEP = 16.000**(-13) FOR LONG FORM ARITHMETIC	87210084
C	CN S360 :::~::~:	87210085
C	DATA MACHEP/Z341CCCCCCCCCCCCO/	87210086
C		87210087
C	IEPR = C	87210088
C	:::~::~: STORE ROOTS ISOLATED BY BALANC :::~::~:	87210089
C	DC 50 I = 1, N	87210090
	IF (I .GE. LCW .AND. I .LE. IGH) GO TO 50	87210091
	WR(I) = P(I,I)	87210092
	WI(I) = C.CCC	87210093
	50 CONTINUE	87210094
C		87210095
	EN = IGH	87210096
	T = C.CCC	87210097
C	:::~::~: SEARCH FOR NEXT EIGENVALUES :::~::~:	87210098
	60 IF (EN .LT. LCW) GO TO 340	87210099
	ITS = C	87210100
	NA = EN - 1	87210101
	ENM2 = NA - 1	87210102
C	:::~::~: LOCK FOR SINGLE SMALL SUB-DIAGONAL ELEMENT	87210103
C	FOR L=EN STEP -1 UNTIL LCW DO -- :::~::~:	87210104
	70 DO 80 LL = LCW, EN	87210105
	L = EN + LCW - LL	87210106
	IF (L .EQ. LCW) GO TO 100	87210107
	IF (DABS(H(L,L-1)) .LE. MACHEP * (DABS(H(L-1,L-1)))	87210108

	X = CABS(F(L,L))) GC TC 100	87210109
	PO CONTINUE	87210110
C	::::::::::: FORM SHIFT :::::::::::	87210111
	100 X = F(EN,EN)	87210112
	IF (L .EQ. EN) GC TC 270	87210113
	Y = H(NA,NA)	87210114
	W = F(EN,NA) * F(NA,EN)	87210115
	IF (L .EQ. NA) GC TO 280	87210116
	IF (ITS .EQ. 30) GC TC 1000	87210117
	IF (ITS .NE. 10 .AND. ITS .NE. 20) GC TC 130	87210118
C	::::::::::: FORM EXCEPTIONAL SHIFT :::::::::::	87210119
	T = T + X	87210120
C		87210121
	DO 120 I = LOW, EN	87210122
	120 H(I,I) = F(I,I) - X	87210123
C		87210124
	S = CABS(H(EN,NA)) + CABS(F(NA,ENM2))	87210125
	X = C.7500 * S	87210126
	Y = X	87210127
	W = -C.437500 * S * S	87210128
	130 ITS = ITS + 1	87210129
C	::::::::::: LOCK FOR TWO CONSECUTIVE SMALL	87210130
C	SUB-DIAGONAL ELEMENTS.	87210131
C	FOR M=EN-2 STEP -1 UNTIL L DO -- :::::::::::	87210132
	DO 140 MM = L, ENM2	87210133
	M = ENM2 + L - MM	87210134
	ZZ = H(M,M)	87210135
	R = X - ZZ	87210136
	S = Y - ZZ	87210137
	P = (R * S - W) / F(M+1,M) + F(M,M+1)	87210138
	Q = H(M+1,M+1) - ZZ - R - S	87210139
	R = H(M+2,M+1)	87210140
	S = CABS(P) + CABS(Q) + CABS(R)	87210141
	P = P / S	87210142
	Q = Q / S	87210143
	R = R / S	87210144

	IF (M .EQ. L) GO TO 150	87210145
	IF (DABS(H(N,M-1)) * (DABS(G) + DABS(R)) .LE. MACHEP * DABS(P)	87210146
X	* (DABS(H(N-1,M-1)) + DABS(ZZ) + DABS(F(N+1,M+1)))) GO TO 150	87210147
140	CONTINUE	87210148
C		87210149
150	MP2 = M + 2	87210150
C		87210151
	DO 160 I = MP2, EN	87210152
	F(I,I-2) = C.CDC	87210153
	IF (I .EQ. MP2) GO TO 160	87210154
	F(I,I-3) = C.CDC	87210155
160	CONTINUE	87210156
C	:::~::~: DOUBLE QR STEP INVOLVING ROWS L TO EN AND	87210157
C	COLUMNS M TO EN :::~::~:	87210158
	DO 260 K = M, NA	87210159
	NCTLAS = K .NE. NA	87210160
	IF (K .EQ. M) GO TO 170	87210161
	P = F(K,K-1)	87210162
	G = F(K+1,K-1)	87210163
	R = C.CDC	87210164
	IF (NCTLAS) R = F(K+2,K-1)	87210165
	X = DABS(P) + DABS(G) + DABS(R)	87210166
	IF (X .EQ. C.CDC) GO TO 260	87210167
	P = P / X	87210168
	G = G / X	87210169
	R = R / X	87210170
170	S = DSIGN(DSQRT(P*P+G*G+R*R),P)	87210171
	IF (K .EQ. M) GO TO 180	87210172
	H(K,K-1) = -S * X	87210173
	GO TO 190	87210174
180	IF (L .NE. M) F(K,K-1) = -F(K,K-1)	87210175
190	P = P + S	87210176
	X = P / S	87210177
	Y = G / S	87210178
	ZZ = R / S	87210179
	G = G / P	87210180

	R = R / P	87210181
C	:::~::~: ROW MODIFICATION :::~::~:	87210182
	CC 210 J = K, N	87210183
	P = H(K,J) + C * H(K+1,J)	87210184
	IF (.NOT. NCTLAS) GO TO 200	87210185
	P = P + R * F(K+2,J)	87210186
	F(K+2,J) = H(K+2,J) - P * Z	87210187
200	F(K+1,J) = H(K+1,J) - P * Y	87210188
	F(K,J) = F(K,J) - P * X	87210189
210	CONTINUE	87210190
C		87210191
	J = MINO(EN,K+3)	87210192
C	:::~::~: COLUMN MODIFICATION :::~::~:	87210193
	CC 220 I = 1, J	87210194
	P = X * F(I,K) + Y * F(I,K+1)	87210195
	IF (.NOT. NCTLAS) GO TO 220	87210196
	P = P + Z * H(I,K+2)	87210197
	F(I,K+2) = H(I,K+2) - P * R	87210198
220	F(I,K+1) = F(I,K+1) - P * Q	87210199
	F(I,K) = F(I,K) - P	87210200
230	CONTINUE	87210201
C	:::~::~: ACCUMULATE TRANSFORMATIONS :::~::~:	87210202
	CC 250 I = LCW, IGT	87210203
	P = X * Z(I,K) + Y * Z(I,K+1)	87210204
	IF (.NOT. NCTLAS) GO TO 240	87210205
	P = P + Z * Z(I,K+2)	87210206
	Z(I,K+2) = Z(I,K+2) - P * R	87210207
240	Z(I,K+1) = Z(I,K+1) - P * C	87210208
	Z(I,K) = Z(I,K) - P	87210209
250	CONTINUE	87210210
C		87210211
260	CONTINUE	87210212
C		87210213
	GO TO 70	87210214
C	:::~::~: ONE RECT FCLND :::~::~:	87210215
270	F(EN,EN) = X + T	87210216

	WR(EN) = H(EN,EN)	87210217
	WI(EN) = C.CDC	87210218
	EN = NA	87210219
	GC TC 60	87210220
C	:::~::~: TWC ROOTS FOUND :::~::~:	87210221
280	P = (Y - X) / Z.CDC	87210222
	G = P * P + W	87210223
	ZZ = DSQRT(DABS(G))	87210224
	F(EN,EN) = X + T	87210225
	X = F(EN,EN)	87210226
	H(NA,NA) = Y + T	87210227
	IF (G .LT. C.CDC) GC TC 32C	87210228
C	:::~::~: REAL PAIR :::~::~:	87210229
	ZZ = P + ESIGN(ZZ,P)	87210230
	WR(NA) = X + ZZ	87210231
	WR(EN) = WR(NA)	87210232
	IF (ZZ .NE. 0.CDC) WR(EN) = X - W / ZZ	87210233
	WI(NA) = C.CDC	87210234
	WI(EN) = C.CDC	87210235
	X = F(EN,NA)	87210236
	R = ESQRT(X*X+ZZ*ZZ)	87210237
	P = X / R	87210238
	Q = ZZ / R	87210239
C	:::~::~: ROW MODIFICATION :::~::~:	87210240
	CC 290 J = NA, N	87210241
	ZZ = H(NA,J)	87210242
	F(NA,J) = Q * ZZ + P * H(EN,J)	87210243
	F(EN,J) = Q * F(EN,J) - P * ZZ	87210244
290	CONTINUE	87210245
C	:::~::~: COLUMN MODIFICATION :::~::~:	87210246
	CC 300 I = 1, EN	87210247
	ZZ = F(I,NA)	87210248
	F(I,NA) = C * ZZ + P * F(I,EN)	87210249
	F(I,EN) = C * F(I,EN) - P * ZZ	87210250
300	CONTINUE	87210251
C	:::~::~: ACCUMULATE TRANSFORMATIONS :::~::~:	87210252

	DC 310 I = LCH, IGH	87210253
	ZZ = Z(I,NA)	87210254
	Z(I,NA) = C * ZZ + P * Z(I,EN)	87210255
	Z(I,EN) = C * Z(I,EN) - P * ZZ	87210256
	310 CONTINUE	87210257
C		87210258
	GC TC 330	87210259
C	:::::::::: COMPLEX PAIR ::::::::::	87210260
320	WR(NA) = X + P	87210261
	WR(EN) = X + P	87210262
	WI(NA) = ZZ	87210263
	WI(EN) = -ZZ	87210264
330	EN = ENM2	87210265
	GC TC 60	87210266
C	:::::::::: ALL ROOTS FOUND. BACKSUBSTITUTE TO FIND	87210267
C	VECTORS OF UPPER TRIANGULAR FORM ::::::::::	87210268
340	NORM = 0.000	87210269
	K = 1	87210270
C		87210271
	DC 360 I = 1, N	87210272
C		87210273
	DC 350 J = K, N	87210274
350	NORM = NORM + DABS(H(I,J))	87210275
C		87210276
	K = I	87210277
360	CONTINUE	87210278
C		87210279
	IF (NORM .EQ. 0.000) GC TO 1000	87210280
C	:::::::::: FOR EN=N STEP -1 UNTIL 1 DO -- ::::::::::	87210281
	DC 800 NN = 1, N	87210282
	EN = N + 1 - NN	87210283
	P = WR(EN)	87210284
	C = WI(EN)	87210285
	NA = EN - 1	87210286
	IF (C) 710, 600, 800	87210287
C	:::::::::: REAL VECTOR ::::::::::	87210288

600	N = EN	87210289
	F(EN,EN) = 1.000	87210290
	IF (NA .EQ. C) GC TO 800	87210291
C	:::::::::: FOR I=EN-1 STEP -1 UNTIL 1 DO -- ::::::::::	87210292
	GC 700 II = 1, NA	87210293
	I = EN - II	87210294
	W = H(I,I) - P	87210295
	R = H(I,EN)	87210296
	IF (M .GT. NA) GC TO 620	87210297
C		87210298
	GC 610 J = M, NA	87210299
610	R = R + F(I,J) * H(J,EN)	87210300
C		87210301
620	IF (W1(I) .GE. C.000) GC TO 630	87210302
	ZZ = W	87210303
	S = R	87210304
	GC TO 700	87210305
630	M = I	87210306
	IF (W1(I) .NE. C.000) GC TO 640	87210307
	T = W	87210308
	IF (W .EG. C.000) T = MACHEP * NORM	87210309
	F(I,EN) = -R / T	87210310
	GC TO 700	87210311
C	:::::::::: SOLVE REAL EQUATIONS ::::::::::	87210312
640	X = H(I,I+1)	87210313
	Y = F(I+1,I)	87210314
	G = (WR(I) - P) * (WP(I) - P) + W1(I) * W1(I)	87210315
	T = (X * S - ZZ * R) / G	87210316
	F(I,EN) = T	87210317
	IF (DABS(X) .LE. DABS(ZZ)) GO TO 650	87210318
	F(I+1,EN) = (-R - W * T) / X	87210319
	GC TO 700	87210320
650	F(I+1,EN) = (-S - Y * T) / ZZ	87210321
700	CONTINUE	87210322
C	:::::::::: END REAL VECTOR ::::::::::	87210323
	GC TO 800	87210324

C	***** COMPLEX VECTOR *****	87210325
710	M = NA	87210326
C	***** LAST VECTOR COMPONENT CHOSEN IMAGINARY SO THAT	87210327
C	EIGENVECTOR MATRIX IS TRIANGULAR *****	87210328
	IF (DABS(H(EN,NA)) .LE. DABS(H(NA,EN))) GO TO 720	87210329
	F(NA,NA) = C / H(EN,NA)	87210330
	F(NA,EN) = -(F(EN,EN) - P) / F(EN,NA)	87210331
	GO TO 730	87210332
720	Z3 = DCOMPLX(C.CDC,-H(NA,EN)) / DCOMPLX(H(NA,NA)-P,C)	87210333
	F(NA,NA) = T3(1)	87210334
	F(NA,EN) = T3(2)	87210335
730	H(EN,NA) = C.CDC	87210336
	F(EN,EN) = 1.CDC	87210337
	ENM2 = NA - 1	87210338
	IF (ENM2 .EQ. C) GO TO 800	87210339
C		87210340
	CC 790 II = 1, ENM2	87210341
	I = NA - II	87210342
	W = H(I,I) - P	87210343
	RA = C.CDC	87210344
	SA = F(I,EN)	87210345
C		87210346
	CC 760 J = M, NA	87210347
	RA = RA + H(I,J) * H(J,NA)	87210348
	SA = SA + H(I,J) * H(J,EN)	87210349
760	CONTINUE	87210350
C		87210351
	IF (WI(I) .GE. C.CDC) GO TO 770	87210352
	ZZ = W	87210353
	R = RA	87210354
	S = SA	87210355
	GO TO 790	97210356
770	M = I	87210357
	IF (WI(I) .NE. C.CDC) GO TO 780	87210358
	Z3 = DCOMPLX(-RA,-SA) / DCOMPLX(W,C)	87210359
	F(I,NA) = T3(1)	87210360

```

      F(I,EN) = T3(2)
      GC TO 79C
C      :::::::::: SOLVE COMPLEX EQUATIONS ::::::::::
780    X = H(I,I+1)
      Y = H(I+1,I)
      VR = (WR(I) - P) * (WR(I) - P) + 5.0 * I(I) * WI(I) - C * C
      VI = (WR(I) - P) * 2.000 * C
      IF (VR .EQ. 0.000 .AND. VI .EQ. 0.000) VR = RACREP * NCRM
      * (DABS(W) + DABS(Q) + DABS(X) + DABS(Y) + DABS(ZZ))
      Z3 = DCMPLEX(X*R-ZZ*RA+Q*SA,X*S-ZZ*SA-C*RA) / DCMPLEX(VR,VI)
      F(I,NA) = T3(1)
      F(I,EN) = T3(2)
      IF (DABS(X) .LE. DABS(ZZ) + DABS(Q)) GC TO 785
      F(I+1,NA) = (-R0 - W * F(I,NA) + C * F(I,EN)) / X
      F(I+1,EN) = (-SA - W * H(I,EN) - C * F(I,NA)) / X
      GC TO 79C
785    Z3 = DCMPLEX(-R-Y*F(I,NA),-S-Y*F(I,EN)) / DCMPLEX(ZZ,Q)
      F(I+1,NA) = T3(1)
      F(I+1,EN) = T3(2)
790    CONTINUE
C      :::::::::: END COMPLEX VECTOR ::::::::::
800    CONTINUE
C      :::::::::: END BACK SUBSTITUTION.
C      VECTORS OF ISOLATED ROOTS ::::::::::
      DC 840 I = 1, N
      IF (I .GE. LCW .AND. I .LE. IGF) GC TO 84C
C
      DC 82C J = 1, N
820    Z(I,J) = H(I,J)
C
840    CONTINUE
C      :::::::::: MULTIPLY BY TRANSFORMATION MATRIX TO GIVE
C      VECTORS OF ORIGINAL FULL MATRIX.
C      FOR J=N STEP -1 UNTIL LCW DO -- ::::::::::
      DO 88C JJ = LCW, N
      J = N + LCW - JJ

```

87210361
87210362
87210363
87210364
87210365
87210366
87210367
87210368
87210369
87210370
87210371
87210372
87210373
87210374
87210375
87210376
87210377
87210378
87210379
87210380
87210381
87210382
87210383
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87210385
87210386
87210387
87210388
87210389
87210390
87210391
87210392
87210393
87210394
87210395
87210396

	M = MINO(IJ, IGH)	87210397
C		87210398
	DO 860 I = LCN, IGH	87210399
	ZZ = 0.000	87210400
C		87210401
	DO 860 K = LCN, M	87210402
860	ZZ = ZZ + Z(I,K) * H(K,J)	87210403
C		87210404
	Z(I,J) = ZZ	87210405
880	CONTINUE	87210406
C		87210407
	GO TO 1001	87210408
C	:::::::::: SET ERROR -- NO CONVERGENCE TO AN	87210409
C	EIGENVALUE AFTER 30 ITERATIONS ::::::::::	87210410
	1000 IERR = FN	87210411
	1001 RETURN	87210412
C	:::::::::: LAST CARD OF HQR2 ::::::::::	87210413
	END	87210414

C		70210001
C	-----	70210002
C		70210003
C	SUBROUTINE BALPAK(NM,N,LCW,IGH,SCALE,M,Z)	70210004
C		70210005
	INTEGER I,J,K,M,N,II,NM,IGH,LOW	70210006
	REAL*8 SCALE(N),Z(NM,M)	70210007
	REAL*8 S	70210008
C		70210009
C	THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE BALBAK,	70210010
C	NUM. MATH. 13, 293-304(1969) BY PARLETT AND REINSCH.	70210011
C	HANDBOOK FOR ALGOL COMP., VOL.II-LINEAR ALGEBRA, 315-326(1971).	70210012
C		70210013
C	THIS SUBROUTINE FORMS THE EIGENVECTORS OF A REAL GENERAL	70210014
C	MATRIX BY BACK TRANSFORMING THOSE OF THE CORRESPONDING	70210015
C	BALANCED MATRIX DETERMINED BY BALANC.	70210016
C		70210017
C	ON INPUT:	70210018
C		70210019
C	NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL	70210020
C	ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM	70210021
C	DIMENSION STATEMENT;	70210022
C		70210023
C	N IS THE ORDER OF THE MATRIX;	70210024
C		70210025
C	LCW AND IGH ARE INTEGERS DETERMINED BY BALANC;	70210026
C		70210027
C	SCALE CONTAINS INFORMATION DETERMINING THE PERMUTATIONS	70210028
C	AND SCALING FACTORS USED BY BALANC;	70210029
C		70210030
C	M IS THE NUMBER OF COLUMNS OF Z TO BE BACK TRANSFORMED;	70210031
C		70210032
C	Z CONTAINS THE REAL AND IMAGINARY PARTS OF THE EIGEN-	70210033
C	VECTORS TO BE BACK TRANSFORMED IN ITS FIRST M COLUMNS.	70210034
C		70210035
C	ON OUTPUT:	70210036

C		7C210037
C	Z CONTAINS THE REAL AND IMAGINARY PARTS OF THE	7C210038
C	TRANSFORMED EIGENVECTORS IN ITS FIRST M COLUMNS.	7C210039
C		7C210040
C	QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBCW,	7C210041
C	APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY	7C210042
C		7C210043
C	-----	7C210044
C		7C210045
C	IF (IGH .EQ. LCW) GO TO 120	7C210046
C		7C210047
C	DO 110 I = LCW, IGH	7C210048
C	S = SCALE(I)	7C210049
C	:::::::::: LEFT HAND EIGENVECTORS ARE BACK TRANSFORMED	7C210050
C	IF THE FOREGOING STATEMENT IS REPLACED BY	7C210051
C	S=1.CDC/SCALE(I). ::::::::::	7C210052
C	DO 100 J = 1, M	7C210053
C	100 Z(I,J) = Z(I,J) * S	7C210054
C		7C210055
C	110 CONTINUE	7C210056
C	:::::::::: FOR I=LCW-1 STEP -1 UNTIL 1,	7C210057
C	IGH+1 STEP 1 UNTIL N DO -- ::::::::::	7C210058
C	120 DO 140 II = 1, N	7C210059
C	I = II	7C210060
C	IF (I .GE. LCW .AND. I .LE. IGH) GO TO 140	7C210061
C	IF (I .LT. LCW) I = LCW - II	7C210062
C	K = SCALE(I)	7C210063
C	IF (K .EQ. 1) GO TO 140	7C210064
C		7C210065
C	DO 130 J = 1, M	7C210066
C	S = Z(I,J)	7C210067
C	Z(I,J) = Z(K,J)	7C210068
C	Z(K,J) = S	7C210069
C	130 CONTINUE	7C210070
C		7C210071
C	140 CONTINUE	7C210072

C

RETLRN

C

***** LAST CARD OF BALBAK *****

END

70210073

70210074

70210075

70210076

```

C
C
C .....
C SUPROUTINE MINV MINV 30
C MINV 40
C MINV 50
C PURPOSE MINV 60
C INVERT A MATRIX MINV 70
C MINV 80
C USAGE MINV 90
C CALL MINV(A,N,D,L,M) MINV 100
C MINV 110
C DESCRIPTION OF PARAMETERS MINV 120
C A - INPUT MATRIX, DESTROYED IN COMPUTATION AND REPLACED BY MINV 130
C RESULTANT INVERSE. MINV 140
C N - ORDER OF MATRIX A MINV 150
C D - RESULTANT DETERMINANT MINV 160
C L - WORK VECTOR OF LENGTH N MINV 170
C M - WORK VECTOR OF LENGTH N MINV 180
C MINV 190
C REMARKS MINV 200
C MATRIX A MUST BE A GENERAL MATRIX MINV 210
C MINV 220
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED MINV 230
C NONE MINV 240
C MINV 250
C METHOD MINV 260
C THE STANDARD GAUSS-JORDAN METHOD IS USED. THE DETERMINANT MINV 270
C IS ALSO CALCULATED. A DETERMINANT OF ZERO INDICATES THAT MINV 280
C THE MATRIX IS SINGULAR. MINV 290
C MINV 300
C ..... MINV 310
C MINV 320
C SUBROUTINE MINV(A,N,D,L,M) MINV 330
C DIMENSION A(1),L(1),M(1) MINV 340
C MINV 350
C ..... MINV 360

```

C		MINV 370
C	IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE	MINV 380
C	C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION	MINV 390
C	STATEMENT WHICH FOLLOWS.	MINV 400
C		MINV 410
C	DOUBLE PRECISION A,D,BIGA,HOLD	MINV 420
C		MINV 430
C	THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS	MINV 440
C	APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS	MINV 450
C	ROUTINE.	MINV 460
C		MINV 470
C	THE DOUBLE PRECISION VERSION OF THIS SUBROUTINE MUST ALSO	MINV 480
C	CONTAIN DOUBLE PRECISION FORTRAN FUNCTIONS. ABS IN STATEMENT	MINV 490
C	10 MUST BE CHANGED TO DABS.	MINV 500
C		MINV 510
C	MINV 520
C		MINV 530
C	SEARCH FOR LARGEST ELEMENT	MINV 540
C		MINV 550
C	D=1.0	MINV 560
C	NK=-N	MINV 570
C	DO 80 K=1,N	MINV 580
C	NK=NK+N	MINV 590
C	L(K)=K	MINV 600
C	M(K)=K	MINV 610
C	KK=NK+K	MINV 620
C	BIGA=A(KK)	MINV 630
C	DO 20 J=K,N	MINV 640
C	IZ=N*(J-1)	MINV 650
C	DO 20 I=K,N	MINV 660
C	IJ=IZ+I	MINV 670
C	10 IF(ABS(BIGA)- ABS(A(IJ))) 15,20,20	MINV 680
C	15 BIGA=A(IJ)	MINV 690
C	L(K)=I	MINV 700
C	M(K)=J	MINV 710
C	20 CONTINUE	MINV 720

C		MINV 730
C	INTERCHANGE ROWS	MINV 740
C	J=L(K)	MINV 750
	IF(J-K) 35,35,25	MINV 760
25	KI=K-N	MINV 770
	DO 30 I=1,N	MINV 780
	KI=KI+N	MINV 790
	HOLD=-A(KI)	MINV 800
	JI=KI-K+J	MINV 810
	A(KI)=A(JI)	MINV 820
30	A(JI)=HOLD	MINV 830
		MINV 840
C		MINV 850
C	INTERCHANGE COLUMNS	MINV 860
C		MINV 870
35	I=M(K)	MINV 880
	IF(I-K) 45,45,38	MINV 890
38	JP=N*(I-1)	MINV 900
	DO 40 J=1,N	MINV 910
	JK=NK+J	MINV 920
	JI=JP+J	MINV 930
	HOLD=-A(JK)	MINV 940
	A(JK)=A(JI)	MINV 950
40	A(JI)=HOLD	MINV 960
		MINV 970
C		MINV 980
C	DIVIDE COLUMN BY MINUS PIVOT (VALUE OF PIVOT ELEMENT IS	MINV 990
C	CONTAINED IN BIGA)	MINV 1000
C		MINV 1010
45	IF(BIGA) 48,46,48	MINV 1020
46	D=0.0	MINV 1030
	RETURN	MINV 1040
48	DO 55 I=1,N	MINV 1050
	IF(I-K) 50,55,50	MINV 1060
50	IK=NK+I	MINV 1070
	A(IK)=A(IK)/(-BIGA)	MINV 1080
55	CONTINUE	

C		MINV1090
C	REDUCE MATRIX	MINV1100
C		MINV1110
	DO 65 I=1,N	MINV1120
	IK=NK+I	MINV1130
	HCLC=A(IK)	MINV1140
	IJ=I-N	MINV1150
	DO 65 J=1,N	MINV1160
	IJ=IJ+N	MINV1170
	IF(I-K) 60,65,60	MINV1180
	60 IF(J-K) 62,65,62	MINV1190
	62 KJ=IJ-I+K	MINV1200
	A(IJ)=HCLC*A(KJ)+A(IJ)	MINV1210
	65 CONTINUE	MINV1220
C		MINV1230
C	DIVIDE ROW BY PIVOT	MINV1240
C		MINV1250
	KJ=K-N	MINV1260
	DC 75 J=1,N	MINV1270
	KJ=KJ+N	MINV1280
	IF(J-K) 70,75,70	MINV1290
	70 A(KJ)=A(KJ)/BIGA	MINV1300
	75 CONTINUE	MINV1310
C		MINV1320
C	PRODUCT OF PIVOTS	MINV1330
C		MINV1340
	D=D*BIGA	MINV1350
C		MINV1360
C	REPLACE PIVOT BY RECIPROCAL	MINV1370
C		MINV1380
	A(KK)=1.0/BIGA	MINV1390
	30 CONTINUE	MINV1400
C		MINV1410
C	FINAL ROW AND COLUMN INTERCHANGE	MINV1420
C		MINV1430
	K=N	MINV1440

```

100 K=(K-1)
    IF(K) 150,150,105
105 I=L(K)
    IF(I-K) 120,120,108
108 JQ=N*(K-1)
    JR=N*(I-1)
    DO 110 J=1,N
        JK=JQ+J
        HOLD=A(JK)
        JI=JR+J
        A(JK)=-A(JI)
110 A(JI) =HOLD
120 J=M(K)
    IF(J-K) 100,100,125
125 KI=K-N
    DO 130 I=1,N
        KI=KI+N
        HOLD=A(KI)
        JI=KI-K+J
        A(KI)=-A(JI)
130 A(JI) =HOLD
    GC TO 100
150 RETRN
    END

```

```

MINV1450
MINV1460
MINV1470
MINV1480
MINV1490
MINV1500
MINV1510
MINV1520
MINV1530
MINV1540
MINV1550
MINV1560
MINV1570
MINV1580
MINV1590
MINV1600
MINV1610
MINV1620
MINV1630
MINV1640
MINV1650
MINV1660
MINV1670
MINV1680

```

APPENDIX B

INPUT DATA AND OUTPUT LISTING OF THE SAMPLE PROBLEMS

B.1 Application of the FREEVI Program to the Wing

B.1.1 Input Data Listing for the Bell Wing

The FREEVI program input data for the wing are illustrated in this section. The structural data are shown in Fig. 6 and in Table 3.

RELL WING

1
2
0

9 20 6

0.001

0.0

0.0

0.0

0.0

0.0

0.0

9202.9

E62653.0

E62653.0

E62653.0

E62653.0

2653.0

E62653.0

E62653.0

E62653.0

E6

18794.0

E610410.0

E610410.0

E610410.0

E610410.0

E6

10410.0

E610410.0

E610410.0

E610410.0

E6

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.00705

0.00705

0.00488

0.00488

0.00488

0.00488

0.00508

0.03248

0.00001

41.0

21.0

21.0

21.0

21.0

21.0

21.0

18.4

14.6

4.71

4288.8

6591.6

6570.0

53.076

16868.0

E62696.0

E62696.0

E62696.0

E62696.0

E6

2696.0

E62696.0

E62696.0

E62696.0

E6

0.389

E00.389

E00.389

E00.389

E00.389

E0

0.389

E00.389

E00.389

E00.389

E0

0.0

E00.0

E00.0

E00.0

E00.0

E0

0.0

E00.0

E00.0

E00.0

E0

8/17/74	DATA0001
ICASE	DATA0002
IPUNCH	DATA0003
IGUEST	DATA0004
NET,NITP,M	DATA0005
ERR	DATA0006
DMFG	DATA0007
RAMDA	DATA0008
COL	DATA0009
SPKB,SPKC	DATA0010
ALPHAH	DATA0011
E6	DATA0012
E6	DATA0013
E6	DATA0014
E6	DATA0015
0.0	DATA0016
0.0	DATA0017
0.00705	DATA0018
0.00001	DATA0019
41.0	DATA0020
14.6	DATA0021
4.71	DATA0022
16868.0	DATA0023
2696.0	DATA0024
0.389	DATA0025
0.389	DATA0026
0.0	DATA0027
0.0	DATA0028

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B.1.2 The FEEVI program output data for the Bell Wing. The example output of the Bell wing is shown in this subsection.

WING

BELL WING

8/17/74

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

* *
INPUT DATA

IPUNCH=0 IGMEST=0
NO OF DEGRE PER NODE= 6
NO OF ELEMENTS= 9
NO OF MAX ITER ALLOWD= 20
NO OF MODES= 6
ERR= 0.00100
OMEG= 0.0
LAMRDA= 0.0
COLLECTIVE PITCH= 0.0
SPRING= 0.0 0.0 0.0
ALPHA= 0.0

881

--FLAPPING BENDING STIFFNESS--
 0.9207901E+10 0.2653000E+10 0.2653000E+10 0.2653000E+10 0.2653000E+10 0.2653000E+10 0.2653000E+10
 0.2653000E+10 0.2653000E+10

--CHORDWISE BENDING STIFFNESS--
 0.1879400E+11 0.1041000E+11 0.1041000E+11 0.1041000E+11 0.1041000E+11 0.1041000E+11 0.1041000E+11
 0.1041000E+11 0.1041000E+11

--ANGLE OF TWIST--
 0.0 0.0 0.0 0.0 0.0 0.0 0.0

--MASS DISTRIBUTION--
 0.00705 0.00705 0.00488 0.00488 0.00488 0.00488 0.01518 0.03248
 0.00011

--ELEMENT SIZE--
 41.00000 21.00000 21.00000 21.00000 21.00000 21.00000 21.00000 10.33333
 14.60000
 TIP MASS ROLL INERTIA YAW INERTIA PITCH INERTIA MASS COUPLING
 4.71000 4288.80078 6591.60156 6570.00000 53.07600

--TORSIONAL RIGIDITY--
 0.1696800E+11 0.2696000E+10 0.2696000E+10 0.2696000E+10 0.2696000E+10 0.2696000E+10 0.2696000E+10
 0.2696000E+10 0.2696000E+10

--MOMENT OF INERTIA--
 0.3890000E+00 0.3890000E+00 0.3890000E+00 0.3890000E+00 0.3890000E+00 0.3890000E+00 0.3890000E+00
 0.3890000E+00 0.3890000E+00

--MASS COUPLING ALONG SPAN--
 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 0.0 0.0

TENSION DUE TO CENTRIF FORCE

0.0 0.0 0.0 0.0 0.0 0.0 0.0

MASS = 0.62615E+01
 MOMENT OF INERTIA AT ROOT= 0.21483E+06
 TOTAL LENGTH OF THE BEAM= 0.20000E+03

MAX. SIZE OF STF IS 484 SPECIFIED SIZE IS 654

NO. OF NEGATIVE DIAGS.= 0 FACT. COMPLETED

EIGENVALUES=
 0.28091D+03 0.89998D+03 0.16245D+05 0.34651D+05 0.26504D+06 0.53303D+06

EIGENVALUES=
 0.27768D+03 0.89084D+03 0.27303D+04 0.12970D+05 0.32610D+05 0.27656D+06

EIGENVALUES=
 0.27768D+03 0.89084D+03 0.27300D+04 0.12968D+05 0.32494D+05 0.26217D+06

EIGENVALUES=
 0.27768D+03 0.89084D+03 0.27300D+04 0.12968D+05 0.32494D+05 0.26097D+06

EIGENVALUES=
 0.27768D+03 0.89084D+03 0.27300D+04 0.12968D+05 0.32494D+05 0.26086D+06

RADIAN/SFC
 0.16664D+02 0.29847D+02 0.52250D+02 0.11388D+03 0.18026D+03 0.51074D+03

HERTZ
 0.26521D+01 0.47503D+01 0.83158D+01 0.18124D+02 0.28689D+02 0.81287D+02

NO. OF ITERATION= 5 CONVERGED WITHIN 0.10000D-02

REDUCED MASS MATRIX

0.10000D+01
 0.11699D-22 0.10000D+01
 -0.51511D-20 -0.33025D-21 0.10000D+01
 -0.11639D-19 -0.13470D-17 -0.92236D-19 0.10000D+01
 0.88490D-24 -0.13376D-20 0.12102D-18 0.10999D-19 0.10000D+01
 -0.51707D-20 0.76081D-20 0.13915D-17 0.86677D-18 -0.20838D-19 0.10000D+01

REDUCED STIF MATRIX

0.27768D+03
 0.12056D-18 0.89084D+03
 -0.59669D-13 0.38420D-17 0.27300D+04
 -0.36503D-17 -0.11888D-16 0.93751D-16 0.12968D+05
 -0.27794D-16 0.63537D-13 -0.98995D-18 -0.58898D-14 0.32494D+05
 -0.44715D-16 -0.12874D-12 -0.11159D-15 -0.89091D-14 0.16965D-15 0.26086D+06

REPRODUCIBILITY OF THIS ORIGINAL PAGE IS POOR.

i= 1

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PHI(I,J)	DPHI(I,J)
1	0.0	0.0	0.0	0.0	0.0	0.4722115E-06
2	0.1096412E-01	-0.4118297E-09	0.5154577E-03	-0.1607660E-10	0.1781619E-04	0.5205245E-05
3	0.2995049E-01	-0.7596179E-09	0.1275148E-02	-0.1562293E-10	0.6824774E-04	0.2253155E-05
4	0.5378090E-01	-0.1020656E-08	0.1929206E-02	-0.8398275E-11	0.1270887E-03	0.2578340E-05
5	0.1102392E+00	-0.1089811E-08	0.2477859E-02	0.2030671E-11	0.1765127E-03	0.2587192E-05
6	0.1671160E+00	-0.9396308E-09	0.2921520E-02	0.1186243E-10	0.2310340E-03	0.2595412E-05
7	0.2322127E+00	-0.6202676E-09	0.3260845E-02	0.1763036E-10	0.2855684E-03	0.2596634E-05
8	0.3033477E+00	-0.2455758E-09	0.3496786E-02	0.1680664E-10	0.3401006E-03	0.2596617E-05
9	0.3689417E+00	0.5387467E-11	0.3620509E-02	0.9286009E-11	0.3878768E-03	0.2596392E-05
10	0.4221950E+00	0.6504591E-10	0.3666978E-02	-0.1889718E-11	0.4257825E-03	0.2596161E-05

i= 2

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PHI(I,J)	DPHI(I,J)
1	0.0	0.0	0.0	0.0	0.0	0.1334282E-13
2	-0.1165887E-08	0.1734024E-01	-0.4099619E-10	0.8156588E-03	0.4967241E-12	0.1503241E-13
3	-0.1780436E-08	0.4120878E-01	-0.1078385E-10	0.1443248E-02	0.1793459E-11	0.5271469E-13
4	-0.1508654E-08	0.7735723E-01	0.3577688E-10	0.1985208E-02	0.2899238E-11	0.4211952E-13
5	-0.4287495E-09	0.1239857E+00	0.6140244E-10	0.2441776E-02	0.3564264E-11	0.1910476E-13
6	0.7976879E-09	0.1793168E+00	0.4901710E-10	0.2813344E-02	0.3702648E-11	-0.5942711E-14
7	0.1419738E-08	0.2415592E+00	0.7250959E-11	0.3100497E-02	0.3337920E-11	-0.2797991E-13
8	0.1085335E-08	0.3089525E+00	-0.3688012E-10	0.3304057E-02	0.2568981E-11	-0.4423085E-13
9	0.2516420E-09	0.3708636E+00	-0.4400005E-10	0.3415339E-02	0.1653754E-11	-0.5236117E-13
10	-0.1154645E-09	0.4211117E+00	0.2109291E-11	0.3461931E-02	0.8527415E-12	-0.5725261E-13

i= 3

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PHI(I,J)	DPHI(I,J)
1	0.0	0.0	0.0	0.0	0.0	-0.1426321E-04
2	0.3132011E-02	0.1007552E-05	0.1483440E-03	0.4164287E-07	-0.5369008E-03	-0.1776540E-04
3	0.8682542E-02	0.1967319E-05	0.3762855E-03	0.4036162E-07	-0.2056599E-02	-0.4788566E-04
4	0.1876992E-01	0.2640408E-05	0.5815080E-03	0.2158016E-07	-0.3678715E-02	-0.7646301E-04
5	0.3290243E-01	0.2815990E-05	0.7615838E-03	-0.5406847E-08	-0.5317826E-02	-0.7790148E-04
6	0.5060757E-01	0.2425011E-05	0.9210168E-03	-0.3075634E-07	-0.6959036E-02	-0.7810385E-04
7	0.7144558E-01	0.1598726E-05	0.1060446E-02	-0.4554926E-07	-0.8599557E-02	-0.7808290E-04
8	0.9502667E-01	0.6317913E-06	0.1182828E-02	-0.4332351E-07	-0.1023867E-01	-0.7811231E-04
9	0.1177033E+00	-0.1453627E-07	0.1292109E-02	-0.2388719E-07	-0.1167341E-01	-0.7793421E-04
10	0.1370279E+00	-0.1678002E-06	0.1366351E-02	0.4879347E-08	-0.1281075E-01	-0.7786400E-04

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I = 4

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PHI(I,J)	DPHI(I,J)
1	0.0	0.0	0.0	0.0	0.0	-0.8024932E-06
2	0.5561896E-01	0.1292796E-04	0.2441053E-02	0.5067098E-06	-0.3020581E-04	-0.4993528E-06
3	0.1320716E+00	0.2396124E-04	0.4596125E-02	0.4992368E-06	-0.1156774E-03	-0.3916693E-05
4	0.2385222E+00	0.3238695E-04	0.5303770E-02	0.2753594E-06	-0.2068353E-03	-0.4294215E-05
5	0.3449906E+00	0.3479325E-04	0.4606590E-02	-0.5469537E-07	-0.2989146E-03	-0.4367300E-05
6	0.4226109E+00	0.3018290E-04	0.2568961E-02	-0.3721857E-06	-0.3907180E-03	-0.4369117E-05
7	0.4440947E+00	0.2005251E-04	-0.7243240E-03	-0.5633744E-06	-0.4823287E-03	-0.4353352E-05
8	0.3840748E+00	0.8010285E-05	-0.5176779E-02	-0.5431260E-06	-0.5735478E-03	-0.4333073E-05
9	0.2462974E+00	-0.1363661E-06	-0.9906098E-02	-0.3031313E-06	-0.6531981E-03	-0.4312168E-05
10	0.7180148E-01	-0.2095530E-05	-0.1494954E-01	0.6066438E-07	-0.7159102E-03	-0.4293397E-05

I = 5

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PHI(I,J)	DPHI(I,J)
1	0.0	0.0	0.0	0.0	0.0	-0.1459670E-10
2	0.2360992E-05	0.6912452E-01	0.8368607E-07	0.2999669E-02	-0.5442764E-09	-0.1754913E-10
3	0.3658400E-05	0.1467586E+00	0.2591068E-07	0.4220549E-02	-0.1985294E-08	-0.5971562E-10
4	0.3202141E-05	0.2391850E+00	-0.6824558E-07	0.4412588E-02	-0.3275932E-08	-0.5190257E-10
5	0.1072496E-05	0.3250876E+00	-0.1235147E-06	0.3604392E-02	-0.4168427E-08	-0.3056966E-10
6	-0.1439291E-05	0.3838446E+00	-0.1026097E-06	0.1835852E-02	-0.4545821E-08	-0.4646506E-11
7	-0.2793039E-05	0.3958154E+00	-0.1964723E-07	-0.8429433E-03	-0.4376279E-08	0.2069658E-10
8	-0.2200011E-05	0.3424572E+00	0.7231574E-07	-0.4376560E-02	-0.3702741E-08	0.4262971E-10
9	-0.5198935E-06	0.2284233E+00	0.9011211E-07	-0.8104231E-02	-0.2779422E-08	0.5684486E-10
10	0.2345656E-06	0.8644497E-01	-0.4498673E-08	-0.1138999E-01	-0.1892494E-08	0.6401313E-10

I = 6

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PHI(I,J)	DPHI(I,J)
1	0.0	0.0	0.0	0.0	0.0	0.109331E-05
2	0.4376729E+00	-0.2575393E-02	0.1791070E-01	-0.1012992E-03	0.4025537E-04	0.1326111E-05
3	0.9022505E+00	-0.4794151E-02	0.2376941E-01	-0.1010866E-03	0.1531777E-03	0.4997642E-05
4	0.1344618E+01	-0.6516449E-02	0.1658912E-01	-0.5725150E-04	0.2711348E-03	0.5471314E-05
5	0.1544214E+01	-0.7044502E-02	0.1633530E-02	0.8975477E-05	0.3861518E-03	0.5325622E-05
6	0.1403761E+01	-0.6153475E-02	-0.1466782E-01	0.7372542E-04	0.4943394E-03	0.4999302E-05
7	0.9648077E+00	-0.4121412E-02	-0.2577179E-01	0.1139852E-03	0.5959135E-03	0.4572572E-05
8	0.3952152E+01	-0.1466956E-02	-0.2639399E-01	0.1115181E-03	0.6983750E-03	0.4292110E-05
9	-0.6146964E-02	0.1676849E-04	-0.1504268E-01	0.6317307E-04	0.7567220E-03	0.3902065E-05
10	-0.7912896E-01	0.4287334E-03	0.3793120E-02	-0.1231682E-04	0.8057512E-03	0.3107408E-05

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B.2 Application of the FREEVI Program to the Blade

B.2.1 The FREEVI Program Input Data Listing for the Boeing Rotor (Hingeless Rotor)

The input data deck setup is illustrated in this subsection for the hingeless rotor. Structural data are shown in Fig. 7.

BOEING BLADE FOR POWERED FLIGHT --- CLAMPED & CLAMPED B.C

2
1
0

10 20 4

0.001
-40.422
-0.7

0.017453

8525.0

106.0

5.0

110.0

520.0

0.6981

-0.0611

0.016583

0.0012303

15.6

15.6

0.0106064

F619.0

F64.51

F640.0

F6510.0

0.4712

-0.1134

0.001036

0.001036

15.6

15.6

0.3403

0.000777

15.6

E68.5

E64.5

E640.0

E6515.0

0.2531

0.000906530.001036

15.6

E67.5

E64.5

E6200.0

E6530.0

0.1833

0.001036

15.6

E65.5

E64.0

E6500.0

E6535.0

0.1222

0.001036

15.6

8/18/74
ICASE
IPUNCH
IGUFST
NET,NITR,M

ERR
OMEG
RAMDA
COL
SPKB,SPKC
ALPHAH

E6
E6
E6
E6

0.0
0.0012303

15.6

DATA0001
DATA0002
DATA0003
DATA0004
DATA0005
DATA0006
DATA0007
DATA0008
DATA0009
DATA0010
DATA0011
DATA0012
DATA0013
DATA0014
DATA0015
DATA0016
DATA0017
DATA0018
DATA0019
DATA0020
DATA0021
DATA0022

**B.2.2 The FREEVI Program Output Data for
the Boeing Blade**

The example output of the Boeing
blade is shown in this subsection.

BLADE BEAM*CANTI CHCRD*CANTI

ROFING BLADE FOR POWERED FLIGHT --- CLAMPED & CLAMPED B.C.

8/18/74

INPUT DATA

IPUNCH=1 IQUEST=0
 NO OF DEGRE PER NODE= 4
 NO OF ELEMENTS= 10
 NO OF MAX ITER ALLOEWD= 20
 NO OF MODES= 4
 ERR= 0.00100
 OMEG= -40.42200
 LAMBDA= -0.70000
 COLLECTIVE PITCH= 0.01745
 SPRING= 0.0 0.0
 ALPHA= 0.85250D+04

--FLAPPING BENDING STIFFNESS--

0.106000E+09	0.190000E+03	0.850000E+07	0.750000E+07	0.550000E+07	0.500000E+07	0.450000E+07
0.450000E+07	0.450000E+07	0.400000E+07				

--CHORDWISE BENDING STIFFNESS--

0.110000E+09	0.400000E+03	0.400000E+08	0.200000E+09	0.500000E+09	0.520000E+09	0.510000E+09
0.515000E+09	0.530000E+09	0.535000E+09				

--ANGLE OF TWIST--

0.69810	0.47120	0.34030	0.25310	0.18330	0.12220	0.06110	0.0
-0.06110	-0.11340						

--MASS DISTRIBUTION--

0.01658	0.00104	0.00078	0.00091	0.00104	0.00104	0.00104	0.00128
0.00123	0.00104						

--ELEMENT SIZE--

15.60000	15.60000	15.60000	15.60000	15.60000	15.60000	15.60000	15.60000
15.60000	15.60000						
TIP MASS	ROLL INERTIA	YAW INERTIA	PITCH INERTIA	MASS COUPLING			
0.01061	0.0	0.0	0.0	0.0			

TENSION DUE TO CENTRIF FORCE

27190.4219	23893.4883	23275.5703	22503.1680	21241.5352	19387.7656	17122.0409	14444.1700
10775.3086	6617.02734	2703.50903					

MASS = 0.41476E+00

MOMENT OF INERTIA AT ROOT= 0.16714E+04

TOTAL LENGTH OF THE BEAM= 0.15600E+03

MAX. SIZE OF STEP IS 244 SPECIFIED SIZE IS 324

NO. OF NEGATIVE DIAGS.= 0 FACT. COMPLETED

EIGENVALUES=
0.20880D+04 0.12950D+05 0.27569D+05 0.42059D+06

EIGENVALUES=
0.11180D+04 0.28840D+04 0.19005D+05 0.90243D+05

EIGENVALUES=
0.11172D+04 0.28520D+04 0.18997D+05 0.75550D+05

EIGENVALUES=
0.11172D+04 0.28519D+04 0.18986D+05 0.74979D+05

EIGENVALUES=
0.11172D+04 0.28519D+04 0.18986D+05 0.74934D+05

RADIAN/SEC
0.33424D+02 0.53403D+02 0.13743D+03 0.27374D+03

HERTZ
0.53197D+01 0.84993D+01 0.21872D+02 0.43567D+02

NO. OF ITERATION= 5 CONVERGED WITHIN 0.10000D-02

REDUCED MASS MATRIX

0.10000D+01
0.92346D-19 0.10000D+01
0.21682D-16 0.54958D-20 0.10000D+01
0.92709D-20 -0.19679D-21 -0.12149D-19 0.10000D+01

REDUCED STIF MATRIX

0.96422D+04
0.59174D-14 0.11377D+05
-0.77329D-15 0.45209D-16 0.27411D+05
0.99997D-15 -0.51587D-16 0.30254D-14 0.83459D+05

**** BLADE MODE SHAPES ****

I= 1

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)
1	0.0	0.0	0.0	0.0
2	-0.3071345E-02	0.3320938E-01	-0.4138651E-03	0.3957305E-02
3	-0.4010361E-02	0.1970022E+00	0.3891176E-04	0.1585099E-01
4	0.1771531E-01	0.5429144E+00	0.2249592E-02	0.2720761E-01
5	0.7252330E-01	0.1007425E+01	0.4471347E-02	0.3180430E-01
6	0.1537749E+00	0.1521890E+01	0.5777858E-02	0.3390279E-01
7	0.2471325E+00	0.2056107E+01	0.6131638E-02	0.3450100E-01
8	0.3411351E+00	0.2593284E+01	0.5890395E-02	0.3432557E-01
9	0.4277322E+00	0.3123945E+01	0.5184587E-02	0.3367477E-01
10	0.5013666E+00	0.3643093E+01	0.4255518E-02	0.3287940E-01
11	0.5611690E+00	0.4150885E+01	0.3513225E-02	0.3230092E-01

I= 2

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)
1	0.0	0.0	0.0	0.0
2	0.4854569E-01	-0.1528439E-01	0.5902052E-02	-0.1984358E-02
3	0.2357861E+00	-0.7704520E-01	0.1740308E-01	-0.6000815E-02
4	0.5839912E+00	-0.1807868E+00	0.2659480E-01	-0.7669512E-02
5	0.1021941E+01	-0.2842678E+00	0.2921298E-01	-0.6042498E-02
6	0.1496003E+01	-0.3587406E+00	0.3124276E-01	-0.3921565E-02
7	0.1999373E+01	-0.4039884E+00	0.3303983E-01	-0.2163647E-02
8	0.2529638E+01	-0.4239655E+00	0.3474081E-01	-0.5953177E-03
9	0.3083344E+01	-0.4232069E+00	0.3608362E-01	0.5515825E-03
10	0.3653433E+01	-0.4089971E+00	0.3684258E-01	0.1142329E-02
11	0.4229228E+01	-0.3904818E+00	0.3681497E-01	0.1111808E-02

I= 3

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)
1	0.0	0.0	0.0	0.0
2	-0.7415771E-01	-0.6834286E-01	-0.8815017E-02	-0.7958513E-02
3	-0.3768928E+00	-0.4091305E+00	-0.2786428E-01	-0.3210701E-01
4	-0.9542273E+00	-0.1096154E+01	-0.4312693E-01	-0.5081352E-01
5	-0.1634645E+01	-0.1890661E+01	-0.4194136E-01	-0.4759142E-01
6	-0.2171334E+01	-0.2465169E+01	-0.2487231E-01	-0.2329279E-01
7	-0.2331151E+01	-0.2544001E+01	0.5753405E-02	0.1486159E-01
8	-0.1917680E+01	-0.1956378E+01	0.4791136E-01	0.6119271E-01
9	-0.8257181E+00	-0.6669863E+00	0.0105462E-01	0.1031131E+00
10	0.8585268E+00	0.1168359E+01	0.1214661E+00	0.1292541E+00
11	0.2855342E+01	0.3263458E+01	0.1302493E+00	0.1361389E+00

I= 4

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)
1	0.0	0.0	0.0	0.0
2	0.5017383E-01	0.2488598E+00	0.6019792E-02	0.2434810E-01
3	0.3397898E+00	0.1251101E+01	0.2845969E-01	0.8702511E-01
4	0.9262698E+00	0.2709785E+01	0.4080152E-01	0.8272529E-01
5	0.1313488E+01	0.3515694E+01	0.4193374E-02	0.1209554E-01
6	0.9240110E+00	0.2383393E+01	-0.6620103E-01	-0.9227397E-01
7	-0.5951878E+00	0.9211577E+00	-0.1073077E+00	-0.1433129E+00
8	-0.2063768E+01	-0.1215673E+01	-0.6792390E-01	-0.1107410E+00
9	-0.2215355E+01	-0.2093109E+01	0.5533580E-01	0.5113750E-02
10	-0.2487896E+00	-0.1083831E+01	0.1872610E+00	0.1102710E+00
11	0.3242643E+01	0.1165529E+01	0.2399881E+00	0.1505680E+00

B.3 The TILDYN Program Examples

B.3.1 Input Data Listing for the TILDYN Program

In this subsection, the sample problem data deck setup is illustrated. The flight condition is powered flight for the Boeing model and autorotation flight for the Bell model. The data for the computation is shown in Table 3 in detail.

BOEING ROTOR --POWERED FLT-- SDCF, U-GUST, FREQ RES & EIGEN ANALYSIS								8/20/74	DATA0001
0								ITYPE	DATA0002
0								IFLT	DATA0003
9								DOF	DATA0004
1								FREQRE	DATA0005
0								IFRMAG	DATA0006
1								IEIGEN	DATA0007
3									DATA0008
1.1468	E-7-40.422	-0.7	4414.082						DATA0009
156.0	1800.0	18.8496	5.7	0.0065	55.224				DATA0010
200.5	62.18	5.7	0.004	-0.05	0.0	0.01	0.031		DATA0011
1.0	0.0	0.0	0.0	0.0	0.0		U GUST		DATA0012
1117.2	2851.9	18886.0	74927.0						DATA0013
217.68	656.97	2002.2	5988.4	25466.0	252710.0				DATA0014
9									DATA0015
0.205	0.105	0.105	0.105	0.105	0.105	0.105	0.092		DATA0016
0.073									DATA0017
0.0	0.56884E-02	0.26480E-01	0.56422E-01	0.97570E-01	0.14798E+00				DATA0018
0.20573E+00	0.26889E+00	0.32718E+00	0.37453E+00						DATA0019
0.0	-0.19216E-09	-0.35539E-09	-0.47946E-09	-0.51490E-09	-0.44798E-09				DATA0020
-0.30091E-09	-0.12576E-09	-0.61370E-11	0.24547E-10						DATA0021
0.0	0.45561E-03	0.11282E-02	0.17080E-02	0.21954E-02	0.25905E-02				DATA0022
0.28939E-02	0.31061E-02	0.32185E-02	0.32613E-02						DATA0023
0.0	-0.75167E-11	-0.73673E-11	-0.40539E-11	0.78800E-12	0.54042E-11				DATA0024
0.81805E-11	0.79227E-11	0.45167E-11	-0.68893E-12						DATA0025
0.0	0.12465E-04	0.47748E-04	0.85418E-04	0.12350E-03	0.16164E-03				DATA0026
0.19980E-03	0.23795E-03	0.27138E-03	0.29790E-03						DATA0027
0.33113E-06	0.41245E-06	0.19763E-05	0.17759E-05	0.18101E-05	0.18159E-05				DATA0028
0.18168E-05	0.18168E-05	0.18167E-05	0.18166E-05						DATA0029
0.0	-0.69305E-09	-0.10621E-08	-0.50808E-09	-0.27148E-09	0.46049E-09				DATA0030
0.84255E-09	0.65858E-09	0.16850E-09	-0.52234E-10						DATA0031
0.0	0.15288E-01	0.36346E-01	0.68257E-01	0.10945E+00	0.15835E+00				DATA0032
0.21341E+00	0.27306E+00	0.32790E+00	0.37243E+00						DATA0033
0.0	-0.24413E-10	-0.67135E-11	0.20905E-10	0.36406E-10	0.29522E-10				DATA0034
0.50409E-11	-0.21349E-10	-0.26157E-10	0.96106E-12						DATA0035
0.0	0.71933E-03	0.12737E-02	0.17530E-02	0.21576E-02	0.24876E-02				DATA0036

C.27435E-C2	C.29258E-C2	C.30262E-02	0.30684E-02					DATA0037
0.0	C.26198E-12	C.94384E-12	C.15192E-11	0.18532E-11	C.19004E-11			DATA0038
0.16760E-11	0.12374E-11	C.73507E-12	0.29310E-12					DATA0039
C.70398E-14	C.83981E-14	0.27607E-13	0.21644E-13	0.90527E-14	-0.45720E-14			DATA0040
-0.16357E-13	-0.24832E-13	-0.29312E-13	-0.30956E-13					DATA0041
C.0	0.20401E-C2	C.56893E-02	0.12371E-C1	0.21795E-C1	C.33683E-01			DATA0042
0.47769E-01	C.63816E-C1	C.79330E-C1	C.92582E-01					DATA0043
0.0	0.51587E-C6	C.95202E-C6	C.12840E-C5	C.13769E-05	0.11962E-05			DATA0044
C.80224E-06	C.33481E-C6	C.16006E-07	-0.65507E-07					DATA0045
C.0	0.96922E-C4	C.24829E-03	0.38574E-03	0.50960E-03	0.62045E-03			DATA0046
C.71923E-C3	C.80735E-C3	C.87878E-03	0.93691E-03					DATA0047
0.0	0.20161E-C7	C.19697E-07	0.10769E-C7	-0.22027E-08	-0.14514E-07			DATA0048
-0.21872E-C7	-0.21124E-C7	-0.12014E-C7	0.18404E-C8					DATA0049
C.0	-0.46056E-C3	-0.17642E-02	-0.31557E-02	-0.45620E-02	-0.59703E-02			DATA0050
-0.73783E-C2	-0.87854E-C2	-0.10017E-01	-0.10994E-01					DATA0051
-0.12235E-C4	-0.15239E-C4	-0.58235E-04	-0.65598E-04	-0.66841E-04	-0.67026E-04			DATA0052
-0.67023E-C4	-0.66980E-C4	-0.66931E-04	-0.66887E-04					DATA0053
10								DATA0054
0.1	0.1	C.1	C.1	0.1	0.1	0.1	0.1	DATA0055
0.1	C.1							DATA0056
0.C165	0.C0877	C.C0091	C.C0085	0.C0098	0.00104	0.00104	0.00116	DATA0057
0.00123	0.C0116	C.C0104						DATA0058
0.6545	0.5236	C.3927	C.2793	C.2007	C.1484	0.0873	0.0291	DATA0059
-0.C297	-0.C873	-C.1396						DATA0060
0.C175								DATA0061
0.0	-0.30837E-C2	-0.40433E-C2	0.17669E-01	0.72429E-01	0.15358E+00			DATA0062
0.24691E+00	C.34107E+00	C.42791E+00	0.50157E+00	0.56107E+00				DATA0063
C.0	0.33251E-C1	C.19717E+00	0.54318E+00	C.10076E+01	0.15219E+01			DATA0064
C.20560E+01	C.25932E+01	C.31241E+01	0.36432E+01	0.41507E+01				DATA0065
0.0	-0.41524E-C3	C.37868E-04	C.22488E-C2	0.44661E-02	0.57715E-02			DATA0066
0.61346E-02	0.59060E-C2	C.51967E-C2	0.42450E-C2	0.34889E-02				DATA0067
C.C	C.39618E-C2	C.15860E-01	0.27209E-01	0.31795E-01	0.33890E-01			DATA0068
C.34499E-01	C.34336E-C1	C.33681E-C1	0.32866E-01	0.32277E-01				DATA0069
C.0	C.48522E-C1	C.23571E+00	0.58387E+00	0.10218E+01	0.14959E+01			DATA0070
0.19993E+01	0.25296E+01	0.30834E+01	0.36535E+01	0.42293E+01				DATA0071
C.0	-0.15271E-C1	-0.76997E-C1	-0.18072E+00	-0.28422E+00	-0.35870E+00			DATA0072

-0.40395E+00	-0.42391E+00	-0.42317E+00	-0.40902E+00	-0.39059E+00			DATA0073
0.0	C.58995E-02	0.17399E-01	0.26594E-01	0.29213E-01	0.31244E-01		DATA0074
C.33043E-01	C.34745E-01	C.36086E-01	0.36842E-01	0.50814E-01			DATA0075
C.0	-0.18829E-02	-C.60045E-02	-0.76701E-02	-0.60446E-02	-0.39221E-02		DATA0076
-0.21631E-02	-C.59548E-03	C.54903E-03	0.11376E-02	0.11063E-02			DATA0077

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1										DATA0001
1										DATA0002
9										DATA0003
1										DATA0004
3										DATA0005
1.1468	F-748.C	C.7	5040.C							DATA0006
150.0	1260.0	14.0	5.7	0.0065	51.3	-0.2618				DATA0007
200.5	62.18	5.7	0.004	-0.005	0.0	0.01	0.031			DATA0008
1.0	0.0	0.0	0.0	0.0	0.0		U GUST			DATA0009
2380.1	4143.4	43503.C	236090.0							DATA0010
277.68	890.84	2730.C	12968.0	32494.0	260860.0					DATA0011
9										DATA0012
0.205	J.105	C.105	C.105	C.105	C.105	0.105	0.092			DATA0013
0.073										DATA0014
0.0	0.10964E-01	0.29950E-01	0.63781E-01	0.11024E+00	0.16712E+00					DATA0015
0.23221E+00	0.30335E+00	0.36894E+00	0.42219E+00							DATA0016
0.0	-0.41183E-09	-0.75962E-09	-0.10207E-08	-0.10898E-08	-0.93963E-09					DATA0017
-0.62027E-09	-0.24558E-09	0.53875E-11	0.65046E-10							DATA0018
0.0	0.51546E-03	0.12751E-02	0.19292E-02	0.24779E-02	0.29215E-02					DATA0019
0.32608E-02	0.34968E-02	0.36205E-02	0.36670E-02							DATA0020
0.0	-0.16077E-10	-0.15623E-10	-0.83983E-11	0.20307E-11	0.11862E-10					DATA0021
0.17630E-10	0.16807E-10	0.92860E-11	-0.18897E-11							DATA0022
0.0	0.17816E-04	0.68248E-04	0.12209E-03	0.17651E-03	0.23103E-03					DATA0023
0.28557E-03	0.34010E-03	0.38788E-03	0.42578E-03							DATA0024
0.47329E-06	0.58952E-06	0.22530E-05	0.25383E-05	0.25872E-05	0.25954E-05					DATA0025
0.25966E-05	0.25966E-05	0.25964E-05	0.25962E-05							DATA0026
0.0	-0.11659E-08	-0.17804E-08	-0.15087E-08	-0.42875E-09	0.79769E-09					DATA0027
0.14197E-08	0.10853E-08	0.25164E-09	-0.11546E-09							DATA0028
0.0	0.17340E-01	0.41209E-01	0.77357E-01	0.12399E+00	0.17932E+00					DATA0029
0.24156E+00	0.30855E+00	0.37086E+00	0.42111E+00							DATA0030
0.0	-0.40996E-10	-0.10784E-10	0.35777E-10	0.61402E-10	0.49017E-10					DATA0031
0.72510E-11	-0.36880E-10	-0.44000E-10	0.21093E-11							DATA0032
0.0	0.81566E-03	0.14432E-02	0.15852E-02	0.24418E-02	0.28133E-02					DATA0033
										DATA0034
										DATA0035
										DATA0036

202

0.31005E-C2	0.23041E-C2	0.34153E-C2	0.34619E-02						DATA0037
0.0	0.49672E-12	0.17935E-11	0.28992E-11	0.35643E-11	0.37026E-11				DATA0038
0.33378E-11	0.25690E-11	0.16638E-11	0.85274E-12						DATA0039
0.13343E-13	0.15940E-13	0.52715E-13	0.42119E-13	0.19105E-13	-0.59927E-14				DATA0040
-0.27980E-13	-0.44235E-12	-0.53361E-13	-0.57253E-12						DATA0041
0.0	0.31320E-C2	0.86825E-02	0.18770E-01	0.32902E-01	0.50608E-01				DATA0042
0.71446E-01	0.95027E-C1	0.11770E+00	0.12703E+00						DATA0043
0.0	0.10676E-C5	0.19673E-C5	0.26404E-C5	0.28160E-05	0.24250E-05				DATA0044
0.15987E-05	0.63175E-C6	-0.14536E-07	-0.16780E-06						DATA0045
0.0	0.14824E-C3	0.37629E-C3	0.58051E-C3	0.76168E-03	0.92102E-03				DATA0046
0.10604E-C2	0.11828E-C2	0.12821E-02	0.13664E-02						DATA0047
0.0	0.41642E-C7	0.40362E-07	0.21587E-07	-0.54068E-08	-0.30756E-07				DATA0048
-0.45549E-C7	-0.43324E-C7	-0.23887E-C7	0.48792E-C8						DATA0049
0.0	-0.53651E-03	-0.20566E-02	-0.36787E-02	-0.53178E-02	-0.69590E-02				DATA0050
-0.85956E-C2	-0.10239E-C1	-0.11673E-C1	-0.12811E-C1						DATA0051
-0.14263E-C4	-0.17765E-C4	-0.67886E-04	-0.76463E-04	-0.77901E-04	-0.78104E-04				DATA0052
-0.78083E-C4	-0.78012E-C4	-0.77934E-C4	-0.77864E-04						DATA0053
10									DATA0054
0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1		DATA0055
0.1	0.1								DATA0056
0.006993	0.005439	0.003108	0.001295	0.001336	0.001465	0.001165	0.001036		DATA0057
0.0009712	0.0008417	0.000712							DATA0058
0.6807	0.5585	0.4363	0.3054	0.2094	0.1222	0.0698	0.0262		DATA0059
-0.0175	-0.0611	-0.1047							DATA0060
0.0218									DATA0061
0.0	0.43406E+00	0.87001E+00	0.13071E+01	0.17459E+01	0.21867E+01				DATA0062
0.26295E+01	0.30737E+01	0.35186E+01	0.35633E+01	0.44072E+01					DATA0063
0.0	-0.42327E-C3	-0.16251E-02	-0.42110E-C2	-0.91843E-02	-0.16809E-01				DATA0064
-0.26659E-C1	-0.37950E-C1	-0.49970E-01	-0.61872E-01	-0.73142E-01					DATA0065
0.28838E-01	0.29028E-01	0.29055E-01	0.29179E-01	0.29315E-01	0.29452E-01				DATA0066
0.29572E-01	0.29644E-01	0.29661E-01	0.29630E-01	0.29554E-01					DATA0067
0.0	-0.53766E-C4	-0.10352E-03	-0.23308E-03	-0.41699E-03	-0.58510E-03				DATA0068
-0.71476E-C3	-0.78626E-C3	-0.80295E-03	-0.77788E-C3	-0.72129E-03					DATA0069
0.0	0.13814E+00	0.27322E+00	0.37629E+00	0.40968E+00	0.35495E+00				DATA0070
0.21551E+00	0.12192E-01	-0.23014E+00	-0.49140E+00	-0.75705E+00					DATA0071
0.0	0.63863E-01	0.22856E+00	0.50534E+00	0.93759E+00	0.15260E+01				DATA0072

0.22362E+01	0.30320E+01	0.38752E+01	0.47389E+01	0.56075E+01			DATA0073
0.90778E-02	0.93612E-02	0.87107E-02	0.52225E-02	-0.39969E-03	-0.64671E-02		DATA0074
-0.11715E-01	-0.15082E-01	-0.16982E-01	-0.17683E-01	-0.17663E-01			DATA0075
0.0	0.81963E-02	0.13524E-01	0.22872E-01	0.34064E-01	0.43729E-01		DATA0076
0.50693E-01	0.54895E-01	0.57104E-01	0.57871E-01	0.57870E-01			DATA0077
798E.699	37453.0	136740.0	376680.0				DATA0078
0.0	0.94671E-01	0.31163E+00	0.59558E+00	0.97291E+00	0.14786E+01		DATA0079
0.21260E+01	0.28973E+01	0.37551E+01	0.46611E+01	0.55816E+01			DATA0080
0.0	0.22730E+00	0.44648E+00	0.61473E+00	0.67209E+00	0.58087E+00		DATA0081
0.33649E+00	-0.31189E-01	-0.47888E+00	-0.96805E+00	-0.14689E+01			DATA0082
0.0	0.12196E-01	0.16565E-01	0.21075E-01	0.28798E-01	0.38043E-01		DATA0083
0.47582E-01	0.54627E-01	0.59182E-01	0.61171E-01	0.61353E-01			DATA0084
0.15072E-01	0.15215E-01	0.14058E-01	0.86605E-02	-0.47470E-03	-0.11016E-01		DATA0085
-0.20858E-01	-0.27575E-01	-0.31613E-01	-0.33246E-01	-0.33377E-01			DATA0086
0.0	0.20944E+00	0.67206E+00	0.12009E+01	0.16929E+01	0.19969E+01		DATA0087
0.19371E+01	0.14438E+01	0.56983E+00	-0.55484E+00	-0.17710E+01			DATA0088
0.0	-0.66471E+00	-0.12762E+01	-0.17966E+01	-0.21002E+01	-0.20027E+01		DATA0089
-0.13642E+01	-0.18150E+00	0.14329E+01	0.33066E+01	0.52677E+01			DATA0090
0.0	0.26660E-01	0.34476E-01	0.35341E-01	0.29105E-01	0.10407E-01		DATA0091
-0.18427E-01	-0.46323E-01	-0.68326E-01	-0.79558E-01	-0.81443E-01			DATA0092
-0.45442E-01	-0.42335E-01	-0.38601E-01	-0.29705E-01	-0.92970E-02	0.23359E-01		DATA0093
0.61542E-01	0.94766E-01	0.11840E+00	0.12938E+00	0.13108E+00			DATA0094

**B.3.2 The Output Printout for the TILDYN
Program**

**The output printout is illustrated
for autorotation flight of the Bell
model in this subsection.**

BELL ROTOR AUTOROTATION FLIGHT 9-DOF U-GUST FREQ ANALYSIS & EIGEN 8/18/74

ITYPE= 1 IFLT= 1 IDOF= 9 IRES= 1 IEIGEN= 1 IFRMAG= 0

NO OF BLADES	ROH	CHORD	IR	HMAST	LOCK NO
3	1.1468001E-07	1.4000000E+01	1.2600000E+03	5.1300003E+01	3.6769247E+00

OMEGA	R	VEL	CL	CD	RANDA
4.8000000E+01	1.5000000E+02	5.0400000E+03	5.6999998E+00	6.4999983E-03	6.9999999E-01

COLLECTIVE PITCH DEL3

2.1800000E-02 -2.6179999E-01

WING L	WING CHOD	WING CL	WING CD	WING CMD	WING CMA
2.0050000E+02	6.2179993E+01	5.6999998E+00	4.0000007E-03	-5.0000001E-02	0.0

DISTANCE AC EA WING ALPHAM

1.0000002E-02 3.0999999E-02

EIGENVALUES (NATURAL FREQUENCIES)

--(RAD/SEC)**2--

BLADE COLLECTIVE

7988.699 37453.000

BLADE CYCLIC

2389.100 4143.398

WING
 277.680 890.840 2730.000

-- RAD/SEC/OMEGA --

BLADE COLLECTIVE/OMEGA
 1.862 4.032

BLADE CYCLIC/OMEGA
 1.016 1.341

WING/OMEGA
 0.347 0.622 1.089

EXCITING FORCE COMPONENTS

U GUST	V GUST	W GUST	THETA 0	THETA 1C	THETA 1S
1.000000E+00	0.0	0.0	0.0	0.0	0.0

***** BLADE MODE SHAPES *****

--- COLLECTIVE MODES ---

I=1

J	XX(J)	V(I,J)	DV(I,J)	W(I,J)	DW(I,J)
1	0.0	0.0	0.1507200E-01	0.0	0.0
2	0.1000000E+00	0.2273000E+00	0.1521500E-01	0.9467101E-01	0.1219600E-01
3	0.2000000E+00	0.4464800E+00	0.1405800E-01	0.3116300E+00	0.1656500E-01
4	0.3000001E+00	0.6147300E+00	0.8660499E-02	0.5955800E+00	0.2107500E-01
5	0.4000001E+00	0.6720900E+00	-0.4747000E-03	0.9729100E+00	0.2879800E-01
6	0.5000001E+00	0.5808700E+00	-0.1101600E-01	0.1478600E+01	0.3804300E-01
7	0.6000001E+00	0.3364900E+00	-0.2085800E-01	0.2126000E+01	0.4758200E-01
8	0.7000002E+00	-0.3118900E-01	-0.2757500E-01	0.2897300E+01	0.5462700E-01
9	0.8000002E+00	-0.4788800E+00	-0.3161300E-01	0.3755100E+01	0.5918200E-01
10	0.9000002E+00	-0.9680500E+00	-0.3324600E-01	0.4661100E+01	0.6117100E-01
11	0.1000000E+01	-0.1468900E+01	-0.3337700E-01	0.5581600E+01	0.6135300E-01

I=2

J	XX(J)	V(I,J)	DV(I,J)	W(I,J)	DW(I,J)
1	0.0	0.0	-0.4544200E-01	0.0	0.0
2	0.1000000E+00	-0.6647100E+00	-0.4233500E-01	0.2094400E+00	0.2666300E-01
3	0.2000000E+00	-0.1276200E+01	-0.3860100E-01	0.6720600E+00	0.3447600E-01
4	0.3000001E+00	-0.1796600E+01	-0.2970500E-01	0.1200900E+01	0.3534100E-01
5	0.4000001E+00	-0.2100200E+01	-0.9296998E-02	0.1692900E+01	0.2910500E-01
6	0.5000001E+00	-0.2002700E+01	0.2335900E-01	0.1996900E+01	0.1040700E-01
7	0.6000001E+00	-0.1364200E+01	0.6154200E-01	0.1937100E+01	-0.1842700E-01
8	0.7000002E+00	-0.1815000E+00	0.9476602E-01	0.1443800E+01	-0.4632300E-01
9	0.8000002E+00	0.1432900E+01	0.1184000E+00	0.5698300E+00	-0.6932600E-01
10	0.9000002E+00	0.3306600E+01	0.1293800E+00	-0.5548400E+00	-0.7955801E-01
11	0.1000000E+01	0.5267700E+01	0.1310800E+00	-0.1771000E+01	-0.8144301E-01

--- CYCLIC MODES ---

I=1

J	XX(J)	V(I,J)	DV(I,J)	W(I,J)	DW(I,J)
1	0.0	0.0	0.2930400E-01	0.0	0.2883800E-01
2	0.1000000E+00	-0.4232700E-03	-0.5376599E-04	0.4340600E+00	0.2902800E-01
3	0.2000000E+00	-0.1625100E-02	-0.1035200E-03	0.8700100E+00	0.2909500E-01
4	0.3000001E+00	-0.4211001E-02	-0.2330800E-03	0.1307100E+01	0.2917900E-01
5	0.4000001E+00	-0.9184301E-02	-0.4169899E-03	0.1745900E+01	0.2931500E-01
6	0.5000001E+00	-0.1680900E-01	-0.5850999E-03	0.2186700E+01	0.2945200E-01
7	0.6000001E+00	-0.2665900E-01	-0.7147600E-03	0.2629500E+01	0.2957200E-01
8	0.7000002E+00	-0.3799000E-01	-0.7862600E-03	0.3073700E+01	0.2964400E-01
9	0.8000002E+00	-0.4997000E-01	-0.8029500E-03	0.3518600E+01	0.2966100E-01
10	0.9000002E+00	-0.6187200E-01	-0.7778800E-03	0.3963300E+01	0.2963000E-01
11	0.1000000E+01	-0.7314199E-01	-0.7212900E-03	0.4407200E+01	0.2955400E-01

I=2

J	XX(J)	V(I,J)	DV(I,J)	W(I,J)	DW(I,J)
1	0.0	0.0	0.1507200E-01	0.0	0.9077799E-02
2	0.1000000E+00	0.6386298E-01	0.8196302E-02	0.1381400E+00	0.9361200E-02
3	0.2000000E+00	0.2285600E+00	0.1352400E-01	0.2733200E+00	0.8710701E-02
4	0.3000001E+00	0.5053400E+00	0.2287200E-01	0.3762900E+00	0.5222499E-02
5	0.4000001E+00	0.9375900E+00	0.3406400E-01	0.4096800E+00	-0.3996899E-03
6	0.5000001E+00	0.1526000E+01	0.4372900E-01	0.3549500E+00	-0.6467100E-02
7	0.6000001E+00	0.2238200E+01	0.5069300E-01	0.2155100E+00	-0.1171500E-01
8	0.7000002E+00	0.3033000E+01	0.5489500E-01	0.1219300E-01	-0.1508200E-01
9	0.8000002E+00	0.3875200E+01	0.5710400E-01	-0.2301400E+00	-0.1698200E-01
10	0.9000002E+00	0.4738900E+01	0.5787100E-01	-0.4914000E+00	-0.1768300E-01
11	0.1000000E+01	0.5607500E+01	0.5787000E-01	-0.7570500E+00	-0.1766300E-01

J	XX(J)	THETN(J)	AMASS(J)
1	0.0	0.6807000E+00	0.6992999E-02
2	0.1000000E+00	0.5585000E+00	0.5438998E-02
3	0.2000000E+00	0.4363000E+00	0.3108000E-02
4	0.3000001E+00	0.3054000E+00	0.1295000E-02
5	0.4000001E+00	0.2094000E+00	0.1336000E-02
6	0.5000001E+00	0.1222000E+00	0.1465000E-02
7	0.6000001E+00	0.6980002E-01	0.1165000E-02
8	0.7000002E+00	0.2620000E-01	0.1036000E-02
9	0.8000002E+00	-0.1750000E-01	0.9711999E-03
10	0.9000002E+00	-0.6110000E-01	0.8417000E-03
11	0.1000000E+01	-0.1047000E+00	0.7120001E-03

***** WING MODE SHAPES *****

II=1

J	WX(J)	G(II,J)	DG(II,J)	Z(II,J)	DZ(II,J)	WPHI(II,J)	DWPHI(II,J)
1	0.0	0.0	0.0	0.0	0.0	0.0	0.4732900E-06
2	0.2050000E+00	0.1096400E-01	0.5154600E-03	-0.4118299E-09	-0.1607730E-10	0.1781600E-04	0.5895200E-06
3	0.3100000E+00	0.2995000E-01	0.1275100E-02	-0.7596199E-09	-0.1562300E-10	0.6824800E-04	0.2253000E-05
4	0.4150000E+00	0.6378102E-01	0.1929200E-02	-0.1020700E-08	-0.8398300E-11	0.1220900E-03	0.2538300E-05
5	0.5200000E+00	0.1102400E+00	0.2477900E-02	-0.1089800E-08	0.2030700E-11	0.1765100E-03	0.2587200E-05
6	0.6250001E+00	0.1671200E+00	0.2921500E-02	-0.9396299E-09	0.1186200E-10	0.2310300E-03	0.2595400E-05
7	0.7300001E+00	0.2322100E+00	0.3260800E-02	-0.6202701E-09	0.1762999E-10	0.2855700E-03	0.2596600E-05
8	0.8350001E+00	0.3033500E+00	0.3496800E-02	-0.2455800E-09	0.1680700E-10	0.3400999E-03	0.2596600E-05
9	0.9270001E+00	0.3689400E+00	0.3620500E-02	0.5387500E-11	0.9286000E-11	0.3878800E-03	0.2596400E-05
10	0.1000000E+01	0.4221900E+00	0.3667900E-02	0.6504600E-10	-0.1889700E-11	0.4257800E-03	0.2596200E-05

II=2

J	WX(J)	G(II,J)	DG(II,J)	Z(II,J)	DZ(II,J)	WPHI(II,J)	DWPHI(II,J)
1	0.0	0.0	0.0	0.0	0.0	0.0	0.1334300E-13
2	0.2050000E+00	-0.1165900E-08	-0.4099600E-10	0.1734000E-01	0.8156600E-03	0.4967200E-12	0.1594000E-13
3	0.3100000E+00	-0.1780400E-08	-0.1078400E-10	0.4120900E-01	0.1443200E-02	0.1793500E-11	0.5271500E-13
4	0.4150000E+00	-0.1508700E-08	0.3577701E-10	0.7735699E-01	0.1985200E-02	0.2899200E-11	0.4211900E-13
5	0.5200000E+00	-0.4287499E-09	0.6140199E-10	0.1239900E+00	0.2441800E-02	0.3564300E-11	0.1910500E-13
6	0.6250001E+00	0.7976899E-09	0.4901700E-10	0.1793200E+00	0.2813300E-02	0.3702600E-11	-0.5992701E-14
7	0.7300001E+00	0.1419700E-08	0.7251000E-11	0.2415600E+00	0.3100500E-02	0.3337800E-11	-0.2798000E-13
8	0.8350001E+00	0.1085300E-08	-0.3688000E-10	0.3089500E+00	0.3304100E-02	0.2569000E-11	-0.4423900E-13
9	0.9270001E+00	0.2516400E-09	-0.4400000E-10	0.3708600E+00	0.3415300E-02	0.1663800E-11	-0.5336100E-13
10	0.1000000E+01	-0.1154600E-09	0.2109300E-11	0.4211100E+00	0.3461900E-02	0.8527400E-12	-0.5725298E-13

II=3

J	WX(J)	G(II,J)	DG(II,J)	Z(II,J)	DZ(II,J)	WPHI(II,J)	DWPHI(II,J)
1	0.0	0.0	0.0	0.0	0.0	0.0	-0.1426300E-04
2	0.2050000E+00	0.3132000E-02	0.1483400E-03	0.1067600E-05	0.4164300E-07	-0.5369100E-03	-0.1776501E-04
3	0.3100000E+00	0.8682501E-02	0.3762899E-03	0.1967300E-05	0.4036200E-07	-0.2056600E-02	-0.6788599E-04
4	0.4150000E+00	0.1877000E-01	0.5805099E-03	0.2640400E-05	0.2158000E-07	-0.3678700E-02	-0.7646299E-04
5	0.5200000E+00	0.3290200E-01	0.7616801E-03	0.2816000E-05	-0.5406800E-08	-0.5317800E-02	-0.7790100E-04
6	0.6250001E+00	0.5060800E-01	0.9210201E-03	0.2425000E-05	-0.3075600E-07	-0.6958999E-02	-0.7810400E-04
7	0.7300001E+00	0.7144600E-01	0.1060400E-02	0.1598700E-05	-0.4554900E-07	-0.8599602E-02	-0.7878300E-04
8	0.8350001E+00	0.9502703E-01	0.1182800E-02	0.6317900E-06	-0.4332400E-07	-0.1023900E-01	-0.7801200E-04
9	0.9270001E+00	0.1177000E+00	0.1282100E-02	-0.1453600E-07	-0.2388700E-07	-0.1167300E-01	-0.7793400E-04
10	0.1000000E+01	0.1370300E+00	0.1366400E-02	-0.1678000E-06	0.4879001E-08	-0.1281100E-01	-0.7786400E-04

 EQUATIONS OF MOTION : $A \cdot X'' + B \cdot X' + C \cdot X = D \cdot E$

A MATRIX=

0.10000E+01	0.0	0.0	0.0	0.0	0.0	0.0	0.20516E-10	0.13282E+00	-0.52925E-07	0.23958E+00
0.0	0.10000E+01	0.0	0.0	0.0	0.0	0.0	-0.14719E-01	-0.98082E-05	0.44288E+00	0.0
0.0	0.0	0.10000E+01	0.0	0.0	0.0	0.0	-0.24523E-04	0.11968E+00	0.28897E-04	0.0
0.0	0.0	0.0	0.10000E+01	0.0	0.0	0.0	0.13386E-10	0.86664E-01	-0.34533E-07	-0.79480E+00
0.0	0.0	0.0	0.0	0.10000E+01	0.0	0.0	-0.25539E-03	-0.56142E-01	0.76842E-02	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.10000E+01	-0.14037E+00	0.20765E-02	0.16444E+00	0.0
0.61547E-10	-0.22079E-01	-0.36785E-04	0.40159E-10	-0.38309E-03	-0.21055E+00	0.10000E+01	0.10000E+01	0.0	0.0	0.0
0.39846E+00	-0.14712E-04	0.17952E+00	0.25999E+00	-0.84213E-01	0.31148E-02	0.0	0.0	0.10000E+01	0.0	0.0
-0.15877E-06	0.66432E+00	0.43345E-04	-0.10360E-06	0.11526E-01	0.24666E+00	0.0	0.0	0.0	0.10000E+01	0.0
0.71574E+00	0.0	0.0	-0.23844E+01	0.0	0.0	0.0	0.0	0.0	0.0	0.37800E+04

B MATRIX=

0.54017E+00	0.0	0.0	-0.26876E+00	0.0	0.0	0.0	0.69574E-11	0.45043E-01	-0.17948E-07	-0.13242E+02
0.0	0.37042E+00	0.20000E+01	0.0	-0.41167E+00	0.0	0.0	-0.53078E-02	0.25859E+00	0.15970E+00	0.0
0.0	-0.20000E+01	0.37042E+00	0.0	0.0	-0.41167E+00	0.0	0.77536E-01	0.43156E-01	-0.94210E+00	0.0
-0.19099E+00	0.0	0.0	0.43642E+00	0.0	0.0	0.0	0.17233E-11	0.11157E-01	-0.44457E-08	-0.23007E+00
0.0	-0.34603E+00	0.0	0.0	0.39483E+00	0.20000E+01	0.0	0.49567E-02	-0.14325E-01	-0.14914E+00	0.0
0.0	0.0	-0.34603E+00	0.0	-0.20000E+01	0.39483E+00	0.0	-0.45688E-01	-0.40302E-01	0.38752E-01	0.0
0.22544E-10	-0.79814E-02	0.25224E-01	-0.21837E-12	0.88643E-02	-0.66846E-01	0.0	0.32997E-01	0.67399E-02	-0.18602E-01	-0.71542E-09
0.14595E+00	-0.33128E+00	0.64894E-01	-0.14137E-02	-0.32659E-01	-0.72073E-01	0.0	0.85543E-02	0.28552E-01	0.22520E-02	-0.46317E+01
-0.58157E-07	0.24015E+00	0.12474E+01	0.56333E-09	-0.26671E+00	0.10046E+00	0.0	-0.18944E-01	0.21209E-02	0.12854E+00	0.18456E-05
-0.33172E+02	0.0	0.0	-0.33280E+01	0.0	0.0	0.0	-0.68859E-09	-0.44580E+01	0.17764E-05	0.11459E+04

C MATRIX=

0.34673E+01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	-0.14993E+00	0.37042E+00	0.0	-0.57593E-01	-0.41167E+00	0.21493E-10	-0.39374E-01	-0.55495E-07	0.0	0.0
0.0	-0.37042E+00	-0.14993E+00	0.0	0.41167E+00	-0.57593E-01	-0.48426E-02	-0.96987E-11	0.14571E+00	0.0	0.0
0.0	0.0	0.0	0.16256E+02	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.17862E+00	-0.34603E+00	0.0	0.85458E+00	0.39483E+00	-0.20644E-10	0.37820E-01	0.53304E-07	0.0	0.0
0.0	0.34603E+00	0.17862E+00	0.0	-0.39483E+00	0.85458E+00	0.46514E-02	0.93158E-11	-0.13995E+00	0.0	0.0
0.0	-0.65434E-01	0.36719E-01	0.0	0.67322E-01	0.22616E-01	0.11688E+00	0.85114E-03	0.10968E+00	0.0	0.0
0.0	-0.95611E-01	-0.43438E-02	0.0	0.62958E-01	-0.36532E-01	-0.82583E-03	0.38097E+00	0.24848E-01	0.0	0.0
0.0	-0.37486E-01	0.33214E+00	0.0	-0.11480E+00	-0.22815E+00	0.14950E-02	-0.25609E-01	0.11399E+01	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

D MATRIX=

0.0	0.0	-0.11231E+02	0.24135E+02	0.0	0.0
0.0	0.11374E+02	0.0	0.0	0.23678E+02	0.0
-0.11374E+02	0.0	0.0	0.0	0.0	0.23678E+02
0.0	0.0	-0.27819E+01	0.37430E+01	0.0	0.0
0.0	-0.10925E+02	0.0	0.0	-0.23117E+02	0.0
0.10925E+02	0.0	0.0	0.0	0.0	-0.23117E+02
-0.10349E+02	-0.24586E+00	0.38116E+00	0.14824E-08	-0.51082E+00	-0.57982E+01
-0.22047E+01	0.16228E+01	-0.45530E+01	0.95973E+01	0.25721E+01	0.41534E+01
0.29504E+01	0.73975E+01	0.37122E+00	-0.38242E-05	0.15370E+02	-0.11503E+02
0.0	0.0	0.15879E+04	-0.23930E+04	0.0	0.0

FREQUENCY RESPONSE

--FREQUENCY/OMEGA--

	Q1D	Q1C	Q1S	Q20	Q2C	Q2S	WING 1	WING 2	WING 3
	D(NU R)/DT								
-- 0.01--	0.188E-06	0.772E+00	0.304E+00	0.549E-07	0.476E-01	0.243E-01	0.162E+00	0.518E-03	0.527E-02
	0.959E-05								
-- 0.02--	0.473E-06	0.771E+00	0.304E+00	0.114E-06	0.486E-01	0.480E-01	0.162E+00	0.531E-03	0.584E-02
	0.196E-04								
-- 0.03--	0.921E-06	0.769E+00	0.305E+00	0.180E-06	0.505E-01	0.719E-01	0.164E+00	0.553E-03	0.667E-02
	0.306E-04								
-- 0.04--	0.159E-05	0.766E+00	0.307E+00	0.259E-06	0.534E-01	0.959E-01	0.165E+00	0.584E-03	0.767E-02
	0.429E-04								
-- 0.05--	0.252E-05	0.762E+00	0.308E+00	0.355E-06	0.576E-01	0.120E+00	0.167E+00	0.623E-03	0.878E-02
	0.570E-04								
-- 0.06--	0.379E-05	0.758E+00	0.311E+00	0.473E-06	0.633E-01	0.145E+00	0.170E+00	0.670E-03	0.994E-02
	0.732E-04								

-- 0.07--

0.548E-05 0.753E+00 0.314E+00 0.619E-06 0.708E-01 0.170E+00 0.173E+00 0.726E-03 0.111E-01
0.920E-04

-- 0.08--

0.766E-05 0.746E+00 0.317E+00 0.798E-06 0.802E-01 0.195E+00 0.177E+00 0.790E-03 0.123E-01
0.114E-03

-- 0.09--

0.104E-04 0.739E+00 0.321E+00 0.102E-05 0.918E-01 0.220E+00 0.181E+00 0.862E-03 0.135E-01
0.139E-03

-- 0.10--

0.140E-04 0.731E+00 0.326E+00 0.129E-05 0.106E+00 0.246E+00 0.186E+00 0.944E-03 0.147E-01
0.167E-03

-- 0.12--

0.237E-04 0.710E+00 0.338E+00 0.203E-05 0.140E+00 0.300E+00 0.198E+00 0.114E-02 0.170E-01
0.237E-03

-- 0.14--

0.384E-04 0.685E+00 0.354E+00 0.312E-05 0.186E+00 0.356E+00 0.213E+00 0.138E-02 0.192E-01
0.329E-03

-- 0.16--

0.602E-04 0.652E+00 0.373E+00 0.474E-05 0.243E+00 0.414E+00 0.231E+00 0.169E-02 0.212E-01
0.449E-03

-- 0.18--	0.921E-04	0.610E+00	0.396E+00	0.713E-05	0.312E+00	0.473E+00	0.253E+00	0.208E-02	0.229E-01
	0.608E-03								
-- 0.20--	0.139E-03	0.558E+00	0.420E+00	0.107E-04	0.391E+00	0.530E+00	0.278E+00	0.259E-02	0.242E-01
	0.820E-03								
-- 0.22--	0.206E-03	0.495E+00	0.444E+00	0.158E-04	0.476E+00	0.579E+00	0.309E+00	0.325E-02	0.253E-01
	0.110E-02								
-- 0.24--	0.302E-03	0.425E+00	0.462E+00	0.232E-04	0.562E+00	0.617E+00	0.348E+00	0.407E-02	0.259E-01
	0.146E-02								
-- 0.26--	0.437E-03	0.355E+00	0.475E+00	0.338E-04	0.644E+00	0.642E+00	0.401E+00	0.512E-02	0.263E-01
	0.194E-02								
-- 0.28--	0.633E-03	0.292E+00	0.484E+00	0.494E-04	0.724E+00	0.662E+00	0.484E+00	0.651E-02	0.264E-01
	0.258E-02								
-- 0.30--	0.944E-03	0.239E+00	0.500E+00	0.745E-04	0.822E+00	0.694E+00	0.635E+00	0.861E-02	0.242E-01
	0.355E-02								
-- 0.32--	0.154E-02	0.183E+00	0.540E+00	0.123E-03	0.987E+00	0.784E+00	0.967E+00	0.125E-01	0.242E-01
	0.536E-02								

-- 0.34--	0.268E-02	0.209E+00	0.569E+00	0.216E-03	0.120E+01	0.932E+00	0.169E+01	0.197E-01	0.105E-01
	0.869E-02								
-- 0.36--	0.185E-02	0.375E+00	0.209E+00	0.151E-03	0.524E+00	0.438E+00	0.130E+01	0.123E-01	0.229E-01
	0.560E-02								
-- 0.38--	0.777E-03	0.360E+00	0.140E+00	0.643E-04	0.161E+00	0.158E+00	0.703E+00	0.471E-02	0.306E-01
	0.220E-02								
-- 0.40--	0.310E-03	0.346E+00	0.169E+00	0.260E-04	0.185E+00	0.116E+00	0.457E+00	0.172E-02	0.332E-01
	0.825E-03								
-- 0.45--	0.795E-03	0.331E+00	0.190E+00	0.684E-04	0.261E+00	0.116E+00	0.234E+00	0.359E-02	0.377E-01
	0.182E-02								
-- 0.50--	0.210E-02	0.323E+00	0.190E+00	0.185E-03	0.273E+00	0.107E+00	0.153E+00	0.785E-02	0.430E-01
	0.417E-02								
-- 0.55--	0.569E-02	0.318E+00	0.191E+00	0.511E-03	0.269E+00	0.103E+00	0.113E+00	0.179E-01	0.524E-01
	0.990E-02								
-- 0.60--	0.344E-01	0.237E+00	0.147E+00	0.314E-02	0.211E+00	0.197E+00	0.919E-01	0.920E-01	0.847E-01
	0.528E-01								

-- 2.50--

0.501E-02 0.408E-01 0.389E-01 0.105E-02 0.273E+00 0.299E+00 0.496E-02 0.105E-02 0.468E-01
0.587E-03

-- 2.60--

0.364E-02 0.463E-01 0.644E-01 0.913E-03 0.194E+00 0.225E+00 0.308E-02 0.811E-03 0.305E-01
0.385E-03

-- 2.70--

0.262E-02 0.470E-01 0.694E-01 0.781E-03 0.139E+00 0.170E+00 0.219E-02 0.617E-03 0.200E-01
0.249E-03

-- 2.80--

0.196E-02 0.436E-01 0.667E-01 0.694E-03 0.105E+00 0.134E+00 0.182E-02 0.485E-03 0.138E-01
0.167E-03

-- 2.90--

0.153E-02 0.392E-01 0.619E-01 0.640E-03 0.820E-01 0.110E+00 0.164E-02 0.393E-03 0.992E-02
0.115E-03

-- 3.00--

0.122E-02 0.350E-01 0.568E-01 0.608E-03 0.662E-01 0.923E-01 0.154E-02 0.326E-03 0.737E-02
0.796E-04

-- 3.50--

0.539E-03 0.201E-01 0.375E-01 0.674E-03 0.298E-01 0.495E-01 0.123E-02 0.156E-03 0.219E-02
0.758E-05

-- 4.00--

0.420E-03	0.125E-01	0.265E-01	0.135E-02	0.169E-01	0.324E-01	0.993E-03	0.999E-04	0.798E-03
0.646E-04								

-- 4.50--

0.227E-03	0.840E-02	0.199E-01	0.492E-03	0.107E-01	0.234E-01	0.807E-03	0.745E-04	0.319E-03
0.331E-04								

-- 5.00--

0.140E-03	0.592E-02	0.155E-01	0.203E-03	0.733E-02	0.178E-01	0.665E-03	0.503E-04	0.174E-03
0.155E-04								

-- 5.50--

0.979E-04	0.435E-02	0.125E-01	0.113E-03	0.526E-02	0.141E-01	0.556E-03	0.366E-04	0.156E-03
0.928E-05								

-- 6.00--

0.727E-04	0.329E-02	0.103E-01	0.731E-04	0.392E-02	0.115E-01	0.471E-03	0.278E-04	0.159E-03
0.626E-05								

-- 6.50--

0.561E-04	0.256E-02	0.861E-02	0.513E-04	0.301E-02	0.959E-02	0.404E-03	0.218E-04	0.159E-03
0.456E-05								

-- 7.00--

0.446E-04	0.203E-02	0.734E-02	0.380E-04	0.236E-02	0.812E-02	0.350E-03	0.176E-04	0.152E-03
0.350E-05								

-- 7.50--

0.362E-04 0.164E-02 0.633E-02 0.294E-04 0.189E-02 0.698E-02 0.306E-03 0.144E-04 0.144E-03
0.279E-05

-- 8.00--

0.300E-04 0.134E-02 0.552E-02 0.234E-04 0.154E-02 0.606E-02 0.269E-03 0.121E-04 0.135E-03
0.230E-05

-- 8.50--

0.252E-04 0.112E-02 0.485E-02 0.191E-04 0.127E-02 0.532E-02 0.239E-03 0.102E-04 0.125E-03
0.194E-05

-- 9.00--

0.215E-04 0.938E-03 0.431E-02 0.159E-04 0.106E-02 0.471E-02 0.214E-03 0.876E-05 0.116E-03
0.167E-05

-- 9.50--

0.185E-04 0.796E-03 0.385E-02 0.134E-04 0.895E-03 0.420E-02 0.192E-03 0.759E-05 0.107E-03
0.146E-05

-- 10.00--

0.162E-04 0.682E-03 0.346E-02 0.115E-04 0.763E-03 0.377E-02 0.174E-03 0.664E-05 0.992E-04
0.130E-05

EIGENVALUES

	** REAL PART **	** IMAGINARY PART ***	** DAMPING RATIO **
NO. 1	0.0	0.0	0.0
NO. 2	-0.2092248D+00	0.4071266D+01	0.5132288E-01
NO. 2	-0.2092248D+00	-0.4071266D+01	0.5132288E-01
NO. 3	-0.1481056D+00	0.2421839D+01	0.6104013E-01
NO. 3	-0.1481056D+00	-0.2421839D+01	0.6104013E-01
NO. 4	-0.2021002D+00	0.1945624D+01	0.1033183E+00
NO. 4	-0.2021002D+00	-0.1945624D+01	0.1033183E+00
NO. 5	-0.2632103D+00	0.1875147D+01	0.1390050E+00
NO. 5	-0.2632103D+00	-0.1875147D+01	0.1390050E+00
NO. 6	-0.3342787D-01	0.1260777D+01	0.2650439E-01
NO. 6	-0.3342787D-01	-0.1260777D+01	0.2650439E-01
NO. 7	-0.1144592D-01	0.6041955D+00	0.1894066E-01
NO. 7	-0.1144592D-01	-0.6041955D+00	0.1894066E-01
NO. 8	-0.1537569D-01	0.3459382D+00	0.4440252E-01
NO. 8	-0.1537569D-01	-0.3459382D+00	0.4440252E-01
NO. 9	-0.1094665D+00	0.2452122D+00	0.4076408E+00
NO. 9	-0.1094665D+00	-0.2452122D+00	0.4076408E+00
NO.10	-0.2820982D+00	0.4124979D-01	0.9894778E+00
NO.10	-0.2820982D+00	-0.4124979D-01	0.9894778E+00
NO.11	-0.3179021D+00	0.0	0.1000000E+01

EIGENVECTORS

-- CORRESPONDING TO NO. 1 EIGENVALUE -- (0.0)+IMAG(0.0)

** ABSOLUTE VALUE ** ** REAL PART ** ** IMAGINARY PART **

0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.100000E+01	0.100000E+01	0.0

-- CORRESPONDING TO NO. 2 EIGENVALUE -- (-0.209D+00)+IMAG(0.407D+01)

** ABSOLUTE VALUE ** ** REAL PART ** ** IMAGINARY PART **

0.1107064E+00	0.5960987E-01	-0.9328753E-01
0.4401162E-02	0.4983202E-03	-0.4372858E-02
0.3052047E-01	0.3021199E-01	-0.4328273E-02
0.1000000E+01	0.1000000E+01	0.0
0.2562390E-01	-0.2548093E-01	0.2702991E-02
0.1051418E-01	0.2121001E-02	0.1029802E-01
0.1073238E-03	0.3453433E-04	0.1016158E-03
0.1779419E-01	-0.1765273E-01	0.2239201E-02
0.5262852E-02	0.1084798E-02	0.5149834E-02
0.1380952E-01	0.1266621E-01	-0.5501822E-02

-- CORRESPONDING TO NO. 3 EIGENVALUE --

(-0.148D+00)+IMAG(0.242D+01)

** ABSOLUTE VALUE **

** REAL PART **

** IMAGINARY PART **

0.1813177E-01
0.4931911E+00
0.3320159E+00
0.3046985E-02
0.9230196E+00
0.1000000E+01
0.1226842E-01
0.3355967E-02
0.1654489E+00
0.9685631E-03

0.5256832E-02
0.4925372E+00
-0.2398358E-01
0.5288171E-03
0.5510997E-02
0.1000000E+01
0.1224252E-01
-0.1360433E-03
-0.1650685E+00
-0.8815918E-03
-0.1735301E-01
-0.2539496E-01
-0.3311487E+00
0.3000749E-02
0.9230042E+00
0.0
-0.7968692E-03
0.3353212E-02
0.1121332E-01
-0.4011374E-03

-- CORRESPONDING TO NO. 4 EIGENVALUE --

(-0.202D+00)+IMAG(0.195D+01)

** ABSOLUTE VALUE **

** REAL PART **

** IMAGINARY PART **

0.2562918E-01
0.1000000E+01
0.9137043E+00
0.1247240E-02
0.3160684E+00
0.3624439E+00
0.4554648E-02
0.1546631E-02
0.1053016E+00
0.2736067E-02

0.2539718E-01
0.1000000E+01
-0.5365834E-01
-0.8799934E-03
-0.2004018E+00
0.2816455E+00
0.4206777E-02
-0.1443410E-02
-0.9349859E-01
0.7346331E-03
0.4704274E-02
0.0
-0.9121275E+00
0.8838666E-03
0.2444144E+00
0.2281262E+00
0.1745808E-02
0.5555502E-03
-0.4844000E-01
-0.2635599E-02

-- CORRESPONDING TO NO. 5 EIGENVALUE --

(-0.2630+00)+IMAG(0.1880+01)

** ABSOLUTE VALUE **

** REAL PART ** ** IMAGINARY PART **

0.1000000E+01
0.9817582E-01
0.5672661E-01
0.3115343E-01
0.1848055E-01
0.5520776E-01
0.6100570E-03
0.2630625E-01
0.4581391E-01
0.1181544E+00

0.1000000E+01 0.0
-0.7606643E-01 -0.6206755E-01
0.2192894E-01 0.5231665E-01
-0.1489975E-01 0.2735936E-01
0.1686821E-01 0.7549502E-02
0.1644658E-02 -0.5518328E-01
0.7883347E-04 -0.6049422E-03
-0.2571483E-01 0.5546831E-02
0.2269105E-01 0.3979991E-01
-0.8819941E-03 -0.1181511E+00

-- CORRESPONDING TO NO. 6 EIGENVALUE --

(-0.3340-01)+IMAG(0.1260+01)

** ABSOLUTE VALUE **

** REAL PART ** ** IMAGINARY PART **

0.5219237E-01
0.1000000E+01
0.3072107E+00
0.4124053E-02
0.5034070E+00
0.2649921E+00
0.1200790E-01
0.2355482E-01
0.7685637E+00
0.1921409E-01

-0.4088937E-01 -0.3243618E-01
0.1000000E+01 0.0
0.1548536E+00 -0.2653276E+00
-0.1214229E-02 -0.3941245E-02
-0.2209883E+00 -0.4523084E+00
-0.9316647E-01 0.2480742E+00
-0.9718515E-02 0.7052649E-02
-0.9464018E-02 -0.2156994E-01
-0.7237886E+00 0.2584966E+00
-0.1733962E-01 0.8277591E-02

-- CORRESPONDING TO NO. 7 EIGENVALUE --

(-0.114D-01)+IMAG(0.604D+00)

** ABSOLUTE VALUE **

** REAL PART ** ** IMAGINARY PART **

0.1899540E+00
0.7186074E+00
0.1000000E+01
0.1727831E-01
0.3531273E+00
0.6229418E+00
0.5332358E-01
0.5013081E+00
0.3995003E+00
0.4824777E+00

-0.9512359E-01 0.1644202E+00
-0.1414695E+00 0.7045444E+00
0.1000000E+01 0.0
-0.1256843E-01 0.1185641E-01
0.1046424E+00 -0.3372667E+00
-0.2424563E+00 -0.5738217E+00
-0.2112583E-01 -0.4896023E-01
-0.3956270E+00 0.3078783E+00
-0.2640249E+00 -0.2998188E+00
0.1262509E+00 0.4656667E+00

-- CORRESPONDING TO NO. 8 EIGENVALUE --

(-0.154D-01)+IMAG(0.346D+00)

** ABSOLUTE VALUE **

** REAL PART ** ** IMAGINARY PART **

0.1800445E-02
0.2911242E+00
0.4352518E+00
0.1424049E-03
0.0451266E+00
0.6462139E+00
0.1000000E+01
0.1269024E-01
0.2067884E-01
0.1675373E-01

0.6788953E-03 0.1667545E-02
0.2866872E+00 0.5063349E-01
0.4194663E+00 -0.1161560E+00
0.4478541E-04 0.1351793E-03
0.5476120E+00 -0.6437076E+00
0.1607376E+00 0.6259041E+00
0.1000000E+01 0.0
0.1486531E-02 0.1260288E-01
-0.9552781E-02 0.1834010E-01
0.1418500E-01 0.8914784E-02

-- CORRESPONDING TO NO. 9 EIGENVALUE --

(-0.109D+00)+IMAG(0.245D+00)

** ABSOLUTE VALUE **

** REAL PART ** ** IMAGINARY PART **

0.2434947E-03
0.5692835E+00
0.5258981E+00
0.1357527E-04
0.9552389E+00
0.1000000E+01
0.8736736E-01
0.2355762E-02
0.8463684E-02
0.4402682E-02

0.8291703E-04
-0.5446492E+00
0.9681088E-01
0.4603972E-05
-0.1093801E-01
0.1000000E+01
-0.8715111E-01
0.1651092E-02
0.7221349E-02
0.4384559E-02
0.2289419E-03
-0.1656526E+00
-0.5169105E+00
0.1277072E-04
-0.9551762E+00
0.0
0.6141596E-02
0.1680330E-02
-0.4414298E-02
-0.3990191E-03

-- CORRESPONDING TO NO.10 EIGENVALUE --

(-0.282D+00)+IMAG(0.412D-01)

** ABSOLUTE VALUE **

** REAL PART ** ** IMAGINARY PART **

0.2436394E-02
0.1000000E+01
0.9246252E+00
0.1798500E-04
0.6785136E+00
0.4797139E+00
0.4522312E-01
0.5225778E-02
0.3273904E-01
0.5858627E-01

-0.2435637E-02
0.1000000E+01
-0.2559280E+00
-0.9399982E-05
-0.5765943E+00
-0.2741120E+00
0.4180256E-01
0.2554759E-02
-0.2485351E-01
0.5792243E-01
0.6074352E-04
0.0
-0.8885002E+00
-0.1533299E-04
-0.3576586E+00
0.3936852E+00
0.1725332E-01
0.4558720E-02
0.2131075E-01
0.8794524E-02

-- CORRESPONDING TO NO.11 EIGENVALUE --

(-0.318D+00)+IMAG(0.0)

** ABSOLUTE VALUE **

** REAL PART **

** IMAGINARY PART **

0.4641774E-01
0.1062824E+00
0.5789774E-01
0.2153117E-03
0.3157100E-01
0.7271057E-01
0.3048246E-02
0.6654162E-02
0.2990245E-02
0.1000000E+01

-0.4641774E-01 0.0
0.1062824E+00 0.0
0.5789774E-01 0.0
0.2153117E-03 0.0
-0.3157100E-01 0.0
-0.7271057E-01 0.0
0.3048246E-02 0.0
-0.6654162E-02 0.0
-0.2990245E-02 0.0
0.1000000E+01 0.0