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NASA/ISC Contract NAS 9-15779 (DRD No. MA-129T)

**DESIGN ANALYSIS AND
COMPUTER-AIDED PERFORMANCE EVALUATION
OF SHUTTLE ORBITER
ELECTRICAL POWER SYSTEM**

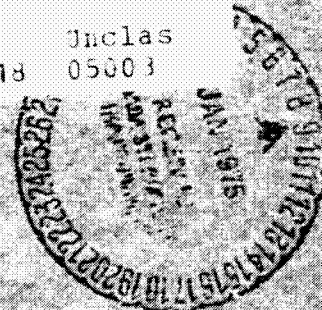


FINAL REPORT

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ELECTRICAL POWER SYSTEM**

HUGHES

HUGHES AIRCRAFT COMPANY
SPACE AND COMMUNICATIONS GROUP

FINAL REPORT

VOLUME I
SUMMARY

REPORT NO. (S)³ 74-085
DRD MA-129T

A DESIGN ANALYSIS AND COMPUTER-AIDED PERFORMANCE
EVALUATION OF THE SHUTTLE ORBITER ELECTRICAL POWER SYSTEM


FINAL CONTRACT REPORT, VOLUME I

NAS 9-13779

OCTOBER 1974

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HUGHES
HUGHES AIRCRAFT COMPANY



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ABSTRACT

This final report summarizes effort expended by Hughes Aircraft over the last ten months in the enhancement of time domain computer-simulation software¹, development of appropriate Shuttle Electrical Power Distribution and Control (EPDC) subsystem simulation models, and illustrative application of these computer simulations to systems analysis of the EPDC. The SYSTID simulation software previously developed had been utilized almost exclusively for telecommunications systems analysis, though it had more general capability. In particular, the SYSTID simulation language allows the user to generate system models of recurrent interest in a program library, which eases the mechanics of user application. The SYSTID software-related tasks addressed in this study under NAS 9-13779 included enhancement of the user utility aspects of the software, increased flexibility, conversion to the UNIVAC 1110 EXEC 8 operating system at Johnson Space Center (JSC), from its former EXEC 2 configuration and interactive graphics capability from the JSC MOPS terminals. In addition, a number of EPDC power generation (fuel cell), conversion (inverter) and control (remote power controller, remote-control circuit breaker, fuse) elements were defined and coded as SYSTID models. Similar attempts were made to characterize and code various EPDC load elements as SYSTID models. Unfortunately, due to the current state of design flux of the shuttle orbiter EPDC and user subsystems, a number of these elements (particularly the load elements) have not been defined by Rockwell International, the prime contractor. Thus, a certain amount of engineering judgement and prescience by the Hughes staff has been necessary to define the detailed electrical characteristics of these devices to a level appropriate for SYSTID coding. A corollary difficulty has been experienced, until very late in the contract effort, in defining the EPDC system topology.

¹SYSTems Time Domain (SYSTID) simulation software, previously developed by the study team under NASA/JSC contract NAS 9-11743.

Recent data obtained from JSC on the topology employed in SEPAP¹ computer-aided analysis has been employed in the final systems-oriented SYSTID simulation runs (fault/circuit protection, power profile analysis). What has been accomplished by this study is; 1) significant enhancement of the SYSTID time domain simulation software, as a general tool, which also exhibits necessary capability to effectively simulate the EPDC, 2) generation of functionally useful shuttle EPDC element models, suitable for useage with SYSTID (though, with minor modification, these models could be extended to represent other spacecraft electrical power system elements), 3) illustrative simulation results in the analysis of EPDC performance, under the conditions of fault, (lightning) current pulse injection, and circuit protection sizing and reaction times. This Volume I is complimented by the SYSTID User Guide, Volume II, and the SYSTID Data Book, Volume III.

Key words: simulation; time-domain; electrical power systems, shuttle orbiter EPS; computer simulation; spacecraft electrical power systems.

¹Shuttle Electrical Power Analysis Program (Lockheed Electronics Co.)

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GLOSSARY OF TERMS

SYSTID	SYSTems TIME Domain (SYSTID) simulation software, the basic simulation language enhanced by this contract and resident on the UNIVAC 1110, EXEC 8 operating system.
EPDC	Electrical Power, Distribution and Control subsystem.
EPS	Electrical Power System (including user loads)
RPC	Remote Power Controller, a device for remotely current-limiting overload current or turning off current to various load elements, and providing a trip signal.
RCCB	Remote Control Circuit Breaker, a device which remotely allows utilization as either/both a relay and circuit breaker.
MEC	Master Events Controller, a fail-safe pyrotechnic ignition device, driven by the computer.
MIA	Multiplexer Interface Adapters, which provide interface with computer and data buses.
PIC	Pyrotechnic (PYRO) Ignition Circuits.
IMU	Inertial Measuring Unit.
CPU	Central Processing Unit (Computer).
FC	Fuel Cell (Hydrogen-Oxygen)
D & C	Display and Control.

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1.0 SUMMARY

This study has pursued a number of objectives dealing with the refinement of computer simulation software, the generation and validation of mathematical models for subsequent reduction to computer code of certain shuttle EPDC elements and limited performance analysis of the EPDC system itself. These objectives, their scope and the technical approach employed in the study will be discussed below.

1.1 Objectives

Three primary objectives have been the basis of the contractual Statement of Work and study effort. These objectives have been: 1) enhancement of computer simulation software (SYSTID) previously developed for primary application to communications system analysis so that its user utility and flexibility would be increased and it would be made compatible with the JSC UNIVAC 1110 EXEC 8 computer system and interactive graphics terminals, 2) collection and distillation of descriptive data, generation of appropriate Shuttle electrical power and distribution (EPDC) subsystem mathematical models and subsequent coding of SYSTID models, and 3) delineation of EPDC topology and functional flow so that limited system analysis can be performed. These EPDC systems-level performance analyses include: fault analysis, inserted current (lightning) pulse sensitivity, circuit protection device validation.

These primary objectives, as well as a number of concurrent secondary objectives have been crystalized in the Statement of Work¹, as follows:

¹Excerpted from the contract document

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
<p>3.2</p> <p>3.2.1</p> <p>3.2.2</p>	<p>EPDC (EPS) ANALYSIS TASKS</p> <p>Define EPDC Load Profile</p> <p>Task Description:</p> <ul style="list-style-type: none"> ● Define baseline EPDC topology and all shuttle load interfaces ● Generate time history of loads <p>Output Expected</p> <ul style="list-style-type: none"> ● EPDC block diagram showing load interfaces ● EPDC mode summary ● Load profile versus time for each subsystem load, and if possible each load element versus time <p>Perform EPDC Redundant Switching & Circuit Protection Analysis</p> <p>Task Description:</p> <ul style="list-style-type: none"> ● Establish redundancy switching and circuit protection topology ● Generate a matrix of switched modes and protected circuits ● Evaluate the switched modes for redundancy capability <p>Output Expected:</p> <ul style="list-style-type: none"> ● Functional diagrams of redundant switching modes ● Evaluation of redundancy and circuit protection adequacy 	

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.2.3	<p>Determine EPDC Fault Conditions</p> <p>Task Description:</p> <ul style="list-style-type: none">● Define possible fault modes● Determine probable fault conditions● Select an illustrative number of fault modes for SYSTID simulation <p>Output Expected:</p> <ul style="list-style-type: none">● Matrix of possible fault modes● Sub-matrix of most probable fault modes● SYSTID simulation topology	

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
<p>3.3 3.3.1 3.3.1.1</p>	<p>COMPUTER-AIDED ANALYSIS AND SIMULATION</p> <p>Simulation Language Enhancement</p> <p>Multinode Models</p> <p><u>Present</u></p> <p>I < Model Reference (arg₁,...arg_n) or Expressions > Ø</p> <p><u>Planned</u></p> <p>I < Expression > Ø</p> <p>and</p> <p> $\left\{ \begin{array}{l} I_1 - I_2 \dots I_K < \text{Model Reference (arg}_1, \dots, \text{arg}_n) > \emptyset_1 - \emptyset \dots \emptyset_K \\ \text{or} \\ I < \text{Model Reference (I}_2, I_3 \dots I_K, \emptyset_2, \emptyset_3 \dots \emptyset_K, \text{arg}_1, \dots, \text{arg}_n) > \emptyset \end{array} \right.$ </p>	<p>selection of the form will be based upon overall software development</p>

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.1.2	<p>Simplify Expression Processing</p> <p><u>Present</u></p> <ul style="list-style-type: none"> ● Model library references (permanent and/or temporary) ● Fortran library functions ● User written Fortran functions ● Fortran arithmetic expressions involving intrinsic parameters, constants, variables, functions, and "TAPS" ● Model reference scanning for valid form and number of arguments <p><u>Planned</u></p> <ul style="list-style-type: none"> ● Fortran arithmetic expressions involving "node" names (i.e., node names become formal variable names) ● Fortran expression scanning for proper form 	

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.1.3	<p>Provide Automatic Checkpoint</p> <p><u>Present</u></p> <p>None - any checkpoint functions are provided by the user</p> <p><u>Planned</u></p> <p>Automatic checkpointing under user control keyed to the system clock's</p>	
3.3.1.4	<p>Provide Conditional Termination</p> <p>See entry under "Misc. SYSTID Enhancements"</p>	

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.1.5	<p>Provide SYSTID Table Definition</p> <p><u>Present</u></p> <p>None - Tables currently are defined within Fortran models</p> <p><u>Planned</u></p> <ul style="list-style-type: none">● Add a SYSTID instruction to allow arbitrary table sizing and data entry (equivalent to the Fortran "dimension" statement)	
3.3.1.6	<p>Provide SYSTID Save Feature</p> <p><u>Present</u></p> <ul style="list-style-type: none">● Simulation results may be saved on tape or disc using a postprocessing routine <p><u>Planned</u></p> <ul style="list-style-type: none">● Provide a SYSTID instruction to automatically save the requested simulation results on tape or disc● Provide a SYSTID instruction to reload the save file for post processing and/or plotting	

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.1.7	<p>Modify Sort Processing</p> <p><u>Present</u></p> <ul style="list-style-type: none">● SYSTID evaluates the system topology according to a rigid sort procedure (First In Last Out starting at node name "INPUT", ending at node name "OUTPUT")● The "DEFINE" instruction allows expression re-evaluation at each reference● The "SET" instruction allows expression evaluation prior to simulation <p><u>Planned</u></p> <ul style="list-style-type: none">● User defined processing sequence● More exhaustive sort procedure	

MAJOR TASK AREA:		
TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.1.8	<p>Provide SYSTID Output Format Capability</p> <p><u>Present</u></p> <ul style="list-style-type: none">● All formatting is fixed within the defined procedures utilized during the simulation phase● Format changes can be made by changing the procedures prior to the generation phase <p><u>Planned</u></p> <ul style="list-style-type: none">● Provide the SYSTID instructions and controls to facilitate:<ul style="list-style-type: none">Page numberingTitlingTime and date labeling	
3.3.1.9	<p>Provide Cross-Reference Output</p> <p>See entry under "Misc. SYSTID Enhancements"</p>	

MAJOR TASK AREA:		
TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.1.10	<p>Provide Automatic Core Sizing</p> <p><u>Present</u></p> <ul style="list-style-type: none"> ● Under the current operating system (Exec II) core sizing of the simulation phase is of no concern as long as it fits ● Core size can be controlled by modifying the defined procedures prior to the generation phase <p><u>Planned</u></p> <ul style="list-style-type: none"> ● Under the new operating system (Exec 8) core size is a predominant cost factor and it is preferable to control core dynamically. This is accomplished by interfacing with the Exec 8 operating system during the simulation ● The generation phase currently requires ~ 45K words. The goal is to decrease this to < 20K words to facilitate generation in the demand (i.e., timesharing) environment 	
3.3.1.11	<p>Provide Automatic Library Directory Updating</p> <p>See entry under "Misc. SYSTID Enhancements"</p>	

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.1.12	<p>Provide Real & Complex Models</p> <p><u>Present</u></p> <ul style="list-style-type: none"> ● All nodes require two core locations ● All nodes are treated as complex quantities with complex arithmetic performed by the user within SYSTID models ● SYSTID expressions are treated as real Fortran expressions rather than complex expressions ● Complex arithmetic is accomplished via the use of some utility functions <p><u>Planned</u></p> <ul style="list-style-type: none"> ● After further study, the development cost for handling both real & complex nodes far out weighs the anticipated advantage (i.e., one storage location for real nodes) ● The obvious and most useful modification is to allow direct complex expressions 	
3.3.1.13	<p>Provide Model Debugging Capability</p> <p>See entry under "Misc. SYSTID Enhancements"</p>	

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.1.14	<p>Provide SYSTID Modeling Aid</p> <p><u>Present</u></p> <ul style="list-style-type: none"> ● Various utility routines and procedures to aid the user in writing a Fortran model <p><u>Planned</u></p> <ul style="list-style-type: none"> ● Additional aids for access to and control of internal SYSTID parameters and storage areas as they are implemented 	
3.3.1.15	<p>Convert to SYSTID Univac 1108 Exec 8 System (1110 JSC System)</p> <p><u>Present</u></p> <ul style="list-style-type: none"> ● SYSTID is written to take advantage of the Univac 1108 system and processors under the Exec II operating system <p><u>Planned</u></p> <ul style="list-style-type: none"> ● Convert the current version of SYSTID to the Exec 8 operating system (Input/output routines) ● Provide JSC with the Exec 8 SYSTID for checkout at JSC ● Use the Exec 8 SYSTID as the starting point for coding modifications 	

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.1.16	<p>Provide SYSTID Interactive Graphics Interface</p> <p><u>Present</u></p> <p>None - Calcomp and printer plotting are available</p> <p><u>Planned</u></p> <ul style="list-style-type: none">● Provide the software interface to allow access to simulation output data for display on the JSC MAPS graphics unit● This task is a joint effort with JSC	
3.3.1.17	<p>Provide Automatic Checkpoint Feature</p> <p>See entry under "Misc. SYSTID Enhancements"</p>	

MAJOR TASK AREA		
TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.1.17	<p><u>Planned</u></p> <ul style="list-style-type: none"> • Provide a SYSTID instruction to interrupt a simulation based upon any simulation parameter, computer run time, or real time to perform ancillary functions or terminate (e.g., the fortran "IF" statement) • Provide a cross reference option for node name versus storage location • Provide automatic permanent update capability to the library directory • Provide additional coding in SYSTID models to facilitate debugging 	

MAJOR TASK AREA:		
TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.2	<p>PMS Model Development</p> <p>Deleted</p>	
3.3.3	<p>Develop SYSTID EPDC Models</p> <p>Task Description:</p> <ul style="list-style-type: none"> ● Gather pertinent data on EPS elements ● Group elements as possible to minimize the number of SYSTID models ● Generate SYSTID models, defining boundary conditions <p>Expected Output:</p> <ul style="list-style-type: none"> ● Reviewed baseline EPDC (JSC) ● Major EPDC block diagram ● SYSTID model code and documentation 	

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.4	<p>Provide SYSTID Software Validation</p> <p>(NOTE: This task was mislabeled in the contract SOW)</p> <p>Task Description:</p> <ul style="list-style-type: none">● Obtain, review & select reliable empirical EPDC performance data● Generate SYSTID runs, using empirical data● Analyze the results <p>Expected Output:</p> <ul style="list-style-type: none">● Distilled empirical data base● SYSTID results● SYSTID validation report	

MAJOR TASK AREA:

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
3.3.5	<p>Develop SYSTID Measuring Techniques</p> <p>Task Description:</p> <ul style="list-style-type: none">● Define and develop performance measuring techniques using SYSTID <p>Expected Output:</p> <ul style="list-style-type: none">● Set of current empirical EPS performance measures● Selected list of performance parameters● List of necessary revisions	
3.3.6	<p>Identify SYCTID Simulation Areas</p> <p>Task Description:</p> <ul style="list-style-type: none">● Using prior study results, and considering related JSC and Rockwell work, define areas which will be usefully attacked by SYSTID simulation <p>Expected Output:</p> <ul style="list-style-type: none">● List of potential study areas● Selected list of SYSTID simulation possibilities● Requirements list for necessary data base, measurements, or expected performance definition in each area	

1.2 Scope

The scope of the study, relative to the objectives given above was more inclusive for the software-related tasks, than for the EPDC performance analysis tasks. The former tasks utilized an available data base, in the form of prior SYSTID code, defined a series of tasks well understood (in detail) by JSC and Hughes personnel, and except for some potentially difficult operational details required interface with the well-defined JSC 1110 computer system (...and knowledgeable personnel in the JSC computer systems area). Therefore, it was reasonable to demand the widest scope for the simulation software enhancement, from fundamental algorithms to validated code and describing documentation.¹ On the other hand, the EPDC element modeling and systems performance analysis tasks required definition of a shuttle subsystem, the EPDC, at a detailed level, when in fact a number of the EPDC element vendors had not been chosen and explicit element characteristics were unavailable. Similarly, the EPDC bus assignments, and resultant EPDC subsystem topology were not finalized. A corresponding lack of intuition was also present in terms of EPDC element criticality for given system performance requirements. Thus, the scope of the EPDC element modeling, and performance evaluation tasks were truncated from what a static subsystem design might have allowed. For instance, the EPDC element modeling was accomplished on the basis of engineering judgement and extrapolation of generically similar device characteristics by Hughes personnel. (A consequence of this limitation is the possibility that devices, such as the Remote Power Controller (RPC) actually chosen for the EPDC may exhibit substantially different characteristics). Further, the performance analysis carried out by SYSTID simulation was limited to illustrative situations, since so little was known about the user load elements. For purposes of establishing a repeatable baseline EPOC topology, the topology employed in SEPAP² was selected, as were the electrical bus assignments employed by it [1].

1.3 Technical Approach

The technical approach used in defining the most critical SYSTID language enhancements, their order of completion, and algorithm design are given in more detail in Volume II of the Final Report, the SYSTID User Guide.

¹See Volume II SYSTID User Guide of this Final Report

²Shuttle Electrical Power (System) Analysis Program, Lockheed Electronics Co./JSC

In general, a number of SYSTID characteristics and capabilities which had existed in the initial implementation¹ were found to be clumsy (the model TAP technique to achieve general multipoint, multinode representation), or excessively rigid (the prior "sort" processing technique) by continued use of the language to simulate telecommunications systems. Therefore, a number of changes were deemed necessary and implemented, as matters of convenience to the user. In addition, the UNIVAC 1110 EXEC 8 operating system requirements imposed some brute force compatibility design tasks, as well as matters of economic operation (i.e., automatic core sizing to dynamically control core requirements and minimize run costs), including "save" and "checkpointing" features so that the user is guaranteed useful output, even with premature termination. A most important and convenient enhancement was the installation of an interactive² graphics capability, so that the CRT/keyboard I/O devices at JSC could be used with SYSTID.

The technical approach employed for EPDC element modeling recognized the lack of firm engineering data on critical units. Therefore, in parallel with data gathering efforts with Rockwell International (the shuttle orbiter prime contractor), generic data was collected and analyzed. For example, hydrogen-oxygen fuel cell modeling data [9] was obtained and scaled for the representative shuttle mission. This generic approach has serious failings, given the very nature of the detailed element responses desired for transient analysis of adequate fidelity. For example, the particular mechanization of a universally present device such as the remote power controller (RPC) has much to do with its transient response³. Thus, the mechanization chosen for the current SYSTID RPC model may not truly reflect the detailed microscopic response of RPC as procured. (The procurement specifications on this device as well as other EPDC elements generally describe the steady-state behavior, and are not complete with respect to the parameters which influence transient response).

¹Reference prior work by the Hughes staff on contract NAS9-11743

²No light-pen, or direct user interaction with the CRT display is implied

³Nominally energy storage components, such as inductance and capacitance, in conjunction with dissipative resistive losses determine this response.

2.0 RESULTS

The study results fall into the categories of SYSTID enhancement, EPDC element modeling, and EPDC performance analysis.

2.1 Software Development Results

Each software enhancement task item given in the SOW SUMMARY of Section 1.1 has been completed and documented. (Task 3.3)

Volume II (SYSTID User Guide) of this Final Report will contain all operational and descriptive data necessary for the user, as well as a task item-by-item description of changes generated during the study.

Volume III, (SYSTID Data Book) of this Final Report contains all program listings, flow charts and data listings.

2.2 EPDC Element Modeling

The shuttle orbiter EPDC subsystem can be characterized by functional subsets as follows:

1. Power source elements (only fuel cells, with the current deletion of stand-by battery power)
2. Power conversion elements (inverters)
3. Distribution elements (cables)
4. Control elements (RPC, RCCB, fuses, diodes)
5. User interface (load element characterization)

The following material will summarize the SYSTID models generated to date, in the order given above. The supporting analysis for these models is summarized in Section 5.3.

SYSTID LIBRARY MODEL DATA

MODEL: INVERTER	GROUP ID CONVERSION	PAGE	DATE
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LIBRARY MODEL NAMES:

INVERTER

DESCRIPTION:

The inverter modulates the DC power flow as supplied by the fuel cell, at a 400 Hz rate, so as to provide single-phase AC user load power...suitable inter-connection of three inverters then provides 3-phase AC power. The inverter consists of three sub-models, a multivibrator, filter, and output coupling transformer.

USAGE:

VIN < INVERTER (FRQ,E,CPF, RL) > VOUT, IS, RS

Where: VIN is the source node voltage, volts

FRQ is the operating frequency, Hz

E is the nominal output node (AC) voltage, volts peak

CPF is the composite power factor of the loads

VOUT is the AC output node voltage, volts

IS is DC current drawn from source

RS is the impedance presented to the source, ohms

SYSTID CODE:

```

MODEL* VIN . INVERTER(FRG,E,CPF,RL) . VOUT,IS,RS
      DEFINE OLD=V(NZ+1)
      1 NZ=ZZ
      2 ZZ=ZZ+1
      VIN . MULTIVIBRATOR(FRG,E) . N1
      N1 . FILTER(2,2,1,0,1.25*FRG,0.,1.,0.1,0.) . N2
      N2 . TRANSFORMER(CPF) . VOUT
      10 OLD=OLD+VOUT*VOUT/RL
      20 IS=OLD*DT/TIME/VIN
      30 RS=VIN/MAX(1.E-20,IS)
END
    
```

SYSTID LIBRARY MODEL DATA

MODEL:	GROUP ID	PAGE	DATE
MULTIVIBRATOR (INVERTER)	CONVERSION		

LIBRARY MODEL NAMES: MULTIVIBRATOR

DESCRIPTION:

This sub-model of the inverter provides the modulation (chopping) capability of the inverter. It is typically an externally-clocked monostable circuit operating nominally at 400 Hz, but with the capability to be clocked at arbitrary rates.

USAGE:

VIN < MULTIVIBRATOR (FRQ, E) > VOUT

Where: VIN is the DC source voltage (node)

FRQ is the clock rate, Hz

E is the nominal output

VOUT is the AC output voltage (node)

SYSTID CODE:

```

MODEL* VIN MULTIVIBRATOR(FRQ,E) , VOUT
      DEFINE TON=V(NZ+1)
      DEFINE TOFF=V(NZ+2)
      DEFINE OLD=V(NZ+3)
      DEFINE A=V(NZ+4)
      DEFINE B=V(NZ+5)
      NZ=ZZ
      XN=E-2.8+.1*VIN
      IF(A)10,,10
      OLD=XN
      A=.5/FRQ
      B=.5/FRQ/LOG(3.)
      ZZ=ZZ+5
      VOUT=OLD
      TR=B*LOG(3*E/XN)
      IF(OLD LE 0) GO TO 100
      IF(T=TON) (T,TR) RETURN
      VOUT=XN
      OLD=VOUT
      TOFF=TIME
      RETURN
      TD=A-TR
      IF(T=TOFF) (T,TD) RETURN
      VOUT=XN
      OLD=VOUT
      TON=TIME
      END
  
```

SYSTID LIBRARY MODEL DATA

MODEL: TRANSFORMER (INVERTER)	GROUP ID CONVERSION	PAGE	DATE
----------------------------------	------------------------	------	------

LIBRARY MODEL NAMES: TRANSFORMER

DESCRIPTION:

This sub-model of the inverter provides coupling of the filtered square-wave output of the multivibrator to the load elements. This is currently a linear transformer model...actual hardware mechanization may require this to be a saturating-core device (non-linear).

USAGE:

VIN < TRANSFORMER (CPF) > VOUT

Where: VIN is the filtered multivibrator (source) voltage (node)

CPF is the composite power factor of the load element(s)

VOUT is the AC output voltage (node)

SYSTID CODE:

```

MODEL* VIN . TRANSFORMER(CPF) . VOUT
      VIN . 1.414*CPF*(VIN+SIGN(0.2,VIN)) . N1
      N1 . QFACTOR(1.,0.,1.0783,0.,1.5E-5,0.263,971.) . VOUT
END
    
```

SYSTID LIBRARY MODEL DATA

MODEL: CABLE	GROUP ID DISTRIBUTION	PAGE	DATE
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LIBRARY MODEL NAMES:

CABLE

DESCRIPTION:

The cable model will output voltage, source current and instantaneous input impedance, as seen by the source. Its main use is as a connection between EPDC subassemblies/elements where the complex impedance transmission characteristics are of importance.

USAGE:

VIN < CABLE (R, C, XL, RL) > VOUT, IS, RS

Where: VIN = input voltage (node)

R = resistance/ft.

C = capacitance/ft.

XL = length of cable, ft.

RL = load impedance (instantaneous)

VOUT = output voltage (node)

IS = current drawn from the source, amperes

RS = instantaneous impedance viewed by source, ohms

SYSTID CODE:

```

MODEL* VIN . CABLE(R,C,XL,RL) . VOUT,IS,RS
      DEFINE RX=R*XL
      DEFINE CX=MAX(C*XL,1E-16)
      VIN . ZED1(1,RL*CX,RX+RL,RL+RX*CX) . IS
      VIN . ZED1(RL,0,RX+RL,RL+RX*CX) . VOUT
10 RS=VIN/MAX(1,E-20,IS)
END

```

SYSTID LIBRARY MODEL DATA

MODEL: REMOTE CONTROL CIRCUIT BREAKER (RCCB)	GROUP ID CONTROL	PAGE	DATE
---	---------------------	------	------

LIBRARY MODEL NAMES:

RCCB

DESCRIPTION:

The remote control circuit breaker is basically a switch that cuts off* if any power exceeds some maximum power threshold. The power rating is a variable determined by the adjunct load and ID number.

USAGE:

VIN < RCCB (ID, RL) > VOUT, IS, RS

Where: VIN = source voltage (node)

ID = identification (Rockwell/SEPAP six-digit number or an arbitrary index of event sequence)

VOUT = output voltage (node)

RL = load impedance, ohms

IS = current drawn from source, amperes

RS = impedance viewed by source, ohms

SYSTID CODE:

```

MODEL* VIN , RCCB(ID,RL) , VOUT,IS,RS
      DIMENSION R(7)/1.E10,1.E-10,5*1.E10/
      DATA T0,CMAX/,01,33/
      DATA C2,C3/6.25E2,19.46E4/      * C2=6.25/T0 C3=19.46/T0/T0
      DEFINE BLOWN=V(NZ+1)
      1  NZ=ZZ
      2  ZZ=ZZ+1
4TRANS  XL=RL
4TRANS  CALL LOADON(ID,MODE)
      10 IF(BLOWN.GT.5) GO TO 35
4TRANS  IF(MODE.GT.1) XL=R(MODE)
      15 IF(VIN/XL.LT.CMAX) GO TO 40
      20 BLOWN=1
      25 WRITE(6,600)ID,TIME
      600 FORMAT(/' *** RCCB LOAD ', I8,' FAULT AT ',F15.4/)
      35 XL=1.E10
      40 CONTINUE
      100 IN=(VIN-.25)/XL
      IN = QFACTOR(1,0,0.,C3,1.,C2,C3) . IS
      110 VOUT=MIN(VIN,IS*XL)
      120 RS=VIN/MAX(1.E-20,IS)
END

```

* Model stays off once tripped, for the duration of the simulation. It also outputs the load element ID and time of trip-off.

SYSTID LIBRARY MODEL DATA

MODEL:	GROUP ID	PAGE	DATE
REMOTE POWER CONTROLLER	CONTROL		

LIBRARY MODEL NAMES:
RPC

DESCRIPTION:

The remote power controller is essentially a current limiter and circuit breaker device that monitors the power drawn by the load, limits and controls* overload currents which can be reset by external command.

USAGE:

VIN < RPC (ID, RL) > VOUT, IS, RS

- Where:
- VIN = source voltage (node)
 - RL = instantaneous load impedance, ohms
 - ID = identification (Rockwell/SEPAP) six-digit number or an arbitrary index of event sequence
 - VOUT = output voltage (node)
 - IS = source current, amperes
 - RS = instantaneous impedance viewed by source, ohms

SYSTID CODE:

```

MODEL* VIN RPC(ID,RL) VOUT,IS,RS
      DIMENSION R(7)/1.E10,1.E-10,5*1.E10/
10 XL=RL
15 CALL LOADON(ID,MODE)
21 IF(MODE.GT.0) XL=R(MODE)
VIN . CURRENT LIMITER(XL,20.) . VOUT,IS,RS
END

```

* Once tripped, the model stays off for the duration of the simulation. An analogous output to the trip signal is given by model indication of load element ID number and time of trip-off.

SYSTID LIBRARY MODEL DATA

MODEL: CURRENT LIMITER (RPC)	GROUP ID CONTROL	PAGE	DATE
LIBRARY MODEL NAMES: CLIM CUR-LIM			

DESCRIPTION:

The current limiter sub-model of the RPC is both a current regulator and a cutoff switch. Its output is both a voltage that is a function of the load impedance and a current that is almost constant under varying load conditions. The cutoff occurs as a function of some maximum rated current.

USAGE:

VIN < CURRENT LIMITER (RL, CMAX) > VOUT, IS, RS

Where: VIN = input voltage (node)
 CMAX = maximum (rated) allowed current, amperes
 VOUT = output voltage (node)
 RL = instantaneous load impedance, ohms
 RS = instantaneous impedance viewed by source, ohms
 IS = instantaneous current drawn from source, amperes

SYSTID CODE:

```

MODEL* VIN CURRENT LIMITER(RL,CMAX) . VOUT,IS,RS
      DEFINE CLIM=V(NZ+3)
      DEFINE COFF=V(NZ+4)
      DEFINE TX=V(NZ+1)
      DEFINE XLIM=V(NZ+2)
      NZ=ZZ
      ZZ=ZZ+4
      IF(CLIM) 6
      CLIM=1.5*CMAX
      COFF=1.25*CMAX
      IF(XLIM.LT.0.5) GO TO 50
      IN=MIN(VIN,0.5)/RL,CLIM)
      IF(IN<COFF),,IS
      XLIM=0
      GO TO 100
      IF(XLIM.GT.0.5) TX=TIME
      XLIM=1
      IF(T=TX.LT.3) GO TO 100
      IF(IN.LE.COFF) GO TO 100
      XLIM=1
      WRITE(6,600)TIME
      FORMAT(/'*** CURRENT LIMITER FAULT AT ',F15.4/)
      IN=0
      100 CONTINUE
      IN=0 QFACTOR(1.0,0,0,1.0,2.026E-5,9.55E-3,1.) . IS
      200 RS=VIN/MAX(1.E-20,IS)
      210 VOUT=IS*RL
      END
    
```

SYSTID LIBRARY MODEL DATA

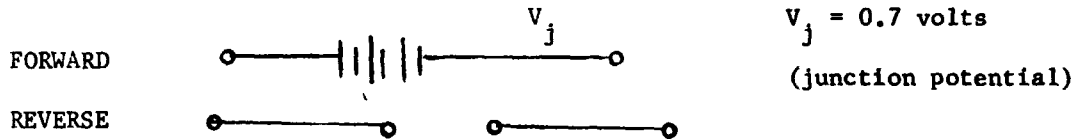
MODEL: IDEAL DIODE	GROUP ID CONTROL	PAGE	DATE
-----------------------	---------------------	------	------

LIBRARY MODEL NAMES:

IDEAL DIODE

DESCRIPTION:

The ideal diode equivalent circuit can be represented by a simple junction potential, if conducting in the forward direction, and an open circuit in the reverse current direction, as follows:



USAGE:

VIN < IDEAL DIODE (RL) > VOUT, IS, RS

Where: VIN is input voltage (node)

RL is load impedance, ohms

IS is the current drawn from the source, amperes

RS is the impedance viewed by the source, ohms

SYSTID CODE:

```

MODEL* VIN . IDEAL DIODE(RL) . VOUT,IS,RS
10 RS=RL
20 VOUT=VIN*.7
30 IS=VOUT/RL
40 IF(VIN.GE.IS*RL+.7) RETURN
50 VOUT=0
60 IS=0
70 RS=1.E20
END
    
```

SYSTID LIBRARY MODEL DATA

MODEL DESCRIPTION: REALISTIC DIODE	GROUP ID CONTROL	PAGE	DATE
---------------------------------------	---------------------	------	------

LIBRARY MODEL NAMES:
REAL DIODE

DESCRIPTION:

This diode model represents a more likely physical realization, employing the diode equation to relate the bulk resistance, to changes in the current flow and junction potential. It is still an ~ ideal device in that the reverse current is 1 ma.

USAGE:

VIN < REAL DIODE (RL) > VOUT, IS, RS

Where: VIN is the source voltage (node)

RL is the load impedance, ohms

IS is the current drawn from the source, amperes

RS is the impedance viewed by the source, ohms

SYSTID CODE:

```

MODEL* VIN , REAL DIODE(RL) , VOUT,IS,RS
      DATA TH,XS/39,1,001/
      5 VX=MIN((VIN-VOUT)*TH,5.)
      10 RD=1./((TH*XS*EXP(VX))
      15 RS=RL+RD
      20 VOUT=VIN*RL/RS
      30 IS=VIN/RS
END
    
```

SYSTID LIBRARY MODEL DATA

MODEL: FUSE	GROUP ID CONTROL	PAGE	DATE
----------------	---------------------	------	------

LIBRARY MODEL NAMES:

FUSE

DESCRIPTION:

The fuse is a load current control device modeled by an instantaneous logical switch actuated* by a rated power threshold.

USAGE:

VIN < FUSE (ID, RL, PMAX) > VOUT, IS, RS

Where: VIN = input voltage (node)
 PMAX = maximum (rated) power allowed, watts
 RL = instantaneous load impedance, ohms
 VOUT = output voltage (node)
 IS = source current, amperes
 RS = instantaneous impedance viewed by source, ohms
 ID = load element identification

SYSTID CODE:

```

MODEL* VIN FUSE(ID,RL,PMAX) VOUT,IS,RS
      DIMENSION R(7)/1.E10,1.E-10,5*1.E10/
      DEFINE BLOWN=V(NZ+1)
      1  NZ=ZZ
      2  ZZ=ZZ+1
      4,RANS RS=RL
      4,TRANS CALL LOADON(ID,MODE)
      3  IF(BLOWN=0.5),,20
      6  IF(MODE.GT.1) RS=R(MODE)
      7  VOUT=VIN
      11 IS=VIN/RS
      15 IF(VIN*IS.LT.PMAX) RETURN
      16 BLOWN=1
      17 WRITE(6,100)ID,TIME
      100 FORMAT(/' *** FUSED LOAD ',I8,' BLOWN AT ',F15.4/)
      20 VOUT=0
      25 RS=1.E10
      40 IS=0
END
    
```

* Model stays off when tripped for the duration of the simulation. It also outputs the load element ID and time of trip-off.

SYSTID LIBRARY MODEL DATA

MODEL: LOGICAL SWITCH	GROUP ID CONTROL	PAGE	DATE
--------------------------	---------------------	------	------

LIBRARY MODEL NAMES:
SWITCH

DESCRIPTION:

The switch element is employed in the SYSTID simulation to provide a lossless connection between any two topological nodes. It is therefore used both for topological and sequence control.

USAGE:

VIN < SWITCH (ID, RL) > VOLT, RS

VOUT = VIN WHEN THE SWITCH IS CLOSED OTHERWISE, VOUT IS ZERO,
RS = RL RS IS INFINITE IN VALUE
ID = ANY EVENT SEQUENCE IDENTIFICATION NUMBER

SYSTID CODE:

```

MODEL * VIN, SWITCH(ID,RL) . VOUT,RS
10 CALL ,OADON(ID,MODE)
20 IF(MODE),,60
30 VOUT=VIN
40 RS=RL
50 GO TO 100
60 VOUT=0
70 RS=1.E10
100 CONTINUE
END

```

SYSTID LIBRARY MODEL DATA

MODEL: FIRST ORDER BI-LINEAR Z-TRANSFORM WITH VARIABLE COEFFICIENTS	GROUP ID MATH	PAGE	DATE
--	------------------	------	------

LIBRARY MODEL NAMES: ZED1

DESCRIPTION

This function is an extension of Q FACTOR where the coefficients may vary with time. The function takes a second order transfer function in the complex variable s,

$$F(s) = \frac{a_1 s + a_0}{b_1 s + b_0}$$

and produces

$$G(z) = \frac{\hat{a}_1 z^{-1} + \hat{a}_0}{\hat{b}_1 z^{-1} + \hat{b}_0}$$

the z-transform in the sampled data operator z^{-1} . The coefficients a_1, b_1 are constants over the sample time interval, but are allowed to change with time.

USAGE

IN < ZED1 (A1, A0, B1, B0) > OUT

where: IN = input s transform
A1 = first instantaneous numerator coefficient
A0 = second instantaneous numerator coefficient
B1 = first instantaneous denominator coefficient
B0 = second instantaneous denominator coefficient
OUT = z transform equivalent output

SYSTID CODE:

```

MODEL*  IN  ZED1(A0,A1,B0,B1) . OUT
        DEFINE OLDIN=V(NZ+1)
        DEFINE OLDOUT=V(NZ+2)
        NZ=NZ+2
        ZZ=ZZ+2
        A11=A1*2/DT
        B11=B1*2/DT
        OUT=A11*(IN-OLDIN)+A0*(IN+OLDIN)+OLDOUT*(B11-B0)
        OUT=OUT/(B11+B0)
        OLDIN=IN
        OLDOUT=OUT
END

```

SYSTID LIBRARY MODEL DATA

MODEL DESCRIPTION: SECOND ORDER BI-LINEAR Z-TRANSFORM WITH VARIABLE COEFFICIENTS	GROUP ID MATH	PAGE	DATE
LIBRARY MODEL NAMES: ZED2			

DESCRIPTION:

This function computes the bi-linear z-transform for a second order transfer function in the s domain whose coefficients vary with time (though constant over a given sample period) i.e., maps

$$G(s) = \frac{a_2 s^2 + a_1 s + a_0}{b_2 s^2 + b_1 s + b_0} \quad \text{into} \quad G(z) = \frac{\hat{a}_2 z^{-2} + \hat{a}_1 z^{-1} + \hat{a}_0}{\hat{b}_2 z^{-2} + \hat{b}_1 z^{-1} + \hat{b}_0}$$

USAGE:

IN < ZED2 (A, A1, A2, B0, B1, B2) > OUT

- Where:
- IN = input transform in s domain
 - A0 = 1st numerator coefficient
 - A1 = 2nd numerator coefficient
 - A2 = 3rd numerator coefficient
 - B0 = 1st denominator coefficient
 - B1 = 2nd denominator coefficient
 - B2 = 3rd denominator coefficient
 - OUT = output z-transform

SYSTID CODE:

```

MODEL*      IN      ZED2(A0,A1,A2,B0,B1,B2) . OUT
1  DEF IN      A1=A1*2/DT
2  DEF IN      A2=A2*4/DT/DT
3  DEF IN      B1=B1*2/DT
4  DEF IN      B2=B2*4/DT/DT
5  DIMENSION  C(3),D(3)
6  DEF IN      X02=V(NZ+1)
7  DEF IN      X01=V(NZ+2)
8  DEF IN      X13=V(NZ+3)
9  DEF IN      X11=V(NZ+4)
10 NZ=Z
11 Z=Z+4
12 C(1)=A0+A1+A2
13 C(2)=2*A0+2*A2
14 C(3)=A0+A1+A2
15 D(1)=B0+B1+B2
16 D(2)=2*B0+2*B2
17 D(3)=B0+B1+B2
18 OUT=C(1)*IN+C(2)*X11+C(3)*X12 -D(2)*X01-D(3)*X02
19 OUT=OUT/D(1)
20 X12=X11
21 X11=IN
22 X02=X01
23 X01=OUT
END
    
```

SYSTID LIBRARY MODEL DATA

MODEL: SEPAP LOADS	GROUP ID CONTROL	PAGE	DATE
-----------------------	---------------------	------	------

LIBRARY MODEL NAMES:

LOADS

DESCRIPTION:

The LOADS model controls the composition and sequence of SEPAP load groups in terms of their load equipments (elements). The model connects the loads through either an RPC, RCCB, or Fuse as given in the equipment/load data base, and is controlled by the Events Generator. The output of the model is the impedance presented to the voltage source.

USAGE:

VIN < LOADS (IL) > RS

where: VIN = source voltage node
 IL = SEPAP load number (load group)
 RS = impedance presented to the source

SYSTID CODE:

```

MODEL *VIN*LOAD(ID)*RS
      DIMENSION ILOD(100)
      LOGICAL FIRST, FALSE,
      DIMENSION IADD(3), IADD, F, LOAD, IZ(1)
      EQUIVALENCE (IZ,V), (IU,IOLDF), (IH,MODE,MO), (IT,ITYP,NE)
      EQUIVALENCE (XWATT,XL,NC), (I,NEWE)
      DEFINE EQUIP=FLD(0,20,IZ(NZ+1))
      DEFINE TYPE=FLD(20,2,IZ(NZ+1))
4TRANS IF (FIRST) GO TO 1
4TRANS FIRST=TRUE
4TRANS DO 2 I=1,100
      2 READ(5,3,END=4)ILOD(I)
4TRANS I=I+1
      3 FORMAT(I3)
      4 NLOD=I-1
      1 CONTINUE
4TRANS NZ=NZ+1
4TRANS $ IF (IZ(NZ+1),NE,0)GO TO 200
4TRANS DO 5 I=1,NLOD
      5 IF (ID.EQ. ILOD(I)) GO TO 6
4TRANS GO TO 22
      6 CONTINUE
4TRANS $ IH=ID/100
4TRANS $ IU=ID-IH*100
4TRANS $ IT=IU/10
4TRANS $ IU=IU-10*IT
4TRANS $ NC=0
4TRANS $ IF (IU.EQ.0)GO TO 50
4TRANS $ FLD(0,6,IADD(3))=IH+48
4TRANS $ NC=1
      10 FLD(NC*6,6,IADD(3))=IT+48
4TRANS $ NC=NC+1
      20 FLD(NC*6,6,IADD(3))=IU+48
4TRANS $ IH=ERCSF(IADD)
4TRANS $ IF (IH.EQ.0)GO TO 60
      22 WRITE(6,100)ID,IH
      100 FORMAT(' LOAD NOT FOUND:',I4,' STATUS OF ADD ='013)
    
```


SYSTID LIBRARY MODEL DATA

MODEL:	SEPAP LOADS	GROUP ID CONTROL	PAGE	DATE
LIBRARY MODEL NAMES:				
LOADS				
LOADS SYSTID CODE (CONTINUED)				
<pre> 4TRAN \$ IZ(ZZ+1)=1 30 RS=1.E10 4TRANS ZZ=ZZ+1 4TRAN \$ RETURN 50 FLD(0,18,IADD(3))=1 4TRAN \$ IF(17.NE.0) GO TO 10 4TRAN \$ GO TO 20 60 IOLDE=0 4TRANS WRITE(6,61)IADD(2),IADD(3) 61 FORMAT(1X,A6,A3/) 4TRAN \$ NZ=NZ+3 70 READ(5,110,END=90)NEW,MODE,ITYP,NTYP,XWATT 4TRANS WRITE(6,110)NEW,MODE,ITYP,NTYP,XWATT 110 FORMAT(7X,I6,I1,2X,A2,26X,T1,F9,2) 4TRAN \$ IF(NTYP.NE.1)GO TO 400 4TRAN \$ IF(MODE.GT.1) GO TO 70 4TRAN \$ IF(IOLDE.NE.NEW) GO TO 80 75 V(MODE+NZ+2)=32.*32./XWATT 4TRAN \$ GO TO 70 80 NZ=NZ+3 4TRAN \$ IOLDE=NEW 4TRAN \$ EQUIP=NEW 4TRAN \$ NTYP=3 4TRAN \$ IF(ITYP.EQ.'RC')NTYP=2 4TRAN \$ IF(ITYP.EQ.'RPI')NTYP=1 4TRAN \$ TYPE=NTYP 4TRAN \$ V(NZ+3)=1.E10 4TRAN \$ V(NZ+2)=1.E10 4TRAN \$ GO TO 75 400 GO TO 70 90 THIS IS THE ENTRY POINT FOR NON RESISTIVE ELEMENTS 90 IZ(ZZ+1)=3+NZ-ZZ 200 IF(IZ(ZZ+1).EQ.1) GO TO 30 4TRAN \$ NE=IZ(ZZ+1)/3 4TRAN \$ NZ=ZZ+1 4TRANS ZZ=ZZ+IZ(ZZ+1)+1 4TRAN \$ RS=1.E10 4TRANS DO 301 I=1,NE 4TRANS XBLOW=2.*32.*32./V(NZ+2) 4TRAN \$ CALL LOADN(EQUIP,MO) 4TRAN \$ IF(MO=2),220,230 4TRAN \$ XL=V(NZ+2+MO) 4TRAN \$ GO TO 240 220 XL=1.E-10 4TRAN \$ GO TO 240 230 XL=1.E10 240 MO=TYPE 4TRAN \$ GO TO (250,260,270),MO 250 CONTINUE @ RCPC VIN = CURRENT LIMITER (XL,20.) - VO , IS , R 4TRAN \$ GO TO 300 260 CONTINUE @ RCCB VIN = RCCB(=EQUIP,XL) . VO,IS,R 4TRAN \$ GO TO 300 270 CONTINUE @ FUSE AND OTHERS VIN = FUSE(=EQUIP,XL,XBLOW) . VO,IS,R 300 RS=1./((1./RS+1./R) 4TRAN \$ IF(R.GT.1.E-5) GO TO 301 4TRAN \$ ROUTXL=R 4TRAN \$ NTYP=EQUIP 4TRAN \$ WRITE(6,8898) ROUTXL,NTYP,MO 8898 FORMAT(150,2X,E14,6,3I10) 301 NZ=NZ+3 END </pre>				
2-17				

2.3 EPDC Performance Analysis

The Events Generator, in conjunction with the LOADS and EPDC models listed in Section 2.2, was employed¹ to excite the step response of an RCCB, RPC, and FUSE driving a resistive load from the fuel cell source, as shown schematically in Figure 2.3-1. In addition, the inverter was also tested for step response when supplying a resistive load. Figures 2.3-2(a) and (b) display the fuel cell bus voltage, and bus current, respectively, as the RPC, RCCB, FUSE, and inverter are excited. Figures 2.3-3, 2.3-4, 2.3-5, and 2.3-6 display the transient current flow of the RPC, RCCB, inverter, and FUSE DC input paths.

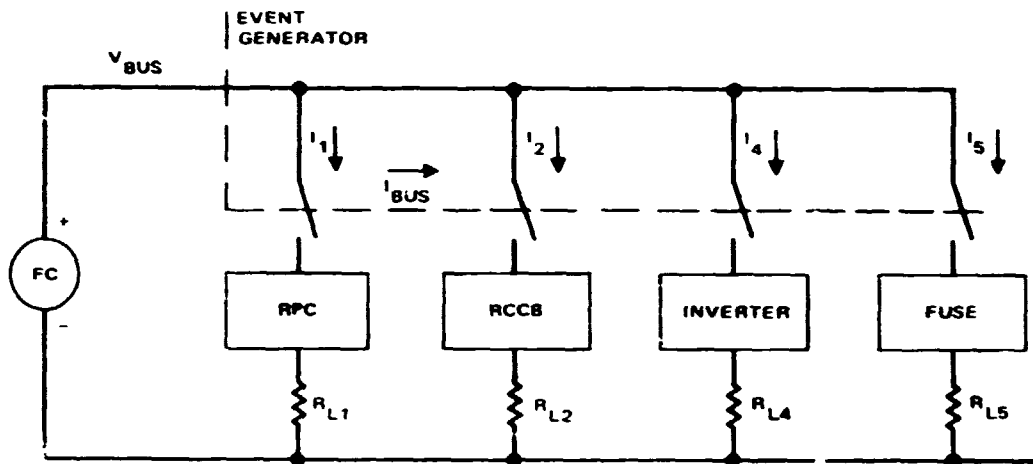


FIGURE 2.3-1. EPDC ELEMENT TRANSIENT RESPONSE
SYSTID TEST CONFIGURATION

¹The Event Generator actually drives logic internal to the device; the logical switches are shown external to the RPC, RCCB, FUSE, and inverter as a matter of convenience.

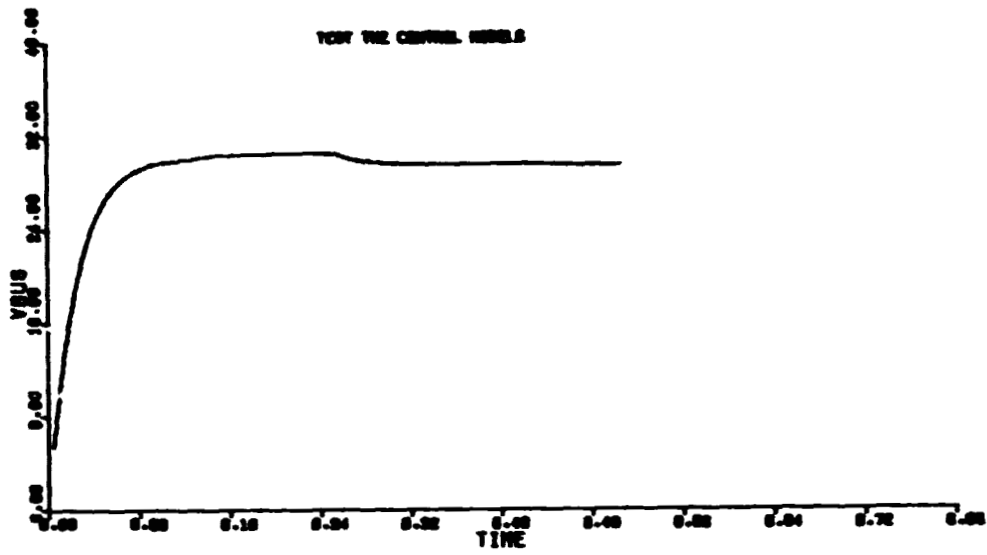


FIGURE 2.3-2a. FUEL CELL BUS VOLTAGE VERSUS TIME, FOR SEQUENCED LOADS

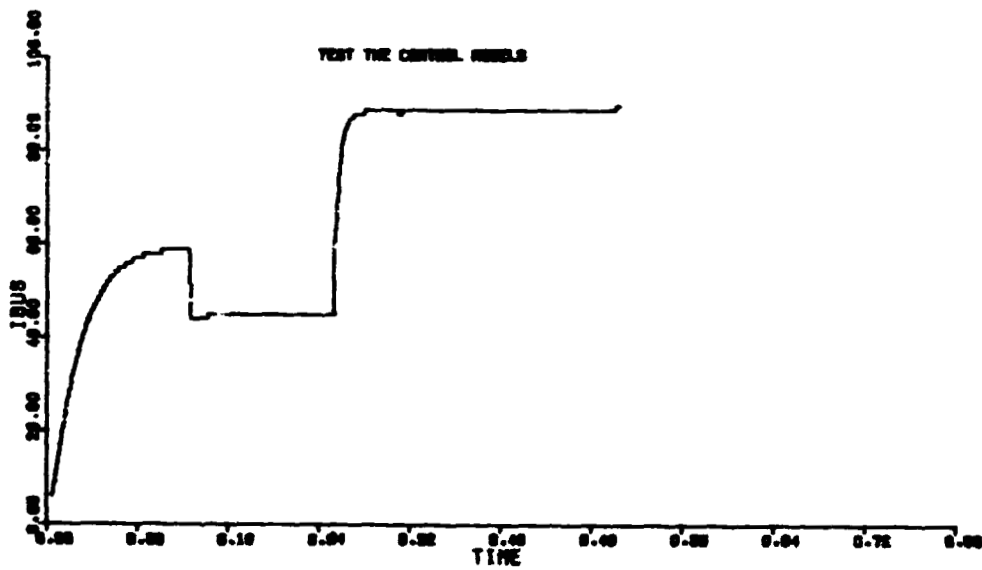


FIGURE 2.3-2b. FUEL CELL OUTPUT CURRENT VERSUS TIME, FOR SEQUENCED LOADS

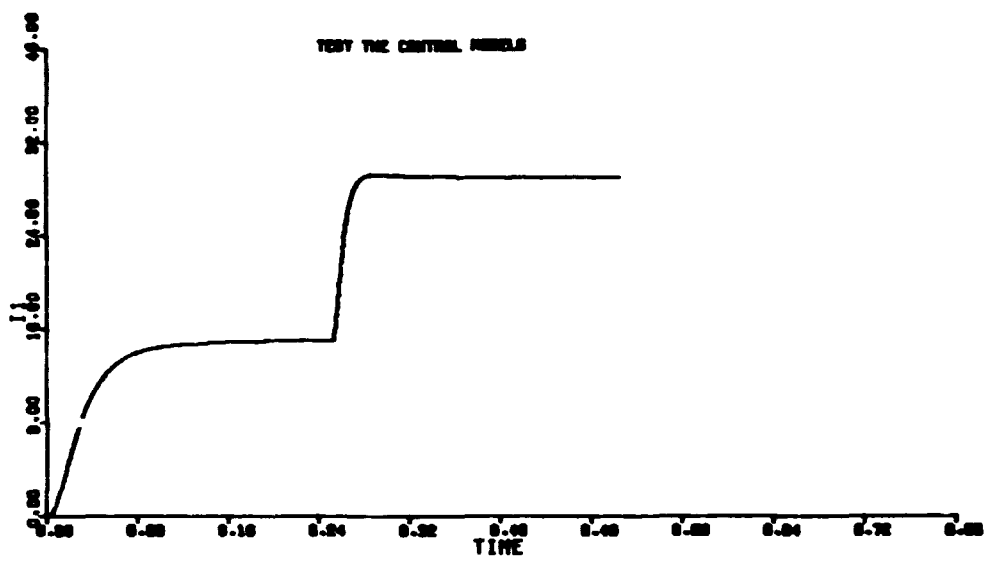


FIGURE 2.3-3. RPC INPUT CURRENT VERSUS TIME
(SEQUENCED OFF/ON)

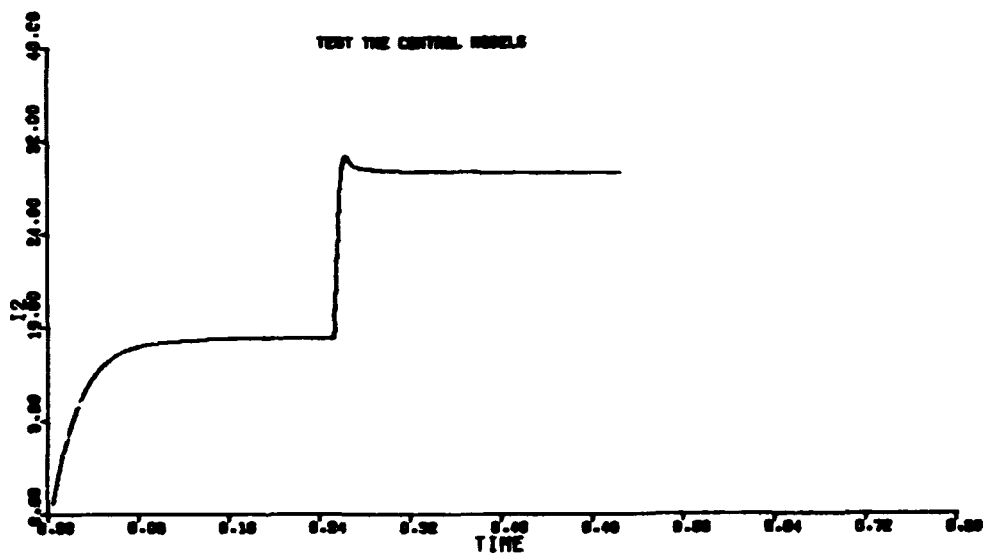


FIGURE 2.3-4. RCCB INPUT CURRENT VERSUS TIME
(SEQUENCED OFF/ON)

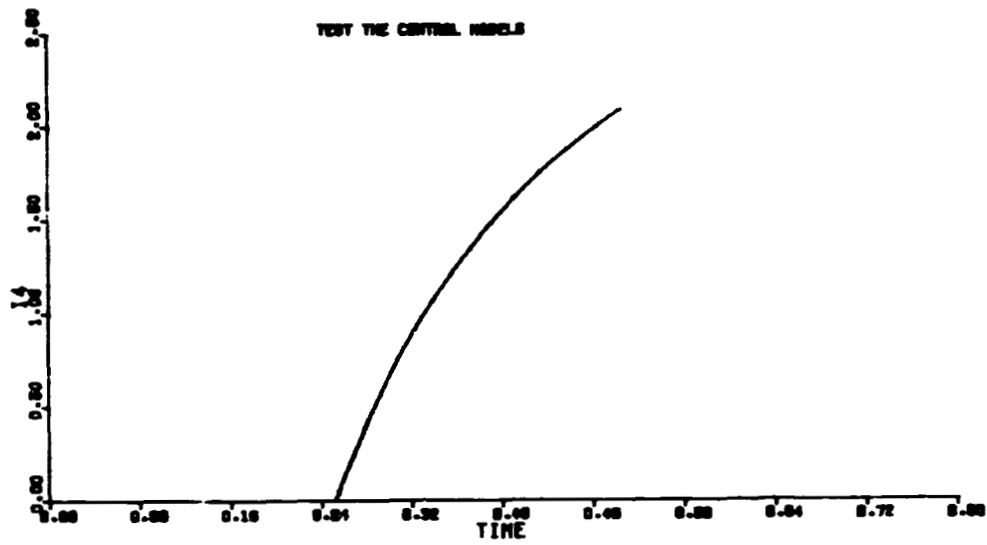


FIGURE 2.3-5. INVERTER DC INPUT CURRENT VERSUS TIME (SEQUENCED OFF/ON)

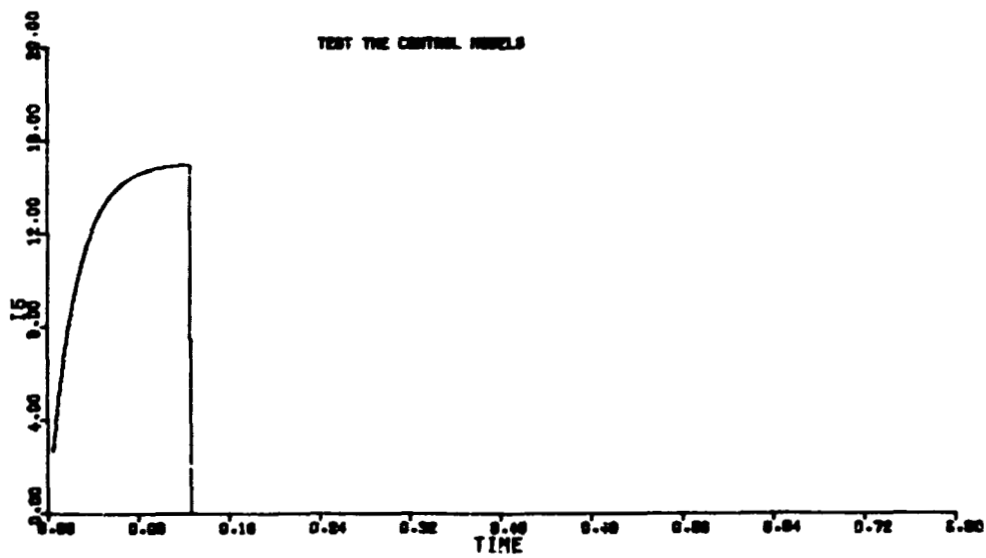


FIGURE 2.3-6. FUSE INPUT CURRENT VERSUS TIME (SEQUENCED OFF/ON)

The complete EPDC subsystem topology of Figure 7.1-1 was exercised by the Event Generator and LOADS model, in order to display the entire simulation capability of SYSTID. To minimize output data to manageable levels for this preliminary stage, only representative subsets of the EPDC topology were selected for output analysis.

These representative subsets included:

- 1) Main DC bus A, main bus B, main bus C voltage and currents
- 2) Local DC bus current fed by the main buses A, B, and C into local DC load groups
- 3) Currents of load group (DC) fed by local buses in A, B, and C main bus groups
- 4) DC current drawn by an inverter as fed by a local bus, for each main bus group (the AC output currents of inverters driving their load groups was not displayed to minimize computer output). A representative sample of the inverter AC output is given in Section 5.3.1.
- 5) Currents of dioded aft sub-bus loads, in groups A, B, and C
- 6) Essential bus currents in the main bus B group

Table 2.3-1 lists these outputs in greater detail by identifying nodes and branch numbers consistent with Figure 7.1-1. The appropriate responses are given in the same order listed in this table by the CALCOMP plots which follow.

TABLE 2.3-1. EPDC FAULT RESPONSE PLOTS IN SEQUENCE IN WHICH THEY FOLLOW

EPDC Element	Current/Voltage Identification*	Figure	Comments
Main bus A	I 101	2.3 - 7	Current drawn from fuel cell 1
Forward, local DC bus A	I 120	2.3 - 8	Current drawn from main bus A by local bus loads
Local bus A DC load group	I 121	2.3 - 9	Current drawn by load group 121
Inverter bus A	I 19	2.3 - 10	DC current drawn by inverter when supplying load group 123
Aft sub-bus AB	I 512A	2.3 - 11	Diode current drawn by load group 512 from aft local bus A
Main bus A	V 10	2.3 - 12	Voltage output of fuel cell 1
Main bus B	I 201	2.3 - 13	Current drawn from fuel cell 2
Forward local DC bus B	I 220	2.3 - 14	Current drawn from main bus B by local bus loads
Local bus B DC load group	I 221	2.3 - 15	Current drawn by DC load group 221
Inverter bus B	I 29	2.3 - 16	DC current drawn by inverter when supplying load group 223

* Refer to Figure 7.1-1, the EPDC topology for symbol keying.

Table 2.3-1 (Continued)

EPDC Element	Current/Voltage Identification	Figure	Comments
Aft sub-bus BC	I 523 B	2.3 - 17	Diode current drawn by aft load group 523 from aft local bus B
Main bus B	V20	2.3 - 18	Voltage output of fuel cell 2
Main bus C	I 301	2.3 - 19	Current drawn from fuel cell 3
Forward local DC bus C	I 320	2.3 - 20	Current drawn from main bus C by local forward DC loads
Local bus C DC load group	I 321	2.3 - 21	Current drawn by DC load group 321
Inverter bus C	I 39	2.3 - 22	DC current drawn by inverter when supplying load group 323
Aft sub-bus CA	I 531C	2.3 - 23	Diode current drawn by aft load group 531 from aft local bus C
Main bus C	V 30	2.3 - 24	Voltage output of fuel cell 3
Essential bus 1BC	I 271 A	2.3 - 25	Current drawn from main bus A by essential load 271
	I 271 B	2.3 - 26	Current drawn from main bus B by essential load 271

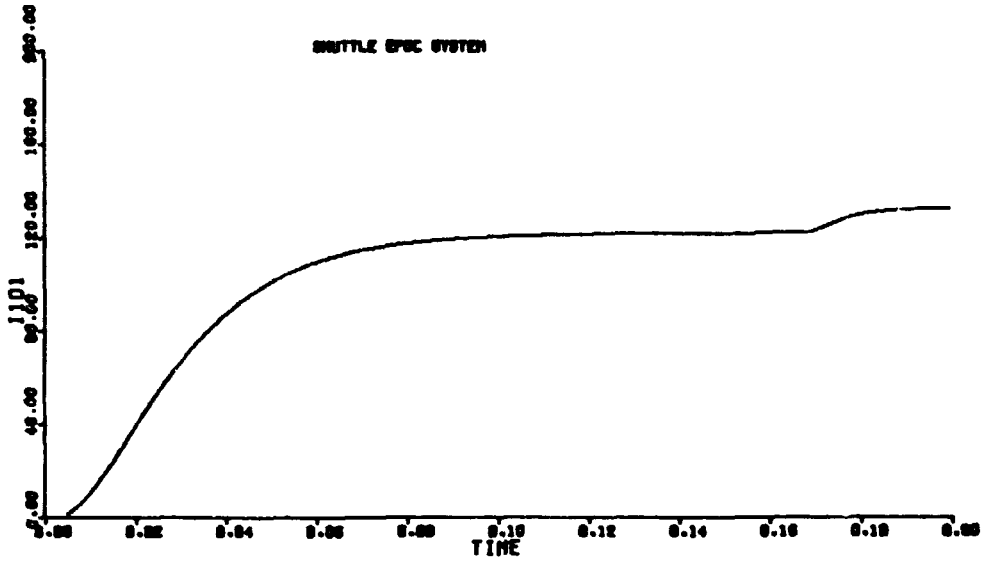


FIGURE 2.3-7.

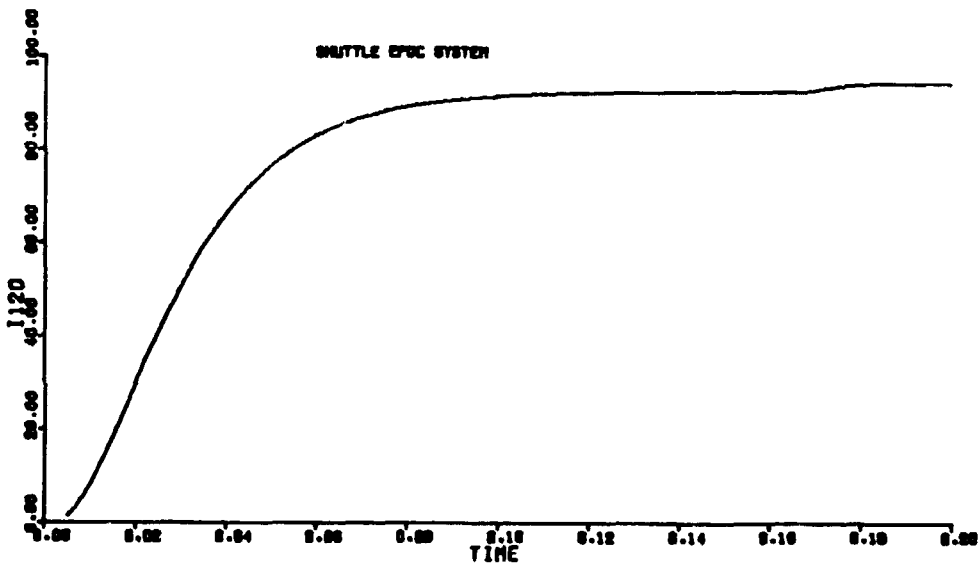


FIGURE 2.3-8.

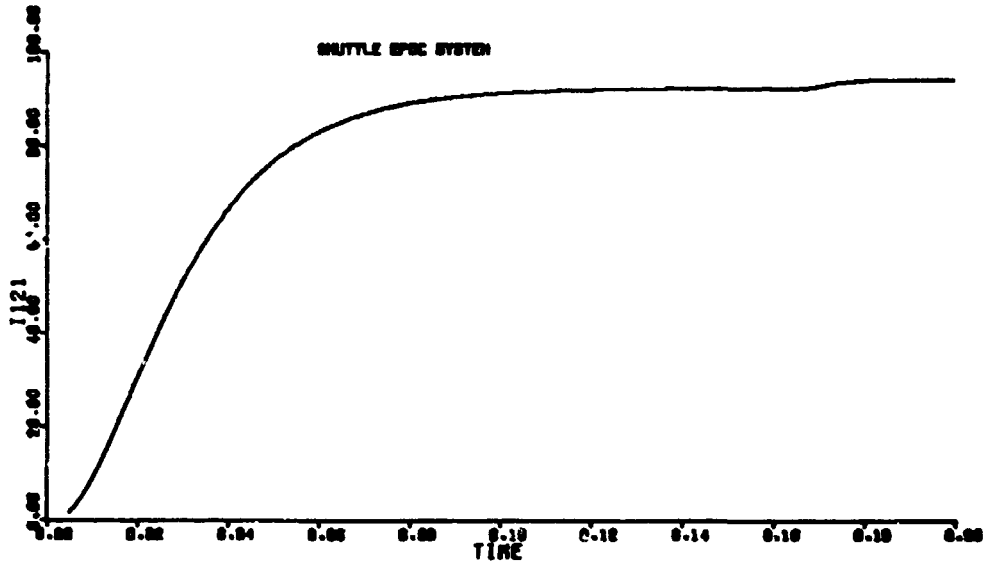


FIGURE 2.3-9.

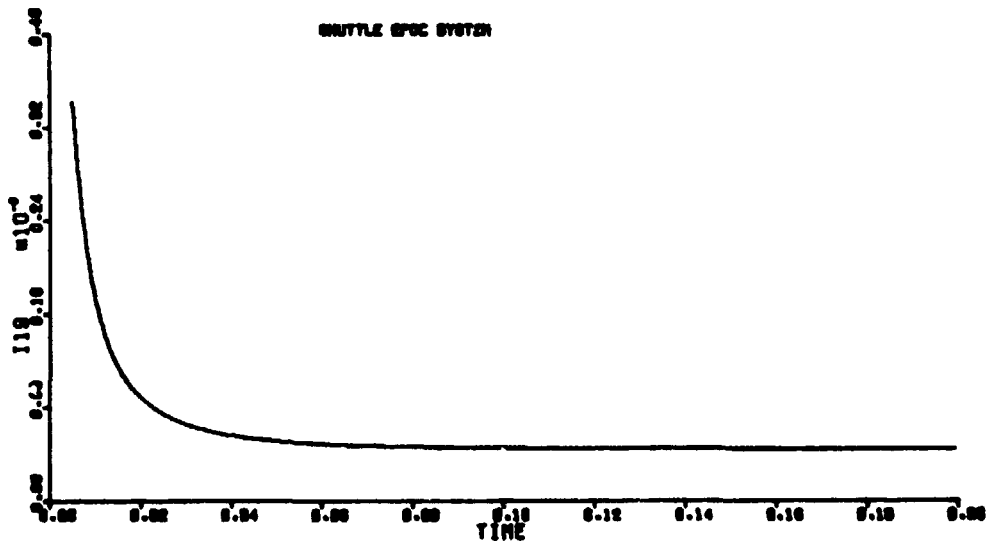


FIGURE 2.3-10.

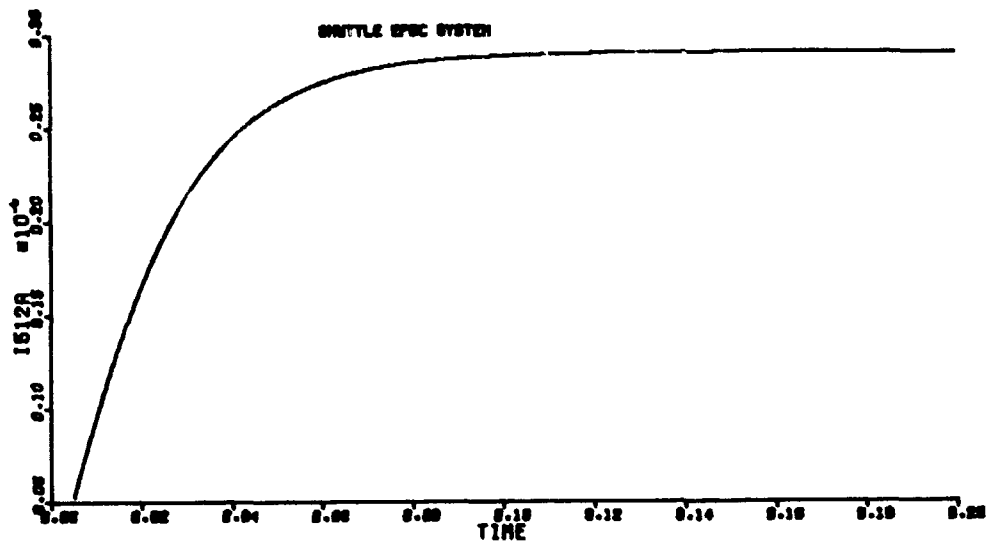


FIGURE 2.3-11.

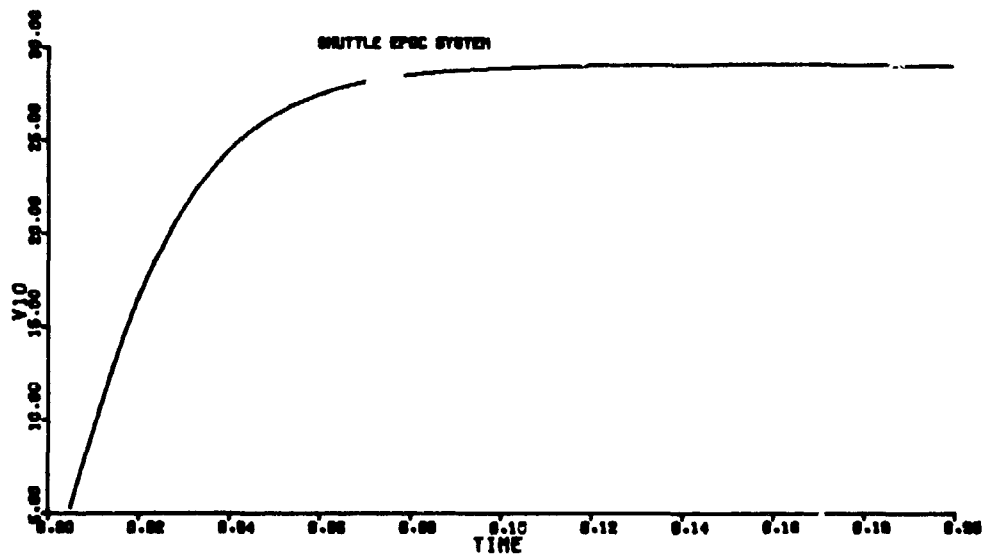


FIGURE 2.3-12.

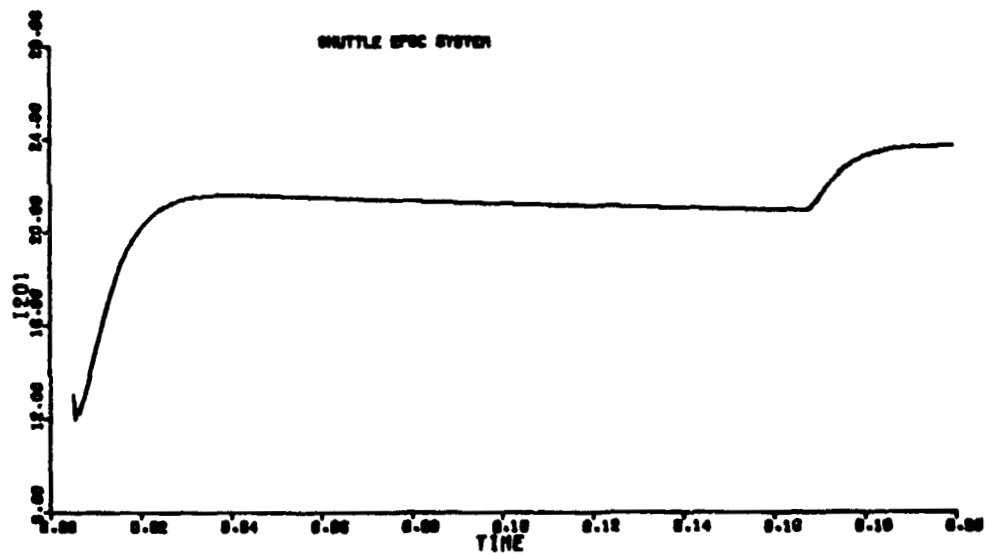


FIGURE 2.3-13.

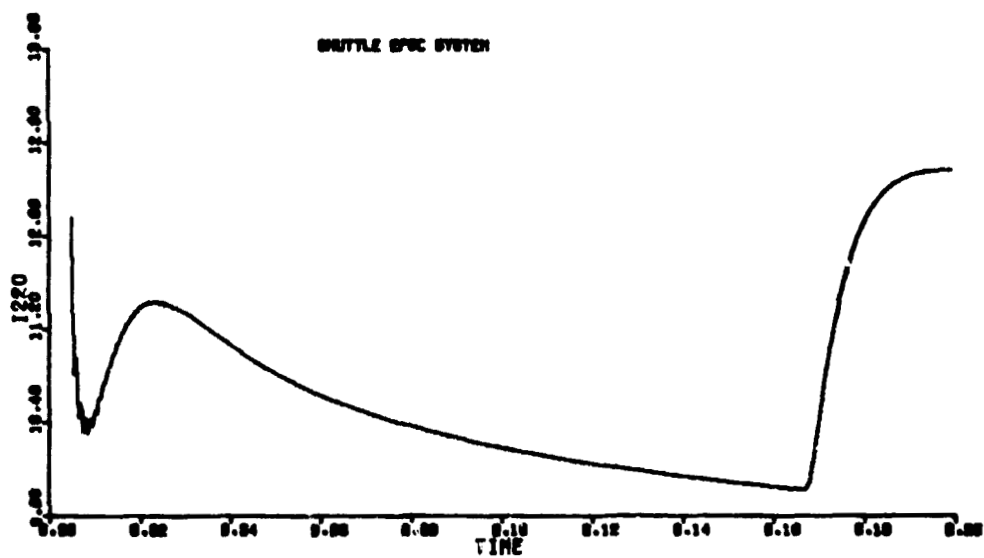


FIGURE 2.3-14.

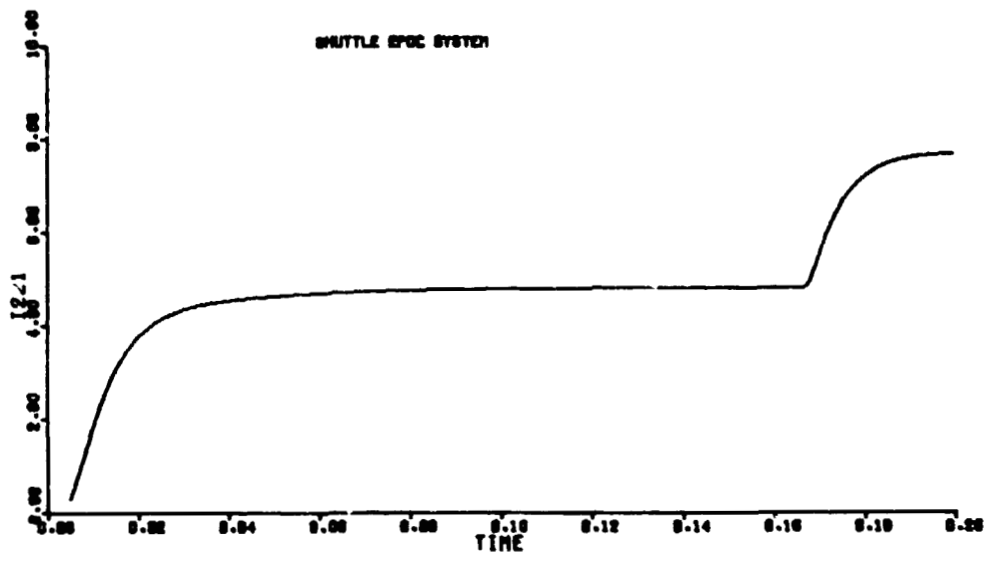


FIGURE 2.3-15.

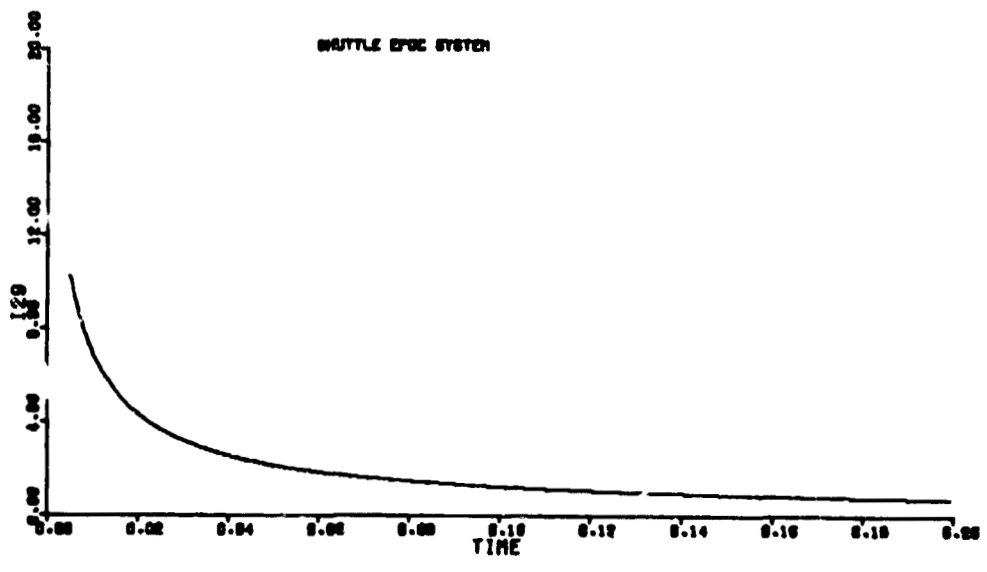


FIGURE 2.3-16.

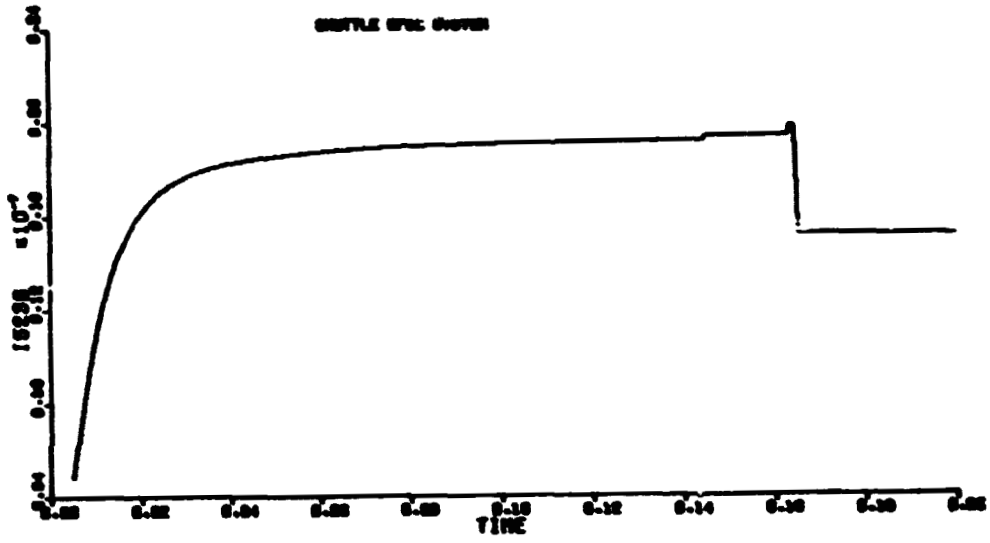


FIGURE 2.3-17.

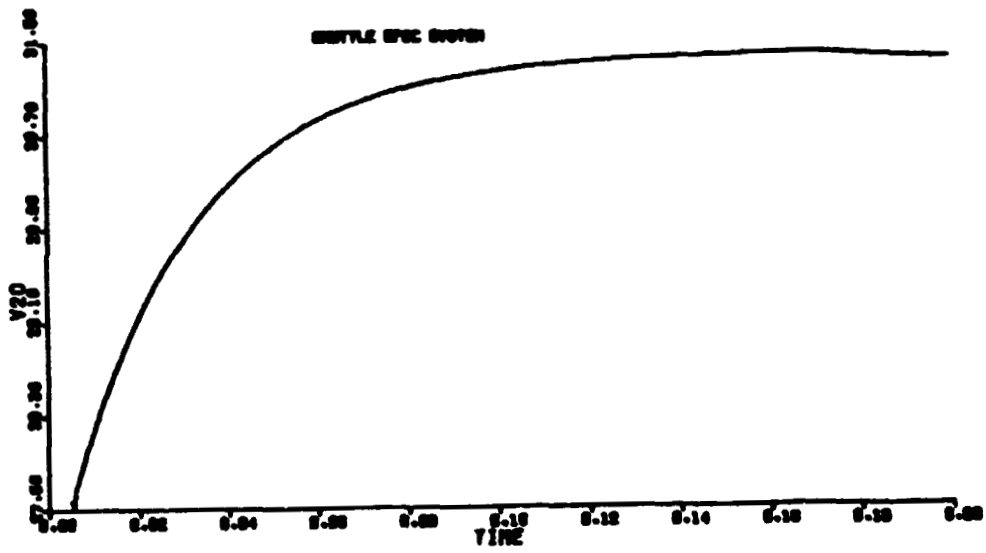


FIGURE 2.3-18.

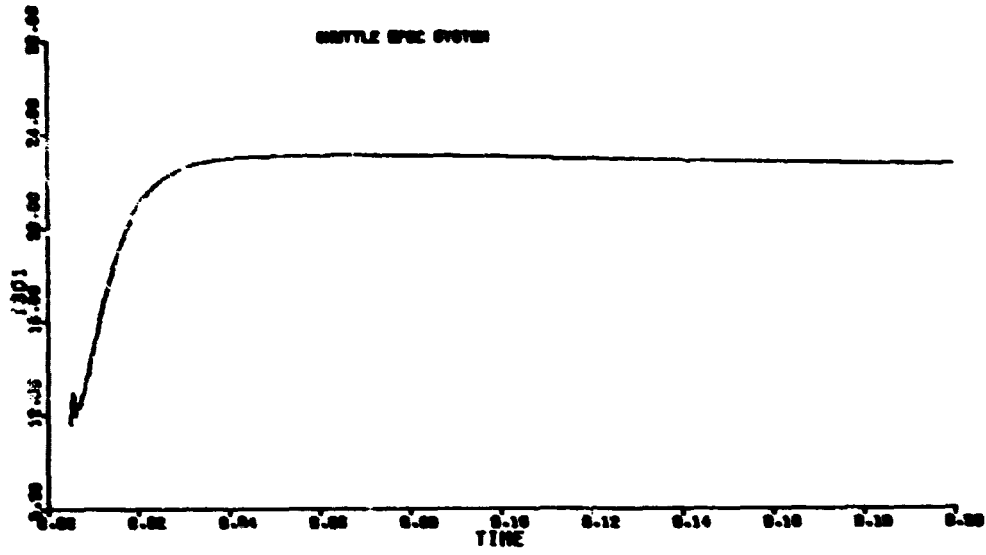


FIGURE 2.3-19.

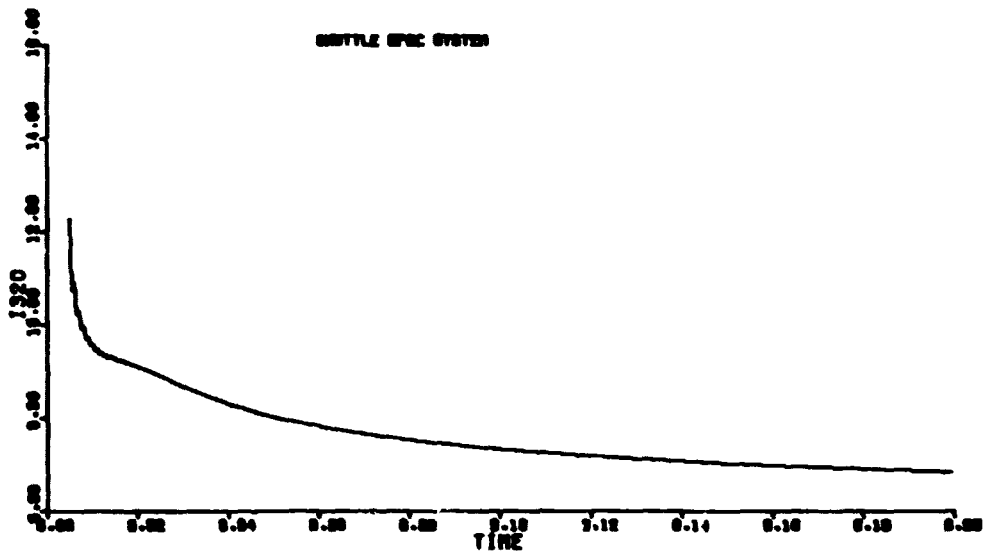


FIGURE 2.3-20.

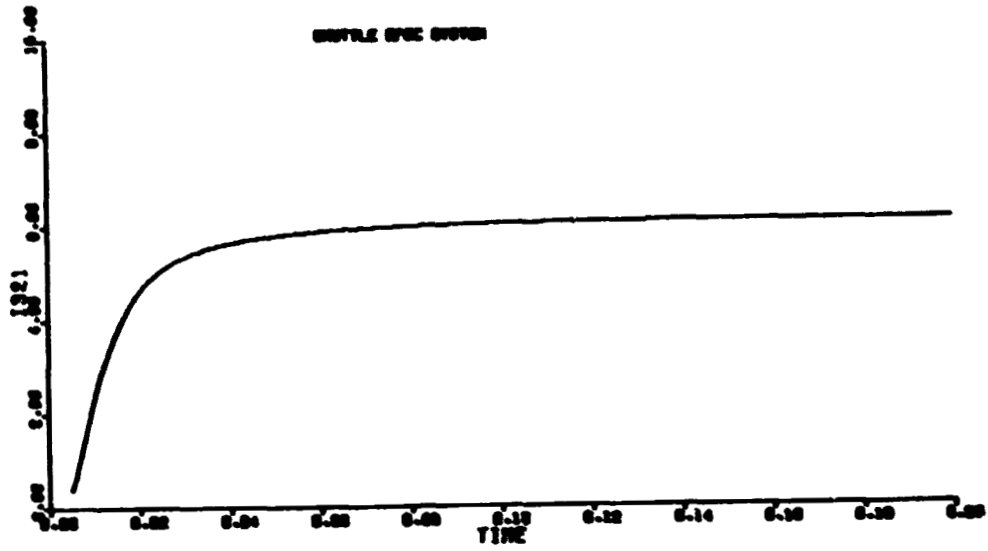


FIGURE 2.3-21.

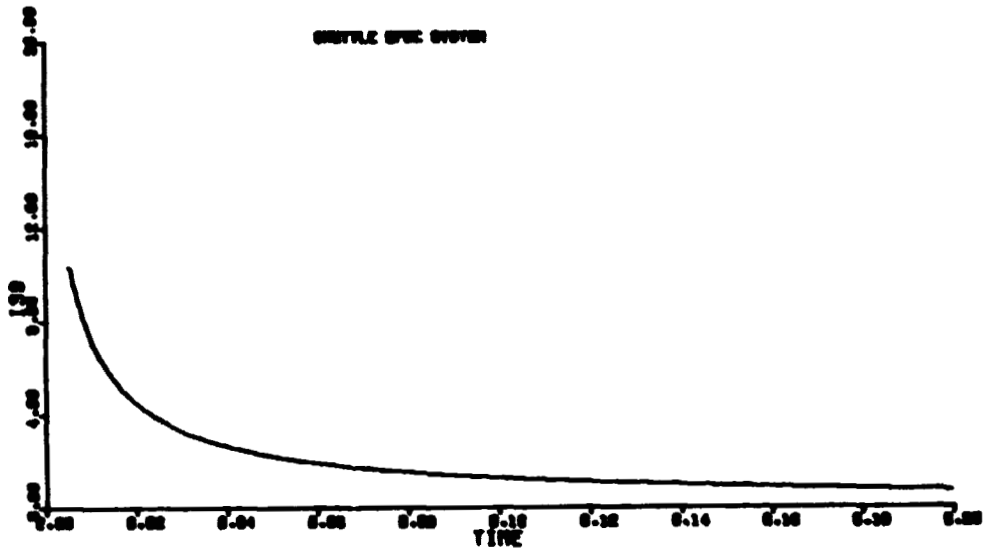


FIGURE 2.3-22.

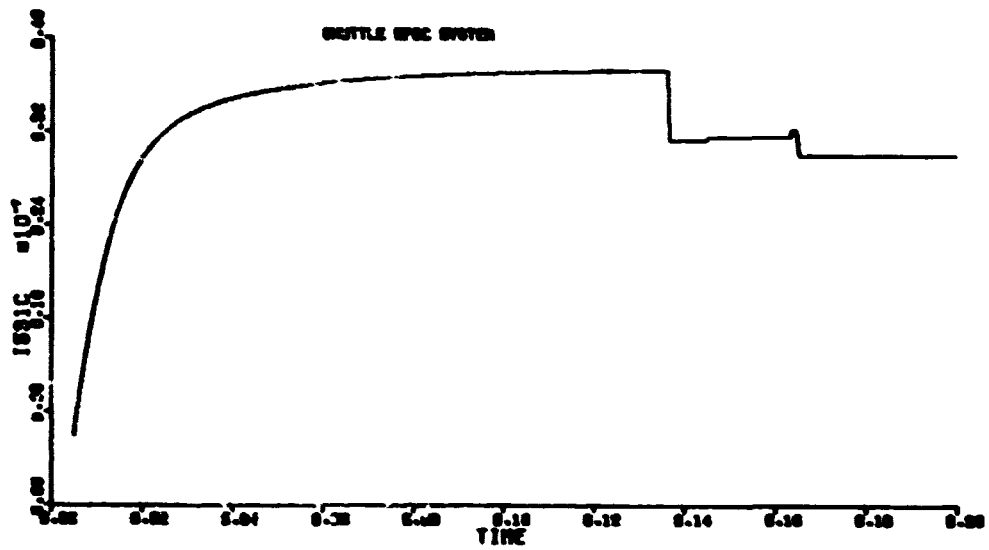


FIGURE 2.3-23.

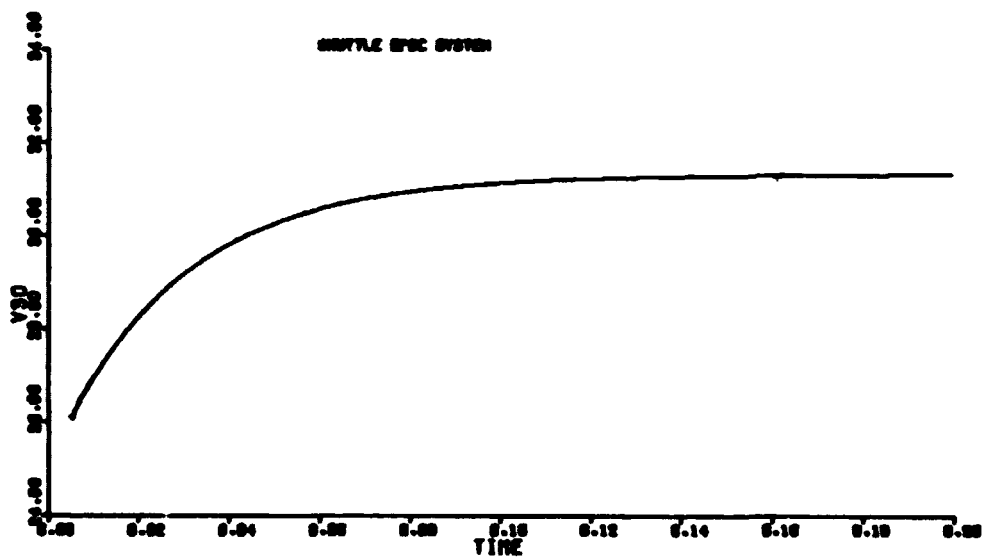


FIGURE 2.3-24.

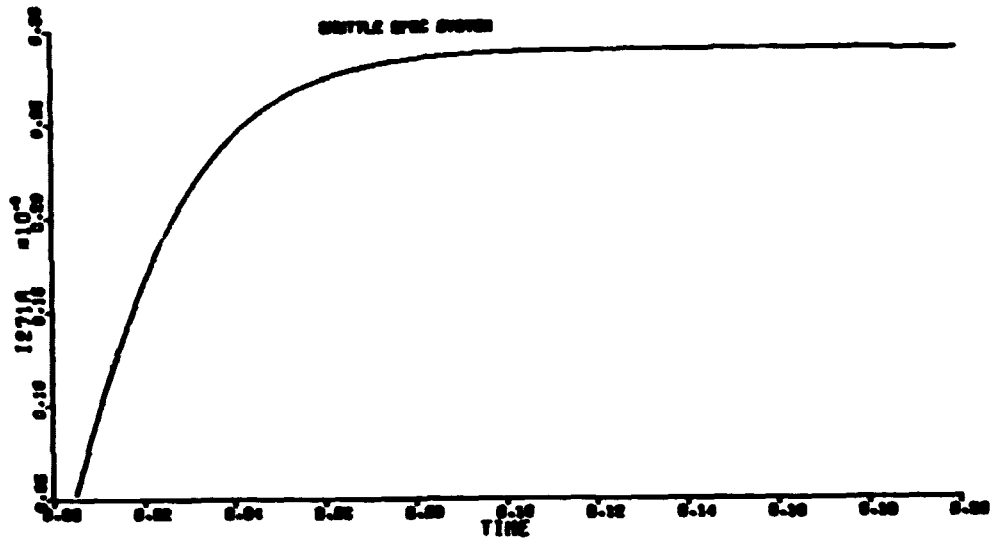


FIGURE 2.3-25.

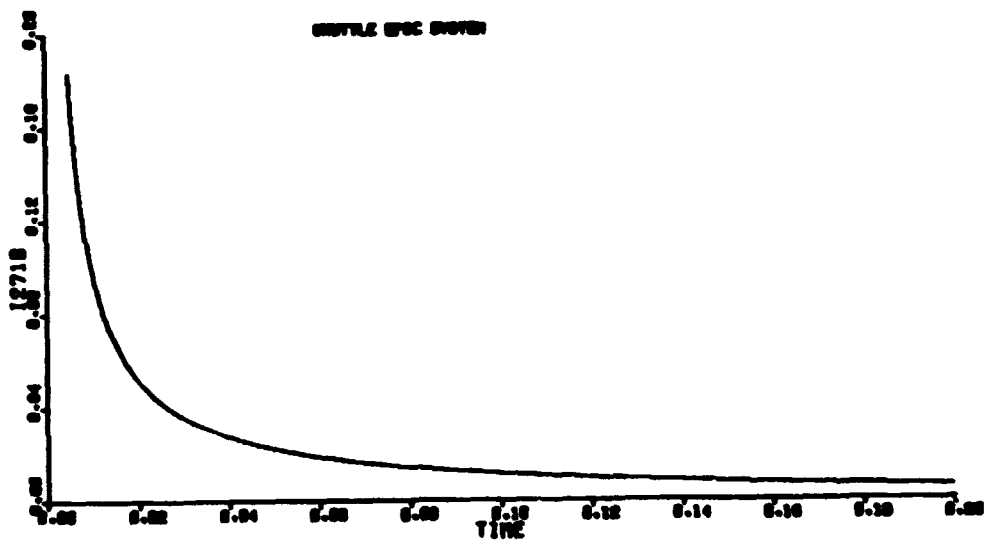


FIGURE 2.3-26.

3.0 CONCLUSIONS

All of the stated objectives for SYSTID simulation software enhancement were realized...in fact exceeded in some respects. The net result of this effort is the presence, on the NASA/JSC UNIVAC 1110 operating system, of a greatly improved SYSTID language, whose user utility and operational flexibility are much improved relative to the original SYSTID software. Incorporation of the JSC MOPS (Hazeltine 4000G) CRT terminal as a device for SYSTID user input/output has added another dimension of user convenience.

The study achievements in the tasked areas of shuttle electrical power system element modeling and performance analysis are more conditional than the clear-cut status of the software tasks. The preliminary discussion in the section on results, and the following general discussion section should make clear that a finalized EPDC topology and EPDC element data base do not currently exist. Therefore, at best, the SYSTID models describe generically similar devices, not necessarily the behaviour of devices which will eventually be specified by Rockwell/JSC. Similarly, due to lack of detail on EPDC elements, their bus assignments, and characterization of load devices, the performance analysis has necessarily been merely illustrative in terms of its utilization of SYSTID simulation capability and the nature of the performance measures, i.e., response of EPDC source/control elements to load shorts, etc.

What has been accomplished, therefore, in the EPDC modeling and performance task efforts, is 1) the establishment of generic models, which may be quite adequate (with parameter adjustment) in the representation of finalized hardware elements, 2) establishment of a "superset" EPDC topology, and associated event generator, which can be modified with additional detail, as the system design solidifies, 3) a qualitative measure of typical EPDC transient responses at certain interesting points, as load states are varied. The latter observations of SYSTID outputs at appropriate points can be used to size circuit protection devices (RPC, RCCB, fuses) determine bus current flows for redundantly-configured loads such as the essential buses, and computers, under fault conditions. In short, the addition of firm hardware characteristics to the model data base and minor changes to the system topology will allow utilization of the study performance simulations for useful system prediction and design analysis.

4.0 RECOMMENDATIONS

Based on the results of the study and the knowledge gained about the shuttle EPDC by Hughes study staff, it is possible to recommend that the following additional tasks, as described in the abbreviated statements below be pursued. A functional task flow overview of the proposed follow-on is presented in Figure 4.0-1.

The original EPDC/user subsystem SYSTID simulation and performance analysis goals continue to be worthy of implementation. However, given the continued fluidity of the EPDC and user (load) subsystem design, more immediate attention to valid detailed modeling of as many EPDC and user subsystem elements as have been defined would appear to be more productive than larger-scale system performance analysis.

Therefore, it is recommended that a well-researched, validated and documented EPDC/load subsystem element modeling effort be undertaken as a follow-on study effort. The enhanced SYSTID software and preliminary EPDC modeling efforts carried out in this contract have provided a secure foundation which will underlay the follow-on element modeling, and eventual system modeling and performance analysis.

MAJOR TASK AREA: SHUTTLE ELECTRICAL POWER, DISTRIBUTION, AND CONTROL (EPDC) SUBSYSTEM ELEMENT MODELING

TASK NAME/ NUMBER	TASK DESCRIPTION	EXPECTED OUTPUT
01	Establish a data base management scheme whereby EPDC and user load element characteristics and specifications are obtained in a timely manner with a formal NASA/JSC/Rockwell/Hughes interface, and clearly stated data requirements.	Organizational data flow, definite schedule and working group meetings, vendor visits.
02	Generate descriptive transfer function data, and equivalent mechanization for each EPDC source, control and distribution element based on current detailed element hardware performance specifications and vendor data.	Set of steady-state transfer functions; unit configuration and parameters.
03	Generate descriptive characteristics on each major important EPDC user subsystem including its admittance parameters, drive voltages or current detailed bus assignments, mission time profile (of adequate detail).	Set of user load characteristics.
04	Generate SYSTID model code for each of the models defined by the prior characterization tasks.	SYSTID code.
05	Obtain or generate transient response (i.e., step response) test data on all EPDC and user subsystem load elements, with adequate time resolution. Compare this data with SYSTID model simulated response data, for equivalent conditions, in order to validate these models...adjust SYSTID model parameters as necessary.	Comparitive transmit response plots and modified SYSTID model parameters.
06	Establish shuttle operating philosophy and mission mode criticality measures. Determine critical paths and EPDC/user elements, for subsequent fault simulation, and circuit protection analysis.	SYSTID simulation runs, and performance analysis.

5.0 GENERAL DISCUSSION

5.1 Introduction

The material in this section will, 1) introduce the basic concepts of the time-domain simulation of continuous systems, as exemplified by the SYSTID software enhanced and utilized in this study effort, 2) provide additional detail on the EPDC element model representations summarized in Section 2.2.

Acknowledgement is made at this point of those Hughes staff members who have contributed directly to this study, or to ancillary efforts. In particular, the outstanding SYSTID enhancements generated by Dale Paynter, with inter-active graphics I/O capability as added by John Forbes, must be noted. The EPDC data research and modeling efforts were carried out by Ivar Highberg, Nels Palmquist, and Johnetta MacCalla.

5.2 SYSTID Discussion

Some time ago, the need to accurately simulate real systems, particularly telecommunications systems, became apparent, and a time-domain simulation effort was initiated [78] at Hughes, on the Surveyor program. These efforts¹ of M. Fashano, W. Mayfield, N. Wagner and others were carried forward in succeeding years by D. Paynter and M. Fashano (and R. J. Rechter) under two NASA JSC contract efforts² [76, 77], culminating in the SYSTID time-domain simulation software. SYSTID represented a starting point for this study effort. Though the main thrust for SYSTID's genesis and application was to simulate telecommunications systems, its design was deliberately made sufficiently general to allow representation of a general set of physical systems. Thus, the application of SYSTID to the shuttle electrical power system was straight forward; only new library models, to represent the shuttle elements was necessary (Volume II, User Guide, report will list the telecommunications system model library currently available in SYSTID).

¹The SAMDAT simulation software

²NAS9-11743

Program Description

SYSTID is a system of computer routines that provides the analyst with a powerful tool for the transient simulation and analysis of complete systems (e.g., telecommunication, power, electronic, and servocontrol subsystems).

The program accepts as input a topological black box description of a system, automatically generates the appropriate algorithms, and then proceeds to execute the simulation program. Thus the user is not necessarily required to write the algorithms in a computer language nor possess a great facility in computer programming. The system description, including both topology and element information, is supplied to the program in a free-form, user-controller engineering language which is easily learned.

SYSTID offers the user enormous flexibility in the representation of system elements (i.e., black boxes). An element may be defined as:

- 1) An SYSTID library model
- 2) A user-written, temporary SYSTID model
- 3) A FORTRAN arithmetic expression involving any intrinsic SYSTID parameter, constants, variables, FORTRAN library functions, SYSTID library functions, model output nodes and user-supplied FORTRAN functions.

The SYSTID model library consists of a set of computer routines either written in FORTRAN or SYSTID, which have been stored on a library file and cataloged in the SYSTID directory. The user, at any time, can modify or replace the library and directory as he may choose; thus every user can easily create his own library. One unique characteristic of SYSTID is the capability of nesting models to a level of 100; that is, any model (or system) can reference up to 100 models, excluding itself. The nesting feature provides the user with the tools necessary to build a model library to suit his needs based on a canonic set of models.

The basic, or canonic, SYSTID library consists mainly of a group of routines that aid in the simulation of continuous functions, which may thus be presented by functions of the complex variable, s , as $G(s)$. The technique applied is that of the bilinear z -transform difference equation representation of $G(s)$. The transfer function may be defined in several ways in terms of its

poles and zeros or as one of the classical filter functions such as Bessel, elliptic, etc. The sample data routines accomplish all the necessary transformations in addition to the numerical processing such as integration and differentiation. In addition, all of the FORTRAN arithmetic features are an intrinsic part of the SYSTID library, although they do not appear in the directory.

The bilinear transform rather than the standard z-transform is used in the representation of continuous functions because it eliminates aliasing errors, making possible the realization of commonly encountered functions whose response does not approach zero at high frequencies. Note that aliasing of the system driving signals, however, is still possible if the user chooses an inappropriately low sampling rate.

Another aspect of the SYSTID model library is that it contains FORTRAN subroutines - that is, when a model (or system) is processed by SYSTID, the result is a FORTRAN subroutine (or main program) which is available to the user for any purpose, whether for SYSTID or not. Thus, SYSTID can be viewed as a FORTRAN program generator that converts a topological, nonprocedural input into a procedural language - FORTRAN. Although not unique to SYSTID, this aspect allows evaluation of mathematical problems via SYSTID with no concern for the input/output coding necessary in FORTRAN programs; that is, SYSTID may be used as a shorthand FORTRAN system.

The functional flow of SYSTID is sketched by Figure 5.2-1.

SYSTID flexibility is in part attained by designing the program to execute as a multipass processor in a batch mode of operation. The first phase reads the user input description of all models and/or a system and proceeds to formulate the corresponding FORTRAN algorithms. In this phase, the program checks for input errors such as erroneous model references, dangling nodes, etc. in which case appropriate error messages are issued. If the first phase terminates without fatal errors, the FORTRAN routines are automatically compiled and collected with the SYSTID library to form the second phase, that of executing the simulation.

Output from the program includes plots as well as tabulated data. Conventional output is any system node which may be individually selected, or

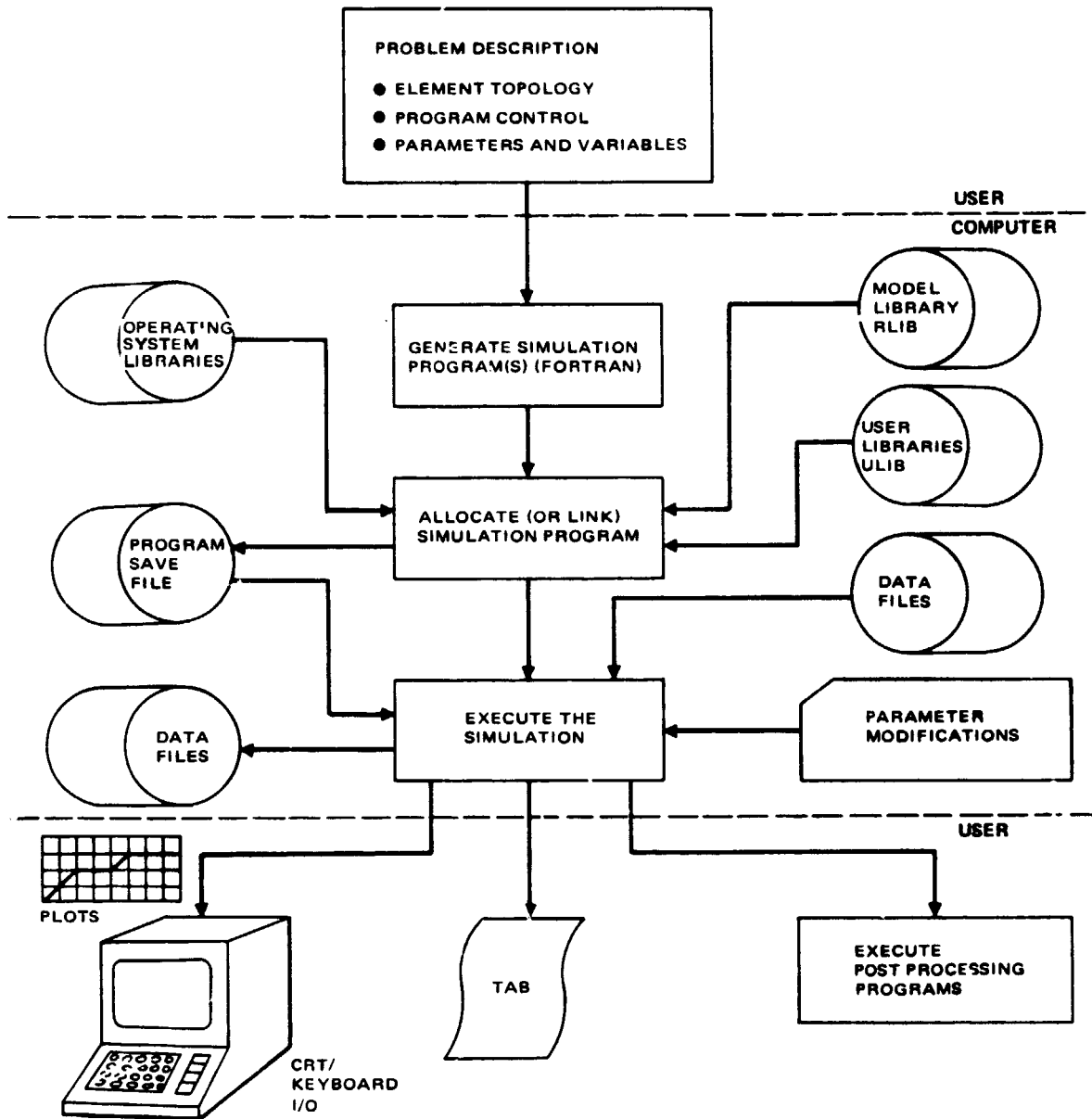


FIGURE 5.2-1. SYSTID TIME-DOMAIN SIMULATION SOFTWARE FUNCTIONAL FLOW

any variable whether intrinsic or user-defined. Plots can be produced on the printer as well as a digital plotter (e.g., CALCOMP, SC 4020). Printed data can be formatted, under user control, for either 8-1/2 by 11 inch pages or the full 11 by 14 inch page. In addition, input/output can be accommodated with a CRT/keyboard terminal, as exemplified by the JSC MOPS (Haxeltine 4000G) terminal. (Digital plotting is installation-dependent.)

The additional flexibility of linking to a user defined post processing routine is intrinsic to SYSTID when utilizing the POST system identifier. This feature allows the user to access the time histories of any node, or variable much the same way as the plot routines. As a matter of fact, the plot routines are indeed intrinsically named postprocessors. Utility routines are available to perform any necessary input/output for the user.

The user, because of the two phase aspect, has available to him several techniques for controlling his computer runs and ensuring that the most effective use is made of the machine time. The primary means is that of saving the results of the first phase (the collected simulation package) for subsequent reruns with alternate input data. Rerun would then simply entail a load-go operation, with input data provided at execution time by use of the DATA identifier in the first phase.

Some theoretical aspects of sampled data simulation which underlie SYSTID are summarized in Appendix 7.6.

5.3 Technical Discussion of SYS.ID Models

As the figure below illustrates, the shuttle EPDC can be functionally represented by 1) source generation, 2) source conversion elements, 3) power/load distribution and control elements, 4) user subsystem load elements. The entire shuttle electrical power system (EPS), from the analysis and simulation viewpoint, must include the user load elements, since they influence the electrical power, distribution and control (EPDC) subsystem so extensively. The status of the EPDC topology and the characterization of the EPDC elements is still in flux at this report's submission. Some reference procurement specifications

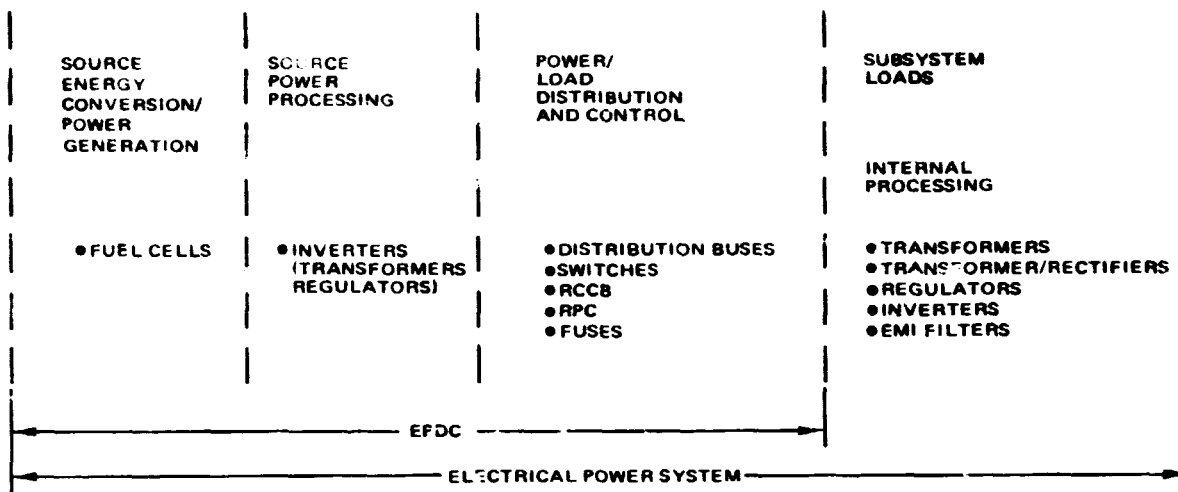


FIGURE 5.3-1. FUNCTIONAL ELEMENTS OF THE SHUTTLE ELECTRICAL POWER SYSTEM

are given in Appendix 7.5 for these EPDC elements, such as the inverter, RPC, RCCB, etc. The level of detail for the user load elements is much poorer, particularly (as the sample data sheets of Appendix 7.4 show) for transient response data, as opposed to steady-state response parameters.

The data to follow will be largely schematic in nature. Much of the detailed analysis is dependent on arbitrarily assumed equipment mechanizations, and lending an unjustified credence to the models should be avoided. Clearly, the modification to these SYSTID models can be made in a straightforward manner, as soon as the equipments are selected and are described in adequate detail for SYSTID modeling.

5.3.1 EPDC Models

Fuel Cell Model Development

The fuel cell is clearly an important, if not the most important EPDC element, in terms of its performance. Unfortunately, little explicit data was available which would indicate the transient response of the device as opposed to its steady-state response. Some data was obtained from an

interesting analysis [78], which unfortunately did not cover a sufficiently wide range of output current variation, or peak current, relative to the fuel cells anticipated for shuttle use. The non-linear second order RC lowpass network proposed¹ by McKechnie as an equivalent circuit thus was not amenable to extrapolation over the wider output current changes anticipated for the shuttle EPDC simulation. Table 5.3-1 is reproduced from this reference. (The Apollo hydrogen-oxygen fuel cell system manufactured by Pratt and Whitney² was deemed most applicable to shuttle EODC simulation).

TABLE 5.3-1. SUMMARY OF TYPICAL FC DATA, IN TERMS OF PARAMETERS SHOWN IN FIGURE 5.3-3 (AFTER McKECHNIE)

I (Amps)	ΔI (Amps)	E_0 (Volts)	R_1 (Ohms)	R_2 (Ohms)	R_3 (Ohms)	C_1 (Farads)	C_2 (Farads)
(Pratt & Whitney, Hydrogen-oxygen)							
0	1.4	37.48	0.1575	0.00951	0.256	15.66	3.41
1.4	1.6	36.71	0.128	0.0143	0.226	18.78	1.79
3.0	1.2	36.03	0.157	0.0129	0.227	13.2	1.45
4.2	1.3	35.44	0.096	0.00389	0.232	8.56	4.43
5.5	1.3	34.99	0.091	0.00314	0.217	10.67	3.83*
6.8	1.2	34.56	0.087	0.00271	0.199	9.25	5.03
(General Electric)							
0	1.6	6.232	0.038	0.00811	0.423	7.99	1.88
1.6	1.6	5.363	0.0561	0.00186	0.0969	5.38	2.445
3.2	1.6	5.132	0.0542	0.00166	0.0613	5.63	1.96
4.8	1.6	4.957	0.0486	0.00175	0.0414	5.46	3.56
6.4	1.6	4.818	0.0204	0.00111	0.0264	6.0	6.91
(Hydrazine-oxygen)							
0	1.28	12.62	0.1755	0.179	0.344	0.244	0.957
1.28	1.12	11.8	0.1392	0.106	0.182	0.2208	0.55
2.4	1.12	11.26	0.170	0.133	0.230	0.167	0.433

*The nominal 34.99 volt case was chosen, with C_1 , C_2 decreased by a factor of 10, in order to reduce the FC's rise time to convenient values.

¹A set of circuit parameters was defined for each load increment.

²The transient responses specified for the SYSTID model are consistent with P and W data (see page 7.4-9).

In particular, the fuel cell supplied only DC loads, with a solid-state inverter (to be discussed next) for conversion to AC, as shown in Figure 5.3-2.

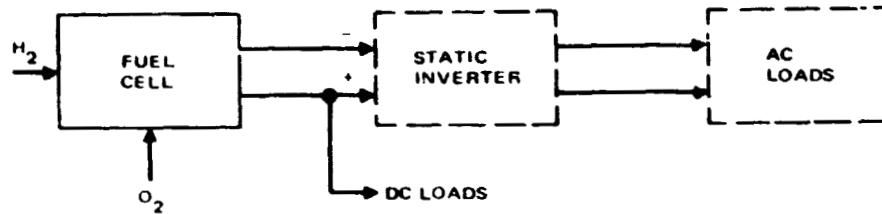


FIGURE 5.3-2. TYPICAL FUEL CELL/INVERTER SYSTEM

The equivalent circuit employed for the fuel cell is given by the simple¹ RC ladder network, as shown in Figure 5.3-3.

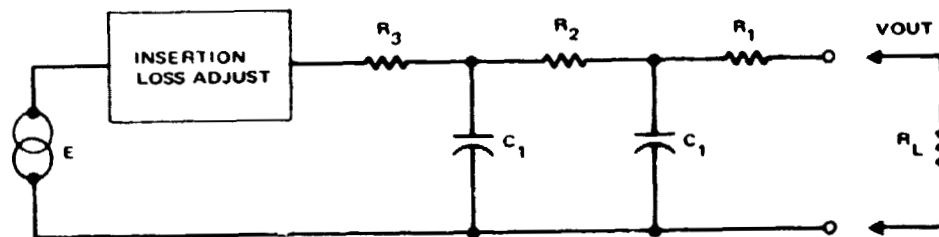


FIGURE 5.3-3. FC EQUIVALENT CIRCUIT

¹Deceptively so, since R_1 , R_2 , C_1 , C_2 are functions of nominal output voltage and load current. In particular, a variable gain compensates for insertion loss, so steady-state response is unaffected by the RC network.

The DC output voltage of this fuel cell versus output power after 5000 hours of performance is given in Figure 5.3-4.

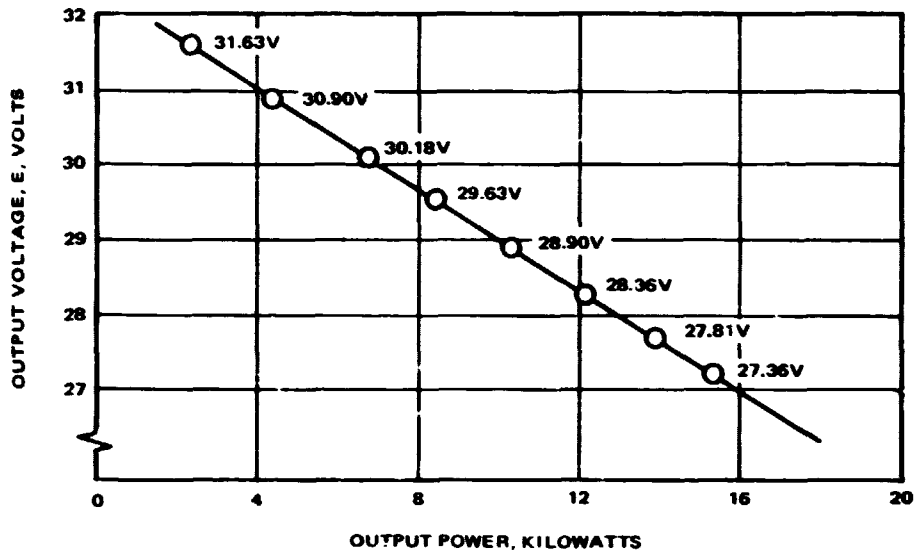


FIGURE 5.3-4. TYPICAL FUEL CELL OUTPUT VOLTAGE-POWER CHARACTERISTIC

In order to establish the reasonableness of the SYSTID model, with respect to its transient response, a step change in FC load was mechanized, as shown in Figure 5.3-5.

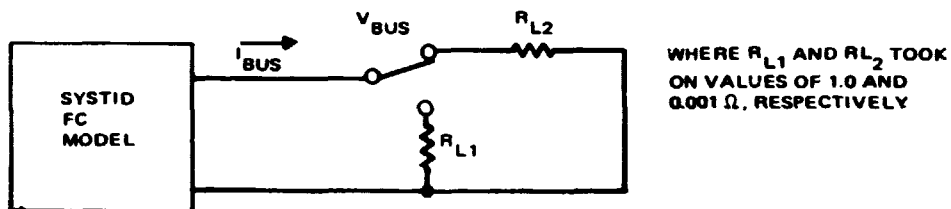


FIGURE 5.3-5. SYSTID STEP RESPONSE TEST CIRCUIT

The resultant fuel cell terminal voltage, BUS, and current delivered to the load, 1BUS are displayed in the CALCOMP plots of Figure 5.3-6(a) and (b).

Inverter Model Development

The inverter procurement specification (see Appendix 7.5) was used as a basis for generation of a representative block diagram. Functionally, the inverter can be represented as the cascade of elements shown in Figure 5.3-7.

This simplistic block diagram ignores some potentially important aspects of the inverter's performance, i.e., internal regulation and circuit protection, output transformer mechanization (nonlinear saturating-core operation with final waveform filtering for instance), and sensitivity to composite load power factor. Obtaining these and other detailed characteristics will require internal definition of the device by the vendor.

Monostable Multivibrator (Inverter)

The output of the multivibrator has an idealized waveform given in Figure 5.3-8.

where

$$t_r = t_d = A \ln \left(\frac{3 E_N}{E} \right)$$

and

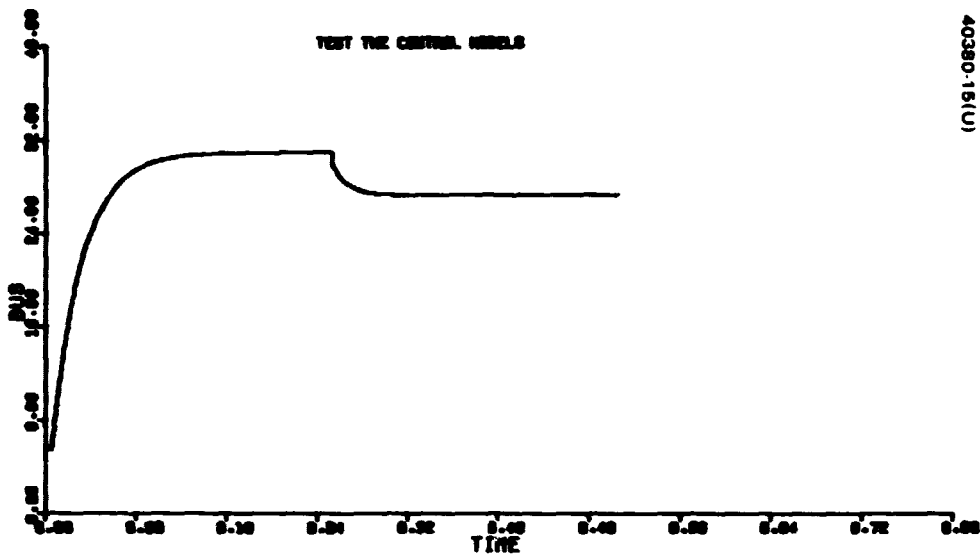
$$A = \frac{T}{2 \ln 3}$$

E = nominal output voltage

$E_N = E - (0.1)(28 - V_{IN})$, where V_{IN} is the input DC fuel cell voltage

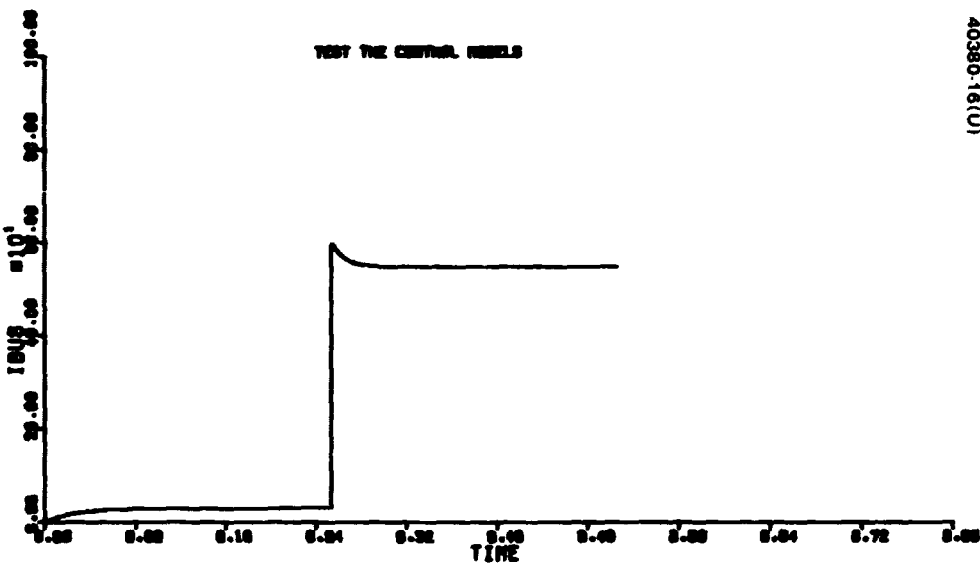
Waveshaping Filter (Inverter)

A lowpass filter is used to attenuate the odd harmonics present in this waveform, and produce an acceptable approximation to a sinusoidal waveform. In particular, a second order Chebyshev function with peak-to-peak ripple of 0.1 dB, and a ripple bandwidth 1.25 times the nominal multivibrator center frequency (clock rate) of 400 Hz.



40380-16(U)

FIGURE 5.3-6a. FUEL CELL TERMINAL (LOAD OR OUTPUT) VOLTAGE VERSUS TIME WITH A STEP CHANGE IN LOAD CURRENT (RESISTANCE)



40380-16(U)

FIGURE 5.3-6b. FUEL CELL OUTPUT CURRENT, I_{bus}, DELIVERED TO LOAD FOR A STEP CHANGE IN LOAD RESISTANCE

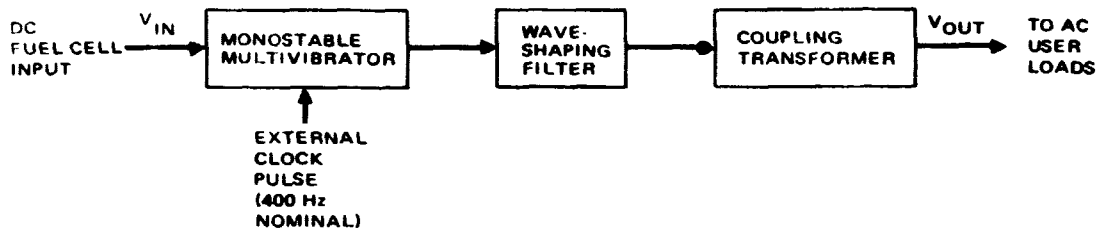


FIGURE 5.3-7. SYSTID INVERTER MODEL BLOCK DIAGRAM

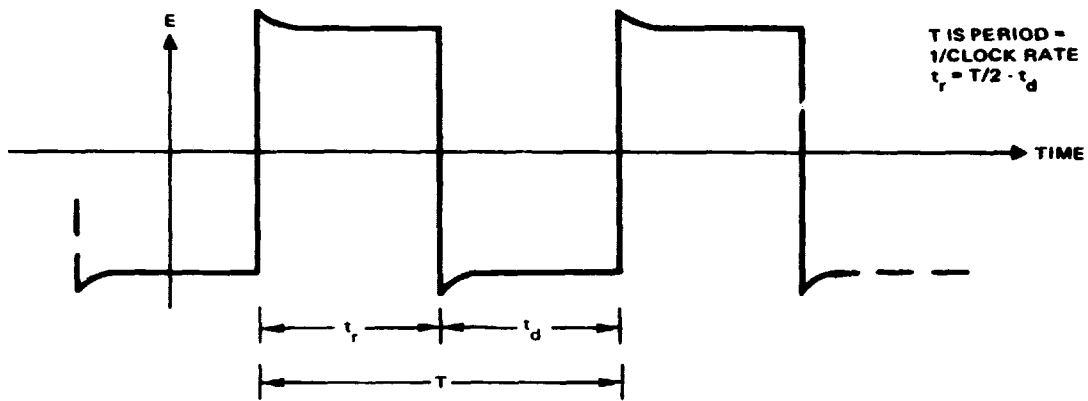


FIGURE 5.3-8. TYPICAL OUTPUT WAVEFORM OF THE SYSTID MULTIVIBRATOR SUBMODEL

Coupling Transformer (Inverter)

The coupling transformer can be represented by an ideal element, with unity coupling and linear operation over the range. (In order to preserve some inherent degree of self-regulation and minimize core weight, this transformer may actually be realized as a saturating core device.)

Given the linear model, a typical realization is shown in Figure 5.3-9.

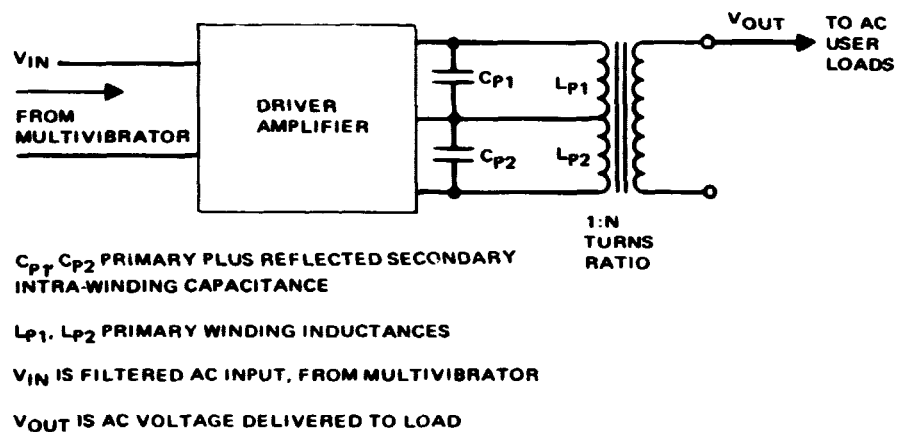
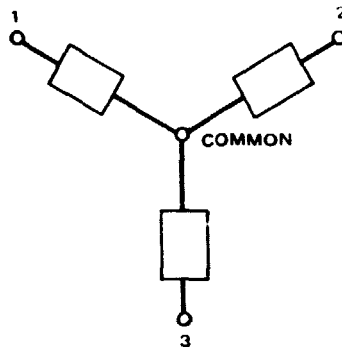


FIGURE 5.3-9. TYPICAL DRIVER AMPLIFIER/COUPLING TRANSFORMER SCHEMATIC

For assumed values of active device and transformer parameters, a voltage transfer function can be written in terms of $G(s)$ as

$$\frac{V_{out}}{V_{in}} = \frac{(1.414 \text{ CPF}) 1.07835}{1.5 \times 10^{-5} s^2 + .263 s + 571.0}$$

NOTE: For three-phase operation, the inverters are configured to effectively couple their outputs in a wye-connection, as sketched below:



In the simulation, the multivibrator outputs are sequenced in phase angle 0° , 120° , 240° , to achieve three-phase operation.

As in the case of the fuel cell, the SYSTID inverter model was tested for step response, as shown in Figure 5.3-10.

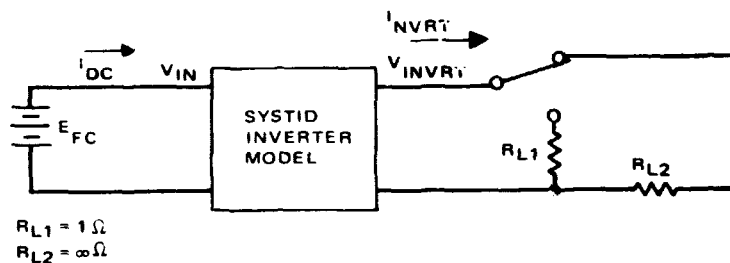


FIGURE 5.3-10. SYSTID INVERTER TEST STEP RESPONSE DIAGRAM

The resultant transient responses are given in Figures 5.3-11(a) and 5.3-11(b).

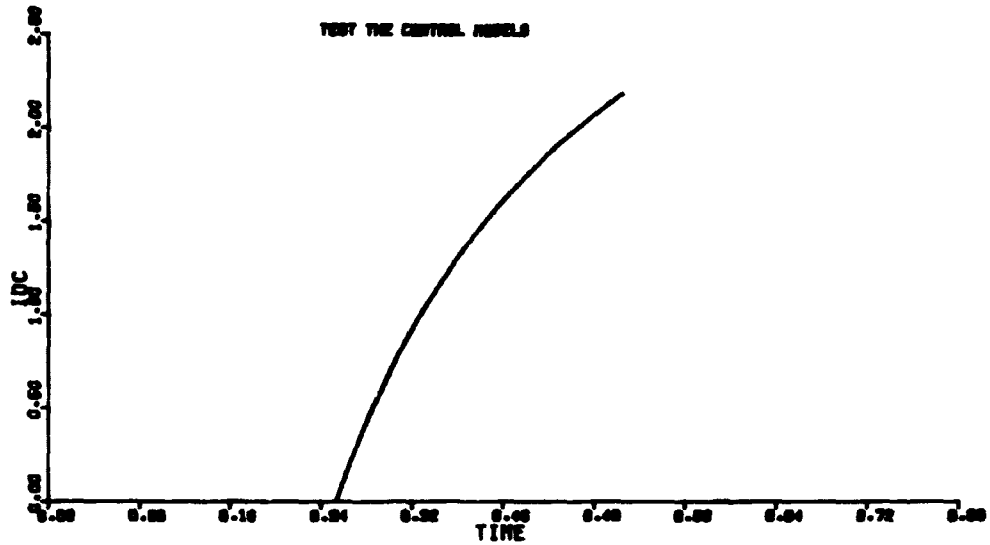


FIGURE 5.3-11a. INPUT DC CURRENT (REPRESENTING FUEL CELL) TO INVERTER VERSUS TIME, FOR A STEP CHANGE IN INVERTER LOAD IMPEDANCE

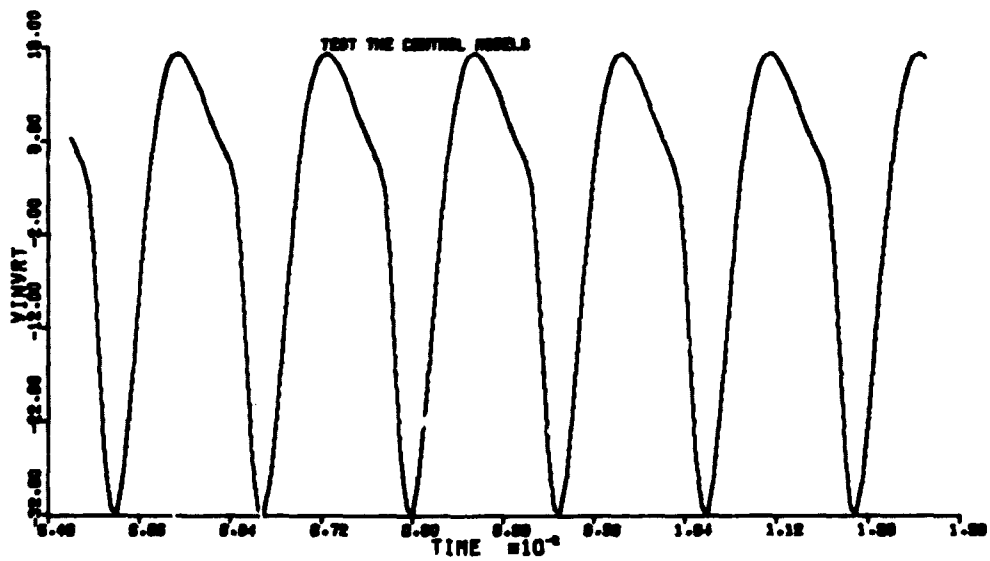
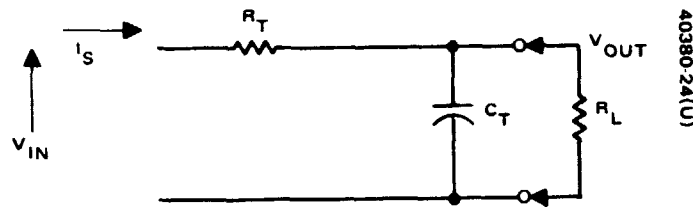


FIGURE 5.3-11b. INVERTER AC OUTPUT VOLTAGE VERSUS TIME, FOR A STEP CHANGE IN INVERTER LOAD IMPEDANCE

Distribution Bus (Cable) Model Development

A physically realizable power transmission cable is best represented by a distributed parameter equivalence. For purposes of convenience, we shall allow a simplified lumped-parameter equivalent circuit, namely a first order RC ladder network



R_T = total cable loss, ohms

C_T = total cable capacitance, farads

R_L = the load resistance, ohms

and where

$R_T = (R) (XL)$ XL , length of cable, feet

$C_T = (C) (XL)$ R , ohms/feet

C , farads/feet

The overall transfer function can be shown to be

$$\frac{V_{out}}{V_{in}} = G(S) = \frac{R_L}{(R R_L C)S + (R + R_L)}$$

Diode Model Development

Two different representations are used for the diode model, one ideal, the other more closely representative of an actual device.

Ideal Diode:

This is essentially a battery, whose voltage is identical to the diode junction potential, in series with a logical switch, to indicate conduction state.

Real Diode:

This representation employs the fundamental diode junction equation

$$I = I_{\text{sat}} \left[e^{\text{TH}\Delta V} - 1 \right]$$

where

I_{sat} = junction reverse (saturation) current, amperes

TH = constant = q/KT

ΔV = junction potential, volts

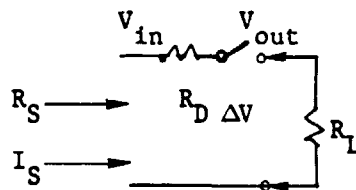
From which we may define

$$\frac{1}{R_D} = \frac{dI}{dV} = 39 I_{\text{sat}} e^{\text{TH}\Delta V}$$

where

R_D = junction impedance.

An equivalent circuit may thus be drawn:



$$\frac{V_{\text{out}}}{V_{\text{in}}} = \frac{R_L}{R_D + R_L} = \frac{R_L 39 I_S e^{39\Delta V}}{(R_L 39 I_S e^{39\Delta V} + 1)}$$

and R_S , the impedance presented to the source, which delivers I_S amperes is given by

$$R_S = R_L + R_D$$

$$I_S = V_{\text{in}}/R_S$$

Remote Control Circuit Breaker (RCCB) Model Development

The RCCB passes load current based on its rating which ranges from 15 to 100 amperes for the various dash numbers utilized in the EPDC, with a voltage drop ≤ 0.25 volt. At some overload condition, given as a percentage of rated current, the RCCB must trip and relieve the load (200 percent of rated current is minimum trip limit with the trip time being a decreasing function of overload current). It is also capable of being remotely energized, i.e., set¹ or opened. The control voltage, applied through a 1.3K ohm source resistance, from a bus other than the main buses, over a range of 24.0 to 40.0 volts shall set the RCCB. Removal of this voltage automatically opens the load circuit. A 28 vdc backup bus circuit can also energize the RCCB, and its load.

The functional flow of the RCCB is given in Figure 5.3-12.

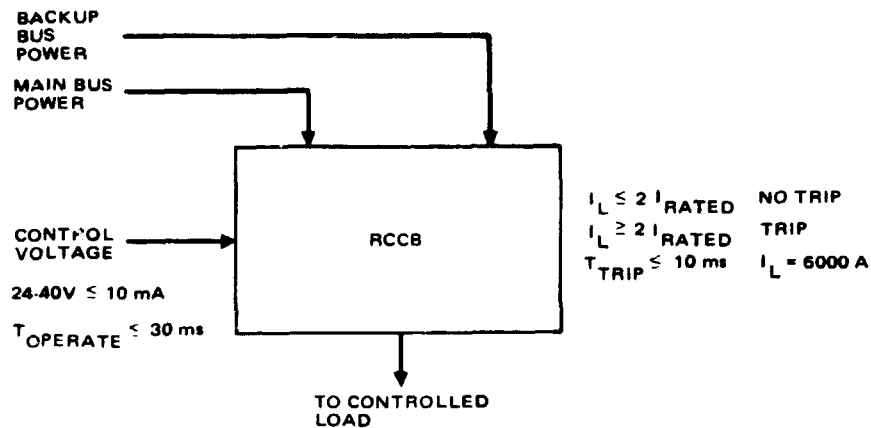


FIGURE 5.3-12. RCCB FUNCTIONAL FLOW DIAGRAM

¹The RCCB cannot be closed while an overload condition exists (magnetically latched).

Operational Sequences: If both main and backup power bus voltages are removed, RCCB is not to change state.

If control voltage is removed, RCCB must open.

If overload occurs, main contacts will trip open. In order to close load circuit again, control voltage must turn RCCB OFF, then ON.

The RCCB was modeled in SYSTID by assuming a dual representation, one a logical control sequence, the other an RLC network simulating a typical relay mechanization. Pictorially,

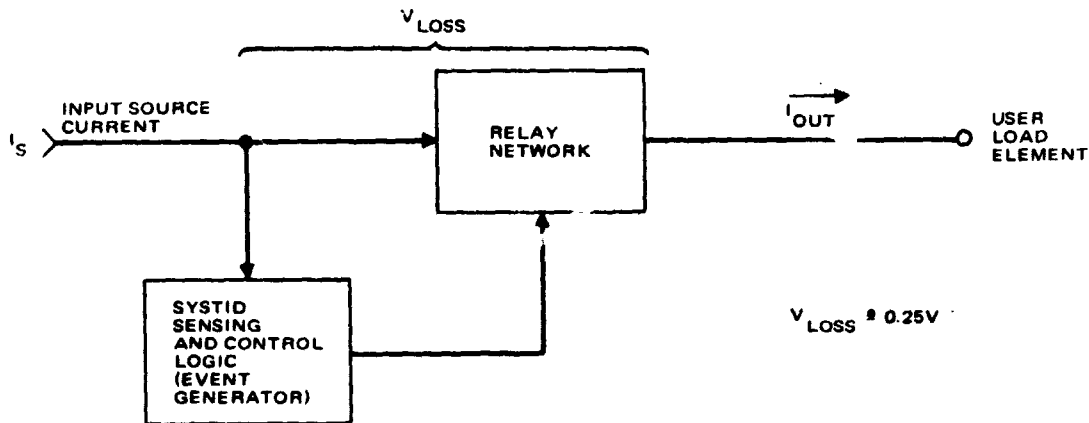


FIGURE 5.3-13. RCCB SYSTID MODEL FUNCTIONAL FLOW DIAGRAM

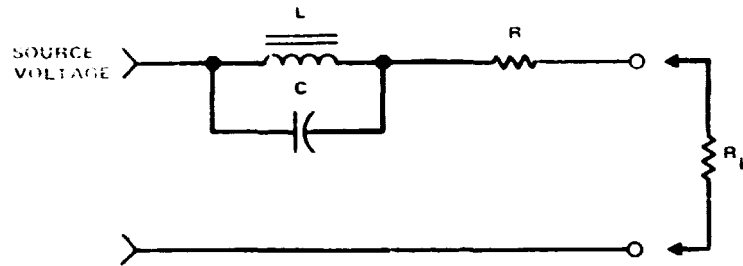
The RCCB transfer function representing load current flow thus becomes that of the relay network. A second order response given by the following $G(s)$

$$G(s) = \frac{(19.46/T_o^2)}{s^2 + (6.25/T_o)s + (19.46/T_o^2)}$$

where

$$T_o = 10 \text{ ms, } \sim \text{the rise time}$$

which represents an RLC network similar to



where R is the relay coil resistance; C its intrawinding (or discrete) capacitance, L the relay coil inductance.

Note that the circuit analyzed for transient response here is the load circuit. Presumably, a similar circuit exists for the control circuits (current simulation technique assumes no RCCB time constants directly in control path).

The transient response of the RCCB is tested in a SYSTID configuration similar to that shown for the inverter in Figure 5.3-10, i.e., driven by an ideal voltage source, allowing the measurement of RCCB input current, as shown in Figure 5.3-14.

Remote Power Controller (RPC) Model Development

The RPC is a power control device which can be controlled remotely, in similar fashion to the RCCB. The RPC differs from the RCCB mainly in its ability to limit the current delivered to the load, as well as provide trip-off overload protection. The RPC can be turned on with control voltages less than 14 volts, but more than 9 volts DC. For voltages between 6.5 volts and 9.0 vdc, the RPC will be shut off. No trip indication is currently anticipated for the RPC, although for analysis purposes, the SYSTID RPC model incorporates trip indication. The overload/trip characteristics of the RPC are given in Figure 5.3-15.

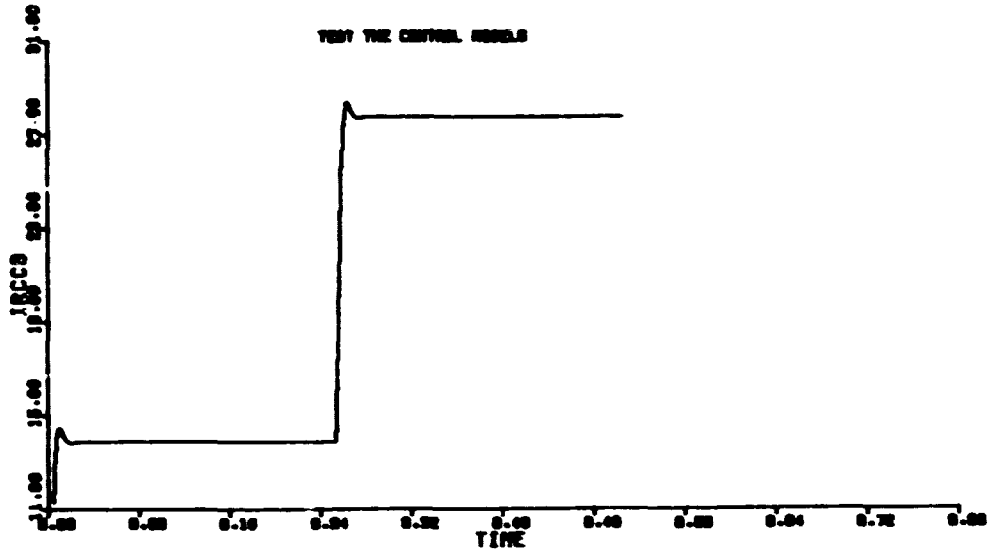


FIGURE 5.3-14. CURRENT DELIVERED TO THE LOAD BY THE RCCB VERSUS TIME, AS A FUNCTION OF A STEP CHANGE IN LOAD RESISTANCE

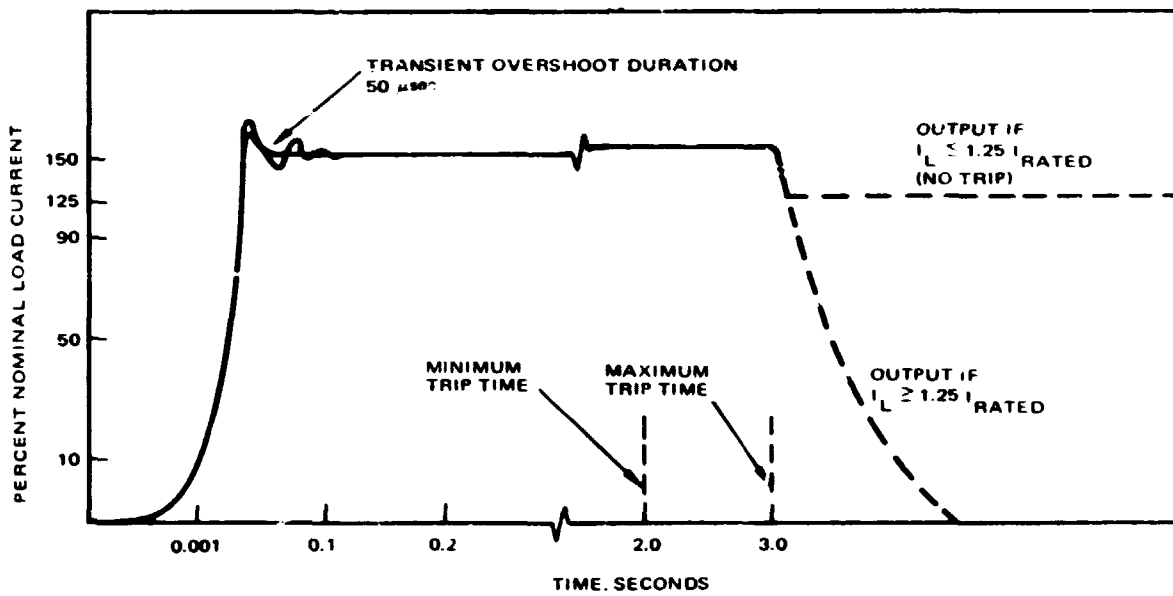


FIGURE 5.3-15. RPC CURRENT LIMITING CHARACTERISTIC

In addition, a fail-safe capability shall exist, i.e., a fusible link. The maximum load range of these devices is 20 amperes. The control voltages are generally supplied from the shuttle essential buses, and may be reset, subsequent to tripping, within 20 ms. Initial turn-on time is ≤ 2.5 ms, with turn-off times ≤ 4 ms. The rise times are generally ≤ 2 ms, the fall times ≤ 4 ms.

The RPC functional flow is given by Figure 5.3-16.

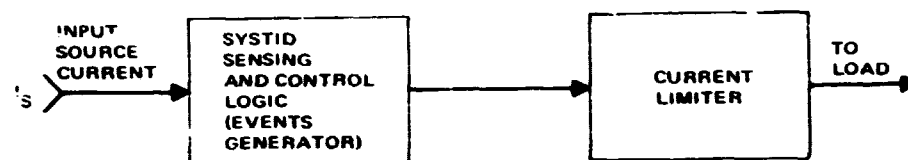


FIGURE 5.3-16. RPC FUNCTIONAL FLOW DIAGRAM

The functional flow in Figure 5.3-16 is similar to that of the RCCB, except that the relay element is replaced with the current limiter model. In similar fashion to that illustrated by Figure 5.3-10, the step response of the RPC is given by Figures 5.3-17(a) and 5.3-17(b).

5.3.2 LOAD MANAGEMENT AND SEQUENCING

In order to effectively interface with the enormous volume of data involved in the shuttle EPS, a model was developed for accessing a standardized load-defining data base. This model and its usage are implemented such that consistency is maintained between the SYSTID simulation and the SEPAP/RI available data format.

In conjunction with the LOADS model, a sequencer and associated software were developed such that a given sequence of events (or equipment time profiles) could be effectively used to control the SYSTID simulation.

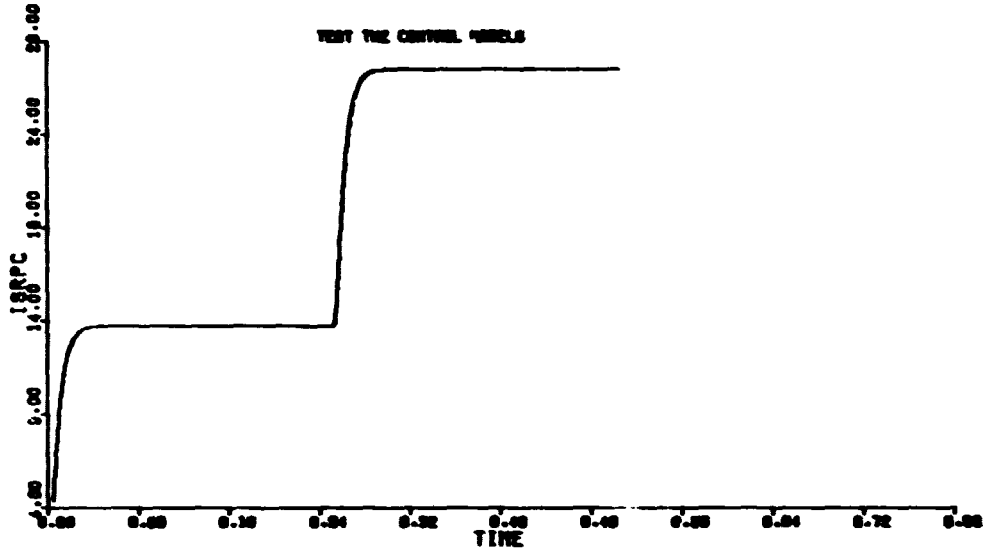


FIGURE 5.3-17a. SOURCE CURRENT DRAWN BY RPC VERSUS TIME, AS A FUNCTION OF A STEP CHANGE IN RPC LOAD IMPEDANCE (CURRENT)

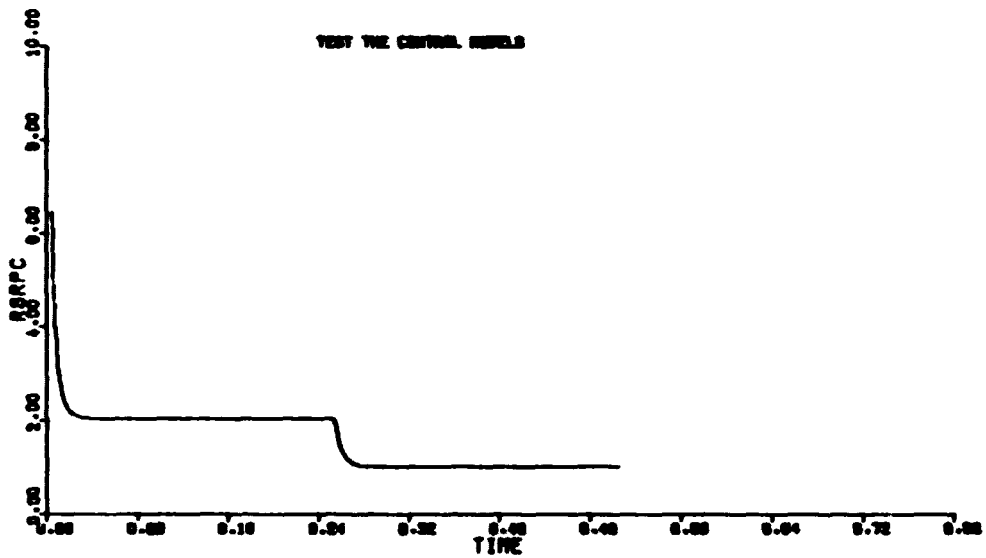


FIGURE 5.3-17b. RPC IMPEDANCE VIEWED BY SOURCE VERSUS TIME, AS A FUNCTION OF A STEP CHANGE IN LOAD IMPEDANCE (CURRENT)

The LOADS model uses input data which define a given SEPAP load number as follows:

- Equipment ID (6 digit RI code)
- Type of circuit protection device connection (RPC, RCCB, or FUSL)
- Type of load (resistive, inductive, etc.)

In conjunction with the above data, the model accesses the sequencer (LOADON) for definition of the equipment mode. Equipment modes have been defined as:

- 0 = ON
- 1 = standby
- 2 = short circuit failure
- 3 = open circuit failure
- 4-6 = open for definition
- 7 = OFF

Operation of the LOADS model requires UNIVAC data elements in TPF\$¹ named "LOADNNN" where NNN = 3 digit load number. If a data element is not available, the particular load is defaulted to an open circuit. The format of the data element can be seen in Appendix 7.1, which describes the procedure for building the load data base.

The sequencer routine LOADON is the interface to the Event Data File sequencer routine SHUTLE. Use of LOADON is as follows:

```
CALL LOADON (ID, MODE)
```

where

ID = 6 digit equipment number or 3 digit SEPAP switch
number

MODE = mode of the device at this time

¹UNIVAC EXEC 8 Temporary Program File.

Creation of the Event Data file is accomplished with the SORT routine, which reads data cards defining the time sequence for all equipment and system configuration and writes a compact data file organized for rapid access using minimal computer core.

Figure 5.3-18 describes the procedure necessary for preparation of the Load Data Base.

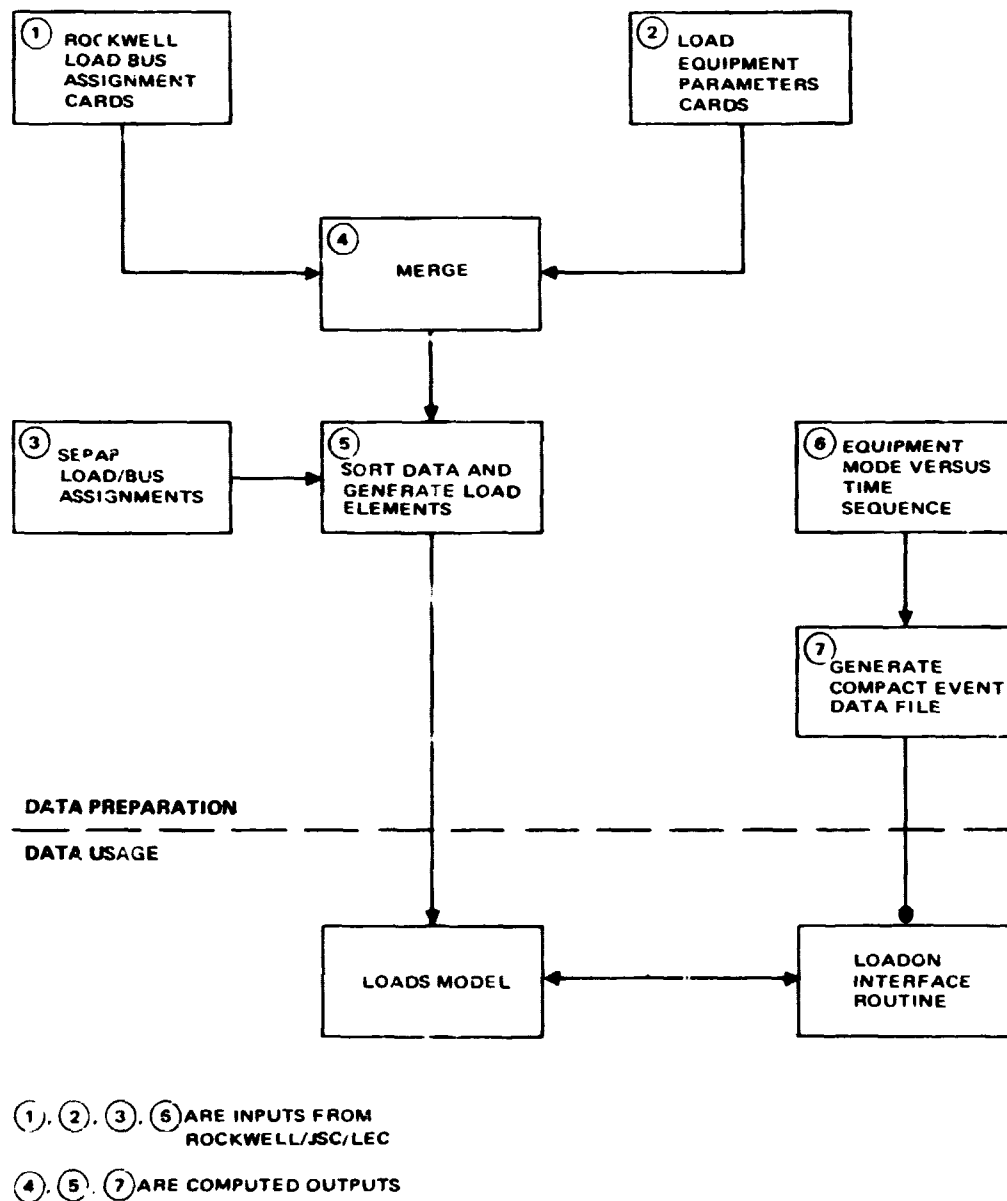


FIGURE 5.3-18. SYSTID EPDC LOAD DATA PREPARATION PROCEDURE AND SEQUENCE

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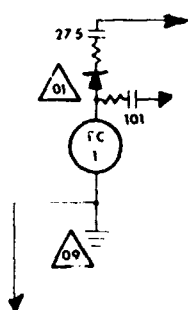
APPENDIX 7.1

EPDC TOPOLOGY AND LOAD BUS ASSIGNMENT DATA
AS PROCESSED FOR SYSTID SIMULATION

APPENDIX 7.1 - EPDC TOPOLOGY AND LOAD BUS ASSIGNMENT AS PROCESSED FOR SYSTID SIMULATION

The data in this appendix subsection provides the following information:
 1) an EPDC topology chosen for SYSTID simulation and performance analysis, namely the LEC schematic reproduced as Figure 7.1-1, 2) a listing of bus assignments derived from this schematic.

The load switches shown in Figure 7.1-1, as displayed in the small portion of the overall topology below, are logical in nature, i.e., for purposes of energizing a given load group in the LEC SEPAP time profile analysis.



Switches 275 and 101 in this topology sector are examples of logical elements found throughout the schematic of 7.1-1...in some instances they also correspond to actual devices.

The actual circuit protection devices, i.e., RPC, RCCB, or fuses are included within each load group...for instance, load group 171 includes load elements given by Table 7.1-1, each load element having its own circuit protection device. The listing of Table 7.1-2 displays the topology in tabular form as generated for SYSTID, from the connectivity data of Figure 7.1-1. The bus assignments shown are in terms of load groups, not yet in load element form.

TABLE 7.1-1. EXAMPLE LISTING OF LOAD GROUP 171 ELEMENTS
(ESSENTIAL SUB-BUS 3 AB/DIE)

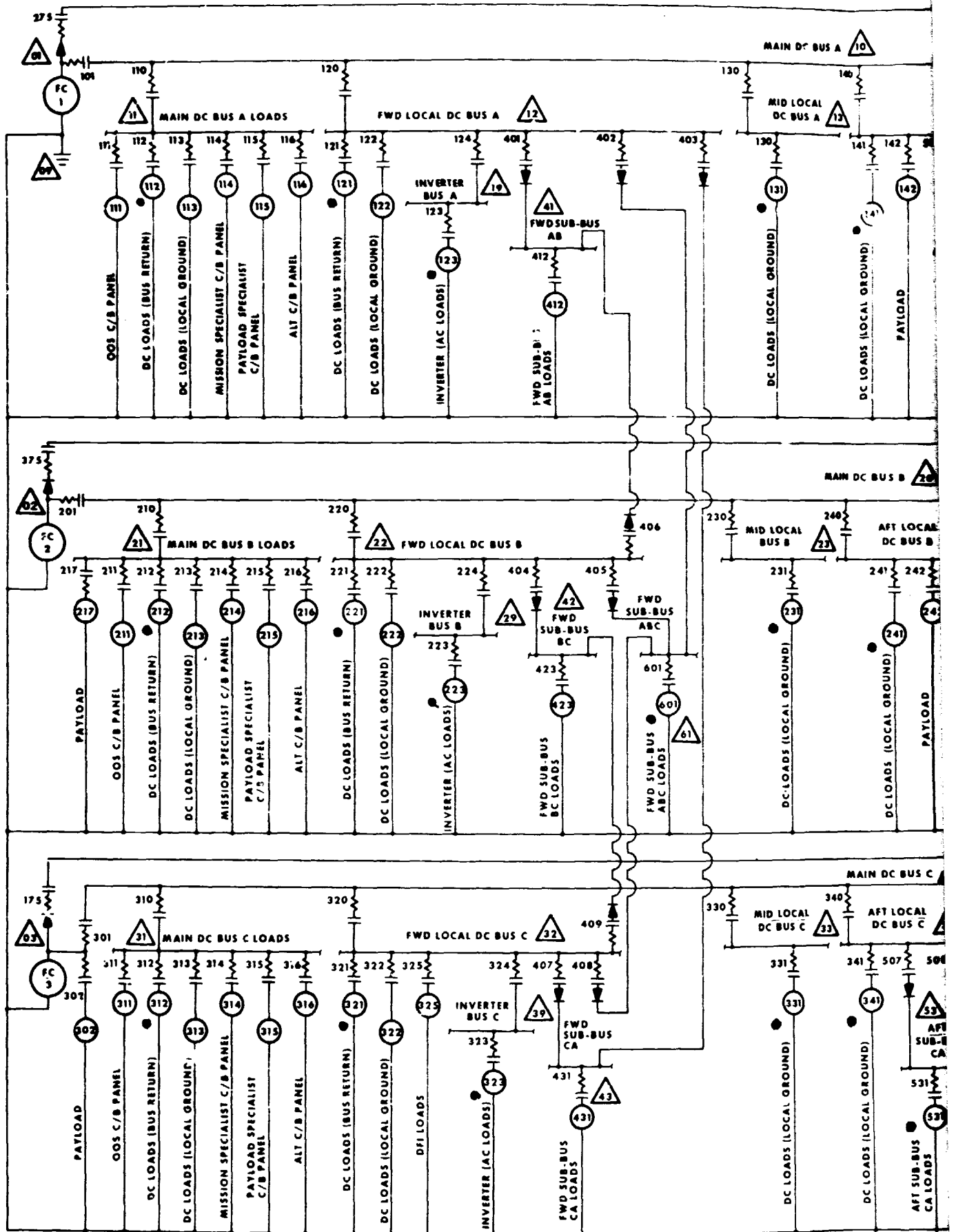
ELEMENT ID NO.	ELEMENT NAME	LOAD SUBSYSTEM NAME	WATTS DISSIPATED
04090000 04090010	MASTER TIMING UNIT { (WARM-UP) (OPERATE)}	ENVIRONMENTAL CONTROL AND LIFE SUPPORT	40 26
06040200	LOAD CONTROL ASSEMBLY UNIT #2	ELECTRICAL POWER DISTRIBUTION AND CONTROL	75
06040300	LOAD CONTROL ASSEMBLY UNIT #3		

Table 7.1-3 tabulates the load groups actually coded in SYSTID, in sequential order as read from left-to-right on Figure 7.1-1, first main bus A, then B, and finally C. Not all of the loads were coded, due to the ominous number of inconsistencies in the base data...a sufficient number were coded, to give a meaningful representation of the EPDC/user system. Straight-forward extension of the coding, given a validated data base, will rectify this situation. Due to discrepancies and omissions in the SEPAP bus assignment data (Appendix 7.2) as furnished to Hughes by LEC/JSC, some arbitrary assignments were made in the construction of these load groups.

As an example of how the Appendix 7.2 data has been utilized in generating these SYSTID load group assignments, we may take load group No. 171, and trace its development as summarized in Table 7.1-1 above.

From Figure 7.1-1, we note that load group 171 is driven by "essential bus 3 AB" (alternately stated, fuel cell No. 1, cross-coupled to both main load group, DC buses A and B). From Table 7.2-1, the EPDC/user subsystem element

C-18

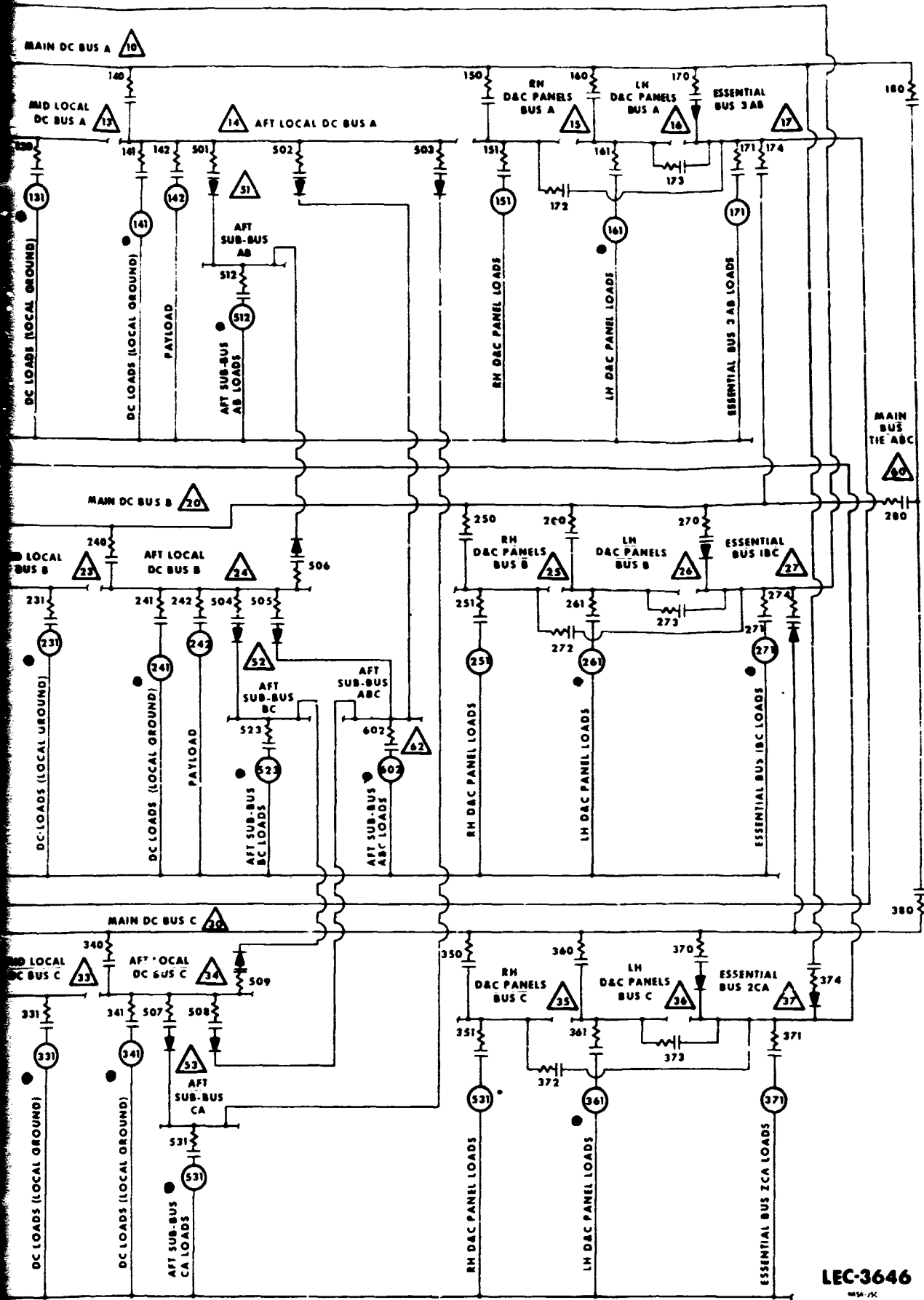


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FOLDOUT FRAME

FIGURE 7.1-1. SEPAP ELECTRICAL POWER DISTRIBUTION NETWORK SCHEMATIC

7.1.3



LEC-3646

FOLDOUT FRAME

bus assignments, that bus DLE, has three load elements. (DLE is the notation for DC load, main bus A, essential DC sub-bus). These three elements (one element has two states) were given in Table 7.1-4. Thus, at any given mission phase, the master timing unit will be in either its off, on or standby mode,¹ and one or both of the load control assembly units will be energized. Additional information can be gleaned from Table 7.2-1, namely, whether a particular circuit protection device has been selected for a given load element. For example, no particular device has been selected for the master timing unit (page 7.2-4, pointer); as a counter-example an RP(C) has been selected for the signal conditioning unit, ID#0413000 (see Appendix 7.3, page 7.3-7). In similar fashion, from Appendix 7.3, page 7.3-5, we determine that the load control assembly units #2 or #3 identified from Appendix 7.3, page 7.3-9, both employ fuses as circuit protection devices. The convention chosen for the illustrative simulation purposes of this study is that an fuse will be chosen as the representative circuit protection device unless otherwise indicated.

Further, to indicate which load groups have actually been represented by load element decomposition and modeled in SYSTID a solid dot has been placed adjacent to the load on the schematic of Figure 7.1-1.

Finally, Table 7.1-4 lists the load elements obtained from the LEC SEPAP card data supplied to Hughes, as a function of bus assignment. Note that this listing does not have load group sorting, per the topology of Figure 7.1-1.

¹As determined by the SYSTID Event Generator

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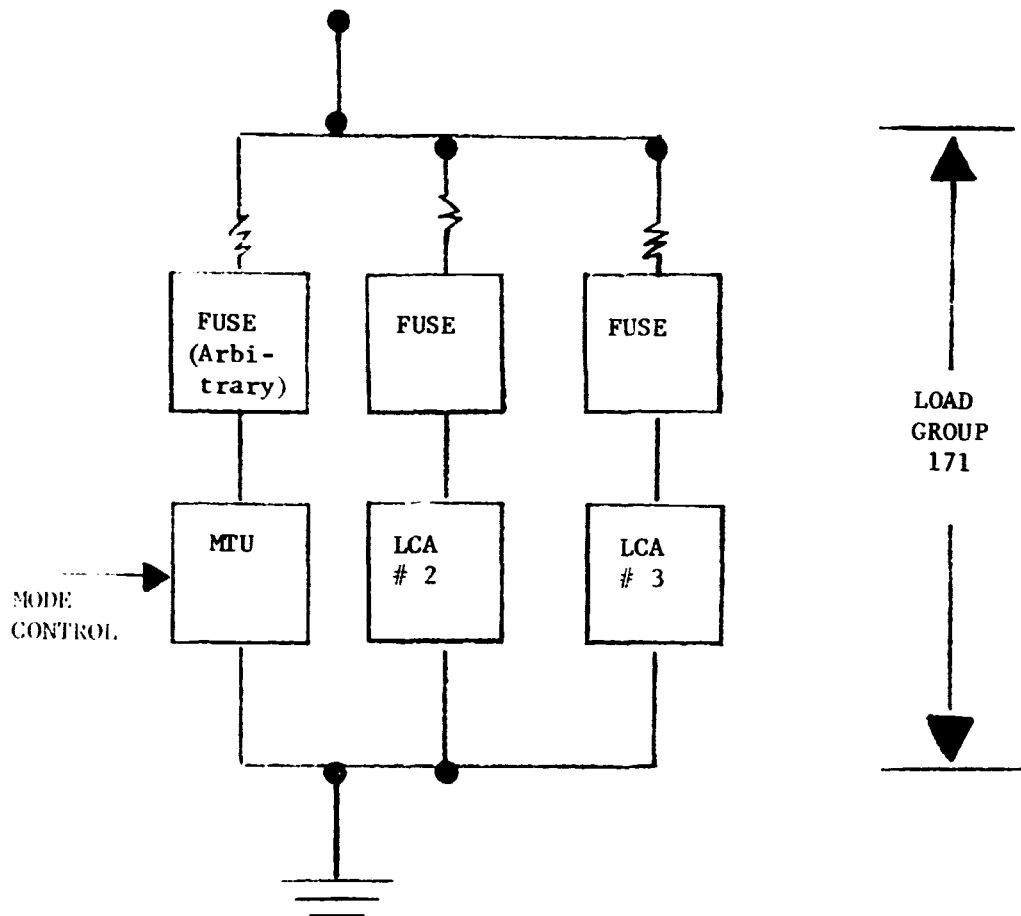


Figure 7.1-2. TYPICAL LOAD GROUP DECOMPOSITION INTO ITS CONSTITUENT LOAD ELEMENTS

SYSTEM LOAD BUS ASSIGNMENT LISTINGS (EPDC TOPOLOGY)

SYSTEM* SHUTTLE EPDC SYSTEM

DEFAULT, TSTOP= 205, DT= .5E-3, VOLT=28., CPF=1., FREQ=400., SFTTLE=5, F=3
 PLOT, I101, I120, I121, I512A, I201, I220, I221, I523B, I301, I320, I321, I531C, I271A,
 I271B, V10, V20, V30, I19, I29, I39

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4TRANS IMPLICIT REAL(I)

***** MAIN BUS A *****

G * FUEL CELL(R101,28.) * V01
 V01 * SWITCH(101,R10) * V10,R101

.....MAIN DC BUS A LOADS

V10 * SWITCH(110,R11) * V11,R110
 V11 * LOAD(111) * R111
 V11 * LOAD(112) * R112
 V11 * LOAD(113) * R113
 V11 * LOAD(114) * R114
 V11 * LOAD(115) * R115
 V11 * LOAD(116) * R116

110 R11=1./(1./R111+1./R112+1./R113+1./R114+1./R115+1./R116)

..... FWD LOCAL DC BUS A

V10 * SWITCH(120,R12) * V12,R120
 V12 * LOAD(121) * R121
 V12 * LOAD(122) * R122

..... INVERTER BUS A AND FWD SUB-BUS AB

V12 * LOAD(123) * R123
 V12 * INVERTER(FREQ,VOLT,CPF,R123) * V19,I19,R19
 V12,V22 * LOAD2(412) * R412A,R412B

120 R12=1./(1./R121+1./R122+1./R19+1./R412A+1./R601A+1./R431A)

..... MID-LOCAL DC BUS A

V10 * SWITCH(130,R13) * V13,R130
 V13 * LOAD(131) * R131

130 R13=R131

..... AFT LOCAL DC BUS A

V10 * SWITCH(140,R14) * V14,R140
 V14 * LOAD(141) * R141
 V14 * LOAD(142) * R142

..... AFT SUB-BUS AB

V14-V24 * LOAD2(512) * R512A,R512B

140 R14=1./(1./R141+1./R142+1./R512A+1./R602A+1./R531A)

..... BUS A PANELS AND ESSENTIAL BUS 3AB

V10 * SWITCH(150,R15) * V15,R150
 V10 * SWITCH(160,R16) * V16,R160
 V10 * SWITCH(170,R171A) * V17,R170
 V15 * SWITCH(172,R171D) * V172,R172
 V16 * SWITCH(173,R171E) * V173,R173
 V15 * LOAD(151) * R151
 V16 * LOAD(161) * R161
 V17,V20,V03,V172,V173 * LOAD5(171) * R171A,R171B,R171C,R171D,R171E

150 R15=1./(1./R151+1./R172)

151 R16=1./(1./R161+1./R173)

152 R17=R170

160 R10=1./(1./R110+1./R120+1./R130+1./R140+1./R150+1./R160+1./R170)

161 R10=1/(1./R10+1./R271A+1./R371A)

TABLE 7.1-2 SYSTID LOAD BUS ASSIGNMENT LISTINGS (EPDC TOPOLOGY)
(Continued)

```

***** MAIN BUS B *****
.
G * FUEL (FILL(R201,28.)) * V02
V02 * SWITCH(201,R20) * V20,R201
.
..... MAIN DC BUS B LOADS
V20 * SWITCH(210,R21) * V21,R210
V21 * LOAD(217) * R217
V21 * LOAD(211) * R211
V21 * LOAD(212) * R212
V21 * LOAD(213) * R213
V21 * LOAD(214) * R214
V21 * LOAD(215) * R215
V21 * LOAD(216) * R216
210 R21=1./(1./R217+1./R211+1./R212+1./R213+1./R214+1./R215+1./R216)
.
..... FWD LOCAL DC BUS B
.
V20 * SWITCH(220,R22) * V22,R220
V22 * LOAD(221) * R221
V22 * LOAD(222) * R222
.
..... INVERTER BUS B AND FWD SUB-BUSES AB AND ABC
.
V22 * LOAD(223) * R223
V22 * INVERTER(FREQ,VOLT,CPF,R223) * V29,I29,R29
V22,V32 * LOAD2(423) * R423A,R423C
V12,V22,V32 * LOAD3(601) * R601A,R601B,R601C
220 R22=1./(1./R221+1./R222+1./R29+1./R423B+1./R601R+1./R412R)
.
..... MID-LOCAL BUS B
.
V20 * SWITCH(203,R23) * V23,R230
V23 * LOAD(231) * R231
230 R23=R231
.
..... AFT LOCAL DC BUS B AND AFT SUB/BUSES BC AND ABC
.
V20 * SWITCH(240,R24) * V24,R240
V24 * LOAD(241) * R241
V24 * LOAD(242) * R242
V24,V34 * LOAD2(523) * R523A,R523C
V14,V24,V34 * LOAD3(602) * R602A,R602B,R602C
240 R24=1./(1./R241+1./R242+1./R523B+1./R602R)
.
..... BUS B PANELS AND ESSENTIAL BUS 1BC
.
V20 * SWITCH(250,R25) * V25,R250
V20 * SWITCH(260,R26) * V26,R260
V20 * SWITCH(270,R271B) * V27,R270
V25 * SWITCH(272,R271D) * V272,R272
V26 * SWITCH(272,R271E) * V273,R273
V25 * LOAD(251) * R251
V26 * LOAD(261) * R261
V01,V27,V30,V272,V273 * LOAD5(271) * R271A,R271B,R271C,R271D,R271E
250 R25=1./(1./R251+1./R272)
251 R26=1./(1./R261+1./R273)
252 R27=R270
260 R20=1./(1./R210+1./R220+1./R230+1./R240+1./R250+1./R260+1./R270)
261 R20=1./(1./R20+1./R171B+1./R371B)

```

TABLE 7.1-2 SYSTID LOAD BUS ASSIGNMENT LISTINGS (EPDC TOPOLOGY)
 (Continued)

```

*****
G * FUEL DEL (301,28.) * V01
V01 * SWITCH(301,R301) * V30,R301
.
.....MAIN DC BUS C LOADS
.
V30 * SWITCH(310,R311) * V31,R310
V31 * LOAD(311) * R311
V31 * LOAD(312) * R312
V31 * LOAD(313) * R313
V31 * LOAD(314) * R314
V31 * LOAD(315) * R315
V31 * LOAD(316) * R316
310 R31=1./(1./R311+1./R312+1./R313+1./R314+1./R315+1./R316)
.
.....FWD LOCAL DC BUS C
.
V30 * SWITCH(320,R32) * V32,R320
V32 * LOAD(321) * R321
V32 * LOAD(322) * R322
V32 * LOAD(325) * R325
.
..... INVERTER BUS C AND FWD SUB-BUS CA
.
V32 * LOAD(323) * R323
V32 * INVERTER(FREQ,VOLT,CPF,R323) * V39,I39,R39
V12,V32 * LOAD2(431) * R431A,R431C
320 R32=1./(1./R321+1./R322+1./R325+1./R39 +1./R431C+1./R601C+1./R423C)
.
.....MID LOCAL DC BUS C
.
V30 * SWITCH(330,R33) * V33,R330
V33 * LOAD(331) * R331
330 R33=R331
.
..... AFT LOCAL DC BUS C AND AFT SUB-BUS CA
.
V30 * SWITCH(340,R34) * V34,R340
V34 * LOAD(341) * R341
V14,V34 * LOAD2(531) * R531A,R531C
340 R34=1./(1./R341+1./R531C+1./R523C+1./R602C)
.
..... BUS C PANELS AND ESSENTIAL BUS 2CA
.
V30 * SWITCH(350,R35) * V35,R350
V30 * SWITCH(360,R36) * V36,R360
V30 * SWITCH(370,R371C) * V37,R370
V35 * SWITCH(372,R371D) * V372,R372
V36 * SWITCH(373,R371E) * V373,R373
V35 * LOAD(351) * R351
V36 * LOAD(361) * R361
V10,V02,V30,V372,V373 * LOAD5(371) * R371A,R371B,R371C,R371D,R371E
350 R35=1./(1./R351+1./R372)
351 R36=1./(1./R361+1./R373)
352 R37=R370
360 R30=1./(1./R310+1./R320+1./R330+1./R340+1./R350+1./R360+1./R370)
361 R30=1./(1./R30+1./R171C+1./R271C)
4TRANS I1101=V10/R101
4TRANS I1120=V10/R120
4TRANS I1121=V12/R121
4TRANS I1122=V12/R122
4TRANS I1512A=V14/R512A
4TRANS I12001=V20/R20
4TRANS I1220=V20/R220
4TRANS I1221=V22/R221
4TRANS I1238=V24/R523B
4TRANS I1301=V30/R301
4TRANS I1320=V30/R320
4TRANS I1321=V32/R321
4TRANS I1331C=V34/R531C
4TRANS I1271A=V01/R271A
4TRANS I1271B=V27/R271B
END
    
```


TABLE 7.1-3 SYSTID LOAD DEFINITION LISTING
(Continued)

MAIN BUS B LOADS

L O A D 2 2 1

1.	D2F	1010200	RP	IMU #2 OPERATE	1	160.00
4.	D2F	1010210	RP	IMU #2 STANDBY	1	55.00
4.	D2F	1110200	RP	REACTION JET DRVR #2 FWD	1	55.00
4.	D2F	4140000		SIG COND UNIT=F/C AREA	1	55.00
6.	D2F	4140000		SIG COND UNIT=FWD RCS	1	55.00
6.	D2F	6010200	RC	INVERTERS 1PH-750VA-80C	1	.00

L O A D 2 1 2

1.	D2G	30080200	FCP #2	START + SUST MTR	1	6000.00
----	-----	----------	--------	------------------	---	---------

L O A D 2 2 3

1.	A2	3A	3310100	INTEGRAL LIGHTS=LEFT/CTR	1	132.00
4.	A2	3A	3310200	INTEGRAL LIGHTS=OVHD	1	132.00
4.	A2	3A	3310300	INTEGRAL LIGHTS=RIGHT	1	132.00
4.	A2	3A	3310400	INTEGRAL LIGHTS=REAR	1	132.00
6.	A2	3C	30090200	FCP #2 PUMP + H2O SENSOR	1	150.00
6.	A2	3C	2170200	TACAN #2	1	150.00

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TABLE 7.1-3 SYSTEM LOAD DEFINITION LISTING
(Continued)

MAIN BUS C LOADS

				L O A D 3 1 2		
1.	D3G	30080300	FCP #3 START + SUST MTR	1	6000.00	
L O A D 3 2 1						
10.00	D3G	1010300	IMU #3 OPERATE	1	160.00	
00.00	D3G	1010310	IMU #3 STANDBY	1	55.00	
00.00	D3G	6010300	INVERTERS 1PH-750VA-80C	1	60.00	
00.00	D3G	6060300	DC PWR CNTLR ASSY-FWD #3	1	260.00	
00.00	D3G	6100300	INV DIST + CNTL ASSY #3	1	20.00	
00.00	D3G	6160000	EVLSS BAT CHARGER	1	5.00	
00.00	D3G	6180000	EVLSS PWR SUPPLY	1	75.00	
00.00	D3G	7030300	MDM #F3	1	40.00	
00.00	D3G	22100000	PROP MANIF ISOL VLV -FWD	1	84.00	
10.00	D3G	40100200	OVEN HEATER #2	1	150.00	
11.00	D3G	40330200	DIVERTER VALVE #2	1	19.50	
L O A D 3 2 3						
1.	A3 3A	30050300	FCP #3 PUMP + H2O SENSOR	1	150.00	
2.	A3 3C	2170300	TACAN #3	1	150.00	
L O A D 3 3 1						
00.00	D3G	6080300	MAIN DC DIST + CNTL ASSY #3	1	20.00	
00.00	D3G	6120300	DC PWR CNTL ASSY-MID #3	1	30.00	
00.00	D3G	60660300	FCP #3 CO2 PURGE VALVE #3	1	10.00	
00.00	D3G	60070300	FCP #3 GHN PURGE VALVE #3	1	10.00	
00.00	D3G	60150300	H2O LINE HEATER #3 FCP #3	1	15.00	
00.00	D3G	60170300	FCP #3 THERMAL CNTL MTR	1	150.00	
00.00	D3G	61120300	SOLENOID VLV FCP #3	1	55.00	
00.00	D3G	61150300	SOL VLV MANIFOLD #3	1	56.00	
00.00	D3G	61170200	HEATERS (OXYGEN) SET #2	1	394.50	
00.00	D3G	61170300	HEATERS (OXYGEN) SET #3	1	394.50	
00.00	D3G	61180200	HEATERS (HYDROGEN) SET #2	1	81.00	
00.00	D3G	61180300	HEATERS (HYDROGEN) SET #3	1	81.00	

TABLE 7.1-3 SYSTID LOAD DEFINITION LISTING
(Continued)

MAIN BUS C LOADS

L O A D 3 4 1

1	D3A	1080300	RP	ASCENT YVC	DRVR #3	AFT	1	190.50
2	D3A	1090200	RP	AFRO	SRRV AMP #2	AFT	1	107.77
3	D3A	1130300	RP	XATE	GYRO ASSY #2	AFT	1	203.00
4	D3A	4060200	RP	SIG COND	UNIT #2	AFT	1	50.00
5	D3A	7060300	RP	SIG COND	UNIT #3	AFT	1	50.00
6	D3A	5120200	P	SIG COND	UNIT #3	AFT	1	50.00
7	D3A	5060200	P	SIG COND	UNIT #3	AFT	1	50.00
8	D3A	5080100	P	SIG COND	UNIT #3	AFT	1	50.00
9	D3A	5080200	P	SIG COND	UNIT #3	AFT	1	50.00
10	D3A	5130100	P	SIG COND	UNIT #3	AFT	1	50.00
11	D3A	5130200	P	SIG COND	UNIT #3	AFT	1	50.00
12	D3A	5160100	P	SIG COND	UNIT #3	AFT	1	50.00
13	D3A	5160200	P	SIG COND	UNIT #3	AFT	1	50.00
14	D3A	6050300	P	LOAD PR CNTL	ASSY #2	AFT	1	190.50
15	D3A	6070300	P	MDM OFI	MDM	AFT	1	160.00
16	D3A	7060000	P	ENG INT	INTERFACE UNIT #3	AFT	1	50.00
17	D3A	7150300	P	RATE	GYRO ASSY	AFT	1	45.00
18	D3A	16010200	P	MDM OFI	SET 2	AFT	1	150.00
19	D3A	16020200	P	PIC	SIGNITION SET 2	AFT	1	150.00
20	D3A	16040200	P	PIC	SIGNITION SET 2	AFT	1	150.00
21	D3A	16050200	P	PIC	SIGNITION SET 2	AFT	1	150.00
22	D3A	16060200	P	PIC	SIGNITION SET 2	AFT	1	150.00
23	D3A	16070200	P	SIG COND	SET 2	AFT	1	320.00
24	D3A	20020300	RP	MAIN ENG	ITR #3	AFT	1	300.00

L O A D 5 3 1

1	D3A	20050000	F	LOZ	FWD VLV #1 (O/B)	SOL	1	40.00
2	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
3	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
4	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
5	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
6	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
7	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
8	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
9	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
10	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
11	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
12	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
13	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
14	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
15	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
16	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
17	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
18	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
19	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
20	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
21	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
22	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
23	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
24	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
25	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
26	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
27	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
28	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
29	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
30	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
31	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
32	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
33	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
34	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
35	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
36	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
37	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
38	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
39	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
40	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
41	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
42	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
43	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
44	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
45	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
46	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
47	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
48	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
49	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
50	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
51	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
52	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
53	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
54	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
55	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
56	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
57	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
58	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
59	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
60	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
61	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
62	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
63	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
64	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
65	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
66	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
67	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
68	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
69	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
70	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
71	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
72	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
73	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
74	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
75	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
76	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
77	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
78	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
79	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
80	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
81	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
82	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
83	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
84	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
85	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
86	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
87	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
88	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
89	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
90	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
91	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
92	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
93	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
94	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
95	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
96	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
97	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
98	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
99	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00
100	D3A	20050000	F	LOZ	TRIP VLV	OPEN SOL	1	40.00

L O A D 3 6 1

1	D3L	1030300		STAR	TRKER + LT SHLD #3		1	20.00
2	D3L	1040300		AIR	DATA XDCR ASSY #3		1	45.00
3	D3L	3010300		ATTI	TUDE DIR IND-AFT #3		1	14.60
4	D3L	3130000		SURV	POSITION IND		1	5.00
5	D3L	3180200		EVENT	TIMER #2		1	4.00
6	D3L	3190400		CRT	DISPLAY UNIT #4		1	90.00
7	D3L	3210400		DISP	PLAY ELECT UNIT #4		1	207.30
8	D3L	4090300		SIG	COND UNIT-FWD #3		1	35.00
9	D3L	7040400	RP	MDM	OFF		1	40.00
10	D3L	7100200		MDM	OFF		1	40.00
11	D3L	7100300		MDM	OFF		1	40.00
12	D3L	7100400		MDM	OFF		1	40.00

TABLE 7.1-4

LISTING OF LOAD ELEMENT BUS ASSIGNMENTS, AS PROCESSED FROM LEC
CARD DATA (APPENDIX 7.2)

0X0T

***** BUS ID A3 *****
2521100 2521200

***** BUS ID D2F *****
22210000

***** BUS ID D3F *****
22210000

***** BUS ID A *****
2180000 3330100 3330200 3330300 2032000 31010100 31010200
31010300 31010400 40080000 40110100 40110200 40140000 40160000
40170000 40320100 40320200 50020100 50020200 50020300 50160100
50160200 50160300 51020000 51030000 51050000 51060100 51060200
51070100 51070200 51080000 51090000 51100000 51110000 51120100
51120200 51150000 51160000 51170000 51180000 52040000 52050000
52060000 52070000 52080000 52100000 52160000 52170000 52180000
52200000 52320000 52330000 52340000 52350000

***** BUS ID A 3A *****
2511000 40010200 40010300 40020200 40050100 40050200 40050300
40050400 40050500 40050600 40060200 40060300 40090200 40090300
40290100 40290110 40290120 40290200 40290210 40290220

***** BUS ID A 3B *****
2511000 40010200 40010300 40020200 40050100 40050200 40050300
40050400 40050500 40050600 40060200 40060300 40090200 40090300
40290100 40290110 40290120 40290200 40290210 40290220

***** BUS ID A 3C *****
2511000 40010200 40010300 40020200 40050100 40050200 40050300
40050400 40050500 40050600 40060200 40060300 40090200 40090300
40290100 40290110 40290120 40290200 40290210 40290220

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TABLE 7.1-4 LISTING OF LOAD ELEMENT BUS ASSIGNMENTS, AS PROCESSED FROM
(Continued) LEC CARD DATA (APPENDIX 7.2)

```

10/30/74 14109131 100748 000155074 000155 829 50
*****
BUS ID A1 *****
50110100 50140100

*****
BUS ID A1 3A *****
2501000 20010100 30050100 40010100 40020100 40020300 40060100
40090100

*****
BUS ID A1 3A *****
20010200

*****
BUS ID A1 3A *****
20010300

*****
BUS ID A1 3B *****
2501000 30050100 40010100 40020100 40020300 40060100 40090100

*****
BUS ID A1 3C *****
2170100 2501000 30050100 40010100 40020100 40020300 40060100
40090100

*****
BUS ID A2 *****
50110200 50140200

*****
BUS ID A2 3A *****
3310100 3310200 3310300 3310400 30050200

*****
BUS ID A2 3B *****
30050200

*****
BUS ID A2 3C *****
2170200 30050200

*****
BUS ID A3 *****
2531100 2531200 50110300 50130100 50130200 50130300 50140300

```

TABLE 7.1-4 LISTING OF LOAD ELEMENT BUS ASSIGNMENTS, AS PROCESSED FROM
(Continued) LEC CARD DATA (APPENDIX 7.2)

```

10/30/74  14:09131  10074R  000155074  000155  S29  50
*****
BUS ID A3 3A *****
3310100  3310200  3310300  3310400  30050300

*****
BUS ID A3 3B *****
30050300

*****
BUS ID A3 3C *****
2170300  30050300

*****
BUS ID D *****
2140000  2150000  2210100  2210200  3550000  3560000  3560010
2190100  2190200  2190300  2160100  7160100  7160200  7160210
3010000  9020000  16050000  16090000  21190000  21200100  21200200
21210000  21220000  21230100  21230200  32120100  32120200  32120300
40210000  40340100  40340200  40350100  50050200  50050100  50050200
50240100  50240200  50240300  50250100  50250200  50250300  50250400
50250500  50250600  50260100  50260200  50260300  51140000

*****
BUS ID D G *****
7120000  7130000

*****
BUS ID D1 *****
4150000

*****
BUS ID D1A *****
1080100  1080300  1090100  1090300  1090400  1120100  1120200
1130100  4060100  4120100  6030100  6050100  6070100  7110100
7110300  7150100  7150300  15010000  20020100  20030100  20030200
20030300  20040100  20040200  20040300  20060000  20070100  20070200
20080100  20080200  20100100  20110100  20110200  20120100  20120200
20130100  20130200  20160000  20170000  20180100  20200100  20210100
20220100  20220200  20230100  20240100  20250100  20270100  20270200
20270300  20280000  20290000  21010100  21010200  21010300  21010400
21020100  21030100  21050100  21050200  21050300  21050400  21060100
21070100  21090100  21100000  21130100  21140100  22010000  22020000
22040000  22080000  22090000  22120000  22140000  22150000  22180000
32020100  32020200  32020300  32030100  32030200  32030300  32050100
32050200  32050300  32070100  32070200  32070300  32080100  32080200
32080300  32090100  32090200  32090300  32100100  32100200  32100300
32110100  32110200  32110300  40030000  40030010  40030020  50010000
50020100  50030100  50040000  50060100  50070100  50090100  50100100
50100200  50100300  50100400  50120100  50150100  52010000  52020000

```

TABLE 7.1-4 LISTING OF LOAD ELEMENT BUS ASSIGNMENTS, AS PROCESSED FROM
(Continued) LEC CARD DATA (APPENDIX 7.2)

```

10/30/74 10109:31 10070R 000155074 000155 S29 50
***** BUS ID D1E *****
4000000 4090010 6040200 6040300

***** BUS ID D1F *****
1010100 1010110 1010300 1010310 1110100 3150000 4030100
4030200 4130000 6010100 6020100 6060100 6100100 7010100
7010200 7010300 7010400 7010500 7030100 7030300 72030000
22060000 22070000 22130000 22170000 22210000 30030100 30030200
40070100 40070200 40070300 40100100 40120100 40270100 40270200
40280100 40280200 40310100 40330100 52270000 52300000

***** BUS ID D1G *****
300A0100 50170000 501A0100 501A0200 50190000 50200100 50200200
50200300 50220100 50220200 50220300

***** BUS ID D1L *****
1030100 1040100 1040000 2110100 3010100 3030100 3040100
3050100 3060000 3120000 3120000 3170100 3180100 3190100
3210100 3220100 3220300 4000000 4050100 4050300 7040100
7040200 7090100 7090110 7100100 7100300 7100400 72190000
22200000 40040100 40141000 40180000 52260000

***** BUS ID D1M *****
6080100 6120100 30010100 30020100 30070100 30150100 30170100
31060000 31060010 31070000 31070010 31120100 31130100 31130200
31150100 31150400 51010000

***** BUS ID D1R *****
1140100 1160100 1170100 1170200 1180100 1190100 2010100
2040100 2050100 2060100 2070000 2100100 2120000 2200100
2200110 2200200 2200210 2200300 2200310 2200100 2200200
2200300 2200400 2330100 2330100 2350000 2420100 2420200
2420300 2470100 2500000 2510000 3350100 3350200 3350300
3350400 3350500 3360000 3390000 3410000 3450100 3450200
3510000 3540000 4070000 22220000 22230000 30040100 31020000
31030100 31040100 31040200 31040300 31040400 31050100 31050200
31050300 31050400 40200100 40200200 40200300 40200400 40300100

***** BUS ID D16 *****
4110000

***** BUS ID D2 *****

```

TABLE 7.1-4 LISTING OF LOAD ELEMENT BUS ASSIGNMENTS, AS PROCESSED FROM
(Continued) LEC CARD DATA (APPENDIX 7.2)

10/3 7/3 10109131 100785 500150070 000155 829 50
0150000

***** BUS TO D2A *****

1080100	1080200	1090100	1090200	1120100	1130200	4060100
4060200	4060300	4120100	4120200	6030100	6030200	6050200
6070200	7110100	7110200	7150100	7150200	16010100	16020100
16060100	16060100	16060100	16070100	20020200	20030100	20030200
20030300	20040100	20040200	20040300	20060000	20070100	20070200
20100200	20100100	20110200	20120100	20120200	20130100	20130200
20150000	20180200	20190100	20200200	20210200	20220100	20230200
20240200	20250200	20270100	20270200	20270300	20280000	20280000
21020200	21030200	21060200	21070200	21090200	21130200	21140200
21150100	21150200	21150300	21150000	22010000	22020000	22040000
22020000	22040000	22100000	22150300	22160000	22180000	32020100
32020200	32020300	32030100	32030200	32030300	32050100	32050200
32050300	32070100	32070200	32070300	32180100	32080200	32080300
32090100	32090200	32090300	32100100	32100200	32100300	32110100
32110200	32110300	50020200	50100200	50170200	50090200	50100100
50100200	50100300	50100000	50120200	50150200		

***** BUS TO D2E *****

6040100	6040300					
---------	---------	--	--	--	--	--

***** BUS TO D2F *****

1010100	1010110	1010200	1010210	1110100	1110200	3150000
4040100	4040200	4130000	4130000	6010200	6020100	6020200
6060200	6100200	7010100	7010200	7010300	7010400	7010500
7030100	7030200	7030400	22030000	22060000	22070000	22170000
40120200	40270100	40270200	40280100	40280200	40310200	52270000

***** BUS TO D2G *****

30080200						
----------	--	--	--	--	--	--

***** BUS TO D2L *****

1030200	1030200	3010200	3030200	3040200	3050200	3140000
3170200	3190200	3190300	3210200	3210300	3220100	3220200
4050100	4050200	7040300	7090200	7090210	7100100	7100200
22190000	22200000	40040200	40111100	40111200	40130000	40190000

***** BUS TO D2M *****

6080200	6120200	30010200	3010200	30060100	30060200	30070200
30150200	30170200	31060000	31060010	31070000	31070010	31120200
31150200	31170100	31180100				

7.1-25
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TABLE 7.1-4 LISTING OF LOAD ELEMENT BUS ASSIGNMENTS, AS PROCESSED FROM
(Continued) LEC CARD DATA (APPENDIX 7.2)

10/30/74 14149131 100748 001185-78 000155 829 50

```

*****
BUS TO 025
*****
1140200 1160200 1170300 1180200 1190200 2010200 2020000
2030000 2040200 2050200 2060200 2070000 2080100 2100200
2110200 2120000 2130100 2130200 2160000 2200100 2200110
2200200 2200210 2200300 2200310 2280100 2280200 2280300
2280000 2280100 2300100 2330200 2340200 2340100 2400100
2470200 3350100 3350200 3350300 3350400 3350500 3360000
3350000 3350100 3450200 2220000 2223000 30040200 3102000
31030200 31040100 31040200 31040300 31040400 31050100 31050200
31050300 31050400 30200100 41200200 41200300 40200400 40300200

*****
BUS TO 03
*****
0150000

*****
BUS TO 034
*****
1000000 1000300 1020000 1090300 1090400 1120200 1130300
4050200 4060300 4120200 5060000 5080100 5080200 5130100
5130200 5150100 5150200 5030200 5050300 5070300 7000000
7110200 7110300 7150200 7150300 1501000 1601000 1602000
1602000 16050200 16060200 16070200 20020300 20030100 20030200
20030300 20040100 20040200 20040300 2005000 2006000 2009000
20100300 20100200 20100200 20100300 2021000 2022000 20240300
20250300 20270100 20270200 20270300 2028000 2028000 21020300
21030300 21030400 2104000 21070400 21130300 2201000 2202000
2205000 2208000 2209000 2211000 2216000 2218000 32020100
32020200 32020300 3203000 32030200 32030300 32050100 32050200
32050300 32070100 32070200 32070300 32070300 32080100 32080200 32080300
32090100 32090200 32090300 32100100 32100200 32100300 32110100
32110200 32110300 50020300 50020400 50030200 50030300 50060300
50070300 50090300 50100100 50100200 50100300 50100400 50120300

*****
BUS TO 03F
*****
6000000 1000010 6000100 20040200

*****
BUS TO 03F
*****
1010200 1010210 1010300 1010310 1110200 3150000 4030100
4030200 6100000 6010200 6020200 6040300 6100300 6160200
6180000 7010100 7010200 7010300 7010400 7010500 7030200
7030300 7030300 2203000 2203000 2207000 2210000 2217000
30030100 30030200 40100200 40330200 52270000

*****
BUS TO 03G
*****
30080300

```

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TABLE 7.1-4 LISTING OF LOAD ELEMENT BUS ASSIGNMENTS, AS PROCESSED FROM
(Continued) LEC CARD DATA (APPENDIX 7.2)

10/30/70 18109131 10070- 0015507 000155 529 50

***** BUS ID 03L *****

1030300	1040300	3010300	3130000	3180200	3190400	3210400
3220200	3220300	4050200	4050300	4110000	7040400	7100200
7100300	7100400	2210000	2220000	4011100	4011200	4014100
4013000	4019000					

***** BUS ID 03M *****

3080300	3120300	3000300	3010300	30150300	30170300	31120300
31130100	31130200	31150300	31170200	31170300	31180200	31180300

***** BUS ID 03P *****

3250000

***** BUS ID 03R *****

1140300	2080200	2160000	2200100	2200110	2200200	2200210
2200300	2200310	2250100	2250200	2250300	2280400	2300200
2310200	2350000	2300200	2410200	2420400	2480000	2490000
2520100	2520200	2530100	2530200	2540000	3350100	3350200
3350300	3350400	3350500	3360000	3380000	3390000	3410000
3420100	3420200	3420300	3420400	3420500	3420600	3430000
3450100	3450200	3460000	3500000	5030100	5030200	5040000
5050100	5050200	5050300	5050400	5070000	5090000	5120000
5150100	5180000	7050000	30040300	31020000	31030300	31030400
40200100	40200200	40200300	40200400			

***** BUS ID 03W *****

8010100	8010200	8020000	8030000	8040000	8040100	8050000
4060000						

0874

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APPENDIX 7.2

SEPAP DATA BASE (CARD IMAGE DATA AS FURNISHED BY LEC)

7.2.0

APPENDIX 7.2

SEPAP DATA BASE

Table 7.2-1 displays the images of card data supplied by LEC. The listed equipment items, reading across are bus identification, circuit protection device (if selected), EPDC or load element procurement specification number, and element identification number. The nomenclature will be defined in the following tables. The equipment list was obtained from the Electrical Equipment List dated July 23, 1974 with modifications based on the data in the latest Rockwell power profile analysis document dated June 26, 1974. The bus description nomenclature used the following format:

<u>Character</u>	<u>Description</u>
1st	<u>POWER TYPE</u> A = ac component D = dc component
2nd	<u>MAIN BUS IDENTIFIERS</u> 1 = Main dc bus A 2 = Main dc bus B 3 = Main dc bus C 4 = P/L Direct from F/C 3
3rd	<u>SUB-BUS ASSIGNMENT</u> F = Forward Local dc bus M = Midbody local dc bus A = Aft local dc bus E = Essential dc bus D = DFI dc bus L = LH D&C Panel R = RH D&C Panel O = OOS CB Panel P = P/L Specialist Panel S = Mission Specialist Station T = ALT Panel W = P/L Bus P = General (any other direct loads)

<u>Character</u>	<u>Description</u>
4th	<p><u>LOAD CLASSIFICATION</u></p> <p>1 = Direct to ground 2 = Return to ground 3 = Inverter or AC 4 = P/L</p>
5th	<p><u>AC PHASE DESCRIPTION</u></p> <p>A or B or C = 1 phase For 2Ø or 3Ø loads enter phase letters consecutively. (NOTE: This is different than Rockwell which requires entry of 2 or 3 BUS IDS).</p>

For instance, BUS ID DIF2 represents the following information: The item (IMU) is a DC load, on main (DC) BUS A, in particular on forward local (DC) bus, with a single point (return wire) ground. Similarly, A2F3B indicates a load element the GSE from bypass control requiring a power, on main BUS B, forward local bus, inverter output.

The EPDC or load element nomenclature convention used in the listing of Table 7.2-1 reading from left-to-right is:

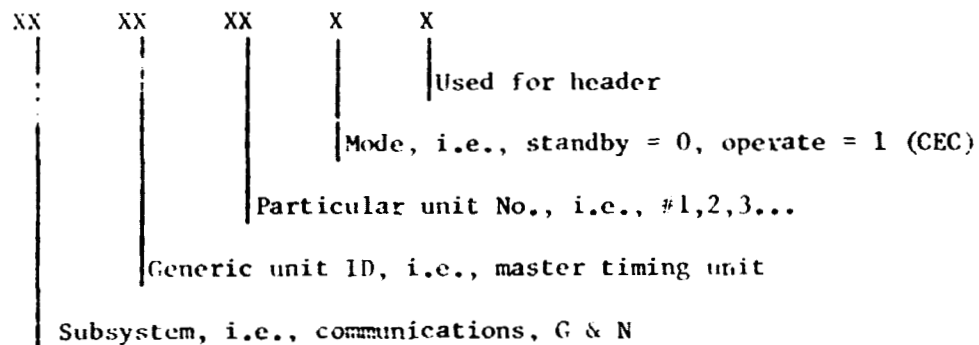


Table 7.2-2 is a reproduction of a SEPAP topology definition obtained from a LEC memorandum to JSC [1].

TABLE 7.2-2 SEPAP TOPOLOGY DEFINITION

SOURCE DEFINITION

(3-TOTAL)

SOURCE CODE NO.	CONNECTS* NODE	TO NODE	IDENTIFICATION
1	09	01	Fuel Cell 1
2	09	02	Fuel Cell 2
3	09	03	Fuel Cell 3

* NOTE: 09 is common ground.

TABLE 7.2-2 (Continued)

BUS/NO. OF MEMBER

(40 NODES)

BUS/NO. OF MEMBER	IDENTIFICATION
01	Fuel Cell 1
02	Fuel Cell 2
03	Fuel Cell 3
09	Ground
10	Main dc Bus A
11	Main dc Bus A Loads
12	Fwd Local dc Bus A
13	Midbody Local dc Bus A
14	Aft Local dc Bus A
15	RH D&C Panels Bus A
16	LH D&C Panels Bus A
17	Essential Bus 3 AB
19	Inverter Bus A
20	Main dc Bus B
21	Main dc Bus B Loads
22	Fwd Local dc Bus B
33	Midbody Local dc Bus B
24	Aft Local dc Bus B
25	RH D&C Panels Bus B
26	LH D&C Panels Bus B

TABLE 7.2-2 (Continued)

BUSES/NODES DEFINITION

(40 NODES)

BUS/NODE NUMBER	IDENTIFICATION
27	Essential Bus 1 BC
29	Inverter Bus B
30	Main dc Bus C
31	Main dc Bus C Loads
32	Fwd dc Bus C
33	Midbody Local dc Bus C
34	Aft Local dc Bus C
35	RH D&C Panels Bus C
36	LH D&C Panels Bus C
37	Essential Bus 2 CA
39	Inverter Bus C
41	Fwd Sub-Bus AB
42	Fwd Sub-Bus BC
43	Fwd Sub-Bus CA
51	Aft Sub-Bus AB
52	Aft Sub-Bus BC
53	Aft Sub-Bus CA
60	Main Bus Tie - A, B, C
61	Fwd Sub-Bus ABC
62	Aft Sub-Bus ABC

TABLE 7.2-2 (Continued)

LOAD DEFINITION
(54 LOADS)

SEPAP LOAD NO.	R/SD NO.	IDENTIFICATION
111	D1O2	Main A On-Orbit c/b Panel
112	D1G2	Main A dc Loads (Bus Return)
113	D1G1	Main A dc Loads (Local Ground)
114	D1S2	Main A Mission Specialist c/b Panel
115	D1P2	Main A Payload Specialist c/b Panel
116	D1T2	Main A ALT c/b Panel
121	D1F2	Fwd Local A dc Loads (Bus Return)
122	D1F1	Fwd Local A dc Loads (Local Ground)
123	D1F3	Fwd Local A Inverter Loads
131	D1M1	Midbody Local A dc Loads (Local Ground)
141	D1A1	Aft Local A dc Local (Local Ground)
142	D1A4	Aft Local A Payload
151	D1R2	RHD&C Panel Bus A Loads
161	D1L2	LHD&C Panel Bus A Loads
171	D3E1,D1E1,D2E1	Essential Bus 3 AB Loads
211	D2O2	Main B On-Orbit c/b Panel
212	D2G2	Main B dc Loads (Bus Return)
213	D2G1	Main B dc Loads (Local Ground)
214	D2S2	Main B Mission Specialist c/b Panel
215	D2P2	Main B Payload Specialist c/b Panel
216	D2T2	Main B ALT c/b Panel

TABLE 7.2-2 (Continued)

LOAD DEFINITION

(54 LOADS)

SEPAP LOAD NO.	R/SD NO.	IDENTIFICATION
221	D2F2	Fwd Local B dc Loads (Bus Returns)
222	D2F1	Fwd Local B dc Loads (Local Ground)
223	D2F3	Fwd Local B Inverter Loads
231	D2M1	Midbody Local B dc Loads (Local Ground)
241	D2A1	Aft Local B dc Loads (Local Ground)
242	D2A4	Aft Local B Payload
251	D2R2	RH D&C Panel Bus B Loads
261	D2L2, D	LH D&C Panel Bus B Loads
271	D1E1, I2E1, D3E1	Essential Bus 1 BC Loads
302	D4W4	Main C Payload
311	D302	Main C On-Orbit c/b Panel
312	D3G2	Main C dc Loads (Bus Return)
313	D3G1	Main C dc Loads (Local Ground)
314	D3S2	Main C Mission Specialist c/b Panel
315	D3P2	Main C Payload Specialist c/b Panel
316	D3T2	Main C ALT c/b Panel
321	D3F2	Fwd Local C dc Loads (Bus Return)
322	D3F1	Fwd Local C dc Loads (Local Ground)
323	D3F3	Fwd Local C Inverter Loads
325	D3D2	Fwd Local C DFI
331	D3M1	Midbody Local C dc Loads (Local Ground)

TABLE 7.2-2 (Continued)

LOAD DEFINITION

(54 LOADS)

SEPAP LOAD NO.	R/SD NO.	IDENTIFICATION
341	D3A1	Aft Local C dc Loads (Local Ground)
351	D3R2	RH D&C Panel Bus C Loads
361	D3L2	LH D&C Panel Bus C Loads
371	D2E1,D3E1,D1E1	Essential Bus 2 CA Loads
412	D1F2,D2F2	Fwd Sub-Bus AB Loads
423	D2F2,D3F2	Fwd Sub-Bus BC Loads
431	D3F2,D1F2	Fwd Sub-Bus CA Loads
512	D1A2,D2A2	Aft Sub-Bus AB Loads
523	D2A2,D3A2	Aft Sub-Bus BC Loads
531	D3A2,D1A2	Aft Sub-Bus CA Loads
601	D1F2,D2F2,D3F2	Fwd Sub-Bus ABC Loads
602	D1A2,D2A2,D3A2	Aft Sub-Bus ABC Loads

TABLE 7.2-2 (Continued)

RESISTOR/SWITCH/DIODE

DEFINITION

(115-TOTAL)

RESISTOR AND SWITCH NO.	CONNECTS NODE	TO NODE	THRU LOAD NO.	THRU DIODE NO.	RESISTOR VALUE (OHMS)	SWITCH POSITION
101	01	10	-	-	.00371	C
110	10	11	-	-	.00001	C
111	11	09	111	-	.02320	C
112	11	09	112	-	.02168	C
113	11	09	113	-	.04339	C
114	11	09	114	-	.02320	C
115	11	09	115	-	.00893	C
116	11	09	116	-	.00234	OP
120	10	12	-	-	.00419	C
121	12	09	121	-	.00243	C
122	12	09	122	-	.00487	C
123	19	09	123	-	.00908	C
124	12	19	-	-	.00001	C
130	10	13	-	-	.00605	C
131	13	09	131	-	.04339	C
140	10	14	-	-	.00946	C
141	14	09	141	-	.04339	C
142	14	09	142	-	.00447	OP
150	10	15	-	-	.00826	C
151	15	09	151	-	.00604	C
160	10	16	-	-	.00826	C

*Nodal connections as listed reflect diode current flow.

TABLE 7.2-2 (Continued)

RESISTOR/SWITCH/DIODE

DEFINITION

(115-TOTAL)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

RESISTOR AND SWITCH NO.	CONNECTS NODE	TO NODE	THRU LOAD NO.	THRU DIODE NO.	RESISTOR VALUE (OHMS)	SWITCH POSITION
161	16	09	161	-	.00845	C
170	10	17	-	170	.00001	C
171	17	09	171	-	.00447	C
172	17	15	-	-	.00001	OP
173	17	16	-	-	.00001	OP
174	20	17	-	174	.00001	C
175	03	17	-	175	.00001	C
180	10	60	-	-	.00001	OP
201	02	20	-	-	.00371	C
210	20	21	-	-	.00001	C
211	21	09	211	-	.02320	C
212	21	09	212	-	.02168	C
213	21	09	213	-	.00523	C
214	21	09	214	-	.01774	C
215	21	09	215	-	.01785	C
216	21	09	216	-	.00199	OP
217	21	09	217	-	.00199	OP
220	20	20	-	-	.00119	C
221	22	09	221	-	.00119	C
222	22	09	222	-	.00199	C
223	29	09	223	-	.00644	C

* Nodal connections as listed reflect diode current flow

TABLE 7.2-2 (Continued)

RESISTOR/SWITCH/DIODEDEFINITION

(115-TOTAL)

RESISTOR AND SWITCH NO.	CONNECTS NODE	TO NODE	THRU LOAD NO.	THRU DIODE NO.	RESISTOR VALUE (OHMS)	SWITCH POSITION
224	22	29	-	-	.00001	C
230	20	23	-	-	.00605	C
231	23	09	231	-	.04339	C
240	20	24	-	-	.00946	C
241	24	09	241	-	.00572	C
242	24	09	242	-	.00447	OP
250	20	25	-	-	.00826	C
251	25	09	251	-	.01256	C
260	20	26	-	-	.00826	C
261	26	09	261	-	.01123	C
270	20	27	-	270	.00001	C
271	27	09	271	-	.00447	C
272	27	25	-	-	.00001	OP
273	27	26	-	-	.00001	OP
274	30	27	-	274	.00001	C
275	01	27	-	275	.00001	C
280	20	60	-	-	.00001	OP
301	03	30	-	-	.00371	C
302	03	09	302	-	.00447	OP
310	30	31	-	-	.00001	C
311	31	09	311	-	.02320	C
312	31	09	312	-	.00574	C

* Nodal connections as listed reflect diode current flow.

TABLE 7.2-2 (Continued)

RESISTOR/SWITCH/DIODE

DEFINITION

(115-TOTAL)

RESISTOR AND SWITCH NO.	CONNECTS NODE	TO NODE	THRU LOAD NO.	THRU* DIODE NO.	RESISTOR VALUE (OHMS)	SWITCH POSITION
513	31	09	513	-	.24125	C
514	31	09	514	-	.01371	C
315	31	09	315	-	.01635	C
316	31	09	316	-	.00639	OP
320	30	32	-	-	.00419	C
321	32	09	321	-	.00243	C
322	32	09	322	-	.00734	C
323	39	09	323	-	.00756	C
324	32	39	-	-	.00001	C
325	32	09	325	-	.06361	OP
330	30	33	-	-	.00605	C
331	33	09	331	-	.04339	C
340	30	34	-	-	.00946	C
341	34	09	341	-	.00846	C
350	30	35	-	-	.00826	C
351	35	09	351	-	.02204	C
360	30	36	-	-	.00826	C
361	36	09	361	-	.01074	C
370	30	37	-	370	.00001	C
371	37	09	371	-	.00447	C
372	37	35	-	-	.00001	OP
373	37	36	-	-	.00001	OP

* Nodal connections as listed reflect diode current flow.

TABLE 7.2-2 (Continued)

RESISTOR/SWITCH/DIODE

DEFINITION

(115-TOTAL)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

RESISTOR AND SWITCH NO.	CONNECTS NODE	TO NODE	THRU LOAD NO.	THRU* DIODE NO.	RESISTOR VALUE (OHMS)	SWITCH POSITION
374	10	37	-	374	.00001	C
375	02	37	-	375	.00001	C
380	30	60	-	-	.00001	OP
401	12	41	-	401	.00001	C
402	12	61	-	402	.00001	C
403	12	43	-	403	.00001	C
404	22	42	-	404	.00001	C
405	22	61	-	405	.00001	C
406	22	41	-	406	.00001	C
407	32	43	-	407	.00001	C
408	32	61	-	408	.00001	C
409	32	42	-	409	.00001	C
412	41	09	412	-	.00447	C
423	42	09	423	-	.00447	C
431	43	09	431	-	.00447	C
501	14	51	-	501	.00001	C
502	14	62	-	502	.00001	C
503	14	53	-	503	.00001	C
504	24	52	-	504	.00001	C
505	24	62	-	505	.00001	C
506	24	51	-	506	.00001	C
507	34	53	-	507	.00001	C

* Nodal connections as listed reflect diode current flow.

TABLE 7.2-2 (Continued)

RESISTOR/SWITCH/DIODE

DEFINITION

(115-TOTAL)

RESISTOR AND SWITCH NO.	CONNECTS NODE	TO NODE	THRU LOAD NO.	THRU* DIODE NO.	RESISTOR VALUE (OHMS)	SWITCH POSITION
508	34	62	-	508	.00001	C
509	34	52	-	509	.00001	C
512	51	09	512	-	.00447	C
523	52	09	523	-	.00447	C
531	53	09	531	-	.00447	C
601	61	09	601	-	.00447	C
602	62	09	602	-	.00447	C

* Nodal connections as listed reflect diode current flow.

APPENDIX 7.3

LISTING OF EPDC AND USER LOAD ELEMENTS BY SUBSYSTEM
(FROM ROCKWELL PROFILE ANALYSIS DOCUMENT, DATED
13 AUGUST 1974 AND LEC MEMORANDA)

TABLE 7.3-1

EPDC USER SUBSYSTEM CODE NUMBER LISTING

01	GUIDANCE NAVIGATION & CONTROL
02	COMMUNICATIONS
03	DISPLAYS & CONTROLS
04	OPERATIONAL FLIGHT INSTRUMENTATION
05	DEVELOPMENT FLIGHT INSTRUMENTATION
06	ELECTRICAL POWER DISTRIBUTION & CONTROL
07	DATA PROCESSING
08	PAYLOAD MANAGEMENT
09	UNMANNED KIT
15	EXTERNAL TANK
16	SOLID ROCKET BOOSTER
20	MAIN PROPULSION
21	ORBIT MANEUVERING SYSTEM
22	REACTION CONTROL SYSTEM
30	POWER GENERATION SYSTEM
31	CRYOGENICS SYSTEM
32	AUXILLARY POWER UNIT
40	ENVIRONMENTAL CONTROL & LIFE SUPPORT
50	HYDRAULICS
51	DOCKING & CARGO HANDLING
52	MECHANICAL SYSTEM & LANDING

TABLE 7.3-2. SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: GUIDANCE AND NAVIGATION CODE 01

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
IMU =1 OPERATE	160.00	010101010100
IMU =1 STANDBY	55.00	010101010110
IMU =2 OPERATE	160.00	010101010200
IMU =2 STANDBY	55.00	010101010210
IMU =3 OPERATE	160.00	010101010300
IMU =3 STANDBY	55.00	010101010310
STAR TRKER + LT SHLD =1	20.00	010301030100
STAR TRKER + LT SHLD =2	20.00	010301030200
STAR TRKER + LT SHLD =3	20.00	010301030300
AIR DATA XDCR ASSY =1	45.00	010401040100
AIR DATA XDCR ASSY =2	45.00	010401040200
AIR DATA XDCR ASSY =3	45.00	010401040300
AIR DATA XDCR ASSY =4	45.00	010401040400
FLIGHT CONTROLS		01070001
ASCENT TVC DRVR =1 - AFT	94.50	010801080100
ASCENT TVC DRVR =2 - AFT	94.50	010801080200
ASCENT TVC DRVR =3 - AFT	94.50	010801080300
AERC SRF SRV AMP =1-AFT	107.77	010901090100
AERC SRF SRV AMP =2-AFT	107.77	010901090200
AERC SRF SRV AMP =3-AFT	107.77	010901090300
AERC SRF SRV MP =4-AFT	107.77	010901090400
REACTION JET DRVR =1 FWD	59.20	011101110100
REACTION JET DRVR =2 FWD	59.20	011101110200
REACT JET CMS DRVR=1-AFT	152.70	011201120100
REACT JET CMS DRVR=2-AFT	152.70	011201120200
RATE GYRO ASSY-AFT =1	23.00	011301130100
RATE GYRO ASSY-AFT =2	23.00	011301130200
RATE GYRO ASSY-AFT =3	23.00	011301130300
ACCELEROMETER ASSY-FWD=1	2.90	011401140100
ACCELEROMETER ASSY-FWD=2	2.90	011401140200
ACCELEROMETER ASSY-FWD=3	2.90	011401140300
TRANS HAND CONTROL =1	4.00	011601160100
TRANS HAND CONTROL =2	4.00	011601160200
ROT HAND CONTROL =1	10.60	011701170100
ROT HAND CONTROL =2	10.60	011701170200
ROT HAND CONTROL =3	10.60	011701170300
RUDDER PEDAL XDCR ASY =1	3.30	011801180100
RUDDER PEDAL XDCR ASY =2	3.30	011801180200
SPEED BRK THRUST CNTL =1	6.00	011901190100
SPEED BRK THRUST CNTL =2	6.00	011901190200

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: COMMUNICATIONS

CODE 02

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
B + W TV MONITOR =1	20.00	020102010100
B + W TV MONITOR =2	20.00	020102010200
TV REMOTE CONTROL	5.00	020202020000
TV CAMERA COLOR + MON	20.00	020302030000
TV CAMERA B+W =1+2	12.50	020402040100
TV CAMERA B+W =3+4	12.50	020402040200
PAN TILT ELECT =1	10.00	020502050100
PAN TILT ELECT =2	10.00	020502050200
PAN TILT MOUNT =1	3.00	020602060100
PAN TILT MOUNT =2	3.00	020602060200
VIDEO SWITCHING NETWORK	5.00	020702070000
NETWORK SIG PROCESSOR =1	24.00	020702080100
NETWORK SIG PROCESSOR =2	24.00	020702080200
CTRL CNTL UNIT AUDIO =1	34.00	021002100100
CTRL CNTL UNIT AUDIO =2	34.00	021002100200
S-BAND FM XMITR =1	100.00	021102110100
S-BAND FM XMITR =2	100.00	021102110200
S-BAND FM SIGNAL PRCC	10.00	021202120000
S-BAND TRANSPONDER =1	15.00	021302130100
S-BAND TRANSPONDRR =2	15.00	021302130200
S-BAND PWR AMP ASSY	400.00	02140000
S-BAND PRE AMP ASSY	25.0	02150000
S-BAND ANT SW ASSY	0.60	021402160000
TACAN =1	150.00	021502170100
TACAN =2	150.00	021502170200
TACAN =3	150.00	021502170300
S-BAND SWITCH COAXIAL	0.60	021802180000

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: COMMUNICATIONS (CONTINUED)

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
MSBLS RF ASSY =1	22.00	022002200100
MSBLS DCDR ASSY =1	78.00	022002200110
MSBLS RF ASSY =2	22.00	022002200200
MSBLS DCDR ASSY =2	78.00	022002200210
MSBLS RF ASSY =3	22.00	022002200300
MSBLS DCDR ASSY =3	78.00	022002200310
RADAR ALTIMETER =1	37.50	022102210100
RADAR ALTIMETER =2	37.50	022102210200
COMSEC UNIT AF =1	35.00	022802280100
COMSEC UNIT AF =2	35.00	022802280200
COMSEC UNIT AF =3	35.00	022802280300
COMSEC UNIT AF =4	35.00	022802280400
P/L INTERG- AF+NASA =1	30.00	023002300100
P/L INTERG- AF+NASA =2	30.00	023002300200
PAYLOAD SIG PROCESSOR =1	17.00	021602310100
PAYLOAD SIG PROCESSOR =2	17.00	021602310200
UHF RCVR =1 MAIN/GUARD	30.00	020902330100
UHF RCVR =2 MAIN/GUARD	30.00	020902330200
UHF TRANSMITTER =1	90.00	020902340100
UHF TRANSMITTER =2	90.00	020902340200
UHF RF NETWORK CPLNG	15.00	023502350000
DOPPLER EXTRACTOR =1	15.00	023902390100
DOPPLER EXTRACTOR =2	15.00	023902390200
EVA SIG PROCESSOR =1	10.00	024002400100
EVA SIG PROCESSOR =2	10.00	024002400200
AUDIO TERM UNIT - FWD	5.00	02410001
AUDIO TERM UNIT - MSS	5.00	02420100
AUDIO TERM UNIT - PSS	5.00	02420200
AUDIO TERM UNIT - REAR	5.00	02420300
SPEAKER MIKE ASSY -RIGHT	4.00	02420400
SPEAKER MIKE ASSY -LEFT	4.00	02470100
S-BAND FM XMTR OFI	100.00	02470200
S-BAND MULTX OFI	0.00	02480000
RNDZ RADAR ELEC ASSY -DC	160.00	02490000
RNDZ RADAR ELEC ASSY -AC	20.00	02500000
RNDZ RADAR ELEC ASSY -DC	50.00	02501000
RNDZ RADAR DPLY ASSY -AC	395.00	02510000
KU-BAND EL ASSY - DC =1	100.00	02511000
KU-BAND EL ASSY - DC =2	100.00	02520100
KU-BAND FL ASSY - AC =1	20.00	02520200
KU-BAND EL ASSY - AC =2	20.00	02521100
KU-BAND COMM LPY ASSY =1	85.00	02521200
KU-BAND COMM LPY ASSY =2	85.00	02530100
KU-BAND COMM LPY ASSY =1	235.00	02530200
KU-BAND COMM LPY ASSY =2	235.00	02531100
KU-HND SIG PROCESSOR	15.00	02531200
		02540000

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: DISPLAYS AND CONTROLS

CODE 03

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
ATTITUDE DIR IND-FWD =1	14.60	03C103010100
ATTITUDE DIR IND-FWD =2	14.60	03C103010200
ATTITUDE DIR IND-AFT =3	14.60	03010300
HCRZ SIT IND=1	35.00	030303030100
HCRZ SIT IND=2	35.00	030303030200
AS/MACH IND AMI =1	40.00	030403040100
AS/MACH IND AMI =2	40.00	030403040200
ALT VER VEL IND =1	40.00	030503050100
ALT VER VEL IND =2	40.00	030503050200
TAPE METERS HYC-APU-MPS	132.00	03060000
CROSS POINTER IND	.00	03120000
SURF POSITION IND	5.00	031303130000
QTY IND CMS/RCS	6.00	03140000
CAUT + WARNING UNIT	20.00	031503150000
MISSION TIMER =1	4.00	031703170100
MISSION TIMER =2	4.00	031703170200
EVENT TIMER =1	4.00	031803180100
EVENT TIMER =2	4.00	031803180200
CRT DISPLAY UNIT =1	90.00	031903190100
CRT DISPLAY UNIT =2	90.00	031903190200
CRT DISPLAY UNIT =3	90.00	031903190300
CRT DISPLAY UNIT =4	90.00	031903190400
DISPLAY ELECT UNIT =1	207.30	03210100
DISPLAY ELECT UNIT =2	207.30	03210200
DISPLAY ELECT UNIT =3	207.30	03210300
DISPLAY ELECT UNIT =4	207.30	03210400
DISP DRV UNIT-CRW FWD=1	120.00	03220100
DISP DRV UNIT-CRW FWD=2	120.00	03220200
DISP DRV UNIT-CRW AFT=3	120.00	03220300
MANIP HAND CONTROLLER	8.00	032503250000

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING
 SUBSYSTEM: DISPLAY AND CONTROL LIGHTING CODE 03

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
INTEGRAL LIGHTS-LEFT/CTR	134.00	033103310100
INTEGRAL LIGHTS-OVHD	134.00	033103310200
INTEGRAL LIGHTS-RIGHT	134.00	033103310300
INTEGRAL LIGHTS-REAR	134.00	033103310400
ANNUNCIATOR LTS-LEFT/CTR	23.30	033303330100
ANNUNCIATOR LTS-OVHD	23.30	033303330200
ANNUNCIATOR LTS-RIGHT	23.30	033303330300
MID DECK FLOOD LTS - 1	19.40	033503350100
MID DECK FLOOD LTS - 2/3	19.40	033503350200
MID DECK FLOOD LTS - 4/6	19.40	033503350300
MID DECK FLOOD LTS - 5	19.40	033503350400
MID DECK FLOOD LTS-PANEL	19.40	033503350500
LWR DECK SLEEP STA LTS	18.50	033603360000
LWR DECK WASTE MGMT LTS	18.50	033803380000
LWR DECK GALLEY LIGHT	15.00	033903390000
AIRLOCK LIGHTS	103.50	034103410000
CABIN FLOOD LIGHTS AFT	29.80	034203420100
GLARESHIELD FLDLTS -LEFT	29.80	034203420200
GLARESHIELD FLDLTS-RIGHT	29.80	034203420300
CENTER CONSOLE FLOODLTS	29.80	034203420400
PILOT CONSOLE FLDLTS-RHT	29.80	034203420500
PILOT CONSOLE FLDLTS-LFT	29.80	034203420600
REAR STA P/L LTS	60.00	034303430000
EMERGENCY LIGHT - 1	29.80	034503450100
EMERGENCY LIGHT - 2	29.80	034503450200
PAYLOAD BAY FLOOD LTS	200.00	034903490000
MANIP SPOT LIGHT	100.00	035003500000
RNDZ LIGHT	30.00	035103510000
DECKING SPOT LIGHTS	150.00	03540000
C+W STATUS BOARD	36.00	03550000
C+W ANNUNCIATOR ASSY	24.00	03560000
C+W ANNUN ASSY - QUIESCT	2.00	03560010

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING CODE 04

SUBSYSTEM: OPERATIONAL FLIGHT INSTRUMENTATION

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
PCM MASTER UNIT DACRU =1	60.00	04030403010J
PCM MASTER UNIT DACBU =2	60.00	C40304030200
MAINT RECCRDER	40.00	04040404000J
SIG CCND UNIT-FWD =1	35.00	04050405010J
SIG CCND UNIT-FWD =2	35.00	04050405020J
SIG CCND UNIT-FWD =3	35.00	C40504050300
SIG CCND UNIT =1 - AFT	35.00	C40604060100
SIG CCND UNIT =2 - AFT	35.00	C40604060200
SIG CCND UNIT =3 - AFT	35.00	04060406030J
LCOP RECORDER	40.00	040704070000
MASTER TIMING UNIT-WPUP	40.00	040904090000
MASTER TIMING UNIT-OPR	26.00	040904090010
PAYLOAD DATA INTERLEAVER	30.00	041104110000
SIG CCND UNIT-CMS/RCS =1	35.00	0412010J
SIG CCND UNIT-CMS/RCS =2	35.00	0412020J
SIG CCND UNIT-F/C AREA	35.00	04130000 ←
SIG CCND UNIT-FWD RCS	35.00	04140000
	C.30	04150000

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: DEVELOPMENT FLIGHT INSTRUMENTATION

CODE 05

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
PCM MASTER UNIT - =1	60.00	040305030100
PCM MASTER UNIT - =2	60.00	040305030200
PCM RECORDER	40.00	040405040000
SIG COND UNIT - FWD =1	35.00	040505050100
SIG COND UNIT - FWD =2	35.00	040505050200
SIG COND UNIT - FWD =3	35.00	040505050300
SIG COND UNIT - FWD =4	35.00	040505050400
SIG COND UNIT -MID =1-12	35.00	040505060000
WIDEBAND FCM UNIT-FWD	50.00	050705070000
WIDEBAND FCM UNIT-MIC =1	50.00	050705080100
WIDEBAND FCM UNIT-MIC =2	50.00	050705080200
WIDEBAND RECORDER	40.00	050905090000
WIDEBAND SIG COND UNIT FWD	0.60	051205120000
WIDEBAND SIG COND UNIT MID	0.60	051305130100
WIDEBAND SIG COND UNIT MID	0.60	051305130200
STRAIN GAGE SIG COND FWD	5.60	051505150000
STRAIN GAGE SIG COND MID	5.60	051605160100
STRAIN GAGE SIG COND MID	5.60	051605160200
CURRENT SENSOR	0.30	051805180000

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: ELECTRICAL POWER DISTRIBUTION & CONTROL CODE 06

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
INVERTERS 1PH,750VA,80C	0.00	060106010100
INVERTERS 1PH,750VA,80C	0.00	060106010200
INVERTERS 1PH,750VA,80C	0.00	060106010300
PYRC EVENT CNTLR -FWD =1	25.00	060206020100
PYRC EVENT CNTLR -FWD =2	25.00	060206020200
MASTER EVENT CNTLR-AFT=1	25.00	060306030100
MASTER EVENT CNTLR-AFT=2	25.00	060306030200
LCAC CNTLR ASSY-FWD =1	75.00	060406040100
LCAC CNTLR ASSY-FWD =2	75.00	060406040200
LCAC CNTLR ASSY-FWD =3	75.00	060406040300
LCAC CNTLR ASSY-AFT =1	90.00	060506050100
LCAC CNTLR ASSY-AFT =2	90.00	060506050200
LCAC CNTLR ASSY-AFT =3	90.00	060506050300
DC PWR CNTLR ASSY-FWD =1	260.00	060606060100
DC PWR CNTLR ASSY-FWD =2	260.00	060606060200
DC PWR CNTLR ASSY-FWD =3	260.00	060606060300
DC PWR CNTLR ASSY-AFT =1	160.00	060706070100
DC PWR CNTLR ASSY-AFT =2	160.00	060706070200
DC PWR CNTLR ASSY-AFT =3	160.00	060706070300
MAIN DC DIST+CNTRL ASSY=1	20.00	060806080100
MAIN DC DIST+CNTRL ASSY=2	20.00	060806080200
MAIN DC DIST+CNTRL ASSY=3	20.00	060806080300
INV DIST + CNTRL ASSY =1	20.00	061006100100
INV DIST + CNTRL ASSY =2	20.00	061006100200
INV DIST + CNTRL ASSY =3	20.00	061006100300
ELEC PWR DST/CNTRL CONT		06110001
DC PWR CNTRL ASSY-MID =1	30.00	061206120100
DC PWR CNTRL ASSY-MID =2	30.00	061206120200
DC PWR CNTRL ASSY-MID =3	30.00	061206120300
EVLSS BAT CHARGER	5.00	061606160000
EVLSS PWR SUPPLY	75.00	061806180000
PROXIMITY SWITCH =1	8.00	061906190100
PROXIMITY SWITCH =2	8.00	061906190200
PROXIMITY SWITCH =3	8.00	061906190300



TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: DATA PROCESSING

CODE 07

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
COMPUTER =1	600.00	070107010100
COMPUTER =2	600.00	070107010200
COMPUTER =3	600.00	070107010300
COMPUTER =4	600.00	070107010400
COMPUTER =5	600.00	070107010500
MDM FF1	40.00	070307030100
MDM FF2	40.00	070307030200
MDM FF3	40.00	070307030300
MDM FF4	40.00	070307030400
MDM FA1	40.00	070307040100
MDM FA2	40.00	070307040200
MDM FA3	40.00	070307040300
MDM FA4	40.00	070307040400
MDM OFI - FWD	40.00	07050000
MDM OFI - MID	40.00	07060000
MASS MEM=1 TAPE OPER	53.00	070907090100
MASS MEM=1 TAPE STBY	8.00	070907090110
MASS MEM=2 TAPE OPER	53.00	070907090200
MASS MEM=2 TAPE STBY	8.00	070907090210
MDM OFI 1	40.00	07100100
MDM OFI 2	40.00	07100200
MDM OFI 3	40.00	07100300
MDM OFI 4	40.00	07100400
MDM OFI AFT 1	40.00	07110100
MDM OFI AFT 2	40.00	07110200
MDM OFI AFT 3	40.00	07110300
MDM LF-1	40.00	071207120000
MDM LA-1	40.00	071307130000
DATA PROCESSING CON T		07140001
ENG INTERFACE UNIT =1	50.60	071507150100
ENG INTERFACE UNIT =2	50.60	071507150200
ENG INTERFACE UNIT =3	50.60	071507150300
DATA BUS ISC AMP =1 GSE	20.00	071607160100
DATA BUS ISC AMP =1 CRB	10.00	071607160110
DATA BUS ISC AMP =2 GSE	20.00	071607160200
DATA BUS ISC AMP =2 CRB	10.00	071607160210

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: PAYLOAD MANAGEMENT

CODE 08

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
MM PAYLOAD FWD =1	40.00	C80108010100
MM PAYLOAD FWD =2	40.00	C80108010200
WIDE BAND RECORDER MSS	175.00	08020000
PCM RECORDER MSS	40.00	08030000
P/L - ASCENT/ENTRY	961.50	08040000
P/L - SORTIE	5769.20	08040100
AUX C+W UNIT	10.00	08050000
AUX C+W ANNUN ASSY	15.00	08060000
UNMANNED KIT		09000001
SUBSYS SEQ CONTR UNIT=1	370.00	0901000J
SUBSYS SEQ CONTR UNIT=2	190.00	09020000
EXTERNAL TANK		15000001
MLM - DEI	20.00	150115010000

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: SOLID ROCKET BOOSTER

CODE 16

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
RATE CYRO ASSY	42.00	150116010100
RATE CYRO ASSY	42.00	150116010200
MLM - SET 1	15.00	150116020100
MLM - SET 2	15.00	150116020200
MDM DFI =1	35.00	16040100
MDM DFI =2	35.00	16040200
PIC IGNITION - SET 1	0.00	150316050100
PIC IGNITION - SET 2	0.00	150316050200
PIC SEPARATION-SET 1	0.00	150316060100
PIC SEPARATION-SET 2	0.00	150316060200
SIG COND - SET 1	20.00	150116070100
SIG COND - SET 2	20.00	150116070200
TVC HYDR RECIRC SYS	706.00	16080000
SAFE + ARM DEVICE	75.00	16090000

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: MAIN PROPULSION SYSTEM

CODE 20

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
MAIN ENG CONTROLLER-1	750.00	200120010100
MAIN ENG CONTROLLER-2	750.00	200120010200
MAIN ENG CONTROLLER-3	750.00	200120010300
MAIN ENG HTR =1	300.00	200220020100
MAIN ENG HTR =2	300.00	200220020200
MAIN ENG HTR =3	300.00	200220020300
LC2 PREVALVE SOLENOID	42.00	200320030100
LC2 PREVALVE SOLENOID	42.00	200320030200
LC2 PREVALVE SOLENOID	42.00	200320030300
LH2 PREVALVE SOLENOID	42.00	200420040100
LH2 PREVALVE SOLENOID	42.00	200420040200
LH2 PREVALVE SOLENOID	42.00	200420040300
LC2 F+D VLV =1 C/B SOL	42.00	20050000
LC2 F+D VLV =2 C/B SOL	42.00	20060000
LH2 F+D VLV =1 C/B SOL	42.00	20070100
LH2 F+D VLV =1 C/B SOL	42.00	20070200
LH2 F+D VLV =2 C/B SOL	42.00	20080100
LH2 F+D VLV =2 C/B SOL	42.00	20080200
LH2 TOPPING VLV OPEN SOL	42.00	20090000
LH2 RECIRC VLV OPEN SOL=1	42.00	20100100
LH2 RECIRC VLV OPEN SOL=2	42.00	20100200
LH2 RECIRC VLV OPEN SOL=3	42.00	20100300
ET/CRP LC2 FEED DISC S V	42.00	20110100
ET/CRP LC2 FEED DISC S V	42.00	20110200
ET/CRP LH2 FEED DISC S V	42.00	20120100
ET/CRP LH2 FEED DISC S V	42.00	20120200
ET/CRP RECIRC DISC S V	42.00	20130100
ET/CRP RECIRC DISC S V	42.00	20130200
LC2 FEEDLN RELF SHUTOFF	42.00	20140000
LH2 FEEDLN RELF SHUTOFF	42.00	20150000
MAIN PROP SYS-CONTINUED		20150901
LH2 PRESS N DISC BYPASS	42.00	20160000
ET VENT VLV ISC SOL VLV	42.00	20170000
LC2 FEEDLN REPRESS VLV=1	42.00	20180100
LC2 FEEDLN REPRESS VLV=2	42.00	20180200

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: MAIN PROPULSION SYSTEM (CONTINUED)

CODE 20

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
LH2 FEEDLN REPRESS VLV=1	42.00	20190100
LH2 FEEDLN REPRESS VLV=2	42.00	20190200
HE CROSSOVER VLV =1	42.00	20200100
HE CROSSOVER VLV =2	42.00	20200200
HE CROSSOVER VLV =3	42.00	20200300
ENG HE SUPPLY ISO SCL =1	42.00	20210100
ENG HE SUPPLY ISO SCL =2	42.00	20210200
ENG HE SUPPLY ISO SCL =3	42.00	20210300
VEH HE SUPPLY ISO SCL=1	42.00	20220100
VEH HE SUPPLY ISO SCL=2	42.00	20220200
HE BLCWDN SCL VLV =1	42.00	20230100
HE BLCWDN SCL VLV =2	42.00	20230200
LO2 PRESS N FL CNTL SV1	42.00	20240100
LO2 PRESS N FL CNTL SV2	42.00	20240200
LO2 PRESS N FL CNTL SV3	42.00	20240300
LH2 PRESS N FL CNTL SV1	42.00	20250100
LH2 PRESS N FL CNTL SV2	42.00	20250200
LH2 PRESS N FL CNTL SV3	42.00	20250300
ET ULLAGE SIG CND PKG =1	33.33	20270100
ET ULLAGE SIG CND PKG =2	33.33	20270200
ET ULLAGE SIG CND PKG =3	33.33	20270300
PROP LOW LEV SNSR SIGCND	7.00	20280000
PROP LOADING SNSR SIGCND	7.00	20290000
MPS DELTA P GSE	14.00	203220320000

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: ORBITAL MANEUVERING SYSTEM

CODE 21

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
ENGINE CONTROL VALVE =1	56.00	210121010100
ENGINE CONTROL VALVE =2	56.00	210121010200
ENGINE CONTROL VALVE =3	56.00	210121010300
ENGINE CONTROL VALVE =4	56.00	210121010400
HE ISCL VLVS-SET 1	24.00	210221020100
HE ISCL VLVS-SET 2	24.00	210221020200
HE ISCL VLVS-SET 3	24.00	210221020300
VAPCR ISCL VLVS-SET 1	24.00	210321030100
VAPCR ISCL VLVS-SET 2	24.00	210321030200
VAPCR ISCL VLVS-SET 3	24.00	210321030300
VAPCR ISCL VLVS-SET 4	24.00	210321030400
QUANTITY GAGING PROBE =1	67.00	210521050100
QUANTITY GAGING PROBE =2	67.00	210521050200
QUANTITY GAGING PROBE =3	67.00	210521050300
QUANTITY GAGING PROBE =4	67.00	210521050400
HE ISC VLV=1-AUX KIT	24.00	210621060100
HE ISC VLV=2-AUX KIT	24.00	210621060200
VAPCR ISC VLV=1-AUX KIT	24.00	21070100
VAPCR ISC VLV=2-AUX KIT	24.00	21070100
ENG GIMBAL ACTUATOR =1	134.50	210921090100
ENG GIMBAL ACTUATOR =2	134.50	210921090200
ENG GIMBAL ACTUATOR =3	134.50	210921090300
ENG GIMBAL ACTUATOR =4	134.50	210921090400
PROP Tnk ISC VLVS	32.00	211021100000
CROSSFEED VLVS-SET 1	32.00	211321130100
CROSSFEED VLVS-SET 2	32.00	211321130200
CROSSFEED VLVS-SET 3	32.00	211321130300
THERMAL CNTL HTR =1	700.00	211421140100
THERMAL CNTL HTR =2	700.00	211421140200
ENG ARMING SOL VALVE =1	56.00	211521150100
ENG ARMING SOL VALVE =2	56.00	211521150200
THERML CNTL HTRS-AUX KIT	700.00	211621160000
PROP Tnk ISO VLV-AUX KIT	32.00	211821180000
CROSSFEED LINE HTRS	50.00	211921190000
ENGINE =1 HEATER	50.00	212021200100
ENGINE =2 HEATER	50.00	212021200200
VALVE POSITION IND	0.40	212121210000
VALVE POS IND-AUX KIT	0.40	212221220000
PROP LOW LEVEL SENSOR =1	11.25	212321230100
PROP LOW LEVEL SENSOR =2	11.25	212321230200

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: REACTION CONTROL SYSTEM

CODE 22

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
THRUSTER - FWD 1402	56.00	220122010000
THRUSTER - AFT 2404	56.00	220222020000
THRUSTER-VERNIER FWD 0202	15.00	220322030000
THRUSTER VERNIER AFT 0404	15.00	220422040000
HP HELIUM ISCL VLV -FWD 0401	84.00	220622060000
LP HEL. ISCL VLV-FWD 0202	84.00	220722070000
HP HELIUM ISCL VLV -AFT 0801	84.00	220822080000
LP HELIUM ISCL VLV -AFT 0402	84.00	220922090000
PROP MANIF ISCL VLV -FWD 0801	84.00	221022100000
PROP MANIF ISCL VLV -AFT 1601	84.00	221122110000
PROPELLANT ISCL VLV-VERNO 0401	56.00	221222120000
TANK ISC THRST VLV- FWD 0401	84.00	221322130000
TANK ISC THRST VLV-AFT 0801	84.00	221422140000
TANK HEATERS-AFT LEFT 0404	55.00	221522150000
TANK HEATERS-AFT RIGHT 0404	55.00	221622160000
MAIN ENG HEATERS-FWD 1414	10.00	221722170000
MAIN ENG HEATERS-AFT 2424	10.00	221822180000
PROP FEED LINE HTRS-AFT 0808	16.00	221922190000
PRESS PANEL HTRS 0404	20.00	222022200000
FEED SYS HTRS-FWD 0404	160.00	222122210000
VERNIER ENG HTRS-FWD 0202	5.00	222222220000
VERNIER ENG HTRS-AFT 0404	5.00	222322230000

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: POWER GENERATION SYSTEM

CODE 30

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
GC2 PURGE VENT HTR =1	33.00	300130010100
GC2 PURGE VENT HTR =2	33.00	300130010200
GH2 PURGE VENT HTR =1	61.00	300230020100
GH2 PURGE VENT HTR =2	61.00	300230020200
H2O RELIEF VENT HTR =1	16.00	300330030100
H2O RELIEF VENT HTR =2	16.00	300330030200
FCP =1 CNTLS + FLCWMETRS	15.00	300430040100
FCP =2 CNTLS + FLCWMETRS	15.00	300430040200
FCP =3 CNTLS + FLCWMETRS	15.00	300430040300
FCP =1 PUMP + H2O SENSOR	150.00	300530050100
FCP =2 PUMP + H2O SENSOR	150.00	300530050200
FCP =3 PUMP + H2O SENSOR	150.00	300530050300
FCP =1 GC2 PURGE VALVE	33.00	300630060100
FCP =2 GC2 PURGE VALVE	33.00	300630060200
FCP =3 GC2 PURGE VALVE	33.00	300630060300
FCP =1 GH2 PURGE VALVE	10.00	300630070100
FCP =2 GH2 PURGE VALVE	10.00	300630070200
FCP =3 GH2 PURGE VALVE	10.00	300630070300
FCP =1 START + SUST HTR	6000.00	300830080100
FCP =2 START + SUST HTR	6000.00	300830080200
FCP =3 START + SUST HTR	6000.00	300830080300
H2O LINE HEATER-FCP =1	15.00	30150100
H2O LINE HEATER-FCP =2	15.00	30150200
H2O LINE HEATER-FCP =3	15.00	30150300
FCP =1 THERMAL CNTL HTR	150.00	30170100
FCP =2 THERMAL CNTL HTR	150.00	30170200
FCP =3 THERMAL CNTL HTR	150.00	30170300

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: CRYOGENICS SYSTEM

CODE 31

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
VAC-ICN PWR SUPL GSE =1	10.00	310131010100
VAC-ICN PWR SUPL GSE =2	10.00	310131010200
VAC-ICN PWR SUPL GSE =3	10.00	310131010300
VAC-ICN PWR SUPL GSE =4	10.00	310131010400
SIG CCND TEMP SNSR	1.30	310231020000
SIG CCND QTY =1	4.00	310331030100
SIG CCND QTY =2	4.00	310331030200
SIG CCND QTY =3	4.00	310331030300
SIG CCND QTY =4	4.00	310331030400
SIG CCND PRESS =1	0.30	310431040100
SIG CCND PRESS =2	0.30	310431040200
SIG CCND PRESS =3	0.30	310431040300
SIG CCND PRESS =4	0.30	310431040400
SIG CCND PRESS CNT =1	1.00	310531050100
SIG CCND PRESS CNT =2	1.00	310531050200
SIG CCND PRESS CNT =3	1.00	310531050300
SIG CCND PRESS CNT =4	1.00	310531050400
SWITCHING UNIT O2-CN	26.00	31060000
SWITCHING UNIT O2-CFF	0.40	31060010
SWITCHING UNIT H2-CN	2.50	31070000
SWITCHING UNIT H2-CFF	0.20	31070010
SOLENOID VLV FCP =1	56.00	311131120100
SOLENOID VLV FCP =2	56.00	311131120200
SOLENOID VLV FCP =3	56.00	311131120300
SOLENOID VALVE ECLSS =1	56.00	311131130100
SOLENOID VALVE ECLSS =2	56.00	311131130200
SOL VLV MANIFOLD =1	56.00	311531150100
SOL VLV MANIFOLD =2	56.00	311531150200
SOL VLV MANIFOLD =3	56.00	311531150300
SOL VLV MANIFOLD =4	56.00	311531150400
HEATERS OXYGEN SET 1	394.50	311731170100
HEATERS OXYGEN SET 2	394.50	311731170200
HEATERS OXYGEN SET 3	81.00	311731170300
HEATERS HYDROGEN SET 1	81.00	311731180100
HEATERS HYDROGEN SET 2	81.00	311731180200
HEATERS HYDROGEN SET 3		311731180300

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: AUXILIARY POWER UNIT

CODE 32

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
FUEL ISOLATION VALVE =1	40.00	320232020100
FUEL ISOLATION VALVE =2	40.00	320232020200
FUEL ISOLATION VALVE =3	40.00	320232020300
APU =1 CONTROLLER	150.00	320332030100
APU =2 CONTROLLER	150.00	320332030200
APU =3 CONTROLLER	150.00	320332030300
TANK HTR =1 - LH SIDE	50.00	320532050100
TANK HTR =2 - LH SIDE	50.00	320532050200
TANK HTR =3 - RH SIDE	50.00	320532050300
APU LINE HEATERS =1	50.00	320732070100
APU LINE HEATERS =2	50.00	320732070200
APU LINE HEATERS =3	50.00	320732070300
FUEL QTY GAGE =1	1.00	320832080100
FUEL QTY GAGE =2	1.00	320832080200
FUEL QTY GAGE =3	1.00	320832080300
APU OIL LINE HTR =1	100.00	320932090100
APU OIL LINE HTR =2	100.00	320932090200
APU OIL LINE HTR =3	100.00	320932090300
APU =1 TURB VLV HTR	68.30	321032100100
APU =2 TURB VLV HTR	68.30	321032100200
APU =3 TURB VLV HTR	68.30	321032100300
APU =1 TURB GAS GEN HTR	68.30	321132110100
APU =2 TURB GAS GEN HTR	68.30	321132110200
APU =3 TURB GAS GEN HTR	68.30	321132110300
SERVICE LINE HEATER =1 0201	50.00	321232120100
SERVICE LINE HEATER =2 0201	50.00	321232120200
SERVICE LINE HEATER =3 0201	50.00	321232120300

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: ENVIRONMENTAL CONTROL & LIFE SUPPORT CODE 40

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
CABIN FAN =1	500.00	400140010100
CABIN FAN =2	500.00	400140010200
CABIN FAN =3	500.00	400140010300
WATER PUMP PKG PRI A	270.00	400240020100
WATER PUMP PKG PRI B	270.00	400240020200
WATER PUMP PKG SEC	270.00	400240020300
CABIN PRESS CNTL SYSTEM	84.00	400340030000
CAB PRESS CNTL-AIRLK SP	30.60	400340030010
CAB PRESS CNTL-EMERG MD	23.00	400340030020
WATER SUPLIMATOR SYS =1	101.00	400440040100
WATER SUPLIMATOR SYS =2	101.00	400440040200
AVIONICS FANS-BAY 1 A	180.00	400540050100
AVIONICS FANS-BAY 1 B	180.00	400540050200
AVIONICS FANS-BAY 2 A	180.00	400540050300
AVIONICS FANS-BAY 2 B	180.00	400540050400
AVIONICS FANS-BAY 3 A	180.00	400540050500
AVIONICS FANS-BAY 3 B	180.00	400540050600
H2O SEPARATORS ARS - =1	40.00	400640060100
H2O SEPARATORS ARS - =2	40.00	400640060200
H2O SEPARATORS ARS - =3	40.00	400640060300
CABIN HEATER =1	333.33	400740070100
CABIN HEATER =2	333.33	400740070200
CABIN HEATER =3	333.33	400740070300
INST + CONTROLS ARS	47.00	400840080000
IMC ASSEMBLY FAN =1	55.00	400940090100
IMC ASSEMBLY FAN =2	55.00	400940090200
IMC ASSEMBLY FAN =3	55.00	400940090300
OVEN HEATER =1	150.00	401040100100
OVEN HEATER =2	150.00	401040100200

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: ENVIRONMENTAL CONTROL & LIFE SUPPORT (CONTINUED) CODE 40

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
INST/CONTLS-EVEN FANS =1	55.00	401140110100
INST/CONTLS-EVEN FANS =2	55.00	401140110200
INST/CONTLS-EVEN FANS =1	5.00	401140111100
INST/CONTLS-EVEN FANS =2	5.00	401140111200
WATER HEATER =1	455.00	401240120100
WATER HEATER =2	455.00	401240120200
DUMP NOZZLE - WATER	10.00	401340130000
INSTR + CONTROLS WATER	12.0	401440140000
INSTR + CONTROLS WATER	10.00	401440141000
SOLIDS COLLECTION SLINGS	120.00	401640160000
WATER SEP -LIFE SUPPORT	50.00	401740170000
DUMP NOZZLE-URINE	10.00	401840180000
INSTR + CONTROLS WASTE	10.00	401940190000
SMOKE DET SENR-FLT/MIC	4.00	402040200100
SMOKE DET SENR-BAY A1	4.00	402040200200
SMOKE DET SENR-BAY A2	4.00	402040200300
SMOKE DET SENR-BAY A3	4.00	402040200400
SMOKE DETECTION ALARM	8.0	40210000
FLASH EVAPORATOR HTR =1	310.00	40270100
FLASH EVAPORATOR HTR =2	310.00	40270200
FLASH EVAPORATOR EL =1	8.00	40280100
FLASH EVAPORATOR EL =2	8.00	40280200
FRECN PUMP LP 1-A/B ASC	500.00	40290100
FRECN PUMP LP 1-A/B 6 PL	420.00	40290110
FRECN PUMP LP 1-A/B 8 PL	460.00	40290120
FRECN PUMP LP 2-A/B ASC	500.00	40290200
FRECN PUMP LP 2-A/B 6 PL	420.00	40290210
FRECN PUMP LP 2-A/B 8 PL	460.0	40290220
SPACE RADIATOR SYSTEM =1	10.00	40300100
SPACE RADIATOR SYSTEM =2	10.00	40300200
AMMONIA BOILER SYSTEM =1	12.50	40310100
AMMONIA BOILER SYSTEM =2	12.50	40310200
FRECN BYPASS CONTROL =1	6.00	40320100
FRECN BYPASS CONTROL =2	6.00	40320200
DIVERTER VALVE =1	19.50	40330100
DIVERTER VALVE =2	19.50	40330200
LCG COOLANT PUMP =1	0.00	40340100
LCG COOLANT PUMP =2	0.00	40340200
FRECN PROPROR VALVE =1	67.00	40350100
FRECN PROPROR VALVE =2	67.00	40350200

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: HYDRAULICS POWER SYSTEM

CODE 50

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
LG EXTEND VALVE	20.00	500150010000
MAIN LDG GEAR UPLK VL =1	20.00	50020100
MAIN LDG GEAR UPLK VL =2	20.00	50020200
MAIN LDG GEAR UPLK VL =3	20.00	50020300
MAIN LDG GEAR UPLK VL =4	20.00	50020400
LDG GEAR DUMP VLV =1	20.00	50030100
LDG GEAR DUMP VLV =2	20.00	50030200
LDG GEAR DUMP VLV =3	20.00	50030300
LG RETRACT CIRC VLV	20.00	50040000
REDUNDANT S/O VALVE =1	20.00	50050100
REDUNDANT S/O VALVE =2	20.00	50050200
MAIN PUMP =1 DEPRES VLV	26.00	50060100
MAIN PUMP =2 DEPRES VLV	26.00	50060200
MAIN PUMP =3 DEPRES VLV	26.00	50060300
CIRC MOTOR PUMP =1	1561.0	50070100
CIRC MOTOR PUMP =2	1561.0	50070200
CIRC MOTOR PUMP =3	1561.0	50070300
RESVOIR =1 VOLUME SENSOR	8.00	50080100
RESVOIR =2 VOLUME SENSOR	8.00	50080200
RESVOIR =3 VOLUME SENSOR	8.00	50080300
SSME =1 SYS S/O VALVE	20.00	50090100
SSME =2 SYS S/O VALVE	20.00	50090200
SSME =3 SYS S/O VALVE	20.00	50090300
LI ELEVON HTR BKT =1/=2	50.00	50100100
LO ELEVON HTR BKT =1/=2	50.00	50100200
RI ELEVON HTR BKT =1/=2	50.00	50100300
RO ELEVON HTR BKT =1/=2	50.00	50100400
HYDRAULICS CONTINUED		50100901
H2O BOILER =1 STM S/O VL	20.00	50110100
H2O BOILER =2 STM S/O VL	20.00	50110200
H2O BOILER =3 STM S/O VL	20.00	50110300
H2O BOILER =1 XFER VLV	50.00	50120100
H2O BOILER =2 XFER VLV	50.00	50120200
H2O BOILER =3 XFER VLV	50.00	50120300
H2O BCLR =1 THRM CNTL VL	20.00	50130100
H2O BCLR =2 THRM CNTL VL	20.00	50130200
H2O BCLR =3 THRM CNTL VL	20.00	50130300
H2O BOILER =1 ELECT CNT	7.00	50140100
H2O BOILER =2 ELECT CNT	7.00	50140200
H2O BOILER =3 ELECT CNT	7.00	50140300
H2O BOILER =1 HEATER	100.00	50150100
H2O BOILER =2 HEATER	100.00	50150200
H2O BOILER =3 HEATER	100.00	50150300
H2O BOILER =1 QTY GAGE	5.0	50160100

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: HYDRAULICS POWER SYSTEM (CONTINUED) CODE 50

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
H2O BUILER =2 QTY GAGE	5.0	50160200
H2O BUILER =3 QTY GAGE	5.0	50160300
ELEVON ACT SW VLV PCS	1.00	50170000
RUD/SPDRK ACT VL PCS =1	1.0	50180100
RUD/SPDRK ACT VL PCS =2	1.0	50180200
TVC ACT SW VLV POS	1.00	50190000
RESVR =1 LCW LEVEL INC	2.0	50190901
RESVR =2 LCW LEVEL INC	2.0	50200200
RESVR =3 LCW LEVEL INC	2.0	50200300
BODYFLAP MTR 1 HTR =1/=2	50.00	50220100
BODYFLAP MTR 2 HTR =1/=2	50.00	50220200
BODYFLAP MTR 3 HTR =1/=2	50.00	50220300
MAIN PUMP =1 HTR - =1/=2	25.00	50240100
MAIN PUMP =2 HTR - =1/=2	25.00	50240200
MAIN PUMP =3 HTR - =1/=2	25.00	50240300
RUDDER SPDRK MTR =1 HTR	50.00	50250100
RUDDER SPDRK MTR =2 HTR	50.00	50250200
RUDDER SPDRK MTR =3 HTR	50.00	50250300
RUDDER SPDRK MTR =4 HTR	50.00	50250400
RUDDER SPDRK MTR =5 HTR	50.00	50250500
RUDDER SPDRK MTR =6 HTR	50.00	50250600
SSME =1 HYDR ISOL VALVE	80.00	50260100
SSME =2 HYDR ISOL VALVE	80.00	50260200
SSME =3 HYDR ISOL VALVE	80.00	50260300

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: DOCKING AND CARGO HANDLING

CODE 51

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
MANIPULATOR	1600.00	51010000
MANIP DEPLOY DRIVE	150.00	51020000
MANIP RETENT LATCH DRIVE	60.00	51030000
PL BAY DOOR RET LCH DRIVE	60.00	51050000
XFER TUNNEL EXT/RET DR 1	200.00	51060100
XFER TUNNEL EXT/RET DR 2	200.00	51060200
XFER TUNNEL LICH DRIVE =1	140.00	51070100
XFER TUNNEL LICH DRIVE =2	140.00	51070200
PBD CIRCUM LATCH DRIVE	140.00	51080000
PBD CENTER LINE LICH DR	220.00	51090000
RADIATOR RET LATCH DRIVE	60.00	51100000
RADIATOR DEPLOY DRIVE	15.00	51110000
REN07 SENSOR DEPL DR =1	200.00	51120100
REN02 SENSOR DEPL DR =2	200.00	51120200
MANIP CNTL INTERFACE UNIT	11.00	511451140000
E/T UMB LH DOOR DRIVE	200.00	51150000
E/T UMB LH DOOR LATCH	200.00	511651160000
E/T UMB RH DOOR DRIVE	200.00	51170000
E/T UMB RH DOOR LATCH	200.00	51180000

TABLE 7.3-2 (Continued)

SHUTTLE SUBSYSTEM ELEMENT CODE AND PRIME POWER LISTING

SUBSYSTEM: MECHANICAL SYSTEM AND LANDING

CODE 52

<u>ELEMENT NAME</u>	<u>S/S WATTS</u>	<u>ELEMENT CODE</u>
RUD/SPL BRKE S/V RUD	15.00	52010000
RUD/SFD BRKE S/V	15.00	52020000
STARTRACKER DCCR DRIVE	200.00	52040000
RCS TCP DCCR ACT	200.00	52050000
RCS LH SIDE DCCR ACT	200.00	52060000
RCS RH SIDE DCCR ACT	200.00	52070000
LAUNCH UMB LH DCCR CR	200.00	52080000
LAUNCH UMB RH DCCR CR	200.00	52100000
P/L BAY RH DR DRIVE	400.00	52160000
P/L BAY LH DR DRIVE	400.00	52170000
GN+C PROBE ACT LH-A-T	5.00	52180000
GN+C PROBE ACT RH-A-T	5.00	52200000
NOSE WHEEL STEERING UNIT	10.00	52260000
BRAKE/SKID POWER SYS	140.00	52270000
GN+C PROBE HEATERS	1100.00	52300000
VENT DCCR MOTORS	10.00	523252320000
VENT DCCR MOTORS	100.00	523352330000
VENT DCCR MOTORS	20.00	523452340000
VENT DCCR MTR PL BAY WNG	100.00	523552350000

APPENDIX 7.4

**SAMPLE SET OF USER LOAD ELEMENT DATA SHEETS
(GENERATED FROM VENDOR INFORMATION BY RI/JSC)**

7.4.0

Subsystem EMFC
 Equipment No. 010101
 Equipment Title IMU

Power Requirements 1
 DC Load

Nominal Power (Watts) 75
 Mode of Operation Stand By

NIF0004-002

Number in System
3

Parameter		Calculated or Estimated Value	Spec. Value	Test Value	Remarks
A M P E R E S	Average (steady state) continuous duty	<u>3.12</u>			24 volts at load interface
		<u>2.67</u>			28 volts at load interface
		<u>2.34</u>			32 volts at load interface
	Peak transient and duration 2	<u>0</u>			Amps
		<u>0</u>			Time in milliseconds
	Load Range 3	<u>120W</u> <u>28V = 4.3A</u>			Max
<u>12W</u> <u>28V = .36A</u>				Min	
Malfunction voltage limit (volts) 4	<u>32V</u>			Max	
	<u>24V</u>			Min	
Duty Cycle 5	Periodic <input type="checkbox"/>	Percent "on" _____ %		Indicate units if other than minutes	
	Aperiodic <input type="checkbox"/>	Period of Cycle _____			
Input voltage Converter	Yes <input checked="" type="checkbox"/>	Converted to <u>30Vdc</u> Volts _____			
	No <input type="checkbox"/>	Frequency <u>15.000</u> <u>5.000 2700</u> AC <input checked="" type="checkbox"/> DC <input checked="" type="checkbox"/>			

Number Normally Operating
3

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

JSC Engineer Bill Swingle TABLE 1 Date 3-27-74

PAGE ENCLOSURE 4

RI 2122 - 15 Jun 75

Subsystem EPDC Power Requirements
 Equipment No. 10100 DC Load
 Equipment Title POWER CONTROL ASSY-FWD

1

Nominal Power (Watts) 30
 Mode of Operation OPERATE

Number in System
3

Number Normally Operating
3

Note:
Component
no. 3 50%
700
200
1000

Parameter		Calculated or Estimated Value	Spec. Value	Test Value	Remarks
A M P E R E S	Average (steady state) continuous duty	1.3			24 volts at load interface
		1.7			28 volts at load interface
		.95			32 volts at load interface
	Peak transient and duration (2)	0			Amps
		0			Time in milliseconds
	Load Range (3)	NA			Max
NI				Min	
Malfunction voltage limit (volts) (4)	TBD			Max	
	TBD			Min	
Duty Cycle (5)	Periodic <input checked="" type="checkbox"/>	Percent "on" <u>100%</u>	Indicate units if other than minutes		
	Aperiodic <input type="checkbox"/>	Period of Cycle _____			
Input voltage Converter	Yes <input type="checkbox"/>	Converted to Volts _____			
	No <input checked="" type="checkbox"/>	Frequency _____ AC <input type="checkbox"/> DC <input type="checkbox"/>			

REPRODUCTION OF THE ORIGINAL PAGE IS POOR

Number in System 2

7.4.3

Number Normally Operating 2

Subsystem OMS (2 Pods)
 Equipment No. 12121
 Equipment Title ENGINE CONTROL VALVES

Power Requirements

1

DC Load

Nominal Power (Watts) 32.0

Mode of Operation START

Parameter		Calculated or Estimated Value	Spec. Value	Test Value	Remarks
A M P E R E S	Average (steady state) continuous duty				24 volts at load interface
					28 volts at load interface
					32 volts at load interface
	Peak transient and duration (2)	1.0			Amps
0.1				Time in milliseconds	
Load Range (3)	Max	NA			
	Min	NA			
Malfunction voltage limit (volts) (4)	Max	TBD			
	Min	TBD			
Duty Cycle (5)	Periodic <input checked="" type="checkbox"/>	Percent "on" <u>100</u> %		Indicate units if other than minutes	
	Aperiodic <input type="checkbox"/>	Period of Cycle _____			
Input voltage Converter	Yes <input type="checkbox"/>	Converted to Volts _____			
	No <input checked="" type="checkbox"/>	Frequency _____ AC <input type="checkbox"/> DC <input type="checkbox"/>			

JSC Engineer E. Beaudet TABLE 1
 From PK

Date 4/23/74

MF0004-002

Page

ENCLOSURE 4

Subsystem OMS (2 PODS) Power Requirements 1
 Equipment No. 12103 DC Load
 Equipment Title HELICOPTER ISOLATION VALVES

Nominal Power (Watts) 24.3
 Mode of Operation OPERATE

MIF0001-002

Parameter		Calculated or Estimated Value	Spec. Value	Test Value	Remarks
A M P E R E S	Average (steady state) continuous duty	<u>8.6</u>			24 volts at load interface 28 volts at load interface 32 volts at load interface
	Peak transient and duration 2	<u>0.0</u>			Amps
		<u>0.0</u>			Time in milliseconds
	Load Range 3	<u>NA</u>			Max
		<u>NA</u>			Min
	Malfunction voltage limit (volts) 4	<u>TBD</u>			Max
		<u>TBD</u>			Min
Duty Cycle 5		Periodic <input checked="" type="checkbox"/>	Percent "on" <u>100</u> %	Indicate units if other than minutes	
		Aperiodic <input type="checkbox"/>	Period of Cycle _____		
Input voltage Converter		Yes <input type="checkbox"/>	Converted to Volts _____		
		No <input type="checkbox"/>	Frequency _____ AC <input type="checkbox"/> DC <input type="checkbox"/>		

Number in System
4

Number Normally Operating
4

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

JSC Engineer E. B. [Signature] TABLE 1 Date 4-23-74

PAGE 4 ENCLOSURE 4

Subsystem _____ Power Requirements 1
 Equipment No. 12095 DC Load _____ Nominal Power (Watts) 72
 Equipment Title L-Ho Receiver Valve Solenoid Mode of Operation Electric

Number in System
3

Number Normally Operating
3

Parameter	Calculated or Estimated Value	Spec. Value	Test Value	Remarks	
A M P E R E S	Average (steady state) continuous duty	<u>1.5</u>		24 volts at load interface	
				28 volts at load interface	
				32 volts at load interface	
	Peak transient and duration 2	<u>0</u>			.Amps
					Time in milliseconds
	Load Range 3	<u>NA</u>			Max
Min					
Malfunction voltage limit (volts) 4	<u>TBD</u>			Max	
				Min	
Duty Cycle 5	Periodic <input type="checkbox"/>	Percent "on" _____ %		Indicate units if other than minutes	
	Aperiodic <input type="checkbox"/>	Period of Cycle _____			
Input voltage Converter	Yes <input type="checkbox"/>	Converted to Volts _____			
	No <input checked="" type="checkbox"/>	Frequency _____ AC <input type="checkbox"/> DC <input type="checkbox"/>			

JSC Engineer E. H. ... TABLE 1 Date 5/13-71

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

(6)

Subsystem PWR GEN Power Requirements
Equipment No. 13006 DC Load
Equipment Title FCP 500 PWR VLV

(1)

Nominal Power (Watts) 10
Mode of Operation Intermittent
Normally Class

MF0006-002

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

Number in System
3

Number Normally Operating
3

7-4-7

note:
On for
≈ 2 minutes
in 12 hours

Parameter		Calculated or Estimated Value	Spec. Value	Test Value	Remarks
A M P E R E S	Average (steady state) continuous duty				24 volts at load interface
		<u>1.178</u>	0.358		28 volts at load interface
					32 volts at load interface
	Peak transient and duration (2)				Amps
					Time in milliseconds
	Load Range (3)	<u>NA</u>			Max
		<u>NA</u>			Min
	Malfunction voltage limit (volts) (4)	<u>TBD</u>			Max
		<u>TBD</u>			Min
	Duty Cycle (5)	Periodic <input checked="" type="checkbox"/>	Percent "on" <u>100</u> %	Indicate units if other than minutes	
		Aperiodic <input type="checkbox"/>	Period of Cycle _____		
	Input voltage Converter	Yes <input type="checkbox"/>	Converted to Volts _____	CONTROL: MANUAL OR AUTO	
		No <input checked="" type="checkbox"/>	Frequency AC <input type="checkbox"/> DC <input checked="" type="checkbox"/>	Source: MN DC Bus	

PAGE

ENCLOSURE 4

JSC Engineer J. K. [unclear] TABLE 1 Date 4/25/75

REPRODUCIBILITY OF THE ORIGINAL PAGE IS FOUR.

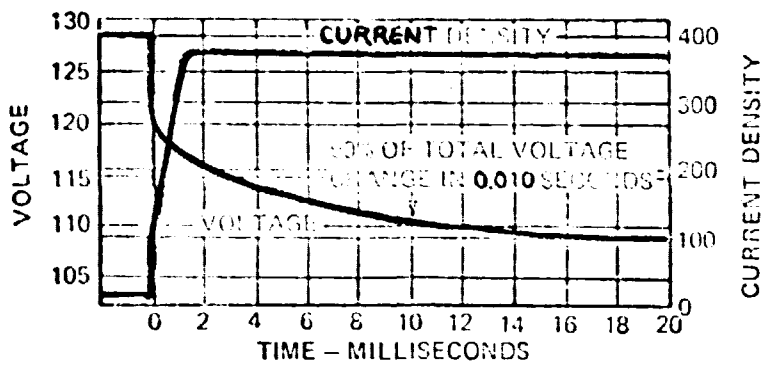


Figure A
PC15 Transient Response to Step Load Change

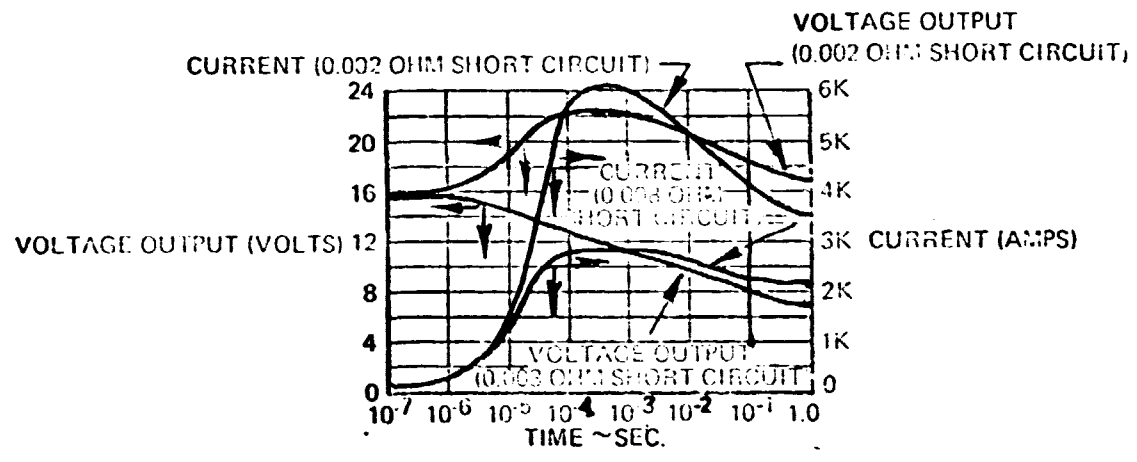


Figure B PC17 Powerplant Impedance

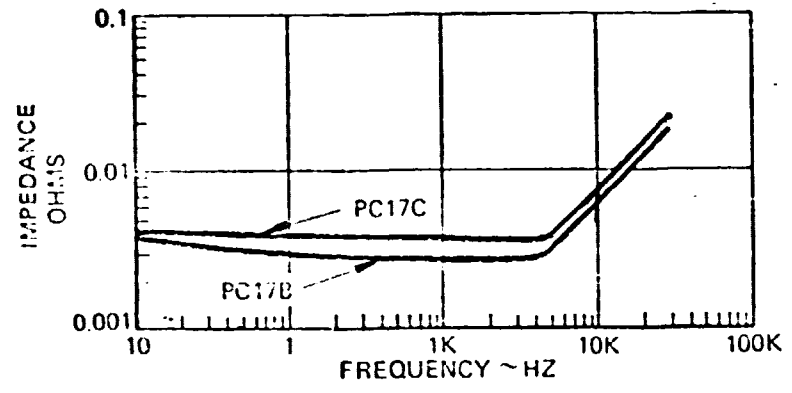


Figure C
PC17 Short Circuit Capability

(REPRODUCED FROM PRATT AND WHITNEY AIRCRAFT DATA)

APPENDIX 7.5

PROCUREMENT SPECIFICATIONS FOR CRITICAL EPDC ELEMENTS

(DOCUMENTS GENERATED BY ROCKWELL INTERNATIONAL)

7.5.0

(S)³ 74-042

PREPARED BY	CODE IDENT. NO.: 03953 SPACE DIVISION NORTH AMERICAN ROCKWELL CORPORATION 17214 LAKEWOOD BOULEVARD • CONNEY, CALIFORNIA 90241 SPECIFICATION	NUMBER	10495-0012
C. J. MURPHY		TYPE	
APPROVALS		DOCUMENT	
<i>C. J. Murphy 9-4-73</i>		DATE	August 30, 1973
<i>L. B. Hale 9-3-73</i>		SUPERSEDES SPEC. DATED:	
		REV. LTR.	PAGE 1 of 59
		<i>VEN</i>	

TITLE Total Pages 54

INVERTER, POWER STATIC, 115 VOLT,
SINGLE-PHASE, 400 HZ

in Paulowski?
af.
Paulowski

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ORIGINAL PAGE IS POOR

NUMBER	REVISION LETTER	PAGE
MC495-0012		2

1. SCOPE

This specification establishes the performance, design, development and verification requirements for a single-phase modular inverter referred to herein as the inverter.

1.1 Seller's Equipment Internal Design. Except as otherwise specified the requirements of this specification are not intended to restrict inverter internal design except for those areas necessary for compatibility with the design requirements specified herein.

1.2 Sub-Tier Supplier Control. Where necessary to meet the requirements of this specification, the seller shall impose this specification on sub-tier suppliers with design responsibility.

2. APPLICABLE DOCUMENTS

The following documents of the exact issue shown form a part of this specification to the extent specified herein. In the event of a conflict between the documents referenced herein and the content of this specification, the content of this specification shall take precedence.

SPECIFICATIONS

Federal Military

MIL-B-5097E(2) 31 August 1970	Bonding, Electrical and Lightning Protection, for Aerospace Systems
MIL-C-5541B(1) 30 June 1970	Chemical Conversion Coatings on Aluminum and Aluminum Alloy
MIL-C-7073B 5 December 1969	Cable, Electrical, Aerospace Vehicle, General Specification for
MIL-C-83723 26 March 1965	Connector, Electric, Circular, Environment Resisting, General Specification for
MIL-I-26860B 17 May 1972	Indicator, Humidity, Plug, Color Change
MIL-I-27273A(3) 3 June 1965	Inverter, Power, Static, General Specification for
MIL-W-81381 15 October 1966	Wire, Electric, Polyimide Insulation, Copper and Copper Alloy
<u>NASA/JSC</u>	
MSC-Spec-Q-1A October 1967	Crimping of Electrical Connections, Requirements for

SPECIFICATIONS

Rockwell International/Space Division

- MC414-0148C
25 March 1966

Connector, Receptacle, Electrical
- MC999-0096B
6 July 1973

Materials and Processes Control and Verification System for Space Shuttle Program Suppliers and Subcontractors
- MF0004-002A
13 July 1973

Electrical Design Requirements for Electrical Equipment Utilized on the Space Shuttle Vehicle
- MF0004-006
27 July 1973

Instrumentation Requirements for Suppliers and Sub-contractors for the Space Shuttle Program
- MF0004-100
31 July 1973

Mechanical Orbiter Project Parts List
- MF0004-400
25 July 1973

Electrical, Electronic and Electromechanical (EEE) Orbiter Project Parts List

STANDARDS

Federal

- FED-STD-101B(2)
8 October 1971

Preservation, Packaging, and Packing Materials: Test Procedures

Military

- MIL-STD-12C(1)
1 February 1971

Abbreviations for Use on Drawings, Specifications, Standards and in Technical Documents
- MIL-STD-129E(6)
10 April 1972

Marking for Shipment and Storage
- MIL-STD-130D(1)
30 July 1971

Identification Marking of U. S. Military Property
- MIL-STD-143B
12 November 1969

Standards and Specifications, Order of Precedence for Selection of

NUMBER	REVISION LETTER	PAGE
PC495-0012		4

STANDARDS

MIL-STD-202D 14 April 1969	Test Methods for Electronic and Electrical Component Parts
MIL-STD-280 7 July 1969	Definitions of Item Levels, Items Exchange, Models and Related Items
MIL-STD-461A 1 August 1968 and Shuttle Amendment 4 June 1973	Electromagnetic Interference Characteristics, Requirements for Equipment
MIL-STD-740 6 July 1964	Noise Measurements of Shipboard Machinery and Equipment
MIL-STD-794C(1) 18 February 1972	Parts and Equipment, Procedure for Packaging and Packing of
MIL-STD-810B(4) 21 September 1970	Environmental Test Methods
<u>SAE Aerospace Standard</u>	
AS1212 December 1971	Electrical Power, Aircraft, Characteristics and Utilization of

OTHER PUBLICATIONS

Handbooks

DODM4-1 Latest Revision	Federal Supply Code for Manufacturers' Name to Code
MMB5300.4(3A) May 1968	Requirements for Soldered Electrical Connections
MMB6000.1(1A) December 1969	Requirements for Packaging, Handling, and Transportation for Aeronautical and Space Systems Equipment and Associated Components

3. REQUIREMENTS

3.1 Item Definition

3.1.1 Item Diagram. Figure 1 is the schematic block diagram showing the function of the inverter assembled as a three-phase array in the electrical power distribution and control sub-system.

3.1.2 Interface Definition

3.1.2.1 Envelope. The inverter envelope and its attachment provisions shall not exceed the dimensions shown in Figure 2.

3.1.2.2 Mounting. The mounting provisions of the inverter shall be as shown in Figure 3 and in accordance with the requirements of paragraph 3.2.5.2.C.2.

3.1.2.3 Weight. The inverter shall have a maximum weight of (TBD) pounds.

3.1.2.4 Cooling

3.1.2.4.1 Coldplate Cooling. The inverter shall be designed for conduction cooling by contact with the mounting surface. An aluminum mounting surface will be provided in the spacecraft by the buyer. The mounting surface will have a contact area of not less than TBD square inches. The spacecraft mounting surface will maintain the inverter baseplate at the following temperatures by coolant flow for rated inverter loads:

<u>Temperature Condition</u>	<u>Inverter Surface Temp. Above Inlet</u>	<u>Inv. Surface Temp. Above Outlet</u>
(a) Maximum	120 F (Maximum)	140 ± 2 F
(b) Minimum	35 ± 2 F	55 ± 2 F

3.1.2.4.2 Heat Flux. Heat flux loading shall be arranged to take maximum advantage of the coldplate temperature distribution. The maximum heat flux in any local inverter surface area shall be shown by calculation not to exceed TBD watts per square inch. Thermal conductance between the inverter baseplate and the coldplate mounting surface shall be 500 BTU per hour per square foot per degree F, minimum.

3.1.2.4.3 Cooling Surface Finish. The inverter baseplate shall have a surface finish of 63 micro-inches RMS and a flatness deviation of not more than 0.010 inch total indicated run-out. The baseplate shall be measured for flatness when bolted to a test plate with 0.25-inch bolts torqued to 70 plus or minus 5 inch-pounds. Depth gage measurements shall indicate the flatness of the inverter baseplate through each of TBD holes in the test plate. The test plate used shall be mutually acceptable to the Seller and the Buyer.

CODE IDENT. NO. 03953

NUMBER	REVISION LETTER	PAGE
MC495-001		6

3.1.2.5 Temperature Sensor. The inverter shall incorporate a transducer in accordance with specification MF0004-006 which shall provide an electrical signal proportional to the inverter internal temperature. The transducer shall consist of a resistance wire wound sensor with the following characteristics: 500 ohms \pm 2 percent at 75 degrees F; 455 ohms \pm 2 percent at 32 degrees F; and 650 ohms \pm 2 percent at 248 degrees F. The transducer shall be located within the inverter to indicate excessive inverter temperature in the event of impending failure due to a malfunction or overload.

3.1.2.6 Sealing. The inverter shall be designed to seal those portions of the circuit that will burn, spark or outgas because of electrical overload or short circuit.

3.1.2.7 Finish. All areas of the inverter exposed to external environments, except coldplate mating surfaces, nameplate and connectors shall be chem-filmed per MIL-C-5541, Class 1A.

3.1.2.8 Vibration Isolation. The inverter shall be designed so that external vibration isolators are not required.

3.1.2.9 Electrical Connectors. The electrical connectors used for the inverter outputs shall be mutually acceptable to the Buyer and the Seller and shall be governed by MF0004-400, Orbiter project parts list and the following:

- a. Keyed cylindrical (preferably bayonet locking) configurations per MIL-C-83723 shall be utilized, if possible.
- b. In applications where the MIL-C-83723 bayonet style cannot be used due to wire gauge limitations, threaded coupling designs may be employed. Buyer approval is required prior to usage.
- c. Rectangular connectors shall be per Buyer specification MC414-0148 and may be employed in those applications where cylindrical connectors will not allow sufficient wire penetration. Buyer approval is required prior to usage.
- d. The inverter connector shall be mounted on the front panel.
- e. Socket contact arrangements shall be used as the "hot" or energized half when a connection is broken.
- f. Connector keys shall be designed such that engagement of the keys occurs prior to engagement of the contacts.

3.1.2.9.1 Keyway Clocking. The connector(s) on the inverter shall be oriented so that the master (largest) key is located at the top-centerline position on the connector. The connector keyway clocking shall be shown on the Seller's drawing of the inverter envelope.

3.1.2.10 Connections. The design of input and output connections shall be mutually acceptable to the Buyer and the Seller. Electrical connectors shall be per paragraph 3.1.2.9. The connections required are as follows: D-C plus, D-C minus, A-C phase output, A-C neutral, two for the inverter temperature transducer output, overload grounding signal, phase synchronization signal output, phase synchronization signal input, and central timing signal input.

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3.1.2.10.1 Negative and Neutral Connections. The direct-current input negative and the alternating current output neutral connections in the inverter shall be isolated from the inverter chassis and from each other.

3.1.2.11 Adjustment. The inverter shall require no external adjustment for voltage or frequency regulation. Provision shall be made for internal voltage adjustment of plus or minus 2 volts of the nominal line-to-neutral ac voltage by selection of fixed components. No provisions for adjustment of frequency shall be made. Potentiometers or sliding contacts of any type shall not be incorporated in the inverter design.

3.1.2.12 Electrical Power Characteristics. The electrical power characteristics of the inverter interface shall comply with the requirements of MF0004-002 and as follows:

3.1.2.12.1 Input Power. The input voltage shall be 28V dc nominal, two wire, structure ground. Steady state input voltage limits shall be 24 to 32 volts dc. Source dynamic impedance shall be 0. TBD ohms at TBD Hz. The dc transient limits shall be in accordance with MF0004-002. During steady-state DC operation the ripple voltage about the mean level of the D-C voltage shall be four volts peak-to-peak or less over the frequency range per AS-1212. The inverter shall switch off at an input voltage TBD volts or lower and shall turn on at TBD volts \pm 0.5 volts.

3.1.2.12.1.1 Voltage Spikes. Short duration spikes at the dc input terminals of the inverter shall not exceed the values specified in MIL-STD-461 paragraph 6.9.

3.1.2.12.1.2 Loss of Input Power. Instantaneous removal of input power while the inverter is operating shall cause no damage or degradation to the inverter.

3.1.2.12.2 Inverter Feedback

3.1.2.12.2.1 Ripple Current. The ripple current induced on the dc power bus by the inverter shall not exceed the limits of Space Shuttle Amendment "A" to MIL-STD-461 under any combination of load ranging from no load to 750 va; of input voltage ranging from 24 to 32 volts dc, or power factor ranging from 0.7 lagging to 0.9 leading including unity.

3.1.2.12.2.2 Voltage Spikes. Short duration voltage spikes induced on the dc bus by the inverter shall not exceed the values specified in MIL-STD-461, paragraph 6.9.

3.1.2.12.3 Inverter In-Rush Current. In-rush current at turn-on at 32 volts dc and under all combinations of line, load and environment shall not exceed TBS amperes at 0. TBD ohm source impedance in series with TPD microhenries and shall stabilize to within 10 percent of normal within 100 milliseconds.

3.1.2.12.4 Inverter Output. The inverter shall have a single-phase two-wire output with the output voltage and frequency in accordance with paragraphs 3.2.1.1.5 and 3.2.1.1.7 respectively. When the inverter is connected to two other inverters the combined output shall form a 115/200 volt, 400 Hz three-phase, 4-wire wye connected assembly rated at 2250 va at power factors ranging from 0.7 lagging to 0.9 leading including unity power factor.

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3.1.2.12.5 Short Circuit Sensing. Current sensing and conditioning circuitry shall be incorporated in the inverter to complete a 28 volt dc circuit external to the inverter under the following conditions. When the inverter is subjected to an overload of 225 percent of rated current for 15 seconds \pm 1 second, and to 300 \pm 30 percent of rated output current for a duration of 5 seconds plus or minus one second, the inverter shall cause a grounding signal (referenced to the dc negative terminal) to be applied to the overload signal output terminal of the inverter. The device used to complete the circuit must be capable of carrying a relay coil current of 0.2 amperes at 28.0 vdc and a light bulb load of 0.040 amperes at 28 vdc. A "push-to-test" switch shall be incorporated on the inverter to verify continuity from the inverter overload indication signal to the warning light in the cabin.

3.1.2.12.6 Single-Phase Half-Wave Load Capability. The inverter shall have a half-wave, single-phase load applied under the following conditions:

- a. A resistive load of 70 ohms in series with a 1N1187 rectifier, or equivalent, while continuing to meet the performance requirements specified herein.
- b. A resistive load of 2.5 ohms in series with a 1N1187 rectifier, or equivalent, shall activate the short-circuit sensing capability of the inverter. This rectifier-resistive load must be removed at the time the overload trip signal is activated. Upon removal of this load the output voltage shall stabilize to within 115 volts plus or minus 10 percent within 100 milliseconds and transient voltages in excess of 195 volts peak shall not appear.

3.1.2.12.7 Vehicle Interface. The inverter shall operate within its specification limits when connected to vehicle wiring which may have a resistance to ground or resistance between adjacent circuits of two megohms.

3.1.3 Item Identification. The identification of the inverter shall be as follows:

<u>Nomenclature and Mfg. Code Ident. No.</u>	<u>Buyer's Control No.</u>	<u>Seller's Part No.</u>	<u>Traceability Classification</u>
Inverter	HC495-0012-0001	TBS	T _S
Capacitor	N/A	TBS	T _L
Diode	N/A	TBS	T _L
Transistor	N/A	TBS	T _H
Resistor	N/A	TBS	T _L
Transformer	N/A	TBS	T _S
Connector	N/A	TBS	T _H
Temperature	N/A	TBS	T _H
Transducer	N/A	TBS	T _H
Push-to-Test Switch	N/A	TBS	T _S

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3.2 CHARACTERISTICS

3.2.1 Performance

3.2.1.1 Inverter Performance

3.2.1.1.1 Insulation Resistance. The exterior configuration of the inverter shall have insulation properties to prevent electrical shock to personnel. Subsequent to assembly and any potting or sealing required, a minimum insulation resistance of 100 megohms is required between the dc input terminals and the inverter case and the ac output terminals and case at a potential of 100 volts minimum.

3.2.1.1.2 Input Power. The inverter shall meet all performance requirements of this specification when operated within the normal steady state dc voltage range specified in paragraph 3.1.2.12.1.

3.2.1.1.2.1 Input Susceptibility. No change in indication, malfunction, or degradation in performance shall be produced in the inverter when subjected to the dc input ripple specified in paragraph 3.1.2.12.1. The ripple energy placed on the dc bus by the inverter shall not be considered as part of the ripple energy for susceptibility.

3.2.1.1.2.2 Input Transients

3.2.1.1.2.2.1 Normal Electrical System Operation. The inverter shall operate within specification requirements without degradation when subjected to the normal condition dc voltage transients specified in paragraph 3.1.2.12.1.

3.2.1.1.2.2.2 Abnormal Electrical System Operation. The inverter shall not incur damage or degradation of reliability when subjected to the abnormal condition dc voltage transient limits in Paragraph 3.1.2.12.1 and shall return to operation within specification requirements when the D-C voltage returns to normal steady-state condition.

3.2.1.1.2.2.3 Voltage Spikes. The inverter shall operate and shall not incur degradation or damage when subjected to the voltage spikes specified in paragraph 3.1.2.12.1.1.

3.2.1.1.3 Warm-Up Time. The inverter shall stabilize to the performance requirements of this specification within one second after turn-on under all combinations of line, load and environment specified herein. Output line-to-neutral voltage shall be 115 volts, plus or minus 10 percent RMS within 100 milliseconds after turn on under all combinations of line, load and environment specified herein.

3.2.1.1.4 Dielectric Withstanding Voltage. The dielectric withstanding voltage of the inverter shall meet the following requirements:

- a. Electrical parts and sub-assemblies prior to being wired shall be capable of withstanding an initial electrical potential of 1500 volts rms, 60 Hz between insulated points and case without electrical breakdown. Current flow in excess of 0.5 milliamperes or breakdown shall be considered a failure. Any exceptions such as EMI filters, etc., shall be subject to Buyer approval.

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- b. Prior to any sealing or potting, if required, and with RF suppression capacitors and similar components disconnected, no break down of the insulation or leakage current in excess of one milliamperere shall occur during a one-minute test in which 1200 volts rms, 60 Hz is applied between the ac output terminals and the chassis and during a one-minute test in which 500 volts rms, 60 Hz is applied between the dc input power terminals and the chassis.
- c. Subsequent to completion of assembly wiring and any sealing or potting, if required, no break down of insulation or leakage current in excess of one milliamperere shall occur during a one-minute test in which 750 volts dc shall be applied between each output terminal and chassis and during a one-minute test in which 400 vdc is applied between each input power terminal and chassis.

3.2.1.1.5 Output Voltage Steady-State. The steady-state output voltage of the inverter shall be 115 plus 3 volts minus 1 volt rms from no load to 750 va rated load.

3.2.1.1.6 Output Voltage Transient. The inverter output voltage shall remain at 115 volts rms plus or minus 10 percent for any step load or input voltage change within the specified limits. Recovery to the steady-state value shall be within 0.005 seconds. Transient voltages in excess of 195 volts peak shall not appear at the output under any condition.

3.2.1.1.7 Output Frequency. Output frequency shall be 400 Hz plus or minus 2 Hz when the inverter is synchronized to an external TBD Hz plus or minus TBD Hz source supplied through a pair of twisted, shielded leads. The inverter shall present a matched TBD ohms plus or minus TBD ohms impedance to this signal through an isolation transformer. The synchronizing signal shall be 5.0 plus or minus 0.5 volts peak square wave with rise and/or fall time no greater than 1 microsecond. In the absence of this external signal, the inverter frequency shall be maintained at 400 plus or minus 7 Hz. The synchronizing source shall not receive reverse current from the inverter. The synchronizing signal shall have a duty cycle of 40 to 60 percent "on" time.

3.2.1.1.8 Output Power. The inverter shall perform as specified herein under any combination of loads varying from no load to 750 va and at power factor ranging from 0.7 lagging to 0.9 leading including unity power factor. When the inverter is connected into a three-phase assembly the combined output rating shall be 2250 va with the power factor range stated above and with the capability of meeting related performance requirements specified herein. Also, if anyone of the inverters fails the remaining two inverters shall continue to produce two-phase output with the proper phase displacement and phase sequence. Under this condition the output of each of the two remaining inverters shall be within specification limits.

3.2.1.1.8.1 Overload. With the input voltage set at 24 volts dc, the inverter shall be capable of delivering 150 percent of rated load at minimum power factor for five minutes while providing steady state output voltage in accordance with paragraph 3.2.1.1.5. No degradation in reliability shall be incurred by the inverter as a result of this overload.

3.2.1.1.8.2 Short Circuit Capacity. The inverter shall conform to short circuit capacity requirements of specification MIL-I-27273 except the input shall be 24 volts dc and the inverter shall automatically limit the maximum short circuit output current to 50 ± 20 percent of rated current.

3.2.1.1.8.3 Motor Starting. A combination of three inverters which forms a three-phase output shall be capable of starting a 590 watt minimum, three-phase induction motor with a starting power factor of no less than 0.25; and a 400 percent motor inrush current, and a 0.75 lagging running power factor while carrying a balanced three-phase 1465 va steady-state load.

3.2.1.1.9 Efficiency. With a dc input of 24 to 30 volts and power factor between 0.85 lagging and 1.0 unity, the inverter shall operate at a minimum of 50 percent efficiency from half-rated load to full-rated load.

3.2.1.1.10 Operating Position. The inverter shall be capable of operating in any position.

3.2.1.1.11 Phase Rotation. When the inverter is connected to two other inverters to form a three-phase output the phase rotation shall be A-B-C.

3.2.1.1.12 Phase Displacement. When the inverter is connected to two other inverters to form three-phase output, the displacement angle between adjacent phases shall be 120° plus or minus 1.5 degrees under conditions from no load to full load and power factors from 0.70 lagging to 0.9 leading including unity power factor with either balanced 3-phase load or with phase unbalance as specified in paragraph 3.2.1.1.13. The angle shall be the relative displacement between the zero voltage points on the wave forms of the three phases. A phase-lock signal shall be supplied from one inverter to the next inverter in the following sequence: phase A to phase B, phase B to phase C and phase C to phase A.

3.2.1.1.13 Phase Unbalance. When the inverter is connected with two other inverters to form a three-phase output, the assembly shall be capable of supplying unbalanced loads and meeting performance requirements in accordance with paragraph 3.6.2 of MIL-I-27273 and in addition, shall meet the requirements of paragraphs 3.2.1.1.5, 3.2.1.1.7 and 3.2.1.1.12 with no load on one phase and 750 va on each of the other two phases.

3.2.1.1.14 Output Voltage Modulation. The inverter output voltage modulation shall not exceed one percent while operating with input power conditions in accordance with paragraph 3.1.2.12.1.

3.2.1.1.15 Output Frequency Modulation. The inverter output frequency modulation shall not exceed 0.5 Hz under any load and power factor combination specified herein.

3.2.1.1.16 Waveform. The line-to-crest factor shall not exceed the limits of 1.414 ± 10 percent and the observed change in the crest factor from no load to full load at any input voltage shall not exceed 10 percent. The total harmonic content shall not exceed 4 percent and no individual harmonic shall exceed 3 percent of the fundamental.

3.2.3.1 Redundant Circuit Separation. Redundant circuits within the inverter shall not be routed through the same connector. Also, redundant paths for electrical wiring shall be so located that an event which damages one path will not damage another.

3.2.3.2 Derating. Derating of inverter components shall be utilized to enhance its reliability.

3.2.3.3 Failure Deterrent. The inverter design shall incorporate the following:

- a. Alternate or redundant means of performing a critical function shall be separated physically by the maximum practical distance, or otherwise protected, such that all functional paths will not be lost due to a single event.
- b. Where similar connections are in close proximity the inverter design shall preclude the capability of cross connection.

3.2.3.4 Failure Protection. There shall be no failure in the inverter which can cause the failure of another inverter when operating as a three-phase assembly.

3.2.4 Maintainability

3.2.4.1 Design Allocations. The design shall incorporate the following maintainability allocations:

- a. The inverter shall be designed to allow failed subassemblies to be replaced on the bench in TBS hours or less after failure identification.
- b. The inverter shall be designed to allow bench verification of its electrical functions within TBS minutes using suitable support equipment in the maintenance area.
- c. The inverter shall be capable of being repaired in the shop in accordance with the skill level of TBS.
- d. The inverter removal/installation time shall not exceed TBD minutes.

3.2.4.2 Design Features. The inverter design shall incorporate the following maintainability features.

- a. Subassembly and component installation within the inverter shall facilitate replacement. Where feasible, functional circuit groups shall be packaged as easily removable and replaceable modules.
- b. Arrangement of subassemblies and components within the inverter shall be relative to failure rate and compatible with redundancy requirement.
- c. The inverter shall require no scheduled maintenance, including physical inspection and parts replacement.
- d. The inverter mounting provisions shall permit removal and replacement using standard installation/handling devices.

- e. The inverter shall be designed to preclude the use of special tools and equipment for the on-site maintenance and repair.
- f. The inverter shall not require pre-installation acceptance checkout prior to use.
- g. Where feasible, the inverter test points shall be accessible and clearly marked.
- h. The inverter design shall preclude the requirement for "inspect and repair as necessary" (Iran.)

3.2.5 Environmental Conditions

3.2.5.1 Transportation, Ground Handling and Storage. The inverter shall be capable of meeting the operating performance requirements specified herein after exposure to the following transportation, ground handling and storage conditions. Exposure to transportation, ground handling and storage environments shall be limited to periods when the inverter is non-operating.

a. Temperature (Air)

- 1. Air Transportation Minimum ambient of minus 65F for six hours (35,000 feet). Maximum ambient of plus 115F (ground) for one hour; maximum compartment temperature while on the ground of plus 190F for one hour and plus 150F for six hours per 24-hour period.
- 2. Ground Transportation Minimum ambient of minus 23F, maximum ambient of plus 115F; maximum compartment of plus 190F for one hour and plus 150F for six hours per 24-hour period.
- 3. Storage Plus 25F to plus 105F for a ten-year period.

b. Pressure. Maximum of 15.23 PSIA (sea level), minimum of 3.47 PSIA (35,000 feet).

c. Humidity 15 to 100 percent relative humidity, including conditions wherein condensation takes place in the form of water or frost for up to 30 days.

d. Sand and Dust As encountered in desert and ocean beach areas, equivalent to 100-mesh silica flour with particle velocity up to 500 feet per minute and a particle density of 0.25 grams per cubic foot.

e. Fungus As experienced in tropical climate. Materials shall not be used which will support or be damaged by fungi.

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PREPARED BY G. A. Marshall	CODE IDENT. NO.: 03950	NUMBER NC450-C017
APPROVALS <i>J. R. [unclear] 1/10/74</i> <i>[unclear] 1/10/74</i> <i>[unclear] 1/15/74</i>	SPACE DIVISION NORTH AMERICAN ROCKWELL CORPORATION 12215 LAKENWOOD BOULEVARD • CONWAY, CALIFORNIA 92021	TYPE Procurement
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3. REQUIREMENTS

3.1 Item Definition. The RPC shall function as a remote power control device in one or more direct current (dc) electrical power systems. The RPC shall also provide short circuit/overload protection and a Trip Signal. The RPC function is illustrated by Figure 1.

3.1.1 Item Diagram. Appendices I, II, and III illustrate the envelope and mounting dimensions of the specific RPC Type and Class.

3.1.2 Electrical Power Characteristics. The Electrical Power Characteristics, at the RPC terminals, shall be as specified herein and in accordance with MF0004-002.

3.1.2.1 Interface Diagram. Figure 2 is a schematic block diagram in which an RPC may be used. The diagram illustrates Shuttle Orbiter aerospace vehicle power systems and current flow. The diagram is intended to assist in determination of the sellers' detail requirements and shall not be construed as a constraint on design.

3.1.3 Item Identification. Identification of the RPC shall be as specified in the applicable Appendix.

3.2 Characteristics.

3.2.1 RPC Performance. The RPC shall be capable of operating, as specified, when subjected to one or any combination of the requirements of this specification.

3.2.1.1 Life Requirements. The RPC shall be designed to provide the most cost effective life capability, considering minimum maintenance and/or refurbishment as well as state-of-the-art hardware design. Upon completion of tradeoffs by the seller to establish the optimum relationship between hardware life capability, maintenance, and/or refurbishment, the RPC operating life objective will be changed to become a requirement.

3.2.1.1.1 Operating Life. The RPC shall be capable of performance, as specified herein, for a minimum of 100,000 RPC operating cycles.

3.2.1.1.2 Useful Life. As a design objective, the RPC shall have a minimum useful life of 72,000 hours which is equivalent to 100 Orbital Missions in a ten-year period from date of delivery.

3.2.1.1.3 Shelf Life. As a design objective, the RPC shall be capable of operating in accordance with the requirements specified herein any time within a period of ten years from date of delivery when exposed to the environments of 3.2.5.

3.2.1.2 Electrical Performance.

3.2.1.2.1 Operating Voltages. The RPC Operating Voltages shall be within the limits specified in Table I and as illustrated in Figure 3.

3.2.1.2.1.1 Turn On Voltage. The Turn On Voltage shall be 14.0 volts, direct current (vdc) minimum. Application of the Turn On Voltage shall initiate current flow to the external load.

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3.2.1.2.1.2 Turn Off Voltage. The Turn Off Voltage shall be 9.0 vdc, plus 0.0, minus 2.5 vdc. The Turn Off Voltage is defined as that voltage at which current flow to the external load is turned off.

3.2.1.2.2 Rated Current. The Rated Current shall be as specified in the applicable Appendix. The RPC shall not be adversely effected when subjected to the higher currents specified in the following subparagraphs.

3.2.1.2.2.1 Current Limiting/Overload. The RPC shall limit/inhibit current flow to the external load within the time/current limits specified in Figure 4.

3.2.1.2.2.2 Rupture Current. The RPC shall fail safe when interrupting the Rupture Current specified in the applicable Appendix. Fail safe operation may be provided by a fusible link.

3.2.1.2.2.3 DC Ripple Current. The dc ripple current during Current Limiting/Overload conditions shall not exceed two percent of the input supply current.

3.2.1.2.3 Trip Signal. The Trip Signal (TS) shall be a steady-state discrete plus 28 vdc, in accordance with Table I. The TS vdc shall be referenced to the control circuit minus voltage. Subsequent to Current Limiting/Overload and Rupture "trip" conditions, the RPC shall provide the TS continuously when 14.0 to 34.0 vdc is applied at the RPC control terminals.

3.2.1.2.4 Reset Capability. Subsequent to "trip" or interruption of current flow, the RPC may be reset within 0.020 seconds.

3.2.1.2.5 Response Times. The RPC Response Times shall be within the limits specified in Table I and Figure 3.

3.2.1.2.6 Common Mode Rejection. The RPC shall incorporate Common Mode (CM) Rejection capability to prevent inadvertent operation when a CM plus 10.0 volts peak, dc to 100 KHz, is present at the control terminals.

3.2.1.2.7 Burn-in. The RPC Electrical Performance shall be demonstrated, as a condition of the Buyers' acceptance of each RPC, 5,000 minimum operating cycles at the rated resistive current specified in the applicable Appendix.

3.2.2 RPC Physical Characteristics.

3.2.2.1 Weight. The maximum weight of the RPC shall not exceed that specified in the applicable Appendix.

3.2.2.2 Envelope. The Envelope of the RPC shall conform to the requirements of the applicable Appendix.

3.2.2.2.1 Enclosure. The RPC Enclosure shall be of sufficient mechanical strength to withstand the normal transit, test, storage, and use (requirements of this specification), without causing malfunction or distortion of parts. The RPC Enclosure shall be all-welded construction and shall not electrically interface with the terminals or operating plus and minus voltages.

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3.2.2.2.2 Terminals. The RPC shall incorporate solder Terminals. The RPC Terminals shall conform to the "Terminals" and "Strength of Terminals" requirements specified in MIL-R-6106, Paragraph 3.4.8.2.

3.2.2.2.3 Hermetic Seal. The RPC shall incorporate a Hermetic Seal. The Hermetic Seal is defined as a gas tight fusion of the Enclosure and Terminals, utilizing metals, vitreous materials, or other metal to metal bonding. The Hermetic Seal leakage rate shall not exceed 1×10^{-8} standard cubic centimeters (cc) per second per cubic inch (in³) of the sealed RPC volume. Prior to sealing, the RPC shall be purged of all gasses and then back-filled to a pressure of one atmosphere with dry nitrogen and sufficient quantity of helium for mass spectrometer leak detection.

Each back-fill gas shall have a 98 percent purity and a dew point not above 85 F.

3.2.2.2.3 Mounting. The RPC shall incorporate integral flange type mounting provisions as illustrated in the applicable Appendix. The mounting surface shall conform to the environmental requirements of this specification and WFO004-009. The mounting surface finish shall ensure the Enclosure Bond Resistance does not exceed 0.0025 ohm.

3.2.2.3 Attitude. The RPC shall operate in accordance with the requirements of this specification when mounted in any position.

3.2.3 Reliability.

3.2.3.1 Failure Rate. As a goal, the RPC flight mission reliability, when operated within the requirements of 3.2.1.1.2 and 3.2.5.4 shall be 150,000 hours mean time before failure.

3.2.3.2 Failure Deterrent. The RPC shall be designed such that transient out-of-tolerance conditions or component failures will not cause other component or sub-system failures.

3.2.4 Maintainability. The RPC is designated as a Shop Replaceable Unit (SRU) and shall not require maintenance.

3.2.5 Environments.

3.2.5.1 Transportation (Packaged). The RPC shall be capable of meeting the Electro-magnetic Interference and Electrical Design requirements specified herein after exposure to the following Transportation conditions when packaged in accordance with Section 5.

a. Air

(1) Temperature

Minimum ambient of minus 65 Fahrenheit (F) for six hours at 35,000 feet (ft). Maximum ambient of plus 115 F (ground) for one hour; maximum compartment temperature while on ground of plus 190 F for one hour and plus 190 F for six hours.

(2) Pressure

Maximum of 15.23 pounds (lbs) per square (sq) inch (in) absolute (psia), sea level; minimum of 3.23 psia; 35,000 ft.

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- (1) Humidity 8 to 100 percent relative humidity, including conditions wherein condensation takes place in the form of water or frost.
- b. Ground
- (1) Temperature Minimum ambient of minus 23 F; maximum ambient of plus 115 F, maximum compartment of plus 190 F for one hour and plus 150 F for six hours.
- (2) Pressure Maximum of 15.23 psia (sea level); minimum of 9.76 psia (10,000 ft).
- (3) Humidity 8 to 100 percent relative humidity, including conditions wherein condensation takes place in the form of water or frost.
- c. Shock Capable of withstanding shock, as specified in 5.2.3.
- d. Vibration Capable of withstanding Vibration, Sinusoidal, as specified in 5.2.3.

3.2.5.2 Storage. The RPC shall be capable of meeting the Electromagnetic Interference and Electrical Design requirements specified herein after exposure to the following storage conditions.

- a. Sheltered Environment
(packaged or unpackaged)
- (1) Temperature Minus 23 F to plus 150 F.
- (2) Humidity 8 to 100 percent relative humidity, including conditions wherein condensation takes place in the form of water or frost.
- (3) Pressure Maximum of 15.23 psia (sea level); minimum of 9.75 psia (10,000 ft).
- (4) Ozone Three years exposure including 72 hours at 0.50 parts per million (ppm), three months at 0.25 ppm, and remainder at 0.05 ppm.
- (5) Fungus As specified in NC999-0096.
- (6) Sand and Dust Suspended dust (as distinguished from blowing sand) is uniformly distributed in the protected atmosphere, with particle sizes ranging from the lower limit of sand (0.08 millimeter (mm)) down to below 0.0001 mm. Ninety percent of the dust particles will be between 0.0001 mm and 0.002 mm in diameter.
- b. Unsheltered Environment
(packaged)
- (1) Temperature Minus 23 F to plus 115 F.

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- (2) **Pressure** Maximum of 15.23 psia (sea level); minimum of 9.76 psia (10,000 ft).
- (3) **Humidity** 8 to 100 percent relative humidity, including conditions wherein condensation takes place in the form of water or frost.
- (4) **Sand and Dust** As encountered in desert and ocean beach areas, equivalent to 140-mesh silica flour with particle velocity up to 500 feet per minute and a particle density of 0.25 grams per cubic foot.
- (5) **Salt Fog** Salt atmosphere as encountered in coastal areas, the effect of which is simulated by exposure to a 1.0 percent salt solution by weight for 30 days.
- (6) **Rain** Maximum of 19 inches in 24-hour period including short period extremes of four inches for one hour.
- (7) **Ozone** Three years exposure including 72 hours at 0.50 ppm, three months at 0.25 ppm, and remainder at 0.05 ppm.
- (8) **Solar Radiation** Solar radiation of 363 British Thermal Unit (BTU)/ft²/hour for six hours per day for two weeks.
- (9) **Fungus** As specified in MC999-0096.

3.2.5.3 Ground Handling Loads (Unpackaged). The RPC shall be capable of meeting the operating performance requirements specified herein after exposure to the following ground handling conditions when unpackaged.

- a. Shock, Bench Handling As specified in MIL-STD-810, Method 514.7, Procedure V
- b. Shock As specified in MIL-STD-840, Method 516.1, Procedure I

3.2.5.4 Flight Environments. The RPC shall be capable of operating as specified herein during and after exposure to any combination of the following environmental extremes:

- a. Pressure 16.0 psia, maximum to 1×10^{-10} mm of Mercury (mmHg or torr).
- b. Atmosphere Circulating Nitrogen/Oxygen at maximum pressure (Oxygen = 3.45 psia, maximum; 2.75 psia, minimum) to nominal at 3.78 psia (35,000 ft).
- c. Temperature Minus 65 F to plus 149 F in specified atmosphere; to plus 130 F at 1×10^{-10} mmHg (when mounted on coldplate).
- d. Humidity Dew point plus 37 F to plus 61 F; salinity one percent by weight; 0 percent relative humidity, including conditions wherein condensation takes place in the form of water or frost for up to 30 days.

- e. Lightning The RPC shall not be adversely affected when exposed to cable core transients at each RPC Terminal. The transient shall be a composite of two triangular wave forms, each having a total energy of 10 millijoules. The first one shall crest at two microseconds after initiation with a total duration of 100 microseconds. The second one shall crest at 300 microseconds after initiation with a total duration of 600 microseconds.
- f. Vibration Random Acceleration spectral density (g^2/Hz) increasing at the rate of plus six decibels (db) per octave (oct) from 25 to 60 Hertz (Hz), constant at $0.2 g^2/Hz$ from 60 to 400 Hz, decreasing at the rate of minus 3 db/oct from 400 to 2,000 Hz, in each axis.
- g. Acceleration Plus and minus 5.0 g, 3 minutes in each direction of each of the three mutual axes.
- h. Shock
- (1) Non-operating Peak acceleration (sawtooth pulses), 40.0 g, 0.011 second minimum in each direction of the three mutual axes.
- (2) Operating Peak acceleration (rectangular pulses), one time, 1.5 g, 0.260 second minimum, in each direction of each of the three mutual axes.

3.2.5.5 Checkout Environments (Installed). The RPC shall be capable of operating as specified herein during and after exposure to environments specified as follows:

- a. Pressure 18.0 psia, maximum, to 14.5 psia, minimum.
- b. Atmosphere Standard; circulating, at the pressure extremes specified herein.
- c. Temperature (Ambient) Minus 23 F to plus 135 F.
- d. Humidity 8 to 100 percent relative humidity, including conditions wherein condensation takes place in the form of water or frost for up to 30 days.
- e. Salt Fog Salt atmosphere as encountered in coastal areas, the effect of which is simulated by exposure to a 1.0 percent salt solution by weight for 30 days.

3.2.6 Transportability. The RPC shall be designed so as to be capable of being handled and transported to using facilities with no damage or degradation, utilizing available methods of transport with the RPC prepared for shipment in accordance with Section 5 requirements.

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3.3 Design and Construction. The RPC shall be of compact design and of sufficiently rugged construction to withstand all stresses and operational conditions specified herein.

3.3.1 Materials, Parts, and Processes.

3.3.1.1 Materials and Processes. Materials and Processes for the RPC shall be in accordance with NC999-0096, to the extent specified in the requirements table of the purchase order.

3.3.1.2 Parts Standardization. Parts utilization shall be based on selection of qualified parts, proper derating, application, and minimizing the number of part types. Parts utilized shall conform to MFC004-400.

3.3.1.3 Parts Attachment. Parts within the RPC Enclosure shall be secured (bonded) to the RPC assembly by mechanical means, except attachment may be effected utilizing approved fusible materials with melting points equal to or greater than 375 F, or structural adhesive bonding in accordance with NC999-0096.

3.3.1.4 Cleanliness. The internal surfaces of the RPC and external surfaces of integral RPC parts within the RPC shall be cleaned to the cleanliness requirements of NC999-0096.

3.3.2 Selection of Specifications and Standards. Specifications and Standards for use in the design and construction of the RPC, other than those specified herein, shall be selected in the order of precedence specified in MIL-STD-143, except that NASA documents, when suitable for the purpose shall take precedence.

3.3.3 Electromagnetic Interference and Electrical Design.

3.3.3.1 Electromagnetic Interference. The RPC shall be designed in accordance with MFC004-002, Class 1, Subclass B.

3.3.3.2 Electrical Design. The RPC Electrical Design shall conform to the requirements specified in MFC004-002, except as follows.

3.3.3.2.1 Power. The power consumed by the RPC shall be the minimum required, consistent with the requirements of the applicable Appendix.

3.3.3.2.2 Voltage Drop. The Voltage Drop shall not exceed 0.5 vdc for current values from zero to 100 percent of the rated resistive current specified in the applicable Appendix.

3.3.3.2.3 Isolation.

3.3.3.2.3.1 Insulation Resistance. The Insulation Resistance, measured at a potential of 500 vdc (minimum) shall be 1,000 megohms (minimum) when tested as specified in 4.2.2.3.1.

3.3.3.2.3.2 Dielectric Strength. The RPC shall be capable of withstanding 1,250 volts rms alternating current (ac), 60 Hz minimum potential, applied between the RPC Terminals and the Enclosure as specified in 4.2.2.3.1, for a period of 60 seconds minimum. During each test, the leakage current shall not exceed 1.0 milliampere for 10 milliseconds. Subsequent to Acceptance Tests, the test potential shall be 1,250 vdc rms, 60 Hz minimum.

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3.3.3.2.3.3 Impedance. The Impedance of the RPC, between the plus control terminal and the RPC Enclosure and all other Terminals, shall not be less than 2,100 ohms plus or minus 100 ohms.

3.3.3.2.3.4 Leakage Current. The RPC Leakage Current with plus 34.0 vdc applied between the load terminals shall not exceed the maximum specified in the applicable Appendix.

3.3.4 Identification and Marking.

3.3.4.1 Identification of Parts. Each part fabricated shall be identified with a part number. The same specification or part number shall be used to identify all like materials, processes, and parts. Seller shall assign a new part number to the part when authorized changes make the superseded part not interchangeable with respect to interface, reliability, safety, logistics, traceability or performance. For traceable items the part identification shall additionally include the manufacturer's identification code in accordance with ECD Handbook H4-1, and be lot/member numbered or serial numbered when required.

3.3.4.2 Identification of All Development/Qualification Test Specimens. Test specimens shall be permanently and obviously identified prior to testing with the words "EX. TEST ONLY" in addition to the identification required by the Drawing/Specification to preclude their use on production items. The letters shall be indelible and provide a distinctive and vivid contrast with the color of the specimen. The lettering size and identification location shall be clearly visible to casual observation. Materials used for the identification shall be compatible with the test specimen and its operating environment. When the size or configuration of the test specimen is such, the identification cannot appear on the specimen, other suitable means such as attached metal tags shall be used.

3.3.4.5 Nameplates. Nameplates shall be marked in accordance with MIL-STD-130 and shall include (as applicable) item name; buyer's control number; Federal Stock Number/North Atlantic Treaty Organization (FSC/NATO); manufacturer; date of manufacture; and manufacturer's serial number, part number, lot number, and code identification number. Abbreviations, in accordance with MIL-STD-12, may be used.

3.3.4.4 Terminal Identification/Wiring Diagram. The RPC shall have permanently affixed to the enclosure an indelible and legible Terminal Identification/Wiring Diagram, that identifies each RPC Terminal function as specified herein, and each RPC Terminal location.

3.3.5 Traceability. Traceability shall be provided by assigning a traceability identification to each RPC identified in 3.1.3. Such identification shall provide the means of correlating each to its historical records. Conversely, the records must be traceable to each RPC.

3.3.5.1 Traceability Classification. For lower tier items, traceability classifications shall be established by classifying raw material, part, assembly, or end item for determining the marking and traceability records required (or excluded for exempt items) for that item. Seller/subordinate supplier engineering documentation (e.g., drawings and specifications) shall specify traceability or exemption for items in accordance with the applicable classifications defined in 6.1.

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3.3.5.2 Traceability Identification. Each item identified as traceable (refer to 6.1 for Ts, Tl, T_v) shall have a traceability identifier consisting of the manufacturer's code identification number as listed in ECD Handbook H4-1 and a serial, lot, or member number. The serial, lot, or member number shall be assigned by the manufacturer and shall not exceed ten characters (alphas, numerics, dashes, etc.).

3.3.6 Interchangeability. The RPC and integral parts of the RPC, identified in 3.1.3 shall be interchangeable in accordance with the definition of "Interchangeable Items" specified in MIL-STD-283. Interchangeability shall be provided at the attachments of these items to their next assembly.

3.3.6.1 Design Tolerances. Provisions shall be made for Design Tolerances such that each RPC having the dimensions and characteristics permitted by this specification or the applicable Appendix are interchangeable without selection or departure from the RPC performance specified herein.

3.3.6.2 Use of Standard Parts. When standard parts specified in 3.3.1.2 are not available and permission is granted for use of a non-standard part due to unavailability of the standard part, the equipment shall be designed so that the nonstandard part can be replaced by the standard part. Appropriate space, mounting holes, and other necessary provisions shall be provided for this purpose.

3.3.7 Safety. The RPC design and operation shall not impair crew or vehicle safety when operated at the temperature and pressure extremes specified in this specification.

3.3.8 Human Performance/Human Engineering. The RPC design shall be homogeneous with the capabilities and limitations of human operators whenever a man-machine interface exists, including torques, forces, and other characteristics relative to service use and work stations. The principal design guide for the man-machine interface shall be MIL-STD-1472.

Figure 1, Change as Follows: (Continued)

Response Times: (second)

Turn-On Minimum, is: [0.0002]

was: [X]

Turn-Off Minimum, is: [0.001]

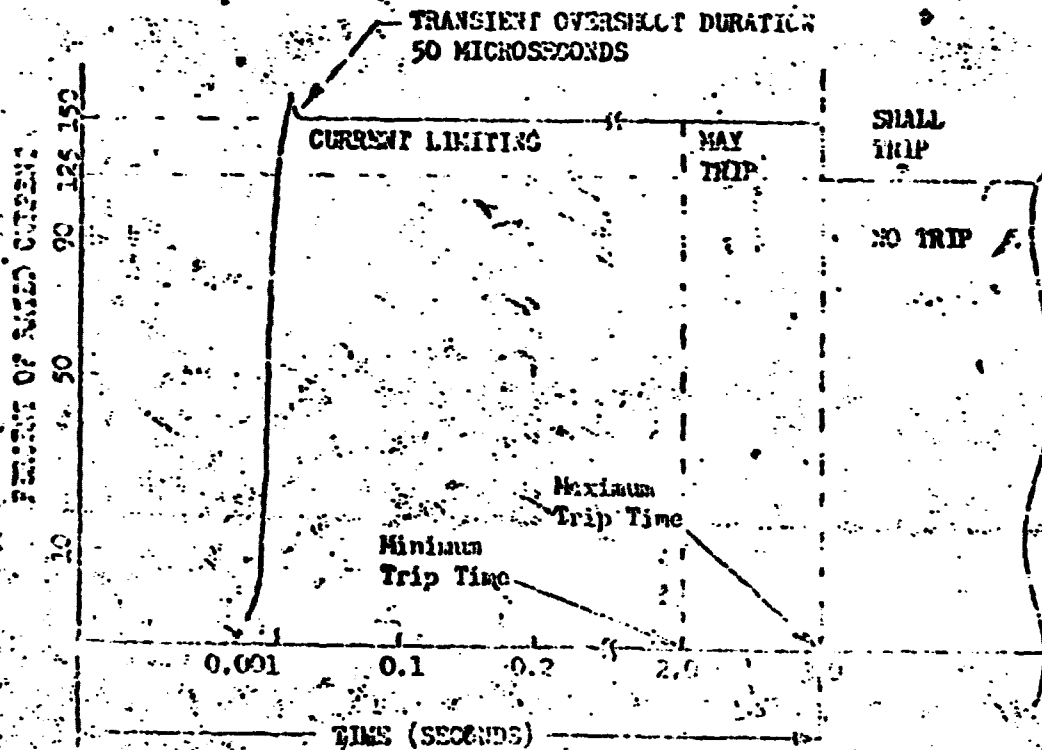
was: [X]

Figure 1, Trip Signal (Output)

Figure 2 RPC Power System Interface.

Figure 3 Operating Characteristics.

Figure 4, Replace With:



(Rev) 321213 Current Limiting / Overload

The RPC shall limit current flow to the external load at 150% of rated current for a duration of 2 sec. (min). 2 sec. (max).

Time shall not be negotiated. If the rated current is exceeded, the RPC shall trip.

RCCB

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3. REQUIREMENTS

3.1 Item Definition. RCCB's built to this specification shall be capable of performing the following functions under all the environmental conditions and other requirements imposed by this specification:

- a. Carry current in accordance with its rating as specified in Table I.
- b. Automatically sense an overload and interrupt (trip) the circuit without damage under the conditions specified.
- c. Provide the capability for closing and opening the circuit from a remote location during all conditions except overload.

This capability shall provide for closing (resetting) the RCCB following an automatic trip but only after the overload condition has been corrected. It shall not be possible to close and maintain the RCCB contacts closed while an overload condition is still present.

3.1.1 Item Diagram. Figure 1 is the block diagram for the RCCB external connections.

3.1.2 Interface Definition.

3.1.2.1 Electrical Power Characteristics. The electrical power characteristics at the RCCB interface shall be in accordance with MF0004-002.

3.1.2.2 Control Input. The RCCB shall be actuated (set) by application of a 24.0-30.0 Vdc signal applied through a 1300 ± 65 ohm, 1 watt resistance at the control input terminal as shown in Figure 1. Removal of the control input voltage shall open the RCCB.

3.1.2.3 Backup Power. The RCCB shall be capable of operation using 28 Vdc backup power applied as shown in Figure 1 at times when line voltage is not available. There shall be no connection within the RCCB to allow the backup voltage to energize the main bus or the load, nor for the main bus to energize the backup voltage bus.

3.1.2.4 Electrical Connections. Connections to external circuits shall be as shown in Figure 1.

3.1.2.4.1 Line and Load Terminals. Terminal studs shall be used for main line and load connections as shown in Figure 2.

3.1.2.4.2 Control Terminals. The control terminals shall be contained in an integrated wire-termination module in accordance with MS27726 to accept pin contact MS39029/01-16-20 per MIL-C-39029/1 and as shown in Figure 2.

3.1.3 Item Identification. The identification of the RCCB shall be as follows:

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Table I. Performance Requirements

Dash Number	Rated Current	Max Voltage Drop at 70°F (Rated Current)	Trip Time 30° to 140°F (Seconds)							
			Percent Rated Current							
			200		400		600		1000	
			min	max	min	max	min	max	min	max
-1015	15	0.25	13	45	1.7	7	0.7	3.4	0.35	1.2
-1020	20	0.25	14	47	2.2	8	0.9	3.5	0.35	1.2
-1025	25	0.25	15	49	2.5	9	1.0	3.7	0.35	1.3
-1035	35	0.25	16	52	2.8	10	1.2	4.1	0.4	1.4
-1050	50	0.25	16	56	2.9	11	1.3	4.6	0.4	1.6
-1075	75	0.25	16	61	3.3	12	1.4	5.2	0.4	1.8
-1100	100	0.25	17	63	3.5	13	1.4	5.4	0.4	1.9

Ultimate Trip	Percent Rated Current		
	30°	70°	140°F
Minimum- No Trip 1 hour	115	115	105
Maximum- Trip 1 Hour Max	145	140	140 ^W

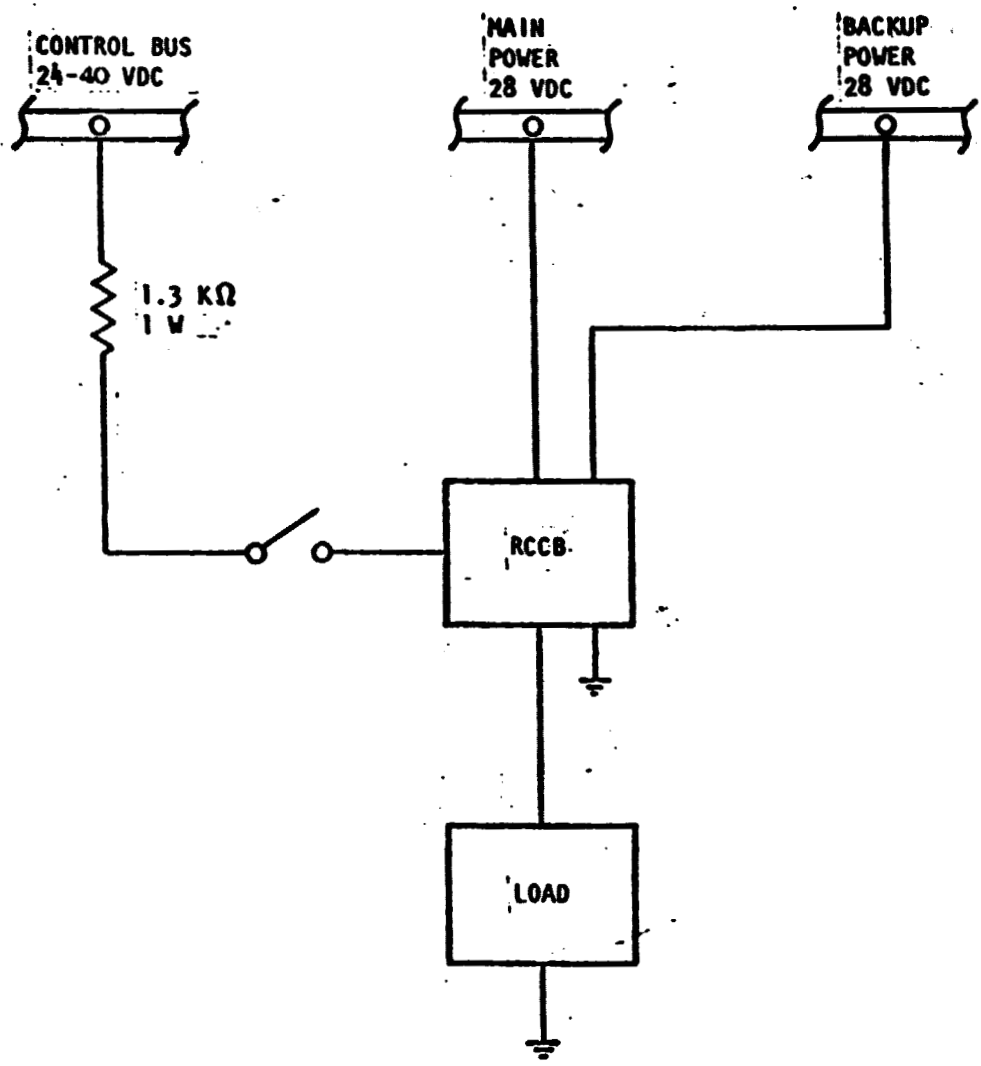
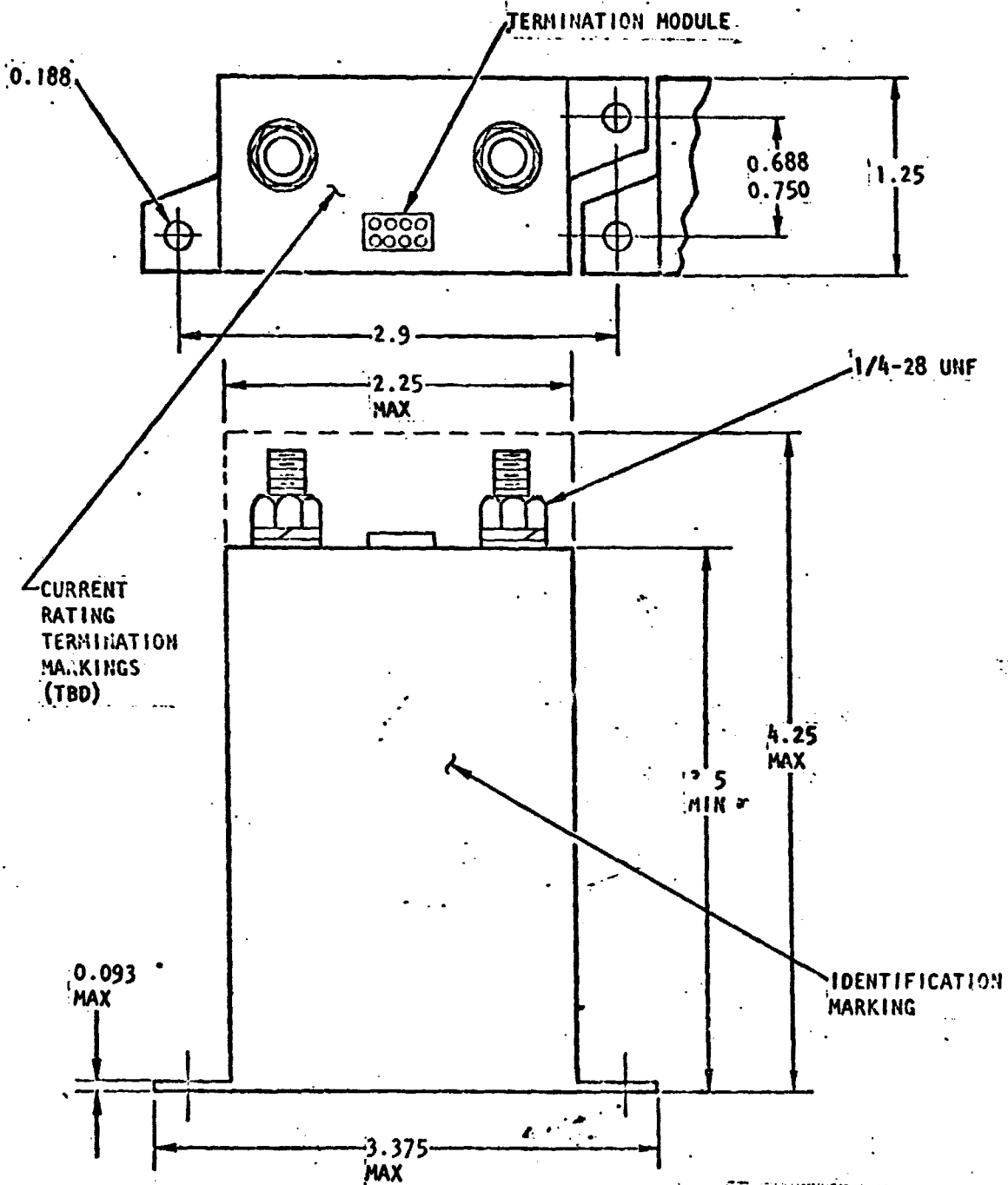


Figure 1. Block Diagram

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NOTE:
DIMENSIONS IN INCHES
TOLERANCE: ± 0.005

Figure 2. Configuration

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Nomenclature & Mfr Code Ident. No.	Buyer Control No.	Seller Part No.	Traceability Classification	LRU/ SRU
RCCB ()	MC454-0027-1015	TBS	Serial	SRU
	↓	↓	↓	↓
	1020			
	1025			
	1035			
	1050			
	1075			
RCCB ()	MC454-0027-1100	TBS	Serial	SRU

3.2 Characteristics.

3.2.1 Performance.

3.2.1.1 Life Requirements. The RCCB shall be designed to provide the most cost effective life capability, considering state-of-the-art hardware design. Upon completion of tradeoffs by the Seller to establish the optimum relationship between hardware life capability and cost, the following life objectives will be changed to requirements.

3.2.1.1.1 Operating Life. As a design objective, the RCCB shall be capable of being remotely cycled "ON" and "OFF" for a minimum of 50,000 cycles at rated current. In addition, the RCCB shall be capable of withstanding 100 cycles of automatic trip at 200 percent rated current with remote reset.

3.2.1.1.2 Useful Life. As a design objective, the RCCB shall have a minimum useful life of 30,000 hours, which are equivalent to 100 orbital missions in a 10 year period from date of delivery.

3.2.1.1.3 Shelf Life. As a design objective, the RCCB shall be capable of operating in accordance with the requirements specified herein any time within a period of 10 years from date of delivery when exposed to the applicable environments of 3.2.3.

3.2.1.2 Electrical Characteristics.

3.2.1.2.1 Ampere Ratings. Ampere ratings shall be as specified in Table I.

3.2.1.2.2 Voltage Drop. With rated voltage and current applied the RCCB voltage drop from line to load terminals shall not exceed the value specified in Table I.

3.2.1.2.3 Interrupting Capacity. The RCCB shall be capable of interrupting currents as specified in Table II when tested in accordance with 4.2.4.1.16.

3.2.1.2.4 Power Requirements. The RCCB shall require a maximum current of 3.5 amperes at 32 Vdc to operate the main contacts and a maximum control current of 10 milliamperes at 40 Vdc.

3.2.1.2.5 Insulation Resistance. The insulation resistance between mutually insulated parts and mounting surfaces shall not be less than 100 megohms when measured with a test potential of 500 volts dc at ambient conditions.

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3.2.1.2.6 Dielectric Withstanding Voltage. The RCCB shall withstand 1250 volts ac (rms) at 60 Hz for a period of 60 seconds and shall show no evidence of breakdown, flashover, or current flow in excess of 100 microamperes.

- a. Between line and load terminals with the RCCB in the OFF or TRIPPED position.
- b. Between terminals and parts normally grounded (such as frame, shell, mounting plate, etc.) with the main contacts in both CLOSED and OFF (or TRIPPED) positions.

3.2.1.3 Operation.

3.2.1.3.1 Control. With power applied to the line or backup power terminals, the RCCB shall be capable of being closed (set) by application of 28Vdc to the control input, and opened when the 28-Vdc signal is removed. If power is removed from both the line and backup power terminals, the RCCB contacts shall remain in the same state as they were before the power was removed. If power is again applied to the line or backup power terminals, the RCCB shall assume the state dictated by the status of the control input. With minimum voltage applied to the control input, the RCCB shall operate in a maximum time of 30 milliseconds.

3.2.1.3.2 Trip Performance. The RCCB shall interrupt the circuit (trip) within the limits specified in Table I.

3.2.1.3.3 Trip Mechanism. When an overload condition occurs, the RCCB trip mechanism shall open the main contacts. The trip mechanism shall not be capable of closing (re-setting) the main contacts until the remote control switch is moved to "OFF" and then to "ON".

3.2.1.3.4 Trip Free Operation. The RCCB shall be designed so that the circuit cannot be maintained closed when the contacts are carrying overload currents that would normally trip the RCCB to the open position.

3.2.2 Physical Characteristics.

3.2.2.1 Envelope. The envelope of the RCCB shall not exceed the dimensions shown in Figure 2.

Table II. Interrupting Capacity

Fault Description *	System Voltage	Open Circuit Voltage	Fault Current Amperes	Recovery Open Circuit Voltage Transient
1 OCO 1 CO Sea Level	28 Vdc	30 ± 2 Vdc	6000 amperes in 0.01 to 0.03 seconds after fault initiation	28 V within 0.002 seconds 50 V maximum
1 OCO 1 CO 1 X 10 ⁻⁶ TORR				

*OCO - Test in which the circuit breaker is closed before initiation of the fault
CO - Test in which the circuit breaker is closed to complete the fault

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3.2.2.2 Mounting. The mounting provisions of the RCCB shall be as shown in Figure 2.

3.2.2.3 Weight. The weight of the RCCB shall not exceed TBS pounds including terminal hardware.

3.2.2.4 Surface Wear. Interacting surfaces in the RCCB shall be sufficiently smooth and wear resistant such that particle generation will not preclude the normal functioning of the item as specified herein.

3.2.2.5 Terminal Nut Torque. The RCCB external terminal fastener torque shall be TBD.

3.2.2.6 Orientation. The RCCB shall be capable of operating in any position and at zero gravity where convection cooling is precluded.

3.2.3 Environments.

3.2.3.1 Operational. The RCCB shall be capable of meeting the operating performance requirements specified herein during and after exposure to any feasible combination of the following conditions:

- | | | | | | | | | | |
|---|---|-----------|----------------|-----------|--------------|------------|----------------|-------------|--------------|
| a. Temperature | Minimum: Plus 30 F
Maximum: Plus 140 F | | | | | | | | |
| b. Pressure | Minimum: 10^{-10} Torr
Maximum: 18.0 psia | | | | | | | | |
| c. Humidity | Minimum: 0 percent, relative
Maximum: 100 percent, relative | | | | | | | | |
| d. Salt Fog | Exposure to one percent salt solution by weight. | | | | | | | | |
| e. Lightning | In accordance with MF0004-002. | | | | | | | | |
| f. Random Vibration | | | | | | | | | |
| (a) Liftoff and Boost Vibration Spectra | <table border="0"> <tr> <td>10 -25 Hz</td> <td>0.02 g^2/Hz</td> </tr> <tr> <td>25 -80 Hz</td> <td>+6 dB/octave</td> </tr> <tr> <td>80 -400 Hz</td> <td>0.2 g^2/Hz</td> </tr> <tr> <td>400-2000 Hz</td> <td>-3 dB/octave</td> </tr> </table> Time duration - 1 hour per axis | 10 -25 Hz | 0.02 g^2/Hz | 25 -80 Hz | +6 dB/octave | 80 -400 Hz | 0.2 g^2/Hz | 400-2000 Hz | -3 dB/octave |
| 10 -25 Hz | 0.02 g^2/Hz | | | | | | | | |
| 25 -80 Hz | +6 dB/octave | | | | | | | | |
| 80 -400 Hz | 0.2 g^2/Hz | | | | | | | | |
| 400-2000 Hz | -3 dB/octave | | | | | | | | |
| (b) Main Engine Vibration Spectra | <table border="0"> <tr> <td>10 -30 Hz</td> <td>0.012 g^2/Hz</td> </tr> <tr> <td>30 -60 Hz</td> <td>-3 dB/octave</td> </tr> <tr> <td>60-2000 Hz</td> <td>0.006 g^2/Hz</td> </tr> </table> Time Duration - 12.5 hours per axis | 10 -30 Hz | 0.012 g^2/Hz | 30 -60 Hz | -3 dB/octave | 60-2000 Hz | 0.006 g^2/Hz | | |
| 10 -30 Hz | 0.012 g^2/Hz | | | | | | | | |
| 30 -60 Hz | -3 dB/octave | | | | | | | | |
| 60-2000 Hz | 0.006 g^2/Hz | | | | | | | | |
| g. Acceleration | Plus and minus 5-g's in all axes | | | | | | | | |
| h. Shock | Maintain structural integrity when subjected to a terminal peak sawtooth shock of 11 milliseconds duration and 40 g acceleration in any direction. | | | | | | | | |
| i. Explosive Atmosphere | In accordance with MIL-STD-810, Method 511, Procedure I, using butane for fuel. | | | | | | | | |

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3.2.3.2 Non-Operational. The RCCB shall be capable of meeting the operating performance requirements specified herein after exposure to the following transportation and storage conditions when packaged in accordance with Section 5.

- a. Temperature (Packaged) Minimum: Minus 65 F for six hours.
Maximum: Plus 115 F for one hour, plus 150 F for six hours and plus 190 for one hour.
- b. Pressure Minimum: 10^{-10} Torr
Maximum: 18.00 psia
- c. Sand and Dust (Packaged)
- (1) As encountered in desert and ocean beach areas, equivalent to 140-mesh silica flour with particle velocity up to 500 feet per minute and a particle density of 0.25 grams per cubic foot.
 - (2) Suspended dust (as distinguished from blowing sand) is uniformly distributed in the protected atmosphere, with particle sizes ranging from the lower limit of sand (0.08 millimeter (MM)) down to below 0.0001 mm (0.01 micron). Ninety percent of the dust particles will be between 0.0001 mm and 0.002 mm in diameter.
- d. Solar Radiation (Packaged) 363 BTU/ft²/hr for 6 hours per day for two weeks.
- e. Rain (Packaged only) Maximum of 19 inches for a 24 hour period, including short period extremes of four inches per hour.
- f. Hail (packaged only) Diameter of 0.30 inches with fall velocity of 66 ft/sec.
- g. Snow (packaged only) 10.2 lb/ft²
- h. Shock (Bench Handling) As specified in MIL-STD-810 Method 516.1, Procedure V.
- i. Ozone Three years exposure, including 72 hours at 6.0 parts per hundred million (ppm) and remainder at 3.0 ppm.
- j. Fungus As specified in NC999-0096
- k. Vibration & Shock (Packaged) In accordance with 5.2.3

3.3 Design and Construction.

3.3.1 Materials, Processes, and Parts.

3.3.1.1 Materials and Processes. Materials and Processes for the RCCB shall be in accordance with NC999-0096 to the extent specified in the requirements table of the purchase order.

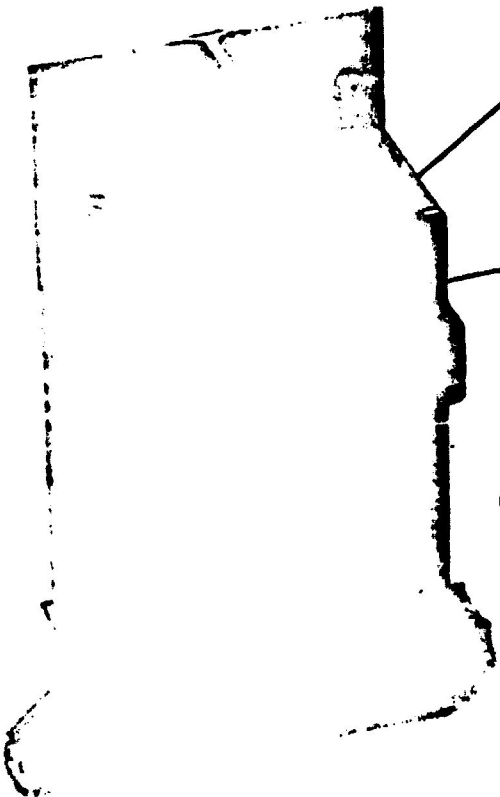
NEW FROM CUTLER-HAMMER

Remote load controllers carry heavy loads lightly.

New Remote Control Circuit Breakers (RCCB) combine the functions of a relay and a circuit breaker in one compact package. Heavyweight performers—they mount near the load or power source and are controlled and/or monitored from remote locations with 22 gauge control wiring. You save weight, simplify control circuitry and eliminate heavy cable runs—for lightweight results.

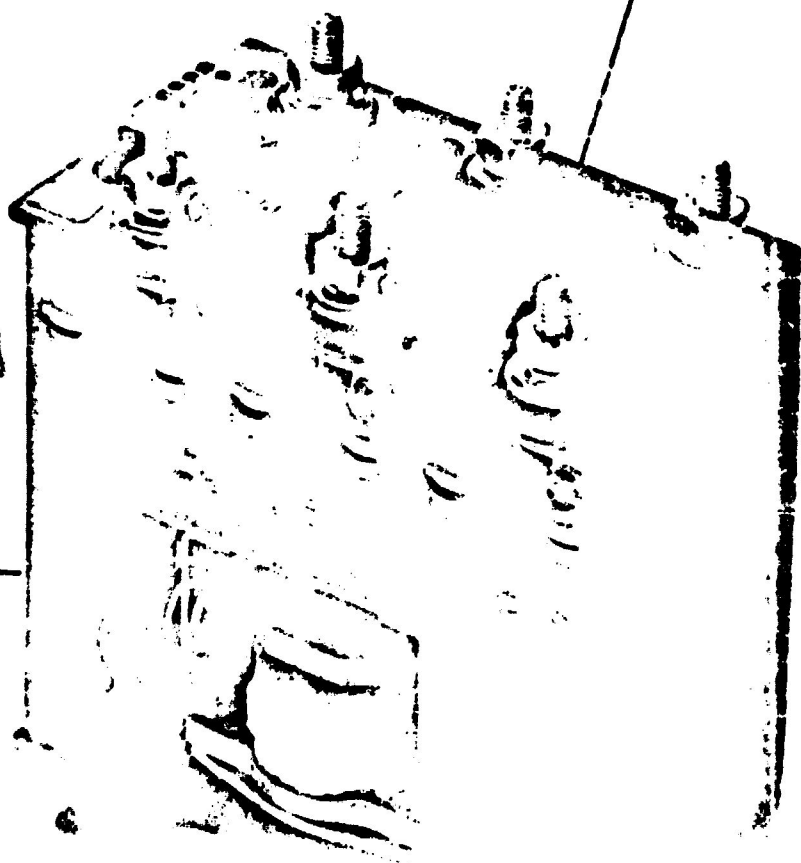
Available in single- and three-pole configurations with auxiliary contacts, RCCBs also feature magnetic latching which assures low power consumption and visual "ON-OFF" indication of contact state. Both types meet rigid MIL-C specification requirements for 28V D-c and 115/200V A-c, 400 Hz. service.

Single-pole ratings range from 5 to 100 amps, measure approximately 3" x 1" x 4" and weigh in at 12.25 ounces maximum.



The three-pole unit is available in 10, 20 and 30 amp ratings, measures 4" x 3" x 4" and weighs 33.6 ounces maximum.

If weight and power consumption economy aren't enough, with minor modifications, RCCBs offer still more. Under- and over-voltage sensing. Phase and frequency sensing. Interface capabilities with multiplexing systems. You name it—RCCBs carry heavy loads—lightly.



To lift more weight off your shoulders, write for the RCCB Data Kit or call your Cutler-Hammer Sales Office.

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RPC

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APPENDIX 7.6

THEORETICAL BASIS FOR SYSTID

7.6.0

APPENDIX 7.6

THEORETICAL BASIS FOR SYSTID

THEORETICAL INTRODUCTION

Direct representation of systems on the digital computer by sample data simulation is a powerful systems analysis technique. Such simulation requires transformation by the computer of continuous system input functions in a manner which characterizes system behavior. The digital computation/process by which this transformation is accomplished is known as a digital filter. This is an algorithm by which sample values of a continuous input function are transformed into sample values of the continuous output function which would result from operating on the input with a given continuous transfer characteristic. The central problem in sample data simulation is obtaining the digital filter algorithm which effects this transformation in the most accurate and efficient manner.

Digital filters may be classified into two major categories as recursive or non-recursive. Non-recursive digital filter outputs depend only on present and previous input samples; recursive filter outputs depend on previous output values as well. The design methods for these two filter types are distinctly different as are their properties. The non-recursive filter has finite memory and excellent phase response characteristics but may require a large number of terms to obtain sharp cutoff properties. The recursive filter has infinite memory but rather poor characteristics. Recursive filters have fewer terms and lend themselves more efficiently to applications requiring sharp cutoff properties. The recursive filter is the digital counterpart of the linear lumped parameter continuous filter. For these reasons, recursive filters are of greater interest in systems analysis by sample data simulation and will be summarized briefly.

If it is assumed that the linear system for which a digital approximation is sought has a transfer characteristic of the form

$$H(s) = \frac{\sum_{m=0}^M C_m s^m}{\sum_{n=0}^N d_n s^n} \quad (7.6-1)$$

where $s = j\omega$, then the corresponding digital transfer characteristic has the form

$$H^*(z) = \frac{\sum_{j=0}^{N-1} a_j z^{-j}}{1 + \sum_{j=1}^N b_j z^{-j}} \quad (7.6-2)$$

where z^{-1} is the unit delay operator. It is assumed that the continuous function $H(s)$ is known or can be determined by established design procedures. The digital filter design problem is thus reduced to determining the coefficients a_j and b_j in $H^*(z)$ such that the continuous filter characteristic $H(s)$ is best approximated for a given number of terms.

One digital filter design technique is based on the standard z -transform, defined so that the impulse response of the digital filter is identical to the sampled impulse response of the corresponding continuous filter. The standard z -transform of $H(s)$ is given by

$$H^*(s) = \sum_{m=-\infty}^{\infty} H(s + jm\omega_s) \quad (7.6-3)$$

or in terms of the filter impulse response $h(t)$:

$$H^*(z) = T \sum_{l=0}^{\infty} h(lT)z^{-l} \quad (7.6-4)$$

where

$$s = \sigma + j\omega$$

$$H(s) = \text{Laplace transform of } h(t)$$

$$\omega_s = \frac{2\pi}{T}, \text{ radian sampling frequency}$$

$$H^*(s) = \text{Laplace transform of sampled filter impulse response}$$

$$z^{-1} = e^{-sT}, \text{ unit delay operator}$$

$$H(z) = H^*(s) \Big|_{s = \ln(z)/T}, \text{ z-transform of } h(t)$$

For s greater than some critical frequency ω_c , $H(s)$ is assumed to have the form

$$H(s) \Big|_{s > j\omega_c} = K/s^n \quad (7.6-5)$$

where $n > 0$ and K is a constant.

Equations 7.6-3 and 7.6-4 are the digital filter transfer functions which approximate that of the continuous filter.

The disagreement between the digital filter characteristics provided by the standard z -transform and the continuous filter characteristic in the baseband ($-\omega_s/2 \leq \omega \leq \omega_s/2$) is known as frequency aliasing error and results from terms of the form $H(s + jm\omega_s)$, $m \neq 0$. This disagreement is present whenever the continuous filter characteristic is not bandlimited to the baseband. Unfortunately this is the case for most lumped parameter systems, for which $H(s)$ is a rational function of s . Thus, for physical systems of

interest, the standard z-transform yields $H^*(s) = H(s)$ in the baseband and aliasing error is present to some degree.

For higher order continuous filter transfer functions (n in Equation 7.6-5 is large) having a critical frequency ω_c much less than the sample frequency ω_s , aliasing error is sufficiently small that the standard z-transform yields useful results. In many practical situations, however, neither of these conditions are met. In these cases, the standard z-transform results in prohibitive aliasing errors in the digital filter frequency characteristic.

Frequency aliasing error may be avoided if digital filters are designed by means of an artifice known as the bi-linear z-transform. The bi-linear z-transform maps the entire complex s plane into an s_1 plane bounded by the lines $s_1 = j\omega_s/2$ and $s_1 = -j\omega_s/2$. The bi-linear z-transform is defined by

$$s = \frac{2}{T} \tanh \frac{s_1 T}{2} \quad (7.6-6)$$

where $s_1 = j\omega_s/2$ and T is the sample interval. This becomes upon substitution of the unit delay operator $z^{-1} = e^{-s_1 T}$,

$$s = \frac{2}{T} \left(\frac{1 - z^{-1}}{1 + z^{-1}} \right) \quad (7.6-7)$$

The digital filter transfer function, $H^*(z)$ is determined by substituting the bi-linear z-transform into the continuous filter transfer function $H(s)$.

$$H^*(z) = H(s) \Big|_{s = \frac{2}{T} \left(\frac{1 - z^{-1}}{1 + z^{-1}} \right)} \quad (7.6-8)$$

One aspect of the digital filter so obtained is that a non-linear warping is imparted to its frequency scale in accord with the transformation

$$\frac{\omega T}{2} = \tan \frac{\omega_1 T}{2} \quad (7.6-9)$$

This transformation is depicted in Figure 7.6-1 which plots normalized warped frequency ω , versus normalized unwarped frequency ω_1 . Frequency warping is not a significant constraint on the versatility of the bi-linear z-transform. The warping may be arbitrarily reduced by making the sample frequency ω_s high compared to the critical frequency ω_c of the continuous filter. Furthermore, frequency warping may be compensated for by prewarping the critical frequencies of the continuous filter so that transformed frequencies will be shifted back to the desired ones. Because it obviates inaccuracies due to aliasing error, the bi-linear z-transform is

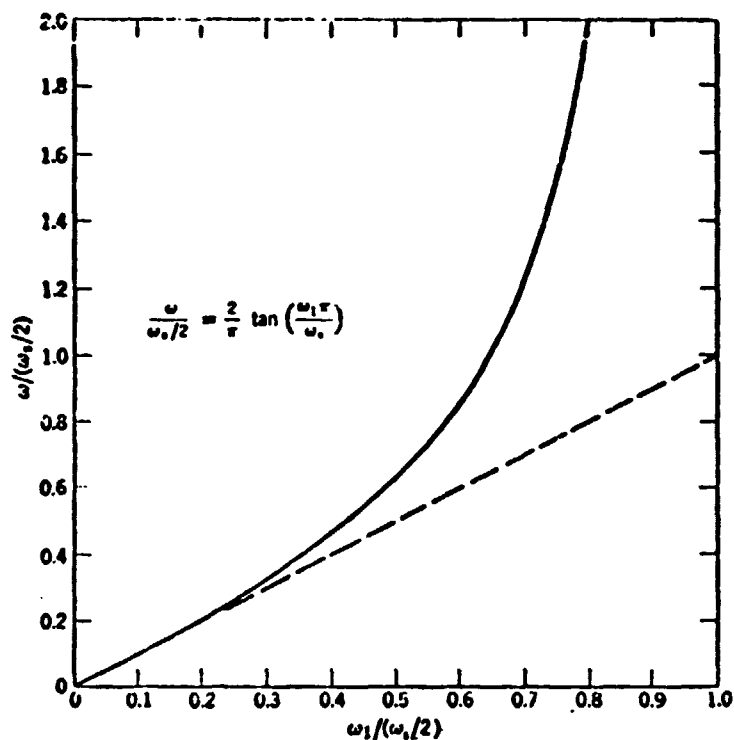


Figure 7.6-1. Non-Linear Warping of the Frequency Scale in the Bi-Linear z-Transformation

a most appealing digital filter design technique. It is applicable to low-pass, band-pass, band-stop, and other continuous filters whose magnitude characteristics are essentially constant within successive pass and stop bands.

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