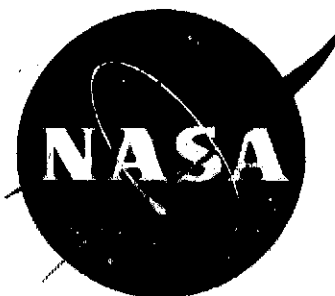


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SIMULATION STUDY OF COMMUNICATION LINK FOR PIONEER SATURN/URANUS ATMOSPHERIC ENTRY PROBE

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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

• WASHINGTON, D. C. •

MARCH 1974

**SIMULATION STUDY OF
COMMUNICATION LINK FOR
PIONEER SATURN/URANUS
ATMOSPHERIC ENTRY PROBE**

by Carl A. Hinrichs

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Prepared Under Contract No. NAS2-7935

by

**MCDONNELL DOUGLAS ASTRONAUTICS COMPANY – EAST
Saint Louis, Missouri**

for

AMES RESEARCH CENTER

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

FOREWORD

This digital simulation study, Contract NAS2-7395, was performed under the auspices of the NASA Ames Research Center. It has determined the performance characteristics of an outer planet's atmospheric probe communications link including the transmitter modulator, the RF channel, and the receiver/bit synchronizer. The study emphasized the acquisition properties and bit error performance of the system under conditions of signal attenuation, Doppler, Doppler rate, and turbulence effects which were modeled during a previous study for a Saturn/Uranus atmospheric probe system definition, Contract NAS2-7328. The simulated flight equipment design was formulated by the TRW Systems Group under subcontract to McDonnell Douglas Astronautics - East.

The author expresses his appreciation for the assistance provided by Dr. Marvin Stone and Mr. Marshall Huang of TRW Systems Group, Redondo Beach, who provided input data and consultation services during the course of this study.

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SIMULATION STUDY OF COMMUNICATION LINK
FOR PIONEER SATURN/URANUS ATMOSPHERIC ENTRY PROBE

SUMMARY

A digital simulation is presented for a candidate modulator-demodulator (modem) in a modeled atmospheric scintillation environment with Doppler, Doppler rate, and signal attenuation typical of the radio link conditions for an outer planets atmospheric entry probe. The results indicate that the signal acquisition characteristics and the channel error rate are acceptable for the system requirements of the radio link. The simulation also outputs data for calculating other error statistics and a quantized symbol stream from which error correction decoding can be analyzed. The results from these data have not yet been evaluated.

The receiver and bit synchronizer are modeled in the simulation at the level of hardware component parameters rather than at the level of loop equation parameters, and the report defines the resultant hardware parameters. Likewise, the scintillation is modeled as a low-pass Gaussian process with the parameters defined in the report.

The receiver performance is plotted for nominal hardware parameters and a range of signal-to-noise ratios both with and without scintillation. The performance is also shown for critical receiver parameter variations.

INTRODUCTION

The objective of this simulation is to determine the performance and to refine design parameters for a receiver which serves as one terminal in an outer planet relay link. The transmitting terminal is a probe entering the planetary atmosphere, and the receiving terminal is in a spacecraft in hyperbolic trajectory about the planet. As with most planetary space systems, the link is power starved, inferring minimal data rates and the use of error correction coding. The link is unique in two respects: First, because of the low data rate, the initial frequency uncertainty due to Doppler and oscillator uncertainty is about 400 times the data bandwidth. Second, atmosphere turbulence may cause significant scintillation on the received signal.

The initial system design (Ref. 1), Saturn/Uranus Atmospheric Entry Probe, conceived a noncoherent link to combat the scintillation at a data rate of 44 bits per second, which was rate 1/2 coded to 88 symbols per second. Preliminary specifications for the transmit and receive terminals were prepared in conjunction with this study (Refs. 2 and 3). In response to these requirements, a preliminary hardware design was defined in Reference 4. Due to the nonanalytic nature of the effect of scintillation on the receiver performance, a simulation was deemed necessary to verify the suitability of the design. A simulation program was written to allow a quantized data stream to be generated on magnetic tape for subsequent decoding and analysis, as well as to investigate receiver acquisition and channel error rate performance, but only the latter two programs are described here.

CONFIGURATION

The configuration details described below are the results of the TRW Systems Group design from Reference 4, and as amended in subsequent meetings. The configuration consists of three pieces of equipment: the modulator, the receiver, and the bit synchronizer.

The modulator, shown in Figure 1, is a continuous phase frequency-shift-keyed modulator. This represents a change from the modulator of the initial study which was a discontinuous phase frequency-shift-keyed modulator, as preliminary studies indicated a severe degradation in performance of a discontinuous phase modulator when operating in conjunction with the candidate receiver. The data symbols drive a 20 MHz VCXO which is upconverted by mixing with a fixed local oscillator to the output frequency. The oscillator will typically switch in 20 microseconds; hence, at an 88 symbol per second rate, the modulation may be considered as true continuous phase frequency shift keying.

Two other continuous phase modulators were also considered, but discarded because of hardware complexity: a three step up-converter and an indirect FM modulator. The modulator candidates are discussed in Appendix X.

The receiver is shown in Figure 2. The receiver signal is first converted to an intermediate frequency and the narrow band filtered and output to two loops: an automatic gain control (AGC) loop, and an automatic frequency control (AFC) loop. The input to the AGC loop drives the coherent amplitude detector via an amplifier which is a soft limiter, i.e., it only limits when the signal is very large (typically 13 dB above nominal). This is to protect the coherent amplitude detector during acquisition, when the gain is wide open, at high signal levels. The AGC loop is completed by low-pass filtering and signal conditioning to the variable gain IF amplifiers.

In the AFC loop, the amplifier before the phase detector originally was a hard limiter, i.e., its output was always $\pm A$. However, early in this study it was felt that the AGC should adequately maintain the signal level and a soft limiter should be used in its place, performing a function similar to that of the coherent amplitude detector amplifier. The AFC loop which tracks the incoming frequency is completed by the loop filter and voltage controlled

oscillator.

If the AGC signal is below threshold, a sweep is activated to acquire the signal. The input to the sweep from the AFC loop is a polarity sense; that is, it reverses the sign of the sweep voltage if the sensed sweep voltage exceeds the design level. The design used in the simulation is different from what is now proposed in the actual hardware. As used, if the voltage to the detector drops below threshold, sweep is immediately initiated. Because of the nature of the scintillation, it was decided during the study to incorporate a resweep initiation delay into the hardware. Thus, if the scintillation caused only a short drop out, the receiver would not start a long (in terms of symbols) search operation. The minimum value for the delay is determined by the fading time constants. Since the amplitude scintillation has a low-pass characteristic with a 3 dB cutoff at 2 Hz (or 4π radians/sec-ond), the delay should be greater than 80 msec. The maximum value of the delay is constrained by the Doppler rate and the actual loop parameters, e.g., the amount of drift the VCO will undergo during the signal absence condition. The Doppler rate is 13.3 Hz/sec. Assuming a nominal VCO scale factor of 4 KHz/V, phase detector offsets of 1.2 mv, and a loop filter time constant τ_1 of 0.45, the phase detector offset voltage will charge up the loop filter capacitor at the rate of $\Delta V/\tau_1 \approx 2.7$ mv/sec. This means the VCO will then drift at approximately 10.7 Hz/sec so the total loop drift, including Doppler rates, is of the order of 24 Hz/sec. Since the receiver has a lock-in range of 38 Hz ($\Delta f_L \approx 2\tau f_n$), the delay should be less than 1.6 sec. Given these two extrema, a time constant of 0.5 sec is recommended to delay the start of sweep after the lock indicator indicates loss of lock. This value could be varied if tests indicate a better value.

Mixer offsets were not simulated since the mixer output drift was only +0.15% over the anticipated voltage range.

A square foot function was considered proper and implementable for the AGC signal conditioner, since the proposed device was linear over a 50 dB range, and the receiver requirements only covered 20 dB, i.e., nonlinearities in the implementation device need not be simulated.

Figure 3 shows the bit synchronizer. This is a conventional early-late gate synchronizer with the addition of a baseline correction circuit to "correct" the effective drift of large numbers of identical bits. As in the case of the receiver proper, drift of the multipliers was determined to have only a 4% timing error, and was judged to be small enough to be idealized as zero for the simulation. A 1-Hz loop noise bandwidth was chosen to maximize the signal-to-noise ratio in the loop while maintaining reasonable acquisition times.

SOFTWARE

In order to simulate the hardware as closely as possible, the approach taken is to simulate the lowest feasible component. For example, each multiplier and filter in a loop are individually simulated, rather than an expression describing the operation of the loop.

A powerful simulation tool is the concept of complex amplitude notation. In this concept, used in the simulation, and described more fully in Appendix I, the "carrier" is normalized out of the simulation. Generically the signal is of the form

$$x(t) = A \cos (w_0 t + \theta),$$

wherein A is the amplitude, w_0 the carrier and θ the phase. By suitable normalization, the signal is thus represented in complex notation as

$$\tilde{x}(t) = A \exp (j\theta).$$

As an example, a frequency-shift-keyed signal (used herein) has two tones,

$$\tilde{x}_1(t) = A \exp (j\pi\Delta f t)$$

and

$$\tilde{x}_2(t) = A \exp (-j\pi\Delta f t)$$

where Δf is the frequency separation between tones.

Amplitude and phase noise are simply introduced as

$$x(t) = A(1 + N_A) \exp [j (\theta + N_p)].$$

One of the principal reasons for this simulation was the determination of the effects, on the modem, of atmospheric scintillation. Atmospheric scintillation arises from localized variations in the refractive index of the atmosphere, chiefly occurring due to temperature variations. Given that a "blob" of atmosphere occurs, it successively breaks into smaller and smaller "blobs" until its energy is dissipated. With numerous blobs across the propagation path, the electromagnetic ray is diffracted in a random fashion, resulting in variations in the signal amplitude and phase. This simulation has modeled amplitude and phase scintillation as

$$A(t) = A_0 (1 + x(t))$$

and

$$\theta(t) = \theta_0 + \theta_1 t + \theta_2 t^2 + s(t),$$

i.e., a linear variation of the amplitude with its scintillation, $x(t)$, and the phase with its scintillation, $s(t)$. The $\theta_1 t$ and $\theta_2 t^2$ terms represent Doppler and Doppler rate, respectively. The $x(t)$ and $s(t)$ terms are taken as low-pass zero-mean Gaussian processes with root variances of 0.23 and 0.47, respectively. The filter corner frequencies are 2. and 0.2 Hz, respectively and both roll off in proportion to frequency to the $-4/3$ power.

The $4/3 f$ rolloff presents significant modeling effort, and is detailed in Appendix II. It was seen that the "more efficient" Z transform approach yielded little or no benefit for a $4/3$ order filter, in marked contrast to its effect on integer order filters. Thus, tapped delay lines were employed in the computer routine. To decrease computer time, the simulation linearly interpolates the scintillation between "tap times".

Figure 4 is a block diagram of the simulation receiver. This is "identical" to the hardware block diagram with two exceptions: first, the simulation receiver starts with the input to the first mixer, the radio frequency amplifier being only a constant; and second, the soft limiters before the coherent amplitude detector and phase detector are not modeled as they only serve in the hardware to protect the following devices from excessive power. It may be argued that the soft limiters would have an effect during high signal-to-noise acquisitions. However, this region of operation was judged to be inappropriate in this study. It should also be noted that the AGC signal processor, a square root device, is treated specially. In the routine, because the square root function is one of the more time consuming functions, the square root is linearly interpolated between logarithmic values yielding a maximal 1.46% error. For similar reasons the trigonometric functions are rounded to one degree and tabulated. Note also in Figure 4 that a soft output is added to aid in coding analyses. A rationale for setting the quanta levels is found in Appendix III.

An abbreviated flow chart for the error rate routine is presented in Figure 5. After the initial conditions are established (data, dimension and complex statements) the conditions for this problem are read in. Typically these are variations in signal strength, bandwidths, etc. Next the loop conditions are calculated (time constants, etc) and the turbulence delay lines

initialized. The routine then generates samples (typically 40) for each bit and the loops (AGC, AFC, and bit synchronizer) exercised. The receiver starts below threshold, i.e., the AGC/AFC must acquire and the number of bits to initial lock is determined. The error counter begins when the receiver and bit synchronizer have locked, typically after the reciprocal of the natural frequency of the bit synchronizer loop or approximately 100 bits. This eliminates the error rate "contamination" by both receiver and bit synchronizer lockup effects. Additionally, three other statistics are tabulated: the bit spacing between errors; the conditional probabilities of each quanta level, given the "preceding" level of the soft decision; and the number of times the AGC signal drops below threshold and the number of bits in that dropout. The printout gives the average number of bits per dropout. The routine then continues until the specified number of bits has been processed. A complete list of symbols is found in Appendix IV, and a complete listing in Appendix V. The language is standard Fortran IV. No special computer library subroutines are required.

A typical error rate printout is found in Figure 6. Block 1 has the inputs (signal level, bandwidths, etc.). Block 2 contains intermediate information such as VCO gains and time constants. Block 3 has the mean error rate data: line 1 for the (baseline) filter and sample, and line 2 for an integrate and dump output. For this run of 9.4 dB E/No, the mean error was 0.0247 with a standard deviation of 0.0035. The mean absolute sample level was 0.456 with a standard deviation of 0.205. Reading in block 4, lockup occurred in one bit, but there was one AGC dropout four bits long. Block 5 is the error spacing matrix, where for this run 8 bits were in error 1 bit spacing apart, 3 bits 2 spacing, 1 bit 3 spacing . . . 1 bit 96 spacing and 4 bits with 100 or greater spacings. In this run a moderate amount of "burstiness" occurred, i.e., errors not randomly spaced. Block 6 is the data for four conditional probability matrices, which are read by the figure in the block. The columns of the matrix signify the quantized level of the "B" symbol (current symbol) and the rows signify the level of the "A" symbol (preceding symbol). The most negative levels occur in the first column and the first row, or the upper left position. For example, given the input was -1, -1, which occurred 453 times, an error occurred 22 times. For this

matrix the -1, -1 quadrant contains all the "corrects", the +1, -1 and -1, +1 quadrants single errors and the +1, +1 quadrant double errors. Reading in the -1, +1 quadrant when B (current bit) was position 5 (in error) the last bit, A, was four times in 1, two times in 2, two times in 3 and two times in 4. Finally block 7 has the end points of the random number generators plus a monitor recommending the best sampling time (phase of the bit synchronizer in sample counts).

As the complete receiver simulation is somewhat lengthy, plus having special steering and routines for error measurement, a special routine was adapted for acquisition studies with its own steering requirements. An abbreviated flow chart is shown in Figure 7, with details in Appendix VI. The initial setup, problem reading and conversions are identical to those of the error rate routine. In this case, however, Doppler is injected, and once the receiver acquires, another "case" is run to determine the probabilities of acquisition under various conditions. It should be noted on the simulation block diagram that the Doppler is injected as a loop stress, rather than a phase time product at the input. Comparing the loop responses in the two cases reveals identical baseband performance even though the double frequency terms which are filtered out are slightly different. Returning to the flow chart, after each acquisition trial, intermediate results are printed. For each trial the receiver is reinitialized and samples are generated. If the sweep goes past the input Doppler, a miss is registered. If the AGC signal goes above threshold an acquisition may have occurred. A check of whether the sweep got to the Doppler determines whether the condition was a true or a false acquisition.

A typical acquisition printout is shown in Figure 8. Blocks 1 and 2 are as stated before. Block 3 shows the conditions at the end of each trial. In the first 12 sweeps the receiver acquired. In the 13th sweep it missed acquisition. From the 14th to the 20th trials it acquired, but missed again on the 21st trial. In no case was a false acquisition found. The fifth column contains the bit count at the end of that run, the following three columns give the sweep voltage, its value after the AFC loop filter, and the value input to the bit synchronizer.

During the "fabrication" of the acquisition software, it was found that serious aliasing could occur if the sample rate were insufficient. Referring to the input mixer in Figure 4, it is seen that as far as the computer is concerned it is merely multiplying two strings of complex numbers. If they appear to correlate after filtering, large correlated numbers (rather than random zero mean numbers) are detected in the CAD circuit signifying lock. Now, if the samples are widely spaced in the time domain, apparent correlation due to aliasing can occur. This happens periodically when uniformly sweeping the VCO, resulting in a false acquisition. Because of the relatively low sweep rates, this condition occurred long enough for the CAD filter to respond. During the error rate studies a sample rate of 40 samples per bit was used. When this rate was used in the acquisition studies, false acquisitions always occurred. The sample rate had to be increased to 200 samples per bit for 1 kHz Doppler before the aliasing effect was negligible. Higher Doppler shifts would require correspondingly higher sampling rates. Therefore, the acquisition studies were run at 1 kHz Hertz Doppler to conserve computer time.

Both of the routines have seven subroutines:

NRANDM: Gaussian Number Generator
RANDM: Uniform Number Generator
BIFILT: Bandpass Filter
BLOBA(P): Amplitude and Phase Scintillation Lines
TRIG: Trigonometry (1-deg table for computer speed up)
ASQRTF: Square Root (linear interpolation for computer speed up)
DATAS: Data Source (six-bit feedback shift register)

Some subroutines used in the checkout phases, but not used in the production runs, are given in Appendix VII.

RESULTS FOR NOMINAL CONDITIONS

The first step in the production runs was to determine the performance for nominal conditions. These are given in Table I. All the performance data points are based on 1900 bit scintillation runs. Before this simulation could be done, however, two additional parameters had to be found: the proper threshold level and the AGC gain.

TABLE I
NOMINAL CONDITIONS

<u>Parameter</u>	<u>Symbol</u>	<u>Value</u>
Bit Rate	BRATE	88. bps
Minimum Loop Signal	ENOMIN	9. dB
Tone Separation	DELF	62. Hz
IF Bandwidth	BIF	1000. Hz
AFC Loop Bandwidth	BL2	176. Hz
AFC Phase Error	PHIDEG	10. deg
AFC Pull-In Range	FDIFF	342. Hz
Bit Sync Bandwidth	BL2B	1. Hz
Bit Sync Phase Error	PHIB	10. deg
Bit Sync Pull-In	FDLFFB	5. Hz
AGC Filter Constant	TAU3	.07957
Sampling Filter Constant	TAU4	.001808
Baseline Filter Constant	TAU5	.01808
Doppler Filter Constant	TAU6	.10603
Baseline Filter Gain	A5	.5

Normally the threshold is initially set at some factor greater than the noise-only output, and then varied to minimize dropouts and minimize false acquisitions. For the simulation, the probabilities of a voltage occurring with noise only (herein -20 dB E/N_0 , since it was easier to reduce the signal than to eliminate it) and with signal was determined. This is shown in Figure 9. All of the data referred to in this section appear in Appendix VIII. It should be noted that these early runs employed a slightly different printout format with more internal diagnostics than used in the production

runs. The symbols are all identical however; thus no confusion is anticipated in reading the data. Based on this information a threshold of 6.5 was used.

The AGC signal processor attempts to keep the voltage into the phase detector constant, to keep a constant open loop gain. This is done by setting the IF gain according to the reciprocal of the square root of the filtered coherent amplitude detector output. For a noise-only input, the gain is maximum, and a gain function ABC on Figure 10 is produced. While determining this function during the debugging operation, it appeared that additional gain below "minimum signal" would be beneficial, particularly in a scintillation environment, e.g., curve ADE or curve AFG. The additional gain herein is termed the dynamic range, DYNR. Results of such runs are shown in Figure 11. A DYNR of 3 dB appears to offer the best performance with scintillation, and was thus chosen for the nominal conditions.

The first parameter of interest is the mean error rate. This is shown in Figure 12. The vertical marks about each experimental point indicate the measurement standard deviation. Note that these runs count errors even during AGC dropout after initial acquisition. The mean error rate without scintillation is well within the "specified" value in the receiver specification, Ref. 3. With scintillation the performance is acceptable to about 10.5 dB. It should be noted that this performance refers only to the mean error rate. In a coded system the distribution of errors is also important. The data dumps in Appendix VIII show that the nonscintillation error distributions are roughly random (the error history matrix), but the scintillation runs have significant burst errors, i.e., groupings of errors. Further coding analysis is required to evaluate the performance of the system with scintillation.

Further study of the conditional probability matrices should enhance the evaluation of the system's capability to support coding. As noted in the previous section, this is moderately influenced by the soft quantization level. The bulk of the data was generated prior to the coding analysis of Appendix III and used a soft quanta of $ASOFT/2 = 0.15$. Figure 13 shows the mean and standard deviation of the sampled level voltages of the data of Figure 12. This was diagnostic information to determine the quantization level. At an E/N_0 of 9.4 dB, the nominal minimum, the standard deviation is 0.2; thus,

$ASOFT/2 = 0.15$ corresponds to a quanta level of 0.75 ($ASOFT/2/\text{std. dev.}$) of the standard deviation. According to Appendix III, 0.6 would be more appropriate, or $ASOFT/2 = (0.6 \text{ std. dev.})$ or 0.12.

Another interesting factor seen in Figure 13 is the slight increase in "output" signal-to-noise ratio with the input. At E/N_0 of 7 dB we have a mean to standard deviation of 0.45/0.23 (5.83 dB) and at E/N_0 of 11 dB we have a mean to standard deviation of 0.47/0.19 (7.87 dB). There is only a 2.04 dB apparent increase in output for a 4 dB input increase indicating some memory, intersymbol interference, or possibly implied "noncoherent" signal detection, i.e., autocorrelation of signal plus noise.

The second parameter of interest is the probability of acquisition. Runs were made at 9.4 and 12.4 dB, with and without scintillation. The data in the appendix indicate 100% acquisition. At lower signal to noise, as in Figure 8, missed acquisitions occur. There was insufficient data, however, to plot the function.

RESULTS FOR PARAMETER VARIATIONS

A number of runs were made to investigate the effects of varying the parameters of the receiver. These may be roughly broken into two cases: system variations, and hardware variations. Table II lists the system variations. The data for this section are given in Appendix IX.

The results of modulation index variation is shown in Figure 14. As expected the optimum is 0.7, with and without scintillation.

TABLE II
SYSTEM PARAMETER VARIATIONS

<u>PARAMETER</u>	<u>VALUES</u>	
DELF (Modulation index oriented)	26.4, 44, 62, 88, 132	Hz
BIF (IF Bandwidth)	500, 750, 1000, 1500, 2000	Hz
BL2 (AFC $2B_L$)	88, 100, 164, 176, 188	Hz
TAU4 (Sampled Output Filter)	88, 144, 200	Hz

The second system parametric, the intermediate frequency bandwidth, is of some implementation importance. If the bandwidth is too narrow the filter could produce sufficient phase shift in the loop to cause instability. An intermediate frequency bandwidth of ten times the loop filter bandwidth, or 1 kHz was initially recommended. Because of the high Q of this device, wider bandwidths might be easier to fabricate. Figure 15 illustrates the data. These represent a second set of runs, because an initial set was required to establish the proper level at the sampled output and to define the simulation sampling requirements in the scintillation. The runs at and below 1 kHz were run with 40 samples per bit, and those above proportionally higher. Without scintillation, the higher bandwidths give slightly better performance; apparently beginning to level out in the vicinity of 1500-2000 Hz. With scintillation, the "knee" appears to be between 1000 and 1500 Hz.

The results with the receiver loop bandwidth parametric are shown in Figure 16. The nominal 176 Hz case is optimal both with and without scintillation.

The final system parametric is the variation of the corner frequency of the sampling filter. In conjunction with this, the output of the

synchronizer integrate-and-dump was also measured. These data, in Figure 17, are also the second set of runs, the first being required to optimize the sampling time. It is seen that wider bandwidths degrade the performance, although less dramatically when scintillation is present. The integrate-and-dump output appears to be uniformly better. Incidentally, the three points shown for each integrate-and-dump output represent one datum; since no parameter change is made for it; the apparent variations are experiment scatter.

The expected hardware variations are summarized in Table III. Of these, only ENODB, DELF, and BL2 are judged significant. Two "worst cases" were defined; ENODB of 9.2, DELF of 66, and BL2 of 164; and ENODB of 9.2, DELF of 60, and BL2 of 188. The simulation results are shown in Figure 18. Worst case 2 shows little variation from the nominal, within one sigma of the measurement. Worst case 1 shows between 0.5 and 0.75 dB degradation.

TABLE III
HARDWARE VARIATIONS

<u>Parameter</u>	<u>Nominal</u>	<u>Min</u>	<u>Max</u>	<u>Comment</u>
ENODB	9.4 dB	9.2	9.9	Based on -142.8 dBm, noise at -174 dBm and NF of 2.3 dB.
DELF	62 Hz	60	66	Oscillator pulling range accuracy
BIF	1000 Hz	- Negligible -		Crystal manufacturer data
BL2	176 Hz	164	188	RSS estimate of gain changes, and scale factors
SVRHZ	2.2 kHz/sec	2.1	2.3	5% variance to sweep and VCO scale factor
EVMAX-EVMIN	35 kHz	33	37	5% sweep drift and VCO scale factor
TAU3	.07957	.07718	.08196	3% RSS time constant
TAU4	.001808	.001754	.001862	Same as TAU3
TAU5	.01808	.01754	.01862	Same as TAU3

CONCLUSION

Digital computer simulation of a data link has shown that the candidate modem appears, from the mean error rate viewpoint, to be acceptable to the systems requirements. A complete verification of the usage of the modem for a coded telemetry system must await further coding analyses. The performance is well within the specified error rate bounds without atmospheric scintillation, and the errors appear to be random. Performance is also acceptable with scintillation but the errors appear to be bursty.

The system parametric studies reveal that:

- o a slightly larger intermediate frequency bandwidth of 1500-Hz would be more advantageous than the current 1000-Hz nominal.
- o the data output sampling filter of the bit synchronizer could be improved, e.g., a straight integrate-and-dump, or perhaps a higher order filter.
- o the effect of hardware degradations are within acceptable range.
- o in the range of signal strengths anticipated by the Reference 1 system studies, the receiver appears to acquire every time. Additional runs are required to fully trace the probability-of-acquisition curve.

Because of scintillation modeling uncertainties, it appears worthwhile to try other scintillation models and also to explore the effects of the resulting error distributions in coding studies.

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- 3 Receiver Specification, SAEP-ES-8 Rev. B, April 30, 1973.
- 4 Data Handling and Communication Subsystem Definition Study for Saturn Atmospheric Entry Probe, TRW S/N 23765, July 1973.

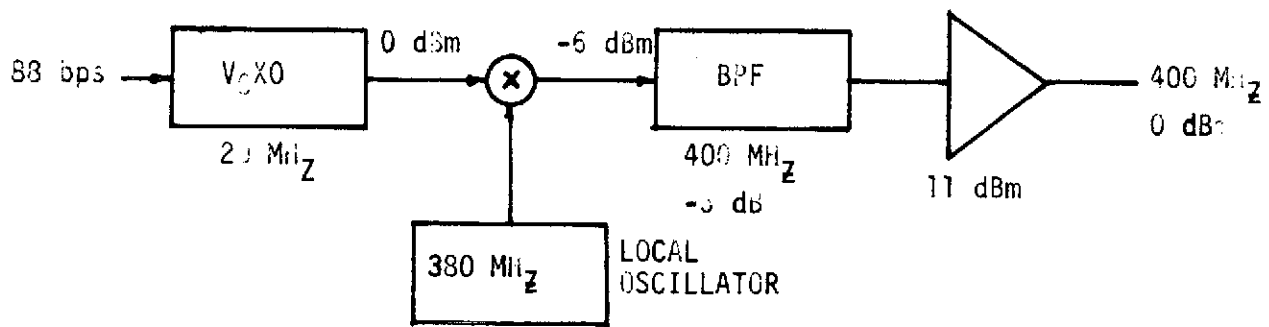


FIGURE 1
SINGLE CONVERSION DIRECT FM MODULATOR

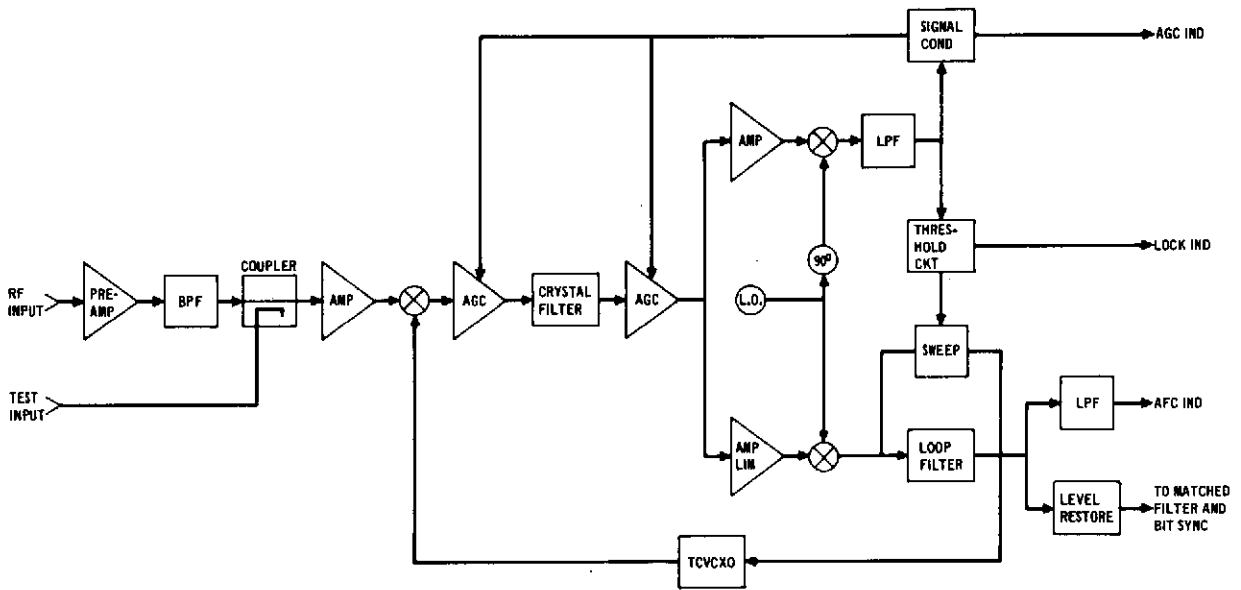


FIGURE 2
RECEIVER DETAILED BLOCK DIAGRAM

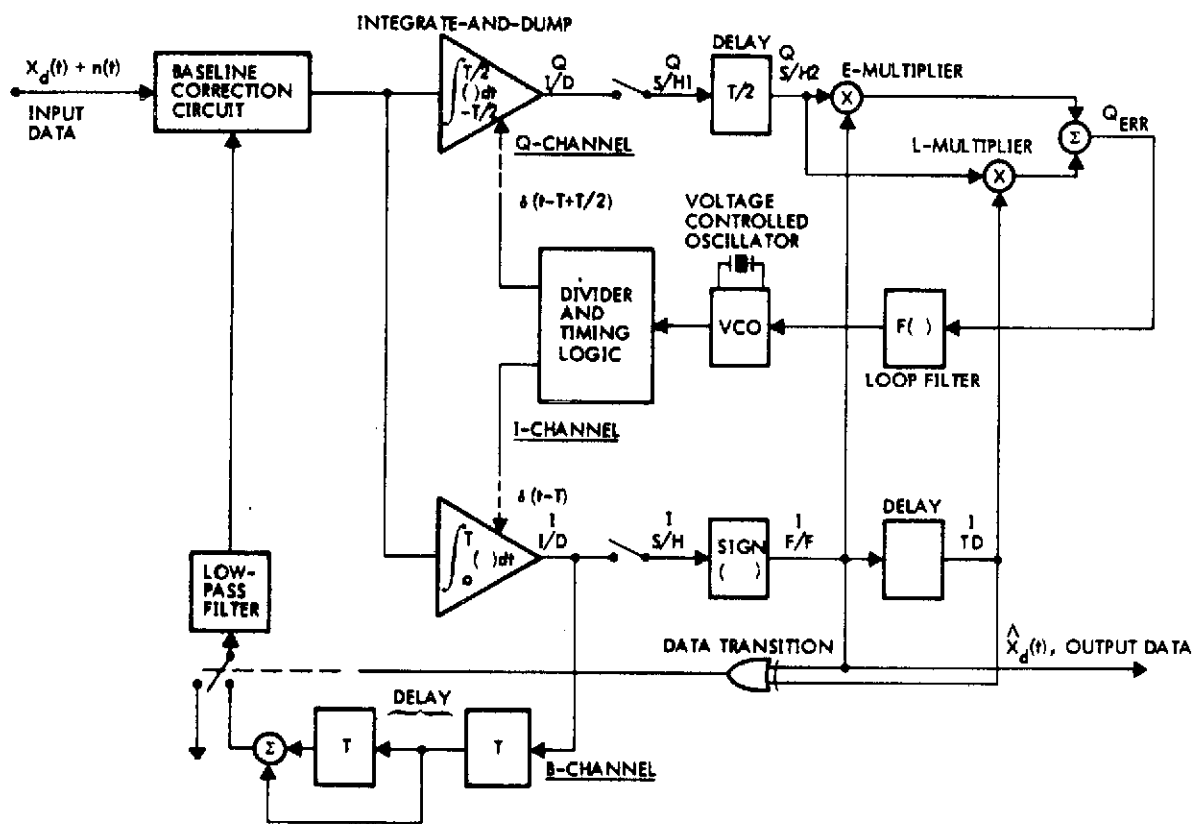


FIGURE 3
BIT SYNCHRONIZER

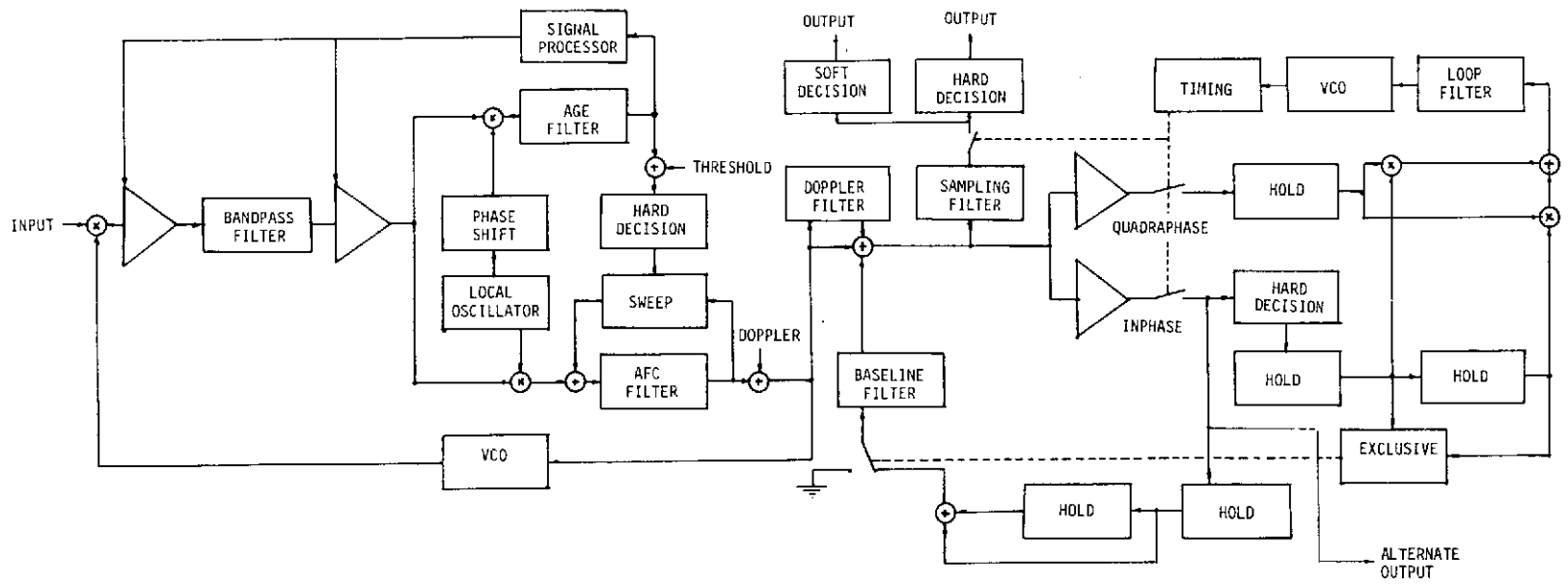
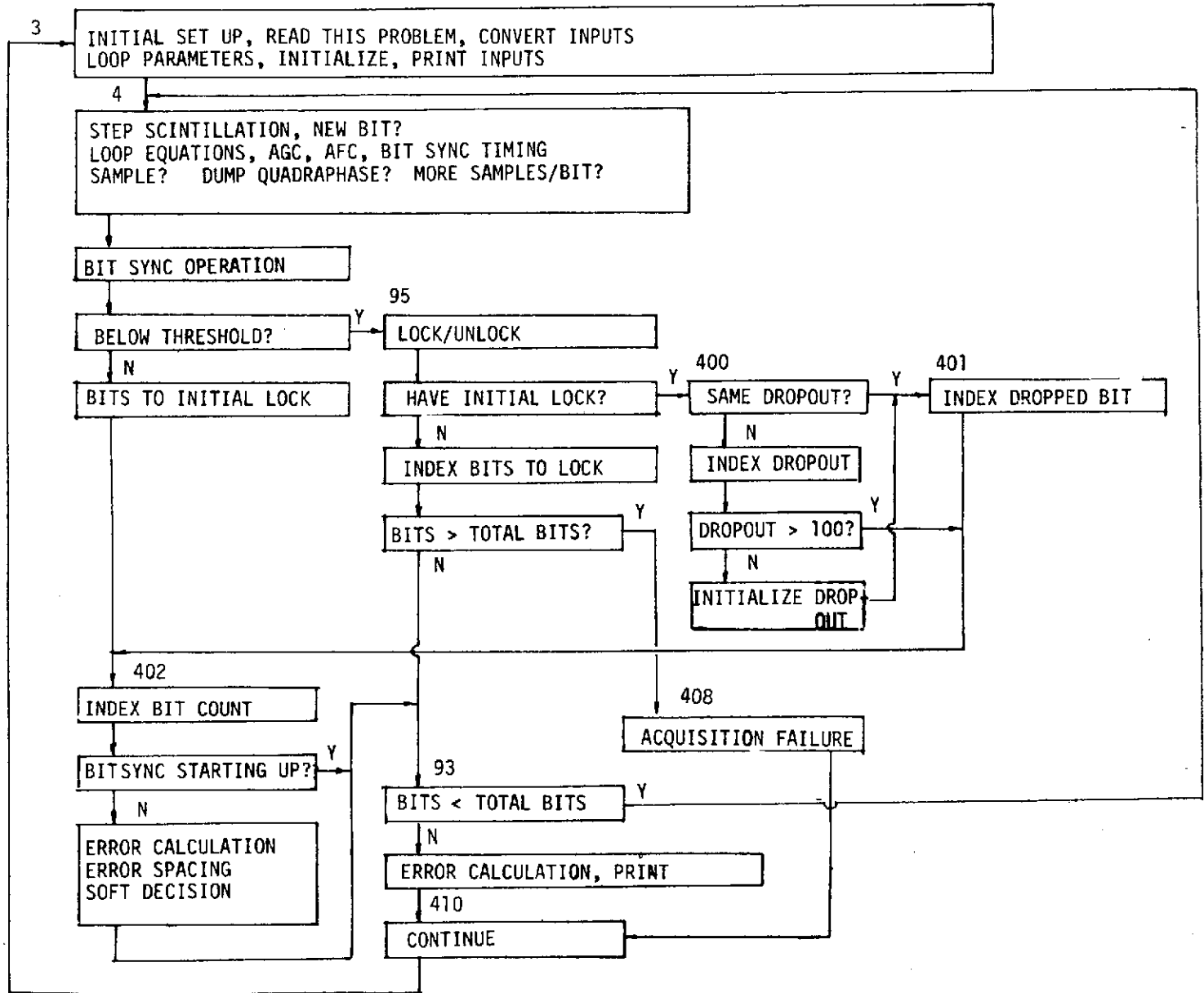


FIGURE 4
SIMULATION BLOCK DIAGRAM

FIGURE 5
ABBREVIATED ERROR RATE FLOW CHART



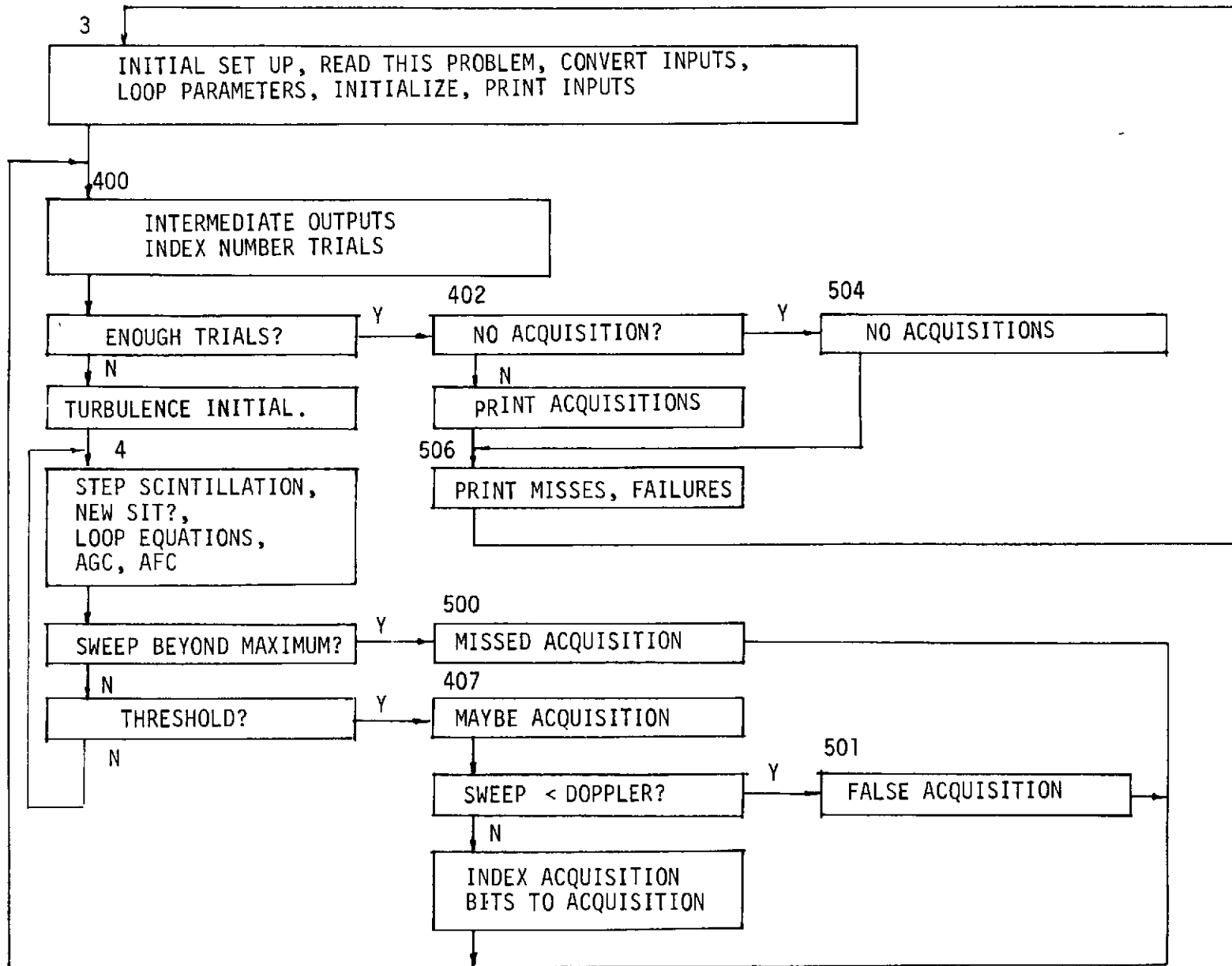


FIGURE 7 ABBREVIATED ACQUISITION FLOW CHART

```

EN0DB= 6.0 ,DELTA= 62.0 ,RTF= 1000 ,RL2= 176
SVRHZ= 2.2000E+03 ,SMX= 2.5000E+03 ,SMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FR000P= 1.0000E+03 ,FODPRT= 1.0000E+01 (1)
TL= -6.50 ,DYNR= 3.0 ,SDAMP= .230 ,SDPHA= .470 ,I1,I2,I11,I22 1 1 1 1
NN= 166.9 ,K= 458.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 (2)
NACQ,AMISS,AFAL,KDATA,ES,EV,EVI
1 0. 0. 1.0000E+00 68 2.2635E+01 1.3609E+01 9.3935E-02
2 0. 0. 2.0000E+00 71 2.3685E+01 1.4497E+01 9.5541E-01
3 0. 0. 3.0000E+00 70 2.3151E+01 1.4069E+01 5.5659E-01
4 0. 0. 4.0000E+00 70 2.3451E+01 1.2962E+01 -5.6855E-01
5 0. 0. 5.0000E+00 69 2.2900E+01 1.4216E+01 5.3746E-01
6 0. 0. 6.0000E+00 66 2.2120E+01 1.3086E+01 -4.1763E-01
7 0. 0. 7.0000E+00 72 2.4047E+01 1.2802E+01 -6.1208E-01
8 0. 0. 8.0000E+00 71 2.3622E+01 1.3369E+01 -1.5158E-01
9 0. 0. 9.0000E+00 67 2.2152E+01 1.2975E+01 -5.3987E-01
10 0. 0. 1.0000E+01 63 2.1671E+01 1.2742E+01 -7.7637E-01
11 0. 0. 1.1000E+01 68 2.2522E+01 1.3121E+01 -3.4843E-01
12 0. 0. 1.2000E+01 74 2.4729E+01 1.4045E+01 5.2396E-01
13 1.0000E+03 0. 1.2000E+01 134 4.4907E+01 3.3571E+01 1.9858E+01 (3)
14 1.0000E+00 0. 1.3000E+01 69 2.2827E+01 1.3989E+01 4.2894E-01
15 1.0000E+00 0. 1.4000E+01 75 2.5100E+01 1.3664E+01 2.4033E-02
16 1.0000E+00 0. 1.5000E+01 72 2.4031E+01 1.3116E+01 -4.1164E-01
17 1.0000E+00 0. 1.6000E+01 71 2.3726E+01 1.3435E+01 -1.2380E-01
18 1.0000E+00 0. 1.7000E+01 73 2.4257E+01 1.2685E+01 -8.1762E-01
19 1.0000E+00 0. 1.8000E+01 77 2.5477E+01 1.4113E+01 5.8743E-01
20 1.0000E+00 0. 1.9000E+01 70 2.3132E+01 1.4589E+01 1.0603E+00
21 2.0000E+00 0. 1.9000E+01 136 4.5311E+01 3.3569E+01 1.9958E+01
22 2.0000E+00 0. 2.0000E+01 70 2.3287E+01 1.4397E+01 8.5247E-01
23 2.0000E+00 0. 2.1000E+01 77 2.5757E+01 1.3887E+01 3.1475E-01
24 2.0000E+00 0. 2.2000E+01 74 2.4483E+01 1.2782E+01 -6.8782E-01
25 2.0000E+00 0. 2.3000E+01 81 2.6995E+01 1.3366E+01 -1.1882E-01
26 2.0000E+00 0. 2.4000E+01 70 2.3246E+01 1.3267E+01 -3.0114E-01
27 2.0000E+00 0. 2.5000E+01 72 2.3830E+01 1.3939E+01 4.2498E-01
28 2.0000E+00 0. 2.6000E+01 64 2.1327E+01 1.3163E+01 -3.4685E-01
29 2.0000E+00 0. 2.7000E+01 69 2.2935E+01 1.4569E+01 1.1191E+00
30 3.0000E+00 0. 2.7000E+01 131 4.3845E+01 3.3573E+01 1.9824E+01
PACQ= 9.0000E-01 ,STDEV= 5.6772E-02
AVEES= 2.3577E+01 ,STDES= 1.2897E+00 (4)
AVE KDATA= 7.0852E+01 ,STDEV= 3.8558E+00
PR MISSED ACQ= 1.0000E-01
PR FALSE ACQ= 0.
I1,I2,I11,I22 282 841 1855 1849

```

(1) INPUTS (2) LOOP VALUES (3) INTERMEDIATE VALUES (4) ACQUISITION PROBABILITIES

FIGURE 8

TYPICAL ACQUISITION PRINTOUT

DATA: APPENDIX VIII P. 18-22

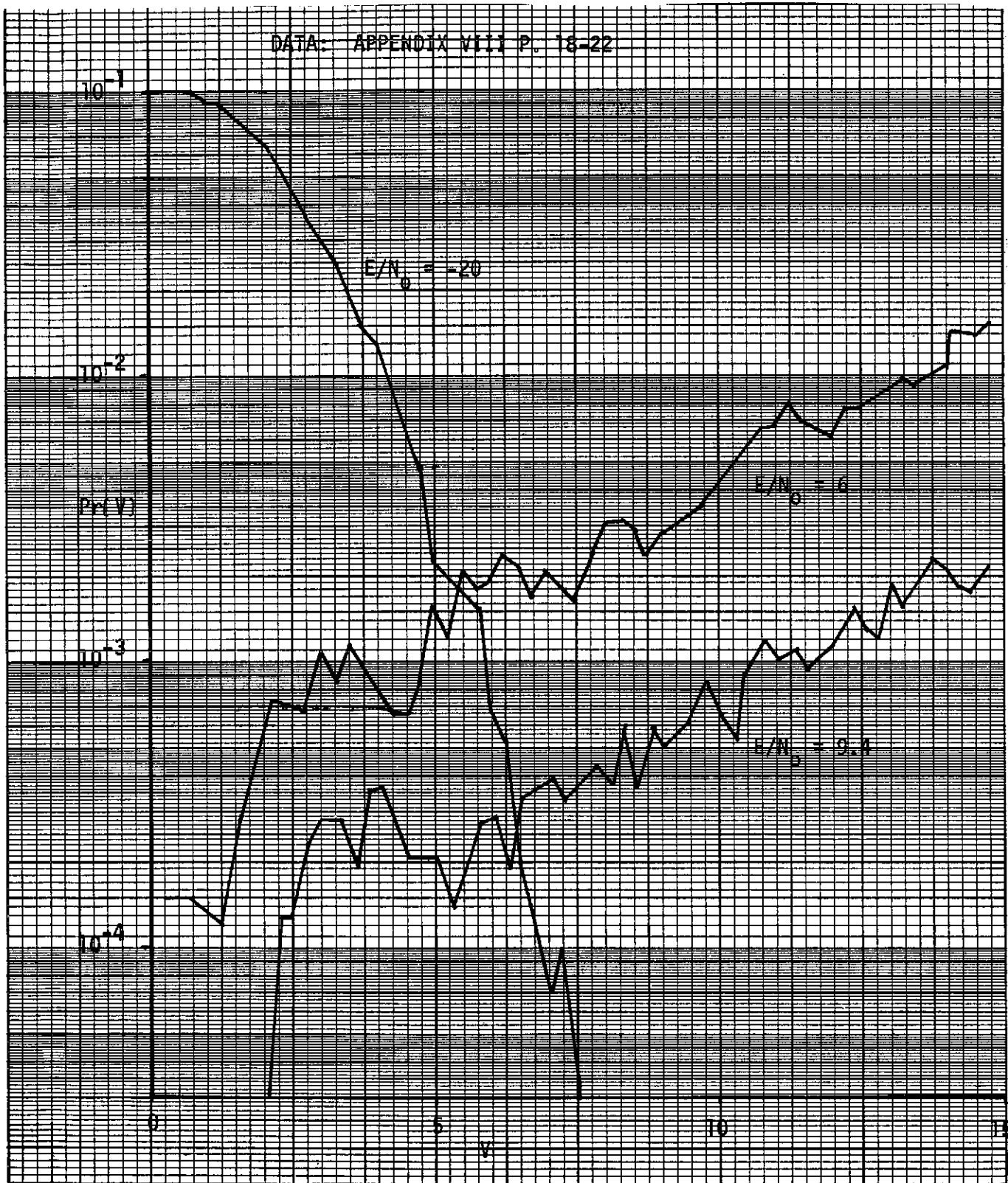


FIGURE 9
AGC VOLTAGE DISTRIBUTION

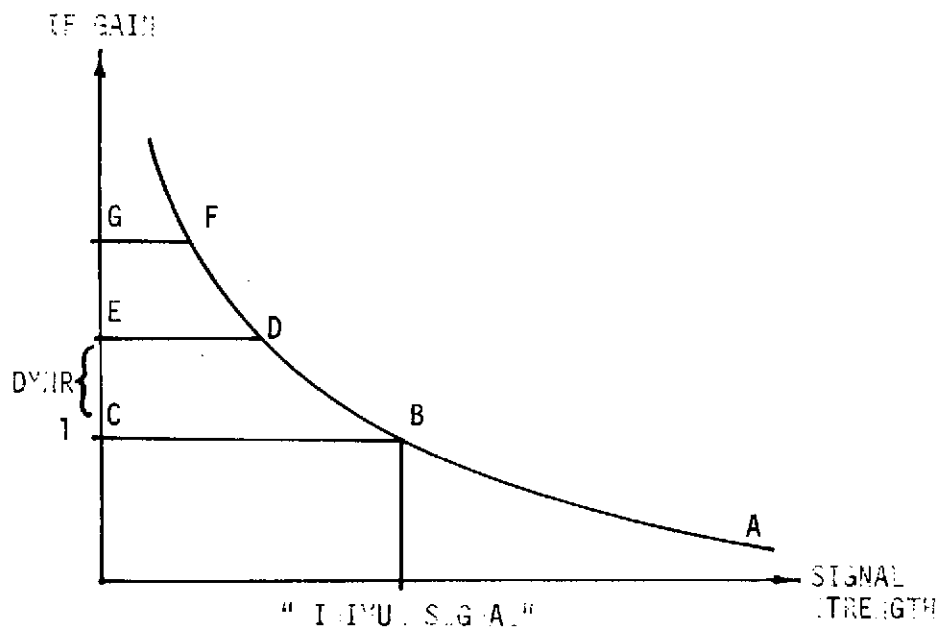


FIGURE 10
AGC GAIN FUNCTION

DATA: APPENDIX VIII P. 23-28

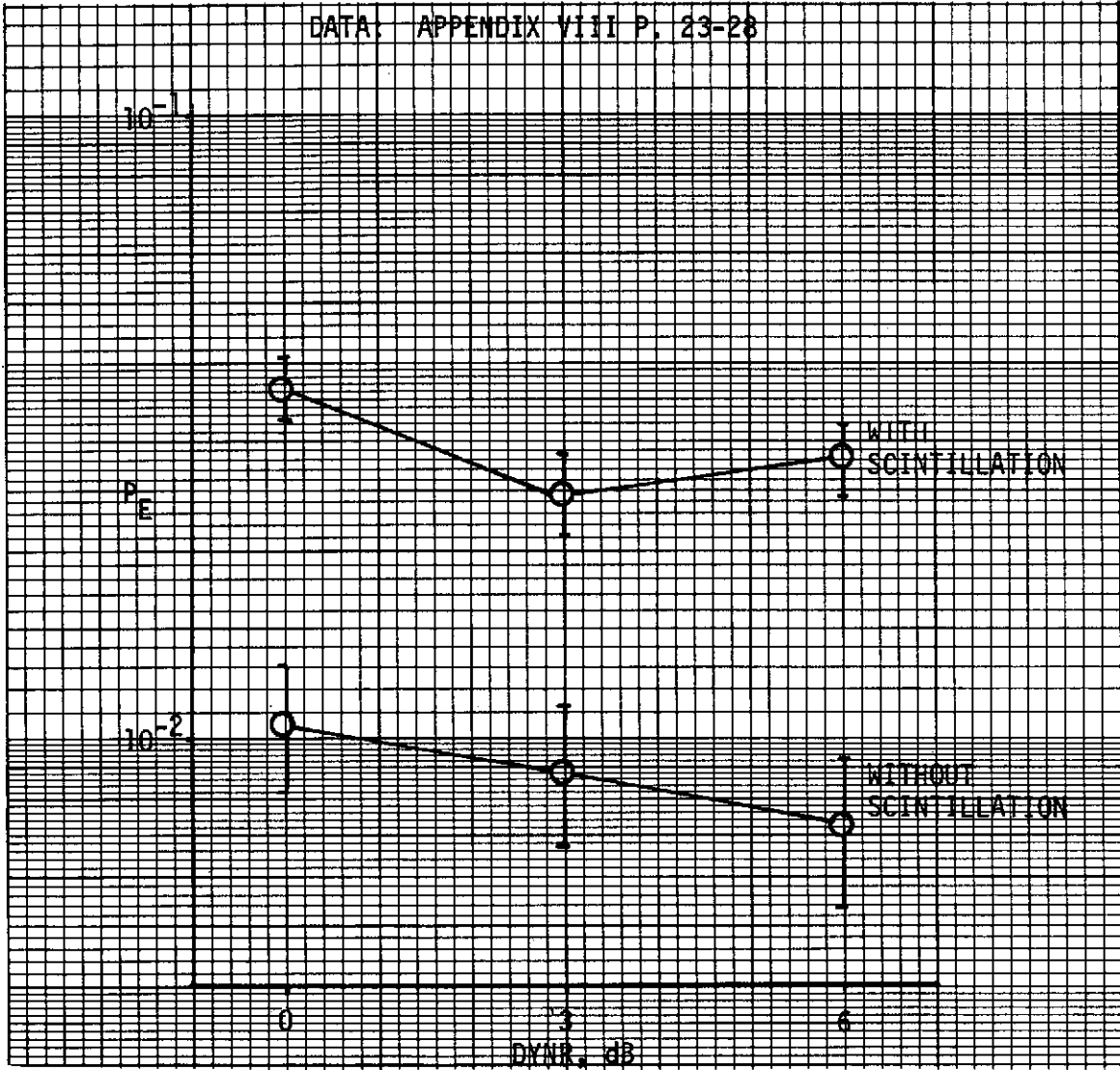


FIGURE 11
MEAN ERROR RATE VERSUS
AGC DYNAMIC RANGE PARAMETRIC

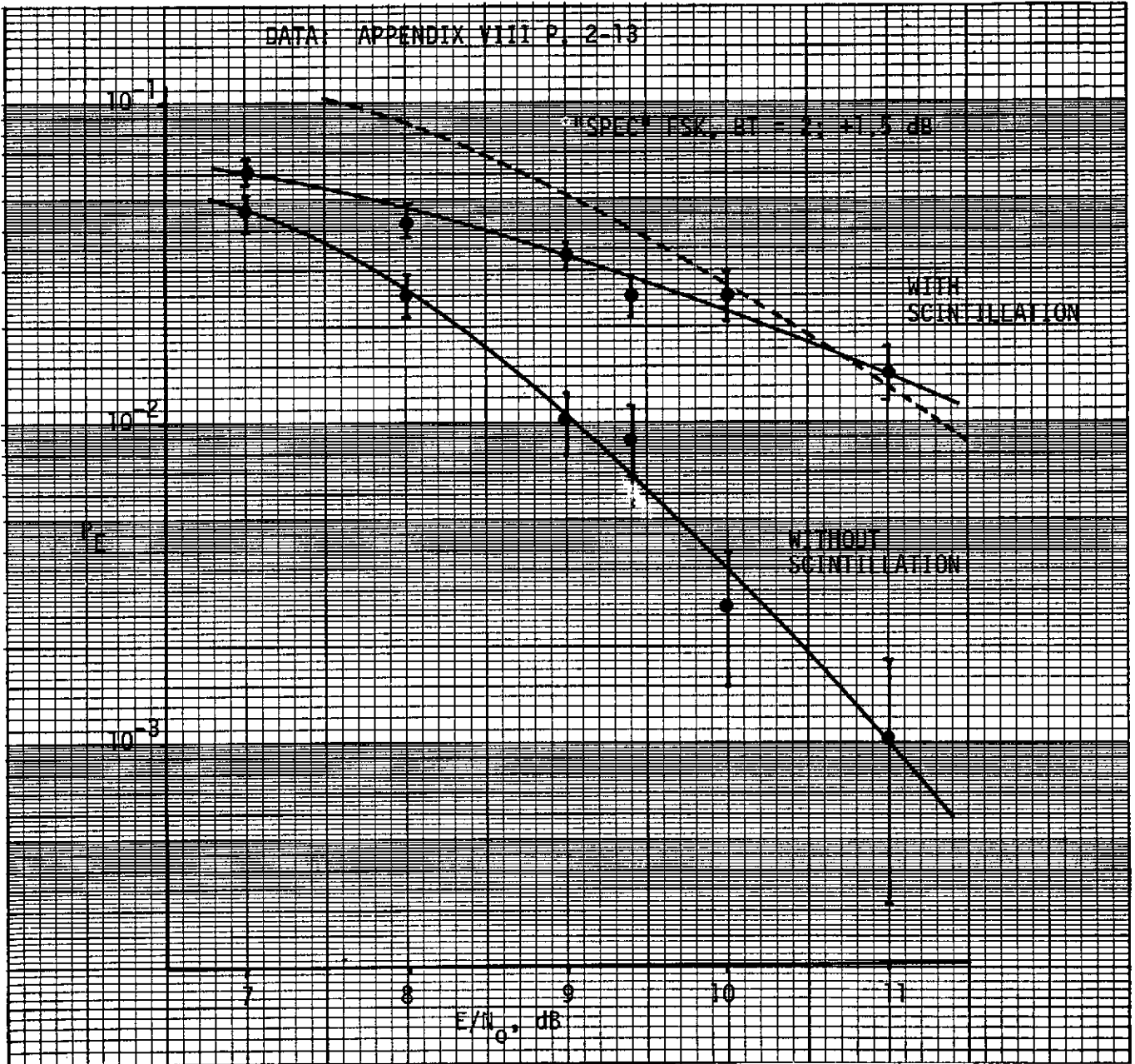


FIGURE 12
 MEAN ERROR RATE VERSUS E/N_0
 FOR NOMINAL CONDITIONS

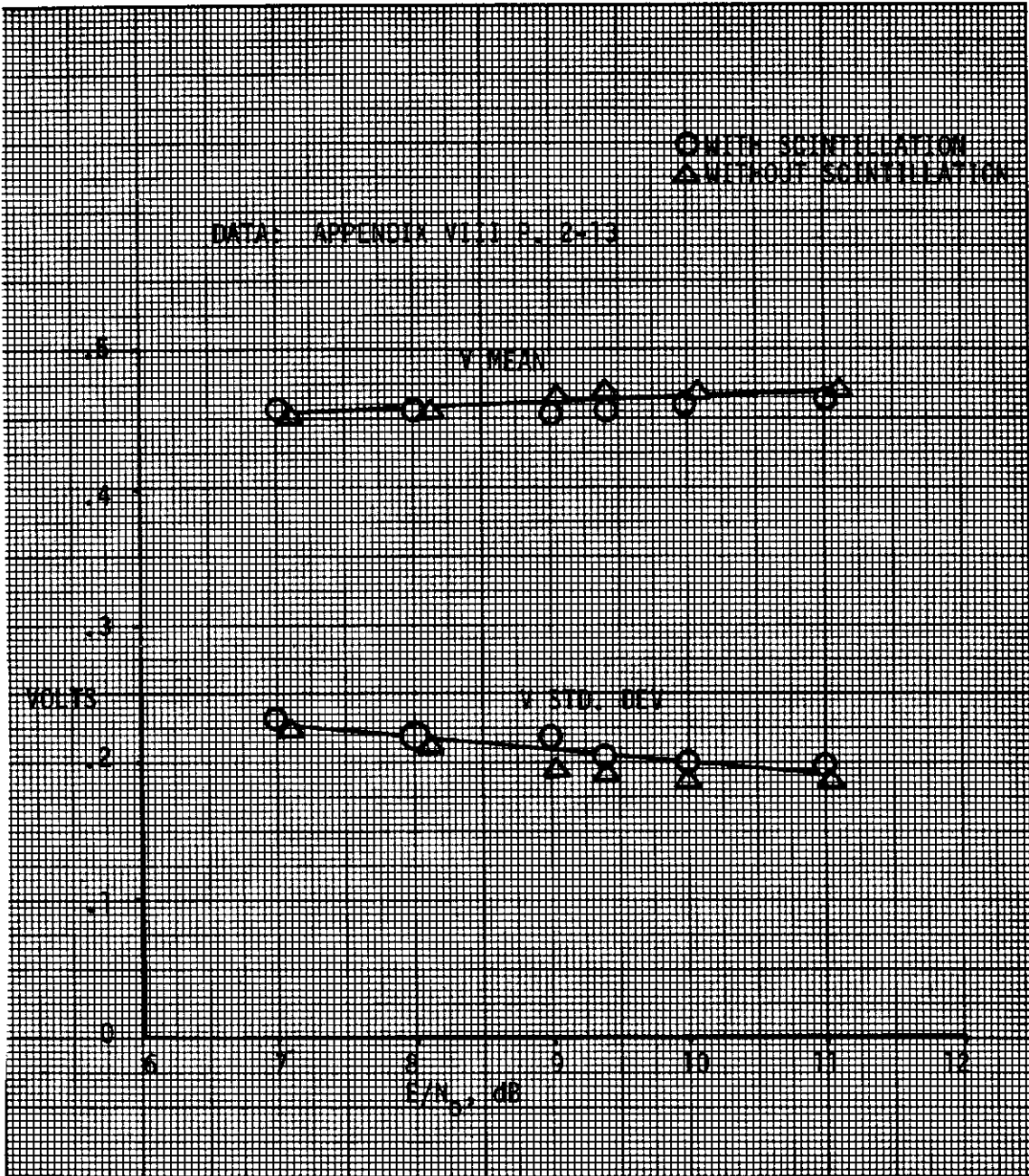


FIGURE 13
 FILTER AND SAMPLE OUTPUT
 VOLTAGE VERSUS E/N_0

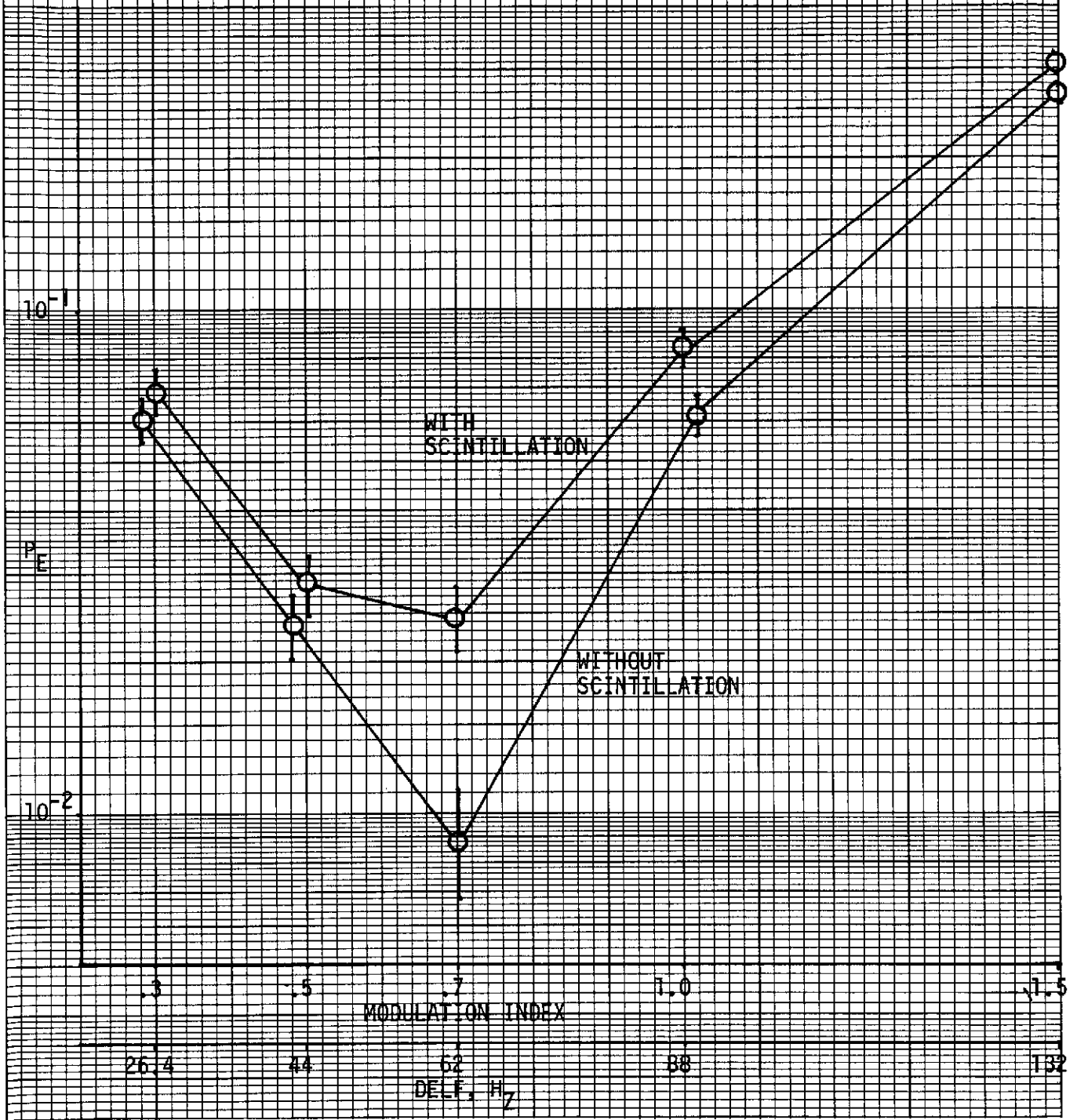


FIGURE 14
MEAN ERROR RATE VERSUS
MODULATION INDEX PARAMETRIC

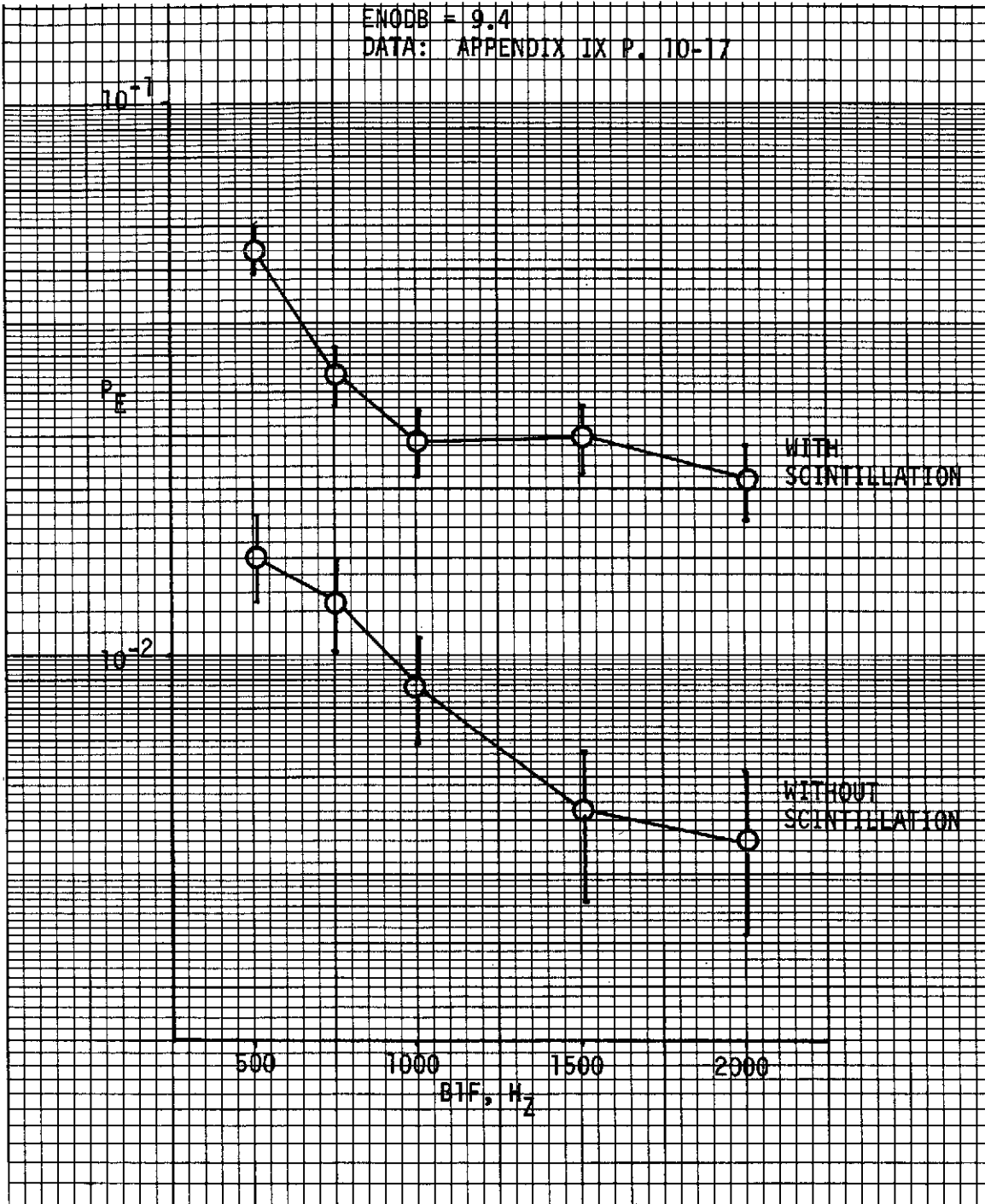


FIGURE 15
MEAN ERROR RATE VERSUS
B1F PARAMETRIC

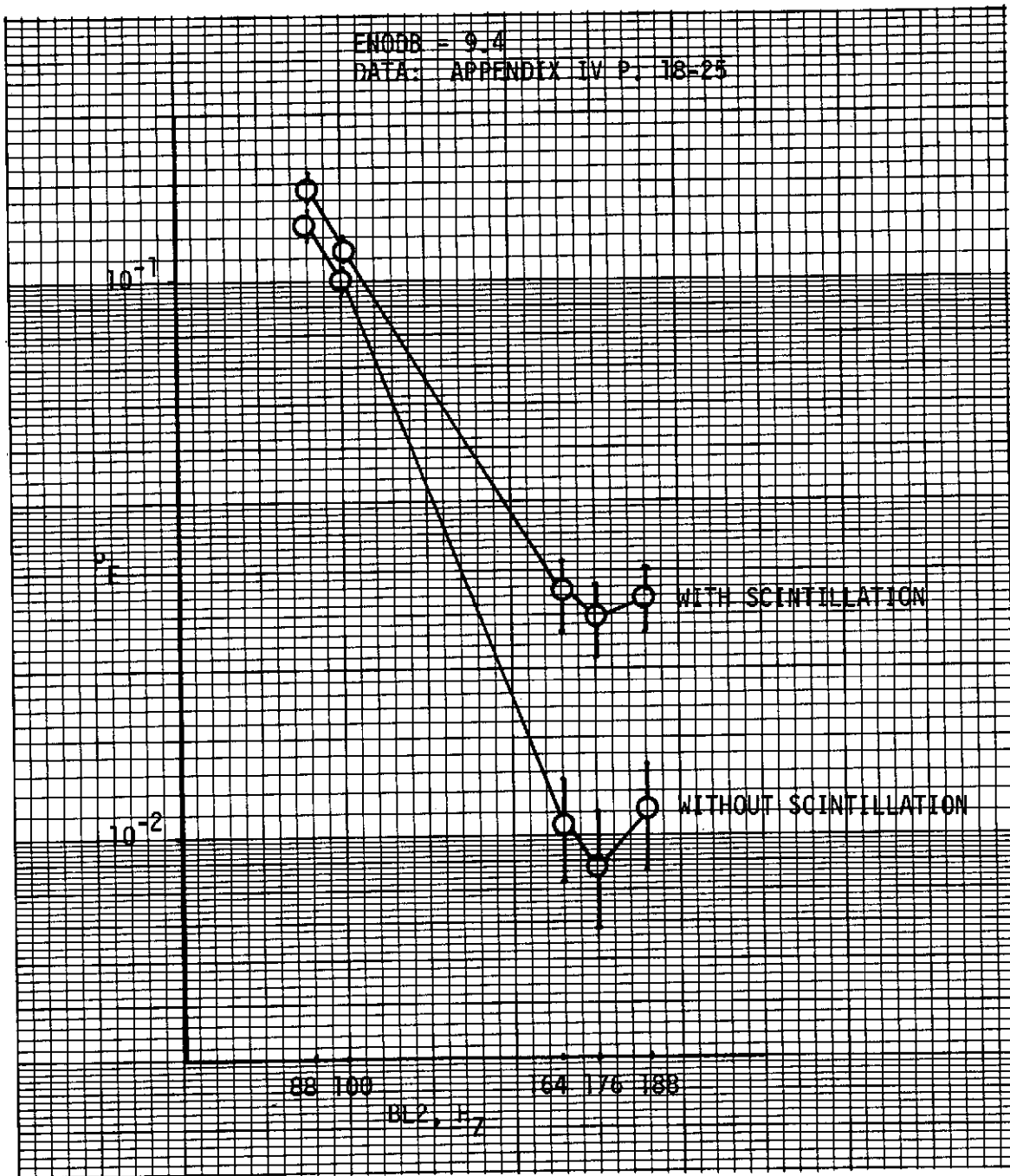


FIGURE 16
 MEAN ERROR RATE VERSUS
 BL2 PARAMETRIC

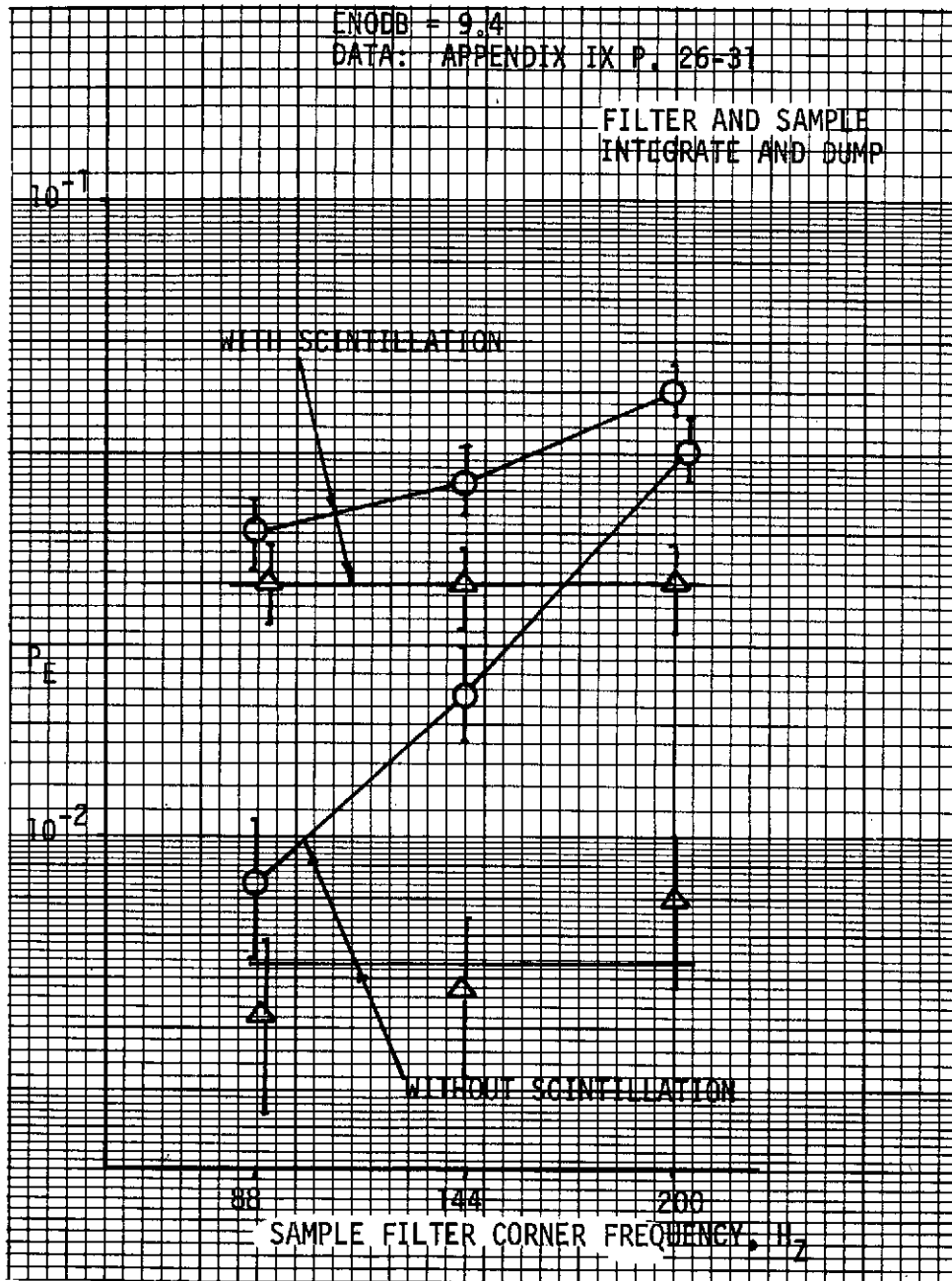


FIGURE 17
 MEAN ERROR RATE VERSUS
 TAU4 PARAMETRIC

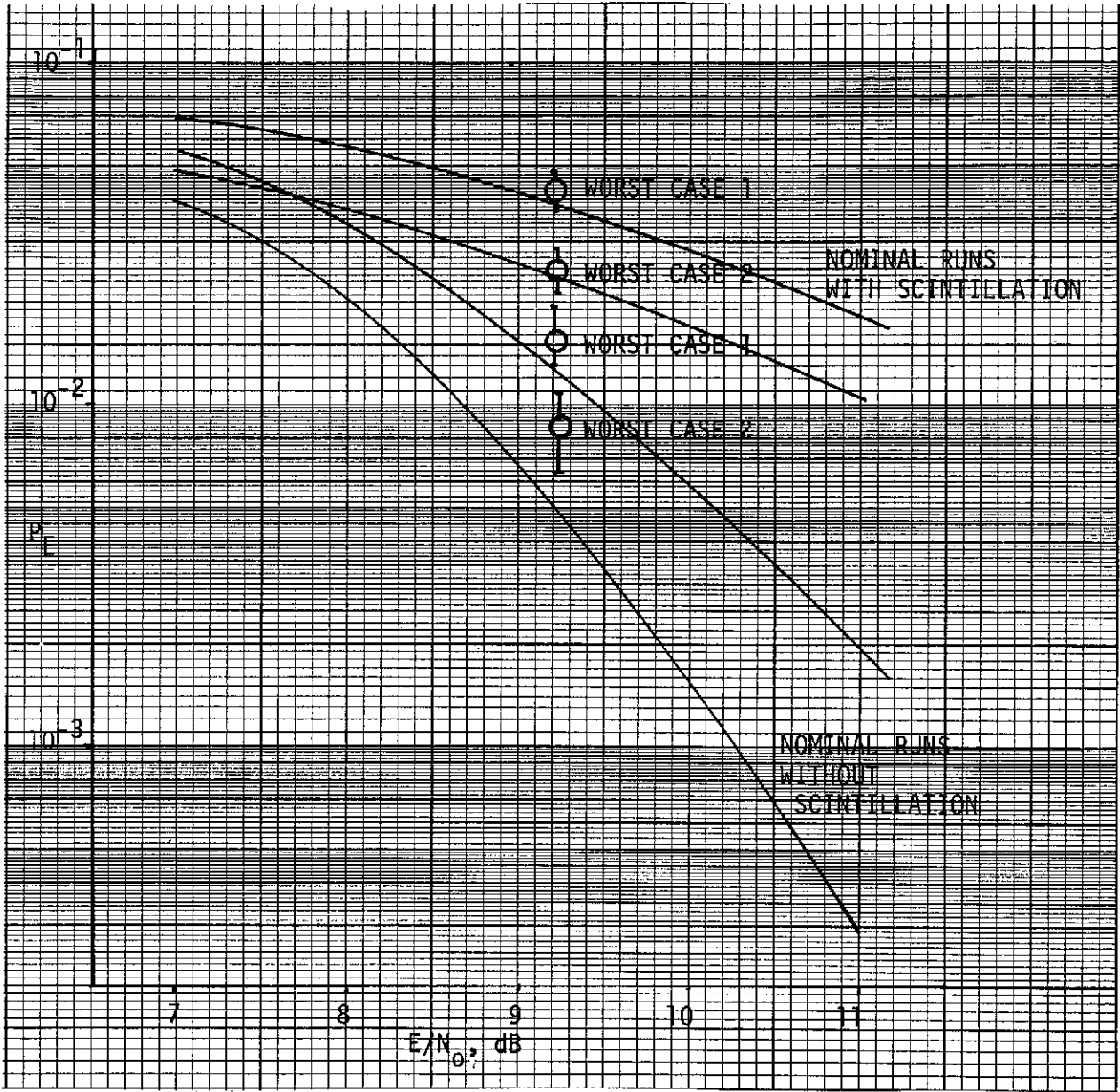


FIGURE 18
 MEAN ERROR RATE UNDER TWO
 WORST CASE HARDWARE VARIATIONS

APPENDIX I
COMPLEX AMPLITUDE NOTATION

Complex amplitude notation is a convenient way to normalize the notation to a reference frequency. The signal waveform is thus

$$x(t) = \text{Re} \{ \tilde{x}(t) \exp(j \omega_0 t) \},$$

where the reference frequency is ω_0 , and the complex amplitude is

$$\tilde{x}(t) = A \exp(j\theta) = A \cos\theta + j A \sin \theta.$$

Herein, A is the signal amplitude, and θ the signal phase. The conventional notation is apparent by combining,

$$\begin{aligned} x(t) &= \text{Re} \{ A \exp(j\theta) \exp(j \omega_0 t) \} \\ &= A \cos(\omega_0 t + \theta). \end{aligned}$$

When multiplying in complex amplitudes

$$z(t) = x(t) y(t)$$

or

$$z(t) = \text{Re} \{ \tilde{x}(t) \exp(j \omega_0 t) \} \text{Re} \{ \tilde{y}(t) \exp(j \omega_0 t) \}.$$

Using the identity

$$\text{Re} \{ \tilde{x}(t) \} \text{Re} \{ \tilde{y}(t) \} = \frac{1}{2} \text{Re} \{ \tilde{x}(t) \tilde{y}(t) + \tilde{x}(t) \tilde{y}^*(t) \},$$

the star denoting the complex conjugate, we have

$$\begin{aligned} z(t) &= \frac{1}{2} \text{Re} \{ \tilde{x}(t) \tilde{y}(t) \exp(j(\omega_0 + \omega_1)t) \\ &\quad + \tilde{x}(t) \tilde{y}^*(t) \exp(j(\omega_0 - \omega_1)t) \}. \end{aligned}$$

Normally one beats down, so the complex amplitude of the difference frequency term is $\frac{1}{2} \tilde{x}(t) \tilde{y}^*(t)$.

When filtering $x(t)$ with $h(t)$ to yield $y(t)$, one normally expresses this as

$$y(t) = \int_{-\infty}^{\infty} x(\tau) h(t-\tau) d\tau.$$

In complex amplitude notation

$$\begin{aligned} y(t) &= \int_{-\infty}^{\infty} \text{Re} \{ \tilde{x}(\tau) \exp(j \omega_0 \tau) \} \text{Re} \{ \hat{h}(t-\tau) \exp(j \omega_1 (t-\tau)) \} d\tau \\ &= \frac{1}{2} \text{Re} \{ \int_{-\infty}^{\infty} \tilde{x}(\tau) \hat{h}(t-\tau) \exp(j(\omega_0 - \omega_1)\tau) \exp(j \omega_1 t) d\tau \} \\ &\quad + \frac{1}{2} \text{Re} \{ \int_{-\infty}^{\infty} \tilde{x}(\tau) \hat{h}^*(t-\tau) \exp(j(\omega_0 + \omega_1)\tau) \exp(-j \omega_1 t) d\tau \}. \end{aligned}$$

Normally, $x(t)$ and $h(t)$ are referenced to the same frequency, so that

$$y(t) = \frac{1}{2} \operatorname{Re} \left\{ \exp(j\omega t) \int_{-\infty}^{\infty} \hat{x}(\tau) \hat{h}(t-\tau) d\tau \right\} \\ + \frac{1}{2} \operatorname{Re} \left\{ \exp(-j\omega t) \int_{-\infty}^{\infty} \hat{x}(\tau) \hat{h}^*(t-\tau) \exp(2j\omega t) d\tau \right\}.$$

When the bandwidths of the signal and the filter are narrow compared to the center frequency, one may neglect the second term, so

$$\hat{y}(t) = \frac{1}{2} \int_{-\infty}^{\infty} \hat{x}(\tau) \hat{h}(t-\tau) d\tau.$$

Finally, when the carrier is zero, to represent baseband signals,

$$\hat{y}(t) = \int_{-\infty}^{\infty} \hat{x}(\tau) \hat{h}(t-\tau) d\tau.$$

Figure I-1 illustrates the usage of complex amplitudes in the simulation. The input has the signal amplitude M_0 and phase θ_1 plus noise θ_n . This represents the radio frequency, and is beat down by the first mixer to intermediate frequency by straightforward multiplication. After filtering, the extraneous phase is represented by ϕ , with M_f representing the filtered amplitude. The real part of the signal from the phase detector is just the amplitude times the sine of the phase. Similarly the real part of the signal from the coherent amplitude detector is just the negative of the amplitude times the cosine of the phase.

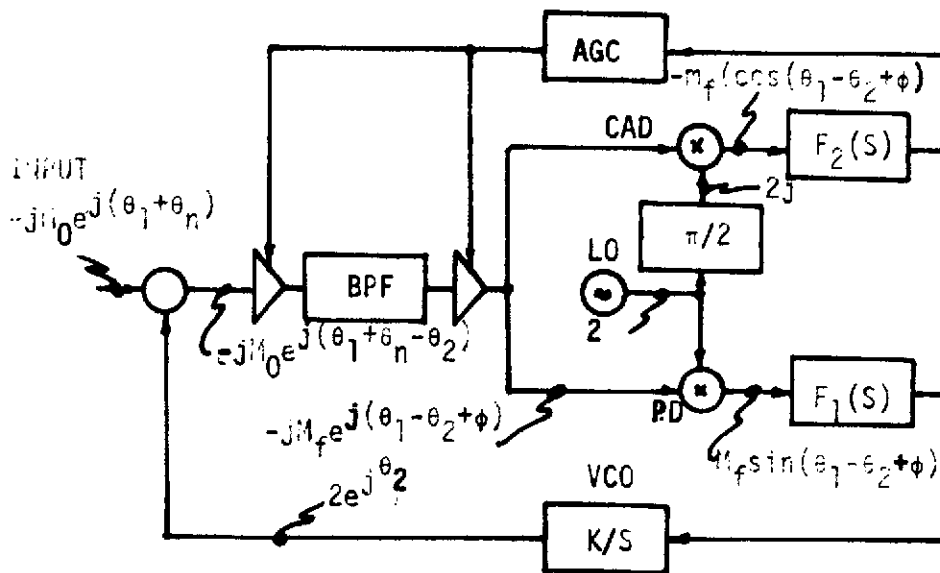


FIGURE I-1
COMPLEX AMPLITUDE USAGE

APPENDIX II
SCINTILLATION FILTERING

ABSTRACT: A tapped delay line filter is presented to represent atmospheric scintillation effects. Data is given to show the aliasing effects of the truncation.

1. Introduction - It is well known that atmospheric turbulence, herein defined as variations in the complex dielectric constant, can cause variation in the amplitude and phase of a received electromagnetic wave. From Tatarski in Ref (A2-1), the power spectral densities of the amplitude and the phase is proportional to the $-8/3$ power of the frequency above cutoff. This assumes the Kolmogorov form of the turbulent flow. The nature of the fluctuations is different however for amplitude and phase; amplitude fluctuations being dominated by the microscale of the turbulence, and phase fluctuations being dominated by the macroscale of the turbulence.

According to Ames Research Center RFP, the atmospheric effects can be adequately modeled by assuming the amplitude effects of the form

$$A(t) = A_0(1 + x(t))$$

where $x(t)$ is a Gaussian process of zero mean and a root variance of 0.23, low pass filtered with a cutoff of 2.0 Hertz and a $f^{-4/3}$ roll off (note herein the signal is a voltage term). Similarly, the phase effects could be modeled as

$$\theta(t) = \theta_0 + \theta_1 t + \theta_2 t^2 + s(t)$$

where $s(t)$ is a Gaussian process of zero mean and a root variance of 0.47, low pass filtered with a cutoff of 0.2 Hertz and a $-4/3$ roll off.

This note presents the digital form these filters will take.

2. Filter Form - In electrical engineering terms the transfer function of the filter is

$$F(s) = (a/(s+a))^{4/3},$$

where a is the cutoff frequency in radians, and s is $j\omega$.

By simple algebra, the corner is then

$$\omega/a = (2^{3/4} - 1)^{1/2} = .8257074727,$$

or for amplitude $a_x = 15.21891351$

and for phase $a_s = 1.521891351$.

The Laplace transform of the impulse response from Ref (A2-2), is

$$h(t) = [a^{4/3}/\Gamma(4/3)]t^{1/3}\exp(-at),$$

and $\Gamma(4/3) = .892979511$.

For t of zero or infinity of course

$$\begin{aligned} h(t) \Big|_{t=0} &= 0 \\ h(t) \Big|_{t=\infty} &= 0 \end{aligned}$$

The function has a maxima at

$$\begin{aligned} dh(t)/dt \Big| &= 0 \\ t &= \frac{1}{3a} \end{aligned}$$

The impulse response is shown in Figure II-1.

3. Z Transform - The quickest computational form of a filter is generally the Z transform (Ref (A2-3)). This is just the Laplace transform with the substitution:

$$z = \exp(sT)$$

Utilizing the simplest interpolator, zero order hold, the discrete transform is

$$(1 - z^{-1}) Z \left(\frac{1}{s} F(s) \right).$$

Since for the case in question

$$\mathcal{L}((a/(s+a))^{4/3}) = a^{4/3} \Gamma^{-1}(4/3) t^{-1/3} e^{-at},$$

then $\mathcal{L}\left(\frac{1}{s}F(s)\right) = \int_0^t a^{4/3} \Gamma^{-1}(4/3) t^{-1/3} e^{-at} dt = f(t)$

and by definition

$$Z\left(\frac{1}{s}F(s)\right) = \sum_{n=0}^{\infty} f(nt)z^{-n}$$

Thus

$$Z\left(\frac{1}{s}F(s)\right) = \sum_{n=0}^{\infty} \{a^{4/3} \Gamma^{-1}(4/3) \int_0^t (nT)^{-1/3} e^{-ant} d(nT)\} z^{-n}$$

From Abramowitz and Stegun, Ref (A2-2), the above incomplete gamma function can be written as a Chi-Squared function, or

$$Z\left(\frac{1}{s}F(s)\right) = \sum_{n=0}^{\infty} \{P(2ant | \frac{8}{3})\} z^{-n},$$

Then the complete transform is

$$\begin{aligned} (1-z^{-1}) Z\left(\frac{1}{s}F(s)\right) &= (1-z^{-1}) \left\{ \sum_{n=0}^{\infty} P(2anT | \frac{8}{3}) z^{-n} \right\} \\ &= P(0 | \frac{8}{3}) z^{-0} + P(2aT | \frac{8}{3}) z^{-1} + P(4aT | \frac{8}{3}) z^{-2} + \dots \\ &\quad - P(2aT | \frac{8}{3}) z^{-2} - P(4aT | \frac{8}{3}) z^{-3} - \dots \\ &= 0 + P(2aT | \frac{8}{3}) z^{-1} + \{P(4aT | \frac{8}{3}) - P(2aT | \frac{8}{3})\} z^{-2} \\ &\quad + \{P(6aT | \frac{8}{3}) - P(4aT | \frac{8}{3})\} z^{-3} \\ &\quad + \dots \end{aligned}$$

The output ϕ for the input I is then

$$\begin{aligned} \phi &= P(2aT | \frac{8}{3}) I((n-1)T) + \{P(4aT | \frac{8}{3}) - P(2aT | \frac{8}{3})\} I((n-2)T) \\ &\quad + \{P(6aT | \frac{8}{3}) - P(4aT | \frac{8}{3})\} I((n-3)T) \\ &\quad + \dots \end{aligned}$$

Since there appears to be no more concise form, at least to the writer, in this case it appears that the Z transform is no better than a conventional delay line representation. Also, since the Chi-Squared function is evaluated as a series,

$$P(\chi^2 | \nu) = \Gamma^{-1}(\nu/2) \sum_{n=0}^{\infty} \frac{(-1)^n (\chi^2/2)^{\frac{\nu}{2} + n}}{n! (\frac{\nu}{2} + n)},$$

the conventional delay line representation appears preferable.

4. Delay Line - There are two design parameters which must be set when representing a filter as a tapped delay line: the tap spacing, T, and the line length, NT. The former describes the "graininess" of the impulse response, and effectively defines the highest frequency represented,

$$f_m = a/(2\gamma) = Kf_b/\gamma$$

Therein $T = \gamma/a$,

f_b is the corner frequency, and for the 4/3 filter

$$K = 3.804728378.$$

The latter describes the fold over aliasing, and effectively defines the lowest frequency (excluding zero) represented,

$$f_L = 1/(NT)$$

As a rule of thumb, the maximum tap contribution, Th(t), should be of the order of 0.1, or

$$T \approx (0.1)^{3/4} \Gamma(4/3) / (ae^{-1/3}) \\ \approx .179740828/a .$$

Similarly, the "length" should sum to 0.95 to 0.99, i.e., for the filter in question

$$P(2aNT | \frac{8}{3}) = a^{4/3} \Gamma^{-1}(4/3) \int_0^{\tau=2aNT} \left(\frac{\tau}{2a}\right)^{1/3} e^{-\frac{\tau}{2a}} \frac{1}{2a} d\tau,$$

where $\tau = nT = \tau/(2a)$.

The function is plotted in Figure II-2. From the figure it appears that a length 2aNT of 8 to 10 should be adequate, or for 10,

$$NT = (\chi^2 = 10)/2a = 5/a .$$

Figures II-3 and II-4 illustrate the amplitude and phase response of three delay lines: $T = .1707/a$, $N = 32$; $T = .09/a$, $N = 64$ and $T = .09/a$, $N = 128$. The magnitude of the error is shown in Figure II-5. The number of taps shown are integer powers of two for convenience in the fast Fourier transform. The rule of thumb filter, $T = .17/a$, $N = 32$ appears quite reasonable to an octave beyond the corner, after which the phase response falls off quickly. The second filter, $T = .09/a$, $N = 64$ is approximately the same length as the first, but with twice the resolution. This filter holds the correct phase response to two octaves beyond the corner. The third filter, $T = .09/a$, $N = 128$ has the same resolution as the second but has twice the length. It shows very little improvement over the second filter.

5. Conclusion - A model for turbulence effects on propagation has been reviewed, and a digital representation designed. The design is summarized in Figure II-6. The magnitude of the amplitude error is less than 1.5% over a decade of frequency beyond the corner.

Reference

- A2-1 - V. I. Tatarski, "The Effects of Turbulent Atmosphere on Wave Propagation", NSF TT-68-50464, 1971.
- A2-2 - C. Abramowitz and I. A. Stegun, "Handbook of Mathematical Functions", NBS App. Math Se. 55, Dec. 1965.
- A2-3 - J. D. Markel, "Z Transform Applications Using Digital Computers", Engineering Technology, Dec. 1968.

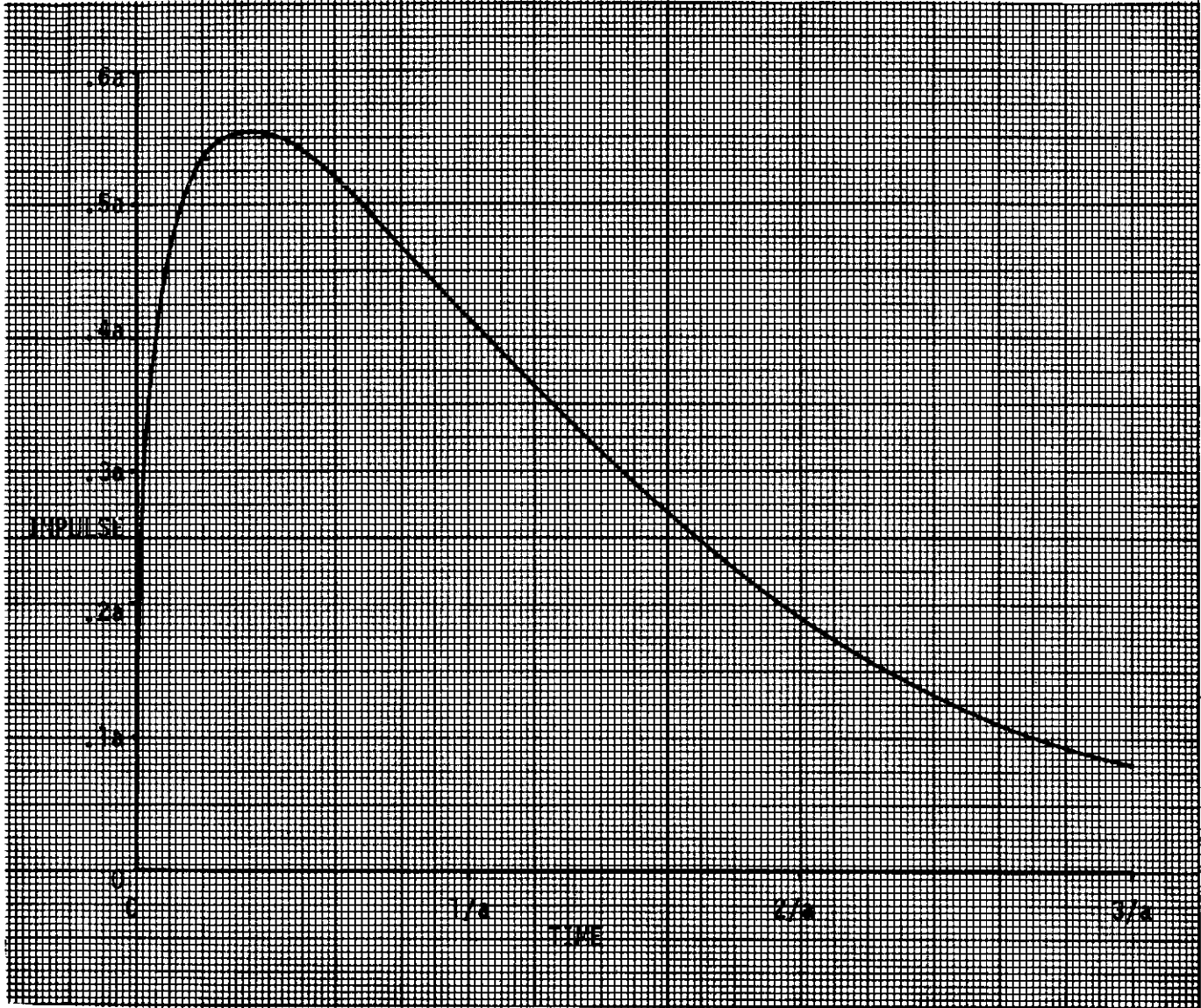


FIGURE II-1
 IMPULSE RESPONSE
 OF $(a/(s+a))^{4/3}$

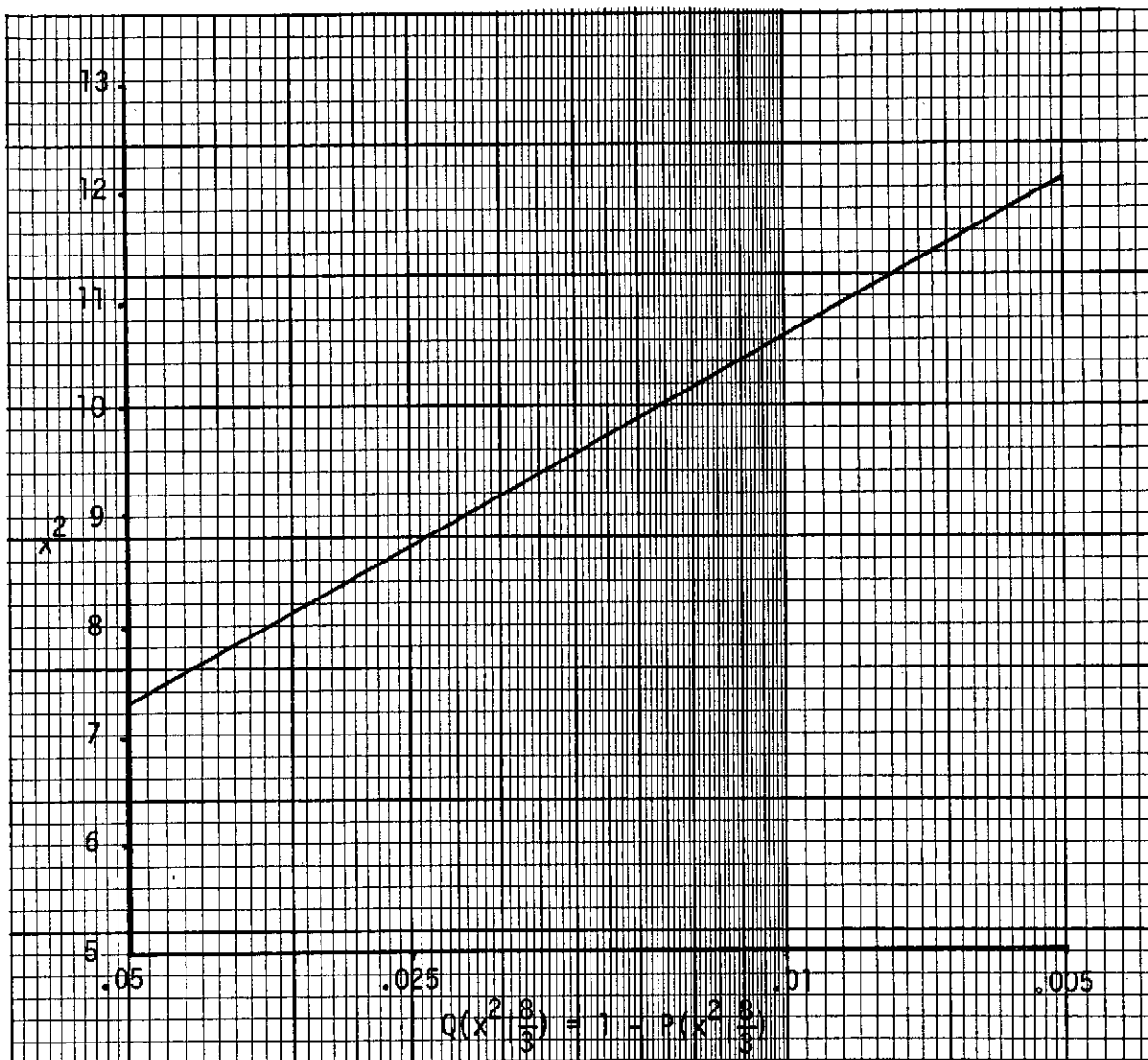
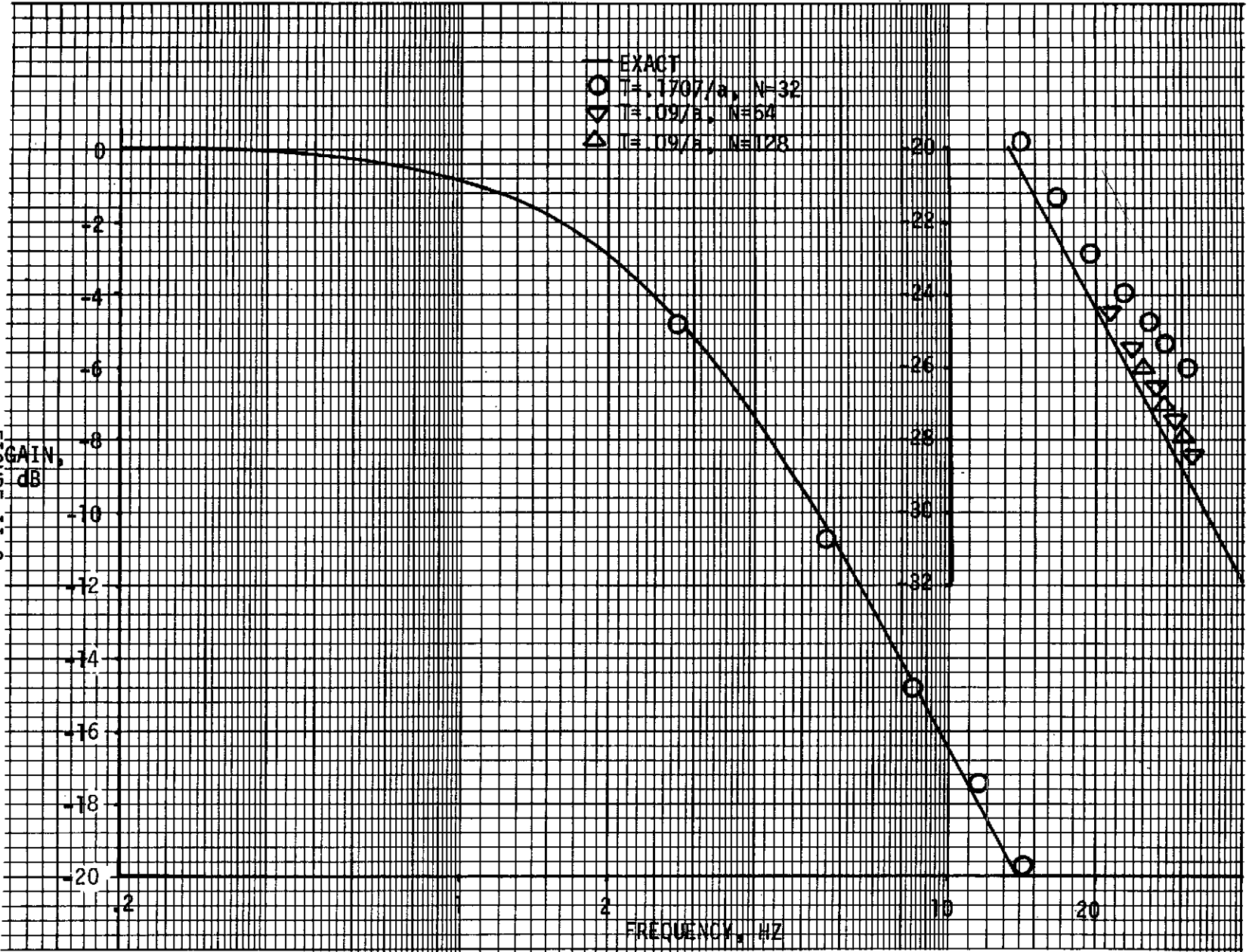


FIGURE II-2
LINE LENGTH APPROXIMATION

AMPLITUDE RESPONSE

FIGURE 11-3



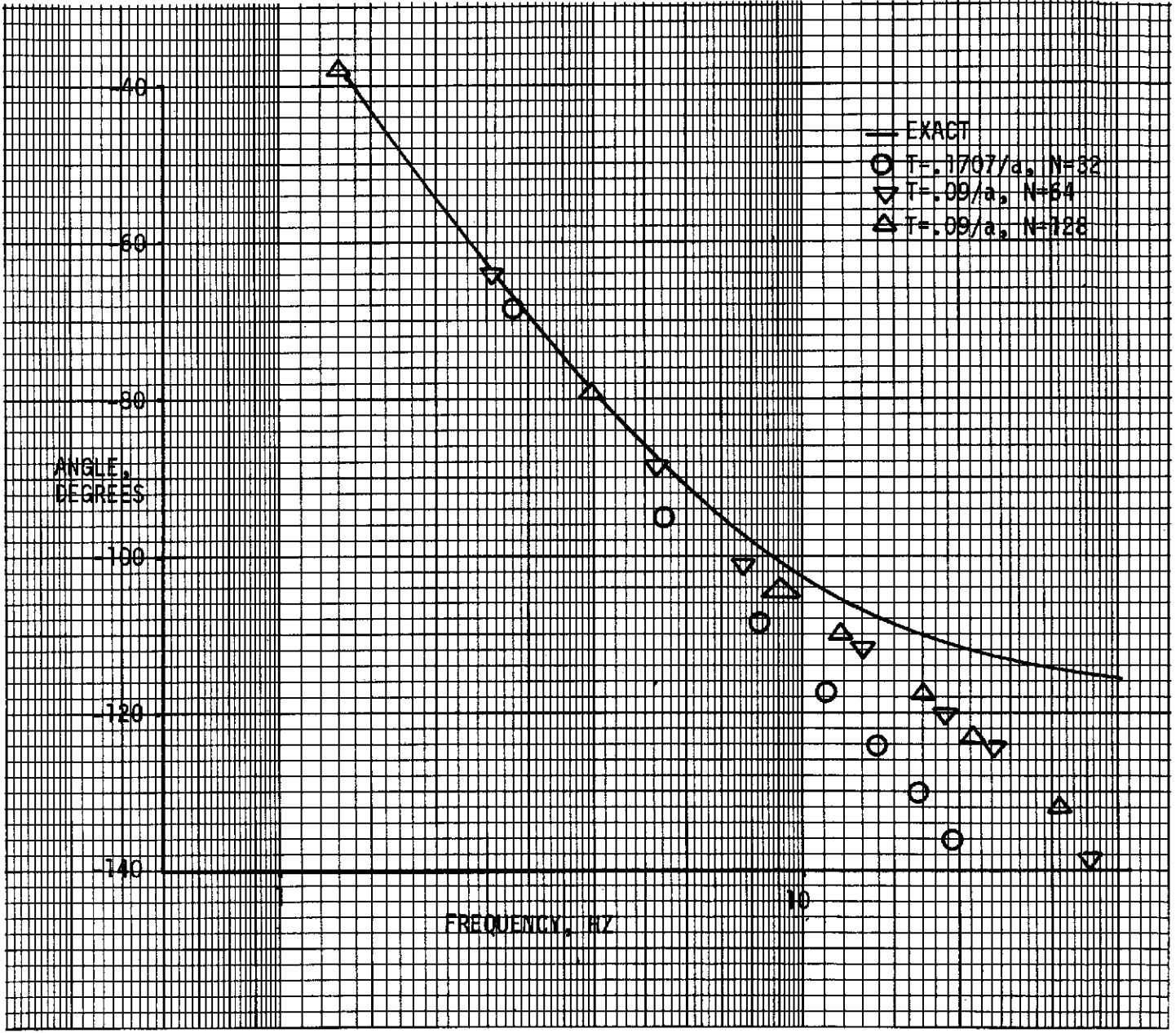


FIGURE II-4
PHASE RESPONSE

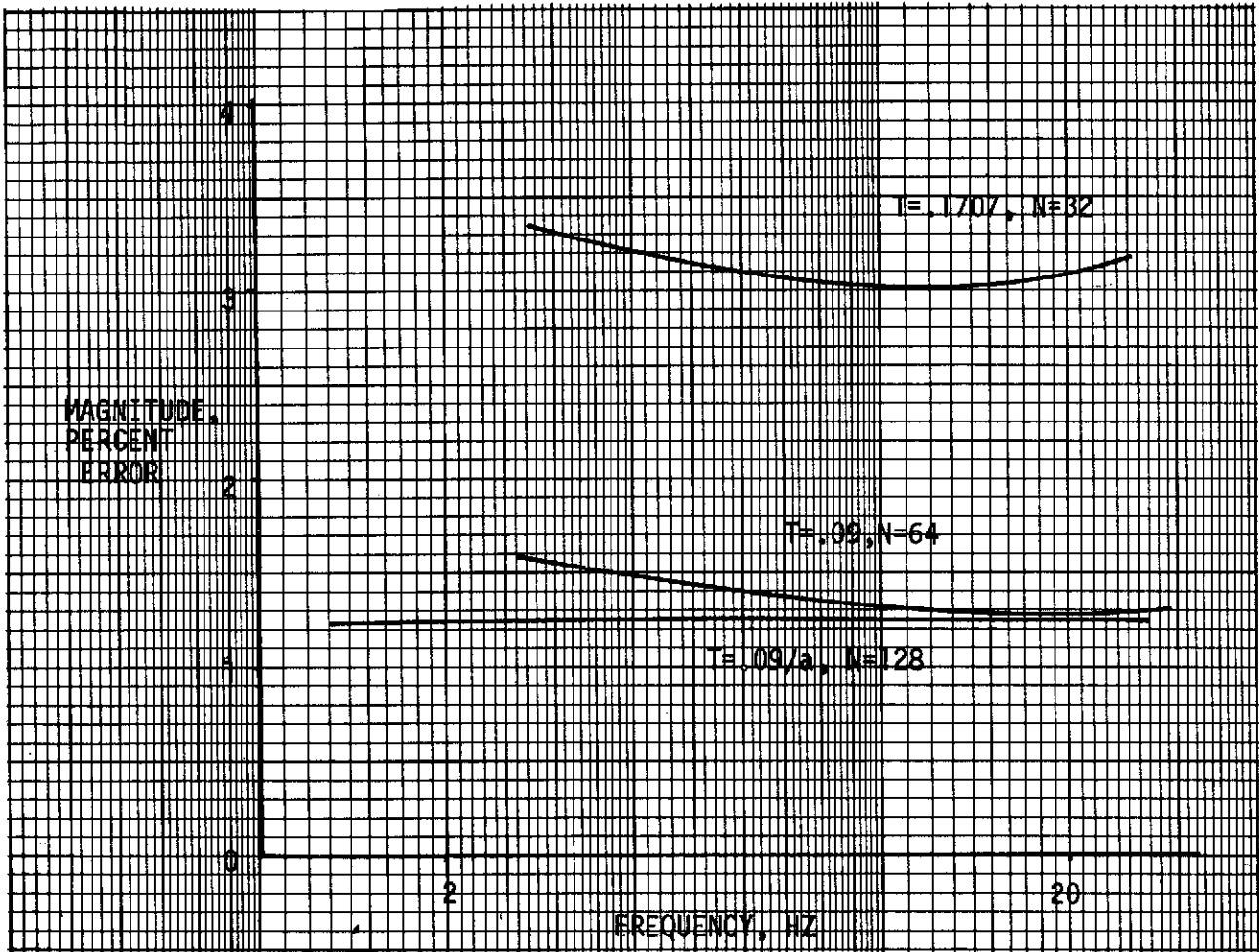
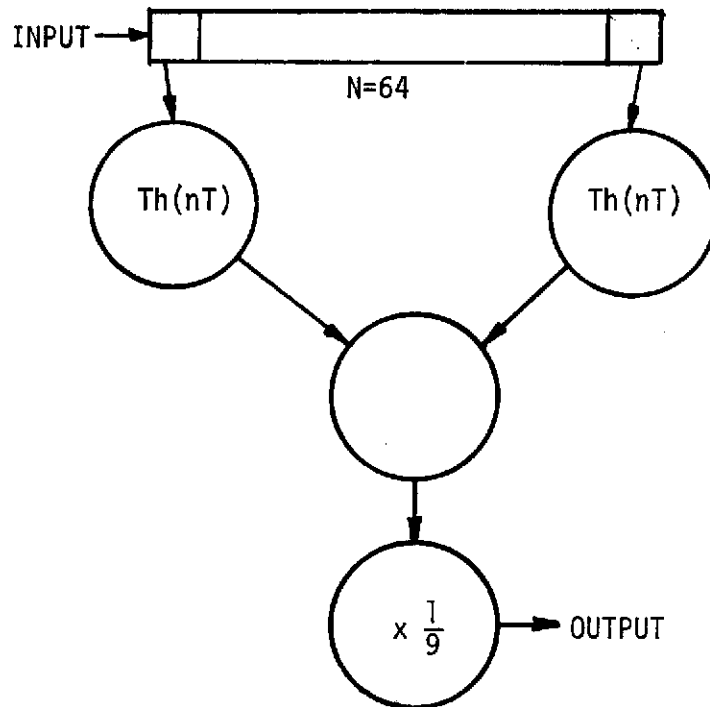


FIGURE II-5
TRUNCATION ERROR



$$\text{Th}(nT) = \gamma \Gamma^{-1} (4/3) (n\gamma)^{1/3} \exp(-n\gamma)$$

$$\gamma = .09$$

$$g = .9807$$

FIGURE II-6
TAPPED DELAY LINE FILTER

APPENDIX III

QUANTIZING STRATEGY FOR INPUTS TO VA DECODERS

1. A Viterbi Algorithm (VA) decoder can function with either hard or soft decisions on the input symbols. Typically, the use of 8 level soft decisions on the symbols permits the decoder to operate satisfactorily with ~ 2 dB less E_b/N_0 than if hard decisions are employed. The normally used quantizing strategy results in quantization level spacings of about 0.5 to 0.7 times the standard deviation of the channel noise. This memo explores the derivation of a rationale for choosing the spacings based on the mean and variance of the received symbols. The selected spacings are found to vary between ~ 0.58 and 0.64 for means between 1. and 2. sigmas. (3 to 9dB E_b/N_0). These results are equally applicable to a sequential decoder.

2. Theory of VA decoder operation

The VA decoder is a device which chooses the most likely state sequence of the encoded data from the set of possible state sequences. The formal statements of this principle are adequately covered in the published literature. The basic operating technique is to associate a path metric with each state sequence which allows the decoder to select the maximum likelihood state sequence, based on a set of observations. The path metric, τ , is formally defined as $-\ln \Pr\{\bar{X}|\bar{Z}\}$, where \bar{X} is the set of observations, and \bar{Z} is the state sequence. For a memoryless, binary symmetric channel, with Gaussian noise statistics, the path metrics can be simply the sum of the observations, weighted by the expected observation, given the state sequence for the specific path metric. In simpler terms, if $M (= +1)$ is the expected symbol at a given point in time, then $\tau_k(i) = \tau_k(i-1) - X_i M_i$, where $\tau_k(i)$ is the K th path metric at time i . The state sequence with the smallest path metric is the maximum likelihood state sequence.

Any two state sequences will have a number of expected symbols which have the same sense, and a number of expected symbols with the opposite sense. If one of these state sequences is the correct state sequence, then $D_{k,j}(i) = \tau_k(i) - \tau_j(i)$ will be less than zero unless $\sum_i X_i M_i < 0$, where the set, i , includes only those observations where the state sequences differ in interpretation. For the correct path, $E\{X_i M_i\} = \eta_x$.

Clearly, if X is a normal random variable, then $\Delta_{K,J}(i)$ is also a normal random variable, with a mean $\eta_\Delta = N\eta_x$, and $\sigma_\Delta^2 = N\sigma_x^2$, where N is the number of observations contributing to the decision. Then, at any point, an error is committed only if $\Delta_{K,J}(i) > 0$, which would occur with probability $Q(\eta_x \sqrt{N}/\sigma_x)$ given N pertinent observations. While this cannot be used to directly predict the decoder performance, it can be used to predict the degradation in performance when X is not normally distributed.

3. Quantization

When the symbols are quantized prior to decoding, the X's are no longer normally distributed, since they take only integer values, and finite range, linear quantization results in significant population groups in only a few values of X. Consider the quantization strategy shown in Figure III-1. We have arbitrarily assigned integer values to Z, the quantized estimate of X. If X is a normal random variable with mean η_X and unit variance, then the probability distribution of Z is given by,

$$\begin{aligned} \Pr\{Z = -7\} &= Q(\eta_X + 3a) \\ \Pr\{Z = -5\} &= Q(\eta_X + 2a) - Q(\eta_X + 3a) \\ \Pr\{Z = -3\} &= Q(\eta_X + a) - Q(\eta_X + 2a) \\ \Pr\{Z = +5\} &= Q(\eta_X - 3a) - Q(\eta_X - 2a) \\ \Pr\{Z = +7\} &= 1 - Q(\eta_X - 3a) \end{aligned}$$

where $Q(X) = \frac{1}{\sigma_X \sqrt{2\pi}} \int_X^\infty \exp\left(-\frac{(t-\eta_X)^2}{2\sigma_X^2}\right) dt$ and "a" is the quantization level.

It is rather awkward to compute the probability that $\Delta > 0$ directly, since the probability distribution of Δ is the result of N convolutions. A more useful approach is to use a Chernov bounds. In this case, we derive these bounds using the Laplace transform of the probability distribution of Z, proceeding as follows:

$$\phi_Z(S) = \sum_{J=1}^8 \Pr\{Z = 2J-9\} e^{S(2J-9)}$$

Since convolution in normal space is simply a product in transform space, the transform of the probability distribution of Δ is,

$$\phi_\Delta(S) = [\phi_Z(S)]^N$$

$$\text{Let } \psi_\Delta(S) = \ln \phi_\Delta(S)$$

$$\psi_\Delta(S) = N \ln \left[\sum_{J=1}^8 \Pr\{Z = 2J-9\} e^{S(2J-9)} \right]$$

$$\psi_\Delta(S) = \frac{d\psi_\Delta(S)}{dS} = \frac{N \sum_{J=1}^8 (2J-9) \Pr\{Z=2J-9\} e^{S(2J-9)}}{\sum_{J=1}^8 \Pr\{Z=2J-9\} e^{S(2J-9)}}$$

Now, the Chernov bound can be expressed,

$$\Pr\{\Delta > 0\} \leq e^{\psi_\Delta(S)} \Big|_{\psi_\Delta'(S)=0}$$

Thus, we need to solve for the value of S such that,

$$\sum_{J=1}^8 (2J-9) \Pr\{Z=2J-9\} e^{S(2J-9)} = 0$$

This can be solved numerically, and a value for $\Pr\{\Delta>0\}$ found for any N. Note, however, that

$$\Pr\{\Delta>0\} \leq [e^{\psi_Z(S)}]^N \quad \left| \quad \psi_Z'(S) = 0 \right.$$

Thus, we need only solve for the case $N=1$, and find the value of "a" which minimized $\Pr\{\Delta>0\} \Big|_{N=1}$. For the case $\eta_x = 2\sigma_x$, which is one of the conditions of interest, the variation of $\Pr\{\Delta>0\}$ with "a" is shown in Figure III-2. We can clearly see that varying "a" over rather broad limits does not change the probability value greatly, however, the optimum is clearly in the vicinity of $a = .62\sigma_x$.

Figure III-3 illustrates the same information over a wider range of mean to standard deviation.

Now, we note that there is a hazard in using any bound to draw a conclusion of this nature, since varying the parameter "a" may result in variations in the relative tightness of the bound which could be on the order of the variations in the results. Thus, if our conclusions were at significant variance with empirical data, it would be necessary to use a more sophisticated approach to eliminate the uncertainty resulting from the use of bounds. However, the fact that the empirical data is in close agreement with the predicted results, and that the optimum is rather broad, suggests that the increased sophistication is unnecessary.

4. Conclusions

It has been shown that the criteria of minimizing the Chernov bounding value of $\Pr\{\Delta>0\}$ leads to a choice of quantization level of $\sim 0.6\sigma_x$, which is halfway between the empirically determined values of 0.5 to $0.7\sigma_x$.

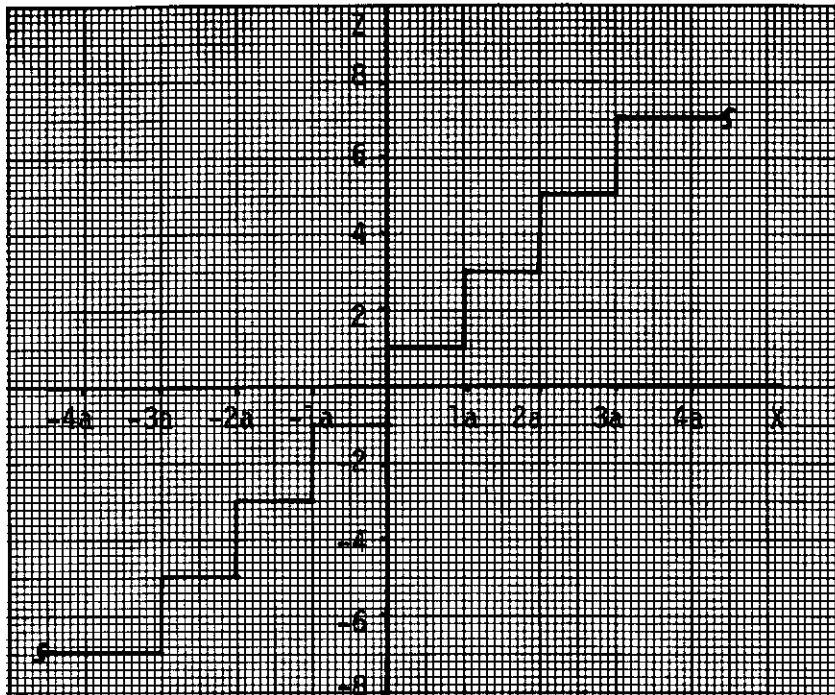


FIGURE III-1
QUANTIZATION SCHEME

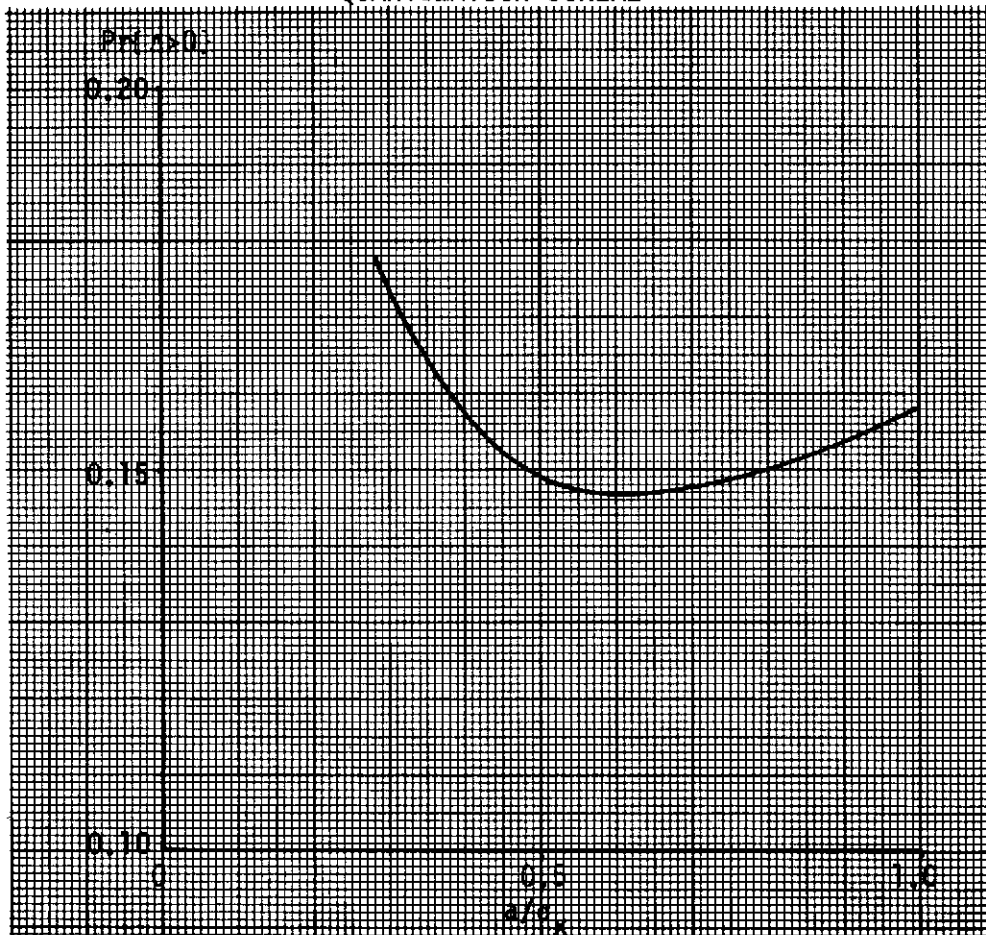


FIGURE III-2
BOUND ON $\text{Pr} \{ \Delta > 0 \}$ VS QUANTIZATION LEVEL

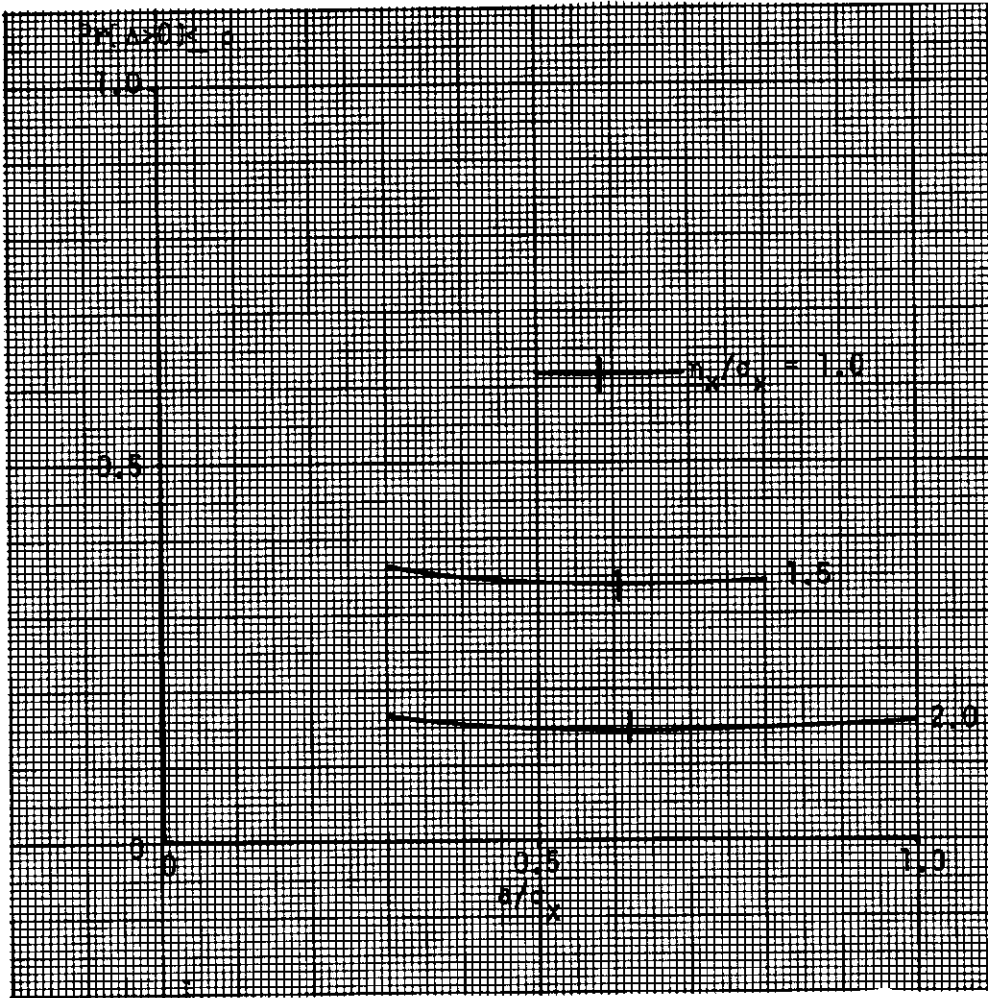


FIGURE III-3
EFFECT OF VARYING MEAN ON
CHOICE OF QUANTIZATION LEVEL

APPENDIX IV
LIST OF SYMBOLS
(Input Symbols)

ASOFT	Soft decision quantization reference
BIF	IF Bandwidth
BL2	$2 B_{LO}$ (AFC)
DELFF	Delta frequency
DYNR	Dynamic range of AGC below "minimum" signal
ENODB	Energy to noise density in decibels
FLO	LO detune
FQDPRT	Frequency Doppler rate
FRQDOP	Frequency Doppler
I1	Random generator number
I11	Random generator number
I2	Random generator number
I22	Random generator number
NSLICE	Phase of bit synchronizer sample data filter
SDAMP	Gam of amplitude scintillation
SDPHA	Gam of phase scintillation
SVRHZ	Sweep slope in Hertz
SWNM	Sweep minimum
SWMX	Sweep maximum
TL	Threshold

(All Symbols)

A	Signal voltage
AAMP	Normalized amplitude scintillation
ACOR	Scintillation normalization
ACQ	Number of true acquisitions
ACTH1	$A \cos(\text{TH1})$
AFAL	Number of false acquisitions
ADB	A dropped bit
ADOA	Average number of bits in a dropout
ADOS	Standard deviation of number of bits per dropout
AGC	AGC gain function
AK	AFC Loop gain
AKOU	KDATA at acquisition
AKBMIN	Bit synchronizer AK minimum
AMIN	Minimum A to AFC
AMIN2	$\text{AMIN}/\text{SQRT}(2)$
AMIN3	AMIN for dynamic range
AMISS	Number of missed acquisitions
APHA	Normalized phase scintillation
ASOFT	Soft decision quantization reference
ASOFTI	Soft decision quantization slope
ASTH1	$A \sin(\text{TH1})$
AVEES	Average ES
A5	Baseline connection filter gain
BAMP	Amplitude scintillation approximation intercept
BIF	IF Bandwidth
BL2	$2 B_{L0}$ (AFC)
BL2B	$2 B_{L0}$ (bit synchronizer)
BPER	Bit period
BPHA	Phase scintillation approximation intercept
BRATE	Bit rate
CAMP	Complex amplitude into BIF
CBINI	Hits in SBINSI

CBIN2	Hits in SBINS2
CBIN3	Hits in SBINS3
CBIN4	Hits in SBINS4
CB1	Bit synchronizer Z transform constant 1
CB2	Bit synchronizer Z transform constant 2
CB3	Bit synchronizer Z transform constant 3
CCL	Control function for scintillation subroutines
CCLT	Control function for TRIG subroutine
CCOUT	Output of last IF amplifier
CDTHX	Cos (DTHX)
CDTH1	Cos (DTH1)
CFILT	IF filter output
COUT	CCOUT
CSCIN	Cos (YP)
CTHX	Cos (THX)
CTH1	Cos (TH1)
CTH2	Cos (TH2)
C1	AFC filter Z Transform constant 1
C2	AFC filter Z transform constant 2
C3	AFC filter Z transform constant 3
C4	Normalized AFC VCO gain
C5	AGC Z transform constant 1
C5DP	Doppler Z transform constant 1
C5MH	Baseline Z transform constant 1
C5MS	Sampling Z transform constant 1 (word "sampling" is synonymous with
C6	AGC Z transform constant 2 word "slice" in computer listings)
C6DP	Doppler Z transform constant 2
C6MH	Baseline Z transform constant 2
C6MS	Sampling Z transform constant 2
DELF	Delta frequency
DES	DT*SVR
DT	Delta time
DTHX	Delta THX
DTH1	Delta TH1

DYNR	Dynamic range of AGC below "minimum" signal
E	Voltage into AFC filter
EDOP	Doppler voltage
EDOPR	Doppler rate voltage
EDOPRX	Doppler plus Doppler rate voltage
ENO	Energy to noise density
ENODB	ENO in decibels
ENOM	Minimum ENO
ENOMIN	ENOM in decibels
ERR	Error count
ERRM	Error spacing matrix
ES	Sweep voltage
EV	Voltage from AFC filter
EVMAX	Maximum sweep voltage
EVMIN	Minimum sweep voltage
EVO	Last EV
EV1	Voltage after Doppler addition
EV1C	Voltage into bit synchronizer
EV1O	Last EV1
EV1OC	Last EV1C
E0	Last E
FBAMP	Amplitude scintillation filter corner
FBPHA	Phase scintillation filter corner
FDIFF	AFC pull in
FDIFFB	Bit synchronizer pull in
FIDO	Float (ID0)
FLO	LO detune
FQDPRT	Frequency Doppler rate
FRQDOP	Frequency Doppler
FVCOB	Frequency VCO bit synchronizer
GAM43	Scintillation filter tap spacing target
GAM43A	GAM43 for amplitude
GAM43P	GAM43 for phase
G1	First IF amplifier gain

G2	Second IF amplifier gain
I	Dummy index
IAMP	Amplitude scintillation counter
IAMPC	Phase scintillation counter
IBIT	Phase of bit synchronizer
IDATA	Current bit
IDATA0	Last IDATA
IDATAW	Last IDATA0
IDLBIT	Number of output bits before error count
IDO	Number of dropouts
IDON	IDO counter
IERRSP	Error space
IH	Histogram bin
IHOLD	In phase bit synchronizer level
IHOLD1	Last IHOLD
ILOC	Counter, bits to lock
ILOCF	Final ILOC
IMS	Hard decision from sampling filter
INIT	Control function for BIFILT subroutine
IPHA	Phase scintillation counter
IPHAC	Amplitude scintillation counter
IX	Bin of soft decision
IXM	Last IX
I1	Random generator number
I1S	I1 to start
I11	I1 for scintillation
I11S	I11 to start
I2	Random generator number
I2S	I2 to start
I22	I2 for scintillation
I22S	I22 to start
J	Counter for samples per bit
K	AFC VCO gain
KB	Bit synchronizer VCO gain

KDATA	Counter of IDATA
KOUNT	Counter of IMS
NACQ	Counter of NACQT trials
NACQT	Number of acquisition
NBIT	Phase of IBIT to dump in phase integrator
NBIT2	Phase of IBIT to dump quadrature integrator
NC	Quadrature noise
NRUNS	Number of bits per run
NS	Quadrature noise
NSLICE	Phase of IBIT to sample data filter
NSPB	Number of samples per bit
NO	Noise density
N43	Number of scintillation filter taps
OMC	Baseband equivalent of IF in radians
PACQ	Probability of acquisition
PFAL	Probability of false acquisition
PE	Probability of error
PEAK	Peak voltage from sampling filter
PHIB	Steady state bit synchronizer phase error
PHIDEG	Steady state AFC phase error
PHISS	PHIB in radians
PHISSB	PHIDEG in radians
PI	π
PI2	2π
PMISS	Probability of missed acquisition
PKAV	Average of IBIT when PEAK occurs
PKSD	Standard deviation of IBIT when PEAK occurs
QERR	Voltage to bit synchronizer filter
QERRO	Last QERR
QV	Voltage from bit synchronizer filter
SBINS1	Probability matrix for -1-1 input
SBINS2	Probability matrix for +1-1 input
SBINS3	Probability matrix for -1+1 input
SBINS4	Probability matrix for +1+1 input

SDAMP	Gain of amplitude scintillation
SDPHA	Gain of phase scintillation
SDTHX	Sin (DTHX)
SDTH0	Sin (DTH0)
SDTH1	Sin (DTH1)
SIG	Normalized noise
SKOU	Standard deviation of acquisition at KDATA
SLOA	Amplitude scintillation approximation slope
SLOP	Phase scintillation approximation slope
SLSIG	Standard deviation of sampling output
SLSUM	Mean of sampling output
SSCIN	Sin (YP)
STDEV	Standard deviation of measurement
STHX	Sin (THX)
STH1	Sin (TH1)
STH2	Sin (TH2)
SVR	Sweep slope
SVRHZ	SVR in hertz
SWMN	Sweep minimum
SWMX	Sweep maximum
TAUB1	Bit synchronizer filter constant 1
TAUB2	Bit synchronizer filter constant 2
TAU1	AFC filter constant 1
TAU2	AFC filter constant 2
TAU3	AGC filter constant
TAU4	Sample filter constant
TAU5	Baseline filter constant
TAU6	Doppler filter constant
TEMP	Temporary dummy
TH2	Phase angle from AFC VCO
TL	Threshold
TSYNC	Period of bit synchronizer VCO
U	Voltage into AGC filter
UMH	Voltage into baseline filter

V	Voltage from AGC filter
VD	Limited version of V
VDP	Voltage from doppler filter
VHIST	V histogram
VMH	Voltage from baseline filter
VMS	Voltage from sampling filter
VMSS	VMS at sampling time
VMSO	Last VMS
VSQRT	Square root of VD
WN	AFC loop natural frequency
WNB	Bit synchronizer natural frequency
X	Dummy
XI	In phase integrator voltage
XIBIT	Random starter for IBIT
XIO	Last XI
XIOO	Last XIO
XISIG	Standard deviation of in phase integrator
XISUM	Mean of in phase integrator
XQ	Quadrature integrator voltage
XQO	Last XQ
YA	Scintillation amplitude
YP	Scintillation phase
ZETA	AFC damping factor
ZETAB	Bit synchronizer damping factor

APPENDIX V
ERROR RATE
COMPUTER SOFTWARE

```

PROGRAM CARL(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)
000003 COMPLEX CAMP(4),CFILT(4),COUT,CCOUT
000003 REAL NS,NC,N0,K,KB
000003 DIMENSION SBINS1(8,8),SBINS2(8,8),SBINS3(8,8),SBINS4(8,8)
000003 DIMENSION ADB(100)
000003 DIMENSION F1(8),F2(8)
000003 DIMENSION ERRM(100)
000003 DATA FBAMP,FBPHA,SDAMP,SDPHA,N0/2.,.2,.23,.47,1./
000003 DATA GAM43,N43/.09,64/
000003 DATA ENODB,BRATE,ENOMIN/8.,88.,9./
000003 DATA DELF,NSPB,NRUNS,BIF/62.,40,10,1000./
000003 DATA BL2,PHIDEG,FDIFF/176.,10.,342.433/
000003 DATA BL2B,PHIB,FDIFFB/1.,10.,5./
000003 DATA I1,I2,I11,I22,NSLICE/1,1,1,1,24/
000003 DATA FRQDOP,FQDPRT,TL,AGC/0.,0.,-2.6,1./
000003 DATA TAU3,ASOFT/.07957,.2474/
000003 DATA TAU4,TAU5,TAU6,A5,FLO/.001808,.01808,.10603,.5,0./
000003 DATA SVRHZ,SHMX,SHMN/2.2E3,28.15E3,6.85E3/
000003 DATA IDLBIT/20/
000003 DATA DYNR/0./
000003 NAMELIST/IN1/NRUNS,NSPB,ENODB,DELF,BIF,ENOMIN
+,BL2,PHIDEG,FDIFF,BL2B,PHIB,FDIFFB
+,FBAMP,FBPHA,SDAMP,SDPHA,GAM43,N43,NSLICE
+,FLO,FRQDOP,FQDPRT,ASOFT,I1,I2,I11,I22
+,SVRHZ,SHMX,SHMN,TL,AGC
+,IBIT,TSYNC,IDLBIT,DYNR
+,TAU4
000003 PI=4.*ATAN(1.)
000007 PI2=2.*PI
000010 ZETA=SQRT(0.5)
000013 ZETAB=ZETA
000014 CCLT=0.
000015 CALL TRIG(CCLT,PI,SSCIN,CSCIN)
000020 CCLT=1.
000022 3 CONTINUE
0 READ INPUTS
000022 READ(5,IN1)
000025 NSLICE=26
000026 CBIN1=0.
000027 CBIN2=0.
000030 CBIN3=0.
000031 CBIN4=0.
000032 ILOC=0
000033 ILOC=-1
000034 IDO=0
000035 IDON=-1
000036 FLO=10.
000037 DYNR=3.
000041 I1=1
000042 I2=1
000043 I11=1
000044 I22=1
000045 FQDPRT=10.8
000046 NRUNS=2000
000047 TL=-6.5
000051 SVRHZ=0.
000052 ASOFT=.3

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```

000053 ----- IOLBIT=100
000054 ----- ASOFTI=2./ASOFT
000056 ----- DO 199 I=1,8
000060 ----- DO 198 J=1,8
000061 ----- SBINS1(I,J)=0.
000064 ----- SBINS2(I,J)=0.
000066 ----- SBINS3(I,J)=0.
000067 ----- SBINS4(I,J)=0.
000071     198 CONTINUE
000073     199 CONTINUE
000075 ----- IXM=0.
000076 ----- CALL RANDOM(I1,I2,XIBIT)
000100 ----- IRIT=INT(39.*XIRIT+1.)
C ----- CONVERT INPUTS (EN0,BPER,PHISS,PHISSB)
000104 ----- EN0=10.** (EN0B9/10.)
000111 ----- EN0M=10.** (EN0MIN/10.)
000117 ----- BPER=1./BRATE
000121 ----- DT=BPER/NSPR
000123 ----- PHISS=PHIDEG*PI/180.
000126 ----- PHISSB=PHIB*PI/180.
000130 ----- AMIN=SQRT (EN0M*NO*BRATE)
000135 ----- AMIN2=AMIN/1.4142
000137 ----- AGC=SGRT (AMIN2)
000141 ----- AMIN3=AMIN2/SQRT (10.** (DYNR/10.))
000152 ----- A=SQRT (EN0*NO*BRATE)
C ----- CALCULATE LOOP PARAMETERS (TAU1,TAU2,K,TAUB1,TAUB2,KB)
000157 ----- WN=BL2/(ZETA+0.25/ZETA)
000162 ----- AK=PI2*FDIFF/SIN(PHISS)
000167 ----- TAU1=AK/(WN*WN)
000171 ----- TAU2=2.*(ZETA-0.5/(WN*TAU1))/WN
000176 ----- K=AK/AMIN
000200 ----- EDOF=PI2*FRQDOP/K
000202 ----- EDOFR=PI2*FQDPR*DT/K
000205 ----- EDORPX=EDOP+EDOPR
000207 ----- SVMAX=PI2*SWMX/K
000211 ----- SVMIN=-PI2*SWMN/K
000213 ----- SVR=PI2*SVRH7/K
000215 ----- WNB=BL2B/(ZETAB+0.25/ZETAB)
000220 ----- AK=PI2*FDIFFR/SIN(PHISSB)
000225 ----- TAUB1=AK/(WNB*WNB)
000227 ----- TAUB2=2.*(ZETAB-0.5/(WNB*TAUB1))/WNB
000234 ----- AKBMIN=PI2*(DELF/2.)/(K*1.4125)
000240 ----- KB=AK/AKBMIN
C ----- DEFINE CONSTANTS
000242 ----- C1=1.-DT/TAU1
000245 ----- C2=TAU2/TAU1
000246 ----- C3=C1+C2-1.
000251 ----- C4=DT*K
000253 ----- C5=DT/TAU3
000255 ----- C6=1.-C5
000256 ----- DTH1=PI*DELF*DT
000251 ----- SDTH0=SIN(DTH1)
000263 ----- CDTH1=COS(DTH1)
000265 ----- DTHX=PI2*FLO*DT
000267 ----- SDTHX=SIN(DTHX)
000272 ----- CDTHX=COS(DTHX)
000274 ----- CB1=1.-BPER/TAUB1
000277 ----- CB2=TAUB2/TAUB1

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000300      C83=C81+C82-1.
000303      C5MS=DT/TAU4
000305      C6MS=1.-C5MS
000306      C5MH=DT/TAU5
000310      C6MH=1.-C5MH
000311      C5DP=DT/TAU6
000313      C6DP=1.-C5DP
000314      SIG=0.5*SQRT(N0/DT)
C          INITIALIZE LOOPS (TH2,E0,XI,XQ,QV,QERR0,ERR)
000321      SLSUM=0.
000322      SLSIG=0.
000323      XISUM=0.
000324      XISIG=0.
000325      NBIT=8PER/DT*.5
000330      NBIT2=NBIT/2
000331      TSYNC=8PER
000332      CAMP(1)=(0.,0.)
000335      CAMP(2)=(0.,0.)
000337      CAMP(3)=(0.,0.)
000342      CFILT(1)=(0.,0.)
000344      CFILT(2)=(0.,0.)
000347      CFILT(3)=(0.,0.)
000351      INIT=0
000352      OMC=PI*BIF
000354      IDATA=-1
000355      PRINT 201,ENQDB,DELF,BIF,BL2,NSLICE,ASOFT
000375      201  FORMAT(1X,*ENQDB=*,F6.1,* ,DELF=*,F6.1,* ,BIF=*,F6.0,
* ,BL2=*,F6.0,* ,NSLICE=*,I6,* ,ASOFT=*,F5.4)
000375      PRINT 202,SVRHZ,SWMX,SWMN,FLO,FRQDOP,FQDOPRI
000415      202  FORMAT(1X,*SVRHZ=*,E12.4,* ,SWMX=*,E12.4,* ,SWMN=*,E12.4,
* ,FLO=*,E12.4,* ,FRQDOP=*,E12.4,* ,FQDOPRI=*,E12.4)
000415      PRINT 203,TL,DYNR,SDAMP,SOPHA,I1,I2,I11,I22
000441      203  FORMAT(1X,*TL=*,F6.2,* ,DYNR=*,F6.1,
* ,SDAMP=*,F6.3,* ,SOPHA=*,F6.3,* ,I1,I2,I11,I22*,4I6)
000441      PRINT 204,WN,K,TAU1,TAU2,WNB,KB,TAUB1,TAUB2
000465      204  FORMAT(1X,*WN=*,F6.1,* ,K=*,F6.1,* ,TAU1=*,E12.4,* ,TAU2=*,E12.4
* ,WNB=*,F6.1,* ,KB=*,F6.1,* ,TAUB1=*,E12.4,* ,TAUB2=*,E12.4)
000465      IERRSP=0
000466      DO 220 I=1,100
000470      ADB(I)=0.
000471      220  ERRM(I)=0.
000474      U=0.
000475      EVG=0.
000476      TH2=0.
000477      CTH2=1.
000500      STH2=0.
000501      CTHX=1.
000502      STHX=0.
000503      EU=C.
000504      EV=0.
000505      XI=0.
000506      XQ=0.
000507      QV=0.
000510      QERR0=0.
000511      G1=1.
000512      G2=1.
000513      V=.1
000514      ES=0.

```

```

J00515.....SIH1=0.
J00516.....OTH1=1.
J00517.....DES=DT*SVR
000521.....ERP=0.
J00522.....ERRDMP=0.
000523.....KOUNT=-1
J00524.....IHOLD=0.
000525.....THOLD1=0
J00526.....VMS=EV-EDOP
000530.....EV10=VMS
J00531.....EV10C=VMS
000532.....VMH=0.
J00533.....UMH=1.
000534.....VDP=0.
000535.....XI0C=0.
000536.....XT0=0.
J00537.....J=NSPB
000540.....PKAV=0.
000541.....PKSD=0.
      C      TURBULENCE INITIALIZATION
000542.....ACOR=SQRT(2.**.75-1.)
000551.....AAMP=PI2*FBAMP/ACOR
J00553.....APHA=PI2*FBPHA/ACOR
000555.....IAMP=INT(.5+GAM43/(AAMP*DT))
J00561.....IPHA=INT(.5+GAM43/(APHA*DT))
000564.....GAM43A=DT*FLOAT(IAMP)*AAMP
000567.....GAM43P=DT*FLOAT(IPHA)*APHA
000572.....CCL=0.
J00573.....CALL BLOBA(N43,GAM43A,SDAMP,CCL,IAMP,SLOA,BAMP,I11,I22)
000604.....CALL BLOBF(N43,GAM43P,SDPHA,CCL,IPHA,SLOP,BPHA,I11,I22)
J00615.....CCL=1.
000617.....IAMPC=0
000620.....IPHAC=0
      C      SELECT DATA (IDATA)
000621.....KDATA=0
000622      4      CONTINUE
J00622.....IAMFC=IAMFC+1
000624.....IPHAC=IPHAC+1
000625.....IF(IAMPC.GT.IAMP) GO TO 10
000630      13     IF(IPHAC.GT.IPHA) GO TO 11
000634.....GO TO 12
000634      10     IAMFC=1
000635.....CALL BLOBA(N43,GAM43A,SDAMP,CCL,IAMP,SLOA,BAMP,I11,I22)
000646.....GO TO 13
000647      11     IPHAC=1
000650.....CALL BLOBF(N43,GAM43P,SDPHA,CCL,IPHA,SLOP,BPHA,I11,I22)
J00661.....12     CONTINUE
000661.....YA=SLOA*FLOAT(IAMPC)+BAMP
J00665.....YB=SLOP*FLOAT(IPHAC)+BPHA
J00670.....CALL TRIG(CCLT,YP,SSGIN,CSCIN)
J00673.....IF(J.LT.NSPB)GO TO 1
000676.....J=0
J00676.....IDATAW=IDATA*
000700.....IDATAJ=IDATA
000701.....CALL DATAS(IDATA)
J00702.....SDTH1=SDTH0*IDATA
J00705.....IF(V.GT.TL)GO TO 1
000710.....PKAV=PKAV+PEAK

```



```

000712      PKSD=PKSD+PEAK*PEAK
000714      PEAK=0.
000714      KDATA=KDATA+1
          C   DEFINE INPUTS (TH1,NS,NC)
000716      1   CONTINUE
000716      TEMP=STHX*CDTHX+CTHX*SDTHX
000722      CTHX=CTHX*CDTHX-STHX*SDTHX
000724      STHX=TEMP
000726      TEMP=STH1*CDTH1+CTH1*SDTH1
000731      CTH1=CTH1*CDTH1-STH1*SDTH1
000733      STH1=TEMP
000734      ASTH1=1.+142*A*(1.+YA)*(STH1*CSCIN+CTH1*SSCIN)
000744      ACTH1=1.+142*A*(1.+YA)*(CTH1*CSCIN-STH1*SSCIN)
000754      CALL NRANDOM(I1,I2,X)
000756      NC=X*SIG
000760      CALL NRANDOM(I1,I2,X)
000763      NS=X*SIG
000765      IBIT=IBIT+1
000767      J=J+1
          C   LOOP EQUATIONS
000770      CAMP(4)=CMPLX(ASTH1+NC,-ACTH1-NS)*CMPLX(CTH2,-STH2)*G1
001007      CALL B1FILT(CAMP,CFILT,CMC,DT,INIT)
001012      CCOUT=G2*CFILT(4)
001020      COUT=CCOUT
001022      V=C6*V+C5*U
          C   AGC
001026      VD=V
001027      IF (ABS(VD).LT.AMIN3)VD=AMIN3
001033      IF (VD.NE.0.)CALL ASQRTF(VD,VSQRT)
001036      G1=AGC/VSQRT
001040      G2=G1
001041      U=AIMAG(COUT)*CTHX-REAL(COUT)*STHX
          C   AFG
001045      E=REAL(COUT)*CTHX+AIMAG(COUT)*STHX+ES
001053      EV=C1*EV+C2*E-C3*E0
001061      EV1=EVJ-EDOPPX
001063      IF (EV.GT.EVMAX)DES=-DES
001066      IF (EV.LT.EVMTN)DES=-DES
001072      EDOPRX=EDOPRX+EDOPR
001074      TH2=TH2+C4*EV1
001077      TH2=AMOD(TH2,PI2)
001102      CALL TRIG(CCLT,TH2,STH2,CTH2)
001105      VMS0=VMS
001107      VMS=C6MS*VMS+C5MS*EV10C
001112      IF (ABS(VMS).GT.ABS(VMS0))PEAK=FLOAT(IBIT)
001120      VDP=C6DP*VDP+C5DP*EV10
001124      EV1C=EV1-VMH-VDP
001127      XI=XI+EV1C
001130      XQ=XQ+EV1C
001132      EVJ=EV
001133      EV=E
001134      EV10=EV1
001135      IF (V.GT.TL)ES=ES+DES
001142      EV10C=EV1C
          C   BIT SYNC TIMING
001144      IF (IBIT.NE.NSLICE)GOTO81
001146      IMS=-1
001147      IF (VMS.GT.0.)IMS=1

```

```

001151      VMSS=VMS
001152      81  CONTINUE
001152      IF (IBIT.NE.NBIT) GO TO 2
001154      XQ0=XQ/FLOAT(NBIT)
001157      XQ=0.
001157      2  IF (IBIT.LT.NBIT) GO TO 4
001162      IF (KOUNT.LT.IDLBIT) GOTO 91
001164      XISUM=XISUM+ABS(XI)
001167      XISIG=XISIG+XI*XI
001171      91  CONTINUE
001171      IHOLD1=IHOLD
001173      IHOLD=-1
001174      IF (XI.GT.0.) IHOLD=1
001176      XIO=XIO
001200      XIO=XI/FLOAT(NBIT)
001202      VMH=(C6MH*VMH+C5MH*UMH)*A5
001206      UMH=0.
001206      IF (IHOLD.NE.IHOLD1) UMH=XIO+XIO
001212      XI=0.
001213      QERR=XQ0*((IHOLD-IHOLD1)/2)
001217      QV=C91*QV+C82*QERR-C83*QERR0
001224      QERR0=QERR
001225      IBIT=0
001226      FVCOB=BRATE+K8*QV
001231      TSYNC=TSYNC-NBIT*DT+1./FVCOB
001236      NBIT=TSYNC/DT+.5
001241      NBIT2=NBIT/2
001243      IF (V.GT.TL) GO TO 95
001246      ILOC=ILOC
001247      402 CONTINUE
001247      KOUNT=KOUNT+1
001251      IF (KOUNT.LT.IDLBIT) GOTO 93
001253      IF (IMS.NE.IDATA0) ERR=ERR+1.
001257      IF (IHOLD.NE.IDATA0) ERRDMP=ERRDMP+1.
C      ERROR SPACING
001263      IF (IMS.EQ.IDATA0) GOTO 221
001264      IF (IERRSP.LT.1) IERRSP=1
001270      IF (IERRSP.GT.100) IERRSP=100
001273      ERRM(IERRSP)=ERRM(IERRSP)+1.
001276      IERRSP=0
001276      GOTO 222
001277      221 IERRSP=IERRSP+1
001301      222 CONTINUE
001301      SLSUM=SLSUM*ABS(VMSS)
001304      SLSIG=SLSIG+VMSS*VMSS
C      SOFT DECISION
001306      IX=INT(ASOFTI*VMSS+.4)+1
001312      IF (IX.GT.8) IX=8
001315      IF (IX.LT.1) IX=1
001320      IF (IXM.EQ.0) GOTO 96
001321      IF (IDATAW.EQ.-1.AND.IDATA0.EQ.-1) SBINS1(IX,IXM)=SBINS1(IX,IXM)+1
001334      IF (IDATAW.EQ.-1.AND.IDATA0.EQ.-1) CBIN1=CBIN1+1.
001345      IF (IDATAW.EQ.-1.AND.IDATA0.EQ.+1) SBINS2(IX,IXM)=SBINS2(IX,IXM)+1
001360      IF (IDATAW.EQ.-1.AND.IDATA0.EQ.+1) CBIN2=CBIN2+1.
001371      IF (IDATAW.EQ.+1.AND.IDATA0.EQ.-1) SBINS3(IX,IXM)=SBINS3(IX,IXM)+1
001404      IF (IDATAW.EQ.+1.AND.IDATA0.EQ.-1) CBIN3=CBIN3+1.
001415      IF (IDATAW.EQ.+1.AND.IDATA0.EQ.+1) SBINS4(IX,IXM)=SBINS4(IX,IXM)+1
001427      IF (IDATAW.EQ.+1.AND.IDATA0.EQ.+1) CBIN4=CBIN4+1.

```

```

001437 96 CONTINUE
001437 IXM=IX
001441 GOTO93
001441 95 CONTINUE
C LOCK/UNLOCK
001441 IF(ILOCF.EQ.ILOC)GOTO400
001443 ILOC=ILOC+1
001444 IF(ILOC.GT.NRUNS)GOTO408
001447 GOTO93
001447 400 IF(IDO.EQ.IDON)GOTO401
001451 IDO=IDO+1
001452 IF(IDO.GT.100)GOTO402
001455 IDON=IDO
001455 ADB(IDON)=0.
001456 401 ADB(IDON)=ADB(IDON)+1.
001461 GOTO402
001461 408 PRINT 409
001465 409 FORMAT(1X,*ACQUISITION FAILURE*)
001465 GOTO10
001466 93 CONTINUE
001466 IF(KOUNT.LT.NRUNS)GO TO 4
C ERROR RATE CALCULATION
001471 92 CONTINUE
001471 PE=ERR/(KOUNT-IDLBIT)
001475 STDEV=SQRT(PE*(1.-PE)/(KOUNT-IDLBIT))
001505 SLSUM=SLSUM/(KOUNT-IDLBIT)
001511 SLSIG=SQRT(SLSIG/(KOUNT-IDLBIT)+SLSUM*SLSUM)
001517 KKK=KOUNT-IDLBIT
001521 PRINT 301,PE,STDEV,SLSUM,SLSIG,KKK
001536 301 FORMAT(1X,*PE=*,E12.4,* ,STDEV=*,E12.4,* ,V MEAN=*,E12.4,
+*V STD DEV=*,E12.4,* ,BITS=*,I6)
001536 PEI=ERRDMP/(KOUNT-IDLBIT)
001542 SPEI=SQRT(PEI*(1.-PEI)/(KOUNT-IDLBIT))
001552 XISUM=XISUM/(KOUNT-IDLBIT)
001556 XISIG=SQRT(XISIG/(KOUNT-IDLBIT)+XISUM*XISUM)
001564 PRINT +11,PEI,SPEI,XISUM,XISIG,KKK
001601 411 FORMAT(1X,*PEI=*,E12.4,* ,STDEV=*,E12.4,* ,I MEAN=*,E12.4,
+* I STD DEV=*,E12.4,* ,BITS=*,E12.4)
001601 ADOA=0.
001602 ADOS=0.
001603 IF(IDO.EQ.0)GOTO405
001604 DO 403 I=1,IDO
001605 ADOA=ADOA+ADB(I)
001607 403 ADOS=ADOS+ADB(I)*ADB(I)
001614 FIDO=FLOAT(IDO)
001615 ADOA=ADOA/FIDO
001616 ADOS=SQRT(ADOS/FIDO-ADOA*ADOA)
001623 PRINT 404,ILOCF,IDO,ADOA,ADOS
001636 404 FORMAT(1X,*LOCKIN=*,I6,* ,DROPOUTS=*,I6,* ,AVE=*,E12.4,
+* ,STD DEV=*,E12.4)
001636 GOTO406
001637 405 PRINT 407,ILOCF
001645 407 FORMAT(1X,*LOCKIN=*,I6,* ,DROPOUTS=0*)
001645 406 CONTINUE
001645 PRINT 223,ERRM
001653 223 FORMAT(1X,*ERRM*,/,10(1X,10E12.4,/))
001653 PRINT 313,CBIN1,CBIN2
001663 313 FORMAT(1X,*-1,-1 P(B/A)TIMES*,F6.0,37X,*-1,+1 P(B/A)TIMES*,F6.0)

```

```

001663      DO 314 I=1,8
001665      DO 315 J=1,8
001666      F1(J)=SBINS1(I,J)
001672      315 F2(J)=SBINS2(I,J)
001676      314 PRINT 316,F1,F2
001710      316 FORMAT(1X,8F6.0,6X,8F6.0)
001710      PRINT 317,CBIN3,CBIN4
001720      317 FORMAT(1X,*+1,-1 P(8/A)TIMES*,F6.0,37X,*+1,+1 P(8/A)TIMES*,F6.0)
001720      DO 318 I=1,8
001722      DO 319 J=1,8
001723      F1(I,J)=SBINS3(I,J)
001727      319 F2(I,J)=SBINS4(I,J)
001733      318 PRINT 318,F1,F2
001745      PRINT 304,I1,I2,I11,I22
001761      304 FORMAT(1X,*I1,I2,I11,I22*,4I6)
001761      PKAV=PKAV/KDATA
001763      PKSD=SQRT(PKSD/KDATA-PKAV*PKAV)
001771      PRINT 305,PKAV,PKSD
002000      305 FORMAT(1X,*REC SLICE=*,E12.4,* ,STD DEV=*,E12.4)
002000      410 CONTINUE
002000      307 PRINT 104
002004      104 FORMAT(1H1,///)
002004      GO TO 3
002005      END

```

```

SUBROUTINE NRANDM(IYN,IZN,RDMN)
000006      RDMN=-6.
000007      DO 1 N=1,12
000010      CALL RANDM(IYN,IZN,RDM)
000011      1 RDMN=RDMN+RDM
000017      RETURN
000017      END

```

```

SUBROUTINE RANDM(IYN,IZN,RDM)
000006      DATA IA,IB/129,1/
000006      DATA T,IRT/4194304.,2048/
000006      IYN=IA*IYN+(IB+IA*IZN)/IRT
000014      IYN=MOD(IYN,IRT)
000020      IZN=MOD((IB+IA*IZN),IRT)
000026      RDM=FLOAT(IYN*IRT+IZN)/T
000031      RETURN
000032      END

```

```

SUBROUTINE B1FILT(X,Y,OMC,T,INIT)
C INPUT INTO X(4), OUTPUT FROM Y(4), INIT=0 FOR NEW OMC OR T
C FIRST ORDER INTERPOLATION
000010 COMPLEX X(4),Y(4)
000010 IF(INIT.NE.0)GO TO 1
000011 INIT=1
000011 OMT=OMC*T
000012 B1=((OMT+8.)*OMT/24.+1.)*OMT+1.
000020 B2=((11.*OMT/24.+1.)*OMT-1.)*OMT-3.)/B1
000027 B3=((11.*OMT/24.-1.)*OMT-1.)*OMT+3.)/B1
000035 B4=((OMT-8.)*OMT/24.+1.)*OMT-1.)/B1
000044 A1=OMT*OMT*OMT/(24.*B1)
000046 A2=11.*A1
C OUTPUT OMT,A1,A2,B1,B2,B3,B4
000050 1 Y(4)=A1*(X(4)+X(1))+A2*(X(3)+X(2))-B2*Y(3)-B3*Y(2)-B4*Y(1)
000125 DO 2 I=1,3
000126 X(I)=X(I+1)
000134 2 Y(I)=Y(I+1)
000144 RETURN
000144 END

```

```

SUBROUTINE BLOBA(N,GAM,VAL,CCL,IL,S,8,IYN,IZN)
000014 DIMENSION TG(128),RC(128)
000014 DATA G43/.892979511/
000014 IF(VAL.EQ.0.)GO TO 30
000015 IF(CCL.EQ.1.)GO TO 10
000017 EX=1./3.
000020 YN=0.
000020 S2=0.
000022 DO 11 I=1,N
000023 V=FLOAT(I-1)*GAM
000025 TG(I)=GAM/G43*V**EX*EXP(-V)
000043 S2=S2+TG(I)*TG(I)
000046 CALL NRANDOM(IYN,IZN,RC(I))
000052 11 YN=YN+TG(I)*RC(I)
000064 S22=SQRT(S2)
000066 YN=YN/S22*VAL
000074 GO TO 20
000075 10 YN=YT
000077 20 NN=N-1
000101 DO 12 J=1,NN
000102 12 RC(N+1-J)=RC(N-J)
000111 CALL NRANDOM(IYN,IZN,RC(1))
000115 YT=0.
000116 DO 13 JJ=1,N
000123 13 YT=YT+TG(JJ)*RC(JJ)
000130 YI=YT/S22*VAL
000132 FILM=FLOAT(IL-1)
000133 S=(YT-YN)/FILM
000136 B=-S*FLOAT(IL)+YT
000142 GO TO 31
000142 30 S=0.
000143 B=0.
000144 31 RETURN
000144 END

```

```

SUBROUTINE BLOBP(N,GAM,VAL,CCL,IL,S,B,IYN,IZN)
000014 DIMENSION TG(128),RC(128)
000014 DATA G43/.892979511/
000014 IF(VAL.EQ.0.) GO TO 30
000015 IF(CCL.EQ.1.) GO TO 10
000017 EX=1./3.
000020 YN=0.
000020 S2=0.
000022 DO 11 I=1,N
000023 V=FLOAT(I-1)*GAM
000025 TG(I)=GAM/G43*V**EX*EXP(-V)
000043 S2=S2+TG(I)*TG(I)
000046 CALL NRANDOM(IYN,IZN,RC(I))
000052 11 YN=YN+TG(I)*RC(I)
000064 S22=SQRT(S2)
000066 YN=YN/S22*VAL
000074 GO TO 20
000075 10 YN=YT
000077 20 NN=N-1
000101 DO 12 J=1,NN
000102 12 RC(N+1-J)=RC(N-J)
000111 CALL NRANDOM(IYN,IZN,RC(1))
000115 YT=0.
000116 DO 13 JJ=1,N
000123 13 YT=YT+TG(JJ)*RC(JJ)
000130 YT=YT/S22*VAL
000132 FILM=FLOAT(IL-1)
000133 S=(YT-YN)/FILM
000136 B=-S*FLOAT(IL)+YT
000142 GO TO 31
000142 30 S=0.
000143 B=0.
000144 31 RETURN
000145 END

```

```

SUBROUTINE TRIG(CCLT,ANGR,S,C)
000007 DIMENSION SINE(91)
000007 DR=.0174532925
000010 IF(CCLT.EQ.1.) GO TO 10
000012 NT=91
000013 DO 9 I=1,NT
000014 9 SINE(I)=SIN(FLOAT(I-1)*DR)
000027 10 IR=INT(ANGR/DR+.5)
000032 IM=ABS(ANGR/DR+.5)
000036 IF(IM.GT.270) GO TO 4
000042 IF(IM.GT.180) GO TO 3
000045 IF(IM.GT.90) GO TO 2
000050 S=SINE(IM+1)
000051 C=SINE(-IM+90+1)
000053 GO TO 30
000053 2 S=SINE(-IM+180+1)
000055 C=-SINE(IM-90+1)
000057 GO TO 30
000057 3 S=-SINE(IM-180+1)
000061 C=-SINE(-IM+270+1)
000063 GO TO 30
000063 4 S=-SINE(-IM+360+1)
000065 C=SINE(IM-270+1)
000067 30 IF(IR.LT.0) S=-S
000072 RETURN
000073 END

```

```

SUBROUTINE ASQRTF (XU,S)
000005 X=ABS(XU)
000006 IF(X.GT.128.) GO TO 1
000012 IF(X.GT.64.) GO TO 2
000015 IF(X.GT.32.) GO TO 3
000020 IF(X.GT.16.) GO TO 4
000023 IF(X.GT.8.) GO TO 5
000026 IF(X.GT.4.) GO TO 6
000031 IF(X.GT.2.) GO TO 7
000034 IF(X.GT.1.) GO TO 8
000037 IF(X.GT..5) GO TO 9
000042 IF(X.GT..25) GO TO 10
000045 IF(X.GT..125) GO TO 11
000050 S=.3535
000051 RETURN
000051 1 S=11.3137
000052 RETURN
000053 2 S=.0517*(X-128.)+11.3137
000057 RETURN
000057 3 S=.07322*(X-64.)+8.
000063 RETURN
000063 4 S=.10355*(X-32.)+5.6568
000067 RETURN
000067 5 S=.14644*(X-16.)+4.
000073 RETURN
000073 6 S=.2071*(X-8.)+2.8284
000077 RETURN
000077 7 S=.2928*(X-4.)+2.
000103 RETURN
000103 8 S=.4142*(X-2.)+1.4142
000107 RETURN
000107 9 S=.5857*(X-1.)+1.
000112 RETURN
000113 10 S=.8284*(X-.5)+.7071
000117 RETURN
000117 11 S=1.17157*(X-.25)+.5
000123 RETURN
000123 END

```

```

SUBROUTINE DATAS (IXU)
000003 DIMENSION IRC(6)
000003 DATA IRC/0,0,0,0,0,1/
000003 IX=0
000003 IF(IRC(1).NE.IRC(6)) IX=1
000007 DO 1 I=1,5
000011 1 IRC(7-I)=IRC(6-I)
000017 IRC(1)=IX
000020 IXU=1
000021 IF(IX.EQ.0) IXU=-1
000023 RETURN
000024 END

```

```

PROGRAM CARL(INPUT,OUTPUT,TAPES=INPUT,TAPES=OUTPUT)
COMPLEX CAMP(4),CFILT(4),COUT,CCOUT
REAL NS,NC,NO,K,KB
DIMENSION SBINS1(8,8),SBINS2(8,8),SBINS3(8,8),SBINS4(8,8)
DIMENSION AOB(100)
DIMENSION F1(8),F2(8)
DIMENSION ERRH(100)
DATA FBAMP,FBPHA,SOAMP,SOPHA,NO/2...2...23..47.1./

```

```

DATA GAM43,N43/.09,64/
DATA ENODB,BRATE,ENOMIN/8..88..9./
DATA DELF,NSPB,NRUNS,BIF/62..40,10,1000./
DATA BL2,PHIDEG,FOIFF/176..10..342.433/
DATA BL2B,PHIB,FOIFFB/1..10..5./
DATA I1,I2,I11,I22,NSLICE/1.1.1.1.24/
DATA FRQOP,FOOPRT,TL,AGC/0..0..-2.6.1./
DATA TAU3,ASOFT/.07957..2474/

```

```

DATA TAU4,TAU5,TAU6,AS,FLO/.001808..01808..10603..5.0./
DATA SVRHZ,SWMX,SWMN/2.2E3,28.15E3,6.85E3/
DATA IOLBIT/20/
DATA DYNR/0./

```

```

NAMELIST/IN1/NRUNS,NSPB,ENODB,DELF,BIF,ENOMIN
,BL2,PHIDEG,FOIFF,BL2B,PHIB,FOIFFB
,FBAMP,FBPHA,SOAMP,SOPHA,GAM43,N43,NSLICE
,FLO,FRQOP,FOOPRT,ASOFT,I1,I2,I11,I22
,SVRHZ,SWMX,SWMN,TL,AGC
,IOLBIT,T6YNC,IOLBIT,DYNR
,TAU4

```

```

PI=4.*ATAN(1.)
PI2=2.*PI
ZETA=SQRT(0.5)
ZETAB=ZETA
CCLT=0.

```

```
CALL TRIG(CCLT,PI,SGCIN,C6CIN)
```

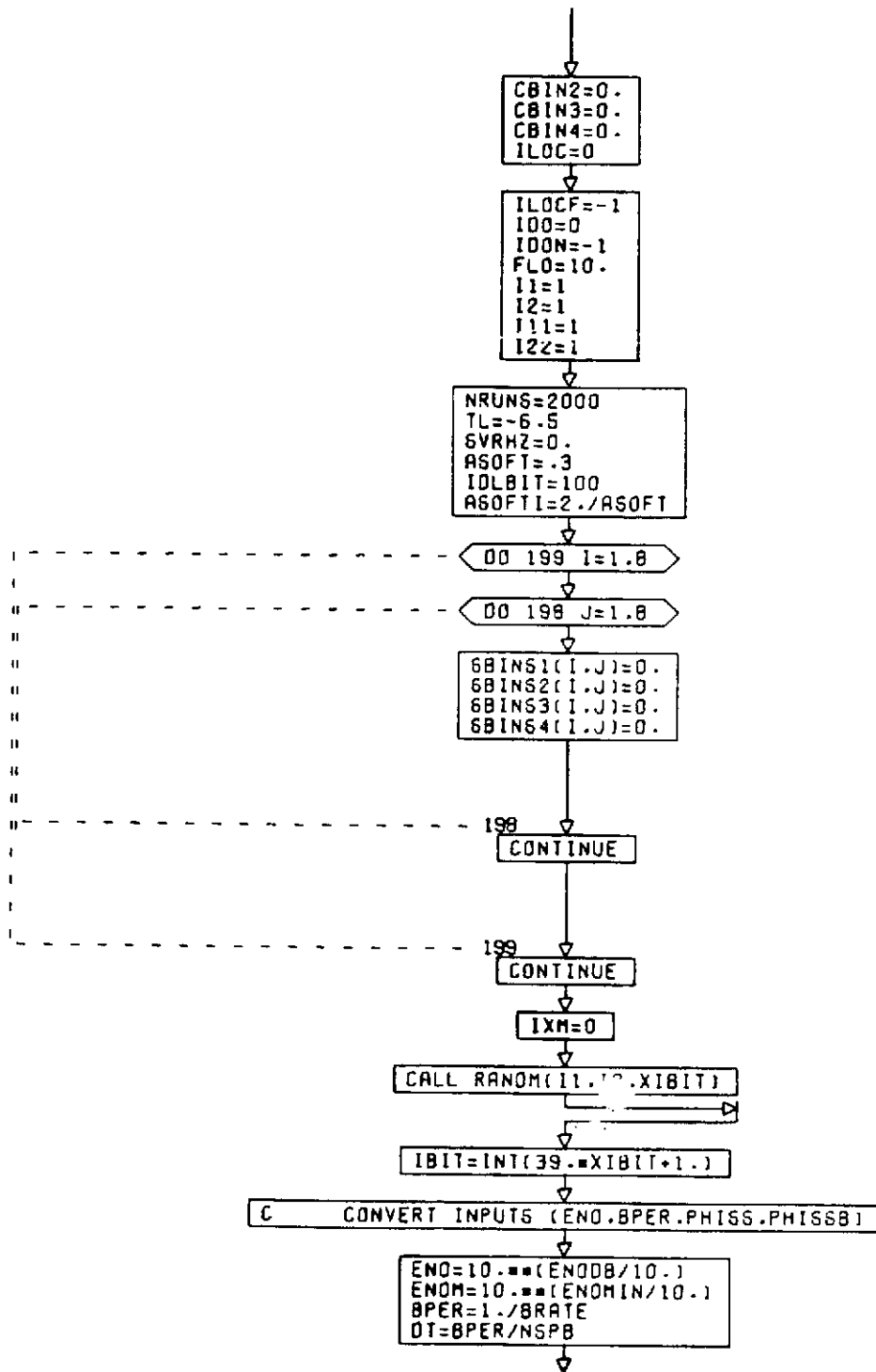
```
CCLT=1.
```

```
A1 23
```

```
CONTINUE
```

```
READ INPUT6
```

```
READ(5,IN1)
DYNR=3.
NSLICE=26
CBIN1=0.
```

CONT. ON PG 3

PG 2 OF 23

PHISS=PHIDEG*PI/180.
PHISSB=PHIB*PI/180.
AMIN=SQRT(ENO*NO*BRATE)
AMIN2=AMIN/1.4142

AGC=SQRT(AMIN2)
AMIN3=AMIN2/SQRT(10.*(DYNR/10.))
A=SQRT(ENO*NO*BRATE)

C CALCULATE LOOP PARAMETERS (TAU1,TAU2,K,TAUB1,TAUB2,KB)

WN=BL2/(ZETA+0.25/ZETA)
AK=PI2*FOIFF/SIN(PHISS)
TAU1=AK/(WN*WN)
TAU2=2.*(ZETA-0.5/(WN*TAU1))/WN
K=AK/AMIN
EDOP=PI2*FRQOOP/K
EDOPR=PI2*FGOPRT/DT/K
EDOPRX=EDOP+EDOPR

EVMAX=PI2*SWMX/K
EVMIN=-PI2*SWMN/K
SVR=PI2*SVRHZ/K
WNB=BL2B/(ZETAB+0.25/ZETAB)
AK=PI2*FOIFFB/SIN(PHISSB)
TAUB1=AK/(WNB*WNB)
TAUB2=2.*(ZETAB-0.5/(WNB*TAUB1))/WNB
AKBMIN=PI2*(DELFL/2.)/(K*1.4125)

KB=AK/AKBMIN

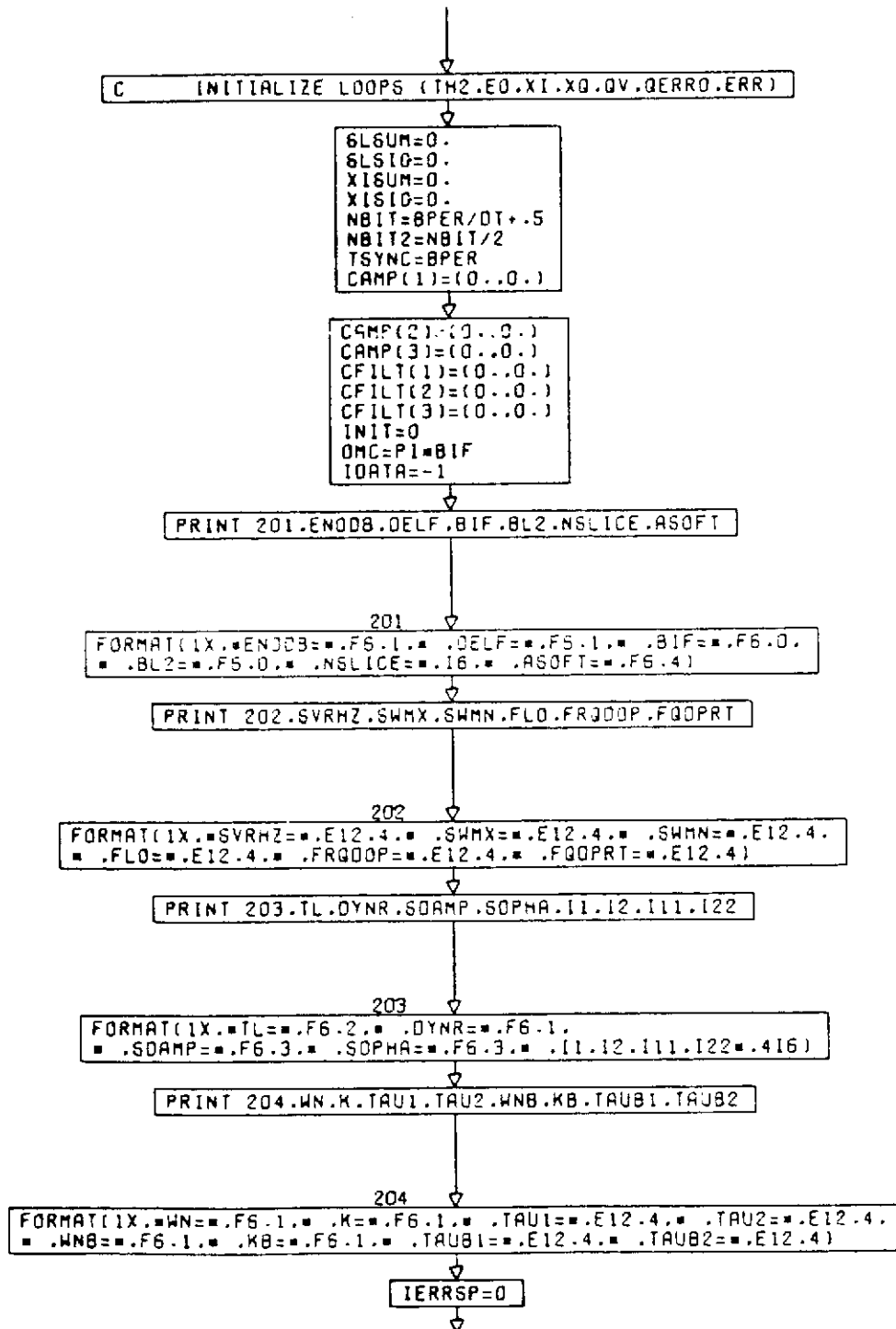
C DEFINE CONSTANTS

C1=1.-DT/TAU1
C2=TAU2/TAU1
C3=C1+C2-1.
C4=DT*K
C5=DT/TAU3
C6=1.-C5
DTH1=PI*DELFL*DT
SDTH0=SIN(DTH1)

COTH1=COS(DTH1)
DTHX=PI2*FLO*DT
SDTHX=SIN(DTHX)
COTHX=COS(DTHX)
CB1=1.-BPER/TAUB1
CB2=TAUB2/TAUB1
CB3=CB1+CB2-1.
CSMS=DT/TAU4

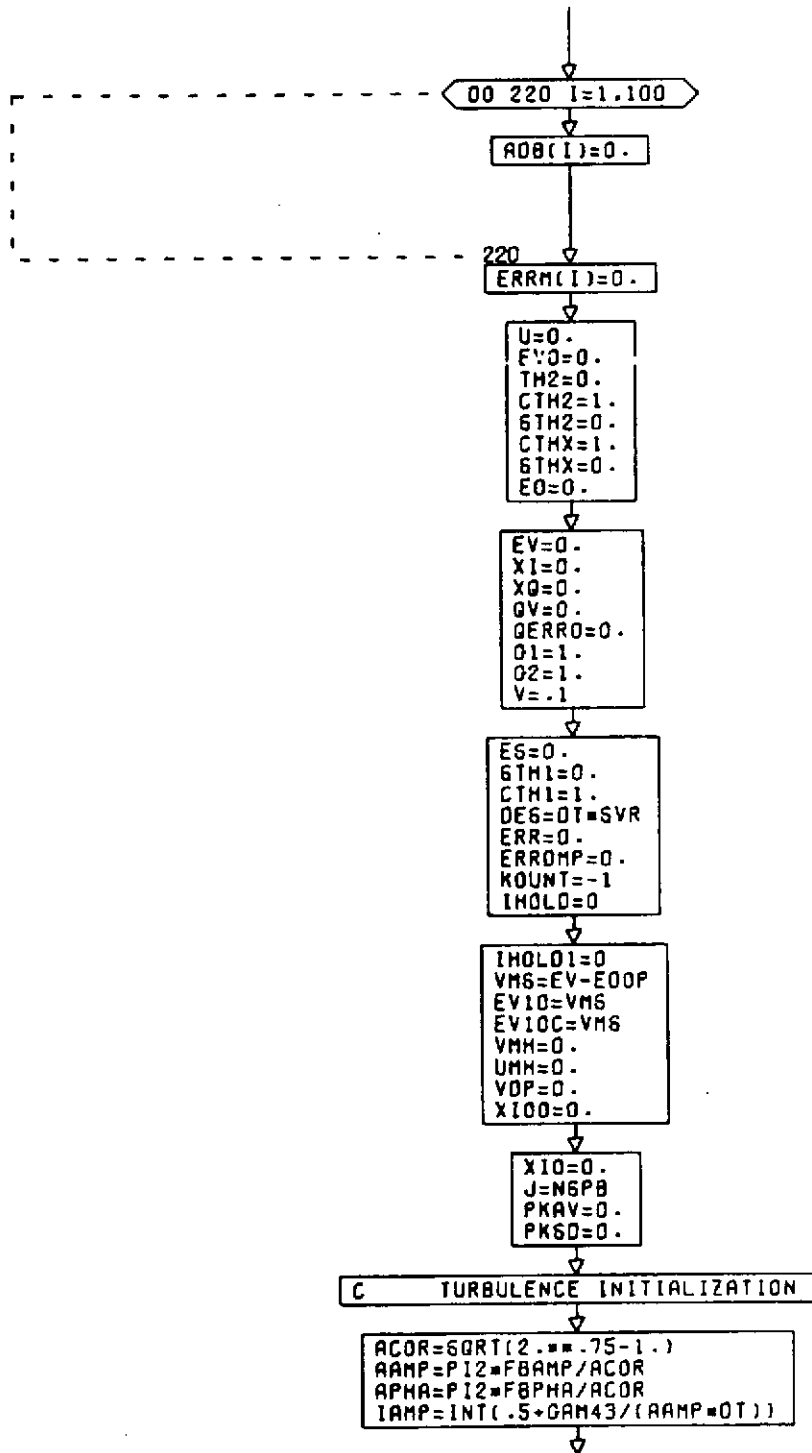
CSMS=1.-CSMS
CSMH=DT/TAU5
CSMH=1.-CSMH
CSOP=DT/TAU6
CSOP=1.-CSOP
SIO=0.5*SQRT(NO/DT)

CONT. ON PG 4



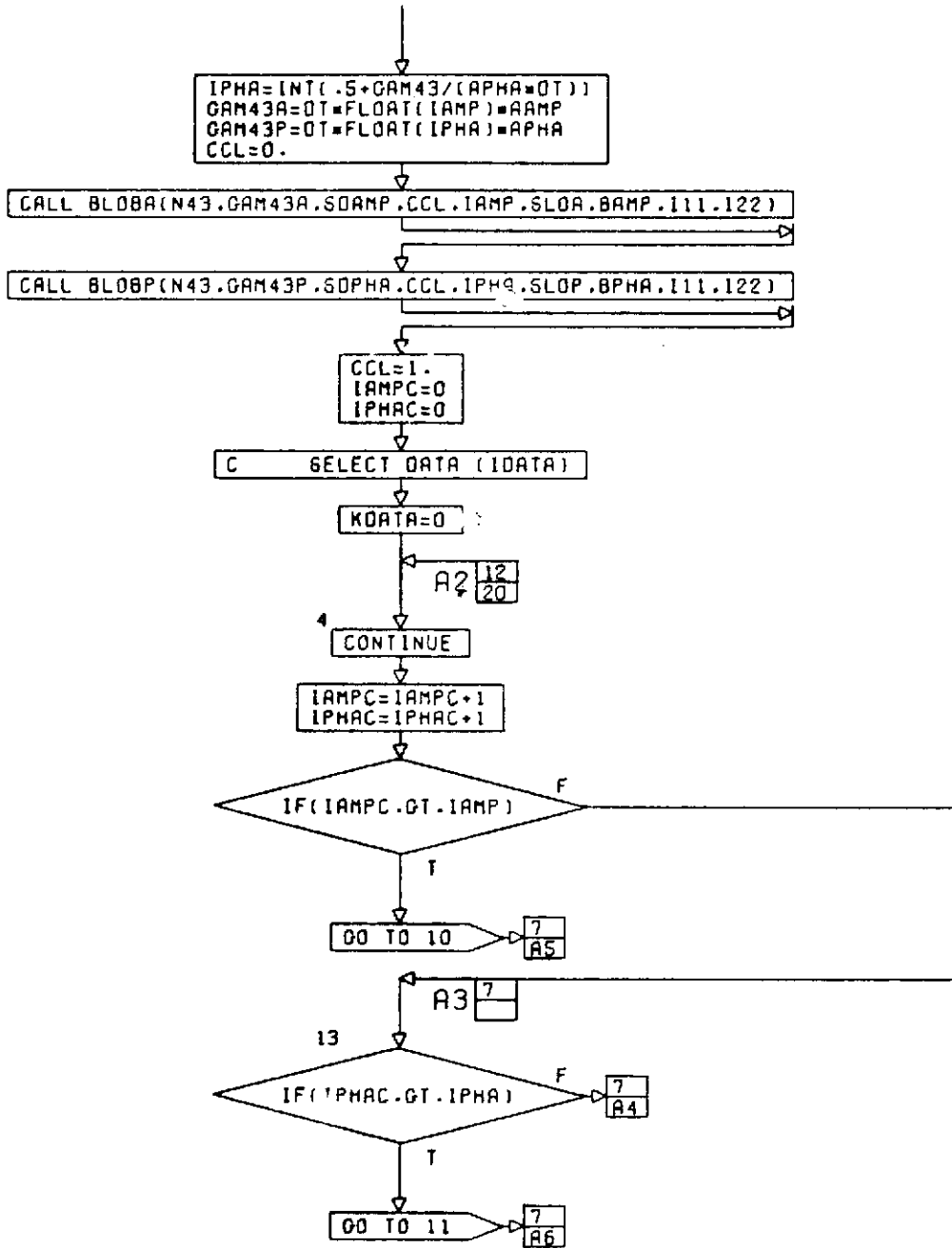
CONT. ON PG 5

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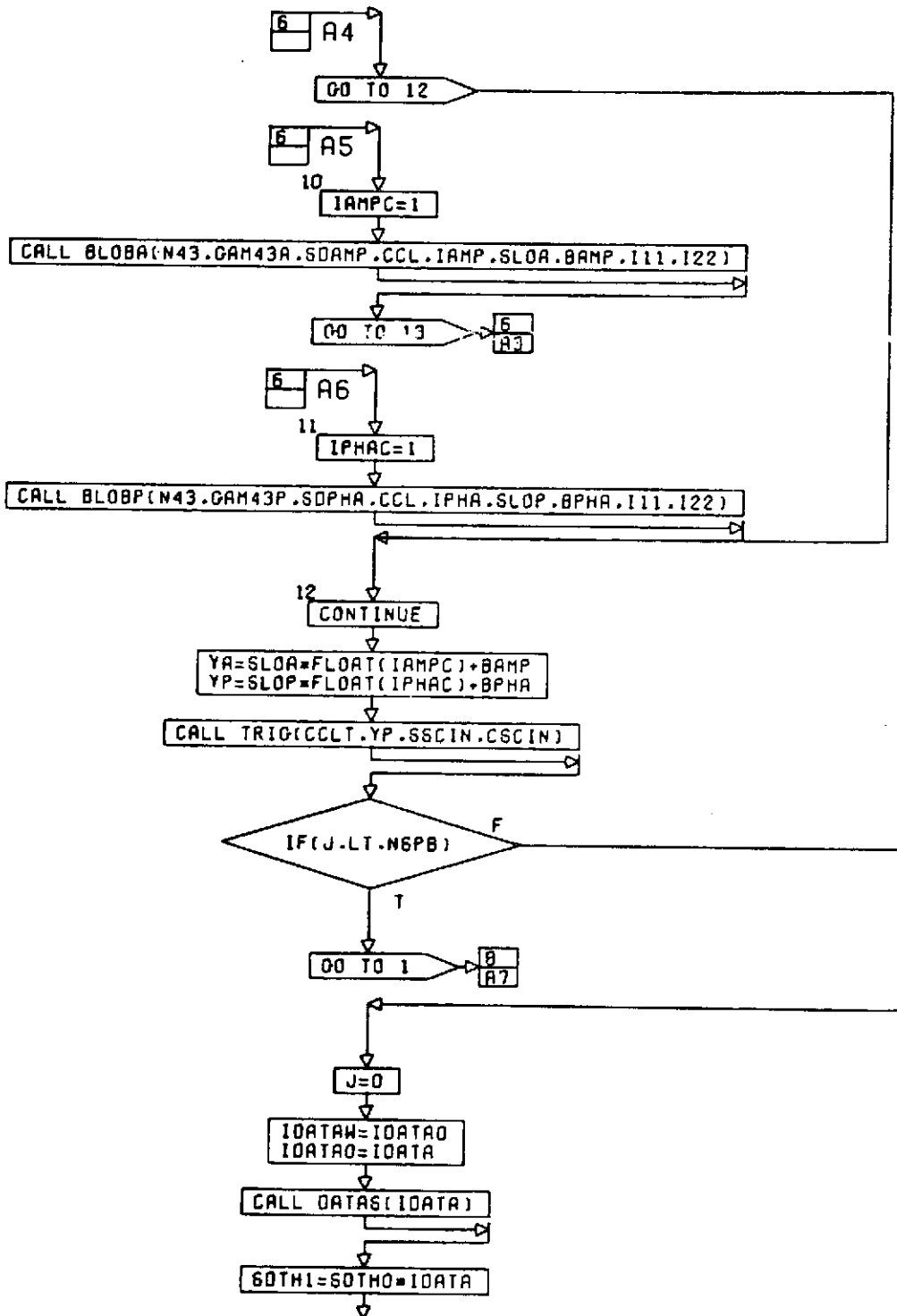
CONT. ON PG 6

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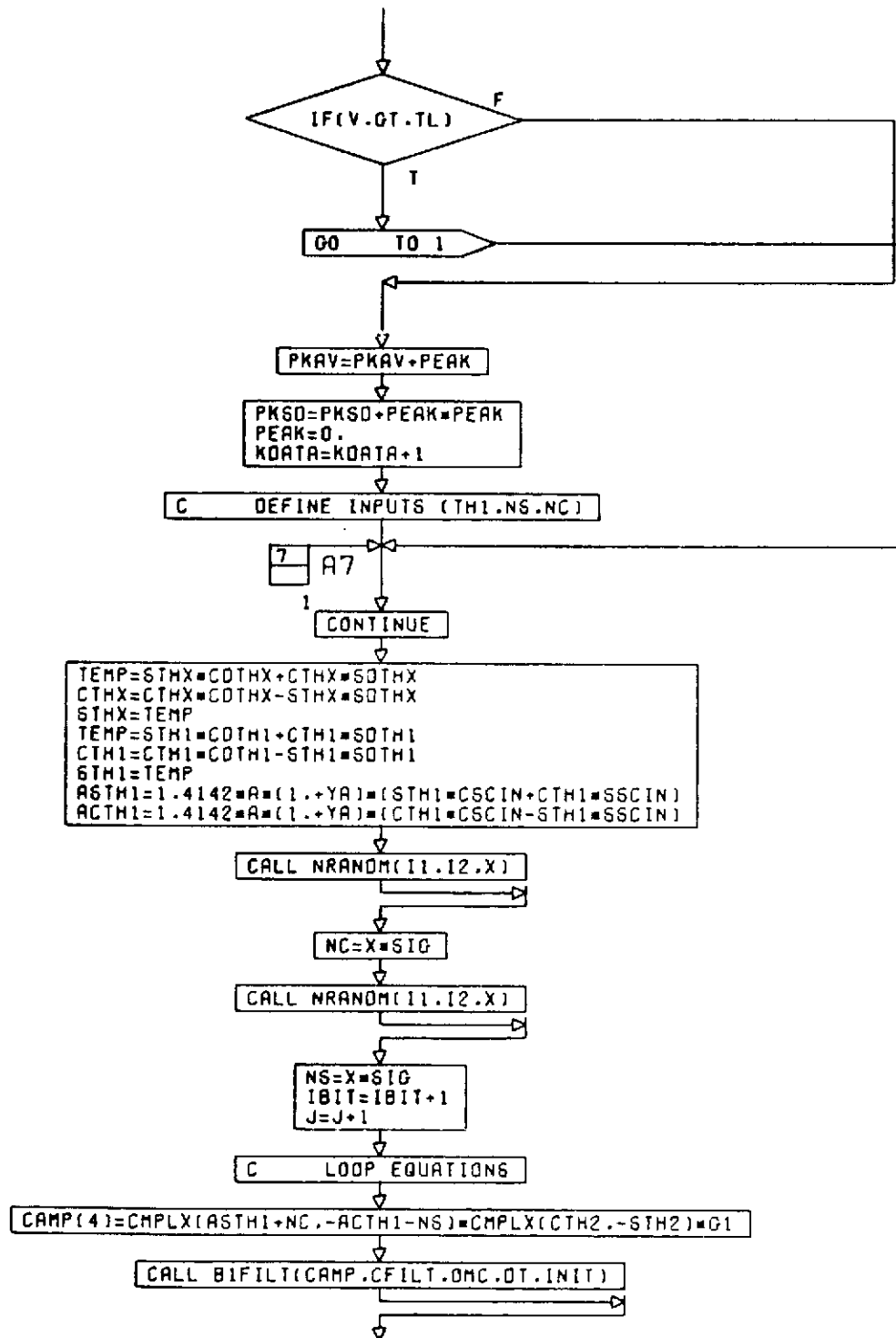


CONT. ON PG 7

PG 6 OF 23

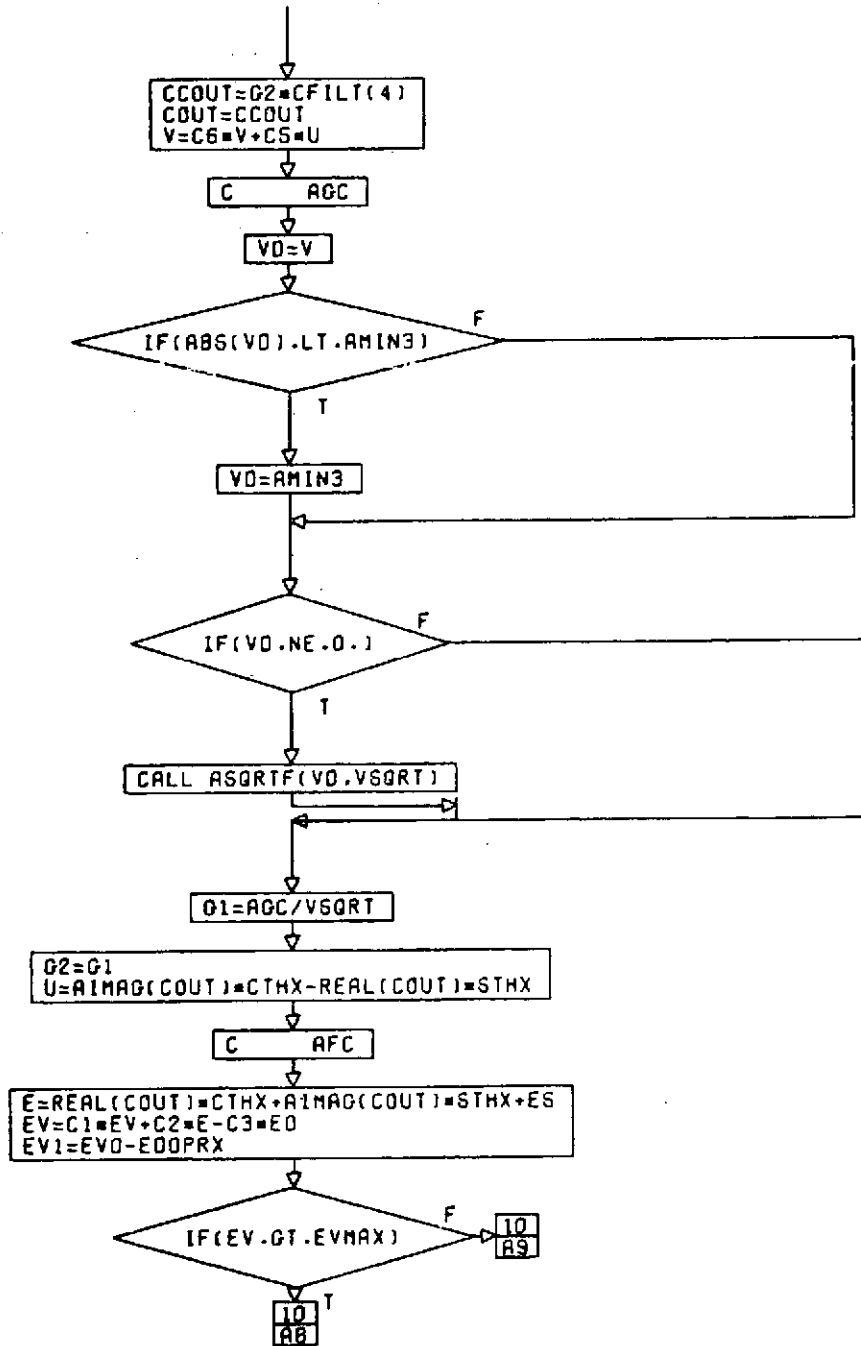


CONT. ON PG 8



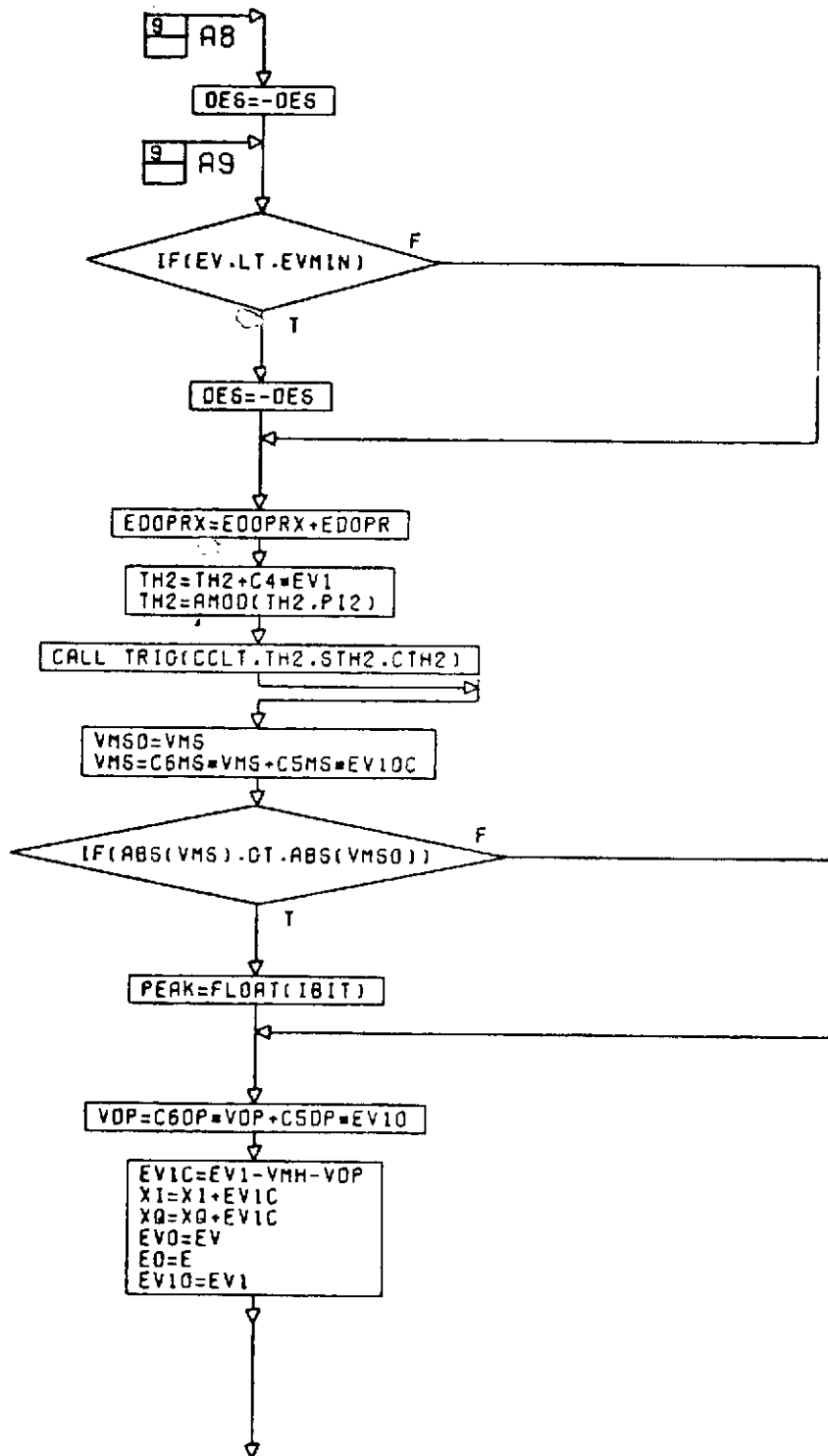
CONT. ON PG 9

PG 8 OF 23



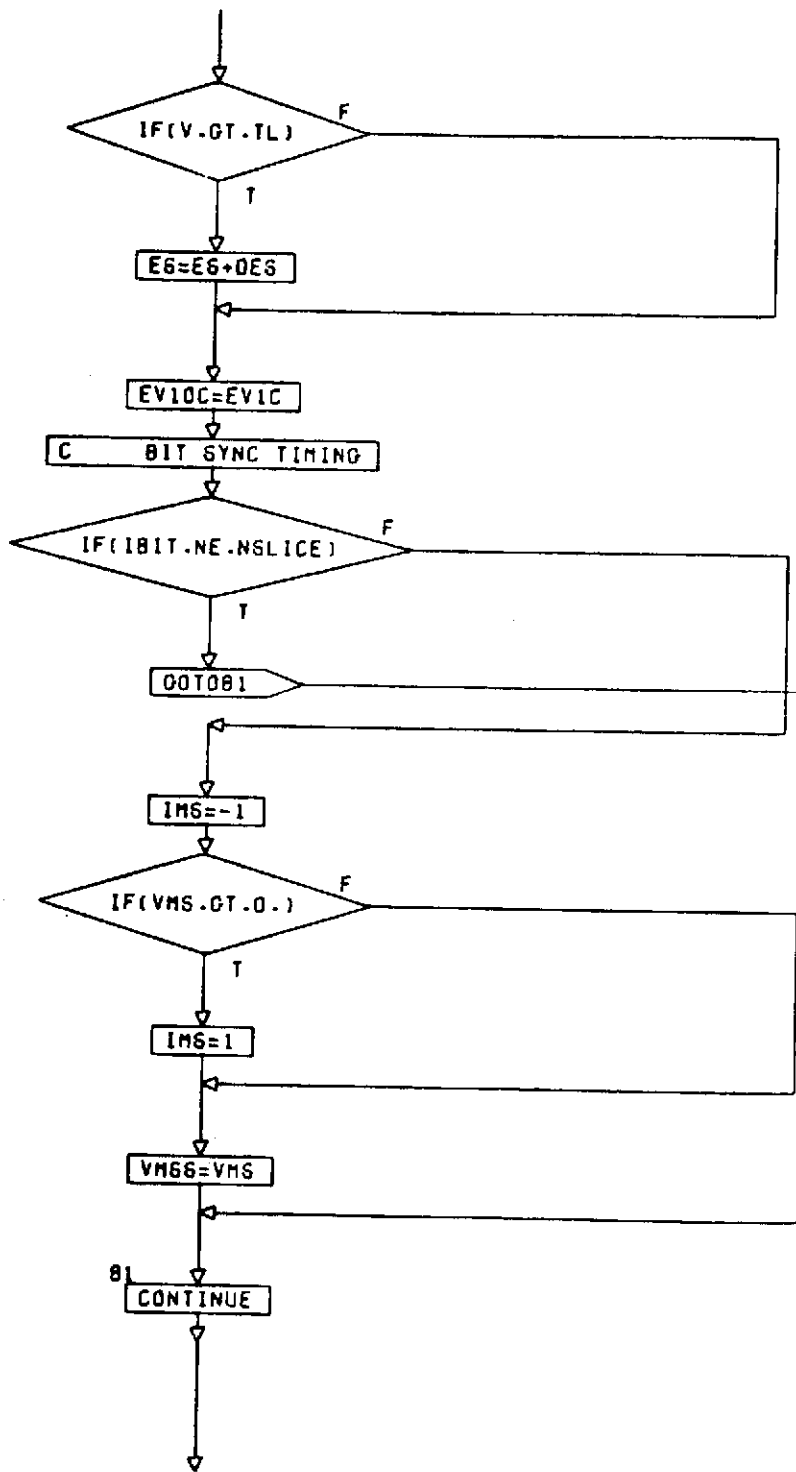
CONT. ON PD 10

PD 9 OF 23

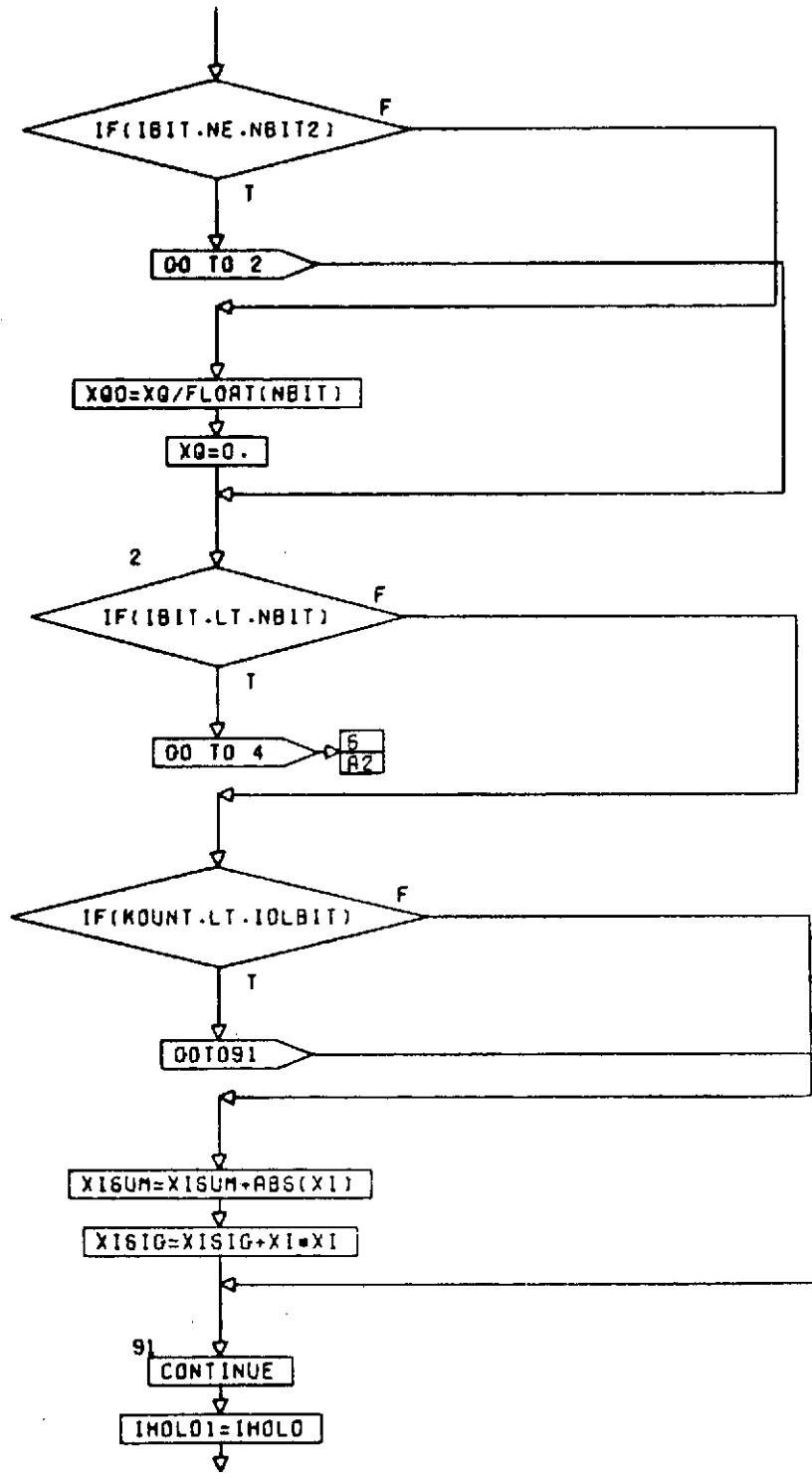


CONT. ON PG 11

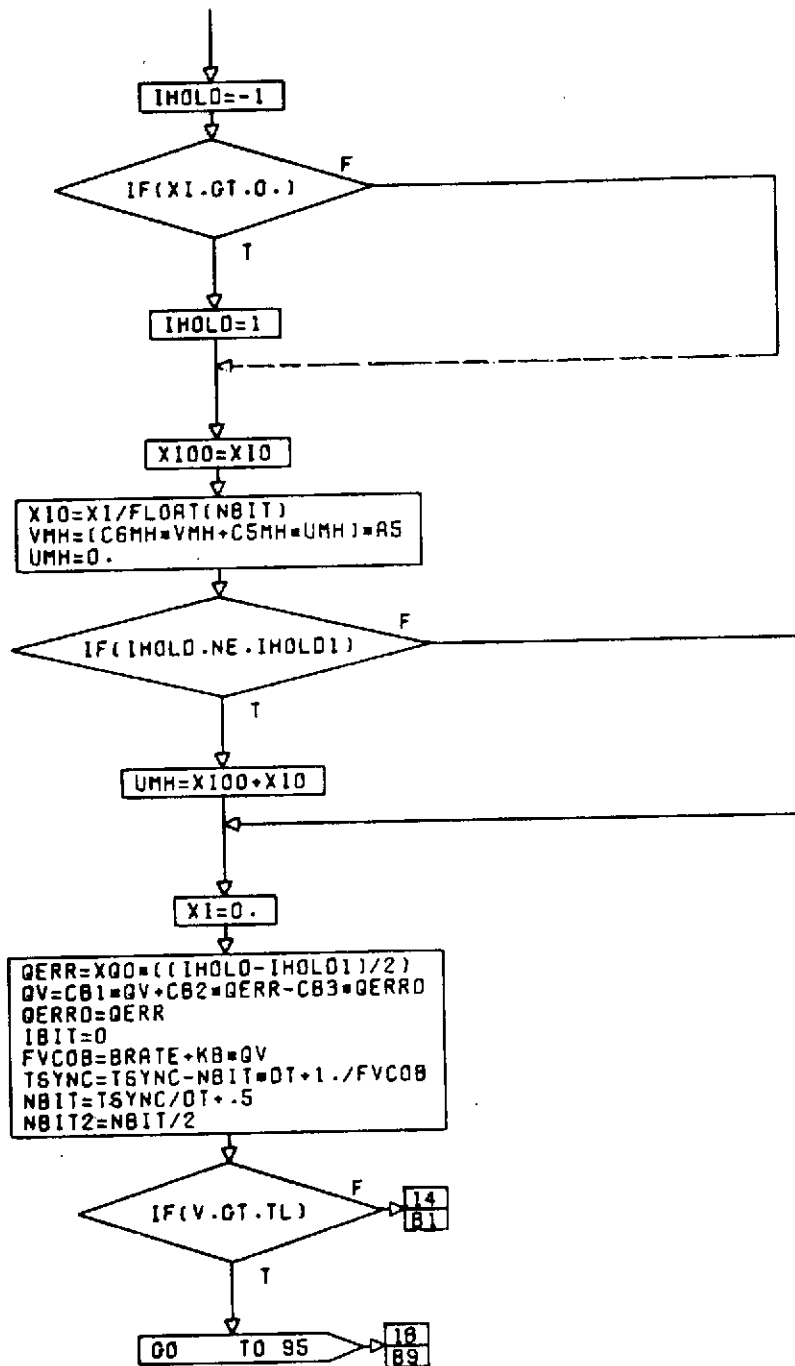
PG 10 OF 23

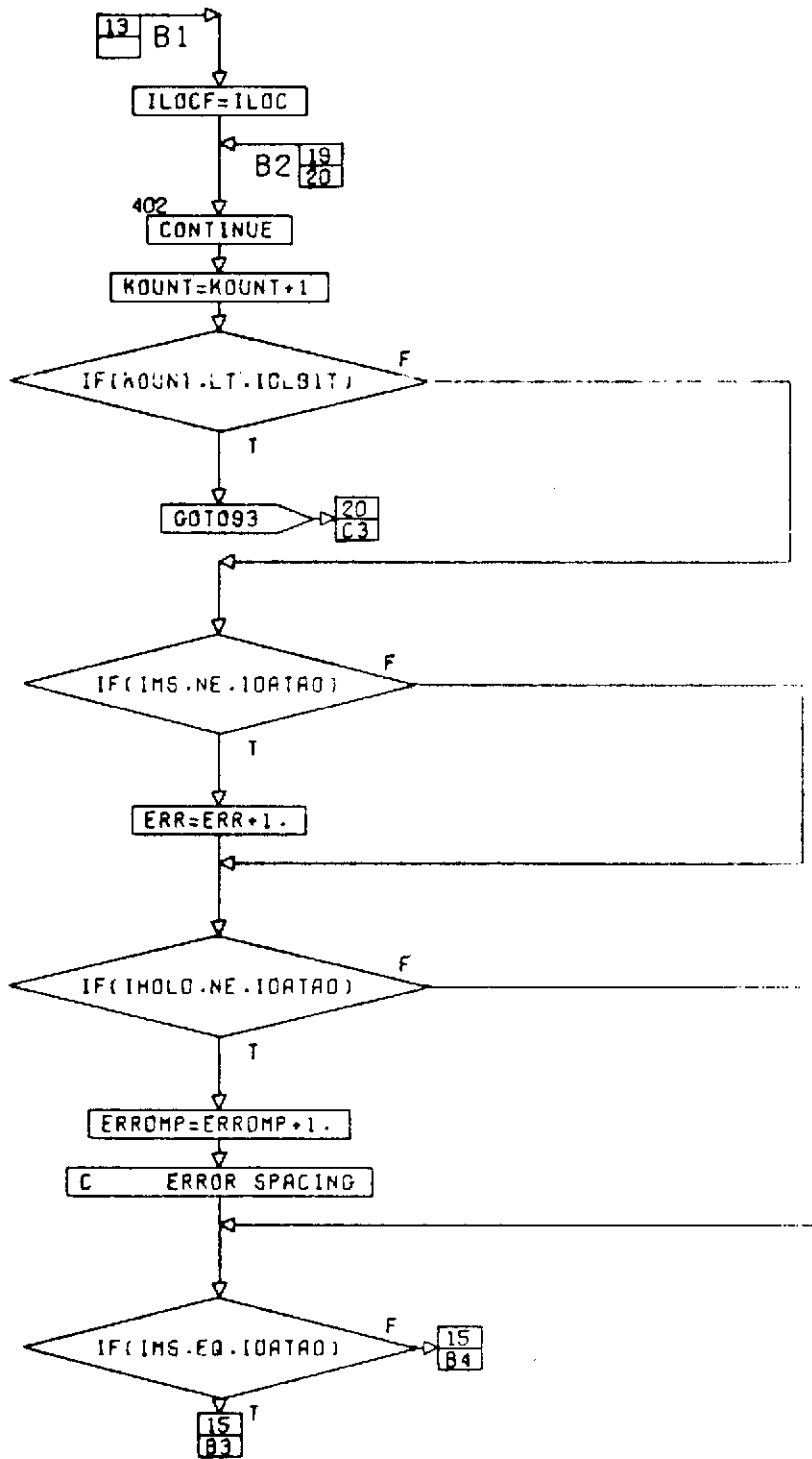


CONT. ON PG 12



CONT. ON PG 13

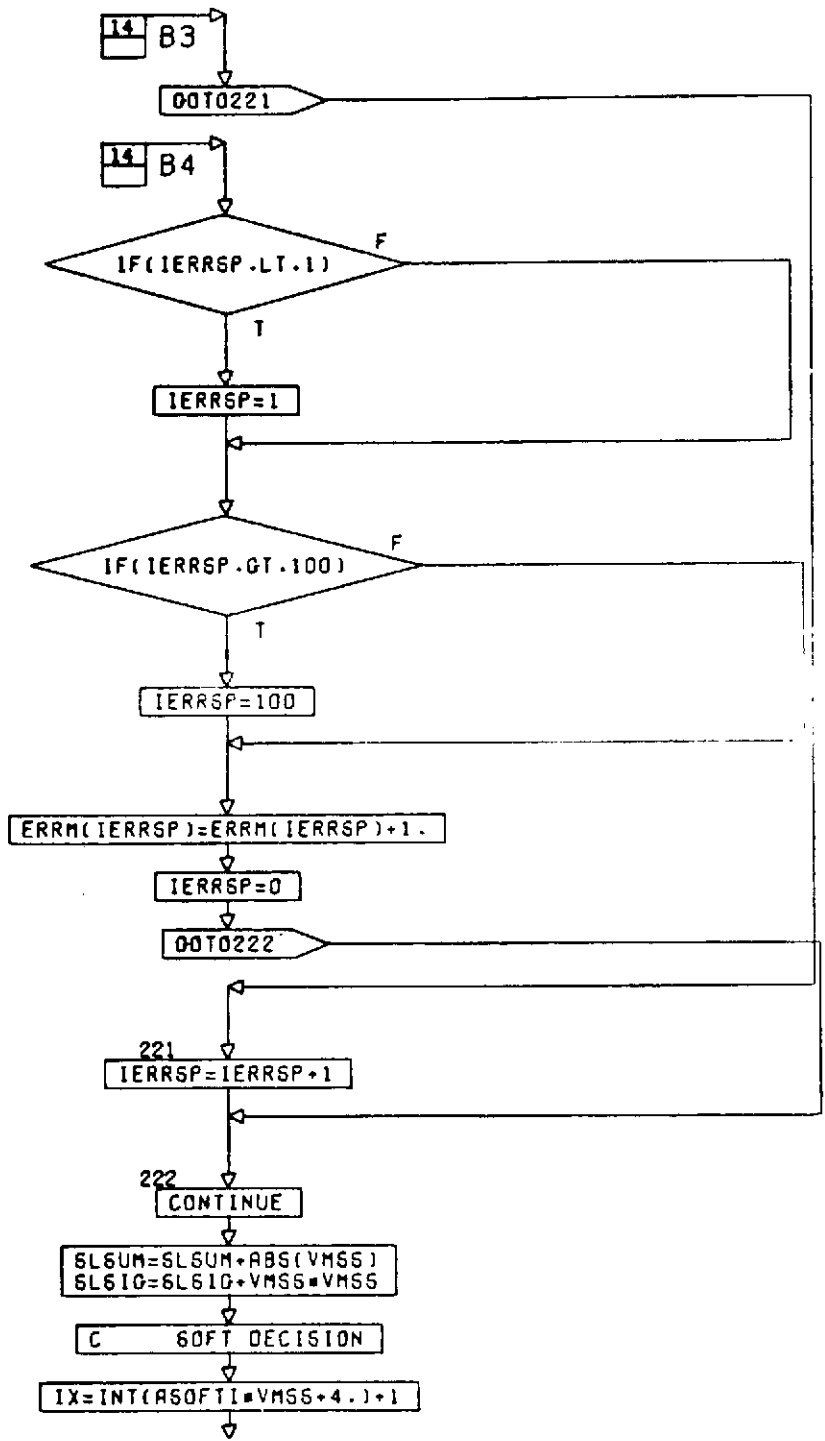


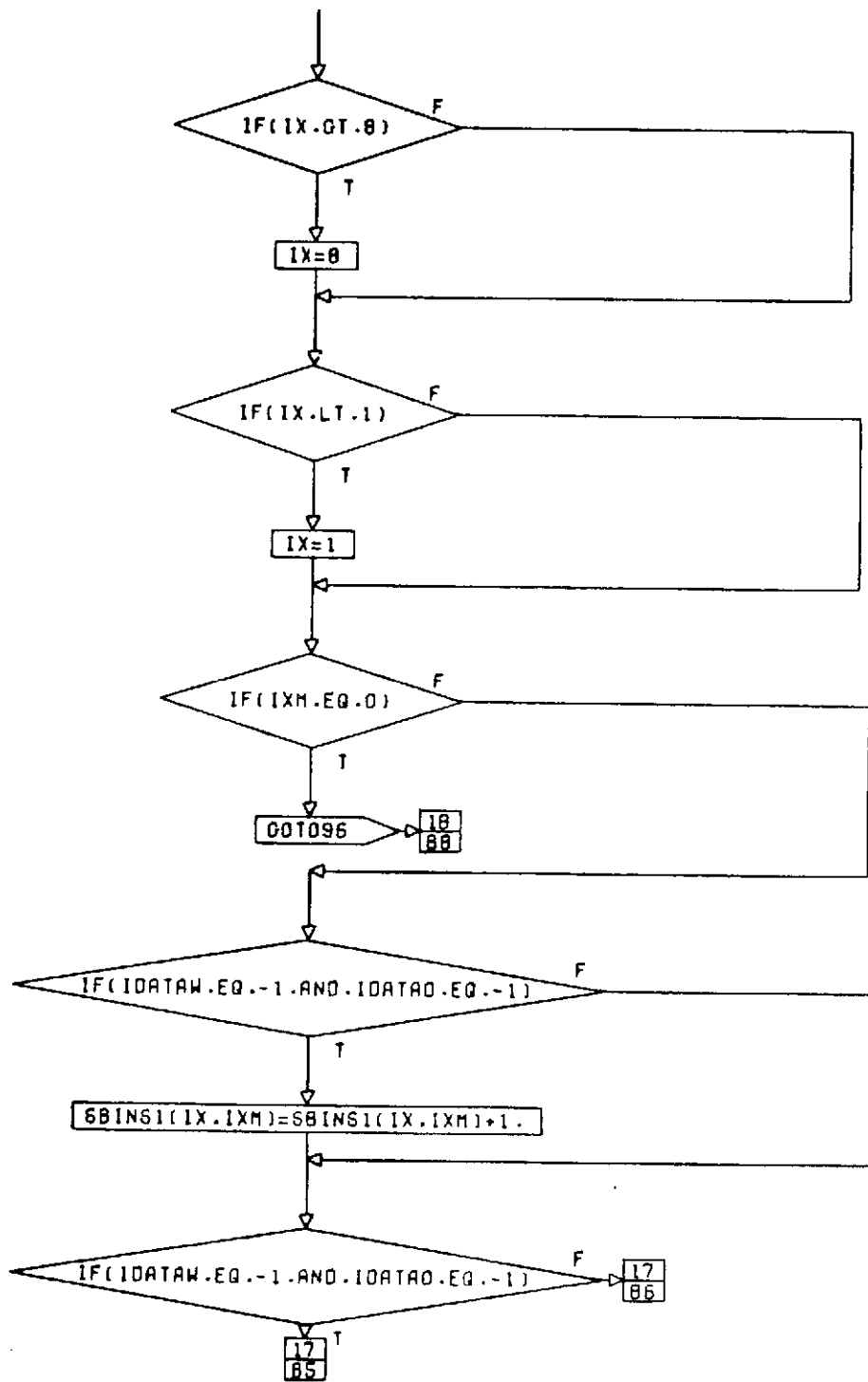


CONT. ON PG 15

PG 14 OF 23

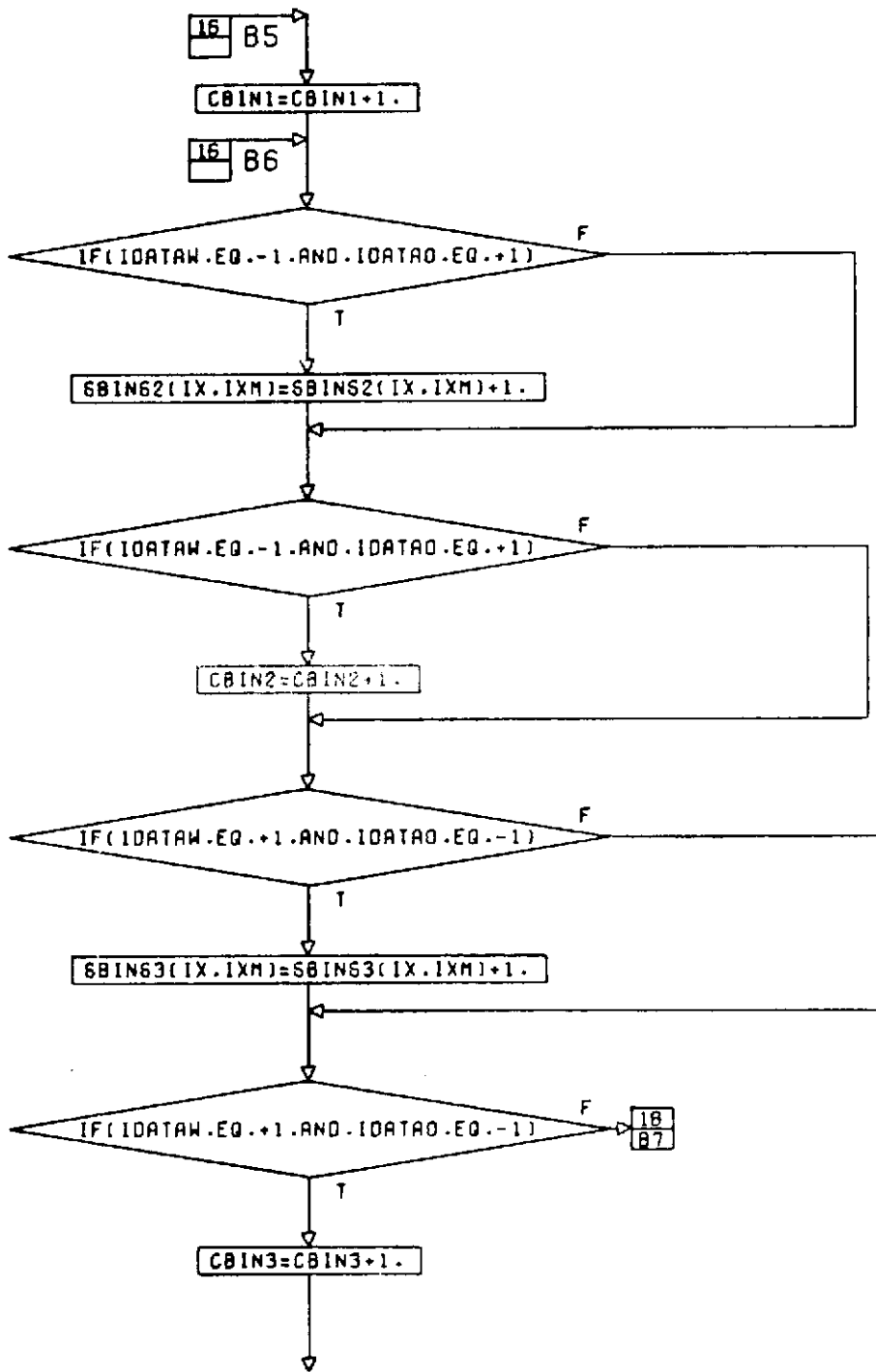
CD





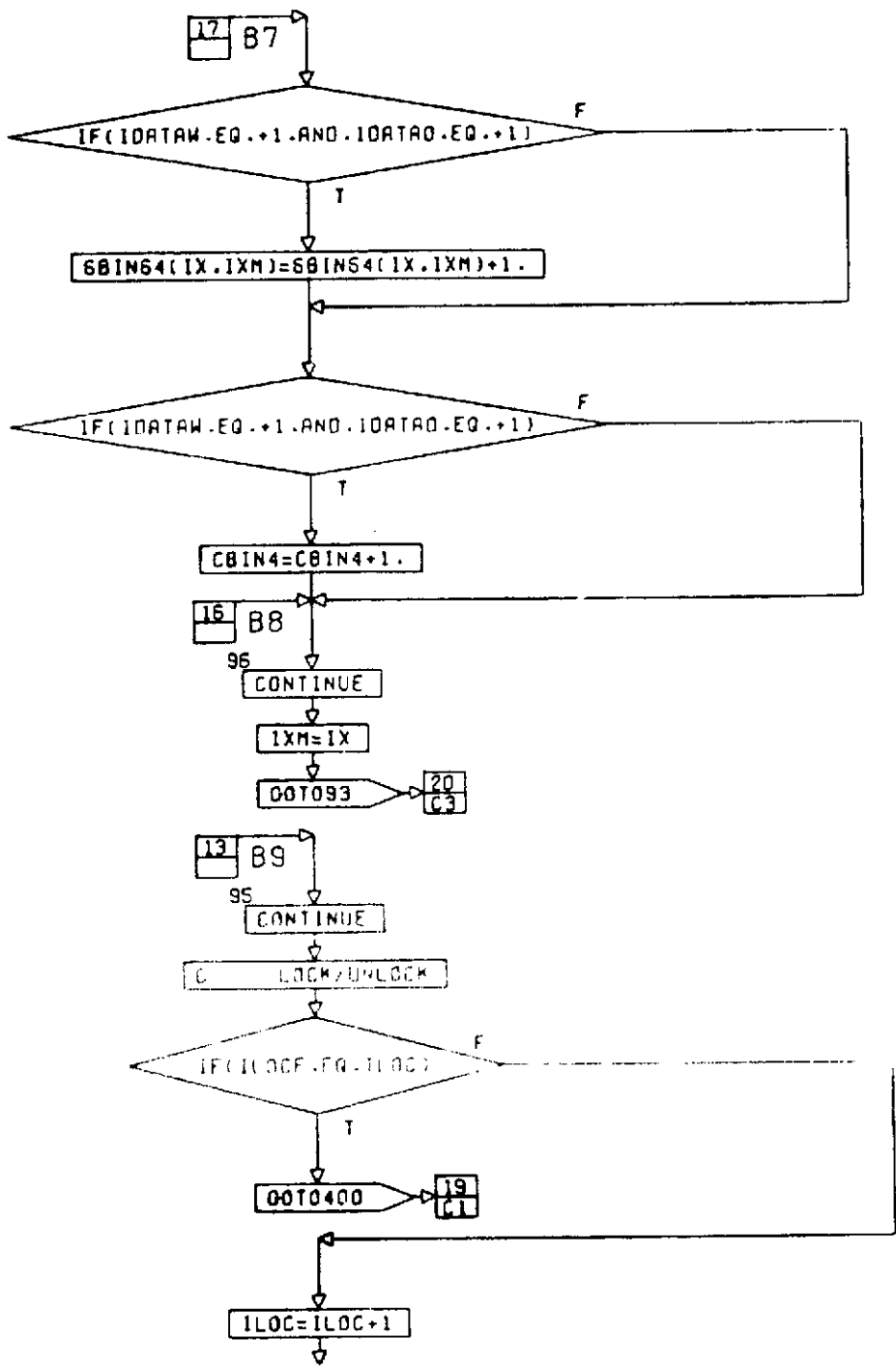
CONT. ON PG 17

PG 16 OF 23



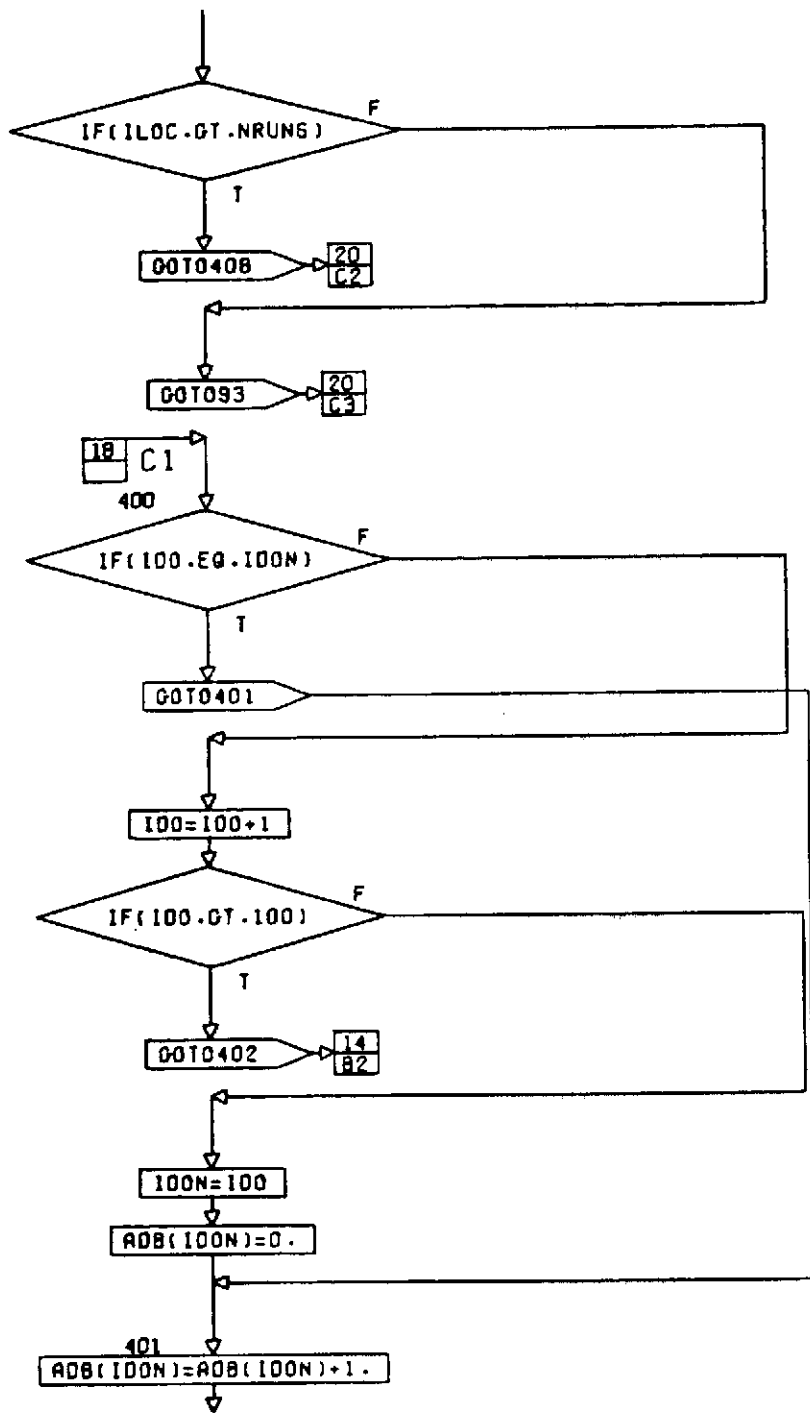
CONT. ON PG 18

PG 17 OF 23



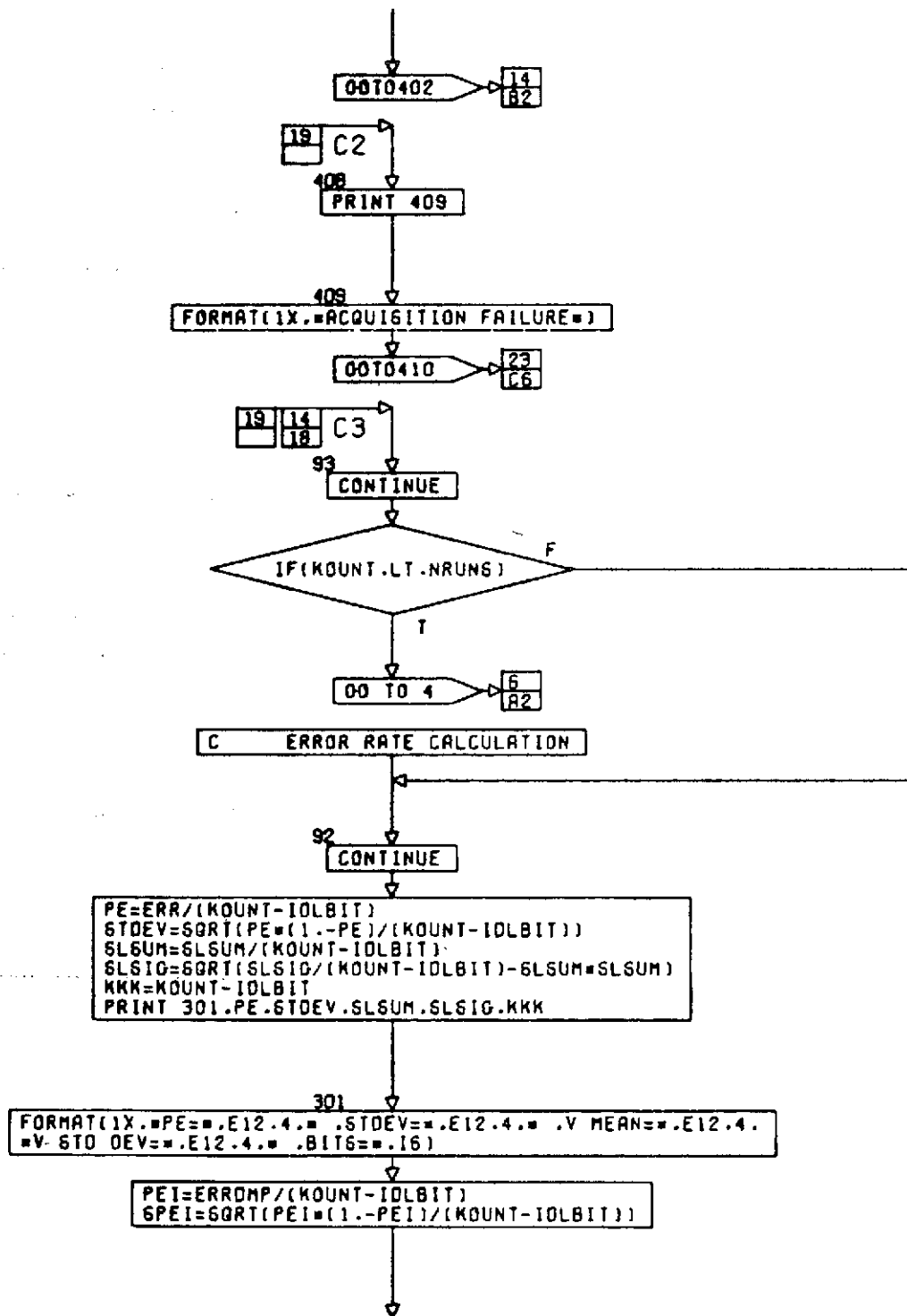
CONT. ON PG 19

PG 18 OF 23



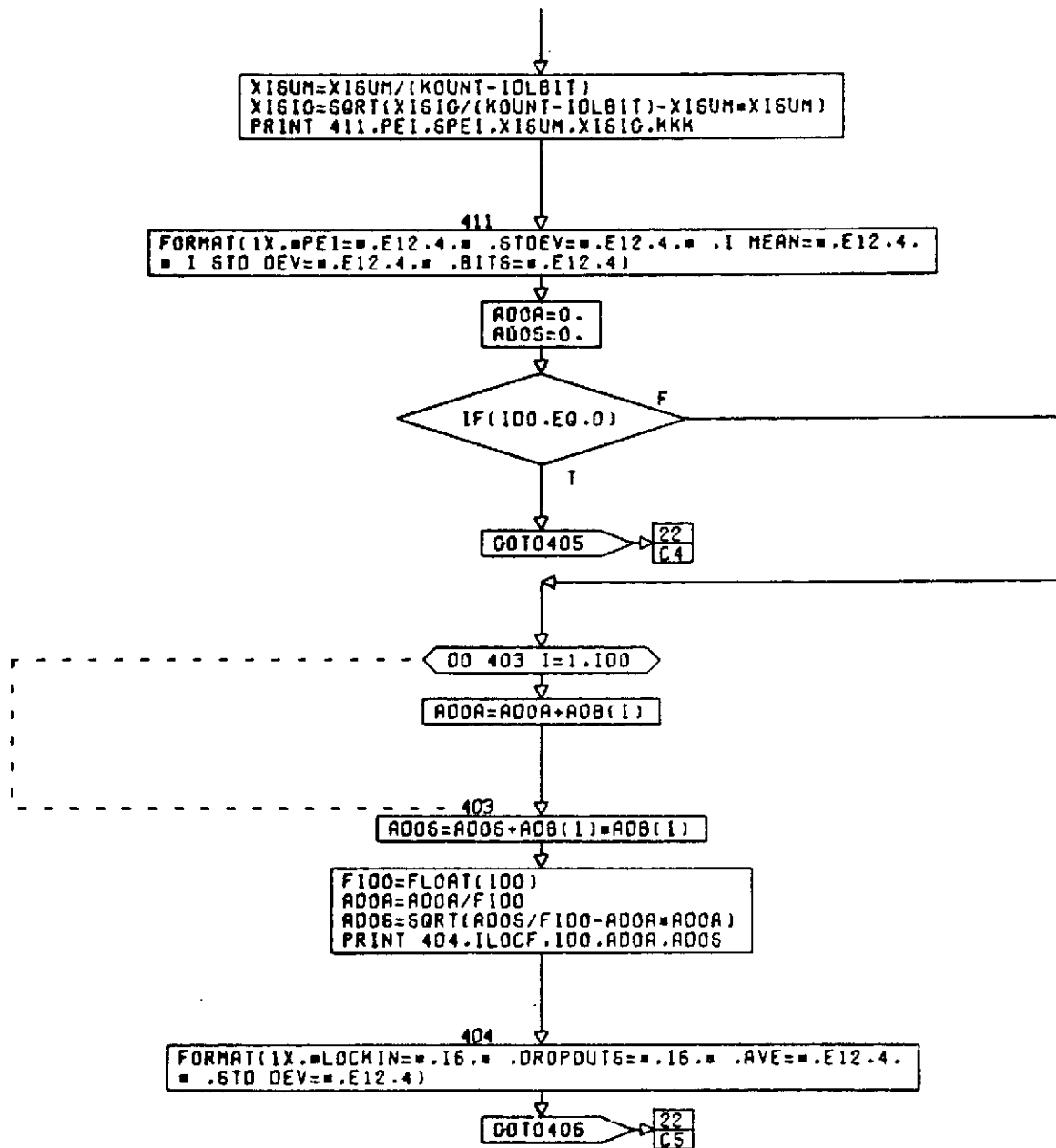
CONT. ON PG 20

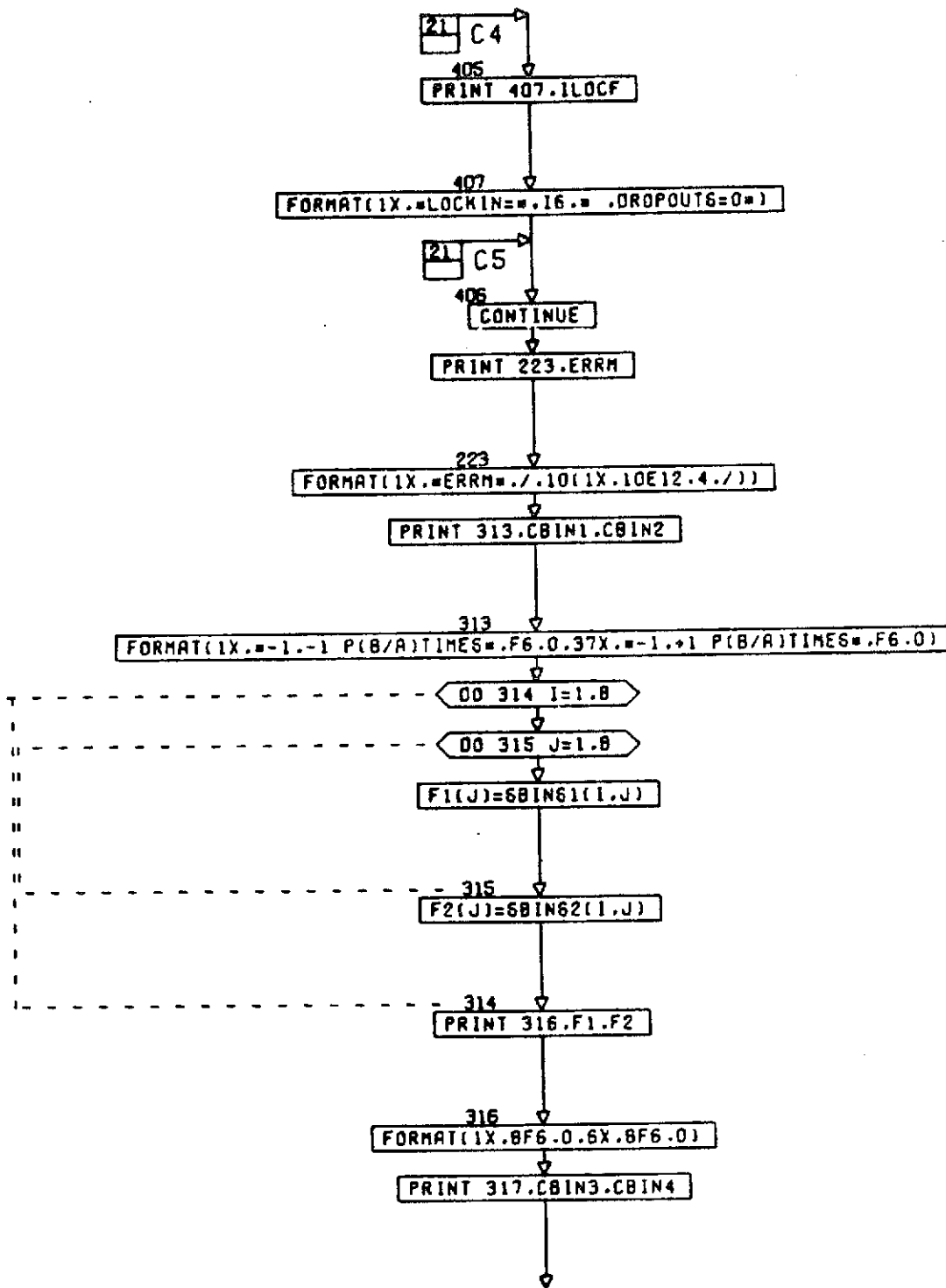
PG 19 OF 23



CONT. ON PG 21

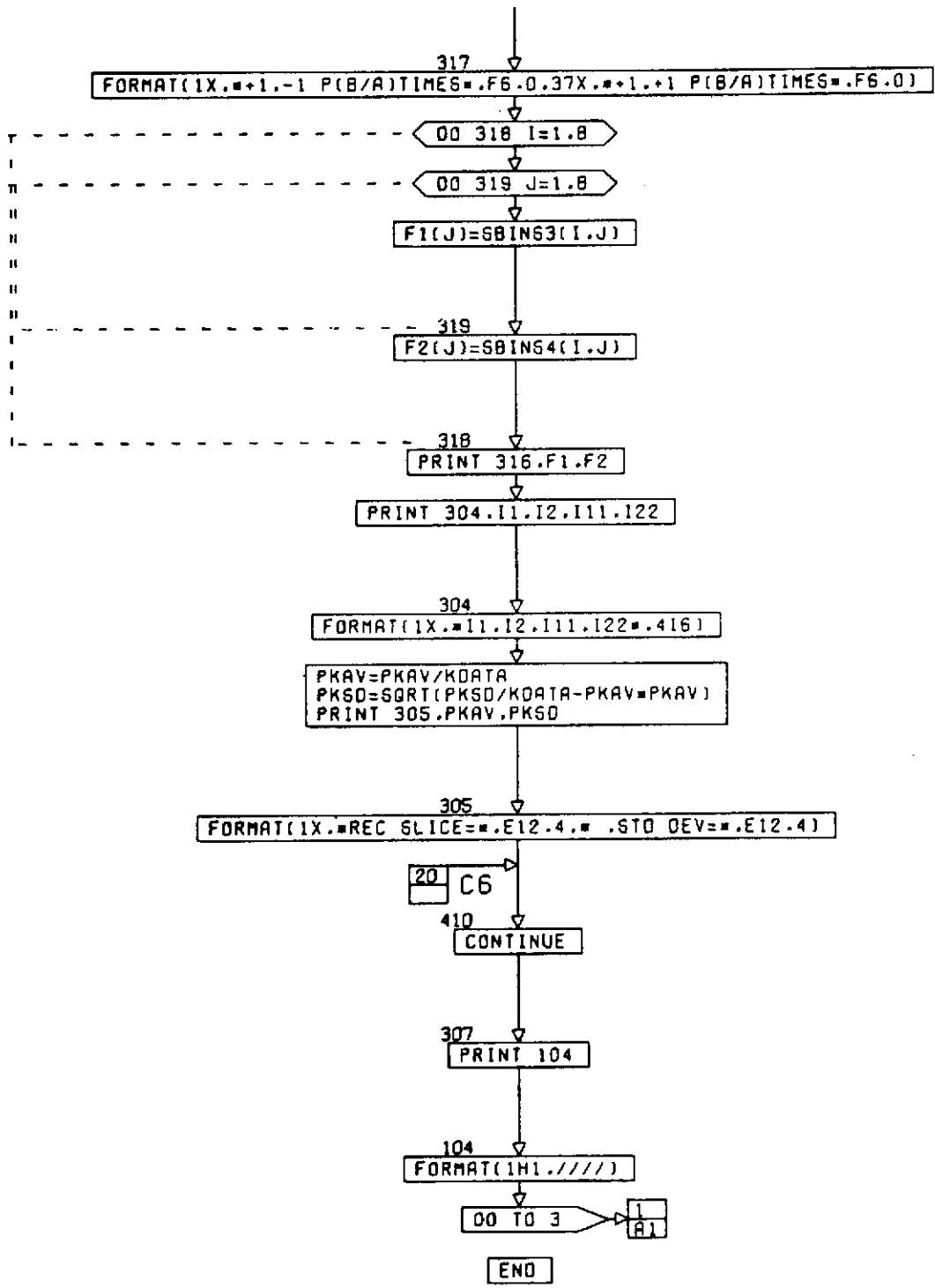
PG 20 OF 23

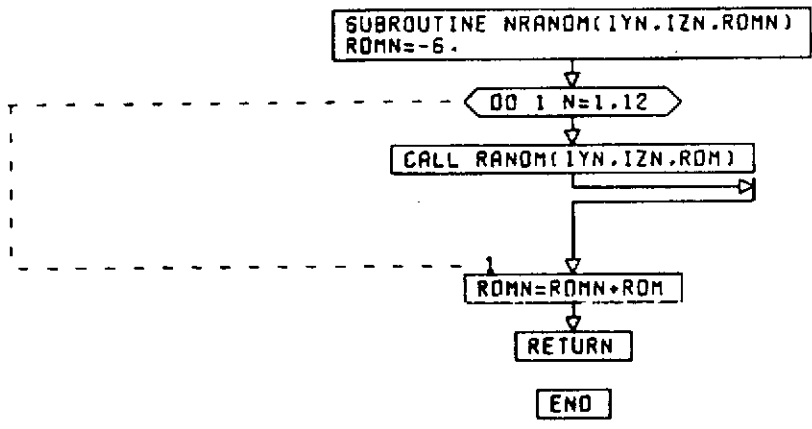




CONT. ON PG 23

PG 22 OF 23



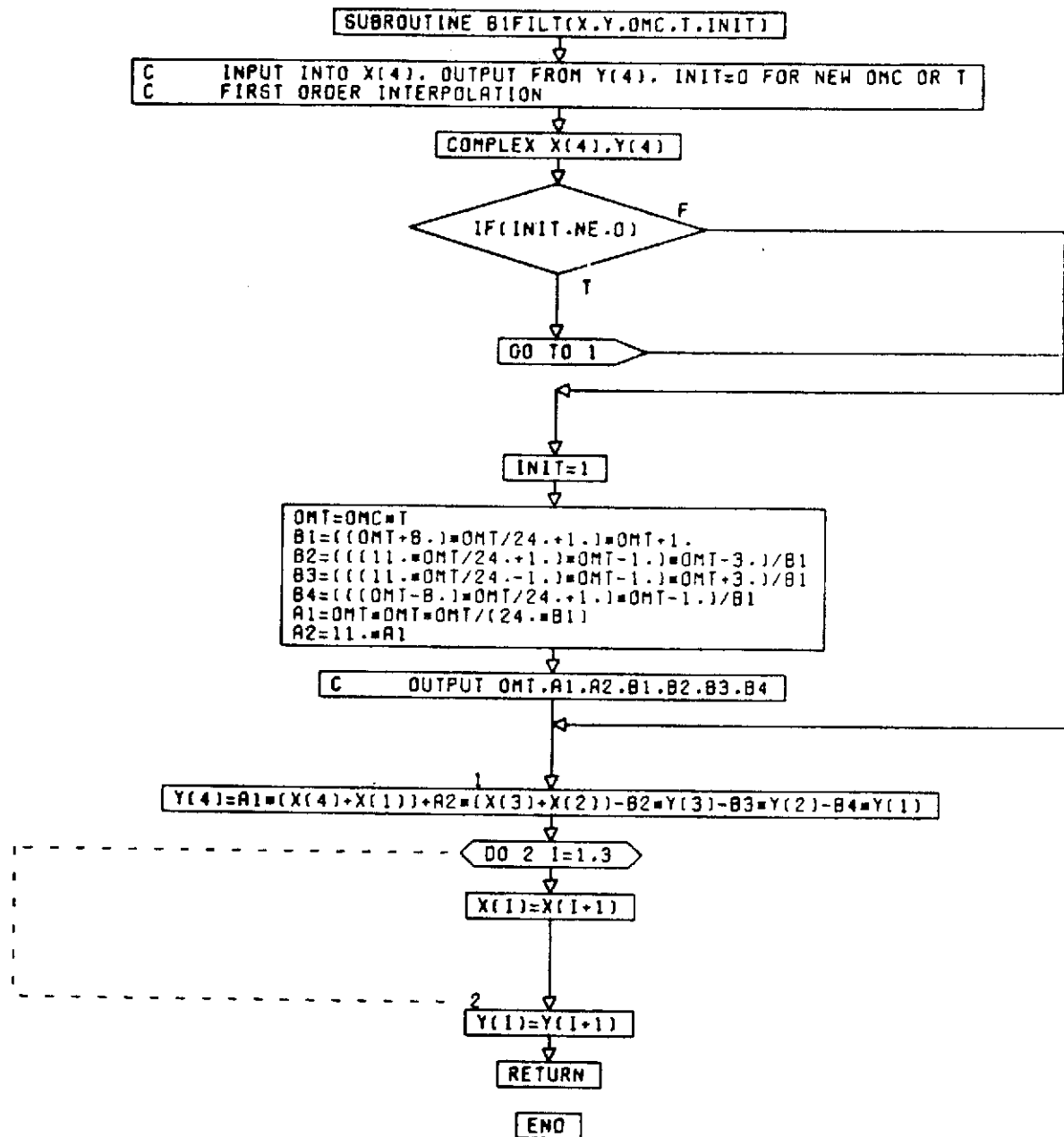


```
SUBROUTINE RANDM(IYN,IZN,RDM)
DATA IA,IB/129,1/
DATA T,IRT/4194304.,.2048/
IYN=IA+IYN+(IB+IA+IZN)/IRT
IYN=MOD(IYN,IRT)
IZN=MOD((IB+IA+IZN),IRT)
RDM=FLOAT(IYN+IRT+IZN)/T
```

↓
RETURN

END

PG 1 FINAL

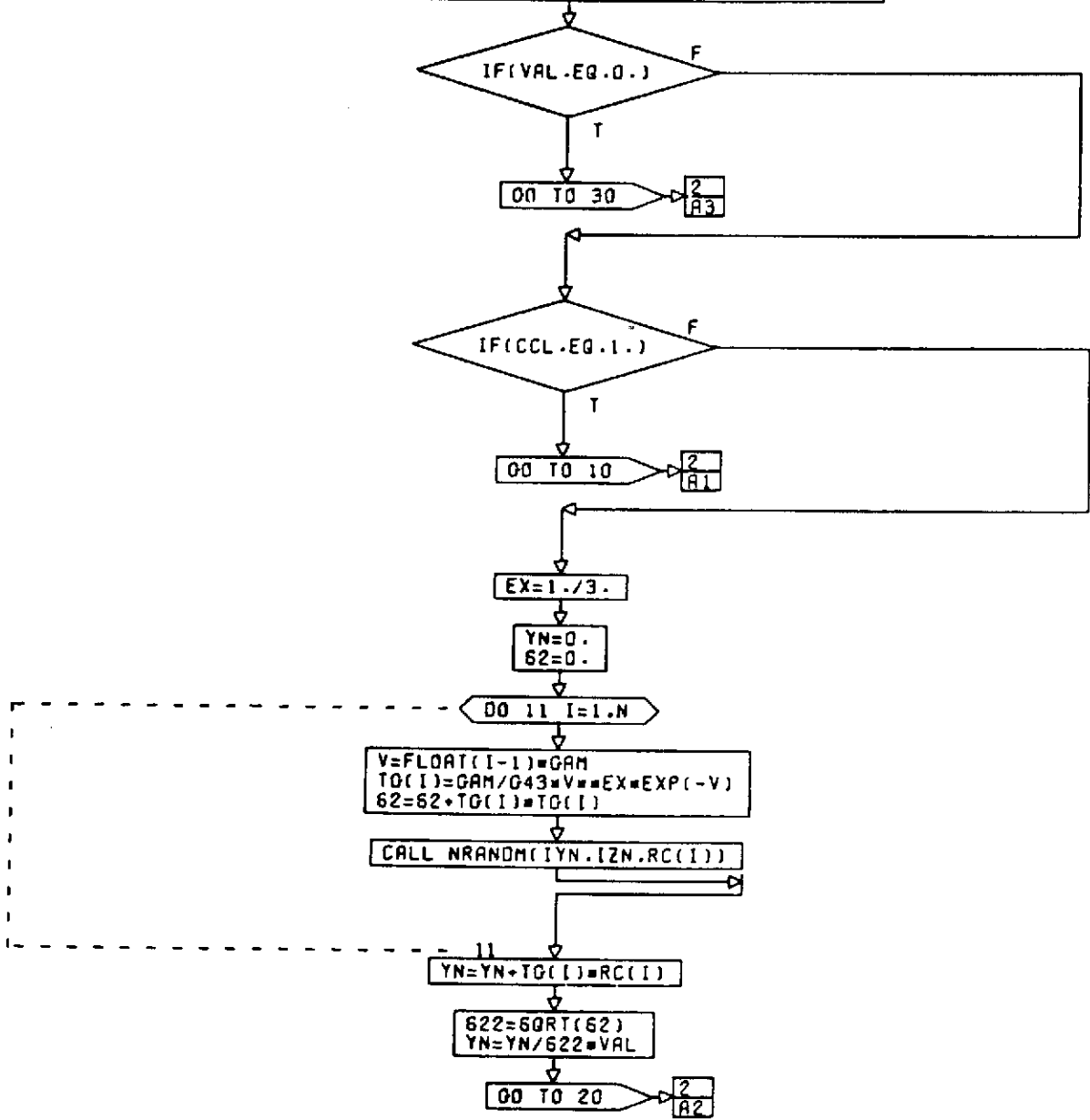


PQ 1 FINAL

```

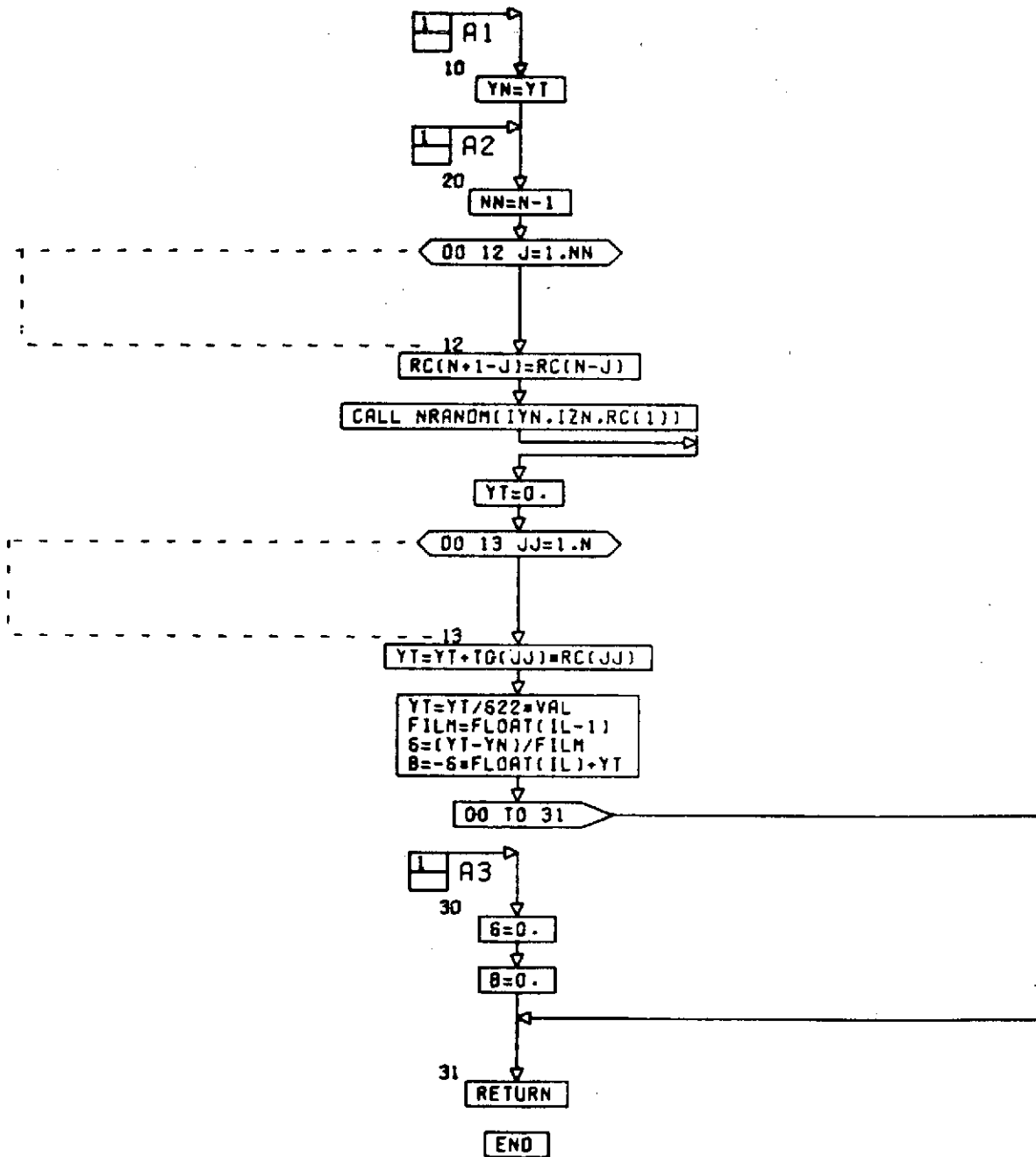
SUBROUTINE BLOBA(N,GAM,VAL,CCL,IL,S,B,IYN,IZN)
DIMENSION TG(128),RC(128)
DATA G43/.892979511/

```



CONT. ON PG 2

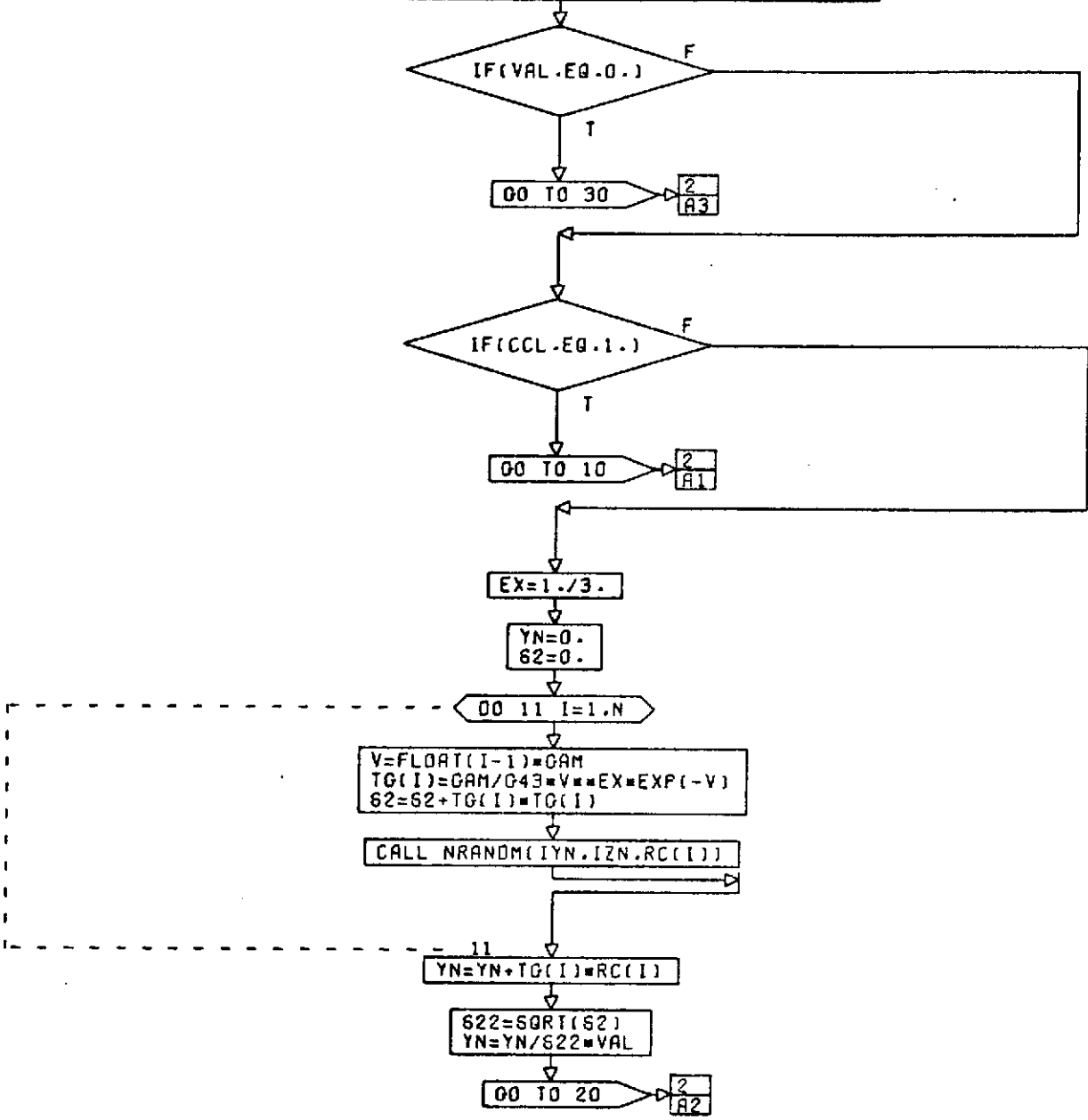
PG 1 OF 2



```

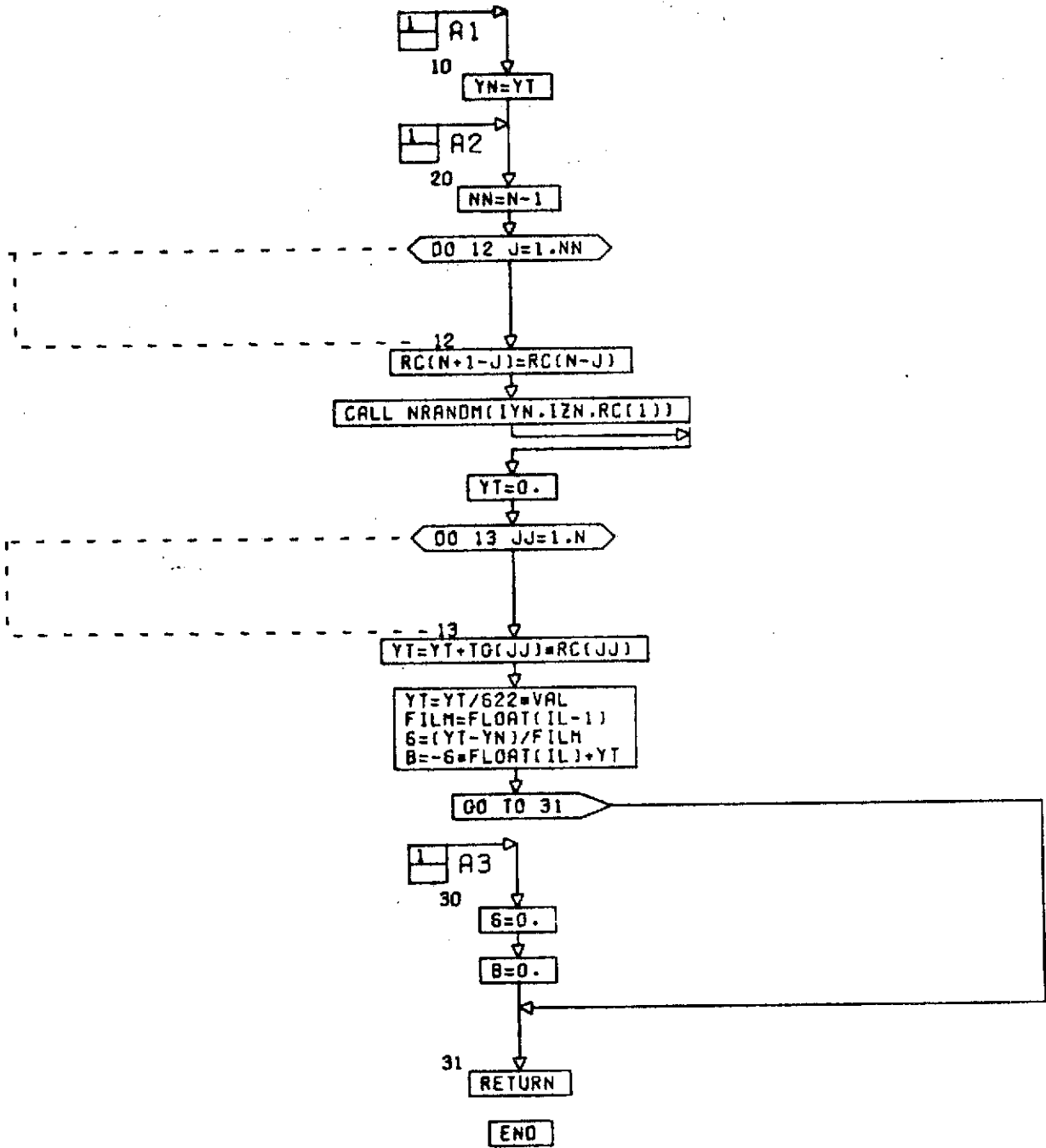
SUBROUTINE BLOBP(N,CAM,VAL,CCL,IL,S,B,IYN,IZN)
DIMENSION TG(128),RC(128)
DATA G43/.892979511/

```



CONT. ON PG 2

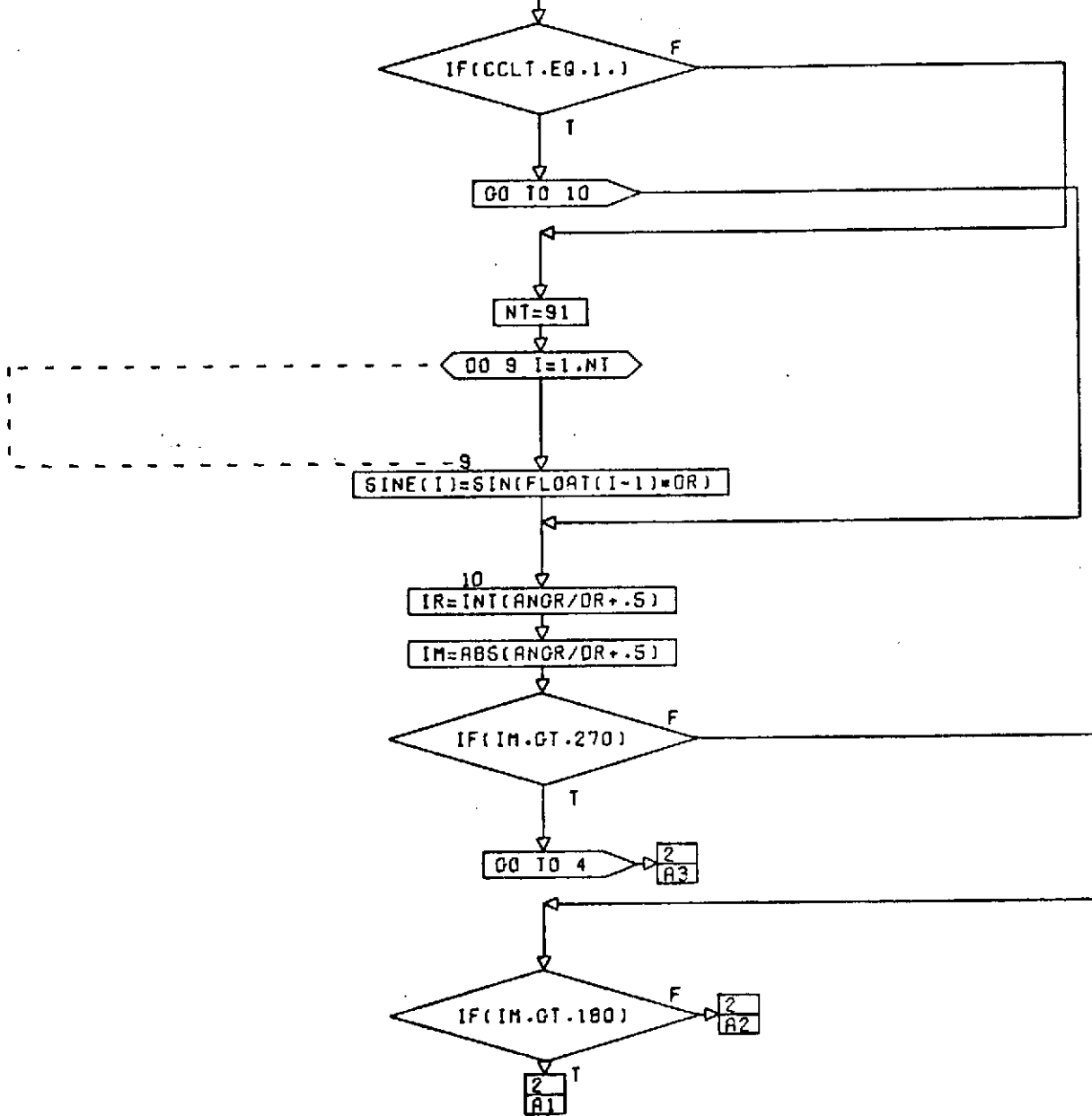
PG 1 OF 2



```

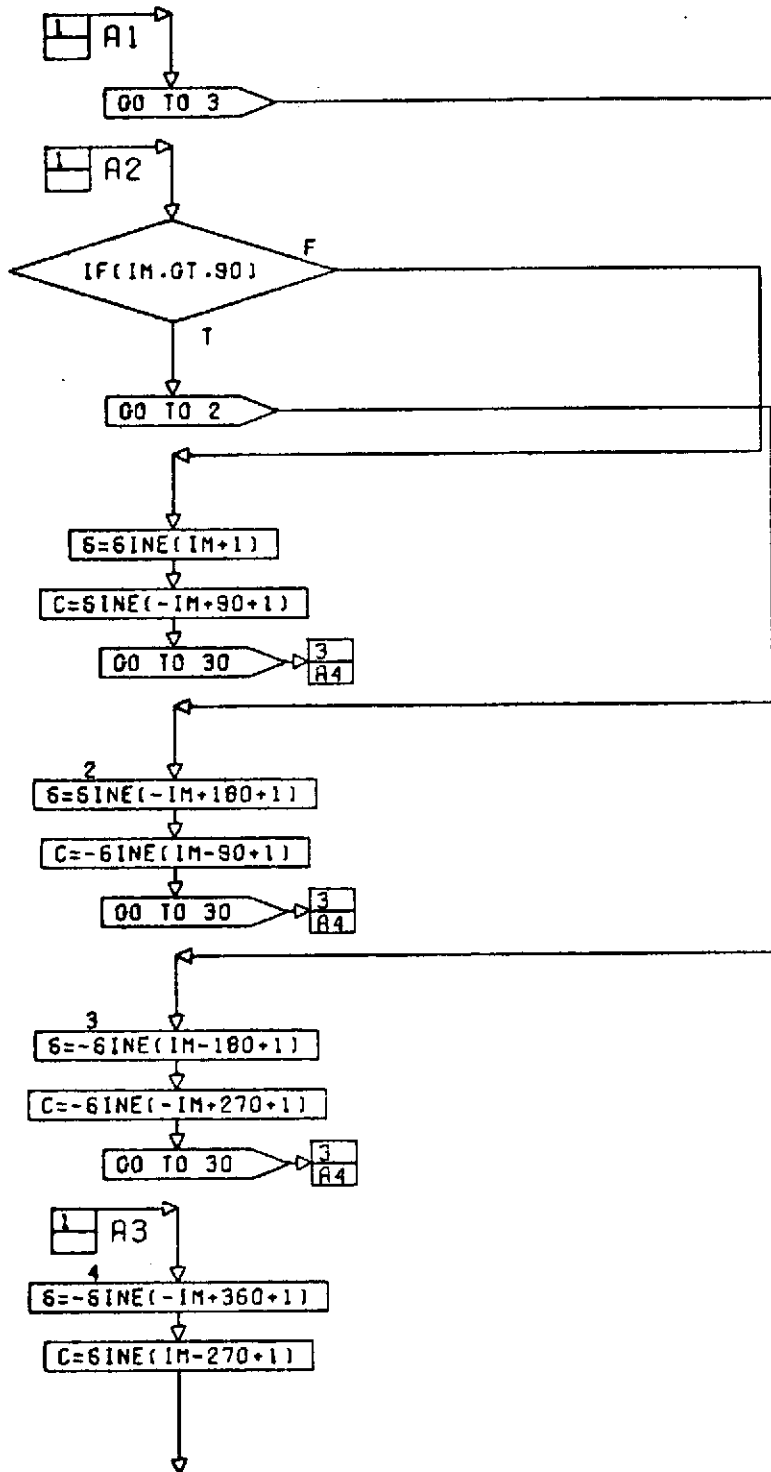
SUBROUTINE TRIG(CCLT, ANGR, S, C)
DIMENSION SINE(91)
DR = .0174532925

```

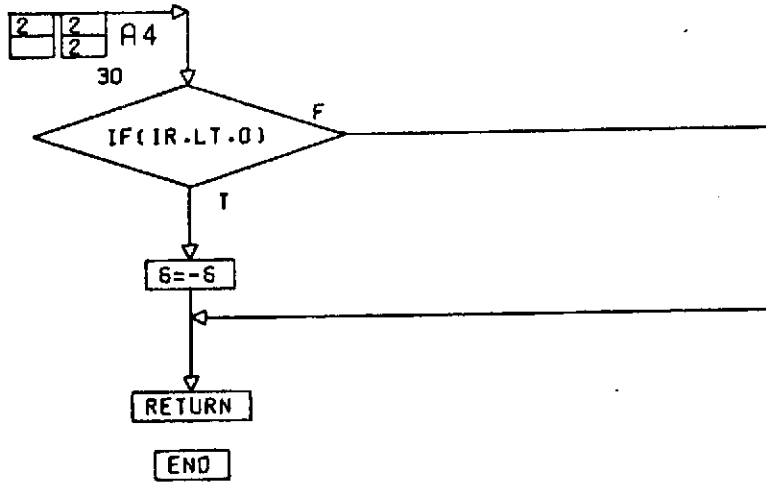


CONT. ON PD 2

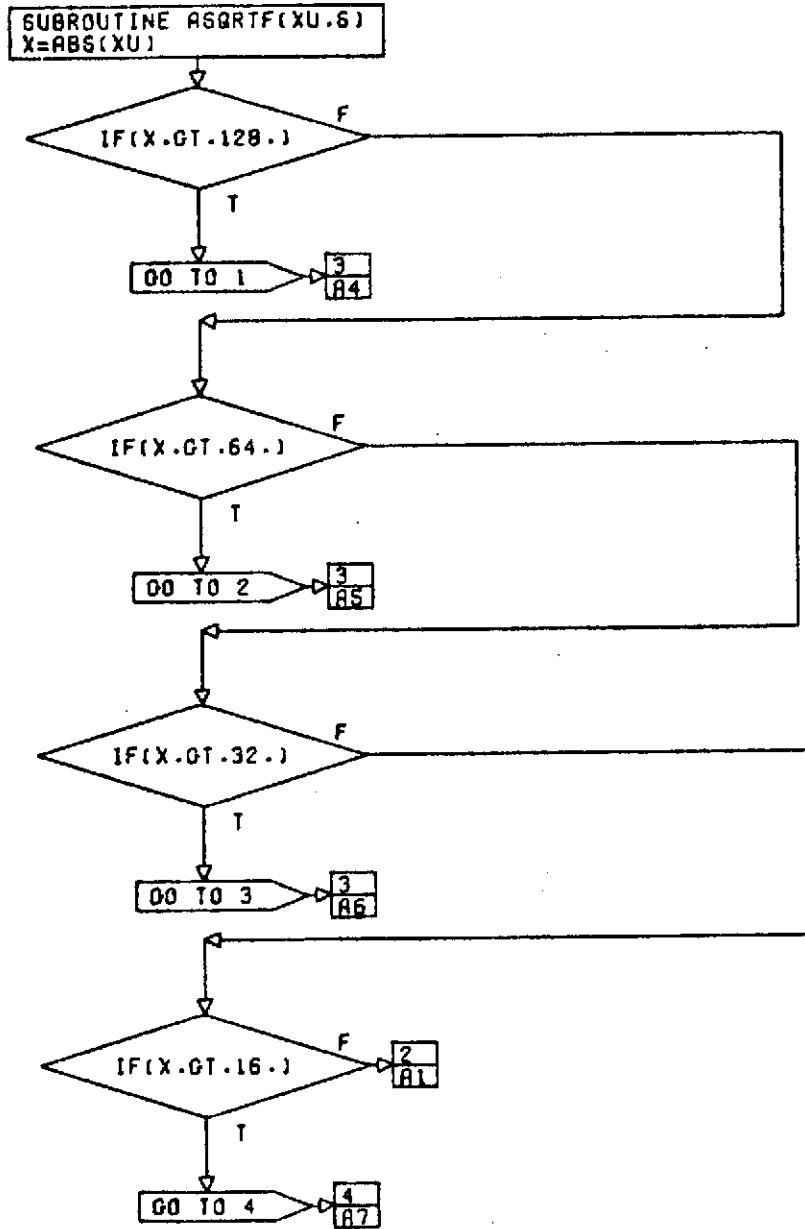
PD 1 OF 3



CONT. ON PG 3

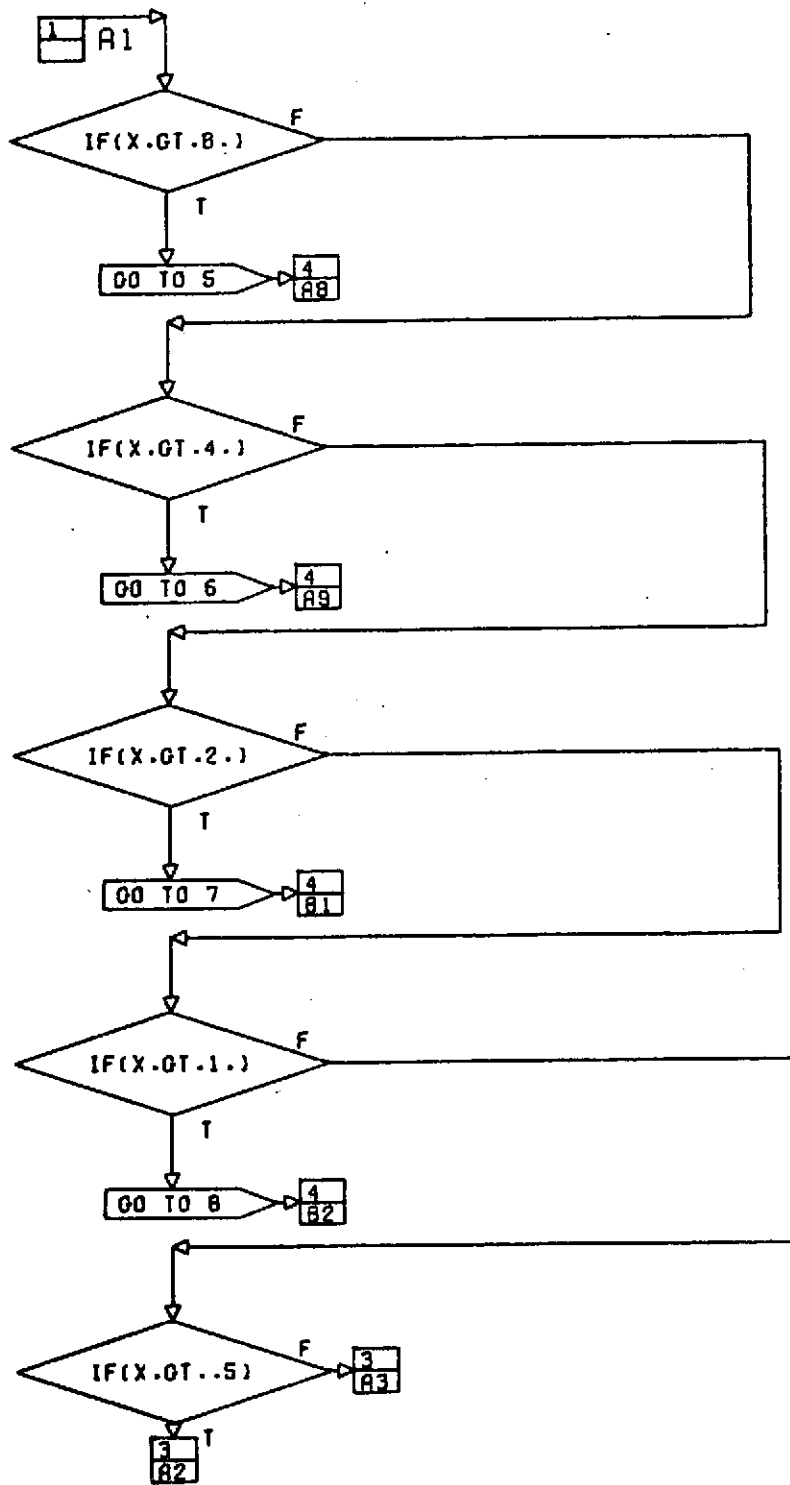


PD 3 FINAL



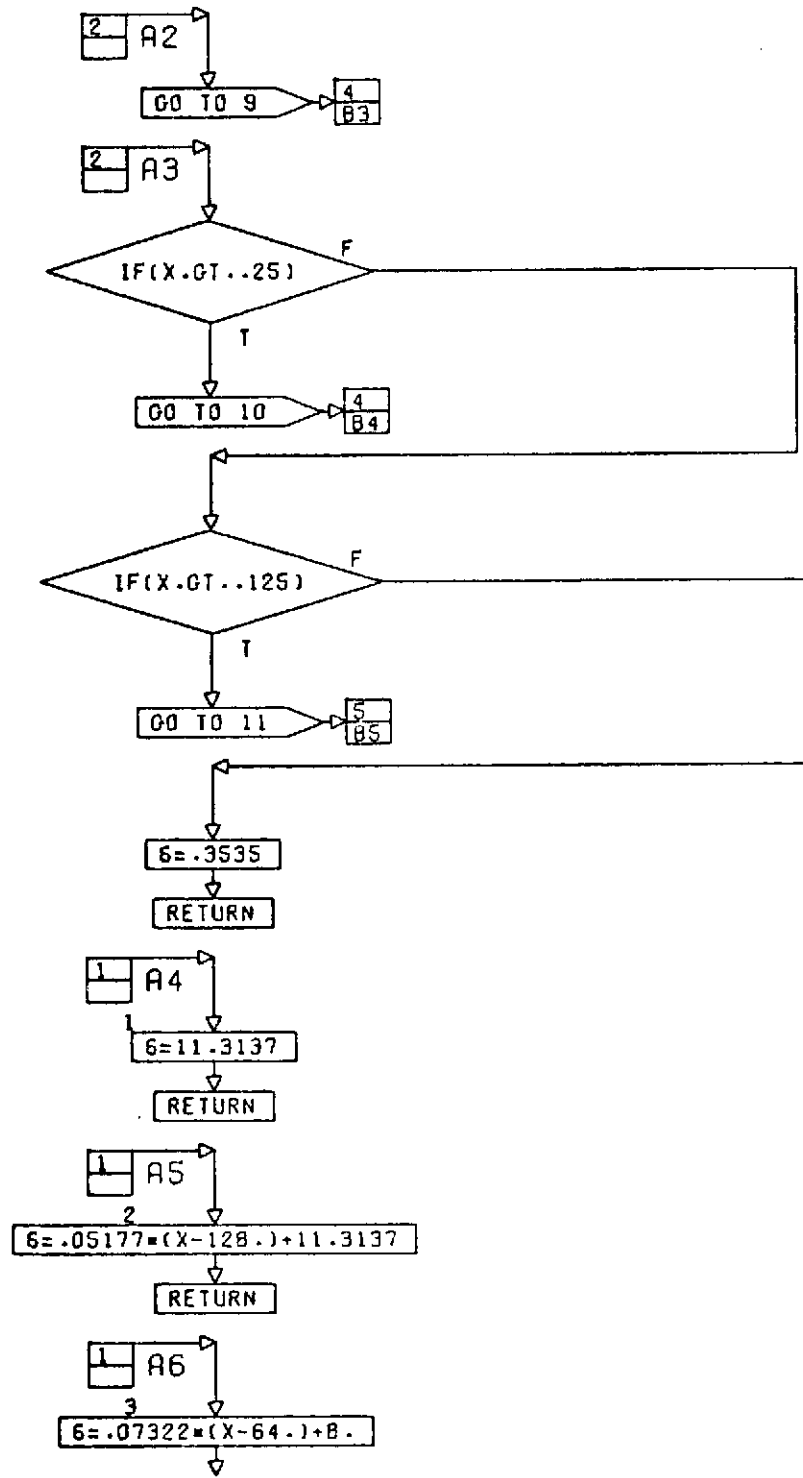
CONT. ON PG 2

PG. 1 OF 5



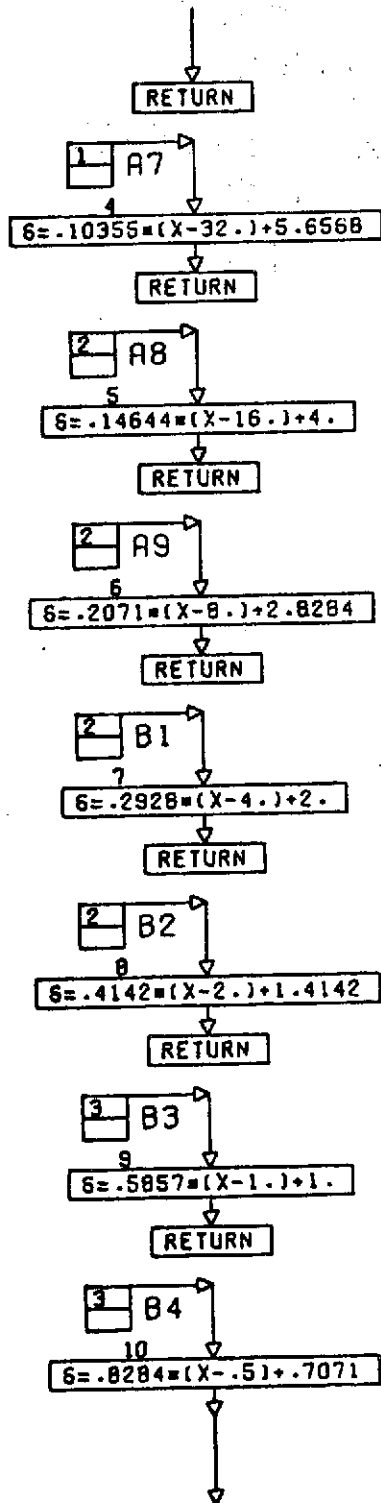
CONT. ON PG 3

PG 2 OF 5



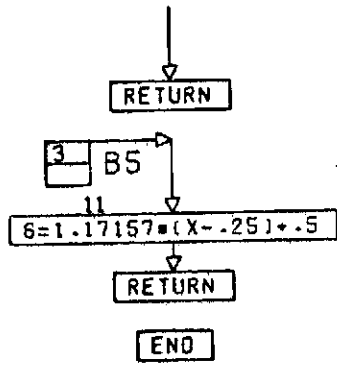
CONT. ON PG 4

PG 3 OF 5

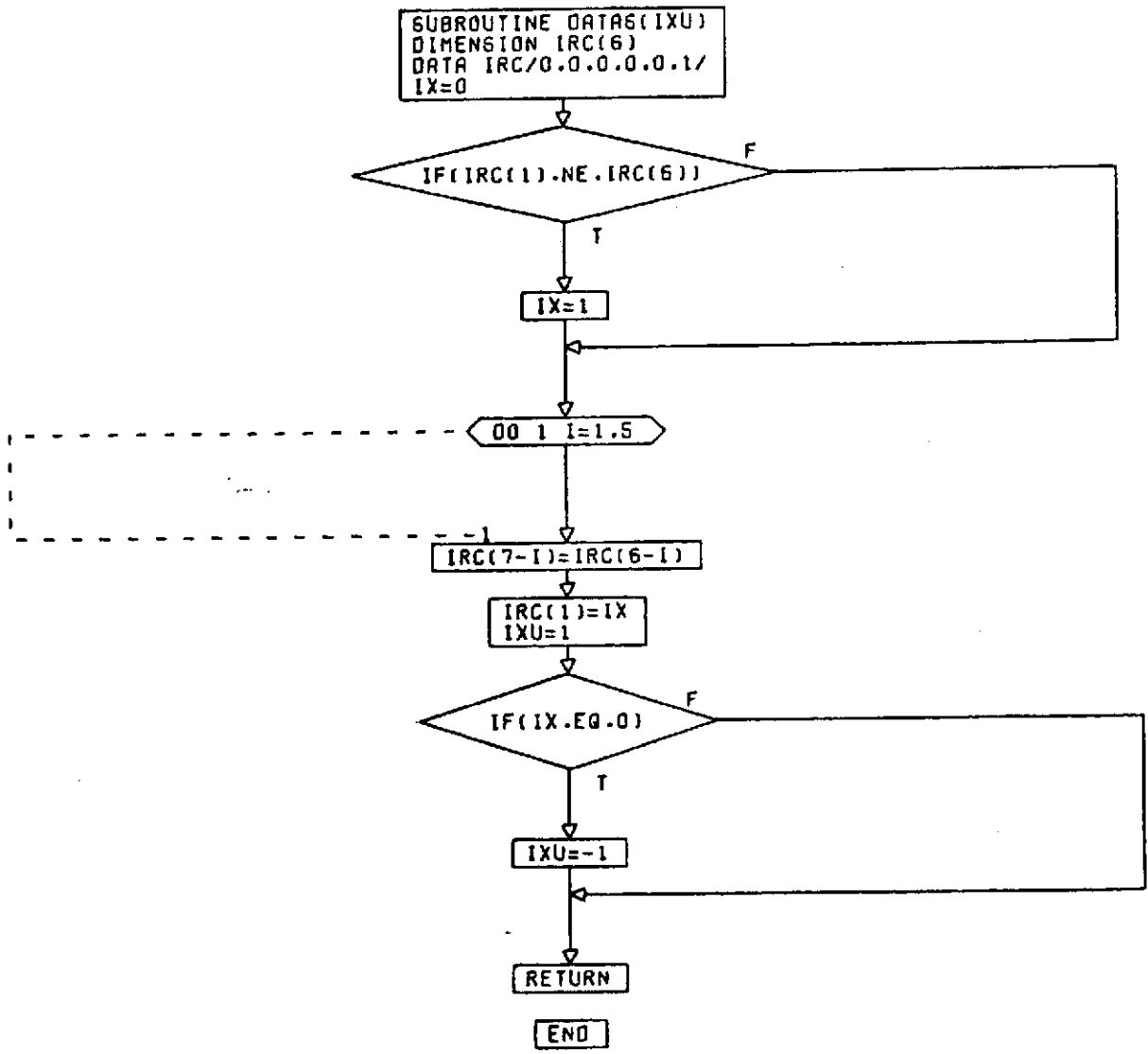


CONT. ON PD 5

PD 4 OF 5



PG 5 FINAL



PG 1 FINAL

APPENDIX VI
ACQUISITION
COMPUTER SOFTWARE

```

PROGRAM MARK(INPUT,CUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)
REAL NS,NG,NO,K,KB
COMPLEX CAMP(4),CFILT(4),COUT,CCOUT
DATA FBAMP,FBPHA,SDAMP,SDPHA,NO/2.,.2,.23,.47,1./
DATA GAM43,N43/.09,64/
DATA ENODB,BRATE,ENOMIN/8.,88.,9./
DATA DELF,NSPB,NACQT,BIF/62.,40,100,1000./
DATA RL2,PHIDEG,FOIFF/176.,10.,342.433/
DATA T1,T2,I11,I22/1,1,1,1/
DATA FRQDCP,FODPRT,TL/13.E3,10.8,-6.5/
DATA TAU3/.07957/
DATA FLO/10./
DATA SVRHZ,SWMX,SWMN/2.2E3,28.15E3,6.85E3/
DATA DYNR/3./
NAMELIST/IN1/NACQT,NSPB,ENODB,DELF,BIF,ENOMIN
+,RL2,PHIDEG,FOIFF
+,FBAMP,FBPHA,SDAMP,SDPHA,GAM43,N43
+,FLO,FRQDCP,FODPRT,I1,I2,I11,I22
+,SVRHZ,SWMX,SWMN,TL,DYNR
000003 PI=4.*ATAN(1.)
000006 PI2=2.*PI
000010 ZETA=SQRT(0.5)
000013 CALL TRIG(CCLT,PI,SSCIN,CSCIN)
000016 CCLT=1.
000020 3 CONTINUE
C READ INPUTS
000020 READ(5,IN1)
000023 NSPB=200
000024 NACQT=30
000025 SWMX=2500.
000026 FRQDCP=1000.
000030 T1=1
000031 I2=1
000032 I11=1
000033 T22=1
000034 T1S=T1
000035 I2S=I2
000037 T11S=T11
000040 I22S=T22
C CONVERT INPUTS (ENO,BPER,PHISS,PHISSB)
000042 ENO=10.** (ENODB/10.)
000050 ENOM=10.** (ENOMIN/10.)
000056 BRATE=1./BRATE
000060 DT=FBEP/NSPB
000062 PHISS=PHIDEG*PI/180.
000064 AMIN=SQRT(ENOM*NG*BRATE)
000071 AMIN2=AMIN/1.4142
000073 A=SQRT(ENO*NG*BRATE)
000080 AGC=SQRT(AMIN2)
000102 AMIN3=AMIN2/SQRT(10.** (DYNR/10.))
C CALCULATE LOOP PARAMETERS (TAU1,TAU2,K,TAUB1,TAUB2,KP)
000113 WN=RL2/(ZETA+0.25/ZETA)
000117 AK=PI2*FOIFF/SIN(PHISS)
000123 TAU1=AK/(WN*WN)
000126 TAU2=2.*(ZETA-0.5/(WN*TAU1))/WN
000132 K=AK/AMIN
000134 EDOP=PI2*FRQDCP/K

```



```

000137      EDOPR=PI2*FQDPRT*DT/K
000142      EVMAX=PI2*SWMX/K
000144      EVMIN=-PI2*SWMN/K
000146      SVR=PI2*SVRHZ/K
000150      DES=DT*SVR
C
000152      C1=1.-DT/TAU1
000155      C2=TAU2/TAU1
000156      C3=C1+C2-1.
000161      C4=DT*K
000163      C5=DT/TAU3
000164      C6=1.-C5
000165      DTH1=PI*DELF*DT
000170      SDTH0=SIN(DTH1)
000172      CDTH1=COS(DTH1)
000174      DTHX=PI2*FLO*DT
000177      SDTHX=SIN(DTHX)
000201      CDTHX=COS(DTHX)
000203      NACQ=0
000204      ACQ=0.
000205      AVEES=0.
000206      STDES=0.
000207      AKOU=0.
000210      SKOU=0.
000211      AMISS=0.
000212      AFAL=0.
000213      SIG=0.5*SQRT(N0/DT)
000221      PRINT 202,ENQDP,DELF,E1F,BL2
000234      202  FORMAT(1X,*ENQDP=*,F6.1,* ,DELF=*,F6.1,
      * ,E1F=*,F6.0,* ,BL2=*,F6.0)
000234      PRINT 204,SVRHZ,SWMX,SWMN,FLO,FRQDOP,FQDPRT
000254      204  FORMAT(1X,*SVRHZ=*,E12.4,* ,SWMX=*,E12.4,* ,SWMN=*,E12.4,
      * ,FLO=*,E12.4,* ,FRQDOP=*,E12.4,* ,FQDPRT=*,E12.4)
000254      PRINT 206,TL,DYNR,SDAMP,SOPHA,I1S,I2S,I11S,I22S
000300      206  FORMAT(1X,*TL=*,F6.2,* ,DYNR=*,F6.1,* ,SDAMP=*,F6.3,
      * ,SOPHA=*,F6.3,* ,I1,I2,I11,I22*,4I6)
000300      PRINT 207,WN,K,TAU1,TAU2
000314      207  FORMAT(1X,*WN=*,F6.1,* ,K=*,F6.1,
      * ,TAU1=*,E12.4,* ,TAU2=*,E12.4)
C
000314      400  INITIALIZE LOOPS (TH2,E0,XI,XQ,QV,QERR0,ERR)
CONTINUE
000314      IF(NACQ.EQ.1)PRINT399
000322      399  FORMAT(1X,*NACQ,AMISS,AFAL,KDATA,ES,EV,EV1*)
000322      IF(NACQ.EQ.0)GOTO396
000323      PRINT 797,NACC,AMISS,AFAL,ACQ,KDATA,ES,EV,EV1
000347      797  FORMAT(1X,I6,3E12.4,I6,3E12.4)
000347      396  CONTINUE
NACQ=NACQ+1
000351      IF(NACQ.GT.NACQT)GOTO402
000354      CAMP(1)=(0.,0.)
000356      CAMP(2)=(0.,0.)
000361      CAMP(3)=(0.,0.)
000363      CFILT(1)=(0.,0.)
000366      CFILT(2)=(0.,0.)
000370      CFILT(3)=(0.,0.)
000373      INIT=0
000373      OMC=PI*BIF
000375      TOATA=-1

```

```

000376      U=0.
000377      EV0=0.
000400      TH2=0.
000401      CTH2=1.
000403      STH2=0.
000403      CTHX=1.
000404      STHX=0.
000405      FG=0.
000406      EV=0.
000407      EDOFRX=EDCF*EDOPR
000411      EV1=EV+EDCFRX
000413      G1=1.
000414      G2=1.
000415      V=.1
000417      ES=0.
000417      STH1=0.
000420      CTH1=1.
000422      J=NSPR
C          TURBULENCE INITIALIZATION
000423      ACOR=SGRT(2.**.75-1.)
000432      AAMP=PI2*FRAMP/ACOR
000435      ALPHA=PI2*FRPHA/ACOR
000437      IAMP=INT(.5+GAM43/(AAMP*DT))
000444      IPHA=INT(.5+GAM43/(ALPHA*DT))
000447      GAM43A=DT*FLOAT(IAMP)*AAMP
000452      GAM43P=DT*FLOAT(IPHA)*ALPHA
000455      CCL=0.
000457      CALL BLC3A(N43,GAM43A,SDAMP,CCL,IAMP,SLOA,BAMP,I11,I22)
000467      CALL BLOBF(N43,GAM43P,SDPHA,CCL,IPHA,SLOP,BPHA,I11,I22)
000500      CCL=1.
000501      IAMP0=0
000502      IPHAC=0
C          SELECT DATA (IDATA)
000503      KDATA=0
000505      4      CONTINUE
000505      IAMP0=IAMP0+1
000507      IPHAC=IPHAC+1
000510      IF(IAMP0.GT.IAMP) GO TO 10
000513      13     IF(IPHAC.GT.IPHA) GO TO 11
000517      GO TO 12
000517      10     IAMP0=1
000520      CALL BLC3A(N43,GAM43A,SDAMP,CCL,IAMP,SLOA,BAMP,I11,I22)
000531      GO TO 13
000532      11     IPHAC=1
000533      CALL BLOBF(N43,GAM43P,SDPHA,CCL,IPHA,SLOP,BPHA,I11,I22)
000544      12     CONTINUE
000544      YA=SLOA*FLOAT(IAMP0)+BAMP
000547      YP=SLOP*FLOAT(IPHAC)+BPHA
000553      CALL TRTG(CCLT,YP,SSCIN,CSCIN)
000556      IF(J.LT.NSPR) GO TO 1
000561      J=0
000561      CALL DATAS(IDATA)
000567      SDTH1=SDTH0*IDATA
000567      KDATA=KDATA+1
C          DEFINE INPUTS (TH1,NS,NC)
000567      1      CONTINUE
000567      TEMP=STHX*CDTHX+CTHX*SDTHX
000573      CTHX=CTHX*CDTHX-STHX*SDTHX

```

```

000575      STHX=TEMP
000576      TEMP=STH1*CDTH1+CTH1*SDTH1
000602      CTH1=CTH1*CDTH1-STH1*SDTH1
000604      STH1=TEMP
000604      ASTH1=1.4142*A*(1.+YA)*(STH1*CSCIN+CTH1*SSCIN)
000614      ACTH1=1.4142*A*(1.+YA)*(CTH1*CSCIN-STH1*SSCIN)
000625      CALL NRANDOM(I1,I2,X)
000627      NC=X*SIG
000631      CALL NRANDOM(I1,I2,X)
000634      NS=X*SIG
000636      J=J+1
-----
C      LOOP EQUATIONS
000640      CAMP(4)=CMPLX(ASTH1*NC,-ACTH1-NS)*CMPLX(CTH2,-STH2)*G1
000657      CALL B1FILT(CAMP,CFILT,CMC,DT,INIT)
000662      CCOUT=G2*CFILT(4)
000670      COUT=CCOUT
000672      V=C6*V+C5*U
-----
000676      VD=V
000676      IF(ABS(VD).LT.AMIN3)VD=AMIN3
000703      IF(VD.NE.0.)CALL ASORTF(VD,VSORT)
000706      G1=AGC/VSORT
000710      G2=G1
000711      U=AIMAG(COUT)*CTHX-REAL(COUT)*STHX
000716      E=REAL(COUT)*CTHX+AIMAG(COUT)*STHX+ES
000723      EV=C1*EV+C2*E-C3*E0
000730      EV1=EV0-EDOPRX
000732      IF(EV.GT.EVMAX)GOTO500
000736      IF(V.LT.TL)GOTO401
-----
C      IF(EV.GT.EVMAX)DES=-DES
C      IF(EV.LT.EVMIN)DES=-DES
000740      EDOPRX=EDOPRX+EDOPR
000741      TH2=TH2+C4*EV1
000744      TH2=AMOD(TH2,PI2)
000750      CALL TRIG(CCLT,TH2,STH2,CTH2)
000753      EV0=EV
000754      E0=E
000756      EV10=EV1
000757      IF(V.GT.TL)ES=ES+DES
000764      GOTO4
000765      401 CONTINUE
-----
C      MAYBE AN ACQUISITION
000765      IF(ES.LT.EDOPRX)GOTO501
000770      ACQ=ACQ+1
000772      AVEES=AVEES+ES
000773      STDES=STDES+ES*ES
000776      AKOU=AKOU+FLOAT(KDATA)
001000      SKOU=SKOU+FLOAT(KDATA)*FLOAT(KDATA)
001002      GOTO400
001003      402 PACQ=ACQ/FLOAT(NACQT)
001005      IF(ACQ.EQ.0.)GOTO504
001006      STDEV=SQRT(PACQ*(1.-PACQ)/FLOAT(NACQT))
001013      AVEES=AVEES/ACQ
001015      STDES=SQRT(STDES/ACQ-AVEES*AVEES)
001022      AKOU=AKOU/ACQ
001024      SKOU=SQRT(SKOU/ACQ-AKOU*AKOU)
001032      PRINT 403,PACQ,STDEV
001041      403 FORMAT(1X,*PACQ=*,E12.4,* ,STDEV=*,E12.4)
001041      PRINT 404,AVEES,STDES

```

```

001051 404 FORMAT(1X,*AVEES=*,E12.4,* ,STDES=*,E12.4)
001051 PRINT 405,AKOU,SKOU
001061 405 FORMAT(1X,*AVE KDATA=*,E12.4,* ,STD DEV=*,E12.4)
001061 506 CONTINUE
001061 PMISS=AMISS/FLOAT(NACQT)
001064 PRINT 502,PMISS
001071 502 FORMAT(1X,*PR MISSED ACQ=*,E12.4)
001071 PFAL=AFAL/FLOAT(NACQT)
001074 PRINT 503,PFAL
001101 503 FORMAT(1X,*PP FALSE ACQ=*,E12.4)
001101 PRINT 304,I1,I2,I11,I22
001115 304 FORMAT(1X,*I1,I2,I11,I22*,4I6)
001115 307 PRINT 104
001121 104 FORMAT(1H1)
001121 GO TO 3
001122 500 CONTINUE
C MISSED ACQ
001122 AMISS=AMISS+1.
001124 GOTO400
001125 501 CONTINUE
C FALSE ACQ
001125 AFAL=AFAL+1.
001127 GOTO400
001130 504 PRINT 505
001134 505 FORMAT(1X,*NO ACQUISITIONS*)
001134 GOTO506
001135 END

```

```

SUBROUTINE NRANDM(IYN,IZN,RDMN)
RDMN=-6.
DO 1 N=1,12
CALL RANDM(IYN,IZN,RDM)
1 RDMN=RDMN+RDM
RETURN
END

```

```

SUBROUTINE RANDM(IYN,IZN,RDM)
DATA IA,IB/129,1/
DATA T,IRT/4194304.,2048/
IYN=IA*IYN+(IB+IA*IZN)/IRT
IYN=MOD(IYN,TPT)
IZN=MOD((IB+IA*IZN),IRT)
RDM=FLOAT(IYN*IRT+IZN)/T
RETURN
END

```

```

SUBROUTINE B1FILT(X,Y,OMC,T,INIT)
C INPUT INTO X(4), OUTPUT FROM Y(4), INIT=0 FOR NEW OMC OR T
C FIRST ORDER INTERPOLATION
000010 COMPLEX X(4),Y(4)
000010 IF(INIT.NE.0) GO TO 1
000011 INIT=1
000011 OMT=OMC*T
000012 B1=((OMT+8.)*OMT/24.+1.)*OMT+1.
000020 B2=((11.*OMT/24.+1.)*OMT-1.)*OMT-3.)/B1
000027 B3=((11.*OMT/24.-1.)*OMT-1.)*OMT+3.)/B1
000035 B4=((OMT-8.)*OMT/24.+1.)*OMT-1.)/B1
000044 A1=OMT*OMT*OMT/(24.*B1)
000046 A2=11.*A1
C OUTPUT OMT,A1,A2,B1,B2,B3,B4
000050 1 Y(4)=A1*(X(4)+X(1))+A2*(X(3)+X(2))-B2*Y(3)-B3*Y(2)-B4*Y(1)
000125 DO 2 I=1,3
000126 X(I)=X(I+1)
000134 2 Y(I)=Y(I+1)
000144 RETURN
000144 END

```

```

SUBROUTINE RLOBA(N,GAM,VAL,CCL,IL,S,B,IYN,IZN)
000014 DIMENSION TG(128),RC(128)
000014 DATA G43/.892979511/
000014 IF(VAL.EQ.0.) GO TO 30
000015 IF(CCL.EQ.1.) GO TO 10
000017 EX=1./3.
000020 YN=0.
000020 S2=0.
000022 DO 11 I=1,N
000023 V=FLOAT(I-1)*GAM
000025 TG(I)=GAM/G43*V**EX*EXP(-V)
000043 S2=S2+TG(I)*TG(I)
000046 CALL NRANDOM(IYN,IZN,RC(I))
000052 11 YN=YN+TG(I)*PC(I)
000064 S22=SQRT(S2)
000066 YN=YN/S22*VAL
000074 GO TO 20
000075 10 YN=YT
000077 20 NN=N-1
000101 DO 12 J=1,NN
000102 12 RC(N+1-J)=RC(N-J)
000111 CALL NRANDOM(IYN,IZN,RC(1))
000115 YT=0.
000116 DO 13 JJ=1,N
000123 13 YT=YT+TG(JJ)*RC(JJ)
000130 YT=YT/S22*VAL
000132 FILM=FLOAT(IL-1)
000133 S=(YT-YN)/FILM
000136 B=-S*FLOAT(IL)+YT
000142 GO TO 31
000142 30 S=0.
000143 B=0.
000144 31 RETURN
000145 END

```

```

000014 DIMENSION TG(128),RC(128)
000014 DATA G43/.892979511/
000014 IF(VAL.EQ.0.) GO TO 30
000015 IF(CCL.EQ.1.) GO TO 10
000017 EX=1./3.
000020 YN=0.
000020 S2=0.
000022 DO 11 T=1,N
000023 V=FLOAT(I-1)*GAM
000025 TG(J)=GAM/G43*V**EX*EXP(-V)
000043 S2=S2+TG(T)*TG(I)
000046 CALL NRANDOM(IYN,IZN,RC(T))
000052 11 YN=YN+TG(I)*RC(I)
000064 S22=SQRT(S2)
000066 YN=YN/S22*VAL
000074 GO TO 20
000075 10 YN=YT
000077 20 NN=N-1
000101 DO 12 J=1,NN
000102 12 RC(N+1-J)=RC(N-J)
000111 CALL NRANDOM(IYN,IZN,RC(1))
000115 YT=0.
000116 DO 13 JJ=1,N
000123 13 YT=YT+TG(JJ)*RC(JJ)
000130 YT=YT/S22*VAL
000132 FTLM=FLOAT(IL-1)
000133 S=(YT-YN)/FTLM
000135 B=-S*FLOAT(IL)+YT
000142 GO TO 31
000142 30 S=0.
000143 R=0.
000144 31 RETURN
000145 END

```

```

SUBROUTINE TRYG(CCLT, ANGR, S, C)
DIMENSION SINE(91)
DR=.0174532925
IF(CCLT.EQ.1.) GO TO 10
NT=91
DO 9 T=1,NT
000014 9 SINE(T)=SIN(FLOAT(I-1)*DR)
000027 10 IP=INT(ANGR/DR+.5)
000032 IM=ABS(ANGR/DR+.5)
000036 IF(IM.GT.270) GO TO 4
000042 IF(IM.GT.180) GO TO 3
000045 IF(IM.GT.90) GO TO 2
000050 S=SINE(IM+1)
000051 C=SINE(-IM+90+1)
000053 GO TO 30
000053 2 S=SINE(-IM+180+1)
000055 C=-SINE(IM-90+1)
000057 GO TO 30
000057 3 S=-SINE(IM-180+1)
000061 C=-SINE(-IM+270+1)
000063 GO TO 30
000063 4 S=-SINE(-IM+360+1)
000065 C=SINE(IM-270+1)
000067 30 IF(IR.LT.0) S=-S
000072 RETURN
000073 END

```

```

SUBROUTINE ASQRTF (XU,S)
C      MAX INTERP ERR=1.46 (1.LE.X.LE.128)
X=ABS(XU)
000005      IF(X.GT.128.) GO TO 1
000006      IF(X.GT.64.) GO TO 2
000012      IF(X.GT.32.) GO TO 3
000015      IF(X.GT.16.) GO TO 4
000020      IF(X.GT.8.) GO TO 5
000023      IF(X.GT.4.) GO TO 6
000026      IF(X.GT.2.) GO TO 7
000031      IF(X.GT.1.) GO TO 8
000034      IF(X.GT..5) GO TO 9
000037      IF(X.GT..25) GO TO 10
000042      IF(X.GT..125) GO TO 11
000045      S=.3535
000050      RETURN
000051      1  S=11.3137
000052      RETURN
000053      2  S=.05177*(X-128.)+11.3137
000057      RETURN
000057      3  S=.07322*(X-64.)+8.
000063      RETURN
000063      4  S=.10355*(X-32.)+5.6568
000067      RETURN
000067      5  S=.14644*(X-16.)+4.
000073      RETURN
000073      6  S=.2071*(X-8.)+2.8284
000077      RETURN
000077      7  S=.2928*(X-4.)+2.
000103      RETURN
000103      8  S=.4142*(X-2.)+1.4142
000107      RETURN
000107      9  S=.5857*(X-1.)+1.
000112      RETURN
000113      10 S=.8284*(X-.5)+.7071
000117      RETURN
000117      11 S=1.17157*(X-.25)+.5
000123      RETURN
000123      END

```

```

SUBROUTINE DATAS (IXU)
DIMENSION IRC(6)
DATA IRC/0,0,0,0,0,1/
IX=0
000003      IF(IRC(1).NE.IRC(6))IX=1
000007      DO 1 I=1,5
000011      1  IRC(I)=IRC(6-I)
000017      IRC(1)=IX
000020      IXU=1
000021      IF(IX.EQ.0)IXU=-1
000023      RETURN
000024      END

```

```

PROGRAM MARK(INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT)
REAL NS,NC,NO,K,KB
COMPLEX CAMP(4),CFILT(4),COUT,CCOUT
DATA FBAMP,FBPHA,SDAMP,SOPHA,NO/2...2..23..47.1./
DATA GAM43,N43/.09.64/
DATA ENODB,BRATE,ENOMIN/8..88..9./
DATA DELF,N6PB,NACQT,BIF/62..40.100.1000./
DATA BL2,PHIDEG,FODIFF/176..10..342.433/

```

```

DATA I1,I2,I11,I22/1.1.1.1/
DATA FRQDOP,FQDPRT,TL/13.E3.10.8.-6.5/
DATA TAU3/.07957/
DATA FLO/10./
DATA SVRHZ,SWMX,SWMN/2.2E3.28.15E3.6.85E3/
DATA DYNR/3./

```

```

NAMELIST/IN1/NACQT,N6PB,ENODB,DELF,BIF,ENOMIN
.BL2,PHIDEG,FODIFF
.FBAMP,FBPHA,SDAMP,SOPHA,GAM43,N43
.FLO,FRQDOP,FQDPRT,I1,I2,I11,I22
.SVRHZ,SWMX,SWMN,TL,DYNR

```

```

P1=4.*ATAN(1.)
P12=2.*P1
ZETA=SQRT(0.5)

```

```
CALL TRIG(CCLT,P1,SSCIN,CSCIN)
```

```
CCLT=1.
```

```
A1 I2
```

```
CONTINUE
```

```
C READ INPUTS
```

```

READ(5,IN1)
N6PB=200
NACQT=30
SWMX=2500.
FRQDOP=1000.
I1=1
I2=1
I11=1

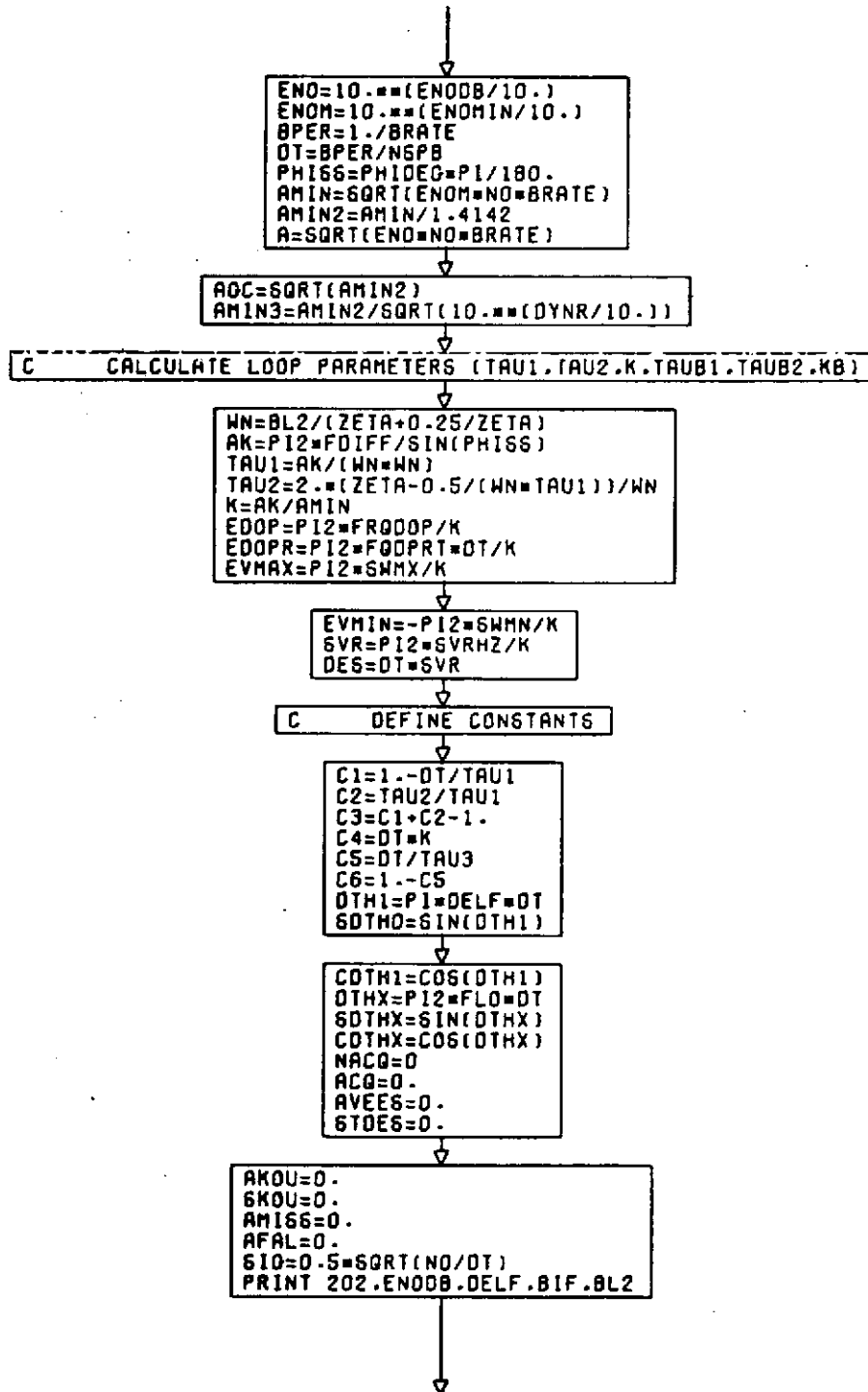
```

```

I22=1
I16=I1
I26=I2
I116=I11
I226=I22

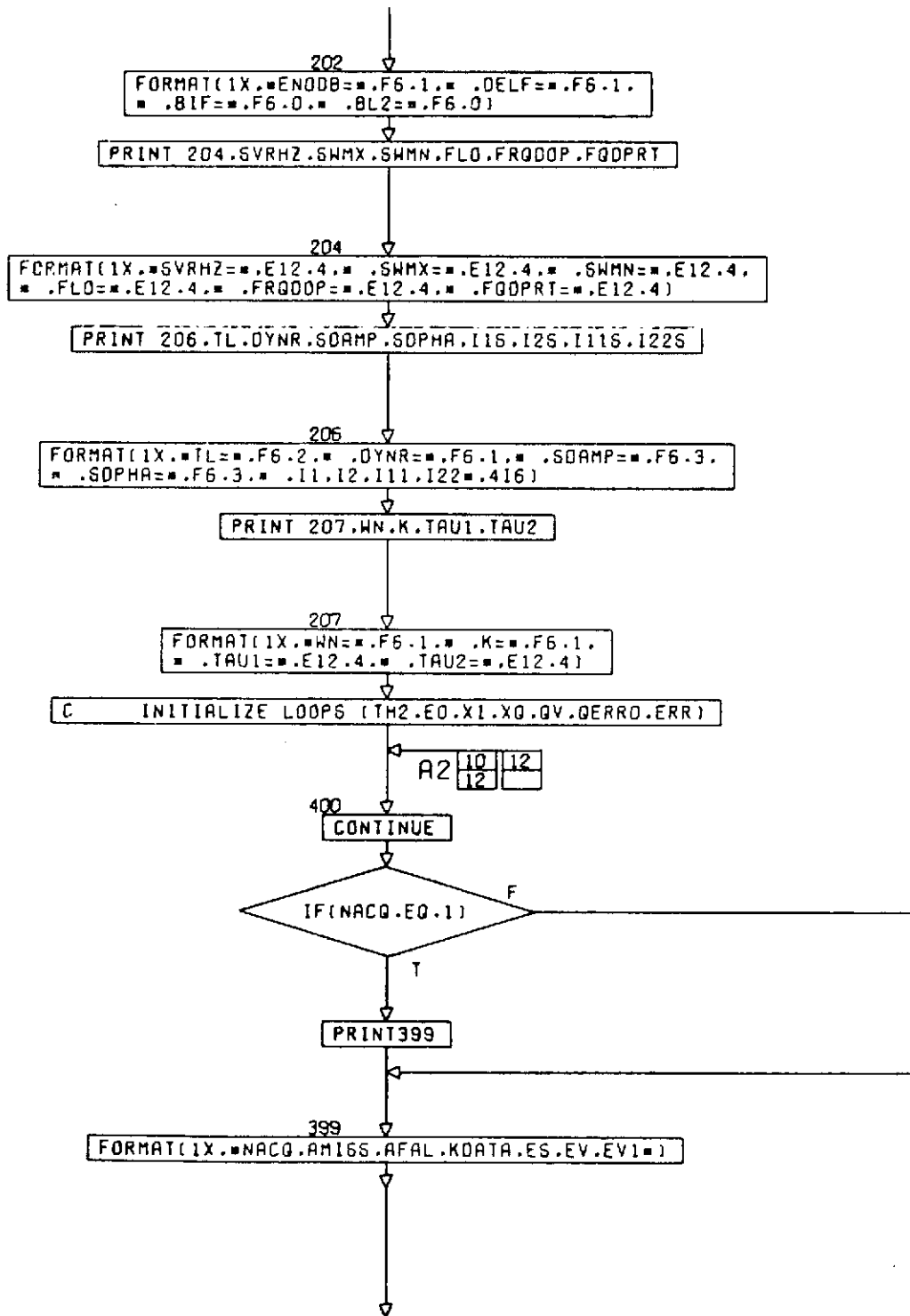
```

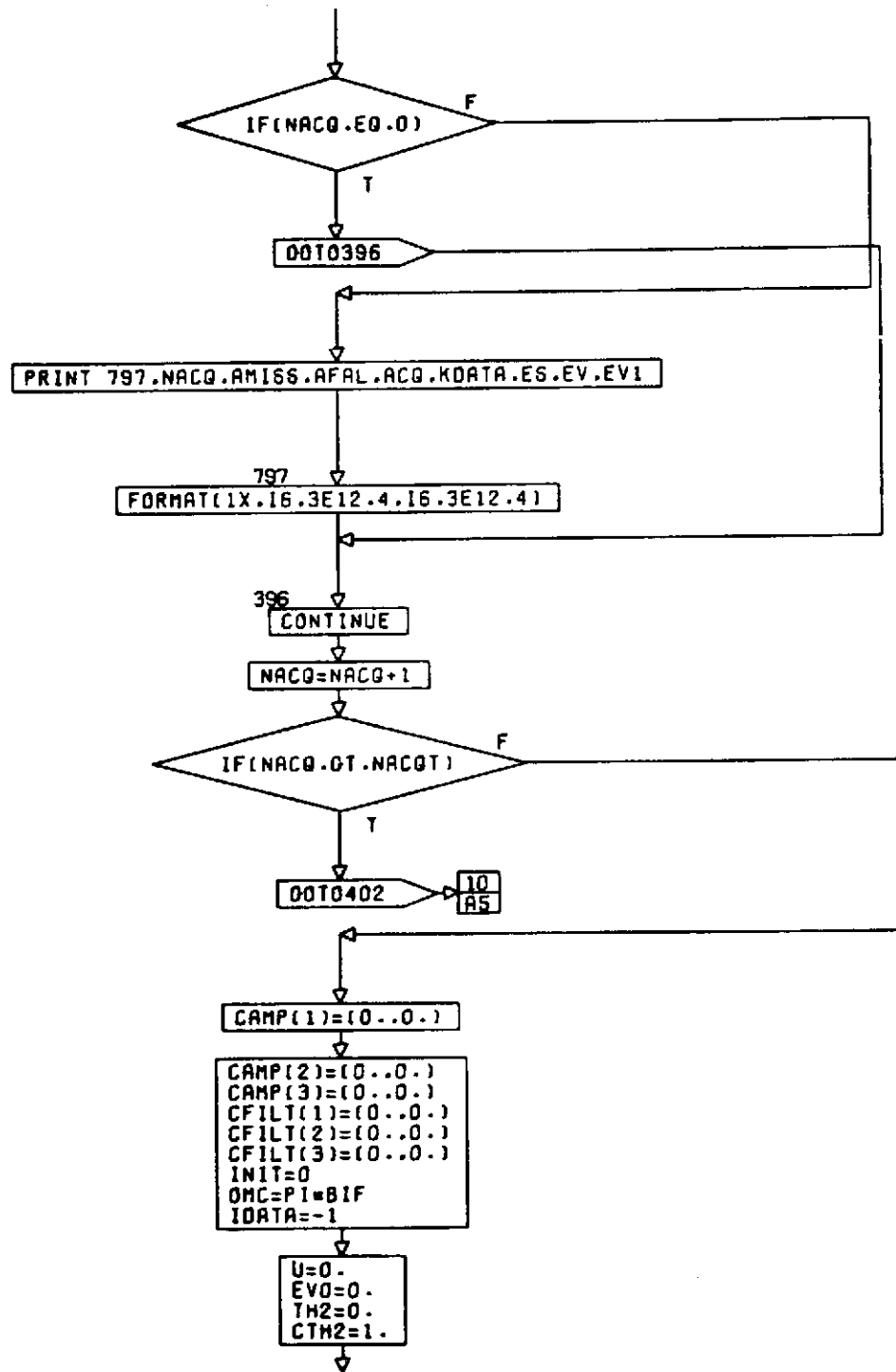
```
C CONVERT INPUTS (ENO,BPER,PHISS,PHISSB)
```

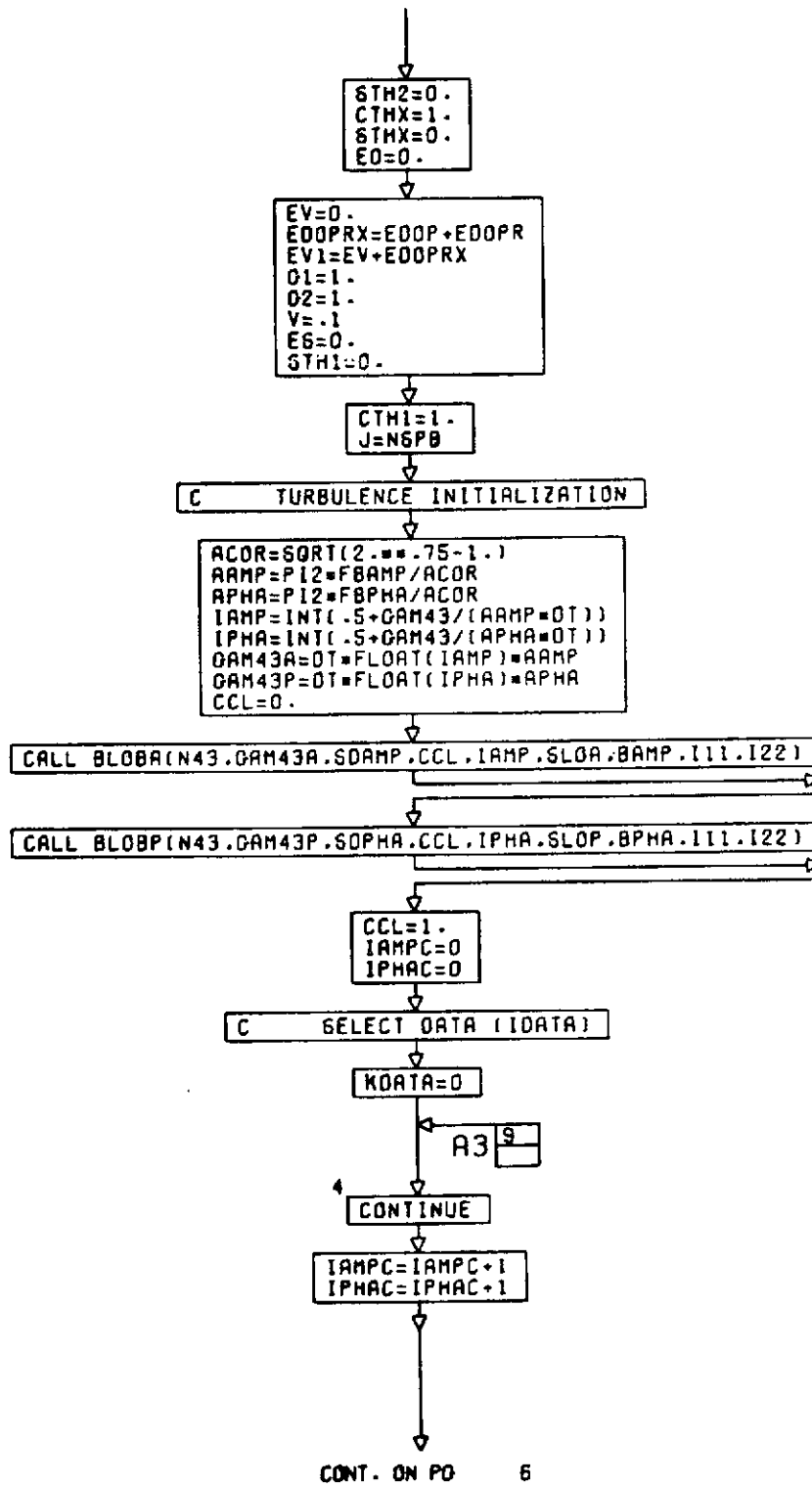



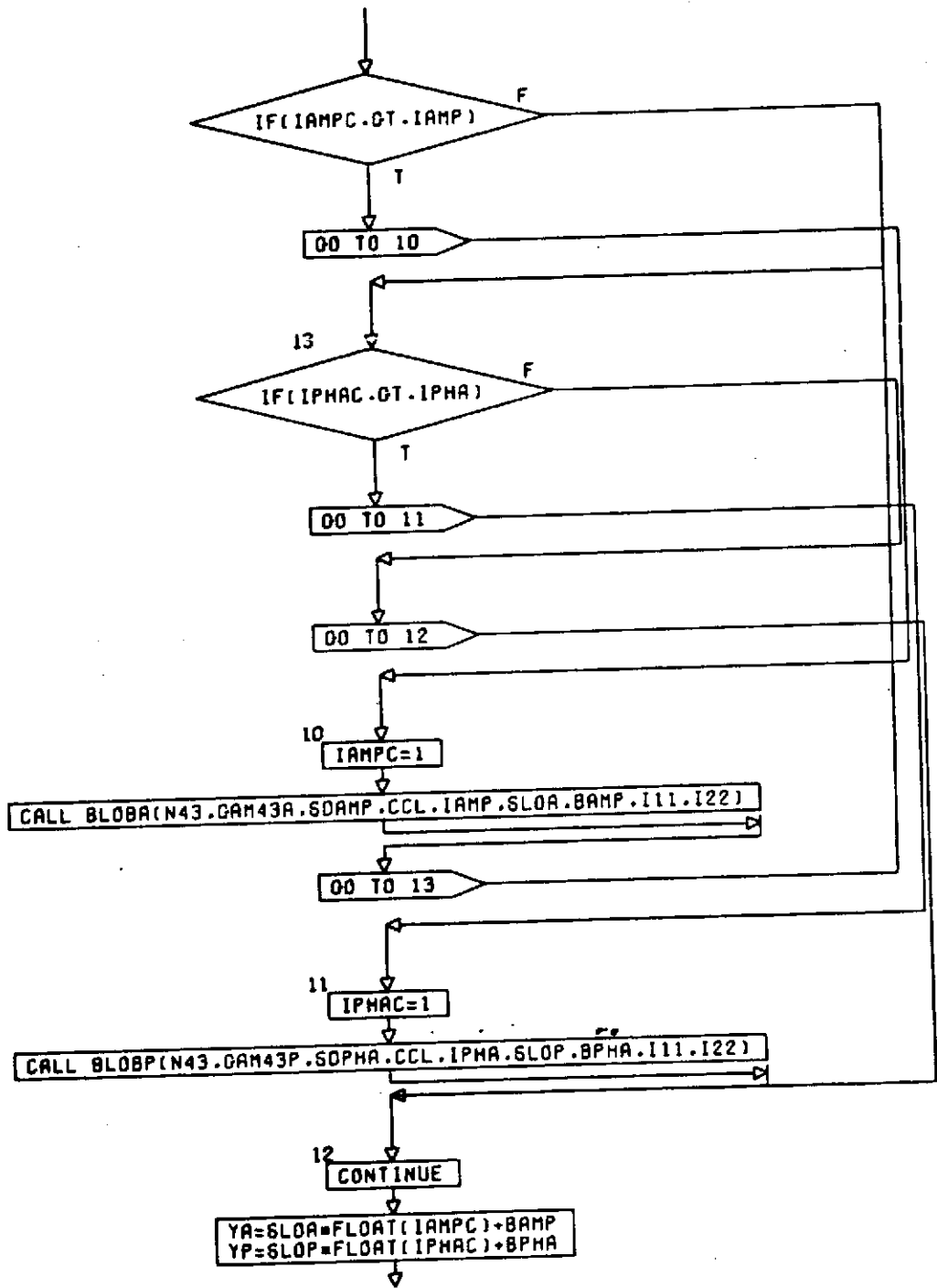
CONT. ON PD 3

PG 2 OF 12



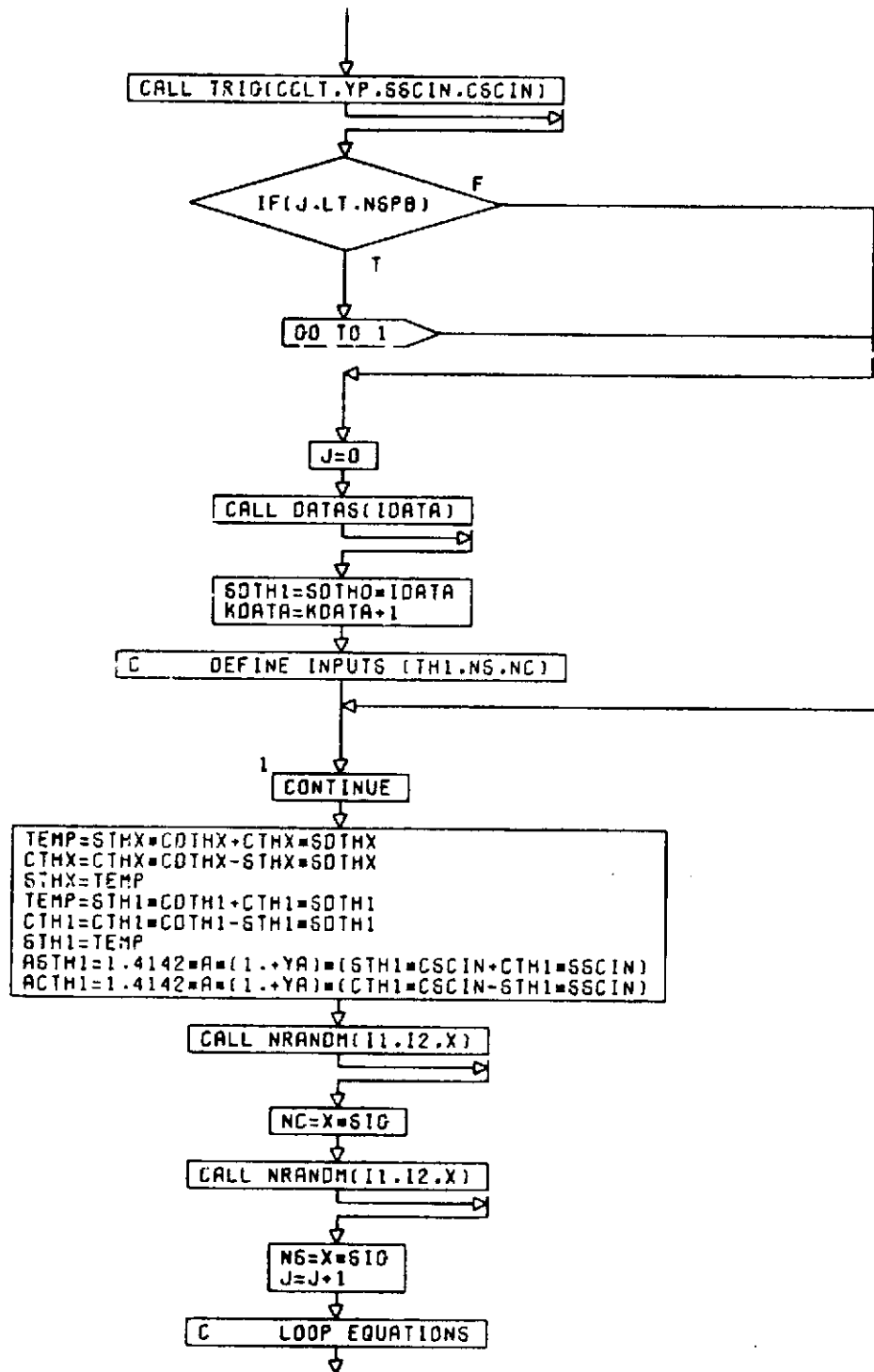






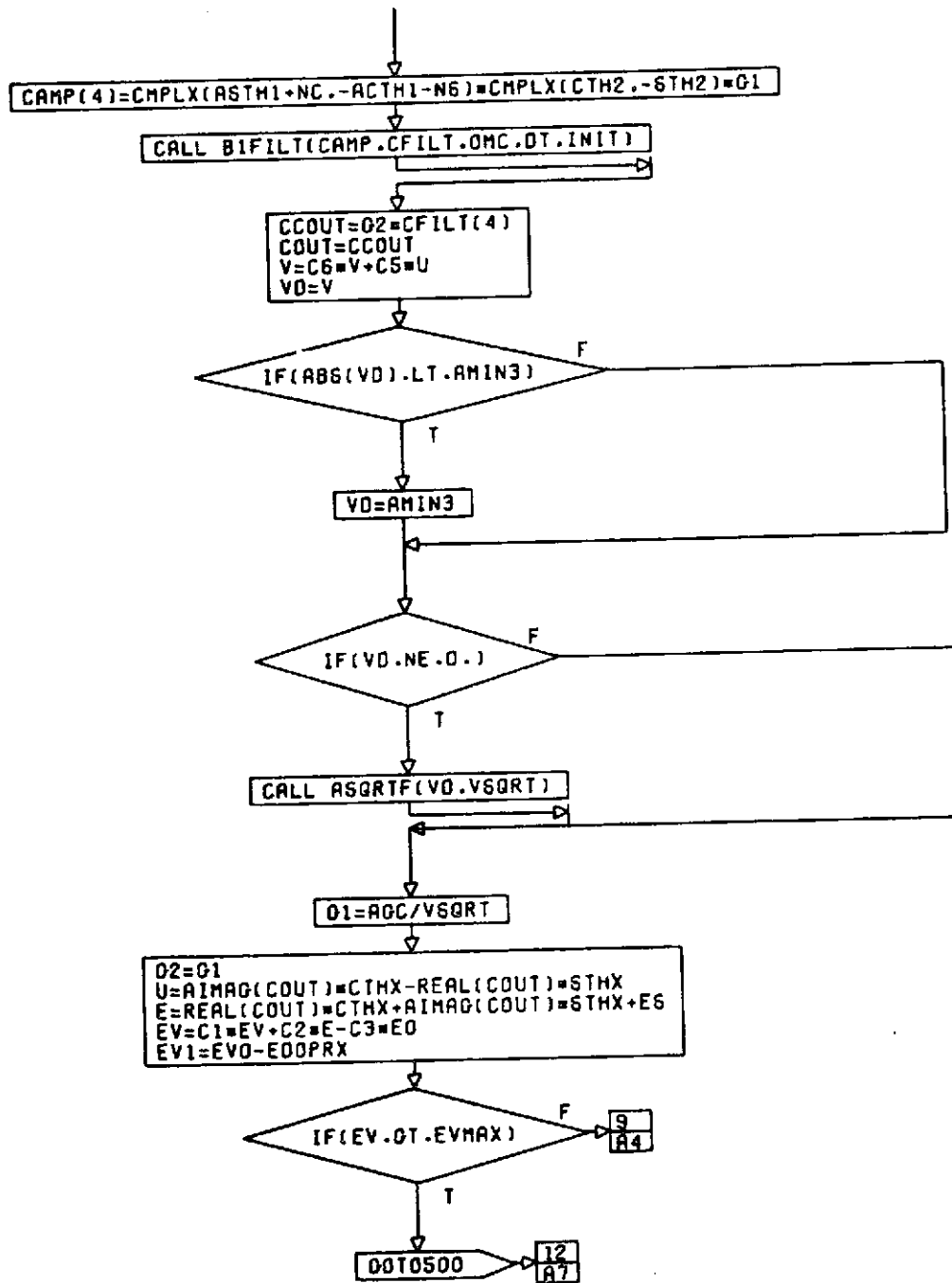
CONT. ON PG 7

PG 6 OF 12



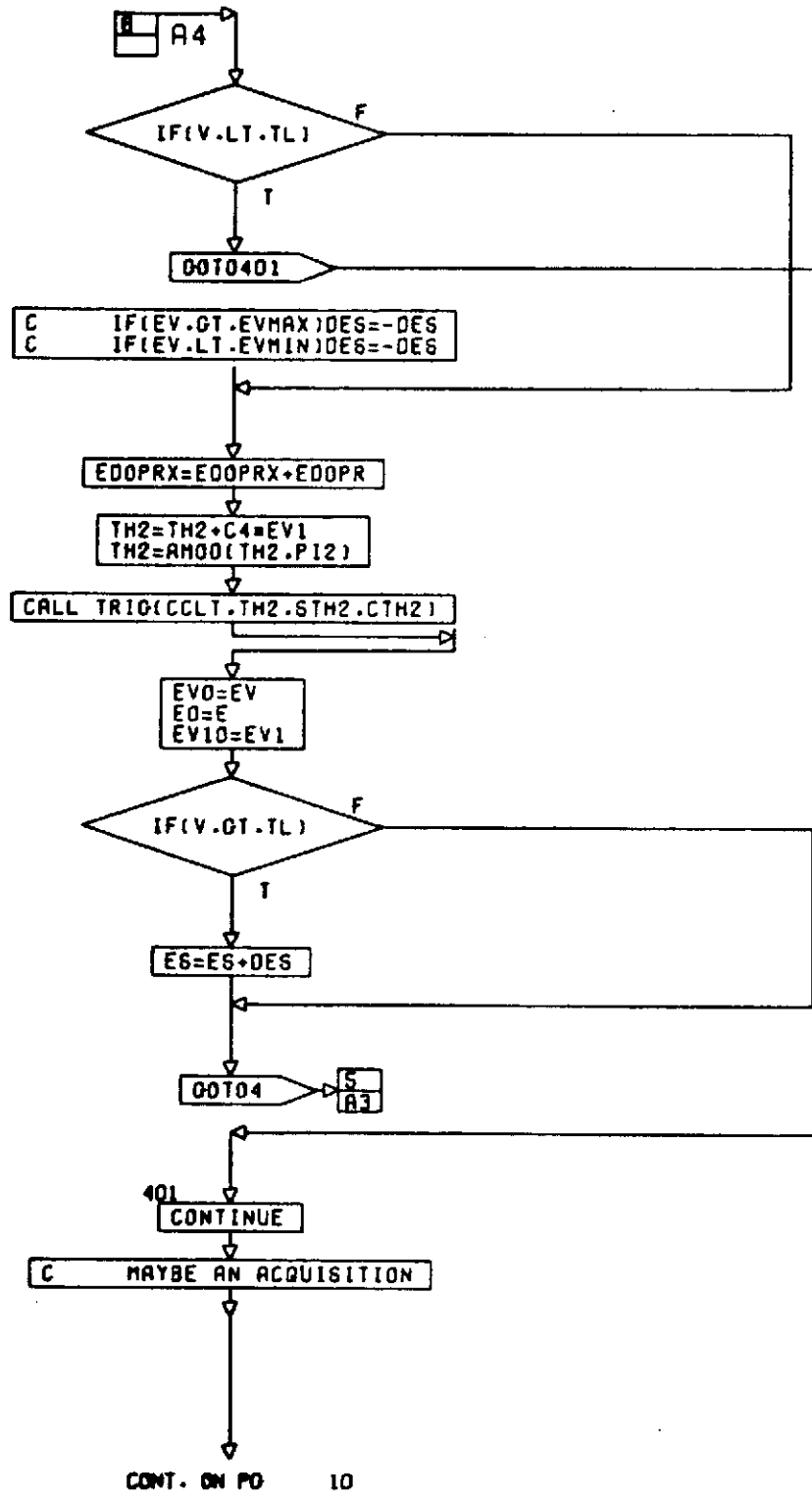
CONT. ON PG 8

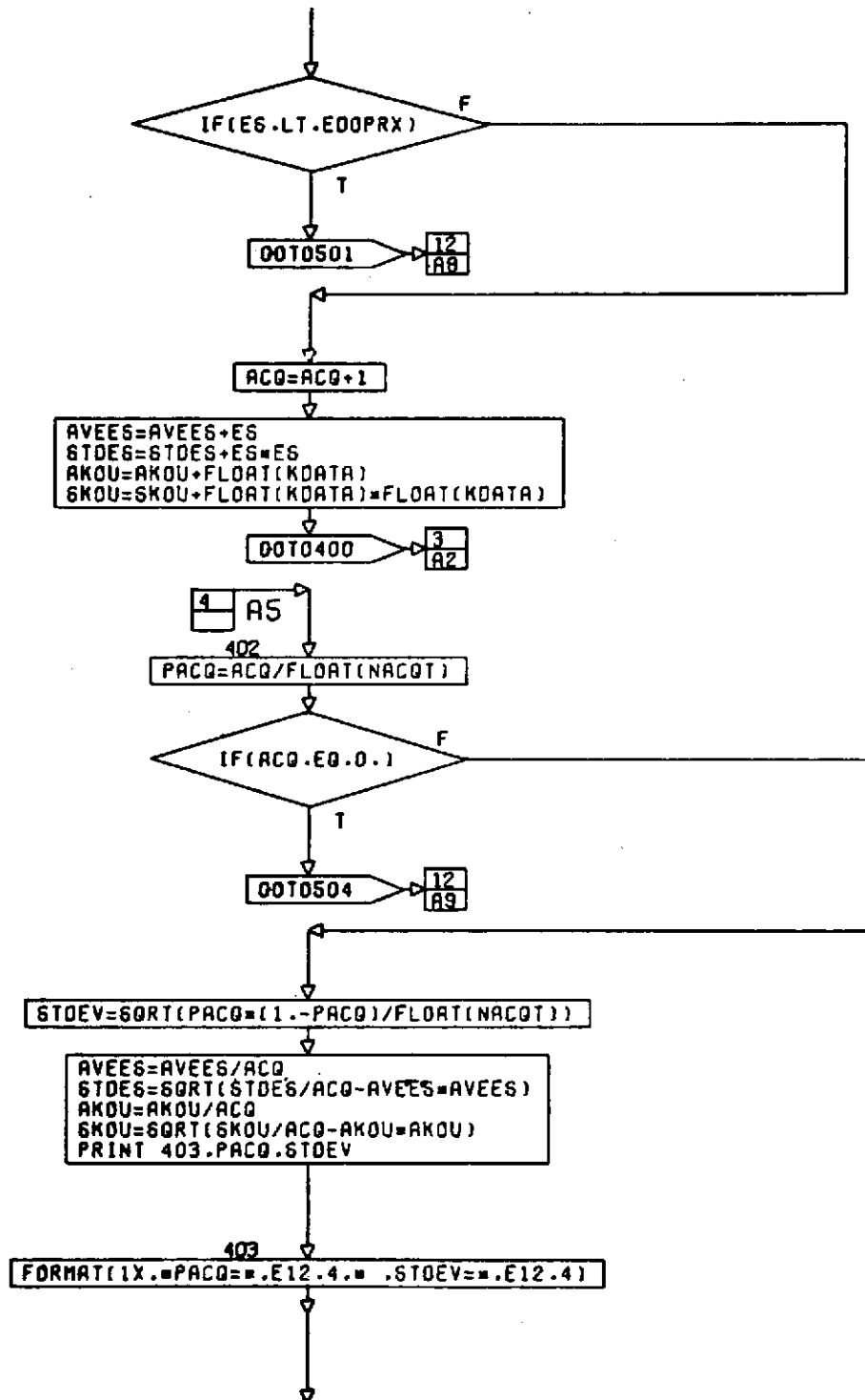
PG 7 OF 12



CONT. ON PD 9

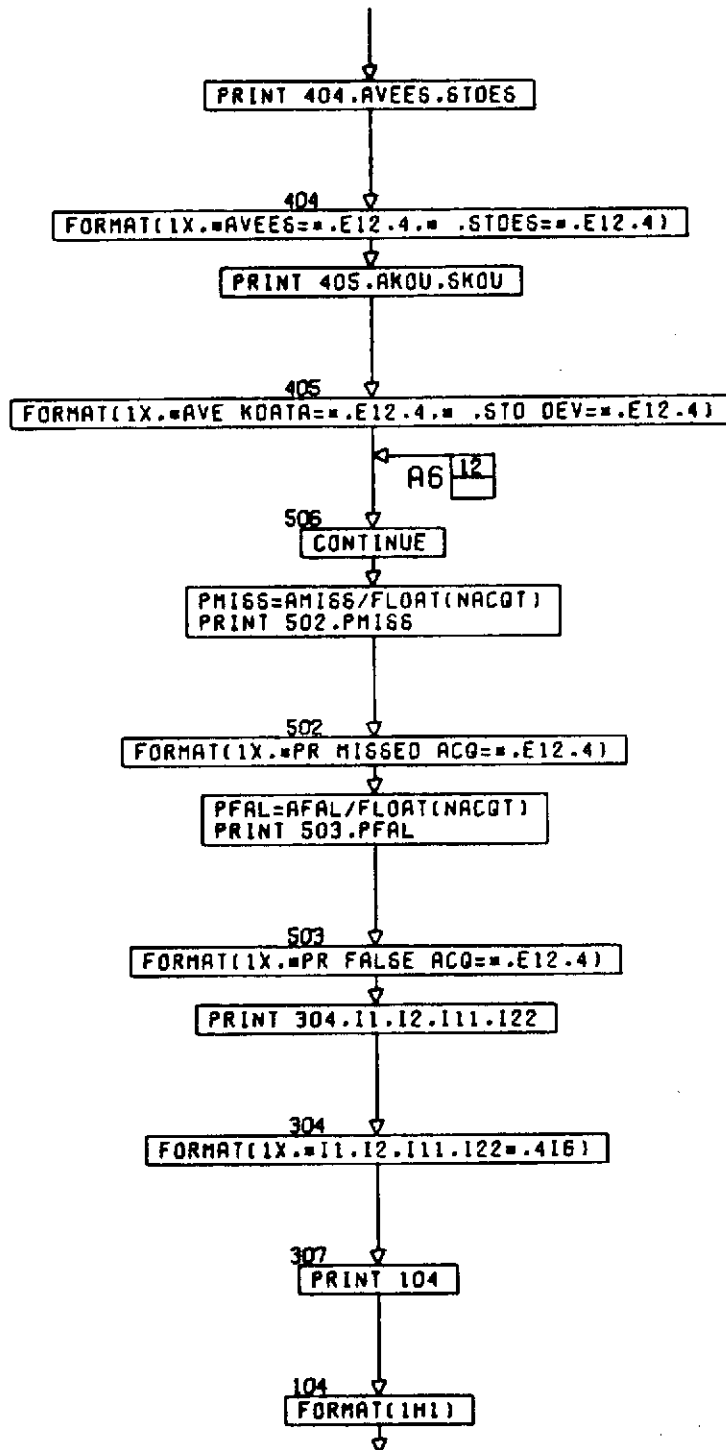
PG 8 OF 12





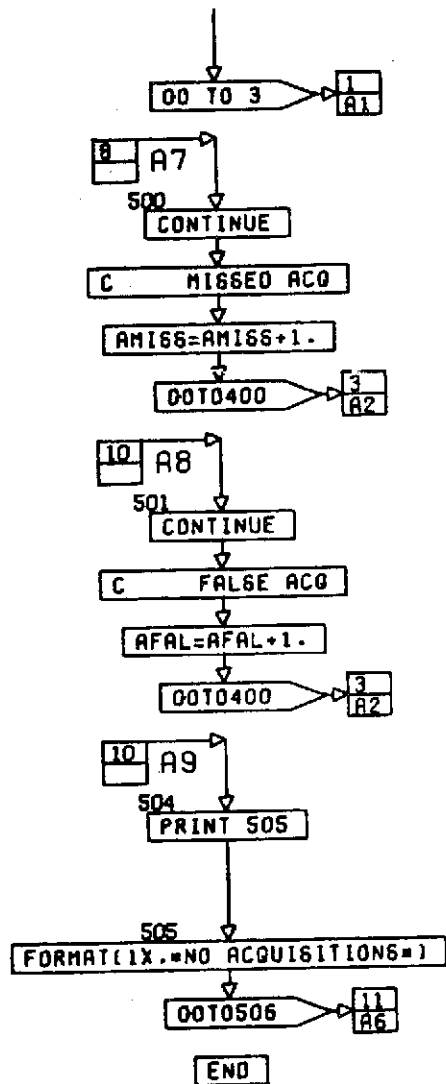
CONT. ON PD 11

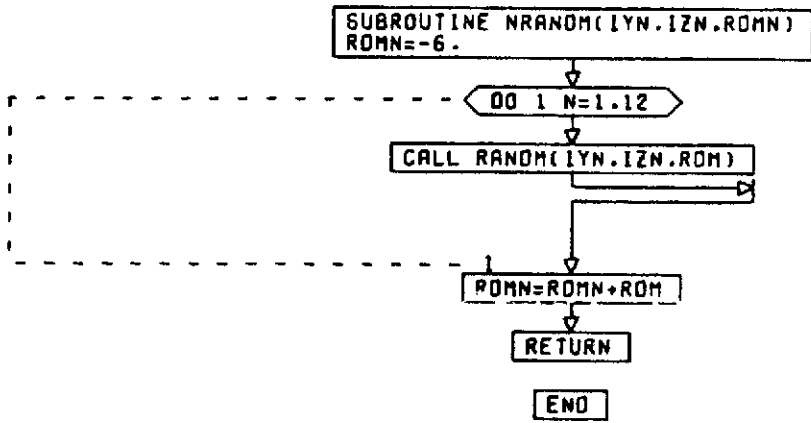
PD 10 OF 12



CONT. ON PG 12

PG 11 OF 12



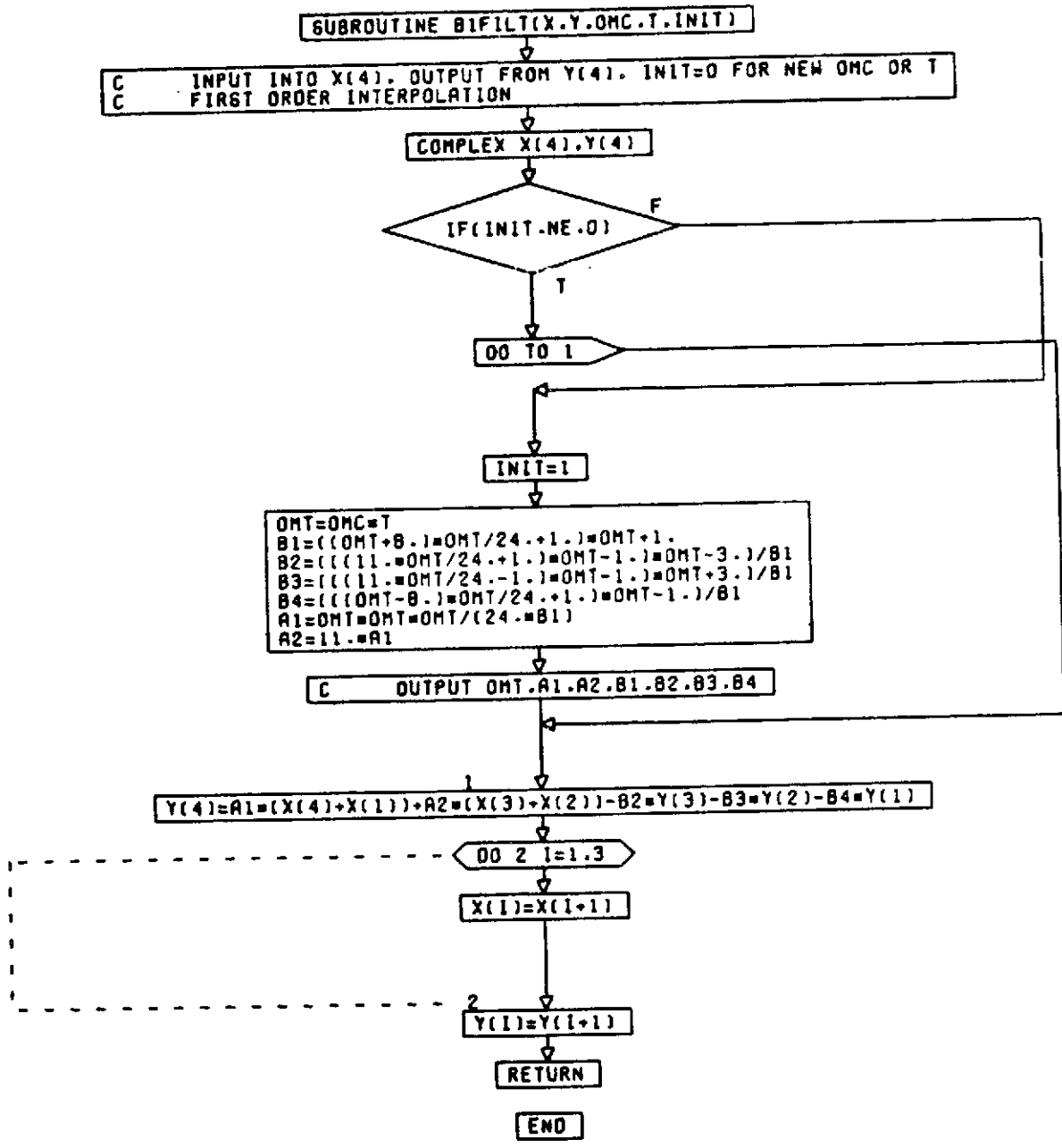


PG 1 FINAL

```
SUBROUTINE RANDM(IYN, IZN, ROM)
DATA IA, IB/129.1/
DATA T, IRT/4194304., 2048/
IYN=IA*(IYN+(IB+IA*IZN)/IRT)
IYN=MOD(IYN, IRT)
IZN=MOD((IB+IA*IZN), IRT)
ROM=FLOAT(IYN*IRT+IZN)/T
```

↓
RETURN

END

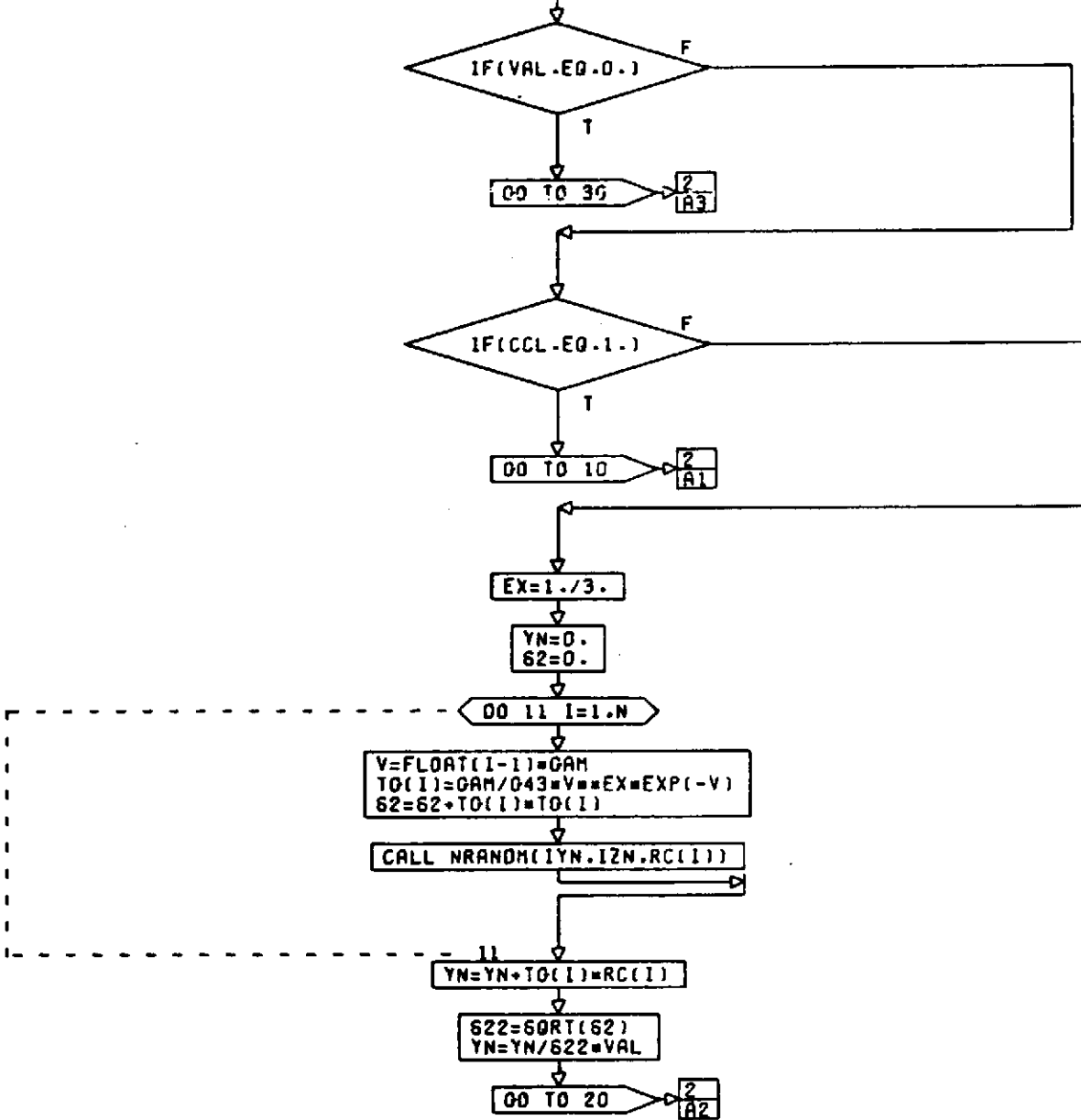


PG 3 FINAL

```

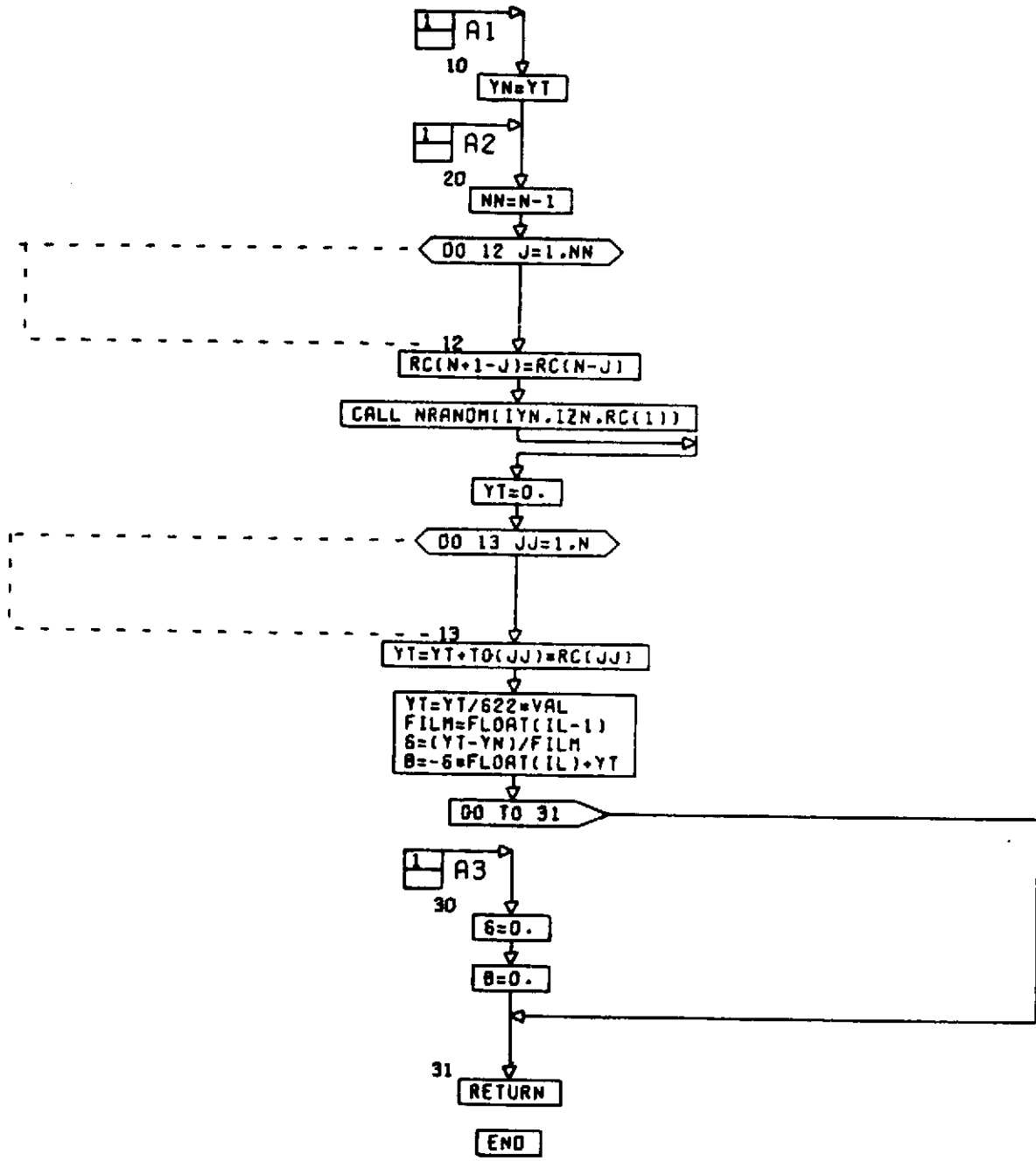
SUBROUTINE BLOBA(N,GAM,VAL,CCL,IL,S,B,IYN,IZN)
DIMENSION TO(128),RC(128)
DATA G43/.892979511/

```



CONT. ON PD 2

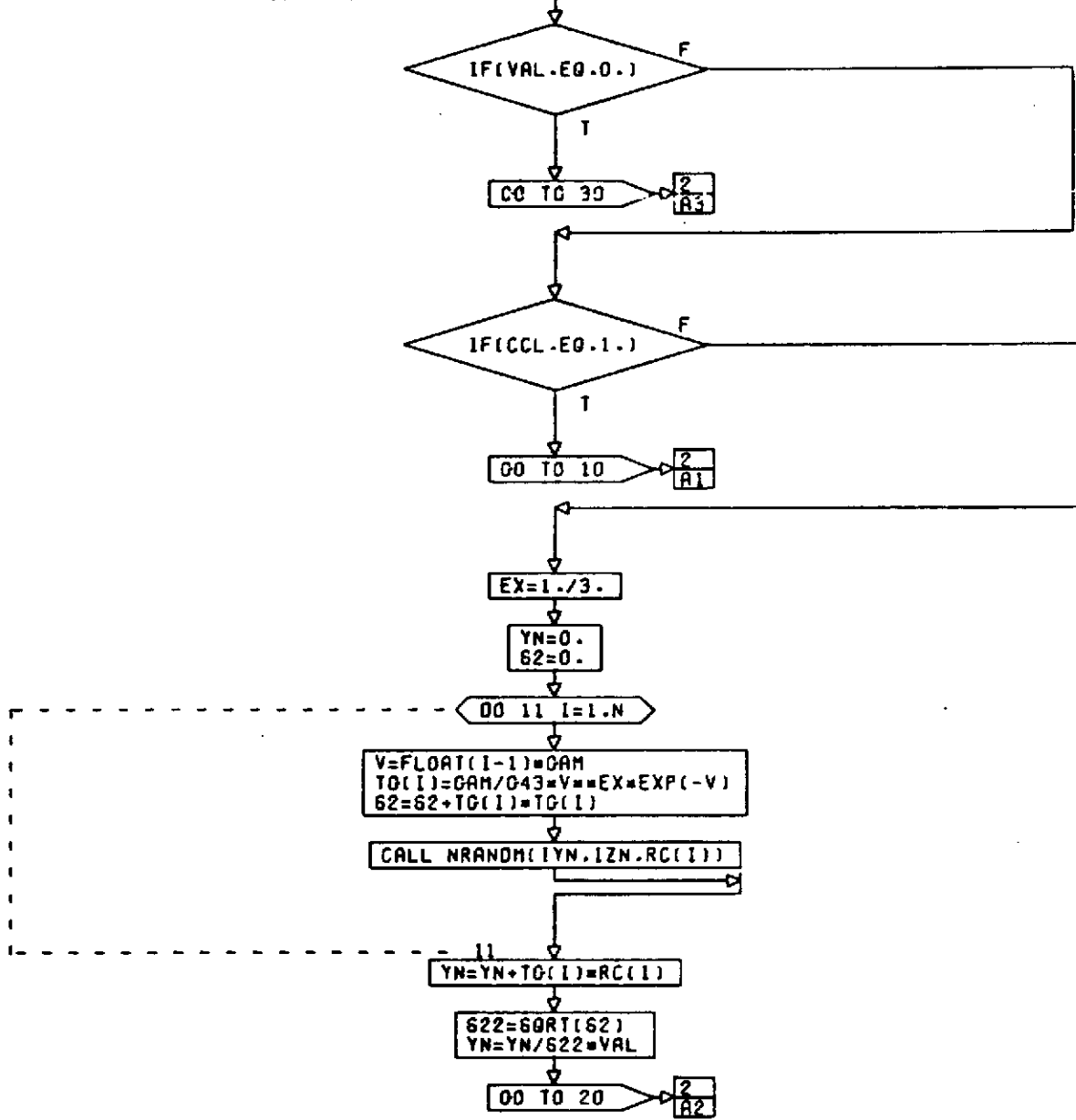
PD 1 OF 2




```

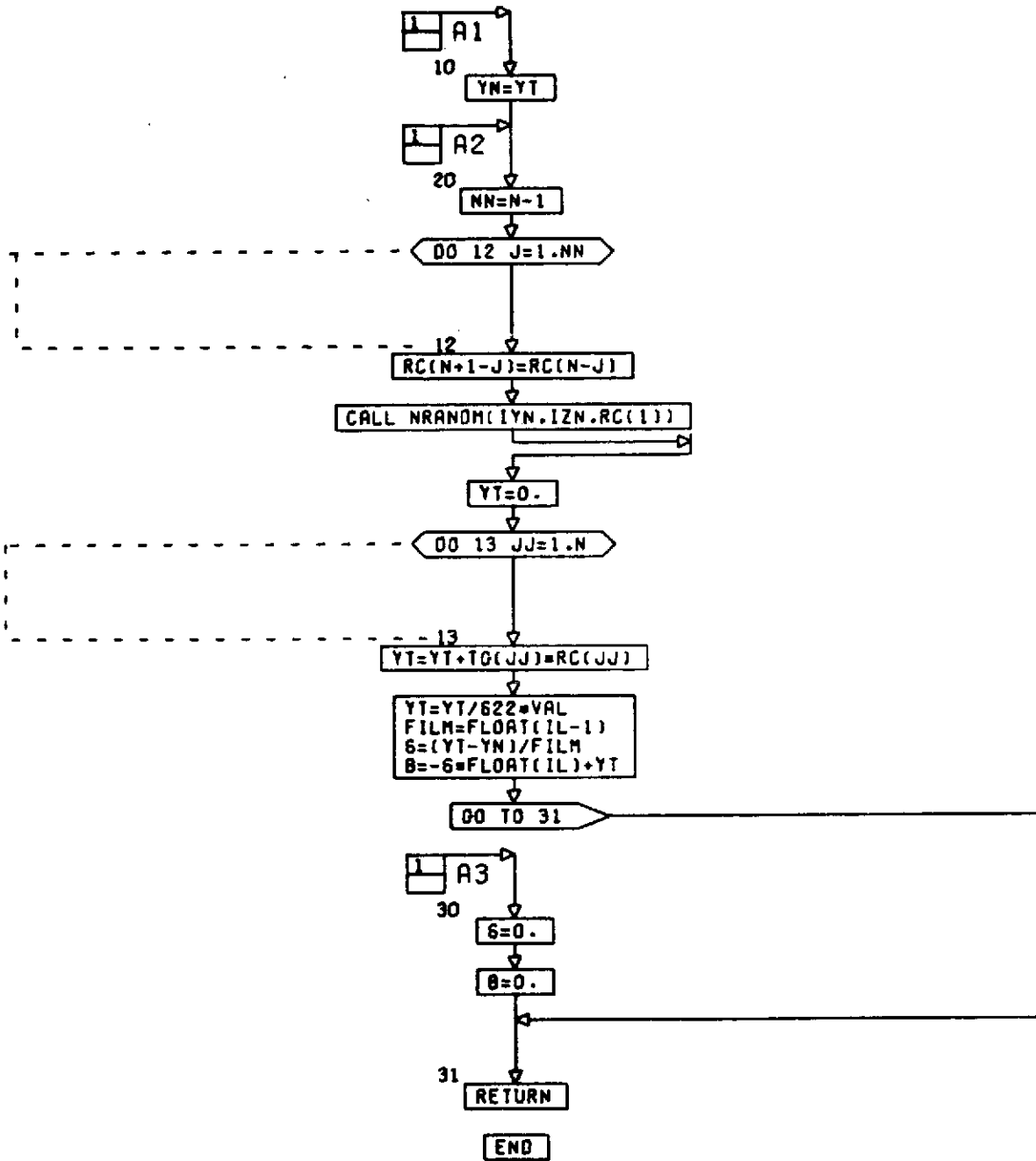
SUBROUTINE BLOBP(N,GAM,VAL,CCL,IL,S,B,IYN,IZN)
DIMENSION TG(128),RC(128)
DATA G43/.892979511/

```



CONT. ON PG 2

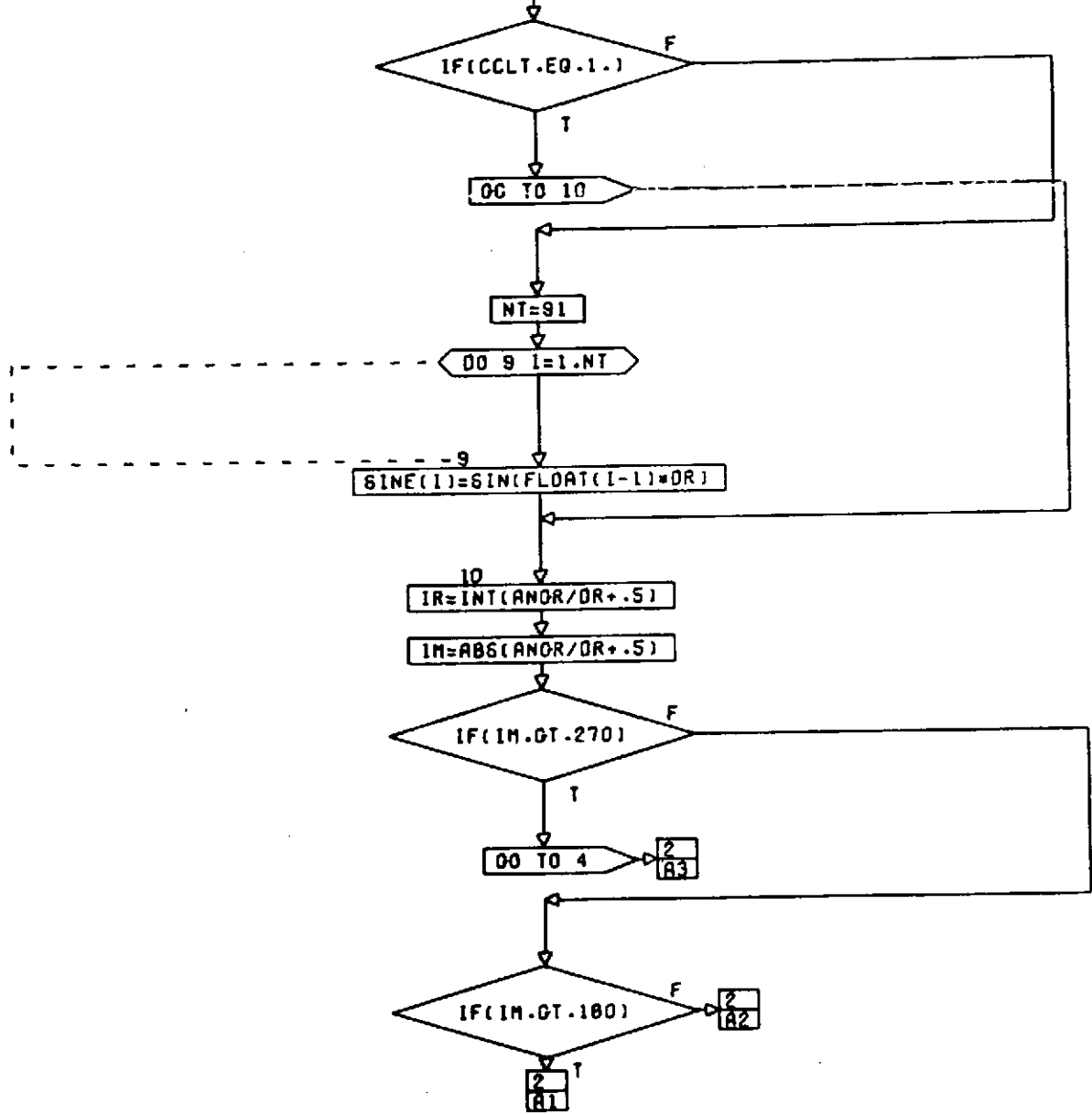
PG 1 OF 2



```

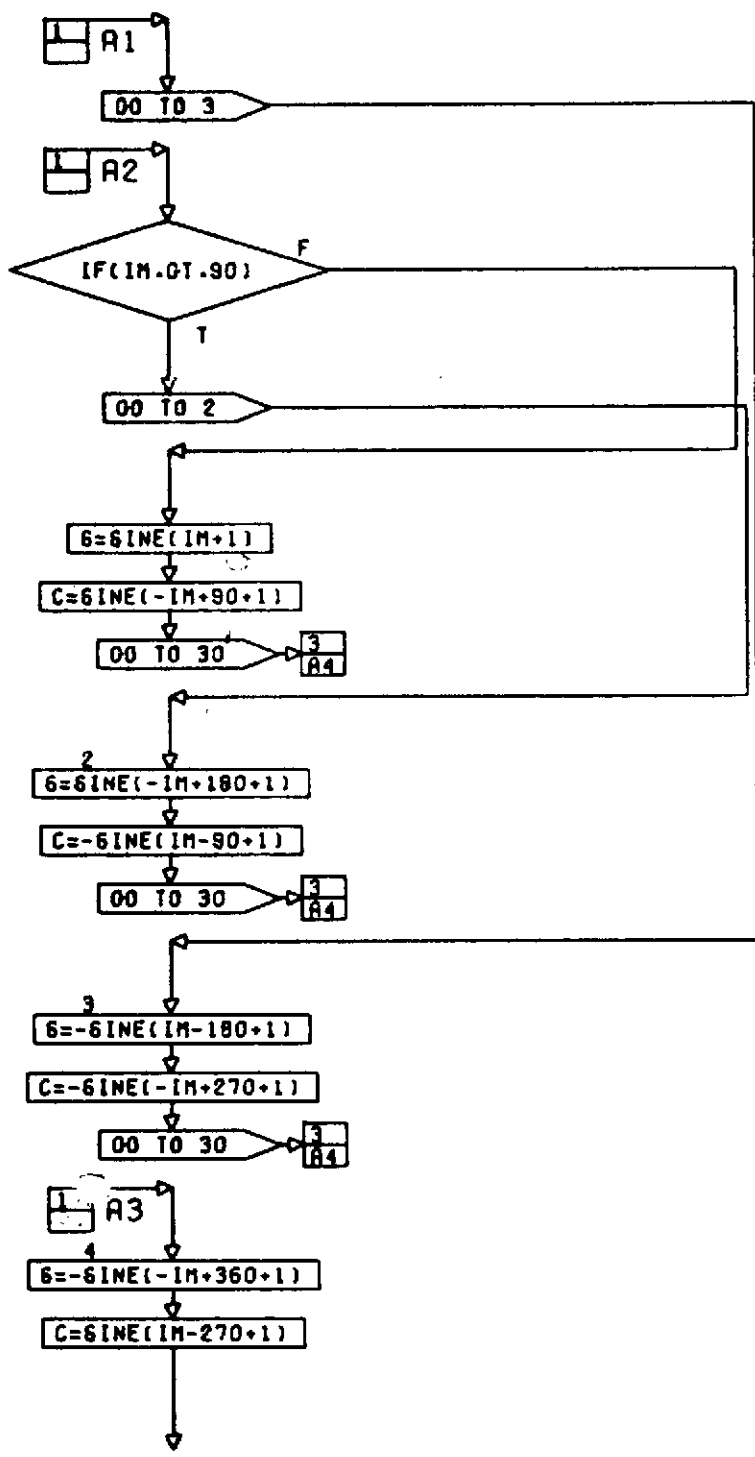
SUBROUTINE TRIG(CCLT,ANOR,S,C)
DIMENSION SINE(91)
DR=.0174532925

```



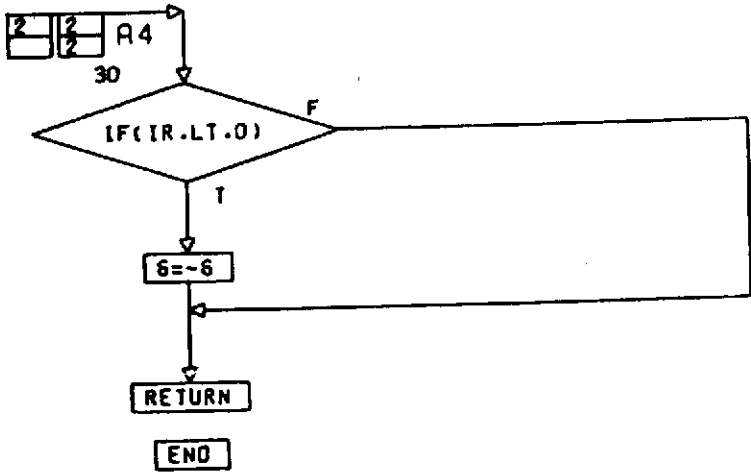
CONT. ON PD 2

PD 1 OF 3

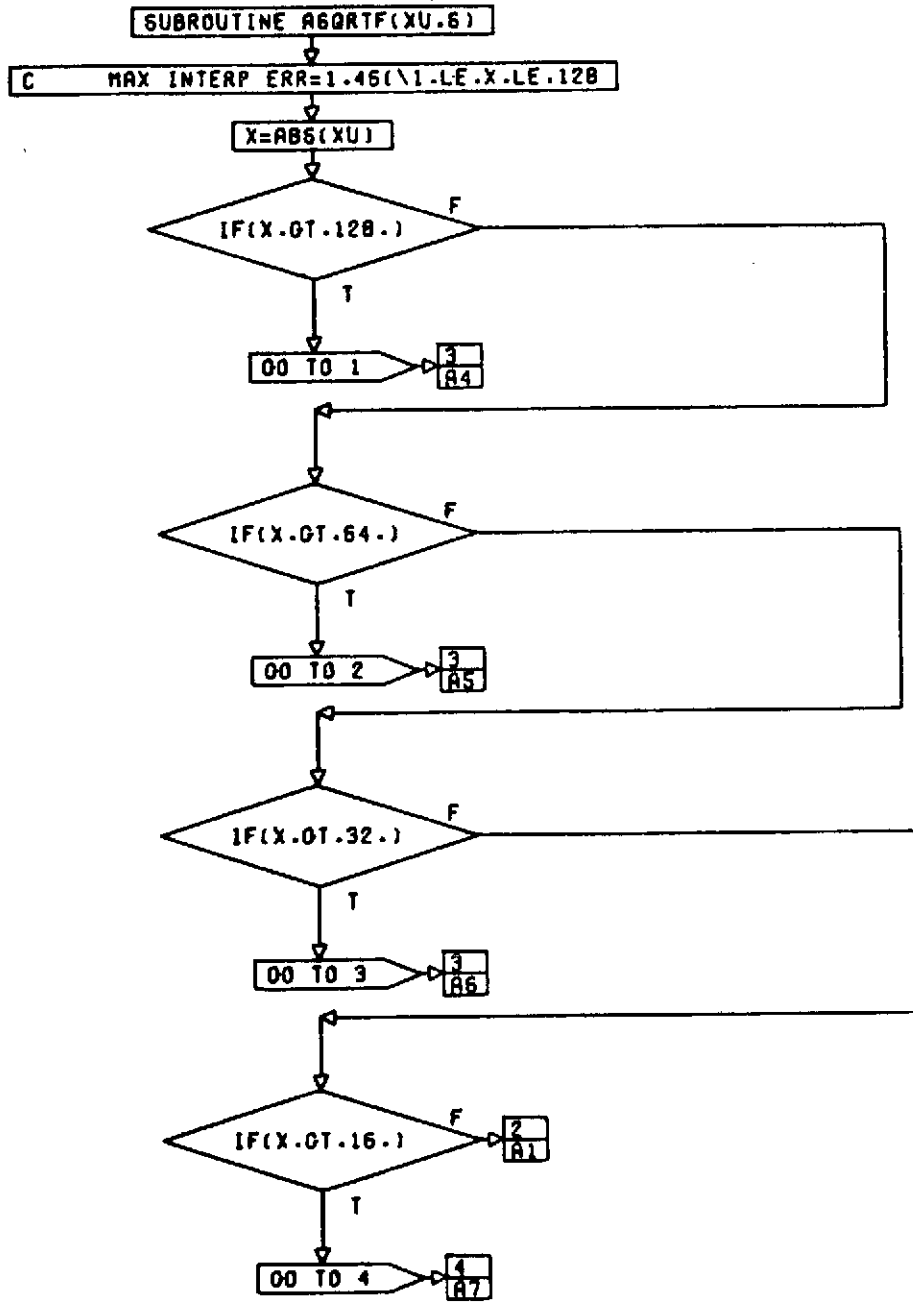


CONT. ON PD 3

PG 2 OF 3

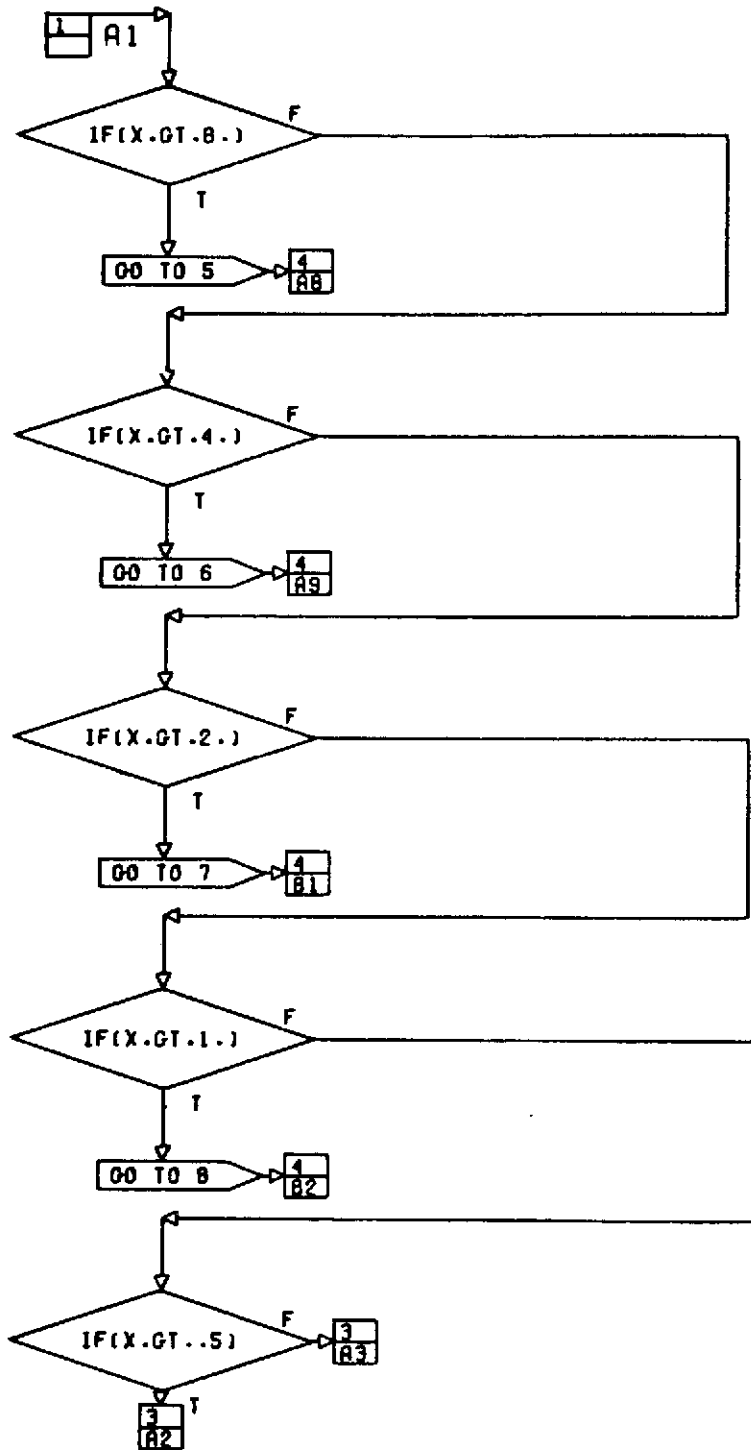


PO 3 FINAL



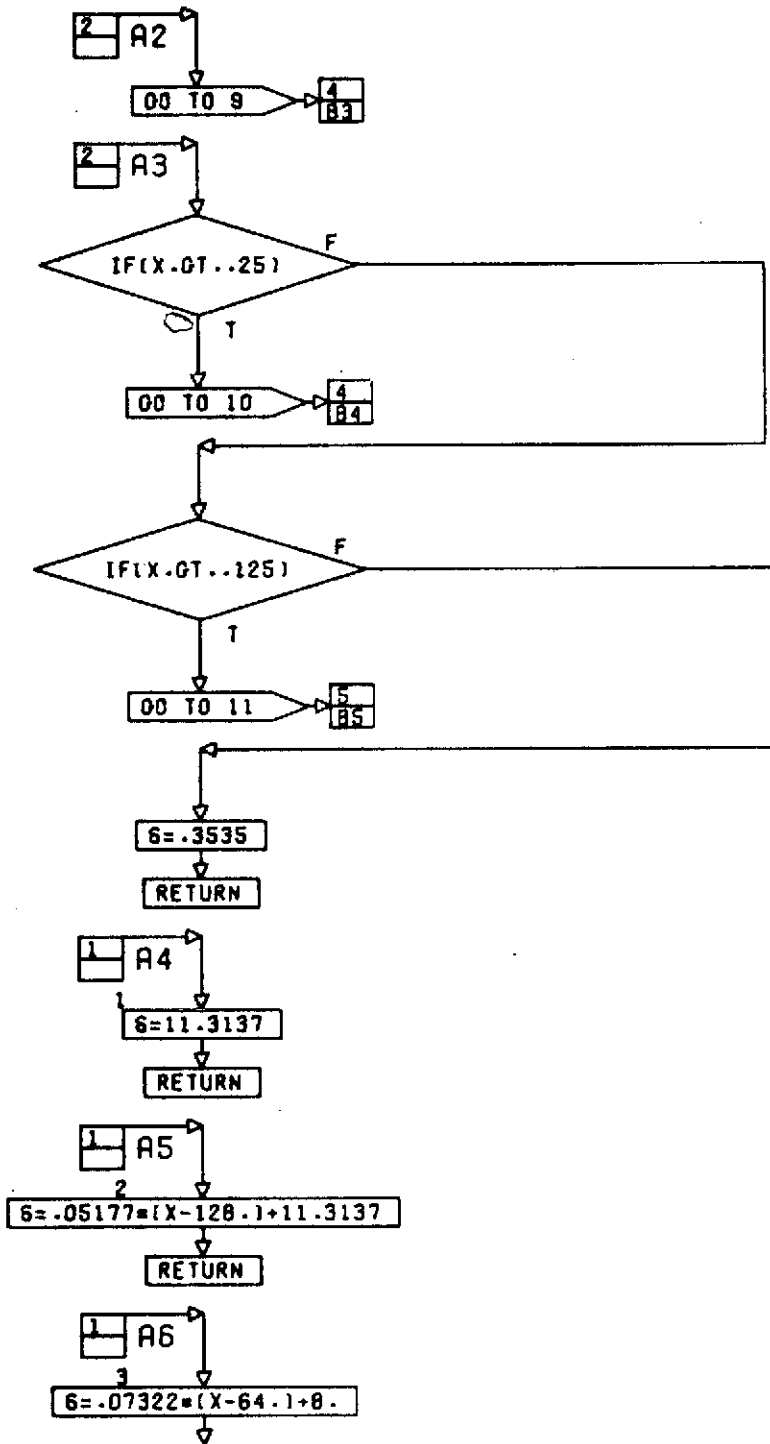
CONT. ON PD 2

PD 1 OF 5



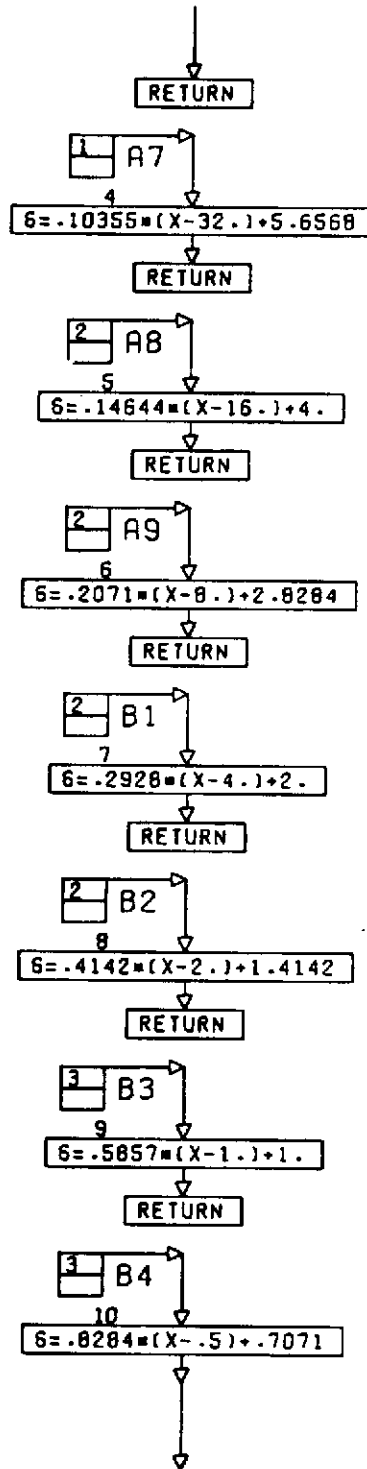
CONT. ON PG 3

PG 2 OF 5



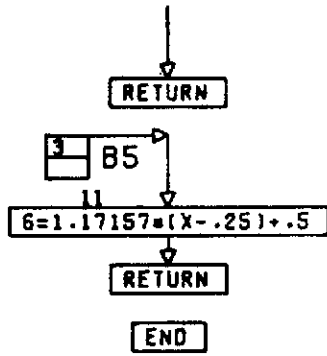
CONT. ON PG 4

PG 3 OF 5

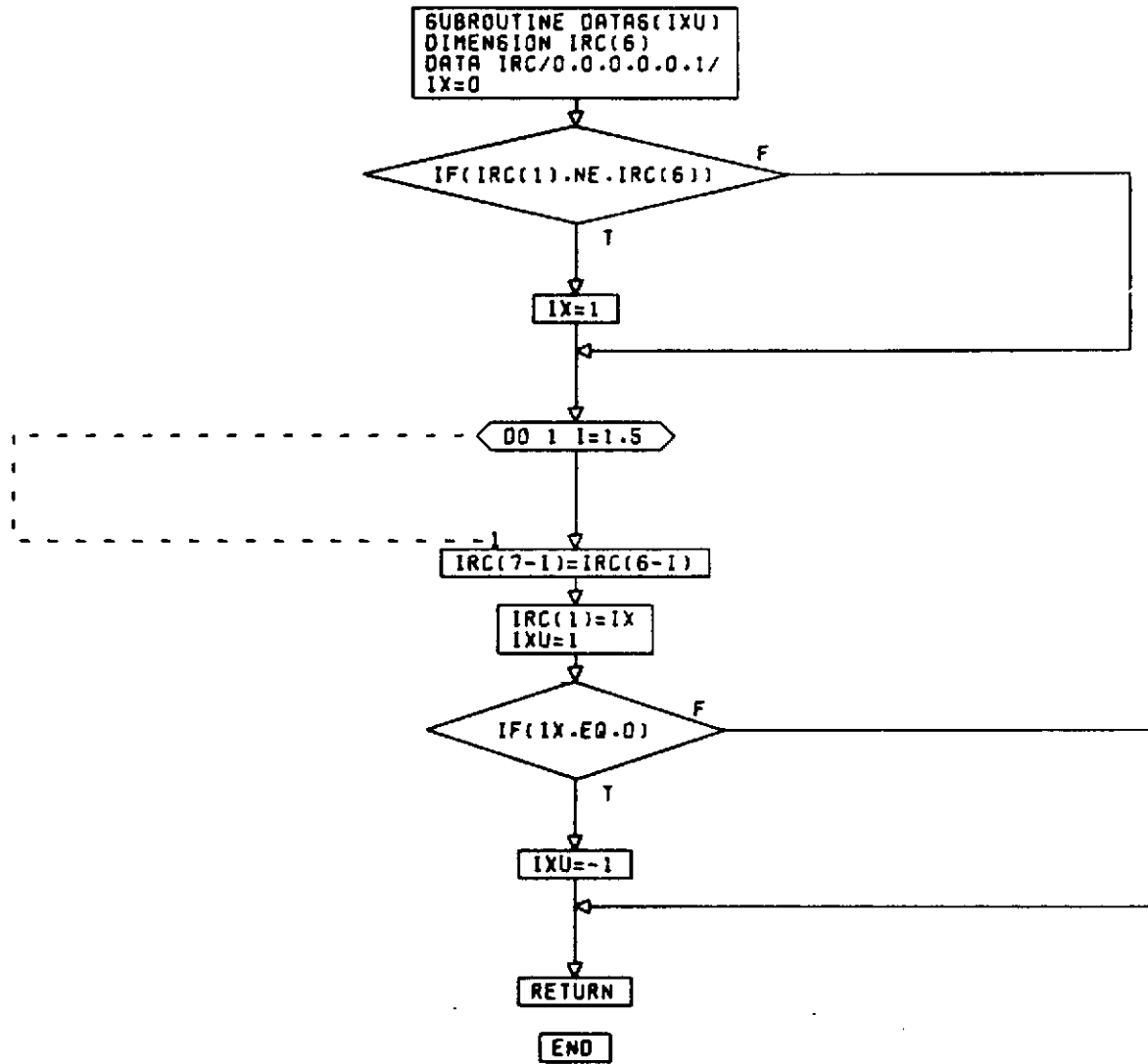


CONT. ON PG 5

PG 4 OF 5



PG. 5 FINAL



PG 1 FINAL

APPENDIX VII
MISCELLANEOUS SUBROUTINES

This appendix presents three subroutines which were found useful in troubleshooting the receiver during the software development, but were not used in the production runs.

The first is OSCILL which is an oscilloscope and plots three inputs. These are entered into the routine by lists. The routine automatically scales the output.

The second is SURV which is a voltmeter. It gives the mean and standard deviation of the input, as well as the mean and standard deviation of the absolute value of the input.

The third is CHMEM. This was used early in the analysis when there was one conditional probability matrix which was the position by position summation of all four of the matrices of this report, i.e., just $P(B/A)$. It generates information to determine the skew of the matrix.

```

SUBROUTINE OSCILL(LLL,X,Y,Z)
C XYZ PLOTTED VS LLL
000007 DIMENSION OUT(66),X(90),Y(90),Z(90)
000007 DATA BLANK,STAR,XX,YY,ZZ,AZ/
+IH,IP*,IH*,IHX,IHY,IHZ,IHO/
000007 L=LLL-1
C 1 ST MAX+MIN
000010 XMAX=-1.E10
000012 XMIN=1.E10
000014 DO 10 I=1,L
000015 IF(Z(I).GT.XMAX) XMAX=Z(I)
000022 IF(Y(I).GT.XMAX) XMAX=Y(I)
000027 IF(Z(I).LT.XMIN) XMIN=Z(I)
000034 IF(Y(I).LT.XMIN) XMIN=Y(I)
000041 IF(X(I).GT.XMAX) XMAX=X(I)
000046 10 IF(X(I).LT.XMIN) XMIN=X(I)
000056 SLO=65./(XMAX-XMIN)
000060 B=-65.*XMAX/(XMAX-XMIN)+66.
C THEN SCALE
000064 XINT=(XMAX-XMIN)/65.
000067 PRINT 99,XMAX,XMIN,XINT
000101 99 FORMAT(1X,*MAX=*,G14.6,*MIN=*,G14.6,
+*INT=*,G14.6)
000101 IF(XMAX.GT.0..AND.XMIN.LT.0.) IYZ=INT(B)
000114 STEER=0.
000115 24 DO 20 I=1,66
000117 20 OUT(I)=STAR
000123 IF(XMAX.GT.0..AND.XMIN.LT.0.) OUT(IYZ)=AZ
000134 IF(STEER.EC.1.) GO TO 25
000136 OUT(INT(SLO*X(1)+B))=XX
000144 OUT(INT(SLO*Y(1)+B))=YY
000150 OUT(INT(SLO*Z(1)+B))=ZZ
000154 LL=1
000155 PRINT 22,LL,OUT
000164 22 FORMAT(1X,I3,66A1)
000164 LEND=L-1
000166 DO 23 LL=2,LEND
000172 DO 28 I=1,66
000173 28 OUT(I)=BLANK
000177 OUT(1)=STAR
000200 OUT(66)=STAR
000200 IF(XMAX.GT.0..AND.XMIN.LT.0.) OUT(IYZ)=STAR
000212 OUT(INT(SLO*X(LL)+B))=XX
000221 OUT(INT(SLO*Y(LL)+B))=YY
000230 OUT(INT(SLO*Z(LL)+B))=ZZ
000237 23 PRINT 22,LL,OUT
000253 STEER=1.
000255 GO TO 24
000255 25 OUT(INT(SLO*X(LL)+B))=XX
000264 OUT(INT(SLO*Y(LL)+B))=YY
000273 OUT(INT(SLO*Z(LL)+B))=ZZ
000302 PRINT 22,L,OUT
000311 RETURN
000312 END

```

```

SUBROUTINE SURV(CX,V,VS)
DIMENSION VS(6)
000006 IF(CX.EQ.1.)GO TO 1
000010 VS(1)=VS(1)+1.
000011 VS(2)=VS(2)+V
000013 VS(4)=VS(4)+ABS(V)
000015 VS(6)=VS(6)+V*V
000020 GO TO 2
000020 1 CONTINUE
000020 IF(VS(1).EQ.0.)GOTO3
000021 VS(2)=VS(2)/VS(1)
000023 VS(4)=VS(4)/VS(1)
000025 DUM=VS(6)/VS(1)-VS(2)*VS(2)
000030 IF(DUM.LT.0.)GOTO4
000032 VS(3)=SQRT(DUM)
000036 DUM=VS(6)/VS(1)-VS(4)*VS(4)
000042 IF(DUM.LT.0.)GOTO5
000044 VS(5)=SQRT(DUM)
000050 PRINT 20,VS
000057 20 FORMAT(6E12.4)
000057 RETURN
000060 3 PRINT 10
000064 10 FORMAT(1X,*MISSED COUNT*)
000064 RETURN
000065 4 PRINT 11
000071 11 FORMAT(1X,*SQRT PBLM 1*)
000071 RETURN
000072 5 PRINT 12
000076 12 FORMAT(1X,*SQRT PBLM 2*)
000076 2 RETURN
000077 END

```

```

SUBROUTINE CHHEW(SB)
000003      DIMENSION SB(8,8)
000003      A=0.
000004      AUL=0.
000005      AUR=0.
000006      ALL=0.
000007      ALR=0.
000010      S=0.
000011      DO 10 I=1,4
000012      DO 20 J=1,4
000013      V=SB(I,J)+SB(9-I,9-J)-SB(I,9-J)-SB(9-I,J)
000033      A=A+V
000035      AUL=AUL+SB(I,J)
000041      AUR=AUR+SB(I,9-J)
000046      ALL=ALL+SB(9-I,J)
000052      ALR=ALR+SB(9-I,9-J)
000057      20 S=S+V*V
000063      10 CONTINUE
000065      A=A/16.
000067      S=SQRT(S/16.-A*A)
000074      PRINT 30,A,S
000103      30 FORMAT(1X,*M+SD MEMORY *,2E12.4)
000103      PRINT 31,AUL,AUR,ALL,ALR
000117      31 FORMAT(1X,*BY QUADRENTS*,2E12.4,/,13X,2E12.4)
000117      RETURN
000120      END

```

APPENDIX VIII
NOMINAL RUN PRINTOUTS

TITLE	PAGE
ENODB-7, Fading	VIII-2
" -8, "	3
" -9, "	4
" -9.4, "	5
" -10, "	6
" -11, "	7
" -7, No Fade	8
" -8, " "	9
" -9, " "	10
" -9.4, " "	11
" -10, " "	12
" -11, " "	13
9.4dB Acquisition, Fading	14
" " No Fade	15
12.4dB Acquisition, Fading	16
" " No Fade	17
Probability of V, 6dB, No Fade	18
" ", 9.4dB, No Fade	19
" ", -20dB, Fade	20
" ", 6dB, Fade	21
" ", 9.4dB, Fade	22
9.4dB, DYNR = 0, Fading	23
" , DYNR = 3, Fading	24
" , DYNR = 6, Fading	25
" , DYNR = 0, No Fade	26
" , DYNR = 3, No Fade	27
" , DYNR = 6, No Fade	28

ENODB= 7.0 ,DELTA= 62.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 26 ,ASOFT= ,3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0000E+01
 TL= -6.50 ,OYNR= 3.0 ,SOAMP= .230 ,SOPHA= .470 ,I1,I2,I11,I22 129 130 1 1
 WN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 6.1053E-02 ,SIDEV= 5.4928E-03 ,V MEAN= 4.5483E-01V STD DEV= 2.3263E-01 ,BITS= 1900
 LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 4.4000E+01 ,STD DEV= 0.

ERRM

4.6000E+01	9.0000E+00	6.0000E+00	2.0000E+00	1.0000E+00	2.0000E+00	0.	1.0000E+00	1.0000E+00	4.0000E+00
2.0000E+00	2.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	2.0000E+00	0.	1.0000E+00	2.0000E+00	0.
3.0000E+00	1.0000E+00	1.0000E+00	2.0000E+00	1.0000E+00	1.0000E+00	0.	1.0000E+00	1.0000E+00	1.0000E+00
0.	1.0000E+00	2.0000E+00	1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.
2.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	1.0000E+00	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.
1.0000E+00	0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	2.0000E+00

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 483							
109	36	18	15	2	1	1	5	6	1	2	0	0	0	0	
50	26	15	10	2	1	0	1	2	0	0	0	0	0	0	
36	19	20	9	3	1	0	1	5	2	1	1	0	1	0	
19	11	12	4	2	1	0	0	7	0	2	2	0	0	1	
2	5	1	2	1	0	0	1	16	6	5	1	2	0	1	
1	0	0	2	1	0	0	0	42	13	11	2	1	1	0	
1	0	1	0	0	0	0	0	66	34	16	10	2	1	0	
0	0	0	0	0	0	1	0	97	50	33	18	7	1	3	
+1,-1 F(B/A)TIMES 483								+1,+1 F(B/A)TIMES 483							
4	0	3	2	20	50	90	103	4	1	2	1	2	0	1	
2	0	2	1	8	21	31	33	1	0	1	0	0	0	1	
2	0	0	0	5	9	15	19	1	0	1	0	0	1	1	
0	0	0	3	2	5	7	10	0	0	0	0	3	0	1	
2	1	0	0	2	2	1	4	1	1	0	1	2	5	7	
0	0	0	0	2	1	0	1	2	0	2	1	5	18	23	
0	0	0	1	1	0	1	2	0	1	1	2	3	24	34	
1	0	1	3	2	1	0	7	2	1	1	3	6	32	50	

I1,I2,I11,I22 371 874 1326 493
 REC SLICE= 2.4069E+01 ,STD DEV= 3.7233E+00
 ENODB = 7 FADING
 1/31/74M

ENODB= 8.0 ,DELF= 62.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0300E+01 ,FRQDOP= 0. ,FQDPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= .230 ,SDFHA= .470 ,I1,I2,I11,I22= 129 130 1 1
 WN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 614.9 ,TAUR1= 2.0353E+02 ,TAUR2= 1.4945E+00
 PE= 8.2632E-02 ,STDEV= 4.6348E-03 ,V MEAN= 4.5854E-01V STD DEV= 2.1929E-01 ,BITS= 1900
 LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 1.4000E+01 ,STD DEV= 0.

ERRM

3.0000E+01	3.0000E+00	4.0000E+00	0.	1.0000E+00	1.0000E+00	0.	2.0000E+00	0.	2.0000E+00
0.	1.0000E+00	1.0000E+00	0.	3.0000E+00	2.0000E+00	0.	0.	0.	0.
3.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	0.	2.0000E+00	1.0000E+00
0.	0.	2.0000E+00	0.	0.	0.	0.	0.	1.0000E+00	0.
1.0000E+00	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.
0.	1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.	1.0000E+00	1.0000E+00
0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.	0.	3.0000E+00

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 483							
111	31	21	9	3	3	1	1	4	0	2	1	1	0	0	
62	29	17	9	0	1	0	0	2	0	0	0	0	1	0	
38	18	12	13	3	1	1	0	0	0	1	0	0	0	0	
15	16	13	4	1	0	0	0	9	1	1	1	0	1	0	
1	2	1	2	0	0	0	1	14	3	4	2	0	0	1	
1	0	1	1	0	0	0	1	37	9	8	3	0	1	2	
0	0	0	0	0	0	0	0	68	28	17	4	2	0	0	
1	0	0	0	0	0	1	0	121	67	33	23	5	2	4	

+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 483							
2	1	1	2	10	63	66	117	1	2	1	1	1	2	0	1
3	0	0	2	6	17	19	40	0	0	0	0	0	0	0	1
0	1	0	0	2	9	16	17	1	0	0	0	1	0	0	1
2	0	0	0	0	5	4	11	0	0	0	1	0	1	0	3
0	0	0	0	2	3	1	2	0	0	1	0	1	5	6	10
0	0	0	2	0	0	1	3	0	0	0	4	6	13	31	45
0	0	0	1	0	1	0	1	3	0	0	2	1	22	41	82
0	0	0	1	1	0	2	4	5	0	1	2	7	18	50	109

I1,I2,I11,I22 371 874 1326 493
 REC SLICE= 2.5389E+01 ,STD DEV= 3.6756E+00

ENODB = 8 FADING
 1/31/74A

ENODB= 9.0 , DELF= 62.0 , BIF= 1000 , BL2= 176 , NSLICE= 26 , ASOFT= 3000
 SVRH2= 0. , SWMX= 2.8150E+04 , SWMN= 6.8500E+03 , FLO= 1.0000E+01 , FRQDOP= 0. , FQDPR= 1.0000E+01
 TL= -6.50 , DYNR= 3.0 , SQAMP= 230 , SDPHA= .470 , I1,I2,I11,I22 129 130 1 1
 MN= 165.9 , K= 468.6 , TAU1= 4.5000E-01 , TAL2= 8.4420E-03 , WNB= .9 , KB= 614.9 , TAUB1= 2.0353E+02 , TAUB2= 1.4945E+00
 PE= 3.2632E-02 , STDEV= 4.0760E-03 , V MEAN= 4.5188E-01 , STD DEV= 2.0716E-01 , BITS= 1900
 LOCKIN= 1 , DROPOUTS= 1 , AVE= 6.0000E+00 , STD DEV= 0.

ERRM

1.5000E+01	4.0000E+00	2.0000E+00	2.0000E+00	2.0000E+00	1.0000E+00	4.0000E+00	1.0000E+00	0.	0.
0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	2.0000E+00	1.0000E+00	0.	0.	0.
0.	1.0000E+00	1.0000E+00	0.	0.	1.0000E+00	0.	0.	0.	0.
2.0000E+00	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00
0.	2.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	1.0000E+00	2.0000E+00	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	5.0000E+00

-1,-1 P(B/A)TIMES 453									-1,+1 P(B/A)TIMES 482								
102	38	24	9	0	2	1	0	3	3	1	0	0	0	0	0	0	
75	23	20	5	3	0	0	0	1	0	0	0	1	0	0	0	0	
37	26	20	11	4	0	0	0	1	0	0	0	0	0	0	0	0	
13	12	9	7	2	1	0	0	6	3	0	1	0	1	0	0	0	
3	3	3	1	0	0	0	0	12	5	3	0	0	1	0	0	0	
0	0	0	2	1	0	0	0	32	7	10	4	0	1	1	0	0	
0	4	0	0	0	0	0	0	84	31	8	3	3	0	1	0	0	
0	0	0	0	0	0	0	0	129	61	41	21	4	1	0	1	1	

+1,-1 P(B/A)TIMES 483									+1,+1 P(B/A)TIMES 482								
0	0	0	2	24	64	102	127	1	0	0	0	1	0	3	1	0	
1	0	1	1	3	16	25	36	0	0	0	0	1	0	2	0	0	
1	1	0	0	1	9	8	25	0	1	0	0	0	1	0	0	1	
1	2	0	1	4	4	6	3	0	0	0	0	1	0	1	0	2	
1	1	0	0	1	2	2	0	0	0	0	0	1	2	7	14	10	
0	0	0	1	1	2	0	0	1	0	0	0	2	4	17	28	50	
0	0	0	0	1	0	1	1	1	1	0	1	1	5	14	46	84	
0	0	0	0	0	0	1	0	3	0	2	3	8	16	49	97		

I1,I2,I11,I22 231 338 529 737
 REC SLICE= 2.6015E+01 , STD DEV= 3.6146E+00
 ENODB = 9 FADING
 1/31/74M

ENODD= 9.4 , DELF= 62.0 , BIF= 1000 , BL2= 176 , NSLICE= 26 , ASOFT= .3000
 SVRHZ= 0. , SWMX= 2.8150E+04 , SWMN= 6.8500E+03 , FLC= 1.0000E+01 , FRQDOP= 0. , FQDPRT= 1.0800E+01
 TL= -6.60 , DYNR= 3.0 , SOAMP= .230 , SDPHA= .470 , I1,I2,I11,I22 129 130 1 1
 WN= 165.9 , K= 468.6 , YAU1= 4.5000E-01 , YAU2= 8.4420E-03 , WNB= .9 , KB= 614.9 , TAMP1= 2.0353E+02 , TAUB2= 1.4945E+00
 PE= 2.4737E-02 , STDEV= 3.5633E-03 , V MEAN= 4.5633E-01V STD DEV= 2.0598E-01 , BITS= 1900
 LOCKIN= 1 , DROPOUTS= 1 , AVE= 4.0000E+00 , STD DEV= 0.

ERRM

0.0000E+00	3.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	3.0000E+00	1.0000E+00	1.0000E+00	0.
0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
1.0000E+00	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	0.	1.0000E+00	0.	1.0000E+00
0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	3.0000E+00	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.	0.	4.0000E+00

-1,-1 P(B/A)TIMES 483									-1,+1 P(B/A)TIMES 482								
107	36	23	6	1	1	0	0	0	2	1	0	0	0	0	0	0	
76	25	20	5	2	0	0	0	0	2	0	0	0	0	0	0	0	
34	28	20	12	2	0	0	0	0	0	0	0	1	0	0	0	0	
12	13	9	6	4	0	0	0	0	4	1	0	1	0	0	0	0	
4	2	2	2	0	0	0	0	0	14	3	2	1	0	0	1	0	
0	0	0	1	0	0	0	0	0	30	10	8	6	0	0	1	0	
0	0	0	1	0	0	0	0	0	90	27	6	4	1	0	0	0	
0	0	0	0	0	0	0	0	0	131	64	44	20	3	2	0	2	
+1,-1 P(B/A)TIMES 483									+1,+1 P(B/A)TIMES 482								
0	1	0	1	24	69	108	130	0	1	0	0	1	0	2	0	1	
0	0	0	3	1	13	23	41	0	0	0	0	1	1	0	1	0	
2	0	1	0	0	7	11	18	0	0	1	0	0	0	1	0	0	
3	1	0	1	3	4	7	3	0	0	0	0	0	1	2	1	1	
0	0	0	0	1	2	0	0	0	0	0	0	0	0	7	11	10	
0	0	0	0	0	1	0	1	1	1	0	0	2	5	13	34	51	
0	0	0	0	0	0	1	0	0	0	1	2	0	6	19	45	86	
0	0	0	0	0	1	1	0	0	1	1	0	2	7	20	45	98	

I1,I2,I11,I22 638 1850 529 737
 REC SLICE= 2.6261E+01 , STD DEV= 3.5269E+00
 ENODD = 9.4 FADING --
 1/31/74A

ENODB= 11.0 , DELF= 62.0 , STF= 1000 , BL2= 176 , NSLICE= 26 , #SOF7= 3000
 SVRHZ= 0. , SMNY= 2.8150E+04 , SMN= 6.8500E+03 , FLO= 1.0000E+01 , FRQDOP= 0. , FQDPRT= 1.0000E+01
 TL= -6.50 , RYNR= -3.0 , SBAMP= 230 , SDFHA= .470 , I1,I2,I11,I22 129 130 -1 -1
 MN= 165.9 , K= 468.F , TAU1= 4.5000E-01 , TAU2= 8.4420E-03 , WNB= .9 , KB= 614.9 , TAU81= 2.0353E+02 , TAU82= 1.4945E+00
 PE= 1.4211E-02 , STDEV= 2.7153E-03 , V MEAN= 4.7051E-01V STD DEV= 1.9098E-01 , BITS= 1900
 LOCKIN= 0 , DROPOUTS= 1 , AVE= 1.0000E+00 , STD DEV= 0.

ERRM

6.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00
0.	0.	0.	0.	0.	0.	1.0000E+00	1.0000E+00	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	0.	0.	1.0000E+00	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.0000E+00

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 482							
107	30	15	4	1	0	0	0	1	0	0	0	0	0	0	
78	28	26	4	1	0	0	0	0	1	1	1	0	0	0	
49	33	25	9	1	1	0	0	1	0	0	0	0	0	0	
6	10	12	4	1	0	0	0	0	0	0	1	1	0	0	
4	0	2	0	0	0	0	0	3	2	1	1	0	0	0	
0	0	0	0	0	0	0	0	25	5	7	2	2	0	0	
0	0	6	0	0	0	0	0	79	27	6	3	0	1	0	
0	0	0	0	0	0	0	0	176	77	41	14	2	0	1	
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 484							
2	1	0	4	11	64	142	149	0	0	0	0	0	1	0	
0	0	0	0	1	8	17	50	0	0	0	1	0	0	0	
0	0	1	0	2	4	6	5	0	0	2	0	0	0	0	
0	0	0	1	0	1	2	6	0	0	0	0	1	1	0	
0	1	0	0	0	0	1	1	0	0	0	0	0	3	11	
0	0	0	0	0	2	0	0	0	1	0	0	2	8	29	
0	0	0	0	0	0	0	1	0	0	0	0	6	21	69	
0	0	0	0	0	0	0	0	0	1	0	0	3	16	47	
0	0	0	0	0	0	0	0	0	0	0	0	0	0	95	

I1,I2,I11,I22 1412 490 1522 122F
 REC SLICE= 2.6837E+01 , STD DEV= 3.7227E+00
 ENODB = 11 FADING
 1/31/74M

ENODB= 7.0 ,DELF= -E2.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0. ,SMMX= 2.8150E+04 ,SMWN= 6.8500E+03 ,FLO= 1.8000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0800E+01
 I1= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SOPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 WN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 4.5789E-02 ,STDDEV= 4.7954E-03 ,V MEAN= 4.5711E-01V STD DEV= 2.3731E-01 ,BITS= 1900
 LOCKIN= 1 ,DROPOUTS=0

ERRM

1.4000E+01	4.0000E+00	2.0000E+00	5.0000E+00	2.0000E+00	2.0000E+00	5.0000E+00	3.0000E+00	1.0000E+00	0.
2.0000E+00	3.0000E+00	1.0000E+00	0.	1.0000E+00	3.0000E+00	5.0000E+00	1.0000E+00	0.	0.
0.	0.	0.	4.0000E+00	2.0000E+00	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00
1.0000E+00	2.0000E+00	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	2.0000E+00	1.0000E+00	1.0000E+00
2.0000E+00	0.	0.	0.	1.0000E+00	0.	2.0000E+00	0.	0.	0.
0.	0.	2.0000E+00	0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 482							
93	37	17	12	3	1	1	0	6	2	0	0	0	0	0	
60	27	17	15	2	0	1	0	1	1	0	0	0	0	0	
38	21	19	11	5	0	1	0	0	0	1	0	0	0	0	
17	16	10	3	1	2	0	0	11	0	4	1	0	0	1	
6	3	6	0	1	0	0	0	21	7	8	0	0	0	1	
1	1	0	0	1	0	0	0	36	11	7	2	3	0	0	
0	1	0	1	0	0	0	0	59	20	11	6	2	0	1	
0	0	0	0	0	0	0	0	119	67	37	25	8	1	1	
+1,-1 P(B/A)TIMES 482								+1,+1 P(B/A)TIMES 485							
1	2	3	9	23	53	73	141	0	0	0	2	2	0	2	0
2	0	0	2	8	11	30	39	0	0	0	0	0	3	0	0
1	0	1	0	3	6	13	18	0	0	0	0	2	2	1	0
2	0	0	1	3	3	4	13	0	0	0	0	2	1	0	4
1	0	0	0	3	1	3	2	0	0	0	2	7	3	7	19
0	0	0	0	0	0	0	1	0	0	0	1	4	13	15	57
1	0	0	1	0	1	0	0	2	0	1	1	5	19	28	63
0	0	0	1	0	0	1	1	4	3	1	4	13	33	42	117

I1,I2,I11,I22 638 1850 1 1
 REC SLICE= 2.4163E+01 ,STD DEV= 3.5649E+00

ENODB = 7 NO FADE
 1/31/74M

ENODB= 8.0 , DELF= 62.0 , BIF= 1000 , BL2= 176 , NSLICE= 26 , ASOFT= 3000
 SVRHZ= 0. , SWHX= 2.8150E+04 , SWHM= 6.8500E+03 , FLO= 1.0000E+01 , FRODOP= 0. , FGDPRF= 1.0000E+01
 TL= -6.50 , DYNR= 3.0 , SDAMP= 0.000 , SOPHA= 0.000 , I1,I2,I11,I22 129 130 1 1
 MN= 165.9 , K= 468.6 , TAU1= 4.5000E-01 , TAU2= 8.4420E-03 , WNB= .9 , KB= 614.9 , TAU11= 2.0353E+02 , TAU22= 1.4945E+00
 PE= 2.5263E-02 , STDEV= 3.6001E-03 , V MEAN= 4.5835E-01V STD DEV= 2.1459E-01 , RITS= 1000
 LOCKIN= 1 , DROPOUTS=0
 ERRM

8.0000E+00	2.0000E+00	1.0000E+00	C.	1.0000E+00	2.0000E+00	1.0000E+00	1.0000E+00	0.	0.
0.	1.0000E+00	1.0000E+00	C.	0.	0.	0.	1.0000E+00	0.	0.
0.	1.0000E+00	2.0000E+00	2.0000E+00	1.0000E+00	0.	0.	1.0000E+00	0.	0.
1.0000E+00	0.	0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.
0.	1.0000E+00	1.0000E+00	0.	0.	0.	2.0000E+00	0.	1.0000E+00	0.
0.	0.	1.0000E+00	C.	1.0000E+00	0.	0.	0.	0.	0.
1.0000E+00	1.0000E+00	0.	1.0000E+00	0.	0.	0.	1.0000E+00	1.0000E+00	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	2.0000E+00	C.	0.	0.	0.	0.	0.	0.
0.	0.	0.	C.	0.	0.	0.	0.	0.	4.0000E+00

-1,-1 P(B/A)TIMES 461								-1,+1 P(B/A)TIMES 482							
9*	34	13	R	2	1	0	1	1	1	1	0	0	0	0	
7*	26	20	13	1	0	0	0	2	1	0	0	0	0	0	
3*	27	19	9	4	1	0	0	1	2	1	0	0	0	0	
2*	11	5	3	2	0	0	0	1	1	1	0	0	0	0	
4	2	4	1	2	0	0	0	15	3	5	1	0	0	2	
1	0	0	0	0	0	0	0	43	5	12	1	1	0	0	
1	0	0	0	0	0	0	0	65	30	11	4	1	0	0	
0	0	0	0	0	0	0	0	125	69	47	23	5	0	1	

+1,-1 P(B/A)TIMES 482								+1,+1 P(B/A)TIMES 485							
2	0	1	4	24	58	106	140	0	0	0	0	1	1	2	0
2	0	0	0	2	14	27	31	0	0	0	0	0	0	0	0
0	1	1	0	3	8	8	23	0	0	0	0	0	2	0	0
1	2	1	0	2	4	2	6	0	0	0	0	1	1	0	3
0	0	1	0	1	1	1	1	0	0	1	0	4	2	10	15
0	0	0	1	0	0	0	0	0	0	0	1	4	12	26	52
0	0	0	0	0	0	0	0	0	0	0	0	5	25	42	84
0	0	1	0	1	0	1	0	2	0	0	2	10	29	42	106

I1,I2,I11,I22 1594 1314 1 1
 REC SLICE= 2.4951E+01 , STD DEV= 3.4991E+00
 ENODB = 8 NO FADE
 1/31/74D

ENODB= 9.0 ,DELTA= -42.4 ,RIF= 1000 ,RL2= 176 ,NSLICE= 26 ,ASOFT= .3000
 SVRH2= 0. ,SMMX= 2.9150E+04 ,SMMY= 6.8500E+03 ,FLC= 1.0000E+01 ,FRQ00P= 0. ,FODPRT= 1.0888E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= -0.600 ,SDFWA= 0.000 ,I1,I2,I11,I22 -129 130 -1 1
 WN= 165.9 ,K= 484.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNP= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 1.0000E-02 ,STDEV= 2.2827E-01 ,V MEAN= 4.7164E-01V STD DEV= 1.9349E-01 ,BITS= 1900
 LOCKIN= 2 ,PROFOUTS=0

ERRM

2.0000E+00	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.0000E+00
1.0000E+00	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	7.0000E+00

-1,-1 P(R/A)TIMES 455								-1,+1 P(R/A)TIMES 482							
108	39	14	2	1	0	0	0	0	0	0	0	0	0	0	0
76	37	21	7	3	0	1	0	0	0	0	0	0	0	0	0
43	27	19	8	1	0	1	0	2	0	0	0	0	0	0	0
17	11	5	2	2	0	0	0	2	0	0	0	0	0	0	0
5	2	2	1	0	0	0	0	5	2	0	0	0	0	0	0
0	0	0	0	0	0	0	0	45	12	6	0	0	0	0	0
0	0	0	0	0	0	0	0	86	24	14	5	0	0	0	0
0	0	0	0	0	0	0	0	136	67	53	18	4	0	0	0
+1,-1 P(R/A)TIMES 482								+1,+1 P(R/A)TIMES 481							
0	0	1	2	18	71	130	140	0	0	0	0	0	0	0	0
0	0	0	0	4	10	23	39	0	0	0	0	0	0	0	0
0	0	1	0	0	5	8	21	0	0	0	0	1	0	0	0
0	0	0	0	0	1	2	3	0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	1	0	0	0	0	0	5	2	16
0	0	0	0	0	0	0	0	0	0	1	0	1	12	26	41
0	0	0	1	0	1	0	0	0	0	0	0	5	20	55	94
0	0	0	0	0	0	0	0	0	0	0	0	2	19	57	123

I1,I2,I11,I22 -121 -752 -1 1
 REC SLICE= 2.5673E+01 ,STD DEV= 3.4843E+00
 ENODB = 9 NO FADE
 1/31/74M

ENODB= 9.4 , DELF= 52.0 , BIF= 1000 , BL2= 176 , NSLICE= 26 , ASOFT= .3000
 SURHZ= 0. , SWMX= 2.8150E+04 , SWMN= 6.8500E+03 , FLO= 1.0000E+01 , FRODOP= 0. , FQDPRT= 1.3800E+01
 TL= -6.50 , DYNR= 3.0 , SDAMP= 0.000 , SDPHA= 0.000 , T1,I2,I11,I22 129 130 1 1
 WN= 165.9 , K= 468.6 , TAU1= 4.5000E-01 , TAU2= 8.4420E-03 , WNB= .9 , KB= 614.9 , TAU1= 2.0353E+02 , TAU2= 1.4949E+00
 PE= 8.9474E-03 , STDEV= 2.1503E-03 , V MEAN= 4.7353E-01V STD DEV= 1.8772E-01 , PITS= 1900

LOCKIN= 1 , DRCFOUTS=C

ERRM

2.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.0000E+00
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	7.0000E+00

-1,-1 P(B/A)TIMES 455										-1,+1 P(B/A)TIMES 482									
117	32	11	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
73	39	27	4	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4F	29	21	7	1	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
16	9	4	3	2	0	0	0	0	0	2	0	0	0	0	0	0	0	0	0
3	2	1	1	0	0	0	0	0	0	5	1	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	46	8	5	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	A1	25	11	3	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	148	71	57	16	2	0	0	0	0	0
+1,-1 F(B/A)TIMES 482										+1,+1 F(B/A)TIMES 481									
0	1	0	3	20	69	131	149			0	0	0	0	0	0	0	0	0	0
0	0	1	0	2	10	23	35			0	0	0	0	0	1	0	0	0	0
0	0	0	0	1	2	8	22			0	0	0	0	0	0	1	0	0	0
0	0	0	0	0	0	2	1			0	0	0	1	0	1	0	1	0	1
0	0	0	0	0	1	0	1			0	0	0	0	0	4	3	17		
0	0	0	0	0	0	0	0			0	0	0	0	0	11	30	36		
0	0	0	0	0	0	0	0			0	0	0	0	0	5	20	57	101	
0	0	0	0	0	0	0	0			0	0	1	1	1	17	49	123		

I1,I2,I11,I22 1594 1314 1 1
 REC SLICE= 2.5978E+01 , STD DEV= 3.3165E+00
 ENODB = 9A NO FADE
 1/31/74A


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ENODB= 9.4 ,DELTA= 62.0 ,RIF= 1000 ,BL2= 176
SVRHZ= 2.2000E+03 ,SNMX= 2.5000E+03 ,SNMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRODDP= 1.0000E+03 ,FQDPR= 1.0000E+01
TL= -6.50 ,DYNP= 3.0 ,SDAMP= .230 ,SDPHA= .470 ,I1,I2,I11,I22 1 1 1 1
NN= 165.9 ,K= 45.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03
NACQ,AMISS,AFAL,KDATA,ES,EV,EV1
1 0. 0. 1.0000E+00 69 2.2827E+01 1.4074E+01 5.8374E-01
2 0. 0. 2.0000E+00 68 2.2470E+01 1.3472E+01 -5.3055E-02
3 0. 0. 3.0000E+00 68 2.2743E+01 1.3875E+01 3.3307E-01
4 0. 0. 4.0000E+00 72 2.3811E+01 1.3907E+01 3.4400E-01
5 0. 0. 5.0000E+00 74 2.4520E+01 1.3216E+01 -1.2795E+00
6 0. 0. 6.0000E+00 75 2.4941E+01 1.3900E+01 4.6619E-01
7 0. 0. 7.0000E+00 72 2.3830E+01 1.2615E+01 -9.5723E-01
8 0. 0. 8.0000E+00 67 2.2288E+01 1.3022E+01 -4.2562E-01
9 0. 0. 9.0000E+00 71 2.3514E+01 1.3099E+01 -4.0001E-01
10 0. 0. 1.0000E+01 72 2.3912E+01 1.3345E+01 -1.9361E-01
11 0. 0. 1.1000E+01 66 2.2103E+01 1.3134E+01 -4.4800E-01
12 0. 0. 1.2000E+01 72 2.3989E+01 1.3283E+01 -2.0432E-01
13 0. 0. 1.3000E+01 65 2.1738E+01 1.4556E+01 9.7550E-01
14 0. 0. 1.4000E+01 71 2.3541E+01 1.3793E+01 2.2185E-01
15 0. 0. 1.5000E+01 71 2.3535E+01 1.2560E+01 -9.7664E-01
16 0. 0. 1.6000E+01 70 2.3152E+01 1.3611E+01 1.4561E-01
17 0. 0. 1.7000E+01 72 2.3933E+01 1.3486E+01 -1.4073E-01
18 0. 0. 1.8000E+01 71 2.3743E+01 1.3470E+01 -1.0426E-02
19 0. 0. 1.9000E+01 73 2.4175E+01 1.3367E+01 -1.0955E-01
20 0. 0. 2.0000E+01 73 2.4424E+01 1.3756E+01 3.1282E-01
21 0. 0. 2.1000E+01 66 2.1927E+01 1.3814E+01 3.0624E-01
22 0. 0. 2.2000E+01 70 2.3221E+01 1.3273E+01 -2.9962E-01
23 0. 0. 2.3000E+01 73 2.4217E+01 1.3482E+01 -5.4756E-02
24 0. 0. 2.4000E+01 73 2.4389E+01 1.3154E+01 -3.0937E-01
25 0. 0. 2.5000E+01 75 2.4892E+01 1.3045E+01 -5.2742E-01
26 0. 0. 2.6000E+01 70 2.3397E+01 1.4643E+01 1.1306E+00
27 0. 0. 2.7000E+01 70 2.3231E+01 1.3816E+01 2.4060E-01
28 0. 0. 2.8000E+01 67 2.2252E+01 1.3197E+01 -2.5854E-01
29 0. 0. 2.9000E+01 67 2.2305E+01 1.3494E+01 -0.3494E-02
30 0. 0. 3.0000E+01 67 2.2185E+01 1.2524E+01 -9.8497E-01
RACQ= 1.0000E+00 ,STDEV= 0.
AVEES= 2.3377E+01 ,STDES= 8.9371E-01
AVE KDATA= 7.0333E+01 ,STD DEV= 2.7366E+00
PR MISSED ACQ= 0.
PR FALSE ACQ= 0.
ENODB = 9.4. ACQUISITION FADING
2/6/74A
I1,I2,I11,I22 312 1977 07 1981

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ENOD9= 9.4 ,DELTA= 62.0 ,BIF= 1000 ,BL2= 176
 SVRHZ= 2.2000E+03 ,SMMX= 2.5000E+03 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 1.0000E+03 ,FODPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,STAMP= 0.000 ,SOPHA= 0.000 ,I1,I2,I11,I22 1 1 1 1
 MN= 165.0 ,K= 38.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03

NACO,AMISS,AFAL,KDATA,ES,EV,EV1

1	0.	0.	1.0000E+00	67	2.2232E+01	1.4411E+01	1.4328E+00
2	0.	0.	2.0000E+00	70	2.3221E+01	1.3254E+01	-3.3428E-01
3	0.	0.	3.0000E+00	68	2.2563E+01	1.2780E+01	-7.2919E-01
4	0.	0.	4.0000E+00	73	2.4379E+01	1.3613E+01	2.0185E-01
5	0.	0.	5.0000E+00	73	2.4248E+01	1.2040E+01	-1.4811E+00
6	0.	0.	6.0000E+00	75	2.5112E+01	1.3833E+01	3.3289E-01
7	0.	0.	7.0000E+00	71	2.3471E+01	1.2966E+01	-5.7815E-01
8	0.	0.	8.0000E+00	69	2.2889E+01	1.3427E+01	-2.2844E-01
9	0.	0.	9.0000E+00	73	2.4161E+01	1.3854E+01	3.5261E-01
10	0.	0.	1.0000E+01	70	2.3382E+01	1.5306E+01	1.8587E+00
11	0.	0.	1.1000E+01	73	2.4260E+01	1.3547E+01	4.2381E-02
12	0.	0.	1.2000E+01	69	2.3085E+01	1.3990E+01	4.6624E-01
13	0.	0.	1.3000E+01	71	2.3755E+01	1.4570E+01	1.0965E+00
14	0.	0.	1.4000E+01	71	2.3560E+01	1.3617E+01	1.3730E-01
15	0.	0.	1.5000E+01	69	2.3107E+01	1.3035E+01	-4.7169E-01
16	0.	0.	1.6000E+01	70	2.3143E+01	1.2883E+01	-5.5778E-01
17	0.	0.	1.7000E+01	75	2.5127E+01	1.4168E+01	6.5151E-01
18	0.	0.	1.8000E+01	71	2.3575E+01	1.3339E+01	-1.9897E-01
19	0.	0.	1.9000E+01	67	2.2314E+01	1.3275E+01	-2.7460E-01
20	0.	0.	2.0000E+01	72	2.3853E+01	1.2641E+01	-9.7835E-01
21	0.	0.	2.1000E+01	73	2.4233E+01	1.3759E+01	2.1434E-01
22	0.	0.	2.2000E+01	74	2.4574E+01	1.3484E+01	-6.9096E-02
23	0.	0.	2.3000E+01	69	2.2864E+01	1.4139E+01	5.6728E-01
24	0.	0.	2.4000E+01	67	2.2291E+01	1.2612E+01	-8.4230E-01
25	0.	0.	2.5000E+01	73	2.4284E+01	1.2445E+01	-1.1641E+00
26	0.	0.	2.6000E+01	77	2.5675E+01	1.3988E+01	4.2820E-01
27	0.	0.	2.7000E+01	73	2.4428E+01	1.2721E+01	-7.7898E-01
28	0.	0.	2.8000E+01	69	2.3093E+01	1.4109E+01	6.4353E-01
29	0.	0.	2.9000E+01	69	2.2998E+01	1.2769E+01	-7.1159E-01
30	0.	0.	3.0000E+01	71	2.3531E+01	1.3569E+01	7.8444E-02

PACQ= 4.0100E+00 ,STDEV= 0.
 AVEES= 2.3648E+01 ,STDES= 8.5854E-01
 AVE KDATA= 7.1067E+01 ,STD DEV= 2.5157E+00
 PR MISSED ACQ= 0.
 PR FALSE ACQ= 0.

ENODB = 9.4 ACQUISITION NO FADE
 2/7/74M

I1,I2,I11,I22 554 713 1 1

ENODB= 12.4 , DELF= 62.0 , BIF= 100J , BL2= 176									
SVRHZ= 2.2000E+03 , SWMX= 2.5000E+03 , SWMN= 6.8500E+03 , FLO= 1.1000E+01 , FRODOP= 1.0000E+03 , FODPRT= 1.0000E+01									
TL= -6.50 , DYNR= 3.0 , SOAMP= .230 , SOPHA= .+70 , I1,I2,I11,I22 1 1 1 1									
WN= 165.9 , K= 468.6 , TAU1= 4.5000E-01 , TAU2= 8.4+20E-03									
NACQ, AMISS, AFAL, KDATA, ES, EV, EV1									
1	0.	0.	1.0000E+00	64	2.1237E+01	1.4830E+01	1.4056E+00		
2	0.	0.	2.0000E+00	72	2.3809E+01	1.3014E+01	-5.9865E-01		
3	0.	0.	3.0000E+00	76	2.5169E+01	1.4236E+01	6.6512E-01		
4	0.	0.	4.0000E+00	76	2.5152E+01	1.3398E+01	-2.6947E-01		
5	0.	0.	5.0000E+00	72	2.4106E+01	1.3916E+01	4.2874E-01		
6	0.	0.	6.0000E+00	79	2.6253E+01	1.3597E+01	4.9693E-03		
7	0.	0.	7.0000E+00	82	2.7250E+01	1.3391E+01	-1.4508E-01		
8	0.	0.	8.0000E+00	74	2.4733E+01	1.2888E+01	-7.0808E-01		
9	0.	0.	9.0000E+00	76	2.5971E+01	1.3726E+01	1.2707E-01		
10	0.	0.	1.0000E+01	74	2.4694E+01	1.2798E+01	-6.5254E-01		
11	0.	0.	1.1000E+01	79	2.6358E+01	1.2965E+01	-5.0201E-01		
12	0.	0.	1.2000E+01	76	2.5277E+01	1.4778E+01	1.2345E+00		
13	0.	0.	1.3000E+01	73	2.4140E+01	1.3675E+01	4.6815E-02		
14	0.	0.	1.4000E+01	79	2.6338E+01	1.4090E+01	4.9934E-01		
15	0.	0.	1.5000E+01	64	2.1121E+01	1.4074E+01	4.8983E-01		
16	0.	0.	1.6000E+01	74	2.4502E+01	1.2881E+01	-6.6133E-01		
17	0.	0.	1.7000E+01	74	2.4597E+01	1.4949E+01	1.5002E+00		
18	0.	0.	1.8000E+01	73	2.4398E+01	1.3452E+01	-7.1677E-02		
19	0.	0.	1.9000E+01	72	2.4116E+01	1.3141E+01	-4.6447E-01		
20	0.	0.	2.0000E+01	75	2.4843E+01	1.3276E+01	-2.4706E-01		
21	0.	0.	2.1000E+01	67	2.2366E+01	1.3852E+01	3.2170E-01		
22	0.	0.	2.2000E+01	73	2.4195E+01	1.1549E+01	-2.0853E+00		
23	0.	0.	2.3000E+01	72	2.4049E+01	1.3130E+01	-3.8302E-01		
24	0.	0.	2.4000E+01	65	2.1589E+01	1.3612E+01	1.2866E-01		
25	0.	0.	2.5000E+01	77	2.5688E+01	1.3264E+01	-1.2554E-02		
26	0.	0.	2.6000E+01	73	2.4168E+01	1.3319E+01	-3.5070E-01		
27	0.	0.	2.7000E+01	66	2.2063E+01	1.4065E+01	1.1704E+00		
28	0.	0.	2.8000E+01	74	2.4507E+01	1.2953E+01	-3.8080E-01		
29	0.	0.	2.9000E+01	67	2.2244E+01	1.3348E+01	-1.0998E-01		
30	0.	0.	3.0000E+01	71	2.3573E+01	1.3723E+01	1.2119E-01		
PACQ= 1.0000E+00 , STDEV= 0.									
AVEES= 2.4284E+01 , STDES= 1.5236E+00									
AVE KDATA= 7.3033E+01 , STD DEV= 4.5496E+00									
PR MISSED ACQ= 0.									
PR FALSE ACQ= 0.									
I1,I2,I11,I22 261 951 1634 241									

ENODB = 12.4 ACQUISITION FADING
2/6/74M

ENODB= 12.4 ,DELTA= 62.0 ,BIF= 1000 ,BL2= 176
 SVRHZ= 2.2000E+03 ,SMX= 2.5000E+03 ,SMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 1.0000E+03 ,FQDPR= 1.0000E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SDPHA= 0.000 ,I1,I2,I11,I22 1 1 1 1
 MN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03

NACO,AMISS,AFAL,KDATA,ES,EV,EV1

1	0.	0.	1.0000E+00	71	2.3516E+01	1.2265E+01	-1.1345E+00
2	0.	0.	2.0000E+00	77	2.5584E+01	1.2110E+01	-1.3762E+00
3	0.	0.	3.0000E+00	76	2.5373E+01	1.2996E+01	-5.2821E-01
4	0.	0.	4.0000E+00	70	2.3223E+01	1.4250E+01	6.9029E-01
5	0.	0.	5.0000E+00	76	2.5190E+01	1.2952E+01	-5.3322E-01
6	0.	0.	6.0000E+00	72	2.4071E+01	1.3547E+01	4.7392E-02
7	0.	0.	7.0000E+00	78	2.5938E+01	1.4894E+01	-1.3724E+00
8	0.	0.	8.0000E+00	75	2.4959E+01	1.2817E+01	-6.9791E-01
9	0.	0.	9.0000E+00	76	2.5395E+01	1.3250E+01	-3.4141E-01
10	0.	0.	1.0000E+01	68	2.2725E+01	1.3790E+01	2.5845E-01
11	0.	0.	1.1000E+01	75	2.4926E+01	1.4054E+01	5.1976E-01
12	0.	0.	1.2000E+01	74	2.4755E+01	1.4168E+01	6.6020E-01
13	0.	0.	1.3000E+01	77	2.5487E+01	1.4116E+01	5.6072E-01
14	0.	0.	1.4000E+01	70	2.3235E+01	1.3964E+01	3.7138E-01
15	0.	0.	1.5000E+01	73	2.4170E+01	1.2082E+01	-1.4648E+00
16	0.	0.	1.6000E+01	72	2.3969E+01	1.3680E+01	8.7723E-02
17	0.	0.	1.7000E+01	77	2.5789E+01	1.2266E+01	-1.2720E+00
18	0.	0.	1.8000E+01	75	2.5132E+01	1.2247E+01	-1.2798E+00
19	0.	0.	1.9000E+01	73	2.4345E+01	1.3938E+01	4.3054E-01
20	0.	0.	2.0000E+01	73	2.4385E+01	1.3620E+01	4.1238E-02
21	0.	0.	2.1000E+01	70	2.3357E+01	1.2656E+01	-8.8830E-01
22	0.	0.	2.2000E+01	72	2.3900E+01	1.2971E+01	-7.2588E-01
23	0.	0.	2.3000E+01	72	2.3819E+01	1.3358E+01	-1.1341E-01
24	0.	0.	2.4000E+01	71	2.3575E+01	1.3110E+01	-3.1621E-01
25	0.	0.	2.5000E+01	74	2.4790E+01	1.3950E+01	3.7404E-01
26	0.	0.	2.6000E+01	72	2.4131E+01	1.4326E+01	8.5348E-01
27	0.	0.	2.7000E+01	73	2.4383E+01	1.3338E+01	-3.0933E-01
28	0.	0.	2.8000E+01	71	2.3566E+01	1.2102E+01	-1.4967E+00
29	0.	0.	2.9000E+01	71	2.3786E+01	1.2928E+01	-6.8400E-01
30	0.	0.	3.0000E+01	74	2.4548E+01	1.2764E+01	-6.9476E-01

PACQ= 1.0000E+00 ,STDEV= 0.
 AVEES= 2.4401E+01 ,STDES= 8.3758E-01
 AVE KDATA= 7.3267E+01 ,STD DEV= 2.4891E+00
 PR MISSED ACQ= 0.
 PR FALSE ACQ= 0.
 I1,I2,I11,I22 1657 745 1 1

ENODB = 12.4 ACQUISITION NO. FADE-
 2/6/74N

NRUNS, NSPB, ENODB, DELF, RIF, ENQMIN
 2000 40 6.0000E+00 6.2000E+01 1.0000E+03 9.0000E+00
 BL2, PHIDEG, FDIFF, BL2E, PHIB, FDIFFB
 1.7600E+02 1.0000E+01 3.4243E+02 1.0000E+00 1.0000E+01 5.0000E+00
 FBAMP, FBPHA, SDAMP, SDPHA, GAM43, N43, ASLICE
 2.0000E+00 2.0000E-01 0. 0. 9.0000E-02 64 26
 FLO, FRQDOP, FQDPR, ASCFT, I1, I2, I11, I22
 1.0000E+01 0. 0. 2.6496E-01 1 1 1 1
 SVRHZ, SWX, SWM, TL

0. 2.8150E+04 6.8500E+03 -8.0000E+00
 CCLOSC, IOLBIT, OYNR
 0. 100 3.0000E+00

WN, K, TAU1, TAU2
 1.659344E+02 4.686449E+02 4.499999E-01 8.442020E-03
 WNB, KB, TAU81, TAU82
 4.201E-01 6.1485E+02 2.0353E+02 1.4949E+00
 IT, TSYNC
 1.1364E-02

PE, STDEV, MSSUM, MSSIG, KOUNT
 6.1979E-02 5.5149E-03 4.5272E-01 2.4763E-01 2000
 LOOKIN 1DRCPOTS 1AVE 4.0000E+00SD 0.

ERRM

2.1000E+01	7.0000E+00	3.0000E+00	5.0000E+00	8.0000E+00	4.0000E+00	1.0000E+01	3.0000E+00	5.0000E+00	3.0000E+00
1.0000E+00	1.0000E+00	2.0000E+00	3.0000E+00	1.0000E+00	1.0000E+00	0.	1.0000E+00	1.0000E+00	2.0000E+00
3.0000E+00	1.0000E+00	4.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	2.0000E+00	1.0000E+00	1.0000E+00
3.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	1.0000E+00	2.0000E+00	2.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	1.0000E+00	0.
1.0000E+00	0.	1.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00

1140 1830 408 1137
 REC SLICE= 2.3453E+01 5.2509E+00
 XXXC, ASUM1, ASUM2, VSUM1, VSUM2, VSUM3,
 7.6017E+04 1.9179E+06 5.8981E+07 -1.3095E+06 2.3027E+07 -4.1166E+08

V HISTCGRAM

0.	1.2486E-05	2.4972E-05	1.2486E-05	3.7458E-05	2.4972E-05	1.2486E-05	1.2486E-05	2.4972E-05	4.9944E-05
4.9944E-05	4.9944E-05	8.7402E-05	6.2430E-05	4.9944E-05	3.7458E-05	6.2430E-05	4.9944E-05	4.9944E-05	1.8729E-04
7.4916E-05	1.2486E-04	9.9888E-05	1.3735E-04	4.9944E-05	4.9944E-05	1.2486E-04	1.9978E-04	2.1226E-04	2.2475E-04
7.8662E-04	5.7435E-04	6.4927E-04	6.3656E-04	1.3360E-03	1.2611E-03	1.6232E-03	1.6981E-03	1.7855E-03	2.8352E-03
1.8979E-03	1.7355E-03	2.2350E-03	2.7469E-03	2.8718E-03	3.7288E-03	4.5449E-03	3.7333E-03	4.5449E-03	5.0194E-03
6.4178E-03	6.5676E-03	8.1159E-03	8.7776E-03	8.9275E-03	1.0064E-02	1.2411E-02	1.3435E-02	1.7438E-02	1.9891E-02
2.1351E-02	2.4023E-02	2.6046E-02	2.5796E-02	3.0253E-02	3.2289E-02	3.5972E-02	4.0167E-02	4.1741E-02	4.5824E-02
4.6648E-02	4.7447E-02	4.6573E-02	4.8346E-02	4.3389E-02	4.1965E-02	4.1154E-02	3.9331E-02	3.7395E-02	3.0428E-02
2.4972E-02	1.9765E-02	1.4034E-02	1.1999E-02	7.3667E-03	5.6312E-03	5.1692E-03	2.8468E-03	1.6856E-03	1.2361E-03
7.2419E-04	1.6232E-04	0.	0.	0.	0.	0.	0.	0.	0.

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NRUNS, NSPB, ENODB, DELF, BIF, ENOMIN
2000 40 9.4000E+00 6.2000E+01 1.0000E+03 9.0000E+00
BL2, PHIDEG, FOIFF, BL2E, PHIB, FOIFFB
1.7600E+02 1.8000E+01 3.4243E+02 1.0000E+00 1.0000E+01 5.0000E+00
FBAMP, FBPHA, SDAMP, SDPHA, GAM43, N43, NSLICE
2.0000E+00 2.0000E-01 0. 0. 9.0000E-02 64 26
FLO, FRQDOP, FQOPRT, ASCFT, I1, I2, I11, I22
1.8000E+01 0. 0. 2.6496E-01 1 1 1 1
SVRNZ, SWMX, SWMN, TL
0. 2.8190E+04 6.2500E+03 -8.0000E+00
CCLOSC, IOLBIT, OYNR
0. 100 3.0000E+00
WN, K, TAU1, TAU2
1.659344E+02 4.866449E+02 4.499999E-01 8.442020E-03
WNB, KB, TAU81, TAU82
9.4261E-01 6.1485E+02 2.0393E+02 1.4945E+00
IBIT, TSYNC
27 1.1364E-02
PE, STDEV, MSSUM, MSSIG, KOUNT
6.3158E-03 1.8174E-03 4.7202E-01 1.9372E-01 2000
LOCKIN 2DROPOUTS=0
ERRM
1.0000E+00 1.0000E+00 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 1.0000E+00 0. 0. 0.
0. 0. 0. 0. 0. 0. 1.0000E+00 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 1.0000E+00 0. 0.
0. 0. 0. 0. 0. 0. 0. 1.0000E+00 0. 6.0000E+00

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1431 1957 408 1137
REC SLICE= 2.5968E+01 2.8701E+00
XXXC, ASUM1, ASUM2, VSUP1, VSUM2, VSUM3,
7.5999E+04 1.9013E+06 5.3991E+07 -1.7817E+06 4.1964E+07 -9.9279E+08
V HISTOGRAM
3.7459E-05 7.4918E-05 2.4973E-05 1.2486E-05 1.2486E-05 2.4973E-05 3.7459E-05 1.2486E-05 1.2486E-05 1.2486E-05
1.2486E-05 2.4973E-05 1.2486E-05 2.4973E-05 1.2486E-05 1.2486E-05 1.2486E-05 2.4973E-05 1.2486E-05 1.2486E-05
1.2486E-05 1.2486E-05 1.2486E-05 1.2486E-05 1.2486E-05 2.4973E-05 1.2486E-05 2.4973E-05 3.7459E-05 4.9949E-05
3.7459E-05 2.4973E-05 1.2486E-05 2.4973E-05 2.4973E-05 2.4973E-05 2.4973E-05 1.2486E-05 2.4973E-05 2.4973E-05
1.2486E-05 1.2486E-05 1.2486E-05 0. 1.2486E-05 1.2486E-05 2.4973E-05 3.7459E-05 1.2486E-05 7.4918E-05
7.4918E-05 7.4918E-05 1.2486E-04 1.6232E-04 9.9890E-05 3.6210E-04 2.7470E-04 3.8707E-04 5.8685E-04 6.9923E-04
6.8674E-04 1.0488E-03 1.2486E-03 1.5982E-03 1.2861E-03 1.9104E-03 2.1227E-03 3.5336E-03 4.1979E-03 4.2828E-03
6.7176E-03 9.1899E-03 1.0801E-02 1.4971E-02 1.8317E-02 2.1252E-02 2.4810E-02 3.2202E-02 3.8732E-02 4.6624E-02
5.5377E-02 5.9722E-02 6.4217E-02 6.9848E-02 6.7838E-02 6.2069E-02 5.8536E-02 5.5214E-02 4.8284E-02 2.8923E-01

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ENODB = 9.4 Pr(v) NO FADE T/28/74N

6L-111A

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NRUNS, NSPE, ENDOB, DELF, BIF, ENOMIN
2000 40 -2.0000E+01 6.2000E+01 1.0000E+03 9.0000E+00
BL2, PHIDEG, FOIFF, BL2P, PHIB, FOIFFB
1.7500E+02 1.0000E+01 3.4243E+02 1.0000E+00 1.0000E+01 5.0000E+00
FBAMP, FBPHA, SDAMP, SDPHA, GAP43, N43, KSLICE
2.0000E+00 2.0000E-01 2.3000E-01 4.7000E-01 9.0000E-02 64 26
FLO, FRQDOP, FOPRT, ASCFT, I1, I2, I11, I22
1.0000E+01 0. 0. 2.6496E-01 1 1 1 1
SVRMZ, SWMX, SWMNI, TL
0. 2.8150E+04 6.8500E+03 -8.0000E+00
CCLOSC, IDLBIT, DYNR
0. 100 3.0000E+00
MN, K, TAU1, TAU2
1.659344E+02 4.686449E+02 4.499999E-01 8.442020E-03
MNB, KB, TAU01, TAU02
9.4281E-01 6.1485E+02 2.0353E+02 1.4945E+00
IBIT, TSYNC
11 1.1364E-02
ACQUISITION FAILURE
▼ HISTOGRAM
9.8989E-02 1.0171E-01 1.0127E-01 9.4058E-02 9.0196E-02 8.2107E-02 7.8609E-02 6.6681E-02 5.9782E-02 4.8802E-02
3.6997E-02 3.2673E-02 2.6964E-02 1.9142E-02 1.5863E-02 1.3263E-02 1.0688E-02 7.3362E-03 4.8827E-03 2.3563E-03
1.9913E-03 1.9434E-03 1.6518E-03 6.8817E-04 5.3442E-04 1.9434E-04 1.2146E-04 7.2876E-05 9.7168E-05 3.4889E-04
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.

```

ENDOB = -20 Pr{v} FADING
T/28/74N

NRUNS, NSPB, ENOCB, DELF, BIF, ENOMIN
 2000 40 6.0000E+00 6.2000E+01 1.0000E+03 9.0000E+00
 BL2, PHIDEG, FDIFF, BL2E, PHIE, FOIFFR
 1.7600E+02 1.0000E+01 3.4243E+02 1.0000E+00 1.0000E+01 5.0000E+00
 FBAMP, FBPHA, SCAMP, SOPHA, GAM43, N43, NSLICE
 2.0000E+00 2.0000E-01 2.3000E-01 4.7000E-01 9.0000E-02 64 26
 FLO, FRQDOP, FQDPR, ASOFT, I1, I2, I11, I22
 1.0000E+01 0. 0. 2.6496E-01 1 1 1 1
 SVRHZ, SWMX, SWMN, TL
 0. 2.8150E+04 6.6500E+03 8.0000E+00
 CCLOSC, IDLBIT, DYNR
 0. 100 3.0000E+00
 WN, K, TAU1, TAU2
 1.659344E+02 4.686449E+02 4.499999E-01 8.442020E-03
 WNB, KB, TAU01, TAU02
 9.4201E-01 6.1405E+02 2.0353E+02 1.4945E+00
 IBIT, TSYNC
 16 1.1364E-02
 PE, STDEV, PSSUM, HSSIG, KCUNT
 8.3158E-02 6.3346E-03 4.3254E-01 2.3406E-01 2000
 LOCKIN 2DROPOUTS 1AVE 7.4000E+01SD 0.

ERRM	5.7000E+01	1.0000E+01	6.0000E+00	9.0000E+00	1.0000E+01	4.0000E+00	2.0000E+00	5.0000E+00	2.0000E+00	2.0000E+00
	2.0000E+00	4.0000E+00	4.0000E+00	0.	2.0000E+00	1.0000E+00	3.0000E+00	2.0000E+00	1.0000E+00	3.0000E+00
	3.0000E+00	2.0000E+00	0.	3.0000E+00	1.0000E+00	0.	1.0000E+00	0.	1.0000E+00	3.0000E+00
	1.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
	1.0000E+00	0.	0.	0.	2.0000E+00	0.	1.0000E+00	0.	0.	0.
	3.0000E+00	0.	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

639 003 934 1229
 REC SLICE= 2.4566E+01 3.9388E+00
 XXXC, ASUM1, ASUM2, VSUM1, VSUM2, VSUM3,
 7.6002E+04 1.9156E+06 5.8732E+07 -1.3133E+06 2.4084E+07 -4.5885E+08

V HISTOGRAM

1.4996E-04	1.4996E-04	1.4996E-04	1.3746E-04	1.2497E-04	2.7492E-04	3.8739E-04	5.1236E-04	7.4979E-04	7.1230E-04
6.8731E-04	1.0747E-03	8.6226E-04	1.1872E-03	9.3724E-04	7.6229E-04	6.7481E-04	6.4982E-04	8.6226E-04	1.5746E-03
1.2122E-03	2.0369E-03	1.6121E-03	1.9745E-03	2.3119E-03	2.2244E-03	1.7120E-03	2.1119E-03	1.7870E-03	1.6745E-03
2.3868E-03	3.0742E-03	3.1241E-03	2.9367E-03	2.3743E-03	2.7243E-03	2.8742E-03	3.1991E-03	3.4116E-03	4.0989E-03
4.6987E-03	5.3485E-03	6.4607E-03	6.6607E-03	8.0228E-03	7.1855E-03	6.4857E-03	6.3732E-03	7.4604E-03	7.7979E-03
8.2227E-03	9.1100E-03	9.8223E-03	9.6224E-03	1.0335E-02	1.0735E-02	1.4971E-02	1.4171E-02	1.5283E-02	1.8520E-02
1.8482E-02	1.8182E-02	2.1094E-02	1.9232E-02	1.9770E-02	2.3469E-02	2.2844E-02	2.2344E-02	2.1981E-02	2.0682E-02
2.3843E-02	2.3731E-02	2.3494E-02	2.2856E-02	2.1944E-02	2.4068E-02	2.5780E-02	2.8017E-02	2.6768E-02	2.6689E-02
2.6243E-02	2.8255E-02	2.7955E-02	2.6430E-02	2.2219E-02	2.0569E-02	1.9382E-02	1.7520E-02	1.4746E-02	1.5571E-02
1.5046E-02	1.3471E-02	1.0972E-02	8.8351E-03	8.3852E-03	6.9231E-03	4.2863E-03	1.7995E-03	1.5371E-03	5.8984E-03

ENOD9= 9.4 , DELF= 62.0 , RIF= 1000 , BL2= 176 , NSLICE= 26 , ASOFT= .3000
 SVRHZ= 0. , SWMX= 2.8150E+04 , SWMN= 6.8500E+03 , FLO= 1.0000E+01 , FRQDOP= 0. , FQOPRT= 1.0800E+01
 TL= -6.50 , DYNR= 0.0 , SDAMP= .230 , SDPHA= .470 , I1,I2,I11,I22 129 130 1 1
 MN= 165.9 , K= 468.6 , TAU1= 4.5000E-01 , TAU2= 8.4420E-03 , WNB= .9 , KB= 614.9 , TAUB1= 2.0353E+02 , TAUB2= 1.4945E+00
 PE= 3.6842E-02 , STDEV= 4.3216E-03 , V MEAN= 4.6193E-01 V STD DEV= 2.0616E-01 , BITS= 1900
 PEI= 3.2632E-02 , STDEV= 4.0760E-03 , I MEAN= 1.6209E+01 I STD DEV= 6.3919E+00 , BITS= 0.
 LOCKIN= 1 , DROPOUTS= 1 , AVE= 2.8000E+01 , STD DEV= 0.

ERRM

3.1000E+01	4.0000E+00	3.0000E+00	2.0000E+00	2.0000E+00	1.0000E+00	0.	0.	0.	0.
1.0000E+00	0.	0.	0.	2.0000E+00	0.	0.	1.0000E+00	0.	0.
2.0000E+00	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	2.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.
1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.
0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.	1.0000E+00	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	8.0000E+00

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 483							
115	24	16	5	0	1	1	0	4	8	2	0	0	0	0	
62	27	23	5	1	0	0	0	1	0	0	1	0	0	0	
41	31	21	13	2	4	1	0	2	0	1	1	0	1	0	
9	10	18	4	1	0	0	0	6	1	0	0	0	0	0	
2	3	2	1	0	0	0	1	8	1	4	1	8	1	0	
2	2	1	0	2	0	0	0	22	8	5	4	0	1	0	
0	0	0	0	0	0	0	0	70	33	17	6	1	0	1	
0	0	0	0	0	0	0	0	163	65	41	19	5	5	1	
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 483							
2	3	3	2	19	57	111	129	2	1	1	1	2	1	0	
1	0	0	3	5	10	27	40	1	1	0	1	0	2	1	
2	1	0	0	1	5	12	17	0	0	0	0	0	1	0	
1	0	0	0	1	4	4	8	0	0	0	0	0	1	1	
0	0	0	0	2	0	1	0	0	0	1	0	2	4	11	
0	0	0	1	0	1	1	3	2	0	1	0	4	14	28	
1	0	0	0	0	1	0	1	1	0	0	0	2	21	51	
0	0	0	1	0	0	1	1	1	2	1	1	3	12	43	

I1,I2,I11,I22 638 1850 529 737
 REC SLICE= 2.6322E+01 , STD DEV= 3.6734E+00
 DYNR = 0 FADE
 2/7/74N

ENDOB= 9.4 ,DELTA= 62.0 ,RIF= 1000 ,BL2= 176 ,NSLICE= 25 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0000E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= .230 ,SDPHA= .470 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 458.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,MNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 2.4737E-02 ,STDEV= 3.5633E-03 ,V MEAN= 4.5633E-01V STD DEV= 2.0590E-01 ,BITS= 1900
 PEI= 2.4737E-02 ,STDEV= 3.5633E-03 ,I MEAN= 1.6204E+01 I STD DEV= 6.2517E+00 ,BITS= 0.
 LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 4.0000E+00 ,STD DEV= 0.
 ERRH

8.0000E+00	3.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	3.0000E+00	1.0000E+00	1.0000E+00	0.
0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
1.0000E+00	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	0.	1.0000E+00	0.	1.0000E+00
0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	3.0000E+00	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.	0.	4.0000E+00

-1,-1 P(B/A)TIMES 453								-1,+1 P(B/A)TIMES 482							
107	35	23	6	1	1	0	0	2	1	0	0	0	0	0	0
76	25	20	5	2	0	0	0	2	0	0	0	0	0	0	0
34	28	20	12	2	0	0	0	0	0	0	1	0	0	0	0
12	13	9	6	4	0	0	0	4	1	0	1	0	0	0	0
4	2	2	2	0	0	0	0	14	3	2	1	0	0	1	0
0	0	0	1	0	0	0	0	30	10	0	6	0	0	1	0
0	0	0	1	0	0	0	0	90	27	6	4	1	0	0	0
0	0	0	0	0	0	0	0	131	64	44	20	3	2	0	2
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 482							
0	1	0	1	24	69	108	130	1	0	0	1	0	2	0	1
0	0	0	3	1	13	23	41	0	0	0	1	1	0	1	0
2	0	1	0	0	7	11	10	0	1	0	0	0	1	0	0
3	1	0	1	3	4	7	3	0	0	0	0	1	2	1	1
0	0	0	0	1	2	0	0	0	0	0	0	0	7	11	10
0	0	0	0	0	1	0	1	1	0	0	2	5	13	34	51
0	0	0	0	0	0	1	0	0	1	2	0	6	19	45	86
0	0	0	0	0	1	1	0	1	1	0	2	7	20	45	98

I1,I2,I11,I22 630 1050 520 737
 REC SLICE= 2.6261E+01 ,STD DEV= 3.5269E+00
 DYNR = 3 FADE
 2/7/74N

ENQDB= 9.4 ,OELF= 62.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0 ,SMMX= 2.8150E+04 ,SMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0 ,FQDPRT= 1.0000E+01
 TL= -6.50 ,DYNR= 6.0 ,SDAMP= .230 ,SOPHA= .470 ,I1,I2,I11,I22 129 130 1 1
 WN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 2.8421E-02 ,STDEV= 3.8123E-03 ,V MEAN= 4.6307E-01V STD DEV= 2.0835E-01 ,BITS= 1900
 DEI= 2.4737E-02 ,STDEV= 3.6633E-03 ,T MEAN= 1.6438E+01 T STD DEV= 6.2763E+00 ,BITS= 0
 LOCKIN= 0 ,DROPOUTS= 1 ,AVE= 8.0000E+00 ,STD DEV= 0.

ERRM

1.4000E+01	3.0000E+00	3.0000E+00	0.	1.0000E+00	1.0000E+00	1.0000E+00	0.	1.0000E+00	0.
3.0000E+00	1.0000E+00	0.	0.	1.0000E+00	0.	2.0000E+00	1.0000E+00	0.	0.
0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.
0.	0.	0.	0.	1.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.	2.0000E+00
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	1.0000E+00	0.
0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	7.0000E+00

-1,-1 P(B/A)TIMES 451									-1,+1 P(B/A)TIMES 482								
93	32	14	5	2	0	2	1	3	1	0	0	0	0	0	0		
74	37	30	4	1	0	1	0	0	0	0	0	0	0	0	1		
35	34	22	10	2	0	0	3	0	1	1	0	0	0	0	0		
11	8	11	6	1	0	0	0	4	3	0	1	0	0	0	0		
2	3	1	1	0	0	0	0	14	3	2	0	0	0	0	0		
1	0	0	0	0	0	0	0	31	16	5	1	1	1	0	1		
0	0	0	2	0	0	0	0	71	36	11	3	0	0	0	1		
0	0	0	1	1	0	0	0	137	72	39	15	3	2	0	2		
+1,-1 P(B/A)TIMES 483									+1,+1 P(B/A)TIMES 484								
1	0	0	4	18	59	111	136	0	0	0	0	2	0	0	0		
0	1	0	1	3	16	24	54	0	0	1	0	1	1	0	0		
2	0	2	0	2	5	10	9	0	0	0	0	2	0	0	0		
0	0	0	1	1	4	2	4	0	0	0	2	1	0	1	2		
0	0	0	0	1	0	2	1	0	0	0	1	0	4	12	7		
0	0	1	0	0	0	0	1	1	1	0	1	1	10	25	41		
0	1	0	0	0	0	0	0	0	0	0	0	4	17	68	101		
1	0	0	1	1	1	1	2	1	1	0	3	6	20	56	90		

I1,I2,I11,I22 1412 890 1522 1225
 REC SLICE= 2.6006E+01 ,STD DEV= 3.7812E+00

DYNR = 6 FADE
 2/7/74N

ENODR= 9.4 ,DEL= 62.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 25 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.0150E+04 ,SWMN= 6.0500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0000E+01
 TL= -6.50 ,DYNR= 0.0 ,SOAMP= 0.000 ,SOPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 WN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 1.0526E-02 ,STDEV= 2.3413E-03 ,V MEAN= 4.7068E-01V STD DEV= 1.9479E-01 ,BITS= 1900
 PEI= 6.3458E-03 ,STDEV= 1.8174E-03 ,I MEAN= 1.6735E+01 I STD DEV= 5.8807E+00 ,BITS= 0.
 LOCKIN= 1 ,DROPOUTS=0
 ERRM

1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	1.0000E+00	2.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.0000E+00

-1,-1 P(B/A)TIMES 451														-1,+1 P(B/A)TIMES 482														
102	26	9	4	0	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
95	30	15	6	3	0	0	0	1	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	30	26	8	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	12	9	2	1	0	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	0	2	2	0	0	0	0	9	3	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	0	35	7	4	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	69	29	9	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	149	86	53	15	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
+1,-1 P(B/A)TIMES 482														+1,+1 P(B/A)TIMES 485														
1	1	0	3	16	60	125	162	0	0	0	0	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	2	11	20	41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	2	4	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	3	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	1	0	1	0	0	0	0	0	0	1	3	7	10	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	1	0	0	0	0	0	0	0	0	0	5	6	31	60	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	1	0	0	0	0	0	0	0	0	0	3	29	52	88	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	1	1	1	1	1	4	25	41	111	0	0	0	0	0	0	0	0	0	0	0

I1,I2,I11,I22 1594 1314 1 1
 REC SLICE= 2.5830E+01 ,STD DEV= 3.5020E+00
 DYNR = 0 NO. FADE
 2/7/74N

EN00B= 9.4 ,DELf= 62.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 25 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SOPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,MNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 8.9474E-03 ,STDEV= 2.1603E-03 ,V MEAN= 4.7353E-01V STD DEV= 1.8772E-01 ,SITS= 1900
 PEI= 5.2632E-03 ,STDEV= 1.6600E-03 ,I MEAN= 1.6677E+01 I STD DEV= 5.7401E+00 ,SITS= 0.
 LOCKIN= 1 ,DROPOUTS=0

ERRM

2.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.0000E+00	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	7.0000E+00

-1,-1 P(B/A)TIMES 455										-1,+1 P(B/A)TIMES 482									
117	32	11	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
73	39	27	4	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
46	29	21	7	1	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0
16	9	4	3	2	0	0	0	0	2	0	0	0	0	0	0	0	0	0	0
3	2	1	1	0	0	0	0	0	5	1	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	46	8	3	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	81	25	11	3	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	148	71	57	16	2	0	0	0	0	0	0
+1,-1 P(B/A)TIMES 482										+1,+1 P(B/A)TIMES 481									
0	1	0	3	20	69	131	149	0	0	0	0	0	0	0	0	0	0	0	0
0	0	1	0	2	10	23	35	0	0	0	0	0	1	0	0	0	0	0	0
0	0	0	0	1	2	8	22	0	0	0	0	0	0	1	0	0	0	0	0
0	0	0	0	0	0	2	1	0	0	0	0	1	0	1	0	1	0	1	0
0	0	0	0	0	1	0	1	0	0	0	0	0	0	4	3	17	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	11	30	36	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	5	20	57	101	0	0	0
0	0	0	0	0	0	0	0	0	0	0	1	1	1	17	49	123	0	0	0

I1,I2,I11,I22 1594 1314 1 1
 REC SLICE= 2.5978E+01 ,STD DEV= 3.3165E+00
 DYNR = 3 NO FADE
 2/7/74N

APPENDIX IX
PARAMETER VARIATION PRINTOUTS

TITLE	PAGE
DELF = 26.4, Fading	IX-2
DELF = 44, "	3
DELF = 88, "	4
DELF = 132, "	5
DELF = 26.4, No Fade	6
DELF = 44, "	7
DELF = 88, "	8
DELF = 132, "	9
B1F = 500, Fading	10
B1F = 750, "	11
B1F = 1500, "	12
B1F = 2000, "	13
B1F = 500, No Fading	14
B1F = 750, "	15
B1F = 1500, "	16
B1F = 2000, "	17
BL2 = 88, Fading	18
BL2 = 100, "	19
BL2 = 164, "	20
BL2 = 188, "	21
BL2 = 88, No Fade	22
BL2 = 100, "	23
BL2 = 164, "	24
BL2 = 188, "	25
TAU4 = 1.8×10^{-3} , Fading	26
TAU4 = 1.1×10^{-3} , "	27
TAU4 = 7.9×10^{-4} , "	28
TAU4 = 1.8×10^{-3} , No Fading	29
TAU4 = 1.1×10^{-3} , "	30
TAU4 = 7.9×10^{-4} , "	31
WORST CASE 1, Fading	32
WORST CASE 2, "	33
WORST CASE 1, No Fading	34
WORST CASE 2, "	35

ENODB= 9.4 ,DELFF= 26.4 ,BIF= 1000 ,BLZ= 176 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= .230 ,SDPHA= .470 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,MNB= .9 ,KB= 1444.8 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 6.9474E-02 ,STDEV= 5.8331E-03 ,V MEAN= 2.1639E-01V STD DEV= 1.2837E-01 ,BITS= 1988
 LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 1.0000E+00 ,STD DEV= 0.

ERRM

2.7000E+01	6.0000E+00	3.0000E+00	9.0000E+00	6.0000E+00	5.0000E+00	5.0000E+00	3.0000E+00	6.0000E+00	8.0000E+00
7.0000E+00	5.0000E+00	1.0000E+00	1.0000E+00	2.0000E+00	6.0000E+00	1.0000E+00	0.	2.0000E+00	0.
2.0000E+00	1.0000E+00	2.0000E+00	3.0000E+00	1.0000E+00	1.0000E+00	0.	0.	2.0000E+00	0.
2.0000E+00	2.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.	1.0000E+00	1.0000E+00	0.
1.0000E+00	0.	1.0000E+00	0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00

-1,-1 P(B/A)TIMES 451

1	3	3	3	1	1	0	0
5	10	25	10	2	0	0	0
9	26	72	53	13	2	0	0
6	38	62	48	10	0	0	0
2	6	17	10	2	1	0	0
0	2	2	2	0	0	0	0
0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	0

+1,-1 P(B/A)TIMES 483

0	0	0	0	18	13	2	6
0	0	0	5	45	53	27	6
0	1	1	10	62	89	37	7
0	1	3	9	23	41	21	4
0	0	0	4	2	8	0	1
0	0	0	1	0	2	0	1
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0

-1,+1 P(B/A)TIMES 483

0	0	0	0	0	0	0	0
0	0	0	1	0	0	0	0
1	0	0	0	0	0	0	0
1	4	8	10	5	0	1	0
4	22	31	32	5	0	0	0
6	48	79	57	11	3	0	0
9	23	54	33	4	3	0	0
6	4	11	6	1	0	0	0

+1,+1 P(B/A)TIMES 483

0	0	0	0	0	0	0	0
0	0	0	1	0	0	0	0
0	0	0	0	1	3	0	0
0	0	0	0	0	9	14	6
0	0	1	9	45	78	37	6
0	0	0	16	43	91	43	7
0	0	0	3	17	30	6	2
0	0	0	1	5	2	5	1

I1,I2,I11,I22 2032 434 1326 493
 REG SLICE= 2.6042E+01 ,STD DEV= 4.6885E+00

DELFF = 26.4 FADING
 2/4/74M

ENODB= 9.4 , DELF= 44.0 , BIF= 1000 , BLZ= 176 , NSLICE= 26 , ASOFT= .3000
 SVRHZ= 0. , SWMX= 2.8150E+04 , SWMN= 6.8500E+03 , FLO= 1.0000E+01 , FRQDOP= 0. , FQOPRT= 1.0800E+01
 TL= -6.50 , DYNR= 3.0 , SDAMP= .230 , SOPHA= .470 , I1, I2, I11, I22 129 130 1 1
 MN= 165.9 , K= 468.6 , TAU1= 4.5000E-01 , TAU2= 8.4420E-03 , WNB= .9 , KB= 866.4 , TAUB1= 2.0363E+02 , TAUB2= 1.4945E+00
 PE= 2.8421E-02 , STDEV= 3.8123E-03 , V MEAN= 3.3653E-01 V STD DEV= 1.6479E-01 , BITS= 1900
 LOCKIN= 1 , DROPOUTS=0

ERRM

7.0000E+00	4.0000E+00	2.0000E+00	2.0000E+00	2.0000E+00	2.0000E+00	0.	1.0000E+00	0.	0.
1.0000E+00	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00
0.	1.0000E+00	2.0000E+00	0.	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	1.0000E+00
1.0000E+00	0.	1.0000E+00	1.0000E+00	0.	1.0000E+00	0.	1.0000E+00	0.	0.
0.	1.0000E+00	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.
1.0000E+00	2.0000E+00	0.	1.0000E+00	1.0000E+00	0.	0.	1.0000E+00	0.	0.
0.	0.	2.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	3.0000E+00

-1,-1 P(B/A)TIMES 453								-1,+1 P(B/A)TIMES 482							
16	20	15	7	1	1	0	0	1	0	0	0	0	0	0	0
37	48	31	10	3	1	0	0	0	0	0	0	0	0	0	0
46	55	48	11	3	1	1	0	0	0	2	0	0	0	0	0
9	24	24	10	4	0	0	0	1	3	1	0	1	0	0	0
2	8	8	3	1	0	0	0	6	18	9	5	0	0	0	0
0	0	1	1	1	0	0	1	36	39	35	14	3	0	0	0
1	0	0	0	0	0	0	0	59	62	39	14	3	1	0	0
0	0	0	0	0	0	0	0	28	35	42	19	6	0	0	0
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 482							
0	0	0	4	23	78	43	34	1	0	0	0	0	0	0	0
0	0	0	6	25	53	65	34	0	0	0	0	0	0	0	0
1	0	0	0	13	33	28	15	0	0	0	0	0	0	0	0
0	0	1	0	3	5	8	6	0	0	0	0	1	2	7	2
0	0	0	0	2	1	0	1	0	0	0	4	9	29	22	22
0	0	0	0	0	0	0	0	0	0	0	1	24	47	63	32
0	0	0	0	0	0	0	0	0	0	0	2	13	28	50	40
0	0	0	1	0	0	0	0	0	0	1	1	10	19	25	27

I1, I2, I11, I22 1594 1314 529 737
 REG SLICE= 2.6237E+01 , STD DEV= 3.7963E+00
 DELF = 44 FADING
 2/4/74M

EN0DB= 9.4 ,DEL= 88.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= .230 ,SDPHA= .470 ,I1,I2,I11,I22 129 130 1 1
 WN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,RB= 433.2 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 8.4737E-02 ,STDEV= 6.3890E-03 ,V MEAN= 5.8023E-01V STD DEV= 3.0239E-01 ,BITS= 1900
 LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 3.0000E+01 ,STD DEV= 0.

ERRM

4.6000E+01	1.1000E+01	6.0000E+00	1.1000E+01	1.0000E+01	6.0000E+00	3.0000E+00	6.0000E+00	4.0000E+00	5.0000E+00
2.0000E+00	3.0000E+00	1.0000E+00	2.0000E+00	2.0000E+00	5.0000E+00	2.0000E+00	0.	4.0000E+00	3.0000E+00
1.0000E+00	1.0000E+00	2.0000E+00	3.0000E+00	0.	0.	0.	2.0000E+00	0.	3.0000E+00
1.0000E+00	2.0000E+00	1.0000E+00	0.	1.0000E+00	2.0000E+00	0.	0.	1.0000E+00	2.0000E+00
1.0000E+00	1.0000E+00	0.	1.0000E+00	1.0000E+00	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

-1,-1 P(B/A)TIMES

451

161	22	19	10	4	3	0	6
45	17	15	7	2	3	0	0
25	12	23	11	3	1	0	1
14	12	7	5	4	1	0	1
2	3	3	3	0	0	0	0
0	1	0	1	0	0	0	0
0	0	1	0	0	0	0	0
0	1	0	1	0	0	0	1

-1,+1 P(B/A)TIMES

483

22	0	3	2	0	0	0	0
3	4	3	1	1	0	0	0
9	2	1	0	1	0	0	0
5	5	2	0	0	0	1	0
16	2	3	1	0	0	0	0
26	6	2	6	1	0	0	1
41	8	9	3	2	1	0	1
193	34	25	15	7	1	1	5

+1,-1 P(B/A)TIMES

483

10	4	7	6	11	34	55	210
3	0	4	1	4	5	7	24
7	4	1	0	3	4	4	17
2	0	1	2	1	1	3	12
0	0	1	1	1	0	1	10
1	0	0	0	0	0	2	5
0	0	0	0	0	0	0	1
1	0	0	0	1	1	2	8

+1,+1 P(B/A)TIMES

483

6	0	1	1	1	2	1	4
0	0	0	0	0	1	1	1
5	2	1	0	0	0	0	0
3	1	1	0	0	0	1	2
3	1	0	1	2	1	2	9
0	0	0	0	3	3	5	21
0	0	1	3	3	5	12	41
10	3	3	6	11	16	34	249

I1,I2,I11,I22 638 1850 529 737

REC SLICE= 2.7043E+01 ,STD DEV= 4.0306E+00

DEL= 88 FADING
 2/4/74M

ENOD8= 9.4 , DELF= 132.0 , BIF= 1000 , BL2= 176 , NSLICE= 26 , ASOFT= .3000
 SVRHZ= 0. , SWMX= 2.8150E+04 , SWMN= 6.8500E+03 , FLO= 1.0000E+01 , FRQDOP= 0. , FQDPRT= 1.0000E+01
 TL= -6.50 , DYNR= 3.0 , SDAMP= .230 , SDPHA= .470 , I1,I2,I11,I22 129 130 1 1
 WN= 165.9 , K= 468.6 , TAU1= 4.5000E-01 , TAU2= 8.4420E-03 , WNB= .9 , KB= 288.8 , TAUB1= 2.0353E+02 , TAUB2= 1.4945E+00
 PE= 3.0709E-01 , STDEV= 1.0590E-02 , V MEAN= 6.4424E-01V STD DEV= 4.1994E-01 , BITS= 1900
 LOCKIN= 1 , DROPOUTS= 1 , AVE= 2.5900E+02 , STD DEV= 0.

ERRM

2.9100E+02	8.7000E+01	5.2000E+01	5.0000E+01	5.2000E+01	1.0000E+01	9.0000E+00	9.0000E+00	6.0000E+00	5.0000E+00
2.0000E+00	2.0000E+00	1.0000E+00	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 484							
147	28	13	10	13	5	6	18	81	12	13	6	4	1	1	8
41	12	10	2	1	1	1	2	9	4	7	3	0	3	2	4
19	13	6	9	4	0	1	5	15	5	3	3	5	0	1	2
8	3	9	2	2	0	1	4	9	3	5	3	1	2	0	3
5	2	2	1	1	2	4	2	5	2	4	3	3	1	0	5
3	0	0	1	1	0	0	4	13	4	4	0	2	4	1	3
4	0	1	2	0	1	0	2	9	5	2	3	5	2	1	12
5	0	0	0	0	3	2	7	65	10	11	4	6	14	12	51
+1,-1 P(B/A)TIMES 481								+1,+1 P(B/A)TIMES 484							
48	11	20	10	10	6	15	75	20	3	5	0	3	3	1	4
8	4	3	0	2	1	2	13	5	2	1	2	2	4	1	1
3	1	3	2	1	7	3	13	15	2	6	3	2	1	2	4
6	2	2	1	1	3	1	7	7	1	2	2	2	2	5	2
8	1	2	1	3	0	3	11	7	1	2	3	2	1	0	10
5	2	1	2	0	1	5	14	3	2	3	5	1	2	3	9
1	0	3	2	2	0	0	15	3	3	0	1	2	4	6	20
8	5	1	5	3	6	11	76	16	10	15	10	13	18	20	174

I1,I2,I11,I22 1054 242 529 737
 REC SLICE= 2.7268E+01 , STD DEV= 9.8678E+00

DELF = 132 FADING
 2/4/74M

9-XI

ENDD= 9.4 ,DELF= 26.4 ,BIF= 1000 ,BL2= 176 ,NSLICE= 25 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SDPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.0 ,K= 488.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 1444.0 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 6.0526E-02 ,STDEV= 5.4706E-03 ,V MEAN= 2.1416E-01V STD DEV= 1.2434E-01 ,BITS= 1900
 REI= 7.8947E-03 ,STDEV= 2.0303E-03
 LOCKIN= 1 ,DROPOUTS= 0

ERRM

1.7000E+01	4.0000E+00	2.0000E+00	8.0000E+00	8.0000E+00	4.0000E+00	3.0000E+00	4.0000E+00	3.0000E+00	4.0000E+00
0.0000E+00	2.0000E+00	1.0000E+00	3.0000E+00	2.0000E+00	5.0000E+00	1.0000E+00	0.0000E+00	1.0000E+00	2.0000E+00
0.0000E+00	1.0000E+00	2.0000E+00	2.0000E+00	0.0000E+00	3.0000E+00	2.0000E+00	0.0000E+00	2.0000E+00	0.0000E+00
1.0000E+00	2.0000E+00	0.0000E+00	4.0000E+00	0.0000E+00	1.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	1.0000E+00
2.0000E+00	0.0000E+00	1.0000E+00	2.0000E+00	0.0000E+00	2.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
0.0000E+00	2.0000E+00	0.0000E+00	1.0000E+00	0.0000E+00	0.0000E+00	1.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00

-1,-1 P(B/A)TIMES 451

0	1	2	0	0	0	0	0
7	13	21	21	1	0	0	0
5	33	65	45	11	4	0	0
5	41	66	48	9	1	0	0
2	6	11	19	4	1	0	0
0	3	4	2	0	0	0	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0

+1,-1 P(B/A)TIMES 483

0	0	0	1	14	16	5	1
0	0	0	9	37	48	25	2
0	0	0	8	56	98	44	4
0	0	1	4	29	33	31	3
0	0	0	2	6	4	1	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0

-1,+1 P(B/A)TIMES 483

0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	0	0	1	0	0	0	0
1	1	5	8	4	0	0	0
3	26	45	28	4	1	0	0
10	33	81	57	13	1	0	0
7	24	61	37	6	1	0	0
1	3	11	5	4	0	0	0

+1,+1 P(B/A)TIMES 483

0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	0	0	0	0	1	0	0
0	0	0	2	6	12	7	1
0	0	0	5	42	71	35	9
0	0	1	14	52	93	41	8
0	0	0	3	25	25	18	3
0	0	0	0	2	3	3	1

I1,I2,I11,I22 1609 450 1 1
 REC SLICE= 2.6199E+01 ,STD DEV= 4.4629E+00

DELF = 26.4 NO FADING
 2/5/74E

ENODR= 9.4 ,DELTA= 44.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 26 ,ASOFT= .3000
 SVRMZ= 0. ,SMMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0000E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SDPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 WN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 866.4 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 2.3604E-02 ,STDEV= 3.4886E-03 ,V MEAN= 3.4551E-01V STD DEV= 1.5815E-01 ,BITS= 1900
 PEI= 1.5789E-03 ,STDEV= 9.1089E-04
 LOCKIN= 1 ,DROPOUTS=0

ERRM

4.0000E+00	2.0000E+00	0.	0.	1.0000E+00	0.	2.0000E+00	3.0000E+00	1.0000E+00	0.
1.0000E+00	0.	3.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.	1.0000E+00
0.	1.0000E+00	0.	1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.
0.	1.0000E+00	0.	0.	1.0000E+00	0.	2.0000E+00	0.	1.0000E+00	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
1.0000E+00	0.	0.	0.	0.	2.0000E+00	2.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	1.0000E+00	0.	0.	0.	1.0000E+00	5.0000E+00

-1,-1 P(B/A)TIMES 452

23	18	13	3	0	0	0	0
52	48	28	6	5	1	0	0
36	52	38	17	8	0	0	0
18	23	24	10	1	0	0	0
3	7	9	5	0	0	0	0
0	2	1	1	0	0	0	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0

-1,+1 P(B/A)TIMES 483

0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
1	1	0	0	0	0	0	0
15	7	4	1	1	0	0	0
25	52	23	4	2	0	0	0
50	77	45	17	5	3	0	0
29	44	49	21	6	0	0	0

+1,-1 P(B/A)TIMES 483

0	0	1	5	28	75	57	29
0	0	0	3	19	59	72	38
0	0	0	1	11	23	38	11
0	0	0	0	1	1	4	3
0	0	0	0	0	3	0	1
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0

+1,+1 P(B/A)TIMES 482

0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	3
0	0	0	0	0	0	7	16
0	0	0	0	0	0	2	12
0	0	0	0	0	0	13	52
0	0	0	0	0	0	1	39
0	0	0	0	0	0	5	8
0	0	0	0	0	0	0	22
0	0	0	0	0	0	0	33

I1,I2,I11,I22 1050 778 1 1
 REC SLICE= 2.5927E+01 ,STD DEV= 4.2009E+00
 DELTA = 44 NO FADING
 2/5/74E

ENODB= 9.4 ,DELTA= 88.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SDPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 433.2 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 6.2105E-02 ,STDEV= 5.5369E-03 ,V MEAN= 5.9443E-01V STD DEV= 2.8558E-01 ,BITS= 1900
 PEI= 7.3684E-02 ,STDEV= 5.9936E-03
 LOCKIN= 2 ,DROFOUTS= 1 ,AVE= 6.0000E+00 ,STD DEV= 0.

ERRM

1.4000E+01	4.0000E+00	9.0000E+00	5.0000E+00	6.0000E+00	5.0000E+00	5.0000E+00	2.0000E+00	5.0000E+00	5.0000E+00
4.0000E+00	4.0000E+00	4.0000E+00	2.0000E+00	1.0000E+00	5.0000E+00	1.0000E+00	0.	1.0000E+00	2.0000E+00
1.0000E+00	3.0000E+00	2.0000E+00	1.0000E+00	4.0000E+00	5.0000E+00	1.0000E+00	0.	2.0000E+00	1.0000E+00
0.	3.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
1.0000E+00	0.	2.0000E+00	2.0000E+00	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

-1,-1 P(B/A)TIMES 451									-1,+1 P(B/A)TIMES 483								
170	24	15	7	0	1	3	4	31	1	1	0	0	0	0	0	0	0
61	24	19	7	0	1	1	1	3	2	3	0	0	0	0	0	0	0
29	19	11	8	0	2	1	0	5	2	2	0	0	0	0	0	0	0
11	9	7	3	0	0	0	0	11	5	0	1	0	0	0	0	0	0
1	0	1	0	0	0	0	0	10	2	3	0	0	0	3	0	0	0
0	2	1	0	0	0	0	0	17	12	2	2	0	0	0	2	2	2
2	2	0	0	0	0	0	0	37	10	7	0	0	1	0	2	2	2
3	1	0	1	0	0	0	0	204	45	32	13	3	2	3	6	6	6
+1,-1 P(B/A)TIMES 483									+1,+1 P(B/A)TIMES 483								
12	1	1	10	15	30	63	238	3	0	0	0	0	1	1	2	2	
5	2	0	0	0	6	8	25	0	0	0	0	0	0	0	3	3	
8	0	2	1	1	3	3	13	1	0	0	0	0	0	0	0	0	
1	2	0	0	0	0	1	8	0	0	0	0	0	0	2	2	2	
1	0	0	3	0	1	0	1	0	0	0	1	0	0	2	11	11	
0	0	0	0	0	0	1	3	0	1	0	0	2	3	7	18	18	
0	0	0	0	1	2	3	1	0	0	0	0	4	4	13	65	65	
0	0	0	0	1	1	1	7	9	2	8	9	8	16	38	247	247	

I1,I2,I11,I22 1748 1738 1 1
 REC SLICE= 2.6151E+01 ,STD DEV= 3.8503E+00
 DELTA = 88. NO FADING
 2/5/74E

ENODB= 9.4 ,DELTA= 132.0 ,BIF= 1000 ,BL2= 175 ,NSLICE= 25 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0000E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SOPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 HN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 288.8 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 2.7789E-01 ,STDEV= 1.0277E-02 ,V MEAN= 6.7795E-01V STD DEV= 4.2504E-01 ,BITS= 1900
 PEI= 2.3368E-01 ,STDEV= 9.7083E-03
 LOCKIN= 2 ,DROPOUTS= 1 ,AVE= 1.5000E+02 ,STD DEV= 0.
 ERRM

2.2300E+02	8.2000E+01	7.4000E+01	3.7000E+01	5.2000E+01	2.3000E+01	1.1000E+01	3.0000E+00	4.0000E+00	8.0000E+00
7.0000E+00	2.0000E+00	2.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

-1,-1 P(B/A)TIMES 450

171	20	9	5	9	9	6	21
27	30	13	8	3	0	1	1
14	11	10	4	0	2	2	3
9	6	6	2	1	0	0	2
2	1	0	2	2	1	1	5
1	1	1	0	1	0	1	4
4	0	0	0	1	1	0	3
3	0	1	0	0	1	1	7

+1,-1 P(B/A)TIMES 492

44	7	12	13	16	18	10	82
7	1	3	0	4	1	2	17
4	2	2	0	1	0	3	11
1	1	3	2	1	1	0	15
4	0	0	1	0	2	4	10
4	1	1	0	0	4	4	17
0	1	1	1	0	7	4	19
2	0	1	2	0	3	11	94

-1,+1 P(B/A)TIMES 483

90	11	6	7	1	0	2	1
9	10	1	2	3	1	0	0
13	2	7	1	0	2	1	1
12	3	1	1	0	1	2	4
11	6	1	0	1	2	2	4
11	1	2	2	1	6	3	5
11	1	0	0	2	5	5	7
64	15	11	17	10	9	15	58

+1,+1 P(B/A)TIMES 485

20	7	4	3	3	1	0	1
4	0	0	1	0	4	1	1
7	0	3	3	0	1	1	4
8	0	2	1	3	1	1	5
8	5	0	0	2	1	2	3
9	2	3	2	3	5	3	12
5	6	2	3	1	3	5	20
29	4	9	13	14	18	25	178

I1,I2,I11,I22 1685 226 1 1
 REC SLICE= 2.7370E+01 ,STD DEV= 7.1083E+00

DELTA = 132 NO FADING
 2/5/74E

01-XI

EN000= 9.4 , DELF= 62.0 , BIF= 500 , BL2= 176 , NSLICE= 24 , ASOFT= .3800
 SVRHZ= 0. , SWMX= 2.8150E+04 , SWMN= 6.8500E+03 , FLO= 1.0000E+01 , FRQDOP= 0. , FQDPRT= 1.0800E+01
 TL= 6.50 , DYNR= 3.0 , SDAMP= .230 , SDPHA= .470 , I1, I2, I11, I22 129 130 1 1
 MN= 165.9 , K= 468.6 , TAU1= 4.5000E-01 , TAU2= 8.4420E-03 , WNB= .9 , KB= 614.9 , TAUB1= 2.0353E+02 , TAUB2= 1.4945E+00
 PE= 5.5789E-02 , STDEV= 5.2654E-03 , V MEAN= 4.7524E-01V STD DEV= 2.4526E-01 , BITS= 1900
 PEI= 3.6316E-02 , STDEV= 4.2918E-03
 LOCKIN= 1 , DROPDUTS= 1 , AVE= 2.1000E+01 , STD DEV= 0.

ERRM									
3.6000E+01	1.1000E+01	3.0000E+00	0.	1.0000E+00	2.0000E+00	3.0000E+00	1.0000E+00	3.0000E+00	0.
2.0000E+00	2.0000E+00	1.0000E+00	2.0000E+00	1.0000E+00	2.0000E+00	2.0000E+00	0.	1.0000E+00	0.
1.0000E+00	0.	3.0000E+00	2.0000E+00	3.0000E+00	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00
2.0000E+00	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	1.0000E+00	1.0000E+00
1.0000E+00	1.0000E+00	0.	2.0000E+00	0.	0.	1.0000E+00	0.	2.0000E+00	0.
0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	2.0000E+00

-1,-1 P(B/A)TIMES 451										-1,+1 P(B/A)TIMES 483									
88	27	18	3	3	2	0	1	7	0	0	0	0	1	0	0	0			
74	21	14	11	3	0	0	0	1	1	0	0	0	0	0	0	0			
38	24	22	15	6	0	3	0	2	0	2	0	1	0	0	0	0			
23	9	18	4	0	0	0	0	6	2	3	0	2	0	0	0	1			
5	4	7	0	0	0	1	1	5	1	2	2	0	0	0	0	0			
2	0	0	0	0	0	0	0	25	5	4	5	1	0	0	0	0			
1	1	0	0	1	0	1	0	55	25	10	3	2	1	0	0	0			
0	0	0	0	0	0	0	0	159	63	45	24	9	5	1	1	1			

+1,-1 P(B/A)TIMES 483										+1,+1 P(B/A)TIMES 483									
3	2	6	14	25	49	96	155	3	2	0	1	1	1	0	0	0			
1	0	0	1	1	11	16	30	1	0	0	2	0	0	0	1	1			
2	0	0	0	3	5	11	16	0	0	0	0	1	0	0	0	1			
1	0	0	1	0	3	4	4	0	0	1	0	2	2	2	9	9			
1	0	0	0	1	4	3	1	1	0	0	1	1	4	12	20	20			
1	0	0	2	0	0	3	1	0	0	0	1	4	12	30	33	33			
0	0	0	0	1	0	0	1	1	1	0	4	6	13	40	95	95			
0	0	0	0	1	0	1	2	1	1	0	3	3	16	38	112	112			

I1, I2, I11, I22 371 874 1326 493
 REC SLICE= 2.3894E+01 , STD DEV= 5.2927E+00
 BIF = 500 FADING
 4/5/74M

EN000* ---9.4, DELF= -62.0, BIF= ---750, BL2= ---176, NSLICE= ---25, ASOFT= ---3000
 SVRHZ= 0., SWMX= 2.8150E+04, SKMN= 6.8500E+03, FLO= 1.0000E+01, FRQDOP= 0., FQDPR= 1.0800E+01
 TL= -6.50, DYNR= 3.0, SBAMP= ---.230, SDFHA= -470, I1, I2, I11, I22 129 136 1 1
 MN= 165.9, K= 468.6, TAU1= 4.5000E-01, TAU2= 8.4420E-03, WNB= .9, KB= 614.9, TAUB1= 2.0353E+02, TAUB2= 1.4945E+00
 PE= 3.2632E-02, STDEV= 4.0760E-02, V MEAN= 4.6091E-01, STD DEV= 2.1695E-01, BITS= 1900
 PEI= 2.7895E-02, STDEV= 3.7778E-03
 LOCKIN= 1, DRFOUITS= 1, AVE= 1.3000E+01, STD DEV= 0.
 ERRM

1.6000E+01	3.0000E+00	3.0000E+00	2.0000E+00	2.0000E+00	1.0000E+00	2.0000E+00	2.0000E+00	1.0000E+00	0.
1.0000E+00	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	2.0000E+00	2.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	0.	0.	2.0000E+00	0.	0.	1.0000E+00	0.	0.	0.
0.	0.	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	2.0000E+00	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	1.0000E+00	1.0000E+00	1.0000E+00	0.
0.	1.0000E+00	0.	0.	1.0000E+00	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	6.0000E+00

-1,-1 F(A/A)TIMES 451					-1,+1 P(B/A)TIMES 483				
92	41	18	7	0	0	0	1	0	0
71	26	21	9	3	1	1	1	0	0
41	27	17	6	2	0	0	2	1	0
13	12	8	6	1	0	0	1	3	1
8	2	4	2	2	0	0	12	1	2
2	0	0	0	0	0	0	36	13	7
0	1	0	0	0	0	0	67	28	9
0	1	1	1	0	0	0	154	64	37

+1,-1 F(A/A)TIMES 483					+1,+1 P(B/A)TIMES 483				
0	3	1	4	21	53	116	144	2	1
2	0	0	1	1	15	28	40	0	0
1	1	1	0	2	5	4	18	0	0
0	0	0	0	2	5	5	1	1	0
0	0	0	0	0	0	1	3	0	0
0	0	0	0	0	0	0	2	1	0
0	0	0	0	0	0	0	1	0	0
0	0	0	0	1	0	0	0	3	1

I1, I2, I11, I22 231 338 529 737
 REG SLICE= 2.5239E+01, STD DEV= 4.1892E+00
 BIF = 750 FADING
 4/5/74M

IX-12

ENODB= 9.4 ,DELTA= 62.0 ,BIF= 1500 ,RL2= 176 ,NSLICE= 40 ,ASOFT= .3000
 SVRHZ= 0. ,SNMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= .230 ,SDPHA= .470 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 2.5263E-02 ,STDEV= 3.6001E-03 ,V MEAN= 4.5685E-01V STD DEV= 1.9627E-01 ,BITS= 1900
 PEI= 1.5789E-02 ,STDEV= 2.8599E-03
 LOCKIN= 1 ,DROPOPTS= 1 ,AVE= 3.0000E+00 ,STD DEV= 0.

ERRM

1.1000E+01	5.0000E+00	1.0000E+00	1.0000E+00	3.0000E+00	1.0000E+00	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	1.0000E+00	0.	2.0000E+00	1.0000E+00
1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.	3.0000E+00	1.0000E+00	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.
0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	1.0000E+00	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	6.0000E+00

-1,-1 P(B/A)TIMES 450										-1,+1 P(B/A)TIMES 483									
111	38	18	5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
61	42	20	6	3	0	1	0	0	0	1	0	0	0	0	0	0	0	0	0
43	33	16	7	0	1	0	0	0	0	2	1	0	0	0	0	0	0	0	0
10	9	8	3	0	0	0	0	0	0	5	3	1	1	1	0	0	0	0	0
2	2	1	1	0	1	0	0	0	0	11	5	6	0	0	0	0	0	0	0
0	2	0	2	0	1	0	0	0	0	25	12	6	1	2	0	1	0	0	0
0	0	1	0	0	0	0	0	0	0	82	30	8	5	1	1	0	0	0	0
0	0	0	0	0	0	0	0	0	0	139	63	52	11	5	1	1	0	0	0
+1,-1 P(B/A)TIMES 482										+1,+1 P(B/A)TIMES 485									
2	0	2	5	11	50	97	151	0	0	0	0	0	1	0	1	2	0	0	0
1	0	0	2	7	18	27	51	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	2	4	3	5	23	0	0	0	0	0	0	0	0	2	0	0	0
0	0	1	0	1	5	3	2	0	0	0	0	0	0	3	1	1	0	0	0
0	0	0	0	0	3	3	1	0	0	0	0	1	1	1	1	4	7	0	0
0	0	0	0	0	0	0	0	0	0	0	1	1	0	3	15	34	36	0	0
0	0	0	1	0	1	0	0	0	0	0	0	0	2	1	21	55	82	0	0
0	0	0	0	0	0	0	0	0	0	1	0	0	2	6	18	64	127	0	0

I1,I2,I11,I22 1122 1858 1930 1993
 REC SLICE= 3.9812E+01 ,STD DEV= 4.4721E+00
 BIF = 1500 FADING
 4/5/74M

- EN00B= 9.4 ,DEL= 62.0 ,RIF= 2000 ,BL2= 176 ,NSLICE= 54 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,S+MN= 5.8540E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0800E+01
 - TL= -6.50 ,DYNR= 3.0 ,SDAMP= .230 ,SDFHA= .470 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 458.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 2.1053E+02 ,STDEV= 3.2935E-03 ,V. MEAN= 4.5533E-01V ,STD DEV= 1.9202E-01 ,BITS= 1900
 PEI= 2.3158E-02 ,STDEV= 3.4505E-03
 - LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 6.0000E+00 ,STD DEV= 0.

ERRM

1.0000E+01	1.0000E+00	3.0000E+01	1.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00
0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	1.0000E+00	0.
0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1.0000E+00	0.	1.0000E+00	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	7.0000E+00

-1,-1 P(B/A)TIMES 453								-1,+1 P(B/A)TIMES 482							
112	40	5	8	1	0	0	0	2	0	0	0	0	0	0	
72	45	17	9	0	0	0	0	2	0	0	0	0	0	0	
33	25	24	7	3	0	0	0	3	1	1	2	0	0	0	
7	13	11	9	0	2	0	0	1	1	1	1	0	0	0	
1	4	2	0	0	0	0	0	11	2	3	0	0	1	0	
1	0	0	1	0	0	0	0	39	9	5	0	0	0	0	
0	1	0	0	0	0	0	0	73	41	14	2	1	0	0	
0	0	0	0	0	0	0	0	125	74	45	16	4	1	1	
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 482							
2	0	2	2	9	58	112	132	3	0	2	0	0	2	1	
1	1	1	0	7	16	39	48	0	0	0	0	0	0	0	
0	0	1	1	3	4	11	16	0	0	1	0	0	0	0	
1	0	0	0	1	1	2	8	0	0	0	0	1	0	1	
0	0	0	1	0	0	1	0	0	0	1	0	2	3	4	
0	0	0	0	1	0	0	-1	0	0	0	0	5	15	30	
0	0	0	0	0	0	0	0	0	1	0	1	6	20	57	
0	0	0	0	0	0	0	0	3	0	0	1	4	28	42	

I1,I2,I11,I22 564 450 529 737
 - REC SLICE= 5.4213E+01 ,STD DEV= 5.5437E+00
 BIF = 2000 FADING
 4/5/74M NSPB = 80

IX-14

ENOD9= 9.4 ,DELf= 62.0 ,BIF= 500 ,BL2= 176 ,NSLICE= 2+ ,ASOFT= .3000
 SVRHZ= 0. ,SMMX= 2.8150E+04 ,SMMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0000E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SOPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-13 ,MNS= .9 ,K0= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 1.5263E-02 ,STDEV= 2.6126E-03 ,V MEAN= 4.7884E-01V STD DEV= 2.2147E-01 ,BITS= 1900
 PEI= 1.6526E-02 ,STDEV= 2.3413E-03
 LOCKIN= 1 ,DROPOUTS=0
 ERRM

1.0000E+00	2.0000E+00	0.	1.0000E+00	1.0000E+00	0.	1.0000E+00	0.	1.0000E+00	0.
0.	0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00
0.	1.0000E+00	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	1.0000E+00	0.	2.0000E+00	0.	0.	1.0000E+00	0.	6.0000E+00

-1,-1 P(B/A)TIMES 455

90	25	7	3	2	0	1	0
86	32	19	13	2	0	0	0
51	28	19	11	2	0	0	0
14	19	15	4	1	1	0	0
1	2	3	2	0	0	0	0
0	0	0	1	0	0	0	0
1	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0

+1,-1 P(B/A)TIMES 482

0	0	0	6	31	65	101	178
0	0	0	1	2	12	21	38
0	1	0	0	3	4	3	6
0	0	0	0	1	1	2	2
0	0	0	0	0	1	0	1
0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	0
0	0	0	0	1	0	0	0

-1,+1 P(B/A)TIMES 482

0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	1	0	0	0	0	0	0
5	0	0	0	0	0	0	0
10	4	1	0	0	0	0	0
23	7	2	1	0	0	0	1
67	25	9	4	0	1	0	0
161	83	53	21	3	0	0	0

+1,+1 P(B/A)TIMES 481

0	0	0	0	1	0	1	0
0	0	0	1	0	0	0	1
0	0	0	0	0	0	0	0
0	0	0	0	0	1	0	4
0	0	0	2	0	7	5	23
0	0	0	0	5	17	21	65
0	0	0	0	4	12	45	76
2	1	1	0	4	22	44	116

I1,I2,I11,I22 371 874 1 1
 REC SLICE= 2.3501E+01 ,STD DEV= 5.4618E+00

BIF = 500 NO FADING
 2/5/74A

ENDB= 9.4 ,DEL= 62.0 ,BIF= 750 ,BL2= 176 ,NSLICE= 25 ,ASOFT= .3000
 SVRHZ= 0. ,SWX= 2.8150E+04 ,SWN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDP= 0. ,FQDPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SDPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,XB= 511.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4946E+00
 PE= 1.2632E-02 ,STDEV= 2.5621E-03 ,V MEAN= 4.6825E-01V STD DEV= 1.9377E-01 ,BITS= 1900
 PEI= 7.8947E-03 ,STDEV= 2.0303E-03
 LOCKIN= 1 ,DROPOUTS=0
 ERM

2.0000E+00	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	9.0000E+00

-1,-1 P(B/A)TIMES 451										-1,+1 P(B/A)TIMES 483						
104	30	11	3	1	0	1	1	1	1	0	0	0	0	0	0	0
81	28	18	6	2	0	0	0	0	0	0	0	0	0	0	0	0
39	29	29	11	3	0	0	0	0	0	0	0	0	0	0	0	0
16	13	7	6	1	0	0	0	0	1	1	0	0	0	0	0	0
5	1	3	1	0	0	0	0	0	7	2	2	0	0	0	0	0
0	0	0	0	0	0	0	0	0	36	10	5	1	0	0	0	0
0	0	0	0	0	0	0	0	0	63	28	12	7	3	0	0	1
0	0	1	0	0	0	0	0	0	167	73	40	13	1	0	0	0
+1,-1 P(B/A)TIMES 483										+1,+1 P(B/A)TIMES 483						
0	0	1	0	15	71	123	159	0	0	0	1	0	0	0	0	0
0	0	0	1	2	11	24	42	0	0	0	0	1	0	0	0	0
0	0	1	0	2	5	4	14	0	0	0	1	0	0	1	0	0
0	1	0	0	0	2	1	1	0	0	0	0	0	0	0	0	3
0	0	0	0	0	1	8	0	0	0	0	0	0	5	7	7	7
0	0	0	0	0	0	0	0	1	0	0	1	0	16	28	52	52
0	0	0	0	1	0	0	0	0	0	0	0	3	20	47	102	102
0	0	0	0	1	0	0	0	1	0	0	1	5	19	52	109	109

I1,I2,I11,I22 638 1850 1 1
 REC SLICE= 2.5109E+01 ,STD DEV= 4.1300E+00
 BIF = 750
 2/6/74A
 NO FADING
 NSPB = 40

ENODB= 9.4 ,DELTA= 62.0 ,BIF= 1500 ,BL2= 176 ,NSLICE= 40 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0000E+01
 TL= -6.50 ,DYNR= 3.0 ,SOAMP= 0.000 ,SDPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-13 ,WNB= .9 ,KB= 614.9 ,TAU01= 2.0353E+02 ,TAU02= 1.4945E+00
 PE= 5.2632E-03 ,STDEV= 1.6600E-03 ,V MEAN= 4.6625E-01V STD DEV= 1.8393E-01 ,BITS= 1900
 PEI= 3.1579E-03 ,STDEV= 1.2872E-03
 LOCKIN= 1 ,DROPOUTS=0

ERRM

0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	6.0000E+00

-1,-1 P(B/A)TIMES 450								-1,+1 P(B/A)TIMES 483							
130	27	15	0	0	0	0	0	1	0	0	0	0	0	0	0
68	42	20	0	1	0	0	0	0	0	0	0	0	0	0	0
39	29	17	9	2	0	0	0	0	0	0	0	0	0	0	0
14	14	8	1	0	0	0	0	1	0	0	0	0	0	0	0
1	1	2	1	0	0	0	0	10	1	0	0	0	0	0	0
0	1	0	0	0	0	0	0	35	16	4	1	0	0	0	0
0	0	0	0	0	0	0	0	96	27	15	7	0	0	0	0
0	0	0	0	0	0	0	0	135	60	43	17	4	1	0	0
+1,-1 P(B/A)TIMES 482								+1,+1 P(B/A)TIMES 485							
0	0	0	0	11	58	120	170	0	0	0	0	0	0	0	0
0	0	0	0	6	17	29	35	0	0	0	0	0	0	0	0
0	0	0	0	1	6	9	11	0	0	0	0	0	0	0	0
0	0	0	0	0	0	5	2	0	0	0	0	0	0	0	0
0	0	0	0	0	2	0	0	0	0	0	0	0	0	3	4
0	0	0	0	0	0	0	0	0	0	0	0	0	0	21	34
0	0	0	0	0	0	0	0	1	0	0	0	0	6	20	55
0	0	0	0	0	0	0	0	0	0	0	1	4	22	56	124

I1,I2,I11,I22 1391 802 1 1
 REC SLICE= 3.9769E+01 ,STD DEV= 4.1080E+00
 BIF = 1500 NO FADING
 2/6/74A NSPB = 60

EN009= 9.4 ,DELTA= 62.0 ,BIF= 2000 ,BL2= 176 ,NSLICE= 54 ,ASOFT= .3000
 SVRHZ= 0 ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQOOP= 0. ,FQDPRT= 1.0000E+01
 TL= -6.50 ,OYNR= 3.0 ,SDAMP= 0.000 ,SDPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-13 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 4.7368E-03 ,STDEV= 1.5752E-03 ,V MEAN= 4.5318E-01V STD DEV= 1.7100E-01 ,BITS= 1900
 PEI= 1.1579E-03 ,STDEV= 1.2872E-03
 LOCKIN= 1 ,DROPOUTS=0
 ERRM

0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	5.0000E+00

-1,-1 P(B/A)TIMES 451										-1,+1 P(B/A)TIMES 483									
121	37	7	1	0	0	1	0	0	0	0	1	0	0	0	0	0	0	0	0
73	41	25	7	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	36	21	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	11	7	3	0	0	0	0	0	0	1	1	0	0	0	0	0	0	0	0
1	2	0	0	0	0	0	0	0	0	8	2	1	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	41	13	5	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	97	41	15	2	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	117	67	53	14	3	0	0	0	0	0
+1,-1 P(B/A)TIMES 483										+1,+1 P(B/A)TIMES 483									
0	0	0	2	16	72	113	139	0	0	0	0	0	0	1	0	0	0	0	0
1	0	0	0	4	17	29	53	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	5	11	15	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	1	3	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	4	7	10	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	6	42	38	0	0
0	0	0	0	1	0	0	0	0	0	0	0	0	0	4	21	66	81	0	0
0	0	0	0	0	0	0	0	1	0	0	0	0	2	24	59	112	0	0	0

I1,I2,I11,I22 567 1426 1 1
 REC SLICE= 5.4336E+01 ,STD DEV= 5.1068E+00
 BIF = 2000 NO FADING
 2/5/74A NSPB = 80.

ENDB= 9.4 , DELF= 62.0 , BIF= 1000 , BL2= 88 , NSLICE= 26 , ASOFT= .3000
 SVRHZ= 0. , SWHX= 2.0150E+04 , SWMN= 6.8500E+03 , FLO= 1.0000E+01 , FRQOP= 0. , FQDPR= 1.0800E+01
 TL= -6.50 , CYNR= 3.0 , SDAMP= .230 , SDFPA= .470 , I1, I2, I11, I22 129 130 1 1
 WN= 83.0 , K= 468.6 , TAU1= 1.8000E+00 , TAU2= 1.6965E-02 , WNB= .9 , KB= 614.9 , TAUB1= 2.0353E+02 , TAUB2= 1.4945E+00
 RE= 1.4421E-01 , STDEV= 8.0E94E-03 , V MEAN= 3.0538E-01 , STD DEV= 1.8453E-01 , BITS= 1900
 LOCKIN= 1 , DROPOUTS= 1 , AVE= 0.3000E+01 , STD DEV= 0.

ERRM

8.0000E+01	1.2000E+01	2.8000E+01	3.5000E+01	2.6000E+01	2.1000E+01	1.2000E+01	6.0000E+00	2.0000E+00	5.0000E+00
4.0000E+00	2.0000E+00	1.0000E+00	4.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	3.0000E+00	0.	2.0000E+00
2.0000E+00	0.	0.	2.0000E+00	2.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	4.0000E+00	0.
0.	2.0000E+00	0.	2.0000E+00	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

-1,-1 P(B/A)TIMES 450								-1,+1 P(B/A)TIMES 483							
32	38	30	9	2	0	1	0	1	1	2	2	0	0	0	
21	35	36	7	5	3	0	0	0	1	2	4	2	1	0	
12	30	54	15	2	3	1	1	3	4	10	4	3	1	0	
5	10	15	21	7	2	0	0	9	14	9	12	7	3	0	
5	1	5	9	8	4	0	1	20	32	32	15	6	2	0	
0	0	4	5	0	1	0	0	32	39	37	14	9	1	3	
0	0	3	5	0	0	0	0	17	24	28	13	8	3	4	
0	0	2	0	0	0	0	0	3	7	12	14	4	4	1	
+1,-1 P(B/A)TIMES 404								+1,+1 P(B/A)TIMES 483							
2	2	4	7	8	14	4	7	0	0	0	0	4	3	2	
3	4	5	8	27	36	27	20	0	0	1	2	7	4	0	
2	3	5	13	21	31	46	42	1	2	0	1	7	4	3	
2	0	2	6	11	14	24	30	1	1	2	8	8	3	3	
0	0	1	0	0	6	7	8	1	2	7	11	4	5	2	
0	0	0	7	2	2	4	3	1	6	1	8	11	12	10	
0	0	0	0	2	0	0	0	2	3	9	7	15	26	43	
0	0	1	1	1	0	1	0	1	1	6	4	5	37	57	

I1, I2, I11, I22 247 1946 1326 493
 REC SLICE= 2.0003E+01 , STD DEV= 6.2894E+00
 BL2 = 88
 2/1/74A
 FADING

EN000= 9.4 ,BELF= 62.0 ,RIF= 1000 ,BL2= 100 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FCOPRT= 1.0000E+01
 TL= -6.50 ,DYNR= 3.0 ,SCAMP= .230 ,SDPHA= .470 ,I1,I2,I11,I22 129 130 1 1
 MN= 94.3 ,K= 468.6 ,TAU1= 1.3939E+00 ,TAU2= 1.4919E-02 ,MNB= .9 ,KB= 614.9 ,TAU81= 2.0353E+02 ,TAU82= 1.4945E+00
 PE= 1.1053E-01 ,STDEV= 7.1932E-03 ,V MEAN= 3.3669E-01V STD DEV= 1.8291E-01 ,BITS= 1900
 LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 2.7000E+01 ,STD DEV= 0.

ERRM

4.9000E+01	1.6000E+01	1.2000E+01	2.4000E+01	2.1000E+01	9.0000E+00	6.0000E+00	8.0000E+00	6.0000E+00	5.0000E+00
6.0000E+00	6.0000E+00	3.0000E+00	1.0000E+00	3.0000E+00	3.0000E+00	1.0000E+00	3.0000E+00	2.0000E+00	3.0000E+00
2.0000E+00	0.	1.0000E+00	2.0000E+00	1.0000E+00	3.0000E+00	1.0000E+00	1.0000E+00	2.0000E+00	0.
3.0000E+00	0.	1.0000E+00	0.	0.	2.0000E+00	1.0000E+00	0.	1.0000E+00	2.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

-1,-1 P(B/A)TIMES 453										-1,+1 P(B/A)TIMES 482									
32	56	29	11	5	0	3	0	0	0	0	0	1	0	0	0				
25	33	39	11	6	2	1	2	1	2	2	4	1	0	0	0				
18	36	50	11	6	2	3	1	7	2	7	3	0	0	0	0				
3	6	13	8	6	2	2	3	10	7	14	8	1	0	0	0				
0	3	4	3	1	0	1	0	17	25	19	12	3	1	0	1				
0	0	0	2	0	0	0	0	55	44	28	13	2	1	1	4				
0	1	3	2	0	0	0	0	27	51	36	14	2	5	2	1				
0	1	3	2	2	0	0	0	12	10	13	7	2	2	1	1				
+1,-1 P(B/A)TIMES 483										+1,+1 P(B/A)TIMES 482									
2	4	0	4	8	18	16	19	0	1	0	1	5	3	4	2				
3	2	7	5	12	38	55	37	0	0	1	0	6	9	1	0				
2	4	3	10	8	30	43	33	0	0	2	1	7	4	0	0				
0	1	0	5	7	19	26	10	0	0	1	1	3	4	4	0				
1	0	3	4	4	3	7	4	0	2	2	4	12	8	3	0				
0	0	1	1	2	6	1	2	0	4	2	6	9	13	20	17				
0	0	1	1	2	2	1	1	2	3	6	6	12	23	31	46				
0	0	0	2	0	1	1	1	7	6	4	2	13	38	54	67				

I1,I2,I11,I22 268 970 1326 493
 REC SLICE= 2.1070E+01 ,STD DEV= 6.3472E+00
 BL2 = 100 FADING
 2/1/74A

ENDD= 9.4 ,DELF= 62.0 ,BIF= 1000 ,BL2= 164 ,NSLICE= 26 ,ASCFT= .3000
 SVRHZ= 0. ,SNMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDP= 0. ,FQDPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SOAMP= .230 ,SDPHA= .470 ,I1,I2,I11,I22 129 130 1
 WN= 154.6 ,K= 468.6 ,TAU1= 5.1826E-01 ,TAU2= 9.0656E-03 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 RE= 2.7388E-02 ,STDEV= 3.7430E-03 ,V NEAN= 4.5167E-01V STD DEV= 2.0411E-01 ,BITS= 1900
 LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 6.8800E+00 ,STD DEV= 0.
 ERRM

1.3000E+01	2.0000E+00	1.0000E+00	4.0000E+00	1.0000E+00	2.0000E+00	0.	1.0000E+00	1.0000E+00	0.
2.0000E+00	0.	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.
0.	1.0000E+00	0.	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	0.	0.
0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.	1.0000E+00	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	7.0000E+00

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 483							
95	36	16	6	2	1	1	0	2	2	0	0	0	0	0	
64	46	21	9	0	0	0	2	1	0	0	0	0	0	0	
32	27	26	10	1	0	0	0	2	0	1	0	0	1	0	
13	11	13	8	2	0	0	0	4	1	1	0	0	0	0	
2	2	0	1	1	0	0	0	18	5	2	0	2	1	0	
1	0	0	0	0	0	0	0	30	18	4	3	0	1	0	
0	0	1	0	0	0	0	0	90	36	12	6	0	0	0	
0	0	0	1	0	0	0	0	111	73	31	19	2	1	0	
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 483							
2	2	1	3	19	52	102	127	0	1	0	1	1	1	1	
0	1	3	0	11	13	38	49	1	0	0	0	2	0	0	
0	0	1	1	2	4	14	10	0	0	0	1	3	1	0	
1	0	1	0	2	5	1	6	1	0	0	0	0	0	1	
0	0	0	1	0	0	0	3	1	0	1	0	1	4	10	
0	0	0	0	0	2	2	0	1	0	1	0	2	8	28	
0	0	0	0	0	0	0	0	0	0	0	0	1	13	58	
0	0	0	0	2	0	1	1	3	0	1	1	11	25	51	

11,I2,I11,I22 638 1856 529 737
 REC SLICE= 2.4849E+01 ,STD DEV= 3.8404E+00

BL2 = 164 FADING
 2/1/74A

ENQDB= 9.4 , DELF= 62.0 , BIF= 1000 , BL2= 188 , NSLICE= 26 , ASOFT= .3000
 SVRHZ= 0. , SWMX= 2.8150E+04 , SPMN= 6.8500E+03 , FLO= 1.0000E+01 , FRODOP= 0. , FQDPR= 1.0800E+01
 TL= -6.50 , DYNR= 3.0 , SDAMP= .230 , SOFMA= .470 , I1,I2,I11,I22 129 130 1 1
 MN= 177.2 , K= 468.6 , TAU1= 3.9439E-01 , TAU2= 7.8980E-03 , MNB= .9 , KB= 614.9 , TAUB1= 2.0353E+02 , TAUB2= 1.4945E+00
 PE= 2.6842E-02 , STDEV= 3.7079E-03 , V MEAN= 4.6826E-01V STD DEV= 2.1528E-01 , BITS= 1900
 LOCKIN= 1 , DROPOUTS= 1 , AVE= 1.0000E+01 , STD DEV= 0.
 ERRM

1.0000E+01	2.0000E+00	5.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	3.0000E+00	2.0000E+00	2.0000E+00	0.
1.0000E+00	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00
0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	1.0000E+00	1.0000E+00	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	6.0000E+00

-1,-1 P(B/A)TIMES 450								-1,+1 P(B/A)TIMES 483							
100	23	14	7	0	0	0	0	2	1	0	0	0	0	0	0
74	29	14	7	6	0	1	1	0	1	0	0	0	0	0	0
39	37	29	9	2	0	0	0	2	0	0	1	0	0	0	0
22	13	7	4	0	0	0	0	3	4	0	1	1	0	0	0
5	2	3	2	0	0	0	0	9	4	1	3	2	0	0	0
0	0	0	0	0	0	0	0	27	15	3	2	1	0	0	0
0	0	0	0	0	0	0	0	66	17	11	3	3	1	0	1
0	0	0	0	0	0	0	0	139	83	52	19	4	0	1	0
+1,-1 P(B/A)TIMES 482								+1,+1 P(B/A)TIMES 485							
1	0	3	6	23	57	102	152	0	0	0	0	2	0	0	0
2	1	0	0	3	15	30	46	0	0	0	0	0	0	0	0
0	0	0	0	1	5	2	10	0	0	1	0	0	1	0	1
0	0	1	1	2	0	2	5	0	0	0	0	0	2	1	3
1	0	0	2	0	1	1	2	1	0	0	0	0	4	10	13
0	0	0	0	0	0	1	0	0	0	0	1	3	19	34	44
0	0	0	0	1	0	1	0	0	0	0	1	4	18	35	97
0	0	0	1	1	0	0	0	0	0	1	3	7	27	38	114

I1,I2,I11,I22 1594 1314 529 737
 REG SLICE= 2.7187E+01 , STD DEV= 3.4492E+00

BL2 = 188 FADING
 2/1/74A

ENDD= 9.4 , DELF= 62.0 , BIF= 1000 , BL2= 88 , NSLICE= 26 , ASOFT= .3000
 SVRHZ= 0. , SWMX= -2.8150E+04 , SWMN= 6.8500E+03 , FLO= -1.0000E+01 , FRQDOP= 0. , FQDPRT= -1.0000E+01
 TL= -6.50 , DYNR= 3.0 , SDAMP= 0.000 , SOPHA= 0.000 , I1,I2,I11,I22 129 130 1 1
 WN= 03.0 , K= 460.6 , TAU1= 1.0000E+00 , TAU2= 1.6965E-02 , WNB= .9 , KB= 614.9 , TAU01= 2.0353E+02 , TAU02= 1.4945E+00
 PE= 1.2526E-01 , STDEV= 7.5941E-03 , V MEAN= 3.0949E-01V STD DEV= 1.7849E-01 , BITS= 1900
 LOGKIN= 1 , DROPOUTS= 1 , AVE= 3.2000E+01 , STD DEV= 0.

ERRM

6.6000E+01	1.0000E+01	1.7000E+01	3.6000E+01	2.9000E+01	1.5000E+01	1.8000E+01	6.0000E+00	3.0000E+00	6.0000E+00
4.0000E+00	2.0000E+00	1.0000E+00	2.0000E+00	1.0000E+00	0.	0.	2.0000E+00	3.0000E+00	2.0000E+00
3.0000E+00	0.	0.	0.	0.	0.	2.0000E+00	2.0000E+00	2.0000E+00	2.0000E+00
0.	2.0000E+00	2.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 483							
34	44	30	0	0	0	1	1	0	0	1	0	1	0	1	0
17	46	39	11	1	1	2	0	0	1	2	1	2	1	0	0
15	34	57	0	5	4	3	4	4	4	5	4	1	0	0	0
4	8	14	6	9	4	0	2	9	12	14	11	2	1	1	0
1	2	4	0	6	3	0	0	23	35	41	14	6	1	0	0
0	0	3	0	2	0	0	0	34	51	37	18	7	5	4	1
0	0	5	2	0	0	0	0	13	22	37	15	3	4	1	0
0	0	0	2	1	0	0	0	4	7	8	10	1	1	1	1
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 483							
1	2	6	4	12	12	0	3	0	0	0	0	5	7	0	0
1	2	5	10	30	45	29	27	0	0	0	2	2	11	3	0
1	3	4	4	23	32	59	41	0	1	0	1	6	7	3	0
0	0	0	7	0	11	17	20	0	0	1	4	4	5	1	1
0	0	0	2	3	6	10	2	1	2	6	4	12	0	4	2
0	0	0	3	0	3	4	2	5	2	3	10	0	7	7	9
0	0	1	4	2	0	0	0	4	3	6	6	17	24	41	37
0	0	0	2	4	0	0	0	3	10	4	3	13	30	56	71

I1,I2,I11,I22 1974 1082 1 1
 REG SLICE= 1.0119E+01 , STD DEV= 5.5119E+00

BL2 = 88
 2/1/74M
 NO FADE

ENODB= 9.4 , DELF= 62.0 , BIF= 1000 , BL2= 100 , NSLICE= 26 , ASOFT= .3000
 SVRHZ= 0. , SWMX= 2.8150E+04 , SWMN= 6.8500E+03 , FLO= 1.0000E+01 , FRQBP= 0. , FQDPR= 1.0000E+01
 TL= -6.50 , DYNR= 3.0 , SDAMP= 0.000 , SDPHA= 0.000 , I1,I2,I11,I22 129 130 1 1
 MN= 94.3 , K= 458.6 , TAU1= 1.3939E+00 , TAU2= 1.4919E-02 , WNB= .9 , KB= 614.9 , TAU01= 2.8353E+02 , TAU02= 1.4945E+00
 PE= 1.0053E-01 , STDEV= 6.8985E-03 , V MEAN= 3.4439E-01V STD DEV= 1.8716E-01 , BITS= 1900
 LOCKIN= 1 , DROPOUTS= 1 , AVE= 2.2000E+01 , STD DEV= 0.

ERRM

4.0000E+01	1.1000E+01	5.0000E+00	1.9000E+01	2.6000E+01	1.7000E+01	1.3000E+01	4.0000E+00	6.0000E+00	5.0000E+00
4.0000E+00	7.0000E+00	0.	2.0000E+00	0.	2.0000E+00	0.	3.0000E+00	0.	2.0000E+00
0.	1.0000E+00	0.	0.	2.0000E+00	1.0000E+00	3.0000E+00	2.0000E+00	3.0000E+00	0.
2.0000E+00	0.	0.	0.	1.0000E+00	3.0000E+00	1.0000E+00	1.0000E+00	0.	0.
0.	2.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

-1,-1 P(B/A)TIMES 452								-1,+1 P(B/A)TIMES 483							
42	53	31	4	1	0	1	0	1	0	0	0	1	0	0	0
30	36	31	9	3	2	2	3	1	3	0	0	0	0	1	0
13	30	61	10	6	6	0	1	1	1	3	2	3	0	0	0
3	7	16	9	4	2	1	0	12	11	15	3	3	2	0	0
2	1	4	3	2	0	0	0	24	27	23	0	2	0	1	1
0	0	5	1	0	0	0	0	55	43	23	17	1	3	3	1
1	1	5	1	0	0	0	0	30	40	39	10	6	2	3	3
0	0	5	4	0	0	0	0	6	8	15	7	5	1	2	3
+1,-1 P(B/A)TIMES 403								+1,+1 P(B/A)TIMES 482							
3	3	5	4	15	22	25	12	0	0	0	0	3	8	2	0
3	0	2	0	10	39	50	33	0	0	0	0	4	5	0	1
1	0	1	3	15	44	43	42	1	0	0	1	3	3	3	0
0	1	0	4	1	15	14	11	0	0	0	3	1	5	2	1
0	0	0	4	6	5	4	6	0	0	1	3	2	7	7	4
0	0	1	0	5	1	4	1	1	3	1	13	10	10	14	23
0	0	0	1	4	1	0	0	4	5	3	7	13	23	35	41
0	0	0	2	0	1	0	0	2	3	6	6	10	32	60	70

I1,I2,I11,I22 2032 434 1 1
 REQ SLICE= 1.9968E+01 , STD DEV= 6.3881E+00
 BL2 = 100 NO FADE!
 2/1/74M

ENODB= 9.4 ,DELF= 62.0 ,BIF= 1000 ,BL2= 164 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= -2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= -1.0000E+01
 TL= -6.50 ,OYNR= 3.0 ,SOAMP= 0.000 ,SOPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 WN= 154.6 ,K= 468.6 ,TAU1= 5.1826E-01 ,TAU2= 9.8556E-03 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 1.0526E-02 ,STDEV= 2.3413E-03 ,V MEAN= 4.5776E-01V STD DEV= 1.8332E-01 ,BITS= 1900
 LOGGIN= 1 ,DROPOUTS=0

ERRM

1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	2.0000E+00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	0.	2.0000E+00	0.	0.	0.	0.	2.0000E+00	1.0000E+00	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	7.0000E+00

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 482							
110	45	10	2	0	1	0	1	0	1	0	0	0	0	0	0
65	25	24	5	1	1	0	0	1	0	0	0	0	0	0	0
43	20	26	9	1	0	0	0	1	1	1	0	0	0	0	0
11	11	11	1	0	0	0	0	2	1	0	0	0	0	0	0
0	1	3	0	0	0	0	0	6	2	1	0	0	0	0	0
0	0	0	0	0	0	0	0	40	15	6	3	0	0	0	0
0	0	0	0	0	0	0	0	104	26	11	3	0	0	0	0
0	0	0	0	0	0	0	0	132	60	42	19	3	0	0	0
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 484							
0	0	2	1	20	65	114	137	0	0	0	0	0	0	1	0
0	0	2	0	1	19	30	43	0	0	0	0	0	0	0	0
0	1	0	0	1	6	5	23	0	0	0	0	0	1	0	1
0	0	0	1	1	2	3	2	0	0	0	0	0	0	1	0
0	0	0	0	0	1	0	0	0	0	0	0	0	3	6	13
0	0	0	0	0	1	0	1	0	0	0	1	3	11	35	48
0	0	0	0	0	0	0	0	1	0	0	1	1	23	54	77
0	0	0	1	0	0	0	0	1	0	1	0	4	30	53	114

I1,I2,I11,I22 231 338 1 1
 REG SLICE= 2.5097E+01 ,STD DEV= 3.5464E+00
 BL2 = 164 NO FADE
 2/1/74M

ENDOB= 9.4 ,DELTA= 62.0 ,BIF= 1000 ,BL2= 188 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0. ,SMMX= 2.8150E+04 ,SMMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPR= 1.0000E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SOPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 MN= 177.2 ,K= 468.6 ,TAU1= 3.9439E-01 ,TAU2= 7.8980E-03 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.8353E+02 ,TAUB2= 1.4945E+09
 PE= 1.1053E-02 ,STDEV= 2.3985E-03 ,V MEAN= 4.8037E-01V STD DEV= 2.0585E-01 ,BITS= 1900
 LOCKIN= 1 ,DROPOUTS=0

ERRM	1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	0.
	0.	0.	0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.
	0.	0.	0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
	1.0000E+00	0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.
	0.	0.	3.0000E+00	0.	0.	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	0.	7.0000E+00

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 482							
94	23	6	5	1	0	1	0	0	0	0	0	0	0	0	0
107	27	20	5	3	0	0	0	0	0	0	0	0	0	0	0
42	31	25	9	1	0	0	0	0	0	0	0	0	0	0	0
14	10	9	6	1	0	0	0	2	0	0	0	0	0	0	0
6	1	2	1	0	0	0	0	7	1	2	1	0	0	0	0
1	0	0	0	0	0	0	0	29	9	4	0	0	0	0	0
0	0	0	0	0	0	0	0	64	19	10	3	0	0	0	0
0	0	0	0	0	0	0	0	157	105	47	16	5	1	0	0
+1,-1 P(B/A)TIMES 482								+1,+1 P(B/A)TIMES 485							
0	0	0	4	16	80	116	176	0	0	0	0	0	0	2	0
0	0	0	0	2	10	13	39	0	0	0	0	0	0	0	0
0	0	0	0	0	2	2	12	0	0	0	0	0	0	0	0
0	0	0	0	0	1	3	2	0	0	0	0	0	0	1	3
0	0	0	0	0	1	0	0	0	0	0	0	1	4	6	13
0	0	0	0	0	0	0	0	0	0	0	1	3	14	30	68
0	0	0	0	0	1	0	0	0	0	0	0	8	29	42	84
0	0	0	0	0	0	0	0	2	0	0	1	3	16	44	110

I1,I2,I11,I22 1050 778 1 1
 REC SLICE= 2.6731E+01 ,STD DEV= 3.4284E+00
 BL2 = 188 NO FADE
 2/1/74M

IX-26

EN000= 9.4 , DELT= 62.0 , BIF= 1000 , Bl2= 176 , NSLICE= 26 , ASOFT= .3000
 SVRHZ= 0. , SWMX= 2.8150E+04 , SWMN= 6.8500E+03 , FLO= 1.0000E+01 , FRQDOP= 0. , FQOPRT= 1.0000E+01
 TL= -6.50 , BYNR= 3.0 , SDAMP= .230 , SDPHA= .470 , I1, I2, I11, I22 129 130 1 1
 WN= 165.9 , K= 468.6 , TAU1= 4.5000E-01 , TAU2= 8.4420E-03 , WNB= .9 , KB= 614.9 , TAUB1= 2.0353E+02 , TAUB2= 1.4945E+00
 PE= 3.0000E-02 , STDEV= 3.9135E-03 , V MEAN= 4.6358E-01V STD DEV= 2.8403E-01 , BITS= 1900
 PEI= 2.5263E-02 , STDEV= 3.6001E-03
 LOGKIN= 1 , DROPOUTS= 1 , AVE= 9.0000E+00 , STD DEV= 0.
 ERRH

2.2000E+01	2.0000E+00	1.8000E+00	0.	1.0000E+00	1.0000E+00	0.	1.0000E+00	0.	2.0000E+00
1.0000E+00	0.	0.	0.	2.0000E+00	0.	0.	0.	0.	1.0000E+00
1.0000E+00	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	0.	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.
1.0000E+00	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	2.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.	1.0000E+00	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	7.0000E+00

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 463							
112	26	16	5	2	0	0	0	4	0	1	1	0	0	0	0
66	29	23	5	1	0	1	0	0	0	0	0	1	0	0	0
41	26	21	12	2	2	1	0	1	0	0	0	0	0	0	0
13	11	17	6	0	0	0	1	4	1	1	0	0	2	0	0
1	4	1	0	0	0	0	0	0	1	5	1	0	0	0	0
1	1	0	2	1	0	0	0	26	7	4	3	0	0	0	0
1	0	0	0	0	0	0	0	69	34	19	6	0	0	1	1
0	0	0	0	0	0	0	0	146	68	38	20	5	4	0	1
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 463							
3	1	2	19	60	110	136	2	0	0	0	2	0	3	1	0
1	0	0	1	6	0	27	39	0	0	0	0	1	0	0	0
2	1	0	1	3	6	13	15	1	0	0	0	0	1	0	1
0	0	0	0	1	2	4	6	0	0	1	0	0	0	1	1
0	0	0	0	0	1	3	2	0	0	0	1	2	3	11	10
0	0	0	0	0	0	2	1	0	0	0	0	4	12	29	43
0	0	0	1	0	0	0	1	1	0	0	0	3	17	56	92
0	0	0	2	0	0	1	0	4	0	1	1	3	15	41	119

I1, I2, I11, I22 638 1850 529 737
 REG SLICE= 2.6309E+01 , STD DEV= 3.5759E+00
 TAU4 = 1.808E-3 (88 Hz) FADING
 2/4/74A

EN000= 9.4 ,DEL= 62.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 26 ,ASOFT= ,3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0000E+01
 FL= -6.50 ,DYNR= 3.0 ,SOAMP= .230 ,SOPHA= .470 ,I1,I2,I11,I22 129 130 1 1
 MN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,MNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 3.6316E-02 ,STDEV= 4.2918E-03 ,V MEAN= 4.7426E-01V STD DEV= 2.3727E-01 ,BITS= 1900
 PEI= 2.4737E-02 ,STDEV= 3.5633E-03
 LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 4.0000E+00 ,STD DEV= 0.

1.0000E+01	4.0000E+00	3.0000E+00	2.0000E+00	1.0000E+00	2.0000E+00	2.0000E+00	1.0000E+00	3.0000E+00	2.0000E+00
0.	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	2.0000E+00	1.0000E+00	0.	0.	1.0000E+00
1.0000E+00	1.0000E+00	0.	1.0000E+00	0.	0.	2.0000E+00	0.	0.	0.
1.0000E+00	0.	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	2.0000E+00
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
1.0000E+00	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	1.0000E+00	0.	0.	1.0000E+00	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	3.0000E+00

-1,-1 P(B/A)TIMES 453										-1,+1 P(B/A)TIMES 482									
109	31	21	6	3	2	0	0	0	0	3	1	0	0	0	0	0	0	0	0
64	19	22	6	1	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
45	23	24	7	2	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0
18	6	12	5	5	2	0	0	0	0	6	0	1	0	0	0	0	0	0	0
6	2	2	3	0	1	0	0	0	0	0	2	1	1	0	0	0	0	0	0
1	0	3	0	0	0	0	0	0	0	31	12	7	4	0	1	2	0	0	0
0	0	0	1	1	0	0	0	0	0	65	24	11	5	0	1	0	0	0	0
0	0	0	0	0	0	0	0	0	0	157	61	41	26	6	0	1	2	0	0
+1,-1 P(B/A)TIMES 483										+1,+1 P(B/A)TIMES 482									
0	1	0	6	26	70	97	142	0	0	1	0	0	1	0	1	1	1	0	0
0	0	0	2	3	17	15	32	0	0	0	1	0	0	0	2	0	1	0	0
2	1	1	0	1	7	9	24	0	0	0	0	0	0	0	1	0	0	0	0
2	0	0	1	1	4	6	2	0	0	0	0	0	0	1	3	5	6	0	0
0	0	0	0	0	1	2	2	0	0	0	0	0	1	2	11	8	18	0	0
1	0	0	0	0	1	0	1	1	0	1	0	0	5	4	11	24	66	0	0
0	0	0	0	0	0	1	0	1	0	1	1	1	2	7	17	29	73	0	0
0	0	0	0	0	1	1	0	1	0	1	1	0	4	5	23	38	103	0	0

I1,I2,I11,I22 638 1050 529 737
 REG SLICE= 2.6399E+01 ,STD DEV= 3.2639E+00
 TAU4 = 1.1052E-3 (144 Hz) FADING
 2/4/74A

IX-28

ENDD= 9.4 , DELF= 62.0 , BIF= 1000 , BL2= 176 , NSLICE= 26 , ASOFT= 3000
 SVRHZ= 0. , SWMX= 2.8150E+04 , SWMN= 6.8500E+03 , FLO= 1.0000E+01 , FRQDOP= 0. , FQDPRY= 1.0000E+01
 TL= 6.50 , BYNR= 3.0 , SOAMP= .230 , SFHA= .470 , I1, I2, I11, I22 129 130 1 1
 WN= 165.9 , K= 468.6 , TAU1= 4.5000E-01 , TAU2= 8.4420E-03 , WNB= .9 , KB= 614.9 , TAUB1= 2.0353E+02 , TAUB2= 1.4945E+00
 PE= 5.0000E-02 , STDEV= 5.0000E-03 , V MEAN= 4.0705E-01V STD DEV= 2.5952E-01 , BITS= 1988
 PEI= 2.5263E-02 , STDEV= 3.6001E-03
 LOCKIN= 1 , DROPOUTS= 1 , AVE= 0.0000E+00 , STD DEV= 0.

ERRM

1.6000E+01	6.6600E+00	8.0000E+00	1.0000E+00	3.0000E+00	3.0000E+00	1.0000E+00	0.	2.0000E+00	5.0000E+00
1.0000E+00	4.0000E+00	2.0000E+00	1.0000E+00	3.0000E+00	2.0000E+00	4.0000E+00	0.	3.0000E+00	3.0000E+00
0.	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	1.0000E+00	2.0000E+00	1.0000E+00	1.0000E+00
0.	2.0000E+00	0.	0.	0.	2.0000E+00	1.0000E+00	1.0000E+00	0.	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.
1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	0.	0.	1.0000E+00	0.	1.0000E+00
0.	0.	0.	0.	0.	0.	1.0000E+00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	2.0000E+00
0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.
0.	2.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 483							
92	24	20	9	4	2	0	2	1	2	0	1	0	0	0	
55	18	17	10	1	0	0	0	0	0	0	0	3	0	0	
56	9	13	10	9	0	0	1	3	0	1	1	0	0	0	
24	8	12	11	1	2	0	0	1	3	1	0	0	0	0	
12	2	5	3	0	1	0	1	17	5	0	0	1	1	0	
3	1	0	2	0	0	0	0	24	10	6	2	0	0	1	
0	1	0	0	0	0	0	0	52	14	13	5	0	1	0	
0	0	0	1	0	1	0	0	177	63	39	20	10	1	1	
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 483							
1	1	2	11	29	56	70	170	0	0	0	0	2	0	0	
0	1	0	3	5	12	11	27	0	0	0	1	3	0	0	
1	2	1	1	0	5	9	18	1	0	0	0	1	0	1	
1	2	0	0	2	2	3	7	0	0	0	1	2	2	3	
0	0	0	0	0	1	1	3	0	0	1	1	4	7	6	
0	0	0	0	0	1	1	1	1	0	1	3	7	11	17	
0	0	0	0	0	0	0	0	0	0	0	1	5	12	26	
0	0	1	1	1	1	1	1	1	1	2	4	9	25	46	

I1, I2, I11, I22 638 1850 529 737 TAU4 = 7.9577E-4 ((200 Hz) FADING
 REC SLICE= 2.6220E+01 , STD DEV= 3.3752E+00 2/4/74A

ENDB= 9.4 ,OELF= 62.0 ,BIF= 1000 ,BL2= 176 ,NSLICE= 26 ,ASOFT= 3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPR= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SDFHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 WN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,MNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 8.4211E-03 ,STDEV= 2.0964E-03 ,V MEAN= 4.6851E-01V STD DEV= 1.9806E-01 ,BITS= 1900
 PEI= 5.2632E-03 ,STDEV= 1.6600E-03
 LOCKIN= 1 ,DROPOUTS=0

ERRM	0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
	0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	0.	0.
	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
	0.	0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
	0.	0.	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.
	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	6.0000E+00

-1,-1 P(B/A)TIMES 450								-1,+1 P(B/A)TIMES 483							
115	31	14	3	1	0	0	0	0	0	0	0	0	0	0	
75	26	13	11	3	0	0	0	0	1	0	0	0	0	0	
38	41	20	6	1	0	0	0	0	1	0	0	0	0	0	
15	10	8	1	1	0	0	0	0	0	0	0	0	0	0	
4	2	3	0	0	0	0	0	0	0	4	0	0	0	0	
0	0	0	0	0	0	0	0	0	37	10	3	1	0	0	
0	0	0	0	0	0	0	0	0	91	26	16	3	0	0	
0	0	0	0	0	0	0	0	0	142	64	52	19	5	0	
+1,-1 P(B/A)TIMES 402								+1,+1 P(B/A)TIMES 485							
0	0	1	2	22	74	110	145	0	0	0	0	0	1	0	
0	1	0	0	3	15	21	47	0	0	0	0	0	0	0	
0	0	0	0	0	5	8	10	0	0	0	0	0	0	0	
0	0	0	0	1	1	3	3	0	0	0	0	0	1	1	
0	0	0	0	2	0	0	0	0	0	0	0	2	4	13	
0	0	0	0	0	0	0	0	0	0	0	0	6	19	30	
0	0	0	0	0	0	0	0	0	0	0	0	6	14	41	
0	0	0	0	0	0	0	0	0	1	0	0	3	24	52	

I1,I2,I11,I22 1594 1314 1 1
 REG SLICE= 2.6191E+01 ,STD DEV= 3.2335E+00
 TAU4 = 1.8086E-8 (88 Hz) NO FADING
 2/24/74A

EN000= 9.4 ,DELTA= 62.0 ,DIF= 1000 ,BL2= 176 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.0150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0000E+01
 FL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SDPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 WN= 165.9 ,K= 468.6 ,TAU1= 4.5000E-01 ,TAU2= 8.4420E-03 ,WNB= .9 ,KB= 614.9 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 4.0526E-02 ,STDEV= 4.5239E-03 ,V MEAN= 4.0521E-01V STD DEV= 2.5101E-01 ,BITS= 1900
 PEI= 7.8947E-03 ,STDEV= 2.0303E-03
 LOCKIN= 1 ,DROPOUTS=0

ERRM

1.0000E+01	3.0000E+00	3.0000E+00	3.0000E+00	1.0000E+00	1.0000E+00	0.	2.0000E+00	1.0000E+00	2.0000E+00
0.	2.0000E+00	1.0000E+00	1.0000E+00	0.	3.0000E+00	2.0000E+00	2.0000E+00	1.0000E+00	1.0000E+00
2.0000E+00	1.0000E+00	1.0000E+00	0.	1.0000E+00	1.0000E+00	0.	2.0000E+00	3.0000E+00	1.0000E+00
0.	0.	0.	3.0000E+00	1.0000E+00	2.0000E+00	0.	0.	2.0000E+00	1.0000E+00
1.0000E+00	0.	3.0000E+00	0.	1.0000E+00	0.	0.	1.0000E+00	0.	0.
1.0000E+00	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	2.0000E+00

-1,-1 P(B/A)TIMES 451								-1,+1 P(B/A)TIMES 483							
106	21	19	6	2	1	0	1	1	1	0	0	0	0	0	
59	24	13	11	3	0	0	0	0	0	0	0	0	0	0	
49	24	29	5	7	0	0	0	0	2	0	0	0	0	0	
20	15	9	4	0	1	0	0	3	1	1	1	0	0	0	
4	5	0	0	3	1	0	0	10	6	4	0	2	0	0	
5	1	4	0	0	0	0	0	25	6	2	2	0	0	0	
0	0	0	0	0	0	0	0	67	13	13	3	1	1	0	
0	0	0	0	0	0	0	0	178	58	47	22	7	6	0	
+1,-1 P(B/A)TIMES 483								+1,+1 P(B/A)TIMES 483							
0	0	2	16	34	57	93	178	1	0	0	0	1	0	1	1
0	0	2	2	5	10	10	39	0	0	0	0	0	0	0	0
0	0	0	1	2	2	5	15	0	0	0	2	0	2	0	0
1	0	0	0	1	1	1	1	0	0	0	2	0	6	4	11
0	0	0	0	1	0	1	2	0	0	0	0	1	7	17	20
0	0	0	0	0	0	0	0	0	0	0	3	5	19	27	49
0	0	0	0	0	0	0	0	1	0	1	0	3	18	23	82
0	0	0	0	0	0	0	1	3	0	1	3	14	16	44	95

I1,I2,I11,I22 1594 1314 1 1
 REG SLICE= 2.6126E+01 ,STD DEV= 3.3029E+00
 TAU4 = 7.9577E-4 (200 Hz) NO FADING
 2/4/74A

IX-32

ENQDB= 9.2 ,DEL= 66.0 ,BIF= 1000 ,BL2= 164 ,NSLICE= 26 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQOP= 0. ,FQDPRT= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= .230 ,SDPHA= .470 ,I1,I2,I11,I22 129 130 1 1
 MN= 154.6 ,K= 468.6 ,TAU1= 5.1826E-01 ,TAU2= 9.0656E-03 ,MNB= .9 ,KB= 577.6 ,TAJ81= 2.0353E+02 ,TAU82= 1.4945E+00
 PE= 4.3158E-02 ,STDEV= 4.6620E-03 ,V MEAN= 4.6717E-01V STD DEV= 2.1551E-01 ,BITS= 1900
 PEI= 4.6316E-02 ,STDEV= 4.8216E-03
 LOCKIN= 1 ,OROPUTS= 1 ,AVE= 9.0000E+00 ,STD DEV= 0.
 ERRM

2.6000E+01	2.0000E+00	3.0000E+00	2.0000E+00	4.0000E+00	0.	3.0000E+00	0.	2.0000E+00	0.
1.0000E+00	0.	1.0000E+00	0.	2.0000E+00	3.0000E+00	1.0000E+00	0.	2.0000E+00	0.
1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	1.0000E+00	0.	1.0000E+00	0.	0.
2.0000E+00	2.0000E+00	1.0000E+00	0.	0.	2.0000E+00	0.	1.0000E+00	2.0000E+00	0.
1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.
0.	2.0000E+00	0.	0.	0.	0.	1.0000E+00	0.	0.	2.0000E+00

-1,-1 P(B/A)TIMES 451

111	39	22	12	2	5	0	1
71	20	16	7	0	1	0	0
32	27	14	9	2	0	0	0
15	9	14	5	2	0	0	0
2	1	4	0	0	0	0	1
1	0	1	0	2	0	0	1
0	0	0	0	0	0	0	0
0	1	1	0	0	0	0	0

-1,+1 P(B/A)TIMES 483

3	2	0	1	0	0	0	0
2	1	0	1	0	0	0	0
3	1	1	0	0	0	0	0
5	1	4	2	0	0	0	0
18	9	5	1	0	0	0	0
31	9	8	1	1	1	0	0
74	20	7	5	3	0	0	1
137	66	30	19	3	6	1	0

+1,-1 P(B/A)TIMES 483

3	0	1	5	11	47	98	148
3	2	1	2	5	13	29	36
1	1	0	1	7	7	11	15
1	0	0	0	3	2	5	7
0	0	0	3	1	2	1	0
0	0	0	1	0	3	3	1
1	0	0	0	0	0	0	0
0	0	0	0	0	0	0	2

+1,+1 P(B/A)TIMES 483

1	1	0	1	4	0	1	1
1	0	0	0	0	0	0	0
0	0	0	0	0	0	2	1
1	1	2	1	1	2	0	1
0	0	0	2	0	1	3	8
0	0	1	2	1	7	16	38
0	0	0	1	4	15	43	84
3	0	3	2	10	15	46	156

I1,I2,I11,I22 231 338 529 737
 REC SLICE= 2.5264E+01 ,STD DEV= 3.8017E+00

WORST CASE 1 FADING
 2/5/74A

ENODS= 9.2 ,DEL= 60.0 ,BIF= 1000 ,BL2= 188 ,NSLICE= 25 ,ASOFT= .3000
 SVRHZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPR= 1.0800E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= .230 ,SOPHA= .470 ,I1,I2,I11,I22 129 130 1
 MN= 177.2 ,K= 468.6 ,TAU1= 3.9439E-01 ,TAU2= 7.8980E-03 ,WNB= .9 ,KB= 635.3 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 2.4737E-02 ,STDEV= 3.5633E-03 ,V MEAN= 4.6380E-01V STD DEV= 2.1519E-01 ,BITS= 1900
 PEI= 1.5789E-02 ,STDEV= 2.8599E-03
 LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 2.0000E+00 ,STD DEV= 0.

ERRM

1.1000E+01	1.0000E+00	3.0000E+00	0.	1.0000E+00	0.	0.	0.	1.0000E+00	0.
0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.	1.0000E+00	0.	0.
0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.	0.	1.0000E+00
0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	1.0000E+00	0.
1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	2.0000E+00
1.0000E+00	0.	0.	0.	1.0000E+00	0.	0.	1.0000E+00	1.0000E+00	0.
0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.
1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.	5.0000E+00

-1,-1 P(B/A)TIMES 453

97	38	7	6	2	1	0	0
73	30	18	10	0	1	0	0
42	24	22	10	3	0	0	0
16	16	14	9	2	0	0	0
2	3	3	1	0	0	0	0
1	0	0	1	0	0	0	0
0	0	0	0	0	0	0	0
0	1	0	0	0	0	0	0

+1,-1 P(B/A)TIMES 483

0	0	1	4	24	76	102	146
1	0	0	0	6	15	19	45
1	1	0	0	2	5	6	10
2	0	1	1	1	2	3	4
1	1	0	0	0	1	0	0
0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	1

-1,+1 P(B/A)TIMES 482

2	1	1	0	1	0	0	1
0	0	0	0	1	0	0	0
2	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0
5	2	2	1	0	0	0	0
28	12	4	0	0	0	0	0
75	19	15	6	0	0	0	1
154	72	40	27	3	1	0	0

+1,+1 P(B/A)TIMES 482

1	0	0	1	0	0	0	0
1	0	0	1	2	0	0	0
0	2	0	0	0	1	0	0
0	0	0	0	1	2	1	2
0	0	1	1	2	5	11	17
0	0	0	1	3	22	32	64
0	0	0	1	1	12	46	82
1	1	2	2	5	25	38	92

I1,I2,I11,I22 1594 1314 529 737
 REC SLICE= 2.6816E+01 ,STD DEV= 3.6702E+00

WORST CASE 2 FADING
 2/5/74A

EN008= 9.2 ,DELf= 66.0 ,BIF= 1000 ,BL2= 164 ,NSLICE= 26 ,ASOFT= .3000
 SVRMZ= 0. ,SWMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRF= 1.0000E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SDPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 MN= 154.6 ,K= 468.6 ,TAU1= 5.1826E-01 ,TAU2= 9.0656E-03 ,MNB= .9 ,KB= 577.6 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 1.5789E-02 ,STDEV= 2.8599E-03 ,V MEAN= 4.7442E-01V STD DEV= 2.0162E-01 ,BITS= 1900
 PEI= 1.4211E-02 ,STDEV= 2.7153E-03
 LOCKIN= 1 ,DROPOUTS= 1 ,AVE= 1.0000E+00 ,STD DEV= 0.

ERRM

3.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.	0.
2.0000E+00	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	0.	0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00	0.
0.	0.	0.	1.0000E+00	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	0.	0.
0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	0.	0.	0.	0.	1.0000E+00	0.	1.0000E+00	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00
0.	0.	0.	0.	0.	0.	0.	0.	0.	6.0000E+00

-1,-1 P(B/A)TIMES 451

123	43	15	3	0	1	0	1
67	34	21	6	2	0	0	1
46	22	19	9	2	0	1	0
8	14	6	1	0	0	0	0
2	1	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	1	2	0	0	0	0	0

-1,+1 P(B/A)TIMES 483

1	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
3	0	1	0	0	0	0	0
3	1	1	0	0	0	0	0
11	2	4	0	0	0	0	1
30	14	5	1	0	0	0	1
105	28	14	1	0	0	0	0
129	65	46	13	3	0	0	0

+1,-1 P(B/A)TIMES 483

0	0	1	3	18	48	126	146
1	0	0	1	3	13	31	45
0	0	1	0	0	8	9	17
0	0	0	0	1	0	1	3
0	0	1	1	0	1	1	0
0	0	0	0	1	0	0	0
0	0	0	0	0	0	0	1
0	0	0	0	1	0	0	0

+1,+1 P(B/A)TIMES 483

0	0	0	0	0	0	1	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	0	0	0	1	1	0	3
0	0	1	0	0	0	0	6
0	0	0	3	3	10	23	39
1	0	0	0	1	20	48	91
0	0	1	2	4	28	60	127

I1,I2,I11,I22 231 338 1 1
 REC SLICE= 2.4032E+01 ,STD DEV= 3.6204E+00

WORST CASE 1 NO FADING
 2/5/74A

ENDB= 9.2 ,DELF= 60.0 ,BIF= 1000 ,BL2= 188 ,NSLICE= 25 ,ASOFT= .3000
 SVRHZ= 0. ,SVMX= 2.8150E+04 ,SWMN= 6.8500E+03 ,FLO= 1.0000E+01 ,FRQDOP= 0. ,FQDPRT= 1.0000E+01
 TL= -6.50 ,DYNR= 3.0 ,SDAMP= 0.000 ,SDPHA= 0.000 ,I1,I2,I11,I22 129 130 1 1
 WN= 177.2 ,K= 468.6 ,TAU1= 3.9439E-01 ,TAU2= 7.8980E-03 ,WNB= .9 ,KB= 635.3 ,TAUB1= 2.0353E+02 ,TAUB2= 1.4945E+00
 PE= 8.4211E-03 ,STDEV= 2.0964E-03 ,V MEAN= 4.6102E-01V STO DEV= 1.9944E-01 ,BITS= 1900
 PEI= 2.1053E-03 ,STDEV= 1.0515E-03
 LOCKIN= 1 ,DROPOUTS=0

ERRM

1.0000E+00	1.0000E+00	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000E+00	0.
1.0000E+00	0.	1.0000E+00	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	9.0000E+00

-1,-1 P(B/A)TIMES 450								-1,+1 P(B/A)TIMES 483							
95	20	15	2	0	0	0	0	0	0	0	0	0	0	0	
72	40	14	12	3	1	0	0	0	0	0	0	0	0	0	
49	33	28	11	1	0	0	0	1	0	0	0	0	0	0	
15	12	12	2	2	0	0	0	1	0	0	0	0	0	0	
5	2	2	1	0	0	0	0	9	2	2	0	0	0	0	
1	0	0	0	0	0	0	0	33	6	4	0	0	0	0	
0	0	0	0	0	0	0	0	83	27	13	4	1	0	0	
0	0	0	0	0	0	0	0	147	80	49	18	7	0	0	
+1,-1 P(B/A)TIMES 482								+1,+1 P(B/A)TIMES 485							
0	0	1	3	26	67	132	150	0	0	0	0	0	0	0	
0	0	0	0	6	16	24	34	0	0	0	0	0	0	0	
0	0	0	0	1	3	6	7	0	0	0	0	0	0	0	
0	0	0	0	2	0	3	1	0	0	0	0	0	1	0	
0	0	0	0	0	0	0	0	0	0	0	0	0	8	13	
0	0	0	0	0	0	0	0	0	0	0	0	1	25	36	
0	0	0	0	0	0	0	0	0	0	0	1	8	24	43	
0	0	0	0	0	0	0	0	0	0	0	0	5	19	35	

I1,I2,I11,I22 1594 1314 1 1
 REC SLICE= 2.6948E+01 ,STD DEV= 3.2632E+00
 WORST CASE 2 NO FADING
 2/5/74A

APPENDIX X
ALTERNATE CONTINUOUS PHASE MODULATORS

Three alternate continuous phase modulators, a three step upconverter, an indirect FM modulator and a single step upconverter, were considered during the course of this study. The latter was finally selected because of its simplicity and minimum parts count. This appendix discusses these alternate designs.

Three Step Upconverter

Figure 1 shows the block diagram for the modulator and upconverter. The 400 MHz FSK signal is synthesized by generating a 1 MHz signal in a voltage controlled crystal oscillator and up-converting this signal by mixing it with higher frequencies derived from a 23 MHz crystal oscillator. The mixing is done in three steps to make filtering practical at each frequency. FSK is accomplished by pulling the 1 MHz VCXO with a ± 3.2 volt DC signal amplified from the TTL data.

The oscillators are specified to have an end-of-life long term drift of ± 10 ppm. The 1 MHz oscillator is voltage controlled to provide the 64 Hz frequency shift. A VCO was chosen over frequency switching to provide phase continuity between frequencies.

A typical modulation range for a crystal oscillator is 80 ppm (Frequency Electronics, Inc.). For the needed 64 Hz modulation, this requires a 1 MHz center frequency and a DC control voltage of ± 3.2 volts. The frequency will typically switch in 20 microseconds.

The power losses and gains are indicated in Figure X-1. The criteria for the design are:

- o An input of 6 dBm into the local oscillator port of the mixer.
- o 0 dBm or less into the signal port to maintain at least a 6 dB ratio to minimize spurs.
- o Limit amplifier gain to approximately 10 dB due to environmental constraints.

The mixers have a loss of approximately 6 dB at a ratio of 6 dB between signal and L.O. (per Relcom Co.).

Filters are provided in the L.O. lines to eliminate the harmonics of the square waves generated by multiplying and dividing. This application is not critical.

Filters are also provided after each mixing operation to eliminate harmonic spurs. The filter bandwidths were chosen to have a -60 dB bandwidth at less than the separation of the closest low order spurs.

The spurs of the first mixer were the closest and a crystal filter is required. The crystal filter is specified by Crystal Network Products. The 2nd and 3rd mixer filters are designed according to Texscan tubular filter specifications and are summarized in Figure 1. The main objection to the Figure 1 design* is its overall hardware complexity, high parts count, and consequently, its lower reliability, higher power consumption, and added weight. Based on information obtained from a crystal oscillator manufacturer alternate designs are possible.

The following are the constraints which dictated the design parameters:

1. The modulation index is .7 radians $\pm 5\%$ over the temperature range of -40°F to $+160^{\circ}\text{F}$.
2. Over the temperature range, an ovenized oscillator can be pulled a minimum of ± 1 ppm and a maximum of ± 100 ppm. The minimum value is indicated by a crystal oscillator vendor as being the value one could pull an oscillator to an accuracy of $< 5\%$. The maximum is constrained by the phase noise of an oscillator which should be > 76 dBc at 100 Hz from the carrier in a 1 Hz bandwidth. To deviate ± 31 Hz, this implies a VCXO may be centered between 300 KHz and 30 MHz. However, due to the limitations of practical crystal cuts, the best oscillators are constructed in the 5 to 20 MHz range.
3. The minimum two-sided bandpass filter 3 dB bandwidth is to be 3%. The filter attenuation of the closest spur should be at least 40 dB down at the modulator output. This is because the non-linear power amplifiers will enhance the spurs approximately 15 dB and also create intermodulation products. Because of the extreme temperature range and associated filter drift problems, 60 dB will be used as the design

*M. D. Saferstain, "SAEP Modulator", TRW IOG 7322.4-15, November 19, 1973.

constraint. The filter will have a maximum of 5 poles to minimize filter size and number of elements and maximize reliability.

Given these constraints, two alternate modulator configurations are realizable as shown in Figures X-2 and X-3.

Indirect FM Modulator

The indirect FM modulator design based on the narrowband phase modulator concept conceived by Armstrong, integrates the data, linearly phase modulates the resultant waveform with a modulation index of 0.0775, and multiplies the modulated carrier 8 times to achieve an output frequency of 400 MHz at a modulation index of 0.7. Linear phase modulation is achieved by summing the carrier in quadrature with the double sideband suppressed carrier modulated signal; i.e., the output $Y(t)$ as a function of the input signal $X(t)$ is,

$$Y(t) = \cos(\omega_c t) + X(t)\sin(\omega_c t)$$

$$= \cos(\omega_c t + \tan^{-1}X(t)) = \cos(\omega_c t + X(t))$$

for $|X(t)| \ll 1$. In this case, $X(t) = \beta \int \phi(t) dt$ where β is the modulation index

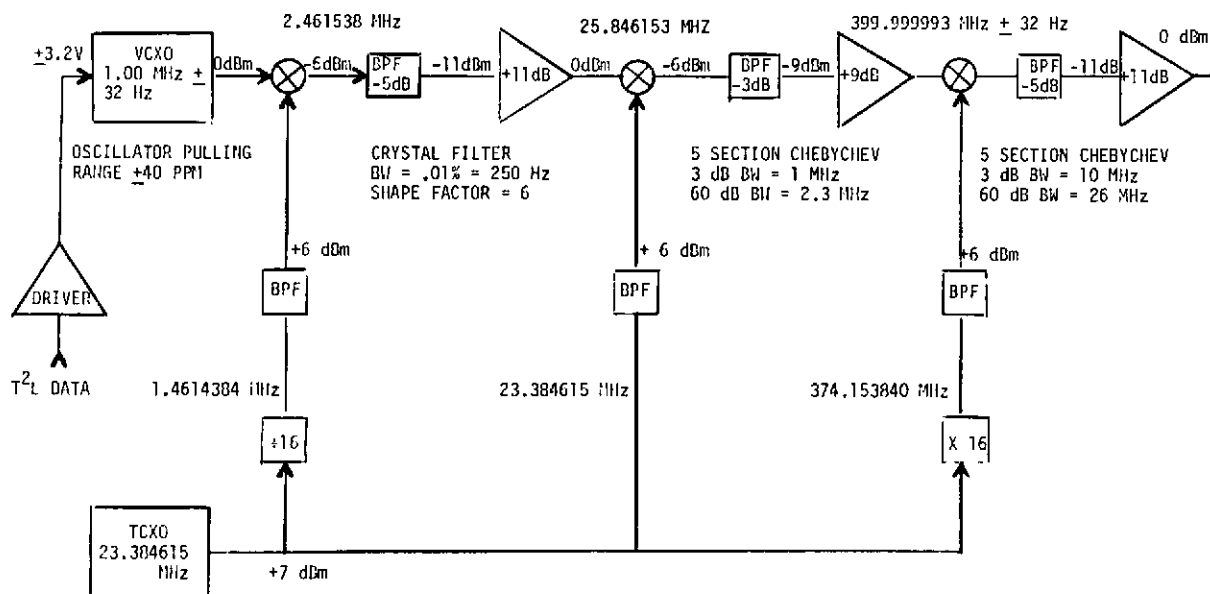


FIGURE X-1
THREE STEP UPCONVERTER MODULATOR

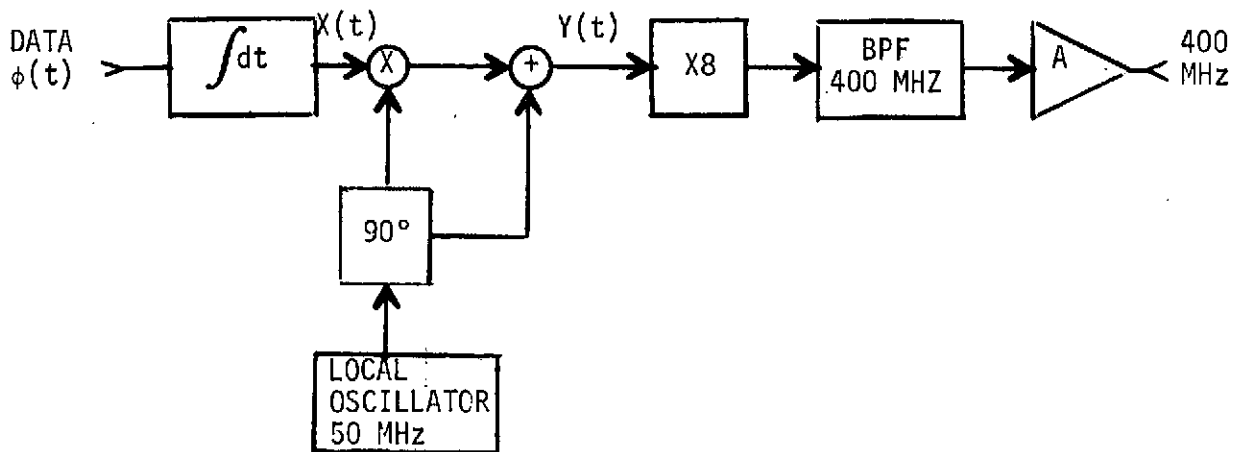


FIGURE X-2
INDIRECT FM MODULATOR

and $\phi(t)$ is the digital data. The one fundamental drawback to this concept is the practical implementation of the integrator and mixer. For long strings of marks or spaces, or where the average number of marks and spaces are not equal, the integrator and mixer must have sufficient dynamic range to operate over the entire period of data transmission. Furthermore, the phase modulation approximation holds only for the range where $|X(t)| \ll 1$. Since $\tan^{-1} \alpha = \alpha - \frac{\alpha^3}{3} + \frac{\alpha^5}{5} \dots$, if we modulate one bit at a modulation index of .0775, a string of data where the marks outnumber the spaces by 10 bits would increase the distortion from .2% to 20%**, clearly an unacceptable situation. Lower modulation indices may be possible by decreasing the 50 MHz LO and increasing the multiplication factor. However, in view of the simplicity of the single conversion direct FM design discussed below, this design is untenable.

** The desired signal at the output of an FM modulator is:

$$Y(t) = \cos(\omega_c t + \beta \int \phi(t) dt).$$

The actual signal out of the narrowband FM modulator is:

$$\begin{aligned} Y(t) &= \cos [\omega_c t + \tan^{-1}(\beta \int \phi(t) dt)] \\ &= \cos [\omega_c t + \beta \int \phi(t) dt - \frac{\beta^3}{3} (\int \phi(t) dt)^3 + \frac{\beta^5}{5} (\int \phi(t) dt)^5 - \dots] \end{aligned}$$

where the higher power terms in the expansion are the distortion terms. If for one bit, $\beta \int \phi(t) dt = .0775$ radians, then the distortion is in the order of $(.0775)^2/3 \approx .2\%$. Where the data is such that $\int \phi(t) dt = 10 \int \phi(t) dt$, the distortion increases to $(.775)^2/3 \approx 20\%$.

Single Conversion FM Modulator

The single conversion direct FM modulator shown in Figure 3 takes the 0 dBm output of a FCXO at 20 MHz and upconverts in one step to the output frequency of 400 MHz. The nearest mixer sideband in the upconversion is 40 MHz away using a doubly balanced mixer which also suppresses the 380 MHz LO a minimum of 25 dB. This implies a 3% bandwidth, 5 pole Chebyshev filter may be used at 400 MHz which would result in the 380 MHz LO being attenuated an additional 40 dB to a total level of 65 dB and the 40 MHz sideband attenuated to 68 dB. The total loss in the filter is approximately 5 dB, thus an 11 dB gain amplifier is needed to bring the output to 0 dBm. This modulation technique is simple and straightforward, requiring a minimum of parts, meets all the design constraints and, based on the new oscillator data, is the TRW recommended design.

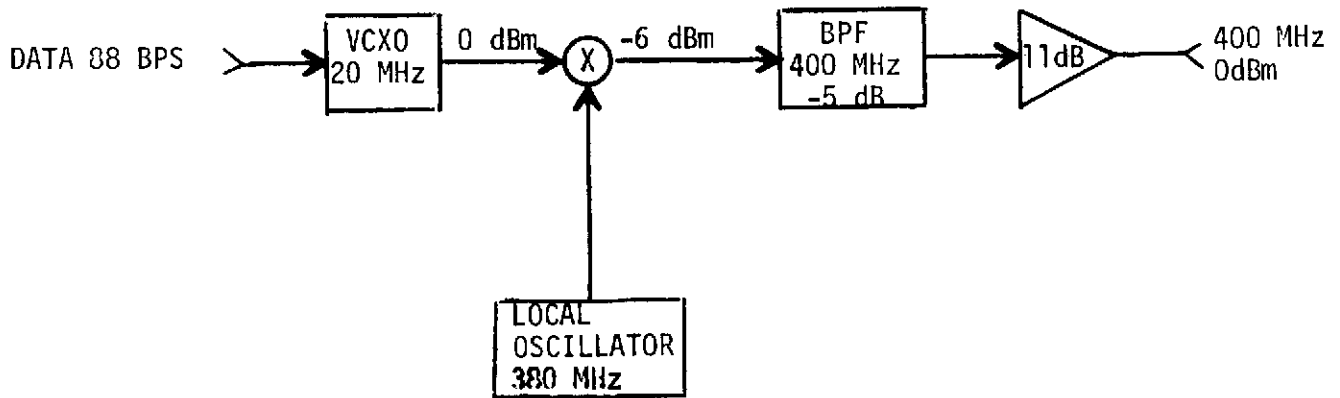


FIGURE X-3
SINGLE CONVERSION DIRECT FM MODULATOR