

2(mix)

NASA CR-112244

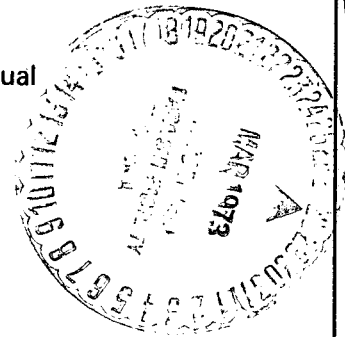
FINAL REPORT

A STUDY OF THE DYNAMICS OF ROTATING SPACE STATIONS WITH ELASTICALLY CONNECTED COUNTERWEIGHT AND ATTACHED FLEXIBLE APPENDAGES

Volume II Computer Program User's Manual

By

Eugene J. Lowe and Fred Austin



Prepared under Contract No. NAS 1-10973 by
Grumman Aerospace Corporation
Bethpage, New York 11714

for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

March 1973

(NASA-CR-112244) A STUDY OF THE
DYNAMICS OF ROTATING SPACE STATIONS WITH
ELASTICALLY CONNECTED COUNTERWEIGHT AND
ATTACHED FLEXIBLE APPENDAGES (Grumman Aerospace
Corp.) 431 p HC \$23.75
CSSL 20K
G3/23
Unclas
65558
N73-19073

NASA CR-112244

FINAL REPORT

**A STUDY OF THE DYNAMICS OF ROTATING
SPACE STATIONS WITH ELASTICALLY
CONNECTED COUNTERWEIGHT AND
ATTACHED FLEXIBLE APPENDAGES**

Volume II Computer Program User's Manual

By

Eugene J. Lowe and Fred Austin

**Prepared under Contract No. NAS 1-10973 by
Grumman Aerospace Corporation
Bethpage, New York 11714**

for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

March 1973

TABLE OF CONTENTS

<u>Section</u>	<u>Page</u>
NOTE ON UNITS	ix
1.0 INTRODUCTION	1-1
2.0 PHASE I -- MODAL COUPLING OF SUBSTRUCTURES	2-1
2.1 Introduction	2-1
2.2 Selection of Substructure Modes	2-3
2.3 Preparation of Data.	2-5
2.3.1 Numbering System and Coordinates	2-5
2.3.2 Constrained Substructure Modes and Nonrectangular Coordinates.	2-8
2.4 Program Limitations	2-9
2.5 Instructions for setting up input data deck for Phase I Program	2-10
2.6 Program Output.	2-14
3.0 PHASE II -- DEVELOPMENT OF TIME HISTORY.	3-1
3.1 Introduction.	3-1
3.2 Symbols	3-4
3.3 Coordinates Used in the Problem	3-11
3.3.1 Coordinate Systems	3-11
3.3.2 Euler Angles	3-11
3.3.3 Main Coordinates Used in the Problem	3-12
3.3.4 Coordinates Used to Describe the Connecting- Structure Deformations	3-12
3.4 Engineering Considerations When Preparing Data.	3-15

Preceding page blank

TABLE OF CONTENTS (Continued)

<u>Section</u>	<u>Page</u>
3.4.9.3 Supplementary Loads	3-31
3.4.10 Determining Quiescent Deflections	3-37
3.5 Program Limitations	3-38
3.6 Instructions for Setting Up Input-Data Deck for Phase II Program	3-39
3.7 Program Output	3-51
 Appendices	
A. Detailed Information for the Phase I Computer Program	A-1
A1. Example of Input Data.	A-2
A2. Example of Program Output.	A-10
A3. Brief Description of Each Subroutine	A-58
A4. Sequence of Operations in Subroutine Late.	A-59
A5. Input, Output, and Intermediate Files.	A-60
A6. Program Flow Charts.	A-61
A7. Fortran Source Deck Listing	A-76
B. Detailed Programming Information for the Phase II Computer Program.	B-1
B1. Examples of Input Data	B-2
B2. Examples of Program Output	B-9
B3. Description of Numerical-Integration Subroutine (MAGIC) Parameters	B-45
B4. Brief Description of Each Subroutine	B-48
B5. Replaceable Subroutines.	B-50
B6. Input, Output, and Intermediate Files.	B-72
B7. Program Flow Charts.	B-73
B8. Fortran Source Deck Listing.	B-94

FOREWORD

This volume of the final report is submitted to the NASA Langley Research Center in partial fulfillment of Contract NAS 1-10973. This contract involves the formulation of a mathematical model for predicting the dynamic behavior of a class of rotating flexible space-station configurations, and the preparation of associated computer programs.

Volume I contains the development of the required theoretical techniques, and Volume II is a computer-program user's manual.

Dr. Robert W. Fralich of the NASA Langley Research Center is the Technical Monitor. Dr. Fred Austin of the Grumman Aerospace Corporation is the Project Engineer.

Mr. Eugene J. Lowe prepared all of the computer programs described in this manual and wrote the descriptions of the programs and the method of setting up the cards. Dr. Fred Austin wrote the engineering descriptions contained in this manual.

The authors gratefully acknowledge the useful comments provided by Dr. R. Fralich and Mr. J. Smedfjeld. Also, Miss B. Durling's help in converting the computer program is sincerely appreciated.

Preceding page blank

PRECEDING PAGE BLANK NOT FILMED

NOTE ON UNITS

The program may be used with all consistent sets of units. For example, if the input data is in the lb-ft-sec-slug system, the output will also be in that set of units; if the input data is in the Newton-meter-sec-kg system, the program will express the solutions in that system.

In the Phase I program only, the user may input the weight and weight moment of inertia of each mass and the acceleration of gravity, G . The program then divides these weight properties by G to obtain the mass properties. If the mass properties are known, the user may input these instead of the weight properties; however, in this case, a value of G equal to one must be input.

Preceding page blank

1.0 INTRODUCTION

This user's manual provides the information required to use and modify two computer programs. The programs were developed on the IBM 370-165 computer located at Grumman Data Systems and then converted for use on the CDC 6600 computer located at the NASA Langley Research Center.

The first program, known as Phase I, is used to obtain the vibration modes of a structure using the modes of the component modules. The structure may consist of up to seventeen modules. The second program, known as Phase II, is used to solve, by numerical integration, the equations of motion of a flexible two-mass Space Station consisting of a Laboratory, a Counterweight, and a Connecting Structure. The modal characteristics and mass distribution of the Laboratory and Counterweight are required input data for the Phase II program. These properties may be generated by using the Phase I program or may be obtained elsewhere. The output format of the Phase I program is compatible with the input of the Phase II program, and the two programs can be run together in one submittal.

The Phase I program requires 70,000 octal core-storage locations, and the Phase II program requires 300,000 octal core-storage locations on the CDC 6600 computer.

2.0 PHASE I -- MODAL COUPLING OF SUBSTRUCTURES

2.1 INTRODUCTION

The Phase I computer program is used to obtain the modes of vibration for a structure using the modes and mass properties of each of its component substructures. Figure 2.1 illustrates, schematically, the most general configuration which may be treated. There is a maximum of seventeen substructures. Also, less complex configurations may be considered since any of the substructures may be absent from the idealization provided, of course, that the absent substructures do not disconnect the configuration. The modules are shown in-plane and perpendicular to each other for schematic purposes only. Actually, they may be skewed at any orientation in three dimensions. In fact, substructure modes can be supplied in a coordinate system which is skewed relative to the total-structure coordinate system. The central modules (numbers 1, 11, 14, 16 and 17) are called core modules, and the outer modules are called appendages.

While the total-structure modes to be used as input data for the Phase II Program are free-free, the Phase I Program may also be used to obtain cantilever modes for the total structure with Module 1 fixed at some point.

It is assumed that the junction surface between modules has no deformation. Another assumption is that appendages may not be connected to each other; i.e., a closed loop may not be formed. However, the user may bypass the Phase I computer program and supply the normal modes and modal masses of any Laboratory and/or Counterweight to Phase II.

One feature of the procedure is that the user is permitted to supply constrained substructure modes. These are modes which were obtained for idealizations where constraints were employed; for example, in a beam analysis axial extension may have been neglected. Constraints may be handled by two different methods. In the first, the user supplies modes containing six rectangular coordinates for each mass point; however, constrained coordinates are either related by equations of constraint or may be zero. By the second method, the user may supply modes containing less than six coordinates to describe the motion of each mass point; however, he must either identify which if any of the six coordinates are zero or he must supply constraint relations which transform the supplied coordinates to

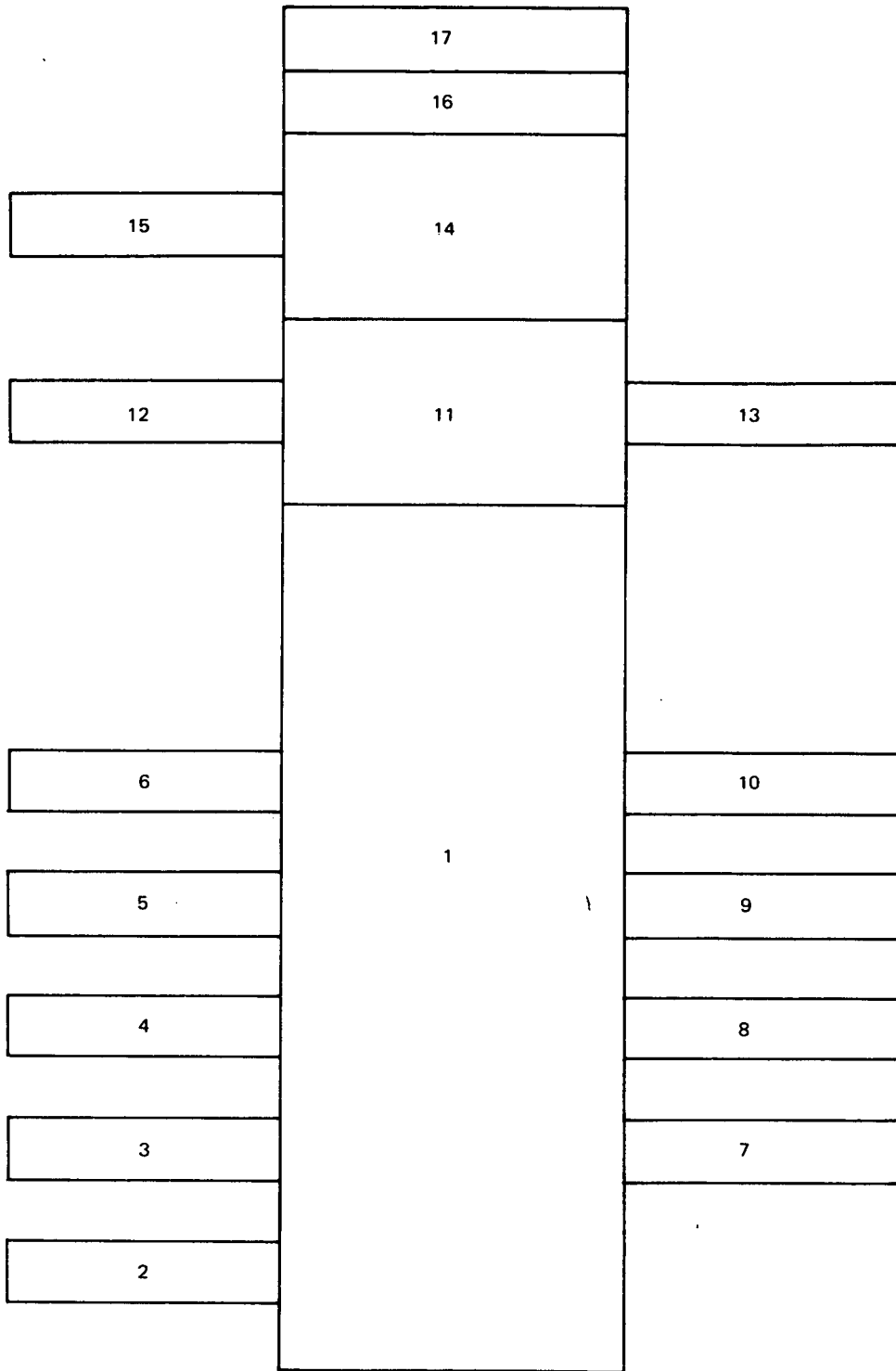


Fig. 2.1 General 17-Module Configuration for Modal Synthesis

the six rectangular coordinates. As described in Section 2.3.2, only certain types of constraint relations may be supplied. This feature was limited by the available computer storage space.

2.2 SELECTION OF SUBSTRUCTURE MODES

The normal modes of vibration of each of the substructures must first be determined from conventional lumped-parameter vibration-analysis procedures. The required input data includes the natural frequencies, mode shapes, generalized masses, and discrete mass matrices associated with each flexible body. As indicated in Figure 2.2, if free-free modes of the coupled structure are desired, then the free-free modes of Module 1 must be supplied; if the cantilevered modes of the coupled structure are desired, then the cantilevered modes of Module 1 must be supplied. Module 1 may also be constrained in some directions and not others. When obtaining the modes of Module 1, it must be supported in the same way as the total structure. Accordingly, the modes of Module 1 may have from 0 to 6 frequencies which are zero. Cantilevered modes are used for all other modules. All of the substructure modes with the exception of the rigid-body modes for Module 1 must be orthogonal; therefore the user must ensure that any equal-frequency elastic modes have been orthogonalized before use in this program.

As with any synthesis technique, the procedures discussed here will yield an exact representation of the coupled system if all of the substructure modes are used. In practice, however, each substructure is approximately represented by its lower-frequency modes. Thus the synthesized modes are approximate, with the lower-frequency modes generally being most accurate. How well the synthesis procedure works is dependent on how many modes are used to represent the substructures, and how accurately these substructure modes represent the motions of the coupled structure.

The analyst can exercise some control over the accuracy of the synthesis through the judicious selection of the substructure modes to be used. Another means of improving accuracy is to use so-called "mass-loaded" modes. This means that the mass and inertia properties of all influencing substructures are included in the preliminary idealization used for obtaining the modes of a core module. For example, referring to Figure 2.2, the modes of Module 1 would be calculated

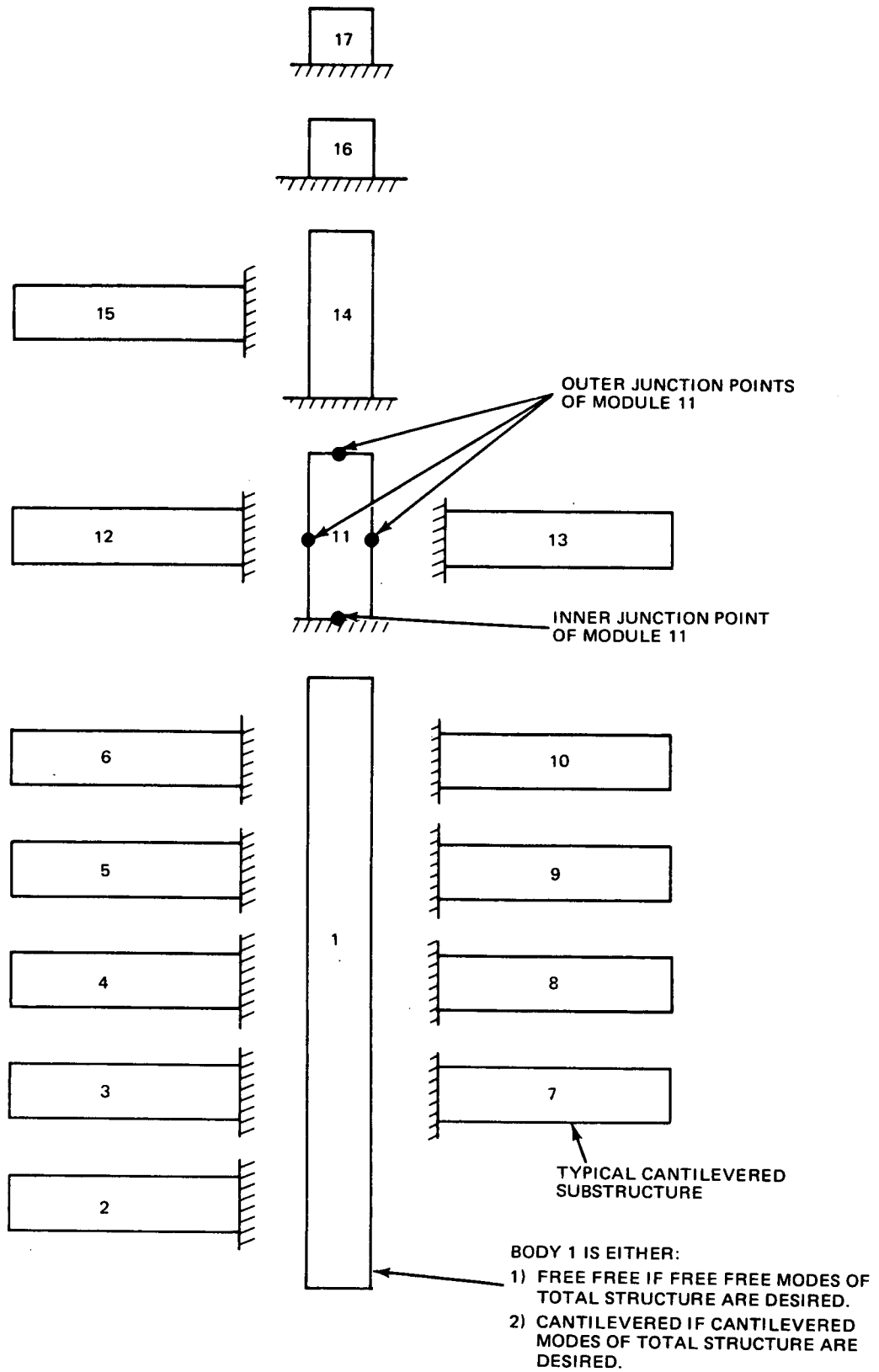


Fig. 2.2 Arrangement of Substructures for Modal Synthesis;

with Module 2 through 17 attached as rigid masses, those of 11 with 12 through 17 attached, those of 14 with 15, 16, and 17 attached, and those of 16 with 17 attached. The modes obtained in this manner are closer to those of the coupled system than modes computed without mass loading, and thus produce consistently better results when used in the synthesis procedure. See Section 3.4 of Volume I for a numerical comparison of frequencies using mass-loaded modes and frequencies using conventional modes.

2.3 PREPARATION OF DATA

2.3.1 Numbering System and Coordinates

Each module is assigned a module number. Its mass points are numbered consecutively beginning with 1 as shown in Figure 2.3. The input modes are expressed in terms of these numbers. The program renumbers the mass points consecutively for the entire structure, starting with Module 1 and continuing, in order, with each higher module number. The coupled structure numbers are shown in parenthesis in Figure 2.3. The output for the entire structure is expressed in terms of these numbers.

Each module (except Module 1) must attach to a mass point of the previous module; however, if there is no mass present at the connection point, an artificial mass may be created which has zero mass.* In the example, Module 14 of Figure 2.3 connects to Mass 3 of Module 11. The attachment point (Point 0) of each module is located by its global coordinates (X_0 , Y_0 , and Z_0). Point 0 for Module 14 and the global coordinates (X , Y , and Z) are also shown in Figure 2.3. The global coordinates are also the mean axes (the \tilde{X} axes for the Laboratory and the \tilde{Y} axes for the Counterweight) of the Phase II program.

Since the user's modes are supplied in a local (x , y , z) coordinate system which is not generally parallel to the global coordinate system, the orientation of the local coordinates must be specified for each module. This is accomplished by the method illustrated in Figure 2.4. As indicated, the local coordinate system of a typical module is translated so that its origin will coincide with the origin of the global coordinate system. Then points a and b are selected as follows:

* In this case, it is advisable to use the mass-loaded modes discussed in the previous subsection.

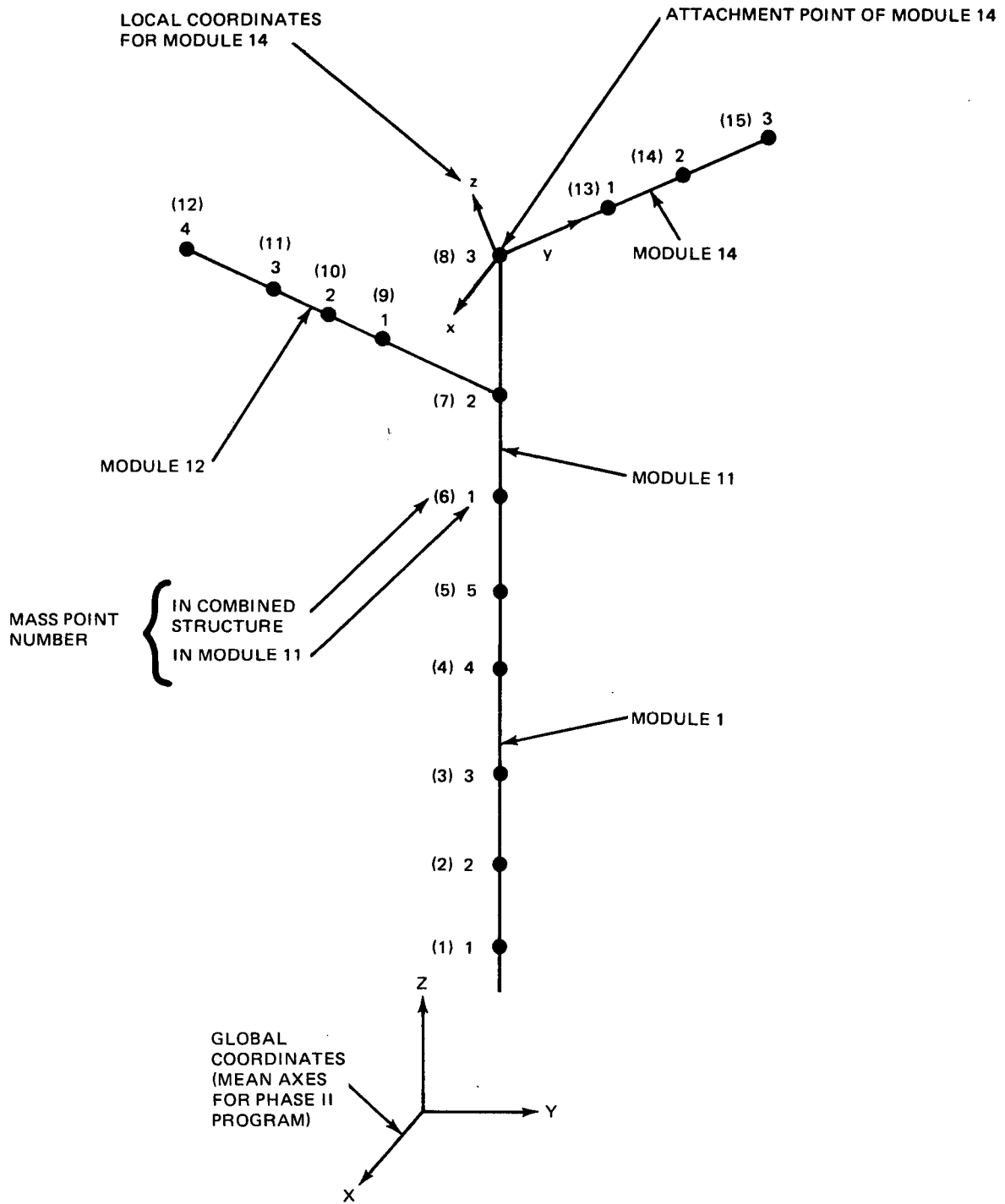


Fig. 2.3 Example of Structure to be Coupled

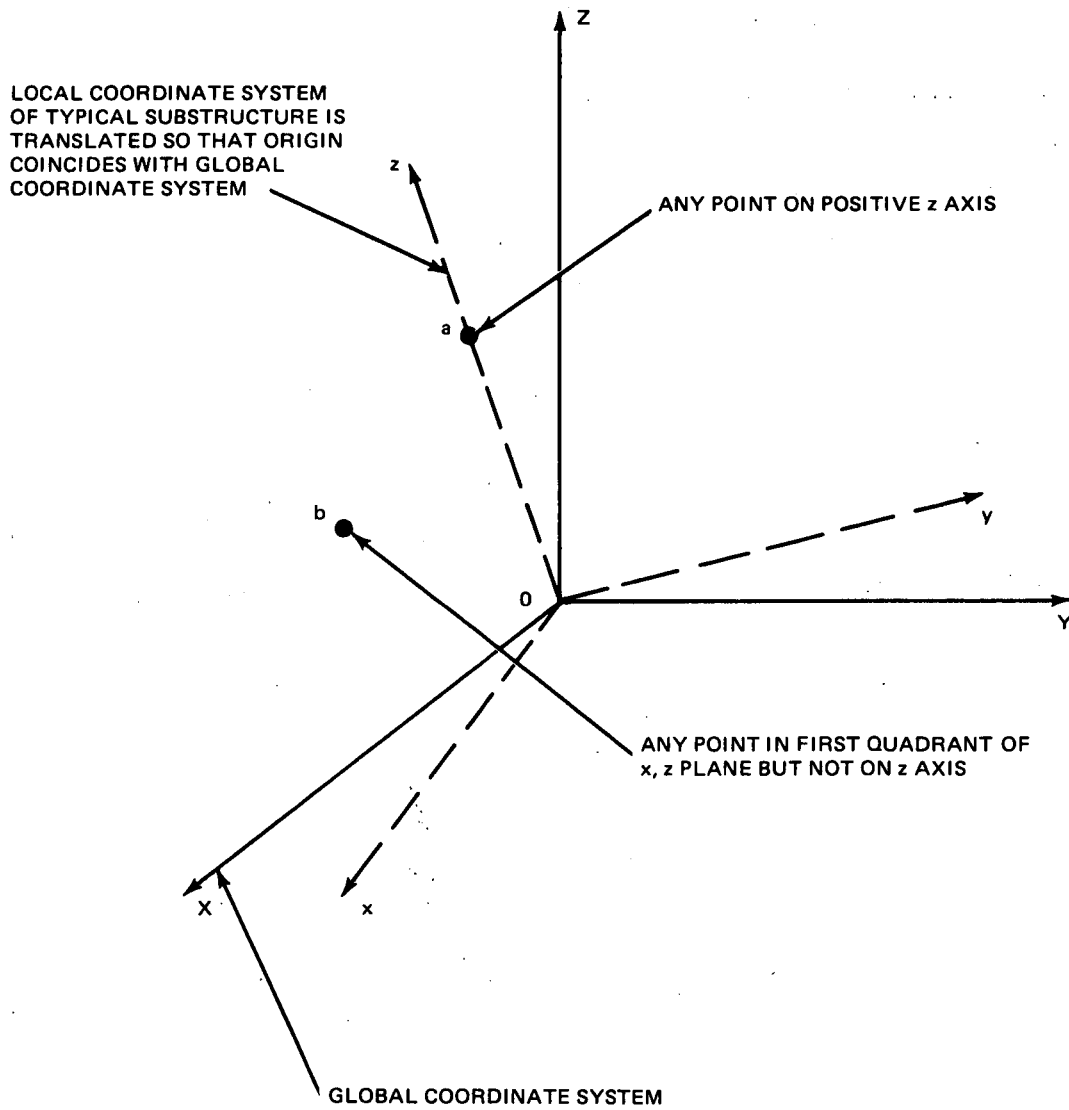


Fig. 2.4 Information Required to Specify Orientation of Local Coordinate System

- Point a is any point on the positive z axis
- Point b is any point in the first quadrant of the x, z plane that is not on the z axis

It is usually convenient to select point b as a point on the positive x axis. The global coordinates of points a and b (X_a, Y_a, Z_a and X_b, Y_b, Z_b) are specified and this information is used by the program to orient the local coordinate system.

2.3.2 Constrained Substructure Modes and Nonrectangular Coordinates

The program normally requires, as input data, substructure mode shapes expressing the motion of each mass point using three rotations and three translations expressed in the local coordinate system for that substructure. However, as a result of the method used for idealizing the substructure, the user may have modes available with less than six degrees of freedom at each mass point. As an example, if the substructure is a beam, axial extension may be neglected. In other types of constraints some coordinates are dependent on others. In addition, coordinates which are not rectangular (for example, polar coordinates) may have been used in describing the substructure modes. The program can accommodate modes which do not use the usual standard six rectangular coordinates to describe the position of each mass provided the N ($N \leq 6$) coordinates used $\{q_y^i\}$ at each mass point M_i can be related to the six rectangular coordinates $\{q_x^i\}$ at M_i by the following equation:

$$\{q_x^i\} = [T_i]^T \{q_y^i\} \quad (2.1)$$

The computer must be informed of the value of the N by $6 \times T$ matrix $[T_i]$ at each mass point; the following program features simplify the required input data in most cases:

- A T matrix need only be input once if it applies to an entire module or to consecutively numbered mass points within a module. This matrix is known as the default T matrix.
- If all degrees of freedom present at a mass point are expressed in the rectangular local coordinate system (e.g., x, y, z for Module 14 in Figure 2.3), it is only necessary to indicate which coordinates are absent in the mode shapes as a result of zero deformation in that direction. The program will construct the T matrices from this information. If all coordinates are present, the T matrix will simply be the identity matrix.

2.4 PROGRAM LIMITATIONS

- 1) Module 1 must be present
- 2) Modules 2-11 if present must attach to Module 1
- 3) Modules 12-14 if present must attach to Module 11
- 4) Modules 15, 16 if present must attach to Module 14
- 5) Module 17 if present must attach to Module 16
- 6) There is a maximum of 30 input-data modes per module
- 7) There is a maximum of 100 total input-data modes
- 8) There is a maximum of 30 mass points per module
- 9) There is a maximum of 100 mass points total

2.5 INSTRUCTIONS FOR SETTING UP INPUT DATA DECK FOR PHASE I PROGRAM

The input deck to the program is organized as follows for each run: a TYPE I deck, then several TYPE II decks, followed by a TYPE III deck. The user may supply two runs back-to-back. If only one run is supplied the program automatically detects the end of the input data deck and terminates execution.

The TYPE I deck describes which modules are present, the number of modes per module, the number of mass points per module, junction points for attached modules or appendages, and the gravity constant (G) for the program. A TYPE II deck is enclosed for each module and gives the location of the attachment point (X_0) and orientation of the local coordinates (X_a and X_b) for the module, each mass point location in local coordinates, the mass matrix in local coordinates corresponding to each mass point, the module modes in local coordinates, and data identifying the degrees of freedom present at each mass point. The TYPE III deck includes the diagonal elements of the modal mass matrix and the substructure eigenvalues (frequencies squared).

Specific instructions are presented below. An example of the input data is given in Appendix A-1

TYPE I Deck

The TYPE I deck consists of 5 cards.

- Card 1: Seventeen two-column fields for modules 1-17. Place a 1 in the two-column field corresponding to a module which is present.
- Card 2: Similar to Card 1. Place the number of modes for each module present in the appropriate two-column field.
- Card 3: Similar to Card 1. Place the number of mass points for each module present in the appropriate two-column field.
- Card 4: Sixteen two-column fields for modules 2-17. Place the number of the mass point to which the module is attached in the appropriate two-column field. Use the mass point number of the root module. (E.g., Module 14 would be connected to mass point 3 in Figure 2.3.)
- Card 5: Enter the gravity constant G in the first 15 columns. The elements of the mass matrix are divided by G. It is read with a FORTRAN format of (E 15.8).

TYPE II Deck (For Each Module Present)

- Group 1: Enter the global coordinates, (X, Y, Z) , of points 0, a and b with (X_0, Y_0, Z_0) on the first card, (X_a, Y_a, Z_a) on the second card and (X_b, Y_b, Z_b) on the third. Each card has three 15 column fields corresponding to the X, Y and Z coordinates respectively. The FORTRAN format is (3E 15.8) for each card.
- Group 2: Enter the local (x, y, z) coordinates of mass points 1, 2, 3, etc. for the module. Use one mass point per card with FORTRAN format (3E 15.8).
- Group 3: Enter the mass and the 3 x 3 inertia matrix for each mass point 1, 2, 3, etc. consecutively. Mass and inertia properties may be supplied in mass or weight units, along with the appropriate value of "G". The actual mass and inertia properties are input without mass loading. Four cards for each mass point must be supplied:
- Card 1: Enter mass in first 15 columns. The FORTRAN format is (E 15.8).
- Card 2: Enter row 1 of inertia matrix. The FORTRAN format is (3E 15.8) for each column.
- Card 3: Enter row 2.
- Card 4: Enter row 3.
- Group 4: This group specifies the module mode shapes and the constraint matrices (T matrices) discussed in Section 2.3.2.
- (a) Enter a T-matrix card to define the default T-matrix for the modules. This matrix will be used for all mass points unless overridden. A T-matrix card is a seven-field card. The first column contains a 0 if the coordinates used for the mode shapes are parallel to the local axes and it is desired that the program generate the T matrix. Otherwise, enter a 1 in the first column. If a zero is entered in the first column, the next six columns contain a 1 if the degree of freedom is present in the mode shape and a zero if not. If a 1 is entered in the first column, the next six columns should be left blank.

- (i) (If column 1 is set to 1) - Enter N on a card, where N is the number of degrees of freedom used to describe the motion of the constrained mass point in the mode. Use a FORTRAN format of (I2).
- (ii) (If column 1 is set to 1) - Enter the NX6 T matrix row by row, four numbers to a card, using format (4E 15.8).
- (b) Enter the coupled-structure mass-point number of the first mass point at which the default T matrix is to be overridden. Use 50 if the default T matrix is not to be overridden. Use a FORTRAN format of (I2).
- (c) For each mass point:
 - (i) (If override was specified for the current mass point) Perform steps (a) and (b) above to define the override T matrix for the mass point and the number of the next mass point at which the default is to be overridden. Do not enter the next mass-point number when overriding the T matrix at the last point.
 - (ii) Enter module modes in local coordinates. If any rigid-body modes are present, these must be the first modes in Module 1. The modes are read in as an NXM matrix row by row where N is the number of degrees of freedom at the current mass point and M is the number of modes for the module. The FORTRAN format is (3 (8X, E15.8, 1X)).

Repeat the TYPE II Deck for each module present.

TYPE III Deck

Group 1: For each module present enter the diagonal elements of the modal mass matrix using format (3 (8X, E15.8, 1X)). Begin a new card for each module.

Group 2: Similar to Group 1. Enter the eigenvalues (frequencies squared in rad^2 per unit time squared).

Group 3: Consists of 2 cards.

Card 1: Enter the number of rigid-body modes in column one. If the program is to be used together with the Phase II program, 6 rigid-body modes should always be used.

Card 2: Enter the number of eigenvectors to be computed, and the number of eigenvalues to be computed. The FORTRAN format is (2I3). The number of eigenvectors must be less than or equal to the number of eigenvalues, and the number of eigenvalues must be less than or equal to the total number of substructure modes.

2.6 PROGRAM OUTPUT

The results of this program are the flexible modes of the coupled structure in the global coordinate system. The trivial rigid-body modes are not printed. The input data for the Phase II program must not contain the rigid body modes*; thus the Phase I output modes are in the form required for the Phase II program. The Phase I output modes are normalized to unit modal mass. In addition to the combined-structure mode shapes and frequencies, the Phase I program output includes the mass-point locations in global coordinates and the mass and inertia matrices in global coordinates for each mass point. This information is also required input for the Phase II computer program. A sample of Phase I output is presented in Appendix A2.

The Phase I and Phase II computer programs may be connected and run together by using the proper job control instructions. To accomplish this, the output of a Phase I run is placed on a file which is then passed to the Phase II run. If two back-to-back Phase I runs are made, two separate files are created. The output files of the Phase I program are discussed in Appendix A5, and the input files of the Phase II program are discussed in Appendix B6.

* The Phase I input data, however, must contain the rigid-body modes of Module I.

3.0 PHASE II - DEVELOPMENT OF TIME HISTORY

3.1 INTRODUCTION

The Phase II computer program solves the equations of motion developed in Volume I by numerical integration and, in this way, develops the time history of the system's motion. The entire vehicle under consideration is referred to as the Space Station, the main body is called the Laboratory and the other body is called the Counterweight. The structure separating these bodies is referred to as the Connecting Structure. Both the Laboratory and the Counterweight are flexible structures with arbitrary shape and mass distribution. The Connecting Structure is also flexible and arbitrary, but its mass is neglected. Figure 3.1 illustrates the general configuration which may be treated, and Figure 3.2 illustrates a particular example.

Problems which may be studied using the simulation include deployment and retraction of the Connecting Structure with simultaneous or sequential spin up and spin down, the effects of moving rigid masses such as a cargo elevator or crew members on board the Laboratory, and the effect of fluid pumped through a piping system on the Laboratory. Five control systems are included to study various types of controlled maneuvers including mass balancing and wobble damping. Various features including control systems and Connecting-Structure characteristics have been included in subroutine form so that these items may be easily replaced with minimum disruption to the main program. Special constraint options permit the user to rigidize the Laboratory, the Counterweight, or the entire Space Station; thus the easier-understood rigid-body results can be compared with the more complex flexible-body solutions.

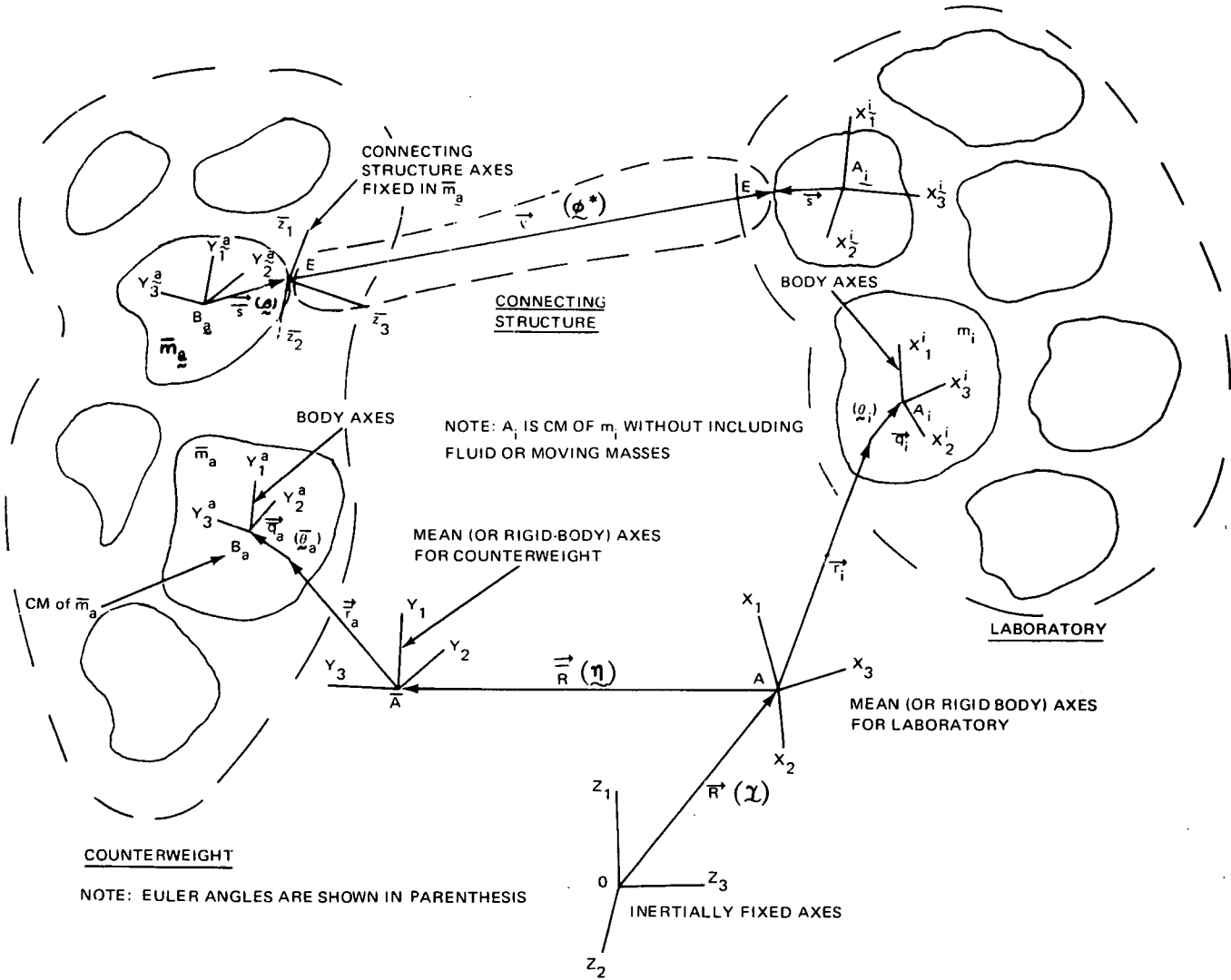
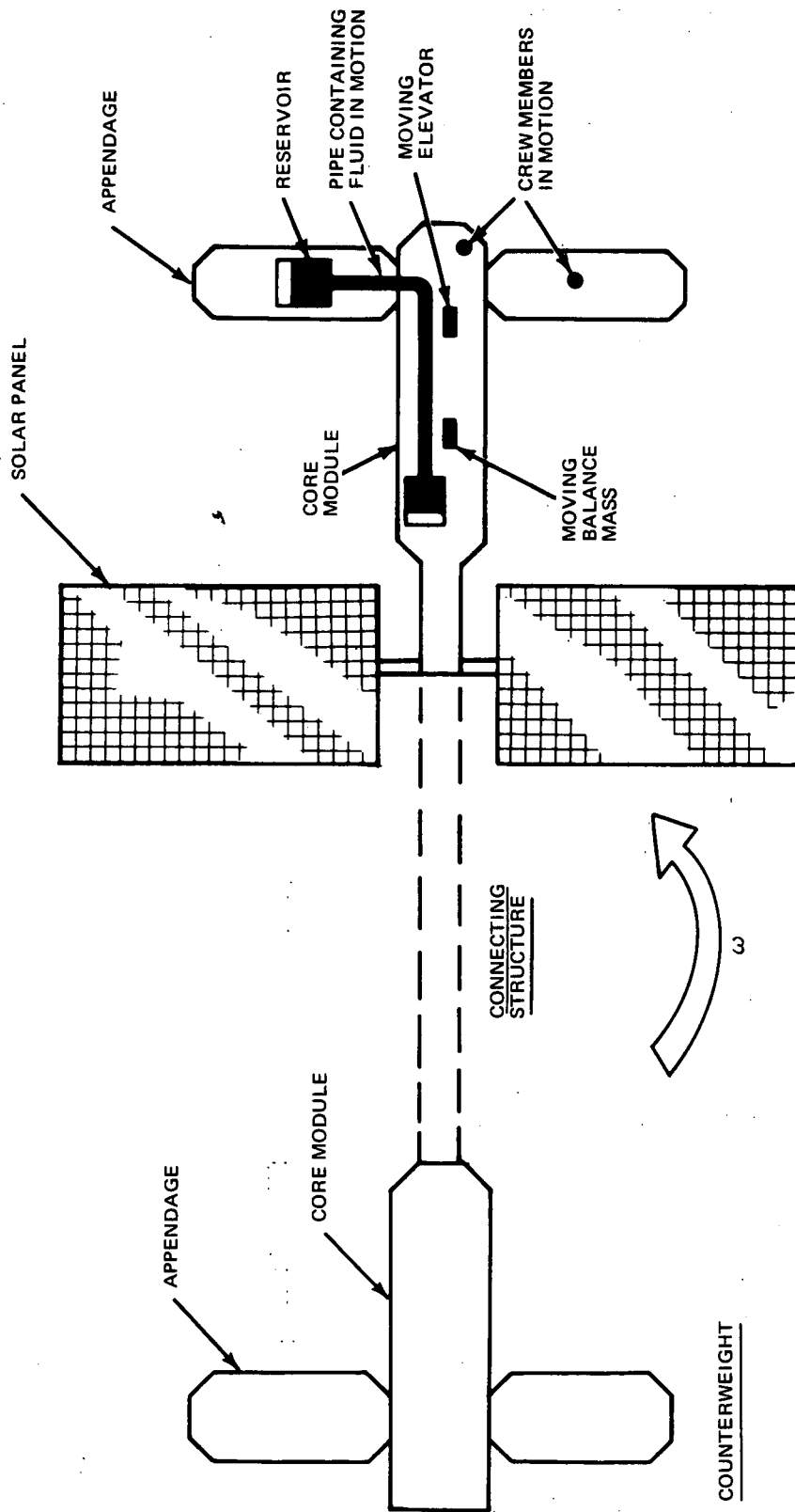


Fig. 3.1 Idealization and Coordinate Systems



LABORATORY

Fig. 3.2 One Example of a Space Station that Can be Studied Using the General Mathematical Model

3.2 SYMBOLS

The analytical symbols used in Section 3 and in Appendix B5 are defined below.

A	cross sectional area of inside of pipe
AE	Axial stiffness of beam-type connecting structure
a	undeformed distance from Laboratory mass center to attachment point of beam-type Connecting Structure
\tilde{a}	index number of mass point on Counterweight to which Connecting Structure is attached
acc_{01C}	magnitude of spin-speed acceleration command
$acc_{103\ MAG}$	magnitude of deployment acceleration command
acc_{MAG}	magnitude of acceleration command
b	undeformed distance from Counterweight mass center to beam attachment point for beam-type Connecting Structure
b_i	inside radius of reservoir on m_i
E, \bar{E}	points at which Laboratory and Counterweight, respectively, attach to Connecting Structure
EI	bending stiffness of beam-type Connecting Structure
$e_{\omega LDB}$	spin speed control error dead band
$e_{\theta DB}$	attitude angle error dead band
$\dot{e}_{\theta MAX}$	magnitude of maximum desired attitude angle error rate at which torque is applied
$\left. \begin{array}{l} err_{KT}, err_{KTI} \\ err_{LL}, err_{LLI} \end{array} \right\}$	used in both gimbal-angle and gimbal-angle rate law (see Figures 3.14 and 3.15)
$\{e_i\}$	unit vector tangent to pipe centerline along nominal direction of fluid velocity ⁽¹⁾
$\{\Delta e_i\}$	value of $\{e_i\}$ at nominal pipe outlet less value at nominal pipe inlet ⁽¹⁾

(1) See Footnotes at end of symbol list

$\{e_i^B\}$	$\{e_i\}$ for pipe section on m_i which is connected to reservoir on m_i . $\{e_i^B\}$ is always directed outward from control volume (see Figure 3.6)
$\{e_i^R\}$	unit vector along reservoir center line in mass m_i directed from reservoir base toward reservoir-pipe connection ⁽¹⁾ (see Figure 3.6)
f_{JET}	jet thrust
$\{f_\ell^i\}, \{\bar{f}_\ell^i\}$	internal force at point on m_ℓ , and \bar{m}_ℓ^i , expressed X_ℓ^i and Y_ℓ^i axes, respectively
$\{f_s^i\}, \{\bar{f}_s^i\}$	supplementary forces on m_i and \bar{m}_a , respectively ⁽¹⁾ ⁽²⁾
$\{f_E^*\}$	force applied by Laboratory on Connecting Structure at point E; vector is expressed in \bar{z} axes
$\{f_c^i\}, \{\bar{f}_c^i\}$	force applied by control system on m_i or \bar{m}_a , respectively ⁽¹⁾ ⁽²⁾
$\{G_i\}$	see Equations (3.4a) and (3.4b) for a through pipe ⁽¹⁾
$\{G_i^P\}$	$\{G_i\}$ for a reservoir pipe ⁽¹⁾
GJ	torsional stiffness for beam-type Connecting Structure
$\{\Delta H_i\}$	$[\Gamma(U_i)] \{e_i\}$ at nominal pipe outlet less value at nominal pipe inlet for pipe on m_i ⁽¹⁾ ⁽⁶⁾
h_i	fluid height in reservoir on m_i
$h_{i0}, h_{i \max}, h_{i \min}$	initial, maximum and minimum values of h_i , respectively
I_L, I_C	transverse moments of inertia of undeformed Laboratory and Counterweight, respectively, used in simplified model to determine damping coefficients of beam-type Connecting Structure in bending
$I_\beta \text{ GIM}$	moment of inertia of CMG wheel including gimbal about transverse wheel axis
$[I_i], [\bar{I}_a]$	moment of inertia matrices of m_i and \bar{m}_a , respectively ⁽¹⁾ ⁽²⁾
$[I_i^P], [I_i^f]$	moment of inertia matrices of fluid in reservoir pipe on through pipe on m_i , respectively

\tilde{i}	index of mass on Laboratory to which Connecting Structure is attached
i_s	index of mass on Laboratory at which sensor and CMG are located
J_L, J_C	axial (roll) moments of inertia of undeformed Laboratory and Counterweight, respectively used in simple model to obtain damping coefficient of beam-type Connecting Structure in torsion
$[J_i]$	area moment of inertia of the elements dA_n on the fluid boundary about point A_i (see Figure 3.5b) ⁽¹⁾
$[J_i^B]$	$[J_i]$ evaluated for area associated with point B on reservoir pipe (see Figure 3.6A)
$[\Delta J_i]$	$[J_i]$ at nominal outlet of through pipe less value monimal inlet ⁽¹⁾ ⁽⁶⁾
K_{eXSE}	gain in balance-mass control system multiplying filtered sensor acceleration error
K_{DESE}	gain in balance-mass control system multiplying balance mass velocity
K_T	gain in wobble control system multiplying error in gimbal angle and gimbal-angle rate in gimbal-angle and gimbal-angle rate control system respectively
$K_{\dot{\theta}}$	gain in wobble control system multiplying gambal-angle rate
l_{03}	component 3 of $\{l_0\}$, length of beam-type Connecting Structure
l_{03U}	update value of l_{03} specified for use in position command routine when deployment or retraction is commanded
$\{l\}, \{l_0\}$	deformed and undeformed vectors, respectively, from Connecting-Structure attachment point on Counterweight to attachment point on Laboratory ⁽⁵⁾
$l_0 \text{ min}$	minimum value of l_{03} used in evaluating stiffness and damping coefficients for beam-type Connecting Structure

M_L, M_C	in list of input data, these values are masses of Laboratory and Counterweight, respectively, used in beam-type Connecting Structure to establish damping coefficients
m_i, \bar{m}_i	mass of i^{th} lumped mass point of Laboratory or Counterweight, respectively
m_i^f	mass of fluid in pipe on m_i
m_i^P	mass of fluid in reservoir pipe on m_i
mom_{CMG}	momentum of CMG used for wobble control
n, \bar{n}	number of mass points on Laboratory and Counterweight, respectively
n_{CMG}	value is 1 when CMG is nominally controlling wobble (gimbal-angle mode) otherwise value is 0 (CMG gimbal angle-rate mode)
p, \bar{p}	number of flexible modes used for Laboratory and Counterweight, respectively
$\{q_i\}, \{\bar{q}_a\}$	linear deflection of cm of m_i or \bar{m}_a , respectively (3) (4)
$\{R\}$	vector from origin of \underline{Z} axes to origin of \underline{X} axes (3)
$\{\bar{R}\}$	vector from origin of \underline{X} axes to origin of \underline{Y} axes (4)
$\{\bar{R}_0\}$	undeformed value of $\{\bar{R}\}$
$\{\Delta\bar{R}\}$	$\{\bar{R}\} - \{\bar{R}_0\}$
$\{R_i\}$	vector from origin of \underline{Z} axes cm of m_i (3)
$\{r_i\}$	vector from origin of \underline{X} axes to cm of m_i when Laboratory is undeformed (3)
$\{\bar{r}_a\}$	vector from origin of \underline{Y} axes to cm of \bar{m}_a when Counterweight is undeformed
$\{s_i\}$	see Equation (3.3b) (1)
$\{s_i^P\}$	value of $\{s_i\}$ for reservoir pipe on m_i (1)

$\{s\}$	vector from cm of m_i to Connecting-Structure attachment point on Laboratory $\tilde{(1)}$
$\{\bar{s}\}$	vector from cm of m_i to Connecting-Structure attachment point on Counterweight $\bar{a}^{(2)}$
t	time
t_U	time of update
t_{fU}	time at which fluid velocity is updated
$t_{\ell 03U}$	time at which ℓ_{03} is updated
t_{qLIM}	limiting torque of CMG gimbal motor
$t_{\omega LCU}$	time at which angular-velocity command is updated
$\{t_{\ell},\}$	vector from cm of m_i , to point on m_ℓ , where internal load is required $^{(1)\ell}$
$\{\bar{t}_{\ell},\}$	vector from cm of \bar{m}_ℓ , to point on \bar{m}_ℓ , where internal load is required
U_U	position update of moving mass
$\{U_j\}, \{U_j(0)\}$	position and initial position, respectively, of moving mass when Laboratory is undeformed $^{(3)}$ ($j = 1$ designates elevator, $j = 2$ designates balance mass)
$\{U_j\}_3$	third component of $\{U_j\}$
$\{u_i\}$	vector from cm of m_i to center line of pipe on m_i $^{(1)}$
$\{\Delta u_i\}$	$\{u_i\}$ at nominal pipe outlet less value at nominal pipe inlet $^{(1)} (6)$
$\{u_i^B\}, \{u_i^R\}$	$\{u_i\}$ at points R and B respectively (see Figure 3.6)
V	fluid velocity in pipe
V_U	command update of fluid velocity in pipe
$vel_{\ell 03 MAX}$	maximum value of $\dot{\ell}_{03}$
vel_{MAX}	maximum commanded velocity
$XJ1$	jet moment arm (see Figure 3.8)

\tilde{X}	mean axes for Laboratory
\tilde{X}^i	body axes in m_i with origin at cm of m_i
$\{X_A^i\}$	coordinates of accelerometer in \tilde{X}^i axes
$\{X_{SENS/CM}^{CMND}\}, \{X_{SENS/CM}\}$	commanded vector and actual vector, respectively, from Space Station center of mass to sensor (accelerometer) for use in balance mass control system (3)
\tilde{Y}	mean axes for Counterweight
\tilde{Y}^a	body axes in \bar{m}_a with origin at cm of \bar{m}_a
$\{\tilde{Y}^{a'}\}$ (a) $\{\tilde{Y}^{a'}\}$ (b)	see Section 3.3.4
\tilde{Z}	inertial coordinate system
$\bar{\tilde{z}}$	Connecting-Structure coordinate system fixed in \bar{m}_a
θ_G	CMG gimbal angle
$\{\theta\}$	Euler angles orienting the $\bar{\tilde{z}}$ axes with respect to the \tilde{Y}^a axes
$\Gamma ()$	cross-product function
$\gamma_A, \gamma_B, \gamma_T$	ratio of actual to critical damping coefficient of beam-type Connecting structure for axial, bending, and torsional vibration modes, respectively
$\{\gamma\}$	Euler angles locating \tilde{X} axes with respect to \tilde{Z} axes
$\{\delta\}$	deformation of Connecting Structure, $\{l\}-\{l_0\}$
$\{\eta\}$	Euler angles orienting \tilde{Y} axes with respect to \tilde{X} axes
$\{\eta^*\}$	$\{\eta\} = \begin{Bmatrix} \pi \\ 0 \\ 0 \end{Bmatrix}$
$\{\theta_i\}, \{\bar{\theta}_a\}$	angular deformation of m_i and \bar{m}_a , respectively
μ_j	mass of j^{th} moving mass
μ_{LEST}	estimated mass of elevator for use in balance mass control system
$\{\xi\}, \{\bar{\xi}\}$	model coordinates for Laboratory and Counterweight, respectively

$[\Pi ()]$	coordinate transformation matrix
ρ	mass density of fluid
τ_{BAL}	filter time constant used in balance mass control system (set to zero to bypass filter)
$\{\tau_E^*\}$	torque exerted by Laboratory on Connecting Structure at point E; vector is expressed in \bar{z} axes
$\{\tau_{\ell'}^i\}, \{\tau_{\ell'}^{-i}\}$	internal torque at point on $m_{\ell'}$, and $m_{\ell'}^{-i}$, expressed in $\underline{X}^{\ell'}$ and $\underline{Y}^{\ell'}$ axes, respectively
$\{\phi^*\}$	Euler angles expressing angular deformation of m^i relative to \bar{m}^a in \bar{z} axes
$\omega_{1C}, \omega_{1CU}$	commanded angular velocity and angular velocity update, respectively
$\omega_{1C BAL}$	minimum value of ω_{1C} at which balance mass control system is in operation
$\{\omega^X\}, \{\omega^Y\}$	angular velocity of \underline{X} and \underline{Y} axes, respectively (3) (4)
$\{\omega^{X^i}\}$	angular velocity of \underline{X}^i axes (1)

Footnotes:

- (1) The matrix form is expressed in the \underline{X}^i axes for the symbol pertaining to the Laboratory
- (2) The matrix form is expressed in the \underline{Y}^a axes for the symbol pertaining to the Counterweight
- (3) The matrix form is expressed in the \underline{X} axes for the symbol pertaining to the Laboratory
- (4) The matrix form is expressed in the \underline{Y} axes for the symbol pertaining to the Counterweight
- (5) The components of the vector are expressed in the \bar{z} axes
- (6) Nominal pipe outlet and inlet refers to outlet and inlet, respectively, when fluid velocity V is positive

3.3 COORDINATES USED IN THE PROBLEM

3.3.1 Coordinate Systems

Figure 3.1 illustrates the coordinates used in the problem. The axes of each coordinate system used are always denoted as the 1, 2, and 3 axes; for example, the \underline{Z} coordinate-system axes are Z_1 , Z_2 , and Z_3 . The main coordinate systems are the \underline{Z} axes, the \underline{X} axes and the \underline{Y} axes. The \underline{Z} axes are an inertially fixed reference coordinate system. The \underline{X} axes are a system of mean axes moving with the average motion of the Laboratory and are used as the reference system for elastic motion of the Laboratory. The \underline{Y} axes are similarly a set of mean axes for the Counterweight. The \underline{X} and \underline{Y} coordinate systems are also the global coordinate systems in which the modes of the Laboratory and Counterweight, respectively, have been computed.

The axes fixed in each mass m_i of the Laboratory are the \underline{X}^i axes with their origin at A_i , the mass center of m_i . The \underline{Y}^a axes are similarly a set of axes fixed in a typical Counterweight mass m_a .

The axes must be selected so that they meet the following orientation specifications when the system is undeformed. First, the \underline{X} axes are selected as any convenient reference system for the Laboratory. All of the \underline{X}^i axes must be parallel to \underline{X} . The \underline{Y} coordinate system is rotated 180° about the number 1 axis with respect to the \underline{X} coordinate system. Thus, the \underline{X} and \underline{Y} coordinates are parallel; however the Y_2 and Y_3 axes are opposite in direction to the X_2 and X_3 axes, respectively. The \underline{Y}^a axes are parallel to the \underline{Y} axes. These parallel requirements on the nominal positions of the coordinate systems do not limit the generality of the program since it is always possible to select the coordinates with the orientations required. In fact, if mass distribution and modal properties of a structure are available in other coordinate systems, the Phase I program may be used to transform these properties into the required coordinate systems.

3.3.2 Euler Angles

Each set of Euler angles is designated by a 1, 2, and a 3 angle; for example, the set of angles used for the coordinate transformation from the \underline{Z} to \underline{X} axes of Figure 3.1 are called $\{\gamma\}$ and the specific angles are γ_1 , γ_2 , γ_3 . The order of rotation is always as follows: the number 1 angle about the 1 axis, the number 2 angle about the carried number 2 axis, and the number

3 angle about the twice-carried number 3 axis. This is illustrated in Figure 3.3 for the angles $\{\gamma\}$. In the figure the \underline{X} axes have been translated so that their origin coincides with that of the \underline{Z} axes for the purpose of illustrating the method of orienting the \underline{X} axes with respect to the \underline{Z} axes. For brevity $\{\gamma\}$ is simply described as the "set of Euler angles orienting the \underline{X} axes relative to the \underline{Z} axes." Similar brief descriptions will be used to define the other Euler-angle sets.

3.3.3 Main Coordinates Used in the Problem

As indicated in Figure 3.1, $\{R\}$ and the Euler Angles $\{\gamma\}$ locate the \underline{X} axes in space, and $\{\bar{R}\}$ and $\{\eta\}$ locate the \underline{Y} axes with respect to the \underline{X} axes. The elastic linear and angular deflections are $\{q_i\}$ and $\{\theta_i\}$, respectively, for a typical mass point m_i ($i = 1, \dots, n$) on the Laboratory and $\{\bar{q}_a\}$ and $\{\bar{\theta}_a\}$ for a typical mass point \bar{m}_a ($a = 1, \dots, \bar{n}$) on the Counterweight. These elastic coordinates were linearized whenever there was an analytical or computational advantage to do so; however, the rigid-body coordinates $\{R\}$, $\{\gamma\}$, $\{\bar{R}\}$, and $\{\eta\}$ are not linearized so that large rigid-body motions may be studied. Instead of Euler-angle rates ($\{\dot{\gamma}\}$ and $\{\dot{\eta}\}$), angular velocities ($\{\omega^X\}$ and $\{\omega^Y\}$) of the \underline{X} and \underline{Y} axes, respectively, are used as coordinates. To improve numerical accuracy, the following perturbation parameters were used as integration coordinates in place of $\{\bar{R}\}$ and $\{\eta\}$:

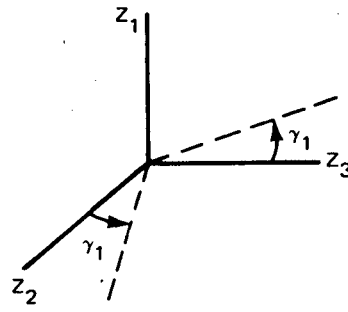
$$\{\Delta\bar{R}\} = \{\bar{R}\} - \{\bar{R}_0\} \quad (3.1)$$

$$\{\eta^*\} = \{\eta\} - \begin{Bmatrix} \pi \\ 0 \\ 0 \end{Bmatrix} \quad (3.2)$$

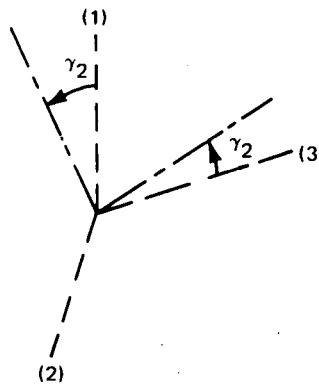
The derivatives of $\{R\}$, $\{\gamma\}$, $\{\omega^X\}$, the $\{q_i\}$'s, the $\{\theta_i\}$'s, $\{\Delta\bar{R}\}$, $\{\eta^*\}$, $\{\omega^Y\}$, the $\{\bar{q}_a\}$'s and the $\{\bar{\theta}_a\}$'s are obtained in the program and numerically integrated. In addition certain control-system variables are also integrated. The integrated variables are given in Equation (3.5).

3.3.4 Coordinates Used to Describe the Connecting-Structure Deformations

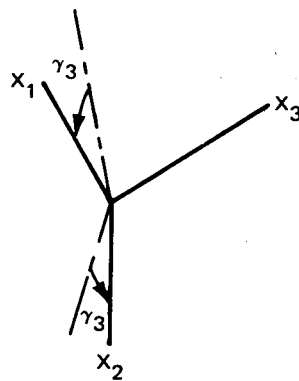
It is assumed that the Connecting-Structure is fastened to \bar{m}_a on the Counterweight and m_i on the Laboratory. (See Figure 3.1.) The \underline{z} axes which are fixed to \bar{m}_a at point \bar{E} are a convenient set of coordinates for expressing the Connecting-Structure deformations. The origin of these axes, point \bar{E} , is



FIRST ROTATION



SECOND ROTATION



THIRD ROTATION

Fig. 3.3 Typical Set of Euler Angles

located with respect to the center of mass of \bar{m}_a by specifying the vector $\{\bar{s}\}$.

The orientation of the \bar{z} axes is specified in the same manner as discussed in Section 2.3.1; i.e., by specifying the vectors $\{Y^{a'}\}_{(a)}$ and $\{Y^{a'}\}_{(b)}$ in the $\bar{Y}^{a'}$ coordinate system which is parallel to the \bar{Y}^a coordinate system but has its origin at \bar{E} . These vectors locate point (a) which is any point on the positive \bar{z}_3 axis and point (b) which is any point in the first quadrant of the $\bar{z}_1\bar{z}_3$ plane.

Point E is a reference point on m_i on the Laboratory. The vector $\{\ell\}$, from \bar{E} to E, may be thought of as the length vector of the Connecting-Structure. $\{\ell\}$ is expressed in the \bar{z} axes and is composed of the undeformed length $\{\ell_0\}$ plus the deformation $\{\delta\}$. During deployment and retraction maneuvers, $\{\ell_0\}$ is a specified function of time. When there is no deformation, a coordinate system \underline{z} may be imagined as fixed in m_i and parallel to \bar{z} . During deformation, the Euler angles expressing the angular deformation of the \underline{z} axes relative to the \bar{z} axes are $\{\phi^*\}$. Thus, the Connecting-Structure deformation is specified by the vectors $\{\delta\}$ and $\{\phi^*\}$.

3.4 ENGINEERING CONSIDERATIONS WHEN PREPARING DATA

The input data deck is to be constructed in accordance with the procedure described in Section 3.5. Special engineering considerations are discussed in this section.

3.4.1 Constraint Options

Constraint options may be used to run the program with portions of the vehicle rigid even though the available data deck was prepared for a flexible vehicle. This enables the analyst to compare the more complex flexible-vehicle results with simpler rigid-body results. It is possible to:

- rigidize the Laboratory
- rigidize the Counterweight
- rigidize the entire Space Station
- rigidize both the Laboratory and the Counterweight while maintaining a flexible Connecting Structure.

3.4.2 Basic Input Data for the Laboratory

The following basic input data is required to define the mass and flexibility characteristics of the Laboratory:

- Coordinates of the center of mass A_i of each mass point m_i in the \tilde{X} coordinate when there is no deformation. (See Figure 3.1).
- Mass m_i of each mass point and the inertia matrix $[I_i]$ in local coordinates X^i .
- Elastic frequencies and mode shapes relative to the \tilde{X} coordinate system. The free-free modes are required and the six rigid-body modes must be omitted. The modes must be orthogonal. Each mode must contain the three translational coordinates and the three rotational coordinates, in sequence, for each mass point. If the moment of inertia at a mass point is neglected and there is no torque at that mass point, the rotational coordinates are not used; thus, the corresponding field on the data card may be left blank if desired.

As indicated in Section 2.6, it is possible to generate all of the above information with the Phase I computer program, and, if desired, connect the two programs so that the information is passed directly to the Phase II program. This information may also be generated elsewhere and input directly into the Phase II computer program.

3.4.3 Basic Input Data for the Counterweight

The basic input data for the Counterweight is analogous to that described above for the Laboratory, and the above comments are also applicable to the Counterweight data. The modes and inertia matrices for the Counterweight must be expressed in the \underline{Y} and \underline{Y}^a axes, respectively (see Figure 3.1).

3.4.4 Initial Conditions and Mean Axes

While the positions of the \underline{X} axes for the Laboratory are arbitrary when there is no deformation, when the structure is deformed the coordinates move with the mean, or rigid-body, motion of the Laboratory. The program computes the position and rate of movement of these axes and prints out this information as $\{R\}$, $\{\gamma\}$, $\{\dot{R}\}$, $\{\omega^X\}$. When the system is initially deformed it would be a burden for the user to average the deformation and deformation rates and compute the initial position and rate of movement of the mean axes. To avoid this burden, the user may supply the initial deformation data ($\{q_i\}$, $\{\theta_i\}$, $\{\dot{q}_i\}$, and $\{\dot{\theta}_i\}$) in terms of any neighboring axes (defined by the initial values of $\{R\}$, $\{\gamma\}$, $\{\dot{R}\}$ and $\{\omega^X\}$) and the program will compute the initial position and rate of the mean axes and convert the initial deformation data to these axes. For this reason the values of $\{R\}$, $\{\gamma\}$, $\{\dot{R}\}$, $\{\omega^X\}$, $\{q_i\}$, $\{\theta_i\}$, $\{\dot{q}_i\}$, and $\{\dot{\theta}_i\}$ (for $i=1, \dots, n$) that are printed out at $t=0$ may not agree with the values that are input to the program.

The Counterweight is located relative to the Laboratory, at $t=0$, by specifying the initial undeformed location of the Connecting Structure its deformation, ($\{\delta\}$ and $\{\phi^*\}$) and the deformation rates $\{\dot{\delta}\}$ and $\{\dot{\phi}^*\}$. The elastic coordinates of the Counterweight $\{\bar{q}_a\}$, $\{\bar{\theta}_a\}$ and their rates $\{\dot{\bar{q}}_a\}$, and $\{\dot{\bar{\theta}}_a\}$ for $a=1, \dots, \bar{n}$ are initially described relative to the \underline{Y} axes. The \underline{Y} axes are a set of mean axes for the Counterweight, and, as is the case for the \underline{X} axes, the program will initially recompute the location of the \underline{Y} axes and transform the elastic coordinates.

3.4.5 Damping in the Laboratory and Counterweight Structures

Modal damping is assumed. The ratio of the damping coefficient to the critical damping coefficient is specified for each mode.

3.4.6 Fluid Motion

The dynamic effect of fluid being pumped through a piping system may be studied using this program. It is assumed that the pipes terminate in two

reservoirs, one called the emptying reservoir and the other called the filling reservoir. (See Figure 3.4A.) These reservoirs are emptying and filling, respectively, when the fluid velocity V is positive; however if the fluid reverses direction, the emptying reservoir would be filling and vice versa so that the names of the reservoirs are reference designations only.

The first step in preparing the fluids data is to separate the fluid system into its elements. To do this, control surfaces are drawn about each structural mass point associated with fluid motion as shown in Figure 3.4A. The fluid contained within each control surface is assumed to vibrate with the associated mass point as shown in Figure 3.4B, in exaggerated form; thus, the selection of the control surface boundaries involves judgement of the user. Each control surface will contain either a through pipe (as shown in Figure 3.5) or a reservoir and reservoir pipe (as shown in Figure 3.6).

3.4.6.1 Through Pipe

For each through pipe, the user must specify the mass distribution and geometrical properties of the fluid in the through pipe. Some of these terms, such as \vec{S}_i , require discussion. \vec{S}_i is defined as follows:

$$\vec{S}_i = \int \vec{u}' dm \quad (3.3a)$$

where dm is a differential fluid mass on m_i , \vec{u}' is the vector from A_i to dm and the integral is taken over all of the fluid in the through pipe. Alternately, the following formula may be used to evaluate \vec{S}_i :

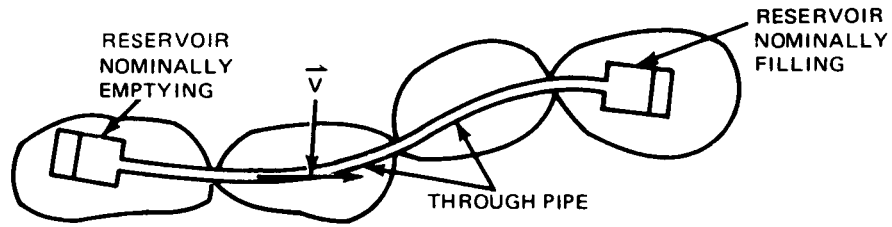
$$\vec{S}_i = \rho A \int \vec{u} ds \quad (3.3b)$$

where ds is the differential arc length along the centerline as shown in Figure 3.5, \vec{u} is the value of \vec{u}' on the centerline, and the integral is taken from the nominal inlet to the nominal outlet. It may also be helpful to notice that \vec{S}_i is simply equal to the mass of the fluid times the vector from A_i to the cm of the fluid.

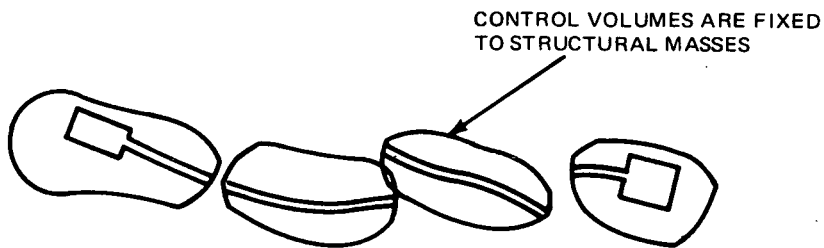
Another vector required as input data is:

$$\vec{G}_i = \int_{\text{NOMINAL INLET}}^{\text{NOMINAL OUTLET}} \vec{u} \times d\vec{u} \quad (3.4a)$$

Note: Only two intermediate masses containing through pipes are shown; however, the analysis was done for an arbitrary number of masses

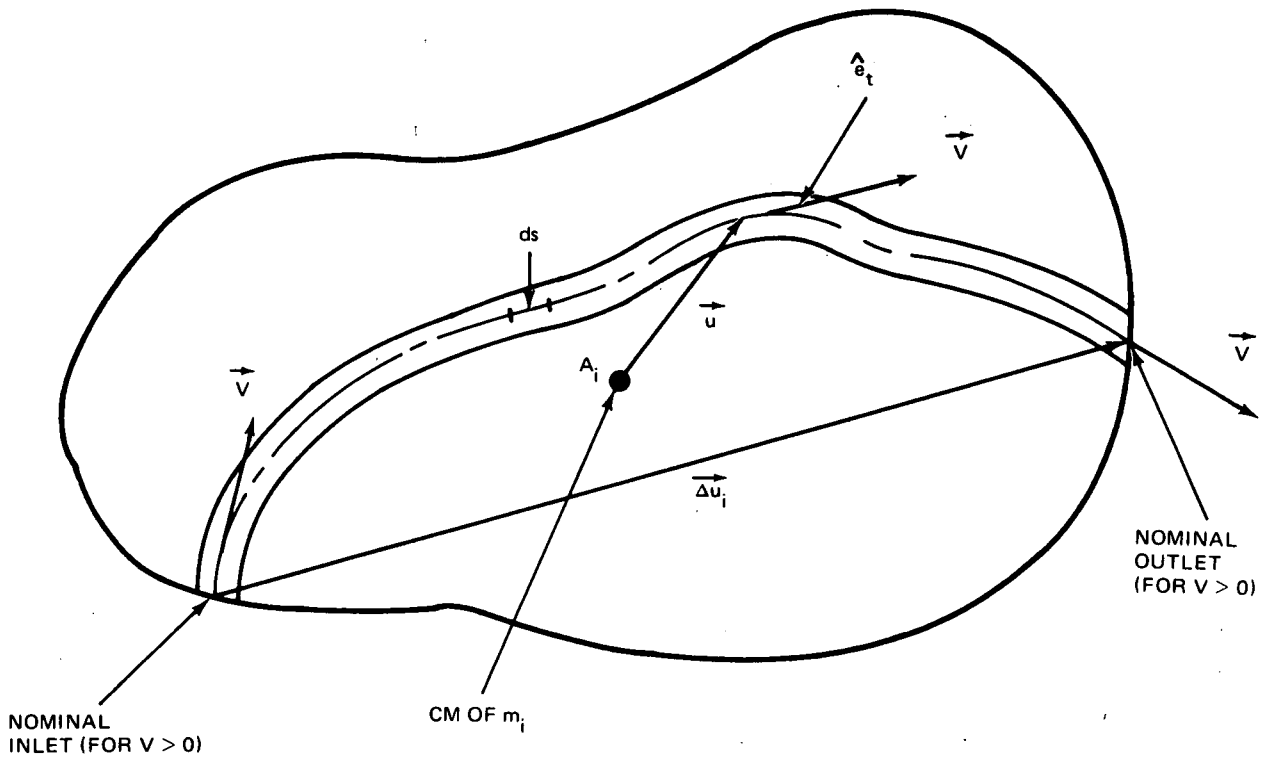


(A) Undeformed System

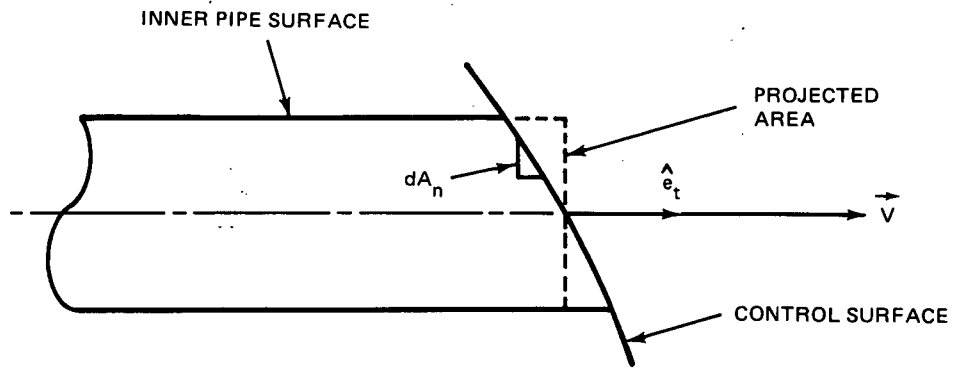


(B) Deformed System

Fig. 3.4 Fluid Control-Volume Idealization Used for Computing Rates of Change of Linear and Angular Momenta

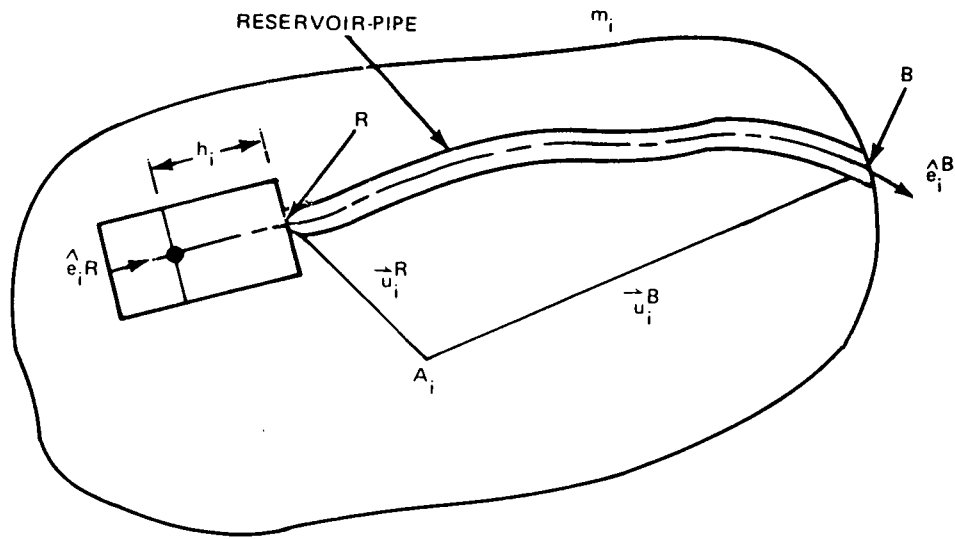


(A) FLUID CONTAINED WITHIN CONTROL SURFACE

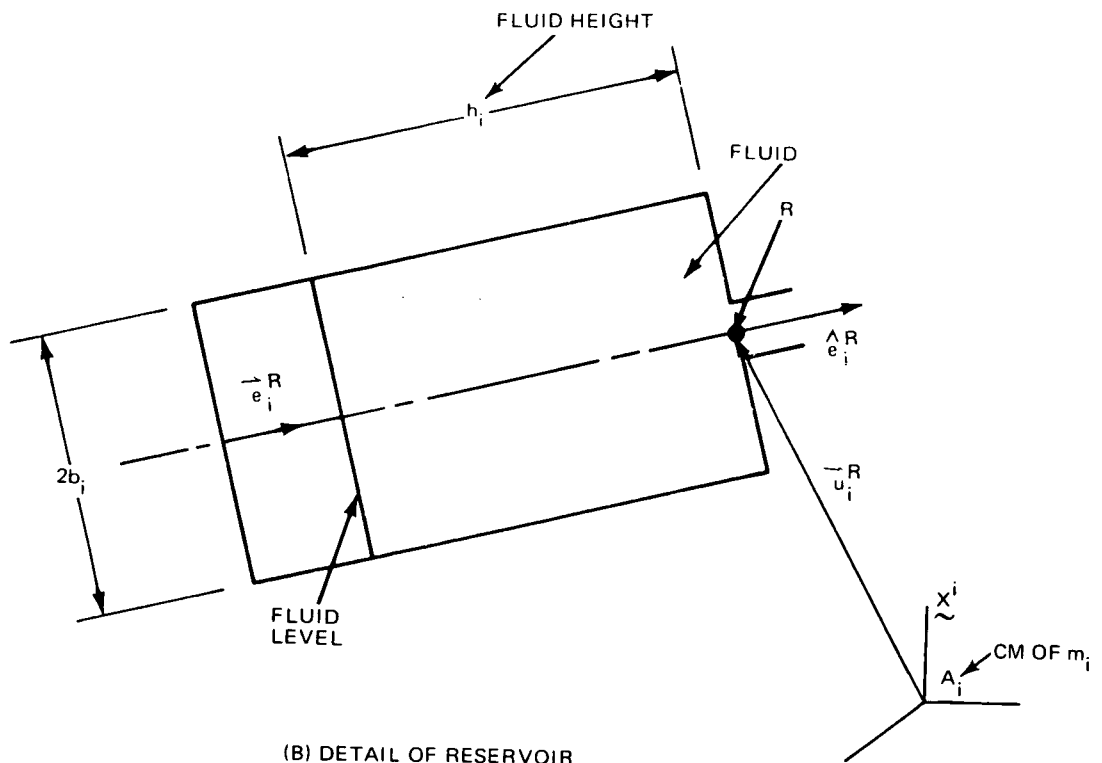


(B) DETAIL OF FLUID CONTROL-SURFACE INTERSECTION

Fig. 3.5 Mass Containing a Through Pipe



(A) RESERVOIR WITH ASSOCIATED PIPE SECTION



(B) DETAIL OF RESERVOIR

Fig. 3.6 Structural Mass Containing a Reservoir

\vec{G}_1 can be evaluated by expanding \vec{u} into components or by noting that \vec{G}_1 is the following function of the area A_p swept out by \vec{u} (see Figure 3.7):

$$\vec{G}_1 = 2 \int_{\text{NOMINAL INLET}}^{\text{NOMINAL OUTLET}} \hat{e}_p dA_p \quad (3.4b)$$

where \hat{e}_p is the unit normal vector which is perpendicular to the plane of \vec{u} and $d\vec{u}$ and directed along $\vec{u} \times d\vec{u}$. When the surface swept out by \vec{u} is a plane, \hat{e}_p is constant and the evaluation of Equation (3.4b) is particularly simple.

The matrix $[J_i]$ is defined as the moment-of-inertia matrix of the elements dA_n shown in Figure 3.5b about point A_i in X_i axes. As an approximation, the moment of inertia of the projected area shown in the illustration could be used. The diagonal elements of $[J_i]$ are the moments of inertia and the off-diagonal elements are the negatives of the cross products of inertia.

3.4.6.2 Reservoirs and Reservoir-Pipes

The reservoir is assumed to be cylindrical with radius b_1 . The pipe-reservoir connection is assumed to be along the reservoir axis. The user specifies the maximum and minimum fluid heights in each reservoir. If either of these limits is reached, the pump is assumed to stop, and no further fluid flow occurs in the problem. Input data for the pump command subroutine, which specifies the fluid velocity V as a function of time, is discussed in Section 3.4.9.2.2.

Much of the input data for each of the two masses containing a reservoir and reservoir pipe is similar to that described in the previous section for a through pipe. For example, $[I_i^P]$ and \vec{S}_i^P denote the values of $[I_i^f]$ and \vec{S}_i^f for the reservoir pipe shown in Figure 3.6A.

3.4.7 Moving Masses

There may be up to eight moving masses present on the Laboratory. These are designated $\mu_1, \mu_2, \dots, \mu_8$. The subroutines that specify the motion of these masses are designed so that they may easily be replaced by the user. A subroutine, discussed in Section 3.4.9.2.1, is supplied with the program so that the user may specify a variety of three-dimensional motions for each mass other than μ_2 . μ_2 is a balance mass which is designed to balance the motion of an elevator along axis X_3 . The motion of μ_2 is determined by the balance mass control system which is discussed in Section 3.4.9.2.6.

D

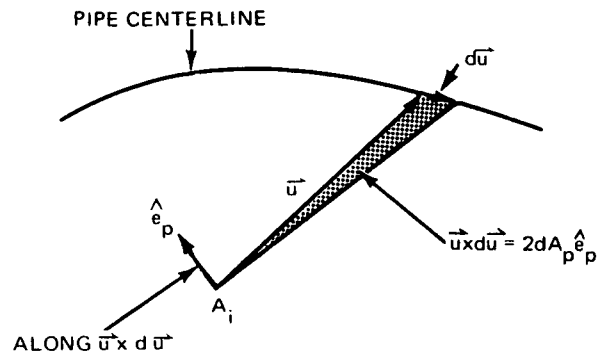


Fig. 3.7 Diagram for the Evaluation of G_i

The motion due to structural deformation is added to the rigid-body motion of each moving mass. In order to determine this structural deformation when the moving mass is between structural mass points (nodes), an averaging procedure is used in the program. The elastic motion of the moving mass is approximated as the weighted average of the motion of those nodes that (in the user's judgement) influence the motion of the moving mass. The weighted average has the following characteristics:

- As a moving mass approaches an influencing node, its motion will approach the motion of that node.
- The greater the distance a moving mass is from a node, the smaller the influence of that node in the averaging procedure.

The set of influencing nodes could differ for each mass point and could vary with time as the moving mass moves through different regions of the Laboratory. This set of node numbers should be programmed into Subroutine LOOK (described in Appendix B5) in table look-up form; i.e., as tables of node numbers versus time. In the version of LOOK supplied with the program, the influencing nodes are 1 through 8 for each moving mass point and remain constant with time.

3.4.8 Internal Loads

The facility is provided to compute internal structural loads between modules or at any other point where the structure (Laboratory or Counterweight) can be separated into two free bodies. This is accomplished by separating the structure at the load-computation point and considering one portion of the structure as a free body. The load applied by the free body is then computed by taking the resultant of all of the inertia and applied loads on the free body. Since Connecting-Structure loads are included in the equations as external loads, the remaining portion of the Laboratory (or Counterweight) may also be used as the free body. Of course, results which are opposite in sign would then be obtained. The index numbers of all mass points in the free body must be supplied as input data in addition to the coordinate vector $\{t_{\ell'}\}$ ($\{\bar{t}_{\ell'}\}$ on the Counterweight) to the load-computation point. $\{t_{\ell'}\}$ is stated in the local $\tilde{X}^{\ell'}$ coordinate system which is fixed in $m_{\ell'}$, the mass containing the load-computation point. The forces $\{f'_{\ell'}\}$ and torques $\{\tau'_{\ell'}\}$ for the Laboratory are expressed in the \tilde{X} axes, and the forces $\{\bar{f}_{\ell'}\}$ and torques $\{\bar{\tau}_{\ell'}\}$ for the Counterweight are expressed in the \tilde{Y} axes. If the option to compute structural loads is exercised, the program will also print the structural loads applied by the Connecting Structure

to the Laboratory (projected onto \tilde{X} axes) and the Counterweight (projected onto \tilde{Y} axes).

The internal structural loads are neither computed nor printed at $t=0$ for the reason discussed in Section 4.5 of Volume I.

3.4.9 Data for Replaceable Subroutines

The physical properties of the Connecting Structure, the control systems, the motion of the moving masses, and the externally applied forces have been programmed in subroutines which were designed to be easily replaced so that different classes of problems could be studied. Details on replacing these subroutines are provided in Appendix B5. The input data required for these subroutines will now be described.

3.4.9.1 Beam-Type Connecting Structure

The Connecting-Structure subroutine computes the force and torque applied by the Laboratory on the Connecting Structure in the \tilde{z} coordinate system. The Connecting Structure is assumed massless, and the program uses equilibrium to compute the loads on the Counterweight. The subroutine supplied with the program contains the equations for a circular beam fixed at each end. During deployment or retraction maneuvers it is simply assumed that the undeformed beam length increases or decreases, and the beam stiffness and damping coefficients are recomputed every cycle based on the updated beam length. Some of the stiffness coefficients go to infinity as the beam length l_0 approaches zero. While this occurs in theory, in practice fixed supports are never perfectly rigid; thus there is always some flexibility. To approximately account for this flexibility and to avoid the numerical problems associated with high stiffnesses, a minimum length, $l_{0 \min}$, is input to the program. Whenever l_0 is less than $l_{0 \min}$, the program uses $l_{0 \min}$ to compute the stiffness and damping coefficients.

Damping is based on a simple model of the Space Station. The user inputs the desired proportion of critical damping, and the mass properties of a rigid Laboratory and Counterweight. The program computes the critical damping of this model for each mode, multiplies the critical modal damping coefficients by the damping ratios and transforms the modal damping matrix to a physical damping matrix. This latter matrix is used in the program. Since the beam is circular, the damping coefficients should be the same for in-plane and out-of-plane bending; therefore the two transverse moments of inertia of each end body in the simple

model must be identical. It is suggested that the average of the two values be used for each body.

3.4.9.2 General Data for Control Systems

The control system subroutines compute the forces and torques applied by the control system actuators to mass points of the Laboratory and/or the Counterweight. In addition, they may determine the motion of moving rigid masses, the undeformed geometry of the Connecting Structure, and the velocity of the fluid being pumped through the Laboratory.

In the control-system subroutines supplied with the program, there are sixteen jets. These are arranged to control spin rate and nonspinning vehicle attitude for the demonstration Space-Station model discussed in Section 6 of Volume I. As indicated in Figure 3.8, there are two clusters of four jets each located on mass point 1 (m_1) of the Laboratory and two clusters of four jets located on mass point 5 of the Laboratory. The jet thrust f_{jet} (which has the same value for each jet) and the jet moment arm $XJ1$ are input data. The jet assignments are indicated in the table on Figure 3.8. Twice as many jets are used for spin control about axis 1 than for attitude control.

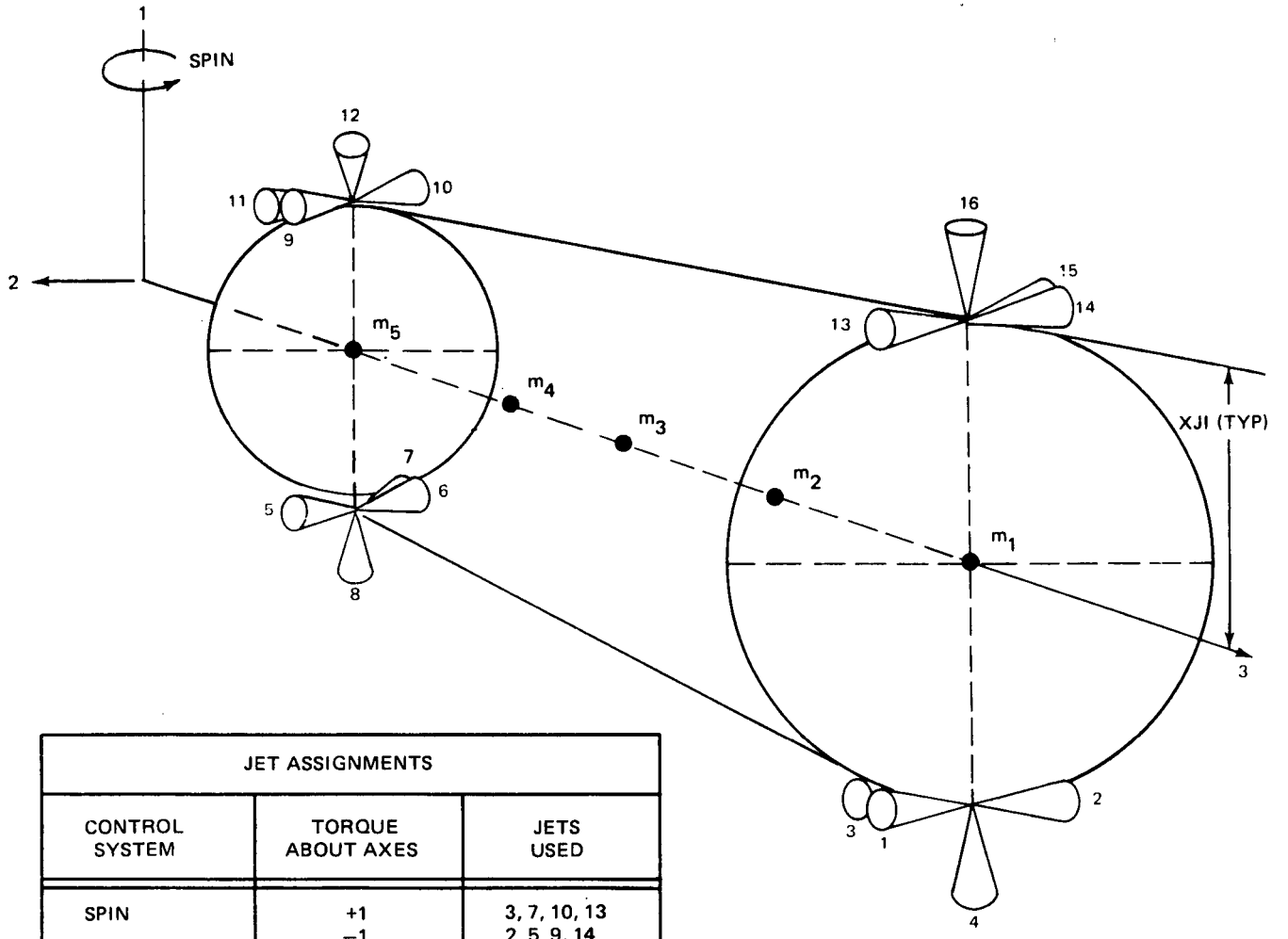
A sensor package may be located at any mass point i_s on the Laboratory. The sensor is assumed to measure the angular position, angular velocity, and angular acceleration as well as the linear acceleration of mass i_s .

The controls subroutine group consists of command routines and control routines. A command routine is used to specify a certain motion, whereas a controls routine is used to achieve that motion. For example, if it is desired to vary the vehicle's spin rate at a prespecified function of time, a command routine would be used to generate the desired spin speed as a function of time. A controls routine might then fire jets in order to achieve the commanded angular velocity. First, the command routines and then the control routines will be described.

3.4.9.2.1 Position Command (For Deployment and Moving Masses)

The same law is used to command the undeformed position of the Counterweight relative to the Laboratory (i.e., third component of $\{\ell_0\}$), and the position of moving masses 1, and 3 through 8 ($\{U_i\}$ with $i=1, 3, 4, \dots, 8$).

The position-command law is illustrated in Figures 3.9 and 3.10. The input data for developing the command consists of the initial position, position update,



JET ASSIGNMENTS		
CONTROL SYSTEM	TORQUE ABOUT AXES	JETS USED
SPIN	+1	3, 7, 10, 13
	-1	2, 5, 9, 14
ATTITUDE	+1	10, 13
	-1	9, 14
	+2	4, 12
	-2	8, 16
	+3	1, 15
	-3	6, 11

NOTE: THE POWER BOOM IS NOT SHOWN

Fig. 3.8 Jet Configuration on Laboratory Core Module

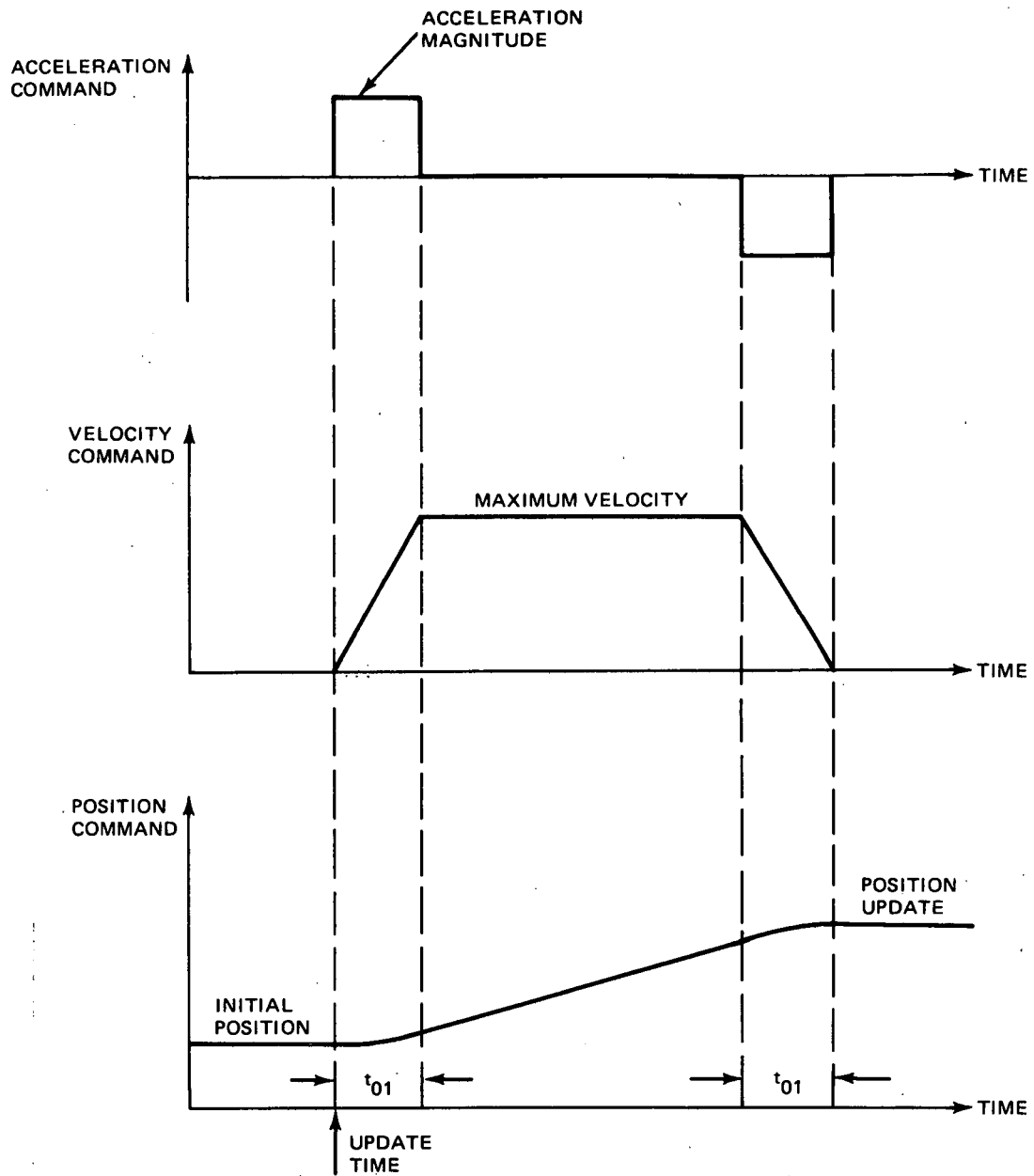


Figure 3.9 Position Command Law for Case Where Velocity Command Achieves Maximum Velocity

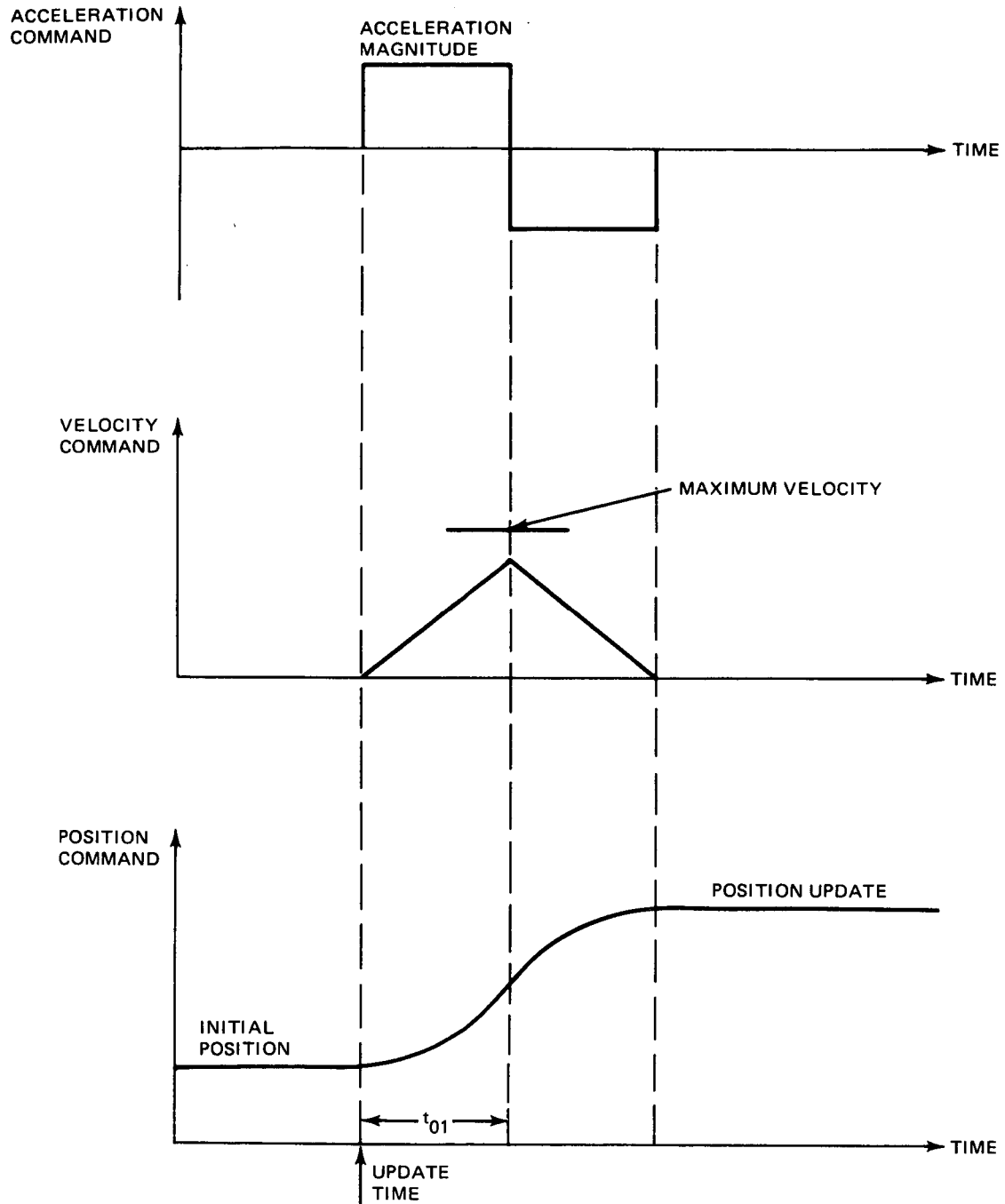


Fig. 3.10 Position Command Law for Case Where Velocity Command Does Not Achieve Maximum Velocity

update time, magnitude of acceleration, and maximum velocity. For the case of moving masses, a different set of input data may be used for each axis. In Figure 3.9 the motion begins at the update time when a constant acceleration occurs until the maximum velocity is achieved. Then cruising occurs at the maximum velocity until deceleration occurs at the negative of the acceleration magnitude.

If the position update is close to the initial position, the maximum velocity is never achieved. In this case the command law is illustrated in Figure 3.10.

In the event that the position update is less than the initial position the negatives of the motions illustrated in Figures 3.9 and 3.10 occur.

The user must always select a numerical integration time interval that is less than the time increment t_{01} illustrated in Figures 3.9 and 3.10. t_{01} may be computed as follows:

$$t_{01} = \text{smaller of } \left\{ \begin{array}{l} \frac{\text{maximum velocity}}{\text{acceleration magnitude}} \\ \sqrt{\frac{|\text{position update} - \text{initial position}|}{\text{acceleration magnitude}}} \end{array} \right.$$

The acceleration magnitude must not be set to zero. If it is desired to maintain a constant position command throughout the run, the user should input an update time which is greater than the final time designating the end of the run.

3.4.9.2.2 Velocity Command (For Spin Speed and Fluid Velocity)

The same law is used to command the spin speed of the Space Station and the fluid velocity. This law is illustrated in Figure 3.11. The required input data consists of the initial velocity, the velocity update, the update time, and the acceleration magnitude.

The selected numerical-integration time interval must always be less than t_{01} of Figure 3.11. t_{01} may be computed as follows:

$$t_{01} = \frac{|\text{update velocity} - \text{initial velocity}|}{\text{acceleration command}}$$

Another precaution that must be taken is never to set the acceleration command to zero. If it is desired to hold the velocity command constant, the user should set the update time greater than the final (end-of-run) time.

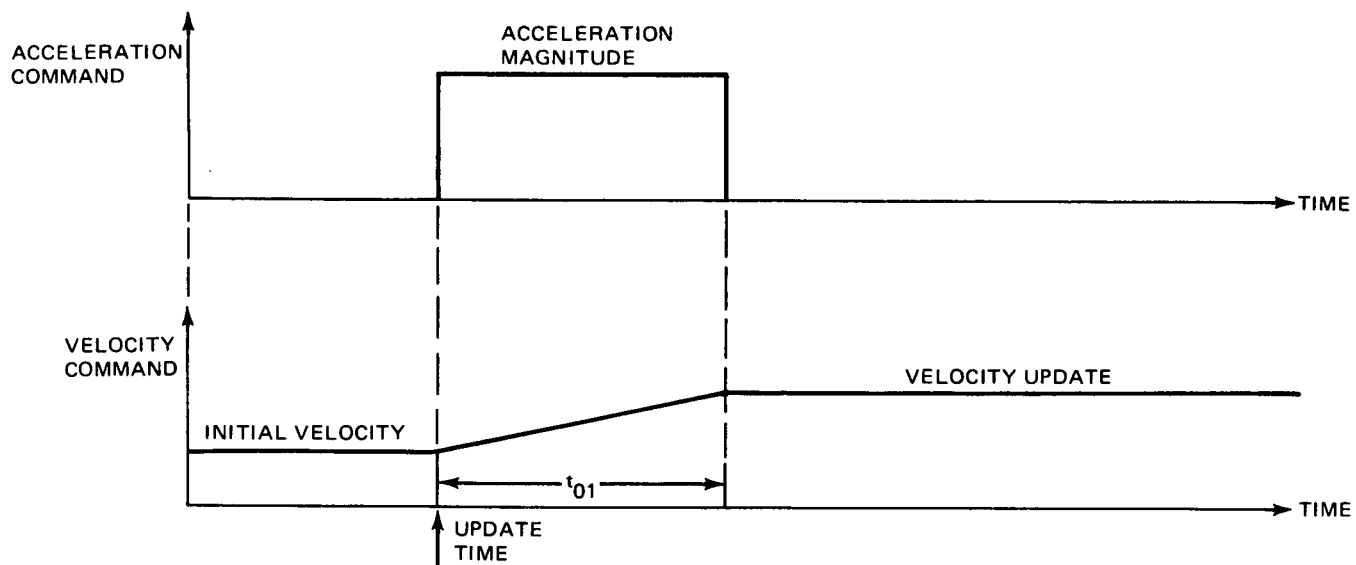


Fig. 3.11 Velocity Command Law

3.4.9.2.3 Attitude Control

The attitude control system is designed to drive the attitude angles $\{\gamma\}$ to zero for the case of the nonrotating Space Station. The same control law is used for each axis. This law is illustrated in Figure 3.12.

3.4.9.2.4 Spin Control

A hysteresis type spin control law is used. This law is illustrated in Figure 3.13.

3.4.9.2.5 Wobble Control

A CMG control law known as the 90° h-lag law is used to eliminate gyroscopic wobble from the rotating Space Station.* The CMG is assumed to be located on the same mass (m_{i_s}) as the sensor package. There are two modes of control, gimbal-angle control and gimbal-angle-rate control. The CMG angle law is used for wobble control. When the wobble drops below a predetermined threshold, wobble control is ended. The CMG angle-rate law is then used to rotate the gimbal relative to the Space Station at the negative of component 1 of the Space Station angular velocity; thus the gimbal angular velocity is approximately zero in inertial space. The CMG gimbal angle law and the CMG angle-rate law are illustrated in Figures 3.14 and 3.15, respectively.

3.4.9.2.6 Balance Mass Control

The balance mass control system is used to balance mass shifts along the long axis of the Space Station (i.e., the X_3 axis of Figure 3.1). For example, mass shifts would occur due to the motion of a freight elevator. An accelerometer senses the acceleration at a point on mass i_s . The control system moves the balance mass until the centrifugal acceleration at the sensor is equal to a commanded value. The commanded vector from the Space-Station center of mass to the accelerometer $\{X_{SENS/CM}^{CMND}\}$ is input data. The user should include the elastic deformation of the structure when determining this vector. One method of determining this deformation is discussed in Section 3.4.10. A block diagram of the control system is illustrated in Figure 3.16.

3.4.9.3 Supplementary Loads

The user may program any set of loads as a function of time on the Laboratory and the Counterweight into subroutine SUPPLM. The equation for the result-

 * The spin speed must be greater than .02 rad/sec for the wobble control system to turn on.

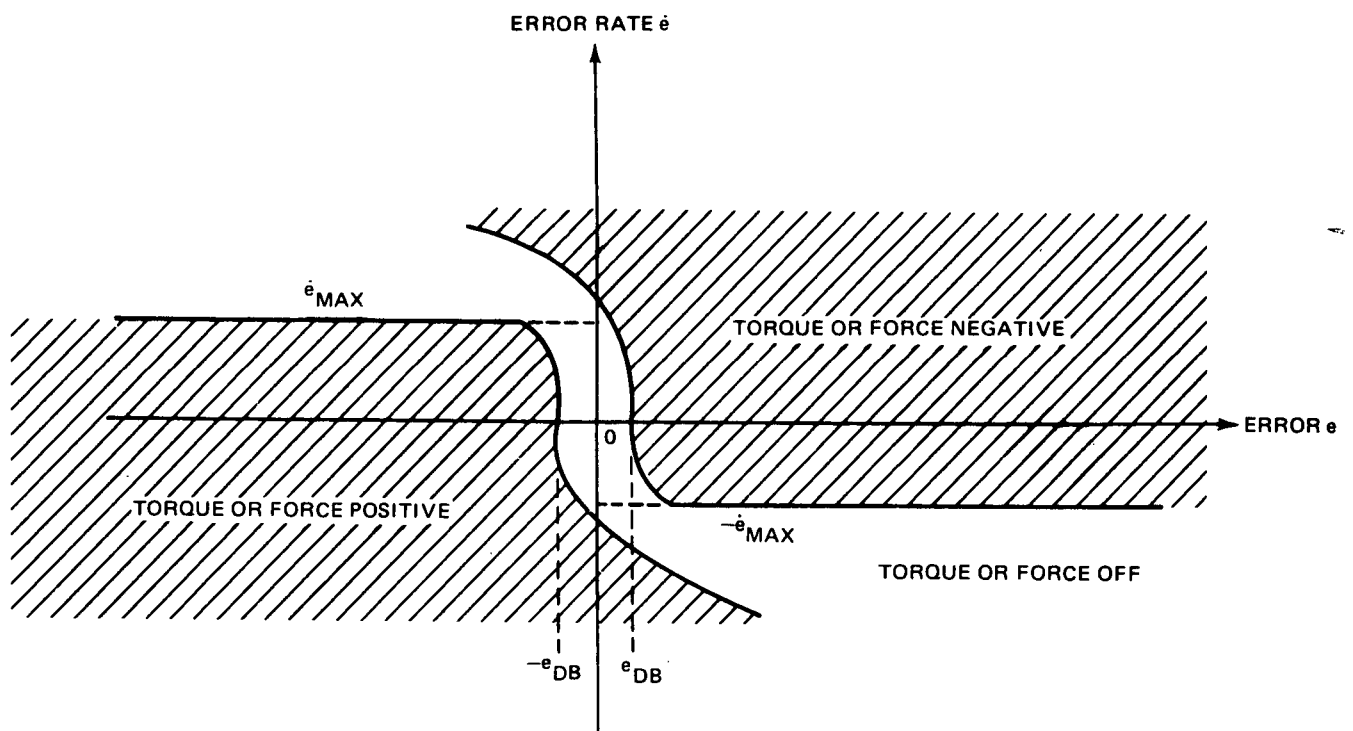
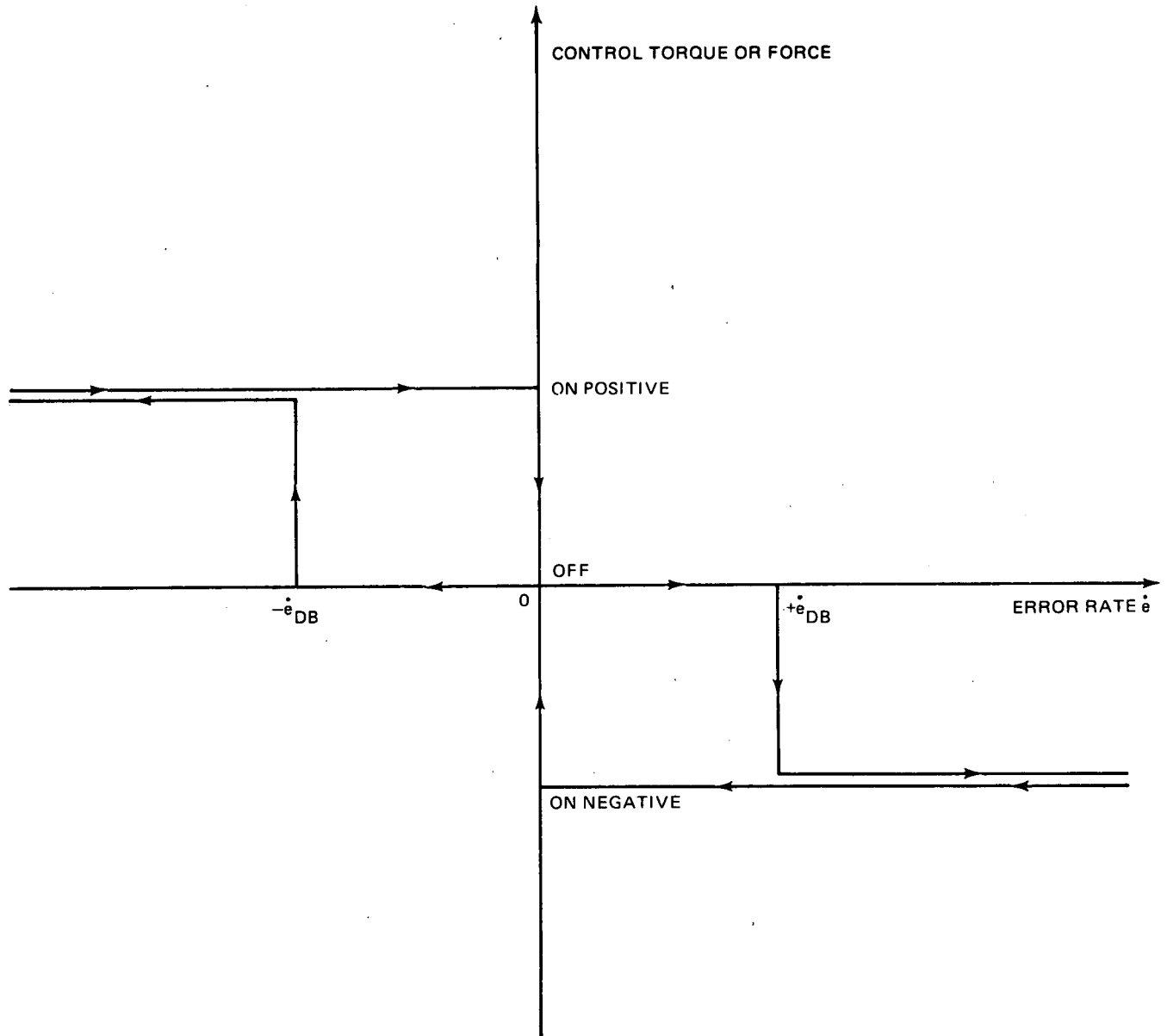


Fig. 3.12 Position Control

**Fig. 3.13 Velocity Control**

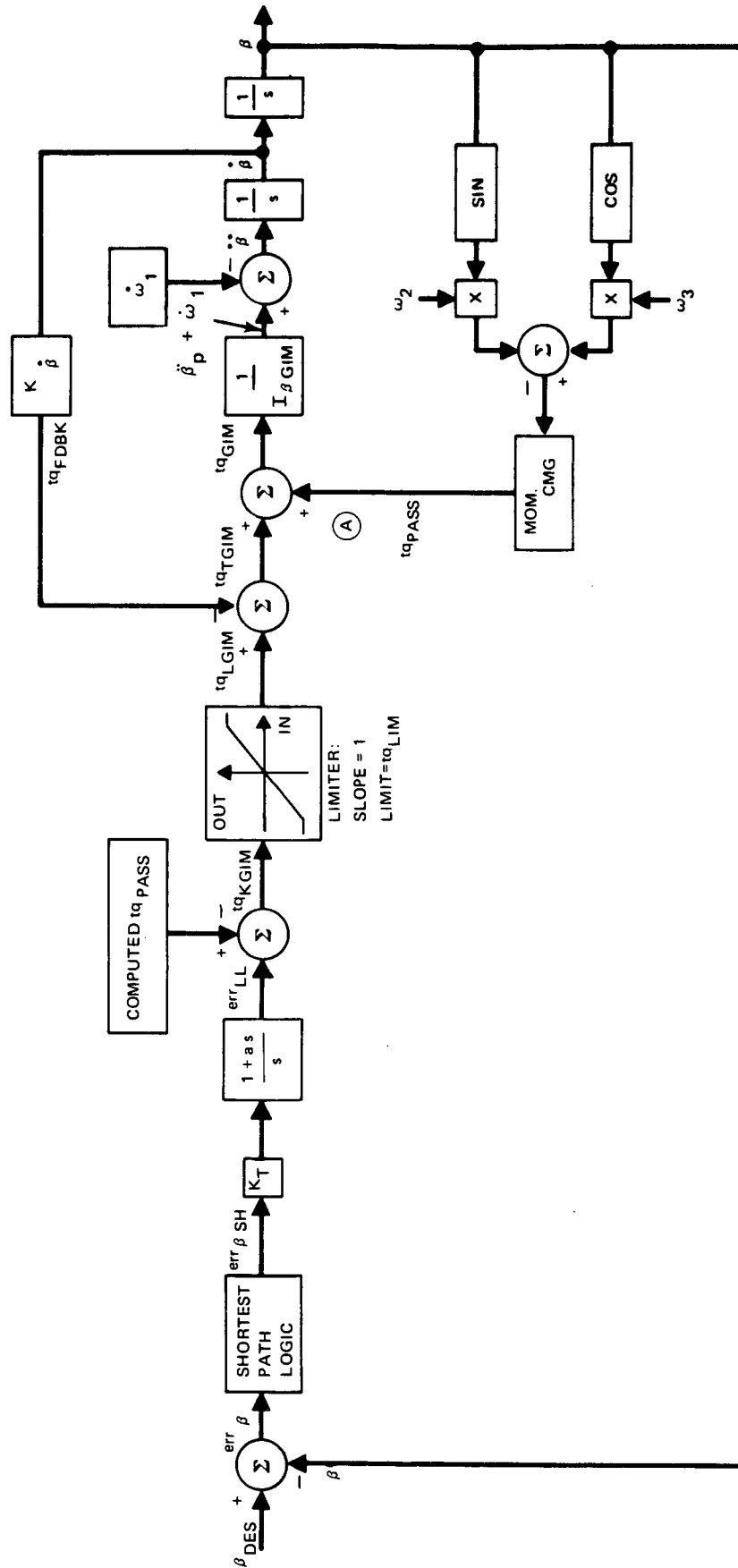


Fig. 3.14 CMG Gimbal Angle Control System

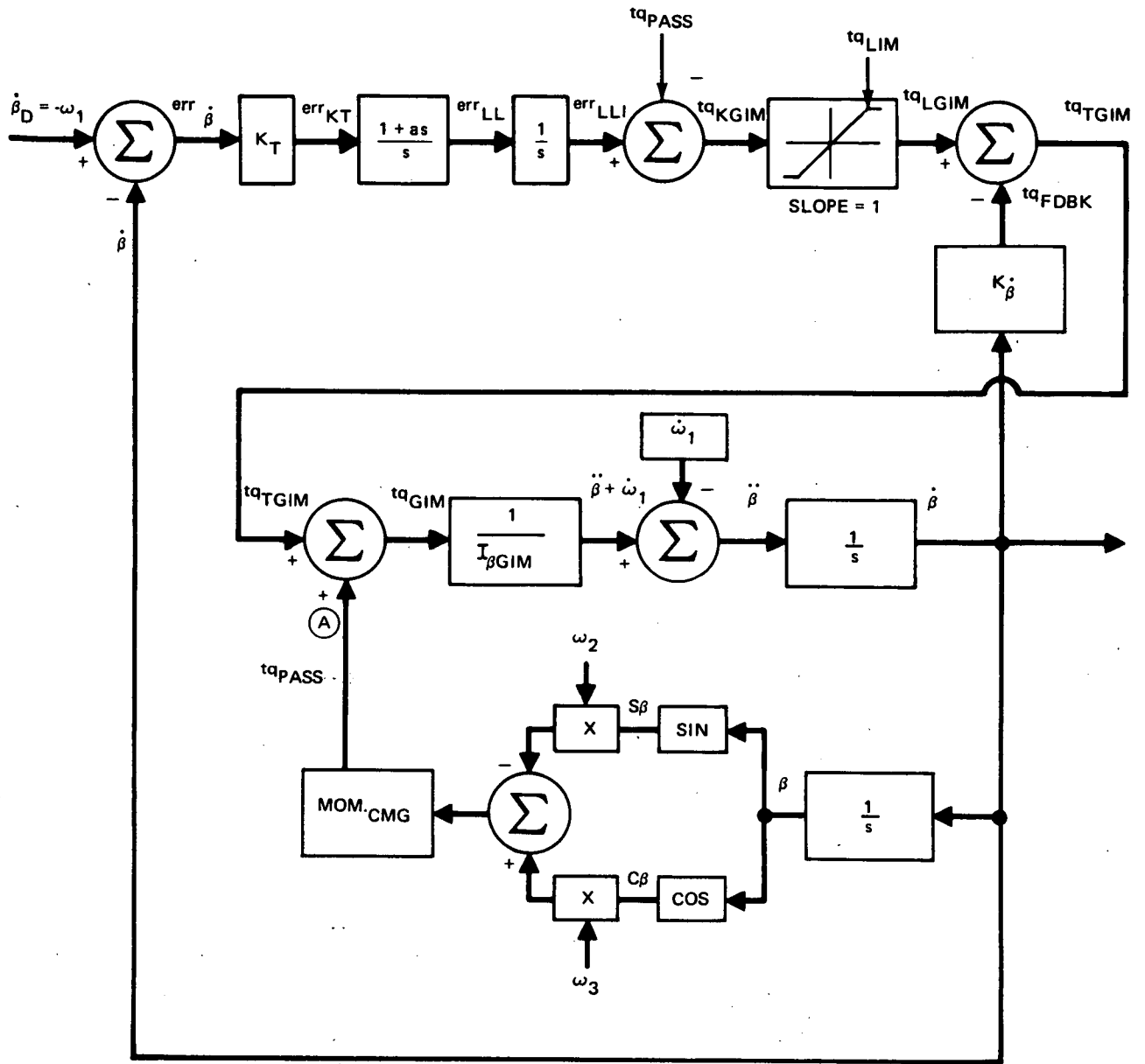


Fig. 3.15 CMG Gimbal Angle Rate Control System

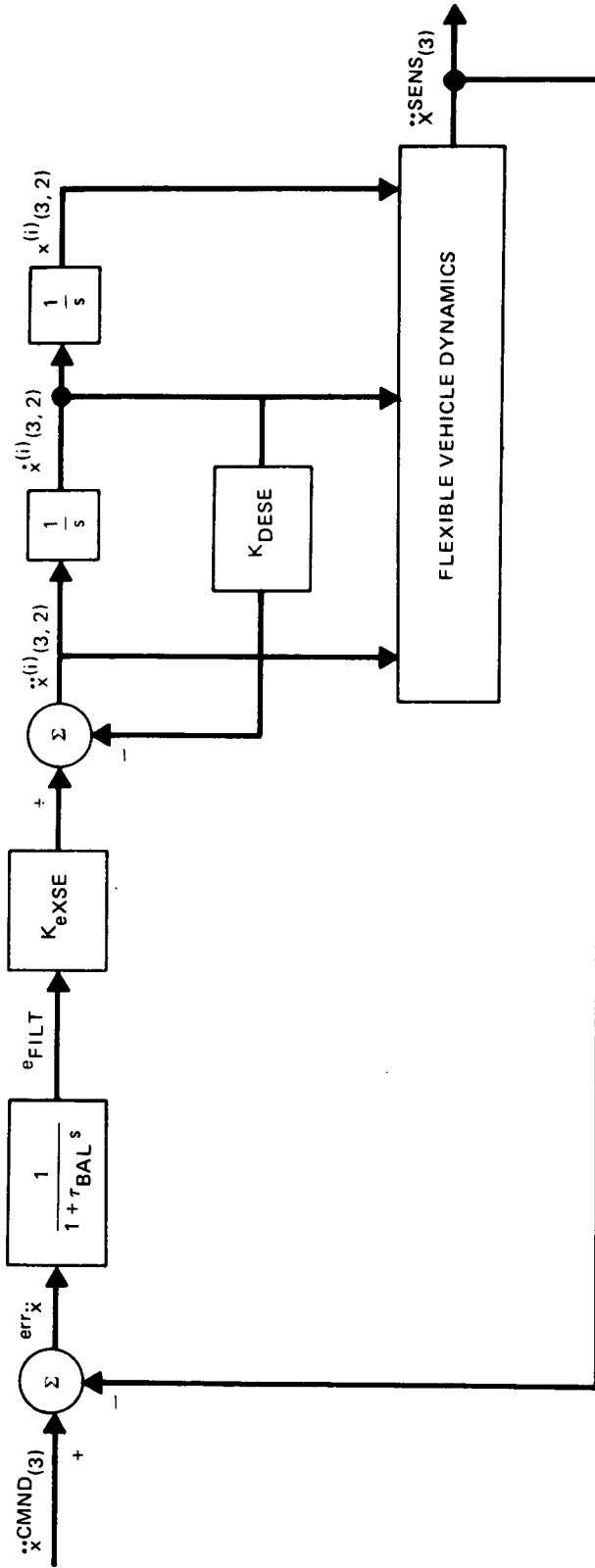


Fig. 3.16 Space-Station Center-of-Mass Position Control System for Flexible Vehicle Idealization

ant force $\{f_s^i\}$ and the resultant torque $\{\tau_s^i\}$ on each mass point m_i of the Laboratory must be programmed. Also, the resultant force $\{\bar{f}_s^a\}$ and $\{\bar{\tau}_s^a\}$ on each mass point \bar{m}_a of the Counterweight must be programmed.

3.4.10 Determining Quiescent Deflections

When the Space Station is in a state of pure spin with no vibration, constant elastic deflections will occur because of the centrifugal forces. This state of motion is known as the quiescent state. In most rotating problems the user will want to set the initial deflections equal to the quiescent deflections or equal to some perturbation about these values. One way of determining the quiescent deflections is to make a short preliminary run with 80% of critical damping in the Laboratory, the Counterweight, and the Connecting Structure. The deflections will quickly damp out to their quiescent values.

3.5 PROGRAM LIMITATIONS

- 1) A maximum of 20 modes may be used to represent the elastic motion of the Laboratory
- 2) A maximum of 20 modes may be used to represent the elastic motion of the Counterweight
- 3) There is a maximum of 100 mass points on the Laboratory
- 4) There is a maximum of 100 mass points on the Counterweight
- 5) There is a maximum of 8 moving masses present
- 6) A maximum of 30 masses may contain pipe segments
- 7) There is a maximum of 16 points on the Laboratory at which internal loads may be printed
- 8) There is a maximum of 16 points on the Counterweight at which internal loads may be printed

3.6 INSTRUCTIONS FOR SETTING UP INPUT-DATA DECK FOR PHASE II PROGRAMTYPE I

Initial Card - To be supplied at the beginning of the group of multiple runs.

Supply the number of runs to be made, plotting clue [(2I2) format]

plotting clue = $\begin{cases} 0 & \text{if no plotting for any run} \\ 1 & \text{if at least 1 run has plotting} \end{cases}$

TYPE II - To be supplied for each run

PART 1 - General data for the runGroup a

Card 1 - final time, plot scale [(2E15.8) format]
(program disregards plot scale if there is no plotting)

plot scale = number of seconds/inch along abscissa

Card 2 - plot clue for the run, fluid clue, number of pipes,
number of moving masses [(4I3) format]

plot clue = $\begin{cases} 0 & \text{no plotting} \\ 1 & \text{plotting} \end{cases}$

fluid clue = $\begin{cases} 0 & \text{no fluids present} \\ 1 & \text{fluids present} \end{cases}$

Card 3 - (insert blank card if no moving masses are present)
enter clues for each moving mass (1-8) [(8I3) format]

each clue = $\begin{cases} 0 & \text{moving mass not present} \\ 1 & \text{moving mass present} \end{cases}$

Card 4 - (insert blank card if no fluids are present)
mass point index numbers of the emptying and filling
reservoirs, respectively [(2I3) format]

Card 5 - (Card 6 if needed) (insert 1 blank card if no pipes are
present) mass point index number of each pipe present
[(15I3) format]

Second card needed if more than 15 pipes are present

Group b

(Skip to group C if there is no plotting on this run)

Card 1 - enter clues for the 13 plotting groups [(13I1) format]

enter 1 if the group is to be plotted, 0 if not. Choose 7 groups maximum. If plotting is selected on a run $\{\omega^x\}$ is always plotted first, followed by the plotting groups selected on this card.

The 13 optional groups are:

<u>Group No.</u>	<u>Variables Plotted</u>
1	$\{\gamma\}$
2	$\{\delta\}$
3	$\{\varphi^*\}$
4	$\{q_a\}$ for some mass no. a
5	$\{\theta_b\}$ for some mass no. b
6	$\{q_c\}$ for some mass no. c
7	$\{\theta_d\}$ for some mass no. d
8	$\{q_e\}$ for some mass no. e
9	$l_{03}, \dot{l}_{03}, \ddot{l}_{03}$
10	$\{U_1\}_3 - \{U_1(0)\}_3, \{U_2\}_3 - \{U_2(0)\}_3$ $\{X_{SENS/CM}^{CMND}\}_3 - \{X_{SENS/CM}\}_3$
11	V, \dot{V}, h_i for emptying reservoir
12	$\{f'_r\}$ for some mass no. r
13	$\{\tau'_s\}$ for some mass no. s

Each group consists of three plots, one above the other, when vectors are plotted, the first component is always plotted on top, followed by the second component, with the third component on the bottom.

Card 2 - enter the mass-point index numbers a, b, c, d, e, r, s as above [(7I3) format]
(insert blank card if none are selected for plotting)

Group c

Card 1 - enter clues KLUE, IFLAB, IFCW, IFCN [(4I4) format]
KLUE denotes the type of problem being run

KLUE = $\left\{ \begin{array}{l} 1 \text{ flexible Space Station} \\ 2 \text{ rigid Laboratory} \\ 3 \text{ rigid Counterweight} \\ 4 \text{ rigid Space Station} \\ 5 \text{ rigid Laboratory and Counterweight} \end{array} \right.$

IFLAB enables the user to run a rigid-Laboratory problem using a (slightly modified) flexible-Laboratory deck.

IFLAB = $\left\{ \begin{array}{l} 1 \text{ is always used when the Laboratory is flexible; also} \\ \text{when the Laboratory is rigid and input data for the} \\ \text{flexible Laboratory is present in the deck. (In this} \\ \text{case the data is read in but disregarded).} \\ 0 \text{ is used when elastic displacements and velocities of} \\ \text{the Laboratory}(\{q_i\}, \{\dot{q}_i\}, \{\theta_i\}, \{\dot{\theta}_i\}) \text{ are not present} \\ \text{in the deck. Also, when IFLAB} = 0 \text{ and the Phase I} \\ \text{input tape is not present, the Laboratory modal data} \\ \text{(number of modes, modal masses, frequencies, and mode} \\ \text{shapes) must be absent from the deck.} \end{array} \right.$

IFCW - same as IFLAB except that it applies to the Counterweight input data.

IFCN - if IFCN = 0, no Connecting Structure data is read in; use IFCN=0 only when the Space Station is rigid (see description of Part 8). Otherwise set IFCN = 1.

Card 2 - enter IFDEPL, IFCON, IFSUPP [(3I4) format]

IFDEPL = $\left\{ \begin{array}{l} 0 \text{ no deployment} \\ 1 \text{ deployment} \end{array} \right.$

IFCON = $\left\{ \begin{array}{l} 0 \text{ no controls} \\ 1 \text{ controls present} \end{array} \right.$

IFSUPP = $\left\{ \begin{array}{l} 0 \text{ no supplementary forces} \\ 1 \text{ supp. forces present} \end{array} \right.$

PART 2 - Type 1 controls input (skip this portion if no controls are present)

Card 1 - i_s, f_{JET}

(I3, E15.8) format

Card 2 - Counterweight command input

$l_{03U}, t_{03U}, acc_{03MAG}, vel_{03MAX}$

(4E15.8) format

- Card 3 - spin command input
 ω_{1C} (initial value), $t_{\omega 1CU}$, $acc_{\omega 1C}$
 (3E15.8) format
- Card 4 - spin control input
 $e_{\omega IDB}$
 (E15.8) format
- Card 5 - attitude control input
 $e_{\theta DB}$, $\dot{e}_{\theta MAX}$, $XJ1$
 (3E15.8) format
- Card 6 - wobble control input
 β_G , $\dot{\beta}_G$, K_T , t_{qLim}
 (4E15.8) format
- Card 7 - wobble control input (continued)
 $K_{\dot{\beta}}$, mom_{CMG} , $I_{\beta GIM}$
 (3E15.8) format

PART 3 - Internal loads

(if no internal load computations are required, use blank card and skip to Part 4)

Group a - (one card)

Card 1 - enter clues KLUCS, KLULAB, KLUCW, N, NB
 (5I2) format

use KLUCS = 1 if structural loads applied by the Connecting Structure are computed. Use 0 otherwise

use KLULAB = 1 if internal loads on the Laboratory are to be computed. Use 0 otherwise

use KLUCW = 1 if internal loads on the Counterweight are to be computed. Use 0 otherwise

N = number of load-computation points on Laboratory

NB = number of load-computation points on Counterweight

Group b - input for each load computation point on Laboratory (skip to Group c if N = 0)

Card 1 - ℓ (the load computation mass-point index number), number of mass points comprising the free body [(2I2) format]

Card 2 - the load coordinates $\{t_{\ell}\}$
 (3E15.8) format

remaining cards (10 maximum)

the index numbers of the mass points comprising the free body, 10 per card

(10I2) format

Group c - input for each load computation point on the Counterweight
 (skip to part 4 if NB=0)
 construct similarly to Group b

PART 4 - Laboratory input data

Group a - (one card)

Card 1 - IPHS1, JUMP
 (2I4) format

IPHS1 = $\begin{cases} 0 & \text{no Phase I tape provided} \\ 1 & \text{Phase I tape provided} \end{cases}$

JUMP = 1 is used to set the elastic displacements and
 velocities = 0 without reading them in.

Group b

(If IPHS1 = 1, skip to group d)

Subgroup 1 - (one card)

Card 1 - enter the number of mass points on the Laboratory
 (I4) format

Subgroup 2 - mass point locations $\{r_i\}$. One card for each mass point
 (3E15.8) format

Subgroup 3 - masses, Inertia matrices
 (repeat for each mass point)

Card 1 - mass m_i [(E15.8) format]

Card 2 - column 1 of inertia matrix $[I_i]$

Card 3 - column 2 of inertia matrix

Card 4 - column 3 of inertia matrix
 (3E15.8) format

Group c

(if IFLAB = 0, skip to Part 5)

Subgroup 1 - (One card)

Card 1 - enter p (number of modes)
 (I4) format

Subgroup 2

enter the p modal masses

3 per card

(3E15.8) format

Subgroup 3

enter the p frequencies

3 per card

(3E15.8) format

Subgroup 4

enter the modal matrix - column by column

Use 3 elements of a column per card

(3E15.8) format

Group d

(if IFLAB = 0 skip to Part 5)

Subgroup 1

(if JUMP = 1 skip to Subgroup 2)

enter the elastic displacements and velocities

all $\{q_i\}$, one card per mass pt [(3E15.8) format]

all $\{\dot{q}_i\}$, one card per mass pt [(3E15.8) format]

all $\{\theta_i\}$, one card per mass pt [(3E15.8) format]

all $\{\dot{\theta}_i\}$, one card per mass pt [(3E15.8) format]

Subgroup 2

enter the ratio of damping to critical damping for each mode.

3 per card

(3E15.8) format

PART 5 - Rigid-body displacements and velocitiesCard 1

{R}

(3E15.8) format

Card 2

$\{\dot{R}\}$

(3E15.8) format

Card 3

{ γ }

(3E15.8) format

Card 4

$\{w^X\}$

(3E15.8) format

PART 6 - Fluids and moving mass inputGroup a - reservoir input

(skip to Group c if no fluids are present)

Subgroup 1 - (one card)

Card 1 - entry ρ, A
(2E15.8) format

Subgroup 2 - emptying reservoir

Card 1 - M_i^D (E15.8) format
Cards 2-4 [I_i^D] 1 row per card (3E15.8) format
Card 5 [S_i^D] (3E15.8) format
Card 6 [e_i^R] (3E15.8) format
Card 7 [u_i^R] (3E15.8) format
Card 8 [u_i^B] (3E15.8) format
Card 9 [e_i^B] (3E15.8) format
Cards 10-12 [J_i^B] 1 row per card (3E15.8) format
Card 13 $b_i, h_{i0}, h_i \text{ max}, h_i \text{ min}$, (4E15.8) format
Card 14 [G_i^P] (3E15.8) format

Subgroup 3 - filling reservoir

same as Subgroup 2

Group b - input for through pipes

(skip to Group c if no fluids or if no pipes)

REPEAT for each pipe.

Card 1 m_i^f (E15.8) format
Card 2 [S_i] (3E15.8) format
Card 3 [Δu_i] (3E15.8) format
Card 4 [Δe_i] (3E15.8) format
Card 5 [G_i] (3E15.8) format
Card 6 [ΔH_i] (3E15.8) format
Cards 7-9 [ΔJ_i] 1 row per card (3E15.8) format
Cards 10-12 [I_i^f] 1 row per card (3E15.8) format

Group c - moving masses input

(skip to part 7 if no moving masses are present)

enter μ_i for each moving mass present

1 per card

(E15.8) format

PART 7 - Counterweight input data

same as instructions for PART 4, but for Counterweight

Group a (one card)

Card 1 - IPHS1, JUMP

(2I4) format

IPHS1 = $\begin{cases} 0 & \text{no Phase I tape provided} \\ 1 & \text{Phase I tape provided} \end{cases}$

JUMP = 1 is used to set the elastic displacements
and velocities = 0 without reading them in.

Group b

(If IPHS1 = 1, skip to group d)

Subgroup 1 (one card)

Card 1 - enter the no. mass points on the Counterweight

(I4) format

Subgroup 2

mass point locations $\{\bar{r}_a\}$. One card for each mass point

(3E15.8) format

Subgroup 3 - masses, inertia matrices

(repeat for each mass point)

Card 1

mass \bar{m}_a

(E15.8) format

Card 2 - column 1 of inertia matrix $[\bar{I}_a]$

Card 3 - column 2 of inertia matrix

Card 4 - column 3 of inertia matrix

(3E15.8) format

Group c

(If IFCW = 0, skip to PART 8)

Subgroup 1 - (one card)

Card 1 - enter \bar{p} (number of modes)
(I4) format

Subgroup 2

enter the \bar{p} modal masses
3 per card
(3E15.8) format

Subgroup 3

enter the \bar{p} frequencies
3 per card
(3E15.8) format

Subgroup 4

enter the modal matrix - column by column.
Use 3 elements of a column per card
(3E15.8) format

Group d

(if IFCW = 0, skip to PART 8)

Subgroup 1

(if JUMP = 1 skip to Subgroup 2)
enter the elastic displacements and velocities

all $\{\bar{q}_a\}$, one card per mass pt (3E15.8) format

all $\{\dot{\bar{q}}_a\}$, one card per mass pt (3E15.8) format

all $\{\bar{\theta}_a\}$, one card per mass pt (3E15.8) format

all $\{\dot{\bar{\theta}}_a\}$, one card per mass pt (3E15.8) format

Subgroup 2

enter the ratio of damping to critical damping for each mode.
3 per card
(3E15.8) format

PART 8 - Connecting Structure input data (skip to part 9 only ifIFCN = 0 and KLUE = 4)

Card 1 i, a
 (2I4) format

Card 2 {s} (3E15.8) format

Card 3 $\{\bar{s}\}$ (3E15.8) format

Card 4 { δ } (3E15.8) format

Card 5 $\{\dot{\delta}\}$ (3E15.8) format

Card 6 $\{\phi^*\}$ (3E15.8) format

Card 7 $\{\dot{\phi}^*\}$ (3E15.8) format

Card 8 $\{Y^a\}$ \textcircled{a} (3E15.8) format

Card 9 $\{Y^a\}$ \textcircled{b} (3E15.8) format

PART 9 - Type 2 controls inputGroup a - (one card)Card 1 - enter $\{l_0\}$

(3E15.8) format

Group b - pump command (PMPCOM) input (skip to Group c if there are no fluids present)Card 1 - $V, V_U, t_{FU}, acc_{MAG}$

(4E15.8) format

Group c - moving mass command (MUCOM) input for Mass 1 ($j = 1$); elevator (skip to Group e if moving mass $j = 1$ is not present)Subgroup 1Card 1 - enter 3 clues, 0 or 1, denoting absence or presence of motion along $X_1, X_2,$ and X_3 axes respectively

(3I2) format

Card 2 - enter initial value of $\{U_j\}$

(3E15.8) format

Subgroup 2

Repeat Card 1 below for each axis present. If the mass does not move, skip to Group d.

Card 1 - enter $U_U, t_U, acc_{MAG}, vel_{MAX}$

(4E15.8) format

Group d - Balance mass control input (controls motion of moving mass $j = 2$) (skip to Group e if moving mass $j = 2$ is not present)

Card 1 - $\{U_2\}$

(3E15.8) format

Card 2 - $\{\dot{U}_2\}^*$

(3E15.8) format

Card 3 - $\mu_{LEST}, K_{eXSE}, K_{DESE}, \tau_{BAL}, \omega_{LC BAL}$

(5E15.8) format

Card 4 - $\{X_A^i\}$

(3E15.8) format

Card 5 - $\{X_{SENS/CM}^{CMND}\}$

(3E15.8) format

Group e - moving mass command (MUCOM) input for masses 3, 4, ...
($j > 2$) (skip to Part 10 if there are no other moving masses present)

repeat input for each moving mass as described in Group c

PART 10 - Beam-type connecting structure, numerical integration, and printout data

Group a - beam connecting structure subroutine input
(skip to Group b if KLUE = 4)

Card 1 - M_C, M_L, I_C (3E15.8) format

Card 2 - I_L, J_C, J_L (3E15.8) format

Card 3 - a, b, AE (3E15.8) format

Card 4 - $EI, GJ, \ell_{O_{MIN}}$ (3E15.8) format

Card 5 - Y_A, Y_B, Y_T

Group b - numerical integration input - see MAGIC writeup in Appendix B2

Card 1 - DELTA, EPSIL, STEP
(3E15.8) format

* For the control systems provided with this program, the first two components of $\{\dot{U}_2\}$ must be read in as zero.

Card 2 - DTAU, NTIME

(E15.8, I3) format

DTAU is the MAGIC output time interval. In this program a distinction is made between the plot output interval and the print output interval. DTAU is used as the plot output interval and NTIME * DTAU is used as the print output interval.

Remaining Cards - enter ERR parameters. 1 parameter for each integrated variable. 3 parameters per card (3E15.8) format

The order of the integrated variables Y_i is as follows:

$$\{Y\} = \left\{ \begin{array}{l} \{R\} \\ \{\omega^x\} \\ \{\dot{\xi}\} \\ \{\Delta \dot{R}\} \\ \{\omega^Y\} \\ \{\dot{\zeta}\} \\ \{R\} \\ \{\delta\} \\ \{F\} \\ \{\Delta \bar{R}\} \\ \{\eta^*\} \\ \{\bar{\zeta}\} \\ \dot{B}_G \\ B_G \\ \text{err}_{KTI} \\ \text{err}_{LLI} \\ \dot{U}_{2,3} \\ U_{2,3} \\ e_{\text{FILT}} \end{array} \right\} \quad \begin{array}{l} \left. \begin{array}{l} \{R\} \\ \{\omega^x\} \end{array} \right\} \text{always present} \\ \left. \begin{array}{l} \{\dot{\xi}\} \\ \{\Delta \dot{R}\} \end{array} \right\} \text{present if Laboratory is flexible} \\ \left. \begin{array}{l} \{\omega^Y\} \\ \{\dot{\zeta}\} \end{array} \right\} \text{present if Space Station is flexible} \\ \left. \begin{array}{l} \{R\} \\ \{\delta\} \end{array} \right\} \text{always present} \\ \left. \begin{array}{l} \{F\} \\ \{\Delta \bar{R}\} \end{array} \right\} \text{present if Laboratory is flexible} \\ \left. \begin{array}{l} \{\eta^*\} \\ \{\bar{\zeta}\} \end{array} \right\} \text{present if Space Station is flexible} \\ \left. \begin{array}{l} \{\bar{\zeta}\} \\ \dot{B}_G \\ B_G \\ \text{err}_{KTI} \\ \text{err}_{LLI} \end{array} \right\} \text{present if Counterweight is flexible} \\ \left. \begin{array}{l} \dot{B}_G \\ B_G \\ \text{err}_{KTI} \\ \text{err}_{LLI} \end{array} \right\} \text{(wobble damping parameters) present if controls are present} \\ \left. \begin{array}{l} \dot{U}_{2,3} \\ U_{2,3} \\ e_{\text{FILT}} \end{array} \right\} \text{(balance mass parameters) present if mass balancing is present} \end{array} \quad (3.5)$$

Group c - flexible problem printout data (skip if KLUE > 3)

Subgroup 1 - (one card)

Card 1 - KLOUTL, KLOUTC

(2I3) format

KLOUTL = number of mass pts for the Laboratory at which
the elastic displacements and velocities are
printed each output cycle

KLOUTC = similar to KLOUTL but for the Counterweight

Subgroup 2 - (skip if KLOUTL = 0)

enter the index numbers of the KLOUTL mass points

20 per card

(20I3) format

Subgroup 3 - (skip if KLOUTC = 0)

enter the index numbers of the KLOUTC mass points

20 per card

(20I3) format

3.7 PROGRAM OUTPUT

Examples of the program output are presented and discussed in Appendix B2.

APPENDIX A

DETAILED INFORMATION

FOR THE PHASE I COMPUTER PROGRAM

This appendix contains detailed programming information for the Phase I computer program. In addition, samples of input and output data are presented.

APPENDIX A1

EXAMPLE OF INPUT DATA

The example on the following pages shows input data for the 9-module cantilevered configuration shown in Figure A1. Module 1 is the core module described in Appendix F of Volume 1, and the remaining modules are identical and have the properties of the typical appended module described in that appendix. The local x axis of each appended module is oriented along the module, and the local z axis is oriented as indicated in the table on Figure A1. The last mass point of the idealized core module is fastened to the ground and therefore does not enter the problem. Mass points 2 and 5 have zero mass and were artificially introduced to serve as connection points. 20 modes of Module 1, and 10 modes of all other modules are used in the synthesis. Mass-loaded modes are used for Module 1 (see Section 2.2). As the T-matrix data indicates, the x-direction deflections in the input modes of masses 7 and 8 are not present. These deflections were constrained to be zero in the core-module idealization. All other mass points have six degrees of freedom.

The results of this problem include printout of all input substructure modes (see Appendix A2).

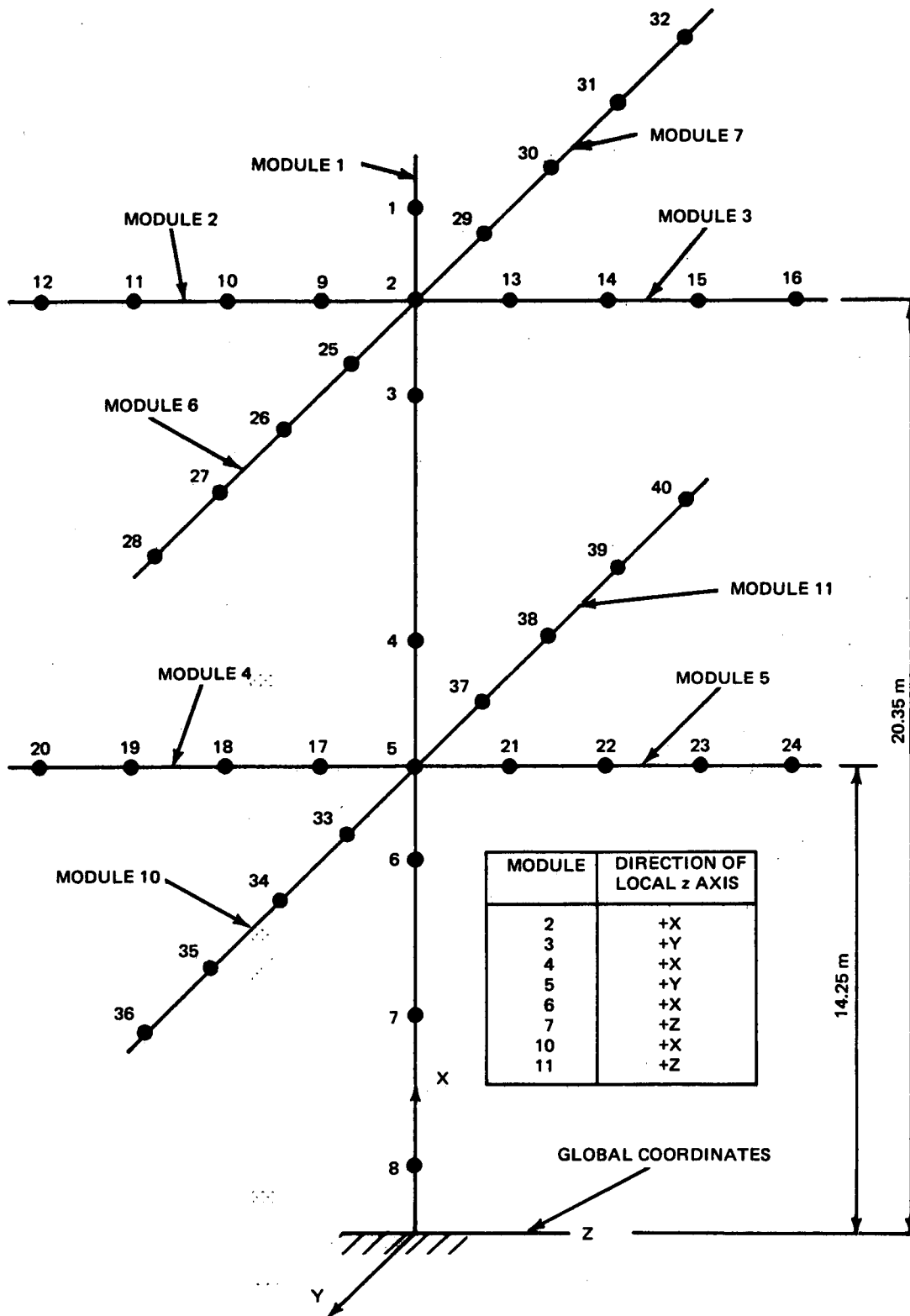


Fig. A1 Configuration Used to Illustrate Input Data for Phase I Program

TYPE I DECK

1 1 1 1 1 1 1 0 0 1 1
 20101010101010 1010
 8 4 4 4 4 4 4 4
 2 2 5 5 2 2 5 5
 386.4 G-CONSTANT

X₀ -
 X_a -
 X_b -
 TYPE II DECK
 FOR MODULE 1

MASS POINT
 LOCATIONS
 FOR MODULE 1

MASS MATRIX -1

0. 15.4E6

0. 15.6E6

0. 15.6E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

MODID

NMO

NMPO

JUNCTION POINTS

MASS POINTS -1

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0. 15.4E6

0111111

MASS POINT # OF OVERRIDE T-MATRIX - 7

T-MATRIX CARD - 7

MODE SHAPES FOLLOW - 1

-0.11885560E-17

0.67255229E-14

-0.8528E-14

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

-0.27002758E-11

-0.42299298E-11

-0.79493825E-11

0.11097984E-02

0.41559248E-16

0.66309993E-16

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.41559248E-16

0.66309993E-16

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

MASS
DATA
FOR
MODULE 1

START OF
MODES FOR
MODULE 1
(46x20 MATRIX)

0.27222044E-11
 0.10599865E-06
 0.10600626E-11
 -0.49743279E-10
 0.33369840E-09
 -0.36391957E-05
 -0.12255741E-05
 -0.77885504E-10
 0.51464450E-07

0011111
 8
 MODE SHAPES FOLLOW - 1

0.45478710E-09
 0.21326930E-07
 -0.50876359E-07
 -0.12417606E-02
 0.12325044E-02
 0.62031E-

PARTITION OF
 MODAL MATRIX
 FOR
 MODULE 1
 CORRESPONDING
 TO MASS POINT
 7

-0.13979170E-01
 0.53713284E-02
 0.10091742E-02
 0.49082349E-10
 -0.12038270E-04
 0.10873823E-03
 -0.10809704E-03
 0.497606E-09

-0.35992798E-05
 -0.27605438E-05
 0.67157099E-10
 0.29985046E-07

0011111

0.13690130E-09
 0.12873201E-07
 -0.45855749E-07
 -0.47514407E-03

PARTITION OF
 MODAL MATRIX
 FOR MODULE 1
 CORRESPONDING
 TO MASS POINT
 8

-0.46200000E-07
 0.61575292E-07
 -0.41042492E-02
 0.32484070E-02
 0.98520843E-03
 0.16543285E-08
 0.40108000E-05
 0.74177113E-04

0.137134E-05
 0.26236321E-05
 0.83648732E-09
 -0.25606090E-06

TYPE II DECK FOR
 MODULE 2

MASS POINTS - 2

MASS POINT LOCATIONS

X0 - 801.
 XA - 1.
 XB - 0.
 132.
 252.
 372.
 492.
 6250.
 19.3E6
 0.
 18.8E6
 0.

MASS MATRIX - 2

0.65956829E-05
 0.36551052E-06

0.0919E-12
 -0.68356501E-11
 0.19447280E-09
 0.79868911E-08
 -0.46700234E-06
 -0.73552314E-07

0.10505745E-09
 -0.51842464E-09
 0.59144412E-07
 -0.80449236E-05
 0.19775543E-02
 0.85294945E-04

0.2018E-06
 -0.35998696E-07

0.72022735E-10
 -0.79453066E-09
 0.22594119E-07
 -0.23799177E-04

```

0. 18.6E6
6250. 0.
19.3E6 0.
0. 18.8E6
0. 18.6E6
6250. 0.
19.3E6 0.
0. 18.8E6
0. 18.6E6
6250. 0.
19.3E6 0.
0. 18.8E6
0. 18.6E6
0111111 0. DEFAULT T
50 MODE SHAPES FOLLOW - 2
-0.19C10506E-13
-0.74030879E-10
-0.11526763E-09
-0.18177777E-09
0.11422608E-11
-0.23546117E-12
0.36286238E-10
0.29617269E-03
0.10326E-09
0.42109510E-10
-0.1760010E-03
-0.15743515E-09
-0.11881178E-03
0.10326E-09

```

INDICATES NO T-MATRIX
OVERIDE

50

MODES FOR
MODULE 2
(24x10 MATRIX)

X₀ -
TYPE II DECK FOR X_A -
MODULE 3 X_B -

```

0.54707634E-08
0.14190640E-08
0.58481510E-05
-0.56819904E-09
0.18939036E-05
801. 0.
0. 1.
0. 1.
0. 0.
132. 0.
252. 0.
372. 0.
492. 0.
6250. 19.3E6
0. 18.8E6
0. 18.6E6
6250. 19.3E6
0. 18.8E6
0. 18.6E6
6250. 19.3E6
0. 18.8E6
0. 18.6E6
6250. 19.3E6
0. 18.8E6
0. 18.6E6

```

MASS POINTS -3

MASS MATRIX - 3

MASS
MATRIX
FOR
MODULE
3

```

0.95977011E-08
0.28841417E-11
0.26273874E-05
-0.17867747E-11
-0.53934457E-08

```

01111111 DEFAULT T
 50 MODE SHAPES FOLLOW - 3
 -0.19010506E-13
 -0.74030879E-10
 -0.11526763E-09
 -0.18177335E-10
 0.11422608E-11
 -0.23546117E-12
 0.36286238E-10
 0.29617269E-03
 -0.36929326E-09
 0.19039799E-06
 0.8444

MODULE 3 MODES

SKIP TO MODULE II

0.42109510E-10
 -0.17600010E-03
 -0.15743515E-09
 -0.11881178E-06
 0.19039799E-06
 0.8444

01111111 DEFAULT T
 50 MODE SHAPES FOLLOW - 11
 -0.19010506E-13
 -0.74030879E-10
 -0.11526763E-09
 -0.18177335E-10
 0.11422608E-11
 -0.23546117E-12
 0.36286238E-10
 0.29617269E-03
 -0.36929326E-09
 0.19039799E-06
 0.8444

START OF
 MODULE II MODES

0.11453504E-04
 -0.37353120E-02
 0.14056076E-06
 0.15822977E-03
 -0.29505678E-07
 0.26880021E-14
 0.85768823E-11
 0.27940905E-11
 0.84623463E-11
 0.95994383E-05
 -0.16646970E-08
 -0.26374564E-05
 0.54707634E-08
 0.14190640E-08
 0.58481510E-05
 -0.56819904E-09
 0.18939036E-05
 0.56086957E 00
 0.16982917E-01
 0.22559012E-02
 0.18632100E-02
 0.26269048E-03
 0.67674802E-04
 0.57138968E-04
 0.36346563E-03
 0.22940032E-04
 0.62864710E-05
 0.39112711E-05
 0.36346563E-03
 0.22940032E-04
 0.62864710E-05
 0.39112711E-05
 0.36346563E-03
 0.22940032E-04
 0.62864710E-05
 0.39112711E-05
 0.36346563E-03
 0.22940032E-04
 0.62864710E-05
 0.39112711E-05
 0.36346563E-03
 0.22940032E-04
 0.62864710E-05
 0.39112711E-05

0.55694539E-00
 -0.50935833E-09
 0.45102368E-07
 -0.42529567E-15
 -0.13830129E-04
 0.56041578E-11
 -0.14313177E-08
 0.38737399E-11
 -0.78068796E-09
 0.95977011E-05
 0.28841417E-11
 0.26273874E-05
 0.55993354E 00
 0.16880568E-01
 0.22344198E-02
 0.42018224E-03
 0.84677653E-04
 0.61886822E-04
 0.57128025E-04
 0.36333827E-03
 0.21471686E-04
 0.62819954E-05
 0.36333827E-03
 0.21471686E-04
 0.62819954E-05
 0.36333827E-03
 0.21471686E-04
 0.62819954E-05
 0.36333827E-03
 0.21471686E-04
 0.62819954E-05
 0.36333827E-03
 0.21471686E-04
 0.62819954E-05

-0.49397163E-03
 -0.17129076E-09
 -0.99157096E-05
 0.22769522E-10
 0.28622619E-13
 0.11358674E-11
 0.58549822E-05
 0.21175206E-11
 0.19211348E-05
 0.15936690E-08
 -0.17867747E-11
 -0.53934457E-08
 0.37350321E 00
 0.96777789E-02
 0.18671064E-02
 0.26273169E-03
 0.84644154E-04
 0.61846105E-04
 0.22968801E-04
 0.17857150E-04
 0.39144079E-05
 0.22968801E-04
 0.17857150E-04
 0.39144079E-05
 0.22968801E-04
 0.17857150E-04
 0.39144079E-05
 0.22968801E-04
 0.17857150E-04
 0.39144079E-05
 0.22968801E-04
 0.17857150E-04
 0.39144079E-05

END OF
MODULE 11 MODES

TYPE III DECK

MODAL MASSES FOR MODULE 1

MODAL MASSES FOR MODULE 2

MODAL MASSES FOR MODULE 3

MODAL MASSES FOR MODULE 4

MODAL MASSES FOR MODULE 5

MODAL MASSES FOR MODULE 6

MODAL MASSES FOR MODULE 7

MODAL MASSES FOR MODULE 11	0.22940032E-04	0.21471686E-04	0.17857150E-04
	0.62864710E-05	0.62819954E-05	0.39144079E-05
EIGENVALUES FOR MODULE 1	0.39112711E-05	0.36333827E-03	0.22968801E-04
	0.36346563E-03	0.21471686E-04	0.17857150E-04
EIGENVALUES FOR MODULE 2	0.22940032E-04	0.62819954E-05	0.39144079E-05
	0.62864710E-05	0.39112711E-05	0.36333827E-03
EIGENVALUES FOR MODULE 3	0.36346563E-03	0.21471686E-04	0.17857150E-04
	0.22940032E-04	0.62819954E-05	0.39144079E-05
EIGENVALUES FOR MODULE 4	0.62864710E-05	0.39112711E-05	0.36333827E-03
	0.36346563E-03	0.21471686E-04	0.17857150E-04
EIGENVALUES FOR MODULE 5	0.22940032E-04	0.62819954E-05	0.39144079E-05
	0.62864710E-05	0.39112711E-05	0.36333827E-03
EIGENVALUES FOR MODULE 6	0.36346563E-03	0.21471686E-04	0.17857150E-04
	0.22940032E-04	0.62819954E-05	0.39144079E-05
EIGENVALUES FOR MODULE 7	0.62864710E-05	0.39112711E-05	0.36333827E-03
	0.36346563E-03	0.21471686E-04	0.17857150E-04
EIGENVALUES FOR MODULE 10	0.22940032E-04	0.62819954E-05	0.39144079E-05
	0.62864710E-05	0.39112711E-05	0.36333827E-03
EIGENVALUES FOR MODULE 11	0.36346563E-03	0.21471686E-04	0.17857150E-04
	0.22940032E-04	0.62819954E-05	0.39144079E-05

0 20100
 NUMBER OF RIGID BODY MODES -
 SPECIFIES 20 EIGENVECTORS, AND
 100 EIGENVALUES TO BE COMPUTED

APPENDIX 2

EXAMPLE OF PROGRAM OUTPUT

The computer printout of the problem described in Appendix A1 appears on the following pages. The illustration of Appendix A1 indicates that 100 frequencies are to be computed; however, the input was revised so that only 20 frequencies were computed.

CONFIGURATION SPECIFIED

MODULE NO.	* NO. AIDS	* NO. MASS POINTS
1	20	8
2	10	4
3	10	4
4	10	4
5	10	4
6	10	4
7	10	4
10	10	4
11	10	4

CONSTANT C FOR THE PROGRAM = C.38530990E 03

JUNCTION POINT DATA

MODULE	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
JUNCTION POINT	2	2	5	5	2	2	0	0	5	0	0	0	0	0	0	0

** MODULE 1 **

MASS POINT LOCATIONS IN LOCAL COORDINATES

MASS NO. COORDINATES

1	0.661000E 03	0.0	0.0
2	0.501000E 03	0.0	0.0
3	0.741000E 03	0.0	0.0
4	0.621000E 03	0.0	0.0
5	0.551000E 03	0.0	0.0
6	0.501000E 03	0.0	0.0
7	0.441000E 03	0.0	0.0
8	0.225000E 03	0.0	0.0

A-11

COORDINATES OF POINT 0

0.0 0.0 0.0

COORDINATES OF POINT A

0.0 0.0 0.100000E 01

COORDINATES OF POINT 9

0.100000E 01 0.0

MASS POINT LOCATIONS IN ABSOLUTE GLOBAL COORDINATES

MASS NO. COORDINATES

1	0.661000E 03	0.0	0.0
2	0.501000E 03	0.0	0.0
3	0.741000E 03	0.0	0.0
4	0.621000E 03	0.0	0.0
5	0.551000E 03	0.0	0.0
6	0.501000E 03	0.0	0.0
7	0.441000E 03	0.0	0.0
8	0.225000E 03	0.0	0.0

MASS AND MOMENTS OF INERTIA IN LOCAL COORDINATES

MASS NO.	MASS	INERTIA MATRIX					
1	0.1617494E 02	0.4373707E 05	C.C	0.0	0.0	0.0	0.0
		0.0	0.4037268E 05	0.0	0.0	0.0	0.0
		0.0	C.C	0.3995508E 05	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0	0.0
3	0.1617494E 02	0.4373707E 05	C.C	0.0	0.0	0.0	0.0
		0.0	0.4037268E 05	0.0	0.0	0.0	0.0
		0.0	C.C	0.3995508E 05	0.0	0.0	0.0
4	0.1617494E 02	0.4373707E 05	C.C	0.0	0.0	0.0	0.0
		0.0	0.4037268E 05	0.0	0.0	0.0	0.0
		0.0	C.C	0.3995508E 05	0.0	0.0	0.0
5	C.C	0.0	C.C	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0	0.0
6	0.1617494E 02	0.4373707E 05	C.C	0.0	0.0	0.0	0.0
		0.0	0.4037268E 05	0.0	0.0	0.0	0.0
		0.0	C.C	0.3995508E 05	0.0	0.0	0.0
7	0.5734474E 01	0.8152176E 04	C.C	0.0	0.0	0.0	0.0
		C.C	0.1275880E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.1262940E 05	0.0	0.0	0.0
8	0.1745655E 02	0.1630435E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.7893375E 05	0.0	0.0	0.0	0.0
		0.0	C.C	0.7815731E 05	0.0	0.0	0.0

A-12'

DEFAULT T-MATRIX FOR MODULE 1

6 ROWS, 6 COLUMNS	1	2	3	4	5	6
0.100000E 01	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0

SUBSTRUCTURE MODAL MATRIX

ROW NO.	COORDINATES OF MASS POINT 1											
1	-0.1182556E-17	-0.2700276E-11	0.415923E-10	0.6725520E-14	-0.4289930E-11	0.6636998E-17	-0.8528516E-12	-0.7849782E-11	-0.2096011E-11	0.6435324E-11	0.1109798E-02	0.3496914E-10
	0.6541373E-09	0.5823155E-09	-0.5594170E-08	-0.2145625E-03	-0.4179520E-07	-0.2087455E-06	0.2803363E-07	-0.2870117E-06				
2	0.1150273E-09	-0.3741656E-01	0.2028304E-10	-0.4703008E-08	-0.9191649E-03	0.6866685E-09						

G

-C.1111135E-07 0.4347209E-03 -0.6923466E-07 0.1470935E-02 0.9774821E-C9 -0.9900526E-07
 C.1151149E-04 C.1590799E-07 0.3922220E-C4 -0.2870975E-06 -C.1148366E-02 -C.8975135E-03
 -C.5325933E-03 -C.1049719E-02

E C.374173E-01 C.1209732E-09 -0.2176829E-09 0.8963019E-03 -0.7483505E-08 0.4442045E-09
 -C.4356249E-03 -C.2577459E-C7 -C.1474976E-02 -C.1316589E-06 -C.2533502E-09 -0.1158140E-C4
 -0.8579667E-C7 C.3861397E-C4 -C.3701305E-06 -C.2997627E-06 0.9047878E-03 -0.1147731E-02
 -C.1028101E-02 -C.5241125E-03

4 C.1125723E-12 -C.3811007E-11 C.8008610E-04 -0.1316836E-10 0.1549211E-10 0.1222102E-04
 -C.1127953E-11 C.4648244E-10 C.4865517E-10 -0.2736939E-10 -C.7925121E-11 -0.2584677E-09
 -0.6586689E-09 0.8875505E-C9 C.2523252E-C8 -0.9155879E-09 -0.9513045E-C8 0.1753776E-C8
 -C.8818645E-03 -C.1529791E-C8

5 -C.8544456E-04 -C.2763759E-11 -0.7787067E-12 -0.2084937E-04 0.7896270E-10 -0.4042535E-11
 -C.7559279E-05 0.4689975E-09 -0.3385974E-05 -C.3373155E-09 -0.5492782E-11 -0.4779735E-07
 -C.4289275E-09 C.1993793E-08 0.4048095E-C9 -0.1385445E-08 -0.5013106E-06 0.6311929E-06
 -C.8706635E-05 C.3490607E-06

F 0.2241613E-11 -C.5543660E-C4 0.6959395E-12 -0.9938294E-10 -0.2087431E-04 -0.1859438E-11
 -C.3463421E-C9 C.7572381E-05 0.1493198E-C9 -0.3395985E-05 -0.7967753E-13 0.3051137E-09
 -C.4936529E-07 C.9232060E-10 -C.1691288E-C8 -0.1501504E-09 -0.6285540E-06 -0.4913744E-06
 -C.3356659E-06 -0.7079634E-C6

COORDINATES OF MASS POINT 2

7 -0.2590143E-17 -0.2700273E-11 0.2483208E-16 0.6719265E-14 -0.4229215E-11 -0.1213351E-16
 -C.8516269E-12 -0.7943244E-11 -0.2092417E-11 0.6432951E-11 0.1101226E-02 0.3453705E-10
 0.3726737E-09 0.5899963E-09 -C.5342511E-08 -0.2042714E-03 0.3959098E-07 -0.1996721E-08
 0.3643484E-07 -0.2592567E-06

8 C.1043219E-08 -0.3408671E-C1 -0.3083792E-10 0.1801900E-08 -0.3365213E-03 0.1086999E-08
 -C.1109104E-07 -0.3124132E-04 -0.7972119E-07 0.1626079E-02 -0.5979076E-10 -0.7360529E-07
 C.1170137E-04 -0.8787407E-07 0.1060143E-04 0.1997650E-07 0.2786228E-C4 0.2154868E-04
 C.5744617E-04 0.1184857E-03

9 C.3408635E-01 0.1059921E-08 -0.2571556E-09 -0.3577841E-03 0.1496986E-C8 -0.4047396E-10
 -C.2551149E-04 C.1058641E-08 -0.1629995E-02 -C.1382514E-06 -0.2741675E-10 -0.1774489E-04
 -0.7764587E-07 0.1081188E-04 0.9016816E-07 -C.1437381E-07 -0.2237782E-04 0.2778514E-04
 -C.1182275E-03 C.5796688E-C4

10 C.5567422E-13 -0.1589302E-13 0.8008465E-04 -0.1213543E-11 -0.1744923E-13 0.1221208E-04
 -0.1235569E-11 -0.1077633E-10 0.8730249E-11 C.1975019E-11 0.5572386E-14 0.5210765E-12
 C.3106990E-11 -0.1509110E-11 -0.4066665E-11 0.131872E-11 0.1099797E-10 0.3179052E-11
 0.1505411E-10 0.6511226E-11

11 -C.8544579E-04 -0.1722992E-11 -0.9541918E-12 -0.2084935E-04 0.8393994E-10 -0.1593267E-11
 C.7540378E-05 C.4447736E-09 -0.3410164E-05 -0.3117815E-09 0.3906196E-13 -0.4875176E-07
 -0.3143656E-09 C.1858567E-07 0.6771554E-10 0.2503411E-10 0.8143206E-07 -0.1037153E-06
 -0.2399239E-07 -0.1340055E-07

12 0.2309047E-11 -0.5543382E-04 0.7747847E-12 0.9808197E-10 -0.2086845E-04 0.1293244E-11
 -C.1459399E-09 0.7554519E-C5 -0.1515521E-09 -0.3420174E-05 -0.1579352E-12 -0.3172125E-09
 -C.4040539E-07 0.9568962E-10 -0.1879881E-07 C.1707763E-10 0.1046743E-06 0.8199333E-C7
 C.1154643E-07 0.2519166E-07

COORDINATES OF MASS POINT 3

13 -C.2294539E-10 -0.2857676E-C9 0.2689404E-11 0.9826459E-10 0.2141731E-09 0.3536890E-11
 0.9215059E-10 -C.7302141E-09 -0.4143894E-09 0.2961853E-C8 -0.9565454E-C3 -0.8758244E-10
 -C.1545155E-07 -C.8474494E-09 0.4558613E-07 -0.3727338E-04 -0.1126559E-06 -0.8534533E-07

R

14	-0.1435521E-07	-0.3564491E-07	-0.5082038F-10	0.6018704E-08	0.1526760E-02	0.5543315E-09
	0.8610556E-09	-0.3070067F-01	-0.4062984F-07	0.8602906E-03	-0.1096483E-09	0.2952444E-06
	0.1852707E-07	-0.7577941E-03	-0.1486876E-07	-0.7510445E-08	0.7382191E-03	0.5804258E-03
	-0.3659400E-04	0.1064738E-05	-0.1486876E-07	-0.7510445E-08	0.7382191E-03	0.5804258E-03
	-0.40334513E-04	-0.8201369E-03				
15	0.3069773E-01	0.9546763E-09	0.2394676E-09	-0.1545201F-02	0.6238366E-08	-0.9111172E-09
	0.3540719E-03	0.2119355E-07	-0.8627232E-03	-0.7608497E-07	-0.3073783E-10	0.3871367E-04
	0.2519772E-05	-0.1485080E-03	-0.6600330E-06	-0.7916032E-07	-0.5745108E-03	0.7383572E-03
	0.5266773E-03	-0.78055779E-07				
16	0.5432715E-13	-0.1571291E-13	0.7901853F-04	0.6987793E-12	-0.1770263E-13	0.5937027E-05
	0.2763337E-11	-0.2901860E-10	0.1950082E-10	-0.1333590E-10	0.4232756E-14	0.5690328E-11
	0.1134316E-09	-0.6699730E-10	0.2195349E-10	0.8653789E-12	-0.2959712E-09	0.7872973E-09
	0.6187890E-09	-0.6266487E-09				
17	-0.5527503E-04	-0.1717817E-11	-0.6371608E-12	-0.1932922E-04	0.7723652E-10	-0.1929997E-11
	0.3392595E-05	0.1564459E-09	-0.1764188E-05	-0.1536972E-09	0.8950939E-14	0.1490588E-06
	0.6858617E-09	-0.1239106E-05	-0.8123873E-09	0.6972757E-11	-0.87964320E-07	0.1036988E-06
	0.3511928E-04	-0.1704807E-06				
18	0.2203272E-11	-0.5526801E-04	0.2925650E-12	-0.8127778E-10	-0.1935715E-04	0.1695464E-11
	-0.1592470E-09	0.3391501E-05	0.7865154E-10	-0.1784922E-05	-0.1747814E-13	-0.9603400E-09
	0.1495428E-05	-0.7738017E-09	0.1235053E-06	0.4215728E-10	-0.1017190E-06	-0.8105832E-07
	0.1720027E-04	0.3509505E-06				
COORDINATES OF MASS POINT 4						
19	0.7154249E-10	-0.1151052E-09	-0.8614568E-11	-0.3075298E-09	0.1203624E-09	-0.7980417E-11
	-0.2054456E-09	0.2461564E-08	0.1395857E-08	-0.9853061E-08	0.6524066E-03	0.8414431E-09
	-0.1290687E-07	0.2696741E-07	0.1054998E-07	0.3004130E-03	-0.1162473E-06	0.5037599E-06
	-0.2456525E-06	0.1241720E-06				
20	0.4570671E-09	-0.2306381E-01	-0.1737291E-10	0.1452325E-07	0.3627090E-02	-0.1376408E-09
	0.4295159E-09	-0.2423984E-03	0.4287939E-07	-0.8531620E-03	-0.1498361E-09	0.9839223E-06
	-0.1437455E-03	0.1645878E-05	-0.2567414E-03	-0.4244573E-07	0.6551309E-03	0.5158854E-03
	-0.4253304E-03	-0.8874990E-03				
21	0.2396189E-01	0.7452712E-09	0.1856772E-09	-0.3639506E-02	0.1458770E-07	-0.6393643E-09
	0.2435219E-03	0.1572089E-07	0.8545085E-03	0.6709871E-07	-0.1925866E-10	0.1490031E-03
	0.9712521E-05	-0.2566457E-03	-0.1428589E-05	-0.6152050E-07	-0.5100141E-03	0.6563414E-03
	0.6539556E-01	-0.4239893E-03				
22	0.5286172E-13	-0.1524365E-13	0.7698318E-04	0.1805013E-11	-0.2661743E-13	-0.6621453E-05
	-0.3874136E-11	-0.4763583E-11	0.6108716E-11	-0.6471845E-11	0.1188570E-14	0.9114119E-11
	0.3090522E-10	-0.3158411E-10	-0.8671506E-10	0.2774763E-12	-0.1030965E-09	0.8237554E-09
	0.2143467E-09	-0.4553159E-09				
23	-0.5470113E-04	-0.1699642E-11	-0.7203331E-12	-0.1637175E-04	0.6536653E-10	-0.2199270E-11
	-0.4921819E-05	-0.3041667E-09	-0.1883142E-05	-0.1228375E-09	-0.1034583E-12	0.3913569E-06
	0.2559674E-08	-0.9776846E-07	-0.6137988E-09	0.3066024E-10	0.2056644E-06	-0.2650776E-06
	-0.2279478E-04	0.1067293E-06				
24	0.1244809E-11	-0.5469159E-04	-0.4783902E-12	-0.6642124E-10	-0.1640110E-04	-0.3632181E-11
	0.1959756E-09	-0.4913157E-05	0.1007245E-09	-0.1925280E-05	0.1144018E-12	-0.2562855E-08
	0.3545348E-06	-0.5149037E-05	0.9843302E-07	0.3701564E-10	0.2654370E-06	0.2084936E-06
	-0.1112843E-06	-0.2257092E-06				
COORDINATES OF MASS POINT 5						

R

26	-0.2035407E-11	0.4647466E-10	0.3626043E-12	0.1455359E-10	-0.4255277E-10	0.1001195E-12
	-0.5804014E-11	-0.1092002E-09	-0.49280718E-10	0.4393775E-09	0.4952974E-03	-0.7980963E-10
	0.4822407E-04	-0.2193785E-08	0.1713576E-07	0.4548664E-03	-0.8747810E-07	0.4340567E-06
	-0.4024447E-07	0.4958803E-06				
27	0.5908027E-09	-0.2062369E-01	0.3587816E-10	0.1810431E-07	0.4532572E-02	-0.9090351E-09
	-0.1799365E-07	0.1945959E-03	0.7511968E-07	-0.1606538E-02	-0.4469679E-10	0.1152222E-05
	-0.1772589E-03	0.7234834E-06	-0.1200759E-03	-0.3645026E-08	-0.49444221E-04	-0.3888304E-04
	0.2936117E-04	0.59968021E-04				
28	0.2062131E-01	0.6414702E-09	0.1496815E-09	-0.4542074E-02	0.1819025E-07	-0.5117300E-09
	-0.1912203E-03	-0.1066275E-07	0.1610749E-02	0.1325091E-06	0.1891440E-10	0.1773425E-03
	0.1155065E-05	-0.1200832E-03	-0.7437700E-06	0.4812120E-08	0.3845221E-04	-0.4945096E-04
	-0.6017811E-04	0.2845982E-04				
29	0.5201835E-13	-0.1505502E-13	0.7581396E-04	0.2379202E-11	-0.3108368E-13	-0.1285583E-04
	0.1234199E-11	0.3761112E-11	-0.4752212E-11	-0.5636690E-11	-0.1277456E-15	-0.87164858E-13
	-0.1246049E-11	0.1662546E-11	0.5215286E-12	-0.3073124E-14	0.4485644E-11	-0.4987680E-11
	-0.6076734E-11	0.2822394E-11				
30	-0.5428953E-04	-0.1686615E-11	-0.7461897E-12	-0.1494066E-04	0.5963827E-10	-0.2791226E-11
	-0.3045850E-05	-0.3554149E-09	-0.3648036E-05	-0.2475404E-09	-0.8024061E-13	0.4598316E-06
	0.3000750E-08	-0.1111895E-06	-0.5666707E-09	-0.4021852E-11	-0.2309046E-07	0.2964742E-07
	0.3222703E-07	-0.1516934E-07				
31	0.1016415E-11	-0.5427728E-04	-0.8538527E-12	-0.5886819E-10	-0.1149684E-04	-0.6668229E-11
	0.1577634E-09	-0.4903306E-05	0.1593674E-09	-0.3700818E-05	0.9616760E-15	-0.3038775E-08
	0.4646389E-05	-0.6853837E-09	0.1123298E-06	0.3332493E-11	-0.2988921E-07	-0.2350006E-07
	0.1588931E-07	0.3226749E-07				
32	-0.4719578E-11	0.3226653E-10	0.6584678E-12	0.2113264E-10	-0.3857816E-11	0.2983980E-11
	0.8221475E-11	-0.1190430E-09	-0.1096018E-09	0.7687579E-09	0.2769716E-03	-0.1913886E-09
	0.3947527E-09	-0.3058295E-08	0.1325372E-07	0.2602290E-03	-0.6569047E-07	0.2411117E-06
	-0.1688417E-07	0.4300683E-06				
33	0.5187779E-07	0.1727842E-01	0.8133851E-10	0.2014149E-07	0.5097321E-02	-0.8427974E-09
	-0.3405585E-07	0.6441453E-03	0.6938978E-07	-0.1446391E-02	0.1345171E-09	-0.3381541E-05
	0.5175641E-03	-0.8844861E-05	0.1451969E-02	0.9921081E-07	0.5552621E-04	0.4343176E-04
	-0.2759065E-04	-0.4772886E-04				
34	0.1727572E-01	0.5375156E-09	0.1049262E-09	-0.5064871E-02	0.2025892E-07	-0.6144274E-09
	-0.4005959E-03	-0.3682637E-07	0.1483175E-02	-0.1224710E-06	-0.1457667E-10	-0.5176899E-03
	-0.3383097E-05	0.1451319E-02	0.8839655E-05	-0.2146430E-08	-0.4283381E-04	0.5495522E-04
	0.4859211E-04	-0.2280121E-04				
35	0.5097553E-13	-0.1473330E-13	0.7373682E-04	0.2442374E-11	-0.2924509E-13	-0.1255348E-04
	0.1100371E-12	-0.4946515E-11	0.8619373E-11	-0.2943769E-11	0.1469339E-15	0.3425569E-11
	-0.3572634E-11	-0.6131955E-10	-0.1114561E-09	-0.6124177E-14	-0.4222072E-09	0.3376937E-09
	0.3559627E-09	-0.2001997E-08				
36	-0.5764374E-04	-0.1666565E-11	-0.7695166E-12	-0.1262840E-04	-0.5040624E-10	-0.2531673E-11
	-0.8245795E-05	-0.5072869E-09	-0.3591671E-05	-0.2507896E-09	0.9977501E-13	-0.1230306E-05
	-0.4739393E-09	0.4679105E-06	0.2740178E-08	-0.2722204E-11	-0.7223980E-07	0.9363470E-07
	0.1055598E-05	-0.5101155E-07				
37	0.1050006E-11	-0.5363605E-04	-0.8495091E-12	-0.4974328E-10	-0.1265583E-04	-0.6835649E-11
	0.1736992E-02	-0.8234211E-05	0.1944728E-09	-0.3639195E-05	-0.5102213E-13	0.7986888E-08
	-0.129573E-05	0.2536297E-08	-0.4674023E-06	-0.7788530E-10	-0.9394927E-07	-0.7355226E-07
	0.5146445E-07	0.1052124E-06				

COORDINATES OF MASS POINT 6

T-MATRIX FOR MASS POINT 7

5 ROWS, 6 COLUMNS

C.0	0.100000E 01	0.0	0.0	0.0	0.0
C.0	0.0	0.100000E 01	0.0	0.0	0.0
C.0	0.0	0.0	0.100000E 01	0.0	0.0
C.0	0.0	0.0	0.0	0.100000E 01	0.0
C.0	0.0	0.0	0.0	0.0	0.100000E 01

COORDINATES OF MASS POINT 7

37	C.4547971E-09	-C.11797917E-01	0.1050574E-09	0.2132693E-07	0.5371325E-02	-0.5184246E-09
	-C.5097435E-07	0.1009174E-02	0.5914441E-07	-0.1241761E-02	0.4908234E-10	-0.8044924E-05
	0.1332504E-02	-0.1203827E-04	0.1977554E-02	0.6203157E-07	0.1087382E-03	0.6529493E-04
	-0.533706E-04	-C.11080970E-03				
38	C.11377523E-01	0.4349761E-09	0.6172658E-10	-0.5377244E-02	0.2148294E-07	-0.7243346E-09
	-C.1033239E-02	-C.5410094E-07	0.1250555E-02	0.1040321E-06	-0.4845242E-10	-0.1233110E-02
	-C.9030404E-05	0.1977175E-02	0.1210366E-04	-0.7689852E-08	-0.8415259E-04	0.1081812E-03
	C.1055345E-03	-C.5143217E-04				
39	0.4556344E-13	-C.1422494E-13	0.7071880E-04	0.2173461E-11	-0.2860187E-13	-0.1197538E-04
	0.2024014E-11	0.1291945E-12	0.2814795E-11	-0.2115907E-11	0.6632052E-15	-0.3186224E-11
	-0.1491716E-10	-C.5005737E-10	-0.1957227E-09	0.1602701E-12	-0.4756628E-09	0.1938809E-09
	0.4477495E-09	-0.3760633E-08				
40	-0.5237517E-04	-C.1626991E-11	-0.7289709E-12	-0.9458077E-05	0.3783190E-10	-0.2289604E-11
	-0.7071520E-05	-C.4489262E-09	-C.3559494E-05	-C.2247516E-09	0.1311944E-12	-0.2764711E-05
	-0.1923837E-07	-C.6444932E-06	-0.3976916E-08	0.5341873E-12	-0.3547722E-07	0.4545558E-07
	0.6263633E-07	-C.2496979E-07				
41	0.1090455E-11	-0.5236930E-04	-0.6554517E-12	-0.3717950E-10	-0.9484636E-05	-0.5136964E-11
	0.2540243E-09	-C.7066294E-05	0.1898172E-09	-0.3599279E-05	0.5163443E-12	0.1800074E-07
	-C.2759546E-05	-C.3040109E-08	0.6450202E-06	0.5715709E-10	-0.4620402E-07	-0.3599879E-07
	0.2598505E-07	0.6157524E-07				

A-16

T-MATRIX FOR MASS POINT 8

5 ROWS, 6 COLUMNS

C.0	0.100000E 01	0.0	0.0	0.0	0.0
C.0	0.0	0.100000E 01	0.0	0.0	0.0
C.0	0.0	0.0	0.100000E 01	0.0	0.0
C.0	0.0	0.0	0.0	0.100000E 01	0.0
C.0	0.0	0.0	0.0	0.0	0.100000E 01

COORDINATES OF MASS POINT 8

42	0.1369013E-09	-C.4104249E-02	0.7202273E-10	0.1287320E-07	0.3248407E-02	-0.7945304E-09
	-C.8345375E-07	0.952092E-03	0.2259412E-07	-0.4753647E-03	0.1654328E-08	-0.2379916E-04
	0.3647375E-02	-C.4010903E-05	-0.6574520E-03	-0.6033451E-07	-0.2417710E-04	-0.1893405E-04
	0.1075355E-04	0.2175942E-04				
43	0.4102472E-02	0.1278637E-09	-0.1069388E-10	-C.3249677E-02	0.1300631E-07	-0.4640281E-09
	-0.5833591E-03	-C.6058309E-07	0.4826672E-03	0.5302029E-07	0.7322955E-10	-0.3647703E-02
	-C.2380204E-04	-C.6578790E-03	-0.4085610E-05	0.9222829E-09	0.1879692E-04	-0.2402415E-04
	-0.2215530E-04	0.1034410E-04				
44	0.2019190E-13	-C.6540276E-14	0.3516150E-04	0.1651500E-11	-0.2300074E-13	-0.6001943E-05
	0.1173757E-10	0.1050477E-09	0.1122418E-09	-0.2654557E-10	0.4399476E-15	0.3552406E-10
	0.1375227E-09	-C.5496739E-09	-C.6195262E-09	0.7482902E-12	-0.3758677E-08	0.3108364E-08

N

45	C.4512155E-03	-C.1347262E-07	-C.9665931E-12	-C.2996879E-12	C.1016520E-04	-0.4121033E-10	0.1150043E-11
	-0.3102778E-04	-C.9665931E-12	-C.2996879E-12	-C.2757901E-05	-0.240402E-09	0.6780264E-12	C.2629457E-05
	C.1631849E-05	0.1356176E-09	-C.6633697E-05	-C.476200E-07	C.4508534E-10	C.3590136E-06	-0.4703703E-06
	0.1711913E-07	-C.6633697E-05	C.2453702E-06	0.1555817E-12	0.4085743E-10	0.1015182E-04	-0.1420983E-11
	-0.5343840E-04	-C.3103318E-04	0.1608211E-05	0.1313537E-09	-0.2742132E-05	-0.1371348E-11	-0.1713027E-07
46	0.8365716E-12	-C.3103318E-04	0.1608211E-05	0.1313537E-09	-0.2742132E-05	-0.1371348E-11	-0.1713027E-07
	0.8372651E-10	-C.4026345E-07	-C.5221339E-04	0.6595683E-05	0.8364871E-09	0.4637600E-06	0.3655105E-06
	0.2621632E-05	-C.5221339E-04					
	-C.2550408E-04						

** MODUL 2 **

MASS POINT LOCATIONS IN LOCAL COORDINATES

MASS NO.	COORDINATES		
1	0.1320000E 03	0.0	0.0
2	0.2590000E 03	0.0	0.0
3	0.3720000E 03	0.0	0.0
4	0.4920000E 03	0.0	0.0

COORDINATES OF POINT 0
 0.9010000E 03 0.0 0.0
 COORDINATES OF POINT A
 0.1000000E 01 0.0 0.0
 COORDINATES OF POINT B
 0.0 0.0 -0.1000000E 01

A-17

MASS POINT LOCATIONS IN ABSOLUTE GLOBAL COORDINATES

MASS NO.	COORDINATES		
1	0.5010000E 03	0.0	-0.1320000E 03
2	0.8010000E 03	0.0	-0.2520000E 03
3	0.8310000E 03	0.0	-0.3720000E 03
4	0.8010000E 03	0.0	-0.4920000E 03

MASS AND MOMENTS OF INERTIA IN LOCAL COORDINATES

MASS NO.	MASS	INERTIA MATRIX		
1	C.1617494E 02	0.4994825E 05	0.0	0.0
		0.0	C.4865425E 05	0.0
		0.0	0.0	C.4813666E 05
2	0.1617494E 02	0.4994825E 05	0.0	0.0
		0.0	C.4865425E 05	0.0
		0.0	0.0	C.4813666E 05
3	0.1617494E 02	0.4994825E 05	0.0	0.0
		0.0	C.4865425E 05	0.0
		0.0	0.0	C.4813666E 05

4 0.1517494E 02 0.4904825E 05 0.0 0.0 C.C
 0.0 C.4865425E 05 0.0 0.0 C.C
 0.0 0.0 0.0 0.0 0.4813666F 05

DEFAULT T-MATRIX FOR MODULE 2

6 ROWS, 6 COLUMNS

0.100000F 01	0.0	0.0	0.0	0.0	0.0
0.0	0.100000F 01	0.0	0.0	0.0	0.0
0.0	0.0	0.100000F 01	0.0	0.0	0.0
0.0	0.0	0.0	0.100000E 01	0.0	0.0
0.0	0.0	0.0	0.0	0.100000F 01	0.0
0.0	0.0	0.0	0.0	0.0	0.100000E 01

SUBSTRUCTURE MODAL MATRIX

ROW NO.

COORDINATES OF MASS POINT 1

1	-0.1901051E-13	0.1142261E-11	0.4210550E-10	-0.7403088E-10	-0.2354611E-12	-0.1760001E-03
	-0.1152474E-09	0.3629624E-10	-0.1574351E-09	-0.1817733E-10		
2	0.4374490E-07	0.2961727E-03	-0.1188117E-06	-0.4335255E-03	-0.3692930E-09	0.1903980E-09
	-0.8978691E-07	0.4197797E-03	0.8460453E-04	-0.2973401E-03		
3	-0.2961124E-03	0.4417892E-07	0.433091E-03	-0.1234335E-06	0.3884362E-09	-0.2632639E-09
	0.4198232E-03	0.1239013E-06	0.2976498E-03	0.8450562E-06		
4	-0.5939573E-13	-0.2336877E-13	0.8576365E-11	0.3087777E-11	-0.4231177E-05	-0.2978269E-13
	-0.1321075E-11	-0.2410089E-11	-0.2406160E-11	-0.1445873E-10		
5	0.3563408E-05	-0.5438570E-09	-0.4955211E-06	0.1313326E-05	0.3007885E-13	-0.2654950E-12
	0.3592785E-06	0.8781902E-10	0.1029374E-05	0.2901647E-08		
6	0.5855695E-09	0.3963214E-05	-0.1324487E-09	-0.4955928E-06	0.4009986E-12	0.1851103E-12
	0.7928499E-10	-0.3541915E-06	-0.2892503E-08	0.1019246E-05		

COORDINATES OF MASS POINT 2

7	-0.4856255E-13	0.2919636E-11	0.1031810F-09	-0.1823023F-09	-0.5751668E-12	-0.4256910E-03
	-0.2485531E-03	0.7638178E-10	-0.3010829E-09	-0.2836582F-10		
8	0.1854239E-05	0.1254493E-02	-0.221059E-06	-0.8070320E-03	-0.3655343E-09	0.2203610E-09
	-0.2701753E-07	0.1274800E-03	-0.9008836E-05	0.3171777E-03		
9	-0.1254381E-02	0.1870263E-06	0.8070411E-03	-0.2296765E-06	0.7820735E-09	0.2684424E-09
	0.1261253E-03	0.3981160E-07	-0.3172413E-03	-0.9001471E-06		
10	0.3334790E-14	-0.3992733E-15	0.1568526E-10	0.5219753E-11	-0.8699092E-05	0.1701074E-13
	-0.2257803E-11	-0.4512868E-11	-0.2878850F-12	-0.1265825E-10		
11	0.136430E-05	-0.1098059E-08	0.1403117E-05	-0.3995317E-09	0.1155445E-11	0.2590962E-12
	0.1132945E-05	0.3320839E-09	0.9827036E-06	0.278931E-08		
12	0.108348E-09	0.7363753E-05	0.3822107E-09	0.1402237F-05	0.3675712E-11	-0.2910222E-12
	0.2415441E-09	-0.1132445E-05	-0.2756888E-08	0.9656496E-06		

COORDINATES OF MASS POINT 3

13	-0.2617017E-11	0.2827315E-11	0.2244906E-09	-0.2035671E-09	0.5805596E-11	-0.6148973E-03
	0.4206595E-10	0.9295687E-10	-0.2363669E-11	-0.1055531E-09		
14	0.2657034E-05	0.2474043E-02	-0.1116898E-06	-0.4111426E-03	-0.3432190E-09	0.1351719E-09
	0.8175577E-07	-0.3604024E-03	0.5262114E-04	-0.1858108E-03		
15	-0.2473572E-02	0.3688750E-06	0.4116769E-03	-0.1168454E-06	0.4072838E-09	0.1825706E-09
	-0.3821817E-03	-0.1134342E-05	0.1847346E-03	0.5246659E-06		
16	0.2405223E-14	-0.4137737E-15	0.1982489E-10	0.7436334E-11	-0.1204278E-04	0.2461058E-13
	0.6336399E-12	0.1243150E-11	-0.4077314E-12	0.7508257E-11		
17	0.5069062E-05	-0.1356711E-08	0.4376129E-05	-0.1245374E-08	0.3666199E-11	0.1464055E-11
	-0.6445630E-06	-0.1940963E-09	0.7505835E-06	0.2143019E-08		
18	0.1745139E-08	0.9097773E-05	0.1192687E-08	0.4372656E-05	0.1568056E-11	-0.1223043E-11
	-0.1412011E-09	0.6416846E-06	-0.2091698E-08	0.7316312E-06		
COORDINATES OF MASS POINT 4						
19	-0.4022739E-11	0.2815221E-11	0.2846121E-09	-0.2252179E-09	-0.8105800E-11	-0.7167356E-03
	0.2137242E-09	0.4504359E-10	0.2271534E-09	-0.9008722E-10		
20	0.5521939E-05	0.3735249E-02	0.1351884E-06	0.4946615E-03	0.3227008E-09	-0.1404600E-09
	-0.1401112E-07	0.1588804E-03	-0.3145836E-07	0.1145350E-04		
21	-0.3735312E-02	0.5558453E-06	-0.4939714E-03	0.1405608E-06	-0.5093581E-09	-0.1712908E-09
	0.1522268E-03	0.4510236E-07	-0.9915710E-05	-0.2950568E-07		
22	0.2583002E-14	-0.4252957E-15	0.2276551E-10	0.8576882E-11	-0.1383013E-04	0.2862262E-13
	0.2794030E-11	0.5604158E-11	0.1135867E-11	0.8462345E-11		
23	0.5559438E-05	-0.1431318E-08	0.5854582E-05	-0.1664697E-08	0.3873740E-11	0.2117521E-11
	-0.2637456E-05	-0.7806880E-09	0.1921135E-05	0.5470763E-08		
24	0.1419064E-05	0.9597700E-05	0.1593665E-08	0.5848151E-05	0.2884141E-11	-0.1786774E-11
	-0.5591588E-09	0.2627386E-05	-0.5393446E-08	0.1893904E-05		

A-19

** MODULE 3 **

MASS POINT LOCATIONS IN LOCAL COORDINATES

MASS NO.	COORDINATES			
1	0.1320000E 03	0.0	0.0	0.0
2	0.2520000E 03	0.0	0.0	0.0
3	0.3720000E 03	0.0	0.0	0.0
4	0.4920000E 03	0.0	0.0	0.0
COORDINATES OF POINT 0				
	0.2010000E 03	0.0	0.0	0.0
COORDINATES OF POINT A				
	0.0	0.1000000E C1	C.C	C.C

COORDINATES OF POINT 1
 C.C 0.10000000 01

MASS POINT LOCATIONS IN ABSOLUTE GLOBAL COORDINATES

MASS NO.	COORDINATES
1	0.8010000E 03 0.0 0.1320000E 03
2	0.8010000E 03 0.0 0.2520000E 03
3	0.8010000E 03 0.0 0.3720000E 03
4	0.8010000E 03 0.0 0.4920000E 03

MASS AND MOMENTS OF INERTIA IN LOCAL COORDINATES

MASS NO.	MASS	INERTIA MATRIX
1	0.1517454E 02	0.4094825E 05 0.0 0.0 0.0 0.4865425E 05 0.0 0.0 0.0 0.4813666E 05
2	0.1517454E 02	0.4994825E 05 0.0 0.0 0.0 0.4865425E 05 0.0 0.0 0.0 0.4813666E 05
3	0.1517454E 02	0.4994825E 05 0.0 0.0 0.0 0.4865425E 05 0.0 0.0 0.0 0.4813666E 05
4	0.1517454E 02	0.4994825E 05 0.0 0.0 0.0 0.4865425E 05 0.0 0.0 0.0 0.4813666E 05

A-20

DEFAULT T-MATRIX FOR MODULE 3

6 ROWS, 6 COLUMNS	0.0	0.0	0.0	0.0	0.0
0.100000E 01	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0

SUBSTRUCTURE GLOBAL MATRIX

FCW NO.	COORDINATES OF MASS POINT	1
1	-0.1501051E-13	0.1142261E-11 0.4210950E-10 -0.7403088E-10 -0.2354611E-12 -0.1760001E-03
	-0.1152876E-09	0.3528624E-10 -0.1574351E-09 -0.1817733E-10 -0.4352555E-03 -0.2973401E-03
2	0.4374490E-07	0.2961727E-03 -0.1198117E-06 0.8460453E-06 -0.1234335E-06 0.3884362E-09
	-0.6578691E-07	0.4197787E-03 0.8460453E-06 -0.2973401E-03 -0.8450562E-06 -0.2632639E-09
3	-0.2561126E-03	0.4417822E-07 0.4333991E-07 -0.1234335E-06 0.3884362E-09 -0.2632639E-09
	0.4159232E-03	0.1239013E-06 0.2970498E-03 -0.2973401E-03 0.8450562E-06 -0.2632639E-09

4	-C.535173E-17	-C.2338877E-13	0.8576359E-11	0.3087777E-11	-0.4231177E-05	-0.2978269E-13
	-C.1921075E-11	-C.2410089E-11	-C.2406616E-11	-0.1445873E-10		
5	C.3563405E-05	-0.5838570E-09	-0.4955231E-06	0.1313326E-05	C.3007895E-13	-0.2654950E-12
	C.353274E-06	C.8781902E-10	C.1029374E-05	C.2901647E-08		
6	C.5855690E-09	0.3963214E-05	-0.1324487E-09	-0.4955928E-06	C.4005986E-12	0.1851103E-12
	0.7923430E-10	-0.3541915E-06	-0.2892503E-08	0.1019246E-05		
COORDINATES OF MASS POINT 2						
7	-C.4856296E-13	0.2919636E-11	C.1031810E-09	-0.1823023E-09	-0.5751668E-12	-0.4256910E-03
	-C.2486531E-09	0.7638178E-10	-0.3010829E-09	-0.2836582E-10		
8	C.1854229E-06	0.1254493E-02	-0.2217059E-06	-0.8070320E-03	-0.3655343E-09	0.2203610E-09
	-C.279179E-07	0.1274800E-03	-0.9008839E-06	0.317177E-03		
9	-C.128439E-02	0.1870263E-06	C.8070411E-03	-0.2296765E-06	0.7820735E-09	0.2684424E-09
	C.1291260E-03	C.3981160E-07	-0.3172413E-03	-0.9001471E-06		
10	C.2334790E-14	-C.3992733E-15	0.1568526E-10	0.5219753E-11	-0.8699092E-05	0.1701074E-13
	-C.2257809E-11	-C.4512489E-11	-C.2875850E-12	-C.1265825E-10		
11	C.7364430E-05	-C.1098059E-08	C.1403117E-05	-0.3995317E-09	0.1155445E-11	0.2590962E-12
	0.1132839E-05	C.3329399E-09	0.9827036E-06	0.2788931E-09		
12	C.10F8638E-08	0.7363753E-05	C.3822107E-09	0.1402237E-05	0.3675712E-11	-0.2910222E-12
	0.2415441E-02	-0.1132445E-05	-C.2756888E-08	0.9656496E-06		
COORDINATES OF MASS POINT 3						
13	-0.2613017E-11	C.2827315E-11	C.2244906E-09	-0.2035671E-09	0.5805596E-11	-0.6148973E-03
	C.429556E-10	C.9298687E-10	-0.2363469E-11	-0.1055531E-09		
14	C.2657059E-06	0.2474043E-02	-0.1116898E-06	-0.4111426E-03	-0.3432190E-09	0.1351719E-09
	C.8175977E-07	-0.3804028E-03	C.5282114E-06	-0.1858108E-03		
15	-0.2473972E-02	0.3688750E-06	0.4116769E-03	-0.1168454E-06	0.4072838E-09	0.1625706E-09
	-0.3801417E-03	-0.1134342E-06	0.1847546E-03	0.5246650E-06		
16	0.2405223E-14	-0.4137737E-15	0.1982489E-10	0.7436374E-11	-0.1204278E-04	0.2461058E-13
	0.5836399E-12	C.1243150E-11	-0.4077314E-12	0.7508257E-11		
17	0.5059062E-05	-0.1356711E-08	0.4376129E-05	-0.1245374E-08	0.3666199E-11	0.1464055E-11
	-0.6445630E-06	-C.1880963E-09	0.7505835E-06	0.2143015E-08		
18	0.1245139E-08	0.9097773E-05	C.1192687E-08	0.4372656E-05	0.1568055E-11	-0.1223043E-11
	-0.1412011E-09	0.6416846E-06	-0.2091058E-08	0.7316312E-06		
COORDINATES OF MASS POINT 4						
19	-0.4022739E-11	C.2915221E-11	0.2846121E-09	-0.2252179E-09	-0.8105800E-11	-0.7167356E-03
	C.2137262E-02	0.4804359E-10	C.2271534E-09	-0.9008722E-10		
20	0.5521939E-05	0.3735249E-02	0.1351884E-06	0.4946615E-03	0.3227008E-09	-0.1104660E-09
	-0.2401112E-07	C.1588904E-03	-0.3145936E-07	0.1145350E-04		
21	-0.2735112E-02	0.558453E-06	-C.4939714E-03	0.1405604E-06	-0.5093281E-09	-0.1712906E-09
	0.1592259E-03	C.4510236E-07	-C.9915710E-05	-0.2950569E-07		

22	0.268300E-14	-0.4252957E-15	0.2276951E-10	0.8576882E-11	-0.1383017E-04	0.2862262E-13
	0.2794697E-11	0.5604158E-11	0.1135867E-11	0.8462346E-11		
23	0.5608438E-05	-0.1431318E-08	0.5854982E-05	-0.1664697E-08	0.3873740E-11	0.2117521E-11
	-0.2637456E-05	-0.7806886E-09	0.1921175E-05	0.5470767E-08		
24	0.1419264E-09	0.0607700E-05	0.1593669E-08	0.5848151E-05	0.2884141E-11	-0.1786774E-11
	-0.581988E-07	0.2627385E-05	-0.5393446E-08	0.1893904E-05		

** MODULE 4 **

MASS POINT LOCATIONS IN LOCAL COORDINATES

MASS NO.	COORDINATES		
1	0.132000E 03	0.0	0.0
2	0.252000E 03	0.0	0.0
3	0.372000E 03	0.0	0.0
4	0.492000E 03	0.0	0.0

COORDINATES OF POINT 2		
0.561000E 03	0.0	0.0

COORDINATES OF POINT 4		
0.100000E 01	0.0	0.0

COORDINATES OF POINT 3		
0.0	0.0	-0.100000E 01

MASS POINT LOCATIONS IN ABSOLUTE GLOBAL COORDINATES

MASS NO.	COORDINATES		
1	0.561000E 03	0.0	-0.132000E-03
2	0.561000E 03	0.0	-0.252000E 03
3	0.561000E 03	0.0	-0.372000E 03
4	0.561000E 03	0.0	-0.492000E 03

MASSSES AND MOMENTS OF INERTIA IN LOCAL COORDINATES

MASS NO.	MASS	INERTIA MATRIX		
1	0.1617454E 02	0.4994825E 05	0.0	0.0
		0.0	0.4865425E 05	0.0
		0.0	0.0	0.4813666E-05
2	0.1617494E 02	0.4994825E 05	0.0	0.0
		0.0	0.4865425E 05	0.0
		0.0	0.0	0.4813666E 05
3	0.1617444E 02	0.4994825E 05	0.0	0.0
		0.0	0.4865425E 05	0.0
		0.0	0.0	0.4813666E 05
4	0.1617454E 02	0.4994825E 05	0.0	0.0
	0.0	0.4865425E 05	0.0	0.0

0.0 0.0 0.481366E C5

0.0

0.0

DEFAULT T-MATRIX FOR MODULE 4

6 ROWS, 6 COLUMNS	C.0	0.0	0.0	0.0	0.0
C.100000E 01	C.0	0.0	0.0	0.0	0.0
C.0	0.100000E 01	0.0	0.0	0.0	0.0
0.0	0.0	C.100000E 01	0.0	0.0	0.0
0.0	0.0	0.0	C.100000E 01	0.0	0.0
0.0	0.0	0.0	0.0	C.100000E 01	0.0
0.0	0.0	0.0	0.0	0.0	C.100000E 01

SUPSTRUCTURE MODAL MATRIX

ROW NO.

COORDINATES OF MASS POINT 1

1	-0.1701951E-13	0.1142261E-11	0.4216550E-10	-0.7403088E-10	-0.2354611E-12	-0.1760001E-03
	-0.1182678E-09	0.3628624E-10	-0.1574351E-09	-0.1817733E-10		
2	0.4374490E-07	0.2561727E-03	-0.1188117E-06	-0.4335255E-03	-0.3692930E-09	0.1903580E-05
	-0.9578691E-07	0.4197787E-03	0.8480453E-06	-0.2973401E-03		
3	-0.2851126E-03	0.4417892E-07	0.4333991E-03	-0.1234335E-06	0.3884362E-09	-0.2632639E-09
	0.4198232E-03	0.1239013E-06	-0.2970498E-03	0.8480453E-06		
4	-0.8393873E-13	-0.2336877E-13	0.8576369E-11	0.3087777E-11	-0.4231177E-05	-0.2978269E-13
	-0.1821075E-11	-0.2410089E-11	-0.2406160E-11	-0.1445873E-10		
5	0.3531409E-05	-0.5838570E-09	-0.4955231E-06	0.1313326E-09	0.3007885E-13	-0.2654950E-12
	0.3532278E-06	0.8781902E-10	0.1029374E-05	0.2901647E-06		
6	0.5955690E-09	0.3963214E-05	-0.1324487E-09	-0.4955928E-06	0.4009866E-12	0.1851103E-12
	0.7928480E-19	-0.3541915E-06	-0.2892503E-08	0.1019246E-05		

A-23

COORDINATES OF MASS POINT 2

7	-0.4856256E-13	0.2919636E-11	0.1031810E-09	-0.1823023E-09	-0.5751668E-12	-0.4256910E-03
	-0.2496531E-09	0.7638178E-10	-0.3010829E-09	-0.2836582E-10		
8	0.1654229E-05	0.1254493E-02	-0.2217059E-06	-0.8070320E-03	-0.3655343E-09	0.2203610E-09
	-0.2791793E-07	0.1274800E-03	-0.9008836E-06	0.3171777E-03		
9	-0.1254383E-02	0.187263E-05	0.8070411E-03	-0.2296765E-06	0.7820735E-09	0.2684424E-09
	0.1251250E-03	0.3981160E-07	-0.3172413E-03	-0.9001471E-06		
10	0.2334790E-14	-0.3992733E-15	0.1568526E-10	0.5219753E-11	-0.8699092E-05	0.1701074E-13
	-0.2257909E-11	-0.4512868E-11	-0.2875850E-12	-0.1265825E-10		
11	0.7344430E-05	-0.1098059E-08	0.1403117E-05	-0.3995317E-09	0.1155445E-11	0.2590962E-12
	0.1132835E-05	0.3329939E-09	0.9827036E-06	0.2788931E-08		
12	0.1088638E-08	0.7363753E-05	0.3822107E-09	0.1402237E-05	0.3675712E-11	-0.2910222E-12
	0.2415441E-09	-0.1132445E-05	-0.2756888E-08	0.9656496E-06		

COORDINATES OF MASS POINT 3

13	-0.2511017E-11	0.2927315E-11	0.2249066E-06	-0.42035671E-09	0.5805596E-11	-0.6148973E-03
	0.4226596E-10	0.9298697E-10	-0.236349E-11	-0.1055531E-09		
14	0.3657054E-06	0.2474044E-02	-0.1116858E-06	-0.4111426E-03	-0.3432190E-09	0.1351719E-09
	0.9175077E-07	-0.3904024E-03	0.5262114E-06	-0.11859109E-03		
15	-0.2473979E-02	0.3688750E-06	0.4116749E-03	-0.1168454E-06	0.4072838E-09	0.1825706E-09
	-0.2901817E-03	-0.1134342E-06	0.1847546E-03	0.5246650E-06		
16	0.2405223E-14	-0.4137737E-15	0.1982489E-10	0.7436334E-11	-0.1204278E-04	0.2461058E-13
	0.6836399E-12	0.1243150E-11	-0.4077314E-12	0.7506257E-11		
17	0.5009062E-05	-0.1336711E-08	0.4376129E-05	-0.1245374E-08	0.3666199E-11	0.1454055E-11
	-0.6445530E-06	-0.1840963E-09	0.7505835E-06	0.2143015E-08		
18	0.1245139E-08	0.9097773E-05	0.1192687E-08	0.4372656E-05	0.1568058E-11	-0.1223043E-11
	-0.1412011E-09	0.6416846E-06	-0.2091098E-08	0.7316312E-06		

COORDINATES OF MASS POINT 4

19	-0.4022739E-11	0.2815221E-11	0.2846121E-09	-0.2252179E-09	-0.8105800E-11	-0.7167356E-03
	0.6137282E-07	0.4504359E-10	0.2271534E-09	-0.9008722E-10		
20	0.3521930E-06	0.3735249E-02	0.1351884E-06	0.4946615E-03	0.3227008E-09	-0.1404600E-09
	-0.3401113E-07	0.1588904E-03	-0.3145936E-07	0.1145350E-04		
21	-0.3735112E-02	0.5569453E-06	-0.4939714E-03	0.1405608E-06	-0.5093581E-09	-0.1712908E-09
	0.1562253E-03	0.4510236E-07	-0.9915710E-05	-0.2950568E-07		
22	0.2689009E-14	-0.4252657E-15	0.2276951E-10	0.9576882E-11	-0.1383013E-04	0.2862262E-13
	0.2734909E-11	0.5404158E-11	0.1135867E-11	0.8462346E-11		
23	0.5559438E-05	-0.1431318E-08	0.5854982E-05	-0.1664697E-08	0.3873740E-11	0.2117521E-11
	-0.2637455E-03	-0.7906980E-09	0.1921135E-05	0.5470763E-08		
24	0.1417064E-08	0.9597700E-05	0.1593669E-08	0.5848151E-05	0.2884141E-11	-0.1786774E-11
	-0.5691693E-09	0.2627386E-05	-0.5393446E-08	0.1893904E-05		

** MOBILE 5 **

MASS POINT LOCATIONS IN LOCAL COORDINATES

MASS NO.	COORDINATES
1	0.1200000E 03 0.0 0.0
2	0.2520000E 03 0.0 0.0
3	0.3720000E 03 0.0 0.0
4	0.4920000E 03 0.0 0.0

COORDINATES OF POINT 0

0.5100000E 01	0.0
---------------	-----

COORDINATES OF POINT A

0.0	0.1000000E 01 0.0
-----	-------------------

COORDINATES OF POINT B

0.0	0.0	0.1000000E 01
-----	-----	---------------

MASS POINT LOCATIONS IN ABSOLUTE GLOBAL COORDINATES

MASS NO. COORDINATES

1	0.5610000E 03	0.0	0.1320000E 03
2	0.5610000E 03	0.0	0.2320000E 03
3	0.5610000E 03	0.0	0.3720000E 03
4	0.5610000E 03	0.0	0.4920000E 03

MASSES AND MOMENTS OF INERTIA IN LOCAL COORDINATES

MASS NO. MASS

1	0.1617494E 02	0.4994825E 05	0.0	0.0	0.0	0.4813666E 05
2	0.1617494E 02	0.4994825E 05	0.0	0.0	0.0	0.4813666E 05
3	0.1617494E 02	0.4994825E 05	0.0	0.0	0.0	0.4813666E 05
4	0.1617494E 02	0.4994825E 05	0.0	0.0	0.0	0.4813666E 05

INERTIA MATRIX

DEFAULT T-MATRIX FOR MODULE 5

5 ROWS, 5 COLUMNS

0.1000000E 01	0.0	0.0	0.0	0.0
0.0	0.1000000E 01	0.0	0.0	0.0
0.0	0.0	0.1000000E 01	0.0	0.0
0.0	0.0	0.0	0.1000000E 01	0.0
0.0	0.0	0.0	0.0	0.1000000E 01

A-25

SUBSTRUCTURE MODAL MATRIX

RCW NO.

COORDINATES OF MASS POINT 1

1	-0.1901051E-13	0.1142261E-11	0.4210950E-10	-0.7403088E-10	-0.2354611E-12	-0.1760001E-03
	-0.1152675E-09	0.3628624E-10	-0.1574351E-09	-0.1817733E-10		
2	0.4174595E-07	0.2961727E-03	-0.1188117E-06	-0.4335255E-03	-0.3692930E-09	0.1903980E-09
	-0.8578651E-07	0.4197787E-03	0.8460453E-06	-0.2973401E-03		
3	-0.2961126E-03	0.4417892E-07	0.4333991E-03	-0.1234335E-06	0.3884362E-09	-0.2632639E-09
	0.4193232E-03	0.1239013E-06	0.2970498E-03	0.8450562E-06		
4	-0.8393573E-13	-0.2336877E-13	0.8576369E-11	0.3087777E-11	-0.4231177E-05	-0.2978269E-13
	-0.1921075E-11	-0.2410089E-11	-0.2406160E-11	-0.1445873E-10		

5	0.356340E-05	-0.5938570E-09	-0.4955231E-06	0.1313326E-09	0.3007885E-13	-0.2654950E-12
	0.3339279E-05	0.8781902E-10	0.1029374E-05	0.2901647E-08		
6	0.3555530E-02	0.3263214E-05	-0.1324687E-09	-0.4955928E-05	0.4009986E-12	0.1951103E-12
	0.723433E-10	-0.3541915E-06	-0.2892503E-08	0.1019246E-05		
COORDINATES OF MASS POINT 2						
7	-0.4556256E-13	0.2919636E-11	0.1031810E-09	-0.1823023E-09	-0.5751668E-12	-0.4256910E-03
	-0.2495531E-02	0.7639179E-10	-0.3010829E-09	-0.2836582E-10		
8	0.1154225E-05	0.1254493E-02	-0.2217059E-05	-0.8070320E-03	-0.3655343E-09	0.2203610E-09
	-0.2791793E-17	0.1274800E-03	-0.9008836E-06	0.317177E-03		
9	-0.1254393E-02	0.1870263E-06	0.8070411E-03	-0.2296765E-06	0.7820735E-09	0.2684424E-05
	0.1291259E-03	0.3981160E-07	-0.3172413E-03	-0.9001471E-06		
10	0.2334750E-14	-0.3592733E-15	0.1568526E-10	0.5219753E-11	-0.8699092E-05	0.1701074E-13
	-0.2257909E-11	-0.4512868E-11	-0.2875850E-12	-0.1265825E-10		
11	0.1364430E-05	-0.1098059E-08	0.1403117E-05	-0.3995317E-09	0.1155445E-11	0.2590962E-12
	0.1122935E-05	0.3329839E-09	9.9827636E-06	0.2788931E-08		
12	0.1084633E-08	0.7363753E-05	0.3822107E-09	0.1402237E-05	0.3675712E-11	-0.2910222E-12
	0.2415441E-09	-0.1132445E-05	-0.2756888E-09	-0.9656496E-06		

COORDINATES OF MASS POINT 3

13	-0.2513117E-11	0.2827315E-11	0.2244906E-09	-0.2035671E-09	0.5805596E-11	-0.6148973E-03
	0.4355543E-10	0.9298687E-10	-0.2363469E-11	-0.1055531E-09		
14	0.7657054E-06	0.2474043E-02	-0.1116898E-06	-0.4111426E-03	-0.2422190E-09	0.1351719E-09
	0.6175977E-07	-0.3804024E-03	0.5262114E-06	-0.1858108E-03		
15	-0.2473572E-02	0.3688759E-06	0.4116769E-03	-0.1168454E-06	0.4072838E-09	0.1825706E-09
	-0.3931817E-03	-0.1134342E-06	0.1847546E-03	0.5246650E-06		
16	0.2405233E-14	-0.4137737E-15	0.1982489E-10	0.7436334E-11	-0.1204278E-04	0.2461058E-13
	0.6836394E-12	0.1243150E-11	-0.4077314E-12	0.7508257E-11		
17	0.6099062E-05	-0.1356711E-08	0.4376129E-05	-0.1245374E-08	0.3666199E-11	0.1464055E-11
	-0.6445630E-06	-0.1440963E-09	0.7505835E-06	0.2143015E-08		
18	0.1345139E-08	0.9097773E-05	0.1192687E-08	0.4372656E-05	0.1568056E-11	-0.1223043E-11
	-0.1412011E-09	0.6416846E-06	-0.2091098E-08	0.7316312E-06		

COORDINATES OF MASS POINT 4

19	-0.4022739E-11	0.2815221E-11	0.2846121E-09	0.2252179E-09	0.8105800E-11	0.7167356E-03
	0.2137262E-09	0.4504359E-10	0.2271534E-09	-0.9008722E-10		
20	0.5521939E-06	0.3735249E-02	-0.1351284E-06	-0.4946615E-03	0.2227088E-09	-0.1404600E-09
	-0.3431112E-07	0.1588804E-03	-0.3145836E-07	0.1145350E-04		
21	-0.3739312E-02	0.5569453E-06	-0.4939714E-03	0.1405688E-06	-0.5093581E-09	0.1712908E-09
	0.1582299E-03	0.4510236E-07	-0.9915710E-05	-0.2950568E-07		
22	0.2583025E-14	-0.4252957E-15	0.2276951E-10	0.8576982E-11	-0.1383013E-04	0.2862262E-13
	0.2794090E-11	0.5604159E-11	0.1135867E-11	0.8462346E-11		

2

23 0.5509439E-05 -0.143118E-08 0.5854952E-05 -0.1664697E-08 0.3873740E-11 0.2117521E-11
 -0.2637455E-05 -0.7806880E-09 0.1921135E-05 0.5470763E-06
 24 0.1419066E-03 0.9597700E-05 0.1593669E-08 0.5848151E-05 0.2894141E-11 -0.1786774E-11
 -0.5591589E-09 0.2627386E-05 -0.5393486E-08 0.1893904E-05

** MODULE 6 **

MASS POINT LOCATIONS IN LOCAL COORDINATES

MASS NO.	COORDINATES
1	0.1320000E 03 0.0 0.0
2	0.2520000E 03 0.0 0.0
3	0.3720000E 03 0.0 0.0
4	0.4920000E 03 0.0 0.0

COORDINATES OF POINT 0
 0.910000E 03 0.0 0.0
 COORDINATES OF POINT A
 0.100000E 01 0.0 0.0
 COORDINATES OF POINT B
 0.100000E 01 0.0 0.0

MASS POINT LOCATIONS IN ABSOLUTE GLOBAL COORDINATES

MASS NO.	COORDINATES
1	0.8010000E 03 0.1320000E 03 0.0
2	0.8010000E 03 0.2520000E 03 0.0
3	0.8010000E 03 0.3720000E 03 0.0
4	0.8010000E 03 0.4920000E 03 0.0

MASSSES AND MOMENTS OF INERTIA IN LOCAL COORDINATES

MASS NO.	MASS	INERTIA MATRIX			
1	0.1617454E 02	0.4994825E 05	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0
2	0.1617494E 02	0.4994825E 05	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0
3	0.1617494E 02	0.4994825E 05	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0
4	0.1617454E 02	0.4994825E 05	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0

DEFAULT T-MATRIX FOR MODULE 6

6 ROWS, 6 COLUMNS

0.100000E 01	0.0	0.0	0.0	0.0	0.0
0.0	0.100000E 01	0.0	0.0	0.0	0.0
0.0	0.0	0.100000E 01	0.0	0.0	0.0
0.0	0.0	0.0	0.100000E 01	0.0	0.0
0.0	0.0	0.0	0.0	0.100000E 01	0.0
0.0	0.0	0.0	0.0	0.0	0.100000E 01

SUBSTRUCTURE MODAL MATRIX

ROW NO.

COORDINATES OF MASS POINT 1

1	-0.1931051E-13	0.1142261E-11	0.4210950E-10	-0.7403088E-10	-0.2354611E-12	-0.1760001E-03
	-0.1152675E-09	0.3628624E-10	-0.1574351E-09	-0.181773E-10		
2	0.4374490E-07	0.2961727E-03	-0.1188117E-06	-0.4335255E-03	-0.3692930E-09	0.1903980E-09
	-0.8578691E-07	0.4197787E-03	0.8460453E-06	-0.2973401E-03		
3	-0.3961126E-03	0.4417892E-07	0.4333991E-03	-0.1234335E-06	0.3884362E-09	-0.2632639E-09
	0.4198232E-03	0.1239013E-06	0.2970498E-03	-0.8450562E-06		
4	-0.8393573E-13	-0.2333687E-13	0.8576369E-11	0.3087777E-11	-0.4231177E-05	-0.2978269E-13
	-0.1921075E-11	-0.2410089E-11	-0.2406160E-11	-0.1449873E-10		
5	0.3963409E-05	-0.5838570E-09	-0.4955231E-06	0.1313326E-09	0.3007895E-13	-0.2654950E-12
	0.359278E-06	0.8781902E-10	0.1029374E-05	0.2901647E-08		
6	0.5855690E-05	0.3963214E-05	-0.1324487E-09	-0.4955928E-06	0.4009586E-12	0.1851103E-12
	0.7229490E-10	-0.3541915E-06	-0.2892503E-08	-0.1019246E-05		

COORDINATES OF MASS POINT 2

7	-0.4856296E-13	0.2919636E-11	0.1031810E-09	-0.1823023E-09	-0.5751668E-12	-0.4256910E-03
	-0.2486531E-09	0.7638179E-10	-0.3010829E-09	-0.2836582E-10		
8	0.1654229E-04	0.1254493E-02	-0.2317059E-06	-0.8070320E-03	-0.2655343E-09	0.2203610E-09
	-0.2791753E-07	0.1274900E-03	-0.9008836E-05	0.3171777E-03		
9	-0.1258387E-02	0.1870263E-06	0.8070411E-03	-0.2296765E-06	0.7820735E-09	0.2684424E-09
	0.1291260E-03	0.3981160E-07	-0.3172413E-03	-0.9001471E-06		
10	0.334790E-14	-0.3992733E-15	0.1568526E-10	0.5219753E-11	-0.8699092E-05	0.1701074E-13
	-0.2257909E-11	-0.4512969E-11	-0.2875950E-12	-0.1265825E-10		
11	0.734430E-05	-0.1098059E-08	0.1403117E-05	-0.3995317E-09	0.1155445E-11	0.2590962E-12
	0.1132835E-05	0.3329839E-09	0.9827036E-06	0.2788931E-08		
12	0.1089638E-08	0.7363753E-05	0.3822107E-09	0.1402237E-05	0.3675712E-11	-0.2910222E-12
	0.2415441E-03	-0.1132445E-05	-0.2756888E-08	0.9656496E-06		
COORDINATES OF MASS POINT 3						
13	-0.2533017E-11	0.2827315E-11	0.2244908E-09	-0.2035671E-09	-0.5805596E-11	-0.6148973E-03
	0.4295585E-10	0.9298087E-10	-0.2363466E-11	-0.1055511E-09		

14	0.36570645-06	0.2474043E-02	-0.1111699F-06	-0.4111424E-03	-0.3432190E-09	0.1351719E-09
	0.517597E-07	-0.3904024E-03	0.5262114E-06	-0.1858108E-03		
15	-0.247397E-02	0.3688750E-06	0.4116769E-03	-0.1168454E-06	0.4072838E-09	0.1825706E-09
	-0.7901817E-03	-0.1174342E-06	0.1847546E-03	0.5246650E-06		
16	0.2405223E-14	-0.4137737E-15	0.1982489E-10	0.7436334F-11	-0.1204278E-04	0.2461058E-13
	0.6936399E-12	0.1243150E-11	-0.4077314E-12	0.7508257E-11		
17	0.5099062E-05	-0.1356711E-08	0.4376129E-05	-0.1245374E-08	0.3666199E-11	0.1464055E-11
	-0.6445630E-05	-0.1840963E-09	0.7505835E-06	0.2143015E-08		
18	0.1245139E-09	0.9097773E-05	0.1192687E-08	0.4372656E-05	0.1568056E-11	-0.1223043E-11
	-0.1412011E-09	0.6416846E-06	-0.2091098E-08	0.7316312E-06		

COORDINATES OF MASS POINT 4

19	-0.402739E-11	0.2815221E-11	0.2846121E-09	-0.2252179E-09	-0.8105800E-11	-0.7167356E-03
	0.2137262E-09	0.4504359E-10	0.2271534E-09	-0.9008722E-10		
20	0.5521939E-06	0.3735249E-02	0.1351884E-06	0.4946615E-03	0.3227008E-09	-0.1404600E-09
	-0.340112E-07	0.1588804E-03	-0.3145836E-07	0.1145350E-04		
21	-0.3735312E-02	0.5569453E-06	-0.4935714E-03	0.1405608E-06	-0.5093581E-09	-0.1712908E-09
	0.1592299E-03	0.4510236E-07	-0.9915710E-05	-0.2950568E-07		
22	0.268902E-14	-0.4252957E-15	0.2276951E-10	0.8576882E-11	-0.1383013E-04	0.2862262E-13
	0.2794090E-11	0.5604159E-11	0.1135867E-11	0.8462346E-11		
23	0.9599439E-05	-0.1431318E-08	0.5854982E-05	-0.1664697E-08	0.3873740E-11	0.2117521E-11
	-0.2637456E-05	-0.7806980E-09	0.1921135E-05	0.5470763E-08		
24	0.1419064E-08	0.9597700E-05	0.1593669E-08	0.5848151E-05	0.2884141E-11	-0.1786774E-11
	-0.5681988E-09	0.2627386E-05	-0.5393446E-08	0.1893904E-05		

A-29

** MODULE 7 **

MASS POINT LOCATIONS IN LOCAL COORDINATES

MASS NO.	COORDINATES
1	0.1220000E 03 0.0 0.0
2	0.2520000E 03 0.0 0.0
3	0.3720000E 03 0.0 0.0
4	0.4920000E 03 0.0 0.0

COORDINATES OF POINT 0 0.0 0.0

COORDINATES OF POINT A 0.0 0.0 0.1000000E 01

COORDINATES OF POINT B 0.0 0.0 -0.1000000E 01 0.0

MASS POINT LOCATIONS IN ABSOLUTE GLOBAL COORDINATES

14

COORDINATES

1	0.5010000E 03	-0.1320000E 03	0.0
2	0.8010000E 03	-0.2520000E 03	0.0
3	0.9010000E 03	-0.3720000E 03	0.0
4	0.8010000E 03	-0.4920000E 03	0.0

MASS AND MOMENTS OF INERTIA IN LOCAL COORDINATES

MASS NO.	MASS	INERTIA MATRIX		
1	0.1517494E 02	0.4994825E 05	0.0	0.0
		0.0	0.4865425E 05	0.0
		0.0	0.0	0.4813666E 05
2	0.1517494E 02	0.4994825E 05	0.0	0.0
		0.0	0.4865425E 05	0.0
		0.0	0.0	0.4813666E 05
3	0.1517494E 02	0.4994825E 05	0.0	0.0
		0.0	0.4865425E 05	0.0
		0.0	0.0	0.4813666E 05
4	0.1517494E 02	0.4994825E 05	0.0	0.0
		0.0	0.4865425E 05	0.0
		0.0	0.0	0.4813666E 05

DEFAULT T-MATRIX FOR MODULE 7

6 ROWS, 6 COLUMNS	1	2	3	4	5
0.100000E 01	0.0	0.0	0.0	0.0	0.0
0.0	0.100000E 01	0.0	0.0	0.0	0.0
0.0	0.0	0.100000E 01	0.0	0.0	0.0
0.0	0.0	0.0	0.100000E 01	0.0	0.0
0.0	0.0	0.0	0.0	0.100000E 01	0.0
0.0	0.0	0.0	0.0	0.0	0.100000E 01

SUBSTRUCTURE MODAL MATRIX

PCW NO.	COORDINATES OF MASS POINT 1					
1	-0.1901051E-13	0.1142261E-11	0.4210950E-10	-0.7403088E-10	-0.2354611E-12	-0.1760001E-03
	-0.1152674E-09	0.3628624E-10	-0.1574351E-09	-0.1817733E-10		
2	0.4374490E-07	0.2561727E-03	-0.1188117E-06	-0.4335255E-03	-0.3692930E-09	0.1903980E-09
	-0.6978651E-07	0.4197787E-03	0.8460453E-06	-0.2973401E-03		
3	-0.2561124E-03	0.4417892E-07	0.4333991E-03	-0.1234335E-06	0.3884362E-09	-0.2632639E-09
	0.4199232E-03	0.1239013E-06	0.2970498E-03	0.8450562E-06		
4	-0.6393571E-13	-0.2336877E-13	0.6576369E-11	0.1087777E-11	-0.4231177E-05	-0.2978269E-13
	-0.1921075E-11	-0.2410089E-11	-0.2406160E-11	-0.1445873E-10		
5	0.3063409E-05	-0.5836570E-09	-0.495231E-06	0.1313326E-09	0.3007885E-13	-0.2654950E-12
	0.3579278E-06	0.8781902E-10	0.1029374E-05	0.2901647E-08		

6 0.585560E-05 0.3963214E-05 -0.1324487E-09 -0.4955928E-06 0.4009986E-12 0.1951103E-12
 0.7523430E-10 -0.3541915E-06 -0.2892503E-08 0.1019246E-05

COORDINATES OF MASS POINT 2

7 -0.495560E-05 0.2919636E-11 0.1071810E-09 -0.1823023E-09 -0.5751668E-12 -0.4256510E-03
 -0.2486531E-09 0.7638178E-10 -0.3010829E-09 -0.2836582E-10

8 0.1654225E-05 0.1254493E-02 -0.2217059E-06 -0.8070320E-03 0.2203610E-09
 -0.2791793E-37 0.1274800E-03 -0.9008836E-06 0.3171777E-03

9 -0.1254383E-02 0.1870263E-06 0.8070411E-03 -0.2296765E-06 0.7820735E-09 0.2684424E-09
 0.1281260E-03 0.3981160E-07 -0.3172415E-03 -0.9001471E-06

10 0.3374790E-14 -0.3992733E-15 0.1568526E-10 0.5219753E-11 0.869902E-05 0.1701074E-13
 -0.2257409E-11 -0.4451286E-11 -0.2879650E-12 -0.1243825E-10

11 0.1344430E-05 -0.1098059E-08 0.1403117E-05 -0.3995317E-09 0.1155445E-11 0.2590962E-12
 -0.113283E-05 -0.3329632E-09 0.9827036E-06 0.2786931E-08

12 0.1088639E-09 0.7363753E-05 0.3822107E-05 0.1402237E-05 -0.3675712E-11 -0.2910222E-12
 0.2415841E-09 -0.1132435E-05 -0.2756888E-08 0.9656496E-06

COORDINATES OF MASS POINT 3

13 -0.2613017E-11 0.2827315E-11 0.2244906E-09 -0.2035671E-09 -0.5805596E-11 -0.6148973E-03
 0.4255595E-10 0.9298687E-10 -0.2363469E-11 -0.1055531E-09

14 0.3657054E-06 0.2474043E-02 -0.1111689E-06 -0.4111426E-03 0.3432190E-09 0.1351719E-09
 0.9175977E-07 -0.3904024E-03 0.5262114E-06 -0.1858108E-03

15 -0.247372E-02 0.3688750E-05 0.4116769E-03 -0.1168454E-06 0.4072838E-09 0.1825706E-09
 -0.3801817E-03 -0.1134342E-05 0.1847546E-03 0.5246650E-06

16 0.240523E-14 -0.4137737E-15 0.1982489E-10 0.7436334E-11 -0.1204278E-04 0.2461058E-13
 0.683639E-12 0.1243150E-11 -0.4077314E-12 0.7508257E-11

17 0.9009062E-05 -0.1356711E-08 0.4376129E-05 -0.1245374E-08 0.3666199E-11 0.1464059E-11
 -0.644563E-05 -0.1840963E-09 0.7505835E-06 0.2143015E-08

18 0.1345139E-08 0.909773E-05 0.1192687E-08 0.4372656E-05 0.1568056E-11 -0.1223043E-11
 -0.1412011E-09 0.6416846E-06 -0.2091098E-08 0.7316312E-06

COORDINATES OF MASS POINT 4

19 -0.4022739E-11 0.2815221E-11 0.2348121E-09 -0.2252179E-09 -0.8105800E-11 -0.7167356E-03
 0.2137262E-09 0.4504359E-10 0.2271534E-09 -0.9008722E-10

20 0.521939E-06 0.375249E-02 0.1951884E-06 0.4946615E-03 0.3227898E-09 -0.1404600E-09
 -0.3401112E-07 0.1588804E-03 -0.3145836E-07 0.1145350E-04

21 -0.373512E-02 0.556945E-06 -0.4939714E-03 0.1405608E-06 0.5093581E-09 0.1712908E-09
 0.1582249E-03 0.4510236E-07 -0.9915710E-05 -0.2950568E-07

22 0.268902E-14 -0.4252957E-15 0.2276951E-10 0.8576882E-11 0.1383813E-04 0.2862262E-13
 0.2794092E-11 0.5604158E-11 0.1135867E-11 0.8462346E-11

23 0.599438E-05 -0.1431319E-08 0.589482E-09 -0.1664697E-08 0.3873740E-11 0.2117921E-11
 -0.2637459E-05 -0.780680E-09 0.1921135E-05 0.5470763E-08

24 0.141904E-08 0.959770E-05 0.159366E-08 0.584815E-05 0.268414E-11 -0.178677E-11
 -0.558198E-09 0.262738E-05 -0.539344E-08 0.189390E-05

** MODULE 10 **

MASS POINT LOCATIONS IN LOCAL COORDINATES

MASS NO.	COORDINATES					
1	0.132000E 03	0.0	0.0	0.0	0.0	0.0
2	0.252000E 03	0.0	0.0	0.0	0.0	0.0
3	0.372000E 03	0.0	0.0	0.0	0.0	0.0
4	0.492000E 03	0.0	0.0	0.0	0.0	0.0
COORDINATES OF POINT 0						
	0.510000E 03	0.0	0.0	0.0	0.0	0.0
COORDINATES OF POINT A						
	0.100000E 01	0.0	0.0	0.0	0.0	0.0
COORDINATES OF POINT B						
	0.0	0.100000E 01	0.0	0.0	0.0	0.0

MASS POINT LOCATIONS IN ABSOLUTE GLOBAL COORDINATES

MASS NO.	COORDINATES					
1	0.551000E 03	0.132000E 03	0.0	0.0	0.0	0.0
2	0.561000E 03	0.252000E 03	0.0	0.0	0.0	0.0
3	0.561000E 03	0.372000E 03	0.0	0.0	0.0	0.0
4	0.561000E 03	0.492000E 03	0.0	0.0	0.0	0.0

MASS AND MOMENTS OF INERTIA IN LOCAL COORDINATES

MASS NO.	MASS	INERTIA MATRIX								
1	0.161745E 02	0.4994825E 05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0	0.0	0.0	0.0	0.0	0.0
2	0.151749E 02	0.4994825E 05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0	0.0	0.0	0.0	0.0	0.0
3	0.161745E 02	0.4994825E 05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0	0.0	0.0	0.0	0.0	0.0
4	0.161745E 02	0.4994825E 05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0	0.0	0.0	0.0	0.0	0.0

DEFAULT T-MATRIX FOR MODULE 10
 6 ROWS, 6 COLUMNS

0.100000E 01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.100000E 01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.100000E 01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.100000E 01	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.100000E 01	0.0	0.0	0.0	0.0	0.0

SUBSTRUCTURE MODAL MATRIX

FCW NO.

	COORDINATES OF MASS POINT 1									
1	-0.193105E-13	0.114226E-11	0.4210950E-10	-0.7403088E-10	-0.2354611E-12	-0.1760001E-03	-0.1152675E-07	0.3628524E-10	-0.1574351E-09	-0.1817733E-10
2	0.4374490E-07	0.2961727E-03	-0.118817E-06	-0.4335255E-03	-0.3692930E-09	0.1903980E-09	-0.9578691E-07	0.4197787E-03	0.8460453E-06	-0.2973401E-03
3	-0.2561126E-03	0.4417892E-07	0.4333991E-03	-0.1234335E-06	0.3884362E-09	-0.2632639E-09	0.4194232E-03	0.1239013E-06	0.2970498E-03	0.8350562E-06
4	-0.8393573E-13	-0.2336877E-13	0.8576365E-11	0.3087777E-11	-0.4231177E-05	-0.2978269E-13	-0.1821075E-11	-0.2410089E-11	-0.1445873E-10	-0.1445873E-10
5	0.3443408E-05	-0.5838570E-09	-0.4955231E-06	0.1313322E-09	0.3007885E-13	-0.2654950E-12	0.3533275E-06	0.8781902E-10	0.1029374E-05	0.2901647E-08
6	0.4453680E-05	0.3963214E-05	-0.1324487E-09	-0.4955928E-06	0.4009886E-12	0.1851103E-12	0.7929430E-10	-0.3541915E-08	-0.2892503E-08	0.1019246E-09

COORDINATES OF MASS POINT 2

7	-0.4456295E-13	0.2919636E-11	0.1031810E-09	-0.1823023E-09	-0.5751668E-12	-0.4256510E-03	-0.2486531E-09	0.7638178E-10	-0.3010829E-09	-0.2836582E-10
8	0.1854229E-06	0.1254493E-02	-0.2217059E-06	-0.8070320E-03	-0.3655343E-09	0.2203610E-09	-0.2791793E-07	0.1274800E-03	-0.9008836E-06	0.3171777E-03
9	-0.1254383E-02	0.1870263E-06	0.8070411E-03	-0.2296765E-06	0.7820735E-09	0.2684424E-09	0.1281260E-03	0.3981160E-07	-0.3172413E-03	-0.9001471E-06
10	0.3334790E-14	-0.3992733E-15	0.1568526E-10	0.5219753E-11	-0.8699092E-05	0.1701074E-13	-0.2257809E-11	-0.4512868E-11	-0.2875850E-12	-0.1265825E-10
11	0.7164433E-05	-0.1098059E-08	0.1403117E-05	-0.3995317E-09	0.1155445E-11	0.2590962E-12	0.1132835E-05	0.3329839E-09	0.9827036E-06	0.2788931E-08
12	0.1088438E-08	0.7363753E-05	0.3822107E-09	0.1402237E-05	0.3675712E-11	-0.2910222E-12	0.2415441E-09	-0.1132445E-05	-0.2756888E-08	0.9656496E-06
13	-0.2313017E-11	0.2827315E-11	0.2244966E-09	-0.2035671E-09	0.5865596E-11	0.66148973E-03	0.4295585E-10	0.9298687E-10	-0.2363469E-11	-0.1055531E-09
14	0.3957034E-08	0.2474043E-02	-0.1110898E-06	-0.4111426E-03	-0.3432130E-09	0.13511719E-09	0.8175977E-07	-0.3904024E-03	0.5262114E-06	-0.1858108E-03

COORDINATES OF MASS POINT 3

15	-0.2313017E-11	0.2827315E-11	0.2244966E-09	-0.2035671E-09	0.5865596E-11	0.66148973E-03	0.4295585E-10	0.9298687E-10	-0.2363469E-11	-0.1055531E-09
16	0.3957034E-08	0.2474043E-02	-0.1110898E-06	-0.4111426E-03	-0.3432130E-09	0.13511719E-09	0.8175977E-07	-0.3904024E-03	0.5262114E-06	-0.1858108E-03

15	-0.2473772E-02	0.7688750E-04	0.4114769E-03	-0.1164454E-06	0.4072838E-09	0.1825706E-09
	-0.3921517E-03	-0.1134342E-06	0.1847546E-03	0.5246650E-06		
16	0.2405233E-14	-0.4413773E-15	0.1982489E-10	0.7436324E-11	-0.1204278E-04	0.2461058E-13
	0.5876307E-12	0.1243150E-11	-0.4677314E-12	0.7508257E-11		
17	0.5093962E-05	-0.1756711E-08	0.4376129E-05	-0.1245374E-09	0.7666190E-11	0.1454055E-11
	-0.644530E-06	-0.1840063E-09	0.7505835E-06	0.2143015E-08		
18	0.1345130E-03	0.0097773E-05	0.1192687E-08	0.4372656E-05	0.1568056E-11	-0.1223043E-11
	-0.1312011E-09	0.6416844E-06	-0.2091098E-08	0.7316312E-06		
COORDINATES OF MASS POINT 4						
19	-0.4023739E-11	0.2815221E-11	0.2846121E-09	-0.2252179E-09	-0.4105809E-11	-0.7167356E-03
	0.2137252E-09	0.4504359E-10	0.2271534E-09	-0.6008722E-10		
20	0.5921933E-05	0.3735240E-02	0.1351884E-06	0.4946615E-03	0.3227038E-09	-0.1404600E-09
	-0.3401112E-07	0.1588904E-03	-0.3145836E-07	0.1145350E-04		
21	-0.3739712E-02	0.4556945E-06	-0.4939714E-03	0.1405608E-06	-0.5093581E-09	-0.1712908E-09
	0.1542234E-03	0.4510236E-07	-0.9915710E-05	-0.2950558E-07		
22	0.2594003E-14	-0.4425295E-15	0.2276951E-10	0.9576882E-11	-0.1383013E-04	0.2862262E-13
	0.2764090E-11	0.5604154E-11	0.1175867E-11	0.9462346E-11		
23	0.5594392E-05	-0.1431318E-08	0.5854932E-05	-0.1664697E-08	0.3973740E-11	0.2117521E-11
	-0.2637445E-03	-0.7806880E-09	0.1921135E-05	0.5470763E-08		
24	0.1410064E-09	0.6597700E-05	0.1593669E-08	0.5848151E-05	0.2884141E-11	-0.1786774E-11
	-0.5631083E-09	0.2627385E-05	-0.5393446E-08	0.1893904E-05		

** MODULE 11 **

A-34

MASS POINT LOCATIONS IN LOCAL COORDINATES

MASS NO.	COORDINATES			
1	0.1350000E 01	0.0	0.0	0.0
2	0.2520000E 01	0.0	0.0	0.0
3	0.3700000E 01	0.0	0.0	0.0
4	0.4590000E 01	0.0	0.0	0.0

COORDINATES OF POINT 0

0.5610000E 01 0.0

COORDINATES OF POINT A

0.0 0.1000000E 01

COORDINATES OF POINT B

0.0 -0.1000000E 01 0.0

MASS POINT LOCATIONS IN ABSOLUTE GLOBAL COORDINATES

MASS NO.	COORDINATES			
1	0.5610000E 01	-0.1320000E 03	0.0	0.0

2 0.561000E 03 -0.252000E 03 0.0
 3 0.561000E 03 -0.372000E 03 0.0
 4 0.561000E 03 -0.492000E 03 0.0

MASS AND MOMENTS OF INERTIA IN LOCAL COORDINATES

MASS NO.	MASS	INERTIA MATRIX					
1	0.1617494E 02	0.4994825E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0	0.0	0.0
2	0.1617494E 02	0.4994825E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0	0.0	0.0
3	0.1617494E 02	0.4994825E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0	0.0	0.0
4	0.1617494E 02	0.4994825E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4813666E 05	0.0	0.0	0.0

DEFAULT T-MATRIX FOR MODULE 11

6 ROWS, 6 COLUMNS	A-35					
0.100000E 01	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.100000E 01	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.100000E 01	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.100000E 01	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.100000E 01	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.100000E 01	0.0

SUBSTRUCTURE MODAL MATRIX

ROW NO.	COORDINATES OF MASS POINT 1											
1	-0.1901051E-13	0.1142261E-11	0.4210950E-10	-0.7403688E-10	-0.2354611E-12	-0.1760001E-03	-0.1152676E-09	0.3628624E-10	-0.1574351E-09	-0.1817733E-10	0.0	0.0
2	0.4374492E-07	0.2961727E-03	-0.1186117E-06	-0.4335255E-03	-0.3692930E-09	0.1903980E-09	-0.9578691E-07	0.4197787E-03	0.8460453E-06	-0.2973401E-03	0.0	0.0
3	-0.2061126E-03	0.4417892E-07	0.4333991E-03	-0.1234335E-06	0.3884362E-09	-0.2632639E-09	0.4198233E-03	0.1239013E-06	0.2970498E-03	0.8450562E-06	0.0	0.0
4	-0.9793575E-13	-0.2336877E-13	0.8576365E-11	0.3087777E-11	-0.4231177E-05	-0.2972669E-13	-0.1921075E-11	-0.2410089E-11	-0.2406160E-11	-0.1445873E-10	0.0	0.0
5	0.3539279E-06	0.8781902E-10	0.1029374E-05	0.495231E-06	0.1313326E-09	-0.2654950E-12	0.3563408E-05	0.8781902E-10	-0.5838570E-09	0.1029374E-05	0.0	0.0
6	0.5655490E-09	0.3963214E-05	-0.1324487E-09	-0.4955028E-06	0.2901647E-08	0.4009586E-12	0.5655490E-09	0.3963214E-05	-0.1324487E-09	-0.4955028E-06	0.0	0.0
	0.1929490E-10	-0.7541915E-06	-0.2892503E-08	-0.2892503E-08	-0.2892503E-08	0.1851103E-12	0.1929490E-10	-0.7541915E-06	-0.2892503E-08	-0.2892503E-08	0.0	0.0

COORDINATES OF MASS POINT 2

7	-0.465255E-13	0.2019634E-11	C.1031810E-00	-0.1823023E-09	-0.5751668E-12	-0.4256510E-03
	-0.2496531E-09	0.7638179E-10	-0.3010929E-09	-0.2836582E-10		
8	0.1054229E-05	0.1254453E-02	-0.2217050E-06	-0.8070320E-03	-0.3655343E-00	0.2203610E-09
	-0.2793793E-07	0.1274900E-03	-0.8008936E-06	0.3171777E-03		
9	-0.1264887E-03	0.1870263E-06	0.8070411E-03	-0.2286765E-06	0.7820735E-09	0.2684424E-09
	0.1281260E-07	0.3081142E-07	-0.3172413E-03	-0.9001471E-06		
10	0.3337903E-13	-0.7092733E-15	0.1568526E-10	0.5210753E-11	-0.8499082E-05	0.1701074E-13
	-0.2257509E-11	-0.4512965E-11	-0.2875850E-12	-0.1265825E-10		
11	0.7364430E-05	-0.1098059E-08	0.1403117E-05	-0.3995317E-09	0.1155445E-11	0.2590962E-12
	0.1173435E-05	0.3329839E-09	0.9827034E-06	0.2788931E-08		
12	0.108679E-08	0.7363753E-05	0.3822107E-00	0.1402237E-05	0.3675712E-11	-0.2910222E-12
	0.2415441E-09	-0.112445E-05	-0.2756888E-08	0.9656496E-06		

COORDINATES OF MASS POINT 3

13	-0.2613017E-11	0.2827315E-11	0.2244906E-09	-0.2035671E-09	0.5805596E-11	-0.6148973E-03
	0.4295355E-17	0.9298687E-10	-0.2363469E-11	-0.1055531E-09		
14	0.3657254E-06	0.2474043E-02	-0.1116898E-06	-0.4111426E-03	-0.3432190E-09	0.1351719E-09
	0.517577E-07	-0.3804024E-03	0.5262114E-06	-0.1858108E-03		
15	-0.2473572E-02	0.3368750E-06	0.4116769E-03	-0.1168454E-06	0.4072838E-09	0.1825706E-09
	-0.3801917E-03	-0.1134742E-05	0.1847546E-03	0.5246650E-06		
16	0.2405223E-14	-0.4337737E-15	0.1982489E-10	0.7436334E-11	-0.1204278E-04	0.2461058E-13
	0.6836389E-12	0.1243150E-11	-0.4077314E-12	0.7508257E-11		
17	0.909062E-05	-0.1356711E-08	0.4376129E-05	-0.1245374E-08	0.3666199E-11	0.1464055E-11
	-0.6445630E-05	-0.1840963E-09	0.7505835E-06	0.2143015E-08		
18	0.1345130E-08	0.909773E-05	0.1192687E-08	0.437656E-05	0.1568056E-11	-0.1223043E-11
	-0.1412011E-09	0.6416845E-06	-0.2091098E-08	0.7316312E-06		

COORDINATES OF MASS POINT 4

19	-0.4022730E-11	0.2815221E-11	0.2846121E-09	-0.2252179E-09	-0.8105800E-11	-0.7167356E-03
	0.2137262E-09	0.4504359E-10	0.2271534E-09	-0.9008722E-10		
20	0.5521935E-05	0.3735249E-02	0.1351884E-06	0.4946615E-03	0.3227008E-09	-0.1404600E-09
	-0.340112E-07	0.158804E-03	-0.3145836E-07	0.1145350E-04		
21	-0.373312E-02	0.5566453E-06	-0.4935714E-03	0.1405608E-06	-0.5093681E-09	-0.1712908E-09
	0.1582298E-03	0.4510236E-07	-0.9915710E-05	-0.2950568E-07		
22	0.268002E-14	-0.4252957E-15	-0.2276951E-10	0.8578882E-11	-0.1383013E-04	0.2862262E-13
	0.2794090E-11	0.5604158E-11	0.1135867E-11	0.8462346E-11		
23	0.5500438E-05	-0.1431318E-08	0.5854982E-05	-0.1664697E-08	0.39973740E-11	0.2117521E-11
	-0.2637455E-05	-0.7806880E-09	0.1921135E-05	0.5470763E-08		
24	0.1419064E-08	0.9507709E-08	0.1593669E-08	0.5848151E-05	0.2884141E-11	-0.1766774E-11
	-0.5581089E-07	0.2627386E-05	-0.5393446E-08	0.1893904E-05		

24

MASS AND MOMENTS OF INERTIA IN GLOBAL COORDINATES FOR MODULE 3

MASS NO.	MASS	INERTIA MATRIX					
1	0.1617494E 02	0.4865425E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4813666E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0
2	0.1617494E 02	0.4865425E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4813666E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0
3	0.1617494E 02	0.4865425E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4813666E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0
4	0.1617494E 02	0.4865425E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4813666E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0

MASS AND MOMENTS OF INERTIA IN GLOBAL COORDINATES FOR MODULE 4

MASS NO.	MASS	INERTIA MATRIX					
1	0.1617494E 02	0.4813666E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0
2	0.1617494E 02	0.4813666E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0
3	0.1617494E 02	0.4813666E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0
4	0.1617494E 02	0.4813666E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4865425E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0

MASS AND MOMENTS OF INERTIA IN GLOBAL COORDINATES FOR MODULE 5

MASS NO.	MASS	INERTIA MATRIX					
1	0.1617494E 02	0.4865425E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4813666E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0
2	0.1617494E 02	0.4865425E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4813666E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0
3	0.1617494E 02	0.4865425E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4813666E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0
4	0.1617494E 02	0.4865425E 05	0.0	0.0	0.0	0.0	0.0
		0.0	0.4813666E 05	0.0	0.0	0.0	0.0
		0.0	0.0	0.4894825E 05	0.0	0.0	0.0

C.C 0.4813666E 05 0.0
 C.C 0.4865425E 05

MASS AND MOMENTS OF INERTIA IN GLOBAL COORDINATES FOR MODULE 6

MASS NO.	MASS	INERTIA MATRIX		
1	0.1617454E 02	0.4813666E 05	0.0	0.0
		0.0	0.4865425E 05	0.0
		0.0	0.0	0.4865425E 05
2	0.1617454E 02	0.4813666E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4865425E 05
3	0.1617454E 02	0.4813666E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4865425E 05
4	0.1617454E 02	0.4813666E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4865425E 05

MASS AND MOMENTS OF INERTIA IN GLOBAL COORDINATES FOR MODULE 7

A-39

MASS NO.	MASS	INERTIA MATRIX		
1	0.1617454E 02	0.4865425E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4813666E 05
2	0.1617454E 02	0.4865425E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4813666E 05
3	0.1617454E 02	0.4865425E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4813666E 05
4	0.1617454E 02	0.4865425E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4813666E 05

MASS AND MOMENTS OF INERTIA IN GLOBAL COORDINATES FOR MODULE 10

MASS NO.	MASS	INERTIA MATRIX		
1	0.1617454E 02	0.4813666E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4865425E 05
2	0.1617454E 02	0.4813666E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4865425E 05

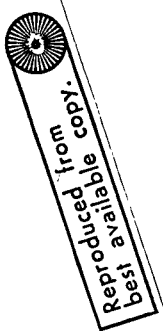
MASS. NO.	MASS	INERTIA MATRIX		
1	0.1617494E 02	0.4865425E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4813666E 05
2	0.1617494E 02	0.4865425E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4813666E 05
3	0.1617494E 02	0.4865425E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4813666E 05
4	0.1617494E 02	0.4865425E 05	0.0	0.0
		0.0	0.4994825E 05	0.0
		0.0	0.0	0.4813666E 05

MASSSES AND MOMENTS OF INERTIA IN GLOBAL COORDINATES FOR MODULE 11

MODULE FREQ NO. TOTAL MASS EIGENVALUE FREQUENCY SQUARED

1	1	0.5509695E 00	0.172945E 01
	2	0.5906735E 00	0.178526E 01
	3	0.3745032E 00	0.2677354E 01
	4	0.1558292E-01	0.5882268E 02
	5	0.1588056E-01	0.5923947E 02
	6	0.0577775E-02	0.1033205E 03
	7	0.2355901E-02	0.4432917E 03
	8	0.2234420E-02	0.475435E 03
	9	0.1867106E-02	0.5355879E 03
	10	0.1463210E-02	0.5367080E 03
	11	0.1201820E-03	0.2375920E 04
	12	0.2577717E-03	0.3806164E 04
	13	0.2526905E-03	0.3806763E 04
	14	0.8457765E-04	0.1180949E 05
	15	0.8464414E-04	0.1181417E 05
	16	0.5747479E-04	0.1477655E 05
	17	0.5188682E-04	0.1615853E 05
	18	0.6194609E-04	0.1616917E 05
	19	0.5713895E-04	0.1750119E 05
	20	0.5712801E-04	0.1750455E 05
2	21	0.3534654E-03	0.2751293E 04
	22	0.3337805E-03	0.2752257E 04
	23	0.2969785E-04	0.4353735E 05
	24	0.2740095E-04	0.4359194E 05
	25	0.2147169E-04	0.4657294E 05

26	C.1785715E-04	0.560002E 05
27	C.18286470E-05	C.1590718E 06
28	C.4331995E-05	C.1591851E 06
29	C.3914408E-05	C.2554665E 06
30	C.3911271E-05	C.2556715E 06
31	C.3634654E-03	0.2751293E 04
32	C.3633380E-03	C.2752257E 04
33	C.2296879E-04	C.4353735E 05
34	C.2294002E-04	C.4359194E 05
35	C.2147169E-04	C.4657296E 05
36	C.1785715E-04	C.560002E 05
37	C.5286470E-05	0.1590718E 06
38	C.5231995E-05	0.1591851E 06
39	C.3914408E-05	C.2554665E 06
40	C.3911271E-05	C.2556715E 06
41	C.3634654E-03	0.2751293E 04
42	C.3633380E-03	C.2752257E 04
43	C.2296879E-04	C.4353735E 05
44	C.2294002E-04	C.4359194E 05
45	C.2147169E-04	C.4657296E 05
46	C.1785715E-04	C.560002E 05
47	C.5286470E-05	0.1590718E 06
48	C.5231995E-05	0.1591851E 06
49	C.3914408E-05	C.2554665E 06
50	C.3911271E-05	C.2556715E 06
51	C.3634654E-03	0.2751293E 04
52	C.3633380E-03	C.2752257E 04
53	C.2296879E-04	C.4353735E 05
54	C.2294002E-04	C.4359194E 05
55	C.2147169E-04	C.4657296E 05
56	C.1785715E-04	C.560002E 05
57	C.5286470E-05	0.1590718E 06
58	C.5231995E-05	0.1591851E 06
59	C.3914408E-05	C.2554665E 06
60	C.3911271E-05	C.2556715E 06
61	C.3634654E-03	0.2751293E 04
62	C.3633380E-03	C.2752257E 04
63	C.2296879E-04	C.4353735E 05
64	C.2294002E-04	C.4359194E 05
65	C.2147169E-04	C.4657296E 05
66	C.1785715E-04	C.560002E 05
67	C.5286470E-05	0.1590718E 06
68	C.5231995E-05	0.1591851E 06
69	C.3914408E-05	C.2554665E 06
70	C.3911271E-05	C.2556715E 06
71	C.3634654E-03	0.2751293E 04
72	C.3633380E-03	C.2752257E 04
73	C.2296879E-04	C.4353735E 05
74	C.2294002E-04	C.4359194E 05
75	C.2147169E-04	C.4657296E 05
76	C.1785715E-04	C.560002E 05
77	C.5286470E-05	0.1590718E 06
78	C.5231995E-05	0.1591851E 06
79	C.3914408E-05	C.2554665E 06
80	C.3911271E-05	C.2556715E 06



10	P1	2.1634650E-07	0.2751293E 04
	P2	2.1633390E-07	0.2752267E 04
	P3	2.2256970E-04	0.4253735E 05
	P4	2.2294002E-04	0.4259194E 05
	P5	2.2147149E-04	0.4257295E 05
	P6	0.1735715E-04	0.5600002E 05
	P7	2.5286477E-05	0.1590719E 06
	P8	2.5281995E-05	0.1591851E 06
	P9	2.3914409E-05	0.2554665E 06
	P0	0.3011271E-05	0.2556715E 06
11	P1	2.7634454E-03	0.2751293E 04
	P2	0.3633390E-03	0.2752267E 04
	P3	0.2256979E-04	0.4253735E 05
	P4	0.2294002E-04	0.4259194E 05
	P5	0.2147149E-04	0.4257295E 05
	P6	0.1785715E-04	0.5600002E 05
	P7	0.5286477E-05	0.1590719E 06
	P8	0.5281995E-05	0.1591851E 06
	P9	0.3914409E-05	0.2554665E 06
	P0	0.3011271E-05	0.2556715E 06

CIRCULAR FREQUENCIES OF THE COUPLED SYSTEM

C.137619E 01	0.133520E 01	0.163539E 01	0.763929E 01	0.763944E 01	0.998457E 01
C.197131E 02	0.197134E 02	0.221189E 02	0.221205E 02	0.498243E 02	
C.524566E 03	0.524581E 03	0.524586E 03	0.524590E 03	0.583547E 03	
C.623634E 02	0.623647E 02				

MODAL SHAPE 1 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.9093519E-12	0.7316374E-04	0.499885E-01	-0.1467795E-10	-0.7406382E-04	0.1084008E-06
2	-0.9213724E-12	0.6665148E-04	0.455395E-01	-0.1474000E-10	-0.7406015E-04	0.1083956E-06
3	-0.3116320E-10	0.603023F-04	0.4101579E-01	-0.1453448E-10	-0.7383853E-04	0.1080707E-06
4	0.5882990E-10	0.468579E-04	-0.3201531E-01	-0.1410057E-10	-0.7396831E-04	0.1069415E-06
5	0.4285559E-11	0.4032665E-04	0.2755290E-01	-0.1388330E-10	-0.7251480E-04	0.1061313E-06
6	-0.6575751E-11	0.3378527E-04	0.2308361E-01	-0.1350489E-10	-0.7165801E-04	0.1048776E-06
7	0.0	0.2734403E-04	0.1867587E-01	-0.1287823E-10	-0.6996545E-04	0.1024066E-06
8	0.0	0.8025001E-05	0.5463683E-02	-0.14660828E-11	-0.4145961E-04	0.6068041E-07
9	0.0778120E-02	0.6663527E-04	0.4554002E-01	0.4510545E-10	-0.7406874E-04	0.1083971E-06
10	0.1867199E-01	0.666829E-04	0.4554066E-01	0.9124440E-10	-0.7411912E-04	0.1083588E-06
11	0.275744E-01	0.666373E-04	0.4554114E-01	0.1117360E-09	-0.7412125E-04	0.1084001E-06
12	0.7646307E-01	0.6669908E-04	0.4554143E-01	0.1168255E-09	-0.7412437E-04	0.1084007E-06
13	0.5778120E-02	0.6665915E-04	0.455402E-01	-0.7457358E-10	-0.7406741E-04	0.1083971E-06
14	-0.1867199E-01	0.6667566E-04	0.4554066E-01	-0.1206299E-09	-0.7411011E-04	0.1084001E-06
15	-0.275744E-01	0.6669463E-04	0.4554114E-01	-0.1410057E-10	-0.7412124E-04	0.1084001E-06
16	-0.3636395E-01	0.6671350E-04	0.4554140E-01	-0.1461734E-09	-0.7412434E-04	0.1084007E-06
17	0.9574071E-02	0.4032829E-04	0.2755317E-01	0.2233792E-10	-0.7254150E-04	0.1061329E-06
18	0.1928239E-01	0.4033555E-04	0.2755355E-01	0.5025874E-10	-0.72556375E-04	0.1061345E-06
19	0.2659221E-01	0.4034428E-04	0.2755395E-01	0.6266042E-10	-0.7257465E-04	0.1061350E-06
20	0.3570222E-01	0.4035301E-04	0.2755400E-01	0.6574158E-10	-0.7257769E-04	0.1061363E-06
21	-0.3574071E-02	0.403191E-04	0.2755317E-01	-0.5009385E-10	-0.7254150E-04	0.1061329E-06
22	-0.1928239E-01	0.4034254E-04	0.2755355E-01	-0.7793353E-10	-0.7256372E-04	0.1061345E-06
23	-0.2659221E-01	0.403545E-04	0.2755395E-01	-0.903189E-10	-0.7257461E-04	0.1061358E-06
24	-0.3570222E-01	0.403661E-04	0.2755400E-01	-0.9338222E-10	-0.7257765E-04	0.1061363E-06
25	-0.1431145E-04	0.6665212E-04	0.4554350E-01	0.4085215E-07	-0.7406122E-04	0.1084355E-06
26	-0.2732857E-04	0.6665305E-04	0.4554350E-01	0.7246274E-07	-0.7406237E-04	0.1084686E-06
27	-0.4034221E-04	0.6665375E-04	0.4554353E-01	0.8636221E-07	-0.7406325E-04	0.1084849E-06

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
28	-0.5376900E-04	0.6665415E-04	0.4557702E-01	0.8093653E-07	-0.7406369E-04	0.1084604E-06
29	-0.1431150E-04	0.6665212E-04	0.4553350E-01	-0.408108E-07	-0.7406122E-04	0.1084355E-06
30	0.2722861E-04	0.6665305E-04	0.4553615E-01	-0.729453F-07	-0.740627E-04	0.108467E-06
31	0.4076823E-04	0.6665375E-04	0.455635E-01	-0.8638864E-07	-0.740632E-04	0.1084850E-06
32	0.5236906E-04	0.6665415E-04	0.455704E-01	-0.896200E-07	-0.7406369E-04	0.108496E-06
33	-0.1401253E-04	0.4032704E-04	0.275527E-01	0.2471188E-07	-0.7251586E-04	0.1061704E-06
34	-0.2575774E-04	0.4032704E-04	0.2756118E-01	0.437961E-07	-0.7251586E-04	0.1062029E-06
35	-0.1956535E-04	0.4032803E-04	0.275684E-01	0.5224703E-07	-0.7251781E-04	0.106218E-06
36	-0.5225328E-04	0.403285E-04	0.275755E-01	0.5434013E-07	-0.725182E-04	0.1062232E-06
37	0.1401253E-04	0.4032704E-04	0.275527E-01	-0.247323E-07	-0.7251586E-04	0.1061704E-06
38	0.2575774E-04	0.4032704E-04	0.2756118E-01	-0.438050E-07	-0.7251586E-04	0.1062029E-06
39	0.1956535E-04	0.4032803E-04	0.275684E-01	-0.522725E-07	-0.7251781E-04	0.106218E-06
40	0.5225328E-04	0.403285E-04	0.275755E-01	-0.543745E-07	-0.725182E-04	0.1062234E-06

MODE SHAPE 2 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.8907493E-11	0.4998950E-01	-0.731698E-04	-0.1518382E-09	0.1084155E-06	0.7406472E-04
2	-0.341397E-11	0.4554021E-01	-0.6665602E-04	-0.1568887E-09	0.1084092E-06	0.7406101E-04
3	0.3765206E-09	0.4101637E-01	-0.6003273E-04	-0.1451284E-09	0.1080851E-06	0.7383943E-04
4	0.1621736E-09	0.3201570E-01	-0.4685450E-04	-0.1215890E-09	0.1059523E-06	0.7306823E-04
5	-0.5085434E-10	0.2755331E-01	-0.4032077E-04	-0.1098239E-09	0.1061361E-06	0.7251564E-04
6	-0.3434731E-10	0.2308307E-01	-0.337955E-04	-0.1067995E-09	0.1048807E-06	0.7165887E-04
7	0.0	0.1867611E-01	-0.2732853E-04	-0.1018446E-09	0.1024015E-06	0.6996637E-04
8	0.0	0.5483188E-02	-0.8022063E-05	-0.5091552E-10	0.6066995E-07	0.4166025E-04
9	-0.1431150E-04	0.4554411E-01	-0.6665669E-04	0.4071124E-07	0.1084481E-06	0.7406209E-04
10	-0.2731169E-04	0.4555419E-01	-0.6665764E-04	0.7222741E-07	0.1084804E-06	0.7406322E-04
11	-0.4335252E-04	0.455591E-01	-0.6665833E-04	0.8622266E-07	0.1084965E-06	0.7406408E-04
12	-0.5337373E-04	0.4557759E-01	-0.6665877E-04	0.866710E-07	0.1085101E-06	0.7406455E-04
13	0.14311309E-04	0.455441E-01	-0.6665669E-04	-0.4102431E-07	0.1084465E-06	0.7406209E-04
14	0.2731125E-04	0.4555427E-01	-0.6665764E-04	-0.7253857E-07	0.1084774E-06	0.7406322E-04
15	0.4335154E-04	0.455603E-01	-0.6665837E-04	-0.7253308E-07	0.1084928E-06	0.7406408E-04
16	0.5327233E-04	0.455773E-01	-0.6665874E-04	-0.8905644E-07	0.1084971E-06	0.7406455E-04
17	-0.1401204E-04	0.2755567E-01	-0.4032128E-04	0.2461653E-07	0.1062047E-06	0.7251669E-04
18	-0.2575345E-04	0.2755177E-01	-0.4032199E-04	0.4368471E-07	0.1062047E-06	0.7251783E-04
19	-0.3950615E-04	0.2757592E-01	-0.4032256E-04	0.5215230E-07	0.1062047E-06	0.7251669E-04
20	-0.5225405E-04	0.2755570E-01	-0.4032128E-04	-0.2483617E-07	0.106244E-06	0.7251669E-04
21	0.1401204E-04	-0.4032199E-04	-0.4032199E-04	-0.4390355E-07	-0.1062047E-06	0.7251783E-04
22	0.2575345E-04	0.2756893E-01	-0.4032256E-04	-0.5237084E-07	0.1062194E-06	0.7251669E-04
23	0.3950592E-04	0.2757602E-01	-0.4032285E-04	-0.5447248E-07	0.1062234E-06	0.7251911E-04
24	0.5225367E-04	0.4554665E-01	-0.6665625E-04	-0.2152221E-09	0.1084186E-06	0.7406887E-04
25	-0.579231E-02	0.4554129E-01	-0.6671615E-04	-0.258173E-09	0.1084122E-06	0.7411098E-04
26	-0.1957221E-01	0.4554177E-01	-0.6675122E-04	-0.2750500E-09	0.1084134E-06	0.7412213E-04
27	-0.2756776E-01	0.4554203E-01	-0.6678574E-04	-0.2785234E-09	0.1084140E-06	0.7412213E-04
28	-0.3646349E-01	0.4554065E-01	-0.6664109E-04	-0.9865384E-09	0.1084106E-06	0.7412524E-04
29	0.9792331E-02	0.4554129E-01	-0.6663696E-04	-0.553717E-10	0.1084122E-06	0.7408827E-04
30	0.1857221E-01	0.4554177E-01	-0.6663638E-04	-0.372252E-10	0.1084135E-06	0.7412213E-04
31	0.2756776E-01	0.4554177E-01	-0.6663144E-04	-0.339195E-10	0.1084135E-06	0.7412213E-04
32	0.3646349E-01	0.4554203E-01	-0.6663064E-04	-0.1458062E-09	0.106137E-06	0.7254235E-04
33	-0.5794194E-02	0.275535E-01	-0.403068E-04	-0.173784E-09	0.1061402E-06	0.725549E-04
34	-0.1929260E-01	0.2755396E-01	-0.4038427E-04	-0.196289E-09	0.1061402E-06	0.7257852E-04
35	-0.2699233E-01	0.275542E-01	-0.4040782E-04	-0.192301E-09	0.1061402E-06	0.7257852E-04
36	-0.3572266E-01	0.2755442E-01	-0.4040782E-04	-0.740835E-10	0.106137E-06	0.72554235E-04
37	0.9574134E-02	0.275535E-01	-0.403068E-04	-0.3482887E-10	0.1061391E-06	0.7256457E-04
38	0.1823260E-01	0.275536E-01	-0.4030537E-04	-0.4672887E-10	0.1061402E-06	0.7257545E-04
39	0.2699233E-01	0.2755426E-01	-0.4030265E-04	-0.3482892E-10	0.1061402E-06	0.7257545E-04
40	0.3572266E-01	0.2755442E-01	-0.4029936E-04	-0.320759E-10	0.1061408E-06	0.7257849E-04

MODE SHAPE 3 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.1117751E-11	0.0095362E-07	-0.2501746E-08	0.1100103E-03	0.3426748E-09	0.3426113E-09
2	-0.1117751E-11	0.7004841E-07	0.1864707E-07	0.1400709E-03	0.3413111E-09	0.3424843E-09
3	0.3450521E-11	0.342125E-07	0.3423333E-07	0.1291652E-03	0.3145422E-09	0.3255045E-09
4	-0.1146347E-10	0.1347037E-07	0.6444555E-07	0.12566748E-03	0.2654990E-09	0.2923635E-09
5	0.1194377E-12	0.3430511E-08	0.8027499E-07	0.1239271E-03	0.2460852E-09	0.2760163E-09
6	0.8134322E-12	-0.1519684E-07	0.6879067E-07	0.1205318E-03	0.2058116E-09	0.2495785E-09
7	0.0	-0.2665844E-07	0.9361452E-07	0.1149444E-03	0.1528705E-09	0.2137265E-09
8	0.0	-0.255309E-07	0.5560093E-07	0.5747579E-04	-0.1779649E-09	-0.4039284E-10
9	-0.4505433E-07	0.1728569E-01	0.1904132E-07	0.1309901E-03	0.3417628E-09	0.3424951E-09
10	-0.6300753E-07	0.3012243E-01	0.1960065E-07	0.1310402E-03	0.3409781E-09	0.3425066E-09
11	-0.1266555E-06	0.4974297E-01	0.2002455E-07	0.1310697E-03	0.3411516E-09	0.3425145E-09
12	-0.1674363E-06	0.6447417E-01	0.2022722E-07	0.1310779E-03	0.3413616E-09	0.3425182E-09
13	0.4507855E-07	-0.1724955E-01	0.1904140E-07	0.1309801E-03	0.3417402E-09	0.3424903E-09
14	0.3565355E-07	-0.3012121E-01	0.1960083E-07	0.1310403E-03	0.3411531E-09	0.3425007E-09
15	0.1267450E-06	-0.4874293E-01	0.2002455E-07	0.1310698E-03	0.3413074E-09	0.3425080E-09
16	0.1577433E-06	-0.6447405E-01	0.2022622E-07	0.1310785E-03	0.3414926E-09	0.3425111E-09
17	-0.3211509E-07	0.1635384E-01	0.8042474E-07	0.1279955E-03	0.2470283E-09	0.2760254E-09
18	-0.5051902E-07	0.3125179E-01	0.8063148E-07	0.1240524E-03	0.2408056E-09	0.2760343E-09
19	-0.4951803E-07	0.4614365E-01	0.8074900E-07	0.1240803E-03	0.2408056E-09	0.2760414E-09
20	-0.1133263E-06	0.6103594E-01	0.8087255E-07	0.1240881E-03	0.2402287E-09	0.2760414E-09
21	0.3203011E-07	-0.1635386E-01	0.8042480E-07	0.1239955E-03	0.2415030E-09	0.2760208E-09
22	0.5046915E-07	-0.3125179E-01	0.8063165E-07	0.1240524E-03	0.2391222E-09	0.2760254E-09
23	0.8365135E-07	-0.4614366E-01	0.8074900E-07	0.1240804E-03	0.2358017E-09	0.2760352E-09
24	0.1145543E-06	-0.6103601E-01	0.8087250E-07	0.1240882E-03	0.2365515E-09	0.2760376E-09
25	-0.4522101E-07	0.700559E-07	0.1728563E-01	0.1309801E-03	0.3419385E-09	0.3424826E-09
26	-0.6300753E-07	0.700559E-07	0.3301214E-01	0.1310403E-03	0.3406802E-09	0.3429901E-09
27	-0.1275715E-06	0.7005966E-07	0.4874290E-01	0.1310697E-03	0.3397378E-09	0.3430944E-09
28	-0.1587424E-06	0.7006037E-07	0.6447411E-01	0.1310779E-03	0.3392349E-09	0.3431051E-09
29	0.4522102E-07	0.7005144E-07	-0.1728560E-01	0.1309801E-03	0.3421292E-09	0.3427505E-09
30	0.6300757E-07	0.7005571E-07	-0.3301216E-01	0.1310403E-03	0.3410570E-09	0.3430092E-09
31	0.1275713E-06	0.7005917E-07	-0.4874289E-01	0.1310697E-03	0.3402749E-09	0.3431269E-09
32	0.1587423E-06	0.7006069E-07	-0.6447411E-01	0.1310780E-03	0.3398490E-09	0.3431522E-09
33	-0.3548173E-07	-0.3430100E-08	0.1636392E-01	0.1239955E-03	0.2447758E-09	0.2763534E-09
34	-0.6361525E-07	-0.3429515E-08	0.3125185E-01	0.1240524E-03	0.2433937E-09	0.2764222E-09
35	-0.1028101E-06	-0.3429141E-08	0.4614372E-01	0.1240803E-03	0.2423592E-09	0.2765055E-09
36	-0.1350933E-06	-0.3428942E-08	0.6103605E-01	0.1240881E-03	0.2418068E-09	0.2765117E-09
37	0.3548266E-07	-0.3430154E-08	-0.1636378E-01	0.1239955E-03	0.2448685E-09	0.2761715E-09
38	0.6361345E-07	-0.3429539E-08	-0.3125171E-01	0.1240525E-03	0.2436209E-09	0.2763356E-09
39	0.1027744E-06	-0.3429069E-08	-0.4614359E-01	0.1240804E-03	0.2426730E-09	0.2764080E-09
40	0.1350934E-06	-0.3428758E-08	-0.6103594E-01	-0.1240882E-03	0.2421670E-09	0.2764220E-09

MODE SHAPE 4 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.5127259E-09	-0.5170081E-02	-0.4299458E-02	0.1450821E-07	0.1009436E-03	-0.1215709E-03
2	-0.5245941E-09	0.2131044E-02	0.1772101E-02	0.1434879E-07	0.1009153E-03	-0.1215372E-03
3	-0.3654872E-09	0.9053439E-02	0.7718079E-02	0.6588703E-08	0.9357420E-04	-0.1126966E-03
4	-0.1137609E-08	0.2125757E-01	0.1765130E-01	-0.8926669E-08	0.7924491E-04	-0.9583952E-04
5	-0.2305057E-09	0.2651639E-01	0.2201772E-01	-0.1667851E-07	0.7231494E-04	-0.8709366E-04
6	-0.1377495E-08	0.2955089E-01	0.2454564E-01	-0.1628613E-07	0.6114682E-04	-0.7368453E-04
7	0.0	0.3137835E-01	0.2605475E-01	-0.1548875E-07	0.4575984E-04	-0.5511208E-04
8	0.0	0.1895670E-01	0.1574036E-01	-0.7767415E-08	-0.4925672E-04	0.5931982E-04
9	-0.1342026E-01	0.2141059E-02	0.1772376E-02	0.7837474E-07	0.1021557E-03	-0.1215953E-03
10	-0.2581243E-01	0.2158603E-02	0.1773378E-02	0.1773378E-06	0.1031891E-03	-0.1216569E-03
11	-0.3311619E-01	0.2173742E-02	0.1773946E-02	0.1499159E-06	0.1036952E-03	-0.1217029E-03

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
12	-0.5030349E-01	0.2149823E-02	0.1774313E-02	0.1554127E-06	0.1038374E-03	-0.1217275E-03
13	0.1349295E-01	0.2137249E-02	0.1775749E-02	-0.4939749E-07	0.1021554E-03	-0.1215953E-03
14	0.2891315E-01	0.2151234E-02	0.1773375E-02	-0.6865909E-07	0.1031884E-03	-0.1216599E-03
15	0.3811532E-01	0.2167894E-02	0.1773929E-02	-0.1205999E-06	0.1036953E-03	-0.1217029E-03
16	0.5030349E-01	0.2184447E-02	0.1774309E-02	-0.1266551E-06	0.1038364E-03	-0.1217275E-03
17	0.6516913E-02	0.2659009E-01	0.2202431E-01	0.7770455E-06	0.7394370E-04	-0.8713580E-04
18	0.1451124E-01	0.2679424E-01	0.2203685E-01	0.1390841E-05	0.7394416E-04	-0.8717946E-04
19	-0.2745707E-01	0.2701049E-01	0.2204249E-01	0.1663640E-05	0.7430749E-04	-0.8721244E-04
20	-0.3640901E-01	0.2723605E-01	0.2204658E-01	0.1731743E-05	0.7440870E-04	-0.8723037E-04
21	0.9516933E-02	0.2659452E-01	0.2202431E-01	-0.8109087E-06	0.7320318E-04	-0.8713580E-04
22	0.1351115E-01	0.2679282E-01	0.2203486E-01	-0.1424708E-05	0.7394351E-04	-0.8717946E-04
23	0.2745590E-01	0.2702322E-01	0.2204249E-01	-0.1698130E-05	0.7430563E-04	-0.8721244E-04
24	0.3640901E-01	0.2723295E-01	0.2204658E-01	-0.1766261E-05	0.7440773E-04	-0.8723037E-04
25	0.1519271E-01	0.2133322E-02	0.1774999E-02	0.6756710E-07	0.1009537E-03	-0.1230309E-03
26	0.311115E-01	0.2134705E-02	0.1793887E-02	0.1086153E-06	0.1010149E-03	-0.1242754E-03
27	0.4614523E-01	0.2135444E-02	0.1810856E-02	0.1267873E-06	0.1010531E-03	-0.1248862E-03
28	0.6115149E-01	0.2135840E-02	0.1827325E-02	0.1312686E-06	0.1010735E-03	-0.1250563E-03
29	0.1516270E-01	0.2133732E-02	0.1775160E-02	-0.3840174E-07	0.1009637E-03	-0.1230304E-03
30	0.3111117E-01	0.2134705E-02	0.1786482E-02	-6.7912570E-07	0.1010148E-03	-0.1242743E-03
31	0.4614523E-01	0.2135444E-02	0.1799923E-02	-0.9720321E-07	0.1010531E-03	-0.1248862E-03
32	0.6119123E-01	0.2135840E-02	0.1813298E-02	-0.1016777E-06	0.1010735E-03	-0.1250547E-03
33	0.1158219E-01	0.2652491E-01	0.2207853E-01	0.6425159E-06	0.7234985E-04	-0.8816407E-04
34	0.2222431E-01	0.2653760E-01	0.2223944E-01	0.1152017E-05	0.7238529E-04	-0.8905909E-04
35	0.3304517E-01	0.2654617E-01	0.2224702E-01	0.1379009E-05	0.7241371E-04	-0.8949357E-04
36	0.4384575E-01	0.2655110E-01	0.2226140E-01	0.1435584E-05	0.7242836E-04	-0.8961547E-04
37	0.1159215E-01	0.2652491E-01	0.2220330E-01	-0.4764881E-06	0.7234963E-04	-0.8816371E-04
38	0.2222431E-01	0.2653760E-01	0.2224490E-01	-0.1186445E-05	0.7238626E-04	-0.8905517E-04
39	0.3304517E-01	0.2654617E-01	0.2224983E-01	-0.1413630E-05	0.7241366E-04	-0.8949258E-04
40	0.4384515E-01	0.2655110E-01	0.2226310E-01	-0.1470230E-05	0.7242832E-04	-0.8961433E-04

MODE SHAPE 5 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.3057931E-09	-0.4300233E-02	0.5177636E-02	0.1885199E-07	-0.1215727E-03	-0.1009460E-03
2	0.3025915E-09	0.1771344E-02	-0.2134499E-02	0.1883443E-07	-0.1215391E-03	-0.1009180E-03
3	-0.8769132E-09	0.1751628E-02	-0.9054799E-02	0.1275905E-07	-0.1125981E-03	-0.9357692E-04
4	-0.3006504E-09	0.1765125E-01	-0.2125857E-01	0.5840835E-09	-0.9544096E-04	-0.7924758E-04
5	-0.1262493E-08	0.2201787E-01	-0.2651713E-01	-0.5498833E-08	-0.8709547E-04	-0.7231759E-04
6	-0.5211431E-09	0.2454584E-01	-0.2956179E-01	-0.5357567E-08	-0.7360608E-04	-0.6111697E-04
7	0.0	0.2605506E-01	-0.3137919E-01	-0.5113714E-08	-0.5511314E-04	-0.4576183E-04
8	0.0	0.1574064E-01	-0.1855179E-01	-0.2564989E-08	0.5932283E-04	0.4925612E-04
9	0.1511293E-01	0.1779921E-02	-0.2135175E-02	0.7209176E-07	-0.1230324E-03	-0.1009664E-03
10	0.3111149E-01	0.1794343E-02	-0.2136137E-02	0.1132635E-06	-0.1242766E-03	-0.1010175E-03
11	0.4614655E-01	0.1811921E-02	-0.2136865E-02	0.1316124E-06	-0.1248872E-03	-0.1010557E-03
12	0.6117229E-01	0.1829455E-02	-0.2137259E-02	0.1361889E-06	-0.1250957E-03	-0.1010761E-03
13	0.1516292E-01	0.1773915E-02	-0.2135177E-02	-0.3401753E-07	-0.1230319E-03	-0.1009664E-03
14	0.3111141E-01	0.1784718E-02	-0.2136141E-02	-0.7484380E-07	-0.1242756E-03	-0.1010175E-03
15	0.4614644E-01	0.1797657E-02	-0.2136870E-02	-0.9302234E-07	-0.1249959E-03	-0.1010957E-03
16	0.6115193E-01	0.1810541E-02	-0.2137263E-02	-0.9754882E-07	-0.1250558E-03	-0.1010761E-03
17	0.1159237E-01	0.2208017E-01	-0.2652263E-01	0.6537298E-06	-0.8816554E-04	-0.7235224E-04
18	0.2222445E-01	0.2224244E-01	-0.2653770E-01	0.1143194E-05	-0.8905710E-04	-0.7238682E-04
19	0.3304513E-01	0.2243134E-01	-0.2654685E-01	0.1390135E-05	-0.8949463E-04	-0.7241622E-04
20	0.4384513E-01	0.2261979E-01	-0.2655177E-01	0.1446690E-05	-0.8961651E-04	-0.7243096E-04
21	-0.1158237E-01	0.2209164E-01	-0.2652563E-01	-0.6649306E-06	-0.8816535E-04	-0.7235224E-04
22	-0.2222493E-01	0.2224528E-01	-0.2653770E-01	-0.1174522E-05	-0.8905672E-04	-0.7238882E-04
23	-0.3304593E-01	0.2243558E-01	-0.2654685E-01	-0.1401549E-05	-0.8949409E-04	-0.7241622E-04
24	-0.4384502E-01	0.2262531E-01	-0.2655177E-01	-0.1458109E-05	-0.8961596E-04	-0.7243085E-04
25	0.1342261E-01	0.1771915E-02	-0.2138040E-02	-0.4455919E-07	-0.1215972E-03	-0.1021584E-03
26	0.2893309E-01	0.1772723E-02	-0.2151425E-02	-0.9375555E-07	-0.1216597E-03	-0.1031919E-03

Reproduced from
best available copy.

MODE SHAPE	5 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS
27	-0.1036989E-03
28	-0.1039402E-03
29	-0.1021580E-03
30	-0.1031909E-03
31	-0.1036978E-03
32	-0.1038389E-03
33	-0.7320642E-04
34	-0.7394694E-04
35	-0.7431036E-04
36	-0.7441158E-04
37	-0.7320610E-04
38	-0.7394634E-04
39	-0.7430954E-04
40	-0.7441067E-04

MODE SHAPE 5 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X (1)	X (2)	X (3)	THETA (1)	THETA (2)	THETA (3)
1	0.3077030E-07	-0.2087203E-05	-0.1537038E-05	-0.1198681E-03	0.3207228E-08	-0.4236166E-07
2	0.5037373E-07	0.3571894E-06	-0.4286905E-06	-0.1197804E-03	0.2952533E-08	-0.4244658E-07
3	0.4715155E-07	0.2924204E-05	-0.5122479E-06	-0.5921380E-04	0.2870308E-08	-0.3957006E-07
4	0.2221135E-07	0.1772989E-05	0.8524122E-06	0.6494156E-04	0.8624852E-09	-0.3387296E-07
5	0.2260843E-07	0.8951062E-05	0.1852003E-05	0.1264481E-03	-0.1401855E-08	-0.3116445E-07
6	0.1261477E-07	0.1006699E-04	0.1802261E-05	0.1231238E-03	-0.1256933E-08	-0.2644717E-07
7	0.0	0.1075318E-04	0.1689507E-05	0.1174532E-03	-0.1829817E-08	-0.1998565E-07
8	0.0	0.6560625E-05	0.8936541E-06	0.5886276E-04	-0.3497447E-08	0.2027960E-07
9	0.2493242E-06	-0.1501513E-01	-0.4372980E-06	-0.1223332E-03	0.2031992E-08	-0.4248049E-07
10	-0.3924344E-06	-0.3101057E-01	-0.8670402E-06	-0.1244605E-03	0.1296446E-08	-0.4251625E-07
11	-0.4706242E-06	-0.4615466E-01	-0.8130107E-06	-0.1255059E-03	0.1000085E-08	-0.4254303E-07
12	-0.5694205E-06	-0.6131641E-01	-0.7851610E-06	-0.1257965E-03	0.9538124E-08	-0.4255732E-07
13	0.3925575E-06	0.1601589E-01	-0.9384955E-06	-0.1223342E-03	0.2114384E-08	-0.4248021E-07
14	0.5245375E-06	0.3101193E-01	-0.8700869E-06	-0.1244629E-03	0.1403633E-08	-0.4251589E-07
15	0.2225455E-06	0.4615537E-01	-0.8182055E-06	-0.1255081E-03	0.1091790E-08	-0.4254253E-07
16	0.7287173E-06	0.6131797E-01	-0.7902759E-06	-0.1257994E-03	0.1029516E-08	-0.4255679E-07
17	0.2323745E-06	0.1692049E-01	0.1845558E-05	0.1291777E-03	-0.3025743E-08	-0.3118964E-07
18	0.9015845E-06	0.3275540E-01	0.8342522E-05	0.1314248E-03	-0.4388184E-08	-0.3421621E-07
19	0.1564153E-05	0.4874644E-01	0.1834475E-05	0.1325280E-03	-0.5011326E-08	-0.3123607E-07
20	0.2225455E-06	0.6475651E-01	0.1831905E-05	0.1328353E-03	-0.5157492E-08	-0.3124671E-07
21	-0.2918259E-06	-0.1692252E-01	0.1845561E-05	0.1291777E-03	-0.3115288E-08	-0.3118983E-07
22	-0.6321974E-06	-0.3273737E-01	0.183258E-05	0.1314249E-03	-0.4559435E-08	-0.3121635E-07
23	-0.1576124E-05	-0.4872832E-01	0.1834475E-05	0.1325280E-03	-0.522741E-08	-0.3123631E-07
24	-0.2225455E-05	-0.6473845E-01	0.1831901E-05	0.1328359E-03	-0.5386624E-08	-0.3124698E-07
25	0.5723651E-05	0.3581505E-06	-0.1601658E-01	-0.1223346E-03	0.2843477E-08	-0.4331920E-07
26	0.1102792E-04	0.3595138E-06	-0.3101242E-01	-0.1244632E-03	0.2729299E-08	-0.4403790E-07
27	0.1638445E-04	0.3605492E-06	-0.4615682E-01	-0.1255079E-03	0.2642101E-08	-0.4439195E-07
28	0.2174464E-04	0.3611067E-06	-0.6131847E-01	-0.1257989E-03	0.2596005E-08	-0.4448975E-07
29	0.5623642E-05	0.3581500E-06	0.1601448E-01	-0.1223332E-03	0.2857753E-08	-0.4330221E-07
30	0.1092293E-04	0.3595122E-06	0.3101021E-01	-0.1244644E-03	0.2757816E-08	-0.4401726E-07
31	-0.1527479E-04	0.3605379E-06	0.4615395E-01	-0.1255068E-03	0.2683000E-08	-0.4436822E-07
32	-0.2153311E-04	0.3610898E-06	0.6131596E-01	-0.1257980E-03	0.2642981E-08	-0.4446588E-07
33	0.419099E-05	0.8956266E-05	0.1691328E-01	0.1328367E-03	-0.1955475E-08	-0.3567361E-07
34	0.828315E-05	0.8963652E-05	0.3274773E-01	0.1314212E-03	-0.1750091E-08	-0.3233790E-07
35	0.1201531E-04	0.8960247E-05	0.4873811E-01	0.1325236E-03	-0.1893949E-08	-0.3259996E-07
36	0.1593379E-04	0.8972258E-05	0.6474757E-01	0.1328367E-03	-0.1955475E-08	-0.3567361E-07
37	-0.4142644E-05	0.8956260E-05	-0.1690975E-01	0.1291798E-03	-0.1554335E-08	-0.3180574E-07
38	-0.3038522E-05	0.8963438E-05	-0.3274512E-01	0.1314200E-03	-0.1715502E-08	-0.3233910E-07
39	-0.1137145E-04	0.8960236E-05	0.4874690E-01	0.1325334E-03	-0.1836088E-08	-0.3260129E-07
40	-0.1523033E-04	0.8972249E-05	-0.6474757E-01	0.1328411E-03	-0.1900521E-08	-0.3267451E-07

MODE SHAPE 7 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	0.74931025E-07	-0.7451735E-02	-0.4500407E-02	0.1344408E-08	0.7081064E-04	-0.1171411E-03
2	0.7351593E-07	-0.2513505E-03	-0.1480928E-03	0.2181366E-08	0.7064681E-04	-0.1169699E-03
3	0.5412305E-07	0.5102780E-02	0.3086525E-02	0.1313934E-09	0.2150516E-04	-0.5211523E-04
4	-0.3743113E-07	0.3956422E-02	0.2331313E-02	-0.1460117E-08	-0.4730020E-04	0.7826858E-04
5	-0.1359433E-07	-0.270077E-02	-0.1652872E-02	-0.2711064E-08	-0.8677461E-04	0.1435965E-03
6	-0.6815732E-08	-0.9769570E-02	-0.5007559E-02	-0.2525886E-08	-0.7904226E-04	0.1307920E-03
7	0.0	-0.1509509E-01	-0.9376216E-02	-0.2468548E-08	-0.6776303E-04	0.1121300E-04
8	0.0	-0.1515458E-01	-0.9150168E-02	-0.2794744E-08	0.1476429E-04	-0.2441472E-04
9	-0.5849072E-02	-0.2563491E-03	-0.1484026E-03	-0.5449169E-07	0.7723256E-04	-0.1172455E-03
10	-0.1993342E-01	-0.2700614E-03	-0.1488417E-03	-0.9882103E-07	0.9273842E-04	-0.1176421E-03
11	-0.3039332E-01	-0.2862242E-03	-0.1491745E-03	-0.1189089E-06	0.8545278E-04	-0.1179389E-03
12	-0.4051615E-01	-0.3024044E-03	-0.1493537E-03	-0.1240207E-06	0.8621207E-04	-0.1180975E-03
13	-0.9849142E-02	-0.3024044E-03	-0.1493537E-03	0.5954815E-07	0.7723016E-04	-0.1172455E-03
14	-0.1993342E-01	-0.2700614E-03	-0.1488417E-03	0.1044422E-06	0.8273363E-04	-0.1176421E-03
15	-0.3039332E-01	-0.2862242E-03	-0.1491745E-03	0.1248174E-06	0.8544636E-04	-0.1179389E-03
16	-0.4051615E-01	-0.3024044E-03	-0.1493537E-03	0.1300076E-06	0.8620482E-04	-0.1180975E-03
17	-0.9849142E-02	-0.2787161E-02	-0.1656243E-02	-0.6221970E-06	-0.1016328E-03	0.1445351E-03
18	0.2449135E-01	-0.2940227E-02	-0.1661308E-02	-0.1107015E-05	-0.1016328E-03	0.1445351E-03
19	0.374071E-01	-0.3120129E-02	-0.1665147E-02	-0.1326830E-05	-0.1049683E-03	0.1448998E-03
20	0.5025937E-01	-0.3300281E-02	-0.1667215E-02	-0.1782800E-05	-0.1059013E-03	0.1450947E-03
21	-0.1205755E-01	-0.2786438E-02	-0.1655243E-02	0.6167116E-06	-0.9486341E-04	0.1440479E-03
22	-0.2448050E-01	-0.2939842E-02	-0.1661308E-02	0.1101498E-05	-0.1016254E-03	0.1445351E-03
23	-0.3733895E-01	-0.3116080E-02	-0.1665146E-02	0.1321308E-05	-0.1049589E-03	0.1448998E-03
24	-0.5025579E-01	-0.3297578E-02	-0.1667211E-02	0.1372778E-05	-0.1058908E-03	0.1450947E-03
25	0.1629363E-01	-0.2518918E-03	-0.1510010E-03	-0.3211315E-07	0.7087395E-04	-0.1277671E-03
26	0.3297155E-01	-0.2525547E-03	-0.1592075E-03	-0.5890037E-07	0.7111381E-04	-0.1368776E-03
27	0.5029019E-01	-0.2532415E-03	-0.1688792E-03	-0.7093677E-07	0.7129331E-04	-0.1413690E-03
28	0.6763548E-01	-0.2535547E-03	-0.1785292E-03	-0.7392211E-07	0.7139925E-04	-0.1426255E-03
29	-0.1629363E-01	-0.2518918E-03	-0.1510010E-03	0.3732983E-07	0.7087394E-04	-0.1277671E-03
30	-0.3297155E-01	-0.2525547E-03	-0.1592075E-03	0.6894264E-07	0.7111380E-04	-0.1368689E-03
31	-0.5026775E-01	-0.2532415E-03	-0.1688792E-03	0.7745143E-07	0.7129330E-04	-0.1413575E-03
32	-0.6769818E-01	-0.2535548E-03	-0.1785292E-03	0.8061937E-07	0.7139924E-04	-0.1426125E-03
33	-0.7001819E-01	-0.2743294E-02	-0.1781043E-02	-0.3786623E-06	-0.8705334E-04	-0.1569747E-03
34	-0.4050975E-01	-0.2743294E-02	-0.1781043E-02	-0.6730260E-06	-0.8734767E-04	-0.1681678E-03
35	-0.6178645E-01	-0.2753017E-02	-0.1999907E-02	-0.8066260E-06	-0.8756793E-04	-0.1736860E-03
36	-0.8316314E-01	-0.2734955E-02	-0.1687237E-02	-0.8406828E-06	-0.8768566E-04	-0.1752296E-03
37	0.2001794E-01	-0.2734955E-02	-0.1687237E-02	0.3720477E-06	-0.8705335E-04	-0.1569694E-03
38	0.4050750E-01	-0.2743294E-02	-0.1779300E-02	0.6533055E-06	-0.8734770E-04	-0.1681572E-03
39	0.6178465E-01	-0.2749612E-02	-0.1887611E-02	-0.7983199E-06	-0.8756797E-04	-0.1736719E-03
40	0.8315943E-01	-0.2753013E-02	-0.1996082E-02	0.8321902E-06	-0.8768574E-04	-0.1752138E-03

A47

MODE SHAPE 8 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	0.1045950E-06	-0.4505161E-02	0.7448763E-02	-0.5571323E-08	-0.1171566E-03	-0.7080479E-04
2	0.1029421E-06	-0.1526318E-03	0.2478261E-03	-0.5207784E-08	-0.1158849E-03	-0.7064070E-04
3	0.9387144E-07	0.3083997E-02	-0.5103291E-02	-0.2176049E-08	-0.5212509E-04	-0.3150241E-04
4	0.1386671E-08	0.2334017E-02	-0.3858754E-02	0.3524926E-08	0.782614E-04	0.4730822E-04
5	-0.1191315E-08	-0.1647489E-02	0.2731669E-02	0.6274384E-08	-0.1435893E-03	-0.8678754E-04
6	-0.5325032E-09	-0.5902998E-02	0.9771988E-02	0.6210421E-08	0.1307867E-03	0.7905458E-04
7	0.0	-0.9372480E-02	0.1551155E-01	0.6210421E-08	0.1121251E-03	0.5777533E-04
8	0.0	-0.9159999E-02	0.1515563E-01	0.1838894E-08	-0.2442523E-04	-0.1475326E-04
9	0.1429541E-01	-0.1505130E-03	0.2483348E-03	-0.4070119E-07	-0.1277808E-03	-0.7086771E-04
10	0.2257442E-01	-0.1659267E-03	0.2490568E-03	-0.6853406E-07	-0.1368903E-03	-0.7110742E-04

MODE SHAPE OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
11	0.5020301E-01	-0.1769174E-03	0.2493078E-07	-0.8118241E-07	-0.1413814E-03	-0.7128691E-04
12	0.6765973E-01	-0.1873600E-03	0.2493078E-07	-0.8441054E-07	-0.1422637E-03	-0.7138270E-04
13	0.1623507E-01	-0.1551144E-03	0.2483320E-03	0.2486431E-07	-0.127766E-03	-0.7086771E-04
14	0.2292375E-01	-0.1628437E-03	0.2487406E-03	0.5511701E-07	-0.1368820E-03	-0.7110740E-04
15	0.5025254E-01	-0.1720239E-03	0.2495935E-03	0.6709154E-07	-0.1413702E-03	-0.7128681E-04
16	0.5768135E-01	-0.1812133E-03	0.249382E-03	0.7011971E-07	-0.1426251E-03	-0.7138269E-04
17	0.2031745E-01	-0.1681495E-02	0.2737551E-02	-0.3758066E-06	0.1569698E-03	0.8705642E-04
18	0.4050764E-01	-0.1772911E-02	0.2745896E-02	-0.6500848E-06	0.1681639E-03	0.8736094E-04
19	0.5174131E-01	-0.180519E-02	0.275220E-02	-0.7927265E-06	0.1752263E-03	0.8758134E-04
20	0.9316129E-01	-0.1989276E-02	0.2755624E-02	-0.8264943E-06	0.1752263E-03	0.8769915E-04
21	0.3021722E-01	-0.1683190E-02	0.2737551E-02	0.3805936E-06	0.1569698E-03	0.8706642E-04
22	0.1950520E-01	-0.1776279E-02	0.2745896E-02	0.6735233E-06	0.1681639E-03	0.8736094E-04
23	0.5174133E-01	-0.1985487E-02	0.275221E-02	0.8063323E-06	0.1736570E-03	0.8758134E-04
24	0.9315997E-01	-0.1984869E-02	0.2755625E-02	0.8401492E-06	0.1752089E-03	0.8769915E-04
25	0.9348472E-02	-0.1529607E-03	0.2524373E-03	0.5199337E-07	-0.1172602E-03	-0.7722725E-04
26	0.1932332E-01	-0.1534275E-03	0.2659108E-03	0.9684859E-07	-0.1172602E-03	-0.7722725E-04
27	0.3939731E-01	-0.1537711E-03	0.2691927E-03	0.1171803E-06	-0.1179537E-03	-0.8544156E-04
28	0.4391402E-01	-0.1539715E-03	0.272811E-03	0.1223367E-06	-0.119119E-03	-0.8620803E-04
29	0.9368131E-02	-0.1529607E-03	0.253995E-03	-0.6379179E-07	-0.1172602E-03	-0.7722454E-04
30	0.1982645E-01	-0.1534273E-03	0.2683450E-03	-0.1099075E-06	-0.1176565E-03	-0.8272955E-04
31	0.3039579E-01	-0.1537208E-03	0.2866241E-03	-0.1309413E-06	-0.118117E-03	-0.8544156E-04
32	0.4331133E-01	-0.1539712E-03	0.3043367E-03	-0.1363099E-06	-0.1179532E-03	-0.8544156E-04
33	0.1295595E-01	-0.151039E-02	0.2793598E-02	0.6275604E-06	0.1440419E-03	0.9497977E-04
34	0.2444333E-01	-0.1556073E-02	0.2943766E-02	0.6275604E-06	0.1440419E-03	0.9497977E-04
35	0.3734539E-01	-0.1556073E-02	0.2943766E-02	0.6275604E-06	0.1440419E-03	0.9497977E-04
36	0.5025509E-01	-0.1556073E-02	0.3125164E-02	0.1334470E-05	0.1448341E-03	0.1049805E-03
37	0.9368131E-02	-0.1529607E-03	0.2544873E-02	0.1396461E-05	0.1448341E-03	0.1049805E-03
38	0.2444333E-01	-0.1556073E-02	0.2793598E-02	-0.6138053E-06	0.1440419E-03	0.9487652E-04
39	0.3734539E-01	-0.1556073E-02	0.2943766E-02	-0.1099083E-05	0.1445293E-03	0.1016388E-03
40	0.5025509E-01	-0.1556073E-02	0.3119755E-02	-0.1319466E-05	0.1448941E-03	0.1049720E-03
41	0.9368131E-02	-0.1529607E-03	0.2539950E-02	-0.1375070E-05	0.1450991E-03	0.1059039E-03
1	0.3393595E-07	-0.3133177E-01	0.5905144E-02	-0.4072586E-08	0.1254051E-04	0.6656956E-04
2	0.1299419E-07	-0.3439555E-01	0.6479446E-02	-0.4784901E-09	0.1262577E-04	0.6702699E-04
3	0.3373075E-07	-0.1927375E-01	0.3442833E-02	-0.2256143E-08	0.5894097E-05	0.3130217E-04
4	0.1839943E-06	0.1806767E-01	-0.3405461E-02	0.2217850E-08	0.572294E-05	0.3038828E-04
5	0.1091353E-07	0.3425762E-01	-0.6457694E-02	0.4513012E-08	0.1228372E-04	0.6529496E-04
6	0.2193374E-07	0.3139968E-01	-0.5915351E-02	0.4313321E-08	0.1228475E-04	0.6520421E-04
7	0.2751328E-01	0.2751328E-01	-0.514807E-02	0.4155964E-08	0.1245232E-04	0.6609020E-04
8	0.3126106E-01	-0.2121038E-02	-0.2121038E-02	0.2799955E-08	0.1126576E-04	0.597249E-04
9	0.1793638E-02	-0.3533471E-01	0.649703E-02	-0.1026651E-04	0.1417601E-04	0.6729865E-04
10	0.3682133E-02	-0.3786350E-01	0.6521918E-02	-0.1832854E-04	0.1547346E-04	0.6758561E-04
11	0.3666209E-02	-0.4084609E-01	0.6560709E-02	-0.2209354E-04	0.1611399E-04	0.6780037E-04
12	0.7661914E-02	-0.483691E-01	0.6550560E-02	-0.2294518E-04	0.1629342E-04	0.6791517E-04
13	0.1785493E-02	-0.353330E-01	0.649703E-02	0.1025582E-04	0.1417466E-04	0.6729865E-04
14	0.3691644E-02	-0.3786070E-01	-0.6521918E-02	0.1831677E-04	0.1547099E-04	0.6758561E-04
15	0.5658351E-02	-0.4084190E-01	0.6540794E-02	0.1831677E-04	0.1611069E-04	0.6780037E-04
16	0.7660605E-02	-0.4383125E-01	0.6550953E-02	0.2293297E-04	0.1628982E-04	0.6791517E-04
17	0.1741173E-02	0.3521343E-01	-0.6475240E-02	0.1826395E-04	0.1505498E-04	0.6574851E-04
18	0.3512978E-02	0.3771332E-01	-0.6500129E-02	0.1826395E-04	0.1505498E-04	0.6574851E-04
19	0.512978E-02	0.407541E-01	-0.6518994E-02	0.2162607E-04	0.1527822E-04	0.6595744E-04
20	0.754635E-02	0.4364559E-01	-0.6529145E-02	0.2286436E-04	0.159577E-04	0.666691E-04
21	0.1741061E-02	0.3521235E-01	-0.6475240E-02	-0.1022172E-04	0.1378096E-04	0.6546934E-04
22	0.3582079E-02	0.3773117E-01	-0.6500129E-02	-0.1825574E-04	0.1505218E-04	0.6574851E-04
23	0.512978E-02	0.4070234E-01	-0.6518994E-02	-0.2191818E-04	0.1557464E-04	0.6595744E-04
24	0.7453315E-02	0.4369194E-01	-0.6529145E-02	-0.2285656E-04	0.1584998E-04	0.6606911E-04
25	0.1610345E-02	-0.3447896E-01	0.6657641E-02	0.1930614E-05	0.1267722E-04	0.7524407E-04

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
26	-0.1054314E-01	-0.3461147E-01	0.7139205E-02	0.3451272E-05	0.1273159E-04	0.8212125E-04
27	-0.4307222E-01	-0.3471184E-01	0.4769570E-02	0.4144415E-05	0.1272228E-04	0.8551650E-04
28	-0.4066414E-01	-0.3476593E-01	0.4859194E-02	0.4321092E-05	0.1273403E-04	0.8646748E-04
29	0.3499375E-02	-0.3447856E-01	0.6654934E-02	-0.1041144E-05	0.1267715E-04	0.7524059E-04
30	0.1954224E-01	-0.3461147E-01	0.7135572E-02	-0.2462822E-05	0.1273142E-04	0.8211442E-04
31	0.3070344E-01	-0.3471184E-01	0.7699952E-02	-0.4156663E-05	0.1277210E-04	0.8550740E-04
32	0.4050053E-01	-0.3476593E-01	0.8264918E-02	-0.4334467E-05	0.1279383E-04	0.8645731E-04
33	-0.3241227E-02	0.3436070E-01	-0.6635197E-02	-0.1921205E-05	0.1233375E-04	0.7319877E-04
34	-0.1931137E-01	0.3449275E-01	-0.7109245E-02	-0.3434845E-05	0.1239659E-04	0.7989904E-04
35	-0.3925432E-01	0.3459283E-01	-0.7658402E-02	-0.4124473E-05	0.1242614E-04	0.8319199E-04
36	-0.3035736E-01	0.3464658E-01	-0.8229088E-02	-0.4301143E-05	0.1248272E-04	0.8411713E-04
37	0.3241047E-02	0.3436070E-01	-0.6636586E-02	0.1933591E-05	0.1233377E-04	0.7319542E-04
38	0.1931106E-01	0.3449275E-01	-0.7112390E-02	0.34491134E-05	0.1239661E-04	0.7988240E-04
39	0.3925402E-01	0.3459283E-01	-0.7673521E-02	0.4140091E-05	0.1242617E-04	0.8318316E-04
40	0.3035443E-01	0.3464659E-01	-0.8236233E-02	0.4317140E-05	0.1244731E-04	0.8419172E-04

MODE SHAPE 10 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.2217547E-06	0.5905095E-02	0.3133890E-01	-0.1562164E-07	0.6651902E-04	-0.1254152E-04
2	-1.2397115E-06	0.6489209E-02	0.3438566E-01	-0.1497614E-07	0.6597532E-04	-0.1262765E-04
3	-0.1397753E-06	0.3444224E-02	0.1827053E-01	-0.8627291E-08	0.3126511E-04	-0.5899566E-05
4	-0.1931151E-06	-0.3402772E-02	-0.1807243E-01	0.5219300E-08	0.3039190E-04	-0.5734209E-05
5	-0.3439574E-07	-0.6484412E-02	-0.3427022E-01	0.1217459E-07	0.6521244E-04	-0.1229792E-04
6	-0.4445011E-07	-0.5911674E-02	-0.3139223E-01	0.1156836E-07	0.6521192E-04	-0.1229623E-04
7	0.0	-0.5180970E-02	-0.2751562E-01	0.1113097E-07	0.6609834E-04	-0.1245102E-04
8	0.0	-0.2119750E-02	-0.1126117E-01	0.3091941E-08	0.5978979E-04	-0.1125969E-04
9	-0.3493755E-02	0.6456911E-02	0.3447901E-01	0.1915455E-05	0.7520360E-04	-0.1267895E-04
10	-0.1957335E-01	0.7130630E-02	0.3461147E-01	0.3431894E-05	0.9209028E-04	-0.1273292E-04
11	-0.3076015E-01	0.7689767E-02	-0.3471835E-01	0.4120323E-05	0.8589032E-04	-0.1273739E-04
12	-0.4064942E-01	0.8259430E-02	0.3476585E-02	0.4300123E-05	0.8642680E-04	-0.1279502E-04
13	-0.2493953E-02	0.6661319E-02	0.3447901E-01	-0.1952666E-05	0.7519721E-04	-0.1267885E-04
14	0.1383162E-01	0.7149502E-02	0.3461145E-01	-0.3475232E-05	0.8207814E-04	-0.1273292E-04
15	0.3065634E-01	0.7705454E-02	0.3471822E-01	-0.4169472E-05	0.8547482E-04	-0.1277335E-04
16	0.4042225E-01	0.8272003E-02	0.3476593E-01	-0.4347401E-05	0.8642585E-04	-0.1279502E-04
17	-0.3243701E-02	-0.6630972E-02	-0.3453330E-01	-0.1915581E-05	0.7322469E-04	-0.1234778E-04
18	-0.1931951E-01	-0.7104456E-02	-0.3449537E-01	-0.3430200E-05	0.7992923E-04	-0.1240043E-04
19	-0.3925490E-01	-0.7663216E-02	-0.3458454E-01	-0.4126693E-05	0.8323944E-04	-0.1243984E-04
20	-0.3957325E-01	-0.9223510E-02	-0.3484932E-01	-0.4297633E-05	0.8416660E-04	-0.1246690E-04
21	0.3243142E-02	-0.6634075E-02	-0.3436330E-01	0.1938552E-05	0.7321752E-04	-0.1234778E-04
22	0.1931750E-01	-0.7110149E-02	-0.3449537E-01	0.3451913E-05	0.7921670E-04	-0.1240043E-04
23	0.3925493E-01	-0.7671393E-02	-0.3459545E-01	0.4147957E-05	0.8323356E-04	-0.1243984E-04
24	0.3957312E-01	-0.8236218E-02	-0.3464932E-01	0.4319550E-05	0.8414905E-04	-0.1246690E-04
25	0.1785454E-02	0.6497901E-02	0.3533306E-01	0.1025749E-04	0.6724757E-04	-0.1417595E-04
26	0.3581712E-02	0.6523875E-02	0.3785220E-01	0.1832801E-04	0.6753525E-04	-0.1547179E-04
27	0.5665421E-02	0.5541796E-02	0.4048555E-01	0.2206647E-04	0.6775049E-04	-0.1611155E-04
28	0.7660753E-02	0.6561685E-02	0.4383701E-01	0.2294865E-04	0.6785553E-04	-0.1629075E-04
29	-0.1789390E-02	0.6497901E-02	0.3533309E-01	-0.1029676E-04	0.6724753E-04	-0.1417597E-04
30	-0.3582312E-02	0.6522875E-02	0.3787955E-01	-0.1836475E-04	0.6753516E-04	-0.1547084E-04
31	-0.5665564E-02	0.6541796E-02	0.4045872E-01	-0.2204567E-04	0.6775036E-04	-0.1610997E-04
32	-0.7589931E-02	0.6551985E-02	0.4395527E-01	-0.2298890E-04	0.6786539E-04	-0.1628996E-04
33	0.1743933E-02	-0.6471951E-02	-0.3521357E-01	0.1020915E-04	0.6547262E-04	-0.1380555E-04
34	0.3585500E-02	-0.6496832E-02	-0.3773042E-01	-0.1823787E-04	0.6575693E-04	-0.1506731E-04
35	0.5517439E-02	-0.6515485E-02	-0.4069988E-01	-0.2189335E-04	0.6696630E-04	-0.1569032E-04
36	0.7460599E-02	-0.6525833E-02	-0.4367579E-01	-0.2284359E-04	0.6607908E-04	-0.1586470E-04
37	-0.1743013E-02	-0.6471951E-02	-0.3521761E-01	0.1024552E-04	0.6547722E-04	-0.1380503E-04
38	-0.3585539E-02	-0.6496832E-02	-0.3774024E-01	-0.1828546E-04	0.6575724E-04	-0.1506827E-04
39	-0.5517471E-02	-0.6515685E-02	-0.4071558E-01	-0.2195084E-04	0.6596644E-04	-0.1568824E-04
40	-0.7460345E-02	-0.6525833E-02	-0.4369929E-01	-0.2289005E-04	0.6607856E-04	-0.1586313E-04

MODE SHAPE 11 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	0.71039395E-01	0.1249720E-06	0.1855413E-05	-0.2919245E-09	0.1091760E-07	0.1275487E-07
2	0.3089774E-01	-0.5216025E-07	0.2588676E-05	-0.1805933E-09	0.1101449E-07	0.1309816E-07
3	0.2675713E-01	-0.3189475E-06	0.2077769E-05	-0.6480119E-09	0.6963337E-08	0.1002605E-07
4	0.1927726E-01	-0.5760239E-07	-0.2371166E-06	-0.1584193E-08	0.3613565E-08	0.5817174E-08
5	0.1397719E-01	0.4012317E-06	-0.1737035E-05	-0.2051796E-08	0.4755464E-08	0.4898595E-08
6	0.7761134E-02	0.5248919E-06	-0.1698155E-05	-0.1996558E-08	0.3978069E-08	0.4119197E-08
7	0.0	0.5280303E-06	-0.1706869E-05	-0.1904665E-08	0.3114229E-08	0.3458158E-08
8	0.0	0.5348049E-06	-0.2140537E-05	-0.9536307E-09	0.3492303E-08	0.1576241E-08
9	0.3477717E-01	-0.2150011E-06	0.2544309E-05	-0.2096358E-08	-0.4607557E-04	0.1325709E-07
10	0.4501673E-01	-0.7062414E-06	0.2481353E-05	-0.37556320F-08	-0.8326571E-04	0.1342775E-07
11	0.5075517E-01	-0.1323187E-05	0.2433414E-05	-0.4561025F-08	-0.1015964E-03	0.1355512E-07
12	0.7357255E-01	-0.1943997E-05	0.2407607E-05	-0.4748307E-08	-0.1064590E-03	0.1362222E-07
13	0.7473924E-01	0.9956563E-07	0.2542108E-05	-0.1631196E-08	0.4610015E-04	0.1326450E-07
14	0.4605437E-01	0.4917599E-06	0.2476043E-05	-0.3010237E-08	0.8365026E-04	0.1343989E-07
15	0.6975503E-01	0.9735677E-06	0.2425919E-05	-0.3692196E-08	0.1016180E-03	0.1357004E-07
16	0.7359173E-01	0.1488342E-05	0.2358930E-05	-0.3915314E-08	0.1064784E-03	0.1364104E-07
17	0.1554335E-01	0.1536173E-06	-0.1765226E-05	-0.1844849E-08	-0.2078255E-04	0.4962594E-08
18	0.2071293E-01	-0.4353938E-07	-0.1805227E-05	-0.1700399E-08	-0.3761400E-04	0.5031509E-08
19	0.2697912E-01	-0.2351157E-06	-0.1835643E-05	-0.1623290F-08	-0.4569958E-04	0.5082931E-08
20	0.7314210E-01	-0.4203074E-06	-0.1852017E-05	-0.1593331E-09	-0.4788692E-04	-0.5110093E-08
21	0.1564539E-01	0.6632247E-06	-0.1765214E-05	-0.1789429E-08	0.2073825E-04	0.4965766E-08
22	0.2071701E-01	0.4549921E-06	0.1805194E-05	-0.1618739E-08	0.3763007E-04	0.5036636E-08
23	0.2699513E-01	0.1024401E-05	-0.1835517E-05	-0.1522169E-08	0.4571270E-04	0.5089177E-08
24	0.7314535E-01	0.1200494E-05	0.1891943E-05	-0.1508671E-08	0.4789904E-04	0.5117908E-08
25	0.777713E-01	-0.5242604E-07	0.2475555E-05	0.3439715F-09	0.1222798E-07	-0.4507612E-08
26	0.4604725E-01	-0.5278599E-07	0.2577473E-05	0.1152463E-08	-0.1506034E-07	-0.8362795E-08
27	0.1975905E-01	-0.5282749E-07	0.2410968E-05	0.1627827E-08	0.1446346E-07	-0.1015991E-03
28	0.7357930E-01	-0.5284299E-07	0.3040783E-05	0.1749286E-08	0.1497500E-07	-0.1064618E-03
29	0.4473119E-01	-0.5357327E-07	0.1937343E-05	0.7471275E-08	0.1212900E-07	-0.4618193E-08
30	0.4603434E-01	-0.555713E-07	0.2566637E-05	0.1384384E-07	0.1330408E-07	0.8365144E-08
31	0.5075611E-01	-0.5703320E-07	-0.2184475E-05	0.1700544E-07	0.1418535E-07	0.1016193E-03
32	0.7369203E-01	-0.5780586E-07	-0.4545343E-05	0.1791151E-07	0.1465498E-07	0.1064798E-03
33	0.1564333E-01	0.4020600E-06	-0.2166174E-05	-0.2705444E-08	0.5943395E-08	-0.2072308E-04
34	0.2071334E-01	0.4032387E-06	-0.2555585E-05	-0.2843956F-08	0.7196522E-08	-0.3762047E-04
35	0.2699077E-01	0.4042358E-06	-0.2945545E-05	-0.2664089E-08	-0.0134489E-08	-0.4570471E-04
36	0.7314434E-01	0.404757E-06	-0.3242137E-05	-0.2539503E-08	0.8636285E-08	-0.4789216E-04
37	0.1564534E-01	0.4017531E-06	-0.1606940E-05	-0.1192512E-08	0.5904191E-08	0.2073604E-04
38	0.2071615E-01	0.4023438E-06	-0.1570211E-05	-0.8110950E-09	0.7717318E-08	0.3762632E-04
39	0.2699337E-01	0.4028553E-06	-0.1512391E-05	-0.7319737E-09	0.8025690E-08	0.4570953E-04
40	0.2314765E-01	0.4031509E-06	-0.1431453E-05	-0.7490086E-09	0.8510511E-08	0.4789848E-04

A-50

MODE SHAPE 12 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.7661206E-02	-0.5383974E-04	-0.5490057E-04	-0.2064315E-07	0.1916371E-07	-0.4540664E-07
2	-0.145733E-02	0.1040535E-05	0.4410876E-05	-0.5054165E-08	-0.2384638E-07	-0.1195124E-07
3	-0.6393315E-03	-0.1675627E-04	0.2391789E-05	-0.3635534E-08	-0.1614629E-07	0.3719598E-08
4	0.5116549E-02	-0.1895026E-04	-0.9035791E-06	-0.7886931E-09	0.3738865E-08	0.1094706E-07
5	0.7749577E-02	0.7751271E-06	0.8561714E-06	0.6461689E-09	0.1455388E-08	0.2595927E-07
6	0.2433331E-02	0.1152527E-05	0.2812003E-05	0.5765282E-09	0.1489499E-07	0.2307262E-07
7	0.0	-0.1033980E-05	0.4176236E-05	0.4950855E-09	0.1373916E-07	0.2281913E-07
8	0.0	-0.3792506E-05	0.4996192E-05	-0.2931902E-10	-0.8307431E-08	0.8136457E-08
9	-0.6357830E-02	-0.6805291E-06	0.4356679E-05	-0.1537919E-07	0.3771899E-04	-0.1220705E-07

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
10	-0.1554633E-01	-0.4747612E-05	0.4276732E-05	-0.3172024E-07	0.6971153E-04	-0.1247900E-07
11	-0.277533E-01	-0.9774729E-05	0.4221465E-05	-0.3903949E-07	0.9579377E-04	-0.1299197E-07
12	-0.1992635E-01	-0.4190120E-05	0.4190120E-05	-0.3985786E-07	0.9035689E-04	-0.1279030E-07
13	-0.6403313E-02	0.4687799E-05	0.4313733E-05	-0.4442267E-07	-0.3775449E-04	-0.1220434E-07
14	-0.155533E-01	0.1481536E-04	0.4175921E-05	-0.7792107E-07	-0.6973454E-04	-0.1247189E-07
15	-0.3707539E-01	0.2747749E-04	0.4071514E-05	-0.9489696E-07	-0.8580722E-04	-0.1257178E-07
16	-0.393837E-01	0.4951899E-04	0.4015319E-05	-0.9975239E-07	-0.9037724E-04	-0.1277890E-07
17	0.1422931E-01	0.7862232E-06	0.7561052E-06	-0.6218478E-09	-0.8331051E-04	0.2651305E-07
18	0.345143E-01	0.5588111E-06	0.6146179E-06	-0.1807289E-09	-0.1550510E-03	0.2710190E-07
19	0.601934E-01	0.2237703E-06	0.5071116E-06	-0.2446634E-08	-0.1908126E-03	0.2754137E-07
20	0.8657233E-01	-0.1317939E-06	0.4492438E-06	-0.2636112E-08	-0.2309950E-03	0.2777589E-07
21	0.1423503E-01	0.1535514E-05	0.7541652E-05	-0.1015939E-07	0.8394967E-04	0.2651996E-07
22	0.3459035E-01	0.4110433E-05	0.6094526E-06	-0.1962341E-07	0.1550928E-03	0.2711270E-07
23	0.5921732E-01	0.7380908E-05	0.4997429E-06	-0.2839981E-07	0.2010149E-03	0.2753554E-07
24	0.8657632E-01	0.1076397E-04	0.4406893E-06	-0.2569946E-07	0.1908483E-03	0.2779287E-07
25	-0.3400534E-02	0.1054953E-05	0.5399195E-05	0.2234616E-07	-0.2408977E-07	0.3775183E-04
26	-0.1555531E-01	0.1075405E-05	0.1115259E-04	0.4805060E-07	-0.2434495E-07	0.679281E-04
27	-0.2708143E-01	0.1099445E-05	0.1966204E-04	0.6281869E-07	-0.245347E-07	0.8585451E-04
28	-0.3495117E-01	0.1099145E-05	0.2851049E-04	0.6743582E-07	-0.2463901E-07	0.9043228E-04
29	-0.6494717E-02	0.1099440E-05	0.1877233E-05	0.3197871E-07	-0.2412446E-07	-0.3777497E-04
30	-0.1555273E-01	0.1085264E-05	-0.6594412E-05	0.6184507E-07	-0.2441780E-07	-0.6978174E-04
31	-0.2709122E-01	0.1106568E-05	-0.1697145E-04	0.7573950E-07	-0.2463768E-07	-0.8586822E-04
32	-0.3852333E-01	0.1117493E-05	-0.2737970E-04	0.7935981E-07	-0.2473494E-07	-0.9044222E-04
33	0.1422631E-01	0.7850319E-06	0.6241641E-06	-0.1900246E-09	0.1515095E-07	0.8391163E-04
34	0.3457735E-01	0.7990911E-06	0.5782570E-07	-0.3804885E-09	0.157737E-07	-0.150627E-03
35	0.5915501E-01	0.8098861E-06	-0.5842947E-06	-0.4780368E-08	0.1628737E-07	-0.1908295E-03
36	0.8657873E-01	0.8159997E-05	-0.1226587E-05	-0.5074767E-08	0.1649900E-07	-0.2010045E-03
37	0.1423729E-01	0.7854267E-06	0.6598619E-06	0.172030E-07	0.1509803E-07	0.8395784E-04
38	0.3459219E-01	0.8000363E-06	-0.4823411E-05	0.3004999E-07	0.1567199E-07	0.1950978E-03
39	0.592193E-01	0.8111583E-06	-0.9699028E-05	0.3596820E-07	0.1610226E-07	0.1909518E-03
40	0.865707E-01	0.8171495E-06	-0.1457162E-04	0.3745998E-07	0.1633155E-07	0.2010181E-03

MODE SHAPE 13 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.2201452E-06	-0.1143950E-04	0.1468499E-04	-0.6368577E-08	-0.1708844E-07	-0.9414748E-08
2	-0.5590237E-06	-0.8843955E-05	0.1201491E-04	-0.6353897E-08	-0.1602291E-07	-0.8118040E-08
3	-0.1417479E-05	-0.7236725E-05	0.1097500E-04	-0.4465480E-08	-0.8153604E-08	-0.141374E-07
4	-0.232478E-05	-0.1589020E-05	0.811394E-05	-0.6890568E-09	0.1199986E-07	-0.2989391E-07
5	-0.2713701E-05	0.2310240E-05	0.663877E-05	0.1198026E-08	0.2485426E-07	-0.2056099E-07
6	-0.1541312E-05	0.5915840E-05	0.1239557E-04	0.1168377E-08	0.2952191E-07	-0.2301388E-07
7	0.0	0.8719081E-05	-0.1690005E-04	-0.1142628E-08	-0.3035248E-07	-0.2940998E-07
8	0.0	0.138107E-04	0.2264747E-04	0.5625076E-09	-0.3626004E-07	0.1769109E-07
9	0.2103134E-02	-0.5280423E-02	0.1203598E-04	-0.7053794E-04	-0.2814894E-04	-0.8566655E-08
10	0.9905914E-02	-0.2233645E-01	-0.1198605E-04	-0.1310588E-03	-0.5226877E-04	-0.9038279E-08
11	0.1756549E-01	-0.4404077E-01	0.117319E-04	-0.1619130E-03	-0.6460107E-04	-0.9392004E-08
12	0.265210E-01	0.664624E-01	0.1106625E-04	-0.1708094E-03	-0.6815259E-04	-0.9581083E-08
13	0.2102529E-02	0.5267527E-02	0.1195951E-04	-0.7062127E-04	0.2913948E-04	-0.8388259E-08
14	0.990709E-02	0.2234148E-01	0.1187607E-04	-0.1312174E-03	0.5229790E-04	-0.8931191E-08
15	0.1755913E-01	0.4407158E-01	0.1191439E-04	-0.1621239E-03	0.6461734E-04	-0.8663271E-08
16	0.252720E-01	0.6654561E-01	-0.1171820E-04	-0.1710394E-03	0.6816917E-04	-0.8744191E-08
17	0.5108434E-02	0.1389996E-02	0.6667084E-05	0.1855382E-04	-0.5843559E-04	-0.2108143E-07
18	0.2165704E-01	0.5875256E-02	0.6688082E-05	0.3447215E-04	-0.1271828E-03	-0.2162817E-07
19	0.4272130E-01	0.158430E-01	0.6689319E-05	-0.4258919E-04	-0.1571462E-03	-0.2203842E-07
20	0.6450599E-01	0.1748827E-01	0.6692353E-05	0.4492924E-04	-0.1657896E-03	-0.2225770E-07
21	0.5115648E-02	-0.1385421E-02	0.6671919E-05	0.1857456E-04	0.6847456E-04	-0.2107097E-07
22	0.2167074E-01	-0.5876174E-02	0.6681330E-05	0.3451253E-04	0.1272063E-03	-0.2160784E-07
23	0.427343E-01	-0.1159160E-01	0.6691942E-05	0.42644167E-04	0.1571553E-03	-0.2201023E-07
24	0.6452209E-01	-0.1750265E-01	0.6696579E-05	0.4498666E-04	0.1657966E-03	-0.2222531E-07

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
25	-0.3121415E-02	-0.8984722E-05	0.5281605E-C2	0.7052129F-04	-0.1681579E-07	0.2912326E-04
26	-0.4937203E-02	-0.9181309E-05	0.2233471E-01	0.1310361F-03	-0.1765094E-07	0.5226268E-04
27	-0.1753754E-01	0.4403671E-C1	0.4403671E-C1	0.1618940F-03	-0.1527674E-07	0.6457469E-04
28	-0.2459235E-01	-0.9415515E-05	0.6647980E-01	0.1709020F-03	-0.1861124E-07	0.6812620E-04
29	-0.2103744E-C2	-0.8083541E-C5	-0.5263947E-02	0.7069104F-04	-0.1652415F-07	-0.2813134E-04
30	-0.8965033E-C2	-0.9186354E-C5	-0.2233949E-01	0.1312267E-03	-0.1705626E-07	-0.5226138E-04
31	-0.1755774E-01	-0.9734489E-05	-0.4407162E-01	0.1621374E-03	-0.1745341E-07	-0.6456587E-04
32	-0.2651042E-C1	-0.9420370E-05	-0.6654769E-01	0.1710339F-03	-0.1766571E-07	-0.6811331E-04
33	-0.5117335E-C2	0.2343532E-C5	-0.1383642E-02	-0.1860959E-04	0.2545753E-07	0.6847728E-04
34	-0.2147659E-01	0.2395601F-05	0.5889191E-02	-0.3457408F-04	0.2609738E-07	0.1272558E-03
35	-0.4375159E-01	0.2437503F-05	-0.1160940E-01	-0.4271490F-04	0.2655717E-07	0.1572348E-03
36	-0.6454343E-01	0.2453903E-C5	-0.1753091E-C1	-0.4506476E-04	0.2683058E-07	0.1658826E-03
37	-0.6123742E-02	0.2347651E-C5	0.1389190E-02	-0.1951085E-04	0.2518907E-07	-0.6850877E-04
38	-0.2169597E-01	0.2400729E-C5	0.5866974E-C2	-0.3439581E-04	0.2554427E-07	-0.1572728E-03
39	-0.4275436E-01	0.2440912E-05	0.1156140E-01	-0.4249983E-04	0.2580947E-07	-0.1572378E-03
40	-0.6456140E-C1	0.2462541E-C5	0.1745295E-C1	-0.4443738E-04	0.2595125E-07	-0.1658768E-03
1	-0.3896313E-06	0.2812531E-C5	0.5068652E-05	0.1701349F-09	-0.2302211E-07	0.2538276E-07
2	-0.3665173E-06	0.6967685E-C6	0.1766818E-05	0.1785451E-09	-0.2713953E-07	0.2498281E-07
3	-0.8200704E-07	-0.2643585E-C5	0.5949111E-C5	0.6223355E-C9	0.0717633F-08	0.1672652E-07
4	0.6526507E-06	-0.4902782E-05	0.1177738F-04	0.1536310E-09	0.8447024F-08	-0.4106109E-08
5	0.1098713E-05	-0.4907601E-05	0.1307601E-04	0.1987578E-08	0.1258894E-C7	0.1610840F-07
6	0.5771031E-06	-0.5650522E-C5	0.2236156F-04	0.1937053E-08	0.2286294E-07	-0.1340813E-07
7	0.0	-0.5845976E-05	0.2904195E-04	0.1848999E-08	0.2648141E-07	-0.1145022E-07
8	0.0	-0.5514352E-C3	0.3553837E-04	0.9455652E-09	-0.6521719E-07	-0.1403260E-07
9	-0.6097976E-C2	0.2845786E-05	0.2045786E-05	0.7365791E-05	0.8163152F-04	0.2593383E-07
10	-0.3583748E-01	0.2334348E-02	-0.2394996E-05	0.1369339E-04	0.1516990E-03	0.2699342E-07
11	-0.3096059E-01	0.4601359E-02	0.2666701E-05	0.1691769E-04	0.1874361E-03	0.2768441E-07
12	-0.7694399E-01	0.6946571E-C2	0.2810791E-05	0.1784707E-04	0.1977450E-03	0.2808537E-07
13	-0.6105947E-02	-0.5502086E-03	0.2026843E-05	0.7374179F-05	0.2545732E-07	0.2545732E-07
14	-0.2555313E-01	-0.2733143E-C2	0.2353175E-05	0.1370229E-C4	-0.151712E-C3	0.2595766E-07
15	-0.7099294E-01	-0.4602395E-C2	0.2600482F-05	0.182973F-04	0.263234F-07	0.263234F-07
16	-0.7597952E-01	-0.6949179E-02	0.273352E-05	0.1746066E-04	-0.1977671E-03	-0.2653263E-07
17	0.3843279E-C2	-0.2838634E-C2	0.1328789E-04	-0.3791884E-04	-0.5143718E-04	-0.1650621E-07
18	0.1623127E-C1	-0.1200783E-01	0.1358566E-04	-0.7045518E-04	-0.9558641E-C4	-0.1692356E-07
19	0.3211145E-01	-0.2367638E-C1	0.1381125E-04	-0.8704612E-04	-0.1181040E-03	-0.1723692E-07
20	0.4943365E-01	-0.3574338E-C1	0.1393268E-04	-0.9182922E-04	-0.1245995E-C3	-0.1740442E-07
21	0.7846702E-C2	0.2831679E-C2	0.1328517E-04	-0.3797063F-04	0.5145039E-04	-0.1650566E-07
22	0.1622611E-01	0.1201241E-01	0.1357908E-04	-0.7055585E-04	-0.958522E-04	-0.1692651E-07
23	0.3211594E-01	0.2369697E-01	0.1380180E-04	-0.8717598E-04	0.1180905E-03	-0.1724053E-07
24	0.4945534E-C1	0.3578168E-C1	0.1392168E-04	-0.9197035E-04	0.1245788E-03	-0.1740856E-07
25	0.5056445E-C2	0.7045618E-C6	-0.5507867E-C3	-0.7397899E-05	-0.2276371E-07	-0.8162641E-04
26	0.2593534E-01	0.7161856E-06	-0.2339712E-02	-0.1374595E-04	-0.2388891E-07	-0.1516924E-C3
27	0.5095727E-01	0.7250487E-06	-0.4516369F-02	-0.1694233F-04	0.2465965E-07	-0.1874287E-03
28	0.7693976E-C1	0.7294198E-06	-0.6670458E-02	-0.179194E-04	-0.2509304E-07	-0.1977373E-03
29	0.5103451E-02	0.7104350E-06	0.5510272E-03	-0.7345282E-04	-0.2279682E-07	0.8166439E-C4
30	0.2586459E-01	0.7303878E-C6	0.2327233E-02	-0.1364921E-04	-0.2391391E-07	0.1517129E-03
31	0.5097243E-01	0.7455325E-06	0.458757E-02	-0.1686339F-04	-0.2474969E-07	-0.1974321E-03
32	0.7595332E-01	0.7536827E-06	0.6252194E-C2	-0.1779060F-04	-0.2512645E-07	0.1977302E-03
33	-0.3933712E-C2	-0.4985220E-05	0.2845391E-02	0.3788978E-04	0.1254955E-07	0.5140741E-04
34	-0.1626699E-01	-0.5095339E-05	0.1200730E-01	0.7039521E-04	0.1271629E-07	-0.9553446E-04
35	-0.3203156E-01	-0.517982E-05	0.2366550E-01	0.8696844E-04	0.1276522E-07	0.1180411E-03
36	-0.1946327E-01	-0.5223768E-05	0.3572142E-01	0.9174606E-04	0.1279138E-07	0.1245334E-03
37	-0.3944279E-02	-0.4985432E-C5	-0.2925644E-C2	0.3800188F-04	0.1265266E-07	-0.5143999E-04
38	-0.1629231E-01	-0.5095951E-05	-0.1201335E-01	0.7061224F-04	0.1266255E-07	-0.9556298E-04
39	-0.3310459E-01	-0.5179514E-C5	-0.2370720E-01	0.8724592E-04	0.1269087E-07	-0.1180624E-03

MODE SHAPE 14 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MODE SHAPE 15 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO. X(1) X(2) X(3) THETA(1) THETA(2) THETA(3)

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.6009074E-06	0.4521144E-06	-0.1552537E-04	0.1378902E-08	-0.2774491E-07	0.1578081E-07
2	-0.5320019E-06	-0.5065333E-06	-0.1157236E-04	0.1351792E-08	-0.3142758E-07	0.1573416E-07
3	-0.2747153E-06	0.3443146E-05	-0.2157863E-04	-0.1809672E-10	-0.3280833E-07	0.5834386E-08
4	0.3455839E-06	0.9853305E-05	-0.2876594E-04	-0.2749094E-08	-0.2090916E-07	-0.4165055E-09
5	0.6381705E-06	0.1191347E-04	-0.2583012E-04	-0.4113343E-08	-0.1521515E-07	0.1666424E-08
6	0.3669324E-06	0.1939181E-04	-0.4370503E-04	-0.4010388E-08	-0.3623446E-07	-0.8025026E-08
7	0.0	0.2450419E-04	-0.5656446E-04	-0.3820077E-08	-0.4437821E-07	-0.1226737E-07
8	0.0	0.2929503E-04	-0.6883870E-04	-0.1963158E-08	0.1282322E-06	0.5593041E-07
9	-0.3553550E-02	-0.1507302E-03	-0.1215681E-04	-0.2021151E-05	0.4764675E-07	0.1603705E-07
10	-0.1508243E-01	-0.6372795E-03	-0.1301500E-04	-0.3738582E-05	0.885517E-04	0.1635481E-07
11	-0.2574732E-01	-0.1256461E-02	-0.1365619E-04	-0.4619635E-05	0.1094255E-03	0.1659340E-07
12	-0.4449161E-01	0.1896575E-02	-0.1400129E-04	-0.4873858E-05	0.1154446E-03	0.1672093E-07
13	-0.3565114E-02	0.1490767E-03	-0.1221932E-04	-0.2002234E-05	-0.4767468E-04	0.1600911E-07
14	-0.1503317E-01	0.6333527E-03	-0.1313717E-04	-0.3720755E-05	-0.8555373E-04	0.1629878E-07
15	-0.2975452E-01	0.1249589E-02	-0.1383267E-04	-0.4597410E-05	-0.1093990E-03	0.1651581E-07
16	-0.4451431E-01	0.1885893E-02	-0.1420701E-04	-0.4890185E-05	-0.1154089E-03	0.1663182E-07
17	-0.3554409E-03	0.6887589E-02	-0.2643891E-04	0.9200456E-04	0.7440141E-05	0.1669791E-08
18	-0.2451135E-02	0.2913521E-01	-0.2730261E-04	0.1709489E-03	0.1383695E-04	0.1671908E-08
19	-0.4647295E-02	0.5747111E-01	-0.2795704E-04	0.2112037E-03	0.1709929E-04	0.1674018E-08
20	-0.7717575E-02	0.8672577E-01	-0.2830989E-04	0.2228092E-03	0.1804023E-04	0.1675144E-08
21	-0.5551344E-03	-0.6870458E-02	-0.2643571E-04	0.9212698E-04	-0.7426633E-05	0.1666453E-08
22	-0.3719090E-02	-0.2014528E-01	-0.2729484E-04	0.1711809E-03	-0.1378628E-04	0.1670483E-08
23	-0.4331533E-02	-0.5749504E-01	-0.2794592E-04	0.2115110E-03	-0.1702964E-04	0.1671991E-08
24	-0.5902135E-02	-0.8681554E-01	-0.2825636E-04	0.2314325E-03	-0.1796486E-04	0.1672815E-08
25	0.3557415E-02	-0.5118608E-06	0.1439089E-03	0.2092461E-05	-0.3153135E-07	-0.4763617E-04
26	0.1507575E-01	-0.5193907E-06	0.6493155E-03	0.3891091E-05	-0.3164302E-07	-0.8852682E-04
27	0.2973739E-01	-0.5250666E-05	0.1293949E-02	0.4811092E-05	-0.3172580E-07	-0.1093827E-03
28	0.4490130E-01	-0.5281212E-06	0.19661279E-02	0.5077007E-07	-0.3177007E-07	-0.1153988E-03
29	0.3562429E-02	-0.5064074E-05	-0.1567580E-03	0.1922269E-05	-0.3157519E-07	0.4765577E-04
30	0.1586235E-01	-0.5062022E-06	-0.6218469E-03	0.3563780E-05	-0.3173174E-07	0.8855049E-04
31	0.2975037E-01	-0.5060276E-06	-0.5211534E-02	0.4395479E-05	-0.3184867E-07	0.1093985E-03
32	0.4491630E-01	-0.5059341E-06	-0.1820309E-02	0.4635281E-05	-0.3191115E-07	0.1154091E-03
33	0.5571737E-03	0.1210304E-04	-0.6899437E-02	-0.9194564E-04	-0.1481333E-07	-0.7450411E-05
34	0.2359701E-02	0.1237109E-04	-0.52913104E-01	-0.1708289E-03	-0.1439048E-07	-0.138474E-04
35	0.4651535E-02	0.1257582E-04	-0.5742244E-01	-0.2110503E-03	-0.1407349E-07	-0.1710611E-04
36	0.7022455E-02	0.1268553E-04	-0.8667945E-01	-0.2226455E-03	-0.1390406E-07	-0.1804699E-04
37	0.5590527E-03	0.1210330E-04	-0.6860230E-02	-0.9219437E-04	-0.1492453E-07	0.7457433E-05
38	0.2361036E-02	0.1237262E-04	0.2914761E-01	-0.1712910E-03	-0.1461366E-07	0.1305459E-04
39	0.4655544E-02	0.1257664E-04	0.5751453E-01	-0.2116419E-03	-0.1438251E-07	0.1711660E-04
40	0.7728349E-02	0.1268645E-04	0.8685344E-01	-0.2328275E-03	-0.1425894E-07	0.1805702E-04

MODE SHAPE 16 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.1436299E-05	-0.1155585E-04	0.3066961E-05	0.8093743E-08	0.2211262E-08	0.8716384E-08
2	-0.1460563E-05	-0.1001548E-04	0.8113047E-07	0.8115904E-08	0.4908993E-08	0.1008390E-07
3	-0.1844732E-05	-0.9795038E-05	-0.5602299E-05	0.6904671E-09	-0.1645422E-07	0.823115E-08
4	-0.2597482E-05	-0.9590757E-05	0.2083083E-04	0.4472312E-08	0.1758247E-07	0.1144501E-07
5	-0.2903342E-05	-0.2967698E-05	0.2195773E-04	0.3296730E-08	0.1645533E-07	0.1834935E-07
6	-0.1647634E-05	-0.6296322E-05	0.3489241E-04	0.3159321E-08	0.2598320E-07	0.2096680E-07
7	0.0	-0.8833134E-05	0.4369949E-04	0.3022073E-08	0.2925778E-07	0.1935580E-07
8	0.0	-0.109040E-04	0.4830514E-04	0.1534258E-08	-0.0902845E-07	-0.1922453E-07

C

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	0.1738550E-08	-0.5650899E-04	0.3085395E-02	-0.2339997E-07	-0.2384480E-06	-0.1776055E-07
2	0.7222643E-08	-0.2759580E-04	0.2389543E-02	-0.3325115E-07	0.2328663E-06	0.7476657E-09
3	-0.2885443E-06	-0.9455638E-04	0.7841963E-02	-0.2805222E-07	0.683989E-05	0.5798663E-07
4	-0.7375355E-06	-0.1368590E-03	0.1366290E-01	-0.2475457E-07	0.7961851E-05	0.5225244E-07
5	-0.1120377E-05	-0.1174797E-03	0.1479966E-01	-0.2300217E-07	0.5410167E-05	0.4343120E-07
6	-0.6066334E-05	-0.4253748E-03	0.45215020E-01	-0.1864125E-07	-0.7414938E-04	0.6098491E-06
7	0.0	-0.6971955E-03	0.9517575E-01	-0.1501864E-07	0.1262643E-03	0.1035283E-05
8	0.0	-0.1370953E-02	0.1676245E 00	0.1611391F-07	-0.1887889E-03	-0.1545232E-05
9	0.7597505E-04	-0.1087130E-04	0.2430713E-02	0.2649351E-06	-0.1217782E-05	0.8881842E-09
10	0.3994235E-03	0.5690726E-04	0.2501071E-02	0.5357235E-06	-0.2466151E-05	0.1036601E-08
11	0.9195931E-03	0.1458510E-03	0.2550597E-02	0.6617007E-06	-0.3105699E-05	0.1147654E-08
12	0.1253598E-02	0.2365113E-03	0.2577255E-02	0.7917660E-06	-0.3291039E-05	0.1204215E-08
13	-0.7397641E-04	-0.1804449E-04	0.2435568E-02	-0.1145272E-06	-0.1202207E-05	0.8490697E-09
14	-0.3000345E-03	0.5355494E-04	0.2500554E-02	-0.1880082E-06	-0.2436269E-05	0.9561096E-09
15	-0.3000345E-03	0.7523680E-04	0.2550429E-02	-0.2277093E-06	-0.3067636E-05	0.1058230E-08
16	-0.1230011E-02	0.6485254E-04	0.2577057E-02	-0.2397708E-06	-0.3250256E-05	0.1079057E-08
17	0.5051325E-03	-0.5478695E-04	0.1509409E-01	0.9185125E-06	-0.1123406E-04	0.4483547E-07
18	0.3972917E-02	0.1689353E-03	0.4155143E-01	-0.1745688E-05	-0.2561987E-04	0.4631885E-07
19	0.8376439E-02	0.4603716E-03	0.1582839E-01	0.2179150E-05	-0.3302540E-04	0.4742872E-07
20	-0.1305872E-01	0.7644929E-03	0.1599876E-01	0.2307307E-05	-0.3517926E-04	0.4802205E-07
21	-0.5109570E-03	-0.6187351E-04	0.1150980E-01	-0.7867131E-05	-0.1136710E-04	0.4484249E-07
22	-0.3893375E-02	0.1243053E-03	0.1551183E-01	-0.1460616E-05	-0.2568048E-04	0.4629628E-07
23	-0.8393733E-02	0.3664584E-03	0.1582839E-01	-0.1915508E-05	-0.3309904E-04	0.4739755E-07

MODE SHAPE 17 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.

X(1)

X(2)

X(3)

THETA(1)

THETA(2)

THETA(3)

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	0.1738550E-08	-0.5650899E-04	0.3085395E-02	-0.2339997E-07	-0.2384480E-06	-0.1776055E-07
2	0.7222643E-08	-0.2759580E-04	0.2389543E-02	-0.3325115E-07	0.2328663E-06	0.7476657E-09
3	-0.2885443E-06	-0.9455638E-04	0.7841963E-02	-0.2805222E-07	0.683989E-05	0.5798663E-07
4	-0.7375355E-06	-0.1368590E-03	0.1366290E-01	-0.2475457E-07	0.7961851E-05	0.5225244E-07
5	-0.1120377E-05	-0.1174797E-03	0.1479966E-01	-0.2300217E-07	0.5410167E-05	0.4343120E-07
6	-0.6066334E-05	-0.4253748E-03	0.45215020E-01	-0.1864125E-07	-0.7414938E-04	0.6098491E-06
7	0.0	-0.6971955E-03	0.9517575E-01	-0.1501864E-07	0.1262643E-03	0.1035283E-05
8	0.0	-0.1370953E-02	0.1676245E 00	0.1611391F-07	-0.1887889E-03	-0.1545232E-05
9	0.7597505E-04	-0.1087130E-04	0.2430713E-02	0.2649351E-06	-0.1217782E-05	0.8881842E-09
10	0.3994235E-03	0.5690726E-04	0.2501071E-02	0.5357235E-06	-0.2466151E-05	0.1036601E-08
11	0.9195931E-03	0.1458510E-03	0.2550597E-02	0.6617007E-06	-0.3105699E-05	0.1147654E-08
12	0.1253598E-02	0.2365113E-03	0.2577255E-02	0.7917660E-06	-0.3291039E-05	0.1204215E-08
13	-0.7397641E-04	-0.1804449E-04	0.2435568E-02	-0.1145272E-06	-0.1202207E-05	0.8490697E-09
14	-0.3000345E-03	0.5355494E-04	0.2500554E-02	-0.1880082E-06	-0.2436269E-05	0.9561096E-09
15	-0.3000345E-03	0.7523680E-04	0.2550429E-02	-0.2277093E-06	-0.3067636E-05	0.1058230E-08
16	-0.1230011E-02	0.6485254E-04	0.2577057E-02	-0.2397708E-06	-0.3250256E-05	0.1079057E-08
17	0.5051325E-03	-0.5478695E-04	0.1509409E-01	0.9185125E-06	-0.1123406E-04	0.4483547E-07
18	0.3972917E-02	0.1689353E-03	0.4155143E-01	-0.1745688E-05	-0.2561987E-04	0.4631885E-07
19	0.8376439E-02	0.4603716E-03	0.1582839E-01	0.2179150E-05	-0.3302540E-04	0.4742872E-07
20	-0.1305872E-01	0.7644929E-03	0.1599876E-01	0.2307307E-05	-0.3517926E-04	0.4802205E-07
21	-0.5109570E-03	-0.6187351E-04	0.1150980E-01	-0.7867131E-05	-0.1136710E-04	0.4484249E-07
22	-0.3893375E-02	0.1243053E-03	0.1551183E-01	-0.1460616E-05	-0.2568048E-04	0.4629628E-07
23	-0.8393733E-02	0.3664584E-03	0.1582839E-01	-0.1915508E-05	-0.3309904E-04	0.4739755E-07

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
24	-0.1305271E-01	0.6192247E-03	0.1596976E-01	-0.1920939E-05	-0.3525537E-04	0.4799635E-07
25	-0.1212005E-05	-0.2811590E-04	0.1247302E-02	-0.1547837E-04	-0.2364427E-06	-0.1595052E-07
26	0.5480934E-06	-0.2883377E-04	-0.272734E-02	-0.3069953E-04	0.2402191E-06	-0.3219471E-07
27	0.1748923E-04	-0.2941290E-04	-0.7461976E-02	-0.3859168E-04	0.2430452E-06	-0.4010931E-07
28	0.1634314E-04	-0.2971385E-04	-0.1324339E-01	-0.405388E-04	0.245550E-06	-0.4244524E-07
29	-0.1231935E-05	-0.2810996E-04	0.1261053E-02	0.1634093E-04	0.2380451E-06	-0.1727595E-07
30	-0.4431969E-05	-0.2893641E-04	-0.2659117E-02	0.3076739E-04	0.2435150E-06	-0.4086582E-07
31	-0.1095734E-04	-0.2939219E-04	-0.7791854E-02	0.4069585E-04	0.2497943E-06	-0.4321791E-07
32	-0.1665117E-04	-0.2968972E-04	-0.131444E-01	-0.105834E-03	0.5570104E-05	-0.1054583E-06
33	0.4134344E-05	-0.1194197E-03	0.7515917E-02	-0.1975004E-03	0.5739979E-05	-0.3302529E-06
34	0.7475543E-04	-0.1231355E-03	-0.1773476E-01	-0.1975004E-03	0.5739979E-05	-0.3302529E-06
35	0.7534655E-04	-0.1256552E-03	-0.5082820E-01	-0.2461986E-03	0.5932941E-05	-0.3196020E-06
36	0.1191211E-03	-0.1273092E-03	-0.9495265E-01	-0.2605964E-03	0.5570833E-05	-0.8962821E-07
37	-0.498234E-05	-0.1198197E-03	0.7545665E-02	0.1047741E-03	0.574084E-05	-0.202724E-06
38	-0.3164459E-04	-0.1231372E-03	-0.1763315E-01	0.1970795E-03	0.574084E-05	-0.202724E-06
39	-0.6727405E-04	-0.1256521E-03	-0.5043993E-01	0.2455851E-03	0.5867451E-05	-0.2613641E-06
40	-0.1041735E-03	-0.1275057E-03	-0.8467865E-01	0.2599668E-03	0.5935319E-05	-0.2783557E-06

MODE SHAPE 13 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	0.5941054E-06	0.2760179E-02	0.6427556E-04	-0.1940317E-07	-0.3440890E-07	-0.1353298E-06
2	0.6111135E-06	0.2154958E-02	0.2145370E-04	-0.1303960E-08	-0.7782205E-08	-0.5664797E-06
3	-0.2583493E-06	0.7614702E-02	0.3410372E-04	0.5637744E-09	0.3949666E-07	-0.7182012E-05
4	0.9313793E-06	0.1343042E-01	0.8086822E-04	-0.114553E-07	0.6978286E-07	-0.8327470E-05
5	0.1153317E-06	0.1468462E-01	0.1186725E-03	-0.1745475E-07	0.4250493E-06	-0.3759834E-05
6	0.1792355E-07	0.5218606E-01	0.4252174E-03	-0.1421888E-07	0.6143301E-06	-0.7480721E-04
7	0.0	0.8536458E-01	0.6978139E-03	-0.1067761E-07	0.1047098E-05	-0.1271695E-03
8	0.0	0.1683443E 00	0.1390263E-02	0.1745320E-07	-0.1536134E-05	0.1887788E-03
9	0.1774130E-05	0.192119E-02	0.2198944E-04	-0.1533958E-04	-0.9138099E-08	-0.5837144E-06
10	0.2245101E-05	-0.2594127E-02	0.2274950E-04	-0.2884748E-04	-0.1032472E-07	-0.6019132E-06
11	0.4363009E-05	-0.7395337E-02	0.232345E-04	-0.3594412E-04	-0.1175932E-07	-0.6155327E-06
12	0.5218451E-05	-0.1240775E-01	0.2363545E-04	-0.3904693E-04	-0.1228359E-07	-0.8228130E-06
13	-0.5391305E-06	0.1093816E-02	0.2190649E-04	0.1532483E-04	-0.1468264E-07	-0.5935044E-06
14	-0.3401923E-05	-0.2588667E-02	0.2253483E-04	0.2882243E-04	-0.2123306E-07	-0.6014814E-06
15	-0.6624929E-05	-0.7386822E-02	0.2301540E-04	-0.3591944E-04	-0.2547157E-07	-0.6149352E-06
16	-0.1015233E-04	-0.1238450E-01	0.2327406E-04	0.3802220E-04	-0.2696590E-07	-0.6221267E-06
17	0.4520722E-05	0.7441483E-02	0.1213679E-03	-0.1045363E-03	-0.9437673E-07	-0.5933353E-05
18	0.3240233E-04	-0.1767844E-01	0.1251919E-03	-0.1969945E-03	-0.2125648E-06	-0.6116584E-05
19	0.6963573E-04	-0.5040347E-01	0.1280817E-03	-0.2449441E-03	-0.2740814E-06	-0.6253711E-05
20	0.1025003E-03	-0.8455431E-01	0.1296493E-03	-0.2592739E-03	-0.2921626E-06	-0.6327008E-05
21	-0.4391894E-05	-0.7454470E-02	0.1213736E-03	0.1844241E-03	-0.9477452E-07	-0.5933347E-05
22	-0.3230305E-04	-0.1763916E-01	0.1252055E-03	0.1964193E-03	-0.2138361E-06	-0.6116569E-05
23	-0.6975339E-04	-0.5033370E-01	0.1281095E-03	-0.2447632E-03	-0.2758796E-06	-0.6253691E-05
24	-0.1049531E-03	-0.8445026E-01	0.1296725E-03	-0.2590985E-03	-0.2941750E-06	-0.6326984E-05
25	-0.4658327E-04	0.2197950E-02	0.225942E-02	-0.1423830E-06	-0.7244502E-08	0.1099595E-05
26	-0.3966555E-03	0.225942E-02	-0.212732E-04	-0.2711420E-06	-0.6676672E-08	0.2540311E-05
27	-0.9296315E-03	0.2305140E-02	-0.6653409E-04	-0.3431422E-06	-0.6251749E-08	0.3582348E-05
28	-0.1294527E-02	0.2330637E-02	-0.1150449E-03	-0.3661133E-06	-0.6024599E-08	0.3498249E-05
29	0.473747E-04	0.2197951E-02	0.1187812E-04	0.1446584E-06	-0.7192465E-08	0.1091076E-05
30	0.8249492E-03	0.2258946E-02	-0.8292251E-04	-0.2571974E-06	-0.6569774E-08	0.2524111E-05
31	0.4249492E-03	0.2305166E-02	-0.6867839E-04	0.3459710E-06	-0.6103743E-08	0.3261935E-05
32	0.1287309E-02	0.2330044E-02	-0.1173072E-03	-0.3679763E-06	-0.5894631E-08	0.3476476E-05
33	-0.480677E-03	0.1497465E-01	-0.6124651E-04	-0.127544E-06	-0.4496975E-07	0.117471E-04
34	-0.3375093E-02	0.1539339E-01	-0.1321689E-03	-0.1512143E-05	0.8570417E-07	0.2581794E-04
35	-0.8422140E-02	0.1570841E-01	-0.3829461E-03	-0.1878479E-05	0.4659337E-07	0.335971E-04
36	-0.1316399E-01	0.1587798E-01	-0.5443584E-03	-0.1986822E-05	0.4759113E-07	0.3555398E-04
37	0.4322725E-03	0.1497765E-01	0.5483895E-04	0.8931087E-06	0.4408261E-07	0.1118788E-04
38	0.3890210E-02	0.1539339E-01	-0.1560933E-03	0.1674752E-05	0.4574819E-07	0.2584080E-04

30 0.2431930E-02
40 0.1317701E-01

0.4697943E-07
0.4766123E-07

0.2099952E-05
0.2212901E-05

-0.4354601E-03
-0.7270490E-03

0.1572801E-01
0.1587708E-01

0.2431930E-02
0.1317701E-01

MODE SHAPE 19 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	0.5270433E-05	-0.4146433E-03	-0.4463866E-01	0.7543190E-07	0.1031159E-04	-0.1084784E-06
2	0.5212345E-05	-0.2403325E-03	-0.3147731E-01	0.1073075E-07	0.3202575E-05	-0.1992852E-07
3	0.5355030E-05	-0.2005030E-03	-0.3405030E-01	0.4576620E-07	0.1293398E-04	-0.0946376E-07
4	0.6751300E-05	-0.1725163E-03	-0.4203370E-01	0.4137092E-08	0.1835216E-04	-0.1451724E-06
5	0.6562300E-05	-0.5244830E-04	-0.6611985E-02	0.5308583E-08	0.6070219E-05	-0.3870353E-07
6	0.3914330E-05	0.7363927E-02	0.4740674E-02	-0.4425252E-08	0.3324419E-04	-0.2477465E-06
7	0.0	0.1309287E-03	0.1689032E-01	-0.9191658E-08	0.5833319E-04	-0.4455031E-06
8	0.0	0.4674444E-03	0.6089112E-01	-0.6265162E-07	-0.3245220E-04	0.2487397E-06
9	-0.0	0.1979040E-03	-0.3556138E-01	0.1263449E-05	-0.1711559E-07	-0.2061191E-07
10	0.7197545E-03	0.120315F-03	0.3667987E-01	0.2390503E-05	-0.5977472E-05	-0.2133303E-07
11	0.1875320E-02	0.5020633E-03	-0.3752699E-01	0.2996639E-05	-0.0183664E-05	-0.2187293E-07
12	0.3072977E-02	0.9215910E-03	-0.3798304E-01	0.3179942E-05	-0.0832902E-05	-0.2216144E-07
13	0.7392047E-04	-0.1930447E-03	-0.4555123E-01	-0.1345516E-05	-0.1695171E-05	-0.2050221E-07
14	-0.7157654E-03	0.1307812E-03	-0.3667924E-01	-0.2561989E-05	-0.5931633E-05	-0.2110773E-07
15	-0.1451921E-02	0.5585745E-03	-0.3752664E-01	-0.3214273E-05	-0.0133235E-05	-0.2156098E-07
16	-0.3044297E-02	0.1009663E-02	-0.3798249E-01	-0.3411156E-05	-0.0777353E-05	-0.2180321E-07
17	-0.3117657E-04	-0.4181845E-04	-0.4676626E-02	0.1789427E-06	-0.0447316E-07	-0.4013116E-07
18	0.1780519E-02	0.1582821E-06	-0.4697398E-02	0.3372782E-06	-0.1563449E-04	-0.4163922E-07
19	0.4324145E-02	0.5645444E-04	-0.7131387E-02	0.4236423E-06	-0.1839194E-04	-0.4274631E-07
20	0.5653030E-02	0.1153426E-03	-0.7216107E-02	0.4500593E-06	-0.1977103E-04	-0.4336925E-07
21	0.4787313E-04	-0.3469549E-04	-0.6766257E-02	-0.2944364E-06	-0.0427457E-05	-0.4012942E-07
22	-0.1782995E-02	0.3657605E-04	-0.6577989E-02	-0.5423528E-06	-0.1354935E-04	-0.4163516E-07
23	-0.4232311E-02	0.1247256E-03	-0.7131390E-02	-0.6801647E-06	-0.1927440E-04	-0.4275202E-07
24	-0.6935813E-02	0.2190566E-03	-0.7216111E-02	-0.7216547E-06	-0.1975664E-04	-0.4336433E-07
25	0.3454759E-05	-0.2867884E-03	-0.24249594E-01	0.1607475E-03	0.3279350E-05	0.4272449E-07
26	-0.9123170E-05	-0.2059478E-03	0.1414955E-01	0.3050664E-03	0.3358367E-05	0.9726705E-07
27	-0.2622193E-04	-0.7029892E-03	0.5512797E-01	0.3925205E-03	0.3419253E-05	0.1261238E-06
28	-0.4421323E-04	-0.7066238E-03	0.1186843E 00	0.4059051E-03	0.3450250E-05	0.1347423E-06
29	0.3375294E-05	-0.2867791E-03	-0.2430567E-01	-0.1506506E-03	0.3276020E-05	-0.2630105E-08
30	0.5793910E-05	-0.2959250E-03	-0.4141337E-01	-0.3049128E-03	0.3353721E-05	0.1174696E-07
31	0.9647452E-05	-0.3028547E-03	0.6506109E-01	-0.3923494E-03	0.3411815E-05	0.180505E-07
32	0.1155937E-04	-0.3065466E-03	0.1185905E 00	-0.4057428E-03	0.3442870E-05	0.2088562E-07
33	0.3919714E-05	-0.5444533E-04	-0.4642259E-02	0.3025559E-04	0.6249047E-05	0.7149032E-07
34	-0.1790333E-04	-0.5514826E-04	0.2505545E-02	0.5739112E-04	0.5437880E-05	0.1680328E-06
35	-0.4763043E-04	-0.5742571E-04	0.1218487E-01	0.7193501E-04	0.6579203E-05	0.2186635E-06
36	-0.7892735E-04	-0.5913329E-04	-0.2225357E-01	0.7631919E-04	0.654743E-05	0.2336517E-06
37	0.5163725E-05	-0.5444764E-04	-0.4465993E-02	-0.3006200E-04	0.6247037E-05	0.9644662E-08
38	0.1222083E-04	-0.5615405E-04	0.2531778E-02	-0.5704904E-04	0.6433754E-05	0.5080776E-07
39	0.2243700E-04	-0.5744700E-04	0.1206393E-01	-0.7152600E-04	0.6573485E-05	0.7163101E-07
40	0.3321132E-04	-0.5914200E-04	0.2226398E-01	-0.7580615E-04	0.6648181E-05	0.7757171E-07

MODE SHAPE 20 OF THE COUPLED SYSTEM IN GLOBAL COORDINATES NORMALIZED TO THE UNIT MODAL MASS

MASS NO.	X(1)	X(2)	X(3)	THETA(1)	THETA(2)	THETA(3)
1	-0.1153519E-05	-0.4648757E-01	0.2215831E-03	-0.3101482E-07	-0.1433701E-07	-0.9410257E-05
2	-0.1253957E-05	-0.3483240E-01	-0.2773616E-03	0.2722057E-07	-0.1695956E-07	-0.2267737E-05
3	-0.3236634E-06	-0.3466570E-01	0.3687798E-03	0.2160227E-07	-0.7258953E-07	-0.1212877E-04
4	0.2401937E-06	-0.2043437E-01	-0.2361594E-03	0.6685849E-08	-0.1743122E-06	-0.1768950E-04
5	0.4223119E-05	-0.6563056E-02	0.6156621E-04	0.4764942E-08	-0.5499115E-07	-0.5104494E-05
6	0.2561451E-05	0.4344650E-02	-0.5705685E-04	-0.46582617E-08	-0.3452563E-06	-0.3150853E-04
7	0.0	0.1607108E-01	-0.1742189E-03	-0.1991074E-07	-0.6042442E-06	-0.5650012E-04

Reproduced from best available copy.

8	0.2	C.590785F-01	-0.6478280F-03	-0.6983414E-07	0.2689002F-06	0.3085230E-04
9	-0.4197309E-05	-0.2436819E-01	0.2936401E-03	0.1613441F-03	0.2068884E-08	-0.2346908E-05
10	-0.6914751E-05	0.1421203E-01	0.2925191E-03	0.3062785E-03	0.1702256E-07	-0.2430515E-05
11	-0.66590102E-05	C.6530999E-01	0.2992472E-03	C.3841151E-03	0.2633532E-07	-0.2493085E-05
12	-0.1053421E-04	0.1191874E 00	0.3024684E-03	C.475280F-03	0.2914995F-07	-0.2526528E-05
13	-0.1249573E-05	-0.2438617E-01	C.2836124E-03	-0.1612087F-03	0.1580245E-07	-0.2346922E-05
14	-0.456591E-05	0.1416143E-01	C.2924521E-03	-0.3060962F-03	0.4473025E-07	-0.2430542E-05
15	C.1276255E-04	0.6531609E-01	0.2991499E-03	-0.3839326E-03	0.5995948E-07	-0.2493117E-05
16	0.2147515E-04	0.1190764E 00	C.3027550E-03	-0.4074634E-03	0.6463955E-07	-0.2526568E-05
17	C.3315539E-05	-0.4587609E-02	0.6280573E-04	0.3037206E-04	0.6355798E-07	-0.5282714E-05
18	-0.1890055E-04	C.2574916E-02	0.6455717E-04	0.5765547F-04	0.1693662E-06	-0.5479070E-05
19	-0.4357545E-04	C.1231061E-01	0.6590186E-04	0.7230778E-04	0.2251012E-06	-0.5611748E-05
20	-0.820937E-04	0.2243604E-01	0.6662028E-04	0.7673394E-04	0.2417817E-06	-0.5587036E-05
21	0.1697745E-04	-0.4590589E-02	0.6280490E-04	-0.3034664E-04	0.2306047E-07	-0.5282714E-05
22	0.3287575E-04	C.2665356E-02	0.6456439E-04	-0.572052E-04	0.9252921E-07	-0.5470911E-05
23	C.5189995E-04	0.1229483E-01	0.6569782E-04	-0.7227255E-04	0.1286747E-06	-0.5611751E-05
24	-0.1497655E-04	C.2241483E-01	C.6661545E-04	-0.7670205E-04	0.1394051E-06	-0.5687036E-05
25	-0.797163E-03	-0.3564682E-01	0.1941328E-03	-0.7670205E-04	-0.1755859E-07	0.2068563E-05
26	-0.1451819E-02	-0.3680809F-01	-0.1190829E-03	-0.2487522E-05	-0.1819065E-07	0.5840303E-05
27	-0.2985574E-02	-0.3767289E-01	-0.5307820E-03	-0.3123926E-05	-0.1865390E-07	0.7797419E-05
28	0.1343997E-04	-0.3565682E-01	-0.9745047E-03	-0.3315687E-05	-0.1891682E-07	0.8370543E-05
29	0.7895593E-03	-0.3580809E-01	0.1948172E-03	0.1245724E-05	-0.1749535E-07	0.2082012E-05
30	C.1857843E-02	-0.3767289E-01	-0.4998476E-04	0.2341140E-05	-0.1805087E-07	0.5865399E-05
31	0.2093333E-02	-0.3811934E-01	-0.4697844E-03	0.3107538E-05	-0.1848417E-07	0.7828092E-05
32	-0.2875179E-04	-0.6714489E-02	0.4398678E-04	-0.2746931E-06	-0.5920363E-07	0.4688478E-05
33	-0.1746695E-02	-0.6929334E-02	-0.2225889E-04	-0.5255266E-06	-0.6154960E-07	0.1320738E-04
34	-0.4203304E-02	-0.7092133E-02	-0.1103080E-03	-0.6602169E-06	-0.6330549E-07	0.1762825E-04
35	-0.6753042E-02	-0.7179759E-02	-0.2029455E-03	-0.7009183E-06	-0.4424803E-07	0.1892502E-04
36	C.3527612E-04	-0.6714489E-02	0.4433481E-04	0.2614727E-06	-0.5906407E-07	0.4654997E-05
37	0.1773473E-02	-0.6929334E-02	-0.1758737E-04	0.4924204E-05	-0.6126311E-07	0.1314259E-04
38	0.4191645E-02	-0.7092133E-02	-0.9967973E-04	0.6168046E-06	-0.6290884E-07	0.1798490E-04
39	0.5729726E-02	-0.7179759E-02	-0.1858864E-03	0.6544718E-06	-0.6378849E-07	0.1863402E-04
40						

APPENDIX A3

BRIEF DESCRIPTION OF EACH SUBROUTINE

- CONFIG - Checks to see that the program limitations are met
- LOGLO - (For each module) Reads the mass point locations in local coordinates and transforms them to global coordinates
- AIJMOD - (For each module) Forms the $[A_{ij}]$ matrix
- MASS - (For each module) Reads the physical mass matrix in local coordinates and transforms to global coordinates
- MODE - (For each module) Sets up T-matrix constraints, reads mode shapes in local coordinates and transforms to global coordinates
- TDEF - Sets up each T-matrix
- FILE - Rewrites the file containing the physical mass matrix in global coordinates for use in later processing
- JOINT - Creates a file of mode shape partitions and one of $[A_{ij}]$ matrix partitions at junction points for use in forming the B-matrix
- FORMB - Forms the B-matrix
- BTMB - Forms B^TMB
- RTDS - Used by BTMB to form R^TDS where D is a partition of the block diagonal mass matrix and R and S are partitions of the B-matrix
- MXI - Reads in modal mass and eigenvalue matrix, stores B^TMB partitions into M_{ξ} matrix and writes it out. MXI then stores the stiffness matrix in the proper form (compressed) for FUTURE. MXI will call CHEAP to perform free-free conversion of problem if needed
- INCH - Used by CHEAP to invert a symmetric matrix
- DIAG - Used by MXI to set up partitions of M_{ξ} matrix lying along diagonal
- OFF - Used by MXI to set up partitions of M_{ξ} matrix lying below the diagonal
- LATE - Solves the eigenvalue problem and orthonormalizes the vectors
- FREE - Back transformation of vectors for free-free systems
- EIGOUT - Transform the eigenvectors back to the physical global coordinate system
- MPRD - Multiply two matrices
- TPRD - Multiply the transpose of a matrix by another matrix
- MCPY - Copy one matrix into another
- LOC810 - Locate member of file 10 - B partition
- LOC811 - Locate member of file 11 - global mass partition
- ZERO - Zeroes out a matrix
- ADD - Obtains the sum of two matrices

APPENDIX A4

SEQUENCE OF OPERATIONS IN SUBROUTINE LATE

Subroutine LATE requires additional discussion. This subroutine solves the coupled-structure eigenvalue problem which is in the following form:

$$AX = \lambda BX \quad \text{where } A \text{ is symmetric} \\ \text{and } B \text{ is symmetric, positive definite}$$

CALL FUTILE to find the Cholesky Decomposition of B

$$B = L L^T$$

CALL DAGGER repeatedly to form $L^{-1} A L^{-T}$

the eigenvalue problem to be solved is

$$(L^{-1} A L^{-T})(L^T X) = \lambda (L^T X)$$

CALL SWITCH to store the matrix $L^{-1} A L^{-T}$ in a form acceptable to SYMEIG

CALL SYMEIG to solve the eigenvalue problem giving the λ 's

CALL SYMVEC (An entry point of SYMEIG) to give the eigenvectors $Y = L^T X$

CALL ORTHON to orthonormalize the set of eigenvectors Y

CALL TRIEQ to find X given $Y = L^T X$

For this program

A is the M_{ξ} matrix, and

B is the k_{ξ} matrix, except for nonsingular systems (those with rigid-body modes) where

$$A = ([M_{22}]_{\xi} - [M_{12}]_{\xi}^T [M_{11}]_{\xi}^{-1} [M_{12}]_{\xi}), \text{ and} \\ B = [k_{22}]_{\xi}$$

APPENDIX A5

INPUT, OUTPUT, AND INTERMEDIATE FILES

FILES 1, 2, 3, 4, 7, 8, 9, 10 - intermediate files

These files are used to temporarily hold matrix partitions to be used later in the program. All files are unformatted. Details are indicated in the program flow charts.

FILE 11 - output file

File 11 is the output file to the Phase II program corresponding to run number 1 (usually the Laboratory run). Write statements are in CONFIG, LOGLO, FILE, and EIGOUT.

FILE 12 - output file

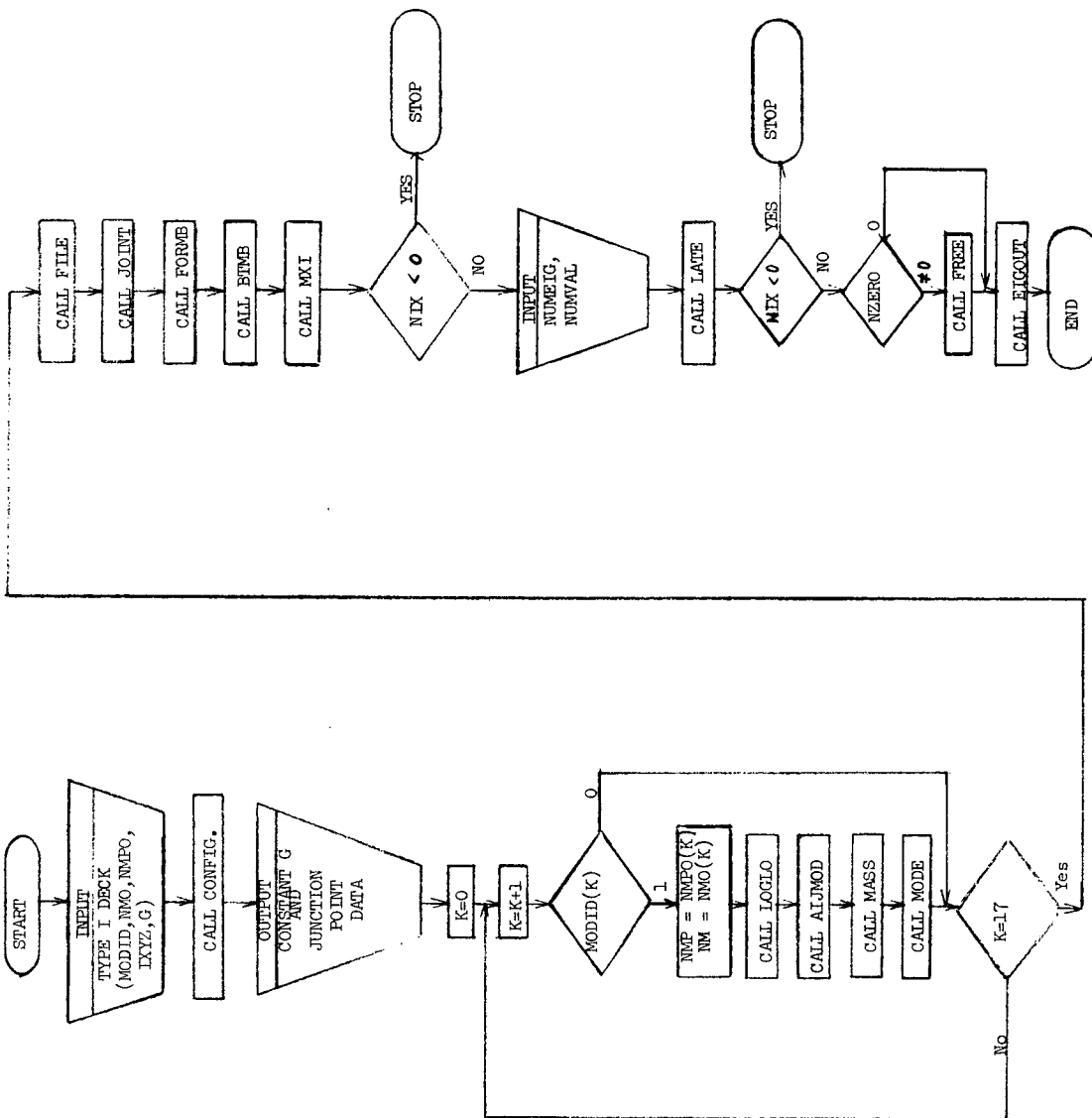
File 12 is the output file to the Phase II program corresponding to run number 2 (usually the Counterweight run). The write statements are the same write statements as those used in FILE 11.

APPENDIX A6

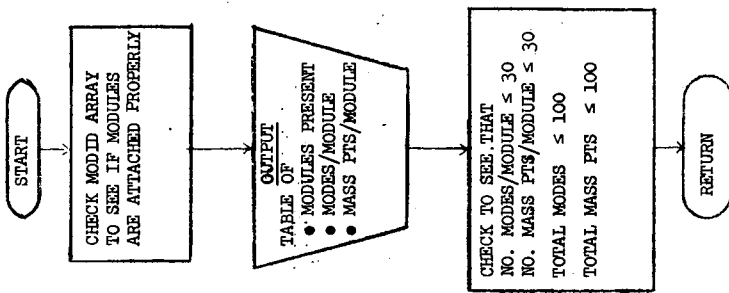
PROGRAM FLOW CHARTSSymbols Used in the Flow Charts

- MODID - The array used to denote absence or presence of each module.
- NMO - The array used to keep the number of modes for each module
- NMPO - The array used to keep the number of mass points for each module
- IXYZ - The array used to store mass point numbers of the attachment points for each attached module
- G - Constant G
- NIX - Error return indicator from INCH and FUTILE
- NUMEIG - Number of eigenvectors to be found by SYMVEC
- NUMVAL - Number of eigenvalues to be found by SYMEIG
- NZERO - Number of rigid body modes
- XYZ - Array containing X_O , X_A , X_B , and mass point locations when read in, then later holding mass point locations in absolute global coordinates
- XYZBAR - Array containing mass point locations in relative global coordinates when computed
- MPN - Current mass point number for a module
- NMP - Number of mass points for a module

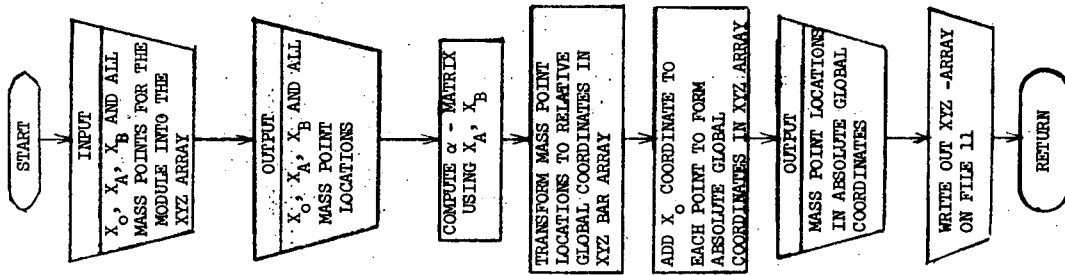
MAIN PROGRAM



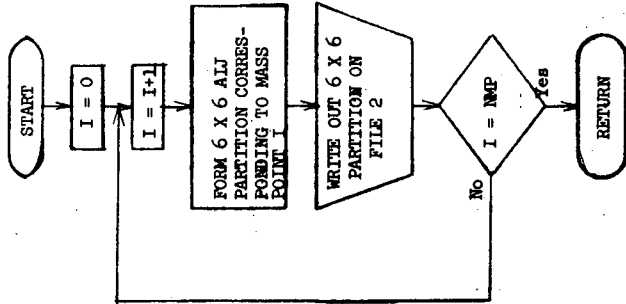
SUBROUTINE CONFIG.



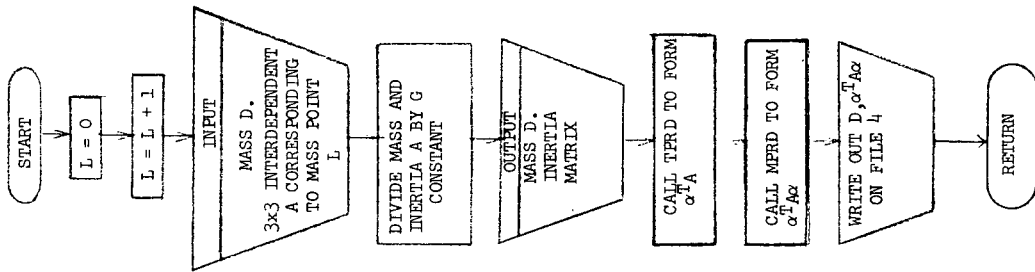
SUBROUTINE LOGLO



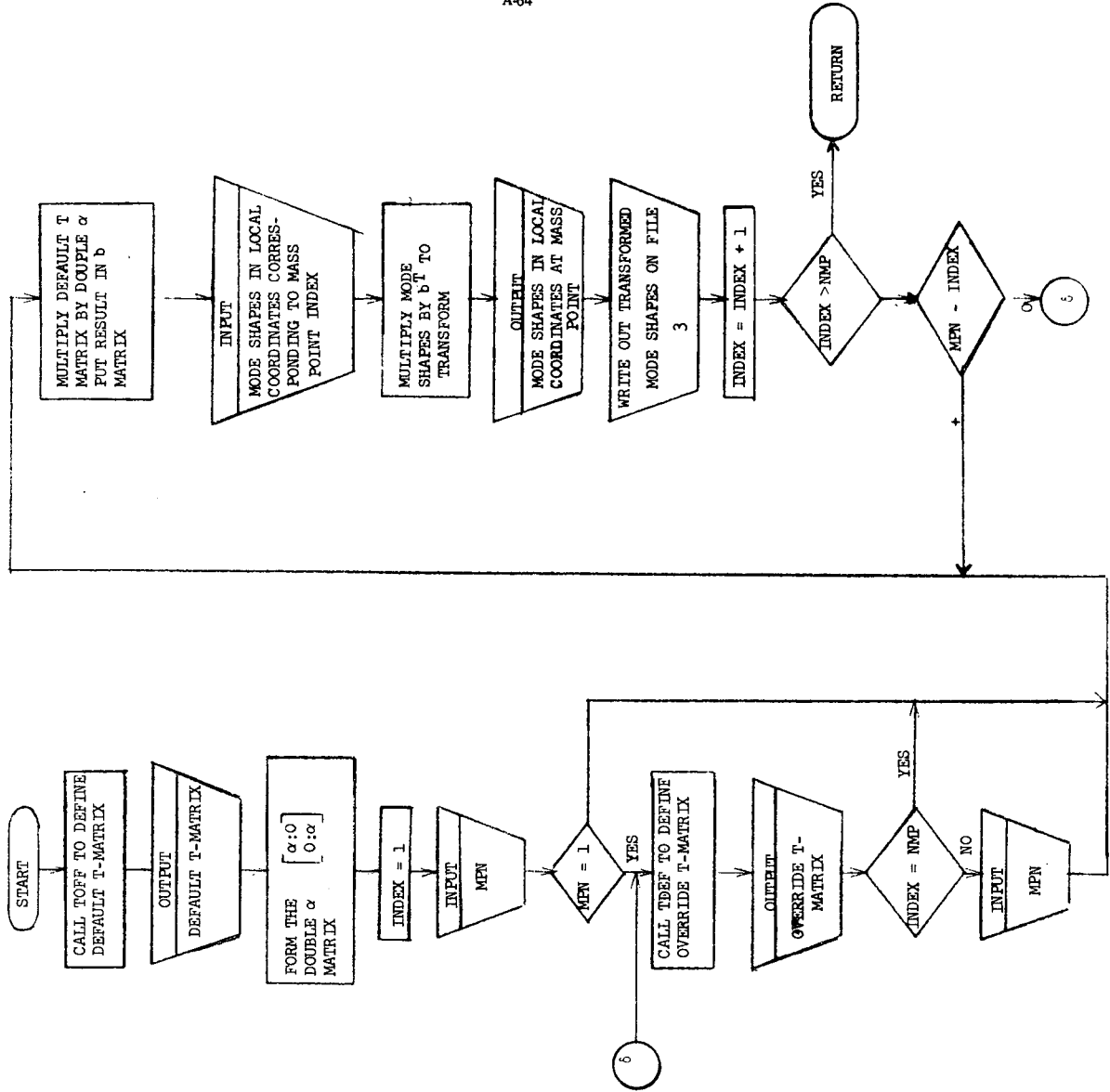
SUBROUTINE ALLMOD



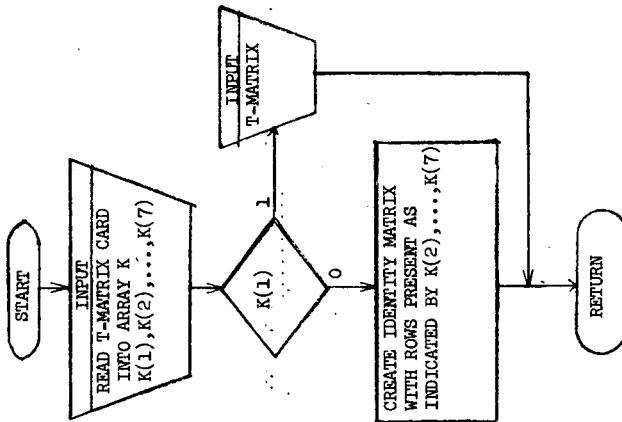
SUBROUTINE MASS



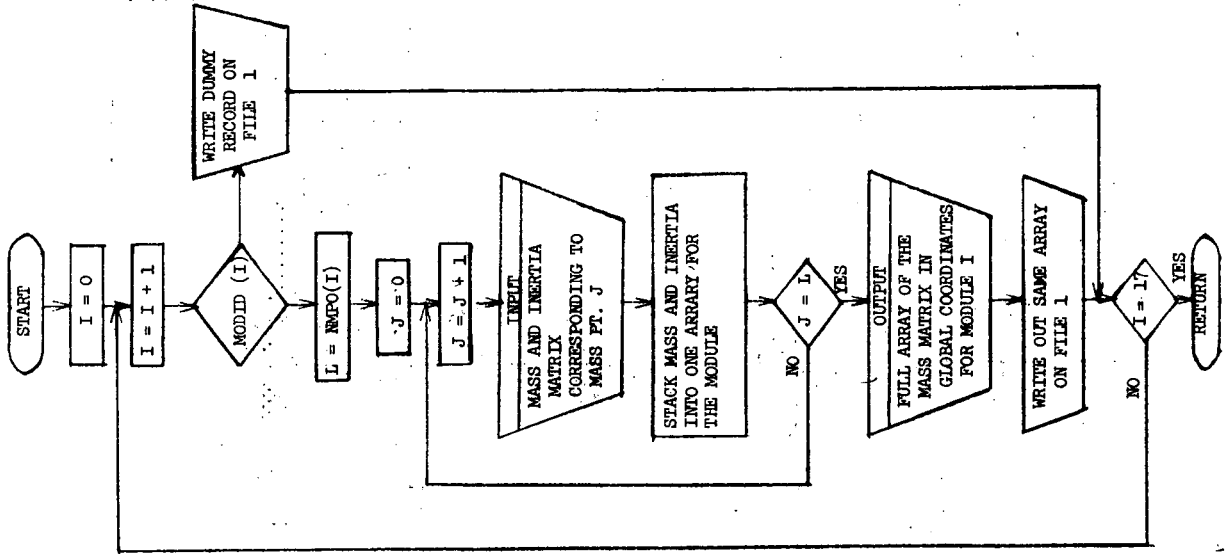
SUBROUTINE MODE



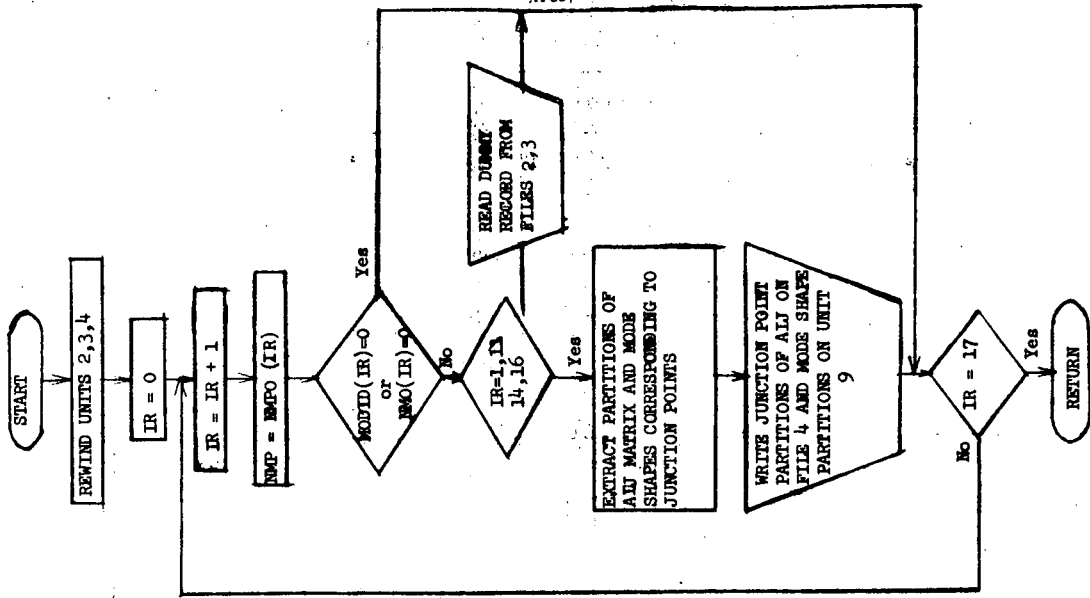
SUBROUTINE TDEF

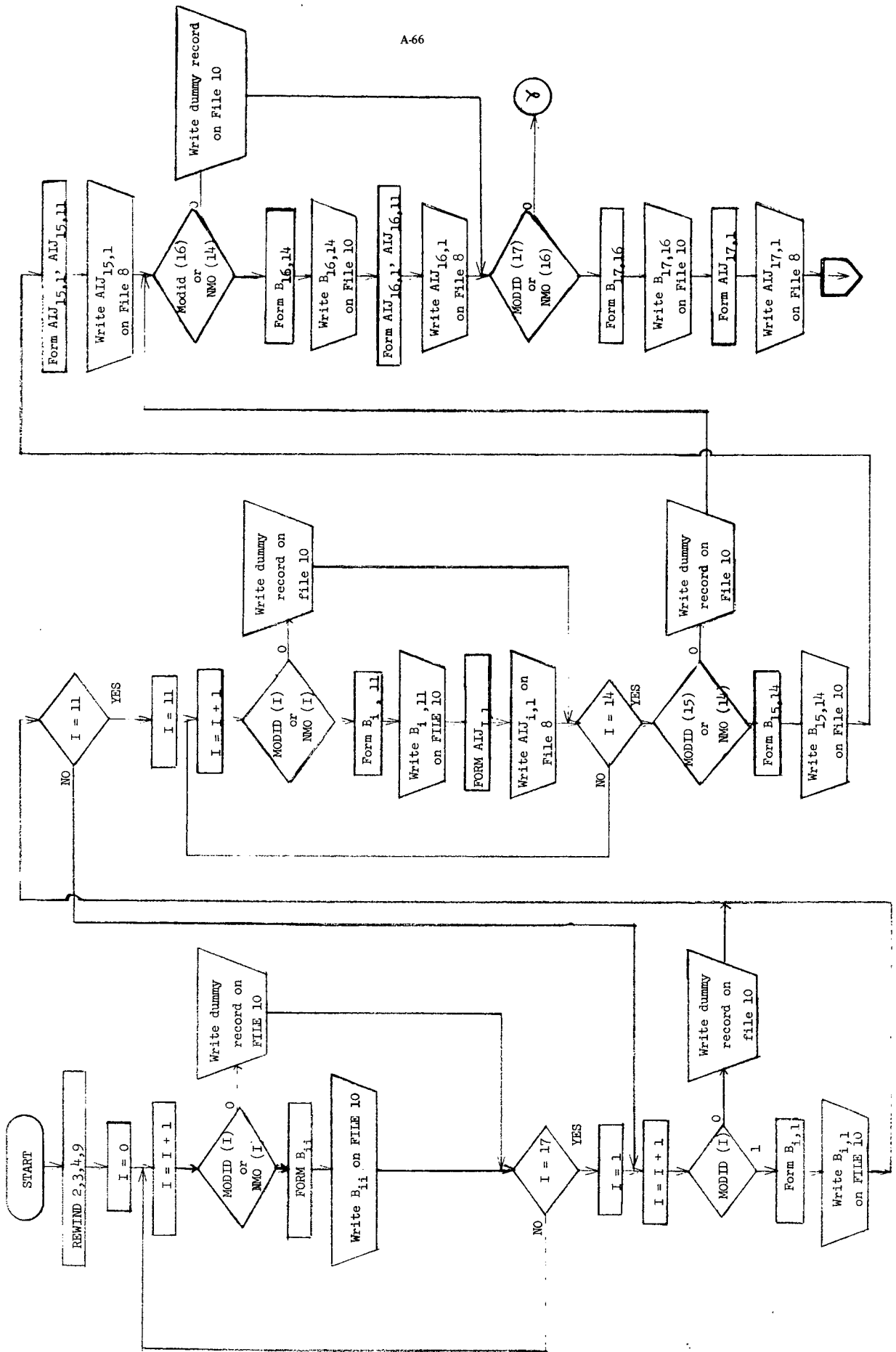


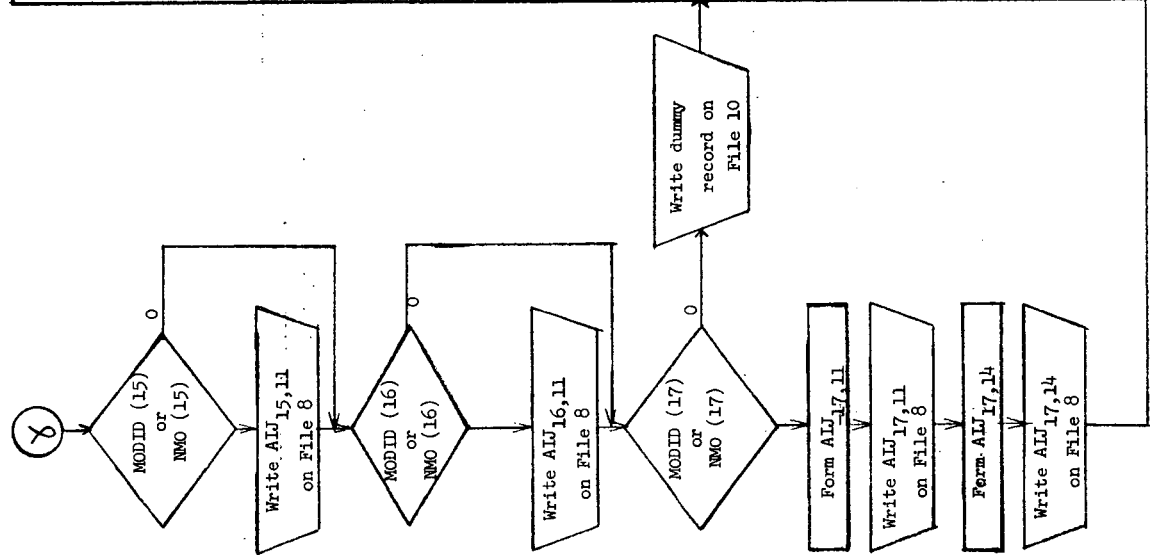
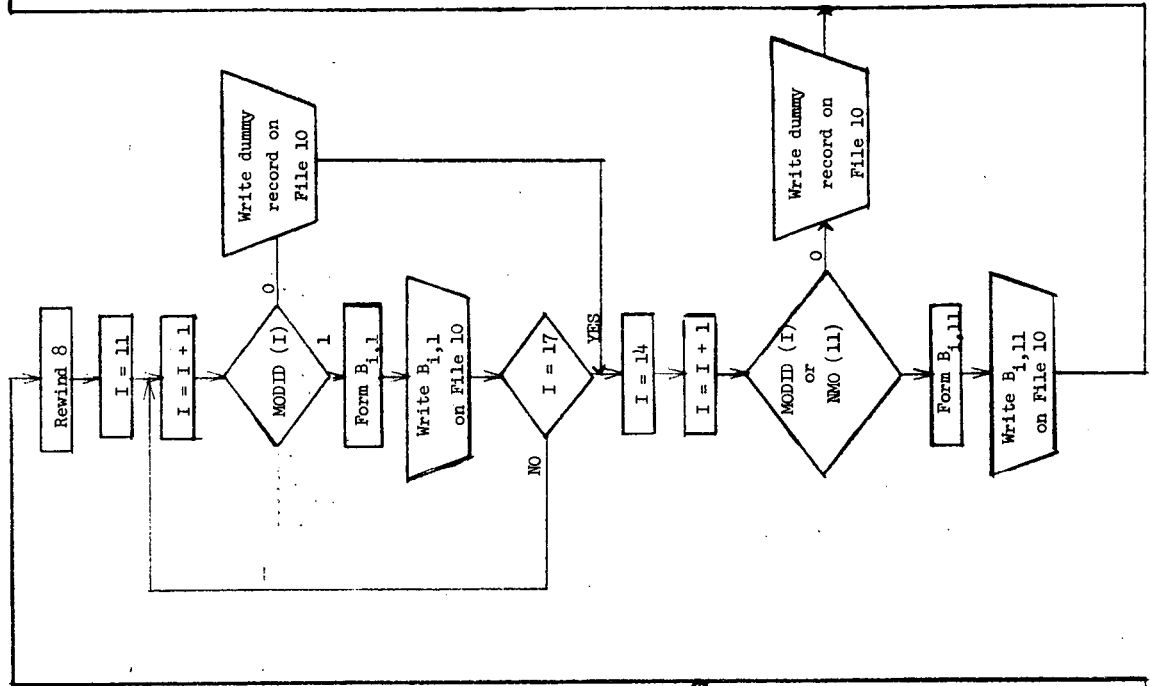
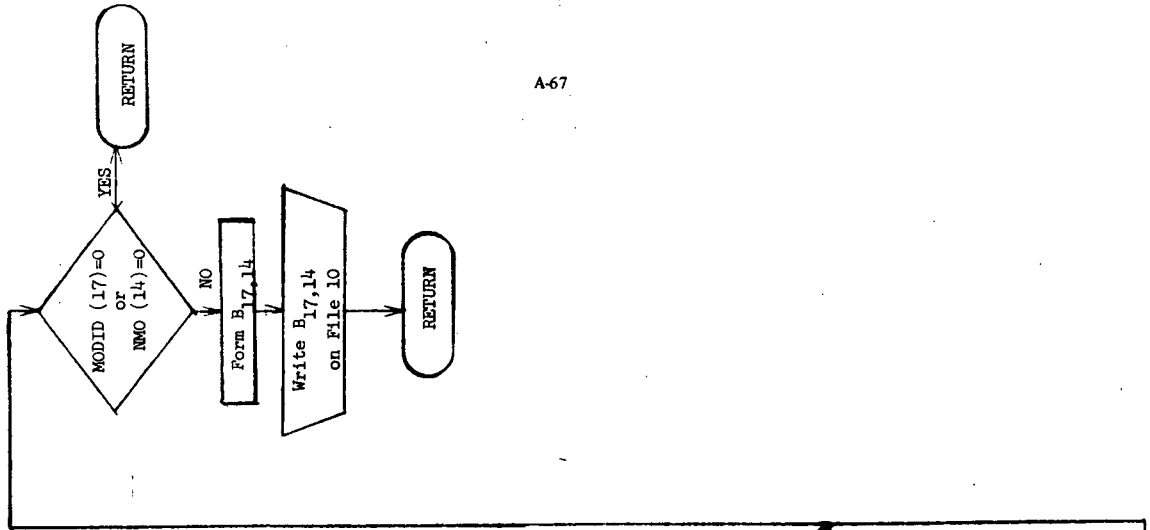
SUBROUTINE FILE



SUBROUTINE JOINT

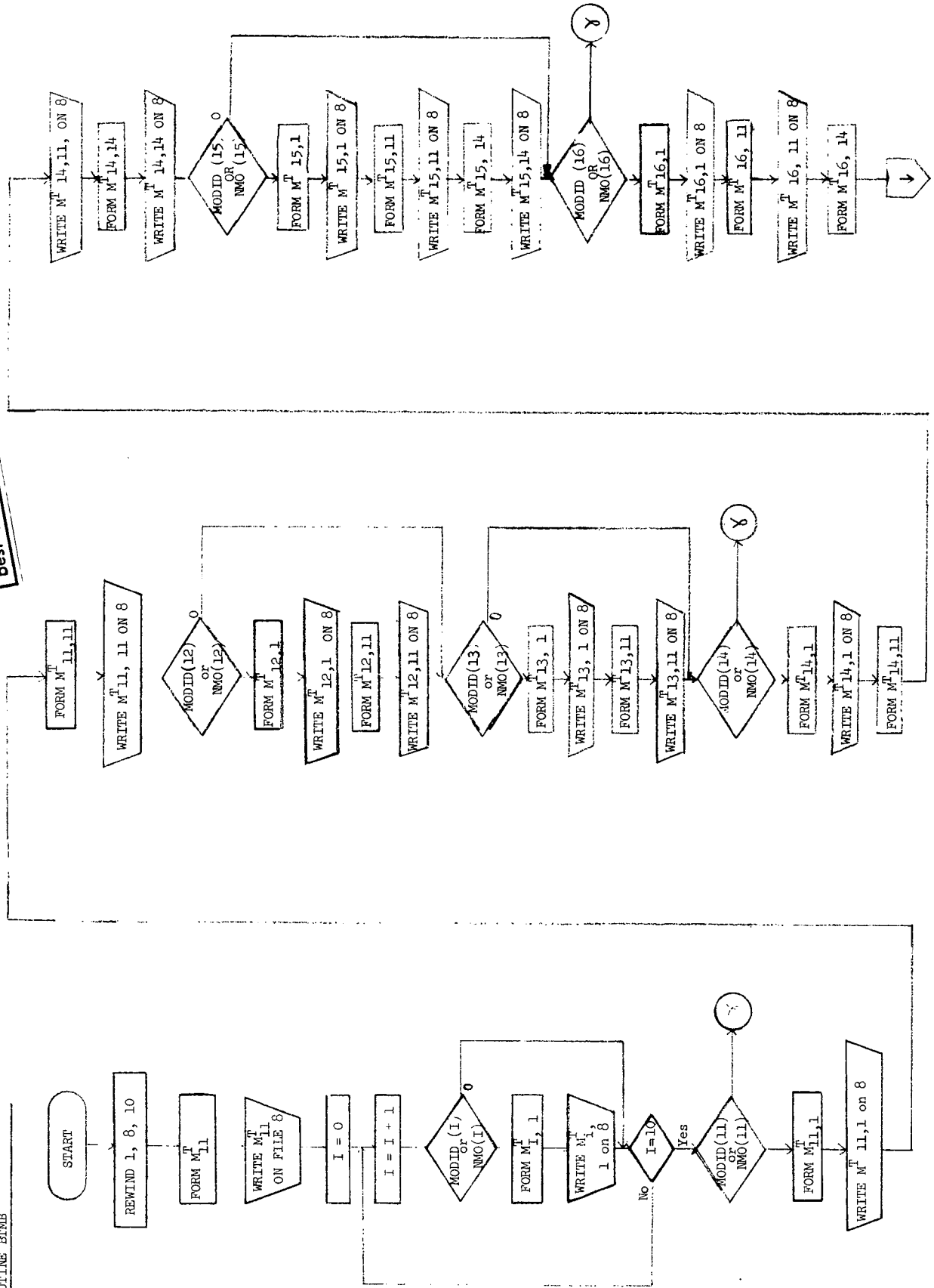


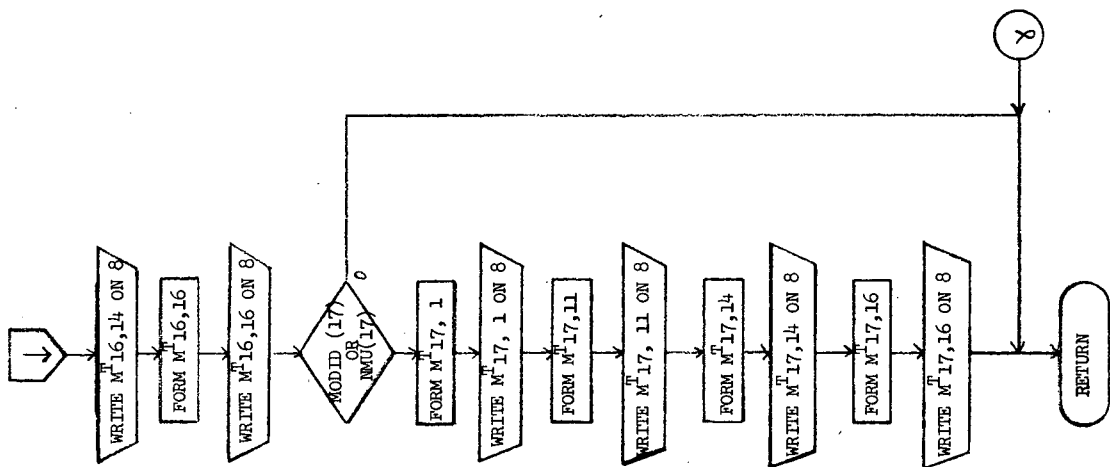


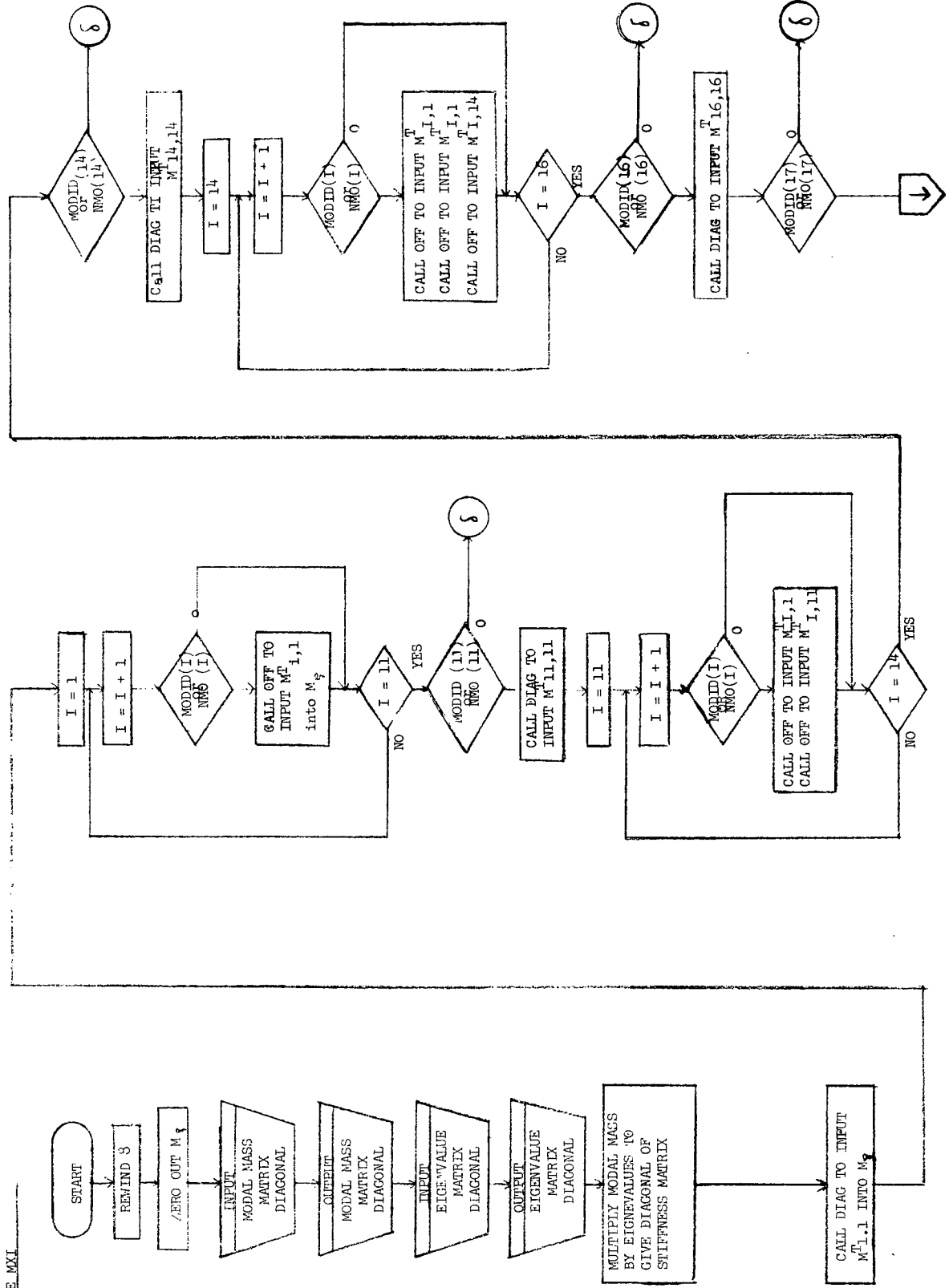


SUBROUTINE BTMB

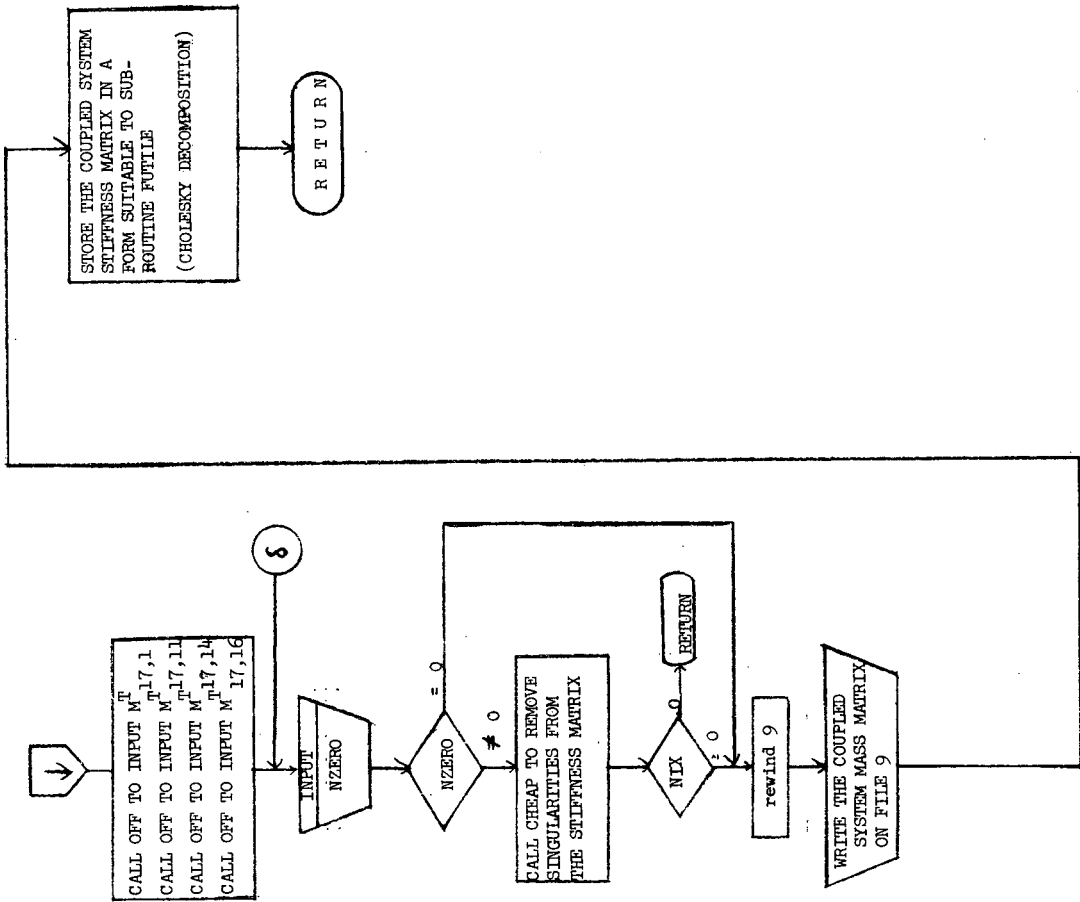
Reproduced from best available copy.



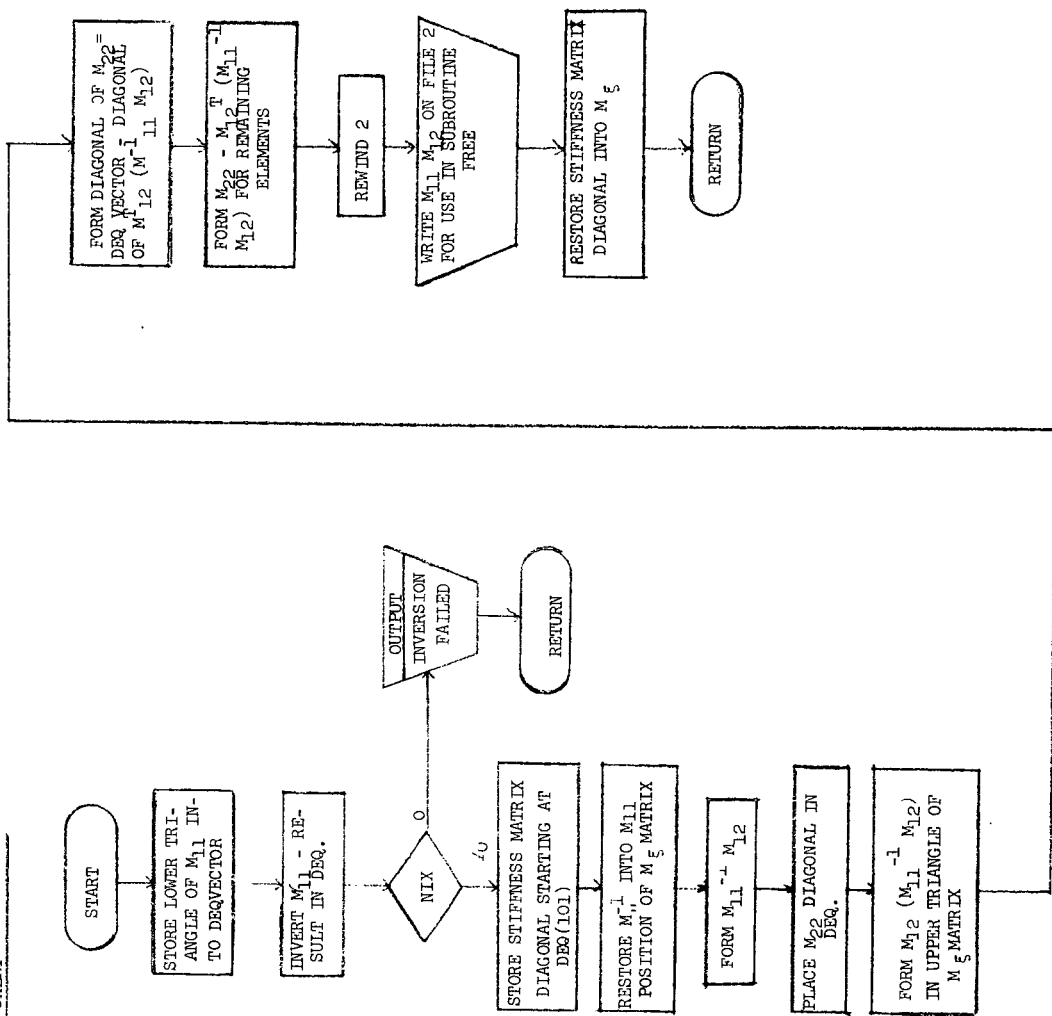




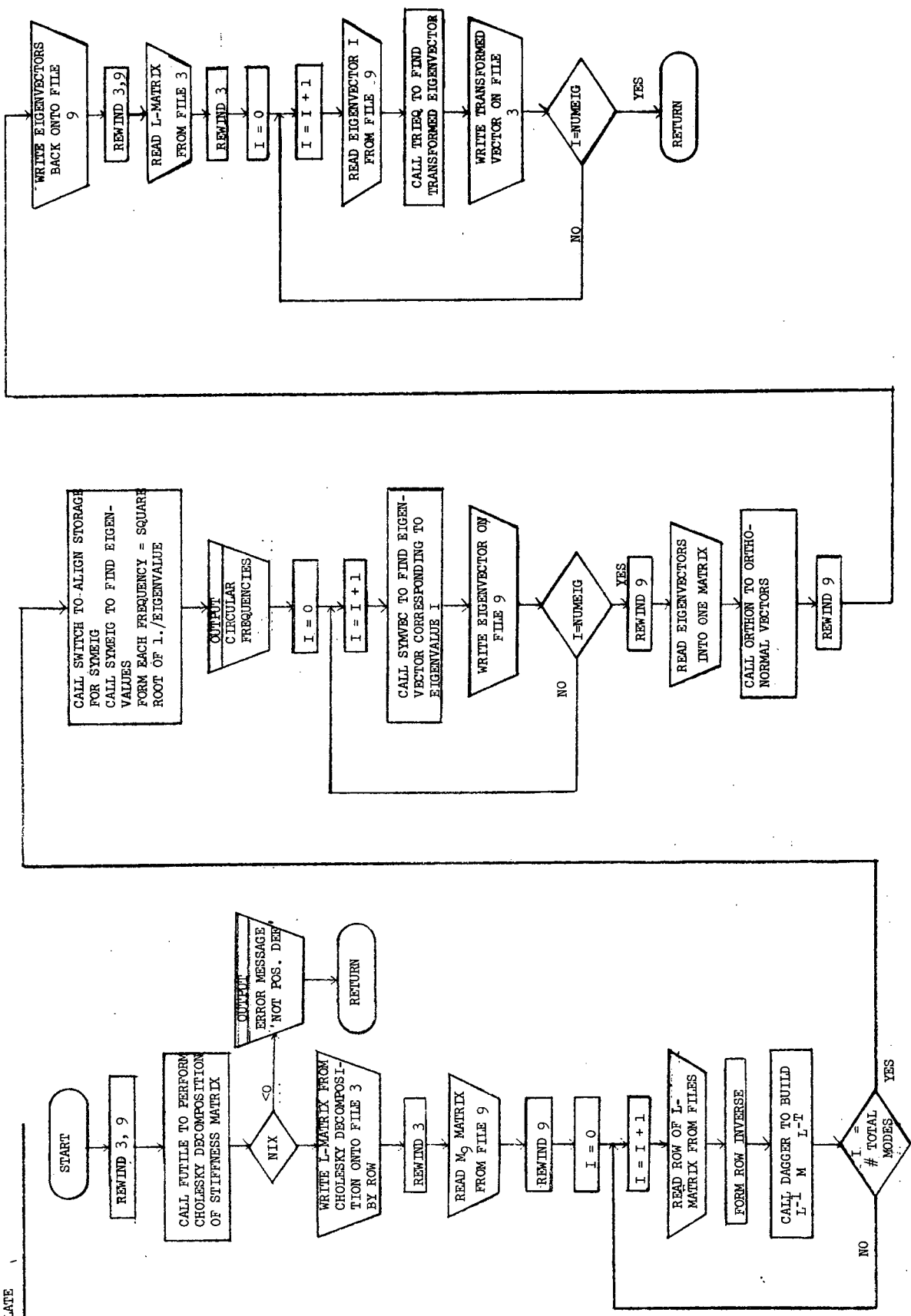
SUBROUTINE MXI



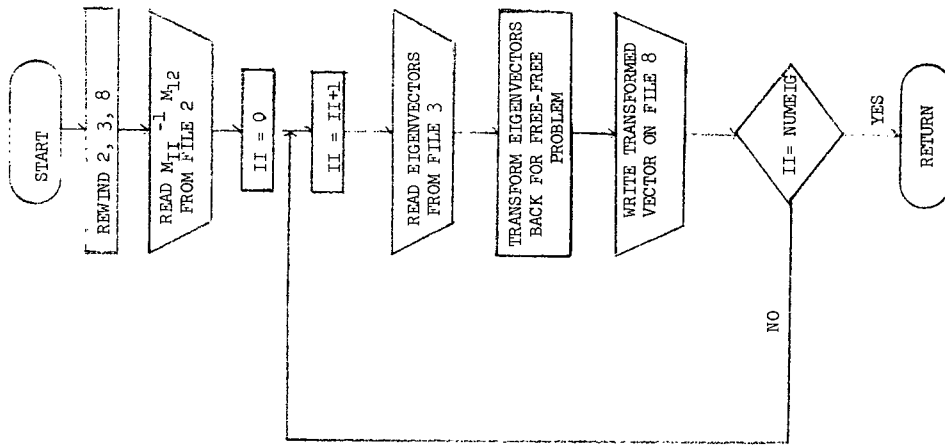
SUBROUTINE CHEAP



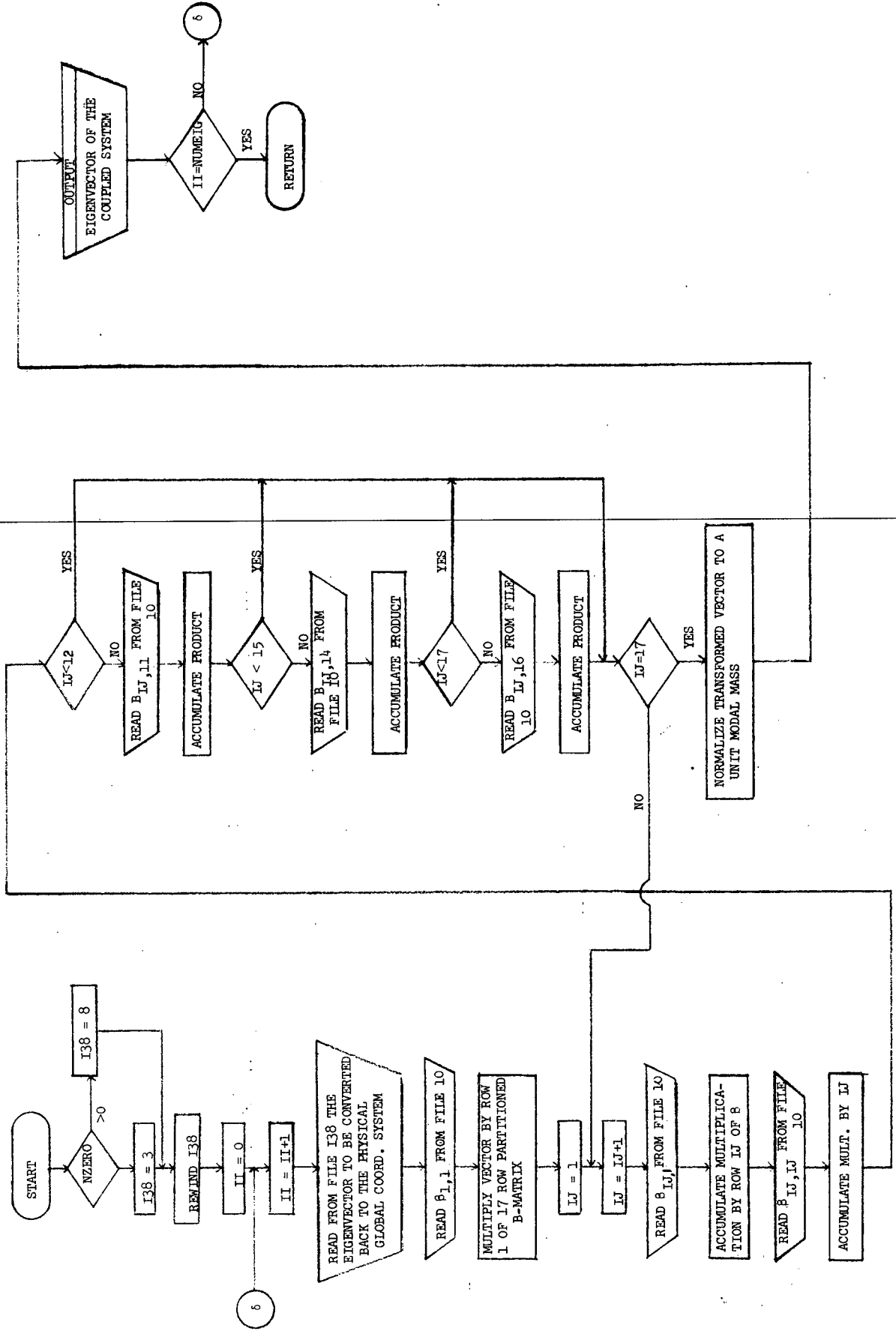
SUBROUTINE
LATE



SUBROUTINE FREE



SUBROUTINE EIGOUT



APPENDIX A7

FORTRAN SOURCE DECK LISTING

The fortran source deck listing appears on the following pages. This listing shows the LRC CDC version of the program.

```

PROGRAM SPACE(INPUT=201,OUTPUT=201,TAPE5=INPUT,TAPE6=OUTPUT,
* TAPE1=401,TAPE2=401,TAPE3=401,TAPE4=401,
* TAPE8,TAPE9=401,TAPE10,TAPE11=401,TAPE12=201)
COMMON A
10000030
10000040
10000050
10000060
10000070
10000080
10000090
10000100
10000110
10000120
10000130
10000140
10000150
10000160
10000170
10000180
10000190
10000200
10000210
10000220
10000230
10000240
10000250
10000260
10000270
10000280
10000290
10000300
10000310
10000320
10000330
10000340
10000350
10000360
10000370
10000380
10000390
10000400
C
C DYNAMICS OF ROTATING SPACE STATIONS
C PHASE I , MODAL COUPLING
C
DIMENSION MODID(17),NMO(17),NMPO(17),A(11300),B(900),IXYZ(16)
COMMON /A1/MODID,NMO,NMPO /A2/B /INPUT/IO5,IO6,IOFF,LL
COMMON /WINTER/Q1
COMMON /BOND/Q2(2)
COMMON /INFU/Q3(5)
COMMON /OPT2/Q4
IO5=5
IO6=6
LL=11
IOFF=0
DO 99 II=1,2
WRITE(IO6,400)
400 FORMAT(1H1,20(/),47X,*DYNAMICS OF ROTATING SPACE STATIONS*////
* 61X,*PHASE I*//57X,*MODAL COUPLING*)
CALL SETIO
CALL SET11
READ(IO5,1)
IF(EOF,IO5)99,199
199 CONTINUE
READ(IO5,5)G
C
C* CHECK FOR REASONABLE CONFIGURATION
C
CALL CONFIG(IER,NTNM,NTNMP,MODHI)
IF(IER.NE.0)STOP
IF(IOFF.GE.20)GO TO 101
WRITE(IO6,6)G
WRITE(IO6,2)(I,I=2,17),(IXYZ(I),I=1,16)
C
C* FOR EACH MODULE OR APPENDAGE...
C
101 DO 10 K=1,17
IF(MODID(K).EQ.0)GO TO 10
IF(IOFF.GE.5)GO TO 102

```

```

WRITE(I06,22)K
102 NMF=NMPO(K)
    NA=NM0(K)
C* CHANGE LOCAL TO GLOBAL COORDINATES + COMPUTE ALPHA
C
C 21 CALL LOGLO (NMP,A,A(310),A(160))
C
C* CONSTRUCT AIJ,STORE K,NMP,AIJ ON DISK
C
C    CALL AIJMOD(A(160),NMP,K,A(320))
C
C* READ MASS MATRIX,TRANSFORM,STORE ON DISK
C
C    CALL MASS(A(310),NMP,A,G)
C
C* READ IN T-MATRIX DATA,READ IN PHI-X,CHANGE PHI-X TO GLOBAL
C COORDINATES,COMPUTE NDOF,STORE NDOF,PHI-X ON DISK
C
C    IF(NM.EQ.0)GO TO 10
C    CALL MODE(A(310),NM,NDJF,NMP,K,A(5000),A(6000))
10 CONTINUE
C    CALL FILE
C    CALL JJINT(A,IXYZ,A(5000),A(9000),A(9500))
C
C* READ JUNCTION POINT DATA,FORM ADDITIONAL AIJ'S,STORE THEM ON DISK,
C COMPUTE B-MATRIX PARTITIONS,STORE THEM ON DISK
C
C    CALL FORMB(A,A(1081),A(6431),A(7561),A(8541),A(8321),A(9001),
*      A(9181),A(9361),A(9637),A(9673),A(9709))
C    CALL BTMB(A,A(301),A(5701),B)
C
C* CHANGE M-XI TO STORE FOR LATENT , ALSO STORE K-XI
C
C    CALL MXI(A,A,NTNM,B,NIX,NZERU)
C    IF(NIX.LT.0)STOP
C    TOL=.1E-9
C    READ(I05,3)NUMEIG,NUMVAL
C
C* SOLVE THE EIGENVALUE PROGRAM
C    (M-XI)(PHI)=(LAMBDA)(K-XI)(PHI)
C
C    N=NTNM

```

```

L0000410
L0000420
L0000430
L0000440
L0000450
L0000460
L0000470
L0000480
L0000490
L0000500
L0000510
L0000520
L0000530
L0000540
L0000550
L0000560
L0000570
L0000580
L0000590
L0000600
L0000610
L0000620
L0000630
L0000640
L0000650
L0000660
L0000670
L0000680
L0000690
L0000700
L0000710
L0000720
L0000730
L0000740
L0000750
L0000760
L0000770
L0000780
L0000790
L0000800
L0000810
L0000820
L0000830
L0000840
L0000850

```

```

CALL LATE(N,A,NUMEIG,TOL,A(9000),NIX,B,NJMVAL)
IF(NIX.LT.0)STOP
C* TRANSFORM EIGENVECTORS TO PHYSICAL GLOBAL COORDINATES
C
IF(NZERO.NE.0)CALL FREE(A,N,NZERO,NJMEIG,B(101))
CALL EIGOUT(N,NZERO,NUMEIG,A,A(5401),A(5501),A(6101),NTNMP,B)
REWIND 1
REWIND 2
REWIND 3
REWIND 4
REWIND 8
REWIND 9
REWIND 10
LL=LL+1
99 CONTINUE
STOP
1 FORMAT(17I2)
2 FORMAT(* JUNCTION POINT DATA*/* MODULE * ,16I3/* JUNCTION
*POINT *,16I3)
3 FORMAT(2I3)
5 FORMAT(E15.8)
6 FORMAT(* CONSTANT G FOR THE PROGRAM =*,E16.8)
22 FORMAT(//11H ** MODULE ,I2,3H **//)
END

```

L0000830	8600000
L0000840	8700000
L0000850	8800000
L0000860	8900000
L0000870	9000000
L0000880	9100000
L0000890	9200000
L0000900	9300000
L0000910	9400000
L0000920	9500000
L0000930	9600000
L0000940	9700000
L0000950	9800000
L0000960	9900000
L0000970	10000000
L0000980	10100000
L0000990	10200000
L0001000	10300000
L0001010	10400000
L0001020	10500000
L0001030	10600000
L0001040	10700000
L0001050	10800000
L0001060	10900000
L0001070	11000000

```

SUBROUTINE CONFIG( IER, NM, NMP, MODHI )
COMMON /AL/MODID(17),NM0(17),NMP0(17)
COMMON /INOUT/IO5,IO6,IOFF,LL
IER=0
J=0
NM=0
NMP=0
MODHI=0
IF(MODID(1).EQ.0)IER=1
K=MCDID(12)+MODID(13)+MODID(14)
IF(K.NE.0 .AND. MODID(11).EQ.0)IER=11
K=MODID(15)+MODID(16)
IF(K.NE.0 .AND. MODID(14).EQ.0)IER=14
IF(MODID(17).NE.0 .AND. MODID(16).EQ.0)IER=16
IF(IOFF.GE.20)GO TO 101
WRITE(IO6,1)
101 DO 5 I=1,17
IF(MODID(I).EQ.0)GO TO 5
IF(IOFF.GE.20)GO TO 102
WRITE(IO6,2)I,NM0(I),NMP0(I)
102 NM=NM+NM0(I)
NMP=NMP+NMP0(I)
J=J+1
IF(NM0(I).GT.30)IER=1
IF(NMP0(I).GT.30)IER=1
MODHI=I
5 CONTINUE
WRITE(LL)J
IF(NM.LE.100 .AND. NMP.LE.100)GO TO 20
IER=20
WRITE(IO6,4)NM,NMP
RETURN
20 IF(IER.NE.0)WRITE(IO6,3)IER
RETURN
1 FORMAT(#ICONFIGURATION SPECIFIED//
* 45H MODULE NO. * NO. MODES * NO. MASS POINTS )
2 FORMAT(5X,I2,I3X,I2,I4X,I2)
3 FORMAT(#11MPRPER CONFIGURATION AT MODULE*,I3)
4 FORMAT(#100 MANY TOTAL MODES OR MASS POINTS*/ * MODES =*,I3/
* * MASS POINTS =*,I4)
END

```

```

L0001080 11100000
L0001090 11200000
L0001100 11300000
L0001110 11400000
L0001120 11500000
L0001130 11600000
L0001140 11700000
L0001150 11800000
L0001160 11900000
L0001170 12000000
L0001180 12100000
L0001190 12200000
L0001200 12300000
L0001210 12400000
L0001220 12500000
L0001230 12600000
L0001240 12700000
L0001250 12800000
L0001260 12900000
L0001270 13000000
L0001280 13100000
L0001290 13200000
L0001300 13300000
L0001310 13400000
L0001320 13500000
L0001330 13600000
L0001340 13700000
L0001350 13800000
L0001360 13900000
L0001370 14000000
L0001380 14100000
L0001390 14200000
L0001400 14300000
L0001410 14400000
L0001420 14500000
L0001430 14600000
L0001440 14700000
L0001450 14800000
L0001460 14900000
L0001470 15000000
L0001480 15100000

```

```

SUBROUTINE LOGLO(NMP,XYZ,ALPHA,XYZBAR)
DIMENSION XYZ(53,3),ALPHA(3,3),XYZBAR(50,3)
COMMON /INOUT/I05,I06,I0FF,LL
C* FIRST 3 POINTS IN XYZ ARE POINTS O,A, AND B
C
NMPP3=NMP+3
READ(I05,2)((XYZ(I,J),J=1,3),I=1,NMPP3)
IF(I0FF.GE.5)GO TO 201
WRITE(I06,24)
DO 20 I=4,NMPP3
  I1=I-3
  20 WRITE(I06,21)I1,(XYZ(I,J),J=1,3)
  WRITE(I06,22)((XYZ(I,J),J=1,3),I=1,3)
C
C* SET UP ALPHA
C
  201 CK=SQRT(XYZ(2,1)*XYZ(2,1)+XYZ(2,2)*XYZ(2,2)+XYZ(2,3)*XYZ(2,3))
  DO 10 I=1,3
    ALPHA(3,I)=XYZ(2,I)/CK
    A21=XYZ(2,2)*XYZ(3,3)-XYZ(3,2)*XYZ(2,3)
    A22=XYZ(3,1)*XYZ(2,3)-XYZ(2,1)*XYZ(3,3)
    A23=XYZ(2,1)*XYZ(3,2)-XYZ(3,1)*XYZ(2,2)
    CK=SQRT(A21*A21+A22*A22+A23*A23)
    ALPHA(2,1)=A21/CK
    ALPHA(2,2)=A22/CK
    ALPHA(2,3)=A23/CK
    ALPHA(1,1)=ALPHA(3,3)*ALPHA(2,2)-ALPHA(3,2)*ALPHA(2,3)
    ALPHA(1,2)=ALPHA(3,1)*ALPHA(2,3)-ALPHA(3,3)*ALPHA(2,1)
    ALPHA(1,3)=ALPHA(3,2)*ALPHA(2,1)-ALPHA(3,1)*ALPHA(2,2)
C
C FORM XYZBAR
C
  202 DO 12 I=1,NMP
    DO 12 J=1,3
      XYZBAR(I,J)=0.
      DO 12 K=1,3
        12 XYZBAR(I,J)=XYZBAR(I,J)+ALPHA(K,J)*XYZ(I+3,K)
      DO 11 I=1,NMP
        DO 11 J=1,3
          I1=I+3
          11 XYZ(I1,J)=XYZBAR(I,J)+XYZ(1,J)

```

```

L0001490 15200000
L0001500 15300000
L0001510 15400000
L0001520 15500000
L0001530 15600000
L0001540 15700000
L0001550 15800000
L0001560 15900000
L0001570 16000000
L0001580 16100000
L0001590 16200000
L0001600 16300000
L0001610 16400000
L0001620 16500000
L0001630 16600000
L0001640 16700000
L0001650 16800000
L0001660 16900000
L0001670 17000000
L0001680 17100000
L0001690 17200000
L0001700 17300000
L0001710 17400000
L0001720 17500000
L0001730 17600000
L0001740 17700000
L0001750 17800000
L0001760 17900000
L0001770 18000000
L0001780 18100000
L0001790 18200000
L0001800 18300000
L0001810 18400000
L0001820 18500000
L0001830 18600000
L0001840 18700000
L0001850 18800000
L0001860 18900000
L0001870 19000000
L0001880 19100000
L0001890 19200000
L0001900 19300000

```

```

IF(ICFF.GE.5)GO TO 30
WRITE(I06,26)
DO 40 I=4,NMPP3
  I1=I-3
  40 WRITE(I06,21)I1,(XYZ(I,J),J=1,3)
C
C  WRITE TRANSFORMED MASS POINTS ON TAPE I1 FOR LATER JOB PHASE
C
30 WRITE(LL)NMP
  WRITE(LL)((XYZ(I,J),J=1,3),I=4,NMPP3)
  RETURN
  2 FORMAT(3E15.8)
  21 FORMAT(3X,I3,3X,3E16.7)
  22 FORMAT(*COORDINATES OF POINT 0*/ 9X , 3E16.7 /
  * * COORDINATES OF POINT A*/ 9X , 3E16.7 /
  * * COORDINATES OF POINT B*/ 9X , 3E16.7 )
  24 FORMAT(// * MASS POINT LOCATIONS IN LOCAL COORDINATES*/*OMASS NU.*
  *,19X,*COORDINATES*/)
  26 FORMAT(// * MASS POINT LOCATIONS IN ABSOLUTE GLOBAL COORDINATES*//
  * * MASS NO.* ,19X,*COORDINATES*//)
END

```

L0001910	19400000
L0001920	19500000
L0001930	19600000
L0001940	19700000
L0001950	19800000
L0001960	19900000
L0001970	20000000
L0001980	20100000
L0001990	20200000
L0002000	20300000
L0002010	20400000
L0002020	20500000
L0002030	20600000
L0002040	20700000
L0002050	20800000
L0002060	20900000
L0002070	21000000
L0002080	21100000
L0002090	21200000
L0002100	21300000
L0002110	21400000

```

SUBROUTINE MASS(ALPHA,NMP,A,G)
DIMENSION ALPHA(3,3),A(1)
COMMON/INOUT/IO5,IO6,IOFF
IF(IOFF.GE.5)GO TO 201
WRITE(IO6,2)
201 DO 10 L=1,NMP
C
C READ MATRIX COLUMN BY COLUMN
C
READ(IO5,1)D,(A(I),I=1,9)
U=D/G
DO 7 I=1,9
7 A(I)=A(I)/G
IF(IOFF.GE.5)GO TO 202
WRITE(IO6,3)I,D,(A(I),I=1,9)
202 CALL TPRD(ALPHA,A,A(10),3,3,3,3,3)
CALL MPRD(A(10),ALPHA,A,3,3,3,3,3)
10 WRITE(4)D,(A(J),J=1,9)
RETURN
1 FORMAT(E15.8/13E15.8)
2 FORMAT(/ * MASSES AND MOMENTS OF INERTIA IN LOCAL COORDINATES*//
* * MASS NO. *,7X,*MASS*,25X,*INERTIA MATRIX*//)
3 FORMAT(3X,13,3X,E16.7,5X,3E16.7/30X,3E16.7/30X,3E16.7/)
END
L0002120 21500000
L0002130 21600000
L0002140 21700000
L0002150 21800000
L0002160 21900000
L0002170 22000000
L0002180 22100000
L0002190 22200000
L0002200 22300000
L0002210 22400000
L0002220 22500000
L0002230 22600000
L0002240 22700000
L0002250 22800000
L0002260 22900000
L0002270 23000000
L0002280 23100000
L0002290 23200000
L0002300 23300000
L0002310 23400000
L0002320 23500000
L0002330 23600000
L0002340 23700000
L0002350 23800000

```



```

SUBROUTINE AIJMOD(XYZ,NMP,K,AIJ)
DIMENSION XYZ(50,3),AIJ(180,6)
NMP16=NMP*6
IF(K.GT.1)GO TO 2
DO 1 I=1,180
  DO 1 J=1,6
    1 AIJ(I,J)=0.
RETURN
2 DO 10 I=1,NMP
  L=I
  M=6*(I-1)
  AIJ(M+1,5)=XYZ(L,3)
  AIJ(M+1,6)=-XYZ(L,2)
  AIJ(M+2,4)=-XYZ(L,3)
  AIJ(M+2,6)=XYZ(L,1)
  AIJ(M+3,4)=XYZ(L,2)
  AIJ(M+3,5)=-XYZ(L,1)
  DO 10 J=1,6
    10 AIJ(M+J,J)=1.0
  DO 20 L=L+1,NMP
    M=6*L-5
    MP5=M+5
    20 WRITE(2)((AIJ(I,J),J=1,6),I=M,MP5)
RETURN
END

```

```

L0002360 23900000
L0002370 24000000
L0002380 24100000
L0002390 24200000
L0002400 24300000
L0002410 24400000
L0002420 24500000
L0002430 24600000
L0002440 24700000
L0002450 24800000
L0002460 24900000
L0002470 25000000
L0002480 25100000
L0002490 25200000
L0002500 25300000
L0002510 25400000
L0002520 25500000
L0002530 25600000
L0002540 25700000
L0002550 25800000
L0002560 25900000
L0002570 26000000
L0002580 26100000
L0002590 26200000
L0002600 26300000

```

```

SUBROUTINE MODE( ALPHA, NM, NDOF, NMP, K, E, F)
DIMENSION ALPHA(3,3), B(6,6) , C(6,6), D(6,6), E(6,30), F(6,30)
COMMON /A2/A(408)
COMMON /INOUT/IO5, IO6, IOFF
EQUIVALENCE (B(1,1), A(1)), (C(1,1), A(37)), (D(1,1), A(73))
C
C READ DEFAULT T-MATRIX FOR MODULE
C
NDOF=0
CALL TDEF(KK,D)
IF(IOFF.GE.5)GO TO 201
WRITE(IO6 ,26)K, KK, (D(I,J), J=1,6), I=1, KK)
C
C CREATE DOUBLE ALPHA MATRIX
C
201 DO 10 I=1,3
DO 10 J=1,3
C(I,J)=ALPHA(I,J)
C(I+3, J+3)=C(I,J)
C(I+3, J)=0.
10 C(I, J+3)=0.
C
C READ MODE SHAPES, TRANSFORM, WRITE ON DISK
C
INDEX=1
READ(IO5,2)MPN
IF(MPN.NE.1)GO TO 50
70 CALL TDEF(KR,E)
IF(IOFF.GE.5)GO TO 202
WRITE(IO6 ,27)MPN, KR, (E(I,J), J=1,6), I=1, KR)
202 IF(INDEX.EQ.NMP)GO TO 60
READ(IO5,2)MPN
GO TO 60
50 CALL MCPY(D,E, KK,6,6)
KR=KK
60 CALL MPRD(E,C,B, KR,6,6,6,6)
DO 61 I=1, KR
61 READ(IO5,4)(E(I,J), J=1, NM)
CALL TPRD(B,E,F, KR,6, NM,6,6)
IF(IOFF.GE.5)GO TU 25
IF(INDEX.GT.1)GO TO 40
WRITE(IO6,28)
L0002610 26400000
L0002620 26500000
L0002630 26600000
L0002640 26700000
L0002650 26800000
L0002660 26900000
L0002670 27000000
L0002680 27100000
L0002690 27200000
L0002700 27300000
L0002710 27400000
L0002720 27500000
L0002730 27600000
L0002740 27700000
L0002750 27800000
L0002760 27900000
L0002770 28000000
L0002780 28100000
L0002790 28200000
L0002800 28300000
L0002810 28400000
L0002820 28500000
L0002830 28600000
L0002840 28700000
L0002850 28800000
L0002860 28900000
L0002870 29000000
L0002880 29100000
L0002890 29200000
L0002900 29300000
L0002910 29400000
L0002920 29500000
L0002930 29600000
L0002940 29700000
L0002950 29800000
L0002960 29900000
L0002970 30000000
L0002980 30100000
L0002990 30200000
L0003000 30300000
L0003010 30400000
L0003020 30500000

```

```

COUNT=0
40 WRITE(I06,29)INDEX
DO 110 I=1,KR
  KOUNT=KOUNT+1
110 WRITE(I06,30)KOUNT,(E(I,J),J=1,NM)
25 WRITE(3)((F(I,J),J=1,NM),I=1,6)
  NDOF=NDOCF+KR
  INDEX=INDEX+1
  IF(INDEX.GT.NMP)GO TO 100
  IF(MPN-INDEX)70,70,50
100 RETURN
  2 FORMAT(I2)
  4 FORMAT(8X,E15.8,9X,E15.8)
26 FORMAT(// * DEFAULT T-MATRIX FOR MODULE*,I3/I3, * ROWS, 6 COLUMNS*
  */(6E15.6))
27 FORMAT(// * T-MATRIX FOR MASS POINT*,I3/I3, * ROWS, 6 COLUMNS* / (6E15.6))
  *5.6))
28 FORMAT(// * SUBSTRUCTURE MODAL MATRIX*// * ROW NO.* )
29 FORMAT(/15X, *COORDINATES OF MASS POINT *,I3)
30 FORMAT(/3X,I3,2X,6E17.7/(3X,6E17.7))
  END
L0003030 30600000
L0003040 30700000
L0003050 30800000
L0003060 30900000
L0003070 31000000
L0003080 31100000
L0003090 31200000
L0003100 31300000
L0003110 31400000
L0003120 31500000
L0003130 31600000
L0003140 31700000
L0003150 31800000
L0003160 31900000
L0003170 32000000
L0003180 32100000
L0003190 32200000
L0003200 32300000
L0003210 32400000
L0003220 32500000
L0003230 32600000

```

```

SUBROUTINE TDEF(N,A)
DIMENSION A(6,6),K(7)
COMMON /INOUT/IO5,IO6,IOFF
READ(IO5,1)K
IF(K(1).EQ.1)GO TO 10
N=0
DO 5 I=1,6
IF(K(I+1).EQ.0)GO TO 5
N=N+1
DO 15 J=1,6
A(N,J)=0.
IF(1.EQ.J)A(N,J)=1.
15 CONTINUE
5 CONTINUE
RETURN
10 READ(IO5,2)N,((A(I,J),J=1,6),I=1,N)
RETURN
1 FORMAT(7I1)
2 FORMAT(I2/(4E15.8))
END

```

```

L0003240 32700000
L0003250 32800000
L0003260 32900000
L0003270 33000000
L0003280 33100000
L0003290 33200000
L0003300 33300000
L0003310 33400000
L0003320 33500000
L0003330 33600000
L0003340 33700000
L0003350 33800000
L0003360 33900000
L0003370 34000000
L0003380 34100000
LJ03390 34200000
L0003400 34300000
L0003410 34400000
L0003420 34500000
L0003430 34600000

```

```

SUBROUTINE FILE
COMMON /A1/MODID(17),NM(17),NMP(17)
COMMON /A2/A
COMMON /INOUT/I05,I06,I0FF,LL
DIMENSION B(10,40)
DIMENSION A(400)
EQUIVALENCE(A(1),B(1,1))
INTEGER TENL
REWIND 4
INDEX=0
DO 10 I=1,17
INDEX=INDEX+1
IF(MODID(I).EQ.0)GO TO 110
L=NMP(I)
DO 20 J=1,L
K= J*10-9
KP9=K+9
20 READ(4)(A(IJ),IJ=K,KP9)
TENL=10*L
WRITE(1)(A(J),J=1,TENL)
WRITE(11)TENL,(A(J),J=1,TENL)
IF(I0FF.GE.10)GO TO 10
WRITE(I06,11),(J,(B(M,J),M=1,10),J=1,L)
GO TO 10
110 WRITE(1)MODID
10 CONTINUE
10 RETURN
1 FORMAT(// * MASSES AND MOMENTS OF INERTIA IN GLOBAL COORDINATES FOR //
* MODULE *,I2// * MASS NO. *,7X, * MASS *,25X, * INERTIA MATRIX* //
* (3X,13,3X,E16.7,5X,3E16.7/30X,3E16.7/30X,3E16.7//)
END

```

```

L0003440 34700000
L0003450 34800000
L0003460 34900000
L0003470 35000000
L0003480 35100000
L0003490 35200000
L0003500 35300000
L0003510 35400000
L0003520 35500000
L0003530 35600000
L0003540 35700000
L0003550 35800000
L0003560 35900000
L0003570 36000000
L0003580 36100000
L0003590 36200000
L0003600 36300000
L0003610 36400000
L0003620 36500000
L0003630 36600000
L0003640 36700000
L0003650 36800000
L0003660 36900000
L0003670 37000000
L0003680 37100000
L0003690 37200000
L0003700 37300000
L0003710 37400000
L0003720 37500000
L0003740 37700000

```

```

SUBROUTINE JOINT(A, IXYZ, B, AX, BX)
  COMMGN/AL/MODID(17), NMO(17), NMP0(17)
  DIMENSION A(60,6), B(60,30), IXYZ(16), AX(6,6), BX(6,30)
  REWIND 2
  REWIND 3
  REWIND 4
  REWIND 9
  JNEW=0
  IRR=0
  DO 1 IRR=1,17
  IF(MODID(IR).EQ.0 .OR. NMO(IR).EQ.0)GO TO 1
  JOLD=JNEW+1
  IF(IR.EQ.1 .OR. IR.EQ.11 .OR. IR.EQ.14 .OR. IR.EQ.16)GO TO 70
  NMP=NMP0(IR)
  DO 80 I=1,NMP
  REAC(2)
  80 IF(NMO(IR).GT.0)READ(3)
  GO TO 1
  70 IRR=IRR+1
  IF(NMO(IR).EQ.0)RETURN
  NUMB=5-IRR
  IF(IRR.EQ.1)NUMB=10
  NMP=NMP0(IR)
  NM=NMO(IR)
  JNEW=JOLD-1+NUMB
  DO 10 I=1,NMP
  IFLAG=0
  JDEX=0
  DO 20 J=JOLD,JNEW
  JDEX=JDEX+1
  IF(I.NE.IXYZ(J))GO TO 20
  IF(IFLAG.EQ.1)GO TO 32
  IF(IR.NE.1)READ(2)((AX(L1,L2),L2=1,6),L1=1,6)
  READ(3)((BX(L1,L2),L2=1,NM),L1=1,6)
  IFLAG=1
  32 JT=(JDEX-1)*6
  DO 30 K=1,6
  IF(IR.EQ.1)GO TO 33
  DO 31 K1=1,6
  31 A(JT+K,K1)=AX(K,K1)
  33 DO 30 K2=1,NM
  30 B(JT+K,K2)=BX(K,K2)

```

```

L0003750 37800000
L0003760 37900000
L0003770 38000000
L0003780 38100000
L0003790 38200000
L0003800 38300000
L0003810 38400000
L0003820 38500000
L0003830 38600000
L0003840 38700000
L0003850 38800000
L0003860 38900000
L0003870 39000000
L0003880 39100000
L0003890 39200000
L0003900 39300000
L0003910 39400000
L0003920 39500000
L0003930 39600000
L0003940 39700000
L0003950 39800000
L0003960 39900000
L0003970 40000000
L0003980 40100000
L0003990 40200000
L0004000 40300000
L0004010 40400000
L0004020 40500000
L0004030 40600000
L0004040 40700000
L0004050 40800000
L0004060 40900000
L0004070 41000000
L0004080 41100000
L0004090 41200000
L0004100 41300000
L0004110 41400000
L0004120 41500000
L0004130 41600000
L0004140 41700000
L0004150 41800000
L0004160 41900000

```

```

20 CONTINUE
  IF (IFLAG.EQ.1) GO TO 10
  IF (IR.NE.1) READ(2)
  READ(3)
10 CONTINUE
  JDEX=0
  DO 11 J=JOLD,JNEW
    JDEX=JDEX+1
    IF (IXYZ(J).EQ.0) GO TO 11
    JT=(JDEX-1)*6
    J1=JT+1
    J2=JT+6
    IF (IR.NE.1) WRITE(4)((A(L1,L2),L2=1,6),L1=J1,J2)
    WRITE(9)NM,((B(L1,L2),L2=1,NM),L1=J1,J2)
11 CONTINUE
  1 RETURN
  END

```

L0004170	42000000
L0004180	42100000
L0004190	42200000
L0004200	42300000
L0004210	42400000
L0004220	42500000
L0004230	42600000
L0004240	42700000
L0004250	42800000
L0004260	42900000
L0004270	43000000
L0004280	43100000
L0004290	43200000
L0004300	43300000
L0004310	43400000
L0004320	43500000
L0004330	43600000
L0004340	43700000

```

SUBROUTINE FORMB(C,D,E,F,U,V,W,X,R,S,T,T1)
DIMENSION C(180,6),D(180,30),E(180,6),F(180,6),
* U(6,30),V(6,30),W(6,30),X(6,30),
* R(6,6),S(6,6),T(6,6),T1(6,6)
COMMON /AL/MODID(17),NM0(17),NMP0(17)
COMMON /INOUT/IO5,IO6,IOFF
REWIND 2
REWIND 3
REWIND 9
REWIND 4
INDEX=0
C* STEP 1 B(I,I),I=1,17
C
DO 10 I=1,17
INDEX=INDEX+1
IF(MODID(I).EQ.0 .OR. NM0(I).EQ.0)GO TO 110
NM=NM0(I)
NMP=NMP0(I)
DO 11 J=1,NMP
J6=J*6-5
J6P5=J6+5
11 READ(3)((D(J1,J2),J2=1,NM),J1=J6,J6P5)
NMP6=NMP*6
WRITE(10)NMP6,NM,((D(J1,J2),J2=1,NM),J1=1,NMP6)
GO TO 10
110 WRITE(10)MODID
10 CONTINUE
C* STEP 2 B(I,1),I=2,11
C
DO 20 I=2,11
INDEX=INDEX+1
IF(MODID(I).EQ.0 )GO TO 120
READ(9)NMI,((X(J1,J2),J2=1,NM1),J1=1,6)
IF(I.EQ.11)CALL MCPY(X,U,6,NM1,6)
NMP=NMP0(I)
CALL CXD(C,X,D,NMI,INDEX,NMP)
GO TO 20
120 WRITE(10)MODID
20 CONTINUE
C

```

```

L0004350 43800000
L0004360 43900000
L0004370 44000000
L0004380 44100000
L0004390 44200000
L0004400 44300000
L0004410 44400000
L0004420 44500000
L0004430 44600000
L0004440 44700000
L0004450 44800000
L0004460 44900000
L0004470 45000000
L0004480 45100000
L0004490 45200000
L0004500 45300000
L0004510 45400000
L0004520 45500000
L0004530 45600000
L0004540 45700000
L0004550 45800000
L0004560 45900000
L0004570 46000000
L0004580 46100000
L0004590 46200000
L0004600 46300000
L0004610 46400000
L0004620 46500000
L0004630 46600000
L0004640 46700000
L0004650 46800000
L0004660 46900000
L0004670 47000000
L0004680 47100000
L0004690 47200000
L0004700 47300000
L0004710 47400000
L0004720 47500000
L0004730 47600000
L0004740 47700000
L0004750 47800000
L0004760 47900000

```



```

C* STEP 3      B(I,11),I=12,14
C
DO 30 I=12,14
INDEX=INDEX+1
IF(MODID(I).EQ.0 .OR. NMO(11).EQ.0)GO TO 130
READ(4)((R(J1,J2),J2=1,6),J1=1,6)
READ(9)NM2,((X(J1,J2),J2=1,NM2),J1=1,6)
IF(I.EQ.14)CALL MCPY(X,V,6,NM2,6)
NMP=NMP0(I)
CALL CXD(C,X,D,NM2,INDEX,NMP)
NMP6 =NMP*6
CALL MPRD(C,R,D,NMP6,6,6,180,6)
WRITE(8)NMP6,((D(J1,J2),J2=1,6),J1=1,NMP6)
GO TO 30
130 WRITE(10)MODID
30 CONTINUE
C
C* STEP 4      B(15,14)
C
INDEX=INDEX+1
IF(MODID(15).EQ.0 .OR. NMO(14).EQ.0)GO TO 140
READ(4)((S(J1,J2),J2=1,6),J1=1,6)
CALL MPRD(S,R,T,6,6,6,6)
READ(9)NM4,((X(J1,J2),J2=1,NM),J1=1,6)
NMP=NMP0(15)
CALL CXD(C,X,D,NM ,INDEX,NMP)
NMP61=NMP*6
CALL MPRD(C,T,D,NMP61,6,6,180,6)
WRITE(8)NMP61,((D(J1,J2),J2=1,6),J1=1,NMP61)
CALL MPRD(C,S,E,NMP61,6,6,180,6)
GO TO 40
140 WRITE(10)MODID
C
C* STEP 5      B(16,14)
C
C
INDEX=INDEX+1
IF(MODID(16).EQ.0 .OR. NMO(14).EQ.0)GO TO 180
READ(4)((S(J1,J2),J2=1,6),J1=1,6)
CALL MPRD(S,R,T,6,6,6,6)
READ(9)NM3,((W(J1,J2),J2=1,NM3),J1=1,6)
NMP=NMP0(16)
CALL CXD(C,W,D,NM3,INDEX,NMP)
NMP62=NMP*6

```

```

L0004770 48000000
L0004780 48100000
L0004790 48200000
L0004800 48300000
L0004810 48400000
L0004820 48500000
L0004830 48600000
L0004840 48700000
L0004850 48800000
L0004860 48900000
L0004870 49000000
L0004880 49100000
L0004890 49200000
L0004900 49300000
L0004910 49400000
L0004920 49500000
L0004930 49600000
L0004940 49700000
L0004950 49800000
L0004960 49900000
L0004970 50000000
L0004980 50100000
L0004990 50200000
L0005000 50300000
L0005010 50400000
L0005020 50500000
L0005030 50600000
L0005040 50700000
L0005050 50800000
L0005060 50900000
L0005070 51000000
L0005080 51100000
L0005090 51200000
L0005100 51300000
L0005110 51400000
L0005120 51500000
L0005130 51600000
L0005140 51700000
L0005150 51800000
L0005160 51900000
L0005170 52000000
L0005180 52100000
L0005190 52200000

```

```

CALL MPRD(C,T,D,NMP62,6,6,180,6)
WRITE(8)NMP62,((D(J1,J2),J2=1,6),J1=1,NMP62)
CALL MPRD(C,S,F,NMP62,6,6,180,6)
GO TO 50
180 WRITE(10)MODID
C
C* STEP 6      8(I,17,16)
C
50 INDEX=INDEX+1
IF(MODID(I7).EQ.0 .OR. NMO(16).EQ.0)GO TO 360
READ(4)((T(I,J1,J2),J2=1,6),J1=1,6)
CALL MPRD(T1,T,R,6,6,6,6)
READ(9)NM,((X(J1,J2),J2=1,NM),J1=1,6)
NMF=NMP0(I7)
CALL CXD(C,X,0,NM , INDEX,NMP)
NMP6 =NMP*6
CALL MPRD(C,R,D,NMP6,6,6,180,6)
WRITE(8)NMP6 , ((D(J1,J2),J2=1,6),J1=1,NMP6)
360 IF(MODID(15).EQ.0 .OR. NMO(15).EQ.0)GO TO 361
WRITE(8)NMP61,((E(J1,J2),J2=1,6),J1=1,NMP61)
361 IF(MODID(16).EQ.0 .OR. NMO(16).EQ.0)GO TO 160
WRITE(8)NMP62,((F(J1,J2),J2=1,6),J1=1,NMP62)
IF(MODID(17).EQ.0 .OR. NMO(17).EQ.0)GO TO 160
CALL MPRD(T1,S,T,6,6,6,6)
CALL MPRD(C,T,D,NMP6,6,6,180,6)
WRITE(8)NMP6,((D(J1,J2),J2=1,6),J1=1,NMP6)
CALL MPRD(C,T1,D,NMP6,6,6,180,6)
WRITE(8)NMP6,((D(J1,J2),J2=1,6),J1=1,NMP6)
GO TO 60
160 WRITE(10)MODID
C
C* STEP 7      B(I,1),I=12,17
C
60 REWIND 8
DO 61 I=12,17
INDEX=INDEX+1
IF(MODID(I).EQ.0 )GO TO 161
CALL Q(C,U,D,NM1,INDEX)
GO TO 61
161 WRITE(10)MODID
61 CONTINUE
C
C* STEP 8      B(I,11),I=15,17

```

```

L0005200 52300000
L0005210 52400000
L0005220 52500000
L0005230 52600000
L0005240 52700000
L0005250 52800000
L0005260 52900000
L0005270 53000000
L0005280 53100000
L0005290 53200000
L0005300 53300000
L0005310 53400000
L0005320 53500000
L0005330 53600000
L0005340 53700000
L0005350 53800000
L0005360 53900000
L0005370 54000000
L0005380 54100000
L0005390 54200000
L0005400 54300000
L0005410 54400000
L0005420 54500000
L0005430 54600000
L0005440 54700000
L0005450 54800000
L0005460 54900000
L0005470 55000000
L0005480 55100000
L0005490 55200000
L0005500 55300000
L0005510 55400000
L0005520 55500000
L0005530 55600000
L0005540 55700000
L0005550 55800000
L0005560 55900000
L0005570 56000000
L0005580 56100000
L0005590 56200000
L0005600 56300000
L0005610 56400000
L0005620 56500000

```

```

C
DO 70 I=15,17
INDEX=INDEX+1
IF(MODID(I).EQ.0 .OR. NM0(11).EQ.0)GO TO 170
CALL Q(C,V,D,NM2,INDEX)
GO TO 70
170 WRITE(10)MODID
70 CONTINUE
C* STEP 9 B(17,14)
C
IF(MODID(17).EQ.0 .OR. NM0(14).EQ.0)RETURN
INDEX=INDEX+1
CALL Q(C,W,D,NM3,INDEX)
RETURN
END
L0005630 56600000
L0005640 56700000
L0005650 56800000
L0005660 56900000
L0005670 57000000
L0005680 57100000
L0005690 57200000
L0005700 57300000
L0005710 57400000
L0005720 57500000
L0005730 57600000
L0005740 57700000
L0005750 57800000
L0005760 57900000
L0005770 58000000
L0005780 58100000

```

L0005790 58200000
L0005800 58300000
L0005810 58400000
L0005820 58500000
L0005830 58600000
L0005840 58700000
L0005850 58800000

SUBROUTINE Q(A,B,C,N,M)
DIMENSION A(180,6),B(6,30),C(180,30)
READ(8)NMP6,((A(I,J),J=1,6),I=1,NMP6)
CALL MPRD(A,B,C,NMP6,6,N,180,6)
WRITE(10)NMP6,N,((C(I,J),J=1,N),I=1,NMP6)
RETURN
END

```

SUBROUTINE CXD(C,X,D,NM,INDEX,NMP)
DIMENSION C(180,6),X(6,6),D(180,30)
DO 20 J=1,NMP
J6=J*6-5
J6P5=J6+5
20 READ(2)((C(I,K),K=1,6),I=J6,J6P5)
NMP6=NMP*6
CALL MPRD(C,X,D,NMP6,6,NM,180,6)
WRITE(10)NMP6,NM,((D(I,J),J=1,NM),I=1,NMP6)
RETURN
END

```

L0005860	58900000
L0005870	59000000
L0005880	59100000
L0005890	59200000
L0005900	59300000
L0005910	59400000
L0005920	59500000
L0005930	59600000
L0005940	59700000
L0005950	59800000
L0005960	59900000

```

SUBROUTINE BTMB(D,R,S,SUM)
COMMON /A1/MODID,NM,NMPO(17)
DIMENSION D(300),R(180,30),S(180,31),SUM(30,30),MODID(17),NM(17)

C BTMB COMPUTES (B-TRANPOSE)(M)(B) LEAVING THE RESULT ON FILE 8.
C IT MUST BE RE-ORDERED BEFORE ENTERING #LATE*.
REWIND 8
REWIND 10
REWIND 1
C* (1,1)
      K=NM(11)
      CALL ZERO(SUM,K,K)
      DO 10 I=1,17
        IF(MODID(I).EQ.0)GO TO 10
        INDEX1=16+I
        IF(I.EQ.1)INDEX1=1
        IF(I.GT.11)INDEX1=INDEX1+6
        CALL RTDS(K,K,INDEX1,INDEX1,D,R,S(1,2),S,I)
        CALL ADD(SUM,S,K,K)
      10 CONTINUE
      WRITE(8)K,K,((SUM(I,J),I=1,K),J=1,K)
C* (2-10,1)
      DO 20 I=2,10
        IF(MODID(I).EQ.0 .OR. NM(I).EQ.0)GO TO 20
        INDEX1=16+I
        L=NM(I)
        CALL RTDS(L,K,INDEX1,I,D,R,S(1,2),S,I)
        WRITE(8)L,K,((S(I1,J),I1=1,L),J=1,K)
      20 CONTINUE
C* (11,1)
      L=NM(11)
      CALL ZERO(SUM,L,K)
      IF(MODID(11).EQ.0 .OR. NM(11).EQ.0)GO TO 200
      CALL RTDS(L,K,27,11,D,R,S(1,2),S,11)
      CALL ADD(SUM,S,L,K)
      DO 30 I=12,17
        IF(MODID(I).EQ.0 .OR. NM(I).EQ.0)GO TO 30
        INDEX1=22+I
        INDEX2=16+I
        IF(I.GT.14)INDEX2=INDEX2+9
        CALL RTDS(L,K,INDEX1,INDEX2,D,R,S(1,2),S,I)
        CALL ADD(SUM,S,L,K)

```

```

L0005970 60000000
L0005980 60100000
L0005990 60200000
L0006000 60300000
L0006010 60400000
L0006020 60500000
L0006030 60600000
L0006040 60700000
L0006050 60800000
L0006060 60900000
L0006070 61000000
L0006080 61100000
L0006090 61200000
L0006100 61300000
L0006110 61400000
L0006120 61500000
L0006130 61600000
L0006140 61700000
L0006150 61800000
L0006160 61900000
L0006170 62000000
L0006180 62100000
L0006190 62200000
L0006200 62300000
L0006210 62400000
L0006220 62500000
L0006230 62600000
L0006240 62700000
L0006250 62800000
L0006260 62900000
L0006270 63000000
L0006280 63100000
L0006290 63200000
L0006300 63300000
L0006310 63400000
L0006320 63500000
L0006330 63600000
L0006340 63700000
L0006350 63800000
L0006360 63900000
L0006370 64000000
L0006380 64100000

```

```

30 CONTINUE
WRITE(8)L,K,((SUM(I,J),I=1,L),J=1,K)
C* (11,11)
CALL ZERO(SUM,L,L)
CALL RTDS(L,L,11,11,D,R,S(1,2),S,11)
CALL ADD(SUM,S,L,L)
DO 35 I=12,17
IF(MODI(I).EQ.0 .OR. NM(I).EQ.0)GO TO 35
INDEX2=16+I
IF(I.GT.14)INDEX2=INDEX2+9
CALL RTDS(L,L,INDEX2,INDEX2,D,R,S(1,2),S,I)
CALL ADD(SUM,S,L,L)
35 CONTINUE
WRITE(8)L,L,((SUM(I,J),I=1,L),J=1,L)
M=NM(11)
IF(MODI(12).EQ.0 .OR. NM(12).EQ.0)GO TO 41
L=NM(12)
CALL RTDS(L,K,34,12,D,R,S(1,2),S,12)
WRITE(8)L,K,((S(I,J),I=1,L),J=1,K)
C* (12,11)
CALL RTDS(L,M,28,12,D,R,S(1,2),S,12)
WRITE(8)L,M,((S(I,J),I=1,L),J=1,M)
C* (13,1)
41 IF(MODI(13).EQ.0 .OR. NM(13).EQ.0)GO TO 42
L=NM(13)
CALL RTDS(L,K,35,13,D,R,S(1,2),S,13)
WRITE(8)L,K,((S(I,J),I=1,L),J=1,K)
C* (13,11)
CALL RTDS(L,M,29,13,D,R,S(1,2),S,13)
WRITE(8)L,M,((S(I,J),I=1,L),J=1,M)
C* (14,1)
42 IF(MODI(14).EQ.0 .OR. NM(14).EQ.0)GO TO 200
L=NM(14)
CALL ZERO(SUM,L,K)
CALL RTDS(L,K,36,14,D,R,S(1,2),S,14)
CALL ADD(SUM,S,L,K)
DO 45 I=15,17
IF(MODI(I).EQ.0 .OR. NM(I).EQ.0)GO TO 45
INDEX1=22+I
INDEX2=16+I
IF(I.EQ.17)INDEX2=INDEX2+10
CALL RTDS(L,K,INDEX1,INDEX2,D,R,S(1,2),S,I)

```

```

L0006380 64200000
L0006390 64300000
L0006400 54400000
L0006410 64500000
L0006420 54600000
L0006430 64700000
L0006440 64800000
L0006450 64900000
L0006460 65000000
L0006470 65100000
L0006480 65200000
L0006490 65300000
L0006500 65400000
L0006510 65500000
L0006520 65600000
L0006530 65700000
L0006540 65800000
L0006550 65900000
L0006560 66000000
L0006570 66100000
L0006580 66200000
L0006590 66300000
L0006600 66400000
L0006610 66500000
L0006620 66600000
L0006630 66700000
L0006640 66800000
L0006650 66900000
L0006660 67000000
L0006670 67100000
L0006680 67200000
L0006690 67300000
L0006700 67400000
L0006710 67500000
L0006720 67600000
L0006730 67700000
L0006740 67800000
L0006750 67900000
L0006760 68000000
L0006770 68100000
L0006780 68200000
L0006790 68300000
L0006800 68400000

```

```

CALL ADD(SUM,S,L,K)
45 CONTINUE
WRITE(8)L,K,((SUM(I,J),I=1,L),J=1,K)
C* (14,11)
CALL ZERO(SUM,L,M)
CALL RTDS(L,M,30,14,D,R,S(1,2),S,14)
CALL ADD(SUM,S,L,M)
DO 48 I=15,17
IF(MODID(I).EQ.0 .OR. NM(I).EQ.0)GO TO 48
INDEX1=25+I
INDEX2=16+I
IF(I.EQ.17)INDEX2=43
CALL RTDS(L,M,INDEX1,INDEX2,D,R,S(1,2),S,I)
CALL ADD(SUM,S,L,M)
48 CONTINUE
WRITE(8)L,M,((SUM(I,J),I=1,L),J=1,M)
C* (14,14)
CALL ZERO(SUM,L,L)
DO 49 I=14,17
INDEX1=16+I
IF(MODID(I).EQ.0 .OR. NM(I).EQ.0)GO TO 49
IF(I.EQ.14)INDEX1=14
IF(I.EQ.17)INDEX1=43
CALL RTDS(L,L,INDEX1,INDEX1,D,R,S(1,2),S,I)
CALL ADD(SUM,S,L,L)
49 CONTINUE
WRITE(8)L,L,((SUM(I,J),I=1,L),J=1,L)
C* (15,1)
N=NM(14)
50 IF(MODID(15).EQ.0 .OR. NM(15).EQ.0)GO TO 60
L=NM(15)
CALL RTDS(L,K,37,15,D,R,S(1,2),S,15)
WRITE(8)L,K,((S(I,J),I=1,L),J=1,K)
C* (15,11)
CALL RTDS(L,M,40,15,D,R,S(1,2),S,15)
WRITE(8)L,M,((S(I,J),I=1,L),J=1,M)
C* (15,14)
CALL RTDS(L,N,31,15,D,R,S(1,2),S,15)
WRITE(8)L,N,((S(I,J),I=1,L),J=1,N)
C* (16,1)
60 IF(MODID(16).EQ.0 .OR. NM(16).EQ.0)GO TO 200
L=NM(16)
CALL ZERO(SUM,L,K)
L0006810 68500000
L0005820 68600000
L0006830 68700000
L0006840 68800000
L0006850 68900000
L0006860 69000000
L0006870 69100000
L0006880 69200000
L0006890 69300000
L0006900 69400000
L0006910 69500000
L0006920 69600000
L0006930 69700000
L0006940 69800000
L0006950 69900000
L0006960 70000000
L0006970 70100000
L0006980 70200000
L0006990 70300000
L0007000 70400000
L0007010 70500000
L0007020 70600000
L0007030 70700000
L0007040 70800000
L0007050 70900000
L0007060 71000000
L0007070 71100000
L0007080 71200000
L0007090 71300000
L0007100 71400000
L0007110 71500000
L0007120 71600000
L0007130 71700000
L0007140 71800000
L0007150 71900000
L0007160 72000000
L0007170 72100000
L0007180 72200000
L0007190 72300000
L0007200 72400000
L0007210 72500000
L0007220 72600000
L0007230 72700000

```



```

CALL RTDS(L,K,38,16,D,R,S(1,2),S,16)
CALL ADD(SUM,S,L,K)
IF(MODID(17).EQ.0 .OR. NM(17).EQ.0)GO TO 62
CALL RTDS(L,K,39,33,D,R,S(1,2),S,17)
CALL ADD(SUM,S,L,K)
62 WRITE(8)L,K,((SUM(I,J),I=1,L),J=1,K)
C* (16,11)
CALL ZERO(SUM,L,M)
CALL RTDS(L,M,41,16,D,R,S(1,2),S,16)
CALL ADD(SUM,S,L,M)
IF(MODID(17).EQ.0 .OR. NM(17).EQ.0)GO TO 64
CALL RTDS(L,M,42,33,D,R,S(1,2),S,17)
CALL ADD(SUM,S,L,M)
64 WRITE(8)L,M,((SUM(I,J),I=1,L),J=1,M)
C* (16,14)
CALL ZERO(SUM,L,N)
CALL RTDS(L,N,32,16,D,R,S(1,2),S,16)
CALL ADD(SUM,S,L,N)
IF(MODID(17).EQ.0 .OR. NM(17).EQ.0)GO TO 66
CALL RTDS(L,N,43,33,D,R,S(1,2),S,17)
CALL ADD(SUM,S,L,N)
66 WRITE(8)L,N,((SUM(I,J),I=1,L),J=1,N)
C* (16,16)
CALL ZERO(SUM,L,L)
CALL RTDS(L,L,16,16,D,R,S(1,2),S,16)
CALL ADD(SUM,S,L,L)
IF(MODID(17).EQ.0 .OR. NM(17).EQ.0)GO TO 68
CALL RTDS(L,L,33,33,D,R,S(1,2),S,17)
CALL ADD(SUM,S,L,L)
68 WRITE(8)L,L,((SUM(I,J),I=1,L),J=1,L)
C* (17,1)
IF(MODID(17).EQ.0 .OR. NM(17).EQ.0)GO TO 200
L=NM(17)
CALL RTDS(L,K,39,17,D,R,S(1,2),S,17)
WRITE(8)L,K,((S(I,J),I=1,L),J=1,K)
C* (17,11)
CALL RTDS(L,M,42,17,D,R,S(1,2),S,17)
WRITE(8)L,M,((S(I,J),I=1,L),J=1,M)
C* (17,14)
CALL RTDS(L,N,43,17,D,R,S(1,2),S,17)
WRITE(8)L,N,((S(I,J),I=1,L),J=1,N)
C* (17,16)
M=NM(16)
L0007240 72800000
L0007250 72900000
L0007260 73000000
L0007270 73100000
L0007280 73200000
L0007290 73300000
L0007300 73400000
L0007310 73500000
L0007320 73600000
L0007330 73700000
L0007340 73800000
L0007350 73900000
L0007360 74000000
L0007370 74100000
L0007380 74200000
L0007390 74300000
L0007400 74400000
L0007410 74500000
L0007420 74600000
L0007430 74700000
L0007440 74800000
L0007450 74900000
L0007460 75000000
L0007470 75100000
L0007480 75200000
L0007490 75300000
L0007500 75400000
L0007510 75500000
L0007520 75600000
L0007530 75700000
L0007540 75800000
L0007550 75900000
L0007560 76000000
L0007570 76100000
L0007580 76200000
L0007590 76300000
L0007600 76400000
L0007610 76500000
L0007620 76600000
L0007630 76700000
L0007640 76800000
L0007650 76900000
L0007660 77000000

```

CALL RTDS(L,M,33,17,D,R,S(1,2),S,17)
WRITE(8)L,M,((S(I,J),I=1,L),J=1,M)
200 RETURN
END

L0007670 77100000
L0007680 77200000
L0007690 77300000
L0007700 77400000

```
SUBROUTINE ZERO(SUM,N,M)
DIMENSION SUM(30,30)
DO 10 I=1,N
  DO 10 J=1,M
    10 SUM(I,J)=0.
  RETURN
END
```

```
L0007710 77500000
L0007720 77600000
L0007730 77700000
L0007740 77800000
L0007750 77900000
L0007760 78000000
L0007770 78100000
```

```

SUBROUTINE RTDS(NM2,NM1,INDEX1,INDEX2,D,R,S,RPREV,INDEX)
DIMENSION D(300),A(3,30),R(180,30),S(180,30),RPREV(180,31)
CALL LOC810(INDEX2)
READ(10)NMP6,NM2,((S(I,J),J=1,NM2),I=1,NMP6)
NMF=NMP6/6
NMP10=NMP*10
CALL LOC811(INDEX)
READ(1)(U(I),I=1,NMP10)
DO 10 I1=1,NMP
I4=10*I1-9
I7=(I1-1)*6+1
I8=I7+2
DO 20 I5=I7,I8
DO 20 I3=1,NM2
20 R(I5,I3)=S(I5,I3)*D(I4)
I6=I8+1
CALL MPRD(I4+1),S(I6,1),A,3,3,NM2,3,180)
DO 10 LMN=1,3
IND=I6+LMN-1
DO 10 LNM=1,NM2
R(IND,LNM)=A(LMN,LNM)
CALL LOC810(INDEX1)
READ(10)NMP6,NM1,((S(I,J),J=1,NM1),I=1,NMP6)
DO 40 I=1,NM1
DO 40 J=1,NM2
RPREV(J,I)=0.
DO 40 K=1,NMP6
40 RPREV(J,I)=RPREV(J,I)+S(K,I)*R(K,J)
RETURN
END

```

```

L0007780 78200000
L0007790 78300000
L0007800 78400000
L0007810 78500000
L0007820 78600000
L0007830 78700000
L0007840 78800000
L0007850 78900000
L0007860 79000000
L0007870 79100000
L0007880 79200000
L0007890 79300000
L0007900 79400000
L0007910 79500000
L0007920 79600000
L0007930 79700000
L0007940 79800000
L0007950 79900000
L0007960 80000000
L0007970 80100000
L0007980 80200000
L0007990 80300000
L0008000 80400000
L0008010 80500000
L0008020 80600000
L0008030 80700000
L0008040 80800000
L0008050 80900000
L0008060 81000000
L0008070 81100000

```

```

SUBROUTINE MXI(A,B,NMTS,D,NIX,NZERO)
DIMENSION A(100,1),B(1),MODID(17),NM(17),D(30,20),NMP0(17)
COMMON /A1/MC0ID,NM,NMPO
COMMON/INOUT/IO5,IO6,IOFF

C READ IN DIAGONAL MATRIX OF MODAL MASS FOLLOWED BY
C DIAGONAL MATRIX OF EIGENVALUES
C
REWIND 8
DO 4 I=1,NMTS
DO 4 J=1,NMTS
4 A(I,J)=0.
INMST=1
DO 60 I=1,17
INM=NM(I)
IF(INM.EQ.0)GO TO 60
INMF=INMST+INM-1
READ(IO5,1)(A(J,J),J=INMST,INMF)
INMST=INMF+1
60 CONTINUE
201 INM=NM(I)
READ(IO5,1)C,(A(I-1,I),I=2,INM)
INMST=INM+1
DO 80 I=2,17
INM=NM(I)
IF(INM.EQ.0)GO TO 80
INMF=INMST+INM-1
READ(IO5,1)(A(J-1,J),J=INMST,INMF)
INMST=INMF+1
80 CONTINUE
IF(IOFF.GE.20)GO TO 202
I=1
INM=NM(I)
IF(INM.EQ.0)GO TO 75
WRITE(IO6,71)I, I,A(1,1),C
IF(INM.LT.2)GO TO 75
WRITE(IO6,72) (J,A(J,J),A(J-1,J),J=2,INM)
INMST=INM+1
75 DO 70 I=2,17
INM=NM(I)
IF(INM.EQ.0)GO TO 70
INMF=INMST+INM-1

```

```

L0008080 81200000
L0008090 81300000
L0008100 81400000
L0008110 81500000
L0008120 81600000
L0008130 81700000
L0008140 81800000
L0008150 81900000
L0008160 82000000
L0008170 82100000
L0008180 82200000
L0008190 82300000
L0008200 82400000
L0008210 82500000
L0008220 82600000
L0008230 82700000
L0008240 82800000
L0008250 82900000
L0008260 83000000
L0008270 83100000
L0008280 83200000
L0008290 83300000
L0008300 83400000
L0008310 83500000
L0008320 83600000
L0008330 83700000
L0008340 83800000
L0008350 83900000
L0008360 84000000
L0008370 84100000
L0008380 84200000
L0008390 84300000
L0008400 84400000
L0008410 84500000
L0008420 84600000
L0008430 84700000
L0008440 84800000
L0008450 84900000
L0008460 85000000
L0008470 85100000
L0008480 85200000
L0008490 85300000

```

```

WRITE(I06,73) I,(J,A(J,J),A(J-1,J),J=INMST,INMF)
INMST=INMF+1
70 CONTINUE
202 C=A(I,1)*C
    DO 10 I=2,NMST
10 A(I,1)=A(I,1)*A(I-1,I)
203 KSUM=0
    L=NM(I)
    CALL DIAG(A,D,L,KSUM,NMST)
    DO 12 I=2,11
    IF(MODID(I).EQ.0 .OR. NM(I).EQ.0)GO TO 12
    L=NM(I)
    CALL OFF(A,L,KSUM,NM(I),0,NMST)
    KSUM=KSUM+L
12 CONTINUE
    IF(MODID(11).EQ.0 .OR. NM(11).EQ.0)GO TO 200
    KSUM=KSUM-L
    KSUM11=KSUM
    CALL DIAG(A,D,L,KSUM,NMST)
    DO 20 I=12,14
    IF(MODID(I).EQ.0 .OR. NM(I).EQ.0)GO TO 20
    L=NM(I)
    CALL OFF(A,L,KSUM,NM(I),0,NMST)
    CALL OFF(A,L,KSUM,NM(11),KSUM11,NMST)
    KSUM=KSUM+L
20 CONTINUE
    IF(MODID(14).EQ.0 .OR. NM(14).EQ.0)GO TO 200
    KSUM14=KSUM-L
    KSUM=KSUM14
    CALL DIAG(A,D,L,KSUM,NMST)
    DO 30 I=15,16
    IF(MODID(I).EQ.0 .OR. NM(I).EQ.0)GO TO 30
    L=NM(I)
    CALL OFF(A,L,KSUM,NM(I),0,NMST)
    CALL OFF(A,L,KSUM,NM(11),KSUM11,NMST)
    CALL OFF(A,L,KSUM,NM(14),KSUM14,NMST)
    IF(I.EQ.15)KSUM=KSUM+L
30 CONTINUE
    IF(MODID(16).EQ.0 .OR. NM(16).EQ.0)GO TO 200
    KSUM16=KSUM
    CALL DIAG(A,D,L,KSUM,NMST)
    IF(MODID(17).EQ.0 .OR. NM(17).EQ.0)GO TO 200
    L=NM(17)

```

```

L0008500 854000000
L0008510 855000000
L0008520 856000000
L0008530 857000000
L0008540 858000000
L0008550 859000000
L0008560 860000000
L0008570 861000000
L0008580 862000000
L0008590 863000000
L0008600 864000000
L0008610 865000000
L0008620 866000000
L0008630 867000000
L0008640 868000000
L0008650 869000000
L0008660 870000000
L0008670 871000000
L0008680 872000000
L0008690 873000000
L0008700 874000000
L0008710 875000000
L0008720 876000000
L0008730 877000000
L0008740 878000000
L0008750 879000000
L0008760 880000000
L0008770 881000000
L0008780 882000000
L0008790 883000000
L0008800 884000000
L0008810 885000000
L0008820 886000000
L0008830 887000000
L0008840 888000000
L0008850 889000000
L0008860 890000000
L0008870 891000000
L0008880 892000000
L0008890 893000000
L0008900 894000000
L0008910 895000000
L0008920 896000000

```

```

CALL OFF(A,L,KSUM,NM(1),0,NMTS)
CALL OFF(A,L,KSUM,NM(11),KSUM11,NMTS)
CALL OFF(A,L,KSUM,NM(14),KSUM14,NMTS)
CALL OFF(A,L,KSUM,NM(16),KSUM16,NMTS)
200 NIX=0
READ(IU5,52)NZERO
IF(NZERO.EQ.0)GO TO 987
CALL CHEAP(A,NMTS,NZERO,C,D,NIX)
IF(NIX.LT.0)RETURN
987 REWIND 9
WRITE(9)((A(I,J),J=1,I),I=1,NMTS)
204 A(1,1)=C
L=1
DO 50 I=2,NMTS
L=L+1
K=(I*(I+1))/2
KM=K-1
DO 7 J=L,KM
7 B(J)=0.
B(K)=A(1,I)
50 L=K
RETURN
1 FORMAT(3(8X,E15.8,1X))
71 FORMAT(//# MODULE FREQ NO. MODAL MASS EIGENVALUE*/33X,
* #FREQUENCY SQUARED*/33X,I2,6X,I3,3X,2E16.7)
72 FORMAT(11X,I3,3X,2E16.7)
73 FORMAT(/ 15,6X,I3,3X,2E16.7/(11X,I3,3X,2E16.7))
52 FORMAT(11)
END
L0008930 89700000
L0008940 89800000
L0008950 89900000
L0008960 90000000
L0008970 90100000
L0008980 90200000
L0008990 90300000
L0009000 90400000
MXI00010 90500000
MXI00020 90600000
MXI00030 90700000
MXI00040 90800000
MXI00050 90900000
MXI00060 91000000
MXI00070 91100000
MXI00080 91200000
MXI00090 91300000
MXI00100 91400000
MXI00110 91500000
MXI00120 91600000
MXI00130 91700000
MXI00140 91800000
MXI00150 91900000
MXI00160 92000000
MXI00170 92100000
92200000
92300000
MXI00200 92400000
MXI00210 92500000

```

```

MXI00220 92600000
MXI00230 92700000
MXI00240 92800000
MXI00250 92900000
MXI00260 93000000
MXI00270 93100000
MXI00280 93200000
MXI00290 93300000
MXI00300 93400000
MXI00310 93500000
MXI00320 93600000

```

```

SUBROUTINE DIAG(A,D,N,M,NMITS)
DIMENSION A(100,1),D(30,1)
READ(B),N,((D(I,J),I=1,N),J=1,N)
DO 10 I=1,N
D0 10 J=1,I
I1=M+1
I2=M+J
10 A(I1,I2)=D(I,J)
M=M+N
RETURN
END

```



```

SUBROUTINE OFF(A,L,LSUM,M,MSUM,NMTS)
DIMENSION A(100,1)
LK=L+LSUM
MK=M+MSUM
LSUMPI=LSUM+1
MSUMPI=MSUM+1
READ(8)L,M,((A(I,J),I=LSUMPI,LK),J=MSUMPI,MK)
RETURN
END
MXI00330 93700000
MXI00340 93800000
MXI00350 93900000
MXI00360 94000000
MXI00370 94100000
MXI00380 94200000
MXI00390 94300000
MXI00400 94400000
MXI00410 94500000
```

```

SUBROUTINE CHEAP(A,NMTS,NZERO,NZERO,C,DEQ,NIX)
DIMENSION A(100,1),DEQ(400)
COMMON/INPUT/IO5,IO6,IOFF
IJ=0
DO 53 J=1,NZERO
DO 53 J=1,I
IJ=IJ+1
53 DEQ(IJ)=A(I,J)
IF(NZERO-1)9,2,3
9 NIX=-8
GO TO 4
2 DEQ(1)=1./DEQ(1)
GO TO 54
3 CALL INCH(DEQ,NZERO,DEQ(50),NIX)
IF(NIX.EQ.0)GO TO 54
4 WRITE(IO5,1)NIX
RETURN
54 NMTS1=NMTS-NZERO
DEQ(101)=C
DO 56 I=2,NMTS
56 DEQ(I+100)=A(I,I)
IJ=0
DO 57 I=1,NZERO
DO 57 J=1,I
IJ=IJ+1
A(I,J)=DEQ(IJ)
A(J,I)=A(I,J)
57 CONTINUE
NZER1=NZERO+1
DO 58 I=NZER1,NMTS
DO 58 J=1,NZERO
A(J,I)=0.
DO 58 K=1,NZERO
58 A(J,I)=A(J,I)+A(J,K)*A(I,K)
DO 61 I=NZER1,NMTS
61 DEQ(I)=A(I,I)
DO 59 J=NZER1,NMTS
DO 59 I=J,NMTS
A(J,I)=0.
DO 59 K=1,NZERO
59 A(J,I)=A(J,I)+A(J,K)*A(K,I)
DO 62 I=1,NMTS1

```

```

MXI00420 94600000
MXI00430 94700000
MXI00440 94800000
MXI00450 94900000
MXI00460 95000000
MXI00470 95100000
MXI00480 95200000
MXI00490 95300000
MXI00500 95400000
MXI00510 95500000
MXI00520 95600000
MXI00530 95700000
MXI00540 95800000
MXI00550 95900000
MXI00560 96000000
MXI00570 96100000
MXI00580 96200000
MXI00590 96300000
MXI00600 96400000
MXI00610 96500000
MXI00620 96600000
MXI00630 96700000
MXI00640 96800000
MXI00650 96900000
MXI00660 97000000
MXI00670 97100000
MXI00680 97200000
MXI00690 97300000
MXI00700 97400000
MXI00710 97500000
MXI00720 97600000
MXI00730 97700000
MXI00740 97800000
MXI00750 97900000
MXI00760 98000000
MXI00770 98100000
MXI00780 98200000
MXI00790 98300000
MXI00800 98400000
MXI00810 98500000
MXI00820 98600000
MXI00830 98700000

```

```

62 A(I,I)=DEQ(I+NZERO)-A(I+NZERO,I+NZERO)
   DO 63 I=2,NMTS1
     IM1=I-1
     DO 63 J=1,IM1
       A(I,J)=A(I+NZERO,J+NZERO)-A(J+NZERO,I+NZERO)
     REWIND 2
     WRITE(2)NZERO,((A(I,J),I=1,NZERO),J=NZERL,NMTS)
     C=DEQ(101+NZERO)
     DO 64 I=NZERL,NMTS
       INZ=I-NZERO +1
       IJ=I+101
       A(I,INZ)=DEQ(IJ)
     NMTS=NMTS1
     RETURN
   I FORMAT(/* INVERSION FAILED*/* NIX = *,I2)
   END
MXI00840 98800000
MXI00850 98900000
MXI00860 99000000
MXI00870 99100000
MXI00880 99200000
MXI00890 99300000
MXI00900 99400000
MXI00910 99500000
MXI00920 99600000
MXI00930 99700000
MXI00940 99800000
MXI00950 99900000
MXI00960 10000000
MXI00970 10010000
MXI00980 10020000
MXI00990 10030000

```

```

SUBROUTINE LATE (N,A,NUMEIG,TOL,Q,NIX,B,NUMVAL)
C
C SOLVE THE EIGENVALUE PROBLEM:
C (A)IX)=(LAMBDA)(B)(X)
C WHERE A IS THE NXN MASS MATRIX
C AND B IS THE NXN STIFFNESS MATRIX
C
C THE STIFFNESS MATRIX IS PASSED VIA THE CALLING SEQUENCE
C THE MASS MATRIX IS STORED ON DISK FILE NO. 9
C
C DIMENSION A(1),Q(1),B(1)
C COMMON /WINTER/INDIC8
C COMMON /BUND/M,L
C COMMON /INOUT/IO5,IO6,IOFFC
REWIND 3
REWIND 9
INDIC8=-1
M=N
L=1
INDEX=(N*N)/2+1
INDEX1=INDEX-1
6 NIX=0
C
C FORM CHOLESKY DECOMPOSITION OF B MATRIX
C
C CALL FUTIL(A,N,NIX)
IF(NIX)2,3,3
2 WRITE(IO6,41)
RETURN
C
C WRITE OUT L-MATRIX TO DISK FILE NO. 3
C
3 IOFF=1
DO 1 I=1,N
J2=IOFF+I-1
WRITE(3)(A(J),J=IOFF,J2)
1 IOFF=IOFF+I
REWIND 3
C
C READ IN A-MATRIX
C
READ(9)(A(I),I=1,INDEX1)

```

```

MXI01000 1004000000
MXI01010 1005000000
MXI01020 1006000000
MXI01030 1007000000
MXI01040 1008000000
MXI01050 1009000000
MXI01060 1010000000
MXI01070 1011000000
MXI01080 1012000000
MXI01090 1013000000
MXI01100 1014000000
MXI01110 1015000000
MXI01120 1016000000
MXI01130 1017000000
MXI01140 1018000000
MXI01150 1019000000
MXI01160 1020000000
MXI01170 1021000000
MXI01180 1022000000
MXI01190 1023000000
MXI01200 1024000000
MXI01210 1025000000
MXI01220 1026000000
MXI01230 1027000000
MXI01240 1028000000
MXI01250 1029000000
MXI01260 1030000000
MXI01270 1031000000
MXI01280 1032000000
MXI01290 1033000000
MXI01300 1034000000
MXI01310 1035000000
MXI01320 1036000000
MXI01330 1037000000
MXI01340 1038000000
MXI01350 1039000000
MXI01360 1040000000
MXI01370 1041000000
MXI01380 1042000000
MXI01390 1043000000
MXI01400 1044000000
MXI01410 1045000000

```

```

C          REWIND 9
C          FORM A-MATRIX COLUMN INVERSES - STORE IN Q
C
C      7 DO 10 I=1,N
C        READ(3)(Q(J),J=1,I)
C        X=-Q(I)
C        Q(I)=-1.
C        DO 20 J=1,I
C          Q(J)=Q(J)/X
C      10 CALL DAGGER(A,N,Q,I,A(INDEX))
C
C      STORE (L)(A)(L-TRANPOSE) IN A FORM SUITABLE FOR SYMEIG
C      *WHERE L IS THE INVERSE OF THE CHOLESKY MATRIX
C
C      CALL SWITCH(A,N)
C      CALL SYMEIG(A,N,L,NUMVAL,Q,TOL,A(INDEX),I,I,N)
C      DO 58 I=1,NUMVAL
C        B(I)=SQRT(1./ABS(Q(I)))
C        IF(IOFFC.GE.25)GO TO 201
C        WRITE(IO6,56)(B(I),I=1,NUMVAL)
C
C      EIGENVALUES ARE IN Q
C
C      201 DO 30 I=1,NUMEIG
C        CALL SYMVEC(A,N,L,NUMVAL,Q,TOL,A(INDEX),I,I,N)
C        IN=INDEX1+IN
C      30 WRITE(9)(A(IND),IND=INDEX,IN)
C        REWIND 9
C        NAP=0
C        DO 27 I=1,NUMEIG
C          J1=NAP+1
C          J2=NAP+N
C        READ(9)(A(IND),IND=J1,J2)
C      27 NAP=NAP+N
C        CALL ORTHON(A,N,N,NUMEIG)
C        REWIND 9
C        NAP=0
C        DO 28 I=1,NUMEIG
C          J1=NAP+1
C          J2=NAP+N
C        WRITE(9)(A(IND),IND=J1,J2)
C      28 NAP=NAP+N

```

```

MXI01420 104600000
MXI01430 104700000
MXI01440 104800000
MXI01450 104900000
MXI01460 105000000
MXI01470 105100000
MXI01480 105200000
MXI01490 105300000
MXI01500 105400000
MXI01510 105500000
MXI01520 105600000
MXI01530 105700000
MXI01540 105800000
MXI01550 105900000
MXI01560 106000000
MXI01570 106100000
MXI01580 106200000
MXI01590 106300000
MXI01600 106400000
MXI01610 106500000
MXI01620 106600000
MXI01630 106700000
MXI01640 106800000
MXI01650 106900000
MXI01660 107000000
MXI01670 107100000
MXI01680 107200000
MXI01690 107300000
MXI01700 107400000
MXI01710 107500000
MXI01720 107600000
MXI01730 107700000
MXI01740 107800000
MXI01750 107900000
MXI01760 108000000
MXI01770 108100000
MXI01780 108200000
MXI01790 108300000
MXI01800 108400000
MXI01810 108500000
MXI01820 108600000
MXI01840 108800000

```

```

REWIND 9
REWIND 3
IOFF=1
DO 40 I=1,N
J2=IOFF+I-1
READ(3)(A(J),J=IOFF,J2)
40 IOFF=IOFF+1
REWIND 3
DO 50 I=1,NJMEIG
READ(9)(Q(J),J=1,N)
CALL TRIEQ(A,Q)
50 WRITE(3)(Q(J),J=1,N)
RETURN
41 FORMAT(50HREDUCED STIFFNESS MATRIX IS NOT POSITIVE DEFINITE )
56 FORMAT(//# CIRCULAR FREQUENCIES OF THE COUPLED SYSTEM#/(6E14.6)
END
MXI01850 108900000
MXI01860 109000000
MXI01870 109100000
MXI01880 109200000
MXI01890 109300000
MXI01900 109400000
MXI01910 109500000
MXI01920 109600000
MXI01930 109700000
MXI01940 109800000
MXI01950 109900000
MXI01960 110000000
MXI01970 110100000
MXI01990 110200000
MXI01990 110300000
MXI02000 110400000

```

```

SUBROUTINE ORTHON(Y,L,N,K)
DIMENSION Y(L,1)
DOUBLE PRECISION DSUM,DSOM,DSAM
DO 1 I=1,K
IF(I.EQ.1) GO TO 2
DO 3 J=I,K
DSCM =0.00
DO 5 II=1,N
DSUM=Y(II,J)
DSAM=Y(II,I)
DSOM=Y(II,I-1)
5 DSCM=DSCM+DSUM*DSAM
DO 6 II=1,N
6 Y(II,J)=Y(II,J)-DSOM*Y(II,I-1)
3 CONTINUE
2 DSUM=0.00
DO 7 II=1,N
DSAM=Y(II,I)
7 DSUM=DSUM+DSAM*DSAM
DSOM=DSQRT(DSUM)
DO 8 II=1,N
8 Y(II,I)=Y(II,I)/DSUM
1 CONTINUE
RETURN
END
MXI02010 110500000
MXI02020 110600000
MXI02030 110700000
MXI02040 110800000
MXI02050 110900000
MXI02060 111000000
MXI02070 111100000
MXI02080 111200000
MXI02090 111300000
MXI02100 111400000
MXI02110 111500000
MXI02120 111600000
MXI02130 111700000
MXI02140 111800000
MXI02150 111900000
MXI02160 112000000
MXI02170 112100000
MXI02180 112200000
MXI02190 112300000
MXI02200 112400000
MXI02210 112500000
MXI02220 112600000
MXI02230 112700000
MXI02240 112800000

```

```

SUBROUTINE FREE(A,N,NZERO,NUMEIG,B)
DIMENSION A(NZERO,1),B(1)
NZEP1=NZERO+1
NMTS=N+NZERO
REWIND 2
REWIND 8
READ(2)NZERO,((A(I,J),I=1,NZERO),J=1,N)
REWIND 3
DO 10 II=1,NUMEIG
READ(3)(H(I),I=NZER1,NMTS)
CALL MPAD(A,B(NZER1),B,NZERO,N,1,NZERO,1)
DO 20 I=1,NZERO
20 B(I)=-B(I)
10 WRITE(8)(B(I),I=1,NMTS)
N=NMTS
RETURN
END

```

```

MXI02250 112900000
MXI02260 113000000
MXI02270 113100000
MXI02280 113200000
MXI02290 113300000
MXI02300 113400000
MXI02310 113500000
MXI02320 113600000
MXI02330 113700000
MXI02340 113800000
MXI02350 113900000
MXI02360 114000000
MXI02370 114100000
MXI02380 114200000
MXI02390 114300000
MXI02400 114400000
MXI02410 114500000

```



```

SUBROUTINE EIGOUT(N,NZERO,NUMEIG,A,V,R,S,NTNMP,B)
COMMON /AL/MODID(17),NMO(17),NMPO(17)
COMMON /INOUT/IO5,IO6,IOFF,LL
DIMENSION A(180,30),V(100),R(600),S(600),B(1)
I38=3
IF(NZERO.GT.0)I38=8
REWIND I38
WRITE(LL)NUMEIG,B(I),I=1,NUMEIG
DO 1 I=1,NUMEIG
READ(I38)(V(I),I=1,N)
CALL LOC810(I)
READ(10)NMP6,NM,((A(I,J),J=1,NM),I=1,NMP6)
NTNMP6=NTNMP*6
DO 2 I=NMP6,NTNMP6
2 S(I)=0.
CALL MPRD(A,V,S,NMP6,NM,1,180,100)
IPOINT=1
IOLD=NMO(1)
JOLD=NMP0(1)*6
JPOINT=1
DO 10 IJ=2,17
IF(MODID(IJ).EQ.0 .OR. NMO(IJ).EQ.0)GO TO 10
IPOINT=IPOINT+IOLD
JPOINT=JPOINT+JOLD
INDEX=IJ+16
IF(IJ.GE.12)INDEX=INDEX+6
CALL LOC810(INDEX)
READ(10)NMP6,NM,((A(I,J),J=1,NM),I=1,NMP6)
CALL MPRD(A,V,R(JPOINT),NMP6,NM,1,180,100)
CALL ADD(S(JPOINT),R(JPOINT),NMP6,1)
CALL LOC810(IJ)
READ(10)NMP6,NM,((A(I,J),J=1,NM),I=1,NMP6)
CALL MPRD(A,V(IPOINT),R(JPOINT),NMP6,NM,1,180,100)
CALL ADD(S(JPOINT),R(JPOINT),NMP6,1)
IF(IJ.EQ.11)I11=IPOINT
IF(IJ.LT.12)GO TO 100
INDEX=IJ+16
IF(IJ.GT.14)INDEX=INDEX+9
CALL LOC810(INDEX)
READ(10)NMP6,NM,((A(I,J),J=1,NM),I=1,NMP6)
CALL MPRD(A,V(I11),R(JPOINT),NMP6,NM,1,180,100)
CALL ADD(S(JPOINT),R(JPOINT),NMP6,1)

```

```

MXI02420 114600000
MXI02430 114700000
MXI02440 114800000
MXI02450 114900000
MXI02460 115000000
MXI02470 115100000
MXI02480 115200000
MXI02490 115300000
MXI02500 115400000
MXI02510 115500000
MXI02520 115600000
MXI02530 115700000
MXI02540 115800000
MXI02550 115900000
MXI02560 116000000
MXI02570 116100000
MXI02580 116200000
MXI02590 116300000
MXI02600 116400000
MXI02610 116500000
MXI02620 116600000
MXI02630 116700000
MXI02640 116800000
MXI02650 116900000
MXI02660 117000000
MXI02670 117100000
MXI02680 117200000
MXI02690 117300000
MXI02700 117400000
MXI02710 117500000
MXI02720 117600000
MXI02730 117700000
MXI02740 117800000
MXI02750 117900000
MXI02760 118000000
MXI02770 118100000
MXI02780 118200000
MXI02790 118300000
MXI02800 118400000
MXI02810 118500000
MXI02820 118600000
MXI02830 118700000

```

```

IF(IJ.EQ.14)I14=IPOINT
IF(IJ.LT.15)GO TO 100
INDEX=IJ+16
IF(IJ.EQ.17)INDEX=INDEX*10
CALL LOC810(INDEX)
READ(10)NMP6,NM,((A(I,J),J=1,NM),I=1,NMP6)
CALL MPRD(A,V(I14),R(JPOINT),NMP6,NM,1,180,100)
CALL ADD(S(JPOINT),R(JPOINT),NMP6,1)
IF(IJ.EQ.16)I16=IPOINT
IF(IJ.LT.17)GO TO 100
CALL LOC810(33)
READ(10)NMP6,NM,((A(I,J),J=1,NM),I=1,NMP6)
CALL MPRD(A,V(I16),R(JPOINT),NMP6,NM,1,180,100)
CALL ADD(S(JPOINT),R(JPOINT),NMP6,1)
100 JOLD=NMP0(IJ)*6
IOLD=NMO(IJ)
10 CONTINUE
JPOINT=NTNMP*6
C
C WRITE EIGENVECTOR PHI-X
C
DO 75 IR=1,JPOINT
75 S(IR)=S(IR)*8(I1)
WRITE(LL)JPOINT,(S(I),I=1,JPOINT)
IF(IOFF.GE.30)GO TO 1
WRITE(IO6,21)I1
DO 50 I=1,JPOINT,6
IM1=I-1
IP=IM1/6+1
50 WRITE(IO6,22)IP,(S(IM1+IR),IR=1,6)
1 CONTINUE
RETURN
21 FORMAT(/ * MODE SHAPE *,I2,* OF THE COUPLED SYSTEM IN GLOBAL COORDM
*INATES NORMALIZED TO THE UNIT MODAL MASS*/
* * MASS NO. *,9X,*X(I1)*,14X,*X(2)*,14X,*X(3)*,12X,
* *THETA(1)*,10X,*THETA(2)*,10X,*THETA(3)*//
22 FORMAT(3X,13,3X,6E18.7)
END
MXI02840 118800000
MXI02850 118900000
MXI02860 119000000
MXI02870 119100000
MXI02880 119200000
MXI02890 119300000
MXI02900 119400000
MXI02910 119500000
MXI02920 119600000
MXI02930 119700000
MXI02940 119800000
MXI02950 119900000
MXI02960 120000000
MXI02970 120100000
MXI02980 120200000
MXI02990 120300000
MXI03000 120400000
MXI03010 120500000
MXI03020 120600000
MXI03030 120700000
MXI03040 120800000
MXI03050 120900000
MXI03060 121000000
MXI03070 121100000
MXI03080 121200000
MXI03090 121300000
MXI03100 121400000
MXI03110 121500000
MXI03120 121600000
MXI03130 121700000
MXI03140 121800000
MXI03150 121900000
MXI03160 122000000
MXI03170 122100000
MXI03180 122200000
MXI03190 122300000
MXI03200 122400000
MXI03210 122500000

```

MXI03220 122600000
MXI03230 122700000
MXI03240 122800000
MXI03250 122900000
MXI03260 123000000
MXI03270 123100000
MXI03280 123200000

SUBROUTINE MCPY(A,B,N,M,NDIM)
DIMENSION A(NDIM,1),B(NDIM,1)
DO 10 I=1,N
DO 10 J=1,M
10 B(I,J)=A(I,J)
RETURN
END

```
SUBROUTINE MPRD(A,B,C,N,M,K,NDIM1,NDIM2)
DIMENSION A(NDIM1,1),B(NDIM2,1),C(NDIM1,1)
DO 10 I=1,N
DO 10 J=1,K
C(I,J)=0.
DO 10 L=1,M
10 C(I,J)=C(I,J)+A(I,L)*B(L,J)
RETURN
END

MXI03290 123300000
MXI03300 123400000
MXI03310 123500000
MXI03320 123600000
MXI03330 123700000
MXI03340 123800000
MXI03350 123900000
MXI03360 124000000
MXI03370 124100000
```

```

SUBROUTINE TPRD(A,B,C,N,M,K,IDIM1,IDIM2)
DIMENSION A(IDIM1,1),B(IDIM1,1),C(IDIM2,1)
DO 10 I=1,M
DO 10 J=1,K
C(I,J)=0.
DO 10 L=1,N
10 C(I,J)=C(I,J)+A(L,I)*B(L,J)
RETURN
END

MXI03380 124200000
MXI03390 124300000
MXI03400 124400000
MXI03410 124500000
MXI03420 124600000
MXI03430 124700000
MXI03440 124800000
MXI03450 124900000
MXI03460 125000000
```

MXI03470 125100000
MXI03480 125200000
MXI03490 125300000
MXI03500 125400000
MXI03510 125500000
MXI03520 125600000
MXI03530 125700000

SUBROUTINE ADD(SUM,S,N,M)
DIMENSION S(180,31),SUM(30,30)
DO 10 I=1,N
DO 10 J=1,M
10 SUM(I,J)=SUM(I,J)+S(I,J)
RETURN
END

```

SUBROUTINE LOC810(INDNEW)
  I=INDGLD-INDNEW+1
  IF(I)1,2,3
  2 INDOLD=INDNEW
  RETURN
  1 I=-1
  DO 21 K=1,I
  21 READ(10)
  GO TO 2
  3 REWIND 10
  I=INDNEW-1
  IF(I.EQ.0)GO TO 2
  DO 22 K=1,I
  22 READ(10)
  GO TO 2
  ENTRY SET10
  INDOLD=0
  RETURN
  END

```

```

MXI03540 125800000
MXI03550 125900000
MXI03560 126000000
MXI03570 126100000
MXI03580 126200000
MXI03590 126300000
MXI03600 126400000
MXI03610 126500000
MXI03620 126600000
MXI03630 126700000
MXI03640 126800000
MXI03650 126900000
MXI03660 127000000
MXI03670 127100000
MXI03680 127200000
MXI03690 127300000
MXI03700 127400000
MXI03710 127500000
MXI03720 127600000

```

```
SUBROUTINE LOC811(INDNEW)
  I=INDCLD-INDNEW+1
  IF(I)1,2,3
  2 INDOLD=INDNEW
  RETURN
  1 I=-I
  DO 21 K=1,I
  21 READ(1)
  GO TO 2
  3 REWIND 1
  I=INDNEW-1
  IF(I.EQ.0)GO TO 2
  DO 22 K=1,I
  22 READ(1)
  GO TO 2
  ENTRY SET11
  INDOLD=0
  RETURN
  END
```

MXI03730 127700000
MXI03740 127800000
MXI03750 127900000
MXI03760 128000000
MXI03770 128100000
MXI03780 128200000
MXI03790 128300000
MXI03800 128400000
MXI03810 128500000
MXI03820 128600000
MXI03830 128700000
MXI03840 128800000
MXI03850 128900000
MXI03860 129000000
MXI03870 129100000
MXI03880 129200000
MXI03890 129300000
MXI03900 129400000
MXI03910 129500000


```
FUNCTION AND(X,Y)
LOGICAL UND,JA,NEIN
REAL NC
EQUIVALENCE(UND,E),(JA,SI),(NEIN,NO)
IFLAG=0
GO TO 1
ENTRY OR
IFLAG=1
1 SI=X
NO=Y
UND=JA.AND.NEIN
IF(IFLAG.EQ.1)UND=JA.OR.NEIN
AND=E
IF(IFLAG.EQ.1)OP=E
RETURN
END
```

```
MXI03920 129600000
MXI03930 129700000
MXI03940 129800000
MXI03950 129900000
MXI03960 130000000
MXI03970 130100000
          130200000
MXI03990 130300000
MXI04000 130400000
MXI04010 130500000
MXI04020 130600000
MXI04030 130700000
MXI04040 130800000
MXI04050 130900000
MXI04060 131000000
MXI04070 131100000
```



```

      ROOT = AMINI(ROOT-EPS,R(K))
      CALL QMIEL(A,R(LD),R(L0),R(LP),R(LQ),R(LR),R(LS),M,ROUT,X(1,I))
200  K = K + 1
      RETURN
      END
MXI04500 135400000
MXI04510 135500000
MXI04520 135600000
MXI04530 135700000
MXI04540 135800000
```

```

SUBROUTINE TFORM(A,N,D,O,S,P)
DIMENSION A(I),D(I),U(I),S(I)
BL = 0.
BU = 0.
OLD = 0.
D(I) = A(I)
KIKI = I
NI = N - 1
DO 230 K = 1,NI
  KPI = K + 1
  KK = KIKI
  KKPI = KK + 1
  NK = N - K
  KN = KK + NK
  KIKI = KN + 1
  SUM = 0.
  DO 100 KJ = KKPI,KN
    S(K) = SUM
    RHO = SQRT(SUM)
    RAD = OLD + RHO
    BL = AMIN1(BL,D(K)-RAD)
    BU = AMAX1(BU,D(K)+RAD)
    IF (K - NI) 120,230,230
  120 OLD = RHO
    IF (A(KKPI)) 140,140,130
  130 RHO = -RHO
  140 O(K) = RHO
  IF (SUM) 150,230,150
  150 A(KKPI) = A(KKPI) - RHO
    RHO = 1. / (RHO*A(KKPI))
    A(KK) = RHO
    IJ = KK
  DO 160 J = KPI,N
    IJ = IJ + 1
    O(IJ) = A(IJ)
  160 O(IJ) = 0.
    II = KIKI
  NI = NK
  DO 190 I = KPI,N
    D(I) = D(I) + A(II)*O(I)
  IJ = II

```

MXI04550 135900000
MXI04560 136000000
MXI04570 136100000
MXI04580 136200000
MXI04590 136300000
MXI04600 136400000
MXI04610 136500000
MXI04620 136600000
MXI04630 136700000
MXI04640 136800000
MXI04650 136900000
MXI04660 137000000
MXI04670 137100000
MXI04680 137200000
MXI04690 137300000
MXI04700 137400000
MXI04710 137500000
MXI04720 137600000
MXI04730 137700000
MXI04740 137800000
MXI04750 137900000
MXI04760 138000000
MXI04770 138100000
MXI04780 138200000
MXI04790 138300000
MXI04800 138400000
MXI04810 138500000
MXI04820 138600000
MXI04830 138700000
MXI04840 138800000
MXI04850 138900000
MXI04860 139000000
MXI04870 139100000
MXI04880 139200000
MXI04890 139300000
MXI04900 139400000
MXI04910 139500000
MXI04920 139600000
MXI04930 139700000
MXI04940 139800000
MXI04950 139900000
MXI04960 140000000

```

MXI04970 140100000
MXI04980 140200000
MXI04990 140300000
MXI05000 140400000
MXI05010 140500000
MXI05020 140600000
MXI05030 140700000
MXI05040 140800000
MXI05050 140900000
MXI05060 141000000
MXI05070 141100000
MXI05080 141200000
MXI05090 141300000
MXI05100 141400000
MXI05110 141500000
MXI05120 141600000
MXI05130 141700000
MXI05140 141800000
MXI05150 141900000
MXI05160 142000000
MXI05170 142100000
MXI05180 142200000
MXI05190 142300000
MXI05200 142400000
MXI05210 142500000
MXI05220 142600000
MXI05230 142700000
MXI05240 142800000
MXI05250 142900000
MXI05260 143000000
MXI05270 143100000
MXI05280 143200000

II = II + NI
NI = NI - 1
IF (NI) 170,190,170
170 X = O(I)
DO 180 J = I,NI
IJ = IJ + 1
D(J+1) = D(J+1) + A(IJ)*X
180 D(I) = D(I) + A(IJ)*D(J+1)
190 D(I) = D(I) * RHO
SUM = 0.
DO 200 I = KPI,N
SUM = SUM + D(I)*O(I)
TAU = RHO * SUM * .5
DO 210 I = KPI,N
D(I) = D(I) + TAU*O(I)
II = KIKI
NI = NK
DO 220 I = KPI,N
RHO = D(I)
TAU = O(I)
IJ = II
II = II + NI
NI = NI - 1
DO 220 J = I,N
A(IJ) = A(IJ) + RHO*O(J) + TAU*D(J)
220 IJ = IJ + 1
230 D(K+1) = A(KIKI)
O(NI) = A(KKPI)
O(N) = A(MINI(BL,D(N)-RHO)
S(N) = A(MAXI(BU,D(N)+RHO)
RETURN
END

```

```

SUBROUTINE STURM (N,LIM1,NUMB,D,OFFD,SEC,PFFD,SIGMA,EPS)
DIMENSION D(1),OFFD(1),SEC(1),SIGMA(1),PFFD(1)
DATA HALF / .5/
BL = OFFD(N)
BU = SEC(N)
LIM2 = LIM1 + NUMB - 1
CALL PREP(N,D,SEC,ROOT,LORD)
N1 = N - 1
IF (N1) 16,200,200
200 TOL = AMAX1(-BL,BU)
OFFD(N) = TOL
TOL = TOL * AMAX1(1.E-15,EPS)
DO 2 I = LIM1,LIM2
SIGMA(I) = BL
2 PFFD(I) = BU
LORD = 0
L = LIM1 - 1
RUTE = 1.E20
GO TO 3
300 DO 400 I = K,L
400 SIGMA(I) = ROOT
3 K = L + 1
IF (K - LIM2) 4,4,16
4 BU = PFFD(K)
ROOT = BU + HALF * (SIGMA(K) - BU)
IF (K - L) 5,7,5
5 DO 6 I = K,LIM2
IF (BU - PFFD(I)) 7,6,7
6 L = I
7 IF (ABS(ROOT - RUTE) - TOL) 300,300,8
8 CALL DET(N,D,SEC,ROOT,LORD)
DO 11 I = K,L
IF (I - LORD) 9,9,10
9 SIGMA(I) = ROOT
GO TO 11
10 PFFD(I) = ROOT
11 CONTINUE
RUTE = ROOT
GO TO 4
16 RETURN
END

```

```

MXI05290 143300000
MXI05300 143400000
MXI05310 143500000
MXI05320 143600000
MXI05330 143700000
MXI05340 143800000
MXI05350 143900000
MXI05350 144000000
MXI05370 144100000
MXI05380 144200000
MXI05390 144300000
MXI05400 144400000
MXI05410 144500000
MXI05420 144600000
MXI05430 144700000
MXI05440 144800000
MXI05450 144900000
MXI05460 145000000
MXI05470 145100000
MXI05480 145200000
MXI05490 145300000
MXI05500 145400000
MXI05510 145500000
MXI05520 145600000
MXI05530 145700000
MXI05540 145800000
MXI05550 145900000
MXI05560 146000000
MXI05570 146100000
MXI05580 146200000
MXI05590 146300000
MXI05600 146400000
MXI05610 146500000
MXI05620 146600000
MXI05630 146700000
MXI05640 146800000
MXI05650 146900000
MXI05660 147000000
MXI05670 147100000
MXI05680 147200000
MXI05690 147300000

```

```

SUBROUTINE PREP(N,D,SEC,R,DT,LORD)
DIMENSION D(1),SFC(1)
EQUIVALENCE (RD2,RE2), (RD4,RE4)
N1 = N - 1
RETURN
ENTRY DET
RDO = ROOT
LOW = 0
LAWD = 0
100 RD2 = 0.00
RD4 = 1.00
DO 120 I = LOW,N1
RD4 = C(I+1) - RDO - RD2
IF (RD4) 120,140,110
110 LAWD = LAWD + 1
120 RE2 = SEC(I+1) / RE4
130 LORD = LAWD
GO TO 200
140 LAWD = LAWD + 1
IF (RE2) 150,160,150
150 I = I + 1
160 LOW = I + 1
IF (LOW - N1) 100,100,130
200 RETURN
END
MXI05700 147400000
MXI05710 147500000
MXI05720 147600000
MXI05730 147700000
MXI05740 147800000
MXI05750 147900000
MXI05760 148000000
MXI05770 148100000
MXI05780 148200000
MXI05790 148300000
MXI05800 148400000
MXI05810 148500000
MXI05820 148600000
MXI05830 148700000
MXI05840 148800000
MXI05850 148900000
MXI05860 149000000
MXI05870 149100000
MXI05880 149200000
MXI05890 149300000
MXI05900 149400000
MXI05910 149500000
MXI05920 149600000
MXI05930 149700000
MXI05940 149800000

```

```

SUBROUTINE QSVEC(A,D,OFFD,P,Q,R,S,N,ROOT,X)
SYMMETRIC MATRIX EIGENVECTOR CALCULATION.
GIVEN THE ENTRIES (D AND OFFD) OF THE HOUSEHOLDER TRI-DIAGONAL FORM B
OF A REAL SYMMETRIC MATRIX A, AND GIVEN A GOOD APPROXIMATE ROOT OF
B (AND A) THIS FORTRAN 4 SUBROUTINE COMPUTES A UNIT EIGENVECTOR X
OF B, THEN TRANSFORMS IT TO A UNIT VECTOR OF A, USING THE VECTORS
STORED IN THE A ARRAY.
DIMENSION A(1),D(1),OFFD(1),P(1),Q(1),R(1),S(1),X(1)
DOUBLE PRECISION SUM
COMMON /INFO/ SUM,M,IX,IA
DATA MINUS2/0.7777777777777777777777777777776/

C PART 1. PRELIMINARIES.
C
IX = 1
IA = 1
N1 = N - 1
N2 = N - 2
RETURN
ENTRY QMIEL
ASSIGN 170 TO KOUNT
TOL = 0.
DO 100 I = 1,N
P(I) = D(I) - ROOT
Q(I) = OFFD(I)
R(I) = 0.
TOL = AMAX1(TOL,ABS(D(I)))
100 X(I) = RDM(X) + .1
TOL = (TOL + 1.E-15) * 1.E-15

C PART 2. MATRIX DECOMPOSITION.
C
DO 150 I = 1,N1
T = ABS (P(I))
U = ABS (OFFD(I))
IF (T + U - TOL) 110,120,120
110 P(I) = TOL
T = P(I)
120 IF (T - U) 130,140,140
130 S(I) = P(I)/OFFD(I)
S(I) = OR(S(I), 1)
TEMP = Q(I)

```

```

MXI05950 149900000
MXI05960 150000000
BMXI05970 150100000
MXI05980 150200000
MXI05990 150300000
WMXI06000 150400000
MXI06010 150500000
MXI06020 150600000
MXI06030 150700000
MXI06040 150800000
MXI06050 150900000
MXI06060 151000000
MXI06070 151100000
MXI06080 151200000
MXI06090 151300000
MXI06100 151400000
MXI06110 151500000
MXI06120 151600000
MXI06130 151700000
151800000
MXI06150 151900000
MXI06160 152000000
MXI06170 152100000
MXI06180 152200000
MXI06190 152300000
MXI06200 152400000
MXI06210 152500000
MXI06220 152600000
MXI06230 152700000
MXI06240 152800000
MXI06250 152900000
MXI06260 153000000
MXI06270 153100000
MXI06280 153200000
MXI06290 153300000
MXI06300 153400000
MXI06310 153500000
MXI06320 153600000
MXI06330 153700000
MXI06340 153800000
MXI06350 153900000
MXI06360 154000000

```



```

P(I) = OFFD(I)
Q(I) = P(I+1)
R(I) = Q(I+1)
P(I+1) = TEMP - S(I)*Q(I)
Q(I+1) = -S(I)*R(I)
GO TO 150
140 S(I) = GFFD(I)/P(I)
S(I) = AND(S(I),MINUS2)
P(I+1) = P(I+1) - S(I)*Q(I)
150 CONTINUE
IF (ABS(P(N)) .LT. TOL) P(N) = TOL
GO TO 210
C
C PART 3. RIGHT SIDE MODIFICATION.
C
170 ASSIGN 330 TO KOUNT
DO 200 I = 1,N1
TEMP = AND(S(I), 1)
IF (TEMP) 180,190,180
180 T = X(I)
X(I) = X(I+1)
X(I+1) = T - S(I)*X(I)
GO TO 200
190 X(I+1) = X(I+1) - S(I)*X(I)
200 CONTINUE
C
C PART 4. TRIANGULAR SYSTEM SOLUTION.
C
210 X(N) = X(N)/P(N)
X(N1) = (X(N1) - Q(N1)*X(N)) / P(N1)
DO 220 I = 2,N1
K = N - I
220 X(K) = (X(K) - Q(K)*X(K+1) - R(K)*X(K+2)) / P(K)
C
C PART 5. SCALING TO UNIT VECTOR.
C
230 SUM = 0.00
M = N
SCALAP = SQRT(DOTPRO(X,X))
DO 250 I = 1,N
250 X(I) = X(I)/SCALAR
GO TO KOUNT, (170,330,370)
C

```

```

MXI06370 154100000
MXI06380 154200000
MXI06390 154300000
MXI06400 154400000
MXI06410 154500000
MXI06420 154600000
MXI06430 154700000
MXI06440 154800000
MXI06450 154900000
MXI06460 155000000
MXI06470 155100000
MXI06480 155200000
MXI06490 155300000
MXI06500 155400000
MXI06510 155500000
MXI06520 155600000
MXI06530 155700000
MXI06540 155800000
MXI06550 155900000
MXI06560 156000000
MXI06570 156100000
MXI06580 156200000
MXI06590 156300000
MXI06600 156400000
MXI06610 156500000
MXI06620 156600000
MXI06630 156700000
MXI06640 156800000
MXI06650 156900000
MXI06660 157000000
MXI06670 157100000
MXI06680 157200000
MXI06690 157300000
MXI06700 157400000
MXI06710 157500000
MXI06720 157600000
MXI06730 157700000
MXI06740 157800000
MXI06750 157900000
MXI06760 158000000
MXI06770 158100000
MXI06780 158200000
MXI06790 158300000

```

C PART 6. TRANSFORMATION BY ORTHOGONAL MATRICES.

```

330 L = (N*(N+1))/2 - 4
DO 360 I = 1,N2
NI = N - I
SUM = 0.00
M = I + 1
SCALAR = A(L-1) * DOTPRO(X(NI),A(L))
IJ = L
DO 350 J = NI,N
X(J) = X(J) + SCALAR*A(IJ)
350 IJ = IJ + 1
360 L = L - I - 3
ASSIGN 370 TO KOUNT
GO TO 230
370 RETURN
END
MXI06800 158400000
MXI06810 158500000
MXI06820 158600000
MXI06830 158700000
MXI06840 158800000
MXI06850 158900000
MXI06860 159000000
MXI06870 159100000
MXI06880 159200000
MXI06890 159300000
MXI06900 159400000
MXI06910 159500000
MXI06920 159600000
MXI06930 159700000
MXI06940 159800000
MXI06950 159900000
MXI06960 160000000

```

```

SUBROUTINE DAGGER(A,M,P,KO,Q)
DIMENSION A(I),P(I),Q(I)
EQUIVALENCE (SUN,SUM)
K = KO
K1 = K + 1
L=1
LL = 0
INDEX = 1
DO 130 I = 2,K1
LJ = INDEX
SUM = 0.
DO 90 J = 1,L
SUM = SUM + A(LJ)*P(J)
90 LJ = LJ + 1
IF (K - L) 100,120,100
100 LL = LL + L
LJ = LL + L
DO 110 J = I,K
SUM = SUM + A(LJ)*P(J)
110 LJ = LJ + J
120 Q(I-1) = SUM
INDEX = INDEX + L
130 L = I
SUM = 0.
DO 140 I = 1,K
SUM = SUM + P(I)*Q(I)
A(LL+1) = Q(I)
A(LL) = SUM
IF (M - K) 150, 200, 150
150 DO 190 L = K1,M
JL = LL+L-K
SUM = 0.
DO 180 J = 1,K
SUM = SUM + P(J)*A(JL)
180 JL = JL + 1
LL = LL + L - 1
190 A(LL) = SUM
200 CONTINUE
RETURN
END
MXI06970 160100000
MXI06980 160200000
MXI06990 150300000
MXI07000 160400000
MXI07010 160500000
MXI07020 160600000
MXI07030 160700000
MXI07040 160800000
MXI07050 160900000
MXI07060 161000000
MXI07070 161100000
MXI07080 161200000
MXI07090 161300000
MXI07100 161400000
MXI07110 161500000
MXI07120 151600000
MXI07130 161700000
MXI07140 161800000
MXI07150 161900000
MXI07160 162000000
MXI07170 162100000
MXI07180 162200000
MXI07190 162300000
MXI07200 162400000
MXI07210 162500000
MXI07220 162600000
MXI07230 162700000
MXI07240 162800000
MXI07250 162900000
MXI07260 163000000
MXI07270 163100000
MXI07280 163200000
MXI07290 163300000
MXI07300 163400000
MXI07310 163500000
MXI07320 163600000
MXI07330 163700000
MXI07340 163800000
MXI07350 163900000
MXI07360 164000000
MXI07370 154100000

```

```

SUBROUTINE SWITCH(A,M)
DIMENSION A(1)
N = IABS(M)
IF (N - 2) 190,190,90
90 L = (N*(N+1)) / 2
KEY = 1
LOCK = N/2 + 1
IF (M) 100,190,160
100 IF (N - 3) 110,140,110
110 KKT = 3
NKF = N - 1
IMAGE = L
INTO = L - 3
I = 3
DO 130 K = 2,LOCK
DO 120 IK = KKT,NKF
X = A(IK)
A(IK) = A(INTO)
A(INTO) = X
INTO = INTO - I
120 I = I + 1
KKT = NKF + K
NKF = NKF + N - K
IMAGE = IMAGE - K
INTO = IMAGE
130 I = K
140 IF (KEY) 150,190,150
150 KEY = 0
160 LOV2 = L / 2
DO 170 I = 3,LOV2
X = A(I)
A(I) = A(K)
A(K) = X
170 K = K - 1
180 IF (KEY) 180,190,180
180 KEY = 0
GO TO 100
190 RETURN
END
MXI07380 164200000
MXI07390 164300000
MXI07400 164400000
MXI07410 164500000
MXI07420 164600000
MXI07430 164700000
MXI07440 164800000
MXI07450 164900000
MXI07460 165000000
MXI07470 165100000
MXI07480 165200000
MXI07490 165300000
MXI07500 165400000
MXI07510 165500000
MXI07520 165600000
MXI07530 165700000
MXI07540 165800000
MXI07550 165900000
MXI07560 166000000
MXI07570 166100000
MXI07580 166200000
MXI07590 166300000
MXI07600 166400000
MXI07610 166500000
MXI07620 166600000
MXI07630 166700000
MXI07640 166800000
MXI07650 166900000
MXI07660 167000000
MXI07670 167100000
MXI07680 167200000
MXI07690 167300000
MXI07700 167400000
MXI07710 167500000
MXI07720 167600000
MXI07730 167700000
MXI07740 167800000
MXI07750 167900000
MXI07760 168000000
MXI07770 168100000

```

```
FUNCTION DOTPRO(X,Y)
DIMENSION X(1),Y(1)
DOUBLE PRECISION S
COMMON /INFO/ S,N,IX,IY
IF (N) 120,120,100
100 JX = 1
    JY = 1
    DO 110 J = 1,N
        S = S + X(JX)*Y(JY)
        JX = JX + IX
        JY = JY + IY
110 JY = JY + IY
120 DOTPRO = S
RETURN
END
```

```
MXI07780 168200000
MXI07790 168300000
MXI07800 168400000
MXI07810 168500000
MXI07820 158600000
MXI07830 168700000
MXI07840 168800000
MXI07850 168900000
MXI07860 169000000
MXI07870 169100000
MXI07880 169200000
MXI07890 169300000
MXI07900 169400000
MXI07910 169500000
```

```

SUBROUTINE INCH (A,MO,Y,NIX)
C
C INVERSION OF POSITIVE DEFINITE REAL SYMMETRIC MATRIX A. A IS ASSUMED
C TO BE STORED BY ROWS IN LOWER TRIANGULAR FORM. THE INVERSE IS STORED
C OVER A.
COMMON /BOND/ M,K /WINTER/ KOLD
COMMON /OPT2/ PRINT
REAL A(I),Y(I)
KOLD = 0
M = IABS(MO)
CALL FUTIL(A,M,NIX)
IF (NIX) 120,100,100
100 KK = 0
    K1 = 1
    DO 115 K = 1,M
        KK = KK + K
        DO 105 I = K,M
            Y(I) = 0.
            Y(K) = 1.
            CALL TRIEQ(A(K1),Y)
            IK = KK
            DO 110 I = K,M
                A(IK) = Y(I)
                IK = IK + I
110 CONTINUE
115 K1 = K1 + K
120 CONTINUE
RETURN
END
MXI08090 169600000
MXI08100 169700000
MXI08110 169800000
MXI08120 169900000
MXI08130 170000000
MXI08140 170100000
MXI08150 170200000
MXI08160 170300000
MXI08170 170400000
MXI08180 170500000
MXI08190 170600000
MXI08200 170700000
MXI08210 170800000
MXI08220 170900000
MXI08230 171000000
MXI08240 171100000
MXI08250 171200000
MXI08260 171300000
MXI08270 171400000
MXI08280 171500000
MXI08290 171600000
MXI08300 171700000
MXI08310 171800000
MXI08320 171900000
MXI08330 172000000
MXI08340 172100000
MXI08350 172200000
MXI08360 172300000
MXI08370 172400000

```

```

SUBROUTINE TRIEQ(A,Y)
REAL A(1),Y(1)
COMMON /WINTER/INDIC8
COMMON /BOND/ M,L
EQUIVALENCE (SUN,SUM)
L1 = L
MML=M-L1
MM1 = M - 1
IF (INDIC8) 130,100,100
100 Y(L1) = Y(L1) / A(L1)
I1 = L1
I1=I1
IF(MML)105,125,105
105 DO 120 I = L1,MML
I1 = I1 + 1
SUM = -Y(I+1)
IJ = I1
DO 110 J = L1,I
SUM = SUM + A(IJ)*Y(J)
110 IJ = IJ + 1
I1 = IJ
120 Y(I+1) = -SUM / A(I1)
125 IF (INDIC8) 170,140,170
130 I1=((MML+1)*(M+L1))/2
140 I = M
145 Y(I) = Y(I) / A(I1)
I1 = I1 - 1
I = I - 1
IF (I - L1) 170,150,150
150 SUN = -Y(I+1)
IJ = I1 + L1
DO 160 J = L1,I
Y(J) = Y(J) + SUN*A(IJ)
160 IJ = IJ + 1
GO TO 145
170 RETURN
END

```

```

MXI08380 172500000
MXI08390 172600000
MXI08400 172700000
MXI08410 172800000
MXI08420 172900000
MXI08430 173000000
MXI08440 173100000
MXI08450 173200000
MXI08460 173300000
MXI08470 173400000
MXI08480 173500000
MXI08490 173600000
MXI08500 173700000
MXI08510 173800000
MXI08520 173900000
MXI08530 174000000
MXI08540 174100000
MXI08550 174200000
MXI08560 174300000
MXI08570 174400000
MXI08580 174500000
MXI08590 174600000
MXI08600 174700000
MXI08610 174800000
MXI08620 174900000
MXI08630 175000000
MXI08640 175100000
MXI08650 175200000
MXI08660 175300000
MXI08670 175400000
MXI08680 175500000
MXI08690 175600000
MXI08700 175700000
MXI08710 175800000
MXI08720 175900000
MXI08730 176000000
MXI08740 176100000

```

```

SUBROUTINE FUTIL(A,N,NIX)
DIMENSION A(I)
DOUBLE PRECISION SUM
EQUIVALENCE (SUM,SUM)
K1 = 1
KK = 0
DO 210 K = 1,N
  KK = KK + K
  IK = KK
  KK1 = KK - 1
  IF (KK1) 60,50,60
50 ASSIGN 100 TO LEAP
  GO TO 70
60 ASSIGN 80 TO LEAP
70 I1 = K1
  DO 140 I = K,N
    SUM = -A(IK)
  GO TO LEAP, (80,100)
80 IJ = I1
  DO 90 KJ = K1,KK1
    SUM = SUM + A(IJ)*A(KJ)
90 IJ = IJ + 1
100 I1 = I1 + 1
  IF (I - K) 120,105,120
105 DENOM = -SUM
  IF (DENOM) 980,980,110
110 DENOM = -SQRT(DENOM)
  A(IK) = -DENOM
  GO TO 130
120 A(IK) = SUM / DENOM
130 IK = IK + 1
140 CONTINUE
  K1 = K1 + K
210 CONTINUE
  NIX = 0
220 RETURN
980 NIX = -K
  GO TO 220
  END
*FOLLOWING VARIABLES EQUIVALENCEED BUT NOT REFERENCED
SUM

```

```

MXI08750 176200000
MXI08760 176300000
MXI08770 176400000
MXI08780 176500000
MXI08790 176600000
MXI08800 176700000
MXI08810 176800000
MXI08820 176900000
MXI08830 177000000
MXI08840 177100000
MXI08850 177200000
MXI08860 177300000
MXI08870 177400000
MXI08880 177500000
MXI08890 177600000
MXI08900 177700000
MXI08910 177800000
MXI08920 177900000
MXI08930 178000000
MXI08940 178100000
MXI08950 178200000
MXI08960 178300000
MXI08970 178400000
MXI08980 178500000
MXI08990 178600000
MXI09000 178700000
MXI09010 178800000
MXI09020 178900000
MXI09030 179000000
MXI09040 179100000
MXI09050 179200000
MXI09060 179300000
MXI09070 179400000
MXI09080 179500000
MXI09090 179600000
MXI09100 179700000
MXI09110 179800000
MXI09120 179900000
MXI09130 180000000

```


FUNCTION ARSIN(X)
ARSIN=ASIN(X)
RETURN
ENTRY ARCOS
ARCOS=ACOS(X)
RETURN
END

MXI09140 180100000
MXI09150 180200000
MXI09160 180300000
MXI09170 180400000
MXI09180 180500000
MXI09190 180600000
MXI09200 180700000

MXI09210 180800000
MXI09220 180900000
MXI09230 181000000
MXI09240 181100000

FUNCTION RDM(X)
RDM=RANF(X)
RETURN
END

APPENDIX B

DETAILED PROGRAMMING INFORMATION FOR

THE PHASE II COMPUTER PROGRAM

This appendix contains detailed programming information for the Phase II computer program. In addition, samples of input and output data are presented.

APPENDIX B1

EXAMPLES OF INPUT DATA

The following two examples illustrate the method of setting up the input data deck. The configuration for both examples is that discussed in Section 6 of Volume I. Computer output for these examples is presented in Appendix B2.

Example 1

This example shows input data for a 40 second rigid body run with plotting. This run has fluids present, no deployment, no controls, no supplementary forces, no moving masses and no structural loads computed. Although flexible-body data is present, the constraint option has been used to rigidize the entire Space Station. The JUMP clue to set all $\{q_i\}$, $\{\dot{q}_i\}$, $\{\theta_i\}$ and $\{\dot{\theta}_i\}$ to zero is used. Fixed-step numerical integration with a step size of .05 is indicated together with a plotting output interval of .09997436 so that plotting will occur the first time a multiple of .05 exceeds each multiple of .0997436. The time-history printer output interval is $2 * .0997436$.

plot clue, fluid clue, no. pipes

reservoir mass points
pipes mass points
plotting groups

KLAE, IFLAB, IFGW, IFGN
IFDEFL, IFCON, IFSUPP
STRUCTURAL LOADS
IPHSL, JUMP

percentage damping

{R}
{R}
{V}
{w}
A, A
m₁

[J]

{S}
{e}
{u}
{u}
{e}

input for
emptying
reservoir

[J]

b₁, b₂, b₃; m₁, m₂, m₃
{e}

input for
filling
reservoir

{S}
{u}, {e}, {u}, {e}, {u}, {e}

input for pipe
at mass point 3

[AJ]

[J]

start of input for
pipe at mass point 4

40. 5.
1 1 5

8 2
3 4 5 6 7
4 4 8 8 17 42 42
4 1 1

1 1
.02 .02
.02 .02

528.

.4189
.9346 E-4 15.
.070095
521.12317

521.12317

.16733949
5.958075
1.
60.
110.
1.

181517.9

181517.9

25.

30.

35.809862
60.

0.

.014019
9.6104029

9.6104029

.033467897
-.364494
-1.
-21.
-31.
-1.

14432.905

14432.905

35.809862
60.

0.

25.

20.

.126171

-2.018736
90.

-43200.

-43200.

117.61581

117.61581

.30121108
-.168228
120.

input for pipe at mass point 4 (continued)	- 3600.	-3600.		
	202.24264	202.24264		.40161477
	.126171			1.766394 90.
input for pipe at mass point 5	37800.	37800.		
	110.04555	110.04555		.30121108
	.196266			-8.046906 140.
input for pipe at mass point 6	-172200.	-172200.		
	650.72522	650.72522		.46845507
	.308418			-.154209 220.
input for pipe at mass point 7	-3300.	-3300.		
	1244.3979	1244.3979		.73629374
				320.
NO. Counterweight mass points	1			
	194.09938			
	.17259834 E8			
mass Inertia Matrix	8	.23447205 E7		.15489648 E8
	1			-320.
V, V ₀ , Z ₀ , acc _{max} DELTA, EPSIL, STEP DTAU, NTIME	1.			-1.
	0.	120.		1685.9158
	.09997436			2. -.05
				60.

{A} {B} {S} {T} {U} {V} {W} {X} {Y} {Z} {AA} {BB} {CC} {DD} {EE} {FF} {GG} {HH} {II} {JJ} {KK} {LL} {MM} {NN} {OO} {PP} {QQ} {RR} {SS} {TT} {UU} {VV} {WW} {XX} {YY} {ZZ} {AAA} {BBB} {CCC} {DDD} {EEE} {FFF} {GGG} {HHH} {III} {JJJ} {KKK} {LLL} {MMM} {NNN} {OOO} {PPP} {QQQ} {RRR} {SSS} {TTT} {UUU} {VVV} {WWW} {XXX} {YYY} {ZZZ} {AAA} {BBB} {CCC} {DDD} {EEE} {FFF} {GGG} {HHH} {III} {JJJ} {KKK} {LLL} {MMM} {NNN} {OOO} {PPP} {QQQ} {RRR} {SSS} {TTT} {UUU} {VVV} {WWW} {XXX} {YYY} {ZZZ}

Example 2

This example shows input data for a 10 second run with with KLUE = 3 (flexible Laboratory and rigid Counterweight). The quiescent-state initial conditions are used for the deformations (see Section 3.4.10). The complete quiescent-state initial conditions are presented in the output shown in Appendix B2. Plotting will be done, and moving masses 1 and 2 are present indicating elevator motion and mass balancing. Controls are present, and loads will be printed. The integration step-size is fixed.

final time, plot scale
 plot clue, no. moving masses
 moving masses present

plotting groups
 plotting group mass points
 KJUE, IFLAB, IFCW, IFCN
 IFEPL, IFCOON, IFSUPP

controls
 input
 Counterweight command
 Spin command
 Spin control
 Attitude control
 wobble
 control

KLUJCS, KJULAB, KJUCW, N, NB
 input for \mathcal{L}' , no. masses
 load-computation
 point $\mathcal{L}'=4$ for free body

input for
 structural
 loads

input for
 load - computation
 point $\mathcal{L}' = 42$

IPHSI, JUMP
 start of input
 for f_{θ_i}

10.
 1
 1 1
 5.

111 11 1 1
 4 4 8 8 17 42 42
 3 1 1
 50.

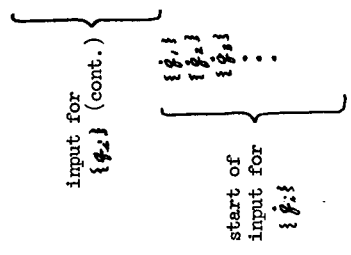
1685.0159 950.
 .4189 950.
 .0002094
 .0001745 .001745
 0. 2400.
 360. 2880.
 1 1 2 160.

1 1 1
 411 60.

1 2 3 910112131415
 16
 4227 0.
 1718190212222422527
 28293031323334353637
 38394041264344

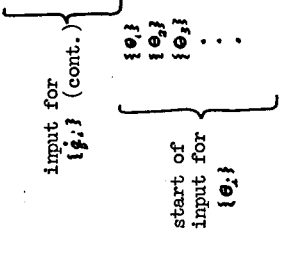
1
 -0.83869551F-08 0.15617466F-06-0.23666996E 00
 0.46313410F-07 0.58134901E-07-0.236666465E 00
 0.92101516E-07-0.11938391E-06-0.23661751E 00
 -0.11785437E-06-0.13196950E-06-0.23631844E 00
 -0.14846518E-06-0.32202860E-06-0.23642584E 00
 -0.11989164E-07 06-0.23637813E 00
 -0.266517 06-0.23637813E 00
 -0. 06-0.23637813E 00
 06-0.23637813E 00
 06-0.23637813E 00

.40029327E-05-0.12099405
 -0.27957019E-06-0.57446596E-06-0.23651801E-00
 -0.25430393E-06 0.28183858E-05-0.22518796E-00
 0.13012941E-05 0.58819816E-04 0.25090857E-01
 -0.29180126E-06-0.89184323E-06-0.23637795E-00
 0.19956877E-06 0.21486398E-04 0.33377537E-00
 0.77029582E-06 0.40153798E-04 0.14100447E-01



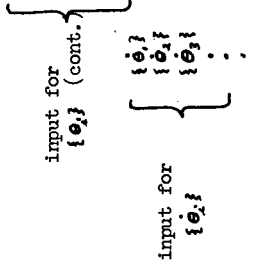
• • •

-0.15526211E-08 0.49180837E-09 0.875660570E-10
 -0.1541877E-08 0.48350324E-09 0.87815380E-10
 -0.14736088E-08 0.53685455E-09 0.21095705E-09
 -0.14289299E-08 0.56446758E-09 0.40990500E-09
 -0.14726993E-08 0.45360271E-09 0.48821147E-09
 -0.142915E-08 0.369E-09 0.43942361E-09
 -08-0.22493392E-09
 0.73632905E-10



• • •

.45169843E-03 0.28689275E-02
 0.59216905E-03-0.59020735E-08-0.12144292E-08
 0.38333496E-02-0.44284395E-07-0.19368720E-08
 -0.86043889E-09 0.53627505E-10 0.73632905E-10
 0.35762596E-02-0.18596209E-07-0.21672610E-08
 0.46098903E-02-0.31490277E-07-0.22528703E-08



• • •

input for $\{\theta_i\}$ (cont.)

percentage damping $\left\{ \begin{array}{l} \{R\} \\ \{N\} \\ \{P\} \\ \{W\} \\ \{L\} \\ \{K_2 \end{array} \right.$

NO. Counterweight mass points IPHSL, JUMP $\left\{ \begin{array}{l} \{F_i\} \\ \text{mass} \\ \text{Inertia Matrix} \\ \xi, \alpha \\ \{A\} \\ \{X\} \\ \{S\} \\ \{S\} \\ \{P\} \\ \{P\} \\ \{Y\} \\ \{Y\} \end{array} \right.$

MICOM input for j=1 $\left\{ \begin{array}{l} \text{axes of motion} \\ \{U(0)\} \\ U, Z, ACC, MAG, VEL, MAX \\ \{U(0)\} \\ \{U(0)\} \\ \{X_{j=1}^{(0)}\} \\ \{X_{j=1}^{(0)}\} \\ \text{beam subroutine input} \\ \text{DELTA, EPSIL, STEP} \\ \text{DTAU, NTIME} \\ \text{KLOUTL, KLOUTC} \end{array} \right.$

Balance Mass control input $\left\{ \begin{array}{l} \{Y_{j=1}^{(0)}\} \\ \{Y_{j=1}^{(0)}\} \\ \text{axes of motion} \\ \{U(0)\} \\ U, Z, ACC, MAG, VEL, MAX \\ \{U(0)\} \\ \{U(0)\} \\ \{X_{j=1}^{(0)}\} \\ \{X_{j=1}^{(0)}\} \\ \text{beam subroutine input} \\ \text{DELTA, EPSIL, STEP} \\ \text{DTAU, NTIME} \\ \text{KLOUTL, KLOUTC} \end{array} \right.$

printout at mass points

•02 •02 •02 •02
 •07 •07 •02 •02
 436.4843

•4189
 25.879917
 12.939959

1 1
 194.09938 320.
 •17259834 FR •23647205 E7
 8 1 •15488648 FH

1. -1.
 1685.9158
 762.1295
 20.
 348.3181

17.939959 17. •364 0.
 194.099 248.954 1057.289
 38.6025 E6 15.4855 E5 17.2560 E6
 624.758 920. 3. 18.2943 E6
 13.57 E10 10.86 F10 300. E7
 •05 •05

•09997436 2
 13 1 4 8 12 16 17 18 29 30 45 46 57 58

APPENDIX B2

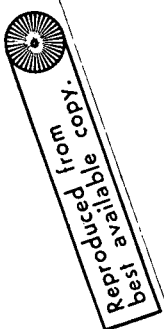
EXAMPLES OF PROGRAM OUTPUT

This appendix shows the output for the two problems described in Appendix B1. The key to reading the titles of the time-history print out is given at time = 0 in these examples.

Example 1

The first portion of the output consists of the input data. The input modes were truncated; however, they are shown in their entirety in Appendix I of Volume I.

The second portion of the print out is the time history. Auxiliary results presented in this portion include the location of the center of mass and the total-system angular momentum.



INPUT DATA

FINAL TIME, PLUTTIC CLUE, PLAT INTERVAL
 0.000000E 02 1 0.000000E 01
 FLDJ CLUE, NO. PILES

RESERVOIR MASS POINTS
 2

NO. MOVING MASSES, MOVING MASSES PRESENT
 0 0 0 0 0 0 0

PIPEL ON MASS POINTS
 3 4 5 6 7

CLJES FOR THIS RUN
 PILEL CLUE, DEPLOYMENT, CONTROLS, SUPP. FORCES
 0 0 0

LAD INPUT
 NO. MASSES = 72
 MASS POINT LOCATIONS

NO.	X(1)	X(2)	X(3)
1	0.0	0.0	0.00100000E 03
2	0.0	0.0	0.00100000E 03
3	0.0	0.0	0.74100000E 03
4	0.0	0.0	0.02100000E 03
5	0.0	0.0	0.50100000E 03
6	0.0	0.0	0.44100000E 03
7	0.0	0.0	0.22050000E 03
8	0.0	0.0	0.0
9	-0.13200000E 03	-0.00100000E 03	0.00100000E 03
10	-0.25000000E 03	-0.00100000E 03	0.00100000E 03
11	-0.47000000E 03	-0.00100000E 03	0.00100000E 03
12	-0.48200000E 03	-0.00100000E 03	0.00100000E 03
13	0.15200000E 03	0.00100000E 03	0.00100000E 03
14	0.25000000E 03	0.00100000E 03	0.00100000E 03
15	0.37200000E 03	0.00100000E 03	0.00100000E 03
16	0.45000000E 03	0.00100000E 03	0.00100000E 03
17	-0.50000000E 03	-0.00100000E 03	0.00100000E 03
18	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
19	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
20	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
21	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
22	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
23	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
24	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
25	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
26	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
27	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
28	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
29	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
30	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
31	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
32	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
33	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
34	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
35	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
36	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
37	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
38	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
39	-0.50400000E 03	-0.00100000E 03	0.00100000E 03
40	-0.50400000E 03	-0.00100000E 03	0.00100000E 03

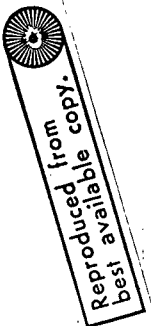
41	0.0	-0.51600000E 03	0.0	
42	0.0	-0.12000000E 02	0.0	
43	0.0	-0.31200000E 03	0.0	
44	0.0	-0.56400000E 03	0.0	
45	0.0	0.56400000E 03	-0.13050000E 03	
46	0.0	0.56400000E 03	0.13050000E 03	
47	0.0	0.56400000E 03	-0.38500000E 02	
48	0.0	0.56400000E 03	0.56500000E 02	
49	0.0	0.81600000E 03	-0.13050000E 03	
50	0.0	0.81600000E 03	0.13050000E 03	
51	0.0	0.81600000E 03	-0.58500000E 02	
52	0.0	0.81600000E 03	0.58500000E 02	
53	0.0	0.31200000E 03	-0.13050000E 03	
54	0.0	0.31200000E 03	0.13050000E 03	
55	0.0	0.31200000E 03	-0.58500000E 02	
56	0.0	0.31200000E 03	0.58500000E 02	
57	0.0	0.10680000E 04	-0.13050000E 03	
58	0.0	0.10680000E 04	0.13050000E 03	
59	0.0	0.10680000E 04	-0.58500000E 02	
60	0.0	0.10680000E 04	0.58500000E 02	
61	0.0	0.60000000E 02	-0.13050000E 03	
62	0.0	0.60000000E 02	0.13050000E 03	
63	0.0	0.60000000E 02	-0.58500000E 02	
64	0.0	0.60000000E 02	0.58500000E 02	
65	0.0	0.10680000E 04	0.0	
66	0.0	0.60000000E 02	-0.38500000E 03	
67	0.0	0.60000000E 02	0.38500000E 03	
68	0.0	0.60000000E 02	0.0	
69	0.0	0.61600000E 03	0.0	
70	0.0	0.12000000E 02	0.0	
71	0.0	0.31200000E 03	0.0	
72	0.0	0.56400000E 03	0.0	
NO.				
1	0.1617494E 02	0.4037268E 05	0.0	0.0
		0.0	0.3985508E 05	0.0
				0.4373707E 05
2	0.0	0.0	0.0	0.0
		0.0	0.0	0.0
		0.0	0.0	0.0
3	0.1617494E 02	0.4037268E 05	0.0	0.0
		0.0	0.3985508E 05	0.0
				0.4373707E 05
4	0.1617494E 02	0.4037268E 05	0.0	0.0
		0.0	0.3985508E 05	0.0
				0.4373707E 05
5	0.1617494E 02	0.4037268E 05	0.0	0.0
		0.0	0.3985508E 05	0.0
				0.4373707E 05
6	0.5734374E 01	0.1275650E 05	0.0	0.0
		0.0	0.1262940E 05	0.0
				0.6152176E 04
7	0.1746395E 02	0.7893375E 05	0.0	0.0
		0.0	0.7815731E 05	0.0
				0.1630435E 05

INERTIA MATRIX

9	0.1617494E 02	0.4813066E 05	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
10	0.1617494E 02	0.4813066E 05	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
11	0.1617494E 02	0.4813066E 05	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
12	0.1617494E 02	0.4813066E 05	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
13	0.1617494E 02	0.4813066E 05	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
14	0.1617494E 02	0.4813066E 05	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
15	0.1617494E 02	0.4813066E 05	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
16	0.1617494E 02	0.4813066E 05	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.4994825E 05	0.4813066E 05	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
17	0.1252000E 00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
18	0.1252000E 00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
19	0.1252000E 00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
20	0.1252000E 00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
21	0.1252000E 00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
22	0.1252000E 00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
23	0.1252000E 00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0

24	0.1252330E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
25	0.1252000E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
26	0.1252000E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
27	0.1252000E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
28	0.1252000E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
29	0.1394000E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
30	0.1394000E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
31	0.8969998E-01	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
32	0.8969998E-01	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
33	0.8638998E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
34	0.8608998E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
35	0.8219999E-01	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
36	0.8219999E-01	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
37	0.1415000E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
38	0.7873000E 00	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0

39	0.0	0.0	0.0	0.0
40	0.0	0.0	0.0	0.0
41	0.0	0.0	0.0	0.0
42	0.0	0.0	0.0	0.0
43	0.0	0.0	0.0	0.0
44	0.0	0.0	0.0	0.0
45	0.0	0.0	0.0	0.0
46	0.0	0.0	0.0	0.0
47	0.0	0.0	0.0	0.0
48	0.0	0.0	0.0	0.0
49	0.0	0.0	0.0	0.0
50	0.0	0.0	0.0	0.0
51	0.0	0.0	0.0	0.0
52	0.0	0.0	0.0	0.0
53	0.0	0.0	0.0	0.0



69	0.136300E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
70	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
71	0.136300E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
72	0.136300E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

NO. MODES = 0

MODAL MASSES

0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01

FREQUENCIES

0.124926E 01 0.125022E 01 0.134624E 01 0.136240E 01 0.234466E 01 0.234707E 01

MODE 1

MASS NO.	W(1)	W(2)	W(3)	THETA(1)	THETA(2)	THETA(3)
1	0.112169E-05	0.1954213E-09	0.4337428E-12	0.7004989E-15	0.3147705E-08	0.9416048E-06
2	0.9322054E-06	0.2018735E-09	0.4339812E-12	0.338663E-13	0.3147599E-08	0.941551E-06
3	0.742629E-06	0.2130735E-09	0.5204435E-12	0.3956326E-13	0.3147808E-08	0.9379382E-06
4	0.3637016E-06	0.2323529E-09	0.5973097E-13	0.4635154E-12	0.3143388E-08	0.9325913E-06
5	0.1478269E-07	0.1208256E-09	0.1350442E-11	0.8471206E-12	0.3135952E-08	0.9232268E-06
6	0.2036758E-06	0.1190724E-10	0.2783560E-12	0.1100793E-11	0.312721E-08	0.9171530E-06
7	0.8817460E-06	0.6813434E-09	0.2783560E-12	0.1151330E-11	0.2959388E-08	0.8546469E-06
8	0.1515687E-05	0.7928840E-09	0.2753500E-11	0.3852099E-11	0.2727572E-08	0.7920815E-06
9	0.125271E-05	0.2018735E-09	0.3595260E-11	0.3035980E-13	0.3147636E-08	0.9418990E-06
10	0.2383129E-03	0.2018693E-09	0.7601192E-11	0.2041635E-13	0.3147679E-08	0.9421519E-06
11	0.3513941E-03	0.2018615E-09	0.9402971E-11	0.2465237E-13	0.3147710E-08	0.9422759E-06
12	0.4044787E-03	0.2018599E-09	0.1237754E-10	0.2467537E-13	0.3147727E-08	0.9423104E-06
13	0.1233825E-03	0.2018735E-09	0.443333E-11	0.3001926E-13	0.3147638E-08	0.9418974E-06
14	0.2304470E-03	0.2018694E-09	0.9545364E-11	0.2766902E-13	0.3147679E-08	0.9421493E-06
15	0.3495789E-03	0.2018693E-09	0.1042791E-10	0.2623732E-13	0.3147710E-08	0.94227
16	0.4626134E	0.2018693E-09	0.147E-12	0.258907E-13	0.3147727E-08	0.94227
17	0	0	0	0.3852099E-11	0.2727572E-08	0.7920815E-06

BEGINNING OF MODE 1

63	0.4469644E-08	0.1722889E-01	0.497244E	0.6253163E-03	0.630558E-10	0.1551449E-10
64	0.5160094E-08	0.1711935E-01	0.4695884E-03	0.730558E-10	0.1551449E-10	0.1551449E-10
65	0.2580129E-06	0.1725150E-01	0.5605907E-03	0.2362658E-05	0.182453E-06	0.1463672E-09
66	0.1121239E-06	0.1707523E-01	0.9283349E-01	0.3617496E-04	0.5811101E-10	0.1551449E-10
67	0.2791745E-07	0.2236763E-01	0.416682E-03	0.2701022E-04	0.5811101E-10	0.1551449E-10
68	0.5314973E-06	0.1172337E-01	0.8921253E-03	0.2023889E-04	0.491319E-10	0.9366517E-11
69	0.1299967E-09	0.1170510E-01	0.3140959E-03	0.2838043E-03	0.1380699E-10	0.1450980E-09
70	0.7489916E-07	0.1707127E-01	0.7408297E-03	0.1060527E-03	0.124248E-10	0.1551449E-10
71	0.1390774E-10	0.1705060E-01	0.1716629E-03	0.1444727E-04	0.4294827E-09	0.6478306E-10
72	0.1251768E-07	0.1706319E-01	0.1340017E-01	0.9711327E-04	0.4294827E-09	0.6478306E-10
72	0.398930E-07	0.1706725E-01	0.432565E-01	0.1298130E-03	0.4294827E-09	0.6478306E-10

END OF MODE 6

INITIAL CONDITIONS FOR DEFORMATION COORDINATES

MASS	Q(1)	Q(2)	Q(3)
1	0.0	0.0	0.0
2	0.0	0.0	0.0
3	0.0	0.0	0.0
4	0.0	0.0	0.0
5	0.0	0.0	0.0
6	0.0	0.0	0.0
7	0.0	0.0	0.0
8	0.0	0.0	0.0

70	0.0	0.0	0.0
71	0.0	0.0	0.0
72	0.0	0.0	0.0

MASS	Q(1)	Q(2)	Q(3)
1	0.0	0.0	0.0
2	0.0	0.0	0.0
3	0.0	0.0	0.0

72	0.0	0.0	0.0
----	-----	-----	-----

MASS	THETA(1)	THETA(2)	THETA(3)
1	0.0	0.0	0.0
2	0.0	0.0	0.0
3	0.0	0.0	0.0
4	0.0	0.0	0.0
5	0.0	0.0	0.0
6	0.0	0.0	0.0
7	0.0	0.0	0.0
8	0.0	0.0	0.0
9	0.0	0.0	0.0

68	0.0	0.0	0.0
69	0.0	0.0	0.0
70	0.0	0.0	0.0
71	0.0	0.0	0.0
72	0.0	0.0	0.0

MASS	THETA(0)	THETA(1)	THETA(2)
1	0.0	0.0	0.0
2	0.0	0.0	0.0
3	0.0	0.0	0.0
4	0.0	0.0	0.0
5	0.0	0.0	0.0
6	0.0	0.0	0.0
7	0.0	0.0	0.0

65	0.0	0.0	0.0
66	0.0	0.0	0.0
67	0.0	0.0	0.0
68	0.0	0.0	0.0
69	0.0	0.0	0.0
70	0.0	0.0	0.0
71	0.0	0.0	0.0
72	0.0	0.0	0.0

MODAL DAMPING RATIOS
0.2000000E-01 0.2000000E-01 0.2000000E-01 0.2000000E-01 0.2000000E-01 0.2000000E-01

INITIAL CONDITION FOR MAIN LABORATORY COORDINATES

R	=	0.0	0.0	0.528000E 03
XDOT	=	0.0	0.0	0.0
GAMMA	=	0.0	0.0	0.0
WX	=	0.410000E 04	0.0	0.0

FLUID DATA

RFU
A
0.9340000E-04 0.100000E 02
EMPTYING RESERVOIR

FLUID IN RESERVOIR PIPE				INERTIA MATRIX			
MASS							
0.7009494E-01		0.5211230E 03	0.0	0.0		0.0	
		0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.0	0.0

SIPE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
SIRE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
UIR	0.0	0.0	0.0	0.0	0.0	0.0	0.0
JIB	0.0	0.0	0.0	0.0	0.0	0.0	0.0
EIB	0.0	0.0	0.0	0.0	0.0	0.0	0.0

JIB	0.1015179E 06	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.1015179E 06	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0

J1
 0.2500000E 02 0.5000000E 02 0.6000000E 02 0.0
 GPIPE 0.0 HIMAX 0.0
 FILLING RESERVOIR HIMIN 0.0
 FLUID IN RESERVOIR PIPE
 MASS
 0.1401900E-01 0.5010402E 01 0.0 0.0
 0.0 0.0 0.9010422E 01 0.0
 0.0 0.0 0.5346790E-01 0.0
 S PIPE 0.0 -0.5044940E 00
 F I R E 0.0 -0.1000000E 01
 J I R E 0.0 -0.2100000E 02
 U I B E 0.0 0.0 -0.3100000E 02
 E I S E 0.0 0.0 -0.1000000E 01
 J I R 0.1443200E 03 0.0 0.0
 0.0 0.1443200E 03 0.0
 0.0 0.0 0.3000000E 02

3I
 0.2500000E 02 0.2000000E 02 0.6000000E 02 0.0
 GPIPE 0.0 HIMAX 0.0
 FLUID IN PIPE UN MASS NU. 3 HIMIN 0.0
 MASS = 0.1201710E 00
 S = 0.0 0.0 -0.2018736E 01
 DELU= 0.0 0.0 0.9000000E 02
 DELE= 0.0 0.0 0.0
 G = 0.0 0.0 0.0
 DELH= 0.0 0.0 0.0
 DELJ 0.0 0.0 0.0
 -0.4320000E 05 0.0 0.0
 0.0 -0.4320000E 05 0.0
 0.0 0.0 0.0
 INERTIA MATRIX
 0.1170158E 03 0.0 0.0
 0.0 0.1170158E 03 0.0
 0.0 0.0 0.5012111E 00
 FLUID IN PIPE UN MASS NU. 4
 MASS = 2.1682200E 03
 S = 0.0 0.0 -0.1652280E 03
 DELU= 0.0 0.0 0.1200000E 03
 DELE= 0.0 0.0 0.0
 G = 0.0 0.0 0.0
 DELH= 0.0 0.0 0.0
 DELJ 0.0 0.0 0.0
 -0.3000000E 04 0.0 0.0
 0.0 -0.3000000E 04 0.0
 0.0 0.0 0.0
 INERTIA MATRIX
 0.2022426E 03 0.0 0.0
 0.0 0.2022426E 03 0.0
 0.0 0.0 0.4010147E 03

FLUID IN PIPE UN MASS NU. 5
 MASS = 0.1201710E 00
 S = 0.0 0.0 0.1766394E 01
 DELU= 0.0 0.0 0.9000000E 02
 DELE= 0.0 0.0 0.0
 G = 0.0 0.0 0.0

Reproduced from
best available copy.

DELH= 0.0 0.0 0.0
 DELJ 0.0 0.0 0.0
 0.370000E 03 0.0 0.0 0.0
 0.0 0.0 0.0
 0.0 0.0 0.0
 INERTIA MATRIX
 0.1100450E 03 0.0 0.0 0.0
 0.0 0.1100450E 03 0.0 0.0 0.0
 0.0 0.0 0.1100450E 03 0.0 0.0 0.0
 FLUID IN PIPE ON MASS NO. 6
 MASS = 0.196200E 00
 S = 0.0 0.0 0.0
 DELU= 0.0 0.0 0.0
 DELE= 0.0 0.0 0.0
 0.0 0.0 0.0
 DELH= 0.0 0.0 0.0
 DELJ 0.0 0.0 0.0

-0.172000E 00 0.0 0.0
 0.0 -0.172000E 00 0.0 0.0
 0.0 0.0 0.0
 INERTIA MATRIX
 0.6507251E 03 0.0 0.0 0.0
 0.0 0.6507251E 03 0.0 0.0 0.0
 0.0 0.0 0.6507251E 03 0.0 0.0 0.0
 FLUID IN PIPE ON MASS NO. 7
 MASS = 0.306410E 00
 S = 0.0 0.0 0.0
 DELU= 0.0 0.0 0.0
 DELE= 0.0 0.0 0.0
 0.0 0.0 0.0
 DELH= 0.0 0.0 0.0
 DELJ 0.0 0.0 0.0

-0.330000E 04 0.0 0.0
 0.0 -0.330000E 04 0.0 0.0
 0.0 0.0 0.0
 INERTIA MATRIX
 0.1244398E 04 0.0 0.0
 0.0 0.1244398E 04 0.0 0.0
 0.0 0.0 0.1244398E 04 0.0 0.0
 DELH= 0.0 0.0 0.0
 DELJ 0.0 0.0 0.0

COUNTERWEIGHT INPUT
 NO. MASSES = 1
 MASS POINT LOCATIONS
 NO. X(1) Y(1) X(2) Y(2) Y(3)
 1 0.0 0.0 0.0 0.0 0.0
 1 0.1940994E 03 0.1725962E 03 0.0 0.0
 0.0 0.0 0.2344720E 07 0.0
 0.0 0.0 0.1549965E 06
 INERTIA MATRIX
 0.320000E 03 0.0 0.0
 0.0 0.320000E 03 0.0 0.0
 0.0 0.0 0.320000E 03 0.0 0.0
 PHISTARDOT= 0.0 0.0 0.0
 YA= 0.0 0.0 -0.100000E 01
 YB= 0.100000E 01 0.0 0.0

CONNECTING STRUCTURE INPUT
 CONNECTS TO MASSES I= 0 , A= 1
 S = 0.0 0.0
 SBAR = 0.0 0.0
 DEL = 0.0 0.0
 DELDOT= 0.0 0.0
 PHISTARDOT= 0.0 0.0
 YA= 0.0 0.0
 YB= 0.100000E 01 0.0 0.0

DEPLOYMENT INPUT - L0
0.0

0.1689918E 04

PUMP COMMAND INPUT

V
0.6

VELCU
0.1200000E 05

TIMCU
0.2000000E 01

ACCMAG
0.6000000E 02

PLOTTING GROUPS SELECTED FOR THIS RUN
11

NUMERICAL INTEGRATION DATA

DELTA
0.0

STEP
0.5000000E-01

DTAU
0.9997433E-01

NTIME
2

TIME HISTORY

RIGID PROBLEM OUTPUT AT TIME T= 0.0 STEP= 0.49999997E-01

RDDT (R)	X (F)	Y (F)	Z (F)	R (F)	GAM (F)	WY (F)
0.0	0.4168999E 00	0.0	0.14339151E-10	0.0	0.0	0.4188999E 00
0.0	0.0	0.4829200E-05	0.0	0.0	0.0	0.0
0.0	0.0	0.3404372E 01	0.0	0.5200000E 03	0.0	0.0

LOCATION OF CENTER OF MASS IN INERTIAL (Z) COORDINATES

0.0	0.2003130E-04	0.1973087E 02
-----	---------------	---------------

ANGULAR MOMENTUM IN Z- COORDINATES

0.3432394E 09	0.0
---------------	-----

TOTAL KINETIC ENERGY

0.7190120E 00

FLUID DATA V= 0.0 VOUT= 0.0

FLUID HEIGHT IN RES(1)= 0.5000000E 02

FLUID HEIGHT IN RES(2)= 0.2000000E 02

RIGID PROBLEM OUTPUT AT TIME T= 0.14999998E 00 STEP= 0.49999997E-01

RDDT	X	Y	Z	R	GAM	WY
0.0	0.4168999E 00	0.0	-0.4791365E-09	0.0	0.8377993E-01	0.4188999E 00
0.5793090E-01	0.0	0.5791200E 00	0.0	0.3867248E-02	0.0	0.0
0.6904300E 00	0.0	0.3429079E 01	0.0	0.5200000E 03	0.0	0.0

LOCATION OF CENTER OF MASS IN INERTIAL (Z) COORDINATES

0.0	-0.1653731E 01	0.1973921E 02
-----	----------------	---------------

ANGULAR MOMENTUM IN Z- COORDINATES

0.3432390E 09	0.0
---------------	-----

TOTAL KINETIC ENERGY

0.7190123E 00

FLUID DATA V= 0.0 VOUT= 0.0

FLUID HEIGHT IN RES(1)= 0.5000000E 02

FLUID HEIGHT IN RES(2)= 0.2000000E 02

RIGID PROBLEM OUTPUT AT TIME T= 0.59999998E 00 STEP= 0.49999997E-01

RDDT	X	Y	Z	R	GAM	WY
0.0	0.4168999E 00	0.0	-0.2492100E-08	0.0	0.1673080E 00	0.4188999E 00
0.2311091E 00	0.0	0.1150120E 01	0.0	0.3087249E-01	0.0	0.0
0.1366324E 01	0.0	0.3318839E 01	0.0	0.5202751E 03	0.0	0.0

LOCATION OF CENTER OF MASS IN INERTIAL (Z) COORDINATES

0.0 -0.53074423E 01 0.19739624E 02

ANGULAR MOMENTUM IN Z- COORDINATES
0.34328934E 09 0.0

TOTAL KINETIC ENERGY
0.71901264E 03

FLUID DATA V= 0.0 VDOT= 0.0
FLUID HEIGHT IN RES(1)= 0.3000000E 02
FLUID HEIGHT IN RES(2)= 0.2000000E 02

RIGID PROBLEM OUTPUT AT TIME T= 0.59999949E 00 STEP= 0.4999997E-01

RDOT	WX	RDDOT	WDDOT	R	GAM	MY
0.0	0.4188998E 00	0.0	-0.3004749E-08	0.0	0.2513397E 00	0.4188998E 00
0.5169525E 00	0.0	0.17049513E 01	0.0	0.1038267E 00	0.0	0.0
0.2013283E 01	0.0	0.3138928E 01	0.0	0.5286133E 01	0.0	0.0

LOCATION OF CENTER OF MASS IN INERTIAL (Z) COORDINATES

0.0 -0.4961104E 01 -0.1973963E 02

ANGULAR MOMENTUM IN Z- COORDINATES
0.3432893E 09 0.0

TOTAL KINETIC ENERGY
0.7190126E 03

FLUID DATA V= 0.0 VDOT= 0.0
FLUID HEIGHT IN RES(1)= 0.3000000E 02
FLUID HEIGHT IN RES(2)= 0.2000000E 02

RIGID PROBLEM OUTPUT AT TIME T= 0.79999930E 00 STEP= 0.4999997E-01

RDOT	WX	RDDOT	WDDOT	R	GAM	MY
0.0	0.4188998E 00	0.0	-0.1121332E-08	0.0	0.3351197E 00	0.4188998E 00
0.9114609E 00	0.0	0.0	0.2489028E 00	0.0	0.0	0.0
0.201722E 01	0.0	0.5290776E 03	0.0	0.0	0.0	0.0

•
•
•

Example 2

The time-history printout for this problem, where the vehicle is flexible, includes the connecting-structure deformations $\{\delta\}$ and $\{\phi^*\}$ as well as the main variables. Elastic deformations are also printed at each mass point requested. In addition, internal structural loads are printed at the requested points. As discussed in Section 4.5 of Volume I, the internal loads are inaccurate at $t = 0$. These loads have been deleted from the printout at $t = 0$; however, this modification was done after making the run on the example presented. After completing the time history, a tabulation is printed of the maximum and minimum (or largest negative) elastic motions that occurred during the run at every mass point. Also, the maximum and minimum internal structural loads are printed at only those points where loads were requested in the input data. The maxima and minima for both deformations and loads are obtained by examining the data at every print-out time point and not at every numerical-integration time point.

INPUT DATA

FINAL TIME, PLOTTING CLUE, PLOT INTERVAL
 0.1000000E-02 1 0.5000000E-01

FLUID CLUE, NO. PIPES
 0 0

RESERVOIR MASS POINTS
 0

NC. MOVING MASSES, MOVING MASSES PRESENT
 2 1 0 0 0 0 0 0

PIPES ON MASS POINTS
 0

CLUES FOR THIS RUN
 PEOPLEM CLUE, DEPLOYMENT, CONTROLS, SUPP. FORCES
 3 1 0

CONTROLS INPUT, SENSO ON MASS POINT 4, FJET= 0.50000000E 02

COUNTERWEIGHT COMMAND

LENGTH UPDATE TIME-DE UPDATE ACCEL-MAG VEL-MAX
 0.1685016E 04 0.3300000E 03 0.1200000E 01 0.2400000E 01

SPIN COMMAND

ANG-VEL-COMMAND ANG-VEL-UPDATE ACCEL MAG TIME OF UPDATE
 0.4189000E 00 -0.4189000E 00 0.4000000E-01 0.9500000E 03

SPIN CONTROL

SPIN RATE ERROR DEAD-BAND= 0.2000000E-03

ATTITUDE CONTROL

DEAD BAND MAX. ANG. VEL. JET MOMENT ARM

0.1745000E-03 0.1750000E-02 0.7200000E-02

MOBILE DAMPING

RET DBET KT TGLTM KDBET MOMCMG GIMBAL INERTIA
 0.0 -0.1130000E 00 0.2880000E-04 0.3600000E-03 0.3600000E-03 0.2400000E-04 0.1800000E 03

LOADS COMPUTED ON LABORATORY

LOAD TO BE COMPUTED AT MASS POINT 4

LOCATION IN LOCAL COORDINATES 0.0 0.0 0.6000000E 02

11 MASS POINT NUMBERS COMPRISING FREE BODY

1 2 3 4 5 10 11 12 13 14 15 16

LOAD TO BE COMPUTED AT MASS POINT 42

LOCATION IN LOCAL COORDINATES 0.0 0.0 0.0

27 MASS POINT NUMBERS COMPRISING FREE BODY

17 18 19 20 21 22 23 24 25 27 28 29 30 31 32 33 34 35 36 37

38 39 40 41 42 43 44

LAR INPUT

NO. MASSES = 72

MASS POINT LOCATIONS

NO.	X(1)	X(2)	X(3)
1	0.0	0.0	0.86100000E 03
2	0.0	0.0	0.80100000E-03
3	0.0	0.0	0.74100000E 03
4	0.0	0.0	0.52100000E 03
5	0.0	0.0	0.50100000E-03
	0.0	0.0	0.44100000E-03

59	0.0				
60	0.0				
61	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
62	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
63	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
64	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
65	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
66	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
67	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
68	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
69	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
70	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
71	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02
72	0.0	0.6000000E 02	0.6000000E 02	0.6000000E 02	0.6000000E 02

INERTIA MATRIX

NO.	1	0.161749E 02	0.403726E 05	0.0	0.0
		0.0	0.398550E 05	0.0	0.0
		0.0	0.0	0.437370E 05	0.0

2	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0

71	0.138300E 00	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0

72	0.138300E 00	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0

NO. MODES - 6
 MODAL MASSES
 0.100000E 01 0.120000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01
 FREQUENCIES
 0.1249565E 01 0.1250221E 01 0.1146283E 01 0.1162402E 01 0.2394608E 01 0.2397697E 01
 MODE 1
 MASS NO. Q(1) Q(2) Q(3) THETA(1) THETA(2) THETA(3)
 1 0.1121143E-03 0.1254213E-03 0.4337425E-12 0.7004969E-15 0.3147705E-09 0.9416044E-04
 2 0.9122254E-04 0.2018765E-03 0.4339812E-12 0.3386963E-13 0.3147599E-08 0.9415951E-06
 3 0.7426522E-06 0.2130753E-09 0.5264435E-12 0.4956325E-13 0.3147065E-08 0.9370000
 4 0.7637010E-06 0.1632047E-06 0.4635154E-12 0.4635154E-12 0.3143456E-08
 5 0.7637010E-06 0.1632047E-06 0.4635154E-12 0.4635154E-12 0.3135952E-08

Reproduced from
 best available copy.

BEGINNING OF
 MODE 1

0.5270955E-01 0.1437958E-01 0.2914850E-01 0.5264169E 00 -0.1444723E-04
 0.3095317E-07 0.1556610E-01 0.5266610E 00 -0.1444727E-04
 0.7029549E-07 0.1146001E-01 0.5266610E 00 -0.1444727E-04
 0.2142737E-05 0.11639250E-01 0.4632576E 00 -0.1444727E-04
 0.1529314E-04 0.1818882E-01 0.4624734E 00 -0.1444727E-04
 0.1144445E-06 0.1655221E-01 0.4631166E 00 -0.1444727E-04
 0.5011299E-07 0.1722273E-01 0.4627649E 00 -0.1444727E-04
 0.7501234E-04 0.1731243E-01 0.9294941E-01 0.2469415E-04 -0.1824961E-08
 0.1260770E-03 0.2104078E-01 0.9284961E-01 0.2713878E-04 0.1824937E-08 -0.1551449E-10
 0.2187583E-03 0.1510410E-01 0.9284228E-01 0.2901509E-04 0.1824721E-08 -0.1551449E-10
 0.5306570E-03 0.1306552E-01 0.9284228E-01 0.3052253E-04 0.1824813E-08 -0.1551449E-10
 0.4067134E-08 0.1732840E-01 0.4670424E-03 -0.9617927E-05 0.7359133E-10 -0.1551449E-10
 0.4469444E-08 0.1711945E-01 0.6253163E-03 -0.7375049E-05 0.1916231E-10 -0.1551449E-10
 0.3160954E-04 0.1602632E-01 0.4495844E-01 0.7399445E-06 0.6230658E-10 -0.1551449E-10
 0.2580129E-08 0.1725150E-01 0.5605407E-03 0.2362654E-05 0.3459513E-10 -0.1551449E-10
 0.1121210E-05 0.1707523E-01 0.9283549E-01 0.3617496E-04 0.1824555E-08 0.1481672E-09
 0.2312445E-07 0.2238763E-01 0.4176642E-03 -0.2701022E-04 -0.8411104E-10 -0.1551449E-10
 0.5314570E-09 0.1172557E-01 0.8651293E-03 -0.7023889E-04 -0.4024672E-11 0.1551449E-10
 0.1299567E-09 0.1705910E-01 0.5140959E-03 0.2938043E-05 0.4013193E-10 0.9065517E-11
 0.7488916E-07 0.1707127E-01 0.7408267E-01 0.1060527E-03 0.1390698E-08 0.1450980E-09
 0.1302344E-10 0.1705640E-01 0.4716629E-03 -0.1444725E-04 -0.1245948E-10 -0.1551449E-10
 0.1251749E-07 0.1706310E-01 0.1340017E-01 0.9711325E-04 0.4920892E-09 0.9478308E-10
 0.3089395E-07 0.1706725E-01 0.4325256E-01 0.1208130E-03 0.9368435E-09 0.1279185E-09

END OF
 MODE 6

INITIAL CONDITIONS FOR DEFORMATION COORDINATES

MASS	q(1)	q(2)	q(3)
1	-0.8395952E-03	0.1661246E-06	-0.2366700E 00
2	0.4631341E-07	0.5913490E-07	-0.2366645E 00
3	-0.9210182E-07	-0.1193839E-06	-0.2366175E-00
4	-0.1178544E-05	-0.1319694E-06	-0.2365184E 00
5	-0.1484652E-06	-0.3020286E-06	-0.2364259E 00
6	-0.1198316E-06	-0.4576431E-06	-0.2363781E-00
7	-0.2665172E-05	-0.6919755E-05	-0.2363781E 00
8	-0.2809310E-05	-0.9918432E-06	-0.2363781E 00
9	-0.5800594E-07	-0.5807669E-07	-0.2362905E-00
10	0.7176317E-07	0.5800939E-07	-0.2368985E 00
11	0.8550951E-07	0.5793117E-07	-0.2370944E 00
12	0.9845075E-07	0.5790207E-07	-0.2372898E-00
13	0.3532824E-07	0.5810580E-07	-0.2367302E 00
14	0.2470910E-07	0.5809125E-07	-0.2368993E 00
15	0.1354361E-07	0.5807669E-07	-0.2370956E-00
16	0.3634133E-03	0.5903304E-07	-0.2372914E 00
17	-0.7231311E-05	-0.1202033E 00	0.2135449E 02
18	-0.5207304E-05	-0.1201248E-00	0.2132310E 02
19	-0.3529372E-05	-0.5963879E-01	0.2134869E 02
20	0.2046355E-05	0.5955905E-01	0.2133441E 02
21	0.1103813E-05	-0.1515666E-00	0.1519842E 02
22	-0.3630829E-05	0.1514618E 00	0.1677711E 02
23	-0.4252430E-05	-0.7359689E-01	0.1679433E 02
24	-0.2591304E-05	0.7347929E-01	0.1678477E 02
25	-0.7332229E-05	-0.9858991E-01	0.1444334E 02
26	0.9339995E-05	0.9857775E-01	0.1441859E 02
27	-0.2740235E-05	-0.4557602E-01	0.1443489E-02
28	0.4720495E-05	0.4550719E-01	0.1442779E 02
29	0.6501295E-05	-0.1826136E 00	0.3220690E 01
30	-0.4594545E-05	-0.1824826E-00	0.3220690E-01
31	0.3445357E-05	-0.8740133E-01	0.3220455E 01
32	-0.1572399E-05	0.8724976E-01	0.3220455E 01
33	0.7645373E-05	-0.5679414E-01	-0.2236958E-00
34	-0.6202392E-05	0.5676814E-01	-0.2287396E 00
35	0.1296652E-06	-0.3136164E-01	-0.2244118E 00
36	-0.4913260E-06	0.3136579E-01	-0.2266729E-00
37	0.9573257E-05	-0.7926005E-04	0.3220241E 01
38	0.3625659E-05	-0.1209540E-05	-0.2221182E 00
39	-0.2667364E-06	-0.5744660E-06	-0.2363778E-00
40	-0.2509854E-05	-0.4601184E-05	-0.2231878E 00
41	0.7949726E-06	-0.6059759E-04	0.2509081E 01
42	-0.2903305E-06	-0.8918432E-06	-0.2363780E-00
43	0.1273315E-05	-0.2326749E-04	0.3377636E 00
44	0.5176919E-05	-0.4193319E-04	0.1410043E 01
45	-0.7408443E-06	0.1202018E 00	0.2135451E 02
46	0.6808415E-05	-0.1201266E 00	0.2132318E 02
47	-0.3202865E-05	0.5963711E-01	0.2134871E 02
48	0.3171558E-05	-0.5955705E-01	0.2133467E 02
49	-0.7559095E-06	0.1515652E 00	0.1679951E 02
50	0.5793919E-05	-0.1514639E 00	0.1677719E 02
51	-0.7095765E-06	-0.7359523E-01	0.1679439E 02
52	-0.1175594E-06	-0.7348114E-01	0.1679484E 02
53	-0.3427355E-05	0.8858836E-01	0.1444337E 02

Reproduced from
Best available copy.

54	C.5502118E-05	-0.49853054E-01	0.1441861E 02
55	C.926169E-05	-0.4555555E-01	0.1443903E-02
56	C.211939E-05	-0.455007E-01	0.142782E 02
57	C.920535E-05	0.1926124E 00	0.3220695E 01
58	C.1569366E-05	0.1924448E-02	0.3220695E 01
59	C.5095555E-05	0.4739978E-01	0.3220661E 01
60	C.1582991E-05	-0.4725178E-01	0.3220661E 01
61	C.8681914E-05	0.5679925E-01	0.2936959E-00
62	C.6679573E-05	-0.5676070E-01	-0.2287397E 00
63	C.1678249E-05	0.1137022E-01	-0.2244119E 00
64	C.5226065E-05	0.7136751E-01	0.2266330E-00
65	C.1755463E-05	0.7745378E-01	0.3220245E 01
66	C.400253E-05	-0.1209540E-05	-0.2221183E 00
67	C.2755765E-05	0.5744440E-04	0.2363780E-00
68	C.254303E-05	0.2918385E-05	-0.225180E 00
69	C.120129E-05	0.5851980E-04	0.2509086E 01
70	C.891901E-05	0.491842E-05	0.2363780E-00
71	C.1995687E-05	0.2148640E-04	0.3377637E 00
72	C.770265E-05	0.4015378E-04	0.1410045E 01
MASS	ODT(1)	ODT(2)	ODT(3)
1	C.C	C.C	0.0
2	C.C	0.0	0.0
3	C.C	C.C	0.0
4	C.C	C.C	0.0
5	C.C	0.0	0.0
6	C.C	C.C	0.0
7	C.C	C.C	0.0
8	C.C	0.0	0.0
9	C.C	0.0	0.0
10	C.C	0.0	0.0
11	C.C	0.0	0.0
12	C.C	C.C	0.0
13	C.C	C.C	0.0
14	C.C	0.0	0.0
15	C.C	0.0	0.0
16	C.C	0.0	0.0
17	C.C	0.0	0.0
18	C.C	0.0	0.0
19	C.C	0.0	0.0
20	C.C	0.0	0.0
	C.C	0.0	0.0
	C.C	0.0	0.0
	C.C	0.0	0.0

MASS	THETA(1)	THETA(2)	THETA(3)
57			
58	0.0		
59	0.0		
60	0.0	0.0	0.0
61	0.0	0.0	0.0
62	0.0	0.0	0.0
63	0.0	0.0	0.0
64	0.0	0.0	0.0
65	0.0	0.0	0.0
66	0.0	0.0	0.0
67	0.0	0.0	0.0
68	0.0	0.0	0.0
69	0.0	0.0	0.0
70	0.0	0.0	0.0
71	0.0	0.0	0.0
72	0.0	0.0	0.0
73			
74			
75			
76			
77			
78			
79			
80			
81			
82			
83			
84			
85			
86			
87			
88			
89			
90			
91			
92			
93			
94			
95			
96			
97			
98			
99			
100			
101			
102			
103			
104			
105			
106			
107			
108			
109			
110			
111			
112			
113			
114			
115			
116			
117			
118			
119			
120			
121			
122			
123			
124			
125			
126			
127			

28	-0.8604365E-09	0.5362749E-10	0.7363289E-10
29	-0.1281719E-02	-0.4254521E-07	-0.7363289E-10
30	-0.1281719E-02	-0.4254521E-07	0.7363289E-10
31	-0.1423743E-02	-0.4254476E-07	0.7363289E-10
32	-0.1403995E-02	-0.4255582E-07	0.7363289E-10
33	-0.1694103E-03	-0.0888488E-09	0.7363289E-10
34	-0.1893227E-03	-0.7001641E-09	0.7363289E-10
35	-0.0664555E-03	0.7635203E-09	0.7363289E-10
36	-0.4862673E-03	-0.2084175E-08	0.7363289E-10
37	-0.1504659E-02	-0.4254733E-07	0.5509802E-09
38	-0.4410322E-03	0.1365193E-07	0.7363289E-10
39	-0.4516561E-03	0.2573689E-08	0.7363289E-10
40	-0.5521697E-03	-0.5304226E-09	0.1223641E-08
41	-0.3432349E-02	0.3223701E-07	0.8271770E-09
42	-0.8604385E-09	0.5762749E-10	0.7363289E-10
43	-0.3576254E-02	-0.1461517E-07	0.1639233E-08
44	-0.4699879E-03	0.3392668E-07	0.1370312E-08
45	-0.8604385E-09	0.5362749E-10	0.7363289E-10
46	-0.8604385E-09	0.5362749E-10	0.7363289E-10
47	-0.8604385E-09	0.5362749E-10	0.7363289E-10
48	-0.8604385E-09	0.5362749E-10	0.7363289E-10
49	-0.8604385E-09	0.5362749E-10	0.7363289E-10
50	-0.8604385E-09	0.5362749E-10	0.7363289E-10
51	-0.8604385E-09	0.5362749E-10	0.7363289E-10
52	-0.8604385E-09	0.5362749E-10	0.7363289E-10
53	-0.8604385E-09	0.5362749E-10	0.7363289E-10
54	-0.8604385E-09	0.5362749E-10	0.7363289E-10
55	-0.8604385E-09	0.5362749E-10	0.7363289E-10
56	-0.8604385E-09	0.5362749E-10	0.7363289E-10
57	0.1281719E-02	-0.5708207E-07	0.7363289E-10
58	0.1282033E-02	-0.5709472E-07	0.7363289E-10
59	0.1403747E-02	-0.5707930E-07	0.7363289E-10
60	0.1403559E-02	-0.5709902E-07	0.7363289E-10
61	0.1894034E-03	-0.108076E-07	0.7363289E-10
62	-0.1893244E-03	0.8017556E-09	0.7363289E-10
63	0.4864361E-03	-0.9446516E-09	0.7363289E-10
64	0.4862666E-03	-0.3345408E-08	0.7363289E-10
65	-0.1606641E-02	0.5707654E-07	0.1749960E-08
66	-0.4518573E-03	-0.1427479E-07	0.7363289E-10
67	-0.4516522E-03	0.2668927E-09	0.7363289E-10
68	-0.6216405E-03	-0.560273E-08	-0.1274439E-08
69	0.3833505E-02	-0.4428439E-07	-0.1936872E-08
70	-0.8604385E-09	0.5362749E-10	0.7363289E-10
71	-0.3576254E-02	-0.1461517E-07	0.2167261E-08
72	0.4609390E-02	-0.3149027E-07	-0.2252870E-08

MASS	IMEIADJ(I)	IMEIADJ(2)	IMEIADJ(3)
1	0.0	0.0	0.0
2	0.0	0.0	0.0
4	0.0	0.0	0.0

•
•
•

61 0.0
 62 0.0
 63 0.0
 64 0.0
 65 0.0
 66 0.0
 67 0.0
 68 0.0
 69 0.0
 70 0.0
 71 0.0
 72 0.0

MODAL DAMPING RATIOS
 0.2000000E-01 0.3000000E-01 0.2000000E-01 0.2000000E-01 0.2000000E-01

INITIAL CONDITION FOR MAIN LABORATORY COORDINATES

R = 0.0 0.0 0.0 0.4364841F 03
 ROT = 0.0 0.0 0.0 0.0
 GAMMA = 0.0 0.0 0.0
 WX = 0.4189000E 00 0.0 0.0

MASS MU(J) OF EACH MOVING MASS
 0.2597001F 02 0.1230000E 02 0.0 0.0 0.0 0.0 0.0 0.0

COUNTERWEIGHT INPUT
 NO. MASSES = 1
 MASS COORDINATE LOCATIONS

NO.	MASS	Y(1)	Y(2)	Y(3)
1	0.0	0.0	0.0	0.3200000E 03
1	0.1940594E 03	0.1725992E 08	0.2344720E 07	0.0

INERTIA MATRIX
 0.0 0.0 0.0
 0.0 0.0 0.0
 0.0 0.0 0.0

CONNECTING STRUCTURE INPUT

CONNECT TO MASSES I-J-A-E
 S = 0.0 0.0 0.0
 SRAP = 0.0 0.0 0.0
 DEL ROT = 0.0 0.0 0.0
 PHISTAP = 0.0 0.0 0.0
 PHISTAROT = 0.0 0.0 0.0
 YA = 0.0 0.0 0.0
 YB = 0.1000000E 01 0.0 0.0

DEPLOYMENT INPUT - L3

C.C. 0.0 0.1485916E 04

MUCOM INPUT FOR MOVING MASS I
UJ = 0.0 0.0 0.76212939E 03
AXIS = 2

UU TU ACCMAG VELMAX
0.73062919E 03 0.2030000E 01 0.2000000E 02 0.4000000E 02

BALANCE MASS CONTROL INPUT

EL MASS EST KEXSF KDESE FILTER TIME CONST OMEGA BAL (MIN)
0.1224000E 02 0.1000000E 02 0.7440000E 00 0.0 0.4000000E 00

LOCAL SENSOR COINPS = 0.0
DIST CM TO SENSOR CANOE = 0.0 0.0 0.1057289E 04

U2D INITIAL = 0.0
U2D INITIAL = 0.0 0.0 0.3495181E 03 0.0

BEAM SUPPORTING INPUT

CWT MASS LAB MASS CWT TRANS INRTA LAB TRANS INPTA CWT ROLL INRTA LAB ROLL INRTA
0.1040000E 03 0.2490540E 03 0.1725600E 08 0.3860250E 08 0.1549550E 08 0.1829829E 08

0.6242578E 03 0.3200000E 03 0.3000000E 08 0.1357000E 12 0.1085000E 12

AXIAL DAMPING RATIO BENDING DAMPING RATIO TORSION DAMPING RATIO
0.5000000E 01 0.5000000E 01 0.5000000E 01

PLOTTING GROUPS SELECTED FOR THIS RUN

- 2
- 3
- 4 AT MASS NO. 4
- 7 AT MASS NO. 8
- 8 AT MASS NO. 17
- 10
- 12 AT MASS NO. 42

NUMERICAL INTEGRATION DATA

DELTA EPSIL STEP CTAU NTIME
0.0 0.0 0.5000000E 01 0.3097433E 01 2

TIME HISTORY

TIME 0.0	STEP 0.400000997E-01	DELPRD (iARi)		DEL (iS)		DELPRD (iARi)		DEL (iS)		DELPRD (iARi)		DEL (iS)		DELPRD (iARi)		DEL (iS)	
		DELPRD (iARi)	DEL (iS)	DELPRD (iARi)	DEL (iS)	DELPRD (iARi)	DEL (iS)	DELPRD (iARi)	DEL (iS)	DELPRD (iARi)	DEL (iS)	DELPRD (iARi)	DEL (iS)	DELPRD (iARi)	DEL (iS)	DELPRD (iARi)	DEL (iS)
1	0.1861835E-08	0.4189000E-08	0.2928215E-06	-0.2408847E-08	0.1683645E-08	0.4189000E-08	0.2928215E-06	-0.2408847E-08	0.1683645E-08	0.4189000E-08	0.2928215E-06	-0.2408847E-08	0.1683645E-08	0.4189000E-08	0.2928215E-06	-0.2408847E-08	0.1683645E-08
2	0.1475933E-05	0.1691727E-05	0.1691727E-05	0.1691727E-05	0.3699243E-09	0.1475933E-05	0.1691727E-05	0.1691727E-05	0.3699243E-09	0.1475933E-05	0.1691727E-05	0.1691727E-05	0.3699243E-09	0.1475933E-05	0.1691727E-05	0.1691727E-05	0.3699243E-09
3	0.226441E-04	0.3244162E-10	0.3009434E-01	0.3009434E-01	0.1257904E-11	0.226441E-04	0.3244162E-10	0.3009434E-01	0.1257904E-11	0.226441E-04	0.3244162E-10	0.3009434E-01	0.1257904E-11	0.226441E-04	0.3244162E-10	0.3009434E-01	0.1257904E-11
4	0.11081153E-05	0.99411352E-07	0.29773384E-08	0.0	0.15605361E-08	0.11081153E-05	0.99411352E-07	0.29773384E-08	0.0	0.15605361E-08	0.11081153E-05	0.99411352E-07	0.29773384E-08	0.0	0.15605361E-08	0.11081153E-05	0.99411352E-07
5	0.2503651E-07	0.13052158E-06	0.56437699E-09	0.0	0.43944604E-09	0.2503651E-07	0.13052158E-06	0.56437699E-09	0.0	0.43944604E-09	0.2503651E-07	0.13052158E-06	0.56437699E-09	0.0	0.43944604E-09	0.2503651E-07	0.13052158E-06
6	0.2365301E-09	0.25612544E-09	0.39324268E-09	0.0	0.30810376E-09	0.2365301E-09	0.25612544E-09	0.39324268E-09	0.0	0.30810376E-09	0.2365301E-09	0.25612544E-09	0.39324268E-09	0.0	0.30810376E-09	0.2365301E-09	0.25612544E-09
7	0.1401043E-05	0.2030465E-06	0.2408847E-08	0.0	0.90813046E-09	0.1401043E-05	0.2030465E-06	0.2408847E-08	0.0	0.90813046E-09	0.1401043E-05	0.2030465E-06	0.2408847E-08	0.0	0.90813046E-09	0.1401043E-05	0.2030465E-06
8	0.23637590E-00	0.25999127E-00	0.60970701E-10	0.0	0.47681206E-10	0.23637590E-00	0.25999127E-00	0.60970701E-10	0.0	0.47681206E-10	0.23637590E-00	0.25999127E-00	0.60970701E-10	0.0	0.47681206E-10	0.23637590E-00	0.25999127E-00
9	0.6024672E-07	0.4746762E-07	0.1498864E-05	0.0	0.14342813E-05	0.6024672E-07	0.4746762E-07	0.1498864E-05	0.0	0.14342813E-05	0.6024672E-07	0.4746762E-07	0.1498864E-05	0.0	0.14342813E-05	0.6024672E-07	0.4746762E-07
10	0.49808521E-05	0.86902174E-07	0.49291326E-09	0.0	0.36150327E-09	0.49808521E-05	0.86902174E-07	0.49291326E-09	0.0	0.36150327E-09	0.49808521E-05	0.86902174E-07	0.49291326E-09	0.0	0.36150327E-09	0.49808521E-05	0.86902174E-07
11	0.23725080E-00	0.22686291E-00	0.95899830E-10	0.0	0.18735555E-10	0.23725080E-00	0.22686291E-00	0.95899830E-10	0.0	0.18735555E-10	0.23725080E-00	0.22686291E-00	0.95899830E-10	0.0	0.18735555E-10	0.23725080E-00	0.22686291E-00
12	0.81005576E-09	0.40796206E-07	0.15050719E-05	0.0	0.14376565E-05	0.81005576E-09	0.40796206E-07	0.15050719E-05	0.0	0.14376565E-05	0.81005576E-09	0.40796206E-07	0.15050719E-05	0.0	0.14376565E-05	0.81005576E-09	0.40796206E-07
13	0.4082317E-05	0.86933142E-07	0.48376259E-09	0.0	0.36231529E-09	0.4082317E-05	0.86933142E-07	0.48376259E-09	0.0	0.36231529E-09	0.4082317E-05	0.86933142E-07	0.48376259E-09	0.0	0.36231529E-09	0.4082317E-05	0.86933142E-07
14	0.23725080E-00	0.22686291E-00	0.95899830E-10	0.0	0.18735555E-10	0.23725080E-00	0.22686291E-00	0.95899830E-10	0.0	0.18735555E-10	0.23725080E-00	0.22686291E-00	0.95899830E-10	0.0	0.18735555E-10	0.23725080E-00	0.22686291E-00
15	0.72403419E-05	0.73594128E-05	0.2408847E-08	0.0	0.90813046E-09	0.72403419E-05	0.73594128E-05	0.2408847E-08	0.0	0.90813046E-09	0.72403419E-05	0.73594128E-05	0.2408847E-08	0.0	0.90813046E-09	0.72403419E-05	0.73594128E-05
16	0.1202043E-00	0.11490214E-00	0.53537313E-10	0.0	0.47681206E-10	0.1202043E-00	0.11490214E-00	0.53537313E-10	0.0	0.47681206E-10	0.1202043E-00	0.11490214E-00	0.53537313E-10	0.0	0.47681206E-10	0.1202043E-00	0.11490214E-00
17	0.2135447E-02	0.20416153E-02	0.60970701E-10	0.0	0.14672976E-11	0.2135447E-02	0.20416153E-02	0.60970701E-10	0.0	0.14672976E-11	0.2135447E-02	0.20416153E-02	0.60970701E-10	0.0	0.14672976E-11	0.2135447E-02	0.20416153E-02
18	0.6109347E-05	0.50008830E-05	0.2408847E-08	0.0	0.90813046E-09	0.6109347E-05	0.50008830E-05	0.2408847E-08	0.0	0.90813046E-09	0.6109347E-05	0.50008830E-05	0.2408847E-08	0.0	0.90813046E-09	0.6109347E-05	0.50008830E-05
19	0.12012416E-00	0.11494629E-00	0.53537313E-10	0.0	0.47681206E-10	0.12012416E-00	0.11494629E-00	0.53537313E-10	0.0	0.47681206E-10	0.12012416E-00	0.11494629E-00	0.53537313E-10	0.0	0.47681206E-10	0.12012416E-00	0.11494629E-00
20	0.21323090E-02	0.20386169E-02	0.60970701E-10	0.0	0.14672976E-11	0.21323090E-02	0.20386169E-02	0.60970701E-10	0.0	0.14672976E-11	0.21323090E-02	0.20386169E-02	0.60970701E-10	0.0	0.14672976E-11	0.21323090E-02	0.20386169E-02
21	0.64937143E-05	0.55211567E-05	0.12817162E-02	0.0	0.12253944E-02	0.64937143E-05	0.55211567E-05	0.12817162E-02	0.0	0.12253944E-02	0.64937143E-05	0.55211567E-05	0.12817162E-02	0.0	0.12253944E-02	0.64937143E-05	0.55211567E-05
22	0.14251455E-00	0.1745945E-00	0.42545302E-07	0.0	0.36050906E-07	0.14251455E-00	0.1745945E-00	0.42545302E-07	0.0	0.36050906E-07	0.14251455E-00	0.1745945E-00	0.42545302E-07	0.0	0.36050906E-07	0.14251455E-00	0.1745945E-00
23	0.2206699E-01	0.20791693E-01	0.60970701E-10	0.0	0.14672976E-11	0.2206699E-01	0.20791693E-01	0.60970701E-10	0.0	0.14672976E-11	0.2206699E-01	0.20791693E-01	0.60970701E-10	0.0	0.14672976E-11	0.2206699E-01	0.20791693E-01
24	0.46122295E-05	0.44118251E-05	0.12820312E-02	0.0	0.12256999E-02	0.46122295E-05	0.44118251E-05	0.12820312E-02	0.0	0.12256999E-02	0.46122295E-05	0.44118251E-05	0.12820312E-02	0.0	0.12256999E-02	0.46122295E-05	0.44118251E-05
25	0.14251455E-00	0.1745945E-00	0.42545302E-07	0.0	0.36050906E-07	0.14251455E-00	0.1745945E-00	0.42545302E-07	0.0	0.36050906E-07	0.14251455E-00	0.1745945E-00	0.42545302E-07	0.0	0.36050906E-07	0.14251455E-00	0.1745945E-00
26	0.2206699E-01	0.20791693E-01	0.60970701E-10	0.0	0.14672976E-11	0.2206699E-01	0.20791693E-01	0.60970701E-10	0.0	0.14672976E-11	0.2206699E-01	0.20791693E-01	0.60970701E-10	0.0	0.14672976E-11	0.2206699E-01	0.20791693E-01
27	0.74036248E-05	0.82263737E-05	0.2408847E-08	0.0	0.90813046E-09	0.74036248E-05	0.82263737E-05	0.2408847E-08	0.0	0.90813046E-09	0.74036248E-05	0.82263737E-05	0.2408847E-08	0.0	0.90813046E-09	0.74036248E-05	0.82263737E-05
28	0.1202043E-00	0.11490214E-00	0.53537313E-10	0.0	0.47681206E-10	0.1202043E-00	0.11490214E-00	0.53537313E-10	0.0	0.47681206E-10	0.1202043E-00	0.11490214E-00	0.53537313E-10	0.0	0.47681206E-10	0.1202043E-00	0.11490214E-00
29	0.21354523E-02	0.20416214E-02	0.60970701E-10	0.0	0.14672976E-11	0.21354523E-02	0.20416214E-02	0.60970701E-10	0.0	0.14672976E-11	0.21354523E-02	0.20416214E-02	0.60970701E-10	0.0	0.14672976E-11	0.21354523E-02	0.20416214E-02

PHISTAR (iP*)

DELDOT (iS)

DEL (iS)

WYDET (iW*)

DELPRD (iARi)

DEL (iS)

PHISTARDOT (iP*)

ETA-STAR (iP*)

WY (iW*)

DELPRD (iARi)

DEL (iS)

WYDET (iW*)

DELPRD (iARi)

DEL (iS)

PHISTARDOT (iP*)

PHISTARDOT (iP*)

ETA-STAR (iP*)

WY (iW*)

DELPRD (iARi)

DEL (iS)

WYDET (iW*)

DELPRD (iARi)

DEL (iS)

PHISTARDOT (iP*)

PHISTARDOT (iP*)

ETA-STAR (iP*)

WY (iW*)

DELPRD (iARi)

DEL (iS)

WYDET (iW*)

DELPRD (iARi)

DEL (iS)

PHISTARDOT (iP*)

PHISTARDOT (iP*)

46 0.6813433E-05 0.0 0.58284531E-05 -0.24088471E-08 0.0 0.90813046E-09
 -0.12012714E 00 0.0 0.11484826E 00 0.53537313E-10 0.0 0.47681206E-10
 0.2132316E 02 0.0 0.20386230E 02 0.60970701E-10 0.0 -0.14672976E-11

57 0.92170285E-05 0.0 0.71661334E-05 0.12817169E-02 0.0 -0.12253982E-02
 0.18261129E 00 0.0 0.17459808E 00 -0.57082158E-07 0.0 0.5198936E-07
 0.32205917E 01 0.0 0.30791750E 01 -0.60970701E-10 0.0 -0.14672976E-11

58 -0.56820735E-05 0.0 0.64043752E-05 0.12820312E-02 0.0 -0.12253982E-02
 0.18261129E 00 0.0 0.17459808E 00 -0.57082158E-07 0.0 0.5198936E-07
 0.32205917E 01 0.0 0.30791750E 01 -0.60970701E-10 0.0 -0.14672976E-11

LOCATION OF CENTER OF MASS IN INERTIAL (Z) COORDINATES
 -0.15045665E-05 0.1519278E-04 -0.20995449E-01

ANGULAR MOMENTUM IN Z- COORDINATES
 0.36072269E 09 0.51022421F-03 -0.51476635E-01

TOTAL KINETIC ENERGY
 0.755280E 03

STRUCTURAL LOADS APPLIED BY CONNECTING STRUCTURE (CN LAB IN X AXES AND ON CMT IN Y AXES)

ON LAB	ON CMT	FORCE	TORQUE
-0.2866994E-05	0.0	0.0	0.0
0.0	0.0	0.0	0.0

STRUCTURAL LOADS ON LAB IN X AXES

MASS POINT = 4
 LOCATION = C.0 0.0 0.6000000E 02

-0.3657064E-08 0.241405F-03 0.4055538E 05 0.1000000E 01 -0.5485803E-02 -0.2502690E-03

MASS POINT = A2
 LOCATION = 0.0 0.0 0.0

-0.434558E-08 -0.330891E-03 0.4704268E-03 -0.1425413E-06 -0.1690800E-03 -0.1444747E-03

MOTION OF MOVING MASS 1
 U1 = 0.0 0.0 0.7621294E 03
 U2 = 0.0 0.0 0.0
 U3 = 0.0 0.0 0.0

BALANCE MASS DATA
 U(2,3) = 0.34951907E 03 UDDT(2,3) = 0.0 UDDT(2,3) = -0.72631836E-01
 SENSOR ACCELERATION ERROR = -0.72631836E-02

CONTROL SYSTEM DATA

JET THRUST
 F1 = 0.0 F2 = 0.0 F3 = 0.0 F4 = 0.0 F5 = 0.0 F6 = 0.0
 F7 = 0.0 F8 = 0.0 F9 = 0.0 F10 = 0.0 F11 = 0.0 F12 = 0.0
 F13 = 0.0 F14 = 0.0 F15 = 0.0 F16 = 0.0
 CMG TORQUE = 0.5694342E-13 0.1782918E-07 0.1294721E-07
 NCMG = 0
 L03 = 0.1685015E 04 L03D = 0.0
 SPIN SPEED COMMAND = 0.4189000E 00
 SPIN ACCELERATION COMMAND = 0.0

57 0.84510430E-05 -0.11707561E-05 -0.62409345F-05 0.12566594E-02 -0.23230158E-03 -0.10451691E-02
 0.12902172E-00 -0.33383265E-01 -0.15131455E-00 -0.55092087E-07 0.96633883E-08 0.45013650E-07
 0.31577644E 01 -0.58320246E 00 -0.26213882F 01 0.73937426E-10 0.27526904E-11 0.36332687E-10

58 -0.55289132E-05 0.13516647E-05 0.55025839E-05 0.12569709E-02 -0.23231718E-03 -0.10450769E-02
 0.17893827E 00 0.32775901E-01 0.14629829E 00 -0.55105751F-07 0.96668380E-08 0.45027132E-07
 0.31577644E 01 -0.58320246E 00 -0.26213882F 01 0.73937426E-10 0.27526904E-11 0.36332687E-10

LOCATION OF CENTER OF MASS IN INERTIAL (Z) COORDINATES
 -0.18762789E-05 0.13170404E-02 -0.21347906F-01

ANGULAR MOMENTUM IN Z- COORDINATES
 0.36072269E 09 0.73643238E-03 -0.51305033F-01

TOTAL KINETIC ENERGY
 0.75552769E 03

STRUCTURAL LOADS APPLIED BY CONNECTING STRUCTURE (ON LAB IN X AXES AND ON CWT IN Y AXES)

ON LAB 0.9391220E-05 0.7229328E-00 -0.5362252E-05 0.7104198E-03 0.6911275E-03 -0.9142247E-03
 ON CWT -0.1393043E-04 0.6617494E 00 -0.5362252E 05 0.3776658E 03 0.2025202E-01 -0.9142209E-03

STRUCTURAL LOADS ON LAB IN X AXES

MASS POINT = 4
 LOCATION = 0.0 FORCE 0.0 -0.6000000E-02 TORQUE

0.2532324E-04 0.4015357F 01 0.4056814E 05 0.1682000E 04 -0.1706076E-02 -0.4119348E-02

MASS POINT = 42
 LOCATION = 0.0 FORCE 0.0 0.0 TORQUE

-0.5481359E-06 -0.3434370E 03 0.4946968E 03 -0.1559525F 05 -0.7490823E-03 -0.7497373E-03

LOCATION OF MOVING MASS 1

UJ = 0.0 0.0 0.0 0.7621294F 03
 UJD = 0.0 0.0 0.0 0.0
 UJDZ = 0.0 0.0 0.0

BALANCE MASS DATA

UJ2-31= 0.3484824E 03 UDDI(2-31)= 0.25701690E 00 UDDI(2-31)= 0.56276190E 00

SENSOR ACCELERATION ERROR = 0.46920776E-01

SENSOR TO CM POS ERROR = 0.15136719E-01

SENSOR ACCELERATION ERROR (FILTERED) = 0.46920776E-01

CONTROL SYSTEM DATA

JET THRUST

F1 = 0.0 F2 = 0.0 F3 = 0.0 F4 = 0.0 F5 = 0.0 F6 = 0.0
 F7 = 0.0 F8 = 0.0 F9 = 0.0 F10 = 0.0 F11 = 0.0 F12 = 0.0
 F13 = 0.0 F14 = 0.0 F15 = 0.0 F16 = 0.0

CMG TORQUE = 0.1617432F-02 0.4670757E-03 0.5559437E-02

NCMG = 0

L03= 0.1685915E 04 L03D= 0.0

SPIN SPEED COMMAND = 0.4189000E 00

SPIN ACCELERATION COMMAND = 0.0

TIME= 0.39999968E 00 STEP= 0.49999997E-01

RDOT WKDOT DELRBD DELRBD DELRBD DELRBD DELRBD DELRBD DELRBD DELRBD DELRBD DELRBD
 0.3222995E-07 0.1111111E-06 0.1575532E 00 0.4128604E 00 -0.2608729E-06 0.5744536E-08 0.4189211E 00
 -0.7490022E-02 -0.4552932E-01 0.2079062E-10 0.8220999E-10 -0.1433192E-02 0.6743193E-02 -0.2654303E-10 0.7634679E-10
 -0.4364789E-03 -0.4039401E-01 0.2454109E-10 0.1041770E-09 0.3299571E-01 -0.9642208E-01 -0.5198038E-10 -0.4500243E-10

PHISTAROT PHISTAROT PHISTAROT PHISTAROT PHISTAROT PHISTAROT PHISTAROT PHISTAROT PHISTAROT PHISTAROT
 0.7156456E-06 0.1419005E-03 0.1450046E-04 0.1652892E-03 0.2573375E-07 0.4143944E-07 0.8632321E-05 0.6127036E-04
 -0.1293970E-01 0.5747107E-00 0.2238345E 00 -0.6988594E-08 -0.1563963E-02 0.5960200E-02 -0.2335773E-10 0.1883040E-09
 0.6156620E-01 0.4245943E-09 0.1119405E 00 -0.7920422E-10 0.3009475E 01 -0.2097189E-01 0.2344572E-10 0.8554135E-10

MASS PT. 2 0-DOT QDOT THETA THETA-DOY THETA-DOY THETA-DOY THETA-DOY THETA-DOY THETA-DOY THETA-DOY THETA-DOY
 0.12744907E-07 0.90553236E-08 0.2117277E-07 0.25416301E-06 0.15200148E-05 0.41094214E-05 0.10404214E-05
 0.55200711E-04 0.37113756E-03 0.89322775E-03 0.41026382E-09 0.95664990E-10 0.10478257E-09 0.10478257E-09
 -0.21996683E 00 0.75543254E-01 0.1276545E 00 0.90202040E-10 0.18231500E-10 0.73726408E-10

4 -0.10318803E-05 0.2970229E-07 0.42789913E-07 -0.24797265E-06 -0.14835014E-05 -0.40018931E-05
 -0.56415255E-05 -0.3316222E-04 -0.89491645E-04 0.47784759E-09 -0.11872808E-09 -0.14362195E-09
 -0.21996683E-01 0.75449495E-01 0.1276545E 00 0.38960338E-09 0.44327697E-10 0.10459040E-09

8 -0.23514502E-05 0.47214745E-07 0.37373558E-07 -0.10929511E-06 -0.65243955E-06 -0.17600951E-05
 -0.12990843E-03 0.73010446E-03 -0.20790540E-02 0.35821014E-11 0.43520432E-10 0.12984273E-09
 -0.21996683E 00 0.75450122E-01 0.12749803E 00 0.75446316E-10 0.13082138E-10 0.56039617E-10

12 -0.3464670E-07 0.63689012E-09 0.12665590E-07 0.11110785E-05 0.89038932E-05 0.49217542E-05
 0.39922345E-03 0.23985686E-03 0.6469234E-03 0.40208659E-09 -0.2807206E-10 -0.99905806E-10
 -0.22081827E 00 0.76430370E-01 0.13001204E 00 0.10959011E-09 0.10763739E-10 0.60333516E-10

16 -0.27702691E-08 0.20826442E-07 -0.53451146E-07 -0.16508220E-05 -0.10447493E-05 -0.33014858E-05
 0.39922345E-03 0.23985686E-03 0.6469234E-03 0.40208659E-09 -0.2807206E-10 -0.99905806E-10
 -0.22081827E 00 0.76430370E-01 0.13001204E 00 0.10959011E-09 0.10763739E-10 0.60333516E-10

17 -0.70833515E-05 0.25564986E-05 0.45340639E-05 -0.10928551E-06 -0.65243955E-06 -0.17600951E-05
 -0.11993541E-00 0.37671845E-01 0.62967644E-01 0.35821014E-11 0.43520432E-10 0.12984273E-09
 0.19842300E 02 -0.68468256E 01 -0.11600830E 02 0.75446316E-10 0.13082138E-10 0.56039617E-10

18 -0.5939559E-05 0.16110403E-05 0.26248380E-05 -0.10288515E-06 0.65243955E-06 -0.17600951E-05
 0.11150271E 00 -0.39210461E-01 -0.6713309E-01 0.35821014E-11 0.43520432E-10 0.12984273E-09
 0.19842300E 02 -0.68468256E 01 -0.11600830E 02 0.75446316E-10 0.13082138E-10 0.56039617E-10

29 0.55149075E-05 -0.16583081E-05 -0.24731498E-05 -0.11910712E-02 0.41022990E-03 0.69434405E-03
 -0.16992549E 00 0.57687581E-01 0.96876323E-01 -0.38844729E-07 0.12325534E-07 0.20169056E-07
 -0.2992699E-01 0.10322161E 01 -0.17484999E-01 0.78446316E-10 0.13082138E-10 0.56039617E-10

30 -0.46252426E-05 0.1592732E-05 0.27919313E-05 -0.11913457E-02 0.4104004E-03 0.69481204E-03
 -0.16992549E 00 0.57687581E-01 0.96876323E-01 -0.38844729E-07 0.12325534E-07 0.20169056E-07
 0.2992699E 01 -0.10322161E 01 -0.17484999E-01 0.78446316E-10 0.13082138E-10 0.56039617E-10

45 -0.71776131E-05 0.3011204E-05 0.56605140E-05 -0.10288515E-06 0.65243955E-06 -0.17600951E-05
 0.11160266E 00 -0.39063700E-01 -0.66712379E-01 0.35821014E-11 0.43520432E-10 0.12984273E-09
 0.19852539E 02 -0.67856054E 01 -0.11435682E 02 0.75446316E-10 0.13082138E-10 0.56039617E-10

46 0.61547244E-05 -0.17547662E-05 -0.25399404E-05 -0.10288515E-06 0.65243955E-06 -0.17600951E-05
 -0.11179290E 00 0.37476078E-01 0.62454257E-01 0.35821014E-11 0.43520432E-10 0.12984273E-09
 -0.19852539E 02 -0.67856054E 01 -0.11435682E 02 0.75446316E-10 0.13082138E-10 0.56039617E-10

57 0.81179860E-05 -0.20262951E-05 -0.26194343E-05 0.11914454E-02 -0.40799892E-03 -0.68873251E-03
 -0.16992549E 00 -0.58889937E-01 -0.1001989E-00 -0.52364989E-07 0.17027919E-07 0.28023305E-07
 0.29940691E 01 -0.10322161E 01 -0.17258663E 01 0.75446316E-10 0.13082138E-10 0.56039617E-10

SR -0.5550213E-05 0.2418492E-05 0.46967625E-05 0.11917565E-02 -C.4C788914E-03 -C.68819708E-03
 -0.1697638E-03 -0.52207170E-01 -0.9586473E-01 -0.52377690E-07 -0.1703410AE-07 0.28035764E-07
 0.2994991E 01 -C.1023F256E C1 -0.17259663F 01 0.75446316E-1C 0.13082138F-10 0.56039617E-10

LOCATION OF CENTER OF MASS IN INERTIAL (Z) COORDINATES
 -0.15757178E-05 0.1493648E-02 -0.2062879E-01

ANGULAR MOMENTUM IN Z COORDINATES
 C.36072243E 09 0.32793704E-03 -0.49777455F-01

SPECIAL KINETIC ENERGY
 C.75553289E 03

STRUCTURAL LOADS APPLIED BY CONNECTING STRUCTURE (ON LAB IN X AXES AND ON CMI IN Y AXES)
 ON LAB -0.1731274E-04 0.7822663F 01 -0.5355625E 05 0.3774086E 04 0.1409157E-01 -0.1710371E-02
 ON CMI -0.1596641E-04 0.3366202E 01 -0.3355625E 05 -0.1827414E 04 -0.1134125E-01 -0.1710328E-02

STRUCTURAL LOADS ON LAB IN X AXES

MASS POINT = 4
 LOCATION = 0.0 0.0 0.0 0.6000000F 02

FORCE
 -0.4755590F-05 0.5305006E 01 0.4052263E 05 0.9930000E 03 -C.5821675E-02 -0.7712673E-02

MASS POINT = 45
 LOCATION = 0.0 0.0 0.0 0.0

FORCE
 -0.2712869E-03 -0.346335E 01 -0.4840446E 01 -0.1515860E-06 -0.8128798E-03 -0.4564971E-03

MOTION OF MOVING MASS 1
 UJ = 0.0 0.0 0.0 0.7621294E-03
 UJD = 0.0 0.0 0.0
 UJDD = 0.0 0.0 0.0

BALANCE MASS DATA
 U(2,3) = 0.3494116E 03 UDDT(2,3) = -0.2186208E 00 UDDDT(2,3) = -0.10976667E 01
 SENSOR ACCELERATION ERROR = -0.11766052F 00
 SENSOR TO CM POS ERROR = 0.10000766E-01
 SENSOR ACCELERATION ERROR (FILTERED) = -C.11766052F 00

CONTROL SYSTEM DATA

JET THRUST
 E1 = 0.0 E2 = 0.0 E3 = 0.0 E4 = 0.0 E5 = 0.0 E6 = 0.0
 F7 = 0.0 F8 = 0.0 F9 = 0.0 F10 = 0.0
 F13 = 0.0 F14 = 0.0 F15 = 0.0 F16 = 0.0
 TORQUE = -0.5431169E-03 C.1479058E-02 -0.8744322E-02

1.030 = 0.0

•
 •
 •

Reproduced from
best available copy.

0.3029609E-01 0.9103608E-01
0.4833094E-02 0.9103614E-01

NN CWT.

STRUCTURAL LOADS - JMWLAR IN X AXES

MASS POINT = 4
LOCATION = 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
FORCE 0.4001966E-05 0.3143094E 02 0.4050630E 05 -0.5235000E 04 -0.4298728E-02 -0.7417214E-C1
TORQUE
MASS POINT = 4? 0.0 0.0 0.0 0.0
LOCATION = 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
FORCE -0.1508770E-05 -0.3352050E 03 0.4731184E 03 -0.1442003E 06 -0.2416530E-03 -0.1726059E-02
TORQUE

MOTION OF MOVING MASS 1
UJ = 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
UJD = 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
UJDD = 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

BALANCE MASS DATA
U(2,3) = 0.3719372E-03 U(3,2) = 0.36915045E-01 UDDCI(2,3) = 0.60239887E-0C
SENSOR ACCELERATION ERROR = 0.12461060E 00
SENSOR TO CM PJS ERROR = 0.57910156E 00
SENSOR ACCELERATION ERROR (FILTERED) = 0.12461060E 00

CONTROL SYSTEM DATA

JET THROUST
F1 = 0.0 F2 = 0.5000000E 02 F3 = 0.0 F4 = 0.0 F5 = 0.5000000E 02 F6 = 0.0
F7 = 0.0 F8 = 0.0 F9 = 0.5000000E 02 F10 = 0.0 F11 = 0.0 F12 = 0.0
F13 = 0.0 F14 = 0.5000000E-02 F15 = 0.0 F16 = 0.0
CMG THROUFE = -0.2531197E-02 -0.2532119E-01 -0.1450925E-01
NCGE C
LC3 = 0.1685916E-04 L013 = 0.0 L000 = 0.0
SPIN SPEED COMMAND = 0.4189000E 00
SPIN ACCELERATION COMMAND = 0.0

END OF TIME
HISTORY AT
TIME = 10. SEC.

STATISTICS ON RUN

MAXIMUM AND MINIMUM ELASTIC MOTIONS										
MACS-NO.	MIN	MAX	QDOTMIN	QDOTMAX	QDOTMIN	QDOTMAX	QDOTMIN	QDOTMAX	QDOTMIN	QDOTMAX
1	-0.1550752E-07	-0.4401918E-08	-0.1102410E-07	0.1255472E-07	-0.2907037E-07	0.2961636E-07	-0.1482033E-01	0.5789861E-02	-0.1482033E-01	0.1576592E-01
2	-0.1579563E-02	0.2827357E-02	-0.6158024E-02	0.5789861E-02	-0.2042857E-00	0.2262704E-00	-0.1781392E-07	0.1781392E-07	-0.4162555E-07	0.3800368E-07
3	-0.2366663E-00	-0.1583115E-00	-0.8580020E-01	0.9166151E-01	-0.2042810E-00	0.2262653E-00	0.4162555E-07	0.4162555E-07	-0.1073269E-01	0.1141747E-01
4	-0.3173205E-07	0.4601385E-07	-0.1474709E-07	0.1781392E-07	-0.2042810E-00	0.2262653E-00	0.1781392E-07	0.1781392E-07	-0.2042810E-00	0.2262653E-00
5	-0.1448142E-02	-0.2047485E-02	-0.4455564E-02	0.4192933E-02	-0.2042810E-00	0.2262653E-00	0.4192933E-02	0.4192933E-02	-0.1073269E-01	0.1141747E-01
6	-0.2366663E-00	-0.1583115E-00	-0.8580020E-01	0.9166151E-01	-0.2042810E-00	0.2262653E-00	0.9166151E-01	0.9166151E-01	-0.2042810E-00	0.2262653E-00
7	-0.4159221E-02	0.0110579E-07	-0.3446035E-02	0.3262310E-07	-0.8927918E-07	0.7901747E-07	0.3262310E-07	0.3262310E-07	-0.8927918E-07	0.7901747E-07
8	-0.3245775E-03	0.1264504E-02	-0.2754533E-02	0.2589834E-02	-0.6629255E-02	0.7052202E-00	0.2589834E-02	0.2589834E-02	-0.6629255E-02	0.7052202E-00
9	-0.2366663E-00	-0.1583115E-00	-0.8580020E-01	0.9166151E-01	-0.2042810E-00	0.2262653E-00	0.9166151E-01	0.9166151E-01	-0.2042810E-00	0.2262653E-00
10	-0.1164115E-05	-0.7061199E-07	-0.4627766E-07	0.3665711E-07	-0.9764523E-07	0.1075160E-06	0.3665711E-07	0.3665711E-07	-0.9764523E-07	0.1075160E-06
11	-0.2835645E-03	0.2003849E-03	-0.5805050E-03	0.6174082E-03	-0.1580705E-02	0.1495987E-02	0.6174082E-03	0.6174082E-03	-0.1580705E-02	0.1495987E-02
12	-0.2166201E-03	-0.1582137E-00	-0.8574730E-01	0.9166151E-01	-0.2042810E-00	0.2262653E-00	0.9166151E-01	0.9166151E-01	-0.2042810E-00	0.2262653E-00
13	-0.1505369E-05	-0.1006683E-06	-0.5946255E-07	0.4483711E-07	-0.9764523E-07	0.1075160E-06	0.4483711E-07	0.4483711E-07	-0.9764523E-07	0.1075160E-06
14	-0.3035255E-02	0.1275131E-02	-0.3692308E-02	0.3927777E-02	-0.9764523E-07	0.1075160E-06	0.3927777E-02	0.3927777E-02	-0.9764523E-07	0.1075160E-06
15	-0.2366663E-00	-0.1583115E-00	-0.8580020E-01	0.9166151E-01	-0.2042810E-00	0.2262653E-00	0.9166151E-01	0.9166151E-01	-0.2042810E-00	0.2262653E-00
16	-0.2661553E-05	-0.1550528E-06	-0.1067478E-06	0.8584607E-07	-0.2104129E-06	0.2709836E-06	0.8584607E-07	0.8584607E-07	-0.2104129E-06	0.2709836E-06
17	-0.6575765E-02	0.4655663E-02	-0.1347300E-01	0.1433000E-01	-0.3668794E-01	0.3448781E-01	0.1433000E-01	0.1433000E-01	-0.3668794E-01	0.3448781E-01
18	-0.2251897E-00	-0.1506455E-00	-0.8157998E-01	0.8718491E-01	-0.1941990E-00	0.2152929E-00	0.8718491E-01	0.8718491E-01	-0.1941990E-00	0.2152929E-00
19	0.5230785E-05	0.1399027E-05	-0.1165135E-05	0.1157413E-05	-0.2970666E-05	0.3252967E-05	0.1157413E-05	0.1157413E-05	-0.2970666E-05	0.3252967E-05
20	-0.6532945E-02	0.4702975E-02	-0.1347234E-01	0.1433000E-01	-0.3668794E-01	0.3448781E-01	0.1433000E-01	0.1433000E-01	-0.3668794E-01	0.3448781E-01
21	-0.1620865E-01	0.2509082E-01	-0.9672360E-00	0.9010762E-00	-0.2398833E-01	0.2140493E-01	0.9010762E-00	0.9010762E-00	-0.2398833E-01	0.2140493E-01
22	-0.3032935E-05	-0.1832236E-06	-0.1217929E-06	0.9488221E-07	-0.2376460E-06	0.3031573E-06	0.9488221E-07	0.9488221E-07	-0.2376460E-06	0.3031573E-06
23	-0.6572015E-02	0.4652116E-02	-0.1347171E-01	0.1432830E-01	-0.3668366E-01	0.3448342E-01	0.1432830E-01	0.1432830E-01	-0.3668366E-01	0.3448342E-01
24	-0.2366663E-00	-0.1583115E-00	-0.8580020E-01	0.9153965E-01	-0.2039745E-00	0.2259912E-00	0.9153965E-01	0.9153965E-01	-0.2039745E-00	0.2259912E-00
25	-0.1146721E-03	0.2016180E-06	-0.1103330E-06	0.1182471E-06	-0.3529888E-06	0.3926633E-06	0.1182471E-06	0.1182471E-06	-0.3529888E-06	0.3926633E-06
26	-0.6552173E-02	0.4671190E-02	-0.1347201E-01	0.1433140E-01	-0.3669122E-01	0.3449275E-01	0.1433140E-01	0.1433140E-01	-0.3669122E-01	0.3449275E-01
27	0.2262271E-00	0.3377614E-00	-0.1299053E-00	0.1209032E-00	-0.3229220E-00	0.2869766E-00	0.1209032E-00	0.1209032E-00	-0.3229220E-00	0.2869766E-00
28	0.3655645E-05	0.8091014E-06	-0.5490822E-06	0.5601734E-06	-0.1418234E-05	0.1616404E-05	0.5601734E-06	0.5601734E-06	-0.1418234E-05	0.1616404E-05
29	-0.6547557E-02	0.4685702E-02	-0.1347259E-01	0.1433278E-01	-0.3669444E-01	0.3449762E-01	0.1433278E-01	0.1433278E-01	-0.3669444E-01	0.3449762E-01
30	-0.5441462E-00	0.1410042E-00	-0.5434635E-00	0.5061950E-00	-0.1248085E-01	0.1202351E-01	0.5061950E-00	0.5061950E-00	-0.1248085E-01	0.1202351E-01

MASS NO.	THETA MIN	THETA MAX	THETA DOT MIN	THETA DOT MAX	THETA DOT DOT MIN	THETA DOT DOT MAX
1	-0.129129E-04 0.324039E-09 -0.269720E-10	0.917048E-05 0.502552E-09 0.166416E-09	-0.265816E-04 -0.155345E-09 -0.260999E-09	0.282718E-04 0.198820E-09 0.277713E-09	-0.723822E-04 -0.485149E-09 -0.779401E-09	0.680408E-04 0.392284E-09 0.779693E-09
2	-0.129803E-04 0.317419E-09 -0.307273E-10	0.917889E-05 0.494478E-09 0.169015E-09	-0.265799E-04 -0.154721E-09 -0.272785E-09	0.282700E-04 0.195694E-09 0.286632E-09	-0.723775E-04 -0.478345E-09 -0.801179E-09	0.680364E-04 0.385679E-09 0.800633E-09
3	-0.129954E-04 0.352084E-09 0.821459E-10	0.911185E-05 0.545717E-09 0.260837E-09	-0.263853E-04 -0.165504E-09 -0.255883E-09	0.280633E-04 0.224736E-09 0.261738E-09	-0.718485E-04 -0.521088E-09 -0.745468E-09	0.675391E-04 0.426119E-09 0.743596E-09
4	-0.126500E-04 0.370284E-09 0.263659E-10	0.895887E-05 0.572277E-09 0.424497E-09	-0.250426E-04 -0.170639E-09 -0.230643E-09	0.275921E-04 0.224736E-09 0.222887E-09	-0.706421E-04 -0.543264E-09 -0.658630E-09	0.664051E-04 0.447235E-09 0.699003E-09
5	-0.124159E-04 0.237219E-09 0.337210E-10	0.878023E-05 0.465187E-09 0.406501E-09	-0.254263E-04 -0.154460E-09 -0.217815E-09	0.270430E-04 0.184118E-09 0.206414E-09	-0.692362E-04 -0.453459E-09 -0.630848E-09	0.650835E-04 0.361279E-09 0.696195E-09
6	-0.121891E-04 0.241930E-09 0.253352E-10	0.861942E-05 0.463819E-09 0.451077E-09	-0.249597E-04 -0.153127E-09 -0.220119E-09	0.265468E-04 0.183712E-09 0.210601E-09	-0.679659E-04 -0.452338E-09 -0.631102E-09	0.638894E-04 0.360412E-09 0.688183E-09
7	-0.011074					0.477463E-04 0.143154E-09 0.842862E-09
70	-0.442844E-07 -0.320520E-08	0.383334E-04 -0.300209E-07 -0.344116E-09	-0.160417E-07 -0.261734E-08	0.121363E-04 0.890994E-10 0.235491E-09	-0.310711 -0.199311E-09 -0.657285E-09	0.263474E-09 0.656503E-09
71	-0.557245E-05 -0.323235E-10 -0.245085E-10	0.364035E-05 0.801832E-10 0.139822E-09	-0.114108E-04 -0.110322E-09 -0.225462E-09	0.128530E-02 0.692868E-08 0.121705E-08	-0.341911E-02 -0.150026E-07 -0.368431E-08	0.305378E-02 0.172895E-07 0.296337E-08
72	-0.309647E-02 -0.314903E-07 -0.245091E-03	0.469980E-02 0.213280E-07 0.8255150E-09	-0.177747E-02 -0.114011E-07 -0.212064E-08	0.165625E-02 0.115121E-07 0.213538E-08	-0.440732E-02 -0.264630E-07 -0.584447E-08	0.393483E-02 0.288559E-07 0.534908E-08



Reproduced from
best available copy.

MAXIMUM LOADS COMPUTED

STRUCTURAL LOADS APPLIED BY CONNECTING STRUCTURE (CN LAB IN X AXES AND ON CMT IN Y AXES)

FORCE	TORQUE
CN LAB 0.1799214E-04 0.2502370E C2 0.0	0.3678967E 05 0.4134485E-01 0.9103509E-01
ON CMT 0.1366991E-04 0.2240135E 02 0.0	0.1511271E 05 0.2025202E-01 0.9103614E-01

STRUCTURAL LOADS ON LAB IN X AXES

MASS POINT = 4	FORCE	TORQUE
LOCATION = 0.0	0.0 0.6000000E 02	
0.7656665E-03	0.7511704E C2 0.4100304E 05	0.4665000E C4 0.5669385E-02 0.9361536E-01

MASS POINT = 43

LOCATION = 0.0	FORCE	TORQUE
0.0	0.0 0.0	
0.6132221E-05	0.4946968E 03	0.0 0.8708135E-03 0.2115173E-02

MINIMUM LOADS COMPUTED

STRUCTURAL LOADS APPLIED BY CONNECTING STRUCTURE (CN LAB IN X AXES AND ON CMT IN Y AXES)

FORCE	TORQUE
CN LAB -0.2877915E-04 -0.9668708E 01 -0.5402790E 05	-0.1847439E 05 -0.5454440E-01 -0.9139854E-01
ON CMT -0.1635344E-04 -0.4427644E-01 -0.6402701E-05	-0.1904321E-06 -0.1352845E-01 -0.9139764E-01

STRUCTURAL LOADS ON LAB IN X AXES

MASS POINT = 4	FORCE	TORQUE
LOCATION = 0.0	0.0 0.6000000E 02	
-0.4587247E-04	-0.7563937E 02 0.0	-0.3451609E 05 -0.1071803E-01 -0.7417214E-01

MASS POINT = 43

LOCATION = 0.0	FORCE	TORQUE
0.0	0.0 0.0	
0.8000000E-05	0.3433728E-03 0.0	-0.1569528E 04 -0.9002411E-03 -0.1726050E-02

APPENDIX B3

Description of Numerical-Integration Subroutine(MAGIC) Parameters

The numerical-integration subroutine provides the user with both a fixed-step and variable-step numerical-integration option. Both options use a Runge-Kutta method. For details of this subroutine, the user is referred to the MAGIC documentation manual.*

The parameters needed to control this integration process are DELTA, EPSIL, STEP, DTAU, and ERR.

B3.1 Fixed-Step Runs

For fixed-step runs set DELTA = 0 and set STEP to the time step size of each numerical-integration cycle. A guideline for-choosing STEP is to set it to 1/20th of the highest frequency present among the integrated variables. DTAU is the time interval between both the print and plot output cycles. EPSIL and ERR are not used in fixed-step runs.

B3.2 Variable-Step Runs

In variable-step runs, the subroutine tests the accuracy of the integration for each variable and uses this information to set the numerical-integration time step size. As explained in detail below, DELTA and EPSIL are small positive numbers used to test the integration accuracy by comparing a precision parameter with a percentage of each variable. When the absolute value of a variable is very small an ERR parameter (one is supplied for each integrated variable) is used for testing accuracy. One guideline for selecting DELTA and EPSIL is to choose DELTA = 1/3 EPSIL. The approximate tests started below describe the usage of EPSIL, DELTA, and ERR and should be used to determine their values†. MAGIC initially selects a step size of .0078125.

* Ball, D., Stoodley, G., and Angelillo, R., "A Fortran Program for the Numerical-Integration of Ordinary Differential Equations," Grumman Aerospace Corporation, Data Systems Department Report, CR-61-2, October 1969.

† The precise test is more complicated and is stated in the previously referenced MAGIC documentation manual.

Let y be a typical element of the vector $\{y\}$ to be integrated. Then y dev is a precision parameter determined by subtracting the values of y obtained by using two somewhat different numerical-integration processes. The tests are as follows:

Dominant test when y is not small:

If $ y \text{ dev} > \text{EPSIL} * y $	for any integrated variable, the step size is halved and the integration is repeated
If $ y \text{ dev} < \text{DELTA} * y $	for each integrated variable, the integration is not repeated and the step size doubles
If $ \text{DELTA} * y \leq y \text{ dev} \leq \text{EPSIL} * y $	integration continues with the current step size

Dominant test when y is small (of order ERR):

If $ y \text{ dev} > \text{ERR}$	for any integrated variable, the step size is halved and the integration is repeated
If $ y \text{ dev} < .01 \cdot \text{ERR}$	for each integrated variable, the integration is not repeated and the step size doubles
If $.01 \text{ ERR} \leq y \text{ dev} \leq \text{ERR}$	integration continues with the current step size

Discontinuities in the analysis (e.g., pulse-type forces or an elevator moving with constant acceleration) may cause the step size to halve indefinitely. To avoid this difficulty, the user must input a value of STEP which is used as the minimum time interval. STEP has no other use in variable step runs.

DTAU is the time interval between print output cycles.

B3.3 Limitations of variable-Step Option

While the variable time-step option often reduces the computer running time considerably, the following problem limits the use of this option.

Whenever the step size is halved all computations needed to obtain the derivatives are repeated at a value of time which is less than the previous value used for these computations. Several control-system subroutines use the value of the variables at the previous time step; however the stored value now corresponds to a future time step. This discrepancy leads to errors when these subroutines are used. For this reason the following problems should not be run using the variable-step option:

Moving masses and mass balancing

Fluid motion

Deployment or retraction maneuvers

Spin up or spin down

APPENDIX B4

BRIEF DESCRIPTION OF EACH SUBROUTINE*

ADD	addition of 3 X N matrices
ATTCTR	attitude control subroutine
BMCON	balance mass control interface routine
BMCTR	balance mass control subroutine
CHASE	solution of equations for symmetric positive definite system
COMMEN	major subroutine for data input and initialization of common areas
CONSTR	connecting structure subroutine for circular beam
CONTRL	interface program for controls subroutines
CW	calculates the contributions to $[\Lambda]$ and $\{\nabla\}$ from the Counterweight
CWCOM	Counterweight command
DOTP	dot product of vectors
FIRST	computes the realignment of the initial conditions
FUTILE	Cholesky decomposition of symmetric positive definite matrix
GAMMA	compute gamma functions [see Appendix B, Volume I]
INCH	inversion of a real symmetric positive definite matrix
LAB	calculates the portions of $[\Lambda]$ and $\{\nabla\}$ corresponding to the Laboratory, not including fluids and moving masses
LAST	compute connecting structure deformations
LOADIN	computations of structural loads
LOOK	look-up subroutine to give the values of k denoting the masses m_k which influence moving mass μ_j
LUMP	calculates the contributions to $[\Lambda]$ and $\{\nabla\}$ from the moving masses
MCPY	matrix copy subroutine
MINCY	sets up and performs integration step, prints time - history output and plotting output and computes the transformations to physical coordinates
MINMAX	computation of minimum and maximum displacements, velocities and accelerations

 * For the definition of the analytical symbols, see Section 4 of Volume I.

MPRD	general matrix multiplication
MTRAN	multiplication by transpose of a 3 x 3 matrix
MUCOM	moving mass command subroutine
MULT	multiplication by a 3 x 3 matrix
PIF	computes Π -function [see Appendix B, Volume I]
PIPE	calculates the contributions to $[\Lambda]$ and $\{\nabla\}$ from the pipes
PLO3AX	Calcomp plotting program
PMPCOM	pump command subroutine
POSCOM	position command subroutine
POSCTR	position control subroutine
PTLP	compute $[P]^T [L] [P]$ where $[P]$ is a 3 x 3 matrix and L is the 3 x 1 diagonal of a 3 x 3 diagonal matrix
RESVR	calculates the contribution to $[\Lambda]$ and $\{\nabla\}$ from the reservoir
SCALR	multiplication of a matrix by a scalar
SETUP (MAGIC)	Runge-Kutta integration program
SPNCOM	spin command subroutine
SPNCTR	spin control subroutine
SSIN	computes S-function or S^{-1} function [see Appendix B, Volume 1]
SUBTR	matrix subtraction subroutine
SUPPLM	supplementary forces subroutine
TPRD	general matrix-transpose multiplication
VELCOM	velocity command subroutine
VELCTR	velocity control subroutine
WBLCTR	wobble control subroutine
XADD	general matrix addition
XMCPY	matrix stacking subroutine
XMPRD	general matrix multiplication
XTPRD	general multiplication by transpose of a matrix
ZCW	calculates portions of $[\Lambda_R]$ and $\{\nabla_R\}$
ZLAB	calculates portions of $[\Lambda_R]$ and $\{\nabla_R\}$

APPENDIX B5

REPLACEABLE SUBROUTINES

The following subroutines may be replaced by the user in order to run different physical problems:

- CONSTR - computes structural loads for beam-type connecting structure
- CONTRL - main controls interface routine; calls and computes data for CWCOM, SPNCOM, ATTCTR, SPNCTR, and WBLCTR
- CWCOM - commands position of Counterweight
- SPNCOM - commands Space-Station spin speed
- MUCOM - commands motion of moving masses (μ_j 's)
- PMPCOM - commands velocity of fluid being pumped
- POSCOM - position command policy
- VELCOM - velocity command policy
- ATTCTR - controls Space-Station attitude
- SPNCTR - controls Space-Station spin speed
- WBLCTR - controls Space-Station wobble
- BMCON - interface for BMCTR; calls and computes data for BMCTR
- BMCTR - controls motion of balance mass to balance mass shifts along long axis of Space-Station
- POSCTR - position control policy
- VELCTR - velocity control policy
- SUPPLM - contains supplementary external loads as a function of time (these are set to zero in the subroutine supplied)
- LOOK - selects structural masses (m_k 's) that influence motion of moving masses (μ_j 's). In the version of LOOK supplied with the program $k = 1, 2, \dots, 8$ for all μ_j 's and the k 's remain constant with time

CONTRL and BMCON are interface subroutines for the major control systems (i.e., the control systems required to control the motion of the Space Station). Figure B1 illustrates the hierarchy of the control-system subroutines.

The read and print statements for the replaceable subroutines are located within these subroutines.

The input and output symbols for all replaceable subroutines are tabulated on the following pages. The analytical symbols used in this chart are defined in Section 3.2.

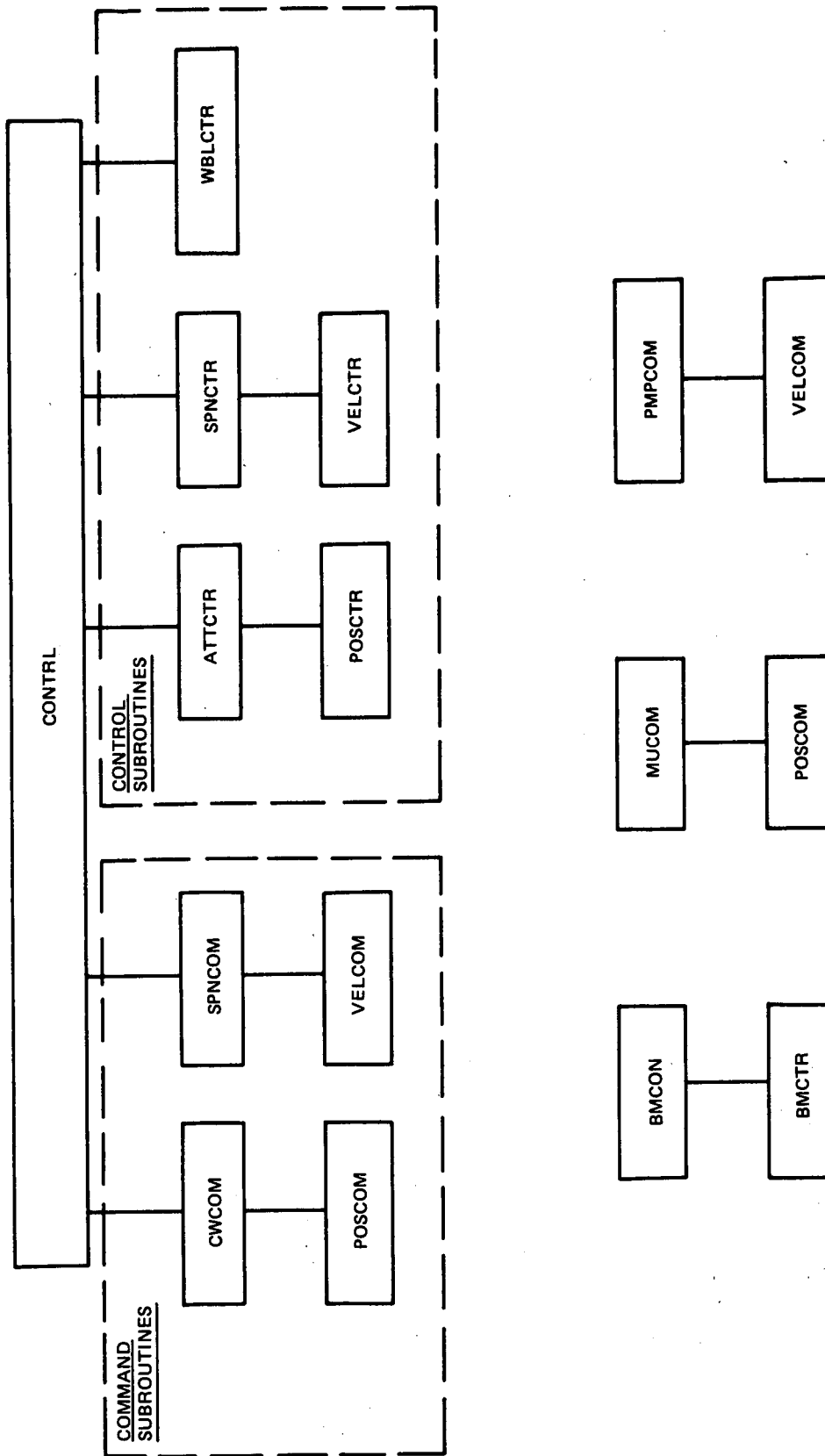


Fig. B1 Hierarchy of Control Subroutines

7

CONSTR - Called from ZLAB and ZCW

INPUT

Main Program Analytical Symbols	CONSTR Symbols	Comments
$\{l_0\}$	EL	} average axial load component in Connecting Structure
$\{P_z\}_3$	P	
$\{\phi^*\}$	PHIST	
$\{\dot{\phi}^*\}$	PHISTD	
$\{\delta\}$	DEL	
$\{\dot{\delta}\}$	DELD	
t	T	
	IN	Card Input Unit
	IOUT	Printer Output Unit

OUTPUT

Main Program Analytical Symbols	CONSTR Symbols	Comments
$\{f_E^*\}$	FETEST	Elements 1-3
$\{\tau_E^*\}$	FETEST	Elements 4-6

CONTRL - Called from ZLAB and ZCW

INPUT

Main Program Analytical Symbols	CONTRL Symbols	Comments
	N	Number of mass points on the vehicle
	IFCON	Clue { Set to 1 if controls are present Set to 0 if controls are not present
	LABCW	Clue { Set to 1 if called from ZLAB Set to -1 if called from ZCW
t	T	
$\{w^X\}$	WX	
all $\{r_i\}$	RI	$\{r_i\}$ begins at RI (3 · i - 2)
all $\{\theta_i\}$	TH	
all $\{\dot{\theta}_i\}$	THD	
$\{R\}$	RDDOT	
$\{\dot{w}^X\}$	WXDOT	
all $\{\ddot{q}_i\}$	XDD	$\{\ddot{q}_i\}$ begins at XDD (1, i)
all $\{\ddot{\theta}_i\}$	XDD	$\{\ddot{\theta}_i\}$ begins at XDD (4, i)
M_C	EMC	mass of Counterweight (see Note 6)
M	TOT	mass of Space Station
M_L	EML	mass of Laboratory (see Note 6)
$\{\gamma\}$	GAM	
$\{\dot{\gamma}\}$	GAMD	
$\{l_0\}$	EL	
$\{\dot{l}_0\}$	ELD	
$\{\ddot{l}_0\}$	ELDD	
	IN	Card Input Unit
	IOUT	Printer Output Unit
$\{w^{X^i} s\}$	O	
$[D_L]$	DL	} See Note 6
$[D_C]$	DC	
$[I_L]$	IL	Inertia matrix of Laboratory
$[I_C]$	IC	Inertia matrix of Counterweight
	YPRED	Integrated controls variable (after t = 0)

Continued

CONTRL (Continued)

OUTPUT

Main Program Analytical Symbols	CONTRL Symbols	Comments
all $\{f_c^i\}$ (or $\{\bar{f}_c^i\}$)	A	$\{f_c^i\}$ (or $\{\bar{f}_c^i\}$) begins at A(3i -2)(see Note 1)
all $\{\tau_c^i\}$ (or $\{\bar{\tau}_c^i\}$)	A	$\{\tau_c^i\}$ (or $\{\bar{\tau}_c^i\}$) begins at A(3i +1)(see Note 1)
$\{\dot{w}^i s\}$	DO	Output when entered via EARLY
i_s	IS	
	NEQS	The number of integrated controls variables (at T = 0)
	YICS	Initial conditions of integrated controls variables (at T = 0)
	YDOT	Time-derivative of integrated controls variables

Special Considerations

- (1) The forces and torques exerted by the control actuators are computed for the:

Laboratory when LABCW = 1
Counterweight when LABCW = -1

- (2) Entry point CONTRD is used to input the controls input data
(3) Entry point EARLY is used to compute the value of

$$\{\dot{w}^i s\}$$

- (4) Entry point LLDLDD is used to call CWCOR and then return
(5) The variables currently being integrated are 4 variables from WBLCTR (if controls are present) and 3 variables from BMCTR (if mass balancing is present)
(6) See Equations (A29) and (A36) of Appendix C, Volume I

CWC0M - Called from CONTRL

INPUT

Control - System Analytical Symbols	CWC0M Symbols	Comments
t	TIME	
l_{03u}	XB3CU	Connecting Structure length update
t_{03u}	TXB3CU	Update time
acc $l_{03 \text{ max}}$	ACCB3C	Magnitude of acceleration of l_{03}
vel $l_{03 \text{ max}}$	VELMBC	Maximum velocity of l_{03}
l_{03}	XB3C	Input at t = 0

OUTPUT

Control - System Analytical Symbols	CWC0M Symbols	Comments
\ddot{l}_{03}	DDXB3C	
\dot{l}_{03}	DXB3C	
l_{03}	XB3C	Undeformed length of connecting Structure

SPNCOM - Called from CONTRL

INPUT

Control - System Analytical Symbols	SPNCOM Symbols	Comments
time	TIME	
ω_{1CU}	O1CU	
$t_{\omega_{1CU}}$	T01CU	
$acc_{\omega_{1C}}$	ACCOLC	At time = 0
f_{JET}	FJET	} These variables are in the argument list but are not currently used.
A_j		
$\{X^j\}$	XAJ	
$[M_{11}]$	WML1	
ω_{1C}	O1C	At time = 0

OUTPUT

Control - System Analytical Symbols	SPNCOM Symbols	Comments
$acc_{\omega_{1C}}$	ACCOLC	
ω_{1C}	O1C	
$\omega_{1C} \text{ mag}$	O1CMAG	

MUCOM - Called from LUMP

INPUT

Main Program Analytical Symbols	CONSTR Symbols	Comments
t	T	
j	L	Moving mass number
	IN	Card input unit
	IOUT	Printer output unit

OUTPUT

Main Program Analytical Symbols	CONSTR Symbols	Comments
$\{U_j\}$	UJ	
$\{\dot{U}_j\}$	UJD	
$\{\ddot{U}_j\}$	UJDD	

PMPCOM - Called from MAIN

INPUT

Main Program Analytical Symbols	PMPCOM Symbols	Comments
t	T IN IOUT	Card input unit Printer output unit

OUTPUT

Main Program Analytical Symbols	PMPCOM Symbols	Comments
V \dot{V}	V VDOT	

POSCOM - Called from MUCOM, CWCUM

INPUT

Control - system Analytical Symbols	POSCOM Symbols	Comments
time	TIME	
poscu	POSCU	Position command update
timecu	TIMCU	Time command update
acc _{mag}	ACCMAG	Magnitude of acceleration command
vel _{max}	VELMAX	Maximum velocity command

OUTPUT

Control - system Analytical Symbols	POSCOM Symbols	Comments	
out	OUT		
time0	TIME0		
time1	TIME1		
time2	TIME2		
time3	TIME3		
acc01	ACC01	Intermediate output to each subroutine that calls POSCOM and returned each time cycle	
acc12	ACC12		
acc23	ACC23		
posc0	POSC0		
posc1	POSC1		
posc2	POSC2		
velc1	VELC1		
velc2	VELC2		
acc _{cmn}	ACCCMN		Acceleration command
vel _{cmn}	VELCMN		Velocity command
pos _{cmn}	POSCMN	Position command	

VELCOM - Called from SPNCOM, FMPCOM

INPUT

Control-system Analytical Symbols	VELCOM Symbols	Comments
time velcu timcu acc mag	TIME VELCU TIMCU ACCMAG	Velocity command update Time command update Magnitude of acceleration command

OUTPUT

Control-system Analytical Symbols	VELCOM Symbols	Comments
out time0 time1 acc01 velc0 acc _{cmn} vel _{cmn}	OUT TIME0 TIME1 ACCO1 VELCO ACCCMN VELCMN	} Intermediate output to be stored in each subroutine that calls, VELCOM and returned each time cycle. Acceleration command Velocity command

ATTCTR - Called from CONTRL

INPUT

Control-system Analytical Symbols	ATTCTR Symbols	Comments
$\{\theta\}$	T	
$\{\dot{\theta}\}$	DT	
$e_{\theta DB}$	ETDB	
$\dot{e}_{\theta MAX}$	DETMAX	
$A_{\{X^j\}}$	XAJ	
$[M_{11}]$	WML1	Inertia matrix of Space Station
f_{jet}	FJET	
ω_{1CMAG}	OICMAG	

OUTPUT

Control-system Analytical Symbols	ATTCTR Symbols	Comments
A_{f^j}	FAJ	CONTRL currently expects values for: FAJ (2, 1)* FAJ (2, 2) FAJ (2, 3) FAJ (1, 4) FAJ (2, 5) FAJ (2, 6) FAJ (2, 7) FAJ (1, 8) FAJ (2, 9) FAJ (2, 10) FAJ (2, 11) FAJ (1, 12) FAJ (2, 13) FAJ (2, 14) FAJ (2, 15) FAJ (1, 16)

* The first index designates the axis and the second designates the jet number (1 through 16) indicated in Figure 3.8. FAJ(I,J)=0 when jet is off. Otherwise FAJ(I,J)= $\pm F_{jet}$ depending whether the jet is directed along the positive or negative jth axis.

SPNCTR - Called from CONTRL

INPUT

Control - System Analytical Symbols	SPNCTR Symbols	Comments
ω_{1C} $\{\omega\}$ $e_{\omega LDB}$ f_{JET} ω_{1CMAG}	O1C O EOLDB FJET O1CMAG	

OUTPUT

Control-System Analytical	SPNCTR Symbols	Comments
f_{Aj}	FAJ	See Table for ATTCTR on previous page

WBLCTR - Called from CONTRL

INPUT

Control - system Analytical Symbols	WBLCTR Symbols	Comments
$\{\omega\}$	O	
$[M_{11}]$	WML1	
β	BET	equivalenced to YPRED (2)
$\dot{\beta}$	DBET	equivalenced to YPRED (1)
K_T	KT	
t_{qLIM}	TQLIM	
K_{β}	WKDBET	
$\{\dot{\omega}\}$	DO	
time	TIME	
mom _{CMG}	WMOMCM	
$I_{\beta GIM}$	WIBGIM	
err _{KT}	ERRKT	
err _{KTI}	ERRKTI	equivalenced to YPRED (3)
$\ddot{\beta}$	DDBET	
ω_{1CMAG}	OICMAG	
err _{LL}	ERRLL	
err _{LLI}	ERRLLI	equivalenced to YPRED (4)
i_s	IS	
	YICS	initial conditions of integrated controls variables
	YPRED	integrated controls variables (after T=0)
	NEQS	the number of integrated controls variables

Continued

WBLCTR (Continued)

OUTPUT

Control - system Analytical Symbols	WBLCTR Symbols	Comments
$\{\tau^A_j\}$ n_{CMG}	YDOT TAJ NCMG	time-derivative of integrated controls variables (β , $\dot{\beta}$, err_{KT} , err_{11})

EMCON - Called from LUMP

INPUT

Main program Analytical Symbols	EMCON Symbols	Comments
	IN	card input unit
	IOUT	printer output unit
all $\{R_i\}$	RI	
all $\{\dot{R}_i\}$	RID	
all $\{w^{X^i}\}$	WXI	
$\{w^X\}$	WX	
all $\{r_i\}$	RID	
all $\{\theta_i\}$	TH	
i_s	IS	
$\{w^{X^i s}\}$	O	
$\{R\}$	R	
	YICS	initial values of integrated controls variables
	YPRED	gives values $\{\dot{U}_2\}_3 = \text{YPRED (5)}$; $\{U_2\}_3 = \text{YPRED (6)}$ for $T > 0$
t	T	
$\{U_1\}$	UJ	
$\{\dot{U}_1\}$	UJD	
$\{\ddot{U}_1\}$	UJDD	
i_s		
$\{\dot{w}^X\}_s$	DO	
w_{1CMAG}	O1CMAG	
$\{\dot{R}\}$	RDDOT	value computed at previous program cycle
$\{\dot{w}^X\}$	WXDOT	value computed at previous program cycle

Continued

BMCON (Continued)

Main - program Analytical Symbols	BMCON Symbols	Comments
$\{ZCM\}$	QDD	value computed at previous program cycle
	ZCM	(after T=0) value computed at previous program cycle (Eq. (A27b), App. C, VI)
M_c	EMC	Mass of Counterweight
M	TOT	Mass of Space Station
all μ_i	U	
$\pi(\eta)$	PIETA	
$\pi(\gamma)$	PIGAM	
$\{l_0\}$	EL	
$\{l_0\}$	ELD	

OUTPUT

Main - program Analytical Symbols	BMCON Symbols	Comments
$\{U_2\}$	UJ	
$\{\dot{U}_2\}$	UJD	
$\{\ddot{U}_2\}$	UJDD	
	YDOT	YDOT (5) set to $\{\ddot{U}_2\}_3$; YDOT (6)
	NEQS	Set to $\{\dot{U}_1\}_3$ set to 2 at T=0 only

REMINDER:

UJ, UJD, UJDD contain the values of $\{U_1\}$, $\{\dot{U}_1\}$, $\{\ddot{U}_1\}$ upon entrance but are expected to contain the values of $\{U_2\}$, $\{\dot{U}_2\}$, $\{\ddot{U}_2\}$ upon exit.

EMCTR - Called from EMCON

INPUT

Control-system Analytical Symbols *	EMCTR Sym	Comments
$\{\dot{X}^B\}$	DXB	
$\{\dot{\omega}\}$	DO	
M	WM	
(m_1, m_2)	WMI	
$[\Gamma(\dot{\omega}^X s^i)]$	GDO	
$[\Gamma(\omega^X s^i)]$	GO	
$\{\dot{X}^{(1)}\}$	DXI	first column
$\{\dot{X}^{(2)}\}$	DXI	second column
m_{LEST}	WMLEST	
K_{eXSE}	WKEXSE	
K_{DESE}	WKDESE	
τ_{BAL}	TAUBAL	
ω_{LCMAG}	OLCMAG	
$\{X_{SENS/CM}^{CMND}\}$	XSCM	
$\{\dot{X}^{SENS}\}_3$	DDXSNS	
$\{\dot{X}^{(1)}\}$	DDXI	first column
ω_{LCBAL}	OLCBAL	
t	T	first element

OUTPUT

Control-system Analytical Symbols	EMCTR Sym	Comments
$\{\dot{X}^{(2)}\}$	DDXI	second column

* See Appendix H13 of Volume I.

POSCTR - Called from ATTCTR for each axis

INPUT

Control-system Analytical Symbols	POSCTR Symbols	Comments
e	E	Position error
e_{DB}	EDB	Position error dead band when $\dot{e} = 0$
\dot{e}	EDOT	
\dot{e}_{MAX}	EDOTMX	
acc_s	ACCS	Nonzero acceleration magnitude used to establish switching curves

OUTPUT

Control-system Analytical Symbols	POSCTR Symbols	Comments
acc_{NOW}	ACCNOW	Multiplier of desired acceleration (+1., 0., or -1.)

VELCTR - Called from BMCTR, SPNCTR

INPUT

Control System Analytical Symbols	VELCTR Symbols	Comments
\dot{e}	EDOT	Velocity error
\dot{e}_{DB}	EDOTDB	Velocity error dead band

OUTPUT

Control System Analytical Symbols	VELCTR Symbols	Comments
acc_{NOW}	ACCNOW	Multiplier of desired acceleration (+1., 0., or -1.)

SUPPLM - Called from ZLAB and ZCW

INPUT

Main Program Analytical Symbols	SUPPLM Symbols	Comments
	N	number of mass points on the vehicle
	K	clue set to $\begin{cases} 1 & \text{if called from ZLAB} \\ -1 & \text{if called from ZCW} \end{cases}$
	IF	clue set to $\begin{cases} 1 & \text{if supplementary forces} \\ & \text{are to be computed} \\ 0 & \text{if supplementary forces} \\ & \text{are not to be computed} \end{cases}$

OUTPUT

Main Program Analytical Symbols	SUPPLM Symbols	Comments
all $\{r_s^i\}$ (or $\{\bar{r}_s^i\}$)	A	$\{f_c^i\}$ (or $\{\bar{f}_c^i\}$) begins at A (3i-2) (see Note)
all $\{\tau_s^i\}$ (or $\{\bar{\tau}_s^i\}$)	A	$\{\tau_c^i\}$ (or $\{\bar{\tau}_c^i\}$) begins at A (3i+1) (see Note)

NOTE:

Supplementary forces and torques are computed for the

$\begin{cases} \text{Laboratory when } K = 1 \\ \text{Counterweight when } K = -1 \end{cases}$

LOOK - Called from LUMP

INPUT

Main program Analytical Symbols	LOOK Symbols	Comments
j	L	moving mass no.

OUTPUT

Main program Analytical Symbols	LOOK Symbols	Comments
k	M	no. of influencing values.
	K	values of k which influence μ ,

APPENDIX B6

INPUT, OUTPUT, AND INTERMEDIATE FILESFILE 1 - intermediate file

File number 1 is used for intermediate data to be used by the plotting program. Write statements are in MAIN and MINCY. Read statements are in PLO3AX.

FILE 11 - input file

Contains Phase I input for the Laboratory. READ statements are in COMMUN.

FILE 12 - input file

Contains Phase I input for the Counterweight. READ statements are in COMMUN.

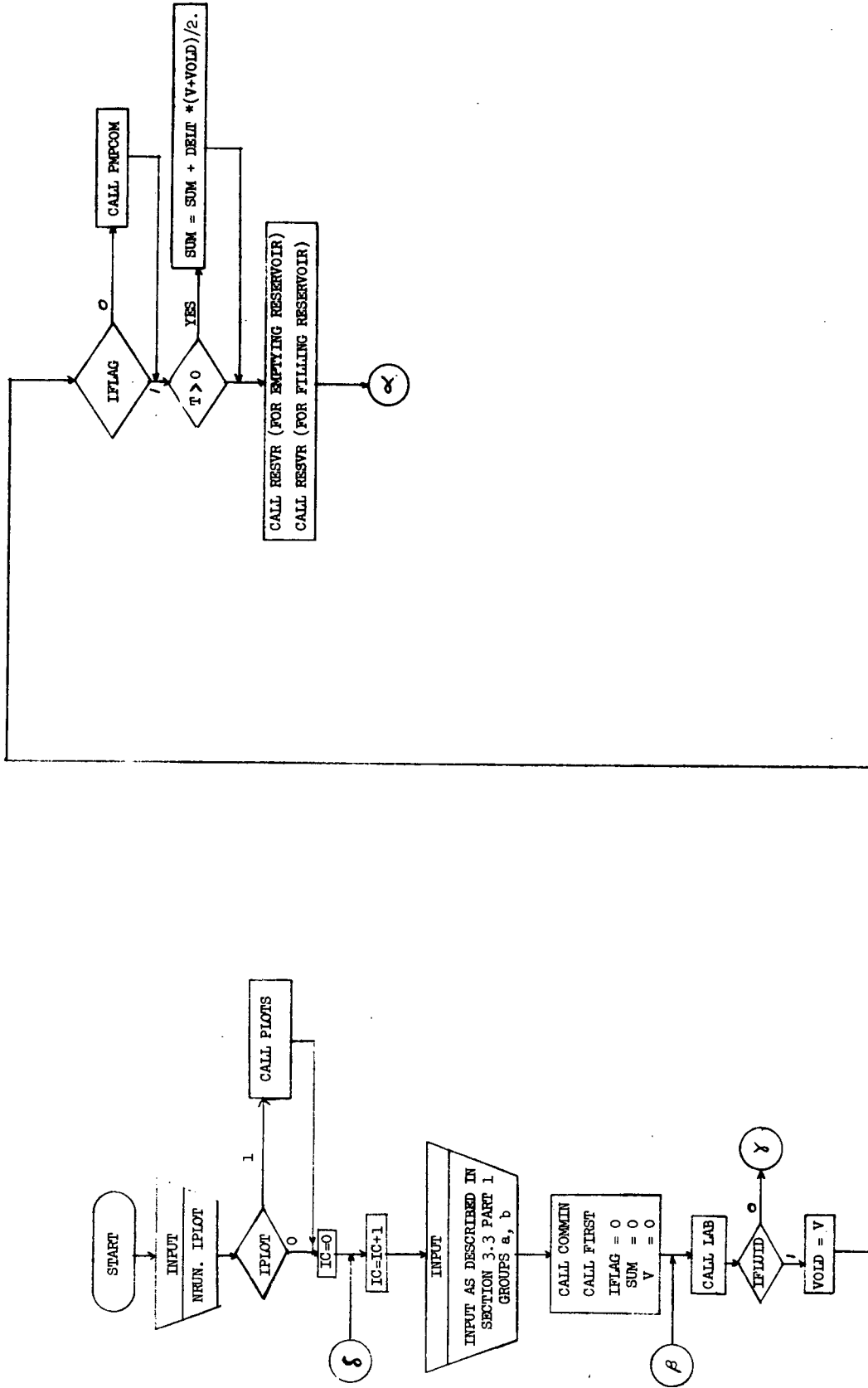
APPENDIX B7

FLOW CHARTSFortran Symbols Used in Flow Charts*

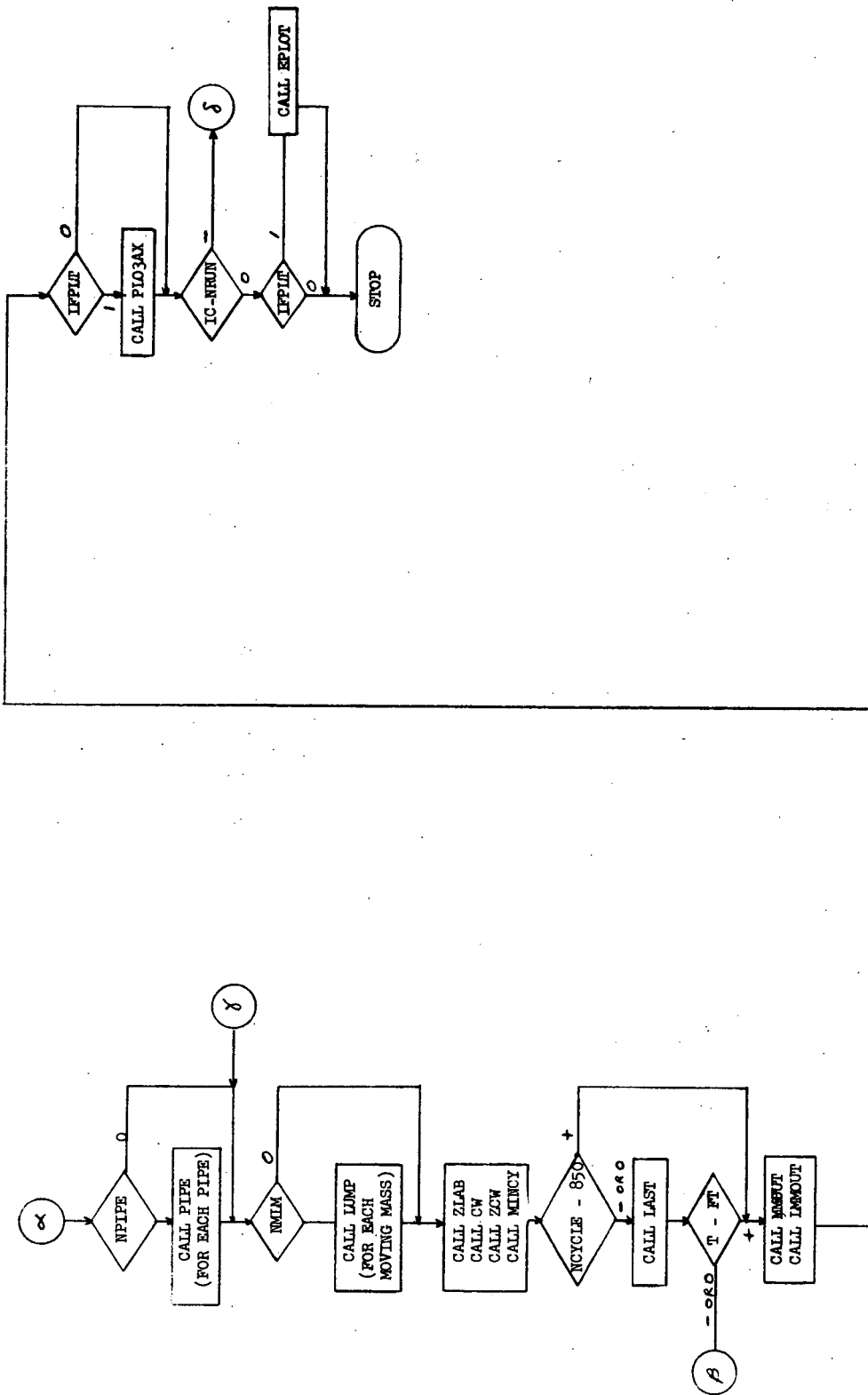
- IFLAG - set to 1 when emptying reservoir becomes empty or when filling reservoir becomes full
- SUM - $\int_0^T V dt$ where V is fluid velocity in pipe
- DELT - time increment
- IPLLOT - set to 1 if plotting is present for any run on the job
- IFPLT - set to 1 if plotting is present for the current run
- T - Time
- IFLUID - fluid clue: set to 1 if fluids are present, set to 0 if not
- NPIPE - number of pipes present
- NMLM - number of moving lumped masses
- NCYCLE - number of output cycles
- FT - final time
- KLUE - problem clue (see Section 3.3, Part 1, Group c)
- LABCW - argument of CONTROL subroutine indicating whether subroutine was called from ZLAB (LABCW=1) or from ZCW(LABCW=-1)
- YICS - vector of initial conditions used in MAGIC integration
- YDOT - vector of derivatives to be integrated by MAGIC
- NTIME - } see Section 3.3, Part 10, Group 6
- DTAU - }
- MAGOUT - Magic output clue. Magic sets MAGOUT=2 to indicate an output cycle
- IFDEPL - deployment clue: set to 1 if deployment is present, set to 0 if not
- IFCON - controls clue: set to 1 if controls are present, set to 0 if not

*For analytical symbols see Volume 1, Section 4.

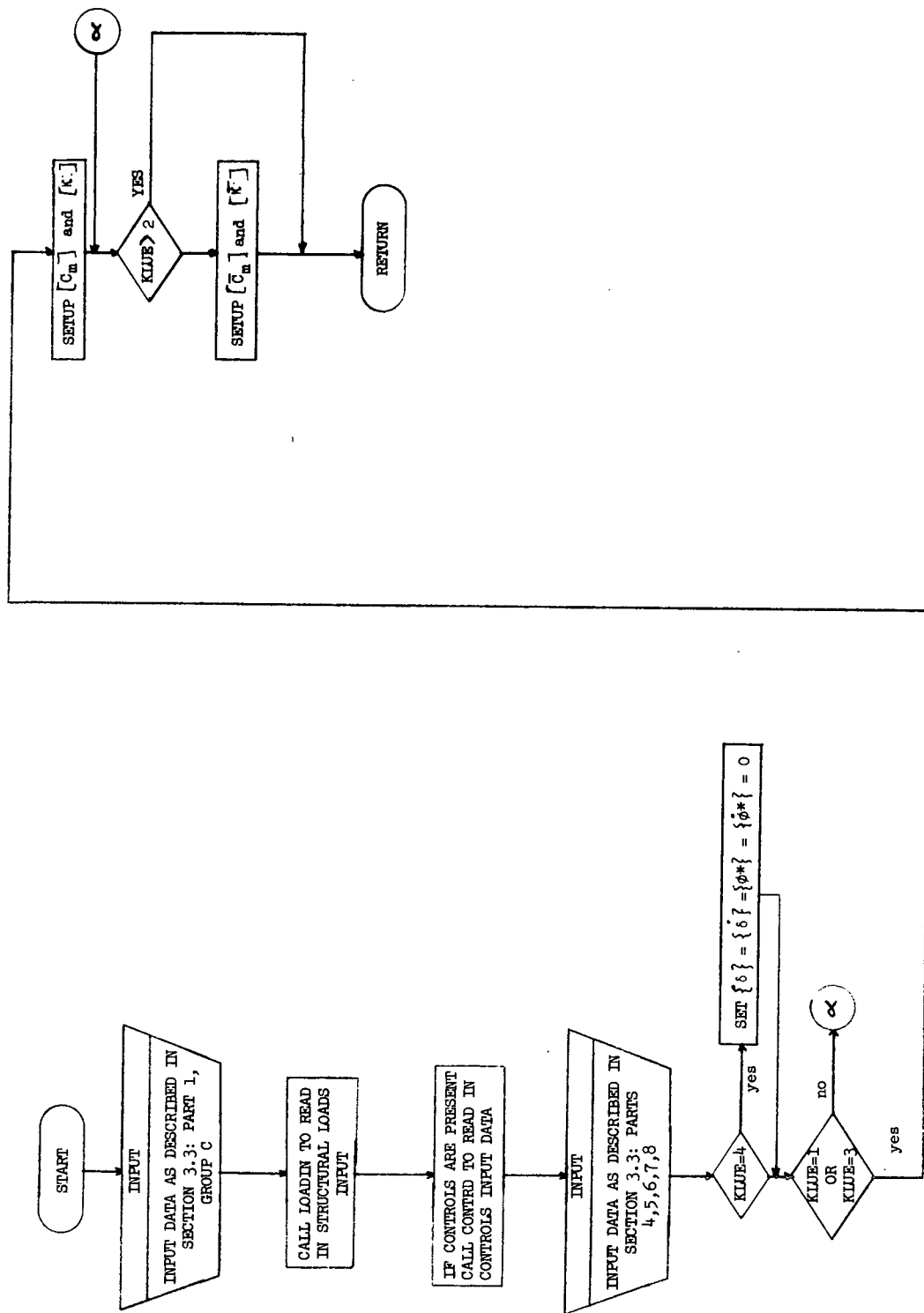
MAIN PROGRAM



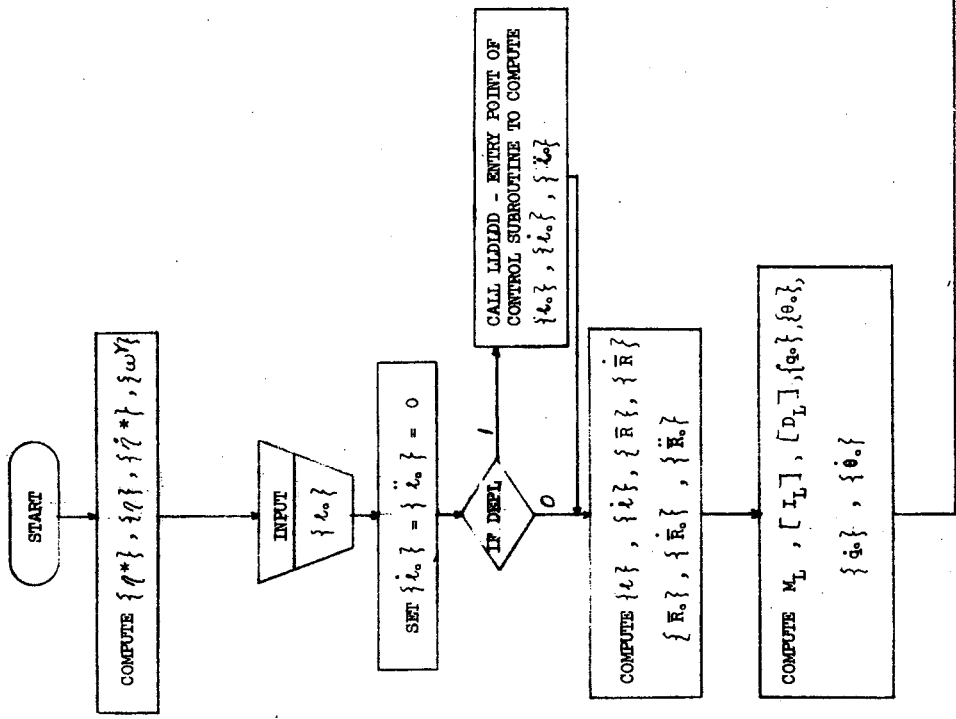
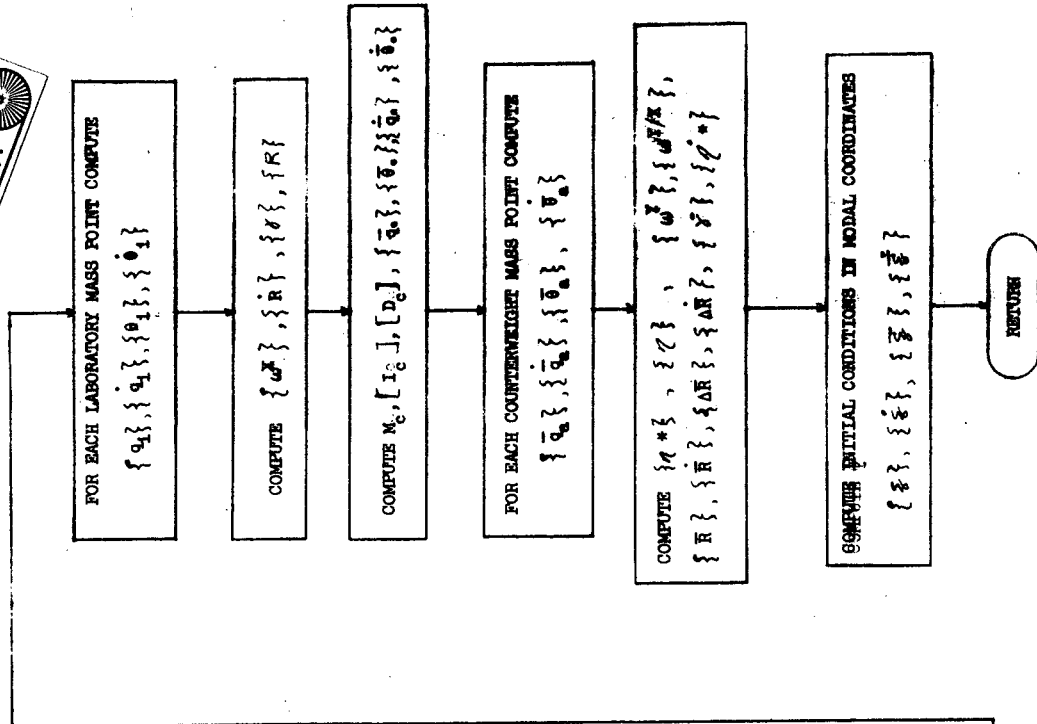
MAIN PROGRAM



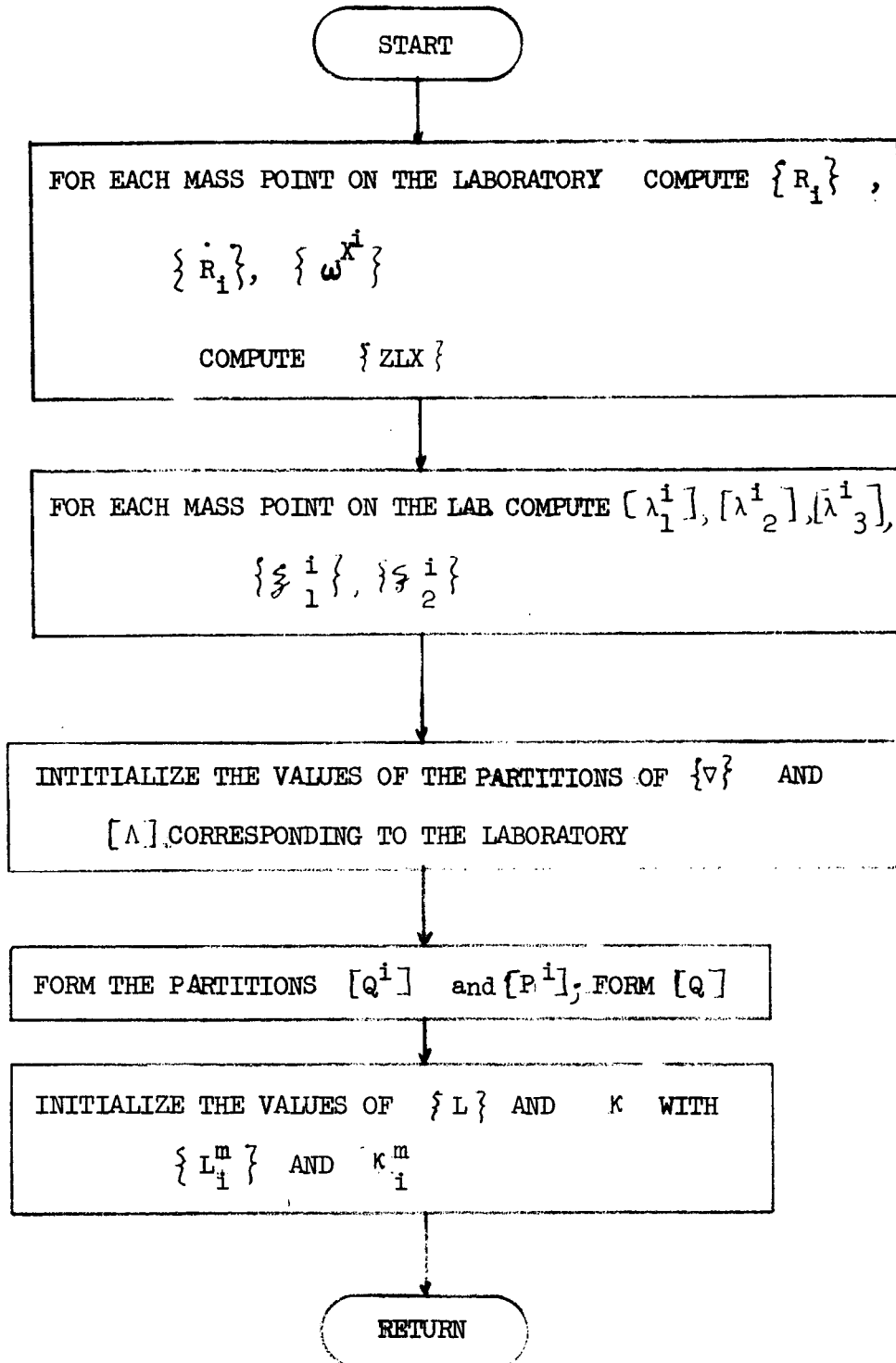
COMMIN



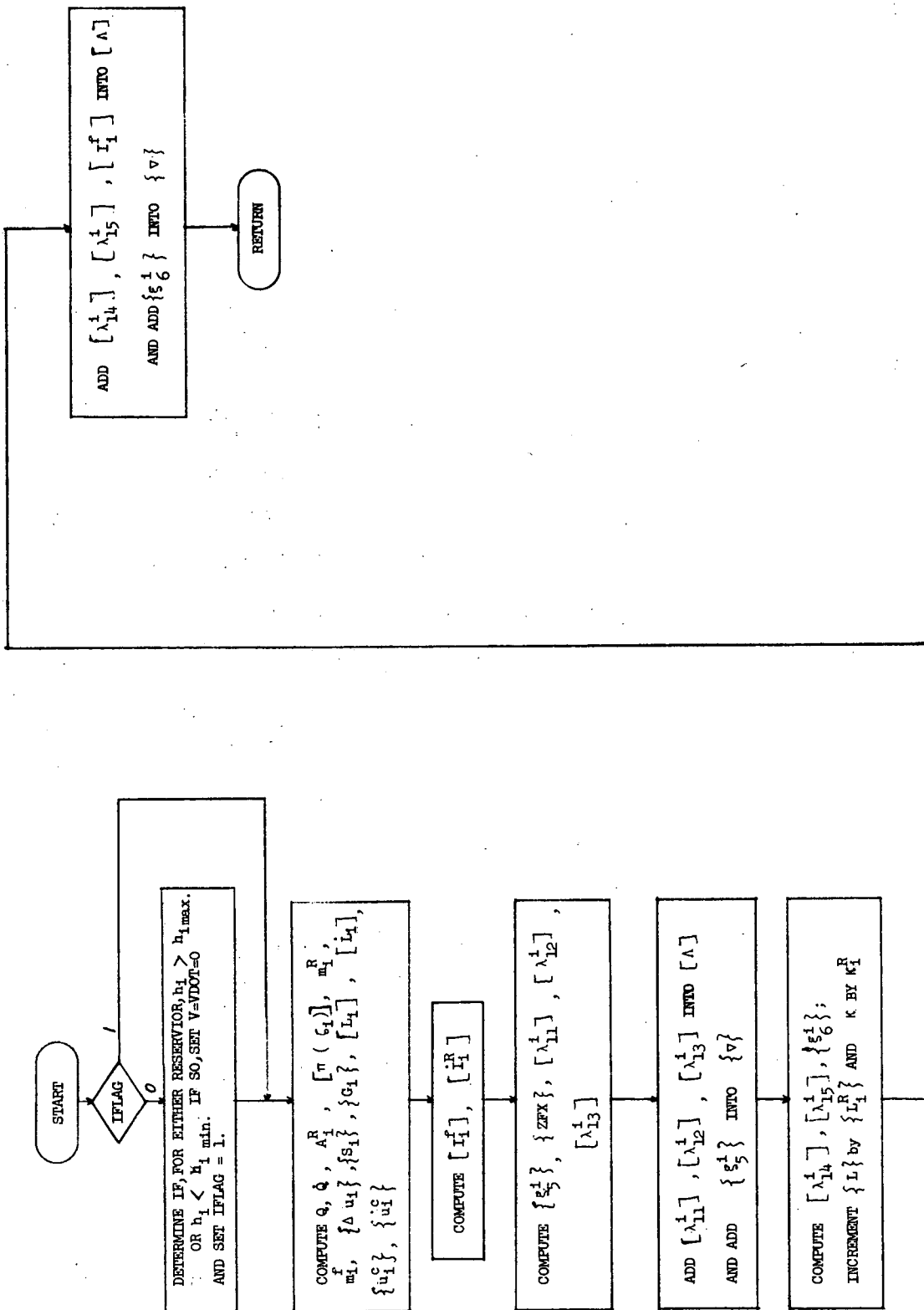
Reproduced from
best available copy.



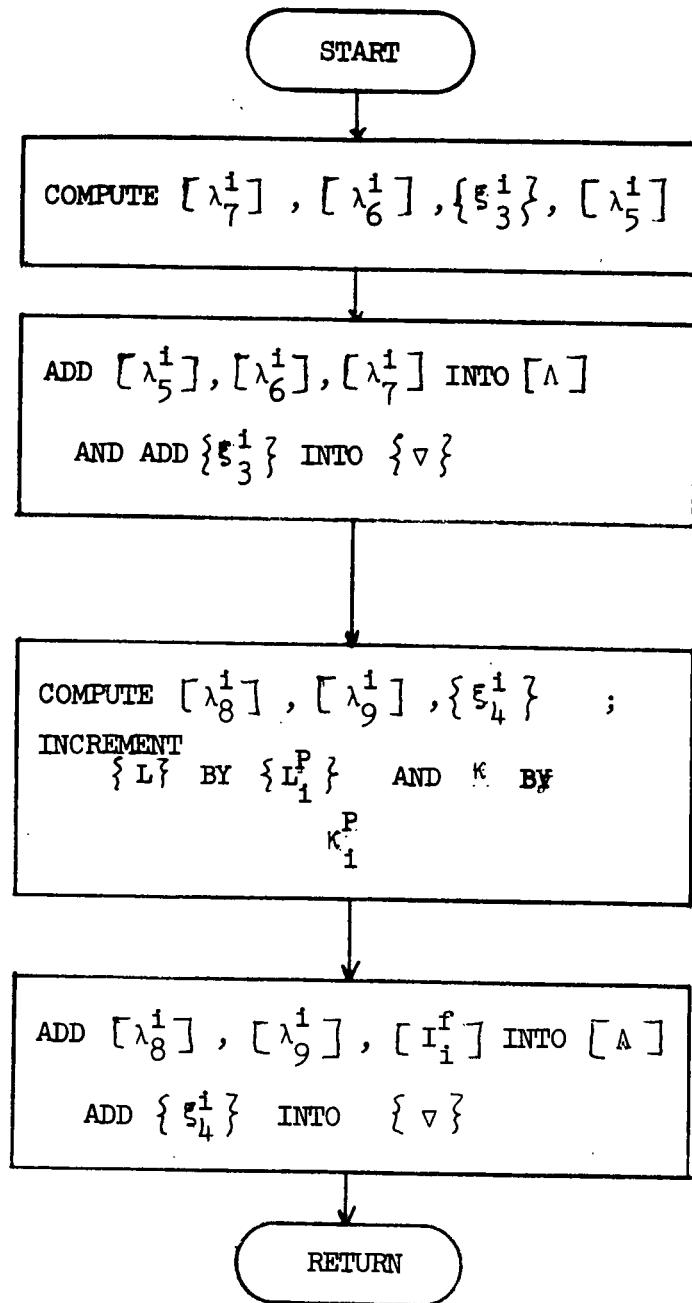
FIRST

LAB

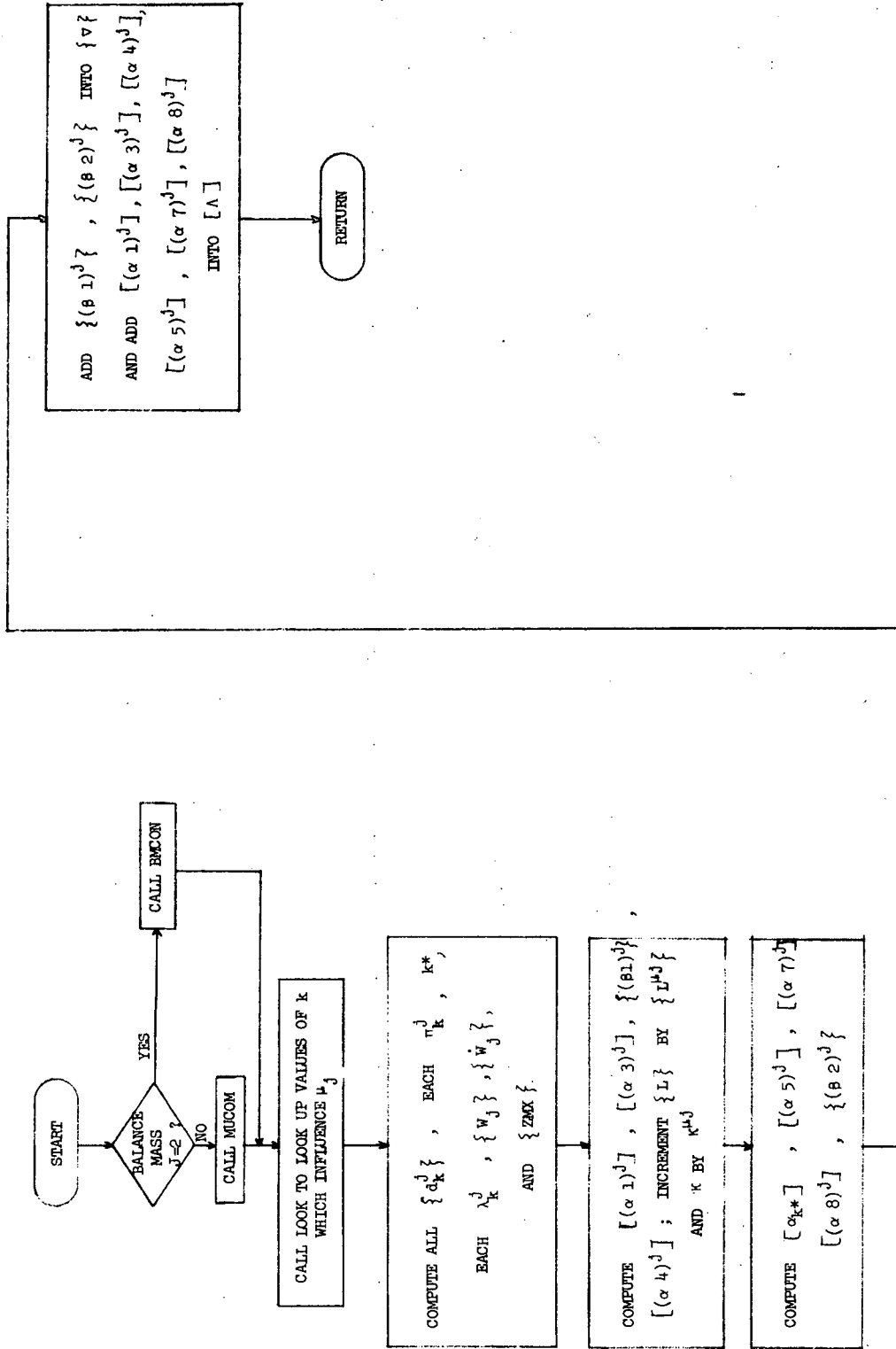
RESVR

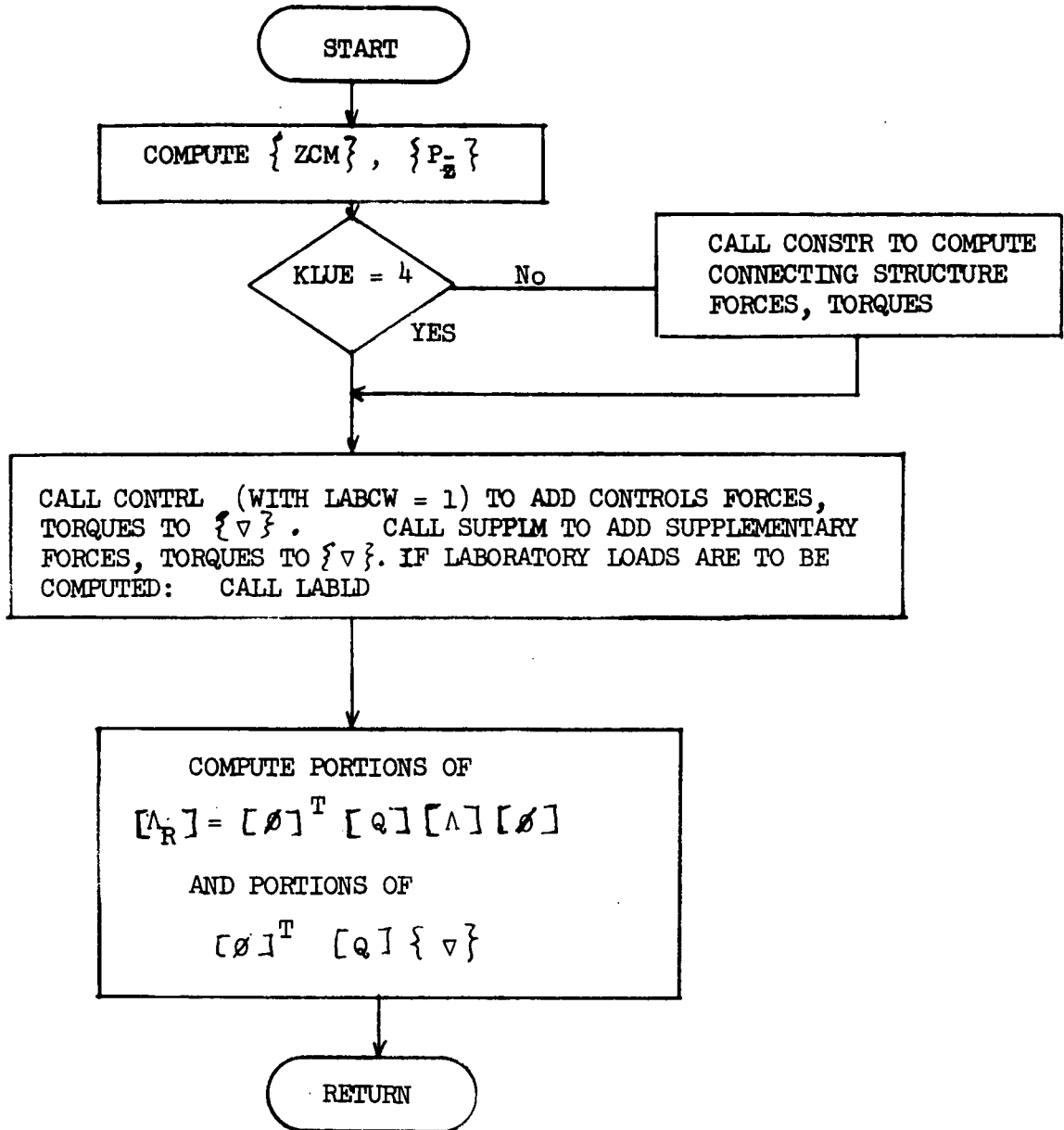


C4

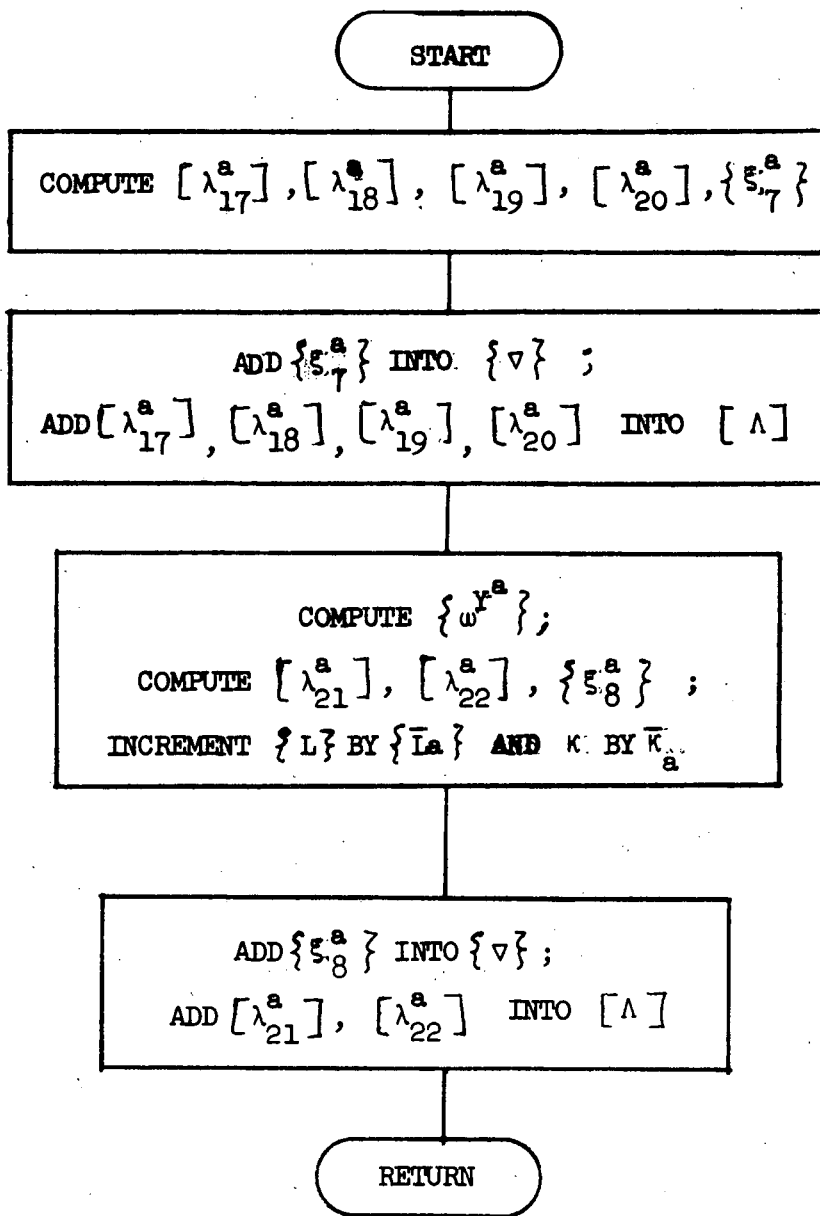
PIPE

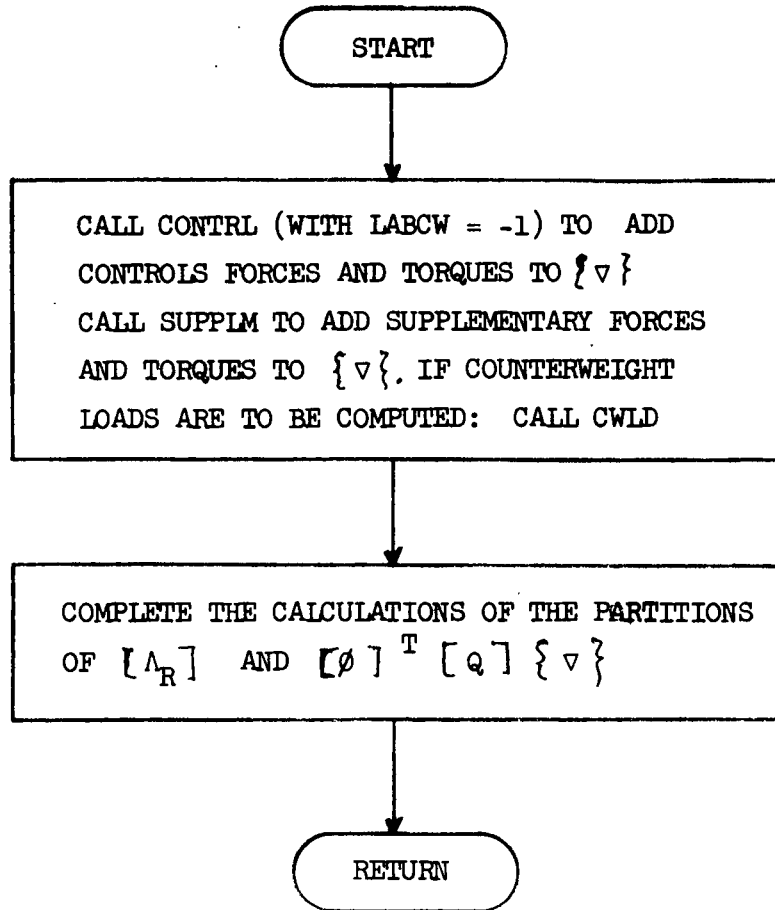
LJMF

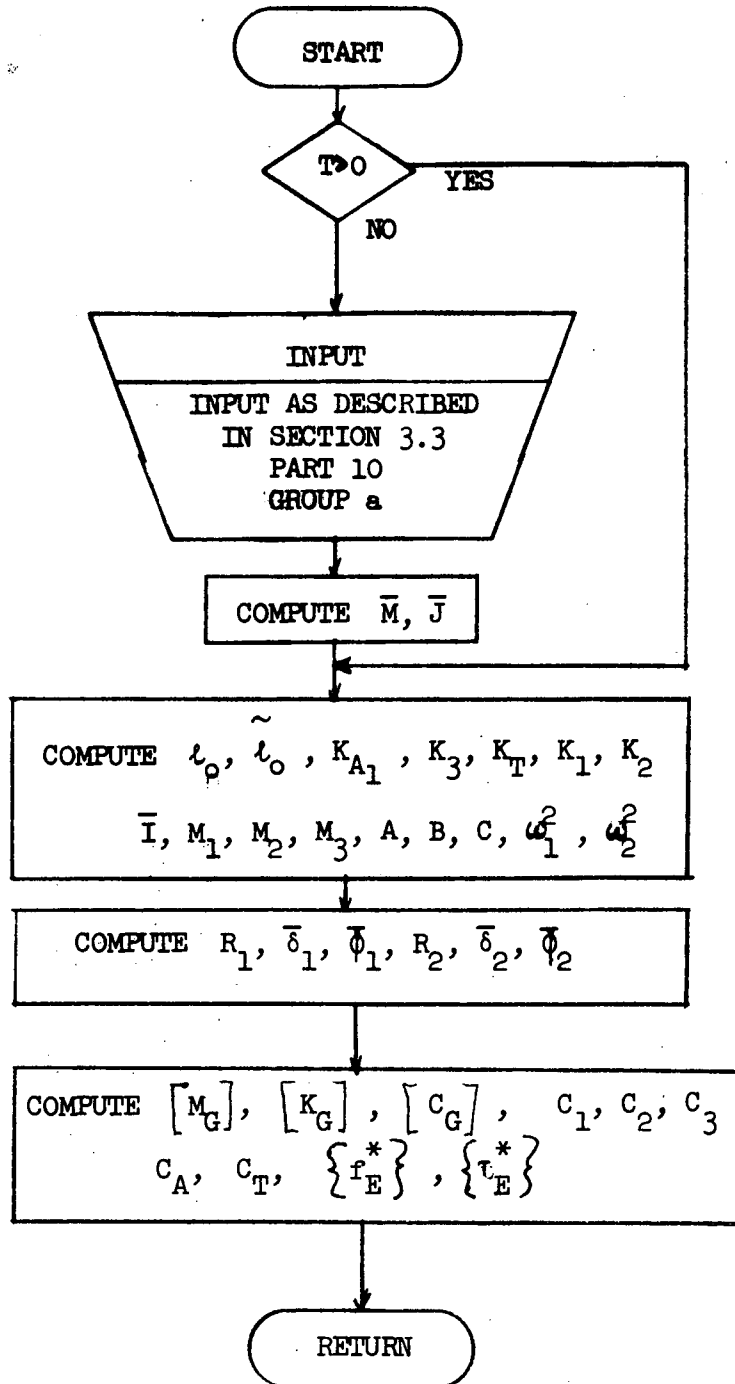


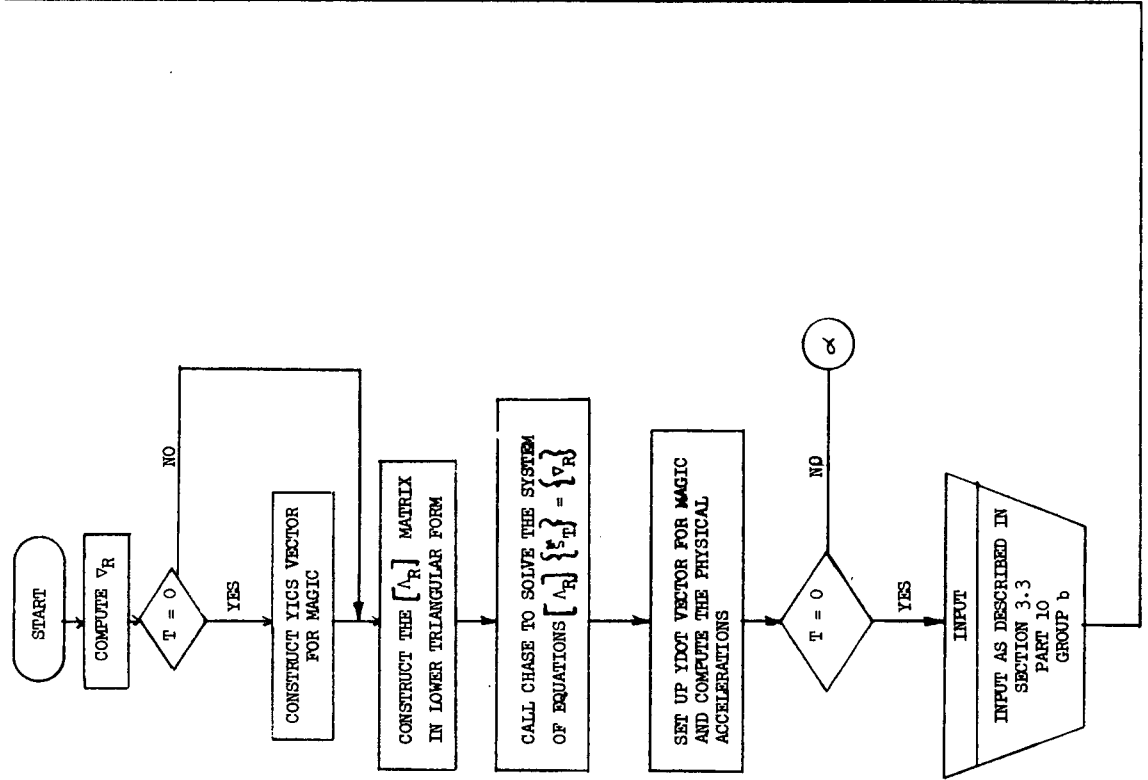
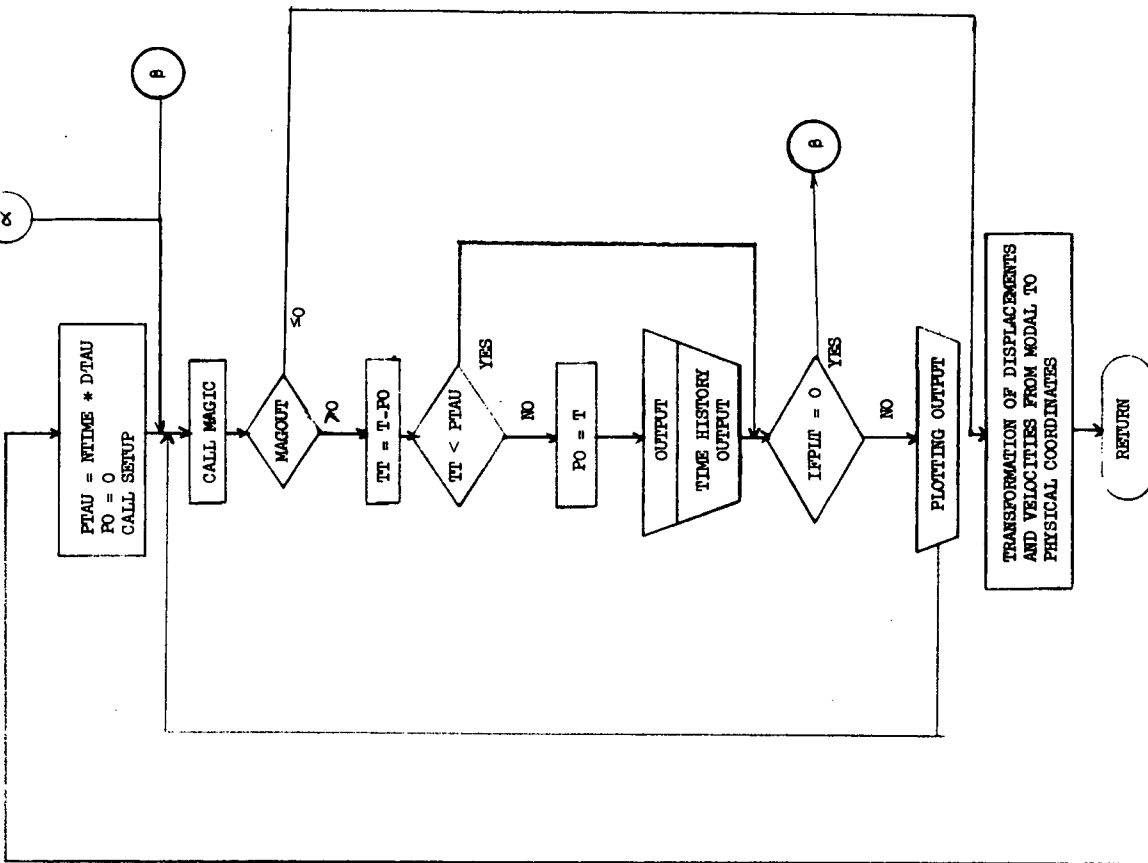
ZLAB

CW

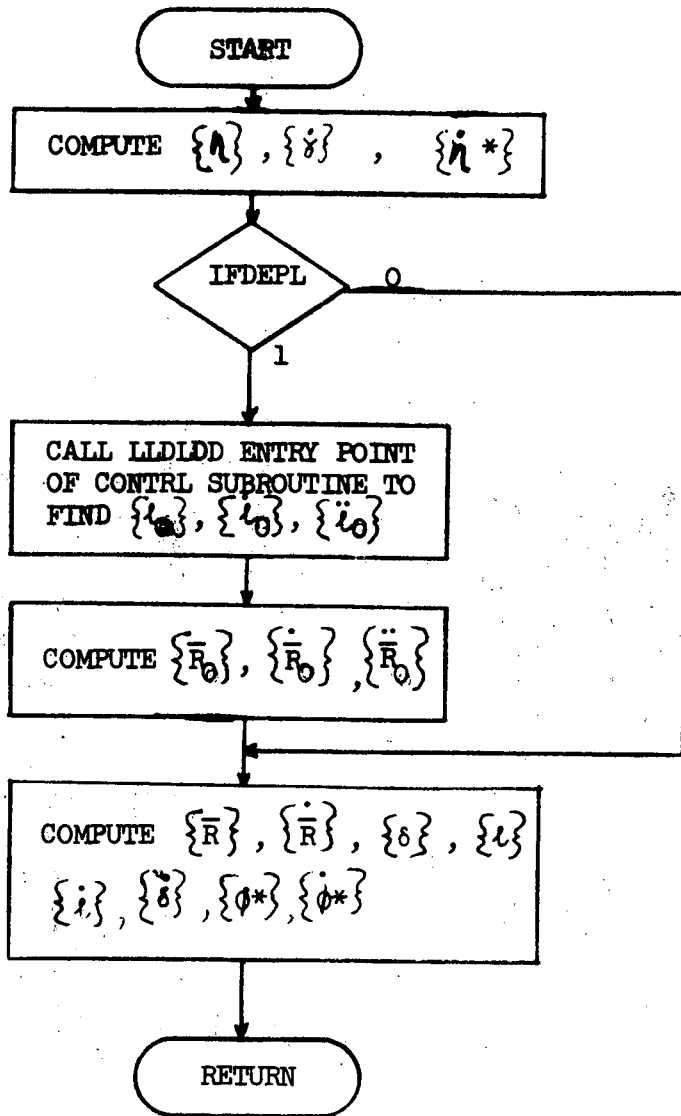


ZCW

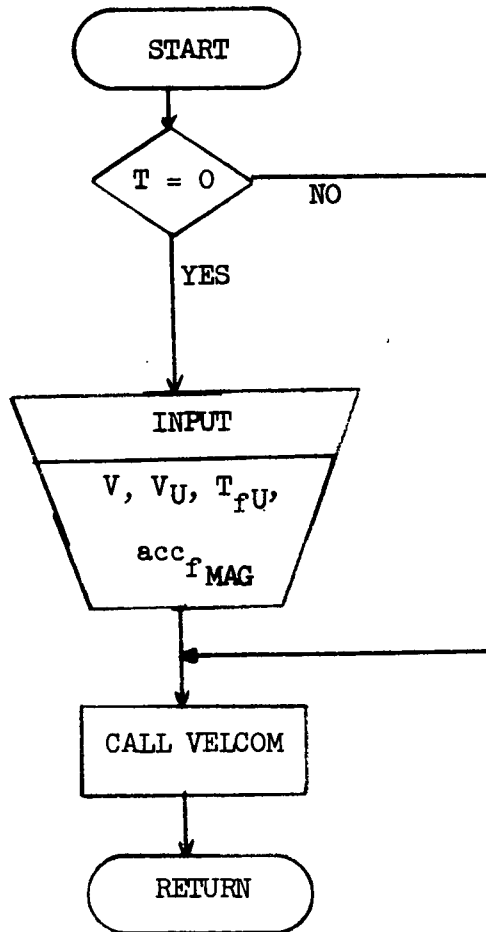
CONFER



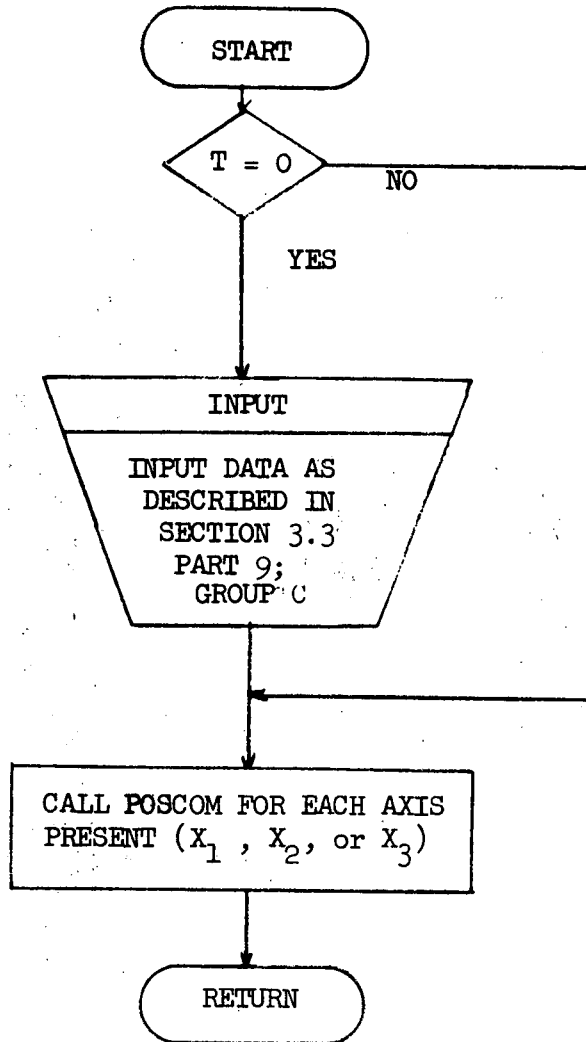
LAST



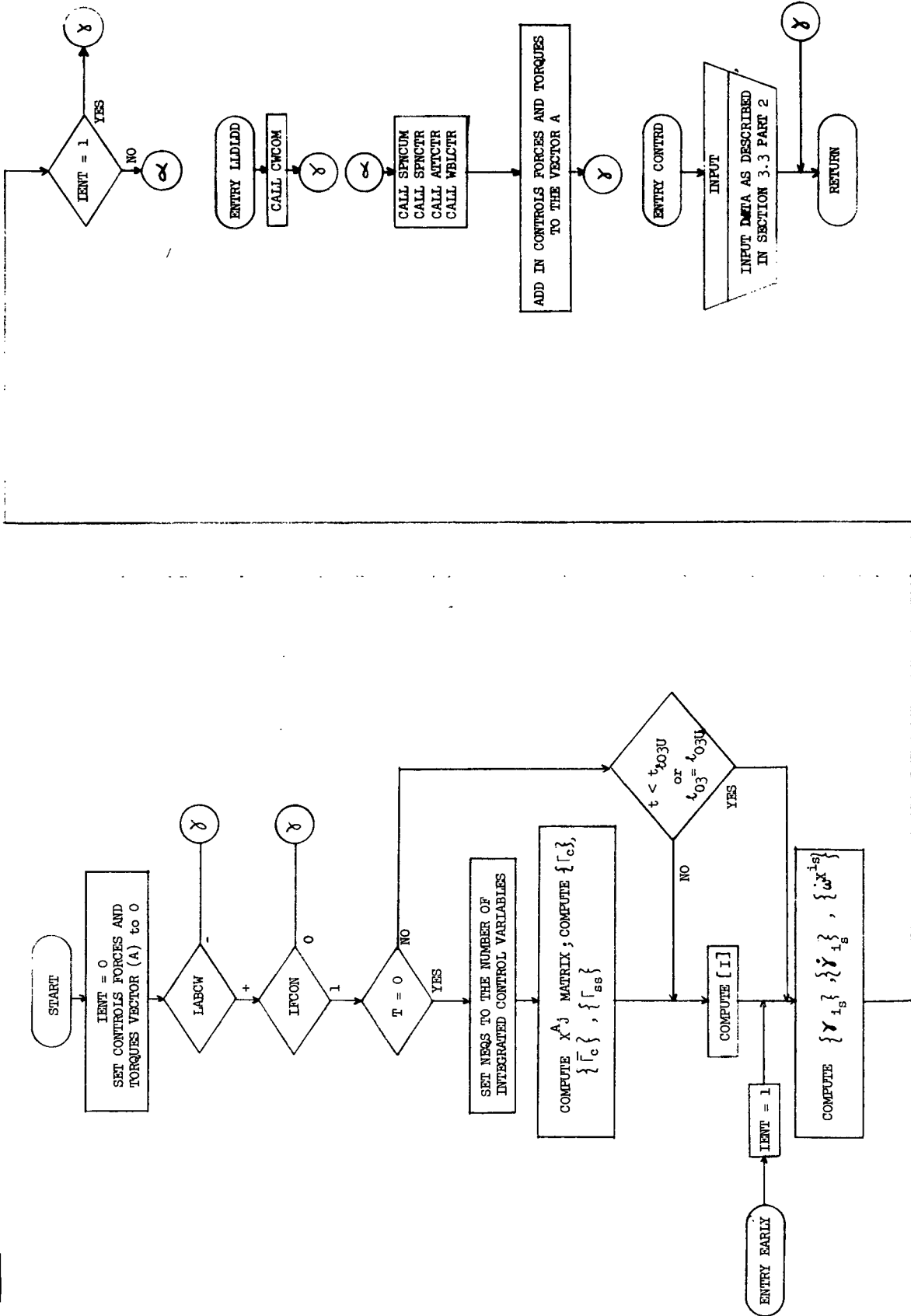
PMPCOM

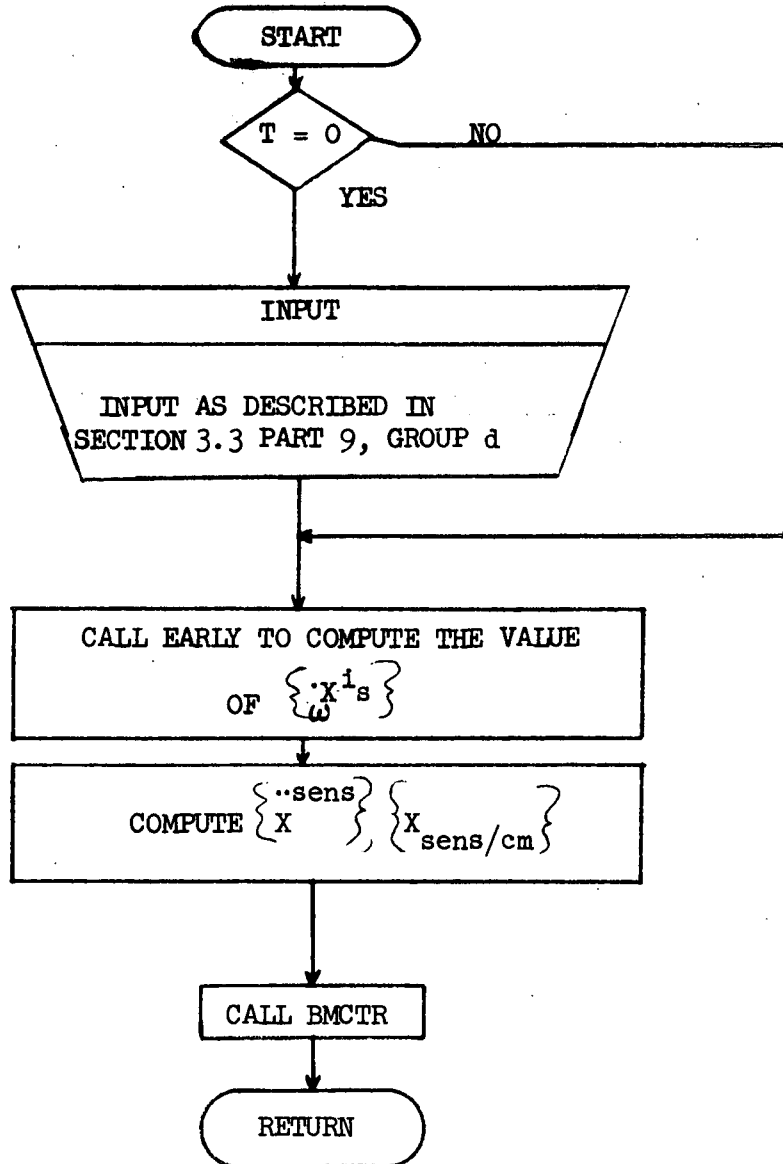


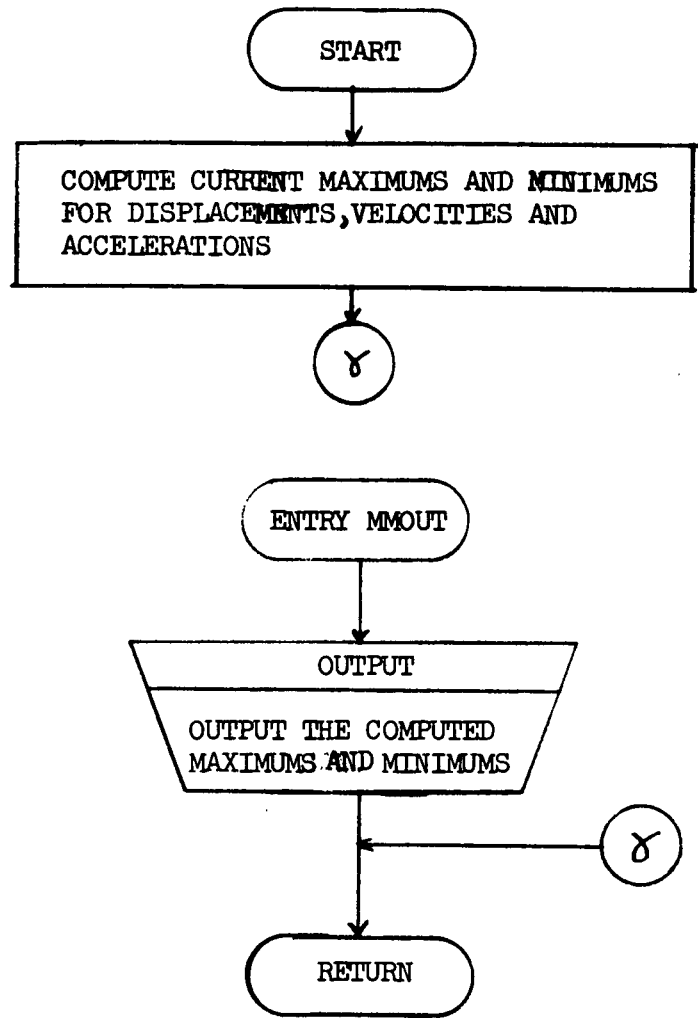
MUCOM



CONTROL

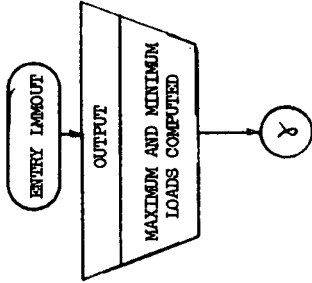
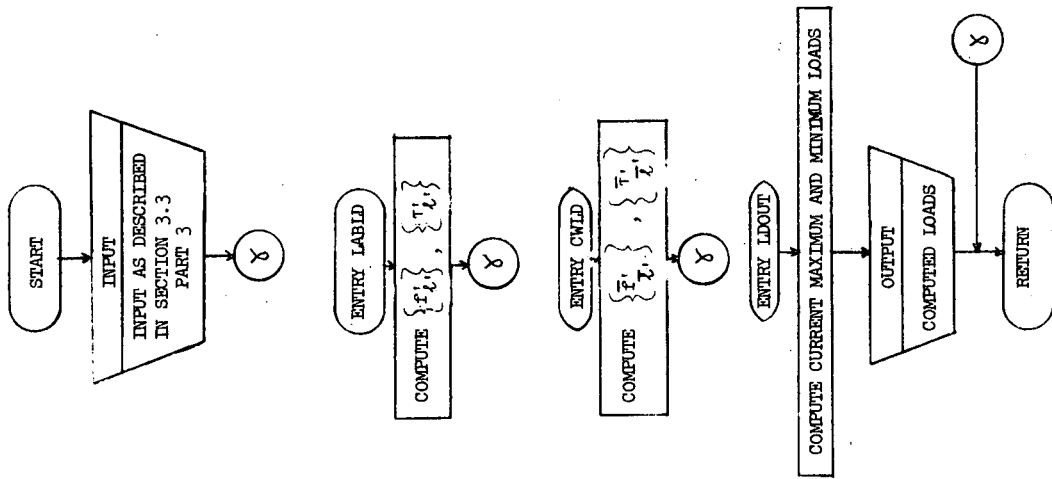






7

LOADIN



APPENDIX B8

FORTRAN SOURCE DECK LISTING

The CDC LRC version of the program appears on the following pages.

**** YOUR SEQUENCED PROGRAM FOLLOWS ****

* SEQUENCE *
* FOR MODS *

```

PROGRAM STATION(INPUT, OUTPUT, TAPE5=INPUT, TAPE6=OUTPUT,
* TAPE1, TAPE11, TAPE12)
C 00020 100000
C 00030 200000
C 00010 300000
C 00040 400000
C 00050 500000
C 00060 600000
C 00070 700000
C 00080 800000
C 00090 900000
C 00100 1000000
C 00110 1100000
C 00120 1200000
C 00130 1300000
C 00140 1400000
C 00150 1500000
C 00160 1600000
C 00170 1700000
C 00180 1800000
C 00190 1900000
C 00200 2000000
C 00210 2100000
C 00220 2200000
C 00230 2300000
C 00240 2400000
C 00250 2500000
C 00260 2600000
C 00270 2700000
C 00280 2800000
C 00290 2900000
C 00300 3000000
C 00310 3100000
C 00320 3200000
C 00330 3300000
C 00340 3400000
C 00350 3500000
C 00360 3600000
C 00370 3700000
C 00380 3800000
C 00390 3900000
C 00400 4000000
C 00410 4100000

```

PROGRAM STATION(INPUT, OUTPUT, TAPE5=INPUT, TAPE6=OUTPUT, TAPE1, TAPE11, TAPE12)

C DYNAMICS OF ROTATING SPACE STATIONS
C PHASE II, NUMERICAL INTEGRATION

COMMON/INOUT/ IN, IOUT, IOFF, IC, IPLOUT(14)

* N1, N2, N3, N4, N5, N6, N7
COMMON /CLUES/IFPLT, IFLUID, NPIPE, NMLM, MLM, IRES, IPIPES

COMMON T, R, RDOT, XIDEN, RHO, A, Z(12009)

COMMON /PASS/Q1(3)

COMMON /LABOR/Q2(2503)

COMMON /CWT/Q3(2512)

COMMON /RES/Q4(88)

COMMON /PIPES/Q5(1020)

COMMON /LUMPS/Q6(8)

COMMON /LOADS/Q7(1912)

COMMON /VAROUT/Q8(108)

COMMON /BIG/Q9(34466)

COMMON /CONNECT/Q10(47)

COMMON /NEWCOM/Q11(191)

COMMON /EXTRA/Q12(17)

COMMON /OPT2/Q13

COMMON /ALLCNT/Q14(94)

COMMON /WINTER/Q15

COMMON /BOND/Q16(2)

COMMON /LODPAS/Q17(113)

EQUIVALENCE (T, D)

DOUBLE PRECISION D

DIMENSION R(3), RDOT(3), XIDEN(3, 3), MLM(8), IRES(2), IPIPES(30)

IN=5

IOUT=6

READ(IN, 1)NRUN, IPLOUT

IF(IPLOUT.EQ.1)CALL CALCOMP

DO 15 IC=1, NRUN

WRITE(IOUT, 400)

400 FORMAT(1H1, 20(/), 47X, #DYNAMICS OF ROTATING SPACE STATIONS*///

* 61X, #PHASE II*///54X, #NUMERICAL INTEGRATION#)

READ(IN, 2)FT, DTPLTOT

T=0

```

C TO PLOT RESULTS USE IFPLT=1.
C NO MORE THAN 950 TIME INTERVALS ARE PLOTTED.
C DTPLOT = NO. SECS. / INCH
C READ(IN,4)IFPLT,IFLUID,NPIPE,NMLM,MLM,MLM,IRES,
* (IPIPES(I),I=1,NPIPE)
WRITE(IOUT,6)
6 FORMAT('INPUT DATA#//')
WRITE(IOUT,700)FT,IFPLT,DTPLOT,IFLUID,NPIPE,IRES,NMLM,MLM,
* (IPIPES(I),I=1,NPIPE)
700 FORMAT(5X,#FINAL TIME , PLOTTING CLUE , PLOT INTERVAL*/E16.8,6X,I1C
*,10X,E15.8/* FLUID CLUE , NO. PIPES*/6X,I1,I1X,I2/
** RESERVOIR MASS POINTS*/1X,2I4/* NO. MOVING MASSES ,
*G MASSES PRESENT #/7X,I2,I2X,8I4/* PIPES ON MASS POINTS*/30I4)
PBLOCK=1.
IF(IFPLT.GT.0)READ(IN,800)IPLUT
IF(IFPLT.GT.0)READ(IN,802)N1,N2,N3,N4,N5,N6,N7
802 FORMAT(7I3)
800 FORMAT(14I1)
DO 900 I=1,13
900 IF(IPLUT(I).EQ.1)PBLOCK=PBLOCK+1
IF(IFPLT.EQ.1)WRITE(I)IC,PBLOCK,FT,DTPLOT
CALL COMM(NLAB,NCW,NPIPE,NMLM,IFLUID,MLM,IPIPES)
SUM=0.
IFLAG=0
V=0.
10 CONTINUE
CALL LAB(NLAB)
IF(IFLUID.EQ.0)GO TO 100
VOLD=V
IF(IFLAG.EQ.0)CALL PMPCOM(V,VDDT)
IF(T.EQ.0)GO TO 98
SUM=SUM+DELT*(V+VOLD)/2.
98 CONTINUE
CALL RESVR(1,IRES(1),SUM,V,VDDT,IFLAG)
CALL RESVR(2,IRES(2),SUM,V,VDDT,IFLAG)
IF(NPIPE.EQ.0)GO TO 100
DO 40 I=1,NPIPE
40 CALL PIPE(I,IPIPES(I),V,VDDT)
100 IF(NMLM.EQ.0)GO TO 200
DO 50 I=1,8
50 IF(MLM(I).EQ.0)GO TO 50
CALL LUMP(I,MLM(I))
50 CONTINUE
200 CALL ZLAB(NLAB,NCW)
CALL CW(NCW)
CALL ZCW(NCW)
CALL MINCY(NLAB,NCW,DELT,NCYCLE,V,VDDT)
IF(NCYCLE.GT.850)GO TO 851
CALL LAST (NLAB,NCW)
IF(T.LE.FT)GO TO 10

```

4200000

C 00420

4300000

C 00430

4400000

C 00440

4500000

C 00450

4600000

C 00460

4700000

C 00470

4800000

C 00480

4900000

C 00490

5000000

C 00500

5100000

C 00510

5200000

C 00520

5300000

C 00530

5400000

C 00540

5500000

C 00550

5600000

C 00560

5700000

C 00570

5800000

C 00580

5900000

C 00590

6000000

C 00600

6100000

C 00610

6200000

C 00620

6300000

C 00630

6400000

C 00640

6500000

C 00650

6600000

C 00660

6700000

C 00670

6800000

C 00680

6900000

C 00690

7000000

C 00700

7100000

C 00710

7200000

C 00720

7300000

C 00730

7400000

C 00740

7500000

C 00750

7600000

C 00760

7700000

C 00770

7800000

C 00780

7900000

C 00790

8000000

C 00800

8100000

C 00810

8200000

C 00820

8300000

C 00830

8400000

C 00840

8500000

C 00850

8600000

C 00860

8700000

C 00870

8800000

C 00880

8900000

C 00890

9000000

C 00900

9100000

C 00910

9200000

C 00920

```

851 WRITE(IOUT,500)
500 FORMAT(///34H ***** END OF TIME HISTORY ***** /IHL,20X,
* 22H STATISTICS DURING RUN //)
CALL MMOUT(NLAB,NCW)
CALL LMMOUT
IF((IPLT.EQ.0)GO TO 15
END FILE 1
CALL PLG3AX
15 CONTINUE
IF((IPLT.EQ.1)CALL CALPLT(0.,0.,999)
99 STOP
1 FORMAT(2I2)
2 FORMAT(2E15.8)
4 FORMAT(4I3/8I3/2I3/(15I3))
END

```

9300000
9400000
9500000
9600000
9700000
9800000
9900000
10000000
10100000
10200000
10300000
10400000
10500000
10600000
10700000

```

SUBROUTINE COMM(NLAB,NCW,NPIPE,NMLM,IFLUID,MLM,IPIPES)
COMMON T,R,RDQT,XIDEN,RHO,A,YA,YB,NMPO(17),FRQLAB(20),FRQCM(20),
* DAMP(20),DAMPS(20)
COMMON /LABUR/WX,R10,Q,QD,TH,THD,XMAS,XINERT
COMMON /CWT/RB,KBD,ETA,WY,RAO,QB,ORD,THB,THBD,XMBAR,XIBAR
COMMON /RES/XMP,XIIP,SIP,UIR,FIR,UIB,EIB,XJIB,BI,HIO,
* HIMAX,HIMIN,GIP,XLI
COMMON /PIPES/XNIF,XIF,S,DELU,DELF,G,DELLJ,VEC
COMMON /LUMPS/U
COMMON /INDUT/IN,IQUT,IOFF
COMMON /LOADS/ZZ(585),DD(1212)
COMMON /VAROUT/ZFRL(16),NZER,ZER2(88)
COMMON /BIG/DUM(40),UMASS(20),NMCW,SMODE(600,20)
* NMLAB,RMODE(600,20),NMCW,SMODE(600,20)
COMMON /CONNECT/IBAR,SS(3),IARAR,SSAR(3),DEL(3),DELDOT(3),
* PHIST(3),PHISTD(3),XX(16),GAMMA(3)
COMMON /NEWCOM/XXX(107),IFDEPL,KLUE,KCM(20,4),IFCON,IFSUPP
DIMENSION R(3),RDQT(3),XIDEN(3,3),WX(3),R10(3,100),Q(3,100),
* QD(3,100),TH(3,100),THD(3,100),RB(3),RBD(3),ETA(3),
* WY(3),RAO(3,100),QB(3,100),QBD(3,100),THR(3,100),
* THBD(3,100),XMAS(100),XINERT(3,3,100)
DIMENSION XMP(2),XIIP(3,3,2),SIP(3,2),UIR(3,2),EIR(3,2),UIR(3,2),
* EIB(3,2),XJIB(3,3,2),GIP(3,2),XLI(3,2),BI(2),HI(2),
* HIMAX(2),HIMIN(2),YA(3),YB(3)
DIMENSION XMBAR(100),XIBAR(3,3,100)
DIMENSION XNIF(30),XIF(3,3,30),S(3,30),DELU(3,30),DELE(3,30),
* G(3,30),DELLJ(3,3,30),VEC(3,30)
DIMENSION U(8),MLM(8),IPIPES(30)
REAL KCM
DO 196 I=1,16
196 ZER1(I)=0.
DO 197 I=1,90
197 ZER2(I)=0.
NZER=0.
DO 210 I=1,1212
210 DD(I)=0.
NMLAB=0
NMCW=0
DO 10 I=1,3
DO 20 J=1,3
20 XIDEN(I,J)=0.
10 XIDEN(I,I)=1.
C READ DEPLOYMENT CLUE AND RIGID PROBLEM CLUE
C READ DEPLOYMENT CLUE AND RIGID PROBLEM CLUE
C READ DEPLOYMENT CLUE AND RIGID PROBLEM CLUE
READ(IN,2)KLUE,IFLAB,IFCW,IFCN
READ(IN,2)IFDEPL,IFCON,IFSUPP
WRITE(10UT,700)KLUE,IFDEPL,IFCON,IFSUPP
700 FORMAT(* CLUES FOR THIS RUN*/ * PROBLEM CLUE , DEPLOYMENT , CONTROL
C 01050
C 01060
C 01070
C 01080
C 01090
C 01100
C 01110
C 01120
C 01130
C 01140
C 01150
C 01160
C 01170
C 01180
C 01190
C 01200
C 01210
C 01220
C 01230
C 01240
C 01250
C 01260
C 01270
C 01280
C 01290
C 01300
C 01310
C 01320
C 01330
C 01340
C 01350
C 01360
C 01370
C 01380
C 01390
C 01400
C 01410
C 01420
C 01430
C 01440
C 01450
C 01460
C 01470
C 01480
C 01490
C 01500
C 01510
C 01520
C 01530

```

```

#S, SUPP. FORCES*/6X,I2,I2X,I2,10X,I2,10X,I2)
IF(IFCON.GT.0)CALL CONTRD
CALL LCADIN
READ(IN,2)IPHS1,JUMP
IF(IPHS1.EQ.0)GO TO 5

```

Line	Code	Text	Address
15	C	PHASE I INPUT FOR LAB	15700000
	C		15800000
	C		15900000
	C		16000000
	C		16100000
	C		16200000
	C		16300000
	C		16400000
	C		16500000
	C		16600000
	C		16700000
	C		16800000
	C		16900000
	C		17000000
	C		17100000
	C		17200000
	C		17300000
	C		17400000
	C		17500000
	C		17600000
	C		17700000
	C		17800000
	C		17900000
	C		18000000
	C		18100000
	C		18200000
	C		18300000
	C		18400000
	C		18500000
	C		18600000
	C		18700000
	C		18800000
	C		18900000
	C		19000000
	C		19100000
	C		19200000
	C		19300000
	C		19400000
	C		19500000
	C		19600000
	C		19700000
	C		19800000
	C		19900000
	C		20000000
	C		20100000
	C		20200000
	C		20300000
	C		20400000
	C		20500000
	C		20600000
	C		20700000
	C		20800000
	C		20900000
	C		21000000
	C		21100000
	C		21200000
	C		21300000
	C		21400000
	C		21500000
	C		21600000
	C		21700000
	C		21800000
	C		21900000
	C		22000000
	C		22100000
	C		22200000
	C		22300000
	C		22400000
	C		22500000
	C		22600000
	C		22700000
	C		22800000
	C		22900000
	C		23000000
	C		23100000
	C		23200000
	C		23300000
	C		23400000
	C		23500000
	C		23600000
	C		23700000
	C		23800000
	C		23900000
	C		24000000
	C		24100000
	C		24200000
	C		24300000
	C		24400000
	C		24500000
	C		24600000
	C		24700000
	C		24800000
	C		24900000
	C		25000000

```

15 NMP0(I1)=NMP
NLAB=NOLD
NOLD=0
DO 16 I1=1,NMODL
NMP=NMP0(I1)
J1=1+NCLO
J2=NMP+NOLD
READ(I1)IX,(XMAS(L),((XINERT(I,J,L),I=1,3),J=1,3),L=J1,J2)
16 READ(I1)NMLAB,(FRQLAB(I),I=1,NMLAB)
DO 17 J=1,NMLAB
UMASS(J)=1.
READ(I1)IX,(RMODE(I,J),I=1,IX)
17 CONTINUE
GO TO 25
C ALTERNATE CARD INPUT FOR LAB
C
5 READ(IN,2)NLAB
READ(IN,1)((RIO(I,J),I=1,3),J=1,NLAB)
READ(IN,54)(XMAS(L),((XINERT(I,J,L),I=1,3),J=1,3),L=1,NLAB)
IF(KLUE.EQ.1 .OR. KLUE.EQ.3)GO TO 9
IF(IFLAB)9,8,9
9 READ(IN,2)NMLAB
READ(IN,1)(UMASS(I),I=1,NMLAB)
READ(IN,1)(FRQLAB(I),I=1,NMLAB)
IX=6*NLAB
READ(IN,1)((RMODE(I,J),I=1,IX),J=1,NMLAB)
C REGULAR CARD INPUT FOR LAB
C
25 CONTINUE
8 DO 11 J=1,NLAB
DO 11 I=1,3

```

```

Q(I,J)=0.
QD(I,J)=0.
TH(I,J)=0.
11 THD(I,J)=C.
IF(IFLAB.EQ.0)GO TO 6
IF(JUMP.EQ.1)GO TO 604
READ(IN,1)(Q(I,J),I=1,3),J=1,NLAB)
* (QD(I,J),I=1,3),J=1,NLAB)
* ((TH(I,J),I=1,3),J=1,NLAB)
* ((THD(I,J),I=1,3),J=1,NLAB)
604 IF(NMLAB.EQ.0)GO TO 6
READ(IN,1)(DAMP(I),I=1,NMLAB)
6 READ(IN,1)(R,ROOT,GAMMA,WX
WRITE(IOUT,701)NLAB
701 FORMAT(*OLAP INPUT#/* NO. MASSES =*,I4)
WRITE(IOUT,702)(J,(R(I,J),I=1,3),J=1,NLAB)
702 FORMAT(* MASS POINT LOCATIONS#/* NO.*9X,*X(1)*,14X,*X(2)*,14X,
**X(3)*/(I4,3E18.8))
WRITE(IOUT,703)(L,XMAS(L),((XINERT(I,J,L),I=1,3),J=1,3),L=1,NLAB)
703 FORMAT(* NO.*8X,*MASS*,27X,*INERTIA MATRIX#/*
* (I4,E17.7,5X,3E16.7/2 (26X,3E16.7/))
IF(IFLAB.EQ.0)GO TO 808
WRITE(IOUT,704)NMLAB
704 FORMAT(* NO. MODES =*,I4)
WRITE(IOUT,705)(UMASS(I),I=1,NMLAB)
705 FORMAT(* MODAL MASSES*/(8E16.7))
WRITE(IOUT,706)(FRQLAB(I),I=1,NMLAB)
706 FORMAT(* FREQUENCIES*/(8E16.7))
DO 720 J=1,NMLAB
WRITE(IOUT,721)J
DO 720 L=1,NLAB
LS=6*(L-1)
J1=LS+1
J2=LS+6
720 WRITE(IOUT,707)L,(RMUDE(I,J),I=J1,J2)
707 FORMAT(I5,6E16.7)
721 FORMAT(* MODE#I4/* MASS NO. Q(1)*,12X,*Q(2)*,12X,*Q(3)*,10X,*THEC
*TA(1)*,8X,*THETA(2)*,8X,*THETA(3)*
WRITE(IOUT,725)
725 FORMAT(*INITIAL CONDITIONS FOR DEFORMATION COORDINATES#/*
* *UMASS*,8X,*Q(1)*,13X,*Q(2)*,13X,*Q(3)*
WRITE(IOUT,708)(J,(I,J),I=1,3),J=1,NLAB)
WRITE(IOUT,726)
726 FORMAT(*MASS*,6X,*QDOT(1)*,10X,*QDOT(2)*,10X,*QDOT(3)*
WRITE(IOUT,708)(J,(Q(I,J),I=1,3),J=1,NLAB)
WRITE(IOUT,727)
727 FORMAT(*OMASS*,6X,*THETA(1)*, 9X,*THETA(2)*,9X,*THETA(3)*
WRITE(IOUT,708)(J,(TH(I,J),I=1,3),J=1,NLAB)
WRITE(IOUT,728)
728 FORMAT(*OMASS*,4X,*THETADOT(1)*,7X,*THETADOT(2)*,7X,*THETADOT(3)*
WRITE(IOUT,708)(J,(THD(I,J),I=1,3),J=1,NLAB)

```

C 02050 208000000

C 02060 209000000

C 02070 210000000

C 02080 211000000

C 02090 212000000

C 02100 213000000

C 02110 214000000

C 02120 215000000

C 02130 216000000

C 02140 217000000

C 02150 218000000

C 02160 219000000

C 02170 220000000

C 02180 221000000

C 02190 222000000

C 02200 223000000

C 02210 224000000

C 02220 225000000

C 02230 226000000

C 02240 227000000

C 02250 228000000

C 02260 229000000

C 02270 230000000

C 02280 231000000

C 02290 232000000

C 02300 233000000

C 02310 234000000

C 02320 235000000

C 02330 236000000

C 02340 237000000

C 02350 238000000

C 02360 239000000

C 02370 240000000

C 02380 241000000

C 02390 242000000

C 02400 243000000

C 02410 244000000

C 02420 245000000

C 02430 246000000

C 02440 247000000

C 02450 248000000

C 02460 249000000

C 02470 250000000

C 02480 251000000

C 02490 252000000

C 02500 253000000

C 02510 254000000

C 02520 255000000

C 02530 256000000

C 02540 257000000

C 02550 258000000

```

708 FORMAT(14,3E17.7)
WRITE(IOUT,709)(DAMP(I),I=1,NMLAB)
709 FORMAT(%MODAL DAMPING RATIOS#/(RE16.7))
808 CONTINUE
WRITE(IOUT,719)
719 FORMAT(*INITIAL CONDITION FOR MAIN LABORATORY COORDINATES*)
WRITE(IOUT,710)R,ROOT,GAMMA,WX
710 FORMAT(*R =#,3E17.7/* RDOT =#,3E17.7/
* GAMMA=#,3E17.7/* WX =#,3E17.7)
IF(IFLUID.EQ.0)GO TO 50
C
C RESERVOIR INPUT
C
READ(IN,1)RHO,A
WRITE(IOUT,760)
760 FORMAT(* FLUID DATA*)
WRITE(IOUT,729)RHO,A
729 FORMAT(8X,*RHO*,15X,*A*/2E17.7)
DO 30 L=1,2
READ(IN,4)XMIPL(L),((XIIP(I,J,L),J=1,3),I=1,3),
*(SIP(I,L),I=1,3),
*(EIR(I,L),I=1,3),
*(UIR(I,L),I=1,3),
*(UIB(I,L),I=1,3),
*(EIB(I,L),I=1,3),
*((XJIB(I,J,L),J=1,3),I=1,3),
*(BI(L),HIO(L),HIMAX(L),HIMIN(L),
*(GIP(I,L),I=1,3)
IF(L.EQ.1)WRITE(IOUT,730)
730 FORMAT(* EMPTYING RESERVOIR*)
IF(L.EQ.2)WRITE(IOUT,731)
731 FORMAT(* FILLING RESERVOIR*)
WRITE(IOUT,732)XMIPL(L),((XIIP(I,J,L),J=1,3),I=1,3),
*(SIP(I,L),I=1,3),
*(EIR(I,L),I=1,3),
*(UIR(I,L),I=1,3),
*(UIB(I,L),I=1,3),
*(EIB(I,L),I=1,3),
*((XJIB(I,J,L),J=1,3),I=1,3),
*(BI(L),HIC(L),HIMAX(L),HIMIN(L),
*(GIP(I,L),I=1,3)
732 FORMAT(8X,*MASS*,27X,*INERTIA MATRIX*/E17.7,5X,3E16.7/2(22X,
*3E16.7//
* # EIR=#,3E17.7/* UIR=#,3E17.7/* UIB=#,3E17.7/
* # JIB#/(3E17.7)/9X,*BI*,14X,*HIO*,13X,*HIMAX*,12X,*HIMIN*/
* 4E17.7/* GIP=#,3E17.7)
30 CONTINUE
4 FORMAT(E15.6/11(3E15.8/),(4E15.8))
IF(NPIPE.EQ.0)GO TO 50

```

```

C 02560 25900000
C 02570 26000000
C 02580 26100000
C 02590 26200000
C 02600 26300000
C 02610 26400000
C 02620 26500000
C 02630 26600000
C 02640 26700000
C 02650 26800000
C 02660 26900000
C 02670 27000000
C 02680 27100000
C 02690 27200000
C 02700 27300000
C 02710 27400000
C 02720 27500000
C 02730 27600000
C 02740 27700000
C 02750 27800000
C 02760 27900000
C 02770 28000000
C 02780 28100000
C 02790 28200000
C 02800 28300000
C 02810 28400000
C 02820 28500000
C 02830 28600000
C 02840 28700000
C 02850 28800000
C 02860 28900000
C 02870 29000000
C 02880 29100000
C 02890 29200000
C 02900 29300000
C 02910 29400000
C 02920 29500000
C 02930 29600000
C 02940 29700000
C 02950 29800000
C 02960 29900000
C 02970 30000000
C 02980 30100000
C 02990 30200000
C 03000 30300000
C 03010 30400000
C 03020 30500000
C 03030 30600000
C 03040 30700000
C 03050 30800000
C 03060 30900000

```

```

C C PIPE INPUT
C C
DO 40 L=1,NPIPE
  READ(IN,7)XMF(L),(S(I,L),I=1,3),
  *(DELU(I,L),I=1,3),
  *(DELE(I,L),I=1,3),
  *(G(I,L),I=1,3),
  *(VEC(I,L),I=1,3),
  *((DELJ(I,J,L),J=1,3),I=1,3),
  *((XIF(I,J,L),J=1,3),I=1,3)
  WRITE(IOUT,740)PIPES(L)
740 FORMAT(* FLUID IN PIPE ON MASS NO. *,I4)
  WRITE(IOUT,742)XMF(L),(S(I,L),I=1,3),
  *(DELU(I,L),I=1,3),
  *(DELE(I,L),I=1,3),
  *(G(I,L),I=1,3),
  *(VEC(I,L),I=1,3),
  *((DELJ(I,J,L),J=1,3),I=1,3),
  *((XIF(I,J,L),J=1,3),I=1,3)
  * * DELE=*3E17.7/* G =*3E17.7/ * DELH=*3E17.7/* DELJ*/3(3E17.7C
  /*),* INERTIA MATRIX*/(3E17.7 )
40 CONTINUE
7 FORMAT(E15.8/(3E15.8))
50 IF(NMLM.EQ.0)GO TO 70
C C MOVING MASS INPUT
C C
DO 51 I=1,8
  U(I)=0.
  IF(MLM(I).EQ.0)GO TO 51
  READ(IN,1)U(I)
51 CONTINUE
  WRITE(IOUT,750)(U(I),I=1,8)
750 FORMAT(*0*MASS MU(J) OF EACH MOVING MASS*/8E16.7)
70 CONTINUE
  READ(IN,2)IPHS1,JUMP
  IF(IPHS1.EQ.0)GO TO 105
C C PHASE I INPUT FOR COUNTERWEIGHT
C C
NOLD=0
REWIND 12
READ(12)NMODL
DO 115 II=1,NMODL
  READ(12)NMP
  J1=NOLD+1
  J2=NOLD+NMP
  READ(12) ((RA0(I,J),I=1,3),J=J1,J2)
  NOLD=NOLD+NMP

```

```

C 03070 31000000
C 03080 31100000
C 03090 31200000
C 03100 31300000
C 03110 31400000
C 03120 31500000
C 03130 31600000
C 03140 31700000
C 03150 31800000
C 03160 31900000
C 03170 32000000
C 03180 32100000
C 03190 32200000
C 03200 32300000
C 03210 32400000
C 03220 32500000
C 03230 32600000
C 03240 32700000
C 03250 32800000
C 03260 32900000
C 03270 33000000
C 03280 33100000
C 03290 33200000
C 03300 33300000
C 03310 33400000
C 03320 33500000
C 03330 33600000
C 03340 33700000
C 03350 33800000
C 03360 33900000
C 03370 34000000
C 03380 34100000
C 03390 34200000
C 03400 34300000
C 03410 34400000
C 03420 34500000
C 03430 34600000
C 03440 34700000
C 03450 34800000
C 03460 34900000
C 03470 35000000
C 03480 35100000
C 03490 35200000
C 03500 35300000
C 03510 35400000
C 03520 35500000
C 03530 35600000
C 03540 35700000
C 03550 35800000
C 03560 35900000
C 03570 36000000

```



```

115 NMPO(11)=NMP
NCW=NOLD
NOLD=0
DO 116 I=1,NMODL
NMP=NMPO(11)
J1=NOLD+1
J2=NOLD+NMP
READ(12)IX,(XIBAR(L),(XIBAR(I,J,L),I=1,3),J=1,3),L=J1,J2)
116 NOLD=NOLD+NMP
READ(12)NMCK,(FRQCK(I),I=1,NMCW)
DO 117 J=1,NMCW
UMASSB(J)=1.
READ(12)IX,(SMODE(I,J),I=1,IX)
117 CONTINUE
GO TO 125

C ALTERNATE CARD INPUT FOR COUNTERWEIGHT
C
C
105 READ(IN,2)NCW
READ(IN,1)((RAO(I,J),I=1,3),J=1,NCW)
READ(IN,54)(XIBAR(L),(XIBAR(I,J,L),I=1,3),J=1,3),L=1,NCW)
IF(KLUE.LT.3)GO TO 29
IF(IFCW)29,28,29
29 READ(IN,2)NMCW
READ(IN,1)(UMASSB(I),I=1,NMCW)
READ(IN,1)(FRQCK(I),I=1,NMCW)
IX=6*NCW
READ(IN,1)((SMODE(I,J),I=1,IX),J=1,NMCW)

C REGULAR CARD INPUT FOR COUNTERWEIGHT
C
C
125 CONTINUE
28 DO 12 J=1,NCW
DO 12 I=1,3
QB(I,J)=0.
QBD(I,J)=0.
THB(I,J)=0.
12 THBD(I,J)=0.
IF(IFCW.EQ.0)GO TO 26
IF(JUMP.EQ.1)GO TO 606
READ(IN,1)((QB(I,J),I=1,3),J=1,NCW),
*((QBD(I,J),I=1,3),J=1,NCW),
*(THB(I,J),I=1,3),J=1,NCW),
*((THBD(I,J),I=1,3),J=1,NCW)

C READ CRITICAL DAMPING
C
C
606 IF(NMCK.EQ.0)GO TO 26
READ(IN,1)(DAMPB(I),I=1,NMCW)
26 CONTINUE
WRITE(1)OUT,751)NCW

```

```

C 03580 36100000
C 03590 36200000
C 03600 36300000
C 03610 36400000
C 03620 36500000
C 03630 36600000
C 03640 36700000
C 03650 36800000
C 03660 36900000
C 03670 37000000
C 03680 37100000
C 03690 37200000
C 03700 37300000
C 03710 37400000
C 03720 37500000
C 03730 37600000
C 03740 37700000
C 03750 37800000
C 03760 37900000
C 03770 38000000
C 03780 38100000
C 03790 38200000
C 03800 38300000
C 03810 38400000
C 03820 38500000
C 03830 38600000
C 03840 38700000
C 03850 38800000
C 03860 38900000
C 03870 39000000
C 03880 39100000
C 03890 39200000
C 03900 39300000
C 03910 39400000
C 03920 39500000
C 03930 39600000
C 03940 39700000
C 03950 39800000
C 03960 39900000
C 03970 40000000
C 03980 40100000
C 03990 40200000
C 04000 40300000
C 04010 40400000
C 04020 40500000
C 04030 40600000
C 04040 40700000
C 04050 40800000
C 04060 40900000
C 04070 41000000
C 04080 41100000

```

```

751 FORMAT(*OCOUNTERWEIGHT INPUT*/ * NO. MASSES =*,I4)
WRITE(IOUT,715)(J,(RAD(I,J),I=1,3),J=1,NCW)
715 FORMAT(* MASS POINT LOCATIONS*/ * NO. *,9X,*Y(1)*,14X,*Y(2)*,14X,
**Y(3)/(I4,3E18.8))
WRITE(IOUT,703)(L,XMBAR(L),(XIBAR(I,J,L),I=1,3),J=1,3),L=1,NCW)
IF(IFCW.EQ.0)GO TO 858
WRITE(IOUT,704)NMCW
WRITE(IOUT,705)(UMASSB(I),I=1,NMCW)
WRITE(IOUT,706)(FRQCW(I),I=1,NMCW)
DO 770 J=1,NMCW
WRITE(IOUT,721)J
DO 770 L=1,NCW
LS=6*(L-1)
J1=LS+1
J2=LS+6
770 WRITE(IOUT,707)I,(SMODE(I,J),I=J1,J2)
WRITE(IOUT,775)
775 FORMAT(*OINITIAL CONDITIONS FOR DEFORMATION COORDINATES*/
*OMASS*,7X,*QBAR(1)*,10X,*QBAR(2)*,
* 10X,*QBAR(3)*)
WRITE(IOUT,708)(J,(QB (I,J),I=1,3),J=1,NCW)
WRITE(IOUT,776)
776 FORMAT(*OMASS*,5X,*QBARDOT(1)*,7X,*QBARDOT(2)*,7X,*QBARDOT(3)*)
WRITE(IOUT,708)(J,(QRD (I,J),I=1,3),J=1,NCW)
WRITE(IOUT,777)
777 FORMAT(*OMASS*,5X,*THETABAR(1)*,6X,*THETABAR(2)*,6X,*THETABAR(3)*)
WRITE(IOUT,708)(J,(THR (I,J),I=1,3),J=1,NCW)
WRITE(IOUT,778)
778 FORMAT(*OMASS*,3X,*THETABARDOT(1)*,4X,*THETABARDOT(2)*,4X,*THETABAR
*ROOT(3)*)
WRITE(IOUT,708)(J,(THBD(I,J),I=1,3),J=1,NCW)
WRITE(IOUT,709)(DAMPB (I),I=1,NMCW)
858 CONTINUE
IF(KLUE.NE.4)GO TO 39
IF(IFCN )39,38,39
C READ CONNECTING STRUCTURE DATA
C
39 READ(IN,2)IBAR,IABAR
READ(IN,1)SS,SSBAR,DEL,DELDOT,PHIST,PHISTD,YA,YB
WRITE(IOUT,780)IBAR,IABAR
780 FORMAT(* CONNECTING STRUCTURE INPUT*/ * CONNECTS TO MASSES I=*,I3,
* , A=*,I3)
WRITE(IOUT,782)SS,SSBAR,DEL,DELDOT
782 FORMAT(* S =*,3E17.7/* SBAR =*,3E17.7/* DEL =*,3E17.7/
* * DELDOT=*,3E17.7)
WRITE(IOUT,784)PHIST,PHISTD,YA,YB
784 FORMAT(* PHISTAR =*,3E17.7/* PHISTARDOT=*,3E17.7/* YA=*,3E17.7/* YB=*,3E17.7)
38 IF(KLUE.NE.4)GO TO 46
DO 13 I=1,3

```

C 04090 41200000

C 04100 41300000

C 04110 41400000

C 04120 41500000

C 04130 41600000

C 04140 41700000

C 04150 41800000

C 04160 41900000

C 04170 42000000

C 04180 42100000

C 04190 42200000

C 04200 42300000

C 04210 42400000

C 04220 42500000

C 04230 42600000

C 04240 42700000

C 04250 42800000

C 04260 42900000

C 04270 43000000

C 04280 43100000

C 04290 43200000

C 04300 43300000

C 04310 43400000

C 04320 43500000

C 04330 43600000

C 04340 43700000

C 04350 43800000

C 04360 43900000

C 04370 44000000

C 04380 44100000

C 04390 44200000

C 04400 44300000

C 04410 44400000

C 04420 44500000

C 04430 44600000

C 04440 44700000

C 04450 44800000

C 04460 44900000

C 04470 45000000

C 04480 45100000

C 04490 45200000

C 04500 45300000

C 04510 45400000

C 04520 45500000

C 04530 45600000

C 04540 45700000

C 04550 45800000

C 04560 45900000

C 04570 46000000

C 04580 46100000

C 04590 46200000

```

DEL(I)=0.
DELDT(I)=0.
PHIST(I)=0.
13 PHISTD(I)=0.
46 IF(KLUE.EQ.2 .OR. KLUE.GT.3)GO TO 59
C C C 04600 46300000
C C 04610 46400000
C C 04620 46500000
C C 04630 46600000
C C 04640 46700000
C C 04650 46800000
C C 04660 46900000
C C 04670 47000000
C C 04680 47100000
C C 04690 47200000
C C 04700 47300000
C C 04710 47400000
C C 04720 47500000
C C 04730 47600000
C C 04740 47700000
C C 04750 47800000
C C 04760 47900000
C C 04770 48000000
C C 04780 48100000
C C 04790 48200000

C C TEST FOR ZERO FREQUENCIES AND SET UP CM AND KAPPA MATRICES
DO 81 I=1,NMLAB
KCM(I,1)=2.*UMASS(I)*DAMP(I)*FRQLAB(I)
81 KCM(I,3)=FRQLAB(I)*FRQLAB(I)*UMASS(I)
59 IF(KLUE.GT.2)GO TO 99
DO 82 I=1,NMCW
KCM(I,2)=2.*UMASS(I)*DAMP(I)*FRQCW(I)
82 KCM(I,4)=FRQCW(I)*FRQCW(I)*UMASS(I)
99 RETURN
1 FORMAT(3E15.7)
2 FORMAT(5I4)
54 FORMAT(E15.8/(3E15.8))
END

```

```

SUBROUTINE FIRST(NLAB,NCW)
COMMON T,R,ROOT,XIDEN,RHO,A,YA,YB,R3,R4,R5,R6,H1,H2,HOLD,SAVE,
* G1,G2,G3,G4,G5,G6,G7,G8,G9,WORK1,WORK2,WORK,R1,R2,G0(9)
COMMON /BIG/PIETA(3,3),PIGAM(3,3),SUML(3),SUMT,SGAM(3,3),SETA(3,3)C
*,EMU(20),EMUBAR(20),WURK(600,2),ZZ(7760),NMLAB,
* RMODE(600,20),NMCW,SMODE(600,20)
COMMON /LABOR/WX,RI,Q,QDNT,TH,THD,XMAS,XINERT
COMMON /INOUT/IN,INOUT,IOFF
COMMON /CWT/RB,RBDDT,ETA,WY,RA,QB,QRD,THR,THBD,XMBAR,XIBAR
COMMON /CONNECT/IPT,S,IAPT,SB,DEL,DELD,PHIST,PHISTD,
* DELR8,DELR8D,GAM,GAMD,ETAST,ETASTD
* ,PZB(3),ELL(3),ELLD(3)
COMMON /NEWCOM/EL,ELD,ELDD,ROB,ROBD,ROBDD,VEC(20,2),VECBAR(20,2)
* ,PIBETA(3,3),IFDEPL,KLUE
COMMON /EXTRA/ZFX(3),ZLX(3),ZMX(3),ZCY(3),ZCM(3),EMC,TOT
DIMENSION R(3),ROOT(3),R1(6),R2(6),R3(6),R4(6),R5(6),R6(6),H1(3),
* H2(3),WORK2(21),WORK1(6,6),WORK(3,3,100),XMAS(100),
* XINERT(3,3,100),RB(3),RBDDT(3),XMBAR(100),XIBAR(3,3,100)C
DIMENSION YA(3),YB(3),G1(3,3),G2(9),G3(9),G4(9),G5(9),G6(9),
* G7(9),G8(9),G9(9),XIDEN(9),TH(3,100),THD(3,100),
* THB(3,100),THRD(3,100),Q(3,100),QDNT(3,100),QB(3,100),
* QBD(3,100),RI(3,100),RA(3,100),ETAST(3),ETASTD(3),
* ETA(3),HOLD(3),SAVE(3),PHIST(3),PHISTD(3),WX(3),WY(3),
* EL(3),ELDD(3),ELDD(3),DEL(3),DELD(3),S(3),SB(3),ROB(3),
* ROBD(3),ROBDD(3),DELR8(3),DELR8D(3),GAM(3),GAMD(3)
COMMON /OPT2/PRINT
COMMON /ALLCNT/ALL(4),DL(3,3),DC(3,3),EM ,XIL(3,3),XIC(3,3)
PRINT=0.
888 CONTINUE
VAR=SQRT(DOTP(YA,YA))
DO 10 I=1,3
10 G1(3,I)=YA(I)/VAR
G1(2,1)=YA(2)*YR(3)-YB(2)*YA(3)
G1(2,2)=YB(1)*YA(3)-YA(1)*YB(3)
G1(2,3)=YA(1)*YB(2)-YB(1)*YA(2)
VAR=G1(2,1)*G1(2,1)+G1(2,2)*G1(2,2)+G1(2,3)*G1(2,3)
VAR=SQRT(VAR)
DO 11 I=1,3
11 G1(2,I)=G1(2,I)/VAR
G1(1,1)=G1(3,3)*G1(2,2)-G1(3,2)*G1(2,3)
G1(1,2)=G1(3,1)*G1(2,3)-G1(3,3)*G1(2,1)
G1(1,3)=G1(3,2)*G1(2,1)-G1(3,1)*G1(2,2)
CALL SCALR(1.,G1,PIBETA,3)
C* A2
CALL SCALR(-1.,XIDEN,G2,3)
G2(1)=1.
CALL PIF(PHIST,G3)
C* A5
CALL GAMMA(THB(1,IAPT),G5)

```

```

C* A6      CALL PIF(TH(1,IPT),G6)
           CALL PIF(THB(1,IAPT),G5)
           CALL MULT(G2,G6,G7,3)
           CALL MULT(G1,G7,G8,3)
           CALL MTRAN(G3,G8,G7,3)
           CALL MTRAN(G1,G7,G8,3)
           CALL MTRAN(G5,G8,G7,3)
           CALL SCALP(1.,G7,PIETA,3)

C* A7      CALL MULT(G7,G2,G4,3)

C* A8      ETAST(2)=ARSIN(G4(3))
           ETAST(1)=ARSIN(-G4(6)/COS(ETAST(2)))
           ETAST(3)=ARSIN(-G4(2)/COS(ETAST(2)))
           ETA(1)=ETAST(1)+3.141592653
           ETA(2)=ETAST(2)
           ETA(3)=ETAST(3)

C* A9      CALL SSIN(PHIST,G4,1)
           CALL SSIN(ETA,G8,1)

C* A10     CALL SSIN(ETA,G9,-1)

C* A11     CALL MULT(G4,PHISTD,HOLD,1)
           CALL MULT(G2,THD(1,IPT),SAVE,1)
           CALL MULT(G1,SAVE,ETASTD,1)
           CALL SUBTR(ETASTD,HOLD,SAVE,1)
           CALL MTRAN(G3,SAVE,HOLD,1)
           CALL MTRAN(G1,HOLD,SAVE,1)
           CALL SUBTR(SAVE,THBD(1,IAPT),HOLD,1)
           CALL MTRAN(G5,HOLD,SAVE,1)
           CALL MULT(G9,SAVE,ETASTD,1)

C* A12     CALL MULT(G7,WX,HOLD,1)
           CALL MULT(G8,ETASTD,SAVE,1)
           CALL ADD(HOLD,SAVE,WY,1)

C* A14     READ(IN,8)EL
           WRITE(10UT,700)EL
           700 FORMAT(*0DEPLOYMENT INPUT - L0*/3E17.7)
           CALL ZEROS(ELD,1)
           CALL ZEROS(ELDD,1)
           IF(IFDEPL)7,9,7
           7 CALL LLDLDD

C* A15     9 CALL ADD(EL,DEL,H1,1)
           CALL ADD(ELD,DELDD,H2,1)
           CALL SCALR(1.,H1,ELL,1)
           CALL SCALP(1.,H2,ELLD,1)

C* A16

```

```

C 05290 53200000
C 05300 53300000
C 05310 53400000
C 05320 53500000
C 05330 53600000
C 05340 53700000
C 05350 53800000
C 05360 53900000
C 05370 54000000
C 05380 54100000
C 05390 54200000
C 05400 54300000
C 05410 54400000
C 05420 54500000
C 05430 54600000
C 05440 54700000
C 05450 54800000
C 05460 54900000
C 05470 55000000
C 05480 55100000
C 05490 55200000
C 05500 55300000
C 05510 55400000
C 05520 55500000
C 05530 55600000
C 05540 55700000
C 05550 55800000
C 05560 55900000
C 05570 56000000
C 05580 56100000
C 05590 56200000
C 05600 56300000
C 05610 56400000
C 05620 56500000
C 05630 56600000
C 05640 56700000
C 05650 56800000
C 05660 56900000
C 05670 57000000
C 05680 57100000
C 05690 57200000
           57300000
           57400000
C 05720 57500000
C 05730 57600000
C 05740 57700000
C 05750 57800000
C 05760 57900000
C 05770 58000000
C 05780 58100000
C 05790 58200000

```

CALL MTRAN(G6,S,HOLD,1)	C	05800	58300000
CALL ADD(-I(1,IPT),Q(1,IPT),SAVE,1)	C	05810	58400000
CALL ADD(HOLD,SAVE,HOLD,1)	C	05820	58500000
CALL MULT(G7,HOLD,RBDDT,1)	C	05830	58600000
CALL ADD(RA(1,IAPT),QB(1,IAPT),HOLD,1)	C	05840	58700000
CALL SUBTR(RBDDT,HOLD,HOLD,1)	C	05850	58800000
CALL MTRAN(G1,HI,SAVE,1)	C	05860	58900000
CALL ADD(SB,SAVE,ROB,1)	C	05870	59000000
CALL MTRAN(G5,ROB,RB,1)	C	05880	59100000
CALL SUBTR(HOLD,RB,RB,1)	C	05890	59200000
C* A19	C	05900	59300000
CALL MULT(G8,ETASTD,HOLD,1)	C	05910	59400000
CALL GAMMA(HOLD,G6)	C	05920	59500000
CALL MULT(G6,RBDDT,HOLD,1)	C	05930	59600000
CALL GAMMA(THD(1,IPT),G8)	C	05940	59700000
CALL MULT(G8,S,SAVE,1)	C	05950	59800000
CALL ADD(SAVE,QDDT(1,IPT),SAVE,1)	C	05960	59900000
CALL MULT(G7,SAVE,RBDDT,1)	C	05970	60000000
CALL SUBTR(RBDDT,HOLD,RBDDT,1)	C	05980	60100000
CALL MTRAN(G1,H2,HOLD,1)	C	05990	60200000
CALL MTRAN(G5,HOLD,SAVE,1)	C	06000	60300000
CALL SUBTR(RBDDT,SAVE,RBDDT,1)	C	06010	60400000
CALL GAMMA(THD(1,IAPT),G4)	C	06020	60500000
CALL MULT(G4,ROB,SAVE,1)	C	06030	60600000
CALL ADD(SAVE,QBD(1,IAPT),SAVE,1)	C	06040	60700000
CALL SUBTR(RBDDT,SAVE,RBDDT,1)	C	06050	60800000
C* A20	C	06060	60900000
CALL MTRAN(G1,ELD,ROB,1)	C	06070	61000000
CALL MTRAN(G1,ELD,ROBDD,1)	C	06080	61100000
CALL MTRAN(G1,EL,SAVE,1)	C	06090	61200000
CALL ADD(SB,SAVE,ROB,1)	C	06100	61300000
CALL ADD(ROB,RA(1,IAPT),ROB,1)	C	06110	61400000
CALL ADD(KI(1,IPT),S,SAVE,1)	C	06120	61500000
CALL MULT(G2,SAVE,HOLD,1)	C	06130	61600000
CALL SUBTR(HOLD,ROB,ROB,1)	C	06140	61700000
C* A21	C	06150	61800000
IF(IFDEPL)28,27,28	C	06160	61900000
27 CALL SCALK(0,ROBDD,RORD,1)	C	06170	62000000
CALL SCALK(0,ROBDD,RORD,1)	C	06180	62100000
GO TO 17	C	06190	62200000
28 CALL SCALK(-1,ROBDD,RORD,1)	C	06200	62300000
CALL SCALK(-1,ROBDD,RORD,1)	C	06210	62400000
17 EM=0.	C	06220	62500000
C* A21A	C	06230	62600000
CALL PIF(GAM,PIGAM)	C	06240	62700000
33 CALL ZEROS(G0,3)	C		62800000
CALL ZEROS(G5,3)	C		62900000
CALL ZEROS(P1,2)	C		63000000
CALL ZEROS(R2,2)	C		63100000
C* A22,A23	C	06290	63200000
ON 210 I=1,NLAB	C	06300	63300000

```

EM=EM+XMAS(I)
CALL GAMMA(RI(1,1),WORK(1,1,1))
CALL SCALR(XMAS(I),WORK(1,1,1),G3,3)
CALL ADD(GO,G3,G0,3)
CALL MULT(G3,WORK(1,1,1),G4,3)
CALL SUBTR(XINERT(1,1,1),G4,G4,3)
CALL ADD(G5,G4,G5,3)
CALL SCALR(XMAS(I),Q(1,1),HOLD,1)
CALL SCALR(XMAS(I),QDOT(1,1),SAVE,1)
CALL SUBTR(R1,HOLD,R1,1)
CALL SUBTR(R2,SAVE,R2,1)
CALL MULT(WORK(1,1,1),HOLD,H1,1)
CALL MULT(XINERT(1,1,1),TH(1,1),HOLD,1)
CALL MULT(XINERT(1,1,1),THD(1,1),SAVE,1)
CALL ADD (H1,HOLD,HOLD,1)
CALL ADD (H2,SAVE,SAVE,1)
CALL SUBTR(R1(4),HOLD,R1(4),1)
CALL MULT(SUBTR(R2(4),SAVE,R2(4),1)
210 CALL SCALP(EM,XIDEN,G8,3)
DO 20 I=1,3
DO 20 J=1,3
IJ=3*(J-1)+I
WORK1(I,J)=G8(IJ)
WORK1(I+3,J)=G5(IJ)
20 WORK1(I+3,J+3)=G5(IJ)
CALL MCPY(GO,DL,3,3)
CALL MCPY(G5,XIL,3,3)
IJ=0
DO 30 I=1,6
DO 30 J=1,1
IJ=IJ+1
30 WORK2(IJ)=WORK1(I,J)
CALL INCH(WORK2,6,WORK1,NIX)
C* A24,A40
IF(NIX.EQ.0)GO TO 35
WRITE(1OUT,4)NIX
4 FORMAT(* INVERSION FAILED*/* NIX= *,I2)
35 IJ=0
DO 40 I=1,6
DO 40 J=1,1
IJ=IJ+1
WORK1(I,J)=WORK2(IJ)
40 WORK1(I,J)=WORK2(IJ)
DO 50 I=1,6
R3(I)=0.
R4(I)=0.
DO 50 J=1,6
R3(I)=R3(I)+WORK1(I,J)*R1(IJ)
50 R4(I)=R4(I)+WORK1(I,J)*R2(IJ)
C* A25,A41

```

```

C 06310 63400000
C 06320 63500000
C 06330 63600000
C 06340 63700000
C 06350 63800000
C 06360 63900000
C 06370 64000000
C 06380 64100000
C 06390 64200000
C 06400 64300000
C 06410 64400000
C 06420 64500000
C 06430 64600000
C 06440 64700000
C 06450 64800000
C 06460 64900000
C 06470 65000000
C 06480 65100000
C 06490 65200000
C 06500 65300000
C 06510 65400000
C 06520 65500000
C 06530 65600000
C 06540 65700000
C 06550 65800000
C 06560 65900000
C 06570 66000000
C 06580 66100000
C 06590 66200000
C 06600 66300000
C 06610 66400000
C 06620 66500000
C 06630 66600000
C 06640 66700000
C 06650 66800000
C 06660 66900000
C 06670 67000000
C 06680 67100000
C 06690 67200000
C 06700 67300000
C 06710 67400000
C 06720 67500000
C 06730 67600000
C 06740 67700000
C 06750 67800000
C 06760 67900000
C 06770 68000000
C 06780 68100000
C 06790 68200000
C 06800 68300000
C 06810 68400000

```

```

DO 60 I=1,NLAB
CALL ADD(TH(1,I),R3(4),TH(1,I),1)
CALL ADD(THD(1,I),R4(4),THD(1,I),1)
CALL ADD(Q(1,I),R3,Q(1,I),1)
CALL ADD(QDOT(1,I),R4,QDOT(1,I),1)
CALL MULT(WORK(1,I),R3(4),HOLD,1)
CALL MULT(WORK(1,I),R4(4),SAVE,1)
CALL SUBTR(Q(1,I),HOLD,Q(1,I),1)
CALL SUBTR(QDOT(1,I),SAVE,QDOT(1,I),1)
60 A28,A42,A45
CALL PIF(R3(4),G3)
CALL GAMMA(R4(4),G6)
CALL MULT(G6,R,SAVE,1)
CALL PIF(GAM,G4)
CALL MTRAN(G3,WX,HOLD,1)
CALL SUBTR(HOLD,R4(4),WX,1)
CALL MTRAN(G3,RDOT,HOLD,1)
CALL ADD(HOLD,SAVE,HOLD,1)
CALL SUBTR(HOLD,R4,RDOT,1)
CALL MTRAN(G3,G4,PIGAM,3)
C* A29
GAM(2)=ARSIN(PIGAM(3,1))
C2=COS(GAM(2))
GAM(3)=ARSIN(-PIGAM(2,1) / C2)
CS=-PIGAM(3,2)/C2
SC=PIGAM(3,3)/C2
GAM(1)=ARSIN(CS)
IF(SC)42,44,44
44 IF(CS.GE.0.)GO TO 45
GAM(1)=GAM(1)+6.283185306
GO TO 45
42 GAM(1)=3.141592653-GAM(1)
45 CONTINUE
C* A30
CALL MTRAN(G3,R,HOLD,1)
CALL SUBTR(HOLD,R3,R,1)
C
C COUNTERWEIGHT DISPLACEMENTS,VELOCITIES
C
C
C LABORATORY DISPLACEMENTS,VELOCITIES
C
36 EMC=0.
38 CALL ZEROS(G0,3)
CALL ZEROS(G5,3)
CALL ZEROS(R1,2)
CALL ZEROS(R2,2)
C* A31,A32
DO 110 I=1,NCW
EMC=EMC+XMBAR(I)
CALL GAMMA(RA(1,I),WORK(1,I),I)

```

C 06820 68500000

C 06830 68600000

C 06840 68700000

C 06850 68800000

C 06860 68900000

C 06870 69000000

C 06880 69100000

C 06890 69200000

C 06900 69300000

C 06910 69400000

C 06920 69500000

C 06930 69600000

C 06940 69700000

C 06950 69800000

C 06960 69900000

C 06970 70000000

C 06980 70100000

C 06990 70200000

C 07000 70300000

C 07010 70400000

C 07020 70500000

C 07030 70600000

C 07040 70700000

C 07050 70800000

C 07060 70900000

C 07070 71000000

C 07080 71100000

C 07090 71200000

C 07100 71300000

C 07110 71400000

C 07120 71500000

C 07130 71600000

C 07140 71700000

C 07150 71800000

C 07160 71900000

C 07170 72000000

C 07180 72100000

C 07190 72200000

C 07200 72300000

C 07210 72400000

C 07220 72500000

C 07230 72600000

C 07240 72700000

C 72800000

C 72900000

C 73000000

C 73100000

C 73200000

C 73300000

C 73400000

C 73500000

C 07290 73000000

C 07300 73300000

C 07310 73400000

C 07320 73500000


```

CALL SCALR(XMBAF(I),WORK(1,1,1),G9,3)
CALL ADD(GO,G9,G0,3)
CALL MULT(G5,WORK(1,1,1),G4,3)
CALL SUBTR(XIBAR(1,1,1),G4,G4,3)
CALL ADD(G5,G4,G5,3)
CALL SCALR(XMBAF(I),QB(1,1),HOLD,1)
CALL SCALR(XMBAF(I),QBD(1,1),SAVE,1)
CALL SUBTR(R1,HOLD,R1,1)
CALL SUBTR(R2,SAVE,R2,1)
CALL MULT(WORK(1,1,1),HOLD,H1,1)
CALL MULT(WORK(1,1,1),SAVE,H2,1)
CALL MULT(XIBAR(1,1,1),THR(1,1),HOLD,1)
CALL MULT(XIBAR(1,1,1),THBD(1,1),SAVE,1)
CALL ADD(H1,HOLD,HOLD,1)
CALL ADD(H2,SAVE,SAVE,1)
CALL SURTR(R1(4),HOLD,RI(4),1)
CALL SURTR(R2(4),SAVE,R2(4),1)
CALL SCALP(EMC,XIDEN,G8,3)
110
DO 120 I=1,3
DO 120 J=1,3
IJ=3*(J-1)+I
WORK1(I,J)=G8(IJ)
WORK1(I+3,J)=G5(IJ)
CALL MCPY(GO,DC,3,3,3)
CALL MCPY(G5,XIC,3,3,3)
IJ=0
DO 130 I=1,6
DO 130 J=1,1
IJ=IJ+1
120 WDRK2(IJ)=WORK1(I,J)
CALL INCH(WORK2,6,WORK1,NIX)
IF(NIX.EQ.0)GO TO 135
WRITE(10UT,4)NIX
135 IJ=0
DO 140 I=1,6
DO 140 J=1,1
IJ=IJ+1
WORK1(J,I)=WORK2(IJ)
140 WDRK1(I,J)=WORK2(IJ)
DO 150 I=1,6
R5(I)=0.
R6(I)=0.
DO 150 J=1,6
R5(I)=R5(I)+WORK1(I,J)*RI(J)
R6(I)=R6(I)+WORK1(I,J)*R2(J)
C* A34,A47
DO 160 I=1,NCW
CALL ADD(THB(1,1),R5(4),THR(1,1),1)
CALL ADD(THBD(1,1),R6(4),THBD(1,1),1)

```

```

C 07330 73600000
C 07340 73700000
C 07350 73800000
C 07360 73900000
C 07370 74000000
C 07380 74100000
C 07390 74200000
C 07400 74300000
C 07410 74400000
C 07420 74500000
C 07430 74600000
C 07440 74700000
C 07450 74800000
C 07460 74900000
C 07470 75000000
C 07480 75100000
C 07490 75200000
C 07500 75300000
C 07510 75400000
C 07510 75500000
C 07520 75600000
C 07530 75700000
C 07540 75800000
C 07550 75900000
C 07560 76000000
C 07570 76100000
C 07580 76200000
C 07590 76300000
C 07600 76400000
C 07610 76500000
C 07620 76600000
C 07630 76700000
C 07640 76800000
C 07650 76900000
C 07660 77000000
C 07670 77100000
C 07680 77200000
C 07690 77300000
C 07700 77400000
C 07710 77500000
C 07720 77600000
C 07730 77700000
C 07740 77800000
C 07750 77900000
C 07760 78000000
C 07770 78100000
C 07780 78200000
C 07790 78300000
C 07800 78400000
C 07810 78500000
C 07820 78600000

```

CALL ADD(QB(1,1),R5,QB(1,1),1)	C	07830	78700000
CALL ADD(QBD(1,1),R6,QBD(1,1),1)	C	07840	78800000
CALL MULT(WORK(1,1,1),R5(4),HOLD,1)	C	07850	78900000
CALL MULT(WORK(1,1,1),R6(4),SAVE,1)	C	07860	79000000
CALL SUBTR(QB(1,1),HOLD,QB(1,1),1)	C	07870	79100000
CALL SUBTR(QBD(1,1),SAVE,QBD(1,1),1)	C	07880	79200000
C* A34-A	C	07890	79300000
CALL PIF(R5(4),G9)	C	07900	79400000
C* A35	C	07910	79500000
CALL MULT(G3,G2,G4,3)	C	07920	79600000
CALL MULT(G7,G4,G5,3)	C	07930	79700000
CALL MTRAN(G9,G5,G7,3)	C	07940	79800000
C* A36,A37	C	07950	79900000
ETAST(2)=ARSIN(G7(3))	C	07960	80000000
SC=-1/COS(ETAST(2))	C	07970	80100000
ETAST(1)=ARSIN(G7(6)*SC)	C	07980	80200000
ETAST(3)=ARSIN(G7(2)*SC)	C	07990	80300000
ETA(1)=ETAST(1)+3.141592653	C	08000	80400000
ETA(2)=ETAST(2)	C	08010	80500000
ETA(3)=ETAST(3)	C	08020	80600000
C* A38	C	08030	80700000
CALL MULT(G7,G2,PIETA,3)	C	08040	80800000
C* A51	C	08050	80900000
CALL MTRAN(G9,WY,HOLD,1)	C	08060	81000000
CALL SUBTR(HOLD,R6(4),WY,1)	C	08070	81100000
C* A54	C	08080	81200000
CALL MULT(PIETA,WX,HOLD,1)	C	08090	81300000
CALL SUBTR(WY,HOLD,HI,1)	C	08100	81400000
C* A39	C	08110	81500000
CALL MULT(PIETA,R3,HOLD,1)	C	08120	81600000
CALL MTRAN(G9,RB,SAVE,1)	C	08130	81700000
CALL ADD(HOLD,SAVE,HOLD,1)	C	08140	81800000
CALL SUBTR(HOLD,R5,HOLD,1)	C	08150	81900000
C* A56	C	08160	82000000
CALL GAMMA(HI,G1)	C	08170	82100000
CALL MULT(PIETA,R3,G4,1)	C	08180	82200000
CALL MULT(G1,G4,H2,1)	C	08190	82300000
CALL MULT(PIETA,R4,G6,1)	C	08200	82400000
CALL SUBTR(G6,H2,G4,1)	C	08210	82500000
CALL GAMMA(R6(4),G1)	C	08220	82600000
CALL MULT(G1,RB,SAVE,1)	C	08230	82700000
CALL SCALK(1,HOLD,RB,1)	C	08240	82800000
CALL ADD(G4,SAVE,G4,1)	C	08250	82900000
CALL MTRAN(G9,RBDDOT,SAVE,1)	C	08260	83000000
CALL ADD(G4,SAVE,G4,1)	C	08270	83100000
CALL SUBTR(G4,R6,RBDDOT,1)	C	08280	83200000
C* A57	C	08290	83300000
CALL SUBTR(RB,ROB,DELRB,1)	C	08300	83400000
CALL SUBTR(RBDDOT,ROBD,DELRBD,1)	C	08310	83500000
C* A58	C	08320	83600000
CALL SSIN(GAM,SGAM,-1)	C	08330	83700000

```

CALL SSIN(ETA, SETA, -1)
C* A59
CALL MULT(SGAM, WX, GAMD, 1)
CALL MULT(SETA, HI, ETASTD, 1)
C* A60, A61
IF(KLUE.NE.1 .AND. KLUE.NE.3)GO TO 215
DO 91 I=1, NLAB
  ISIX=I*6-5
  DO 92 J=1, 3
    IJ=ISIX+J-1
    WURK(IJ, 1)=O(J, I)*XMAS(I)
  92 WURK(IJ, 2)=QDOT(J, I)*XMAS(I)
  CALL MULT(XINERT(1, 1, I), TH(1, I), WURK(ISIX+3, 1), 1)
  91 CALL MULT(XINERT(1, 1, I), THD(1, I), WURK(ISIX+3, 2), 1)
  N6=NLAB*6
  CALL TPRD(RMODE, WURK, VEC, N6, NMLAB, 2, 600, 20)
DO 93 I=1, NMLAB
  VEC(I, 1)=VEC(I, 1)/EMU(I)
  93 VEC(I, 2)=VEC(I, 2)/EMU(I)
C* A63, A64
215 IF(KLUE.GT.2)GO TO 99
DO 94 I=1, NCM
  ISIX=I*6-5
  DO 95 J=1, 3
    IJ=ISIX+J-1
    WURK(IJ, 1)=O(J, I)*XMBAR(I)
  95 WURK(IJ, 2)=OBD(J, I)*XMBAR(I)
  CALL MULT(XIBAR(1, 1, I), THB(1, I), WURK(ISIX+3, 1), 1)
  94 CALL MULT(XIBAR(1, 1, I), THBD(1, I), WURK(ISIX+3, 2), 1)
  N6=NCM*6
  CALL TPRD(SMODE, WURK, VECBAR, N6, NMCW, 2, 600, 20)
DO 96 I=1, NMCW
  VECBAR(I, 1)=VECBAR(I, 1)/EMUBAR(I)
  VECBAR(I, 2)=VECBAR(I, 2)/EMUBAR(I)
  96 VECBAR(I, 2)=VECBAR(I, 2)/EMUBAR(I)
  99 TOT=EM+EMC
  CALL SSIN(GAM, SGAM, 1)
  CALL SSIN(ETA, SETA, 1)
  RETURN
  8 FORMAT(3E15.8)
  END

```

```

C 08340 83800000
C 08350 83900000
C 08360 84000000
C 08370 84100000
C 08380 84200000
C 08390 84300000
C 08400 84400000
C 08410 84500000
C 08420 84600000
C 08430 84700000
C 08440 84800000
C 08450 84900000
C 08460 85000000
C 08470 85100000
C 08480 85200000
C 08490 85300000
C 08500 85400000
C 08510 85500000
C 08520 85600000
C 08530 85700000
C 08540 85800000
C 08550 85900000
C 08560 86000000
C 08570 86100000
C 08580 86200000
C 08590 86300000
C 08600 86400000
C 08610 86500000
C 08620 86600000
C 08630 86700000
C 08640 86800000
C 08650 86900000
C 08660 87000000
C 08670 87100000
C 08680 87200000
C 08690 87300000
C 08700 87400000
C 08710 87500000
C 08720 87600000
C 08730 87700000

```

```

SUBROUTINE LAB(NLAB)
COMMON I,K,RDOT,XIDEN,RHO,A,RI,RID,WXI,LAMI,LAM2,LAM3,
* G1,G2,USE,HOLD,SAVE,XCI,XC2,G3,G4,G5
COMMON /RIG/PIETA(3,3),PIGAM(3,3),SUML(3,3),SUMT,SCAM(3,3),SETA(3,3)C
* ,QP(3,6,100),EMA(6,6,100),EMD(6,6,100)
COMMON /LABOR/WX,RI,QS,QSD,THS,THSD,XMAS,XINERT
COMMON /LCADS/ZZ(3,3),PHSI(6,100)
COMMON /EXTRA/ZFX(3),ZLX(3),ZMX(3),ZCY(3),ZCM(3),EMC,TOT
COMMON /ALLCNT/IS,0(3)
REAL LAMI(3,3),LAM2(3,3),LAM3(3,3),XIDEN(3,3),G1(3,3),
1 G2(3,3),USE(3,3),G3(3,3),G4(3,3),G5(3,3),
2 R(3),RDOT(3),WX(3),WXI(3,100),RI(3,100),RID(3,100),
3 HOLD(3),SAVE(3),XCI(3),XC2(3),
4 RIO(3,100),XINERT(3,3,100),QS(3,100),
5 QSD(3,100),THS(3,100),THSD(3,100),XMAS (100)
CALL GAMMA(WX,G5)
DO 98 I=1,3
ZFX(I)=0.
ZLX(I)=0.
SUML(I)=0.
SUMT=0.
98 ZMX(I)=0.
DO 100 L=1,NLAB
XMASS=XMAS(L)
DO 20 I=1,3
RI(I,L)=R(I)+RIO(I,L)+QS(I,L)
ZLX(I)=ZLX(I)+XMASS*RI(I,L)
20 RID(I,L)=RDOT(I)+QSD(I,L)
CALL GAMMA(THS(I,L),G1)
CALL ADD(XIDEN,G1,G3,3)
CALL SUBTR(XIDEN,G1,USE,3)
CALL MULT(USE,WX,G1,1)
CALL ADD(G1,THSD(1,L),WXI(1,L),1)
IF(L.EQ.IS)CALL MCPY(WXI(1,L),0,3,1,1)
COMPUTE LAMI
CALL SCALR(XMASS,XIDEN,LAMI,3)
COMPUTE LAM2
CALL GAMMA(RI(1,L),G4)
SC=-XMASS
CALL SCALR(SC,G4,LAM2,3)
COMPUTE LAM3
CALL MULT(XINERT(1,1,L),USE,LAM3,3)
COMPUTE XCI
CALL SCALR(2.,G5,G2,3)
CALL MULT(G2 ,RID(1,L),HOLD,1)
CALL MULT(G5,G5,USE,3)
CALL MULT(USE,RI(1,L),SAVE,1)
CALL ADD(HOLD,SAVE,XCI,1)
CALL SCALR(XMASS,XCI,XCI,1)

```

87800000

C 08740

87900000

C 08750

88000000

C 08760

88100000

C 08770

88200000

C 08780

88300000

C 08790

88400000

C 08800

88500000

C 08810

88600000

C 08820

88700000

C 08830

88800000

C 08840

88900000

C 08850

89000000

C 08860

89100000

C 08870

89200000

C 08880

89300000

C 08890

89400000

C 08900

89500000

C 08910

89600000

C 08920

89700000

C 08930

89800000

C 08940

89900000

C 08950

90000000

C 08960

90100000

C 08970

90200000

C 08980

90300000

C 08990

90400000

C 09000

90500000

C 09010

90600000

C 09020

90700000

C 09030

90800000

C 09040

90900000

C 09050

91000000

C 09060

91100000

C 09070

91200000

C 09080

91300000

C 09090

91400000

C 09100

91500000

C 09110

91600000

C 09120

91700000

C 09130

91800000

C 09140

91900000

C 09150

92000000

C 09160

92100000

C 09170

92200000

C 09180

92300000

C 09190

92400000

C 09200

92500000

C 09210

92600000

C 09220

```

CALL SCALR(-1.,XC1,RHSI(1,L),1)
COMPUTE XC2
CALL GAMMA(WXI(1,L),G2)
CALL GAMMA(THSD1(L),G1)
CALL MULT(XINERT(1,L),G1,G1,USE,3)
CALL MULT(USE,WX,HOLD,1)
CALL MULT(G2,XINERT(1,L),USE,3)
CALL MULT(USE,WX,HOLD,1)
CALL SURTR(SAVE,HOLD,XC2,1)
CALL SCALR(-1.,XC2,RHSI(4,L),1)
C* INITIALIZE A,D PARTITIONS
DO 10 I=1,3
DO 10 J=1,3
EMD(I,J,L)=LAM1(I,J)
EMD(I+3,J+3,L)=XINERT(I,J,L)
EMD(I+3,J,L)=0.
EMD(I,J+3,L)=0.
EMA(I,J,L)=LAM1(I,J)
EMA(I,J+3,L)=LAM2(I,J)
EMA(I+3,J,L)=0.
10 EMA(I+3,J+3,L)=IAM3(I,J)
C* FORM OP MATRIX PARTITIONS
CALL SCALR(1.,G3,OP(1,4,L),3)
CALL SCALR(1.,G4,OP(1,1,L),3)
C* SUM L AND T
CALL MULT(G5,RI(1,L),HOLD,1)
CALL ADD(RID(1,L),HOLD,HOLD,1)
SUM=.5*XMSS*OTP(HOLD,HOLD)
CALL MULT(G4,HOLD,SAVE,1)
CALL SCALR(XMSS,SAVE,SAVE,1)
CALL MULT(XINERT(1,L),WXI(1,L),HOLD,1)
SUMT=SUMT+SUM+.5*OTP(WXI(1,L),HOLD)
CALL MULT(G3,HOLD,USE,1)
CALL ADD(SAVE,USE,SAVE,1)
CALL MTRAN(PIGAM,SAVE,HOLD,1)
CALL ADD(SUMI,HOLD,SUMI,1)
100 CONTINUE
RETURN
END

```

```

C 09230 92700000
C 09240 92800000
C 09250 92900000
C 09260 93000000
C 09270 93100000
C 09280 93200000
C 09290 93300000
C 09300 93400000
C 09310 93500000
C 09320 93600000
C 09330 93700000
C 09340 93800000
C 09350 93900000
C 09360 94000000
C 09370 94100000
C 09380 94200000
C 09390 94300000
C 09400 94400000
C 09410 94500000
C 09420 94600000
C 09430 94700000
C 09440 94800000
C 09450 94900000
C 09460 95000000
C 09470 95100000
C 09480 95200000
C 09490 95300000
C 09500 95400000
C 09510 95500000
C 09520 95600000
C 09530 95700000
C 09540 95800000
C 09550 95900000
C 09560 96000000
C 09570 96100000
C 09580 96200000
C 09590 96300000
C 09600 96400000
C 09610 96500000

```

```

SUBROUTINE RESVK(L,IPOINT,SUM,V,VDOT,IFLAG)
COMMON /INOUT/IN,OUT,IOFF
COMMON T,F,ROOT,XIDEN,RHO,A,RI,RID,WXI,LAM1,LAM2,LAM3,
* HOLD,SAVE,XC,G1,G2,G3,G4,DELU,S,G,XL,XLDDOT,UC,
* UCDDOT,XIF,XDIR,HXC,G5,G6,H1,H2,H3,H4
COMMON /LABOR/WX,RI0(900),TH,THD,XMAS,XINERT
COMMON/RIG/PIETA(3,3),PIGAM(3,3),SUML(3),SUMT,SGAM(3,3),
* SETA(3,3),QP(3,6,100),EMA(6,6,100),EMD(6,6,100)
COMMON /RES/XMIP,XIIP,SIP,UIR,EIR,UIB,EIR,XJIB,BI,HIO,
* HIMAX,HIMIN,GIP,XLI
COMMON /LGADS/ZZ(33),RHSI(6,100)
COMMON /PASS/Q,QDOT,STEP
COMMON /EXTRA/ZFX(3),ZLX(3),ZMX(3),ZCY(3),ZCM(3),EMC,TOT
DIMENSION XIDEN(3,3),R(3),ROOT(3),TH(3,100),THD(3,100),
* XMIP(2),XIIP(3,3,2),SIP(3,2),UIR(3,2),FIR(3,2),UIB(3,2),
* EIR(3,2),XJIB(3,3,2),GIP(3,2),XLI(3,2),HI(2),HIO(2),
* HIMAX(2),HIMIN(2),G1(3,3),G2(3,3),G3(3,3),G4(3,3),
* HOLD(3),SAVE(3),XC(3),DELU(3),S(3),G(3),XL(3),XLDDOT(3),
* UC(3),UCDDOT(3),XIF(3,3),XDIR(3,3),HXC(3)
* ,RI(3,100),RID(3,100),WX(3),WXI(3,100)
* ,G5(3,3),G6(3,3),HI(3),H2(3),H3(3),H4(3)
* ,XMAS(100),XINERT(3,3,100)
* ,HIL(2)
COMMON /VAROUT/DDD(92),HIL
REAL LAM1(3,3),LAM2(3,3),LAM3(3,3),K
IF(IFLAG.FQ.1)GO TO 10
IF(L.EQ.2)GO TO 3
K=-1.
DO 15 I=1,2
K=-K
AIR=3.141592653*BI(I)*BI(I)
HIL(I)=HI0(I)-K*(A/AIR)*SUM
IF(HIL(I).LE.HIMAX(I))GO TO 19
IFLAG=1
HIL(I)=HIMAX(I)
GO TO 15
19 IF(HIL(I).GE.HIMIN(I))GO TO 15
IFLAG=1
HIL(I)=HIMIN(I)
15 CONTINUE
IF(IFLAG.EQ.0)GO TO 3
VDOT=-V/(STEP/2.)
V=0
THOLD=T
GO TO 3
10 IF(T.LE.THOLD)GO TO 3
VDOT=0
3 CONTINUE
HI=HIL(L)

```

```

C 09620 96600000
C 09630 96700000
C 09640 96800000
C 09650 96900000
C 09660 97000000
C 09670 97100000
C 09680 97200000
C 09690 97300000
C 09700 97400000
C 09710 97500000
C 09720 97600000
C 09730 97700000
C 09740 97800000
C 09750 97900000
C 09760 98000000
C 09770 98100000
C 09780 98200000
C 09790 98300000
C 09800 98400000
C 09810 98500000
C 09820 98600000
C 09830 98700000
C 09840 98800000
C 09850 98900000
C 09860 99000000
C 09870 99100000
C 09880 99200000
C 09890 99300000
C 09900 99400000
C 09910 99500000
C 09920 99600000
C 09930 99700000
C 09940 99800000
C 09950 99900000
C 09960 10000000
C 09970 10010000
C 09980 10020000
C 09990 10030000
C 10000 10040000
C 10010 10050000
C 10020 10060000
C 10030 10070000
C 10040 10080000
C 10050 10090000
C 10060 10100000
C 10070 10110000
C 10080 10120000
C 10090 10130000
C 10100 10140000

```

```

Q=RHO*A*V
QDOT=RHO*A*VDDOT
K=1.
IF(L.EQ.2)K=-1.
AIR=3.14159265*BI(L)*BI(L)
20 XLI(2,L)=ARSIN(EIR(1,L))
XLI(3,L)=0.
CS=COS(XLI(2,L))
SC=EIR(3,L)/CS
CS=-EIR(2,L)/CS
XLI(1,L)=ARSIN(CS)
IF(SC)42,44,44
44 IF(CS.GE.0.160 TO 45
XLI(1,L)=XLI(1,L)+6.283185306
GO TO 45
42 XLI(1,L)=3.141592653-XLI(1,L)
45 CONTINUE
CALL PIF(XLI(1,L),LAMI)
XMIR=RHO*AIR*HI
XMIF=XMIP(L)+XMIR
CALL GAMMA(UIR(1,L),GL)
DO 30 I=1,3
DELU(I)=UIR(1,L)-UIR(I,L)+HI*EIR(I,L)
S(I)=SJP(I,L)+XMIR*(UIR(I,L)-HI*EIR(I,L)/2.)
G(I)=GIP(I,L)+HI*(GI(1,L)+GIR(1,L)+GI(1,2)*EIR(2,L)+GI(I,3)
**EIR(3,L))
XL(I)=(3.*BI(L)*BI(L)+HI*HI)*XMIR/12.
IF(I.EQ.3)XL(I)=.5*HI(L)*BI(L)*XMIR
XLDOT(I)=-K*Q*RI(L)*BI(L)+HI*HI)/4.
IF(I.EQ.3)XLDOT(I)=-K*Q*BI(L)*RI(L)/2.
UC(I)=UIR(I,L)-.5*HI*LAMI(3,I)
30 UCDDOT(I)=K/2.*V*A/AIR*LAMI(3,I)
COMPUTE XIF
CALL GAMMA(UC,G4)
CALL MULT(G4,G4,G1,3)
CALL SCALP(XMIR,G1,G3,3)
CALL PTLP(LAMI,XL,G2)
CALL SUBTR(G2,G3,G2,3)
CALL ADD(XIIP(1,L),G2,XIF,3)
COMPUTE XDIR
CALL PTLP(LAMI,XLDDOT,G2)
SC=K*Q
CALL SCALR(SC,G1,G1,3)
CALL ADD(G1,G2,G1,3)
CALL GAMMA(UCDDOT,G3)
CALL MULT(G3,G4,G2,3)
CALL MULT(G4,G3,XDIR,3)
CALL ADD(G2,XDIR,G3,3)
CALL SCALR(XMIR,G3,G3,3)
CALL SUBTR(G1,G3,XDIR,3)
COMPUTE XC5

```

```

C 10110 101500000
C 10120 101600000
C 10130 101700000
C 10140 101800000
C 10150 101900000
C 10160 102000000
C 10170 102100000
C 10180 102200000
C 10190 102300000
C 10200 102400000
C 10210 102500000
C 10220 102600000
C 10230 102700000
C 10240 102800000
C 10250 102900000
C 10260 103000000
C 10270 103100000
C 10280 103200000
C 10290 103300000
C 10300 103400000
C 10310 103500000
C 10320 103600000
C 10330 103700000
C 10340 103800000
C 10350 103900000
C 10360 104000000
C 10370 104100000
C 10380 104200000
C 10390 104300000
C 10400 104400000
C 10410 104500000
C 10420 104600000
C 10430 104700000
C 10440 104800000
C 10450 104900000
C 10460 105000000
C 10470 105100000
C 10480 105200000
C 10490 105300000
C 10500 105400000
C 10510 105500000
C 10520 105600000
C 10530 105700000
C 10540 105800000
C 10550 105900000
C 10560 106000000
C 10570 106100000
C 10580 106200000
C 10590 106300000
C 10600 106400000
C 10610 106500000

```

CALL GAMMA(WX,G1)	C	10620	1066000000
CALL GAMMA(TH(1,IPOINT),G2)	C	10630	1067000000
CALL MULT(G1,RID(1,IPOINT),HOLD,1)	C	10640	1068000000
CALL MULT(G1,G1,G3,3)	C	10650	1069000000
C	C	10660	1070000000
C	C	10670	1071000000
L,T	C	10680	1072000000
CALL MULT(G1,RI(1,IPOINT),H1,1)	C	10690	1073000000
CALL ADD(RID(1,IPOINT),H1,H1,1)	C	10700	1074000000
C	C	10710	1075000000
C	C	10720	1076000000
CALL MULT(G3,RI(1,IPOINT),SAVE,1)	C	10730	1077000000
CALL SCALR(2,,HOLD,HOLD,1)	C	10740	1078000000
CALL ADD(HOLD,SAVE,HXC,1)	C	10750	1079000000
CALL SCALP(XMIF,HXC,XC,1)	C	10760	1080000000
CALL ADD(G2,XIDEN,G6,3)	C	10770	1081000000
C	C	10780	1082000000
C	C	10790	1083000000
C	C	10800	1084000000
C	C	10810	1085000000
C	C	10820	1086000000
C	C	10830	1087000000
C	C	10840	1088000000
C	C	10850	1089000000
C	C	10860	1090000000
CALL GAMMA (THD(1,IPOINT),G1)	C	10870	1091000000
CALL MULT(G1,WX,H2,1)	C	10880	1092000000
CALL GAMMA(S,G1)	C	10890	1093000000
CALL MULT(G1,H2,HOLD,1)	C	10900	1094000000
CALL GAMMA(WXI(1,IPOINT),G1)	C	10910	1095000000
CALL MULT(G1,G1,G4,3)	C	10920	1096000000
CALL MULT(G4,S,SAVE,1)	C	10930	1097000000
C	C	10940	1098000000
L,T	C	10950	1099000000
CALL MULT(G1,S,H2,1)	C	10960	1100000000
SC=K#0	C	10970	1101000000
CALL SCALR(SC,DELU,H3,1)	C	10980	1102000000
CALL ADD(H2,H3,H3,1)	C	10990	1103000000
CALL MULT(G6,H3,H2,1)	C	11000	1104000000
SUMT=SUMT+DOTP(H1,H2)	C	11010	1105000000
CALL SCALR(XMIF,H1,H3,1)	C	11020	1106000000
CALL ADD(H3,H2,H2,1)	C	11030	1107000000
SUMT=SUMT+.5*DOTP(H3,H1)	C	11040	1108000000
L,T	C	11050	1109000000
C	C	11060	1110000000
CALL ADD(HOLD,SAVE,HOLD,1)	C	11070	1111000000
CALL MULT(G1,DELU,SAVE,1)	C	11080	1112000000
SC=K#2.*Q	C	11090	1113000000
CALL SCALR(SC,SAVE,SAVE,1)	C	11100	1114000000
CALL ADD(HOLD,SAVE,HOLD,1)	C	11110	1115000000
SC=A/AIR	C	11120	1116000000
CALL SCALR(SC,EIR(1,L),SAVE,1)	C		


```

CALL SUBTR(EB(1,L),SAVE,SAVE,1)
SC=Q*V
CALL SCALR(SC,SAVE,SAVE,1)
CALL ADD(SAVE,HOLD,HOLD,1)
SC=K*QDOT
CALL SCALR(SC,DELJ,SAVE,1)
CALL ADD(SAVE,HOLD,HOLD,1)
CALL MULT(G6,HOLD,SAVE,1)
CALL ADD(XC,SAVE,XC,1)
CALL SUBTR(RHS(1,IPOINT),XC,RHS(1,IPOINT),1)
COMPUTE LAM1
CALL SCALR(XMIF,XIDEN,LAM1,3)
CCOMPUTE LAM12
CALL SUBTR(XIDEN,G2,G2,3)
CALL GAMMA(S,G1)
CALL MULT(G6,G1,G4,3)
CALL MULT(G4,G2,G5,3)
CALL GAMMA(RI(1,IPOINT),G3)
C
C *L,T*
CALL MULT(G3,H2,H3,1)
CALL MULT(G5,H1,H4,1)
CALL ADD(H3,H4,H4,1)
C *L,T*
C
CALL SCALR(XMIF,G3,LAM3,3)
CALL ADD(G5,LAM3,LAM2,3)
CALL SCALR(-1.,LAM2,LAM2,3)
COMPUTE LAM13
CALL SCALR(-1.,G4,LAM3,3)
C* ADD TO A AND D
DO 40 I=1,3
DO 40 J=1,3
EMA(I,J,IPOINT)=EMA(I,J,IPOINT)+LAM1(I,J)
EMA(I,J+3,IPOINT)=EMA(I,J+3,IPOINT)+LAM2(I,J)
EMD(I,J,IPOINT)=EMD(I,J,IPOINT)+LAM1(I,J)
40 EMD(I,J+3,IPOINT)=EMD(I,J+3,IPOINT)+LAM3(I,J)
COMPUTE LAM14
CALL MULT(G1,G2,LAM1,3)
COMPUTE LAM15
CALL MULT(LAM1,G3,LAM2,3)
CALL MULT(XIF,G2,LAM3,3)
CALL SUBTR(LAM3,LAM2,LAM2,3)
COMPUTE XC6
CALL MULT(LAM1,HXC,XC,1)
CALL GAMMA(THD(1,IPOINT),G1)
CALL MULT(G1,WX,HOLD,1)
CALL MULT(XIF,HOLD,SAVE,1)
CALL SUBTR(XC,SAVE,XC,1)
SC=K*RHO*V
CALL SCALR(SC,XJIB(1,L),G1,3)
C 11130 111700000
C 11140 111800000
C 11150 111900000
C 11160 112000000
C 11170 112100000
C 11180 112200000
C 11190 112300000
C 11200 112400000
C 11210 112500000
C 11220 112600000
C 11230 112700000
C 11240 112800000
C 11250 112900000
C 11260 113000000
C 11270 113100000
C 11280 113200000
C 11290 113300000
C 11300 113400000
C 11310 113500000
C 11320 113600000
C 11330 113700000
C 11340 113800000
C 11350 113900000
C 11360 114000000
C 11370 114100000
C 11380 114200000
C 11390 114300000
C 11400 114400000
C 11410 114500000
C 11420 114600000
C 11430 114700000
C 11440 114800000
C 11450 114900000
C 11460 115000000
C 11470 115100000
C 11480 115200000
C 11490 115300000
C 11500 115400000
C 11510 115500000
C 11520 115600000
C 11530 115700000
C 11540 115800000
C 11550 115900000
C 11560 116000000
C 11570 116100000
C 11580 116200000
C 11590 116300000
C 11600 116400000
C 11610 116500000
C 11620 116600000
C 11630 116700000

```

```

CALL ADD(XDIR,G1,G1,3)
CALL MULT(G1,WXI(1,IPOINT),HOLD,1)
CALL ADD(XC,HOLD,XC,1)
SC=K*Q
CALL SCALR(SC,G,HOLD,1)
CALL MULT(XIF,WXI(1,IPOINT),SAVE,1)
CALL ADD(HOLD,SAVE,HOLD,1)
C
C
C *L,T*
SUMT=SUMT+.5*DOTP(WXI(1,IPOINT),SAVE)
*
+SC*DOTP(WXI(1,IPOINT),G)
CALL MULT(G6,HOLD,H2,1)
CALL ADD(H2,H4,H4,1)
CALL MTRAN(PIGAM,H4,H3,1)
CALL ADD(SUML,H3,SUML,1)
SUMT=SUMT+.5*V*V*(XIMP(L)+XIMP*A*/(AIR*AIR))
C
C *L,T*
CALL GAMMA(WXI(1,IPOINT),G1)
CALL MULT(G1,HOLD,SAVE,1)
CALL ADD(XC,SAVE,XC,1)
SC=K*QDOT
CALL SCALP(SC,G,HOLD,1)
CALL ADD(XC,HOLD,XC,1)
CALL GAMMA(UIR(1,L),G1)
CALL MULT(G1,EIR(1,L),HOLD,1)
SC=-A/AIR
CALL SCALR(SC,HOLD,HOLD,1)
CALL GAMMA(UIB(1,L),G1)
CALL MULT(G1,EIB(1,L),SAVE,1)
CALL ADD(HOLD,SAVE,HOLD,1)
SC=Q*V
CALL SCALR(SC,HOLD,HOLD,1)
CALL ADD(XC,HOLD,XC,1)
CALL SUBTR(RHSI(4,IPOINT),XC,RHSI(4,IPOINT),1)
C*
ADD TO A AND D
DO 50 I=1,3
DO 50 J=1,3
EMA(I+3,J,IPOINT)=EMA(I+3,J,IPOINT)+LAM1(I,J)
EMA(I+3,J+3,IPOINT)=EMA(I+3,J+3,IPOINT)+LAM2(I,J)
EMD(I+3,J,IPOINT)=EMD(I+3,J,IPOINT)+LAM1(I,J)
EMD(I+3,J+3,IPOINT)=EMD(I+3,J+3,IPOINT)+XIF(I,J)
50
RETURN
END

```

```

C 11640 116800000
C 11650 116900000
C 11660 117000000
C 11670 117100000
C 11680 117200000
C 11690 117300000
C 11700 117400000
C 11710 117500000
C 11720 117600000
C 11730 117700000
C 11740 117800000
C 11750 117900000
C 11760 118000000
C 11770 118100000
C 11780 118200000
C 11790 118300000
C 11800 118400000
C 11810 118500000
C 11820 118600000
C 11830 118700000
C 11840 118800000
C 11850 118900000
C 11860 119000000
C 11870 119100000
C 11880 119200000
C 11890 119300000
C 11900 119400000
C 11910 119500000
C 11920 119600000
C 11930 119700000
C 11940 119800000
C 11950 119900000
C 11960 120000000
C 11970 120100000
C 11980 120200000
C 11990 120300000
C 12000 120400000
C 12010 120500000
C 12020 120600000
C 12030 120700000
C 12040 120800000
C 12050 120900000
C 12060 121000000
C 12070 121100000

```

```

SUBROUTINE PIPE(L, IPOINT, V, VDOT)
COMMON /INOUT/IN, IOUT, IOFF
COMMON T, R, ROOT, XIDEN, RHC, A, RI, RID, WXI, LAM1, LAM2, LAM3,
* G1, G2, G3, G4, XC, HXC, SAVE, HOLD
* G5, G6, H1, H2, H3, H4
COMMON /LABDR/WX, AI(900), TH, THD
COMMON/BIG/PIETA(3,3), PIGAM(3,3), SUML(3), SUMT, SGAM(3,3),
* SETA(3,3), QP(3,6,100), EMA(6,6,100), FMD(6,6,100)
COMMON /PIPES/XMIF, XIF, S, DELU, DELF, G, DELJ, VEC
COMMON /LOADS/ZZ(33), RHSI(6,100)
COMMON /PASS/Q, QDOT
COMMON /EXTRA/ZFX(3), ZLX(3), ZMX(3), ZCY(3), ZCM(3), EMC, TOT
DIMENSION R(3), ROOT(3), TH(3,100), THD(3,100), WX(3), WXI(3,100),
* G1(3,3), G2(3,3), G3(3,3), G4(3,3), XC(3,3), HXC(3), SAVE(3),
* HOLD(3), RI(3,100), RID(3,100), XIDEN(3,3)
* G5(3,3), G6(3,3), H1(3), H2(3), H3(3), H4(3)
REAL LAM1(3,3), LAM2(3,3), LAM3(3,3)
DIMENSION XMIF(30), XIF(3,3,30), S(3,30), DELU(3,30), DELE(3,30),
* G(3,30), DELJ(3,3,30), VFC(3,30)
CALL GAMMA(TH(1, IPOINT), G1)
CALL SUBTR(XIDEN, G1, G2, 3)
CALL ADD(XIDEN, G1, G1, 3)

C NEXT 5 LINES ADD TO ZFX AND TOT
CALL MULT(G1, S(1,1), HOLD, 1)
CALL SCALK(XMIF(L), RI(1, IPOINT), SAVE, 1)
CALL ADD(HOLD, SAVE, HOLD, 1)
CALL ADD(HOLD, ZFX, ZFX, 1)
IF(T.EQ.0.)TOT=TOT+XMIF(L)

CALL GAMMA(S(1, L), LAM2)
CALL MULT(G1, LAM2, LAM3, 3)
C - LAM7
CALL SCALR(-1., LAM3, LAM3, 3)
CALL MULT(LAM3, G2, LAM2, 3)
C
C *L,T*
CALL SCALR(-1., LAM2, G5, 3)
C
CALL GAMMA(RI(1, IPOINT), G4)
SC=-XMIF(L)
CALL SCALR(SC, G4, G3, 3)
C - LAM6
CALL ADD(G3, LAM2, LAM2, 3)
COMPUTE XC
CALL GAMMA(WX, G3)
CALL MULT(G3, G3, LAM1, 3)

```

```

C 12080 121200000
C 12090 121300000
C 12100 121400000
C 12110 121500000
C 12120 121600000
C 12130 121700000
C 12140 121800000
C 12150 121900000
C 12160 122000000
C 12170 122100000
C 12180 122200000
C 12190 122300000
C 12200 122400000
C 12210 122500000
C 12220 122600000
C 12230 122700000
C 12240 122800000
C 12250 122900000
C 12260 123000000
C 12270 123100000
C 12280 123200000
C 12290 123300000
C 12300 123400000
C 12310 123500000
C 12320 123600000
C 12330 123700000
C 12340 123800000
C 12350 123900000
C 12360 124000000
C 12370 124100000
C 12380 124200000
C 12390 124300000
C 12400 124400000
C 12410 124500000
C 12420 124600000
C 12430 124700000
C 12440 124800000
C 12450 124900000
C 12460 125000000
C 12470 125100000
C 12480 125200000
C 12490 125300000
C 12500 125400000
C 12510 125500000
C 12520 125600000
C 12530 125700000
C 12540 125800000
C 12550 125900000
C 12560 126000000

```

C	CALL MULT(LAMI,RI(1,IPOINT),HOLD,1)	C	12570	126100000
C	CALL MULT(G3,RID(1,IPOINT),SAVE,1)	C	12580	126200000
		C	12590	126300000
C	*L,T*	C	12600	126400000
	CALL MULT(G3,RI(1,IPOINT),H1,1)	C	12610	126500000
	CALL ADD(FID(1,IPOINT),H1,H1,1)	C	12620	126600000
	SUMT=SUMT+.5*X*MIF(L)*(DOTP(H1,H1)+*V)	C	12630	126700000
C		C	12640	126800000
C		C	12650	126900000
	CALL SCALR(2.,SAVE,SAVE,1)	C	12660	127000000
	CALL ADD(SAVE,HOLD,HXC,1)	C	12670	127100000
	CALL SCALR(XMIF(L),HXC,XC,1)	C	12680	127200000
	CALL SCALF(QDOT,DELU(1,L),HOLD,1)	C	12690	127300000
	CALL GAMMA(WXI(1,IPOINT),G3)	C	12700	127400000
	CALL MULT(G3,DELU(1,L),SAVE,1)	C	12710	127500000
	SC=2.*Q	C	12720	127600000
	CALL SCALR(SC,SAVE,SAVE,1)	C	12730	127700000
	CALL ADD(HOLD,SAVE,SAVE,1)	C	12740	127800000
	CALL MULT(G3,S(1,L),HOLD,1)	C	12750	127900000
C		C	12760	128000000
C	*L,T*	C	12770	128100000
	CALL SCALR(Q,DELU(1,L),H4,1)	C	12780	128200000
	CALL ADD(HOLD,H4,H4,1)	C	12790	128300000
	CALL MULT(G2,H4,H3,1)	C	12800	128400000
	SUMT=SUMT+DOTP(H1,H3)	C	12810	128500000
	CALL SCALR(XMIF(L),H1,H2,1)	C	12820	128600000
	CALL ADD(H3,H2,H2,1)	C	12830	128700000
	CALL MULT(G4,H2,H3,1)	C	12840	128800000
	CALL MULT(G5,H1,H2,1)	C	12850	128900000
	CALL ADD(H2,H3,H3,1)	C	12860	129000000
C		C	12870	129100000
C		C	12880	129200000
	CALL MULT(G3,HOLD,LAMI,1)	C	12890	129300000
	CALL ADD(SAVE,LAMI,SAVE,1)	C	12900	129400000
	SC=V*Q	C	12910	129500000
	CALL SCALR(SC,DELETE(1,L),HOLD,1)	C	12920	129600000
	CALL ADD(HOLD,SAVE,SAVE,1)	C	12930	129700000
	CALL GAMMA(THD(1,IPOINT),G3)	C	12940	129800000
	CALL MULT(G3,WX,H2,1)	C	12950	129900000
	CALL GAMMA(S(1,L),G3)	C	12960	130000000
	CALL MULT(G3,H2,HOLD,1)	C	12970	130100000
	CALL ADD(HOLD,SAVE,SAVE,1)	C	12980	130200000
	CALL MULT(G1,SAVE,HOLD,1)	C	12990	130300000
	CALL ADD(XC,HOLD,XC,1)	C	13000	130400000
	CALL SUBTR(RHSI(1,IPOINT),XC,RHSI(1,IPOINT),1)	C	13010	130500000
COMPUTE	LAM5	C	13020	130600000
	CALL SCALR(XMIF(L),XIDEN,LAMI,3)	C	13030	130700000
C*	ADD TO A AND D	C	13040	130800000
	DD 40 I=1,3	C	13050	130900000
	DD 40 J=1,3	C	13060	131000000
	EMA(I,J,IPOINT)=EMA(I,J,IPOINT)+LAMI(I,J)	C	13070	131100000

```

EMAI(I,J+3,IPOINT)=EMA(I,J+3,IPOINT)+LAM2(I,J)
EMD(I,J,IPOINT)=EMD(I,J,IPOINT)+LAMI(I,J)
40 EMD(I,J+3,IPOINT)=EMD(I,J+3,IPOINT)+LAM3(I,J)
C - LAMB
CALL MULT(G3 ,G2,LAMI,3)
CALL MULT(XIF(1,1,1),G2,LAM2,3)
CALL MULT(LAMI,G4,LAM3,3)
C - LAM9
CALL SUBTR(LAM2,LAM3,LAM2,3)
COMPUTE XC
CALL MULT(LAMI,HXC,XC,1)
SC=Q*V
CALL SCALAR(SC,VEC(1,L),HOLD,1)
CALL ADD(XC,HOLD,XC,1)
CALL SCALAR(QDOT,G(1,L),HOLD,1)
CALL ADD(XC,HOLD,XC,1)
SC=RHO*V
CALL MULT(DELJ(1,1,L),WXI(1,IPOINT),HOLD,1)
CALL SCALAR(SC,HOLD,HOLD,1)
CALL ADD(XC,HOLD,XC,1)
CALL MULT(XIF(1,1,L),H2 ,SAVE,1)
CALL SUBTR(XC,SAVE,XC,1)
CALL MULT(XIF(1,1,L),WXI(1,IPOINT),HOLD,1)
CALL SCALAR(Q,G(1,L),SAVE,1)
C
C *L,T*
SUMT=SUMT+.5*DOTP(WXI(1,IPOINT),HOLD)+DOTP(WXI(1,IPOINT),SAVE)
C
C
CALL ADD(HOLD,SAVE,SAVE,1)
C
C *L,T*
CALL MULT(G2,SAVE,HOLD,1)
CALL ADD(H3,HOLD,H3,1)
CALL MTRAN(PIGAM,H3,H2,1)
CALL ADD(SUML,H2,SUML,1)
C
C
CALL GAMMA(WXI(1,IPOINT),G1)
CALL MULT(G1,SAVE,HOLD,1)
CALL ADD(XC,HOLD,XC,1)
CALL SUBTR(RHSI(4,IPOINT),XC,RHSI(4,IPOINT),1)
C* ADD TO A AND D
DO 50 I=1,3
DO 50 J=1,3
EMA(I+3,J,IPOINT)=EMA(I+3,J,IPOINT)+LAMI(I,J)
EMA(I+3,J+3,IPOINT)=EMA(I+3,J+3,IPOINT)+LAM2(I,J)
EMD(I+3,J,IPOINT)=EMD(I+3,J,IPOINT)+LAMI(I,J)
50 EMD(I+3,J+3,IPOINT)=EMD(I+3,J+3,IPOINT)+XIF(I,J,L)
RETURN
END

```

```

C 13080 131200000
C 13090 131300000
C 13100 131400000
C 13110 131500000
C 13120 131600000
C 13130 131700000
C 13140 131800000
C 13150 131900000
C 13160 132000000
C 13170 132100000
C 13180 132200000
C 13190 132300000
C 13200 132400000
C 13210 132500000
C 13220 132600000
C 13230 132700000
C 13240 132800000
C 13250 132900000
C 13260 133000000
C 13270 133100000
C 13280 133200000
C 13290 133300000
C 13300 133400000
C 13310 133500000
C 13320 133600000
C 13330 133700000
C 13340 133800000
C 13350 133900000
C 13360 134000000
C 13370 134100000
C 13380 134200000
C 13390 134300000
C 13400 134400000
C 13410 134500000
C 13420 134600000
C 13430 134700000
C 13440 134800000
C 13450 134900000
C 13460 135000000
C 13470 135100000
C 13480 135200000
C 13490 135300000
C 13500 135400000
C 13510 135500000
C 13520 135600000
C 13530 135700000
C 13540 135800000
C 13550 135900000
C 13560 136000000
C 13570 136100000
C 13580 136200000

```

```

SUBROUTINE LUMP(L, IPOINT)
COMMON /INOUT/IN, IOUT, IOFF
COMMON T, P, RDOT, XIDEN, RHO, A, RI, RID, WXI, LAM1, LAM2, LAM3,
* K, LAM, DK, W, WD, HOLD, SAVE, G1, G2, G3, G4, XC
* HI, H2, HXC
* , LAM4, LAM5, LAM6, DIGA(6,6), BIGD(6,6)
COMMON /BIG/PIETA(3,3), PIGAM(3,3), SUML(3), SUMT
* , SGAM(1818), EMA(6,6,100), EMP(6,6,100)
COMMON /LABOR/WX(3), RIO, Q, QD, TH, THD
COMMON /LUMPS/U
COMMON /GADS/77(33), RHSI(6,100)
COMMON /EXTRA/ZEX(3), ZLX(3), ZMX(3), ZCY(3), ZCM(3), EMC, TOT
DIMENSION U(8), UJ(3), UJD(3), UJDD(3), K(16), DK(3,16), RIO(3,100),
* W(3), WD(3), HOLD(3), SAVE(3), G1(3,3), G2(3,3), G3(3,3),
* G4(3,3), XC(6), TH(3,100), THD(3,100), Q(3,100), QD(3,100),
* XIDEN(3,3), F(3), RDOT(3), RI(3,100), RID(3,100), PI(16)
* HI(3), H2(3), HXC(3), WXI(3,100)
REAL LAM(16), LAM1(3,3), LAM2(3,3), LAM3(3,3)
* , LAM4(3,3), LAM5(3,3), LAM6(3,3)
IF(T.EQ.0.)TOT=TOT+U(L)
IF(L.NE.2)CALL MUCOM(UJ, UJD, UJDD, L)
IF(L.EQ.2)CALL BMCEN(UJ, UJD, UJDD)
CALL LOOK(L, K, M, IPOINT)
DO 10 I=1, M
PI(I)=1.
KI=K(I)
10 CALL SUBTR(UJ, RIO(1, KI), DK(1, I), I)
IF(M.EQ.1)GO TO 29
DO 20 I=1, M
20 LAM(I)=DOTP(DK(1, I), DK(1, I))
SUM=0.
DO 22 I=1, M
DO 24 J=1, M
IF(I.EQ.J)GO TO 24
PI(I)=PI(I)*LAM(J)
24 CONTINUE
22 SUM=SUM+PI(I)
GO TO 25
29 KSTAR=K(I)
LSTAR=1
LAM(I)=1.
SUM=1.
GO TO 33
25 KSTAR=K(I)
LSTAR=1
A=PI(I)
DO 30 I=1, M
IF(PI(I).LE.A)GO TO 30
KSTAR=K(I)

```

```

C 13590
C 13600
C 13610
C 13620
C 13630
C 13640
C 13650
C 13660
C 13670
C 13680
C 13690
C 13700
C 13710
C 13720
C 13730
C 13740
C 13750
C 13760
C 13770
C 13780
C 13790
C 13800
C 13810
C 13820
C 13830

```

```

C 13850
C 13860
C 13870
C 13880
C 13890
C 13900
C 13910
C 13920
C 13930
C 13940
C 13950
C 13960
C 13970
C 13980
C 13990
C 14000
C 14010
C 14020
C 14030
C 14040
C 14050
C 14060

```

```

136300000
136400000
136500000
136600000
136700000
136800000
136900000
137000000
137100000
137200000
137300000
137400000
137500000
137600000
137700000
137800000
137900000
138000000
138100000
138200000
138300000
138400000
138500000
138600000
138700000
138800000
138900000
139000000
139100000
139200000
139300000
139400000
139500000
139600000
139700000
139800000
140000000
140100000
140200000
140300000
140400000
140500000
140600000
140700000
140800000
140900000
141000000
141100000

```

```

LSTAR=I
A=PI(I)
30 CONTINUE
33 DO 35 I=1,3
W(I)=UJ(I)
35 WD(I)=UJD(I)
DO 40 I=1,M
KI=K(I)
LAM(I)=PI (I)/SUM
CALL GAMMA(TH(I,KI ),G1)
CALL GAMMA(THD(I,KI ),G2)
CALL MULT(G1,DK(I,1),HOLD,1)
CALL ADD(Q(I,KI ),HOLD,HOLD,1)
CALL SCALR(LAM(I),HOLD,HOLD,1)
CALL ADD(W,HOLD,W,1)
CALL MULT(G1,UJD,HOLD,1)
CALL MULT(G2,DK(I,1),SAVE,1)
CALL ADD(HOLD,SAVE,SAVE,1)
CALL ADD(QD(I,KI ),SAVE,SAVE,1)
CALL SCALR(LAM(I),SAVE,SAVE,1)
40 CALL ADD(WD,SAVE,WD,1)
ADD TO ZMX AND TDT
CALL ADD(R,W,HOLD,1)
CALL SCALR(U(L),HOLD,HOLD,1)
CALL ADD(ZMX,HOLD,ZMX,1)
COMPUTE ALPHA,ALPHA3
CALL SCALR(U(L),XIDEN ,LAMI,3)
CALL ADD(R,W,HOLD,1)
CALL GAMMA(HOLD,G3)
SC=-U(L)
CALL SCALR(SC,G3,LAM2,3)
COMPUTE BETA1
CALL GAMMA(WX,G1)
CALL ADD(PDOT,WD,H1 ,1)
CALL MULT(G1,H1 ,SAVE,1)
CALL SCALR(2.,SAVE,SAVE,1)
CALL MULT(G1,G1,G2,3)
C
CALL SCALR(SC,G3,LAM2,3)
COMPUTE BETA1
CALL GAMMA(WX,G1)
CALL ADD(PDOT,WD,H1 ,1)
CALL MULT(G1,H1 ,SAVE,1)
CALL SCALR(2.,SAVE,SAVE,1)
CALL MULT(G1,G1,G2,3)
C
C
C *L,T*
CALL MULT(G1,HOLD,H2,1)
CALL ADD(H1,H2,H1,1)
SUMT=SUMT+.5*U(L)*DOTP(H1,H1)
CALL MULT(G3,H1,H2,1)
CALL MTRAN(PIGAM,H2,H1,1)
CALL SCALR(U(L),H1,H1,1)
CALL ADD(SUML,H1,SUML,1)
C *L,T*
C
CALL MULT(G2,HOLD,XC,1)
CALL ADD(XC,SAVE,XC,1)
CALL ADD(XC,UJDD,XC,1)

```

```

C 14070 141200000
C 14080 141300000
C 14090 141400000
C 14100 141500000
C 14110 141600000
C 14120 141700000
C 14130 141800000
C 14140 141900000
C 14150 142000000
C 14160 142100000
C 14170 142200000
C 14180 142300000
C 14190 142400000
C 14200 142500000
C 14210 142600000
C 14220 142700000
C 14230 142800000
C 14240 142900000
C 14250 143000000
C 14260 143100000
C 14270 143200000
C 14280 143300000
C 14290 143400000
C 14300 143500000
C 14310 143600000
C 14320 143700000
C 14330 143800000
C 14340 143900000
C 14350 144000000
C 14360 144100000
C 14370 144200000
C 14380 144300000
C 14390 144400000
C 14400 144500000
C 14410 144600000
C 14420 144700000
C 14430 144800000
C 14440 144900000
C 14450 145000000
C 14460 145100000
C 14470 145200000
C 14480 145300000
C 14490 145400000
C 14500 145500000
C 14510 145600000
C 14520 145700000
C 14530 145800000
C 14540 145900000
C 14550 146000000
C 14560 146100000
C 14570 146200000

```

```

DO 50 I=1,M
  KI=K(I)
  CALL GAMMA(TH(1,KI),G1)
  CALL GAMMA(THD(1,KI),G2)
  CALL MULT(G2,UJD,HOLD,1)
  CALL SCALR(2.,HOLD),HOLD,1)
  CALL MULT(G1,UJDD,SAVE,1)
  CALL ADD(HOLD,SAVE,SAVE,1)
  CALL SCALR(LAM(I),SAVE,SAVE,1)
  50 CALL ADD(XC,SAVE,XC,1)
  CALL SCALR(U(I),XC,XC,1)
  COMPUTE ALPHA4
  SC=-U(I)
  CALL GAMMA(DK(I),LSTAR),G1)
  CALL SCALR(SC,G1,LAM3,3)
  COMPUTE ALPHA-KSTAR
  DO 78 I=1,3
    78 DK(I,1)=W(I)-RIQ(I,KSTAR)-Q(I,KSTAR)
    CALL GAMMA(DK,G1)
    CALL GAMMA(TH(I,KSTAR),G2)
    CALL MULT(G2,G1,G3,3)
    CALL SUBTR(G1,G3,G4,3)
  COMPUTE ALPHA5,ALPHA7,ALPHA8, XC
  CALL MULT(G4,LAM1,LAM4,3)
  CALL MULT(G4,LAM2,LAM5,3)
  CALL MULT(G4,LAM3,LAM6,3)
  CALL MULT(G4,XC,XC(4),1)
  C
  C INSFT RHS PARTITION
  C
  C CALL SUBTR(RHSI(1,KSTAR),XC,RHSI(1,KSTAR),2)
  C
  C INSERT LHS PARTITIONS
  C
  C
  DO 60 I=1,3
    DO 60 J=1,3
      BIGA(I,J)=LAM1(I,J)
      BIGA(I+3,J)=LAM4(I,J)
      BIGA(I,J+3)=LAM2(I,J)
      BIGA(I+3,J+3)=LAM5(I,J)
      BIGD(I,J)=LAM1(I,J)
      BIGD(I+3,J)=LAM4(I,J)
      BIGD(I,J+3)=LAM3(I,J)
      BIGD(I+3,J+3)=LAM5(I,J)
  60 CALL XADD(BIGA,FMA(1,1,KSTAR),EMA(1,1,KSTAR),6,6,6,6)
  CALL XADD(BIGD,EMD(1,1,KSTAR),EMD(1,1,KSTAR),6,6,6,6)
  RETURN
  END

```

C	14570	146300000
		146400000
		146500000
		146600000
C	14600	146700000
C	14610	146800000
C	14620	146900000
C	14630	147000000
C	14640	147100000
C	14650	147200000
C	14660	147300000
C	14670	147400000
C	14680	147500000
C	14690	147600000
C	14700	147700000
C	14710	147800000
C	14720	147900000
C	14730	148000000
C	14740	148100000
C	14750	148200000
C	14760	148300000
C	14770	148400000
C	14780	148500000
C	14790	148600000
C	14800	148700000
C	14810	148800000
C	14820	148900000
C	14830	149000000
C	14840	149100000
C	14850	149200000
C	14860	149300000
C	14870	149400000
C	14880	149500000
C	14890	149600000
C	14900	149700000
C	14910	149800000
C	14920	149900000
C	14930	150000000
C	14940	150100000
C	14950	150200000
C	14960	150300000
C	14970	150400000
C	14980	150500000
C	14990	150600000
C	15000	150700000
LUM00010		150800000
LUM00020		150900000
LUM00030		151000000


```

SURROUTINE ZLAB(NLAB,NCW)
COMMON T,R(3),W(1,1),DR(12000),H1(3)
COMMON /CWT/RB(3),RBD(6),WY(3),RAO(3,100),QB(3,100),QBD(300),
      THB(3,100),THBU(300),XMBAR(100)
*
COMMON /INDUT/IN,INUT,IOFF
COMMON /BIG/PIETA(3,3),PIGAM(3,3),VI(22),QP(3,6,100),
      EMA(6,6,100),EMD(6,6,100),NMLAB,
*
      RMODE(600,20),NMCW,SMODE(600,20),Z1(6,6),
*
      Z3(20,6),Z4(20,20),WORK(3,6),WORKR(6,1)
COMMON /LOADS/GAML(3,3),GAMS(3,3),PIMIX(3,3),FETEST(6),
      PHSI(6,100),DELAR(26)
*
      DELCW(26),XDD(1212),KLUCS,KLULAB,KLUCW,CSLDA(6)
COMMON /NEWCOM/FL(3),XX(95),PIBETA(3,3),IFDEPL,
      KLUE,CMK(80),IFCGN,IFSUPP
*
COMMON /LABOR/WX(303),Q(3,100)
COMMON /CONNECT/IPT,S(3),IAPT,SS(9),PHIST(3),WP(21),PZB(3),ELL(3)
COMMON /EXTRA/ZFX(3),ZLX(3),ZMX(3),ZCY(3),ZCM(3),EMC,TOT
CALL GAMMA(ELL,GAML)
CALL PIF(PHIST,GAMS)
CALL MTRAN(PIBETA,GAMS,PIMIX,3)
CALL GAMMA(S,GAMS)
DO 7 I=1,3
7 PIMIX(1,I)=-PIMIX(1,I)
C
C COMPUTE ZCY,ZCM,PZB
C
CALL MULT(PIETA,R,ZCY,1)
CALL ADD(ZCY,RB,ZCY,1)
CALL SCALR(EMC,ZCY,ZCY,1)
DO 6 I=1,NCW
DO 6 J=1,3
6 ZCY(J)=ZCY(J)+XMBAR(I)*(RAO(J,I)+QB(J,I))
CALL MTRAN(PIETA,ZCY,WORK,1)
DO 8 I=1,3
8 WORK(I,1)=(WORK(I,1)+ZFX(I,1)+ZLX(I,1)+ZMX(I,1))/TOT
CALL MTRAN(PIGAM,WORK,ZCM,1)
CALL MULT(PIGAM,ZCM,ZFX,1)
SC=1./EMC
CALL SCALR(SC,ZCY,ZCY,1)
CALL MULT(PIETA,ZFX,H1,1)
CALL SUBTR(ZCY,H1,H1,1)
CALL GAMMA(WY,WORK)
CALL MULT(WORK,H1,ZFX,1)
CALL MULT(WORK,ZFX,H1,1)
CALL GAMMA(THB(I,IAPT),WORK)
CALL MULT(WORK,H1,ZFX,1)
CALL SUBTR(H1,ZFX,ZFX,1)
CALL MULT(PIBETA,ZFX,H1,1)
CALL SCALR(EMC,H1,PZB,1)

```

```

LUM00040 151100000
LUM00050 151200000
LUM00060 151300000
LUM00070 151400000
LUM00080 151500000
LUM00090 151600000
LUM00100 151700000
LUM00110 151800000
LUM00120 151900000
LUM00130 152000000
LUM00140 152100000
LUM00150 152200000
LUM00160 152300000
LUM00170 152400000
LUM00180 152500000
LUM00190 152600000
LUM00200 152700000
LUM00210 152800000
LUM00220 152900000
LUM00230 153000000
LUM00240 153100000
LUM00250 153200000
LUM00260 153300000
LUM00270 153400000
LUM00280 153500000
LUM00290 153600000
LUM00300 153700000
LUM00310 153800000
LUM00320 153900000
LUM00330 154000000
LUM00340 154100000
LUM00350 154200000
LUM00360 154300000
LUM00370 154400000
LUM00380 154500000
LUM00390 154600000
LUM00400 154700000
LUM00410 154800000
LUM00420 154900000
LUM00430 155000000
LUM00440 155100000
LUM00450 155200000
LUM00460 155300000
LUM00470 155400000
LUM00480 155500000
LUM00490 155600000
LUM00500 155700000
LUM00510 155800000
LUM00520 155900000

```

```

C   SET UP RHS VECTOR TO MULTIPLIED BY (PHI-TRAN)*Q
C
C
      IL=0
      IF(KLUE.EQ.2 .OR. KLUE.GT.3)IL=1
      IF(KLUE.NE.4)GO TO 14
      CALL ZEROS(FETEST,2)
      GO TO 15
14  CONTINUE
      CALL CCNSTR(FETEST)
15  CONTINUE
      CALL MULT(PIMIX,FETEST,WORK8,2)
      IF(KLUCS.GT.0)CALL MULT(QP(1,4,1PT),WORK8,CSLDA,2)
      CALL CTRL(DR,NLAB,IFCON,1)
      CALL SUPPLM(DR(601),NLAB,IFSUPP,1)
      CALL XADD(DR,DK(601),DR,6,NLAB,6,6)
      CALL MULT(GAMS,WORK8,HI ,1)
      CALL ADD(WORK8(4,1),HI ,WORK8(4,1),1)
      ISIX=IPT*6-5
      CALL ADD(DR(ISIX),WORK8,DR(ISIX),2)
      DO 5 I=1,NLAB
      ISIX=I*6-5
      CALL MULT(QP(1,4,I),DR(ISIX),HI,1)
      CALL ADD(RHSI(1,I),HI ,RHSI(1,I),1)
5    CALL ADD(RHSI(4,I),DR(ISIX+3),RHSI(4,I),1)
      IF(KLULAB.GT.0)CALL LABLD
      IF(IL.EQ.1)GO TO 80
C   FORM D*K
C
      DO 10 I=1,NLAB
      ISIX=6*I-5
10   CALL XMPRD(EMD(1,1,I),RMODE(ISIX,1),DR(ISIX ,6,6,NMLAB,6,600,
      *600)
C   FORM (R-T)*D*K IN Z4
C
      NLAB6=NLAB*6
      CALL TPRD(RMODE,DR,Z4,NLAB6,NMLAR,NMLAB,600,20)
C   ZERO OUT Z1
C
      DO 80 I=1,6
      DELAB(I)=0.
      DO 30 J=1,6
      Z1(I,J)=0.
30   Z1(I,J)=0.
C   FORM
C
      F*A IN Z1 AND F * RHSI IN DELAB
C
      DO 50 I=1,NLAB
      ISIX=6*I-5

```

```

LUM00530 156000000
LUM00540 156100000
LUM00550 156200000
LUM00560 156300000
LUM00570 156400000
LUM00580 156500000
LUM00600 156600000
LUM00610 156700000
LUM00620 156800000
LUM00630 156900000
LUM00640 157000000
LUM00650 157100000
LUM00660 157200000
LUM00670 157300000
LUM00680 157400000
LUM00690 157500000
LUM00700 157600000
LUM00710 157700000
LUM00720 157800000
LUM00730 157900000
LUM00740 158000000
LUM00750 158100000
LUM00760 158200000
LUM00770 158300000
LUM00780 158400000
LUM00790 158500000
LUM00800 158600000
LUM00810 158700000
LUM00820 158800000
LUM00830 158900000
LUM00840 159000000
LUM00850 159100000
LUM00860 159200000
LUM00870 159300000
LUM00880 159400000
LUM00890 159500000
LUM00900 159600000
LUM00910 159700000
LUM00920 159800000
LUM00930 159900000
LUM00940 160000000
LUM00950 160100000
LUM00960 160200000
LUM00970 160300000
LUM00980 160400000
LUM00990 160500000
LUM01000 160600000
LUM01010 160700000
LUM01020 160800000
LUM01030 160900000
LUM01030 161000000

```

```

CALL ADD(RHSI(1,1), DELAB, DELAB, 1)
CALL XADD(EMA(1,1,1), Z1, Z1, 3, 6, 6, 6)
CALL MPRD(QP(1,1,1), RHSI(1,1), WORK, 3, 6, 1, 3, 1)
CALL ADD(DELAB(4), WORK, DELAB(4), 1)
CALL MPRD(QP(1,1,1), EMA(1,1,1), WORK, 3, 6, 6, 3, 6)
50 CALL XADD(WORK, Z1(4,1), Z1(4,1), 3, 6, 3, 6)
IF(IL.EQ.1) GO TO 99

C
C PLACE A IN DR
C
DO 60 I=1, NLAB
  ISIX=6*I-5
  DO 60 L=1, 6
    K=ISIX+L-1
    DO 60 J=1, 6
      JA=(J-1)*600+K
      60 DR(JA)=EMAIL(J,I)

C
C FORM (R-T)  *A IN Z3 AND R-T  *RHSI IN DELAB
C
CALL TPRD(RMODE, DR, Z3, NLAB6, NMLAB, 6, 600, 20)
CALL TPRD(RMODE, RHSI, DELAB(7), NLAB6, NMLAB, 1, 600, 1)
99 RETURN
END
LUM01040 161100000
LUM01050 161200000
LUM01060 161300000
LUM01070 161400000
LUM01080 161500000
LUM01090 161600000
LUM01100 161700000
LUM01110 161800000
LUM01120 161900000
LUM01130 162000000
LUM01140 162100000
LUM01150 162200000
LUM01160 162300000
LUM01170 162400000
LUM01180 162500000
LUM01190 162600000
LUM01200 162700000
LUM01210 162800000
LUM01220 162900000
LUM01230 163000000
LUM01240 163100000
LUM01250 163200000
LUM01260 163300000
LUM01270 163400000

```

```

SUBROUTINE CONSTR(FETEST)
COMMON T
COMMON /NEWCOM/EL(3)
COMMON /CONFACT/XX(8),DEL(3),PHIST(3),PHISTD(3),W(20),P
COMMON /INOUT/IN,OUT,IOFF
DIMENSION FETEST(6)
IF(T.GT.0)GO TO 10
READ(IN,1)CMC,CML,CJC,CIL,CIC,CIL,A,B,AE,EI,GJ,YMIN,GA,GB,GT
WRITE(OUT,770)CMC,CML,CJC,CIL,CIC,CIL,CJC,CJL
770 FORMAT(0BEAM SUBROUTINE INPUT#76X,*CWT MASS*,9X,*LAB MASS*,6X,
* CWT TRANS INRTA LAB TRANS INRTA CWT ROLL INRTA LAB ROLL INRLUM01380
*TA#76F17.7)
WRITE(OUT,771)A,B,AE,EI,GJ
771 FORMAT(9X,*A*,16X,*B*,16X,*AE*,15X,*EI*,15X,*GJ*/5E17.7)
WRITE(OUT,772)GA,GB,GT
772 FORMAT(* AXIAL DAMPING RATIO BENDING DAMPING RATIO TORSION DALUM01430
*MPING RATIO*/4X,E14.7,2E24.7)
1
FORMAT(3E15.8)
CMB=CMC*CML/(CMC+CML)
CJR=CJC*CJL/(CJC+CJL)
10 Y=SQRT(DO0TP(EL,EL))
Z=AMAX1(Y,YMIN)
CKA=AE/Z
CK3=4.*EI/Z
CKT=GJ/Z
CK2= 1.5*CK3/Z
CK1=2.*CK2/Z
CK2=-CK2
TEMP=(A+B*Y)
CIB=CIC+CIL+CMB*TEMP*TEMP
CM1=CMB*(CIC+CIL)/CIB
CM2=CMB*(CIC*A-CIL*(B+Y))/CIB
CM3=(CMB*(CIL*(B+Y)+(B+Y)*CIC*A)+CIC*CIL)/CIB
AA=CM1*CM3-CM2*CM2
BB=2.*CK2*CM2-CK1*CM3-CK3*CM1
CC=CK1*CK3-CK2*CK2
TEMP=SQRT(BB*BB-4.*AA*CC)
WLW1=(-BB-TEMP)/(2.*AA)
W2W2=(-BB+TEMP)/(2.*AA)
IF(CK1-WLW1*CM1)20,30,20
30 DELB1=1.
PHIB1=0.
GO TO 14
20 IF(CK2-WLW1*CM2)40,50,40
50 DELB1=0.
PHIB1=1.
GO TO 14
40 RI=(CK1-WLW1*CM1)/(WLW1*CM2-CK2)
IF(ABS(RI).GT.1.160 TO 11
LUM01280 163500000
LUM01290 163600000
LUM01300 163700000
LUM01310 163800000
LUM01320 163900000
LUM01330 164000000
LUM01340 164100000
LUM01350 164200000
LUM01360 164300000
LUM01370 164400000
LUM01380 164500000
LUM01390 164600000
LUM01400 164700000
LUM01410 164800000
LUM01420 164900000
LUM01430 165000000
LUM01440 165100000
LUM01450 165200000
LUM01460 165300000
LUM01470 165400000
LUM01480 165500000
LUM01490 165600000
LUM01500 165700000
LUM01510 165800000
LUM01520 165900000
LUM01530 166000000
LUM01540 166100000
LUM01550 166200000
LUM01560 166300000
LUM01570 166400000
LUM01580 166500000
LUM01590 166600000
LUM01600 166700000
LUM01610 166800000
LUM01620 166900000
LUM01630 167000000
LUM01640 167100000
LUM01650 167200000
LUM01660 167300000
LUM01670 167400000
LUM01680 167500000
LUM01690 167600000
LUM01700 167700000
LUM01710 167800000
LUM01720 167900000
LUM01730 168000000
LUM01740 168100000
LUM01750 168200000
LUM01760 168300000

```

```

DELBI=1.
PHIR1=R1
GO TO 14
11 PHIR1=1.
DELBI=1./R1
14 TEMP=CK1-W2W2*CM1
   TEMP=CK2-W2W2*CM2
   IF(TEMP)60,70,50
70 DELB2=1.
   PHIR2=0.
   GO TO 18
60 IF(TEMPA)60,90,80
90 DELB2=0.
   PHIR2=1.
   GO TO 18
80 R2=-TEMP/TEMPA
   IF(ABS(R2).GT.1.)GO TO 100
   DELR2=1.
   PHIR2=R2
   GO TO 18
100 PHIR2=1.
   DELB2=1./R2
18 T1=DELBI*CM1+PHIB1*CM2
   T2=DELBI*CM2+PHIB1*CM3
   T3=DELBI*CM1+PHIB2*CM2
   T4=DELBI*CM2+PHIB2*CM3
   CM11=T1*DELBI+T2*PHIR1
   CM22=T3*DELBI+T4*PHIR2
   T1=DELBI*CK1+PHIB1*CK2
   T2=DELBI*CK2+PHIB1*CK3
   T3=DELBI*CK1+PHIB2*CK2
   T4=DELBI*CK2+PHIB2*CK3
   CK11=T1*DELBI+T2*PHIR1
   CK22=T3*DELBI+T4*PHIR2
   T1=2.*GB *SQRT(CK11*CM11)
   T2=2.*GB *SQRT(CK22*CM22)
   TEMP=DELBI*PHIB2-DELB2*PHIR1
   TEMP=1./TEMP*TEMP
   C1=TEMP*( PHIB2*T1*PHIR2+PHIB1*T2*PHIR1)
   C2=TEMP*(-PHIB2*T1*DELB2-PHIB1*T2*DELB1)
   C3=TEMP*( DELB2*T1*DELB2+DELB1*T2*DELB1)
   CA=2.*GA *SQRT(CMB*CKA1)
   CT=2.*GT *SQRT(CJB*CKT)
   P=P/10.
   FETEST(1)=(CK1+P*12./Z)*DEL(1)+(CK2-P)*PHIST(2)
   +C1*DELD(1)+C2*PHISTD(2)
*
   FETEST(2)=(CK1+P*12./Z)*DEL(2)-(CK2-P)*PHIST(1)
   +C1*DELD(2)-C2*PHISTD(1)
*
   FETEST(3)=CKA*DEL(3)+CA*DELD(3)
   FETEST(4)=(P-CK2)*DEL(2)+(CK3+1.333333*P*Z)*PHIST(1)
   -C2*DELD(2)+C3*PHISTD(1)
*
LUM01770 168400000
LUM01780 168500000
LUM01790 168600000
LUM01800 168700000
LUM01810 168800000
LUM01820 168900000
LUM01830 169000000
LUM01840 169100000
LUM01850 169200000
LUM01860 169300000
LUM01870 169400000
LUM01880 169500000
LUM01890 169600000
LUM01900 169700000
LUM01910 169800000
LUM01920 169900000
LUM01930 170000000
LUM01940 170100000
LUM01950 170200000
LUM01960 170300000
LUM01970 170400000
LUM01980 170500000
LUM01990 170600000
LUM02000 170700000
LUM02010 170800000
LUM02020 170900000
LUM02030 171000000
LUM02040 171100000
LUM02050 171200000
LUM02060 171300000
LUM02070 171400000
LUM02080 171500000
LUM02090 171600000
LUM02100 171700000
LUM02110 171800000
LUM02120 171900000
LUM02130 172000000
LUM02140 172100000
LUM02150 172200000
LUM02160 172300000
LUM02170 172400000
LUM02180 172500000
LUM02190 172600000
LUM02200 172700000
LUM02210 172800000
LUM02220 172900000
LUM02230 173000000
LUM02240 173100000
LUM02250 173200000
LUM02260 173300000
LUM02270 173400000

```

```
FETEST(5)=(CK2-P)*DEL(1)+(CK3+1.333333*P*Z)*PHIST(2)
*
+C2*DEL(1)+C3*PHISTD(2)
FETEST(6)=CKT*PHIST(3)+CT*PHISTD(3)
RETURN
END

LUM02280 173500000
LUM02290 173600000
LUM02300 173700000
LUM02310 173800000
LUM02320 173900000
```

```

SUBROUTINE CW(NCW)
COMMON/INOUT/IN, IOUT, IOFF
COMMON T, R, RDOT, XIDEN, RHO, A ,G1, G2, G3, G4, XC, LAM1, LAM2, LAM3, LAM4
* , H1, H2, H3, H4, H5, HOLD, SAVE
* , G5(3,3), G6(3,3), SX(11886), RA(3,3)
COMMON /BIG/PIETA(3,3), PIGAM(3,3), SUML(3), SUMT, SGAM(3,3), SETA(3,3), LUM02380
* , SASAB(3,3,100), RABAR(3,3,100), EMB(3,6,100), EMC(600,6), LUM02390
* , EME(3,6,100) LUM02400
COMMON /LABOR/WX(3) LUM02410
COMMON /CWT/RB, RBDOT, FTA, WY, RAO, QR, QDR, THB, THDB, XMBAR, XIBAR LUM02420
COMMON /LOADS/ZZ(3), RHSA(6,100) LUM02430
COMMON /NEWCOM/ZN(15), RORDD(3) LUM02440
DIMENSION XIBAR(3,3,100), XMBAR(100), QR(3,100), QDR(3,100), LUM02450
* THB(3,100), THDB(3,100), HOLD(3), SAVE(3), G1(3,3), G2(3,3), LUM02460
* G3(3,3), G4(3,3), XC(3), RB(3), RBDOT(3), ETA(3), WY(3), LUM02470
* RAO(3,100), R(3), RDGT(3), XIDEN(3,3) LUM02480
* , H1(3), H2(3), H3(3), H4(3), H5(3) LUM02490
REAL LAM1(3,3), LAM2(3,3), LAM3(3,3), LAM4(3,3) LUM02500
CALL GAMMA(R, G2) LUM02510
CALL GAMMA(WY, G4) LUM02520
CALL GAMMA(WX, G6) LUM02530
CQP LUM02540
DO 20 I=1,3 LUM02550
DO 20 J=1,3 LUM02560
RA(I, J) = 0. LUM02570
DO 20 K=1,3 LUM02580
20 RA(I, J) = RA(I, J) + G2(I, K) * PIETA(J, K) LUM02590
DO 100 L=1, NCW LUM02600
COMPUTE LAM17, LAM18, LAM19, LAM20 LUM02610
CALL SCALR(XMBAR(L), PIETA, LAM1, 3) LUM02620
CALL MULT(LAM1, G2, LAM2, 3) LUM02630
CALL SCALR(-1., LAM2, LAM2, 3) LUM02640
CALL SCALR(XMBAR(L), XIDEN, LAM3, 3) LUM02650
CALL ADD(RR, RAO(1, L), HOLD, 1) LUM02660
CALL ADD(HOLD, QB(1, L), H2, 1) LUM02670
CALL GAMMA(H2, G3) LUM02680
CQP LUM02690
CALL SCALR(L., G3, RABAR(1, L), 3) LUM02700
SC=XMBAR(L) LUM02710
CALL SCALR(SC, G3, LAM4, 3) LUM02720
COMPUTE XC7 LUM02730
CALL ADD(RBDOT, QDB(1, L), H4, 1) LUM02740
CALL MULT(G4, H4, XC, 1) LUM02750
CALL SCALR(2., XC, XC, 1) LUM02760
CALL MULT(G4, G4, G3, 3) LUM02770
CALL MULT(G3, H2, SAVE, 1) LUM02780
C***** L, T ***** LUM02790
CALL MULT(G4, H2, H3, 1) LUM02800
CALL ADD(H4, H3, H3, 1) LUM02810

```

```

C*****
CALL ADD(XC,SAVE,XC,1)
CALL MULT(G6,ROOT,HOLD,1)
CALL SCALR(2,,HOLD,HOLD,1)
CALL MULT(G6,G6,G3,3)
CALL MULT(G3,R,SAVE,1)
C***** L,T *****
CALL MULT(G6,R,H4,1)
CALL ADD(ROOT,H4,H4,1)
CALL MULT(PIETA,H4,H5,1)
CALL ADD(H5,H3,H3,1)
CALL MULT(PIETA,R,H4,1)
CALL ADD(H2,H4,H2,1)
CALL GAMMA(H2,G3)
CALL MULT(G3,H3,H4,1)
CALL SCALR(XMBAR(L),H4,H4,1)
C*****
CALL ADD(HOLD,SAVE,SAVE,1)
CALL MULT(PIETA,SAVE,HOLD,1)
CALL ADD(HOLD,XC,XC,1)
CALL SCALR(XMBAR(L),XC,XC,1)
CALL SCALR(-1,,XC,RHSA(L,L),1)
CALL MULT(LAM3,ROBDD,HOLD,1)
CALL SUBTR(RHSA(L,L),HOLD,RHSA(L,L),1)
C* FORM B,C,E PARTITIONS
DO 40 I=1,3
  IL=6*(L-1)+1
  DO 40 J=1,3
    EMB(I,J,L)=LAM1(I,J)
    EMC(I,J,3,L)=LAM2(I,J)
    EMC(IL,J)=LAM3(I,J)
    EMC(IL,J+3)=LAM4(I,J)
    40 EME(I,J,L)=LAM3(I,J)
  COMPUTE LAM21,LAM22
  CALL GAMMA(THB(I,L),G1)
  CALL ADD(XIDEN,G1,G3,3)
  CALL SUBTR(XIDEN,G1,G1,3)
CQP
DO 60 I=1,3
  DO 60 J=1,3
    60 SASAB(I,J,L)=G3(I,J)
  CALL MULT(XIBAR(I,L),G1,LAM1,3)
  CALL GAMMA(THDR(I,L),G5)
  CALL MULT(G5,WY,HOLD,1)
  CALL MULT(XIBAR(I,L),HOLD,SAVE,1)
  CALL MULT(G1,WY,HOLD,1)
  CALL ADD(HOLD,THDR(I,L),HOLD,1)
  CALL MULT(XIBAR(I,L),HOLD,H1,1)
C***** L,T *****
SUMT=SUMT+.5*(DOTP(HOLD,H1)+XMBAR(L)*DOTP(H3,H3))
C*****

```

```

LUM02820 178900000
LUM02830 179000000
LUM02840 179100000
LUM02850 179200000
LUM02860 179300000
LUM02870 179400000
LUM02880 179500000
LUM02890 179600000
LUM02900 179700000
LUM02910 179800000
LUM02920 179900000
LUM02930 180000000
LUM02940 180100000
LUM02950 180200000
LUM02960 180300000
LUM02970 180400000
LUM02980 180500000
LUM02990 180600000
LUM03000 180700000
LUM03010 180800000
LUM03020 180900000
LUM03030 181000000
LUM03040 181100000
LUM03050 181200000
LUM03060 181300000
LUM03070 181400000
LUM03080 181500000
LUM03090 181600000
LUM03100 181700000
LUM03110 181800000
LUM03120 181900000
LUM03130 182000000
LUM03140 182100000
LUM03150 182200000
LUM03160 182300000
LUM03170 182400000
LUM03180 182500000
LUM03190 182600000
LUM03200 182700000
LUM03210 182800000
LUM03220 182900000
LUM03230 183000000
LUM03240 183100000
LUM03250 183200000
LUM03260 183300000
LUM03270 183400000
LUM03280 183500000
LUM03290 183600000
LUM03300 183700000
LUM03310 183800000
LUM03320 183900000

```



```

LUM03330 184000000
LUM03340 184100000
LUM03350 184200000
LUM03360 184300000
LUM03370 184400000
LUM03380 184500000
LUM03390 184600000
LUM03400 184700000
LUM03410 184800000
LUM03420 184900000
LUM03430 185000000
LUM03440 185100000
LUM03450 185200000
LUM03460 185300000
LUM03470 185400000
LUM03480 185500000
LUM03490 185600000
LUM03500 185700000
LUM03510 185800000
LUM03520 185900000
LUM03530 186000000

```

```

CALL GAMMA(HOLD,G1)
CALL MULT(G1,H1,HOLD,1)
C***** L,T *****
CALL MULT(G3,H1,H2,1)
CALL ADD(H2,H4,H2,1)
CALL MTRAN(P,ETA,H2,H3,1)
CALL MTRAN(P,GAM,H3,H2,1)
CALL ADD(SUML,H2,SUML,1)
C*****
CALL SUBTR(HOLD,SAVE,XC,1)
CALL SCALE(-1,XC,RHSA(4,1),1)
C* FORM B,C,E PARTITIONS
DO 50 I=1,3
  IL=6*I+I-3
  DO 50 J=1,3
    EMC(IL,J)=0.
    EMC(IL,J+3)=LAMI(I,J)
  50 EMC(I,J+3,L)=XIBAR(I,J,L)
100 CONTINUE
RETURN
END

```

```

SUBROUTINE ZCW(NCW)
COMMON /CWT/RAO(312),OR(3,100)
COMMON /BIG/PIETA(3,3),PIGAM(3,3),S(4),SGAM(3,3),SETA(3,3),
      SASAB(3,3,100),RABAR(3,3,100),EMB(3,6,100),EMC(600,6),
      EME(3,6,100),NMLAB,RMODE(600,20),NMCK,
      SMODE(600,20),Z1(6,6),Z(520)
      ,Z7(6,6)
      ,Z9(20,6),Z10(20,6),Z11(20,20),
      WORK(3,6),WORKA(3,3),WORKB(20,6),WORKC(3,3)
COMMON /LOADS/GAML(3,3),GAMSB(3,3),PIMIX(3,3),FETEST(6),
      RHSA(6,100),DELAB(26),DELCW(26)
      , XDD(1212),KLUCS,KLULAR,KLUCW,CSLDA(6),CSLDR(6)
COMMON /NEWCOM/EL(98),PIBETA(10),KLUE,CMK(80),IFCON,IFSUPP
COMMON /CONNECT/IPT,SZ(3),IAPT,SB(3)
COMMON W(18),ES(600,20),RA(3,3)
CALL GAMMA(SB,GAMSB)

C SET UP RHS VECTOR TO BE MULTIPLIED BY (PHI-TRAN)*Q
C ZERO OUT Z6,Z7,Z9
C
CALL MULT(GAML,FETEST,WORKC,1)
CALL ADD(FETEST(4),WORKC,FETEST(4),1)
CALL MTRAN(PIBETA,FETEST,WORKC,2)
IF(KLUCS.GT.0)CALL MULT(SASAB(1,1),IAPT),WORKC,C.SLDB,2)
CALL CONTRL(ES,NCW,IFCON,-1)
CALL SUPPLM(ES(1,2),NCW,IFSUPP,-1)
CALL XADD(ES,ES(1,2),ES,6,NCW,6,6)
CALL MULT(GAMSB,WORKC,GAML,1)
CALL ADD(WORKC(1,2),GAML,WORKC(1,2),1)
ISIX=IAPT*6-5
CALL ADD(ES(ISIX,1),WORKC,ES(ISIX,1),2)
DO 20 I=1,NCW
  ISIX=6*I-5
  CALL MULT(SASAB(1,1),I),ES(ISIX,1),GAML,1)
  CALL ADD(RHSA(1,I),GAML,RHSA(1,I),1)
  CALL ADD(RHSA(4,I),ES(ISIX+3,1),RHSA(4,I),1)
  IF(KLUCW.GT.0)CALL CWLD
20 CALL ADD(ES(ISIX,1),WORKC,ES(ISIX,1),2)
NCW6=NCW*6
C
C FORM ES
C
IF(KLUE.GT.2)GO TO R0
DO 10 I=1,NCW
  ISIX=6*I-5
  CALL XMPRD(EME(1,1,I),SMODE(ISIX,1),ES(ISIX,1),3,3,NMCW,3,600,600)
  CALL XMPRD(EME(1,4,I),SMODE(ISIX+3,1),ES(ISIX+3,1),3,3,NMCH,
    *3,600,600)
10 CALL XMPRD(EME(1,4,I),SMODE(ISIX+3,1),ES(ISIX+3,1),3,3,NMCH,
    *3,600,600)

```

```

LUM03540 186100000
LUM03550 186200000
LUM03560 186300000
LUM03570 186400000
LUM03580 186500000
LUM03590 186600000
LUM03600 186700000
LUM03610 186800000
LUM03620 186900000
LUM03630 187000000
LUM03640 187100000
LUM03650 187200000
LUM03660 187300000
LUM03670 187400000
LUM03680 187500000
LUM03690 187600000
LUM03700 187700000
LUM03710 187800000
LUM03720 187900000
LUM03730 188000000
LUM03740 188100000
LUM03750 188200000
LUM03760 188300000
LUM03770 188400000
LUM03780 188500000
LUM03790 188600000
LUM03800 188700000
LUM03810 188800000
LUM03820 188900000
LUM03830 189000000
LUM03840 189100000
LUM03850 189200000
LUM03860 189300000
LUM03870 189400000
LUM03880 189500000
LUM03890 189600000
LUM03900 189700000
LUM03910 189800000
LUM03920 189900000
LUM03930 190000000
LUM03940 190100000
LUM03950 190200000
LUM03960 190300000
LUM03970 190400000
LUM03980 190500000
LUM03990 190600000
LUM04000 190700000
LUM04010 190800000
LUM04020 190900000

```

```

C      80 DO 35 I=1,6
      DELCW(I)=0.
      DO 30 J=1,6
      Z6(I,J)=0.
      DO 30 Z7(I,J)=0.
      DO 35 J=1,NMCW
      Z9(J,I)=0.

C      DO 50 I=1,NCH
      ISIX=I#6-5

C      C      FORM HB,HC      AND H*RHSA
      CALL XADD(EMB(1,1,I),Z6,Z6,3,6,3,6)
      CALL XADD(EMC(ISIX,I),Z7,Z7,3,6,600,6)
      CALL ADD(RHSA(1,I),DELCW,DELCW,1)
      CALL MULT(RABAR(1,I),EMB(1,I),I),WORK,6)
      CALL XADD(WORK,Z6(4,I),Z6(4,I),3,6,3,6)
      CALL MULT(RABAR(1,I),I),RHSA(1,I),I),WORK,1)
      CALL ADD(WORK,DELCW(4),DELCW(4),1)
      CALL MPRD(RABAR(1,I),I),EMC(ISIX,I),WORK,3,3,6,3,600)
      CALL XADD(WORK,Z7(4,I),Z7(4,I),3,6,3,6)
      CALL MPRD(SASAB(1,I),I),EMC(ISIX+3,I),WORK,3,3,6,3,600)
      CALL XADD(WORK,Z7(4,I),Z7(4,I),3,6,3,6)
      CALL MULT(SASAB(1,I),I),RHSA(4,I),I),WORK,1)
      CALL ADD(WORK,DELCW(4),DELCW(4),1)
      IF(KLUE.GT.2)GO TO 81

C      C      FORM (S-TRANSPONSE)B
      CALL XTPRD(SMODE(ISIX,I),EMB(1,I),I),WORKB,3,NMCH,6,600,3,20)
      CALL XADD(WORKB,Z9,Z9,NMCW,6,20,20)

C      81 CONTINUE

C      C      FORM GB AND ADD TO Z1 AND G*RHSA AND ADD TO DELAB
      DO 90 CALL MTRAN(PIETA,EMB(1,I),I),WORK,6)
      DO 91 CALL XADD(WORK,Z1,Z1,3,6,3,6)
      CALL MULT(RA,EMB(1,I),I),WORK,6)
      DO 93 CALL XADD(WORK,Z1(4,I),Z1(4,I),3,6,3,6)
      CALL MTRAN(PIETA,RHSA(1,I),I),WORK,1)
      CALL ADD(WORK,DELAB,DELAB,1)
      CALL MULT(RA,RHSA(1,I),I),WORK,1)
      DO 50 CALL ADD(WORK,DELAB(4),DELAB(4),1)
      IF(KLUE.NE.4)GO TO 99
      DELAB(4)=DELAB(4)+DELCW(4)
      DELAB(5)=DELAB(5)-DELCW(5)
      DELAB(6)=DELAB(6)-DELCW(6)
      CALL XADD(Z1(4,I),Z6(4,I),Z1(4,I),1,6,6,6)

```

LUM04030 191000000

LUM04040 191100000

LUM04050 191200000

LUM04060 191300000

LUM04070 191400000

LUM04080 191500000

LUM04090 191600000

LUM04100 191700000

LUM04110 191800000

LUM04120 191900000

LUM04130 192000000

LUM04140 192100000

LUM04150 192200000

LUM04160 192300000

LUM04170 192400000

LUM04180 192500000

LUM04190 192600000

LUM04200 192700000

LUM04210 192800000

LUM04220 192900000

LUM04230 193000000

LUM04240 193100000

LUM04250 193200000

LUM04260 193300000

LUM04270 193400000

LUM04280 193500000

LUM04290 193600000

LUM04300 193700000

LUM04310 193800000

LUM04320 193900000

LUM04330 194000000

LUM04340 194100000

LUM04350 194200000

LUM04360 194300000

LUM04370 194400000

LUM04380 194500000

LUM04390 194600000

LUM04400 194700000

LUM04410 194800000

LUM04420 194900000

LUM04430 195000000

LUM04440 195100000

LUM04450 195200000

LUM04460 195300000

LUM04470 195400000

LUM04480 195500000

LUM04490 195600000

LUM04500 195700000

LUM04510 195800000

LUM04520 195900000

LUM04530 196000000

```

DO 65 I=5,6
DO 65 J=1,6
65 Z1(I,J)=Z1(I,J)-Z6(I,J)
DO 66 I=1,6
DO 66 J=1,1
IF(I.EQ.J)GO TO 66
SC=Z6(I,J)
Z6(I,J)=Z6(J,I)
Z6(J,I)=SC
66 CONTINUE
CALL SCALR(-1.,Z6(1,5),Z6(1,5),4)
DO 67 I=5,6
Z7(I,4)=-Z7(I,4)
67 Z7(4,I)=-Z7(4,I)
CALL XADD(Z6(4,4),Z7(4,4),Z6(4,4),3,3,6,6)
CALL ADD(Z1(1,4),Z6(1,4),Z1(1,4),6)
99 CONTINUE
IF(KLUE.GT.2)GO TO 100
C
C FORM (S-TRANSP)ES IN Z11 AND (S-T) *RHS IN DELCW
C
CALL TPRD(SMODE,ES,Z11,NCW6,NMCH,NMCH,600,20)
CALL TPRD(SMODF,RHSA,DELCW(7),NCW6,NMCH,1,600,1)
C
C FORM (S-TRANSP) *C IN Z10
C
CALL TPRD(SMODE,EMC,Z10,NCW6,NMCH,6,600,20)
100 CONTINUE
RETURN
END
LUM04540 196100000
LUM04550 196200000
LUM04560 196300000
LUM04570 196400000
LUM04580 196500000
LUM04590 196600000
LUM04600 196700000
LUM04610 196800000
LUM04620 196900000
LUM04630 197000000
LUM04640 197100000
LUM04650 197200000
LUM04660 197300000
LUM04670 197400000
LUM04680 197500000
LUM04690 197600000
LUM04700 197700000
LUM04710 197800000
LUM04720 197900000
LUM04730 198000000
LUM04740 198100000
LUM04750 198200000
LUM04760 198300000
LUM04770 198400000
LUM04780 198500000
LUM04790 198600000
LUM04800 198700000
LUM04810 198800000
LUM04820 198900000
LUM04830 199000000

```

```

SUBROUTINE MINCY(NLAB,NCW,DELT,NCYCLE,V,VDOOT)
DOUBLE PRECISION YPRED,YDERV,YNEW
COMMON T,R(3),RDOT(3),X(11),YICS(120),YDOT(120),B(600),C(600),
* PRED(120)
DIMENSION YPRED(120),YDERV(120),YNEW(120),YCORR(120),Z(720)
COMMON /LOADS/ZZ(633),DELAR(26),DELCH(26),XDDI(606)
COMMON /LABUR/WX(3),RTO(300),Q(3,100),QD(3,100),TH(3,100),
* THD(3,100)
COMMON /CWT/XC(9),WY(3),XCW(300),QR(3,100),QBD(3,100),THB(3,100),
* THRD(3,100)
COMMON/INOUT/ IN,IOUT,IOFF,IC,IPLOUT(14)
* ,N1,N2,N3,N4,N5,N6,N7
COMMON /PASS/QDUM(2),STEP
COMMON /CLUES/IFPLT,IFLUID,NPIPE,NMLM,MLM(8),IRES(2),IPIPES(30)
COMMON /NEWCOM/XNEW(18),VEC(20,2),VECBAR(20,2),XNEWC(10),KLUE,
* CMK(20,4),IFCON
COMMON /CONNECT/IPT,S(3),IAPT,SB(3),DEL(3),DELD(3),PHIST(3),
* PHISTD(3),DELRB(3),DELRBD(3),GAM(3),GAMD(3),ETAST(3),
* ETASTD(3),PZR(3),ELL(3),ELLD(3)
COMMON /BTG/XBIG(18),SUM(3),SUMT,XB(18),
* A(52,52),XBI(5296),NMLAR,RMODE(600,20),NMCW,
* SMODE(600,20),Z1(6,6),Z2(20,6),Z3(20,6),Z4(20,20),
* Z5(20,6),Z6(6,6),Z7(6,6),Z8(20,6),Z9(20,6),
* Z10(20,6),Z11(20,20)
COMMON /EXTRA/XEX(12),ZCM(3)
COMMON /ALLCNT/DUMAL(41),YICSCN(10),YPREDC(10),YDOTCN(10),NEQCN
* ,ADUM(12),TAJ(3),BDUM(6),BETDES
COMMON /VAROUT/F01,DO1C,F3,F9,F10,F16,F4,F11,F15,DO1,EL03D,ELD3,
* ELD03,9ICD,OD
* ,O1C,NCMG
* ,UJ0(3,3,8),XXCS,ERRDDX,UJ3,HIL(2),UJD23
* ,F1,F2,F5,F6,F7,F8,F12,F13,F14
* ,U13M0,U23M0
* ,EFILT
COMMON /LODPAS/LL(16),FTL(6,16),NLL
DIMENSION ERR(120)
DIMENSION LPCINT(100),JPINT(100)
DIMENSION XDBL(6,202)
EQUIVALENCE (XDD(1),XDBL(1,1))

```

LUM04840	199100000
LUM04850	199200000
LUM04860	199300000
LUM04870	199400000
LUM04880	199500000
LUM04890	199600000
LUM04900	199700000
LUM04910	199800000
LUM04920	199900000
LUM04930	200000000
LUM04940	200100000
LUM04950	200200000
LUM04960	200300000
LUM04970	200400000
LUM04980	200500000
LUM04990	200600000
LUM05000	200700000
LUM05010	200800000
LUM05020	200900000
LUM05030	201000000
LUM05040	201100000
LUM05050	201200000
LUM05060	201300000
LUM05070	201400000
LUM05080	201500000
LUM05090	201600000
LUM05100	201700000
LUM05110	201800000
LUM05120	201900000
LUM05130	202000000
LUM05140	202100000
LUM05150	202200000
LUM05160	202300000
LUM05170	202400000
LUM05180	202500000
LUM05190	202600000
LUM05200	202700000
LUM05210	202800000
LUM05220	202900000
LUM05230	203000000
LUM05240	203100000
LUM05250	203200000
LUM05260	203300000
LUM05270	203400000
LUM05280	203500000
LUM05290	203600000
LUM05300	203700000
	203800000
	203900000

C ADD FM TO DELR

NC6=NCW*6

NL6=NLAB*6

IOFF=1

KLAB=0

TOLD=T

IF(KLUE.EQ.2 .OR. KLUE.GT.3)KLAB=1

```

IF(KLAB.EQ.1)GO TO 15
DO 10 I=1,NMLAB
L=I+6
10 DELAB(L)=DELAB(L)-CMK(I,3)*VEC(I,1)-CMK(I,1)*VEC(I,2)
15 IF(KLUE.GT.2)GO TO 25
DO 20 I=1,NMCW
L=I+6
20 DELCW(L)=DELCW(L)-CMK(I,4)*VECBAR(I,1)-CMK(I,2)*VECBAR(I,2)
C
C CONSTRUCT YICS
C
25 IF(T.GT.0.1)GO TO 100
NEQNS=6
DO 30 I=1,3
YICS(I)=ROOT(I)
30 YICS(I+3)=WX(I)
IF(KLAB.EQ.1)GO TO 45
NEQNS=NEQNS+NMLAB
DO 35 I=1,NMLAB
35 YICS(I+6)=VEC(I,2)
45 IF(KLUE.EQ.4)GO TO 50
DO 40 I=1,3
J=NEQNS+I
YICS(J)=DELRBD(I)
40 YICS(J+3)=WY(I)
NEQNS=NEQNS+6
IF(KLUE.GT.2)GO TO 50
DO 48 I=1,NMCW
48 YICS(NEQNS+I)=VECBAR(I,2)
NEQNS=NEQNS+NMCW
50 NEQ=NEQNS
DO 55 I=1,3
J=NEQNS+I
YICS(J)=R(I)
55 YICS(J+3)=GAM(I)
NEQNS=NEQNS+6
IF(KLAB.EQ.1)GO TO 65
DO 60 I=1,NMLAR
60 YICS(NEQNS+I)=VEC(I,1)
NEQNS=NEQNS+NMLAB
65 IF(KLUE.EQ.4)GO TO 100
DO 70 I=1,3
J=NEQNS+I
YICS(J)=DELRB(I)
70 YICS(J+3)=ETAST(I)
NEQNS=NEQNS+6
IF(KLUE.GT.2)GO TO 100
DO 75 I=1,NMCH
75 YICS(NEQNS+I)=VECBAR(I,1)
NEQNS=NEQNS+NMCW
C

```

LUM05310 204000000

LUM05320 204100000

LUM05330 204200000

LUM05340 204300000

LUM05350 204400000

LUM05360 204500000

LUM05370 204600000

LUM05380 204700000

LUM05390 204800000

LUM05400 204900000

LUM05410 205000000

LUM05420 205100000

LUM05430 205200000

LUM05440 205300000

LUM05450 205400000

LUM05460 205500000

LUM05470 205600000

LUM05480 205700000

LUM05490 205800000

LUM05500 205900000

LUM05510 206000000

LUM05520 206100000

LUM05530 206200000

LUM05540 206300000

LUM05550 206400000

LUM05560 206500000

LUM05570 206600000

LUM05580 206700000

LUM05590 206800000

LUM05600 206900000

LUM05610 207000000

LUM05620 207100000

LUM05630 207200000

LUM05640 207300000

LUM05650 207400000

LUM05660 207500000

LUM05670 207600000

LUM05680 207700000

LUM05690 207800000

LUM05700 207900000

LUM05710 208000000

LUM05720 208100000

LUM05730 208200000

LUM05740 208300000

LUM05750 208400000

LUM05760 208500000

LUM05770 208600000

LUM05780 208700000

LUM05790 208800000

LUM05800 208900000

LUM05810 209000000

```

C SET UP LAMBDA MATRIX IN ARRAY A
C
100 CALL XMCOPY(Z1,A,6,6,6)
   NQ=6
   IF(KLAB.EQ.1)GO TO 120
   CALL XMCOPY(Z3,A(7,1),NMLAB,6,20)
   CALL XMCOPY(Z4,A(7,7),NMLAB,NMLAB,20)
   NQ=NQ+NMLAB
120 IF(KLUE.EQ.4)GO TO 200
   J=NQ+1
   CALL XMCOPY(Z6,A(J,1),6,6,6)
   CALL XMCOPY(Z7,A(J,J),6,6,6)
   IF(KLAB.EQ.1)GO TO 140
   DO 130 I=7,NQ
   DO 130 L=1,6
130 A(L+NQ,I)=0.
140 IF(KLUE.GT.2)GO TO 200
   CALL XMCOPY(Z9,A(NQ+7,1),NMCW,6,20)
   CALL XMCOPY(Z10,A(NQ+7,NQ+1),NMCW,6,20)
   CALL XMCOPY(Z11,A(NQ+7,NQ+7),NMCW,NMCW,20)
   IF(KLAB.EQ.1)GO TO 200
   DO 180 I=1,NMLAB
   DO 180 J=1,NMCW
   NL=NQ+6+J
180 A(NL,I+6)=0.
C
C SET UP DEL SUR R
C
200 NL=NMLAB+6
   NQ=NMCW+6
   IF(KLUE.EQ.4)GO TO 211
   IF(KLUE.GT.2)NQ=6
   IF(KLAB.EQ.1)NL=6
   DO 210 I=1,NQ
210 DELAB(NL+1)=DELWC(I)
C
C SOLVE SYSTEM OF EQUATIONS , PUT INTO YDOT
C
211 IJ=0
   DO 214 I=1,NEQ
   DO 214 J=1,I
   IJ=IJ+1
214 XBI(IJ)=A(I,J)
   CALL CHASE(XBI,NEQ,DELAB,1,1,IND)
   IF(IND)220,220,221
221 WRITE(10UT,215)
215 FORMAT(* ERROR IN SOLVING SYSTEM OF EQUATIONS*/ )
   RETURN
C
C SET UP YDOT
C

```

```

LUM05820 209100000
LUM05830 209200000
LUM05840 209300000
LUM05850 209400000
LUM05860 209500000
LUM05870 209600000
LUM05880 209700000
LUM05890 209800000
LUM05900 209900000
LUM05910 210000000
LUM05920 210100000
LUM05930 210200000
LUM05940 210300000
LUM05950 210400000
LUM05960 210500000
LUM05970 210600000
LUM05980 210700000
LUM05990 210800000
LUM06000 210900000
LUM06010 211000000
LUM06020 211100000
LUM06030 211200000
LUM06040 211300000
LUM06050 211400000
LUM06060 211500000
LUM06070 211600000
LUM06080 211700000
LUM06090 211800000
LUM06100 211900000
LUM06110 212000000
LUM06120 212100000
LUM06130 212200000
LUM06140 212300000
LUM06150 212400000
LUM06160 212500000
LUM06170 212600000
LUM06180 212700000
LUM06190 212800000
LUM06200 212900000
LUM06210 213000000
LUM06220 213100000
LUM06230 213200000
LUM06240 213300000
LUM06250 213400000
LUM06260 213500000
LUM06270 213600000
LUM06280 213700000
LUM06290 213800000
LUM06300 213900000
LUM06310 214000000
LUM06320 214100000

```

```

220 DO 291 I=1,NEQ
291 YDOT(I)=DEL LAB(I)
      NEQP=NEQ
      DO 300 I=1,3
      J=I+NEQ
      YDOT(J)=YDOT(I)
300 YDOT(J+3)=GAMD(I)
      NEQ=NEQ+6
      DO 410 I=1,3
      XDD(I)=YDOT(I)
410 XDD(I+3)=YDOT(I+3)
      DO 510 I=1,3
      INML=I+NMLAB+6
      XDD(I+606)=YDOT(INML)
510 XDD(I+609)=YDOT(INML+3)
      IF(KLUE.EQ.4)GO TO 400
      IF(KLAB.EQ.1)GO TO 320
      DO 340 I=1,NMLAB
340 YDOT(NEQ+I)=VEC(I,2)
      NEQ=NEQ+NMLAB
      CALL MPRD(RMODE,YDOT(7),XDD(7),NL6,NMLAB,1,600,1)
320 IF(KLUE.EQ.4)GO TO 400
      DO 360 I=1,3
      J=I+NEQ
      YDOT(J)=DEL RBD(I)
360 YDOT(J+3)=ETASTD(I)
      NEQ=NEQ+6
      IF(KLUE.GT.2)GO TO 400
      DO 380 I=1,NMCW
380 YDOT(NEQ+I)=VECBAR(I,2)
      NEQ=NEQ+NMCW
      CALL MPRD(SMODE,YDOT(NMLAB+13),XDD(613),NC6,NMCW,1,600,1)
C
C SET UP THE INTEGRATION CYCLE
C
400 IF(IFCON.EQ.0)GO TO 401
      DO 381 I=1,NEQCN
381 YDOT(I+NEQ)=YDOTCN(I)
401 IF(T.GT.0)GO TO 550
      READ(IN,405)DELTA,EPSIL,STEP,DTAU,NTIME
405 FORMAT(3E15.8/E15.8,I3)
      PTAU=NTIME*DTAU
      IF(IFPLT.EQ.0)GO TO 943
      WRITE(IOUT,944)
944 FORMAT(#PLOTTING GROUPS SELECTED FOR THIS RUN*)
      DO 945 I=1,13
      IF(IPLOUT(I).EQ.0)GO TO 945
      WRITE(IOUT,946)I
946 FORMAT(I7X,I2)
      IF(I.EQ. 4)WRITE(IOUT,947)N1
      IF(I.EQ. 5)WRITE(IOUT,947)N2

```

```

LUM06330 214200000
LUM06340 214300000
LUM06350 214400000
LUM06360 214500000
LUM06370 214600000
LUM06380 214700000
LUM06390 214800000
LUM06400 214900000
LUM06410 215000000
LUM06420 215100000
LUM06430 215200000
LUM06440 215300000
LUM06450 215400000
LUM06460 215500000
LUM06470 215600000
LUM06480 215700000
LUM06490 215800000
LUM06500 215900000
LUM06510 216000000
LUM06520 216100000
LUM06530 216200000
LUM06540 216300000
LUM06550 216400000
LUM06560 216500000
LUM06570 216600000
LUM06580 216700000
LUM06590 216800000
LUM06600 216900000
LUM06610 217000000
LUM06620 217100000
LUM06630 217200000
LUM06640 217300000
LUM06650 217400000
LUM06660 217500000
LUM06670 217600000
LUM06680 217700000
LUM06690 217800000
LUM06700 217900000
LUM06710 218000000
LUM06720 218100000
LUM06730 218200000
LUM06740 218300000
LUM06750 218400000
LUM06760 218500000
LUM06770 218600000
LUM06780 218700000
LUM06790 218800000
LUM06800 218900000
LUM06810 219000000
LUM06820 219100000
LUM06830 219200000

```



```

IF(I.EQ. 6)WRITE(IOUT,947)N3
IF(I.EQ. 7)WRITE(IOUT,947)N4
IF(I.EQ. 8)WRITE(IOUT,947)N5
IF(I.EQ.12)WRITE(IOUT,947)N6
IF(I.EQ.13)WRITE(IOUT,947)N7
947 FORMAT(IH+,20X,*AT MASS NO.*,I3)
945 CONTINUE
943 CONTINUE
WRITE(IOUT,471)
471 FORMAT(#NUMERICAL INTEGRATION DATA*)
WRITE(IOUT,900)DELTA,EPSIL,STEP,DTAU,NTIME
900 FORMAT(6X,*DELTA*,12X,*EPSIL*,12X,*STEP*,13X,*DTAU*,13X,*NTIME*/
*4E17.7,6X,I3)
PO=0.
402 FORMAT(3E15.8)
IF(IFCON.EQ.0)GO TO 404
DO 382 I=1,NEQCN
382 YICS(I+NEQ)=YICSCN(I)
NEQNS=NEQNS+NEQCN
404 NCYCLF=0
N=0
TIC=0.
IF(DELTA.EQ.0.)GO TO 440
READ(IN,402)(ERR(I),I=1,NEQNS)
WRITE(IOUT,910)(FRR(I),I=1,NEQNS)
910 FORMAT(* ERROR PARAMETERS*/(8E16.7))
440 CONTINUE
WRITE(IOUT,619)
619 FORMAT(*TIME HISTORY*//)
I6=1
I7=1
IF(NLL.EQ.0)GO TO 971
DO 970 I=1,NLL
IF(N6.EQ.LL(I))I6=I
970 IF(N7.EQ.LL(I))I7=I
971 CONTINUE
CALL SETUP(MAGIN,MAGOUT,TIC,STEP,NEQNS,DTAU,EPSIL,DELTA,ERR,T,
* DTIME,YICS,YPRED,YCORR,YDOOT,YNEW,YDERV,Z,7(105),Z(209),
* Z(313),Z(417),Z(521))
MAGIN=-1
550 CALL MAGIC(MAGIN,MAGOUT,TIC,STEP,NEQNS,DTAU,EPSIL,DELTA,ERR,T,
* DTIME,YICS,YPRED,YCORR,YDOOT,YNEW,YDERV,Z,7(105),Z(209),
* Z(313),Z(417),Z(521))
IF(IFCON.EQ.0)GO TO 403
DO 554 I=1,NEQCN
554 YPRED(I)=YPRED(NEQ+I)
403 CONTINUE
IF(MAGOUT)560,560,570
560 MAGIN=-1
DO 565 I=1,NEQNS
565 PRED(I)=YPRED(I)
LUM06840 2193000000
LUM06850 2194000000
LUM06860 2195000000
LUM06870 2196000000
LUM06880 2197000000
LUM06890 2198000000
LUM06900 2199000000
LUM06910 2200000000
LUM06920 2201000000
LUM06930 2202000000
LUM06940 2203000000
LUM06950 2204000000
LUM06960 2205000000
LUM06970 2206000000
LUM06980 2207000000
LUM06990 2208000000
LUM07000 2209000000
LUM07010 2210000000
LUM07020 2211000000
LUM07030 2212000000
LUM07040 2213000000
LUM07050 2214000000
LUM07060 2215000000
LUM07070 2216000000
LUM07080 2217000000
LUM07090 2218000000
LUM07100 2219000000
LUM07110 2220000000
LUM07120 2221000000
LUM07130 2222000000
LUM07140 2223000000
LUM07150 2224000000
LUM07160 2225000000
LUM07170 2226000000
LUM07180 2227000000
LUM07190 2228000000
LUM07200 2229000000
LUM07210 2230000000
LUM07220 2231000000
LUM07230 2232000000
LUM07240 2233000000
LUM07250 2234000000
LUM07260 2235000000
LUM07270 2236000000
LUM07280 2237000000
LUM07290 2238000000
LUM07300 2239000000
LUM07310 2240000000
LUM07320 2241000000
LUM07330 2242000000
LUM07340 2243000000

```

```

NEQ=NEQP
GO TO 600
570 IF(T.EQ.0.)GO TO 230
TT=T-PO
IF(TT.LT.PTAU)GO TO 831
PO=T
230 CONTINUE
WRITE(IOUT,235)
235 FORMAT(/53H*****
IF(KLUE.NE.4)GO TO 1700
WRITE(IOUT,620)T,DTIME
620 FORMAT(/ * RIGID PROBLEFM OUTPUT AT TIME T=*,F15.8, * STEP=*,E15.8/
*5X,*RDOT*,13X,*WX*,12X,*RDOT*,11X,*WXDOT*,12X,*R*,13X,
*GAM*,14X,*WY*)
DO 630 I=1,3
630 WRITE(IOUT,640)RDOT(I),WX(I),YDOT(I),YDOT(I+3),R(I),GAM(I),WY(I)
640 FORMAT(7E16.8)
GO TO 1000
1700 CONTINUE
IF(T.GT.0.)GO TO 9
IF(KLUE.GF.4)GO TO 9
READ(IN,1)KLOUTL,KLOUTC
1 FORMAT(2I3)
DO 6 I=1,100
LPOINT(I)=I
6 JPOINT(I)=I
IF(KLOUTL.GT.0)READ(IN,2)(LPOINT(I),I=1,KLGUTL)
IF(KLOUTC.GT.0)READ(IN,2)(JPOINT(I),I=1,KLOUTC)
2 FORMAT(2O13)
9 CONTINUE
WRITE(IOUT,711)T,DTIME
711 FORMAT(/ * TIME=*,E15.8, * STEP=*,E15.8, /8X *R
* GAMMA
* ETA-STAR
* WX
* WY*)
DO 712 I=1,3
712 WRITE(IOUT,713)R(I),RDOT(I),GAM(I),WX(I),DELRB(I),DELRBD(I),
*ETA-STAR,WY(I)
713 FORMAT(8E16.7)
WRITE(IOUT,813)(XCD(I),XDD(I+3),XDD(I+606),XDD(I+609),DEL(I),
* DEL(I),PHIST(I),PHISTD(I),I=1,3)
813 FORMAT(*0 RDOT*,11X,*WXDOT*,10X,*DELRBD*,10X,*WYDOT*,14X,*DEL
* 12X,*DELDOT*,10X,*PHI STAR*,8X,*PHI STAR DOT*/(8E16.7))
IF(KLAB.EQ.1)GO TO 1998
WRITE(IOUT,751)
751 FORMAT(/ * MASS PT. *,5X,*Q*,16X,*Q-DOT *,12X,*QDDOT*,12X,*THETA*,
* 12X,*THETA-DOT*,9X,*THETADDOT*)
DO 811 I=1,KLOUTL
IJ=6*LPOINT(I)
IJ3=IJ+3
JI=LPOINT(I)
811 WRITE(IOUT,752)JI,(Q(J,JI),QD(J,JI),XDBL(J,JI+1),

```

```

224400000
224500000
224600000
224700000
224800000
224900000
225000000
225100000
225200000
225300000
225400000
225500000
225600000
225700000
225800000
225900000
226000000
226100000
226200000
226300000
226400000
226500000
226600000
226700000
226800000
226900000
227000000
227100000
227200000
227300000
227400000
227500000
227600000
227700000
227800000
227900000
228000000
228100000
228200000
228300000
228400000
228500000
228600000
228700000
228800000
228900000
229000000
229100000
229200000
229300000
229400000

```

```

LUM07350
LUM07360
LUM07370
LUM07380
LUM07390
LUM07400
LUM07410
LUM07420
LUM07430
LUM07440
LUM07450
LUM07460
LUM07470
LUM07480
LUM07490
LUM07500
LUM07510
LUM07520
LUM07530
LUM07540
LUM07550
LUM07560
LUM07570
LUM07580
LUM07590
LUM07600
LUM07610
LUM07620
LUM07630
LUM07640
LUM07650
LUM07660
LUM07670
LUM07680
LUM07690
LUM07700
LUM07710
LUM07720
LUM07730
LUM07740
LUM07750
LUM07760
LUM07770
LUM07780
LUM07790
LUM07800
LUM07810
LUM07820
LUM07830

```

```

* TH(J,JI),THD(J,JI),XDBL(J+3,JI+1),J=1,3)
752 FORMAT(/I4,6E18.8/(4X,6E18.8))
1998 IF(KLUE.GT.2)GO TO 1000
WRITE(IOUT,780)
780 FORMAT(/ * MASS PT. Q BAR*,12X,*Q BAR-DDOT*,7X,*Q BAR-DDOT*
,5X,*THETA BAR*,7X,*THETA BAR-DDOT*, 4X,*THETA BAR-DDOT*)
*
DO 812 I=1,KLOUTC
IJ=6*JPOINT(I)+606
IJ3=IJ+3
JI=JPOINT(I)
812 WRITE(IOUT,752)JI,(QB(J,JI),QBD(J,JI),XDBL(J,JI+102),
* THB(J,JI),THBD(J,JI),XDBL(J+3,JI+102),J=1,3)
1000 CONTINUE
WRITE(IOUT,I1)ZCM
11 FORMAT(/ * LOCATION OF CENTER OF MASS IN INERTIAL (Z) COORDINATES*/LUM08000
*(3F17.8))
WRITE(IOUT,I001)SUML,SUMT
1001 FORMAT(/ * ANGULAR MOMENTUM IN Z- COORDINATES*/3E18.8//
* TOTAL KINETIC ENERGY*/E18.8)
*
CALL MINMAX(NLAB,NCW)
CALL LCOUT
1234 CONTINUE
2010 IF(IFLUID.EQ.0)GO TO 2020
WRITE(IOUT,2015)V,VDMT,IRES(1),HIL(1),IRES(2),HIL(2)
2015 FORMAT(*OFUID DATA V=*,E15.8,* VDMT=*,E15.8/
* (* FLUID HEIGHT IN RES(*,I3,*)=*,E15.8)
2020 IF(NMLM.EQ.0)GO TO 2030
DO 2021 I=1,8
IF(MLM(I).EQ.0 .OR. I.EQ.2)GO TO 2021
WRITE(IOUT,2022)I,((UJ0(J,L,I),J=1,3),L=1,3)
2022 FORMAT(*MOTION OF MOVING MASS*,I3/* UJ =*,3E17.7/* UJD =*,3E17.7)
*/* UJDD=*,3E17.7)
2021 CONTINUE
2030 IF(MLM(2).EQ.0)GO TO 2040
IF(I.EQ.0)GO TO 2041
WRITE(IOUT,2031)UJ3,UJ023,YDOTCN(5),ERRDDX,XXCS
2031 FORMAT(*BALANCE MASS DATA*/ * U(2,3)=*,E15.8,* UDOT(2,3)=*,E15.8
*/* UDDOT(2,3)=*,E15.8/
** SENSOR ACCELERATION ERROR =*,E15.8/* SENSOR TO CM POS ERROR =*,
*E15.8)
WRITE(IOUT,2048)EFILT
2048 FORMAT(* SENSOR ACCELERATION ERROR (FILTERED) =*,E15.8)
GO TO 2040
2041 WRITE(IOUT,2031)UJ3,UJ023,YDOTCN(5),ERRDDX
2040 CONTINUE
IF(IFCON.EQ.0)GO TO 831
WRITE(IOUT,2050)F1,F2,F3,F4,F5,F6,F7,F8,F9,F10,F11,F12,F13,F14,F15
*F16,IAJ
2050 FORMAT(/ * CONTROL SYSTEM DATA*/ * JET THRUST*/
** F1 =*,E14.7,* F2 =*,E14.7,* F3 =*,E14.7,
** F4 =*,E14.7,* F5 =*,E14.7,* F6 =*,E14.7/

```

```

229500000
229600000
229700000
229800000
229900000
230000000
230100000
230200000
230300000
230400000
230500000
230600000
230700000
230800000
230900000
231000000
231100000
231200000
231300000
231400000
231500000
231600000
231700000
231800000
231900000
232000000
232100000
232200000
232300000
232400000
232500000
232600000
232700000
232800000
232900000
233000000
233100000
233200000
233300000
233400000
233500000
233600000
233700000
233800000
233900000
234000000
234100000
234200000
234300000
234400000
234500000

```

```

LUM07870
LUM07880
LUM07890
LUM07920
LUM07930
LUM07940
LUM07980
LUM07990
LUM08000
LUM08010
LUM08020
LUM08030
LUM08040
LUM08050
LUM08060
LUM08070
LUM08080
LUM08090
LUM08100
LUM08110
LUM08120
LUM08130
LUM08140
LUM08150
LUM08160
LUM08170
LUM08180
LUM08190
LUM08200
LUM08210
LUM08220
LUM08230
LUM08240
LUM08250
LUM08260
LUM08270
LUM08280
LUM08290
LUM08300
LUM08310
LUM08320
LUM08330
LUM08340
LUM08350
LUM08360

```

```

** F7 =*,E14.7,* F8 =*,E14.7,* F9 =*,E14.7,
** F10=*,E14.7,* F11=*,E14.7,* F12=*,E14.7/
** F13=*,E14.7,* F14=*,E14.7,* F15=*,E14.7,
** F16=*,E14.7/* CMG TORQUE =*,3E17.7)
WRITE(IOUT,664)
664 FORMAT(
WRITE(IOUT,2060)XNEW(3),ELD3,ELD03
2060 FJRMAT(* L03=*,E14.7,* L03D=*,E14.7,* L03DD=*,E14.7)
WRITE(IOUT,2070)DIC,DDIC
2070 FORMAT(* SPIN SPEED COMMAND =*,E14.7/* SPIN ACCELERATION COMMAND
*,E14.7)
831 CONTINUE
MAGIN=0
IF(IFPLT.EQ.0)GO TO 550
NCYCLF=NCYCLE+1
IF(NCYCLE.GT.850)GO TO 550
WRITE(I),WX
IF(IPLGT( 1).EQ.1)WRITE(I)GAM
IF(IPLGT( 2).EQ.1)WRITE(I)DEL
IF(IPLGT( 3).EQ.1)WRITE(I)PHIST
IF(IPLGT( 4).EQ.1)WRITE(I)(Q(I,N1),I=1,3)
IF(IPLGT( 5).EQ.1)WRITE(I)(TH(I,N2),I=1,3)
IF(IPLGT( 6).EQ.1)WRITE(I)(Q(I,N3),I=1,3)
IF(IPLGT( 7).EQ.1)WRITE(I)(TH(I,N4),I=1,3)
IF(IPLGT( 8).EQ.1)WRITE(I)(Q(I,N5),I=1,3)
IF(IPLGT( 9).EQ.1)WRITE(I)XNEW(3),XNEW(6),XNEW(9)
IF(IPLGT(10).EQ.1)WRITE(I)U13M0,U23M0 ,XXCS
IF(IPLGT(11).EQ.1)WRITE(I)V,VDDT,HIL(1)
IF(IPLGT(12).EQ.1)WRITE(I)(FTL(I,16),I=1,3)
IF(IPLGT(13).EQ.1)WRITE(I)(FTL(I,17),I=4,6)
GO TO 550
C
C TRANSFORM COORDINATES
C
600 IF(KLUE.NE.4)GO TO 700
DO 610 I=1,3
RDOT(I)=YPRED(I)
WX(I)=YPRED(I+3)
XDD(I)=YDOT(I)
XDD(I+3)=YDOT(I+3)
J=I+NEQ
R(I)=YPRED(J)
GAM(I)=YPRED(J+3)
610 WY(I)=-YPRED(I+3)
WY(I)=-WY(I)
GO TO 999
700 DO 710 I=1,3
RDOT(I)=YPRED(I)
WX(I)=YPRED(I+3)
J=I+NEQ
R(I)=YPRED(J)

```

```

LUM08370 234600000
LUM08380 234700000
LUM08390 234800000
LUM08400 234900000
LUM08410 235000000
LUM08420 235100000
LUM08430 235200000
LUM08440 235300000
LUM08450 235400000
LUM08460 235500000
LUM08470 235600000
LUM08480 235700000
LUM08490 235800000
LUM08500 235900000
LUM08510 236000000
LUM08520 236100000
LUM08530 236200000
LUM08540 236300000
LUM08550 236400000
LUM08560 236500000
LUM08570 236600000
LUM08580 236700000
LUM08590 236800000
LUM08600 236900000
LUM08610 237000000
LUM08620 237100000
LUM08630 237200000
LUM08640 237300000
LUM08650 237400000
LUM08660 237500000
LUM08670 237600000
LUM08680 237700000
LUM08690 237800000
LUM08700 237900000
LUM08710 238000000
LUM08720 238100000
LUM08730 238200000
LUM08740 238300000
LUM08750 238400000
LUM08760 238500000
LUM08770 238600000
LUM08780 238700000
LUM08790 238800000
LUM08800 238900000
LUM08810 239000000
LUM08820 239100000
LUM08830 239200000
LUM08840 239300000
LUM08850 239400000
LUM08860 239500000
LUM08870 239600000

```

```

GAM(I)=YPRED(J+3)
NQ=NMLAB+6+I
IF(KLUE.EQ.2 .OR. KLUE.EQ.5)NQ=I+6
DELRB(I)=YPRED(NQ)
WY(I)=YPRED(NQ+3)
NQ=NQ+NEQ
DELRB(I)=YPRED(NQ)
710 ETAST(I)=YPRED(NQ+3)
716 IF(KLAB.EQ.1)GO TO 998
CALL MPRD(RMODE, PRED(7),B ,NL6,NMLAB,1,600,1)
CALL MPRD(RMODE, PRED(NEQ*7),C ,NL6,NMLAR,1,600,1)
DO 740 I=1,NMLAB
IJ=NEQ+I+5
VEC(I,1)=YPRED(IJ)
740 VEC(I,2)=YPRED(I+6)
DO 750 I=1,NLAB
ISIX=6*(I-1)
DO 750 J=1,3
IJ=ISIX+J
QD(J,I)=8(IJ)
THD(J,I)=8(IJ+3)
Q(J,I)=C(IJ)
750 TH(J,I)=C(IJ+3)
998 IF(KLUE.GT.2)GO TO 959
NQ=NMLAR+13
IF(KLUE.EQ.2)NQ=13
CALL MPRD(SMODE, PRED(NQ),R,NC6,NMCW,1,600,1)
CALL MPRD(SMODE, PRED(NEQ+NQ),C,NC6,NMCW,1,600,1)
DO 760 I=1,NMCW
IJ=I+NMLAB+12
IF(KLUE.EQ.2)IJ=I+12
760 VECBAR(I,1)=YPRED(IJ+NEQ)
VECBAR(I,2)=YPRED(IJ)
DO 775 I=1,NCW
ISIX=6*(I-1)
DO 775 J=1,3
IJ=ISIX+J
QBD(J,I)=8(IJ)
THBD(J,I)=8(IJ+3)
QBJ(I)=C(IJ)
775 THB(J,I)=C(IJ+3)
999 DELT=T-TOLD
RETURN
END

```

```

LUM08880 239700000
LUM08890 239800000
239900000
LUM08900 240000000
LUM08910 240100000
LUM08920 240200000
LUM08930 240300000
LUM08940 240400000
LUM08950 240500000
LUM08960 240600000
LUM08970 240700000
LUM08980 240800000
LUM08990 240900000
LUM09000 241000000
LUM09010 241100000
LUM09020 241200000
LUM09030 241300000
LUM09040 241400000
LUM09050 241500000
LUM09060 241600000
LUM09070 241700000
LUM09080 241800000
LUM09090 241900000
LUM09100 242000000
LUM09110 242100000
242200000
LUM09120 242300000
LUM09130 242400000
LUM09140 242500000
LUM09150 242600000
242700000
LUM09160 242800000
LUM09170 242900000
LUM09180 243000000
LUM09190 243100000
LUM09200 243200000
LUM09210 243300000
LUM09220 243400000
LUM09230 243500000
LUM09240 243600000
LUM09250 243700000
LUM09260 243800000
LUM09270 243900000
LUM09280 244000000

```

```

SUBROUTINE LAST(NLAB,NCW)
COMMON T,R(3),RBDT(3),XIDEN(3,3),RHO,A,H1(3),H2(3),H3(3),H4(3),
* G1(3,3),G2(3,3),G3(3,3),G4(3,3),G5(3,3),H5(3)
COMMON /RIG/PIETA(3,3),PIGAM(3,3),SUM(4),SGAM(3,3),SETA(3,3)
COMMON /LABOR/WX(3),RI(3,100),Q(3,100),QDOT(3,100),TH(3,100),
* THD(3,100)
COMMON /CWT/RB(3),RBDOT(3),ETA(3),WY(3),RA(3,100),QB(3,100),
* QBD(3,100),THB(3,100),THBD(3,100)
COMMON /CONNECT/IPT,S(3),IAPT,SB(3),DEL(3),DELD(3),PHIST(3),
* PHISTD(3),DELRB(3),DELRD(3),GAM(3),GAMD(3),ETAST(3),
* ETASTD(3),PZR(3),ELL(3),ELLD(3)
COMMON /NEWCOM/VEL(3),ELD(3),ELDD(3),ROB(3),ROBD(3),ROHDD(3),
* VEC(30),PIBETA(3,3),IFDEPL

C* STEP 79
ETA(1)=ETAST(1)*3.141592653
ETA(2)=ETAST(2)
ETA(3)=ETAST(3)

C* STEP 80
CALL SSIN(ETA,G2,-1)
CALL SSINIGAM,G3,-1)

C* STEP 81
CALL PIF(ETAST,G1)

C* STEP 82
CALL SCALR(-1.,G1,PIETA,3)
CALL SCALR(-1.,PIETA,PIETA,1)

C* STEP 83
CALL MULT(G3,WX,GAMD,1)

C* STEP 84
CALL MULT(PIETA,WX,H1,1)
CALL SUBTR(WY,H1,H1,1)
CALL MULT(G2,H1,ETASTD,1)

C* STEP 85
IF(IFDEPL.EQ.0)GO TO 20
CALL LLDLDD

C* STEP 86
CALL MTRAN(PIBETA,EL,ROB,1)
CALL MTRAN(PIBETA,ELD,ROBD,1)
CALL MTRAN(PIBETA,ELDD,ROBDD,1)
CALL SCALR(-1.,ROBD,ROBD,1)
CALL SCALR(-1.,ROBDD,ROBDD,1)
CALL ADD(S,RI(1,IPT),H1,1)
HI(1)=-HI(1)
CALL ADD(SB,RA(1,IAPT),H2,1)
DO 10 I=1,3
10 ROB(I)=-ROB(I)-HI(I)-H2(I)
C* STEP 87
20 CALL ADD(ROB,DELRB,RB,1)
CALL ADD(ROBD,DELRD,RBDOT,1)
C* STEP 88

```

```

LUM09290 244100000
LUM09300 244200000
LUM09310 244300000
LUM09320 244400000
LUM09330 244500000
LUM09340 244600000
LUM09350 244700000
LUM09360 244800000
LUM09370 244900000
LUM09380 245000000
LUM09390 245100000
LUM09400 245200000
LUM09410 245300000
LUM09420 245400000
LUM09430 245500000
LUM09440 245600000
LUM09450 245700000
LUM09460 245800000
LUM09470 245900000
LUM09480 246000000
LUM09490 246100000
LUM09500 246200000
LUM09510 246300000
LUM09520 246400000
LUM09530 246500000
LUM09540 246600000
LUM09550 246700000
LUM09560 246800000
LUM09570 246900000
LUM09580 247000000
LUM09590 247100000
LUM09600 247200000
LUM09610 247300000
LUM09620 247400000
LUM09630 247500000
LUM09640 247600000
LUM09650 247700000
LUM09660 247800000
LUM09670 247900000
LUM09680 248000000
LUM09690 248100000
LUM09700 248200000
LUM09710 248300000
LUM09720 248400000
LUM09730 248500000
LUM09740 248600000
LUM09750 248700000
LUM09760 248800000
LUM09770 248900000

```

```

CALL GAMMA1TH(I,IPT),G2)
CALL GAMMA1THR(I,IAPT),G3)
CALL GAMMA1THD(I,IPT),G4)
CALL GAMMA1THD(I,IAPT),G5)
C* STEP 89
DO 30 I=1,3
H1(I)=SIN(ETAST(I)/2.)
H1(I)=H1(I)*H1(I)
H2(I)=SIN(ETAST(I))
H3(I)=COS(ETAST(I))
30 H3(I)=2.*I2.*H1(2)*H1(3)-H1(2)*H1(3)
G1(1,2)=-(H2(3)*H3(1)+H3(3)*H2(2)*H2(1))
G1(1,3)=-(H2(3)*H2(1)-H3(3)*H2(2)*H3(1))
G1(2,1)=-H2(3)*H3(2)
G1(2,2)=-2.*I2.*H1(1)*H1(3)-H1(1)*H1(3)-H2(1)*H2(2)*H2(3))
G1(2,3)=-H3(3)*H2(1)+H2(3)*H2(2)*H3(1))
G1(3,1)=H2(2)
G1(3,2)=H3(2)*H2(1)
G1(3,3)=-2.*I2.*H1(1)*H1(2)-H1(1)-H1(2))
C* STEP 90
CALL MULT(G2,S,H4,I)
DO 40 I=1,3
40 H2(I)=RI(I,IPT)+Q(I,IPT)+S(I)+H4(I)
CALL MULT(PIETA,H2,H1,I)
DO 50 I=1,3
50 H2(I)=H1(I)-RB(I,I)-RA(I,IAPT)-QB(I,IAPT)
CALL MULT(G3,H2,H3,I)
CALL ADD(O(I,IPT),H4,H4,I)
CALL MULT(PIETA,H4,H2,I)
CALL ADD(RI(I,IPT),S,H5,I)
CALL MULT(G1,H5,H4,I)
DO 60 I=1,3
60 H5(I)=-DELRB(I)+H4(I)-QB(I,IAPT)+H2(I)-H3(I)
CALL MULT(PIBETA,H5,DEL,I)
C* STEP 91
CALL SSIN(ETA,SETA,I)
CALL SSIN(GAM,SGAM,I)
CALL PIF(GAM,PIGAM)
C* STEP 92
CALL ADD(EL,DEL,H2,I)
CALL SCALR(I.,H2,ELL,I)
C* STEP 93
CALL MULT(SETA,ETASTD,H3,I)
CALL GAMMA(H3,G1)
CALL MULT(G1,H1,H4,I)
CALL MULT(G4,S,H1,I)
CALL ADD(H1,QUOT(I,IPT),H1,I)
CALL MULT(PIETA,H1,H5,I)
CALL MTRAN(PIBETA,H2,H1,I)
CALL ADD(H1,SB,H1,I)
CALL MULT(G5,H1,H2,I)
LUM09780 249000000
LUM09790 249100000
LUM09800 249200000
LUM09810 249300000
LUM09820 249400000
LUM09830 249500000
LUM09840 249600000
LUM09850 249700000
LUM09860 249800000
LUM09870 249900000
LUM09880 250000000
LUM09890 250100000
LUM09900 250200000
LUM09910 250300000
LUM09920 250400000
LUM09930 250500000
LUM09940 250600000
LUM09950 250700000
LUM09960 250800000
LUM09970 250900000
LUM09980 251000000
LUM09990 251100000
LUM10000 251200000
LUM10010 251300000
LUM10020 251400000
LUM10030 251500000
LUM10040 251600000
LUM10050 251700000
LUM10060 251800000
LUM10070 251900000
LUM10080 252000000
LUM10090 252100000
LUM10100 252200000
LUM10110 252300000
LUM10120 252400000
LUM10130 252500000
LUM10140 252600000
LUM10150 252700000
LUM10160 252800000
LUM10170 252900000
LUM10180 253000000
LUM10190 253100000
LUM10200 253200000
LUM10210 253300000
LUM10220 253400000
LUM10230 253500000
LUM10240 253600000
LUM10250 253700000
LUM10260 253800000
LUM10270 253900000
LUM10280 254000000

```

```

DD 70 I=1,3
70 HI(I)=-H2(I)-R8DOT(I)-QB8D(I,IAPT)-H4(I)+H5(I)
  CALL MULT(G3,H1,H2,1)
  CALL SUBTR(H1,H2,H1,1)
  CALL MULT(PIBETA,H1,H2,1)
  CALL SCALAR(1.,H2,ELLD,1)
C* STEP 94
  CALL SUBTR(H2,ELD,DELD,1)
C* STEP 95
DD 80 I=1,3
DD 80 J=1,3
G4(I,J)=0.
DD 80 K=1,3
G=G3(I,K)
IF(I.EQ.K)G=G+1.
80 G4(I,J)=G4(I,J)+G*PIBETA(J,K)
  CALL MTRAN(PIETA,G4,G1,3)
  CALL MULT(G2,G1,G4,3)
  CALL SUBTR(G1,G4,G4,3)
DD 90 I=2,3
DD 90 J=1,3
90 G4(I,J)=-G4(I,J)
  CALL MULT(PIETA,G4,G1,3)
C* STEP 96
  PHIST(2)=ARSIN(G1(3,1))
  G=COS(PHIST(2))
  PHIST(1)=ARSIN(-G1(3,2)/G)
  PHIST(3)=ARSIN(-G1(2,1)/G)
C* STEP 97
  CALL SSIN(PHIST,G4,-1)
C* STEP 98
  CALL MULT(G3,H3,H2,1)
  CALL SUBTR(H3,H2,H2,1)
  CALL ADD(H2,THRD(1,IAPT),H2,1)
  CALL MULT(PIBETA,H2,H1,1)
  CALL MULT(G1,H1,H2,1)
  HI(1)=THD(1,IPT)
  HI(2)=-THD(2,IPT)
  HI(3)=-THD(3,IPT)
  CALL MULT(PIBETA,H1,H3,1)
  CALL SUBTR(H3,H2,H2,1)
  CALL MULT(G4,H2,PHIST0,1)
  RETURN
END
LUM10290 254100000
LUM10300 254200000
LUM10310 254300000
LUM10320 254400000
LUM10330 254500000
LUM10340 254600000
LUM10350 254700000
LUM10360 254800000
LUM10370 254900000
LUM10380 255000000
LUM10390 255100000
LUM10400 255200000
LUM10410 255300000
LUM10420 255400000
LUM10430 255500000
LUM10440 255600000
LUM10450 255700000
LUM10460 255800000
LUM10470 255900000
LUM10480 256000000
LUM10490 256100000
LUM10500 256200000
LUM10510 256300000
LUM10520 256400000
LUM10530 256500000
LUM10540 256600000
LUM10550 256700000
LUM10560 256800000
LUM10570 256900000
LUM10580 257000000
LUM10590 257100000
LUM10600 257200000
LUM10610 257300000
LUM10620 257400000
LUM10630 257500000
LUM10640 257600000
LUM10650 257700000
LUM10660 257800000
LUM10670 257900000
LUM10680 258000000
LUM10690 258100000
LUM10700 258200000
LUM10710 258300000
LUM10720 258400000

```



```
SUBROUTINE SUBTR(A,B,C,N)  
DIMENSION A(3,N),B(3,N),C(3,N)  
DO 10 I=1,3  
DO 10 J=1,N  
10 C(I,J)=A(I,J)-B(I,J)  
RETURN  
END
```

```
LUM10730 258500000  
LUM10740 258600000  
LUM10750 258700000  
LUM10760 258800000  
LUM10770 258900000  
LUM10780 259000000  
LUM10790 259100000
```

```
SUBROUTINE MULT(A,B,C,N)
DIMENSION A(3,3),B(3,N),C(3,N)
DO 10 I=1,3
DO 10 J=1,N
C(I,J)=0.
DO 10 K=1,3
10 C(I,J)=C(I,J)+A(I,K)*B(K,J)
RETURN
END
```

```
LUM10800 2592000000
LUM10810 2593000000
LUM10820 2594000000
LUM10830 2595000000
LUM10840 2596000000
LUM10850 2597000000
LUM10860 2598000000
LUM10870 2599000000
LUM10880 2600000000
```

LUM10890 2601 000000
LUM10900 2602 000000
LUM10910 2603 000000
LUM10920 2604 000000
LUM10930 2605 000000
LUM10940 2606 000000
LUM10950 2607 000000

SUBROUTINE ADD(A,B,C,N)
DIMENSION A(3,N),B(3,N),C(3,N)
DO 10 I=1,3
DO 10 J=1,N
10 C(I,J)=A(I,J)+B(I,J)
RETURN
END

```
SUBROUTINE SCALR(S,A,B,N)
DIMENSION A(3,N),R(3,N)
DO 10 I=1,3
DO 10 J=1,N
10 B(I,J)=A(I,J)*S
RETURN
END
```

```
LUM10960 260800000
LUM10970 260900000
LUM10980 261000000
LUM10990 261100000
LUM11000 261200000
LUM11010 261300000
LUM11020 261400000
```

```

SUBROUTINE PIF(A,B)
DIMENSION A(3),B(9),C(6)
DO 10 I=1,3
C(I)=COS(A(I))
10 C(I+3)=SIN(A(I))
B(1)=C(3)*C(2)
B(2)=-C(6)*C(2)
B(3)=C(5)
B(4)=C(6)*C(1)+C(4)*C(5)*C(3)
B(5)=C(3)*C(1)-C(5)*C(6)*C(4)
B(6)=-C(2)*C(4)
B(7)=C(6)*C(4)-C(5)*C(3)*C(1)
B(8)=C(3)*C(4)+C(5)*C(6)*C(1)
B(9)=C(1)*C(2)
RETURN
END
LUM11030 261500000
LUM11040 261600000
LUM11050 261700000
LUM11060 261800000
LUM11070 261900000
LUM11080 262000000
LUM11090 262100000
LUM11100 262200000
LUM11110 262300000
LUM11120 262400000
LUM11130 262500000
LUM11140 262600000
LUM11150 262700000
LUM11160 262800000
LUM11170 262900000
LUM11180 263000000

```

LUM11190 263100000
LUM11200 263200000
LUM11210 263300000
LUM11220 263400000
LUM11230 263500000
LUM11240 263600000
LUM11250 263700000
LUM11260 263800000
LUM11270 263900000

```
SUBROUTINE PTLP(A,R,C)
DIMENSION A(3,3),B(3),C(3,3)
DO 10 I=1,3
DO 10 J=1,3
C(I,J)=0.
DO 10 K=1,3
10 C(I,J)=C(I,J)+R(K)*A(K,I)*A(K,J)
RETURN
END
```

```
SUBROUTINE MTRAN(A,B,C,N)
DIMENSION A(3,3),B(3,1),C(3,1)
DO 10 I=1,3
DO 10 J=1,N
C(I,J)=0.
DO 10 K=1,3
10 C(I,J)=C(I,J)+A(K,I)*B(K,J)
RETURN
END
```

```
LUM11280 264000000
LUM11290 264100000
LUM11300 264200000
LUM11310 264300000
LUM11320 264400000
LUM11330 264500000
LUM11340 264600000
LUM11350 264700000
LUM11360 264800000
```

```
FUNCTION DOTP(A,B)
DIMENSION A(3),B(3)
DOTP=A(1)*B(1)+A(2)*B(2)+A(3)*B(3)
RETURN
END
```

```
LUM11370 264900000
LUM11380 265000000
LUM11390 265100000
LUM11400 265200000
LUM11410 265300000
```



```
SUBROUTINE XADD(A,B,C,M,N,IDI,ID2)  
DIMENSION A(ID1,1),B(ID2,1),C(ID2,1)  
DO 10 I=1,M  
  DO 10 J=1,N  
    10 C(I,J)=A(I,J)+B(I,J)  
RETURN  
END
```

```
LUM11420 265400000  
LUM11430 265500000  
LUM11440 265600000  
LUM11450 265700000  
LUM11460 265800000  
LUM11470 265900000  
LUM11480 266000000
```

```

SUBROUTINE XMPRD(A,B,C,N,M,K,NDIM1,NDIM2,NDIM3)
DIMENSION A(NDIM1,1),B(NDIM2,1),C(NDIM3,1)
DO 10 I=1,N
DO 10 J=1,K
C(I,J)=0.
DO 10 L=1,M
10 C(I,J)=C(I,J)+A(I,L)*B(L,J)
RETURN
END

LUM11490 266100000
LUM11500 266200000
LUM11510 266300000
LUM11520 266400000
LUM11530 266500000
LUM11540 266600000
LUM11550 266700000
LUM11560 266800000
LUM11570 266900000

```

```
SUBROUTINE XTPRD(A,B,C,N,M,K, IDIM1, IDIM2, IDIM3)
DIMENSION A(IDIM1,1),R(IDIM2,1),C(IDIM3,1)
DO 10 I=1,M
DO 10 J=1,K
C(I,J)=0.
DO 10 L=1,N
10 C(I,J)=C(I,J)+A(L,I)*R(L,J)
RETURN
END
```

LUM11580	267000000
LUM11590	267100000
LUM11600	267200000
LUM11610	267300000
LUM11620	267400000
LUM11630	267500000
LUM11640	267600000
LUM11650	267700000
LUM11660	267800000

```

SUBROUTINE SSIN(A,B,KLUE)
DIMENSION A(3),B(3,3)
  B(1,3)=0.
  B(2,3)=0.
  S2=SIN(A(2))
  S3=SIN(A(3))
  C2=COS(A(2))
  C3=COS(A(3))
  B(3,3)=1.
  B(2,2)=C3
  IF(KLUE.LT.0)GO TO 10
  B(1,1)=C3*C2
  B(1,2)=S3
  B(3,1)=S2
  B(3,2)=0.
  B(2,1)=-S3*C2
  GO TO 20
10 B(1,1)=C3/C2
  B(1,2)=-S3/C2
  B(3,1)=-C3*S2/C2
  B(3,2)=S3*S2/C2
  B(2,1)=S3
20 RETURN
  END
LUM11670 267900000
LUM11680 268000000
LUM11690 268100000
LUM11700 268200000
LUM11710 268300000
LUM11720 268400000
LUM11730 268500000
LUM11740 268600000
LUM11750 268700000
LUM11760 268800000
LUM11770 268900000
LUM11780 269000000
LUM11790 269100000
LUM11800 269200000
LUM11810 269300000
LUM11820 269400000
LUM11830 269500000
LUM11840 269600000
LUM11850 269700000
LUM11860 269800000
LUM11870 269900000
LUM11880 270000000
LUM11890 270100000
LUM11900 270200000

```

```
SUBROUTINE XMCOPY(A,B,N,M,K)
DIMENSION A(K,I),B(52,I)
DO 10 I=1,N
DO 10 J=1,M
10 B(I,J)=A(I,J)
RETURN
END
```

```
LUM11910 2703000000
LUM11920 2704000000
LUM11930 2705000000
LUM11940 2706000000
LUM11950 2707000000
LUM11960 2708000000
LUM11970 2709000000
```

```
SUBROUTINE MCPY(A,B,N,M,NDIM)  
DIMENSION A(NDIM,1),B(NDIM,1)  
DO 10 I=1,N  
DO 10 J=1,M  
10 B(I,J)=A(I,J)  
RETURN  
END
```

```
LUM11980 271000000  
LUM11990 271100000  
LUM12000 271200000  
LUM12010 271300000  
LUM12020 271400000  
LUM12030 271500000  
LUM12040 271600000
```

```

SUBROUTINE MPRD(A,B,C,N,M,K,NDIM1,NDIM2)
DIMENSION A(NDIM1,1),R(NDIM2,1),C(NDIM1,1)
DO 10 I=1,N
DO 10 J=1,K
C(I,J)=0.
DO 10 L=1,M
10 C(I,J)=C(I,J)+A(I,L)*B(L,J)
RETURN
END
LUM12050 271700000
LUM12060 271800000
LUM12070 271900000
LUM12080 272000000
LUM12090 272100000
LUM12100 272200000
LUM12110 272300000
LUM12120 272400000
LUM12130 272500000

```

```

SUBROUTINE TPRD(A,B,C,N,M,K, IDIM1, IDIM2)
DIMENSION A(IDIM1,1),B(IDIM1 ,1),C(IDIM2,1)
DO 10 I=1,M
DO 10 J=1,K
C(I,J)=0.
DO 10 L=1,N
10 C(I,J)=C(I,J)+A(L,I)*B(L,J)
RETURN
END

```

```

LUM12140 272600000
LUM12150 272700000
LUM12160 272800000
LUM12170 272900000
LUM12180 273000000
LUM12190 273100000
LUM12200 273200000
LUM12210 273300000
LUM12220 273400000

```



```

SUBROUTINE INCH (A,MO,Y,NIX)
C
C INVERSION OF POSITIVE DEFINITE REAL SYMMETRIC MATRIX A. A IS ASSUMED
C TO BE STORED BY ROWS IN LOWER TRIANGULAR FORM. THE INVERSE IS STORED
C OVER A.
COMMON /BOND/ M,K /WINTER/ KOLD
COMMON /OPT2/ PRINT
REAL A(1),Y(1)
10 FORMAT ( SHINVERSE/1H0)
20 FORMAT (I5,IP6E20.7/(5X,IP6E20.7))
IF (PRINT .GT. 0.) WRITE (6,10)
KOLD = 0
M = IABS(MO)
CALL FUTILE(A,M,NIX)
IF (NIX) 120,100,100
100 KK = 0
K1 = 1
DO 115 K = 1,M
KK = KK + K
DO 105 I = K,M
105 Y(I) = 0.
Y(K) = 1.
CALL TRIEG(A(K1),Y)
IK = KK
DO 110 I = K,M
A(IK) = Y(I)
IK = IK + I
110 CONTINUE
IF (PRINT .GT. 0.) WRITE (6,20) K,(Y(I), I = K,M)
115 K1 = K1 + K
120 CONTINUE
RETURN
END
LUMI2230 273500000
LUMI2240 273600000
LUMI2250 273700000
LUMI2260 273800000
LUMI2270 273900000
LUMI2280 274000000
LUMI2290 274100000
LUMI2300 274200000
LUMI2310 274300000
LUMI2320 274400000
LUMI2330 274500000
LUMI2340 274600000
LUMI2350 274700000
LUMI2360 274800000
LUMI2370 274900000
LUMI2380 275000000
LUMI2390 275100000
LUMI2400 275200000
LUMI2410 275300000
LUMI2420 275400000
LUMI2430 275500000
LUMI2440 275600000
LUMI2450 275700000
LUMI2460 275800000
LUMI2470 275900000
LUMI2480 276000000
LUMI2490 276100000
LUMI2500 276200000
LUMI2510 276300000
LUMI2520 276400000
LUMI2530 276500000
LUMI2540 276600000
LUMI2550 276700000

```

```

SURROUTINE GAMMA(A,B)
DIMENSION A(3),B(3,3)
DO 10 I=1,3
  B(I,I)=0.
  B(1,2)=-A(3)
  B(2,1)=A(3)
  B(1,3)=A(2)
  B(3,1)=-A(2)
  B(2,3)=-A(1)
  B(3,2)=A(1)
RETURN
END

```

```

LUM12560 276800000
LUM12570 276900000
LUM12580 277000000
LUM12590 277100000
LUM12600 277200000
LUM12610 277300000
LUM12620 277400000
LUM12630 277500000
LUM12640 277600000
LUM12650 277700000
LUM12660 277800000
LUM12670 277900000

```

```

SUBROUTINE PL03AX
COMMON VAR, SCPT, TPL, PLT1, PLT2, PLT3, PLT4, PLT5, PLT6,
* PLT7, PLT8, PLT9, PLT10, PLT11, PLT12
DIMENSION TPL(852), PLT1(852), PLT2(852), PLT3(852), PLT4(852),
1 PLT5(852), PLT6(852), PLT7(852), PLT8(852), PLT9(852),
2 PLT10(852), PLT11(852), PLT12(852)
DIMENSION VAR(30), SCPT(50)
COMMON /BIG/PLT13(852), PLT14(852), PLT15(852), PLT16(852), PLT17(852),
* PLT18(852), PLT19(852), PLT20(852), PLT21(852),
* PLT22(852), PLT23(852), PLT24(852)
EQUIVALENCE (VAR(1), DYP1), (VAR(2), DYP2), (VAR(3), DYP3),
1 (VAR(4), DYP4), (VAR(5), DYP5), (VAR(6), DYP6),
1 (VAR(7), DYP7), (VAR(8), DYP8), (VAR(9), DYP9),
1 (VAR(10), DYP10), (VAR(11), DYP11), (VAR(12), DYP12),
1 (VAR(13), DYP13), (VAR(14), DYP14), (VAR(15), DYP15),
1 (VAR(16), DYP16), (VAR(17), DYP17), (VAR(18), DYP18),
1 (VAR(19), DYP19), (VAR(20), DYP20), (VAR(21), DYP21),
1 (VAR(22), DYP22), (VAR(23), DYP23), (VAR(24), DYP24)
NC=1
JL=0.
S=0.
BCD=0.
REWIND 1
READ(1)NRUN, PBLOCK, TEND, DTPL0T
NPOINT=1
10 READ(1) TPL(NPOINT), PLT1(NPOINT), PLT2(NPOINT), PLT3(NPOINT)
IF(EOF, 1)20, 101
101 CONTINUE
IF(PBLOCK.EQ.1)GO TO 15
READ(1) PLT4(NPOINT), PLT5(NPOINT), PLT6(NPOINT)
IF(EOF, 1)20, 102
102 CONTINUE
IF(PBLOCK.EQ.2)GO TO 15
READ(1) PLT7(NPOINT), PLT8(NPOINT), PLT9(NPOINT)
IF(EOF, 1)20, 103
103 CONTINUE
IF(PBLOCK.EQ.3)GO TO 15
READ(1) PLT10(NPOINT), PLT11(NPOINT), PLT12(NPOINT)
IF(EOF, 1)20, 104
104 CONTINUE
IF(PBLOCK.EQ.4)GO TO 15
READ(1) PLT13(NPOINT), PLT14(NPOINT), PLT15(NPOINT)
IF(EOF, 1)20, 105
105 CONTINUE
IF(PBLOCK.EQ.5)GO TO 15
READ(1) PLT16(NPOINT), PLT17(NPOINT), PLT18(NPOINT)
IF(EOF, 1)20, 106
106 CONTINUE
IF(PBLOCK.EQ.6)GO TO 15

```

```

LUM12680 278000000
LUM12690 278100000
LUM12700 278200000
LUM12 278300000
LU 278400000
278500000
LUM12740 278600000
LUM12750 278700000
LUM12760 278800000
LUM12770 278900000
LUM12780 279000000
LUM12790 279100000
LUM12800 279200000
LUM12810 279300000
LUM12820 279400000
LUM12830 279500000
LUM12840 279600000
LUM12850 279700000
LUM12860 279800000
279900000
280000000
280100000
280200000
LUM12870 280300000
LUM12880 280400000
LUM12890 280500000
LUM12900 280600000
280700000
LUM12910 280800000
280900000
281000000
281100000
LUM12930 281200000
281300000
281400000
281500000
LUM12950 281600000
281700000
281800000
281900000
LUM12970 282000000
282100000
282200000
282300000
LUM12990 282400000
282500000
282600000
282700000
LUM13010 282800000

```

```

READ(1)      PLT19(NPOINT), PLT20(NPOINT), PLT21(NPOINT)
IF(EOF,1)20,107
107 CONTINUE
IF(PBLOCK.EQ.7.JGO TO 15
READ(1)      PLT22(NPOINT), PLT23(NPOINT), PLT24(NPOINT)
IF(EOF,1)20,108
108 CONTINUE
15 NPOINT=NPOINT+1
GO TO 10
20 NPOINT=NPOINT-1
REWIND 1
D0 67 I=1,24
67 VAR(I)=0.0
SCPT(1)=0.0001
SCPT(2)=0.0002
SCPT(3)=0.0004
SCPT(4)=0.0006
SCPT(5)=0.0008
SCPT(6)=0.001
SCPT(7)=0.002
SCPT(8)=0.004
SCPT(9)=0.006
SCPT(10)=0.008
SCPT(11)=0.01
SCPT(12)=0.02
SCPT(13)=0.04
SCPT(14)=0.06
SCPT(15)=0.08
SCPT(16)=0.1
SCPT(17)=0.2
SCPT(18)=0.4
SCPT(19)=0.6
SCPT(20)=0.8
SCPT(21)=1.0
SCPT(22)=2.0
SCPT(23)=4.0
SCPT(24)=6.0
SCPT(25)=8.0
SCPT(26)=10.0
SCPT(27)=20.0
SCPT(28)=40.0
SCPT(29)=60.0
SCPT(30)=80.0
SCPT(31)=100.0
SCPT(32)=200.0
SCPT(33)=400.0
SCPT(34)=600.0
SCPT(35)=800.0
SCPT(36)=1000.0
SCPT(37)=2000.0
SCPT(38)=4000.0
282900000
283000000
283100000
283200000
283300000
283400000
283500000
283600000
283700000
283800000
283900000
284000000
284100000
284200000
284300000
284400000
284500000
284600000
284700000
284800000
284900000
285000000
285100000
285200000
285300000
285400000
285500000
285600000
285700000
285800000
285900000
286000000
286100000
286200000
286300000
286400000
286500000
286600000
286700000
286800000
286900000
287000000
287100000
287200000
287300000
287400000
287500000
287600000
287700000
287800000
287900000
LUM13030
LUM13050
LUM13060
LUM13070
LUM13080
LUM13090
LUM13100
LUM13110
LUM13120
LUM13130
LUM13140
LUM13150
LUM13160
LUM13170
LUM13180
LUM13190
LUM13200
LUM13210
LUM13220
LUM13230
LUM13240
LUM13250
LUM13260
LUM13270
LUM13280
LUM13290
LUM13300
LUM13310
LUM13320
LUM13330
LUM13340
LUM13350
LUM13360
LUM13370
LUM13380
LUM13390
LUM13400
LUM13410
LUM13420
LUM13430
LUM13440
LUM13450
LUM13460
LUM13470
LUM13480

```

```

SCPT(39)=6000.0
SCPT(40)=6000.0
SCPT(41)=10000.0
SCPT(42)=20000.0
SCPT(43)=40000.0
SCPT(44)=60000.0
SCPT(45)=80000.0
SCPT(46)=100000.0
SCPT(47)=1.E6
SCPT(48)=5.E6
SCPT(49)=1.E7
SCPT(50)=1.E8
RUN=NRUN
CALL NUMBER(3.00,9.8,0.17,RUN,0.0,-1)
CALL SYMBL4(1.0,9.8,0.2,10HRUN NUMBER,0.0,10)
CALL SCALF(TPL,NPOINT,S,0.0,DTPLDT,1,1)
DO 8000 I=1,NPOINT
  DYP1=AMAX1(DYP1,ABS(PLT1(I)))
  DYP2=AMAX1(DYP2,ABS(PLT2(I)))
  DYP3=AMAX1(DYP3,ABS(PLT3(I)))
  IF(PBLOCK.EQ.1.160 TO 8000)
  DYP4=AMAX1(DYP4,ABS(PLT4(I)))
  DYP5=AMAX1(DYP5,ABS(PLT5(I)))
  DYP6=AMAX1(DYP6,ABS(PLT6(I)))
  IF(PBLOCK.EQ.2.160 TO 8000)
  DYP7=AMAX1(DYP7,ABS(PLT7(I)))
  DYP8=AMAX1(DYP8,ABS(PLT8(I)))
  DYP9=AMAX1(DYP9,ABS(PLT9(I)))
  IF(PBLOCK.EQ.3.160 TO 8000)
  DYP10=AMAX1(DYP10,ABS(PLT10(I)))
  DYP11=AMAX1(DYP11,ABS(PLT11(I)))
  DYP12=AMAX1(DYP12,ABS(PLT12(I)))
  IF(PBLOCK.EQ.4.160 TO 8000)
  DYP13=AMAX1(DYP13,ABS(PLT13(I)))
  DYP14=AMAX1(DYP14,ABS(PLT14(I)))
  DYP15=AMAX1(DYP15,ABS(PLT15(I)))
  IF(PBLOCK.EQ.5.160 TO 8000)
  DYP16=AMAX1(DYP16,ABS(PLT16(I)))
  DYP17=AMAX1(DYP17,ABS(PLT17(I)))
  DYP18=AMAX1(DYP18,ABS(PLT18(I)))
  IF(PBLOCK.EQ.6.160 TO 8000)
  DYP19=AMAX1(DYP19,ABS(PLT19(I)))
  DYP20=AMAX1(DYP20,ABS(PLT20(I)))
  DYP21=AMAX1(DYP21,ABS(PLT21(I)))
  IF(PBLOCK.EQ.7.160 TO 8000)
  DYP22=AMAX1(DYP22,ABS(PLT22(I)))
  DYP23=AMAX1(DYP23,ABS(PLT23(I)))
  DYP24=AMAX1(DYP24,ABS(PLT24(I)))
8000 CONTINUE
DO 8813 I=1,24
DO 8814 J=1,49

```

```

LUM13490 288000000
LUM13500 288100000
LUM13510 288200000
LUM13520 288300000
LUM13530 288400000
LUM13540 288500000
LUM13550 288600000
LUM13560 288700000
LUM13570 288800000
LUM13580 288900000
LUM13590 289000000
LUM13600 289100000
LUM13610 289200000
LUM13620 289300000
      289400000
LUM13640 289500000
LUM13650 289600000
LUM13660 289700000
LUM13670 289800000
LUM13680 289900000
LUM13690 290000000
LUM13700 290100000
LUM13710 290200000
LUM13720 290300000
LUM13730 290400000
LUM13740 290500000
LUM13750 290600000
LUM13760 290700000
LUM13770 290800000
LUM13780 290900000
LUM13790 291000000
LUM13800 291100000
LUM13810 291200000
LUM13820 291300000
LUM13830 291400000
LUM13840 291500000
LUM13850 291600000
LUM13860 291700000
LUM13870 291800000
LUM13880 291900000
LUM13890 292000000
LUM13900 292100000
LUM13910 292200000
LUM13920 292300000
LUM13930 292400000
LUM13940 292500000
LUM13950 292600000
LUM13960 292700000
LUM13970 292800000
LUM13980 292900000
LUM13990 293000000

```

```

8814 CONTINUE
8815 VAR(I)=SCPT(J)
8813 CONTINUE
  VGP1 =-7.5*DYP1
  VGP2 =-4.5*DYP2
  VGP3 =-1.5*DYP3
  IF(PBLOCK.EQ.1.)GO TO 25
  VGP4 =-7.5*DYP4
  VGP5 =-4.5*DYP5
  VGP6 =-1.5*DYP6
  IF(PBLOCK.EQ.2.)GO TO 25
  VGP7 =-7.5*DYP7
  VGP8 =-4.5*DYP8
  VGP9 =-1.5*DYP9
  IF(PBLOCK.EQ.3.)GO TO 25
  VGP10=-7.5*DYP10
  VGP11=-4.5*DYP11
  VGP12=-1.5*DYP12
  IF(PBLOCK.EQ.4.)GO TO 25
  VGP13=-7.5*DYP13
  VGP14=-4.5*DYP14
  VGP15=-1.5*DYP15
  IF(PBLOCK.EQ.5.)GO TO 25
  VGP16=-7.5*DYP16
  VGP17=-4.5*DYP17
  VGP18=-1.5*DYP18
  IF(PBLOCK.EQ.6.)GO TO 25
  VGP19=-7.5*DYP19
  VGP20=-4.5*DYP20
  VGP21=-1.5*DYP21
  IF(PBLOCK.EQ.7.)GO TO 25
  VGP22=-7.5*DYP22
  VGP23=-4.5*DYP23
  VGP24=-1.5*DYP24
25 CONTINUE
  CALL SCALE(PLT1 ,NPOINT,S,VGP1 ,DYP1 ,1,1)
  CALL SCALE(PLT2 ,NPOINT,S,VGP2 ,DYP2 ,1,1)
  CALL SCALE(PLT3 ,NPOINT,S,VGP3 ,DYP3 ,1,1)
  CALL AXIS(0,0,5,5,5HPLT1 ,5,2,0,90,0,VGP1 ,DYP1 ,0)
  CALL AXIS(0 ,3,5,5HPLT2 ,5,2,0,90,0,VGP2 ,DYP2 ,0)
  CALL AXIS(0,0,0,5,5HPLT3 ,5,2,0,90,0,VGP3 ,DYP3 ,0)
  TAXIS=TEND/DTPLOT
  CALL AXIS(0,7,5,BCD,NC,TAXIS,0,0,0,0,DTPLOT,3)
  CALL AXIS(0,4,5,15HTIME IN SECONDS,15,TAXIS,0,0,0,0,DTPLOT,0)
  CALL AXIS(0,1,5,BCD,NC,TAXIS,0,0,0,0,DTPLOT,3)
  CALL LINE(TPL,PLT1 ,NPOINT,1,1,1,JL,S)
  CALL LINE(TPL,PLT2 ,NPOINT,1,1,1,JL,S)
  CALL LINE(TPL,PLT3 ,NPOINT,1,1,1,JL,S)
  XNEW=TAXIS+5
  CALL PLOT(XNEW,0,0,-3)
LUM14000 293100000
LUM14010 293200000
LUM14020 293300000
LUM14030 293400000
LUM14040 293500000
LUM14050 293600000
LUM14060 293700000
LUM14070 293800000
LUM14080 293900000
LUM14090 294000000
LUM14100 294100000
LUM14110 294200000
LUM14120 294300000
LUM14130 294400000
LUM14140 294500000
LUM14150 294600000
LUM14160 294700000
LUM14170 294800000
LUM14180 294900000
LUM14190 295000000
LUM14200 295100000
LUM14210 295200000
LUM14220 295300000
LUM14230 295400000
LUM14240 295500000
LUM14250 295600000
LUM14260 295700000
LUM14270 295800000
LUM14280 295900000
LUM14290 296000000
LUM14300 296100000
LUM14310 296200000
LUM14320 296300000
LUM14330 296400000
LUM14340 296500000
LUM14350 296600000
LUM14360 296700000
LUM14370 296800000
LUM14380 296900000
297000000
297100000
297200000
297300000
LUM14420 297400000
LUM14430 297500000
LU
LUM14450 297600000
LUM14460 297700000
LUM14470 297800000
LUM14480 297900000
LUM14490 298000000
LUM14500 298100000

```

```

IF(PBLOCK.EQ.1.)GO TO 703
CALL SCALE(PLT4 ,NPOINT,S,VGP4 ,DYP4 ,1,1)
CALL SCALE(PLT5 ,NPOINT,S,VGP5 ,DYP5 ,1,1)
CALL SCALE(PLT6 ,NPOINT,S,VGP6 ,DYP6 ,1,1)
CALL AXIS(0,0,6,5,5HPLT4 ,5,2,0,90,0,VGP4 ,DYP4 ,0)
CALL AXIS(0,0,3,5,5HPLT5 ,5,2,0,90,0,VGP5 ,DYP5 ,0)
CALL AXIS(0,0,0,5,5HPLT6 ,5,2,0,90,0,VGP6 ,DYP6 ,0)
CALL AXIS(0,0,7,5,BCD,NC,TAXIS,0,0,0,DTPL0T,3)
CALL AXIS(0,0,4,5,15HTIME IN SECONDS,15,TAXIS,0,0,0,DTPL0T,0)
CALL AXIS(0,0,1,5,BCD,NC,TAXIS,0,0,0,DTPL0T,3)
CALL LINE(TPL,PLT4 ,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT5 ,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT6 ,NPOINT,1,1,1,JL,S)
XNEW=TAXIS+5
CALL PLOT(XNEW,0,0,-3)
IF(PBLOCK.EQ.2.)GO TO 703
8500 CALL SCALE(PLT7 ,NPOINT,S,VGP7 ,DYP7 ,1,1)
CALL SCALE(PLT8 ,NPOINT,S,VGP8 ,DYP8 ,1,1)
CALL SCALE(PLT9 ,NPOINT,S,VGP9 ,DYP9 ,1,1)
CALL AXIS(0,0,6,5,5HPLT7 ,5,2,0,90,0,VGP7 ,DYP7 ,0)
CALL AXIS(0,0,3,5,5HPLT8 ,5,2,0,90,0,VGP8 ,DYP8 ,0)
CALL AXIS(0,0,0,5,5HPLT9 ,5,2,0,90,0,VGP9 ,DYP9 ,0)
CALL AXIS(0,0,7,5,BCD,NC,TAXIS,0,0,0,DTPL0T,3)
CALL AXIS(0,0,4,5,15HTIME IN SECONDS,15,TAXIS,0,0,0,DTPL0T,0)
CALL AXIS(0,0,1,5,BCD,NC,TAXIS,0,0,0,DTPL0T,3)
CALL LINE(TPL,PLT7 ,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT8 ,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT9 ,NPOINT,1,1,1,JL,S)
XNEW=TAXIS+5
CALL PLOT(XNEW,0,0,-3)
IF(PBLOCK.EQ.3.)GO TO 703
CALL SCALE(PLT10,NPOINT,S,VGP10,DYP10,1,1)
CALL SCALE(PLT11,NPOINT,S,VGP11,DYP11,1,1)
CALL SCALE(PLT12,NPOINT,S,VGP12,DYP12,1,1)
CALL AXIS(0,0,6,5,5HPLT10,5,2,0,90,0,VGP10,DYP10,0)
CALL AXIS(0,0,3,5,5HPLT11,5,2,0,90,0,VGP11,DYP11,0)
CALL AXIS(0,0,0,5,5HPLT12,5,2,0,90,0,VGP12,DYP12,0)
CALL AXIS(0,0,7,5,BCD,NC,TAXIS,0,0,0,DTPL0T,3)
CALL AXIS(0,0,4,5,15HTIME IN SECONDS,15,TAXIS,0,0,0,DTPL0T,0)
CALL AXIS(0,0,1,5,BCD,NC,TAXIS,0,0,0,DTPL0T,3)
CALL LINE(TPL,PLT10,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT11,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT12,NPOINT,1,1,1,JL,S)
XNEW=TAXIS+5
CALL PLOT(XNEW,0,0,-3)
IF(PBLOCK.EQ.4.)GO TO 703
CALL SCALE(PLT13,NPOINT,S,VGP13,DYP13,1,1)
CALL SCALE(PLT14,NPOINT,S,VGP14,DYP14,1,1)
CALL SCALE(PLT15,NPOINT,S,VGP15,DYP15,1,1)
CALL AXIS(0,0,6,5,5HPLT13,5,2,0,90,0,VGP13,DYP13,0)
CALL AXIS(0,0,3,5,5HPLT14,5,2,0,90,0,VGP14,DYP14,0)

```

```

LUM14510 298200000
LUM14520 298300000
LUM14530 298400000
LUM14540 298500000
298600000
298700000
298800000
LUM14580 298900000
299000000
LUM14600 299100000
LUM14610 299200000
LUM14620 299300000
LUM14630 299400000
LUM14640 299500000
LUM14650 299600000
LUM14660 299700000
LUM14670 299800000
LUM14680 299900000
LUM14690 300000000
300100000
300200000
300300000
LUM14730 300400000
300500000
LUM14750 300600000
LUM14760 300700000
LUM14770 300800000
LUM14780 300900000
LUM14790 301000000
LUM14800 301100000
LUM14810 301200000
LUM14820 301300000
LUM14830 301400000
LUM14840 301500000
301600000
301700000
301800000
LUM14880 301900000
302000000
LUM14900 302100000
LUM14910 302200000
LUM14920 302300000
LUM14930 302400000
LUM14940 302500000
LUM14950 302600000
LUM14960 302700000
LUM14970 302800000
LUM14980 302900000
LUM14990 303000000
303100000
303200000

```

```

CALL AXIS(0.0,0.5,5HPLT15,5,2.0,90.0,90.0,90.0,90.0,DTPLT,0)
CALL AXIS(0.0,7.5,BCD,NC,TAXIS,0.0,0.0,DTPLT,3)
CALL AXIS(0.0,4.5,15HTIME IN SECONDS,15,TAXIS,0.0,0.0,DTPLT,0)
CALL AXIS(0.0,1.5,BCD,NC,TAXIS,0.0,0.0,DTPLT,3)
CALL LINE(TPL,PLT13,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT14,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT15,NPOINT,1,1,1,JL,S)
XNEW=TAXIS+5
CALL PLOT(XNEW,0.0,-3)
IF(PRLCK.EQ.5.IGD TO 703
CALL SCALE(PLT16,NPOINT,S,VGP16,DYP16,1,1)
CALL SCALE(PLT17,NPOINT,S,VGP17,DYP17,1,1)
CALL SCALE(PLT18,NPOINT,S,VGP18,DYP18,1,1)
CALL AXIS(0.0,6.5,5HPLT16,5,2.0,90.0,90.0,90.0,DTPLT,3)
CALL AXIS(0.0,3.5,5HPLT17,5,2.0,90.0,90.0,90.0,DTPLT,0)
CALL AXIS(0.0,0.5,5HPLT18,5,2.0,90.0,90.0,90.0,DTPLT,0)
CALL AXIS(0.0,7.5,BCD,NC,TAXIS,0.0,0.0,DTPLT,3)
CALL AXIS(0.0,4.5,15HTIME IN SECONDS,15,TAXIS,0.0,0.0,DTPLT,0)
CALL LINE(TPL,PLT16,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT17,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT18,NPOINT,1,1,1,JL,S)
XNEW=TAXIS+5
CALL PLOT(XNEW,0.0,-3)
IF(PBLOCK.EQ.6.IGD TO 703
CALL SCALE(PLT19,NPOINT,S,VGP19,DYP19,1,1)
CALL SCALE(PLT20,NPOINT,S,VGP20,DYP20,1,1)
CALL SCALE(PLT21,NPOINT,S,VGP21,DYP21,1,1)
CALL AXIS(0.0,6.5,5HPLT19,5,2.0,90.0,90.0,90.0,DTPLT,3)
CALL AXIS(0.0,3.5,5HPLT20,5,2.0,90.0,90.0,90.0,DTPLT,0)
CALL AXIS(0.0,0.5,5HPLT21,5,2.0,90.0,90.0,90.0,DTPLT,0)
CALL AXIS(0.0,7.5,BCD,NC,TAXIS,0.0,0.0,DTPLT,3)
CALL AXIS(0.0,4.5,15HTIME IN SECONDS,15,TAXIS,0.0,0.0,DTPLT,0)
CALL LINE(TPL,PLT19,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT20,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT21,NPOINT,1,1,1,JL,S)
XNEW=TAXIS+5
CALL PLOT(XNEW,0.0,-3)
IF(PBLOCK.EQ.7.IGD TO 703
CALL SCALE(PLT22,NPOINT,S,VGP22,DYP22,1,1)
CALL SCALE(PLT23,NPOINT,S,VGP23,DYP23,1,1)
CALL SCALE(PLT24,NPOINT,S,VGP24,DYP24,1,1)
CALL AXIS(0.0,6.5,5HPLT22,5,2.0,90.0,90.0,90.0,DTPLT,3)
CALL AXIS(0.0,3.5,5HPLT23,5,2.0,90.0,90.0,90.0,DTPLT,0)
CALL AXIS(0.0,0.5,5HPLT24,5,2.0,90.0,90.0,90.0,DTPLT,0)
CALL AXIS(0.0,7.5,BCD,NC,TAXIS,0.0,0.0,DTPLT,3)
CALL AXIS(0.0,4.5,15HTIME IN SECONDS,15,TAXIS,0.0,0.0,DTPLT,0)
CALL LINE(TPL,PLT22,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT23,NPOINT,1,1,1,JL,S)
CALL LINE(TPL,PLT24,NPOINT,1,1,1,JL,S)

```

```

3033000000
3034000000
3035000000
3036000000
3037000000
3038000000
3039000000
3040000000
3041000000
3042000000
3043000000
3044000000
3045000000
3046000000
3047000000
3048000000
3049000000
3050000000
3051000000
3052000000
3053000000
3054000000
3055000000
3056000000
3057000000
3058000000
3059000000
3060000000
3061000000
3062000000
3063000000
3064000000
3065000000
3066000000
3067000000
3068000000
3069000000
3070000000
3071000000
3072000000
3073000000
3074000000
3075000000
3076000000
3077000000
3078000000
3079000000
3080000000
3081000000
3082000000
3083000000

```

```

E 00030
E 00050
E 00060
E 00070
E 00080
E 00090
E 00100
E 00110
E 00120
E 00130
E 00140
E 00180
E 00200
E 00210
E 00220
E 00230
E 00240
E 00250
E 00260
E 00270
E 00280
E 00290
E 00330
E 00350
E 00360
E 00370
E 00380
E 00390
E 00400
E 00410
E 00420
E 00430
E 00440
E 00480
E 00500
E 00510
E 00520

```


CALL LINE(TPL,PLT24,NPOINT,1,1,1,JL,S)
XNEW=TAXIS+5
CALL PLOT(XNEW,0.0,-3)
703 CONTINUE
RETURN
END

E 00530 308400000
E 00540 308500000
E 00550 308600000
E 00560 308700000
E 00570 308800000
E 00580 308900000

SUBROUTINE SYM4(X,Y,HEIGHT,BCD,THETA,N)
CALL NOTATE(X,Y,HEIGHT,BCD,THETA,N)
RETURN
END

E	00590	309000000
E	00600	309100000
E	00610	309200000
E	00620	309300000

05

SUBROUTINE PLOT(A,B,I)
CALL CALPLT(A,B,I)
RETURN
END

E 00630 309400000
E 00640 309500000
E 00650 309600000
E 00660 309700000

```
SUBROUTINE SCALE(V,N,S,VORG,DV,JV,K)
DIMENSION V(1)
DO 10 I=1,N
  10 V(I)=(V(I)-VORG)/DV
  V(N+1)=0.
  V(N+2)=1.
RETURN
END
```

E	00670	3098000000
E	00680	3099000000
E	00690	3100000000
E	00700	3101000000
		3102000000
E	00730	3103000000
E	00740	3104000000
		3105000000

```
SUBROUTINE LINE(TPL,PLT,NPOINT,I,J,K,L,M)
DIMENSION TPL(1),PLT(1)
CALL LINPL(TPL,PLT,NPOINT,1,0,0,0,0)
RETURN
END
E 00750 310600000
E 00760 310700000
E 00770 310800000
E 00780 310900000
E 00790 311000000
```

```
SUBROUTINE AXIS(X0,Y0,BC),NC,S,THETA,VORG,DV,N)
DIMENSION BCD(1)
IF(VORG.NE.0.)VORG=-DV
IF(NC.EQ. 1)CALL AXES(X0,Y0,THETA,S,VORG,DV,1.,0.,1H,0.,1)
IF(NC.EQ. 5)CALL AXES(X0,Y0,THETA,S,VORG,DV,1.,0.,BCD,.1875,5)
IF(NC.EQ.15)CALL AXES(X0,Y0,THETA,S,VORG,DV,1.,0.,BCD,.1875,-15)
RETURN
END
```

```
E 00800 311100000
E 00810 311200000
E 00820 311300000
E 00830 311400000
E 00840 311500000
E 00850 311600000
E 00860 311700000
E 00860 311800000
```

```

SUBROUTINE PMPCOM(V,VDGT)
COMMON T
COMMON /INOUT/IN, IOUT,IOFF
IF(T.GT.0.1GG TO 100
READ(IN,1)V,VELCU,TIMCU,ACCMAG
1 FORMAT(4E15.8)
WRITE(IOUT,300)
300 FORMAT(#OPUMP COMMAND INPUT*)
WRITE(IOUT,2)V,VELCU,TIMCU,ACCMAG
2 FORMAT(RX,*,V*,14X,*VELCU*,12X,*TIMCU*,12X,*ACCMAG*/4E17.7)
A=V
100 IF(T.GT.TIMCU)GG TO 10
OUT=0.
V=A
VDOT=0.
10 CONTINUE
CALL VELCOM(T,VELCU,TIMCU,OUT,TIME0,TIME1,ACCO1,VELCO,ACCMAG,
VDGT,V)
*
200 RETURN
END

```

```

E 00870 311900000
E 00880 312000000
E 00890 312100000
E 00900 312200000
E 00910 312300000
E 00920 312400000
E 00930 312500000
E 00940 312600000
E 00950 312700000
E 00960 312800000
E 00970 312900000
E 00980 313000000
E 00990 313100000
E 01000 313200000
E 01010 313300000
E 01020 313400000
E 01030 313500000
E 01040 313600000
E 01050 313700000
E 01060 313800000

```

```

SUBROUTINE MUCOM(UJ,UJC,UJDD,L)
COMMON T
COMMON /INOUT/IN,IOUT,IOFF
DIMENSION UJ(3),UJD(3),UJDD(3),X(3,8,13),UJ0(3,3,8),UU(3,8),TU(3,8),
* ACCMAG(3,8),IAXIS(3,8),VELMAX(3,8),A(3,8)
COMMON /VAROUT/XX(17),UJ0
IF(T.GT.0.)GO TO 100
DO 8 I=1,3
  UJ(I)=0.
  UJD(I)=0.
  UJDD(I)=0.
DO 8 J=1,3
  UJ0(I,J,L)=0.
8 UJ0(I,J,L)=0.
  READ(IN,1)(IAXIS(I,L),I=1,3)
1 FORMAT(3I2)
  READ(IN,5)(UJ0(I,1,L),I=1,3)
  WRITE(IOUT,6)L,(UJ0(I,1,L),I=1,3)
6 FORMAT(*OMUCOM INPUT FOR MOVING MASS*,I4/* UJ =*,3E17.8)
DO 10 I=1,3
  IF(IAXIS(I,L).EQ.0)GO TO 10
  A(I,L)=UJ0(I,1,L)
  READ(IN,5)UU(I,L),TU(I,L),ACCMAG(I,L),VELMAX(I,L)
  WRITE(IOUT,7)I,UU(I,L),TU(I,L),ACCMAG(I,L),VELMAX(I,L)
7 FORMAT(* AXIS =*,I3/*
  * 11X,*VELMAX* /4E17.8)
5 FORMAT(4E15.8)
10 CONTINUE
100 CALL MCPY(UJ0(1,1,L),UJ,3,3,3)
DO 120 I=1,3
  IF(IAXIS(I,L).EQ.0)GO TO 120
  IF(T.GT.TU(I,L))GO TO 20
  UJ(I)=A(I,L)
  UJD(I)=0.
  UJDD(I)=0.
  X(I,L,1)=0.
20 CONTINUE
  CALL POSCOM(T,UJ(I,L),TU(I,L),X(I,L,1),X(I,L,2),X(I,L,3),X(I,L,4),
  * X(I,L,5),X(I,L,6),X(I,L,7),X(I,L,8),X(I,L,9),X(I,L,10),
  * X(I,L,11),X(I,L,12),X(I,L,13),ACCMAG(I,L),
  * VELMAX(I,L),UJDD(I),UJD(I),UJ(I) )
120 CONTINUE
  CALL MCPY(UJ,UJ0(1,1,L),3,3,3)
  RETURN
  END

```

E	01070	3139000000
E	01080	3140000000
E	01090	3141000000
E	01100	3142000000
E	01110	3143000000
E	01120	3144000000
E	01130	3145000000
E	01140	3146000000
E	01150	3147000000
E	01160	3148000000
E	01170	3149000000
E	01180	3150000000
E	01190	3151000000
E	01200	3152000000
E	01210	3153000000
E	01220	3154000000
E	01230	3155000000
E	01240	3156000000
E	01250	3157000000
E	01260	3158000000
E	01270	3159000000
E	01280	3160000000
E	01290	3161000000
E	01300	3162000000
E	01310	3163000000
E	01320	3164000000
E	01330	3165000000
E	01340	3166000000
E	01350	3167000000
E	01360	3168000000
E	01370	3169000000
E	01380	3170000000
E	01390	3171000000
E	01400	3172000000
E	01410	3173000000
E	01420	3174000000
E	01430	3175000000
E	01440	3176000000
E	01450	3177000000
E	01460	3178000000
E	01470	3179000000
E	01480	3180000000
E	01490	3181000000
E	01500	3182000000


```

SUBROUTINE TRIFQ(A,Y)
REAL A(1),Y(1)
COMMON /WINTER/INDIC8
COMMON /BOND/ M,L
EQUIVALENCE (SUN,SUM)
LI = L
MML=M-LI
MM1 = M - I
IF (INDIC8) 130,100,100
100 Y(LI) = Y(LI) / A(LI)
II = LI
IF(MML)105,125,105
DO 120 I = LI,MM1
II = II + I
SUM = -Y(I+I)
IJ = II
DO 110 J = LI,I
SUM = SUM + A(IJ)*Y(J)
110 IJ = IJ + I
II = IJ
120 Y(I+I) = -SUM / A(II)
125 IF (INDIC8) 170,140,170
130 II = ((MML+1)*(M+LI))/2
140 I = M
145 Y(I) = Y(I) / A(II)
II = II - I
I = I - I
IF (I - LI) 170,150,150
150 SUN = -Y(I+I)
IJ = II + LI
DO 160 J = LI,I
Y(J) = Y(J) + SUN*A(IJ)
160 IJ = IJ + I
GO TO 145
170 RETURN
END
SUBROUTINE FUTILE(A,N,NIX)
DIMENSION A(1)
DOUBLE PRECISION SUM
EQUIVALENCE (SUN,SUM)
KI = I
KK = 0
DO 210 K = 1,N
KK = KK + K
IK = KK
KK1 = KK - I
IF (KK1) 60,50,60
50 ASSIGN 100 TO LFAP

```

```

E 01510 318300000
E 01520 318400000
E 01530 318500000
E 01540 318600000
E 01550 318700000
E 01560 318800000
E 01570 318900000
E 01580 319000000
E 01590 319100000
E 01600 319200000
E 01610 319300000
E 01620 319400000
E 01630 319500000
E 01640 319600000
E 01650 319700000
E 01660 319800000
E 01670 319900000
E 01680 320000000
E 01690 320100000
E 01700 320200000
E 01710 320300000
E 01720 320400000
E 01730 320500000
E 01740 320600000
E 01750 320700000
E 01760 320800000
E 01770 320900000
E 01780 321000000
E 01790 321100000
E 01800 321200000
E 01810 321300000
E 01820 321400000
E 01830 321500000
E 01840 321600000
E 01850 321700000
E 01860 321800000
E 01870 321900000
E 01880 322000000
E 01890 322100000
E 01900 322200000
E 01910 322300000
E 01920 322400000
E 01930 322500000
E 01940 322600000
E 01950 322700000
E 01960 322800000
E 01970 322900000
E 01980 323000000
E 01990 323100000

```

```

60 TO 70
60 ASSIGN 80 TO LEAP
70 I1 = K1
80 I4 = K,N
SUM = -A(IK)
GO TO LEAP, (80,100)
80 IJ = I1
90 90 KJ = K1,KK1
SUM = SUM + A(IJ)*A(KJ)
90 IJ = IJ + 1
100 I1 = I1 + 1
IF (I - K) 120,105,120
105 DENOM = -SUM
IF (DENOM) 980,980,110
110 DENOM = -SQRT(DENOM)
A(IK) = -DENOM
GO TO 130
120 A(IK) = SUM / DFNOM
130 IK = IK + 1
140 CONTINUE
KI = K1 + K
210 CONTINUE
NIX = 0
220 RETURN
980 NIX = -K
GO TO 220
END
SUBROUTINE CONTRL(A,N,IFCON,LABCW)
DIMENSION A(1),GAMIS(3),GAMDIS(3),FAJ(3,16),XAJ(3,17)
* RC(3),KC8(3),RSS(3)
COMMON T,W(1000),HOLD(3),SAVE(3),
* G1(3,3),G2(3,3),G3(3,3)
COMMON /LABOR/WX(3), RI (900),TH(3,100),THD(3,100)
* /LOADS/ZZ(685),RDOT(3),WXDOT(3),XDD(6,100)
* /EXTRA/CC(15),EMC,TOT
COMMON /CONNECT/DUM3(26),GAM(3),GAMD(3)
COMMON /NEWCOM/EL(3),ELD(3),ELDD(3),ROR(3)
* /INOUT/IN,IOUT,IOFF
* /ALLCNT/IS,O(3),DL(3,3),DC(3,3),EML,XIL(3,3),XIC(3,3),
* YICS(10),YPRED(10),YDOT(10),NEQS,DO(3),XI(3,3),TAJ(3),
* WKT,TQLIM,WKDBRET,WMDMCM,WIBGIM,OICMAG
COMMON /VAROUT/EOL,DOIC,F3,F9,F10,F16,F4,F11,F15,DOI,EL03D,ELD3,
* ELDD3,OICD,ND
* ,OIC,NCMG
* ,UJDDUM(78)
* ,F1,F2,F5,F6,F7,F8,F12,F13,F14
N6=6*N
IENT=0
DO 5 I=1,N6
5 A(I)=0.
IF(LABCW.LT.0)GO TO 99
E 02000 323200000
E 02010 323300000
E 02020 323400000
E 02030 323500000
E 02040 323600000
E 02050 323700000
E 02060 323800000
E 02070 323900000
E 02080 324000000
E 02090 324100000
E 02100 324200000
E 02110 324300000
E 02120 324400000
E 02130 324500000
E 02140 324600000
E 02150 324700000
E 02160 324800000
E 02170 324900000
E 02180 325000000
E 02190 325100000
E 02200 325200000
E 02210 325300000
E 02220 325400000
E 02230 325500000
E 02240 325600000
E 02250 325700000
E 02260 325800000
E 02270 325900000
E 02280 326000000
E 02290 326100000
E 02300 326200000
E 02310 326300000
E 02320 326400000
E 02330 326500000
E 02340 326600000
E 02350 326700000
E 02360 326800000
E 02370 326900000
E 02380 327000000
E 02390 327100000
E 02400 327200000
E 02410 327300000
E 02420 327400000
E 02430 327500000
E 02440 327600000
E 02450 327700000
E 02460 327800000
E 02470 327900000
E 02480 328000000
E 02490 328100000
E 02500 328200000

```

```

IF(IFCCN.EQ.0)GO TO 99
IF(T.GT.0)GO TO 20
IF(NFQS.NE.3)NEQS=0
NEQS=NEQS+4
OI=0(1)
OICI=01C
EL03I=EL(3)
DO 140 I=1,4
XAJ(1,I)=-XJ1
XAJ(2,I)=0.
XAJ(3,I)=RI(3)
XAJ(1,I+4)=-XJ1
XAJ(2,I+4)=0.
XAJ(3,I+4)=RI(15)
XAJ(1,I+8)=XJ1
XAJ(2,I+8)=0.
XAJ(3,I+8)=RI(15)
XAJ(1,I+12)=XJ1
XAJ(2,I+12)=0.
140 XAJ(3,I+12)=RI(3)
RC(1)=DL(3,2)
RC(2)=DL(1,3)
RC(3)=DL(2,1)
SC=1./EML
CALL SCALR(SC,RC,RC,1)
RCR(1)=DC(3,2)
RCB(2)=DC(1,3)
RCB(3)=DC(2,1)
SC=1./EMC
CALL SCALR(SC,RCB,RCB,1)
CALL ADD(ROB,RCB,HOLD,1)
HOLD(2)=-HOLD(2)
HOLD(3)=-HOLD(3)
CALL SCALR(EMC,HOLD,HOLD,1)
CALL SCALR(EML,RC,SAVE,1)
CALL ADD(HOLD,SAVE,HOLD,1)
SC=1./(EML+EMC)
CALL SCALR(SC,HOLD,RSS,1)
GO TO 21
20 IF(T.LE.TX83CU.OR.EL(3).EQ.XB3CU)GO TO 25
21 CALL ADD(XIL,XIC,XI,3)
CALL GAMMA(RC,G1)
CALL MULT(G1,G1,G2,3)
CALL SUBTR(RC,RSS,HOLD,1)
CALL GAMMA(HOLD,G1)
CALL MULT(G1,G1,G3,3)
CALL SUBTR(G2,G3,G2,3)
CALL SCALR(EML,G2,G2,3)
CALL ADD(XI,G2,XI,3)
CALL GAMMA(RCB,G1)
CALL MULT(G1,G1,G2,3)

```

E	02510	3283000000
E	02520	3284000000
E	02530	3285000000
E	02540	3286000000
E	02550	3287000000
E	02560	3288000000
E	02570	3289000000
E	02580	3290000000
E	02590	3291000000
E	02600	3292000000
E	02610	3293000000
E	02620	3294000000
E	02630	3295000000
E	02640	3296000000
E	02650	3297000000
E	02660	3298000000
E	02670	3299000000
E	02680	3300000000
E	02690	3301000000
E	02700	3302000000
E	02710	3303000000
E	02720	3304000000
E	02730	3305000000
E	02740	3306000000
E	02750	3307000000
E	02760	3308000000
E	02770	3309000000
E	02780	3310000000
E	02790	3311000000
E	02800	3312000000
E	02810	3313000000
E	02820	3314000000
E	02830	3315000000
E	02840	3316000000
E	02850	3317000000
E	02860	3318000000
E	02870	3319000000
E	02880	3320000000
E	02890	3321000000
E	02900	3322000000
E	02910	3323000000
E	02920	3324000000
E	02930	3325000000
E	02940	3326000000
E	02950	3327000000
E	02960	3328000000
E	02970	3329000000
E	02980	3330000000
E	02990	3331000000
E	03000	3332000000
E	03010	3333000000

```

DD 10 I=1,3
10 HOLD(I)=R08(I)+RCB(I)+RSS(I)
   HOLD(I)=HOLD(I)-2.*RSS(I)
   CALL GAMMA(HOLD,G1)
   CALL MULT(G1,G1,G3,3)
   CALL SUBTP(G2,G3,G1,3)
   CALL SCALR(EMC,G1,G1,3)
   CALL ADD(XI,G1,XI,3)
   GO TO 25
   ENTRY EARLY
   IENT=1
25 CONTINUE
   CALL ADD(GAM,TH(1,IS),GAMIS,1)
   CALL ADD(GAMD,THD(1,IS),GAMDIS,1)
   CALL GAMMA(TH(1,IS),G1)
   CALL MULT(G1,WXDOT,HOLD,1)
   CALL SUBTR(WXDOT,HOLD,HOLD,1)
   CALL GAMMA(THD(1,IS),G1)
   CALL MULT(G1,WX,SAVE,1)
   DD 30 I=1,3
30 DD(I)=HOLD(I)-SAVE(I)+XDD(I+3,IS)
   IF(IENT.EQ.1)RETURN
   GO TO 89
   ENTRY LLDLDD
   CALL CWCOM(T,XB3CU,ACC33C,VELM8C,ELDD(3),ELD(3),EL(3))
   GO TO 99
89 CONTINUE
   CALL SPNCOM(T,OICU,TOICU,ACCOIC,FJET,XAJ,XI,OIC,OICMAG)
   CALL SPNCTR(OIC,O,EOIDB,FJET,OICMAG,FAJ)
   OICD=OIC-OICI
   DD=O(1)-O1
   CALL ATTCTR(GAMIS,GAMDIS,ETDR,DETMX,XAJ,FJET,FAJ)
   CALL WBLCTR
   F1 =FAJ(2,1)
   F2 =FAJ(2,2)
   F3 =FAJ(2,3)
   F4 =FAJ(1,4)
   F5 =FAJ(2,5)
   F6 =FAJ(2,6)
   F7 =FAJ(2,7)
   F8 =FAJ(1,8)
   F9 =FAJ(2,9)
   F10 =FAJ(2,10)
   F11 =FAJ(2,11)
   F12 =FAJ(1,12)
   F13 =FAJ(2,13)
   F14 =FAJ(2,14)
   F15 =FAJ(2,15)
   F16 =FAJ(1,16)
   EL03D =EL(3) -EL03I
   EL03 =ELD(3)

```

```

E 03020 333400000
E 03030 333500000
E 03040 333600000
E 03050 333700000
E 03060 333800000
E 03070 333900000
E 03080 334000000
E 03090 334100000
E 03100 334200000
E 03110 334300000
E 03120 334400000
E 03130 334500000
E 03140 334600000
E 03150 334700000
E 03160 334800000
E 03170 334900000
E 03180 335000000
E 03190 335100000
E 03200 335200000
E 03210 335300000
E 03220 335400000
E 03230 335500000
E 03240 335600000
E 03250 335700000
E 03260 335800000
E 03270 335900000
E 03280 336000000
E 03290 336100000
E 03300 336200000
E 03310 336300000
E 03320 336400000
E 03330 336500000
E 03340 336600000
E 03350 336700000
E 03360 336800000
E 03370 336900000
E 03380 337000000
E 03390 337100000
E 03400 337200000
E 03410 337300000
E 03420 337400000
E 03430 337500000
E 03440 337600000
E 03450 337700000
E 03460 337800000
E 03470 337900000
E 03480 338000000
E 03490 338100000
E 03500 338200000
E 03510 338300000
E 03520 338400000

```

```

ELDD3=ELDD(3)
A( 1)=FAJ(1,4)+FAJ(1,16)
A( 2)=FAJ(2,1)+FAJ(2,2)+FAJ(2,3)+FAJ(2,13)+FAJ(2,14)+FAJ(2,15)
A( 3)=0.
A( 4)=0.
A( 5)=0.
A( 6)=XJ1*(-FAJ(2,1)-FAJ(2,2)-FAJ(2,3)+FAJ(2,13)+FAJ(2,14)+FAJ(2,15))
*5)
A(25)=FAJ(1,8)+FAJ(1,12)
A(26)=FAJ(2,5)+FAJ(2,6)+FAJ(2,7)+FAJ(2,10)+FAJ(2,11)
A(27)=0.
A(28)=0.
A(29)=0.
A(30)=XJ1*(-FAJ(2,5)-FAJ(2,6)-FAJ(2,7)+FAJ(2,9)+FAJ(2,10)+FAJ(2,11))
*)
IL=6*IS-3
DO 40 I=1,3
40 A(IL+I)=TAJ(I)
GO TO 99
ENTRY CONTD
C
C GENERAL INPUT
C
E01=0.
DO 88 I=1,3
DO 88 J=1,16
88 FAJ(I,J)=0.
READ(IN,2)IS,FJET
2 FORMAT(13,E15.8)
WRITE(1OUT,102)IS,FJET
102 FORMAT(10)CONTROLS INPUT , SENSOR ON MASS POINT*,I4,* , FJET=*,E15.
*8)
C CWCOM
READ(IN,1)XB3CU, TXB3CU, ACCB3C, VELMBC
WRITE(1OUT,103)XB3CU, TXB3CU, ACCB3C, VELMBC
103 FORMAT(8) COUNTERWEIGHT COMMAND*/* LENGTH UPDATE TIME OF UPDATE
* ACCEL. MAG VEL. MAX*/E16.7, E17.7, E17.7, E15.7)
C SPNCOM
READ(IN,1)O1C, TO1CU, O1CU, ACCO1C
O1CMAG=ABS(O1C)
WRITE(1OUT,104)O1C, O1CU, ACCO1C, TO1CU
104 FORMAT(8) SPIN COMMAND*/* ANG. VEL. COMMAND ANG. VEL. UPDATE
* ACCEL MAG*/9X,*TIME OF UPDATE*/4(2X,E14.7,4X))
C SPNCTR
READ(IN,1)E01DB
WRITE(1OUT,105)E01DB
105 FORMAT(8) SPIN CONTROL*/* SPIN RATE ERROR DEAD BAND=*,E15.8)
C ATTCR
READ(IN,1)ETDB, NETMAX, XJ1
WRITE(1OUT,106)ETDB, DETMAX, XJ1
106 FORMAT(8) ATTITUDE CONTROL*/4X,*DEAD BAND*,6X,*MAX. ANG. VEL.
JETE 04030
338500000
338600000
338700000
338800000
338900000
339000000
339100000
339200000
339300000
339400000
339500000
339600000
339700000
339800000
339900000
340000000
340100000
340200000
340300000
340400000
340500000
340600000
340700000
340800000
340900000
341000000
341100000
341200000
341300000
341400000
341500000
341600000
341700000
341800000
341900000
342000000
342100000
342200000
342300000
342400000
342500000
342600000
342700000
342800000
342900000
343000000
343100000
343200000
343300000
343400000
343500000

```

```

C      * MOMENT ARM*/E15.7,3X,E14.7,3X,E14.7)
      WBLCTR
      READ(IN,1)  YICS(2),YICS(1),WKT,TQLIM,WKBET,WMMCM,WIBGIM
      WRITE(OUT,701)YICS(2),YICS(1),WKT,TQLIM,WKBET,WMMCM,WIBGIM
      701 FORMAT(= WOBBLE DAMPING*/8X,=BET*,12X,=DBET*,13X,=KT*,13X,=TQLIM*,E
      =11X,=KOBET*,10X,=MOMCMG*,7X,=GIMBAL INERTIA* / 7E16.7)
      I FORMAT(4E15.8)
      99 RETURN
      END

```

```

E 04040 3436000000
E 04050 3437000000
E 04060 3438000000
E 04070 3439000000
E 04080 3440000000
E 04090 3441000000
E 04100 3442000000
E 04110 3443000000
E 04120 3444000000

```

```

SUBROUTINE ATTCTR(T,DT,ETDB,DETMX,XAJ, FJET, FAJ)
THIS SUBROUTINE GENERATES THE FORCES APPLIED BY JETS
TO CONTROL THE ATTITUDE OF THE VEHICLE AS MEASURED BY
EULER ANGLES.
T =THETA,EULER ANGLES
DT =DERIVATIVE OF THETA
ETDB =DEAD BAND OF ET
DETMX=DERIVATIVE OF ERROR,THETA,MAXIMUM VALUE
ACCTS =ACCELERATION MAGNITUDE USED TO COMPUTE PARABOLIC
SWITCHING CURVE
FAJ =FORCES EXERTED BY JETS LOCATED AT POINTS AJ

DIMENSION T(3),DT(3),XAJ(3,17),WM11(3,3),FAJ(3,16),FBJ(3,16),
1 ACCTS(3),ET(3),DET(3),ACCT(3)
COMMON /ALLCNT/DUM1(75),WM11,DUM2(8),D1CMAG
IF(D1CMAG)192,61,192
61 DO 181 J=1,16
DO 181 I=1,3
181 FAJ(I,J)=0.
ACCTS(1)=FJET*(XAJ(3,13)-XAJ(3,10))/WM11(1,1)
ACCTS(2)= FJET*(XAJ(3,4)-XAJ(3,12))/WM11(2,2)
ACCTS(3)= FJET*(XAJ(1,15)-XAJ(1,1))/WM11(3,3)
DO 191 J=1,3
ET(J)=T(J)-0.
DET(J)=DT(J)-0.
CALL PCSCTR(ET(J),ETDR,DET(J),DETMX,ACCTS(J),ACCT(J))
IF(J-2)182,185,188
182 IF(ACCT(1))184,191,183
183 FAJ(2,13)=-FJET
FAJ(2,10)=+FJET
GO TO 191
184 FAJ(2,14)=+FJET
FAJ(2,9) =-FJET
GO TO 191
185 IF(ACCT(2))187,191,186
186 FAJ(1,4) =+FJET
FAJ(1,12)=-FJET
GO TO 191
187 FAJ(1,16)=-FJET
FAJ(1,8) =+FJET
GO TO 191
188 IF(ACCT(3))190,191,189
189 FAJ(2,15)=+FJET
FAJ(2,1) =-FJET
GO TO 191
190 FAJ(2,11)=-FJET
FAJ(2,6)=FJET
191 CONTINUE
GO TO 192

```

344500000	E	04130
344600000	E	04140
344700000	E	04150
344800000	E	04160
344900000	E	04170
345000000	E	04180
345100000	E	04190
345200000	E	04200
345300000	E	04210
345400000	E	04220
345500000	E	04230
345600000	E	04240
345700000	E	04250
345800000	E	04260
345900000	E	04270
346000000	E	04280
346100000	E	04290
346200000	E	04300
346300000	E	04310
346400000	E	04320
346500000	E	04330
346600000	E	04340
346700000	E	04350
346800000	E	04360
346900000	E	04370
347000000	E	04380
347100000	E	04390
347200000	E	04400
347300000	E	04410
347400000	E	04420
347500000	E	04430
347600000	E	04440
347700000	E	04450
347800000	E	04460
347900000	E	04470
348000000	E	04480
348100000	E	04490
348200000	E	04500
348300000	E	04510
348400000	E	04520
348500000	E	04530
348600000	E	04540
348700000	E	04550
348800000	E	04560
348900000	E	04570
349000000	E	04580
349100000	E	04590
349200000	E	04600
349300000	E	04610

E	04620	349400000
E	04630	349500000

192 RETURN
END


```

SURROUTINE WBLCTR
THIS SUBROUTINE GENERATES THE CMG GIMBAL ANGLE ACCELERATION.
THIS ACCELERATION IS INTEGRATED TO GET THE CMG GIMBAL ANGLE
RATE AND POSITION. THE TORQUES EXERTED BY THE CMG ON THE
VEHICLE ARE ALSO COMPUTED.
O =OMEGA,ANGULAR VELOCITY OF LAB
WM11 =MOMENT OF INERTIA, STATION INCLUDING MOVING PARTS
RBT =CMG GIMBAL ANGLE, REFERENCE COORDINATE IS LAB AXIS 3
DBET =CMG GIMBAL ANGLE RATE
DBETMX=MAXIMUM CMG GIMBAL ANGLE RATE (USED IN SHORTEST PATH LOGIC)
WKT =CONSTANT, MULTIPLIES ERROR ERRF TO GIVE TORQUE TQKGM
TQLIM =TORQUE LIMIT
WKDBET=CONSTANT, MULTIPLIES DBET TO GIVE TQFDBK
WMOMCM=MOMENT OF MOMENTUM, CMG
WIBGIM=CMG GIMBAL INERTIA (SAME FOR ALL 3 VEHICLE AXES, ROTOR
INERTIA NOT INCLUDED ALCNG ROTOR AXIS)
TIME= TIME
TIMEL = TIME ONE IRRATION AGO
DOBET =CMG GIMBAL ANGLE ACCELERATION
TAJ =TORQUES EXERTED BY CMG ON LAB

COMMON TIME
COMMON /ALLCNT/IS,O,DLC(37),YICS(10),YPRED(10),YDOT(10),NEQS,DO,
* WM11,TAJ,WKT,TQLIM,WKDBET,WMOMCM,WIBGIM,DLCMAG
* ,RETDES
COMMON /VAROUT/DUM(16),NCMG
DIMENSION O(3),WM11(3,3),TAJ(3),DO(3)
EQUIVALENCE (BET,YPRED(2)),(DBET,YPRED(1)),(ERRKTI,YPRED(3))
* ,(ERRLLI,YPRED(4))

TIME=TIME
IF(TIME .NE. 0.1GD TO 10
RET=YICS(2)
DBET=YICS(1)

C
C FDR TEST
C
DBETMX=TQLIM/WKDBET
WLEAD=10.*WIBGIM/WKDBET
RETDES=0.
NCMG=0
ERRKTI=0.
ERRLLI=WKDBET*DBET
TIMEL=-0.025
10 IF(OLCMAG-0.02193,84,84
93 DOBET=0.
90 83 I=1,3
83 TAJ(I)=0.
GO TO 94

```

```

E 04640 3496000000
E 04650 3497000000
E 04660 3498000000
E 04670 3499000000
E 04680 3500000000
E 04690 3501000000
E 04700 3502000000
E 04710 3503000000
E 04720 3504000000
E 04730 3505000000
E 04740 3506000000
E 04750 3507000000
E 04760 3508000000
E 04770 3509000000
E 04780 3510000000
E 04790 3511000000
E 04800 3512000000
E 04810 3513000000
E 04820 3514000000
E 04830 3515000000
E 04840 3516000000
E 04850 3517000000
E 04860 3518000000
E 04870 3519000000
E 04880 3520000000
E 04890 3521000000
E 04900 3522000000
E 04910 3523000000
E 04920 3524000000
E 04930 3525000000
E 04940 3526000000
E 04950 3527000000
E 04960 3528000000
E 04970 3529000000
E 04980 3530000000
E 04990 3531000000
E 05000 3532000000
E 05010 3533000000
E 05020 3534000000
E 05030 3535000000
E 05040 3536000000
E 05050 3537000000
E 05060 3538000000
E 05070 3539000000
E 05080 3540000000
E 05090 3541000000
E 05100 3542000000
E 05110 3543000000
E 05120 3544000000

```

```

84 CONTINUE
2 WMU=SQRT((WM11(1,1)-WM11(3,3))*(WM11(1,1)-WM11(2,2))/
  (WM11(2,2)*WM11(3,3)))
1 SWITCH=3.1415926*(1.-(WMU#0(1)/DRETMX))
  Q23=0.
  IF(O(3) .EQ. 0.0 .AND. O(2) .EQ. 0.0)GO TO 6
5 Q23=ATAN2(O(3),C(2))
6 EI=0.5*(WM11(2,2)*(O(2))**2)+((WM11(1,1)-WM11(3,3))/
  (WM11(1,1)-WM11(2,2))*WM11(3,3)*(O(3))**2)
  F2=WMOMCM#O(1)
  E3=10.*(EI/E2)
  IF(BET)200,202,202
200 BET=BET+6.2831853
202 BETDE=023-1.5707963
  IF(BETDE)204,215,215
204 BETDE=BETDE+6.2831853
215 IF(NCMG .EQ. 1)GO TO 206
  IF(E3-.01)208,205,205
205 SPCASE=2.*WMU#O(1)*(TIME-TIMEL)
  IF(BETDE .LE. SPCASE)GO TO 213
  IF(BETDE-BET)208,208,211
213 BBETDE=BETDE+6.2831853
206 IF(E3-.001)207,212,212
207 NCMG=0
  ERRKTI=0.
  ERRLLI=WKDBET#DBET
208 ERBET=-C(1)-DBFT
  ERKT=WKT#ERDBET
  ERRLL=ERRKTI+WLEAD*ERRKT
  SINBET=SIN(BET)
  COSBET=COS(BET)
  TQPASS=WMCMCM#O(3)*COSBET-O(2)*SINBET)
  TQKIM=ERKLLI-TQPASS
  IF(ABS(TQKIM)-TQLIM)622,622,621
211 NCMG=1
  ERKTI=WKDBET#DBET
212 BETDES=BETDE
604 ERBET=BETDES-BET
  IF(ERBET)607,610,605
605 IF(ERBET-SWITCH)610,610,606
606 ERBET=ERBET-6.2831853
  GO TO 610
607 ERBET=ERBET+6.2831853
  IF(ERBET-SWITCH)610,610,609
609 ERBET=ERBET-6.2831853
610 ERRF=ERBET
  C
  C
  C
  GIMBAL DYNAMICS
624 SINBET=SIN(BET)

```

```

E 05130 354500000
E 05140 354600000
E 05150 354700000
E 05160 354800000
E 05170 354900000
E 05180 355000000
E 05190 355100000
E 05200 355200000
E 05210 355300000
E 05220 355400000
E 05230 355500000
E 05240 355600000
E 05250 355700000
E 05260 355800000
E 05270 355900000
E 05280 356000000
E 05290 356100000
E 05300 356200000
E 05310 356300000
E 05320 356400000
E 05330 356500000
E 05340 356600000
E 05350 356700000
E 05360 356800000
E 05370 356900000
E 05380 357000000
E 05390 357100000
E 05400 357200000
E 05410 357300000
E 05420 357400000
E 05430 357500000
E 05440 357600000
E 05450 357700000
E 05460 357800000
E 05470 357900000
E 05480 358000000
E 05490 358100000
E 05500 358200000
E 05510 358300000
E 05520 358400000
E 05530 358500000
E 05540 358600000
E 05550 358700000
E 05560 358800000
E 05570 358900000
E 05580 359000000
E 05590 359100000
E 05600 359200000
E 05610 359300000
E 05620 359400000
E 05630 359500000

```

```

COSBET=COS(BET)
TOPASS=WMDMCM*(O(3)*COSBET-O(2)*SINBET)
ERRKT=WKT*ERRF
ERRLL=ERRKTI+WLEAD*ERRKT
TQKGIM=ERRLL-TQPASS
IF(ABS(TQKGIM)-TOLIM) 622,622,621
621 TQLGIM=SIGN(TQLIM,TQKGIM)
GO TO 623
622 TQLGIM=TQKGIM
623 TQFDBK=WKDBET*DBET
TQTGIM=TQLGIM-TQFDBK
TQGIM=TQTGIM+TQPASS
DDBETP=TQGIM/WIRGIM
DDBET=DDBETP-DQ(1)
      BET IS COMPUTED IN INTEGRATION SECTION
      DBET IS COMPUTED IN INTEGRATION SECTION
C
C
C
C
C
TORQUES ON VEHICLE DUE TO CMG
E1=DRET+O(1)
TAJ(1)=WMDMCM*(-SINBET*O(2)+COSBET*O(3))-WIRGIM*(DO(1)+DDBET)
TAJ(2)=WMDMCM*SINBET*E1-WIRGIM*(DO(2)+O(3)*DBET)
TAJ(3)=-WMDMCM*COSBET*E1-WIRGIM*(DO(3)+O(2)*DBET)
C
94 IF(TIME.GT.O.160 TO 96
YICS(3)=ERRKTI
YICS(4)=ERRLLI
96 YDOT(1)=DDBET
YDOT(2)=DBET
YDOT(3)=ERRKT
YDOT(4)=ERRLL
RETURN
END

```

```

E 05640 359600000
E 05650 359700000
E 05660 359800000
E 05670 359900000
E 05680 360000000
E 05690 360100000
E 05700 360200000
E 05710 360300000
E 05720 360400000
E 05730 360500000
E 05740 360600000
E 05750 360700000
E 05760 360800000
E 05770 360900000
E 05780 361000000
E 05790 361100000
E 05800 361200000
E 05810 361300000
E 05820 361400000
E 05830 361500000
E 05840 361600000
E 05850 361700000
E 05860 361800000
E 05870 361900000
E 05880 362000000
E 05890 362100000
E 05900 362200000
E 05910 362300000
E 05920 362400000
E 05930 362500000
E 05940 362600000
E 05950 362700000
E 05960 362800000

```

```

SURROUTINE SPNCOM(TIME,OICU,TOICU,ACCOIC,FJET,XAJ,WMI
1 OICMAG)
DIMENSION XAJ(3,17),WMI(3,3)
COMMON /VAROUT/ED1,DOIC
IF(TIME.EQ.0.)A=OIC
IF(TIME.GT.TOICU)GO TO 10
OIC=A
DOIC=0.
OUTO=0.
10 CONTINUE
CALL VELCOM(TIME,OICU,TOICU,OUTO,TIME00,TIME10,ACCO10,
1 OICMAG=ABS(OIC)
RETURN
END

```

	E	OIC,			
	05970				3629000000
	05980				3630000000
	05990				3631000000
	06000				3632000000
	06010				3633000000
	06020				3634000000
	06030				3635000000
	06040				3636000000
	06050				3637000000
	06060				3638000000
	06070				3639000000
	06080				3640000000
	06090				3641000000
	06100				3642000000
	06110				3643000000

```

SUBROUTINE SPNCTR(OIC, O, EO1D8, FJET, OICMAG, FAJ)
THIS SUBROUTINE GENERATES THE FORCES EXERTED BY THE JETS
ON THE VEHICLE TO CONTROL THE SPIN RATE ABOUT AXIS 1.
OIC =OMEGA 1 COMMAND (SPIN RATE ABOUT LAB AXIS 1)
O =OMEGATANGULAR VELOCITY VECTOR OF LAB)
EO1D8 =ERROR, OMEGA 1, DEAD BAND
FAJ =FORCES EXERTED BY JETS ON VEHICLE. JETS ARE LOCATED
AT POINTS AJ IN LAB.
FJET =THRUST OF JET

DIMENSION O(3), FAJ(3, 16)
COMMON /VAROUT/EO1
IF(OICMAG)61, 196, 61
61 DO 181 J=1, 16
DO 181 I=1, 3
181 FAJ(I, J)=0.
EO1=O(1)-OIC
CALL VELCTR(EO1, EO1D8, ACCNO1)
IF(ACCNO1)195, 196, 194
194 FAJ(2, 13)=-FJET
FAJ(2, 10)=+FJET
FAJ(2, 3)=-FJET
FAJ(2, 7)=+FJET
GO TO 196
195 FAJ(2, 14)=+FJET
FAJ(2, 9 )=-FJET
FAJ(2, 2)=+FJET
FAJ(2, 5)=-FJET
C
196 RETURN
END
E 06120 3644000000
E 06130 3645000000
E 06140 3646000000
E 06150 3647000000
E 06160 3648000000
E 06170 3649000000
E 06180 3650000000
E 06190 3651000000
E 06200 3652000000
E 06210 3653000000
E 06220 3654000000
E 06230 3655000000
E 06240 3656000000
E 06250 3657000000
E 06260 3658000000
E 06270 3659000000
E 06280 3660000000
E 06290 3661000000
E 06300 3662000000
E 06310 3663000000
E 06320 3664000000
E 06330 3665000000
E 06340 3666000000
E 06350 3667000000
E 06360 3668000000
E 06370 3669000000
E 06380 3670000000
E 06390 3671000000
E 06400 3672000000
E 06410 3673000000
E 06420 3674000000

```

```

C SURROUTINE VELCTR(EDOT,EDOTDB,ACCNOW)
C THIS SUBROUTINE GENERATES VELOCITY CONTROL.
C EDOT ERROR RATE(RATE - RATE COMMAND)
C EDOTDB ERROR RATE DEAD BAND
C ACCNOW ACCELERATION TO BE APPLIED NOW (+1.,0.,OR -1.)
C
COMMON T
IF(T.EQ.0.)ACCNOW=0.
IF(EDOT-EDOTDB)10,5,5
5 ACCNOW=-1.
GO TO 30
10 IF(EDOT + EDOTDB)20,20,15
20 ACCNOW=+1.
GO TO 30
15 IF(EDOT)25,26,26
26 IF(ACCNOW .EQ. -1.)GO TO 5
ACCNOW=0.
GO TO 30
25 IF(ACCNOW .EQ. +1.)GO TO 20
ACCNOW=0.
30 RETURN
END
E 06430 3675000000
E 06440 3676000000
E 06450 3677000000
E 06460 3678000000
E 06470 3679000000
E 06480 3680000000
3681000000
3682000000
E 06490 3683000000
E 06500 3684000000
E 06510 3685000000
E 06520 3686000000
E 06530 3687000000
E 06540 3688000000
E 06550 3689000000
E 06560 3690000000
E 06570 3691000000
E 06580 3692000000
E 06590 3693000000
E 06600 3694000000
E 06610 3695000000
E 06620 3696000000

```

```

SUBROUTINE POSCOM(TIME,POSCU,TIMCU,OUT,TIME0,TIME1,TIME2,TIME3,
1 ACC01,ACC12,ACC23,POSC0,POSC1,POSC2,VELC1,VELC2,
1 ACCMAG,VELMAX,ACCMN,VELCMN,POSCMN)
C THIS SUBROUTINE GENERATES A POSITION COMMAND
C TIME = TIME
C POSCU = POSITION COMMAND UPDATE
C TIMCU = TIME OF POSITION COMMAND UPDATE
C OUT = 0. FIRST UPDATE NOT YET ACTIVATED
C 1. FIRST UPDATE DATA COMPUTED
C ACCMAG=MAGNITUDE OF NONZERO ACCELERATION COMMAND
C VELMAX= MAXIMUM VELOCITY OF COMMAND
C TIME0 COMMENCE ACCELERATION
C TIME1 END ACCELERATION, COMMENCE COAST
C TIME2 END COAST, COMMENCE DECELERATION
C TIME3 END DECELERATION, OBJECT HAS ARRIVED
C ACC01 ACCELERATION FROM TIME0 TO TIME1
C ACC12 ACCELERATION FROM TIME1 TO TIME2
C ACC23 ACCELERATION FROM TIME2 TO TIME3
C POSC0 =POSITION COMMAND AT TIME0
C POSC1 =POSITION COMMAND AT TIME1
C POSC2 =POSITION COMMAND AT TIME2
C VELC1=VELOCITY COMMAND AT TIME1
C VELC2 =VELOCITY COMMAND AT TIME2
C ACCCMN= ACCELERATION COMMAND
C VELCMN= VELOCITY COMMAND
C POSCMN= POSITION COMMAND
C
C IF(TIME .NE. 0.)GO TO 143
C OUT=0.
C ACCCMN=0.
C VELCMN=0.
143 IF(TIME-TIMCU)162,144,144
144 IF(OUT)145,145,160
145 ERROR=POSCU-POSCMN
ABSERR=ABS(ERROR)
C
2 TLHAF=SQRT(ABSERR/ACCMAG)
VELHAF=SQRT(ABSERR*ACCMAG)
IF(VELHAF-VELMAX)4,4,10
C
4 TIME0=TIMCU
TIME1=TIME0+TLHAF
TIME2=TIME1
TIME3=TIME2+TLHAF
ACC01=(ERROR/ABSERR)*ACCMAG
ACC12=0.
ACC23=(-ERROR/ABSERR)*ACCMAG
OUT=1.

```

```

C
GO TO 160
10 T1=VELMAX/ACCMAG
T2=ABSERR/VELMAX
TIME0=TIMCU
TIME1=TIME0+T1
TIME2=TIME0+T2
TIME3=TIME2+T1
ACCO1=(ERROR/ABSERR)*ACCMAG
ACC12=0.
ACC23=(-ERROR/ABSERR)*ACCMAG
OUT=1.
160 IF((TIME-TIME3))150,159,159
150 IF((TIME-TIME2))153,50,50
50 IF(ACCCMN .EQ. ACC23)GO TO 58
IF(ACCCMN .EQ. ACC01)GO TO 52
POSCMN=POSCI+VELC1*(TIME2-TIME1)
GO TO 54
52 VELCMN=ACCO1*(TIME1-TIME0)
POSCMN=POSC0+0.5*ACCO1*((TIME1-TIME0)**2)
POSCMN=POSCMN+VELCMN*(TIME2-TIME1)
54 VELC2=VELCMN
POSC2=POSCMN
ACCCMN=ACC23
58 VELCMN=VELC2+ACC23*(TIME-TIME2)
POSCMN=POSC2+VELC2*(TIME-TIME2)+0.5*ACC23*((TIME-TIME2)**2)
GO TO 162
153 IF((TIME-TIME1))156,60,60
60 IF(ACCCMN .EQ. ACC12)GO TO 62
VELCMN=ACCO1*(TIME1-TIME0)
POSCMN=POSC0+0.5*ACCO1*((TIME1-TIME0)**2)
VELC1=VELCMN
POSCI=POSCMN
ACCCMN=ACC12
VELCMN=VELC1
62 POSCMN=POSCI+VELC1*(TIME-TIME1)
GO TO 162
156 IF((TIME-TIME0))159,70,70
70 IF(ACCCMN .EQ. ACC01)GO TO 72
ACCCMN=ACC01
POSC0=POSCMN
72 VELCMN=+ACCO1*(TIME-TIME0)
POSCMN=POSC0+0.5*ACCO1*((TIME-TIME0)**2)
GO TO 162
159 IF(ACCCMN .EQ. 0.)GO TO 162
VELCMN=0.
POSCMN=POSC2+VELC2*(TIME3-TIME2)+0.5*ACC23*((TIME3-TIME2)**2)
ACCCMN=0.
162 RETURN
END

```

Line	Code	Address	Value
10	T1=VELMAX/ACCMAG	07120	374600000
	T2=ABSERR/VELMAX	07130	374700000
	TIME0=TIMCU	07140	374800000
	TIME1=TIME0+T1	07150	374900000
	TIME2=TIME0+T2	07160	375000000
	TIME3=TIME2+T1	07170	375100000
	ACCO1=(ERROR/ABSERR)*ACCMAG	07180	375200000
	ACC12=0.	07190	375300000
	ACC23=(-ERROR/ABSERR)*ACCMAG	07200	375400000
	OUT=1.	07210	375500000
160	IF((TIME-TIME3))150,159,159	07220	375600000
150	IF((TIME-TIME2))153,50,50	07230	375700000
50	IF(ACCCMN .EQ. ACC23)GO TO 58	07240	375800000
	IF(ACCCMN .EQ. ACC01)GO TO 52	07250	375900000
	POSCMN=POSCI+VELC1*(TIME2-TIME1)	07260	376000000
	GO TO 54	07270	376100000
52	VELCMN=ACCO1*(TIME1-TIME0)	07280	376200000
	POSCMN=POSC0+0.5*ACCO1*((TIME1-TIME0)**2)	07290	376300000
	POSCMN=POSCMN+VELCMN*(TIME2-TIME1)	07300	376400000
54	VELC2=VELCMN	07310	376500000
	POSC2=POSCMN	07320	376600000
	ACCCMN=ACC23	07330	376700000
58	VELCMN=VELC2+ACC23*(TIME-TIME2)	07340	376800000
	POSCMN=POSC2+VELC2*(TIME-TIME2)+0.5*ACC23*((TIME-TIME2)**2)	07350	376900000
	GO TO 162	07360	377000000
153	IF((TIME-TIME1))156,60,60	07370	377100000
60	IF(ACCCMN .EQ. ACC12)GO TO 62	07380	377200000
	VELCMN=ACCO1*(TIME1-TIME0)	07390	377300000
	POSCMN=POSC0+0.5*ACCO1*((TIME1-TIME0)**2)	07400	377400000
	VELC1=VELCMN	07410	377500000
	POSCI=POSCMN	07420	377600000
	ACCCMN=ACC12	07430	377700000
	VELCMN=VELC1	07440	377800000
62	POSCMN=POSCI+VELC1*(TIME-TIME1)	07450	377900000
	GO TO 162	07460	378000000
156	IF((TIME-TIME0))159,70,70	07470	378100000
70	IF(ACCCMN .EQ. ACC01)GO TO 72	07480	378200000
	ACCCMN=ACC01	07490	378300000
	POSC0=POSCMN	07500	378400000
72	VELCMN=+ACCO1*(TIME-TIME0)	07510	378500000
	POSCMN=POSC0+0.5*ACCO1*((TIME-TIME0)**2)	07520	378600000
	GO TO 162	07530	378700000
159	IF(ACCCMN .EQ. 0.)GO TO 162	07540	378800000
	VELCMN=0.	07550	378900000
	POSCMN=POSC2+VELC2*(TIME3-TIME2)+0.5*ACC23*((TIME3-TIME2)**2)	07560	379000000
	ACCCMN=0.	07570	379100000
	162 RETURN	07580	379200000
	END	07590	379300000
		07600	379400000
		07610	379500000


```

SUBROUTINE BMCON(UJ,UJD,UJDD)
DIMENSION UJ0(3),UJ(3),UJD(3),UJDD(3),UJDO(3),G0(3,3),GDO(3,3),
* XAIS(3),XSNCM(3),DDXSNS(3),XSCM(3),DDXI(3,2)
COMMON /INOUT/IN, IOUT, IOFF
COMMON T,R(17),RI(3,100),RID(3,100),WXI(3,100),HI(3),H2(3),H3(3),
* H4(3),G1(3,3),G2(3,3)
COMMON /LABOR/WX(3),RIO(900),TH(3,100)
COMMON /ALLCNT/IS,O(40),YICS(10),YPRED(10),YDOT(10),NEQS,DD(3),
* XI(17),OICMAG
COMMON /LOADS/ZZ(685),RDDOT(3),WXDOT(3),QDD(6,100)
COMMON /EXTRA/ZFX(12),ZCM(3),EMC,TOT
COMMON /LUMPS/U(8)
COMMON /BIG/PIETA(9),PIGAM(3,3)
COMMON /VAROUT/DD(89),XXCS,ERRDDX,UJ3,HIL(2),UJD23
*,FI(9),U13M0,U23M0
*,EFILT
COMMON /NEWCOM/EL(3),ELD(3)
DO 8 I=1,2
UJ(I)=0.
UJD(I)=0.
UJDD(I)=0.
8 IF(T.GT.0.)GO TO 100
READ(IN,2)UJ,UJD,WMIEST,WKEXSE,WKDESE,TAUBAL,OICBAL,XAIS,XSCM
2 FORMAT(2(3E15.8/),5E15.8/3E16.7)
WRITE(IOUT,3)WMIEST,WKEXSE,WKDESE,TAUBAL,OICBAL,XAIS,XSCM,UJ,UJD
3 FORMAT(ORALANCE MASS CONTROL INPUT*/3X,*EL MASS EST*/9X,* KEXSE*,
* IIX,*KDESL*,6X,*FILTER TIME CONST*
*,2X,*OMEGA BAL (MIN)*/5E17.7/
** LOCAL SENSOR COORDS =*,3E16.7/
** DIST CM TO SENSOR CMND=*,3E16.7/
** U2 INITIAL =*,3E16.7/
** U2D INITIAL =*,3E16.7/
YICS(5)=UJDO(3)
YICS(6)=UJ0(3)
YICS(7)=0.
XSNCM(3)=0.
U13M0=0.
U13H=UJ(3)
CALL MCPY(UJ0,UJ,3,1,3)
CALL MCPY(UJDO,UJD,3,1,3)
NEQS=3
DDXI(3,2)=0.
100 CALL EARLY
C
C COMPUTE DDXSNS
C
CALL GAMMA(KX,G1)
CALL MULT(G1,RID(1,IS),HI,1)
CALL SCALP(2.,HI,H1,1)

```

```

E 07620 379600000
E 07630 379700000
E 07640 379800000
E 07650 379900000
E 07660 380000000
E 07670 380100000
E 07680 380200000
E 07690 380300000
E 07700 380400000
E 07710 380500000
E 07720 380600000
E 07730 380700000
E 07740 380800000
E 07750 380900000
E 07760 381000000
E 07770 381100000
E 07780 381200000
E 07790 381300000
E 07800 381400000
E 07810 381500000
E 07820 381600000
E 07830 381700000
E 07840 381800000
E 07850 381900000
E 07860 382000000
E 07870 382100000
E 07880 382200000
E 07890 382300000
E 07900 382400000
E 07910 382500000
E 07920 382600000
E 07930 382700000
E 07940 382800000
E 07950 382900000
E 07960 383000000
E 07970 383100000
E 07980 383200000
E 07990 383300000
E 08000 383400000
E 08010 383500000
E 08020 383600000
E 08030 383700000
E 08040 383800000
E 08050 383900000
E 08060 384000000
E 08070 384100000
E 08080 384200000
E 08090 384300000
E 08100 384400000

```

```

CALL MULT(G1,RI(1,IS),H3,1)
CALL MULT(G1,H3,H2,1)
CALL GAMMA(RI(1,IS),G1)
CALL MULT(G1,WXDOT,H3,1)
DO 10 I=1,3
10 H1(I)=RDOT(I)+QDD(I,IS)+H1(I)+H2(I)-H3(I)
CALL GAMMA(H1,IS),G1)
CALL MULT(G1,H1,H2,1)
CALL SUBTR(H1,H2,H1,1)
CALL GAMMA(WX(1,IS),G0)
CALL GAMMA(DG,G0)
CALL MULT(G0,XAIS,H3,1)
CALL MULT(G0,H3,H2,1)
CALL GAMMA(XAIS,G2)
CALL MULT(G2,DO,H3,1)
DO 20 I=1,3
20 DDXSNS(I)=F1(I)+H2(I)-H3(I)
IF(T.EQ.O.)GO TO 40
C
COMPUTE XSNCM
C
CALL MULT(G1,XAIS,H1,1)
CALL ADD(XAIS,H1,H1,1)
CALL MULT(PIGAM,ZCM,H2,1)
DO 30 I=1,3
30 XSNCM(I)=RI(I,IS)+H1(I)-H2(I)
U13M0=UJ(3)-U13H
UJ(3)=YPRED(6)
UJD(3)=YPRED(5)
EFILT=YPRED(7)
40 CONTINUE
CALL MCPY(UJDD,DUXI,3,1,3)
CALL BMCTR(FLD,DO,TOT,U,GDO,GO,UJ,WMIEST,WKEXSE
*          OICMAG,DDXSNS(3),DDXI,XSCM,OICBAL,TAURAL,EFILTD,WKDESE)E
CALL MCPY(DDXI(1,2),UJDD,3,1,3)
XXCS=XSCM(3)-XSNCM(3)
IF(T.EQ.O.)XXCS=0.
UJ3=UJ(3)
UJD23=UJD(3)
YDOT(5)=UJDD(3)
YDOT(6)=UJD(3)
YDOT(7)=EFILTD
U23M0=UJ3-UJ0(3)
RETURN
END

```

```

E 08110 384500000
E 08120 384600000
E 08130 384700000
E 08140 384800000
E 08150 384900000
E 08160 385000000
E 08170 385100000
E 08180 385200000
E 08190 385300000
E 08200 385400000
E 08210 385500000
E 08220 385600000
E 08230 385700000
E 08240 385800000
E 08250 385900000
E 08260 386000000
F 08270 386100000
F 08280 386200000
E 08290 386300000
E 08300 386400000
F 08310 386500000
F 08320 386600000
E 08330 386700000
E 08340 386800000
E 08350 386900000
F 08360 387000000
E 08370 387100000
E 08380 387200000
E 08390 387300000
E 08400 387400000
E 08410 387500000
E 08420 387600000
E 08430 387700000
E 08440 387800000
E 08450 387900000
E 08460 388000000
E 08470 388100000
E 08480 388200000
E 08490 388300000
E 08500 388400000
E 08510 388500000
E 08520 388600000
E 08530 388700000
E 08540 388800000
E 08550 388900000

```

```

SUBROUTINE HMCTR(DXB,DD,WM,WMI,GDO,GO,DXI,WMIEST,WKEXSE
* ,OICMAG,DDXSNS,DDXI,XSCM,OICBAL,TAUBAL,EFILT,DKDESE)
DIMENSION DXB(3),DD(3), DXI(3,2),DDXI(3,2),
1 WMI(2),
2 A1(3),A2(3),A3(3),A4(3),
3 GDO(3,3),GO(3,3),
4 XSCM(3)
COMMON T(918),A1,A2,A3,A4
COMMON /VAROUT/DDD(90),ERRDDX
* ,E(15),EFILT
IF(T(1) .NE. 0.)GO TO 10
DDXI(1,2)=0.
DDXI(2,2)=0.
EFILT=0.
EFILT=0.
10 IF(DXB(3))66,63,66
63 IF(OICMAG-OICBAL)66,65,65
66 DDXI(3,2)=0.
DXI(3,2)=0.
EFILT=0.
GO TO 64
65 CONTINUE
CALL MULT(GO,XSCM,A1,1)
CALL MULT(GO,A1,A2,1)
CALL MULT(GDO,XSCM,A1,1)
SC=WMIEST/WM
CALL SCALR(SC,DDXI,A3,1)
SC=WMI(2)/WM
CALL SCALR(SC,DDXI(1,2),A4,1)
DO 20 I=1,3
20 A4(I)=A1(I)+A2(I)-A3(I)-A4(I)
DDXCMN=A4(3)
ERRDDX=DDXCMN-DDXSNS
IF(TAUBAL.NE.0.)GO TO 80
EFILT=ERRDDX
GO TO 90
80 EFILT=(ERRDDX-EFILT)/TAUBAL
C MASS 2 POSITION CONTROL
C
C 90 DDXI(3,2)=-WKDESE*DXI(3,2)+WKEXSE*EFILT
C
C 64 RETURN
END

```

```

E 08560 389000000
E 08570 389100000
E 08580 389200000
E 08590 389300000
E 08600 389400000
E 08610 389500000
E 08620 389600000
E 08630 389700000
E 08640 389800000
E 08650 389900000
E 08660 390000000
E 08670 390100000
E 08680 390200000
E 08690 390300000
E 08700 390400000
E 08710 390500000
E 08720 390600000
E 08730 390700000
E 08740 390800000
E 08750 390900000
E 08760 391000000
E 08770 391100000
E 08780 391200000
E 08790 391300000
E 08800 391400000
E 08810 391500000
E 08820 391600000
E 08830 391700000
E 08840 391800000
E 08850 391900000
E 08860 392000000
E 08870 392100000
E 08880 392200000
E 08890 392300000
E 08900 392400000
E 08910 392500000
E 08920 392600000
E 08930 392700000
E 08940 392800000
E 08950 392900000
E 08960 393000000
E 08970 393100000
E 08980 393200000
E 08990 393300000
E 09000 393400000
E 09010 393500000

```

```
SUBROUTINE LOOK(L,K,M,IPOINT)
  DIMENSION K(8)
  COMMON T
  M=8
  DO 10 I=1,8
  10 K(I)=I
  RETURN
  END
```

```
E 09020 393600000
E 09030 393700000
393800000
E 09040 393900000
E 09050 394000000
E 09060 394100000
E 09070 394200000
E 09080 394300000
```

```

SUBROUTINE LOADIN
COMMON T,N(17),HOLD(6),SAVE(6),XLP(3),XLPI(3),WFI(6),CI(3,3)
COMMON /INOUT/IN,IOUT,IOFF
COMMON /LABOR/WX(3),RI(3,100),Q(3,100)
COMMON /CWT/DUMMY(9),WY(3),RA(3,100),QB(3,100)
COMMON /BIG/V(40),QP(3,6,100),A(6,6,100),D(6,6,100)
COMMON /LCADS/DUML(33),RHS(6,100),DEL(52),DDLAB(606),DDCW(606),
* KLUCS,KLULAB,KLUCW,CSLDA(6),CSLDB(6)
COMMON /LODPAS/L,FTL,N
DIMENSION SA(3,3,100),L(16),TL(3,16),LB(16),TLB(3,16),FTL(6,16),
* FTC(6,16),IXL(100),IXC(100),NIXL(16),NIXC(16),B(3,6,100),
* C(600,6),E(3,6,100)
DIMENSION FTCSMM(6,17,4)
EQUIVALENCE(SA(1,1,1),QP(1,1,1)),(A(1,1,1),B(1,1,1)),
(A(1,1,51),C(1,1)),(E(1,1,1),D(1,1,51))
* READ(IN,1)KLUCS,KLULAB,KLUCW,N,NB
I
FORMAT(5I2)
DO 10 I=1,6
DO 10 J=1,17
FTL(J,I)=0.
DO 10 K=1,4
10 FTCSMM(I,J,K)=0.
LOOP=0
IF(KLULAB.EQ.0)GO TO 30
INEW=0
IOLD=1
WRITE(IOUT,600)
600 FORMAT(*LOADS COMPUTED ON LABORATORY*)
DO 20 IL=1,N
READ(IN,1)L(IL),NIXL(IL)
INEW=INEW+NIXL(IL)
READ(IN,2)(TL(J,IL),J=1,3),(IXL(I),I=IOLD,INEW)
2 FORMAT(3E15.8/10I2)
WRITE(IOUT,45) L(IL),
* ,(IXL(I),I=IOLD,INEW)
20 IOLD=INEW+1
30 IF(KLUCW.EQ.0)GO TO 50
INEW=0
IOLD=1
WRITE(IOUT,700)
700 FORMAT(*LOADS COMPUTED ON COUNTERWEIGHT*)
DO 40 IL=1,NB
READ(IN,1) LB(IL),NIXC(IL)
INEW=INEW+NIXC(IL)
READ(IN,2)(TLB(J,IL),J=1,3),(IXC(I),I=IOLD,INEW)
WRITE(IOUT,45)LB(IL),
* ,(IXC(I),I=IOLD,INEW)
40 IOLD=INEW+1
50 RETURN

```

```

ENTRY I ABLD
INEW=0
IOLD=1
IF(T.EQ.0.)RETURN
DO 100 I=1,N
LI=LI(I)
DO 101 J=1,6
FTL(J,I)=0.
CALL MULT(OP(1,4,LI ),TL(1,I),SAVE,1)
DO 110 J=1,3
XLP(J)=SAVE(J)+RI(J,LI )+Q(J,LI )
INEW=INEW+IXL(J)
DO 120 J=IOLD,INEW
IXLJ=IXL(J)
ISIX=6*IXL(J)-5
CALL MPRD(A(1,1,IXLJ ),DDLAB,HOLD,6,6,1,6,1)
CALL MPRD(D(1,1,IXLJ ),DDLAB(ISIX+6),SAVE,6,6,1,6,1)
DO 140 K=1,6
WFI(K)=RHS(K,IXLJ )-HOLD(K)-SAVE(K)
CALL MULT(OP(1,4,IXLJ ),WFI(4),HOLD,1)
DO 160 K=1,3
XLP(K)=RHS(K,IXLJ )+Q(K,IXLJ )-XLP(K)
CALL GAMMA(XLP(1),G1)
CALL MULT(G1,WFI,SAVE,1)
DO 180 K=1,3
FTL(K,I)=FTL(K,I)+WFI(K)
180 FTL(K+3,I)=FTL(K+3,I)+HOLD(K)+SAVE(K)
120 CONTINUE
100 IOLD=INEW+1
RETURN
ENTRY CWLD
INEW=0
IOLD=1
IF(T.EQ.0.)RETURN
DO 200 I=1,NB
LI=LI(I)
DO 201 J=1,6
FTC(J,I)=0.
CALL MULT(SA(1,1,LI ),TLB(1,I),SAVE,1)
DO 210 J=1,3
XLP(J)=SAVE(J)+RA(J,LI )+QB(J,LI )
INEW=INEW+IXC(J)
DO 220 J=IOLD,INEW
IXLJ=IXC(J)
ISIX=6*IXC(J)-5
CALL MPRD(B(1,1,IXLJ ),DDLAB,HOLD,3,6,1,3,1)
CALL MPRD(C(ISIX,1),DDCW,SAVE,6,6,1,600,1)
CALL MPRD(E(1,1,IXLJ ),DDCW(ISIX+6),G1,3,3,1,3,1)
CALL MPRD(F(1,4,IXLJ ),DDCW(ISIX+9),G1(1,2),3,3,1,3,1)
DO 240 K=1,3
WFI(K)=RHS(K,IXLJ )-HOLD(K)-SAVE(K)-GI(K,1)

```

399300000

E 09570

399400000

E 09580

399500000

E 09590

399600000

E 09630

399700000

E 09600

399800000

E 09610

399900000

E 09620

400000000

E 09650

400100000

E 09670

400200000

E 09680

400300000

E 09690

400400000

E 09720

400500000

E 09750

400600000

E 09770

400700000

E 09780

400800000

E 09790

400900000

E 09800

401000000

E 09810

401100000

E 09820

401200000

E 09830

401300000

E 09840

401400000

E 09850

401500000

E 09860

401600000

E 09870

401700000

E 09910

401800000

E 09880

401900000

E 09890

402000000

E 09900

402100000

E 09930

402200000

E 09950

402300000

E 09960

402400000

E 09970

402500000

E 09990

402600000

E 10020

402700000

E 10020

402800000

E 10020

402900000

E 10020

403000000

E 10020

403100000

E 10020

403200000

E 10020

403300000

E 10020

403400000

E 10020

403500000

E 10020

403600000

E 10020

403700000

E 10020

403800000

E 10020

403900000

E 10020

404000000

E 10020

404100000

E 10020

404200000

E 10020

404300000

E 10020

```

240 WFI(K+3)=RHS(K+3,IXLJ )-SAVE(K+3)-GI(K,2)
CALL MULT(SA(1,1,IXLJ ),WFI(4),HOLD,I)
DO 260 K=1,3
260 XLP(K)=RA(K,IXLJ )+QB(K,IXLJ )-XLP(K)
CALL GAMMA(XLP,I,GI)
CALL MULT(GI,WFI,SAVE,I)
DO 280 K=1,3
280 FTC(K,I)=FTC(K,I)+WFI(K)
280 FTC(K+3,I)=FTC(K+3,I)+HOLD(K)+SAVE(K)
220 CONTINUE
200 IOLD=INNEW+1
RETURN
ENTRY LMMOUT
JUMP=KLUCS+KLULAB+KLUCW
IF(JUMP.EQ.0)RETURN
800 LOOP=LOOP+1
IF(LOOP.EQ.1)WRITE(IOUT,801)
IF(LOOP.EQ.2)WRITE(IOUT,802)
801 FORMAT(// * MAXIMUM LOADS COMPUTED*/)
802 FORMAT(// * MINIMUM LOADS COMPUTED*/)
DO 850 I=1,6
CSLDA(I)=FTCSMM(I,17,LOOP)
CSLDB(I)=FTCSMM(I,17,LOOP+2)
DO 850 J=1,16
FTL(I,J)=FTCSMM(I,J,LOOP)
850 FTC(I,J)=FTCSMM(I,J,LOOP+2)
ENTRY LDMOUT
IF(T.EQ.0)RETURN
IF(KLUCS.EQ.0)GO TO 310
DO 400 I=1,6
FTCSMM(I,17,1)=AMAX1(FTCSMM(I,17,1),CSLDA(I))
FTCSMM(I,17,2)=AMIN1(FTCSMM(I,17,2),CSLDA(I))
FTCSMM(I,17,3)=AMAX1(FTCSMM(I,17,3),CSLDB(I))
400 FTCSMM(I,17,4)=AMIN1(FTCSMM(I,17,4),CSLDB(I))
WRITE(IOUT,301)CSLDA,CSLDB
301 FORMAT(#0STRUCTURAL LOADS APPLIED BY CONNECTING STRUCTURE*
*,* (ON LAB IN X AXES AND ON CWT IN Y AXES)*/31X,
* * FORCE*,50X,*TORQUE*/# ON LAB *,3E16.7,8X,3E16.7/
* * ON CWT. *,3E16.7,8X,3E16.7)
310 IF(KLULAB.EQ.0)GO TO 350
DO 410 I=1,6
DO 410 J=1,N
FTCSMM(I,J,1)=AMAX1(FTCSMM(I,J,1),FTL(I,J))
410 FTCSMM(I,J,2)=AMIN1(FTCSMM(I,J,2),FTL(I,J))
WRITE(IOUT,320)
320 FORMAT(#0STRUCTURAL LOADS ON LAB IN X AXES*)
DO 340 I=1,N
340 WRITE(IOUT,330)L(I),(FTL(J,I),J=1,3),(FTL(J,I),J=1,6)
330 FORMAT(#0MASS POINT =*I2 /# LOCATION =*,3E17.7/21X,*FORCE*,
* 50X,*TORQUE*/3E16.7,8X,3E16.7)
350 IF(KLUCW.EQ.0)GO TO 300

```

```

404400000
404500000
404600000
404700000
404800000
404900000
405000000
405100000
405200000
405300000
405400000
405500000
405600000
405700000
405800000
405900000
406000000
406100000
406200000
406300000
406400000
406500000
406600000
406700000
406800000
406900000
407000000
407100000
407200000
407300000
407400000
407500000
407600000
407700000
407800000
407900000
408000000
408100000
408200000
408300000
408400000
408500000
408600000
408700000
408800000
408900000
409000000
409100000
409200000
409300000
409400000

```

E 10060

E 10080

E 10090

E 10100

E 10110

E 10120

E 10130

E 10140

E 10150

E 10160

E 10170

E 10180

E 10190

E 10200

E 10210

E 10220

E 10230

E 10240

E 10250

E 10260

E 10270

E 10280

E 10290

E 10300

E 10310

E 10320

E 10330

E 10340

E 10350

E 10360

E 10370

E 10380

E 10390

E 10400

E 10410

E 10420

E 10430

E 10440

E 10450

E 10460

E 10470

E 10480

E 10490

E 10500

E 10510

E 10520

E 10530

E 10540

```

DO 420 J=1,6
DO 420 J=1,NB
FTCSMM(I,J,3)=AMAX1(FTCSMM(I,J,3),FTC(I,J))
420 FTCSMM(I,J,4)=AMIN1(FTCSMM(I,J,4),FTC(I,J))
WRITE(IOUT,360)
360 FORMAT(*0STRUCTURAL LOADS ON COUNTERWEIGHT IN Y AXES*)
DO 380 I=1,NB
380 WRITE(IOUT,330)LB(I),(TLB(J,I),J=1,3),(FTC(J,I),J=1,6)
300 IF(LOOP.EQ.1)GO TO 800
RETURN
45 FOPMAT(* LOAD TO BE COMPUTED AT MASS POINT*,I4/
* * LOCATION IN LOCAL COORDINATES*,3E17.7/
* I4,* MASS POINT NUMBERS COMPRISING FREE BODY#7(2014))
END

```

E	10550	4095000000
E	10560	4096000000
E	10570	4097000000
E	10580	4098000000
E	10590	4099000000
E	10600	4100000000
E	10610	4101000000
E	10620	4102000000
E	10630	4103000000
E	10640	4104000000
E	10650	4105000000
E	10660	4106000000
E	10670	4107000000
E	10680	4108000000


```

SURROUTINE MINMAX(NLAB,NCW)
COMMON T
COMMON /LABOR/QL(303),Q(3,100,4)
COMMON /INOUT/IN,IOUT,IOFF
COMMON /CWT/QC(312),QB(3,100,4)
COMMON /NEWCOM/XXX(108),KLUE
COMMON /LOADS/ZZ(691),XDD(3,2,101),YDD(3,2,100)
DIMENSION QMAX(3,100,4),QMIN(3,100,4),QBMIN(3,100,4),QBMAX(3,100,4)
*)DDMIN(3,100,4),DDMAX(3,100,4)
IF(T.GT.0.)GO TO 100
IF(KLUE.EQ.2 .OR. KLUE.GT.3)GO TO 20
DO 10 I=1,3
DO 10 J=1,NLAB
DDMIN(I,J,1)=XDD(I,1,J)
DDMIN(I,J,2)=XDD(I,2,J)
DDMAX(I,J,1)=XDD(I,1,J)
DDMAX(I,J,2)=XDD(I,2,J)
DO 10 L=1,4
QMIN(I,J,L)=Q(I,J,L)
QMAX(I,J,L)=Q(I,J,L)
10 IF(KLUE.GE.3)GO TO 50
DO 30 I=1,3
DO 30 J=1,NCW
DDMIN(I,J,3)=YDD(I,1,J)
DDMIN(I,J,4)=YDD(I,2,J)
DDMAX(I,J,3)=YDD(I,1,J)
DDMAX(I,J,4)=YDD(I,2,J)
DO 30 L=1,4
QBMIN(I,J,L)=QB(I,J,L)
QBMAX(I,J,L)=QB(I,J,L)
30 QBMAX(I,J,L)=QB(I,J,L)
50 RETURN
100 IF(KLUE.EQ.2 .OR. KLUE.GT.3)GO TO 120
DO 110 I=1,3
DO 110 J=1,NLAB
IF(XDD(I,1,J).LT.DDMIN(I,J,1))DDMIN(I,J,1)=XDD(I,1,J)
IF(XDD(I,2,J).LT.DDMIN(I,J,2))DDMIN(I,J,2)=XDD(I,2,J)
IF(XDD(I,1,J).GT.DDMAX(I,J,1))DDMAX(I,J,1)=XDD(I,1,J)
IF(XDD(I,2,J).GT.DDMAX(I,J,2))DDMAX(I,J,2)=XDD(I,2,J)
DO 110 L=1,4
IF(Q(I,J,L).LT.QMIN(I,J,L))QMIN(I,J,L)=Q(I,J,L)
IF(Q(I,J,L).GT.QMAX(I,J,L))QMAX(I,J,L)=Q(I,J,L)
110 CONTINUE
120 IF(KLUE.GE.3)GO TO 200
DO 130 I=1,3
DO 130 J=1,NCW
IF(YDD(I,1,J).LT.DDMIN(I,J,3))DDMIN(I,J,3)=YDD(I,1,J)
IF(YDD(I,2,J).LT.DDMIN(I,J,4))DDMIN(I,J,4)=YDD(I,2,J)
IF(YDD(I,1,J).GT.DDMAX(I,J,3))DDMAX(I,J,3)=YDD(I,1,J)
IF(YDD(I,2,J).GT.DDMAX(I,J,4))DDMAX(I,J,4)=YDD(I,2,J)

```

E	10690	410900000
E	10700	411000000
E	10710	411100000
E	10720	411200000
E	10730	411300000
E	10740	411400000
E	10750	411500000
E	10760	411600000
E	10770	411700000
E	10780	411800000
E	10790	411900000
E	10800	412000000
E	10810	412100000
E	10820	412200000
E	10830	412300000
E	10840	412400000
E	10850	412500000
E	10860	412600000
E	10870	412700000
E	10880	412800000
E	10890	412900000
E	10900	413000000
E	10910	413100000
E	10920	413200000
E	10930	413300000
E	10940	413400000
E	10950	413500000
E	10960	413600000
E	10970	413700000
E	10980	413800000
E	10990	413900000
E	11000	414000000
E	11010	414100000
E	11020	414200000
E	11030	414300000
E	11040	414400000
E	11050	414500000
E	11060	414600000
E	11070	414700000
E	11080	414800000
E	11090	414900000
E	11100	415000000
E	11110	415100000
E	11120	415200000
E	11130	415300000
E	11140	415400000
E	11150	415500000
E	11160	415600000
E	11170	415700000

```

DO 130 L=1,4
IF(QB(I,J,L).LT.QBMIN(I,J,L))QBMIN(I,J,L)=QB(I,J,L)
IF(QB(I,J,L).GT.QBMAX(I,J,L))QBMAX(I,J,L)=QB(I,J,L)
130 CONTINUE
200 RETURN
ENTRY MMOUT
IF(KLUE.LE.3)WRITE(IOUT,300)
300 FORMAT(//# MAXIMUM AND MINIMUM ELASTIC MOTIONS#)
IF(KLUE.EQ.2 .OR. KLUE.GT.3)GO TO 350
WRITE(IOUT,600)
600 FORMAT(* MASS NO.,7X,*QMIN*,13X,*QMAX*,12X,*QDOTMIN*,10X,
* QDOTMAX*,9X,*QDDOTMIN*,9X,*QDDOTMAX*)
WRITE(IOUT,500)(J,(QMIN(I,J,1),QMAX(I,J,1),QMIN(I,J,2),
* QMAX(I,J,2),DDMIN(I,J,1),DDMAX(I,J,1) ,I=1,3),J=1,NLAB)
WRITE(IOUT,601)
601 FORMAT(* MASS NO.,5X,*THETAMIN*,9X,*THETAMAX*,8X,*THETADOTMIN*,6XE
* THETADOTMAX*,5X,*THETADOTMIN*,5X,*THETADOTMAX*)
WRITE(IOUT,500)(J,(QMIN(I,J,3),QMAX(I,J,3),QMIN(I,J,4),
* QMAX(I,J,4),DDMIN(I,J,2),DDMAX(I,J,2) ,I=1,3),J=1,NLAB)
350 IF(KLUE.GT.3)GO TO 1000
WRITE(IOUT,602)
602 FORMAT(* MASS NO.,5X,*QBARMIN*,10X,*QBARMAX*,9X,*QBARDDOTMIN*,7X,
* QBARDDOTMAX*,6X,*QBARDDOTMIN*,6X,*QBARDDOTMAX*)
WRITE(IOUT,500)(J,(QBMIN(I,J,1),QBMAX(I,J,1),QBMIN(I,J,2),
* QBMAX(I,J,2),DDMIN(I,J,3),DDMAX(I,J,3),I=1,3),J=1,NCW)
WRITE(IOUT,603)
603 FORMAT(* MASS NO. THETABARMIN THETABARMAX THETABARDDOTMIN THETABARDDOTMAX)
* N THETABARDDOTMAX THETABARDDOTMIN THETABARDDOTMAX*)
WRITE(IOUT,500)(J,(QBMIN(I,J,3),QBMAX(I,J,3),QBMIN(I,J,4),
* QBMAX(I,J,4),DDMIN(I,J,4),DDMAX(I,J,4),I=1,3),J=1,NCW)
1000 RETURN
500 FORMAT(2X,I3,3X,6E17.7/9X,6E17.7/8X,6F17.7/)
END

```

```

E 11180 415800000
E 11190 415900000
E 11200 416000000
F 11210 416100000
E 11220 416200000
E 11230 416300000
F 11240 416400000
E 11250 416500000
E 11260 416600000
E 11270 416700000
F 11280 416800000
F 11290 416900000
E 11300 417000000
E 11310 417100000
E 11320 417200000
E 11330 417300000
E 11340 417400000
E 11350 417500000
E 11360 417600000
E 11370 417700000
E 11380 417800000
E 11390 417900000
E 11400 418000000
E 11410 418100000
E 11420 418200000
E 11430 418300000
E 11440 418400000
E 11450 418500000
E 11460 418600000
E 11470 418700000
E 11480 418800000
E 11490 418900000
E 11500 419000000

```

```
SUBROUTINE SUPPLM(A,N,IF,K)
DIMENSION A(1)
N6=N*6
DO 10 I=1,N6
10 A(I)=0.
99 RETURN
END
```

E	11510	419100000
E	11520	419200000
E	11530	419300000
E	11540	419400000
E	11550	419500000
E	11560	419600000
E	11570	419700000

```

SUBROUTINE CWC0M(TIME,XB3CU,AXB3C,DXB3C,VELMBC,
1   DDXB3C,DXB3C,XB3C)
IF(TIME.EQ.0.JA=XB3C
IF(TIME.GT.TXB3CU)GO TO 10
XB3C=A
OUTXB=0.
DXB3C=0.
DDXB3C=0.
10 CALL POSCOM(TIME,XB3CU,AXB3C,OUTXB,TIME08,TIME18,TIME28,TIME38,
1   ACC01B,ACC12B,ACC23R,POSC08,POSC18,POSC28,VELC1B,VELC2B,
1   ACCB3C,VELMBC,DDXB3C,DXB3C,XB3C)
RETURN
END

```

E	11580	419800000
E	11590	419900000
E	11600	420000000
E	11610	420100000
F	11620	420200000
E	11630	420300000
E	11640	420400000
E	11650	420500000
E	11660	420600000
E	11670	420700000
E	11680	420800000
F	11690	420900000
E	11700	421000000

```

SUBROUTINE POSCTR(E,EDR,EDOT,EDOTMX,ACCS,ACCNOW)
THIS SUBROUTINE GENERATES A CONTROL POLICY. A CONSTANT
ACCELERATION +A, 0, OR -A IS COMMANDED, BASED ON THE
LOCATION OF THE STATE IN THE PHASE PLANE E, EDOT. PARABOLIC
AND CONSTANT RATE SWITCHING CURVES ARE USED.
C
C
C      ERROR, ATTITUDE - ATTITUDE COMMAND
C      EDB      ERROR DEAD BAND
C      EDOT     ERROR RATE, RATE-RATE COMMAND
C      EDOTMX   ERROR RATE MAXIMUM(FOR SWITCHING)
C      ACCS    = ACCELERATION MAGNITUDE (FOR SWITCHING)
C      ACCNOW  ACCELERATION COMMANDED NOW +1.0,-1.1
C
C      E1=+1.
C      IF(EDOT)40,5,5
C
C      5 IF(E+EDB)10,24,24
C      10 E2=SQRT(-2.*ACCS*(E+EDR))
C      IF(EDOT-E2)20,20,25
C      20 IF(EDOT-EDOTMX)21,21,22
C
C      24 IF(E-EDB)25,36,36
C      25 E3=SQRT(-2.*ACCS*(E-EDB))
C      IF(EDOT-E3)22,36,36
C      21 ACCNOW=E1
C      GO TO 80
C      22 ACCNOW=0.
C      GO TO 80
C      36 ACCNOW=-E1
C      GO TO 80
C
C      40 E=-E
C      EDOT=-EDOT
C      E1=-1.
C      GO TO 5
C
C      80 RETURN
C      END

```

E	11710	421100000
E	11720	421200000
E	11730	421300000
E	11740	421400000
E	11750	421500000
E	11760	421600000
E	11770	421700000
E	11780	421800000
E	11790	421900000
E	11800	422000000
E	11810	422100000
E	11820	422200000
E	11830	422300000
E	11840	422400000
E	11850	422500000
E	11860	422600000
E	11870	422700000
E	11880	422800000
E	11890	422900000
E	11900	423000000
E	11910	423100000
E	11920	423200000
E	11930	423300000
E	11940	423400000
E	11950	423500000
E	11960	423600000
E	11970	423700000
E	11980	423800000
E	11990	423900000
E	12000	424000000
E	12010	424100000
E	12020	424200000
E	12030	424300000
E	12040	424400000
E	12050	424500000
E	12060	424600000
E	12070	424700000

```

SUBROUTINE VELCOM(TIME,VELCU,TIMCU,OUT,TIMEO,TIMEL,ACCO1,VELCO,
1 ACCMAG,ACCCMN,VELCMN)
C THIS SUBROUTINE GENERATES A VELOCITY COMMAND
C TIME= TIME
C VELCU = VELOCITY COMMAND UPDATE
C TIMCU = TIME OF VELOCITY COMMAND UPDATE
C OUT = 0. FIRST UPDATE NOT YET ACTIVATED
C 1. ALL DATA ASSOCIATED WITH FIRST UPDATE COMPUTED
C ACCMAG= MAGNITUDE OF NON-ZERO ACCELERATION COMMAND
C TIMEO TIME TO COMMENCE ACCELERATION OF COMMAND
C TIME1 TIME TO END ACCELERATION. OCOM IS NOW OCOMU.
C ACCO1 ACCELERATION OF COMMAND FROM TIMEO TO TIME1
C VELCO =VELOCITY COMMAND AT TIMEO
C ACCCMN= ACCELERATION COMMAND
C VELCMN= VELOCITY COMMAND
C
C IF(TIME.NE. 0.)GO TO 163
ACCCMN=0.
OUT=0.
163 IF(TIME-TIMCU)175,164,164
164 IF(OUT)165,165,174
165 ERROR=VELCU-VELCMN
ABSERR=ABS(ERROR)
10 T1=ABSERR/ACCMAG
TIMEO=TIMCU
TIME1=TIMEO+T1
ACCO1=(ERROR/ABSERR)*ACCMAG
OUT=1.
C
174 IF(TIME-TIME1)170,172,172
170 IF(TIME-TIMEO)175,171,171
171 IF(ACCCMN.EQ. ACCO1)GO TO 20
VELCO=VELCMN
ACCCMN=ACCO1
20 VELCMN=VELCO+ACCO1*(TIME-TIMEO)
GO TO 175
172 IF(ACCCMN.EQ. 0.)GO TO 175
VELCMN=VELCO+ACCO1*(TIME1-TIMEO)
ACCCMN=0.
C
175 RETURN
END

```

```

E 12080 424800000
E 12090 424900000
E 12100 425000000
E 12110 425100000
E 12120 425200000
E 12130 425300000
E 12140 425400000
E 12150 425500000
E 12160 425600000
E 12170 425700000
E 12180 425800000
E 12190 425900000
E 12200 426000000
E 12210 426100000
E 12220 426200000
E 12230 426300000
E 12240 426400000
E 12250 426500000
E 12260 426600000
E 12270 426700000
E 12280 426800000
E 12290 426900000
E 12300 427000000
E 12310 427100000
E 12320 427200000
E 12330 427300000
E 12340 427400000
E 12350 427500000
E 12360 427600000
E 12370 427700000
E 12380 427800000
E 12390 427900000
E 12400 428000000
E 12410 428100000
E 12420 428200000
E 12430 428300000
E 12440 428400000
E 12450 428500000
E 12460 428600000
E 12470 428700000
E 12480 428800000
E 12490 428900000

```

```
SUBROUTINE ZEROS(A,N)
DIMENSION A(1)
K=3*N
DO 10 I=1,K
10 A(I)=0.
RETURN
END
```

429000000
429100000
429200000
429300000
429400000
429500000
429600000

```

SUBROUTINE SETUP ( MAGIN , MAGOUT , TIC,STEP, NEQNS , DTAU , EPSIL E
1, DELTA ,ERR, TIME , DTIME ,YICS,YPRD,YCORR,YDOT,YNEW
2 ,YDERV, YDEV,FWDEL,BKDEL,TBDEL,PARTY,YNEWB)
DIMENSION YICS( 1),YPRD( 1),YCORR( 1), YDOT( 1), YNEW( 1),
YDERV( 1), YDEV( 1),FWDEL( 1),BKDEL( 1),TBDEL( 1),
PARTY( 1),YNEWB( 1), ERR( 1)
DIMENSION C(3),D(3)
DOUBLE PRECISION YNEW,YPRD,YDERV
DATA C,D / .5,.5,1.0,.5,.0,.5/
TIME = TIC
TAU = TIC
IF (DELTA)200,201,200
200 DTIME = 0.0078125
GO TO 225
201 DTIME = STFP
225 DO 102 I = 1,NEQNS
YDEV(I) = 0.0
YPRD(I) = YICS(I)
YCORR(I) = YICS(I)
102 YNEW(I) = YICS(I)
MAGOUT =-2
GO TO 264
ENTRY MAGIC
300 CONTINUE
IF (MAGOUT) 305,101,101
101 IF (MAGIN) 21, 27, 14
27 K = 0
DO 202 I = 1,NEQNS
202 YNEW(I) = YPRD(I)
21 K = K +1
210 DO 2 I = 1,NEQNS
GO TO (9,6,7,4,11),K
9 FWDEL(I) = YDOT(I)
GO TO 105
6 TBDEL(I) = YDOT(I)
GO TO 105
7 TBDEL(I) = TBDEL(I) + YDOT(I)
105 YPRD(I) = YNEW(I) + C(K)*DTIME*YDOT(I)
GO TO (2,2,400),K
400 YCORR(I) = YPRD(I)
2 CONTINUE
TIME = TIME + D(K)*DTIME
99 MAGOUT = 0.0
264 RETURN
4 DO 8 I = 1,NEQNS
YPRD(I) = YNEW(I) + DTIME*(FWDEL(I) + 2.*TBDEL(I) + YDOT(I))/6.
8 YDEV(I) = YCORR(I) - YPRD(I)
GO TO 99
11 IF (DELTA)80, 5,80
4297000000
4298000000
4299000000
4300000000
4301000000
4302000000
4303000000
4304000000
4305000000
4306000000
4307000000
4308000000
4309000000
4310000000
4311000000
4312000000
4313000000
4314000000
4315000000
4316000000
4317000000
4318000000
4319000000
4320000000
4321000000
4322000000
4323000000
4324000000
4325000000
4326000000
4327000000
4328000000
4329000000
4330000000
4331000000
4332000000
4333000000
4334000000
4335000000
4336000000
4337000000
4338000000
4339000000
4340000000
4341000000
4342000000
4343000000
4344000000
4345000000
12510
12530
12540
12550
12560
12570
12580
12590
12600
12610
12620
12630
12640
12650
12660
12670
12680
12690
12700
12710
12720
12730
12740
12750
12760
12770
12780
12790
12800
12810
12820
12830
12840
12850
12860
12870
12880
12890
12900
12910
12920
12930
12940
12950
12960
12970
12980
12990

```



```

80 IF(DTIME.LT.STEP)GO TO 500
   DO 13 I = 1,NEQNS
   IF (EPSIL* ABS(YCORR(I)) + ERR(I) - ABS(YDEV(I)))14, 13, 13
13 CONTINUE
500 IF (SIGR)15,15,205
205 SIGR = 0.0
   GO TO 5
15 SIGR = 0.0
   DO 207 I = 1,NEQNS
   IF (ERR(I)/100.+ DELTA* ABS(YCORR(I)) - ABS(YDEV(I))) 5,207,207
207 CONTINUE
   DTIME = 2.*DTIME
5   DO 208 I = 1,NEQNS
208 YCORR(I) = YPKED(I)
305 IF (DTAU) 19,30,19
19 IF (TAU - TIME)20,20,27
20 TAU = TAU + DTAU
30 MAGOUT = 2
   GO TO 264
14 DTIME = DTIME/2.0
25 IF (K-3)48,26,26
26 TIME = TIME - DTIME - DTIME
   GO TO 47
48 TIME = TIME - DTIME
47 SIGR = +2.
   DO 209 I = 1,NEQNS
209 YDOT(I) = FWDEL(I)
212 K = 0
   GO TO 21
   END
SUBROUTINE CHASE(A,MO,Y,NO,MID,NIX)
REAL A(I),Y(I)
COMMON /WINTER/ INDICR
COMMON /RND/ M,L
COMMON /OPT2/ PRINT
9  FORMAT(I2H1SOLUTION(S)/IHO)
10 FORMAT (I5,I8E15.7/(5X,8E15.7))
   M = MO
   INDICR = 0
   N = IABS(NO)
   IF (NO) 110,100,100
100 CALL FUTURE(A,M,NIX)
   IF (NIX) 170,110,110
110 IF (PRINT .GT. 0.) WRITE (6,9)
   MK1 = 1
   L = 1.
   I1 = M
   DO 160 K = 1,N
   CALL TRIEQ(A,Y(MK1))
   IF (PRINT .GT. 0.) WRITE (6,10) K,(Y(K1), K1 = MK1,I1)
   I1 = I1 + MID

```

```

F 13000 4346000000
E 13010 4347000000
E 13020 4348000000
E 13030 4349000000
E 13040 4350000000
E 13050 4351000000
E 13060 4352000000
E 13070 4353000000
F 13080 4354000000
E 13090 4355000000
E 13100 4356000000
E 13110 4357000000
E 13120 4358000000
E 13130 4359000000
E 13140 4360000000
E 13150 4361000000
E 13160 4362000000
E 13170 4363000000
E 13180 4364000000
E 13190 4365000000
E 13200 4366000000
E 13210 4367000000
E 13220 4368000000
E 13230 4369000000
E 13240 4370000000
E 13250 4371000000
E 13260 4372000000
E 13270 4373000000
E 13280 4374000000
E 13290 4375000000
E 13300 4376000000
E 13310 4377000000
E 13320 4378000000
E 13330 4379000000
E 13340 4380000000
E 13350 4381000000
E 13360 4382000000
E 13370 4383000000
E 13380 4384000000
E 13390 4385000000
E 13400 4386000000
E 13410 4387000000
E 13420 4388000000
E 13430 4389000000
E 13440 4390000000
E 13450 4391000000
E 13460 4392000000
E 13470 4393000000
E 13480 4394000000
E 13490 4395000000
E 13500 4396000000

```

MK1 = MK1 + MID
160 CONTINUE
170 RETURN
END

E 13510 439700000
E 13520 439800000
E 13530 439900000
E 13540 440000000

FUNCTION APSIN(X)
ARSIN=ASIN(X)
RETURN
ENTRY ARCOS
ARCOS=ACOS(X)
RETURN
END

E 1355 440100000
E 1356 440200000
E 1357 440300000
E 1358 440400000
E 1359 440500000
E 1360 440600000
E 1361 440700000

A