



**FINAL REPORT**  
**STUDY**  
**OF**  
**INDUCER LOAD AND STRESS**

**CASE FILE**  
**COPY**

**Pratt & Whitney Aircraft**  
**FLORIDA RESEARCH AND DEVELOPMENT CENTER**  
BOX 2691, WEST PALM BEACH, FLORIDA 33402

**Prepared for**  
**NATIONAL AERONAUTICS**  
**AND**  
**SPACE ADMINISTRATION**

**NASA Lewis Research Center**  
**Contract NAS3-11216**

1. Report No. NASA CR 72712 Vol. II Revised	2. Government Accession No.	3. Recipient's Catalog No.	
4. Title and Subtitle Study of Inducer Load and Stress		5. Report Date November, 1972	6. Performing Organization Code
		8. Performing Organization Report No. PWA FR-3704 Vol. II Revised	
7. Author(s) Anonymous	10. Work Unit No.		
9. Performing Organization Name and Address Pratt & Whitney Aircraft Florida Research and Development Center West Palm Beach, Florida 33402		11. Contract or Grant No. NAS3-11216	
		13. Type of Report and Period Covered Contractor Report	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, D.C. 20546		14. Sponsoring Agency Code	
		15. Supplementary Notes Project Manager, Dean D. Scheer, Chemical Propulsion Division, NASA Lewis Research Center, Cleveland, Ohio	
16. Abstract  Three turbopump inducer computer programs are presented for the prediction of: (1) Inducer internal flow conditions, including blade pressure loading, and inducer performance under both noncavitating and cavitating flow conditions; (2) Inducer blade stress distribution caused by pressure loading and centrifugal force; and (3) Inducer blade natural frequencies and the distribution of relative displacements and stresses at resonance. Input-output descriptions and sample cases for the computer programs are included.			
17. Key Words (Suggested by Author(s))  Inducer                      Hydrodynamic Load Hydrodynamics              Sweepback Tip Clearance                Internal Flow Cavitation                    Blade Loading		18. Distribution Statement  Unclassified - Unlimited	
9. Security Classif. (of this report) Unclassified	20. Security Classif. (of this page) Unclassified	21. No. of Pages 224	22. Price* \$3.00

\* For sale by the National Technical Information Service, Springfield, Virginia 22151



## FOREWORD

This volume (II) documents the computer programs developed under Contract NAS3-11216. The volume was originally published in December 1970 and contained the programs as described in report Volume I. Additional work on the hydrodynamic analysis and computer program (in the areas of tip clearance and leading edge sweepback) was later conducted under Contract Modification 3. This additional work is reported in Volume III and the modified computer program is included in this revised issue of Volume II.

The work was sponsored by the Lewis Research Center, National Aeronautics and Space Administration, Cleveland, Ohio, under the technical direction of the Chemical Rocket Division with Mr. D. D. Scheer, Project Manager. Further information regarding the programs and their application may be obtained by contacting Mr. Scheer.

Pratt and Whitney Aircraft's Florida Research and Development Center at West Palm Beach, Florida was the contractor and Mr. W. E. Young was the Program Manager. The following Pratt & Whitney personnel contributed to the program:

Mr. R. E. Davis supervised the analytic effort.

Mr. H. J. Barten, Mr. L. L. Coons, and Mr. G. G. Roberts performed the analytic work.

Mr. D. R. Edmonds Jr. and Mr. J. A. Scheurenbrand did the computer programming.

## CONTENTS

SECTION	PAGE
	ILLUSTRATIONS . . . . . vi
I	INTRODUCTION . . . . . 1
II	HYDRODYNAMIC COMPUTER PROGRAM (PWA 6091) . . . . . 3
	A. General . . . . . 3
	B. Input Description . . . . . 3
	C. Output Description . . . . . 5
	D. Hydrodynamic Computer Program Sample Case (Noncavitating flow) . . . . . 10
	E. Hydrodynamic Computer Program Listing . . . . . 34
III	STRESS COMPUTER PROGRAM (PWA 6098) . . . . . 61
	A. General . . . . . 61
	B. Input Description. . . . . 61
	C. Output Description . . . . . 70
	D. Stress Computer Program (89 Deg Helicoid with Pressure Load) . . . . . 71
	E. Stress Computer Program Listing . . . . . 81
IV	VIBRATION COMPUTER PROGRAM (PWA 6140). . . . . 137
	A. General . . . . . 137
	B. Input Description. . . . . 137
	C. Output Description . . . . . 141
	D. Vibration Computer Program Sample Case (Simulated Cantilevered Flat Plate). . . . . 142
	E. Vibration Computer Program Listing . . . . . 151
	DISTRIBUTION LIST. . . . . 215

## ILLUSTRATIONS

FIGURE		PAGE
1	Finite Element Breakup. . . . .	62
2	Finite Element Nodes. . . . .	63
3	Geometric Parameters of Middle Surface of Inducer Blade . . . . .	66
4	Triangulation of Inducer Blade. . . . .	68

## SECTION I

### INTRODUCTION

The computer programs that were developed as a result of the work reported in Volumes I and III are listed in this volume. Three computer programs are included:

- 1) Hydrodynamic Computer Program - This program calculates the internal flow, blade loading, and performance of an inducer under noncavitating and cavitating conditions. The basic flow analysis uses a mean streamline, two dimensional, axisymmetric model. It is assumed that all cavitation is contained in a cavity on the blade suction surface and, because the vapor cavity merely displaces liquid, it is considered that the actual blade can be replaced by a pseudo blade consisting of the real blade plus the cavity. The analysis includes viscous effects and the program input provides for leading edge sweep-back and tip clearance.
- 2) Stress Computer Program - The stress program calculates stresses and deflections of the inducer blade which result from blade pressure loading and centrifugal force. The analysis uses the finite element matrix displacement method where the blade is replaced by contiguous polygonal elastic elements of finite size which are joined at their vertices or nodes. The program input provides for blade lean and for variable thickness blades.
- 3) Vibration Computer Program - The vibration program calculates blade natural frequencies and the distribution of relative deflections and stresses for each resonance. This program is a finite element analysis which uses many of the same subroutines as the stress program.

Input and output descriptions, and a sample case are included for each program.

The stress and vibration programs are identical to the listings given in the original issue of this volume. The hydrodynamic analysis has been modified as reported in Volume III and the program changes are included in this revised issue of Volume II.

SECTION II  
HYDRODYNAMIC COMPUTER PROGRAM (PWA 6091)

A. GENERAL

The hydrodynamic computer program predicts internal flow conditions and blade pressure loadings within an inducer.

The basic flow analysis uses a mean streamline, two-dimensional, meridional flow model. It is assumed that average flow conditions in the blade-to-blade space can be represented on a meridional surface. A two-dimensional streamline balancing analysis is then used to satisfy radial equilibrium and establish mean velocities, pressures, and flow angles. The program also employs a deviation model to calculate flow conditions downstream of the inducer. Inducer inlet and exit conditions are then integrated to obtain predictions of performance.

The program requires approximately 180,000 bytes of core (165,000 bytes program and 15,000 bytes buffer) on an IBM 370 Model 165 Computer. Computer language is Fortran IV-G Release 1.1. Approximate running time for a typical case (one set flow conditions) with tip clearance is 2 minutes.

B. INPUT DESCRIPTION

The hydrodynamic computer program input can be divided into two parts:

1. A geometric description of the inducer; and
2. A description of the inducer operating flow parameters. More than one set of flow parameters may be input for a given inducer geometry.

Unless otherwise specified, data may be input in any consistent set of units. The same units must be used for force and mass. Output will correspond to the input units used. Several examples are listed below.

<u>Input</u>			<u>Output</u>	
<u>Force</u>	<u>Mass</u>	<u>Length</u>	<u>Velocity</u>	<u>Pressure</u>
lb	lb	ft	ft/sec	lb/ft <sup>2</sup>
lb	lb	in.	in./sec	lb/in. <sup>2</sup>
gram	gram	meter	meter/sec	gram/meter <sup>2</sup>

Input data to be written on each card are described below. "F" format data should be left adjusted in the column field and should contain a decimal point. "I" format data should be right adjusted and should not contain a decimal point.



Columns	Variable		Format
Card 1	Title Card		
1-80	Job Identification data		20A4
Card 2	General Geometry		
1-5	NI	Number of streamlines to be considered Maximum of 15	I5
6-10	NJ	Number of axial stations to be considered Maximum of 60	I5
11-15	NB	Number of inducer blades	I5
16-20	CASES	Number of flow conditions	I5
21-35	G	Gravitational constant	F15.5
36-45	ALPWH	Hub leading edge wedge angle, degrees	F10.4
46-55	ALPWT	Tip leading edge wedge angle, degrees	F10.4
56-65	CBHR	Tip clearance to blade height ratio, may be zero if tip clearance analysis is not required.	F10.4
Card 3	Geometry at Each Axial Station (NJ Cards)		
1-10	Z	Axial dimension from the station to the leading edge. Stations spacing may be varied to provide fine resolution in areas where flow conditions are expected to change rapidly.	F10.4
11-20	RH	Hub radius	F10.4
21-30	RT	Tip radius	F10.4
31-40	BHS	Hub blade angle, degrees from tangential	F10.4
41-50	BTS	Tip blade angle, degrees from tangential	F10.4
51-60	TT	Blade tip thickness	F10.4
61-70	TA	Blade taper angle, degrees	F10.4
Card 4	+NJ Leading Edge Shape		
1-40	Z <sub>0</sub> , Z <sub>1</sub> Z <sub>2</sub> , Z <sub>3</sub>	Coefficients of the third degree quad- ratic equation which defines the leading edge curvature as projected on the meridional plane	4F10.4

Columns	Variable	Format
Card 5	+NJ Fluid Properties, Speed, & Print Option	
1-10	RHO Specific weight	F10.4
11-20	MU Kinematic viscosity	F10.4
21-30	PSAT Saturation pressure	F10.4
31-40	SN Rotating speed, rev/sec	F10.4
41-50	LOADOP 0 if no blade loading data desired 1 if blade loading data is desired Automatically 1 if CBHR is positive	I10
Card 6	+NJ Inlet Flow Conditions at Each Streamline (NI Cards)	
1-10	PO Relative inlet total pressure	F10.0
11-20	VA Inlet axial velocity	F10.0
21-30	ALPHI Inlet absolute flow angle, degrees from tangential	F10.0

For more than 1 set of flow conditions (CASES > 1), repeat cards (5+NJ) and (6+NJ)

### C. OUTPUT DESCRIPTION

The output of the program is in the following seven parts. Parts 3 thru 7 are printed twice if CBHR is a positive number, first for zero and then for the specified tip clearance.

#### 1. Geometry

The input geometry is printed out for reference. Also solidity at the inlet tip is calculated and printed out.

#### 2. Fluid Properties and Inlet Flow Conditions

The input fluid properties (Card 5) and the input inlet flow conditions (Cards 6 thru NI) are printed.

#### 3. Inlet Conditions

The above flow conditions and the following additional inlet conditions are listed for each streamtube.

I	Streamtube number
ALPHA	Absolute flow angle, degrees from tangential
R	Streamtube radius
BETA	Relative flow angle, degrees from tangential
Q	Volumetric flow
K	Cavitation number, k
W	Relative velocity
U	Inducer tangential velocity

PO Absolute total pressure  
 V Absolute velocity  
 PREL Relative total pressure  
 VM Meridional velocity  
 P Static pressure  
 VU Absolute tangential velocity  
 PHI Mass averaged inlet flow coefficient,  $\phi$   
 NPSH Mass averaged net positive suction head  
 THOMA Cavitation parameter  
 VT Inducer tip speed  
 PT Mass averaged total pressure

4. Internal Flow Conditions

The following are listed for each axial station

J Station number  
 Z Axial dimension to station  
 ITE Number of iterations required to obtain radial pressure equilibrium.

The following are listed for each streamtube at each axial station.

I Streamtube number  
 P Static pressure  
 BETA Relative flow angle, degrees from tangential  
 ALPHA Absolute flow angle, degrees from tangential  
 RST Streamline radius  
 PREL Relative total pressure of the core flow  
 BETA\* Blade angle, degrees from tangential  
 ETA Efficiency  
 PCR Ratio (RST-RH) / (RT-RH)

POREL Relative total pressure (mass-averaged)  
 DEV Deviation angle, degrees  
 W Relative velocity  
 R Streamtube radius  
 PT Absolute total pressure  
 DLB\* Vapor cavity slope angle, degrees  
 U Inducer tangential velocity  
 TAU Blade tangential spacing  
 M\* Distance along blade  
 XMTH Momentum thickness  
 V Absolute velocity  
 THK Normal blade thickness  
 BN Normal cavity height  
 DEL\* Boundary layer displacement thickness  
 VU Absolute tangential velocity  
 B Tangential cavity height  
 PCB Ratio of tangential cavity height to blade tangential spacing,  $B/TAU$   
 HSF Ratio  $DEL*/XMTH$   
 VM Meridional velocity

#### 5. Exit Conditions

The following are listed for each streamtube at an axial station downstream of the inducer.

I Streamtube number  
 ALPHA Absolute flow angle, degrees from tangential  
 R Radius of streamtube  
 BETA Relative flow angle, degrees from tangential  
 DEV Deviation angle

V Absolute velocity  
H Head rise  
VM Meridional velocity  
P Static pressure  
VU Absolute tangential velocity  
PT Total pressure  
WU Relative tangential velocity  
ETA Efficiency  
W Relative velocity

#### 6. Performance Parameters

The following listed parameters represent the mass averaged performance of the inducer.

NPSH Net positive suction head  
PHI Flow coefficient  
PSI Head coefficient  
H Head rise  
HI Ideal head rise  
RN Reynolds number  
ETA Efficiency  
SS Specific speed  
QI Volumetric flow  
CVOL Total blade suction surface cavity volume (all blades)  
PSI IDEAL Ideal head coefficient  
PSI LOSS Head loss coefficient

#### 7. Blade Loading Data

This data is listed if "LOADOP" is input as 1. The following are listed for each axial station.

J Station number  
Z Axial dimension to station  
Z/ZT Ratio of axial length to total axial length

The following are listed for each streamtube at each axial station.

I	Streamtube number
R	Streamtube radius
PS	Static pressure on blade suction surface
PP	Static pressure on blade pressure surface
WS	Relative velocity along blade suction surface
WP	Relative velocity along blade pressure surface
DPB	Normal pressure difference across blade
PSIS	Suction surface static head coefficient
PSIP	Pressure surface static head coefficient

D. HYDRODYNAMIC COMPUTER PROGRAM  
Sample Case (Noncavitating Flow)

INDUCER HYDRODYNAMIC PROGRAM

COURSE GRID - RADIAL L.E. -

NI	NJ	NB	CASES	G	CBHR	ET*	TT	TA
7	25	3	1	32.20000	0.0290			
Z	RH	RT	BH*	ET*	TT	TA		
1	0.0	0.29180	19.34599	8.00000	0.00100	0.0		
2	0.00500	0.29180	19.34599	8.00000	0.01082	0.0		
3	0.01000	0.29180	19.34599	8.00000	0.01082	0.0		
4	0.01500	0.29180	19.34599	8.00000	0.01082	0.0		
5	0.02000	0.29180	19.34599	8.00000	0.01082	0.0		
6	0.02500	0.29180	19.34599	8.00000	0.01082	0.0		
7	0.03000	0.29180	19.34599	8.00000	0.01082	0.0		
8	0.03500	0.29180	19.34599	8.00000	0.01082	0.0		
9	0.04000	0.29180	19.34599	8.00000	0.01082	0.0		
10	0.04500	0.29180	19.34599	8.00000	0.01082	0.0		
11	0.05000	0.29180	19.34599	8.00000	0.01082	0.0		
12	0.05500	0.29180	19.34599	8.00000	0.01082	0.0		
13	0.06000	0.29180	19.34599	8.00000	0.01082	0.0		
14	0.06000	0.29180	19.32899	8.06000	0.01082	0.0		
15	0.10000	0.29180	19.31000	8.21000	0.01082	0.0		
16	0.12000	0.29180	19.30000	8.35000	0.01082	0.0		
17	0.14000	0.29180	19.20000	8.55000	0.01082	0.0		
18	0.16000	0.29180	19.10001	8.77000	0.01082	0.0		
19	0.18000	0.29180	19.00000	9.05000	0.01082	0.0		
20	0.20000	0.29180	16.80000	9.35000	0.01082	0.0		
21	0.22000	0.29180	16.89999	9.70000	0.01082	0.0		
22	0.24000	0.29180	19.00000	10.05000	0.01082	0.0		
23	0.26000	0.29180	19.25000	10.40000	0.01082	0.0		
24	0.28000	0.29180	19.60001	10.80000	0.01082	0.0		
25	0.29200	0.29180	19.69999	11.00000	0.00100	0.0		

SWEPT LEADING EDGE COEFFICIENTS

Z0= 0.0  
 Z1= 0.0  
 Z2= 0.0  
 Z3= 0.0

SOLIDITY 2.8948708 ALPHM 19.3499908 ALPWT 7.9999961



CASE NUMBER - 1

RHC 62.30000 MU 0.00064 PSAT 52.20000 SN 81.81400 LOADOP 1 FLR 0.200992

PO VM ALPHA  
 6909.50000 12.60000 90.00000  
 6909.50000 12.60000 90.00000  
 6909.50000 12.60000 90.00000  
 6909.50000 12.60000 90.00000  
 6909.50000 12.60000 90.00000  
 6909.50000 12.60000 90.00000

INLET CONDITIONS

I	R	Q	W	PO	PREL	P
ALPHA	BETA	K	U	V	VM	VU
1	0.13563	0.13478	70.84999	6909.50000	11611.9453	6755.91406
89.99997	10.24401	1.38049	69.72055	12.60000	12.60000	0.00000
2	0.16952	0.13478	88.04974	6909.50000	14255.8594	6755.91406
89.99997	8.22733	0.89383	87.14352	12.60000	12.60000	0.00000
3	0.19752	0.13478	102.31271	6909.50000	16882.4570	6755.91406
89.99997	7.07405	0.66199	101.53381	12.60000	12.60000	0.00000
4	0.22195	0.13478	114.78851	6909.50000	19502.6484	6755.91406
89.99997	6.30189	0.52592	114.09482	12.60000	12.60000	0.00000
5	0.24393	0.13478	126.02280	6909.50000	22119.7695	6755.91406
89.99997	5.73813	0.43633	125.39127	12.60000	12.60000	0.00000
6	0.26407	0.13478	136.32800	6909.50000	24735.1914	6755.91406
89.99997	5.30309	0.37286	135.74437	12.60000	12.60000	0.00000
7	0.28277	0.13478	145.90343	6909.50000	27349.5506	6755.91406
89.99997	4.95415	0.32552	145.35822	12.60000	12.60000	0.00000

PHI 0.0840 NPSH 110.0690 THOMA 0.3150 VT 150.0009 PT 6909.5000 KTIP 0.3058

STATION J = 1 , Z = 0.0 , ITE = 1

I	P	BETA	ALPHA	RST	PREL	BETA*	ETA	PCR	PCREL	DEV	W	R	PT	DLB*	U	TAU	M*	XMTH	V	THK	BN	DEL*	VU	B	PCB	HSF	VM
1				0.15446E+00	0.11612E+05	0.16823E+02	0.10000E+01	0.21519E+00	0.11612E+05	0.65790E+01	0.70850E+02	0.13563E+00	0.69095E+04	0.65790E+01	0.69721E+02	0.28406E+00	0.0	0.10586E-03	0.12600E+02	0.0	0.0	0.15259E-04	0.0	0.0	0.14000E+01	0.12600E+02	
2				0.18459E+00	0.14256E+05	0.13599E+02	0.10000E+01	0.38735E+00	0.14256E+05	0.53717E+01	0.88050E+02	0.16952E+00	0.69095E+04	0.53717E+01	0.87143E+02	0.35505E+00	0.0	0.94957E-04	0.12600E+02	0.0	0.0	-0.30518E-04	0.0	0.0	0.14000E+01	0.12600E+02	
3				0.21045E+00	0.16862E+05	0.11729E+02	0.10000E+01	0.53512E+00	0.16862E+05	0.46552E+01	0.10231E+03	0.19752E+00	0.69095E+04	0.46552E+01	0.10153E+03	0.41368E+00	0.0	0.88090E-04	0.12600E+02	0.0	0.0	-0.15259E-04	0.0	0.0	0.14000E+01	0.12600E+02	
4				0.23346E+00	0.19503E+05	0.10488E+02	0.10000E+01	0.66661E+00	0.19503E+05	0.41664E+01	0.11479E+03	0.22195E+00	0.69095E+04	0.41664E+01	0.11409E+03	0.46465E+00	0.0	0.83165E-04	0.12600E+02	0.0	0.0	-0.45776E-04	0.0	0.0	0.14000E+01	0.12600E+02	
5				0.25440E+00	0.22120E+05	0.95434E+01	0.10000E+01	0.78626E+00	0.22120E+05	0.38053E+01	0.12602E+03	0.24393E+00	0.69095E+04	0.38053E+01	0.12539E+03	0.51088E+00	0.0	0.79372E-04	0.12600E+02	0.0	0.0	-0.45776E-04	0.0	0.0	0.14000E+01	0.12600E+02	
6				0.27374E+00	0.24735E+05	0.88275E+01	0.10000E+01	0.89678E+00	0.24735E+05	0.35244E+01	0.13633E+03	0.26407E+00	0.69095E+04	0.35244E+01	0.13574E+03	0.55306E+00	0.0	0.76313E-04	0.12600E+02	0.0	0.0	-0.16785E-03	0.0	0.0	0.14000E+01	0.12600E+02	
7				0.29180E+00	0.27350E+05	0.82520E+01	0.10000E+01	0.10000E+01	0.27350E+05	0.32979E+01	0.14590E+03	0.28277E+00	0.69095E+04	0.32979E+01	0.14536E+03	0.59223E+00	0.0	0.75766E-04	0.12600E+02	0.0	0.0	-0.12207E-03	0.0	0.0	0.14000E+01	0.12600E+02	

STATION J = 2 , Z = 0.00500 , ITE = 100

I	RST	PCR	R	TAU	THK	B
P	PREL	POREL	PT	M*	BN	PCB
BETA	BETA*	DEV	DLB*	XMTH	DEL*	HSF
ALPHA	ETA	W	U	V	VU	VM
1	0.15412E+00	0.21327E+00	0.13546E+00	0.26419E+00	0.56544E-02	0.0
	0.76115E+04	0.11600E+05	0.11525E+05	0.17269E-01	0.0	0.0
	0.12817E+02	0.16843E+02	0.40260E+01	0.16865E-03	0.27971E-03	0.14827E+01
	0.58189E+02	0.93511E+00	0.62582E+01	0.16337E+02	0.86113E+01	0.13883E+02
2	0.18442E+00	0.36641E+00	0.16927E+00	0.32876E+00	0.60664E-02	0.21685E-02
	0.14234E+05	0.14207E+05	0.90931E+04	0.23365E-01	0.51059E-03	0.65962E-02
	0.10498E+02	0.31227E+01	0.12510E+01	0.19106E-03	0.28528E-03	0.14931E+01
	0.46189E+02	0.98772E+00	0.87015E+02	0.18968E+02	0.13131E+02	0.13688E+02
3	0.21043E+00	0.53504E+00	0.19743E+00	0.36308E+00	0.61854E-02	0.78720E-02
	0.16873E+05	0.16837E+05	0.93966E+04	0.32299E-01	0.16010E-02	0.20549E-01
	0.88909E+01	0.11734E+02	0.28371E+01	0.16028E-03	0.26522E-03	0.14712E+01
	0.47166E+02	0.98543E+00	0.10149E+03	0.18907E+02	0.12854E+02	0.13865E+02
4	0.23345E+00	0.66659E+00	0.22194E+00	0.43117E+00	0.61163E-02	0.12856E-01
	0.19502E+05	0.19455E+05	0.95561E+04	0.40161E-01	0.23360E-02	0.29817E-01
	0.10469E+02	0.26203E+01	0.33288E+01	0.17350E-03	0.25250E-03	0.14553E+01
	0.98266E+00	0.10285E+03	0.11409E+03	0.18604E+02	0.12201E+02	0.14045E+02
5	0.25440E+00	0.76627E+00	0.24393E+00	0.47517E+00	0.59194E-02	0.18095E-01
	0.22120E+05	0.22063E+05	0.96643E+04	0.48002E-01	0.30000E-02	0.38080E-01
	0.95434E+01	0.24675E+01	0.35762E+01	0.16962E-03	0.24501E-03	0.14444E+01
	0.97975E+00	0.11467E+03	0.12539E+03	0.18272E+02	0.11590E+02	0.14126E+02
6	0.27374E+00	0.89679E+00	0.26407E+00	0.51640E+00	0.56270E-02	0.23246E-01
	0.24735E+05	0.24668E+05	0.97284E+04	0.55552E-01	0.35673E-02	0.45016E-01
	0.88275E+01	0.23446E+01	0.36830E+01	0.16731E-03	0.24035E-03	0.14364E+01
	0.97664E+00	0.12556E+03	0.13575E+03	0.17937E+02	0.10990E+02	0.14176E+02
7	0.29180E+00	0.10000E+01	0.26277E+00	0.55559E+00	0.52596E-02	0.26042E-01
	0.27350E+05	0.26946E+05	0.94585E+04	0.60609E-01	0.37377E-02	0.46672E-01
	0.82520E+01	0.21673E+01	0.35289E+01	0.16615E-03	0.23767E-03	0.14305E+01
	0.86328E+00	0.13562E+03	0.14536E+03	0.17763E+02	0.10499E+02	0.14328E+02

STATION J = 3 , Z = 0.01000 , ILE = 100

I	P	BETA	ALPHA	RST	PREL	BETA*	ETA	PCR	POREL	DEV	W	R	PT	OLB*	U	TAU	M*	XMTH	V	THK	BN	DEL*	VU	B	PCB	HSF	VM	
1				0.15406E+00	0.11598E+05	0.16848E+02	0.94277E+00	0.21292E+00	0.11504E+05	0.21513E+01	0.59305E+02	0.13543E+00	0.84655E+04	0.0	0.69618E+02	0.24631E+00	0.34527E-01	0.25479E-03	0.19403E+02	0.10820E-01	0.0	0.38386E-03	0.12253E+02	0.0	0.0	0.15066E+01	0.15044E+02	
2				0.18446E+00	0.13494E+05	0.13619E+02	0.75584E+00	0.38665E+00	0.13423E+05	0.14415E+01	0.68641E+02	0.16928E+00	0.94184E+04	0.0	0.87010E+02	0.30855E+00	0.42499E-01	0.28348E-03	0.24468E+02	0.10820E-01	0.0	0.43682E-03	0.19717E+02	0.0	0.0	0.15409E+01	0.14522E+02	
3				0.21045E+00	0.16876E+05	0.11733E+02	0.98605E+00	0.53513E+00	0.16826E+05	0.11374E+01	0.81307E+02	0.19746E+00	0.11097E+05	0.0	0.87010E+02	0.36034E+00	0.60214E-01	0.28120E-03	0.26254E+02	0.10820E-01	0.0	0.22920E-02	0.42916E-03	0.0	0.0	0.11271E-01	0.31279E-01	
4				0.23349E+00	0.19505E+05	0.10488E+01	0.98734E+00	0.66678E+00	0.19438E+05	0.92906E+00	0.91734E+02	0.22197E+00	0.12062E+05	0.0	0.10150E+03	0.40533E+00	0.72816E-01	0.28558E-03	0.28104E+02	0.10820E-01	0.0	0.32845E-02	0.43466E-03	0.0	0.0	0.16079E-01	0.44602E-01	
5				0.25457E+00	0.22132E+05	0.95396E+01	0.98704E+00	0.78723E+00	0.22050E+05	0.78147E+00	0.10048E+03	0.24403E+00	0.13169E+05	0.0	0.12544E+03	0.44560E+00	0.85048E-01	0.29342E-03	0.30281E+02	0.10820E-01	0.0	0.41551E-02	0.44686E-03	0.0	0.0	0.25072E-01	0.56239E-01	
6				0.27386E+00	0.24755E+05	0.88227E+01	0.98597E+00	0.89749E+00	0.24655E+05	0.66831E+00	0.10996E+03	0.26421E+00	0.13897E+05	0.0	0.13582E+03	0.48282E+00	0.96659E-01	0.29393E-03	0.31155E+02	0.10820E-01	0.0	0.48867E-02	0.44497E-03	0.0	0.0	0.31861E-01	0.65988E-01	
7				0.29180E+00	0.27358E+05	0.82503E+01	0.92456E+00	0.10000E+01	0.26795E+05	0.57042E+00	0.11992E+03	0.28283E+00	0.13814E+05	0.0	0.14539E+03	0.51909E+00	0.10485E+00	0.29057E-03	0.31009E+02	0.10514E-01	0.0	0.50995E-02	0.43601E-03	0.0	0.0	0.35538E-01	0.68462E-01	
				0.13447E+05	0.76798E+01	0.31110E+02																						

Printout for Stations J=4 thru J=23 is omitted for Brevity.

STATION J = 24 , Z = 0.28000 , ITE = 100

I	RST	PCR	R	TAU	THK	B
P	PREL	POREL	PT	M*	BN	PCB
BETA	BETA*	DEV	DLB*	XMTH	DEL*	HSF
ALPHA	ETA	W	U	V	VU	VM
1	0.16966E+00	0.24747E+00	0.17289E+00	0.32676E+00	0.10820E-01	0.0
0.12193E+05	0.14551E+05	0.14133E+05	0.13653E+05	0.97354E+00	0.0	0.0
0.16907E+02	0.17826E+02	0.91886E+00	0.0	0.18614E-02	0.26494E-02	0.14233E+01
0.19020E+02	0.94171E+00	0.49364E+02	0.88875E+02	0.44050E+02	0.41645E+02	0.14356E+02
2	0.21263E+00	0.41656E+00	0.20115E+00	0.35069E+00	0.10820E-01	0.0
0.12446E+05	0.16514E+05	0.16253E+05	0.14040E+05	0.11690E+01	0.0	0.0
0.14573E+02	0.15454E+02	0.88132E+00	0.0	0.16299E-02	0.22348E-02	0.13711E+01
0.21874E+02	0.87696E+00	0.64849E+02	0.10340E+03	0.43795E+02	0.40642E+02	0.16316E+02
3	0.23121E+00	0.55351E+00	0.22192E+00	0.42028E+00	0.10820E-01	0.0
0.12557E+05	0.18596E+05	0.18204E+05	0.13817E+05	0.13235E+01	0.0	0.0
0.13215E+02	0.14071E+02	0.65636E+00	0.0	0.16565E-02	0.22642E-02	0.13669E+01
0.25922E+02	0.84215E+00	0.79010E+02	0.11408E+03	0.41318E+02	0.37161E+02	0.18062E+02
4	0.24773E+00	0.67527E+00	0.23947E+00	0.45374E+00	0.10820E-01	0.0
0.12633E+05	0.20241E+05	0.19721E+05	0.13740E+05	0.14556E+01	0.0	0.0
0.12247E+02	0.13079E+02	0.83145E+00	0.0	0.17547E-02	0.24048E-02	0.13705E+01
0.27308E+02	0.78714E+00	0.88684E+02	0.12310E+03	0.41006E+02	0.36436E+02	0.18613E+02
5	0.26272E+00	0.78568E+00	0.25523E+00	0.48375E+00	0.10820E-01	0.0
0.12696E+05	0.21970E+05	0.21297E+05	0.13593E+05	0.15742E+01	0.0	0.0
0.11492E+02	0.12299E+02	0.80635E+00	0.0	0.18693E-02	0.25756E-02	0.13776E+01
0.28958E+02	0.74690E+00	0.97910E+02	0.13120E+03	0.40290E+02	0.35233E+02	0.19507E+02
6	0.27654E+00	0.88756E+00	0.26963E+00	0.51118E+00	0.10820E-01	0.0
0.12744E+05	0.23687E+05	0.22841E+05	0.13418E+05	0.16820E+01	0.0	0.0
0.10879E+02	0.11662E+02	0.76263E+00	0.0	0.19954E-02	0.27658E-02	0.13661E+01
0.30439E+02	0.71044E+00	0.10635E+03	0.13860E+03	0.59622E+02	0.34161E+02	0.20073E+02
7	0.29160E+00	0.10000E+01	0.26417E+00	0.53868E+00	0.10820E-01	0.0
0.12785E+05	0.26253E+05	0.21783E+05	0.96180E+04	0.17851E+01	0.0	0.0
0.10327E+02	0.11082E+02	0.75501E+00	0.0	0.20657E-02	0.29037E-02	0.13922E+01
0.35188E+02	0.31946E+00	0.11799E+03	0.14608E+03	0.36706E+02	0.29998E+02	0.21152E+02

STATION J = 25 , Z = 0.29200 , ITE = 100

I	RST	PCR	R	TAU	THK	B
P	PREL	POREL	PT	M*	BN	PCB
BETA	BETA*	DEV	ULB*	XMTH	DEL*	HSF
ALPHA	ETA	W	U	V	VU	VM
1	0.18957E+00	0.24666E+00	0.17284E+00	0.35877E+00	0.10000E-02	0.0
0.12452E+05	0.14546E+05	0.14114E+05	0.14095E+05	0.10125E+01	0.0	0.0
0.16799E+02	0.18113E+02	0.13134E+01	0.0	0.22740E-02	0.33752E-02	0.14843E+01
0.16878E+02	0.94328E+00	0.46519E+02	0.88847E+02	0.46308E+02	0.44313E+02	0.13445E+02
2	0.21251E+00	0.41566E+00	0.20104E+00	0.41736E+00	0.10000E-02	0.0
0.13026E+05	0.16502E+05	0.16244E+05	0.14970E+05	0.12137E+01	0.0	0.0
0.14468E+02	0.15718E+02	0.12503E+01	0.0	0.20999E-02	0.30161E-02	0.14363E+01
0.18293E+02	0.86991E+00	0.59943E+02	0.10334E+03	0.47713E+02	0.45302E+02	0.14976E+02
3	0.23107E+00	0.55249E+00	0.22179E+00	0.46047E+00	0.10000E-02	0.0
0.13370E+05	0.18581E+05	0.18195E+05	0.15001E+05	0.13724E+01	0.0	0.0
0.13109E+02	0.14319E+02	0.12093E+01	0.0	0.21092E-02	0.30104E-02	0.14273E+01
0.21378E+02	0.86257E+00	0.73397E+02	0.11401E+03	0.45669E+02	0.42527E+02	0.16647E+02
4	0.24753E+00	0.67376E+00	0.23930E+00	0.49685E+00	0.10000E-02	0.0
0.13602E+05	0.20220E+05	0.19709E+05	0.15102E+05	0.15082E+01	0.0	0.0
0.12145E+02	0.13318E+02	0.11707E+01	0.0	0.22105E-02	0.31577E-02	0.14285E+01
0.22434E+02	0.81665E+00	0.82715E+02	0.12301E+03	0.45601E+02	0.42150E+02	0.17402E+02
5	0.26238E+00	0.78323E+00	0.25496E+00	0.52937E+00	0.10000E-02	0.0
0.13760E+05	0.21934E+05	0.21275E+05	0.15070E+05	0.16300E+01	0.0	0.0
0.11396E+02	0.12530E+02	0.11337E+01	0.0	0.23205E-02	0.33256E-02	0.14332E+01
0.23838E+02	0.78379E+00	0.91812E+02	0.13106E+03	0.44888E+02	0.41059E+02	0.18142E+02
6	0.27604E+00	0.88367E+00	0.26921E+00	0.55899E+00	0.10000E-02	0.0
0.13929E+05	0.23629E+05	0.22804E+05	0.14994E+05	0.17408E+01	0.0	0.0
0.10791E+02	0.11890E+02	0.10995E+01	0.0	0.24463E-02	0.35246E-02	0.14397E+01
0.25100E+02	0.75437E+00	0.10014E+03	0.13839E+03	0.44197E+02	0.40023E+02	0.18746E+02
7	0.29180E+00	0.10000E+01	0.28392E+00	0.58954E+00	0.10000E-02	0.0
0.14075E+05	0.26217E+05	0.21644E+05	0.11119E+05	0.18469E+01	0.0	0.0
0.10237E+02	0.11295E+02	0.10584E+01	0.0	0.25012E-02	0.36007E-02	0.14396E+01
0.29146E+02	0.41756E+00	0.11203E+03	0.14595E+03	0.40879E+02	0.35702E+02	0.19910E+02

EXIT CONDITIONS

I ALPHA	R BETA	DEV V	H VM	P VU	PT WU	ETA M
1	0.172035E+00	0.154844E+01	0.137005E+03	0.136596E+05	0.154449E+05	0.112052E+01
0.164293E+02	0.166425E+02	0.464144E+02	0.131275E+02	0.445193E+02	0.439162E+02	0.458362E+02
2	0.200244E+00	0.294012E+01	0.129374E+03	0.128025E+05	0.149695E+05	0.889810E+00
0.160590E+02	0.128369E+02	0.473285E+02	0.130923E+02	0.454816E+02	0.574548E+02	0.589276E+02
3	0.221793E+00	0.197607E+01	0.129868E+03	0.130141E+05	0.150003E+05	0.862470E+00
0.201947E+02	0.123424E+02	0.453118E+02	0.156421E+02	0.425263E+02	0.714872E+02	0.731785E+02
4	0.239159E+00	0.168981E+01	0.131486E+03	0.131129E+05	0.151011E+05	0.816554E+00
0.215175E+02	0.116335E+02	0.453345E+02	0.166281E+02	0.421749E+02	0.807657E+02	0.824596E+02
5	0.254637E+00	0.175825E+01	0.130973E+03	0.131511E+05	0.150691E+05	0.763705E+00
0.225924E+02	0.107868E+02	0.445276E+02	0.171063E+02	0.41106E+02	0.897666E+02	0.914017E+02
6	0.269133E+00	0.218657E+01	0.129747E+03	0.131686E+05	0.149927E+05	0.754285E+00
0.227860E+02	0.970718E+01	0.434241E+02	0.168177E+02	0.400352E+02	0.983136E+02	0.997419E+02
7	0.284021E+00	0.154373E+01	0.667594E+02	0.133931E+05	0.110686E+05	0.412540E+00
0.279670E+02	0.974753E+01	0.440408E+02	0.189502E+02	0.356898E+02	0.110312E+03	0.111926E+03

OVERALL PERFORMANCE

NPSH	PHI	PSI	H	HI	RN	ETA	SS	GI
110.0690	0.08400	0.17484	122.173	154.318	4260759.00	0.79170	1.88276	2.83045

CVOL

0.1092E-03

PSI IDEAL = 0.2208+ PSI LOSS = 0.04600

BLADE LOADING DATA

J	Z	Z/ZT	PS	PP	WS	WP	DPB	PSIS	PSIP
1	0.0	0.0	0.52200E+02	0.11612E+05	0.10931E+03	0.0	0.11560E+05	-0.15752E+00	0.10802E+00
2	0.16952E+00		0.52200E+02	0.14256E+05	0.12117E+03	0.0	0.14204E+05	-0.15752E+00	0.16875E+00
3	0.19752E+00		0.52200E+02	0.16882E+05	0.13190E+03	0.0	0.16830E+05	-0.15752E+00	0.22909E+00
4	0.22195E+00		0.52200E+02	0.19503E+05	0.14180E+03	0.0	0.19450E+05	-0.15752E+00	0.28928E+00
5	0.24393E+00		0.52200E+02	0.22120E+05	0.15103E+03	0.0	0.22068E+05	-0.15752E+00	0.34940E+00
6	0.26407E+00		0.52200E+02	0.24735E+05	0.15973E+03	0.0	0.24683E+05	-0.15752E+00	0.40947E+00
7	0.28277E+00		0.52200E+02	0.27350E+05	0.16798E+03	0.0	0.27297E+05	-0.15752E+00	0.46953E+00

J	Z	Z/ZT
2	0.00500	0.01712

I	R	PS	PP	WS	WP	DPB	PSIS	PSIP
1	0.13546E+00	0.67559E+04	0.87457E+04	0.70850E+02	0.54321E+02	0.19698E+04	-0.35280E-02	0.42180E-01
2	0.16927E+00	0.52200E+02	0.97950E+04	0.12117E+03	0.67741E+02	0.97428E+04	-0.15752E+00	0.66283E-01
3	0.19743E+00	0.52200E+02	0.10981E+05	0.13190E+03	0.78046E+02	0.10929E+05	-0.15752E+00	0.93524E-01
4	0.22194E+00	0.52200E+02	0.11990E+05	0.14160E+03	0.88116E+02	0.11938E+05	-0.15752E+00	0.11671E+00
5	0.24393E+00	0.52200E+02	0.12977E+05	0.15103E+03	0.97217E+02	0.12924E+05	-0.15752E+00	0.13937E+00
6	0.26407E+00	0.52200E+02	0.13712E+05	0.15973E+03	0.10675E+03	0.13659E+05	-0.15752E+00	0.15625E+00
7	0.28277E+00	0.52200E+02	0.14100E+05	0.16798E+03	0.11703E+03	0.14047E+05	-0.15752E+00	0.16516E+00



J	Z	Z/ZT	I	R	PS	PP	WS	WP	DPB	PSIS	PSIP
3	0.01000	0.03425	1	0.13543E+00	0.67559E+04	0.87259E+04	0.70850E+02	0.54489E+02	0.19700E+04	-0.35280E-02	0.41726E-01
			2	0.16926E+00	0.67559E+04	0.98057E+04	0.88050E+02	0.61750E+02	0.30498E+04	-0.35280E-02	0.66529E-01
			3	0.19746E+00	0.52200E+02	0.10967E+05	0.13190E+03	0.78159E+02	0.10915E+05	-0.15752E+00	0.93200E-01
			4	0.22197E+00	0.52200E+02	0.11985E+05	0.14180E+03	0.86167E+02	0.11932E+05	-0.15752E+00	0.11658E+00
			5	0.24403E+00	0.52200E+02	0.12977E+05	0.15103E+03	0.97285E+02	0.12924E+05	-0.15752E+00	0.13937E+00
			6	0.26421E+00	0.52200E+02	0.13665E+05	0.15973E+03	0.10697E+03	0.13633E+05	-0.15752E+00	0.15564E+00
			7	0.28283E+00	0.52200E+02	0.14048E+05	0.16798E+03	0.11730E+03	0.13996E+05	-0.15752E+00	0.16398E+00

J	Z	Z/ZT	I	R	PS	PP	WS	WP	DPB	PSIS	PSIP
4	0.01500	0.05137	1	0.13540E+00	0.67559E+04	0.87295E+04	0.70650E+02	0.54434E+02	0.19735E+04	-0.35280E-02	0.41806E-01
			2	0.16916E+00	0.67559E+04	0.99256E+04	0.88050E+02	0.60662E+02	0.31697E+04	-0.35280E-02	0.69283E-01
			3	0.19735E+00	0.67559E+04	0.10947E+05	0.10231E+03	0.72008E+02	0.41911E+04	-0.35280E-02	0.92745E-01
			4	0.22191E+00	0.52200E+02	0.12072E+05	0.14180E+03	0.81061E+02	0.12020E+05	-0.15752E+00	0.11660E+00
			5	0.24397E+00	0.52200E+02	0.12952E+05	0.15103E+03	0.91940E+02	0.12900E+05	-0.15752E+00	0.13880E+00
			6	0.26417E+00	0.52200E+02	0.13563E+05	0.15973E+03	0.10268E+03	0.13530E+05	-0.15752E+00	0.15329E+00
			7	0.28281E+00	0.52200E+02	0.13941E+05	0.16798E+03	0.11453E+03	0.13888E+05	-0.15752E+00	0.16151E+00

Printout for Stations J=5 thru J=21 is omitted for Brevity.

J Z Z/ZT  
 22 0.24000 0.62192

I	R	PS	PP	WS	WP	DPB	PSIS	PSIP
1	0.16762E+00	0.10244E+05	0.12464E+05	0.37606E+02	0.40761E+02	0.22405E+04	0.76594E-01	0.12806E+00
2	0.19746E+00	0.10611E+05	0.12809E+05	0.59673E+02	0.58660E+02	0.19981E+04	0.89624E-01	0.13552E+00
3	0.21949E+00	0.11298E+05	0.13018E+05	0.75980E+02	0.74050E+02	0.17200E+04	0.10080E+00	0.14031E+00
4	0.23794E+00	0.11696E+05	0.13178E+05	0.89831E+02	0.84308E+02	0.14823E+04	0.10995E+00	0.14400E+00
5	0.25436E+00	0.12019E+05	0.13293E+05	0.10218E+03	0.94085E+02	0.12739E+04	0.11737E+00	0.14664E+00
6	0.26927E+00	0.12305E+05	0.13377E+05	0.11336E+03	0.10299E+03	0.10721E+04	0.12393E+00	0.14856E+00
7	0.28411E+00	0.12539E+05	0.13546E+05	0.12373E+03	0.11457E+03	0.10070E+04	0.12932E+00	0.15245E+00

J Z Z/ZT  
 23 0.26000 0.89041

I	R	PS	PP	WS	WP	DPB	PSIS	PSIP
1	0.17065E+00	0.10707E+05	0.13654E+05	0.30580E+02	0.45899E+02	0.29467E+04	0.87239E-01	0.15493E+00
2	0.19981E+00	0.11252E+05	0.12798E+05	0.55728E+02	0.58970E+02	0.15462E+04	0.99740E-01	0.13526E+00
3	0.22112E+00	0.11629E+05	0.13013E+05	0.73695E+02	0.73184E+02	0.13646E+04	0.10840E+00	0.14021E+00
4	0.23900E+00	0.11942E+05	0.13112E+05	0.68403E+02	0.82464E+02	0.11700E+04	0.11560E+00	0.14248E+00
5	0.25498E+00	0.12217E+05	0.13150E+05	0.10117E+03	0.91407E+02	0.93287E+03	0.12193E+00	0.14335E+00
6	0.26955E+00	0.12462E+05	0.13168E+05	0.11264E+03	0.99745E+02	0.70569E+03	0.12755E+00	0.14376E+00
7	0.28417E+00	0.12654E+05	0.13393E+05	0.12325E+03	0.11193E+03	0.73902E+03	0.13196E+00	0.14893E+00

21 J Z Z/ZT  
 24 0.28000 0.95890

I	R	PS	PP	WS	MP	DPB	PSIS	PSIP
1	0.17289E+00	0.11134E+05	0.13660E+05	0.22233E+02	0.45838E+02	0.25257E+04	0.97035E-01	0.15505E+00
2	0.20115E+00	0.11623E+05	0.12802E+05	0.52173E+02	0.58928E+02	0.11798E+04	0.10827E+00	0.13537E+00
3	0.22192E+00	0.11963E+05	0.13014E+05	0.71311E+02	0.73179E+02	0.10510E+04	0.11608E+00	0.14023E+00
4	0.23947E+00	0.12210E+05	0.13113E+05	0.86822E+02	0.82460E+02	0.90251E+03	0.12177E+00	0.14250E+00
5	0.25523E+00	0.12410E+05	0.13151E+05	0.10019E+03	0.91402E+02	0.74129E+03	0.12635E+00	0.14337E+00
6	0.26963E+00	0.12596E+05	0.13169E+05	0.11202E+03	0.99742E+02	0.57230E+03	0.13063E+00	0.14378E+00
7	0.28417E+00	0.12748E+05	0.13393E+05	0.12286E+03	0.11193E+03	0.64527E+03	0.13411E+00	0.14894E+00

J Z Z/ZT  
 25 0.29200 1.00000

I	R	PS	PP	WS	MP	DPB	PSIS	PSIP
1	0.17284E+00	0.11259E+05	0.13660E+05	0.19114E+02	0.45836E+02	0.24011E+04	0.99901E-01	0.15506E+00
2	0.20104E+00	0.11718E+05	0.12803E+05	0.51224E+02	0.58928E+02	0.10850E+04	0.11044E+00	0.13537E+00
3	0.22179E+00	0.12046E+05	0.13014E+05	0.70710E+02	0.73178E+02	0.96841E+03	0.11798E+00	0.14023E+00
4	0.23930E+00	0.12276E+05	0.13113E+05	0.86433E+02	0.82460E+02	0.83734E+03	0.12326E+00	0.14250E+00
5	0.25496E+00	0.12450E+05	0.13151E+05	0.99976E+02	0.91402E+02	0.70064E+03	0.12728E+00	0.14337E+00
6	0.26921E+00	0.12619E+05	0.13169E+05	0.11191E+03	0.99742E+02	0.54977E+03	0.13115E+00	0.14378E+00
7	0.28392E+00	0.12760E+05	0.13393E+05	0.12281E+03	0.11193E+03	0.63289E+03	0.13440E+00	0.14894E+00

INLET CONDITIONS

I	R	BETA	Q	M	U	PC	PREL	P
ALPHA			K			V	VM	VU
1	89.99997	0.13563	0.13478	70.84999	6909.50000	12.60000	11611.9453	6755.91406
		10.24401	1.38049	69.72055	12.60000		12.60000	0.00000
2	89.99997	0.16952	0.13478	88.04974	6909.50000	12.60000	14255.8594	6755.91406
		8.22733	0.89383	87.14352	12.60000		12.60000	0.00000
3	89.99997	0.19752	0.13478	102.31271	6909.50000	12.60000	16882.4570	6755.91406
		7.07405	0.66199	101.53381	12.60000		12.60000	0.00000
4	89.99997	0.22195	0.13478	114.78851	6909.50000	12.60000	19502.6484	6755.91406
		6.30189	0.52592	114.09482	12.60000		12.60000	0.00000
5		0.24393	0.13478	126.02280	6909.50000		22119.7095	6755.91406

89.99997	5.73813	0.43633	125.39127	12.60000	12.60000	0.00000
6	0.26407	0.13478	136.32800	6909.50000	24735.1914	6755.91406
89.99997	5.30309	0.37286	135.74437	12.60000	12.60000	0.00000
7	0.28277	0.13478	145.90343	6909.50000	27349.5508	6755.91406
89.99997	4.95415	0.32552	145.35822	12.60000	12.60000	0.00000

PHI	NPSH	THOMA	VT	PT	KTIP
0.0840	110.0690	0.3150	150.0009	6909.5000	0.3058

STATION J = 1 , Z = 0.0 , ITE = 1

I	P	BETA ALPHA	RST PREL BETA* ETA	PCR POREL DEV M	R PT DLB* U	TAU M* XMTH V	THK BN DEL* VU	B PCB HSF VM
1		0.15446E+00 0.67559E+04 0.10244E+02 0.90000E+02	0.21519E+00 0.11612E+05 0.65790E+01 0.70850E+02	0.13563E+00 0.69095E+04 0.65790E+01 0.69721E+02	0.28406E+00 0.0 0.10586E-03 0.15259E-04	0.0 0.0 0.0 0.0	0.0 0.0 0.14000E+01 0.12600E+02	
2		0.18459E+00 0.67559E+04 0.82273E+01 0.90000E+02	0.38735E+00 0.14256E+05 0.53717E+01 0.88050E+02	0.16952E+00 0.69095E+04 0.53717E+01 0.87143E+02	0.35505E+00 0.0 0.94957E-04 0.12600E+02	0.0 0.0 0.0 -0.30518E-04	0.0 0.0 0.14000E+01 0.12600E+02	
3		0.21045E+00 0.67559E+04 0.70740E+01 0.90000E+02	0.53512E+00 0.16882E+05 0.46552E+01 0.10231E+03	0.19752E+00 0.69095E+04 0.46552E+01 0.10153E+03	0.41368E+00 0.0 0.88090E-04 0.12600E+02	0.0 0.0 0.0 -0.15259E-04	0.0 0.0 0.14000E+01 0.12600E+02	
4		0.23346E+00 0.67559E+04 0.63019E+01 0.90000E+02	0.66661E+00 0.19503E+05 0.41664E+01 0.11479E+03	0.22195E+00 0.69095E+04 0.41664E+01 0.11409E+03	0.46485E+00 0.0 0.83165E-04 0.12600E+02	0.0 0.0 0.0 -0.45776E-04	0.0 0.0 0.14000E+01 0.12600E+02	
5		0.25440E+00 0.67559E+04 0.57361E+01 0.90000E+02	0.78626E+00 0.22120E+05 0.38053E+01 0.12602E+03	0.24393E+00 0.69095E+04 0.38053E+01 0.12539E+03	0.51068E+00 0.0 0.79372E-04 0.12600E+02	0.0 0.0 0.0 -0.45776E-04	0.0 0.0 0.14000E+01 0.12600E+02	
6		0.27374E+00 0.67559E+04 0.53031E+01 0.90000E+02	0.89678E+00 0.24735E+05 0.88275E+01 0.10000E+01	0.26407E+00 0.69095E+04 0.35244E+01 0.13574E+03	0.55306E+00 0.0 0.76313E-04 0.12600E+02	0.0 0.0 0.0 -0.16785E-03	0.0 0.0 0.14000E+01 0.12600E+02	
7		0.29180E+00 0.67559E+04 0.49542E+01 0.90000E+02	0.10000E+01 0.27350E+05 0.82520E+01 0.14590E+03	0.28277E+00 0.69095E+04 0.32979E+01 0.14536E+03	0.59223E+00 0.0 0.73766E-04 0.12600E+02	0.0 0.0 0.0 -0.12207E-03	0.0 0.0 0.14000E+01 0.12600E+02	

STATION J = 2 , Z = 0.00500 , ITE = 100

I P	BETA ALPHA	RST		PCK		R		TAU		THK		B	
		PREL BETA*	ETA	POREL DEV	W	PT DLB*	U	M*	XMTH V	BN DEL*	VU	PCB HSF VM	
1		0.15407E+00	0.21299E+00	0.13544E+00	0.26415E+00	0.13544E+00	0.13544E+00	0.26415E+00	0.56537E-02	0.0	0.0	0.0	0.0
0.77981E+04		0.11523E+05	0.11523E+05	0.79797E+04	0.17268E-01	0.79797E+04	0.79797E+04	0.17268E-01	0.0	0.0	0.0	0.0	0.0
0.12817E+02		0.16846E+02	0.40280E+01	0.0	0.18816E-03	0.0	0.18816E-03	0.18816E-03	0.27879E-03	0.14817E+01	0.14817E+01	0.14817E+01	0.14817E+01
0.58549E+02		0.93421E+00	0.62679E+02	0.69622E+02	0.16300E+02	0.69622E+02	0.69622E+02	0.16300E+02	0.65046E+01	0.13905E+02	0.13905E+02	0.13905E+02	0.13905E+02
2		0.18450E+00	0.38667E+00	0.16929E+00	0.32879E+00	0.16929E+00	0.16929E+00	0.32879E+00	0.60670E-02	0.24840E-02	0.24840E-02	0.24840E-02	0.24840E-02
0.87843E+04		0.14236E+05	0.14236E+05	0.91058E+04	0.23671E-01	0.91058E+04	0.91058E+04	0.23671E-01	0.58481E-03	0.75550E-02	0.75550E-02	0.75550E-02	0.75550E-02
0.10468E+02		0.13617E+02	0.31467E+01	0.14143E+01	0.19133E-03	0.14143E+01	0.14143E+01	0.19133E-03	0.28578E-03	0.14936E+01	0.14936E+01	0.14936E+01	0.14936E+01
0.45925E+02		0.98779E+00	0.75067E+02	0.87023E+02	0.18985E+02	0.87023E+02	0.87023E+02	0.18985E+02	0.13206E+02	0.13639E+02	0.13639E+02	0.13639E+02	0.13639E+02
3		0.21050E+00	0.53540E+00	0.19750E+00	0.58322E+00	0.19750E+00	0.19750E+00	0.58322E+00	0.61851E-02	0.80038E-02	0.80038E-02	0.80038E-02	0.80038E-02
0.90706E+04		0.16861E+05	0.16844E+05	0.93771E+04	0.32431E-01	0.93771E+04	0.93771E+04	0.32431E-01	0.16272E-02	0.20886E-01	0.20886E-01	0.20886E-01	0.20886E-01
0.86811E+01		0.11730E+02	0.28491E+01	0.28722E+01	0.17987E-03	0.28722E+01	0.28722E+01	0.17987E-03	0.26448E-03	0.14704E+01	0.14704E+01	0.14704E+01	0.14704E+01
0.47413E+02		0.98530E+00	0.89852E+02	0.10153E+03	0.18841E+02	0.10153E+03	0.10153E+03	0.18841E+02	0.12750E+02	0.13872E+02	0.13872E+02	0.13872E+02	0.13872E+02
4		0.23349E+00	0.66678E+00	0.22199E+00	0.43128E+00	0.22199E+00	0.22199E+00	0.43128E+00	0.61152E-02	0.12801E-01	0.12801E-01	0.12801E-01	0.12801E-01
0.92579E+04		0.19507E+05	0.19460E+05	0.95451E+04	0.40110E-01	0.95451E+04	0.95451E+04	0.40110E-01	0.23254E-02	0.29681E-01	0.29681E-01	0.29681E-01	0.29681E-01
0.78499E+01		0.10466E+02	0.26165E+01	0.33183E+01	0.17332E-03	0.33183E+01	0.33183E+01	0.17332E-03	0.25217E-03	0.14549E+01	0.14549E+01	0.14549E+01	0.14549E+01
0.49167E+02		0.98258E+00	0.10293E+03	0.11412E+03	0.18580E+02	0.11412E+03	0.11412E+03	0.18580E+02	0.12149E+02	0.14058E+02	0.14058E+02	0.14058E+02	0.14058E+02
5		0.25440E+00	0.78626E+00	0.24394E+00	0.47521E+00	0.24394E+00	0.24394E+00	0.47521E+00	0.59190E-02	0.17943E-01	0.17943E-01	0.17943E-01	0.17943E-01
0.93861E+04		0.22122E+05	0.22065E+05	0.96515E+04	0.47853E-01	0.96515E+04	0.96515E+04	0.47853E-01	0.29746E-02	0.37757E-01	0.37757E-01	0.37757E-01	0.37757E-01
0.70812E+01		0.95428E+01	0.24617E+01	0.35571E+01	0.16949E-03	0.35571E+01	0.35571E+01	0.16949E-03	0.24477E-03	0.14442E+01	0.14442E+01	0.14442E+01	0.14442E+01
0.50799E+02		0.97966E+00	0.11474E+03	0.12540E+03	0.16252E+02	0.12540E+03	0.12540E+03	0.16252E+02	0.11536E+02	0.14144E+02	0.14144E+02	0.14144E+02	0.14144E+02
6		0.27374E+00	0.89662E+00	0.26407E+00	0.51640E+00	0.26407E+00	0.26407E+00	0.51640E+00	0.56270E-02	0.23344E-01	0.23344E-01	0.23344E-01	0.23344E-01
0.94730E+04		0.24736E+05	0.24668E+05	0.97157E+04	0.55650E-01	0.97157E+04	0.97157E+04	0.55650E-01	0.35824E-02	0.45206E-01	0.45206E-01	0.45206E-01	0.45206E-01
0.64799E+01		0.88274E+01	0.23475E+01	0.36833E+01	0.16722E-03	0.36833E+01	0.36833E+01	0.16722E-03	0.24017E-03	0.14362E+01	0.14362E+01	0.14362E+01	0.14362E+01
0.52336E+02		0.97653E+00	0.12561E+03	0.13575E+03	0.17907E+02	0.13575E+03	0.13575E+03	0.17907E+02	0.10942E+02	0.14175E+02	0.14175E+02	0.14175E+02	0.14175E+02
7		0.29180E+00	0.10000E+01	0.28277E+00	0.55559E+00	0.28277E+00	0.28277E+00	0.55559E+00	0.52596E-02	0.25411E-01	0.25411E-01	0.25411E-01	0.25411E-01
0.95131E+04		0.27350E+05	0.26946E+05	0.94105E+04	0.54985E-01	0.94105E+04	0.94105E+04	0.54985E-01	0.36472E-02	0.45737E-01	0.45737E-01	0.45737E-01	0.45737E-01
0.60512E+01		0.82519E+01	0.22007E+01	0.34794E+01	0.16586E-03	0.34794E+01	0.34794E+01	0.16586E-03	0.23717E-03	0.14300E+01	0.14300E+01	0.14300E+01	0.14300E+01
0.54166E+02		0.86094E+00	0.13579E+03	0.14536E+03	0.17652E+02	0.14536E+03	0.14536E+03	0.17652E+02	0.10329E+02	0.14314E+02	0.14314E+02	0.14314E+02	0.14314E+02

STATION J = 3 , Z = 0.01000 , ITE = 100

I P ALPHA	RST PREL BETA*	PCR PCREL DEV W	R PT DLB*	TAU			THK			B		
				M*	XMTH	V	BN	DEL*	VU	PCB	HSF	VM
1	0.15393E+00	0.21219E+00	0.13537E+00	0.24619E+00	0.10820E-01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.81730E+04	0.11594E+05	0.11499E+05	0.84394E+04	0.34524E-01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.14698E+02	0.16854E+02	0.21554E+01	0.0	0.25353E-03	0.36147E-03	0.15046E+01	0.15088E+02	0.15088E+02	0.15088E+02	0.15088E+02	0.15088E+02	0.15088E+02
0.51349E+02	0.94173E+00	0.59465E+02	0.69585E+02	0.19320E+02	0.12067E+02	0.15088E+02	0.15088E+02	0.15088E+02	0.15088E+02	0.15088E+02	0.15088E+02	0.15088E+02
2	0.18451E+00	0.38691E+00	0.16922E+00	0.30847E+00	0.10820E-01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.96276E+04	0.14230E+05	0.14194E+05	0.10167E+05	0.46055E-01	0.86135E-03	0.11856E-01	0.11856E-01	0.11856E-01	0.11856E-01	0.11856E-01	0.11856E-01	0.11856E-01
0.12179E+02	0.13622E+02	0.14434E+01	0.0	0.28203E-03	0.43386E-03	0.15384E+01	0.15384E+01	0.15384E+01	0.15384E+01	0.15384E+01	0.15384E+01	0.15384E+01
0.36635E+02	0.98902E+00	0.68973E+02	0.86988E+02	0.24385E+02	0.19568E+02	0.14551E+02	0.14551E+02	0.14551E+02	0.14551E+02	0.14551E+02	0.14551E+02	0.14551E+02
3	0.21051E+00	0.53550E+00	0.19751E+00	0.36044E+00	0.10820E-01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.10486E+05	0.16862E+05	0.16631E+05	0.11103E+05	0.60403E-01	0.23284E-02	0.31775E-01	0.31775E-01	0.31775E-01	0.31775E-01	0.31775E-01	0.31775E-01	0.31775E-01
0.10590E+02	0.11730E+02	0.11397E+01	0.0	0.28159E-03	0.42996E-03	0.15269E+01	0.15269E+01	0.15269E+01	0.15269E+01	0.15269E+01	0.15269E+01	0.15269E+01
0.34668E+02	0.98804E+00	0.81310E+02	0.10153E+03	0.26270E+02	0.21606E+02	0.14943E+02	0.14943E+02	0.14943E+02	0.14943E+02	0.14943E+02	0.14943E+02	0.14943E+02
4	0.23360E+00	0.66740E+00	0.22205E+00	0.40549E+00	0.10820E-01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.11410E+05	0.19514E+05	0.19448E+05	0.12119E+05	0.72759E-01	0.32703E-02	0.44409E-01	0.44409E-01	0.44409E-01	0.44409E-01	0.44409E-01	0.44409E-01	0.44409E-01
0.95369E+01	0.10464E+02	0.92659E+00	0.0	0.28698E-03	0.43758E-03	0.15241E+01	0.15241E+01	0.15241E+01	0.15241E+01	0.15241E+01	0.15241E+01	0.15241E+01
0.32410E+02	0.98747E+00	0.91527E+02	0.11415E+03	0.28293E+02	0.23886E+02	0.15164E+02	0.15164E+02	0.15164E+02	0.15164E+02	0.15164E+02	0.15164E+02	0.15164E+02
5	0.25462E+00	0.78752E+00	0.24411E+00	0.44595E+00	0.10820E-01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.12331E+05	0.22142E+05	0.22060E+05	0.13127E+05	0.84867E-01	0.41216E-02	0.55786E-01	0.55786E-01	0.55786E-01	0.55786E-01	0.55786E-01	0.55786E-01	0.55786E-01
0.87582E+01	0.95365E+01	0.77837E+00	0.0	0.29240E-03	0.44488E-03	0.15215E+01	0.15215E+01	0.15215E+01	0.15215E+01	0.15215E+01	0.15215E+01	0.15215E+01
0.30580E+02	0.98695E+00	0.10071E+03	0.12548E+03	0.30142E+02	0.25950E+02	0.15334E+02	0.15334E+02	0.15334E+02	0.15334E+02	0.15334E+02	0.15334E+02	0.15334E+02
6	0.27378E+00	0.89704E+00	0.26420E+00	0.46260E+00	0.10820E-01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.12895E+05	0.24753E+05	0.24653E+05	0.13699E+05	0.96755E-01	0.49020E-02	0.66195E-01	0.66195E-01	0.66195E-01	0.66195E-01	0.66195E-01	0.66195E-01	0.66195E-01
0.81543E+01	0.88232E+01	0.66890E+00	0.0	0.29056E-03	0.43853E-03	0.15092E+01	0.15092E+01	0.15092E+01	0.15092E+01	0.15092E+01	0.15092E+01	0.15092E+01
0.30920E+02	0.98554E+00	0.11071E+03	0.13581E+03	0.30561E+02	0.26218E+02	0.15704E+02	0.15704E+02	0.15704E+02	0.15704E+02	0.15704E+02	0.15704E+02	0.15704E+02
7	0.29160E+00	0.10000E+01	0.28279E+00	0.51899E+00	0.10518E-01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.12818E+05	0.27353E+05	0.26786E+05	0.13047E+05	0.10405E+00	0.49853E-02	0.66932E-01	0.66932E-01	0.66932E-01	0.66932E-01	0.66932E-01	0.66932E-01	0.66932E-01
0.74558E+01	0.82514E+01	0.79564E+00	0.0	0.27970E-03	0.41565E-03	0.14861E+01	0.14861E+01	0.14861E+01	0.14861E+01	0.14861E+01	0.14861E+01	0.14861E+01
0.33721E+02	0.91574E+00	0.12258E+03	0.14537E+03	0.28651E+02	0.23830E+02	0.15905E+02	0.15905E+02	0.15905E+02	0.15905E+02	0.15905E+02	0.15905E+02	0.15905E+02

Printout for Stations J=4 thru J=23 is omitted for Brevity.

STATION J = 24 , Z = 0.28000 , ILE = 100

I P	BETA ALPHA	RST PREL BETA* ETA	PCR POREL DEV W	K PT DLB* U	TAU M* XMTH V	THK BN DEL* VU	B PCB HSF VM
1	0.11858E+05 0.16951E+02 0.21571E+02	0.18864E+00 0.14505E+05 0.17876E+02 0.93877E+00	0.23977E+00 0.14100E+05 0.92466E+00 0.52305E+02	0.17237E+00 0.13116E+05 0.0 0.88607E+02	0.32576E+00 0.97327E+00 0.15670E-02 0.41480E+02	0.10820E-01 0.0 0.21607E-02 0.38575E+02	0.0 0.0 0.13789E+01 0.15250E+02
2	0.12005E+05 0.14678E+02 0.24830E+02	0.21043E+00 0.16440E+05 0.15573E+02 0.87511E+00	0.40038E+00 0.16168E+05 0.89511E+00 0.67705E+02	0.19953E+00 0.13348E+05 0.0 0.10257E+03	0.37760E+00 0.11659E+01 0.15518E-02 0.40853E+02	0.10820E-01 0.0 0.21179E-02 0.37076E+02	0.0 0.0 0.13649E+01 0.17155E+02
3	0.12113E+05 0.13342E+02 0.27953E+02	0.22873E+00 0.18331E+05 0.14215E+02 0.82763E+00	0.53522E+00 0.17923E+05 0.87252E+00 0.80175E+02	0.21958E+00 0.13211E+05 0.0 0.11288E+03	0.41583E+00 0.13162E+01 0.16775E-02 0.39470E+02	0.10820E-01 0.0 0.23049E-02 0.34865E+02	0.0 0.0 0.13740E+01 0.18501E+02
4	0.12238E+05 0.12367E+02 0.28842E+02	0.24519E+00 0.19934E+05 0.13212E+02 0.77004E+00	0.65654E+00 0.19384E+05 0.84524E+00 0.89193E+02	0.23696E+00 0.13205E+05 0.0 0.12181E+03	0.44895E+00 0.14458E+01 0.18337E-02 0.39599E+02	0.10820E-01 0.0 0.25407E-02 0.34687E+02	0.0 0.0 0.13856E+01 0.19103E+02
5	0.12352E+05 0.11601E+02 0.30242E+02	0.26020E+00 0.21657E+05 0.12418E+02 0.73010E+00	0.76717E+00 0.20939E+05 0.81665E+00 0.98074E+02	0.25270E+00 0.13117E+05 0.0 0.12990E+03	0.47893E+00 0.15619E+01 0.19868E-02 0.39159E+02	0.10820E-01 0.0 0.27753E-02 0.33830E+02	0.0 0.0 0.13969E+01 0.19722E+02
6	0.12458E+05 0.12225E+02 0.30059E+02	0.27324E+00 0.22537E+05 0.11765E+02 0.65368E+00	0.86322E+00 0.21664E+05 -0.43942E+00 0.10208E+03	0.26672E+00 0.13386E+05 0.0 0.13711E+03	0.50565E+00 0.16635E+01 0.22232E-02 0.43151E+02	0.10820E-01 0.0 0.31417E-02 0.37348E+02	0.0 0.0 0.14132E+01 0.21614E+02
7	0.12547E+05 0.61459E+01 0.36038E+02	0.29180E+00 0.27086E+05 0.11145E+02 0.27413E+00	0.10000E+01 0.22444E+05 0.29991E+01 0.12259E+03	0.28252E+00 0.87486E+04 0.0 0.14523E+03	0.53573E+00 0.17732E+01 0.23252E-02 0.29526E+02	0.10820E-01 0.0 0.33059E-02 0.23875E+02	0.0 0.0 0.14216E+01 0.17370E+02



I	RST	PCR	R	TAU	THK	B
P	PREL	POREL	PT	M*	BN	PCB
BETA	BETA*	DEV	DLB*	XMTH	DEL*	HSF
ALPHA	ETA	W	U	V	VU	VM
1	0.18661E+00	0.23958E+00	0.17236E+00	0.35777E+00	0.10000E-02	0.0
0.12117E+05	0.14503E+05	0.14084E+05	0.13530E+05	0.10121E+01	0.0	0.0
0.16839E+02	0.13160E+02	0.13207E+01	0.0	0.18843E-02	0.26835E-02	0.14242E+01
0.19307E+02	0.94044E+00	0.49664E+02	0.58600E+02	0.43513E+02	0.41065E+02	0.14387E+02
2	0.21039E+00	0.40010E+00	0.19950E+00	0.41417E+00	0.10000E-02	0.0
0.12673E+05	0.16437E+05	0.16168E+05	0.14363E+05	0.12102E+01	0.0	0.0
0.14564E+02	0.15832E+02	0.12683E+01	0.0	0.20173E-02	0.28867E-02	0.14310E+01
0.20397E+02	0.89054E+00	0.62376E+02	0.10255E+03	0.45005E+02	0.42183E+02	0.15685E+02
3	0.22873E+00	0.53523E+00	0.21956E+00	0.45565E+00	0.10000E-02	0.0
0.12998E+05	0.18329E+05	0.17926E+05	0.14468E+05	0.13647E+01	0.0	0.0
0.13227E+02	0.14457E+02	0.12304E+01	0.0	0.21519E-02	0.30956E-02	0.14386E+01
0.22702E+02	0.65258E+00	0.74235E+02	0.11287E+03	0.44010E+02	0.40601E+02	0.16985E+02
4	0.24516E+00	0.65627E+00	0.23694E+00	0.49195E+00	0.10000E-02	0.0
0.13253E+05	0.19932E+05	0.19391E+05	0.14608E+05	0.14978E+01	0.0	0.0
0.12254E+02	0.13443E+02	0.11887E+01	0.0	0.23137E-02	0.33502E-02	0.14480E+01
0.23475E+02	0.60456E+00	0.83089E+02	0.12180E+03	0.44270E+02	0.40606E+02	0.17635E+02
5	0.26005E+00	0.76600E+00	0.25260E+00	0.52448E+00	0.10000E-02	0.0
0.13459E+05	0.21644E+05	0.20942E+05	0.14607E+05	0.16173E+01	0.0	0.0
0.11495E+02	0.12642E+02	0.11476E+01	0.0	0.24607E-02	0.35830E-02	0.14561E+01
0.24778E+02	0.77160E+00	0.91985E+02	0.12985E+03	0.43737E+02	0.39711E+02	0.18330E+02
6	0.27303E+00	0.86166E+00	0.26654E+00	0.55343E+00	0.10000E-02	0.0
0.13625E+05	0.22512E+05	0.21662E+05	0.14974E+05	0.17217E+01	0.0	0.0
0.12049E+02	0.12005E+02	-0.43232E-01	0.0	0.27402E-02	0.40422E-02	0.14752E+01
0.24811E+02	0.70292E+00	0.95846E+02	0.13701E+03	0.47679E+02	0.43278E+02	0.20006E+02
7	0.29180E+00	0.10000E+01	0.28241E+00	0.58641E+00	0.10000E-02	0.0
0.13760E+05	0.27070E+05	0.22303E+05	0.10091E+05	0.18347E+01	0.0	0.0
0.82264E+01	0.11353E+02	0.31269E+01	0.0	0.27234E-02	0.39950E-02	0.14669E+01
0.29961E+02	0.38910E+00	0.11727E+03	0.14518E+03	0.33600E+02	0.29110E+02	0.16780E+02

EXIT CONDITIONS

I	ALPHA	R	BETA	DEV	H	VM	P	PT	ETA
				V			VU	MU	W
1	0.171517E+00	0.237785E+01	0.126320E+03	0.132517E+05	0.147792E+05	0.111794E+01	0.469026E+02	0.147792E+05	0.111794E+01
	0.179004E+02	0.433654E+02	0.133289E+02	0.412662E+02	0.469026E+02	0.487598E+02			
2	0.198671E+00	0.289563E+01	0.119626E+03	0.124422E+05	0.143622E+05	0.890414E+00	0.423591E+02	0.143622E+05	0.890414E+00
	0.180424E+02	0.445497E+02	0.137979E+02	0.423591E+02	0.597687E+02	0.613408E+02			
3	0.219578E+00	0.198616E+01	0.121316E+03	0.126259E+05	0.144675E+05	0.852463E+00	0.405976E+02	0.144675E+05	0.852463E+00
	0.214899E+02	0.436307E+02	0.159836E+02	0.405976E+02	0.722772E+02	0.740234E+02			
4	0.236798E+00	0.169440E+01	0.123563E+03	0.127349E+05	0.146074E+05	0.804451E+00	0.127349E+05	0.146074E+05	0.804451E+00
	0.225566E+02	0.439967E+02	0.168770E+02	0.406310E+02	0.810957E+02	0.828332E+02			
5	0.252275E+00	0.184470E+01	0.123547E+03	0.127917E+05	0.146065E+05	0.771504E+00	0.397619E+02	0.146065E+05	0.771504E+00
	0.233616E+02	0.433126E+02	0.171749E+02	0.397619E+02	0.899212E+02	0.915468E+02			
6	0.266331E+00	0.995323E+00	0.129427E+03	0.128368E+05	0.149728E+05	0.702833E+00	0.433110E+02	0.149728E+05	0.702833E+00
	0.228219E+02	0.469896E+02	0.182258E+02	0.433110E+02	0.935972E+02	0.953553E+02			
7	0.282380E+00	0.381874E+01	0.512748E+02	0.129023E+05	0.101039E+05	0.390682E+00	0.291135E+02	0.101039E+05	0.390682E+00
	0.278028E+02	0.753595E+01	0.153517E+02	0.291135E+02	0.116045E+03	0.117056E+03			

OVERALL PERFORMANCE

NPSH	PHI	PSI	H	HI	RN	ETA	SS	QI
110.0690	0.08400	0.15274	106.727	145.541	4260759.00	0.73331	1.88276	2.83045

CVOL

0.1090E-03

PSI IDEAL = 0.20828      PSI LOSS = 0.05555

BLADE LOADING DATA

J	Z	Z/ZT	R	PS	PP	MS	WP	DPB	PSIS	PSIP
1	0.0	0.0								
I										
1	0.13563E+00	0.52200E+02	0.11612E+05	0.10931E+03	0.0	0.11560E+05	-0.15752E+00	0.10802E+00		
2	0.16952E+00	0.52200E+02	0.14256E+05	0.12117E+03	0.0	0.14204E+05	-0.15752E+00	0.16875E+00		
3	0.19752E+00	0.52200E+02	0.16882E+05	0.13190E+03	0.0	0.16830E+05	-0.15752E+00	0.22909E+00		
4	0.22195E+00	0.52200E+02	0.19503E+05	0.14180E+03	0.0	0.19450E+05	-0.15752E+00	0.28928E+00		
5	0.24393E+00	0.52200E+02	0.22120E+05	0.15103E+03	0.0	0.22068E+05	-0.15752E+00	0.34940E+00		
6	0.26407E+00	0.52200E+02	0.24735E+05	0.15973E+03	0.0	0.24683E+05	-0.15752E+00	0.40947E+00		
7	0.26277E+00	0.52200E+02	0.27350E+05	0.16798E+03	0.0	0.27297E+05	-0.15752E+00	0.46953E+00		

J	Z	Z/ZT	R	PS	PP	MS	WP	DPB	PSIS	PSIP
2	0.00500	0.01712								
I										
1	0.13544E+00	0.67559E+04	0.89449E+04	0.70850E+02	0.52376E+02	0.21889E+04	-0.35280E-02	0.46754E-01		
2	0.16929E+00	0.52200E+02	0.98840E+04	0.12117E+03	0.67069E+02	0.98318E+04	-0.15752E+00	0.68327E-01		
3	0.19750E+00	0.52200E+02	0.10976E+05	0.13190E+03	0.78124E+02	0.10924E+05	-0.15752E+00	0.93420E-01		
4	0.22199E+00	0.52200E+02	0.11940E+05	0.14180E+03	0.68443E+02	0.11888E+05	-0.15752E+00	0.11556E+00		
5	0.24394E+00	0.52200E+02	0.12721E+05	0.15103E+03	0.98580E+02	0.12668E+05	-0.15752E+00	0.13349E+00		
6	0.26407E+00	0.52200E+02	0.10435E+05	0.15973E+03	0.12159E+03	0.10382E+05	-0.15752E+00	0.80977E-01		
7	0.26277E+00	0.52200E+02	0.22113E+04	0.16796E+03	0.16120E+03	0.21591E+04	-0.15752E+00	-0.10792E+00		

J	Z	Z/ZT	R	PS	PP	MS	MP	DPB	PSIS	PSIP
3	0.01000	0.03425								
I										
1	0.13537E+00	0.67559E+04	0.89471E+04	0.70850E+02	0.52305E+02	0.21912E+04	-0.35280E-02	0.46807E-01		
2	0.16922E+00	0.52200E+02	0.98776E+04	0.12117E+03	0.67073E+02	0.98254E+04	-0.15752E+00	0.68180E-01		
3	0.19751E+00	0.52200E+02	0.10973E+05	0.13190E+03	0.78153E+02	0.10921E+05	-0.15752E+00	0.93345E-01		
4	0.22205E+00	0.52200E+02	0.11924E+05	0.14180E+03	0.68578E+02	0.11872E+05	-0.15752E+00	0.11519E+00		
5	0.24411E+00	0.52200E+02	0.12708E+05	0.15103E+03	0.98752E+02	0.12656E+05	-0.15752E+00	0.13320E+00		
6	0.26420E+00	0.52200E+02	0.98319E+04	0.15973E+03	0.12419E+03	0.97797E+04	-0.15752E+00	0.67130E-01		
7	0.28279E+00	0.52200E+02	0.15381E+04	0.16798E+03	0.16335E+03	0.14859E+04	-0.15752E+00	-0.12339E+00		

J	Z	Z/ZT
4	0.01500	0.05137

I	R	PS	PP	MS	MP	DPB	PSIS	PSIP
1	0.13530E+00	0.67559E+04	0.89311E+04	0.70850E+02	0.52418E+02	0.21752E+04	-0.35280E-02	0.46439E-01
2	0.16908E+00	0.67559E+04	0.98767E+04	0.88050E+02	0.61789E+02	0.31208E+04	-0.35280E-02	0.68160E-01
3	0.19738E+00	0.67559E+04	0.10965E+05	0.10231E+03	0.71890E+02	0.42095E+04	-0.35280E-02	0.93169E-01
4	0.22197E+00	0.52200E+02	0.11901E+05	0.14180E+03	0.82149E+02	0.11849E+05	-0.15752E+00	0.11466E+00
5	0.24405E+00	0.52200E+02	0.12729E+05	0.15103E+03	0.93223E+02	0.12677E+05	-0.15752E+00	0.13369E+00
6	0.26409E+00	0.52200E+02	0.83918E+04	0.15973E+03	0.12617E+03	0.83396E+04	-0.15752E+00	0.34051E-01
7	0.28270E+00	0.52200E+02	0.15086E+04	0.16798E+03	0.16269E+03	0.14564E+04	-0.15752E+00	-0.12408E+00

Printout for Stations J=5 thru J=21 is omitted for Brevity.

J Z Z/zt  
22 0.24000 0.82192

I	R	PS	PP	WS	WP	DP6	PSIS	PSIP
1	0.16718E+00	0.10120E+05	0.12172E+05	0.39276E+02	0.44104E+02	0.20528E+04	0.73740E-01	0.12089E+00
2	0.19598E+00	0.10551E+05	0.12445E+05	0.61687E+02	0.61304E+02	0.18939E+04	0.83642E-01	0.12715E+00
3	0.21721E+00	0.10836E+05	0.12646E+05	0.79061E+02	0.74858E+02	0.18099E+04	0.90188E-01	0.13176E+00
4	0.23537E+00	0.11095E+05	0.12850E+05	0.93228E+02	0.84405E+02	0.17552E+04	0.96137E-01	0.13648E+00
5	0.25166E+00	0.11338E+05	0.13024E+05	0.10557E+03	0.93729E+02	0.16861E+04	0.10172E+00	0.14045E+00
6	0.26604E+00	0.11507E+05	0.13127E+05	0.11694E+03	0.98143E+02	0.16202E+04	0.10560E+00	0.14282E+00
7	0.28225E+00	0.11855E+05	0.13372E+05	0.12656E+03	0.11869E+03	0.15179E+04	0.11359E+00	0.14846E+00

J Z Z/zt  
23 0.26000 0.89041

I	R	PS	PP	WS	WP	DP6	PSIS	PSIP
1	0.17026E+00	0.10527E+05	0.13244E+05	0.33483E+02	0.48841E+02	0.27166E+04	0.83106E-01	0.14551E+00
2	0.19804E+00	0.10894E+05	0.12437E+05	0.58954E+02	0.61386E+02	0.15432E+04	0.91519E-01	0.12697E+00
3	0.21863E+00	0.11170E+05	0.12625E+05	0.76843E+02	0.74029E+02	0.14549E+04	0.97872E-01	0.13129E+00
4	0.23638E+00	0.11402E+05	0.12734E+05	0.91509E+02	0.82838E+02	0.13322E+04	0.10319E+00	0.13380E+00
5	0.25234E+00	0.11600E+05	0.12791E+05	0.10428E+03	0.91552E+02	0.11904E+04	0.10775E+00	0.13510E+00
6	0.26648E+00	0.11736E+05	0.12836E+05	0.11592E+03	0.95360E+02	0.11001E+04	0.11066E+00	0.13613E+00
7	0.28242E+00	0.12049E+05	0.12902E+05	0.12576E+03	0.11706E+03	0.85332E+03	0.11805E+00	0.13765E+00

J Z Z/zt  
24 0.28000 0.95690

I	R	PS	PP	WS	WP	DPB	PSIS	PSIP
1	0.17237E+00	0.10897E+05	0.13251E+05	0.27180E+02	0.48762E+02	0.23542E+04	0.91603E-01	0.14568E+00
2	0.19953E+00	0.11266E+05	0.12442E+05	0.55589E+02	0.61341E+02	0.11757E+04	0.10008E+00	0.12709E+00
3	0.21958E+00	0.11511E+05	0.12626E+05	0.74518E+02	0.74023E+02	0.11153E+04	0.10569E+00	0.13131E+00
4	0.23696E+00	0.11709E+05	0.12735E+05	0.89759E+02	0.82833E+02	0.10261E+04	0.11024E+00	0.13381E+00
5	0.25270E+00	0.11885E+05	0.12792E+05	0.10286E+03	0.91547E+02	0.90660E+03	0.11429E+00	0.13512E+00
6	0.26672E+00	0.12013E+05	0.12837E+05	0.11466E+03	0.95355E+02	0.82400E+03	0.11723E+00	0.13616E+00
7	0.26252E+00	0.12278E+05	0.12902E+05	0.12482E+03	0.11706E+03	0.62443E+03	0.12332E+00	0.13766E+00

J Z Z/ZT

25 0.29200 1.00000

I	R	PS	PP	WS	WP	DPB	PSIS	PSIP
1	0.17236E+00	0.10993E+05	0.13252E+05	0.25266E+02	0.48760E+02	0.22583E+04	0.93810E-01	0.14569E+00
2	0.19950E+00	0.11367E+05	0.12442E+05	0.54650E+02	0.61341E+02	0.10756E+04	0.10238E+00	0.12709E+00
3	0.21956E+00	0.11598E+05	0.12626E+05	0.73910E+02	0.74023E+02	0.10260E+04	0.10770E+00	0.13131E+00
4	0.23694E+00	0.11788E+05	0.12735E+05	0.69296E+02	0.82833E+02	0.94638E+03	0.11208E+00	0.13381E+00
5	0.25260E+00	0.11968E+05	0.12792E+05	0.10244E+03	0.91547E+02	0.82342E+03	0.11620E+00	0.13512E+00
6	0.26654E+00	0.12107E+05	0.12837E+05	0.11426E+03	0.95355E+02	0.73011E+03	0.11938E+00	0.13616E+00
7	0.28241E+00	0.12355E+05	0.12902E+05	0.12450E+03	0.11706E+03	0.54758E+03	0.12508E+00	0.13766E+00

E. HYDRODYNAMIC COMPUTER PROGRAM LISTING

```

C *****
C *          INDUCER HYDRODYNAMIC PROGRAM          *
C *
C *****
C          F.O.R.D.C.
REAL LI,LOW,M1,M2,M3,M4,N1,N2,N3,N4,LOWLIM
REAL ML,M,K,MP,NU,MU,MSTR,NPSH,MOM,MOMP
INTEGER CASE,CASES
LOGICAL ERROR
D I M E N S I O N
1  RIN (15),  BSIN (15),  TCBSI (15),  WIN (15),
2  PRELI(15), BSEX (15),  WJ1 (15),  WEX (15),
3  WNJ (15),  DBS (15),  REX (15),  VEX (15),
4  DBSP (15), PORELP(15), RVU (15),  MOM (15),
5  A (15),   AP (15),   MOMP (15),  PCR (15),
6  SI (15),  SIB (15),  R (15),   M (15),
7  DM (15),  HIO (15),  BETA (15),  W (15),
8  B (15),  PREL (15),  RP (15),  BETAP(15),
9  SIP (15), MP (15),  TT (60),  BP (15),
1  PRELP(15), DY (15),  DYP (15),  BETAS(15),
2  TAU (15), ZBL (15),  PX (15),  TA (60),
3  E (15),  PCR1 (15),  TAUP (15),  RSTL (15),
4  SIS (15), SISP (15),  WP (15),  PXP (15),
5  RSTS (15), PRELEX(15),  ESV (15),  ITB (15),
6  POREL(15), DBDM (15),  DWDM (15),  HSF (15),
7  XMTH (15), HSFP (15),  XMTHP (15),  PO (15),
8  VA (15),  ALPHI (15),  Q (15),  HO (15),
9  XIOI (15), XMTHI (15),  BIN (15),  TERM1(15)
D I M E N S I O N
1  TERM2(15), BTS (60),  BETASP(15),  T (15),
2  TP (15),  SBS (15),  TBS (15),  CBS (15),
3  TITLE(20), CSB (15),  PCBB (15),  DELW (15),
4  Z (60),  RH (60),  RT (60),  BHS (60)
D I M E N S I O N
1  TCBS (60,15), ML(60,15),  BL (60,15),  PRELL(60,15),
2  PXL (60,15), DPBN(60,15), RL (60,15)
DIMENSION DC(15),DCP(15)
DIMENSION WNC(60,15),DBTC(60,15),WPX(60,15),WSX(60,15),
1  PSX(60,15),PPX(60,15),WVX(60,15),TAUVX(60,15),DMVX(60,15),
2  DYX(60,15),BETASX(60,15),FUNC(60),YOUT(60),TGIF(4),XCODM(20),
3  YFLR(20)
DATA XCODM / .01,.02,.03,.04,.05,.06,.07,.08,.09,.10,.12,.14,.16,
1  .18,.20,.25,.30,.35,.40/,
2  YFLR / .007,.007,.007,.008,.01,.014,.025,.041,.054,.06,.075,
3  .085,.094,.10,.107,.123,.134,.143,.152/
CALL ZERO ( NI,TGIF(4) )
***** INPUT *****
READ(5,2,END=999) TITLE
WRITE(6,4) TITLE
READ(5,3) NI , NJ ,NB ,CASES ,G, ALPWH, ALPWT, CBHR
WRITE(6,5) NI,NJ,NB,CASES,G,CBHR

```



```

C      BLADE HUB AND TIP DESCRIPTION                                00000560
C                                                                 00000570
C      WRITE(6,6)                                                00000580
C      READ(5,7) (Z(I), RH(I), RT(I), BHS(I), BTS(I), TT(I), TA(I), 00000590
1      I = 1, NJ )                                               00000600
C      WRITE(6,8) (I, Z(I), RH(I), RT(I), BHS(I), BTS(I), TT(I), TA(I), 00000610
1      I = 1, NJ )                                               00000620
C      DO 88 J = 1, NJ                                           00000630
C      BHS(J) = BHS(J) / 57.2958                                  00000640
C      BTS(J) = BTS(J) / 57.2958                                  00000650
88 CONTINUE                                                       00000660
C                                                                 00000670
C      COEFFICIENTS FOR SWEEPED LEADING EDGE                       00000680
C      READ(5,6091) Z0,Z1,Z2,Z3                                   00000690
C                                                                 00000700
C      ALPWT = ALPWT / 57.29577                                   00000710
C      ALPWH = ALPWH / 57.29577                                   00000720
C      BTSB = ( BTS(1) + BTS(NJ) ) / 2.0                          00000730
C      C2 = 6.2832 / NB                                           00000740
C      XYZ = Z0 + Z1*RT(1) + Z2*RT(1)**2 + Z3*RT(1)**3          00000750
C      SIG = ( Z(NJ) - XYZ ) / ( C2 * RT(1) * SIN(BTSB) )        00000760
C                                                                 00000770
C      IF( CBHR .EQ. 0.0 ) GO TO 770                               00000780
C      CLEAR = CBHR * ( RT(1) - RH(1) )                           00000790
C      CODM = CLEAR / ((Z(NJ) - Z(1)) * SIN(BTSB))                00000800
C      CALL NEWGG (19, CODM, FLR, XCODM, YFLR )                    00000810
C      FLR = FLR * 3.141592                                         00000820
770 WRITE(6,760) Z0,Z1,Z2,Z3                                       00000830
760 FORMAT(// ' SWEEPED LEADING EDGE COEFFICIENTS' // ' Z0=',F10.5// ' Z1=', 00000840
1      F10.5// ' Z2=',F10.5// ' Z3=',F10.5// )                    00000850
C      ALPH = ALPWH * 57.29578                                     00000860
C      ALPT = ALPWT * 57.29578                                     00000870
C      WRITE(6,761) SIG,ALPH,ALPT                                  00000880
761 FORMAT(T9, ' SOLIDITY', T24, ' ALPWH', T38, ' ALPWT' / 3F15.7) 00000890
C                                                                 00000900
C      ***** END OF INPUT *****                                00000910
C                                                                 00000920
C      OPERATING CONDITIONS                                       00000930
C                                                                 00000940
C      CASE = 1                                                    00000950
20 READ (5,17,END=999) RHO, MU, PSAT, SN, LOADOP                 00000960
C      IF( CBHR .EQ. 0.0 ) GO TO 775                              00000970
C      LOADOP = 1                                                 00000980
C      WRITE(6,785) CASE,RHO,MU,PSAT,SN,LOADOP,FLR               00000990
C      GO TO 790                                                  00010000
775 WRITE (6,22) CASE, RHO, MU, PSAT, SN, LOADOP                 00010100
790 READ (5,19) (PO(I), VA(I), ALPHI(I), I=1,NI)                 00010200
C      WRITE (6,23) (PO(I), VA(I), ALPHI(I), I=1,NI)             00010300
C      NREV = 0                                                   00010400
926 NREV = NREV + 1                                              00010500
C      KILL = 0                                                   00010600
C                                                                 00010700
C      INTERNAL PROGRAM CONSTANTS                                  00010800
C                                                                 00010900
C      NXXI = NI - 1                                              00011000
C      CVOL = 0.0                                                 00011100
C      PI = 3.141592                                              00011200

```

	NU = MU / RHO	00001130
	OMEGA = SN * 6.2832	00001140
	C1 = RHO / 2.0 / G	00001150
	C3 = C1 * OMEGA**2	00001160
	VT = OMEGA * RT(1)	00001170
C		00001180
C	INLET ROUTINE	00001190
C	( UPSTREAM )	00001200
C		00001210
C	CONSTANT PARAMETERS	00001220
		00001230
	DZ = 0.0	00001240
	DR = RT(1) - RH(1)	00001250
	DR2 = ( RT(1)**2 - RH(1)**2 ) / NI	00001260
	CE = 0.284 / SIG **0.5	00001270
	SLOP = ( RT(1)*TAN(BTS(1)) - RH(1) *TAN(BHS(1)) ) / DR	00001280
	SIT = ATAN( (RT(2) - RT(1)) / ( Z (2) - Z (1) ) )	00001290
	SIH = ATAN( (RH(2) - RH(1)) / ( Z (2) - Z (1) ) )	00001300
	DSI = SIT - SIH	00001310
	DELS = 0.0	00001320
	ZP = Z(1) - .001*( Z(2) - Z(1) )	00001330
	RSTP = RH(1)	00001340
	DRZE = (RT(NJ)**2 - RH(NJ)**2) / NI	00001350
	RSTEP = RH(NJ)	00001360
	QI = 0.	00001370
	ZZ1 = 0.	00001380
	ZZ2 = 0.	00001390
	WRITE (6,30)	00001400
		00001410
C		00001420
C	VARIABLE PARAMETERS	00001430
		00001440
	DO 40 I = 1 , NI	00001450
	RSTE = SQRT(RSTEP**2 + DRZE)	00001460
	RST = SQRT( RSTP**2 + DR2 )	00001470
	RSTS(I) = RST	00001480
	PCR(I) = ( RST - RH(1) ) / DR	00001490
	DY(I) = RST - RSTP	00001500
	R(I) = (RSTP + RST ) / 2.0	00001510
	TAU(I) = C2 * R(I)	00001520
	RTNB = RT(1) * TAN(BTS(1)) - SLOP * (RT(1) - R(I) )	00001530
	BETAS(I) = ATAN( RTNB / R(I) )	00001540
	SI(I) = SIH + (R(I) - RH(1)) / DR * DSI	00001550
	SIS(I) = SI(I)	00001560
	SIB(I) = SI(I)	00001570
	A(I) = TAU(I) * DY(I) * COS(SI(I))	00001580
	U = OMEGA * R(I)	00001590
	ALPHA = ALPHI(I) / 57.29578	00001600
	VM = VA(I)	00001610
	V = VM / SIN(ALPHA)	00001620
	VU = V * COS(ALPHA )	00001630
	WU = U - VU	00001640
	BETA(I) = ATAN( VM / WU )	00001650
	XIOI(I) = BETAS(I) - BETA(I)	00001660
	W(I) = VM / SIN(BETA(I))	00001670
	PX(I) = PO(I) - C1 * V**2	00001680
	QD = C1 * W(I)**2	

```

PREL(I) = PX(I)+QD                                00001690
K =(PX(I)-PSAT ) / QD                            00001700
HIO(I) = U * VU / G                              00001710
HO(I) = PO(I) / RHO                              00001720
Q(I) = VM * A(I)                                 00001730
QI = QI + Q(I) * FLOAT(NB)                       00001740
ZZ1 = ZZ1 + VM                                    00001750
ZZ2 = ZZ2 + PO(I) * Q(I)                         00001760
DELW(I) = 0.0                                     00001770
E(I) = 0.                                         00001780
T(I) = 0.                                         00001790
B(I) = 0.                                         00001800
BL(1,I) = 0.                                      00001810
M(I) = 0.0                                        00001820
DC(I) = 0.0                                       00001830
DM(I) = 0.0                                       00001840
HSF(I) = 1.4                                       00001850
XMTH(I)=0.278 * SQRT(NU / W(I) )                 00001860
ZBL(I) = 0.0                                       00001870
F = 1.0                                           00001880
XMTHI(I) = XMTH(I)                               00001890
BIN(I) = BETA(I)                                  00001900
MOM(I)=PX(I)*A(I) * SIN(BETAS(I)) + 2.0 * C1 * Q(I) *W(I)*COS(XIOI00001910
1 (I))                                           00001920
TCBSI(I) = TAU(I) * COS(BETAS(I))                00001930
RVU(I) = R(I) * VU                               00001940
DBS(I) = XIOI(I)                                  00001950
RIN(I) = R(I)                                     00001960
BSIN(I) = BETAS(I)                               00001970
WIN(I) = W(I)                                     00001980
PRELI(I) = PREL(I)                               00001990
RSTP = RST                                        00002000
RSTEP = RSTE                                      00002010
BETADG = BETA(I) * 57.2958                       00002020
ALPHDGD = ALPHA * 57.29578                       00002030
WRITE (6,41) I, R(I),Q(I),W(I),PO(I),PREL(I),PX(I),ALPHDGD, BETADGD,00002040
1 K, U, V, VM, VU                               00002050
40 CONTINUE                                       00002060
C                                                  00002070
C MAIN PROGRAM                                   00002080
C                                                  00002090
PH = ZZ1 / NI / VT                               00002100
PHCRT = .50 * BTS(1)                             00002110
IF(PH .GT. PHCRT) GOTO47327                      00002120
47328 FORMAT(///// ' FLOW COEFFICIENT=',F10.5,3X, ' AND IS LESS THAN CRO0002130
1ITICAL FLOW = ',F10.5)                          00002140
WRITE(6,47328)PH,PHCRT                           00002150
GOTO4501                                          00002160
47327 CONTINUE                                    00002170
PT = ZZ2 / QI * FLOAT(NB)                         00002180
NPSH = ( PT - PSAT ) / RHO                       00002190
XKTIP = 2.*G*NPSH / VT**2 / (1.+PH**2) - PH**2 / (1.+PH**2) 00002200
THOMA = 2.0 * G * NPSH / VT**2                  00002210
WRITE(6,7090) PH,NPSH,THOMA,VT,PT,XKTIP         00002220
PTU = PT                                          00002230
DB = 0.0                                          00002240
FD = 0.0                                          00002250

```

	AV = 0.0	00002260
	CGAM = 0.0	00002270
	GAM = 0.0	00002280
	PP = 0.0	00002290
	PS = 0.0	00002300
	V1 = 0.0	00002310
	XLAM = 0.0	00002320
	DO 300 J = 1 , NJ	00002330
C		00002340
C	J-STATION	00002350
C	CONSTANT PARAMETERS	00002360
1252	PCRD1 = 0.01 / NI	00002370
	ETOL = .10	00002380
	SMH = 0.0	00002390
	SMHI = 0.0	00002400
	DZE = Z(NJ) - Z(J)	00002410
	IF( J .NE. 1 ) ZP = Z( J - 1 )	00002420
	DZ = Z(J) - ZP	00002430
	DR = RT(J) - RH(J)	00002440
	SLOP = ( RT(J)*TAN(BTS(J)) - RH(J)*TAN(BHS(J)) ) / DR	00002450
	IF( J .EQ. 1 ) GO TO 44	00002460
	ZZ5 = PCRD1*DR/DZ	00002470
	IF ( ZZ5 .LE. 0.01 ) GO TO 44	00002480
	PCRD1 = 0.01 * DZ/DR	00002490
44	CONTINUE	00002500
	PCRD1 = PCRD1	00002510
C		00002520
C	RESET INITIAL VALUES	00002530
C		00002540
	DO 125 I = 1 , NI	00002550
	MP(I) = M(I)	00002560
	RSTL(I) = RSTS(I)	00002570
	RP(I) = R(I)	00002580
	BETASP(I)=BETAS(I)	00002590
	TP(I)=T(I)	00002600
	TAUP(I) = TAU(I)	00002610
	AP(I) = A(I)	00002620
	DYP(I) = DY(I)	00002630
	SIP(I)= SI(I)	00002640
	SISP(I) = SIS(I)	00002650
	WP(I) = W(I)	00002660
	BETAP(I) = BETA(I)	00002670
	PXP(I) = PX(I)	00002680
	HSFP(I) = HSF(I)	00002690
	XMTHP(I) = XMTH(I)	00002700
	MOMP(I) = MOM(I)	00002710
	DBSP(I) = DBS(I)	00002720
	DBTC(1,I) = 0.	00002730
	WNC(1,I) = 0.	00002740
	BP(I) = B(I)	00002750
	DCP(I) = DC(I)	00002760
125	PRELP(I) = PREL(I)	00002770
C		00002780
C	START STREAMLINE ITERATION	00002790
C		00002800
	DO 130 ITE = 1 , 100	00002810

```

ERROR = .FALSE.
IF( ITE .GE. 25 .AND. ITE .LE. 50) PCRD1 = 0.1 * PCRD1
IF( ITE .GT. 50 ) PCRD1 = 0.01 * PCRD1
SME2 = 0.0
RSTP = RH(J)
DO 131 I = 1 , NI
RST = RH(J) + PCR(I) * DR
SIS(I) = ATAN ( ( RST - RSTL(I) ) / DZ )
IF ( J .EQ. 1 ) SIS(I) = SISP(I)
RSTS(I) = RST
DY(I) = RST - RSTP
DYX(J,I) = DY(I)
R(I) = (RSTP + RST) / 2.0
RL(J,I) = R(I)
ZLE = Z0 + Z1*R(I) + Z2*R(I)**2 + Z3*R(I)**3
DZLE = ZLE - Z(J)
U = OMEGA * R(I)
RSTP = RST
RB = (RP(I) + R(I) ) / 2.0
RTNB = RT(J)*TAN(BTS(J)) - SLOP*(RT(J) - R(I) )
BETAS(I) = ATAN( RTNB / R(I) )
BETASX(J,I) = BETAS(I)
SBS(I) = SIN(BETAS(I))
TBS(I) = TAN(BETAS(I))
CBS(I) = COS(BETAS(I))
POWER2 = -DZE * NB / 2.0 / R(I) / (SBS(I))
IF(J .GT. NJ) GO TO 44444
T(I) = TT(J) + TA(J) / 57.3 * ( RT(J) - R(I) )
BETASB = ( BETAS(I) + BETASP(I)) * 0.5
SBSB = SIN(BETASB)
SI(I) = ATAN((R(I) - RP(I))/DZ)
IF(J .EQ.1 ) SI(I) = SIP(I)
SIB(I) = .5 * ( SI(I) + SIP(I) )
CSB(I) = COS(SIB(I))
GO TO 135
C
C SET VALUES FOR EXIT STATION
C
44444 BSEX(I) = BETAS(I)
SI(I) = 0.0
SIB(I) = 0.0
T(I) = 0.0
REX(I) = R(I)
GO TO 126
135 DM(I) = DZ / CSB(I) / SBSB
DMVX(J,I) = DM(I)
DMB = DM(I)
IF(DZLE .LT. 0. .AND. ZLE .GT. ZP) DMB = DM(I) * (-DZLE/DZ)
IF(DZLE .GT. 0.) DMB = 0.
M(I) = MP(I) + DMB
IF(DZLE .GE. 0.) M(I) = 0.
ALW = ALPWT - ( RT(J) - R(I) ) / ( RT(J) - RH(J) ) * ( ALPWT - ALPWH )
TLE = M(I) * TAN(ALW) * COS(SI(I))
IF(TLE .LT. T(I)) T(I) = TLE
TCBS(J,I) = ( C2 * R(I) - T(I) / SBS(I) ) * CBS(I)
IF(DZLE .GT. 0) T(I) = 0.0
TAU(I) = C2 * R(I) - T(I) / SBS(I)

```

```

00002820
00002830
00002840
00002850
00002860
00002870
00002880
00002890
00002900
00002910
00002920
00002930
00002940
00002950
00002960
00002970
00002980
00002990
00003000
00003010
00003020
00003030
00003040
00003050
00003060
00003070
00003080
00003090
00003100
00003110
00003120
00003130
00003140
00003150
00003160
00003170
00003180
00003190
00003200
00003210
00003220
00003230
00003240
00003250
00003260
00003270
00003280
00003290
00003300
00003310
00003320
00003330
00003340
00003350
00003360
00003370
00003380

```

	TAUVX(J,I) = TAU(I)	00003390
	ML(J,I) = M(I)	00003400
	DPDMP = 0.0	00003410
	IF(DZLE .GT. 0) GO TO 1248	00003420
C		00003430
C	START CAVITY ITERATION	00003440
C		00003450
	DBSSAV = DBS(I)	00003460
	ITB(I) = 1	00003470
	IF( DBSP(I) .GT. (0.10 * BETASP(I)) ) GO TO 140	00003480
	DBS(I) = 0.0	00003490
	IF(DELW(I) .GT. 0.0 ) GO TO 791	00003500
	IF(PCBB(I) .GT. 0. .AND. PCBB(I) .LE. 0.05)	00003510
	1 DELW(I) = (-5.389049E 04) * PCBB(I)**3 + (2.853374E 04) *	00003520
	2 PCBB(I)**2 + (-2.984396E 03) * PCBB(I) + 90.04968	00003530
	IF ( PCBB(I) .GT. 0.05 .AND. PCBB(I) .LE. 0.069 )	00003540
	1 DELW(I) = (-5.706232E 10) * PCBB(I)**8 + (3.597064E 09)	00003550
	2 * PCBB(I)**7 + (2.303375E 08) * PCBB(I)**6 +	00003560
	3 (-3.853306E 06) * PCBB(I)**5 + (1.692314E 05) * PCBB(I)	00003570
	4 **4 + (-8.575639E 04) * PCBB(I)**3 + (-6.183219E 02)	00003580
	5 * PCBB(I)**2 + (-2.479463E 01) * PCBB(I) + 14.903	00003590
	IF ( PCBB(I) .GE. .069 ) DELW(I) = 2.902 -10.4651* PCBB(I)	00003600
	IF ( PCBB(I) .GE. .155 ) DELW(I) = 1.28	00003610
	DELW(I) = DELW(I) / 57.295	00003620
	791 TDW = TAN( DELW(I) )	00003630
		00003640
C		00003650
C	CALCULATE CAVITY HEIGHT.	00003660
C		00003670
	B(I) = BP(I) - DZ*TDW/SBS(I)**2	00003680
	1 / (1.0 + TDW/TBS(I))	00003690
	IF (B(I) .LT. 0.0) B(I) = 0.0	00003700
	GO TO 1248	00003710
140	CONTINUE	00003720
	DBSB = 0.5 * (DBS(I) + DBSP(I) )	00003730
	IF(ZLE .GE. ZP) DBSB=DBS(I)	00003740
	DB= DMB * SIN(DBSB) /SIN(BETASB - DBSB)	00003750
	B(I) = BP(I) + DB	00003760
	PCBB(I) = B(I) / TAU(I)	00003770
	IF( DZLE .EQ. 0.0) B(I) = 0.0	00003780
1248	BL(J,I)=B(I)	00003790
	TAUL= TAU(I) -B(I)	00003800
	ZZ1 = 2.0	00003810
	IF(B(I) .GT. 0.0) ZZ1=1.0	00003820
	ZZ2 = ZZ1 * DELS * DY(I) * COS(SI(I)) / SBS(I)	00003830
	IF(I .EQ. 1 .OR. I .EQ. NI) ZZ2 = ZZ2 + DELS * (TAUL - ZZ1 * DELS	00003840
	1 / SBS(I))	00003850
	A(I) = DY(I) * TAUL * COS(SI(I))	00003860
	VM = Q(I) / (A(I) - ZZ2)	00003870
	IF(DZLE .GE. 0.) BETA(I)=ATAN(VM/(R(I)*OMEGA-RVU(I)/R(I)))	00003880
C		00003890
C	EXIT DEVIATION	00003900
C		00003910
	DEL2 = 0.0	00003920
	IF(POWER2 .LT. -100. ) GO TO 1250	00003930
	DELE = ( BETAS(I) - BIN(I) ) * CE	00003940
	DEL2 = DELE * EXP(POWER2)/(1- DELE * (1- EXP(POWER2)) / TAN	

	1 (BETAS(I))	00003950
C		00003960
C	FLUID INERTIA EFFECTS	00003970
C		00003980
	1250 BESEF = BETAS(I) - 0.5 * DBS(I)	00003990
	DELI = 0.	00004000
	IF(DZLE .GE. 0.) GO TO 137	00004010
	IF(DEL2 .GT. 0.001*BETAS(I)) GO TO 1354	00004020
	POWER1 = - PI * DMB / TAUL / SIN(BETAS(I))	00004030
	DELO = BESEF - BETAP(I)	00004040
	DELI = DELO*EXP(POWER1)/(1.-DELO*(1.-EXP(POWER1))/TBS(I))	00004050
C		00004060
C	END FLUID INERTIA EFFECTS	00004070
C		00004080
	1354 IF( NREV .EQ. 1 .OR. CBHR .EQ. 0.0 ) DBTC(J,I) = 0.0	00004090
	BETA(I) = BESEF - DELI - DEL2 + DBTC(J,I)	00004100
	IF( BETA(I) .LT. 0.0 ) BETA(I) = 0.5/57.2957	00004110
	137 DBETA = BETA(I) - BETAP(I)	00004120
	BETAB = 0.5 * ( BETA(I) + BETAP(I) )	00004130
	SBB = SIN(BETAB)	00004140
	CBB = COS(BETAB)	00004150
	DBDM(I) = DBETA / DM(I)	00004160
	IF(DZLE .GE. 0.) DBS(I) = BETAS(I) - BETA(I)	00004170
	W(I) = VM / SIN (BETA(I))	00004180
	WVX(J,I) = W(I)	00004190
	IF(DZLE .GE. 0.)WJ1(I)=W(I)	00004200
	IF (J .EQ. NJ) WNJ(I) = W(I)	00004210
	QD = C1 * W(I)**2	00004220
	WB = ( WP(I) + W(I) ) / 2.0	00004230
	VMB = WB*SBB	00004240
	WUB = WB*CBB	00004250
	UB = OMEGA*RB	00004260
	VUB = UB-WUB	00004270
	TAULB =(TAU(I) - B(I) + TAUP(I) - BP(I) ) / 2.0	00004280
	QDB = C1 * WB**2	00004290
	F=1.0	00004300
	DWDM(I) = ( W(I) - WP(I) ) / DM(I)	00004310
	IF(DZLE .GE. 0.) GO TO 996	00004320
	IF ( MU .NE. 0.0 ) GO TO 1372	00004330
	XMTH(I) = 0.0	00004340
	DELS = 0.0	00004350
	CF = 0.0	00004360
	GO TO 996	00004370
	1372 CONTINUE	00004380
C		00004390
C	START BOUNDARY LAYER CALCULATIONS	00004400
C		00004410
	RET = WP(I) * XMTHP(I) / NU	00004420
	XKL=XMTHP(I)/WP(I)* DWDM(I)	00004430
	CF = 0.246/(10.**((0.678*HSFP(I)) * RET**0.268 )	00004440
	DTDM = CF / 2.0 - ( HSFP(I) + 2.0 ) * XKL	00004450
	CL = RET**0.16666 * XMTHP(I) / 0.0135 / EXP(5.0*(HSFP(I) - 1.4))	00004460
	HSF(I) = 1.4 - RET**0.16666 * XKL / 0.0135	00004470
	HSF(I)=HSF(I) -(HSF(I)-HSFP(I))*EXP(-DMB/CL)	00004480
	IF( HSF(I) .GT. 3.0 ) HSF(I) = 3.0	00004490
	IF( HSF(I) .LT. 1.0 ) HSF(I) = 1.0	00004500
	XMTH(I)= DTDM * DMB +XMTHP(I)	00004510

```

ZZ5=.05 * TAUL * SBS(I)
IF(XMTH(I) .GT. ZZ5) XMTH(I) =ZZ5
IF( XMTH(I) .LE. 0.0 ) XMTH(I) = XMTH(I)
DELS = XMTH(I) * HSF(I)
F = 1.0 - ZZ1 *XMTH(I) / TAUL / SBS(I)*2.
IF( I .EQ. 1 .OR. I .EQ. NI ) F = F*(1.0-XMTH(I) / DY(I) * 2.0)
996 IF( DZLE .GE. 0.0 ) DELS = 0.0
ZBL(I) = DELS

C
C
C
END BOUNDARY LAYER CALCULATIONS

IF( DBSP(I) .GT. ( 0.10 * BETASP(I)) ) GO TO 997
IF( BP(I) .EQ. 0.0 ) GO TO 997
AR = W(I) / WP(I)
ZZ5=(TAUL +TAUP(I)-BP(I))*(DY(I)-DYP(I))/(2*TAUL*DY(I))
DPDMP = C1*(WP(I)*(1.0 - AR)**2 + (PXP(I) - PSAT)*(1. - AR-ZZ5)
IF( DPDMP .LT. 0.0) DPDMP =0.0
997 CONTINUE
PREL(I) = PRELP(I) + C3 * ( R(I)**2 - RP(I)**2 ) - DPDMP
PRELL(J,I) = PREL(I)
WNC(J,I) = ABS(WNC(J,I))
IF( NREV .EQ. 1 .OR. CBHR .EQ. 0.0 ) WNC(J,I) = 0.0
POREL(I) = PREL(I) - ( 1.0 - F ) * QD -(RHO/2./G*WNC(J,I)**2.)
PX(I) = PREL(I) - QD
PXL(J,I) = PX(I)
DC(I)=0.0
XA = A(I) - DY(I) * COS(SI(I)) * DC(I)
XA=A(I)
IF(DZLE .LT. 0.)GO TO 96
DPBN(J,I) = 2.0* (PX(I) - PSAT)
GO TO 952
96 TERM1(I) = ( 2.0 * OMEGA / WB - CBB / R(I)) * SIN(SI(I))
TERM2(I) = DBDM(I)
DPBN(J,I) = 2.0 * TAULB * QDB * SBB**2/SBS(I)
I * (TERM1(I) + TERM2(I))
IF( DBSP(I) .GT. (0.10 * BETASP(I)) ) GO TO 121
GO TO 204

C
C
C
CHECK MOMENTUM BALANCE (FOR EACH STREAMTUBE)
121 DTH=T(I)-TP(I)
DYB = ( DY(I) + DYP(I)) * 0.5
AB=(AP(I)*SIN(BETASP(I))+ XA *SBS(I))/2.
PB = ( PX(I) + PXP(I)) / 2.0
IF( J .EQ. 1 ) GO TO 951
WETP = ZZ1 * DYB
IF(I .EQ. 1) WETP= ZZ1*DYB + TAULB*(RH(J-1) + RH(J))/(RP(I) + R(
1 I))* SBSB
IF(I .EQ.NI) WETP= ZZ1*DYB + TAULB*(RT(J-1) + RT(J))/(RP(I) + R(
1 I))* SBSB
FD =CF * QDB * WETP * DMB
951 FC = 2.0 *C1*AB*(R(I)-RP(I))*VUB**2/RB
ZZ1 = PSAT * DYB * DTH
DB = DB + DC(I) - DCP(I)
ZZ2=PSAT*DYB*DB*SBSB
ZZ3 = 2.0 * PB *(DYB - DY(I)) * SBSB * (TAULB - DC(I) / 2.)

```

```

00004520
00004530
00004540
00004550
00004560
00004570
00004580
00004590
00004600
00004610
00004620
00004630
00004640
00004650
00004660
00004670
00004680
00004690
00004700
00004710
00004720
00004730
00004740
00004750
00004760
00004770
00004780
00004790
00004800
00004810
00004820
00004830
00004840
00004850
00004860
00004870
00004880
00004890
00004900
00004910
00004920
00004930
00004940
00004950
00004960
00004970
00004980
00004990
00005000
00005010
00005020
00005030
00005040
00005050
00005060
00005070

```



```

ZZ3=ZZ3+PB*C2*(RP(I)*SIN(BETASP(I))-R(I)*SBS(I))*DYB      00005080
FP = (ZZ1 + ZZ2 + ZZ3) * CSB(I)                             00005090
DMOM= FC - FP - FD                                          00005100
952 MOM(I) = PX(I) * XA * SBS(I) + 2.0 * C1 * Q(I) * W(I) * 00005110
1 COS(BETAS(I) - BETA(I)) * F **0.5                        00005120
IF(DZLE .GE. 0.) GO TO 204                                  00005130
ERROR1= MOM(I) - MOMP(I) - DMOM                             00005140
C IF( B(I) .GE.(.8*TAU(I))) GO TO 204                       00005150
C CONVERENGE TEST FOR MOMENTUM BALANCE.                     00005160
IF ( ABS (ERROR1 ) .LT. 0.0001*MOM(I)) GO TO 204           00005170
C                                                            00005180
C ADJUST CAVITY SLOPE                                       00005190
C                                                            00005200
DDBSSV = DBS(I) - DBSSAV                                    00005210
DBSSAV = DBS(I)                                             00005220
IF ( ERROR1 ) 142, 204 , 150                                00005230
142 DBS(I) = DBS(I) - 0.001 * BETAS(I)                     00005240
IF ( DBS(I) .LT. 0.0 ) DBS(I) = 0.0                       00005250
GO TO 151                                                    00005260
150 DBS(I) = DBS(I) + 0.001 * BETAS(I)                     00005270
IF(DBS(I) .GT. BETAS(I)) DBS(I)=0.95*BETAS(I)             00005280
151 ITB(I)= ITB(I)+1                                        00005290
IF( ITB(I) .LE. 2 ) GO TO 140                               00005300
IF( ( DBS(I) - DBSSAV) * DDBSSV .GT. 0.0 ) GO TO 140     00005310
GO TO 204                                                    00005320
C                                                            00005330
C END CAVITY ITERATION                                       00005340
C                                                            00005350
C                                                            00005360
C EXIT STATION FLOW CALCULATIONS                             00005370
C                                                            00005380
126 PREL(I) = PRELP(I) + C3 * ( R(I)**2 - RP(I)**2)        00005390
PRELEX(I) = PREL(I)                                         00005400
ZZ1 = 0.0                                                    00005410
IF ( I .EQ. 1 .OR. I .EQ. NI ) ZZ1 = ZBL(I)                00005420
VM = Q(I) / (DY(I)*COS(SI(I))-ZZ1)/C2/R(I)                 00005430
VU = RVU(I) / R(I)                                          00005440
WU = U - VU                                                 00005450
BETA(I) = ATAN( VM/WU)                                       00005460
W(I) = VM / SIN(BETA(I))                                     00005470
WEX(I) = W(I)                                               00005480
QD = C1 * W(I)**2                                           00005490
PX(I) = PREL(I) - QD                                        00005500
C                                                            00005510
C CALCULATE RADIAL PRESSURE GRADIENT                         00005520
C FOR ALL STREAM TUBES                                       00005530
C                                                            00005540
204 IF( I .EQ. 1 ) GO TO 131                                00005550
C GOTO131                                                     00005560
DPR = PX(I) - PX(I-1)                                       00005570
DSR = R(I) - R(I-1)                                         00005580
ZZ5=(R(I) *OMEGA - W(I) * COS(BETA(I))) ** 2 /R(I)         00005590
ZZ6=(R(I-1) * OMEGA - W(I-1) * COS(BETA(I-1))) **2 /R(I-1) 00005600
DPDSR= RHO * (ZZ5 + ZZ6) / G/2.0                            00005610
IF ( J .GT. NJ .OR. DZLE .GE.0.)GOTO 1311                  00005620
ZZ1 = SIS(I-1)                                              00005630
ZZ5=(SIS(I-1) -SISP(I-1)) / DZ                             00005640

```

	ZZ6 = (W(I)*SIN(BETA(I)) + W(I-1)*SIN(BETA(I-1))) *0.5	00005650
	DPDSR = DPDSR - 2.0*C1*ZZ6*ZZ6*ZZ5*COS(ZZ1)**2	00005660
	ZZ4 = (WP(I)*SIN(BETAP(I)) + WP(I-1)*SIN(BETAP(I-1)))*0.5	00005670
	ZZ2=(ZZ6 - ZZ4)/DZ	00005680
	DPDSR = DPDSR - C1*ZZ2*SIN(2.0*ZZ1)*ZZ6	00005690
1311	ESV(I) = E(I)	00005700
	E(I) = (DPR/DSR - DPDSR)	00005710
	SME2 = SME2 + ABS(E(I))	00005720
131	CONTINUE	00005730
	GOTO144	00005740
C		00005750
C	CHECK RADIAL EQUILIBRIUM	00005760
C		00005770
	IF( SME2 .LT. ( ETOL * PX(NI)) / DR ) GO TO 144	00005780
	IF( ITE .LT. 53 ) GO TO 133	00005790
	DO 132 I = 2 , NI	00005800
	IF( ESV(I) * E(I) .LT. 0.0 ) GO TO 132	00005810
	ERROR=.TRUE.	00005820
132	CONTINUE	00005830
	IF( .NOT. ERROR ) GO TO 144	00005840
133	CONTINUE	00005850
	IF(ITE .EQ. 200) GO TO 130	00005860
C		00005870
C	ADJUST STREAMLINES	00005880
C		00005890
	DO 141 I = 1,NXXI	00005900
	NXI = I + 1	00005910
	ZZ4 = PCRDL	00005920
	ZZ5 = E( NXI)	00005930
	IF (ITE .EQ. 1 ) GO TO 139	00005940
	ZZ6 = ESV( NXI)	00005950
	ZZ1 = PCR(I) - PCR1(I)	00005960
	ZZ2 = ABS(ZZ6) - ABS(ZZ5)	00005970
	IF ((ZZ1*ZZ2) .LT. 0.0) ZZ4 = -PCRDL	00005980
139	PCR1(I) = PCR(I)	00005990
141	PCR(I) = PCR(I) + ZZ4 / SME2 * ABS( ZZ5 )	00006000
130	CONTINUE	00006010
C		00006020
C	END STREAMLINE ITERATION	00006030
C		00006040
144	IF ( J .GT. NJ ) GO TO 404	00006050
	VOL = 0.	00006060
C		00006070
C	CALCULATE J-STATION STREAM TUBE PARAMETERS	00006080
C		00006090
	CALL PRNT5(J,Z(J),ITE)	00006100
	JSTOP = 0	00006110
	DO 299 I=1,NI	00006120
	VOL = VOL + (B(I) * SIN(BETAS(I)) + BP(I) * SIN(BETASP(I)))	00006130
1	* DM(I) * (DY(I) + DYP(I)) / 4.	00006140
	U = OMEGA * R(I)	00006150
	VM = W(I) * SIN(BETA(I) )	00006160
	WU = W(I) * COS(BETA(I) )	00006170
	VU = U - WU	00006180
	RVU(I) = R(I) * VU	00006190
	ALPHA=ATAN2(VM,VU)	00006200

```

V = VM / SIN(ALPHA)                                00006210
PT = POREL(I) + C1 * (V**2 - W(I)**2 )             00006220
H = PT / RHO - H0(I)                                00006230
HII = U * VU / G - H10(I)                           00006240
ETA = H / HII                                        00006250
IF(M(I) .LE. 0.)ETA=1.0                              00006260
PCB = B(I) / TAU(I)                                  00006270
DEV = ( BETAS(I) - BETA(I) )                        00006280
BN = B(I) * SIN(BETAS(I))                           00006290
MSTR= M(I) + B(I) * COS(BETAS(I))                   00006300
IF (PX(I) .GE. 0.0) GO TO 9085                       00006310
JSTOP = 1                                             00006320
PXS = PX(I)                                          00006330
9085 CONTINUE                                        00006340
CALL PRNT67(J,Z(J),I,RSTS(I),PCR(I),R(I),TAU(I),T(I),B(I),PX(I), 00006350
1 PREL(I),POREL(I),PT,MSTR,BN,PCB,BETA(I),BETAS(I),DEV, 00006360
2 DBS(I),XMTH(I),ZBL(I),HSF(I),ALPHA,ETA,W(I),U,V,VU, 00006370
3 VM,ITE)                                           00006380
IF ( J .NE. NJ) GO TO 299                           00006390
POREL(I) = POREL(I) - QD * (T(I) / C2 / R(I) / SIN(BETAS(I)))**2 00006400
PREL(I) = POREL(I)                                  00006410
IF (I .EQ. 1 .OR. I .EQ. NI) PREL(I)=POREL(I) + 2.0*XMTH(I)/ 00006420
1 DY(I)*QD                                          00006430
299 CONTINUE                                        00006440
CVOL = CVOL + VOL * NB                              00006450
IF( JSTOP .EQ. 0 ) GO TO 300                        00006460
WRITE(6,9086) PXS                                    00006470
9086 FORMAT(///// ' NEGATIVE PRESSURE OF ',F16.5, 00006480
1 ' EXECUTION SUPPRESSED' )                        00006490
GO TO 4501                                           00006500
300 CONTINUE                                        00006510
J = NJ + 1                                           00006520
Z(J) = Z(NJ) + DZ                                    00006530
RT(J) = RT(NJ)                                       00006540
RH(J) = RH(NJ)                                       00006550
BTS(J) = BTS(NJ)                                     00006560
BHS(J) = BHS(NJ)                                     00006570
GO TO 1252                                           00006580
C                                                    00006590
C EXIT ROUTINE                                       00006600
C (DOWNSTREAM)                                       00006610
C                                                    00006620
404 CONTINUE                                        00006630
WRITE (6,405)                                        00006640
405 FORMAT (1H1, T54, 'EXIT CONDITIONS'// T19, 'I', T33, 'R', T46, 'DE00006650
1V', T61, 'H', T75, 'P', T88, 'PT', T102, 'ETA' /T17, 'ALPHA', T31,00006660
2 'BETA', T47, 'V', T60, 'VM', T74, 'VU', T88, 'WU', T103, 'W') 00006670
SMH = 0.                                             00006680
SMHI = 0.                                           00006690
DO 450 I = 1,NI                                     00006700
U = OMEGA * R(I)                                    00006710
VU = RVU(I) / R(I)                                  00006720
WU = U - VU                                         00006730
VM = W(I) * SIN(BETA(I))                            00006740
VEX(I) = VM                                         00006750
ALPHA=ATAN2(VM,VU)                                   00006760
V = VM / SIN(ALPHA)                                  00006770

```

```

BETA E = ATAN(VM/WU) 00006780
QD = C1 * WP(I)**2 00006790
POREL(I) = PREL(I) 00006800
IF ( I .EQ. 1 .OR. I .EQ. NI ) POREL(I) =PREL(I)-2.*XMTH(I)/DY(I)*QD 00006810
PT = POREL(I) + C1 * ( V**2 - W(I)**2 ) 00006820
H = PT / RHO - H0(I) 00006830
HII = U * VU / G - HIO(I) 00006840
ETA = H / HII 00006850
SMH = SMH + H * Q(I) 00006860
SMHI = SMHI + HII * Q(I) 00006870
DEV = (BETAS(I) - BETAE ) * 57.2958 00006880
ALPHA = ALPHA * 57.2958 00006890
BETA E = BETAE * 57.2958 00006900
WRITE (6,411) I, R(I), DEV, H, PX(I), PT, ETA, ALPHA, BETAE, V, 00006910
1 VM, VU, WU, W(I) 00006920
411 FORMAT ( 1H0 , T12,10X,I4,6E14.6 / T12, 7E14.6 ) 00006930
450 CONTINUE 00006940
C 00006950
C 00006960
C OVERALL PERFORMANCE 00006970
C 00006980
H = SMH / QI * FLOAT(NB) 00006990
HII = SMHI / QI * FLOAT(NB) 00007000
ETA = SMH / SMHI 00007010
SIOP = G * H / ( OMEGA * RT(1) ) **2 00007020
RN = OMEGA * RT(1)**2 / NU 00007030
SS = OMEGA * QI**.5 / ( G * NPSH)**.75 00007040
SIID = SIOP/ETA 00007050
SIL = SIID - SIOP 00007060
C 00007070
IF( CBHR .EQ. 0.0 .OR. NREV .EQ. 1 ) GO TO 250 00007080
DELTR = (RT(1) - RH(1) + RT(NJ) - RH(NJ)) / 2. 00007090
ARR = DELTR / (Z(NJ) - Z(1)) * SIN(BTSB) 00007100
SIL = (SILSAV/SIID +(0.7 * CBHR/ SIN(BTSB) * SIID) * (1.+10.0*( 00007110
1 PH/SIID * CBHR / SIN(BTSB) * ARR)**0.5 )) * SIID 00007120
SIOP = SIID - SIL 00007130
ETA = SIOP / SIID 00007140
H = SIOP / G * (OMEGA*RT(1))**2 00007150
HII = SIID / G * (OMEGA*RT(1))**2 00007160
250 SILSAV = SIL 00007170
CALL PRNT8 (NPSH, PH, SIOP, H, HII, RN, ETA, SS, QI,CVOL) 00007180
WRITE(6,27) SIID,SIL 00007190
27 FORMAT(///' PSI IDEAL = ',F10.5,5X,' PSI LOSS = ',F10.5) 00007200
C 00007210
IF(LOADOP .EQ. 0) GO TO 4501 00007220
CALL LOAD(PXL,ML,DPBN,NJ,NI,TCBSI,TCBS,PSAT,BL,PRELL,C1,WIN,WJ1, 00007230
1NB,RIN,BSIN,PRELI,VA,WNJ,REX,BSEX,VEX,Z,RL, WEX ,PRELEX, VT, PTU , 00007240
1 RHO,G,PCZ,TP,T,BETAS,DZ,C2,WPX,WSX,PPX,PSX) 00007250
IF( CBHR .EQ. 0.0 .OR. NREV .EQ. 2 ) GO TO 4501 00007260
C 00007270
C VORTEX CALCULATIONS 00007280
C 00007290
DO 906 J=2,NJ 00007300
CGAMP = CGAM 00007310
GAMP = GAM 00007320
AVP = AV 00007330

```

	V1P = V1	00007340
	XLAMP = XLAM	00007350
	I = NI	00007360
	IF ( KILL .EQ. 1) GO TO 9081	00007370
	IF ( PSX(J,I) .LE. PPX(J,I) ) GO TO 9078	00007380
9081	AV = AVP	00007390
	KILL = 1	00007400
	GO TO 9079	00007410
9078	XLAM = ARCOS (WPX(J,I) / WSX(J,I) )	00007420
	XLAMX = XLAM * 57.2958	00007430
	XLAMB = (XLAM + XLAMP) / 2.	00007440
	GAM = 2. * WSX(J,I) * SIN(XLAM / 2.)	00007450
	GAMB = (GAM + GAMP) / 2.	00007460
	V1 = WSX(J,I) * COS(XLAM / 2.)	00007470
	V1B = (V1 + V1P) / 2.	00007480
C		00007490
C	VORTEX RADIUS ITERATION	00007500
C		00007510
	KK = 0.	00007520
	AVC = GAMB * DMVX(J,I) / (4. * PI * V1B)	00007530
	AVC1 = AVC	00007540
925	KK = KK + 1	00007550
	IF (KK .GT. 300) STOP	00007560
	DADM = GAMB / (4.*PI * V1B) * ALOG( 1 + CLEAR / AVC)	00007570
	IF ( XLAM .EQ. 0.) DADM = 0.	00007580
	AV = AVP + DADM * DMVX(J,I)	00007590
	IF ( ABS ( ( AV - AVC ) / AV ) .LE. .001 ) GO TO 98	00007600
	AVC = (AV + AVC) / 2.	00007610
	GO TO 925	00007620
98	CGAM=(CGAMP+GAMB*TAN(XLAMB/2.)*DMVX(J,I) * FLR ) / (1.+ GAMB *	00007630
1	DMVX(J,I)*FLR / (4. * PI *(AV + CLEAR) * V1B) )	00007640
9079	OTCV = CGAM / ( 2. * PI * AV **2 )	00007650
	UPLIM = RT(J)	00007660
	LOWLIM = RT(J) - 2. * AV	00007670
C		00007680
	DO 906 I=1,NI	00007690
	RW = RT(J) + CLEAR	00007700
	R1 = RL(J,I) - DYX(J,I) / 2.	00007710
	R2 = RL(J,I) + DYX(J,I) / 2.	00007720
	IF(I .EQ. NI ) R2 = R2 + CLEAR	00007730
	RC = RT(J) - AV	00007740
	Y1 = RW - R2	00007750
	Y4 = RW - R1	00007760
	Y2 = RW - (RC + AV)	00007770
	Y2 = AMAX1(Y2,Y1)	00007780
	Y2 = AMIN1(Y2,Y4)	00007790
	Y3 = RW - (RC - AV)	00007800
	Y3 = AMAX1(Y3,Y1)	00007810
	Y3 = AMIN1(Y3,Y4)	00007820
	S = TAU VX(J,NI) * SIN(BETASX(J,NI))	00007830
	BTIP = S / 2.	00007840
	LI = TAU VX(J,I) * SIN(BETASX(J,I))	00007850
	BI = (LI / S) * BTIP	00007860
	X1 = BI - AV	00007870
	X2 = BI + AV	00007880
	AFAS = LI *(Y4 - Y1)	00007890
	TGIS = AV* (Y3**2 - Y2**2) -2*AV *(RW -RC)* (Y3 -Y2)	00007900

	TPS=2. * PI / S	00007910
	APC = AV + CLEAR	00007920
	M1 = TPS * (Y1-APC)	00007930
	M2 = TPS * (Y2-APC)	00007940
	M3 = TPS * (Y3-APC)	00007950
	M4 = TPS * (Y4-APC)	00007960
	N1 = TPS * (Y1+APC)	00007970
	N2 = TPS * (Y2+APC)	00007980
	N3 = TPS * (Y3+APC)	00007990
	N4 = TPS * (Y4+APC)	00008000
	DO 57 N=1,4	00008010
	GO TO(51,52,54,54),N	00008020
51	UP = LI	00008030
	LOW = X2	00008040
	GO TO 58	00008050
52	UP = X1	00008060
	LOW = 0.	00008070
	GO TO 58	00008080
54	UP = X2	00008090
	LOW = X1	00008100
58	DX =(UP - LOW) /25.	00008110
	XX = LOW -DX	00008120
	DO 59 KX=1,26	00008130
	XX = XX + DX	00008140
	XL = 2. * PI / S * (XX - BI)	00008150
	GO TO (61,61,63,64),N	00008160
61	FUNC(KX) = ALOG( ((COSH(M4)-COS(XL))/(COSH(M1)-COS(XL))) /((	00008170
	1 COSH(N4)-COS(XL))/(COSH(N1)-COS(XL)) )	00008180
	GO TO 59	00008190
	GO TO 59	00008190
63	FUNC(KX)= ALOG( ((COSH(M2)-COS(XL))/(COSH(M1)-COS(XL))) /((	00008200
	1 COSH(N2)-COS(XL))/(COSH(N1)-COS(XL)) )	00008210
	GO TO 59	00008220
64	FUNC(KX)= ALOG( ((COSH(M4)-COS(XL))/(COSH(M3)-COS(XL))) /((	00008230
	1 COSH(N4)-COSH(XL))/(COSH(N3)-COS(XL)) )	00008240
59	CONTINUE	00008250
	CALL QSF(DX,FUNC,YOUT,26)	00008260
57	TGIF(N) = S / (2.*PI) * YOUT(26)	00008270
	TGSUM = TGIF(1) + TGIF(2) + TGIF(3) + TGIF(4)	00008280
	WNC(J,I) =1./ AFAS *(FLR * CGAM / (2.*S ) * TGSUM + OTCV * TGIS)	00008290
	DBTC(J,I) = ATAN( WNC(J,I) / WVX(J,I) )	00008300
	R1 = R1*12.	00008310
	R2 = R2*12.	00008320
	RC = RC*12.	00008330
	RW = RW*12.	00008340
	AVX = AV * 12.	00008350
	X1 = X1*12.	00008360
	X2 = X2*12.	00008370
	Y1 = Y1*12.	00008380
	Y2 = Y2*12.	00008390
	Y3 = Y3*12.	00008400
	Y4 = Y4*12.	00008410
	TGIS = TGIS*12.	00008420
	TGSUM= TGSUM*12.	00008430
	S = S * 12.	00008440
	LI = LI * 12.	00008450

```

BTIP = BTIP * 12. 00008460
BI = BI * 12. 00008470
APC = APC * 12. 00008480
TPS = TPS * 12. 00008490
AFAS = AFAS * 12. 00008500
M1 = M1 * 12. 00008510
M2 = M2 * 12. 00008520
M3 = M3 * 12. 00008530
M4 = M4 * 12. 00008540
N1 = N1 * 12. 00008550
N2 = N2 * 12. 00008560
N3 = N3 * 12. 00008570
N4 = N4 * 12. 00008580
TX = FLR * CGAM / (2.*S ) 00008590
DO 68 KKK=1,4 00008600
68 TGIF(KKK) = TGIF(KKK) * 12. 00008610
906 CONTINUE 00008620
IF ( NREV .EQ. 1) GO TO 926 00008630
4501 IF( CASE .EQ. CASES ) GO TO 1 00008640
CASE = CASE + 1 00008650
GO TO 20 00008660
2 FORMAT( 20A4 ) 00008670
6091 FORMAT(4F10.0) 00008680
4 FORMAT(1H1 , 61X , 'DECK 6091' // 51X , 'INDUCER HYDRODYNAMIC P00008690
1PROGRAM' /// 3X, 20A4 // ) 00008700
3 FORMAT( 4I5 , F15.5 , 3F10.4) 00008710
5 FORMAT( 4X , 'NI' , 9X , 'NJ ' , 7X , 'NB' , 9X , 'CASES' , 00008720
16X , 'G' , 10X , 'CBHR' // 3X , I3 , 8X , I3 , 2(7X , I4) , 4X , F10.5 , F12.4) 00008730
6 FORMAT(///6X , 'Z' , 14X , 'RH' , 13X , 'RT' , 13X , 'BH*' , 12X , 'BT*' , 12X , 00008740
1'TT' , 13X , 'TA' // ) 00008750
8 FORMAT(1X , I3 , F9.5 , 6F15.5 ) 00008760
23 FORMAT (// T45 , 'PO' , T60 , 'VM' , T75 , 'ALPHA' / (T36 , 3F15.5)) 00008770
17 FORMAT(4F10.4 , I10) 00008780
7 FORMAT(7F10.4) 00008790
22 FORMAT(1H1 , 10X , 'CASE NUMBER -' , I4 // 31X , 'RHO' , 13X , 'MU' , 00008800
1 11X , 'PSAT' , 12X , 'SN' , 12X , 'LOADOP' // 23X , 4F15.5 , I10 // ) 00008810
785 FORMAT(1H1 , 10X , 'CASE NUMBER -' , I4 // 31X , 'RHO' , 13X , 'MU' , 11X , 00008820
1 'PSAT' , 12X , 'SN' , 12X , 'LOADOP' , 12X , 'FLR' // 23X , 4F15.5 , I10 , F20.6 // ) 00008830
19 FORMAT (3F10.0) 00008840
7090 FORMAT(///T21 , 'PHI' , T36 , 'NPSH' , T51 , 'THOMA' , T66 , 'VT' , T81 , 'PT' , 00008850
1 T96 , 'KTIP' // 11X , 6F15.4) 00008860
30 FORMAT(//T54 , 'INLET CONDITIONS' // T12 , 'I' , T29 , 'R' , T46 , 'Q' , 00008870
1 T63 , 'W' , T80 , 'PO' , T95 , 'PREL' , T114 , 'P' / T10 , 'ALPHA' , T27 , 00008880
2 'BETA' , T46 , 'K' , T63 , 'U' , T81 , 'V' , T96 , 'VM' , T113 , 'VU' ) 00008890
41 FORMAT ( / T11 , I2 , T18 , 6(5X , F12.5) / T6 , F12.5 , 6(5X , F12.5)) 00008900
999 CONTINUE 00008910
END 00008920

```

```

*
SUBROUTINE LOAD( PX , M , DPBN , NJ , NI , TCBSI , TCBS , PSAT , 00010
1 B , PREL , C11 , WIN , WJ1 , NB , RIN , BSIN , PRELI , VA , 00020
2 WNJ , REX , BSEX , VEX , Z , R , WEX , PRELEX , VT , PTU , RHO , G , PCZ , 00030
3 TP , T , BETAS , DZ , C22 , WP , WS , PP , PS ) 00040
REAL M 00050
      DIMENSION 00060
1 M( 30 , 15 ) , PX( 30 , 15 ) , DPBN( 30 , 15 ) , 00070
2 A1( 30 , 15 ) , B1( 30 , 15 ) , C1( 30 , 15 ) , 00080
3 D1( 30 , 15 ) , A2( 30 , 15 ) , B2( 30 , 15 ) , 00090
4 C2( 30 , 15 ) , D2( 30 , 15 ) , TCBS( 30 , 15 ) , 00100
5 B( 30 , 15 ) , PREL( 30 , 15 ) , TCBSI( 15 ) , 00110
6 DPB( 15 ) , PS( 30 , 15 ) , PXC( 15 ) , 00120
7 WS( 30 , 15 ) , W( 15 ) , WIN( 15 ) , 00130
8 WJ1( 15 ) , PRELI( 15 ) , BETA( 15 ) , 00140
9 VA( 15 ) , RIN( 15 ) , BSIN( 15 ) , 00150
A PP( 30 , 15 ) , WEX( 15 ) , WNJ( 15 ) , 00160
B VEX( 15 ) , BSEX( 15 ) , REX( 15 ) , 00170
C WP( 30 , 15 ) , Z( 30 ) , R( 30 , 15 ) 00180
D , PRELEX( 15 ) , PSIS( 15 ) , PSIP( 15 ) , TP( 15 ) , T( 15 ) , XSI( 15 ) , BETAS( 15 ) 00190
DATA IFV , ZRO , PI / 5 , 0.0 , 3.141592 / 00200
DO 2 I = 1 , NI 00210
CALL BMFIT( IFV , NJ , M( 1 , I ) , PX( 1 , I ) , ZRO , ZRO , 00220
1 A1( 1 , I ) , B1( 1 , I ) , C1( 1 , I ) , D1( 1 , I ) ) 00230
CALL BMFIT( IFV , NJ , M( 1 , I ) , DPBN( 1 , I ) , ZRO , ZRO , 00240
1 A2( 1 , I ) , B2( 1 , I ) , C2( 1 , I ) , D2( 1 , I ) ) 00250
2 CONTINUE 00260
J = 1 00270
9 I = 1 00280
C 00290
C CALCULATE SUCTION SURFACE CONDITIONS 00300
C 00310
10 SMN = M( J , I ) - TCBS( J , I ) / 2.0 00320
XSI( I ) = 0. 00330
DT = ATAN( ( TP( I ) - T( I ) ) / 2. * SIN( BETAS( I ) ) / DZ ) 00340
IF( DT .GT. 0.0 ) XSI( I ) = ( C22 * R( J , I ) / 2. - T( I ) / SIN( BETAS( I ) ) ) * 00350
1 SIN( BETAS( I ) ) * TAN( DT ) 00360
IF( DT .GT. 0.0 ) SMN = SMN + XSI( I ) 00370
IF( SMN .LT. 0.0 ) GO TO 30 00380
PS( J , I ) = PSAT 00390
IF( J .EQ. 1 ) GO TO 31 00400
IF( B( J , I ) .GT. 0.0 ) GO TO 31 00410
CALL BMEVAL ( NJ , M( 1 , I ) , PX( 1 , I ) , SMN , MERR , A1( 1 , I ) , 00420
1 B1( 1 , I ) , C1( 1 , I ) , D1( 1 , I ) , PXC( I ) , DUM ) 00430
CALL BMEVAL ( NJ , M( 1 , I ) , DPBN( 1 , I ) , SMN , MERR , A2( 1 , I ) , 00440
1 B2( 1 , I ) , C2( 1 , I ) , D2( 1 , I ) , DPB( I ) , DUM ) 00450
PS( J , I ) = PXC( I ) - DPB( I ) / 2.0 00460
IF( PS( J , I ) .LT. PSAT ) PS( J , I ) = PSAT 00470
GO TO 31 00480
C 00490
C UNCOVERED LEADING EDGE REGION 00500
C 00510
30 W( I ) = WIN( I ) - ( WIN( I ) - WJ1( I ) ) * EXP( SMN * NB / RIN( I ) / 00520
1 SIN( BSIN( I ) ) ) 00530
PS( J , I ) = PSAT 00540
IF ( J .EQ. 1 ) GO TO 31 00550

```



```

IF( B(J,I) .GT. 0.0 ) GO TO 31
PXC(I) = PRELI(I) - C11* W(I)**2
BETA(I) = ARSIN( VA(I) / W(I) )
DPB(I) = 2.0 * PI * C11* VA(I) / COS(BETA(I)) * SIN(BETA(I))**2
1 / SIN( BSIN(I))**2 * ( WIN(I) - WJ1(I) ) * EXP( SMN * NB /
2 RIN(I) / SIN( BSIN(I)) )
PS(J,I) = PXC(I) - DPB(I) / 2.0
IF( PS(J,I) .LT. PSAT ) PS(J,I) = PSAT
31 WS(J,I)=SQRT((PRELI(I) - PS(J,I)) / C11
C
C CALCULATE PRESS. SURFACE CONDITIONS
C
40 SMN = M(J,I) + TCBS(J,I) /2.0 + XSI(I)
PP(J,I) = PREL(J,I)
IF( J .EQ. 1 ) GO TO 59
IF( SMN .GT. M(NJ,I) ) GO TO 50
CALL BMEVAL ( NJ , M(1,I) , PX(1,I) , SMN , MERR , A1(1,I) ,
1 B1(1,I) , C1(1,I) , D1(1,I) , PXC(I) , DUM )
CALL BMEVAL ( NJ , M(1,I),DPBN(1,I) , SMN , MERR , A2(1,I) ,
1 B2(1,I) , C2(1,I) , D2(1,I) , DPB(I) , DUM )
PP(J,I) = PXC(I) + DPB(I) / 2.0
IF( PP(J,I) .GT. PREL(J,I) ) PP(J,I) = PREL(J,I)
59 WP(J,I)=SQRT((PREL( J,I) - PP(J,I)) / C11)
GO TO 60
C
C UNCOVERED TRAILING EDGE REGION
C
50 SMNE = SMN - M(NJ,I)
W(I) = WEX(I) - ( WEX(I) - WNJ(I) ) * EXP( -SMNE * NB / REX(I) /
1 SIN( BSEX(I)) )
PXC(I) = PRELEX(I) - C11* W(I)**2
BETA(I) =ARSIN( VEX(I) / W(I) )
DPB(I) = 2.0 * PI * C11* VEX(I) / COS(BETA(I)) * SIN(BETA(I))**2
1 / SIN(BSEX(I))**2 *( WEX(I) - WNJ(I)) * EXP(-SMNE * NB /
2 REX(I) / SIN( BSEX(I)) )
PP(J,I) = PXC(I) + DPB(I) /2.0
IF( PP(J,I) .GT. PRELEX(I) ) PP(J,I) = PRELEX(I)
WP(J,I)=SQRT((PRELEX(I) - PP(J,I))/ C11)
60 DPB(I) = PP(J,I) - PS(J,I)
PSIS(I)= G* (PS(J,I)-PTU)/RHO/VT **2
PSIP(I)= G* (PP(J,I)-PTU)/RHO/VT **2
I = I + 1
IF( I .LE. NI ) GO TO 10
PCZ = Z(J) / Z(NJ)
C
IF( J .EQ. 1) WRITE(6,11)
11 FORMAT(1H1,T45,'BLADE LOADING DATA')
WRITE(6,1)J,Z(J),PCZ
1 FORMAT(/////10X,'J',14X,'Z',14X,'Z/ZT'//I11,2F19.5)
WRITE(6,7)(I,R(J,I),PS(J,I),PP(J,I),WS(J,I),WP(J,I),DPB(I),PSIS(I)
1 , PSIP(I),I=1,NI)
7 FORMAT(/// 9X,'I',14X,'R',13X,'PS',13X,'PP',13X,'WS',13X,'WP',13X,
1'DPB',12X,'PSIS',12X,'PSIP'//(I11,8E15.5//)
J = J + 1
IF( J .LE. NJ) GO TO 9
RETURN
END

```

```

C      PRINT SUBROUTINE FOR DECK 6091                                00000010 *
      SUBROUTINE PRNT5(J,Z,ITE)                                       00000020
      WRITE(6,22) J,Z,ITE                                             00000030
22     FORMAT(1H1,' STATION J =',I3,' , Z = ' F10.5 , ' , ITE = ',I4) 00000040
      WRITE(6,1)                                                       00000050
1      FORMAT(// T8,'I',T23,'RST ',T38,'PCR',T53,'R',T68,'TAU',T83,   00000060
1      'THK',T98,'B'/T8,'P',T23,'PREL',T38,'POREL',T53,'PT',T68,'M*', 00000070
2      T83,'BN',T98,'PCB'/T8,'BETA',T23,'BETA*',T38,'DEV',T53,'DLB*', 00000080
3      T68,'XMTH',T83,'DEL*',T98,'HSF'/T8,'ALPHA',T23,'ETA',T38,'W', 00000090
4      T53,'U',T68,'V',T83,'VU',T98,'VM')                             00000100
      RETURN                                                            00000110
      ENTRY PRNT67(J,Z,I,RSTS,PCR,R,TAU,T,B,P,PREL,POREL,PT,MSTR,BN, 00000120
1      PCB,BETA,BETAS,DEV,DBS,XMTH,ZBL,HSF,ALPHA,ETA,W,U,V,          00000130
2      VU,VM,ITE)                                                      00000140
25     BETADG = BETA * 57.2958                                         00000150
      ALPH = ALPHA * 57.2958                                           00000160
      DE = DEV * 57.2958                                               00000170
      BETS = BETAS * 57.2958                                           00000180
      DB1 = DBS * 57.2957                                              00000190
      WRITE(6,2) I,RSTS,PCR,R,TAU,T ,B,P,PREL,POREL,PT,MSTR,BN,PCB, 00000200
1     BETADG,BETS ,DE ,DB1,XMTH,ZBL,HSF,ALPH ,ETA,W,U,V,VU,VM       00000210
2     FORMAT( /6X,I3,6X,E15.5,                                         00000220
1     5E15.5 / 7E15.5 / 7E15.5 / 7E15.5)                             00000230
      RETURN                                                            00000240
      ENTRY PRNT8 (NPSH, PHI, PSI, H, HI, RN, ETA, SS, QI, CVOL )    00000250
      WRITE (6,3) NPSH, PHI, PSI, H, HI, RN, ETA, SS, QI             00000260
3     FORMAT(/// 45X,' OVERALL PERFORMANCE'//T6,'NPSH',T21,'PHI',T35, 00000270
1     'PSI', T50, 'H', T65, 'HI', T79, 'RN', T95, 'ETA', T110, 'SS', 00000280
2     T123, 'QI' // T3,F10.4, 2(2X,F12.5), 2(2X, F13.3), 2X, F14.2, 00000290
3     3(2X, F12.5))                                                    00000300
      WRITE(6,30) CVOL                                                 00000310
30     FORMAT(// T6,' CVOL' // E15.4)                                  00000320
      RETURN                                                            00000330
      END                                                                00000340

```

		*
	SUBROUTINE QSF H,Y,Z,NDIM	00010
	DIMENSION Y 1 ,Z 1	00020
	HT .3333333*H	00030
	L1 1	00040
	L2 2	00050
	L3 3	00060
	L4 4	00070
	L5 5	00080
	L6 6	00090
	IF NDIM-5 7,8,1	00100
C	NDIM IS GREATER THAN 5. PREPARATIONS OF INTEGRATION LOOP	00110
1	SUM1 Y L2 &Y L2	00120
	SUM1 SUM1&SUM1	00130
	SUM1 HT* Y L1 &SUM1&Y L3	00140
	AUX1 Y L4 &Y L4	00150
	AUX1 AUX1&AUX1	00160
	AUX1 SUM1&HT* Y L3 &AUX1&Y L5	00170
	AUX2 HT* Y L1 &3.875* Y L2 &Y L5 &2.625* Y L3 &Y L4 &Y L6	00180
	SUM2 Y L5 &Y L5	00190
	SUM2 SUM2&SUM2	00200
	SUM2 AUX2-HT* Y L4 &SUM2&Y L6	00210
	Z L1 0.	00220
	AUX Y L3 &Y L3	00230
	AUX AUX&AUX	00240
	Z L2 SUM2-HT* Y L2 &AUX&Y L4	00250
	Z L3 SUM1	00260
	Z L4 SUM2	00270
	IF NDIM-6 5,5,2	00280
C	INTEGRATION LOOP	00290
2	DO 4 I 7,NDIM,2	00300
	SUM1 AUX1	00310
	SUM2 AUX2	00320
	AUX1 Y I-1 &Y I-1	00330
	AUX1 AUX1&AUX1	00340
	AUX1 SUM1&HT* Y I-2 &AUX1&Y I	00350
	Z I-2 SUM1	00360
	IF I-NDIM 3,6,6	00370
3	AUX2 Y I &Y I	00380
	AUX2 AUX2&AUX2	00390
	AUX2 SUM2&HT* Y I-1 &AUX2&Y I&1	00400
4	Z I-1 SUM2	00410
5	Z NDIM-1 AUX1	00420
	Z NDIM AUX2	00430
	RETURN	00440
6	Z NDIM-1 SUM2	00450
	Z NDIM AUX1	00460
	RETURN	00470
C	END OF INTEGRATION LOOP	00480
7	IF NDIM-3 12,11,8	00490
C	NDIM IS EQUAL TO 4 OR 5	00500
8	SUM2 1.125*HT* Y L1 &Y L2 &Y L2 &Y L2 &Y L3 &Y L3 &Y L3 &Y L4	00510
	SUM1 Y L2 &Y L2	00520
	SUM1 SUM1&SUM1	00530
	SUM1 HT* Y L1 &SUM1&Y L3	00540
	Z L1 0.	00550

	AUX1 Y L3 &Y L3	00560
	AUX1 AUX1&AUX1	00570
	Z L2 SUM2-HT* Y L2 &AUX1&Y L4	00580
	IF NDIM=5 10,9,9	00590
9	AUX1 Y L4 &Y L4	00600
	AUX1 AUX1&AUX1	00610
	Z L5 SUM1&HT* Y L3 &AUX1&Y L5	00620
10	Z L3 SUM1	00630
	Z L4 SUM2	00640
	RETURN	00650
C	NDIM IS EQUAL TO 3	00660
11	SUM1 HT* 1.25*Y L1 &Y L2 &Y L2 -.25*Y L3	00670
	SUM2 Y L2 &Y L2	00680
	SUM2 SUM2&SUM2	00690
	Z L3 HT* Y L1 &SUM2&Y L3	00700
	Z L1 0.	00710
	Z L2 SUM1	00720
12	RETURN	00730
	END	00740

		*
	SUBROUTINE NEWGG (NPT, Z, W, X, Y)	00010
	DIMENSION X(1),Y(1)	00020
C		00030
C	SUBROUTINE NEWGN(NPT,X,Y,XBLK,YBLK)	00040
C	NPT = NUMBER OF POINTS PER BLOCK	00050
C	X = KNOWN VALUE	00060
C	Y = UNKNOWN (OUTPUT)	00070
C	XBLK = BLOCK OF X VALUES	00080
C	YBLK = BLOCK OF Y VALUES	00090
C		00100
	IF (Z-X(1))5,5,6	00110
5	W=Y(1)	00120
	GO TO 10	00130
6	DO 7 I=2,NPT	00140
	IF (Z-X(I))9,8,7	00150
7	CONTINUE	00160
	I=NPT	00170
8	W=Y(I)	00180
	GO TO 10	00190
9	W=(Y(I)-Y(I-1))/(X(I)-X(I-1))*(Z-X(I-1))+Y(I-1)	00200
10	RETURN	00210
	END	00220

		*
	SUBROUTINE BMFIT L,N,X,Y,SLOPE0,SLOPEN,A,B,C,D	00010
	DIMENSION X 100 ,Y 100 ,A 100 ,B 100 ,C 100 ,D 100	00020
	KN 3* L-L/3 - 2*L	00030
	K0 L-1 /3	00040
	DO 1 J 2,N	00050
	A J X J -X J-1	00060
1	D J Y J -Y J-1 /A J	00070
	K2 N-2	00080
	IF KN-1 4,5,6	00090
4	C N 3.0* SLOPEN-D N /A N	00100
	B N 0.5	00110
	K3 N	00120
	K1 1	00130
	GO TO 8	00140
5	T 2.0* A N &A N-1	00150
	B N SLOPEN	00160
	GO TO 7	00170
6	T 3.0*A N &A N-1 &A N-1	00180
	SLOPEN 0.0	00190
7	C N-1 6.0* D N -D N-1 -SLOPEN*A N /T	00200
	B N-1 A N-1 /T	00210
	K3 N-1	00220
	K1 2	00230
8	DO 9 J K1,K2	00240
	K N-J	00250
	T 2.0* A K &A K&1 -A K&1 *B K&1	00260
	B K A K /T	00270
9	C K 6.0* D K&1 -D K -A K&1 *C K&1 /T	00280
10	IF K0-1 12,13,11	00290
11	B 1 6.0* D 2 -SLOPE0 -C 2 *A 2 / A 2 * 2.0-B 2	00300
	K1 2	00310
	GO TO 15	00320
12	B 1 SLOPE0	00330
	B 2 C 2 -B 2 *B 1	00340
	GO TO 14	00350
13	B 1 6.0* D 3 -D 2 -A 3 *C 3 / 3.0*A 2 &A 3 * 2.0-B 3	00360
	B 2 B 1	00370
14	K1 3	00380
15	DO 16 J K1,K3	00390
16	B J C J -B J *B J-1	00400
	IF KN-1 18,18,17	00410
17	B N B N-1	00420
C	CUBIC COEFFICIENTS	00430
18	DO 19 J 2,N	00440
	TA 6.0 * A J	00450
	TM B J-1 *X J	00460
	TN X J-1 *B J	00470
	TX X J * X J -X J-1 -X J-1	00480
	TY X J-1 * X J &X J -X J-1	00490
	A J-1 B J -B J-1 /TA	00500
	C J-1 D J & B J * -TX &2.*X J-1 *TN-B J-1 *TY-2.*X J *TM /TA	00510
	B J-1 TM-TN *3.0/TA	00520
19	D J-1 TX*TN &TY*TM /TA &Y J-1 -X J-1 *D J	00530
20	RETURN	00540
	END	00550

		*
	CSBMVAL BEAM EVALUATION SUBROUTINE	00010
	SUBROUTINE BMEVAL N,X,Y,VALU,L,A,B,C,D,YVALU,DERIV	00020
	DIMENSION X 100 ,Y 100 ,A 100 ,B 100 ,C 100 ,D 100	00030
	L 0	00040
	DO 1 J 1,N	00050
	IF X J -VALU 1,2,3	00060
C	1 CONTINUE	00070
	OUT OF RANGE	00080
	L 1	00090
	J N	00100
	2 YVALU Y J	00110
	DERIV VALU* 3.0*VALU*A J &2.0*B J &C J	00120
	RETURN	00130
	3 IF J-1 5,5,4	00140
	4 YVALU VALU* VALU* VALU*A J-1 &B J-1 &C J-1 &D J-1	00150
	DERIV VALU* 3.0*VALU*A J-1 &2.0*B J-1 &C J-1	00160
	RETURN	00170
	5 L -1	00180
	GO TO 2	00190
	END	00200

ZEROC - FILL DESIGNATED AREA OF CORE WITH ZERO OR WITH  
A CONSTANT SUPPLIED IN THE CALLING SEQUENCE.

CALLING SEQUENCE  
CALL ZEROC (FROM,TO)  
OR  
CALL ZEROC (FROM,TO,CONST)

WHERE-FROM-IS THE STARTING ADDRESS  
TO-FINAL ADDRESS TO BE CLEARED  
CONST-THE CONSTANT CORE IS TO BE  
FILLED WITH. IF NOT SUPPLIED  
IN CALLING SEQUENCE, CORE  
WILL BE FILLED WITH ZEROES.

```

PWZERO START 0
BR0 EQU 0
BR1 EQU 1
BR2 EQU 2
BR3 EQU 3
BR4 EQU 4
BR5 EQU 5
BR6 EQU 6
BR7 EQU 7
BR8 EQU 8
BR9 EQU 9
BR10 EQU 10
BR11 EQU 11
BR12 EQU 12
BR13 EQU 13
BR14 EQU 14
BR15 EQU 15
*
ENTRY ZERO
USING *,BR15
ZERO SAVE (14,12),,*
ST BR13,SAVE+4
LA BR10,SAVE
ST BR10,8(0,BR13)
L BR3,0(0,BR1)
L BR4,4(0,BR1)
N BR3,BIGAD
N BR4,BIGAD
CLR BR3,BR4
BNL SWITCH
MODE1 TM 4(BR1),X'80'
MODE BZ NTZRO
MODE A BR4,FORBT
SR BR4,BR3
MORE C BR4,TWO56
BL LESTN
S BR4,TWO56
L BR5,TWO56
MONE S BR5,TWO
STC BR5,MOVE+1
MOVE XC 0(0,BR3),0(BR3)

```

BASE REGISTER 0

INSURE ADDRESS ONLY.  
INSURE ADDRESS ONLY.  
1ST ARG. LESS THAN 2ND ARG.  
NO, THEN SWITCH REGISTERS.  
MORE ARGUMENTS.  
YES,CALCULATE BYTES TO BE CLEARED.  
BR4 EQUAL NO. OF BYTES.  
OVER 255 BYTES TO CLEAR  
YES  
REDUCE BY 256

\*  
ZER00000  
ZER00010  
ZER00020  
ZER00030  
ZER00040  
ZER00050  
ZER00060  
ZER00070  
ZER00080  
ZER00090  
ZER00100  
ZER00110  
ZER00120  
ZER00130  
ZER00140  
ZER00150  
ZER00160  
ZER00170  
ZER00180  
ZER00190  
ZER00200  
ZER00210  
ZER00220  
ZER00230  
ZER00240  
ZER00250  
ZER00260  
ZER00270  
ZER00280  
ZER00290  
ZER00300  
ZER00310  
ZER00320  
ZER00325  
ZER00340  
ZER00330  
ZER00350  
ZER00360  
ZER00370  
ZER00390  
ZER00400  
ZER00410  
ZER00420  
ZER00430  
ZER00440  
ZER00470  
ZER00480  
ZER00450  
ZER00460  
ZER00500  
ZER00510  
ZER00520  
ZER00530  
ZER00540  
ZER00550  
ZER00560



```

A      BR3,TWO56
LTR    BR4,BR4
BC     2,MORE
RETRN  RETURN (14,12),T
LESTN  LR   BR5,BR4
      LA   BR4,0
      B    MONE
SWITCH LR   BR5,BR3
      LR   BR3,BR4
      LR   BR4,BR5
      B    MODE1
NTZRO  L    BR6,8(0,BR1)
      L    BR6,0(0,BR6)
NTZR1  ST   BR6,0(0,BR3)
      CR   BR3,BR4
      BE   RETRN
      A    BR3,FORBT
      B    NTZR1
SAVE   DS   18F
BIGAD  DC   X'00FFFFFF'
FORBT  DC   F'4'
TWO56  DC   F'256'
TWO    DC   F'1'
      END

```

RESTORE AND RETURN

```

ZERO0570
ZERO0580
ZERO0590
ZERO0600
ZERO0610
ZERO0620
ZERO0630
ZERO0640
ZERO0650
ZERO0660
ZERO0670
ZERO0680
ZERO0685
ZERO0690
ZERO0700
ZERO0710
ZERO0720
ZERO0730
ZERO1000
ZERO1010
ZERO1020
ZERO1030
ZERO1050
ZERO9990

```

SECTION III  
STRESS COMPUTER PROGRAM (PWA 6098)

A. GENERAL

The stress computer program breaks the inducer blade into flat triangular elements for analysis. The program then calculates stress magnitude and distribution caused by pressure loading and centrifugal force using the matrix displacement method.

Computer capacity limits the number of free element nodes to 150 which is equivalent to 900 simultaneous equations. Computer time for handling such a problem is approximately 90 minutes. An input option is provided to permit analysis by subsystems. This is a conventional technique in which the structure is divided into a maximum of 10 subsystems with a total of 200 nodes (including hub nodes). Use of the subsystem option reduces computing time by as much as a factor of 10 for a typical inducer. The program requires 180,000 bytes of core (including buffers) on an IBM 360 Model 75 computer. Single precision with 4 bytes/word and 8 bits/byte is used. Fortran IV-G, Level 1, Mod. 3 compilations dated March 1969 were used.

B. INPUT DESCRIPTION

The input to the stress computer program generally consists of: a physical description of the inducer, a description of the finite element breakup to be used, and a description of the blade pressure distribution.

The inducer physical description and blade pressure distribution input are straightforward but the finite element breakup input requires further explanation. When preparing the finite element breakup input it is helpful to sketch the desired pattern as in the example of figure 1. The following limitations should be remembered:

1. The maximum number of free boundary nodes (on boundary generator lines) for the entire system is 50. The minimum is 3.
2. The maximum number of free boundary nodes per subsystem is 15.
3. The maximum number of free internal nodes per subsystem is 15.
4. The maximum number of nodes (fixed, free, boundary and internal) per subsystem is 30.
5. The maximum number of nodes for the entire system is 200.
6. The maximum number of elements for the entire system is 200.

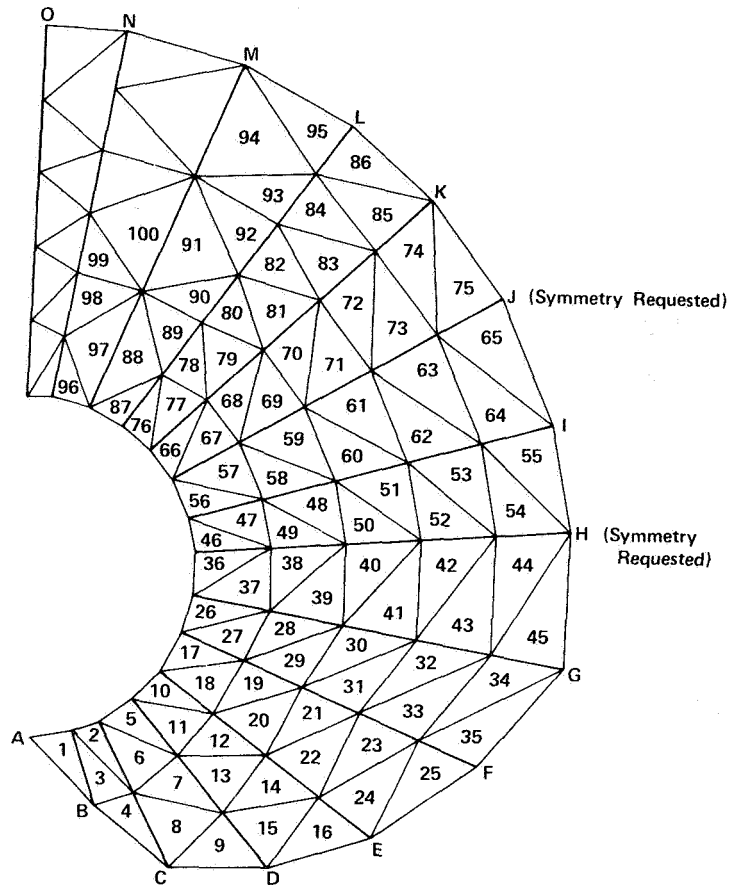


Figure 1. Finite Element Breakup

FD 48167

The computer program will reproduce the sketched elemental breakup properly if the following is remembered when writing the input:

1. If generator line "i" has "ii" points and generator line "i+1" has "ii±1" points, then the lines forming the edges of the finite elements start at the first point of the generator with the least number of points and zig zag between the generator lines. The areas between generators A and B, B and C, D and E, etc., of figure 1 are examples.
2. The area between the first two generator lines with the same number of points will be broken up as shown between generators F and G and G and H of figure 1.
3. The procedure of (2) will be followed for all generators with the same number of points until symmetry about a generator is requested, as was done about generator H in figure 1.
4. The altered breakup will continue for sections between generators with the same number of points, until symmetry is again requested, as was done about generator J in figure 1. After symmetry is again requested, the breakup will revert to the original pattern.

5. If two generators "i" and "j" have "m" and "n" points respectively such that

$$m = 2n-1 \quad \text{and } n > 2$$

or

$$n = 2m-1 \quad \text{and } m > 2$$

then the breakup will be as in the sections between K and L, and L and M of figure 1.

6. Notice that generator A of figure 1 has only one point. In this case

$$RHUB = RTIP \quad \text{and} \quad THHUB = THTIP$$

7. Elements are identified as shown in figure 2.

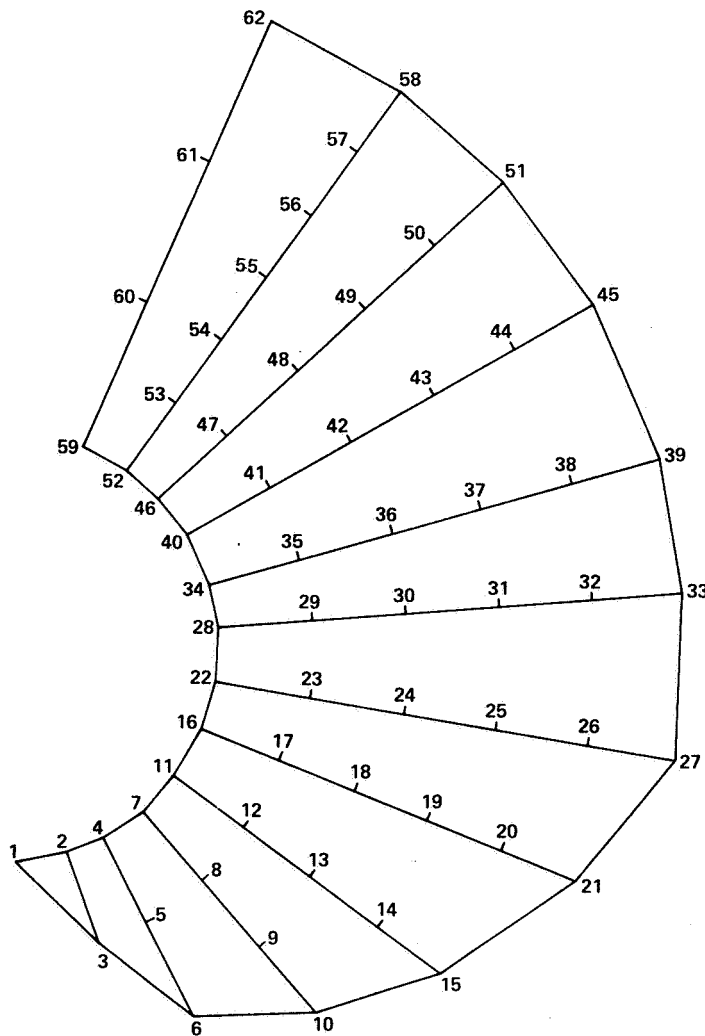


Figure 2. Finite Element Nodes

FD 48168

Unless otherwise specified, data may be input in any consistent set of units. The same units may be used for force and mass. Output will correspond to the input units used. Several examples are listed below:

	Input			Output	
Force	Mass	Length	Displacement	Stress	
lb	lb	ft	ft	lb/ft <sup>2</sup>	
lb	lb	in.	in.	lb/in. <sup>2</sup>	
gram	gram	meter	meter	gram/meter <sup>2</sup>	

Input data to be written on each card is described below. "F" format data should be left adjusted in the column field and should contain a decimal point. "E" format data (.300E08) must be right adjusted. "I" format data should not contain a decimal point and should be right adjusted.

Column	Variable	Format
Card 1	Title Card	
1-80	Input job identification data. As many title cards as required may be input. With a 1 in column 1 the machine will read in another title card. Omit the 1 in column 1 on the last title card to stop the machine from reading title cards.	
Card 2		
1-10	RHO Specific weight of the inducer blade material (MASS=RHO/G).	F10.0
11-20	RPM Rotational speed of the inducer blade (revolutions per minute)	F10.0
21-30	POISSO Poisson's ratio for the material of the inducer blade.	F10.0
31-40	YOUNGS Young's modulus of elasticity for the material of the inducer blade	E10.0
41-50	RADGEN Generator line offset radius. $R_G$ in figure 3 (May be 0).	F10.0
51-55	NCF Centrifugal force option.	I5

Leave blank if the following approximate equation is desired  
 This equation should be used where bending stresses due to gas loading  
 alone are predominant.

$$\left\{ F_c \right\}_N = \frac{\rho \omega^2 \bar{A}_i}{3} \begin{bmatrix} F_{x_1} \\ F_{y_1} \\ F_{z_1} \\ M_{x_1} \\ M_{y_1} \\ M_{z_1} \\ F_{x_2} \\ F_{y_2} \\ F_{z_2} \\ M_{x_2} \\ M_{y_2} \\ M_{z_2} \\ F_{x_3} \\ F_{y_3} \\ F_{z_3} \\ M_{x_3} \\ M_{y_3} \\ M_{z_3} \end{bmatrix} = \begin{bmatrix} \bar{t}_1 x_1 \\ \bar{t}_1 y_1 \\ 0 \\ 0 \\ 0 \\ 0 \\ \bar{t}_2 x_2 \\ \bar{t}_2 y_2 \\ 0 \\ 0 \\ 0 \\ 0 \\ \bar{t}_3 x_3 \\ \bar{t}_3 y_3 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

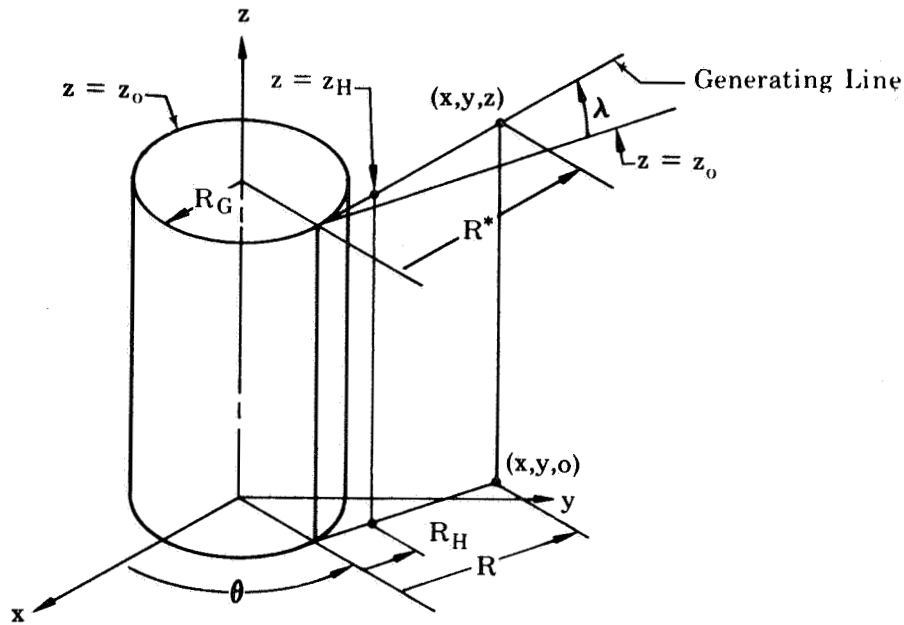


Figure 3. Geometric Parameters of Middle Surface of Inducer Blade

FD 25602A

Input as 1 if the following equation is desired. Use this equation where bending stresses due to centrifugal loads dominate.

$$\left\{ \bar{F}_c \right\}_N = \rho \omega^2 \int_S \bar{t} \left[ H \right]^T \begin{Bmatrix} 1 \\ 0 \\ 3 \end{Bmatrix} \left[ R_I \right]^T \left\{ \begin{array}{c} x_1 \\ y_1 \\ -\bar{x} \cos(z, \bar{x}) - \bar{y} \cos(z, \bar{y}) \end{array} \right\} + \left[ R_I \right] \left\{ \begin{array}{c} \bar{x} \\ \bar{y} \\ 0 \end{array} \right\} d\bar{x}d\bar{y}$$

Column		Variable	Format
55-60	NGL	Total number of input generator lines. Maximum of 100.	I5
61-65	NGS	Number of generator lines about which geometric break-up symmetry is desired.	I5
66-70	NGP	Total number of input elemental pressures	I5
71-75	NSUBS	Total number of subsystems into which the inducer blade is to be divided. Maximum of 100.	I5
76-80	IPRINT	Intermediate print option which should be used only for the checkout of the program. Leave blank for no intermediate print.	I5

Input as 1 for the following intermediate print:

- a. Elemental local membrane stiffness matrices.
- b. Elemental local bending stiffness matrices.
- c. Elemental local pressure force matrices.
- d. Elemental common centrifugal force matrices.
- e. Elemental assembled common stiffness matrices.

Input as 2 (right adjusted with no decimal point) for the following intermediate print:

- a. All of the above
- b. The 6 (N + 1) coefficients for each of the 6 (N) simultaneous equations for nodal deflections (only for NSUBS = 0).

Column	Variable	Format
Card 3	Boundary Lines and G	
1-5	LBOUND (1)-	15
6-10	LBOUND (9)	
etc.		
41-45		
	Generator line numbers which form the boundaries between adjacent subsystems. If NSUBS = 0, leave blank. Otherwise LBOUND (1) is the number of the generator line which forms the boundary between subsystems I and I+1. In the latter case there must be NSUBS-1 values input.	
71-80	G	The gravitational constant in the appropriate F10.0 units. If left blank or input as 0.0, a value of 386.4 is used. MASS = RHO/G.
Card 4	(Symmetry Requests (Optional))	
1-5	NCHB(1)-	I5
6-10	NCBH(NGS)	
etc.		
	Numbers of the generator lines about which geometric break-up symmetry is desired. The only condition allowing this request for break-up symmetry is that the previous generator line and the next generator line must each have the same number of points as does the generator line about which symmetry is requested that is	

$$NUP_{I-1} = NUP_I = NUP_{I+1}$$

Sixteen values per card, as many cards as needed. If NGS on Card 3 was input as zero or left blank, omit this card



Column	Variable	Format
Cards 5, 7, 9, 11	Generator Line Properties (NGL Cards)	
1-10	RAPANG(I) Wrap angle in degrees of the Ith generator line ( $\theta_1$ , and $\theta_2$ in figure 4). No two adjacent wrap angles may be equal. All wrap angles must be either continually increasing or continually decreasing in size.	F10.0
11-20	ZGL(I) z value at the hub of the Ith generator line ( $z_1$ and $z_2$ in figure 4). No two adjacent generator lines may have the same z value unless one of the two lean angles is non-zero.	F10.0
21-30	RHUB(I) If RADGEN $\neq$ 0, then RHUB(I) is the horizontal (x-y plane) distance from the point where the generator line is tangent to a cylinder with a radius of RADGEN to the hub of the Ith generator. If RADGEN = 0, then RHUB (I) is the radial distance from the z-axis to the hub of the Ith generator.	F10.0
31-40	RTIP(I) Measured the same as RHUB(I) except that it is the distance to the tip instead of the hub of the Ith generator.	F10.0

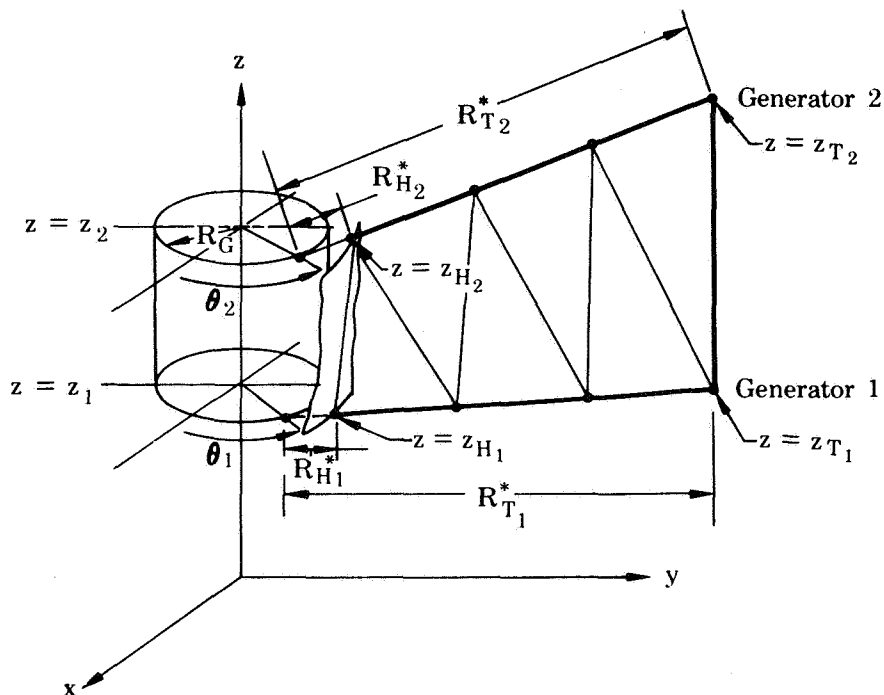


Figure 4. Triangulation of Inducer Blade

FD 25630A

Column	Variable	Format
41-50	THHUB(I) Thickness of the inducer blade at the hub of the Ith generator line.	F10.0
51-60	THTIP(I) Thickness of the inducer blade at the tip of the Ith generator line. Thickness is varied linearly from the hub to the tip of a generator line.	F10.0
61-65	NUP(I) Number of points on the Ith generator line which are used for the division of the inducer blade into triangular elements. These points are evenly spaced between and including the hub and the tip.	I5
66-70	NI Number of pressures on the following card(s) which describes the pressure distribution along the Ith generator line. The pressures will correspond to the points on the generator line which are obtained by dividing the line into NI-1 equal segments. Minimum of 2 and maximum of 15.	I5
71-80	ALEAN(I) Lean angle in degrees of the Ith generator line measured positive upward from the horizontal (x-y plane). These are illustrated in figure 3.	F10.0
Cards 6, 8, 10	Inducer Blade Pressure Distribution (NGL Cards)	
1-10 11-20 etc.	PRESSI(1)- Pressures (positive upward) which describe the pressure distribution along the Ith generator line. Linear interpolation between points is used. Eight values per card; as many cards as needed. Input starting with the hub and ending with the tip.	F10.0
Card 13	NGP Elemental Pressures -(Optional) (NGP Cards)	
These cards are used for inputting elemental pressures which cannot be obtained from the generator line pressures.		
1-5	JI Number of the element to which the following input pressure corresponds.	I5
11-20	PRESSE(JI)- Pressure which corresponds to element JI. This pressure will override the pressure obtained from the generator line pressure distributions.	F10.0

C. OUTPUT DESCRIPTION

X, Y, Z or X COMMON, Y COMMON, Z COMMON	Common coordinates of vertices or nodes of triangular elements.
XL, YL, or X LOCAL, Y LOCAL	Local coordinates of vertices or nodes of triangular elements.
TH	Nodal thickness at vertices of triangular elements.
PRESSURE	Average normal pressure acting on triangular element.
AREA	Area of triangular element.
LOAD	Normal uniform load acting on triangular element.
U, V, W, THETAX, THETAY	Common displacements of nodes or vertices of triangular elements.
U LOCAL, V LOCAL, W LOCAL	Local displacement of nodes or vertices of triangular elements.
SIGMA X BAR, SIGMA Y BAR SHEAR	Stresses at centroid of triangular element.
PRINCIPAL SIGMA X BAR, PRINCIPAL SIGMA Y BAR	Principal stresses at centroid of triangular element.
PRINCIPAL THETA	Principal direction of principal stress at centroid of triangular element.
MAXIMUM SHEAR	Maximum shear stress at centroid of triangular element.
EFFECTIVE STRESS	Relative effective stress at centroid of triangular element.
A, B, C	Bending stress coefficients.
KM	Triangular element local membrane stiffness matrix.
KB	Triangular element local bending stiffness matrix.

D. STRESS COMPUTER PROGRAM

Sample Case (89 Deg Helicoid with Pressure Load)

LISTING OF INPUT CARDS

\*

	2	3	5	7	2
0.298	0.0	0.333	0.30000E08	0.0	
3	3	1.0	4.0	0.1	0.1
2	4	1.0	4.0	0.1	0.1
0.0	0.0	1.0	4.0	0.1	0.1
10.0	10.0	1.0	4.0	0.1	0.1
0.25	0.5	1.0	4.0	0.1	0.1
10.0	10.0	1.0	4.0	0.1	0.1
0.50	1.0	1.0	4.0	0.1	0.1
10.0	10.0	1.0	4.0	0.1	0.1
0.75	1.5	1.0	4.0	0.1	0.1
10.0	10.0	1.0	4.0	0.1	0.1
1.0	2.0	1.0	4.0	0.1	0.1
10.0	10.0	1.0	4.0	0.1	0.1

OUTPUT

INDUCER STRESS PROGRAM - DECK 6098

DATE 6/29/70

TEST CASE FOR 89 DEGREE HELICOID WITH PRESSURE LOAD .

NO. OF SUB-SYSTEMS = 2    CENTRIFUGAL FORCE OPTION = 0  
SUB-SYSTEM BOUNDARIES FORMED BY GENERATOR LINES 3 0 0 0 0 0 0 0 0 0 0

DENSITY = 0.2980    G = 0.3864E 03    RPM = 0.0    POISSON'S RATIO = 0.333    YOUNG'S MODULUS = 0.3000E 08

NO. OF GENERATING LINES = 5    NO. OF SYMMETRY CHANGES REQUESTED = 3

GENERATOR LINE OFFSET RADIUS = 0.0

0 INPUT ELEMENT PRESSURES

SYMMETRY CHANGE ABOUT GENERATOR LINES 2 3 4

INDUCER STRESS PROGRAM - DECK 6098

WRAP ANGLE = 0.0		ZHUB = 0.0		LEAN ANGLE = 0.0		HUB RADIUS = 1.0000		TIP RADIUS = 4.0000	
HUB THICKNESS = 0.1000		TIP THICKNESS = 0.1000		NO. OF POINTS = 7		NO. OF PRESSURES = 2		NO. OF PRESSURES = 2	
10.0000 10.0000									
GENERATOR LINE NUMBER 1 (ANGLES IN DEG.)									
WRAP ANGLE = 0.250000		ZHUB = 0.500		LEAN ANGLE = 0.0		HUB RADIUS = 1.0000		TIP RADIUS = 4.0000	
HUB THICKNESS = 0.1000		TIP THICKNESS = 0.1000		NO. OF POINTS = 7		NO. OF PRESSURES = 2		NO. OF PRESSURES = 2	
10.0000 10.0000									
GENERATOR LINE NUMBER 2 (ANGLES IN DEG.)									
WRAP ANGLE = 0.500000		ZHUB = 1.000		LEAN ANGLE = 0.0		HUB RADIUS = 1.0000		TIP RADIUS = 4.0000	
HUB THICKNESS = 0.1000		TIP THICKNESS = 0.1000		NO. OF POINTS = 7		NO. OF PRESSURES = 2		NO. OF PRESSURES = 2	
10.0000 10.0000									
GENERATOR LINE NUMBER 3 (ANGLES IN DEG.)									
WRAP ANGLE = 0.750000		ZHUB = 1.500		LEAN ANGLE = 0.0		HUB RADIUS = 1.0000		TIP RADIUS = 4.0000	
HUB THICKNESS = 0.1000		TIP THICKNESS = 0.1000		NO. OF POINTS = 7		NO. OF PRESSURES = 2		NO. OF PRESSURES = 2	
10.0000 10.0000									
GENERATOR LINE NUMBER 4 (ANGLES IN DEG.)									
WRAP ANGLE = 1.000000		ZHUB = 2.000		LEAN ANGLE = 0.0		HUB RADIUS = 1.0000		TIP RADIUS = 4.0000	
HUB THICKNESS = 0.1000		TIP THICKNESS = 0.1000		NO. OF POINTS = 7		NO. OF PRESSURES = 2		NO. OF PRESSURES = 2	
10.0000 10.0000									
GENERATOR LINE NUMBER 5 (ANGLES IN DEG.)									

RESULTING TRIANGULAR ELEMENTS

AREA = 0.125005		ELEMENT NO. 1				LOAD = 0.12500E 01	
NODE NO.		X	Y	Z	TH	XL	YL
LA	8	-0.004	1.000	0.500	0.1000	0.0	0.0
LB	9	-0.007	1.500	0.500	0.1000	0.5000	0.0
LC	1	0.0	1.000	0.0	0.1000	-0.0000	-0.5000

AREA = 0.125011		ELEMENT NO. 2				LOAD = 0.12501E 01	
NODE NO.		X	Y	Z	TH	XL	YL
LA	1	0.0	1.000	0.0	0.1000	0.0	0.0
LB	2	0.0	1.500	0.0	0.1000	0.5000	0.0
LC	9	-0.007	1.500	0.500	0.1000	0.5000	0.5000

AREA = 0.125011		ELEMENT NO. 3				LOAD = 0.12501E 01	
NODE NO.		X	Y	Z	TH	XL	YL
LA	9	-0.007	1.500	0.500	0.1000	0.0	0.0
LB	10	-0.009	2.000	0.500	0.1000	0.5000	0.0
LC	2	0.0	1.500	0.0	0.1000	-0.0000	-0.5000

AREA = 0.125019		ELEMENT NO. 4				LOAD = 0.12502E 01	
NODE NO.		X	Y	Z	TH	XL	YL
LA	2	0.0	1.500	0.0	0.1000	0.0	0.0
LB	3	0.0	2.000	0.0	0.1000	0.5000	0.0
LC	10	-0.009	2.000	0.500	0.1000	0.5000	0.5001

AREA = 0.125019		ELEMENT NO. 5				LOAD = 0.12502E 01	
NODE NO.		X	Y	Z	TH	XL	YL
LA	10	-0.009	2.000	0.500	0.1000	0.0	0.0
LB	11	-0.011	2.500	0.500	0.1000	0.5000	0.0
LC	3	0.0	2.000	0.0	0.1000	-0.0000	-0.5001

AREA = 0.125030		ELEMENT NO. 6				LOAD = 0.12503E 01	
NODE NO.		X	Y	Z	TH	XL	YL
LA	3	0.0	2.000	0.0	0.1000	0.0	0.0
LB	4	0.0	2.500	0.0	0.1000	0.5000	0.0
LC	11	-0.011	2.500	0.500	0.1000	0.5000	0.5001

AREA = 0.125030		ELEMENT NO. 7				LOAD = 0.12503E 01	
NODE NO.		X	Y	Z	TH	XL	YL
LA	11	-0.011	2.500	0.500	0.1000	0.0	0.0
LB	12	-0.013	3.000	0.500	0.1000	0.5000	0.0
LC	4	0.0	2.500	0.0	0.1000	-0.0000	-0.5001

(CONTINUING TO ELEMENT NO. 48)



COMMON SYSTEM  
DEFLECTION PRINTOUT

NODE NO.	X	Y	Z	U	V	W	THETA X	THETA Y
1	0.0	1.000	0.0	0.0	0.0	0.0	0.0	0.0
2	0.0	1.500	0.0	0.25089E-02	0.17052E-06	0.24327E-04	0.38714E 00	-0.53928E-03
3	0.0	2.000	0.0	0.98944E-02	0.26466E-06	0.11042E-03	0.30205E 00	-0.68889E-03
4	0.0	2.500	0.0	0.20361E-01	0.27758E-06	0.25211E-03	0.20527E 00	-0.65898E-03
5	0.0	3.000	0.0	0.32631E-01	0.24037E-06	0.43287E-03	0.12100E 00	-0.55074E-03
6	0.0	3.500	0.0	0.45705E-01	0.18167E-06	0.63427E-03	0.63318E-01	-0.43868E-03
7	0.0	4.000	0.0	0.59018E-01	0.16761E-06	0.84282E-03	0.44800E 00	-0.44323E-03
8	-0.004	1.000	0.500	0.0	0.0	0.0	0.0	0.0
9	-0.007	1.500	0.500	0.23020E-02	0.99425E-05	0.20302E-04	0.14297E 00	0.48113E-03
10	-0.009	2.000	0.500	0.95196E-02	0.41318E-04	0.10388E-03	0.44259E-01	-0.70705E-05
11	-0.011	2.500	0.500	0.20009E-01	0.87003E-04	0.2445E-03	-0.84348E-02	-0.24951E-03
12	-0.013	3.000	0.500	0.32343E-01	0.14079E-03	0.42536E-03	-0.35288E-01	-0.34709E-03
13	-0.015	3.500	0.500	0.45486E-01	0.19813E-03	0.62760E-03	-0.39057E-01	-0.34380E-03
14	-0.017	4.000	0.500	0.58810E-01	0.25627E-03	0.83556E-03	-0.37464E-01	-0.34855E-03
15	-0.009	1.000	1.000	0.0	0.0	0.0	0.0	0.0
16	-0.013	1.500	1.000	0.24665E-02	0.21536E-04	0.22431E-04	0.42030E 00	0.36714E-02
17	-0.017	2.000	1.000	0.96494E-02	0.84231E-04	0.10613E-03	0.31171E 00	0.27319E-02
18	-0.022	2.500	1.000	0.20098E-01	0.17543E-03	0.24640E-03	0.20020E 00	0.17702E-02
19	-0.026	3.000	1.000	0.32396E-01	0.28277E-03	0.42677E-03	0.10203E 00	0.92733E-03
20	-0.031	3.500	1.000	0.45509E-01	0.39721E-03	0.62834E-03	0.38456E-01	0.39161E-03
21	-0.035	4.000	1.000	0.58828E-01	0.51345E-03	0.83623E-03	0.11255E 02	0.98275E-01
22	-0.013	1.000	1.500	0.0	0.0	0.0	0.0	0.0
23	-0.020	1.500	1.500	0.23050E-02	0.30261E-04	0.20342E-04	0.14309E 00	0.20231E-02
24	-0.026	2.000	1.500	0.95296E-02	0.12494E-03	0.10407E-03	0.44731E-01	0.79626E-03
25	-0.033	2.500	1.500	0.20027E-01	0.26244E-03	0.24488E-03	-0.75670E-02	0.12469E-03
26	-0.039	3.000	1.500	0.32370E-01	0.42405E-03	0.42613E-03	-0.34728E-01	-0.25220E-03
27	-0.046	3.500	1.500	0.45522E-01	0.59621E-03	0.62878E-03	-0.38685E-01	-0.32426E-03
28	-0.052	4.000	1.500	0.58852E-01	0.77071E-03	0.83717E-03	-0.37969E-01	-0.25258E-03
29	-0.017	1.000	2.000	0.0	0.0	0.0	0.0	0.0
30	-0.026	1.500	2.000	0.26164E-02	0.45414E-04	0.24442E-04	0.38722E 00	0.73072E-02
31	-0.035	2.000	2.000	0.99145E-02	0.17261E-03	0.11082E-03	0.30149E 00	0.59716E-02
32	-0.044	2.500	2.000	0.20395E-01	0.35543E-03	0.25294E-03	0.20423E 00	0.42543E-02
33	-0.052	3.000	2.000	0.32679E-01	0.56980E-03	0.43428E-03	0.11952E 00	0.26772E-02
34	-0.061	3.499	2.000	0.45762E-01	0.79818E-03	0.63625E-03	0.64346E-01	0.16011E-02
35	-0.070	3.999	2.000	0.59082E-01	0.10307E-02	0.84537E-03	-0.98223E 00	-0.16653E-01

LOCAL SYSTEM  
DEFLECTION AND STRESS PRINTOUT

NODE NO.	ELEMENT NO. 1			ELEMENT NO. 2		
	X	Y	Z	U	V	W
LA	COMMON	COMMON	COMMON	LOCAL	LOCAL	LOCAL
LB	-0.004	1.000	0.500	0.0	0.0	0.0
LC	-0.007	1.500	0.500	-0.10169E-06	0.21391E-06	0.23021E-02
	0.0	1.000	0.0	0.0	0.0	0.0

BENDING STRESSES = A \* ( LOCAL X VALUE ) + B \* ( LOCAL Y VALUE ) + C

	A			B			C			PRINCIPAL SIGMAYBAR	PRINCIPAL SIGMAXBAR	SHEAR	PRINCIPAL SIGMAYBAR	PRINCIPAL SIGMAXBAR	THETA (DEG)	MAXIMUM SHEAR	EFFECTIVE STRESS
	SIGMAXBAR	SIGMAYBAR	SHEAR	SIGMAXBAR	SIGMAYBAR	SHEAR	SIGMAXBAR	SIGMAYBAR	SHEAR								
MEMBRANE	-0.68627E 01	-0.22855E 01	0.48143E 01	-0.99047E 01	-0.99047E 01	0.75644E 00	-0.32287E 02	-0.32287E 02	-0.53306E 01	-0.32287E 02	0.10304E 02	-0.53306E 01	-0.32287E 02	0.10304E 02	-0.53306E 01	0.10304E 02	
BEND. (TOP)	-0.31391E 05	-0.10453E 05	-0.21430E 03	-0.31393E 05	-0.31393E 05	-0.10451E 05	0.58636E 00	0.58636E 00	-0.10471E 05	0.58636E 00	0.27689E 05	-0.10471E 05	0.58636E 00	0.27689E 05	-0.10471E 05	0.27689E 05	
TOT. (TOP)	-0.31398E 05	-0.10456E 05	-0.20949E 03	-0.31400E 05	-0.31400E 05	-0.10454E 05	0.57306E 00	0.57306E 00	-0.10473E 05	0.57306E 00	0.27695E 05	-0.10473E 05	0.57306E 00	0.27695E 05	-0.10473E 05	0.27695E 05	
BEND. (BOT)	0.31391E 05	0.10453E 05	0.21430E 03	0.31393E 05	0.31393E 05	0.10451E 05	0.58636E 00	0.58636E 00	0.10471E 05	0.58636E 00	0.27689E 05	0.10471E 05	0.58636E 00	0.27689E 05	0.10471E 05	0.27689E 05	
TOT. (BOT)	0.31384E 05	0.10451E 05	0.21912E 03	0.31386E 05	0.31386E 05	0.10449E 05	0.59966E 00	0.59966E 00	0.10469E 05	0.59966E 00	0.27683E 05	0.10469E 05	0.59966E 00	0.27683E 05	0.10469E 05	0.27683E 05	

NODE NO.	ELEMENT NO. 1			ELEMENT NO. 2		
	X	Y	Z	U	V	W
LA	COMMON	COMMON	COMMON	LOCAL	LOCAL	LOCAL
LB	0.0	1.000	0.0	0.0	0.0	0.0
LC	0.0	1.500	0.0	0.17052E-06	-0.98223E-05	0.26090E-02
	-0.007	1.500	0.500	0.99425E-05	-0.98292E-05	0.23020E-02

BENDING STRESSES = A \* ( LOCAL X VALUE ) + B \* ( LOCAL Y VALUE ) + C

	A			B			C			PRINCIPAL SIGMAYBAR	PRINCIPAL SIGMAXBAR	SHEAR	PRINCIPAL SIGMAYBAR	PRINCIPAL SIGMAXBAR	THETA (DEG)	MAXIMUM SHEAR	EFFECTIVE STRESS
	SIGMAXBAR	SIGMAYBAR	SHEAR	SIGMAXBAR	SIGMAYBAR	SHEAR	SIGMAXBAR	SIGMAYBAR	SHEAR								
MEMBRANE	0.54296E 05	-0.84832E 04	-0.35774E 05	-0.11497E 01	-0.11507E 02	0.31835E 01	-0.80186E 01	-0.80186E 01	0.41617E 01	-0.80186E 01	0.10291E 02	0.41617E 01	-0.80186E 01	0.10291E 02	0.41617E 01	0.10291E 02	
BEND. (TOP)	-0.27530E 05	-0.44909E 05	0.18353E 05	0.40850E 04	-0.19864E 05	0.24651E 04	-0.10731E 02	-0.10731E 02	-0.11164E 05	0.24651E 04	0.21204E 05	-0.11164E 05	0.24651E 04	0.21204E 05	-0.11164E 05	0.21204E 05	
TOT. (TOP)	-0.19078E 05	0.16943E 04	0.40838E 04	0.40838E 04	-0.19852E 05	0.24683E 04	-0.10732E 02	-0.10732E 02	-0.11160E 05	0.24683E 04	0.21194E 05	-0.11160E 05	0.24683E 04	0.21194E 05	-0.11160E 05	0.21194E 05	
BEND. (BOT)	0.19089E 05	0.16910E 04	-0.40850E 04	-0.40850E 04	0.19864E 05	-0.24651E 04	-0.10731E 02	-0.10731E 02	0.11164E 05	-0.24651E 04	0.21204E 05	0.11164E 05	-0.24651E 04	0.21204E 05	0.11164E 05	0.21204E 05	
TOT. (BOT)	0.19101E 05	-0.16976E 04	-0.40861E 04	-0.40861E 04	0.19875E 05	-0.24619E 04	-0.10730E 02	-0.10730E 02	0.11168E 05	-0.24619E 04	0.21213E 05	0.11168E 05	-0.24619E 04	0.21213E 05	0.11168E 05	0.21213E 05	

LOCAL SYSTEM  
DEFLECTION AND STRESS PRINTOUT

NODE NO.	ELEMENT NO. 3			VALUE AT CENTROID			EFFECTIVE STRESS
	X	Y	Z	A	B	C	
MEMBRANE	SIGMAXBAR	SIGMAYBAR	SIGMAXBAR	PRINCIPAL SIGMAXBAR	PRINCIPAL SIGMAYBAR	PRINCIPAL THETA (DEG)	MAXIMUM SHEAR
BEND.(TOP)	-0.81366E 01	-0.31418E 01	0.47579E 01	-0.11013E 02	-0.26573E 00	-0.31153E 02	-0.53735E 01
TOT.(TOT)	-0.19667E 05	-0.39326E 04	0.39986E 04	-0.20625E 05	-0.29747E 04	-0.13471E 02	-0.88252E 04
BEND.(BOT)	0.19667E 05	0.39326E 04	0.40034E 04	-0.20635E 05	-0.29760E 04	-0.13481E 02	-0.88296E 04
TOT.(TOT)	0.19659E 05	0.39294E 04	-0.39938E 04	0.20615E 05	0.29735E 04	-0.13461E 02	0.88209E 04

NODE NO.	ELEMENT NO. 4			VALUE AT CENTROID			EFFECTIVE STRESS
	X	Y	Z	A	B	C	
MEMBRANE	SIGMAXBAR	SIGMAYBAR	SIGMAXBAR	PRINCIPAL SIGMAXBAR	PRINCIPAL SIGMAYBAR	PRINCIPAL THETA (DEG)	MAXIMUM SHEAR
BEND.(TOP)	0.63159E 01	0.20000E 01	-0.14551E 00	0.63208E 01	0.19951E 01	-0.19288E 01	0.21629E 01
TOT.(TOT)	-0.14473E 05	0.26268E 03	0.30943E 04	-0.15097E 05	0.88605E 03	-0.11390E 02	-0.79914E 04
BEND.(BOT)	0.14473E 05	-0.26268E 03	-0.30942E 04	-0.15091E 05	0.88817E 03	-0.11393E 02	-0.79894E 04
TOT.(TOT)	0.14480E 05	-0.26068E 03	-0.30945E 04	0.15103E 05	-0.88395E 03	-0.11388E 02	0.79935E 04

LOCAL SYSTEM  
DEFLECTION AND STRESS PRINTOUT

NODE NO.	ELEMENT NO. 5					
	X	Y	Z	U	V	W
LA 10	COMMON	COMMON	COMMON	LOCAL	LOCAL	LOCAL
LB 11	-0.009	2.000	0.500	-0.21986E-06	-0.62258E-04	0.95201E-02
LC 3	-0.011	2.500	0.500	-0.30360E-06	-0.10476E-03	0.20011E-01
	0.0	2.000	0.0	-0.42908E-04	-0.62255E-04	0.98948E-02

BENDING STRESSES = A \* ( LOCAL X VALUE ) + B \* ( LOCAL Y VALUE ) + C

	A			B			C			VALUE AT CENTROID	PRINCIPAL THETA (DEG)	MAXIMUM SHEAR	EFFECTIVE STRESS
	SIGMAXBAR	SIGMAYBAR	SHEAR	SIGMAXBAR	SIGMAYBAR	SHEAR	SIGMAXBAR	SIGMAYBAR	SHEAR				
MEMBRANE	-0.56875E 01	-0.19883E 01	0.41350E 01	-0.83403E 01	0.66454E 00	-0.32872E 02	-0.45024E 01	-0.32872E 02	-0.45024E 01	-0.32872E 02	-0.45024E 01	0.86917E 01	
BEND. (TOP)	-0.12337E 05	-0.32823E 04	0.30754E 04	-0.13283E 05	-0.23365E 04	-0.17094E 02	-0.54731E 04	-0.17094E 02	-0.54731E 04	-0.17094E 02	-0.54731E 04	0.12282E 05	
TOT. (TOP)	-0.12343E 05	-0.32843E 04	0.30795E 04	-0.13290E 05	-0.23365E 04	-0.17106E 02	-0.54770E 04	-0.17106E 02	-0.54770E 04	-0.17106E 02	-0.54770E 04	0.12290E 05	
BEND. (BOT)	0.12337E 05	0.32823E 04	-0.30754E 04	0.13283E 05	0.23365E 04	-0.17094E 02	0.54731E 04	-0.17094E 02	0.54731E 04	-0.17094E 02	0.54731E 04	0.12282E 05	
TOT. (BOT)	0.12331E 05	0.32803E 04	-0.30713E 04	0.13275E 05	0.23365E 04	-0.17082E 02	0.54693E 04	-0.17082E 02	0.54693E 04	-0.17082E 02	0.54693E 04	0.12275E 05	

NODE NO.	ELEMENT NO. 6					
	X	Y	Z	U	V	W
LA 3	COMMON	COMMON	COMMON	LOCAL	LOCAL	LOCAL
LB 4	0.0	2.000	0.0	0.26466E-06	-0.10541E-03	0.98945E-02
LC 11	0.0	2.500	0.0	0.27758E-06	-0.19204E-03	0.20361E-01
	-0.011	2.500	0.500	0.87003E-04	-0.19203E-03	0.20010E-01

BENDING STRESSES = A \* ( LOCAL X VALUE ) + B \* ( LOCAL Y VALUE ) + C

	A			B			C			VALUE AT CENTROID	PRINCIPAL THETA (DEG)	MAXIMUM SHEAR	EFFECTIVE STRESS
	SIGMAXBAR	SIGMAYBAR	SHEAR	SIGMAXBAR	SIGMAYBAR	SHEAR	SIGMAXBAR	SIGMAYBAR	SHEAR				
MEMBRANE	0.40188E 05	-0.70864E 04	-0.20935E 05	-0.87210E 04	0.98945E-02	-0.87210E 04	0.17093E 01	0.43231E 02	-0.87210E 04	0.43231E 02	0.17093E 01	0.31091E 01	
BEND. (TOP)	-0.17507E 04	-0.20203E 05	0.38288E 04	-0.12277E 03	0.31225E 03	-0.12377E 02	-0.47342E 04	-0.12377E 02	-0.12277E 03	-0.12377E 02	-0.47342E 04	0.93161E 04	
TOT. (TOP)	-0.17507E 04	-0.20203E 05	0.38288E 04	-0.12277E 03	0.31225E 03	-0.12377E 02	-0.47342E 04	-0.12377E 02	-0.12277E 03	-0.12377E 02	-0.47342E 04	0.93161E 04	
BEND. (BOT)	0.87210E 04	0.12277E 03	-0.19823E 04	0.91557E 04	-0.31382E 03	-0.12387E 02	0.47342E 04	-0.12387E 02	0.91557E 04	-0.12387E 02	0.47342E 04	0.93161E 04	
TOT. (BOT)	0.87221E 04	0.12362E 03	-0.19806E 04	0.91564E 04	-0.31068E 03	-0.12368E 02	0.47335E 04	-0.12368E 02	0.91564E 04	-0.12368E 02	0.47335E 04	0.93156E 04	

LOCAL SYSTEM  
DEFLECTION AND STRESS PRINTOUT

NODE NO.	ELEMENT NO. 7			VALUE AT CENTROID			EFFECTIVE STRESS
	X COMMON	Y COMMON	Z COMMON	A	B	C	
LA 11	-0.011	2.500	0.500	-0.11476E 05	0.45882E 04	-0.39954E 04	0.34335E 01
LB 12	-0.013	3.000	0.500	0.12030E 05	0.14485E 05	-0.21150E 04	0.67966E 04
LC 4	0.0	2.500	0.0	0.17628E 03	-0.11891E 05	0.0	0.67966E 04

MEMBRANE	ELEMENT NO. 7			VALUE AT CENTROID			EFFECTIVE STRESS
	X COMMON	Y COMMON	Z COMMON	A	B	C	
BEND. (TOP)	-0.20977E 01	-0.18750E 00	0.16069E 01	-0.30119E 01	0.72676E 00	-0.29637E 02	0.18693E 01
TOT. (TOP)	-0.66728E 04	-0.25248E 04	0.20117E 04	-0.74882E 04	-0.17095E 04	-0.22063E 02	0.28894E 04
BEND. (BOT)	0.66728E 04	0.25248E 04	-0.20117E 04	0.74882E 04	0.17095E 04	-0.22063E 02	0.28894E 04
TOT. (BOT)	0.66707E 04	0.25246E 04	-0.20101E 04	0.74852E 04	0.17101E 04	-0.22058E 02	0.28876E 04

BENDING STRESSES = A \* ( LOCAL X VALUE ) + B \* ( LOCAL Y VALUE ) + C

NODE NO.	ELEMENT NO. 8			VALUE AT CENTROID			EFFECTIVE STRESS
	X COMMON	Y COMMON	Z COMMON	A	B	C	
LA 4	0.0	2.500	0.0	0.22784E 05	-0.48489E 04	-0.11054E 05	0.34932E 01
LB 5	0.0	3.000	0.0	0.15478E 04	-0.10656E 05	-0.42677E 04	0.45423E 04
LC 12	-0.013	3.000	0.500	0.97439E 03	0.45308E 04	0.10802E 03	0.45454E 04

MEMBRANE	ELEMENT NO. 8			VALUE AT CENTROID			EFFECTIVE STRESS
	X COMMON	Y COMMON	Z COMMON	A	B	C	
BEND. (TOP)	-0.21953E 01	0.12891E 00	0.15366E 01	-0.29598E 01	0.89337E 00	-0.26450E 02	0.19266E 01
TOT. (TOP)	-0.42677E 04	-0.27051E 03	0.10802E 04	-0.45409E 04	0.27222E 01	-0.14195E 02	0.22718E 04
BEND. (BOT)	0.42677E 04	0.27051E 03	-0.10817E 04	0.45437E 04	0.34421E 01	-0.14205E 02	0.22736E 04
TOT. (BOT)	0.42655E 04	0.27064E 03	-0.10786E 04	0.45381E 04	-0.20027E 01	-0.14185E 02	0.22701E 04

BENDING STRESSES = A \* ( LOCAL X VALUE ) + B \* ( LOCAL Y VALUE ) + C

(CONTINUING TO ELEMENT NO. 48)

E. STRESS COMPUTER PROGRAM LISTING

```

C THIS IS THE MAIN PROGRAM FOR THE INDUCER STRESS PROGRAM -DECK 6098MAIN001
C
COMMON X ( 200) , Y ( 200) , Z ( 200) , TH ( 200) ,MAIN0002
1 PRESSE( 200) , XL ( 200,3) , YL ( 200,3) , MAIN0003
2 RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) ,MAIN0004
3 THHUB ( 100) , THIP ( 100) , PRESSL(100,15),EDCM ( 3,3) ,MAIN0005
4 RHO , OMEGA , POISSO , YOUNGS , RADGEN , MAIN0006
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT , MAIN0007
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) , MAIN0008
7 PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) , MAIN0009
8 PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200) , FORCE( MAIN0010
9 200,6) , ALEAN(100) MAIN0011
COMMON / MANE / NSUBS, IPOS(200), NBTS(10,15), NITS(10,15), NBN(10), MAIN0012
1 INTN(10) MAIN0013
COMMON / TBAR / THBAR(200) MAIN0014
DEFINE FILE 1(200,324,U,IR1),3(900,900,U,IR3),4(500,602,U,IR4) MAIN0015
C SET UP ALL ELEMENTAL AND NODAL INFORMATION . MAIN0016
5 CALL MAIN1 ( IPUNCH ) MAIN0017
IF ( NSUBS .EQ. 0 ) GO TO 10 MAIN0018
C ASSEMBLE THE KAA AND KAB PORTIONS OF THE COMMON STIFFNESS MATRIX MAIN0019
C FOR EACH SUB-SYSTEM . MAIN0020
CALL ASSEM1 MAIN0021
C ASSEMBLE THE KBA AND KBB-1 PORTIONS OF THE COMMON STIFFNESS MAIN0022
C MATRIX FOR EACH SUB-SYSTEM . MAIN0023
CALL ASSEM2 MAIN0024
IF ( NSUBS .LT. 0 ) GO TO 5 MAIN0025
C CALCULATE THE SUB-SYSTEM PORTIONS OF THE SYSTEM STIFFNESS MATRIX MAIN0026
C AND SYSTEM BOUNDARY FORCE COEFFICIENT MATRIX . MAIN0027
CALL CALC MAIN0028
C ASSEMBLE THE SUB-SYSTEM MATRICES INTO THE SYSTEM MATRIX . MAIN0029
CALL ASSEM3 ( NBNODE ) MAIN0030
C SOLVE FOR THE BOUNDARY NODE DEFLECTIONS IN THE COMMON COORDINATE MAIN0031
C SYSTEM . MAIN0032
CALL BDEFL ( NBNODE ) MAIN0033
IF ( NSUBS .LT. 0 ) GO TO 5 MAIN0034
C SOLVE FOR THE INTERNAL NODE DEFLECTIONS OF EACH SUB-SYSTEM . MAIN0035
CALL IDEFL . MAIN0036
C CALCULATE THE LOCAL NODAL DISPLACEMENT MATRIX (DISPLL), THE MAIN0037
C LOCAL MEMBRANE STRESS MATRIX (STRSLM), AND THE LOCAL BENDING MAIN0038
C STRESS MATRIX (STRSLB) . MAIN0039
10 CALL STRESS ( IPUNCH ) MAIN0040
GO TO 5 MAIN0041
END MAIN0042
MAIN0043

```

SUBROUTINE MAIN1 ( IPUNCH )		
		MAIN1001
C	COMMON X ( 200 ) , Y ( 200 ) , Z ( 200 ) , TH ( 200 )	MAIN1002
	1 PRESSE( 200 ) , XL ( 200,3 ) , YL ( 200,3 ) ,	MAIN1003
	2 RAPANG( 100 ) , ZGL ( 100 ) , RHUB ( 100 ) , RTIP ( 100 )	MAIN1004
	3 THHUB ( 100 ) , THTIP ( 100 ) , PRESSL(100,15),EDCM ( 3,3 )	MAIN1005
	4 RHO , OMEGA , POISSO , YOUNGS , RADGEN ,	MAIN1006
	5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3 ) , NP , NT ,	MAIN1007
	6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,	MAIN1008
	7 PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) ,	MAIN1009
	8 PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200) ,	MAIN1010
	9 FORCE(200,6) , ALEAN(100)	MAIN1011
	COMMON / MANE / NSUBS,IPOS(200),NBTS(10,15),NITS(10,15),NBN(10),	MAIN1012
	1 INTN(10)	MAIN1013
	COMMON / TBAR / THBAR(200)	MAIN1014
	DIMENSION ICOL(15) , NUP(100) , NCHB(100) , LBOUND(10)	MAIN1015
	DIMENSION SYS(2) , SYS1(2) , SYS2(2)	MAIN1016
	DATA ICOL / 1 , 2 , 7 , 8 , 13 , 14 , 3 , 4 , 5 , 9 , 10 , 11 ,	MAIN
	1 15 , 16 , 17 /	MAIN1017
	DATA SYS1 , SYS2 / 4H COM , 4H MON , 4H LO , 4H CAL /	MAIN1018
	WRITE (3*1) RHO	MAIN
	WRITE (4*1) RHO	MAIN1019
	WRITE (1*1) RHO	MAIN1020
	5 CALL ZERO (X,FORCE(200,6))	MAIN1021
C	READ AND PRINT ALL INPUT	MAIN1022
	CALL INPUT ( IPRINT,NGP,NUP,NCHB,LBOUND,NCF,IPUNCH )	MAIN1023
	SYS(1) = SYS1(1)	MAIN1024
	SYS(2) = SYS1(2)	MAIN
	IF ( NCF .EQ. 0 ) GO TO 10	MAIN
	SYS(1) = SYS2(1)	MAIN
	SYS(2) = SYS2(2)	MAIN
C	TRIANGULATION OF INDUCER BLADE AND DETERMINATION OF THICKNESS AT	MAIN1025
C	EACH VERTEX AND PRESSURE ON EACH TRIANGLE .	MAIN1026
10	CALL GEOM ( NUP,NCHB,LBOUND )	MAIN1027
	IF ( NGP .LE. 0 ) GO TO 13	MAIN1028
	DO 11 I = 1,NGP	MAIN1029
11	READ (5,12) J,PRESSE(J)	MAIN1030
12	FORMAT ( 15,5X,F10.0 )	MAIN1031
13	IF ( ( NP .GT. 200 ) .OR. ( NT .GT. 200 ) ) GO TO 5	MAIN1032
	DO 30 I = 1,NT	MAIN1033
	LA = NEXT(I,1)	MAIN1034
	LB = NEXT(I,2)	MAIN1035
	LC = NEXT(I,3)	MAIN1036
	IMEX(LA) = IMEX(LA) + 1	MAIN1037
	IMEX(LB) = IMEX(LB) + 1	MAIN1038
	IMEX(LC) = IMEX(LC) + 1	MAIN1039
	MEX(LA,IMEX(LA)) = I	MAIN1040
	MEX(LB,IMEX(LB)) = I	MAIN1041
	MEX(LC,IMEX(LC)) = I	MAIN1042
C	CALCULATE THE DIRECTION COSINE MATRIX (EDCM) FOR A TRIANGULAR ELEM	MAIN1043
	CALL DIRCOS (LA,LB,LC,I)	MAIN1044
C	CALCULATE THE LOCAL COORDINATES (XL,YL,ZL) FOR A TRIANGULAR ELEMEN	MAIN1045
	CALL LCOORD (LA,LB,LC,I)	MAIN1046
C	CALCULATE THE MEMBRANE STIFFNESS MATRIX (ELMSM) FOR A TRIANGULAR	MAIN1047
C	ELEMENT IN THE LOCAL COORDINATE SYSTEM (XL,YL,ZL)	MAIN1048
	CALL MEMSTF ( LA,LB,LC,I )	MAIN1049
C	CALCULATE THE BENDING STIFFNESS MATRIX (ELBSM) FOR A TRIANGULAR	MAIN1050
C	ELEMENT IN THE LOCAL COORDINATE SYSTEM (XL,YL,ZL)	MAIN1051



```

CALL BEVSTF ( LA, LB, LC, I )
IF ( IPRINT .GE. 1 )
14 WRITE (6,14) ((ELMSM(J,K),K=1,6),J=1,6),((ELBSM(J,K),K=1,9),J=1,9)
C FORMAT(1H1/45X,2HKM / 6(10X,6E14.6/) //65X,2HKB/9( 1X,9E14.6/))
C ASSEMBLE LOCAL STIFFNESS MATRIX (ELSTIF) FOR A TRIANGULAR ELEMENT
DO 20 J = 1,6
DO 20 K = 1,6
20 ELSTIF(ICOL(J),ICOL(K)) = ELMSM(J,K)
DO 25 J = 1,9
DO 25 K = 1,9
25 ELSTIF(ICOL(J+6),ICOL(K+6)) = ELBSM(J,K)
C CALCULATE THE LOCAL GENERALIZED PRESSURE FORCE MATRIX (PFLGN) FOR
C A TRIANGULAR ELEMENT
CALL NPFORC ( I )
C CALCULATE THE COMMON GENERALIZED CENTRIFUGAL FORCE MATRIX (CFLGN)
C FOR A TRIANGULAR ELEMENT
CALL NCFORC (LA, LB, LC, I, NCF)
IF ( IPRINT .GE. 1 ) WRITE (6,24) PFLGN, SYS, CFLGN
24 FORMAT (//20X,39HLOCAL GENERALIZED PRESSURE FORCE MATRIX /9E12.4
1 //20X, 2A4 , 36HGENERALIZED CENTRIFUGAL FORCE MATRIX /9E12.4/
2 9E12.4 )
C CALCULATE THE STIFFNESS MATRIX (ECSTIF), NODAL PRESSURE FORCE
C MATRIX (PFCGN), AND NODAL CENTRIFUGAL FORCE MATRIX (CFCGN) OF A
C TRIANGULAR ELEMENT IN THE COMMON COORDINATE SYSTEM (X,Y,Z) .
CALL COMSTF ( I , NCF )
WRITE (1,1) ECSTIF
IF ( IPRINT .GE. 1 ) WRITE (6,15)
15 FORMAT (1H //25X,55HCOMMON COORDINATE SYSTEM TRIANGULAR STIFFNESS
1 MATRIX )
IF ( IPRINT .GE. 1 ) WRITE (6,26) ((ECSTIF(J,K),K=1,18),J=1,18)
26 FORMAT (//18(10E12.4/8E12.4/))
C ADD VALUES OF PFCGN AND CFCGN WHICH ARE COMMON TO A COMMON NODE .
30 CALL ADDF ( I )
C PRINT GEOMETRIC BREAK-UP AND ASSOCIATED PROPERTIES .
CALL PRINT1
IF ( NSUBS .GT. 0 ) RETURN
C SOLVE FOR THE NODAL DEFLECTIONS (DISPL) IN THE COMMON COORDINATE
C SYSTEM .
35 CALL DEFL ( IPRINT )
IF ( NP .LE. 0 ) GO TO 5
RETURN
END

```

```

MAIN1052
MAIN1053
MAIN1054
MAIN1055
MAIN1056
MAIN1057
MAIN1058
MAIN1059
MAIN1060
MAIN1061
MAIN1062
MAIN1063
MAIN1064
MAIN1065
MAIN1066
MAIN1067
MAIN1068
MAIN1069
MAIN1070
MAIN1071
MAIN1072
MAIN1073
MAIN1074
MAIN1075
MAIN1076
MAIN1077
MAIN1078
MAIN1079
MAIN1080
MAIN1081
MAIN1082
MAIN1083
MAIN1084
MAIN1085
MAIN1086
MAIN1087
MAIN1088
MAIN1089
MAIN1090
MAIN1091
MAIN1092
MAIN1093

```

	SUBROUTINE INPUT ( IPRINT,NGP,NUP,NCHB,LBOUND,NCF,IPUNCH )	INPUT001
C	READ AND PRINT ALL INPUT	INPUT002
C	COMMON X ( 200) , Y ( 200) , Z ( 200) , TH ( 200) ,	INPUT003
1	PRESSE( 200) , XL ( 200,3) , YL ( 200,3) ,	INPUT005
2	RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) ,	INPUT006
3	THHUB ( 100) , THTIP ( 100) , PRESSL(100,15),EDCM ( 3,3) ,	INPUT007
4	RHO , OMEGA , POISSO , YOUNGS , RADGEN ,	INPUT008
5	NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT ,	INPUT009
6	ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,	INPUT010
7	PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) ,	INPUT011
8	PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200) ,	INPUT012
9	FORCE(200,6) , ALEAN(100)	INPUT013
	COMMON / MANE / NSUBS,IPOS(200),NBTS(10,15),NITS(10,15),NBN(10),	INPUT014
1	INTN(10)	INPUT015
	DIMENSION NUP(100) , NCHB(100) , LBOUND(10)	INPUT016
	REAL TITLE (18)	INPUT017
1	WRITE (6,5)	INPUT018
5	FORMAT (1H1/35H0INDUCER STRESS PROGRAM - DECK 6098 //)	INPUT019
	CALL DATE (BMONTH,DAY,YEAR)	INPUT020
	WRITE (6,7) BMONTH,DAY,YEAR	INPUT021
7	FORMAT (6H DATE ,A2,1H/,A2,1H/,A2//)	INPUT022
10	READ (5,15,END=50) NT,TITLE	INPUT023
15	FORMAT (11,18A4)	INPUT024
	WRITE (6,20) TITLE	INPUT025
20	FORMAT (5X,18A4 /)	INPUT026
	IF ( NT .GT. 0 ) GO TO 10	INPUT027
	READ (5,25) RHO,RPM,POISSO,YOUNGS,RADGEN,NCF,NGENLI,LINE1,NGP,	INPUT028
1	NSUBS,IPRINT,LBOUND,IPUNCH,G	INPUT029
25	FORMAT (3F10.0, E10.0,F10.0,6I5/10I5,15X,15,F10.0)	INPUT030
	IF ( G .EQ. 0.0 ) G = 386.4	INPUT031
	WRITE (6,26) NSUBS,NCF,LBOUND,IPUNCH	INPUT032
26	FORMAT (//10X,20HNO. OF SUB-SYSTEMS = 13,7X,27HCENTRIFUGAL FORCE O	INPUT033
	PTION = 12/10X,47HSUB-SYSTEM BOUNDARIES FORMED BY GENERATOR LINES	INPUT034
2	10I5/10X,15HPUNCH OPTION = ,15)	INPUT035
	IF ( LINE1 .GT. 0 ) READ (5,27) (NCHB(I),I=1,LINE1)	INPUT036
27	FORMAT (16I5)	INPUT037
	DO 29 I = 1,100	INPUT038
	IF ( NCHB(I) .GT. 0 ) GO TO 29	INPUT039
	NCHB(I) = NGENLI + 1	INPUT040
29	CONTINUE	INPUT041
	WRITE (6,30)RHO,G,RPM,POISSO,YOUNGS,NGENLI,LINE1,RADGEN,NGP	INPUT042
30	FORMAT(//10X,10HDENSITY = F6.4,5X,4HG = ,E12.4,5X,6HRPM = F10.1,5X	INPUT043
1,18HPOISSON'S RATIO = F5.3,5X,18HYOUNG'S MODULUS = E12.4 //10X,	INPUT044	
2 26HNO. OF GENERATING LINES = 14,5X,40HNO. OF SYMMETRY CHANGES REQ	INPUT045	
3UESTED = 13 //10X,31HGENERATOR LINE OFFSET RADIUS = F9.3 //	INPUT046	
4 10X,15,2X,23HINPUT ELEMENT PRESSURES //)	INPUT047	
	IF ( LINE1 .EQ. 0 ) GO TO 32	INPUT048
	WRITE (6,31) (NCHB(I),I=1,LINE1)	INPUT049
31	FORMAT (10X,38HSYMMETRY CHANGE ABOUT GENERATOR LINES 15I5//)	INPUT050
32	RHO = RHO / G	INPUT051
	OMEGA = RPM * 3.14159265 / 30.0	INPUT052
	KOUNT = 0	INPUT053
	WRITE (6,5)	INPUT054
	DO 45 I = 1,NGENLI	INPUT055
	READ (5,35) RAPANG(I),ZGL(I),RHUB(I),RTIP(I),THHUB(I),THTIP(I),	INPUT056
1	NUP(I),N,ALEAN(I)	INPUT057
35	FORMAT (6F10.0,2I5,F10.0)	

```

NPRES(I) = N
READ (5,37) (PRESSL(I,J),J=1,N)
37 FORMAT (8F10.0)
WRITE (6,39) I
39 FORMAT (30X,22HGENERATOR LINE NUMBER I3,5X,16H(ANGLES IN DEG.) /)
WRITE (6,40) RAPANG(I),ZGL(I),ALEAN(I),RHUB(I),RTIP(I),THHUB(I),
1 THTIP(I),NUP(I),NPRES(I),(PRESSL(I,J),J=1,N)
40 FORMAT ( 5X,13HWRAP ANGLE = F12.6,5X, 7HZHUB = F7.3,5X,12HLE
1AN ANGLE =F12.6, 5X,13HHUB RADIUS = F8.4,5X,13HTIP RADIUS =
2 F8.4/ 5X,16HHUB THICKNESS = F7.4,4X,16HTIP THICKNESS = F7.4,4X,
3 16HNO. OF POINTS = I2,9X,
419HNO. OF PRESSURES = I3/ 40X,10HPRESSURES /10X,10F12.4/10X,5F12.4
5 //)
KOUNT = KOUNT + 1
IF (KOUNT .EQ. 8) WRITE (6,5)
IF (KOUNT .EQ. 8) KOUNT = 0
ALEAN(I) = ALEAN(I) * 0.0174533
45 RAPANG(I) = RAPANG(I) * 0.0174533
GO TO 55
50 STOP
55 RETURN
END

```

INPUT058  
INPUT059  
INPUT060  
INPUT061  
INPUT062  
INPUT063  
INPUT064  
INPUT065  
INPUT066  
INPUT067  
INPUT068  
INPUT069  
INPUT070  
INPUT071  
INPUT072  
INPUT073  
INPUT074  
INPUT075  
INPUT076  
INPUT077  
INPUT078  
INPUT079

```

SUBROUTINE GEOM (NUP,NCHB,LBOUND )
TRIANGULATION OF INDUCER BLADE AND DETERMINATION OF THICKNESS AT
EACH VERTEX AND PRESSURE ON EACH TRIANGLE .
COMMON X ( 200) , Y ( 200) , Z ( 200) , TH ( 200) ,
1 PRESSE( 200) , XL ( 200,3) , YL ( 200,3) ,
2 RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) ,
3 THHUB ( 100) , THTIP ( 100) , PRESSL(100,15),EDCM ( 3,3) ,
4 RHO , OMEGA , POISSO , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT ,
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,
7 PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) ,
8 PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200) ,
9 FORCEI(200,6) , ALEAN(100)
COMMON / MANE / NSUBS , IPOS(200) , NBTS(10,15) , NITS(10,15) , NBN(10) ,
1 INTN(10)
DIMENSION PRESN(200) , NUP(100) , NCHB(100) , LBOUND(10)
ICHB = 1
KOUNT = -1
IPOS(1) = -1
LIP1 = 0
LIP2 = 0
LSUB = 1
NP1 = 1
NT = 0
NP = NUP(1)
NS = NGENLI - 1
DO 90 I = 1,NS
NT1 = NUP(I) + NUP(I+1) - 2
IF ( I .NE. 1 ) GO TO 15
LINE = NUP(I)
DR = 0.0
IF ( LINE .EQ. 1 ) GO TO 1
DR = ( RTIP(I) - RHUB(I) ) / FLOAT( LINE - 1 )
1 RADIUS = RHUB(I) - DR
SINA = SIN( RAPANG(I) )
COSA = COS( RAPANG(I) )
TANL = TAN ( ALEAN(I) )
DRP = ( RTIP(I) - RHUB(I) ) / FLOAT( NPRES(I) - 1 )
LINE = NUP(I)
DO 10 J = 1,LINE
IF ( J .EQ. 1 ) GO TO 2
KOUNT = KOUNT + 1
IPOS(J) = KOUNT
LIP1 = LIP1 + 1
NITS(LSUB,LIP1) = J
2 RADIUS = RADIUS + DR
Z(J) = ZGL(I) + ( RADIUS - RHUB(I) ) * TANL
X(J) = RADGEN * COSA - RADIUS * SINA
Y(J) = RADGEN * SINA + RADIUS * COSA
TH(J) = THHUB(I) + ( THTIP(I) - THHUB(I) ) * ( RADIUS - RHUB(I) )
1 / ( RTIP(I) - RHUB(I) )
IF ( TH(J) .LT. 0.0 ) TH(J) = 0.0
J1 = ( RADIUS - RHUB(I) + 0.0001 ) / DRP
J1 = J1 + 1
IF ( J1 .GT. NPRES(I) ) GO TO 5
PRESN(J) = PRESSL(I,J1) + ( PRESSL(I,J1+1) - PRESSL(I,J1) ) *
1 ( RADIUS - DRP * FLOAT( J1 - 1 ) - RHUB(I) ) / DRP

```

	GO TO 10	GEOM0570
5	PRESN(J) = PRESSL(I,NPRES(I))	GEOM0580
10	CONTINUE	GEOM0590
15	LINE = NUP(I+1)	GEOM0600
	DR = 0.0	GEOM0601
	IF ( LINE .EQ. 1 ) GO TO 16	GEOM0602
	DR = ( RTIP(I+1) - RHUB(I+1) ) / FLOAT( LINE - 1 )	GEOM0610
16	IF ( I+1 .EQ. LBOUND(LSUB) ) LIPI = 0	GEOM0620
	RADIUS = RHUB(I+1) - DR	GEOM0630
	DRP = ( RTIP(I+1) - RHUB(I+1) ) / FLOAT( NPRES(I+1) - 1 )	GEOM0640
	J2 = NP + 1	GEOM0650
	J3 = NP + NUP(I+1)	GEOM0660
	SINA = SIN( RAPANG(I+1) )	GEOM0670
	COSA = COS( RAPANG(I+1) )	GEOM0680
	TANL = TAN( ALEAN(I+1) )	GEOM0690
	IPOS(J2) = -1	GEOM0700
	DO 25 J = J2,J3	GEOM0710
	IF ( J .EQ. J2 ) GO TO 17	GEOM0720
	KOUNT = KOUNT + 1	GEOM0730
	IPOS(J) = KOUNT	GEOM0740
	IF ( NSUBS .EQ. 0 ) GO TO 17	GEOM0750
	IF ( (LSUB .EQ. 1) .AND. (I+1 .LT. LBOUND(1)) ) LIPI = LIPI + 1	GEOM0760
	IF ( (LSUB .EQ. 1) .AND. (I+1 .LT. LBOUND(1)) ) NITS(LSUB,LIPI) = J	GEOM0770
	IF ( LSUB .EQ. NSUBS ) LIPI = LIPI + 1	GEOM0780
	IF ( LSUB .EQ. NSUBS ) NITS(LSUB,LIPI) = J	GEOM0790
	IF ( (LSUB .NE. 1) .AND. (LSUB .NE. NSUBS) .AND. (I+1 .NE. LBOUND(LSUB)) ) LIPI = LIPI + 1	GEOM0800
1	IF ( (LSUB .NE. 1) .AND. (LSUB .NE. NSUBS) .AND. (I+1 .NE. LBOUND(LSUB)) ) NITS(LSUB,LIPI) = J	GEOM0810
	IF ( I+1 .NE. LBOUND(LSUB) ) GO TO 17	GEOM0820
	LIP2 = LIP2 + 1	GEOM0830
	NBTS(LSUB,LIP2) = J	GEOM0840
	III = LIP2	GEOM0850
	IF ( LSUB .NE. 1 ) K = LBOUND(LSUB-1)	GEOM0860
	IF ( LSUB .NE. 1 ) III = III - NUP(K) + 1	GEOM0870
	NBTS(LSUB+1,III) = J	GEOM0880
17	RADIUS = RADIUS + DR	GEOM0890
	Z(J) = ZGL(I+1) + ( RADIUS - RHUB(I+1) ) * TANL	GEOM0900
	X(J) = RADGEN * COSA - RADIUS * SINA	GEOM0910
	Y(J) = RADGEN * SINA + RADIUS * COSA	GEOM0920
	TH(J) = THHUB(I+1) + ( THTIP(I+1) - THHUB(I+1) ) * ( RADIUS - RHUB(I+1) ) / ( RTIP(I+1) - RHUB(I+1) )	GEOM0930
1	J1 = ( RADIUS - RHUB(I+1) + 0.0001 ) / DRP	GEOM0940
	J1 = J1 + 1	GEOM0950
	IF ( TH(J) .LT. 0.0 ) TH(J) = 0.0	GEOM0960
	IF ( J1 .GE. NPRES(I+1) ) GO TO 20	GEOM0970
	PRESN(J) = PRESSL(I+1,J1) + ( PRESSL(I+1,J1+1) - PRESSL(I+1,J1) ) * ( RADIUS - DRP * FLOAT(J1-1) - RHUB(I+1) ) / DRP	GEOM0980
	GO TO 25	GEOM0990
20	PRESN(J) = PRESSL(I+1,NPRES(I+1))	GEOM1000
25	CONTINUE	GEOM1010
	IF ( I+1 .NE. LBOUND(LSUB) ) GO TO 26	GEOM1020
	LSUB = LSUB + 1	GEOM1030
	K = LBOUND(LSUB-1)	GEOM1040
	LIP2 = NUP(K) - 1	GEOM1050
26	J1 = NT + 1	GEOM1060
	J2 = NT + NT1	GEOM1070
	NB = 0	GEOM1080
		GEOM1090
		GEOM1100
		GEOM1110
		GEOM1120

```

K = 0
NB1 = -2
NPT1 = NUP(I)
NPT2 = NUP(I+1)
IF (NPT1 .EQ. NPT2) GO TO 27
IF (NPT2 - NPT1 .EQ. 1) GO TO 275
IF (NPT1 - NPT2 .EQ. 1) GO TO 270
IF (NPT2 - NPT1 .GT. 1) GO TO 265
C BOTTOM GENERATOR HAS AT LEAST TWO MORE NODES THAN THE TOP
C GENERATOR.
DO 264 J = J1,J2
K = K + 1
L = MOD(K,3)
IF (L .EQ. 0) L = 3
GO TO (261, 262, 263), L
261 NB1 = NB1 + 2
NEXT(J,1) = NP1 + NB1
NEXT(J,2) = NP1 + NB1 + 1
NEXT(J,3) = NP + NB1 / 2 + 1
GO TO 264
262 NEXT(J,1) = NEXT(J-1,3)
NEXT(J,2) = NEXT(J,1) + 1
NEXT(J,3) = NEXT(J-1,2)
GO TO 264
263 NEXT(J,1) = NEXT(J-1,3)
NEXT(J,2) = NEXT(J,1) + 1
NEXT(J,3) = NEXT(J-1,2)
264 CONTINUE
GO TO 85
C TOP GENERATOR HAS AT LEAST TWO MORE NODES THAN
C THE BOTTOM GENERATOR.
265 DO 269 J = J1, J2
K = K + 1
L = MOD(K,3)
IF (L .EQ. 0) L = 3
GO TO (266,267,268), L
266 NB1 = NB1 + 2
NEXT(J,1) = NP + NB1 + 1
NEXT(J,2) = NP + NB1 + 2
NEXT(J,3) = NP1 + NB1 / 2
GO TO 269
267 NEXT(J,1) = NEXT(J-1,3)
NEXT(J,2) = NEXT(J,1) + 1
NEXT(J,3) = NEXT(J-1,2)
GO TO 269
268 NEXT(J,1) = NEXT(J-1,3)
NEXT(J,2) = NEXT(J,1) + 1
NEXT(J,3) = NEXT(J-1,2)
269 CONTINUE
GO TO 85
C BOTTOM GENERATOR HAS ONE MORE NODE THAN THE TOP GENERATOR.
270 NEXT(J1,1) = NP1
NEXT(J1,2) = NP1 + 1
NEXT(J1,3) = NP + 1
IF (J1 .EQ. J2) GO TO 85
J11 = J1 + 1
DO 271 J = J11,J2
NEXT(J,1) = NEXT(J-1,3)

```

```

GEOM1130
GEOM1140
GEOM1150
GEOM1160
GEOM1170
GEOM1180
GEOM1190
GEOM1200
GEOM1210
GEOM1220
GEOM1230
GEOM1240
GEOM1250
GEOM1260
GEOM1270
GEOM1280
GEOM1290
GEOM1300
GEOM1310
GEOM1320
GEOM1330
GEOM1340
GEOM1350
GEOM1360
GEOM1370
GEOM1380
GEOM1390
GEOM1400
GEOM1410
GEOM1420
GEOM1430
GEOM1440
GEOM1450
GEOM1460
GEOM1470
GEOM1480
GEOM1490
GEOM1500
GEOM1510
GEOM1520
GEOM1530
GEOM1540
GEOM1550
GEOM1560
GEOM1570
GEOM1580
GEOM1590
GEOM1600
GEOM1610
GEOM1620
GEOM1630
GEOM1640
GEOM1650
GEOM1660
GEOM1670
GEOM1680
GEOM1690
GEOM1700

```

	NEXT(J,2) = NEXT(J,1)+1	GEOM1710
271	NEXT(J,3) = NEXT(J-1,2)	GEOM1720
	GO TO 85	GEOM1730
C	TOP GENERATOR HAS ONE MORE NODE THAN THE BOTTOM GENERATOR.	GEOM1740
275	NEXT(J1,1) = NP + 1	GEOM1750
	NEXT(J1,2) = NP + 2	GEOM1760
	NEXT(J1,3) = NP1	GEOM1770
	IF (J1 .EQ. J2) GO TO 85	GEOM1780
	J11 = J1 + 1	GEOM1790
	DO 276 J = J11, J2	GEOM1800
	NEXT(J,1) = NEXT(J-1,3)	GEOM1810
	NEXT(J,2) = NEXT(J,1)+1	GEOM1820
276	NEXT(J,3) = NEXT(J-1,2)	GEOM1830
	GO TO 85	GEOM1840
C	SAME NUMBER OF NODES ON TOP AND BOTTOM GENERATORS .	GEOM1850
27	IF ( RADGEN .NE. 0.0 ) GO TO 55	GEOM1860
	IF ( NCHB(ICHB) .EQ. 1 ) GO TO 40	GEOM1870
	IF ( ICHB .GE. 2 ) GO TO 42	GEOM1880
28	DO 35 J = J1,J2	GEOM1890
	K = J - J1 + 1	GEOM1900
	IF ( MOD(K,2) .EQ. 0 ) GO TO 30	GEOM1910
	NB = NB + 1	GEOM1920
	NEXT(J,1) = NP + NB	GEOM1930
	NEXT(J,2) = NP + NB + 1	GEOM1940
	NEXT(J,3) = NP1 + NB - 1	GEOM1950
	GO TO 35	GEOM1960
30	NEXT(J,1) = NP1 + NB - 1	GEOM1970
	NEXT(J,2) = NP1 + NB	GEOM1980
	NEXT(J,3) = NP + NB + 1	GEOM1990
35	CONTINUE	GEOM2000
	GO TO 85	GEOM2010
40	ICHB = ICHB + 1	GEOM2020
42	IF ( MOD(ICHB,2) .EQ. 1 ) GO TO 28	GEOM2030
	DO 50 J = J1,J2	GEOM2040
	K = J - J1 + 1	GEOM2050
	IF ( MOD(K,2) .EQ. 0 ) GO TO 45	GEOM2060
	NB = NB + 1	GEOM2070
	NEXT(J,1) = NP1 + NB - 1	GEOM2080
	NEXT(J,2) = NP1 + NB	GEOM2090
	NEXT(J,3) = NP + NB	GEOM2100
	GO TO 50	GEOM2110
45	NEXT(J,1) = NP + NB	GEOM2120
	NEXT(J,2) = NP + NB + 1	GEOM2130
	NEXT(J,3) = NP1 + NB	GEOM2140
50	CONTINUE	GEOM2150
	GO TO 85	GEOM2160
55	IF ( NCHB(ICHB) .EQ. 1 ) GO TO 70	GEOM2170
	IF ( ICHB .GE. 2 ) GO TO 72	GEOM2180
58	DO 65 J = J1,J2	GEOM2190
	K = J - J1 + 1	GEOM2200
	IF ( MOD(K,2) .EQ. 0 ) GO TO 60	GEOM2210
	NB = NB + 1	GEOM2220
	NEXT(J,1) = NP1 + NB - 1	GEOM2230
	NEXT(J,2) = NP1 + NB	GEOM2240
	NEXT(J,3) = NP + NB	GEOM2250
	GO TO 65	GEOM2260
60	NEXT(J,1) = NP + NB	GEOM2270
	NEXT(J,2) = NP + NB + 1	GEOM2280

<pre> 65  NEXT(J,3) = NP1 + NB     CONTINUE     GO TO 85 70  ICHB = ICHB + 1 72  IF ( MOD(ICHB,2) .EQ. 1 ) GO TO 58     DO 80 J = J1,J2       K = J - J1 + 1       IF ( MOD(K,2) .EQ. 0 ) GO TO 75       NB = NB + 1       NEXT(J,1) = NP + NB       NEXT(J,2) = NP + NB + 1       NEXT(J,3) = NP1 + NB - 1       GO TO 80 75  NEXT(J,1) = NP1 + NB - 1       NEXT(J,2) = NP1 + NB       NEXT(J,3) = NP + NB + 1 80  CONTINUE 85  CONTINUE       NP1 = NP + 1       NP = NP + NUP(I+1)       NT = NT + NT1       IF ( NP .LE. 200 ) GO TO 87       WRITE (6,86) 86  FORMAT (//20X,35HMORE THAN 200 POINTS WERE GENERATED ,           RETURN 87  IF ( NT .LE. 200 ) GO TO 90       WRITE (6,88) 88  FORMAT (//20X,37HMORE THAN 200 ELEMENTS WERE GENERATED )           RETURN 90  CONTINUE       DO 95 I = 1,NT         J1 = NEXT(I,1)         J2 = NEXT(I,2)         J3 = NEXT(I,3) 95  PRESSE(I) = ( PRESN(J1) + PRESN(J2) + PRESN(J3) ) / 3.0       IF ( NSUBS .EQ. 0 ) RETURN       I = LBOUND(I)       NBN(I) = NUP(I) - 1       DO 110 I = 1,NSUBS         IF ( I .EQ. 1 ) GO TO 100         J = LBOUND(I-1)         NBN(I) = NUP(J) - 1         IF ( I .EQ. NSUBS ) GO TO 100         J = LBOUND(I)         NBN(I) = NBN(I) + NUP(J) - 1 100  J2 = LBOUND(I) - 1         IF ( I .EQ. NSUBS ) J2 = NGENLI         J1 = 1         IF ( I .GT. 1 ) J1 = LBOUND(I-1) + 1         INTN(I) = 0         DO 110 J = J1,J2 110  INTN(I) = INTN(I) + NUP(J) - 1           RETURN           END </pre>	<pre> GEOM2290 GEOM2300 GEOM2310 GEOM2320 GEOM2330 GEOM2340 GEOM2350 GEOM2360 GEOM2370 GEOM2380 GEOM2390 GEOM2400 GEOM2410 GEOM2420 GEOM2430 GEOM2440 GEOM2450 GEOM2460 GEOM2470 GEOM2480 GEOM2490 GEOM2500 GEOM2510 GEOM2520 GEOM2530 GEOM2540 GEOM2550 GEOM2560 GEOM2570 GEOM2580 GEOM2590 GEOM2600 GEOM2610 GEOM2620 GEOM2630 GEOM2640 GEOM2650 GEOM2660 GEOM2670 GEOM2680 GEOM2690 GEOM2700 GEOM2710 GEOM2720 GEOM2730 GEOM2740 GEOM2750 GEOM2760 GEOM2770 GEOM2780 GEOM2790 GEOM2800 GEOM2810 GEOM2820 </pre>
---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------	--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------



```

SUBROUTINE DIRCOS (LA, LB, LC, I)                                DIRCOS01
C  CALCULATE THE DIRECTION COSINE MATRIX (EDCM) OF ELEMENT LOCAL AXES DIRCOS02
C  (XL, YL, ZL) RELATIVE TO COMMON AXES (X, Y, Z) .            DIRCOS03
C                                                                DIRCOS04
COMMON X      ( 200) , Y      ( 200) , Z      ( 200) , TH      ( 200) , DIRCOS05
1  PRESSE( 200) , XL ( 200,3) , YL ( 200,3) ,                DIRCOS06
2  RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) , DIRCOS07
3  THHUB ( 100) , THTIP ( 100) , PRESSL(100,15), EDCM ( 3,3) , DIRCOS08
4  RHO , OMEGA , POISSO , YOUNGS , RADGEN ,                DIRCOS09
5  NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT   DIRCOS10
DOUBLE PRECISION L12 , S1X , S1Y , S1Z , S1 , S2X , S2Y , S2Z , DIRCOS11
1  S2                                                                DIRCOS12
L12 = SQRT( (X(LB)-X(LA))**2 + (Y(LB)-Y(LA))**2 + (Z(LB)-Z(LA))**2) DIRCOS13
S1X = (Y(LB)-Y(LA)) * (Z(LC)-Z(LA)) - (Y(LC)-Y(LA)) * (Z(LB)-Z(LA)) DIRCOS14
S1Y = (Z(LB)-Z(LA)) * (X(LC)-X(LA)) - (Z(LC)-Z(LA)) * (X(LB)-X(LA)) DIRCOS15
S1Z = (X(LB) - X(LA)) * (Y(LC) - Y(LA)) - (X(LC) - X(LA)) * DIRCOS16
1  (Y(LB) - Y(LA))                                               DIRCOS17
SIGN = 1.0                                                       DIRCOS18
IF ( LC .LT. LB ) SIGN = -1.0                                     DIRCOS19
5  S1X = S1X * SIGN                                               DIRCOS20
S1Y = S1Y * SIGN                                               DIRCOS21
S1Z = S1Z * SIGN                                               DIRCOS22
10 S1 = DSQRT( S1X**2 + S1Y**2 + S1Z**2 )                          DIRCOS23
S2X = S1Y * (Z(LB) - Z(LA)) - S1Z * (Y(LB) - Y(LA))             DIRCOS24
S2Y = S1Z * (X(LB) - X(LA)) - S1X * (Z(LB) - Z(LA))             DIRCOS25
S2Z = S1X * (Y(LB) - Y(LA)) - S1Y * (X(LB) - X(LA))             DIRCOS26
S2 = DSQRT( S2X**2 + S2Y**2 + S2Z**2 )                          DIRCOS27
EDCM(1,1) = (X(LB) - X(LA)) / L12                                 DIRCOS28
EDCM(2,1) = (Y(LB) - Y(LA)) / L12                                 DIRCOS29
EDCM(3,1) = ( Z(LB) - Z(LA) ) / L12                               DIRCOS30
EDCM(1,2) = S2X / S2                                             DIRCOS31
EDCM(2,2) = S2Y / S2                                             DIRCOS32
EDCM(3,2) = S2Z / S2                                             DIRCOS33
EDCM(1,3) = S1X / S1                                             DIRCOS34
EDCM(2,3) = S1Y / S1                                             DIRCOS35
EDCM(3,3) = S1Z / S1                                             DIRCOS36
RETURN                                                            DIRCOS37
END                                                                DIRCOS38

```

```

SUBROUTINE LCOORD (LA, LB, LC, I)                                LCOORD01
C  DETERMINE LOCAL NODAL COORDINATES (XL, YL, ZL) OF TRIANGULAR ELEMENT LCOORD02
C  FROM COMMON NODAL COORDINATES (X, Y, Z) .                  LCOORD03
C                                                                LCOORD04
COMMON X ( 200) , Y ( 200) , Z ( 200) , TH ( 200) , LCOORD05
1  PRESSE( 200) , XL ( 200,3) , YL ( 200,3) , LCOORD06
2  RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) , LCOORD07
3  THHUB ( 100) , THTIP ( 100) , PRESSL(100,15), EDCM ( 3,3) , LCOORD08
4  RHO , OMEGA , POISSD , YOUNGS , RADGEN , LCOORD09
5  NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT LCOORD10
XL(I,2)= EDCM(1,1) * (X(LB) - X(LA)) + EDCM(2,1) * (Y(LB) - Y(LA)) LCOORD11
1  +EDCM(3,1) * (Z(LB) - Z(LA)) LCOORD12
XL(I,3)= EDCM(1,1) * (X(LC) - X(LA)) + EDCM(2,1) * (Y(LC) - Y(LA)) LCOORD13
1  +EDCM(3,1) * (Z(LC) - Z(LA)) LCOORD14
YL(I,3)= EDCM(1,2) * (X(LC) - X(LA)) + EDCM(2,2) * (Y(LC) - Y(LA)) LCOORD15
1  +EDCM(3,2) * (Z(LC) - Z(LA)) LCOORD16
RETURN LCOORD17
END LCOORD18

```

```

SUBROUTINE MEMSTF ( LAA,LBB,LCC,IE )
C
C
C
CALCULATE THE LOCAL MEMBRANE STIFFNESS MATRIX (FLMSM) FOR A
TRIANGULAR ELEMENT .
MEMSTF01
MEMSTF02
MEMSTF03
MEMSTF04
COMMON X ( 200 ) , Y ( 200 ) , Z ( 200 ) , TH ( 200 ) ,MEMSTF05
1 PRESSE( 200 ) , XLL ( 200,3 ) , YLL ( 200,3 ) , MEMSTF06
2 RAPANG( 100 ) , ZGL ( 100 ) , RHUB ( 100 ) , RTIP ( 100 ) ,MEMSTF07
3 THHUB ( 100 ) , THTIP ( 100 ) , PRESSL(100,15),EDCM ( 3,3 ) ,MEMSTF08
4 RHO , OMEGA , PUISSO , YOUNGS , RADGEN , MEMSTF09
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3 ) , NP , NI , MEMSTF10
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) , MEMSTF11
7 PFLGN(9,1) MEMSTF12
COMMON / TBAR / THBAR(200) MEMSTF13
DIMENSION AMNIT(6,6) , WM(3,6) , WMT(6,3) , EM(3,3) , MEMSTF14
1 TN(6,1) , ZINT (1,6) , Z1(6,6) , Z2 (6,6) MEMSTF15
DIMENSION YL(3) , XL(3) MEMSTF16
DOUBLE PRECISION ZINT , XL , YL , TERM , AMNIT , WM , WMT , EM , MEMSTF17
1 TN , Z1 , Z2 MEMSTF18
DATA LA,LB,LC / 1 , 2 , 3 / MEMSTF19
DATA WM / 1.000,4*0.000,1.000,2*0.000,1.000,0.000,1.000,7*0.000 / MEMSTF20
DATA WMT / 1.000,8*0.000,1.000,3*0.000,2*1.000,3*0.000 / MEMSTF21
DATA AMNIT,EM,TN / 51*0.000 / MEMSTF22
XL(LB) = XLL(IE,2) MEMSTF23
XL(LC) = XLL(IE,3) MEMSTF24
YL(LC) = YLL(IE,3) MEMSTF25
TERM = YOUNGS / ( 1.0 - POISSO**2 ) MEMSTF26
EM(1,1) = TERM MEMSTF27
EM(1,2) = TERM * PUISSU MEMSTF28
EM(2,1) = EM(1,2) MEMSTF29
EM(2,2) = TERM MEMSTF30
EM(3,3) = ( 1.0 - POISSO ) * TERM / 2.0 MEMSTF31
AMNIN(1,1) = -1.0 / XL(LB) MEMSTF32
AMNIN(1,3) = - AMNIN(1,1) MEMSTF33
AMNIN(2,2) = AMNIN(1,1) MEMSTF34
AMNIN(2,4) = AMNIN(1,3) MEMSTF35
AMNIN(3,1) = ( XL(LC) - XL(LB) ) / XL(LB) / YL(LC) MEMSTF36
AMNIN(3,3) = - XL(LC) / XL(LB) / YL(LC) MEMSTF37
AMNIN(3,5) = 1.0 / YL(LC) MEMSTF38
AMNIN(4,2) = AMNIN(3,1) MEMSTF39
AMNIN(4,4) = AMNIN(3,3) MEMSTF40
AMNIN(4,6) = AMNIN(3,5) MEMSTF41
AMNIN(5,1) = 1.0 MEMSTF42
AMNIN(6,2) = 1.0 MEMSTF43
DO 10 I = 1,6 MEMSTF44
ZINT(1,1) = 0.0 MEMSTF45
DO 10 J = 1,6 MEMSTF46
10 AMNIT(I,J) = AMNIN(J,1) MEMSTF47
TN(1,1) = TH(LAA) MEMSTF48
TN(3,1) = TH(LBB) MEMSTF49
TN(5,1) = TH(LCC) MEMSTF50
CALL ZINT1 ( IE,ZINT ) MEMSTF51
DO 15 J = 1,6 MEMSTF52
Z1(1,J) = 0.0 MEMSTF53
DO 15 K = 1,6 MEMSTF54
15 Z1(1,J) = Z1(1,J) + ZINT(1,K) * AMNIN(K,J) MEMSTF55
Z2(1,1) = 0.0 MEMSTF56
DO 20 K = 1,6 MEMSTF57
20 Z2(1,1) = Z2(1,1) + Z1(1,K) * TN(K,1) MEMSTF58

```

```

THBAR(IE) = ( TH(LAA) + TH(LBB) + TH(LCC) ) / 3.0
DO 25 I = 1,6
DO 25 J = 1,3
Z1(I,J) = 0.0
DO 25 K = 1,3
25 Z1(I,J) = Z1(I,J) + Z2(I,1) * WMT(I,K) * EM(K,J)
DO 30 I = 1,6
DO 30 J = 1,6
Z2(I,J) = 0.0
DO 30 K = 1,3
30 Z2(I,J) = Z2(I,J) + Z1(I,K) * WM(K,J)
DO 35 I = 1,6
DO 35 J = 1,6
Z1(I,J) = 0.0
DO 35 K = 1,6
35 Z1(I,J) = Z1(I,J) + AMNIT(I,K) * Z2(K,J)
DO 40 I = 1,6
DO 40 J = 1,6
ELMSM(I,J) = 0.0
DO 40 K = 1,6
40 ELMSM(I,J) = ELMSM(I,J) + Z1(I,K) * AMNIN(K,J)
RETURN
END

```

```

MEMSTF59
MEMSTF60
MEMSTF61
MEMSTF62
MEMSTF63
MEMSTF64
MEMSTF65
MEMSTF66
MEMSTF67
MEMSTF68
MEMSTF69
MEMSTF70
MEMSTF71
MEMSTF72
MEMSTF73
MEMSTF74
MEMSTF75
MEMSTF76
MEMSTF77
MEMSTF78
MEMSTF79
MEMSTF80
MEMSTF81

```

```

SUBROUTINE ZINT1 ( IE,ZINT )                                ZINT1001
C USING GAUSSIAN QUADRATURE, INTEGRATE THE FOLLOING FUNCTIONS OVER THE SURFACE OF THE TRIANGLE ZINT1002
C                                                                 ZINT1003
C                                                                 F(XL,YL) = 1.0 ZINT1004
C                                                                 F(XL,YL) = XL ZINT1005
C                                                                 F(XL,YL) = YL ZINT1006
C                                                                 ZINT1007
COMMON X ( 200) , Y ( 200) , Z ( 200) , TH ( 200) , ZINT1008
1 PRESSE( 200) , XLL ( 200,3) , YLL ( 200,3) , ZINT1009
2 RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) , ZINT1010
3 THHUB ( 100) , THIP ( 100) , PRESSL(100,15),EDCM ( 3,3) , ZINT1011
4 RHO , OMEGA , POISSO , YOUNGS , RADGEN , ZINT1012
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT , ZINT1013
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) , ZINT1014
7 PFLGN(9,1) ZINT1015
DIMENSION ZINT(1,6) , A(10) , H(10) , YI(10) , XI(10) , AREA(10) , ZINT1016
1 XIL(10) , XIR(10) ZINT1017
DIMENSION YL(3) , XL(3) ZINT1018
DOUBLE PRECISION YU , HT , XO , ZINT , A , H , YI , XI , AREA , ZINT1019
1 XIL , XIR , XL , YL ZINT1020
DATA LA, LB, LC / 1 , 2 , 3 / ZINT1021
DATA A / -.97390652851717 , -.86506336668899 , -.67940956829902 , ZINT1022
1 -.43339539412925 , -.14887433898163 , .14887433898163 , ZINT1023
2 .43339539412925 , .67940956829902 , .86506336668899 , ZINT1024
3 .97390652851717 / ZINT1025
DATA H / .06667134430869 , .14945134915058 , .21908636251598 , ZINT1026
1 .26926671930100 , .29552422471475 , .29552422471475 , ZINT1027
2 .26926671930100 , .21908636251598 , .14945134915058 , ZINT1028
3 .06667134430869 / ZINT1029
XL(LB) = XLL(IE,2) ZINT1030
XL(LC) = XLL(IE,3) ZINT1031
YL(LC) = YLL(IE,3) ZINT1032
YO = 0.5 * YL(LC) ZINT1033
DO 3 I = 1,10 ZINT1034
YI(I) = YO + A(I) * YO ZINT1035
XIL(I) = XL(LC) * YI(I) / YL(LC) ZINT1036
XIR(I) = XL(LB) - ( XL(LB) - XL(LC) ) * YI(I) / YL(LC) ZINT1037
IF ( I .NE. 1 ) GO TO 2 ZINT1038
HT = 0.0 ZINT1039
DO 1 J = 1,10 ZINT1040
1 HT = HT + H(J) ZINT1041
2 AREA(I)= XL(LB) * ( 1.0 - A(I) ) * 0.25 * HT ZINT1042
ZINT(1,5) = ZINT(1,5) +DABS(YL(LC)) * 0.5 * AREA(I) * H(I) ZINT1043
3 ZINT(1,3) = ZINT(1,3) +DABS(YL(LC)) * 0.5 *YI(I) * AREA(I) * H(I) ZINT1044
DO 5 I = 1,10 ZINT1045
XO = XIL(I) + 0.5 * ( XIR(I) - XIL(I) ) ZINT1046
AREA(I)= 0.0 ZINT1047
DO 4 J = 1,10 ZINT1048
XI(J) = XO + A(J) * ( XO - XIL(I) ) ZINT1049
4 AREA(I)= AREA(I) + XL(LB) * ( 1.0 - A(I) ) * 0.25 * H(J) * XI(J) ZINT1050
5 ZINT(1,1) = ZINT(1,1) +DABS(YL(LC)) * 0.5 * AREA(I) * H(I) ZINT1051
RETURN ZINT1052
END ZINT1053

```

```

SUBROUTINE BENSTF ( LAA,LBB,LCC,IE )
CALCULATE THE ELEMENTAL LOCAL BENDING STIFFNESS MATRIX (ELBSM) .
COMMON X ( 200 ) , Y ( 200 ) , Z ( 200 ) , TH ( 200 ) ,
1 PRESSE( 200 ) , XLL ( 200,3 ) , YLL ( 200,3 ) ,
2 RAPANG( 100 ) , ZGL ( 100 ) , RHUB ( 100 ) , RTIP ( 100 ) ,
3 THHUB ( 100 ) , THTIP ( 100 ) , PRESSL(100,15),EDCM ( 3,3 ) ,
4 RHO , OMEGA , POISSD , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3 ) , NP , NT ,
6 ELM5M(6,6) , AMNIN(6,6) , ELRSM(9,9) , ABNIN(9,9) ,
7 PFLGN(9,1)
DIMENSION ABNIT(9,9) , Z1(9,9) , ZINT(9,9)
DIMENSION YL(3) , XL(3)
DOUBLE PRECISION ZJ1 , ZJ2 , ZJ3 , ZJ4 , ZJ5 , ZJ6 , ABNIT , Z1 ,
1 ZINT , XL , YL
DATA LA, LB, LC / 1 , 2 , 3 /
XL(LB) = XLL(IE,2)
XL(LC) = XLL(IE,3)
YL(LC) = YLL(IE,3)
ABNIN(1,1) = 1.0
ABNIN(2,3) = -1.0
ABNIN(3,2) = 1.0
ABNIN(4,1) = -3.0 / XL(LB) / XL(LB)
ABNIN(4,3) = 2.0 / XL(LB)
ABNIN(4,4) = - ABNIN(4,1)
ABNIN(4,6) = 1.0 / XL(LB)
ABNIN(5,1) = 3.0 * ( XL(LC)**2 - XL(LB)**2 ) / ( XL(LB)*YL(LC) )**2
ABNIN(5,2) = -2.0 / YL(LC)
ABNIN(5,3) = 2.0 * ( XL(LB) - XL(LC) ) * XL(LC) / XL(LB) / YL(LC)
1 / YL(LC)
ABNIN(5,4) = -3.0 * ( XL(LC) / XL(LB) / YL(LC) )**2
ABNIN(5,6) = - ( XL(LC) / YL(LC) )**2 / XL(LB)
ABNIN(5,7) = 3.0 / YL(LC) / YL(LC)
ABNIN(5,8) = - 1.0 / YL(LC)
ABNIN(5,9) = XL(LC) / YL(LC) / YL(LC)
ABNIN(6,1) = 2.0 / XL(LB)**3
ABNIN(6,3) = - 1.0 / XL(LB) / XL(LB)
ABNIN(6,4) = - ABNIN(6,1)
ABNIN(6,6) = ABNIN(6,3)
ABNIN(7,2) = ABNIN(6,3)
ABNIN(7,5) = - ABNIN(6,3)
ABNIN(8,1) = 6.0 * XL(LC) / XL(LB)**3 / YL(LC)**2 * ( XL(LB) - XL(LC) )
ABNIN(8,2) = 2.0 * XL(LC) / XL(LB) / XL(LB) / YL(LC)
ABNIN(8,3) = ( XL(LB) - 3.0*XL(LC) ) * ( XL(LB) - XL(LC) ) /
1 ( XL(LB) * YL(LC) )**2
ABNIN(8,4) = 6.0 * XL(LC) * ( XL(LC) - XL(LB) ) / XL(LB)**3 /
1 YL(LC)**2
ABNIN(8,5) = -2.0 * XL(LC) / XL(LB) / XL(LB) / YL(LC)
ABNIN(8,6) = XL(LC) * ( 3.0*XL(LC) - 2.0*XL(LB) ) / ( XL(LB) *
1 YL(LC) )**2
ABNIN(8,9) = -1.0 / YL(LC) / YL(LC)
ABNIN(9,1) = 2.0 * ( 2.0*XL(LC)**3 - XL(LB)*( 3.0*XL(LC)**2 -
1 XL(LB)**2 ) ) / ( XL(LB) * YL(LC) )**3
ABNIN(9,2) = ( XL(LB)**2 - XL(LC)**2 ) / ( XL(LB) * YL(LC) )**2
ABNIN(9,3) = -2.0 * XL(LC) * ( XL(LB) - XL(LC) )**2 / XL(LB)**2 /
1 YL(LC)**3
ABNIN(9,4) = 2.0 * XL(LC)**2 * ( 3.0*XL(LB) - 2.0*XL(LC) ) /
1 ( XL(LB) * YL(LC) )**3

```

```

ABNIN(9,5) = ( XL(LC) / XL(LB) / YL(LC) )**2
ABNIN(9,6) = 2.0 * XL(LC)**2 * ( XL(LB) - XL(LC) ) / XL(LB)**2 /
1      YL(LC)**3
ABNIN(9,7) = -2.0 / YL(LC)**3
ABNIN(9,8) = 1.0 / YL(LC)**2
DO 5 I = 1,9
DO 5 J = 1,9
ZINT(I,J) = 0.0
5 ABNIT(I,J) = ABNIN(J,I)
CALL ZINT2 ( LAA,LBB,LCC,ZJ1,ZJ2,ZJ3,ZJ4,ZJ5,ZJ6,IE )
ZINT(4,4) = 4.0 * ZJ1
ZINT(4,5) = POISSO * ZINT(4,4)
ZINT(4,6) = 12.0 * ZJ2
ZINT(4,7) = 4.0 * ZJ3
ZINT(4,8) = 4.0 * POISSO * ZJ2
ZINT(4,9) = POISSO * ZINT(4,7) * 3.0
ZINT(5,5) = ZINT(4,4)
ZINT(5,6) = POISSO * ZINT(4,6)
ZINT(5,7) = POISSO * ZINT(4,7)
ZINT(5,8) = ZINT(4,8) / POISSO
ZINT(5,9) = ZINT(4,9) / POISSO
ZINT(6,6) = 36.0 * ZJ4
ZINT(6,7) = 12.0 * ZJ5
ZINT(6,8) = 12.0 * POISSO * ZJ4
ZINT(6,9) = ZINT(6,7) * POISSO * 3.0
ZINT(7,7) = 4.0 * ZJ6 + 8.0 * ( 1.0 - POISSO ) * ZJ4
ZINT(7,8) = 4.0 * ( 2.0 - POISSO ) * ZJ5
ZINT(7,9) = 12.0 * POISSO * ZJ6
ZINT(8,8) = 8.0 * ( 1.0 - POISSO ) * ZJ6 + 4.0 * ZJ4
ZINT(8,9) = 12.0 * ZJ5
ZINT(9,9) = 36.0 * ZJ6
DO 10 I = 4,8
I1 = I + 1
DO 10 J = I1,9
10 ZINT(J,I) = ZINT(I,J)
ZJ1 = YOUNGS / ( 12.0 * ( 1.0 - POISSO**2 ) )
DO 15 I = 4,9
DO 15 J = 4,9
15 ZINT(I,J) = ZINT(I,J) * ZJ1
DO 20 I = 1,9
DO 20 J = 1,9
Z1(I,J) = 0.0
DO 20 K = 1,9
20 Z1(I,J) = Z1(I,J) + ABNIT(I,K) * ZINT(K,J)
DO 25 I = 1,9
DO 25 J = 1,9
ELBSM(I,J) = 0.0
DO 25 K = 1,9
25 ELBSM(I,J) = ELBSM(I,J) + Z1(I,K) * ABNIN(K,J)
RETURN
END
BENS0590
BENS0600
BENS0610
BENS0620
BENS0630
BENS0640
BENS0650
BENS0660
BENS0670
BENS0680
BENS0690
BENS0700
BENS0710
BENS0720
BENS0730
BENS0740
BENS0750
BENS0760
BENS0770
BENS0780
BENS0790
BENS0800
BENS0810
BENS0820
BENS0830
BENS0840
BENS0850
BENS0860
BENS0870
BENS0880
BENS0890
BENS0900
BENS0910
BENS0920
BENS0930
BENS0940
BENS0950
BENS0960
BENS0970
BENS0980
BENS0990
BENS1000
BENS1010
BENS1020
BENS1030
BENS1040
BENS1050
BENS1060
BENS1070
BENS1080
BENS1090

```

```

SUBROUTINE ZINT2 ( LAA,LBB,LCC,ZJ1,ZJ2,ZJ3,ZJ4,ZJ5,ZJ6,IE )      ZINT2010
C USING GAUSSIAN QUADRATURE, INTEGRATE THE FOLLOWING FUNCTIONS OVER ZINT2020
C THE SURFACE OF THE TRIANGLEF                                     ZINT2030
C      F(XL,YL) = TERM ** 3                                       ZINT2040
C      F(XL,YL) = TERM ** 3 * XL                                   ZINT2050
C      F(XL,YL) = TERM ** 3 * YL                                   ZINT2060
C      F(XL,YL) = TERM ** 3 * XL ** 2                             ZINT2070
C      F(XL,YL) = TERM ** 3 * XL * YL                             ZINT2080
C      F(XL,YL) = TERM ** 3 * YL ** 2                             ZINT2090
C WHERE
C      TERM = ((XL(LB)*YL(LC) + (XL(LC) - XL(LB))*YL - YL(LC)*XL)* ZINT2110
C      TH(LAA)+ (YL(LC)*XL - XL(LC)*YI)*TH(LBB)+ XL(LB)*      ZINT2120
C      TH(LCC)*XL)/XL(LB)/YL(LC)                                   ZINT2130
C                                                                    ZINT2140
COMMON X ( 200 ) , Y ( 200 ) , Z ( 200 ) , IH ( 200 ) , ZINT2150
1 PRESSE( 200 ) , XLL ( 200,3 ) , YLL ( 200,3 ) , ZINT2160
2 RAPANG( 100 ) , ZGL ( 100 ) , RHUB ( 100 ) , RTIP ( 100 ) , ZINT2170
3 THHUB ( 100 ) , THTIP ( 100 ) , PRESSL(100,15),EDCM ( 3,3 ) , ZINT2180
4 RHO , OMEGA , PUISSO , YOUNGS , RADGEN , ZINT2190
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3 ) , NP , NT , ZINT2200
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) , ZINT2210
7 PFLGN(9,1) ZINT2220
DIMENSION A(10) , H(10) , YI(10) , XI(10) , AREA(10,6) , XIL(10) , ZINT2230
1 XIR(10) ZINT2240
DIMENSION YL(3) , XL(3) ZINT2250
DOUBLE PRECISION ZJ1 , ZJ2 , ZJ3 , ZJ4 , ZJ5 , ZJ6 , Y0 , X0 , ZINT2260
1 TERM , A , H , XI , YI , AREA , XIL , XIR , XL , ZINT2270
2 YL ZINT2280
DATA LA,LB,LC / 1 , 2 , 3 / ZINT2290
DATA A / -.97390652851717 , -.86506336668899 , -.67940956829902 , ZINT2300
1 -.43339539412925 , -.14887433898163 , .14887433898163 , ZINT2310
2 .43339539412925 , .67940956829902 , .86506336668899 , ZINT2320
3 .97390652851717 / ZINT2330
DATA H / .06667134430869 , .14945134915058 , .21908636251598 , ZINT2340
1 .26926671930100 , .29552422471475 , .29552422471475 , ZINT2350
2 .26926671930100 , .21908636251598 , .14945134915058 , ZINT2360
3 .06667134430869 / ZINT2370
XL(LB) = XLL(IE,2) ZINT2380
XL(LC) = XLL(IE,3) ZINT2390
YL(LC) = YLL(IE,3) ZINT2400
ZJ1 = 0.0 ZINT2410
ZJ2 = 0.0 ZINT2420
ZJ3 = 0.0 ZINT2430
ZJ4 = 0.0 ZINT2440
ZJ5 = 0.0 ZINT2450
ZJ6 = 0.0 ZINT2460
Y0 = 0.5 * YL(LC) ZINT2470
DO 4 I = 1,10 ZINT2480
YI(I) = Y0 + A(I) * Y0 ZINT2490
XIL(I) = XL(LC) * YI(I) / YL(LC) ZINT2500
XIR(I) = XL(LB) - ( XL(LB) - XL(LC) ) * YI(I) / YL(LC) ZINT2510
X0 = XIL(I) + 0.5 * ( XIR(I) - XIL(I) ) ZINT2520
DO 2 J = 1,10 ZINT2530
DO 1 K = 1,6 ZINT2540
1 ARFA(J,K) = 0.0 ZINT2550
2 XI(J) = X0 + A(J) * ( X0 - XIL(I) ) ZINT2560
DO 3 J = 1,10 ZINT2570
TERM = ( ( XL(LB)*YL(LC) + ( XL(LC) - XL(LB) ) * YI(I) - YL(LC)* ZINT2580

```



```

1      XI(J) ) * TH(LAA) - ( XL(LC)*YI(I) - YL(LC)*XI(J) ) * TH(LBB) ZINT2590
2      + XL(LB)*TH(LCC)*YI(I)**3 * XL(LB)*( 1.0 - A(I) ) * 0.25 ZINT2600
3      * H(J) / XL(LB)**3 / YL(LC)**3 ZINT2610
AREA(I,1) = AREA(I,1) + TERM ZINT2620
AREA(I,2) = AREA(I,2) + TERM * XI(J) ZINT2630
AREA(I,3) = AREA(I,3) + TERM * YI(I) ZINT2640
AREA(I,4) = AREA(I,4) + TERM * XI(J)**2 ZINT2650
AREA(I,5) = AREA(I,5) + TERM * XI(J) * YI(I) ZINT2660
3 AREA(I,6) = AREA(I,6) + TERM * YI(I)**2 ZINT2670
ZJ1 = ZJ + 0.5 * H(I) * AREA(I,1)*DABS(YL(LC)) ZINT2680
ZJ2 = ZJ2 + 0.5 * H(I) * AREA(I,2)*DABS(YL(LC)) ZINT2690
ZJ3 = ZJ3 + 0.5 * H(I) * AREA(I,3)*DABS(YL(LC)) ZINT2700
ZJ4 = ZJ4 + 0.5 * H(I) * AREA(I,4) *DABS(YL(LC)) ZINT2710
ZJ5 = ZJ5 + 0.5 * H(I) * AREA(I,5) *DABS(YL(LC)) ZINT2720
4 ZJ6 = ZJ6 + 0.5 * H(I) * AREA(I,6) *DABS(YL(LC)) ZINT2730
RETURN ZINT2740
END ZINT2750

```

```

SUBROUTINE NPFORC ( I )
C   CALCULATE THE LOCAL GENERALIZED NODAL PRESSURE FORCE (PFLGN) FOR
C   A TRIANGULAR ELEMENT .
C
COMMON X      ( 200) , Y      ( 200) , Z      ( 200) , TH      ( 200) ,
1  PRESSE( 200) , XLL ( 200,3) , YLL ( 200,3) ,
2  RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) ,
3  THHUB ( 100) , THTIP ( 100) , PRESSL(100,15),EDCM ( 3,3) ,
4  RHO , OMEGA , POISSO , YOUNGS , RADGEN ,
5  NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT ,
6  ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,
7  PFLGN(9,1)
DIMENSION ABNIT(9,9) , ZINT(9,1)
DOUBLE PRECISION ABNIT , ZINT
DO 10 J = 1,9
ZINT(J,1) = 0.0
DO 10 K = 1,9
10 ABNIT(J,K) = ABNIN(K,J)
CALL ZINT3 ( I,ZINT )
DO 15 J = 1,9
PFLGN(J,1) = 0.0
DO 15 K = 1,9
15 PFLGN(J,1) = PFLGN(J,1) + PRESSE(I) * ABNIT(J,K) * ZINT(K,1)
RETURN
END

```

```

NPFOR010
NPFOR020
NPFOR030
NPFOR040
NPFOR050
NPFOR060
NPFOR070
NPFOR080
NPFOR090
NPFOR100
NPFOR120
NPFOR130
NPFOR140
NPFOR150
NPFOR160
NPFOR170
NPFOR180
NPFOR190
NPFOR200
NPFOR210
NPFOR220
NPFOR230
NPFOR240
NPFOR250
NPFOR260

```

```

SUBROUTINE ZINT3 ( IE,ZINT )
C USING GAUSSIAN QUADRATURE, INTEGRATE THE FOLLOWING FUNCTIONS OVER THE SURFACE OF THE TRIANGLE
C
C F(XL,YL) = 1.0
C F(XL,YL) = XL
C F(XL,YL) = YL
C F(XL,YL) = XL**2
C F(XL,YL) = YL**2
C F(XL,YL) = XL**3
C F(XL,YL) = XL**2 * YL
C F(XL,YL) = YL**2 * XL
C F(XL,YL) = YL**3
C
COMMON X ( 200 ) , Y ( 200 ) , Z ( 200 ) , TH ( 200 ) ,
1 PRESSE( 200 ) , XLL ( 200,3 ) , YLL ( 200,3 ) ,
2 RAPANG( 100 ) , ZGL ( 100 ) , RHUB ( 100 ) , RTIP ( 100 ) ,
3 THHUB ( 100 ) , TH TIP ( 100 ) , PRESSL(100,15),EDCM ( 3,3 ) ,
4 RHO , OMEGA , POISSO , YOUNGS , RADGEN ,
5 VGENLI , LINE1 , NPRES(100) , NEXT ( 200,3 ) , NP , NT ,
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,
7 PFLGN(9,1)
DIMENSION ZINT(9,1) , A(10) , H(10) , YI(10) , XI(10) , AREA(10,9)
1 ,XIL(10) , XIR(10) , XL(3) , YL(3)
DOUBLE PRECISION YI,XI , AREA , XIL , XIR , XL , YL , XO , YO ,
1 TERM , ZINT , A , H
DATA LA, LB, LC / 1 , 2 , 3 /
DATA A / -.97390652851717 , -.86506336668899 , -.67940956829902 ,
1 -.43339539412925 , -.14887433898163 , .14887433898163 ,
2 .43339539412925 , .67940956829902 , .86506336668899 ,
3 .97390652851717 /
DATA H / .06667134430869 , .14945134915058 , .21908636251598 ,
1 .26926671930100 , .29552422471475 , .29552422471475 ,
2 .26926671930100 , .21908636251598 , .14945134915058 ,
3 .06667134430869 /
XL(LB) = XLL(IE,2)
XL(LC) = XLL(IE,3)
YL(LC) = YLL(IE,3)
YO = 0.5 * YL(LC)
DO 5 I = 1,10
YI(I) = YO + A(I) * YO
XIL(I) = XL(LC) * YI(I) / YL(LC)
XIR(I) = XL(LB) - ( XL(LB) - XL(LC) ) * YI(I) / YL(LC)
XO = XIL(I) + 0.5 * ( XIR(I) - XIL(I) )
DO 2 J = 1,10
DO 1 K = 1,9
1 AREA(J,K) = 0.0
2 XI(J) = XO + A(J) * ( XO - XIL(I) )
DO 3 J = 1,10
TFRM = XL(LB) * ( 1.0 - A(I) ) * 0.25 * H(J)
AREA(I,1) = AREA(I,1) + TFRM
AREA(I,2) = AREA(I,2) + TFRM * XI(J)
AREA(I,3) = AREA(I,3) + TFRM * YI(I)
AREA(I,4) = AREA(I,4) + TFRM * XI(J)**2
AREA(I,5) = AREA(I,5) + TFRM * YI(I)**2
AREA(I,6) = AREA(I,6) + TFRM * XI(J)**3
AREA(I,7) = AREA(I,7) + TFRM * XI(J)**2 * YI(I)
AREA(I,8) = AREA(I,8) + TFRM * XI(J) * YI(I)**2
3 AREA(I,9) = AREA(I,9) + TFRM * YI(I)**3

```

```
TERM = DABS( YL(LC) ) * 0.5 * H(I)
DO 4 J = 1,9
4 ZINT(J,1) = ZINT(J,1) + TERM * AREA(I,J)
5 CONTINUE
RETURN
END
```

```
ZINT3590
ZINT3600
ZINT3610
ZINT3620
ZINT3630
ZINT3640
```

```

SUBROUTINE NCFURC ( LAA,LBB,LCC,IE,NCF )
C      CALCULATE THE COMMON GENERALIZED CENTRIFUGAL FORCE MATRIX (CFLGN)
C      FOR A TRIANGULAR ELEMENT .
C
COMMON X      ( 200 ) , Y      ( 200 ) , Z      ( 200 ) , TH      ( 200 ) ,
1  PRESSE( 200 ) , XLL ( 200,3 ) , YLL ( 200,3 ) ,
2  RAPANG( 100 ) , ZGL      ( 100 ) , RHUB      ( 100 ) , RTIP      ( 100 ) ,
3  THHUB ( 100 ) , THHUB ( 100 ) , PRESSL(100,15),EDCM ( 3,3 ) ,
4  RHO , UMEGA , POISSO , YOUNGS , RADGEN ,
5  NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3 ) , NP , NT ,
6  ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,
7  PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) ,
8  PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200) ,
9  FORCE(200,6)
DIMENSION A(10) , H(10) , YI(10) , XI(10) , AREA(10,15) , XIL(10) ,
1  XIR(10) , TERM(9) , XL(3) , YL(3)
DOUBLE PRECISION AREE , TERN , YU , XO , TERMO , TERM1 , TERM2 ,
1  TERM3 , TERM4 , TERM5 , A , H , YI , XI ,
2  AREA , XIL , XIR , TERM , XL , YL
DATA A / -.97390652851717 , -.86506336668899 , -.67940956829902 ,
1  -.43339539412925 , -.14887433898163 , .14887433898163 ,
2  .43339539412925 , .67940956829902 , .86506336668899 ,
3  .97390652851717 /
DATA H / .06667134430869 , .14945134915058 , .21908636251598 ,
1  .26926671930100 , .29552422471475 , .29552422471475 ,
2  .26926671930100 , .21908636251598 , .14945134915058 ,
3  .06667134430869 /
DATA LA,LB,LC / 1 , 2 , 3 /
IF ( NCF .GT. 0 ) GO TO 9
DO 8 J = 1,18
8  CFLGN(J,1) = 0.0
AREE = 0.5 * ABS( XLL(IE,2) * YLL(IE,3) )
TERN = RHO * UMEGA**2 * AREE / 3.0
CFLGN(1,1) = X(LAA)* TH(LAA)* TERN
CFLGN(2,1) = Y(LAA)* TH(LAA)* TERN
CFLGN(7,1) = X(LBB)* TH(LBB)* TERN
CFLGN(8,1) = Y(LBB)* TH(LBB)* TERN
CFLGN(13,1) = X(LCC)* TH(LCC)* TERN
CFLGN(14,1) = Y(LCC)* TH(LCC)* TERN
RETURN
9  XL(LB) = XLL(IE,2)
XL(LC) = XLL(IE,3)
YL(LC) = YLL(IE,3)
DO 10 I = 1,18
10 CFLGN(I,1) = 0.0
YU = 0.50 * YL(LC)
DO 6 I = 1,10
YI(I) = YU + A(I) * YU
XIL(I) = XL(LC) * YI(I) / YL(LC)
XIR(I) = XL(LB) - (XL(LB) - XL(LC) ) * YI(I) / YL(LC)
XO = XIL(I) + 0.5 * ( XIR(I) - XIL(I) )
DO 2 J = 1,10
DO 1 K = 1,15
1  AREA(J,K) = 0.0
2  XI(J) = XO + A(J) * (XO - XIL(I))
DO 4 J = 1,10
TERMO = XL(LB)*(1.0 - A(I))*0.25*H(J)*((XL(LB)*YL(LC) + (XL(LC) -
1  XL(LB))*YI(I) - YL(LC)*XI(J))*TH(LAA) - (XL(LC)*YI(I) -

```

```

2      YL(LC)*XI(J))*TH(LBB) + XL(LB)*TH(LCC)*YI(I)          NCF00590
3      / XL(LB) / YL(LC)                                     NCF00595
TFRM1 = (EDCM(1,1)*(EDCM(1,1) + EDCM(2,1)**2)NCF00600
1*X I(J)+ (EDCM(1,1)*EDCM(1,2) + EDCM(2,1)*( EDCM(2,2)))*YI(I) NCF00610
2      + X(LAA) * EDCM(1,1) + Y(LAA) * EDCM(2,1)          NCF00620
TERM2 = (EDCM(1,2)*( EDCM(1,1) + EDCM(2,2)*EDCM(2,1))*X I(J) NCF00630
1      + (EDCM(1,2)**2 + EDCM(2,2)*( EDCM(2,2)))*YI(I)   NCF00640
2      + X(LAA) * EDCM(1,2) + Y(LAA) * EDCM(2,2)          NCF00650
TERM3=(EDCM(1,3)*(EDCM(1,1) +EDCM(2,3)*EDCM(2,NCF00660
11))*X I(J)+(EDCM(1,3)*EDCM(1,2) + EDCM(2,3)*( EDCM(2,2)))*YI(I)NCF00670
2      + X(LAA) * EDCM(1,3) + Y(LAA) * EDCM(2,3)          NCF00680
TERM4 = 1.0 - X I(J)/XL(LB) + (XL(LC) - XL(LB))/XL(LB)/YL(LC)*YI(I)NCF00690
TERM5 = X I(J)/XL(LB) - XL(LC)*YI(I)/XL(LB)/YL(LC)          NCF00700
TERM(1) = ABNIN(1,1) + X I(J)**2*ABNIN(4,1) + YI(I)**2*ABNIN(5,1) NCF00710
1      + X I(J)**3*ABNIN(6,1) + X I(J)*YI(I)**2*ABNIN(8,1) + NCF00720
2      YI(I)**3*ABNIN(9,1)                                  NCF00730
TERM(2) = YI(I)*ABNIN(3,2) + YI(I)**2*ABNIN(5,2) + X I(J)**2*YI(I) NCF00740
1      *ABNIN(7,2) + X I(J)*YI(I)**2*ABNIN(8,2) + YI(I)**3* NCF00750
2      ABNIN(9,2)                                           NCF00760
TERM(3) = X I(J)*ABNIN(2,3) + X I(J)**2*ABNIN(4,3) + YI(I)**2* NCF00770
1      ABNIN(5,3) + X I(J)**3*ABNIN(6,3) + X I(J)*YI(I)**2* NCF00780
2      ABNIN(8,3) + YI(I)**3*ABNIN(9,3)                     NCF00790
TERM(4) = X I(J)**2*ABNIN(4,4) + YI(I)**2*ABNIN(5,4) + X I(J)**3 * NCF00800
1      ABNIN(6,4) + X I(J)*YI(I)**2 * ABNIN(8,4) + YI(I)**3 * NCF00810
2      ABNIN(9,4)                                           NCF00820
TERM(5) = X I(J)**2 *YI(I)*ABNIN(7,5) + X I(J)*YI(I)**2 * ABNIN(8,5)NCF00830
1      + YI(I)**3 * ABNIN(9,5)                               NCF00840
TERM(6) = X I(J)**2 * ABNIN(4,6) + YI(I)**2 * ABNIN(5,6) + X I(J)**3NCF00850
1      *ABNIN(6,6) + X I(J)*YI(I)**2 *ABNIN(8,6) + YI(I)**3 * NCF00860
2      ABNIN(9,6)                                           NCF00870
TERM(7) = YI(I)**2 * ABNIN(5,7) + YI(I)**3 * ABNIN(9,7)     NCF00880
TERM(8) = YI(I)**2 * ABNIN(5,8) + YI(I)**3 * ABNIN(9,8)     NCF00890
TERM(9) = YI(I)**2 * ABNIN(5,9) + X I(J)*YI(I)**2 * ABNIN(8,9) NCF00900
AREA(I,1) = AREA(I,1) + TERMO * TERM4 * TERM1                NCF00910
AREA(I,2) = AREA(I,2) + TERMO * TERM4 * TERM2                NCF00920
AREA(I,3) = AREA(I,3) + TERMO * TERMS * TERM1                NCF00930
AREA(I,4) = AREA(I,4) + TERMO * TERMS * TERM2                NCF00940
AREA(I,5) = AREA(I,5) + TERMO / YL(LC) * YI(I) * TERM1       NCF00950
AREA(I,6) = AREA(I,6) + TERMO / YL(LC) * YI(I) * TERM2       NCF00960
DO 3 K = 1,9                                                  NCF00970
3 AREA(I,K+6) = AREA(I,K+6) + TERMO * TERM(K) * TERM3        NCF00980
4 CONTINUE                                                    NCF00990
TERMO = 0.5 * H(I) * RHU * UMEGA**2 *DABS(YL(LC))           NCF01000
DO 5 J = 1,15                                                NCF01010
5 CFLGN(J,1) = CFLGN(J,1) + TERMO * AREA(I,J)                NCF01020
6 CONTINUE                                                    NCF01030
RETURN                                                         NCF01040
END                                                            NCF01050

```

```

SUBROUTINE COMSTF ( IE , NCF )
C CALCULATE THE STIFFNESS MATRIX (ECSTIF), NODAL PRESSURE FORCE
C MATRIX (PFCGN), AND NODAL CENTRIFUGAL FORCE MATRIX (CFCGN) OF A
C TRIANGULAR ELEMENT IN THE COMMON COORDINATE SYSTEM (X,Y,Z) .
C
COMMON X ( 200 ) , Y ( 200 ) , Z ( 200 ) , TH ( 200 ) ,
1 PRESSE( 200 ) , XL ( 200,3 ) , YL ( 200,3 ) ,
2 KAPANG( 100 ) , ZGL ( 100 ) , RHUB ( 100 ) , RTIP ( 100 ) ,
3 THHUB ( 100 ) , THTIP ( 100 ) , PRESSL(100,15),EDCM ( 3,3 ) ,
4 RHO , OMEGA , PUISSO , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3 ) , NP , NT ,
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,
7 PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) ,
8 PFCGN(18,1) , CFCGN(18,1)
DIMENSION R6(18,18) , RESULT(18,18) , EPFLGN(18,1) , IND(18)
DOUBLE PRECISION RESULT , EPFLGN
DATA IND / 1,2,7,8,9,16, 3,4,10,11,12,17, 5,6,13,14,15,18 /
DO 5 I = 1,18
DO 5 J = 1,18
5 R6(I,J) = 0.0
DO 10 I = 1,3
DO 10 J = 1,3
R6(I,J) = EDCM(I,J)
R6(I+3,J+3) = EDCM(I,J)
R6(I+6,J+6) = EDCM(I,J)
R6(I+9,J+9) = EDCM(I,J)
10 R6(I+12,J+12) = EDCM(I,J)
R6(I+15,J+15) = EDCM(I,J)
WRITE (4,'IE) R6,AMNIN,ABNIN
DO 20 I = 1,18
DO 20 J = 1,18
RESULT(I,J) = 0.0
DO 20 K = 1,18
20 RESULT(I,J) = RESULT(I,J) + R6(I,K) * ELSTIF(K,J)
DO 30 I = 1,18
DO 30 J = 1,18
ECSTIF(I,J) = 0.0
DO 30 K = 1,18
30 ECSTIF(I,J) = ECSTIF(I,J) + RESULT(I,K) * R6(J,K)
DO 40 I = 1,18
40 EPFLGN(I,1) = 0.0
DO 50 I = 1,3
EPFLGN(I+2,1) = PFLGN(I,1)
EPFLGN(I+8,1) = PFLGN(I+3,1)
50 EPFLGN(I+14,1) = PFLGN(I+6,1)
DO 60 I = 1,18
PFCGN(I,1) = 0.0
IF ( NCF .EQ. 0 ) GO TO 53
CFCGN(I,1) = CFLGN(IND(I),1)
GO TO 55
53 CFCGN(I,1) = CFLGN(I,1)
55 DO 60 J = 1,18
60 PFCGN(I,1) = PFCGN(I,1) + R6(I,J) * EPFLGN(J,1)
IF ( NCF .EQ. 0 ) GO TO 75
DO 65 I = 1,18
RESULT(I,1) = 0.0
DO 65 J = 1,18
65 RESULT(I,1) = RESULT(I,1) + R6(I,J) * CFCGN(J,1)

DO 70 I = 1,18
70 CFCGN(I,1) = RESULT(I,1)
75 RETURN
END

```

```

SUBROUTINE ACDF ( I )                                ADDF0010
C  ADD VALUES OF COMMON NODAL PRESSURE FORCE (PFCGN) AND COMMON NODAL ADDF0020
C  CENTRIFUGAL FORCE (CFCGN) WHICH ARE COMMON TO A COMMON NODE . ADDF0030
C  ADDF0040
COMMON X      ( 200) , Y      ( 200) , Z      ( 200) , TH      ( 200) , ADDF0050
1  PRESSE( 200) , XL ( 200,3) , YL ( 200,3) ,      ADDF0060
2  RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) , ADDF0070
3  THHUB ( 100) , THTIP ( 100) , PRESSL(100,15),EDCM ( 3,3) , ADDF0080
4  RHO , OMEGA , POISSO , YOUNGS , RADGEN ,      ADDF0090
5  NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT ,      ADDF0100
6  ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ARNIN(9,9) ,      ADDF0110
7  PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) , ADDF0120
8  PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200) , FORCE( ADDF0130
9  200,6)      ADDF0140
20 LA = NEXT(I,1)      ADDF0150
   LB = NEXT(I,2)      ADDF0160
   LC = NEXT(I,3)      ADDF0170
   DO 30 J = 1,6      ADDF0180
   FORCE(LA,J) = FORCE(LA,J) + PFCGN(J ,1) + CFCGN(J ,1)      ADDF0190
   FORCE(LB,J) = FORCE(LB,J) + PFCGN(J+6 ,1) + CFCGN(J+6 ,1)      ADDF0200
30 FORCE(LC,J) = FORCE(LC,J) + PFCGN(J+12,1) + CFCGN(J+12,1)      ADDF0210
   RETURN      ADDF0220
   END      ADDF0230

```



```

SUBROUTINE PRINT1
PRINT GEOMETRIC BREAK-UP AND ASSOCIATED PROPERTIES .
C
COMMON X ( 200) , Y ( 200) , Z ( 200) , TH ( 200) ,
1 PRESSE( 200) , XL ( 200,3) , YL ( 200,3) ,
2 RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) ,
3 THHUB ( 100) , THTIP ( 100) , PRESSL(100,15),EDCM ( 3,3) ,
4 RHO , OMEGA , POISSO , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT
KOUNT = 0
WRITE (6,5)
5 FORMAT (1H1//38X,29HRESULTING TRIANGULAR ELEMENTS ///)
DO 20 I = 1,NT
AREA = ABS( XL(I,2) * YL(I,3) ) / 2.0
PLOAD = AREA * PRESSE(I)
WRITE (6,10) I , AREA , PRESSE(I) , PLOAD
10 FORMAT (45X 'ELEMENT NO. ' I3 / 14X 'AREA =' F10.6,10X 'PRESSURE ='
1 ' E12.5,10X 'LOAD = ' E12.5 / 20X 'NODE NO. ' X Y
2 Z TH XL YL )
LA = NEXT(I,1)
LB = NEXT(I,2)
LC = NEXT(I,3)
WRITE (6,15) LA,X(LA),Y(LA),Z(LA),TH(LA),XL(I,1),YL(I,1),LB,X(LB),
1 Y(LB),Z(LB),TH(LB),XL(I,2),YL(I,2),LC,X(LC),Y(LC),
2 Z(LC),TH(LC),XL(I,3),YL(I,3)
15 FORMAT (17X,5HLA ,I3,5X,3F10.3,3F10.4/ 17X,5HLB ,I3,5X,3F10.3,
1 3F10.4 / 17X,5HLC ,I3,5X,3F10.3,3F10.4// )
KOUNT = KOUNT + 1
IF ((KOUNT .EQ. 7) .AND. (I .NE. NT)) WRITE (6,5)
IF ( KOUNT .EQ. 7 ) KOUNT = 0
20 CONTINUE
RETURN
END
PRINT010
PRINT020
PRINT030
PRINT040
PRINT050
PRINT060
PRINT070
PRINT080
PRINT090
PRINT100
PRINT110
PRINT120
PRINT130
PRINT140
PRINT150
PRINT155
PRINT160
PRINT165
PRINT170
PRINT180
PRINT190
PRINT200
PRINT210
PRINT220
PRINT230
PRINT240
PRINT250
PRINT260
PRINT270
PRINT280
PRINT290
PRINT300
PRINT310

```

```

SUBROUTINE DEFL ( IPRINT )                                DEFLO010
C SOLVE FOR THE NODAL DEFLECTIONS (DISPL) IN THE COMMON COORDINATE DEFLO020
C SYSTEM .                                                DEFLO030
C                                                         DEFLO040
COMMON X ( 200 ) , Y ( 200 ) , Z ( 200 ) , TH ( 200 ) , DEFLO050
1 PRESSE( 200 ) , XL ( 200,3 ) , YL ( 200,3 ) ,          DEFLO060
2 RAPANG( 100 ) , ZGL ( 100 ) , RHUB ( 100 ) , RTIP ( 100 ) , DEFLO070
3 THHUB ( 100 ) , THTIP ( 100 ) , PRESSL(100,15),EDCM ( 3,3 ) , DEFLO080
4 RHO , OMEGA , POISSO , YOUNGS , RADGEN ,              DEFLO090
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3 ) , NP , NT , DEFLO100
6 FLMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,    DEFLO110
7 PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) , DEFLO120
8 PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200) , FORCE( DEFLO130
9 200,6)                                                  DEFLO140
COMMON / MANE / NSUBS, IPOS(200),NBTS(10,15),NITS(10,15),NBN(10), DEFLO150
1 INTN(10)                                               DEFLO160
DIMENSION DISPLA(900) , COEFF(900) , EQUAT(6,900) , COEFR(900) , DEFLO170
1 MEXT(8) , DISPL(18,200)                                DEFLO180
DATA DISPL / 3600*0.0 /                                  DEFLO190
IEQ = 6 * ( NP - NGENLI )                                DEFLO200
II = IEQ + 1                                             DEFLO210
IF ( IPRINT .GT. 1 ) WRITE (6,5) II,IEQ                 DEFLO220
5 FORMAT (1H1//10X,18HFOLLOWING ARE THE ,14,30H COEFFICIENTS FOR EACDEFLO230
1H OF THE ,14,45H SIMULTANEOUS EQUATIONS FOR NODAL DEFLECTIONS //) DEFLO240
KOUNT = 0                                               DEFLO250
DO 90 I = 1, NP                                         DEFLO260
IF ( IPOS(I) .LT. 0 ) GO TO 90                          DEFLO270
KOUNT = KOUNT + 1                                       DEFLO280
IMEXT = IMEX(I)                                         DEFLO290
DO 40 J = 1, IMEXT                                       DEFLO300
40 MEXT(J) = MEX(I,J)                                    DEFLO310
DO 50 J = 1, II                                          DEFLO320
DO 50 K = 1, 6                                           DEFLO330
50 EQUAT(K,J) = 0.0                                       DEFLO340
DO 80 J = 1, IMEXT                                       DEFLO350
K2 = MEXT(J)                                             DEFLO360
FIND (1*K2)                                              DEFLO370
LA = NEXT(K2,1)                                         DEFLO380
LB = NEXT(K2,2)                                         DEFLO390
LC = NEXT(K2,3)                                         DEFLO400
NA = 6 * IPOS(LA)                                       DEFLO410
NB = 6 * IPOS(LB)                                       DEFLO420
NC = 6 * IPOS(LC)                                       DEFLO430
READ (1*K2) ECSTIF                                       DEFLO440
DO 75 K = 1, 6                                           DEFLO450
IF ( LA .EQ. I ) IND1 = K                               DEFLO460
IF ( LB .EQ. I ) IND1 = K + 6                           DEFLO470
IF ( LC .EQ. I ) IND1 = K + 12                          DEFLO480
DO 70 L = 1, 6                                           DEFLO490
KA = NA + L                                             DEFLO500
KB = NB + L                                             DEFLO510
KC = NC + L                                             DEFLO520
IF ( IPOS(LA) .LT. 0 ) GO TO 60                          DEFLO530
EQUAT(K,KA) = EQUAT(K,KA) + ECSTIF(IND1,L)             DEFLO540
60 IF ( IPOS(LB) .LT. 0 ) GO TO 65                       DEFLO550
EQUAT(K,KB) = EQUAT(K,KB) + ECSTIF(IND1,L+6)           DEFLO560
65 IF ( IPOS(LC) .LT. 0 ) GO TO 70                       DEFLO570
EQUAT(K,KC) = EQUAT(K,KC) + ECSTIF(IND1,L+12)         DEFLO580

```

70	CONTINUE	DEFLO590
75	CONTINUE	DEFLO600
80	CONTINUE	DEFLO610
	DO 85 K = 1,6	DEFLO620
	J1 = 6 * ( KOUNT - 1 ) + K	DEFLO630
	EQUAT(K,IEQ+1) = FORCE(I,K)	DEFLO640
	IF ( IPRINT .GT. 1 ) WRITE (6,86) (EQUAT(K,J),J=1,11)	DEFLO650
85	WRITE (3,J1) (EQUAT(K,J),J=1,1201)	DEFLO660
86	FORMAT (10E12.4)	DEFLO670
90	CONTINUE	DEFLO680
	K = 1	DEFLO690
100	READ (3*K) COEFF	DEFLO700
	I = K + 1	DEFLO710
	IF ( ABS( COEFF(K) ) .GT. 1.0E-10 ) GO TO 120	DEFLO720
	DO 105 J = 1,IEQ	DEFLO730
	READ (3*J) COEFR	DEFLO740
	J1 = J	DEFLO750
	IF ( ABS( COEFR(K) ) .GT. 1.0E-10 ) GO TO 115	DEFLO760
105	CONTINUE	DEFLO770
	WRITE (6,110)	DEFLO780
110	FORMAT (32H DISPLACEMENT MATRIX IS SINGULAR )	DEFLO790
	NP = -NP	DEFLO800
	RETURN	DEFLO810
115	WRITE (3*J1) COEFF	DEFLO820
	WRITE (3*K) COEFR	DEFLO830
	DO 117 J = 1,11	DEFLO840
117	COEFF(J) = COEFR(J)	DEFLO850
120	READ (3*I) COEFR	DEFLO860
	ZM = COEFR(K) / COEFF(K)	DEFLO870
	COEFR(K) = 0.0	DEFLO880
	J = K + 1	DEFLO890
130	COEFR(J) = COEFR(J) - ZM * COEFF(J)	DEFLO900
	IF ( J .EQ. IEQ ) GO TO 140	DEFLO910
	J = J + 1	DEFLO920
	GO TO 130	DEFLO930
140	COEFR(J+1) = COEFR(J+1) - ZM * COEFF(J+1)	DEFLO940
	WRITE (3*I) COEFR	DEFLO950
	IF ( I .EQ. IEQ ) GO TO 150	DEFLO960
	I = I + 1	DEFLO970
	GO TO 120	DEFLO980
150	IF ( K .EQ. IEQ - 1 ) GO TO 160	DEFLO990
	K = K + 1	DEFL1000
	GO TO 100	DEFL1010
160	CONTINUE	DEFL1020
	READ (3*IEQ) COEFF	DEFL1030
	DISPLA( IEQ ) = COEFF(IEQ + 1) / COEFF(IEQ)	DEFL1040
	I = IEQ - 1	DEFL1050
210	READ (3*I) COEFF	DEFL1060
	J = I + 1	DEFL1070
	S = 0.0	DEFL1080
220	S = S + COEFF(J) * DISPLA( J	DEFL1090
	IF ( J .EQ. IEQ ) GO TO 230	DEFL1100
	J = J + 1	DEFL1110
	GO TO 220	DEFL1120
230	DISPLA( I ) = (COEFF(IEQ+1) - S) / COEFF(I)	DEFL1130
	IF ( I .EQ. 1 ) GO TO 240	DEFL1140
	I = I - 1	DEFL1150
	GO TO 210	DEFL1160

240	CONTINUE	DEFL1170
	FIND (3*1)	DEFL1180
	DO 260 I = 1,NT	DEFL1190
	LA = NEXT(I,1)	DEFL1200
	LB = NEXT(I,2)	DEFL1210
	LC = NEXT(I,3)	DEFL1220
	NA = 6 * IPOS(LA)	DEFL1230
	NB = 6 * IPOS(LB)	DEFL1240
	NC = 6 * IPOS(LC)	DEFL1250
	DO 250 J = 1,6	DEFL1260
	IF ( IPOS(LA) .LT. 0 ) GO TO 243	DEFL1270
	DISPL(J,I) = DISPLA(NA + J)	DEFL1280
243	IF ( IPOS(LB) .LT. 0 ) GO TO 246	DEFL1290
	DISPL(J+6,I) = DISPLA(NB + J)	DEFL1300
246	IF ( IPOS(LC) .LT. 0 ) GO TO 250	DEFL1310
	DISPL(J+12,I) = DISPLA(NC + J)	DEFL1320
250	CONTINUE	DEFL1330
260	CONTINUE	DEFL1340
	FIND (4*1)	DEFL1350
	WRITE (6,270)	DEFL1360
270	FORMAT (1H1/43X,14HCOMMON SYSTEM /	DEFL1370
	1 40X,20HDEFLECTION PRINTOUT //8X,8HNODE NU.,6X,1HX,	DEFL1380
	1 9X,1HY,9X,1HZ,11X,1HU,14X,1HV,14X,1HW,10X,6HTHE TAX,9X,6HTHE TAY//)	DEFL1390
	J = 0	DEFL1400
	DO 280 I = 1,NP	DEFL1410
	LA = I	DEFL1420
	K = 6 * IPOS(LA)	DEFL1430
	D1 = 0.0	DEFL1440
	D2 = 0.0	DEFL1450
	D3 = 0.0	DEFL1460
	D4 = 0.0	DEFL1470
	D5 = 0.0	DEFL1480
	IF ( IPOS(LA) .LT. 0 ) GO TO 275	DEFL1490
	D1 = DISPLA(K+1)	DEFL1500
	D2 = DISPLA(K+2)	DEFL1510
	D3 = DISPLA(K+3)	DEFL1520
	D4 = DISPLA(K+4)	DEFL1530
	D5 = DISPLA(K+5)	DEFL1540
275	J = J + 1	DEFL1550
	IF ( J .EQ. 50 ) WRITE (6,27C)	DEFL1560
	IF ( J .EQ. 50 ) J = 0	DEFL1570
280	WRITE (6,290) I,X(I),Y(I),Z(I),D1,D2,D3,D4,D5	DEFL1580
290	FORMAT (10X,15,3F10.3,5E15.5)	DEFL1590
	K1 = -49	DEFL1600
	K2 = 0	DEFL1610
	DO 300 I = 1,4	DEFL1620
	K1 = K1 + 50	DEFL1630
	K2 = K2 + 50	DEFL1640
300	WRITE(3*I) ((DISPL(J,K),J=1,18),K=K1,K2)	DEFL1650
	RETURN	DEFL1660
	END	DEFL1670

```

SUBROUTINE ASSEM1
C ASSEMBLE THE KAA AND KAB PORTIONS OF THE COMMON STIFFNESS MATRIX
C FOR EACH SUB-SYSTEM.
C
COMMON X ( 200) , Y ( 200) , Z ( 200) , TH ( 200) ,
1 PRESSE( 200) , XL ( 200,3) , YL ( 200,3) ,
2 RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) ,
3 THHUB ( 100) , THTIP ( 100) , PRESSL(100,15),EDCM ( 3,3) ,
4 RHU , OMEGA , PUISSU , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT ,
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,
7 PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) ,
8 PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200) , FORCE(
9 200,6)
COMMON / MANE / NSUBS,IPDS(200),NBTS(10,15),NITS(10,15),NBN(10),
1 INTN(10)
DIMENSION KAA(90,90) , KAB(90,90) , MEXT(8)
REAL KAA , KAB
KREC = 0
DO 110 I = 1,NSUBS
KAAM = 0
IEQ1 = 6 * NBN(I)
DO 5 J = 1,90
DO 5 K = 1,90
KAA(J,K) = 0.0
5 KAB(J,K) = 0.0
J1 = NBTS(I,1)
J2 = NBTS(I,NBN(I))
DO 90 J = J1, J2
IF (J .NE. NBTS(I,KAAM+1)) GO TO 90
KAAM = KAAM + 1
IMEXT = IMEX(J)
DO 10 K = 1,IMEXT
10 MEXT(K) = MEX(J,K)
DO 85 K = 1,IMEXT
K2 = MEXT(K)
FIND (1*K2)
LA = NEXT(K2,1)
LB = NEXT(K2,2)
LC = NEXT(K2,3)
IF (I .EQ. 1) GO TO 15
IF (I .EQ. NSUBS) GO TO 20
IF ((LA .LT. J1-1) .OR. (LA .GT. J2)) .OR.
1 ((LB .LT. J1-1) .OR. (LB .GT. J2)) .OR.
2 ((LC .LT. J1-1) .OR. (LC .GT. J2)) GO TO 85
GO TO 25
15 IF ((LA .GT. J2) .OR. (LB .GT. J2) .OR. (LC .GT. J2)) GO TO 85
GO TO 25
20 IF ((LA .LT. J1-1) .OR. (LB .LT. J1-1) .OR. (LC .LT. J1-1)) GO TO
1 85
25 L2 = NBN(I)
NA = -1
NB = -1
NC = -1
DO 30 L = 1,L2
IF (LA .EQ. NBTS(I,L)) NA = 6* (L-1)
IF (LB .EQ. NBTS(I,L)) NB = 6* (L-1)
IF (LC .EQ. NBTS(I,L)) NC = 6* (L-1)

```

30	CONTINUE	ASMI0590
	L2 = INTN(I)	ASMI0600
	DO 35 L = 1,L2	ASMI0610
	IF (LA .EQ. NITS(I,L)) NA = 6* (L+NBNI(I)-1)	ASMI0620
	IF (LB .EQ. NITS(I,L)) NB = 6* (L+NBNI(I)-1)	ASMI0630
	IF (LC .EQ. NITS(I,L)) NC = 6* (L+NBNI(I)-1)	ASMI0640
35	CONTINUE	ASMI0650
45	READ (1,K2) ECSTIF	ASMI0660
	DO 80 L = 1,6	ASMI0670
	IF (LA .EQ. J) INDI = L	ASMI0680
	IF (LB .EQ. J) INDI = L + 6	ASMI0690
	IF (LC .EQ. J) INDI = L + 12	ASMI0700
	M1 = 6*(KAAM-1) + L	ASMI0710
	DO 80 M = 1,6	ASMI0720
	KA = NA + M	ASMI0730
	KB = NB + M	ASMI0740
	KC = NC + M	ASMI0750
	IF (NA .LT. 0) GO TO 55	ASMI0760
	IF (NA .GT. 6*(NBNI(I)-1)) GO TO 50	ASMI0770
	KAA(M1,KA) = KAA(M1,KA) + ECSTIF(INDI,M)	ASMI0780
	GO TO 55	ASMI0790
50	KA = M + NA - IEQ1	ASMI0800
	KAB(M1,KA) = KAB(M1,KA) + ECSTIF(INDI,M)	ASMI0810
55	IF (NB .GT. 6*(NBNI(I)-1)) GO TO 60	ASMI0820
	KAA(M1,KB) = KAA(M1,KB) + ECSTIF(INDI,M+6)	ASMI0830
	GO TO 65	ASMI0840
60	KB = M + NB - IEQ1	ASMI0850
	KAB(M1,KB) = KAB(M1,KB) + ECSTIF(INDI,M+6)	ASMI0860
65	IF (NC .LT. 0) GO TO 75	ASMI0870
	IF (NC .GT. 6*(NBNI(I)-1)) GO TO 70	ASMI0880
	KAA(M1,KC) = KAA(M1,KC) + ECSTIF(INDI, M+12)	ASMI0890
	GO TO 75	ASMI0900
70	KC = M + NC - IEQ1	ASMI0910
	KAB(M1,KC) = KAB(M1,KC) + ECSTIF(INDI, M+12)	ASMI0920
75	CONTINUE	ASMI0930
80	CONTINUE	ASMI0940
85	CONTINUE	ASMI0950
90	CONTINUE	ASMI0960
	K1 = -9	ASMI0970
	K2 = 0	ASMI0980
	DO 95 L = 1,9	ASMI0990
	KREC = KREC + 1	ASMI1000
	IF ( K2 .GE. IEQ1 ) GO TO 95	ASMI1010
	K1 = K1 + 10	ASMI1020
	K2 = K2 + 10	ASMI1030
	WRITE (3*KREC) ((KAA(K,J),J=1,90),K=K1,K2)	ASMI1040
95	CONTINUE	ASMI1050
	K1 = -9	ASMI1060
	K2 = 0	ASMI1070
	DO 100 L = 1,9	ASMI1080
	KREC = KREC + 1	ASMI1090
	IF ( K2 .GE. IEQ1 ) GO TO 100	ASMI1100
	K1 = K1 + 10	ASMI1110
	K2 = K2 + 10	ASMI1120
	WRITE (3*KREC) ((KAB(K,J),J=1,90),K=K1,K2)	ASMI1130
100	CONTINUE	ASMI1140
110	CONTINUE	ASMI1150
	RETURN	ASMI1160

END

ASMI1170

	SUBROUTINE ASSEM2	ASM20010
C	ASSEMBLE THE KBA AND KBB-1 PORTIONS OF THE COMMON STIFFNESS	ASM20020
C	MATRIX FOR EACH SUB-SYSTEM.	ASM20030
C		ASM20040
	COMMON X11 ( 200) , Y ( 200) , Z ( 200) , TH ( 200) ,	ASM20050
1	PRESSE( 200) , XL ( 200,3) , YL ( 200,3) ,	ASM20060
2	RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) ,	ASM20070
3	THHUB ( 100) , THTIP ( 100) , PRESSL(100,15),EDCM ( 3,3) ,	ASM20080
4	RHO , UMEGA , POISSU , YOUNGS , RADGEN ,	ASM20090
5	NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT ,	ASM20100
6	ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,	ASM20110
7	PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) ,	ASM20120
8	PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMCX(200) , FORCE(	ASM20130
9	200,6)	ASM20140
	COMMON / MANE / NSUBS, IPUS(200), NBTS(10,15), NITS(10,15), NBN(10),	ASM20150
1	INTN(10)	ASM20160
	DIMENSION KBA(90,90) , KBB(90,90) , MEXT(8)	ASM20170
	REAL KBA, KBB	ASM20180
	KREC = 18 * NSUBS	ASM20190
	DO 135 I = 1, NSUBS	ASM20200
	KBAM = 0	ASM20210
	IEQ1 = 6 * INTN(I)	ASM20220
	IEQ2 = 6 * NBN(I)	ASM20230
	DO 5 J = 1, 90	ASM20240
	DO 5 K = 1, 90	ASM20250
	KBA(J,K) = 0.0	ASM20260
5	KBB(J,K) = 0.0	ASM20270
	J1 = NITS(I,1)	ASM20280
	J2 = NITS(I,INTN(I))	ASM20290
	DO 90 J = J1, J2	ASM20300
	IF (J .NE. NITS(I,KBAM+1)) GO TO 90	ASM20310
	KBAM = KBAM + 1	ASM20320
	IMEXT = IMEX(J)	ASM20330
	DO 15 K = 1, IMEXT	ASM20340
15	MEXT(K) = MEX(J,K)	ASM20350
	DO 85 K = 1, IMEXT	ASM20360
	K2 = MEXT(K)	ASM20370
	FIND (1*K2)	ASM20380
	LA = NEXT(K2,1)	ASM20390
	LB = NEXT(K2,2)	ASM20400
	LC = NEXT(K2,3)	ASM20410
	L2 = NBN(I)	ASM20420
	NA = -1	ASM20430
	NB = -1	ASM20440
	NC = -1	ASM20450
	DO 30 L = 1, L2	ASM20460
	IF (LA .EQ. NBTS(I,L)) NA = 6*(L-1)	ASM20470
	IF (LB .EQ. NBTS(I,L)) NB = 6*(L-1)	ASM20480
	IF (LC .EQ. NBTS(I,L)) NC = 6*(L-1)	ASM20490
30	CONTINUE	ASM20500
	L2 = INTN(I)	ASM20510
	DO 35 L = 1, L2	ASM20520
	IF (LA .EQ. NITS(I,L)) NA = 6* (L + NBN(I)-1)	ASM20530
	IF (LB .EQ. NITS(I,L)) NB = 6* (L + NBN(I)-1)	ASM20540
	IF (LC .EQ. NITS(I,L)) NC = 6* (L + NBN(I)-1)	ASM20550
35	CONTINUE	ASM20560
45	READ (1*K2) ECSTIF	ASM20570
	DO 80 L = 1, 6	ASM20580

IF (LA .EQ. J) IND1 = L	ASM20590
IF (LB .EQ. J) IND1 = L + 6	ASM20600
IF (LC .EQ. J) IND1 = L + 12	ASM20610
M1 = 6 * (KBAM-1) + L	ASM20620
DO 80 M = 1,6	ASM20630
KA = NA + M	ASM20640
KB = NB + M	ASM20650
KC = NC + M	ASM20660
IF (NA .LT. 0) GO TO 55	ASM20670
IF (NA .GT. 6*(NBN(I)-1)) GO TO 50	ASM20680
KBA(M1,KA) = KBA(M1,KA) + ECSTIF(IND1,M)	ASM20690
GO TO 55	ASM20700
50 KA = M + NA - IEQ2	ASM20710
KBB(M1,KA) = KBB(M1,KA) + ECSTIF(IND1,M)	ASM20720
55 IF (NB .GT. 6*(NBN(I)-1)) GO TO 60	ASM20730
KBA(M1,KB) = KBA(M1,KB) + ECSTIF(IND1,M+6)	ASM20740
GO TO 65	ASM20750
60 KB = M + NB - IEQ2	ASM20760
KBB(M1,KB) = KBB(M1,KB) + ECSTIF(IND1,M+6)	ASM20770
65 IF (NC .LT. 0) GO TO 75	ASM20780
IF (NC .GT. 6*(NBN(I)-1)) GO TO 70	ASM20790
KBA(M1,KC) = KBA(M1,KC) + ECSTIF(IND1,M+12)	ASM20800
GO TO 75	ASM20810
70 KC = M + NC - IEQ2	ASM20820
KBB(M1,KC) = KBB(M1,KC) + ECSTIF(IND1,M+12)	ASM20830
75 CONTINUE	ASM20840
80 CONTINUE	ASM20850
85 CONTINUE	ASM20860
90 CONTINUE	ASM20870
K2 = INTN(I) * 6	ASM20880
DO 120 K = 1,K2	ASM20890
IF (KBB(K,K)) 105,95,105	ASM20900
95 WRITE (6,100) I	ASM20910
100 FORMAT (22H KBB OF SUB-SYSTEM NO., I3, 13H IS SINGULAR)	ASM20920
NSUBS = -NSUBS	ASM20930
RETURN	ASM20940
105 X = 1.0 / KBB(K,K)	ASM20950
KBB(K,K) = 1.0	ASM20960
DO 110 J = 1,K2	ASM20970
110 KBB(K,J) = KBB(K,J) * X	ASM20980
IF (K-K2) 115,125,115	ASM20990
115 M = K + 1	ASM21000
DO 120 N = M,K2	ASM21010
X = KBB(N,K)	ASM21020
KBB(N,K) = 0.0	ASM21030
DO 120 J = 1,K2	ASM21040
120 KBB(N,J) = KBB(N,J) - X * KBB(K,J)	ASM21050
125 LL = K2 - 1	ASM21060
DO 130 J = 1,LL	ASM21070
M = J + 1	ASM21080
DO 130 K = M,K2	ASM21090
X = KBB(J,K)	ASM21100
KBB(J,K) = 0.0	ASM21110
DO 130 L = 1,K2	ASM21120
130 KBB(J,L) = KBB(J,L) - KBB(K,L) * X	ASM21130
K1 = -9	ASM21140
K2 = 0	ASM21150
DO 131 L = 1,9	ASM21160



	KREC = KREC + 1	ASM21170
	IF ( K2 .GE. 1EQ1 ) GO TO 131	ASM21180
	K1 = K1 + 10	ASM21190
	K2 = K2 + 10	ASM21200
	WRITE (3*KREC) ((KBA(K,J),J=1,90),K=K1,K2)	ASM21210
131	CONTINUE	ASM21220
	K1 = -9	ASM21230
	K2 = 0	ASM21240
	DO 132 L = 1,9	ASM21250
	KREC = KREC + 1	ASM21260
	IF ( K2 .GE. 1EQ1 ) GO TO 132	ASM21270
	K1 = K1 + 10	ASM21280
	K2 = K2 + 10	ASM21290
	WRITE (3*KREC) ((KBB(K,J),J=1,90),K=K1,K2)	ASM21300
132	CONTINUE	ASM21310
135	CONTINUE	ASM21320
	RETURN	ASM21330
	END	ASM21340

	SUBROUTINE CALC	CALC0010
C	CALCULATE THE SUB-SYSTEM PORTION OF THE SYSTEM STIFFNESS	CALC0020
C	MATRIX AND SYSTEM BOUNDARY FORCE COEFFICIENT MATRIX.	CALC0030
C		CALC0040
	COMMON / MANE / NSUBS,IPUS(200),NBTS(10,15),NITS(10,15),NBN(10),	CALC0050
	1 INTN(10)	CALC0060
	REAL KSS	CALC0070
	DIMENSION B(90,90), KSS(50,90), A(90,90)	CALC0080
	J3 = 36 * NSUBS	CALC0090
	J4 = 45 * NSUBS	CALC0100
	DO 20 I = 1,NSUBS	CALC0110
	IEQ1 = 6 * NBN(I)	CALC0120
	IEQ2 = 6 * INTN(I)	CALC0130
	KA = 18 * I - 9	CALC0140
	K1 = -9	CALC0150
	K2 = 0	CALC0160
	DO 1 L = 1,9	CALC0170
	KA = KA + 1	CALC0180
	IF ( K2 .GE. IEQ1 ) GO TO 1	CALC0190
	K1 = K1 + 10	CALC0200
	K2 = K2 + 10	CALC0210
	READ (3*KA) ((A(K,J),J=1,90),K=K1,K2)	CALC0220
1	CONTINUE	CALC0230
	KB = 18 * (NSUBS + I) - 9	CALC0240
	K1 = -9	CALC0250
	K2 = 0	CALC0260
	DO 2 L = 1,9	CALC0270
	KB = KB + 1	CALC0280
	IF ( K2 .GE. IEQ2 ) GO TO 2	CALC0290
	K1 = K1 + 10	CALC0300
	K2 = K2 + 10	CALC0310
	READ (3*KB) ((B(K,J),J=1,90),K=K1,K2)	CALC0320
2	CONTINUE	CALC0330
	J1 = IEQ1	CALC0340
	J2 = IEQ2	CALC0350
	IF ( J1 .GT. 50 ) J1 = 50	CALC0360
	DO 3 J = 1,J1	CALC0370
	DO 3 K = 1,J2	CALC0380
	KSS(J,K) = 0.0	CALC0390
	DO 3 L = 1,J2	CALC0400
3	KSS(J,K) = KSS(J,K) + A(J,L) * B(L,K)	CALC0410
	K1 = -9	CALC0420
	K2 = 0	CALC0430
	DO 4 L = 1,5	CALC0440
	J3 = J3 + 1	CALC0450
	IF ( K2 .GE. IEQ1 ) GO TO 4	CALC0460
	K1 = K1 + 10	CALC0470
	K2 = K2 + 10	CALC0480
	WRITE (3*J3) ((KSS(K,J),J=1,90),K=K1,K2)	CALC0490
4	CONTINUE	CALC0500
	IF ( IEQ1 .LE. 50 ) J3 = J3 + 4	CALC0510
	IF ( IEQ1 .LE. 50 ) GO TO 7	CALC0520
	J1 = IEQ1 - 50	CALC0530
	DO 5 J = 1,J1	CALC0540
	DO 5 K = 1,J2	CALC0550
	KSS(J,K) = 0.0	CALC0560
	DO 5 L = 1,J2	CALC0570
5	KSS(J,K) = KSS(J,K) + A(J+50,L) * B(L,K)	CALC0580

	K1 = -9	CALC0590
	K2 = 0	CALC0600
	DO 6 L = 1,4	CALC0610
	J3 = J3 + 1	CALC0620
	IF ( K2 .GE. IEQ1-50 ) GO TO 6	CALC0630
	K1 = K1 + 10	CALC0640
	K2 = K2 + 10	CALC0650
	WRITE (3,J3) ((KSS(K,J),J=1,90),K=K1,K2)	CALC0660
6	CONTINUE	CALC0670
7	KB = KB - 18	CALC0680
	K1 = -9	CALC0690
	K2 = 0	CALC0700
	DO 8 L = 1,9	CALC0710
	KB = KB + 1	CALC0720
	IF ( K2 .GE. IEQ2 ) GO TO 8	CALC0730
	K1 = K1 + 10	CALC0740
	K2 = K2 + 10	CALC0750
	READ (3,KB) ((B(K,J),J=1,90),K=K1,K2)	CALC0760
8	CONTINUE	CALC0770
	J11 = IEQ1	CALC0780
	J1 = IEQ1	CALC0790
	IF ( J11 .LE. 50 ) GO TO 11	CALC0800
	J11 = J11 - 50	CALC0810
	DO 9 J = 1,J11	CALC0820
	DO 9 K = 1,J1	CALC0830
	A(J+50,K) = 0.0	CALC0840
	DO 9 L = 1,J2	CALC0850
9	A(J+50,K) = A(J+50,K) + KSS(J,L) * B(L,K)	CALC0860
	J3 = J3 - 9	CALC0870
	K1 = -9	CALC0880
	K2 = 0	CALC0890
	DO 10 L = 1,5	CALC0900
	J3 = J3 + 1	CALC0910
	IF ( K2 .GE. IEQ1 ) GO TO 10	CALC0920
	K1 = K1 + 10	CALC0930
	K2 = K2 + 10	CALC0940
	READ (3,J3) ((KSS(K,J),J=1,90),K=K1,K2)	CALC0950
10	CONTINUE	CALC0960
	J3 = J3 + 4	CALC0970
11	J11 = IEQ1	CALC0980
	IF ( J11 .GT. 50 ) J11 = 50	CALC0990
	DO 12 J = 1,J11	CALC1000
	DO 12 K = 1,J1	CALC1010
	A(J,K) = 0.0	CALC1020
	DO 12 L = 1,J2	CALC1030
12	A(J,K) = A(J,K) + KSS(J,L) * B(L,K)	CALC1040
	KA = KA - 18	CALC1050
	K1 = -9	CALC1060
	K2 = 0	CALC1070
	DO 14 L = 1,9	CALC1080
	KA = KA + 1	CALC1090
	IF ( K2 .GE. IEQ1 ) GO TO 14	CALC1100
	K1 = K1 + 10	CALC1110
	K2 = K2 + 10	CALC1120
	READ (3,KA) ((B(K,J),J=1,90),K=K1,K2)	CALC1130
14	CONTINUE	CALC1140
	DO 15 J = 1,J1	CALC1150
	DO 15 K = 1,J1	CALC1160

```

15 B (J,K) = B(J,K) - A(J,K)
   K1 = -9
   K2 = 0
   DO 16 L = 1,9
   J4 = J4 + 1
   IF ( K2 .GE. 1EQ1 ) GO TO 16
   K1 = K1 + 10
   K2 = K2 + 10
   WRITE (3,J4) ((B (K,J),J=1,90),K=K1,K2)
16 CONTINUE
20 CONTINUE
   RETURN
   END

```

```

CALC1170
CALC1180
CALC1190
CALC1200
CALC1210
CALC1220
CALC1230
CALC1240
CALC1250
CALC1260
CALC1270
CALC1280
CALC1290

```

```

SUBROUTINE ASSEM3 ( NBNODE )
ASSEMBLE THE SUB-SYSTEM MATRICES INTO THE SYSTEM MATRIX.
REAL KSS
COMMON X ( 200 ) , Y ( 200 ) , Z ( 200 ) , TH ( 200 ) ,
1 PRESSE( 200 ) , XL ( 200,3 ) , YL ( 200,3 ) ,
2 RAPANG( 100 ) , ZGL ( 100 ) , RHUB ( 100 ) , RTIP ( 100 ) ,
3 THHUB ( 100 ) , THTIP ( 100 ) , PRESSL(100,15),EDCM ( 3,3 ) ,
4 RHD , OMEGA , POISSO , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3 ) , NP , NT ,
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,
7 PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) ,
8 PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200) , FORCE(
9 200,6)
COMMON / MANE / NSUBS , IPOS(200) , NBTS(10,15) , NITS(10,15) , NBN(10) ,
1 INTN(10)
DOUBLE PRECISION COEFF
DIMENSION COEFF(301) , F(90) , KSS(90,90) , NBNEW(10)
NBNEW(1) = NBN(1)
DO 2 I = 2 , NSUBS
2 NBNEW(I) = NBN(I) - NBNEW(I-1)
NBNODE = NBN(1)
J2 = NBTS(1, NBNODE)
J1 = IPOS(J2)
NSUB = NSUBS - 1
DO 4 I = 2 , NSUB
J = NBN(I)
DO 3 K = 1 , J
J2 = NBTS(1, K)
IF ( IPOS(J2) .LE. J1 ) GO TO 3
J1 = IPOS(J2)
NBNODE = NBNODE + 1
3 CONTINUE
4 CONTINUE
I1 = 6 * NBNODE + 1
DO 40 I = 1 , NSUBS
K1 = 36 * NSUBS + 9 * (I-1)
IEQ1 = 6 * NBN(I)
J2 = -9
J3 = 0
DO 5 L = 1 , 9
K1 = K1 + 1
IF ( J3 .GE. IEQ1 ) GO TO 5
J2 = J2 + 10
J3 = J3 + 10
READ (3,K1) ((KSS(K,J) , J=1,90) , K=J2,J3)
5 CONTINUE
J2 = NBN(I)
J3 = INTN(I)
DO 10 J = 1 , J2
DO 10 K = 1 , 6
J1 = 6 * (J-1) + K
F(J1) = 0.0
DO 10 L = 1 , J3
DO 10 M = 1 , 6
M1 = 6 * (L-1) + M
10 F(J1) = F(J1) + KSS(J1,M1) * FORCE(NITS(I,L) , M )
K1 = 45 * NSUBS + 9 * (I-1)

```

```

ASEM3010
ASEM3020
ASEM3030
ASEM3040
ASEM3050
ASEM3060
ASEM3070
ASEM3080
ASEM3090
ASEM3100
ASEM3110
ASEM3120
ASEM3130
ASEM3140
ASEM3150
ASEM3160
ASEM3170
ASEM3180
ASEM3190
ASEM3200
ASEM3210
ASEM3220
ASEM3230
ASEM3240
ASEM3250
ASEM3260
ASEM3270
ASEM3280
ASEM3290
ASEM3300
ASEM3310
ASEM3320
ASEM3330
ASEM3340
ASEM3350
ASEM3360
ASEM3370
ASEM3380
ASEM3390
ASEM3400
ASEM3410
ASEM3420
ASEM3430
ASEM3440
ASEM3450
ASEM3460
ASEM3470
ASEM3480
ASEM3490
ASEM3500
ASEM3510
ASEM3520
ASEM3530
ASEM3540
ASEM3550
ASEM3560
ASEM3570
ASEM3580

```

L1 = -9	ASEM3590
L2 = 0	ASEM3600
DO 11 L = 1,9	ASEM3610
K1 = K1 + 1	ASEM3620
IF ( L2 .GE. IEQ1 ) GO TO 11	ASEM3630
L1 = L1 + 10	ASEM3640
L2 = L2 + 10	ASEM3650
READ (3*K1) ((KSS(K,J),J=1,90),K=L1,L2)	ASEM3660
11 CONTINUE	ASEM3670
J1 = I - 2	ASEM3680
ICOL1 = 1	ASEM3690
IF ( I .LE. 2 ) GO TO 13	ASEM3700
DO 12 J = 1,J1	ASEM3710
12 ICOL1 = ICOL1 + 6 * NBNEW(J)	ASEM3720
13 ICOL2 = ICOL1 + 6 * NBN(I) - 1	ASEM3730
K3 = ICOL1 - 1	ASEM3740
DO 40 J = 1,J2	ASEM3750
DO 40 K = 1,6	ASEM3760
DO 15 L = 1,301	ASEM3770
15 COEFF(L) = 0.0	ASEM3780
K1 = 6 * (J-1) + K	ASEM3790
K2 = K1 + K3	ASEM3800
IF ( I .EQ. 1 ) GO TO 20	ASEM3810
IF ( J .GT. NBNEW(I-1) ) GO TO 20	ASEM3820
READ (4*K2+200) COEFF	ASEM3830
20 DO 25 L = ICOL1, ICOL2	ASEM3840
25 COEFF(L) = COEFF(L) + KSS(K1, L-ICOL1+1)	ASEM3850
COEFF(I1) = COEFF(I1) - F(K1)	ASEM3860
IF ( I .EQ. 1 ) GO TO 27	ASEM3870
IF ( J .LE. NBNEW(I-1) ) GO TO 30	ASEM3880
27 COEFF(I1) = COEFF(I1) + FORCE(NBTS(I,J),K)	ASEM3890
30 WRITE (4*K2+200) COEFF	ASEM3900
40 CONTINUE	ASEM3910
RETURN	ASEM3920
END	ASEM3930

	SUBROUTINE BDEFL ( NBNODE )	BDEFL010
	IMPLICIT REAL*8 (A-H, U-Z)	BDEFL020
C	SOLVE FOR THE BOUNDARY NODE DEFLECTIONS IN THE COMMON	BDEFL030
C	COORDINATE SYSTEM	BDEFL040
C		BDEFL050
	COMMON / MANE / NSUBS, IPOS(200), NBTS(10,15), NITS(10,15), NBN(10),	BDEFL060
	1 INTN(10)	BDEFL070
	DIMENSION COEFF(301) , DISPLA(1200) , COEFR(301) , IDIS(300)	BDEFL080
	DIMENSION NBNEW(10)	BDEFL090
	DATA IDIS / 300 * 0 /	BDEFL100
	IEQ = 6 * NBNODE	BDEFL110
	NBNEW(1) = NBN(1)	BDEFL120
	DO 5 I = 2, NSUBS	BDEFL130
5	NBNEW(I) = NBN(I) - NBNEW(I-1)	BDEFL140
	I1 = IEQ + 1	BDEFL150
	K = 1	BDEFL160
10	READ (4*K+200) COEFF	BDEFL170
	I = K + 1	BDEFL180
	IF(DABS(COEFF(K)).GT. 1.0D-10) GO TO 35	BDEFL190
	DO 15 J = I, IEQ	BDEFL200
	J1 = J	BDEFL210
	READ (4*J+200) COEFR	BDEFL220
	IF(DABS(COEFR(K)) .GT. 1.0D-10) GO TO 25	BDEFL230
15	CONTINUE	BDEFL240
	WRITE (6,20)	BDEFL250
20	FORMAT (32H DISPLACEMENT MATRIX IS SINGULAR )	BDEFL260
	NSUBS = -NSUBS	BDEFL270
	RETURN	BDEFL280
25	WRITE (4*J1+200) COEFF	BDEFL290
	WRITE (4*K+200) COEFR	BDEFL300
	DO 30 J = 1, I1	BDEFL310
30	COEFF(J) = COEFR(J)	BDEFL320
35	READ (4*I+200) COEFR	BDEFL330
	ZM = COEFR(K) / COEFF(K)	BDEFL340
	COEFR(K) = 0.0	BDEFL350
	J = K + 1	BDEFL360
40	COEFR(J) = COEFR(J) - ZM * COEFF(J)	BDEFL370
	IF (J .EQ. IEQ) GO TO 45	BDEFL380
	J = J + 1	BDEFL390
	GO TO 40	BDEFL400
45	COEFR(J+1) = COEFR(J+1) - ZM * COEFF(J+1)	BDEFL410
	WRITE (4*I+200) COEFR	BDEFL420
	IF (I .EQ. IEQ) GO TO 50	BDEFL430
	I = I + 1	BDEFL440
	GO TO 35	BDEFL450
50	IF (K .EQ. IEQ - 1) GO TO 55	BDEFL460
	K = K + 1	BDEFL470
	GO TO 10	BDEFL480
55	K = K + 1	BDEFL490
	READ (4*K+200) COEFF	BDEFL500
	K2 = 0	BDEFL510
	DO 60 I = 2, NSUBS	BDEFL520
	K1 = K2 + 1	BDEFL530
	K2 = K1 + NBNEW(I-1) - 1	BDEFL540
	J12 = 0	BDEFL550
	DO 60 J = K1, K2	BDEFL560
	J12 = J12 + 1	BDEFL570
	J11 = NBTS(I, J12)	BDEFL580

```

DO 60 K = 1,6
L = 6 * (J-1) + K
60 IDIS(L) = 6 * IPOS(J11) + K
62 DISPLA(IDIS(IEQ)) = COEFF(IEQ+1) / COEFF(IEQ)
I = IEQ - 1
65 READ (4*I+200) COEFF
J = I + 1
S = 0.0
70 S = S + COEFF(J) * DISPLA(IDIS(J))
IF (J .EQ. IEQ) GO TO 75
J = J + 1
GO TO 70
75 DISPLA(IDIS(I)) = (COEFF( IEQ + 1 ) - S) / COEFF(I)
IF (I .EQ. 1) GO TO 80
I = I - 1
GO TO 65
80 CONTINUE
WRITE (3*1) (DISPLA(I),I=1,300)
WRITE (3*2) (DISPLA(I),I=301,600)
WRITE (3*3) (DISPLA(I),I=601,900)
WRITE (3*4) (DISPLA(I),I=901,1200)
RETURN
END

```

```

BDEFL590
BDEFL600
BDEFL610
BDEFL620
BDEFL630
BDEFL640
BDEFL650
BDEFL660
BDEFL670
BDEFL680
BDEFL690
BDEFL700
BDEFL710
BDEFL720
BDEFL730
BDEFL740
BDEFL750
BDEFL760
BDEFL770
BDEFL780
BDEFL790
BDEFL800
BDEFL810

```



	SUBROUTINE IDEFL	IDFL0010
	SOLVE FOR THE INTERNAL NODE DEFLECTION OF EACH SUB-SYSTEM.	IDFL0020
C		IDFL0030
C	COMMON X ( 200) , Y ( 200) , Z ( 200) , TH ( 200) ,	IDFL0040
	1 PRESSE( 200) , XL ( 200,3) , YL ( 200,3) ,	IDFL0050
	2 RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) ,	IDFL0060
	3 THHUB ( 100) , THTIP ( 100) , PRESSL(100,15),EDCM ( 3,3) ,	IDFL0070
	4 RHO , OMEGA , POISSO , YOUNGS , RADGEN ,	IDFL0080
	5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT ,	IDFL0090
	6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,	IDFL0100
	7 PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) ,	IDFL0110
	8 PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200) , FORCE(	IDFL0120
	9 200,6)	IDFL0130
	COMMON / MANE / NSUBS , IPOS(200) , NBTS(10,15) , NITS(10,15) , NBN(10) ,	IDFL0140
	1 INTN(10)	IDFL0150
	DOUBLE PRECISION DISPLA	IDFL0160
	DIMENSION DISPLA(1200) , A(90,90) , B(90) , DISPL(18,200)	IDFL0170
	DATA DISPL / 3600*0.0 /	IDFL0180
	READ (3*1) (DISPLA(I) , I=1,300)	IDFL0190
	READ (3*2) (DISPLA(I) , I=301,600)	IDFL0200
	READ (3*3) (DISPLA(I) , I=601,900)	IDFL0210
	READ (3*4) (DISPLA(I) , I=901,1200)	IDFL0220
	DO 25 I = 1, NSUBS	IDFL0230
	KBA = 18 * NSUBS + 18 * (I-1)	IDFL0240
	IEQ1 = 6 * INTN(I)	IDFL0250
	K1 = -9	IDFL0260
	K2 = 0	IDFL0270
	DO 5 L = 1,9	IDFL0280
	KBA = KBA + 1	IDFL0290
	IF ( K2 .GE. IEQ1 ) GO TO 5	IDFL0300
	K1 = K1 + 10	IDFL0310
	K2 = K2 + 10	IDFL0320
	READ (3*KBA) ((A(K,J) , J=1,90) , K=K1, K2)	IDFL0330
5	CONTINUE	IDFL0340
	J1 = INTN(I)	IDFL0350
	L1 = NBN(I)	IDFL0360
	DO 15 J = 1, J1	IDFL0370
	DO 15 K = 1,6	IDFL0380
	K1 = 6 * (J-1) + K	IDFL0390
	B(K1) = 0.0	IDFL0400
	DO 10 L = 1, L1	IDFL0410
	L3 = NBTS(I, L)	IDFL0420
	L2 = 6 * IPOS(L3)	IDFL0430
	DO 10 M = 1,6	IDFL0440
	M1 = L2 + M	IDFL0450
	N = 6 * (L-1) + M	IDFL0460
10	B(K1) = B(K1) + A(K1, N) * DISPLA(M1)	IDFL0470
15	B(K1) = FORCE(NITS(I, J), K) - B(K1)	IDFL0480
	K1 = -9	IDFL0490
	K2 = 0	IDFL0500
	DO 17 L = 1,9	IDFL0510
	KBA = KBA + 1	IDFL0520
	IF ( K2 .GE. IEQ1 ) GO TO 17	IDFL0530
	K1 = K1 + 10	IDFL0540
	K2 = K2 + 10	IDFL0550
	READ (3*KBA) ((A(K,J) , J=1,90) , K=K1, K2)	IDFL0560
17	CONTINUE	IDFL0570
	J1 = INTN(I)	IDFL0580

L1 = 6 * J1	IDFL0590
DO 20 J = 1,J1	IDFL0600
K3 = NITS(I,J)	IDFL0610
DO 20 K = 1,6	IDFL0620
K1 = 6 * IPOS(K3) + K	IDFL0630
K2 = 6 * ( J - 1 ) + K	IDFL0640
DISPLA(K1) = 0.0	IDFL0650
DO 20 L = 1,L1	IDFL0660
20 DISPLA(K1) = DISPLA(K1) + A(K2,L) * B(L)	IDFL0670
25 CONTINUE	IDFL0680
DO 50 I = 1,NT	IDFL0690
LA = NEXT(I,1)	IDFL0700
LB = NEXT(I,2)	IDFL0710
LC = NEXT(I,3)	IDFL0720
NA = 6 * IPOS(LA)	IDFL0730
NB = 6 * IPOS(LB)	IDFL0740
NC = 6 * IPOS(LC)	IDFL0750
DO 40 J = 1,6	IDFL0760
IF (IPOS(LA) .LT. 0) GO TO 30	IDFL0770
DISPL(J,I) = DISPLA(NA + J)	IDFL0780
30 IF (IPOS(LB) .LT. 0) GO TO 35	IDFL0790
DISPL(J+6,I) = DISPLA(NB+J)	IDFL0800
35 IF (IPOS(LC) .LT. 0) GO TO 40	IDFL0810
DISPL(J+12,I) = DISPLA(NC+J)	IDFL0820
40 CONTINUE	IDFL0830
50 CONTINUE	IDFL0840
K1 = -49	IDFL0850
K2 = 0	IDFL0860
DO 52 I = 1,4	IDFL0870
K1 = K1 + 50	IDFL0880
K2 = K2 + 50	IDFL0890
52 WRITE (3,I) ((DISPL(J,K),J=1,18),K=K1,K2)	IDFL0900
WRITE (6,55)	IDFL0910
55 FORMAT (1H1/ 43X, 14HCOMMON SYSTEM / 40X, 20HDEFLECTION PRINTOUT	IDFL0920
1 // 8X, 8HNODE NU., 6X, 1HX, 9X, 1HY, 9X, 1HZ, 11X, 1HU, 14X, 1HV,	IDFL0930
2 14X, 1HW, 10X, 6HTHETAX, 9X, 6HTHETAY /)	IDFL0940
J = 0	IDFL0950
DO 70 I = 1,NP	IDFL0960
LA = I	IDFL0970
K = 6 * IPOS(LA)	IDFL0980
D1 = 0.0	IDFL0990
D2 = 0.0	IDFL1000
D3 = 0.0	IDFL1010
D4 = 0.0	IDFL1020
D5 = 0.0	IDFL1030
IF (IPOS(LA) .LT. 0) GO TO 60	IDFL1040
D1 = DISPLA(K+1)	IDFL1050
D2 = DISPLA(K+2)	IDFL1060
D3 = DISPLA(K+3)	IDFL1070
D4 = DISPLA(K+4)	IDFL1080
D5 = DISPLA(K+5)	IDFL1090
60 J = J + 1	IDFL1100
IF (J .EQ. 50) WRITE (6,55)	IDFL1110
IF (J .EQ. 50) J = 0	IDFL1120
70 WRITE (6,80) I, X(I), Y(I), Z(I), D1, D2, D3, D4, D5	IDFL1130
80 FORMAT (10X, 15, 3F10.3, 5E15.5)	IDFL1140
RETURN	IDFL1150
END	IDFL1160

```

SUBROUTINE STRESS ( IPUNCH )
C CALCULATE THE LOCAL NODAL DISPLACEMENT MATRIX (DISPLL), THE LOCAL STRS0010
C MEMBRANE STRESS MATRIX (STRSLM), AND THE LOCAL BENDING STRESS STRS0020
C MATRIX (STRSLB) . STRS0030
C STRS0040
COMMON X ( 200) , Y ( 200) , Z ( 200) , TH ( 200) , STRS0050
1 PRESSE( 200) , XL ( 200,3) , YL ( 200,3) , STRS0070
2 RAPANG( 100) , ZGL ( 100) , RHUB ( 100) , RTIP ( 100) , STRS0080
3 THHUB ( 100) , THTIP ( 100) , PRESSL(100,15),EDCM ( 3,3) , STRS0090
4 RHO , OMEGA , POISSO , YOUNGS , RADGEN , STRS0100
5 NGENLI , LINE1 , NPRES(100) , NEXT ( 200,3) , NP , NT , STRS0110
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) , STRS0120
7 PFLGN(9,1) , CFLGN(18,1) , ELSTIF(18,18) , ECSTIF(18,18) , STRS0130
8 PFCGN(18,1) , CFCGN(18,1) , MEX(200,8) , IMEX(200J) , FORCE( STRS0140
9 200,6) STRS0150
COMMON / TBAR / THBAR(200) STRS0160
DIMENSION EM(3,3) , WM(3,6) , PRST(15) , DISPLL(18,1) , STRS0170
1 R6(18,18) , Z1(3,9) , Z2(3,9) , IND(6) , BST(3) , TST(3) STRS0180
2 , VB(3,3) , STRSLM(3) , STRSLB(3) , EB(3,9) , A(3) , B(3) , STRS0190
3 C(3) , DISPL(18,200) STRS0200
DATA WM / 1.0,4*0.0,1.0,2*0.0,1.0,0.0,1.0, 7*0.0 / STRS0210
DATA IND/ 1 , 2 , 7 , 8 , 13 , 14 / STRS0220
K1 = -49 STRS0230
K2 = 0 STRS0240
DO 1 I = 1,4 STRS0250
K1 = K1 + 50 STRS0260
K2 = K2 + 50 STRS0270
1 READ (3'I) ((DISPL(J,K),J=1,18),K=K1,K2) STRS0280
TERM = YOUNGS / ( 1.0 - POISSO**2 ) STRS0290
EM(1,1) = TERM STRS0300
EM(1,2) = TERM * POISSO STRS0310
EM(1,3) = 0.0 STRS0320
EM(2,1) = EM(1,2) STRS0330
EM(2,2) = EM(1,1) STRS0340
EM(2,3) = 0.0 STRS0350
EM(3,1) = 0.0 STRS0360
EM(3,2) = 0.0 STRS0370
EM(3,3) = TERM * ( 1.0 - POISSO ) / 2.0 STRS0380
WRITE (6,5) STRS0390
5 FORMAT (1H1 / 44X,13HLOCAL SYSTEM / 35X,30HDEFLECTION AND STRESS STRS0400
1PRINTOUT ) STRS0410
KOUNT = -1 STRS0420
DO 65 I = 1,NT STRS0430
IPASS = 0 STRS0431
SIGNSS = 1.0 STRS0432
READ (4'I) R6 , AMNIN , ABNIN STRS0440
DO 10 J = 1,18 STRS0450
DISPLL (J,1) = 0.0 STRS0460
DO 10 K = 1,18 STRS0470
10 DISPLL(J,1) = DISPLL(J,1) + R6(K,J) * DISPL(K,I) STRS0480
KOUNT = KOUNT + 1 STRS0490
IF ( KOUNT .EQ. 2 ) WRITE (6,5) STRS0500
IF ( KOUNT .EQ. 2 ) KOUNT = 0 STRS0510
LA = NEXT(I,1) STRS0520
LB = NEXT(I,2) STRS0530
LC = NEXT(I,3) STRS0540
WRITE (6,15) I,LA,X(LA),Y(LA),Z(LA),DISPLL(1,1),DISPLL(2,1), STRS0550
1 DISPLL(3,1) , LB,X(LB),Y(LB),Z(LB),DISPLL(7,1),DISPLL(8,1), STRS0560

```

```

2 DISPLL( 9,1), LC,X(LC),Y(LC),Z(LC),DISPLL(13,1),DISPLL(14,1), STRS0570
3 DISPLL(15,1) STRS0580
15 FORMAT (// 43X,12HELEMENT NO. 14 /11X,72HNODE X Y STRS0590
1 Z U V W / 12X,73HNO. COSTRS0600
2MMON COMMON COMMON LOCAL LOCAL LOCAL /STRS0610
38X,2HLA,15,3F10.3,3E15.5 / 8X,2HLB,15,3F10.3,3E15.5 / 8X,2HLC,15, STRS0620
43F10.3,3E15.5 ) STRS0630
DO 20 J = 1,3 STRS0640
DO 20 K = 1,6 STRS0650
Z1(J,K) = 0.0 STRS0660
DO 20 L = 1,3 STRS0670
20 Z1(J,K) = Z1(J,K) + EM(J,L) * WM(L,K) STRS0680
DO 30 J = 1,3 STRS0690
DO 30 K = 1,6 STRS0700
Z2(J,K) = 0.0 STRS0710
DO 30 L = 1,6 STRS0720
30 Z2(J,K) = Z2(J,K) + Z1(J,L) * AMNIN(L,K) STRS0730
DO 40 J = 1,3 STRS0740
STRSLM(J) = 0.0 STRS0750
DO 40 K = 1,6 STRS0760
40 STRSLM(J) = STRSLM(J) + Z2(J,K) * DISPLL(IND(K),1) STRS0770
C STRS0780
C STRS0790
C STRS0800
TERM1= YOUNGS * THBAR(1) / 2.0 / ( 1.0 - POISSO**2 ) STRS0810
A(1) = -2.0 * TERM1 * ( ( 3.0 * ABNIN(6,1) + POISSO * ABNIN(8,1) ) STRS0820
1 * DISPLL(3,1) + POISSO * ABNIN(8,2) * DISPLL(4,1) + ( 3.0 * STRS0830
2 ABNIN(6,3) + POISSO * ABNIN(8,3) ) * DISPLL(5,1) + ( 3.0 * STRS0840
3 ABNIN(6,4) + POISSO * ABNIN(8,4) ) * DISPLL(9,1) + POISSO * STRS0850
4 ABNIN(8,5) * DISPLL(10,1) + ( 3.0 * ABNIN(6,6) + POISSO * STRS0860
5 ABNIN(8,6) ) * DISPLL(11,1) + POISSO * ABNIN(8,9) * STRS0870
6 DISPLL(17,1) ) STRS0880
A(2) = -2.0 * TERM1 * ( ( 3.0 * POISSO * ABNIN(6,1) + ABNIN(8,1) ) STRS0890
1 * DISPLL(3,1) + ABNIN(8,2) * DISPLL(4,1) + ( 3.0 * POISSO * STRS0900
2 ABNIN(6,3) + ABNIN(8,3) ) * DISPLL(5,1) + ( 3.0 * POISSO * STRS0910
3 ABNIN(6,4) + ABNIN(8,4) ) * DISPLL(9,1) + ABNIN(8,5) * STRS0920
4 DISPLL(10,1) + ( 3.0 * POISSO * ABNIN(6,6) + ABNIN(8,6) ) * STRS0930
5 DISPLL(11,1) + ABNIN(8,9) * DISPLL(17,1) ) STRS0940
A(3) = 2.0 * TERM1 * ( ABNIN(7,2) * DISPLL(4,1) + ABNIN(7,5) * STRS0950
1 DISPLL(10,1) ) * ( 1.0 - POISSO ) STRS0960
B(1) = -2.0 * TERM1 * ( 3.0 * POISSO * ABNIN(9,1) * DISPLL(3,1) + STRS0970
1 ( ABNIN(7,2) + 3.0 * POISSO * ABNIN(9,2) ) * DISPLL(4,1) + STRS0980
2 3.0 * POISSO * ABNIN(9,3) * DISPLL(5,1) + 3.0 * POISSO * STRS0990
3 ABNIN(9,4) * DISPLL(9,1) + ( ABNIN(7,5) + 3.0 * POISSO * STRS1000
4 ABNIN(9,5) ) * DISPLL(10,1) + 3.0 * POISSO * ABNIN(9,6) * STRS1010
5 DISPLL(11,1) + 3.0 * POISSO * ABNIN(9,7) * DISPLL(15,1) + STRS1020
6 3.0 * POISSO * ABNIN(9,8) * DISPLL(16,1) ) STRS1030
B(2) = -2.0 * TERM1 * ( 3.0 * ABNIN(9,1) * DISPLL(3,1) + ( POISSO * STRS1040
1 ABNIN(7,2) + 3.0 * ABNIN(9,2) ) * DISPLL(4,1) + 3.0 * STRS1050
2 ABNIN(9,3) * DISPLL(5,1) + 3.0 * ABNIN(9,4) * DISPLL(9,1) STRS1060
3 + ( POISSO * ABNIN(7,5) + 3.0 * ABNIN(9,5) ) * DISPLL(10,1) STRS1070
4 + 3.0 * ABNIN(9,6) * DISPLL(11,1) + 3.0 * ABNIN(9,7) * STRS1080
5 DISPLL(15,1) + 3.0 * ABNIN(9,8) * DISPLL(16,1) ) STRS1090
B(3) = 2.0 * TERM1 * ( ABNIN(8,1) * DISPLL(3,1) + ABNIN(8,2) * STRS1100
1 DISPLL(4,1) + ABNIN(8,3) * DISPLL(5,1) + ABNIN(8,4) * STRS1110
2 DISPLL(9,1) + ABNIN(8,5) * DISPLL(10,1) + ABNIN(8,6) * STRS1120
3 DISPLL(11,1) + ABNIN(8,9) * DISPLL(17,1) ) * ( 1.0 - POISSO ) STRS1130
C(1) = -2.0 * TERM1 * ( ( ABNIN(4,1) + POISSO * ABNIN(5,1) ) * STRS1140

```

```

1      DISPLL(3,1) + POISSO * ABNIN(5,2) * DISPLL(4,1) +          STRS1150
2      ( ABNIN(4,3) + POISSO * ABNIN(5,3) ) * DISPLL(5,1) +      STRS1160
3      ( ABNIN(4,4) + POISSO * ABNIN(5,4) ) * DISPLL(9,1) +      STRS1170
4      ( ABNIN(4,6) + POISSO * ABNIN(5,6) ) * DISPLL(11,1) +     STRS1180
5      POISSO * ABNIN(5,7) * DISPLL(15,1) + POISSO * ABNIN(5,8) * STRS1190
6      DISPLL(16,1) + POISSO * ABNIN(5,9) * DISPLL(17,1))        STRS1200
C(2) = -2.0 * TERM1 * (( POISSO * ABNIN(4,1) + ABNIN(5,1) ) *   STRS1210
1      DISPLL(3,1) + ABNIN(5,2) * DISPLL(4,1) + ( POISSO *      STRS1220
2      ABNIN(4,3) + ABNIN(5,3) ) * DISPLL(5,1) + ( POISSO *    STRS1230
3      ABNIN(4,4) + ABNIN(5,4) ) * DISPLL(9,1) + ( POISSO *    STRS1240
4      ABNIN(4,6) + ABNIN(5,6) ) * DISPLL(11,1) + ABNIN(5,7) * STRS1250
5      DISPLL(15,1) + ABNIN(5,8) * DISPLL(16,1) + ABNIN(5,9) * STRS1260
6      DISPLL(17,1))                                             STRS1270
C(3) = 0.0                                                       STRS1280
XG = ( XL(I,1) + XL(I,2) + XL(I,3) ) / 3.0                       STRS1290
YG = ( YL(I,1) + YL(I,2) + YL(I,3) ) / 3.0                       STRS1300
45  DO 50 K = 1,3                                                STRS1310
      BST(K) = ( A(K)*XG + B(K)*YG + C(K) ) * SIGNSS              STRS1320
C      STRS1330
C      STRS1340
C      STRS1350
C      STRS1360
C      STRS1370
50  TST(K) = BST(K) + STRSLM(K)                                    STRS1380
      TERM1 = ( TST(1) + TST(2) ) / 2.0                           STRS1390
      TERM2 = SQRT( ( TST(1) - TST(2) )**2 / 4.0 + TST(3)**2 )   STRS1400
      SIGNS = 1.0                                                 STRS1410
      IF ( TST(2) .GT. TST(1) ) SIGNS = -1.0                     STRS1420
      PRST(1) = TERM1 + SIGNS * TERM2                             STRS1430
      PRST(2) = TERM1 - SIGNS * TERM2                             STRS1440
      PRST(3) = 0.5 * ATAN( 2.0 * TST(3) / ( TST(1) - TST(2) ) ) * STRS1450
1      57.29578                                                  STRS1460
      PRST(4) = ( PRST(1) - PRST(2) ) / 2.0                       STRS1470
      PRST(5) = SQRT( PRST(1)**2 - PRST(1) * PRST(2) + PRST(2)**2 ) STRS1480
      IF ( IPASS .EQ. 0 ) WRITE (6,55) (A(K),B(K),C(K),BST(K),K=1,3) STRS1490
55  FORMAT (/20X,74HBENDING STRESSES = A * ( LOCAL X VALUE ) + B * STRS1500
1 ( LOCAL Y VALUE ) + C // 42X,1HA,14X,1HB,14X,1HC,7X,17HVALUE AT STRS1510
2 CENTRCID / 26X,9HSIGMAXBAR , 4E15.5 / 26X,9HSIGMAYBAR ,4E15.5 / STRS1520
3 26X,9HSHEAR ,4E15.5)                                          STRS1530
      TERM1 = ( BST(1) + BST(2) ) / 2.0                           STRS1540
      TERM2 = SQRT( ( BST(1) - BST(2) )**2 / 4.0 + BST(3)**2 )   STRS1550
      SIGNS = 1.0                                                 STRS1560
      IF ( BST(2) .GT. BST(1) ) SIGNS = -1.0                     STRS1570
      PRST(6) = TERM1 + SIGNS * TERM2                             STRS1580
      PRST(7) = TERM1 - SIGNS * TERM2                             STRS1590
      PRST(8) = 0.5 * ATAN( 2.0 * BST(3) / ( BST(1) - BST(2) ) ) * STRS1600
1      57.29578                                                  STRS1610
      PRST(9) = ( PRST(6) - PRST(7) ) / 2.0                       STRS1620
      PRST(10) = SQRT( PRST(6)**2 - PRST(6) * PRST(7) + PRST(7)**2 ) STRS1630
      TERM1 = ( STRSLM(1) + STRSLM(2) ) / 2.0                       STRS1640
      TERM2 = SQRT( ( STRSLM(1) - STRSLM(2) )**2 / 4.0 + STRSLM(3)**2 ) STRS1650
      SIGNS = 1.0                                                 STRS1660
      IF ( STRSLM(2) .GT. STRSLM(1) ) SIGNS = -1.0               STRS1670
      PRST(11) = TERM1 + SIGNS * TERM2                            STRS1680
      PRST(12) = TERM1 - SIGNS * TERM2                            STRS1690
      PRST(13) = 0.5 * ATAN( 2.0 * STRSLM(3) / ( STRSLM(1) - STRSLM(2) ) STRS1700
1      ) * 57.29578                                             STRS1710
      PRST(14) = ( PRST(11) - PRST(12) ) / 2.0                  STRS1720

```

```

PRST(15) = SQRT( PRST(11)**2 - PRST(11) * PRST(12) + PRST(12)**2 )STRS1730
IF ( IPASS .EQ. 0 ) WRITE (6,60) (STRSLM(J),J=1,3) , (PRST(J),J=1,3)STRS1740
1 ,15) , (BST(J),J=1,3) , (PRST(J),J=6,10) , (TST(J),J=1,3) , STRS1750
2 (PRST(J),J=1,5) STRS1755
60 FORMAT (/ 61X,3( 'PRINCIPAL' 6X ) , ' MAXIMUM EFFECTIVE' / STRS1760
1 16X 'SIGMAXBAR SIGMAYBAR SHEAR SIGMAXBAR STRS1770
2SIGMAYBAR THETA (DEG) SHEAR STRESS' / ' MEMBRANESTRS1780
3 ' 8E15.5 / ' BEND.(TOP)' 8E15.5 / ' TOT. (TOP)' 8E15.5 ) STRS1790
IF ( IPASS .EQ. 1 ) WRITE (6,61) (BST(J),J=1,3) , (PRST(J),J=6,10 STRS1791
1 ) , (TST(J),J=1,3) , (PRST(J),J=1,5) STRS1792
61 FORMAT ( ' BEND.(BOT)' 8E15.5 / ' TOT. (BOT)' 8E15.5 //// ) STRS1793
IPASS = IPASS + 1 STRS1794
SIGNSS = -1.0 STRS1795
IF ( IPASS .NE. 1 ) GO TO 65 STRS1796
XG = ( XL(I,2) + XL(I,3) ) / 3.0 STRS1797
IF ( IPUNCH .NE. 0 ) WRITE (7,62) XL(I,2), XG, PRST(4), TST(1), STRS1798
1 PRST(5), PRST(10), PRST(15) STRS1799
62 FORMAT ( 2F10.6, 1P5E10.3 ) STRS179A
GO TO 45 STRS179B
65 CONTINUE STRS1800
RETURN STRS1810
END STRS1820

```

CLOCK	START	0		CLOK0000
BR0	EQU	0		CLOK0010
BR1	EQU	1		CLOK0021
BR2	EQU	2		CLOK0022
BR3	EQU	3		CLOK0023
BR4	EQU	4		CLOK0024
BR5	EQU	5		CLOK0025
BR6	EQU	6		CLOK0026
BR7	EQU	7		CLOK0027
BR8	EQU	8		CLOK0028
BR9	EQU	9		CLOK0029
BR10	EQU	10		CLOK0030
BR11	EQU	11		CLOK0031
BR12	EQU	12		CLOK0032
BR13	EQU	13		CLOK0033
BR14	EQU	14		CLOK0034
BR15	EQU	15		CLOK0035
ENTRY HCLOCK, ICLOCK, SCLOCK, DATE				
USING *,BR15				
HCLOCK	SAVE	(14,5),,*		CLOK0100
LR	BR1,BR13			CLOK0103
LA	BR13,SAVE			CLOK0105
ST	BR13,8(0,BR1)			CLOK0107
ST	BR1,4(0,BR13)			CLOK0109
TIME				CLOK0110
L	BR13,4(0,BR13)			CLOK0112
L	BR15,16(0,BR13)	RESTORE BASE REGISTER		CLOK0115
O	BR0,ZFBYT	INSURE PROPER SIGN FOR PACKED DIGIT.		CLOK0120
ST	BR0,PTIME	TEMP STORAGE FOR PACKED TIME.		CLOK0130
UNPK	ZTIME(7),PTIME(4)	UNPACK TIME TO ZONED DECIMAL.		CLOK0140
L	BR3,ZTIME	HOURS AND MINUTES.		CLOK0150
SLDL	BR2,16	SHIFT IN		CLOK0160
SLL	BR2,16	HOURS WITH		CLOK0170
O	BR2,BLNK2	TRAILING BLANKS.		CLOK0180
L	BR1,24(0,BR13)			CLOK0190
L	BR5,0(0,BR1)	ADDRESS OF FIRST PARAMETER.		CLOK0200
ST	BR2,0(0,BR5)	SAVE TIME.		CLOK0210
SLDL	BR2,16	SHIFT IN		CLOK0220
SLL	BR2,16	MINUTES WITH		CLOK0230
O	BR2,BLNK2	TRAILING BLANKS.		CLOK0240
L	BR5,4(0,BR1)			CLOK0245
ST	BR2,0(0,BR5)	SAVE MINUTES.		CLOK0250
L	BR3,ZTIME+4	MINUTE AND TENTHS		CLOK0260
SLDL	BR2,16	SHIFT IN		CLOK0270
SLL	BR2,16	SECONDS WITH		CLOK0280
O	BR2,BLNK2	TRAILING BLANKS.		CLOK0290
L	BR5,8(0,BR1)			CLOK0295
ST	BR2,0(0,BR5)	SAVE SECONDS.		CLOK0300
RETURN	(14,5),T			CLOK0310
USING *,BR15				
ICLOCK	SAVE	(14,5),,*		CLOK0100
LR	BR1,BR13			CLOK0
LA	BR13,SAVE			CLOK0
ST	BR13,8(0,BR1)			CLOK0
ST	BR1,4(0,BR13)			CLOK0
TIME	BIN			CLOK0330
L	BR13,4(0,BR13)			CLOK0333
L	BR15,16(0,BR13)	RESTORE BASE REGISTER		CLOK0335

	LR	BRI,BRO		CLOK0337
	SR	BRO,BRO		CLOK0339
	D	BRO,F100	CHANGE TO SECONDS FROM HUNDREDTHS	CLOK0340
	LR	BRO,BRI		CLOK0350
	L	BRI,24(0,BR13)	RELOAD ADDRESS OF PARAMETER LIST.	CLOK0360
	L	BR5,0(0,BR1)		CLOK0370
	ST	BRO,0(0,BR5)	STORE TIME	CLOK0380
		RETURN (14,5),T		CLOK0390
		USING *,BR15		
SCLOCK	SAVE	(14,5),,*		CLOK0100
	LR	BRI,BR13		CLOK0
	LA	BR13,SAVE		CLOK0
	ST	BR13,8(0,BR1)		CLOK0
	ST	BRI,4(0,BR13)		CLOK0
	TIME	BIN		CLOK0410
	L	BR13,4(0,BR13)		CLOK0420
	L	BRI,24(0,BR13)		CLOK0430
	L	BR5,0(0,BR1)		CLOK0440
	ST	BRO,0(0,BR5)	STORE TIME	CLOK0450
		RETURN (14,5),T		CLOK0460
		USING *,BR15		
DATE	SAVE	(14,5),,*		CLOK0100
	LR	BRI,BR13		CLOK0
	LA	BR13,SAVE		CLOK0
	ST	BR13,8(0,BR1)		CLOK0
	ST	BRI,4(0,BR13)		CLOK0
	TIME	DEC		CLOK0480
	L	BR13,4(0,BR13)		CLOK0483
	L	BR15,16(0,BR13)	RESTORE BASE REGISTER	CLOK0485
	LR	BR4,BRI	LOAD DATE INTO EVEN REGISTER.	CLOK0490
	SRDL	BR4,16	SHIFT DAY OF YEAR TO ODD REGISTER.	CLOK0500
	SRL	BR5,16	RIGHT JUSTIFY IT WITH LEADING ZEROES.	CLOK0510
	SLL	BR4,4	SET-UP YEAR TO ACCEPT A SIGN	CLOK0520
	O	BR5,ZFBYT	INSURE PROPER SIGN FOR DAY OF YEAR.	CLOK0530
	O	BR4,ZFBYT	INSURE PROPER SIGN FOR YEAR.	CLOK0540
	ST	BR4,PYEAR	STORE YEAR.	CLOK0550
	ST	BR4,LYEAR	STORE YEAR	CLOK0555
	ST	BR5,PDOFY	STORE DAY OF YEAR.	CLOK0560
*		IS THIS LEAP YEAR.		CLOK0570
	DP	LYEAR(4),PF0UR(1)		CLOK0580
	CP	LYEAR+3(1),ZF0YT+3(1)	REMAINDER = 0 - MEANS LEAP YEAR	CLOK0590
	BE	LPYER	BRANCH IF LEAP YEAR.	CLOK0600
*		IS IT DECEMBER		CLOK0610
FINDY	L	BR4,DEC12		CLOK0620
	CP	PDOFY(4),PK334(4)	IS IT DECEMBER.	CLOK0630
	BH	DECSI	YES.	CLOK0640
*		IS IT NOVEMBER		CLOK0650
	L	BR4,NOV11		CLOK0660
	CP	PDOFY(4),PK304(4)	IS IT NOVEMBER.	CLOK0670
	BH	NOVSI	YES	CLOK0680
*		IS IT OCTOBER		CLOK0690
	L	BR4,OCT10		CLOK0700
	CP	PDOFY(4),PK273(4)		CLOK0710
	BH	OCTSI		CLOK0720
*		IS IT SEPTEMBER		CLOK0730
	L	BR4,SEP09		CLOK0740
	CP	PDOFY(4),PK243(4)	IS IT SEPTEMBER.	CLOK0750
	BH	SEPSI	YES	CLOK0760



*		IS IT AUGUST		CLOK0770
	L	BR4,AUG08		CLOK0780
	CP	PDOFY(4),PK212(4)	IS IT AUGUST	CLOK0790
	BH	AUGSI	YES	CLOK0800
*		IS IT JULY		CLOK0810
	L	BR4,JUL07		CLOK0820
	CP	PDOFY(4),PK181(4)	IS IT JULY	CLOK0830
	BH	JULSI	YES	CLOK0840
*		IS IT JUNE		CLOK0850
	L	BR4,JUN06		CLOK0860
	CP	PDOFY(4),PK151(4)	IS IT JUNE	CLOK0870
	BH	JUNSI	YES	CLOK0880
*		IS IT MAY		CLOK0890
	L	BR4,MAY05		CLOK0900
	CP	PDOFY(4),PK120(4)	IS IT MAY	CLOK0910
	BH	MAYSI	YES	CLOK0920
*		IS IT APRIL		CLOK0930
	L	BR4,APR04		CLOK0940
	CP	PDOFY(4),PK090(4)	IS IT APRIL	CLOK0950
	BH	APRSI	YES	CLOK0960
*		IS IT MARCH		CLOK0970
	L	BR4,MAR03		CLOK0980
	CP	PDOFY(4),PK059(4)	IS IT MARCH	CLOK0990
	BH	MARSI	YES	CLOK1000
*		IS IT FEBRUARY		CLOK1010
FERJA	L	BR4,FEB02		CLOK1020
	CP	PDOFY(4),PK031(4)	IS IT FEBRUARY	CLOK1030
	BH	FEBSI	YES	CLOK1040
*		IT MUST BE JANUARY		CLOK1050
	L	BR4,JAN01		CLOK1060
STDAT	L	BR1,24(0,BR13)		CLOK1070
	L	BR5,0(0,BR1)		CLOK1080
	ST	BR4,0(0,BR5)	STORE MONTH - MM .	CLOK1090
	UNPK	ZTIME+2(2),PDOFY+2(2)	UNPACK DAY OF MONTH.	CLOK1100
	L	BR4,ZTIME		CLOK1110
	SLL	BR4,16	LEFT JUSTIFY.	CLOK1120
	O	BR4,BLNK2	PUT IN TRAILING BLANKS.	CLOK1130
	L	BR5,4(0,BR1)		CLOK1140
	ST	BR4,0(0,BR5)	STORE DAY - DD .	CLOK1150
	UNPK	ZTIME+2(2),PYEAR+2(2)		CLOK1160
	L	BR4,ZTIME		CLOK1170
	SLL	BR4,16		CLOK1180
	O	BR4,BLNK2		CLOK1190
	L	BR5,8(0,BR1)		CLOK1200
	ST	BR4,0(0,BR5)	STORE YEAR - YY .	CLOK1210
		RETURN (14,5),T		CLOK1220
*		ITS LEAP YEAR		CLOK1230
LPYER	CP	PDOFY(4),PK060(4)	IS IT JANUARY OR FEBRUARY	CLOK1240
	BNH	FERJA	YES	CLOK1250
	SP	PDOFY(4),PK001(4)	REDUCE DAYS BY ONE.	CLOK1260
	B	FINDT	GO FIND DATE.	CLOK1270
*		CALCULATE DAY OF MONTH.		CLOK1280
DECSI	SP	PDOFY(4),PK334(4)		CLOK1290
	B	STDAT		CLOK1300
NOVSI	SP	PDOFY(4),PK304(4)		CLOK1310
	B	STDAT		CLOK1320
OCTSI	SP	PDOFY(4),PK273(4)		CLOK1330
	B	STDAT		CLOK1340

SEPSI	SP	PDOFY(4),PK243(4)	CLOK1350
	B	STDAT	CLOK1360
AUGSI	SP	PDOFY(4),PK212(4)	CLOK1370
	B	STDAT	CLOK1380
JULSI	SP	PDOFY(4),PK181(4)	CLOK1390
	B	STDAT	CLOK1400
JUNSI	SP	PDOFY(4),PK151(4)	CLOK1410
	B	STDAT	CLOK1420
MAYSI	SP	PDOFY(4),PK120(4)	CLOK1430
	B	STDAT	CLOK1440
APRSI	SP	PDOFY(4),PK090(4)	CLOK1450
	B	STDAT	CLOK1460
MARSI	SP	PDOFY(4),PK059(4)	CLOK1470
	B	STDAT	CLOK1480
FEBSI	SP	PDOFY(4),PK031(4)	CLOK1490
	B	STDAT	CLOK1500
JAN01	DC	C' 1 '	CLOK1600
FEB02	DC	C' 2 '	CLOK1610
MAR03	DC	C' 3 '	CLOK1620
APR04	DC	C' 4 '	CLOK1630
MAY05	DC	C' 5 '	CLOK1640
JUN06	DC	C' 6 '	CLOK1650
JUL07	DC	C' 7 '	CLOK1660
AUG08	DC	C' 8 '	CLOK1670
SEP09	DC	C' 9 '	CLOK1680
OCT10	DC	C'10 '	CLOK1690
NOV11	DC	C'11 '	CLOK1700
DEC12	DC	C'12 '	CLOK1710
BLNK2	DC	C'00 '	CLOK1720
ZFBYT	DC	PL4'0'	CLOK1730
PYEAR	DC	PL4'0'	CLOK1740
LYEAR	DC	PL4'0'	CLOK1750
PDOFY	DC	PL4'0'	CLOK1760
PK334	DC	PL4'334'	CLOK1770
PK304	DC	PL4'304'	CLOK1780
PK273	DC	PL4'273'	CLOK1790
PK243	DC	PL4'243'	CLOK1800
PK212	DC	PL4'212'	CLOK1810
PK181	DC	PL4'181'	CLOK1820
PK151	DC	PL4'151'	CLOK1830
PK120	DC	PL4'120'	CLOK1840
PK090	DC	PL4'090'	CLOK1850
PK059	DC	PL4'059'	CLOK1860
PK031	DC	PL4'031'	CLOK1870
PK060	DC	PL4'060'	CLOK1880
PK001	DC	PL4'001'	CLOK1890
PFOUR	DC	P'4'	CLOK1900
ZTIME	DS	ZF	CLOK1910
PTIME	DS	IF	CLOK1920
F100	DC	F'6000'	CLOK1930
SAVE	DS	I8F	CLOK0705
	END		CLOK0720

SAVE AREA FOR THIS PROGRAM.

*	ZEROC - FILL DESIGNATED AREA OF CORE WITH ZERO OR WITH		ZER00000
*	A CONSTANT SUPPLIED IN THE CALLING SEQUENCE.		ZER00010
*			ZER00020
*	CALLING SEQUENCE		ZER00030
*	CALL ZEROC (FROM,TO)		ZER00040
*	OR		ZER00050
*	CALL ZEROC (FROM,TO,CONST)		ZER00060
*			ZER00070
*	WHERE-FROM-IS THE STARTING ADDRESS		ZER00080
*	TO-FINAL ADDRESS TO BE CLEARED		ZER00090
*	CONST-THE CONSTANT CORE IS TO BE		ZER00100
*	FILLED WITH. IF NOT SUPPLIED		ZER00110
*	IN CALLING SEQUENCE, CORE		ZER00120
*	WILL BE FILLED WITH ZEROES.		ZER00130
*			ZER00140
PWZERO	START	0	ZER00150
BR0	EQU	0	ZER00160
BR1	EQU	1	ZER00170
BR2	EQU	2	ZER00180
BR3	EQU	3	ZER00190
BR4	EQU	4	ZER00200
BR5	EQU	5	ZER00210
BR6	EQU	6	ZER00220
BR7	EQU	7	ZER00230
BR8	EQU	8	ZER00240
BR9	EQU	9	ZER00250
BR10	EQU	10	ZER00260
BR11	EQU	11	ZER00270
BR12	EQU	12	ZER00280
BR13	EQU	13	ZER00290
BR14	EQU	14	ZER00300
BR15	EQU	15	ZER00310
*			ZER00320
ENTRY	ZERO		ZER00325
USING	*,BR15		ZER00340
SAVE	(14,12),,*		ZER00330
ST	BR13,SAVE+4		ZER00350
LA	BR10,SAVE		ZER00360
ST	BR10,8(0,BR13)		ZER00370
L	BR3,0(0,BR1)		ZER00390
L	BR4,4(0,BR1)		ZER00400
N	BR3,BIGAD	INSURE ADDRESS ONLY.	ZER00410
N	BR4,BIGAD	INSURE ADDRESS ONLY.	ZER00420
CLR	BR3,BR4	1ST ARG. LESS THAN 2ND ARG.	ZER00430
BNL	SWITCH	NO, THEN SWITCH REGISTERS.	ZER00440
MODE1	TM	4(BR1),X'80'	ZER00470
BZ	NTZRO	MORE ARGUMENTS.	ZER00480
MODE	A	BR4,FORBT	YES,CALCULATE BYTES TO BE CLEARED.
SR	BR4,BR3	BR4 EQUAL NO. OF BYTES.	ZER00460
MORE	C	BR4,TWO56	OVER 255 BYTES TO CLEAR
BL	LESTN	YES	ZER00510
S	BR4,TWO56	REDUCE BY 256	ZER00520
L	BR5,TWO56		ZER00530
S	BR5,TWO		ZER00540
STC	BR5,MOVE+1		ZER00550
MOVE	XC	0(0,BR3),0(BR3)	ZER00560
A	BR3,TWO56		ZER00570
LTR	BR4,BR4		ZER00580

	BC	2, MORE		ZERO0590
RETRN	RETURN	(14, 12), T	RESTORE AND RETURN	ZERO0600
LESTN	LR	BR5, BR4		ZERO0610
	LA	BR4, 0		ZERO0620
	B	NONE		ZERO0630
SWITCH	LR	BR5, BR3		ZERO0640
	LR	BR3, BR4		ZERO0650
	LR	BR4, BR5		ZERO0660
	B	MODE1		ZERO0670
NTZRO	L	BR6, 8(0, BR1)		ZERO0680
	L	BR6, 0(0, BR6)		ZERO0685
NTZRI	ST	BR6, 0(0, BR3)		ZERO0690
	CR	BR3, BR4		ZERO0700
	BE	RETRN		ZERO0710
	A	BR3, FORBT		ZERO0720
	B	NTZRI		ZERO0730
SAVE	DS	18F		ZERO1000
BIGAD	DC	X'00FFFFFF'		ZERO1010
FORBT	DC	F'4'		ZERO1020
TWO56	DC	F'256'		ZERO1030
TWO	DC	F'1'		ZERO1050
	END			ZERO9990



SECTION IV  
VIBRATION COMPUTER PROGRAM (PWA 6140)

A. GENERAL

The vibration computer program is a finite element analysis which uses many of the same subroutines as the stress program. This program calculates natural frequencies and the distribution of relative displacement and stress for each resonant frequency. The resonant frequencies which satisfy the eigen-value equation: are obtained by reducing the term

$$\begin{bmatrix} A \end{bmatrix} = \begin{bmatrix} M \end{bmatrix}_T^{*-1} \begin{bmatrix} K \end{bmatrix}_T^*$$

to an almost triangular Hessenburg form  $[H]$  by elementary similarity transformation. The eigen-values are then determined by an extension of Hyman's method followed by iterations using a modification of Laguerre's method.

The size of the eigen-value subroutine limits the number of free finite element nodes to 50 (100 total nodes). The program requires 210,000 bytes of core on the IBM System 360, Model 75 computer. Computer time for the full 50 nodes is approximately 3 minutes. Single precision with 4 bytes/word and 8 bits/byte is used. Fortran IV-G, Level 1, Mod. 3 compilations were used.

B. INPUT DESCRIPTION

The input to the vibration computer program generally consists of: a physical description of the inducer, a description of the finite element breakup to be used, and a specification of the number of vibratory nodes required.

The finite element breakup should be sketched to aid in preparing the program input. An example is shown in figure 1. The program is limited to 50 free nodes (all nodes at the hub are fixed), 100 total nodes, and 100 triangular elements.

The program will reproduce the required finite element breakup properly if the following rules are observed when preparing the input.

1. If generator line "i" has "ii" points and generator line "i+1" has "ii+1" points, then the lines forming the edges of the finite elements start at the first point of the generator with the least number of points and zig zag between the generator lines. The areas between generators A and B, B and C, D and E, etc., of figure 1 are examples.
2. The area between the first two generator lines with the same number of points will be broken up as shown between generators F and G and G and H of figure 1.

3. The procedure of (2) will be followed for all generators with the same number of points until symmetry about a generator is requested, as was done about generator H in figure 1.
4. The altered breakup will continue for sections between generators with the same number of points, until symmetry is again requested, as was done about generator J in figure 1. After symmetry is again requested, the breakup will revert to the original pattern.
5. If two generators "i" and "j" have "m" and "n" points respectively such that

$$m = 2n - 1 \quad \text{and } n > 2$$

or

$$n = 2m - 1 \quad \text{and } m > 2$$

then the breakup will be as in the sections between L and M, and M and N of figure 1.

6. Notice that generator A of figure 1 has only one point. In this case

$$RHUB = RTIP \quad \text{and} \quad THHUB = THTIP$$

7. Elements are identified as shown in figure 1 and nodes are identified as shown in figure 2.

Unless otherwise specified, data may be input in any consistent set of units. The same units must be used for force and mass. Output will correspond to the input units used. Several examples are listed below:

	Input			Output	
Force	Mass	Length	Displacement	Stress	
lb	lb	ft	ft	lb/ft <sup>2</sup>	
lb	lb	in.	in.	lb/in. <sup>2</sup>	
gram	gram	meter	meter	gram/meter <sup>2</sup>	

Input data to be written on each card is described below. "F" format data should be left adjusted in the column field and should contain a decimal point. "E" format data (.300E08) must be right adjusted. "I" format data should not contain a decimal point and should be right adjusted.

#### Card 1 Title Card

As many title cards as required may be input. With a 1 in column 1 the machine will read in another title card. Omit the 1 in column 1 on the last title card to stop the machine from reading title cards.

Column		Variable	Format
Card 2			
1-10	RHO	Density of the inducer blade (MASS= RHO/G)	F10.0
11-20	POISSO	Poisson's ratio for the material of the inducer blade.	F10.0
21-30	YOUNGS	Youngs modulus of elasticity for the material of the inducer blade.	F10.0
31-40	RADGEN	Generator line offset radius. $R_G$ in figure 3.	F10.0
41-50	NGL	Total number of input generator lines. Maximum of 50.	I10
51-60	NGS	Number of generator lines about which geometric break-up symmetry is desired.	I10
61-65	MODE	Total number of vibratory modes requested. Maximum is the number of free nodes.	I5
66-70	IPRINT	Intermediate print option which should be used for check-out of the program Leave blank for no intermediate print. Input as 1 (right adjusted with no decimal point) for the following intermediate print:  a. Elemental local membrane stiffness matrices. b. Elemental local bending stiffness matrices. c. Elemental local membrane inertia matrices. d. Elemental local bending inertia matrices. e. Elemental local assembled stiffness matrices. f. Elemental local assembled inertia matrices.	I5
71-80	G	Gravitational constant in the appropriate units. If left blank or input as 0.0, a value of 386.4 is used. MASS = RHO/G.	F10.0
Card 3	Symmetry Requests (Optional)		
1-5	NCHB(1)	Generator line numbers of the generator lines	I5
6-10 etc.	NCHB (NGS)	about which geometric break-up symmetry is desired. The only condition allowing this request for break-up symmetry is that the previous generator line and the next generator line must each have the same number of points as does the generator line about which symmetry is requested.	



Column	Variable	Format
--------	----------	--------

That is

$$NUP_{I-1} = NUP_I = NUP_{I+1}$$

Sixteen values per card, as many cards as needed. If NGS on line 3 was input as zero or left blank, omit this card(s).

Card 4	Generator Lines (NGL Cards)		
1-10	RAPANG(I)	Wrap angle in degrees of the Ith generator line ( $\theta_1$ , and $\theta_2$ in figure 4). No two adjacent wrap angles may be equal. All wrap angles must be either continually increasing or continually decreasing in size.	F10.0
11-20	ZGL(I)	z value at the hub of the Ith generator line. ( $z_1$ and $z_2$ in figure 4). No two adjacent generator lines may have the same z value unless one of the two lean angles is non-zero.	F10.0
21-30	RHUB(I)	If RADGEN $\neq$ 0, then RHUB(I) is the horizontal (x-y plane) distance from the point where the generator line is tangent to a cylinder with a radius of RADGEN to the hub of the Ith generator.  If RADGEN = 0, then RHUB(I) is the radial distance from the z-axis to the hub of the Ith generator.	F10.0
31-40	RTIP(I)	Measured the same as RHUB(I) except that it is the distance to the tip instead of the hub of the Ith generator.	F10.0
41-50	THHUB(I)	Thickness of the inducer blade at the hub of the Ith generator line.	F10.0
51-60	THTIP(I)	Thickness of the inducer blade at the tip of the Ith generator line. Thickness is varied linearly from the hub to the tip of a generator line.	F10.0

Column	Variable	Format
61-65	NUP(I)	I5
	Number of points on the Ith generator line which are used for the division of the inducer blade into triangular elements. These points are evenly spaced between and including the hub and the tip.	
71-80	ALEAN(I)	F10.0
	The lean angle in degrees of the Ith generator line measured positive upward from the horizontal (x-y plane). These are illustrated by $\lambda$ in figure 3.	

### C. OUTPUT DESCRIPTION

X, Y, Z	Common coordinates of vertices or nodes of triangular elements.
XL, YL	Local coordinates of vertices or nodes of triangular elements.
TH	Nodal thickness of vertices of triangular elements.
FREQUENCY	Natural frequency.
AMPLITUDE	Relative amplitude ratio of node.
SIGMA X BAR, SIGMA Y BAR SHEAR	Relative bending stress of centroid of triangular element.
PRINCIPAL SIGMA X BAR, PRINCIPAL SIGMA Y BAR	Relative principle bending stresses at centroid of triangular element.
MAX SHEAR	Relative maximum shear stress at centroid of triangular element
EFFECTIVE STRESS	Effective combined stress at centroid of triangular element.
KM	Triangular element local membrane stiffness matrix.
KB	Triangular element local bending stiffness matrix.
MM	Triangular element local mass matrix.
MB	Triangular element reduced mass matrix.

D. VIBRATION COMPUTER PROGRAM  
Sample Case (Simulated Cantilevered Flat Plate)

LISTING OF INPUT CARDS

0.283	0.3000	0.3000E08C.C	5	3	10
0.00000	0.C00	100.C00	102.C00	0.100	0.000
0.01255	0.250	100.C00	102.C00	0.100	0.000
0.02510	0.500	100.C00	102.C00	0.100	0.000
0.03764	0.750	100.C00	102.C00	0.100	0.000
0.05013	1.C00	100.C00	102.C00	0.100	0.000

OUTPUT

INDUCER VIBRATION PROGRAM - DECK 6140

DATE 6/30/70

VIBRATION STUDY OF A SIMULATED CANTILEVERED FLAT PLATE  
J. A. SCHEURENBRAND DESIGN STA. A DEPT. 712 EXT. 395

DENSITY = 0.2830    G = 0.3864E 03    POISSON'S RATIO = 0.300    YOUNG'S MODULUS = 0.3000E 08  
 NO. OF GENERATING LINES = 5    NO. OF SYMMETRY CHANGES REQUESTED = 3  
 GENERATOR LINE OFFSET RADIUS = 0.0  
 NO. OF MODES REQUESTED = 10  
 SYMMETRY CHANGE ABOUT GENERATOR LINES    2    3    4

INDUCER VIBRATION PROGRAM - DECK 6140

WRAP ANGLE = 0.0	GENERATOR LINE NUMBER 1	(ANGLES IN DEG.)	TIP RADIUS = 102.0000
HUB THICKNESS = 0.1000	ZHUB = 0.0	HUB RADIUS = 100.0000	VJ. OF JOINTS = 9
	TIP THICKNESS = 0.1000	LEAN ANGLE = 0.0	
	GENERATOR LINE NUMBER 2	(ANGLES IN DEG.)	
WRAP ANGLE = 0.012550	ZHUB = 0.2500	HUB RADIUS = 100.0000	TIP RADIUS = 102.0000
HUB THICKNESS = 0.1000	TIP THICKNESS = 0.1000	LEAN ANGLE = 0.0	VJ. OF JOINTS = 9
	GENERATOR LINE NUMBER 3	(ANGLES IN DEG.)	
WRAP ANGLE = 0.025100	ZHUB = 0.5000	HUB RADIUS = 100.0000	TIP RADIUS = 102.0000
HUB THICKNESS = 0.1000	TIP THICKNESS = 0.1000	LEAN ANGLE = 0.0	VJ. OF JOINTS = 9
	GENERATOR LINE NUMBER 4	(ANGLES IN DEG.)	
WRAP ANGLE = 0.037640	ZHUB = 0.7500	HUB RADIUS = 100.0000	TIP RADIUS = 102.0000
HUB THICKNESS = 0.1000	TIP THICKNESS = 0.1000	LEAN ANGLE = 0.0	VJ. OF JOINTS = 9
	GENERATOR LINE NUMBER 5	(ANGLES IN DEG.)	
WRAP ANGLE = 0.050130	ZHUB = 1.0000	HUB RADIUS = 100.0000	TIP RADIUS = 102.0000
HUB THICKNESS = 0.1000	TIP THICKNESS = 0.1000	LEAN ANGLE = 0.0	VJ. OF JOINTS = 9

RESULTING TRIANGULAR ELEMENTS

ELEMENT NO. 1		ELEMENT NO. 2		ELEMENT NO. 3		ELEMENT NO. 4		ELEMENT NO. 5		ELEMENT NO. 7	
NODE NO.		NODE NO.		NODE NO.		NODE NO.		NODE NO.		NODE NO.	
LA	10	LA	1	LA	11	LA	2	LA	12	LA	3
LB	11	LB	2	LB	12	LB	3	LB	13	LB	4
LC	1	LC	11	LC	2	LC	12	LC	3	LC	4
X	-0.022	X	-0.0	X	-0.022	X	-0.0	X	-0.022	X	-0.0
Y	100.000	Y	100.000	Y	100.250	Y	100.250	Y	100.500	Y	100.750
Z	0.250	Z	0.0	Z	0.250	Z	0.0	Z	0.250	Z	0.0
TH	0.1000	TH	0.1000	TH	0.1000	TH	0.1000	TH	0.1000	TH	0.1000
TL	0.0	TL	0.0	TL	0.0	TL	0.0	TL	0.0	TL	0.0
KL	0.0000	KL	0.0000	KL	0.0000	KL	0.0000	KL	0.0000	KL	0.0000
YL	-0.2510	YL	0.2510	YL	-0.2510	YL	0.2510	YL	-0.2510	YL	0.2510

(CONTINUING TO ELEMENT NO. 64)

.....

.....

.....

.....

.....

.....



AMPLITUDES FOR MODE 1

FREQUENCY = 0.71916E 03

NODE	AMPLITUDE
2	0.23737E-01
3	0.92537E-01
4	0.19944E 00
5	0.33480E 00
6	0.48952E 00
7	0.65566E 00
8	0.82709E 00
9	0.10000E 01
11	0.21975E-01
12	0.90760E-01
13	0.19742E 00
14	0.33259E 00
15	0.48726E 00
16	0.65351E 00
17	0.82513E 00
18	0.99815E 00
20	0.22868E-01
21	0.90887E-01
22	0.19732E 00
23	0.33233E 00
24	0.48684E 00
25	0.65292E 00
26	0.82433E 00
27	0.99721E 00
29	0.21921E-01
30	0.90588E-01
31	0.19712E 00
32	0.33216E 00
33	0.48667E 00
34	0.65275E 00
35	0.82416E 00
36	0.99693E 00
38	0.23600E-01
39	0.92175E-01
40	0.19883E 00
41	0.33392E 00
42	0.48833E 00
43	0.65414E 00
44	0.82518E 00
45	0.99748E 00

RELATIVE VIBRATORY BENDING STRESSSES  
EVALUATED AT CENTRIDS

ELEMENT	SIGMAXBAR	SHEAR	PRIN SIGMA1BAR	PRIN SIGMA2BAR	MAX SHEAR	MIN. STRESS
1	0.1000E 01	0.30332E-01	0.1000E 01	0.1000E 01	0.9376E 00	0.1000E 01
2	-0.71152E-01	-0.89250E 00	-0.15109E 00	0.68434E 00	0.9773E 00	0.79666E 00
3	0.30774E 00	-0.85959E 00	0.22170E 00	0.71435E 00	0.8677E 00	0.75902E 00
4	0.18592E 00	-0.71735E 00	0.12645E 00	0.67179E 00	0.84904E 00	0.73541E 00
5	0.21514E 00	-0.70370E 00	0.14373E 00	0.55102E 00	0.68034E 00	0.59717E 00
6	0.16572E 00	-0.53233E 00	0.12288E 00	0.51889E 00	0.64567E 00	0.55420E 00
7	0.18140E 00	-0.52325E 00	0.12501E 00	0.39811E 00	0.48283E 00	0.42837E 00
8	0.14394E 00	-0.37071E 00	0.11411E 00	0.36924E 00	0.44875E 00	0.39757E 00
9	0.15162E 00	-0.36525E 00	0.10729E 00	0.25966E 00	0.30470E 00	0.27582E 00
10	0.12448E 00	-0.2372E 00	0.10520E 00	0.23608E 00	0.27395E 00	0.24975E 00
11	0.11823E 00	-0.23175E 00	0.93066E-01	0.14356E 00	0.15892E 00	0.14949E 00
12	0.10224E 00	-0.12371E 00	0.80977E-01	0.12682E 00	0.13332E 00	0.13009E 00
13	0.82802E-01	-0.12384E 00	0.51265E-01	0.59260E-01	0.58780E-01	0.59925E-01
14	0.77515E-01	-0.49216E-01	0.70568E-01	0.47913E-01	0.35824E-01	0.45789E-01
15	0.56156E-01	-0.49152E-01	0.11319E-01	0.20661E-01	0.23127E-01	0.21590E-01
16	0.50802E-01	-0.20370E-01	0.25617E-01	0.16373E-01	0.11638E-01	0.15953E-01
17	0.98725E 00	0.30458E-01	0.98725E 00	0.98723E 00	0.92569E 00	0.98723E 00
18	-0.67994E-01	0.97598E 00	-0.16207E 00	0.69794E 00	0.10000E 01	0.81397E 00
19	0.24019E 00	0.10300E 01	0.12873E 00	0.70713E 00	0.89546E 00	0.77477E 00
20	0.17166E 00	0.75238E 00	0.10876E 00	0.68849E 00	0.87853E 00	0.75592E 00
21	0.16895E 00	0.76895E 00	0.84234E-01	0.54459E 00	0.69563E 00	0.59900E 00
22	0.15705E 00	0.56156E 00	0.11058E 00	0.52755E 00	0.66221E 00	0.57578E 00
23	0.14920E 00	0.57130E 00	0.83129E-01	0.39444E 00	0.49495E 00	0.43044E 00
24	0.12988E 00	0.39031E 00	0.97782E-01	0.37571E 00	0.46397E 00	0.40721E 00
25	0.12495E 00	0.39524E 00	0.74664E-01	0.25736E 00	0.31473E 00	0.27781E 00
26	0.10304E 00	0.24108E 00	0.83298E-01	0.23927E 00	0.28702E 00	0.25530E 00
27	0.99680E-01	0.24211E 00	0.62687E-01	0.14206E 00	0.16510E 00	0.15037E 00
28	0.79776E-01	0.12315E 00	0.69328E-01	0.12663E 00	0.14176E 00	0.13233E 00
29	0.75198E-01	0.12302E 00	0.45133E-01	0.58189E-01	0.15909E-01	0.59335E-01
30	0.62048E-01	0.47334E-01	0.56161E-01	0.45530E-01	0.38421E-01	0.44859E-01
31	0.57794E-01	0.47430E-01	0.12616E-01	0.20964E-01	0.22879E-01	0.21661E-01
32	0.47690E-01	0.20558E-01	0.23458E-01	0.15542E-01	0.11392E-01	0.15155E-01
33	0.98614E 00	-0.24091E-01	0.98618E 00	0.98616E 00	0.92469E 00	0.98616E 00
34	-0.68251E-01	-0.96936E 00	-0.16096E 00	0.69674E 00	0.99799E 00	0.81242E 00
35	0.23752E 00	-0.98374E 00	0.12930E 00	0.70681E 00	0.89480E 00	0.77432E 00
36	0.16694E 00	-0.74315E 00	0.10551E 00	0.68641E 00	0.87704E 00	0.75509E 00
37	0.16571E 00	-0.75355E 00	0.84436E-01	0.54439E 00	0.69523E 00	0.59874E 00
38	0.15238E 00	-0.55210E 00	0.10742E 00	0.52554E 00	0.66079E 00	0.57401E 00
39	0.14445E 00	-0.55595E 00	0.82046E-01	0.39391E 00	0.49466E 00	0.43000E 00
40	0.12605E 00	-0.38042E 00	0.95568E-01	0.37381E 00	0.46231E 00	0.42540E 00
41	0.11910E 00	-0.37951E 00	0.773138E-01	0.23650E 00	0.31419E 00	0.27707E 00
42	0.99063E-01	-0.22923E 00	0.81140E-01	0.23717E 00	0.28509E 00	0.25425E 00
43	0.93540E-01	-0.22329E 00	0.62233E-01	0.14078E 00	0.16356E 00	0.14900E 00
44	0.75704E-01	-0.10953E 00	0.57334E-01	0.12410E 00	0.13917E 00	0.12975E 00
45	0.70355E-01	-0.10201E 00	0.49157E-01	0.55870E-01	0.55082E-01	0.56422E-01
46	0.59471E-01	-0.30534E-01	0.455756E-01	0.42259E-01	0.33801E-01	0.41433E-01
47	0.58108E-01	-0.25954E-01	0.19795E-01	0.18678E-01	0.17065E-01	0.18597E-01
48	0.43512E-01	-0.10294E-02	0.18198E-01	0.13057E-01	0.10177E-01	0.12779E-01
49	0.99649E 00	-0.25412E-01	0.99652E 00	0.99652E 00	0.93430E 00	0.99550E 00
50	-0.68739E-01	0.89952E 00	-0.14989E 00	0.68393E 00	0.97634E 00	0.79597E 00

51	0.30366E 00	0.68686E 00	0.88935E 00	0.21541E 00	0.71332E 00	0.86893E 00	0.75878E 00
52	0.18820E 00	0.65501E 00	0.72435E 00	0.12789E 00	0.67309E 00	0.85020E 00	0.73554E 00
53	0.21114E 00	0.52824E 00	0.71358E 00	0.13715E 00	0.55043E 00	0.68218E 00	0.59748E 00
54	0.16851E 00	0.50710E 00	0.54178E 00	0.12429E 00	0.52036E 00	0.64707E 00	0.55554E 00
55	0.17750E 00	0.37974E 00	0.53737E 00	0.11814E 00	0.39755E 00	0.48504E 00	0.42873E 00
56	0.14694E 00	0.36129E 00	0.38052E 00	0.11557E 00	0.37069E 00	0.45010E 00	0.39899E 00
57	0.14718E 00	0.24460E 00	0.38198E 00	0.99118E-01	0.25901E 00	0.30712E 00	0.27521E 00
58	0.12736E 00	0.23127E 00	0.24353E 00	0.12631E 00	0.23753E 00	0.27545E 00	0.25123E 00
59	0.11303E 00	0.13092E 00	0.24931E 00	0.72706E-01	0.14301E 00	0.16235E 00	0.15015E 00
60	0.10553E 00	0.12446E 00	0.13543E 00	0.32131E-01	0.12848E 00	0.13508E 00	0.13179E 00
61	0.77073E-01	0.47278E-01	0.14288E 00	0.37095E-01	0.59271E-01	0.64487E-01	0.51390E-01
62	0.79730E-01	0.46575E-01	0.53098E-01	0.68861E-01	0.49836E-01	0.39086E-01	0.48794E-01
63	0.47536E-01	0.44568E-02	0.57774E-01	-0.55597E-02	0.20385E-01	0.29539E-01	0.23928E-01
64	0.50470E-01	0.78168E-02	0.51993E-01	0.13212E-01	0.19894E-01	0.22545E-01	0.20874E-01

1	-0.34997E 06	-0.11665E 07	-0.17000E 05	-0.34994E 06	-0.11666E 07	0.43545E 06	0.10369E 07
1							
19							
1							
1							
18							
1							

(PROGRAM CONTINUES ON THRU NUMBER OF MODE SELECTED AT INPUT.)

E. VIBRATION COMPUTER PROGRAM LISTING

```

C      THIS IS THE MAIN PROGRAM FOR THE INDUCER VIBRATIONS PROGRAM      MAIN0001
C      DECK 6140                                                         MAIN0002
C                                                                           MAIN0003
COMMON X      ( 100) , Y      ( 100) , Z      ( 100) , TH      ( 100) ,MAIN0004
1          XL ( 100,3) , YL ( 100,3) ,      MAIN0005
2      RAPANG( 50) , ZGL ( 50) , RHUB ( 50) , RTIP ( 50) ,MAIN0006
3      THHUB ( 50) , THIP ( 50) ,      EDCM ( 3,3) ,MAIN0007
4      RHO ,      POISSD , YOUNGS , RADGEN ,      MAIN0008
5      VGENLI , LINE1 ,      NEXT ( 100,3) , NP , NT ,      MAIN0009
6      ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,      MAIN0010
7      SIGMAX(100) , SIGMAY(100) , ELSTIF(18,18) ,      MAIN0011
8      TAUXY(100) , ELSSM(9,9) , MEX(100,8) , IMEX(100) ,      MAIN0012
9      ELINR(18,18) , ELMIM(6,6) , ELBIM(9,9) , ALEAN(50)      MAIN0013
DIMENSION ICOL(15) , ZCOS(100) , NUP(100) , NCHB(50) , IPOS(100)      MAIN0014
DIMENSION OMEGA(50) , IGEN(100)      MAIN0015
DATA ICOL / 1 , 2 , 7 , 8 , 13 , 14 , 3 , 4 , 5 , 9 , 10 , 11 ,      MAIN0016
1          15 , 16 , 17 /      MAIN0017
DEFINE FILE 1(100,657,U,IR1),2(48,900,U,IR2),3(100,324,U,IR3)      MAIN0018
5      CALL ZERO(X,ELBIM(9,9))      MAIN0019
C      READ AND PRINT ALL INPUT      MAIN0020
10     CALL INPUT ( IPRINT,NUP,NCHB,MODE )      MAIN0021
C      TRIANGULATION OF INDUCER BLADE AND DETERMINATION OF THICKNESS AT      MAIN0022
C      EACH VERTEX .      MAIN0023
CALL GEOM ( NUP,NCHB,IPOS,IGEN )      MAIN0024
IF ( ( NP .GT. 100 ) .OR. ( NT .GT. 100 ) ) GO TO 5      MAIN0025
DO 30 I = 1,NT      MAIN0026
LA = NEXT(I,1)      MAIN0027
LB = NEXT(I,2)      MAIN0028
LC = NEXT(I,3)      MAIN0029
IMEX(LA) = IMEX(LA) + 1      MAIN0030
IMEX(LB) = IMEX(LB) + 1      MAIN0031
IMEX(LC) = IMEX(LC) + 1      MAIN0032
MEX(LA,IMEX(LA)) = I      MAIN0033
MEX(LB,IMEX(LB)) = I      MAIN0034
MEX(LC,IMEX(LC)) = I      MAIN0035
C      CALCULATE THE DIRECTION COSINE MATRIX (EDCM) FOR A TRIANGULAR ELEMMAIN0036
CALL DIRCOS (LA,LB,LC,I)      MAIN0037
ZCOS(I) = EDCM(3,3)      MAIN0038
C      CALCULATE THE LOCAL COORDINATES (XL,YL,ZL) FOR A TRIANGULAR ELEMMAIN0039
CALL LCOORD (LA,LB,LC,I)      MAIN0040
C      CALCULATE THE MEMBRANE STIFFNESS MATRIX (ELMSM) FOR A TRIANGULAR      MAIN0041
C      ELEMENT IN THE LOCAL COORDINATE SYSTEM (XL,YL,ZL)      MAIN0042
CALL MEMSTF ( LA,LB,LC,I )      MAIN0043
C      CALCULATE THE BENDING STIFFNESS MATRIX (ELBSM) FOR A TRIANGULAR      MAIN0044
C      ELEMENT IN THE LOCAL COORDINATE SYSTEM (XL,YL,ZL)      MAIN0045
CALL BEVSTF ( LA,LB,LC,I )      MAIN0046
IF ( IPRINT .GE. 1 )      MAIN0047
14     IWRITE (6,14) ((ELMSM(J,K),K=1,6),J=1,6),((ELBSM(J,K),K=1,9),J=1,9)      MAIN0048
FORMAT(1H1/45X,2HKM / 6(10X,6E14.6/) //65X,2HKB/9( 1X,9E14.6/))      MAIN0049
C      CALCULATE THE LOCAL MEMBRANE INERTIA      MAIN0050
C      MATRIX (ELMIM) FOR A TRIANGULAR      MAIN0051
C      ELEMENT.      MAIN0052
CALL MEMINR (LA,LB,LC,I)      MAIN0053
C      CALCULATE THE LOCAL BENDING INERTIA MATRIX (ELBIM) FOR A      MAIN0054
C      TRIANGULAR ELEMENT.      MAIN0055
CALL BENINR (LA,LB,LC,I)      MAIN0056
IF ( IPRINT .GE. 1 ) WRITE (6,15) ((ELMIM(J,K),K=1,6),J=1,6),      MAIN0057
1          ((ELBIM(J,K),K=1,9),J=1,9)      MAIN0058

```

```

15  FORMAT (//45X,2HMM/6(10X,6E14.6//65X,2HMB/9(1X,9E14.6//) MAIN0059
C   ASSEMBLE LOCAL STIFFNESS MATRIX (ELSTIF) AND LOCAL INERTIA MATRIX MAIN0060
C   (ELINR) FOR A TRIANGULAR FLEMENT . MAIN0061
      DO 20 J = 1,6 MAIN0062
      DO 20 K = 1,6 MAIN0063
      ELINR(ICOL(J),ICOL(K)) = ELMIM(J,K) MAIN0064
20  ELSTIF(ICOL(J),ICOL(K)) = ELMSM(J,K) MAIN0065
      DO 24 J = 1,9 MAIN0066
      DO 24 K = 1,9 MAIN0067
      ELINR(ICOL(J+6),ICOL(K+6)) = ELBIM(J,K) MAIN0068
24  ELSTIF(ICOL(J+6),ICOL(K+6)) = ELBSM(J,K) MAIN0069
      WRITE (1*1) ELSTIF,ELINR,EDCM MAIN0070
      IF ( IPRINT .GE. 1 ) WRITE (6,25) MAIN0071
25  FORMAT (1H //25X,55H LOCAL COORDINATE SYSTEM TRIANGULAR STIFFNESSMAIN0072
      I MATRIX ) MAIN0073
      IF ( IPRINT .GE. 1 ) WRITE (6,26) ((ELSTIF(J,K),K=1,18),J=1,18) MAIN0074
26  FORMAT (//18(10E12.4/8E12.4//)) MAIN0075
      IF ( IPRINT .GE. 1 ) WRITE (6,27) MAIN0076
27  FORMAT (1H //25X,52H LOCAL COORDINATE SYSTEM TRIANGULAR INERTIA MAIN0077
      ITRIX ) MAIN0078
      IF ( IPRINT .GE. 1 ) WRITE (6,26) ((ELINR(J,K),K=1,18),J=1,18) MAIN0079
30  CONTINUE MAIN0080
C   PRINT GEOMETRIC BREAK-UP AND ASSOCIATED PROPERTIES . MAIN0081
      CALL PRINT1 MAIN0082
C   CALCULATE NORMAL DIRECTION COSINE MATRIX AT EACH NODE . MAIN0083
      CALL NORM ( ZCOS,IGEN ) MAIN0084
C   TRANSFORM STIFFNESS MATRICES TO NORMAL SYSTEMS AND ASSEMBLE MAIN0085
C   INTO A (3N X 3N) MATRIX . MAIN0086
      CALL ASSEMK ( ZCOS , IPOS ) MAIN0087
C   TRANSFORM INERTIA MATRICES TO NORMAL SYSTEMS AND ASSEMBLE MAIN0088
C   INTO A (3N X 3N) MATRIX . MAIN0089
      CALL ASSEMM ( ZCOS , IPOS ) MAIN0090
C   REDUCE THE ASSEMBLED STIFFNESS MATRIX TO AN (N X N) MATRIX . MAIN0091
      N = NP - NGENLI MAIN0092
      CALL REDUCK ( N ) MAIN0093
      IF ( N .LE. 0 ) GO TO 5 MAIN0094
C   REDUCE THE ASSEMBLED INERTIA MATRIX TO AN (N X N) MATRIX . MAIN0095
      CALL REDUCM ( N ) MAIN0096
      IF ( N .LE. 0 ) GO TO 5 MAIN0097
C   SOLVE FOR THE NATURAL FREQUENCIES . MAIN0098
      CALL EIGEN ( N,OMEGA ) MAIN0099
C   SOLVE FOR THE AMPLITUDES FOR EACH REQUESTED FREQUENCY . MAIN0100
      DO 35 I = 1,MODE MAIN0101
      IF ( I .GT. N ) GO TO 5 MAIN0102
      WRITE (6,32) I MAIN0103
32  FORMAT (1H1,//50X,22HAMPLITUDES FOR MODE I3 ) MAIN0104
      M = NP - NGENLI MAIN0105
      I1 = N + 1 - I MAIN0106
      CALL AMPL ( M , OMEGA(I1) , IPOS) MAIN0107
35  CALL STRESS ( ZCOS, IPOS ) MAIN0108
      GO TO 5 MAIN0109
40  STOP MAIN0110
      END MAIN0111

```

```

SUBROUTINE INPUT ( IPRINT,NUP,NCHB,MODE )
READ AND PRINT ALL INPUT
COMMON X ( 100) , Y ( 100) , Z ( 100) , IH ( 100) ,
1 XL ( 100,3) , YL ( 100,3) ,
2 RAPANG( 50) , ZGL ( 50) , RHUB ( 50) , RTIP ( 50) ,
3 THHUB ( 50) , THTIP ( 50) , EDCM ( 3,3) ,
4 RHO , POISSO , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NEXT ( 100,3) , NP , NT ,
6 ELMSM(6,6) , AMNIN(6,6) , ELRSM(9,9) , ABNIN(9,9) ,
7 SIGMAX(100) , SIGMAY(100) , ELSTIF(18,18) ,
8 TAUXY(100) , ELSSM(9,9) , MFX(100,8) , IMEX(100) ,
9 ELINR(18,18) , ELMIM(6,6) , ELBIM(9,9) , ALEAN(50)
DIMENSION NUP(100) , NCHB(50)
REAL TITLE (18)
1 WRITE (6,5)
5 FORMAT (1H1/38H0INDUCER VIBRATION PROGRAM - DECK 6140 //)
CALL DATE (BMONTH,DAY,YEAR)
WRITE (6,7) BMONTH,DAY,YEAR
7 FORMAT (6H DATE ,A2,1H/,A2,1H/,A2//)
10 READ (5,15,END=50) NT,TITLE
15 FORMAT (11,18A4)
WRITE (6,20) TITLE
20 FORMAT (5X,18A4 /)
IF ( NT .GT. 0 ) GO TO 10
READ (5,25) RHO,POISSO,YOUNGS,RADGEN,NGENLI,LINE1,MODE,IPRINT,G
25 FORMAT (2F10.0, F10.0,F10.0,2I10,2I5,F10.0)
IF ( G .EQ. 0.0 ) G = 386.4
IF ( LINE1 .GT. 0 ) READ (5,26) (NCHB(I),I=1,LINE1)
26 FORMAT (16I5)
DO 29 I = 1,50
IF ( NCHB(I) .GT. 0 ) GO TO 29
NCHB(I) = NGENLI + 1
29 CONTINUE
WRITE (6,30)RHO,G, POISSO,YOUNGS,NGENLI,LINE1,RADGEN,MODE
30 FORMAT (//10X,10H DENSITY = F6.4,5X,4HG = ,E12.4,5X,
1 18HPOISSON'S RATIO = F5.3,5X,18HYOUNG'S MODULUS = E12.4 //10X,
2 26HND. OF GENERATING LINES = I4,5X,40HND. OF SYMMETRY CHANGES REQ
3 UESTED = I3 //10X,31HGENERATOR LINE OFFSET RADIUS = F9.3 //
4 10X,24HND. OF MODES REQUESTED = I4//)
IF ( LINE1 .EQ. 0 ) GO TO 32
WRITE (6,31) (NCHB(I),I=1,LINE1)
31 FORMAT (10X,38HSYMMETRY CHANGE ABOUT GENERATOR LINES 15I5/)
KOUNT = 0
32 RHO = RHO / G
WRITE (6,5)
DO 45 I = 1,NGENLI
READ (5,35) RAPANG(I),ZGL(I),RHUB(I),RTIP(I),THHUB(I),THTIP(I),
1 NUP(I) , ALEAN(I)
35 FORMAT (6F10.0,15,5X,F10.0)
WRITE (6,39) I
39 FORMAT (30X,22HGENERATOR LINE NUMBER I3,5X,16H(ANGLES IN DEG.) //)
WRITE (6,40) RAPANG(I),ZGL(I),RHUB(I),RTIP(I),THHUB(I),THTIP(I),
1 ALEAN(I) , NUP(I)
40 FORMAT (
. 10X,13HWRAP ANGLE = F12.6
1,5X, 7HZHUB = F8.4,5X,13HHUB RADIUS = F8.4,5X,13HTIP RADIUS
2 = F8.4/ 5X,16HHUB THICKNESS = F7.4,5X,16HTIP THICKNESS = F7.4,5X,
3 12HLEAN ANGLE = F12.6, 5X,16HND. OF POINTS = I2//)

```

```

INPUT001
INPUT002
INPUT003
INPUT004
INPUT005
INPUT006
INPUT007
INPUT008
INPUT009
INPUT010
INPUT011
INPUT012
INPUT013
INPUT014
INPUT015
INPUT016
INPUT017
INPUT018
INPUT019
INPUT020
INPUT021
INPUT022
INPUT023
INPUT024
INPUT025
INPUT026
INPUT027
INPUT028
INPUT029
INPUT030
INPUT031
INPUT032
INPUT033
INPUT034
INPUT035
INPUT036
INPUT037
INPUT038
INPUT039
INPUT040
INPUT041
INPUT042
INPUT043
INPUT044
INPUT045
INPUT046
INPUT047
INPUT048
INPUT049
INPUT050
INPUT051
INPUT052
INPUT053
INPUT054
INPUT055
INPUT056
INPUT057

```

```
KOUNT = KOUNT + 1
IF (KOUNT .EQ.11) WRITE (6,5)
IF (KOUNT .EQ.11) KOUNT = 0
ALEAN(I) = ALEAN(I) * 0.0174533
45  RAPANG(I) = RAPANG(I) * 0.0174533
GO TO 55
50  STOP
55  RETURN
END
```

```
INPUT058
INPUT059
INPUT060
INPUT061
INPUT062
INPUT063
INPUT064
INPUT065
INPUT066
```



```

SUBROUTINE GEOM ( NUP,NCHB,IPOS,IGEN )
C TRIANGULATION OF INDUCER BLADE AND DETERMINATION OF THICKNESS AT
C EACH VERTEX AND PRESSURE ON EACH TRIANGLE .
C
COMMON X ( 100 ) , Y ( 100 ) , Z ( 100 ) , TH ( 100 ) ,GEOM0010
1 XL ( 100,3 ) , YL ( 100,3 ) , GEOM0020
2 RAPANG( 50 ) , ZGL ( 50 ) , RHUB ( 50 ) , RTIP ( 50 ) ,GEOM0030
3 THHUB ( 50 ) , THTIP ( 50 ) , EDCM ( 3,3 ) ,GEOM0040
4 RHD , POISSD , YOUNGS , RADGEN , GEOM0050
5 NGENLI , LINE1 , NEXT ( 100,3 ) , NP , NT , GEOM0060
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) , GEOM0070
7 SIGMAX(100) , SIGMAY(100) , ELSTIF(18,18) , GEOM0080
8 TAUXY(100) , ELSSM(9,9) , MEX(100,8) , IMEX(100) , GEOM0090
9 ELINR(18,18) , ELMIM(6,6) , ELBIM(9,9) ; ALEAN(50) GEOM0100
DIMENSION NUP(100) , NCHB(50) , IPOS(100) , IGEN(100) GEOM0110
ICHB = 1 GEOM0120
KOUNT = -1 GEOM0130
IPOS(1) = -1 GEOM0140
NP1 = 1 GEOM0150
NT = 0 GEOM0160
NP = NUP(1) GEOM0170
NS = NGENLI - 1 GEOM0180
DO 90 I = 1,NS GEOM0190
NT1 = NUP(I) + NUP(I+1) -2 GEOM0200
IF ( I .NE. 1 ) GO TO 15 GEOM0210
LINE = NUP(I) GEOM0220
DR = 1.0 GEOM0230
IF ( LINE .EQ. 1 ) GO TO 1 GEOM0240
DR = ( RTIP(I) - RHUB(I) ) / FLOAT( LINE - 1 ) GEOM0250
1 RADIUS = RHUB(I) - DR GEOM0260
SINA = SIN( RAPANG(I) ) GEOM0270
COSA = COS( RAPANG(I) ) GEOM0280
TANL = TAN ( ALEAN(I) ) GEOM0290
C GEOM0300
DO 10 J = 1,LINE GEOM0310
IF ( J .EQ. 1 ) GO TO 5 GEOM0320
KOUNT = KOUNT + 1 GEOM0330
IPOS(J) = KOUNT GEOM0340
5 RADIUS = RADIUS + DR GEOM0350
Z(J) = ZGL(I) + ( RADIUS - RHUB(I) ) * TANL GEOM0360
X(J) = RADGEN * COSA - RADIUS * SINA GEOM0370
Y(J) = RADGEN * SINA + RADIUS * COSA GEOM0380
TH(J) = THHUB(I) + ( THTIP(I) - THHUB(I) ) * ( RADIUS - RHUB(I) ) GEOM0390
1 / ( RTIP(I) - RHUB(I) ) GEOM0400
IGEN(J) = I GEOM0410
IF ( TH(J) .LT. 0.0 ) TH(J) = 0.0 GEOM0420
10 CONTINUE GEOM0430
15 LINE = NUP(I+1) GEOM0440
DR = 1.0 GEOM0441
IF ( LINE .EQ. 1 ) GO TO 16 GEOM0442
DR = ( RTIP(I+1) - RHUB(I+1) ) / FLOAT( LINE - 1 ) GEOM0443
16 RADIUS = RHUB(I+1) - DR GEOM0450
J2 = NP + 1 GEOM0460
J3 = NP + NUP(I+1) GEOM0470
IPOS(J2) = -1 GEOM0480
SINA = SIN( RAPANG(I+1) ) GEOM0490
COSA = COS( RAPANG(I+1) ) GEOM0500
TANL = TAN( ALEAN(I+1) ) GEOM0510
GEOM0520

```

	DO 25 J = J2,J3	GEOM0530
	IF ( J .EQ. J2 ) GO TO 20	GEOM0540
	KOUNT = KOUNT + 1	GEOM0550
	IPOS(J) = KOUNT	GEOM0560
20	RADIUS = RADIUS + DR	GEOM0570
	Z(J) = ZGL(I+1) + ( RADIUS - RHUB(I+1) ) * TANL	GEOM0580
	X(J) = RADGEN * COSA - RADIUS * SINA	GEOM0590
	Y(J) = RADGEN * SINA + RADIUS * COSA	GEOM0600
	TH(J) = THHUB(I+1) + ( THTIP(I+1) - THHUB(I+1) ) * ( RADIUS -	GEOM0610
	1 KHUB(I+1) ) / ( RTIP(I+1) - RHUB(I+1) )	GEOM0620
	IGEN(J) = I + 1	GEOM0621
	IF ( TH(J) .LT. 0.0 ) TH(J) = 0.0	GEOM0630
25	CONTINUE	GEOM0640
	J1 = NT + 1	GEOM0650
	J2 = NT + NT1	GEOM0660
	NB = 0	GEOM0670
	K = 0	GEOM0671
	NB1 = -2	GEOM0672
	NPT1 = NUP(I)	GEOM0673
	NPT2 = NUP(I+1)	GEOM0674
	IF (NPT1 .EQ. NPT2) GO TO 27	GEOM0675
	IF (NPT2 - NPT1 .EQ. 1) GO TO 275	GEOM0676
	IF (NPT1 - NPT2 .EQ. 1) GO TO 270	GEOM0677
	IF (NPT2 - NPT1 .GT. 1) GO TO 265	GEOM0678
C	BOTTOM GENERATOR HAS AT LEAST TWO MORE NODES THAN THE TOP	GEOM0679
C	GENERATOR.	GEOM0680
	DO 264 J = J1,J2	GEOM0681
	K = K + 1	GEOM0682
	L = MOD(K,3)	GEOM0683
	IF (L .EQ. 0) L =	GEOM0684
	GO TO (261, 262, 263), L	GEOM0685
261	NB1 = NB1 + 2	GEOM0686
	NEXT(J,1) = NP1 + NB1	GEOM0687
	NEXT(J,2) = NP1 + NB1 + 1	GEOM0688
	NEXT(J,3) = NP + NB1 / 2 + 1	GEOM0689
	GO TO 264	GEOM0690
262	NEXT(J,1) = NEXT(J-1,3)	GEOM0691
	NEXT(J,2) = NEXT(J,1) + 1	GEOM0692
	NEXT(J,3) = NEXT(J-1,2)	GEOM0693
	GO TO 264	GEOM0694
263	NEXT(J,1) = NEXT(J-1,3)	GEOM0695
	NEXT(J,2) = NEXT(J,1) + 1	GEOM0696
	NEXT(J,3) = NEXT(J-1,2)	GEOM0697
264	CONTINUE	GEOM0698
	GO TO 85	GEOM0699
C	TOP GENERATOR HAS AT LEAST TWO MORE NODES THAN	GEOM0700
C	THE BOTTOM GENERATOR.	GEOM0701
265	DO 269 J = J1, J2	GEOM0702
	K = K + 1	GEOM0703
	L = MOD(K,3)	GEOM0704
	IF (L .EQ. 0) L = 3	GEOM0705
	GO TO (266,267,268), L	GEOM0706
266	NB1 = NB1 + 2	GEOM0707
	NEXT(J,1) = NP + NB1 + 1	GEOM0708
	NEXT(J,2) = NP + NB1 + 2	GEOM0709
	NEXT(J,3) = NP1 + NB1 / 2	GEOM0710
	GO TO 269	GEOM0711
267	NEXT(J,1) = NEXT(J-1,3)	GEOM0712

	NEXT(J,2) = NEXT(J,1) + 1	GEOM0713
	NEXT(J,3) = NEXT(J-1,2)	GEOM0714
	GO TO 269	GEOM0715
268	NEXT(J,1) = NEXT(J-1,3)	GEOM0716
	NEXT(J,2) = NEXT(J,1) + 1	GEOM0717
	NEXT(J,3) = NEXT(J-1,2)	GEOM0718
269	CONTINUE	GEOM0719
	GO TO 85	GEOM0720
C	BOTTOM GENERATOR HAS ONE MORE NODE THAN THE TOP GENERATOR.	GEOM0721
270	NEXT(J1,1) = NP1	GEOM0722
	NEXT(J1,2) = NP1 + 1	GEOM0723
	NEXT(J1,3) = NP + 1	GEOM0724
	IF (J1 .EQ. J2) GO TO 85	GEOM0725
	J11 = J1 + 1	GEOM0726
	DO 271 J = J11, J2	GEOM0727
	NEXT(J,1) = NEXT(J-1,3)	GEOM0728
	NEXT(J,2) = NEXT(J,1)+1	GEOM0729
271	NEXT(J,3) = NEXT(J-1,2)	GEOM0730
	GO TO 85	GEOM0731
C	TOP GENERATOR HAS ONE MORE NODE THAN THE BOTTOM GENERATOR.	GEOM0732
275	NEXT(J1,1) = NP + 1	GEOM0733
	NEXT(J1,2) = NP + 2	GEOM0734
	NEXT(J1,3) = NP1	GEOM0735
	IF (J1 .EQ. J2) GO TO 85	GEOM0736
	J11 = J1 + 1	GEOM0737
	DO 276 J = J11, J2	GEOM0738
	NEXT(J,1) = NEXT(J-1,3)	GEOM0739
	NEXT(J,2) = NEXT(J,1)+1	GEOM0740
276	NEXT(J,3) = NEXT(J-1,2)	GEOM0741
	GO TO 85	GEOM0742
C	SAME NUMBER OF NODES ON TOP AND BOTTOM GENERATORS .	GEOM0743
27	IF ( RADGEN .NE. 0.0 ) GO TO 55	GEOM0744
	IF ( NCHB(ICHB) .EQ. 1 ) GO TO 40	GEOM0745
	IF ( ICHB .GE. 2 ) GO TO 42	GEOM0746
28	DO 35 J = J1, J2	GEOM0747
	K = J - J1 + 1	GEOM0748
	IF ( MOD(K,2) .EQ. 0 ) GO TO 30	GEOM0749
	NB = NB + 1	GEOM0750
	NEXT(J,1) = NP + NB	GEOM0751
	NEXT(J,2) = NP + NB + 1	GEOM0760
	NEXT(J,3) = NP1 + NB - 1	GEOM0770
	GO TO 35	GEOM0780
30	NEXT(J,1) = NP1 + NB - 1	GEOM0790
	NEXT(J,2) = NP1 + NB	GEOM0800
	NEXT(J,3) = NP + NB + 1	GEOM0810
35	CONTINUE	GEOM0820
	GO TO 85	GEOM0830
40	ICHB = ICHB + 1	GEOM0840
42	IF ( MOD(ICHB,2) .EQ. 1 ) GO TO 28	GEOM0850
	DO 50 J = J1, J2	GEOM0860
	K = J - J1 + 1	GEOM0870
	IF ( MOD(K,2) .EQ. 0 ) GO TO 45	GEOM0880
	NB = NB + 1	GEOM0890
	NEXT(J,1) = NP1 + NB - 1	GEOM0900
	NEXT(J,2) = NP1 + NB	GEOM0910
	NEXT(J,3) = NP + NB	GEOM0920
	GO TO 50	GEOM0930
45	NEXT(J,1) = NP + NB	GEOM0940

	NEXT(J,2) = NP + NB + 1	GEOM0950
	NEXT(J,3) = NP1 + NB	GEOM0960
50	CONTINUE	GEOM0970
	GO TO 85	GEOM0980
55	IF ( NCHB(ICHB) .EQ. 1 ) GO TO 70	GEOM0990
	IF ( ICHB .GE. 2 ) GO TO 72	GEOM1010
58	DO 65 J = J1,J2	GEOM1020
	K = J - J1 + 1	GEOM1030
	IF ( MOD(K,2) .EQ. 0 ) GO TO 60	GEOM1040
	NB = NB + 1	GEOM1050
	NEXT(J,1) = NP1 + NB - 1	GEOM1060
	NEXT(J,2) = NP1 + NB	GEOM1070
	NEXT(J,3) = NP + NB	GEOM1080
	GO TO 65	GEOM1090
60	NEXT(J,1) = NP + NB	GEOM1100
	NEXT(J,2) = NP + NB + 1	GEOM1110
	NEXT(J,3) = NP1 + NB	GEOM1120
65	CONTINUE	GEOM1130
	GO TO 85	GEOM1140
70	ICHB = ICHB + 1	GEOM1150
72	IF ( MOD(ICHB,2) .EQ. 1 ) GO TO 58	GEOM1160
	DO 80 J = J1,J2	GEOM1170
	K = J - J1 + 1	GEOM1180
	IF ( MOD(K,2) .EQ. 0 ) GO TO 75	GEOM1190
	NB = NB + 1	GEOM1200
	NEXT(J,1) = NP + NB	GEOM1210
	NEXT(J,2) = NP + NB + 1	GEOM1220
	NEXT(J,3) = NP1 + NB - 1	GEOM1230
	GO TO 80	GEOM1240
75	NEXT(J,1) = NP1 + NB - 1	GEOM1250
	NEXT(J,2) = NP1 + NB	GEOM1260
	NEXT(J,3) = NP + NB + 1	GEOM1270
80	CONTINUE	GEOM1280
85	CONTINUE	GEOM1290
	NP1 = NP + 1	GEOM1300
	NP = NP + NUP(I+1)	GEOM1310
	NT = NT + NT1	GEOM1320
	IF ( NP .LE. 100 ) GO TO 87	GEOM1330
	WRITE (6,86)	GEOM1340
86	FORMAT (//20X,35HMORE THAN 100 POINTS WERE GENERATED )	GEOM1350
	RETURN	GEOM1360
87	IF ( NT .LE. 100 ) GO TO 90	GEOM1370
	WRITE (6,88)	GEOM1380
88	FORMAT (//20X,37HMORE THAN 100 ELEMENTS WERE GENERATED )	GEOM1390
	RETURN	GEOM1400
90	CONTINUE	GEOM1410
	NP1 = NP - NGENLI	GEOM1411
	IF ( NP1 .LE. 50 ) GO TO 100	GEOM1412
	NP = 150	GEOM1413
	WRITE (6,95)	GEOM1414
95	FORMAT (//20X,38HMORE THAN 50 FREE NODES WERE GENERATED )	GEOM1415
100	RETURN	GEOM1420
	END	GEOM1430

```

SUBROUTINE DIRCOS (LA, LB, LC, I)                                DIRCOS01
C  CALCULATE THE DIRECTION COSINE MATRIX (EDCM) OF ELEMENT LOCAL AXES DIRCOS02
C  (XL, YL, ZL) RELATIVE TO COMMON AXES (X, Y, Z) .           DIRCOS03
C                                                                DIRCOS04
COMMON X ( 100) , Y ( 100) , Z ( 100) , TH ( 100) , DIRCOS05
1 XL ( 100,3) , YL ( 100,3) , ZL ( 100,3) , DIRCOS06
2 RAPANG( 50) , ZGL ( 50) , RHUB ( 50) , RTIP ( 50) , DIRCOS07
3 THHUB ( 50) , TH TIP ( 50) , FDCM ( 3,3) , DIRCOS08
4 RHO , PUISSO , YOUNGS , RADGEN , DIRCOS09
5 NGENLI , LINE1 , NEXT ( 100,3) , NP , NT , DIRCOS10
DOUBLE PRECISION L12 , S1X , S1Y , S1Z , S1 , S2X , S2Y , S2Z , DIRCOS11
1 S2 , DIRCOS12
L12 = SQRT( (X(LB)-X(LA))**2 + (Y(LB)-Y(LA))**2 + (Z(LB)-Z(LA))**2) DIRCOS13
S1X = (Y(LB)-Y(LA)) * (Z(LC)-Z(LA)) - (Y(LC)-Y(LA)) * (Z(LB)-Z(LA)) DIRCOS14
S1Y = (Z(LB)-Z(LA)) * (X(LC)-X(LA)) - (Z(LC)-Z(LA)) * (X(LB)-X(LA)) DIRCOS15
S1Z = (X(LB)-X(LA)) * (Y(LC)-Y(LA)) - (X(LC)-X(LA)) * DIRCOS16
1 (Y(LB)-Y(LA)) DIRCOS17
SIGN = 1.0 DIRCOS18
IF ( LC .LT. LB ) SIGN = -1.0 DIRCOS19
5 S1X = S1X * SIGN DIRCOS20
S1Y = S1Y * SIGN DIRCOS21
S1Z = S1Z * SIGN DIRCOS22
10 S1 = DSQRT( S1X**2 + S1Y**2 + S1Z**2 ) DIRCOS23
S2X = S1Y * (Z(LB) - Z(LA)) - S1Z * (Y(LB) - Y(LA)) DIRCOS24
S2Y = S1Z * (X(LB) - X(LA)) - S1X * (Z(LB) - Z(LA)) DIRCOS25
S2Z = S1X * (Y(LB) - Y(LA)) - S1Y * (X(LB) - X(LA)) DIRCOS26
S2 = DSQRT( S2X**2 + S2Y**2 + S2Z**2 ) DIRCOS27
EDCM(1,1) = (X(LB) - X(LA)) / L12 DIRCOS28
EDCM(2,1) = (Y(LB) - Y(LA)) / L12 DIRCOS29
FDCM(3,1) = ( Z(LB) - Z(LA) ) / L12 DIRCOS30
EDCM(1,2) = S2X / S2 DIRCOS31
EDCM(2,2) = S2Y / S2 DIRCOS32
EDCM(3,2) = S2Z / S2 DIRCOS33
EDCM(1,3) = S1X / S1 DIRCOS34
EDCM(2,3) = S1Y / S1 DIRCOS35
EDCM(3,3) = S1Z / S1 DIRCOS36
RETURN DIRCOS37
END DIRCOS38

```

```

SUBROUTINE LCOORD (LA, LB, LC, I)                                LCOORD01
C   DETERMINE LOCAL NODAL COORDINATES (XL, YL, ZL) OF TRIANGULAR ELEMENT LCOORD02
C   FROM COMMON NODAL COORDINATES (X, Y, Z) .                  LCOORD03
C                                                                LCOORD04
COMMON X      ( 100) , Y      ( 100) , Z      ( 100) , TH      ( 100) , LCOORD05
1      XL ( 100,3) , YL ( 100,3) ,                               LCOORD06
2      RAPANG( 50) , ZGL ( 50) , RHUB ( 50) , RTIP ( 50) , LCOORD07
3      THHUB ( 50) , THTIP ( 50) ,                               EDCM ( 3,3) , LCOORD08
4      RHO , POISSO , YOUNGS , RADGEN ,                          LCOORD09
5      NGENLI , LINE1 , NEXT ( 100,3) , NP , NT                LCOORD10
XL(I,2)= EDCM(1,1) * (X(LB) - X(LA)) + EDCM(2,1) * (Y(LB) - Y(LA)) LCOORD11
1      +EDCM(3,1) * (Z(LB) - Z(LA))                               LCOORD12
XL(I,3)= EDCM(1,1) * (X(LC) - X(LA)) + EDCM(2,1) * (Y(LC) - Y(LA)) LCOORD13
1      +EDCM(3,1) * (Z(LC) - Z(LA))                               LCOORD14
YL(I,3)= EDCM(1,2) * (X(LC) - X(LA)) + EDCM(2,2) * (Y(LC) - Y(LA)) LCOORD15
1      +EDCM(3,2) * (Z(LC) - Z(LA))                               LCOORD16
RETURN                                             LCOORD17
END                                               LCOORD18

```

```

SUBROUTINE MEMSTF ( LAA,LBB,LCC,IE ) MEMST101
CALCULATE THE LOCAL MEMBRANE STIFFNESS MATRIX (ELMSM) FOR A MEMST102
TRIANGULAR ELEMENT . MEMST103
C MEMST104
C MEMST105
C MEMST106
COMMON X ( 100) , Y ( 100) , Z ( 100) , TH ( 100) , MEMST107
1 XLL ( 100,3) , YLL ( 100,3) , MEMST108
2 RAPANG( 50) , ZGL ( 50) , RHUB ( 50) , RTIP ( 50) , MEMST109
3 THHUB ( 50) , THTIP ( 50) , EDCM ( 3,3) , MEMST110
4 RHO , POISSO , YOUNGS , RADGEN , MEMST111
5 NGENL1 , LINE1 , NEXT ( 100,3) , NP , NT , MEMST112
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) MEMST113
DIMENSION AMNIT(6,6) , WM(3,6) , WMT(6,3) , EM(3,3) , MEMST114
1 TN(6,1) , ZINT (1,6) , Z1(6,6) , Z2 (6,6) MEMST115
DIMENSION YL(3) , XL(3) MEMST116
DOUBLE PRECISION ZINT , XL , YL , TERM , AMNIT , WM , WMT , EM , MEMST117
1 TN , Z1 , Z2 MEMST118
DATA LA, LB, LC / 1 , 2 , 3 / MEMST119
DATA WM / 1.000,4*0.000,1.000,2*0.000,1.000,0.000,1.000,7*0.000 / MEMST120
DATA WMT / 1.000,8*0.000,1.000,3*0.000,2*1.000,3*0.000 / MEMST121
DATA AMNIT,EM,TN / 51*0.000 / MEMST122
XL(LB) = XLL(IE,2) MEMST123
XL(LC) = XLL(IE,3) MEMST124
YL(LC) = YLL(IE,3) MEMST125
TERM = YOUNGS / ( 1.0 - POISSO**2 ) MEMST126
EM(1,1) = TERM MEMST127
EM(1,2) = TERM * POISSO MEMST128
EM(2,1) = EM(1,2) MEMST129
EM(2,2) = TERM MEMST130
EM(3,3) = ( 1.0 - POISSO ) * TERM / 2.0 MEMST131
AMNIN(1,1) = -1.0 / XL(LB) MEMST132
AMNIN(1,3) = - AMNIN(1,1) MEMST133
AMNIN(2,2) = AMNIN(1,1) MEMST134
AMNIN(2,4) = AMNIN(1,3) MEMST135
AMNIN(3,1) = ( XL(LC) - XL(LB) ) / XL(LB) / YL(LC) MEMST136
AMNIN(3,3) = - XL(LC) / XL(LB) / YL(LC) MEMST137
AMNIN(3,5) = 1.0 / YL(LC) MEMST138
AMNIN(4,2) = AMNIN(3,1) MEMST139
AMNIN(4,4) = AMNIN(3,3) MEMST140
AMNIN(4,6) = AMNIN(3,5) MEMST141
AMNIN(5,1) = 1.0 MEMST142
AMNIN(6,2) = 1.0 MEMST143
DO 10 I = 1,6 MEMST144
ZINT(1,I) = 0.0 MEMST145
DO 10 J = 1,6 MEMST146
10 AMNIT(I,J) = AMNIN(J,I) MEMST147
TN(1,1) = TH(LAA) MEMST148
TN(3,1) = TH(LBB) MEMST149
TN(5,1) = TH(LCC) MEMST150
CALL ZINT1 ( IE,ZINT ) MEMST151
DO 15 J = 1,6 MEMST152
Z1(1,J) = 0.0 MEMST153
DO 15 K = 1,6 MEMST154
15 Z1(1,J) = Z1(1,J) + ZINT(1,K) * AMNIN(K,J) MEMST155
Z2(1,1) = 0.0 MEMST156
DO 20 K = 1,6 MEMST157
20 Z2(1,1) = Z2(1,1) + Z1(1,K) * TN(K,1) MEMST158
DO 25 I = 1,6
DO 25 J = 1,3

```

	Z1(I,J) = 0.0	MEMSTI59
	DO 25 K = 1,3	MEMSTI60
25	Z1(I,J) = Z1(I,J) + Z2(I,1) * WMT(I,K) * EM(K,J)	MEMSTI61
	DO 30 I = 1,6	MEMSTI62
	DO 30 J = 1,6	MEMSTI63
	Z2(I,J) = 0.0	MEMSTI64
	DO 30 K = 1,3	MEMSTI65
30	Z2(I,J) = Z2(I,J) + Z1(I,K) * WM(K,J)	MEMSTI66
	DO 35 I = 1,6	MEMSTI67
	DO 35 J = 1,6	MEMSTI68
	Z1(I,J) = 0.0	MEMSTI69
	DO 35 K = 1,6	MEMSTI70
35	Z1(I,J) = Z1(I,J) + AMNIT(I,K) * Z2(K,J)	MEMSTI71
	DO 40 I = 1,6	MEMSTI72
	DO 40 J = 1,6	MEMSTI73
	ELMSM(I,J) = 0.0	MEMSTI74
	DO 40 K = 1,6	MEMSTI75
40	ELMSM(I,J) = ELMSM(I,J) + Z1(I,K) * AMNIN(K,J)	MEMSTI76
	RETURN	MEMSTI77
	END	MEMSTI78



```

SUBROUTINE ZINT1 ( IE,ZINT )                                ZINT1001
C USING GAUSSIAN QUADRATURE, INTEGRATE THE FOLLOWING FUNCTIONS OVER THE SURFACE OF THE TRIANGLE ZINT1002
C F(XL,YL) = 1.0                                          ZINT1003
C F(XL,YL) = XL                                           ZINT1004
C F(XL,YL) = YL                                           ZINT1005
C                                                         ZINT1006
C                                                         ZINT1007
COMMON X ( 100) , Y ( 100) , Z ( 100) , TH ( 100) , ZINT1008
1 XLL ( 100,3) , YLL ( 100,3) , ZINT1009
2 RAPANG( 50) , ZGL ( 50) , RHUB ( 50) , RTIP ( 50) , ZINT1010
3 THHUB ( 50) , THTIP ( 50) , EDCM ( 3,3) , ZINT1011
4 RHU , PUISSU , YOUNGS , RADGEN , ZINT1012
5 NGENLI , LINE1 , NEXT ( 100,3) , NP , NT , ZINT1013
6 ELMSM(6,6) , AMNIN(6,6) , ELRSM(9,9) , ABNIN(9,9) , ZINT1014
DIMENSION ZINT(1,6) , A(10) , H(10) , YI(10) , XI(10) , AREA(10) , ZINT1015
1 XIL(10) , XIR(10) , ZINT1016
DIMENSION YL(3) , XL(3) , ZINT1017
DOUBLE PRECISION YO , HT , XO , ZINT , A , H , YI , XI , AREA , ZINT1018
1 XIL , XIR , XL , YL , ZINT1019
DATA LA, LB, LC / 1 , 2 , 3 / ZINT1020
DATA A / -.97390652851717 , -.86506336668899 , -.67940956829902 , ZINT1021
1 -.43339539412925 , -.14887433898163 , -.14887433898163 , ZINT1022
2 .43339539412925 , .67940956829902 , .86506336668899 , ZINT1023
3 .97390652851717 / ZINT1024
DATA H / .06667134430869 , .14945134915058 , .21908636251598 , ZINT1025
1 .26926671930100 , .29552422471475 , .29552422471475 , ZINT1026
2 .26926671930100 , .21908636251598 , .14945134915058 , ZINT1027
3 .06667134430869 / ZINT1028
XL(LB) = XLL(IE,2) ZINT1029
XL(LC) = XLL(IE,3) ZINT1030
YL(LC) = YLL(IE,3) ZINT1031
YO = 0.5 * YL(LC) ZINT1032
DO 3 I = 1,10 ZINT1033
YI(I) = YO + A(I) * YO ZINT1034
XIL(I) = XL(LC) * YI(I) / YL(LC) ZINT1035
XIR(I) = XL(LB) - ( XL(LB) - XL(LC) ) * YI(I) / YL(LC) ZINT1036
IF ( I .NE. 1 ) GO TO 2 ZINT1037
HT = 0.0 ZINT1038
DO 1 J = 1,10 ZINT1039
HT = HT + H(J) ZINT1040
2 AREA(I) = XL(LB) * ( 1.0 - A(I) ) * 0.25 * HT ZINT1041
ZINT(1,5) = ZINT(1,5) + DABS(YL(LC)) * 0.5 * AREA(I) * H(I) ZINT1042
3 ZINT(1,3) = ZINT(1,3) + DABS(YL(LC)) * 0.5 * YI(I) * AREA(I) * H(I) ZINT1043
DO 5 I = 1,10 ZINT1044
XO = XIL(I) + 0.5 * ( XIR(I) - XIL(I) ) ZINT1045
AREA(I) = 0.0 ZINT1046
DO 4 J = 1,10 ZINT1047
XI(J) = XO + A(J) * ( XO - XIL(I) ) ZINT1048
4 AREA(I) = AREA(I) + XL(LB) * ( 1.0 - A(I) ) * 0.25 * H(J) * XI(J) ZINT1049
5 ZINT(1,1) = ZINT(1,1) + DABS(YL(LC)) * 0.5 * AREA(I) * H(I) ZINT1050
RETURN ZINT1051
END ZINT1052

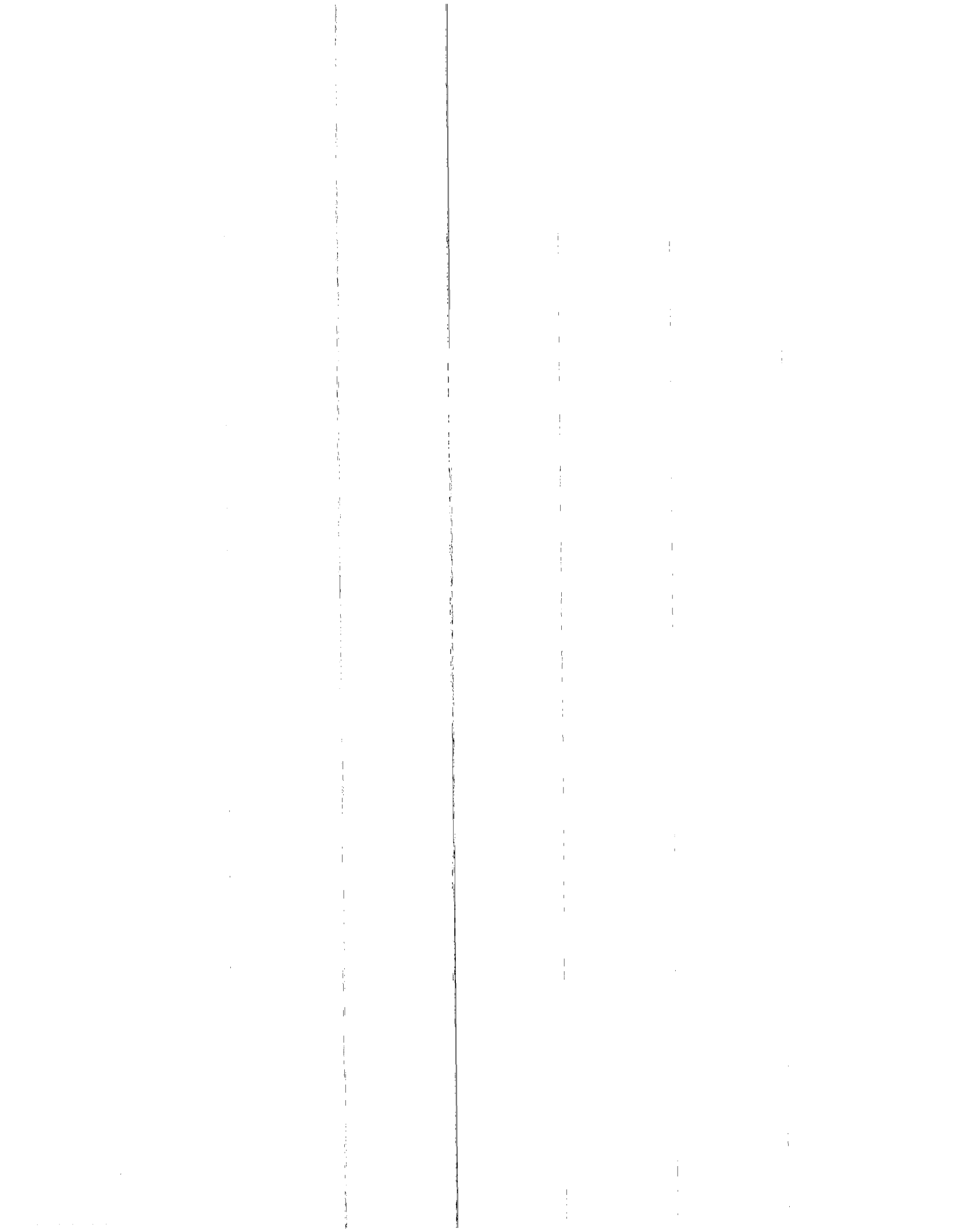
```



```

ABNIN(9,6) = 2.0 * XL(LC)**2 * ( XL(LB) - XL(LC) ) / XL(LB)**2 / YL(LC)**3 BENST059
1 ABNIN(9,7) = -2.0 / YL(LC)**3 BENST060
ABNIN(9,8) = 1.0 / YL(LC)**2 BENST061
DO 5 I = 1,9 BENST062
DO 5 J = 1,9 BENST063
ZINT(I,J) = 0.0 BENST064
5 ABNIT(I,J) = ABNIN(J,I) BENST065
CALL ZINT2 ( LAA,LBB,LCC,ZJ1,ZJ2,ZJ3,ZJ4,ZJ5,ZJ6,IE ) BENST066
ZINT(4,4) = 4.0 * ZJ1 BENST067
ZINT(4,5) = POISSO * ZINT(4,4) BENST068
ZINT(4,6) = 12.0 * ZJ2 BENST069
ZINT(4,7) = 4.0 * ZJ3 BENST070
ZINT(4,8) = 4.0 * POISSO * ZJ2 BENST071
ZINT(4,9) = POISSO * ZINT(4,7) * 3.0 BENST072
ZINT(5,5) = ZINT(4,4) BENST073
ZINT(5,6) = POISSO * ZINT(4,6) BENST074
ZINT(5,7) = POISSO * ZINT(4,7) BENST075
ZINT(5,8) = ZINT(4,8) / POISSO BENST076
ZINT(5,9) = ZINT(4,9) / POISSO BENST077
ZINT(6,6) = 36.0 * ZJ4 BENST078
ZINT(6,7) = 12.0 * ZJ5 BENST079
ZINT(6,8) = 12.0 * POISSO * ZJ4 BENST080
ZINT(6,9) = ZINT(6,7) * POISSO * 3.0 BENST081
ZINT(7,7) = 4.0 * ZJ6 + 8.0 * ( 1.0 - POISSO ) * ZJ4 BENST082
ZINT(7,8) = 4.0 * ( 2.0 - POISSO ) * ZJ5 BENST083
ZINT(7,9) = 12.0 * POISSO * ZJ6 BENST084
ZINT(8,8) = 8.0 * ( 1.0 - POISSO ) * ZJ6 + 4.0 * ZJ4 BENST085
ZINT(8,9) = 12.0 * ZJ5 BENST086
ZINT(9,9) = 36.0 * ZJ6 BENST087
DO 10 I = 4,8 BENST088
I1 = I + 1 BENST089
DO 10 J = I1,9 BENST090
10 ZINT(J,I) = ZINT(I,J) BENST091
ZJ1 = YOUNGS / ( 12.0 * ( 1.0 - POISSO**2 ) ) BENST092
DO 15 I = 4,9 BENST093
DO 15 J = 4,9 BENST094
15 ZINT(I,J) = ZINT(I,J) * ZJ1 BENST095
DO 20 I = 1,9 BENST096
DO 20 J = 1,9 BENST097
Z1(I,J) = 0.0 BENST098
DO 20 K = 1,9 BENST099
20 Z1(I,J) = Z1(I,J) + ABNIT(I,K) * ZINT(K,J) BENST100
DO 25 I = 1,9 BENST101
DO 25 J = 1,9 BENST102
ELBSM(I,J) = 0.0 BENST103
DO 25 K = 1,9 BENST104
25 ELBSM(I,J) = ELBSM(I,J) + Z1(I,K) * ABNIN(K,J) BENST105
RETURN BENST106
END BENST107
BENST108

```



```

2      + XL(LB)*TH(LCC)*YI(I)**3 * XL(LB)*( 1.0 - A(I) ) * 0.25 ZINT2059
3      * H(J) / XL(LB)**3 / YL(LC)**3 ZINT2060
AREA(I,1) = AREA(I,1) + TERM ZINT2061
AREA(I,2) = AREA(I,2) + TERM * XI(J) ZINT2062
AREA(I,3) = AREA(I,3) + TERM * YI(I) ZINT2063
AREA(I,4) = AREA(I,4) + TERM * XI(J)**2 ZINT2064
AREA(I,5) = AREA(I,5) + TERM * XI(J) * YI(I) ZINT2065
3 AREA(I,6) = AREA(I,6) + TERM * YI(I)**2 ZINT2066
ZJ1 = ZJ1 + 0.5 * H(I) * AREA(I,1)*DABS(YL(LC)) ZINT2067
ZJ2 = ZJ2 + 0.5 * H(I) * AREA(I,2)*DABS(YL(LC)) ZINT2068
ZJ3 = ZJ3 + 0.5 * H(I) * AREA(I,3)*DABS(YL(LC)) ZINT2069
ZJ4 = ZJ4 + 0.5 * H(I) * AREA(I,4) *DABS(YL(LC)) ZINT2070
ZJ5 = ZJ5 + 0.5 * H(I) * AREA(I,5) *DABS(YL(LC)) ZINT2071
4 ZJ6 = ZJ6 + 0.5 * H(I) * AREA(I,6) *DABS(YL(LC)) ZINT2072
RETURN ZINT2073
END ZINT2074

```

```

SUBROUTINE MEMINR (LAA,LBB,LCC,IE)
C CALCULATE THE LOCAL MEMBRANE INERTIA
C MATRIX (ELMIM) FOR A TRIANGULAR
C ELEMENT.
C
COMMON X ( 100) , Y ( 100) , Z ( 100) , ( 100) ,
1 XLL ( 100,3) , YLL ( 100,3) ,
2 RAPANG( 50) , ZGL ( 50) , RHUB ( 50) , RTIP ( 50) ,
3 THHUB ( 50) , THTIP ( 50) , EDCM ( 3,3) ,
4 RHO , POISSD , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NEXT ( 100,3) , NP , NT ,
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,
7 SIGMAX(100) , SIGMAY(100) , ELSTIF(18,18) ,
8 TAUXY(100) , ELSSM(9,9) , MEX(100,8) , IMEX(100) ,
9 ELINR(18,18) , ELMIM(6,6) , ELBIM(9,9)
DIMENSION AMNIT(6,6) , R1(6,6) , A(10) , H(10) , YI(10) ,
IXI(10) , AREA(10,6) , XIL(10) , XIR(10) , XL(3) , YL(3) ,
ZZINT(6) , R2(6,6)
DOUBLE PRECISION YD , XD , TERM1 , AMNIT , R1 , A , H , YI ,
1 XL , YL , ZINT , R2
DATA LA, LB, LC / 1,2,3 /
DATA A / -.97390652851717 , -.86506336668899 , -.67940956829902 ,
1 -.43339539412925 , -.14887433898163 , .14887433898163 ,
2 .4333739412925 , .67940956829902 , .86506336668899 ,
3 .97390652851717 /
DATA H / .06667134430869 , .14945134915058 , .21908636251598 ,
1 .26926671930100 , .29552422471475 , .29552422471475 ,
2 .26926671930100 , .21908636251598 , .14945134915058 ,
3 .06667134430869 /
XL(LB) = XLL(IE,2)
XL(LC) = XLL(IE,3)
YL(LC) = YLL(IE,3)
DO 10 I = 1,6
ZINT(I) = 0.0
DO 10 J = 1,6
R1(I,J) = 0.0
R2(I,J) = 0.0
ELMIM(I,J) = 0.0
10 AMNIT(I,J) = AMNIN(J,I)
C USING GAUSSIAN QUADRATURE, INTEGRATE THE FOLLOWING FUNCTIONS OVER
C THE SURFACE OF THE TRIANGLE
C F(XL,YL) = TERM
C F(XL,YL) = TERM * XL
C F(XL,YL) = TERM * YL
C F(XL,YL) = TERM * XL*YL
C F(XL,YL) = TERM * XL**2
C F(XL,YL) = TERM * YL**2
C WHERE
C TERM = ((XL(LB)*YL(LC) + (XL(LC)-XL(LB))*YL - YL(LC)*XL*TH(LAA) -
C (XL(LC)*YL - YL(LC)*XL)*TH(LBB) + XL(LB)*TH(LCC)*YL)/XL(LB)
C
YD = 0.50 * YL(LC)
DO 35 I = 1,10
YI(I) = YD + A(I)*YD
XIL(I) = XL(LC)*YI(I) / YL(LC)
XIR(I) = XL(LB) - (XL(LB) - XL(LC))*YI(I) / YL(LC)
XD = XIL(I) + 0.5*(XIR(I)-XIL(I))
DO 20 J = 1,10
DO 15 K = 1,6
MEMIN001
MEMIN002
MEMIN003
MEMIN004
MEMIN005
MEMIN006
MEMIN007
MEMIN008
MEMIN009
MEMIN010
MEMIN011
MEMIN012
MEMIN013
MEMIN014
MEMIN015
MEMIN016
MEMIN017
MEMIN018
MEMIN019
MEMIN020
MEMIN021
MEMIN022
MEMIN023
MEMIN024
MEMIN025
MEMIN026
MEMIN027
MEMIN028
MEMIN029
MEMIN030
MEMIN031
MEMIN032
MEMIN033
MEMIN034
MEMIN035
MEMIN036
MEMIN037
MEMIN038
MEMIN039
MEMIN040
MEMIN041
MEMIN042
MEMIN043
MEMIN044
MEMIN045
MEMIN046
MEMIN047
MEMIN048
MEMIN049
MEMIN050
MEMIN051
MEMIN052
MEMIN053
MEMIN054
MEMIN055
MEMIN056
MEMIN057
MEMIN058

```

15	AREA(J,K) = 0.0	MEMIN056
20	XI(J) = XO + A(J)*(XO-XIL(I))	MEMIN060
	DO 25 J = 1,10	MEMIN061
	TFRM1 = XL(LB)*(1.0-A(I))*0.25*H(J)*((XL(LB)*YL(LC)	MEMIN062
1	+ (XL(LC)-XL(LB))*YI(I)-YL(LC)*XI(J))*TH(LAA)	MEMIN063
2	+ (YL(LC)*XI(J)-XL(LC)*YI(I))*TH(LBB)+XL(LB)*TH(LCC)	MEMIN064
3	*YI(I)/XL(LB)/YL(LC)	MEMIN065
	AREA(I,1) = AREA(I,1) + TERM1	MEMIN066
	AREA(I,2) = AREA(I,2) + TERM1*XI(J)	MEMIN067
	AREA(I,3) = AREA(I,3) + TERM1*YI(I)	MEMIN068
	AREA(I,4) = AREA(I,4) + TERM1*XI(J)*YI(I)	MEMIN069
	AREA(I,5) = AREA(I,5) + TERM1*XI(J)**2	MEMIN070
	AREA(I,6) = AREA(I,6) + TERM1*YI(I)**2	MEMIN071
25	CONTINUE	MEMIN072
	TERM1 = DABS( YL(LC) ) * 0.5 * H(I)	MEMIN073
	DO 30 J = 1,6	MEMIN074
30	ZINT(J) = ZINT(J) + TERM1*AREA(I,J)	MEMIN075
35	CONTINUE	MEMIN076
C	END OF INTEGRATION	MEMIN077
	R2(1,1) = ZINT(5)*RHO	MEMIN078
	R2(1,3) = ZINT(4)*RHO	MEMIN079
	R2(1,5) = ZINT(2)*RHO	MEMIN080
	R2(2,2) = R2(1,1)	MEMIN081
	R2(2,4) = R2(1,3)	MEMIN082
	R2(2,6) = R2(1,5)	MEMIN083
	R2(3,3) = ZINT(6)*RHO	MEMIN084
	R2(3,5) = ZINT(3)*RHO	MEMIN085
	R2(4,4) = R2(3,3)	MEMIN086
	R2(4,6) = R2(3,5)	MEMIN087
	R2(5,5) = ZINT(1)*RHO	MEMIN088
	R2(6,6) = R2(5,5)	MEMIN089
	DO 40 I = 1,5	MEMIN090
	I1 = I+1	MEMIN091
	DO 40 J = I1,6	MEMIN092
40	R2(J,I) = R2(I,J)	MEMIN093
	DO 45 I = 1,6	MEMIN094
	DO 45 J = 1,6	MEMIN095
	DO 45 K = 1,6	MEMIN096
45	R1(I,J) = R1(I,J) + AMNIT(I,K)*R2(K,J)	MEMIN097
	DO 50 I = 1,6	MEMIN098
	DO 50 J = 1,6	MEMIN099
	DO 50 K = 1,6	MEMIN100
50	ELMIM(I,J) = ELMIM(I,J) + R1(I,K)*AMNIN(K,J)	MEMIN101
	RETURN	MEMIN102
	END	MEMIN103

```

SUBROUTINE BENI4R (LAA, LBB, LCC, IE)                                BENIN001
CALCULATE THE LOCAL BENDING INERTIA MATRIX (ELBIM) FOR A          BENIN002
TRIANGULAR ELEMENT.                                              BENIN003
                                                                    BENIN004
COMMON X      ( 100) , Y      ( 100) , Z      ( 100) , TH      ( 100) , BENIN005
1      XLL ( 100,3) , YLL ( 100,3) ,                                BENIN006
2      RAPANG( 50) , ZGL      ( 50) , RHUB      ( 50) , RTIP      ( 50) , BENIN007
3      THHUB ( 50) , THHIP ( 50) ,                ECCM      ( 3,3) , BENIN008
4      RHO ,                POISSO , YOUNGS , RADGEN ,                BENIN009
5      NGENLI , LINE1 ,                NFXT ( 100,3) , NP , NT ,                BENIN010
6      ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,                BENIN011
7      SIGMAX(100) , SIGMAY(100) , ELSTIF(18,18) ,                BENIN012
8      TAUXY(100) , ELSSM(9,9) , MEX(100,8) , IMEX(100) ,                BENIN013
9      ELINR(18,18) ,                ELMIM(6,6) , ELBIM(9,9)                BENIN014
DIMENSION ABNIT(9,9) , R1(9,9) , R2(9,9) , A(10) , H(10) , YI(10) , BENIN015
1      XI(10) , AREA(10,28) , XIL(10) , XIR(10) , XL(3) , YL(3) , BENIN016
2      ZINT(28) ;                                                  BENIN017
DOUBLE PRECISION YO , XO , TERMI , ABNIT , R1 , R2 , A , H , BENIN018
1      YI , XI , AREA , XIL , XIR , XL , YL , ZINT                BENIN019
DATA LA , LB , LC / 1,2,3 /                                       BENIN020
DATA A / -.97390652851717 , -.86506336668899 , -.67940956829902 , BENIN021
1      -.43339539412925 , -.14887433898163 , .14887433898163 , BENIN022
2      .43339539412925 , .67940956829902 , .86506336668899 , BENIN023
3      .97390652851717 /                                       BENIN024
DATA H / .06667134430869 , .14945134915058 , .21908636251598 , BENIN025
1      .26926671930100 , .2952422471475 , .2952422471475 , BENIN026
2      .26926671930100 , .21908636251598 , .14945134915058 , BENIN027
3      .06667134430869 /                                       BENIN028
XL(LB) = XLL(IE,2)                                               BENIN029
XL(LC) = XLL(IE,3)                                               BENIN030
YL(LC) = YLL(IE,3)                                               BENIN031
DO 10 I = 1,9                                                    BENIN032
DO 10 J = 1,9                                                    BENIN033
R1(I,J) = 0.0                                                    BENIN034
R2(I,J) = 0.0                                                    BENIN035
ELBIM(I,J) = 0.0                                                BENIN036
10 ABNIT(I,J) = ABNIN(J,I)                                       BENIN037
DO 15 I = 1,28                                                  BENIN038
15 ZINT(I) = 0.0                                                BENIN039
C USING GAUSSIAN QUADRATURE, INTEGRATE THE FOLLOWING FUNCTIONS   BENIN040
C OVER THE SURFACE OF THE TRIANGLE.                               BENIN041
C      F(XL,YL) = TERM                                           BENIN042
C      F(XL,YL) = TERM * YL                                       BENIN043
C      F(XL,YL) = TERM * YL**2                                     BENIN044
C      F(XL,YL) = TERM * YL**3                                     BENIN045
C      F(XL,YL) = TERM * YL**4                                     BENIN046
C      F(XL,YL) = TERM * YL**5                                     BENIN047
C      F(XL,YL) = TERM * YL**6                                     BENIN048
C      F(XL,YL) = TERM * XL                                       BENIN049
C      F(XL,YL) = TERM * XL**2                                     BENIN050
C      F(XL,YL) = TERM * XL**3                                     BENIN051
C      F(XL,YL) = TERM * XL**4                                     BENIN052
C      F(XL,YL) = TERM * XL**5                                     BENIN053
C      F(XL,YL) = TERM * XL**6                                     BENIN054
C      F(XL,YL) = TERM * XL * YL                                   BENIN055
C      F(XL,YL) = TERM * XL * YL**2                               BENIN056
C      F(XL,YL) = TERM * XL * YL**3                               BENIN057
C      F(XL,YL) = TERM * XL * YL**4                               BENIN058

```



```

C          F(XL,YL) = TERM * XL * YL**5                      BENIN059
C          F(XL,YL) = TERM * XL**2 * YL                      BENIN060
C          F(XL,YL) = TERM * XL**2 * YL**2                  BENIN061
C          F(XL,YL) = TERM * XL**2 * YL**3                  BENIN062
C          F(XL,YL) = TERM * XL**2 * YL**4                  BENIN063
C          F(XL,YL) = TERM * XL**3 * YL                      BENIN064
C          F(XL,YL) = TERM * XL**3 * YL**2                  BENIN065
C          F(XL,YL) = TERM * XL**3 * YL**3                  BENIN066
C          F(XL,YL) = TERM * XL**4 * YL                      BENIN067
C          F(XL,YL) = TERM * XL**4 * YL**2                  BENIN068
C          F(XL,YL) = TERM * XL**5 * YL                      BENIN069
C          WHERE                                              BENIN070
C          TERM = ((XL(LB)*YL(LC) + (XL(LC)-XL(LB))*YL - YL(LC)*XL*TH(LAA) -
C          (XL(LC)*YL - YL(LC)*XL)*TH(LBB) + XL(LB)*TH(LCC)*YL)/XL(LB) BENIN071
C          Y0 = 0.50 * YL(LC)                                BENIN073
C          DO 40 I = 1,10                                     BENIN074
C          YI(I) = Y0 + A(I) * YU                             BENIN075
C          XIL(I) = XL(LC) * YI(I) / YL(LC)                  BENIN076
C          XIR(I) = XL(LB) - (XL(LB) - XL(LC)) * YI(I) / YL(LC) BENIN077
C          X0 = XIL(I) + 0.5 * (XIR(I) - XIL(I))              BENIN078
C          DO 25 J = 1,10                                     BENIN079
C          DO 20 K = 1,28                                     BENIN080
C          AREA(J,K) = 0.0                                    BENIN081
C          XI(J) = X0 + A(J) * (X0 - XIL(I))                  BENIN082
C          DO 30 J = 1,10                                     BENIN083
C          TERM1 = XL(LB) * (1.0 - A(I)) * 0.25 * H(J) * ((XL(LB) * YL(LC) +
C          1 (XL(LC) - XL(LB)) * YI(I) - YL(LC) * XI(J)) * TH(LAA) + BENIN084
C          2 (YL(LC) * XI(J) - XL(LC) * YI(I)) * TH(LBB) + XL(LB) * BENIN085
C          3 TH(LCC) * YI(I))/XL(LB)/YL(LC)                    BENIN086
C          AREA(I,1) = AREA(I,1) + TERM1                     BENIN088
C          AREA(I,2) = AREA(I,2) + TERM1*YI(I)                BENIN089
C          AREA(I,3) = AREA(I,3) + TERM1*YI(I)**2            BENIN090
C          AREA(I,4) = AREA(I,4) + TERM1*YI(I)**3            BENIN091
C          AREA(I,5) = AREA(I,5) + TERM1*YI(I)**4            BENIN092
C          AREA(I,6) = AREA(I,6) + TERM1*YI(I)**5            BENIN093
C          AREA(I,7) = AREA(I,7) + TERM1*YI(I)**6            BENIN094
C          AREA(I,8) = AREA(I,8) + TERM1*XI(J)                BENIN095
C          AREA(I,9) = AREA(I,9) + TERM1*XI(J)**2            BENIN096
C          AREA(I,10) = AREA(I,10) + TERM1*XI(J)**3           BENIN097
C          AREA(I,11) = AREA(I,11) + TERM1*XI(J)**4           BENIN098
C          AREA(I,12) = AREA(I,12) + TERM1*XI(J)**5           BENIN099
C          AREA(I,13) = AREA(I,13) + TERM1*XI(J)**6           BENIN100
C          AREA(I,14) = AREA(I,14) + TERM1*XI(J)*YI(I)        BENIN101
C          AREA(I,15) = AREA(I,15) + TERM1*XI(J)*YI(I)**2     BENIN102
C          AREA(I,16) = AREA(I,16) + TERM1*XI(J)*YI(I)**3     BENIN103
C          AREA(I,17) = AREA(I,17) + TERM1*XI(J)*YI(I)**4     BENIN104
C          AREA(I,18) = AREA(I,18) + TERM1*XI(J)*YI(I)**5     BENIN105
C          AREA(I,19) = AREA(I,19) + TERM1*XI(J)**2*YI(I)     BENIN106
C          AREA(I,20) = AREA(I,20) + TERM1*XI(J)**2*YI(I)**2   BENIN107
C          AREA(I,21) = AREA(I,21) + TERM1*XI(J)**2*YI(I)**3   BENIN108
C          AREA(I,22) = AREA(I,22) + TERM1*XI(J)**2*YI(I)**4   BENIN109
C          AREA(I,23) = AREA(I,23) + TERM1*XI(J)**3*YI(I)     BENIN110
C          AREA(I,24) = AREA(I,24) + TERM1*XI(J)**3*YI(I)**2   BENIN111
C          AREA(I,25) = AREA(I,25) + TERM1*XI(J)**3*YI(I)**3   BENIN112
C          AREA(I,26) = AREA(I,26) + TERM1*XI(J)**4*YI(I)     BENIN113
C          AREA(I,27) = AREA(I,27) + TERM1*XI(J)**4*YI(I)**2   BENIN114
C          AREA(I,28) = AREA(I,28) + TERM1*XI(J)**5*YI(I)     BENIN115
C          CONTINUE                                           BENIN116
30

```

	TERM1 = DABS( YL(LC) ) * 0.5 * H(I)	
	DO 35 J = 1,28	BENIN117
35	ZINT(J) = ZINT(J) + TERM1 * AREA(I,J)	BENIN118
40	CONTINUE	BENIN119
	R1(1,1) = ZINT(1) * RHO	BENIN120
	R1(1,2) = ZINT(8) * RHO	BENIN121
	R1(1,3) = ZINT(2) * RHO	BENIN122
	R1(1,4) = ZINT(9) * RHO	BENIN123
	R1(1,5) = ZINT(3) * RHO	BENIN124
	R1(1,6) = ZINT(10) * RHO	BENIN125
	R1(1,7) = ZINT(19) * RHO	BENIN126
	R1(1,8) = ZINT(15) * RHO	BENIN127
	R1(1,9) = ZINT(4) * RHO	BENIN128
	R1(2,2) = R1(1,4)	BENIN129
	R1(2,3) = ZINT(14) * RHO	BENIN130
	R1(2,4) = R1(1,6)	BENIN131
	R1(2,5) = R1(1,8)	BENIN132
	R1(2,6) = ZINT(11) * RHO	BENIN133
	R1(2,7) = ZINT(23) * RHO	BENIN134
	R1(2,8) = ZINT(20) * RHO	BENIN135
	R1(2,9) = ZINT(16) * RHO	BENIN136
	R1(3,3) = R1(1,5)	BENIN137
	R1(3,4) = R1(1,7)	BENIN138
	R1(3,5) = R1(1,9)	BENIN139
	R1(3,6) = R1(2,7)	BENIN140
	R1(3,7) = R1(2,8)	BENIN141
	R1(3,8) = R1(2,9)	BENIN142
	R1(3,9) = ZINT(5) * RHO	BENIN143
	R1(4,4) = R1(2,6)	BENIN144
	R1(4,5) = R1(2,8)	BENIN145
	R1(4,6) = ZINT(12) * RHO	BENIN146
	R1(4,7) = ZINT(26) * RHO	BENIN147
	R1(4,8) = ZINT(24) * RHO	BENIN148
	R1(4,9) = ZINT(21) * RHO	BENIN149
	R1(5,5) = R1(3,9)	BENIN150
	R1(5,6) = R1(4,8)	BENIN151
	R1(5,7) = R1(4,9)	BENIN152
	R1(5,8) = ZINT(17) * RHO	BENIN153
	R1(5,9) = ZINT(6) * RHO	BENIN154
	R1(6,6) = ZINT(13) * RHO	BENIN155
	R1(6,7) = ZINT(28) * RHO	BENIN156
	R1(6,8) = ZINT(27) * RHO	BENIN157
	R1(6,9) = ZINT(25) * RHO	BENIN158
	R1(7,7) = R1(6,8)	BENIN159
	R1(7,8) = R1(6,9)	BENIN160
	R1(7,9) = ZINT(22) * RHO	BENIN161
	R1(8,8) = R1(7,9)	BENIN162
	R1(8,9) = ZINT(18) * RHO	BENIN163
	R1(9,9) = ZINT(7) * RHO	BENIN164
	DO 45 I = 1,8	BENIN165
	I1 = I + 1	BENIN166
	DO 45 J = I1,9	BENIN167
45	R1(J,I) = R1(I,J)	BENIN168
	DO 50 I = 1,9	BENIN169
	DO 50 J = 1,9	BENIN170
	DO 50 K = 1,9	BENIN171
50	R2(I,J) = R2(I,J) + ABNIT(I,K) * R1(K,J)	BENIN172
	DO 55 I = 1,9	BENIN173
		BENIN174

```
DO 5> J = 1,9
DO 55 K = 1,9
55 ELBIM(I,J) = ELBIM(I,J) + R2(I,K) * ABNIN(K,J)
RETURN
END
```

```
BENIN175
BENIN176
BFNIN177
BENIN178
BENIN179
```

```

SUBROUTINE PRINT1
C PRINT GEOMETRIC BREAK-UP AND ASSOCIATED PROPERTIES .
C
COMMON X ( 100) , Y ( 100) , Z ( 100) , TH ( 100) ,
1 XL ( 100,3) , YL ( 100,3) ,
2 RAPANG( 50) , ZGL ( 50) , RHUB ( 50) , RTIP ( 50) ,
3 THHUB ( 50) , TH TIP ( 50) , EDCM ( 3,3) ,
4 RHO , POISSD , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NEXT ( 100,3) , NP , NT
KOUNT = 0
WRITE (6,5)
5 FORMAT (1H1//30X,29HRESULTING TRIANGULAR ELEMENTS ///)
DO 20 I = 1,NT
10 FORMAT (35X,12HELEMENT NO. ,I3,//
1 20X,67HNUDE NO. X Y Z TH XL
2 YL )
LA = NEXT(I,1)
LB = NEXT(I,2)
LC = NEXT(I,3)
WRITE (6,15) LA,X(LA),Y(LA),Z(LA),TH(LA),XL(I,1),YL(I,1),LB,X(LB),
1 Y(LB),Z(LB),TH(LB),XL(I,2),YL(I,2),LC,X(LC),Y(LC),
2 Z(LC),TH(LC),XL(I,3),YL(I,3)
15 FORMAT (17X,5HLA ,I3,5X,3F10.3,3F10.4/ 17X,5HLB ,I3,5X,3F10.3,
1 3F10.4 / 17X,5HLC ,I3,5X,3F10.3,3F10.4// )
KOUNT = KOUNT + 1
IF ((KOUNT .EQ. 7) .AND. (I .NE. NT)) WRITE (6,5)
IF ( KOUNT .EQ. 7 ) KOUNT = 0
20 CONTINUE
RETURN
END
PRINT101
PRINT102
PRINT103
PRINT104
PRINT105
PRINT106
PRINT107
PRINT108
PRINT109
PRINT110
PRINT111
PRINT112
PRINT113
PRINT114
PRINT115
PRINT116
PRINT117
PRINT118
PRINT119
PRINT120
PRINT121
PRINT122
PRINT123
PRINT124
PRINT125
PRINT126
PRINT127
PRINT128
PRINT129
PRINT130
PRINT131

```

```

SUBROUTINE NORM ( ZCOS,IGEN )
C   CALCULATE NORM DIRECTION COSINE MATRIX AT EACH NODE.
C
COMMON X      ( 100) , Y      ( 100) , Z      ( 100) , TH      ( 100) ,
1      XL      ( 100,3) , YL      ( 100,3) ,
2      RAPANG( 50) , ZGL      ( 50) , RHUB      ( 50) , RTIP      ( 50) ,
3      THHUB ( 50) , TH TIP      ( 50) ,          EDCM      ( 3,3) ,
4      RHO      ,          POISSO , YOUNGS , RADGEN ,
5      NGENLI , LINE1 ,          NEXT      ( 100,3) , NP , NT ,
6      ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,
7      SIGMAX(100) , SIGMAY(100) , ELSTIF(18,18) ,
8      TAUXY(100) , ELSSM(9,9) , MEX(100,8) , IMEX(100) ,
9      ELINR(18,18) , ELMIM(6,6) , ELBIM(9,9) , ALEAN(50)
DIMENSION ZCOS(100) , IT(4) , IGEN(100)
DIMENSION R6(18,18)
DATA R6 / 324*0.0 /
EDCM(1,1) = 1.0
EDCM(2,1) = 0.0
EDCM(3,1) = 0.0
EDCM(1,2) = 0.0
EDCM(1,3) = 0.0
DO 40 I = 1, NP
IF ( IMEX(I) .NE. 1 ) GO TO 15
C   POINT I IS COMMON TO ONLY ONE TRIANGLE .
DO 10 J = 1, 18
DO 5 K = 1, 18
5  R6(J,K) = 0.0
10  R6(J,J) = 1.0
WRITE (3'I) R6
GO TO 40
C   POINT I IS COMMON TO MORE THAN 1 TRIANGLE .
15  ITS = IMEX(I)
KUUNT = 0
DO 20 J = 1, ITS
J1 = MEX(I,J)
IF ( NEXT(J1,3) .EQ. I ) GO TO 20
KUUNT = KUUNT + 1
IT(KUUNT) = MEX(I,J)
20  CONTINUE
ZNO = KUUNT
EDCM (2,2) = 0.0
EDCM (2,3) = 0.0
DO 25 J = 1, KUUNT
J1 = IT(J)
25  EDCM(2,2) = EDCM(2,2) + ARCOS( ZCOS(J1) )
EDCM(2,2) = EDCM(2,2) / ZNO
EDCM(3,3) = EDCM(2,2)
DO 30 J = 1, 3
DO 30 K = 1, 3
R6(J ,K ) = EDCM(J,K)
R6(J+3 ,K+3 ) = EDCM(J,K)
R6(J+6 ,K+6 ) = EDCM(J,K)
R6(J+9 ,K+9 ) = EDCM(J,K)
R6(J+12,K+12) = EDCM(J,K)
30  R6(J+15,K+15) = EDCM(J,K)
WRITE (3'I) R6
40  CONTINUE
RETURN

```

END

NORM0420

```

SUBROUTINE ASSEMK ( ZCOS , IPOS )
TRANSFORM STIFFNESS MATRICES TO NORMAL SYSTEMS AND ASSEMBLE
INTO A (3N X 3J) MATRIX .
COMMON X ( 100) , Y ( 100) , Z ( 100) , TH ( 100) ,
1 XL ( 100,3) , YL ( 100,3) ,
2 RAPANG( 50) , ZGL ( 50) , RHUB ( 50) , RTIP ( 50) ,
3 THHUB ( 50) , THTIP ( 50) , EDCM ( 3,3) ,
4 RHO , POISSU , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NEXT ( 100,3) , NP , NT ,
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ARNIN(9,9) ,
7 SIGMAX(100) , SIGMAY(100) , ELSTIF(18,18) ,
8 TAUXY(100) , ELSSM(9,9) , MEX(100,8) , IMEX(100) ,
9 ELINR(18,18) , ELMIM(6,6) , ELBIM(9,9)
1 DIMENSION ENSTIF(9,9) , R6(18,18) , AK(50,50) ,
1 BK(100,100) , CK(100,50) , IPOS(100) , MEXT(8) , IND(9) ,
2 R1(18,18) , ZCOS(100)
DATA IN / 3, 9, 15, 4, 10, 16, 5, 11, 17 /
DO 1 I = 1,50
DO 1 J = 1,50
AK(I,J) = 0.0
CK(I,J) = 0.0
1 CK(I+50,J) = 0.0
DO 2 I = 1,18
DO 2 J = 1,18
2 R6(I,J) = 0.0
DO 5 I = 1,100
DO 5 J = 1,100
5 BK(I,J) = 0.0
N = NP - NGENLI
KUUNT = 0
DO 55 I = 1,NP
IF ( IPOS(I) .LT. 0 ) GO TO 55
KUUNT = KUUNT + 1
IMEXT = IMEX(I)
DO 10 J = 1,IMEXT
10 MEXT(J) = MEX(I,J)
DO 50 J = 1,IMEXT
K2 = MEXT(J)
FIND (I*K2)
LA = NEXT(K2,1)
LB = NEXT(K2,2)
LC = NEXT(K2,3)
NA = IPOS(LA)
NB = IPOS(LB)
NC = IPOS(LC)
READ (I*K2) ELSTIF,ELINR,EDCM
FIND (3*I)
IF ( LA .EQ. 1 ) IND1 = 1
IF ( LB .EQ. 1 ) IND1 = 2
IF ( LC .EQ. 1 ) IND1 = 3
RFAD (3*I) R6
IF ( IMEXT .EQ. 1 ) GO TO 17
J1 = MEXT(J)
R6(3,2) = SIN( R6(3,3) - ARCUS( ZCOS(J1) ) )
R6(3,3) = COS( R6(3,3) - ARCUS( ZCOS(J1) ) )
R6(2,2) = R6(3,3)
R6(2,3) = -R6(3,2)
ASSEK001
ASSEK002
ASSEK003
ASSEK004
ASSEK005
ASSEK006
ASSEK007
ASSEK008
ASSEK009
ASSEK010
ASSEK011
ASSEK012
ASSEK013
ASSEK014
ASSEK015
ASSEK016
ASSEK017
ASSEK018
ASSEK019
ASSEK020
ASSEK021
ASSEK022
ASSEK023
ASSEK024
ASSEK025
ASSEK026
ASSEK027
ASSEK028
ASSEK029
ASSEK030
ASSEK031
ASSEK032
ASSEK033
ASSEK034
ASSEK035
ASSEK036
ASSEK037
ASSEK038
ASSEK039
ASSEK040

```

```

DO 15 K = 1,3
DO 15 L = 1,3
R6(K+3,L+3) = R6(K,L)
R6(K+6,L+6) = R6(K,L)
R6(K+9,L+9) = R6(K,L)
R6(K+12,L+12) = R6(K,L)
15 R6(K+15,L+15) = R6(K,L)
17 DO 20 K = 1,18
DO 20 L = 1,18
R1(K,L) = 0.0
CO 20 M = 1,18
20 R1(K,L) = R1(K,L) + R6(K,M) * ELSTIF(M,L)
DO 25 K = 1,9
DO 25 L = 1,9
ENSTIF(K,L) = 0.0
DO 25 M = 1,18
25 ENSTIF(K,L) = ENSTIF(K,L) + R1(IND(K),M) * R6(IND(L),M)
IF ( IPOS(LA) .LT. 0 ) GO TO 40
AK(KOUNT,NA+1) = AK(KOUNT,NA+1) + ENSTIF(IND1,1)
CK(KOUNT,NA+1) = CK(KOUNT,NA+1) + ENSTIF(IND1+3,1)
CK(KOUNT+N,NA+1) = CK(KOUNT+N,NA+1) + ENSTIF(IND1+6,1)
BK(KOUNT,NA+1) = BK(KOUNT,NA+1) + ENSTIF(IND1+3,4)
BK(KOUNT,N+NA+1) = BK(KOUNT,N+NA+1) + ENSTIF(IND1+3,7)
BK(KOUNT+N,NA+1) = BK(KOUNT+N,NA+1) + ENSTIF(IND1+6,4)
BK(KOUNT+N,N+NA+1) = BK(KOUNT+N,N+NA+1) + ENSTIF(IND1+6,7)
40 IF ( IPOS(LB) .LT. 0 ) GO TO 45
AK(KOUNT,NB+1) = AK(KOUNT,NB+1) + ENSTIF(IND1,2)
CK(KOUNT,NB+1) = CK(KOUNT,NB+1) + ENSTIF(IND1+3,2)
CK(KOUNT+N,NB+1) = CK(KOUNT+N,NB+1) + ENSTIF(IND1+6,2)
BK(KOUNT,NB+1) = BK(KOUNT,NB+1) + ENSTIF(IND1+3,5)
BK(KOUNT,N+NB+1) = BK(KOUNT,N+NB+1) + ENSTIF(IND1+3,8)
BK(KOUNT+N,NB+1) = BK(KOUNT+N,NB+1) + ENSTIF(IND1+6,5)
BK(KOUNT+N,N+NB+1) = BK(KOUNT+N,N+NB+1) + ENSTIF(IND1+6,8)
45 IF ( IPOS(LC) .LT. 0 ) GO TO 50
AK(KOUNT,NC+1) = AK(KOUNT,NC+1) + ENSTIF(IND1,3)
CK(KOUNT,NC+1) = CK(KOUNT,NC+1) + ENSTIF(IND1+3,3)
CK(KOUNT+N,NC+1) = CK(KOUNT+N,NC+1) + ENSTIF(IND1+6,3)
BK(KOUNT,NC+1) = BK(KOUNT,NC+1) + ENSTIF(IND1+3,6)
BK(KOUNT,N+NC+1) = BK(KOUNT,N+NC+1) + ENSTIF(IND1+3,9)
BK(KOUNT+N,NC+1) = BK(KOUNT+N,NC+1) + ENSTIF(IND1+6,6)
BK(KOUNT+N,N+NC+1) = BK(KOUNT+N,N+NC+1) + ENSTIF(IND1+6,9)
50 CONTINUE
55 CONTINUE
WRITE (2*1) ((AK(I,J),J=1,50),I=1,17)
WRITE (2*2) ((AK(I,J),J=1,50),I=18,34)
WRITE (2*3) ((AK(I,J),J=1,50),I=35,50)
K1 = -8
K2 = 0
DO 60 K = 1,11
K1 = K1 + 9
K2 = K2 + 9
L = K + 3
60 WRITE (2*L) ((BK(I,J),J=1,100),I=K1,K2)
WRITE (2*15) (BK(100,J),J=1,100)
K1 = -8
K2 = 0
DO 65 K = 1,5
K1 = K1 + 9
ASSEK048
ASSEK049
ASSEK050
ASSEK051
ASSEK052
ASSEK053
ASSEK054
ASSEK055
ASSEK056
ASSEK057
ASSEK058
ASSEK059
ASSEK060
ASSEK061
ASSEK062
ASSEK063
ASSEK064
ASSEK065
ASSEK066
ASSEK067
ASSEK068
ASSEK069
ASSEK070
ASSEK071
ASSEK072
ASSEK073
ASSEK074
ASSEK075
ASSEK076
ASSEK077
ASSEK078
ASSEK079
ASSEK080
ASSEK081
ASSEK082
ASSEK083
ASSEK084
ASSEK085
ASSEK086
ASSEK087
ASSEK088
ASSEK089
ASSEK090
ASSEK091
ASSEK092
ASSEK093
ASSEK094
ASSEK095
ASSEK096
ASSEK097
ASSEK098
ASSEK099
ASSEK100
ASSEK101
ASSEK102
ASSEK103
ASSEK104
ASSEK105

```



```
        K2 = K2 + 9
        L = K + 15
6>      WRITE (2*L) ((CK(I,J),I=1,100),J=K1,K2)
        WRITE (2*21) ((CK(I,J),I=1,100),J=46,50)
        RETURN
        END
```

```
ASSEK106
ASSEK107
ASSEK108
ASSEK109
ASSEK110
ASSEK111
```

	SUBROUTINE ASSEMM ( ZCOS , IPOS )	ASSEM001
C	TRANSFORM INERTIA MATRICES TO NORMAL SYSTEMS AND ASSEMBLE	ASSEM002
C	INTO A (3N X 3N) MATRIX .	ASSEM003
C		ASSEM004
	COMMON X ( 100 ) , Y ( 100 ) , Z ( 100 ) , TH ( 100 )	ASSEM005
1	XL ( 100,3 ) , YL ( 100,3 ) ,	ASSEM006
2	RAPANG( 50 ) , ZGL ( 50 ) , RHUB ( 50 ) , RTIP ( 50 )	ASSEM007
3	THHUB ( 50 ) , THTIP ( 50 ) , EDCM ( 3,3 )	ASSEM008
4	RHO , POISSO , YOUNGS , RADGEN ,	ASSEM009
5	NGENLI , LINE1 , NEXT ( 100,3 ) , NP , NT ,	ASSEM010
6	ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,	ASSEM011
7	SIGMAX(100) , SIGMAY(100) , ELSTIF(18,18) ,	ASSEM012
8	TAUXY(100) , ELSSM(9,9) , MEX(100,8) , IMEX(100) ,	ASSEM013
9	ELINR(18,18) , ELMIM(6,6) , ELBIM(9,9)	ASSEM014
	DIMENSION ENINR(9,9) , R6(18,18) , AM(50,50) ,	ASSEM015
1	BM(100,100) , CM(100,50) , IPOS(100) , MEXT(8) ,	ASSEM016
2	IND(9) , R1(18,18) , ZCOS(100)	ASSEM017
	DATA IND / 3, 9, 15, 4, 10, 16, 5, 11, 17 /	ASSEM018
	DO 1 I = 1,50	ASSEM019
	DO 1 J = 1,50	ASSEM020
	AM(I,J) = 0.0	ASSEM021
	CM(I,J) = 0.0	ASSEM022
1	CM(I+50,J) = 0.0	ASSEM023
	DO 2 I = 1,18	
	DO 2 J = 1,18	
2	R6(I,J) = 0.0	
	DO 5 I = 1,100	
	DO 5 J = 1,100	
5	BM(I,J) = 0.0	
	N = NP - NGENLI	
	KOUNT = 0	
	DO 55 I = 1, NP	
	IF ( IPOS(I) .LT. 0 ) GO TO 55	
	KOUNT = KOUNT + 1	ASSEM024
	IMEXT = IMEX(I)	ASSEM025
	DO 10 J = 1, IMEXT	ASSEM026
10	MEXT(J) = MEX(I,J)	ASSEM027
	DO 50 J = 1, IMEXT	ASSEM028
	K2 = MEXT(J)	ASSEM029
	FIND (1*K2)	ASSEM030
	LA = NEXT(K2,1)	ASSEM031
	LB = NEXT(K2,2)	ASSEM032
	LC = NEXT(K2,3)	ASSEM033
	NA = IPOS(LA)	ASSEM034
	NB = IPOS(LB)	ASSEM035
	NC = IPOS(LC)	ASSEM036
	READ (1*K2) ELSTIF,ELINR,EDCM	ASSEM037
	FIND (3*I)	
	IF ( LA .EQ. 1 ) IND1 = 1	ASSEM038
	IF ( LB .EQ. 1 ) IND1 = 2	ASSEM039
	IF ( LC .EQ. 1 ) IND1 = 3	ASSEM040
	READ (3*I) R6	
	IF ( IMEXT .EQ. 1 ) GO TO 20	
	J1 = MEXT(J)	
	R6(3,2) = SIN( R6(3,3) - ARCCOS( ZCOS(J1) ) )	
	R6(3,3) = COS( R6(3,3) - ARCCOS( ZCOS(J1) ) )	
	R6(2,2) = R6(3,3)	
	R6(2,3) = -R6(3,2)	

	DO 15 K = 1,3	ASSEM048
	DO 15 L = 1,3	ASSEM049
	R6(K+3,L+3) = R6(K,L)	ASSEM050
	R6(K+6,L+6) = R6(K,L)	ASSEM051
	R6(K+9,L+9) = R6(K,L)	ASSEM052
	R6(K+12,L+12) = R6(K,L)	ASSEM053
15	R6(K+15,L+15) = R6(K,L)	ASSEM054
20	DO 30 K = 1,18	ASSEM055
	DO 30 L = 1,18	ASSEM056
	R1(K,L) = 0.0	ASSEM057
	DO 30 M = 1,18	ASSEM058
30	R1(K,L) = R1(K,L) + R6(K,M) * ELINR(M,L)	ASSEM059
	DO 35 K = 1,9	ASSEM060
	DO 35 L = 1,9	ASSEM061
	ENINR(K,L) = 0.0	ASSEM062
	DO 35 M = 1,18	ASSEM063
35	ENINR(K,L) = ENINR(K,L) + R1(IND(K),M) * R6(IND(L),M)	ASSEM064
	IF ( IPOS(LA) .LT. 0 ) GO TO 40	ASSEM065
	AM(KOUNT,NA+1) = AM(KOUNT,NA+1) + ENINR(IND1,1)	ASSEM066
	CM(KOUNT,NA+1) = CM(KOUNT,NA+1) + ENINR(IND1+3,1)	ASSEM067
	CM(KOUNT+N,NA+1) = CM(KOUNT+N,NA+1) + ENINR(IND1+6,1)	ASSEM068
	BM(KOUNT,NA+1) = BM(KOUNT,NA+1) + ENINR(IND1+3,4)	ASSEM069
	BM(KOUNT,N+NA+1) = BM(KOUNT,N+NA+1) + ENINR(IND1+3,7)	ASSEM070
	BM(KOUNT+N,NA+1) = BM(KOUNT+N,NA+1) + ENINR(IND1+6,4)	ASSEM071
	BM(KOUNT+N,N+NA+1) = BM(KOUNT+N,N+NA+1) + ENINR(IND1+6,7)	ASSEM072
40	IF ( IPOS(LB) .LT. 0 ) GO TO 45	ASSEM073
	AM(KOUNT,NB+1) = AM(KOUNT,NB+1) + ENINR(IND1,2)	ASSEM074
	CM(KOUNT,NB+1) = CM(KOUNT,NB+1) + ENINR(IND1+3,2)	ASSEM075
	CM(KOUNT+N,NB+1) = CM(KOUNT+N,NB+1) + ENINR(IND1+6,2)	ASSEM076
	BM(KOUNT,NB+1) = BM(KOUNT,NB+1) + ENINR(IND1+3,5)	ASSEM077
	BM(KOUNT,N+NB+1) = BM(KOUNT,N+NB+1) + ENINR(IND1+3,8)	ASSEM078
	BM(KOUNT+N,NB+1) = BM(KOUNT+N,NB+1) + ENINR(IND1+6,5)	ASSEM079
	BM(KOUNT+N,N+NB+1) = BM(KOUNT+N,N+NB+1) + ENINR(IND1+6,8)	ASSEM080
45	IF ( IPOS(LC) .LT. 0 ) GO TO 50	ASSEM081
	AM(KOUNT,NC+1) = AM(KOUNT,NC+1) + ENINR(IND1,3)	ASSEM082
	CM(KOUNT,NC+1) = CM(KOUNT,NC+1) + ENINR(IND1+3,3)	ASSEM083
	CM(KOUNT+N,NC+1) = CM(KOUNT+N,NC+1) + ENINR(IND1+6,3)	ASSEM084
	BM(KOUNT,NC+1) = BM(KOUNT,NC+1) + ENINR(IND1+3,6)	ASSEM085
	BM(KOUNT,N+NC+1) = BM(KOUNT,N+NC+1) + ENINR(IND1+3,9)	ASSEM086
	BM(KOUNT+N,NC+1) = BM(KOUNT+N,NC+1) + ENINR(IND1+6,6)	ASSEM087
	BM(KOUNT+N,N+NC+1) = BM(KOUNT+N,N+NC+1) + ENINR(IND1+6,9)	ASSEM088
50	CONTINUE	ASSEM089
55	CONTINUE	ASSEM090
	WRITE (2'22)((AM(I,J),J=1,50),I=1,17)	ASSEM091
	WRITE (2'23)((AM(I,J),J=1,50),I=18,34)	ASSEM092
	WRITE (2'24)((AM(I,J),J=1,50),I=35,50)	ASSEM093
	K1 = -8	ASSEM094
	K2 = 0	ASSEM095
	DO 60 K = 1,11	ASSEM096
	K1 = K1 + 9	ASSEM097
	K2 = K2 + 9	ASSEM098
	L = K + 24	ASSEM099
60	WRITE (2'L) ((BM(I,J),J=1,100),I=K1,K2)	ASSEM100
	WRITE (2'36) ((BM(100,J),J=1,100)	ASSEM101
	K1 = -8	ASSEM102
	K2 = 0	ASSEM103
	DO 65 K = 1,5	ASSEM104
	K1 = K1 + 9	ASSEM105

```
        K2 = K2 + 9  
        L = K + 36  
65     WRITE (2'L) ((CM(I,J),I=1,100),J=K1,K2)  
        WRITE (2'42) ((CM(I,J),I=1,100),J=46,50)  
        RETURN  
        END
```

```
ASSEM106  
ASSEM107  
ASSEM108  
ASSEM109  
ASSEM110  
ASSEM111
```

	SUBROUTINE REDUCK(N)	REDUCK01
C	REDUCE THE ASSEMBLED STIFFNESS MATRIX TO AN (N X N) MATRIX.	REDUCK02
C		REDUCK03
	DIMENSION AK(50,50), BK(100,100), CK(100,50), SK(50,50), R1(50,100)	REDUCK04
	1)	REDUCK05
	EQUIVALENCE (AK(1,1), SK(1,1))	REDUCK06
	DATA R1 / 5000 * 0.0 /	REDUCK07
	READ (2*1) ((AK(I,J),J=1,50),I=1,17)	REDUCK08
	READ (2*2) ((AK(I,J),J=1,50),I=18,34)	REDUCK09
	READ (2*3) ((AK(I,J),J=1,50),I=35,50)	REDUCK10
	K1 = -8	REDUCK11
	K2 = 0	REDUCK12
	DO 1 K = 1,11	REDUCK13
	K1 = K1 + 9	REDUCK14
	K2 = K2 + 9	REDUCK15
	L = K + 3	REDUCK16
1	READ (2*L) ((BK(I,J),J=1,100),I=K1,K2)	REDUCK17
	READ (2*15) (BK(100,J),J=1,100)	REDUCK18
	K1 = -8	REDUCK19
	K2 = 0	REDUCK20
	DO 2 K = 1,5	REDUCK21
	K1 = K1 + 9	REDUCK22
	K2 = K2 + 9	REDUCK23
	L = K + 15	REDUCK24
2	READ (2*L) ((CK(I,J),I=1,100),J=K1,K2)	REDUCK25
	READ (2*21) ((CK(I,J),I=1,100),J=46,50)	REDUCK26
	N2 = 2 * N	REDUCK27
	DO 30 K = 1,N2	REDUCK28
	IF (BK(K,K))15,5,15	REDUCK29
	5 WRITE (6,10)	REDUCK30
10	FORMAT (52H B PORTION OF ASSEMBLED STIFFNESS MATRIX IS SINGULAR )	REDUCK31
	WRITE (6,12) ((BK(I,J),J=1,N2),I=1,N2)	REDUCK32
12	FORMAT (10E12.4)	REDUCK33
	N = -N	REDUCK34
	RETURN	REDUCK35
15	X = 1.0 / BK(K,K)	REDUCK36
	BK(K,K) = 1.0	REDUCK37
	DO 20 J = 1,N2	REDUCK38
20	BK(K,J) = BK(K,J) * X	REDUCK39
	IF (K - N2) 25, 35, 25	REDUCK40
25	M = K + 1	REDUCK41
	DO 30 I = M, N2	REDUCK42
	X = BK(I,K)	REDUCK43
	BK(I,K) = 0.0	REDUCK44
	DO 30 J = 1,N2	REDUCK45
30	BK(I,J) = BK(I,J) - X * BK(K,J)	REDUCK46
35	LL = N2 - 1	REDUCK47
	DO 40 I = 1, LL	REDUCK48
	M = I + 1	REDUCK49
	DO 40 K = M, N2	REDUCK50
	X = BK(I,K)	REDUCK51
	BK(I,K) = 0.0	REDUCK52
	DO 40 J = 1, N2	REDUCK53
40	BK(I,J) = BK(I,J) - BK(K,J) * X	REDUCK54
	DO 45 I = 1,N	REDUCK55
	DO 45 J = 1,N2	REDUCK56
	DO 45 K = 1,N2	REDUCK57
45	R1(I,J) = R1(I,J) + CK(K,I) * BK(K,J)	REDUCK58

	DO 50 I = 1,N	REDUCK59
	DO 50 J = 1,N	REDUCK60
	DO 50 K = 1,N2	REDUCK61
50	SK(I,J) = SK(I,J) - R1(I,K) * CK(K,J)	REDUCK62
	WRITE (2'1) ((SK(I,J),J=1,50),I=1,17)	REDUCK63
	WRITE (2'2) ((SK(I,J),J=1,50),I=18,34)	REDUCK64
	WRITE (2'3) ((SK(I,J),J=1,50),I=35,50)	REDUCK65
	DO 55 I = 1,N2	REDUCK66
	DO 55 J = 1,N	REDUCK67
	R1(J,I) = 0.0	REDUCK68
	DO 55 K = 1,N2	REDUCK69
55	R1(J,I) = R1(J,I) + BK(I,K) * CK(K,J)	REDUCK70
	K1 = -8	REDUCK71
	K2 = 0	REDUCK72
	DO 60 K = 1,5	REDUCK73
	K1 = K1 + 9	REDUCK74
	K2 = K2 + 9	REDUCK75
	L = K + 42	REDUCK76
60	WRITE (2'L) ((R1(I,J),J=1,100),I=K1,K2)	REDUCK77
	WRITE (2'48)((R1(I,J),J=1,100),I=46,50)	REDUCK78
	RETURN	REDUCK79
	END	REDUCK80

	SUBROUTINE REDUCM(N)	REDUCM01
C	REDUCE THE INERTIA MATRIX TO AN (N X N) MATRIX.	REDUCM02
C	DIMENSION AM(50,50), BM(100,100), CM(100,50), SM(50,50), R1(100,50)	REDUCM03
	1)	REDUCM04
	EQUIVALENC (AM(1,1),SM(1,1))	REDUCM05
	DATA R1 / 5000 * 0.0 /	REDUCM06
	READ (2'22)((AM(I,J),J=1,50),I=1,17)	REDUCM07
	READ (2'23)((AM(I,J),J=1,50),I=18,34)	REDUCM08
	READ (2'24)((AM(I,J),J=1,50),I=35,50)	REDUCM09
	K1 = -8	REDUCM10
	K2 = 0	REDUCM11
	DO 1 K = 1,11	REDUCM12
	K1 = K1 + 9	REDUCM13
	K2 = K2 + 9	REDUCM14
	L = K + 24	REDUCM15
1	READ (2'L)((BM(I,J),J=1,100),I=K1,K2)	REDUCM16
	READ (2'36)(BM(100,J),J=1,100)	REDUCM17
	K1 = -8	REDUCM18
	K2 = 0	REDUCM19
	DO 2 K = 1,5	REDUCM20
	K1 = K1 + 9	REDUCM21
	K2 = K2 + 9	REDUCM22
	L = K + 36	REDUCM23
2	READ (2'L)((CM(I,J),I=1,100),J=K1,K2)	REDUCM24
	READ (2'42)((CM(I,J),I=1,100),J=46,50)	REDUCM25
	K1 = -8	REDUCM26
	K2 = 0	REDUCM27
	DO 3 K = 1,5	REDUCM28
	K1 = K1 + 9	REDUCM29
	K2 = K2 + 9	REDUCM30
	L = K + 42	REDUCM31
3	READ (2'L)((R1(J,I),J=1,100),I=K1,K2)	REDUCM32
	READ (2'48)((R1(J,I),J=1,100),I=46,50)	REDUCM33
	N2 = 2 * N	REDUCM34
	DO 4 I = 1,N2	REDUCM35
	DO 4 J = 1,N	REDUCM36
	DO 4 K = 1,N2	REDUCM37
4	CM(I,J) = CM(I,J) - BM(I,K) * R1(K,J)	REDUCM38
	DO 5 I = 1,N	REDUCM39
	DO 5 J = 1,N	REDUCM40
	DO 5 K = 1,N2	REDUCM41
5	SM(I,J) = SM(I,J) - R1(K,I) * CM(K,J)	REDUCM42
	K1 = -8	REDUCM43
	K2 = 0	REDUCM44
	DO 6 K = 1,5	REDUCM45
	K1 = K1 + 9	REDUCM46
	K2 = K2 + 9	REDUCM47
	L = K + 36	REDUCM48
6	READ (2'L)((CM(I,J),I=1,100),J=K1,K2)	REDUCM49
	READ (2'42)((CM(I,J),I=1,100),J=46,50)	REDUCM50
	DO 7 I = 1,N	REDUCM51
	DO 7 J = 1,N	REDUCM52
	DO 7 K = 1,N2	REDUCM53
7	SM(I,J) = SM(I,J) - CM(K,I) * R1(K,J)	REDUCM54
	WRITE (2'43)((SM(I,J),J=1,50),I=1,17)	REDUCM55
	WRITE (2'44)((SM(I,J),J=1,50),I=18,34)	REDUCM56
	WRITE (2'45)((SM(I,J),J=1,50),I=35,50)	REDUCM57
		REDUCM58

RFTURN  
END

REDUCM59  
REDUCM60



	SUBROUTINE EIGEN (N,OMEGA)	EIGEN000
C		EIGEN001
C	SOLVE FOR THE NATURAL FREQUENCIES.	EIGEN002
	DOUBLE PRECISION COEF, EIGVR, EIGVI	EIGEN003
	DIMENSION SK(50,50), SM(50,50), OMEGA(50), COEF(50,50), EIGVR(50),	EIGEN004
	1EIGVI(50),FREQ(50)	EIGEN005
	DATA COEF , EIGVI , EIGVR / 2600 * 0.000 /	EIGEN006
	READ (2'1) ((SK(I,J),J=1,50),I=1,17)	EIGEN007
	READ (2'2) ((SK(I,J),J=1,50),I=18,34)	EIGEN008
	READ (2'3) ((SK(I,J),J=1,50),I=35,50)	EIGEN009
	READ (2'43)((SM(I,J),J=1,50),I=1,17)	EIGEN010
	READ (2'44)((SM(I,J),J=1,50),I=18,34)	EIGEN011
	READ (2'45)((SM(I,J),J=1,50),I=35,50)	EIGEN012
	DO 30 K = 1,N	EIGEN013
	IF (SM(K,K))15, 5, 15	EIGEN014
	5 WRITE (6,10)	EIGEN015
	10 FORMAT (35H REDUCED INERTIA MATRIX IS SINGULAR )	EIGEN016
	N = -N	EIGEN017
	RETURN	EIGEN018
	15 X = 1.0 / SM(K,K)	EIGEN019
	SM(K,K) = 1.0	EIGEN020
	DO 20 J = 1,N	EIGEN021
	20 SM(K,J) = SM(K,J) * X	EIGEN022
	IF (K - N) 25, 35, 25	EIGEN023
	25 M = K + 1	EIGEN024
	DO 30 I = M,N	EIGEN025
	X = SM(I,K)	EIGEN026
	SM(I,K) = 0.0	EIGEN027
	DO 30 J = 1,N	EIGEN028
	30 SM(I,J) = SM(I,J) - X * SM(K,J)	EIGEN029
	35 LL = N - 1	EIGEN030
	DO 40 I = 1,LL	EIGEN031
	M = I + 1	EIGEN032
	DO 40 K = M,N	EIGEN033
	X = SM(I,K)	EIGEN034
	SM(I,K) = 0.0	EIGEN035
	DO 40 J = 1,N	EIGEN036
	40 SM(I,J) = SM(I,J) - SM(K,J) * X	EIGEN037
	DO 45 I = 1,N	EIGEN038
	DO 45 J = 1,N	EIGEN039
	DO 45 K = 1,N	EIGEN040
	45 COEF(I,J) = COEF(I,J) + SK(I,K) * SM(K,J)	EIGEN041
	M = N	EIGEN042
	CALL EIG3 (COEF, N, M, EIGVR, EIGVI)	EIGEN043
	KOUNT = 0	EIGEN044
	DO 50 I = 1,N	EIGEN045
	IF (SNGL(EIGVI(I)) .NE. 0.0) GO TO 50	EIGEN046
	IF ( EIGVR(I) .LT. 0.000 ) GO TO 50	EIGEN047
	KOUNT = KOUNT + 1	EIGEN048
	SIGNS = 1.0	EIGEN049
	OMEGA(KOUNT) = SIGNS * DSQRT( DABS(EIGVR(I)))	EIGEN050
	FREQ(KOUNT) = OMEGA(KOUNT) / 6.283185	EIGEN051
	50 CONTINUE	EIGEN052
	IF (KOUNT .GT. 0) GO TO 60	EIGEN053
	N = - N	EIGEN054
	WRITE (6,55)	EIGEN055
	55 FORMAT (49H ALL CALCULATED FREQUENCIES ARE IMAGINARY NUMBERS )	EIGEN056
	RETURN	EIGEN057

```
60 WRITE (6,65) ( FREQ(KOUNT+1-I),I=1,KOUNT)
65 FORMAT (1H1, // 40X, 19HNATURAL FREQUENCIES //(43X, E12.5  ))
      N = KOUNT
      RETURN
      END
```

```
EIGEN058
EIGEN059
EIGEN060
EIGEN061
EIGEN062
```

```

SUBROUTINE LAGER(A, EPS, N1, NU, N, RTR, RTI)
IMPLICIT REAL*8 (A-H, O-Z)
DIMENSION A(50,50), P(6,101)
DIMENSION RTR(50), RTI(50), B(6)
REAL SSSSSS
C      ****      DOUBLE PRECISION LAGER      ****
ONCE=0.0
DATA X /0.000 /
DATA Z /1.000/
BL1=1.0
NUQ=NU-1
LLY=0
DELOLD=1.0
ROLD=1.0
EGSUM1=0.0
EGSUM2=0.0
DO 10 L=1,6
DO 10 LLX=1,101
10  P(L,LLX)=0.0
    NU1=NU+1
    CUP=0.0
    DO 11 J=NU1,N
11  CUP=CUP+DABS(A(J-1,J))
    IF (N .NE. NU) GO TO 200
    CUP = 0.
    GO TO 201
200 CUP=CUP/DFLOAT(N-NU)
201 CAP=0.
    P(1,NU)=1.0
C
C      FIND TRACE OF H AND H SQUARED
C
    SPUR1=A(NU,NU)
    SPUR2=A(NU,NU)**2
    DO 13 J=NU1,N
    SPUR1=SPUR1+A(J,J)
13  SPUR2=SPUR2+A(J,J)**2+2.000*A(J-1,J)*A(J,J-1)
C
C      INITIAL ITERATE FROM INFINITY
C
14  S1R=EGSUM1-SPUR1
    S2R=SPUR2-EGSUM2
    F1=N-NUQ
    IF(CABS(S1R) + DABS(S2R) -1.D-7*CAP) 15,15,16
15  XBAR=CUP
    YBAR=0.0
    GO TO 23
16  F2=F1-1.000
    DR=F2*(F1*S2R-S1R**2)
    ER=DSQRT(DABS(DR))
    IF(DR)17,18,18
17  IF(F1 .NE. 0.000) GO TO 202
    XBAR=0.
    YBAR=0.
    GO TO 23
202 XBAR=-2.000*S1R/F1
    YBAR=2.000*ER/F1
    GO TO 23
LAGR0010
LAGR0020
LAGR0030
LAGR0040
LAGR0050
LAGR0060
LAGR0070
LAGR0080
LAGR0090
LAGR0100
LAGR0110
LAGR0120
LAGR0130
LAGR0140
LAGR0150
LAGR0160
LAGR0170
LAGR0180
LAGR0190
LAGR0200
LAGR0210
LAGR0220
LAGR0230
LAGR0240
LAGR0250
LAGR0260
LAGR0270
LAGR0280
LAGR0290
LAGR0300
LAGR0310
LAGR0320
LAGR0330
LAGR0340
LAGR0350
LAGR0360
LAGR0370
LAGR0380
LAGR0390
LAGR0400
LAGR0410
LAGR0420
LAGR0430
LAGR0440
LAGR0450
LAGR0460
LAGR0470
LAGR0480
LAGR0490
LAGR0500
LAGR0510
LAGR0520
LAGR0530
LAGR0540
LAGR0550
LAGR0560
LAGR0570
LAGR0580

```

18	YBAR=0.0	LAGR0590
	S1RX=S1R	LAGR0600
	F2 = DSIGN( 1.000, S1RX )	LAGR0610
	IF(S1R)22,20,22	LAGR0620
20	F2=0.0	LAGR0630
22	IF(F1.NE. 0.000) GO TO 203	LAGR0640
	XBAR=0.	LAGR0650
	GO TO 23	LAGR0660
203	XBAR= -(S1R+F2*ER)/F1	LAGR0670
C		LAGR0680
C	EVALUATE POLYNOMIAL AND DERIVATIVES	LAGR0690
C		LAGR0700
23	IF (DABS(YBAR)-DABS(XBAR) *1.0-6 )24,25,25	LAGR0710
24	YBAR=0.0	LAGR0720
25	M=6	LAGR0730
	IF(YBAR)27,26,27	LAGR0740
26	M=3	LAGR0750
27	DO 207 K=NU,N	LAGR0760
	T=-A(K,K+1)	LAGR0770
	DO 207 L=1,M	LAGR0780
	S = DSIGN( 1.000, 3.500-DFLOAT(L) )	LAGR0790
	SSSSSS = S	LAGR0800
	M1=L+3*IFIX(SSSSSS)	LAGR0810
	R=-XBAR*P(L,K)+YBAR*S*P(M1,K)-DFLOAT(MOD(L-1,3))*P(L-1,K)	LAGR0820
	DO 28 J=NU,K	LAGR0830
28	R=R+P(L,J)*A(K,J)	LAGR0840
	IF(Z)29,32,29	LAGR0850
29	Z=0.0	LAGR0860
	P(1,NU)=1.0-10*P(1,NU)	LAGR0870
	IF(P(1,NU))30,30,27	LAGR0880
30	IF(N-NU+1) 204,305,204	LAGR0890
305	F=0.	LAGR0900
	GO TO 205	LAGR0910
204	F=DFLOAT(K-NU)/DFLOAT(N-NU+1)	LAGR0920
205	CONTINUE	LAGR0930
	XBAR=XBAR+F	LAGR0940
	YBAR=YBAR+F	LAGR0950
	P(1,NU)=1.0	LAGR0960
	GO TO 27	LAGR0970
32	IF(N-K)33,33,34	LAGR0980
33	T=1.0	LAGR0990
34	IF (T.NE. 0.000) GO TO 206	LAGR1000
	P(L,K+1)=0.	LAGR1010
	GO TO 207	LAGR1020
206	P(L,K+1)=R/T	LAGR1030
C		LAGR1040
207	CONTINUE	LAGR1050
C	SCALE DOWN	LAGR1060
C		LAGR1070
	DO 39 K=1,6	LAGR1080
39	B(K)=0.0	LAGR1090
	DO 35 J=1,M	LAGR1100
35	B(J)=P(J,N+1)	LAGR1110
	G1= DABS(B(1))+DABS(B(4))	LAGR1120
	G2= DABS(B(2))+DABS(B(5))	LAGR1130
	G3= DABS(B(3))+DABS(B(6))	LAGR1140
	C=DABS(B(1))	LAGR1150
	DO 36 K=2,M	LAGR1160

```

36  D= DMAX1(D,DABS(B(K)))
    CALL SCALE(D,B,M)
    IF (G1) 41,41,43
C
C  REMOVE KNOWN ROOTS
C
43  Q1R=0.0
    Q1I=0.0
    Q2R=0.0
    Q2I=0.0
    IF(NUQ-NU)19,21,21
21  DO 44 J=NU,NUQ
    D1=RTR(J)-XBAR
    D2=RTI(J)-YBAR
    D=D1**2+D2**2
    IF (D.NE. 0.000) GO TO 208
    D1=0.
    D2=0.
    GO TO 209
208 D1=D1/D
    D2=-D2/D
209 Q1R=Q1R+D1
    Q1I=Q1I+D2
    Q2R=Q2R+D1**2-D2**2
44  Q2I=Q2I+2.000*D1*D2
C
C  FIND S1 AND S2
C
19  IF (B(1) .NE. 0.000) GO TO 210
    T1R = 0.
    GO TO 211
210 T1R= B(2)/B(1)
211 T1I= 0.
    IF(B(2) .NE. 0.000) GO TO 212
    T2R = 0.
    GO TO 213
212 T2R = B(3)/B(2)
213 T2I = 0.
    IF(YBAR)45,46,45
45  D1=B(1)**2+B(4)**2
    D2=B(2)**2+B(5)**2
    IF (D1 .NE. 0.000) GO TO 214
    T1R = 0.
    T1I = 0.
    GO TO 215
214 T1R=(B(2)*B(1)+B(5)*B(4))/D1
    T1I=(B(5)*B(1)-B(4)*B(2))/D1
215 IF (D2 .NE. 0.000) GO TO 315
    T2R = 0.
    T2I = 0.
    GO TO 46
315 T2R=(B(3)*B(2)+B(6)*B(5))/ 2
    T2I=(B(6)*B(2)-B(5)*B(3))/ 2
46  S1R=T1R+Q1R
    S1I=T1I+Q1I
    S2R=T1R*(T1R-T2R)-T1I*(T1I-T2I)-Q2R
    S2I=T1R*(T1I-T2I)+T1I*(T1R-T2R)-Q2I
C

```

```

LAGR1170
LAGR1180
LAGR1190
LAGR1200
LAGR1210
LAGR1220
LAGR1230
LAGR1240
LAGR1250
LAGR1260
LAGR1270
LAGR1280
LAGR1290
LAGR1300
LAGR1310
LAGR1320
LAGR1330
LAGR1340
LAGR1350
LAGR1360
LAGR1370
LAGR1380
LAGR1390
LAGR1400
LAGR1410
LAGR1420
LAGR1430
LAGR1440
LAGR1450
LAGR1460
LAGR1470
LAGR1480
LAGR1490
LAGR1500
LAGR1510
LAGR1520
LAGR1530
LAGR1540
LAGR1550
LAGR1560
LAGR1570
LAGR1580
LAGR1590
LAGR1600
LAGR1610
LAGR1620
LAGR1630
LAGR1640
LAGR1650
LAGR1660
LAGR1670
LAGR1680
LAGR1690
LAGR1700
LAGR1710
LAGR1720
LAGR1730
LAGR1740

```

C	FIND THE NEXT ITERATE	LAGR1750
C		LAGR1760
	LLY=LLY+1	LAGR1770
	D= DABS(XBAR)+DABS(YBAR )	LAGR1780
	IF (1.0+7 -D *(DABS(SIR)+DABS(SII))) 41,41,42	LAGR1790
41	MARK=1	LAGR1800
	GO TO 100	LAGR1810
42	G=N-NUQ	LAGR1820
48	IF (YBAR-DABS(X))50,50,491	LAGR1830
491	IF (YBAR .NE. 0.000) GO TO 49	LAGR1840
	GO TO 216	LAGR1850
49	SII=SII+1.000 / ( 2.000 * YBAR )	LAGR1860
	S2R=S2R+1.000 / ( 4.000 * YBAR**2 )	LAGR1870
216	G=G-1.000	LAGR1880
50	IF (BL1)65,65,66	LAGR1890
65	H = 0.500 * ( G - 2.000 )	LAGR1900
	GO TO 67	LAGR1910
66	H=G-1.000	LAGR1920
67	DR=H*(C*S2R-SIR**2+SII**2)	LAGR1930
	DI=H*(G*S2I-2.000*SIR*SII)	LAGR1940
	IF (DI)53,51,53	LAGR1950
51	EI=0.0	LAGR1960
	ER=DSCRT(DABS(DR))	LAGR1970
	IF (DR)52,54,54	LAGR1980
52	EI=ER	LAGR1990
	ER=0.0	LAGR2000
	GO TO 54	LAGR2010
53	CALL CXSQRT(DR,DI,ER,EI)	LAGR2020
54	IF (SIR*ER+SII*EI)55,56,56	LAGR2030
55	ER=-ER	LAGR2040
	EI=-EI	LAGR2050
56	D1=SIR+ER	LAGR2060
	D2=SII+EI	LAGR2070
	D=D1**2+D2**2	LAGR2080
	IF (D .NE. 0.000) GO TO 217	LAGR2090
	X=0.	LAGR2100
	Y=0.	LAGR2110
	GO TO 218	LAGR2120
217	X=-G*DI/D	LAGR2130
	Y=G*D2/D	LAGR2140
218	XBAR=XBAR+X	LAGR2150
	YBAR=YBAR+Y	LAGR2160
	DELNEW =DABS(X)+DABS(Y)	LAGR2170
	IF (DELOLD .NE. 0.000) GO TO 219	LAGR2180
	RNEW = 0.	LAGR2190
	GO TO 220	LAGR2200
219	RNEW =DELNEW/DELOLD	LAGR2210
220	D= DABS(XBAR)+DABS(YBAR)	LAGR2220
C		LAGR2230
C	TEST FOR LINEAR CONVERGENCE	LAGR2240
C		LAGR2250
	IF (LLY-3)62,62,57	LAGR2260
57	IF (DELNEW-DMAX1(3.000*DELOLD,.500*D))571,571,570	LAGR2270
570	IF (BL1) 571,571,572	LAGR2280
572	DELOLD=CAP	LAGR2290
	ROLDC=3.0	LAGR2300
	IF (LLY-15) 14,14,100	LAGR2310
571	IF (RNEW-.700*ROLDC) 62,58,58	LAGR2320

58	MARK=3	LAGR2330
	IF(DELNEW-.001D0*EPS*CAP) 70,59,59	LAGR2340
59	IF(BL1)61,61,60	LAGR2350
60	XBAR=XBAR-X	LAGR2360
	YBAR=YBAR-Y	LAGR2370
	BL1=0.0	LAGR2380
	GO TO 48	LAGR2390
61	BL1=1.0	LAGR2400
	GO TO 63	LAGR2410
C		LAGR2420
C	TFST FOR AN EIGENVALUE	LAGR2430
C		LAGR2440
62	IF (DELNEW-EPS*DMAX1 (D,.001D0*CAP))64,64,63	LAGR2450
63	DELOLD=DELNEW	LAGR2460
	ROLD=RNEW	LAGR2470
	IF (LLY-15) 23,23,100	LAGR2480
C		LAGR2490
C	DO WE HAVE A COMPLEX APPROACH TO A REAL ROOT	LAGR2500
C		LAGR2510
64	MARK=2	LAGR2520
70	BL1=1	LAGR2530
	IF(YBAR)71,100,71	LAGR2540
71	IF(G2 *DABS(YBAR)-G1) 72,100,100	LAGR2550
72	IF(ONCE)73,73,100	LAGR2560
73	X=0.0	LAGR2570
	ONCE=1.0	LAGR2580
	YBAR=0.0	LAGR2590
	GO TO 63	LAGR2600
C		LAGR2610
C	WE ACCEPT (XBAR,YBAR) AS A ROOT	LAGR2620
C		LAGR2630
100	NUQ=NUQ+1	LAGR2640
	RTR(NUQ)=XBAR	LAGR2650
	IF(DABS(YBAR)-.001D0*DABS(XBAR))74,74,75	LAGR2660
74	YBAR=0.0	LAGR2670
75	IF(NUQ-NU) 9,76, 9	LAGR2680
9	IF(RTI(NUQ-1))76,76,77	LAGR2690
76	YBAR=DABS(YBAR)	LAGR2700
	RTI(NUQ)=YBAR	LAGR2710
	GO TO 78	LAGR2720
77	RTI(NUQ)=-DABS(YBAR)	LAGR2730
78	CONTINUE	LAGR2740
	LLY=0	LAGR2750
	CAP=DMAX1(D,CAP)	LAGR2760
	DELULC=1.0	LAGR2770
	ROLD=1.0	LAGR2780
	EGSUM1=EGSUM1+RTR(NUQ)	LAGR2790
	EGSUM2=EGSUM2+RTR(NUQ)**2-RTI(NUQ)**2	LAGR2800
	IF(NUQ-V1)80,101,101	LAGR2810
80	IF(YBAR)83,84,81	LAGR2820
81	YBAR=-YBAR	LAGR2830
	GO TO 23	LAGR2840
83	IF(NUQ-NU)31,84,31	LAGR2850
31	RTI(NUQ-1)=.5D0*(RTI(NUQ-1)-RTI(NUQ))	LAGR2860
	RTI(NUQ)=-RTI(NUQ-1)	LAGR2870
C		LAGR2880
C	A NEWTON ITERATE TOWARDS NEXT ROOT	LAGR2890
C		LAGR2900

84	CNCE=0.0	LAGR2910
	Z=0.0	LAGR2920
	IF(( DABS(Q1R)+DABS(Q1I))*D-10000.00)85,85,14	LAGR2930
85	IF (DABS (EGSUM1-SPUR1)+ DABS(EGSUM2-SPUR2)-1.D-5 *CAP)15,15,86	LAGR2940
86	DR=B(3)+2.000*(B(2)*Q1R-B(5)*Q1I)	LAGR2950
	DI=B(6)+2.000*(B(2)*Q1I+B(5)*Q1R)	LAGR2960
	D2=DR**2+DI**2	LAGR2970
	IF (D2 .NE. 0.000) GO TO 221	LAGR2980
	YBAR= DABS(YBAR)	LAGR2990
	GO TO 23	LAGR3000
221	CONTINUE	LAGR3010
	XBAR=XBAR-2.000*(DR*B(2)+DI*B(5))/D2	LAGR3020
	YBAR= DABS(YBAR-2.000*(DR*B(5)-DI*B(2))/D2)	LAGR3030
	GO TO 23	LAGR3040
101	RETURN	LAGR3050
	END	LAGR3060



	SUBROUTINE EIG3(A,N,M,RTR,RTI)	EIG30010
	IMPLICIT REAL*8 (A-H, U-Z)	EIG30020
C	EIGENVALUES OF NON-SYMMETRIC MATRICES	EIG30030
	DIMENSION A(50,50)	EIG30040
	DIMENSION NC(50),RTR(50),RTI(50)	EIG30050
C	**** DOUBLE PRECISION EIG3 ****	EIG30060
	TRACE=A(1,1)	EIG30070
	DO 10 I=2,N	EIG30080
10	TRACE=TRACE+A(I,I)	EIG30090
	B= 1.E-7	EIG30100
	CALL TRING (A,B,N,NC )	EIG30110
	TRACE=A(1,1)	EIG30120
	DO 11 I=2,N	EIG30130
11	TRACE=TRACE+A(I,I)	EIG30140
	NU=0	EIG30150
	NV=0	EIG30160
13	IF (N-N)14,12,14	EIG30170
14	NV=N+1	EIG30180
	NU=N	EIG30190
16	IF (NC(NV))15,17,15	EIG30200
15	NV=N+1	EIG30210
	GO TO 16	EIG30220
17	IF (N-NU)19,18,19	EIG30230
18	RTR(NU)=A(NU,NU)	EIG30240
	RTI(NU)=0.0	EIG30250
	GO TO 13	EIG30260
19	IF (N-NU-1)20,21,20	EIG30270
20	NP=MINO(M,NV)	EIG30280
	CALL LAGER(A,1.D-4,NP,NU,NV,RTR,RTI)	EIG30290
	GO TO 13	EIG30300
21	RR=.500*(A(NU,NU)+A(NV,NV))	EIG30310
	E1=RR**2-A(NU,NU)*A(NV,NV)+A(NU,NV)*A(NV,NU)	EIG30320
	S=DSQRT(DABS(E1))	EIG30330
	IF(E1)22,23,23	EIG30340
23	RTR(NU)=RR+S	EIG30350
	RTI(NU)=0.0	EIG30360
	RTR(NV)=RR-S	EIG30370
	RTI(NV)=0.0	EIG30380
25	CONTINUE	EIG30390
	GO TO 13	EIG30400
22	RTR(NU)=RR	EIG30410
	RTI(NU)=S	EIG30420
	RTR(NV)=RR	EIG30430
	RTI(NV)=-S	EIG30440
	GO TO 25	EIG30450
12	X=0.0	EIG30460
	DO 24 J=1,M	EIG30470
24	X=X+RTR(J)	EIG30480
	RETURN	EIG30490
	END	EIG30500

	SUBROUTINE TRING(A, EPS, N, K000FX)	TRIN0010
	IMPLICIT REAL*8 (A-H, U-Z)	TRIN0020
C	ALMOST TRIANGULAR (HESSENBERG) SUBROUTINE	TRIN0030
	DIMENSION A(50,50)	TRIN0040
	DIMENSION K000FX(50)	TRIN0050
C	**** DOUBLE PRECISION TRING ****	TRIN0060
	N1=N-1	TRIN0070
	N2=N-2	TRIN0080
	DO 21 J=1, N1	TRIN0090
	S=DABS (A(J, J+1))	TRIN0100
	J1=J+1	TRIN0110
	J2=J+2	TRIN0120
	L=J1	TRIN0130
	NJ1=N-J1	TRIN0140
	IF (NJ1) 15, 15, 6	TRIN0150
6	DO 12 K=J2, N	TRIN0160
	T=DABS (A(J, K))	TRIN0170
	IF(T-S)12, 12, 11	TRIN0180
11	L=K	TRIN0190
	S=T	TRIN0200
12	CONTINUE	TRIN0210
	IF(L-J1)13, 15, 13	TRIN0220
13	DO 131 K=1, N	TRIN0230
	T=A(K, J+1)	TRIN0240
	A(K, J+1)=A(K, L)	TRIN0250
131	A(K, L)=T	TRIN0260
14	DO 141 K=1, N	TRIN0270
	T=A(J+1, K)	TRIN0280
	A(J+1, K)=A(L, K)	TRIN0290
141	A(L, K)=T	TRIN0300
15	IF(S-EPS* DMIN1(DABS(A(J, J)), DABS(A(J+1, J+1)))) 16, 16, 17	TRIN0310
16	L=0	TRIN0320
	NJ1=0	TRIN0330
	GO TO 181	TRIN0340
17	T=A(J, J+1)	TRIN0350
	DO 18 K=J2, N	TRIN0360
	IF(T) 30, 31, 30	TRIN0370
31	A(J, K)=0.	TRIN0380
	GO TO 18	TRIN0390
30	A(J, K)=A(J, K)/T	TRIN0400
18	CONTINUE	TRIN0410
181	DO 20 I=1, N	TRIN0420
	M= MINO(J, I-2)	TRIN0430
	U=0.0	TRIN0440
	IF (NJ1) 19, 19, 7	TRIN0450
7	DO 8 K=J2, N	TRIN0460
8	U=U+A(K, I)*A(J, K)	TRIN0470
19	IF (M) 20, 20, 9	TRIN0480
9	DO 10 K=1, M	TRIN0490
10	U=U-A(K, I)*A(J+1, K+1)	TRIN0500
20	A(J+1, I)=A(J+1, I)+U	TRIN0510
21	K000FX(J)=L	TRIN0520
22	K000FX(N)=0	TRIN0530
	RETURN	TRIN0540
	END	TRIN0550

	SUBROUTINE SCALE (D,B,M)	SCAL0010
C	SUBROUTINE SCALE - FOR USE WITH DECK NO. 6140 FORTRAN IV	SCAL0020
	DIMENSION B(6)	SCAL0030
	EQUIVALENCE (G,IG),(E,IE),(IE1,IE1),(GP,IGP),(Q,IQ)	SCAL0040
	DOUBLE PRECISION D,B,DP	SCAL0050
	FMASK = SWL(127,24)	SCAL0060
	FMASK1= SWL(7,21)	SCAL0070
	Q = SWL(1,30)	SCAL0080
	DP = SNGL (DABS(D))	SCAL0090
	E = ANCA(DP,FMASK)	SCAL0100
	IE = IE-IQ	SCAL0110
	G = ANCA(DP,FMASK1)	SCAL0120
	G = SWR(IG,21)	SCAL0130
	IG1= IG/2	SCAL0140
	IF (IG1 - 1)21,10,23	SCAL0150
23	IG1 = 0	SCAL0160
	GO TO 10	SCAL0170
21	IF (IG EQ.0)IG1=1	SCAL0180
	IG1 = IG1+2	SCAL0190
10	E1 = SWR(IABS(IE),22)	SCAL0200
	IE1 = IE1 - IG1	SCAL0210
	IF(E.LT.0.)IE1=-IE1	SCAL0220
	DO 5 I = 1,M	SCAL0230
5	B(I) = B(I)/2.000**IE1	SCAL0240
	RETURN	SCAL0250
	END	SCAL0260

	SUBROUTINE CXSQRT(A,B,X,Y)	CXSQ0010
	IMPLICIT REAL*8 (A-H, O-Z)	CXSQ0020
C	COMPLEX SQUARE ROOT	CXSQ0030
	F=DMAX1(DABS(A),CABS(B))	CXSQ0040
	IF(F) 5,7,5	CXSQ0050
5	F=F*USQRT((A/F)**2 + (B/F)**2)	CXSQ0060
7	IF(A) 1,1,2	CXSQ0070
1	Y=DSQRT((F-A)*.5D0)	CXSQ0080
	IF(Y) 8,9,8	CXSQ0090
9	X=0.	CXSQ0100
	GO TO 3	CXSQ0110
8	X=.5D0 * B / Y	CXSQ0120
	IF(X)4,3,3	CXSQ0130
4	X=-X	CXSQ0140
	Y=-Y	CXSQ0150
	GO TO 3	CXSQ0160
2	X=DSQRT ((F+A)*.5D0)	CXSQ0170
	IF(X) 10,11,10	CXSQ0180
11	Y=0.	CXSQ0190
	GO TO 3	CXSQ0200
10	Y=.5D0 * B / X	CXSQ0210
3	RETURN	CXSQ0220
	END	CXSQ0230

```

SUBROUTINE AMPL (M, OMEGA, IPOS)
SOLVE FOR THE AMPLITUDES AT EACH REQUESTED FREQUENCY.
COMMON X ( 100) , Y ( 100) , Z ( 100) , TH ( 100) ,
1 XL ( 100,3) , YL ( 100,3) ,
2 RHPANG( 50) , ZGL ( 50) , RHUB ( 50) , RTIP ( 50) ,
3 THHUB ( 50) , THTIP ( 50) , EDCM ( 3,3) ,
4 RHO , POISSO , YOUNGS , RADGEN ,
5 NGENLI , LINE1 , NEXT ( 100,3) , NP , NT ,
6 ELMSM(6,6) , AMNIN(6,6) , ELBSM(9,9) , ABNIN(9,9) ,
7 SIGMAX(100) , SIGMAY(100) , ELSTIF(18,18) ,
8 TAUXY(100) , ELSSM(9,9) , MEX(100,8) , IMEX(100) , AMP(100)
DIMENSION SM(50,50),SK(50,50),ROW(50),IPOS(100)
DO 1 I = 1,100
AMP(I) = 0.0
FREQ = OMEGA / 6.283185
N = M - 1
READ (2*1) ((SK(I,J), J=1,50), I=1,17)
READ (2*2) ((SK(I,J), J=1,50), I=18,34)
READ (2*3) ((SK(I,J), J=1,50), I=35,50)
READ (2*4) ((SM(I,J), J=1,50), I=1,17)
READ (2*44) ((SM(I,J), J=1,50), I=18,34)
READ (2*45) ((SM(I,J), J=1,50), I=35,50)
DO 7 I = 1,N
DO 5 J = 1,M
5 SM(I,J) = -OMEGA ** 2 * SM(I,J) + SK(I,J)
7 SM(I,M) = - SM(I,M)
K = 1
10 I = K + 1
IF (ABS(SM(K,K)) .GT. 1.0E-10) GO TO 30
DO 15 J = I,N
J1 = J
IF (ABS(SM(J,K)) .GT. 1.0E-10) GO TO 20
15 CONTINUE
WRITE (6,16)
16 FORMAT (// 29H AMPLITUDE MATRIX IS SINGULAR)
N = -N
RETURN
20 DO 25 J = 1,M
ROW(J) = SM(J1,J)
SM(J1,J) = SM(K,J)
25 SM(K,J) = ROW(J)
30 ZM = SM(I,K) / SM(K,K)
SM(I,K) = 0.0
J = K + 1
35 SM(I,J) = SM(I,J) - ZM * SM(K,J)
IF (J .EQ. N) GO TO 40
J = J + 1
GO TO 35
40 SM(I,M) = SM(I,M) - ZM * SM(K,M)
IF (I .EQ. N) GO TO 45
I = I + 1
GO TO 30
45 IF (K .EQ. N-1) GO TO 50
K = K + 1
GO TO 10
50 ROW(M) = 1.0
ROW(N) = SM(N,M) / SM(N,N)

```

```

AMPL0001
AMPL0002
AMPL0003
AMPL0004
AMPL0005
AMPL0006
AMPL0007
AMPL0008
AMPL0009
AMPL0010
AMPL0011
AMPL0012
AMPL0013
AMPL0014
AMPL0015
AMPL0016
AMPL0017
AMPL0018
AMPL0019
AMPL0020
AMPL0021
AMPL0022
AMPL0023
AMPL0024
AMPL0025
AMPL0026
AMPL0027
AMPL0028
AMPL0029
AMPL0030
AMPL0031
AMPL0032
AMPL0033
AMPL0034
AMPL0035
AMPL0036
AMPL0037
AMPL0038
AMPL0039
AMPL0040
AMPL0041
AMPL0042
AMPL0043
AMPL0044
AMPL0045
AMPL0046
AMPL0047
AMPL0048
AMPL0049
AMPL0050
AMPL0051
AMPL0052
AMPL0053
AMPL0054
AMPL0055
AMPL0056
AMPL0057

```

I = N-1	AMPL0058
55 J = I+1	AMPL0059
S = 0.0	AMPL0060
60 S = S + SM(I,J) * ROW(J)	AMPL0061
IF (J .EQ. N) GO TO 65	AMPL0062
J = J + 1	AMPL0063
GO TO 60	AMPL0064
65 ROW(I) = (SM(I,M) - S) / SM(I,I)	AMPL0065
IF (I .EQ. 1) GO TO 70	AMPL0066
I = I - 1	AMPL0067
GO TO 55	AMPL0068
70 CONTINUE	AMPL0069
K = 0	AMPL0070
DO 75 I = 2,NP	AMPL0071
IF (IPCS(I) .LT. 0) GO TO 75	AMPL0072
K = K + 1	AMPL0073
AMP(I) = ROW(K)	AMPL0074
75 CONTINUE	AMPL0075
WRITE (6,80) FREQ	AMPL0076
80 FORMAT (//50X,12HFREQUENCY = E12.5//48X,4HNODE,16X,9HAMPLITUDE /)	AMPL0077
AMX = 0.0	AMPL0078
DO 82 I = 2,NP	AMPL0079
IF (IPUS(I) .LT. 0) GO TO 82	AMPL0080
IF (ABS(AMP(I)) .LE. AMX) GO TO 82	AMPL0081
AMX = ABS(AMP(I))	AMPL0082
82 CONTINUE	AMPL0083
DO 90 I = 1,NP	AMPL0084
IF (IPCS(I) .LT. 0) GO TO 90	AMPL0085
AMP(I) = AMP(I) / AMX	AMPL0086
WRITE (6,85) I, AMP(I)	AMPL0087
85 FORMAT (47X, 15, 10X, E15.5)	AMPL0088
90 CONTINUE	AMPL0089
RETURN	AMPL0090
END	AMPL0091

```

SUBROUTINE STRESS ( ZCOS, IPOS )
C SOLVE FOR THE RELATIVE VIBRATORY BENDING STRESSES AT THE CENTROID
C OF EACH ELEMENT .
C
COMMON X(100) , Y(100) , Z(100) , TH(100) , XL(100,3) , YL(100,3) ,
1 RAPANG(50) , ZGL(50) , RHUB(50) , RTIP(50) , THHUB(50) ,
2 THTIP(50) , EDCM(3,3) , RHO , PCISSC , YOUNGS , KADGEN ,
3 NGENLI , LINE1 , NEXT(100,3) , NP , NT , ELMSM(6,6) ,
4 AMNIN(6,6) , ELBSM(9,5) , ABNIN(9,9) , SIGMAX(100) ,
5 SIGMAY(100) , ELSTIF(18,18) , TAUXY(100) , ELSSM(9,9) ,
6 MEX(100,8) , IMEX(100) , AMP(150)
DIMENSION IPCS(100) , ZCOS(100) , BK(100,100) , CK(100,50) ,
1 BC(100,50) , R6(18,18) , WL(9) , SIG1(100) , SIG2(100) ,
2 TAUMAX(100) , SIGEFF(100)
EQUIVALENCE ( R6(1,1) , ELSTIF(1,1) )
J = 0
DO 5 I = 1, NP
IF ( IPOS(I) .LT. 0 ) GO TO 5
J = J + 1
AMP(J) = AMP(I)
5 CONTINUE
K1 = -8
K2 = 0
DO 10 K = 1, 11
K1 = K1 + 9
K2 = K2 + 9
L = K + 3
10 READ (2*L) ((BK(I,J),J=1,100),I=K1,K2)
READ (2*15) (PK(100,J),J=1,100)
K1 = -8
K2 = 0
DO 15 K = 1, 5
K1 = K1 + 9
K2 = K2 + 9
L = K + 15
15 READ (2*L) ((CK(I,J),I=1,100),J=K1,K2)
READ (2*21) ((CK(I,J),I=1,100),J=46,50)
M = NP - NGENLI
M2 = 2 * M
DO 30 K = 1, M2
XX = 1.0 / BK(K,K)
BK(K,K) = 1.0
DO 20 J = 1, M2
20 BK(K,J) = BK(K,J) * XX
IF ( K - M2 ) 25,35,25
25 M = K + 1
DO 30 I = M, M2
XX = BK(I,K)
BK(I,K) = 0.0
DO 30 J = 1, M2
30 BK(I,J) = BK(I,J) - XX * BK(K,J)
35 LL = M2 - 1
DO 40 I = 1, LL
M = I + 1
DO 40 K = M, M2
XX = BK(I,K)
BK(I,K) = 0.0
DO 40 J = 1, M2

```

```

STRS0010
STRS0020
STRS0030
STRS0040
STRS0050
STRS0060
STRS0070
STRS0080
STRS0090
STRS0100
STRS0110
STRS0120
STRS0130
STRS0135
STRS0140
STRS0150
STRS0160
STRS0170
STRS0180
STRS0190
STRS0200
STRS0210
STRS0220
STRS0230
STRS0240
STRS0250
STRS0260
STRS0270
STRS0280
STRS0290
STRS0300
STRS0310
STRS0320
STRS0330
STRS0340
STRS0350
STRS0360
STRS0370
STRS0380
STRS0390
STRS0400
STRS0410
STRS0420
STRS0430
STRS0440
STRS0450
STRS0460
STRS0470
STRS0480
STRS0490
STRS0500
STRS0510
STRS0520
STRS0530
STRS0540
STRS0550
STRS0560
STRS0570

```

```

40 BK(I,J) = BK(I,J) - BK(K,J) * XX STRS0580
M = NP - NGENLI STRS0590
CC 45 I = 1,M2 STRS0600
CC 45 J = 1,M STRS0610
BC(I,J) = 0.0 STRS0620
CC 45 K = 1,M2 STRS0630
45 BC(I,J) = BC(I,J) - BK(I,K) * CK(K,J) STRS0640
CC 50 I = 1,M2 STRS0650
AMP(M+I) = 0.0 STRS0660
CC 50 J = 1,M STRS0670
50 AMP(M+I) = AMP(M+I) + BC(I,J) * AMP(J) STRS0680
COEF1 = YOUNGS / 2.0 / ( 1.0 - POISSU**2 ) STRS0690
DO 120 I = 1,NT STRS0700
LA = NEXT(I,1) STRS0710
LB = NEXT(I,2) STRS0720
LC = NEXT(I,3) STRS0730
NA = IPOS(LA) + 1 STRS0740
NB = IPOS(LB) + 1 STRS0750
NC = IPOS(LC) + 1 STRS0760
XLC = ( XL(I,1) + XL(I,2) + XL(I,3) ) / 3.0 STRS0770
YLC = ( YL(I,1) + YL(I,2) + YL(I,3) ) / 3.0 STRS0780
TBAR = ( XL(I,2) * YL(I,3) + ( XL(I,3) - XL(I,2) ) * YLC - STRS0790
1 YL(I,3) * XLC ) * TH(LA) + ( - XL(I,3) * YLC + YL(I,3) * STRS0800
2 XLC ) * TH(LB) + ( XL(I,2) * YLC ) * TH(LC) STRS0810
COEF = CCEF1 * ABS( TBAR / XL(I,2) / YL(I,3) ) STRS0820
CC 55 J = 1,9 STRS0830
CC 55 K = 1,9 STRS0840
55 ABNIN(J,K) = 0.0 STRS0850
ABNIN(1,1) = 1.0 STRS0860
ABNIN(2,3) = -1.0 STRS0870
ABNIN(3,2) = 1.0 STRS0880
ABNIN(4,1) = -3.0 / XL(I,2) / XL(I,2) STRS0890
ABNIN(4,3) = 2.0 / XL(I,2) STRS0900
ABNIN(4,4) = - ABNIN(4,1) STRS0910
ABNIN(4,6) = 1.0 / XL(I,2) STRS0920
ABNIN(5,1) = 3.0 * (XL(I,3)**2 - XL(I,2)**2) / (XL(I,2)*YL(I,3))**2 STRS0930
ABNIN(5,2) = -2.0 / YL(I,3) STRS0940
ABNIN(5,3) = 2.0 * (XL(I,2) - XL(I,3)) * XL(I,3) / XL(I,2) / YL(I,3) STRS0950
1 / YL(I,3) STRS0960
ABNIN(5,4) = -3.0 * ( XL(I,3) / XL(I,2) / YL(I,3) ) **2 STRS0970
ABNIN(5,6) = - ( XL(I,3) / YL(I,3) ) **2 / XL(I,2) STRS0980
ABNIN(5,7) = 3.0 / YL(I,3) / YL(I,3) STRS0990
ABNIN(5,8) = - 1.0 / YL(I,3) STRS1000
ABNIN(5,9) = XL(I,3) / YL(I,3) / YL(I,3) STRS1010
ABNIN(6,1) = 2.0 / XL(I,2) **3 STRS1020
ABNIN(6,3) = - 1.0 / XL(I,2) / XL(I,2) STRS1030
ABNIN(6,4) = - ABNIN(6,1) STRS1040
ABNIN(6,6) = ABNIN(6,3) STRS1050
ABNIN(7,2) = ABNIN(6,3) STRS1060
ABNIN(7,5) = - ABNIN(6,3) STRS1070
ABNIN(8,1) = 6.0 * XL(I,3) / XL(I,2) **3 / YL(I,3) **2 * (XL(I,2) - XL(I,3)) STRS1080
ABNIN(8,2) = 2.0 * XL(I,3) / XL(I,2) / XL(I,2) / YL(I,3) STRS1090
ABNIN(8,3) = (XL(I,2) - 3.0 * XL(I,3)) * (XL(I,2) - XL(I,3)) / STRS1100
1 ( XL(I,2) * YL(I,3) ) **2 STRS1110
ABNIN(8,4) = 0.0 * XL(I,3) * (XL(I,3) - XL(I,2)) / XL(I,2) **3 / STRS1120
1 YL(I,3) **2 STRS1130
ABNIN(8,5) = - 2.0 * XL(I,3) / XL(I,2) / XL(I,2) / YL(I,3) STRS1140
ABNIN(8,6) = XL(I,3) * ( 3.0 * XL(I,3) - 2.0 * XL(I,2) ) / ( XL(I,2) * STRS1150

```



```

1          YL(I,3)**2          STRS1160
ABNIN(8,9) = -1.0 / YL(I,3)/ YL(I,3)          STRS1170
ABNIN(9,1) = 2.0 * ( 2.0 *XL(I,3)**3 - XL(I,2)* ( 3.0 *XL(I,3)**2          STRS1180
1          - XL(I,2)**2 ) ) / ( XL(I,2)* YL(I,3)**3          STRS1190
ABNIN(9,2) = (XL(I,2)**2 - XL(I,3)**2) / (XL(I,2) * YL(I,3))**2          STRS1200
ABNIN(9,3) = -2.0 *XL(I,3) * (XL(I,2) - XL(I,3))**2 /XL(I,2)**2 /          STRS1210
1          YL(I,3)**3          STRS1220
ABNIN(9,4) = 2.0 * XL(I,3)**2* ( 3.0 * XL(I,2)- 2.0 * XL(I,3) ) /          STRS1230
1          ( XL(I,2)* YL(I,3))**3          STRS1240
ABNIN(9,5) = ( XL(I,3)/ XL(I,2)/ YL(I,3))**2          STRS1250
ABNIN(9,6) = 2.0 * XL(I,3)**2* ( XL(I,2)- XL(I,3) ) / XL(I,2)**2/          STRS1260
1          YL(I,3)**3          STRS1270
ABNIN(9,7) = -2.0 / YL(I,3)**3          STRS1280
ABNIN(9,8) = 1.0 / YL(I,3)**2          STRS1290
ELPSM(1,1) = -2.0 * POISSO * ABNIN(4,1) - 2.0 * ABNIN(5,1) - ( 6.0          STRS1300
1          * PCISSO * ABNIN(6,1) + 2.0 * ABNIN(8,1) ) * XLC -          STRS1310
2          6.0 * ABNIN(9,1) * YLC          STRS1320
ELBSM(1,2) = -2.0 * ABNIN(5,2) - 2.0 * ABNIN(8,2) * XLC - ( 2.0 *          STRS1330
1          POISSO * ABNIN(7,2) + 6.0 * ABNIN(9,2) ) * YLC          STRS1340
ELBSM(1,3) = -2.0 * ( POISSO * ABNIN(4,3) + ABNIN(5,3) ) - 2.0 *          STRS1350
1          ( 3.0 * POISSO * ABNIN(6,3) + ABNIN(8,3) ) * XLC -          STRS1360
2          6.0 * ABNIN(9,3) * YLC          STRS1370
ELBSM(1,4) = -2.0 * ( POISSO * ABNIN(4,4) + ABNIN(5,4) ) - 2.0 *          STRS1380
1          ( 3.0 * POISSO * ABNIN(6,4) + ABNIN(8,4) ) * XLC          STRS1390
2          - 6.0 * ABNIN(9,4) * YLC          STRS1400
FLBSM(1,5) = -2.0 * ABNIN(8,5) * XLC - 2.0 * ( POISSO * ABNIN(7,5)          STRS1410
1          + 3.0 * ABNIN(9,5) ) * YLC          STRS1420
ELBSM(1,6) = -2.0 * ( POISSO * ABNIN(4,6) + ABNIN(5,6) ) - 2.0 *          STRS1430
1          ( 3.0 * POISSO * ABNIN(6,6) + ABNIN(8,6) ) * XLC -          STRS1440
2          6.0 * ABNIN(9,6) * YLC          STRS1450
ELBSM(1,7) = -2.0 * ABNIN(5,7) - 6.0 * ABNIN(9,7) * YLC          STRS1460
ELBSM(1,8) = -2.0 * ABNIN(5,8) - 6.0 * ABNIN(9,8) * YLC          STRS1470
ELBSM(1,9) = -2.0 * ABNIN(5,9) - 2.0 * ABNIN(8,9) * XLC          STRS1480
ELBSM(2,1) = -2.0 * ( ABNIN(4,1) + POISSO * ABNIN(5,1) ) - 2.0 *          STRS1490
1          ( 3.0 * ABNIN(6,1) + POISSO * ABNIN(8,1) ) * XLC -          STRS1500
2          6.0 * POISSO * ABNIN(9,1) * YLC          STRS1510
ELBSM(2,2) = -2.0 * POISSO * ABNIN(5,2) - 2.0 * POISSO * ABNIN(8,          STRS1520
1          2) * XLC - 2.0 * ( ABNIN(7,2) + 3.0 * POISSO *          STRS1530
2          ABNIN(9,2) ) * YLC          STRS1540
ELBSM(2,3) = -2.0 * ( ABNIN(4,3) + POISSO * ABNIN(5,3) ) - 2.0 *          STRS1550
1          ( 3.0 * ABNIN(6,3) + PCISSC * ABNIN(8,3) ) * XLC -          STRS1560
2          6.0 * POISSO * ABNIN(9,3) * YLC          STRS1570
ELBSM(2,4) = -2.0 * ( ABNIN(4,4) + POISSO * ABNIN(5,4) ) - 2.0 *          STRS1580
1          ( 3.0 * ABNIN(6,4) + POISSO * ABNIN(8,4) ) * XLC -          STRS1590
2          6.0 * PCISSC * ABNIN(9,4) * YLC          STRS1600
ELBSM(2,5) = -2.0 * POISSO * ABNIN(8,5) * XLC - 2.0 * ( ABNIN(7,5)          STRS1610
1          + 3.0 * POISSO * ABNIN(9,5) ) * YLC          STRS1620
ELPSM(2,6) = -2.0 * ( ABNIN(4,6) + POISSO * ABNIN(5,6) ) - 2.0 *          STRS1630
1          ( 3.0 * ABNIN(6,6) + PCISSO * ABNIN(8,6) ) * XLC -          STRS1640
2          6.0 * POISSO * ABNIN(9,6) * YLC          STRS1650
ELBSM(2,7) = -2.0 * POISSO * ( ABNIN(5,7) + 3.0*ABNIN(9,7)*YLC )          STRS1660
ELBSM(2,8) = -2.0 * POISSO * ( ABNIN(5,8) + 3.0*ABNIN(9,8)*YLC )          STRS1670
ELPSM(2,9) = -2.0 * POISSO * ( ABNIN(5,9) + ABNIN(8,9) * XLC )          STRS1680
ELRSM(3,1) = 2.0 * ABNIN(8,1) * ( 1.0 - POISSO ) * YLC          STRS1690
ELPSM(3,2) = 2.0 * ( 1.0 - PCISSO ) * ( ABNIN(7,2) * XLC +          STRS1700
1          ABNIN(8,2) * YLC )          STRS1710
FLHSM(3,3) = 2.0 * ABNIN(8,3) * ( 1.0 - POISSO ) * YLC          STRS1720
ELPSM(3,4) = 2.0 * ABNIN(8,4) * ( 1.0 - POISSO ) * YLC          STRS1730

```

```

ELBSM(3,5) = 2.0 * ( 1.0 - POISSO ) * ( ABNIN(7,5) * XLC +
1 ABNIN(8,5) * YLC )
ELBSM(3,6) = 2.0 * ABNIN(8,6) * ( 1.0 - POISSO ) * YLC
ELBSM(3,7) = 0.0
ELBSM(3,8) = 0.0
ELBSM(3,9) = 2.0 * ABNIN(8,9) * ( 1.0 - POISSO ) * YLC
DO 60 J = 1,3
CC 60 K = 1,9
60 ELBSM(J,K) = ELBSM(J,K) * COEF
DO 65 J = 1,9
65 WL(J) = 0.0
IF ( NA .LE. 0 ) GO TO 80
READ (3'LA) R6
IF ( IMEX(LA) .EQ. 1 ) GO TO 70
R6(3,2) = SIN( R6(3,3) - ARCOS( ZCOS(I) ) )
R6(3,3) = COS( R6(3,3) - ARCOS( ZCOS(I) ) )
R6(2,2) = R6(3,3)
R6(2,3) = -R6(3,2)
70 DO 75 J = 1,3
75 WL(J) = AMP(NA) * R6(1,J) + AMP(M+NA) * R6(2,J) + AMP(M+M+NA) *
1 R6(3,J)
80 IF ( NB .LE. 0 ) GO TO 95
READ (3'LB) R6
IF ( IMEX(LB) .EQ. 1 ) GO TO 85
R6(3,2) = SIN( R6(3,3) - ARCOS( ZCOS(I) ) )
R6(3,3) = COS( R6(3,3) - ARCOS( ZCOS(I) ) )
R6(2,2) = R6(3,3)
R6(2,3) = -R6(3,2)
85 CC 90 J = 1,3
90 WL(J+3) = AMP(NB) * R6(1,J) + AMP(M+NB) * R6(2,J) + AMP(M+M+NB) *
1 R6(3,J)
95 IF ( NC .LE. 0 ) GO TO 110
READ (3'LC) R6
IF ( IMEX(LC) .EQ. 1 ) GO TO 100
R6(3,2) = SIN( R6(3,3) - ARCOS( ZCOS(I) ) )
R6(3,3) = COS( R6(3,3) - ARCOS( ZCOS(I) ) )
R6(2,2) = R6(3,3)
R6(2,3) = -R6(3,2)
100 DO 105 J = 1,3
105 WL(J+6) = AMP(NC) * R6(1,J) + AMP(M+NC) * R6(2,J) + AMP(M+M+NC) *
1 R6(3,J)
110 CC 115 K = 1,9
SIGMAX(I) = SIGMAX(I) + ELBSM(2,K) * WL(K)
SIGMAY(I) = SIGMAY(I) + ELBSM(1,K) * WL(K)
115 TAUXY(I) = TAUXY(I) + ELBSM(3,K) * WL(K)
120 CONTINUE
DO 125 I = 1,NT
TERM1 = ( SIGMAX(I) + SIGMAY(I) ) / 2.0
TERM2 = SQRT( ( SIGMAX(I) - SIGMAY(I) )**2 / 4.0 + TAUXY(I)**2 )
SIG1(I) = TERM1 + TERM2
SIG2(I) = TERM1 - TERM2
TAUMAX(I) = ( SIG1(I) - SIG2(I) ) / 2.0
125 SIGEFF(I) = SQRT( SIG1(I)**2 + SIG2(I)**2 - SIG1(I) * SIG2(I) )
JO = 1
J1 = 1
J2 = 1
J3 = 1
J4 = 1
STRS1740
STRS1750
STRS1760
STRS1770
STRS1780
STRS1790
STRS1800
STRS1810
STRS1820
STRS1830
STRS1840
STRS1850
STRS1860
STRS1870
STRS1880
STRS1890
STRS1900
STRS1910
STRS1920
STRS1930
STRS1940
STRS1950
STRS1960
STRS1970
STRS1980
STRS1990
STRS2000
STRS2010
STRS2020
STRS2030
STRS2040
STRS2050
STRS2060
STRS2070
STRS2080
STRS2090
STRS2100
STRS2110
STRS2120
STRS2130
STRS2140
STRS2150
STRS2160
STRS2170
STRS2180
STRS2190
STRS2200
STRS2210
STRS2220
STRS2230
STRS2240
STRS2250
STRS2260
STRS2270
STRS2280
STRS2290
STRS2300
STRS2310

```

```

J5 = 1
J6 = 1
AMX = C.O
BMX = C.O
CMX = C.O
DMX = C.O
EMX = C.C
FMX = C.C
GMX = C.O
CC 160 J = 1,NT
IF ( ABS( SIGMAX(J) ) .LE. BMX ) GO TO 130
J1 = J
BMX = ABS( SIGMAX(J) )
130 IF ( ABS( SIGMAY(J) ) .LE. AMX ) GO TO 135
J0 = J
AMX = ABS( SIGMAY(J) )
135 IF ( ABS( TAUXY(J) ) .LE. CMX ) GO TO 140
J2 = J
CMX = ABS( TAUXY(J) )
140 IF ( ABS( SIG1(J) ) .LE. DMX ) GO TO 145
J3 = J
DMX = ABS( SIG1(J) )
145 IF ( ABS( SIG2(J) ) .LE. EMX ) GO TO 150
J4 = J
EMX = ABS( SIG2(J) )
150 IF ( ABS( TAUMAX(J) ) .LE. FMX ) GO TO 155
J5 = J
FMX = ABS( TAUMAX(J) )
155 IF ( ABS( SIGEFF(J) ) .LE. GMX ) GO TO 160
J6 = J
GMX = ABS( SIGEFF(J) )
160 CONTINUE
AMX = SIGMAY(J0)
BMX = SIGMAX(J1)
CMX = TAUXY(J2)
DMX = SIG1(J3)
EMX = SIG2(J4)
FMX = TAUMAX(J5)
GMX = SIGEFF(J6)
DO 165 J = 1,NT
SIGMAY(J) = SIGMAY(J) / AMX
SIGMAX(J) = SIGMAX(J) / BMX
TAUXY (J) = TAUXY (J) / CMX
SIG1 (J) = SIG1 (J) / DMX
SIG2 (J) = SIG2 (J) / EMX
TAUMAX(J) = TAUMAX(J) / FMX
165 SIGEFF(J) = SIGEFF(J) / GMX
WRITE (6,170) (I,SIGMAY(I),SIGMAX(I),TAUXY(I),SIG1(I),SIG2(I),
1 TAUMAX(I),SIGEFF(I) , I = 1,NT )
170 FORMAT ( '1' //4CX 'RELATIVE VIBRATORY BENDING STRESSES' / 45X
1 'EVALUATED AT CENTRIDS' // ' ELEMENT SIGMAYBAR SIGMAXSTRS2820
2BAR SHEAR PRIN SIGMA1BAR PRIN SIGMA2BAR MAX SHEASTRS2830
3R FFF. STRESS' / 50(4X,I3,7E16.5 /), '1' /// 50(4X,I3,7E16.5 STRS2840
4 / ) )
WRITE (6,175) J0,AMX,J1,BMX,J2,CMX,J3,DMX,J4,EMX,J5,FMX,J6,GMX STRS2860
175 FORMAT ( / 4X,I3,F16.5 / 4X,I3,I6X,E16.5 / 4X,I3,32X,E16.5 / STRS2870
1 4X,I3,48X,E16.5 / 4X,I3,64X,E16.5 / 4X,I3,80X,E16.5 / STRS2880
2 4X,I3,96X,E16.5 ) STRS2890
RETURN STRS2900
END STRS2910

```

LOGIC	START	0
	ENTRY	ANDA
	ENTRY	DRA
	ENTRY	XOR
	ENTRY	COM
	ENTRY	SWR
	ENTRY	SWL
	ENTRY	IANDA
	ENTRY	IORA
	ENTRY	IXOR
	ENTRY	ICOM
	ENTRY	ISWR
	ENTRY	ISWL
	DC	C'AND'
	DC	X'03'
	USING	ANDA,15
ANDA	STM	2,3,28(13)
	LM	2,3,0(1)
	L	2,0(2)
	L	3,0(3)
	NR	2,3
	ST	2,X0
	LE	0,X0
	L	0,X0
	LM	2,3,28(13)
	BCR	15,14
	DC	C'OR'
	DC	X'03'
	USING	DRA,15
DRA	STM	2,3,28(13)
	LM	2,3,0(1)
	L	2,0(2)
	L	3,0(3)
	OR	2,3
	ST	2,X0
	LE	0,X0
	L	0,X0
	LM	2,3,28(13)
	BCR	15,14
	DC	C'XOR'
	DC	X'03'
	USING	XDR,15
XOR	STM	2,3,28(13)
	LM	2,3,0(1)
	L	2,0(2)
	L	3,0(3)
	XR	2,3
	ST	2,X0
	LE	0,X0
	L	0,X0
	LM	2,3,28(13)
	BCR	15,14
	DC	C'COM'
	DC	X'03'
	USING	COM,15
COM	STM	2,3,28(13)
	LM	2,3,0(1)
	L	2,0(2)

```

LCR 2,2
ST 2,X0
LE 0,X0
L 0,X0
LM 2,3,28(13)
BCR 15,14
DC C*SWR*
DC X*03*
        USING SWR,15
SWR STM 2,3,28(13)
    LM 2,3,0(1)
    L 2,0(2)
    L 3,0(3)
    SRL 2,0(3)
    ST 2,X0
    LE 0,X0
    L 0,X0
    LM 2,3,28(13)
    BCR 15,14
    DC C*SWL*
    DC X*03*
        USING SWL,15
SWL STM 2,3,28(13)
    LM 2,3,0(1)
    L 2,0(2)
    L 3,0(3)
    SLL 2,0(3)
    ST 2,X0
    LE 0,X0
    L 0,X0
    LM 2,3,28(13)
    BCR 15,14
X0 DS 1F
IANDA EQU ANDA
IORA EQU ORA
IXOR EQU XOR
ICOM EQU COM
ISWR EQU SWR
ISWL EQU SWL
END

```

CLOCK	START	0		CLOCK0000
BR0	EQU	0		CLOCK0010
BR1	EQU	1		CLOCK0021
BR2	EQU	2		CLOCK0022
BR3	EQU	3		CLOCK0023
BR4	EQU	4		CLOCK0024
BR5	EQU	5		CLOCK0025
BR6	EQU	6		CLOCK0026
BR7	EQU	7		CLOCK0027
BR8	EQU	8		CLOCK0028
BR9	EQU	9		CLOCK0029
BR10	EQU	10		CLOCK0030
BR11	EQU	11		CLOCK0031
BR12	EQU	12		CLOCK0032
BR13	EQU	13		CLOCK0033
BR14	EQU	14		CLOCK0034
BR15	EQU	15		CLOCK0035
	ENTRY		HCLOCK, ICLOCK, SCLOCK, DATE	
	USING	*	BR15	
HCLOCK	SAVE	(14,5),,*		CLOCK0100
	LR	BR1, BR13		CLOCK0103
	LA	BR13, SAVE		CLOCK0105
	ST	BR13, 8(0, BR1)		CLOCK0107
	ST	BR1, 4(0, BR13)		CLOCK0109
	TIME			CLOCK0110
	L	BR13, 4(0, BR13)		CLOCK0112
	L	BR15, 16(0, BR13)	RESTORE BASE REGISTER	CLOCK0115
	O	BR0, ZFBY	INSURE PROPER SIGN FOR PACKED DIGIT.	CLOCK0120
	ST	BR0, PTIME	TEMP STORAGE FOR PACKED TIME.	CLOCK0130
	UNPK	ZTIME(7), PTIME(4)	UNPACK TIME TO ZONED DECIMAL.	CLOCK0140
	L	BR3, ZTIME	HOURS AND MINUTES.	CLOCK0150
	SLDL	BR2, 16	SHIFT IN	CLOCK0160
	SLL	BR2, 16	HOURS WITH	CLOCK0170
	O	BR2, BLNK2	TRAILING BLANKS.	CLOCK0180
	L	BR1, 24(0, BR13)		CLOCK0190
	L	BR5, 0(0, BR1)	ADDRESS OF FIRST PARAMETER.	CLOCK0200
	ST	BR2, 0(0, BR5)	SAVE TIME.	CLOCK0210
	SLDL	BR2, 16	SHIFT IN	CLOCK0220
	SLL	BR2, 16	MINUTES WITH	CLOCK0230
	O	BR2, BLNK2	TRAILING BLANKS.	CLOCK0240
	L	BR5, 4(0, BR1)		CLOCK0245
	ST	BR2, 0(0, BR5)	SAVE MINUTES.	CLOCK0250
	L	BR3, ZTIME+4	MINUTE AND TENTHS	CLOCK0260
	SLDL	BR2, 16	SHIFT IN	CLOCK0270
	SLL	BR2, 16	SECONDS WITH	CLOCK0280
	O	BR2, BLNK2	TRAILING BLANKS.	CLOCK0290
	L	BR5, 8(0, BR1)		CLOCK0295
	ST	BR2, 0(0, BR5)	SAVE SECONDS.	CLOCK0300
	RETURN	(14,5), T		CLOCK310
	USING	*	BR15	
ICLOCK	SAVE	(14,5),,*		CLOCK0100
	LR	BR1, BR13		CLOCK0
	LA	BR13, SAVE		CLOCK0
	ST	BR13, 8(0, BR1)		CLOCK0
	ST	BR1, 4(0, BR13)		CLOCK0
	TIME	BIN		CLOCK0330
	L	BR13, 4(0, BR13)		CLOCK0333
	L	BR15, 16(0, BR13)	RESTORE BASE REGISTER	CLOCK0335

	LR	BR1,BR0		CLOK0337
	SR	BR0,BR0		CLOK0339
	D	BR0,F100	CHANGE TO SECONDS FROM HUNDREDTHS	CLOK0340
	LR	BR0,BR1		CLOK0350
	L	BR1,24(0,BR13)	RELOAD ADDRESS OF PARAMETER LIST.	CLOK0360
	L	BR5,0(0,BR1)		CLOK0370
	ST	BR0,0(0,BR5)	STORE TIME	CLOK0380
	RETURN	(14,5),T		CLOK0390
	USING	*,BR15		
SCLOCK	SAVE	(14,5),,*		CLOK0100
	LR	BR1,BR13		CLOK0
	LA	BR13,SAVE		CLOK0
	ST	BR13,8(0,BR1)		CLOK0
	ST	BR1,4(0,BR13)		CLOK0
	TIME	BIN		CLOK0410
	L	BR13,4(0,BR13)		CLOK0420
	L	BR1,24(0,BR13)		CLOK0430
	L	BR5,0(0,BR1)		CLOK0440
	ST	BR0,0(0,BR5)	STORE TIME	CLOK0450
	RETURN	(14,5),T		CLOK0460
	USING	*,BR15		
DATE	SAVE	(14,5),,*		CLOK0100
	LR	BR1,BR13		CLOK0
	LA	BR13,SAVE		CLOK0
	ST	BR13,8(0,BR1)		CLOK0
	ST	BR1,4(0,BR13)		CLOK0
	TIME	DEC		CLOK0480
	L	BR13,4(0,BR13)		CLOK0483
	L	BR15,16(0,BR13)	RESTORE BASE REGISTER	CLOK0485
	LR	BR4,BR1	LOAD DATE INTO EVEN REGISTER.	CLOK0490
	SRDL	BR4,16	SHIFT DAY OF YEAR TO ODD REGISTER.	CLOK0500
	SRL	BR5,16	RIGHT JUSTIFY IT WITH LEADING ZEROES.	CLOK0510
	SLL	BR4,4	SET-UP YEAR TO ACCEPT A SIGN	CLOK0520
	O	BR5,ZFBYT	INSURE PROPER SIGN FOR DAY OF YEAR.	CLOK0530
	O	BR4,ZFBYT	INSURE PROPER SIGN FOR YEAR.	CLOK0540
	ST	BR4,PYEAR	STORE YEAR.	CLOK0550
	ST	BR4,LYEAR	STORE YEAR	CLOK0555
	ST	BR5,PDOFY	STORE DAY OF YEAR.	CLOK0560
*		IS THIS LEAP YEAR.		CLOK0570
	DP	LYEAR(4),PF0UR(1)		CLOK0580
	CP	LYEAR+3(1),ZFBYT+3(1)	REMAINDER = 0 - MEANS LEAP YEAR	CLOK0590
	BE	LPYER	BRANCH IF LEAP YEAR.	CLOK0600
*		IS IT DECEMBER		CLOK0610
FINDT	L	BR4,DEC12		CLOK0620
	CP	PDOFY(4),PK334(4)	IS IT DECEMBER.	CLOK0630
	BH	DECSI	YES.	CLOK0640
*		IS IT NOVEMBER		CLOK0650
	L	BR4,NOV11		CLOK0660
	CP	PDOFY(4),PK304(4)	IS IT NOVEMBER.	CLOK0670
	BH	NOVSI	YES	CLOK0680
*		IS IT OCTOBER		CLOK0690
	L	BR4,OCT10		CLOK0700
	CP	PDOFY(4),PK273(4)		CLOK0710
	BH	OCTSI		CLOK0720
*		IS IT SEPTEMBER		CLOK0730
	L	BR4,SEP09		CLOK0740
	CP	PDOFY(4),PK243(4)	IS IT SEPTEMBER.	CLOK0750
	BH	SEPSI	YES	CLOK0760

*		IS IT AUGUST		CLOK0770
	L	BR4,AUG08		CLOK0780
	CP	PDOFY(4),PK212(4)	IS IT AUGUST	CLOK0790
	BH	AUGSI	YES	CLOK0800
*		IS IT JULY		CLOK0810
	L	BR4,JUL07		CLOK0820
	CP	PDOFY(4),PK181(4)	IS IT JULY	CLOK0830
	BH	JULSI	YES	CLOK0840
*		IS IT JUNE		CLOK0850
	L	BR4,JUN06		CLOK0860
	CP	PDOFY(4),PK151(4)	IS IT JUNE	CLOK0870
	BH	JUNSI	YES	CLOK0880
*		IS IT MAY		CLOK0890
	L	BR4,MAY05		CLOK0900
	CP	PDOFY(4),PK120(4)	IS IT MAY	CLOK0910
	BH	MAYSI	YES	CLOK0920
*		IS IT APRIL		CLOK0930
	L	BR4,APR04		CLOK0940
	CP	PDOFY(4),PK090(4)	IS IT APRIL	CLOK0950
	BH	APRSI	YES	CLOK0960
*		IS IT MARCH		CLOK0970
	L	BR4,MAR03		CLOK0980
	CP	PDOFY(4),PK059(4)	IS IT MARCH	CLOK0990
	BH	MARSI	YES	CLOK1000
*		IS IT FEBRUARY		CLOK1010
FERJA	L	BR4,FEB02		CLOK1020
	CP	PDOFY(4),PK031(4)	IS IT FEBRUARY	CLOK1030
	BH	FEBSI	YES	CLOK1040
*		IT MUST BE JANUARY		CLOK1050
	L	BR4,JAN01		CLOK1060
STDAT	L	BR1,24(0,BR13)		CLOK1070
	L	BR5,0(0,BR1)		CLOK1080
	ST	BR4,0(0,BR5)	STORE MONTH - MM .	CLOK1090
	UNPK	ZTIME+2(2),PDOFY+2(2)	UNPACK DAY OF MONTH.	CLOK1100
	L	BR4,ZTIME		CLOK1110
	SLL	BR4,16	LEFT JUSTIFY.	CLOK1120
	O	BR4,BLNK2	PUT IN TRAILING BLANKS.	CLOK1130
	L	BR5,4(0,BR1)		CLOK1140
	ST	BR4,0(0,BR5)	STORE DAY - DD .	CLOK1150
	UNPK	ZTIME+2(2),PYEAR+2(2)		CLOK1160
	L	BR4,ZTIME		CLOK1170
	SLL	BR4,16		CLOK1180
	O	BR4,BLNK2		CLOK1190
	L	BR5,8(0,BR1)		CLOK1200
	ST	BR4,0(0,BR5)	STORE YEAR - YY .	CLOK1210
		RETURN (14,5),T		CLOK1220
*		ITS LEAP YEAR	-	CLOK1230
LPYER	CP	PDOFY(4),PK060(4)	IS IT JANUARY OR FEBRUARY	CLOK1240
	BNH	FERJA	YES	CLOK1250
	SP	PDOFY(4),PK001(4)	REDUCE DAYS BY ONE.	CLOK1260
	B	FINDT	GO FIND DATE.	CLOK1270
*		CALCULATE DAY OF MONTH.		CLOK1280
DECSI	SP	PDOFY(4),PK334(4)		CLOK1290
	B	STDAT		CLOK1300
NOVSI	SP	PDOFY(4),PK304(4)		CLOK1310
	B	STDAT		CLOK1320
OCTSI	SP	PDOFY(4),PK273(4)		CLOK1330
	B	STDAT		CLOK1340



SEPSI	SP	PDOFY(4),PK243(4)	CLOK1350
	B	STDAT	CLOK1360
AUGSI	SP	PDOFY(4),PK212(4)	CLOK1370
	B	STDAT	CLOK1380
JULSI	SP	PDOFY(4),PK181(4)	CLOK1390
	B	STDAT	CLOK1400
JUNSI	SP	PDOFY(4),PK151(4)	CLOK1410
	B	STDAT	CLOK1420
MAYSI	SP	PDOFY(4),PK120(4)	CLOK1430
	B	STDAT	CLOK1440
APRSI	SP	PDOFY(4),PK090(4)	CLOK1450
	B	STDAT	CLOK1460
MARSI	SP	PDOFY(4),PK059(4)	CLOK1470
	B	STDAT	CLOK1480
FEBSI	SP	PDOFY(4),PK031(4)	CLOK1490
	B	STDAT	CLOK1500
JAN01	DC	C' 1 '	CLOK1600
FEB02	DC	C' 2 '	CLOK1610
MAR03	DC	C' 3 '	CLOK1620
APR04	DC	C' 4 '	CLOK1630
MAY05	DC	C' 5 '	CLOK1640
JUN06	DC	C' 6 '	CLOK1650
JUL07	DC	C' 7 '	CLOK1660
AUG08	DC	C' 8 '	CLOK1670
SEP09	DC	C' 9 '	CLOK1680
OCT10	DC	C'10 '	CLOK1690
NOV11	DC	C'11 '	CLOK1700
DEC12	DC	C'12 '	CLOK1710
BLNK2	DC	C'00 '	CLOK1720
ZFBYT	DC	PL4'0'	CLOK1730
PYEAR	DC	PL4'0'	CLOK1740
LYEAR	DC	PL4'0'	CLOK1750
PDOFY	DC	PL4'0'	CLOK1760
PK334	DC	PL4'334'	CLOK1770
PK304	DC	PL4'304'	CLOK1780
PK273	DC	PL4'273'	CLOK1790
PK243	DC	PL4'243'	CLOK1800
PK212	DC	PL4'212'	CLOK1810
PK181	DC	PL4'181'	CLOK1820
PK151	DC	PL4'151'	CLOK1830
PK120	DC	PL4'120'	CLOK1840
PK090	DC	PL4'090'	CLOK1850
PK059	DC	PL4'059'	CLOK1860
PK031	DC	PL4'031'	CLOK1870
PK060	DC	PL4'060'	CLOK1880
PK001	DC	PL4'001'	CLOK1890
PFOUR	DC	P'4'	CLOK1900
ZTIME	DS	2F	CLOK1910
PTIME	DS	1F	CLOK1920
F100	DC	F'6000'	CLOK1930
SAVE	DS	18F	CLOK0705
	END		CLOK0720
		SAVE AREA FOR THIS PROGRAM.	

*	ZEROC - FILL DESIGNATED AREA OF CORE WITH ZERO OR WITH	ZERO0000
*	A CONSTANT SUPPLIED IN THE CALLING SEQUENCE.	ZERO0010
*		ZERO0020
*	CALLING SEQUENCE	ZERO0030
*	CALL ZEROC (FROM,TO)	ZERO0040
*	OR	ZERO0050
*	CALL ZEROC (FROM,TO,CONST)	ZERO0060
*		ZERO0070
*	WHERE-FROM-IS THE STARTING ADDRESS	ZERO0080
*	TO-FINAL ADDRESS TO BE CLEARED	ZERO0090
*	CONST-THE CONSTANT CORE IS TO BE	ZERO0100
*	FILLED WITH. IF NOT SUPPLIED	ZERO0110
*	IN CALLING SEQUENCE, CORE	ZERO0120
*	WILL BE FILLED WITH ZEROES.	ZERO0130
*		ZERO0140
	PWZERO START 0	ZERO0150
	BR0 EQU 0	ZERO0160
	BR1 EQU 1	ZERO0170
	BR2 EQU 2	ZERO0180
	BR3 EQU 3	ZERO0190
	BR4 EQU 4	ZERO0200
	BR5 EQU 5	ZERO0210
	BR6 EQU 6	ZERO0220
	BR7 EQU 7	ZERO0230
	BR8 EQU 8	ZERO0240
	BR9 EQU 9	ZERO0250
	BR10 EQU 10	ZERO0260
	BR11 EQU 11	ZERO0270
	BR12 EQU 12	ZERO0280
	BR13 EQU 13	ZERO0290
	BR14 EQU 14	ZERO0300
	BR15 EQU 15	ZERO0310
*		ZERO0320
	ENTRY ZERO	ZERO0325
	USING *,BR15	ZERO0340
ZERO	SAVE (14,12),,*	ZERO0330
	ST BR13,SAVE+4	ZERO0350
	LA BR10,SAVE	ZERO0360
	ST BR10,8(0,BR13)	ZERO0370
	L BR3,0(0,BR1)	ZERO0390
	L BR4,4(0,BR1)	ZERO0400
	N BR3,BIGAD	INSURE ADDRESS ONLY.
	N BR4,BIGAD	INSURE ADDRESS ONLY.
	CLR BR3,BR4	1ST ARG. LESS THAN 2ND ARG.
	BNL SWITCH	NO, THEN SWITCH REGISTERS.
MODE1	TM 4(BR1),X*80*	ZERO0470
	BZ NTZRO	MORE ARGUMENTS.
MODE	A BR4,FORBT	YES,CALCULATE BYTES TO BE CLEARED.
	SR BR4,BR3	BR4 EQUAL NO. OF BYTES.
MORE	C BR4,TWO56	OVER 255 BYTES TO CLEAR
	BL LESTN	YES
	S BR4,TWO56	REDUCE BY 256
	L BR5,TWO56	ZERO0520
MONE	S BR5,TWO	ZERO0530
	STC BR5,MOVE+1	ZERO0540
MOVE	XC 0(0,BR3),0(BR3)	ZERO0550
	A BR3,TWO56	ZERO0560
	LTR BR4,BR4	ZERO0570
		ZERO0580

	BC	2,MORE		ZERO0590
RETRN		RETURN (14,12),T	RESTORE AND RETURN	ZERO0600
LESTN	LR	BR5,BR4		ZERO0610
	LA	BR4,0		ZERO0620
	B	MONE		ZERO0630
SWITCH	LR	BR5,BR3		ZERO0640
	LR	BR3,BR4		ZERO0650
	LR	BR4,BR5		ZERO0660
	B	MODE1		ZERO0670
NTZRO	L	BR6,8(0,BR1)		ZERO0680
	L	BR6,0(0,BR6)		ZERO0685
NTZR1	ST	BR6,0(0,BR3)		ZERO0690
	CR	BR3,BR4		ZERO0700
	BE	RETRN		ZERO0710
	A	BR3,FORBT		ZERO0720
	B	NTZR1		ZERO0730
SAVE	DS	18F		ZERO1000
BIGAD	DC	X'00FFFFFF'		ZERO1010
FORBT	DC	F'4'		ZERO1020
TWO56	DC	F'256'		ZERO1030
TWO	DC	F'1'		ZERO1050
	END			ZERO9990

Distribution List  
For Report No. CR-72712  
Volume II

	Copies
National Aeronautics and Space Administration Lewis Research Center 21000 Brookpark Road Cleveland, Ohio 44135	
Attn: T. J. Flanagan Mail Stop 500-313	1
Technical Report Control Office Mail Stop 5-5	1
Technology Utilization Office Mail Stop 3-19	1
AFSC Liaison Office Mail Stop 501-3	2
Library Mail Stop 60-3	1
M. J. Hartmann Mail Stop 5-9	1
D. W. Drier Mail Stop 21-4	1
R. L. Lantz Mail Stop 21-4	1
W. E. McKissock Mail Stop 21-4	1
D. D. Scheer Mail Stop 500-203	6
J. C. Montgomery Mail Stop 54-5	1
R. E. Connelly Mail Stop 500-116	1

	Copies
National Aeronautics and Space Administration Washington, D. C. 20546	
Attn: Code RPX	2
RPL	1
Scientific and Technical Information Facility P. O. Box 33 College Park, Maryland 20740	
Attn: NASA Representative	
Code CRT	6
National Aeronautics and Space Administration Ames Research Center Moffett Field, California 94035	
Attn: Library	1
National Aeronautics and Space Administration Flight Research Center P. O. Box 273 Edwards, California 93523	
Attn: Library	1
National Aeronautics and Space Administration Goddard Space Flight Center Greenbelt, Maryland 20771	
Attn: Library	1
National Aeronautics and Space Administration John F. Kennedy Space Center Kennedy Space Center, Florida 32899	
Attn: Library	1
National Aeronautics and Space Administration Langley Research Center Langley Station Hampton, Virginia 23365	
Attn: Library	1

	Copies
National Aeronautics and Space Administration Manned Spacecraft Center Houston, Texas 77058	
Attn: Library	1
National Aeronautics and Space Administration George C. Marshall Space Flight Center Marshall Space Flight Center, Alabama 35812	
Attn: Library	1
Keith Chandler	1
Loren Gross	1
Jet Propulsion Laboratory 4800 Oak Grove Drive Pasadena, California 91103	
Attn: Library	1
U. S. Atomic Energy Commission AEC-NASA Space Nuclear Propulsion Office Washington, D. C. 20546	
Attn: F. C. Schwenk	1
Chemical Propulsion Info. Agency Applied Physics Laboratory 8621 Georgia Avenue Silver Spring, Maryland 20910	1
Defense Documentation Center Cameron Station Alexandria, Virginia 22314	1
Office of the Director of Defense Research and Engineering Washington, D. C. 20301	1
Advanced Research Projects Agency Washington, D. C. 20525	
Attn: D. E. Mock	1
Research and Technology Division Air Force Systems Command Bolling Air Force Base Washington, D. C. 20332	
Attn: RTD (RTNP)	1

Copies

<p>Arnold Engineering Development Center          Air Force Systems Command          Tullahoma, Tennessee 37389</p>	
<p>Attn: AEOIM</p>	1
<p>Air Force Aero Propulsion Laboratory          Research and Technology Division          Air Force Systems Command          United States Air Force          Wright Patterson AFB, Ohio 45433</p>	
<p>Attn: APRP</p>	1
<p>Aeronautical Systems Division          Air Force Systems Command          Wright Patterson Air Force Base,          Dayton, Ohio 45433</p>	
<p>Attn: Library</p>	1
<p>Air Force Missile Test Center          Patrick Air Force Base, Florida 32925</p>	
<p>Attn: L. J. Ullian</p>	1
<p>Air Force Systems Command          Andrews Air Force Base          Washington, D. C. 20332</p>	
<p>Attn: SCLT</p>	1
<p>Air Force Rocket Propulsion Laboratory (RPR)          Edwards Air Force Base, California 93523</p>	1
<p>Air Force Office of Scientific Research          Washington, D. C. 20333</p>	
<p>Attn: SREP, Dr. J. F. Masi</p>	1
<p>Office of Research Analyses (OAR)          Holloman Air Force Base, New Mexico 88330</p>	
<p>Attn: Library</p>	1
<p>Commanding Officer          U. S. Army Research Office (Durham)          Box CM, Duke Station          Durham, North Carolina 27706</p>	1

	Copies
U. S. Army Missile Command Redstone Scientific Information Center Redstone Arsenal, Alabama 35808	
Attn: Chief, Document Section	1
Bureau of Naval Weapons Department of the Navy Washington , D. C. 20360	
Attn: J. Kay, Code RTMS-41	1
Commander U. S. Naval Missile Center Point Mugu, California 93041	
Attn: Technical Library	1
Commanding Officer Office of Naval Research 1030 E. Green Street Pasadena, California 91101	1
Director (Code 6180) U. S. Naval Research Laboratory Washington, D. C. 20390	
Attn: H. W. Carhart	1
Picatinny Arsenal Dover, New Jersey 07801	
Attn: Chief, Liquid Propulsion Laboratory	1
Aerojet-General Corporation P. O. Box 296 Azusa, California 91703	
Attn: Librarian	1
Aerojet-General Corporation 11711 South Woodruff Avenue Downey, California 90241	
Attn: F. M. West, Chief Librarian	1



Copies

Aerojet-General Corporation  
P. O. Box 1947  
Sacramento, California 95809

Attn: Tech. Library 2484-2015A	1
K. R. Collins	1
R. Jones	1
J. Farquhar	1
F. Viteri	1
M. Huppert	1
B. Lindley	1
L. Severud	1

Aerospace Corporation  
P. O. Box 95085  
Los Angeles, California 90045

Attn: Library-Documents	1
-------------------------	---

Allis Chalmers Mfg. Co. Box 512 Milwaukee, Wisconsin 53201	1
------------------------------------------------------------------	---

Battelle Memorial Institute  
505 King Avenue  
Columbus, Ohio 43201

Attn: Report Library Room 6A	1
---------------------------------	---

Bell Aerospace Company  
Box 1  
Buffalo, New York 14240

Attn: Technical Library	1
M. Messina	1

The Boeing Company  
Aero Space Division  
P. O. Box 3707  
Seattle, Washington 98124

Attn: Ruth E. Peerenboom, Library Processes Sup. (1190)	1
------------------------------------------------------------	---

Brown Engineering Co., Inc.  
Research Park  
Huntsville, Alabama 35807

Attn: Library	1
---------------	---

	Copies
Chrysler Corporation Space Division New Orleans, Louisiana 70150	
Attn: Library	1
Curtiss-Wright Corporation Wright Aeronautical Division Woodridge, New Jersey 07075	
Attn: Library	1
Fairchild Stratos Corporation Aircraft Missiles Division Hagerstown, Maryland 20740	
Attn: Library	1
The Franklin Institute Research Laboratories Benjamin Franklin Parkway Philadelphia, Pennsylvania 19103	
Attn: Library	1
The Garrett Corporation AiResearch Manufacturing Co. 9851 Sepulveda Blvd. Los Angeles, California 90009	
Attn: Library	1
General Dynamics/Astronautics P. O. Box 1128 San Diego, California 92112	
Attn: Library and Information Services (128-00)	1
General Electric Company Flight Propulsion Laboratory Dept. Cincinnati, Ohio 45215	
Attn: D. Suichu	1
P. R. Gliebe	1
General Motors Corporation Allison Division P. O. Box 24013 Indianapolis, Indiana 46206	
Attn: Library	1

Copies

Grumman Aircraft  
Bethpage Long Island  
New York 11714

Attn: Library

Hydronautics, Incorporated  
Pindell School Road  
Laurel, Maryland

1

IIT Research Institute  
Technology Center  
Chicago, Illinois 60616

Attn: Library

1

Lockheed Missiles & Space Company  
Propulsion Engineering Division (D. 55-11)  
1111 Lockheed Way  
Sunnyvale, California 94087

1

Lockheed Propulsion Company  
P. O. Box 111  
Redlands, California 92374

Attn: Library

1

Marquardt Corporation  
16555 Saticoy Street  
Box 2013 - South Annex  
Van Nuys, California 91404

Attn: Library

1

McDonnell Douglas Aircraft Corporation  
P. O. Box 516  
Lambert Field, Missouri 63166

Attn: Library

1

McDonnell Douglas Astronautics Company  
Western Division  
5301 Bolsa Avenue  
Huntington Beach, California 92647

Attn: Library

1

	Copies
Pesco Products Division of Borg-Warner Corp. 24700 N. Miles Road Bedford, Ohio 44146	1
Rocketdyne, A Division of North American Rockwell Corporation 6633 Canoga Avenue Canoga Park, California 91304	
Attn: Library, Dept. 596-306	1
J. Hale	1
K. Rothe	1
R. K. Hoshide	1
J. A. King	1
J. K. Jacobsen	1
Rocket Research Corporation 520 South Portland Street Seattle, Washington 98108	1
Sundstrand Corporation Hydraulics Division Rockford, Illinois 61101	1
Sundstrand-Denver Industrial Products Group 2480 W. 70th Street Denver, Colorado 80221	1
TRW Systems One Space Park Redondo Beach, California 90278	
Attn: STL Tech. Lib. Doc. Acquisitions	1
United Aircraft Corporation Corporation Library 400 Main Street East Hartford, Connecticut 06118	
Attn: Library	1
United Aircraft Corporation Pratt & Whitney Fla. Res. Development Center P. O. Box 2691 West Palm Beach, Florida 33402	
Attn: Library	1
J. Hill	1

	Copies
United Aircraft Corporation United Technology Center P. O. Box 358 Sunnyvale, California 94088	
Attn: Library	1
Worthington Corp. Advanced Products Division Harrison & Worthington Avenues Harrison, New Jersey 07029	
	1
Dr. George F. Wislicenus 4641 E. Coronado Drive Tuscon, Arizona 85718	
	1
California Institute of Technology Pasadena, California	
Attn: Dr. A. Acosta	1
Iowa State University Ames, Iowa	
Attn: Dr. George Serovy	1
Pennsylvania State University State College, Pennsylvania	
Attn: Dr. B. Lakshminarayana	1
Scanivalve Corp. P. O. Box 20005 San Diego, California 92120	
Attn: J. C. Pemberton	1