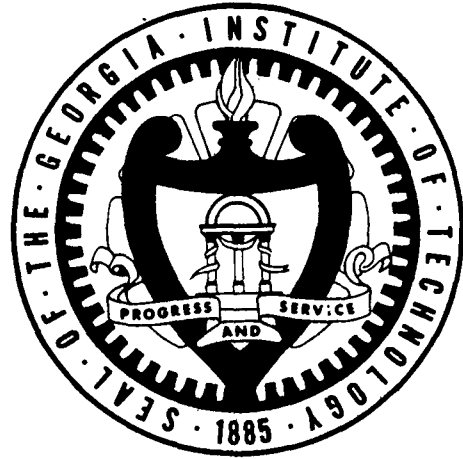


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GEORGIA INSTITUTE OF TECHNOLOGY
School of Mechanical Engineering
Atlanta, Georgia

SIMPLIFIED ANALYSIS AND OPTIMIZATION
OF
SPACE BASE AND SPACE SHUTTLE HEAT
REJECTION SYSTEMS



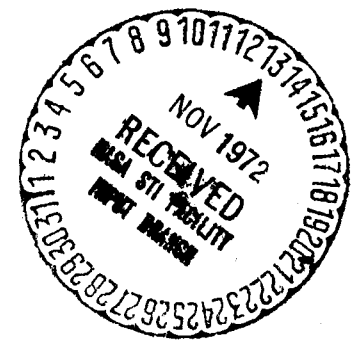
Contract No. NAS 9-10415

by

Wolfgang Wulff

Sponsored by the
Power Generation Branch
Manned Spacecraft Center

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
Houston, Texas



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GEORGIA INSTITUTE OF TECHNOLOGY
SCHOOL OF MECHANICAL ENGINEERING
ATLANTA, GEORGIA

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I

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SCHOOL OF MECHANICAL ENGINEERING
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FOREWORD

This report covers part of the work performed during the second year phase of a two year research project, at the School of Mechanical Engineering at the Georgia Institute of Technology in Atlanta, Georgia, for the NASA Manned Spacecraft Center, Houston, Texas. The contract designation is NAS 9-10415 and the project title is "Study of Design Parameters of Space Base and Shuttle Heat Rejection Systems." The project was monitored by Dr. W.E. Simon of the Power Generation Branch of NASA MSC, Houston, Texas, and was performed by Dr. W.Z. Black and Dr. W. Wulff as Co-Investigators. The project resulted in one Annual Report [2]* and two Final Reports, the first one of which covers a detailed and rigorous space radiator simulation analysis [1] and includes a computer program users manual. The second Final Report is this report.

Although the study of system parameters and the system optimization were originally conceived to be performed on the basis of the rigorous radiator system simulation [1], the growing complexity of this simulation soon gave rise to the need for a simplified analysis. The simplified system simulation was later expanded into systematic optimization procedures. Both the simplified simulation and the optimization procedures serve to supplement and support the originally intended system parameter study [1].

The work presented here was supported by the contributions of computer coding by Mr. Richard J. Huntley and Mr. Wallace W. Carr, both Graduate Research Assistants and M.S. Candidates.

*Numbers in brackets refer to the Bibliography at the end of this report.

SUMMARY

A simplified radiator system analysis was performed to predict steady-state radiator system performance. The system performance was found to be describable in terms of five non-dimensional system parameters. The governing differential equations are integrated numerically to yield the enthalpy rejection for the coolant fluid.

The simplified analysis was extended to produce firstly the derivatives of the coolant exit temperature with respect to the governing system parameters and secondly a procedure to find the optimum set of system parameters which yields the lowest possible coolant exit temperature for either a given projected area or a given total mass. The process can be inverted to yield either the minimum area or the minimum mass, together with the optimum geometry, for a specified heat rejection rate.

The major accomplishments of the simplified radiator system analysis are:

- (1) the reduction of the number of necessary systems parameters from twelve or more to six,
- (2) the graphical representation of system performance in terms of non-dimensional groups, suitable to aid in the design of radiative heat rejection systems, and
- (3) an efficient computer code suitable for preliminary performance prediction.

The accomplishments of the systematic optimization analysis are two computer codes which perform iterative optimizations processes leading to the maximum heat rejection for either a given projected fin-plus-tube area or a given total system mass.

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NOMENCLATURE

A^*	Normalized projected radiator area, Eq. 38
A	Coefficient matrix in Eq. 49
A_{ij}	Elements of coefficient matrix A
a_i	Coefficients of power polynomial
$B_{ij} = \partial^2 \theta_b / \partial x_i \partial x_j$	Second-order derivatives of θ_b
c	Constant in Nusselt number relation, Eq. 35
c_p	Coolant fluid specific heat (Btu/(lbm R))
d	Tube diameter (ft)
$d^* = d/L_o$	Normalized tube diameter
F_{fs}	Fin to sink view factor, Eq. 15
f	Blockage coefficient, defined by Eq. 16
H	Fin height, from base to tip (ft)
$H^* = H/L_o$	Normalized fin height
\bar{h}_c	Average convective film coefficient for convection from fluid to tube (Btu/(hr ft ² R))
i	Number of radiatively active sides
k	Thermal conductivity (Btu/(hr ft R)) of structural material
k_f	Thermal conductivity (Btu/(hr ft R)) of coolant fluid
L	Tube length (ft)
L_o	Reference length (ft), defined by Eq. 37
$L^* = L/L_o$	Normalized tube length
M	Parameter, defined by Eq. 12 (viewfactor augmentation)
M	Structural mass, per fin-tube element (lbm)
$M_o = \rho L_o^3$	Reference mass (lbm)

M_f	Coolant fluid mass (lbm)
$M^* = M / (M_o \phi_1)$	Normalized structural mass
$M_f^* = M_f / (M_o \phi_1)$	Normalized coolant mass
$M_{tot}^* = M_f^* + M^*$	Normalized total mass
m	Exponent on N_{Re} in Nusselt number relation, Eq. 35
\dot{m}	Coolant mass flow rate (lbm/hr)
N	Tube to sink view factor, Eq. 17
$N_c = \bar{N}_c \theta_b^3$	Conduction parameter, Eq. 14
\bar{N}_c, N_c^*	Reference conduction parameter, defined by Eqs. 20 and 58*
N_{Gr}, N_{Gr}^*	Graetz number, Eqs. 23 and 55
N_{Nu}, N_{Nu}^*	Nusselt number, Eqs. 8, 9, 10, 35 and 57*
N_{Pr}	Prandtl number, Eq. 7
N_{Re}, N_{Re}^*	Reynolds number, Eqs. 6 and 56*
n	Number of coolant channels
n	Exponent on N_{Pr} in Nusselt number relation, Eq. 35
p	Exponent on d/L-ratio in Nusselt number relation, Eq. 35
q''	Incident radiant heat flux (Btu/(hr ft ²))
r	Number of constraints
T	Absolute temperature (R)
t	Fin panel thickness (ft)
$t^* = t/L_o$	Normalized fin panel thickness
U	System parameter, defined by Eq. 22
V	System parameter, ratio of convective to radiative resistances, Eq. 21
\underline{X}	Vector whose components are the system parameters x_i

*Superscripted stars on symbol N indicate non-dimensional groups evaluated by replacing all dimensions L, H, d and t by L_o .

x_i	General system parameters, $x_1 = U$, $x_2 = V$, $x_3 = \bar{N}_c$, $x_4 = \lambda$
$\Delta \tilde{X}$	Computed changes of \tilde{X} , in iteration process
Y	Generalized distance from optimum, defined by Eqs. 49 and 50
y_i	Components of \tilde{Y} , defined by Eqs. 50
z	Distance along the tube (ft)

GREEK SYMBOLS

α_s	Solar absorptance
$\tilde{\delta}$	Incremental component vector defining a neighborhood about potential optimum, Eq. 47
ϵ	Surface emittance
$\zeta = z/L_o$	Normalized axial distance
η	Effectiveness of unobstructed fin
$\bar{\eta}$	Combined fin and tube effectiveness
$\theta = T/T_o$	Normalized temperature
$\lambda = 4H/d$	
σ	Stefan Boltzmann constant $\sigma = 0.1714 \times 10^{-8}$ Btu/(hr ft ² R ⁴)
μ	Dynamic viscosity (lbm/(sec ft))
ρ	Structural material density (lbm/ft ³)
ρ_f	Fluid density (lbm/ft ³)
ϕ_1	Parameter, defined by Eq. 42
ϕ_2	Parameter, defined by Eq. 44
ϕ_3	Parameter, defined by Eq. 63
ψ_i	Constraints, Eqs. 39, 40, 41 and 46

SUBSCRIPTS

b	Fin base
c	Conduction

e	Channel exit
f	Fluid, bulk property
i,j	Component subscripts
k	Iteration step counting index
m	at optimum
s	sink
w	Fluid, at tube wall
o	Channel inlet

I. INTRODUCTION

A large-scale, complete and rigorous computer simulation of space radiator systems was developed under the same contract as the work presented here [1].* The computer code consists of over fifty program units and is capable of simulating transient as well as steady-state radiator system performances under prescribed time-dependent operational and environmental conditions. The program accommodates both gaseous and liquid coolant fluids with any consistently prescribed set of thermodynamic and transport properties. In principle, this large-scale computer program could serve to not only predict radiator system performance but also to optimize certain design parameters via enumeration of performance characteristics, associated with selected parameter combinations

Any large computer simulation must be tested during its development; the greater the number of independent verification modes the greater will be the confidence in the program performance. In addition to the tests described in Reference [1], a simplified radiator system analysis was developed to verify the large-scale computer program performance. This simplified analysis served later (1) to extend the rigorous analysis to a wider class of radiator geometries and operating conditions [1] than would have been possible otherwise and (2) to develop systematic optimization procedures in support of system parameter studies on the basis of the rigorous computer simulation.

The essence of the simplified analysis lies in the recognition of the dominant performance characteristics and in the parameter reduction through normalization of the governing differential equations. The optimization is based on standard requirements of extrema subject to suitable constraints. These requirements are imposed on the governing differential equations prior to their numerical integration.

Chapter II below is a discussion of the simplified analysis and is followed by the presentation of the optimization analysis in Chapter III.

*Numbers in brackets refer to the Bibliography.

II. SIMPLIFIED RADIATOR SYSTEM ANALYSIS

A. Objective and Background

The purpose of this analysis is to provide an efficient process of least complexity which serves to describe the steady-state performance of a space radiator system. The radiator system is described in detail in the following chapter.

The analysis is intended to accommodate the essential features of the radiator system performance but to require less computational effort than the rigorous system simulation described in Reference [1]. Finally, the simplified analysis should serve as the basis for systematic optimization of the radiator system.

A first simplified analysis was developed during the first year of the contract period [2], also in support of the rigorous computer analysis, and for the purpose of treating approximately some radiator system geometries which deviate from the basic geometry underlying the rigorous system analysis, such as cylindrical shell radiator structures, asymmetrically loaded coolant channels etc. [1]. This analysis was based on two global energy balances, one for the coolant fluid and one for the radiator panel, and included the two thermal resistances associated with the energy transfer from the fluid to the tube and from the radiator into space. The mean tube wall temperature (and with it, the fin base temperature) was obtained from a single, transcendental equation (Eq. D.11, [2]) and the cooling capacity was found explicitly in terms of the mean tube wall temperature (Eq. 1.1 or 3, [2]). Agreement between this simplified analysis and the full-scale computer simulation was found to be approximately 4%.

The search for an optimum radiator geometry on the basis of the first simplified analysis lead to the conclusion that for optimum radiator geometries neighboring coolant channels should be expected to be close enough to each other so as to obstruct each other's, and the fin panel's, view of space. Moreover, the rigorous computer simulation indicated that the tube wall temperature changes significantly in the direction of the flow even though conduction parallel to the flow direction, both in the fluid, in the

tube wall and in the fin, is negligible. These effects are not accounted for in the first simplified analysis.

The new simplified analysis presented here, for the prediction of steady-state radiator heat rejection performance, takes into account

- (i) temperature variations within the fluid, tube and fin, along the direction of the flow,
- (ii) temperature variation within the fin, normal to the direction of the flow,
- (iii) direct radiative interaction between fin panel and space, tube and space, fin and tubes, tube and neighboring tubes (by approximation),

but does not take into account

- (i) thermal conduction in the direction of the coolant flow, both in the fin-tube structure and the fluid
- (ii) temperature variation of thermal properties,
- (iii) end effects at the coolant fluid manifold,
- (iv) cross-sectional changes in the fin panel,
- (v) secondary reflections of radiant heat.

The analysis reduces to an initial value problem consisting of two ordinary, first-order, coupled differential equations, with one of its initial conditions given through a transcendental equation. The new formulation is suitable for optimization.

B. Description of Radiator System

The radiator system considered here consists of a given number of parallel coolant channels, equally spaced in one plane, and connected by rectangular fin panels which have constant thickness and are symmetric with respect to the plane through the tube areas.

The coolant channels are taken to be thin-walled tubes of circular cross-section, with diameter d and length L . Substitution of the hydraulic diameter for the diameter permits readily the inclusion of channels with non-circular cross-sections, except for possible effects from radiative interaction between tube, fin and environment.

Let the distance between tube centers be designated by $d+2H$ and the fin panel thickness by t . Then the radiator can be considered to consist of the given number n of identical fin elements as shown in Figure 1.

The coolant fluid enters the channel at $z = 0$ with time-invariant temperature $T_f = T_o$. Both the fluid temperature $T_f(z)$ and the fin base temperature $T_b(z)$ decrease along the tube provided the equivalent sink temperature T_s is less than T_o . The coolant fluid emerges from the radiator at $z = L$ with the exit temperature T_e .

The objective of the analysis is to predict the rate of heat rejection $\dot{m} c_p (T_o - T_e)$ per tube for a given mass flow rate \dot{m} per tube and given fluid properties, namely density ρ , specific heat c_p , thermal conductivity k_f , dynamic viscosity μ , and given properties of the fin, that is, surface emittance ϵ , solar absorptance α_s , and thermal conductivity k .

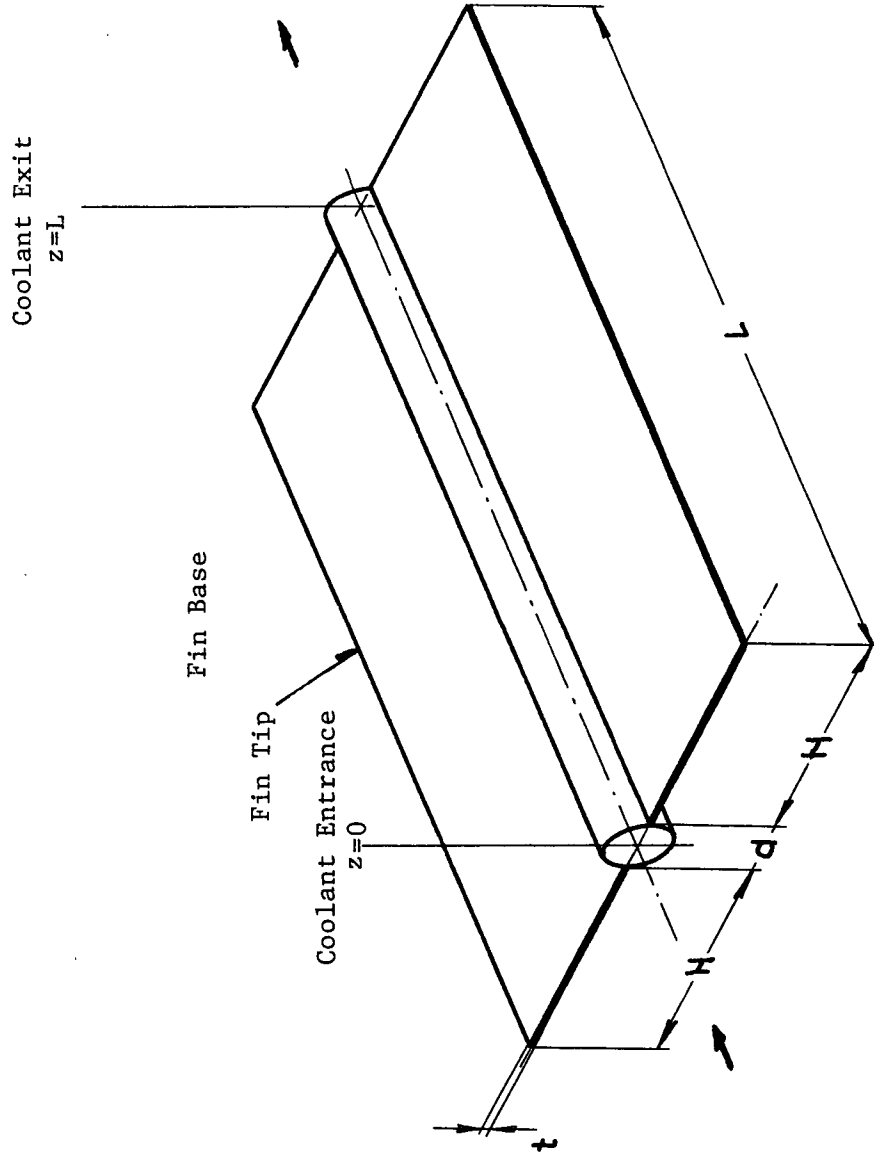


Figure 1. Geometry of Fin System Element

C. Governing Equations

1. Conservation of Energy

Setting the local change of the fluid enthalpy flux first equal to the local heat exchange per unit tube length between fluid and tube wall, and then equal to the radiative heat rejection per unit tube length one obtains, for i effective sides of the radiator:

$$-\dot{m} c_p \frac{dT_f}{dz} = \pi d \bar{h}_c (T_f - T_b) \quad (1)$$

$$\pi d \bar{h}_c (T_f - T_b) = 2iH\epsilon\sigma\bar{\eta}(T_b^4 - T_s^4) \quad (2)$$

where \bar{h}_c and σ represent, respectively, the convective film coefficient and the Stefan-Boltzmann constant. The symbol $\bar{\eta}$ represents the overall tube-and-fin effectiveness and is evaluated in Section 3. The convective film coefficient is computed from the Nusselt number N_{Nu}

$$\bar{h}_c = N_{Nu} \frac{k_f}{d} \quad (3)$$

the evaluation of which is deferred to Section 2. The equivalent sink temperature T_s is computed from the known incident normal radiant heat flux q'' by

$$T_s = \sqrt[4]{\frac{\alpha_s q''}{\epsilon \sigma}} \quad (4)$$

The first-order differential equation, Eq. 1, is subject to the initial condition at $z = 0$

$$T_f(0) = T_o \quad (5)$$

Equations 1 and 2 determine the two dependent variables $T_f(z)$ and $T_b(z)$.
Integration of Eq. 1 from $z = 0$ to $z = L$ gives the unknown fluid exit temperature T_e .

2. Convective Film Coefficient

The Nusselt number N_{Nu} in Eq. 3 depends on the Reynolds number N_{Re} , the Prandtl number N_{Pr} and the d/L ratio.

$$N_{Re} = \frac{4\dot{m}}{\pi d \mu} \quad (6)$$

$$N_{Pr} = \frac{\mu c_p}{k_f} \quad (7)$$

For laminar flow, $N_{Re} \leq 2300$, of non-metallic fluids, $N_{Pr} \geq 0.1$, Hausen [3] established the relation

$$N_{Nu} = \left[3.65 + \frac{0.0668 N_{Re} N_{Pr} \frac{d}{L}}{1 + 0.045 (N_{Re} N_{Pr} \frac{d}{L})^{2/3}} \right] \left(\frac{\mu_f}{\mu_w} \right)^{0.14} \quad (8)$$

The nomogram in Figure 2, taken from the VDI Waermeatlas,* facilitates the estimate of the Nusselt number in accordance with Eq. 8.

For turbulent flow, $N_{Re} > 2300$, of non-metallic fluids, $N_{Pr} \geq 0.1$, similarity considerations lead to

$$N_{Nu} = 0.116 \left[1 + \left(\frac{d}{L} \right)^{2/3} \right] (N_{Re}^{2/3} - 125) N_{Pr}^{1/3} \left(\frac{\mu_f}{\mu_w} \right)^{0.14} \quad (9)$$

which is also presented in a nomogram in Figure 3.

Liquid metal convective heat transfer in tubes, $N_{Pr} < 0.1$, may be represented by the result of the work by Seban and Shimazaki [4] which is

*VDI-Verlag GMBH, Düsseldorf, West Germany

valid for $(N_{Re} N_{Pr}) > 100$ and $L/d > 60$

$$N_{Nu} = 5.0 + 0.025 (N_{Re} N_{Pr})^{0.8} \quad (10)$$

Other Nusselt number relationships may be more suitable in a particular case. Their selection does not affect the ensuing analysis because the Nusselt number calculation is part of the input data preparation, prior to the numerical evaluation of the solution.

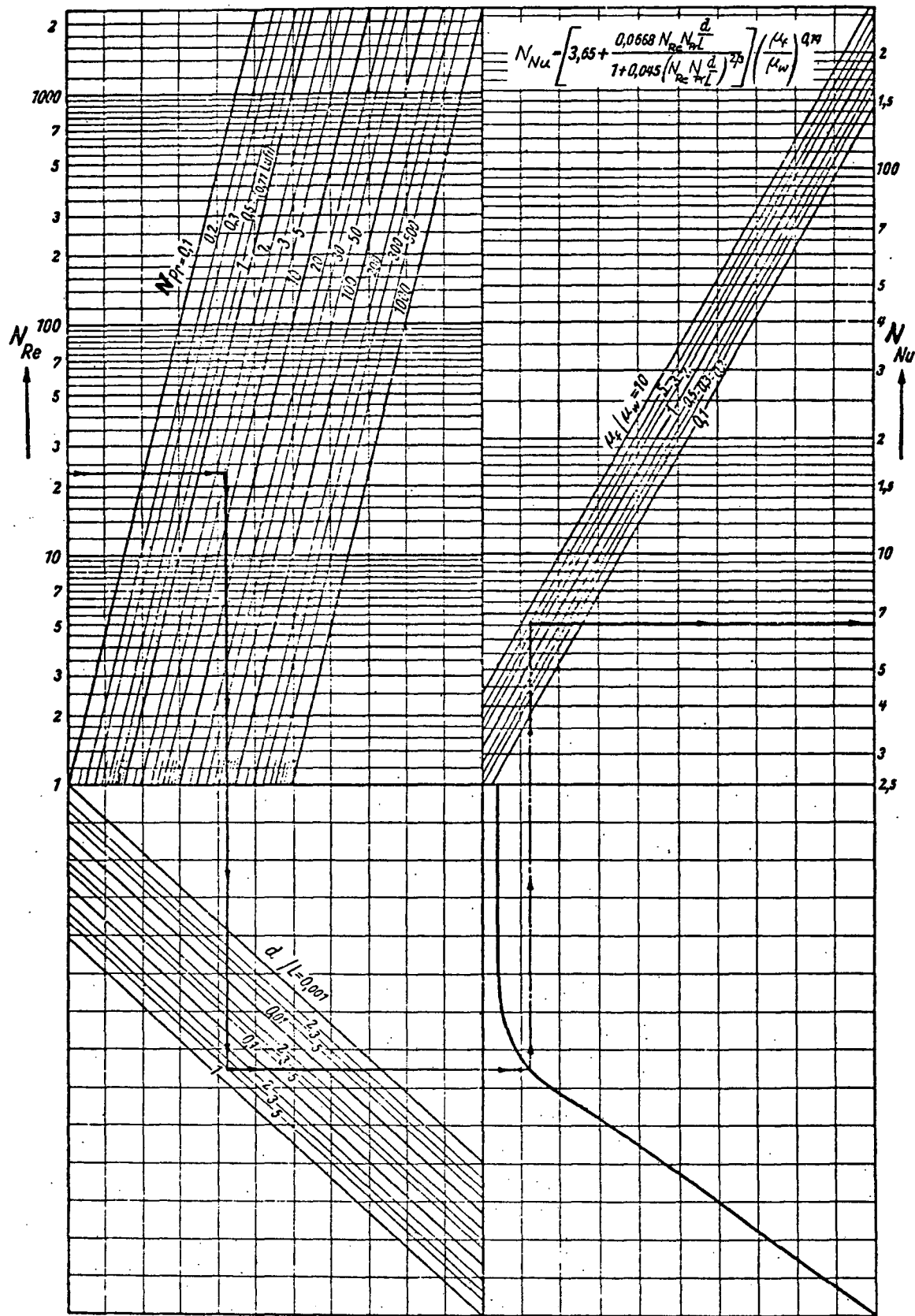


Figure 2. Nusselt Number Nomogram for Laminar Flow of Non-Metallic Coolant Fluids, Eq. 8. (VDI Waermeatlas)

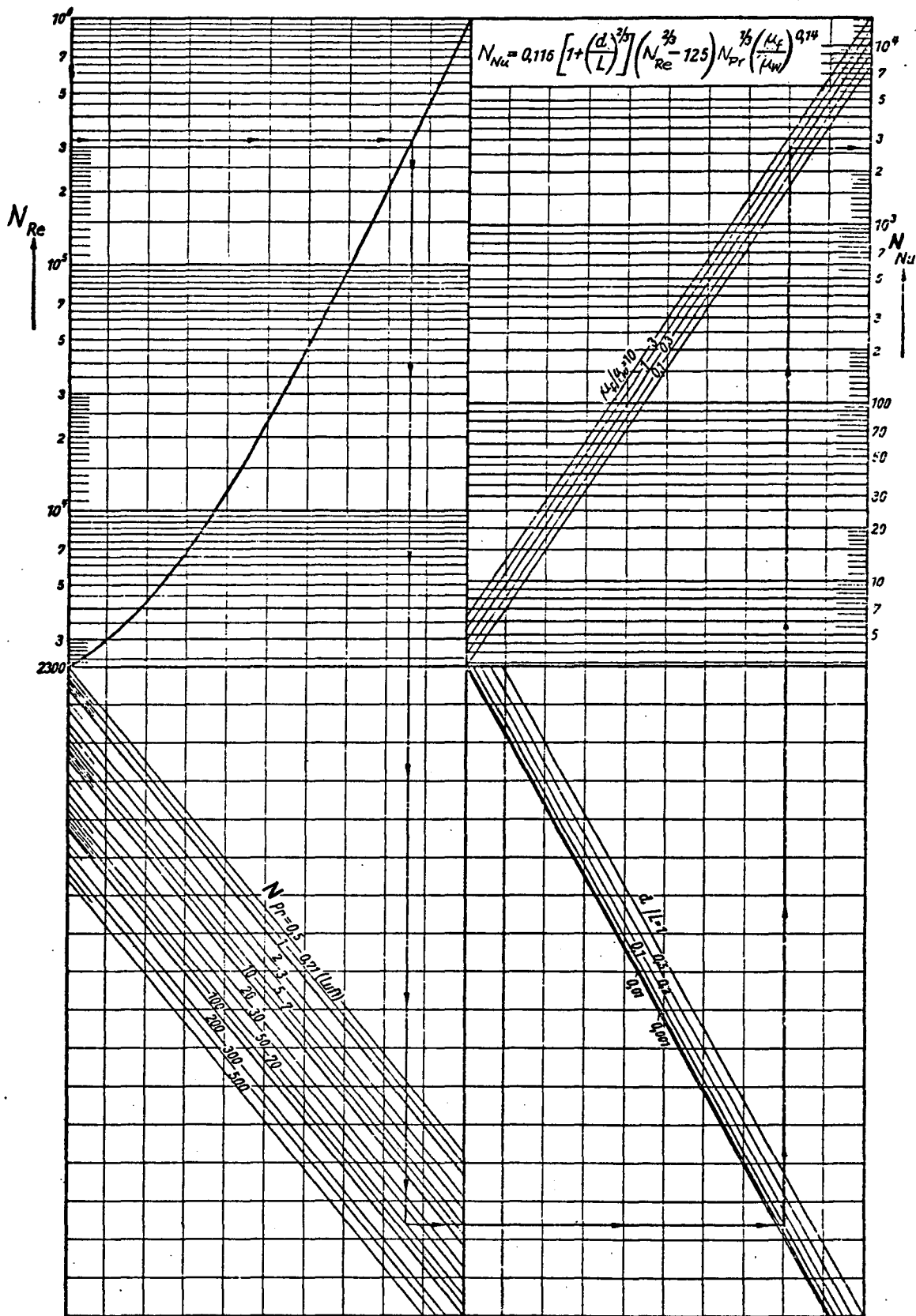


Figure 3

Figure 3. Nusselt Number Nomogram for Turbulent Flow of Non-Metallic Coolant Fluids, Eq. 9. (VDI Waermeatlas).

3. Total Fin-Tube Effectiveness

The symbol $\bar{\eta}$ in Eq. 2 denotes the overall radiative fin-and-tube effectiveness and accounts not only for the non-uniform temperature distribution within the fin and normal to the flow direction, but also for the effects on the radiative heat transfer from the tube. These effects are due to the additional radiating tube area and the partial blockage of emission from the fin and the tubes by the tubes of the neighboring fin elements. Adding the contributions from the tube to that of the fin, one obtains

$$\bar{\eta}(z) = M(z) \cdot \eta(z) + N \quad (11)$$

Here, $\eta(z)$ is the radiative fin effectiveness of the unobstructed fin, Eqs. 32, [5,6,7] and varies with the fin base temperature $T_b(z)$. The factor M is the product of the shape factor of the fin with respect to the sink, F_{fs} , and the corrective term f on η for the temperature profile distortion resulting from the tube-fin interaction [8]:

$$M = F_{fs}(\lambda) \cdot f(\lambda, N_c) \quad (12)$$

where

$$\lambda = \frac{4H}{d} \quad (13)$$

and

$$N_c = \frac{2\epsilon\sigma H^2}{kt} [T_b(z)]^3 \quad (14)$$

which is the well-known conduction parameter. Hottel's crossed-string method yields

$$F_{fs}(\lambda) = \left(\sqrt{\lambda(\lambda + 2)} + \arcsin \frac{1}{1 + \lambda} - \pi/2 \right) / \lambda \quad (15)$$

and the curve fit of data in Reference [8] resulted in

$$f(\lambda, N_c) = 1 - (N_c/\lambda)(0.1460 N_c - 0.02866) . \quad (16)$$

Finally, the symbol N in Eq. 11 represents the radiative heat rejection contributed by the tubes and is the shape factor of the tube with respect to the sink, multiplied by the tube-to-fin area ratio

$$N(\lambda) = \pi \left[1/2 + \left[\lambda + 2 - \sqrt{\lambda(\lambda + 2)} - \arcsin \frac{1}{\lambda + 1} \right] / \pi \right] / \lambda \quad (17)$$

This completes the description of the overall fin-and-tube effectiveness. In summary it should be emphasized that axial conduction, radial tube wall temperature variation, kinetic and potential coolant energies, and end effects are ignored, that radiative interaction between tube and fin and between tubes is only approximate and that the representation of Eq. 16 is limited to $T_s < 0.8 T_b$ (but could be extended, in principle).

D. Scaling Parameters

Effective analysis, numerical integration, graphical representation of numerical results and, ultimately, the system optimization makes the reduction of parameters mandatory. Introduce the non-dimensional

$$\text{axial distance} \quad \zeta = \frac{z}{L} \quad (18)$$

$$\text{temperature} \quad \theta = T/T_o \quad (19)$$

$$\text{reference conduction parameter} \quad \bar{N}_c = \frac{2\epsilon\sigma T_o^3 H^2}{kt} \quad (20)$$

$$\text{ratio of convective to radiative resistance} \quad V = \frac{1}{\pi} \frac{t}{H} \frac{k}{k_f} \frac{\bar{N}_c}{N_{Nu}} \quad (21)$$

$$\text{convection number} \quad U = \pi N_{Nu} / N_{Gz} \quad (22)$$

where the Graetz number N_{Gz} is defined by

$$N_{Gz} = (c_p \dot{m}) / (k_f L) = \frac{\pi}{4} \frac{d}{L} N_{Re} N_{Pr} \quad (23)$$

With these parameters and the λ defined by Eq. 13 one may recast the problem as previously established by Eqs. 1,2 and 5 as given by Eqs. 24 through 26:

$$\frac{d\theta_f}{d\zeta} = -U(\theta_f - \theta_b) \quad (24)$$

$$\theta_f - \theta_b = V\bar{n}(\theta_b^4 - \theta_s^4) \quad (25)$$

subject to the initial condition at $\zeta = 0$

$$\theta_f(0) = 1 . \quad (26)$$

Integration of Eq. 24 subject to Eqs. 25 and 26 yields the coolant fluid exit temperature θ_e sought

$$\theta_e = \theta_f(1) \quad (27)$$

and, consequently, this coolant fluid exit temperature is a function of five parameters

$$\theta_e = \theta_e(U, V, \bar{N}_c, \lambda; \theta_s) . \quad (28)$$

The first four parameters correspond to the geometrical dimensions L, H, t and d of the radiator system and θ_s represents the environment.

E. Solution

Equation 25 is transcendental because of $\bar{\eta}(\theta_b)$ and would require iterative solutions at every step of the numerical integration of Eq. 24. It is more economical to derive a second differential equation for θ_b by differentiating Eq. 25

$$\frac{d\theta_b}{d\zeta} = \frac{-U}{\frac{1}{\theta_f - \theta_b} + \frac{1}{\bar{\eta}} \frac{d\bar{\eta}}{d\theta_b} + \frac{4\theta_b^3}{\theta_b^4 - \theta_s^4}} \quad (29)$$

and to obtain the initial condition for Eq. 29 through a single iterative process (Newton Raphson method) from

$$V\bar{\eta}(\theta_b^4 - \theta_s^4) + \theta_b = 1 \quad \text{at} \quad \zeta = 0 \quad (30)$$

The derivative $d\bar{\eta}/d\theta_b$ is obtained from Eqs. 11 and 16

$$\begin{aligned} \frac{d\bar{\eta}}{d\theta_b} &= \frac{d\bar{\eta}}{dN_c} \frac{dN_c}{d\theta_b} = 3 \bar{N}_c \theta_b^2 \frac{\partial}{\partial N_c} (M\eta) \\ &= 3\bar{N}_c \theta_b^2 \left\{ \eta F_{fs} \left[0.02866 - 0.2920 \bar{N}_c \theta_b^3 \right] / \lambda \right. \\ &\quad \left. + M \frac{d\eta}{dN_c} \right\} \end{aligned} \quad (31)$$

which can be evaluated once the fin effectiveness $\eta(N_c)$, that is the ratio of the actual power loss from an unobstructed (tubless) fin panel to the power loss from an ideal, unobstructed fin of infinite thermal conductivity, is represented by a power polynomial:

$$\eta(N_c) = \sum_{i=0}^6 a_i (N_c)^i \quad (32a)$$

where

$$\begin{aligned} a_0 &= 1.000\ 000 \\ a_1 &= -1.163\ 143 \\ a_2 &= 1.478\ 836 \\ a_3 &= -1.267\ 550 \\ a_4 &= 0.632\ 522\ 3 \\ a_5 &= -0.162\ 706\ 7 \\ a_6 &= 0.016\ 542\ 23 \end{aligned}$$

Equation 32 is valid for $0 \leq N_c \leq 2.5$. For greater values, $N_c > 2.5$

$$\eta(N_c) = 0.686\ 609\ 5 e^{-0.229\ 771\ 8} \quad (32b)$$

Equations 24 and 29 have been integrated by a fourth-order Runge-Kutta procedure [2], subject to initial conditions given by Eqs. 26 and 30. The result of the integration yields primarily Θ_e in the form of Eq. 28.

F. Results

A typical computer print-out of the results is shown in Figure 4. First are presented the five parameters $\{\theta_s; U, V, \bar{N}_c, \lambda\}$ of Eq. 28, as read-in. Following that is a table in which are listed, as functions of axial distance measured from the coolant fluid inlet, the fluid temperature $\theta_f = \text{THETAF}$, the fin base temperature $\theta_b = \text{THETAB}$, next the local conduction parameter $N_c = \text{NC}$, the local total fin-plus-tube effectiveness $\bar{\eta} = \text{ETABAR}$, the local fin effectiveness $\eta = \text{ETA}$, the nondimensional axial position $\zeta = \text{ZETA}$ and, finally, the number of integration steps required to reach the particular axial position. The number of integration steps depends on the chosen error limits and the rates of variable changes.

The time rate of heat rejection per fin element (tube) is to be computed from

$$\dot{m} c_p (T_o - T_e) = \dot{m} c_p T_o (1 - \theta_e) \quad (32)$$

Parameter studies are presented in Figures 5 through 9. The non-dimensional fluid exit temperature is plotted versus non-dimensional fin panel area with the temperature θ_s (Fig. 5), the non-dimensional tube spacing λ (Figs. 6 and 7) and the reference conduction parameter \bar{N}_c (Figs. 8 and 9) as parameters.

THETA-S = .90000
 U = .100003+01
 V = .200000+01
 ETAR = .200000+00
 LAMDA = .250000+02

THETA	THETA3	MC	ETAR	ETA	ZETA	STEP NO
1.00000	.83159	.11763	.96420	.881581	.00	1
.99967	.835315	.116568	.965251	.882615	.10	2
.976137	.83277	.115468	.966145	.883569	.20	4
.950937	.83231	.114453	.967048	.884452	.30	5
.924763	.827954	.113513	.967806	.885267	.40	6
.893554	.825842	.112656	.968583	.886020	.50	7
.863200	.823916	.111861	.969283	.886716	.60	8
.833659	.822113	.111128	.969892	.887359	.70	9
.804875	.820473	.110453	.970473	.887953	.80	10
.776764	.818898	.109830	.971009	.888501	.90	11
.749284	.817467	.109255	.971503	.889008	1.00	12

FIGURE 4. TYPICAL COMPUTER PRINT-OUT FOR RADIATOR SYSTEM PERFORMANCE

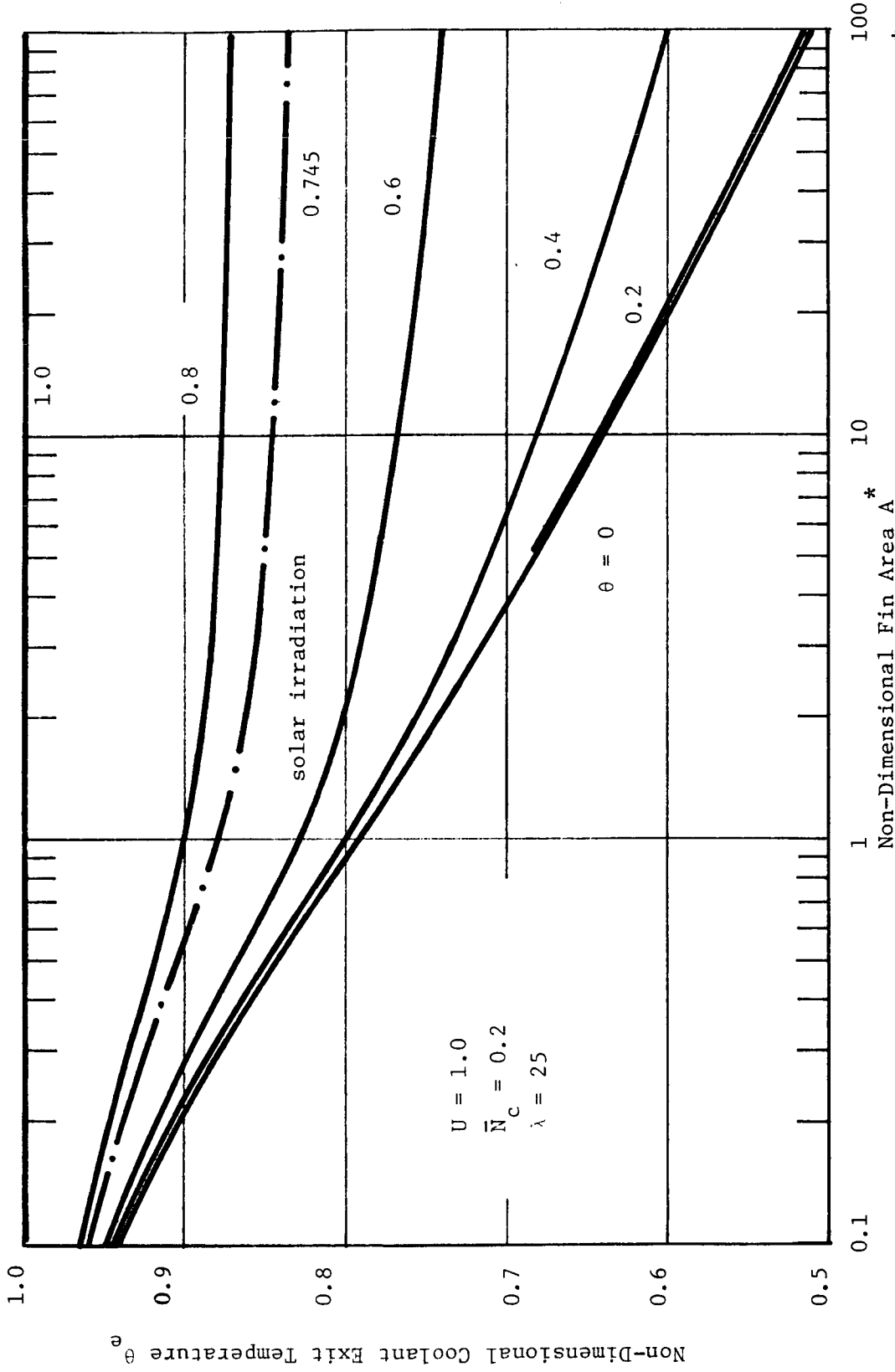


Figure 5. Non-Dimensional Coolant Exit Temperature θ vs. Non-Dimensional Fin Panel Area A^* with Sink Temperature θ_s As Parameter.

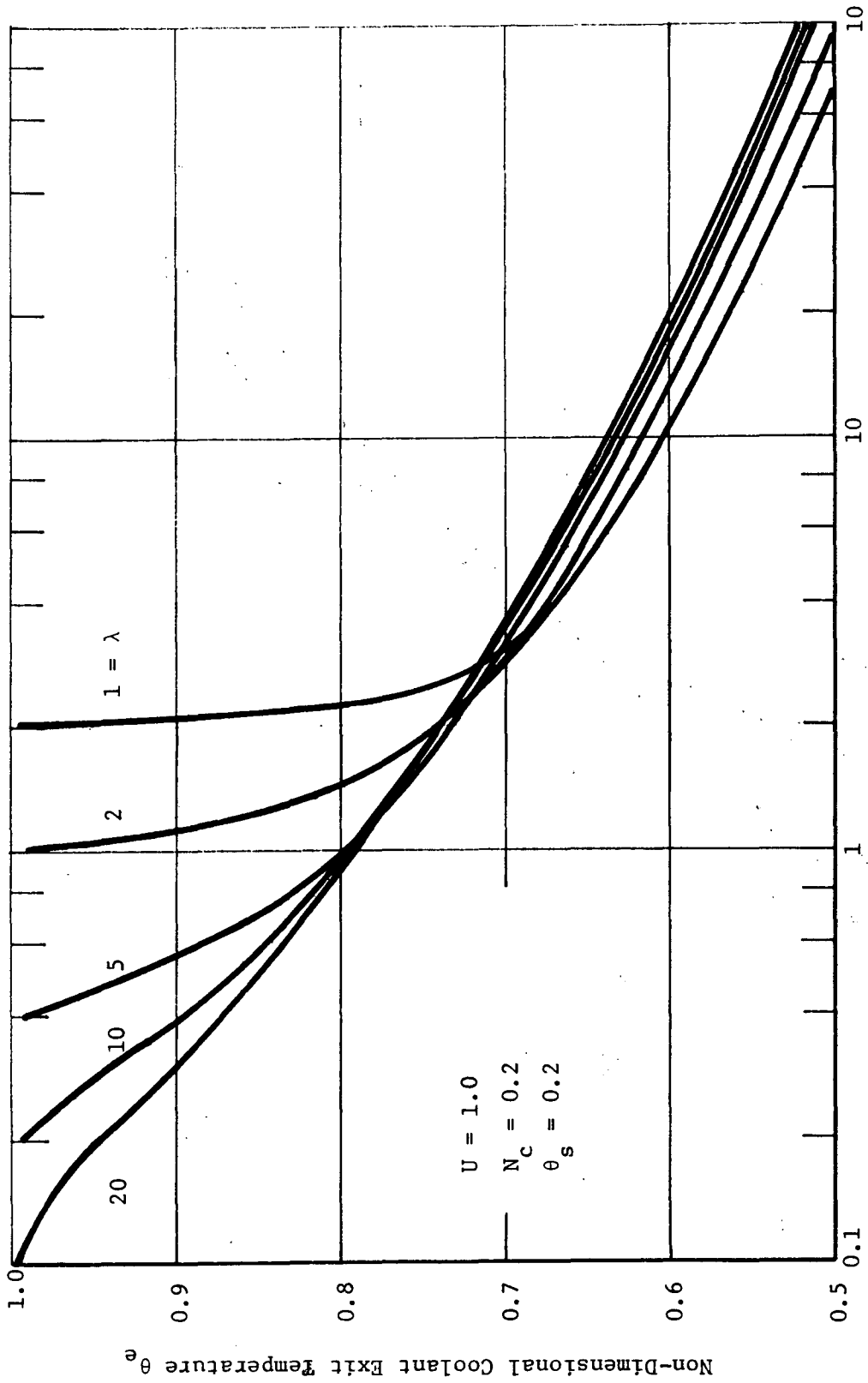


Figure 6. Non-Dimensional Coolant Exit Temperature vs. Non-Dimensional Fin Area For Constant U and Varying λ

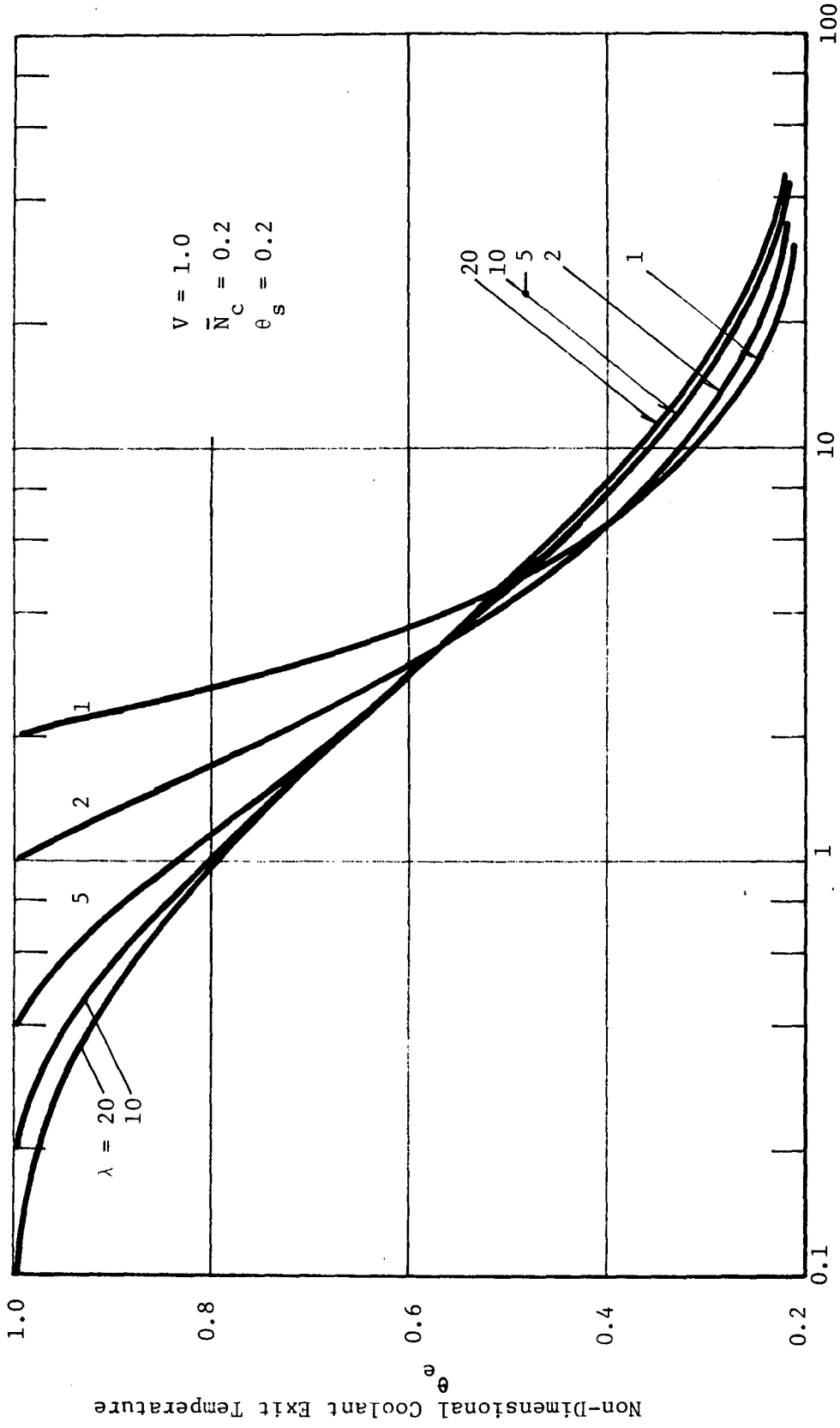


Figure 7. Non-Dimensional Coolant Exit Temperature vs. Non-Dimensional Fin Area A^* For Constant V and Varying λ

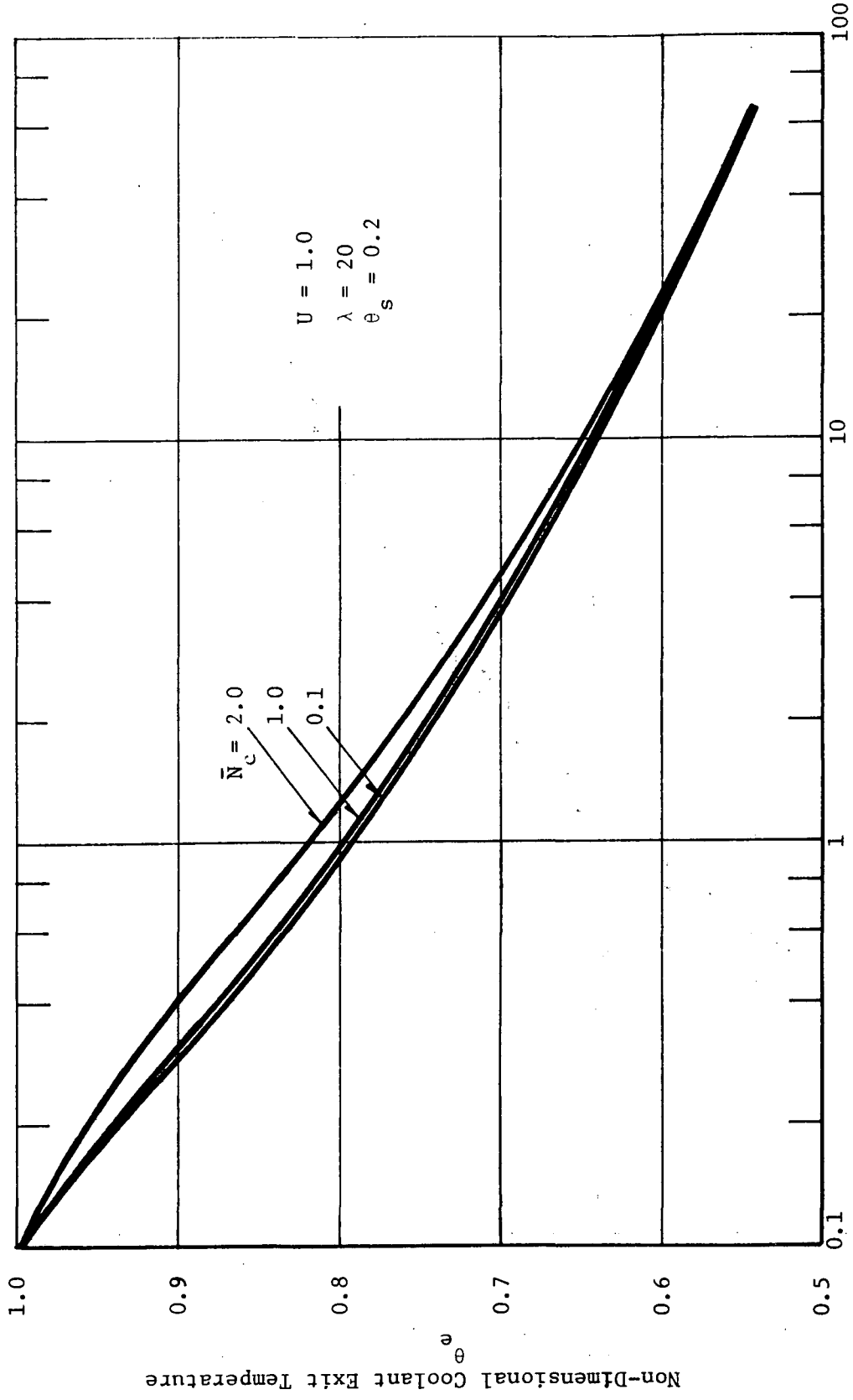


Figure 8. Non-Dimensional Coolant Exit Temperature VS. Non-Dimensional Fin Area For Varying Conduction Parameter and Long Fins.

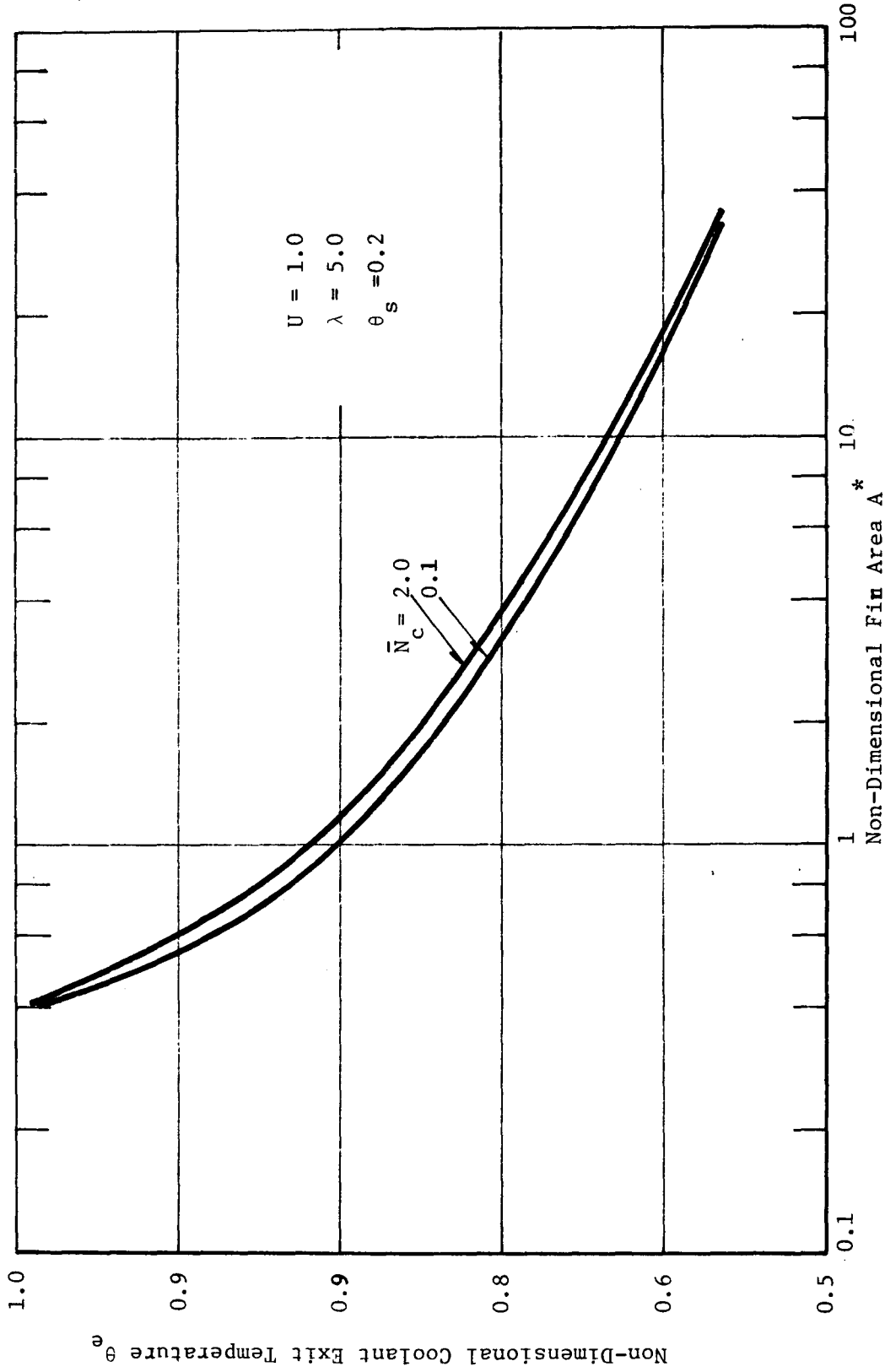


Figure 9. Non-Dimensional Coolant Exit Temperature VS. Non-Dimensional Fin Area For Varying Conduction Parameter and Short Fins

III. OPTIMIZATION OF THE RADIATOR SYSTEM

A. Purpose

In the design of the radiator system all parameters describing the system objectives and the system environment are prescribed beforehand while, at some occasions and within certain limits, the geometry of the system may be selected in the process of the design. This possible freedom of choice leads to the optimization of the radiator system geometry.

The primary purpose of the radiator system is to lower the coolant fluid temperature. For a given set of constraints the radiator with the lowest fluid exit temperature is considered here to be an optimum radiator system.

The set of constraints to be imposed on the optimum radiator system must be selected for a particular set of circumstances. In this analysis two sets out of many possible constraints were selected, that is, weight (or volume) and projected area of the radiator are considered to be prescribed.

The process of optimization proposed here, namely to find the minimum coolant fluid exit temperature for either a fixed radiator area or a fixed mass may be inverted to yield the minimum radiator area or weight for a prescribed cooling rate.

The optimization process can be outlined in the following steps:

- (i) select, for given coolant exit temperature

$$\theta_e = \theta_e \{U, V, \bar{N}_c, \lambda; \theta_s\} \quad (28)$$

that optimum set $\{U, V, \bar{N}_c, \lambda\}$ of geometric parameters which constitutes, under selected constraints, the system geometry for the lowest possible coolant exit temperature,

- (ii) transform the non-dimensional groups U , V and \bar{N}_c into suitable, non-dimensional radiator length L^* , fin height H^* and panel thickness t^* ,

(iii) calculate the physical dimensions L , H , t and d of the optimum radiator system.

If all fin elements operate under optimum conditions then the radiator as a whole operates under optimum conditions.

B. Problem Formulation

1. General

Of the five parameters U , V , \bar{N}_c , λ and θ_s which define θ_e only the first four can be considered independent while θ_s is determined by the incident radiant flux. For simplicity let us introduce the vector \underline{X} with components $x_1 = U$, $x_2 = V$, $x_3 = \bar{N}_c$ and $x_4 = \lambda$. The minimum coolant fluid exit temperature $\theta_e(\underline{X})$, subject to $r \leq 3$ constraints may be obtained from the necessary conditions for a relative extremum

$$\frac{\partial \theta_e}{\partial x_i} = 0 \quad i = 1, \dots, (4 - r) \quad (33)$$

and the r constraints

$$\varphi_j(\underline{X}) = 0 \quad j = 1, \dots, r \quad (34)$$

This problem formulation implies that the r constraint equations can be solved explicitly for r components of \underline{X} which can be substituted into Eqs. 33 to yield $(4 - r)$ equations for the remaining $(4 - r)$ components. This was in effect achieved by replacing the Nusselt number relationships given in Eqs. 8 and 9 by a simpler relation of the form

$$N_{Nu} = c N_{Re}^m N_{Pr}^n (d/L)^p \quad (35)$$

with appropriate constants $c = 0.023$, $m = 0.8$, $n = 1/3$, $p = 0$, for $N_{Re} \geq 2,300$; and $c = 1.86$, $m = n = p = 1/3$ for $N_{Re} < 2,300$. The method of Lagrangian multipliers, however, permits the retention of the original constraints at the expense of additional, computational efforts in the case of fixed-mass constraints, since Eqs. 34 need not to be solved explicitly for \underline{X} .

Two sets of constraints have been considered. Both sets have in common four sets of bounds

$$\left. \begin{aligned}
 U_{\min} &\leq x_1 \leq U_{\max} \\
 V_{\min} &\leq x_2 \leq V_{\max} \\
 (\bar{N}_c)_{\min} &\leq x_3 \leq (\bar{N}_c)_{\max} \\
 \lambda_{\min} &\leq x_4 \leq \lambda_{\max}
 \end{aligned} \right\} \quad (36)$$

which represent practical limits of the design parameters x_i , $i = 1, \dots, 4$. Should the search procedure lead to the intersection of any of the above limits, then their appropriate equalities would enter the set of constraints. The other two constraints, namely of fixed volume or of fixed area, are discussed below.

2. Area Constraint

Introduce the characteristic length of a single fin element

$$L_o = \sqrt{\frac{\dot{m} c_p}{i \epsilon \sigma T_o^3}} \quad (37)$$

which may be interpreted as the length of a square fin element whose effectiveness is unity and which reduces the fluid temperature to zero. Dividing the physical dimensions L , H , t and d by the reference length L_o one obtains the non-dimensional geometric quantities L^* , H^* , t^* and d^* respectively. The normalized projected fin element area is (for $t \ll d$)

$$A^* = A/L_o^2 = [2HL + dL]/L_o^2 \quad (38)$$

Consequently, the constraint of "fixed area," the first of Eq. 34, becomes

$$\varphi_1 = 2H^*L^*[1 + 2/\lambda] - A^* = 0 \quad (39)$$

or

$$\varphi_1(x_1, x_2, x_4) = x_1 x_2 (1 + 2/x_4) - A^* = 0 \quad (40)$$

This constraint equation can be solved explicitly for any one of its arguments, regardless of applicable Nusselt number relationship (see comments following Eq. 34).

The constant area constraint may be supplemented by an additional constraint reflecting the preference for a particular fin panel thickness, arising from manufacturing considerations. A fixed panel thickness t , or equivalently t^* would require

$$\varphi_2(\underline{X}) = t^* - \phi_1 x_2^2 / x_3 \cdot N_{Nu}^2(\underline{X}) = 0 \quad (41)$$

where ϕ_1 is known beforehand

$$\phi_1 = (1/2i) (\pi k_f/k)^2 k^2 / (i \dot{m} C_p \epsilon \sigma T_o^3) \quad (42)$$

Equation 41 depends on the Nusselt number relationship used. It becomes a necessary constraint when the optimization tends toward panel thicknesses which approach the tube diameter.

3. Volume Constraint

The volume constraint is stipulated by the desire to design a radiator system of minimum mass. The coolant mass may (liquids) or may not (gases) contribute significantly to the total mass.

The mass of one fin element is, under the assumption of a tube wall thickness, equal to the fin panel thickness

$$M^* = \frac{M}{\phi_1 M_o} = L^* t^* [2H^* + \pi(d^* - t^*)] \approx \frac{UV^3}{\bar{N}_c} \left[1 + \frac{2\pi}{\lambda} \right] N_{Nu}^2 \quad (43)$$

provided $t^* \ll d^*$. Here $M_o = \rho L_o^3$ is the reference mass and M the physical mass of the structure. With

$$\phi_2 = 2i(\rho_f/\rho)(k/k_f) \quad (44)$$

the coolant fluid mass may be expressed as

$$M_f^* = \frac{M_f}{\phi_1 M_o} = \phi_2 N_{Nu} \left(\frac{V}{\lambda} \right)^2 U \quad (45)$$

Consequently, the "volume constraint" becomes

$$\varphi_1(\bar{X}) = M_{tot}^* - x_1 x_2^2 N_{Nu}(\bar{X}) \left\{ x_2 [1 + 2\pi/x_4] N_{Nu}/x_3 + \phi_2/x_4^2 \right\} = 0 \quad (46)$$

where $M_{tot}^* = M^* + M_f^*$. Equation 46 reveals that while $\phi_2 > 1$ the fluid mass contributes to the total mass only when x_4 becomes small. For the expected cases of $x_4 \approx 10$ Eq. 46 reduces to a volume constraint as the influence of the density ratio ρ/ρ_f vanishes.

4. Sufficiency Requirements

An optimum radiator is found at \underline{X}_m when $\theta_e(\underline{X}_m)$ is a minimum, that is, when in the vicinity of \underline{X}_m

$$\theta_e(\underline{X}_m + \underline{\delta}) > \theta_e(\underline{X}_m) \quad (47)$$

where $\underline{\delta}$ is a small vector, with components $\{\Delta x_1, \dots, \Delta x_4\}$, and with its endpoint on the hypersurface defined by Eqs. 34.

There exist analytical expressions for the sufficiency conditions in terms of second-order derivatives $\partial^2 \theta_e / \partial x_i \partial x_j$ which are applicable when either all constraints can be solved explicitly as implied by Eqs. 33 and 34 or the number of constraints is at least two. Since, however, θ_e is obtained through numerical integration of Eqs. 24 and 29 and the sufficiency test is to be performed only once the potential optimum is found, it appears economical to evaluate Eq. 47 directly. Further developments concerning the sufficiency criteria are necessary at this time.

C. Solution

1. The Optimum

The remaining task is to solve the system of Eqs. 33 as they are obtained after substitution of Eqs. 34. The solution is obtained through an iterative process based on the Newton-Raphson procedure. Starting with an estimated set of parameters \underline{X}_1 the iteration is carried on according to

$$\underline{X}_{k+1} = \underline{X}_k + \Delta \underline{X}_k, \quad k = 1, 2, \dots \quad (48)$$

where \underline{X}_k represents the current, \underline{X}_{k+1} the future parameter set and the increments $\Delta \underline{X}_k$ are the solution to the system of linear algebraic equations

$$\underline{Y}_k = (\underline{A})_k (\Delta \underline{X})_k. \quad (49)$$

The current components $(y_i)_k$ of \underline{Y}_k are the current values of the derivatives

$$y_i = - \frac{\partial \theta_e}{\partial x_i}, \quad i = 1, \dots, (4 - r). \quad (50)$$

The current elements $\{A_{ij}\}_k$ of the square matrix $(\underline{A})_k$ are the second-order derivatives

$$A_{ij} = \frac{\partial^2 \theta_e}{\partial x_i \partial x_j}; \quad i, j = 1, \dots, (4 - r). \quad (51)$$

It is obvious that the matrix A_{ij} is symmetric and one needs to compute only $(5 - r)(4 - r)/2$ independent, second-order derivatives.

The derivatives in Eq. 50 and 51 are obtained from Eqs. 24 and 25 by first differentiating with respect to x_i , $i = 1, \dots, (4 - r)$ and then interchanging the order of differentiation. This leads first to $2(4 - r)$ first-order, ordinary, non-linear differential equations for

$$\begin{aligned}
 -\frac{dy_i}{d\zeta} &= \frac{d}{d\zeta} \left(\frac{\partial \theta_f}{\partial x_i} \right), \quad i = 1, \dots, (4 - r) \\
 -\frac{dy_i}{d\zeta} &= \frac{d}{d\zeta} \left(\frac{\partial \theta_b}{\partial x_i} \right), \quad i = (5 - r), \dots, (8 - 2r)
 \end{aligned} \tag{52}$$

and then to $(5 - r)(4 - r)$ first-order, ordinary non-linear differential equations for

$$\left. \begin{aligned}
 \frac{dA_{ij}}{d\zeta} &= \frac{d}{d\zeta} \left(\frac{\partial^2 \theta_f}{\partial x_i \partial x_j} \right) \\
 \frac{dB_{ij}}{d\zeta} &= \frac{d}{d\zeta} \left(\frac{\partial^2 \theta_b}{\partial x_i \partial x_j} \right)
 \end{aligned} \right\} \tag{53}$$

The second sets of equations in Eqs. 52 and 53 are necessary because of the dependence of θ_e on θ_b . All initial conditions, at $\zeta = 0$, for Eqs. 52 and 53 can be derived from Eqs. 26 and 30

$$y_i(0) = (y_o)_i, \quad A_{ij}(0) = (A_o)_{ij}, \quad B_{ij}(0) = (B_o)_{ij}. \tag{54}$$

In summary, one needs to integrate, together with Eqs. 24 and 29, the Eqs. 52 and 53, subject to the initial conditions given by Eqs. 26, 30 and 54. The integration is carried out from $\zeta = 0$ to $\zeta = 1$ where it yields not only θ_e and $\theta_b(1)$ but also all derivatives in Eqs. 49. This system is solved for the components of $\Delta \underline{X}$, then a new set of parameters \underline{X} is computed from Eqs. 48 and the iterative cycle repeated. The repetitions are continued until either the first $(4 - r)$ y_i 's are small or one of the inequalities in Eqs. 36 is violated. Should that happen then an additional constraint is introduced, r is incremented by one, and the cycle is continued until either all limits in Eqs. 36 are reached or the remaining y_i 's are sufficiently small. The result may or may not be an optimum for the initially chosen A^* or M^* . Finally, the potential optimum is tested in accordance with Eq. 47.

2. Parameter Transformation and Physical Dimension of Optimum Radiator System.

Once the optimum set $\{x_1, \dots, x_4\}_m$ is found it is necessary to compute from this the physical dimensions L , H , t and d which define the geometry of the radiator system. To accomplish this task the set $\{x_1, \dots, x_4\}_m$ is first transformed into the previously introduced set of normalized dimensions $\{L^*, H^*, t^*, d^*\}$. This transformation is, in general, not possible in explicit form. However, when the simplified Nusselt number relation of the form given by Eq. 35 is substituted for the more general expressions in Eqs. 8 and 9 then L^* , H^* , t^* and d^* can be expressed explicitly in terms of the parameters $\{x_1, \dots, x_4\}$.

Define first the starred quantities.

$$N_{Gz}^* = \frac{c \dot{m}}{k_f L_o} \quad (55)$$

$$N_{Re}^* = \frac{4 \dot{m}}{\pi \mu L_o} \quad (56)$$

$$N_{Nu}^* = c (N_{Re}^*)^m (N_{Pr})^n \quad (57)$$

$$N_c^* = \frac{2 \epsilon \sigma T_o^3 L_o}{k} \quad (58)$$

which are essentially the unstarred quantities evaluated with the reference length instead of any other dimension and which are all known from system objectives and environmental conditions.

Next one needs to distinguish between laminar and turbulent coolant flow as the constants c , m , n and p are different for the two regimes.

For laminar flow, $c = 1.86$, $m = n = p = 1/3$.

$$L^* = \frac{N_{Gz}^*}{2\pi \sqrt{c^3}} \sqrt{x_1^3} \quad (59)$$

$$H^* = \pi \sqrt{c^3 / N_{Gz}^*} \frac{x_2}{\sqrt{x_1}} \quad (60)$$

$$t^* = \pi^2 c N_c^* / (N_{Gz}^*)^2 \frac{x_2^2}{x_1 x_3} \quad (61)$$

and

$$d^* = 4\pi \sqrt{c^3} / N_{Gz}^* \frac{x_2}{x_4 \sqrt{x_1}} \quad (62)$$

For turbulent flow, $c = 0.023$, $m = 4/5$, $n = 1/3$, $p = 0$.

With

$$\phi_3 = \pi N_{Nu}^* / N_{Gz}^* \quad (63)$$

one obtains

$$L^* = 1 / [2^5 \phi_3^{14}]^{1/9} x_1 \left[\frac{x_2}{x_4} \right]^{4/9} \quad (64)$$

$$H^* = 1/2 [2^5 \phi_3^{14}]^{1/9} (x_2^5 x_4^4)^{1/9} \quad (65)$$

$$t^* = N_c^* / 4 [2^5 \phi_3^{14}]^{2/9} \frac{(x_2^5 x_4^4)^{2/9}}{x_3} \quad (66)$$

$$d^* = \left[2 \phi_3 \frac{x_2}{x_4} \right]^{5/9} \quad (67)$$

Finally, multiplication of the starred quantities L^* , H^* , t^* and d^* by the reference length L_0 gives the dimension L , H , t and d of the fin radiator system with optimum performance.

D. Results

The ultimate presentation of the results from the radiator system optimization is the plot of the optimum non-dimensional geometric parameters L^* , H^* , t^* , and d^* versus the non-dimensional enthalpy rejection $(1 - \Theta_e)$. These graphs would include three or more parameters, namely the sink temperature Θ_s and the parameters occurring in the constraint equations. However, the optimum geometry is not expected to depend strongly on all parameters because of physical considerations, and convenient graphical presentation should be possible.

As indicated in the Introduction, the systematic optimization based on analytical extrema search techniques was developed in addition to the original program objectives but could not be completed within the contract period. The graphical presentation of the optimum geometry in terms of intended enthalpy rejection is therefore not included in this report.

However, computer codes were written on the basis of the solution discussed in Section C. These codes produce the optimum radiator parameters L^* , H^* , t^* and d^* based on the Nusselt number relationship in Eq. 35, for any particular set of input parameters computed from mission requirements and environmental conditions. These results are described in detail in Chapter IV, Sections C. 4 and D. 4.

IV. COMPUTER CODES

A. Introduction

Three separate FØRTRAN codes were developed, one for the simplified radiator system simulation, one for the minimum area optimization and one for the minimum mass system optimization.

The three codes have several subprograms in common and could be united into a single code to avoid duplication. The simulation program, however, is more efficient as a single program and will remain a tool by itself. The optimization programs, on the other hand, are means to develop a tool, namely suitable working charts from which to read optimum system parameters. Once these diagrams are obtained, the codes are no longer needed.

The three FØRTRAN codes are discussed separately in the following three sections but reference is made in the description of subprograms which have previously been discussed.

B. Radiator System Simulation

1. Objective

The purpose of the Simplified Radiator System Simulation (SRSS) is to evaluate the analysis developed in Chapter II for determining the coolant exit temperature

$$\theta_e(U, V, \bar{N}_c, \lambda; \theta_s)$$

in terms of the five governing groups U , V , \bar{N}_c , λ and θ_s defined by Eqs. 13, 19 through 22.

The coolant exit temperature and also the fin base temperature are obtained by integrating simultaneously Eqs. 24 and 29, subject to the initial conditions given by Eqs. 27 and 30. The integration is performed by the Runge Kutta integration procedure described in Reference [1], under variable step size mode.

The individual program units are discussed in the subsequent sections to the extent deemed necessary for the proper utilization of the code. Following the program description are presented the input and output specifications.

2. Deck Assembly

The Simplified Radiator System Simulation (SRSS) code consists of:

one		main program	MAIN
three	SUBROUTINE	subprograms	RKS SDRV SCNTL
three	FUNCTION	subprograms	ETA POLY

A block diagram is shown in Figure 7 below.

a. The MAIN Program accepts data input and lists the accepted input data. Following the input data management, the initial conditions for integration are set, an initial step size is computed and control variables are set to control the integration procedure. Then the Runge Kutta procedure RKS is called which performs the integration and indirectly the listing of results. After return from the integration, control is transferred to the start of the program for arbitrarily many repetitions of the program execution. When all input data are exhausted then control is transferred to a normal exit.

The input data preparation is discussed in Section 3 below.

The initial conditions are given through Eqs. 27 and 30. The dependent variables θ_f and θ_b are, during integration, placed in the array Y; $Y(1) = \theta_f$ and $Y(2) = \theta_b$. Equation 27 leads to the statement $Y(1) = 1.0$ and Eq. 30 is solved for θ_b by the Newton-Raphson iteration which follows the listing of accepted input data. The iteration process leads to the statement $Y(2) = \text{THETAB} (= \theta_b)$.

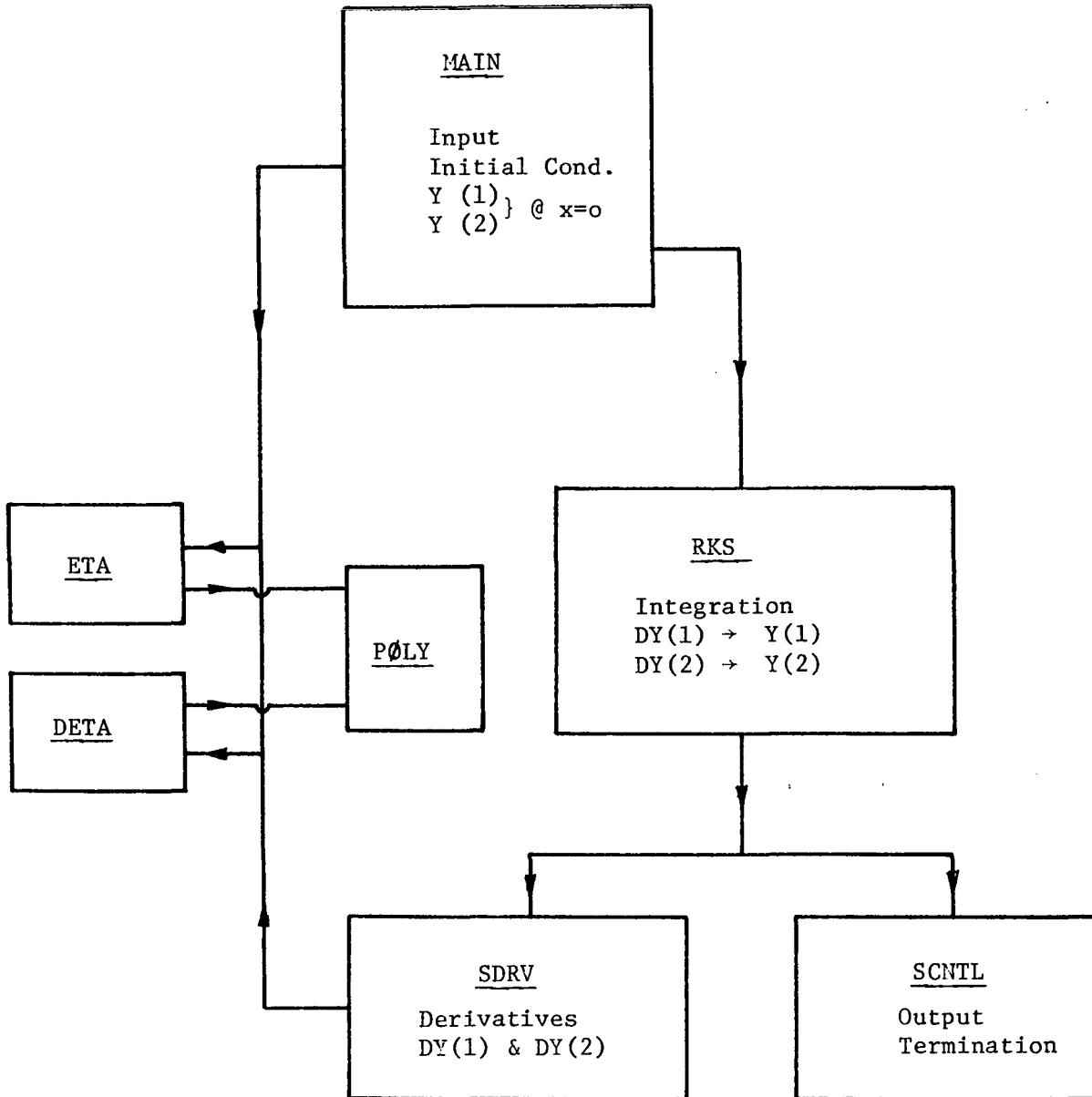


Figure 10. Block Diagram For Simplified Radiator System Simulation Code

Control variables which direct the Runge Kutta Integration
RKS are:

ZZZ = 0.0	initial value for independent variable
DX = $1/(U(1 - \theta_b))$	initial step size
IFVD = 0	variable step size selection
N = 2	two equations to be integrated
IBKP = 1	cut interval as required
NTRY = 1	normal integration mode
IERR = 0	normal error condition ($DX \neq 0$)
A(I) = 5×10^{-5} ; I = 1,2	absolute error per step
R(I) = 5×10^{-5}	relative error per step

Control variables which direct output during the integration
are:

DLMT = DXWRT/500	error limit for output interval
XWRT = 0.0	first value of independent variable at first output listing
LSTEP = 0	controls change to fixed step, LSTEP = 1 once integration step exceeds write interval DXWRT
LCNT = 0	senses cut-back (LCNT = 1) of step size prior to listing of results; used to save uncut time step
ICNT = 0	integration step counter

The CALL statement for the Runge-Kutta SUB-ROUTINE is explained in Reference [1] together with the specification of necessary DIMENSION and EXTERNAL declarations. SDRV and SCNTL must be declared EXTERNAL. The necessary array allocations can be read from the listing of the RKS code: all arrays with variable dimension (N) must be declared in MAIN for N = 2 elements. Only the elements of Y, A and R must be specified prior to the CALL RKS statement.

b. The Runge-Kutta SUBROUTINE RKS is described in detail in Reference [1]. The user is not expected to alter this code in any way and needs to know only the control features discussed in paragraph a above and the fact that RKS calls two subroutines SDRV and SCNTL.

c. The SUBROUTINE SDRV serves to evaluate the derivatives $d\theta_f/d\zeta = dY(1)$ and $d\theta_b/d\zeta = dY(2)$ in accordance to Eqs. 24 and 29. The fin effectiveness $\eta(N_c)$ and its derivative $d\eta/dN_c$ are evaluated externally by the FUNCTION subprograms ETA and DETA.

SDRV is called from RKS and supplies the derivatives, via argument list, as functions of the independent variable X and dependent variables $Y(1)$ and $Y(2)$, to the integrating procedure RKS. SDRV is called four times per integration step.

d. The SUBROUTINE SCNTL serves to provide

- (i) output listing at prescribed intervals DXWRT,
- (ii) transfer to fixed-step integration mode once the automatically selected (by RKS) step size DX exceeds the print-out interval DXWRT,
- (iii) termination of the integration procedure and RETURN to the MAIN program (via RKS). The same program, with different WRITE commands is used in the Minimum Area and Minimum Mass Optimization codes.

In the argument list are available

- (i) the dependent variables $Y(1)$ and $Y(2)$
- (ii) their derivatives $DY(1)$ and $DY(2)$
- (iii) the dependent variable X
- (iv) the step size DX which may be altered for repeat of last step
- (v) NTRY = 1 normal continuation of RKS
2 return from RKS to MAIN

- 3 repeat with new DX
- 4 restart
- (vi) IFVD = 0 variable integration step
- 1 fixed integration step

e. The FUNCTION ETA Subprogram computes the fin effectiveness $\eta(N_c)$ for the unobstructed fin in accordance to Eqs. 32a and b. The power polynomial is evaluated by calling the FUNCTION PØLY subprogram [1].

FUNCTION ETA (X) receives the independent variable $X = N_c$ and returns the fin effectiveness ETA. The two functions represented by Eqs. 32 a and b apply strictly to zero sink temperature, but the effectiveness is insensitive to the sink temperature and the equations hold sufficiently well for $\theta_s < 0.8 \theta_b$.

ETA (X) is called from MAIN and SDRV.

f. The FUNCTION DETA Subprogram computes the derivative $d\eta/dN_c$ of the fin effectiveness $\eta(N_c)$ for the unobstructed fin. The derivative is derived from Eqs. 32 a and b, and evaluated by calling the FUNCTION PØLY subprogram [1].

FUNCTION DETA (X) receives the independent variable $X = N_c$ and returns DETA = $d\eta/dN_c$. DETA (X) is called from MAIN and SDRV.

g. The FUNCTION PØLY Subprogram [1] serves to evaluate power polynomials $f(x)$ of any degree $(N - 1)$.

$$f(x) = \sum_{i=1}^N A_i X^i$$

by computing the recurrence expression

$$f_i = A_N$$

$$f_{k+1} = f_k X + A_{N-k}, k = 1, \dots, (N-1)$$

(N-1) times. The argument list of FUNCTION PØLY (N, A, X) transfers to the subprogram the number N of coefficients A_i , the one-dimensional array A(N) and the independent variable X; it returns PØLY = $f(x)$. PØLY is called from ETA and DETA.

3. Input Data Preparation

The non-dimensional groups

$$\text{THETAS} = \theta_s = T_s/T_o \quad (19)$$

$$U = \pi N_{\text{Nu}} / N_{\text{Gz}} \quad (22)$$

$$V = (i/\pi)(t/H)(k/k_f)(\bar{N}_c / N_{\text{Nu}}) \quad (21)$$

$$\text{FNGBR} = \bar{N}_c = 2\epsilon\sigma T_o^3 H^2 / (kt) \quad (20)$$

$$\text{RHOD} = \lambda = 4H/d \quad (13)$$

$$\text{DXWRT} = \Delta z/L, \text{ output intervals}$$

are computed and punched, in the above sequence, on two cards in

FORMAT (5F16.8)

There may be arbitrarily many pairs of cards as specified above, one pair for each desired simulation. They will be executed in succession. The End-of-Job card will cause normal exit from the program.

The expected run time on the UNIVAC 1108 is 0.24 seconds per simulation plus necessary compiling and collecting times. There were 32 runs executed in 14.8 seconds.

4. Output Presentation

For each simulation are printed, on a separate page, first the governing parameters as read in:

$$\text{THETAS} = \theta_s, \text{ defined by Eqs. 4 \& 19}$$

$$U, \quad " \quad \text{Eq. 22}$$

$$V, \quad " \quad \text{Eq. 21}$$

$$\text{FNGBAR} = \bar{N}_c, \quad " \quad \text{Eq. 20}$$

$$\text{LAMBDA} = \lambda, \quad " \quad \text{Eq. 13}$$

and then a table consisting of seven columns. In the first two columns are listed, as functions of axial distance ZETA = ζ at the selected intervals

$\Delta\zeta = \text{DXWRT}$, the coolant fluid temperature $\text{THETAF} = \theta_f$ and the fin base temperature $\text{THETAB} = \theta_b$. The positions $\text{ZETA} = \zeta$ are listed in the sixth column.

The conduction parameter $\text{NC} = N_c$, the combined fin-plus-tube effectiveness $\text{ETABAR} = \bar{\eta}$, defined by Eq. 11, and the fin effectiveness (unobstructed fin, Eqs. 32 a and b) $\text{ETA} = \bar{\eta}$, are listed, respectively, in the third, fourth and fifth columns. The last columns indicate the integration steps required to reach the respective axial position ζ . The desired coolant fluid exit temperature $\theta_e(U, V, \bar{N}_c, \lambda; \theta_s)$ is found in the last entry of the first column.

Figure 11 shows a typical output listing

C. Minimum Area Optimization

1. Objective

The Minimum Area Optimization (MAO) code serves to find the minimum coolant fluid exit temperature for a given projected fin panel area, on the basis of the optimization analysis developed in Chapter III and the constraints as discussed in Section III-2. From the results, evaluated for a number of selected areas, one can determine the minimum area required for a chosen heat rejection rate. The optimum parameter set X_o is sought which satisfies Eqs. 33, 36, 40 and 41 by performing the iterations specified in Eqs. 48 through 53 until Eq. 33 is satisfied.

From the optimum parameter set X_o one computes the normalized system dimensions L^* , H^* , t^* and d^* in accordance to Eqs. 59 through 62 or Eqs. 64 through 67, depending on the flow regime in the coolant channels.

The necessary derivatives occurring in Eqs. 50 and 51 are obtained by Runge-Kutta Integration of the first-order, ordinary, non-linear differential equations given by Eqs. 52 and 53.

The individual program units are discussed in the following sections. Reference is made to program description in Section 3 of this Chapter and to Reference [1].

THETA-S = .200000
 U = .100000+01
 V = .100000+01
 FRIGBAR = .200000+00
 LAMBDA = .250000+02

THETA-F	THETA-B	NC	ETA-FAR	ETA	ZETA	STEP-NO
1.000000	.72992	.076213	1.001229	.919403	.00	1
.973292	.713938	.072780	1.004461	.922709	.10	2
.948092	.703261	.069563	1.007515	.925632	.20	3
.924291	.692944	.066546	1.010401	.928785	.30	5
.901791	.682975	.063715	1.013130	.931576	.40	6
.880499	.67333A	.061056	1.015711	.934216	.50	7
.860331	.664019	.058556	1.018158	.936714	.60	8
.841212	.655007	.056204	1.020465	.939079	.70	9
.823168	.646288	.053989	1.022655	.941319	.80	10
.805835	.637851	.051902	1.024729	.943441	.90	11
.789432	.629684	.049934	1.026696	.945453	1.00	12

FIGURE 11. SAMPLE RESULTS OF SIMPLIFIED RADIATOR SYSTEM SIMULATION

2. Deck Assembly

In its current state the Minimum Area Optimization (MAO) code consists of

1		main program	MAIN		
14	SUBROUTINE	subprograms	RKS	}	integration
			SDRV		
			SCNTL		
			BNDCND	}	restraints
			RESBND		
			REST		
			NDERV	}	partial derivatives
			MDER		
			NCDERV		
			MIXDER		
			DERV		
			INITIAL	}	initial conditions
			INTMIX		
			FMINV		matrix inversion
5	FUNCTION	subprograms	ETA	}	η and its derivatives
			DETA		
			DDETA		
			DDDETA		
			POLY		

The basic concept of the program is as described in Chapter B before and the block diagram in Figure 7 applies in principle. The exceptions are

- (i) there are 20 simultaneous differential equations to be solved:
 - 2 for θ_f and θ_b
 - 6 for the derivatives of θ_f and θ_b with respect to U , V and \bar{N}_c
 - 12 for the second derivatives of θ_f and θ_b with respect to U , V , and \bar{N}_c ,
- (ii) the initial conditions on the last 18 differential equations are obtained in subroutines,

- (iii) partial derivatives occurring in the differential equations for the last 18 of the above derivatives are computed by subroutines,
- (iv) at the end of each integration, the system of Eq. 49 is solved by FMINV and the integration repeated until the optimum is reached.

a. The MAIN Program performs the same functions as described in Chapter IV, Section B.2.a. and, in addition, calls INITIAL and INTMIX which compute the remaining 18 initial conditions for the partial derivatives as defined through Eq. 54. Moreover, instead of returning to the next input data set after completion of an integration, new system parameters \bar{X} are computed by solving, via FMINV, the system of Eq. 49. The results are tested, through SUBROUTINE BNDEND, to satisfy the Inequalities 36. If necessary, the newly computed parameters are adjusted to fall within the above limits, and the integration is repeated.

b. The SUBROUTINES RKS, SDRV and SCNTL perform the integration as explained in Sections B.2.b, c and d. There are, however, 18 additional dependent variables $Y(3), \dots, Y(20)$ to be integrated by RKS and, consequently, 18 additional derivatives to be evaluated in accordance with Eqs. 52 and 53. These derivatives are evaluated by calling DERV for $\partial\theta_f/\partial X_i$, $\partial\theta_b/\partial X_i$, $\partial^2\theta_f/\partial X_i^2$ and $\partial^2\theta_b/\partial X_i^2$ and by calling MIXDER for $\partial^2\theta_f/\partial X_i\partial X_j$ and $\partial^2\theta_b/\partial X_i\partial X_j$, $i \neq j$. SCNTL contains a slightly altered output specification.

c. The Restraint SUBROUTINES BNDEND, RESBND and REST serve to, respectively,

- (i) test newly computed components \bar{X} for compliance with Inequalities 36.
- (ii) solve Eqs. 40 and 41 for x_3 and x_4 .

When newly computed components \bar{X} do not comply with Inequalities 36 then they are set to meet the minimum and maximum conditions and the system of Eq. 49 is solved again, all from within BNDEND.

SUBROUTINE REST is the only particular program which differentiates the two optimization modes, minimum area and minimum mass. It may be replaced to accommodate other constraints. BNDEND and REST are called from MAIN.

d. The SUBROUTINES NDERV, MDER, NCDER, MIXDER and DERV are used to compute, respectively,

- (i) N and its derivatives $dN/d\lambda$, $d^2N/d\lambda^2$ from Eq. 17,
- (ii) M and its derivatives, up to third order, with respect to its arguments λ and N_c , in accordance to Eqs. 12, 15 and 16,
- (iii) N_c and its derivatives $\partial N_c / \partial \theta_b$, $\partial^2 N_c / \partial \theta_b^2$ and $\partial^2 N_c / \partial T \partial \bar{N}_c$,
- (iv) the mixed derivatives defined by Eq. 53 for $i \neq j$,
- (v) the derivatives defined by Eqs. 52 and 53.

e. The SUBROUTINES INITIAL and INTMIX serve to compute the initial conditions for the dependent variable $Y(3), \dots, Y(20)$, at the channel inlet $\zeta = 0$ which represent simple and mixed derivatives $\partial^2 \theta_f / \partial X_i \partial X_j$ and $\partial^2 \theta_b / \partial X_i \partial X_j$ in Eq. 53.

f. The SUBROUTINE FMINV is capable of performing two related tasks:

- (i) to invert a square, invertible matrix $\underline{\underline{A}}$
- (ii) to solve a non-trivial system of equations $\underline{\underline{AZ}} = \underline{\underline{X}}$.

The solutions are obtained through a sequence of elementary row operations which lead from the properly augmented coefficient matrix to the row-reduced echelon matrix, a standard procedure described in most elementary introductions to linear algebra [1].

SUBROUTINE FMINV (A, X, N, M) accepts, through its argument list, the square, invertible matrix $\underline{\underline{A}}$ of rank N, and if task (i) above is intended, M is set equal to $M = 2N$. Then, upon return from FMINV there will be the inverted matrix $\underline{\underline{A}}^{-1}$ placed in $XMAT(I,J)$ with $I = 1, \dots, N, J = N + 1, N + 2, \dots, 2N$. The two-dimensional array $XMAT$ is transferred to the calling program via a COMMON declaration. When task (ii) above is intended, M is set equal to $M = N + 1$ and, upon return from FMINV, the unknown vector $\underline{\underline{Z}}$ is placed in the one-dimensional array $\underline{\underline{X}}$.

FMINV is used to solve Eq. 49 and is called from MAIN and from BNDEND.

g. The FUNCTION subprograms ETA, DETA and PØLY are described in Sections B.2.e, f, and g of this chapter.

h. The FUNCTION subprograms DDETA and DDDETA are used to compute the second and third-order derivatives d^2n/dN_c^2 and d^3n/dN_c^3 as derived from Eqs. 32 a and b. The derivatives are evaluated via FUNCTION PØLY subprogram.

3. Input Data Preparation

Each optimization run is carried out for a selected $ASTAR = A^*$ (Eq. 38) and $TSTAR = t^*$ (Eq. 41) as the independent variables. The necessity of specifying t^* is not yet completely established at this time but included in the program for additional flexibility and to prevent the search from reading excessively large values of t^* .

The optimization produces

- (i) the optimum coolant exit temperature
- (ii) the optimum parameters $\underline{X} = \{x_1, \dots, x_4\}$ from which to compute L^* , H^* , d^* and λ (Eqs. 59-67).

For each optimization one computes

THETAS = θ_s	,	defined by Eqs. 19 & 4
U, starting value	,	" " Eq. 22
V, starting value	,	" " Eq. 21
FNCBR = \bar{N}_c starting value	,	" " Eq. 20
ASTAR = A^*	,	" " Eq. 40

and selects

DXWRT = $\Delta\zeta$ the axial interval for which results are to be printed.

The first five values are punched on one card in

FORMAT (5F16.8).

The last value is punched on a second card in

FORMAT(F16.8)

There may be arbitrarily many pairs of cards as specified above, one pair for each optimization run. They will be carried out in succession. The End-of-Job card will cause normal exit from the program.

The expected run time per optimization is approximately 15 seconds plus necessary compilation and collection times.

4. Presentation of Results

Each iteration produces one page of output, first the three parameters THETAS, ASTAR and TSTARI as read in. Next the current values of the system parameters U , V , $FNCBAR = \bar{N}_c$, $LAMBDA = \lambda$ and the identification of the flow regime, followed by the iteration count for establishing initial conditions

The table lists, as functions of $\zeta = Z/L$, in this order

THETAF = $\theta_f(\zeta)$ coolant temperature

THETAB = $\theta_b(\zeta)$ fin base temperature

NC = $N_c(\zeta) = \bar{N}_c \theta_b^3$, Eq. 14

ETABAR = $\bar{\eta}$, defined by Eq. 11

ETA = η , defined by Eq. 32

M defined by Eq. 12

N defined by Eq. 17

X = ζ , the non-dimensional distance along the channel.

Following the table is a list of the three system parameters U , V , \bar{N}_c and the first and second derivatives of θ_f with respect to these parameters. Finally are listed the newly computed changes of the above parameters.

A typical listing of the results is shown in Figure 9.

THETA-S = .7030000
 ASTAR = .675000
 U = 250.00000
 V = .000050
 ENCBAR = .000100
 LAMBDA = .037736

NUMBER OF ITERATIONS = 14

THETA F	THETA R	VC	ETARAR	ETA	M	N	ZETA
1.0000000	.9179813	.0000094	53.0099905	.9998844	.1801294	53.8198819	.0000000
.9211307	.9182655	.0000776	53.0099919	.9990098	.1801264	53.8198819	.2000000
.8677819	.8689164	.0000652	53.0099928	.9999242	.1801247	53.8198819	.4000000
.8309971	.8303729	.0000573	53.0099933	.9999334	.1801236	53.8198819	.6000000
.8039970	.8035309	.0000519	53.0099938	.9999397	.1801229	53.8198819	.8000000
.7835871	.7832305	.0000480	53.0099938	.9999441	.1801224	53.8198819	1.0000000

PARAMETERS AT END OF TUBE

THETA F = .783587
 U = .250000+03 V = .500000-04 RCHAR = .100000-03
 D2FDV = -.247174-05 D2FDV = .117912+00 D2FNCHAR = .771548-04
 D2F72U = .197315-07 D2FD2V = .979100+01 D2FD2NCHAR = .844942-03
 D2FUDV = .530919-05 D2FD00'CHAR = .105256-05 D2FDV0NCHAR = .525590+01
 DELTA U = .126478+03 DELTA V = -.363925-04 DELTA NCHAR = -.224943-01

OPTIMUM REACHED

FIGURE 12. RESULTS LISTING OF MINIMUM AREA OPTIMIZATION

and selected

DXWRT = $\Delta\zeta$ the axial interval for which results are to
be printed.

DA, DR absolute and relative integration step errors.

The data values are punched on the data card in NAMELIST format.

The NAMELIST is called INPUT.

There may be arbitrarily many additional input data cards as specified above, or with only one datum, one NAMELIST for each optimization run. They will be carried out in succession until an End-of-Job card causes normal exit from the program.

The expected run time per optimization is approximately 20 seconds plus necessary machine preparation times.

4. Representation of Results

Results are presented in the format identical to that described in section C.4 above, except that instead of the single TSTAR1 are listed MSTAR = M^* , PHI2 = ϕ_2 and FNUSTR = N^*_{Nu} , as read in. The representative output example is shown in Figure 10.

THETA-S = .60000000
 U = 13.363489
 V = 2.792685
 FNCR = 5.731686
 TOTMAS = 95.000000
 PH12 = 2000.000000
 ALPHA = 5.000000
 LAMBDA = 31297273.250000

NUMBER OF ITERATIONS = 8

THETA-S	U	V	FNCR	TOTMAS	PH12	ALPHA	LAMBDA	THETAF	THETAB	NC	ETABAR	ETA	M	N	X
1.00000000	.7686288	2.6027493	.3775592	.3775592	1.0000000	.0000001	.0000000	.0000001	.0000001	.0000000	.0000000	.0000000	.0000000	.0000000	.0000000
.7134382	.6486320	1.0316816	.5284999	.5284999	1.0000000	.0000001	.0000000	.0000001	.0000001	.0000000	.0000000	.0000000	.0000000	.0000000	.0000000
.6322974	.6138584	1.1674339	.5047780	.5047780	1.0000000	.0000001	.0000000	.0000001	.0000001	.0000000	.0000000	.0000000	.0000000	.0000000	.0000000
.6088749	.6038113	1.2169663	.4969006	.4969006	1.0000000	.0000001	.0000000	.0000001	.0000001	.0000000	.0000000	.0000000	.0000000	.0000000	.0000000
.6024210	.6010400	1.2322024	.4945601	.4945601	1.0000000	.0000001	.0000000	.0000001	.0000001	.0000000	.0000000	.0000000	.0000000	.0000000	.0000000
.6006592	.6002832	1.2364472	.4939149	.4939149	1.0000000	.0000001	.0000000	.0000001	.0000001	.0000000	.0000000	.0000000	.0000000	.0000000	.0000000

PARAMETERS AT END OF TUBE

THETAF = .600659
 U = .133635+02
 V = .27269+01
 NCBAR = .573169+01
 D1FDU = -.496030-04
 D1FDV = -.131301-03
 D1FNCBAR = .384840-04
 D2TF02U = .105462+03
 D2TF02V = .455954+04
 D2TFD2NCBAR = .120270+03
 D2TFD0UV = -.222946-02
 D2TFD0DNCBAR = .294970-03
 D2TFD0VNCBAR = -.740525+03
 INCR. SOUGHT DELTA U = .100314+00
 DELTA V = -.807482-01
 DELTA NCBAR = -.497181+00
 INCR. USED DELTA U = .100314+00
 DELTA V = -.832025-01
 DELTA NCBAR = -.497181+00

INSIGNIFICANT IMPROVEMENT OVER LAST STEP

FIGURE 13. RESULTS LISTING OF MINIMUM MASS OPTIMIZATION

V. CONCLUSIONS

The work presented herein resulted in a simplified radiator system analysis and a systematic optimization procedure.

Comparison of the simplified with the rigorous [1] system analyses indicated that the agreement between the two analyses can be expected to be within approximately 5%.

The optimization procedures carried out lead frequently to an optimum on the boundaries of the parameter domain. Mass optimization tends toward widely spaced tubes between thin fins.

Optimization was originally intended to be achieved through the parametric study of trends rather than through analytical procedures. Within the resources provided by this contract two analytical iterative optimization procedures were developed beyond the original goal of work. These procedures lead to the maximum heat rejection for given system area or system mass. Future work should be aimed toward the development of

- (1) a parameter domain within which relative extrema exist,
- (2) suitable working diagrams, through repeated applications of the developed codes, which depict the optimum geometric system parameters and produce either the least area or the least weight requirements for a given heat rejection rate.

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APPENDIX A

COMPUTER CODE FOR SIMPLIFIED

RADIATOR SYSTEM SIMULATION

QFOR*IS MAIN
 FOR 59A-07/25/72-22:59:39 (70)

MAIN PROGRAM

STORAGE USED: CODE(1) 000464; DATA(0) 000355; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 SDR 000014
 0004 MCT 000006

EXTERNAL REFERENCES (BLOCK, NAME)

0005 SDRV
 0006 SCNTL
 0007 ETA
 0010 DELTA
 0011 RKS
 0012 NINTR\$
 0013 NMDUS\$
 0014 NIO2\$
 0015 NRDU\$
 0016 SORT
 0017 ASIN
 0020 NSTOP\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000150	100	0001	000327	105L	0001	000345	110L	0000	000265	120F	0001	000405	232G
0001	000007	45L	0000	000233	5F	0000	000234	50F	0000	000236	55F	0001	000131	85L
0001	000145	90L	0000	000304	900F	0000	000311	905F	0001	000452	920L	0000	000313	925F
0001	000147	95L	0001	000460	950L	0000	R 000030	A	0000	R 000213	AYY	0000	R 000205	A1
0000	R 000214	BYT	0010	R 000000	DELTA	0000	R 000220	DETZ	0003	R 000007	DFM	0003	000010	DFMX
0003	R 000011	DFM<	0004	R 000000	DLMT	0000	R 000060	DLY	0003	000012	DROU	0003	000013	DROV
0000	R 000224	DX	0004	R 000003	DXWRT	0000	R 000014	DY	0000	R 000140	DYST	0000	R 000221	DYY
0007	R 000000	ETA	0000	R 000216	ETY	0000	R 000215	ETYY	0003	R 000006	FM	0003	R 000005	FN
0000	R 000212	FNC	0003	R 000002	FNCBR	0000	I 000232	I	0000	I 000227	IBKP	0004	I 000001	ICNT
0000	I 000231	IER<	0000	I 000235	IFVD	0004	I 000005	LCNT	0004	I 000004	LSTEP	0000	I 000226	N
0000	I 000207	NCT	0000	I 000230	NTRY	0000	R 000074	PD	0000	R 000044	R	0003	R 000004	RHOD
0006	R 000000	SCNTL	0000	R 000110	SD	0005	R 000000	SDRV	0000	R 000206	THETAB	0000	R 000204	THETAS
0003	R 000003	TH4	0000	R 000210	T2	0000	R 000211	T3	0003	R 000000	U	0003	R 000001	V
0004	R 000002	XWRT	0000	R 000000	Y	0000	R 000124	YS	0000	R 000170	YSIMP	0000	R 000154	YST
0000	R 000217	YY	0000	R 000222	ZZ	0000	R 000223	ZZZ						

00100 1* C
 00100 2* C SIMPLIFIED RADIATOR SYSTEM SIMULATION
 00100 3* C
 00100 4* C *****
 00100 5* C
 00100 6* C

THETAS,U,V,FNCBR, AND RHOD ARE SYSTEM PARAMETERS
 DXWRT IS THE INCREMENT OF AXIAL DISTANCE FOR OUTPUT LISTING

FORMAT (5F16.8)

7* C
8* C
9* C
10*
11*
12*
13* C
14* C
15* C
16*
17*
18*
19*
20*
21*
22* C
23* C
24*
25*
26*
27* C
28*
29*
30*
31*
32*
33*
34*
35* C
36*
37*
38*
39*
40*
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46*
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62*
63*

```
EXTERNAL SDRV,SCNTL  
DIMENSION Y(12),DY(12),A(12),R(12),DLX(12),PD(12),SD(12),YS(12),  
DYSI(12),YSI(12),YSIMP(12)  
COMMON /SDR/ U,V,FNCBR,TH4,RHOD,FN,FM,DFM,DFMX,DFNX,DROU,DROV/MCT/  
1 DLMT,ICNT,XWRT,DXWRT,LSIEP,LCNT  
FNN(X) = (X+3.570796-SQRT(X*(X+2.0)))-ASIN(1.0/(1.0+X))/X  
FFS(X) = (SQRT(X*(X+2.0)))+ASIN(1.0/(X+1.0))-1.570796/X  
DFN(X,Y) = 1.0-Y*(0.1460*Y-0.02866)/X  
DFFN(X,Y) = (-0.2920*Y+0.02866)/X  
DFFX(X,Y) = Y*(0.1460*Y-0.02866)/(X*X)  
DFFS(X) = -SQRT(X+2.0)/X/(X*(X+1.0))+1.5708-ASIN(1.0/(X+1.0))/  
1 (X*X)  
WRITE(6,5)  
5 FORMAT(1H1)  
45 READ(5,50,END=95) THETAS,U,V,FNCBR,RHOD,DXWRT  
50 FORMAT(5E16.8)  
55 FORMAT(1H0,10X,10HTHETA-S = ,F19.6r//,  
1 11X,10H U = ,E20.6r//,  
2 11X,10H V = ,E20.6r//,  
3 11X,10H FNCBR = ,E20.6r//,  
4 11X,10H LAMBDA = ,E20.6r//)  
C  
IF(THETAS.GE. 1.0) GO TO 920  
FN = FNN(RHOD)  
DFNX = (-FN+1.0-SQRT(RHOD*(RHOD+2.0)))/RHOD  
TH4 = THETAS**4  
IF(V.GT.0.2) GO TO 90  
A1 = 2.0+1.0/(V*ETA(FNCBR))  
IF(A1.GE.2.45) GO TO 85  
THETAB = 1.0-1.0/(2.0*A1)  
GO TO 95  
85 THETAB = 1.0-(A1-SQRT(A1**2-6.0))/6.0  
GO TO 95  
90 THETAB = 0.9  
95 NCT = 0  
100 T2 = THETAB**2  
T3 = T2*THETAB  
FNC = FNCBR*T3  
FM = FFN(RHOD,FNC)*FFS(RHOD)  
DFM = DFFN(RHOD,FNC)*FFS(RHOD)  
AYY = T3*THETAB-TH4  
BYY = 1.0-THETAB  
ETYY = ETA(FNC)  
ETV = ETV*FM+FN  
YY = 1.0/V-ETV*AYY/BYY  
DETZ = (DFM*ETYY*FM+DETA(FNC))*3.0*T2*FNCBR  
DY = -AYY/BYY*(DETA*ETV/BYY)-4.0*ETV*T3/BYY  
Z2 = THETAB-YY/DYY  
IF(NCT.GT.1.20) WRITE(6,900)
```



```

00177 64* IF(ZZ.LT.1.0) GO TO 105
00201 65* THETAB = (THETAB+1.0)/2.0
00202 66* NCT = NCT+1
00203 67* GO TO 100
00204 68* 105 IF(ABS(ZZ-THETAB)/ZZ.LT.1.0E-06) GO TO 110
00206 69* NCT = NCT+1
00207 70* THETAB = ZZ
00210 71* GO TO 100
00210 72* C
00211 73* 110 Y(1) = 1.0
00212 74* Y(2) = THETAB
00213 75* ZZ = 0.0
00214 76* DX = 1.0/(U*(1.0-THETAB))
00215 77* IFVD = 0
00216 78* IF(DX.GT.DXWRT) DX = DXWRT
00220 79* N = 2
00221 80* IBKP = 1
00222 81* NTRY = 1
00223 82* IERR = 0
00223 83* C
00224 84* DLMT = DXWRT/500.0
00225 85* XWRT = 0.0
00226 86* LSTEP = 0
00227 87* LCNT = 0
00230 88* ICNT = 0
00231 89* 00 115 I=1,12
00234 90* A(I) = 5.0E-05
00235 91* 115 R(I) = 5.0E-05
00235 92* C
00237 93* WRITE(6,120)
00241 94* 120 FORMAT(1H0,13X,6HTHETAF,14X,6HTHETAB,16X,2HNC,17X,6HETABAR,15X,
00241 95* 3HETA,8X,4HZETA,6X,7HSTEP NO,/)
00241 96* C
00242 97* CALL RKS(SDRV,SCNTLY,DY,A,R,ZZZ,DX,N,IFVD,IBKP,NTRY,IERR,
00242 98* 1 DLY,PD,SD,Y,YST,DYST,YSIMP)
00243 99* WRITE(6,905)
00245 100* GO TO 45
00246 101* 900 FORMAT(1H0,20HNEWTON-RAPHSON FAILS)
00247 102* 905 FORMAT(1H,////)
00250 103* 920 WRITE(6,925)
00252 104* 925 FORMAT(1H0,37HRADIATIVE HEATING CANNOT BE SIMULATED)
00253 105* GO TO 45
00254 106* 950 STOP
00255 107* END

```

END OF COMPILATION: NO DIAGNOSTICS.

OFOR15 SUB1
FOR 59A-07/25/72-23:00:14 (10)

SUBROUTINE SORV ENTRY POINT 000150

STORAGE USED: CODE(1) 0001557 DAYAT(0) 0000371 BLANK COMMENT(2) 0000000

COMMON BLOCKS:

0003 SOR 000014
0004 SOC 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0005 EYA
0006 DELTA
0007 ASIN
0010 SORT
0011 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000136 10L 0001 000103 5L 0000 R 000005 A0 0000 R 000006 A1 0000 R 000007 A2
0000 R 000010 A3 0000 R 000011 A4 0000 R 000012 A5 0000 R 000000 DELTA 0003 R 000007 DFM
0003 000010 DFMX 0003 000011 DFNX 0003 000012 DROU 0003 000013 DROV 0005 R 000000 EIA
0004 R 000001 ETY 0004 R 000002 ETZ 0000 R 000003 FFN 0000 R 000004 FFS 0003 R 000006 FM
0003 R 000005 FN 0003 R 000002 FNCBR 0000 000024 INJPS 0003 R 000004 RHOD 0003 R 000003 TH4
0003 R 000000 U 0003 000001 V 0000 R 000000 Y2 0000 R 000001 Y3 0000 R 000002 Y4
0004 R 000000 Z

00101 1* SUBROUTINE SORV(Y,DY,X)

00101 2* C

00101 3* C COMPUTES DERIVATIVES

00101 4* C

00103 5* DIMENSION Y(12),DY(12)

00104 6* COMMON /SOR/ U,V,FNCBR,TH4,RHOD,FN,FM,DEM,DFMX,DFNX,DROU,DROV,SOC/

00104 7* Z,ETY,ETZ

00104 8* C

00105 9* Y2 = Y(2)**2

00106 10* Y3 = Y(2)*Y2

00107 11* Y4 = Y2*Y2

00110 12* Z = FNCBR*Y3

00111 13* ETY = ETA(2)

00112 14* FFN = 1.-Z*(0.146082-0.028661)/RHOD

00113 15* FFS = (SQRT(RHOD*(RHOD+2.))+ASIN(1./((RHOD+1.))-1.5708))/RHOD

00114 16* FM = FFS*FFS

00115 17* DFM = (-0.29202Z+0.028661)/RHOD*FFS

00116 18* ETZ = ETY*FM+FN

00117 19* DY(1) = -U*(Y(1)-Y(2))

00120 20* A0 = Y4-TH4

```

00121 21* IF(A0.GT.1.0E-08) GO TO 5
00122 22* DY(2) = 0.0
00123 23* GO TO 10
00124 24*
00125 24* 5 A1 = Y(1)-Y(2)
00126 25* A2 = (EY*DFM+DETA(2)*FH)
00127 26* A3 = 3.*A2*Y2*FNCR/ETZ
00130 27* A4 = 4.0*Y3/A0
00131 28* A5 = 1.0*A1*(A3+A4)
00132 29* DY(2) = DY(1)/A5
00133 30* C
00134 31* 10 CONTINUE
00135 32* RETURN
00136 33* END

```

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS SUB2
FOR S9A-07/25/72-23:01:21 (10)

SUBROUTINE SCNTL ENTRY POINT 000146

STORAGE USED: CODE(1) 000173; DATA(0) 000016; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 SOC 000003
0004 MCT 000005

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NMOJ5
0006 NIOZ5
0007 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000054 5L 0001 000061 50L 0000 000002 55F 0001 000134 60L 0004 R 000000 DLMT
0000 R 000000 DXSTR 0004 R 000003 DXWRT 0003 R 000001 ETY 0003 R 000002 ETZ 0004 I 000001 ICNT
0000 000010 I-JP5 0000 I 000001 LCNT 0004 I 000004 LSTEP 0004 R 000002 XWRT 0003 R 000000 Z

00101 1* SUBROUTINE SCNTL(Y,DY,DX,X,NTRY,IFVD)

00101 2* C CONTROLS INTEGRATION

00101 3* C

00101 4* C

00103 5* DIMENSION Y(12),DY(12)

00104 6* COMMON /SDC/ Z,ETY,ETZ /MCI/ DLMT,ICNT,XWRT,DXWRT,LSTEP

00105 7* ICNT = ICNT+1

00106 8* IF(DX.GE.DXWRT.AND.ICNT.GT.1) LSTEP = 1

00110 9* IF(ABS(X-XWRT).LT.DLMT) GO TO 50

00112 10* IF(XWRT.GT.X) GO TO 5

00112 11* C

00114 12* DXSTR = DX

00115 13* DX = DX+XWRT-X

00116 14* LCNT = 1

00117 15* NTRY = 3

00120 16* RETURN

00120 17* C

00121 18* 5 NTRY = 1

00122 19* RETURN

00122 20* C

00123 21* 50 WRITE(6,55) Y(1),Y(2),Z,ETZ,ETY,X,ICNT

00134 22* 55 FORMAT(1H,5E20.6,F10.2,I10)

00135 23* IF(LCNT.EQ.1) DX = DXSTR

00137 24* LCNT = 0

00140 25* IF(ABS(1.0-XWRT).LE.DLMT) GO TO 60

00142 26* XWRT = XWRT+DXWRT

```

00143      27*      NTRY = 1
00144      28*      IF(LSTEP.EQ.0) RETURN
00146      29*      DX = DXMRT
00147      30*      IFVD = 1
00150      31*      RETURN
00150      32*      C
00151      33*      60 NTRY = 2
00152      34*      RETURN
00153      35*      END

```

END OF COMPILATION: NO DIAGNOSTICS.

QFOR,IS SUB3
FOR S9A-07/25/72-23:01:28 (1.0)

FUNCTION ETA ENTRY POINT 000036

STORAGE USED: COJE(1) 000044) DATA(0) 000022) BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 POLY
0004 EXP
0005 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000016 1L 0000 R 000001 A 0000 R 000010 B 0000 R 000000 ETA 0000 000014 INJPS
0003 R 000000 POLY

00101 1* FUNCTION ETA(X)
00101 2* C
00101 3* C COMPUTES FIN EFFECTIVENESS ETA
00101 4* C
00103 5* DIMENSION A(7), B(2)
00104 6* DATA A(1),A(2),A(3),A(4),A(5),A(6),A(7)/0.10E+01, -0.1163143E+01,
00104 7* 1 0.1478836E+01, -0.1267550E+01, 0.6325223E+00, -0.1627067E+00,
00104 8* 2 0.1654223E-01/ B(1),B(2)/0.5966695E+00, -0.2297718E+00/
00116 9* IF(X.GT.2.5) GO TO 1
00120 10* ETA = POLY(7,A,X)
00121 11* RETURN
00122 12* 1 ETA = R(1)*EXP(R(2)*X)
00123 13* RETURN
00124 14* END

END OF COMPILATION: NO DIAGNOSTICS.

QFOR:IS SUB4
FOR S9A-07/25/72-23:01:35 (7,0)

FUNCTION DETA ENTRY POINT 000036

STORAGE USED: CODE(1) 000044 DATA(0) 0000211 BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK# NAME)

0003 POLY
0004 EXP
0005 NERR35

STORAGE ASSIGNMENT (BLOCK#, TYPE, RELATIVE LOCATION, NAME)

0001 000016 IL 0000 R 000001 A 0000 R 000007 B 0000 R 000000 DETA 0000 000013 INJPS
0003 R 000000 POLY

00101 1* FUNCTION DETA(X)
00101 2* C
00101 3* C COMPUTES FIRST DERIVATIVE DETA/DNC
00101 4* C
00103 5* DIMENSION A(6), B(2)
00104 6* DATA A(1),A(2),A(3),A(4),A(5),A(6)/-0.1163143E+01, 0.2957672E+01,
00104 7* -0.3802650E+01, 0.2530089E+01, -0.8135335E+00, 0.925338E-01/
00104 8* B(1),B(2)/-0.1577635E+00, -0.2297718E+00/
00115 9* IFX.GT.2.5) GO TO 1
00117 10* DETA = POLY(6,A,X)
00120 11* RETURN
00121 12* 1 DETA = B(1)*EXP(B(2)*X)
00122 13* RETURN
00123 14* END

END OF COMPILATION: NO DIAGNOSTICS.

GEOR, IS SUBS
FOR S9A-07/25/72-23101:39 (,0)

FUNCTION POLY ENTRY POINT 000036

STORAGE USED: CODE(1) 000044; DATA(0) 000015; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK NAME)

0003 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 00012 107\$ 0000 000003 INJPS 0000 I 000002 K 0000 I 000001 L 0000 R 000000 POLY

```
00101 1* FUNCTION POLY(N,A,X)
00101 2* C
00101 3* C EVALUATES POLYNOMIALS
00101 4* C
00103 5* DIMENSION A(N)
00104 6* POLY = 0.
00105 7* L = N
00106 8* DO 1 K=1,N
00111 9* POLY = POLY*X+A(L)
00112 10* 1 L = L-1
00114 11* RETURN
00115 12* END
```

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS SUB6
FOR S9A-07/25/72-23:01:48 (.0)

SUBROUTINE RKS ENTRY POINT 000643

STORAGE USED: CODE(1) 001040(1) DATA(1) 000064(1) BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR2\$
0004 NEXP5\$
0005 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000010 10L 0001 000313 110L 0001 000333 120L 0001 000045 1266 0001 000343 130L
 0001 000071 140G 0001 000355 140L 0001 000105 146G 0001 000130 156G 0001 000417 160L
 0001 000150 164G 0001 000177 174G 0001 000500 185L 0001 000510 190L 0001 000013 20L
 0001 000232 205G 0001 000270 217G 0001 000524 220L 0001 000530 230L 0001 000243 240L
 0001 000374 245G 0001 000032 25L 0001 000552 250L 0001 000554 251L 0001 000572 257L
 0001 000604 259L 0001 000823 270L 0001 000456 300L 0001 000615 336G 0001 000054 40L
 0001 000060 45L 0001 000006 5L 0001 000076 50L 0001 000123 70L 0001 000054 40L
 0000 R 000014 AM 0000 R 000007 AMAX 0000 R 000011 C 0000 R 000010 D 0000 R 000135 80L
 0000 R 000003 DELT 0000 R 000012 E 0000 R 000000 FR10 0000 I 000004 I 0000 R 000001 DST
 0000 000030 INJP\$ 0000 I 000002 ISYMP 0000 I 000013 J 0000 I 000005 IFLAG

00101 1* SUBROUTINE RKSTDERR, CNTRL, Y, DY, A, R, T, DEL, N, IFVD, IBKP, NTRY, DG000100
 00101 2* IERR, DELY, PD, SD, YS, YSI, DYST, YSIMP) DG000200
 00101 3* C
 00101 4* C
 00101 5* C
 00101 6* DIMENSION Y(N), DY(N), A(N), R(N), DELY(N), DGO 3
 00103 7* IPO(N), YSD(N), YS(N), DYST(N), YST(N), YSIMP(N) DG00040
 00104 8* EXTERNAL DERIV, CNTRL DG000500
 00104 9* FR10 IS FIFTH ROOT OF TEN DG00 60
 00105 10* FR10=1.5848932 DG000700
 00106 11* IERR=0 DG000800
 00106 12* YS CONTAINS Y VALUES AT LEFT END POINT OF INTEGRATION INTERVAL DG00090
 00106 13* C
 00106 14* C
 00106 15* C
 00106 16* C
 00106 17* C
 00106 18* C
 00106 19* C
 00106 20* C
 00106 21* C
 00106 22* C
 00106 23* C
 00106 24* C

YS CONTAINS Y VALUES AT LEFT END POINT OF INTEGRATION INTERVAL
 YSIMP CONTAINS Y FOR SIMPSONS RULE CHECK CHECK NOT MADE FOR
 FIXED STEP MODE ISYMP IS CONTROL PARAMETER =1, FIXED/2 VAR/DG00120
 IF FIXED STEP SIZE GO ONE INTERVAL OF LENGTH DELT AND RETURN TO DG00140
 CNTRL, IF VAR GO TWO INTERVALS BEFORE RETURN TO CONTRL DG00150
 IFVD = 0 VARIABLE INTERVAL DG001600
 = 1 FIXED DG00170
 IBKP = 0 CUT INTERVAL ONCE BEFORE REPEAT (UNDER IFVD=0) DG001800
 = 1 CUT AS REQUIRED DG00190
 NTRY = 1 CONTINUE INTEGRATING OGO 200
 DG002100

00106	25*	C	2	RETURN FROM RKS	D60 220
00106	26*	C	3	STEP REPEATED WITH NEW DELT	D6002300
00106	27*	C	4	RESTART	D600240
00106	28*	C	IERR = 0	NORMAL	D6002500
00106	29*	C	-1	DELT=0, RETURN FROM RKS	D6002600
00106	30*	C	1	A(I)+R(I)*ABS(Y(I)) = 0, RETURN FROM RKS	D6002700
00107	31*	C	5	IF (DEL) 20,10,20	D6002800
00112	32*	C	10	IERR=-1	D6002900
00113	33*	C	GO TO 270		D7003000
00114	34*	C	20	CALL DERIV(Y,DY,T)	D6003100
00115	35*	C	NTRY=1		D6003200
00116	36*	C	CALL CNTRL(Y,DY,DEL,T,NTRY,IFVD)	D6003300	
00117	37*	C	25	DDT=DEL	D6003400
00120	38*	C	IF (IFVD) 40,30,40		D6003500
00123	39*	C	30	ISYMP=2	D6003600
00124	40*	C	DELT=DEL/2.		D600370
00125	41*	C	DO 31 I=1,N		D7003800
00130	42*	C	31	SD(I)=0.0	D600390
00132	43*	C	IFLAG=1		D600400
00133	44*	C	S=1.		D6004100
00134	45*	C	GO TO 45		D6004200
00135	46*	C	40	ISYMP=1	D6004300
00136	47*	C	DELT=DEL		D600440
00137	48*	C	45	DO 46 I=1,N	D6004500
00142	49*	C	YST(I)=Y(I)		D600460
00143	50*	C	46	DYST(I)=DY(I)	D60 470
00145	51*	C	50	DO 60 I=1,N	D6004800
00150	52*	C	DELY(I)=DELT*DY(I)		D6004900
00151	53*	C	PD(I)=DELY(I)		D600500
00152	54*	C	60	CONTINUE	D6005100
00154	55*	C	GO TO (80,70),ISYMP		D6005200
00155	56*	C	70	DO 71 I=1,N	D6005300
00160	57*	C	71	SD(I)=SQ(I)+S*DY(I)	D6005400
00162	58*	C	80	T+DELT/2.	D6005500
00163	59*	C	DO 85 I=1,N		D6005600
00166	60*	C	YS(I)=Y(I)		D600570
00167	61*	C	Y(I)=YS(I)+DELY(I)/2.		D6005800
00170	62*	C	85	CONTINUE	D6005900
00172	63*	C	CALL DERIV(Y,DY,T)		D6006000
00173	64*	C	DO 90 I=1,N		D6006100
00176	65*	C	DELY(I)=DELT*DY(I)		D600620
00177	66*	C	PD(I)=PD(I)+2.*DELY(I)		D6006300
00200	67*	C	Y(I)=YS(I)+DELY(I)/2.		D600640
00201	68*	C	90	CONTINUE	D6006500
00203	69*	C	CALL DERIV(Y,DY,T)		D6006600
00204	70*	C	DO 95 I=1,N		D600670
00207	71*	C	DELY(I)=DELT*DY(I)		D600680
00210	72*	C	PD(I)=PD(I)+2.*DELY(I)		D6006900
00211	73*	C	Y(I)=YS(I)+DELY(I)		D600700
00212	74*	C	95	CONTINUE	D6007100
00214	75*	C	T+DELT/2.		D6007200
00215	76*	C	CALL DERIV(Y,DY,T)		D600730
00216	77*	C	DO 100 I=1,N		D6007400
00221	78*	C	DELY(I)=DELT*DY(I)		D6007500
00222	79*	C	PD(I)=PD(I)+DELY(I)		D600760
00223	80*	C	Y(I)=YS(I)+PD(I)/6.		D600770
00224	81*	C	100	CONTINUE	D6007800

```

00226 82* GO TO (110,120),ISYMP
00227 83* 110 NTRY=1
00230 84* CALL DERIV(Y,DY,T)
00231 85* CALL CNTRL(Y,DY,DEL,T,NTRY,IFVD)
00232 86* GO TO 300
00233 87* 120 GO TO (130,140),IFLAG
00234 88* 130 S=4.
00235 89* IFLAG=2
00236 90* CALL DERIV(Y,DY,T)
00237 91* GO TO 50
00240 92* 140 CALL DERIV(Y,DY,T)
00241 93* AMAX =0.0
00242 94* DO 180 I=1,N
00245 95* SD(I)=SD(I)+DY(I)
00246 96* YSYMP(X)=YSI(I)+DELT*SD(I)/3.
00247 97* D =ABS(Y(I)-YSYMP(I))
00250 98* C =A(I)+R(I)*ABS(Y(I))
00251 99* IFIC ) 160,150,160
00254 100* 150 IERR=1
00255 101* GO TO 270
00256 102* 160 E =ABS(D /C )
00257 103* AMAX=AMAX1(AMAX,E)
00260 104* 180 CONTINUE
00262 105* IF(AMAX-1.) 215,215,230
00265 106* 215 NTRY= 1
00266 107* CALL CNTRL(Y,DY,DEL,T,NTRY,IFVD)
00267 108* 30) IF(NTRY-1) 185,185,310
00272 109* 310 IF(NTRY-2) 270,270,330
00275 110* 330 IF(NTRY-3) 340,340,5
00300 111* 340 I=I-DDT
00301 112* IF(DEL) 259,10,259
00304 113* 18) GO TO (40,190),ISYMP
00305 114* 19) IF(AMAX-.75) 200,25,220
00310 115* 20) IF(AMAX-.075) 210,25,25
00313 116* 21) DEL=DEL*FR10
00314 117* GO TO 25
00315 118* 22) DEL=DEL/FR10
00316 119* GO TO 25
00317 120* 23) I =I+ 18KP
00320 121* GO TO (240,250),I
00321 122* 24) I=I-DEL
00322 123* DEL=DEL/FR10
00323 124* GO TO 259
00324 125* 25) J=1
00325 126* 251 AM=AMAX/10.**J
00326 127* IF(1.-AM) 255,257,257
00331 128* 255 J=J+1
00332 129* GO TO 251
00333 130* 257 I=I-DEL
00334 131* DEL=DEL/(FR10**J)
00335 132* 259 DO 245 I=1,N
00340 133* DY(I)=DYST(I)
00341 134* 245 Y(I)=YSI(I)
00343 135* GO TO 25
00344 136* 270 RETURN
00345 137* END

```

END OF COMPILATIONS: NO DIAGNOSTICS.

Q XGT
MAP 0023-07/25-23:02

ADDRESS LIMITS 001000 013206 040000 044714
 STARTING ADDRESS 012523
 WORDS DECIMAL 5255 IBANK 2509 OBANK

	SEGMENT	MAIN	001000	013206	040000	044714
NSWTC\$/FOR	1	001000	001021			
NRBLK\$/FOR	1	001022	001044			
NRWNC\$/FOR	1	001045	001124	2	040000	040011
NWFF\$/FOR	1	001125	001326	2	040012	040031
NFCH\$/FOR	1	001327	001617	2	040032	040067
NBCV\$/FOR	1	001620	001752	2	040070	040125
NFTV\$/FOR	1	001753	001775			
NCNVT\$/FOR	1	001776	002222	2	040126	040215
NCLOSS\$/FOR	1	002223	002371	2	040216	040247
NBLK\$/FOR	1	002372	002513			
NBSL\$/FOR	1	002514	002550			
NUPJA\$/FOR	1	002551	002603			
NBF00\$/FOR	1	002604	003014	2	040250	042451
NININ\$/FOR	1	003015	003657	2	042452	042463
NINPT\$/FOR	1	003660	004173	2	042464	042503
NOTIN\$/FOR	1	004174	005162	2	042504	042507
NOUI\$/FOR	1	005163	005041	2	042510	042534
NWY\$/FOR	1	006042	006214	2	042612	042716
NIOER\$/FOR	1	006215	007076	2	042717	043055
NFC4K\$/FOR	1			4	043056	043127
NYAB\$/FOR	1			2	043130	043166
ERUB/MISC						
NIBJF\$/FOR	1	007077	007141	2	043167	043167
TIR\$/TECH	1	007142	007626	0	043170	043220
				2	043221	043500
SRQTS\$/FOR	1	007627	007667	2	043501	043512
ASINCO\$/FOR	1	007670	010104	0	043513	043540
NIE\$/FOR	1	010105	010166	2	043541	043674
NOBJF\$/FOR	1	010167	010233			
EXP\$/FOR	1	010234	010323	2	043675	043715
NEXP5\$/FOR	1	010324	010411	2	043716	043725
NERR\$/FOR	1	010412	010736	2	043726	044071
SDR (COMMON BLOCK)					044072	044105
MCT (COMMON BLOCK)					044106	044113
SDC (COMMON BLOCK)					044114	044116
BLANK\$COMMON (COMMON BLOCK)						
SUB6	1	010737	011776	0	044117	044202
				2	BLANK\$COMMON	

SUB5	1	011777	012042	0	044203	044217
				2	BLANK\$COMMON	
SUB4	1	012043	012106	0	044220	044240
				2	BLANK\$COMMON	
SUB3	1	012107	012152	0	044241	044262
				2	BLANK\$COMMON	
SUB2	1	012153	012345	0	044263	044300
	3	SOC		2	BLANK\$COMMON	
				4	MCT	
SUB1	1	012346	012522	0	044301	044337
	3	SDR		2	BLANK\$COMMON	
				4	SOC	
MAIN	1	012523	013206	0	044340	044714
	3	SDR		2	BLANK\$COMMON	
				4	MCT	

SYS\$RLIB\$, LEVEL 63
 END OF COLLECTION - TIME 1.677 SECONDS

APPENDIX B

COMPUTER CODE FOR MINIMUM

AREA OPTIMIZATION

2 JFOR, IS MAIN
FOR S9A-07/27/72-17:43:15 (1.0)

MAIN PROGRAM:

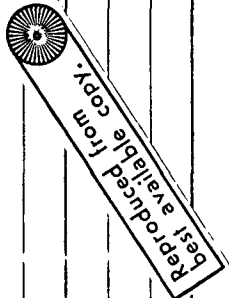
STORAGE USED: CODE() 0010451 DATA(0) 0006771 BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 BLK1 0000.4
0004 BLK2 0000.2
0005 PCT 0000.5
0006 BLK3 0000.2
0007 BLK4 0000.2

EXTERNAL REFERENCES (BLOCK, NAME)

0010 SERV
0011 SCJTL
0012 REST
0013 SERV
0014 EIA
0015 DETA
0016 SERV
0017 SERV
0020 LPIAL
0021 INPIK
0022 RAS
0023 ENPIW
0024 RDCNO
0025 PESSD
0026 NITRE
0027 BRJUF
0030 S425
0031 S4705
0032 S471
0033 SRT
0034 S1015
0035 STOP5



STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000002 JL 0001 000153 100L 00.0 000421 1000F 0001 000333 105L 0001 000551 100L
0001 000354 109L 0001 000361 110L 00.0 000423 2000F 0000 000454 2010F 0000 000467 2000F
0000 000505 205F 0000 000522 2050F 00.0 000616 2070F 0001 001033 2080L 0000 000631 2085F
0000 000514 210F 0000 000521 215F 00.0 000602 220F 0000 000533 230F 0001 000515 233G
0000 000547 240F 0000 000564 250F 0001 001024 300L 0001 001041 3000L 0001 000725 300G
0001 000020 50L 0001 000160 50L 00.0 000462 900F 0000 R 000050 A 0000 R 000737 AV
0000 R 000353 ASTA 0000 R 000362 AYY 0004 000003 A1 0004 000004 A2 0004 000005 A3
0004 000007 A5 0004 000010 F6 0000 R 000363 BYY 0015 R 000000 DETA
0000 R 000367 DETZ 0003 000023 DEIDL 0003 000021 DE4DTR 0003 R 000013 DF4 0003 R 000012 DFMX
0003 R 000010 DFNX 0006 R 000006 DLNCS 0006 R 000001 DLOU 0006 R 000002 DLOV 0005 R 000000 DLMY
0000 R 000120 DLY 0007 000000 DMCSDU 0007 000001 DMCSDV 0003 R 000007 DMCSTI 0000 R 000405 DX
0005 R 000003 DXWRT 0000 R 000024 DY 0000 R 000240 DYST 0000 R 000370 DYT 0000 R 000373 DZCDRT


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0000 R 000374 D2C1B 0000 R 000402 D2E4LN 0000 R 000376 D2E4LU 0000 R 000400 D2E4LV 0000 R 000401 D2E4TN
0000 R 000375 D2E4V 0000 R 000377 D2E4V 0000 R 000403 D2E4V 0000 R 000404 D2E4V
0006 R 000005 D2L0V 0006 R 000007 D2LNCB 0006 R 000010 D2LVNR 0006 R 000011 D2LV4B 0003 R 000015 D2MNC
0003 R 000014 D2MLC 0003 R 000011 D2NDLL 0004 R 000001 D3M2LN 0004 R 000002 D3M2XL 0004 R 000011 E9
0014 R 000000 ETA 0000 R 000365 FTY 0000 R 000364 FTY 0003 R 000422 E3 0003 R 000002 F4
0003 R 000003 EN 0003 R 000005 FMC 0003 R 000004 FICBR 0000 I 000403 I 0000 I 000410 IAKP
0005 I 000001 ICNT 0000 I 000412 TERR 0000 I 000406 IFVD 0000 I 000413 LCNT 0005 I 000004 LSTEP
0000 I 000407 N 0000 I 000357 MCT 0000 I 000354 NIT 0000 I 000414 NITMAX 0000 I 000411 NTRY
0000 R 000144 PC 0000 R 000074 R 0000 R 000000 SDRV 0000 R 000355 RHOD 0006 R 000000 SCNTL 0001 R 000000 SCNTL
0000 R 000170 S2 0010 R 000000 SDRV 0003 R 000000 THETAB 0000 R 000372 THETAF 0003 R 000001 THETAS
0000 R 000356 TH4 0000 R 000360 T2 0000 R 000361 T3 0004 R 000000 U 0003 R 000006 V
0000 R 000334 X1 0005 R 000002 XWT 0000 R 000000 Y 0000 R 000214 Y2 0000 R 000410 YSIMP 0000 R 000371 Z2
0000 R 000404 ZZZ 0000 R 000415 Z1 0000 R 000416 Z2 0000 R 000417 Z3 0000 R 000420 Z5

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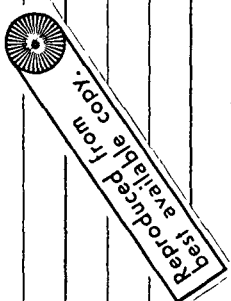
RADIATOR SYSTEMS OPTIMIZATION FOR MINIMUM AREA

```

00100 1* C
00100 2* C
00100 3* C
00101 4*
00103 5*
00103 6*
00104 7*
00104 8*
00104 9*
00104 10*
00104 11*
00104 12*
00104 13*
00105 14*
00106 15*
00107 16*
00110 17*
00120 18*
00121 19*
00122 20*
00124 21*
00126 22*
00130 23*
00130 24*
00131 25*
00132 26*
00133 27*
00143 28*
00143 29*
00143 30*
00143 31*
00143 32*
00143 33*
00144 34*
00147 35*
00150 36*
00151 37*
00153 38*
00155 39*

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EXTERNAL SDRV,SCNTL
DIMENSION Y(20),DY(20),A(20),P(20),PLY(20),PU(20),SD(20),
YS(20),DYST(20),YST(20),YSIMP(20),XA(3),XB(3),YC(3,4),
COMMON /BLKI/THETAS,FX,FXFNCBR,FNC,V,ONCOT1,DFNX,D2NDLL,
DFNX,DFM,D2VLC,D2VLC,D2VLC,D2VLC,D2VLC,D2VLC,
/BLK/RLAM,DL0U,DL0V,D2L,DL0U,DL0UV,D2L0UV,D2L0NCR,
D2L0NCR,D2L0UR,D2L0NB
/BLK/INCRD,INCRD
FFS(X) = (S0RT(VX+2.0))AST ((1.0/(X+1.0))-1.570796)/X
FFN(X,Y) = 1.0-Y*(0.1460*X-Y-0.02166)/X
DFN(X,Y) = (-0.2920*X+0.028666)/X
R=AT(5,1000*E-PI*3000) THETAS=0,V=FNCBR,ASTAR,DXWRT
FORMAT(5F16.0)
NIT = 1
5. IF (U,LI,4,00E-06,OR,U,GT,250.1) GO TO 1
IF (V,LI,4,00E-05,OR,V,GT,50.0) GO TO 1
IF (FNCBR,LI,0.00009,OR,FNCBR,GT,4.0) GO TO 1
5. CALL REST(U,V,ASTAR,RLAM,DL0U,DL0V,D2L0UV,D2L0NCR,D2L0NB,
D2L0NCR,D2L0UR,D2L0NB)
CALL NBERV(PLAM,FN,DFNX,D2NDLL)
R=03 = RLAM
WRITE(6,2000) THETAS,ASTAR,U,V,FNCBR,RLAM
200. FORMAT (I11.10X,I10H,THETAS = F20.6/
4. 11X,10H ASTAR = F20.6/
1. 11X,10H U = F20.6/
2. 11X,10H V = F20.6/
3. 11X,10H FNCBR = F20.6/
5. 11X,10H LAMBDA = F20.6//)
WRITE(6,2010) NIT
201. FORMAT (5X,NUMBER OF ITERATIONS = I2)
TH4 = THETAS*4
IF (V,GT,0.2) GO TO 90
IF (V,LE,1.0E-10) GO TO 108
9. THETAB = 0.9



```

02 00156 40* 95 NCT = 0
00157 41* 00 I2 = JHETAB**2
00160 42* T3 = T**HETAB
00161 43* FNC = FNC**T3
00162 44* FM = FM*(RHO)*FNC**FFS*(PHOD)
00163 45* OFM = OFM*(RHO)*FNC**FFS*(R40D)
00164 46* AYY = T**HETAB-TH4
00165 47* BYY = 1.0-IDET**3
00166 48* ETY = E*ETALFNC
00167 49* ETY = E*FM*FM
00170 50* YY = 1.0*V-ET*AYY/RYY
00171 51* DET = (DE*ET*FM*DE*DETALFNC)**3.0*T2*FNCBR
00172 52* OY = -AY/3Y*(DEI2*ET*BY) - 4.0*ET*Y3/BY
00173 53* ZZ = JHETAB-Y/9Y
00174 54* IF(CT.GT.20) GO TO 109
00176 55* IF(Z.LI.1.0) GO TO 105
00200 56* HETAB = (HETAB+1.0)/2.0
00201 57* NCT = NCT+1
00202 58* GO TO 100
00203 59* 05 IF(.25(ZZ-HETAB)/ZZ.LI.1.0E-06) GO TO 110
00205 60* NCT = NCT+1
00206 61* HETAB = ZZ
00207 62* GO TO 100
00210 63* 08 HETAB = 1.0
00211 64* GO TO 110
00212 65* 09 WRITE(6,900)
00214 67* C
00215 68* 10 Y(1) = 1.0
00216 69* Y(2) = HETAB
00217 70* 00 FOR=1(100,20)HIEYTON-RAPHSON FAILS
00220 71* Y1 = Y(1)
00221 72* Y2 = Y(2)
00222 73* CALL NCDESV(FMCHR,HETAB,FM,NCOT1,D2C2T,D2CTNA)
00223 74* CALL MDERIRLAV,FNC,FM,DFMX,DM,D2F4LL,D24DNC,D24LNC,D342LN,D3M2NL)
00224 75* CALL INITIAL(DLDV,DLDVY(3),Y(4),Y(5),Y(6),D2E4LU)
00225 76* CALL INITIAL(DLDV,DLDVY(7),Y(8),Y(9),Y(10),0.0,D2E4LV)
00226 77* CALL INITIAL(D24NC3,D24LNCB,Y(11),Y(12),Y(13),Y(14),1.1,D2E4TN,
00226 78* D2E4L3)
00227 79* CALL INTMIX(D2E4TV,Y(4),DLDV,D2E4LV,D2LDV,Y(16),Y(15))
00230 80* CALL INTMIX(D2E4TY(4),DLDV,D2E4LN,D2LUNB,Y(18),Y(17))
00231 81* CALL INTMIX(D2E4TY(8),DLDV,D2E4LN,D2LVNB,Y(20),Y(19))
00232 82* 00 I15 I=1,20
00235 83* A(I) = 1.0E-05
00236 84* R(I) = 1.0E-05
00236 85* C
00240 86* WRITE(6,2040)
00242 87* 2 40 FORMAT(/Z,6HETAB,9X,6HETAB,9X,2HNC,13X,6HETAB,
00242 88* 1 9X,5HETA,13X,14X,14X,4HZEYTA/)
00242 89* C
00243 90* ZZ = 0.0
00244 91* DX = 1.0/(U*(1.0-HETAB))
00245 92* IFV = 0
00246 93* IF(DX.GI.DXRT) DX = DXRT
00250 94* N = 20
00251 95* IBKP = 1
00252 96* NTRY = 1

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C2      97*      IERR = 0
00253  98*      DLNT = DXWRT/500.0
00254  99*      XWRT = 0.0
00255  100*     LSTEP = 0
00256  101*     LCVT = 0
00257  102*     ICVT = 0
00260  103*     CALL RK5(SDRV,SCNTL,Y,DY,A,R,ZZ,DX,N,IEVD,IBKP,NTRY,IERR,
00261  104*     ,DLY,PD,SO,YSYST,DYST,YSIMP)
00262  105*     XM(1) = -Y(3)
00263  107*     XM(2) = -Y(7)
00264  108*     XM(3) = -Y(11)
00265  109*     AM(1*1) = Y(5)
00266  110*     AM(1*2) = Y(15)
00267  111*     AM(1*3) = Y(17)
00270  112*     AM(2*1) = Y(15)
00271  113*     AM(2*2) = Y(9)
00272  114*     AM(2*3) = Y(19)
00273  115*     AM(3*1) = Y(17)
00274  116*     AM(3*2) = Y(19)
00275  117*     AM(3*3) = Y(13)
00276  118*     CALL FMIN(AM, XM, 3,4)
00277  119*     WRITE (6,205)
00301  120*     205  FORMAT (//45,274 PARAMETERS AT END OF TURF.//)
00302  121*     WRITE (6,210) Y(1)
00305  122*     210  FORMAT (1X,51(10HTHIAE =F10.6,/)
00306  123*     ,WRITE (6,215) Y,V,F,CBR
00313  124*     215  FORMAT (1X,23(3HU =E14.6,15X,3HV =E14.6,12X,7HNCBAR =E14.6,/)
00314  125*     ,WRITE (6,230) Y(3),Y(7),Y(11)
00321  126*     230  FORMAT (1X,19(7HDFDU =E14.6,12X,7HDFDV =E14.6,9X,
00322  127*     ,WRITE (6,240) Y(5),Y(9),Y(13)
00327  128*     ,WRITE (6,245) Y(17),Y(21),Y(25)
00327  129*     245  FORMAT (1X,17(9HDFDU =E14.6,10X,9HDFDV =E14.6,6X,
00327  130*     ,WRITE (6,250) Y(15),Y(17),Y(19)
00335  131*     250  FORMAT (1X,15(10HDFDUV =E14.6,5X,14HDFDUVNCBAR =E14.6,
00335  132*     ,WRITE (6,220) (XM(I),I=1,3)
00336  133*     ,WRITE (6,220) (XM(I),I=1,3)
00344  134*     220  FORMAT (719X9DELTA U =E14.6,10X,9HDELTA V =E14.6,6X,
00344  135*     ,WRITE (6,220) (XM(I),I=1,3)
00345  136*     200  IF (NIT,GT,NITMAX) GO TO 300
00346  137*     NIT = NIT+1
00350  138*     Z1 = U
00351  139*     Z2 = V
00352  140*     Z3 = F,C,IR
00353  141*     CALL BNDEND(Y,U,V,FNCBR,YM)
00354  142*     CALL RESBND(U,V,XM,ASTAR)
00355  143*     Z5 = Y(11)-THETAS
00356  144*     IF (Z5,LT,0.0001) GO TO 2080
00357  145*     IF (ABS(XM(1))/Z1,GT,0.0001) GO TO 50
00361  146*     IF (ABS(XM(2))/Z2,GT,0.0001) GO TO 50
00363  147*     IF (ABS(XM(3))/Z3,GT,0.0001) GO TO 50
00365  148*     WRITE(6,2070)
00371  149*     2070 FORMAT(1H0.15HOPTIMUM REACHED)
00372  150*     GO TO 1
00373  151*     300  WRITE(6,2050) NITMAX
00373  152*     GO TO 1
00373  153*

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00376 154* 2050 FORMAT (1X,30H NUMBER OF ITERATIONS EXCEEDS ,I2)
00377 155* GO TO 1
00400 156* 2080 WRITE(6,2085)
00402 157* 2085 FORMAT(1H0,24HVANISHING HEAT REJECTION)
00403 156* GO TO 1
00404 159* 3000 STOP
00405 161* END

END OF COMPILATION: NO DIAGNOSTICS.

FOR 15 RKS
FOR S9A-07/27/72-17:43:28 (,0)

SUBROUTINE RKS ENTRY POINT 000643
STORAGE USED: CODE(1) 001040; DATA(0) 000064; BLANK COMMON(2) 000000

EXTERNAL REFERENCE: (BLOCK, NAME)
0003 NERR25
0004 NEXP55
0005 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)
0001 000010 10L 0001 000313 110L 0'01 000333 120L 0001 00045 126G 0001 000343 130L
0001 000071 14G 0001 000355 140L 0'01 000105 146G 0001 000130 156G 0001 000417 160L
0001 000150 164 0001 000177 174G 0'01 000500 185L 0001 000510 190L 0001 000013 20L
0001 000232 205 0001 000270 217G 0'01 000524 220L 0001 000530 230L 0001 000543 240L
0001 000374 243 0001 000323 25L 0'01 000552 250L 0001 000554 251L 0001 000572 257L
0001 000604 259 0001 000623 270L 0'01 000456 300L 0001 000615 336G 0001 000654 40L
0001 000660 45L 0001 000006 5L 0'01 000076 50L 0001 000123 70L 0001 000135 80L
0000 R 000014 7M 0000 R 000007 8MAX 0'00 R 000011 C 0000 R 000010 D 0000 R 000001 00Y
0000 R 000003 0ELI 0000 R 000012 F 0'00 R 000000 FR10 0000 I 000004 I 0000 I 000005 IFLAG
0000 000030 INJF 0000 I 000002 TSIMP 0'00 I 000013 J 0000 R 000006 S

00101 1* SUBROUTINE RKS(deriv,ctrl,y,ya,r,t,del,n,ifvd,irkp,ntry,
00101 2* 1ERRVDELYPPC,SD,YS,YST,DYST,YJMP) D600020
00103 3* DIMENSION Y(4),DY(4),AIN,R(N),DELY(N), D60 3
00103 4* IP5(N),SD(N),YS(N),YST(N),YST(4),YSIMP(N) D600040
00104 5* EXTERNAL DERIV,CTRL D6000500
00104 6* FR10 IS FIFTH ROOT OF TEN D600 60
00105 7* FR10=1.5848932 D60000700
00106 8* 1ERR=0 D6000000
00106 9* C YS CONTAINS Y VALUES AT LEFT END POINT OF INTEGRATION INTERVAL D6000000
00106 10* C YSIMP CONTAINS Y FOR SIMPSON'S RULF CHECK CHECK NOT MADE FOR D6000100
00106 11* C FIXED STEP MODE ISYMP IS CONTROL PARAMETER #1, FIXED #2 VARD600120
00106 12* C IF FIXED STEP SIZE GO ONE INTERVAL OF LENGTH DELT AND RETURN TO D6000140
00106 13* C CNTRL, IF VAR GO TWO INTERVALS BEFORE RETURN TO CONTRL D600150
00106 14* C IFVD = 0 VARIABLE INTERVAL D600160
00106 15* C IFVD = 1 FIXED D600170
00106 16* C IRKP = 0 CUT INTERVAL ONCE BEFORE REPEAT (UNDER IFVD=0) D600180
00106 17* C NTRY = 1 CUT AS REQUIRED D60 200
00106 18* C CONTINUE INTEGRATING D6002100
00106 19* C RETURN FROM RKS D60 220
00106 20* C STEP REPEATED WITH NEW DELT D6002300
00106 21* C RESTART D600240
00106 22* C
00106 23* C
00106 24* C

00106	25*	C	IERR = 0	NORMAL			D5002500
00106	26*	C	-1	DELTD, RETURN FROM RKS			D5002500
00106	27*	C	1	A(I)+R(I)*ABS(Y(I))-0., RETURN FROM RKS			D5002700
00107	28*	5	IF(DEL) 20, 10, 20				D5002800
00112	29*	1)	IERR=-1				D5002900
00113	30*	60	TO 270				D7003000
00114	31*	2)	CALL DERIV(Y, DY, T)				D5003100
00115	32*	NIRY=1					D5003200
00116	33*	CALL CURL(Y, DY, DEL, T, NTRY, IFV)					D5003300
00117	34*	2)	DDI=DEL				D5003400
00120	35*	3)	IF(IFV) 40, 30, 40				D5003500
00123	36*	3)	ISY=PS2				D5003600
00124	37*	DELTD=DEL/2.					D500370
00125	38*	DO 31	IELN				D7003900
00130	39*	3)	SJAT)=0.0				D5003900
00132	40*	IFLAGE=1					D5004000
00133	41*	S=1.					D5004100
00134	42*	50	TO 45				D6004200
00135	43*	4)	ISY=PF1				D5004300
00136	44*	DELTD=DEL					D5004400
00137	45*	4)	DO 46	IELN			D5004500
00142	46*	YSI(I)=Y(I)					D5004500
00143	47*	4)	NYST(I)=DY(I)				D50 470
00145	48*	5)	DO 66	IELN			D6004800
00150	49*	DLY(I)=DELTD*DY(I)					D5004900
00151	50*	PDI)=DELY(I)					D500500
00152	51*	6)	CONTINUE				D5005100
00154	52*	3)	TO (80, 70), ISYMP				D5005200
00155	53*	7)	DO 71	IELN			D5005300
00160	54*	7)	SJAT)=SD(I)+S*DY(I)				D5005400
00162	55*	8)	T=1+DELTD/2.				D5005500
00163	56*	DO 95	IELN				D5005600
00166	57*	YSI(I)=Y(I)					D500570
00167	58*	Y(I)=YS(I)+DELY(I)/2.					D5005800
00170	59*	9)	CONTINUE				D5005900
00172	60*	CALL	DERIV(Y, DY, T)				D5005900
00173	61*	DO 96	IELN				D5006100
00176	62*	DLY(I)=DELTD*DY(I)					D500620
00177	63*	P(I)=P0(I)+2.*DELY(I)					D5006300
00200	64*	Y(I)=YS(I)+DELY(I)/2.					D500640
00201	65*	9)	CONTINUE				D5006500
00203	66*	CALL	DERIV(Y, DY, T)				D5006500
00204	67*	DO 95	IELN				D500670
00207	68*	DLY(I)=DELTD*DY(I)					D500680
00210	69*	P(I)=P0(I)+2.*DELY(I)					D5006900
00211	70*	Y(I)=YS(I)+DELY(I)					D500700
00212	71*	9)	CONTINUE				D5007100
00214	72*	IFLAGE=1/2.					D5007200
00215	73*	CALL	DERIV(Y, DY, T)				D500730
00216	74*	DO 100	IELN				D5007400
00221	75*	DLY(I)=DELTD*DY(I)					D5007500
00222	76*	P(I)=P0(I)+DELY(I)					D500760
00223	77*	Y(I)=YS(I)+P0(I)/6.					D600770
00224	78*	10)	CONTINUE				D6007800
00226	79*	50	TO (110, 120), ISYMP				D6007900
00227	80*	11)	NIRY=1				D6008000
00230	81*	CALL	DERIV(Y, DY, T)				D6008100

00231	82*	CALL CNTRL(Y,DY,DEL,T,NTRY,IFV)	D600920
00232	83*	GO TO 300	D600930
00233	84*	12) GO TO (130,140),IFLAG	D600940
00234	85*	13) S=4	D600950
00235	86*	IFLAG=2	D600960
00236	87*	CALL DERIV(Y,DY,I)	D600970
00237	88*	GO TO 50	D600980
00240	89*	14) CALL DERIV(Y,DY,I)	D600990
00241	90*	AMAX =0	D601000
00242	91*	DO 180 I=1,N	D601010
00245	92*	S(I)=SD(I)+DY(I)	D601020
00246	93*	YSIMP(I)=YS(I)+DELT*S(I)/3	D601030
00247	94*	D =ABS(Y(I))-YSIMP(I)	D601040
00250	95*	C =A(I)+R(I)*ABS(Y(I))	D601050
00251	96*	IF(C) 160,150,160	D601060
00254	97*	15) IERR=1	D601070
00255	98*	GO TO 270	D601080
00256	99*	16) E =ABS(D /C)	D601090
00257	100*	AMAX=AMAX1(AMAX,E)	D601100
00260	101*	18) CONTINUE	D601110
00262	102*	IF(AMAX-1.) 215,215,230	D601120
00265	103*	21) NTRY= 1	D601130
00266	104*	CALL CNTRL(Y,DY,DEL,T,NTRY,IFV)	D601140
00267	105*	30) IF(NTRY-1) 185,185,310	D601150
00272	106*	31) IF(NTRY-2) 270,270,330	D601160
00275	107*	33) IF(NTRY-3) 340,340,5	D601170
00300	108*	34) I=20	D601180
00301	109*	IF(DEL) 259,10,259	D601190
00304	110*	15) GO TO (40,190),ISYMP	D601200
00305	111*	19) IF(AMAX-.75) 200,25,220	D601210
00310	112*	20) IF(AMAX-.075) 210,25,225	D601220
00313	113*	21) DEL=DEL*FR10	D601230
00314	114*	GO TO 25	D601240
00315	115*	22) DEL=DEL/FR10	D601250
00316	116*	GO TO 25	D601260
00317	117*	23) I =1+ I9KP	D601270
00320	118*	GO TO (240,250),I	D601280
00321	119*	24) I=I-DEL	D601290
00322	120*	DEL=DEL/FR10	D601300
00323	121*	GO TO 259	D601310
00324	122*	25) J=1	D601320
00325	123*	25) AME=AMAX/10.**J	D601330
00326	124*	IF(1.-AME) 255,257,257	D601340
00331	125*	25) J=J+1	D601350
00332	126*	GO TO 251	D601360
00333	127*	25) I=I-DEL	D601370
00334	128*	DEL=DEL/(FR10**J)	D601380
00335	129*	25) DO 245 I=1,N	D601390
00340	130*	DY(I)=DYST(I)	D601400
00341	131*	24) Y(I)=YS(I)	D601410
00343	132*	GO TO 25	D601420
00344	133*	27) RETURN	D601430
00345	134*	END	D601440

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS SDRV
FOR 59A-07/27/72-17:43:39 (90)

SUBROUTINE SDRV ENTRY POINT 000601

STORAGE USED: CODE(1) 000605; DATA(0) 000056; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 ELKI 000024
0004 BLX0 000011
0005 BLX8 000011
0006 VAS 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0007 ETA
0010 MCDERV
0011 WIER
0012 DELTA
0013 DELTA
0014 MIXDER
0015 MERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R	000003	AA	0004	000003	A1	0000	000004	A2	0004	000005	A3	0004	000006	AA
0004	000007	A5	0004	000010	A6	0000	000005	B8B	0000	000037	DA1DU	0000	000007	DA1DU
0000 R	000023	DA1DV	0000 R	000040	DA2DH	0000	000010	DA2DU	0000 R	000024	DA2DV	0000 R	000041	DA3DH
0000 R	000011	DA3DU	0000 R	000025	DA3DV	0000	000042	DA4DH	0000 R	000012	DA4DV	0000 R	000026	DA4DU
0000 R	000043	DA5DN	0000 R	000013	DA5DU	0000	000027	DA5DV	0000 P	000044	DA6DN	0000 R	000014	DA6DU
0000 R	000030	DA6DV	0000 R	000045	DE5DH	0000	000004	DE8TB	0000 R	000015	DE9DU	0000 R	000031	DE9DV
0000 R	000046	DE1	0000 R	000047	DEPH	0000	000017	DFPU	0000 R	000035	DEVA	0012	000000	DETA
0000 R	000016	DEU	0000 R	000032	DEV	0000	000023	DF1DL	0000	000021	DF4TR	0003	000013	DFW
0003 R	000012	DFVX	0005	000010	DFVX	0000	000006	DL0ICB	0005	000001	DL0U	0005	000002	DL0V
0000 R	000050	DFDN	0000 R	000020	DFDU	0000	000034	DF0V	0000 R	000036	DF0DN	0003	000016	DF0TL
0005 R	000006	DF0DU	0000 R	000022	DF0DV	0000	000001	D2C02T	0000 R	000002	D2CTM9	0003	000016	D2EMIL
0005 R	000003	D2LDU	0005 R	000004	D2LDUW	0000	000005	D2LD0V	0005	000007	D2LNCR	0005	000010	D2LUN9
0005 R	000011	D2LVN	0003 R	000015	D2M0NC	0003	000014	D2MLNC	0000 R	000051	D2MHCN	0000 R	000021	D2MNCU
0000 R	000035	D2MNC	0003	000011	D2HDL	0004	000001	D3M2LN	0004	000002	D3M2NL	0004	000011	ER
0006 R	000002	ET	0007 R	000000	ETA	0003	000022	F3	0003	000002	F4	0003	000003	F4
0003 R	000005	FJC	0003 R	000024	FNCBR	0000	000056	INUP5	0005	000000	RLAN	0003	000000	THETA9
0000 R	000000	THETA	0003 R	000001	THETAS	0004	000000	U	0003	000006	V	0003	000017	Y1
0003 R	000020	Y2	0006 R	000000	Z1	0006	000001	Z2						

00101 1* SUBROUTINE SDRV(Y,DY,X)
00101 2* C
00101 3* C CALCULATION OF DERIVATIVES FOR THE INTEGRATION SUBROUTINE
00101 4* C
00103 5* DIMENSION Y(20),DY(20)


```

02 COMMON /BLK1/THE TAB, THE TAB, FNC, FNC, FNC, FNC, V, DMCOT1, OFNX, D2N2LL,
00104 6* DFNX, OFM, D2MLNC, D2VONC, D2EMLL, Y1, Y2, DE4DTB, E3, DE1DL/
00104 7* BLK0/0, D3V2LN, D3M2NL, A1, A2, A3, A4, A5, A6, EB
00104 8* /BLK3/R/LA, DL0V, DL0V, DL0V, D2LVNB
00104 9* D2LVNB, D2LVNB, D2LVNB
00104 10* /VAB7, Z1, Z2, ET
00104 11* Z1 = FNC
00104 12* Z2 = FNC*ETA(FNC)+FN
00106 13* ET = ETA(FNC)
00107 14* THE TAB = Y(1)
00110 15* THE TAB = Y(2)
00111 16* Y1 = Y(1)
00112 17* Y2 = Y(2)
00113 18* CALL NCDER(VEN, THE TAB, FNC, ANCDT1, D2C92T, D2CTNB)
00114 19* CALL MDER(R/LA, FNC, FNC, OFMX, OFM, D2FMLL, D2VONC, D2MLNC, D3V2LN, D3M2NL)
00115 20* AAA = THE TAB - THE TAB
00116 21* Y(1) = -1/A44
00117 22* F8 = FNC*ETA(FNC)+FN
00120 23* DE8DTB = 3*THE TAB**2*FNCBR*(FNC*ETA(FNC)+ETA(FNC)*OFM)
00121 24* DE8 = 4*THE TAB**3/(THE TAB**4 - THE TAB**4)
00122 25* Y(2) = -1/(1/AAA + DE8DTB/F8 + B8)
00123 26* CALL DER(V(3), Y(4), Y(5), Y(6), DL0V, D2LVNB, DY(3), DY(4), DY(5),
00124 27* DY(6), 0, 1, DMCOT1, A10V, D2C92T, D3V2LN, D440V, D450V,
00124 28* D630V, DER(V, DEU, DEU, DEU, DEU, DEU, D2VNCU)
00125 29* CALL DER(V(7), Y(8), Y(9), Y(10), Y(11), DL0V, D2LVNB, DY(7), DY(8), DY(9),
00125 30* DY(10), 0, 0, DMCOT1, A10V, D2C92T, D3V2LN, D440V, D450V,
00125 31* D630V, DER(V, DEU, DEU, DEU, DEU, DEU, D2VNCU)
00126 32* CALL DER(V(11), Y(12), Y(13), Y(14), DL0V, D2LVNB, DY(11), DY(12),
00126 33* DY(13), DY(14), 1, 0, DMCOT1, A10V, D2C92T, D3V2LN, D440V, D450V,
00126 34* D630V, DER(V, DEU, DEU, DEU, DEU, DEU, D2VNCU)
00126 35* D450N, D460N, D480N, E4, DEPN, D40N, D2MNCU)
00127 36* CALL MIXDER(Y(4), Y(10), Y(7), Y(16), Y(15), DMCOT1, DMCOT1, DY(4), DA10V,
00127 37* DA10V, D420V, D420V, D420V, D430V, D440V, D450V, D450V, D450V,
00127 38* D460V, D460V, D460V, D460V, D460V, D460V, D460V, D460V, D460V,
00127 39* DEPU, JF, PV, D40V, D40V, D40V, D2MNCU, D2MNCU, 1, 0, DY(16),
00127 40* DY(15))
00130 41* CALL MIXDER(Y(4), Y(11), Y(12), Y(18), Y(17), DMCOT1, DMCOT1, DY(4),
00130 42* DA10V, DA10V, DA20V, DA20V, DA30V, DA30V, DA40N, DA40N, DA50V,
00130 43* D450V, D460V, D460V, D460V, D460V, D460V, D460V, D460V, D460V,
00130 44* DEU, DEU, DEU, DEU, DEU, DEU, DEU, DEU, DEU, DEU,
00130 45* DY(18), DY(17))
00130 46* CALL MIXDER(Y(4), Y(12), Y(11), Y(20), Y(19), DMCOT1, DMCOT1, DY(8),
00131 47* DA10V, DA10V, DA20V, DA20V, DA30V, DA30V, DA40N, DA40N, DA50V,
00131 48* D450N, D460V, D460V, D460V, D460V, D460V, D460V, D460V, D460V,
00131 49* DEU, DEU, DEU, DEU, DEU, DEU, DEU, DEU, DEU, DEU,
00131 50* DY(20), DY(19))
00132 51* RETURN
00133 52* END

```

END OF COMPILATION: NO DIAGNOSTICS.

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FOR IS SCNTL
FOR S9A-07/27/72-17:42:50 (1,0)

SUBROUTINE SCNTL ENTRY POINT 000147

STORAGE USED: CODE(1) 000174; DATA(0) 000014; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 XCI 000005
0004 VAB 000003
0005 BLKI 000024

EXTERNAL REFERENCES (BLOCK, NAME)

0006 WZJUB
0007 NIC2\$
0010 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000002 2000 F 0001 000054 5L 0001 000061 50L 0001 000135 60L 0003 R 000000 PLMT
0000 R 000000 DXSTR 0003 R 000003 XWRT 0004 R 000002 ET 0003 I 000001 ICNT 0000 000006 INJPS
0000 I 000001 LCNT 0003 I 000004 LSTEP 0005 R 000000 VAL 0003 R 000002 XWRT 0004 R 000000 Z1
0004 R 000001 Z2

00101 1* SUBROUTINE SCNTL(Y,XY,DX,X,NTRY,IFVD)

00101 2* C
00101 3* C INTEGRATION CONTROL PROGRAM
00101 4* C
00103 5* DIMENSION Y(20),DY(20)
00104 6* COMMON /MCT/ PLMT,ICNT,XWRT,DXSTR,LSSTEP
00104 7* 1 /VAR/ Z1,Z2,ET
2 /BLKI/VAL(20)
00105 8* ICNT = ICNT+1
00106 10* IF(DX.GE.DXWRT.AND.ICNT.GT.1) LSTEP = 1
00110 11* IF(ABS(X-XWRT).LT.PLMT) GO TO 50
00112 12* IF(XWRT.GT.X) GO TO 5
00112 13* C
00114 14* DXSTR = DX
00115 15* DA = DX+XWRT-X
00116 16* LCNT = 1
00117 17* NTRY = 3
00120 18* RETURN
00120 19* C
00121 20* 5 NTRY = 1
00122 21* RETURN
00122 22* C
00123 23* 51. WRITE(6,2000) Y(1),Y(2),Z1,Z2,ET,VAL(3),VAL(4),X
00135 24* 2000 FORMAT (BF15.7)

```

02 00136 25* IF(LCNT.EQ.1) DX = DXSTR
    00140 26* LCNT = 0
    00141 27* IF(ABS(1.0-YWRT).LE.DLMT) GO TO 60
    00143 28* XWRT = XWRT+DXSTR
    00144 29* NTRY = 1
    00145 30* IF(LSTEP.EQ.0) RETURN
    00147 31* DX = DXWRT
    00150 32* IF(VJ = 1
    00151 33* RETURN
    00151 34* C
    00152 35* GO NTRY = 2
    00153 36* RETURN
    00154 37* END

```

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS BNCND
FOR 59A-07/27/72-17:43:54 (10)

SUBROUTINE BNCND ENTRY POINT 000350

STORAGE USED: CODE(1) 000411; DATA(0) 000065; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 BLK3 00000

EXTERNAL REFERENCES (BLOCK, NAME)

0004 FMINV
0005 SER35

STORAGE ASSIGNMENT BLOCK, TYPE, RELATIVE LOCATION, NAME

0001	000115	601L	0001	000130	601L	0001	000134	602L	0001	000137	603L	0001	000167	610L					
0001	000202	611L	0001	000206	612L	0001	000211	613L	0001	000241	620L	0001	000254	621L					
0001	000260	622L	0001	000263	623L	0001	000313	630L	0001	000040	700L	0000	R	000000					
0003	000000	DNCBD	0003	000001	DNCBDV	0000	I	000017	I	0000	000044	INJPS	0000	I	000020	J			
0000	I	000021	K	0000	R	000014	XV	0000	R	000022	Z1	0000	R	000023	Z2	0000	R	000024	Z3

00101 1* SUBROUTINE BNCND(Y,U,V,FNCB,X)

00101 2* C

00101 3* C

00101 4* C

00104 6* DIMENSION AM(3,1),XN(3),XN(3),Y(20)

00104 6* COMMON /BLK3/DNCBDU,DNCBDV

00105 7* I = 0

00106 8* J = 0

00107 9* K = 0

00110 10* Z1 = 0

00111 11* Z2 = V

00112 12* Z3 = FNCB

00113 13* J = Z1+X*(1)

00114 14* J = Z2+Y*(2)

00115 15* FNCB = Z3+Y*(3)

00116 16* AN(1,1) = Y(5)

00117 17* AN(1,2) = Y(15)

00120 18* AN(1,3) = Y(17)

00121 19* AN(2,1) = Y(15)

00122 20* AN(2,2) = Y(9)

00123 21* AN(2,3) = Y(19)

00124 22* AN(3,1) = Y(17)

00125 23* AN(3,2) = Y(19)

00126 24* AN(3,3) = Y(13)

00127 25* 700 IF (U.LI.4.00E-06.OR.U.GT.250.1) GO TO 600

00131 26* IF (V.LI.4.00E-05.OR.V.GT.50.01) GO TO 610

```

00133 27* IF (FNCBR.LT.0.00009.OR.FNCBR.GT.4.01) GO TO 620
00135 28* RETURN
00136 29* 60: IF (U.LE.5.0E-06) GO TO 601
00140 30* IF (U.GE.250.) GO TO 602
00142 31* GO TO 610
00143 32* 60: XN(1) = 5.0E-06-Z1
00144 33* GO TO 603
00145 34* 60: XN(1) = 250.-Z1
00146 35* 60: AN(1,1) = 1.
00147 36* AN(1,2) = 0.
00150 37* AN(1,3) = 0.
00151 38* I = 1
00152 39* IF (I.EQ.0) XN(1) = -Y(3)
00154 40* IF (J.EQ.0) XN(2) = -Y(7)
00156 41* IF (K.EQ.0) XN(3) = -Y(11)
00160 42* CALL FMINV(AN,XN,3,4)
00161 43* 61 IF (V.LE.5.0E-05) GO TO 611
00163 44* IF (V.GE.50.) GO TO 612
00165 45* GO TO 620
00166 46* 61: X(2) = 5.0E-05-Z2
00167 47* GO TO 613
00170 48* 61: X(2) = 50.-Z2
00171 49* 61: AN(2,1) = 0.
00172 50* 61: AN(2,2) = 1.
00173 51* 61: AN(2,3) = 0.
00174 52* J = 1
00175 53* IF (I.EQ.0) XN(1) = -Y(3)
00177 54* IF (J.EQ.0) XN(2) = -Y(7)
00201 55* IF (K.EQ.0) XN(3) = -Y(11)
00203 56* CALL FMINV(AN,XN,3,4)
00204 57* 62: IF (FNCBR.LE.1.0E-04) GO TO 62.
00206 58* IF (FNCBR.GE.4.00) GO TO 622
00210 59* GO TO 630
00211 60* 62: XN(3) = 1.0E-04-Z3
00212 61* GO TO 623
00213 62* XN(3) = 4.00-Z3
00214 63* 62: AN(3,1) = 0.
00215 64* AN(3,2) = 0.
00216 65* AN(3,3) = 1.
00217 66* X = 1
00220 67* IF (I.EQ.0) XN(1) = -Y(3)
00222 68* IF (J.EQ.0) XN(2) = -Y(7)
00224 69* IF (K.EQ.0) XN(3) = -Y(11)
00226 70* CALL FMINV(AN,XN,3,4)
00227 71* 63: XN(1) = XN(1)
00230 72* XN(2) = XN(2)
00231 73* XN(3) = XN(3)
00232 74* U = Z1+XN(1)
00233 75* V = Z2+XN(2)
00234 76* FNCBR = Z3+XN(3)
00235 77* GO TO 700
00236 78* END

```

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS RESND
FOR 59A-07/27/72-17:44:04 (10)

SUBROUTINE RESND ENTRY POINT 000203

STORAGE USED: CODE(), 000232; DATA(0) 000053; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 SORT
0004 NRJPS
0005 N122\$
0006 NARR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 00026 1L 0001 000126 2L 00:0 000007 2000F 0001 000144 3L 0001 000161 4L
0000 R 000003 A 0000 R 000004 B 00:0 R 000005 C 0000 R 000006 EPS 0000 000037 INJPS
0000 R 000000 U2 00:0 R 000001 V2 00:0 R 000002 Z

00101 1* SUBROUTINE RESND(U,V,XM,ASTAR)
00101 2* C
00101 3* C RESND CHECKS THE BOUNDARY OF LAMBDA AND KEEPS ASTAR
00101 4* C GREATER THAN U*V
00101 5* C
00103 6* DIMENSION X4(3)
00104 7* U2 = U-X4(1)
00105 8* V2 = V-X4(2)
00106 9* Z = ASTAR-U*V
00107 10* IF(Z.LT.2.*U*V*1.0E-06) GO TO 1
00111 11* RETURN
00111 12* C
00112 13* A = X4(1)*X4(2)
00113 14* B = U2*X4(2)+V2*X4(1)
00114 15* C = U2*Z-0.09*ASTAR
00115 16* IF(ABS(C).LE.1.0E-05.AND.XM(2).LT.0.) GO TO 2
00117 17* IF(ABS(C).LE.1.0E-05.AND.XM(1).LT.0.) GO TO 3
00117 18* C
00121 19* EPS = (-3+SQRT(3**2.-4.*A*C))/2./A
00122 20* X4(1) = EPS*X4(1)
00123 21* X4(2) = EPS*X4(2)
00124 22* U = U2*XM(1)
00125 23* V = V2*X4(2)
00126 24* GO TO 4
00127 25* EPS = (0.99*ASTAR-U2*V)/(V*XM(1))
00130 26* X4(1) = EPS*X4(1)
00131 27* U = U2*X4(1)
00132 28* GO TO 4
00133 29* EPS = (0.99*ASTAR-U*V2)/(U*XM(2))
00134 30* XM(2) = EPS*XM(2)

```

00135 31* V = V2+X*(2)
00136 32* C
00136 33* 4 WRITE(6,2000) X(1),X(2),EPS
00143 34* 2000 FORMAT (//5X'EPSILON CALCULATED' DELTAU =E14.6/
00143 35* 1 31X' DELTAV =E14.6/31X'EPSILON = 'E14.6)
00143 36* C
00144 37* RETURN
00145 38* END

```

END OF COMPILATION: NO DIAGNOSTICS.

02 3FOR,IS REST
FOR S9A-07/27/72-17:44;10 (,0)

SUBROUTINE REST ENTRY POINT 000066

STORAGE USED: CODE(1) 0001201 DATA(0) 0000231 BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R 000000 A1 0000 000003 INJP5

00101 1* SUBROUTINE REST(U,V,ASTAR,RLAM,DLDU,DLDV,D2LDUU,D2LDUV,D2LDVV,
00101 2* 1DLDCB,D2LNCB,D2LUNR,D2LVNB)
00101 3* C
00101 4* C
00101 5* C
00101 6* C
00103 A1 = ASTAR-I*V
00104 RLAM = 2*U*V/A1
00105 DLDJ = 2.*ASTAR-V/A1**2.
00106 DLDV = 2.*ASTAR-U/A1**2.
00107 10* D2LDUU = 4.*ASTAR**2./A1**3.
00110 11* D2LDUV = 2.*ASTAR*(ASTAR+U*V)/A1**3.
00111 12* D2LDVV = 4.*ASTAR*U**2./A1**3.
00112 13* DLDCB = 0.
00113 14* D2LNCB = 0.
00114 15* D2LUNR = 0.
00115 16* D2LVNB = 0.
00116 17* RETURN
00117 18* END

END OF COMPILATION: NO DIAGNOSTICS.

02 JFOR.IS NDERV FOR 59A-07/27/72-17:49:13 (L0)

SUBROUTINE NDERV ENTRY POINT 000056

STORAGE USED: CODE(1) 0000701 DATA(0) 0000151 BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 SORT
0004 ASIN
0005 NERR36

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R 000000 C4 0000 R 000001 C5 0000 R 000002 C6 0000 000006 INJPS

00101 1* SUBROUTINE NDERV(RLAM, FN, DFNX, D2NDLL)
00101 2* C
00101 3* C N AND ITS DERIVATIVES
00101 4* C
00103 5* C4 = RLA+1.0
00104 6* C5 = RLA+2.0
00105 7* C6 = SORT(RLAM*C5)
00106 8* FN = (1.5707963*C5-C6-ASIN(1.0/C4))/RLAM
00107 9* DFNX = -(FN+C6/C4-1.0)/RLAM
00110 10* D2NDLL = -(2.0*DFNX+1.0/(C4*C4*C6))/RLAM
00111 11* RETURN
00112 12* END

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS MDER
FOR S9A-07/27/72-1714416 (P0)

SUBROUTINE MDER ENTRY POINT 000251

STORAGE USED: CODE(1) 000304) DATA(0) 000066) BLANK COMMON(2) 000000

EXTERNAL REFERENCES (LOCK, NAME)

0003 SGR1
0004 ASI1
0005 NERR35

STORAGE ASSIGNMENT (LOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R 000011 CFN 0000 R 000030 C1 0000 R 000017 C10 0000 R 000020 C11 0000 R 000022 C12
0000 R 000001 C2 0000 R 000003 C4 0000 R 000004 C5 0000 R 000005 C6
0000 R 000006 C7 0000 R 000007 C8 0000 R 000010 C9 0000 R 000015 DCFDNC 0000 R 000013 DCFNCL
0000 R 000014 DFFSOL 0000 R 000015 D2CELL 0000 R 000025 D2CFNC 0000 R 000026 D2CLNC 0000 R 000023 D2C2LL
0000 R 000021 D2C3LL 0000 R 000024 D2FSLL 0000 R 000027 D3C2LN 0000 R 000030 D3C2NL 0000 R 000012 FFS
0000 000040 INJP5

SUBROUTINE MDER (RLAM, FNC, FM, DFMX, DFM, D2FMLL, D2MDNC, D2MLNC, D3M2LN,

1 3M2NL)

AND ITS DERIVATIVES

00101 1* = 1
00101 2* = 2
00101 3* = 3
00101 4* = 4
00101 5* = 5
00101 6* = 6
00101 7* = 7
00101 8* = 8
00101 9* = 9
00101 10* = 10
00101 11* = 11
00101 12* = 12
00101 13* = 13
00101 14* = 14
00101 15* = 15
00101 16* = 16
00101 17* = 17
00101 18* = 18
00101 19* = 19
00101 20* = 20
00101 21* = 21
00101 22* = 22
00101 23* = 23
00101 24* = 24
00101 25* = 25
00101 26* = 26
00101 27* = 27
00101 28* = 28

```

00132 29* 02FSLL = (D2C2LL+D2C3LL-2.*DFF5DL)/RLAM
00133 30* 02EVLL = CFN*02FSLL+2.*DFF5DL*DCFNDL+FFS*02CFLL
00134 31* 02CFNC = -0.2920/RLAM
00135 32* 02UDNC = FFS*02CFNC
00136 33* 02CLHC = (0.146*FNC+C1)*C7
00137 34* 02VLNC = DCEMNC*DEFSDL+D2CLNC*FFS
00140 35* 03CPLN = -2.*D2CLNC/RLAM
00141 36* 03V2LI = DCEMNC*02FSLL+2.*DFF5DL*02CLNC+FFS*03C2LN
00142 37* 03C2NL = 0.2920*C7
00143 38* 03I2NL = FFS*03C2NL+DEFSDL*02CFNC
00144 39* RETURN
00145 40* END

```

END OF COMPILATION: NO DIAGNOSTICS.

02 9FOR,IS NCDERV
FOR 59-07/27/72-17:44:19 (10)

SUBROUTINE NCDERV ENTRY POINT 000031

STORAGE USED: CODE(1) 000044; DATA(0) 000013; BLANK COMMON(2) 000000

EXTERNAL REFERENCES: (BLOCK, NAME)

0003 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION), NAME)

0010 C00004 IN: S 0000 R 000000 T2 0000 R 000001 T3

00101 1* SUBROUTINE NCDERV(FNCR,THETA1,FNC,DNCD1,D2CD2T,D2CTNR)
00101 2* C TIC AND ITS DERIVATIVES
00101 3* C
00101 4* C
00103 5* T2 = THETA**2
00104 6* T3 = T2*THETA
00105 7* FNC = FNCR*T3
00106 8* DNCD1 = 3.*FNCR*T2
00107 9* D2CD2T = 6.*FNCR*THETA
00110 10* D2CTNB = 3.*T2
00111 11* RETURN
00112 12* END

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS MIXDER
FOR S9A-07/27/72-17:44:49 (J0)

SUBROUTINE MIXDER ENTRY POINT 000347

STORAGE USED: CODE(1) 00054; DATA(0) 000104; BLANK COMMON(2) 000000

COMMON BLOCKS:

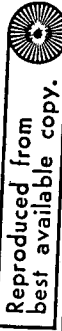
0003 BLKI 000021
0004 BLKD 000012

EXTERNAL REFERENCES (BLOCK, NAME)

0005 DDETA
0006 DETA
0007 DDDETA
0010 ETA
0011 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0004 R 000003 A1 0004 R 000004 A2 0004 R 000005 A3 0004 R 000006 A4 0004 R 000007 A5
0004 R 000010 I6 0007 R 000000 DDDETA 0005 R 000010 DETA 0006 R 000000 DETA 0003 R 000023 DF101
0003 00021 DE4DT 0003 R 000013 CFM 0003 R 000010 DFNX 0003 000007 D12DT1
0000 R 000006 D12DX 0000 R 000003 D2A1XY 0000 R 000020 D2A2XY 0000 R 000021 D2A3XY 0000 R 000022 D2A4XY
0000 R 000015 D2A5XY 0000 R 000004 D2A6XY 0000 R 000017 D2E0XY 0000 R 000012 D2E1XY 0000 R 000011 D2E2XY
0003 R 000016 D2E3ML 0000 R 000013 D2E4ML 0000 R 000015 D2E5HC 0000 R 000014 D2E6LC 0003 R 000014 D2E7LC
0003 R 000011 D2E8DL 0000 R 000016 D2E9DX 0000 R 000007 D3MNL 0000 R 000010 D3MNL 0004 R 000001 D3M2LN
0004 R 000002 D3M2NY 0000 R 000005 D3M2NY 0000 R 000011 EN 0010 R 000000 ETA 0003 000022 F3
0003 R 000002 FM 0003 000003 FN 0003 R 000005 FNC 0003 R 000004 FNCBR 0000 000026 I4DP\$
0003 000000 THEI 1 0003 000001 THEIAS 0004 R 000000 U 0003 R 000006 V 0000 R 000000 Y
0003 000017 Y1 0003 R 000020 Y2 0000 R 000002 Z



SUBROUTINE MIXDER(D12DX,D12DY,D12FY,D2A1XY,D2A2XY,D2A3XY,D2A4XY,D2A5XY,D2A6XY,D2E0XY,D2E1XY,D2E2XY,D2E3ML,
D2E4ML,D2E5HC,D2E6LC,D2E7LC,D2E8DL,D2E9DX,D3MNL,D3M2LN,D3M2NY,EN,FN,FNC,FNCBR,FNC,V,DNCOT1,DFNX,D2NDLL,
DFMX,DFY,D2LNC,D2VNC,D2MNC,D2MLL,Y1,Y2,DE4DT8,E3,DE1DL,
D2LXY,DE0Y,DE1Y,DE2Y,DE3Y,DE4Y,DE5Y,DE6Y,DE7Y,DE8Y,DE9Y,
D3Y,D3MNCX,D3MNCY,R,C,D3TXE,D3TFXY)

C FOR MIXED DERIVATIVES OF U AND V SET BE1. AND CE 0.
C FOR MIXED DERIVATIVES OF U AND FNCBR SET BE1. AND CE 1.
C FOR MIXED DERIVATIVES OF V AND FNCBR SET BE0. AND CE 1.

00101 DIMENSION Y(2)

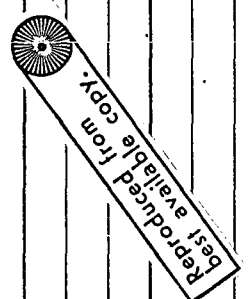
00103 COMMON /BLKI/THETAR,THETAS,FM,FV,FNCBR,FNC,V,DNCOT1,DFNX,D2NDLL,
DFMX,DFY,D2LNC,D2VNC,D2MNC,D2MLL,Y1,Y2,DE4DT8,E3,DE1DL/

00104 1 BLK0/U,D3M2LN,D3M2NL,A1,A2,A3,A4,A5,A6,EB
00104 14 = Y2
00105 15 = Y2
00106 16 = FNC

```

00107 17* 01F0Y = U*(0213XY-021FX1)+9*(1180Y-01F0Y)
00110 18* 02A1XY = 2*0A12X*0A10Y/A1-A1**2*(021FX1-021FX0)
00111 19* 0216XY = 6*F1C3R*0180X*0180Y+6*Y(2)*FNC9R*0218XY+C*6*Y(2)*0180X
00112 20* 0342XY = 010Y*0342Y
00113 21* 0MCDXY = 6*F1C3R*Y(2)*0180X*0180Y+3*FNC9R*(Y(2)**2)*0218XY+
00114 22* C*3*(Y(2)**2)*0180X
00115 23* 0342XY = 010Y*0342Y+0MCDXY*0342Y
00116 24* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX+02MCDX*0MCDX
00117 25* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00118 26* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00119 27* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00120 28* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00121 29* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00122 30* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00123 31* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00124 32* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00125 33* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00126 34* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00127 35* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00128 36* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00129 37* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00130 38* 02E2XY = 005TA(Z)*0MCDX*0180Y+0218XY+0342XY*0MCDX
00131 39* RETURN
00132 40* END

```



END OF COMPILATION: NO DIAGNOSTICS.

02 FOR IS DERV
FOR 59A-07/27/72-17:44:54 (10)

SUBROUTINE DERV ENTRY POINT 000604

STORAGE USED: CODE(1) 000721; DATA(0) 000130; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 ELKI 000024
0004 ELKD 000012

EXTERNAL REFERENCES (R-LOCAL, NAME)

0005 ETA
0006 DELTA
0007 DDELTA
0010 DDDELTA
0011 MERR35

STORAGE ASSIGNMENT (R-LOCAL, TYPE, RELATIVE LOCATION, TIME)

0004 R 000003 A1 0004 R 000004 A2 0004 R 000005 A3 0004 R 000006 A4 0004 R 000007 A5
0004 R 000010 A6 0004 R 000011 A7 0004 R 000012 A8 0004 R 000013 A9 0004 R 000014 A10
0004 R 000015 A11 0004 R 000016 A12 0004 R 000017 A13 0004 R 000018 A14 0004 R 000019 A15
0004 R 000020 A16 0004 R 000021 A17 0004 R 000022 A18 0004 R 000023 A19 0004 R 000024 A20
0004 R 000025 A21 0004 R 000026 A22 0004 R 000027 A23 0004 R 000028 A24 0004 R 000029 A25
0004 R 000030 A26 0004 R 000031 A27 0004 R 000032 A28 0004 R 000033 A29 0004 R 000034 A30
0004 R 000035 A31 0004 R 000036 A32 0004 R 000037 A33 0004 R 000038 A34 0004 R 000039 A35
0004 R 000040 A36 0004 R 000041 A37 0004 R 000042 A38 0004 R 000043 A39 0004 R 000044 A40
0004 R 000045 A41 0004 R 000046 A42 0004 R 000047 A43 0004 R 000048 A44 0004 R 000049 A45
0004 R 000050 A46 0004 R 000051 A47 0004 R 000052 A48 0004 R 000053 A49 0004 R 000054 A50
0004 R 000055 A51 0004 R 000056 A52 0004 R 000057 A53 0004 R 000058 A54 0004 R 000059 A55
0004 R 000060 A56 0004 R 000061 A57 0004 R 000062 A58 0004 R 000063 A59 0004 R 000064 A60
0004 R 000065 A61 0004 R 000066 A62 0004 R 000067 A63 0004 R 000068 A64 0004 R 000069 A65
0004 R 000070 A66 0004 R 000071 A67 0004 R 000072 A68 0004 R 000073 A69 0004 R 000074 A70
0004 R 000075 A71 0004 R 000076 A72 0004 R 000077 A73 0004 R 000078 A74 0004 R 000079 A75
0004 R 000080 A76 0004 R 000081 A77 0004 R 000082 A78 0004 R 000083 A79 0004 R 000084 A80
0004 R 000085 A81 0004 R 000086 A82 0004 R 000087 A83 0004 R 000088 A84 0004 R 000089 A85
0004 R 000090 A86 0004 R 000091 A87 0004 R 000092 A88 0004 R 000093 A89 0004 R 000094 A90
0004 R 000095 A91 0004 R 000096 A92 0004 R 000097 A93 0004 R 000098 A94 0004 R 000099 A95
0004 R 000100 A96 0004 R 000101 A97 0004 R 000102 A98 0004 R 000103 A99 0004 R 000104 A100

00101 1* SUBROUTINE DERV(Y3,Y4,Y5,Y6,DL,DU,D2L,DU1,DY3,DY4,DY5,DY6,B,C,
00101 2* DMC,DA1,DA2,DA3,DA4,DA5,DA6,DA7,DA8,DA9,DA10,DA11,DA12,DA13,DA14,DA15,DA16,DA17,DA18,DA19,DA20,
00101 3* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 4* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 5* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 6* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 7* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 8* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 9* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 10* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 11* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 12* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 13* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 14* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 15* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,
00101 16* D2L,DU1,DU2,DU3,DU4,DU5,DU6,DU7,DU8,DU9,DU10,DU11,DU12,DU13,DU14,DU15,DU16,DU17,DU18,DU19,DU20,

FOR FIRST AND SECOND DERIVATIVES OF U SET C=1 AND B=0
FOR FIRST AND SECOND DERIVATIVES OF V SET C=0 AND B=0
FOR FIRST AND SECOND DERIVATIVES OF FNCBR SET C=U AND B=1
DIMENSION Y(20),DY(20)
COMMON /BLKI/THETAB,THETAS,FM,FN,FNCBR,FNC,V,DNCOT1,DFNX,D2NDLL,
DFMY,DFM,D2MLNC,D2MLN,DA1,DA2,DA3,DA4,DA5,DA6,EB,
BLKDU,DM2LN,DM2NL,A1,A2,A3,A4,A5,A6,EB
Y(1) = Y1
Y(2) = Y2

00107	17*	Y(3)	= Y3
00110	18*	Y(4)	= Y4
00111	19*	Y(5)	= Y5
00112	20*	Y(6)	= Y6
00113	21*	Z	= FNC
00114	22*	F3	= FM*ETA(Z)+FN
00115	23*	F1	= 1.7*(Y(1)-Y(P1))
00116	24*	F3	= FM*ETA(Z)+ETA(Z)*DFM
00117	25*	F3	= 3*Y(2)**2*F1*CRP
00120	26*	A2	= A6*A5/53
00121	27*	A3	= 4*Y(2)**3/(Y(2)**4)-THEIAS**4
00122	28*	A4	= A1+A2+A3
00123	29*	DA1DU	= -A1**2*(Y(3)-Y(4))
00124	30*	DECU	= A6*Y(4)+9*Y(2)**3
00125	31*	DETA(7)*DNCU	= DETA(7)*DNCU
00126	32*	DECU	= DECU+DLU+DFH+DNCU
00127	33*	DEMCU	= DEMLNC+DLU+D2*DNCG+DNCU
00130	34*	DEU	= DETA(7)*DNCU
00131	35*	DA5DU	= FM*DEPU+ETA(7)*DNDU+ETA(7)*D2*DNCG+DFM*DEU
00132	36*	DA6DU	= 6*Y(2)*FNCBR*Y(4)+3*3*Y(2)**2
00133	37*	A7	= A6*DA5DU+A5*DA6DU
00134	38*	DECU	= DECU+DLU
00135	39*	DECU	= FM*DEU+ETA(7)*DNDU+DNDU
00136	40*	DA2DU	= (A7-A2*DECU)/ZB
00137	41*	DA3DU	= A3*Y(4)+3*(Y(2)-A3)
00140	42*	DA4DU	= D/1DU+DA2DU+DA3DU
00141	43*	F(4)	= -C/A4+1/A4**2*A4DU
00142	44*	DA1DU	= -A1**2*(Y(5)-Y(6))-2*A1*DA1DU*(Y(3)-Y(4))
00143	45*	DEMCU	= A6*Y(5)+DA6DU*Y(4)+8*3*Y(4)*Y(2)**2
00144	46*	DEPU	= DETA(7)*D2*DNCG+DNCU**2+DDETA(Z)
00145	47*	DECU	= FM*DECU+DLU+DLU*(D2*FNC+DNCU)
00146	48*	DEMCU	= DEMLNC+DLU+DLU*(D2*FNC+DNCU)
00146	49*	DEMCU	= DEMLNC+DLU+DLU*(D2*FNC+DNCU)
00146	50*	DEMCU	= DEMLNC+DLU+DLU*(D2*FNC+DNCU)
00147	51*	DECU	= DETA(7)*D2*DNCG+DETA(7)*DNCU**2
00150	52*	DA5DU	= FM*DEPU+2*DEPU*DMGU+ETA(Z)*D2*DNCG+ETA(Z)*D3*DNCG
00150	53*	DA6DU	= +2*DEU+D2*DNCG+DFH+D2*DEU
00151	54*	DA7DU	= 6*Y(2)*FNCBR*Y(6)+6*FNCBR*Y(4)**2+B*12*Y(2)*Y(4)
00152	55*	DA8DU	= A6*DA5DU+DA5DU*DA6DU+3*DA6DU+DA6DU+DA6DU
00153	56*	DA9DU	= DECU+DLU+DLU**2
00154	57*	DA10DU	= FM*DEPU+2*DEPU*DMGU+ETA(Z)*D2*DNCG+D2*DNCG
00155	58*	DA2DU	= (DA7DU-A2*DECU)-2*DECU*DA2DU/ZB
00156	59*	DA3DU	= A3*(Y(2)-A3)*Y(6)+Y(4)*(-3*Y(2)**2*Y(4)-DA3DU)
00156	60*	DA4DU	= (1/13)*DA3DU**2
00157	61*	DA5DU	= DA1DU+DA2DU+DA3DU
00158	62*	DA6DU	= -2/34*DY(4)+DA9DU+ZA4**2*DA4DU
00161	63*	Y(3)	= U*(Y(4)-Y(3))*Y(2)-Y(1)*C
00162	64*	Y(5)	= U*(Y(6)-Y(5))+2*(Y(4)-Y(3))*C
00163	65*	Y3	= DY(3)
00164	66*	Y4	= DY(4)
00165	67*	Y5	= DY(5)
00166	68*	Y6	= DY(6)
00167	69*	RETURN	
00170	70*	END	

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS INITIAL
FOR S9A-07/27/72-17:44:59 (10)

SUBROUTINE INITIAL ENTRY POINT 000470

STORAGE USED: CODE(1) 000522; DATA(0) 000123; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 BLKI 00002

EXTERNAL REFERENCES (BLOCK, NAME)

0004 ETA
0005 DELTA
0006 DDELTA
0007 MER33

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R 000037 A1	0000 R 000040 A2	0000 R 000041 A3	0000 R 000053 R1	0000 R 000054 R2
0006 R 000000 DDEIA	0000 R 000051 DDEIDU	0000 R 000000 DELTA	0000 R 000046 DETAU	0003 R 000023 DE1DI
0000 R 000032 DE1DN	0000 R 000027 DE1DTR	0000 R 000047 DE1DU	0000 R 000030 DE2DTR	0000 R 000014 DE2DRI
0000 R 000031 DE3DI	0000 R 000035 DE3DU	0000 R 000021 DE4DTR	0000 R 000033 DE4DU	0000 R 000044 DECNFIJ
0003 R 000013 DF4	0000 R 000045 DF4DU	0000 R 000012 DFMX	0000 R 000043 DFN7UJ	0003 R 000010 DFNX
0003 R 000007 DNCDT	0000 R 000061 D1	0000 R 000062 D2	0000 R 000065 D2E1CR	0000 R 000060 D2E1LU
0000 R 000055 D2E1T	0000 R 000036 D2E2TU	0000 R 000042 D2E3TU	0000 R 000066 D2E4CR	0000 R 000071 D2E4UJ
0003 R 000016 D2FML	0000 R 000056 D2M0LU	0000 R 000015 D2M0NC	0003 R 000014 D2MLNC	0000 R 000052 D2M0NCU
0000 R 000067 D2M0CN	0000 R 000050 D24CTU	0000 R 000011 D2NDLL	0000 R 000057 D2NDLU	0000 R 000065 D3
0000 R 000064 D4	0004 R 000000 ET4	0000 R 000025 F1	0000 R 000026 F2	0003 R 000022 F3
0003 R 000002 F4	0003 R 000003 F4	0000 R 000005 F4C	0003 R 000004 F4C8R	0000 D00100 INQJF4
0000 R 000070 TERMJ	0003 R 000000 THETAB	0000 R 000001 THETAS	0003 R 000006 V	0000 R 000000 Y
0003 R 000017 Y1	0003 R 000020 Y2	0000 R 000024 Z		

SUBROUTINE INITIAL(D0LDU,D2LDUU,Y4,Y5,Y6,B,C,D2E4TU,D2E4LU)

INITIAL CONDITIONS

FOR FIRST AND SECOND DERIVATIVES OF U SET C=1 AND B=0
FOR FIRST AND SECOND DERIVATIVES OF V SET C=0 AND B=0
FOR FIRST AND SECOND DERIVATIVES OF F4C8R SET C=1 AND B=1

DIMENSION Y(20)

COMMON /BLKI/THETAB,THETAS,F4,F4C,F4C8R,F4C,D2E4LU,Y1,Y2,D2E4DTR,E3,DE1DL,
DF4,DF4C,D2MLNC,D2M0NC,D2E4LU,Y1,Y2,D2E4DTR,E3,DE1DL

Y(1)	= Y1
Y(2)	= Y2
Z	= F4C
E1	= F4C*Y(2)+F4
E2	= THETAB**4-THETAS**4

```

00112 17*      = E2/(1-THETAB)
00113 18*      = 0.
00114 19*      = DMCOT1*(DFM*ETA(Z)+FM*DETA(Z))
00115 20*      = 4*(THETAP**3)
00116 21*      = E3*(DE2DIB+E3)/E2
00117 22*      = E1*DE3DIB+E3*DE1DIB
00118 23*      = ETA(Z)*DFVK+DFNK
00119 24*      = ETA(Z)*DFM*DEIA(Z)*FM
00120 25*      = E3*DE1DL*DLDU+R*E3*DE1DNC*THETAB**3
00121 26*      = -(C1/V**2*DE4DU)/DE4DIB
00122 27*      = 0.
00123 28*      = DE2DIB*(4)
00124 29*      = E3*(E3*Y(4)+DE2DU)/E2
00125 30*      = 12*Y(4)*(THETAB**2)
00126 31*      = E3*(DE2TU+DF3DU)/E2
00127 32*      = DE2DIB+E3
00128 33*      = -E3*DE2DU/(E3**2)+DE3DU/E2
00129 34*      = AL*P**3
00130 35*      = DFVK*DLDU
00131 36*      = DMCOT1*Y(4)+B*Y(2)**3
00132 37*      = DFVK*DLDU+DFM*DFCNDU
00133 38*      = DEL(Z)*DFCNDU
00134 39*      = FM*DEIADU+ETA(Z)*DFM*DFCNDU
00135 40*      = 6*E3*DE3Y(2)*Y(4)+B**2*Y(2)**2
00136 41*      = DEIADU*(Z)*DFCNDU
00137 42*      = DE2MLNC*DLDU+DE2M*DFCNDU
00138 43*      = DFVK*DEIADU+ETA(Z)*DE2V*CU+FM*DEIADU*DETA(Z)*DFCNDU
00139 44*      = DEIADU*DE2M*DLDU/RNC911
00140 45*      = DMCOT1*Y(4)+B2
00141 46*      = DE2MLL*DLDU+DE2MLNC*DFCNDU
00142 47*      = DE2MLL*DLDU
00143 48*      = ETA(Z)*DE2V*DLDU+DEIADU*DFM*DE2NDLU
00144 49*      = E3*DE2E1LU+DE1DL*DE3DU
00145 50*      = DEL(Z)*DE2DU*DFM
00146 51*      = ETA(Z)*DFCNDU
00147 52*      = DEIADU*(Z)*FM*DFCNDU
00148 53*      = DEIADU*(Z)*DFCNDU
00149 54*      = DE1DL*DLDU+DE2M*DLDU
00150 55*      = DE3DU*DE1DNC+E3*DE2E1C
00151 56*      = 3*Y(4)*Y(2)**2
00152 57*      = 9*(E3*DE1DNC+DE2M*DLDU+DE2M*DLDU)*Y(2)**3+DE2E4CB
00153 58*      = E3*DE1DL*DLDU+DE2E4LU+TERMN
00154 59*      = E1*DE2E3TU+DE3DU*DE1D**3+DE2E1TU+DE1DIB*DE3DU
00155 60*      = -(Y(4)+DE2E4TU+DE2E4DU)*((C-1)/V**3)/DE4DIB
00156 61*      = Y(3)
00157 62*      = Y(4)
00158 63*      = Y(5)
00159 64*      = Y(6)
00160 65*      = RETURN
00161 66*      = END

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END OF COMPILATION: NO DIAGNOSTICS.

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02 FOR IS INTMIX
FOR S9A-07/27/72-17:45:03 (1,0)

SUBROUTINE INTMIX ENTRY POINT 000024

STORAGE USED: CODE(1) (000321 DATA(0) 000007) BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 BLKI 000024

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0003 R	000023	DEIDL	0000 R	000000	DE4DL	0003 R	000021	DE4DT8	0000 R	000001	DE4DX	0003	000013	DFM
0003	000012	DFMX	0003	000010	DFMX	0003	000007	DNCDT1	0003	000016	D2FMLL	0003	000015	D2MDMC
0003	000014	D2MLNC	0003	000011	D2MDLL	0003 R	000022	E3	0003	000002	F4	0003	000003	FN
0003	000005	FNC	0003	000004	FNCRR	0000	000002	INJPS	0003	000000	THETAB	0003	000001	THETAS
0003	000006	Y	0003	000017	Y1	0003	000020	Y2						

00101 1* SUBROUTINE INTMIX(D2E4TY,DT8DX,DL0X,D2E4LY,D2L0XY,D2Y8XY,D2TFXY)

00101 2* C INITIAL MIXED DERIVATIVES

00101 3* C

00101 4* C

00103 5* COMMON /BLKI/THETAS,FM,FNF,NCBR,FNC,V,NCOTI,DFMX,D2MDLL,
DFM(*,DFM,D2MLNC,D2MDMC,D2FMLL,Y1,Y2,DE4DT8,E3,DEIDL

00104 6* D2TFXY = 0.

00105 7* DE4DL = E3*DE4DL

00106 8* D243XY = D2E4LY*DL0X+DE4DL*D2L0XY

00107 9* D218XY = -(DE43XY+DT8DX*D2E4TY)/DE4DT8

00110 11* RETURN

00111 12* END

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS FMINV
FOR S9A-07/27/72-17:45:07 (r.0)

SUBROUTINE FMINV ENTRY POINT 000254

STORAGE USED: CODE(1) 000306J DATA(0) 001260J BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000346	1056	0001	000151	111L	0001	000051	111G	0001	000071	117S	0001	000104	123G
0001	000125	133G	0001	000130	137G	0001	000172	150G	0001	000175	154S	0001	000227	144G
0001	000212	20L	0000	R	0001214	AA	0000	R	0000	I	001212	I	0000	001224
0000	I	001215	II	0000	I	001220	12	0000	I	001213	J	0000	R	000000
														XMAT

LINE	CODE	TEXT	LINE	CODE	TEXT
00101	1*	SUBROUTINE FMINV (I,X,N,M)	1		
00101	2*	C			
00101	3*	C			
00101	4*	C			
00103	5*	DIMENSION A(N,N),X(N),XMAT(25,5)	2		
00104	6*	DO 1 I=1,N	3		
00107	7*	XMAT(I,N) = X(I)	4		
00110	8*	DO 1 J=1,N	5		
00113	9*	XMAT(I,J) = A(I,J)	6		
00116	10*	DO 20 I=1,N	7		
00121	11*	AA = XMAT(I,I)	8		
00122	12*	DO 5 J=1,M	9		
00125	13*	XMAT(I,J) = XMAT(I,J)/AA	10		
00127	14*	IF (I.EQ.N) GO TO 11	11		
00131	15*	I = I + 1	12		
00132	16*	DO 10 K=1,I+1	13		
00135	17*	B = XMAT(K,I)	14		
00136	18*	DO 10 J=1,M	15		
00141	19*	XMAT(K,J) = XMAT(K,J) - XMAT(I,J) * B	16		
00144	20*	IF (I.EQ.N) GO TO 20	17		
00147	21*	I = I + 1	18		
00152	22*	DO 15 K=12,N	19		
00153	23*	B = XMAT(K,I)	20		
00156	24*	DO 15 J=1,M	21		
00161	25*	XMAT(K,J) = XMAT(K,J) - XMAT(I,J) * B	22		
00163	26*	CONTINUE	23		
00163	27*	DO 25 I=1,N	24		
00166	28*	X(I) = XMAT(I,M)	25		
00170	29*	RETURN	26		
00171	30*	END			

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS ETA
FOR SPA-072772-17:45:11 (,0)

FUNCTION ETA ENTRY POINT 000036

STORAGE USED: CODE(1) 000044; DATA(0) 000022; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 POLY
0004 EXP
0005 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000015 1L 0000 R 000001 A 0000 R 000010 R 0000 R 000000 ETA 0000 000014 INJP5
0003 R 000000 POLY 1

00101 1* FUNCTION ET*(X)
00101 2* C
00101 3* C FIN EFFECTIVENESS OF THE UNOBSERVED FIN
00101 4* C
00101 5* C DIMENSION A(7), B(2)
00104 6* DATA A(1)*A(2)*A(3)*A(4)*A(5)*A(6)*A(7)/0.10E+01, -0.1163143E+01,
00104 7* 1 0.1428335E+01, -0.1267550E+01, 0.6328223E+00, -0.1627067E+00,
00104 8* 2 0.1654223E-01/ B(1)*A(2)/0.6866095E+00, -0.2297718E+00/
00116 9* IF(X*SI,2,5) GO TO 1
00120 10* ETA = POLY(7,A,X)
00121 11* RETURN
00122 12* 1 ETA = B(1)*EXP(B(2)*X)
00123 13* RETURN
00124 14* END

END OF COMPILATION: NO DIAGNOSTICS.

92 9FOR.15 DETA
FOR S9A-07/27/72-17:45:15 (.0)

FUNCTION DETA ENTRY POINT 000036

STORAGE USED: CODE(1) 000044; DATA(0) 000021; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 POLY
0004 EXP
0005 XERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000016 JL 0000 R 000001 A 0000 R 000007 B 0000 R 000000 DETA 0000 000013 INJPF
0003 R 000000 POL

00101 1* FUNCTION DETA(X)

00101 2* C

00101 3* C DETA/DNC

00101 4* C

00101 5* DIMENSION A(6), B(2)

00104 6* DATA A(1),A(2),A(3),A(4),A(5),A(6)/-0.1163143E+01, 0.2957672E+01,

00104 7* 1 -0.3802650E+01, 0.253008E+01, -0.8135335E+00, 0.9925338E-01/

00104 8* 2 R(1),B(2)/-0.1577635E+00, -0.2297718E+00/

00115 9* IF(X.GT.2.5) GO TO 1

00117 10* DETA = POLY(6,A,X)

00120 11* RETURN

00121 12* 1 DETA = B(1)*EXP(3(2)*X)

00122 13* RETURN

00123 14* E 10

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS DDETA
FOR 59A-07/27/72-17:45:23 (10)

FUNCTION DDETA ENTRY POINT 000036

STORAGE USED: CODE(1) 000044J DATA(0) 000020I BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 POLY
0004 EXP
0005 HERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000016 IL 0000 R 000001 A 0000 R 000006 B 0000 R 000000 DDETA 0000 00012 INJPS
0003 R 000000 POLY

00101 1* FUNCTION DDETA(X)
00101 2* C
00101 3* C DDETA/22NC
00101 4* C
00103 5* DIMENSION A(5), B(2)
00104 6* DATA A(1),A(2),A(3),A(4),A(5)/0.2957672E+01, -0.7605300E+01,
00104 7* 1 0.7590257E+01, -0.3254134E+01, 0.4962669E+00/ B(1),B(2)/
00104 8* 2 0.3624960E-01, -0.2297714E+00/
00116 9* IF(X.GT.2.5) GO TO 1
00116 10* DDETA = POLY(5,A,X)
00117 11* RETURN
00120 12* 1 DDETA = B(1)*EXP(B(2)*X)
00121 13* RETURN
00122 14* END

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS DDETA
FOR 59A-07/2772-17:45:35 (.0)

FUNCTION DDETA ENTRY POINT 000036

STORAGE USED: CODE(1) 000044; DATA(0) 000017; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 POLY
0004 EXP
0005 MERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000016 1L 0000 R 000001 A 0000 R 000005 R 0000 R 000000 DDETA 0000 000011 INJP*

0003 R 000000 POLY

00101	1*	FUNCTION	DDETA(X)
00101	2*	C	
00101	3*	C	DJETA/D3NC
00101	4*	C	
00103	5*	DIMENSION	A(4), J(2)
00104	6*	DATA	A(1),A(2),A(3),A(4)/-0.7405300E+01.0.1518053E+02,
00104	7*		1-0.2762402E+01.0.1985068E+01/
00104	8*		2 B(1),B(2)/-0.8329136E-02,-0.297718E+00/
00113	9*	IF(X.GI.2.5) GO TO 1	
00115	10*	DDETA	= POLY(4,A,X)
00116	11*	RETURN	
00117	12*	DDETA	= B(1)*EXP(R(2)*X)
00120	13*	RETURN	
00121	14*	END	

END OF COMPILATION: NO DIAGNOSTICS.

2 FOR 15 POLY
FOR 59A-07/27/72-17145:32 (1,0)

FUNCTION POLY ENTRY POINT 000036

STORAGE USED: CODE(1) 000044: DATA(0) 000015: BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000012 1076 0000 000003 INJPS 0000 I 000002 K 0000 I 000001 L 0000 R 000000 POLY

```
00101 1* FUNCTION POLY(N,A,X)
00101 2* C
00101 3* C POLYNOMIAL EVALUATION Y = A(N)*X*(N-1)+X**2*A(N-2)+...
00101 4* C
00103 5* DIMENSION A(N)
00104 6* POLY = 0.
00105 7* L = N
00106 8* DO I K=1,N
00111 9* POLY = POLY*X+A(I)
00112 10* L = L-1
00114 11* RETURN
00115 12* END
```

END OF COMPILATION: NO DIAGNOSTICS.

0XGT
MAP_023-07/27-17:45

ADDRESS LIMITS 00100 020432 040000 047526
STARTING ADDRESS 047366

WORDS DECIMAL 7 163 IBANK 3927 DBANK

SEGMENT IAIJ 001000 020432 040000 047526

NSWTS/FOR	1	001000	001021				
NRWTS/FOR	1	001022	001044				
NRWTS/FOR	1	001045	001124	2	040000	040011	
NWTS/FOR	1	001125	001326	2	040012	040031	
NFCHS/FOR	1	001327	001617	2	040032	040067	
NBCLB/FOR	1	001620	001752	2	040070	040125	
NFVTS/FOR	1	001753	001775				
NCVTS/FOR	1	001776	002222	2	040126	040215	
NCLOS/FOR	1	002223	002371	2	040216	040247	
NWTKS/FOR	1	002372	002513				
NBSHS/FOR	1	002514	002550				
NUPOAS/FOR	1	002551	002603				
N3FOR/FOR				2	040250	042451	
N1M1B/FOR	1	002604	003014	2	042452	042463	
N1M2B/FOR	1	003015	003657	2	042464	042503	
NOVTS/FOR	1	003660	004173	2	042504	042507	
NOU13/FOR	1	004174	005162	2	042510	042534	
NEVTS/FOR	1	005163	005041	2	042535	042511	
NIGERB/FOR	1	006042	006214	2	042612	042716	
NECHK/FOR	1	006215	007076	2	042717	043055	
				4	043056	043127	
				2	043130	043166	
NI3B/FOR				2	043167	043167	
ERUS/MISC	1	007077	007141	2	043170	043220	
NIQUEB/FOR	1	007142	007626	0	043221	043500	
TIR3/TECH				2	043501	043510	
NEAPB/FOR	1	007627	007714	2	043511	043544	
NIERS/FOR	1	007715	007775	2			
NO3UF3/FOR	1	007777	010043	0	043645	043672	
ASINCS3/FOR	1	010044	010260	2	043673	043704	
SRPTS/FOR	1	010261	010321	2	043705	043725	
EXPS/FOR	1	010322	010411	2	043726	044071	
NIERS/FOR	1	010412	010736	2	044072	044103	
BLKB (COMMON BLOCK)					044104	044106	
VAB (COMMON BLOCK)					044107	044113	
MCI (COMMON BLOCK)					044114	044115	
BLKB (COMMON BLOCK)					044116	044127	
BLKD (COMMON BLOCK)					044130	044153	
BLKI (COMMON BLOCK)							

62	BLANK\$COMMON (COMMON BLOCK)	1	010737	011002	0	044154	044170
	POLY	2			0	BLANK\$COMMON	
	DDDETA	1	011003	011046	0	044171	044207
	DDETA	2			0	BLANK\$COMMON	
	DDETA	1	011047	011112	0	044210	044227
	DDETA	2			0	BLANK\$COMMON	
	DDETA	1	011113	011156	0	044230	044250
	DDETA	2			0	BLANK\$COMMON	
	EIA	1	011157	011222	0	044251	044272
	EIA	2			0	BLANK\$COMMON	
	FMMW	1	011223	011530	0	044273	045552
	FMMW	2			0	BLANK\$COMMON	
	INIMIX	1	011531	011562	0	045553	045561
	INIMIX	2			0	BLANK\$COMMON	
	INITIAL	3	011563	012304	0	045562	045704
	INITIAL	2			0	BLANK\$COMMON	
	DERV	1	012305	013225	0	045705	046034
	DERV	2			0	BLANK\$COMMON	
	DERV	3	013226	013701	0	046035	046140
	DERV	4			0	BLANK\$COMMON	
	MIXDER	1	013702	013745	0	046141	046153
	MIXDER	2			0	BLANK\$COMMON	
	NCDERV	1	013746	014251	0	046154	046241
	NCDERV	2			0	BLANK\$COMMON	
	NDERV	1	014252	014341	0	046242	046256
	NDERV	2			0	BLANK\$COMMON	
	REST	1	014342	014461	0	046257	046301
	REST	2			0	BLANK\$COMMON	
	RESBND	1	014462	014713	0	046302	046354
	RESBND	2			0	BLANK\$COMMON	
	BNDEND	1	014714	015324	0	046355	046441
	BNDEND	2			0	BLANK\$COMMON	
	SCMTL	1	015325	015520	0	046442	046455
	SCMTL	2			0	BLANK\$COMMON	
	SDRV	3	MCT		4	VAB	
	SDRV	4	BLKI		4	VAB	
	SDRV	1	015521	016325	0	046456	046543
	SDRV	2			0	BLANK\$COMMON	
	SDRV	3	BLKI		4	RLKD	
	SDRV	5	BLKR		4	RLKD	
	RAS	1	016326	017365	0	046544	046627
	RAS	2			0	BLANK\$COMMON	
	MAIN	1	017366	020432	0	046630	047526
	MAIN	2			0	BLANK\$COMMON	
	MAIN	3	BLKI		4	RLKD	
	MAIN	5	MCT		4	RLKR	
	MAIN	7	BLKB		6	RLKR	

SYSS*RLIBS. LEVEL 63
END OF COLLECTION - TIME 2.084 SECONDS

APPENDIX C

COMPUTER CODE FOR MINIMUM

MASS OPTIMIZATION

DFOR, IS MAIN
FOR S9A=072772=19137:17 (10)

MAIN PROGRAM

STORAGE USED: CODE(1) 001035; DATA(0) 000776; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 BLKI 000324
0004 BLKD 000012
0005 MCT 000005
0006 BLKR 000012

EXTERNAL REFERENCES (BLOCK, NAME)

0007 SORV
0010 SCNTL
0011 CONST
0012 NDERV
0013 ETA
0014 DEYA
0015 NCDERV
0016 MDER
0017 INITIAL
0020 INTVIX
0021 RKS
0022 FWINV
0023 BNDEND
0024 NINTR\$
0025 NRNL\$
0026 NWDU\$
0027 NI02\$
0030 SORT
0031 ASIN
0032 NI01\$
0033 NSTOP\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000002 1L 0001 000122 100L 0001 000273 105L 0001 000311 108L 0001 000314 109L
0001 000321 110L 0000 000466 200F 0000 000526 2010F 0000 000541 2040F 0000 000557 205F
0000 000733 2095F 0000 000712 2060F 0001 001015 2070L 0001 001023 2090L
0000 000605 230F 0001 000566 210F 0000 000573 215F 0000 000673 221F
0001 000462 2336 0000 000621 240F 0000 000636 250F 0001 001007 300L
0001 001031 3000L 0000 R 000703 3466 0001 000725 3556 0001 000117 90L
0000 000534 900F 0000 R 000050 A 0000 R 000355 ALPHA 0000 R 000372 AY 0000 R 000372 AY
0004 000003 A1 0004 000004 A2 0004 000005 A3 0004 000006 A4 0004 000007 A5
0004 000010 A6 0000 R 000373 BY 0000 R 000356 DA 0014 R 000000 DETA 0000 R 000377 DETZ
0003 000023 DE1DL 0003 000021 DE4DTB 0003 R 000013 DFM 0003 R 000012 DFMX 0003 R 000010 DFNX
0006 R 000006 DLNCH 0006 R 000001 DLDV 0006 R 000002 DLDV 0005 R 000000 DLMY 0000 R 000120 DLY
0003 R 000007 DNCY1 0000 R 000357 DR 0000 R 000414 DX 0005 R 000003 DXRT 0000 R 000024 DY
0000 R 000240 DYST 0000 R 000400 DYY 0000 R 000403 DZC02Y 0000 R 000404 DZCTNB 0000 R 000412 DZE4LN
0000 R 000406 DZE4LU 0000 R 000410 DZE4LV 0000 R 000411 DZE4TN 0000 R 000405 DZE4TU 0000 R 000407 DZE4TV

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0003 R 000016 D2FILL 0006 R 000003 D2LDUU 0006 R 000004 D2LDVV 0006 R 000005 D2LDVW 0006 R 000007 D2LNCB
0006 R 000010 D2LVNB 0006 R 000011 D2LVNC 0003 R 000014 D2MLNC 0003 R 000011 D2NDLL
0004 R 000001 D3M2LN 0004 R 000002 D3M2NL 0004 000011 EB 0013 R 000000 ETA 0000 R 000375 ETY
0000 R 000374 ETY 0003 000022 E3 0003 R 000002 FM 0003 R 000003 FN 0003 R 000005 FNC
0000 R 000004 FNC:R 0000 I 000415 I 0000 I 000420 IBKP 0005 I 000001 ICNT 0000 I 000422 IERR
0000 I 000416 IFVD 0000 000426 INPUT 0000 I 000424 LCNT 0005 000004 LSTEP 0000 I 000423 LSTEP
0000 I 000417 N 0000 I 000367 NCT 0000 I 000360 NIT 0000 I 000421 NTRY 0000 R 000144 PD
0000 R 000354 PHI2 0000 R 000074 R 0000 R 000365 RH00 0006 R 000000 RLAM 0010 R 000000 SCNTL
0000 R 000170 SD 0007 R 000000 SDRV 0000 R 000364 TFLEX 0003 R 000000 THETAB 0000 R 000402 THETAF
0003 R 000001 THETAS 0000 R 000366 TH4 0000 R 000353 TOTMAS 0000 R 000370 T2 0000 R 000371 T3
0004 R 000000 U 0003 R 000006 V 0000 R 000334 XM 0005 R 000002 XWRT 0000 R 000000 Y
0000 R 000214 YS 0000 R 000310 YSIMP 0000 R 000264 YST 0000 R 000376 YY 0003 R 000017 YI
0003 R 000020 Y2 0000 R 000425 Z5 0000 R 000401 ZZ 0000 R 000413 ZZZ 0000 R 000361 Z1
0000 R 000362 Z2 0000 R 000363 Z3

```

```

00100 1* C
00100 2* C
00100 3* C
00100 4* C
00100 5* C
00101 6*
00103 7*
00103 8*
00104 9*
00104 10*
00104 11*
00104 12*
00104 13*
00104 14*
00105 15*
00105 16* C
00106 17*
00107 18*
00110 19*
00111 20*
00114 21*
00115 22*
00116 23*
00117 24*
00120 25*
00121 26*
00122 27*
00123 28*
00124 29*
00124 30*
00125 31*
00125 32*
00127 33*
00141 34*
00141 35*
00141 36*
00141 37*
00141 38*
00141 39*

```

RADIATOR SYSTEMS OPTIMIZATION FOR MINIMUM MASS

```

EXTERNAL SDRV:SCNTL
DIMENSION Y(20),DY(20),A(20),R(20),DLY(20),PD(20),SD(20),
YS(20),YST(20),YST(20),YSIP(20),XN(3),AM(3,4),
COMMON /BLKI/THETAS,THETAS,FM,FN,FNCBR,FNC-V,DNCOT1,DFNX,D2NDLL,
DFMX,DFM,D2MLNC,D2MNC,D2FMMLTY1,Y2,DE4DTB,E3,DE1DL/
BLKD/U,D3M2LN,D3M2NL,A1,A2,A3,A4,A5,A6,EB
/ACT/DLNT,ICNT,XWRT,XWRT,LSTEP
/BLKR/RLAM,DLDU,DLDV,D2LDUU,D2LDUV,D2LDVV,D2LNCB,
D2LNCB,D2LVNB,D2LVNB
NAMELIST /INPUT/ THETAS,U,V,FNCBR,TOTMAS,PHI2,ALPHA,DXWRT,DA,DR
FFS(X) = (SQRT(X*(X+2.0))+ASIN(1.0/(X+1.0)))-1.570796)/X
FFN(X,Y) = 1.0-Y*(0.1468XY-0.286677X
UFFN(X,Y) = (-0.2920XY+0.028661/X
I READ(5,INPUT,END=3000)
= 1
= U
= V
= FNCBR
X4(1) = 0.
X4(2) = 0.
X4(3) = 0.
TFLEX = 2.0
50 CALL CONST(TOTMAS,PHI2,ALPHA,U,V,FNCBR,RLAM,DLDU,DLDV,D2LNCB,
D2LDUU,D2LDUV,D2LDU:B,D2LDVV,D2LVNB,D2LNCB)
CALL NDERV(RLAM,FN,DFNX,D2NDLL)
RHDD = RLAM
WRITE(6,2000) THETAS,U,V,FNCBR,TOTMAS,PHI2,ALPHA,RLAM
2000 FORMAT (PHI,10X,10HTHETA-S = F20.8/
11X,10H U = F20.6/
2 11X,10H V = F20.6/
3 11X,10H FNCBR = F20.6/
4 11X,10H TOTMAS = F20.6/
5 11X,10H PHI2 = F20.6/

```

```

00141 40*      6      11X*10H ALPHA = F20.6/
00141 41*      9      11X*10H LAMBDA = F20.6/771
00142 42*      WRITE(6,2010) NIT
00145 43*      2010 FORMAT(5X,'NUMBER OF ITERATIONS =',I2)
00146 44*      TH4 = THETAS**4
00147 45*      IF(V.61.0.2) GO TO 90
00151 46*      IF(V.LE.1.0E-10) GO TO 108
00153 47*      90 THETAB = 0.9
00154 48*      95 NCT = 0
00155 49*      100 T2 = THETAB**2
00156 50*      T3 = T2*THETAB
00157 51*      FNC = FNCBR**T3
00160 52*      FM = FFN(RHOD,FNC)*FFS(RHOD)
00161 53*      DFM = DFFN(RHOD,FNC)*FFS(RHOD)
00162 54*      AYY = T3*THETAB-TH4
00163 55*      BYY = 1.0-THETAB
00164 56*      EYY = ETA(FNC)
00165 57*      EY = EYY*FM+FN
00166 58*      YY = 1.0-V-EY*AYY/BYY
00167 59*      DEYZ = (DFM*EY+FM*DETA(FNC))*3.0*T2*FNCBR
00170 60*      DYY = -AYY/BYY*(DEYZ*EY/BYY)-4.0*EY*T3/BYY
00171 61*      ZZ = THETAB-YY/DYY
00172 62*      IF(FACT.6T.20) GO TO 109
00174 63*      IF(ZZ.LT.1.0) GO TO 105
00176 64*      THETAB = (THETAB+1.0)/2.0
00177 65*      NCT = NCT+1
00200 66*      GO TO 100
00201 67*      105 IF(ABS(ZZ-THETAB)/ZZ.LT.1.0E-06) GO TO 110
00203 68*      NCT = NCT+1
00204 69*      THETAB = ZZ
00205 70*      GO TO 100
00206 71*      108 THETAB = 1.0
00207 72*      GO TO 110
00210 73*      109 WRITE(6,'900')
00210 74*      C
00212 75*      110 Y(1) = 1.0
00213 76*      Y(2) = THETAB
00214 77*      900 FORMAT(1X,'208NEWTON-RAPHSON FAILS')
00215 78*      THETAF = Y(1)
00216 79*      Y1 = Y(1)
00217 80*      Y2 = Y(2)
00220 81*      CALL MCDERVFNCBR,THETAB,FNC,DYCDT1,D2CD2T,D2CTNR)
00221 82*      CALL MDER(RLAM,FNC,FM,DFM,DFM,D2FM,LL,D2M,NC,D3M2LN,D3M2NL)
00222 83*      CALL INITIAL(DLDV,D2LDV,Y(1),Y(2),Y(3),Y(4),Y(5),Y(6),Y(7),Y(8),Y(9),Y(10),Y(11),Y(12),Y(13),Y(14),Y(15))
00223 84*      CALL INITIAL(DLDV,D2LDV,Y(1),Y(2),Y(3),Y(4),Y(5),Y(6),Y(7),Y(8),Y(9),Y(10),Y(11),Y(12),Y(13),Y(14),Y(15))
00224 85*      CALL INITIAL(DLDN,NCB,D2LNCB,Y(1),Y(2),Y(3),Y(4),Y(5),Y(6),Y(7),Y(8),Y(9),Y(10),Y(11),Y(12),Y(13),Y(14),Y(15))
00224 86*      1
00225 87*      CALL INTMIX(D2E4TN,Y(1),Y(2),Y(3),Y(4),Y(5),Y(6),Y(7),Y(8),Y(9),Y(10),Y(11),Y(12),Y(13),Y(14),Y(15))
00226 88*      CALL INTMIX(D2E4TN,Y(1),Y(2),Y(3),Y(4),Y(5),Y(6),Y(7),Y(8),Y(9),Y(10),Y(11),Y(12),Y(13),Y(14),Y(15))
00230 89*      ZZ = 0
00231 90*      DLM = 0
00232 91*      100 115 I=1,20
00233 92*      A(I) = DA
00235 93*      115 R(I) = DR
00236 94*      95*
00236 95*      C
00240 96*      WRITE(6,'2040')

```

```

02 00242 97* 2040 FORMAT(/7X,6HTHETAF,10X,6HTHETAB,10X,2HNC,13X,6HETABAR,
00242 98* 11X,3HETA,13X,1HM,14X,1HN,14X,1HX,17
00242 99* C
00243 100* ZZZ = 0.0
00244 101* DX = 1.0/(U*(1.0-THETAB))
00245 102* IFVD = 0
00246 103* IF(DX.GT.DXWRT) DX = DXWRT
00250 104* N = 20
00251 105* IBKP = 1
00252 106* NTRY = 1
00253 107* IERR = 0
00253 108* C
00254 109* DLMT = DXWRT/500.0
00255 110* XWRT = 0.0
00256 111* DTEP = 0
00257 112* LCNT = 0
00260 113* ICNT = 0
00261 114* CALL RRS(SORV,SCNTLC,Y,DYFA,RZZZ,DX,N,IFVD,IBKP,NTRY,IERR,
00261 115* OLY,PD,SD,YS,YST,DYST,YSIMP)
00262 116* AM(1) = -Y(3)
00263 117* AM(2) = -Y(7)
00264 118* AM(3) = -Y(11)
00265 119* AM(1,1) = Y(5)
00266 120* AM(1,2) = Y(15)
00267 121* AM(1,3) = Y(17)
00270 122* AM(2,1) = Y(15)
00271 123* AM(2,2) = Y(9)
00272 124* AM(2,3) = Y(19)
00273 125* AM(3,1) = Y(17)
00274 126* AM(3,2) = Y(19)
00275 127* AM(3,3) = Y(13)
00276 128* CALL FMIN(VAV,XM,3,4)
00277 129* 205 FORMAT (//45X,27H PARAMETERS AT END OF TUBE //)
00300 130* 210 FORMAT (1X,51X,8HTHETAF =F10.6,/)
00301 131* 215 FORMAT (1X,23X,3HU =E14.6,16X,3HV =E14.6,12X,7HNCBAR =E14.6,/)
00302 132* 230 FORMAT (1X,19X,7HDTFDDU =E14.6,12X,7HDTFDDV =E14.6,8X,
00302 133* 11HDTFNGBAR =E14.6,/)
00303 134* 240 FORMAT (1X,17X,9HD2TFDDU =E14.6,10X,9HD2TFDDV =E14.6,6X,
00303 135* 13HD2TFDDNGBAR =E14.6,/)
00304 136* 250 FORMAT (1X,16X,10HD2TFDDUV =E14.6,75X,14HD2TFDDNGBAR =E14.6,
00304 137* 5X,14HD2TFDDNGBAR =E14.6,/)
00305 138* 220 FORMAT (7,3X,24HINCR, 50UGHY DELTA U =E14.6,10X,9HDELTA V =,
00305 139* E14.6,6X,13HDELTA NGBAR =E14.6,/)
00306 140* 221 FORMAT (7,3X,24HINCR, USED DELTA U =E14.6,10X,9HDELTA V =,
00306 141* E14.6,6X,13HDELTA NGBAR =E14.6,/)
00307 142* NIT = NIT+1
00310 143* Z1 = U
00311 144* Z2 = V
00312 145* Z3 = FNGBR
00313 146* WRITE (6,205)
00315 147* WRITE (6,210) Y(11)
00320 148* WRITE (6,215) Z1,Z2,Z3
00325 149* WRITE (6,230) Y(3),Y(7),Y(11)
00332 150* WRITE (6,240) Y(5),Y(9),Y(13)
00344 152* WRITE (6,250) Y(15),Y(17),Y(19)
00352 153* CALL BNDNC(U,V,FNGBR,XM,TOTMAS,ALPHA)

```



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00353 154* WRITE(6,221) (XM(I),I=1,3)
00361 155* 200 IF (NIT.GT. 20) GO TO 300
00363 156* ZS = Y(1)-THETAS
00364 157* IF(ZS.LT.0.0001) GO TO 2070
00366 158* IF(ABS(Y(1))-TFLX(Y(1)) .LE. 5.0E-04) GO TO 2090
00370 159* TFLX(Y(1)) = Y(1)
00371 160* IF (ABS(XM(1))/Z1.GT.0.0001) GO TO 50
00373 161* IF (ABS(XM(2))/Z2.GT.0.0001) GO TO 50
00375 162* IF (ABS(XM(3))/Z3.GT.0.0001) GO TO 50
00377 163* WRITE(6,2060)
00401 164* 2060 FORMAT(1H0,15HOPTIMUM REACHED)
GO TO 1
00402 165* GO TO 1
00403 166* 300 WRITE (6,2050)
00405 167* 2050 FORMAT (1X,32H NUMBER OF ITERATIONS EXCEEDS 20 )
00406 168* GO TO 1
00407 169* 2070 WRITE(6,2075)
00411 170* 2075 FORMAT(1H0,24HVANISHING HEAT REJECTION)
00412 171* GO TO 1
00413 172* 2090 WRITE(6,2095)
00415 173* 2095 FORMAT(1H0,40HINSIGNIFICANT IMPROVEMENT OVER LAST STEP)
00416 174* GO TO 1
00417 175* 3000 STOP
00420 176* END

```

END OF COMPILATION: NO DIAGNOSTICS.

QFOR:IS CONST
FOR:59A=0727772-19:37:44 (70)

SUBROUTINE CONST ENTRY POINT 000373

STORAGE USED: CODE(1) 000446; DATA(0) 000071; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 SGR1
0004 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R 000003 A 0000 R 000002 AZ 0000 R 000004 B 0000 R 000005 C 0000 R 000006 D
 0000 R 000010 DAN 0000 R 000007 DAV 0000 R 000014 DBN 0000 R 000017 DCU
 0000 R 000020 DCV 0000 R 000026 DDN 0000 R 000024 DDV 0000 R 000025 DDV 0000 R 000023 DZ
 0000 R 000012 DZANN 0000 R 000031 DZAVN 0000 R 000011 DZAVV 0000 R 000016 DZBNN 0000 R 000032 DZBNN
 0000 R 000015 DZBVV 0000 R 000021 DZCUU 0000 R 000033 DZCVV 0000 R 000022 DZCVV 0000 R 000030 DZDNN
 0000 R 000034 DZDVV 0000 R 000027 DZDVV 0000 000043 INDP5 0000 R 000000 PI 0000 R 000001 Z

00101 1* SUBROUTINE CONST(TOTMAS,PHI2,ALPHA,U,V,FNCBR,HOD,DLDDU,DLDDV,DLONCB,DLONCB,
 00101 2* DLDDUU,DLDDVV,ZCLONB,ZCLONB,ZCLDDVV,ZCLVNB,ZCLNCB)

00101 3* C PI = 3.1415926

00104 4* Z = V**3/FNCBR

00105 5* AZ = ALPHA*ALPHA

00106 6* A = TOTMAS-AZ*Z

00107 8* IF (A.LY. 1.0E-06) A = 1.0E-06

00107 9* C B = PI*ALPHA*Z

00111 10* C C = PHI2*ALPHA*V**2*SQRT(U)

00112 11* D = SQRT(B*B+A*C)

00113 12* HOD = (B*D)/A

00114 13* C DAV = -3.0*B*ALPHA/(PI*V)

00115 14* DAN = AZ*Z/FNCBR

00116 15* DZAVV = -6.0*AZ*V/FNCBR

00117 16* DZANN = -2.0*DAN/FNCBR

00120 18* C DBV = 3.0*B/V

00121 19* DBN = -B/FNCBR

00122 20* DZBVV = 6.0*B/(V*V)

00123 21* DZBNN = 2.0*B/(FNCBR*FNCBR)

00124 22* DCU = C/(2.0*U)

00125 23* DCV = 2.0*C/V

00127 24* DZCUU = -DCU/(2.0*U)

00130 26* DZCVV = DCV/V

00130 28* C

00131 30* DZ = 2.0*D
 00132 31* DDU = A*DCU/DZ
 00133 32* DDV = (2.0*B*DBV+A*DCV+C*DAV)/DZ
 00134 33* DDN = (2.0*B*DBN+C*DBN)/DZ
 00135 34* D2DVV = (-DDV*DDV+DBV*DBV+B*D2BVV+DAV*DCV+(D2CVV*A+D2AVV*C)/2.0)
 00136 35* D2DNN = (-DDN*DDN+DBN*DBN+B*D2BNN+C*D2ANN/2.0)/D
 00137 36* D2AVN = -3.0*DBN*ALPHA/(PI*V)
 00138 37* D2BVN = 3.0*DBN/V
 00139 38* D2CUV = C/(U*V)
 00140 39* D2DVN = (-DDN*DDV+DBV*DBN+B*D2BVN+(DCV*DBN+C*D2AVN)/2.0)/D
 00141 40* DLDU = DCU/DZ
 00142 41* DLDV = (-HOD*DAV+DBV+DDV)/A
 00143 42* DLDNCB = (-HOD*DAN+DBN+DDN)/A
 00144 43* D2LDUU = (D2CUU-DDU*DCU/D)/DZ
 00145 44* D2LDVV = (-2.0*DLDV*DAV-HOD*D2AVV+D2BVV+D2DVV)/A
 00146 45* D2LNCB = (-2.0*DLDNCB*DAN-HOD*D2ANN+D2BNN+D2DNN)/A
 00147 46* D2LDUV = (D2CUV-2.0*DLOU*DDV)/DZ
 00148 47* D2LUNB = -DLOU*DDN/D
 00149 48* D2LVNB = (-DLDV*DAN-DLNCB*DAV-HOD*D2AVN+D2BVN+D2DVN)/A
 00150 49* RETURN
 00151 50* END
 00152 51*
 00153 52*
 00154 53*
 00155 54*
 00156 55*

END OF COMPILATION: NO DIAGNOSTICS.

FOR 15 BNDEND
FOR 59A-0772772=19:37:47 (10)

SUBROUTINE BNDEND ENTRY POINT 000154

STORAGE USED: C0C011) 000207; DATA(07 000027) BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NEXP6\$
0004 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000011 500L 0000 000014 INJPS 0000 I 000000 L 0000 R 000004 X1 0000 R 000005 X2
0000 R 000001 Z1 0000 R 000002 Z2 0000 R 000003 Z3

00101 1* SUBROUTINE BNDEND(U,V,FNCBR,XM,TOTMAS,ALPHA)

00101 2* C
00101 3* C BNDEND INSURES U,V, AND NCBAR ARE WITHIN THEIR BOUNDARY CONDITIONS

00101 4* C
00104 6* DIMENSION XM(3)
00105 L = I
00106 Z1 = U
00107 9* Z2 = V
00110 10* Z3 = FNCBR
00111 11* 500 U = Z1*XM(1)
00112 12* V = Z2*XM(2)
00113 13* FNCBR = Z3*XM(3)
00113 14* IF(L.EQ.2) RETURN

00115 15* IF(U.LT.5.0E-06) XM(1) = 5.0E-06-Z1
00117 16* IF(U.GT.250.0) XM(1) = 250.0-Z1
00121 17* IF(V.LT.5.0E-06) XM(2) = 5.0E-06-Z2
00123 18* IF(V.GT.50.0) XM(2) = 50.0-Z2
00125 19* IF(FNCBR.LT.1.0E-04) XM(3) = 1.0E-04-Z3
00127 20* IF(FNCBR.GT.6.0) XM(3) = 6.0-Z3

00131 21* X1 = TOTMAS*FNCBR
00132 22* X2 = ALPHA**2
00133 23* IF(X1-X2**3.LT.0.0) XM(2) = (X1/X2)**(1.0/3.0)-Z2

00135 24* L = 2
00136 25* GO TO 500
00137 26* END

END OF COMPILATION: NO DIAGNOSTICS.

QFOR,IS NDERV
FOR 59A-072772-19:37:49 (70)

SUBROUTINE NDERV ENTRY POINT 000056

STORAGE USED: CODE(1) 0000707 DATA(0) 0000151 BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 SORT
0004 ASIN
0005 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R 000000 C4 0000 R 000001 C5 0000 R 000002 C6 0000 000006 INCPS

00101 1* SUBROUTINE NDERV(RLAM, FN, DFNX, D2NDLL)
00101 2* C
00101 3* C N AND ITS DERIVATIVES
00101 4* C
00103 5* C4 = RLAM+1.0
00104 6* C5 = RLAM*2.0
00105 7* C6 = SORT(RLAM*C5)
00106 8* FN = (1.5707963+C5-C6-ASIN(1.0/C4))/RLAM
00107 9* DFNX = -(FN*C6/C4-1.0)/RLAM
00110 10* D2NDLL = -(2.0*DFNX+1.0)/(C5*C4*C6)/RLAM
00111 11* RETURN
00112 12* END

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS MDER
FOR S9A=0772772=19:37:57 (10)

SUBROUTINE MDER ENTRY POINT 000251

STORAGE USED: CODE (1) 0003041 DATAT07 0000661 BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK# NAME)

0003 SORT
0004 ASIN
0005 NERR3\$

STORAGE ASSIGNMENT (BLOCK# TYPE, RELATIVE LOCATION, NAME)

0000 R 000011 CFN 0000 R 000000 C1 0000 R 000017 C10 0000 R 000020 C11 0000 R 000022 C12
 0000 R 000001 C2 0000 R 000003 C3 0000 R 000002 C4 0000 R 000004 C5 0000 R 000005 C6
 0000 R 000006 C7 0000 R 000007 C8 0000 R 000010 C9 0000 R 000015 DCFDNC 0000 R 000013 DCFNDL
 0000 R 000014 DFFSOL 0000 R 000016 D2CFLL 0000 R 000025 D2CFNC 0000 R 000026 D2CLNC 0000 R 000023 D2C2LL
 0000 R 000021 D2C3LL 0000 R 000024 D2FSLL 0000 R 000027 D3C2LN 0000 R 000030 D3C2NL 0000 R 000012 FFS
 0000 000040 IN.P\$

00101 1* SUBROUTINE MDER(RLAM)*FNC*FMDFMX*DFMTDZFMCL*D2MDNC*D2MENC*D3M2LN*

00101 2* 103M2NL)

00101 3* C
 00101 4* C
 00101 5* C
 00101 6* C

00104 7* C1 = 0.1460*FNC-0.02866

00105 8* C2 = SORT(RLAM*(2+RLAM))

00106 9* C3 = 1.0/(RLAM+1.0)

00107 10* C4 = ASIN(C4)

00110 11* C5 = 1/(C4*C2)

00111 12* C6 = (C4**2)/SORT(1-C4**2)

00112 13* C7 = 1/(RLAM**2)

00113 14* C8 = FNC/RLAM

00114 15* C9 = 2.*C7*CR

00115 16* CFN = 1.0-C1*C8

00116 17* FFS = (C2*C3-1.57079635)/RLAM

00117 18* FM = CFN*FFS

00120 19* DCFNDL = C1*C7*FNC

00121 20* DFFSOL = (C5-C6-FFS)/RLAM

00122 21* DFMX = CFN*DFFSOL+FFS*DCFNDL

00123 22* DCFDNC = -(0.1460*FNC+C1)/RLAM

00124 23* D2CFLL = FFS*DCFNDL

00125 24* D2CFLL = -C1*C9

00126 25* C10 = 1-C4**2

00127 26* C11 = +1.*0.5/C10*C4**2

00130 27* D2C3LL = 2*(C4**3)*C11/SORT(C10)

00131 28* D2C2LL = 1/C2-C2*(C4**2)

```

00132 29* 02FSLL = (02C2LL*02C3LL-2.*0FF5DL)/RLAM
00133 30* 02FMLL = CFN*02FSLL*2.*0FF5DL*0CFNDL*FFS*02CFLL
00134 31* 02CFNC = -0.2920/RLAM
00135 32* 02M0NC = FFS*02CFNC
00136 33* 02CLNC = (0.146*FNC+C1)*C7
00137 34* 02MLNC = DCFDNC*0FF5DL*02CLNC*FFS
00140 35* 03C2LN = -2.*02CLNC/RLAM
00141 36* 03M2LN = DCFDNC*02FSLL*2.*0FF5DL*02CLNC*FFS*03C2LN
00142 37* 03C2NL = 0.2920*C7
00143 38* 03M2NL = FFS*03C2NL*0FF5DL*02CFNC
00144 39* RETURN
00145 40* END

```

END OF COMPILATION: NO DIAGNOSTICS.

GFOR15 INITIAL
FOR SPA-0772772-19:38:01 (70)

SUBROUTINE INITIAL ENTRY POINT 000470

STORAGE USED: CODE(1) 0005221 DATA(0) 0001231 BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 BLK1 000014

EXTERNAL REFERENCES (BLOCK, NAME)

0004 ETA
0005 DELTA
0006 DETA
0007 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R 000037 A1 0000 R 000040 A2 0000 R 000041 A3 0000 R 000053 B1 0000 R 000054 B2
0006 R 000000 DETA 0000 R 000051 DETA 0005 R 000000 DELTA 0000 R 000046 DELTA 0003 R 000023 DELTA
0000 R 000032 DELTA 0000 R 000027 DELTA 0000 R 000047 DELTA 0000 R 000030 DELTA 0000 R 000034 DELTA
0000 R 000031 DELTA 0000 R 000035 DELTA 0003 R 000021 DELTA 0000 R 000044 DELTA
0000 R 000013 DELTA 0000 R 000045 DELTA 0003 R 000012 DELTA 0000 R 000043 DELTA 0003 R 000010 DELTA
0003 R 000007 DELTA 0000 R 000061 DELTA 0000 R 000062 DELTA 0000 R 000065 DELTA 0000 R 000060 DELTA
0000 R 000055 DELTA 0000 R 000036 DELTA 0000 R 000042 DELTA 0000 R 000066 DELTA 0000 R 000071 DELTA
0003 R 000016 DELTA 0000 R 000056 DELTA 0003 R 000015 DELTA 0003 R 000014 DELTA 0000 R 000052 DELTA
0000 R 000067 DELTA 0000 R 000050 DELTA 0003 R 000011 DELTA 0000 R 000057 DELTA 0000 R 000063 DELTA
0000 R 000064 DELTA 0004 R 000000 DELTA 0000 R 000025 DELTA 0000 R 000026 DELTA 0003 R 000022 DELTA
0003 R 000002 DELTA 0003 R 000003 DELTA 0003 R 000005 DELTA 0003 R 000004 DELTA 0000 R 000100 DELTA
0000 R 000070 DELTA 0003 R 000000 DELTA 0003 R 000001 DELTA 0003 R 000006 DELTA
0003 R 000017 DELTA 0003 R 000020 DELTA 0000 R 000024 DELTA

00101 1* SUBROUTINE INITIAL DELTA 000037 A1 0000 R 000040 A2 0000 R 000041 A3 0000 R 000053 B1 0000 R 000054 B2

00101 2* C

00101 3* C

00101 4* C

00101 5* C

00101 6* C

00101 7* C

00101 8* C

00103 9* DIMENSION Y(20)

00104 10* COMMON /BLK1/ THETA, THETA5, FNC, FNCB, FNC, V, DNCDT1, DFNX, D2NDLL,

00104 11* I DFNX, DFM, D2MENC, D2MENC, D2MENC, Y1, Y2, D2E4TU, D2E4LU

00105 12* Y(1) = Y1

00105 13* Y(2) = Y2

00107 14* Z = FNC

00110 15* E1 = FNC*Y1 + FNC*Y2 + FNC

00111 16* E2 = THETA**4 - THETA**4

02

00112 17* E3 = E2/(1-THETAB)

00113 18* Y(3) = 0.

00114 19* DE10TB = DNCOT1*(OFM*ETA(Z)+FM*DETA(Z))

00115 20* DE20TB = 4.*(THETAB**3)

00116 21* DE30TB = E3*(DE20TB+E3)/E2

00117 22* DE40TB = E1*DE30TB+E3*DE10TB

00120 23* DE1DL = ETA(Z)*DFM*DFNX

00121 24* DE1DNC = ETA(Z)*DFM*DETA(Z)*FN

00122 25* DE4DU = E3*DE1DL*DL0U+B*E3*DE1DNC*THETAB**3

00123 26* Y(4) = -(1-C17V**2+DE4DU)/DE40TB

00124 27* Y(5) = 0.

00125 28* DE2DU = DE20TB*Y(4)

00126 29* DE3DU = E3*(E3*Y(4)+DE2DU)/E2

00127 30* DE2ETU = 12.*Y(4)*(THETAB**2)

00130 31* A1 = E3*(DE2ETU+DE3DU)/E2

00131 32* A2 = DE20TB*E3

00132 33* A3 = -E3*DE2DU/(E2**2)+DE3DU/E2

00133 34* DE3TU = A1+A2*A3

00134 35* DFNDU = DFNX*DL0U

00135 36* DFCNDU = DNCOT1*(4)*5*Y(2)**3

00136 37* DFNDU = DFNX*DL0U+DFM*DFCNDU

00137 38* DETA0U = DETA(Z)*DFCNDU

00140 39* DE1DU = FM*DETA0U+ETA(Z)*DFNDU+DFNDU

00141 40* D2VCTU = 6*FNCR*Y(2)*Y(4)+B*3*Y(2)**2

00142 41* DDETOU = DETA(Z)*DFCNDU

00143 42* D2VNCU = D2MLNC*DL0U+D2VNC*DFCNDU

00144 43* B1 = DFM*DETA0U+ETA(Z)*D2VNCU+FM*DETOU+DETA(Z)*DFMDU

00145 44* B2 = DE1DT3*D2VCTU/DNCOT1

00146 45* D2E1TU = DNCOT1*B1+B2

00147 46* D2MDLU = D2F*MLC*DL0U+D2MLNC*DFCNDU

00150 47* D2NDLU = D2NDLL*DL0U

00151 48* D2E1LU = ETA(Z)*D2MDLU+DETA0U+DFM*D2NDLU

00152 49* D2E4LU = E3*D2E1LU+DE1DL*DE3DU

00153 50* D1 = DETA(Z)*DFCNDU*DFM

00154 51* D2 = ETA(Z)*D2VNCU

00155 52* D3 = DDETA(Z)*FM*DFCNDU

00156 53* D4 = DETA(Z)*DFMDU

00157 54* D2E1C8 = D1+D2+D3+D4

00160 55* D2E4C8 = DE3DU*DE1DNC+E3*D2E1C3

00161 56* D2VNCB = 3*Y(4)*Y(2)**2

00162 57* TERVNB = B*(E3*DE1DNC+D2VNCB+Y(2)**3*D2E4CB)

00163 58* D2E4UU = E3*DE1DL*DE3DU+D2E4UU+D2E4LU*TERVNB

00164 59* D2E4TU = E1*D2E3TU+DE30TB*DE1DU+E3*D2E1TU+DE1DTB*DE3DU

00165 60* Y(6) = -(Y(4)+D2E4TU+D2E4UU+2*(C-1)*V**3)/DE40TB

00166 61* Y3 = Y(3)

00167 62* Y4 = Y(4)

00170 63* Y5 = Y(5)

00171 64* Y6 = Y(6)

00172 65* RETURN

00173 66* END

END OF COMPILATION: NO DIAGNOSTICS.

9FOR, IS DERV
FOR S9A=07727772=19:38:07 (70)

62

SUBROUTINE DERV ENTRY POINT 000604

STORAGE USED: CODE(1) 0007211 DATA(0) 0001301 BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 BLK1 000024
0004 BLKD 000012

EXTERNAL REFERENCES (BLOCK, NAME)

0005 ETA
0006 DETA
0007 DDETA
0010 DDETA
0011 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0004 R 000003 A1	0004 R 000004 A2	0004 R 000005 A3	0004 R 000006 A4	0004 R 000007 A5
0004 R 000010 A6	0000 R 000051 A7	0000 R 000063 DA70U	0010 R 000000 DDETA	0007 R 000000 DDETA
0006 R 000000 DETA	0003 000023 DEIDL	0003 000021 DE4DTB	0003 R 000013 DFM	0003 R 000012 DFMX
0003 R 000010 DFNX	0003 000007 DNCOT1	0000 R 000052 DNOU	0000 R 000024 DY	0000 R 000053 D2A10U
0000 R 000066 D2A2JU	0000 R 000067 D2A3JU	0000 R 000070 D2A4JU	0000 R 000061 D2A5JU	0000 R 000062 D2A6U
0000 R 000065 D2EEJU	0000 R 000055 D2EPUU	0000 R 000060 D2EJU	0003 R 000016 D2FMLL	0003 R 000015 D2MDNC
0003 R 000014 D2MLVC	0000 R 000056 D2MUU	0000 R 000054 D2NGUU	0003 R 000011 D2NDLL	0000 R 000064 D2NUU
0000 R 000057 D3M2JU	0004 R 000001 D3M2LN	0004 R 000002 D3M2NL	0004 R 000011 EB	0005 R 000000 ETA
0003 000022 E3	0003 R 000002 FM	0003 R 000003 FN	0003 R 000005 FNC	0003 R 000004 FNCBR
0000 000077 INJP5	0003 000000 THETAB	0003 R 000001 THETAS	0004 R 000000 U	0003 000006 V
0000 R 000000 Y	0003 R 000017 Y1	0003 R 000020 Y2	0000 R 000050 Z	

00101 1* SUBROUTINE DERV(Y1,Y2,Y3,Y4,Y5,Y6,Y7,D0L000,DY3,DY4,DY5,DY678,C,
00101 2* 1 DNC0U,DA10U,DA20U,DA30U,DA40U,DA50U,DA60U,
00101 3* 2 DEBDU,DEU,DEPU,DH0U,D2MNCU)

00101 4* C DERIVATIVES

00101 5* C FOR FIRST AND SECOND DERIVATIVES OF U SET C=1 AND B=0
00101 6* C FOR FIRST AND SECOND DERIVATIVES OF V SET C=0 AND B=0
00101 7* C FOR FIRST AND SECOND DERIVATIVES OF FNCBR SET C=0 AND B=1

00101 8* C DIMENSION Y(207),DY(207)

00101 9* C COMMON /BLK1/THETAB,THETAS,FM,FN,FNCBR,FNC,V,DNCOT1,DFNX,D2NDLL,
00101 10* 1 DFMX,DFM,D2MNCU,D2MNC,D2FMLL,Y1,Y2,DEVDYB7E3,DEIDL/
00101 11* 2 BLKD/U,D3M2LN,D3M2NL,A1,A2,A3,A4,A5,A6,EB

00101 12* Y(1) = Y1

00101 13* Y(2) = Y2

00101 14* Y(1) = Y1

00101 15* Y(2) = Y2

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00107 17* Y(3) = Y3
00110 18* Y(4) = Y4
00111 19* Y(5) = Y5
00112 20* Y(6) = Y6
00113 21* Z = FNC
00114 22* EB = FM*ETA(Z)*FN
00115 23* A1 = 1./(Y(1)-Y(2))
00116 24* A5 = FM*ETA(Z)+ETA(Z)*DFM
00117 25* A6 = 3*Y(2)**2*FNCR
00120 26* A2 = A6*AS/EB
00121 27* A3 = 4*Y(2)**3/(Y(2)**4-THETAS**4)
00122 28* A4 = A1*A2*A3
00123 29* DA1DU = -A1**2*(Y(3)-Y(4))
00124 30* DNCDU = A6*Y(4)+B*Y(2)**3
00125 31* DEPU = DETA(Z)*DNCDU
00126 32* DMDU = DFMX*DLOU+DFV*DNCDU
00127 33* D2MNCU = D2MLNC*DLOU+D2MD*IC*DNCDU
00130 34* DEU = DETA(Z)*DNCDU
00131 35* DA5DU = FM*DEPU+DETA(Z)*DMDU+ETA(Z)*D2MNCU+DFM*DEU
00132 36* DA6DU = 6*Y(2)*FNCR*Y(4)+B*3*Y(2)**2
00133 37* A7 = A6*DA5DU+A5*DA6DU
00134 38* DNDU = DFNX*DLOU
00135 39* DE8DU = FM*DEU+ETA(Z)*DMDU+DNDU
00136 40* DA2DU = (A7-A2*D8E8DU)/EB
00137 41* DA3DU = A3*Y(4)*(3*Y(2)-A3)
00140 42* DA4DU = DA1DU+DA2DU+DA3DU
00141 43* DY(4) = -C/A4+U/A4**2*DA4DU
00142 44* D2A1DU = -A1**2*(Y(5)-Y(6))-2*A1*DA1DU*(Y(3)-Y(4))
00143 45* D2NCDU = A6*Y(6)+DA6DU*Y(4)+B*3*Y(4)*Y(2)**2
00144 46* D2EPU = DETA(Z)*D2NCDU+Y(4)*D2EPU**2*DDETA(Z)
00145 47* D2MUDU = DFMX*D2LDDU+DLOU*(D2F*LL*DLOU+D2MLNC*DNCDU)+DFM*D2NCDU
00146 48* D3MNUU = D2MLNC*D2LDDU+DLOU*(D3M2LN*DLOU+D3M2NL*DNCDU)
00147 51* D2EUDU = DETA(Z)*D2NCDU+D2EUDU**2
00150 52* D2A5DU = FM*D2EPU**2*DDEPU+DMDU*DETA(Z)*D2MUDU+ETA(Z)*D3MNUU
00150 53* D2A6DU = +2*DEU*D2MNCU+DFV*D2EUDU
00151 54* DA7DU = 6*Y(2)*FNCR*Y(6)+6*FNCR*Y(4)**2*B*I2*Y(2)*Y(4)
00152 55* D2NUDU = A6*D2A5DU+DA5DU*DA6DU+A5*D2A6DU+DA6DU*DA5DU
00153 56* D2EBUDU = DFNX*D2LDDU+D2NLL*DLOU**2
00154 57* D2AZUDU = FM*D2EUDU+2*DDEU*DLOU+ETA(Z)*D2MUDU+D2NNUU
00156 59* D2A3DU = A3*(3*Y(2)-A3)*Y(6)+Y(4)*(-3*Y(2)**2*Y(4)-DA3DU)
00156 60* D2A4DU = +1/A3*DA3DU**2
00157 61* D2A5DU = D2A1DU+D2A2DU+D2A3DU
00158 62* DY(6) = -2/A4+DY(4)*DA4DU+D/4**2*D2A5DU
00161 63* DY(3) = U*(Y(4)-Y(3))+Y(2)-Y(1)*C
00162 64* DY(5) = U*(Y(6)-Y(5))+2*(Y(4)-Y(3))*C
00163 65* DY(3) = DY(3)
00164 66* DY(4) = DY(4)
00165 67* DY(5) = DY(5)
00166 68* DY(6) = DY(6)
00167 69* RETURN
00170 70* END

```

END OF COMPILATION: NO DIAGNOSTICS.

9FOR15 INTMIX
FOR S9A-072772-19:38:11 (70)

SUBROUTINE INTMIX ENTRY POINT 000024

STORAGE USED: CODE (X) 0000321 DATAT07 0000077 BLANK COMMON27 000000

COMMON BLOCKS:

0005 BK1 000024

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0003 R 000025 DE1DL 0000 R 000000 DE4DL 0003 R 000021 DE4DTB 0000 R 000001 DE4DXY 0003 000013 DFM
0003 000012 DFM< 0003 000010 DFNK 0003 000007 DNC011 0003 000016 D2FMLL 0003 000015 D2MNC
0003 000014 D2MLNC 0003 000011 D2NDLL 0003 R 000022 E3 0003 000002 FM 0003 000003 FN
0003 000005 FNC 0003 000004 FNCR 0000 000002 INJPS 0003 000000 THETAB 0003 000001 THETAS
0003 000006 V 0003 000017 Y1 0003 000020 Y2

00101 1* SUBROUTINE INTMIX(D2E4TY,DTBOX,DLDX,D2E4LY,D2LDXY,D2T8XY,D2TFXY)
00103 2* COMMON /BK1/THETAB,THETAS,FM,FN,FNCR,FNC,V,DNC011,DFNX,D2NDLL,
00103 3* 1 DFMX,DFM,D2MLNC,D2MNC,D2FMLL,Y1,Y2,DE4DTB,E3,DE1DL
00104 4* D2TFXY = 0.
00105 5* DE4DL = E3*DE1DL
00106 6* DE4DXY = D2E4LY*DLDX+DE4DL*D2LDXY
00107 7* D2T8XY = -(DE4DXY+DTBOX*D2E4TY)/DE4DTB
00110 8* RETURN
00111 9* END

END OF COMPILATION: NO DIAGNOSTICS.

FOR IS MIXDER
FOR 59A-0772772-19738:18 (70)

SUBROUTINE MIXDER ENTRY POINT 000347

STORAGE USED: CODE(1) 0004547 DATA(7) 0001047 BLANK COMMON(2) 000000

COMMON-BLOCKS:

0003 BLK1 000014
0004 BLK0 000012

EXTERNAL REFERENCES (BLOCK NAME)

0005 DDETA
0006 DETA
0007 DDETA
0010 ETA
0011 NERR33

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0004 R 000003 A1 0004 R 000004 A2 0004 R 000005 A3 0004 R 000006 A4 0004 R 000007 A5
0004 R 000010 A6 0007 R 000000 DDETA 0005 R 000000 DETA 0006 R 000000 DETA 0003 000023 DEIDL
0007 000021 DE4D19 0003 R 000013 DFM 0003 R 000010 DFMX 0003 000007 DMCDT1
0000 R 000005 DMCDT1 Y 0000 R 000003 DZAIXY 0000 R 000020 DZAZXY 0000 R 000021 DZAXXY 0000 R 000022 DZ44XY
0000 R 000015 DZASXY 0000 R 000004 DZ66XY 0000 R 000017 DZEBXY 0000 R 000012 DZEPXY 0000 R 000014 DZMLNC
0003 R 000016 DZFMLL 0000 R 000013 DZMDLY 0003 R 000015 DZMNC 0000 R 000012 DZMDXY 0003 R 000014 DZMLNC
0003 R 000011 DZNDLL 0000 R 000016 DZNDXY 0000 R 000007 DZMNL 0000 R 000010 DZMNX 0004 R 000001 DZM2LN
0004 R 000002 DZM2LN 0000 R 000005 DZM2NY 0004 R 000011 EB 0010 R 000000 ETA 0003 000022 E3
0003 R 000002 FM 0003 000003 FN 0003 R 000005 FNC 0003 R 000004 FNCBR 0000 000026 INJPS
0003 000000 THETAB 0003 000001 THETAS 0004 R 000000 U 0003 000006 V 0000 R 000000 Y
0003 000017 Y1 0003 R 000020 Y2 0000 R 000002 Z

00101 1* SUBROUTINE MIXDER(D2BX,D2BT,D2BTY,D2BTXY,D2T8XY,D2T8Y,D2T8XY,D2T8Y,D2T8XY,D2T8Y)
00101 2* 1 D2T8X,DA1DX,DA1DY,DA2DX,DA2DY,DA3DX,DA3DY,DA3DX,DA3DY,
00101 3* 2 DA4DY,DA5DX,DA5DY,DA6DX,DA6DY,DLDX,DLDY,
00101 4* 3 D2LDXY,DEBDY,DEBDX,DEY,DEY,DEPY,DMDX,
00101 5* 4 DNDY,D2MNCX,D2MNCY,B,C,D3TXVE,D3FDXY)
00101 6* C
00101 7* C FOR MIXED DERIVATIVES OF U AND V SET B=1. AND C= U.
00101 8* C FOR MIXED DERIVATIVES OF U AND FNCBR SET B=1. AND C= 1.
00101 9* C FOR MIXED DERIVATIVES OF V AND FNCBR SET B=0. AND C= 1.
00101 10* C
00103 11* DIMENSION Y(2)
00104 12* COMMON /BLK1/THETAB,THETAS,FM,FN,FNCBR,FNCV,DNCDT1,DFNX,D2NDLL,
00104 13* 1 DFMX,DFM,D2MNC,D2MNC,D2MNC,D2MNC,D2MNC,D2MNC,D2MNC,D2MNC,
00104 14* 2 BLKD/U,D3M2LN,D3M2LN,A1,A2,A3,A4,A5,A6,EB
00105 15* Y(2) = Y2
00106 16* Z = FNC

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00107 17* 01FDXY = U*(D2TBXY-D2TFXY)+B*(D1BDY-D1FDY)
00110 18* D2A1XY = 2*DA1DX+DA1DY/A1-41**2+D2TFXY-D2TBXY)
00111 19* D2A6XY = 6*FNCBR*D1BDX*D1BDY*6*Y(2)*FNCBR*D2TBXY+C*6*Y(2)*D1BDX
00112 20* D3W2NY = DLDY*D3W2NL
00113 21* DNCDDY = 6*FNCBR*Y(2)*D1BDX+D1BDY*5*FNCBR*Y(2)**2)*D2TBXY+
00113 22* C*3*(Y(2)**2)*D1BDX
00114 23* D3WNLV = DLDY*D3W2LN+DNCDDY*D3W2NL
00115 24* D3WNLV = D3WNLV*DLDX+D2WNLNC*D2LDXY+D3W2NY*DNCDDY+D2WNLNC*DNCDDY
00116 25* D2EXY = DDETA(Z)*DNCDDY+DNCDDY+DETA(Z)*DNCDDY
00117 25* D2EPXY = DDETA(Z)*DNCDDY+DNCDDY+DDETA(Z)*DNCDDY
00120 27* D2WDLV = DLDY+D2WDLV+DNCDDY+D2WDLV
00121 28* D2WDXV = DLDX+D2WDLV+D2WDXV+D2WDXV+D2WDXV+D2WDXV+D2WDXV+D2WDXV+
00122 29* D2A5XY = FV*D2EPXY+DEPX*D4MDY*CEPY*DMDX+DETA(Z)*D2MDXY+DEY*D2MNCX+
00122 30* ETA(Z)*D3WNLV+DEX*D2WVCY+DFM*D2EXY
00123 31* D2WDXV = DFNX+D2LDXY+DLDX+DLDY*D2WDLV
00124 32* D2EBXY = FV*D2EXY+DMDY+DEX+ETA(Z)*D2MDXY+DEY*DMDX+D2WDXV
00125 33* D2A2XY = -(DEBDY+D2DXX+DEBDX+D2DY+A2*D2EBXY-(A6*D2A5XY)+
00125 34* DA6DY+DA5DY+DA5DY+DA6JX+A5*D2A6XY))/EB
00126 35* D2A3XY = DA3DX+DA3DY/A3+D2TBXY+DA3DX/D1BDX+
00126 36* A3*D1BDX*(-3*D1BDY/Y(2)**2-DA3DY)
00127 37* D2A4XY = D2A1XY+D2A2XY+D2A3XY
00130 38* D3TXYE = U*D2A4XY/A4**2-DA4DY*(2*A4+D2TBXE*B)/A4**2
00131 39* RETURN
00132 40* END

```

END OF COMPILATION: NO DIAGNOSTICS.

QFOR, IS ETA
FOR S9A*U72772=I9J38:27 (10)

FUNCTION ETA ENTRY POINT 000036

STORAGE USED: CODE (1) 0000441 DATA (0) 0000221 BLANK COMMENT (2) 000000

EXTERNAL REFERENCES (BLOCK# NAME)

0003 POLY
0004 EXP
0005 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000016 IL 0000 R 000001 A 0000 R 000010 B 0000 R 000000 ETA 0000 000014 INJPS
0003 R 000000 POLY

00101 1* FUNCTION ETA(X)
00103 2* DIMENSION A(7), B(2)
00104 3* DATA A(1),A(2),A(3),A(4),A(5),A(6),A(7),A(7)/0.10E+01, -0.1163143E+01,
00104 4* 1 0.1478836E+01, -0.1267550E+01, 0.6325223E+00, -0.1627067E+00,
00104 5* 2 0.1658223E-01/ B(1),B(2)/0.6866099E+00, -0.2297718E+00
00116 6* IF (X.GT.2.5) GO TO 1
00120 7* ETA = POLY(7,A,X)
00121 8* RETURN
00122 9* 1 ETA = B(1)*EXP(B(2)*X)
00123 10* RETURN
00124 11* END

END OF COMPILATION: NO DIAGNOSTICS.

FOR: IS DETA
FOR S9A-0772772-19:38:44 (70)

FUNCTION DETA ENTRY POINT 000036

STORAGE USED: CODE(I) 0000447 DATA(0) 0000217 BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 POLY
0004 EXP
0005 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000015 IL 0000 R 000001 A 0000 R 000007 B 0000 R 000000 DETA 0000 000013 INJPS
0003 R 000000 POLY

00101 1* FUNCTION DETA(X)
00103 2* DIMENSION A(6), B(2)
00104 3* DATA A(1),A(2),A(3),A(4),A(5),A(6)/-0.1163145E+01, 0.2957672E+01,
00104 4* 1 -0.3802650E+01, 0.2530089E+01, -0.8135335E+00, 0.9925338E-01/
00104 5* 2 B(1),B(2)/-0.1577635E+00, -0.2297718E+00/
00115 6* IF(X.GT.2.5) GO TO 1
00117 7* DETA = POLY(B,A,X)
00120 8* RETURN
00121 9* 1 DETA = B(1)*EXP(B(2)*X)
00122 10* RETURN
00123 11* END

END OF COMPILATION: NO DIAGNOSTICS.

2FOR15 DDETA
FOR S9A=07/27/72-19:39:00 (170)

FUNCTION DDETA ENTRY POINT 000036

STORAGE USED: CODE(1) 000044; DATA(0) 000020; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 POLY
0004 EXP
0005 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000016 IL 0000 R 000001 A 0000 R 000006 B 0000 R 000000 DDETA 0000 000012 INJPS
0003 R 000000 POLY

```
00101 1* FUNCTION DDETA(X)
00103 2* DIMENSION A(5), B(2)
00104 3* DATA A(1),A(2),A(3),A(4),A(5)/0.295767E+01, -0.7605300E+01,
00104 4* 1 0.7590267E+01, -0.3254134E+01, 0.4962669E+00/ B(1),B(2)/
00104 5* 2 0.3624960E-01, -0.2297718E+00
00114 6* IF(X.GT.2.5) GO TO 1
00116 7* DDETA = POLY(A,X)
00117 8* RETURN
00120 9* 1 DDETA = B(1)*EXP(B(2)**X)
00121 10* RETURN
00122 11* END
```

END OF COMPILATION: NO DIAGNOSTICS.

QFOR, IS DDETA
FOR S9A*07/27/72-19:39:17 (10)

FUNCTION DDETA ENTRY POINT 000036

STORAGE USED: CODE(1) 000044 DATA(0) 000017 BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 POLY
0004 EXP
0005 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000016 IL 0000 R 000001 A 0000 R 000005 B 0000 R 000000 DDETA 0000 000011 INJPS
0003 R 000000 POLY

00101 1* FUNCTION DDETA(X)
00103 2* DIMENSION A(4), B(2)
00104 3* DATA A(1),A(2),A(3),A(4)/-0.7605300E+01,0.1518053E+02,
00104 4* 1-0.9762402E+01,0.1985068E+01/
00104 5* 2 B(1),B(2)/-0.8329136E-02,-0.2297718E+00/
00113 6* IF(X.GT.2.5) GO TO 1
00115 7* DDETA = POLY(4;A;X)
00116 8* RETURN
00117 9* 1 DDETA = B(1)*EXP(B(2)*X)
00120 10* RETURN
00121 11* END

END OF COMPIATION: NO DIAGNOSTICS.

FOR IS POLY
FOR 59A-07/27/72-19:39:21 (70)

FUNCTION POLY ENTRY POINT 000036

STORAGE USED: CODE(1) 0000447 DATA(0) 0000157 BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000012 1076 0000 000003 INJPS 0000 Y 000001 L 0000 R 000000 POLY

00101 1* FUNCTION POLY(N,A,X)
00103 2* DIMENSION A(N)
00104 3* POLY = 0.
00105 4* L = N
00106 5* DO 1 K=1,N
00111 6* POLY = POLY*(X**A(L))
00112 7* 1 L = L-1
00114 8* RETURN
00115 9* END

END OF COMPILATION: NO DIAGNOSTICS.

9FOR, IS SDRV
FOR 59A-0772772-19739:24 (70)

SUBROUTINE SDRV ENTRY POINT 000601

STORAGE USED: CODE(1) 0006051 DATA(0) 0000667 BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 BLKI 000024
0004 BLKD 000012
0005 BLRR 000012
0006 VAB 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0007 ETA
0010 MCDERV
0011 MDER
0012 DETA
0013 DERV
0014 MIXDER
0015 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R	000003	/AA	0004	000003	A1	0004	000004	A2	0004	000005	A3	0004	000006	A4
0004	000007	/5	0004	000010	A6	0000 R	000005	BR	0000 R	000037	DA1DN	0000 R	000007	DA1DU
0000 R	000023	LA1DV	0000 R	000040	DA2DN	0000 R	000010	DA2DN	0000 R	000024	DA2DV	0000 R	000041	DA3DN
0000 R	000011	LA3DU	0000 R	000025	DA3DV	0000 R	000042	DA4DN	0000 R	000012	DA4DV	0000 R	000026	DA4DV
0000 R	000043	LA5DN	0000 R	000013	DA5DU	0000 R	000027	DA5DV	0000 R	000044	DA6DN	0000 R	000014	DA6DU
0000 R	000030	LA6DV	0000 R	000045	DEB3N	0000 R	000004	DEB3TB	0000 R	000015	DEB3U	0000 R	000031	DEB3V
0000 R	000046	CEN	0000 R	000047	DEPN	0000 R	000017	DEPU	0000 R	000033	DEPV	0012 R	000000	DETA
0000 R	000016	LEU	0000 R	000032	DEV	0003	000023	DE1DL	0003	000021	DE4DTB	0003 R	000013	DFM
0003 R	000012	LF4X	0003	000010	DFNX	0005 R	000006	DLNGB	0005 R	000001	DLDU	0005 R	000002	DLDV
0000 R	000050	CMDN	0000 R	000020	DMDU	0000 R	000034	DMDV	0000 R	000036	DNCON	0003 R	000007	DNCDTI
0000 R	000006	LYCDU	0000 R	000022	DNCDV	0000 R	000001	D2C02T	0000 R	000002	D2CTNB	0003 R	000016	D2FMLL
0005 R	000003	L2LDUU	0005 R	000004	D2LDUV	0005 R	000005	D2LDVW	0005 R	000007	D2LNGB	0005 R	000010	D2MNCU
0005 R	000011	L2LVNB	0003 R	000015	D2M0NC	0003 R	000014	D2MLNC	0000 R	000051	D2MNCN	0000 R	000021	D2MNCU
0000 R	000035	L2MNCV	0003	000011	D2NDLL	0004 R	000001	D3M2LN	0004 R	000002	D3M2NL	0004 R	000011	EB
0006 R	000002	ET	0007 R	000000	ETA	0003	000022	E3	0003 R	000002	FM	0003 R	000003	FN
0003 R	000005	FNC	0003 R	000004	FNCBR	0000	000056	INJPS	0003 R	000000	RLAM	0003 R	000000	THETAB
0000 R	000000	THETAF	0003 R	000001	THETAS	0004 R	000000	U	0003 R	000006	V	0003 R	000017	Y1
0003 R	000020	Y2	0006 R	000000	Z1	0006 R	000001	Z2						

00101 1* SUBROUTINE SDRV(Y,DY,X)
00103 2* DIMENSION Y(20),DY(20)
00104 3* COMMON /BLKI/THETAB,THETAS,FM,FN,FNCBR,FNC,V,DNCDTI,DFNX,D2NDLL,
00104 4* DFMCXDFM,D2MLNC,D2MNCB,D2MNC,D2MNC,D2MNC,Y1,Y2,DE4DTB7E3,DE1DL,
00104 5* BLKO/U,D3M2LN,D3M2NL,A1,A2,A3,A4,A5,A6,EB

FOR:IS SCNTL
FOR S9A=07/27/72=19:40:52 (10)

SUBROUTINE SCNTL ENTRY POINT 000147

STORAGE USED: CODE(1) 000174) DATA(0) 0000147 BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 NCT 000003
0004 VAB 000003
0005 BLKI 000024

EXTERNAL REFERENCES (BLOCK, NAME)

0006 NHDJ5
0007 NI023
0010 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000002-2000 0001 000054 5L 0001 000061 50L 0001 000135 60L 0003 R 000000 DLMT
0000 R 000000 DXSTR 0003 R 000003 DXWRT 0004 R 000002 ET 0003 I 000001 ICNT 0000 000006 INJPS
0000 I 000001 LCNT 0003 I 000004 LSTEP 0005 R 000000 VAL 0003 R 000002 XWRT 0004 R 000000 ZI
0004 R 000001 Z2

00101 1* SUBROUTINE SCNTL(Y,DY,DX,X,NTRY,IFVD)
00103 2* DIMENSION Y(20),DY(20)
00104 3* COMMON /ACT/ DLMT,ICNT,XWRT,DXWRT,LSTEP
00104 4* 1 /VAB/ Z1,Z2,ET
00104 5* 2 /BLKI/VAL(20)
00105 6* ICNT = ICNT+1
00106 7* IF(DX.GE.DXWRT.AND.ICNT.GT.1) LSTEP = 1
00110 8* IF(ABS(X-XWRT).LT.DLMT) GO TO 50
00112 9* IF(XWRT.GT.X) GO TO 5
00112 10* C
00114 11* DXSTR = DX
00115 12* DX = DX+XWRT-X
00116 13* LCNT = 1
00117 14* NTRY = 3
00120 15* RETURN
00120 16* C
00121 17* 5 NTRY = 1
00122 18* RETURN
00122 19* C
00123 20* 50 WRITE(6,2000) Y(1),Y(2),Z1,Z2,ET,VAL(3),VAL(4),X
00135 21* 2000 FORMAT (8F15.7)
00136 22* IF(LCNT.EQ.1) DX = DXSTR
00140 23* LCNT = 0
00141 24* IF(ABS(1.0-XWRT).LE.DLMT) GO TO 60

```

00143      25*      XVRT = XVRT+DXVRT
00144      26*      NTRY = 1
00145      27*      IF (LSTEP.EQ.0) RETURN
00147      28*      DX = DXVRT
00150      29*      IFVD = 1
00151      30*      RETURN
00151      31*      C
00152      32*      60 NTRY = 2
00153      33*      RETURN
00154      34*      END

```

END OF COMPIATION: NO DIAGNOSTICS.

FOR IS RKS
FOR S9A-0772772-19:41:32 (70)

SUBROUTINE RKS ENTRY POINT 006643

STORAGE USED: CODE(I) 001040I DATA(I) 000064I BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR2\$
0004 NEXP5\$
0005 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000010	10L	0001	000313	110L	0001	000333	120L	0001	000045	126G	0001	000343	130L	
0001	000071	140;	0001	000355	140L	0001	000105	146G	0001	000130	156G	0001	000417	160L	
0001	000150	164;	0001	000177	174G	0001	000500	185L	0001	000510	190L	0001	000013	20L	
0001	000232	205;	0001	000270	217G	0001	000524	220L	0001	000530	230L	0001	000543	240L	
0001	000374	245;	0001	000332	251L	0001	000552	250L	0001	000554	251L	0001	000572	257L	
0001	000604	259L	0001	000623	270L	0001	000456	300L	0001	000615	336G	0001	000054	40L	
0001	000060	45L	0001	000006	5L	0001	000076	50L	0001	000123	70L	0001	000135	80L	
0000	R	000014	AM	0000	R	000007	AMAX	0000	R	000011	C	0000	R	000001	DOT
0000	R	000003	DEL	0000	R	000012	E	0000	R	000000	FR10	0000	I	000004	I
0000	000030	INJ1\$	0000	I	000002	ISYMP	0000	I	000013	J	0000	R	000006	S	

00101	1*	SUBROUTINE RKS(deriv, cntrl, y, yatr, t, del, n, ifvdt, bkp, ntry,)	D6000200
00101	2*	11ERR, DELY, PD, SDAYS, YST, DYST, YSIMP)	D60 3
00103	3*	DIMENSION Y(N), DY(N), AT(N), R(N), DELY(N),)	D600040
00103	4*	IPD(N), SD(N), YS(N), DYST(N), YST(N), YSIMP(N)	D6000500
00104	5*	EXTERNAL DERIV, CNTRL	D600 60
00104	6*	FR10 IS FIFTH ROOT OF TEN	D6000700
00105	7*	FR10=1.5848932	D6000800
00106	8*	1ERR=0	D6000900
00106	9*	C	D6001000
00106	10*	C	D6001100
00106	11*	C	D6001200
00106	12*	C	D6001300
00106	13*	C	D600140
00106	14*	C	D600150
00106	15*	C	D6001600
00106	16*	C	D600170
00106	17*	C	D6001800
00106	18*	C	D600190
00106	19*	C	D60 200
00106	20*	C	D6002100
00106	21*	C	D60 220
00106	22*	C	D6002300
00106	23*	C	D600240
00106	24*	C	D6002500

00106	25*	C	IERR = 0	NORMAL		D6002500
00106	26*	C	-1	DELTA=0, RETURN FROM RKS		D6002600
00106	27*	C	1	A(I)+R(I)*ABS(Y(I)) = 0., RETURN FROM RKS		D6002700
00107	28*		5	IF(DEL) 20,10,20		D6002800
00112	29*		10	IERR=-1		D6002900
00113	30*		60	TO 270		D7003000
00114	31*		20	CALL DERIV(Y,DY,T)		D6003100
00115	32*		NTRY=1			D6003200
00116	33*		CALL CNTRL(Y,DY,DEL,T,NTRY,IFVD)		D6003300	
00117	34*		25	DOT=DEL		D6003400
00120	35*		30	IF(IFVD) 40,30,40		D6003500
00123	36*		30	ISYMP=2		D6003600
00124	37*		DELTA=DEL/2.			D600370
00125	38*		DO 31 I=1,N			D7003800
00130	39*		31	SD(I)=0.*0		D600390
00132	40*		IFLAG=1			D600400
00133	41*		S=1.			D6004100
00134	42*		60	TO 45		D6004200
00135	43*		40	ISYMP=1		D6004300
00136	44*		DELTA=DEL			D600440
00137	45*		45	DO 46 I=1,N		D6004500
00142	46*		YS(I)=Y(I)			D600460
00143	47*		46	DYST(I)=DY(I)		D60 470
00145	48*		30	DO 60 I=1,N		D6004800
00150	49*		DELTA=DEL			D6004900
00151	50*		PD(I)=DEL*DY(I)			D600500
00152	51*		60	CONTINUE		D6005100
00154	52*		60	TO (80,70), ISYMP		D6005200
00155	53*		70	DO 71 I=1,N		D6005300
00160	54*		71	SD(I)=SD(I)+5*DY(I)		D6005400
00163	56*		DO 85 I=1,N			D6005500
00166	57*		YS(I)=Y(I)			D600570
00167	58*		Y(I)=YS(I)+DEL*Y(I)/2.			D6005800
00170	59*		45	CONTINUE		D6005900
00172	60*		CALL DERIV(Y,DY,T)			D6006000
00173	61*		DO 90 I=1,N			D6006100
00176	62*		DELTA=DEL*DY(I)			D600620
00177	63*		PD(I)=PD(I)+2.*DEL*Y(I)			D6006300
00200	64*		Y(I)=YS(I)+DEL*Y(I)/2.			D600640
00201	65*		90	CONTINUE		D6006500
00203	66*		CALL DERIV(Y,DY,T)			D6006600
00204	67*		DO 95 I=1,N			D600670
00207	68*		DELTA=DEL*DY(I)			D600680
00210	69*		PD(I)=PD(I)+2.*DEL*Y(I)			D6006900
00211	70*		Y(I)=YS(I)+DEL*Y(I)			D600700
00212	71*		95	CONTINUE		D6007100
00214	72*		1+DEL/2.			D6007200
00215	73*		CALL DERIV(Y,DY,T)			D600730
00216	74*		DO 100 I=1,N			D6007400
00221	75*		DELTA=DEL*DY(I)			D6007500
00222	76*		PD(I)=PD(I)+DEL*Y(I)			D600760
00223	77*		Y(I)=YS(I)+PD(I)/6.			D600770
00224	78*		100	CONTINUE		D6007800
00226	79*		GO TO (110,120), ISYMP			D6007900
00227	80*		110	NTRY=1		D6008000
00230	81*		CALL DERIV(Y,DY,T)			D6008100

0231	82*	CALL CNTRL(Y,DY,DEL,T,NTRY,IFVD)	D600820
0232	83*	GO TO 300	D6008300
0233	84*	120 GO TO (130,140),IFLAG	D6008400
0234	85*	130 S=4	D6008500
0235	86*	IFLAG=2	D6008600
0236	87*	CALL DERIV(Y,DY,T)	D6008700
0237	88*	GO TO 50	07008800
0240	89*	140 CALL DERIV(Y,DY,T)	D6008900
0241	90*	AMAX = 0.0	D6009000
0242	91*	DO 180 I=1,N	D6009100
0245	92*	SD(I)=SD(I)+DY(I)	D6009200
0246	93*	YSIMP(I)=YS(I)+DEL*SD(I)/3.	D6009300
0247	94*	D = ABS(Y(I))-YSIMP(I)	D6009400
0250	95*	C = A(I)+R(I)*ABS(Y(I))	D6009500
0251	96*	IF(C) 160,150,160	D500960
0254	97*	150 FERREI	D6009700
0255	98*	GO TO 270	D6009800
0256	99*	160 E =ABS(D / 7C)	D6009900
0257	100*	AMAX=AMAX1(AMAX,E)	D501000
0260	101*	180 CONTINUE	07010100
0262	102*	IF(AMAX-1.) 215,215,230	D601020
0265	103*	215 NTRY= I	D6010300
0266	104*	CALL CNTRL(Y,DY,DEL,T,NTRY,IFVD)	D6010400
0267	105*	300 IF(NTRY-1) 185,185,310	D601050
0272	106*	310 IF(NTRY-2) 270,270,330	D601060
0275	107*	330 IF(NTRY-3) 340,340,5	D601070
0300	108*	340 I=T-DDT	D601080
0301	109*	IF(DEL) 259,107,259	D6010900
0304	110*	185 GO TO (40,190),IISYMP	D601100
0305	111*	190 IF(AMAX-.75) 200,25,220	D6011100
0310	112*	200 IF(AMAX-.075) 210,25,225	D601120
0313	113*	210 DEL=DEL*FR10	D6011300
0314	114*	GO TO 25	D6011400
0315	115*	220 DEL=DEL/FR10	D6011500
0316	116*	GO TO 25	D6011600
0317	117*	I = I + I3KP	D6011700
0320	118*	GO TO (240,250),I	D6011800
0321	119*	240 I=T-DEL	D6011900
0322	120*	DEL=DEL/FR10	D6012000
0323	121*	GO TO 259	D601210
0324	122*	250 J=1	D6012200
0325	123*	25 AV=AMAX/10.**J	D6012300
0326	124*	IF(1.-AV) 255,257,257	D601240
0331	125*	255 J=J+1	D6012500
0332	126*	GO TO 251	D601260
0333	127*	257 I=T-DEL	D601270
0334	128*	DEL=DEL/(FR10**J)	D601280
0335	129*	254 DO 245 I=1,N	D601290
0340	130*	DY(I)=DYS(I)	D6013000
0341	131*	245 Y(I)=YS(I)	D6013100
0343	132*	GO TO 25	D6013200
0344	133*	270 RETURN	D6013300
0345	134*	END	D6013400

END OF COMPILATION: NO DIAGNOSTICS.

QFOR, IS FMINV
FOR S9A=0772772=I94R:5B (70)

SUBROUTINE FMINV ENTRY POINT 00254

STORAGE USED: CODE(I) 000306F DATA(0) 001260F BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000046	105	0001	000151	11L	0001	000051	1116	0001	000071	1176	0001	000104	1236	
0001	000125	133	0001	000130	1376	0001	000172	1506	0001	000175	1546	0001	000227	1646	
0001	000212	20L	0000	R	001214	AA	0000	R	001217	B	0000	I	001224	INJPS	
0000	I	001215	11	0000	I	001220	12	0000	I	001213	J	0000	I	001216	K
				0000	I	001220	12	0000	I	001213	J	0000	R	000000	XMAT

```

00101 1* SUBROUTINE FMINV (ATXFN,M)
00103 2* DIMENSION A(N,N),X(N),XMAT(25,26)
00104 3* DO 1 I=1,N
00107 4* XMAT(I,M) = X(I)
00110 5* DO 1 J=1,N
00113 6* 1 XMAT(I,J) = A(I,J)
00116 7* DO 20 I=1,N
00121 8* AA = XMAT(I,I)
00122 9* DO 5 J=1,M
00125 10* 5 XMAT(I,J) = XMAT(I,J)/AA
00127 11* IF (I.EQ.N) GO TO 11
00131 12* 11 = I-1
00132 13* DO 10 K=1,I
00135 14* B = XMAT(K,I)
00136 15* DO 10 J=1,M
00141 16* 10 XMAT(K,J) = XMAT(K,J) - XMAT(I,J) * B
00144 17* IF (I.EQ.N) GO TO 20
00146 18* 11 12 = I+1
00147 19* DO 15 K=12,N
00152 20* B = XMAT(K,I)
00153 21* DO 15 J=1,M
00156 22* 15 XMAT(K,J) = XMAT(K,J) - XMAT(I,J) * B
00161 23* 20 CONTINUE
00163 24* DO 25 I=1,N
00166 25* 25 X(I) = XMAT(I,M)
00170 26* RETURN
00171 27* END

```

END OF COMPLETION: NO DIAGNOSTICS.

0FOR,IS NCDERV
FOR S9A-07/27/72-19:42:07 (70)

92

SUBROUTINE NCDERV ENTRY POINT 000031

STORAGE USED: CODE(1) 000044; DATA(0) 000013; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000004 I IJPS 0000 R 000000 T2 0000 R 000001 T3

00101	1*	SUBROUTINE NCDERV(FNCBR,THETAB,FNC,DNCDT1,D2CD2T,D2CTNB)
00101	2*	C
00101	3*	C NC AND ITS DERIVATIVES
00101	4*	C
00103	5*	T2 = THETAB**2
00104	6*	T3 = T2*THETAB
00105	7*	FNC = FNCBR**3
00106	8*	DNCDT1 = 3**FNCBR**T2
00107	9*	D2CD2T = 6**FNCBR*THETAB
00110	10*	D2CTNB = 3.**T2
00111	11*	RETURN
00112	12*	END

END OF COMPLETION: NO DIAGNOSTICS.

0X01
MAP 0023-0727-19142

ADDRESS LIMITS 001000 021317 040000 047773
STARTING ADDRESS 020263
WORDS DECIMAL 8400 IBANK 4092 DBANK

	SEGMENT	MAIN	001000	021317	040000	047773
NSWCS/FOR	1	001000	001021			
NRBKS/FOR	1	001022	001044			
NRWDS/FOR	1	001045	001124	2	040000	040011
NRFSS/FOR	1	001125	001326	2	040012	040031
NFTCS/FOR	1	001327	001617	2	040032	040067
NBCCV3/FOR	1	001620	001752	2	040070	040125
NFTVS/FOR	1	001753	001775			
NCL053/FOR	1	001776	002144	2	040126	040157
NWBLKS/FOR	1	002145	002266			
NBSBL3/FOR	1	002267	002323			
NUPDAS/FOR	1	002324	002356			
NBF003/FOR	1	002357	002603	2	040160	042361
NCNVT3/FOR	1	002604	003014	2	042362	042451
NIVINS/FOR	1	003015	003330	2	042452	042463
NOTINS/FOR	1	003331	004317	2	042464	042467
NOUTS3/FOR	1	004320	005176	2	042470	042514
NFWTS/FOR	1	005177	005351	2	042515	042571
NIDERS/FOR	1	005352	006233	2	042572	042676
NFCHK3/FOR	1	006234	007747	2	042677	043035
NT433/FOR	1	007750	010434	4	043036	043107
ERUS/MISC	1	007750	010434	2	043110	043146
NLIVP3/FOR	1	010435	010631	2	043147	043330
TIRS/TECH	1	010632	011046	0	043331	043361
NEXP63/FOR	1	011047	011107	2	043362	043641
ASIVC033/FOR	1	011110	011177	0	043642	043713
SGRT3/FOR	1	011200	011261	2	043714	043741
EXPS/FOR	1	011262	011326	2	043742	043753
NTERS7/FOR	1	011327	011414	2	043754	043774
NO3JFS/FOR	1	011415	011741	2	043775	044130
NERR3/FOR	1			2	044131	044140
BLKQ (COMMON BLOCK)				2	044141	044304
BLKJ (COMMON BLOCK)					044305	044316
BLKI (COMMON BLOCK)					044317	044330
VAB (COMMON BLOCK)					044331	044354
MCT (COMMON BLOCK)					044355	044357
BLANK\$COMMON (COMMON BLOCK)					044360	044364

NCDERV	1	011742	012005	0	04365	044377	0	04365	044377
FMINV	1	012006	012313	0	04400	045657	0	04400	045657
RKS	1	012314	013353	0	04566	045743	0	04566	045743
SCNTL	1	013354	013547	0	04574	045757	0	04574	045757
SURV	1	013550	014354	0	04576	046045	0	04576	046045
POLY	1	014355	014420	0	04604	046062	0	04604	046062
DUETA	1	014421	014464	0	04606	046101	0	04606	046101
DETA	1	014531	014574	0	04612	046142	0	04612	046142
ETA	1	014575	014640	0	04614	046164	0	04614	046164
MIXDR	1	014641	015314	0	04616	046270	0	04616	046270
INTMIX	1	015315	015346	0	04627	046277	0	04627	046277
DERV	1	015347	016267	0	04630	046427	0	04630	046427
INITIAL	1	016270	017011	0	04643	046552	0	04643	046552
MUER	1	017012	017315	0	04655	046640	0	04655	046640
NDERV	1	017316	017405	0	04664	046655	0	04664	046655
BDCND	1	017406	017614	0	04665	046704	0	04665	046704
CONST	1	017615	020262	0	04670	046775	0	04670	046775
MAIN	1	020263	021317	0	04676	047773	0	04676	047773
	3	BLKI		2	HLANK	COMMON	2	HLANK	COMMON
	5	MCT		4	BLKD		4	BLKD	
				6	BLKR		6	BLKR	

SYSTRIBS. LEVEL 63
END OF COLLECTION - TIME 1.955 SECONDS