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Metric Analysis of Minitrack Optical and Interferometer Data

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16. Abstract <p>The Network Analysis Program (NAP-II), which has the capability of simultaneously solving for orbits and tracking station error model terms, was, after several modifications, used in the calibration of Minitrack stations using Minitrack satellite measurements (self-calibration). Several support programs were written to aid in this task.</p> <p>A simultaneous four-arc solution was obtained. A comparison with optically determined arcs for the same time spans showed RMS position differences of 67m, 86m, 124m and 168m for the 4 arcs considered.</p> <p>An apparatus incorporating a diffraction grating was designed and successfully used to measure the drift rate of the Fort Myers MOTS camera drive.</p>			
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PREFACE

The objective of this work was to perform a study, prepare a Minitrack error model with as many of the coefficients as practical being established by pre-flight calibration measurements, prepare a computational method to utilize the error model, and to monitor the MOTS camera drive stability using a diffraction grating.

The NAP-II program, which has the capability of simultaneously solving for orbits and tracking station error model terms, was modified to substantially increase its computational speed and substantially reduce its disk memory requirements, thus making it possible to meet the contract objective within the required time-scale.

Twenty-five short optically determined reference arcs were used to calibrate the Fort Myers Minitrack station.

The NAP program was used to obtain a simultaneous four-arc solution (total length 25 days) of the 4 orbits and Minitrack station calibration numbers (for all stations).

A diffraction grating was designed and used for monitoring the stability of the Fort Myers MOTS camera drive.

The multi-arc approach to the self-calibration of Minitrack stations appears to give very good results when judged on the comparison between Minitrack and optically determined orbits. The four arcs processed under this contract showed RMS position differences of 67m, 86m, 124m and 168m, respectively. This compares favorably with an RMS position difference of 165m for the first arc based on "aircraft calibrated" Minitrack measurements.

Use of the diffraction grating apparatus developed under this contract provides a simple and inexpensive means of correcting plate errors caused by the (periodic) instability of the MOTS camera drive.

It is recommended that the approach to Minitrack self-calibration developed under this contract be further tested using other satellites (than GEOS-I) before "aircraft calibration" is finally abandoned.

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SECTION 1

MONITORING OF MOTS STABILITY BY MEANS OF A DIFFRACTION GRATING APPARATUS

1.1 INTRODUCTION

The NASA MOTS camera and the U. S. Air Force PC-1000 camera employ the same 1000mm f/5 Baker telephoto lens. The PC-1000 uses an alt-azimuth mount and is locked in a fixed orientation (relative to the earth) throughout each exposure. A precisely timed shutter provides intermittent exposures of star trails to serve as control points. The MOTS camera, by contrast, uses an equatorial mount and is sidereally driven to maintain a fixed orientation with respect to the right ascension declination frame. By virtue of this mode of operation, MOTS does not require a precisely timed shutter and provides a greater abundance of stellar images than a PC-1000. Both MOTS and PC-1000 can potentially produce accuracies of about 0.6 seconds of arc for satellite directions. This potential, however, may not be routinely realized.

One of the key advantages claimed for the PC-1000 (and for the fixed camera mode of operation, in general) is that any significant drift in the orientation of the camera throughout an exposure can be detected (and generally corrected for) by virtue of separate reductions performed on each sequence of stellar exposures. Brown, (Reference 1) reports results of an investigation of the stability of a PC-1000 over a period of about one half hour. Reductions were performed on exposures made at 5 minute intervals, leading to results plotted in Figure 1, which depicts the temporal variation of the three angular elements of orientation about their respective means. The plotted results for hour angle are normalized by the customary process of multiplication by cosine of declination. Each point is accompanied by a vertical bar defining its plus and minus 1 sigma confidence intervals. The 1 sigma values for declination and normalized hour angle are slightly less than 0.2 second of arc; for swing angle, they are

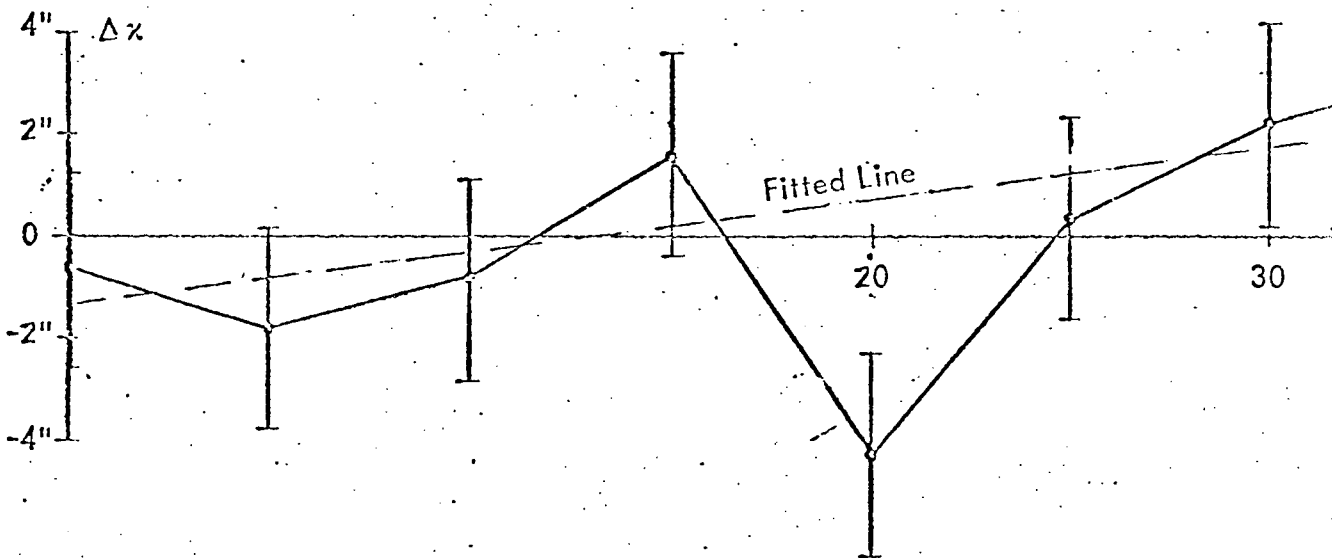
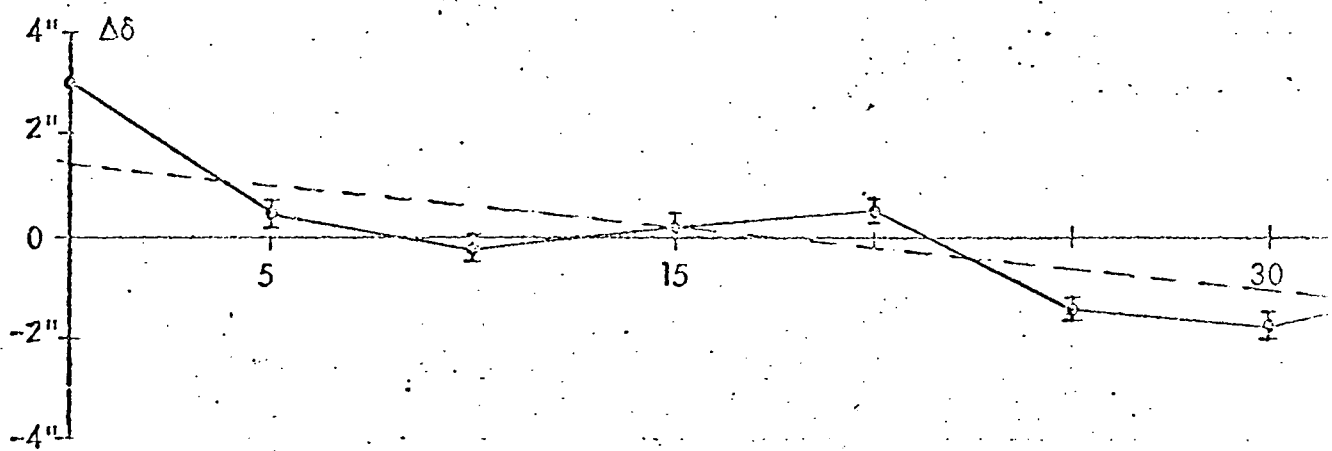
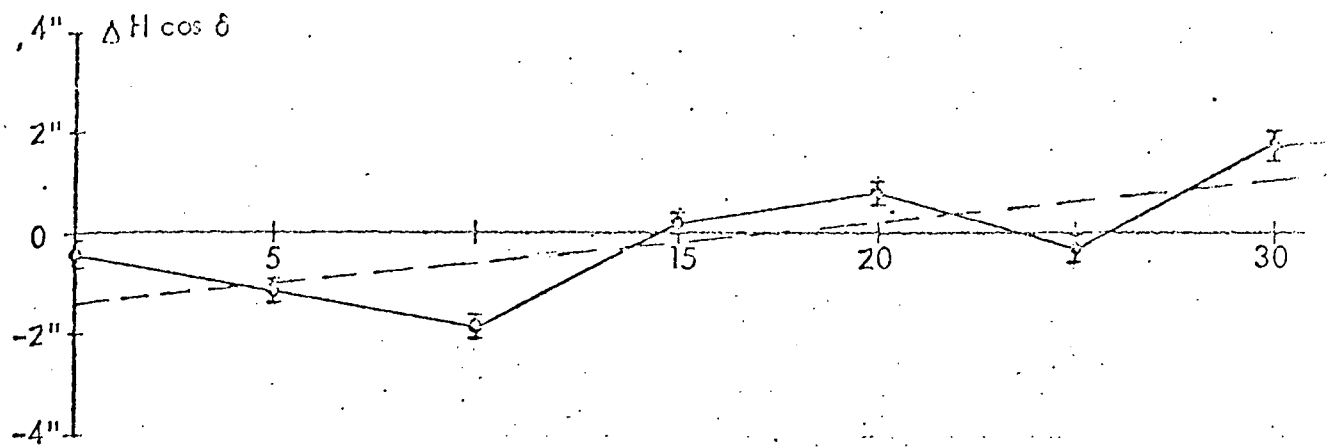


FIGURE 1. Variation in angular stability of PC-1000 camera over period of 35 minutes as reported in reference 1.

generally about ten times greater, averaging close to 2 seconds of arc. This disparity in sigmas is attributable to the fact that the focal length (1000mm) of the PC-1000 is about 10 times greater than the semi-diagonal of the plate format. The projective effect of an error of 0.2 second of arc in the direction of the camera axis is equivalent to that of an error of about 1 micron on the plate. By the same token, the projective effect of an error of 2 seconds in swing angle is equivalent to that of an error of about 1 micron near the edge of the plate. Thus, there is no actual projective disparity in the relative sigmas of the angular elements.

Figure 1 clearly demonstrates that significant changes in the orientation of the PC-1000 can occur throughout a period as short as 5 minutes. Indeed, changes in hour angle and declination of as much as 2 seconds of arc in 5 minutes are not unusual. Be this as it may, the fact is that in a fixed camera operation, any changes of significance can be detected and their effects on directions of satellites can be largely removed by an interpolative process. Thus while stability is a problem in PC-1000 operations, it is a problem that can be routinely overcome.

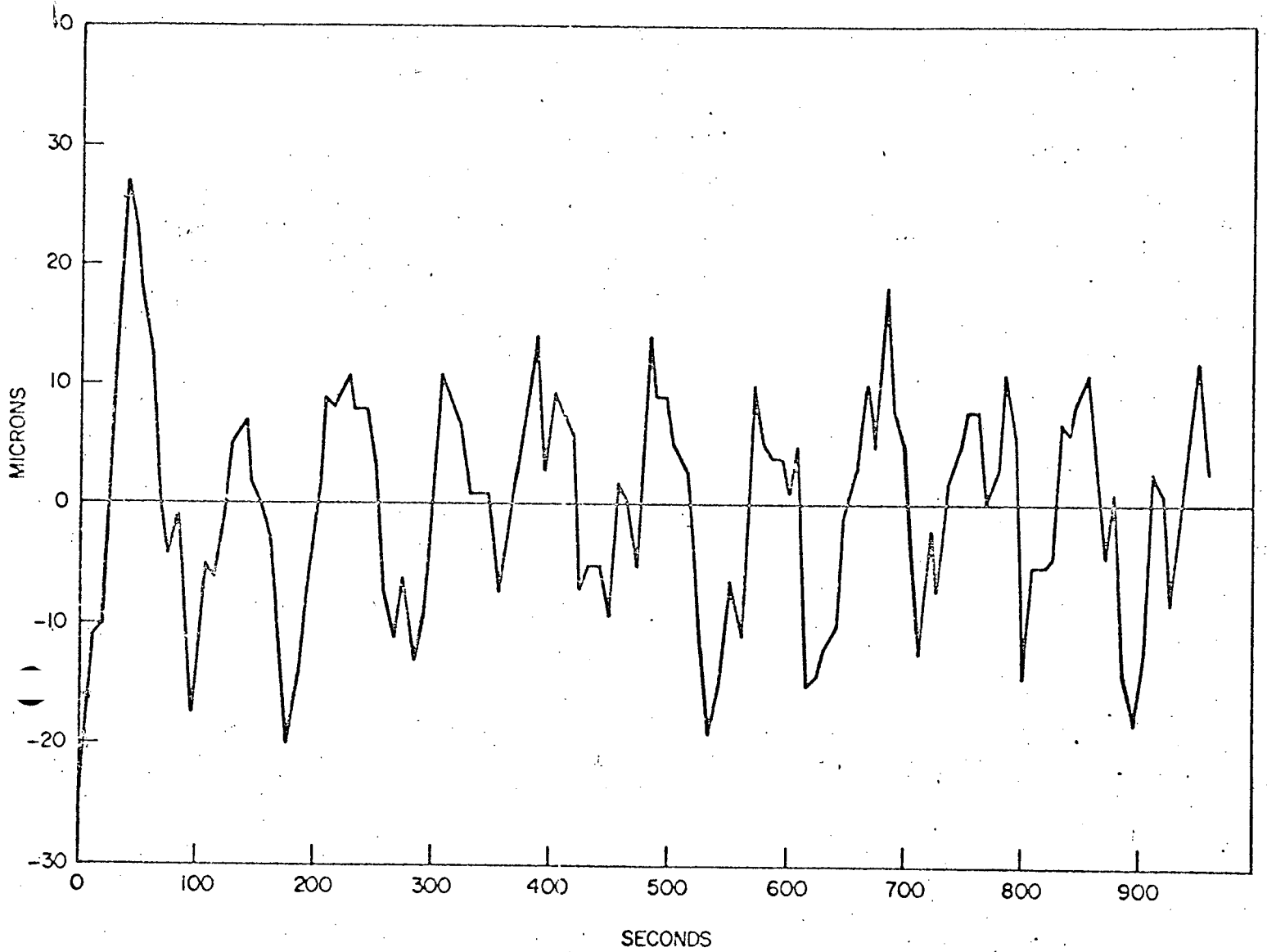
In general, MOTS is subject to the same sources of instability as the PC-1000 (e.g., thermal imbalances, wind loading, etc.). However, MOTS is also subject to drifts induced by the sidereal drive. Whatever their origin, small instabilities in MOTS orientation cannot be routinely detected because their primary effect is merely to cause a slight enlargement in the sizes of stellar images. This is a matter of no consequence insofar as the plate reduction itself is concerned, for instability affects all stars alike and hence does not degrade the residuals produced by the least squares adjustment. However, flashes are affected by the instantaneous rather than the integrated effects of instability. Hence, satellite directions derived from MOTS observations inherit fully the instantaneous departures in orientation of the camera from the mean orientation deduced from the stellar exposures. Clearly then, a simple, practical, routine means for monitoring the stability of MOTS orientation throughout an exposure would constitute a significant advance. The objective of the present investigation is to evaluate an approach that holds promise in this regard.

1.2 GENERAL CHARACTERISTICS OF ERROR INDUCED BY MOTS SIDEREAL DRIVE

A study reported by Harris, Cartwright and Oosterhout (Reference 2) provides a good understanding of the nature of the errors induced by the MOTS sidereal drive. The data analyzed in Reference 2 consists of MOTS images of a stationary collimator generating an artificial star produced by a pinhole illuminated by a strobe light of 1 millisecond duration flashing at 10 second intervals. The exposures of the flashing collimator were made over a period of 16 minutes with the MOTS axis in a nominally horizontal orientation and with the camera being driven in the normal sidereal mode. This generated a set of almost 100 successive images which, with a flawless drive, would ideally be at a constant declination and spaced at equal increments of hour angle. Departures of actual images from their ideal positions provide the desired measure of errors of the drive. In the analysis provided in Reference 1, polynomials in time were fitted to the measured x and y coordinates of the collimator images in order to account for low order effects such as the slight curvature of the trials. The residuals about the fitted polynomials reflect the combined effect of plate measuring errors and higher order sidereal drifts (slow thermal drifts and the like would be absorbed by the fitted polynomials).

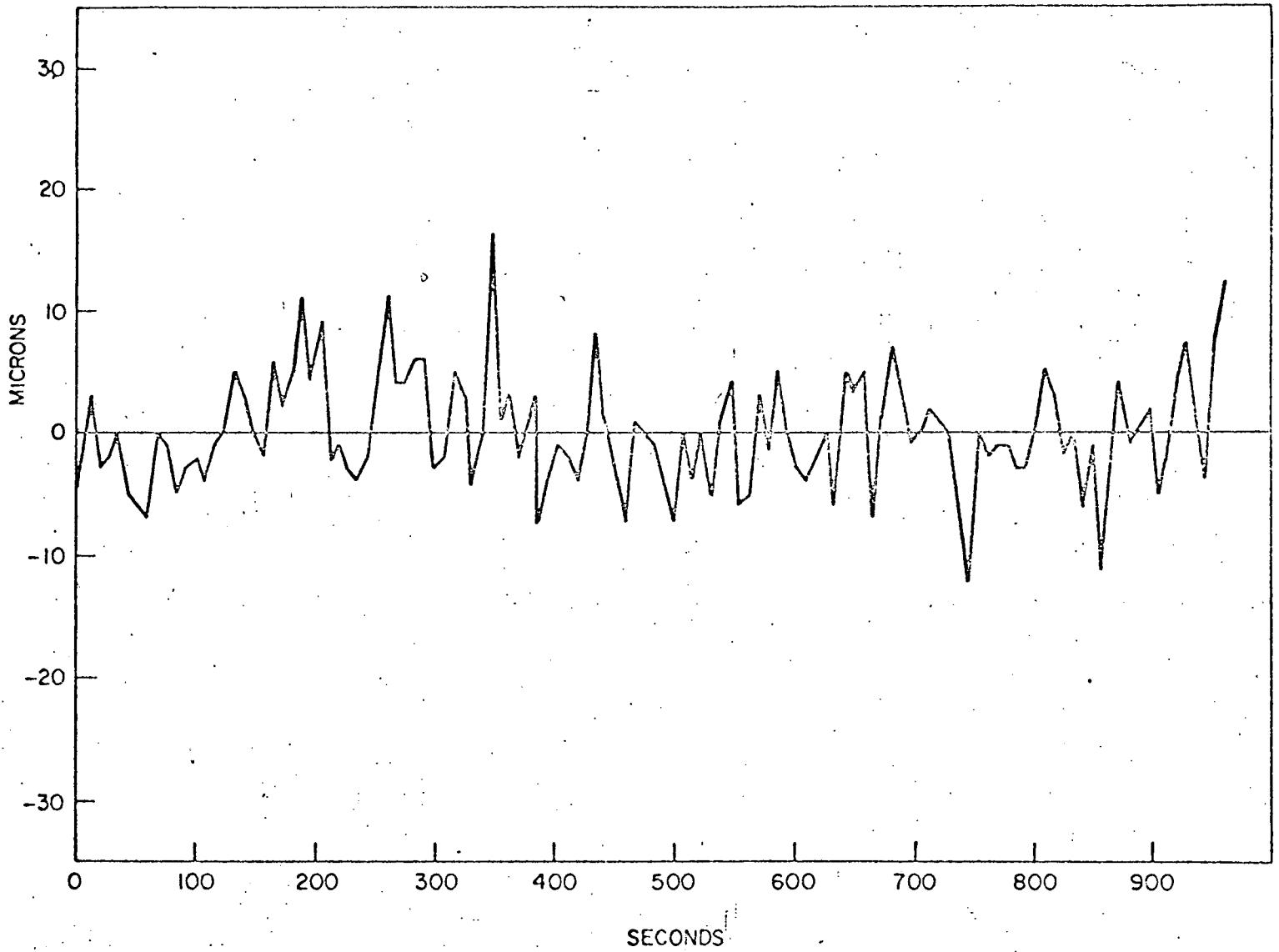
Graphs of residuals in right ascension and declination for a particular trial presented in Reference 2 are reproduced in Figures 2 and 3 below. The most significant finding of Reference 1, namely the existence of a well defined periodic drift in right ascension, is well illustrated in Figure 2. The period of the drift is almost precisely 90 seconds and is attributed to the interaction of the worm and sector gears of the drive system. The amplitude of the drift is reported in most cases to range between 2 and 3 arc seconds in right ascension and to be only about half as great in declination.

Because of geometrical considerations, the procedure employed in Reference 1 to monitor MOTS stability is not one that can be practically adopted to effect a routine calibration of drift affecting operational plates. The procedure has served well, however, to define the essential characteristics of MOTS drift, thereby making clear the problem to be overcome by any method designed for routine operational calibration of drift.



Sudbury Data Pass No.6 6th Power Residuals ΔX vs. Time


FIGURE 2. Angular stability of MOTS in right ascension as determined by flashing collimator method reported in reference [2] (5 microns = 1 second of arc).



Sudbury Data Pass No. 6 Quadratic Residuals ΔY vs. Time

FIGURE 3. Angular stability of MOTS in declination as determined by flashing collimator method reported in reference [2] (5 microns = 1 second of arc).

1.3 THE DIFFRACTION GRATING METHOD

The present investigation is concerned with the evaluation of a method of monitoring MOTS stability proposed to NASA by DBA Systems. As originally conceived, it involved placement of a coarse diffraction grating in front of the MOTS lens to generate measurable first order diffraction images of sufficiently bright stars. A series of six exposures would be made at suitable intervals with orientation of the grating being changed in nominal 15 degree steps between exposures. This sequence of exposures was to provide material for a 'precalibration' of MOTS drift. Shortly before the exposure of the satellite, the diffraction grating would be automatically retracted; immediately following the completion of the satellite observations, the grating would be returned in front of the objective for a series of six 'postcalibration' exposures at 15 degree steps. A ten times enlargement of the image generated by this process for a sufficiently bright star would have the general appearance shown here: . Now, in theory, the mean of a pair of opposing diffraction images will coincide precisely with the center of the associated primary central image. It follows that, should the central image wander slightly in position (because of drift of the mount), the locus of the wander can be reconstructed from the means of diffraction images taken at different times. The principle of the diffraction grating approach is thus straightforward and simple.

From early experiments, a more satisfactory operational method of implementing the diffraction grating approach evolved. It was learned that it was not really necessary to employ the entire aperture of the MOTS in order to obtain satisfactory images; rather, a diffraction grating having a diameter of less than half that of the MOTS objective could provide altogether acceptable results. This finding meant that the grating could remain in place and undergo its series of step rotations throughout the period in which satellite observations were being made. This obviates the need for interpolation between pre and post-calibration series of exposures and provides instead a running calibration spanning the interval of actual interest.

The final version of the apparatus that evolved from exploratory exercises is shown at half scale in Figure 4. The grating itself is of 3.5-inch diameter and is supported over the center of the field of the objective by a three-legged spider. The grating and spider obscure about 20 percent of the area of the aperture. With the particular grating employed, 25 percent of the light incident on the grating goes into the central image. Accordingly, the effective loss of light due to the imposition of the grating is only about 15 percent. The grating is rotated by means of a belt-driven turntable connected to a motor. A remote manually operated, pushbutton switch causes a spring loaded solenoid plunger to retract from one of a series of slots spaced at 15 degree intervals near the rim of the turntable. This retraction immediately trips a microswitch which starts the drive motor. The turntable is driven 15 degrees, whereupon the spring loaded plunger slips into the next slot, tripping a microswitch which turns off the drive motor. This rotation of 15 degrees is accomplished in about one half second. Thus the operator merely activates the pushbutton switch for an instant whenever he wishes to effect an increment of rotation of the grating.

The grating itself is constructed from nylon monofilament of 0.015 inch diameter spaced at 0.030 inch intervals (thus the width of the grating openings is equal to the diameter of the monofilament, causing half the light to be absorbed by the grating). This generates about $N = 115$ openings over the 3.5-inch aperture of the grating. A Xerox print of the grating is provided by Figure 5. For the adopted design, the theory of diffraction gratings shows that one fourth of the light impinging on the grating will be directed to the central image; each of the first order images will receive about 10 percent of the original light (or, more precisely, a fraction of $1/\pi^2$ of the light). The angular distance between the central image and each of the first order images is $\theta = \lambda/d$ where λ is the wavelength of the light and d is the center to center spacing of the grating divisions. For blue light ($\lambda = 0.0005\text{mm}$) and a spacing of $d = 0.030$ inches (or 0.75mm), the value of θ becomes $1/1500$ radian. Because the MOTS focal length is nominally 1000mm , this corresponds to a spacing of about 0.670mm on the MOTS plate.

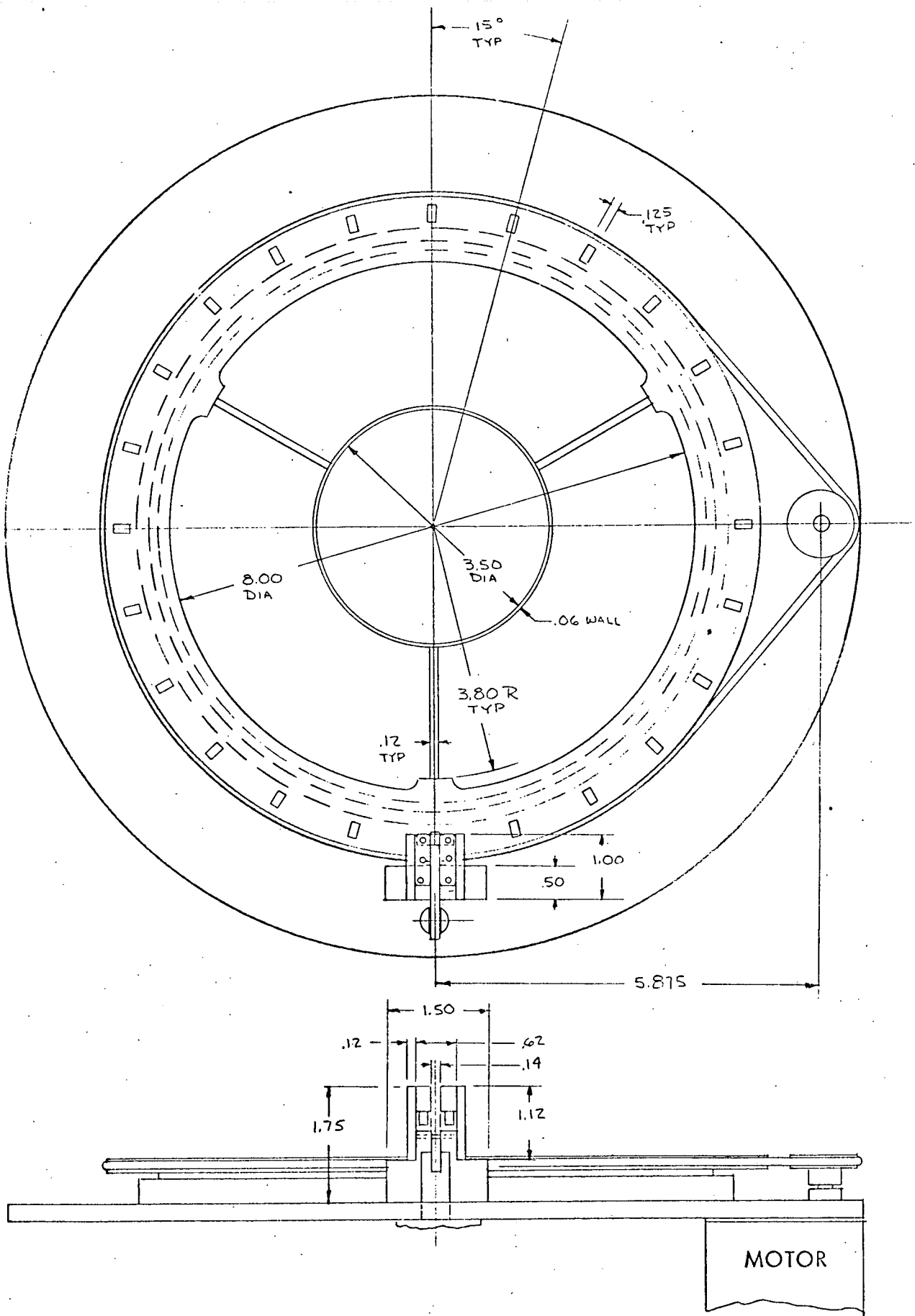


FIGURE 4. Half scale drawing of diffraction grating apparatus employed to monitor MOTS stability.

Event	Time	EST	Event	Time	Event	Time
Start Drive	T = 1 ^h 55 ^m		Start Drive	T + 10 ^m 00 ^s	Start Drive	T + 20 ^m 00 ^s
Open Shutter	T + 0 ^m 59 ^s		Open Shutter	T + 10 ^m 59 ^s	Open Shutter	T + 20 ^m 59 ^s
Shift Grating	T + 1 ^m 15 ^s		Shift Grating	T + 11 ^m 15 ^s	Shift Grating	T + 21 ^m 15 ^s
Shift Grating	T + 1 ^m 30 ^s		Shift Grating	T + 11 ^m 30 ^s	Shift Grating	T + 21 ^m 30 ^s
Shift Grating	T + 1 ^m 45 ^s		Shift Grating	T + 11 ^m 45 ^s	Shift Grating	T + 21 ^m 45 ^s
Shift Grating	T + 2 ^m 00 ^s		Shift Grating	T + 12 ^m 00 ^s	Shift Grating	T + 22 ^m 00 ^s
Shift Grating	T + 2 ^m 15 ^s		Shift Grating	T + 12 ^m 15 ^s	Shift Grating	T + 22 ^m 15 ^s
Shift Grating	T + 2 ^m 30 ^s		Shift Grating	T + 12 ^m 30 ^s	Shift Grating	T + 22 ^m 30 ^s
Shift Grating	T + 2 ^m 45 ^s		Shift Grating	T + 12 ^m 45 ^s	Shift Grating	T + 22 ^m 45 ^s
Shift Grating	T + 3 ^m 00 ^s		Shift Grating	T + 13 ^m 00 ^s	Shift Grating	T + 23 ^m 00 ^s
Shift Grating	T + 3 ^m 15 ^s		Shift Grating	T + 13 ^m 15 ^s	Shift Grating	T + 23 ^m 15 ^s
Shift Grating	T + 3 ^m 30 ^s		Shift Grating	T + 13 ^m 30 ^s	Shift Grating	T + 23 ^m 30 ^s
Shift Grating	T + 3 ^m 45 ^s		Shift Grating	T + 13 ^m 45 ^s	Shift Grating	T + 23 ^m 45 ^s
Close Shutter & Stop Drive	T + 4 ^m 00 ^s		Close Shutter & Stop Drive	T + 14 ^m 00 ^s	Close Shutter & Stop Drive	T + 24 ^m 00 ^s

Event	Time	Event	Time
Start Drive	T + 5 ^m 00 ^s	Start Drive	T + 25 ^m 00 ^s
Open Shutter	T + 5 ^m 59 ^s	Open Shutter	T + 25 ^m 59 ^s
Shift Grating	T + 6 ^m 15 ^s	Shift Grating	T + 26 ^m 15 ^s
Shift Grating	T + 6 ^m 30 ^s	Shift Grating	T + 26 ^m 30 ^s
Shift Grating	T + 6 ^m 45 ^s	Shift Grating	T + 26 ^m 45 ^s
Shift Grating	T + 7 ^m 00 ^s	Shift Grating	T + 27 ^m 00 ^s
Shift Grating	T + 7 ^m 15 ^s	Shift Grating	T + 27 ^m 15 ^s
Shift Grating	T + 7 ^m 30 ^s	Shift Grating	T + 27 ^m 30 ^s
Shift Grating	T + 7 ^m 45 ^s	Shift Grating	T + 27 ^m 45 ^s
Shift Grating	T + 8 ^m 00 ^s	Shift Grating	T + 28 ^m 00 ^s
Shift Grating	T + 8 ^m 15 ^s	Shift Grating	T + 28 ^m 15 ^s
Shift Grating	T + 8 ^m 30 ^s	Shift Grating	T + 28 ^m 30 ^s
Shift Grating	T + 8 ^m 45 ^s	Shift Grating	T + 28 ^m 45 ^s
Close Shutter & Stop Drive	T + 9 ^m 00 ^s	Close Shutter & Stop Drive	T + 29 ^m 00 ^s

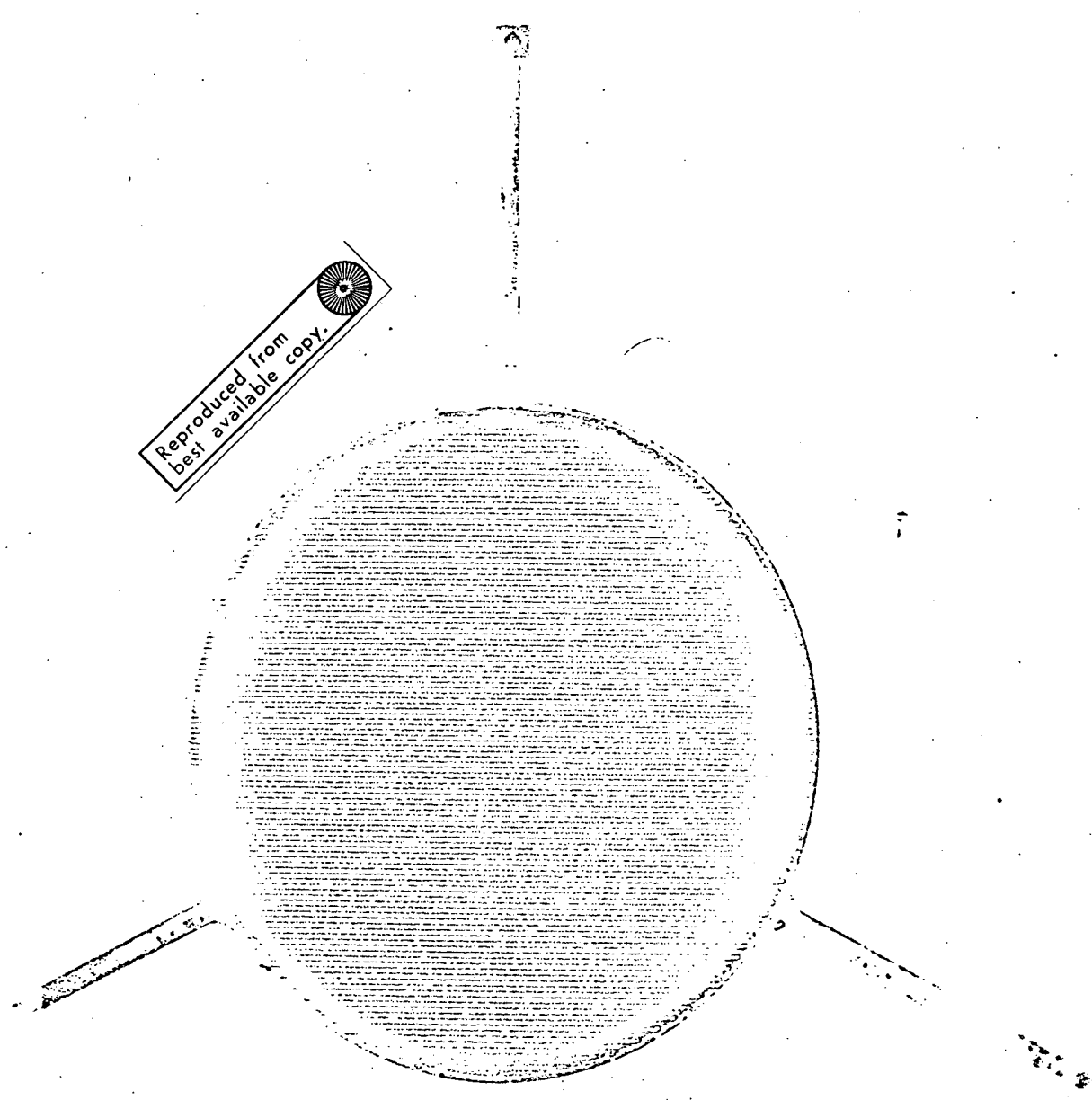


Figure 5. Direct Xerox print of diffraction grating employed in apparatus of Figure 4.

1.4 EXPERIMENTAL PROCEDURE

Short visits were made to the MOTS camera at the Ft. Myers STADAN station in April, September and November 1970 to gather data needed for the evolving design of the apparatus just described. Finally, on the night of December 2, a highly successful series of observations was made with the final version of the diffraction grating. In this section and the next we shall review the results of this test.

Because of other tests being conducted at the same time, the MOTS cameras had been refocussed for optimum imagery with blue light. For this reason, an orthochromatic emulsion (103 Ao) was employed for the diffraction grating experiment. For the data plate that was actually reduced, the MOTS was pointed toward the star β Persius, the drive was started at 01^h 55^m EST (December 3), and the initial exposure was started one minute later. Thereafter, exposures were made in accordance with the pre-established log reproduced on the next page. The total exposure for a complete set of 12 successive grating positions amounted to 180 seconds (or to two complete periods of the drive error), the grating being shifted at 15 second intervals throughout the exposure. Thus each central image of a star received the full 180 second exposure (not only from the grating but also from the unobscured aperture of the objective, as well), while each pair of diffraction images received a 15 second exposure (from the grating only). To simulate the taking of multiple plates, this process was repeated a total of six times, the drive being turned off for one minute between each sequence. Although all six sequences were recorded on a common plate, the practical end result was equivalent to what would have been obtained from the exposure of a single sequence on each of six separate plates. For this reason, we shall hereafter refer to the results from exposure sequences, 1 through 6 as being from plates 1 through 6.

The star β Persius toward which the camera was initially aimed, generated diffraction images that were too large for precise measurement. However, usable diffraction images were generated by eight other stars ranging in stellar magnitude from 2.5 to 4.0. Inasmuch as a set of diffraction images from a single star is sufficient for monitoring

stability, there was ample data from which to make a selection for reduction. In order to obtain a measure of redundancy, we selected two stars from each 'plate' for measurement and reduction. A 40X enlargement of the diffraction images generated by one of the two selected stars is provided in Figure 6. The total exposure of the central image is almost 600 times greater than the exposure of a given diffraction image. This explains the relatively large diameter of the central image. Although somewhat ragged because of their small size (about 20 to 30 microns on the plate), the diffraction images are, nonetheless, of a satisfactory quality for precise measurement.

1.5 EXPERIMENTAL RESULTS

On each of the 6 'plates', the 24 diffraction images (12 pairs) for each of the two selected stars were measured by an experienced operator on DBA's Mann comparator. The first phase of the data reduction consisted simply of determining the mean of the coordinates of each of the 12 pairs of diffraction images and then of subtracting from these the grand mean obtained by averaging the set of 12 means. If there were no drift of the camera and no measuring error, the departures from the grand mean would be precisely zero for each averaged pair of diffraction images. Significant, systematic departures were found to exist, and, within acceptable measuring tolerances, were found to be the same for the two stars measured on each plate. Accordingly, the departures for the two stars measured on each plate were themselves averaged for corresponding pairs of diffraction images.

The first stage in the analysis of the results consisted merely of plotting as functions of time the x (right ascension) and y (declination) departures obtained by the process just described. In addition, a program was written to perform a least squares regression based on functions of the form:

$$\delta x_j = a_0 + a_1 \tau_j + a_2 \sin \frac{2\pi}{90} \tau_j + a_3 \cos \frac{2\pi}{90} \tau_j$$

$$\delta y_j = b_0 + b_1 \tau_j + b_2 \sin \frac{2\pi}{90} \tau_j + b_3 \cos \frac{2\pi}{90} \tau_j$$

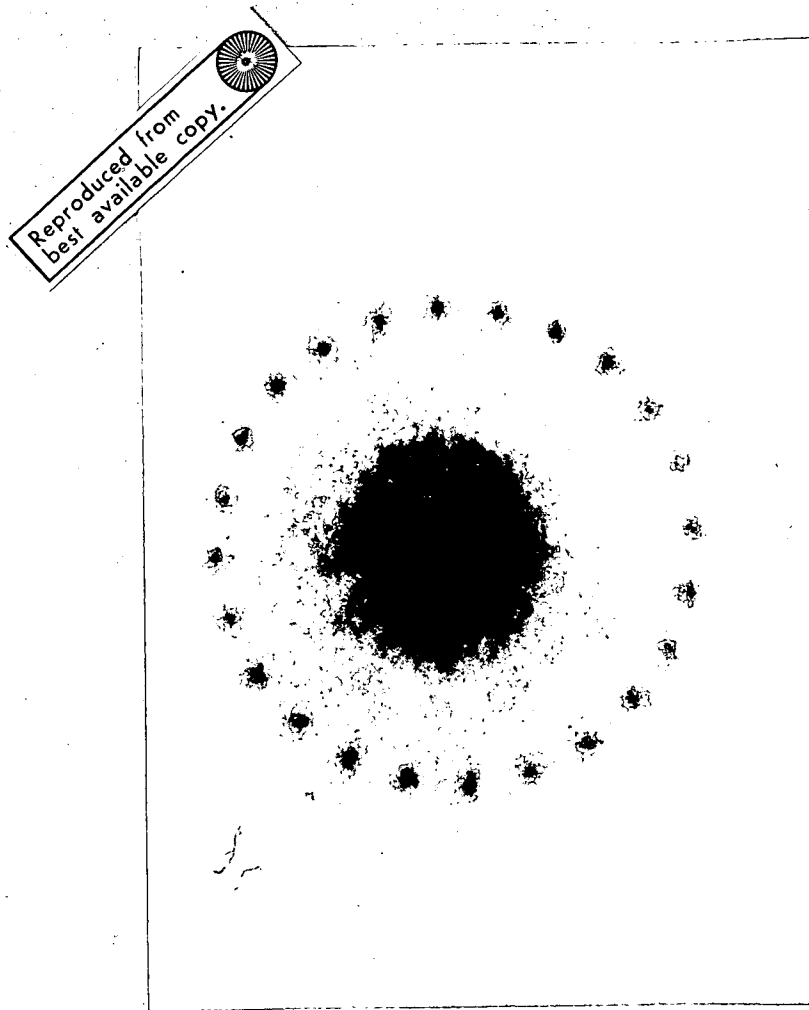


Figure 6. Enlargement (40X) of star exposed through diffraction grating apparatus mounted on MOTS (15 second exposure for each set of diffraction images and 180 second cumulative exposure for central image).

in which,

$\delta x_j, \delta y_j$ = observed departures in x and y from grand mean of averaged coordinates for j th pair of diffraction images,

τ_j = relative time of midpoint of exposure of j th pair of diffraction images

= 15 (j - 1) second (i.e., $\tau_1 = 0, \tau_2 = 15, \dots, \tau_{12} = 165$ seconds),

a_0, b_0 = zero set coefficients,

a_1, b_1 = linear drift coefficients,

a_2, a_3

b_2, b_3 = periodic drift coefficients (90 second period assumed).

Values of the observed $\delta x_j, \delta y_j$ plotted against τ_j are presented in Figures 7 through 12. Also plotted in the same figures are corresponding values of $\delta x_j, \delta y_j$ as computed from the fitted functions.

In reviewing Figures 7 through 12, we find that the departures in right ascension and declination are not randomly distributed about zero, but rather, for the most part, display fairly well defined trends. However, with a few notable exceptions, the fit of the regression functions can be said to be only fair. This is especially clear from the results presented in Table 1 on the following page. These show that goodness of fit indicated by S_x and S_y is generally only modestly better than the dispersion about zero means as indicated by s_x and s_y . Indeed, in a few instances, values of S_x and S_y are slightly larger than their counterparts s_x and s_y , a result attributable to the fewer degrees of freedom associated with the residuals from the fitted functions (i.e., 8 degrees of freedom are associated with S_x, S_y , whereas 11 are associated with s_x, s_y).

It will be noted that the values of s_x and S_x for plate 6 are exceptionally large (9.1 and $7.8\mu\text{m}$, respectively). Referring to the plotted results in Figure 12, we see the presence of two pronounced jumps in the trends as indicated by the heavy arrows. To make sure that these jumps were actually real and not the result of a measuring or recording

Table 1. RMS values of x and y drifts before and after regression.

Plate	RMS Values Before Regression (μm)		RMS Values After Regression (μm)	
	s_x	s_y	S_x	S_y
1	3.4	2.5	2.4	1.8
2	3.5	2.3	3.4	1.8
3	4.0	1.7	3.7	1.9
4	5.3	2.3	4.3	1.1
5	3.2	2.1	3.3	1.9
6	9.1	2.3	7.8	2.2

$$s_x = \left[\frac{\sum \delta x_j^2}{11} \right]^{\frac{1}{2}} \qquad S_x = \left[\frac{\sum (\delta x_j - \delta x'_j)^2}{8} \right]^{\frac{1}{2}}$$

$$s_y = \left[\frac{\sum \delta y_j^2}{11} \right]^{\frac{1}{2}} \qquad S_y = \left[\frac{\sum (\delta y_j - \delta y'_j)^2}{8} \right]^{\frac{1}{2}}$$

$\delta x_j, \delta y_j$ = observed values
 $\delta x'_j, \delta y'_j$ = values computed from regression

PLATE NO. 1

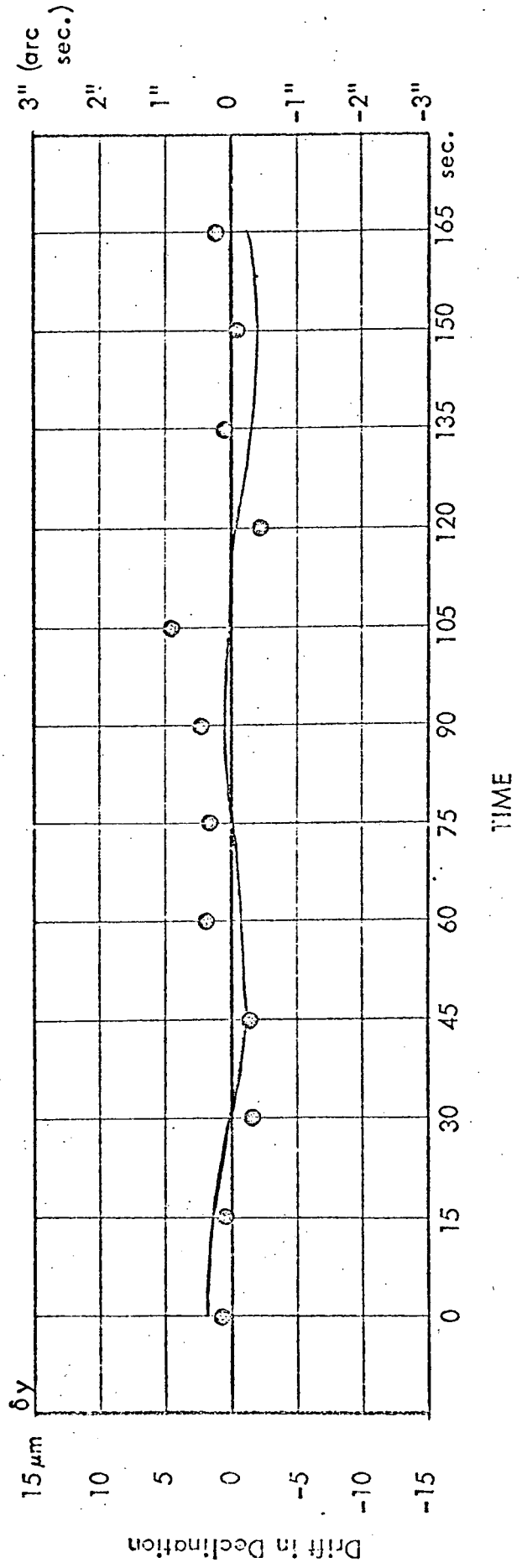
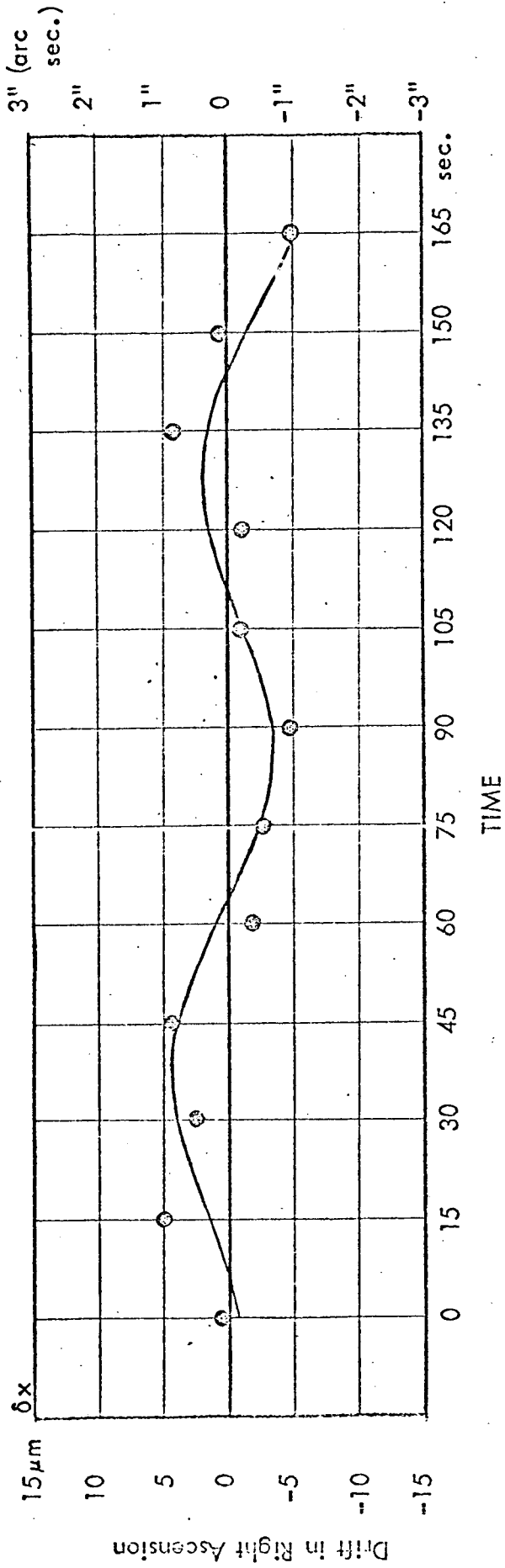


Figure 7 . MOTS drift as indicated by rotating diffraction grating, plate no. 1 .

PLATE NO. 2

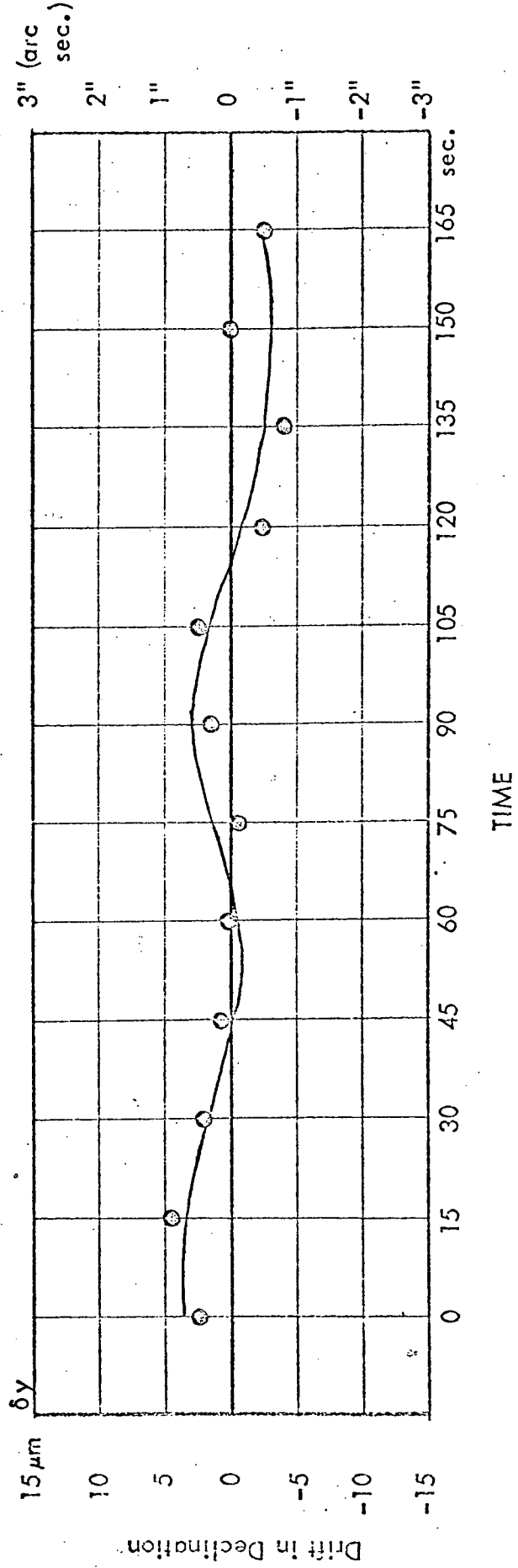
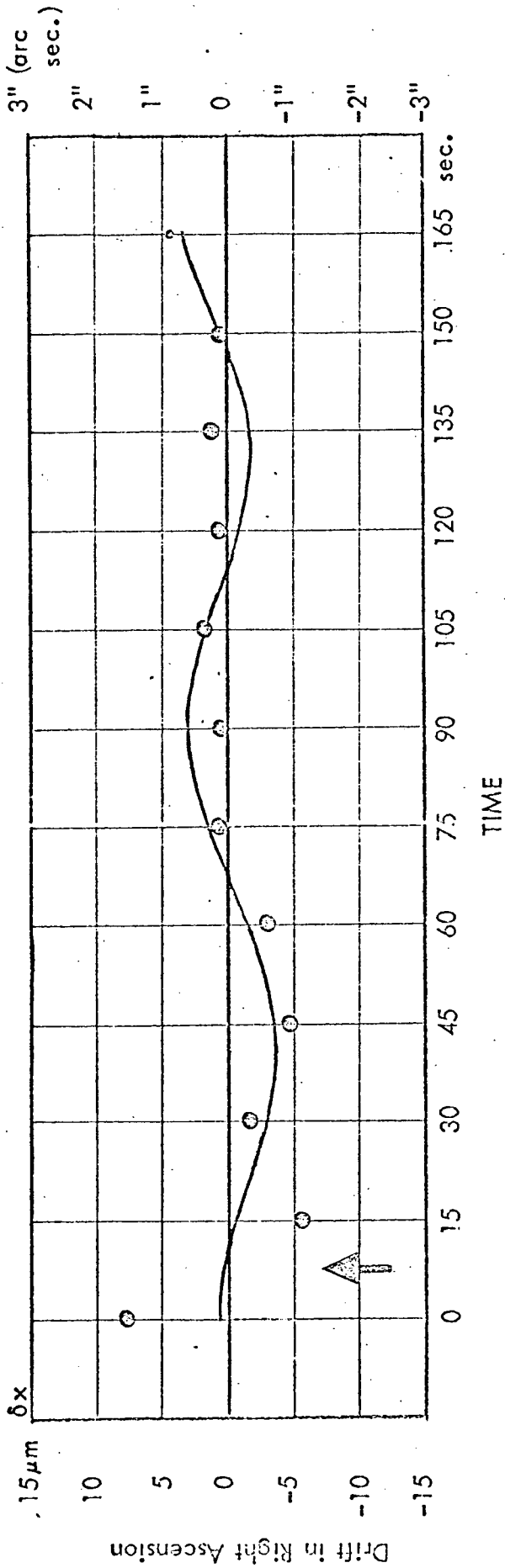


Figure 8 . MOTS drift as indicated by rotating diffraction grating, plate no. 2 .

PLATE NO. 3

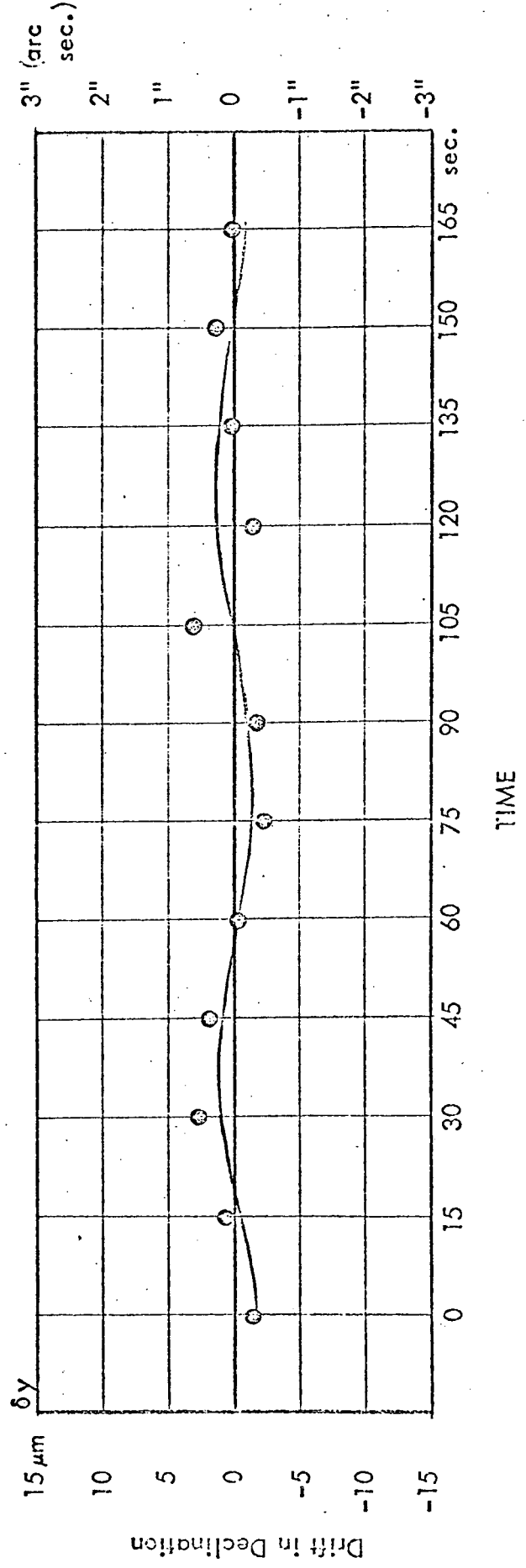
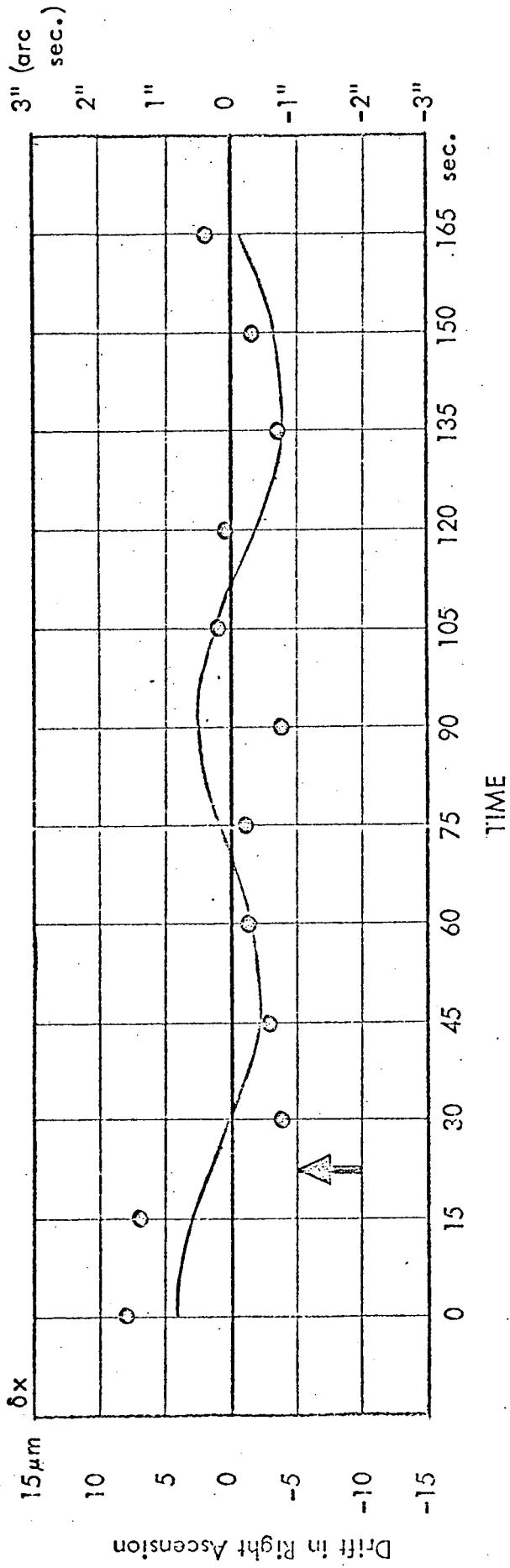


Figure 9 . MOTS drift as indicated by rotating diffraction grating, plate no. 3 .

PLATE NO. 4

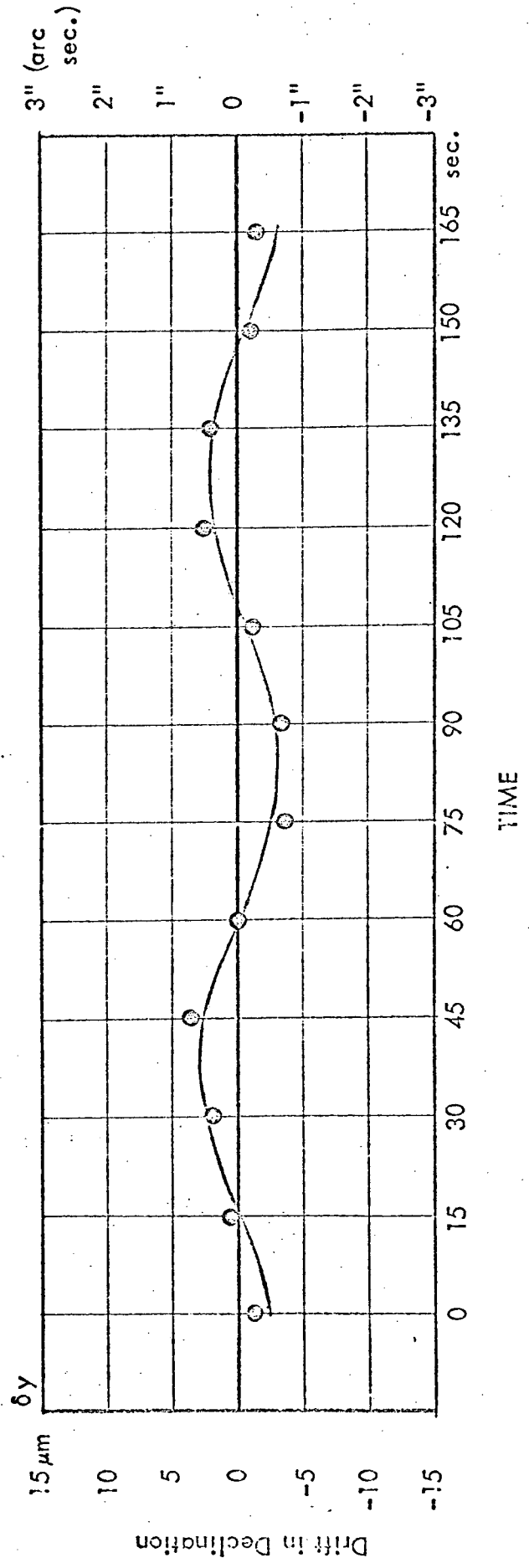
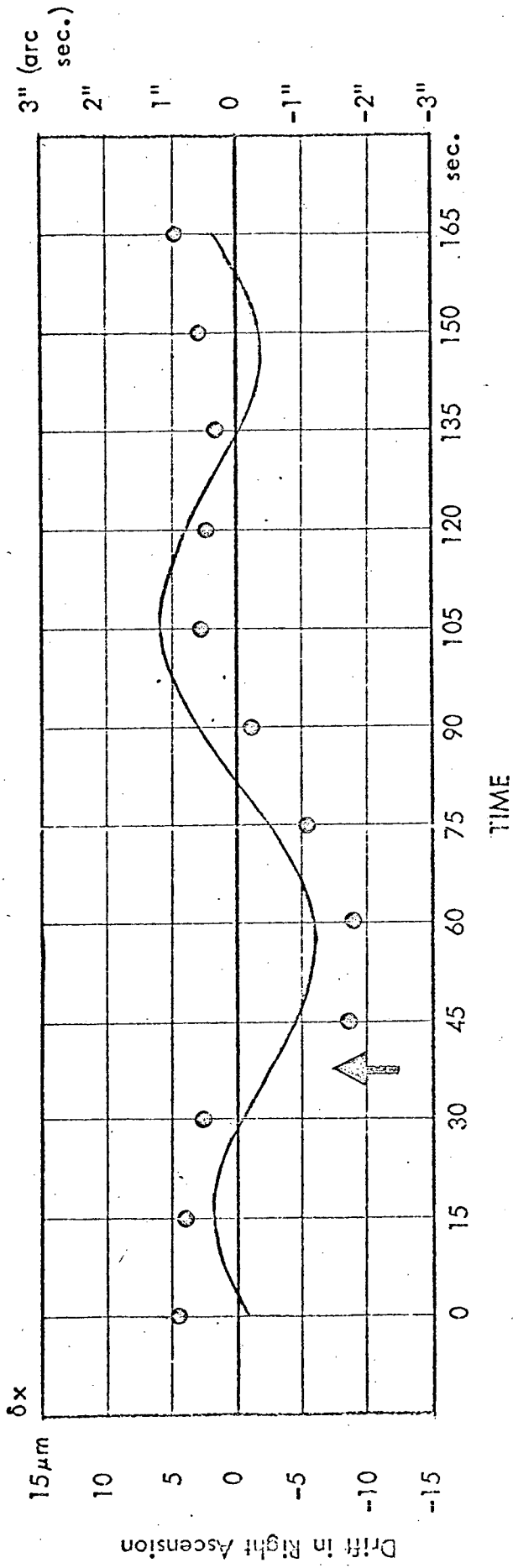


Figure 10. MOTS drift as indicated by rotating diffraction grating, plate no. 4 .

PLATE NO. 5

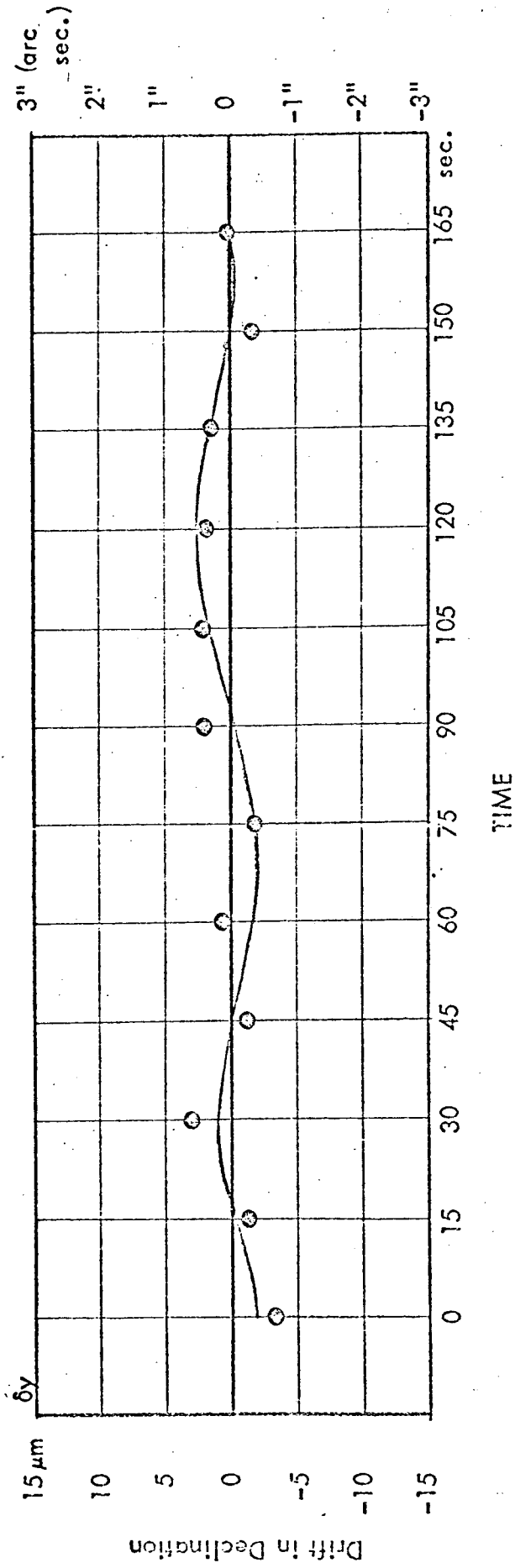
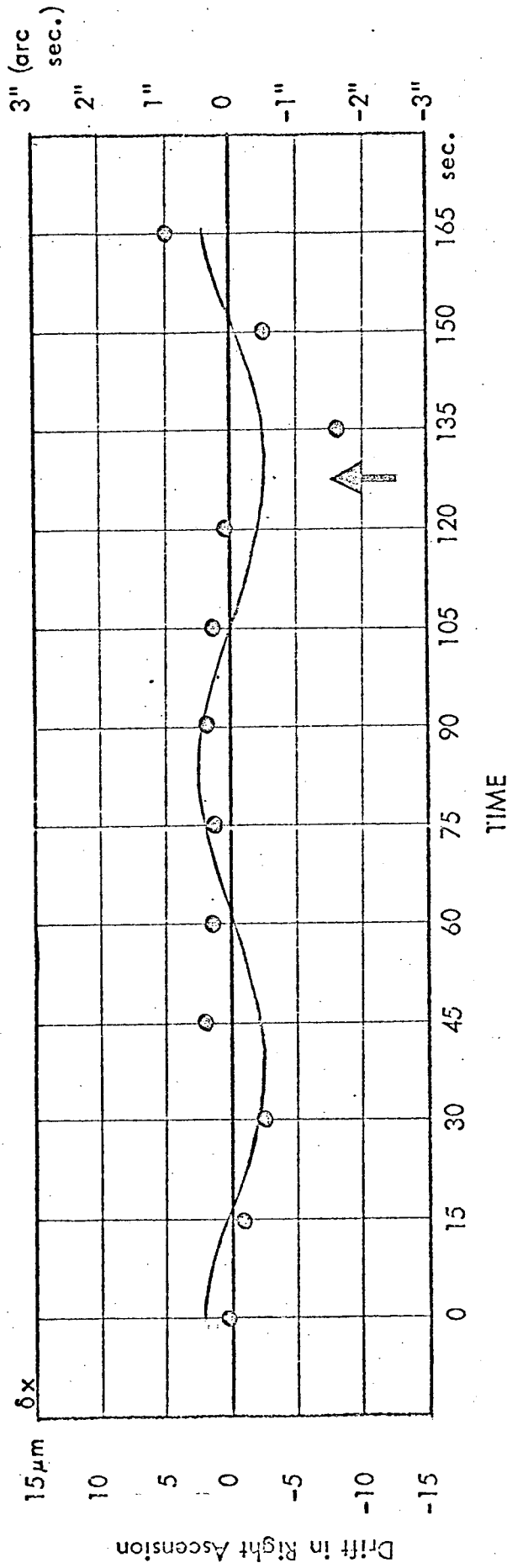


Figure 11 . MOTS drift as indicated by rotating diffraction grating, plate no. 5 .

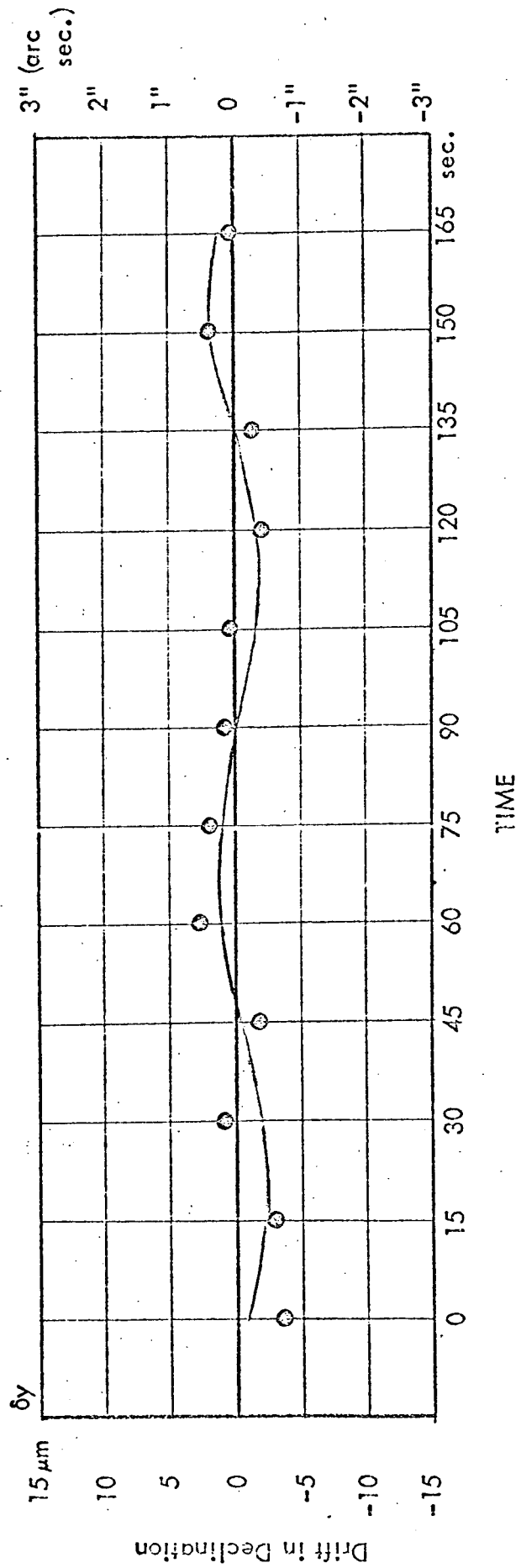
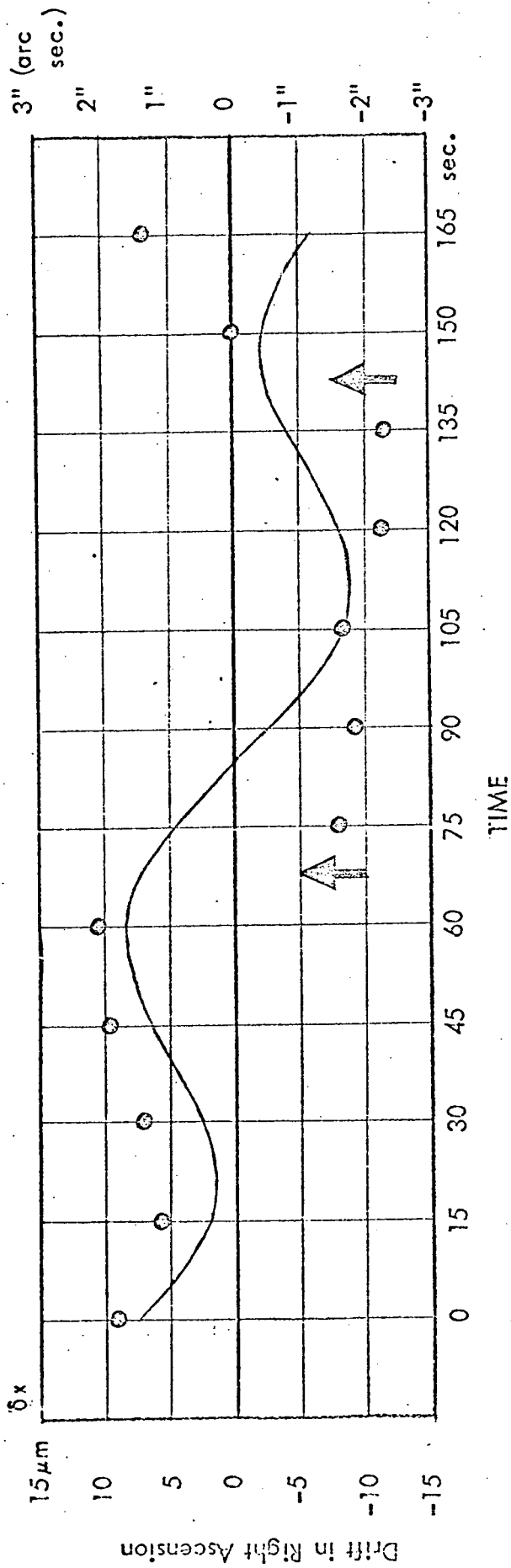


Figure 12. MOTS drift as indicated by rotating diffraction grating, plate no. 6 .

PLATE NO. 6

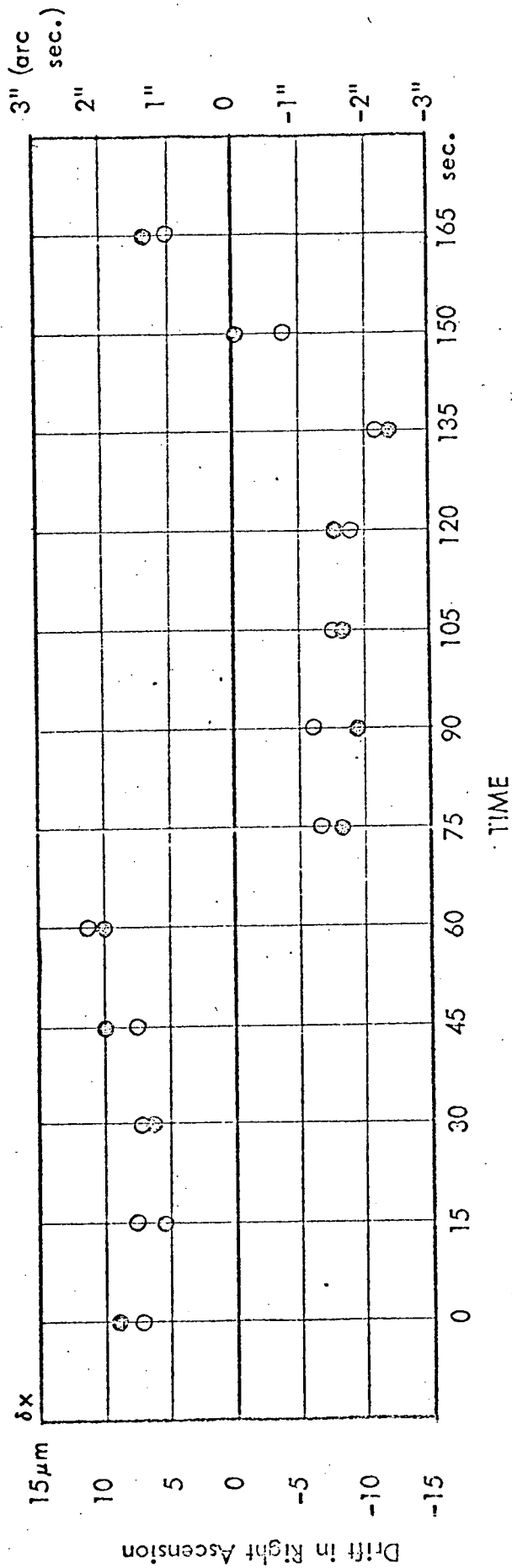


Figure 13. Comparison of original measurements of drift in right ascension for plate 6 with remeasurements made on different comparator by different operator.

blunder, we had plate 6 remeasured by another operator on another comparator (namely, the DBA multilaterative comparator). Comparative results presented in Figure 13 show good agreement between the two sets of measurements and verify that the jumps are indeed real. Reviewing the plots for the other plates, we find indications of similar jumps occurring on Plates 2, 3, 4 and 5 at the points indicated by the arrows in Figures 8, 9, 10 and 11. These suggest the presence of stiction in the drive train. Stiction being the occasional slight binding of the gears followed by sudden release. Whether or not this is the correct explanation for the abrupt changes remains to be determined. For convenience, we shall nonetheless refer to the abrupt changes as 'stiction jumps'.

It seemed that the generally mediocre fits obtained from the regressions performed on δx could well be attributable to the compromising effect of stiction jumps. To test this hypothesis we revised the regression model so that the single zero set term a_0 was replaced by the expression:

$$\xi_1 a_0 + \xi_2 a_0' + \xi_3 a_0''$$

in which,

$$\begin{aligned} \xi_1 &= 1 \text{ for } \tau_1 < T_1 \\ &= 0 \text{ for } \tau_1 > T_1 \end{aligned}$$

$$\begin{aligned} \xi_2 &= 1 \text{ for } T_1 < \tau_1 < T_2 \\ &= 0 \text{ otherwise} \end{aligned}$$

$$\begin{aligned} \xi_3 &= 1 \text{ for } \tau_1 > T_2 \\ &= 0 \text{ otherwise.} \end{aligned}$$

This artifice makes it possible to reinitialize the zero set term up to two times per plate. When no reinitializations are desired, we need merely set T_1 and T_2 to values greater than the maximum value of τ_1 (say to 180 seconds). The values of T_1 and T_2 adopted in the revised regressions for δx are as indicated in the following table.

Plate	Number of Stiction Jumps	T_1	T_2	Degrees of Freedom For Regression
1	0	180	180	8
2	1	7.5	180	7
3	1	22.5	180	7
4	1	37.5	180	7
5	1	127.5	180	7
6	2	67.5	142.5	6

The results of the revised regressions are plotted in Figures 14 through 19. The results for Plate 1 are unchanged, which is as it should be, since no stiction jumps were exercised. Results for the remaining plates represent substantial improvements over those from the original regressions. The fitted functions now very closely follow the observed values. This is verified by Table 2 in which Table 1 is extended to reflect the results of the revised regressions. The grand rms value for the fit in δx for all six plates is $2.1 \mu\text{m}$, a value only insignificantly greater than the grand rms of $1.8 \mu\text{m}$ for y .

The amplitude of the periodic error from the revised regressions averages about 0.6 second of arc in right ascension and about 0.4 second of arc in declination. This is appreciably lower than the values considered typical (i.e. 2 to 3 arc seconds in right ascension) in Reference 2. However, specific results from the MOTS at Fort Myers were not reported in Reference 2.

1.6 GENERAL CONSIDERATIONS

When stiction jumps are duly taken into account whenever they occur, excellent fits are obtained from the simple regression model that was adopted. This demonstrates the effectiveness of the rotating diffraction grating as a means for monitoring the stability of the MOTS camera throughout routine operations.

Because of the exploratory nature of our investigation, we took the liberty of ignoring a few fine points that should be implemented when the diffraction data are actually to be used to generate corrections applicable to satellite observations. Because

Table 2. Extension of Table 1 to include results of revised regressions.

Plate	RMS Values Before Regression (μm)		RMS Values After Original Regression (μm)		RMS Values After Revised Regression (μm)	
	s_x	s_y	S_x	S_y	S'_x	S'_y
1	3.4	2.5	2.4	1.8	2.4	1.8
2	3.5	2.3	3.4	1.8	1.5	1.8
3	4.0	1.7	3.7	1.9	2.0	1.9
4	5.3	2.3	4.3	1.1	1.4	1.1
5	3.2	2.1	3.3	1.9	2.8	1.9
6	9.1	2.3	7.8	2.2	2.0	2.2

$$s_x = \left[\frac{\sum \delta x_j^2}{11} \right]^{\frac{1}{2}}$$

$$s_y = \left[\frac{\sum \delta y_j^2}{11} \right]^{\frac{1}{2}}$$

$$S_x = \left[\frac{\sum (\delta x_j - \delta x_j')^2}{8} \right]^{\frac{1}{2}}$$

$$S_y = \left[\frac{\sum (\delta y_j - \delta y_j')^2}{8} \right]^{\frac{1}{2}}$$

$$S'_x = \left[\frac{\sum (\delta x_j - \delta x_j'')^2}{f} \right]^{\frac{1}{2}}$$

$$S'_y = \text{same as } S_y$$

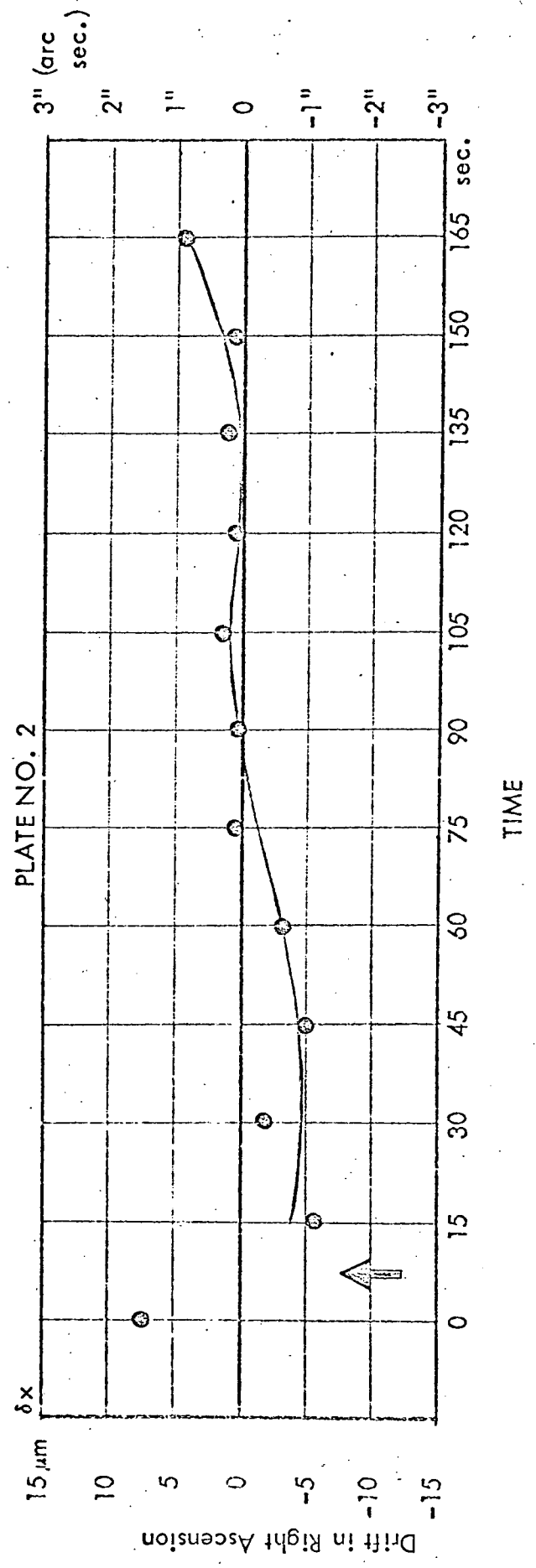
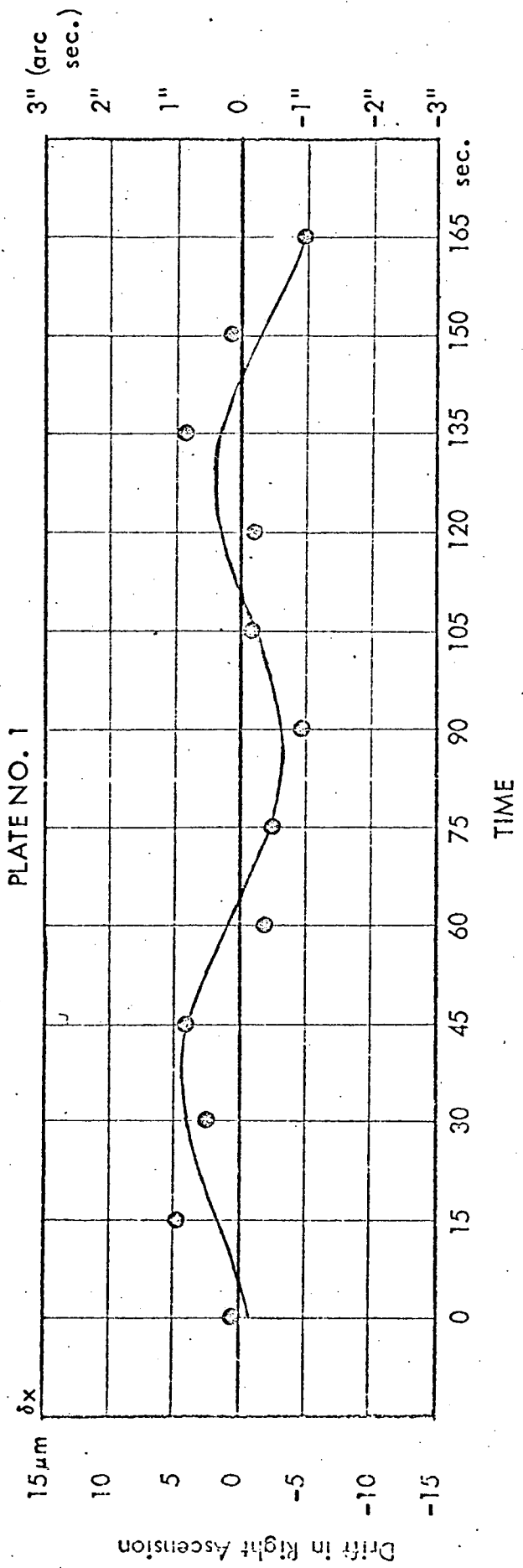
$\delta x_j, \delta y_j$ = observed values

$\delta x_j', \delta y_j'$ = values computed from original regression

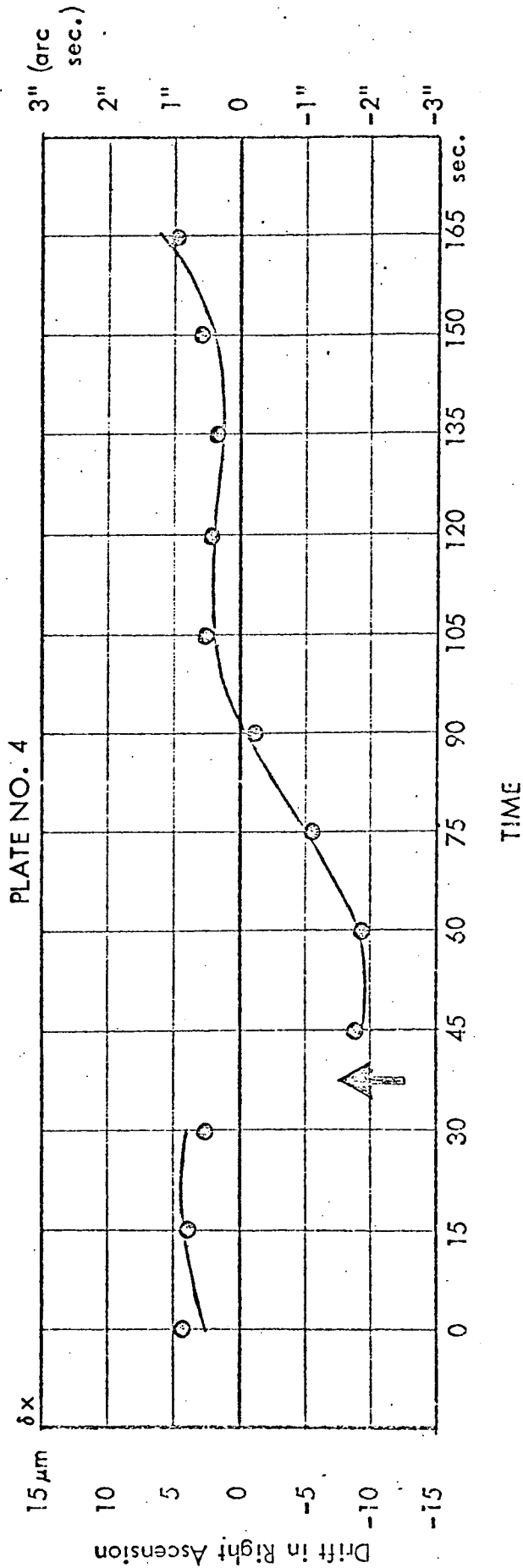
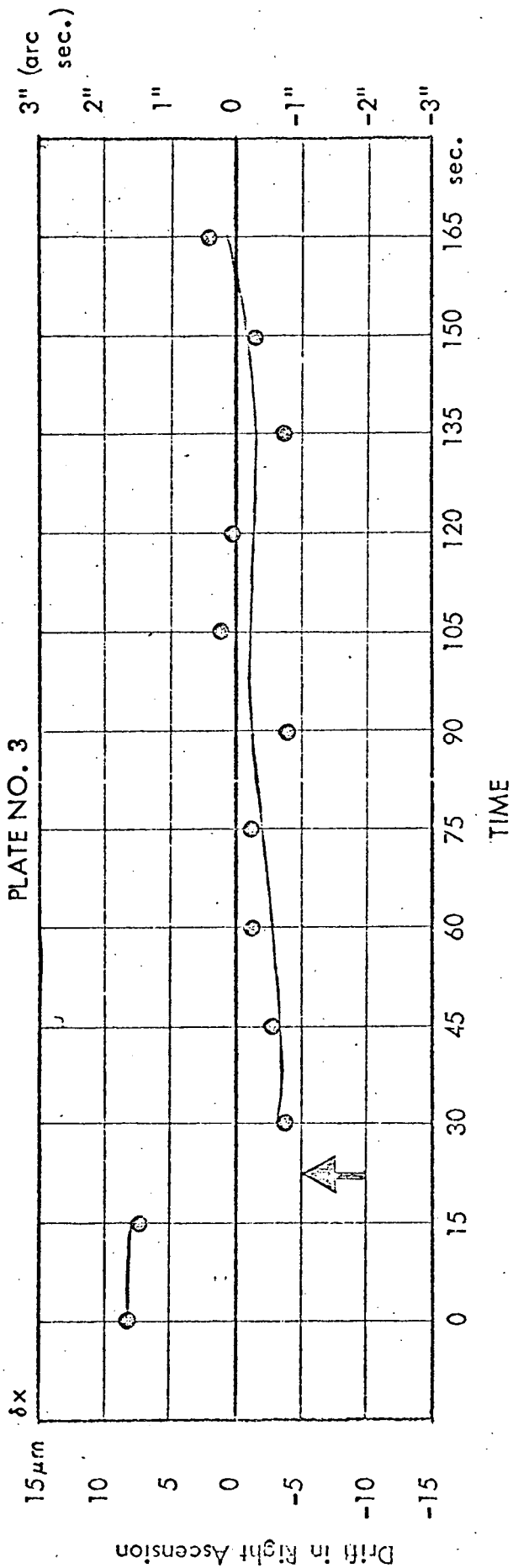
$\delta x_j'', \delta y_j''$ = values computed from revised regression

f = degrees of freedom

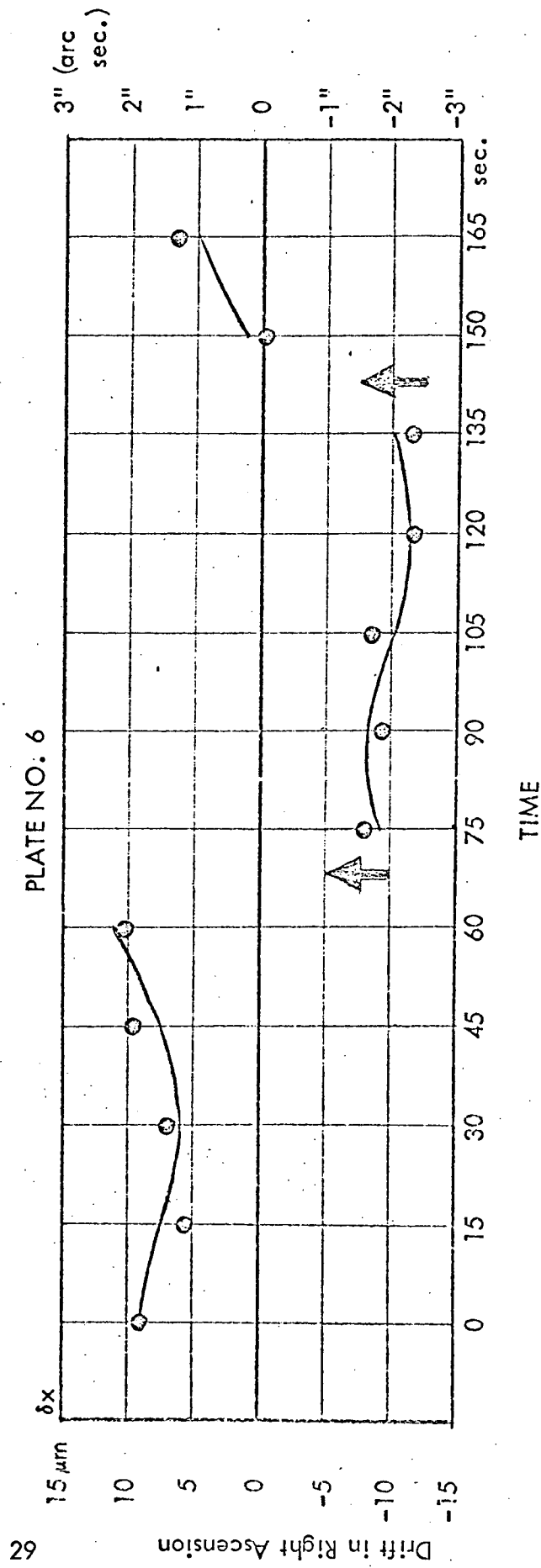
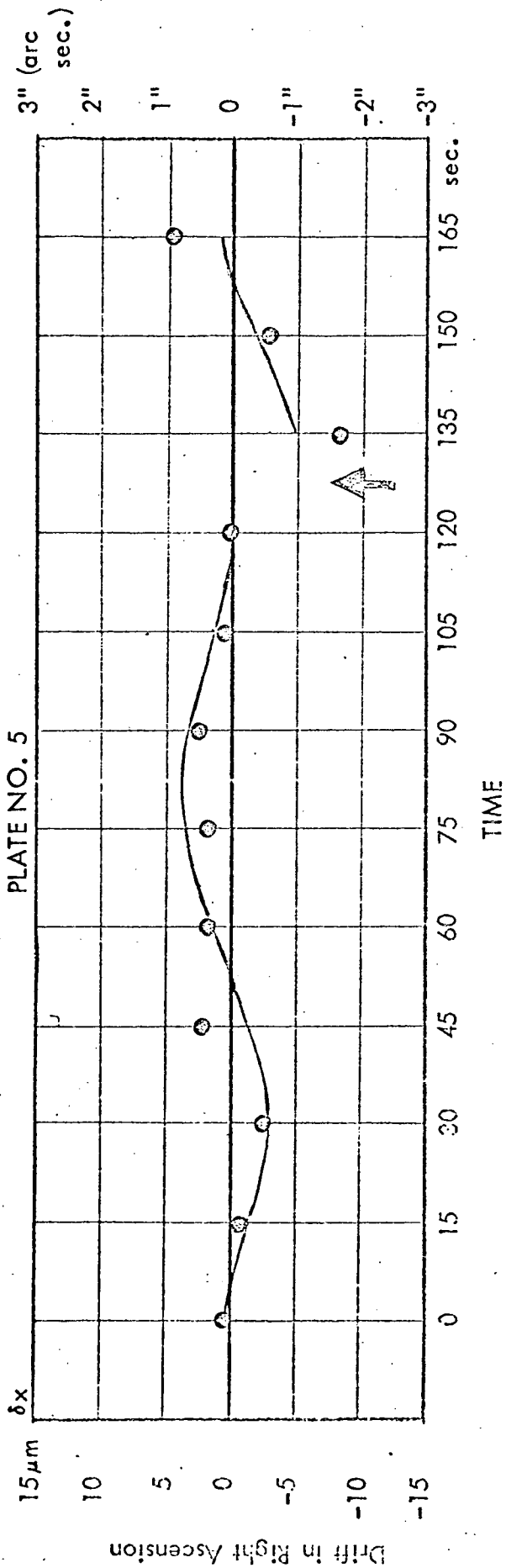
= 8, 7 or 6 depending on number of stiction jumps



Figures 14 and 15. Plots showing fit from revised regressions in right ascension, plates 1 and 2.



Figures 18 and 19. Plots showing fit from revised regressions in declination, plates 3 and 4.



Figures 16 and 17. Plots showing fit from revised regressions in right ascension, plates 5 and 6.

the length of each exposure through the grating may be a significant fraction of the 90 second period of the drive, the integrated effect of the drift over exposure increments should be recognized as being what is actually observed. Accordingly, if 2Δ denotes the length of each exposure through the grating, the expression

$$a_2 \sin \frac{2\pi}{90} \tau_1 + a_3 \cos \frac{2\pi}{90} \tau_1$$

in the formula for δx_1 , for example, should more properly be replaced by the expression

$$\frac{1}{2\Delta} \int_{\tau_1 - \Delta}^{\tau_1 + \Delta} [a_2 \sin \frac{2\pi}{90} t + a_3 \cos \frac{2\pi}{90} t] dt.$$

However, this reduces to the form

$$a_2' \sin \frac{2\pi}{90} \tau_1 + a_3' \cos \frac{2\pi}{90} \tau_1$$

in which

$$a_2' = K a_2$$

$$a_3' = K a_3$$

where

$$K = \left(\sin \frac{2\pi}{90} \Delta \right) / \left(\frac{2\pi}{90} \Delta \right).$$

Thus, while a_2' and a_3' are the values actually obtained from the least squares regression, the values to be used in the correction formulas should be a_2, a_3 which will, of course, be slightly larger. For $2\Delta = 15$ seconds (the value used in our experimental investigation), the value of K is $(\sin \pi/6)/(\pi/6) = 0.956$, which means that the amplitudes obtained from the regressions should be increased by a factor of $1/0.956 = 1.044$.

The second fine point to be considered in operational applications of the diffraction grating concerns effects induced by changes in atmospheric refraction resulting from the gradual changes in zenith distance occurring throughout the operation. Even if the MOTS were perfectly stable in the right ascension-declination frame, the gradual change in refraction with change in zenith distance would be manifested as a secular drift if appropriate corrections were not applied. In Reference 3 we showed that the correction for this effect is given by:

$$d(\Delta\zeta) = 4.5 \times 10^{-3} t_i \sin A_i \cos \Phi \sec^2 \zeta_i$$

(arc sec)

in which, for the present application,

$d(\Delta\zeta)$ = angular correction to be applied zenith distance of mean of pair of diffraction images

t_i = time of exposure of i th set of diffraction images relative to mean time of total exposure

A_i = azimuth of star at t_i

ζ_i = zenith distance of star at t_i

Φ = latitude of station.

By means of standard astronomical formulas, this correction for zenith distance can be propagated into right ascension and declination and thence into x, y plate coordinates. It is the corrected x, y coordinates that properly should be employed in the diffraction grating regressions.

1.7 CONCLUSIONS AND RECOMMENDATIONS

The diffraction grating apparatus evolved from this study has proven to provide a simple, inexpensive, effective, and operationally unobtrusive means for monitoring the stability of the MOTS camera to a precision of a few tenths of a second of arc.

We recommend that NASA employ the breadboard apparatus developed by DBA in further tests on other MOTS cameras, particularly those that are known to be affected by larger drift errors than the MOTS at Ft. Myers. Should these tests confirm the promise of the approach, NASA should undertake the procurement of operationally optimized units to be used routinely in future operations at all MOTS stations. Such units should preferably be controlled by an automatic programmer with a suitable range of selectable exposure rates.

While the diffraction grating method provides a way of correcting for drift in future MOTS operations, the question naturally arises as to whether anything can be done about the many hundreds of plates gathered on past operations, particularly on GEOS I and GEOS II. We believe that quite possibly something effective can be done. Because a formal standardized procedure was followed in the exposure of GEOS plates, a fairly high level of repeatability of drive error may well exist. In any event, whether or not this is the case can be determined experimentally by employing the grating in repeated trials simulating GEOS operations. If acceptably repetitive results are obtained for a given camera, a pooled result can be used to derive corrections to be applied to directions obtained from previous plates taken by the camera. The validity of such corrections can be tested by determining whether or not improved residuals are generally obtained from short arc reductions based on revised directions.

1.8 REFERENCES

- [1] Brown, D., "Advanced Methods for the Calibration of Metric Cameras," final report, Contract No.: DA-44-009-AMC-1457(X), U.S. Army Engineering Topographic Laboratories, Fort Belvoir, Virginia, 9 December 1968.
- [2] Harris, D., Cartwright, M., Oosterhaut, J., "Analysis of the MOTS Camera Drive," GSFC Report X-514-69-482, November 1969.
- [3] Brown, D., Hartwell, J., Stephenson, J., "Geodetic Data Analysis for GEOS A, An Experimental Design," final report prepared for NASA Goddard under Contract No. NAS5-9860, November 1965.

SECTION 2

MINITRACK DATA REDUCTION

2.1 INTRODUCTION

This section covers work done by DBA Systems, Inc., over a 2-year period. Work for the contract was initially being performed by the DBA Florida Office. In order to provide better liaison between NASA and DBA, it was decided to transfer the project to the DBA Washington Office. This was done nine months after the start of the contract. The section dealing with the Minitrack geometrical error model, contributed by James B. Willmann, was written prior to the transfer of the project to Washington. Several thousand NAP (Network Analysis Program-II) control cards for processing optical orbits had also been prepared, but this work became largely redundant after the development of a new optical preprocessing program.

After the project was transferred to Washington, work was concentrated on calibrating Minitrack using short optically determined reference arcs. This was done in order to demonstrate the feasibility of using the NAP program for the purpose of calibrating Minitrack. At this time too, the magnitude of the Doppler effect was being investigated, and the relevant equations were implemented into the NAP program.

Concurrently, the new optical preprocessing program, already mentioned, was developed. The reason for writing a new optical preprocessing program was that the old program could not process data for SAO stations and required an enormous amount of data preparation. The new program in addition would punch out most of the NAP control cards.

Twelve months after the start of the contract, work began on the calibration of Minitrack using Minitrack data only. Initially, little progress was made. At this time the Minitrack extract and sort programs were developed. The Minitrack preprocessor was modified to punch out most of the NAP control cards. After three months, it was found that the NAP program had been requested to compute and apply the effect of the earth's precession and nutation. Unfortunately, an error was known

to exist in these computations. After the NAP control cards were changed, so as not to request these computations, progress was again made. (To the order of the accuracy of the Minitrack system, it would not appear to be necessary to consider precession and nutation. However, because of the surprisingly good agreement between orbits determined from Minitrack and optical data, this point of view may have to be modified).

Definite but slow progress was now being made. A post NAP program-- later extensively modified-- was written to summarize the results of the NAP program. This also involved modifications to NAP subroutines RESID and FINALP.

About 17 months after the start of the contract, the contract Technical Monitor (W. M. Rice) proposed an analysis of the NAP program by Boole & Babbage, Inc., to determine the feasibility (within the time scale of the contract) of increasing the computational speed of NAP and hence the overall rate of progress. The analysis showed that the majority of the computing time was being spent in a few relatively short subroutines. A new algorithm was then developed for the computation of spherical harmonics and this was implemented into NAP. The modifications to the NAP program doubled its overall computational speed.

Advantage was now taken of the faster NAP program, the length of arc considered was increased from 2.5 to 5 days; however, this led to further problems. A meeting was called by E. P. Damon of the Computer Systems Branch to call attention to the amount of computer disk space being required by the NAP program. (As the length of arc had been doubled, so had the amount of data being stored on disk memory). We had, however, become aware of the problem before the above mentioned meeting because of the frequently aborted runs due to non-availability of enough disk space. To overcome this problem, the special subroutines PRTIAL and RESID were written and the NAP disk space requirements were substantially reduced. The post-NAP program was modified to be consistent with the latest NAP program.

With the increasing amount of data being processed on each run, the number of NAP control cards became very large and it was decided to write them on tape. To handle modifications to individual NAP "cards" the pre-NAP card updater program was written.

In checking out the new special subroutine PRTIAL a discrepancy was discerned in the printed out time. This was traced back to the Minitrack preprocessing program, which was corrected. All Minitrack data used in the data processing now had to be reprocessed.

At about 21 months from the start of the contract it was decided to investigate the puzzlingly slow rate of convergence of the solutions computed by NAP. The investigation revealed that the NAP matrix inversion was not being handled as described in the NAP documentation but in an iterative manner, which was extremely time consuming for the long arcs being considered. The complete equations as given in the existing NAP documentation were incorporated into NAP by R. Garza-Robles of Goddard Space Flight Center (Code 551). The rate of convergence was at least doubled.

With the help of the support programs already described and with the modified NAP program a four-arc run was now made on the 360/95. The total time span covered was 25 days and the computer time taken was 20 minutes. (At the start of this program, one 2.5 day arc was processed in 24 minutes and then the convergence rate of the solution was half of its present rate). "Optical" reference arcs were computed for the same time spans and a comparison of results was made. Advantage was taken of the current DBA contract (NAS5-11730) to develop an ionospheric error model for incorporation in the NAP program and one run was made using ionospheric corrections.

It should also be mentioned that the NAP-II program was successfully overlaid reducing its core requirements from 700,000 to 500,000 bytes.

This section is devoted to discussion of the reduction of Minitrack data using the NAP-II program and auxiliary programs written specifically for this task. Included in this section are discussions of the Minitrack error model and the Doppler effect and wave-propagation time delay as applied to predicted Minitrack measurements.

The second and third parts of this section discuss the handling and preprocessing of the Minitrack and Optical data respectively. The fourth part is devoted to the reduction of the data using the NAP-II program.

Results for a reduction effort are given in the fifth part. Results are given for the station at Ft. Myers and then a multi-station network which includes all of the Minitrack stations.

The last part of this section is a recommended procedure for reducing Minitrack data on a production basis.

As of special note: Appendix A-4 should be continuously referenced in the data processing cycle, as it contains restrictions on the programs and assumptions pertaining to the data.

2.1.1 The Minitrack Geometrical Error Model

This discussion will consider some of the general geometric properties of the Minitrack system. As with any interferometer system, the basic measurement mode is that of the phase path difference between the target and two antennas located some distance apart. The line between the antennas is referred to as the base line. The geometry for two cases is depicted below; 'A' for a target at a close range, and 'B' for a target at infinity.

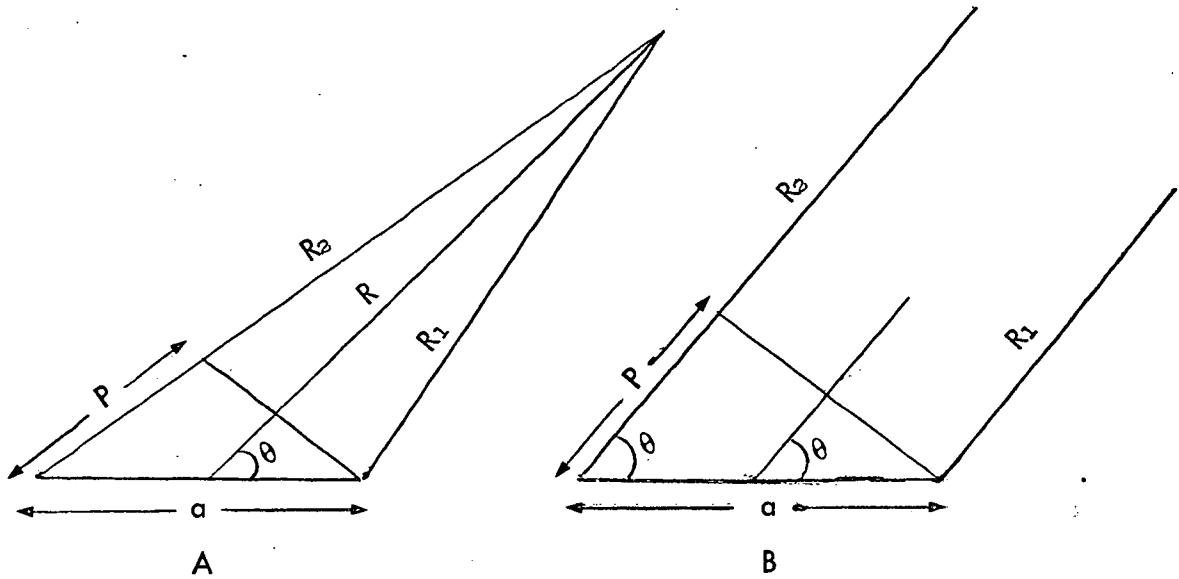


Figure 1

In Figure (1), A and B, the antennas are at the end of the base line a . The measurement made by the system can be interpreted as being proportional to the distance P . In both cases, P is defined as

$$P = R_2 - R_1 .$$

Generally, we say that the system measures the cosine of the angle θ since

$$\cos \theta \approx \frac{P}{a} .$$

For the case of a point at infinity, the above expression is exact. For the case depicted in Figure 1A, it is only approximately true and $\cos \theta$ depends upon R as well as P and a .

For the Minitrack system, there are four antennas located at the ends of two perpendicular base lines. These base lines are usually located to intersect each other at their centers. However, since exact location of the phase centers of the antennas is not possible, there will be errors in the resulting data if they are interpreted as a true measurement of the cosine of the direction to the target. Therefore, the discussion which follows will investigate two areas. First, we will derive the relationship between the angle θ and the measurement P . Then, we will investigate errors in the antenna locations and how they effect the interpretation of the data.

To derive the desired expression, we can refer to Figure 1A. From this figure, the following relationships can be written.

$$\begin{aligned} P &= R_2 - R_1 \\ R_1^2 &= R^2 + \left(\frac{a}{2}\right)^2 - R a \cos \theta \\ R_2^2 &= R^2 + \left(\frac{a}{2}\right)^2 + R a \cos \theta \end{aligned}$$

We will redefine the measurement as

$$l_0 = \frac{P}{a} = \frac{R_2 - R_1}{a}$$

Then l_0 approximates the cosine of θ . Proceeding with the algebra, give

$$\begin{aligned} P^2 + 2PR_1 + R_1^2 &= R_2^2 \\ P^2 + 2PR_1 - 2Ra \cos \theta &= 0 \\ (P^2 - 2Ra \cos \theta)^2 &= 4P^2 R_1^2 = 4P^2 \left(R^2 + \frac{a^2}{4} - Ra \cos \theta\right) \\ P^4 + 4R^2 a^2 \cos^2 \theta &= 4P^2 R^2 + P^2 a^2 \end{aligned}$$

solving for $\cos \theta$ give

$$\cos \theta = l_0 \sqrt{1 + \frac{a^2}{4R^2} (1 - l_0^2)}$$

the desired result. Note that as $R \rightarrow \infty$ then $l_0 \rightarrow \cos \theta$. Expanding gives

$$\cos \theta = l_0 + \frac{a^2}{8R^2} l_0 (1 - l_0^2) \dots$$

The maximum error in assuming $\cos \theta = l_0$ occurs when l_0 is approximately $1/\sqrt{3}$. This leads to a maximum error of about

$$\cos \theta - l_0 \approx \frac{a^2}{20R^2} .$$

For this analysis, we will consider the three dimensional case pictured in Figure (2). The antennas are located along the x and y base lines which are approximately a and b in length. We will then relate the path difference measurements to the desired cosines as a function of a , b and the errors in antenna location. This is pictured below.

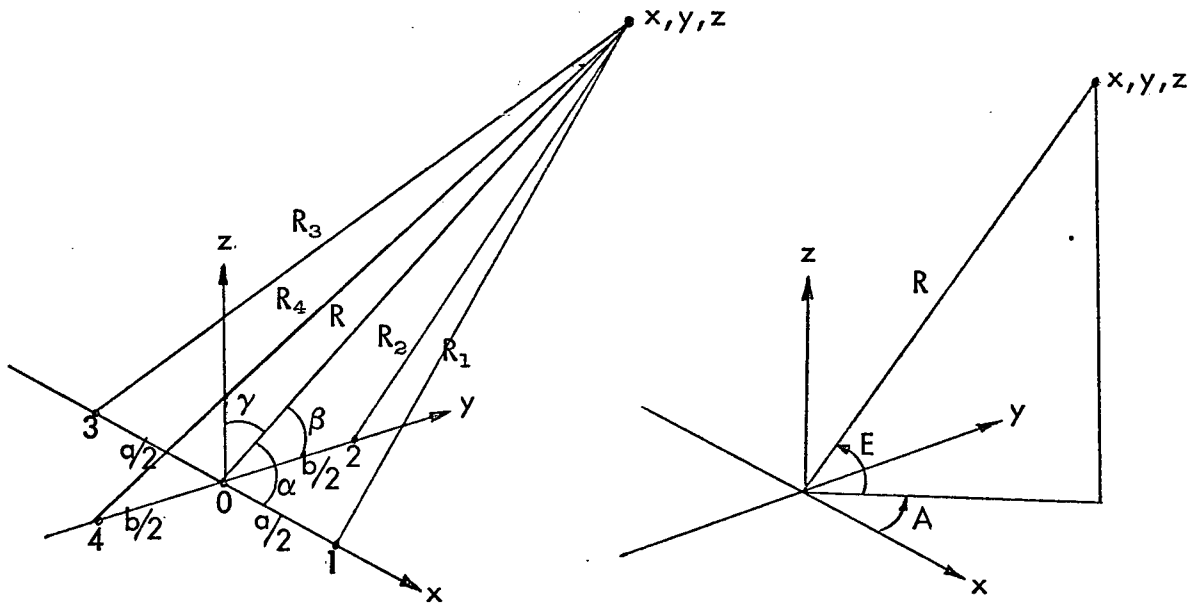


Figure 2

We have also included a figure which defines the measurements of azimuth and elevation. First a few definitions.

$$l = \cos \alpha$$

$$m = \cos \beta$$

$$n = \cos \gamma = \sqrt{1 - \cos^2 \alpha - \cos^2 \beta} = \sqrt{1 - l^2 - m^2}$$

$$x = R \cdot l = R \cdot \cos A \cos E$$

$$y = R \cdot m = R \cdot \sin A \cos E$$

$$z = R \cdot n = R \cdot \sin E$$

Thus,

$$\tan A = m/l ; \quad \cos E = \sqrt{l^2 + m^2} .$$

The measurements made by the system are given by

$$P = R_3 - R_1 = \sqrt{(x + \frac{a}{2} - x_3)^2 + (y - y_3)^2 + (z - z_3)^2} \\ - \sqrt{(x - \frac{a}{2} - x_1)^2 + (y - y_1)^2 + (z - z_1)^2}$$

$$Q = R_4 - R_1 = \sqrt{(x - x_4)^2 + (y + \frac{b}{2} - y_4)^2 + (z - z_4)^2} \\ - \sqrt{(x - x_2)^2 + (y - \frac{b}{2} - y_2)^2 + (z - z_2)^2} .$$

In the above, we have chosen the coordinates of the antennas to be

$$1 \quad x_1 + a/2, y_1, z_1$$

$$2 \quad x_2, y_2 + b/2, z_2$$

$$3 \quad x_3 - a/2, y_3, z_3$$

$$4 \quad x_4, y_4 - b/2, z_4 .$$

In the case where there are no errors, then $x_1, y_1, \dots, y_4, z_4$ would all be zero. In that case, if P_0 is the value of P when all survey errors are zero, then

$$P_0 = \sqrt{(x + a/2)^2 + y^2 + z^2} - \sqrt{(x - a/2)^2 + y^2 + z^2} \\ = \sqrt{R^2 + ax + a^2/4} - \sqrt{R^2 - ax + a^2/4}$$

and

$$Q_0 = \sqrt{R^2 + by + b^2/4} = \sqrt{R^2 - by + b^2/4}$$

The solution to these two equations is the same as that presented in Section II. That is

$$\begin{aligned} \ell &= \frac{P_0}{a} \sqrt{1 + \frac{a^2}{4R^2} \left(1 - \frac{P_0^2}{a^2}\right)} = \frac{P_0}{a} + \frac{a^2}{8R^2} \frac{P_0}{a} \left(1 - \frac{P_0^2}{a^2}\right) + \dots \\ m &= \frac{Q_0}{b} \sqrt{1 + \frac{b^2}{4R^2} \left(1 - \frac{Q_0^2}{b^2}\right)} = \frac{Q_0}{b} + \frac{b^2}{8R^2} \frac{Q_0}{b} \left(1 - \frac{Q_0^2}{b^2}\right) + \dots \end{aligned}$$

However, of more importance is the effect on ℓ and m when the errors in antenna location are not zero. To explore this, we can expand the equations for P and Q about $x_1 \dots z_4 = 0$. This gives

$$P = P_0 - \frac{(x + a/2)x_3 + yy_3 + zz_3}{R_3} + \frac{(x - a/2)x_1 + yy_1 + zz_1}{R_1}$$

For purposes of this expansion, we can let $R_3 = R_1 = R$, giving

$$P = P_0 + \frac{x}{R} (x_1 - x_3) + \frac{y}{R} (y_1 - y_3) + \frac{z}{R} (z_1 - z_3) - \frac{a}{2R} (x_1 + x_3)$$

but

$$\ell = \frac{x}{R}, \quad m = \frac{y}{R}, \quad n = \frac{z}{R}$$

thus,

$$P = P_0 + \ell(x_1 - x_3) + m(y_1 - y_3) + n(z_1 - z_3) - \frac{a}{2R} (x_1 + x_3)$$

The actual measurement is given by

$$\ell_0 = \frac{P}{a},$$

and from before

$$\frac{P_0}{a} \approx \ell - \frac{a^2}{8R^2} \ell(1 - \ell^2) \approx \ell$$

Therefore, we finally have

$$\ell = \ell_0 - \ell_0 \frac{(x_1 - x_3)}{a} - m_0 \frac{(y_1 - y_3)}{a} - n_0 \frac{(z_1 - z_3)}{a} + \frac{(x_1 + x_3)}{2R}$$

Proceeding in the same manner, we have for m

$$m = m_0 - \ell_0 \frac{(x_2 - x_4)}{b} - m_0 \frac{(y_2 - y_4)}{b} - n_0 \frac{(z_2 - z_4)}{b} + \frac{y_2 + y_4}{2R} .$$

Normally, the last term of both expressions can be neglected. Alternately, if a and b are chosen so that $x_1 + x_3$ and $y_2 + y_4$ are zero, then it can be dropped from consideration.

For close-in ranges when the approximation

$$\ell = \frac{P_0}{a}$$

cannot be made, then the value of ℓ and m above can be used to compute the exact cosine value through the solution of

$$\ell = \frac{P_0}{a} + \frac{a^2}{8R^2} \frac{P_0^2}{a^2} \left(1 - \frac{P_0^2}{a^2} \right) .$$

2.1.2 The Doppler Effect and Wave-Propagation Time-Delay as Applied to Predicted Minitrack Measurements

Consider a satellite at position $\underline{r}(t)$ at time t transmitting an unmodulated signal at a constant frequency ν . The signal is received by two MINITRACK antennas situated at $\frac{a}{2}\underline{i}$ and $-\frac{a}{2}\underline{i}$, respectively, where a is the baseline length and \underline{i} is a unit vector in the x -direction. The phase difference between two signals arriving at the two antennas at the same time t is measured. If the two signals left the satellite at times t_A and t_B , respectively, then the phase-difference between the two signals is $2\pi\nu(t_A - t_B)$. The actual measurement, $\Delta\phi$, is the phase-difference divided by 2π . Hence,

$$\Delta\phi = \nu (t_A - t_B) . \quad (1)$$

or equivalently,

$$\Delta\phi = \frac{c (t_A - t_B)}{\lambda} . \quad (2)$$

where c is the velocity of light and λ the wavelength. We must also have,

$$|\underline{r}_A - \frac{a}{2}\underline{i}| = c(t - t_A) , \quad (3)$$

and

$$|\underline{r}_B + \frac{a}{2}\underline{i}| = c(t - t_B) , \quad (4)$$

where, in general, $\underline{r}_i = \underline{r}(t_i)$

Writing,

$$\tau = t_A - t_B , \quad (5)$$

we have by the mean-value theorem

$$\underline{t}_B = \underline{t}_A - \tau \dot{\underline{r}}_A + \frac{1}{2} \tau^2 \ddot{\underline{r}}_M , \quad (6)$$

where t_M is a time between t_A and t_B .

Writing

$$r_A = |\underline{r}_A| \text{ and } \underline{p}_A = \underline{r}_A/r_A, \quad (7)$$

we obtain from (6),

$$\underline{r}_B + \frac{1}{2} a \underline{i} = r_A \left[\underline{p}_A - \left(\frac{a}{r_A} \right) \left(\frac{cT}{a} \right) \frac{\dot{\underline{r}}_A}{c} + \frac{1}{2} \left(\frac{cT}{a} \right)^2 \left(\frac{a}{r_A} \right) \frac{a \ddot{\underline{r}}_M}{c^2} + \frac{1}{2} \left(\frac{a}{r_A} \right) \underline{i} \right] \quad (8)$$

Since $\underline{p}_A^2 = 1$, $\underline{p}_A \cdot \dot{\underline{r}}_A = \dot{r}_A$, and $\underline{i} \cdot \underline{p}_A = l_A$,

the direction cosine at time t_A , we obtain from (8),

$$\begin{aligned} |\underline{r}_B + \frac{1}{2} a \underline{i}| = r_A \left\{ 1 + \left(\frac{a}{r_A} \right) \left[l_A - 2 l_0 \frac{\dot{r}_A}{c} + l_0^2 \frac{a \underline{p}_A \cdot \ddot{\underline{r}}_M}{c^2} \right] \right. \\ \left. + \left(\frac{a}{r_A} \right)^2 \left[\frac{1}{2} \underline{i} - l_0 \frac{\dot{\underline{r}}_A}{c} + \frac{1}{2} l_0^2 \frac{a \ddot{\underline{r}}_M}{c^2} \right]^2 \right\}^{\frac{1}{2}} \quad (9) \end{aligned}$$

where $l_0 = \frac{cT}{a}$ (10)

Next we make some assumptions regarding the magnitude of the terms in (9).

We assume that,

$$|l_0| \cong 1 \quad (11)$$

(This will be justified later on when we shall show that l_0 is a first approximation to the direction cosine l_A)

Write, $\frac{a}{r_A} = a_3$, (12)

and assume that $a_3 < 10^{-3}$, i.e. that the satellite is always more than 1000 baseline lengths from the station.

Write $\frac{\dot{\underline{r}}_A}{c} = u_4$ (13)

and assume that $|\dot{\underline{r}}_A|/c < 10^{-4}$, i.e. that the satellite velocity is less than 10^{-4} times the velocity of light. Since $|\dot{\underline{r}}_A| \cong |\dot{\underline{r}}_A|$ it follows that $|u_4| < 10^{-4}$.

Next assume that, $\frac{r}{c^2} |\underline{\dot{r}}| < 10^{-7}$ (14)

Hence by the assumption made in (12) ,

$$\frac{a}{c^2} |\underline{\dot{r}_M}| < 10^{-10} \quad (15)$$

With the above assumptions equation (9) may be rewritten as,

$$|\underline{r}_B + \frac{1}{2} a \underline{i}| = r_A \left\{ 1 + a_3 \left[l_A - 2l_0 u_4 + \frac{1}{4} a_3 + 0(10^{-7}) \right] \right\}^{\frac{1}{2}} \quad (16)$$

where $0(10^{-n})$ denotes terms of order 10^{-n} or less.

Equation (16) may be rewritten in the form:

$$\begin{aligned} |\underline{r}_B + \frac{1}{2} a \underline{i}| &= r_A \left\{ 1 + a_3 l_A + \frac{1}{4} a_3^2 l_A^2 + a_3 \left[\frac{1}{4} a_3 (1 - l_A^2) - 2l_0 u_4 + 0(10^{-7}) \right] \right\}^{\frac{1}{2}} \\ &= r_A \left(1 + \frac{1}{2} a_3 l_A \right) \left\{ 1 + a_3 \left[\frac{1}{4} a_3 (1 - l_A^2) - 2l_0 u_4 + 0(10^{-7}) \right] \left[1 - a_3 l_A + 0(10^{-6}) \right] \right\}^{\frac{1}{2}} \\ &= r_A \left(1 + \frac{1}{2} a_3 l_A \right) \left\{ 1 + \frac{1}{2} a_3 \left[\frac{1}{4} a_3 (1 - l_A^2) - 2l_0 u_4 + 0(10^{-7}) \right] \left[1 - a_3 l_A \right] \right\} \\ &= r_A \left\{ 1 + \frac{1}{2} a_3 l_A + \frac{1}{2} a_3 \left[\frac{1}{4} a_3 (1 - l_A^2) (1 - \frac{1}{2} a_3 l_A) - 2l_0 u_4 + 0(10^{-7}) \right] \right\} \quad (16)' \end{aligned}$$

We obtain a similar expression for $|\underline{r}_1 - \frac{1}{2} a \underline{i}|$ with a_3 replaced by $-a_3$ and $u_4 = 0$.

Hence:

$$|\underline{r}_1 - \frac{1}{2} a \underline{i}| = r_A \left\{ 1 - \frac{1}{2} a_3 l_A + \frac{1}{2} a_3 \left[\frac{1}{4} a_3 (1 - l_A^2) (1 + \frac{1}{2} a_3 l_A) + 0(10^{-7}) \right] \right\} \quad (17)$$

Hence from (3), (4), (5), (16)', and (17),

$$c\tau = r_A a_3 \left\{ l_A - \frac{1}{8} a_3^2 (1 - l_A^2) l_A - l_0 u_4 + 0(10^{-7}) \right\} \quad (18)$$

It is easy to show that $\frac{1}{8} a_3^2 (1 - l_A^2) l_A = O(10^{-7})$. Hence from (10), (12), and (18)

$$l_0 = l_A - l_0 u_4 + O(10^{-7}).$$

Whence, by (13)

$$l_A = l_0 \left(1 + \frac{\dot{r}_A}{c}\right) + O(10^{-7}) \quad (19)$$

Hence we have shown that l_0 is a first approximation to the direction cosine l_A .

From (2), (5), and (10)

$$l_0 = \frac{\lambda \Delta\varphi}{a}, \quad (20)$$

and hence

$$l_A = \frac{\Delta\varphi}{a} \left[\lambda \left(1 + \frac{\dot{r}_A}{c}\right) \right] + O(10^{-7}) \quad (21)$$

From expression (21) it is easy to see that the term in (\dot{r}_A/c) represents the Doppler effect. We shall show that expression (21) may be further simplified.

From (3) and (17) we have

$$c(t - t_A) = r_A \left[1 + O(10^{-3}) \right] \quad (22)$$

Hence denoting the direction cosine at time t by l , we have by the mean value theorem

$$l = l_A + \frac{r_A}{c} \left[1 + O(10^{-3}) \right] l_A + \frac{1}{2} \frac{r_A^2}{c^2} \left[1 + O(10^{-3}) \right] l_N'' \quad (23)$$

where l_N is the direction cosine at some time t_N between t and t_A . Writing $\underline{p} = \underline{r}/r$ we obtain

$$\begin{aligned} r \underline{\dot{p}} &= \underline{\dot{r}} - \dot{r} \underline{p} \\ &= \underline{p} \times (\underline{\dot{r}} \times \underline{p}) \end{aligned} \quad (24)$$

since $\underline{p}^2 = 1$ and $\underline{p} \cdot \underline{\dot{r}} = \dot{r}$. Differentiating (24) gives,

$$r \underline{\ddot{p}} = \underline{\dot{p}} \times (\underline{\dot{r}} \times \underline{p}) + \underline{p} \times (\underline{\ddot{r}} \times \underline{p}) + \underline{p} \times (\underline{\dot{r}} \times \underline{\dot{p}}) - \dot{r} \underline{\dot{p}} \quad (25)$$

Since $l = \underline{p} \cdot \underline{i}$ it follows that,

$$l \cong |\underline{p}|, \quad \dot{l} \cong |\dot{\underline{p}}| \quad \text{and} \quad \ddot{l} \cong |\ddot{\underline{p}}| \quad (26)$$

By (24),

$$r |\dot{\underline{p}}| \cong |\dot{\underline{r}}| \quad (27)$$

From (25) and (27)

$$\begin{aligned} r^2 |\ddot{\underline{p}}| &\cong |\dot{\underline{r}}|^2 + r |\ddot{\underline{r}}| + |\dot{\underline{r}}|^2 + \dot{r} |\dot{\underline{r}}| \\ &\cong 3 |\dot{\underline{r}}|^2 + r |\ddot{\underline{r}}| \end{aligned} \quad (28)$$

From (26) and (27) we have

$$\begin{aligned} \frac{r \dot{l}}{c} &\cong \left| \frac{\dot{\underline{r}}}{c} \right| \\ &= 0 (10^{-4}) \end{aligned} \quad (29)$$

by our previous assumptions. From (26) and (28) we obtain

$$\begin{aligned} \frac{1}{2} \frac{r^2 \ddot{l}}{c^2} &\cong \frac{1}{2} \left[3 \frac{|\dot{\underline{r}}|^2}{c^2} + r \frac{|\ddot{\underline{r}}|}{c^2} \right] \\ &= 0 (10^{-7}), \end{aligned} \quad (30)$$

by the assumptions made in (13) and (14) above.

We then have from (23), (29), and (30),

$$l = l_A + \frac{r_A}{c} \dot{l}_A + 0(10^{-7}) + \frac{r_A^2}{r_N^2} 0(10^{-7}) \quad (31)$$

By the mean value theorem

$$r_N = r_A + (t_N - t_A) \dot{r}_K$$

But $t_N - t_A \cong t - t_A = \frac{r_A}{c} [1 + 0(10^{-3})]$, Hence

$$\begin{aligned} |t_N - t_A| |\dot{r}_K| &\cong r_A \left| \dot{r}_K \right| / c [1 + 0(10^{-3})] \\ &= r_A 0(10^{-4}), \quad \text{where} \end{aligned}$$

$$r_N > r_A - r_A 0(10^{-4}), \quad \text{and} \quad (r_A/r_N) \cong 1 + 0(10^{-4})$$

$$\text{Hence } l = l_A + \frac{r_A}{c} \dot{l}_A + 0(10^{-7}) \quad (32)$$

$$\text{But } r_A \dot{l}_A = \dot{x}_A - \dot{r}_A l_A, \quad (33)$$

$$\text{where } \dot{x}_A = \dot{r}_A \cdot \underline{i}$$

$$\text{Hence } l = l_A + \frac{\dot{x}_A}{c} - l_A \left(\frac{\dot{r}_A}{c} \right) + 0 (10^{-7}) \quad (34)$$

From (19) we obtain

$$l_0 = l_A \left(1 - \frac{\dot{r}_A}{c} \right) + 0 (10^{-7}),$$

Hence from the above and (36)

$$l = l_0 + \frac{\dot{x}_A}{c} + 0 (10^{-7}) \quad (35)$$

By the mean value theorem and (22)

$$\frac{\dot{x}}{c} = \frac{\dot{x}_A}{c} + \frac{r_A}{c} \frac{\ddot{x}_D}{c} \left[1 + 0 (10^{-3}) \right]$$

$$= \frac{\dot{x}_A}{c} + 0 (10^{-7}), \text{ by (14), where } \dot{x} \text{ is the x-component of the velocity at time } t.$$

Hence,

$$l_0 = l - \frac{\dot{x}}{c} + 0 (10^{-7}).$$

Finally from the above and (20),

$$\boxed{\frac{\lambda \Delta \varphi}{a} = l - \frac{\dot{x}}{c} + 0 (10^{-7})} \quad (38)$$

The following assumptions were made in deriving (38)

$$(a/r) < 10^{-3}, \quad (|\dot{r}|/c) < 10^{-4},$$

and $r |\ddot{r}|/c^2 < 10^{-7}$. If the only forces acting on the satellite are due to the Earth's gravity field then $|\ddot{r}| = gR_E^2/R^2$, where g is the acceleration due to gravity at the Earth's surface, R_E is the radius of the Earth and R is the radius vector from the center of the Earth to the satellite. Since $r \leq 2R$ it then follows that $r |\ddot{r}|/c^2 \leq [2gR_E/c^2][R_E/R]$ which is always less than 10^{-7} .

For the m direction cosine a formula similar to (38) holds true:

$$\boxed{\frac{\lambda \Delta\varphi_m}{a} = m - \frac{\dot{y}}{c} + 0(10^{-7}),} \quad (39)$$

where in this case $\Delta\varphi_m$ represents the phase difference of the North-South antenna pair.

2.2 MINITRACK DATA

2.2.1 Standard Minitrack Data Format

The following is the Standard Minitrack data message that is stored on magnetic tapes by satellite and by station. The message appears on teletype output as in the following sample.

```
Satellite ID and date → &6406401 1 690103
                          4350.2639114.3580.2639114.1230.2639114.00380.2639114.215.2639114.
                          1456.3071750.4503.3231736.1217.3121830.00354.3251831.215.3391904.
                          1662.3591152.4505.3581199.1222.3761243.00335.3771280.215.3751324.
                          1861.4081559.4504.4241597.1217.4221636.00339.4252685.215.4321729.
                          2061.4741972.4505.4672022.1220.4761060.00342.4812083.215.4881142.
                          2263.5342388.4506.5391436.1222.5301463.00347.5411519.215.5472546.
                          2463.5911798.4507.5912840.1227.6082386.00348.6062920.215.6102969.
                          2664.6502208.4507.6491255.1228.6522305.00350.6721342.215.6792385.
                          2863.7162633.4505.7212679.1232.7312717.00351.7372762.215.7452802.
                          3064.7882057.4508.7992104.1236.8062143.00354.8202186.215.8192239.
                          3265.8572483.4507.8672528.1238.8342574.00358.8842604.215.8961652.
                          3467.9482918.4507.9431950.1238.9612006.00359.9592031.215.9802078.
                          3668.0162345.4508.0281380.1241.0372431.00366.0482459.215.0582517.
Data →                    3867.1022771.4509.1162812.1247.1242870.00365.1312904.215.1412946.
                          4068.1892200.4507.2011247.1249.2102297.00366.2152342.215.2252384.
                          4269.2831634.4510.2992684.1251.2932731.00371.3131768.215.3051830.
                          4469.3721086.4511.3871115.1256.3921171.00370.4031207.215.4121258.
                          4670.4741514.4511.4821560.1259.4921607.00376.4941661.215.5021704.
                          4870.5701966.4511.5801993.1261.5871055.00376.5981087.215.6031146.
                          5071.6691395.4513.6841450.1265.6931503.00379.6941544.215.7081598.
                          5271.7781848.4512.7841909.1268.7951947.00383.8001990.215.8281045.
                          5472.8891289.4514.8961351.1271.9131397.00385.9151439.215.9310481.
                          5672.9841751.4515.0030801.1273.0231826.00387.0161901.215.0611942.
                          5874.1140218.4516.1190238.1278.1370292.00390.1691338.215.1500394.
                          0074.2341658.4615.2440702.1281.2700739.00393.2860777.215.2850835.
                          0274.3590109.4616.3740175.1283.3990211.00397.3930246.215.4070299.
                          0475.4750568.4619.5000613.1287.5170665.00300.4830695.215.5330745.
                          0676.6200003.4619.6460072.1290.6330121.00302.6540176.215.6470231.
                          0879.7680522.4620.7230527.1294.7930567.00305.7900650.215.3420678.
                          1078.8850954.4620.8280014.1298.9310025.00308.9620126.215.9890143.
                          1280.1020389.4621.0980426.1200.0230478.00309.0300507.215.0990595.

Satellite ID → 6406401
Terminating Message → 03/1321Z JAN LWNK
```

The format for the message is as follows:

MESSAGE FORMAT

<u>Character(s)</u>	<u>Contents</u>
1, 2	second (time) of frame start
3, 4	hundreds and tens digits of east-west medium phase
5	period "." separator
6 to 8	first east-west fine phase
9	signal strength indicator (AGC)
10 to 12	first north-south fine phase
13	period "." separator
14, 15	minute of frame start
16, 17	hundreds and tens digits of east-west coarse phase
18	period "." separator
19 to 21	second east-west fine phase
22	signal strength indicator (AGC)
23 to 25	second north-south fine phase
26	period "." separator
27, 28	hour of frame start
29, 30	hundreds and tens digits of north-south medium phase
31	period "." separator
32 to 34	third east-west fine phase
35	signal strength indicator (AGC)
36 to 38	third north-south fine phase
39	period "." separator
40 to 42	day of year for frame start
43, 44	hundreds and tens digits of north-south coarse phase
45	period "." separator
46 to 48	fourth east-west fine phase

MESSAGE FORMAT (Cont'd)

<u>Character(s)</u>	<u>Contents</u>
49	signal strength indicator (AGC)
50 to 52	fourth north-sound fine phase
53	period "." separator
54	equatorial/polar antenna indicator 1 = equatorial 2 = polar
55, 56	station number 03 = FTM YRS 15 = WNKFLD 01 = BPOINT 05 = QUITOE 16 = JOBURG 13 = COLEGE 06 = LIMAPU 19 = ALASKA 17 = MOJAVE 08 = SNTAGO 21 = ORORAL 14 = GRDFKS 12 = NEWFLD 23 = MADGAR 18 = WOOMER
57	period "." separator
58 to 60	fifth east-west fine phase
61	signal strength indicator (AGC)
62 to 64	fifth north-south fine phase'
65	period "." separator

2.2.2 Extracting and Sorting Minitrack Data

The GEOS-A Minitrack data extracting program and the sorting program are special purpose programs each with a single function. The extracting program reads a Master Minitrack data storage tape and extracts only data taken on the GEOS-A satellite. This data is copied to another magnetic tape in the same format (same as given in the example in 2.2.1). This results in a data tape of GEOS-A Minitrack data grouped by station in chronological order. The FORTRAN listing of the extracting program is given in Appendix A-2.1. The requirements for the program operation are:

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Card Input	Card Reader	Program Source Deck
Tape Input	Data Set 9 (FT09F001)	Minitrack messages for several satellites
Tape Output	Data Set 11 (FT11F001)	Minitrack messages for GEOS-A (Satellite ID 65891)
Printed Output	Data Set 6	Total number of messages Number of GEOS-A messages First 100 messages from output tape

The tape output (Data Set 11) from the extract program is the input data tape for the sort program. This program sorts messages in time-sequence. It also eliminates duplicate messages. Messages for the same station and antenna configuration are assumed to be duplicates if they commence within 30 seconds of each other. If two duplicate messages are of unequal length, then the shorter message is discarded. If they are of the same length, then the last received message is discarded.

The length of a message is determined by the number of good records it contains. The characters in each record are checked for numeric characters and periods in the appropriate places. A record with an error is discarded. The first "proper" record of a message is the calibration line. If this contains an error, the whole message is discarded. It has been found that in some messages the calibration line and subsequent records are repeated within the same message. For this reason, every record is compared with the calibration line. If a record is found to be identical to the calibration line, then this is regarded as the first "proper" record of the message. All previous "proper" records are ignored.

Messages containing fewer than 5 records are discarded. The output tape from the sort program is in the same format as the input tape.

The FORTRAN listing of the sort program is given in Appendix A-2.2.

The requirements for running the sort program are as follows.

<u>Function</u>	<u>Unit</u>	<u>Description</u>																				
Card Input	Card Reader	Source Program																				
Data Cards	Data Set 5	17 Cards Required (See Appendix A-2.2) Cards 1-16 (One card for each Station)																				
		<table border="1"> <thead> <tr> <th><u>Card Column</u></th> <th><u>Word</u></th> <th><u>Definition</u></th> <th><u>Format</u></th> </tr> </thead> <tbody> <tr> <td>1-5</td> <td>KSTA</td> <td>Station ID</td> <td>I5</td> </tr> <tr> <td>6-10</td> <td></td> <td>Blank</td> <td></td> </tr> <tr> <td>11-16</td> <td>STATIO</td> <td>Station Name</td> <td>A6</td> </tr> </tbody> </table>	<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>	1-5	KSTA	Station ID	I5	6-10		Blank		11-16	STATIO	Station Name	A6				
<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>																			
1-5	KSTA	Station ID	I5																			
6-10		Blank																				
11-16	STATIO	Station Name	A6																			
		Card 17																				
		<table border="1"> <thead> <tr> <th><u>Card Column</u></th> <th><u>Word</u></th> <th><u>Definition</u></th> <th><u>Format</u></th> </tr> </thead> <tbody> <tr> <td>1-8</td> <td>INTAPE</td> <td>Input tape No.</td> <td>A8</td> </tr> <tr> <td>9-13</td> <td>INFILE</td> <td>File No.</td> <td>I5</td> </tr> <tr> <td>14-21</td> <td>NDTAPE</td> <td>Output tape No.</td> <td>A8</td> </tr> <tr> <td>22-26</td> <td>NDFILE</td> <td>File No.</td> <td>I5</td> </tr> </tbody> </table>	<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>	1-8	INTAPE	Input tape No.	A8	9-13	INFILE	File No.	I5	14-21	NDTAPE	Output tape No.	A8	22-26	NDFILE	File No.	I5
<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>																			
1-8	INTAPE	Input tape No.	A8																			
9-13	INFILE	File No.	I5																			
14-21	NDTAPE	Output tape No.	A8																			
22-26	NDFILE	File No.	I5																			
Tape Input	Data Set 9 (FT09F001)	Input tape containing Minitrack messages (Output tape from Extract program)																				
Tape Output	Data Set 10 (FT10F001)	Output tape containing sorted Minitrack messages																				
Printer Output	Data Set 6	A list of message numbers (as sequenced on input tape) of rejected messages together with reasons for rejection A list of output information giving the following. (The actual data message is not printed out):																				
		<ul style="list-style-type: none"> Sequence number on output tape Sequence number on input tape Station ID (KSTA) Station Name (STATIO) Day Number (1 to 366) Month Day of Month (not correct for leap year) Seconds of day Hours Minutes Seconds 																				
		<ul style="list-style-type: none"> (of day) Number of lines in message 																				

2.2.3 The Minitrack Preprocessor

The purpose of the Minitrack preprocessor is to make known corrections to the Minitrack data and output a magnetic tape containing corrected data in a format acceptable to the NAP-II program. Basically, the preprocessor reads the raw phase data message, computes phase differences, makes corrections and then converts the corrected phase differences to direction cosines. This process is explained in detail in references 1 and 2.

The Minitrack preprocessor used was based on that developed by the Goddard Space Flight Center Network Computation Section (references 1 and 2). The program was extensively modified by W. M. Rice (GSFC, Code 551). A few minor modifications were then made by DBA Systems, Inc. under this contract. A complete listing of the preprocessor program is given in Appendix A-2.3. Sample JCL for running the program is also given.

Changes Made by W. M. Rice. A Minitrack message contains, in general, 155 measurements of phase differences between two antenna pairs. The preprocessor converts these to 155 pairs of direction cosines. A quadratic fit is then made to each set of 155 direction cosines. The resultant output is a single pair of direction cosines (the fitted midpoint values). The program is made more complicated by the fact that the ambiguity of the direction cosines must be resolved using additional information in the Minitrack message (Reference 2). However, this is only done to the fitted midpoint values. In the Rice version of the program the ambiguity is resolved for all direction cosines. The output consists of all direction cosines and is in a format that can be used as an input to the NAP program. The time associated with each measurement is given at the instant that the signal being analyzed arrived at the relevant antenna pair.

Changes Made by DBA Systems, Inc. To facilitate the data preparation for the NAP program, the Minitrack preprocessor was modified to punch out the three control cards (Categories 201, 202, and 999) required for each data message. (For a description of the required control cards, see reference 4).

Although nominally there is a single time associated with each pair of direction cosines, this is not so in practice. Differences arise due to different filter delays associated with each direction cosine and also due to different counter delays (reference 3). As the volume of printed output from the NAP program is proportional to the total number of different time points, the output volume could be reduced by one half, if each pair of direction cosines were adjusted to the same time point. This was done. The adjusted time point was chosen as the average time of the two measurements. For a typical NAP run, this reduced the output volume by half.

A modification was also made to output on tape in a NAP input format, the fitted midpoint values of the original program. The idea behind this was that the fitted midpoint values could be used initially as an input to NAP, the "all data points" input being reserved for the final iterations through NAP. This in theory should have reduced the total computer time required. In practice, however, it was found that the "all data points" input when processed through NAP, provided the user with an extremely useful criterion for determining the quality of the data in a Minitrack message -- the standard deviation of the error of all measurements within a message. For this reason, little use was made of the "fitted midpoint" input.

To help in the analysis of the results of the NAP program, a modification was made to print out a summary of the results of the preprocessing. This summary contained the following information for each station: For each data message the midpoint time, the three midpoint direction cosines and their rates of change, plus the prepass calibration constants.

Finally, an error in the way the 2 Hz filter delay was being applied was corrected.

A Program Error. Messages spanning midnight are not handled correctly by the program. A Minitrack message typically spaces a time interval of one minute or one half of a minute, so that this occurs very infrequently, but the program error should be corrected.

The Minitrack preprocessor exists as a modified version of the original program developed by GSFC. Some of the information used in the original program is not used in its present form. The input cards to the program, however, are the same as with the original program. Consequently, a large number of cards containing little information are required.

The following information is required for operation of the program.

<u>Function</u>	<u>Unit</u>	<u>Description</u>			
Card Input	Data Set 5	Station Calibration Constants			
		Card 1 Blank			
		Card 2 Station Constants			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		1-6	STATIO	Any 6 alpha-numeric characters	A6
		7		Blank	

<u>Function</u>	<u>Unit</u>	<u>Description</u>			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		8, 9	KSTA	Station number	I2
		10-13	KFA	Time adjustment EW-channel	I4
		14-17	KFB	Time adjustment NS-channel	I4
		18-20		Blank	
		21-24	EWM	Phase bias medium antenna, EW-channel	F4.3
		25-27	CLEWM	Cable length in- equality, EW- medium channel	F3.3
		28-31	EWC	Phase bias coarse antenna, EW-channel	F4.3
		32-34	CLEWC	Cable length in- equality, EW- coarse channel	F3.3
		35		Blank	
		36-39	EWFEQ	Phase bias equatorial fine antenna, EW-channel	F4.3
		40-43	EWFPO	Phase bias polar fine antenna, EW-channel	F4.3
		44-46		Blank	
		47-50	NSM	Phase bias medium antenna, NS-channel	F4.3
		51-53	CLNSM	Cable length in- equality NS-medium channel	F3.3
		54-57	NSC	Phase bias coarse antenna, NS-channel	F4.3
		58-60	CLNSC	Cable length in- equality NS-coarse channel	F3.3
		61		Blank	

<u>Function</u>	<u>Unit</u>	<u>Description</u>			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		62-65	NSFEQ	Phase bias equatorial fine antenna, NS-channel	F4.3
		66-69	NSFPO	Phase bias polar fine antenna, NS-channel	F4.3
		70-74		Blank	
		75-79	DATE	Date of calibration	I6
		Cards 3 thru 10		Blank	
		Cards 11-135		15 sets of cards 2 thru 10 are required. One set for each of the Minitrack stations	
		Card 136			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		1-5	KSAID	Satellite ID	I5
		6-24		Blank	
		25-32	FREQ	Satellite transmitter frequency (MHZ)	F8.3
		Card 137		Blank card terminates data set.	

<u>Function</u>	<u>Unit</u>	<u>Description</u>			
Card Input	Data Set 8	Data Selection Control Cards			
		Card 1	80 alphanumeric characters used to write a message in the pre-processed printout		
		Card 2	(more than one card can be used)		
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		1-10	ILOW, IHIGH	Program will process messages between ILOW and IHIGH	I15

<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
11-15	IYEAR	2-digit integer for year of measurements e.g. 1966 = 66	I5
16-20	NEWARC	Arc number assigned to measurements. If several ILOW, IHIGH cards define some arc, NEWARC should be blank on all but first card.	I5
21-25	NAPEND	Normally left blank -1 = more data tape to follow 0 = normal termination 1 = no terminal record written (for tape addition)	

According to Ref. 4, the input tape to NAP should terminate with a negative number in the last record. However, with current versions of NAP this is no longer necessary. If NAPEND is left blank, this terminal record is written on the tape. If on the last "ILOW, IHIGH" card NAPEND is set equal to a positive non-zero integer, then the terminal record is not written. (The reason for this option is to facilitate combination of two or more data tapes into a single tape).

If the messages being processed are contained on more than one tape, then NAPEND should be set to a negative integer on the last "ILOW, IHIGH" card referring

<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
--------------------	-------------	-------------------	---------------

to a tape that is to be followed by another tape. e.g., if data messages to be processed are contained on three tapes such that

FT09F001 defines tape 1,
 FT09F002 defines tape 2,
 FT09F003 defines tape 3,

then the last "ILOW,IHIGH" card of tape 1 should have a negative NAPEND, the last "ILOW,IHIGH" card of tape 2 should have a negative NAPEND, the last "ILOW,IHIGH" card of tape 3 should have either a blank or a positive NAPEND.

Card 3, 4

Blank

Each "ILOW,IHIGH" card should be followed by two blank cards. The program actually has a restart capability. The blank cards must be inserted if the user does not wish to avail himself of the restart facility. For use of the restart facility the user is referred to the program listing, Appendix 2.3

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Tape Input	Data Set 9	Data tape(s) containing Minitrack messages to be processed
Tape Output	Data Set 12	Preprocessed output of "all data points" in a NAP-II input format
Tape Output	Data Set 19	Preprocessed output of "fitted midpoint" in NAP-II input format

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Punched Card Output	Data Set 7	NAP-II control cards for each data message. These are the start-stop times for that station data set (NAP-II cards group 201, 202, 999)
Printed Output	Data Set 6	Raw Minitrack messages with each message followed by the computed direction cosines for each data point. (Direction cosines are also given in terms of Minitrack counts.)
	Data Set 11	Printout of intermediate results obtained in pre-processing
	Data Set 13	Input station constants (See data set 5) List of all messages that have not been preprocessed and reasons why. Pass summary information (number of messages per station, time of last message for each station) Information required for restart.
	Data Set 14	Summary of preprocessed results arranged in time sequence (station, time, direction cosines, direction cosine rates)
	Data Sets 20 thru 51	32 data sets -- 1 per station. Although there are only 16 stations the program treats a station operating in the equatorial mode as one station with station number KSTA (See data set 5) and the same station operating in the polar mode as a different station with station numbers KSTA+100. Each data set contains preprocessed results (for each station) arranged in time sequence (time, direction cosines, direction cosine rates, prepass calibration constants.)

Suggested Running Time

For the 360/91	CPU time	11 minutes per 1000 messages
For the 360/95	CPU time	14 minutes per 1000 messages

2.3 Optical Data

2.3.1 Standard Optical Data Format

The optical data used in this study was obtained from the NASA Space Sciences Data Center (NSSDC) at Goddard Space Flight Center. The data was on magnetic tape in the "GEOS format." A complete description of the data format is available from the NSSDC. The "GEOS format" for optical data is basically 80 column card images stored on magnetic tape. Each card image contains the following.

<u>Card Column</u>	<u>Description</u>
1-6	Satellite identification
7	Type of coordinates (RA and DEC)
8	Observation identifier
9-11	Timing standard deviation
12-13	Time identifier
14-18	Station number
19-34	GMT of observation
35-53	Observation data
54-59	Date of plate reduction
60-71	Code information as to processing
72-80	Description of random error

A separate data tape for each tracking network is normally obtained from the NSSDC. For example, in this study optical data from the STADAN network and the SAO network was to be used. Two data tapes were obtained, one for STADAN and one for SAO. In order to simplify the optical preprocessing, it was necessary to merge the two tapes. A special program was written to this task. The program listing is given in Appendix A-2.4. The program merges two time sequenced optical data tapes into a single tape which will be the input data tape for the optical pre-processor. Data for each month is written on a separate file numbered sequentially on the same tape.

The following is required to execute the merge program:

<u>Function</u>	<u>Unit</u>	<u>Description</u>																
Card Input	Data Set 5	Tape and file number of output tape used for printout.																
		<table border="1"> <thead> <tr> <th><u>Card Column</u></th> <th><u>Word</u></th> <th><u>Definition</u></th> <th><u>Format</u></th> </tr> </thead> <tbody> <tr> <td>1-8</td> <td>TAPE</td> <td>8-character tape number</td> <td>A8</td> </tr> <tr> <td>9-10</td> <td></td> <td>Blank</td> <td></td> </tr> <tr> <td>11-15</td> <td>IFILE</td> <td>File number of first month of the combined tape</td> <td>15</td> </tr> </tbody> </table>	<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>	1-8	TAPE	8-character tape number	A8	9-10		Blank		11-15	IFILE	File number of first month of the combined tape	15
<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>															
1-8	TAPE	8-character tape number	A8															
9-10		Blank																
11-15	IFILE	File number of first month of the combined tape	15															
Tape Input	Data Set 1	Data tape with STADAN stations.																
Tape Input	Data Set 2	Data tape with SAO station.																
	NOTE:	The user should examine the printed output of the input data tapes to determine if there are dummy or non-essential data records on the tapes.																
Tape Output	Data Set 3	Merged data output (Input tape to Optical Preprocessor) JCL cards required for each month there is data. FT03F001 should have tape and file no. corresponding to card input, data set 5. The reason for writing a separate file for each month is to minimize tape search required in the optical preprocessor.																
Printed Output	Data Set 6	Printed output of the merged output data tape (data set 3). Each page has a heading giving the year and month of the data and the tape and file number on which the data may be found on tape.																

2.3.2 Optical Data Preprocessing

The program assumes that the data on the input tape (data set 1) is arranged in time sequence. The program resequences the data such that the data for each station/orbit combination is sequential. An orbit is defined as consisting of TORBT seconds (45 minutes). Furthermore, each "station/orbit" is subdivided into passes (photographic plates) where each pass may be TPASS seconds (45 seconds) long. The data itself is converted to radians and output on data set 2 in the NAP input format. NAP control cards are punched (data set 7) for each pass.

For SAO stations (station ID 29XXX), the input data is given in the 1950.0 coordinate system. This is converted to the "true of date" coordinate system. The precession and nutation formulae used are based on those given in the Explanatory Supplement to the Astronomical Ephemeris and the American Ephemeris and Nautical Almanac (Her Majesty's Stationary Office, London, 1961). Also, the time of the SAO stations is given as Atomic time. This is converted to UTC using information provided by the user (data set 4). A further complication arises in the case of the SAO stations because, for those stations, the time associated with the data is the time of observation rather than the time that the signal left the satellite. An "r/c" correction should thus be applied to the timing of the orbit determination program. Unfortunately, NAP-II does not possess this capability. A temporary fix has, therefore, been made (subroutine SAOCOR) utilizing the fact that, nominally, the GEOS satellite always flashes on the even second. Since this is not exactly true, it is recommended that the user compare the output time for the SAO stations with those of other stations and make the appropriate adjustments on NAP "704" cards (see reference 4).

The following cards are required for running the optical preprocessor.

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Card Input	Data Set 5	Station and data set control cards.

FunctionUnitDescription

Station Cards: Up to 30 observing stations may be used. One card for each station.

<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
1-5	KSTA	Station No. given on NAP 201/202 cards.	I5
6-10		Blank	
11-18	STNAM	8-alphanumeric character station name.	A8
19-20		Blank	
21-25	ISTA	Station ID	I5
26-30	IEND	Blank except for last "station" card where a negative integer is used to indicate last station card.	I5

Data Set Cards: One card for each arc of data.

<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
7-5	NARC	Arc number required for NAP control cards.	I5
6-10		Blank	
11-16	IYMDB	Year, month and day of beginning of arc (e.g. 660312).	I6
17-19	IHB	Hour of beginning of arc.	I3
20-22	IMB	Minute of beginning of arc.	I3
23-32	SECB	Seconds of beginning of arc.	D10.0
33-38	IYMDE	Year, month and day of end of arc.	I6

<u>Function</u>	<u>Unit</u>	<u>Description</u>			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		39-41	IHE	Hour of end of arc.	I3
		42-44	IME	Minutes of end of arc.	I3
		45-54	SECE	Seconds of end of arc.	D10.0
Card Input	Data Set 4	Correction from A.1 to UTC time. Required only if SAO stations are to be processed. Any number of these cards may be used and the program will use a linear interpolation to any required time. At least two cards required.			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		1-2	IYR	Year	I2
		3-4	IMO	Month	I2
		5-6	IDA	Day	I2
		7-10		Blank	
		11-20	COR	A.1 minus UTC on year, month, day (IYR, IMO, IDA)	F10.5
Tape Input	Data Set 1	Data tapes to be processed (output from Merge or GEOS formatted data tape). If more than one data tape is used, then JCL will be modified to accommodate (e.g. FT01F001 for first tape, FT01F002 for second tape, etc.).			
Tape Output	Data Set 2	Preprocessed data tape to be input to NAP-II.			
Printed Output	Data Set 6	Print of preprocessed data.			
	Data Set 3	Printed output of input (data sets 4 and 5).			
	Data Set 12	Summary of data.			
Punched Output	Data Set 7	NAP Control Cards for timing/station information, NAP Cards 201, 202, 999 (see Reference 4).			

2.4 REDUCTION OF MINITRACK DATA

2.4.1 PRENAP Program

The processing of 20 days of Minitrack data requires about 5000 input cards. In order to reduce the number of cards that must be handled for a NAP-II run, the NAP-II control cards are written on magnetic tape. This "control card" tape is then updated and communicated to the NAP-II program via the PRENAP program. In this mode of operation, execution of the PRENAP program becomes the first step of a complete NAP-II run.

The following is a listing of the program to copy the NAP-II control cards onto magnetic tape.

Job Card

```
// EXEC FORTRAN
//SOURCE.SYSIN DD*
      IMPLICIT REAL * 8 (A-H,0-7)
      DIMENSION KAT(2),KEY(10),DATA(2)
100  FORMAT (13,12,A8, 10I3,D22.8,D15.8)
      DO 300 I=1, 10000
      READ (5, 100,END=400) KAT,XLABEL,KEY,DATA
      WRITE (9) KAT,XLABEL,KEY,DATA,I
300  CONTINUE
400  ENDFILE 9
      REWIND 9
200  FORMAT (1X,3I8,A8, 10I3,2D19.8)
      DO 330 J=1, 10000
      READ(9,END=500) KAT,XLABEL,KEY,DATA,I
      WRITE(6,200) I,KAT,XLABEL,KEY,DATA
330  CONTINUE
500  STOP
      END
```

```

/*
// EXEC LOADER, PARM='MAP, CALL, SIZE=100K', REGION.GO=110K
//GO.FT09=001 DD UNIT=9TRACK, LABEL=(4, BLP), DSN=MRGDAP, DISP=(NEW, KEEP),
// DCB=(RECFM=VBS, LRECL=80, BLKSIZE=3204) VOL=SER=34517C
//GO.DATA5 DD*

```

Once the NAP-II cards are written on tape, the function of the PRENAP program is to update the "cards" on tape and to convert the binary "cards" tape to a format acceptable to the NAP-II program. The PRENAP program is listed in Appendix A-2.6. At the end of the program listing is an example of the JCL cards needed and a sample set of update cards.

The program is normally loaded as a binary object deck (Appendix A-2.6 JCL cards). The function of the peripheral equipment needed to execute the PRENAP program are:

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Input Tape	Data Set 9	NAP-II control cards on magnetic tape. (Output from program given above).
Disk File	Data Set 10	Used as an intermediate scratch tape.
Disk File	Data Set 12	Used to pass "updated" NAP-II control cards to NAP-II program for execution.
Card Input	Data Set 5	Updater cards for NAP-II control cards. If no update is required, data set 5 should be left empty. There would probably be no update the first time NAP-II is run for a particular job. The program prints out instructions on how to update "cards".

2.4.2 Use of NAP-II Program

The NAP-II program is a very flexible analysis tool providing the user with considerable freedom for designing and executing data reductions. Consequently, the user must have a good understanding of the program uses to attain efficient

utilization. This can only be done through use of the program and its various options.

The functions of the program are discussed in reference 4.

The type of information required to execute NAP-II is given as follows:

<u>Type of Information</u>	<u>Categories</u>
General and planetary information	101, 102, 103, 151
Comments	150
Station survey	301, 302, 303
Totally stable parameters	601, 602
Measurement definitions	701, 702, 703, 704 (Sets 0 only)
General arc information	104, 205, 206
Arc stable parameters	601, 602
General pass information	201, 202, 203, 204
Pass stable parameters	601, 602
Pass comments	152
Overrides for measurement definitions for a pass	701, 702, 703, 704 (Sets 1 only)
End of pass, arc, or all control data	999

The station numbers (category 300) are preassigned by the Minitrack and the optical data preprocessors, depending on the order of the Minitrack Station Calibration Cards and the Optical Stations Control Cards. This controls both the station ID numbers and the user assigned station numbers. These two programs also provide the timing information cards (category 200 and 999) as part of their output. The other cards must be set up by the user. The information required by the various groups of cards is given in reference 4.

Once a "master" set of cards has been set-up, subsequent runs can be made with new data sets by changing the following quantities,

- State vectors - Category 601, 205
- Greenwich Hour Angle - Category 206

- Lunar and Solar Coordinates - Category 104
- Timing information - Output from data preprocessors.

These cards can be changed via the PRENAP program.

To run the NAP program, it is essential to have a reasonably good estimate of the state vector at the initial epoch. Before the user tries to solve for any parameters, he should make an initial run, which will allow the POSTNAP program to edit out obviously bad data and correct the lobe assignments made by the Minitrack preprocessor. Once this has been done, the user can go ahead and solve for any parameters he wishes. As the user improves his estimate of the initial state vector, he may wish to modify his definition as to what constitutes bad data.

The NAP-II program outputs the following information on disk or tape:

- measurement discrepancies (FT37F001)
- current estimates of error model parameters (FT37F002)
- data tape with the mid-data point for each pass (FT37F003) .

For multi-arc data processing, it is recommended that the user switch from using the data tape output from the Minitrack preprocessor to the "single data point per pass" data tape. When using the single data point prepass, the Category 704 cards have to be deleted, because the biases have already been applied. The run time advantage of using one data point instead of all data points (which may be as many as 155) is considerable. The loss of accuracy is negligible.

The recommended procedure for reducing Minitrack data is summarized in Section 2.6.

There were changes made to the NAP-II program to effect the procedure for reducing Minitrack data. The need for some of these changes was discussed in the preface of this report. Without going into great detail, the changes to the particular subroutines are as follows:

- Changes to Subroutine ENEXPS

This subroutine computes two sets of series: (1) the power series expansions of n -heavenly bodies, and (2) the power series expansion defining whether or not the satellite is exposed to solar radiation. The subroutine was completely reprogrammed, making the new version seven times faster than the old. One of the factors contributing to the increased computational speed of the new program is that it computes the $n(n-1)/2$ different distances between n bodies, and no more. The old program somehow managed to compute more distances than this so that some distances had to be identical. The old program had a programming error in the computation of the "shadow" series so that the two programs do not agree as far as shadow series expansion is concerned. The FORTRAN listing of the subroutine is given in Appendix A-3.1.

- Changes to Subroutine EXPAND

Subroutine EXPAND computes two sets of series: (1) the power series expansion of the acceleration due to the full gravity field, expressed as a sum of spherical harmonics, of the main attacking body, and (2) the power series expansion of the acceleration due to atmospheric drag. The part dealing with the gravity field was completely rewritten. The mathematical analysis for this is given in reference 5. The FORTRAN listing of the subroutine is given in Appendix A-3.2.

- Changes to Subroutine VARIEQ

Subroutine VARIEQ computes the two sets of series: (1) the power series expansion of the variational matrix due to the full gravity field of the main attracting body, and (2) the power series expansion of the variational matrix due to atmospheric drag. The FORTRAN listing of the subroutine is given in Appendix A-3.3.

- Changes to Subroutine FINALP

A small change was made in this subroutine to output on disk (data set 10) the computed values for the error model terms. Note that the call to this routine precedes the final call to subroutine RESID so that the quantities output by this routine on data set 10 precede those output by RESID. The FORTRAN listing is given in Appendix A-3.4.

- Special Subroutine PRTIAL

The standard subroutine PRTIAL computes the discrepancies between observed and predicted measurements and also the partial derivatives of the predicted measurements with respect to those error model terms that affect the predicted measurements. The computed values are then stored on a disk file (ISFILE). Later in the program subroutine SOLVER forms the normal equations from this disk file and solves the equations to give the computed values for the error model terms. The quantities on the disk file are also used by subroutine RESID which prints the measurement residuals. (The residuals are updated discrepancies between observed and predicted measurements, where the predicted measurements reflect the latest values (from SOLVER) of computed error model terms. The quantities involved in this computation are the discrepancies and partial derivatives from subroutine PRTIAL, which are stored on disk file, and the difference between the computed values for the error model terms and the values used by subroutine PRTIAL for the predicted measurements).

Obviously, the more data points that are stored on ISFILE the longer it will be. For a one-week long arc of Minitrack data, ISFILE is about 3,000,000 bytes long (20 cylinders of disk space).

To print the final residuals would require a further 9,000,000 bytes (60 cylinders of disk space). Together with the remaining disk requirements of the NAP program this puts a severe strain on the total 360 system.

To make it practicable to use the NAP program for multi-arc cases, several changes were made to subroutine PRTIAL.

Changes to Subroutine PRTIAL. For each measurement all discrepancies for a pass (Minitrack message) are averaged to give the mean measurement discrepancy. The standard deviations are also computed and any discrepancies differing from the mean by more than three standard deviations are rejected. (The process is iterative, since as soon as a discrepancy is rejected a new mean and standard must be computed). The mean discrepancies are then output on ISFILE together with the appropriate partial derivatives. The time associated with the mean discrepancies is also computed. These measurements are written on the same tape on disk file as the discrepancies (FT37F001). They are also written on disk (FT35F001) in a NAP observation tape format. The standard deviations and the number of measurement points (not rejected) are written on disk (FT36F001). The FORTRAN listing of the subroutine is given in Appendix A-3.6.

• Changes to Subroutine RESID

There are two subroutines RESID that can be used in NAP-II. These are identified as STANDARD Subroutine RESID and SPECIAL Subroutine RESID. The Special subroutine was written to make multi-arc runs practical in terms of run time.

Standard Subroutine RESID. Three sets of changes were made to this subroutine. The new subroutine will work only if there are two or fewer kinds of measurements per station-pass. The first change involved writing the printed (as on data set 6) pass summary on disk (data set 10) for use by some postNAP program, and also on data set 34, which is a printed pass summary. The second change involved plotting the measurement residuals in addition to giving the numerical values. The third change involved the computation of the correlation coefficient between the errors of the two measurements. The reason for computing the correlation coefficient was that when the plotting facility was added to this subroutine, it looked as if there was some correlation between the two measurement errors. However, in most cases the correlation coefficient is very small. The FORTRAN listing of the subroutine is given in Appendix A-3.5.1.

Special Subroutine RESID. The computed values of the error model terms are copied from disk (FT10F001) and written on tape (FT37F002). The measurement residuals are computed as before. However, since there now is only one measurement time point per pass, the standard deviation cannot be computed. Instead, the standard deviation computed in subroutine PRTIAL is copied from disk (FT36F001) as is the number of measurement points. This information is written on the same tape as the new values for the error model terms. Finally, the new observation tape is copied from disk (FT35F001) to tape (FT37F003). The FORTRAN listing is given in Appendix A-3.5.2.

• Changes to Subroutine MESOLD

Terms were added to Subroutine MESOLD to reflect the complete Minitrack geometrical error model. The following should be added to the NAP-II User's Guide (Reference 4) to be consistent with these changes (Appendix IV, Page IV-2).

		12		15		16	
		ERROR MODEL TERM NO	MEASUREMENT CODE	RE	RP	RM	RL
6							
7		TM					

where measurement code 6 corresponds to direction cosine alpha (or ℓ), and measurement code 7 corresponds to direction cosine beta (or m), and $n = \sqrt{1 - (\ell^2 + m^2)}$

The 12th error model term (TM) is not part of the geometrical error model but corresponds to a timing bias.

RE and RP are rotation terms about the local vertical of the equatorial and polar m measurements, respectively. RL and RM are rotations or tilt about the ℓ or m measurements.

2.4.3 The NAP-II Minitrack Post-Processing Program

The post-processing program summarizes the results of a NAP-II Minitrack run and prepares the NAP-II "input cards" for the next iteration. Any lobe assignment errors of the Minitrack preprocessor can also be corrected through the NAP-II "input cards".

In order to execute the post-processing program, the NAP-II program must be a version employing the special subroutine PRTIAL and RESID given in Appendix A-3.6 and 3.5.2, respectively.

The program assumes that the station numbers assigned by NAP are odd for equatorial stations and even for polar stations and that measurement numbers are odd for "L" measurements and even for "M" measurements. (See Appendix A-4.)

The NAP-II control cards must be in a particular order required by the POSTNAP program. In general, error model terms should be setup in order of totally stable, arc stable and pass stable. The error model parameter numbers (Category 601, Key 7), must be in ascending and consecutive order. Cards must not be repeated.

This is not a restriction on the NAP-II program but a restriction imposed by POSTNAP.

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Card Input	Data Set 5	Only one card required.
	<u>Card Column</u>	<u>Word</u>
	1-5	IOPT
		<u>Definition</u>
		Determines which NAP "701" (continuation 1) cards are to be output. If measurements were previously edited out of the solution and no value for the pass standard deviation is available, the measurements are edited out again. IOPT can assume values of 0, -1 and +1. In all three cases the above applies. In all cases key 7 of 701 card is set to "1".
		= 0, measurements are edited out if mean pass measurement error exceeds MAXERR or if pass standard deviation exceeds SDMAX. If measurements are edited out, DATA 2 of 701 card is set to 1.D15.
		= -1, measurements are edited out if mean pass measurement exceeds MAXERR or if no pass standard deviation is available or if pass standard deviation exceeds SDMAX. If measurements are edited, DATA 2 is set to 1.D15.
		= +1, same as -1 case except if measurements are not edited out, they are assigned "a priori" sigma of 10 times pass standard deviation. If measurements are edited out, DATA 2 is set to 1.D7 times the pass standard deviation.

<u>Function</u>	<u>Unit</u>	<u>Description</u>	
	<u>Card Column</u>	<u>Word</u>	<u>Definition</u>
	6-10	MAXERR	Maximum mean measurement error in Minitrack counts.
	11-20	SDMAX	Maximum pass standard deviation (unscaled).
	21-30	FREQCY	Satellite transmitter frequency in MHz.

Note on the availability of a Pass Standard Deviation.

A pass standard deviation can only be computed if there is more than one measurement per pass. If IOPT = 1, the pass standard deviation is saved on a "701" card. (If key 7 = 0, it is equal to DATA 2 times 1.D-1; if Key 7 = 1, it is equal to DATA 2 times 1.D-7). Use is made of this facility when the data processing switches from using all measurements for a pass to the single new measurement computed in special subroutine PRTIAL.

Note on data editing.

A bad pass is defined as one whose mean error exceeds MAXERR or whose standard deviation exceeds SDMAX. Bad passes are edited out of the solution in all cases. If no standard deviation is available, then in the case of Iopt = -1 the pass will be edited out of the solution. (It is recommended that Iopt = -1 only be used if there are more than one data point per pass. The non-availability of a pass standard deviation may in that case be the result of the pass not meeting the elevation requirements. NAP in that case would output a zero mean pass error). Iopt = 1 should be used if the user wishes to weight the measurements of a pass in inverse proportion to their standard deviation, in other words, a noisy pass would be given less weight than one that is less noisy.

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Disk Input (on tape)	Data Set 27	NAP input cards used in making NAP run. This would normally be on a disk file created by the PRENAP card updating program.
Disk input (on tape)	Data Set 10, File 1 (FT10F001)	Output from NAP data set 37 (FT37F002). The computed values of error model parameters.
Disk input (on tape)	Data Set 10, File 2 (FT10F002)	Output from NAP data set 37 (FT37F001). Current measurement discrepancies.
Disk output (on tape)	Data Set 10, File 3 (FT10F003)	Output of sequenced NAP "input cards" for use by the PRENAP card updater program on the next iteration.
Printed output	Data Set 6	Prints the following <ul style="list-style-type: none"> • Some instructions on the use of the program. • Printout of input cards (data set 5). • Printout of NAP "output cards" (FT10F003) for the next iteration. The first column of this list are the sequence numbers.
Printed output	Data Set 20	The following is printed out for each station/pass. <ul style="list-style-type: none"> • Time of midpoint of pass. • Mean measurement error (This is the mean discrepancy computed in special subroutine PRTIAL and equals the mean residual error computed in subroutine RESID when the solution converges). • Standard deviation of the measurements for a pass. For only one measurement the standard deviation is equal to zero. • For each measurement, the time relative to midpoint and the error relative to mean pass error. This error is also plotted.
Printed Output	Data Set 31	Printout of the bias values used in the Minitrack preprocessor (built into the program) and the new bias. New biases are obtained by converting the bias obtained by NAP to Minitrack counts and adding the result to the preprocessor bias.

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Printed output	Data Set 31-60	<p>A summary for each station is written on a different data set. Each pass contains</p> <ul style="list-style-type: none"> • Time of midpoint measurement • Arc number • Pass number • Mean error in Minitrack counts • Whether () or not (*) the measurement met elevation requirement given on NAP "702" card • Whether () or not (*) measurement contributed to present solution • Measurement standard deviation in Minitrack counts • Bias correction made to the measurement for the next iteration expressed in Minitrack lobes (in 1000 Minitrack counts). The errors being corrected are due to wrong lobe assignments in the Minitrack preprocessor and are corrected via NAP "704" cards • Number of measurement points per pass on the data tape • Number of measurement points deleted by special subroutine PRTIAL • The mean error rate • The reduction in standard deviation, expressed as a percentage, that would result if the standard deviation were computed about the line defined by the mean error and mean error rate and not the mean error alone • The computed measurement. The predicted (NAP) measurement plus the mean pass measurement error, (computed in special subroutine PRTIAL). • Whether () or not (*) the measurement will contribute to the solution of the next iteration.

2.5 RESULTS OF MINITRACK DATA REDUCTIONS USING NAP-II

2.5.1 Estimation of Calibration Parameters for the Fort Myers Minitrack Station Using the GEOS-I Satellite and Optically Determined Reference Arcs

A number of GEOS-A arcs determined from optical observations were used as reference arcs. These arcs had previously been obtained by DBA Systems, Inc. for work on another contract. Since optical observations are considerably more accurate than Minitrack, the optical reference arcs could be considered perfect. The NAP program was then used to recover measurement biases and measurement scale factor errors. The Minitrack measurements for each pass were weighted in inverse proportion to the variance of the measurement error for each pass (Minitrack message).

The results are shown in Tables 2 and 4. Tables 1 and 3 give the actual measurements. Table 5 is a comparison of calibration results. Table 6 tabulates some observed frequencies. It shows that the fluctuation in the GEOS-A transmitter frequency is very small. Table 7 shows the effect of including the Doppler effect and wave propagation time delay in the computations. The total effect can be seen to be of the order of 1 Minitrack count.

TABLE 1

POLAR ARRAY. Observed values of direction cosines, direction cosines rates and prepass internal bias (KS2).

ARC Number	ORBIT Number	DATE(1966)			GMT			Direction Cosines			Direction Cosine Rates			KS2 (l) - 067	KS2 (m) - 560
		MTH	DAY	HRS.	MIN	l	m	n	\dot{l}	\dot{m}	\dot{n}				
1	700	1	4	6	23	.84	.00	.55	.0009	-.0030	-.0014	0	0		
2	712	1	5	6	27	.68	.01	.73	.0017	-.0037	-.0015	0	2		
3	784	1	11	6	50	-.87	.00	.49	.0004	-.0031	.0007	2	14		
5	831	1	15	5	4	-.21	.00	.98	.0026	-.0047	.0006	2	0		
7	843	1	16	5	7	-.52	.00	.85	.0017	-.0043	.0010	2	4		
9	855	1	17	5	11	-.72	.00	.69	.0009	-.0037	.0010	0	1		
10	866	1	18	3	14	.86	.07	.51	.0010	-.0027	-.0013	2	2		
11	867	1	18	5	16	-.84	.00	.54	.0005	-.0032	.0008	3	2		
12	914	1	22	3	30	-.10	.00	.99	.0027	-.0046	.0003	2	8		
15	938	1	24	3	37	-.67	.00	.74	.0011	-.0038	.0010	2	0		
16	949	1	25	1	40	.90	.00	.44	.0006	-.0024	-.0013	3	0		
17	961	1	26	1	44	.80	.01	.61	.0011	-.0029	-.0014	1	-1		
18	1080	2	5	0	20	.11	.00	.99	.0027	-.0043	-.0003	2	10		
19	1092	2	6	0	25	-.25	.00	.97	.0023	-.0043	.0006	4	3		
20	1408	3	4	9	19	-.43	.00	.90	.0012	.0022	.0006	6	-41		
21	1479	3	10	7	40	-.13	.00	.99	.0014	.0024	.0002	4	-51		
22	1680	3	27	2	40	.76	-.12	.64	.0005	.0021	-.0003	16	14		
23	1681	3	27	4	41	-.63	.00	.77	.0010	.0020	.0008	16	14		
24	1740	4	1	3	0	-.15	.00	.99	.0015	.0025	.0002	18	15		
25	1752	4	2	3	3	-.38	.02	.93	.0014	-.0023	.0005	18	15		

TABLE 2

POLAR ARRAY. Measurement Errors.

ARC No.	Standard Deviation Of Measurement Error About Mean For Pass		Mean Measurement Error For Pass MINITRACK COUNTS			
	σ_l	σ_m	Δl	Δm	Δl	Δm
1	.000072	.000147	-.000001	-.000135	0	-8
2	.000036	.000034	-.000038	-.000097	-2	-6
3	.000749	.000660	-.000164	-.000034	-9	-2
5	.000068	.000072	.000027	.000085	2	5
7	.000040	.000063	.000009	.000033	1	2
9	.000044	.000056	.000116	-.000005	7	0
10	.000239	.000141	-.000042	-.000023	-2	-1
11	.000261	.000353	.000033	-.000057	2	-3
12	.000044	.000032	.000155	-.000068	9	-4
15	.000071	.000081	.000048	.000125	3	7
16	.000133	.000173	.000112	.000029	6	2
17	.000042	.000048	.000011	.000005	1	0
18	.000035	.000034	.000003	.000098	0	6
19	.000044	.000057	-.000057	.000136	-3	8
20	*	.000038	*	.000036	*	2
21	.000052	.000048	.000087	.000047	5	3
22	.000085	.000092	.000130	.000118	7	7
23	.000029	.000032	.000003	.000018	0	1
24	.000039	.000034	-.000046	-.000005	-3	0
25	.000021	.000028	-.000062	-.000066	-4	-4

EW - BIAS: 137 MINICTS - .000021 = 136 MINICTS

NS - BIAS: 431 MINICTS + .000071 = 435 MINICTS

EW - SCALE FACTOR: -.00022

(Base Line is Shorter Than Assumed.)

TABLE 3

EQUATORIAL ARRAY. Observed values of direction cosines, direction cosine rates and prepass internal bias (KS2).

ARC Number	ORBIT No.	DATE(1966)		GMT		Direction Cosines			Direction Cosine Rates			KS2 (l) - 067	KS2 (m) - 560
		MTH	DAY	HRS.	MIN.	l	m	n	i	m	n		
1	700	1	4	6	18	.00	.88	.48	.0020	-.0007	.0013	-1	0
2	712	1	5	6	23	.00	.78	.62	.0022	-.0013	.0017	-1	2
4	819	1	14	4	59	.00	.26	.97	.0028	-.0042	.0011	-2	11
13	926	1	23	3	36	-.04	-.65	.76	.0023	-.0027	-.0022	4	-1
15	938	1	24	3	43	-.03	-.90	.43	.0016	-.0009	-.0018	2	0
17	961	1	26	1	38	.00	.85	.53	.0019	-.0008	.0013	1	-1
20	1408	3	4	9	23	.00	.57	.82	.0014	.0014	-.0010	6	-42
21	1479	3	10	7	42	.01	.21	.98	.0014	.0022	-.0005	5	-51
23	1681	3	27	4	48	.00	.73	.68	.0013	.0009	-.0010	16	14
25	1752	4	2	3	7	.00	.52	.85	.0014	.0016	-.0010	18	15

TABLE 4

EQUATORIAL ARRAY. Measurement Errors.

ARC No.	Standard Deviation Of Measurement Error About Mean For Pass		Mean Measurement Error For Pass			
	σl	σm	Δl	Δm	MINITRACK COUNTS	
					Δl	Δm
1	.000191	.000213	.000151	-.000080	7	-4
2	.000081	.000053	-.000013	-.000050	-1	-2
4	.000033	.000040	.000062	.000025	3	1
13	.000189	*	.000157	*	7	*
15	.000657	.000757	.000192	-.000397	9	-18
17	.000088	.000076	.000056	.000006	3	0
20	*	.000041	*	-.000007	*	0
21	.000031	.000041	-.000054	-.000040	-2	-2
23	.000071	.000043	.000113	.000012	5	1
25	.000034	.000039	-.000045	.000038	-2	2

EW - BIAS: 957 MINICTS + .000026 = 958 MINICTS

NS - BIAS: 988 MINICTS - .000544 = 988 MINICTS

NS - SCALE FACTOR: -.00049

(Base line is shorter than assumed.)

TABLE 5

COMPARISON OF CALIBRATION RESULTS

Source	DBA*	RCA**	Aircraft Calibration			Actual Values Used	
			July 1965	5 Nov 1965	3 Mar. 1966	5 Nov 1965	3 Mar. 1966
Equatorial Array							
EW - BIAS	958	956	956	957	969	954	959
NS - BIAS	988	985	988	992	988	988	988
Polar Array							
EW - BIAS	136	136	137	140	153	138	143
NS - BIAS	435	437	431	435	433	435	433
Equatorial Array							
NS - Scale Factor	-.00049	-.00015					
Polar Array							
EW - Scale Factor	-.00022	-.00022					

* The DBA computed calibration values are the ones shown in Tables I and II. They are based on observations from 4 January to 2 April 1966.

** The RCA results have been verbally communicated by Mr. Jerry Casto and are based on satellite observations covering approximately the same time period as those used by DBA.

TABLE 6

OBSERVED GEOS - A FREQUENCIES

(Source: Harry Pritchard, GSFC)

Date (1966)	Value (MHz)	Scale Error Relative To Nominal Value (136.83 MHz)
1 January	136.830360	26×10^{-7}
5 January	136.830350	26×10^{-7}
3 February	136.830038	3×10^{-7}
8 February	136.829675	-24×10^{-7}
17 March	136.830540	40×10^{-7}

TABLE 7

CHANGE IN PREDICTED MEASUREMENTS DUE TO INCLUSION OF
THE DOPPLER EFFECT AND WAVE PROPAGATION TIME DELAY

POLAR ARRAY			EQUATORIAL ARRAY		
<u>ARC No.</u>	<u>$10^6 \Delta I$</u>	<u>$10^6 \Delta m$</u>	<u>ARC No.</u>	<u>$10^6 \Delta I$</u>	<u>$10^6 \Delta m$</u>
1	-14	19	1	-15	17
2	-14	20	2	-15	18
3	-10	21	4	-13	20
5	-12	21	13	-11	x
7	-11	21	15	-11	21
9	-11	21	17	-14	18
10	-14	18	20	x	-17
11	-10	21	21	-11	-18
12	-12	20	23	-13	-16
15	-11	21	25	-12	-17
16	-14	18			
17	-14	19			
18	-13	20			
19	-11	20			
20	x	-18			
21	-11	-18			
22	- 8	-20			
23	-12	-17			
24	-11	-18			
25	-11	-17			

POLAR ARRAY: 1 MINITRACK Count = .0000175

EQUATORIAL ARRAY: 1 MINITRACK Count = .0000216

2.5.2 The Calibration of all Minitrack Stations Using GEOS-A Minitrack Measurements

The procedures followed in processing the Minitrack data are described in Section 2.6 of this report. The four arcs described in Table 15 were at first processed separately. A new data tape was created for each of the four arcs (see special subroutines PRTIAL and RESID). The arcs were then combined in pairs to give two, two-arc runs, and finally all the data were combined into a single four-arc run. Three sets of runs were made under slightly varying conditions (see Table 15): In the first run scale factors and antenna rotation terms were recovered in addition to measurement biases and the four state vectors. The second run was similar to the first except that no rotation terms were considered. This resulted in very slight differences in the solutions. The third run was similar to the first but in this run ionospheric corrections were made using the ionospheric model developed by DBA under Contract NAS511730. In all runs, data were edited out of the solution using the criteria listed in Tables 12 and 13. It should be mentioned that when the runs were made, no ionospheric data could be obtained for 1966. The 1971 values were therefore substituted. This may account for the relatively bad results obtained for run 3. Tables 8 through 14 refer to run 1. Table 8 is a comparison of calibration results. Table 9 lists the scale factor errors and antenna alignment errors. It can be seen that the scale errors are predominantly negative. This is the kind of effect that would be expected if no ionospheric corrections were made, i.e., it seems likely that the scale factors have absorbed some of the effect of ionospheric refraction. When ionospheric corrections were made (run 3), the recovered scale factors were indeed reduced in magnitude (the actual numbers are not included in this report).

Table 10 is a listing of the number of observations for each station. Table 11 gives the RMS values of the observed residuals. It is interesting to note that the Polar Array, which has a larger baseline, shows a larger RMS error than the Equatorial Array when the errors are expressed in Minitrack counts, but more or less the same RMS error in terms of angular error. From this, it could be inferred that the errors are caused less by the electronics of the observing stations, which measures Minitrack counts, than

by general uncertainties in conditions outside the observing station. This, in general, is probably true. However, it has been observed that large variations in the pre-calibration biases, which is part of the Minitrack message, have been accompanied by large residuals in the orbital fit. The Woomera Polar Station was particularly bad in this report. The measurement residuals and precalibration constants for that station are listed in Table 14 for illustrative purposes. Tables 12 and 13 are self-explanatory, as are Tables 15.1 through 15.4. It should be emphasized that the results given in Tables 15 are the most important results of this report.

In all orbital computations the Earth model used was that given in Appendix A-1. The affect of solar radiation pressure was not taken into account, and neither was the effect of the Earth's precession and nutation.

In all three runs the measurements were weighted proportionately to the standard deviation of the measurements within each message.

TABLE 8

Comparison of Calibration Results for
Equatorial and Polar Station Biases

<u>Station</u>	<u>This Program *</u>		<u>Aircraft</u> <u>65.12.31</u>		<u>Aircraft</u> <u>66.02.25</u>	
	<u>EW</u>	<u>NS</u>	<u>EW</u>	<u>NS</u>	<u>EW</u>	<u>NS</u>
Fort Myers (E)	956	981	954	988	953	984
Fort Myers (P)	135	435	138	435	137	435
Quito (E)	817	036	812	036	837	030
Quito (P)	756	000	760	002	763	006
Lima (E)	949	252	955	263	955	259
Lima (P)	023	881	028	882	028	882
Santiago (E)	078	057	073	060	076	059
Santiago (P)	950	972	943	967	943	963
New Foundland (E)	930	937	934	935	934	935
New Foundland (P)	170	920	171	919	171	919
Winkfield (E)	071	973	067	976	067	976
Winkfield (P)	868	001	870	011	870	011
Johannesburg (E)	048	937	054	932	054	932
Johannesburg (P)	084	876	090	871	090	871
Blossom Point (E)	948	094	948	096	948	096
Blossom Point (P)	081	887	082	889	082	889
College (E)	955	807	961	804	960	804
College (P)	846	932	854	916	859	919
Mojave (E)	030	576	017	579	029	575
Mojave (P)	079	123	062	129	079	121
Grand Forks (E)	068	951	060	954	061	951
Grand Forks (P)	602	001	598	990	598	990
Woomera (E)	020	944	031	938	031	938
Woomera (P)	934	118	948	118	948	118

* Time span covered was 66.1.1 - 66.2.3 and 66.3.12 - 66.3.19.

Table 9

Scale Factor Errors and Antenna Alignment Errors in Minitrack Counts

1000 Equatorial Minitrack Counts = .0216 radians
 1000 Polar Minitrack Counts = .0174 radians

	<u>Equatorial Array</u>		<u>Polar Array</u>	
	<u>Scale Error</u>	<u>Antenna Rotation</u>	<u>Scale Error</u>	<u>Antenna Rotation</u>
Fort Myers	-14	4	-15	2
Quito	9	-4	- 6	-2
Lima	-24	-4	30	-3
Santiago	- 2	-8	- 8	-2
New Foundland	- 8	0	-13	-2
Winkfield	- 4	-3	- 8	5
Johannesburg	- 6	-1	-14	-4
Blossom Point	-11	6	- 1	0
College	-10	8	- 4	0
Mojave	- 3	-3	- 7	4
Grand Forks	8	-5	- 8	-9
Woomera	-11	-3	- 8	-4

Scale Error

The predicted measurement is in error by an amount equal to the "scale error" multiplied by the actual measurement.

Antenna Rotation

The predicted measurement is in error because the antenna baselines are rotated anti-clockwise by the "antenna rotation".

In the equatorial mode the scale error only affects the m measurement and the antenna rotation only the l measurement.

In the polar mode the scale error only affects the l measurement and the antenna rotation only the m measurement.

Table 10

The Number of Minitrack Messages Used in the Orbit Determination
and the Determination of Biases, Scale Factors and Antenna Rotations

<u>Equatorial Array</u>	<u>Direction Cosine l</u>					<u>Direction Cosine m</u>				
	<u>Arc 1</u>	<u>Arc 2</u>	<u>Arc 3</u>	<u>Arc 4</u>	<u>Total</u>	<u>Arc 1</u>	<u>Arc 2</u>	<u>Arc 3</u>	<u>Arc 4</u>	<u>Total</u>
Fort Myers	4	4	11	12	31	4	4	11	12	31
Quito	1	-	2	4	7	1	-	-	3	4
Lima	-	3	-	2	5	-	3	2	-	5
Santiago	1	1	3	3	8	1	1	3	3	8
New Foundland	17	19	26	31	93	16	19	26	31	92
Winkfield	12	-	9	11	32	12	-	15	11	38
Johannesburg	-	1	3	2	6	-	1	3	2	6
Blossom Point	12	9	20	16	57	12	9	21	16	58
College	12	12	18	17	59	13	12	17	17	59
Mojave	12	11	17	14	54	12	11	17	14	54
Grand Forks	11	14	22	7	54	12	14	22	7	55
Woomera	<u>1</u>	<u>-</u>	<u>1</u>	<u>3</u>	<u>5</u>	<u>-</u>	<u>-</u>	<u>2</u>	<u>3</u>	<u>5</u>
Total	83	74	132	122	411	83	74	139	119	415

Table 10 (Continued)

The Number of Minitrack Messages Used in the Orbit Determination
and the Determination of Biases, Scale Factors and Antenna Rotations

<u>Polar Array</u>	<u>Direction Cosine l</u>					<u>Direction Cosine m</u>				
	<u>Arc 1</u>	<u>Arc 2</u>	<u>Arc 3</u>	<u>Arc 4</u>	<u>Total</u>	<u>Arc 1</u>	<u>Arc 2</u>	<u>Arc 3</u>	<u>Arc 4</u>	<u>Total</u>
Fort Myers	11	9	14	19	53	10	9	14	19	52
Quito	4	3	5	5	17	4	4	5	5	18
Lima	5	5	5	4	19	5	6	6	6	21
Santiago	4	2	5	5	16	4	3	5	4	16
New Foundland	9	14	14	17	54	9	14	14	18	55
Winkfield	3	-	2	3	8	3	-	2	2	7
Johannesburg	2	3	7	7	19	2	3	7	8	20
Blossom Point	13	9	15	20	57	12	9	15	20	58
College	7	5	9	8	29	7	6	9	7	29
Mojave	14	11	13	20	58	14	11	13	20	58
Grand Forks	4	7	18	10	39	4	7	18	10	39
Woomera	4	2	3	7	16	3	3	5	7	18
Total	80	71	110	125	385	77	75	112	124	389

Table 11
RMS Value of Residuals* in Minitrack Counts

<u>Station</u>	<u>Equatorial Array</u>		<u>Polar Array</u>	
	<u>l</u>	<u>m</u>	<u>l</u>	<u>m</u>
Fort Myers	2.7	5.6	5.1	4.5
Quito	3.2	8.9	7.4	5.2
Lima	3.7	9.3	6.6	5.7
Santiago	4.7	3.8	7.2	7.0
New Foundland	4.9	3.3	7.1	5.3
Winkfield	7.3	3.5	4.5	5.4
Johannesburg	3.6	2.8	4.5	4.0
Blossom Point	4.8	3.4	4.8	3.2
College	3.7	5.9	5.8	8.4
Mojave	3.1	5.3	5.2	5.1
Grand Forks	4.9	4.2	6.0	7.1
Woomera	<u>4.1</u>	<u>11.8</u>	<u>7.2</u>	<u>8.1</u>
All **	4.3	4.7	5.9	5.6

*The residuals are the differences between observed and predicted values.
 The predicted values are based on the computed orbit.

**It is of interest to note that the four RMS residuals for all stations expressed as unscaled quantities assume the values:

.000093, .000102, .000102, .00097.

The same residuals expressed as equivalent angular discrepancies at zenith assume the values: 19", 21", 21", 20", i.e., values around the quoted Minitrack accuracy of 20".

Table 12

Total Number of Minitrack Messages
and the Number of Rejected Messages

<u>Equatorial Array</u>	<u>Total Number Messages</u>	<u>Rejected (Elevation)</u>	<u>Direction Cosine l</u>		<u>Direction Cosine m</u>	
			<u>Rejected (Discrepancy)</u>	<u>Rejected (S.D.)</u>	<u>Rejected (Discrepancy)</u>	<u>Rejected (S.D.)</u>
Fort Myers	52	20		1		1
Quito	7				3	
Lima	5					
Santiago	9		1			1
New Foundland	99	5	1		3	
Winkfield	41		9		3	
Johannesburg	6					
Blossom Point	73	15	1			
College	69	6	3	1	3	1
Mojave	79	25				
Grand Forks	59	4	1			
Woomera	<u>6</u>	<u> </u>	<u>1</u>	<u> </u>	<u>1</u>	<u> </u>
Total	505	75	17	2	12	3

Rejection Criteria

Elevation. All messages the mean elevation of which was below 25° .

Discrepancy. All direction cosines having a residual error in excess of 20 Minitrack Counts.

S.D. All direction cosines having an error with a standard deviation in excess of 0.00050, the computed standard deviation being based on all measurements within a Minitrack message.

Rejected measurements are only listed under one heading even if they should have been rejected for more than one reason. Thus, the total number of measurements less the number of rejected measurements equals the number of measurements used in the computations (Table 3).

Table 12 (Continued)

Total Number of Minitrack Messages
and the Number of Rejected Messages

<u>Polar Array</u>	<u>Total Number Messages</u>	<u>Rejected Elevation</u>	<u>Direction Cosine l</u>		<u>Direction Cosine m</u>	
			<u>Rejected Discrepancy</u>	<u>Rejected (S.D.)</u>	<u>Rejected Discrepancy</u>	<u>Rejected (S.D.)</u>
Fort Myers	72	18		1		2
Quito	19		1	1	1	
Lima	21			2		
Santiago	22	1	4	1	3	2
New Foundland	74	19	1			
Winkfield	8				1	
Johannesburg	20		1			
Blossom Point	82	24	1		2	
College	76	40	1	6	1	6
Mojave	70	10	1	1	1	1
Grand Forks	51	11	1			1
Woomera	<u>20</u>	<u>—</u>	<u>4</u>	<u>—</u>	<u>2</u>	<u>—</u>
Total	535	123	15	12	11	12

Rejection Criteria

- Elevation. All messages the mean elevation of which was below 25° .
- Discrepancy. All direction cosines having a residual error in excess of 20 Minitrack Counts.
- S.D. All direction cosines having an error with a standard deviation in excess of 0.00050, the computed standard deviation being based on all measurements within a Minitrack message.

Rejected measurements are only listed under one heading even if they should have been rejected for more than one reason. Thus, the total number of measurements less the number of rejected measurements equals the number of measurements used in the computations (Table 3).

Table 13

Total Number of Measurements and Number of Rejected Messages

	Total Measurements	Rejected (Elevation)	Rejected (Discrepancy)	Rejected (S.D.)	Used In Computation
Number	2080	396	55	29	1600
Percent	100	19.0	2.6	1.4	77.0

Rejection Criteria

- Elevation. All measurements at a mean elevation below 25° .
- Discrepancy All measurements having a residual error in excess of 20 Minitrack Counts
- S.D. All measurements having an error with a standard deviation in excess of 0.00050, the computed standard deviation being based on all measurements within a Minitrack message.
- Rejected measurements are only listed under one heading even if they should have been rejected for more than one reason.

Table 14
Residual Measurement Errors and Prepass Calibration Constants
for the Woomera Polar Station

<u>Arc</u>	<u>Date</u>	<u>Time (hrs)</u>	<u>Residual Measurement</u>		<u>KC-KS1 + KS2</u>	
			<u>l</u>	<u>m</u>	<u>l</u>	<u>m</u>
1	1.2.66	5.2	11	3	345	557
1	1.3.66	18.7	-10	5	344	545
1	1.4.66	18.8	- 2	30	343	551
1	1.5.66	18.8	0	5	342	570
2	1.11.66	17.2	- 9	-14	345	584
2	1.12.66	17.2	5	- 8	343	584
2	1.13.66	17.3	31	-16	305	576
3	1.28.66	14.2	65	7	152	546
3	1.28.66	22.8	98	- 2	124	544
3	1.29.66	14.3	-34	65	224	545
3	1.29.66	22.9	-16	12	222	541
3	1.30.66	22.9	3	4	221	540
3	2.3.66	12.6	14	10	160	541
4	3.12.66	4.8	1	-11	561	719
4	3.12.66	13.4	- 4	0	561	717
4	3.13.66	4.9	0	- 1	560	717
4	3.13.66	13.5	4	- 5	560	717
4	3.15.66	13.6	0	- 1	560	717
4	3.16.66	13.7	- 2	1	561	713
4	3.19.66	3.3	2	-12	563	716

Table 15.1

Comparison of a GEOS-A Arc Determined from Minitrack Data with an Orbit
Determined from Optical Data

Start Time 1.1.66 6 hours
 Stop Time 1.5.66 19 hours
 Length of Arc 4.5 days

	Run 1	Run 2	Run 3
RMS Position Difference (m)	67	69	149
RMS Velocity Difference (m./sec)	.044	.046	0.100
Maximum Position Difference (m)	103	122	237
Maximum Velocity Difference (m./sec)	.063	.074	0.140

- Run 1. Minitrack orbit with measurement bias, scale factor, and rotation recovery. No ionospheric corrections.
- Run 2. Minitrack orbit with measurement bias and scale factor recovery. No ionospheric corrections.
- Run 3. Minitrack orbit with measurement bias, scale factor, and rotation recovery. Ionospheric corrections.

It is of interest to compare the above results with those quoted in "Intercomparison of the Minitrack and Optical Tracking Networks using GEOS-I Long Arc Orbital Solutions" (by J. G. Marsh, C. E. Doll, R. J. Sandifer and W. A. Taylor, NASA-TND-5337, February 1970). For an arc covering almost the identical period, they obtained an RMS position difference of 165 meters in a similar comparison. However, they did not attempt to recover any station calibration parameters. They made no ionospheric corrections.

Table 15.2

Comparison of a GEOS-A Arc Determined from Minitrack Data with an Orbit
Determined from Optical Data

Start Time	1.8.66	0 hours			
Stop Time	1.14.66	5 hours			
Length of Arc	6.2	days			
			Run 1	Run 2	Run 3
RMS Position Difference (m)			86	116	160
RMS Velocity Difference (m/sec)			.075	.099	.127
Maximum Position Difference (m)			127	180	262
Maximum Velocity Difference (m/sec)			.120	.158	.180

- Run 1. Minitrack orbit with measurement bias, scale factor, and rotation recovery. No ionospheric corrections.
- Run 2. Minitrack orbit with measurement bias and scale factor recovery. No ionospheric corrections.
- Run 3. Minitrack orbit with measurement bias, scale factor, and rotation recovery. Ionospheric corrections.

Table 15.3

Comparison of a GEOS-A Arc Determined from Minitrack Data with an Orbit

Determined from Optical Data

Start Time 1.28.66 2 hours
 Stop Time 2.4.66 0 hours
 Length of Arc 6.9 days

	Run 1	Run 2	Run 3
RMS Position Difference (m)	124	114	182
RMS Velocity Difference (m/sec)	.103	.099	.155
Maximum Position Difference (m)	194	181	272
Maximum Velocity Difference (m/sec)	.155	.153	.231

- Run 1. Minitrack orbit with measurement bias, scale factor, and rotation recovery. No ionospheric corrections.
- Run 2. Minitrack orbit with measurement bias and scale factor recovery. No ionospheric corrections.
- Run 3. Minitrack orbit with measurement bias, scale factor, and rotation recovery. Ionospheric corrections.

Table 15.4

Comparison of a GEOS-A Arc Determined from Minitrack Data with an Orbit
Determined from Optical Data

Start Time 3.12.66 3 hours
 Stop Time 3.19.66 20 hours
 Length of Arc 7.6 days

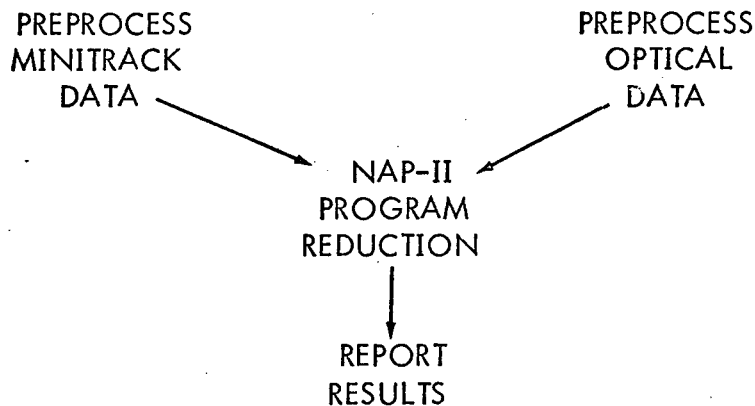
	Run 1	Run 2	Run 3
RMS Position Difference (m)	168	179	249
RMS Velocity Difference (m/sec)	.142	.152	.207
Maximum Position Difference (m)	251	250	406
Maximum Velocity Difference (m /sec)	.207	.215	.315

- Run 1. Minitrack orbit with measurement bias, scale factor, and rotation recovery. No ionospheric corrections.
- Run 2. Minitrack orbit with measurement bias and scale factor recovery. No ionospheric corrections.
- Run 3. Minitrack orbit with measurement bias, scale factor, and rotation recovery. Ionospheric corrections.

2.6 RECOMMENDED PROCEDURE FOR REDUCING MINITRACK DATA

2.6.1 Reduction Procedure

The purpose of this section is to provide a step-by-step procedure to be followed for the reduction of Minitrack data and optical data. This procedure can be simplified into three or four parts.



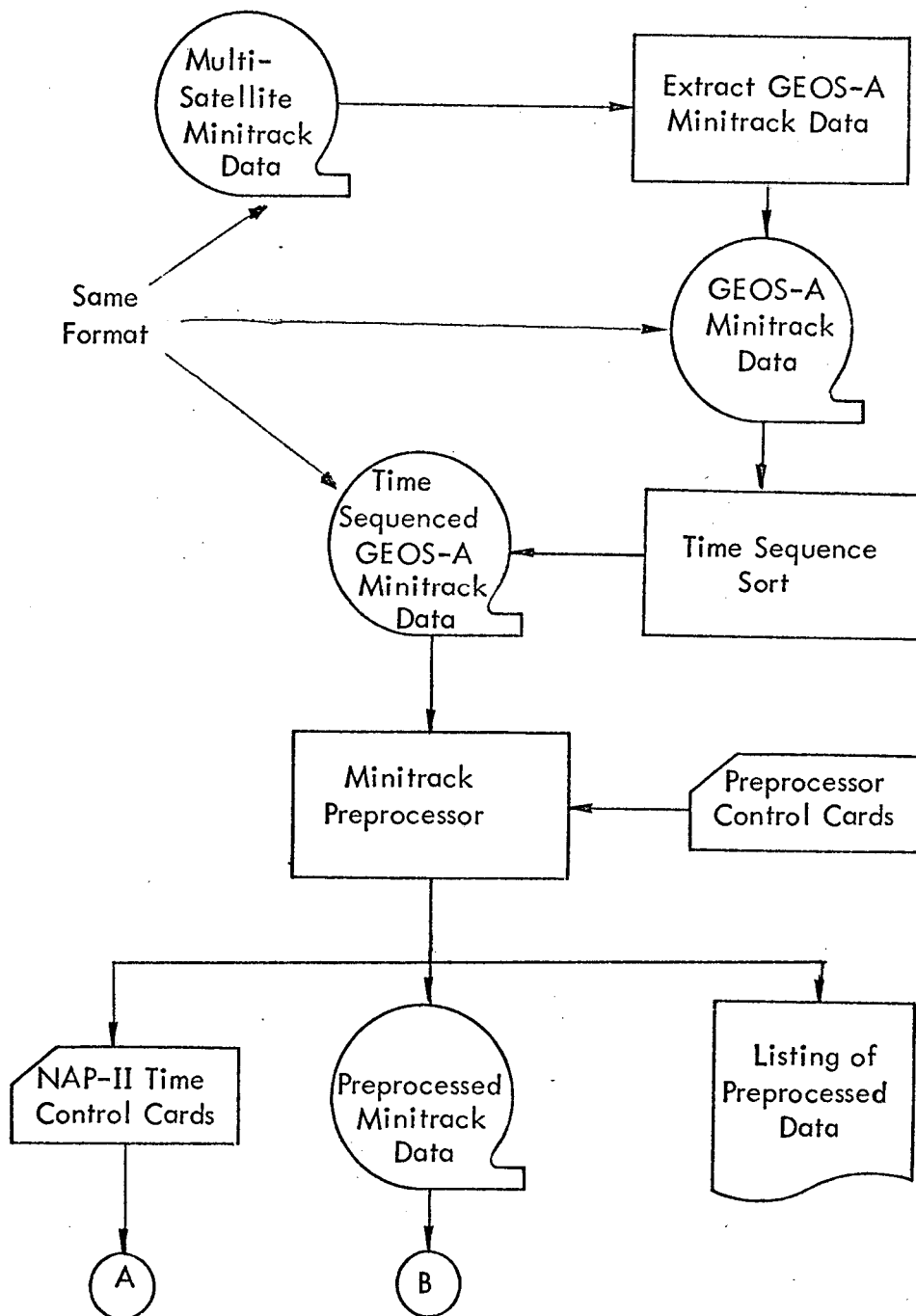
The preprocessing of the Minitrack data and the Optical data can be done as a series or parallel effort. The same applies to the NAP-II reduction of the data.

The steps to a complete reduction of the Minitrack data are:

1. Extract desired data from Minitrack and/or Optical data tapes.
 2. Sort Minitrack messages in time sequence (not required for Optical data when GEOS formatted data tapes are used).
 3. Preprocess Minitrack and/or Optical data.
 4. Set up NAP-II control cards and write cards on magnetic tape.
 5. Make PRENAP card updater run.
 6. NAP-II program execution.
 7. POSTNAP program execution.
 8. Report results after reduction has converged.
- } Iterate on these
3 steps until
convergence
achieved

A flow diagram for the preprocessing of the Minitrack data is given in Figure 1. Note: In setting up these runs, refer to Appendix A-4 for restriction place on card set-up.

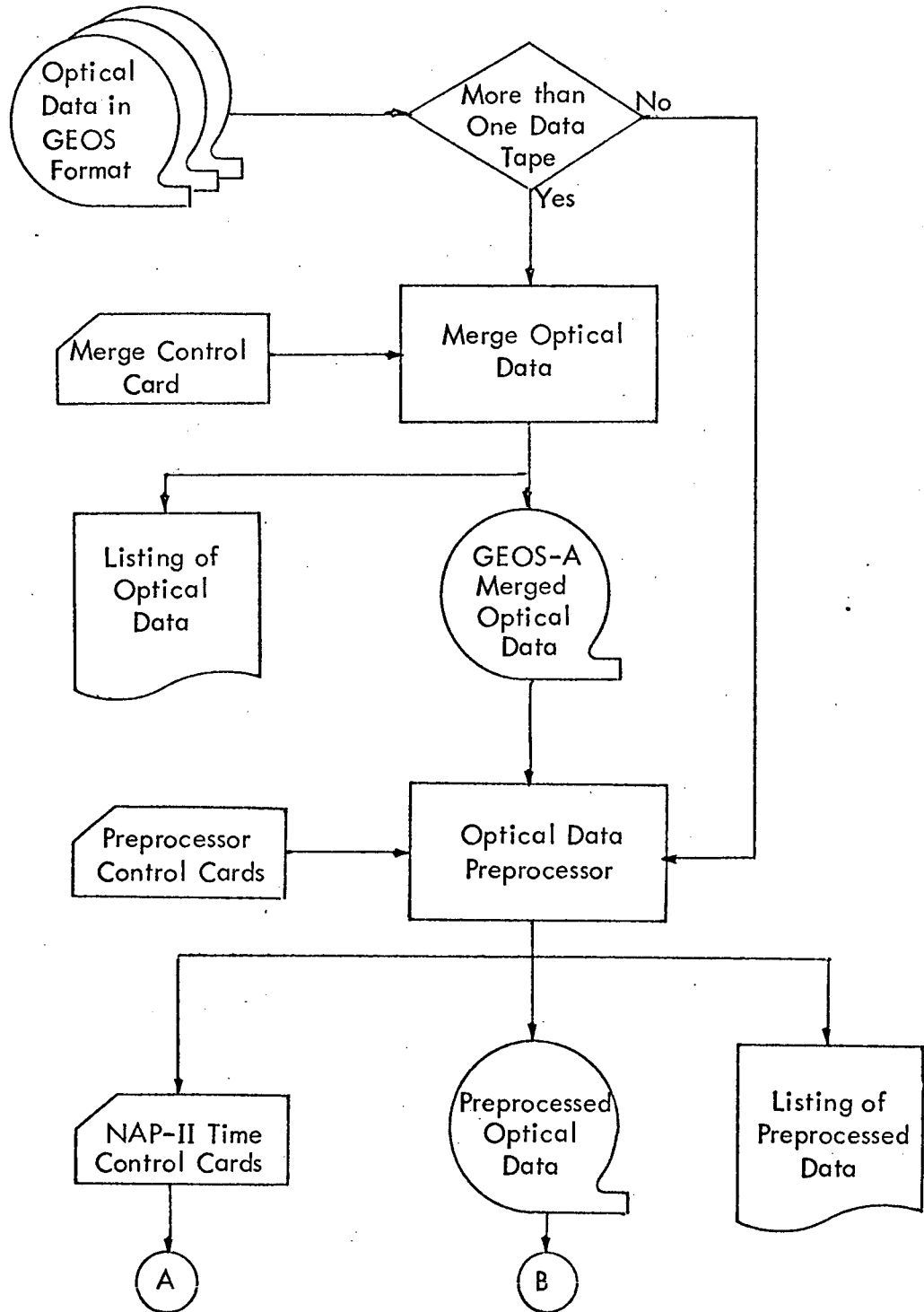
FIGURE 1
MINITRACK PREPROCESSING



The process starts with a magnetic tape containing Minitrack messages from several satellites. This tape is input to a program to extract just the messages from GEOS-1 satellite and writes them on another magnetic tape in the same format. This tape is then input to a program that sorts the messages, and also edits duplicate messages and puts them in time sequence on magnetic tape. This tape is now in the right form for the preprocessor program. The time-sequenced data tape, along with preprocessor control cards, are now input to the Minitrack preprocessor program. The preprocessor makes known corrections to the data and converts the corrected phase differences to direction cosines. The program outputs a data tape in a format acceptable to NAP-II and also a listing of the corrected data. The preprocessor also outputs a bulk of the NAP-II control cards dealing with the station times for the data (Category 201, 202, and 999). These are used in selection of data to be processed. This ends the pre-processing phase of the procedure. The preprocessing of Minitrack data is discussed in Section 2.2 of this report.

Figure 2 is a flow diagram of the preprocessing of optical data. The data input to the Optical preprocessing program must be in time sequence. If there are more than one tracking systems data to be processed, the data tapes must be "merged" onto one data tape. The output from the merge program is a data tape, in GEOS format, and a listing of the data. This data tape is input to the Optical preprocessor with control cards that specify the stations and times of the data to be processed. In the case of the SAO stations, these cards are also used to correct the observation times from A.1 to UTC. The Optical preprocessor outputs a data tape in a format acceptable to NAP-II and punched cards used in NAP-II to control data times. There is also a printed output of the reformatted and corrected data. The optical data preprocessing is discussed in Section 2.3 of this report.

FIGURE 2
OPTICAL PREPROCESSING



Once the data has been preprocessed, it is ready to be reduced using the NAP-II program. This process is flowed in Figure 3. The first step is to set up the NAP-II control cards as specified by the NAP-II User's Guide. The timing cards (Category 201, 202, and 999) are output as a result of the preprocessor. After the cards are set up, they are written on magnetic tape, for ease of handling. The cards on tape can be changed via the PRENAP card updater. This program is discussed in Section 2.4.1 of this report.

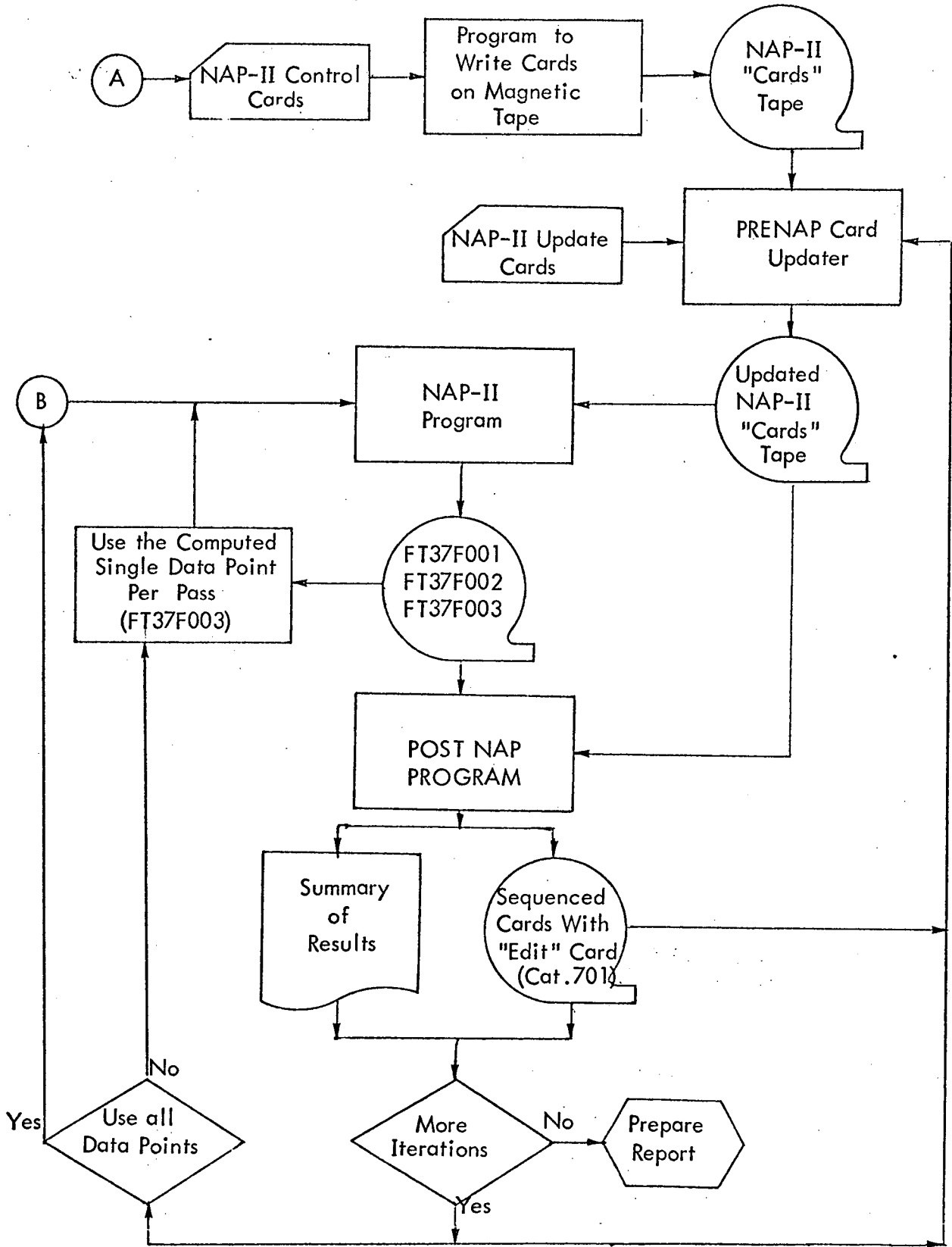
The NAP-II control cards (now on tape) and the data tape output from the preprocessor are now input to the NAP-II program. At the end of each iteration, NAP-II outputs a disk file (on tape) with the current values of the error model parameters and the measurement discrepancies. Also output is a "single point" data tape which can be used on successive iterations to reduce the computation time. When using the "single point" data tape for Minitrack data, delete the Category 704 cards.

The output from the NAP-II program is then input to the POSTNAP program which, in effect, gives a status report of the reduction and prepares information for the next iteration.

The PRENAP, NAP, POSTNAP sequence is continued until the solution has converged.

FIGURE 3

NAP-II REDUCTION



C.5

2.6.2 Recommended Error Model

The results of this study indicate the following error models to be sufficient for reducing Minitrack data.

The error model terms to be used are dependent on whether the data was collected in the equatorial or polar modes.

EQUATORIAL ARRAY

$$l = l_0 + b_1 + r_e m_0 + \tau \dot{l}$$

$$m = m_0 + b_2 + s_e m_0 + \tau \dot{m}$$

POLAR ARRAY

$$l = l_0 + b_3 + s_p l_0 + \tau \dot{l}$$

$$m = m_0 + b_4 + r_p l_0 + \tau \dot{m}$$

where,

l_0 and m_0 are Minitrack measurements in
Minitrack counts/1000.

b_1, b_2, b_3 and b_4 are zero-set biases

r_e and r_p are rotation terms about the local vertical
of equatorial l and polar m measurements
respectively

s_e and s_p are scale factors of equatorial m and polar l
measurements respectively

τ is the timing error associated with the station

\dot{l} and \dot{m} are computed rates obtained from the orbital
equations within NAP-II

These error model terms are coded for input to NAP-II (see Reference 4,
The NAP-II User's Guide, Appendix IV-B).

The error model terms would correspond to the following term numbers for direction cosine data types (measurement code 6 and 7).

<u>Error Model Term</u>	<u>Error Model Term No.</u>
b_1, b_2, b_3, b_4	10
r_e and r_p	15 (see changes to MESOLD in Section 2.4.2)
s_e and s_p	14
τ	11

Note: Consult NAP-II User's Guide, Appendix IV-2.

2.6.3 Typical Set-up for NAP-II Program

The following is an example of a set of NAP-II control cards. This listing is output from the NAP-II program on each run.

Note that each station is defined twice (category 301, 302, and 303); once for the equatorial array and once for the polar array. Following the survey cards are the error model cards (category 601). For ease of recognition, the labels have been coded as to which term it is, i.e. FTMYRELB is the FTMYR station equatorial "l" measurement zero-set bias "B". FTMYRPLB is the polar "l" measurement bias. Other codes used are "ELS" and "PLS" for equatorial "l" scale and polar "l" scale, "ELR" and "PLR" for equatorial "l" rotation and polar "l" rotation.

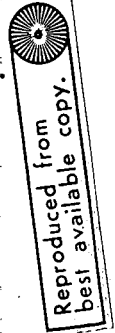
It is recommended that a new user of NAP-II take the following listing and, using the NAP-II User's Guide, cross-reference the codes used in the listing to their meaning given in the User's Guide.

See Appendix A-4 for restriction on deck setup.

CENTRAL DATA LISTING

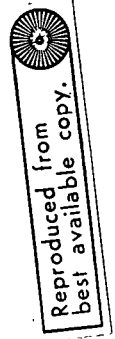
DATA1

CATEGORY	CONTINUE	LABEL	KEY1	KEY2	KEY3	KEY4	KEY5	KEY6	KEY7	KEY8	KEY9	KEY10	DATA1	DATA2
101	0	MIRARC2	2	1	0	0	2	2	0	1	0	0	1	0.0
102	0	LCENTRCH	5	0	0	0	0	0	0	0	0	0	0	0.0
103	6		2	13	12	0	0	0	0	0	0	0	0	-0.126297000000000000-18
103	7		2	13	12	0	0	0	0	0	0	0	0	0.165220000000000000-18
103	7		2	14	12	0	0	0	0	0	0	0	0	0.139578000000000000-20
103	7		2	14	12	0	0	0	0	0	0	0	0	-0.131772000000000000-19
103	6		2	15	12	0	0	0	0	0	0	0	0	-0.132126000000000000-19
103	7		2	15	12	0	0	0	0	0	0	0	0	-0.138635000000000000-20
103	7		2	9	1	0	0	0	0	0	0	0	0	0.788000000000000000-09
103	6		2	12	12	0	0	0	0	0	0	0	0	-0.273300000000000000-18
103	7		2	12	12	0	0	0	0	0	0	0	0	0.710000000000000000-20
103	7		2	13	12	0	0	0	0	0	0	0	0	0.116520000000000000-18
103	6		2	13	13	0	0	0	0	0	0	0	0	-0.239000000000000000-19
103	7		2	13	13	0	0	0	0	0	0	0	0	0.211000000000000000-19
103	6		2	14	11	0	0	0	0	0	0	0	0	0.56255555555555550000-21
103	7		2	14	11	0	0	0	0	0	0	0	0	-0.47295555555555550000-21
103	6		2	14	13	0	0	0	0	0	0	0	0	0.575000000000000000-21
103	7		2	14	13	0	0	0	0	0	0	0	0	0.690000000000000000-20
103	6		2	14	14	0	0	0	0	0	0	0	0	-0.153100000000000000-21
103	7		2	14	14	0	0	0	0	0	0	0	0	0.413000000000000000-22
103	6		2	15	9	0	0	0	0	0	0	0	0	-0.241000000000000000-18
103	7		2	15	9	0	0	0	0	0	0	0	0	0.483000000000000000-18
103	6		2	15	13	0	0	0	0	0	0	0	0	-0.776000000000000000-21
103	7		2	15	13	0	0	0	0	0	0	0	0	-0.37355555555555550000-21
103	6		2	15	14	0	0	0	0	0	0	0	0	0.114000000000000000-22
103	7		2	15	14	0	0	0	0	0	0	0	0	-0.53755555555555550000-22
104	0	INTEGRAT	4	0	3	4	1	2	0	0	0	0	0	0.216000000000000000-05
104	1	SPRCH 01	3	1	0	0	68	2	27	23	50	0	0	0.584000000000000000-02
104	4	SUN X	4	1	0	0	0	0	0	0	0	0	0	0.13743918395200000000-12
104	4	SUN Y	4	2	0	0	0	0	0	0	0	0	0	-0.45288863295895950000-11
104	4	SUN Z	4	3	0	0	0	0	0	0	0	0	0	-0.21636261132300000000-11
104	4	SUN XC	4	4	0	0	0	0	0	0	0	0	0	0.11424768069600000000-05
104	4	SUN YD	4	5	0	0	0	0	0	0	0	0	0	0.22530418236700000000-05
104	4	SUN ZD	4	6	0	0	0	0	0	0	0	0	0	0.11473121980100000000-05
104	4	RCEN X	3	1	0	0	0	0	0	0	0	0	0	0.38152809466700000000-09
104	4	RCEN Y	3	2	0	0	0	0	0	0	0	0	0	-0.14952777913100000000-09
104	4	RCEN Z	3	3	0	0	0	0	0	0	0	0	0	-0.87005198765999000000-08
104	4	RCEN XD	3	4	0	0	0	0	0	0	0	0	0	0.49592155211200000000-03
104	4	RCEN YD	3	5	0	0	0	0	0	0	0	0	0	0.80035027314000000000-03
104	4	RCEN ZD	3	6	0	0	0	0	0	0	0	0	0	0.41547918292800000000-03
301	0	FTREQ	1	5	0	3	0	0	0	26	32	0	0	0.531900000000000000-02
302	0	FTREQ	1	0	0	0	0	0	0	278	8	0	0	0.374000000000000000-01
301	0	FTREQ	2	5	0	103	0	0	0	0	0	0	0	-0.436810000000000000-02
302	0	FTREQ	2	0	0	0	0	0	0	278	6	0	0	0.374000000000000000-01
303	0	FTREQ	2	0	0	0	0	0	0	0	0	0	0	-0.436810000000000000-02
301	0	QUITDGE	3	5	0	5	0	0	0	0	0	0	0	0.227500000000000000-02
302	0	QUITDGE	3	0	0	0	0	0	0	291	25	0	0	0.153490000000000000-02
303	0	QUITDGE	3	0	0	0	0	0	0	0	0	0	0	0.335780000000000000-04
301	0	QUITDGP	4	5	0	105	0	0	0	0	0	0	0	0.227490000000000000-02



CATEGORY CONTINUE

	LAGLL	KEY1	KEY2	KEY3	KEY4	KEY5	KEY6	KEY7	KEY8	KEY9	KEY10		DATA1	DATA2
302	0	QUITSP	4	0	0	0	0	0	0	0	201	25	0.153450000000000000000000000000	02 0.0
303	0	QUITBP	4	0	0	0	0	0	0	0	0	0	0.3557001000000000000000000000	04 0.0
301	0	LIMAPSE	5	0	0	0	0	0	0	-1	11	40	0.3762000000000000000000000000	02 0.0
302	0	LIMAPGE	5	0	0	0	0	0	0	0	232	50	0.5802100000000000000000000000	02 0.0
303	0	LIMAPPE	5	0	0	0	0	0	0	0	0	0	0.8727900000000000000000000000	02 0.0
301	0	LIMAPAP	6	5	0	0	0	0	0	-1	11	40	0.3762000000000000000000000000	02 0.0
302	0	LIMAPAP	6	0	0	0	0	0	0	0	202	50	0.5902100000000000000000000000	02 0.0
303	0	LIMAPAP	6	0	0	0	0	0	0	0	0	0	0.8727900000000000000000000000	02 0.0
301	0	SNTASGE	7	0	0	0	0	0	0	-1	23	10	0.5902000000000000000000000000	02 0.0
302	0	SNTASGE	7	0	0	0	0	0	0	0	201	10	0.5902000000000000000000000000	02 0.0
303	0	SNTASGE	7	0	0	0	0	0	0	0	0	0	0.7325400000000000000000000000	03 0.0
301	0	SNTAGAP	8	5	0	0	0	0	0	-1	33	10	0.5902000000000000000000000000	02 0.0
302	0	SNTAGAP	8	0	0	0	0	0	0	0	201	19	0.5902000000000000000000000000	02 0.0
303	0	SNTAGAP	8	0	0	0	0	0	0	0	0	0	0.7325400000000000000000000000	03 0.0
301	0	HEMFLGE	9	5	0	12	0	0	0	0	47	44	0.2502000000000000000000000000	02 0.0
302	0	HEMFLGE	9	0	0	0	0	0	0	0	307	15	0.4686200000000000000000000000	02 0.0
303	0	HEMFLGE	9	0	0	0	0	0	0	0	0	0	0.5222800000000000000000000000	02 0.0
301	0	HEMFLAP	10	5	0	112	0	0	0	0	47	44	0.2502000000000000000000000000	02 0.0
302	0	HEMFLAP	10	0	0	0	0	0	0	0	307	15	0.4686200000000000000000000000	02 0.0
303	0	HEMFLAP	10	0	0	0	0	0	0	0	0	0	0.5222800000000000000000000000	02 0.0
301	0	WAKFLGE	11	5	0	15	0	0	0	0	51	26	0.4559300000000000000000000000	02 0.0
302	0	WAKFLGE	11	0	0	0	0	0	0	0	359	15	0.7937600000000000000000000000	01 0.0
303	0	WAKFLGE	11	0	0	0	0	0	0	0	0	0	0.7606800000000000000000000000	02 0.0
301	0	WAKFLAP	12	5	0	115	0	0	0	0	51	26	0.4559300000000000000000000000	02 0.0
302	0	WAKFLAP	12	0	0	0	0	0	0	0	359	18	0.7907000000000000000000000000	01 0.0
303	0	WAKFLAP	12	0	0	0	0	0	0	0	0	0	0.7606800000000000000000000000	02 0.0
301	0	JOBFLGE	13	5	0	16	0	0	0	-1	25	33	0.2705000000000000000000000000	01 0.0
302	0	JOBFLGE	13	0	0	0	0	0	0	0	27	42	0.2542600000000000000000000000	02 0.0
303	0	JOBFLGE	13	0	0	0	0	0	0	0	0	0	0.1530776000000000000000000000	04 0.0
301	0	JOBFLAP	14	5	0	116	0	0	0	-1	25	33	0.2705000000000000000000000000	01 0.0
302	0	JOBFLAP	14	0	0	0	0	0	0	0	27	42	0.2542600000000000000000000000	02 0.0
303	0	JOBFLAP	14	0	0	0	0	0	0	0	0	0	0.1530776000000000000000000000	04 0.0
301	0	ULASKGE	15	0	0	19	0	0	0	0	64	58	0.3575200000000000000000000000	02 0.0
302	0	ULASKGE	15	0	0	0	0	0	0	0	212	26	0.3027600000000000000000000000	02 0.0
303	0	ULASKGE	15	0	0	0	0	0	0	0	0	0	0.2646340000000000000000000000	03 0.0
301	0	ULASKAP	16	5	0	119	0	0	0	0	04	58	0.3075200000000000000000000000	02 0.0
302	0	ULASKAP	16	0	0	0	0	0	0	0	212	28	0.3027600000000000000000000000	02 0.0
303	0	ULASKAP	16	0	0	0	0	0	0	0	0	0	0.2646340000000000000000000000	03 0.0
301	0	MAGFLGE	17	5	0	21	0	0	0	-1	35	37	0.3005500000000000000000000000	02 0.0
302	0	MAGFLGE	17	0	0	0	0	0	0	0	140	57	0.1359000000000000000000000000	02 0.0
303	0	MAGFLGE	17	0	0	0	0	0	0	0	0	0	0.9400150000000000000000000000	03 0.0
301	0	MAGFLAP	18	5	0	121	0	0	0	-1	35	37	0.3005500000000000000000000000	02 0.0
302	0	MAGFLAP	18	0	0	0	0	0	0	0	140	57	0.1359000000000000000000000000	02 0.0
303	0	MAGFLAP	18	0	0	0	0	0	0	0	0	0	0.9400150000000000000000000000	03 0.0
301	0	MAGDAGE	19	5	0	23	0	0	0	-1	35	37	0.3005500000000000000000000000	02 0.0
302	0	MAGDAGE	19	0	0	0	0	0	0	0	47	17	0.3005500000000000000000000000	02 0.0
303	0	MAGDAGE	19	0	0	0	0	0	0	0	0	0	0.1355900000000000000000000000	04 0.0
301	0	MAGDAP	20	5	0	123	0	0	0	-1	35	37	0.3005500000000000000000000000	02 0.0
302	0	MAGDAP	20	0	0	0	0	0	0	0	47	17	0.3005500000000000000000000000	02 0.0
303	0	MAGDAP	20	0	0	0	0	0	0	0	0	0	0.1355900000000000000000000000	04 0.0



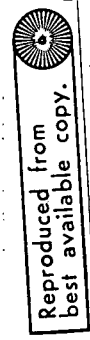
CONTROL DATA LISTING

CATEGORY CONTINUE LABEL KEY1 KEY2 KEY3 KEY4 KEY5 KEY6 KEY7 KEY8 KEY9 KEY10 DATA1 DATA2

CATEGORY	CONTINUE	LABEL	KEY1	KEY2	KEY3	KEY4	KEY5	KEY6	KEY7	KEY8	KEY9	KEY10	DATA1	DATA2
301	0	SPRINGE	21	5	0	1	0	0	0	0	0	29	25	0.456345600000000000 02 0.0
302	0	SPRINGE	21	5	0	0	0	0	0	0	0	29	25	0.486782000000000000 02 0.0
303	0	SPRINGE	21	5	0	0	0	0	0	0	0	29	25	0.555000000000000000 02 0.0
301	0	SPRINGE	22	5	0	101	0	0	0	0	0	28	25	0.456345600000000000 02 0.0
302	0	SPRINGE	22	5	0	0	0	0	0	0	0	202	54	0.486782000000000000 02 0.0
303	0	SPRINGE	22	5	0	0	0	0	0	0	0	202	54	0.555000000000000000 02 0.0
301	0	COLLEGE	23	5	0	13	0	0	0	0	0	64	52	0.177850000000000000 02 0.0
302	0	COLLEGE	23	5	0	0	0	0	0	0	0	212	9	0.365570000000000000 02 0.0
303	0	COLLEGE	23	5	0	0	0	0	0	0	0	212	9	0.139850000000000000 03 0.0
301	0	COLLEGE	24	5	0	113	0	0	0	0	0	64	52	0.177850000000000000 02 0.0
302	0	COLLEGE	24	5	0	0	0	0	0	0	0	212	9	0.365570000000000000 02 0.0
303	0	COLLEGE	24	5	0	0	0	0	0	0	0	212	9	0.139850000000000000 02 0.0
301	0	MCJAVSP	25	5	0	17	0	0	0	0	0	35	19	0.478300000000000000 03 0.0
302	0	MCJAVSP	25	5	0	0	0	0	0	0	0	243	5	0.595000000000000000 02 0.0
303	0	MCJAVSP	25	5	0	0	0	0	0	0	0	243	5	0.672200000000000000 02 0.0
301	0	MCJAVSP	26	5	0	117	0	0	0	0	0	35	19	0.478300000000000000 03 0.0
302	0	MCJAVSP	26	5	0	0	0	0	0	0	0	243	5	0.595000000000000000 02 0.0
303	0	MCJAVSP	26	5	0	0	0	0	0	0	0	243	5	0.672200000000000000 03 0.0
301	0	GEORGE	27	5	0	14	0	0	0	0	0	43	1	0.205700000000000000 02 0.0
302	0	GEORGE	27	5	0	0	0	0	0	0	0	262	59	0.135300000000000000 02 0.0
303	0	GEORGE	27	5	0	0	0	0	0	0	0	262	59	0.178500000000000000 03 0.0
301	0	GEORGE	28	5	0	114	0	0	0	0	0	45	1	0.456700000000000000 02 0.0
302	0	GEORGE	28	5	0	0	0	0	0	0	0	262	59	0.153000000000000000 02 0.0
303	0	GEORGE	28	5	0	0	0	0	0	0	0	262	59	0.193000000000000000 02 0.0
301	0	GEORGE	29	5	0	18	0	0	0	0	0	31	23	0.265600000000000000 03 0.0
302	0	GEORGE	29	5	0	0	0	0	0	0	0	136	52	0.142600000000000000 02 0.0
303	0	GEORGE	29	5	0	0	0	0	0	0	0	136	52	0.190000000000000000 03 0.0
301	0	GEORGE	30	5	0	113	0	0	0	0	0	31	23	0.265600000000000000 03 0.0
302	0	GEORGE	30	5	0	0	0	0	0	0	0	136	52	0.142600000000000000 02 0.0
303	0	GEORGE	30	5	0	0	0	0	0	0	0	136	52	0.142600000000000000 02 0.0
301	0	FTWYPLJ	3	1	0	1	10	1	1	1	0	0	0	0.89817230931658000000 04
301	0	FTWYPLB	0	1	0	1	10	2	2	1	0	0	0	0.12505932220302000000 03
301	0	FTWYPLC	0	2	0	1	10	3	3	1	0	0	0	0.10334503265461400000 03
301	0	FTWYPLD	0	2	0	1	10	4	4	1	0	0	0	0.80214159779716600000 03
301	0	FTWYPLE	0	3	0	1	10	5	5	1	0	0	0	0.67843673526717450000 03
301	0	FTWYPLF	0	3	0	1	10	6	6	1	0	0	0	0.11872657355683700000 03
301	0	FTWYPLG	0	4	0	1	10	7	7	1	0	0	0	0.14535948255083300000 03
301	0	FTWYPLH	0	4	0	1	10	8	8	1	0	0	0	0.21256226369071900000 03
301	0	FTWYPLI	0	5	0	1	10	9	9	1	0	0	0	0.0
301	0	FTWYPLJ	0	5	0	1	10	10	10	1	0	0	0	0.0
301	0	FTWYPLK	0	6	0	1	10	11	11	1	0	0	0	0.30906691377115600000 03
301	0	FTWYPLL	0	6	0	1	10	12	12	1	0	0	0	0.88750460516858340000 04
301	0	FTWYPLM	0	6	0	1	10	13	13	1	0	0	0	0.22619264117230000000 04
301	0	FTWYPLN	0	7	0	1	10	14	14	1	0	0	0	0.46725431365306900000 03
301	0	FTWYPLO	0	7	0	1	10	15	15	1	0	0	0	0.22011013546457290000 04
301	0	FTWYPLP	0	8	0	1	10	16	16	1	0	0	0	0.21154163756295000000 03
301	0	FTWYPLQ	0	8	0	1	10	17	17	1	0	0	0	0.13325685744215000000 03
301	0	FTWYPLR	0	9	0	1	10	18	18	1	0	0	0	0.12217752903750000000 02
301	0	FTWYPLS	0	10	0	1	10	19	19	1	0	0	0	0.58597822648453000000 04
301	0	FTWYPLT	0	10	0	1	10	20	20	1	0	0	0	0.53466975115840390000 03

CONTROL DATA LISTING

CATEGORY	CONTINUE	LABEL	KEY1	KEY2	KEY3	KEY4	KEY5	KEY6	KEY7	KEY8	KEY9	KEY10	DATA1	DATA2
601	0	WAKFLD	0	11	0	1	10	21	21	1	0	0	C-0.102613000752338000000-04	0.1000000000000000 03
601	0	WAKFLD	0	11	0	1	10	22	22	1	0	0	-0.07330434562159400000-03	0.1000000000000000 03
601	0	WAKFLD	0	12	0	1	10	23	23	1	0	0	C-0.33588145000001000000-04	0.1000000000000000 03
601	0	WAKFLD	0	12	0	1	10	24	24	1	0	0	-0.324052100000000000-03	0.1000000000000000 03
601	0	WAKFLD	0	13	0	1	10	25	25	1	0	0	-0.112327752564730000-03	0.1000000000000000 03
601	0	WAKFLD	0	17	0	1	10	26	26	1	0	0	C-0.22610055317355760000-03	0.1000000000000000 03
601	0	WAKFLD	0	17	0	1	10	27	27	1	0	0	-0.472213057345550000-04	0.1000000000000000 03
601	0	WAKFLD	0	14	0	1	10	28	28	1	0	0	-0.234679274825670000-03	0.1000000000000000 03
601	0	WAKFLD	0	15	0	1	10	29	29	1	0	0	-0.421078416536336000-05	0.1000000000000000 03
601	0	WAKFLD	0	15	0	1	10	30	30	1	0	0	-0.427025727917645000-03	0.1000000000000000 03
601	0	WAKFLD	0	16	0	1	10	31	31	1	0	0	-0.175925004375116000-03	0.1000000000000000 03
601	0	WAKFLD	0	16	0	1	10	32	32	1	0	0	-0.56536035243763600000-03	0.1000000000000000 03
601	0	WAKFLD	0	17	0	1	10	33	33	1	0	0	-0.73476711731564890000-04	0.1000000000000000 03
601	0	WAKFLD	0	17	0	1	10	34	34	1	0	0	-0.42405617581853360000-04	0.1000000000000000 03
601	0	WAKFLD	0	18	0	1	10	35	35	1	0	0	-0.11712625397782000000-03	0.1000000000000000 03
601	0	WAKFLD	0	16	0	1	10	36	36	1	0	0	-0.376516232745000000-03	0.1000000000000000 03
601	0	WAKFLD	0	19	0	1	10	37	37	1	0	0	-0.743655852462400000-04	0.1000000000000000 03
601	0	WAKFLD	0	19	0	1	10	38	38	1	0	0	-0.59330633224153400000-03	0.1000000000000000 03
601	0	WAKFLD	0	20	0	1	10	39	39	1	0	0	-0.10754911672316300000-04	0.1000000000000000 03
601	0	WAKFLD	0	20	0	1	10	40	40	1	0	0	-0.23974754213318000000-03	0.1000000000000000 03
601	0	WAKFLD	0	1	0	1	14	2	41	1	0	0	-0.59413659352716000000-14	0.1000000000000000 02
601	0	WAKFLD	0	2	0	1	14	3	42	1	0	0	-0.42327653552195000000-12	0.1000000000000000 02
601	0	WAKFLD	0	3	0	1	14	4	43	1	0	0	-0.10144573758536000000-12	0.1000000000000000 02
601	0	WAKFLD	0	4	0	1	14	7	44	1	0	0	-0.05444727676766590000-03	0.1000000000000000 02
601	0	WAKFLD	0	5	0	1	14	10	45	1	0	0	0.0	0.1000000000000000 02
601	0	WAKFLD	0	6	0	1	14	11	46	1	0	0	-0.13285772114190000000-03	0.1000000000000000 02
601	0	WAKFLD	0	7	0	1	14	14	47	1	0	0	-0.195351659579000000-03	0.1000000000000000 02
601	0	WAKFLD	0	8	0	1	14	15	48	1	0	0	-0.75530182762715900000-03	0.1000000000000000 02
601	0	WAKFLD	0	9	0	1	14	18	49	1	0	0	-0.210033490000000000-03	0.1000000000000000 02
601	0	WAKFLD	0	10	0	1	14	19	50	1	0	0	-0.65733424372466500000-02	0.1000000000000000 02
601	0	WAKFLD	0	11	0	1	14	22	51	1	0	0	-0.35866491106362000000-04	0.1000000000000000 02
601	0	WAKFLD	0	12	0	1	14	23	52	1	0	0	-0.2327476172294179000000-03	0.1000000000000000 02
601	0	WAKFLD	0	13	0	1	14	25	53	1	0	0	-0.13414416559675000000-05	0.1000000000000000 02
601	0	WAKFLD	0	14	0	1	14	27	54	1	0	0	-0.46791732445739000000-03	0.1000000000000000 02
601	0	WAKFLD	0	15	0	1	14	30	55	1	0	0	-0.43446335265959000000-03	0.1000000000000000 02
601	0	WAKFLD	0	16	0	1	14	31	56	1	0	0	-0.43471845513191900000-03	0.1000000000000000 02
601	0	WAKFLD	0	17	0	1	14	34	57	1	0	0	-0.19295550353702800000-04	0.1000000000000000 02
601	0	WAKFLD	0	18	0	1	14	35	58	1	0	0	-0.23845032244400000000-03	0.1000000000000000 02
601	0	WAKFLD	0	19	0	1	14	36	59	1	0	0	-0.726683254579000000-04	0.1000000000000000 02
601	0	WAKFLD	0	20	0	1	14	39	60	1	0	0	-0.22318073278420000000-03	0.1000000000000000 02
601	0	WAKFLD	0	1	0	1	15	1	61	1	0	0	-0.18244693122036100000-04	0.1000000000000000 02
601	0	WAKFLD	0	2	0	1	15	4	62	1	0	0	-0.75946546466014900000-04	0.1000000000000000 02
601	0	WAKFLD	0	3	0	1	15	5	63	1	0	0	-0.57290723805334890000-13	0.1000000000000000 02
601	0	WAKFLD	0	4	0	1	15	8	64	1	0	0	-0.13864045002216500000-04	0.1000000000000000 02
601	0	WAKFLD	0	5	0	1	15	9	65	1	0	0	0.0	0.1000000000000000 02
601	0	WAKFLD	0	6	0	1	15	12	66	1	0	0	-0.8970564804666649000000-05	0.1000000000000000 02
601	0	WAKFLD	0	7	0	1	15	17	67	1	0	0	-0.23456262001735900000-03	0.1000000000000000 02
601	0	WAKFLD	0	8	0	1	15	18	68	1	0	0	-0.10052148552940000000-02	0.1000000000000000 02
601	0	WAKFLD	0	9	0	1	15	17	69	1	0	0	-0.15483627566157500000-02	0.1000000000000000 02
601	0	WAKFLD	0	10	0	1	15	20	70	1	0	0	-0.20724628225637000000-03	0.1000000000000000 02



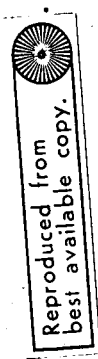
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best available copy.

CONTROL DATA LISTING

CATEGORY	CONTINUE	LABEL	KEY1	KEY2	KEY3	KEY4	KEY5	KEY6	KEY7	KEY8	KEY9	KEY10	DATA1	DATA2
601	0	WKFLEDR	0	11	0	1	15	21	71	1	0	0	-C.4320564159126C50000000-04	0.10000000000000000000-02
601	0	WKFLEDR	0	12	0	1	15	24	72	1	0	0	0.1326575654301463000000-03	0.10000000000000000000-02
601	0	JURUFLR:	0	13	0	1	15	25	73	1	0	0	-C.6560137011785C09000000-06	0.10000000000000000000-02
601	0	JURUFLR	0	14	0	1	15	28	74	1	0	0	0.1546452414820446000000-04	0.10000000000000000000-02
601	0	ULASKELS	0	15	0	1	15	29	75	1	0	0	0.7342127120233360000000-05	0.10000000000000000000-02
601	0	ULASKPR	0	16	0	1	15	32	76	1	0	0	0.429084648150129000000-04	0.10000000000000000000-02
601	0	CHISALLR	0	17	0	1	15	33	77	1	0	0	0.150945459959125000000-03	0.10000000000000000000-02
601	0	UPWAPAS	0	18	0	1	15	37	78	1	0	0	0.130051617576388000000-03	0.10000000000000000000-02
601	0	MEGSELR	0	19	0	1	15	37	79	1	0	0	0.1093228503584000000-03	0.10000000000000000000-02
601	0	RAJUPMR	0	20	0	1	15	40	80	1	0	0	0.21994475310602000000-03	0.10000000000000000000-02
601	0	FTHYER T	0	2	0	1	11	1	81	1	0	0	0.1240405786881872900000-02	0.0
602	0	FTHYER T	11	1	2	3	4	0	0	0	0	0	0.0	0.0
601	0	QUITO T	0	0	0	1	11	5	82	1	0	0	-C.053867599270076900000-04	0.10000000000000000000-01
602	0	QUITO T	11	5	7	3	0	0	0	0	0	0	0.0	0.0
601	0	LIMA T	0	0	0	1	11	9	83	1	0	0	-C.63840233125636000000-04	0.10000000000000000000-01
602	0	LIMA T	11	9	12	11	12	0	0	0	0	0	0.0	0.0
601	0	SANTIA T	0	0	0	1	11	13	84	1	0	0	0.446454860076375900000-02	0.10000000000000000000-01
602	0	SANTIA T	11	13	15	15	0	0	0	0	0	0	0.0	0.0
601	0	REWFLD T	0	0	0	1	11	17	85	1	0	0	-C.158008311048637000000-02	0.10000000000000000000-01
602	0	REWFLD T	11	17	19	20	0	0	0	0	0	0	0.0	0.0
601	0	WKFLEDR	0	0	0	1	11	21	86	1	0	0	-C.12020727410479000000-02	0.10000000000000000000-01
602	0	WKFLEDR	11	21	22	23	24	0	0	0	0	0	0.0	0.0
601	0	JURUFLR T	0	0	0	1	11	25	87	1	0	0	-C.019344428130102200000-02	0.10000000000000000000-01
602	0	JURUFLR T	11	25	26	27	28	0	0	0	0	0	0.0	0.0
601	0	ULASKA T	0	0	0	1	11	29	88	1	0	0	-C.702566930032346900000-04	0.10000000000000000000-01
602	0	ULASKA T	11	29	30	31	32	0	0	0	0	0	0.0	0.0
601	0	BRDAL T	0	0	0	1	11	33	89	1	0	0	-C.014570386973839500000-02	0.10000000000000000000-01
602	0	BRDAL T	11	33	34	35	36	0	0	0	0	0	0.0	0.0
601	0	MADGAR T	0	0	0	1	11	37	90	1	0	0	-C.31247150703672600000-03	0.10000000000000000000-01
602	0	MADGAR T	11	37	38	39	40	0	0	0	0	0	0.0	0.0
605	0		1	0	0	0	0	0	0	0	0	0	0.0	0.0
601	0	X	0	0	0	2	1	0	1	0	0	0	-C.5840000000000000000000 02	0.0
601	0	Y	1	0	0	2	2	0	2	0	0	0	0.2121325950563730000000 07	0.10000000000000000000 10
601	0	Z	1	0	0	2	3	0	3	0	0	0	0.7007230205675695000000 05	0.10000000000000000000 10
601	0	XO	1	0	0	2	4	0	4	0	0	0	0.7146098172622490000000 07	0.10000000000000000000 10
601	0	YO	1	0	0	2	5	0	5	0	0	0	0.23477572805239000000 04	0.10000000000000000000 10
601	0	ZO	1	0	0	2	6	0	6	0	0	0	-C.7915285710641380000000 04	0.10000000000000000000 10
701	0	FTMGL	1	1	6	3	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	FTMGL	2	1	7	4	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	FTMGL	3	2	8	5	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	FTMGL	4	3	7	4	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	OTLUL	5	3	5	3	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	ATEGL	6	3	7	4	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	ATEGL	7	4	9	3	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	ATEGL	8	7	4	0	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	LMAEOL	9	5	3	0	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	LMAEOL	10	5	7	4	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	LMAEOL	11	6	5	3	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	LMAEOL	12	6	7	4	0	0	0	0	0	0	0.0	0.30000000000000000000-03
701	0	STAEOL	13	7	5	3	0	0	0	0	0	0	0.0	0.30000000000000000000-03

CONTROL DATA LISTING

CATEGORY	CONTINGE	LABEL	KEY1	KEY2	KEY3	KEY4	KEY5	KEY6	KEY7	KEY8	KEY9	KEY10	DATA1	DATA2
701	0	STALOM	14	7	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	STAPOL	15	8	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	STAPPM	16	8	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	NFLPOL	17	9	6	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	NFLPOL	18	9	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	NFLPOL	19	10	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	NFLPOL	20	10	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	WKFPOL	21	11	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	WKFPOL	22	11	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	WKFPOL	23	12	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	WKFPM	24	12	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	JWFLPOL	25	13	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	JWFLPOL	26	13	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	JWFLPOL	27	14	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	JWFLPOL	28	14	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	LEPOL	29	15	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	LEPOL	30	15	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	LEAPOL	31	16	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	LEAPOL	32	16	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	CRAPOL	33	17	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	CRAPOL	34	17	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	CRAPOL	35	18	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	CRAPOL	36	18	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	MSAEPOL	37	19	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	MSAEPOL	38	19	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	MSAPOL	39	20	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	MSAPOL	40	20	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	41	21	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	42	21	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	43	24	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	44	24	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	45	24	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	46	25	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	47	24	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	48	24	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	49	25	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	50	25	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	51	21	6	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	52	21	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	53	27	6	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	54	27	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	55	23	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	56	23	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	57	29	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	58	29	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	59	30	5	3	0	0	0	0	0	0	0.0	0.300000000000000000-03
701	0	UPFLPOL	60	30	7	4	0	0	0	0	0	0	0.0	0.300000000000000000-03
702	0	UPFLPOL	1	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	UPFLPOL	2	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	UPFLPOL	3	0	1	0	0	0	0	0	0	0	0.0	0.0



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CATEGORY CONTINUE LABEL KEY1 KEY2 KEY3 KEY4 KEY5 KEY6 KEY7 KEY8 KEY9 KEY10 DATA1 DATA2

702	0	RTMPDH	4	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	GTCEBL	5	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	STOLDM	6	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	STOPPL	7	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	STOPDH	8	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	LMAEOL	9	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	LWAECH	10	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	LWAPVL	11	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	LWAPDH	12	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	STALOL	13	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	STALGH	14	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	STAPBL	15	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	STAPDH	16	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	NFLEOL	17	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	NFLECH	18	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	NFLPOL	19	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	NFLPEH	20	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	NFLPOL	21	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	NFLECH	22	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	NFLPOL	23	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	NFLPEH	24	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	JREVL	25	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	JRECH	26	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	JRPOL	27	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	JRPDH	28	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	LSKPOL	29	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	LSKPEH	30	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	LSKPOL	31	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	LSKPEH	32	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	BRASOL	33	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	BRPECH	34	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	BRAPOL	35	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	BRAPDH	36	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	MSALOL	37	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	MSALCH	38	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	MGAPOL	39	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	MGAPDH	40	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	BRPOL	41	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	BRPEH	42	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	BRPOL	43	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	BRPEH	44	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	CLPOL	45	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	CLPEH	46	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	CLPOL	47	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	CLPEH	48	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	KJVEOL	49	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	KJVECH	50	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	KJVPOL	51	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	KJVPEH	52	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
702	0	GPKEOL	53	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONTROL DATA LISTING

CATEGORY	CONTINUE	LABEL	KEY1	KEY2	KEY3	KEY4	KEY5	KEY6	KEY7	KEY8	KEY9	KEY10	DATA1	DATA2
702	0	GFKEUM	54	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GFKPOL	55	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GFKROM	56	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GMLCBL	57	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GMLFLM	58	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GMPCLM	59	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GMPPCM	60	0	1	0	0	0	0	0	0	0	0.0	0.0
201	0	LIMAPAP	1	0	1	0	0	0	0	0	0	0	0.34370000000000000000	04
202	0	LIMAPOL	11	0	1	0	0	0	0	0	0	0	0.34678000000000000000	04
701	1	LIMAPCH	12	0	1	0	0	0	0	0	0	0	0.10000000000000000000	01
999	0	LIMAPCD	1	0	1	0	0	0	0	0	0	0	0.10000000000000000000	01
201	0	QUITUCH	1	0	1	0	0	0	0	0	0	0	0.36390000000000000000	04
202	0	QUITCAP	1	0	1	0	0	0	0	0	0	0	0.39518000000000000000	04
701	1	LITCPBL	7	4	5	3	0	0	0	0	0	0	0.10000000000000000000	01
701	1	QUITPCH	3	4	7	4	0	0	0	0	0	0	0.10000000000000000000	01
999	0	QUITPCH	1	4	1	1	0	0	0	0	0	0	0.41510000000000000000	04
201	0	FTMYRSP	1	2	1	0	0	0	0	0	0	0	0.42137000000000000000	04
202	0	FTMYRCP	1	2	1	0	0	0	0	0	0	0	0.10000000000000000000	01
701	1	FTKPOL	3	2	5	3	0	0	0	0	0	0	0.10000000000000000000	01
701	1	FTMPCH	4	2	7	4	0	0	0	0	0	0	0.10000000000000000000	01
999	0	FTMYRCP	1	2	1	1	0	0	0	0	0	0	0.44480000000000000000	04
201	0	FTMYRGE	1	1	1	0	0	0	0	0	0	0	0.45457000000000000000	04
202	0	FTMYRGE	1	1	1	0	0	0	0	0	0	0	0.10000000000000000000	01
701	1	FTLFLM	1	1	0	3	0	0	0	0	0	0	0.10000000000000000000	01
701	1	FTLFLM	2	1	7	4	0	0	0	0	0	0	0.10000000000000000000	01
999	0	FTMYRGE	1	1	1	1	0	0	0	0	0	0	0.45209000000000000000	04
201	0	ULASKAE	1	15	1	0	0	0	0	0	0	0	0.52717000000000000000	04
202	0	ULASKAE	1	15	1	0	0	0	0	0	0	0	0.52717000000000000000	04
701	1	LKREUL	29	15	5	3	0	0	0	0	0	0	0.10000000000000000000	01
701	1	LKREUM	30	15	7	4	0	0	0	0	0	0	0.10000000000000000000	01
999	0	ULASKAE	1	15	1	1	0	0	0	0	0	0	0.10000000000000000000	01
201	0	STASAP	1	0	1	0	0	0	0	0	0	0	0.57290000000000000000	04
202	0	STASAP	1	0	1	0	0	0	0	0	0	0	0.57918000000000000000	04
701	1	STAPOL	15	0	5	3	0	0	0	0	0	0	0.10000000000000000000	01
701	1	STAPUM	16	8	7	4	0	0	0	0	0	0	0.10000000000000000000	01
999	0	STASAP	1	0	1	1	0	0	0	0	0	0	0.10000000000000000000	01
201	0	LIMAPAP	1	0	2	0	0	0	0	0	0	0	0.10187000000000000000	05
202	0	LIMAPAP	1	0	2	0	0	0	0	0	0	0	0.10215000000000000000	05
701	1	LWAPOL	11	0	5	3	0	0	0	0	0	0	0.10000000000000000000	01
701	1	LWAPOL	12	0	7	4	0	0	0	0	0	0	0.10000000000000000000	01
999	0	LIMAPAP	1	0	2	1	0	0	0	0	0	0	0.10900000000000000000	05
201	0	FTMYRCP	1	2	2	0	0	0	0	0	0	0	0.10581800000000000000	05
202	0	FTMYRCP	1	2	2	0	0	0	0	0	0	0	0.10581800000000000000	05
701	1	FTMPCH	4	2	0	0	0	0	0	0	0	0	0.17502676875594000000	01
701	1	FTMPOL	3	2	5	3	0	0	0	0	0	0	0.10000000000000000000	01
999	0	FTMPCH	4	2	7	4	0	0	0	0	0	0	0.10000000000000000000	01
201	0	FTMYRCP	1	2	2	1	0	0	0	0	0	0	0.10000000000000000000	01
202	0	ULASKAE	1	15	2	0	0	0	0	0	0	0	0.11780000000000000000	05
701	1	ULASKAE	1	15	2	0	0	0	0	0	0	0	0.11845600000000000000	05

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4. DBA Systems, Inc., "Network Analysis Program, Phase II, User's Guide to Data Preparation", December 1969, NASA Contract NAS5-10588.
5. Morduch, G. E., "An Algorithm for the Computation of the Gradient Of a Newtonian Potential Expressed as a Sum of Spherical Harmonics", June 1971, NASA/GSFC X-551-71-248.

APPENDIX A-1
CONSTANTS USED IN NAP-II

THE GRAVITY MODEL USED

The gravity model used for data processing under this contract was the Smithsonian M1 model, (Reference 1), which is built into the NAP program, modified by the GEOS-A resonant harmonics (Reference 2). The GEOS-A resonant harmonics were not obtained from the original source, but from (Reference 3).

The gravitational mass of the Earth was taken as $.3986032 \text{ D15 m}^3/\text{sec}^2$, which is the NAP default value.

The Smithsonian M1 values for the spherical harmonics coefficients are listed below:

<u>(N, M)</u>	<u>C(N, M)</u>	<u>S(N, M)</u>
(0, 0)	1.	0.
(1, 0)	0.	0.
(2, 0)	- .108264500002 D-2	0.
(3, 0)	.254599999999 D-5	0.
(4, 0)	.164900000002 D-5	0.
(5, 0)	.21 D-6	0.
(6, 0)	- .645999999993 D-6	0.
(7, 0)	.332999999998 D-6	0.
(8, 0)	.269999999997 D-6	0.
(9, 0)	.529999999998 D-7	0.
(10, 0)	.540000000002 D-7	0.
(11, 0)	- .302 D-6	0.
(12, 0)	.357000000006 D-6	0.
(13, 0)	.113999999999 D-6	0.
(14, 0)	- .178999999999 D-6	0.
(1, 1)	0.	0.
(2, 1)	0.	0.
(3, 1)	.209111899862 D-5	.287312837632 D-6
(4, 1)	- .542646846485 D-6	- .444932466779 D-6
(5, 1)	- .676515582477 D-7	- .88203930748 D-7
(6, 1)	- .36979402246 D-7	- .21243486397 D-7
(7, 1)	.14418923578 D-6	.114180308536 D-6
(8, 1)	- .515388203208 D-7	.446669776114 D-7
(9, 1)	.76024995806 D-7	.779743547594 D-8
(10, 1)	.648810099708 D-7	- .778572119639 D-7
(11, 1)	- .312872807930 D-7	.885489079044 D-8
(12, 1)	- .922805782847 D-7	- .401958347128 D-7
(13, 1)	0.	0.
(14, 1)	- .788307409236 D-8	.278535284599 D-8

<u>(N,M)</u>	<u>C(N,M)</u>	<u>S(N,M)</u>
(2, 2)	.153563789676 D-5	- .872066750118 D-6
(3, 2)	.250708728736 D-6	- .183761983737 D-6
(4, 2)	.737902432577 D-7	.147804093315 D-6
(5, 2)	.102117707526 D-6	- .375456547484 D-7
(6, 2)	.858383031385 D-8	- .455316216648 D-7
(7, 2)	.362552678174 D-7	.162351886106 D-7
(8, 2)	.21354899813 D-8	.320323497197 D-8
(9, 2)	- .27706980487 D-9	.242436079257 D-8
(10, 2)	- .624317809516 D-8	- .249727123811 D-8
(11, 2)	0.	0.
(12, 2)	- .469893640425 D-8	- .232665783121 D-9
(3, 3)	.782277124813 D-7	.225898207164 D-6
(4, 3)	.508569773273 D-7	- .113546717887 D-7
(5, 3)	- .171778742888 D-7	.231240615425 D-9
(6, 3)	- .111963004094 D-8	.642750579065 D-9
(7, 3)	.352147606138 D-8	.253546276422 D-9
(8, 3)	- .374070918995 D-9	.404400993503 D-10
(9, 3)	0.	0.
(10, 3)	- .378977225408 D-9	.174912565571 D-9
(4, 4)	- .11198293875 D-8	.485963696475 D-8
(5, 4)	- .206336328204 D-8	.498321698304 D-9
(6, 4)	- .166560812946 D-9	- .196087502512 D-8
(7, 4)	- .322776554575 D-9	- .216600056362 D-9
(8, 4)	- .276702101966 D-9	- .156623831302 D-10
(9, 4)	0.	0.
(10, 4)	- .435831320535 D-10	- .653746980798 D-10
(5, 5)	.384108946188 D-9	- .145764420605 D-8
(6, 5)	- .252611520257 D-9	- .369636026451 D-9
(7, 5)	.268980462153 D-10	.191117696793 D-10
(8, 5)	- .959291939079 D-11	.213578205308 D-10
(6, 6)	- .931919036559 D-11	- .36111862666 D-10
(7, 6)	- .145066373826 D-10	.437281413924 D-11
(8, 6)	- .474787418211 D-12	.88813175875 D-11

<u>(N, M)</u>	<u>C(N, M)</u>	<u>S(N, M)</u>
(7, 7)	.102027945339 D-11	.178085140954 D-11
(8, 7)	- .443617740607 D-13	.158070689181 D-12
(8, 8)	- .316141378363 D-12	.130025889487 D-12
(12, 12)	0.	0.
(13, 12)	- .1082186306 D-18	.895602460152 D-19
(14, 12)	0.	0.
(15, 12)	- .114596608272 D-19	.107203278705 D-19
(13, 13)	- .274440770475 D-19	.365921027295 D-20
(14, 13)	0.	0.
(15, 13)	- .127051846403 D-20	- .133101934329 D-20
(14, 14)	0.	0.
(15, 14)	.219788278315 D-22	- .532258360739 D-22

The GEOS-A resonant spherical harmonics coefficients are listed below:

<u>(N, M)</u>	<u>C(N, M)</u>	<u>S(N, M)</u>
(13, 12)	- .126299 D-18	.165220 D-18
(14, 12)	.139978 D-20	- .131772 D-19
(15, 12)	- .138126 D-19	- .189639 D-20

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1. Lundquist, C. A., Veis, G., "Geodetic Parameters for a 1966 Smithsonian Institution Standard Earth," SAO Special Report Number 200, Volume 1.
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3. Lerch, F. J., Marsh, J. G., O'Neill, B., "Evaluation of the Goddard Range and Range Rate System at Rosman by Intercomparison With GEOS-I Long Arc Orbital Solutions," Goddard Space Flight Center, Maryland, X-552-68-72, November 1967.

The C-5 Earth Model was adopted for the data processing. According to this model the Earth is defined geometrically by the following constants:

Rotation Rate	=	.7292115854937	D-4 radians/sec
Semi-Major Axis	=	6378165	meters
Eccentricity Squared	=	.669454185459	D-2.

The station coordinates are given below:

<u>Station Coordinates (Optical)</u>				
<u>Station</u>	<u>Station ID</u>	<u>Latitude</u>	<u>Longitude</u>	<u>Height Above Geoid</u>
COLDLK	29424	54°44'37.26"	249°57'21.90"	548 meters
NEWFL	31032	47°44'28.73"	307°16'46.67"	58 meters
JUPTH	37073	27°1'14.33"	279°53'12.72"	- 41 meters
JUPTR	29010	27°1'14.23"	279°53'12.95"	- 36 meters
JBC4L	37074	27°1'14.55"	279°53'12.76"	- 38 meters
COLEG	31033	64°52'17.78"	212°9'37.29"	139 meters
OOMER	31024	-31°23'26.96"	136°52'14.25"	148 meters
EDINB	37036	26°22'46.35"	261°40'7.34"	15 meters
JUP40	37072	27°1'14.39"	279°53'12.49"	- 38 meters
GFORK	31034	48°1'20.81"	262°59'19.55"	200 meters
ROSMA	31042	35°12'7.03"	277°7'40.81"	857 meters
PURIO	37040	18°15'28.30"	294°0'23.63"	5 meters
ORGAN	29001	32°25'24.70"	253°26'48.29"	1610 meters
GSFCP	37043	39°1'14.78"	283°10'20.39"	- 1 meter
BPOIN	31021	38°25'49.44"	282°54'48.65"	- 50 meters
EDWAFB	29425	34°57'50.17"	242°5'7.80"	754 meters

Station Coordinates (Optical) (Continued)

<u>Station</u>	<u>Station ID</u>	<u>Latitude</u>	<u>Longitude</u>	<u>Height Above Geoid</u>
JUP24	37071	27°1'14.00"	279°53'12.30"	- 38 meters
DENVR	37045	39°38'47.54"	255°23'38.52"	1751 meters
COLBA	37037	38°53'35.81"	267°47'40.85"	218 meters
FTMYR	31022	26°32'53.08"	278°8'3.80"	- 42 meters
BERMD	37039	32°21'48.94"	295°20'34.18"	- 28 meters
MOJAV	31030	35°19'47.57"	243°5'59.18"	874 meters
SATAG	31028	-33°8'58.76"	289°19'52.59"	705 meters

Station Coordinates (Minitrack)

<u>Station</u>	<u>Latitude</u>	<u>Longitude</u>	<u>Height Above Geoid</u>
Fort Myers	26°32'53.08"	278°8'3.80"	- 42 meters
Quito	-37'22.63"	281°25'15.23"	3554 meters
Lima	-11°46'37.56"	282°50'58.86"	34 meters
Santiago	-33°8'58.76"	289°19'52.59"	705 meters
New Foundland	47°44'28.73"	307°16'46.67"	58 meters
Winkfield	51°26'40.67"	359°18'8.35"	76 meters
Johannesburg	-25°53'2.7"	27°42'25.41"	1546 meters
Blossom Point	38°25'49.44"	282°54'48.65"	- 50 meters
College	64°52'17.78"	212°9'37.29"	139 meters
Mojave	35°19'47.57"	243°5'59.18"	874 meters
Grand Fork	48°1'20.81"	262°59'19.55"	200 meters
Woomera	-31°23'26.96"	136°52'14.25"	148 meters

APPENDIX A-2

SPECIAL PROGRAMS WRITTEN TO AID
MINITRACK DATA REDUCTION

A-2.1 PROGRAM FOR EXTRACTING MINITRACK MESSAGES
FOR GEOS I AND SAMPLE JCL

PROGRAM FOR EXTRACTING MINITRACK MESSAGES FOR SATELLITE ID 65891

```

DIMENSION D(65),T(8)
DATA T,'8','6','5','8','9','1',' ',' ' /
LOGICAL*1 D,T,D1,T1
REAL*8 DATA,TEST
EQUIVALENCE (DATA,C1,U(1)),(TEST,T1,T(1))
REWIND 9
REWIND 11
NPASST = 0
NPASSG = 0
100 READ (9, 601, END=900, ERR=100) D
IF(U1.NE.T1) GO TO 100
200 NPASST = NPASST + 1
IF (DATA.NE.TEST) GO TO 100
NPASSG=NPASSG+ 1
WRITE(6,602) NPASST, NPASSG
300 WRITE(11,601) D
400 REAC(9,601,END=900,ERR=400) D
IF(D1.EQ.T1) GO TO 200
GO TO 300
900 CONTINUE
REWIND 9
END FILE 11
REWIND 11
CO 940 I =1,100
910 CONTINUE
READ(11,601,END=950,ERR=910) D
WRITE(6,603) D
940 CONTINUE
950 CONTINUE
REWIND 11
STOP
601 FORMAT (65A1)
602 FORMAT (//2X,'TOTAL NUMBER OF MESSAGES', I10/
* 2X,'NUMBER OF GOES-A MESSAGES', I10)
603 FORMAT (10X,65A1)
STOP
END

```

```
/*  
//STEP2 EXEC LINKGO  
//GO.FT09F001 DD UNIT=(9TRACK,DEFER),DISP=(OLD,KEEP),LABEL=(2,BLP),  
// DC8=(RECFM=FB,BLKSIZE=3250,LRECL=65,DEN=2),VOL=SER=31027G,DSN=&DEO  
//GO.FT11F001 DD UNIT=2400-9,LABEL=(7,BLP),DISP=(NEW,DELETE),  
// DC8=(RECFM=FB,BLKSIZE=3250,LRECL=65,DEN=2),VOL=SER=33951C,DSN=&MOR  
/*
```

0059 CARDS

A-2.2 MINITRACK SORT PROGRAM AND JCL


```

//Z7GEMSRJ JOB (G7004)1150A,T,C00138,007007),Z7,MSGLEVEL=1
//STEPI EXEC FORTRANH,PARM='OPT=2'
//SOURCE.SYSIN DD *
DEFINE FILE 11(120C,2145,L,1D11)
DIMENSION BLANKS(65),AMPID(65),MINI(65,33),DATA(65),MINY(2145)
DIMENSION WORD(1202),LRECD(1200),K1(8),K2(8),K3(8),KD(8)
DIMENSION KSTA(16),STATIO(16),JCNE(10),MON(14)
LOGICAL*1 BLANKS,AMPID,MINI,DATA,MINY,BIN,PEZ,DI,AMP
REAL*8 STATIO
REAL*8 INTAPE,NDTAPE
INTEGER*2 K1,K2,K3,KD,KSTA,NSTAD,NSTAT,L,LINED
COMPLEX*16 WORD,WORC1,WORC2,WORC3,WOR00
EQUIVALENCE (AMP,AMPID(1)),(MINI(1,1),MINY(1,1)),(DI,DATA(1,1)),
1(WOR01,K1(1),ISEC1),(K1(3),IFROM1),(K1(5),IG01),(WORD2,K2(1)),
2 JSEC,ISEC2),(K2(3),IFROM2),(K2(5),IG02),(K2(7),NSTAT),
3(K2(8),L),(WORD3,K3(1),ISEC3),(K3(3),IFROM3),(K3(5),IG03),
4(WOR00,KD(1),ISEC0),(KD(3),IFROM0),(KD(5),IG00),
5(KD(7),NSTAD),(KD(8),LINED)
DATA AMPID(1),AMPID(2),AMPID(3),AMPID(4),AMPID(5),AMPID(6)
1,'6','6','5','8','9','1','/'
DATA BLANKS(1),BIN,PEZ/' ','0',' ','/'
DATA MON/0,31,59,90,120,151,181,212,243,273,304,334,365,500/
REWIND 9
REWIND 10
1D11=1
DO 10 I=2,65
10 BLANKS(I)=BLANKS(1)
DO 20 I=7,65
20 AMPID(I)=BLANKS(1)
IFROM3 = 1201
IG01 = 1202
ISEC3 = 200000000
ISEC1 = - 200000000
WORC(1201) = WORD1
WORC(1202) = WORD3
DO 30 I=1,16
30 REAC(5,1050) KSTA(I),STATIO(I)
JONE(1)=5
JONE(2)=13
JONE(3)=18
JONE(4)=26
JONE(5)=31
JONE(6)=39
JONE(7)=45

```

```

JCNE(8)=53
JONE(9)=57
JONE(10)=65
NDYR=365
IPAGE=1
40 CONTINUE
READ (5,1090,END=950) INTAPE,INFILE,NOTAPE,NDFILE
MTOT=C
M=1
C CHECK FOR AMPERSAND
100 READ(9,1000,ERR=100,END=500) DATA
IF(DI.NE.AMP) GO TO 100
C WHEN AMPERSAND HAS BEEN FOUND UPDATE TOTAL
C NUMBER OF MESSAGES
110 MTOT=MTOT+1
NENDAM=0
L=1
C READ MESSAGE
200 REAC(9,1000,ERR=200,END=350)(MINI(I,L),I=1,65)
IF(MINI(1,L).EQ.AMP) GO TO 360
210 J=1
J2=1
300 J1=JCNE(J2)
310 MTEST=MINI(J,L)-BIN
IF(MTEST.GT.9) GO TO 34C
IF(MTEST.LT.0) GO TO 34C
J=J+1
IF(J.LT.J1) GO TO 310
C CHECK FOR PERIOD
IF(MINI(J,L).NE.PEZ) GO TO 340
IF(J2.EC.10) GO TO 320
J=J+1
J2=J2+1
GO TO 300
C ONE GOOD LINE OF DATA HAS BEEN PROCESSED
320 IF(L.GT.1) GO TO 33C
C COMPUTE STATION NUMBER FROM FIRST LINE
NSTAT=MINY(56)-BIN+10*(MINY(55)-BIN)
322 L = 2
GO TO 200
330 DO 334 IK = 1,65
IF (MINI(IK,L).NE.MINI(IK,1)) GO TO 336
334 CONTINUE
GO TO 322

```

```

336 CONTINUE
IF ( MINI(56,L).NE.MINY(56)) GO TO 200
IF ( MINI(55,L).NE.MINY(55)) GO TO 200
IF (L.GE.33) GO TO 380
C READ NEXT LINE
L=L+1
GO TO 200
C BAD LINE. IF CALIBRATION LINE BAD IGNORE THIS RECORD
340 CONTINUE
IF(L.LT.2) GO TO 348
DO 345 IK = 1,65
IF(MINI(IK,L).NE.BLANKS(1)) GO TO 200
345 CONTINUE
GO TO 370
348 CONTINUE
WRITE(6,107C) MTOY
GO TO 100
C END OF MESSAGES
350 NENDAM=1
GO TO 370
C NEW MESSAGE AMPERSAND HAS BEEN READ
360 NENDAM=-1
370 L=L-1
380 IF(L.GE.5) GO TO 385
WRITE (6,1080) MTOY
GO TO 415
385 CONTINUE
IDAY=MINY(107)-BIN+10*(MINY(106)-BIN+10*(MINY(105)-BIN))
IF(M.LE.1) IDAY1=IDAY
ICAY=IDAY-IDAY1
IF(ICAY.GT.180) IDAY=IDAY-NOYR
IF(IDAY.LT.(-180)) IDAY=IDAY+NDYR
IH=MINY(93)-BIN+10*(MINY(92)-BIN)
IM=MINY(80)-BIN+10*(MINY(79)-BIN)
IS=MINY(67)-BIN+10*(MINY(66)-BIN)
JSEC=IS+60*(IM+60*(IH+24*IDAY))
JPLUS = JSEC + 30
JMINUS = JSEC - 30
L=65*L
LI = M
M = M + 1
390 IF(JSEC.GE.ISEC3) GO TO 410
IFROM1 = IFROM3
400 WORD1 = WORD(IFROM1)

```

```

IF(JSEC.LI.ISEC1) GO TO 400
WORD3 = WORD(IG01)
C
C
GO TO 420
410 WORD3 = WORD(IG03)
IF(JSEC.GE.ISEC3) GO TO 410
WORD1 = WORD(IFROM3)
C
C
420 CONTINUE
IF(JPLUS.GT.ISEC3) GO TO 2000
430 IF(JMINUS.LI.ISEC1) GO TO 2020
C
C NO DUPLICATE MESSAGES
C
440 CONTINUE
IFROM2 = IFROM3
IG02 = IG01
IFROM3 = LI
IG01 = LI
WORD(IFROM2) = WORD1
WORD(LI) = WORD2
WORD(IG02) = WORD3
LREC(LI) = MNOT
WRITE(11,LI)(MINY(I),I=1,L)
IF(M.GT.1200) GO TO 500
415 IF(NENDAM) 110,100,500
500 CONTINUE
M = M - 1
WRITE(6,1010) MNOT,M
WRITE (6,1100) IPAGE,NDIAPPE,INTAPE,NDIAPPE,INFILE
N = C
WORD2 = WORD(1201)
510 CONTINUE
IG01 = IG02
IF(IG01.GT.1200) GO TO 500
N = N + 1
WORD2 = WORD(IG01)
DO 810 K=1,16
IF(STAT.EQ.KSTAK(K)) GO TO 820
810 CONTINUE
K = 16
820 ITO = ISEC2/86400

```

```
ITS = ISEC2 - ITD*86400
IF(ITS.GE.0) GO TO 815
ITC = ITD - 1
ITS = ITS + 86400
815 CONTINUE
IHR = ITS/3600
IMIN = (ITS - IHR*3600)/60
IS = ITS - IHR*3600 - IMIN*60
ITD = ITD + IDAY1
IF(ITD.GT.NDYR) ITD = ITD - NDYR
IF(ITD.LE.0) ITD = ITC + NDYR
IMON = 2 + ITD/32
IF (ITD.LE.MON(IMON)) IMON = IMON - 1
IMD = ITD - MON(IMON)
READ(11,IG01,ERR=83C)(MINY(I),I=1,L)
L=L/65
WRITE(6,1020)N,LRECE(IGCL),NSTAT,STATIC(K),ITD,IMON,IMD,ITS,
* IHR,IMIN,IS,L
WRITE(10,1000) AMPIC
WRITE(10,1000)((MINI(J,I),J=1,65),I=1,L)
WRITE(10,1000) BLANKS
WRITE(6,1030) AMPID
C WRITE(6,1030)((MINI(J,I),J=1,65),I=1,L)
C WRITE(6,1030) BLANKS
GO TO 510
830 WRITE(6,1040) N
GO TO 510
900 CONTINUE
ENC FILE 10
WRITE(6,1060) IPAGE
WRITE(6,1060) IPAGE
GO TO 40
950 CONTINUE
REWIND 9
REWIND 10
STOP
1000 FORMAT(65A1)
1010 FORMAT(15X,'TOTAL NUMBER OF MESSAGES='',15)
1 6X,'NUMBER OF PROCESSED MESSAGES='',15)
1020 FORMAT(6X,14,14X,14,16X,12,12X,13,5X,12,7X,15,5X,12,
12X,12,2X,12,15)
1030 FORMAT(6X,65A1)
1040 FORMAT(6X,'ERROR RECORD NO.',15)
1050 FORMAT(15,5X,A6)
```

```

1060 FORMAT(11)
1070 FORMAT(6X,'BAD CALIBRATION LINE MESSAGE NO.',I4,X,'REJECTED.')
```

```

1080 FORMAT(6X,'TOO FEW LINES MESSAGE NO.',I4,X,'REJECTED.')
```

```

1090 FORMAT(A8,I5,A8,I5)
1100 FORMAT(11,5X,'OUTPUT TAPE',7X,'INPUT TAPE',10X,'STATION',25X,'DAY',
1,5X,'MONTH',2X,'DAY',6X,'SEC',7X,'HR',2X,'MIN',X,'SEC',X,'LINE',/6X
1,'NO.',A8,7X,'NO.',A8,9X,'ID',12X,'NAME',60X,'NO.',/6X,'FILE',I5,9X
1,'FILE',I5/6X,'MESSAGE NO.',7X,'MESSAGE NO.')
```

```

1110 FORMAT(6X,'DUPLICATE MESSAGES',I5,X,'AND',I5,'. THE SECOND MESSAGE
1 HAS BEEN REJECTED.')
```

```

2000 WORDC = WORD3
2010 IF(NSTAT.EQ.NSTAD) GO TC 2040
WORDC= WORD(IGOD)
IF(JPLUS.GT.ISECD) GO TC 2010
GO TC 430
2020 WORDC = WORD1
2030 IF(NSTAT.EQ.NSTAD) GO TC 2040
WORDC= WORD(IFROMD)
IF(JMINUS.LT.ISECD) GO TO 2030
GO TO 440
2040 CONTINUE
M = M - 1
WORD1 = WORD(IFROMD)
IF(LINED.GE.L) GO TO 2100
WRITE(6,1110) MTOT,LRECC(IGOI)
WORD3 = WORD(IGOD)
LI = IGO1
IGOI = IGO0
IFRCM3 = IFRM0D
WORD(IFROM3) = WORD1
WORD(IGCI) = WORD3
GO TO 390
2100 CONTINUE
WRITE(6,1110) LRECO(IGOI),MTOT
GO TO 415
END
```

```

/*
//STEP2 EXEC LINKGO
//GO.FT09FC01 DD UNIT=(9TRACK,DEFER),DISP=(OLD,KEEP),LABEL=(7,BLP),
// DCB=(RECFM=FB,BLKSIZE=3250,LRECL=65,DEN=2),VOL=SER=34248B
//GO.FT10F001 DD UNIT=(9TRACK,DEFER),DISP=(NEW,DELETE),LABEL=(7,BLP),
// DCB=(RECFM=FB,LRECL=65,BLKSIZE=3250,DEN=2),VOL=SER=2135H
//GO.FT11F001 DD UNIT=2314,DSN=6MINI,DISP=(NEW,DELETE),
// DCB=RECFM=FT,SPACE=(CYL,(3C,2))
```

//GO.CLEAR DD DSN=&L0DM00(GSFC),DISP=(OLD,DELETE)
//GO.SYSABEND DD SYSUUT=A,DCB=(RECFM=VBA,LRECL=137,8LKSIZE=7265),
// SPACE=(CYL,(1))

//GO.DATAS DD *

03 FTMYRS
05 QUITOE
06 LIMAPU
08 SNTAGO
12 NEWFLD
15 WNKFLD
16 JOBURG
19 ALASKA
21 CRORAL
23 MAUGAR
01 BPOINT
13 COLEGE
17 MOJAVE
14 GRDFKS
18 WOOMER
00 NGNAME

342488 7 2135H 7

/*

0286 CARDS

A-2.3 THE MINITRACK PREPROCESSOR


```

//Z7GEMRWB JOB (G70041150A,T,000138,005005),Z7,MSGLEVEL=1
// EXEC  LOADER,PARM=MAP,CALL,SIZE=440K,REGION.CO=450K
//GO.SYSLIN DD UNIT=2400-9,LABEL=(1,BLP),DISP=(OLD,KEEP),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200),VOL=SER=2023G
//GO.FT06F001 DD DUMMY
//GO.FT07F001 DD SYSOUT=B,DSN=DECK
//GO.FT09F001 DD UNIT=2400-9,LABEL=(2,BLP),DISP=(OLD,DELETE),
// DCB=(RECFM=FB,LRECL=65,BLKSIZE=3250,DEN=2),VOL=SER=1664J
//GO.FT11F001 DD DUMMY
//GO.FT12F001 DD UNIT=2400-9,LABEL=(2,BLP),DISP=(NEW,KEEP),
// DCB=(RECFM=VBS,LRECL=52,BLKSIZE=5204),VOL=SER=30060D
//GO.FT13F001 DD SYSOUT=A,SPACE=(CYL,(1,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT14F001 DD SYSOUT=A,SPACE=(CYL,(1,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT19F001 DD DUMMY
//GO.FT20F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT21F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT22F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT23F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT24F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT25F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT26F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT27F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT28F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT29F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT30F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT31F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT32F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT33F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)

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//GO.FT34F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT35F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT36F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT37F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT38F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT39F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT40F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT41F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT42F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT43F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT44F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT45F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT46F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT47F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT48F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT49F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT50F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT51F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.SYSABEND DD SYSOUT=A,SPACE=(CYL,(1))
//GO.DATA5 DD *

```

FTMYR6 03 369 369 064 28 372 25 957 137 902 00 120 26 013 431 690107

FTM1E 03
FTM2E 03
FTM3E 03
FTM4E 03

FTM1P 03

FTM2P 03

FTM3P 03

FTM4P 03

QUIT06 05 380 379 952 00 889 00 822 766 082 00 726 00 054 020 690107

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SNTAG6 08 391 391 983 00 106 00 078 938 013 00 976 00 042 970 690107

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NEWFL6 12 372 372 467 29 070 25 935 174 887 00 518 28 929 914 690107

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WNKEL6 15 385 384 540 29 222 25 072 872 100 00 791 28 975 012 690107

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JOBUR6 16 413 412 418-29 186 00 053 094 575-29 835 00 938 870 690107
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ULASK6 19 362 363 660 00 967 00 942 450 069 00 490 00 076 927 690107
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ORORA6 21 364 364 010 00 785 00 783 008 775 00 303 00 121 933 690107
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MADGA6 23 413 412 676 00 030 00 047 015 039 00 856 00 884 154 690107
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BPOIN6 01 363 363 743 00 223 00 948 083 255 00 933 00 094 889 690107
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13	COLEG6	13	381 381	668 00 624 00	959 842	253 00 011 00	807 926	690107				
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17	MOJAV6	17	375 375	009 00 844 00	030 076	067 00 169 00	577 126	690107				
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14	GFORK6	14	370 370	481 00 161 00	064 603	976 00 704 00	949 002	690107				
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18	WOMER6	18	395 395	945 00 109 00	031 950	173 00 033 00	935 120	690107				
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/*

//GO.FT08F001 DD *

GEOS-A MINITRACK DATA STARTING 08 JAN 1966 ARC 3

1 217 66 2 1

/*

//GO.FT08F002 DD DUMMY

//GO.FT08F003 DD DUMMY

//GO.FT08F004 DD DUMMY

/*

0239 CARDS

INTEGER SIG1, SIG2, SIG3, SIG4, SIG5, INQ, ISO 0000010
 INTECER AMP, END, CSTA, CANT, SIG, ANTD, HORD, MIND, SECD, SAT, DATE, KFA, KFB 0000020
 INTEGER IGRADE 0000030
 REAL NSFD, NSCD, NSMD 0000040
 REAL IDIF1, IDIF2, IDIF3, IDIF4, IDIF5 0000050
 REAL NSM, NSC, NSFPO, NSFEG, IDIF, NSF1, NSF2, NSF3, NSF4, NSF5 0000060
 LOGICAL #1 SLE, SLN 0000070
 LOGICAL #1 ASTA, ARMODA, ACUR, IALOB, IARATE, IAACC, IAWMER, IAWCER, IBLOB 0000080
 XE, IBRATE, IBACC, IBNMR, IBNCER, ICIGA, IOUR, ISEC, LCOS, MCOS, IEND, INNO 0000090
 LOGICAL #1 DATA, PEZ, BIN, SPX, IAMP 0000100
 LOGICAL #1 MSGR 0000110
 LOGICAL #1 LFILE 000012
 REAL #8 XNAP 000013
 REAL #8 STATIO 0000140
 REAL #8 DNAP 0000150
 REAL #8 A, A1, A2, A3 0000160
 DIMENSION STATIO(34), KFA(17), KF8(17), EWM(17), CLEWM(17), EWC(17), 000017
 1 CLEWC(17), EWFEQ(17), NSM(17), CLNSM(17), NSC(17), CLNSC(17), 000018
 2 NSFEG(17), NSFPU(17), ISTA(68), IANI(68), C1(68), C2(68), C3(68), 000019
 3 C4(68), C5(68), C6(68), C7(68), C8(68), KSAID(50), FREQ(50), 000020
 4 KSTA(48), EWFP(17), TIM(31), CO(68) 000021
 DIMENSION SECD(31), EWMD(31), EWCD(31), EWFD(31), NSMD(31), NSCD(31), NS 0000220
 IFD(31), MIND(31), HORD(31), DAYD(31), ANTD(31), STAD(31), SIGD(31), EEW 0000230
 2(31), ENSF(31), IDAYD(31), AST(17), DATE(17), CD(68) 000024
 DIMENSION ASTA(3), ARMODA(7), ADUR(7), IALOB(6), IARATE(5), IAACC(4), I 0000250
 XAWMER(3), IAWCER(3), IBLOB(6), IBRATE(5), IBACC(4), IBNMR(3), IBNCER(3 0000260
 X), ICIGA(3), IOUR(5), ISEC(6), LCOS(6), MCOS(8), IEND(3), INNO(3) 0000270
 DIMENSION MSGR(80) 0000280
 DIMENSION DATA(100) 0000290
 DIMENSION SLE(4), SLN(4) 0000300
 DIMENSION TFOVEW(31, 5), FOVEW(31, 5), TFOVNS(31, 5), FOVNS(31, 5) 0000310
 DIMENSION DNAP(6), JUDY(34), IPASS(34), JUSEC(34) 000032
 DIMENSION XNAP(6) 000033
 DIMENSION IA(17) 000034
 DIMENSION IPASST(34) 000035
 EQUIVALENCE (SLN(1), INOVER) 0000360
 EQUIVALENCE (SLE(1), IEOVER) 0000370
 DIMENSION AACOS(31, 5), BBCOS(31, 5) 0000380
 DATA PER, ASK, SPA, POL, EQ, F1, F2, F3, F4, F5, F6, F7, IAMP, SLA, PEZ, BIN, SPX / 0000390
 IZ4B404040, Z5C404040, Z40404040, ZD7404040, ZC5404040, ZC1404040, ZC2404 0000400
 2040, ZC3404040, ZC4404040, ZC5404040, ZC6404040, ZC7404040, Z50, Z6140404 0000410

```

30,Z4B,ZF0,Z40/
DATA STATIO(I7)/'NONAME'//
DATA A1,A2,A3/'PASS','JUDAY','JUSEC'//
SLA=SLA
KDEG=25
LFILE=.FALSE.
DEGREE=KDEG
CCUS=COS(DEGREE*3.1459265/180.)
KSTA(I7)=0
XNAP(5)=0.00
XNAP(6)=0.00
DNAP(6)=0.00
DNAP(5)=0.00
DO 330 I=1,34
IPASS(I)=0
IPASST(I) = 0
JUDY(I)=0
330 JUSEC(I)=0
READ( 5,760)IGRADE
760 FORMAT(9X,I1)
JL=0
JM=0
WRITE( 6,760)IGRADE
1340 FORMAT (1H1,19(*),80X,20(*))
* //50X,'INPUT STATION CONSTANTS'//
* 2X,'STATION KFA KFB EWM CLEWM EWC CLEWC EWFEQ',
* 1X,'EWFP0 NSM CLNSM NSC CLNSC NSFEQ NSFPO DATE'//
* 2X,'NAME NO.'//)
WRITE (13,1340)
1341 FORMAT (1X,A6,1X,I3,2(2X,I3),1X,F4.3,2X,F4.3,1X,F4.3,
* 2(3X,F4.3,2X,F4.3),1X,F4.3,2X,F4.3,2(3X,F4.3),3X,I6)
DO 35 J=1,16
C INPUT STATION CONSTANTS
READ( 5,80) STATIO(J),KSTA(J),KFA(J),KFB(J),EWM(J),CLEWM(J),EWC(J)
1,CLEWC(J),EWFEQ(J),EWFP0(J),NSM(J),CLNSM(J),NSC(J),CLNSC(J),NSFEQ(
2J),NSFPO(J),DATE(J)
WRITE(6,580)STATIO(J),KSTA(J),KFA(J),KFB(J),EWM(J),CLEWM(J),EWC(J)
1,CLEWC(J),EWFEQ(J),EWFP0(J),NSM(J),CLNSM(J),NSC(J),CLNSC(J),NSFEQ(
2J),NSFPO(J),DATE(J)
80 FORMAT(A6,X,I2,I4,I4,3X,F4.3,F3.3,F4.3,X,F4.3,3X,F4.3,F4.3,F3
X.3,F4.3,F3.3,X,F4.3,F4.3,5X,I6)
580 FORMAT(X,A6,X,I2,X,I3,X,I3,3X,F4.3,F4.3,F4.3,X,F4.3,
X3X,F4.3,F4.3,F4.3,X,F4.3,2X,I6)
WRITE (13,1341) STATIO(J),KSTA(J),KFA(J),KFB(J),EWM(J),CLEWM(J),

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* EWC(J),CLEWC(J),EWFEC(J),EWFPO(J),NSM(J),CLNSM(J), 000086
* NSC(J),CLNSC(J),NSFEQ(J),NSFPO(J),DATE(J) 000087
DO 36 M=1,4 0000880
JL=JM+M 0000890
C INPUT STATION COEFF. 0000900
READ( 5,81) IANT(JL),ISIA(JL),CO(JL),C1(JL),C2(JL),C3(JL),C4(JL) 0000910
WRITE(6,811) IANT(JL),ISIA(JL),CO(JL),C1(JL),C2(JL),C3(JL),C4(JL) 0000920
811 FORMAT(4X,A1,X,I2,5(X,E15.8)) 0000930
READ( 5,581) C5(JL),C6(JL),C7(JL),C8(JL) 0000940
581 FORMAT(8X,4(X,E12.8)) 0000950
WRITE(6,681) C5(JL),C6(JL),C7(JL),C8(JL) 0000960
681 FORMAT(9X,4(X,E15.8)) 0000970
81 FORMAT(4X,A1,X,I2,5(X,E12.8)) 0000980
36 CONTINUE 0000990
JM=JM+4 0001000
35 CONTINUE 0001010
WRITE(6,500)(KSTA(I),I=1,16) 000102
500 FORMAT(X, 16(X,I2)) 000103
DO 2 I=1,17 000104
STATIO(I+17)=STATIO(I) 000105
KSTA(I+17)=KSTA(I)+100 000106
2 CONTINUE 0001070
DO 37 J=1,50 0001080
C INPUT SATELLITE CONSTANTS 0001090
READ( 5,82) KSAID(J),FREQ(J) 0001100
82 FORMAT(15,19X,F8.3) 0001110
WRITE( 6,582) KSAID(J),FREQ(J) 0001120
582 FORMAT(X,15,19X,F8.3) 0001130
IF(KSAID(J))37,38,37 0001140
37 CONTINUE 0001150
38 KSAID=J-1 0001160
305 READ(8,305,END=321,ERR=902)(MSGR(I),I=1,80) 0001170
FORMAT(80A1) 0001180
NAPEND = 0 000119
IB1 = 0 000120
REWIND 9 000121
IARC = 1 000122
IARCS=-1 000123
I201 = 201 000124
I202 = 202 000125
WRITE(13,340)(MSGR(I),I=1,80) 0001260
340 FORMAT(1H1,19(*),80A1,20(*))/50X,'PROCESSING MESSAGES'// 0001270
WRITE(14,340)(MSGR(I),I=1,80) 0001280
WRITE(14,352) 0001290

```

```

352 FORMAT (3X, 'SUMMARY OF DATA MESSAGES PRODUCED', //3X, 'MESSAGE', 1X, 000130
* 'DATA', 3X, 'STATION', 3X, 'ARC', 2X, 'PASS', 2X, 'START TIME', 000131
* 6X, 'L', 9X, 'M', 9X, 'N', 7X, 'LDOT', 6X, 'MDOT', 6X, 'NDOT', 000132
* / 3X, 'NUMBER', 3X, 'PTS', 2X, 'NO.', 2X, 'NAME', 14X, 'DAY', 2X, 000133
* 'SEC.', //) 000134
902 CONTINUE 000135
IF(NAPEND) 910, 920, 3 000136
910 READ(9, 601, END=915, ERR=910) (DATA(I), I=1, 65) 000137
GO TO 910 000138
915 IB1 = 0 00139
920 CONTINUE 000140
READ(8, 901, END=1, ERR=920) ILOW, IHIGH, IYEAR, NEWARC, NAPEND 000141
IF(NEWARC.LE.0) GO TO 2010 000142
IARC = NEWARC 000143
IF(IARCS.EQ.IARC) GO TO 2010 000144
DO 2005 I= 1, 24 000145
IPASST(I)=IPASS(I)+IPASST(I) 000146
2005 IPASS(I) = 0 000147
2010 CONTINUE 000148
IF(ILOW.GT. IHIGH) IHIGH=ILOW 000149
312 FORMAT(A5, 13I5) 000150
K=0 000151
324 READ(8, 312, ERR=313, END=313) A, N, (IA(I), I=1, 12) 000152
READ(8, 901, ERR=313, END=313) (IA(I), I=13, 17) 000153
K=K+1 000154
IF(A.EQ.A1) GO TO 314 000155
IF(A.EQ.A2) GO TO 315 000156
IF(A.EQ.A3) GO TO 316 000157
GO TO 313 000158
314 DO 317 I=1, 17 000159
317 IPASS(I+N-1)=IA(I) 000160
GO TO 318 000161
315 DO 319 I=1, 17 000162
319 JUDY(I+N-1)=IA(I) 000163
GO TO 318 000164
316 DO 323 I=1, 17 000165
323 JUSEC(I+N-1)=IA(I) 000166
318 IF(K.LT.6) GO TO 324 000167
313 CONTINUE 000168
IPAGE=1 000169
WRITE(6, 302) IPAGE, (MSGR(I), I=1, 80) 000170
302 FORMAT(11, 19X, 80A1, /) 000171
IPAGE=0 000172
WRITE(6, 903) ILOW, IHIGH 000173

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```

903 FORMAT('ODATA SET RANGES FROM DATA FILE   LOW = ',15,4X,'HIGH = ',1,15)
      KEND=0
901  FORMAT(5I5)
      IF(1B1.LT.ILOW) GO TO 39
      IF(1B1.EQ.ILOW) GO TO 2001
      1B1=0
      REWIND 9
      C  READ SATELLITE IDENTIFICATION,CHECK FOR AMPERSAND*****
      39 CONTINUE
      READ(9,601,END=902,ERR=39)(DATA(I),I=1,65)
      601 FORMAT(65A1)
      94 CONTINUE
      IF(DATA(1).NE.IAMP)GO TO 39
      IF(DATA(7).EQ.SPX)GO TO 83
      IF(DATA(8).EQ.SPX)GO TO 83
      IF(DATA(4)-BIN.EQ.0)GO TO 85
      SAT=((DATA(3)-BIN)*1000.)+(DATA(4)-BIN)*1000.+(DATA(5)-BIN)*10
      X0.+(DATA(6)-BIN)*10.+(DATA(8)-BIN)
      GO TO 84
      85 SAT=((DATA(2)-BIN)*1000.)+(DATA(3)-BIN)*1000.+(DATA(5)-BIN)*10
      X0.+(DATA(6)-BIN)*10.+(DATA(8)-BIN)
      IGRADE=(DATA(10)-BIN)
      IYEAR=(DATA(12)-BIN)*10+(DATA(13)-BIN)
      GO TO 84
      83 SAT=((DATA(2)-BIN)*1000.)+(DATA(3)-BIN)*1000.+(DATA(4)-BIN)*10
      X0.+(DATA(5)-BIN)*10.+(DATA(6)-BIN)
      84 CONTINUE
      1B1=1B1+1
      IF(1B1.LT.ILOW)GO TO 39
      IF(1B1.GT.IHIGH)GO TO 9C2
      2001 CONTINUE
      DO 602 M=1,50
      IF(SAT.EQ.KSAID(M))GO TO 603
      602 CONTINUE
      WRITE(6,635)
      635 FORMAT(19H SAID NOT IN TABLE )
      WRITE(6,183)IAMP,SAT
      183 FORMAT(X,A1,I5)
      GO TO 604
      603 CONTINUE
      IF(IPAGE.EQ.0)GO TO 320
      WRITE(6,302)IPAGE,(MSGR(I),I=1,80)
      IPAGE=0

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320 WRITE(6,310) IPAGE, IBI
WRITE(6,660)(DATA(I), I=1,65)
KKS AID=KSAID(M)
C READ CAL. LINE WITH FORMAT CHECK *****
READ(9,601,END=902,ERR=30)(DATA(I), I=1,65)
IF(DATA(1).EQ.IAMP) GO TO 83
WRITE(6,660)(DATA(I), I=1,65)
C CHECK PERIODS IN CAL. LINE
IF(DATA(5).NE.PEZ) GO TO 604
IF(DATA(13).NE.PEZ) GO TO 604
IF(DATA(18).NE.PEZ) GO TO 604
IF(DATA(26).NE.PEZ) GO TO 604
IF(DATA(31).NE.PEZ) GO TO 604
IF(DATA(39).NE.PEZ) GO TO 604
IF(DATA(45).NE.PEZ) GO TO 604
IF(DATA(53).NE.PEZ) GO TO 604
IF(DATA(57).NE.PEZ) GO TO 604
IF(DATA(65).NE.PEZ) GO TO 604
DO 605 K=1,4
IF(DATA(K)-BIN.GT.9) GO TO 604
IF(DATA(K)-BIN.LT.0) GO TO 604
DATA(K)=DATA(K)-BIN
605 CONTINUE
DO 606 K=6,12
IF(DATA(K)-BIN.GT.9) GO TO 604
IF(DATA(K)-BIN.LT.0) GO TO 604
DATA(K)=DATA(K)-BIN
606 CONTINUE
DO 607 K=14,17
IF(DATA(K)-BIN.GT.9) GO TO 604
IF(DATA(K)-BIN.LT.0) GO TO 604
DATA(K)=DATA(K)-BIN
607 CONTINUE
DO 608 K=19,25
IF(DATA(K)-BIN.GT.9) GO TO 604
IF(DATA(K)-BIN.LT.0) GO TO 604
DATA(K)=DATA(K)-BIN
608 CONTINUE
DO 609 K=27,30
IF(DATA(K)-BIN.GT.9) GO TO 604
IF(DATA(K)-BIN.LT.0) GO TO 604
DATA(K)=DATA(K)-BIN
609 CONTINUE
DO 610 K=32,38

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0002180
0002190
0002200
0002210
0002220
0002230
0002240
0002250
0002260
0002270
0002280
0002290
0002300
0002310
0002320
0002330
0002340
0002350
0002360
0002370
0002380
0002390
0002400
0002410
0002420
0002430
0002440
0002450
0002460
0002470
0002480
0002490
0002500
0002510
0002520
0002530
0002540
0002550
0002560
0002570
0002580
0002590
0002600
0002610

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IF(DATA(K)-BIN.GT.9)GO TO 604
IF(DATA(K)-BIN.LT.0)GO TO 604
DATA(K)=DATA(K)-BIN
610 CONTINUE
DO 611 K=40,44
IF(DATA(K)-BIN.GT.9)GO TO 604.
IF(DATA(K)-BIN.LT.0)GO TO 604.
DATA(K)=DATA(K)-BIN
611 CONTINUE
DC 612 K=46,52
IF(DATA(K)-BIN.GT.9)GO TO 604
IF(DATA(K)-BIN.LT.0)GO TO 604
DATA(K)=DATA(K)-BIN
612 CONTINUE
DO 613 K=54,56
IF(DATA(K)-BIN.GT.9)GO TO 604.
IF(DATA(K)-BIN.LT.0)GO TO 604.
DATA(K)=DATA(K)-BIN
613 CONTINUE
DO 614 K=58,64
IF(DATA(K)-BIN.GT.9)GO TO 604
IF(DATA(K)-BIN.LT.0)GO TO 604
DATA(K)=DATA(K)-BIN
614 CONTINUE
X=DATA(9)+DATA(22)+DATA(35)+DATA(49)+DATA(61)
IF(X.NE.45.)GO TO 604
CSTA=(DATA(55)*10.)+(DATA(56))
DO 616 L=1,17
IF(KSTA(L).EQ.CSTA)GO TO 617
616 CONTINUE
WRITE( 6,618)
618 FORMAT(27H WRONG STATION IN CAL.LINE )
GO TO 604
617 D=DATA(3)*10+DATA(4)
CEWM=D/100.
D=DATA(16)*10+DATA(17)
CEWC=D/100.
D=DATA(6)*100+DATA(7)*1C+DATA(8)
CEWF1=D/1000.
D=DATA(19)*100+DATA(20)*10+DATA(21)
CEWF2=D/1000.
D=DATA(32)*100+DATA(33)*10+DATA(34)
CEWF3=D/1000.
D=DATA(46)*100+DATA(47)*10+DATA(48)
0002620
0002630
0002640
0002650
0002660
0002670
0002680
0002690
0002700
0002710
0002720
0002730
0002740
0002750
0002760
0002770
0002780
0002790
0002800
0002810
0002820
0002830
0002840
0002850
0002860
0002870
0002880
000289
0002900
0002910
0002920
0002930
0002940
0002950
0002960
0002970
0002980
0002990
0003000
0003010
0003020
0003030
0003040
0003050

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CEWF4=D/1000.
D=DATA(58)*100+DATA(59)*10+DATA(60)
CEWF5=D/1000.
D=DATA(10)*100+DATA(11)*10+DATA(12)
CNSF1=D/1000.
D=DATA(23)*100+DATA(24)*10+DATA(25)
CNSF2=D/1000.
D=DATA(36)*100+DATA(37)*10+DATA(38)
CNSF3=D/1000.
D=DATA(50)*100+DATA(51)*10+DATA(52)
CNSF4=D/1000.
D=DATA(62)*100+DATA(63)*10+DATA(64)
CNSF5=D/1000.
D=DATA(29)*10+DATA(30)
CNSM=D/100.
D=DATA(43)*10+DATA(44)
CNSC=D/100.
CSTA=DATA(55)*10+DATA(56)
I11 = 1
WRITE(11,310) I11,I11
WRITE(11,501)IAMP,SAT,CSTA,STATIO(L)
501  FORMAT(X,A1,I5,X,I2,X,A6)
CANT=DATA(54)
END=DATA(65)
43  CEWM=EWM(L)+CEWM
CEWC=EWC(L)+CEWC
CNSM=NSM(L)+CNSM
CNSC=NSC(L)+CNSC
KM=5.
RATE=0.
IDIF1=CEWF2-CEWF1
IDIF2=CEWF3-CEWF2
IDIF3=CEWF4-CEWF3
IDIF4=CEWF5-CEWF4
CEWF1=CEWF3+((9.*(IDIF3-IDIF2))-3.*(IDIF4-IDIF1))/35.)
IDIF=0.
IF(CANT-2.)162,160,161
NARROW BAND TRACKING FILTER *****
C 160 IDIF=.0
AST(1)=SPA
GO TO 164
161 ICIF=.0
AST(1)=ASK
GO TO 164
0003060
0003070
0003080
0003090
0003100
0003110
0003120
0003130
0003140
0003150
0003160
0003170
0003180
0003190
0003200
0003210
0003220
0003230
000324
000325
0003260
0003270
0003280
0003290
0003300
0003310
0003320
0003330
0003340
0003350
0003360
0003370
0003380
0003390
0003400
0003410
0003420
0003430
0003440
0003450
0003460
0003470
0003480
0003490

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162 IF(CANT.EQ.1.)GO TO 164
163 IDIF=.120
C 2 CPS TRACKING FILTER *****
AST(1)=PER
164 IDIF1=CNSF2-CNSF1
IDIF2=CNSF3-CNSF2
IDIF3=CNSF4-CNSF3
IDIF4=CNSF5-CNSF4
CNSF1=CNSF3+((9.*(IDIF3-IDIF2))-(3.*(IDIF4-IDIF1)))/35.)
CABLE LENGTH INEQUALITIES
CEWM=((CLEWM(L)/.846)*(136.5-FREQ(M)))+CEWM
CEWC=((CLEWC(L)/.846)*(136.5-FREQ(M)))+CEWC
CNSM=((CLNSM(L)/.846)*(136.5-FREQ(M)))+CNSM
CNSC=((CLNSC(L)/.846)*(136.5-FREQ(M)))+CNSC
WRITE(11,636)
636 FORMAT(55H CALIBRATED PHASE READINGS,5 POINT FITTED FINE READINGS)
C CALIBRATED ZENITH *****
WRITE(11,639)
639 FORMAT(63H CEWM CEWC CNSM CNSC CEWF
X CNSF )
WRITE(11,150)CEWM,CEWC,CNSM,CNSC,CEWF1,CNSF1
150 FORMAT(6(X,F10.6))
WRITE(11,640)
640 FORMAT(74H HRMNSC EWFINE EWMED EWCORS NSFINE
XNSMED NSCORS )
READ DATA WITH FORMAT CHECK*****
DO 41 JK=1,60
K=JK
IF(K.EQ.32.)GO TO 120
621 READ(9,601,END=95,ERR=32)(DATA(I),I=1,65)
IF(DATA(1).EQ.IAMP)GO TO 120
WRITE(6,660)(DATA(I),I=1,65)
IF(DATA(10).EQ.SPX)GO TO 122
GO TO 124
122 IF(DATA(30).EQ.SPX)GO TO 123
GO TO 124
123 IF(DATA(50).EQ.SPX)GO TO 120
124 IF(DATA(5).NE.PEZ)GO TO 621
CHECK PERIODS IN DATA LINE
IF(DATA(13).NE.PEZ)GO TO 621
IF(DATA(18).NE.PEZ)GO TO 621
IF(DATA(26).NE.PEZ)GO TO 621
IF(DATA(31).NE.PEZ)GO TO 621
IF(DATA(39).NE.PEZ)GO TO 621
0003500
0003510
0003520
0003530
0003540
0003550
0003560
0003570
0003580
0003590
0003600
0003610
0003620
0003630
0003640
0003650
0003660
0003670
0003680
0003690
0003700
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0003770
0003780
0003790
0003800
0003810
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0003840
0003850
0003860
0003870
0003880
0003890
0003900
0003910
0003920
0003930

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IF(DATA(45).NE.PEZ)GO TC 621
IF(DATA(53).NE.PEZ)GO TC 621
IF(DATA(57).NE.PEZ)GO TO 621
IF(DATA(65).NE.PEZ)GO TO 621
DO 622 J=1,4
IF(DATA(J)-BIN.GT.9)GO TO 621
IF(DATA(J)-BIN.LT.0)GO TO 621
DATA(J)=DATA(J)-BIN
622 CONTINUE
DO 623 J=6,12
IF(DATA(J)-BIN.GT.9)GO TO 621
IF(DATA(J)-BIN.LT.0)GO TO 621
DATA(J)=DATA(J)-BIN
623 CONTINUE
DO 624 J=14,17
IF(DATA(J)-BIN.GT.9)GO TO 621
IF(DATA(J)-BIN.LT.0)GO TO 621
DATA(J)=DATA(J)-BIN
624 CONTINUE
DO 625 J=19,25
IF(DATA(J)-BIN.GT.9)GO TO 621
IF(DATA(J)-BIN.LT.0)GO TO 621
DATA(J)=DATA(J)-BIN
625 CONTINUE
DO 626 J=27,30
IF(DATA(J)-BIN.GT.9)GO TO 621
IF(DATA(J)-BIN.LT.0)GO TO 621
DATA(J)=DATA(J)-BIN
626 CONTINUE
DO 627 J=32,38
IF(DATA(J)-BIN.GT.9)GO TO 621
IF(DATA(J)-BIN.LT.0)GO TO 621
DATA(J)=DATA(J)-BIN
627 CONTINUE
DO 628 J=40,44
IF(DATA(J)-BIN.GT.9)GO TO 621
IF(DATA(J)-BIN.LT.0)GO TO 621
DATA(J)=DATA(J)-BIN
628 CONTINUE
DO 629 J=46,52
IF(DATA(J)-BIN.GT.9)GO TO 621
IF(DATA(J)-BIN.LT.0)GO TO 621
DATA(J)=DATA(J)-BIN
629 CONTINUE

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0003940
0003950
0003960
0003970
0003980
0003990
0004000
0004010
0004020
0004030
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0004050
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0004070
0004080
0004090
0004100
0004110
0004120
0004130
0004140
0004150
0004160
0004170
0004180
0004190
0004200
0004210
0004220
0004230
0004240
0004250
0004260
0004270
0004280
0004290
0004300
0004310
0004320
0004330
0004340
0004350
0004360
0004370

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DO 630 J=54,56
IF(DATA(J)-BIN.GT.9)GO TO 621
IF(DATA(J)-BIN.LT.0)GO TO 621
DATA(J)=DATA(J)-BIN
630 CONTINUE
DO 631 J=58,64
IF(DATA(J)-BIN.GT.9)GO TO 621
IF(DATA(J)-BIN.LT.0)GO TO 621
DATA(J)=DATA(J)-BIN
631 CONTINUE
SECD(K)=DATA(1)*10+DATA(2)
MIND(K)=DATA(14)*10+DATA(15)
HORD(K)=DATA(27)*10+DATA(28)
ANTD(K)=DATA(54)
IDAYD(K)=DATA(40)*100+DATA(41)*10+DATA(42)
SYAD(K)=DATA(55)*10+DATA(56)
D=DATA(3)*10+DATA(4)
EWM(D(K)=D/100.
D=DATA(16)*10+DATA(17)
EWCD(K)=D/100.
D=DATA(29)*10+DATA(30)
NSMD(K)=D/100.
D=DATA(43)*10+DATA(44)
NSCD(K)=D/100.
D=DATA(6)*100+DATA(7)*10+DATA(8)
EWF1=D/1000.
D=DATA(19)*100+DATA(20)*10+DATA(21)
EWF2=D/1000.
D=DATA(32)*100+DATA(33)*10+DATA(34)
EWF3=D/1000.
D=DATA(46)*100+DATA(47)*10+DATA(48)
EWF4=D/1000.
D=DATA(58)*100+DATA(59)*10+DATA(60)
EWF5=D/1000.
D=DATA(10)*100+DATA(11)*10+DATA(12)
NSF1=D/1000.
D=DATA(23)*100+DATA(24)*10+DATA(25)
NSF2=D/1000.
D=DATA(36)*100+DATA(37)*10+DATA(38)
NSF3=D/1000.
D=DATA(50)*100+DATA(51)*10+DATA(52)
NSF4=D/1000.
D=DATA(62)*100+DATA(63)*10+DATA(64)
NSF5=D/1000.

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0004380
0004390
0004400
0004410
0004420
0004430
0004440
0004450
0004460
0004470
0004480
0004490
0004500
0004510
0004520
0004530
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0004550
0004560
0004570
0004580
0004590
0004600
0004610
0004620
0004630
0004640
0004650
0004660
0004670
0004680
0004690
0004700
0004710
0004720
0004730
0004740
0004750
0004760
0004770
0004780
0004790
0004800
0004810

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0004820
0004830
0004840
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0004860
0004870
0004880
0004890
0004900
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0004920
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0004950
0004960
0004970
0004980
0004990
0005000
0005010
0005020
0005030
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0005060
0005070
0005080
0005090
0005100
0005110
0005120
0005130
000514
0005150
0005160
0005170
0005180
0005190
0005200
0005210
0005220
0005230
0005240
0005250

SIG1=DATA(9)
SIG2=DATA(22)
SIG3=DATA(35)
SIG4=DATA(49)
SIG5=DATA(61)
END=DATA(65)
100 IF(ANTD(K)-2)102,101,101
101 ANT=57.
102 GO TO 103
103 ANT=46.
104 TIM(K)={(HORD(K)*3600.)+(60.*MIND(K))+SECD(K)}
FOVEW(K,1)=EWF1
FOVEW(K,2)=EWF2
FOVEW(K,3)=EWF3
FOVEW(K,4)=EWF4
FOVEW(K,5)=EWF5
FOVNS(K,1)=NSF1
FOVNS(K,2)=NSF2
FOVNS(K,3)=NSF3
FOVNS(K,4)=NSF4
FOVNS(K,5)=NSF5
FIT FIVE FINES EACH LINE
IDIF1=EWF2-EWF1
CALL NORMAL(IDIF1)
IDIF2=EWF3-EWF2
CALL NORMAL(IDIF2)
IDIF3=EWF4-EWF3
CALL NORMAL(IDIF3)
IDIF4=EWF5-EWF4
CALL NORMAL(IDIF4)
EWF(K)=EWF3+((9.*(IDIF3-IDIF2))-(3.*(IDIF4-IDIF1)))/35.)
IDIF5=((IDIF1+IDIF2+IDIF3+IDIF4)/4.)
ICTEW = IDIF5 * 0.05
COUNTER DELAY (TIME) *****
EWF(K)=(EWF(K)-(.05*IDIF5*EWF3))
IDIF1=NSF2-NSF1
CALL NORMAL(IDIF1)
IDIF2=NSF3-NSF2
CALL NORMAL(IDIF2)
IDIF3=NSF4-NSF3
CALL NORMAL(IDIF3)
IDIF4=NSF5-NSF4
CALL NORMAL(IDIF4)
ENSF(K)=NSF3+((9.*(IDIF3-IDIF2))-(3.*(IDIF4-IDIF1)))/35.)

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0005260 IDIF5=((IDIF1+IDIF2+IDIF3+IDIF4)/4.)
000527 ICTNS = IDIF5 * 0.05
000528 TIM2 = TIM(K) - TIM(1) + 0.000001
000529 DO 300 IFOV = 1,5
000530 TFOVEW(K,IFOV)=TIM2+0.2*(IFOV-1)+FOVEW(K,IFOV)*0.01
000531 TFOVNS(K,IFOV)=TIM2+0.2*(IFOV-1)+FOVNS(K,IFOV)*0.01
000532
300 CONTINUE
C FILTER DELAY (TIME)
ENSF(K)=ENSF(K)-(.05*IDIF5*NSF3)
IDIF1=SIG2-SIG1
IDIF2=SIG3-SIG2
IDIF3=SIG4-SIG3
IDIF4=SIG5-SIG4
SIGD(K)=SIG3+((9.*(IDIF3-IDIF2))-3.*(IDIF4-IDIF1))/35)
WRITE(11,151)HORD(K),MIND(K),SECD(K),EWF(K),EWD(K),EWC(D(K),ENSF(
XK),NSMD(K),NSCD(K)
151 FORMAT(X,12,12,12,X,(6(F10.6,X)))
41 CONTINUE
GO TO 120
95 CONTINUE
KEND=1
C DATA MSG.COMPLETE,START SMOOTHING *****
120 SL=.01
AST(6)=SPA
K=K-1
NBRK=K
IF(K.LE.5)GO TO 780
GO TO 782
780 WRITE( 6,781)
781 FORMAT(27H LESS THAN 5 LINES OF DATA )
KZ=K-1
WRITE(13,341)IB1,CSTA,STATIO(L)
WRITE(13,346)
346 FORMAT(1H+,32X,'MESSAGE TOO SHORT.1)
IF(KEND.EQ.1)GO TO 902
GO TO 78
782 JK=K
IF(ANT.EQ.57.) GO TO 90
GO TO 91
90 CEWF1=CEWF1+EWFPO(L)
CNSF1=CNSF1+NSFPO(L)
AST(2)=POL
GO TO 121
91 CEWF1=CEWF1+EWFEO(L)
0005600
0005610
0005620
0005630
0005640
0005650
0005660
0005670
0005680
0005690

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CNSF1=CNSF1+NSFEQ(L)
AST(2)=EQ
121 SM=2.0
WRITE(11,638)
638 FORMAT(32H KC-KS1 USING STATION CONSTANTS )
WRITE(11,1152)CEWF1,EWFP0(L),EWFEQ(L),CNSF1,NSFPO(L),NSFEQ(L)
CHECK TIME SEQUENCE *****
IB=0
IC=0
ID=0
IE=0
IF=0
IG=0
IH=0
KC=K-1
DO 20 KS=1,KQ
806 ITZM=TIM(KS+1)-TIM(KS)
IF(ITZM)807,807,808
807 TIM(KS+1)=TIM(KS+1)+86400.
GO TO 806
808 IF(ITZM.NE.1)GO TO 21
IB=IB+1
GO TO 20
21 IF(ITZM.NE.2 )GO TO 22
IC=IC+1
GO TO 20
22 IF(ITZM.NE.10 )GO TO 23
ID=ID+1
GO TO 20
23 IF(ITZM.NE.20 )GO TO 24
IE=IE+1
GO TO 20
24 IF(ITZM.NE.60 )GO TO 25
IF=IF+1
GO TO 20
25 IF(ITZM.NE.120 )GO TO 26
IG=IG+1
GO TO 20
26 IF(ITZM.NE.600 )GO TO 20
IH=IH+1
GO TO 20
20 CONTINUE
ITZM=MAXO(IB,IC,ID,IE,IF,IG,IH)
IF(IB.EQ.ITZM)GO TO 200

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0005700
0005710
0005720
0005730
0005740
0005750
0005760
0005770
0005780
0005790
0005800
0005810
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0005830
0005840
0005850
0005860
0005870
0005880
0005890
0005900
0005910
0005920
0005930
0005940
0005950
0005960
0005970
0005980
0005990
0006000
0006010
0006020
0006030
0006040
0006050
0006060
0006070
0006080
0006090
0006100
0006110
0006120
0006130

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IF(IC.EQ.ITZM)GO TO 201	0006140
IF(ID.EQ.ITZM)GO TO 202	0006150
IF(IE.EQ.ITZM)GO TO 203	0006160
IF(IF.EQ.ITZM)GO TO 204	0006170
IF(IG.CQ.ITZM)GO TO 205	0006180
IF(IH.EQ.ITZM)GO TU 206	0006190
200 AST(3)=F1	0006200
TILI=1.	0006210
GO TO 207	0006220
201 AST(3)=F2	0006230
TILI=2.	0006240
GO TO 207	0006250
202 AST(3)=F3	0006260
TILI=10.	0006270
GO TO 207	0006280
203 AST(3)=F4	0006290
TILI=20.	0006300
GO TO 207	0006310
204 AST(3)=F5	0006320
TILI=60.	0006330
GO TO 207	0006340
205 AST(3)=F6	0006350
TILI=120.	0006360
GO TO 207	0006370
206 AST(3)=F7	0006380
TILI=600.	0006390
GO TO 207	0006400
72 WRITE(6,73)	0006410
73 FORMAT(22H TIME OUT OF SEQUENCE)	0006420
WRITE(13,341)IB1,CSTA,STATIO(L)	0006430
WRITE(13,345)	0006440
345 FORMAT(IH+,23X,'FRAME TIME OUT OF SEQUENCE')	0006450
KZ=K-1	0006460
78 WRITE(6,77)SAT,CSTA,STATIO(L),HORD(KZ),MIND(KZ),IDAYD(KZ)	0006470
77 FORMAT(X,I5,X,I2,X,A6,X,I2,I2,X,I3)	0006480
GO TO 65	0006490
74 WRITE(6,75)	0006500
75 FORMAT(25H DATA EXCEEDS TIME CHECK)	0006510
WRITE(13,341)IB1,CSTA,STATIO(L)	0006520
WRITE(13,347)	0006530
347 FORMAT(IH+,31X,'EXCEEDS TIME CHECK')	0006540
KZ=K-1	0006550
GO TO 78	0006560
50 WRITE(11,51)	0006570

```

51 FORMAT(40H EAST MEDIUM CHANNEL EXCEEDS 100 COUNTS ) 0006580
   AST(6)=F1 0006590
   RATE=0. 0006600
   GO TO 58 0006610
52 WRITE(11,53) 0006620
53 FORMAT(40H EAST COURSE CHANNEL EXCEEDS 100 COUNTS ) 0006630
   AST(6)=F1 0006640
   RATE=0. 0006650
   GO TO 58 0006660
   GO TO 58 0006670
54 WRITE(11,55) 0006680
55 FORMAT(41H NORTH MEDIUM CHANNEL EXCEEDS 100 COUNTS ) 0006690
   AST(6)=F2 0006700
   RATE=0. 0006710
   GO TO 59 0006720
56 WRITE(11,57) 0006730
57 FORMAT(41H NORTH COURSE CHANNEL EXCEEDS 100 COUNTS ) 0006740
   AST(6)=F2 0006750
   RATE=0. 0006760
   GO TO 59 0006770
804 WRITE(11,805) 0006780
805 FORMAT(27H DATA WILL NOT LOBE ASSIGN ) 0006790
   WRITE(13,341)IB1,CSTA,STATIO(L) 0006800
   WRITE(13,348) 0006810
348 FORMAT(1H+,29X,'WILL NOT LOBE ASSIGN') 0006820
   KZ=K-1 0006830
   GO TO 78 0006840
   EW AMBIGUITY LOBE ASSIGN. 0006850
   C 207 SL=.015 0006860
   K=JK-1 0006870
   DO 70 N=1,K 0006880
   IF(TIM(N+1)-TIM(N))72,72,71 0006890
71 IF(TIM(N+1)-TIM(N)-(5.*TILI))70,70,74 0006900
70 CONTINUE 0006910
   K=JK 0006920
   CALL LOBASN(TIM,K,EWMD,RATE,ITD) 0006930
   IF(ITD.GE.100)GO TO 804 0006940
   CALL LOBASN(TIM,K,EWCD,RATE,ITD) 0006950
   IF(ITD.GE.100)GO TO 804 0006960
   CALL LSQUA(TIM,ALPHA,EWMD,K,MID,SIA,SL,EWMB,EWMC,SM,ENA,EOA) 0006970
   EWMA=ALPHA+EWMD(MID) 0006980
   EWMT=TIM(MID)-.15 0006990
   SA=SIA 0007000
   WRITE(11,643) 0007010
643 FORMAT(83H ALPHA.EWM MID.PT. RATE SIGMA

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X      BETA      GAMMA      )
WRITE(11,152)ALPHA,MID,RATE,SIA,EWMB,EWMC
152  FORMAT(X,F14.6,X,I6,X,4(F14.6,X))
K=JK
CALL LSQQUA(TIM,ALPHA,EWCD,K,MID,SIA,SL,EWCB,EWCC,SM,ENB,EOB)
EWCA=ALPHA+EWCD(MID)
EWCT=TIM(MID)+.05
SB=SIA
WRITE(11,644)
644  FORMAT(83H      ALPHA,EWC      MID,PT.      RATE      SIGMA
X      BETA      GAMMA      )
WRITE(11,152)ALPHA,MID,RATE,SIA,EWCB,EWCC
RATE=((EWMB*ANT/4.)+(EWCB*ANT/3.5))/2.
IF(ABS(RATE).LE..05)RATE=0.0
C      EWF LOBE ASSIGN.
IF(ABS(SB).GT..1)GO TO 52
IF(ABS(SA).GT..1)GO TO 50
58  SL=.01
SM=2.5
K=JK
CALL LOBASN(TIM,K,EWF,RATE,ITD)
IF(ITD.GE.100)GO TO 804
CALL LSQQUA(TIM,ALPHA,EWF,K,MID,SIA,SL,EWFB,EWFC,SM,ENC,ECC)
MIDEN=MID
EWF=TIM(MID)
EWF=ALPHA+EWF(MID)
224  SC=SIA
INO=SIA*1000.+5
227  CALL ZERO(3,INO,IENG)
IDAYD(1)=IDAYD(MID)
WRITE(11,642)
642  FORMAT(83H      ALPHA,EWF      MID,PT.      RATE      SIGMA
X      BETA      GAMMA      )
WRITE(11,152)ALPHA,MID,RATE,SIA,EWFB,EWFC
WRITE(11,153)EWMA,EWT,EWCA,EWCT,RATE
153  FORMAT(6(F14.6,X))
C      NS AMBIGUITY LOBE ASSIGN.
SL=.015
RATE=0.
K=JK
SM=2.0
CALL LOBASN(TIM,K,NSMD,RATE,ITD)
IF(ITD.GE.100)GO TO 804
CALL LOBASN(TIM,K,NSCD,RATE,ITD)
0007020
0007030
0007040
0007050
0007060
0007070
0007080
0007090
0007100
0007110
0007120
0007130
0007140
0007150
0007160
0007170
0007180
0007190
0007200
0007210
0007220
0007230
0007240
0007250
0007260
0007270
0007280
0007290
0007300
0007310
0007320
0007330
0007340
0007350
0007360
0007370
0007380
0007390
0007400
0007410
0007420
0007430
0007440
0007450

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IF(ITD,GE,100)GO TU 804
CALL LSQQUA(TIM,ALPHA,NSMD,K,MID,SIA,SL,SNMB,SNMC,SM,ENX,EOE)
SNMA=ALPHA+NSMD(MID)
SNMT=TIM(MID)+.25
SD=SIA
WRITE(11,646)
646 FORMAT(83H ALPHA,NSM MID,PT. RATE SIGMA
X BETA GAMMA )
WRITE(11,152)ALPHA,MID,RATE,SIA,SNMB,SNMC
K=JK
CALL LSQQUA(TIM,ALPHA,NSCD,K,MID,SIA,SL,SNCB,SNCC,SM,ENE,EOE)
SNCA=ALPHA+NSCD(MID)
SNCT=TIM(MID)+.45
SE=SIA
RATE={((SNMB*ANT/4.)+(SNCB*ANT/3.5))/2.}
IF(ABS(RATE).LE..05)RATE=0.0
WRITE(11,647)
647 FORMAT(83H ALPHA,NSC MID,PT. RATE SIGMA
X BETA GAMMA )
WRITE(11,152)ALPHA,MID,RATE,SIA,SNCB,SNCC
NSF LOBE ASSIGN.
IF(ABS(SD).GT..1)GO TO 54
IF(ABS(SE).GT..1)GO TO 56
59 SL=.01
SM=2.5
K=JK
CALL LOBASN(TIM,K,ENSF,RATE,ITD)
IF(ITD,GE,100)GO TO 804
CALL LSQQUA(TIM,ALPHA,ENSF,K,MID,SIA,SL,SNFB,SNFC,SM,ENF,EOF)
MIDNS=MID
SNFT=TIM(MID)
SNFA=ALPHA+ENSF(MID)
230 SF=SIA
ISO=SIA*1000+.5
229 CALL ZERO(3,ISO,INNO)
IL=0
IK=0
IJ=50.
IF(ABS(SC).GT..05)GO TO 231
234 IF(ABS(SF).GT..05)GO TO 235
GO TO 239
231 AST(6)=F1
IK=50
GO TO 234

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235 AST(6)=F2
IL=50
239 WRITE(11,645)
645 FORMAT(83H
X BETA
ALPHA,NSF MID.PT. RATE SIGMA
GAMMA )
WRITE(11,152)ALPHA,MID,RATE,SIA,SNFB,SNFC
WRITE(11,153)SNMA,SNMT,SNCA,SNCT,RATE
WRITE(11,777)
C LOBE ASSIGNED DATA AFTER THE FIT HAS BEEN APPLIED *****
WRITE(11,641)
641 FORMAT(99H FRA.TIME EWFINE O-C EWMEOM O-C EWCORS O-C
XNSFINE O-C NSMEOM O-C NSCORS O-C )
K=JK
DO 790 I=1,K
T=TIM(I)-EWMT-.15
AM=EWA+(EWMB*T)+(EWMCT**2)
T=TIM(I)-EWCT+.05
AN=EWCA+(EWCB*T)+(EWCC*T**2)
T=TIM(I)-EWFT
AO=EWFA+(EWFb*T)+(EWFCT**2)
T=TIM(I)-SNMT+.25
AP=SNMA+(SNMB*T)+(SNMC*T**2)
T=TIM(I)-SNCT+.45
AQ=SNCA+(SNCB*T)+(SNCC*T**2)
T=TIM(I)-SNFT
AR=SNFA+(SNFB*T)+(SNFC*T**2)
AO=EEWF(I)-AO
AM=EWMD(I)-AM
AN=EWCD(I)-AN
AR=ENSF(I)-AR
AP=NSMD(I)-AP
AQ=NSCD(I)-AQ
WRITE(11,791)TIM(I),EEWF(I),AO,EWMD(I),AM,EWCD(I),AN,ENSF(I),AR,NS
XMD(I),AP,NSCD(I),AQ
791 FORMAT(X,F7.1,6(X,F7.3,X,F6.3))
790 CONTINUE
WRITE(11,792)ENA,SA,EOA,ENB,SB,EOB,ENC,SC,EOC
WRITE(11,793)
WRITE(11,794)
WRITE(11,792)ENX,SD,EOD,ENE,SE,EOE,ENF,SF,EOF
792 FORMAT(3(X,I2,4X,F5.3,8X,I2))
793 FORNAT( 67H IN EWN SIGMA OT IN EWC SIGMA OT IN EWF
X SIGMA OT )
794 FORNAT( 67H IN NSM SIGMA OT IN NSC SIGMA OT IN NSF
0007900
0007910
0007920
0007930
0007940
0007950
0007960
0007970
0007980
0007990
0008000
0008010
0008020
0008030
0008040
0008050
0008060
0008070
0008080
0008090
0008100
0008110
0008120
0008130
0008140
0008150
0008160
0008170
0008180
0008190
0008200
0008210
0008220
0008230
0008240
0008250
0008260
0008270
0008280
0008290
0008300
0008310
0008320
0008330

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C.4

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X SIGMA      OT )
C  ADJUST TIME TO EWFINE FITTED TIME
XKFA=(KFA(L)/1000.)+LDIF
XKFB=(KFB(L)/1000.)+LDIF
EW4SEC=(EWFC*XKFA-EWFB)*XKFA
SN4SEC=(SNFC*(EWFT-SNFT-XKFB)+SNFB)*(EWFT-SNFT-XKFB)
EWA=EWA+EWA4SEC
SNFA=SNFA+SN4SEC
EWFBEWFB+2.*EWFC*(-XKFA)
SNFBSNFB+2.*SNFC*(-XKFB)
EWMA=EWMA+EWMB*(EWFT-EWMT)+EWMC*((EWFT-EWMT)**2)
EWCA=EWCA+EWCB*(EWFT-EWCT)+EWCC*((EWFT-EWCT)**2)
SNMA=SNMA+SNMB*(EWFT-SNMT)+SNMC*((EWFT-SNMT)**2)
SNCA=SNCA+SNCB*(EWFT-SNCT)+SNCC*((EWFT-SNCT)**2)
EWFBB=EWA-CEWFI
C 118 PHASE ANGLE (FITTED) MINUS KS2+KC-KS1
EWMBB=EWMA-CEWM
EWCBB=EWCA-CEWC
SNFBB=SNFA-CNSFI
SNMBB=SNMA-CNSM
SNCBB=SNCA-CNSC
C  REMOVE LOBE INTERGER
LDIF=EWFBB
EWFBB=EWFBB-LDIF
LDIF=EWMBB
EWMBB=EWMBB-LDIF
LDIF=EWCBB
EWCBB=EWCBB-LDIF
LDIF=SNFBB
SNFBB=SNFBB-LDIF
LDIF=SNMBB
SNMBB=SNMBB-LDIF
LDIF=SNCBB
SNCBB=SNCBB-LDIF
AB=EWMBB-EWCBB
LDIF=AB
AB=AB-LDIF
CALL NORMAL(AB)
BC=SNMBB-SNCBB
LDIF=BC
BC=BC-LDIF
CALL NORMAL(BC)
AB4=AB*8.
BC4=BC*8.
0008340
0008350
0008360
0008370
000838
000839
000840
000841
0008420
0008430
0008440
0008450
0008460
0008470
0008480
0008490
0008500
0008510
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0008600
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0008620
0008630
0008640
0008650
0008660
0008670
0008680
0008690
0008700
0008710
0008720
0008730
0008740
0008750
0008760
0008770

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AB3=AB*7. 0008780
 BC3=BC*7. 0008790
 EAB4=AB4-EWMBB 0008800
 LDIF=EAB4 0008810
 EAB4=EAB4-LDIF 0008820
 CALL NORMAL(EAB4) 0008830
 EBC4=BC4-SNMBB 0008840
 LDIF=EBC4 0008850
 EBC4=EBC4-LDIF 0008860
 CALL NORMAL(EBC4) 0008870
 DE=AB4-EAB4 0008880
 FG=BC4-EBC4 0008890
 EAB3=AB3-EWCB8 0008900
 LDIF=EAB3 0008910
 EAB3=EAB3-LDIF 0008920
 CALL NORMAL(EAB3) 0008930
 EBC3=BC3-SNCBB 0008940
 LDIF=EBC3 0008950
 EBC3=EBC3-LDIF 0008960
 CALL NORMAL(EBC3) 0008970
 DE3=AB3-EAB3 0008980
 FG3=BC3-EBC3 0008990
 CORE=DE+DE3 009000
 CORN=FG+FG3 009010
 COREF=(ANT/7.5)*CORE 009020
 CORNF=(ANT/7.5)*CORN 009030
 FE=COREF-EWFBB 009040
 LDIF=FE 009050
 FE=FE-LDIF 009060
 CALL NORMAL(FE) 009070
 FN=CORNF-SNFBB 009080
 LDIF=FN 009090
 FN=FN-LDIF 009100
 CALL NORMAL(FN) 009110
 EWLOBE=COREF-FE 009120
 SNLOBE=CORNF-FN 009130
 AMBIGUITY ERRORS 009140
 EWMER=4./ANT*EWLOBE-DE 009150
 CALL NORMAL(EWMER) 009160
 EWGER=3.5/ANT*EWLOBE-DE3 009170
 CALL NORMAL(EWGER) 009180
 SNMER=4./ANT*SNLOBE-FG 009190
 CALL NORMAL(SNMER) 009200
 SNCER=3.5/ANT*SNLOBE-FG3 009210

C

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CALL NORMAL(SNCER)
ABB=AB*2
ADE=DE/4
ADE3=DE3/3.5
ACORE=CORE/7.5
AEWLOB=EWLOBE/ANT
WRITE(11,1152)ABB,ADE3,ADE,ACORE,AEWLOB,EWFT
ABC=8C*2
AFG=FG3/3.5
AFG3=FG3/3.5
AFG=FG/4
ACORN=CORN/7.5
ASNLOB=SNLOBE/ANT
WRITE(11,1152)ABC,AFG3,AFG,ACORN,ASNLOB,SNFT
1152 FORMAT(6(X,F14.6))
IF(ANTD(K)-2)650,651,651
651 WRITE(11,648)
648 FORMAT(12H POLAR PASS )
GO TO 652
650 WRITE(11,649)
649 FORMAT(17H EQUATORIAL PASS )
GO TO 652
652 IAO=2
IBO=3
SMITTY=((FREQ(M)/136.)*ANT)
ACOS=EWLOBE/SMITTY
BCOS=SNLOBE/SMITTY
DCOS= 1.-ACOS*ACOS-BCOS*BCOS
IF(DCOS.GE.0.0) DCOS = SQRT(DCOS)
ADOT = EWFB/SMITTY
BDOT = SNFB/SMITTY
IF(DCOS.NE.0.) DDOT = -(ACOS * ADOT + BCOS * BDOT)/DCOS
LL = L
IF(ANT.EQ.57.) LL = L + 17
IPASS(LL) = IPASS(LL) + 1
WRITE(6,1017) ACOS,BCOS,DCOS,ADOT,BDOT,DDOT,IARC,IPASS(LL)
1017 FORMAT(3X,4HL = ,F9.7,3X,4HM = ,F9.7,3X,4HN = ,F9.7,3X,7HLDOT = ,
F9.7,3X,7HMDOT = ,F9.7,3X,7HNDOT = ,F9.7/X,6HARC = ,I3,3X,
17HPASS = ,I3)
IF(LFILE) GO TO 1042
WRITE HEADINGS ON FILES
DO 1040 LF=1,16
LX=(LF-1)*2+20
WRITE(LX,1051) STATIO(LF),KSTA(LF)

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C

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WRITE (LX, 1052)
LX=LX+1
WRITE (LX, 1051) STATIO(LF), KSTA(LF+17)
WRITE (LX, 1052)
1040 CONTINUE
LFILE=.TRUE.
DETERMINE FILE NUMBER
C
1042 LF=(L-1)*2 +20
IF(ANT .EQ. 57.) LF=LF+1
1050 FORMAT (1X, I3, 3(1X, I3) , 2X, I3, 2X, I3, 2X, 6(2X, F9.6), 2(3X, F9.6))
1051 FORMAT (// 1X, '+++++')
*+++++
*+++++ //
*
20X, 'STATION NAME ', A6/20X, 'STATION NO. ', I4/)
1052 FORMAT (1X, 'DAY', 5X, 'GMT', 5X, 'ARC', 2X, 'PASS', 7X, 'L', 10X, 'M', 10X,
'N', 8X, 'LDT', 8X, 'MDOT', 8X, 'NDOT',
1 3X, 'KC-KS1+KS2', 3X, 'KC-KS1+KS2' /
2 6X, 'HR MIN SEC', 83X, '(EW)', 8X, '(NS)' //)
IGMH=TIM(MID)/3600.
IGMM=(TIM(MID)-(IGMH*3600.))/60.
IGMS=TIM(MID)-IGMH*3600.-IGMM*60.
WRITE(LF, 1050) IDAYD(MID), IGMH, IGMM, IGMS, IARC, IPASS(LL),
ACOS, BCOS, DCOS, ADOT, BDOT, DOOF, CEWFI, CNSFI
*
IF(SMITTY.GI.0.D0) GO TO 325
IF((ABS(ACOS).LT.CCOS).AND.(ABS(BCOS).LT.CCOS))GO TO 325
WRITE(I3, 341) IBI, CSTA, STATIO(L)
WRITE(I3, 326) KDEG
326 FORMAT(1H+, 26X, 'ELEV. LESS THAN ', I2, ' DEG. ')
GO TO 94
325 CONTINUE
EWLOBE = EWLOBE - EW4SEC
SNLOBE = SNLOBE - SN4SEC
XKFA = 0.4 - XKFA
XKFB = 0.4 - XKFB
EWTMP=EEWF(MIDEW)-CEWFI
SNTMP=ENSF(MIDEW)-CNSFI
CALL FIXUPI(EWLOBE, EWTMP, JOE)
CALL FIXUPI(SNLOBE, SNTMP, JON)
DO 301 IFOV=1, NBRK
EEWF(IFOV)=EEWF(IFOV)+JCE-CEWFI
ENSF(IFOV)=ENSF(IFOV)+JCN-CNSFI
DO 327 IFIX=1, 5
TFOVEW(IFOV, IFIX)=(TFOVEW(IFOV, IFIX)+TFOVNS(IFOV, IFIX)-XKFA
-XKFB)*0.5
*
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000998
000999
001000
001001
001002
001003
001004
001005
001006
001007
001008
001009

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DELTAT=TFOVEW(IFOV, IFIX)-TFOVNS(IFOV, IFIX)+XKFB      001010
FOVEW(IFOV, IFIX)=FOVEW(IFOV, IFIX)-DELTAT * EWF8 -CEWF1 001011
FOVNS(IFOV, IFIX)=FOVNS(IFOV, IFIX)+DELTAT *SNF8 - CNSF1 001012
CONTINUE      0010130
CALL FIXUP2(FOVEW(IFOV, 3), EWF(IFOV))      0010140
CALL FIXUP2(FOVNS(IFOV, 3), ENSF(IFOV))      0010150
CALL FIXUP2(FOVEW(IFOV, 2), FOVEW(IFOV, 3))      0010160
CALL FIXUP2(FOVEW(IFOV, 1), FOVEW(IFOV, 2))      0010170
CALL FIXUP2(FOVEW(IFOV, 4), FOVEW(IFOV, 3))      0010180
CALL FIXUP2(FOVEW(IFOV, 5), FOVEW(IFOV, 4))      0010190
CALL FIXUP2(FOVNS(IFOV, 2), FOVNS(IFOV, 3))      0010200
CALL FIXUP2(FOVNS(IFOV, 1), FOVNS(IFOV, 2))      0010210
CALL FIXUP2(FOVNS(IFOV, 4), FOVNS(IFOV, 3))      0010220
CALL FIXUP2(FOVNS(IFOV, 5), FOVNS(IFOV, 4))      0010230
DO 301 JOUT=1,5      0010240
AACOS(IFOV, JOUT)=FOVEW(IFOV, JOUT)/SMITTY      0010250
BBCOS(IFOV, JOUT)=FOVNS(IFOV, JOUT)/SMITTY      0010260
CONTINUE      0010270
N5=5*NBK      0010280
IPAGE=1      0010290
IGMT=TIM(1)      0010300
WRITE(6,310) IPAGE, IBL, IGMT      0010310
IPAGE=0      0010320
WRITE(6,302) IPAGE, (MSGR(I), I=1,80)      0010330
IPAGE=1      0010340
WRITE(6,306) KKSaid, STATIO(L), IDAYD(1), N5      0010350
FORMAT('OSATELLITE = ', I6, 7X, 'STATION = ', A6, 6X, 'DAY = ', I3, 7X,      0010360
1, DATA CARDS = ', I3/)      0010370
WRITE(6,308)      0010380
FORMAT(6X, 'EWF TIME', 2X, 'EWF COUNT', 6X, 'L', 9X, 'NSF TIME', 2X, 'NSF C      0010390
OUNT', 6X, 'M/')      0010400
FORMAT(' SATELLITE = ', I6, 7X, 'STATION = ', A6, 6X, 'DAY = ', I3, 7X,      0010410
1, DATA CARDS = ', I3)      0010420
FORMAT(6X, 'EWF TIME', 2X, 'EWF COUNT', 6X, 'L', 9X, 'NSF TIME', 2X, 'NSF C      0010430
OUNT', 6X, 'M')      0010440
FORMAT(11, 'S', '/', ' DATA MESSAGE NO. ', I5, 6X, 'GMT IN SEC. ', I5/)      0010450
FORMAT( ' &', '/', ' DATA MESSAGE NO. ', I5, 6X, 'GMT IN SEC ', I5)      0010460
DO 303 IOUT=1, NBK      0010470
DO 303 JOUT=1, 5      0010480
KLM=(IOUT-1)*5+JOUT      0010490
WRITE(6,304) TFOVEW(IOUT, JOUT), FOVEW(IOUT, JOUT), AACOS(IOUT, JOUT),      0010500
* TFOVEW(IOUT, JOUT), FOVNS(IOUT, JOUT), BBCOS(IOUT, JOUT), KLM      001051
FORMAT(2(4X, F10.5, 2X, F9.5, 2X, F8.5), 6X, I4)      0010520
JOY=JULDY(IYEAR, IDAYD(1))      0010530

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001054
0010550
0010560
0010570
0010580
0010590
001060
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0010620
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L = LL
IF(JDY.LT.JUDY(L))GO TO 331
IF((JDY.EQ.JUDY(L)).AND.(IGMT.LT.JUSEC(L)))GO TO 331
JUSEC(L)=IGMT
JUDY(L)=JDY
DNAP(1)=0.00
DNAP(2) = IARC
DNAP(3)=KSTA(L)
DNAP(4)=IPASS(L)
WRITE(12)(DNAP(I),I=1,6)
WRITE (19) DNAP
JDAY=JDY
DNAP(1)=JDAY
JDAY1=1
I=2*N5
WRITE(14,353)IBL,I,KSTA(L),STATIO(L),IARC,IPASS(L),JDAY,IGMT
*,ACOS,BCOS,DCOS,ADCT,BDOT,DDOT
353 FORMAT (3X,I5,I6,2X,I3,2X,A6,I4,I5,2X,I5,I6,6(2X,F8.6))
DO 332 IUUT=1,NBRK
DO 332 JUUT=1,5
DNAP(2)=IGMT+TFOVEW(IOUT,JOUT)
DNAP(3)=AACOS(IOUT,JOUT)
DNAP(4)=BBCOS(IOUT,JOUT)
335 IF(DNAP(2).LT.86400.00)GO TO 333
JDAY=JDAY+JDAY1
DNAP(1)=JDAY
JDAY1=0
DNAP(2)=DNAP(2)-86400.00
333 WRITE(12)(DNAP(I),I=1,6)
332 CONTINUE
I=DNAP(2)
XNAP(1)=JULDY(IYEAR,IDAYD(MID))
XNAP(2)=TIM(MID)
XNAP(3)=ACOS
XNAP(4)=BCOS
WRITE(19) XNAP
IF(IARCS.LT.0) GO TO 1995
II = 1
IF(IARCS.NE.IARC) II = 2
WRITE(7,2501) STATIO(LS),POLEQ,IARCS,JS,IPASSS,II
1995 IF(ANT.EQ.57.) GO TO 2000
POLEQ = EQ
JS = L + L - 1
GO TO 2100

```

```

2000 POLEQ = POL
      JS = L + L - 34
2100 TIMSTR = IGMT + TFOVEW(1,1) - 1.
      TIMEND = IGMT + TFOVEW(NBRK,5) + 1.
      WRITE(7,2500) I201,STATIO(L),POLEQ,IARC,JS,IPASS(L),
* IYEAR,IDAYD(1),TIMSTR
      WRITE(7,2500) I202,STATIO(L),POLEQ,IARC,JS,IPASS(L),
* IYEAR,IDAYD(1),TIMEND
      IARCS = IARC
      LS = L
      IPASS = IPASS(L)
2500 FORMAT(I3,2X,A6,A2,3I3,6X,I3,' 1',I3,10X,F9.1)
2501 FORMAT('999',2X,A6,A2,4I3)
      GO TO 94
331 CONTINUE
      WRITE(13,341)IB1,CSTA,STATIO(L)
341 FORMAT(' DATA MESSAGE NC.',I5,38X,'STATION NO.',I3,6X,'STATION NAM
      IE ',A6)
      WRITE(13,342)
342 FORMAT(1H+,26X,'MESSAGE OUT OF SEQUENCE')
      GO TO 94
30 WRITE( 6,31)
31 FORMAT(17H CAL.LINE PARITY )
      WRITE(13,341)IB1,CSTA,STATIO(L)
      WRITE(13,343)
343 FORMAT(1H+,33X,'CAL. LINE PARITY')
      GO TO 94
32 WRITE(11,33)
33 FORMAT(24H DATA PARITY,NO MSG.END )
      GO TO 621
604 CONTINUE
      WRITE(13,341)IB1,CSTA,STATIO(L)
      WRITE(13,344)
344 FORMAT(1H+,34X,'CAL. LINE ERROR')
      DO 60 JZ=1,60
      JY=JZ
      IF(JY.EQ.32)GO TO 94
61 READ(9,601,END=902,ERR=61)(DATA(I),I=1,65)
      IF(CATA(1).EQ.IAMP)GO TC 94
      IF(DATA(10).EQ.SPX)GO TC 62
      GO TO 64
62 IF(CATA(30).EQ.SPX)GO TO 63
      GO TO 64
63 IF(DATA(50).EQ.SPX)GO TC 39

```

```

001098
001099
001100
001101
001102
001103
001104
001105
001106
001107
001108
001109
001110
001111
001112
001113
001114
001115
001116
001117
001118
001119
001120
001121
001122
001123
001124
001125
001126
001127
001128
001129
001130
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001141

```



```

64 WRITE( 6,660)(DATA(I), I=1,65) 0011420
660 FORMAT(X,65A1) 0011430
60 CONTINUE 0011440
GO TO 94 0011450
65 K=JK-1 0011460
DO 66 I=1,K 0011470
WRITE( 6,67)HOR(I),MIND(I),SECD(I),EWF(I),EWM(I),EWC(I),ENSF(I) 0011480
X),NSMD(I),NSCD(I),AMTD(I),IDAYD(I),STAD(I) 0011490
67 FORMAT(X,I2,I2,I2,X,(6(F10.6,X)),I2,X,I3,X,I2,X) 0011500
66 CONTINUE 0011510
GO TO 94 0011520
777 FORMAT(IH1) 0011530
1 CONTINUE 001154
DNAP(1) = -1.00 001155
DNAP(2) = 0.00 001156
DNAP(4) = 0.00 001157
WRITE(I2) (DNAP(I), I = 1,6) 001158
WRITE(I9) DNAP 001159
END FILE 19 001160
REWIND 19 001161
3 WRITE (6,990) 001162
WRITE(11,990) 0011630
WRITE(13,340)(MSGR(I), I=1,80) 0011640
WRITE(13,349) 0011650
349 FORMAT(3X,'SUMMARY OF PASSES'//3X,'STATION NO.',9X,'STATION NAME', 0011660
113X,'PASSES',14X,'JUL DAY',17X,'SEC') 0011670
II = 3 001168
WRITE(7,2501) STATIO(LS),POLEQ,IARCS,JS,IPASSS,II 001169
DO 350 J=1,I7 001170
I=J 0011710
DO 350 JJ=1,2 0011720
IPASST(I) = IPASST(I) + IPASS(I) 001173
WRITE(13,351)KSTA(I),STATIO(I),IPASST(I),JUDY(I),JUSEC(I) 001174
I=I+17 001175
350 CONTINUE 0011760
351 FORMAT(4X,I5,17X,A6,15X,I5,2(17X,I5)) 0011770
WRITE(13,990) 0011780
END FILE 12 0011790
REWIND 12 0011800
990 FORMAT(50X,'JOB IS COMPLETE',2(/1H1)) 0011810
DO 355 J=1,2 0011820
N1=17*NJ 001183
N=N1-16 001184
WRITE(13,336)A1,N,(IPASS(I), I=N,N1) 0011850

```

```

355 CONTINUE                                0011860
DO 356 J=1,2                                0011870
N1=17*J                                     001188
N=N1-16                                     001189
WRITE(13,336)A2,N,(JUDY(I),I=N,N1)        0011900
356 CONTINUE                                0011910
DO 357 J=1,2                                0011920
N1=17*J                                     001193
N=N1-16                                     001194
WRITE(13,336)A3,N,(JUSEC(I),I=N,N1)        0011950
357 CONTINUE                                0011960
336 FORMAT(1X,A5,1815)                      001197
STOP                                         0011980
321 WRITE(6,322)                             0011990
322 FORMAT('1 *STOP* NO DATA IN FT08 FILE') 0012000
STOP                                         0012010
END                                           0012020
SUBROUTINE FIXUP1(EWLOBE,EWF,JOE)           0012030
FOVEWF=EWLOBE-EWF                           0012040
JOE=FOVEWF                                  0012050
IF (ABS(FOVEWF-JOE)-0.5) 1,1,2              0012060
2 IF (FOVEWF-JOE) 3,3,4                     0012070
3 JOE=JOE-1                                  0012080
RETURN                                       0012090
4 JOE=JOE+1                                  0012100
1 RETURN                                     0012110
END                                           0012120
SUBROUTINE FIXUP2(EWMID,EWF)               0012130
IF (EWF.LT.0.0) EWMID=CWMID-1.0            0012140
DIFF=EWF-EWMID                              0012150
NDIFF=DIFF                                   0012160
IF (ABS(DIFF-NDIFF)-0.5) 1,1,2              0012170
1 EWMID=EWMID+NDIFF                          0012180
RETURN                                       0012190
2 IF (DIFF) 3,3,4                            0012200
3 NDIFF=NDIFF-1                              0012210
GO TO 1                                       0012220
4 NDIFF=NDIFF+1                              0012230
GO TO 1                                       0012240
END                                           0012250
SUBROUTINE LOBASN(TEM,I,A,RATE,L)           0012260
DIMENSION A(31),TEM(31)                    0012270
K=I-1                                         0012280
IF (RATE.GT.0.) A(1)=A(1)+1.               0012290

```

```

IF(RATE*LT*0.0)*A(1)=A(1)-1.
DO 10 J=1,K
L=0
JJ=J+1
DELTA=RATE*(TEM(JJ)-TEM(J))
11 X=A(JJ)-A(J)
L=L+1
IF(L*GE.100)GO TO 12
IF(ABS(DELTA-X)-.500)10,10,6
6 IF(DELTA)4,5,3
4 A(JJ)=A(JJ)-1
GO TO 11
3 A(JJ)=A(JJ)+1
GO TO 11
5 IF(X)3,10,4
10 CONTINUE
12 RETURN
END
SUBROUTINE LSQUA(T,ALPHA,XY,ITO,L,SIGMA,F,BETA,GAMMA,SM,INN,IOI)
DIMENSION B(3,4),A(3,4),T(32),XY(32)
DO 1 I=1,3
DO 1 J=1,4
1 A(I,J)=0.0
L=(ITO+1)/2
A(1,1)=ITO
INN=ITO
DELSQ=0.
DO 10 I=1,ITO
RAPPA=XY(I)-XY(L)
TAU=T(I)-T(L)
A(1,2)=A(1,2)+TAU
A(1,3)=A(1,3)+TAU**2
A(1,4)=A(1,4)+RAPPA
A(2,3)=A(2,3)+TAU**3
A(2,4)=A(2,4)+RAPPA*TAU
A(3,3)=A(3,3)+TAU**4
A(3,4)=A(3,4)+RAPPA*TAU**2
10 DELSQ=RAPPA**2+DELSQ
67 A(2,2)=A(1,3)
A(2,1)=A(2,4)
A(3,1)=A(3,4)
N=1
DO20 K=1,3
N=N+1
0012300
0012310
0012320
0012330
0012340
0012350
0012360
0012370
0012380
0012390
0012400
0012410
0012420
0012430
0012440
0012450
0012460
0012470
0012480
0012490
0012500
0012510
0012520
0012530
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0012550
0012560
0012570
0012580
0012590
0012600
0012610
0012620
0012630
0012640
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0012660
0012670
0012680
0012690
0012700
0012710
0012720
0012730

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0012740
0012750
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0012800
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0012990
0013000
0013010
0013020
0013030
0013040
0013050
0013060
0013070
0013080
0013090
0013100
0013110
0013120
0013130
0013140
0013150
0013160
0013170

0015 J=N,4
15 B(K,J)=A(K,J)/A(K,K)
   IF(N-4)12,21,11
12 D020I=N,3
   D020J=I,4
20 A(I,J)=A(I,J)-A(K,I)*B(K,J)
21 GAMMA=B(3,4)
   BETA=B(2,4)-GAMMA*B(2,3)
   ALPHA =B(1,4)-BETA*B(1,2)-GAMMA*B(1,3)
   N=A(1,1)
   SIGMA=((DELSQ-ALPHA*A(1,4)-BETA*A(2,1)-GAMMA*A(3,1))/A(1,1))
   IF(SIGMA)70,71,71
70 SIGMA=0.
71 SIGMA=SQRT(SIGMA)
   IF(SIGMA-F )59,59,35
35 D061I=1,3
   D061J=I,4
61 A(I,J)=0.0
   DELSQ=0.0
   D065I=1,ITO
   RAPPA=XY(I)-XY(L)
   TAU= T(I)-T(L)
   R=RAPPA-ALPHA-BETA*TAU-GAMMA*TAU**2
   IF(R)2,3,3
2 R=-R
3 IF(R-SM*SIGMA)32,32,65
32 A(1,1)=A(1,1)+1.
   A(1,2)=A(1,2)+TAU
   A(1,3)=A(1,3)+TAU**2
   A(1,4)=A(1,4)+RAPPA
   A(2,3)=A(2,3)+TAU**3
   A(2,4)=A(2,4)+RAPPA*TAU
   A(3,3)=A(3,3)+TAU**4
   A(3,4)=A(3,4)+RAPPA*TAU**2
   DELSQ=RAPPA**2+DELSQ
65 CONTINUE
66 IF(A(1,1)-5)59,66,66
59 ITO=A(1,1)
   IOT=ITO
   RETURN
11 WRITE( 6,7)
7 FORMAT(30H THIS MSG. HAS EXCESSIVE NOISE)
   RETURN

```

```

0013180
SUBROUTINE NORMAL(X)
IF(X)113,114,115
113 IF(ABS(X)-.5)114,114,116
116 X=X+1.0
GO TO 114
115 IF(ABS(X)-.5)114,114,117
117 X=X-1.0
114 RETURN
END
SUBROUTINE ZERO(N,IIN,AREA)
DIMENSION DIV(7)
INTEGER DIV
LOGICAL*1 PLUS,MINUS,ASK,IC(10),AREA(80)
DATA PLUS,MINUS,ASK,IC(1),IC(2),IC(3),IC(4),IC(5),IC(6),IC(7),IC(8)
X,IC(9),IC(10)/Z40,Z60,Z5C,ZF0,ZF1,ZF2,ZF3,ZF4,ZF5,ZF6,ZF7,ZF8,ZF9
X/
DATA DIV(1),DIV(2),DIV(3),DIV(4),DIV(5),DIV(6),DIV(7)/1000000,1000
X00,10000,1000,100,10,1/
AREA(1)=PLUS
IF(IIN)1,2,2
1 AREA(1)=MINUS
2 IIN=IABS(IIN)
K=2
J=N-1
DO 4 I=1,J
ITEMP=IIN/DIV(IJ)
IF(ITEMP.LE.9.)GO TO 6
AREA(K)=ASK
GO TO 5
6 AREA(K)=IC(ITEMP+1)
5 IIN=IIN-(ITEMP*DIV(IJ))
IJ=IJ+1
K=K+1
4 CONTINUE
RETURN
END
INTEGER FUNCTION JULDY(Y,D)
INTEGER Y,D
L=(Y-50+1)/4
JULDY=L*366
JULDY=(Y-50-L)*365+JULDY+D-1
RETURN
0013190
0013200
0013210
0013220
0013230
0013240
0013250
0013260
0013270
0013280
0013290
0013300
0013310
0013320
0013330
0013340
0013350
0013360
0013370
0013380
0013390
0013400
0013410
0013420
0013430
0013440
0013450
0013460
0013470
0013480
0013490
0013500
0013510
0013520
0013530
0013540
0013550
0013560
0013570
0013580
0013590
0013600
0013610

```

END

0013620

1371 CARDS

A-2.4 A PROGRAM FOR MERGING TWO OPTICAL DATA TAPES
(IN A GEOS FORMAT) INTO A SINGLE TAPE - SAMPLE JCL

PROGRAM FOR COMBINING TWO GEOS-FCRMATED DATA TAPES
 FOR USE BY OPTICAL PREPROCESSOR PROGRAM

```

REAL*8 TAPE
INTEGER*2 ID, I10
LOGICAL*1 A, B, AA, BB, ZERC, BLANK, AA1, BB1, I9
DIMENSION A(78), B(78), AA(2), BB(2)
EQUIVALENCE (A(17), IYMA), (A(21), IDHA), (A(25), IMSA), (A(29), IFSA),
1(B(5), ID), (B(17), IYMB), (B(21), IDHB), (B(25), IMSB), (B(29), IFSB),
2(AA1, AA(1)), (BB1, BB(1)))
COMMON TAPE, IFILE, IYM, INIT, LINE
DATA ZERO, BLANK / 0, ' ' /
DATA I9, I10 / 9, 10 /
INIT = 0
READ (5, 900) TAPE, IFILE
READ (1, 1000, END = 300) AA, A
READ (1, 1000, END = 300) BB, B
READ (1, 1000, END = 300) AA, A
DO 5 I = 23, 32
IF (A(I).EQ.BLANK) A(I) = ZERO
5 CONTINUE
10 READ (2, 1000, END = 400) BB, B
IF (ID.NE.I10) GO TO 10
DO 15 I = 23, 32
IF (B(I).EQ.BLANK) B(I) = ZERO
15 CONTINUE
C
IF (IYMA - IYMB) 20, 20, 30
20 CALL RESET (IYMA)
GO TO 35
30 CALL RESET (IYMB)
35 INIT = -1
40 CONTINUE
IF (IYMA - IYMB) 100, 50, 200
50 IF (IDHA - IDHB) 100, 60, 200
60 IF (IMSA - IMSB) 100, 70, 200
70 IF (IFSA.GT.IFSB) GC TO 200
100 CONTINUE
IF (IYMA.GT.IYM) CALL RESET (IYMA)
WRITE (3, 1000) AA, A
  
```



```

IF(KEY7L.GT.0) PLOT(1)=STAR
IF(KEY7M.GT.0) PLOT(2)=STAR
WRITE(LF,1107) IDAY,IH,IM,SEC,NOARC,NOPASS,LERROR,MERROR,ELEV,WT,
*LSD,MSD,LLOBE,MLOBE,NOBS,NEBIT,SLOPE,IROPE,DMS,PLOT
GO TO 10
200 RETURN
500 ERR(I)=10.050
KI(I)=1
GO TO 30
520 IF (ERRORP.GT.20.00) KI(I)= IGRAPH(I)+20
IF(ERRORP.LT.-20.00) KI(I)= IGRAPH(I)-20
GRAPH(KI(I))= STAR
GO TO 30
1104 FORMAT (//1X,132(=)//10X,A8,10X,STATION ID',I4//47X,'IN STD
* LOBE NUMBER PTS',6X,'ERROR RATE',7X,'RD IN COMPUTED
* NEW*/32X*ERROR ELEVA SOL DEV CORR OF PTS DELTD'
*,22X,'ST OV MEASUREMENT WT'/1X,'DAY HR MN SECOND ARC PASS
* L M TION L M L M L M L M L',8X,'
*M',7X,'L M L',8X,'M L M'//)
1105 FORMAT(//1X,132(=)//1X,A8,'STATION',I4,'ARC',I3,'PASS',
113/43X,'MIDPOINT TIME',14X,'MEAN ERROR',9X,'STANDARD DEVIATION'
242X,'DAY HR MN SECOND',2(12X,'L',9X,'M')/2X,
3'TIME ERROR RELATIVE TO',12X,3I3,F7.3,6X,2F10.5,4X,2F9.5/
41X,'RELATIVE MEAN PASS ERROR'/1X,'TO MIDPT L',9X,'M'//)
1106 FORMAT(F9.3,2F10.5,5X,83A1)
1107 FORMAT (1X,3I3,F7.3,I3,I5,1X,2I6,5X,A1,3X,A1,1X,A1,2I4,2(1X,2I4),1
*X,2I3,1X,2D9.2,1X,2I3,2F9.5,2(1X,A1))
END

```

0424 CARDS

PROGRAM FOR COMBINING TWO GEOS-FCRMATED DATA TAPES
FOR USE BY OPTICAL PREPROCESSOR PROGRAM

```

REAL*8 TAPE
INTEGER*2 ID, I10
LOGICAL*1 A, B, AA, BB, ZERC, BLANK, AA1, BB1, I9
DIMENSION A(78), B(78), AA(2), BB(2)
EQUIVALENCE (A(17), IYMA), (A(21), IDHA), (A(25), IMSA), (A(29), IFSA),
1(B(5), ID), (B(17), IYMB), (B(21), IDHB), (B(25), IMSB), (B(29), IFSB),
2(AA1, AA(1)), (BB1, BB(1)))
COMMGN TAPE, IFILE, IYM, INIT, LINE
DATA ZERO, BLANK / 0., 0. /
DATA I9, I10 / 9., 10. /
INIT = 0
READ (5, 900) TAPE, IFILE
READ (1, 1000, END = 300) AA, A
READ (1, 1000, END = 300) BB, B
READ (1, 1000, END = 300) AA, A
DO 5 I = 23, 32
IF (A(I).EQ.BLANK) A(I) = ZERO
5 CONTINUE
10 READ (2, 1000, END = 400) BB, B
IF (ID.NE.I10) GO TC 10
DO 15 I = 23, 32
IF (B(I).EQ.BLANK) B(I) = ZERO
15 CONTINUE
C
IF (IYMA - IYMB) 20, 20, 30
20 CALL RESET (IYMA)
GO TO 35
30 CALL RESET (IYMB)
35 INIT = -1
40 CONTINUE
IF (IYMA - IYMB) 100, 50, 200
50 IF (IDHA - IDHB) 100, 60, 200
60 IF (IMSA - IMSB) 100, 70, 200
70 IF (IFSA.GT.IFSB) GC TO 200
100 CONTINUE
IF (IYMA.GT.IYM) CALL RESET (IYMA)
WRITE (3, 1000) AA, A

```

```

WRITE (6,1010) AA,A
LINE = LINE - 1
IF (LINE.LT.0) CALL TITLE
READ (1,1000,END = 300) AA,A
IF(AA1.EQ.19) GO TO 300
DO 150 I = 23,32
IF (A(I).EQ.BLANK) A(I) = ZERO
150 CONTINUE
GO TO 40
200 IF (IYMB.GT.IYM) CALL RESET (IYMB)
WRITE (3,1000) BB,B
WRITE (6,1010) BB,B
LINE = LINE - 1
IF (LINE.LT.0) CALL TITLE
210 READ (2,1000,END = 400) BB,B
IF(BB1.EQ.19) GO TO 400
IF (ID.NE.110) GO TO 210
DO 215 I = 23,32
IF (B(I).EQ.BLANK) B(I) = ZERO
215 CONTINUE
GO TO 40
300 IF (IYMB.GT.IYM) CALL RESET (IYMB)
WRITE (3,1000) BB,B
WRITE (6,1010) BB,B
LINE = LINE - 1
IF (LINE.LT.0) CALL TITLE
310 READ (2,1000,END = 500) BB,B
IF(BB1.EQ.19) GO TO 500
IF (ID.NE.110) GO TO 310
GO TO 300
400 IF (IYMA.GT.IYM) CALL RESET (IYMA)
WRITE (3,1000) AA,A
WRITE (6,1010) AA,A
LINE = LINE - 1
IF (LINE.LT.0) CALL TITLE
READ (1,1000,END = 500) AA,A
IF(AA1.EQ.19) GO TO 500
GO TO 400
500 CONTINUE
END FILE 3
REWIND 1
REWIND 2
REWIND 3
WRITE (6,1040)

```


// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200),VOL=SER=1666H
//GO.FT03F001 DD UNIT=2400-9,LABEL=(12,BLP),DISP=(NEW,PASS),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200,DEN=2),VOL=SER=3826F
//GO.FT03FC02 DD UNIT=2400-9,LABEL=(13,BLP),DISP=(NEW,DELETE),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200,DEN=2),VOL=SER=3826F

//GO.DATAS DD *
3826F 12
/*

0140 CARDS

A-2.5 OPTICAL PREPROCESSING PROGRAM - SAMPLE JCL

C	1	
C	2	
C	3	
C	4	
C	5	
C	6	IMPLICIT REAL*8 (A-H,O-Z)
C	7	
C	8	
C	9	DIMENSION A(13),NOSTA(3C),NONAME(30),C(80),MONTH(12)
C	10	
C	11	COMMON/W/ TIM(49,30),RA(49,30),DEC(49,30),STNAM(30),TPASS,
C	12	IJDAYA(30),NUM(30),NCRDER(30),IYR1,IYR2,IM01,IM02,IDA1,IDA2,JDAY1,
C	13	IJDAY2,IARC,IARCS,ISIA(3C),JSTA(3C),NPASS(30),KSTA(30),KEY4,K,JS
C	14	COMMON /M/ TIM2
C	15	
C	16	
C	17	
C	18	THE NUMBERS IN ARRAY MONTH ARE THE DAY NUMBERS OF THE LAST DAY OF
C	19	THE PRECEDING MONTH. THE DAY NUMBERS ARE OBTAINED BY NUMBERING
C	20	THE DAYS OF THE YEAR CONSECUTIVELY STARTING WITH DAY NUMBER ZERO
C	21	ON 1 JANUARY.
C	22	
C	23	DATA MONTH/-1,30,58,89,119,150,180,211,242,272,303,333/
C	24	DATA MINUS/0,0,0/
C	25	
C	26	
C	27	TORBT IS USED BY THE PROGRAM TO SEPARATE ORBITS. OBSERVATIONS
C	28	(FOR ANY ONE STATION) SEPARATED BY MORE THAN TORBT SECONDS ARE
C	29	REGARDED AS BELONGING TO DIFFERENT ORBITS.
C	30	TPASS IS USED BY THE PROGRAM TO SEPARATE PASSES. A PASS IS
C	31	REGARDED AS CONSISTING OF THE OBSERVATIONS OF ONE PHOTOGRAPHIC
C	32	PLATE. OBSERVATIONS(FOR ANY ONE STATION) SEPARATED BY MORE THAN
C	33	TPASS SECONDS ARE REGARDED AS BELONGING TO DIFFERENT PASSES.
C	34	DELT IS THE TIME(IN SECONDS) ADDED TO THE OBSERVATION TIME TO
C	35	ACCOUNT FOR SATELLITE FLASH BUILD-UP.
C	36	NMAX IS THE MAXIMUM NUMBER OF OBSERVATIONS THAT THE PROGRAM
C	37	CAN ACCEPT FOR ANY ONE STATION AND ORBIT.
C	38	
C	39	TORBT = 2700.00
C	40	TPASS = 45.00
C	41	DELT = .000500

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42 NMAX = 49
43
44
45
46
47
48
49 C SET UP INITIAL CONDITIONS. SETTING KEY4 TO A NEGATIVE NUMBER
50 C ENSURES THAT THE FIRST NAP CARD PUNCHED BY SUBROUTINE DATAW
51 C IS A '201' CARD.
52 C 'IS' IS THE NUMBER OF STATIONS FOR WHICH OBSERVATIONS HAVE BEEN
53 C ACCUMULATED BUT NOT YET OUTPUT ON TAPE.
54 C IYMD2 IS THE CURRENT (YEAR,MONTH,DAY). SETTING IT TO A LARGE
55 C NUMBER ENSURES THAT WHEN THE FIRST OBSERVATION PAST THE START TIME
56 C FOR THE ARC IS READ IN, THE PROGRAM WILL ASSUME THAT A NEW DAY HAS
57 C COMMENCED.
58 C IYMD IS, IN GENERAL, THE (YEAR,MONTH,DAY) OF THE LAST OBSERVATION
59 C READ IN. HOWEVER, THE FIRST TIME IT IS USED NOTHING HAS BEEN
60 C READ IN. SETTING IT TO A LARGE NEGATIVE NUMBER ENSURES THAT
61 C THE PROGRAM WILL CONTINUE TESTING FOR THE START OF THE FIRST ARC.
62 C JDAY2 IS THE CURRENT JULIAN DAY NUMBER. SETTING IT EQUAL TO A
63 C LARGE NEGATIVE NUMBER ENSURES THAT THE PREVIOUS JULIAN DAY NUMBER
64 C ALWAYS IS LESS THAN THE CURRENT ONE, SINCE THE NEXT OBSERVATION
65 C READ IN MUST OF NECESSITY HAVE A LARGER JULIAN DAY NUMBER.
66 C TIM2 IS SET TO A LARGE NEGATIVE NUMBER (-1.0+30) TO INITIALIZE
67 C SUBROUTINE TIMCOR.
68 C
69 C KEY4 = -1
70 C IS = 0
71 C IYMD2 = 1000000
72 C IYMD = -1000000
73 C JDAY2 = -1000000
74 C IARC = -1000000
75 C TIM2 = -1.0+30
76 C NOLIST = 0
77 C
78 C SECATR IS THE CONVERSION CONSTANT FROM ARC-SECONDS TO RADIAN.
79 C SECTTR IS THE CONVERSION CONSTANT FROM HOUR-ANGLE SECONDS TO
80 C RADIAN.
81 C
82 C SECATR = .0174532925200/3600.00
83 C SECTTR = SECATR*15.00
84 C WRITE(3,1060)
85 C DO 10 NUMSTA = 1,30

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86 READ(5,1000) KSTA(NUMSTA),STNAM(NUMSTA),ISTA(NUMSTA),IEND
87 WRITE(3,1001) KSTA(NUMSTA),STNAM(NUMSTA),ISTA(NUMSTA)
88 JSTA(NUMSTA) = ISTA(NUMSTA) - (ISTA(NUMSTA)/10000) * 10000
89 NUM(NUMSTA) = 0
90 IF (IEND.LT.0) GO TO 15
91 10 CONTINUE
92 C NUMBER OF STATIONS EXCEEDS 30
93 WRITE(6,2000)
94 GO TO 700
95 C
96 15 WRITE(3,1070)
97 20 CONTINUE
98 READ(5,1010,END=600) NARC,IYMDB,IHB,IMB,SECB,IYMDE,IHE,IME,SECE
99 WRITE(3,1011) NARC,IYMCB,IHB,IMB,SECB,IYMDE,IHE,IME,SECE
100 BTIME = 3600*IHB + 60*IMB + SECB
101 ETIME = 3600*IHE + 60*IME + SECE
102 C
103 C KEY 4 IS INITIALLY NEGATIVE. IT IS SET EQUAL TO 1 AFTER THE FIRST
104 CALL TO SUBROUTINE DATAWT.
105 C
106 C
107 C IF (IARC.EQ.NARC) GO TO 100
108 C
109 C A NEW ARC HAS COMMENCED. IF DATA HAS BEEN ACCUMULATED FOR THE PRE-
110 VIOUS ARC, BUT NOT YET OUTPUT (IS>0), THEN IT IS OUTPUT NOW.
111 C
112 K = IS
113 IF (K.GT.0) CALL DATAWT
114 IARC = NARC
115 C IF A NEW ARC HAS BEEN STARTED SET KEY4 TO 2 IN ORDER THAT
116 SUBROUTINE DATAWT SHOULD PUNCH A '2' IN KEY4 OF THE NEXT NAP '999'
117 CARD
118 C
119 IF (KEY4.GE.0) KEY4 = 2
120 C
121 C NOLIST IS THE NUMBER OF NONLISTED STATIONS FOR THE ARC.
122 NUMSTA IS THE NUMBER OF LISTED STATIONS (CONSTANT FOR THIS RUN).
123 C
124 IF (NCLIST.GT.0) WRITE(6,2020) (NONAME(I),NOSTA(I),I=1,NOLIST)
125 NOLIST = 0
126 DO 40 I = 1,NUMSTA
127 NPASS(I) = 0
128 40 CONTINUE
129 WRITE(12,3000) IARC

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130 C
131 C READ DATA TAPE TILL THE TIME OF OBSERVATION IS PASSED THE START
132 C TIME FOR THE ARC, THEN GO TO 200. (IYMD IS INITIALIZED TO A
133 C LARGE NEGATIVE NUMBER.)
134 C
135 C 100 CONTINUE
136 C IF (IYMD-IYMDB)110,120,200
137 C 110 READ(1,1020,END=110) A,NSIA,IYMD,IH,IM,SEC,NHR,MIN,RSEC,NSIGN,
138 C INDEG,NMIN,DSEC,NRED
139 C GO TO 100
140 C 120 TIME = IH*3600 + IM*60 + SEC
141 C IF (TIME.LT.BTIME) GO TO 110
142 C
143 C 200 CONTINUE
144 C IF THE TIME OF OBSERVATION IS PASSED THE END TIME FOR THE ARC GO
145 C TO 20, OTHERWISE PROCEED TO 220.
146 C
147 C IF (IYMD-IYME) 220,210,20
148 C 210 IF (TIME.GT.EIME) GO TO 20
149 C
150 C 220 CONTINUE
151 C
152 C IYMD2 IS THE CURRENT (YEAR,MONTH,DAY). IT IS INITIALIZED TO A LARGE
153 C POSITIVE NUMBER.
154 C
155 C TIME = TIME + DELT
156 C IF (IYMD.EQ.IYMD2) GO TO 270
157 C IF (IS.LE.0) GO TO 260
158 C
159 C NORCEK IS AN ARRAY OF STATION NUMBERS FOR WHICH OBSERVATIONS HAVE
160 C BEEN ACCUMULATED. THE STATIONS HAVE BEEN ARRANGED IN A SEQUENCE
161 C SUCH THAT IF I<J THEN THE TIME OF THE FIRST ACCUMULATED (BUT NOT
162 C YET OUTPUT) OBSERVATION FOR STATION NORDER(I) PRECEDES THAT FOR
163 C STATION NORDER(J).
164 C
165 C JDAY1 IS THE JULIAN DAY PRECEDING THE CURRENT ONE (JDAY2). JDAY(L)
166 C IS THE JULIAN DAY OF THE FIRST OBSERVATION OF STATION NUMBER L.
167 C
168 C DO 230 K = 1,IS
169 C L = NORDER(K)
170 C IF (JDAY(L).GT.JDAY1) GO TO 240
171 C 230 CONTINUE
172 C K = IS
173 C GO TO 250

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240 K = K - 1
C
C K IS THE NUMBER OF OBSERVATIONS IN ARRAY NORDEK FOR WHICH THE DAY
C OF THE FIRST OBSERVATION PRECEDES THE CURRENT DAY, WHICH HAS JUST
C COME TO AN END. THE OBSERVATIONS FOR THOSE STATIONS ARE OUTPUT.
C
250 IF (K.GT.0) CALL DATANT
260 CONTINUE
    JDAY1 = JDAY2
    IYR1 = IYR2
    IMO1 = IMO2
    IDA1 = IDA2
    IYMU2 = IYMD
    IYR2 = IYMD/10000
    IMO2 = IYMD/100 - 100*IYR2
    IDA2 = IYMD - 10000*IYR2 - 100*IMO2
C COMPUTE JULIAN DAY NUMBER
    LEAPYR = 49
    IF (IMO2.GT.2) LEAPYR = 48
    JDAY2 = (IYR2 - 50)*365 + (IYR2 - LEAPYR)/4 + MONTH(IMO2) + IDA2
C
270 CONTINUE
    DO 280 I = 1, NUMSTA
    IF (NSTA.EQ. I) GO TO 290
280 CONTINUE
    IF (NCLIST.LE.0) GO TO 284
    DO 282 I = 1, NOLIST
    IF (NSTA.EQ. NONAME(I)) GO TO 286
282 CONTINUE
    IF (NCLIST.GE.30) GO TO 450
284 NOLIST = NOLIST + 1
    NSTA(NOLIST) = 1
    NUNAME(NOLIST) = NSTA
    GO TO 320
286 NOSTA(I) = NOSTA(I) + 1
    GO TO 320
C
290 RADRA = (NHR*3600 + MIN*60 + RSEC)*SECTTR
    RADDEC = (NDEG*3600 + NMIN*60 + DSEC)*SECATR
    IF (NSIGN.EQ. MINUS) RADDEC = -RADDEC
C
300 CONTINUE
    N = NUM(I) + 1
    IF (N.GT.1) GO TO 340

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C FIRST POINT IN STATION-OBSERVATION ARRAY 218
JDAYA(I) = JDAY2 219
IS = IS + 1 220
NORDER(IS) = I 221
222
310 CONTINUE 223
IF (N.LE.NMAX) GO TO 315 224
WRITE(6,2030) SINAM(I), ISTA(I) 225
GO TO 700 226
227
C 315 CONTINUE 228
TIM(N,I) = TIME 229
RA(N,I) = RADRA 230
DEC(N,I) = RADDEC 231
NUM(I) = N 232
C 320 READ(1,1020,END=320) A,NSTA,IYMD,IH,IM,SEC,NHR,MIN,RSEC,NSIGN, 233
INDEG,NMIN,DSEC,NREQ 234
TIME = IH*3600 + IM*60 + SEC 235
GO TO 200 236
237
C 340 CONTINUE 238
TIMDIF = (JDAY2 - JDAYA(I))*86400 + TIME - TIM(I,I) 239
IF (TIMDIF.LT.TORBT) GO TO 310 240
DO 350 K = 1,IS 241
IF (NORDER(K).EQ.I) GO TO 360 242
350 CONTINUE 243
360 CALL DATAWT 244
GO TO 300 245
246
C 450 CONTINUE 247
WRITE(6,2010) NONAME,NSTA 248
GO TO 700 249
600 K = IS 250
IF (K.GT.0) CALL DATAWT 251
KEY4 = 3 252
CALL DATAWT 253
IF(NOLIST.GT.0)WRITE(6,2020) (NONAME(I),NSTA(I),I=1,NOLIST) 254
WRITE(12,1050) 255
700 CONTINUE 256
REWIND 1 257
END FILE 2 258
REWIND 2 259
STOP 260
1000 FORMAT (I5,5X,A8,2X,2I5) 261

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1001 FORMAT(11X, I5, 15X, A8, 12X, I5) 262
1010 FORMAT(15, 5X, 16, 2I3, D10.0, 16, 2I3, D10.0) 263
1011 FORMAT(7X, I5, 4X, 2(8X, 2I6, 13, F9.5)) 264
1020 FORMAT(13A1, I5, 16, 2I2, F6.4, I3, I2, F5.3, A1, 2I2, F4.2, I6) 265
1050 FORMAT(15X, // 'JOB CCMPLETED') 266
1060 FORMAT(3(12X, 'STATION')/10X, 'NUMBER(NAP)', 11X, 'NAME', 16X, 'ID'//) 267
1070 FORMAT(//10X, 'ARC', 19X, 'START', 28X, 'STOP'/9X, 'NUMBER', 2(10X, 'DATE' 268
1, 5X, 'HR MN SECONDS'))
1080 FORMAT(80A1) 269
2000 FORMAT(15X, 'NUMBER OF STATIONS EXCEEDS 30') 270
2010 FORMAT('1', 15X, 'THE FOLLOWING STATION NUMBERS ARE NOT IN THE TABLE 271
*'//3(//10(5X, I5))//5X, I5//15X, 'JOB ABORTED')
2020 FORMAT('1', 15X, 'THE FOLLOWING STATION NUMBERS WERE NOT IN THE TABL 272
*'//15X, 'STATION NUMBER', 20X, 'NUMBER OF OBSERVATIONS', /30(18X, I5, 27
*X, I5//)
2030 FORMAT(15X, A8, '-', 15, 5X, 'NUMBER OF DATA POINTS EXCEEDS 49') 277
3000 FORMAT(//20X, 'DATA SUMMARY FOR ARC NUMBER', I5//14X, 'STATION', 6X, 278
*'DATE', 7X, 'GMT', 9X, 'PASS', 5X, 'NUMBER OF DATA', /12X, 'ID', 4X, 'NAME', 93 279
*X, 'YR MO DA', 3X, 'HR MN SEC', 6X, 'NO.', 4X, 'POINTS FOR ORBIT'//) 280
END
SUBROUTINE DATAWT 281
IMPLICIT REAL*8 (A-H, O-Z) 282
COMMON/W/ TIM(49, 30), RA(49, 30), DEC(49, 30), STNAM(30), TPASS, 283
IJDAYA(30), NUM(30), NCRDER(30), IYR1, IYR2, IMO1, IDA1, IDA2, JDAY1, 284
IJDAY2, IARC, IARCS, ISTA(30), JSIA(30), NPASS(30), KSTA(30), IT, K, IS 285
COMMON /SAO/ M, N 286
DATA I1, I201, I202, I999/1, 201, 202, 999/ 287
C IT = -1 ON FIRST ENTRY, IT = 1 SUBSEQUENTLY, IT = 3 ON LAST ENTRY 288
C 289
IF (IT.GE.3) GO TO 200 290
DO 100 I = 1, K 291
IF (IT.LT.0) GO TO 10 292
WRITE (7, 1000) I999, SNAME, IARCS, NSTAS, NPASS, IT 293
10 CONTINUE 294
IT = 1 295
IARCS = IARC 296
M = NORDER(I) 297
SNAME = STNAM(M) 298
NSTAS = KSTA(M) 299
NSTI2 = ISTA(M) 300
NSTA = JSTA(M) 301
WRITE (6, 1010) I1, SNAME, ISTA(M), IARC 302
WRITE (6, 1020) 303
N = NUM(M) 304
305

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306 NUM(M) = 0
307 IF((JSTA(M)+20000).EQ.NST12) CALL SAOCOR
308 DO 90 J = 1,N
309 TIMP = TIM(J,M)
310 IF (J.LE.1) GO TO 50
311 TIMDIF = TIMP - TIM(J-1,M)
312 IF (TIMDIF.GT.TPASS) GO TO 40
313 IF (TIMDIF.GE.0.00) GO TO 20
314 IF TIMDIF IS NEGATIVE THEN THE LAST OBSERVATION HAS BEEN MADE ON
315 THE DAY FOLLOWING THE PREVIOUS OBSERVATION
316 IF((TIMDIF + 86400.DO).GT.TPASS) GO TO 40
317 UPDATE DATE TO NEXT DAY WHICH MUST BE DAY 2
318 IYRM = IYR2
319 IMOM = IMO2
320 IDAM = IDA2
321 DDAYM = JDAY2
322
323 20 CONTINUE
324 DELTRA = RA(J,M) - RA(J-1,M)
325 DELDEC = DEC(J,M) - DEC(J-1,M)
326
327 30 CONTINUE
328 IHP = TIMP/3600.DO
329 IMP = TIMP/60.DO - 60*IHP
330 SECP = TIMP - 3600*IHP - 60*IMP
331 GO TO 80
332 40 S = SECP + 0.01D0
333 WRITE(7,1001) I202,SNAME,IARC,NSTAS,NPASS(M),IYRM,IMOM,IDAM,IHP,
334 IIMP,S
335 WRITE(7,1000) I999,SNAME,IARC,NSTAS,NPASS(M),IT
336 WRITE (12,1040) NST12,SNAME,IYRM,IMOM,IDAM,IHP,IMP,SECP,NPASS(M)
337 IF (TIMDIF.LT.0.00) GO TO 60
338 GO TO 70
339 50 CONTINUE
340 IF (JDAYA(M).GT.JDAY1) GO TO 60
341 IYRM = IYR1
342 IMOM = IMO1
343 IDAM = IDA1
344 DDAYM = JDAY1
345 GO TO 70
346 60 IYRM = IYR2
347 IMOM = IMO2
348 IDAM = IDA2
349 DDAYM = JDAY2
350 70 CONTINUE
351 DELTRA = 0.00

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350 DELDFC = 0.00
351 IHP = TIMP/3600.00
352 IMP = TIMP/60.00 - 60*IHP
353 SECP = TIMP - 3600*IHP - 60*IMP
354 S = SECP - 0.0100
355 NPASS(M) = NPASS(M) + 1
356 WRITE (7,1001) I201,SNAME,IARC,NSTAS,NPASS(M),IYRM,IMOM,IDAM,IHP,
357 IIMP,S
358
359 80 CONTINUE
360 WRITE (6,1030) IYRM,IMOM,IDAM,IHP,IMP,SECP,NPASS(M),RA(J,M),
361 IDELTRA,DEC(J,M),DELDEC
362 WRITE(2) NSTA,DDAYM,TIMP,RA(J,M),DEC(J,M)
363
364 90 CONTINUE
365 S = SECP + 0.0100
366 WRITE(7,1001)I202,SNAME,IARC,NSTAS,NPASS(M),IYRM,IMOM,IDAM,IHP,
367 IIMP,S
368 NPASS = NPASS(M)
369 WRITE (12,1040) NST12,SNAME,IYRM,IMOM,IDAM,IHP,IMP,SECP,NPASS(M),N
370
371 100 CONTINUE
372 IS = IS - K
373 IF(IS.LE.0) GO TO 130
374 DO 120 I = 1,IS
375 NORDER(I) = NORDER(I + K)
376
377 120 CONTINUE
378 130 CONTINUE
379 RETURN
380 WRITE(7,1000)I999,SNAME,IARCS,NSTAS,NPASSS,IT
381 RETURN
382 1000 FORMAT (I3,2X,A8,4I3)
383 1001 FORMAT (I3,2X,A8,3I3,6X,5I3,F15.3)
384 1010 FORMAT(I1,9X,A8, - ,I5,15X,ARC NUMBER',I8//)
385 1020 FORMAT(4X,DATE',7X,GMT',9X,PASS',3X,RIGHT ASCENSION',4X,DELTA
386 1 RA',9X,DECLINATION',8X,DELTA DEC/2X,YR MO DA',2X,HR MN SEC '
387 1,5X,NO.,5X,(RADIANS)',8X,(RADIANS)',9X,(RADIANS)',9X,(RADIAN
388 IS)')/
389
390 1030 FORMAT(X,3I3,I4,I3,F8.4,I4,4(3X,F15.10))
391 1040 FORMAT(10X,15,X,A8,3I3,15,I3,F4.0,I8,8X,I5)
392 END
393 SUBROUTINE TIMCOR
394 IMPLICIT REAL*8(A-H,O-Z)
395 COMMON/T/ TIM,COR,STHETA,CTHETA,ZETA,Z
396 COMMON/M/ TIM2
397 DIMENSION MONTH(12)
398 DATA MONTH/-1,30,58,89,119,150,180,211,242,272,303,333/

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394 DATA TIM2IN /-1.0+30/
395 5 TIMDIF = TIM - TIM2
396 IF (TIMDIF.LE.0.00) GO TO 15
397 10 COR1 = COR2
398 TIM1 = TIM2
399 IYR1 = IYR2
400 IMO1 = IMO2
401 IDA1 = IDA2
402 READ (4,30,END=20) IYR2,IMO2,IDA2,COR2
403 WRITE (3,60) IYR2,IMO2,IDA2,COR2
404 LEAPYR = 49
405 IF (IMO2.GT.2) LEAPYR = 48
406 TIM2 = (IYR2 - 50)*365 + (IYR2 - LEAPYR)/4 + MONTH(IMO2) + IDA2
407 IF (TIM1.LE.TIM2IN) GO TO 10
408 F = (COR2 - COR1)/(TIM2 - TIM1)
409 GO TO 5
410 15 COR = COR2 + F*TIMDIF
411 RETURN
412 20 WRITE (6,50)
413 STOP
414 30 FORMAT (3I2,4X,F10.5)
415 50 FORMAT (X,END OF DATA SET 4,(TIME CORRECTIONS),JOB ABORTED.9)
416 60 FORMAT (90X,3I3,2X,'A.1 - UTC = ',F10.5)
417 END
418 SUBROUTINE PRENUT
419 C
420 C IMPLICIT REAL*8(C-H,O-Z)
421 C
422 COMMON/T/ DAYS,COR,SHP,CHP,UP,ZP
423 DIMENSION A(23),AS(30),ADP(30),ADE(30),ADELE(23),ADELP(23)
424 C
425 C
426 DATA ADELE/0.,0.,-2.,2.,2.,-2.,3.,3.,0.,5.,7.,8.,0.,0.,0.,-24.,-66
427 *,0.,0.,0.,0.,0.,0./
428 C
429 DATA ADELP/-2.,-3.,3.,-3.,-4.,4.,-5.,-5.,10.,-10.,-15.,-15.,16.,-2
430 *,1.,45.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0./
431 C
432 C
433 DATA ADE/-3.,3.,3.,-2.,3.,3.,3.,0.,0.,-3.,0.,0.,5.,7.,-7.,-10.,0.,11.,-1
434 *,1.,0.,14.,23.,22.,30.,-31.,0.,-50.,0.,0.,183.,0.,0.,0./
435 C
436 DATA ADP/5.,-5.,-5.,6.,-6.,-6.,-6.,6.,6.,7.,-7.,-9.,-13.,14.,19.,25.,
437 *-26.,26.,28.,-32.,-44.,-52.,-57.,58.,60.,114.,-149.,-261.,0.,0.,0.,0.

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*/		438
C	DATA STRAD,DPLUS/.4848136811D-5,18262.5D0/	439
	DATA ADR/57.2957795/	440
C		441
C		442
	DD = DPLUS + DAYS	443
	TD = DD/36525.D0	444
	AT = TD	445
	ADD = DD/1000.D0	446
	ADD2 = ADD * ADD	447
	ELD = 13.0649924465D0*DD + 296.104608D0	448
	CALL PRINCP(ELD,AL)	449
	ELPD = .985600269D0*DD + 358.475833D0	450
	CALL PRINCP(ELPD,ALP)	451
	EFD = 13.2293504490D0*DC + 11.250889D0	452
	CALL PRINCP(EFD,AF)	453
	DED = 12.1907491914C0*DC + 350.737486D0	454
	CALL PRINCP(DED,AD)	455
	OMEGU = .0529539222C0*DC - 259.183275D0	456
	CALL PRINCP(OMEGD,AMEG)	457
	AL = (AL + (.0006890 + .000000295*ADD) * ADD2)/ADR	458
	ALP = (ALP - (.0000112 + .000000068 * ADD) * ADD) * ADD2)/ADR	459
	AF = (AF - (.0002407 + .000000007 * ADD) * ADD) * ADD2)/ADR	460
	AD = (AD - (.0001076 - .000000039 * ADD) * ADD) * ADD2)/ADR	461
	AMEG = (.0001557 + .000000046 * ADD) * ADD2 - AMEG)/ADR	462
	A(23) = AMEG	463
	A(21) = AMEG + AMEG	464
	A(9) = 2. * (AL - AF)	465
	A(16) = AMEG - A(9)	466
	A(5) = 2. * (AF - ALP - AD) + AMEG	467
	A(4) = A(16) + AMEG	468
	A(1) = AL - ALP - AD	469
	A(22) = 2. * (AF-AD+AMEG)	470
	A(20) = ALP	471
	A(19) = ALP + A(22)	472
	A(18) = A(22) - ALP	473
	A(17) = A(22) - AMEG	474
	A(15) = 2. * (AL-AD)	475
	A(14) = 2. * (AF-AD)	476
	A(13) = ALP + ALP	477
	A(12) = ALP + AMEG	478
	A(11) = A(12) + A(12) + A(14)	479
	A(10) = AMEG - ALP	480
		481

A(8) = AMEG - A(15) 482
 A(7) = A(10) + A(14) 483
 A(6) = A(15) + AMEG 484
 A(3) = A(12) + A(14) 485
 A(2) = AL - AD 486
 AS(30) = 2 * (AF + AMEG) 487
 AS(29) = AL 488
 AS(28) = AS(30) - AMEG 489
 AS(27) = AS(30) + AL 490
 AS(26) = AL - AD - AD 491
 AS(25) = AS(30) - AL 492
 AS(24) = AD + AD 493
 AS(23) = AL + AMEG 494
 AS(22) = AMEG - AL 495
 AS(21) = AS(24) + AS(25) 496
 AS(20) = AS(27) - AMEG 497
 AS(19) = AS(30) + AS(24) 498
 AS(18) = AL + AL 499
 AS(17) = AS(27) - AS(24) 500
 AS(16) = AS(30) + AS(18) 501
 AS(15) = AF + AF 502
 AS(14) = AS(22) + AS(15) 503
 AS(13) = AS(22) + AS(24) 504
 AS(12) = AS(23) - AS(24) 505
 AS(11) = AS(14) + AS(24) 506
 AS(10) = AS(26) + ALP 507
 AS(9) = AS(30) + ALP 508
 AS(8) = AL + AS(24) 509
 AS(7) = AMEG + AS(24) 510
 AS(6) = AS(30) - ALP 511
 AS(5) = AS(30) + AS(8) 512
 AS(4) = AS(17) + AL 513
 AS(3) = AMEG - AS(24) 514
 AS(2) = AS(19) - AMEG 515
 AS(1) = AS(17) - AMEG 516
 ASS16 = AD 517
 ASS15 = AS(10) - AL 518
 ASS14 = AL - ALP 519
 ASS13 = AL - AF - AF 520
 ASS12 = AS(16) - AMEG 521
 ASS11 = AL + AF + AF 522
 ASS10 = AL + ALP 523
 ASS9 = AS(30) + ASS14 524
 ASS8 = AMEG - AL - AL 525

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526 ASS7 = AS(14) - AD - AD
527 ASS6 = AL + AL + AMEG
528 ASS5 = AS(25) - ASS15
529 ASS4 = ASS5 + AL
530 ASS3 = AL + AMEG + AMEG
531 ASS2 = AS(27) + ALP
532 ASS1 = AS(27) + AL + AL
533 ADEL(23) = -172327. - 173.7*AT
534 ADEL(21) = 2088. + 0.2 * AT
535 ADEL(22) = - 12729. - 1.3 * AT
536 ADEL(20) = 1261. - 3.1 * AT
537 ADEL(19) = -497. + 1.2 * AT
538 ADEL(18) = 214. - 0.5 * AT
539 ADEL(17) = 124. + 0.1 * AT
540 ADEL(13) = 16. - 0.1 * AT
541 ADEL(11) = -15. + 0.1 * AT
542 ACELE(23) = 92100. + 9.1 * AT
543 ADELE(21) = - 904. + 0.4 * AT
544 ACELE(22) = 5522. - 2.9 * AT
545 ADELE(19) = 216. - 0.6 * AT
546 ADELE(18) = -93. + 0.3 * AT
547 ADP(20) = -2037. - 0.2 * AT
548 ADP(29) = 675. + 0.1 * AT
549 ADP(28) = -342. - 0.4 * AT
550 ADE(30) = 884. - 0.5 * AT
551 ADE(27) = 113. - 0.1 * AT
552 BDELE = 0.
553 BDEL(1) = 0.
554 DO 100 I = 1,23
555 BDELE = BDELE + ADELE(I) * COS(A(I))
556 BDEL(1) = BDEL(1) + ADEL(I) * SIN(A(I))
557 100 CONTINUE
558 BDE = 2. * COS(ASS12)
559 BDP = 2. * (-SIN(ASS1) + SIN(ASS2) - SIN(ASS3) - SIN(ASS4) - SIN(ASS5)
1 + SIN(ASS6) - SIN(ASS7) - SIN(ASS8)
2 3. * (-SIN(ASS9) - SIN(ASS10) + SIN(ASS11)) +
3 4. * (-SIN(ASS12) + SIN(ASS13) + SIN(ASS14) - SIN(ASS15) - SIN(ASS16))
DO 200 I = 1,30
563 BDE = BDE + ADE(I) * COS(AS(I))
564 BDP = BDP + ADP(I) * SIN(AS(I))
565 200 CONTINUE
566 DELTAE = (BDE + BDELE)/36000000.
567 BDTAP = (BDP + BDEL)/10000.
568 EPSC=23.4522944DO - TD*(0.0130125DO + TD*(0.00000164DO -
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1TD*0.00000050300)) + DELTAE
T50 = DAYS/36525.00
TDRAD = T50 * STRAD
C
C
C
U = ZETA, H = THETA, UAZ = ZETA + Z
U = TORAD*(2304.997DC + T50*(.30200 + T50*.017900))
Z = TORAD*(2304.997DC + T50*(1.09300 + T50*.019200))
H = TDRAD*(2004.298DC - T50*(.042600 + T50*.041600))
XPSI = BDTAP*STRAD
XEPS = DELTAE/ADR
EPSC = EPSD/ADR
CZ = DCOS(Z)
SZ = DSIN(Z)
SH = DSIN(H)
CH = DCOS(H)
CEPSD = DCOS(EPSD)
SEPSD = DSIN(EPSD)
EPSO = EPSD - XEPS
CEPSO = DCOS(EPSD)
SEPSO = DSIN(EPSD)
SXPSI = DSIN(XPSI)
CXPSI = DCOS(XPSI)
SUI = SEPSO*CEPSD - CEPSO*SEPSD*CXPSI
CUI = SEPSD*SXPSI
SZI = SEPSD*CEPSO - CEPSD*SEPSO*CXPSI
CZI = SEPSO*SXPSI
CHI = CEPSD*CEPSO + SEPSD*SEPSO*CXPSI
ZI = DATAN2(SZI,CZI)
CUAZ = CZ * CUI - SZ*SUI
CHP = CH*CHI - SH*CUAZ
CUPMU = SH*CHI + CH*CUAZ
SUPMU = CZ*SUI + SZ*CUI
UPMU = DATAN2(SUPMU,CUPMU)
UP = U + UPMU
CUPLU = DCOS(UPMU)
SUPLU = DSIN(UPMU)
SHP = CUPMU*CUPLU + SUPMU*SUPLU
CZPMZ = CH*SHP - SH*CHP*CUPLU
SZPMZ = SH * SUPLU
ZP = ZI + DATAN2(SZPMZ,CZPMZ)
RETURN
END
SUBROUTINE PRINCP(XCOURL,X)

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REAL*8 XDOUBL,XT
I = XDOUBL
XT = ((I + 180)/360)*36C
XDOUBL = XDOUBL - XT
X = XDOUBL
RETURN
END
SUBROUTINE SAOCOR
IMPLICIT REAL*8 (A-H,G-Z)
COMMON/W/ TIM(49,30),RA(49,30),DEC(49,30),STNAM(30),TPASS,
1JDAYA(30),NUM(30),NCRDER(30),IYR1,IYR2,IM01,IM02,IDA1,IDA2,JDAY1,
1JDAY2,IARC,IARCS,ISTA(30),JSTA(30),NPASS(30),KSTA(30),KEY4,K,IS
COMMON/SAO/ M,N
COMMON/T/ DAYS,COR,STHETA,CTHETA,ZETA,Z
DATA PI,TWOPI/3.141592653589793,6.283185307179586/
DAYS = JDAYA(M) + TIM(1,M)/86400.DO
CALL PRENUT
CALL TIMCOR
DO 500 I = 1,N
UARO = ZETA + RA(I,M)
CDECO = DCOS(DEC(I,M))
SDECO = DSIN(DEC(I,M))
SRMZ = CDECO * DSIN(UARC)
DUM = CDECO * DCOS(UARO)
CRMZ = CTHETA*DUM - STHETA*SDECO
SDEC = CTHETA*SDECO + STHETA*DUM
RMZ = DATAN2(SRMZ,CRMZ)
CDEC = SRMZ * DSIN(RMZ) + CRMZ*DCOS(RMZ)
DECF = DATAN2(SDEC,CDEC)
AF = RMZ + Z
IF (DECF.GT.PI) DECF = DECF - TWOPI
IF (AF.GE.TWOPI) AF = AF - TWOPI
RA(I,M) = AF
DEC(I,M) = DECF
TIM(I,M) = TIM(I,M) - CCR
THIS IS A TEMPORARY CHANGE TO FIX ERROR IN SAO TIME
ITIME=TIM(I,M)
TIM(I,M)=ITIME
500 CONTINUE
RETURN
END

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//Z7GEMOPB JOB (G70041150A,T,000138,H00H00),69,MSGLEVEL=1
// EXEC  LOADER,PARM='MAP,CALL,SIZE=150K',REGION.GO=160K
//GO.FT06F001 DD SYSOUT=A,SPACE=(CYL,(8,2))
//GO.FT07F001 DD SYSOUT=B,DSN=DECK
//GO.SYSLIN  DD UNIT=2400-9,LABEL=(5,BLP),DISP=(NEW,KEEP),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200),VOL=SER=33599C
//GO.FT01F001 DD UNIT=2400-9,LABEL=(3,BLP),DISP=(OLD,DELETE),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200,DEN=2),VOL=SER=3826F
//GO.FT02F001 DD DUMMY
//GO.FT03F001 DD SYSOUT=A,SPACE=(CYL,(2,2))
//GO.FT12F001 DD SYSOUT=A,SPACE=(CYL,(2,2))
//GO.SYSABEND DD SYSOUT=A,SPACE=(CYL,(1))
//GO.DATAS DD *

```

9	ORGAN	29001
19	SPAIN	29004
10	JUPTR	29010
50	COLDLK	29424
11	EDWAFB	29425
3	BPOIN	31021
1	FTMYR	31022
47	OMER	31024
48	SATAG	31028
2	MOJAV	31030
68	NEWFL	31032
52	COLEG	31033
4	GFORK	31034
25	ROSMa	31042
6	EDINB	37036
5	COLBA	37037
14	BERMD	37039
16	PURIO	37040
7	GSFCP	37043
26	DENVR	37045
32	JUP24	37071
40	JUP40	37072
53	JUPTH	37073
33	JBC4L	37074
2	660108	0 0

/*

//GO.FT04F001 DD *

651225 4.3395

661225 4.3576

/*

-1

660115 0 0

A-2.6 PRENAP CARD UPDATER PROGRAM
AND SAMPLE JCL

C UPDATER ROUTINE FOR NAP-2 INPUT CARDS.

IMPLICIT REAL*8 (A-H,O-Z)

LOGICAL*1 A,B,BLANK

DIMENSION A(80),B(80),M(80),KAT(2),KEY(10),DATA(2)

EQUIVALENCE (B(1),BETA)

DATA INS,REP,DEL,MCD/,INS , ,REP , ,DEL , ,MOD , /

DATA BLANKS,BLANK/ , , /

INTEGER*4 ALPHA,INS,REP,DEL

1000 FORMAT (A4,X,I5,5X,I5)

1001 FORMAT (10X,A4,X,I5,5X,I5)

1010 FORMAT (10X,'UPDATE ERRCR ',A4)

2020 FORMAT (I3,I2,A8,10I3,D22.15,D15.8)

2010 FORMAT (80A1)

2011 FORMAT (10X,80A1)

WRITE (6,3000)

WRITE (6,3010)

3000 FORMAT (I1,30X,'PRCGRAM TO UPDATE NAP INPUT CARDS STORED ON TAPE'

*//3X,INS I1,9X,'INSERTS CARDS AFTER SEQUENCE NUMBER I1./3X,'D

*EL I1 I2 DELETES CARDS BETWEEN (AND INCLUDING) SEQUENCE NUMB

*ERS I1 AND I2./3X,'REP I1 I2 DELETES CARDS BETWEEN (AND INC

*LUDING) SEQUENCE NUMBERS I1 AND I2,AND THEN INSERTS CARDS./3X,'MO

*D I1 I2 MODIFIES CARDS BETWEEN (AND INCLUDING) SEQUENCE NUMB

*ERS I1 AND I2.///)

3010 FORMAT (22X,'FORMAT FOR ABOVE FOUR CARDS (A4,X,I5,5X,I5) NOTE THA

*T INS ,DEL ,REP , AND MCD START IN'/17X,'COLUMN 1 AND THAT COLUMN

* 4 SHOULD BE BLANK.///22X,'INS AND REP MUST BE FOLLOWED BY THE CAR

*DS TO BE INSERTED. THE CARDS MUST'/17X,'BE FOLLOWED BY A BLANK CA

*RD TO SIGNIFY THE END OF THE PARTICULAR SET OF INSERTED CARDS.///2

*2X,'THE MOD CARDS MUST BE FOLLOWED BY A MODIFYING CARD. COLUMNS N

*OT TO BE MODIFIED'/17X,'SHOULD BE LEFT BLANK.///1X, '*****

I=0

10 READ (5,1000,END = 100) ALPHA, I1,I2

WRITE (6,1001) ALPHA,I1,I2

IF (ALPHA.EQ.INS) GC TO 20

IF (ALPHA.EQ.REP) GC TO 30

IF (ALPHA.EQ.DEL) GC TO 30

IF (ALPHA.EQ.MOD) GO TO 30

WRITE (6,1010) ALPHA

STOP

20 IF (I.GE.I1) GO TO 40

READ(9,END=200) KAT,XLABL,KEY,DATA,I

WRITE (12,2020) KAT, XLABL,KEY,DATA


```

GO IC 20
30 I1=I1-1
GO TO 20
40 IF (ALPHA.EQ.DEL) GC TO 70
IF (ALPHA.EQ.MOD) GC TO 300
50 READ (5,2010) B
WRITE (6,2011) B
IF (BETA.EQ.BLANKS) GO TO 60
WRITE (12,2010) B
GO TO 50
60 IF (ALPHA.EQ.INS) GC TO 10
70 IF (I.GE.I2) GO TO 10
REAC(9,END=200) KAT,XLABL,KEY,DATA,I
GO TO 70
100 READ (9,END=200) KAT,XLABL,KEY,DATA,I
WRITE(12,2020) KAT,XLABL,KEY,DATA
GO TO 100
200 STOP
300 READ (5,2010) B
WRITE(6,2011) B
L=0
DO 310 J=1,80
IF(B(I).EQ.BLANK) GO TO 310
L=L+1
M(L)=J
310 CONTINUE
320 CONTINUE
IF(I.GE.I2) GO TO IC
REWIND 10
REAC (9,END=200) KAT,XLABL,KEY,DATA,I
WRITE (10,2020) KAT,XLABL,KEY,DATA
REWIND 10
REAC (10,2010) A
DO 330 K=1,L
J=M(K)
330 A(J)=B(J)
WRITE(12,2010) A
GO TO 320
END

```

```
// EXEC LOADER, PARM=MAP,CALL,SIZE=100K,REGION.GO=L1OK
//GO.SYSLIN DD *
```

```
***** PRENAP CARD UPDATER OBJECT DECK IS INSERTED HERE *****
```

```
/*
//GO.FT09F001 DD UNIT=9TRACK,LABEL=(3,BLP),DSN=ITAPEGEM,
// DCB=(RECFM=VBS,LRECL=80,BLKSIZE=3204),DISP=(OLD,PASS),
// VOL=SER=5630
//GO.FT10F001 DD UNIT=DISK,SPACE=(TRK,(1,1)),
// DCB=(RECFM=VBS,LRECL=84,BLKSIZE=172),DISP=(NEW,DELETE)
//GO.FT12F001 DD UNIT=DISK,SPACE=(CYL,(3,2)),DSN=NAPOLEON,
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200),DISP=(NEW,PASS)
//GO.DATAS DD *
```

```
INS 12
959 OMQJAV6E 2 25 22 1 0 0 0 0 0 0.0 0.0
```

```
DEL 30 35
REP 36 40
999 OGFORK6E 2 27 21 1 0 0 0 0 0 0.0 0.0
201 OFMYR6E 2 1 22 0 0 66 1 34 0 0 0.51500000D 03 0.0
202 OFMYR6E 2 1 22 0 0 66 1 34 0 0 0.57780000D 03 0.0
701 IFTMEQL 1 1 6 3 1 0.10000000D 01 0.10000000D 16
701 IFTMEQM 2 1 7 4 1 0.10000000D 01 0.10000000D 16
```

```
MCC 50 55
0
```

A-2.7 POST NAP PROGRAM


```

C      KOUNT = 0
C      READ OPTION CARD FOR 701 CONTINUATION 1 CARDS
C      IF THE STANDARD DEVIATION OF A SET OF MEASUREMENTS FOR A PASS
C      (SDEVL AND SOCUM) EXCEEDS SOMAX OR IF THE MEAN MEASUREMENT ERROR
C      IN MINTRACK COUNTS EXCEEDS MAXERR THEN THE MEASUREMENT IS
C      EFFECTIVELY WEIGHTED OUT OF THE SOLUTION.
C      IOPT = -1,0,OR 1 IF IOPT = 1 THEN (UNLESS ACCORDING TO THE ABOVE
C      CRITERION THE MEASUREMENT HAS BEEN WEIGHTED OUT OF THE SOLUTION)
C      THE A PRIORI MEASUREMENT SIGMA FOR THE PASS IS GIVEN AS
C      10 TIMES THE OBSERVED STANDARD DEVIATION FOR THE PASS.
C      NOTE THAT SDEVL = 0.00 DOES NOT INDICATE THAT
C      THE STANDARD DEVIATION EQUALS ZERO, BUT RATHER THAT NO STANDARD
C      DEVIATION HAS BEEN COMPUTED FOR THIS NAP RUN. IF THAT IS THE
C      CASE, AND A 701, CONTINUATION 1, FOR THE L-MEASUREMENT WAS USED
C      IN THIS RUN THEN THAT CARD IS COPIED (UNLESS THE MEASUREMENT
C      HAS BEEN WEIGHTED OUT BECAUSE OF AN EXCESSIVE ERROR -SEE ABOVE)
C      HOWEVER, IF NO PREVIOUS CARD EXISTS AND IOPT IS NOT EQUAL TO ZERO
C      THEN THE MEASUREMENT IS EFFECTIVELY WEIGHTED OUT. THE SAME APPLIES
C      TO THE M-MEASUREMENTS.
C      FREQCY = 136.8300 (GEOS I)
C      = 136.3200 (GEOS II)
C
C      READ (5,1100) IOPT, MAXERR, SOMAX, FREQCY
C      WRITE(6,1101) IOPT,MAXERR,SDMAX,FREQCY
C
C      WRITE (31,1102)
C      I=0
C      2 READ(10) N,X,Y
C      IF(N.NE.601) GO TO 4
C      I=I+1
C      WRITE(12) N,X,Y
C      GO TO 2
C      4 REWIND 10
C      REWIND 12
C      DO 6 J=1,I
C      6 READ(10)
C
C      PLOB=136.00/(FREQCY*57.00)
C      PCNT=PLOB/1000.00
C      EMPLOB=136.00/(FREQCY*46.00)-PLOB
C      EMPCNT=EMPLOB/1000.00
C
C      READ NAP CONTROL CARDS

```

```

10 READ(27,1110,END=999) KAT,KONT,XLABL,KEY,DATA
   IF(KAT.EQ.601) CALL UP601
20 KOUNT=KOUNT+1
   WRITE(8) KAT,KONT,XLABL,KEY,DATA,KOUNT
   WRITE(6,1000) KOUNT,KAT,KONT,XLABL,KEY,DATA
   IF(KAT.NE.202) GO TO 10

```

```

C
C
C
PROCESS PASS

```

```

100 X701(1)=0.00
    X701(2)=0.00
    X704(1)=0.00
    X704(2)=0.00
    KSEVEN(1)=0
    KSEVEN(2)=0
    SL701=-1.00
    SM701=-1.00
    SL704=0.00
    SM704=0.00

```

```

C
C
C
C
XK=0 OR 1 AND CNT= PCNT OR ECNT DEPENDING ON WHETHER THE STATION
IS POLAR(EVEN) OR EQUATORIAL(ODD)

```

```

SEC=DATA(1)
IDAY=KEY(8)
NSTATN=KEY(2)
LF= NSTATN+30
XK=NSTATN-NSTATN/2*2
CNT=PCNT+EMPCNT*XK

```

```

C
READ(10) XLABLM,MN2,NUMPT1,NUMPT2,XLABLL,XMEANL,SDEVL,XMEANM,SDEVM
MN1=MN2-1
110 READ(27,1110,END=999) KAT,KONT,XLABL,KEY,DATA
   IF(KAT.EQ.999) GO TO 200

```

```

C
C
C
LM12 = 1 OR 2 ACCORDING AS KEY(1) IS ODD(L) OR EVEN(M)

```

```

LM12=2-KEY(1) + KEY(1)/2*2
IF(KAT.EQ.701) GO TO 130
IF(KAT.EQ.704) GO TO 140
120 KOUNT = KOUNT + 1

```

```

WRITE(8) KAT,KONT,XLABL,KEY,DATA,KOUNT
WRITE(6,1000) KOUNT,KAT,KONT,XLABL,KEY,DATA
GO TO 110

```

```

C
C
C 130 X701(LM12) = DATA(2)
    KSEVEN(LM12)=KEY(7)
    GO TO 110
C
C 140 X704(LM12) = DATA(1)
    GO TO 110
    999 CARD
C
C
C 200 ERRORL=(XMEANL-X704(1)+ABIAS(MN1))/CNT
    IF(ERRORL.LT.0.00) GO TO 210
    LERROR=ERRORL + 0.500
    LLOBE=- (LERROR + 500)/1000
    GO TO 220
    210 LERROR=ERRORL-0.500
        LLOBE= -(LERROR-500)/1000
    220 ERRORM=(XMEANM-X704(2)+ABIAS(MN2))/CNT
        IF(ERRORM.LT.0.00) GO TO 230
        MERROR=ERRORM + 0.500
        MLOBE=- (MERROR + 500)/1000
        GO TO 240
        230 MERROR = ERRORM -0.500
            MLOBE=- (MERROR-500)/1000
    240 IF(LLOBE.EQ.0) GO TO 250
        LERROR=LERROR + 1000*LLOBE
        SL704=1000*LLOBE
        SL704=SL704*CNT
        KOUNT=KOUNT + 1
        WRITE(8) K704,XLABLL,MN1,KEY704,SL704,BLANK,KOUNT
        WRITE(6,1000) KOUNT,K704,XLABLL,MN1,KEY704,SL704
    250 IF(MLOBE.EQ.0) GO TO 255
        MERROR=MERROR + 1000*MLOBE
        SM704=1000*MLOBE
        SM704=SM704*CNT
        KOUNT=KOUNT + 1
        WRITE (8) K704,XLABLM,MN2,KEY704,SM704,BLANK,KOUNT
        WRITE(6,1000) KOUNT,K704,XLABLM,MN2,KEY704,SM704
C
C
C 255 IF(SDEV.LE.0.00) GO TO 320

```

```
260 IF(IABS(LERROR).GT.MAXERR) GO TO 330
   IF(SDEVL.LE.0.00) GO TO 300
   IF(SDEVL.GT.SDMAX) GO TO 340
   IF(IOPT.LE.0) GO TO 355
   SL701= SDEVL*10.00
   KL701(5)=0
280 KOUNT=KOUNT + 1
   WRITE(8) K701,XLABLL,MN1,NSTATN,KL701,XI,SL701,KOUNT
   WRITE(6,1000) KOUNT,K701,XLABLL,MN1,NSTATN,KL701,XI,SL701
   GO TO 355
```

C

```
290 SL701=D15
295 KL701(5)=1
   GO TO 280
300 IF(X701(1).GT.0.00) GO TO 290
   IF(IOPT.NE.0) GO TO 290
   GO TO 355
320 IF(X701(1).GE.D15) GO TO 260
   SDEVL=X701(1)*I.D-1
   IF(KSEVEN(1).GT.0) SDEVL=SDEVL*1.D-6
   GO TO 260
330 IF(SDEVL.LE.0.00) GO TO 290
340 IF(IOPT.LE.0) GO TO 290
   SL701=SDEVL*1.D7
   GO TO 295
```

C

```
355 IF(SDEVM.LE.0.00) GO TO 420
360 IF(IABS(MERROR).GT.MAXERR) GO TO 430
   IF(SDEVM.LE.0.00) GO TO 400
   IF(SDEVM.GT.SDMAX) GO TO 440
   IF(IOPT.LE.0) GO TO 500
   SM701=SDEVM * 10.00
   KM701(5)= 0
380 KOUNT=KOUNT + 1
   WRITE(8)K701,XLABLM,MN2,NSTATN,KM701,XI,SM701,KOUNT
   WRITE (6,1000) KOUNT,K701,XLABLM,MN2,NSTATN,KM701,XI,SM701
   GO TO 500
390 SM701=D15
395 KM701(5)=1
   GO TO 380
400 IF(X701(2).GT.0.00) GO TO 390
   IF(IOPT.NE.0) GO TO 390
   GO TO 500
420 IF(X701(2).GE.D15) GO TO 360
```



```

SDEVM=X701(2)*1.D-1
IF(KSEVEN(2).GT.0) SDEVM=SDEVM*1.D-6
GO TO 360
430 IF(SDEVM.LE.0.D0) GO TO 390
440 IF(IOPT.LE.0) GO TO 390
SM701=SDEVM*1.D7
GO TO 395
C
500 LSD=SDEVL/CNT+0.500
MSD=SDEVM/CNT+0.500
WRITE(11) LF, IDAY, SEC, KEY(1), KEY(3), LERROR, MERROR, LLOBE, MLOBE,
* LSD, MSD, KL701(5), KM701(5), KSEVEN
GO TO 30
C
999 REWIND 11
READ(10, END=998)
998 CALL IWRITE
REWIND 8
997 READ(8, END=996) KAT, KONT, XLABL, KEY, DATA, KOUNT
WRITE(10) KAT, KONT, XLABL, KEY, DATA, KOUNT
GO TO 997
996 CONTINUE
WRITE(6, 1006)
STOP
1000 FORMAT(2I8, I2, A8, 10I3, D22.15, D22.8)
1100 FORMAT(2I5, 2D10.1)
1101 FORMAT(IX, IOPT=, I2, 5X, MAXERR=, I4, 5X, SDMAX=, D11.3, 5X, FREQCY=
*, F9.3////)
1102 FORMAT('1'///30X, 'B I A S V A L U E S'//
314X, 'STATION', 13X, 'PREPROCESSOR', 12X, 'NEW' /
412X, 'NAME NUMBER', 13X, 'BIAS', 16X, 'BIAS'//)
1006 FORMAT (///20X, 'PROCESS COMPLETE')
END
SUBROUTINE UP601
IMPLICIT REAL*8 (A-H, O-Z)
COMMON /U601/ PLOB, EMPLOB, ABIAS(60), XLABL, DATA(2), KAT, KONT,
*KEY(10)
DIMENSION IBIAS(60)
DATA IBIAS/957, 13, 137, 431, 822, 54, 766, 20, 950, 247, 22, 876,
* 78, 42, 938, 970, 935, 929, 174, 914, 72, 975, 872, 12,
2 53, 938, 94, 870, 12*0,
3 948, 94, 83, 889, 959, 807, 842, 926, 30, 577, 76, 126,

```

```

4      64,949,603, 2, 31,935,950,120/
1103  FORMAT(11X,A8,I5,I4X,I4,I6X,I4)
      READ(12) N,YLABL,DATA(1)
      IF(KEY(5).NE.10) RETURN

```

C
C
C
C
C

UPDATE BIAS

```

      XK=0 OR 1 AND ULOBE=PLOB OR ELOB DEPENDING ON WHETHER THE STATION
      NUMBER IS EVEN(POLAR) OR ODD(EQUATORIAL)
      IV=KEY(7)

```

```

      XK=KEY(2)-KEY(2)/2*2
      ULOBE=PLOB+EMPL0B*XK
      BIAS=DATA(1)/ULOB

```

```

      LBIAS=BIAS+0.500
      IF(BIAS.LT.0.00) LBIAS=BIAS-0.500
      BIAS=(BIAS-DFLOAT(LBIAS))

```

```

      DATA(1)=BIAS*ULOB
      BIAS=BIAS*1000.00 + DFLOAT(ICIAS(IV))
      ABIAS(IV)=DFLOAT(LBIAS)*ULOB
      IF(BIAS.LT.-0.500) BIAS=BIAS+1000.00
      IF(BIAS.GE.999.500) BIAS=BIAS-1000.00
      LBIAS=BIAS+0.500

```

```

      WRITE (31,1103) XLABL,KEY(2),IBIAS(IV),LBIAS
      RETURN

```

END

SUBROUTINE IWRITE

```

      IMPLICIT REAL*8 (A-H,O-Z)

```

```

      LOGICAL*1 GRAPH,SYMBOL,STAR,ELEVOK,PLOT,BLANK,ELEV,WT

```

```

      DIMENSION SYMBOL(2),GRAPH(83),SIGMA(2),DMS(2),NOBS(2),PLOT(2),

```

```

1      SUMT(2),SUMTSQ(2),SUMET(2),SCALE(2),TIMSEC(160),QMEAS(160,2),

```

```

2      ERR(2),IGRAPH(2),KI(2),SLOPE(2),IROPE(2),NEDIT(2),STATIO(30),

```

```

3      QMEAN(2),WT(2),KSEVEN(2)

```

```

      DATA BLANK,GRAPH /84*0 0/

```

```

      DATA SYMBOL,STAR/'L','M','*','*'/

```

```

      DATA IGRAPH /21,63/

```

```

      DATA STATIO/'FTMYR6E ','FTMYR6P ','QUITO6E ','QUITO6P ','

```

```

*      'LIMA6E ','LIMA6P ','SNTAG6E ','SNTAG6P ','

```

```

*      'NEWFL6E ','NEWFL6P ','WNKFL6E ','WNKFL6P ','

```

```

*      'JOBUR6E ','JOBUR6P ','ULASK6E ','ULASK6P ','

```

```

*      'ORORA6E ','ORORA6P ','MADG6E ','MADGA6P ','

```

```

*      'BPOIN6E ','BPCIN6P ','COLEG6E ','COLEG6P ','

```

```

*      'MOJAV6E ','MOJAV6P ','GFORK6E ','GFORK6P ','

```

```

*      'WOMER6E ','WOMER6P ' /

```

DO 5 I=31,60

```

M=I-30
WRITE(I,1104) STATIO(M),M
5 CONTINUE
10 READ(10,END=200) NOARC,NOPASS,ISTSID,STLABL,ELEVOK,LMEAN,LA,SIGMA,
  *DMS,TOCURR,TSCURR,(TIMSEC(L),L=1,LA),((QMEAS(L,I),L=1,LA),I=1,2)
  READ(11) LF,IDAY,SEC,KEY1,KEY3,LERROR,MERROR,
  * LLOBE,MLOBE,LSD,MSD,KEY7L,KEY7M,KSEVEN
  IH= TSCURR/3600.00
  SEC= TSCURR - (IH*3600)
  IM=SEC/60.00
  SEC=SEC-(60*IM)
  DO 20 I=1,2
  PLOT(I) = STAR
  WT(I)=BLANK
  IF(KSEVEN(I).GT.0) WT(I)=STAR
  IF(ELEVOK) PLOT(I)= SYMBOL(I)
  NOBS(I)=0
  SUMT(I)=0.00
  SUMFSQ(I)=0.00
  SUMET(I)=0.00
  SCALE(I)= 0.1500*SIGMA(I)
20 CONTINUE
  IF(LA.LE.1) GO TO 45
  DO 28 I=1,2
  N=0
  SUM=0.00
  TWOSIG=SIGMA(I)*3.00
  DO 22 L=1,LA
  IF(QMEAS(L,I).GE.10.020) GO TO 22
  SUM=SUM+QMEAS(L,I)
  N=N+1
22 CONTINUE
  NI=N
  SUMI=SUM
24 CONTINUE
  NOLD=N
  EN=N
  AVRAVE=SUM/EN
  N=NI
  SUM=SUMI
  DO 26 L=1,LA
  IF(QMEAS(L,I).GE.10.020) GO TO 26
  IF(DABS(QMEAS(L,I)-AVRAVE).LE.TWOSIG) GO TO 26
  SUM = SUM-QMEAS(L,I)

```

```

N=N-1
26 CONTINUE
IF(N.LT.NOLD) GO TO 24
QMEAN(I)= AVRAE
28 CONTINUE
WRITE(20,1105) STLABL,ISTSID,NOARC,NOPASS,IDAY,IH,IM,SEC,QMEAN,
*SIGMA
DO 40 L= 1,LA
TIM= TIMSEC(L)- TSCURR
IF(TIM.GT.3600.00) TIM= TIM- 86400.00
IF(TIM.LT.-3600.00) TIM = TIM + 86400.00
DO 30 I=1,2
ERR(I)= QMEAS(L,I)-QMEAN(I)
IF(ERR(I).GE.10.D20) GO TO 500
ERRORP= ERR(I)/SCALE(I)
IF (DABS(ERRORP).GT.20.00) GO TO 520
KI(I) = ERRORP + IGRAPH(I)
GRAPH(KI(I)) = PLOT(I)
NOBS(I)= NOBS(I)+1
SUMT(I)= SUMT(I)+ TIM
SUMTSQ(I) = SUMTSQ(I) + TIM*TIM
SUMET(I)= SUMET(I)+ ERR(I)*TIM
30 CONTINUE
WRITE(20,1106) TIM,ERR,GRAPH
GRAPH(KI(1)) = BLANK
GRAPH(KI(2)) = BLANK
40 CONTINUE
45 CONTINUE
DO 50 I=1,2
PLOT(I)= BLANK
IF(LA.LE.1) NOBS(I)=LA
NEDIT(I)= LA - NOBS(I)
SLOPE(I)= 0.00
IROPE(I)=0
IF(NOBS(I).LE.2) GO TO 50
OBSNUM= NOBS(I)
TBAR= SUMT(I)/OBSNUM
SLOPE(I)= SUMET(I)/(SUMTSQ(I)-SUMT(I)*TBAR)
IROPE(I)=100
TP=1.00+(1.00-SLOPE(I)*SUMET(I)/(SIGMA(I)*SIGMA(I)))/(OBSNUM-2.00)
IF(TP.GT.0.00) IROPE(I)=100.00*(1.00500-DSQRT(TP))
50 CONTINUE
ELEV=STAR
IF(ELEVOK) ELEV=BLANK

```

A-2.8 SAMPLE JCL FOR COMPLETE NAP RUN

JCL FOR COMPLETE NAP RUN

***** (JOB CARD) *****

JCL FOR PRENAP:

// EXEC LOADER, PARM=MAP, CALL, SIZE=100K, REGION=GO=110K
 // GO.SYSLIN DD *

***** OBJECT DECK FOR PRENAP-CARD-UPDATE PROGRAM INSERTED HERE *****

/*
 // GO.FT09F001 DD UNIT=9TRACK, LABEL=(11, BLP), DSN=ITAPEGEM,
 // DCB=(RECFM=VBS, LRECL=80, BLKSIZE=3204), DISP=(OLD, PASS),
 // VOL=SER=34503G
 // GO.FT10F001 DD UNIT=DISK, SPACE=(TRK,(1,1)),
 // DCB=(RECFM=VBS, LRECL=84, BLKSIZE=172), DISP=(NEW, DELETE)
 // GO.FT12F001 DD UNIT=DISK, SPACE=(CYL,(3,1)), DSN=NAPOLEON,
 // DCB=(RECFM=FB, LRECL=80, BLKSIZE=3200), DISP=(NEW, PASS)
 // GO.DATAS DD *

MOD 1 1
 MOD 9 9

REP	141	152	.720000000000000000000004.5000000000-13									
601	OFTMYREL	0 1 0 1 15 1 29 1 0 0.0	0.10-2									
601	OFTMYRPMR	0 2 0 1 15 4 30 1 0 0.0	0.10-2									
601	QUITCEL	0 3 0 1 15 5 31 1 0 0.0	0.10-2									
601	QUITOPMR	0 4 0 1 15 8 32 1 0 0.0	0.10-2									
601	OLIMAPELR	0 5 0 1 15 9 33 1 0 0.0	0.10-2									
601	OLIMAPPMR	0 6 0 1 15 12 34 1 0 0.0	0.10-2									
601	OSNTAGELR	0 7 0 1 15 13 35 1 0 0.0	0.10-2									
601	OSNTAGPMR	0 8 0 1 15 16 36 1 0 0.0	0.10-2									
601	ONEWFLELR	0 9 0 1 15 17 37 1 0 0.0	0.10-2									
601	ONEWFLPMR	0 10 0 1 15 20 38 1 0 0.0	0.10-2									
601	OWNKFLELR	0 11 0 1 15 21 39 1 0 0.0	0.10-2									
601	OWNKFLPMR	0 12 0 1 15 24 40 1 0 0.0	0.10-2									

MOD 173 186

REP	187	192	0.000000000000000000.100000000-02									
601	OJOBURELR	0 13 0 1 15 25 75 1 0 0.0	0.10-2									
601	OJOBURPMR	0 14 0 1 15 28 76 1 0 0.0	0.10-2									
601	OBPOINELR	0 21 0 1 15 41 77 1 0 0.0	0.10-2									
601	OBPOINPMR	0 22 0 1 15 44 78 1 0 0.0	0.10-2									
601	OCOLEGELR	0 23 0 1 15 45 79 1 0 0.0	0.10-2									

601	OCOLEGPMR	0	24	0	1	15	48	80	1	0	0.0	0.10-2
M00	193	202	0.00000000000000000000.1000000000-02									
INS	202	202										
601	OMOJAVELR	0	25	0	1	15	49	91	1	0	0.0	0.10-2
601	OMOJAVPMR	0	26	0	1	15	52	92	1	0	0.0	0.10-2
601	OGFORKELR	0	27	0	1	15	53	93	1	0	0.0	0.10-2
601	OGFORKPMP	0	28	0	1	15	56	94	1	0	0.0	0.10-2
601	OOOMERELR	0	29	0	1	15	57	95	1	0	0.0	0.10-2
601	OOOMERPMP	0	30	0	1	15	60	96	1	0	0.0	0.10-2
M00	1403	1403	0.7000000000-03									
M00	1436	1436	.7200000000000000000004.5000000000-13									
M00	2523	2523	.7200000000000000000004.5000000000-13									
M00	2763	2763	0.5000000000-3									
M0C	2802	2802	0.7000000000-03									
M00	3177	3177	0.3000000000-03									
M0C	3297	3297	0.3500000000-02									
M00	3443	3443	0.7470000000-03									
M0C	3708	3708	0.8650000000-03									
M0C	4087	4087	0.3610000000-03									
M0D	4230	4230	.7200000000000000000004.5000000000-13									
M0D	5165	5165	0.3000000000-02									
M0D	5400	5400	0.2810000000-02									
M0D	5515	5515	0.6000000000-02									
M0C	5555	5555	0.8000000000-03									

JCL FOR NAP:

```

// EXEC LINKGO, PARM=OVLY, MAP, LIST, XREF, NBLK=300, REGION, GO=499K
//LINK.SYSPRINT DD SYSOUT=A, SPACE=(CYL,(2,1))
//LINK.SYSUT1 DD SPACE=(CYL,(5,2))
//LINK.TAPELIB DD UNIT=24CO-9, LABEL=(2, BLP, IN), DISP=(OLD, PASS),
// DSN=NAPOBJ,
// DCB=(RECFM=FB, LRECL=80, BLKSIZE=3200), VOL=SER=34503G
//LINK.SYSLIN DD *
INSERT CLEAN
INSERT COMSOL, TSPARM, A SPARM, ACINFO, PSPARM, STINFO, TYLE, GENCOM, MSINFO
INSERT CDEBUG, IONUMB, GPCOM, EXTCM, EARTH, ICONST, FCONST, CONMET
INSERT CINTEG, CMEASR, RSUMR
INSERT MAIN, PAGE, ROTFIX, ROTINT, RESID, SIGWT, DAYHMS, CWORK
INSERT CLEAR
CVERLAY ALPHA
INSERT DREDIT, SPOLCD, DEFALT, INPCRD, GENFIL, EDIT, GAUSS, RANDU
INSERT UNIFD2, GPRSM2, GEOS, EDPOLY, REPRT2, RDMS, COMGHA, JULDAY, ECINT
CVERLAY ALPHA
INSERT PRTRIAL
INSERT MATMUT
INSERT REFRCT, ROTPAR, MEASUR, RSUM, MESOLD, ROTBAK, ROTOLO, ROTOMA, AZIM
INSERT ELEV, RARIES, SPOVEL, SVAREQ
INSERT SOFORT, SOFSEC, KICKER, ENGRAT
INSERT EXPAND
INSERT SOLVEX, SOVARY, ENTRNS, SOLANG, ENROOT, CLEAR
INSERT CKTIME, ENUTAT, PENMAT, PRENUT, VARIEQ, ENEXPS
INSERT ENVARY, SUMBDY, ENDIST, KCOM, JCOM, HCOM, GCOM, FCOM, ECOM
INSERT DCOM, CCOM, BCOM, ACOM, PRIMY
CVERLAY ALPHA
INSERT SOLVER, INVERT, FINALP
CVERLAY ALPHA
INSERT SIMOUT

```

*****ANY OBJECT DECKS FOR LINK STEP ARE INSERTED HERE*****

INCLUDE TAPELIB
ENTRY MAIN

```

//LINK.SYSUCCUMP DD SYSOUT=A, SPACE=(CYL,(1))
//GO.FT06FC01 DD SYSOUT=A, DCB=(RECFM=VBA, LRECL=137, BLKSIZE=7265),
// SPACE=(CYL,(9,1))
//SYSPRINT DD SYSOUT=A, DCB=(RECFM=VBA, LRECL=137, BLKSIZE=7265)
//GO.FT10FC01 DD UNIT=DISK, SPACE=(TRK,(3,1)), DSN=ATGOUTP,

```



```

//      DCB=(RECFM=VBS,LRECL=64,BLKSIZE=644),DISP=(NEW,PASS)
//GO.FT21F001 DD UNIT=DISK,SPACE=(CYL,(10,1)),DSN=Z7GEM21,
//      DCB=(RECFM=VBS,LRECL=156,BLKSIZE=7180)
//GO.FT22F001 DD UNIT=DISK,SPACE=(CYL,(4,1)),
//      DCB=(RECFM=VBS,LRECL=304,BLKSIZE=6996)
//GO.FT23F001 DD UNIT=2314,SPACE=(TRK,(4,1)),
//      DCB=(RECFM=VBS,LRECL=200,BLKSIZE=404)
//GO.FT24F001 DD UNIT=2314,SPACE=(TRK,(8,1)),
//      DCB=(RECFM=VBS,LRECL=200,BLKSIZE=404)
//GO.FT25F001 DD UNIT=DISK,SPACE=(CYL,(1,1)),
//      DCB=(RECFM=VBS,LRECL=200,BLKSIZE=404)
//GO.FT26F001 DD UNIT=2314,SPACE=(TRK,(8,1)),
//      DCB=(RECFM=VBS,LRECL=200,BLKSIZE=404)
//GO.FT27F001 DD UNIT=DISK,SPACE=(CYL,(3,1)),DSN=ATGCARDS,
//      DCB=(RECFM=VBS,LRECL=88,BLKSIZE=884),DISP=(NEW,DELETE)
//GO.FT28F001 DD DUMMY
//GO.FT29F001 DD UNIT=2400-9,LABEL=(5,BLP),DISP=(OLD,PASS),
//      DCB=(RECFM=VBS,LRECL=52,BLKSIZE=5204),VOL=SER=34503G
//GO.FT30F001 DD DUMMY
//GO.FT31F001 DD UNIT=2314,SPACE=(TRK,(4,1)),
//      DCB=(RECFM=VBS,LRECL=200,BLKSIZE=404)
//GO.FT32F001 DD UNIT=DISK,SPACE=(CYL,(9,1)),DSN=Z7GEM32,
//      DCB=(RECFM=VBS,LRECL=2168,BLKSIZE=2172)
//GO.FT33F001 DD DUMMY
//GO.FT35F001 DD DUMMY
//GO.FT36F001 DD UNIT=DISK,SPACE=(CYL,(1,1)),DSN=Z7GEM36,
//      DCB=(RECFM=VBS,LRECL=36,BLKSIZE=364),DISP=(NEW,DELETE)
//GO.FT37F001 DD UNIT=AFF=FT25F001,LABEL=(13,BLP),DSN=NURXTE,
//      DCB=(RECFM=VBS,LRECL=3825,BLKSIZE=7654),DISP=(NEW,PASS),
//      VOL=SER=34503G
//GO.FT37F002 DD UNIT=AFF=FT25F001,LABEL=(14,BLP),DSN=NUPASS,
//      DCB=(RECFM=VBS,LRECL=64,BLKSIZE=644),DISP=(NEW,PASS),
//      VOL=SER=34503G
//GO.FT37F003 DD DUMMY
//GO.SYSABEND DD SYSOUT=A,SPACE=(CYL,(1))
//GO.DATAS DD UNIT=DISK,DSN=NAPOLEON,DISP=(OLD,PASS)
/*

```

A-2-94

JCL FOR POST NAP:

```

// EXEC  LOADER,PARM=MAP,CALL,SIZE=180K,REGION.GO=190K
//GO.SYSLIN DD *

```

*****OBJECT DECK INSERTED HERE*****

```
/*
//GO.FT06F001 DD SYSOUT=A,DCB=(RECFM=VBA,LRECL=137,BLKSIZE=7265),
//    SPACE=(CYL,(5,1))
//GO.FT08F001 DD UNIT=DISK,SPACE=(CYL,(4,1)),DSN=Z7GEM08,
//    DCB=(RECFM=VBS,LRECL=80,BLKSIZE=1604),DISP=(NEW,DELETE)
//GO.FT10F001 DD UNIT=9TRACK,LABEL=(14,BLP),DSN=Z7GEM10,
//    DCB=(RECFM=VBS,LRECL=64,BLKSIZE=3204),DISP=(OLD,PASS),
//    VOL=SER=34503G
//GO.FT10F002 DD UNIT=9TRACK,LABEL=(13,BLP),DSN=Z7GEM1A,
//    DCB=(RECFM=VBS,LRECL=3825,BLKSIZE=7654),DISP=(OLD,PASS),
//    VOL=SER=34503G
//GO.FT10F003 DD UNIT=9TRACK,LABEL=(15,BLP),DSN=Z7GEM1B,
//    DCB=(RECFM=VBS,LRECL=80,BLKSIZE=1604),DISP=(NEW,KEEP),
//    VOL=SER=34503G
//GO.FT11F001 DD UNIT=DISK,SPACE=(CYL,(3,1)),DSN=Z7GEM11,
//    DCB=(RECFM=VBS,LRECL=76,BLKSIZE=764),DISP=(NEW,DELETE)
//GO.FT12F001 DD UNIT=DISK,SPACE=(TRK,(1,1)),DSN=Z7GEM12,
//    DCB=(RECFM=VBS,LRECL=24,BLKSIZE=244),DISP=(NEW,DELETE)
//GO.FT20F001 DD DUMMY
//GO.FT27F001 DD UNIT=DISK,DSN=NAPOLEON,DISP=(OLD,DELETE)
//GO.FT31F001 DD SYSOUT=A,SPACE=(TRK,(4,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT32F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT33F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT34F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT35F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT36F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT37F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT38F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT39F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT40F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT41F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
//    DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
```

```

//GO.FT42F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT43F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT44F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT45F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT46F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT47F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT48F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT49F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT50F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT51F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT52F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT53F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT54F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT55F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT56F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT57F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT58F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT59F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT60F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.DATAS DD *

```

1 20 0.50-3 136.83DC

/*

APPENDIX A-3
SUBROUTINE MODIFICATIONS TO NAP-II

A-3.1 SUBROUTINE ENEXPS

SUBROUTINE ENEXPS(ITN) 101430

SUBROUTINE ENEXPS(ITN) COMMENTS 101440

1. FOR EACH POWER SERIES COMPUTED THIS SUBROUTINE IS CALLED 101450

(KTR-2) TIMES BY SUBROUTINE EXPAND. KTR IS THE NUMBER OF 101460

TERMS IN THE POWER SERIES FOR POSITION (X,Y,Z) AND ITN IS THE 101470

TERM NUMBER BEING COMPUTED ON THE CURRENT ITERATION. 101480

INITIAL POSITION AND VELOCITY WOULD CORRESPOND TO ITN=1 AND 2 101490

RESPECTIVELY AND ARE NOT COMPUTED BY THIS SUBROUTINE. FOR EACH 101500

POWER SERIES THAT THIS SUBROUTINE IS CALLED THE INITIAL VALUE 101510

OF ITN IS THUS 3. 101520

2. THIS SUBROUTINE COMPUTES THE EFFECTS OF THE GRAVITATIONAL 101530

FORCE OF N-BODIES ON EACH OTHER. THE EFFECT OF SOLAR RADIATION 101540

PRESSURE IS ALSO COMPUTED. HOWEVER, THE GRAVITATIONAL PULL 101550

OF THE PRIMARY SOURCE ON THE PROBE IS NOT COMPUTED HERE BUT 101560

IN SUBROUTINE EXPAND. 101570

3. DENOTING (ITN-3) BY K, THE COEFFICIENTS OF T**K FOR RELATIVE 101580

DISTANCES AND THE COEFFICIENTS T**(K+2) FOR POSITIONS RELATIVE 101590

TO THE PRIMARY SOURCE ARE COMPUTED. NOTE THAT THE COEFFICIENT OF 101600

T**(K+2) IS ACTUALLY THE (3+K)TH, I.E. ITN-TH COEFFICIENT. THE 101610

CONTRIBUTION TO THE ITN-TH POSITION COEFFICIENTS OF THE PROBE 101620

OF THE PRIMARY SOURCE GRAVITY FIELD AND DRAG ARE CONTAINED IN 101630

(XPO,YPO,ZPO) WHEN THIS ROUTINE IS CALLED. 101640

4. THE COEFFICIENTS OF THE RELATIVE BODY POSITIONS ARE ARRANGED 101650

SUCH THAT SEQUENTIAL COEFFICIENTS OF ANY ONE BODY ARE ALWAYS 101660

'NBD' COEFFICIENTS APART 'NBD' THUS APPEARS AS A UNIT AND HAS 101670

FOR THIS REASON BEEN EQUIVALENCED TO 'ONE'. THE UNIT 'UNIT' 101680

CORRESPONDING TO RELATIVE DISTANCES IS NBD(NBD-1)/2, THE NUMBER OF 101690

RELATIVE DISTANCES BETWEEN NBD BODIES. THE VALUE OF K APPEARING 101700

IN THE PROGRAM IS GIVEN BY (ITN-3)*ONE AND CORRESPONDS THE 101710

K OF COMMENT 3 ABOVE. THUS X(N+K) IS THE COEFFICIENT OF T**K OF 101720

X-POSITION OF BODY N. 101730

5. SINCE ITN IS INITIALLY 3 (SEE COMMENT 1) IT FOLLOWS THAT K 101740

IS INITIALLY 0. 101750

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6A. IF SOLAR PRESSURE IS NOT BEING COMPUTED (KSP=0) THEN NO COMPUTATIONS ARE PERFORMED FOR THE PROBE-PRIMARY SOURCE COMBINATION (SEE COMMENT 2).

IF SOLAR PRESSURE IS BEING COMPUTED THEN THE PROBE-PRIMARY SOURCE DISTANCE MUST BE COMPUTED (BUT NOT THE PRIMARY SOURCE GRAVITATIONAL FORCE).

6B. IF THE SUN IS NOT THE PRIMARY SOURCE, THEN SHADOW COMPUTATIONS ARE PERFORMED, BUT

6C. IF THE SUN IS THE PRIMARY SOURCE, THEN NO SHADOW COMPUTATIONS ARE PERFORMED.

DENOTING THE PROBE-PRIMARY SOURCE POSITION IN THE R, THETA AND PHI ARRAYS BY N (WHERE N.LE.45) THE FOLLOWING QUANTITIES ARE COMPUTED

FOR CASE 6A. (NPRNPS= N, NPSNPR= 100, KSP2= 0)

FOR CASE 6B. (NPRNPS= 100, NPSNPR= N, KSP2= 1)

FOR CASE 6C. (NPRNPS= 100, NPSNPR= 100, KSP2= 0)

IMPLICIT REAL*8 (A-H,O-Z)

INTEGER*4 ONE,TWO,UNIT,S

REAL*8 KP1KP2

COMMON /CCOM/

1XPO(16),YPO(16),ZPO(16),XBD(160),YBD(160),ZBD(160),CGB(14),SGB(14)

2,XTL(14),YTL(14),CLB(14),SLB(14),CLT(14),SLT(14),VRB(14),

3RPT(14),RMT(14),RMO(14),RZR(14),RMR(14)

COMMON /ECOM/

1BDY(10),8MU(10),BTM(10),HTL(16),BRT(10),BRA(10),8DT(10),STL(16)

2,RST(825),VST(825),WST(770),NCN(10),NBT(10)

COMMON /ICOM/

1NBD,NTE,NHT,NSU,NPR,NPS,NOS,IGN,KTR,KDR,KVE,KDV,KSP,ISP,KIN,MPT

EQUIVALENCE (A(1),STL(1)),(THETAC(1),HTL(1)),(X(1),XBD(1)),

* (Y(1),YBD(1)),(Z(1),ZBD(1)),(R(1),RST(1)),(THETA(1),VST(1)),

* (PHI(1),WST(1)),(ONE,NBD)

DIMENSION A(16),THETAC(16),X(160),Y(160),Z(160),R(825),THETA(825),

* PHI(770)

IJO= 0

```

102310 XK= ITN - 3
102320 OK3= -XK/3.DO
102330 KPIKP2= (XK+1.00)*(XK+2.00)
102340 K= (ITN-3) * ONE
102350
102360 FOR (K=0) SEE COMMENT 5.
102370 IF(K.LE.0) GO TO 1300
102380
102390 100 KMONE= K - ONE
102400 KPTWO= K + TWO
102410
102420 DO 700 IO= 1,NBDMI
102430 IK= IO + K
102440 IKPTWO= IK + TWO
102450 GMI= BMU(IO)
102460
102470 IOPI=IO+1
102480 DO 600 JO=IOPI,NBD
102490 JK= JO + K
102500 IJO= IJO + 1
102510 IJS= IJO
102520 IJK= IJK + 1
102530 IJKMS= IJK
102540
102550 FOR 'IJO=NPRNPS' SEE COMMENT 6.
102560
102570 IF(IJO.EQ.NPRNPS) GO TO 600
102580
102590 XIJO= X(IO) - X(JO)
102600 YIJO= Y(IO) - Y(JO)
102610 ZIJO= Z(IO) - Z(JO)
102620
102630 FOR 'K=0' SEE COMMENT 5.
102640
102650 IF(K.LE.0) GO TO 1200
102660
102670 FXIJK= THETA(IJO) * (X(IK)-X(JK))
102680 FYIJK= THETA(IJO) * (Y(IK)-Y(JK))
102690 FZIJK= THETA(IJO) * (Z(IK)-Z(JK))
102700 RIJK= XIJO*(X(IK)-X(JK)) + YIJO*(Y(IK)-Y(JK)) + ZIJO*(Z(IK)-Z(JK))
102710 THIJK= 0.DO
102720 PHIJK= 0.DO
102730
102740 IF(KMONE.LE.0) GO TO 400

```



```

C
DO 300 S= ONE, KMONE, ONE
IJS = IJS + UNIT
IJKMS= IJKMS - UNIT
PHIJK= R(IJS) * PHI(IJKMS) + PHIJK
THIJK= THETA(IJS) * PHI(IJKMS) + THIJK
FXIJK= THETA(IJS) * (X(IK-S) - X(JK-S)) + FXIJK
FYIJK= THETA(IJS) * (Y(IK-S) - Y(JK-S)) + FYIJK
FZIJK= THETA(IJS) * (Z(IK-S) - Z(JK-S)) + FZIJK
IF(IJS-IJKMS) 200, 1000, 300

C
200 RIJK= (X(IO+S)-X(JO+S)) * (X(IK-S)-X(JK-S))
1 + (Y(IO+S)-Y(JO+S)) * (Y(IK-S)-Y(JK-S))
2 + (Z(IO+S)-Z(JO+S)) * (Z(IK-S)-Z(JK-S))
3 - R(IJS) * R(IJKMS) + RIJK
300 CONTINUE

C
400 R(IJK) = RIJK/R(IJO)

C
FOR *IJO=NPSNPR* SEE COMMENT 6.
IF(IJO.EQ.NPSNPR) GO TO 2000

C
PHI(IJK) = (R(IJK)*XK - PHIJK)/R(IJO)
THETA(IJK) = (PHI(IJK)*THETA(IJO) + THIJK)/QK3
FXIJK = THETA(IJK)*XIJO + FXIJK
FYIJK = THETA(IJK)*YIJO + FYIJK
FZIJK = THETA(IJK)*ZIJO + FZIJK

C
500 IF(IJO.EQ.NPRNSU) GO TO 1100

C
X(IKPTWO) = - BMU(JO)*FXIJK + X(IKPTWO)
Y(IKPTWO) = - BMU(JO)*FYIJK + Y(IKPTWO)
Z(IKPTWO) = - BMU(JO)*FZIJK + Z(IKPTWO)

C
X(JK+TWO) = GMI*FXIJK + X(JK+TWO)
Y(JK+TWO) = GMI*FYIJK + Y(JK+TWO)
Z(JK+TWO) = GMI*FZIJK + Z(JK+TWO)

C
600 CONTINUE
700 CONTINUE

C
800 L1= KPTWO + 1
L2= L1 + NBDMI

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C
FXIJK= X(NPS+KPTWO)
FYIJK= Y(NPS+KPTWO)
FZIJK= Z(NPS+KPTWO)
DO 900 L= LI,L2
X(L)= (X(L) - FXIJK)/KPIKP2
Y(L)= (Y(L) - FYIJK)/KPIKP2
Z(L)= (Z(L) - FZIJK)/KPIKP2
900 CONTINUE
C
C SEC COMMENT 3.
C
C
C
X(NPR+KPTWO) = X(NPR+KPTWO) + XPO(ITN)
XPO(ITN) = X(NPR+KPTWO)
Y(NPR+KPTWO) = Y(NPR+KPTWO) + YPO(ITN)
YPO(ITN) = Y(NPR+KPTWO)
Z(NPR+KPTWO) = Z(NPR+KPTWO) + ZPO(ITN)
ZPO(ITN) = Z(NPR+KPTWO)
C
C KSP2 IS GREATER THAN ZERO IF SHADOW COMPUTATIONS ARE REQUIRED.
C
C IF(KSP2.GT.0) GO TO 2300
C
C RETURN
C
C
1000 RIJK= ((X(IK-S) -X(JK-S))**2 + (Y(IK-S) - Y(JK-S))**2
* (Z(IK-S) -Z(JK-S))**2 - R(IJS)**2) * 0.5D0 + RIJK
GO TO 300
C
C
1100 X(NPR+KPTWO) = GMSUN * FXIJK + X(NPR+KPTWO)
Y(NPR+KPTWO) = GMSUN * FYIJK + Y(NPR+KPTWO)
Z(NPR+KPTWO) = GMSUN * FZIJK + Z(NPR+KPTWO)
GO TO 600
C
C
1200 RIJK = XIJO**2 + YIJO**2 + ZIJO**2
R(IJO) = DSQRT(RIJK)
THETA(IJO) = R(IJU)/RIJK/RIJK
FXIJK = THETA(IJO) * XIJO

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FYIJK = THETA(IJO) * YIJO
FZIJK = THETA(IJO) * ZIJO
IF (IJO .EQ. NPSNPR) GO TO 600
GO TO 500
C
C
C
C
1300 NBDM1= NBD - 1
UNIT= NBDM1*NBD/2
TWO= ONE + ONE
L1 = TWO + 1
L2 = KTR*ONE
C
DO 1400 L= L1,L2
X(L)= 0.00
Y(L)= 0.00
Z(L)= 0.00
1400 CONTINUE
C
ITNM2=1
IJK= 0
MNSU= NBD*(NSU-1) - NSU*(NSU+1)/2
MNPR= NBD*(NPR-1) - NPR*(NPR+1)/2
MNPS= NBD*(NPS-1) - NPS*(NPS+1)/2
NPRNSU= MNPR + NSU
IF(NSU.LT.NPR) NPRNSU= MNSU + NPR
NPRNPS= MNPR + NPS
IF(NPS.LT.NPR) NPRNPS= MNPS + NPR
GMSUN= BMU(NSU)
IF(KSP.GT.0) GO TO 1500
1440 NPSNPR= 100
KSP2= 0
1450 IF(NPR.LT.NSU) GMSUN= -GMSUN
GO TO 100
C
1500 NPSNPR= NPRNPS
NPRNPS= 100
IF(NPS.EQ.NSU) GO TO 1550
NSUNPS= MNPS + NSU
IF(NSU.LT.NPS) NSUNPS= MNSU + NPS
KSP2 = 1
A(KTR) = 0.00
THETAC(KTR) = 0.00

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104070 A(KTR-1) = 0.00
104080 THETAC(KTR-1) = 0.00
104090 IF(ISP.GT.0) GMSUN= GMSUN - SPC
104100 GO TO 1450
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SOLAR PRESSURE SHADOW SERIES.

2000 AK = R(IJK)* R(IJO)
ITNM2 = ITN - 2
L = ITNM2/2

NOTE THAT, PROVIDED THAT K IS GREATER THAN ZERO, THEN AT THE END
OF DO-LOOP 300 IJS = (K-1) UNITS AND IJKMS = 1 UNIT.
L IS CHOSEN SUCH THAT IF ITN IS EVEN THEN L = (ITN-1-L)-1 AND
IF ITN IS ODD THEN L = (ITN-1-L)-2. IN THE LATTER CASE AN
EXTRA TERM MUST BE ADDED TO AK. THE LATTER CONDITION IS
EQUIVALENT TO IJKMS = IJS.

IF(L.LE.1) GO TO 2200
DO 2100 S = 2,L
AK= R(IJKMS)*R(IJS) - A(S)*A(ITN-1-S) + AK
IJKMS= IJKMS + UNIT
IJS = IJS - UNIT

2100 CONTINUE
2200 IF(IJKMS.LE.IJS) AK= (R(IJS)**2 - A(L+1)**2) * 0.500 + AK
A(ITNM2)= AK/A(1)
GO TO 600

IJK AT THIS POINT EQUALS (K+1) UNITS.

2300 THETAK= 0.00
DO 2400 S= 1,ITNM2
THETAK= X(NSU-ONE+S*ONE) * X(NPR+K+ONE-S*ONE)

1 + Y(NSU-ONE+S*ONE) * Y(NPR+K+ONE-S*ONE)
2 + Z(NSU-ONE+S*ONE) * Z(NPR+K+ONE-S*ONE)
3 + A(S)*R(NSUNPS+IJK-S*UNIT) + THETAK

2400 CONTINUE

THETAC(ITNM2)= THETAK

RETURN

C

END

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0316 CARDS

A-3.2 SUBROUTINE EXPAND

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SUBROUTINE EXPAND (KEY, NNA)
IMPLICIT REAL*8(A-H,O-Z)
INTEGER*4 ONE
DIMENSION IDUMMY(2), U(2394), V(2394)
COMMON BLOCK - REDUCED FORM
COMMON /ACOM/
1CNM(136), SNM(136), F(171), C00, C20, EXTRA(99), UMT(2394), VMT(2394)
2, LCT(16), ICI(17), ONE
COMMON /CCOM/
1XPO(16), YPO(16), ZPO(16), XBD(160), YBD(160), ZBD(160), CGB(14), SGB(14)
2, XTL(14), YTL(14), CLB(14), SLB(14), CLT(14), SLT(14), VRB(14),
3RPT(14), RMT(14), RMO(14), RZR(14), RMR(14)
COMMON /DCOM/
1HTS(12), CAV(12), CBV(12), ALT(12), CNA(12), CNB(12), XRD(14), YRD(14),
2ZRD(14), XDD(14), YDD(14), ZDD(14), RHO(14), RPO(14), RVR(14), HNV(14),
3VRN(14), VSR(14)
COMMON /HCOM/
1TON, TEN, EPS, TIN, DEL, SPC, PSA, FSA, TOJ, UPD, TOP, DTP
2, CUD, CUV, CUT, ERD, XMU, ALF, OMG, ECC, CDC, CTW, XIT(6)
COMMON /ICOM/
1NBD, NTE, NHT, NSU, NPR, NPS, NOS, ICN, KTR, KDR, KVE, KDV, KSP, ISP, KIN, MPT
COMMON BLOCK COMPLETED
EQUIVALENCE (IDUMMY(1), I, XXXX), (IDUMMY(2), J2),
*(U(1), UMT(1)), (V(1), VMT(1))
EQUIVALENCE (ONE, J3)
SIN(XXX) = DSIN(XXX)
COS(XXX) = DCOS(XXX)
EXP(XXX) = DEXP(XXX)
ATAN(XXX) = DATAN(XXX)
SQRT(XXX) = DSQRT(XXX)
IF (KEY .GT. 2) GO TO 100
XMUE = XMU / (ERD + ERD)
J = 1
DO 30 M = 1, NTE
NM = LCT (M)
IF (NM .LE. 0) GO TO 30
XMN = XMUE
I2MPI = M + M - 1
XMNO = I2MPI
XDIV = 0.00
DO 10 I = 1, I2MPI, 2
X = I
10 XMN = XMN * X
DO 20 K = 1, NM

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CNM (J) = CNM (J)*XMN
SNM (J) = SNM(J) * XMN
J= J+1
XMNO = XMNO + 2.00
XDIV = XDIV +1.00
20 XMN = XMN * XMNO/XDIV
30 CONTINUE
J1 = 1
NA = NTE +1
KMAZ = 0
LA = 0
LB = LCT (1)
IF(KVE.LE.2) GO TO 50
C00= 6.00*CNM(1)/ERD
C20= 14.00*CNM(3)/ERD
IF(LB.LE.2) C20= 0.00
IF ( NA . GE. 3 ) GO TO 40
NA = 3
LCT (2) = 0
40 KMAZ = 3
IF (LB . GT. 2 ) KMAZ = 5
50 CONTINUE
DO 90 MPI = 1,NA
IF (LA . LT. (KMAZ-MPI)) LA = KMAZ-MPI
IF (LA . LT. LB) LA = LB
IF (MPI . GE. NA ) GO TO 60
LC = LCT (MPI+1)
IF (LC . LE. 0 ) GO TO 60
IF ( LA . LE. LC ) LA = LC +1
60 J3 = J1 + LA
J2 = J3 -1
IF ( LA . LE. 0 ) GO TO 80
JPI = J1 + 1
XMSQ = (MPI-1) * (MPI-1)
XN = MPI
DO 70 J = JPI,J3
F(J) = (XMSQ - XN**2)/(4.00*XN**2 - 1.00 )
70 XN = XN + 1.00
80 I = 1 - LA
IF ( I . LT. 0 ) I = -1
IF (MPI .GT. 1) I = I + 2
IF ( MPI . GE. NA ) I = I + 3
F(J1) = XXXX
J1 = J3 + 1

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97830 ICT(MPI)= J3
97840 LA = LB - 1
97850 LB = LC
97860 CONTINUE
97870 KEY = 3
97880 CONTINUE
97890 ITR=3
97900 K = 1
97910 KO=0
97920 KJ=1
97930 CGB(1)=DCOS(ALF)
97940 SGB(1)=DSIN(ALF)
97950 CLB(1)=XPO(1)*CGB(1)+YPO(1)*SGB(1)
97960 SLB(1)=YPO(1)*CGB(1)-XPO(1)*SGB(1)
97970 RPT(1)=XPO(1)*XPO(1)+YPO(1)*YPO(1)+ZPO(1)*ZPO(1)
97980 RMT(1)=1.00/RPT(1)
97990 CLT(1)=ERD*RMT(1)*CLB(1)
98000 SLT(1)=ERD*RMT(1)*SLB(1)
98010 RZR(1)=ERD*RMT(1)*ZPO(1)
98020 RMR(1)=ERD*ERD*RMT(1)
98030 RMO(1)=DSQRT(RMT(1))
98040 RMO TWO= RMO(1)+RMO(1)
98050 U(1)= RMO(1)
98060 GO TO 490
98070 CONTINUE
98080 TX=0.00
98090 TY=0.00
98100 TZ=0.00
98110 KONE= KJ-ONE
98120 IF(NTE.LE.1) GO TO 340
98130 KO= LCT(1)
98140 L= ICT(1) + 1 + KONE
98150 LMI= 2 + KONE
98160 LPI=ICT(2)+ KONE
98170 IN= LCT(2)
98180 IF(IN.LE.0) GO TO 312
98190 DO 310 I=1,IN
98200 TX=(U(LMI+I)-U(LPI+I))*CNM(KO+I)- V(LPI+I) *SNM(KO+I)+TX
98210 TY=(U(LMI+I)+U(LPI+I))*SNM(KO+I)- V(LPI+I) *CNM(KO+I)+TY
98220 TZ = -U(L+I)*CNM(KO+I) - V(L+I)*SNM(KO+I) + TZ
98230 CONTINUE
98240 IF(NTE.LT.3)GO TO 340
98250 DO 330 MPI=3,NTE
98260 KO= KO+IN

```

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LM1= L+1
L= LPI +1
LPI=ICT(MPI) + KONE
IN= LCT(MPI)
IF(IN.LE.0) GO TO 330
DO 320 I=1,IN
TX=(U(LM1+I)-U(LPI+I))*CNM(KO+I)+(V(LM1+I)-V(LPI+I))*SNM(KO+I)+TX
TY=(U(LM1+I)+U(LPI+I))*SNM(KO+I)-(V(LM1+I)+V(LPI+I))*CNM(KO+I)+TY
320 TZ= -U(L+I)*CNM(KO+I) - V(L+I)*SNM(KO+I) + TZ
330 CONTINUE
340 IN=LCT(I)
L= IN + 1
LPI= L+ 1 + KONE
L2= ICT(1) + LCT(2) + KONE + 2
TXO=0.00
TYO=0.00
DO 350 I=1,IN
TXO= -CNM(L-I)*U(L2-I) + TXO
TYO= -CNM(L-I)*V(L2-I) + TYO
350 TZ= -CNM(L-I)*U(LPI-I) + TZ
XTL(K) = TXO+TXO+TX
YTL(K) = TYO+TYO+TY
TX= DRX
TY=DRY
KPI = K+1
DO 360 I=1,K
TX=CGB(I)*XTL(KPI-I) - SGB(I)*YTL(KPI-I) + TX
360 TY=CGB(I)*YTL(KPI-I) + SGB(I)*XTL(KPI-I) + TY
XK=K*KPI
XPO(ITR)= TX/XK
YPO(ITR)= TY/XK
ZPO(ITR)= (TZ+TZ+DRZ)/XK
IF(NB0.GT.2) CALL ENEXPS(ITR)
IF(ITR.GE.KTR) RETURN
KPI= ITR
K= ITR-1
KMI=K-1
OMGK=KMI
OMGK=OMG/OMGK
L=K/2
ITR=ITR+1
R2K=XPO(I)*XPO(K)+YPO(I)*YPO(K)+ZPO(I)*ZPO(K)
RM1K=0.00
IF(L.LT.2) GO TO 380

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98690
98700

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DC 370 N=2,L
R2K=XPO(N)*XPO(KPI-N)+YPO(N)*YPO(KPI-N)+ZPO(N)*ZPO(KPI-N)+R2K
370 RMIK=RMO(N)*RMO(KPI-N) + RMIK
380 R2K = R2K+R2K
RMIK= RMIK+RMIK
IF((L+L).GE.K) GO TO 390
R2K= XPO(L+1)**2 + YPO(L+1)**2 + ZPO(L+1)**2 + R2K
RMIK= RMO(L+1)**2 + RMIK
390 RPI(K)= R2K
CGB(K)= -OMGK*SGB(KMI)
SGB(K)= OMGK*CGB(KMI)
RCLA=XPO(1)*CGB(K) + YPO(1)*SGB(K) + XPO(K)*CGB(1) + YPO(K)*SGB(1)
RSLA=YPO(1)*CGB(K) - XPO(1)*SGB(K) + YPO(K)*CGB(1) - XPO(K)*SGB(1)
RHOC= 0.00
RHOSL= 0.00
RHODL= 0.00
RM2K= R2K*RM2(1)
IF(KMI.LT.2) GO TO 410
DO 400 N= 2,KMI
RHOC= CLB(N)*RMT(KPI-N) + RHOC
PHOSL= SLB(N)*RMT(KPI-N) + RHOSL
RHODL= ZPO(N)*RMT(KPI-N) + RHODL
RM2K = RPT(N)*RMT(KPI-N) + RM2K
RCLA = XPO(N)*CGB(KPI-N) + YPO(N)*SGB(KPI-N) + RCLA
RSLA = YPO(N)*CGB(KPI-N) - XPO(N)*SGB(KPI-N) + RSLA
400 CLB(K)= RCLA
410 SLB(K) = RSLA
RMT(K) = - RM2K*RMT(1)
CLT(K)= (CLB(1)*RMT(K)+RCLA*RMT(1)+ RHOC) * ERD
SLT(K)= (SLB(1)*RMT(K)+RSLA*RMT(1)+ RHOSL) * ERD
RZR(K) = (ZPO(1)*RMT(K) + ZPO(K)*RMT(1) + RHODL) * ERD
RMR(K)= RMT(K) * ERD*ERD
KU=KJ
KJ=K0+1
RMD(K) = (RMT(K)-RMIK)/RMTWO
U(KJ)= RMO(K)
490 CONTINUE
XXXX = F(1)
UA = 0.00
UB=0.00
VB=0.00
IF (I .GE. 0 ) G O TO 1000
UAN = 0.00
DO 500 N = 1, K

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99140

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UA = RZR (N) * U (KJ) + UA
UAM= RMR(N)*U(KJ) + UAM
UB= CLT(N)*U(KJ) + UB
VB= SLT(N)*U(KJ) + VB
500 KJ = KJ - ONE
KJ = KO +2
U(KJ) = UA
UA = UAM * F( 2)
IF ( J2 . LE. 2) GO TO 530
DO 520 J = 3, J2
UAM = 0
DO 510 N = 1, K
UA = RZR (N) * U (KJ) + UA
UAM= RMR(N)*U(KJ) + UAM
510 KJ = KJ - ONE
KJ = KO + J
U (KJ) = UA
520 UA = UAM * F(J)
530 CONTINUE
DO 540 N = 1,K
UA = RZR (N) * U (KJ) + UA
540 KJ = KJ - ONE
542 J = J2 + 1
KJ = KO + J
U(KJ) = UA
550 IF (J . GE. ONE ) GO TO 570
551 J = J +1
KJ = KO + J
U ( KJ) = UB
V(KJ) = VB
XXXX = F(J)
UA = 0.00
UB = 0.00
VA = 0.00
VB = 0.00
GO TO ( 552, 1020, 1040, 1060, 560, 570), I
552 UAM = 0.00
VAM = 0.00
DO 554 N = 1, K
UA = RZR (N) * U (KJ) + UA
VA = RZR (N) * V(KJ) + VA
UAM= RMR(N)*U(KJ) + UAM
VAM= RMR(N)*V(KJ) + VAM
UB = CLT (N) * U(KJ) - SLT (N) * V (KJ) + UB
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99160
99170
99180
99190
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99210
99220
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99470
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99500
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554 VB = CLT (N) * V (KJ) + SLT (N) * U (KJ) + VB 99590
555 KJ = KJ - ONE 99600
556 J = J + 1 99610
KJ = KO + J 99620
U(KJ) = UA 99630
V(KJ) = VA 99640
UA = UAM * F( J ) 99650
VA = VAM * F(J) 99660
IF (J . GE. J2) GO TO 560 99670
J1 = J +1 99680
DO 558 J = J1,J2 99690
UAM = 0.00 99700
VAM = 0.00 99710
DO 556 N = 1,K 99720
UA = RZR (N) * U (KJ) + UA 99730
VA = RZR (N) * V(KJ) + VA 99740
UAM= RMR(N)*U(KJ) + UAM 99750
VAM= RMR(N)*V(KJ) + VAM 99760
556 KJ = KJ- ONE 99770
KJ = KO + J 99780
U(KJ)= UA 99790
V(KJ) = VA 99800
UA = UAM * F(J) 99810
VA = VAM*F(J) 99820
560 CONTINUE 99830
DO 562 N= 1,K 99840
UA = RZR (N) * U (KJ) + UA 99850
VA = RZR (N) * V(KJ) + VA 99860
562 KJ = KJ-ONE 99870
564 J = J2+1 99880
KJ = KO + J 99890
U(KJ) = UA 99900
V(KJ) = VA 99910
GO TO 550 99920
570 CONTINUE 99930
DRX=0.00 99940
DRY=0.00 99950
DRZ=0.00 99960
IF (KDR . LE. 0 ) GO TO 300 99970
C COMPUTE THE CORRECTION TERMS FOR DRAG 99980
IF (KA-1)610,610,700 99990
610 TMA=SQRT(XPO(1)*XPO(1)+YPO(1)*YPO(1)) 10000
TMB=ZPO(1)/TMA 100010
TMC=ATAN(TMB) 100020

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XAD= TMC
TMA=TMA+1.DO
XRD(KA)=TMA*XPO(KC)-XAD
YRD(KA)=TMA*YPO(KC)-YAD
ZRD(KA)=TMA*ZPO(KC)
TMA=0.DO
KC=KA
K=KA/2
DO 720 I=1,K
TMA=TMA+XRD(I)*XRD(KC)+YRD(I)*YRD(KC)+ZRD(I)*ZRD(KC)
720 KC=KC-1
TMA=TMA+TMA
IF (KC-K)740,740,730
730 TMA=TMA+XRD(KC)*XRD(KC)+YRD(KC)*YRD(KC)+ZRD(KC)*ZRD(KC)
740 VSR(KA)=TMA
TMB=RPT(KA)
KC=KB
IF (KB-1)770,770,750
750 DO 760 I=2,KB
TMA=TMA-VRB(I)*VRB(KC)
TMB=TMB-RPO(I)*RPO(KC)
760 KC=KC-1
770 VRB(KA)=TMA/(2.0*VRB(1))
RPO(KA)=TMB/(2.0*RPO(1))
IF (KA-2)780,780,790
780 TMB=ECC*RZR(1)/SQRT(1.0-ECC*RM(1)*ZPO(1)*ZPO(1))
TMA=RPO(2)-TMB*(ZPO(1)*RMO(1)*RPO(2)-ZPO(2))
TMB=CPB*RHO(1)
HDI=TMA
GO TO 810
790 KC=KB-1
TMA=KB
TMA=CPB/TMA
TMB=HDT*RHO(KB)
TMC=2.DO
DO 800 I=3,KA
TMB=TMB+TMC*RPO(I)*RHO(KC)
TMC=TMC+1.DO
800 KC=KC-1
810 RHO(KA)=TMA*TMB
TMA=0.DO
KC=KA
DO 820 I=1,KA
TMA=TMA+RHO(I)*VRB(KC)

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TMD=ERD/637816.500
TME=U.00
KB=10
GO TO 630
620 TMC=ATAN(TMB*(TME+TMF)/(TME+TMF*(1.0-ECC)))
630 TMF = ERD / DSQRT(1.00-ECC*SIN(TMC)**2)
HIT=TMA/COS(TMC)-TMF
TMC=HIT-TME
TME=HIT
IF (TMC)640,670,650
640 TMC=-TMC
650 KB=KB-1
IF (TMC-TMD)670,670,660
660 IF (KB) 670,670,620
670 CONTINUE
DO 680 I=1,NHT
K=I
IF (HIT-ALT(I))680,690,690
680 CONTINUE
690 CPA=CNA(K)
CPB=CNB(K)
CTW=CPB
XAD=-OMG*YPO(I)
YAD= OMG*XPO(I)
XRD(1)=XPO(2)-XAD
YRD(1)=YPO(2)-YAD
ZRD(1)=ZPO(2)
VSR(1)=XRD(1)*XRD(1)+YRD(1)+ZRD(1)*ZRD(1)
VRB(1)=DSQRT(VSR(1))
RPO(1)=DSQRT(RPT(1))
RHD(1)=CPA*EXP(CPB*HIT)
RVR(1)=RHO(1)*VRB(1)
TMA=CDC*RVR(1)
XDD(1)=XRD(1)*TMA
YDD(1)=YRD(1)*TMA
ZDD(1)=ZRD(1)*TMA
GO TO 840
700 IF (ITR-KDR)710,710,300
710 KB=KA-1
KC=KA+1
TMA=KB
TMB=OMG/TMA
TMC=-TMB*YAD
YAD= TMB*XAD

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100430
100440
100450
100460

XAD= TMC 100470
 TMA=TMA+1.00 100480
 XRD(KA)=TMA*XPO(KC)-XAD 100490
 YRD(KA)=TMA*YPO(KC)-YAD 100500
 ZRD(KA)=TMA*ZPO(KC) 100510
 TMA=0.00 100520
 KC=KA 100530
 K=KA/2 100540
 DO 720 I=1, K 100550
 TMA=TMA+XRD(I)*XRD(KC)+YRD(I)*YRD(KC)+ZRD(I)*ZRD(KC) 100560
 720 KC=KC-I 100570
 TMA=TMA+TMA 100580
 IF (KC-K) 740, 740, 730 100590
 730 TMA=TMA+XRD(KC)*XRD(KC)+YRD(KC)*YRD(KC)+ZRD(KC)*ZRD(KC) 100600
 740 VSR(KA)=TMA 100610
 TMB=RPT(KA) 100620
 KC=KB 100630
 IF (KB-1) 770, 770, 750 100640
 DO 760 I=2, KB 100650
 TMA=TMA-VRB(I)*VRB(KC) 100660
 TMB=TMB-RPO(I)*RPO(KC) 100670
 760 KC=KC-I 100680
 770 VRB(KA)=TMA/(2.0*VRB(I)) 100690
 RPO(KA)=TMB/(2.0*RPO(I)) 100700
 IF (KA-2) 780, 780, 790 100710
 780 TMB=ECC*RZR(I)/SQRT(1.0-ECC*RM(I)*ZPO(I)*ZPO(I)) 100720
 TMA=RPO(2)-TMB*(ZPO(1)*RMO(1)*RPO(2)-ZPO(2)) 100730
 TMB=CPB*RRHO(1) 100740
 HDT=TMA 100750
 GO TO 810 100760
 790 KC=KB-I 100770
 TMA=KB 100780
 TMA=CPB/TMA 100790
 TMB=HDT*RRHO(KB) 100800
 TMC=2.00 100810
 DO 800 I=3, KA 100820
 TMB=TMB+TMC*RPO(I)*RHO(KC) 100830
 TMC=TMC+1.00 100840
 800 KC=KC-I 100850
 810 RHO(KA)=TMA*TMB 100860
 TMA=0.00 100870
 KC=KA 100880
 DO 820 I=1, KA 100890
 TMA=TMA+RHO(I)*VRB(KC) 100900

820	KC=KC-1	100910
	RVR(KA)=TMA	100920
	KC=KA	100930
	TMA=0.DO	100940
	TMB=0.DO	100950
	TMC=0.DO	100960
	DO 830 I=1,KA	100970
	TMD=RVR(I)	100980
	TMA=TMA+TMD*XRD(KC)	100990
	TMB=TMB+TMD*YRD(KC)	101000
	TMC=TMC+TMD*ZRD(KC)	101010
830	KC=KC-1	101020
	XDD(KA)=CDC*TMA	101030
	YDD(KA)=CDC*TMB	101040
	ZDD(KA)=CDC*TMC	101050
840	DRX=XDD(KA)	101060
	DRY=YDD(KA)	101070
	DRZ=ZDD(KA)	101080
	K=KA	101090
	GO TO 300	101100
1000	CONTINUE	101110
	DO 1010 N = 1, K	101120
	UA = RZR (N) * U (KJ) + UA	101130
	UB = CLT(N)*U(KJ) + UB	101140
	VB = SLT(N)*U(KJ) + VB	101150
1010	KJ = KJ-ONE	101160
	GO TO 542	101170
1020	CONTINUE	101180
	DO 1030 N = 1,K	101190
	UA = RZR (N) * U (KJ) + UA	101200
	VA = RZR (N) * V(KJ) + VA	101210
	UB = CLT (N) * U(KJ) - SLT (N) * V (KJ) + UB	101220
	VB = CLT (N) * V (KJ) + SLT (N) * U (KJ) + VB	101230
1030	KJ = KJ-ONE	101240
	GO TO 564	101250
1040	CONTINUE	101260
	DO 1050 N = 1,K	101270
	UB = CLT (N) * U(KJ) - SLT (N) * V (KJ) + UB	101280
	VB = CLT (N) * V (KJ) + SLT (N) * U (KJ) + VB	101290
1050	KJ = KJ-ONE	101300
	GO TO 551	101310
1060	CONTINUE	101320
	UAM = 0.DO	101330
	VAM = 0.DO	101340

DO 1070 N = 1,K
UA = RZR (N) * U (KJ) + UA
VA = RZR (N) * V(KJ) + VA
UAM = RMR(N)*U(KJ) + UAM
VAM = RMR(N)*V(KJ) + VAM
1070 KJ = KJ-ONE
GO TO 555
END

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0448 CARDS

A-3.3 SUBROUTINE VARIEQ

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SUBROUTINE VARIEQ
IMPLICIT REAL*8(A-H,O-Z)
INTEGER*4 ONE
DIMENSION TMT(9)
COMMON BLOCK - REDUCED FORM
COMMON /ACOM/
1CNM(136),SNM(136),F(171),C00,C20,EXTRA(99),UMT(2394),VMT(2394)
2,LCT(16),ICT(17),ONE
COMMON /CCGM/
1XPO(16),YPO(16),ZPO(16),XBD(160),YBD(160),ZBD(160),CGB(14),SGB(14)
2,CSQ(14),XVR(14),SSQ(14),YVR(14),SCS(14),ZVR(14)
3,QAV(14),QBV(14),QCV(14),BXB(14),BYB(14),BZB(14)
COMMON /DCOM/
1H,S(12),CAV(12),CBV(12),ALT(12),CNA(12),CNB(12),XRD(14),YRD(14),
2ZRD(14),XDD(14),YDD(14),ZDD(14),RHO(14),RPO(14),RVR(14),HNV(14),
3VIN(14),VSR(14)
COMMON /FCOM/
1AMT(126),BMT(126),EMT(126),FXXMY(14),TWOEXY(14),FXZ(14),FYZ(14)
2,SPARE(70)
COMMON /HCOM/
1TON,TEN,EPS,TIN,DEL,SPC,PSA,FSA,TOJ,UPD,TOP,DTP
2,CUD,CUV,CUT,ERD,XMU,ALF,OMG,ECC,CDC,CTW,XIT(6)
COMMON /ICOM/
INBD,NTE,NHT,NSU,NPR,NPS,NOS,ICN,KTR,KDR,KVE,KOV,KSP,ISP,KIN,MPT
DATA I,L,KA,KB,KC,KOG /6*0/
DATA AU,AV,BU,BV,CU,CV,CFO,FMQ,CTH,TMR,IMS,TMT /20*0.DO/
COMMON BLOCK COMPLETED
EQUIVALENCE (TMT(1),TMA),(TMT(2),TMB),(TMT(3),TMC)
EQUIVALENCE (TMT(4),TMD),(TMT(5),TME),(TMT(6),TMF)
EQUIVALENCE (TMT(7),TMG),(TMT(8),TMH),(TMT(9),TMI)
C
C INITIALIZE ALL OF THE EXTERNAL ARRAYS.
KMAX=KVE-2
IF(KMAX.LE.0) RETURN
CSQ(1)=CGB(1)**2-0.500
SCS(1)=CGB(1)*SGB(1)
TWOMEG=OMG+OMG
K=1
I02=3
I12=ICT(1)+2
I22=ICT(2)+1
KDG=KDV-2
IF(KMAX.LT.KDG) KDG=KMAX
IF(KDG.LE.0) GO TO 100

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105030 CTH= CDC*OMG
105040 CFO=CDC*CTW
105050 HNV(I)=1.00/RPO(I)
105060 VRN(I)=1.00/VSR(I)
105070 L=9*KDG
105080 CALL CLEAR (BMT,L)
105090
105100
105110
105120
105130
105140
105150
105160
105170
105180
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C

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100 CONTINUE
FXXMY(K)= C00*UMT(I22) + C20*UMT(I22+2)
TWOXY(K)= C00*VMT(I22) + C20*VMT(I22+2)
FXZ(K) = C00*UMT(I12) + C20*UMT(I12+2)
FYZ(K) = C00*VMT(I12) + C20*VMT(I12+2)
FZZK = C00*UMT(I02) + C20*UMT(I02+2)

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C

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TMA= -0.500*FZZK
TMB= 0.00
TMC= 0.00
TMF= 0.00
KMI= K
DO 110 I= 1,K
TMA= CSQ(I)*FXXMY(KMI) - SCS(I)*TWOXY(KMI) + TMA
TMB= SCS(I)*FXXMY(KMI) + CSQ(I)*TWOXY(KMI) + TMB
TMC= CGB(I)*FXZ(KMI) - SGB(I)*FYZ(KMI) + TMC
TMF= SGB(I)*FXZ(KMI) + CGB(I)*FYZ(KMI) + TMF
110 KMI= KMI-1

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C

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L= 9*K
AMT(L) = FZZK
AMT(L-4)= -FZZK - TMA
AMT(L-8)= TMA
AMT(L-7)= TMB
AMT(L-5)= TMB
AMT(L-6)= TMC
AMT(L-2)= TMC
AMT(L-3)= TMF
AMT(L-1)= TMF
IF(KDG.LE.0) GO TO 500
CALL CLEAR(TMT,9)
KA= K-1

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310

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KDG=KDG-1
KB=KA+1

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320

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IF (KA) 350,350,320
KC=KA
DO 330 I=2,KB

```

TMA=TMA-HNV(KC)*RPO(I)	105470
TMB=TMB-VRN(KC)*VSR(I)	105480
KC=KC-1	105490
HNV(KB)=TMA*HNV(I)	105500
VRN(KB)=TMB*VRN(I)	105510
TMA=0.000	105520
TMB=0.000	105530
KC=KB	105540
DO 360 I=1,KB	105550
TMA=RVR(KC)	105560
TMB=TMB+TMA*XPO(I)	105570
TMC=TMC+TMA*YPO(I)	105580
TMD=TMD+TMA*ZPO(I)	105590
TMA=VRN(I)	105600
TME=TME+TMA*XDD(KC)	105610
TMF=TMF+TMA*YDD(KC)	105620
TMG=TMG+TMA*ZDD(KC)	105630
KC=KC-1	105640
BXB(KB)=TMB	105650
BYB(KB)=TMC	105660
BZB(KB)=TMD	105670
XVR(KB)=TME	105680
YVR(KB)=TMF	105690
ZVR(KB)=TMG	105700
TMR=-OMG*TMF	105710
TMS=OMG*TME	105720
CALL CLEAR (TMT,9)	105730
KC=KB	105740
DO 380 I=1,KB	105750
TMO=HNV(I)	105760
TMA=TMA+TMQ*BXB(KC)	105770
TMB=TMB+TMQ*BYB(KC)	105780
TMC=TMC+TMQ*BZB(KC)	105790
KC=KC-1	105800
QAV(KB)=CFO*TMA+TMR	105810
QBV(KB)=CFO*TMB+TMS	105820
QCV(KB)=CFO*TMC	105830
TMA=0.000	105840
TMB=0.000	105850
TMC=0.000	105860
KC=KB	105870
DO 400 I=1,KB	105880
AU=XRDK(KC)	105890
BU=YRDK(KC)	105900

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CU=ZRD(KC)
AV=QAV(I)
BV=QBV(I)
CV=QCV(I)
TMA=TMA+AU*AV
TMB=TMB+BU*AV
TMC=TMC+CU*AV
TMD=TMD+AU*BV
TME=TME+BU*BV
TMF=TMF+CU*BV
TMG=TMG+AU*CV
TMH=TMH+BU*CV
TMI=TMI+CU*CV
400 KC=KC-1
TMQ=CTH*RVR(KB)
TMB=TMB-TMQ
TMD=TMD+TMQ
L=9*KA+1
DO 410 I=1,9
AMT(L)=TMT(I)+AMT(L)
410 L=L+1
CALL CLEAR(TMT,9)
IF(KDG)500,500,420
420 CONTINUE
TMA=CDC*RVR(KB)
TME=TMA
TMI=4.000*TMA
KC=KB
DU 430 I=1,KB
AU=YVR(KC)
BU=ZVR(KC)
AV=XRD(I)
BV=YRD(I)
TMA=TMA+XVR(KC)*AV
TMB=TMB+AU*AV
TMC=TMC+BU*AV
TME=TME+AU*BV
TMF=TMF+BU*BV
430 KC=KC-1
TMD=TMB
TMG=TMC
TMH=TMF
TMI=TMI-TMA-TME
L=9*KA+1

```

```

105910
105920
105930
105940
105950
105960
105970
105980
105990
106000
106010
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106100
106110
106120
106130
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106200
106210
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106240
106250
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106320
106330
106340

```

```

DD 450 I=1,9
BMT(L)=TMT(I)
450 L=L+1
500 CONTINUE
IF(K.GE.KMAX) RETURN
KMI=K
TWOMGK=KMI
TWOMGK=TWOMEG/TWOMGK
K=K+1
I02= I02 + ONE
I12= I12 + ONE
I22= I22 + ONE
CSQ(K)= -SCS(KMI)*TWOMGK
SCS(K)= CSQ(KMI)*TWOMGK
GO TO 100
END

```

0192 CARDS

A-3.4 SUBROUTINE FINALP

	SUBROUTINE FINALP	137790			
	IMPLICIT REAL*8(A-H,O-Z)	137800			
C		137810			
C		137820			
C	PURPOSE TO PRINT FINAL RESULTS AND RESIDUALS	137830			
C		137840			
C		137850			
C	INPUT FILES IARCIN - ARC STABLE PARAMETERS	137860			
C	IPASIN - PASS STABLE PARAMETERS	137870			
C		137880			
C	OUTPUT FILES NONE	137890			
C		137900			
C		137910			
C		137920			
C		137930			
C	COMMON BLOCKS	137940			
C		137950			
C		137960			
C	COMMON /GENCOM/	137970			
1	CONVG,	SUM1,	137980		
2	COST,	MXDIVG,	ITERNO,	137990	
3	ITERSW,	IDIVNO,	IUNITS,	IGEOFL,	138000
4	IATOR,	IOINP,	ISIGNO,	IUPDNO,	138010
5	IPRES,	NARCS,	NSTA,	MXMEAS,	138020
6	MXARCS,	MXPARM,	MXSTA,	MXLIN,	138030
7	IPGND,	PGID(10)			138040
C					138050
C					138060
C	COMMON /TYLE/				138070
1	TITLE(100)				138080
C					138090
C					138100
C	COMMON /TSPARM/				138110
1	NOTS,	NOTS2,	TSLABL(200),	TSINT(200),	138120
2	TSCUR(200),	TSIMT(200),	TSCWT(200),	TSDELT(200),	138130
3	ITSEVL(200),	IS2LAB(200),	IS2INI(200)		138140
C					138150
C					138160
C	COMMON /ASPARM/				138170
1	NOAS,	NOAS2,	ASLABL(200),	ASINT(200),	138180
2	ASCUR(200),	ASIMT(200),	ASCNT(200),	ASDELT(200),	138190
3	IASEVL(200),	AS2LAB(200),	AS2INT(200)		138200
C					136210

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138240
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138370
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138390
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138620
138630
138640
138650

COMMON /PSPARM/
1 NCPS, NOPS2, PSLABL(200), PSINT(200),
2 PSCUR(200), PSWT(200), PSCWT(200), PSDELT(200),
3 IPSEVL(200), PS2EVL(200), PS2INT(200)

COMMON /CWORK/
1 ICATA(500), CATA(500), ICTL, NINT,
2 NFLT

COMMON /IONUMB/
1 MFILE, ISFILE, IARCIN, IPASIN,
2 IARCOT, IPASCT, ICARD, IRESID,
3 ITAPE, IALPFA, LUA, LUB,
4 LUC

COMMON /STINFO/
1 STLABL(100), STLAT(100), STLON(100), SHT(100),
2 ISTSUR(100), ISTDID(100)

COMMON /ACINFO/
1 ACLABL(100), EPOCH(100), EPOCHD(100), GHA(100),
2 IROTAT(100), IASTAB(100,6), IAPNO(100,6)

COMMON /EARTH/ ROTAT, GRHA, RADIUS, GRAV, ECC

DIMENSION XI(6), XC(6), XL(6)
DIMENSION NFLAG(3)
DATA N601/601/,NFLAG/1,2,3/,DATA2/100.00/,IX/0/,DATA3/1.020/

FORMAT STATEMENTS

5001 FORMAT(0,39X,' F I N A L R E S U L T S ')
5002 FORMAT(0,9X,' COMMENTS ',9A8,A3/, (20X,9A8,A3))
5003 FORMAT(//,10X,' NUMBER OF ITERATIONS PERFORMED ',I5)
5004 FORMAT(0,9X,' ANALYSIS TERMINATED BY ')

```

```

5005 FORMAT('+',32X,'MAXIMUM ITERATIONS') 138660
5006 FORMAT('+',32X,'CONVERGENCE') 138670
5007 FORMAT('+',32X,'DIVERGENCE') 138680
5008 FORMAT('+',32X,'MAXIMUM DIVERGENT ITERATIONS') 138690
5009 FORMAT('0',9X,'CONVERGENCE RATIO (COST FUNCTION)',F20.8) 138700
5010 FORMAT('0',9X,'PARAMETER PARAMETER',7X,'APRIORI',11X, 138710
    'CALCULATED',11X,'TCTAL',13X,'APRIORI',11X,'CALCULATED',/, 138720
1 12X,'NUMBER',6X,'LABEL',10X,'VALUE',15X,'VALUE',11X, 138730
2 'CORRECTION',11X,'SIGMA',15X,'SIGMA') 138740
3 138750
5011 FORMAT('0',4X,60(' ')) 138760
5012 FORMAT('0',35X,'TOTALLY STABLE PARAMETERS') 138770
5013 FORMAT('0',25X,'ARC STABLE PARAMETERS ARC NO.',I4,4X,A8) 138780
5014 FORMAT('0',10X,'PASS STABLE PARAMETERS ARC NO.',I4,4X, 138790
1 A8,6X,'STATION NO.',I4,4X,A8,6X,'PASS NO.',I4) 138800
5015 FORMAT('0',12X,13,7X,A8,1P,D18.8,4D19.8) 138810
5016 FORMAT('0',25X,'STATE VECTOR ARC NO.',I4,4X,A8) 138820
5017 FORMAT('0',9X,'EARTH CENTERED INERTIAL COORDINATES') 138830
5018 FORMAT('///',10X,'EARTH CENTERED FIXED COORDINATES') 138840
5019 FORMAT('0',20X,'LABEL',12X,'APRIORI',15X,'CALCULATED',I4X, 138850
1 'TOTAL',/,39X,'VALUE',18X,'VALUE',15X,'CORRECTION') 138860
5020 FORMAT('0',19X,A8,1P,3(7X,D15.8)) 138870
C 138880
C 138890
C 138900
C 138910
C 138920
C 138930
C 138940
C 138950
C 138960
C 138970
C 138980
C 138990
C 139000
C 139010
C 139020
C 139030
C 139040
C 139050
C 139060
C 139070
C 139080
C 139090

```

```

C DISPLAY COMMENTS AND COST FUNCTION, ETC

```

```

CALL PAGE
WRITE (6,5001)
WRITE (6,5002) TITLE
WRITE (6,5003) ITERNO
WRITE (6,5004)
GO TO ( 11, 12, 13, 14 ), ITERS#
GO TO 15
11 CONTINUE
WRITE (6,5006)
GO TO 15
12 CONTINUE
WRITE (6,5005)
GO TO 15
13 CONTINUE
WRITE (6,5007)
GO TO 15
14 CONTINUE
WRITE (6,5008)

```

```

139100
139110
139120
139130
139140
139150
139160
139170
139180
139190
139200
139210
139220
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139250
139260
139270
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139500
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139520
139530

15 CONTINUE
WRITE (6,5009) COST
C
C
C DISPLAY TOTALLY STABLE PARAMETER RESULTS
C
C
IF( NOTS .LE. 0 ) GC TO 30
ICNT = MXLIN + 1
NEMT=10
DO 25 I=1,NOTS
IF( ICNT .LT. MXLIN ) GC TO 22
CALL PAGE
WRITE (6,5001)
WRITE (6,5011)
WRITE (6,5012)
WRITE (6,5011)
WRITE (6,5010)
ICNT = 11
22 CONTINUE
CALL SIGWT (2,SIGI,TSIWT(I) )
CALL SIGWT(2,SIGC,TSICWT(I) )
CORR = TSCUR(I) - TSINT(I)
WRITE (6,5015) I, TSLABL(I), TSINT(I), TSCUR(I), CORR, SIGI, SIGC
C WRITE VALUES ON DISK TO UPDATE 601 CARDS
WRITE (10) N601, TSLABL(I), TSCUR(I)
ICNT = ICNT + 2
25 CONTINUE
C
C
C DISPLAY ARC STABLE PARAMETER RESULTS
C
C
30 CONTINUE
IRD = 0
C READ ARC STABLE RECORD
C
C
32 CONTINUE
READ (IARCIN,END=90C) ICIL,NINI,NELI,(IDATA(I),I=L,NINI),
1 (DATA(I),I=1,NFLT)
IF( ICTL .NE. 1 ) GC TO 32
IARC = IDATA(1)
NOAS = IDATA(2)

```

```

139540
139550
139560
139570
139580
139590
139600
139610
139620
139630
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139650
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139670
139680
139690
139700
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139720
139730
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139800
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139880
139890
139900
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139940
139950
139960
139970

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```

IF( NOAS .LE. 0 ) GC TO 60

```

```

C STORE ARC STABLE PARAMETERS

```

```

DO 34 I=1,NCAS
IASEVL(I) = IDATA(I+2)
J = 6*I - 5
ASLABL(I) = DATA(J)
ASINT(I) = DATA(J+1)
ASCUR(I) = DATA(J+2)
ASINT(I) = DATA(J+3)
ASCHT(I) = DATA(J+4)
ASDELT(I) = DATA(J+5)
34 CONTINUE

```

```

C ISOLATE AND DISPLAY STATE VECTOR

```

```

DO 350 I=1,6
J = IASTAB(IARC,I)
K = IAPNO(IARC,I)
GO TO (351,352),J
GO TO 35
351 CONTINUE
XI(I) = TSINT(K)
XC(I) = TSCUR(K)
XL(I) = TSLABL(K)
GO TO 350
352 CONTINUE
XI(I) = ASINT(K)
XC(I) = ASCUR(K)
XL(I) = ASLABL(K)
GO TO 350
350 CONTINUE

```

```

CALL PAGE

```

```

WRITE (6,5001)
WRITE (6,5011)
WRITE (6,5016) IARC,ACLABL(IARC)
WRITE (6,5011)
WRITE (6,5017)
WRITE (6,5019)
DO 354 I=1,6
CORR = XC(I) - XI(I)
WRITE (6,5020) XL(I),XI(I),XC(I),CORR

```

```

354 CONTINUE
IF( IROTAT(IARC) .LE. 0 ) GO TO 35
WRITE (6,5018)
WRITE (6,5019)
GRHA = GHA(IARC)
CALL ROTFIX(XI,EPOCH(IARC))
CALL ROTFIX(XC,EPOCH(IARC))
DO 356 I=1,6
CORR = XC(I) - XI(I)
WRITE (6,5020) XL(I), XI(I),XC(I), CORR
356 CONTINUE
C
C
35 CONTINUE
ICNT = MXLIN + 1
DO 38 I=1,NOAS
IF( ICNT .LT. MXLIN ) GC TO 36
CALL PAGE
WRITE (6,5001)
WRITE (6,5011)
WRITE (6,5013) IARC,ACLABL(IARC)
WRITE (6,5011)
WRITE (6,5010)
ICNT = 11
36 CONTINUE
CALL SIGT(2,SIGI,ASINT(I))
CALL SIGT(2,SIGC,ASCWT(I))
CORR = ASCUR(I) - ASINT(I)
WRITE (6,5015) I,ASLABL(I),ASINT(I),ASCUR(I),CORR,SIGI,SIGC
WRITE (10) N601,ASLABL(I),ASCUR(I)
WRITE ON DISK TO UPDATE 601 CARDS
ICNT = ICNT + 2
38 CONTINUE
C
C
C DISPLAY PASS STABLE PARAMETER RESULTS
140320
140330
140340
140350
140360
140370
140380
140390
140400
140410
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140690
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140980
140990
141000
141010
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141080
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141100
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141120
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141180
141190
141200
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144970
144980
144990
145000

```

```

140420 KARC = IDATA(I)
140430 ISTA = IDATA(2)
140440 IPASS = IDATA(3)
140450 NOPS = IDATA(4)
140460
140470 C STORE PASS STABLE PARAMETERS
140480 IF( NOPS .LE. 0 ) GO TO 66
140490 DO 64 I=1,NOPS
140500 IPSEVL(I) = IDATA(I+4)
140510 J = 6*I - 5
140520 PSLABL(I) = DATA(J)
140530 PSINT(I) = DATA(J+1)
140540 PSCUR(I) = DATA(J+2)
140550 PSWT(I) = DATA(J+3)
140560 PSCWT(I) = DATA(J+4)
140570 PSELT(I) = DATA(J+5)
140580 64 CONTINUE
140590
140600 C
140610 C 66 CONTINUE
140620 IF( KARC .EQ. IARC ) GO TO 70
140630 IRD = 1
140640 GO TO 32
140650
140660 C
140670 C 70 CONTINUE
140680 IF( NOPS .LE. 0 ) GO TO 62
140690 ICNT = MXLIN + 1
140700 NEMT=10
140710 DO 76 I=1,NOPS
140720 IF( ICNT .LE. MXLIN ) GO TO 74
140730 CALL PAGE
140740 WRITE (6,5001)
140750 WRITE (6,5011)
140760 WRITE (6,5014 ) IARC,ACLABL(IARC),ISTA,SILABL(ISTA),IPASS
140770 WRITE (6,5011)
140780 WRITE (6,5010)
140790 ICNT = 11
140800 74 CONTINUE
140810 CALL SIGWT(2,SIGI,PSWT(I))
140820 CALL SIGWT( 2,SIGC,PSCWT(I))
140830 CORR = PSCUR(I) - PSINT(I)
140840 WRITE (6,5015) I,PSLABL(I),PSINT(I),PSCUR(I),CORR,SIGI,SIGC
140850 MN=ISTA*2-2+I

```


WRITE (10) N601, PSLABL(1), PSCUR(1)	140860
WRITE CN DISK TO UPDATE 601 CARDS	140870
ICNT = ICNT + 2	140880
76 CONTINUE	140890
GO TO 62	140900
C	140910
C	140920
C	140930
END OF PRINT OUT	140940
C	140950
C	140960
900 CONTINUE	140970
REWIND IARCIN	140980
REWIND IPASIN	140990
C	141000
C	141010
CALL RESID	141020
C	141030
C	141040
RETURN	141050
END	

0331 CARDS

A-3.5 SUBROUTINE RESID

A-3.5.1 STANDARD SUBROUTINE RESID

LINE NO	PROGRAM NAME	COMMON BLOCKS	PURPOSE	COMPUTE	DISPLAY	AND OUTPUT MEASUREMENT RESIDUALS	ADDRESS
130840	SUBROUTINE RESID						
130850	IMPLICIT REAL*8(A-H,O-Z)						
130860	LOGICAL*1 LFILE,GRAPH,SYM,SI,BLNK,SO						
130870							
130880							
130890							
130900							
130910							
130920							
130930							
130940							
130950							
130960							
130970							
130980							
130990							
131000							
131010							
131020							
131030							
131040							
131050							
131060							
131070							
131080							
131090							
131100							
131110							
131120							
131130							
131140							
131150							
131160							
131170							
131180							
131190							
131200							
131210							
131220							
131230							
131240							
131250							
131260							

```

COMMON /ACINFO/  ACLABL(100),  EPOCH(100),  EPOCHD(100),  131270
1  GRA(100),  IROTAT(100),  IASTAB(100,6),  IAPNO(100,6)  131280
C  131290

COMMON /STINFO/  STLABL(100),  SILAT(100),  STLON(100),  131300
1  STH(100),  ISTSUR(100),  ISTSID(100)  131310
C  131320
COMMON /GENCOM/
1CONVG  ,DIVRG  ,SUMO  ,SUMI  ,  131340
2COST  ,MXITER  ,MXDIVG  ,ITERNO  ,  131350
AITERSW  ,  131360
3DIVNO  ,IUNITS  ,IGEFL  ,IAUTOR  ,  131370
4IOINP  ,ISIGND  ,IUPDNO  ,IPRRES  ,  131380
5NARCS  ,NSTA  ,MXMEAS  ,MXARCS  ,  131390
6MXPARM  ,MXSTA  ,MXLIN  ,IPGNO  ,  131400
7  PGIC(10)  ,  131410
C  131420

COMMON /CDEBUG/  IDEFLG(2),  IPRFLG(2),  ISLFLG(2)  131430
C  131440
COMMON /TYLE/  TITLE(100)  131450
C  131460
COMMON /IONUMB/  MFILE,  ISFILE,  IARCIN,  131470
1  IPASIN,  IARCCT,  IPASOT,  ICARD,  131480
2  IRESID,  ITAPE,  IALPHA  131490
C  131500
C  131510
DIMENSION XMSNA(20)
DIMENSION GRAPH(83),KI(2),SYM(2)
DATA SYM/'L','M','/','GRAPH/83*',''/
DATA SI/'I','/','BLNK/'/'/','SO/'*'/
DATA ISEQ/0/
DATA XMSNA/'RANGE  ', 'AZ COS E', 'ELEV  ', 'RA COS D',
1  'DECLIN  ', 'COS ALPHA', 'COS BETA', 'X 30  ',  131570
2  'Y 30  ', 'ALTIMETR', 'R DOT  ', 'AZ DOT  ',  131580
3  'ELEV DOT', 'X 85  ', 'Y 85  ',  131590
4  ' ', ' ', ' ', ' ', ' ', ' ',  131600
C  131610
C  131620
C  131630
C  131640
5001 FORMAT(0,20X,'M E A S U R E M E N T  R E S I D U A L S',  131650
1  19X,'ITERATION NO.',I4)  131660
5002 FORMAT(0,10X,'DESIGNATION  MEASUREMENT  MEASUREMENT',4X,  131670
1  'MEASUREMENT',13X,'ALPHA',/,'29X','LABEL',8X,'NUMBER',10X,  131680
2  'TYPE',10X,'USED')  131690
5003 FORMAT(0,10X,'DESIGNATION  MEASUREMENT  MEASUREMENT',4X,  131700

```

```

1 'MEASUREMENT',/,29X,'LABEL',8X,'NUMBER',10X,'TYPE'
131710
5004 FORMAT('0',12X,'MEAS',I2,8X,A8,8X,I4,7X,I3,'-',A8,5X,D15.8)
131720
5005 FORMAT('0',YR MO DA HR MI SEC',6X,'MEAS',I2,9X,'MEAS',I2)
131730
5006 FORMAT('0',4X,'NO. CF PCINTS',4X,F11.0,5(7X,F11.0),/,
131740
1 (15X,6F18.0) )
131750
5007 FORMAT('0',8X,'MEAN',6X,6(3X,D15.8),/, (19X,6(3X,D15.8)))
131760
5008 FORMAT('0', 'STANDARD DEVIATION',6(3X,D15.8),/, (19X,6(3X,D15.8)))
131770
5009 FORMAT('0',22X,'ARC NO.',I4,3X,A8,3X,'STATION NO.',I4,3X,A8,
131780
1 3X,'PASS NO.',I4)
131790
5010 FORMAT('0',I2,4I3,F6.2)
131800
5011 FORMAT ('+',2I,X,D12.4)
131810
5012 FORMAT ('+',35X,D12.4)
131820
5013 FORMAT ('+',57X,D15.8)
131830
5014 FORMAT ('+',75X,D15.8)
131840
5015 FORMAT ('+',93X,D15.8)
131850
5016 FORMAT ('+',111X,D15.8)
131860
5017 FORMAT(24X)
131870
5801 FORMAT('1',10X,'PREMATURE END OF FILE ENCOUNTERED ON IARCIN',,
131880
1 'PROGRAM TERMINATED')
131890
5802 FORMAT('1',10X,'PREMATURE END OF FILE ENCOUNTERED ON IPASIN',,
131900
1 'PROGRAM TERMINATED')
131910
131920
131930
131940
131950
131960
131970
131980
131990
132000
132010
132020
132030
132040
132050
132060
132070
132080
132090
132100
132110
132120
132130
132140

```

INITIALIZATION

```

REWIND ISFILE
REWIND IARCIN
REWIND IPASIN
REWIND IALPHA
REWIND IRESID
REWIND IARCOT

```

CLEAR ALL STORAGE AREAS

```

DO 5 I=1,NSIZEM
NBL(I) = 0
NBL(I) = 0
CMW(I) = 0.00
EPS(I) = 0.00
EPSL(I) = 0.00
AUTOR(I) = 0.00
ASUM(I) = 0.00
APROD(I) = 0.00
ANUMB(I) = 0.00
NMSNC(I) = 0

```

```

DO      5 J=1, NSIZEB
NBP(I,J) = 0.00
NBPL(I,J) = 0.00
B(I,J) = 0.00
BL(I,J) = 0.00
5 CONTINUE
COVAR=0.00
C
C
LFILS=.FALSE.
GRAPH(42)=SI
C SET FLAGS FOR 1ST ARC + PASS
IASOLN = 0
IPSO LN = 0
C
C READ CONTROL FILE
C
C 100 CONTINUE
READ (ISFILE,END=400)ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),
I (DATA(I),I=1,NFLT)
C
C GO TO ( 1000, 2000, 3000 ), ICTL
GO TO 100
C
C BEGINNING OF AN ARC
C
C 1000 CONTINUE
C
C TEST FOR FIRST ARC
IF(IASOLN.NE.0) GO TO 1002
IASCLN = 1
GO TO 1010
C
C GO TO PRINT STATISTICS ROUTINE .
C
1002 CONTINUE
ISTAT = 1
GO TO 6000
C
1004 CONTINUE
C
C READ + STORE ARC PARAMETERS
C

```

```

132150
132160
132170
132180
132190
132200
132210
132220
132230
132240
132250
132260
132270
132280
132290
132300
132310
132320
132330
132340
132350
132360
132370
132380
132390
132400
132410
132420
132430
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132450
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132480
132490
132500
132510
132520
132530
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132550
132560
132570
132580

```

```

132590 1010 CONTINUE
132600 IARC = IDATA(I)
132610 1012 CONTINUE
132620 READ (IARCIN,END=4100) ICIL,NINI,NFLI,(IDATA(I),I=1,NINI),
132630 I (DATA(I),I=1,NFLI)
132640 C
132650 C IF NOT TYPE 1 RECORD, READ AGAIN
132660 IF(ICIL.NE.1) GO TO 1012
132670 C
132680 C STORE PARAMETERS
132690 NOAS = IDATA(2)
132700 KARC = IDATA(1)
132710 C
132720 C SET FLAGS FOR FIRST PASS OF AN ARC
132730 IPSCN = 0
132740 IF( NOAS.LE.0) GO TO 1018
132750 DO 1016 I=1,NOAS
132760 IASEVL(I) = IDATA(I+2)
132770 J = 6*I - 5
132780 ASLABL(I) = DATA(J)
132790 ASIN(I) = DATA(J+1)
132800 ASCUR(I) = DATA(J+2)
132810 ASWT(I) = DATA(J+3)
132820 ASCWT(I) = DATA(J+4)
132830 ASDEL(I) = DATA(J+5)
132840 1016 CONTINUE
132850 1018 CONTINUE
132860 GO TO 100
132870 C
132880 C
132890 C BEGINNING OF A PASS
132900 C
132910 C
132920 2000 CONTINUE
132930 C
132940 C IF NOT FIRST PASS OF AN ARC, PRINT STATISTICS FROM LAST PASS
132950 IF( IPSCN.NE.0) GO TO 2002.
132960 IPSCN = 1
132970 GO TO 2008
132980 2002 CONTINUE
132990 ISTAT = 2
133000 GO TO 6000
133010 2004 CONTINUE
133020 C

```



```

C STORE MEASUREMENT INFO FOR THIS PASS 133030
C 2008 CONTINUE 133040
KARC = IDATA(1) 133050
ISTA = IDATA(2) 133060
IPASS = IDATA(3) 133070
NMEAS = IDATA(4) 133080
DO 2010 I=1,NMEAS 133090
NMSNO(I) = IDATA(I+4) 133100
CMW(I) = DATA(I) 133110
2010 CONTINUE 133120
133130
133140
C IF FINAL PRINT AND AUTOREGRESSIVE CONSTANTS USED, READ IALPHA 133150
C AND SCORE CONSTANTS 133160
C 133170
IF ((ITERSW .EQ. 0) .OR. 133180
1 (IAUTOR .NE. 0)) GO TO 2020 133190
READ (IALPHA) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT), 133200
1 (CATA(I),I=1,NFLT) 133210
DO 2016 I=1,NMEAS 133220
DO 2014 J=1,NMEAS 133230
IF( IDATA(I+4) .NE. NMSNO(J)) GO TO 2014 133240
AUTOR(J) = DATA(I) 133250
GO TO 2016 133260
2014 CONTINUE 133270
2016 CONTINUE 133280
C 133290
C READ PASS STABLE PARAMETERS 133300
C 133310
2020 CONTINUE 133320
READ (IPASIN,END=41C1) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT), 133330
1 (CATA(I),I=1,NFLT) 133340
IF( ICTL .NE. 1 ) GC TO 2020 133350
C 133360
C STORE PARAMETER VALUES FROM TYPE 1 RECORD 133370
JARC = IDATA(1) 133380
JSTA = IDATA(2) 133390
JPASS = IDATA(3) 133400
NOPS = IDATA(4) 133410
IF(NOPS .LE. 0 ) GC TO 2030 133420
DO 2024 I=1,NOPS 133430
IPSEVL(I) = IDATA(I+4) 133440
J = 6*I - 5 133450
PSLABL(I) = DATA(J) 133460

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```

133470 PSINT(I) = DATA(J+1)
133480 PSCUR(I) = DATA(J+2)
133490 PSWT(I) = DATA(J+3)
133500 PSCWT(I) = DATA(J+4)
133510 PSDELT(I) = DATA(J+5)
2024 CONTINUE
C
C PRINT HEADINGS AND MEASUREMENT LEGEND
C
2030 CONTINUE
CALL PAGE
WRITE (6,5001) ITERN0
WRITE (6,5009) JARC,ACLABL(IARC),ISTA,STLABL(ISTA),IPASS
IF ((ITERSW .NE. 0) .AND.
1 (IAUTOR .EQ. 0)) GO TO 2036
C
C NO AUTOREGRESSIVE CONSTANTS PRINTED
C
WRITE (6,5003)
DO 2034 I=1,NMEAS
WRITE (6,5004) I, XMLABL(NMSNO(I)),NMSNO(I),MSTYPE(NMSNO(I)),
1 XMSNA(MSTYPE(NMSNO(I)))
2034 CONTINUE
GO TO 2040
C
C PRINT ALPHAS Y00
C
2036 CONTINUE
WRITE (6,5002)
DO 2038 I=1,NMEAS
WRITE (6,5004) I, XMLABL(NMSNO(I)),NMSNO(I),MSTYPE(NMSNO(I)),
1 XMSNA(MSTYPE(NMSNO(I))),AUTOR(I)
2038 CONTINUE
C
C
2040 CONTINUE
WRITE (6,5005) (I,I=1,NMEAS)
ICNT = 10 + 2 *NMEAS
GO TO 100
C
C MEASUREMENT POINT RECORD
C
3000 CONTINUE
C

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133470
133480
133490
133500
133510
133520
133530
133540
133550
133560
133570
133580
133590
133600
133610
133620
133630
133640
133650
133660
133670
133680
133690
133700
133710
133720
133730
133740
133750
133760
133770
133780
133790
133800
133810
133820
133830
133840
133850
133860
133870
133880
133890
133900

```

```

C CHECK FOR PAGE OVERFLOW 133910
IF(ICNT.LT.MXLIN) GO TO 3002 133920
CALL PAGE 133930
WRITE (6,5001) ITERNO 133940
WRITE (6,5009) IARC,ACLABL(IARC),ISTA,STLABL(ISTA),IPASS 133950
WRITE (6,5005) (I,I=1,NMEAS) 133960
ICNT = 7 133970
3002 CONTINUE 133980
C 133990
C CONVERT DAYS + TIME TO YR,MON,DAY,HR,MIN,SEC + DISPLAY 134000
CALL DAYHMS(DATA(1),DATA(2),IYR,IMO,IDA,IHR,IMIN,SEC) 134010
WRITE (6,5010) IYR,IMO,IDA,IHR,IMIN,SEC 134020
134030
C 134040
C PROCESS THE MEASUREMENT POINT RECORD 134050
C 134060
C CLEAR STORAGE AREAS 134070
DO 3004 I=1,NSIZEM 134080
EPS(I) = 0.00 134090
RES(I) = 0.00 134100
NB(I) = 0 134110
IWORK(I) = 0 134120
DO 3004 J=1,NSIZED 134130
B(I,J) = 0 134140
134150
3004 CONTINUE 134160
C 134170
C STORE MEASUREMENT DISCREPANCIES 134180
NMSPT = IDATA(1) 134190
NPAR = IDATA(2) 134200
DO 3008 I=1,NMSPT 134210
DO 3006 J=1,NMEAS 134220
IF(ICATA(I+2).NE.NMSNC(J)) GO TO 3006 134230
IWORK(J) = NMSNC(J) 134240
EPS(J) = DATA(I+2) 134250
GO TO 3008 134260
3006 CONTINUE 134270
C NO MATCH ERROR 134280
3008 CONTINUE 134290
C 134300
C STORE PARTIALS BY MEASUREMENT NO INDICATOR 134310
IF(NPAR.LE.0) GO TO 2016 134320
DO 3012 I=1,NPAR 134330
CALCULATE PARAMETER NO 134340
IPNC = IDATA(I*3+NMSPT +1)

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```

134350 ITY = IDATA(I*3+NMSPT)
134360 MNO = IOATA(I*3+NMSPT+2)
134370 IF( ITY .GE. 2 ) IPNO = IPNO + NOTS
134380 IF( ITY .EQ. 3 ) IPNO = IPNO+NOAS
134390 C
134400 FIND MEAS NO INDICATOR
134410 DO 3010 J=1,NMEAS
134420 IF( MNO .NE. NMSNO(J) ) GO TO 3010
134430 N8(J) = N8(J) + 1
134440 B(J,N8(J)) = DATA(NMSPT+I+2)
134450 NBP(J,N8(J)) = IPNO
134460 GO TO 3012
134470 3010 CONTINUE
134480 C NO MATCH ERROR
134490 C
134500 3012 CONTINUE
134510 C
134520 CALCULATE RESIDUALS AND DISPLAY
134530 C OUTPUT RESIDUALS IF FINAL CALL TO RESID
134540 C
134550 3016 CONTINUE
134560 DO 3036 I=1,NMEAS
134570 SKIP TO NEXT LINE IF LINE IS FULL
134580 J = I/6*6 + 1
134590 IF( I.NE.1).AND.(I.EQ.J)) WRITE(6,5017)
134600 IF( EPS(I) .EQ. 0.DC ) GO TO 3036
134610 E = EPS(I)
134620 CHECK FOR USE OF AUTOREGRESSIVE CONSTANTS
134630 IF( (ITERSW .NE. 0).AND. (IAUTOR.EQ. 0)) E = E - AUTOR(I)*EPSL(I)
134640 RES(I) = E
134650 C
134660 IF NO PARTIALS, DISPLAY AND GO TO NEXT MEAS
134670 IF( NB(I) .LE. 0 ) GO TO 3034
134680 NPARS = NB(I)
134690 DO 3032 J=1,NPARS
134700 BI = B(I,J)
134710 CHECK FOR USE OF AUTOREGRESSIVE CONSTANTS
134720 IF( (ITERSW .NE. 0).AND. (IAUTOR.EQ. 0)) BI = BI - AUTOR(I)*BL(I,J)
134730 IPNO = NBP(I,J)
134740 IF( IPNO .GT. NOTS ) GO TO 3020
134750 RES(I) = RES(I) - TSDDEL(I,IPNO) * BI
134760 GO TO 3032
134770 3020 CONTINUE
134780 IPNO = IPNO - NOTS
134790 IF( IPNO .GT. NOAS ) GO TO 3022
134800 RES(I) = RES(I) - ASDEL(I,IPNO) * BI
134810 GO TO 3032

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```

3022 CONTINUE
IPNC = IPNO - NOAS
RES(I) = RES(I) - PSELT(IPNO) * B1
134790
134800
134810
134820
134830
134840
134850
134860
134870
134880
134890
134900
134910
134920
134930
134940
134950
134960
134970
134980
134990
135000
135010
135020
135030
135040
135050
135060
135070
135080
135090
C
C
ACD TO COUNTS, SUMS, PRODUCTS
ANUMB(I) = ANUMB(I) + 1.00
ASUM(I) = ASUM(I) + RES(I)
APROD(I)=APROD(I)+RES(I)*#2
135100
135110
135120
135130
135140
135150
135160
135170
135180
135190
135200
135210
135220
3026 CONTINUE
GO TO (3041,3042,3043,3044,3045,3046),J
3041 CONTINUE
WRITE (6,5011) RES(I)
GO TO 3050
3042 CONTINUE
WRITE (6,5012) RES(I)
GO TO 3050
3043 CONTINUE
WRITE (6,5013) RES(I)
GO TO 3050
3044 CONTINUE
WRITE (6,5014) RES(I)
GO TO 3050
3045 CONTINUE
WRITE (6,5015) RES(I)
GO TO 3050
3046 CONTINUE
WRITE (6,5016) RES(I)
3050 CONTINUE
C
C
COVAR=COVAR + RES(I)* RES(I)
DO 3090 I=1,2
IF (RES(I)) 3070,3070,3080
3070 KK=(RES(I)-.05D-04)/(-.2D-04)
IF (KK .GT. 40) KK=41
GRAPH (42-KK)=SYM(I)
KI(I)=42-KK
GO TO 3090

```

```

3080 KK=(RES(I)+.05D-04)/.2D-04      135230
IF (KK .GT. 40) KK=41              135240
GRAPH(42+KK)=SYM(I)                 135250
KI(I)=42+KK                          135260
3090 CONTINUE                        135270
IF (KI(I) .NE. KI(2)) GC TO 3095    135280
GRAPH(KI(I))=S0                      135290
3095 WRITE (6,3091) GRAPH           135300
3091 FORMAT ('+',49X,83A1)          135310
GRAPH(KI(I))=BLNK                   135320
GRAPH(KI(2))=BLNK                   135330
IF (KI(I) .EQ. 42) GRAPH(42)=SI     135340
IF (KI(2) .EQ. 42) GRAPH(42)=SI     135350
ICNT = ICNT + (NMEAS+5)/6           135360
C                                     135370
C IF FINIAL CALL TO RESID, QIUTP RESIDUALS 135380
C                                     135390
IF( ITERSW .EQ. 0 ) GO TO 3060      135400
C                                     135410
ICTL = 1                             135420
NINT = NMEAS + 4                    135430
NFLT = NMEAS + 2                    135440
C WRITE(IRESID) ICTL,NINT,NFLT,IARC,ISTA,IPASS,NMEAS, 135450
C * (IWORK(I),I=1,NMEAS),DATA(1),DATA(2),(RES(I),I=1,NMEAS) 135460
C                                     135470
C IF USING AUTOREGRESSIVE CONSTANTS MOVE CURRENT VALUES TO PREVIOUS 135480
3060 CONTINUE                        135490
IF(IITERSW.EQ.0).OR.(IAUTOR.NE.0)) GO TO 100 135500
DO 3066 I=1,NSIZEM                  135510
NBL(I) = NB(I)                      135520
EPSL(I) = EPS(I)                    135530
DO 3066 J=1,NSIZEB                  135540
BL(I,J) = B(I,J)                   135550
NBP(I,J) = NBP(I,J)                 135560
3066 CONTINUE                        135570
GO TO 100                            135580
C                                     135590
C                                     135600
C DISPLAY RESIDUAL STATISTICS       135610
C                                     135620
C                                     135630
6000 CONTINUE                        135640
WRITE (6,5006) (ANUMB(I),I=1,NMEAS) 135650
C COMPUTE MEAN AND STANDARD DEVIATION 135660

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135670 GO 6004 I=1,NMEAS
135680 IF( ANUMB(I) .LE. 1.00 ) GO TO 6002
135690 APRCD(I) = DSQRT((APROD(I)-ASUM(I)**2/ANUMB(I))/(ANUMB(I)-1.00))
135700 ASUM(I) = ASUM(I)/ANUMB(I)
135710 GO TO 6004
135720 6002 APROD(I) = 0.00
135730 6004 CONTINUE
135740 WRITE (6,5007) (ASUM(I),I=1,NMEAS)
135750 WRITE (6,5008) (APROD(I),I=1,NMEAS)
135760 IF (ANUMB(I) .LE. 1.00) SCV=0.00
135770 IF (ANUMB(I) .GT. 1.00) SCV= (COVAR-ANUMB(I)*ASUM(2))/
135780 ((ANUMB(I)-1.00)*APROD(I)*APROD(2))
135790 * WRITE (6,8000) SCV
135800 8000 FORMAT (0,'CORRELATION COEFFICIENT',3X,F6.2)
135810 C WRITE RESIDUALS ON SUMMARY FILE
135820 9000 FORMAT (1H,30X,'M E A S U R E M E N T R E S I D U A L S U M M A
135830 *R,Y'//)
135840 9002 FORMAT (3X,'STATION',6X,'ARC PASS YR MO DAY HR MIN SEC',17X,
135850 'MEAN',22X,'STANDARD DEVIATION',9X,'CORRELATION',/
135860 2X,'NO. NAME',45X,'MEAS 1',11X,'MEAS 2',11X,'MEAS 1',
135870 11X,'MEAS 2',5X,'COEFFICIENT'//)
135880 IF (LFILE) GO TO 9050
135890 LFILE =.TRUE.
135900 WRITE (34,9000)
135910 WRITE (34,9002)
135920 9001 FORMAT (1X,13,3X,A8,3(2X,13),213,15,13,1X,F5.2,1X,4(D15.8,2X),
135930 F7.2)
135940 9050 WRITE (34,9001) ISTA,STLABL(ISTA),IARC,IPASS,
135950 IYR,IMO,IDA,IHR,IMIN,SEC
135960 ASUM(1),A UM(2),APROD(1),APROD(2) ,SCV
135970 C WRITE ON DISK TO BE USED BY SUMMARY PRINT PROGRAM
135980 C C OUTPUT : MEAS 2 LABEL, MEAS 2 NO.,CORRELATION COEFFICIENT,
135990 MEAN 1, STD DEV 1, MEAN2, STD DEV 2
136000 WRITE (10) XMLABL(NMSNO(2)),NMSNO(2),SCV,ANUMB(2),ASUM(1),
136010 APROD(1),ASUM(2),APROD(2)
136020 C
136030 IF( ITERSW .EQ. 0 ) GO TO 6010
136040 IC = 1
136050 NI = 4 + NMEAS
136060 NF = 3 * NMEAS
136070 WRITE (IARCOT) IC,NI,NF,IARC,ISTA,IPASS,NMEAS,(NMSNO(I),I=1,NMEAS)
136080 I , (ANUMB(I),ASUM(I),APROD(I),I=1,NMEAS)
136090 6010 CONTINUE
136100 C

```


WRITE (6,5802)

GO TO 4103

END

136550

136560

136570

0576 CARDS

A-3.5.2 SPECIAL SUBROUTINE RESID

SUBROUTINE RESID 130840
 IMPLICIT REAL*8(A-H,O-Z) 130850
 LOGICAL*1 LFILE,GRAPH,SYM,SI,BLNK,SO 130860
 130870
 130880
 130890
 130900
 130910
 130920
 130930

PURPOSE COMPUTE, DISPLAY, AND OUTPUT MEASUREMENT RESIDUALS

COMMON BLOCKS
 COMMON /COMSOL/ U(110,110), C(110), AUTOR(20), 130950
 ASUM(20), APR00(20), ANUMB(20), CMN(20),
 EPSL(20), B(20,40), BL(20,40), 130960
 RES(20), E1, B2,
 Z, TIME, DAYS, WT,
 DIS, SIG, TEST, 130980
 130990
 131000
 131010
 131020
 131030
 131040
 131050
 131060
 131070
 131080
 131090

COMMON /TSPARM/ NOTS2, TSLABL(200), 131100
 TSINT(200), TSWT(200), TSCWT(200), 131110
 TSDEL(200), TSEVL(200), TS2LAB(200), TS2INT(200) 131120
 131130

COMMON /ASPARM/ N0AS2, ASLABL(200), 131140
 ASINT(200), ASCUR(200), ASIWT(200), ASCWT(200), 131150
 ASDEL(200), IASEVL(200), AS2LAB(200), AS2IWT(200) 131160
 131170

COMMON /PSPARM/ N0PS2, PSLABL(200), 131180
 PSINT(200), PSCUR(200), PSIWT(200), PSCWT(200), 131190
 PSDEL(200), IPSEVL(200), PS2LAB(200), PS2IWT(200) 131200
 131210

COMMON /CWORK/ IDATA(500), DATA(500), ICTL, 131220
 NINT, NFLT 131230
 131240

COMMON /MSINFO/ XMLABL(300), MSTYPE(300) 131250
 131260
 COMMON /ACINFO/ ACLABL(100), EPOCH(100), EPOCHD(100), 131270

```

C      1   GHA(100),      IROTAT(100),      IASTAB(100,6),      IAPND(100,6)      131280
      131290
      COMMON /STINFO/      STLABL(100),      STLAT(100),      STLON(100),      131300
      1   SHTT(100),      ISTSUR(100),      ISTSID(100)      131310
      131320
      COMMON /GENCOM/
      1CONVG      ,DIVRG      ,SUMI      ,131330
      2COST      ,MXITER      ,MXDIVG      ,ITERNO      ,131340
      AITERSW
      3DIDVNO      ,IUNITS      ,IGEOfL      ,IAUTOR      ,131360
      4IOINP      ,ISIGNO      ,IUPDNO      ,IPRRES      ,131370
      5NARCS      ,NSTA      ,MXMEAS      ,MXARCS      ,131380
      6MXPARM      ,MXSTA      ,MXLIN      ,IPGNO      ,131390
      7      PGID(10)      131400
      131410
      131420
      COMMON /CDEBUG/      IDEFLG(2),      IPRFLG(2),      ISLFLG(2)      131430
      131440
      COMMON /TYLE/      TITLE(100)      131450
      131460
      COMMON /IONUMB/      MFILE,      ISFILE,      IARCIN,      131470
      1   IPASIN,      IARCOT,      IPASOT,      ICARD,      131480
      2   IRESID,      ITAPE,      IALPHA      131490
      131500
      131510

      DIMENSION ADUM(6)
      DIMENSION XMSNA(20)
      DIMENSION GRAPH(83),KI(2),SYM(2)
      DATA SYM/'L','M','/',GRAPH/83*'/
      DATA SI/'I','BLNK/'/'/,'SO/'*'/
      DATA ISEQ/0/
      DATA XMSNA/'RANGE',      'AZ COS E','ELEV',      'RA COS D',      131520
      'DECLIN',      'COS ALPHA',      'COS BETA',      'X 30',      131530
      'Y 30',      'ALTIMETR',      'R DOT',      'AZ DOT',      131540
      'ELEV DOT',      'X 85',      'Y 85',      131550
      131560
      131570
      131580
      131590
      131600
      131610
      131620
      131630
      131640

      C      FORMAT STATEMENTS
      C
      C      9001  FORMAT ( I4, IX, A8, I4, 2I3, I4, I3, F7.3, I5, 20I4.5,
      *      20I2.3, I8, I5)
      C      9002  FORMAT ( 79X 'STANDARD' /
      1   52X 'MEAN ERROR' 16X 'DEVIATION' 11X 'NO. PTS.' /
      2   2X 'STATION' 29X 'PASS' 6X 'MEAS' 10X 'MEAS' 9X 'MEAS' /
      3   8X 'MEAS' 7X 'MEAS MEAS' /

```

```

4 2X 'NO NAME' 6X 'Y M D H M SEC NO' 8X '1. 13X '2'
5 12X '1' 11X '2' 11X '1 2' ///)
5001 FORMAT(0',10X,'M E A S U R E M E N T R E S I D U A L S',
* 10X,'ARC',13,10X,'ITERATION',I4//)
5017 FORMAT(24X)
5801 FORMAT(1',10X,'PREMATURE END OF FILE ENCOUNTERED ON IARCIN,',
1 'PROGRAM TERMINATED')
5802 FORMAT(1',10X,'PREMATURE END OF FILE ENCOUNTERED ON IPASIN,',
1 'PROGRAM TERMINATED')

```

131870
131880
131890
131900
131910
131920
131930
131940
131950
131960
131970
131980
131990
132000
132010

```

INITIALIZATION
REWIND ISFILE
REWIND IARCIN
REWIND IPASIN
REWIND IALPHA
REWIND IRESID
REWIND IARCOT
NUTAPE=35
NUPASS=36
NURITE=37
END FILE NURITE
IF(ITERSW.EQ.0) GO TO 4
REWIND 10

```

```

3 READ(10,END=4) N,X,Y
WRITE(NURITE) N,X,Y
GO TO 3
4 REWIND 10

```

132020
132030
132040
132050
132060
132070
132080
132090
132100
132110
132120
132130
132140
132150
132160

```

CLEAR ALL STORAGE AREAS
DO 5 I=1,NSIZEM
NB(I) = 0
NBL(I) = 0
CMW(I) = 0.00
EPS(I) = 0.00
EPSL(I) = 0.00
AUTOR(I) = 0.00
ASUM(I) = 0.00
APROD(I) = 0.00
ANUMB(I) = 0.00
NMSNO(I) = 0
DO 5 J=1,NSIZESB
NBP(I,J) = 0.00

```

```

NBPL(I,J) = 0.00
B(I,J) = 0.00
BL(I,J) = 0.00
5 CONTINUE
COVAR=0.00
C
C
LFILE=.FALSE.
GRAPH(42)=SI
SET FLAGS FOR 1ST ARC + PASS
IASOLN = 0
IPSOLN = 0
C
C READ CONTROL FILE
C
C 100 CONTINUE
READ (ISFILE,END=400) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),
1 (DATA(I),I=1,NFLT)
C
GO TO ( 1000, 2000, 3000 ), ICTL
GO TO 100
C
C BEGINNING OF AN ARC
C
C 1000 CONTINUE
C
ICNT=MXLIN
IARC = IDATA(I)
1012 CONTINUE
READ (IARCIN,END=4100) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),
1 (DATA(I),I=1,NFLT)
C
IF NOT TYPE 1 RECORD,READ AGAIN
IF(ICTL .NE. 1 ) GO TO 1012
C
C STORE PARAMETERS
NOAS = IDATA(2)
KARC = IDATA(1)
C
C SET FLAGS FOR FIRST PASS OF AN ARC
IPSOLN = 0

```

132170

132180

132190

132200

132210

132220

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132240

132250

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132270

132280

132290

132300

132310

132320

132330

132340

132350

132360

132370

132380

132390

132400

132410

132420

132430

132440

132450

132600

132610

132620

132630

132640

132650

132660

132670

132680

132690

132700

132710

132720

132730

```

IF( NOAS .LE. 0) GO TO 1018
DO 1016 I=1,NOAS
IASEVL(I) = IDATA(I+2)
J = 6*I - 5
ASLABL(I) = DATA(J)
ASINT(I) = DATA(J+1)
ASCUR(I) = DATA(J+2)
ASIW(I) = DATA(J+3)
ASCWT(I) = DATA(J+4)
ASDELT(I) = DATA(J+5)
1016 CONTINUE
1018 CONTINUE
GO TO 100
C
C
C
C
C
C
2000 CONTINUE
STORE MEASUREMENT INFO FOR THIS PASS
C
C
2008 CONTINUE
KARC = IDATA(1)
ISTA = IDATA(2)
IPASS = IDATA(3)
NMEAS = IDATA(4)
DO 2010 I=1,NMEAS
NMSNO(I) = IDATA(I+4)
CMW(I) = DATA(I)
2010 CONTINUE
C
C
C
C
READ PASS STABLE PARAMETERS
C
2020 CONTINUE
READ (IPASIN,END=4101) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),
1 (DATA(I),I=1,NFLT)
IF( ICTL .NE. 1 ) GO TO 2020
C
C
STORE PARAMETER VALUES FROM TYPE 1 RECORD
JARC = IDATA(1)
JSTA = IDATA(2)
JPASS = IDATA(3)
NOPS = IDATA(4)

```

132740

132750

132760

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132780

132790

132800

132810

132820

132830

132840

132850

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132870

132880

132890

132900

132910

132920

133030

133040

133050

133060

133070

133080

133090

133100

133110

133120

133130

133140

133290

133300

133310

133320

133330

133340

133350

133360

133370

133380

133390

133400

133410

```

IF(NOPS .LE. 0 ) GO TO 100
DO 2024 I=1,NOPS
IPSEVL(I) = IDATA(I+4)
J = 6*I - 5
PSLABL(I) = DATA(J)
PSINT(I) = DATA(J+1)
PSCUR(I) = DATA(J+2)
PSINT(I) = DATA(J+3)
PSCWT(I) = DATA(J+4)
PSDEL(I) = DATA(J+5)
2024 CONTINUE
C
GO TO 100
C
MEASUREMENT POINT RECORD
C
3000 CONTINUE
C
CHECK FOR PAGE OVERFLOW
IF(ICNT .LT. MXLIN ) GO TO 3002
CALL PAGE
WRITE(6,5001) IARG,ITERNO
WRITE(6,9002)
ICNT = 7
3002 CONTINUE
C
CONVERT DAYS + TIME TO YR,MON,DAY,HR,MIN,SEC + DISPLAY
CALL DAYHMS(DATA(1),DATA(2),IYR,IMO,IDA,IHR,IMIN,SEC)
PROCESS THE MEASUREMENT POINT RECORD
C
CLEAR STORAGE AREAS
DO 3004 I=1,NSIZEM
EPS(I) = 0.00
RES(I) = 0.00
NB(I) = 0
IWORK(I) = 0
DO 3004 J=1,NSIZEB
B(I,J) = 0
3004 CONTINUE
C
STORE MEASUREMENT DISCREPANCIES

```

133430
133440
133450
133460
133470
133480
133490
133500
133510
133520
133530
133830
133840
133850
133860
133870
133880
133890
133900
133910
133920
133930

133970
133980
133990
134000
134010
134030
134040
134050
134060
134070
134080
134090
134100
134110
134120
134130
134140
134150
134160

C6


```

NMSPT = IDATA(1) 134170
NPAR = IDATA(2) 134180
DO 3008 I=1,NMSPT 134190
DO 3006 J=1,NMEAS 134200
IF(IDATA(I+2) .NE. NMSNO(J) ) GO TO 3006 134210
IWORK(J) = NMSNO(J) 134220
EPS(J) = DATA(I+2) 134230
GO TO 3008 134240
CONTINUE 134250
C NO MATCH ERROR 134260
3006 CONTINUE 134270
3008 CONTINUE 134280
C
C STORE PARTIALS BY MEASUREMENT NO INDICATOR 134290
C 134300
IF(NPAR .LE. 0 ) GO TO 3016 134310
DO 3012 I=1,NPAR 134320
CALCULATE PARAMETER NO 134330
IPNO = IDATA(I*3+NMSPT +1) 134340
ITY = IDATA(I*3+NMSPT) 134350
MNO = IDATA(I*3+NMSPT+2) 134360
IF( ITY .GE. 2 ) IPNO = IPNO + NOTS 134370
IF( ITY .EQ. 3 ) IPNO = IPNO+NOAS 134380
FIND MEAS NO INDICATOR 134390
DO 3010 J=1,NMEAS 134400
IF( MNO .NE. NMSNO(J) ) GO TO 3010 134410
NB(J) = NB(J) + 1 134420
B(J,NB(J)) = DATA(NMSPT+I+2) 134430
NBP(J,NB(J)) = IPNO 134440
GO TO 3012 134450
CONTINUE 134460
3010 CONTINUE 134470
C NO MATCH ERROR 134480
3012 CONTINUE 134490
C
C CALCULATE RESIDUALS AND DISPLAY 134500
C OUTPUT RESIDUALS IF FINAL CALL TO RESID 134510
C 134520
CONTINUE 134530
DO 3036 I=1,NMEAS 134540
SKIP TO NEXT LINE IF LINE IS FULL 134550
J = I/6*6 + 1 134560
IF((I.NE.1).AND.(I.EQ.J)) WRITE(6,5017) 134570
IF( EPS(I) .EQ. 0.DO ) GO TO 3036 134580
E = EPS(I) 134590
C CHECK FOR USE OF AUTOREGRESSIVE CONSTANTS 134600

```

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IF((ITERSW .NE.0).AND.(IAUTOR.EQ.0)) E = E - AUTOR(I)*EPSL(I)
RES(I) = E
134610
134620
C IF NO PARTIALS, DISPLAY AND GO TO NEXT MEAS
134630
IF( NB(I) .LE. 0 ) GO TO 3034
134640
NPARS = NB(I)
134650
DO 3032 J=1,NPARS
134660
BI = B(I,J)
134670
CHECK FOR USE OF AUTOREGRESSIVE CONSTANTS
134680
IF((ITERSW .NE.0).AND.(IAUTOR.EQ.0)) BI = BI -AUTOR(I)*BL(I,J)
134690
IPNO = NBP(I,J)
134700
IF( IPNO .GT. NOTS ) GO TO 3020
134710
RES(I) = RES(I) - TSDELTA(IPNO) * BI
134720
GO TO 3032
134730
3020 CONTINUE
134740
IPNO = IPNO - NOTS
134750
IF( IPNO .GT. NOAS ) GO TO 3022
134760
RES(I) = RES(I) - ASDELTA(IPNO) * BI
134770
GO TO 3032
134780
3022 CONTINUE
134790
IPNO = IPNO - NOAS
134800
RES(I) = RES(I) - PSDELTA(IPNO) * BI
134810
3032 CONTINUE
134820
C PRINT CALCULATED RESIDUALS
134830
3034 CONTINUE
134840
3036 CONTINUE
READ(NUPASS) NOSTA,NOPASS,L1,L2,SIGMA1,SIGMA2
WRITE(6,9001) ISTA,STLABL(ISTA),IYR,IMD,IDA,IHR,IMIN,SEC,IPASS,
* RES(1),RES(2),SIGMA1,SIGMA2,L1,L2
IF((ITERSW.NE.0) WRITE(NURITE) XMLABL(NMSNO(2)),NMSNO(2),L1,L2,
* XMLABL(NMSNO(1)),RES(1),SIGMA1,RES(2),SIGMA2
ICNT= ICNT+1
CLEAR ARRAYS
136110
DO 6008 I=1,NSIZEM
136120
NMSNO(I) = 0
136160
NBL(I) = 0
136170
DO 6008 J= 1,NSIZEB
136180
BL(I,J) = 0.00
136190
NBPL(I,J) =0
136200
6008 CONTINUE
136210
GO TO 100
136230
C
136270
C
136280
C
136290

```

136300
136380
136390
136400
136410

4000 CONTINUE
REWIND ISFILE
REWIND IARCIN
REWIND IPASIN
REWIND IALPHA
REWIND NUPASS
IF(ITERSW.EQ.0) RETURN
END FILE NURITE
4010 READ(NUTAPE,END=4020) ADUM
WRITE(NURITE) ADUM
GO TO 4010
4020 REMIND NURITE
RETURN

C 136450
C 136460
C 136470
C 136480
C 136490
C 136500
C 136510
C 136520
C 136530
C 136540
C 136550
C 136560
C 136570

PREMATURE END OF FILE - IARCIN - ERROR
CONTINUE
WRITE (6,5801)
CONTINUE
STOP
PREMATURE END OF FILE - IPASIN - ERROR
CONTINUE
WRITE (6,5802)
GO TO 4103
END

0378 CARDS

A-3.6 SPECIAL SUBROUTINE PRTIAL

	70980
SUBROUTINE PRTIAL	
IMPLICIT REAL*8 (A-H,O-Z)	70990
LOGICAL*1 ELEVOK,IEND	
	71000
VERSION OF 12/05/68 FOR THE NETWORK ANALYSIS PROGRAM (NAP-2)	71010
FORTAN SUBROUTINE	71020
FOR USE WITH H LEVEL FORTRAN COMPILER ON IBM 360/MOD 95.	71030
	71040
PURPOSE	71050
PRTIAL IS THE CONTROL PROGRAM FOR THE CALCULATION OF THE	71060
PARTIAL DERIVATIVES, FUNCTIONAL DISCREPANCIES, AND PARAMETER	71070
DISCREPANCIES.	71080
	71090
CALLING SEQUENCE	71100
CALL PRTIAL	71110
	71120
INPUT	71130
	71140
OUTPUT	71150
	71160
REFERENCE	71170
	71180
	71190
	71200
METHOD	71210
	71220
	71230
RESTRICTIONS	71240
	71250
	71260
ACCURACY	71270
FLOATING POINT - ALL CONSTANTS AND VARIABLES ARE CARRIED IN	71280
DOUBLE PRECISION TO 16 DECIMAL DIGITS.	71290
MIN. MAGNITUDE = 1.D-75	71300
MAX. MAGNITUDE = 1.D+75	71310
FIXED POINT - MAGNITUDE OF ALL CONSTANTS AND VARIABLES ARE	71320
.LE. 2147483647	71330
	71340
REQUIRED SUBPROGRAMS - FORTRAN LIBRARY	71350
	71360
	71370
REQUIRED SUBPROGRAMS - OTHER	71380
ERRORP - CONTROL THE PRINT-OUT OF ERROR MESSAGES	71390
	71400

```

C MEASUR - PARTIAL DERIVATIVES WRT MASTER COORDINATE SYSTEM AND - 71410
C WRT THE ERROR MODEL COEFFICIENTS 71420
C REFRACT - REFRACTION CORRECTION 71430
C ROTFIX - ROTATES VECTOR FROM INERTIAL TO EARTH FIXED COORD. 71440
C ROTINT - ROTATION MATRIX FROM EARTH-FIXED TO LOCAL STABLE - 71450
C COORDINATES. 71460
C STORAGE REQUIREMENTS 71470
C 71480
C 71490
C TIMING 71500
C NO ESTIMATE AVAILABLE 71510
C ANALYSIS 71520
C JOE LYNN ,PROJECT LEADER ,DBA SYSTEMS INC. 71530
C RAUL GARZA-ROBLES ,SEN. PROGRAMMER/ANALYST , 71540
C MRS. SHIRAS GUION , 71550
C ROBERT DEVANEY , 71560
C PROGRAMMER 71570
C ROBERT DEVANEY , 71580
C 71590
C 71600
C 71610
C PROGRAM MODIFICATIONS 71620
C 71630
C 71640
C 71650
C ***** START PROGRAM *****
C
C COMMON - ARC INFORMATION 71680
C COMMON /COMSOL/ FREP(500) , IFREP(500) , NTSPN,NEGTP,IRITKN,KOUT 71690
C COMMON /ACINFO/ 71700
C IACLABL(100) ,EPOCH(100) ,EPOCHD(100) ,GHA(100) , 71710
C ZIROSTAT(100) ,IASTAB(100,6) ,IAPNO(100,6) 71720
C 71730
C COMMON - ARC STABLE PARAMETERS 71740
C COMMON /ASPARM/ 71750
C INOAS ,NOAS2 ,ASLABL(200) ,ASINT(200) , 71760
C ZASCUR(200) ,ASWT(200) ,ASCWT(200) ,ASDEL(200) , 71770
C ZIASEVL(200) ,AS2LAB(200) ,AS2INT(200) 71780
C 71790
C COMMON - DEBUG PRINTING 71800
C 71810
C COMMON /CDEBUG/ 71820
C IIDEFLG(2) ,IPRFLG(2) ,ISLFLG(2) 71830
C 71840

```

```

COMMON - PARAMETERS COMPUTED ON INITIAL CALL TO MEASURE
COMMON /CMEASR/
1RANGE ,EL ,RDOT ,EODT
2SINE ,COSE
71850
71860
71870
71880
71890
71900
71910
71920
71930
71940
71950
71960
71970
71980
71990
72000
72010
72020
72030
72040
72050
72060
72070
72080
72090
72100
72110
72120
72130
72140
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - CONVERSION CONSTANTS LOADED BY MAIN PROGRAM
COMMON /CONMET/
1XMETKM ,XMETUD
71900
71910
71920
71930
71940
71950
71960
71970
71980
71990
72000
72010
72020
72030
72040
72050
72060
72070
72080
72090
72100
72110
72120
72130
72140
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - WORK AREA
COMMON /CWORK/
1IDATA(500) ,DATA(500) ,ICTL ,NINT
2NFLT
71960
71970
71980
71990
72000
72010
72020
72030
72040
72050
72060
72070
72080
72090
72100
72110
72120
72130
72140
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - INTEG I/O
COMMON /CINTEG/ PV(6), VEM(6,6), SV(6), SVEM(6,6), TE, JT
1 , T2
72010
72020
72030
72040
72050
72060
72070
72080
72090
72100
72110
72120
72130
72140
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - GENERAL CONTROL INFORMATION
COMMON /GENCOM/
1CONVG ,DIVRG ,SUMO ,SUM1
2COST ,MXITER ,MXDIVG ,ITERNO
AITERSW ,IUNITS ,IGEOfL ,IAUTOR
3IDIVNO ,ISIGNO ,IUPDNO ,IPRES
4IOINP ,NSTA ,MXMEAS ,MXARCS
5NARCS ,MXSTA ,MXLIN ,IPGNO
6MXPARM ,PGID(10)
7
72060
72070
72080
72090
72100
72110
72120
72130
72140
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - INTEG I/O
COMMON /EXTCM/ XP(10), YP(10), ZP(10), XV(10), YV(10), ZV(10),
1 BD(10), BT(10), BR(10), BM(10), BG(10), TZ, TF, TJ, TU, DP,
3 EP, SP, CD, D, V, T, NB, NS, NE, NM, NP, NC, KT, KO, KV, KE,
3 KS, LA, LB, LW
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - I/O FILE ASSIGNMENTS
COMMON /IONUMB/
1MFILE ,ISFILE ,IARCIN ,IPASIN
2IARCOT ,IPASOT ,ICARD ,IRESID
3ITAPE ,IALPHA ,LUA ,LUB
4 LUC
72230
72240
72250
72260
72270
72280

COMMON - MEASUREMENT INFORMATION
COMMON /MEAS/
72280

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COMMON /MSINFO/
1XMLABL(300) ,MSTYPE(300)
72290
72300
72310
COMMON - PASS STABLE PARAMETERS
COMMON /PSPARM/
INOPS ,NOPS2 ,PSLABL(200) ,PSINT(200) ,
2PSCUR(200) ,PSIWT(200) ,PSCWT(200) ,PSDELT(200) ,
3IPSEVL(200) ,PS2LAB(200) ,PS2INT(200)
72320
72330
72340
72350
72360
72370
COMMON - STATION INFORMATION
COMMON /STINFO/
1STLABL(100) ,STLAT(100) ,STHT(100) ,
21STSUR(100) ,1STSID(100)
72380
72390
72400
72410
72420
72430
COMMON - TOTALLY STABLE PARAMETERS
COMMON /TSPARM/
1NOTS ,NOTS2 ,TSLABL(200) ,TSINT(200) ,
2TSCUR(200) ,TSIWT(200) ,TSCWT(200) ,TSDELT(200) ,
3ITSEVL(200) ,TS2LAB(200) ,TS2INT(200)
72440
72450
72460
72470
72480
72490
COMMON /EARTH/ ROTAT, GRHA, RADIUS, GRAV, ECC
72500
72510
COMMON /RSUMR/DRXP(6),DRRXS(6),DRXS(6),DRRXS(6),RSVAL,RSR
72520
72530
DIMENSION IDATAW(100),DATAW(100)
DIMENSION LO(2),QSUM(2),QSQ(2),TIMSEC(156),QMEAS(156,2)
72540
72550
72560
72570
72580
72590
DIMENSION NMS(30), DMS(30)
72600
72610
DIMENSION BDO(6), 8DOM(6), BDOOS(6), NBDO(6),
1 NBDOOS(6)
72620
72630
72640
72650
DIMENSION XX(6)
DIMENSION PVI(6), AVVEM(6,6)
72660
72670
72680
72690
72700

```

```

ALL FORMAT STATEMENTS ARE CONTAINED HERE.
1 *****
1 *****
1 *****

```



```

2   . *** PRTIAL SPEAKING ***'/          72710
3   . ***'/'                               72720
4   . *****'/'                          72730
2  FORMAT('O*** STANDARD FILE FORMAT *** - FOR INTERPRETATION REFER T 72740
10 DOCUMENTATION WITH INDICATED FILE AND ICTL'/ 72750
2'OICTL ='I4/ 72760
3' NINT ='I4/ 72770
4' NFLT ='I4/ 72780
5'OIDATA(I) , I=1,NINT'/(10X,20I5)) 72790
3  FORMAT('ODATA(I) , I=1,NFLT'/(9X,1P6D18.10)) 72800
8  FORMAT('O IASTAB('I3,IH,I1,3H) =I2,'WILL CONTINUE PROCESSING WIT 72840
1H STABILITY FLAG (IASTAB) = 1.' 72850
10 FORMAT('O MASTER TABLE OF MEAS. NUMBERS DOES NOT CONTAIN MEAS. N 72860
10. FOR THIS POINT. PRTIAL WILL IGNORE THIS PT.'/ 72870
2' NMS(N) ='I3) 72880
11 FORMAT('O*** ISFILE OUTPUT RECORD ***') 72890
12 FORMAT('O NMEAS AND/OR NPARMS ARE TOO LARGE. PRTIAL CANNOT PRO 72900
1CEED.'/5X,'NMEAS ='I5,' , NPARMS ='I5) 72910
13 FORMAT(' E = ',D20.12,' E PRIME = ',D20.12/ 72920
1 ' F = ',D20.12,' F PRIME = ',D20.12/ 72930
2 ' G = ',D20.12,' G PRIME = ',D20.12) 72940
15 FORMAT(' TIME',D20.10/' XYZ ',6D20.10/(6D20.10)) 72950
17 FORMAT(' COS(DEC) AND COS(EL) ',2D20.10) 72960
72970
C SET UP C = SPEED OF LIGHT IN APPROPRIATE UNITS 72980
C 72990
C C = 2.99792508 73000
IF( IUNITS .EQ. 1 ) C = C * XMETKM 73010
IF( IUNITS .EQ. 2 ) C = C * XMETFT 73020
IF( IUNITS .EQ. 3 ) C = C * XMETUD 73030
C 73040
C 73050
ZERO= 0.00
NUTAPE= 35
NUPASS= 36
NURITE=37
IF(ITERNO.LE.1) REWIND ITAPE
REWIND NURITE
73060
C ALL REFERENCES TO IPRFLG(I) .NE. 0 EXERCISES DEBUG PRINTOUT 73070
IF((IPRFLG(1).NE.0).AND.(IPRFLG(2).GE.ITERNO)) WRITE (6,1) 73080
C 73090
C INPUT MFILE - ARC NUMBER 73100
READ (MFILE) 73110

```

I ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT) 73120

1000 CONTINUE NOARC = IDATA(1) 73200

C STORE INFORMATION FOR INTEGRATOR IN /EXTCM/ 73210

C 73220

C 73230

NOSEC = IDATA(2) 73240

NB = IDATA(3) 73250

NS = IDATA(4) 73260

NE = IDATA(5) 73270

NM = IDATA(6) 73280

NP = IDATA(7) 73290

NC = IDATA(8) 73300

KT = IDATA(9) 73310

KD = IDATA(10) 73320

KV = IDATA(11) 73330

KE = IDATA(12) 73340

KS = IDATA(13) 73350

LA = IDATA(14) 73360

LB = IDATA(15) 73370

LW = IDATA(16) 73380

TZSEC = DATA(2) 73390

TZDAY = DATA(1) 73400

TFSEC = DATA(4) 73410

TFDAY = DATA(3) 73420

DO 1003 I=1,10 73430

XP(I) = DATA(I+4) 73440

YP(I) = DATA(I+14) 73450

ZP(I) = DATA(I+24) 73460

XV(I) = DATA(I+34) 73470

YV(I) = DATA(I+44) 73480

ZV(I) = DATA(I+54) 73490

BD(I) = DATA(I+64) 73500

BT(I) = DATA(I+74) 73510

BR(I) = DATA(I+84) 73520

BM(I) = DATA(I+94) 73530

BG(I) = DATA(I+104) 73540

1003 CONTINUE

TZ = DATA(115) 73550

TF = DATA(116) 73560

TJ = DATA(117) 73570

TU = DATA(118) 73580

DP = DATA(119) 73590

EP = DATA(120) 73600

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73620 SP = DATA(121)
73630 CD = DATA(122)
73640 O = DATA(123)
73650 V = DATA(124)
73660 T = DATA(125)
73670 XPOLAR = DATA(126)
73680 YPOLAR = DATA(127)
C
C
C
C OUTPUT ISFILE - ARC RECORD - ICTL=1
  NINT = 1
  NFLT = 1
  WRITE (ISFILE)
  I ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)
C
  READ (MFILE) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(FREP(J),J=1,NFLT)
  NTSPN = IDATA(1)
  NEGTS = IDATA(2)
  DO 1005 I = 1,500
1005 IFREP(I) = 0
  IRIITKN = 0
  KOUT = 0
C INPUT IARCIN - ARC STABLE PARAMETERS
  READ (IARCIN)
  I ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)
1010 IF(ICTL .EQ. 1) GO TO 1020
C
C STORE ARC STABLE PARAMETERS NOT ENTERING INTO SOLUTION
  NOAS2 = IDATA(2)
  DO 1011 I = 1,NOAS2
  K = 2*I - 1
  AS2LAB(I) = DATA(K)
1011 AS2INT(I) = DATA(K+1)
C
C INPUT IARCIN - ARC STABLE PARAMETERS
  READ (IARCIN)
  I ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)
1020 NOAS = IDATA(2)
  IF(NOAS .EQ. 0) GO TO 1050
C
C STORE ARC STABLE PARAMETERS ENTERING INTO SOLUTION
  DO 1030 I = 1,NOAS
  K = 6*I - 5

```



```

C STORE PASS INFORMATION 74670
C 2010 NOSTA = IDATA(2) 74680
NOPASS = IDATA(3) 74690
NMEAS = IDATA(4) 74700
NPARMS = IDATA(5) 74710
IF((NMEAS .LE. 30) .AND. (NPARMS .LE. 300)) GO TO 2018 74720
74730
74740
74750
C *** ERROR CONDITION 74760
2014 CONTINUE 74770
WRITE(6,12) NMEAS,NPARMS 74780
GO TO 7100 74790
2018 DO 2020 I = 1,NMEAS
LO(I)=0
QSUM(I)=0.00
QSQ(I)=0.00
K = 3*I + 3 74800
NOMEAS(I) = IDATA(K) 74810
NRFRC(I) = IDATA(K+1) 74820
NRC(I) = IDATA(K+2) 74830
K = 4*I - 3 74840
ELMIN(I) = DATA(K) 74850
ELMAX(I) = DATA(K+1) 74860
RINDEX(I) = DATA(K+2) 74870
2020 WGTM(I) = DATA(K+3) 74880
74890
74900
C STORE PARAMETER TABLE 74910
ITEMP = 3 * NMEAS 74920
DO 2025 I = 1,NPARMS 74930
K = 4*I + ITEMP - 3 74940
NPMEAS(I) = IDATA(K+5) 74950
NEMT(I) = IDATA(K+6) 74960
NOPARM(I) = IDATA(K+7) 74970
2025 NPTYPE(I) = IDATA(K+8) 74980
L=0 74990
C INPUT IPASIN - PASS STABLE PARAMETERS 75000
READ (IPASIN) 75010
I ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT) 75080
2100 IF(ICTL .EQ. 1) GO TO 2200 75090
C STORE PASS STABLE PARAMETERS NOT ENTERING INTO SOLUTION 75100
NCP2 = IDATA(4) 75110
DO 2110 I = 1,NOPS2 75120

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```

75130 K = 2*I - 1
75140 PS2LAB(I) = DATA(K)
75150 2110 PS2INT(I) = DATA(K+1)
75160
75170 C INPUT IPASIN - PASS STABLE PARAMETERS
75180 READ (IPASIN)
75190 I ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)
75260 2200 NOPS = IDATA(4)
75270 IF(NOPS .EQ. 0) GO TO 2250
75280
75290 C STORE PASS STABLE PARAMETERS ENTERING INTO SOLUTION
75300 DO 2230 I = 1,NOPS
75310 K = 6*I - 5
75320 PJLABL(I) = DATA(K)
75330 PSINT(I) = DATA(K+1)
75340 PCCUR(I) = DATA(K+2)
75350 PSIWT(I) = DATA(K+3)
75360 PSCWT(I) = DATA(K+4)
75370 PSELT(I) = DATA(K+5)
75380 2230 IPSEVL(I) = IDATA(I+4)
75390
75400 C OUTPUT ISFILE (FOR SOLVER) - PASS RECORD - ICTL=2
75410 2250 ICTL = 2
75420 NINT = NMEAS + 4
75430 NFLT = NMEAS
75440 IDATA(4) = NMEAS
75450 DO 2275 I = 1,NMEAS
75460 IDATA(I+4) = NMEAS(I)
75470 2275 DATA(I) = WGTM(I)
75480 WRITE (ISFILE)
75490 I ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)
75500
75510 C ROTATION MATRIX FROM EARTH-FIXED TO LOCAL STABLE COORDINATES
75520 = TLC(1,1) TO TLC(3,3)
75530
75540 C TRANSLATION VECTOR
75550 = TLC(1,4) TO TLC(3,4)
75560 CALL ROTINT(STLAT(NOSTA),STLON(NOSTA),STHT(NOSTA),TLC)
75570
75580 C APPLY POLAR MOTION IF DEFAULTS OF 0.000 ON X,Y ANGLES WERE OVERRIDDEN
75590
75600 E = TLC(1,4)
75610 F = TLC(2,4)
75620 G = TLC(3,4)

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TLC(1,4) = E - XPOLAR * G
TLC(2,4) = F + YPOLAR * G
TLC(3,4) = G + XPOLAR * E - YPOLAR * F
IF ((IPRFLG(1) .EQ. 0) .OR. (ITERNO .GT. 1)) GO TO 2280
WRITE (6,13) E, TLC(1,4) , F, TLC(2,4) , G, TLC(3,4)
2280 CONTINUE
SAVE1 = TLC(1,1)
SAVE2 = TLC(2,1)
C
C STATION OFFSETS
      = TLC(1,5) TO TLC(3,5)
DO 2300 I = 1,3
2300 TLC(I,5) = 0.00
C
C SEARCH ERROR MODEL TABLE FOR SURVEY CORRECTIONS , IF ANY
C
DO 2500 I=1,NPARMS
IF{(NEMT(I)-LT.7).OR.(NEMT(I).GT.9)} GO TO 2500
K= NPTYPE(I)
GO TO (2410,2420,2430,2440,2450,2460), K
2410 TLC(NEMT(I)-6,5) = TSCUR(NOPARM(I))
GO TO 2500
2420 TLC(NEMT(I)-6,5) = ASCUR(NOPARM(I))
GO TO 2500
2430 TLC(NEMT(I)-6,5) = PSCUR(NOPARM(I))
GO TO 2500
2440 TLC(NEMT(I)-6,5) = TS2INT(NOPARM(I))
GO TO 2500
2450 TLC(NEMT(I)-6,5) = AS2INT(NOPARM(I))
GO TO 2500
2460 TLC(NEMT(I)-6,5) = PS2INT(NOPARM(I))
2500 CONTINUE
C
C INPUT MFILE - MEASUREMENT POINT RECORD - ICTL=3
7000 CONTINUE
READ (MFILE,END=7100)
      ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)
      GO TO (5100,5100,3000), ICTL
C
C *** NORMAL EXIT ***
7100 IEND=.TRUE.
      IF(L.GT.0) GO TO 5110

```

75630
75640
75650
75660
75670
75680
75690
75700
75710
75720
75730
75740
75750
75760
75770
75780
75790
75800
75810
75820
75830
75840
75850
75860
75870
75880
75890
75900
75910
75920
75930
75940
75950
75960
75970
75980
75990
76000
76020
76030
76040

```

7105 REWIND ISFILE
REWIND NUTAPE
REWIND NUPASS
REWIND MFILE
REWIND IARCIN
REWIND IPASIN
RETURN
76070
76080
76090
76100
76110
76120

C PROCESS MEASUREMENT POINT DATA
3000 CONTINUE
76190
C STORE MEASUREMENT POINT DATA
76200
3010 NMSPT = NINT
76210
DU 3020 I = 1,NMSPT
76220
NMS(I) = IDATA(I)
76230
3020 DMS(I) = DATA(I+2)
76240
76250
C DTARR = DELTA TIME FOR AVERAGE RANGE RATE DATA
76260
76270
C DTARR = DATA (NMSPT + 3)
76280
76290
76300
C CURRENT TIME OF MEAS. PT. (JULIAN DAYS SINCE 1950)
76310
TDCURR = DATA(1)
76320
76330
C TIME IN SECONDS OF GIVEN DAY
76340
TSCURR = DATA(2)
76350
76360
C

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```

L=L+1
TIMSEC(L)=TSCURR
DO 3030 I=1,NMEAS
3030 QMEAS(L,I) = 1.D50
3040 CONTINUE
C T FOR NAP INTEG = TIME(SEC) FROM MIDNIGHT OF EPOCH DAY
76370
T1 = EPOCH(NOARC)
76380
DTDAY = TDCURR - EPOCHD(NOARC)
76390
T2 = DTDAY * 86400.D0 + TSCURR
76400
76410
76420
76430
C SOLVE FOR VECTOR AND MATRIZANT
76440
76450
76460
TT= TDCURR*86400.D0 + TSCURR

```



```

TMP = TT - TJ
C PRIMARY ARC
C
3050 CONTINUE
CALL SOFORT(IPS1,LUB,O.DO,TMP,D,V,T,PV,VEM)
C
C
IPSI = 2
GRHA = GHA ( NOARC)
C
C ROTATE STATE VECTOR FROM INERTIAL TO EARTH-CENTERED/EARTH FIXED COORD
CALL ROTFIX(PV,T2)
C
NPAK = 0
C
C SAVE PARAMETERS THAT WOULD BE DESTROYED BY MEASUR
3270 CONTINUE
SAVE3 = PV(1)
C ***
C *** MAIN LOOP - PROCESS EACH MEASUREMENT FOR THIS POINT
C ***
IF(NMSPT.LE.0) GO TO 6100
DO 4000 N = 1,NMSPT
DO 3200 I = 1,NMEAS
:F(NMS(N) .NE. NOMEAS(I)) GO TO 3200
MINDEX = I
GO TO 3250
3200 CONTINUE
C *** ERROR CONDITION
C
C MEAS. NO. FOR THIS PT DOES NOT MATCH MASTER TABLE OF MEAS. NUMBERS

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76480
76580
76590
76600
76610
76620
76650
76660
76670
76680
76690
76700
76710
76720
76730
76740
76750
76760
76770
76780
76790
76800
76810
76820
76830
76840
76850
76860
76870
76880

```

```

WRITE(6,10) NMS(N)          76890
GO TO 4000

C RESTORE PARAMETERS THAT ARE DESTROYED BY MEASUR
C
C 3250 CONTINUE
TLC(1,1) = SAVE1          76910
TLC(2,1) = SAVE2          76920
PV(1) = SAVE3             76930
MS = MSTYPE(NOMEAS(MINDEX)) 76940
                                76950
                                76960
                                76970
                                76980
                                76990
C AVERAGE RANGE-RATE DATA (MYTPE=18) 77000
C PRIMARY ARC ONLY          77010
C
C IF (MS .NE. 18) GO TO 3254 77020
RPLUS = 0.000             77030
RMINUS = 0.000            77040
DTARR2 = DTARR/2.00       77050
TMP1 = TMP + DTARR2       77060
                                77070
                                77080
                                77090
C CALL SOFOT(IPSI,LUB,0.000,TMP1,D,V,T,PV1,AVVEM)
T3 = T2 + DTARR2          77100
CALL ROTFIX(PV1,T3)       77110
C COMPUTE RANGE FOR TIME + DT/2 (RPLUS) 77120
DO 3252 I=1,3
TMP1 = PV1(I) - TLC(I,4)
RPLUS = RPLUS + TMP1 * TMP1
CONTINUE
RPLUS = DSQRT (RPLUS)
                                77130
                                77140
                                77150
                                77160
                                77170
                                77180
C TMP1 = TMP - DTARR2
                                77190
                                77200
C CALL SOFOT(IPSI,LUB,0.000,TMP1,D,V,T,PV1,AVVEM)
T3 = T2 / - DTARR2
CALL ROTFIX(PV1,T3)
                                77210
                                77220
                                77230
                                77240
                                77250
C COMPUTE RANGE FOR TIME - DT/2 (RMINUS)

```

```

VALUE = (RPLUS - RMINUS ) / DTARR
C
3254 CONTINUE
C
C
C
C
C MEASUR RETURNS RANGE,EL,RDCT,EDOT,SINE,COSE FOR JTERM = 0
C
C CALL MEASUR( MS, 0, TLC, PV, VALUE )
C
C SAVE COS(DEC)
C
C COSDEC = VALUE
C VALUE = 0.000
C
C COMPUTE COS(ELEV)
C COSEL = DCOS(EL)
C IF ((IPRFLG(1).GE.2).AND.(ITERNO.LE.IPRFLG(2))) WRITE(6,17)
C 1 COSDEC,COSEL
C
C CHECK FOR ACCEPTABLE ELEVATION
C
C
C
C
C ELEVOK=.TRUE.
C IF((EL.LT.ELMIN(MINDEX)).OR.(EL.GT.ELMAX(MINDEX))) ELEVOK=.FALSE.
C
C ELEVATION OK
C 3300 CONTINUE
C
C CLEAR ARRAYS FOR SAVING PARTIAL DERIVATIVES OF VECTOR
C DO 3290 I=1,6
C NBDO(I) = 0
C NBDOOS(I) = 0
C BDO(I) = 0.00
C BDOS(I) = 0.00
C 3290 CONTINUE
C
C CALL MEASUR WITH JTERM=1 TO GET CALCULATED MEASUREMENT
C CALL MEASUR( MS, 1, TLC, PV, VALUE )
C
C DO 3500 I = 1,NPARMS
C IF(NOMEAS(MINDEX) .NE. NPMEAS(I)) GO TO 3500
C

```

77330

77340

77350

77360

77370

77380

77390

77400

77410

77420

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77450

77460

77470

77480

77490

77500

77510

77520

77530

77540

77550

77560

77580

77590

77600

77610

77620

77630

77640

77650

77660

77670

77680

77690

77700

77710

77720

77730

77740

77750

```

C FOR ERROR MODEL TERMS GE 10, FIND CURRENT PARAMETER VALUE 77760
C 77770
IF( NEMT(I) .EQ. 1 ) GO TO 3390 77780
IF( NEMT(I) .LT. 10 ) GO TO 3380 77790
K = NPTYPE(I) 77800
GO TO (3310,3320,3330,3340,3350,3360), K 77810
3310 CONTINUE 77820
TLC(1,1) = TSCUR(NOPARM(I)) 77830
GO TO 3380 77840
3320 CONTINUE 77850
TLC(1,1) = ASCUR(NOPARM(I)) 77860
GO TO 3380 77870
3330 CONTINUE 77880
TLC(1,1) = PSCUR(NOPARM(I)) 77890
GO TO 3380 77900
3340 CONTINUE 77910
TLC(1,1) = TS2INT(NOPARM(I)) 77920
GO TO 3380 77930
3350 CONTINUE 77940
TLC(1,1) = AS2INT(NOPARM(I)) 77950
GO TO 3380 77960
3360 CONTINUE 77970
TLC(1,1) = PS2INT(NOPARM(I)) 77980
3380 CONTINUE 77990
CALL MEASUR( MS, NEMT(I), TLC, PV, VALUE ) 78000
78010
C CHECK FOR PARAMETER EVALUATION TYPE 2 - NOT TRANSMITTED TO SOLVER 78020
C NPTYPE(I) = 4 TOTALLY STABLE - NOT ENTERING SOLUTION 78030
C = 5 ARC STABLE - NOT ENTERING SOLUTION 78040
C = 6 PASS STABLE - NOT ENTERING SOLUTION 78050
78060
C 3390 CONTINUE 78070
IF(L.GT.0) GO TO 3500
IF(.NOT.ELEVOK) GO TO 3500
IF(NPTYPE(I) .GT. 3) GO TO 3500
IF( MS .EQ. 2) PV(1) = PV(I) * COSEL
IF( MS .EQ. 4) PV(1) = PV(I) * COSDEC
NPAR = NPAR + 1
ITEMP = NPAR + NMSPT
ITEMP1 = 3*NPAR + NMSPT - 2
C IF PARTIAL OF VECTOR WRT MEAS, SAVE IT FOR ROTATION IT INERTIAL COORD 78080
C 78090
78100
78110
78120
78130
78140
78150
78160
78170
IF(NEMT(I) .GT. 6 ) GO TO 3400

```

```

NBD0(NEMT(I)) = ITEMP + 2
BDO(NEMT(I)) = PV(1)
3400 CONTINUE
C
C
C PARAMETER
  IDATAW(ITEMP1+2) = NPTYPE(I)
C PARAMETER NUMBER
  IDATAW(ITEMP1+3) = NOPARM(I)
C MEASUREMENT NUMBER
  IDATAW(ITEMP1+4) = NPMEAS(I)
C PARTIAL
  DATAW(ITEMP + 2) = PV(1)
3500 CONTINUE
C
C IF NO PARTIALS OF VECTOR, SKIP ROTATION
  IF( NBD0(I) .LE.0 ) GO TO 3540
C
C ROTATE PARTIALS OF VECTOR FROM FIXED TO INERTIAL COORDINATES
  CALL ROTPAR( BDO, T2 )
C
C RELATE VECTOR TO EPOCH TIME
  DO 3520 K=1,6
  BDOM(K) = 0.00
  DO 3520 J=1,6
  3520 BDOM(K) = BDOM(K) + BDO(J) * VEM(J,K)
C
  3530 DATAW(NBD0(J)) = BDOM(J)
C
3540 CONTINUE
C
C CHECK FOR PARTIALS OF SECONDARY VECTOR
  IF( NBDOS(1) .LE. 0 ) GO TO 3570
C ROTATE TO INERTIAL
  CALL ROTPAR( BDOS, T2 )
C RELATE TO EPOCH VIA MATRIZANT
  IF ((IPRFLG(1).GE.2) .AND. (ITERNO .LE. IPRFLG(2))) WRITE (6,15)
  1  T, (SV(I), I=1,6), ((SVEM(I,J), I=1,6), J=1,6)
  DO 3550 K=1,6
  BDOM(K) = 0.00
  DO 3550 J=1,6
  3550 BDOM(K) = BDOM(K) + BDOS(J) * SVEM(J,K)
78180
78190
78200
78210
78280
78290
78310
78330
78350
78370
78380
78390
78400
78410
78420
78430
78440
78450
78460
78470
78480
78490
78500
78510
78520
78540
78550
78560
78570
78580
78590
78600
78610
78620
78630
78640
78650
78660
78670

```



```

DATAW(2)= ISTDID(NOSTA)
DATAW(3)= NOPASS
IF(LC(1).GT.0) GO TO 4020
DMS(2)= DMS(1)
DMS(1)= 0.00
GSQ(1)= 0.00
4020 IF(LC(2).GT.0) GO TO 4030
DMS(2)= 0.00
QSQ(2)= 0.00
4030 WRITE(NUTAPE) ZERO,DATAW(1),DATAW(2),DATAW(3),ZERO,ZERO
WRITE(NUTAPE) TDCURR,TSCURR,DMS(1),DMS(2),ZERO,ZERO
WRITE(NUPASS) NOSTA,NOPASS,LO,OSQ
WRITE(NURITE)NOARC,NOPASS,ISTDID(NOSTA),STLABL(NOSTA),
*ELEVOK,LMEAN,LA,QSQ,DMS(1),DMS(2),TDCURR,TSCURR,
*(TIMSEC(L),L=1,LA),((QMEAS(L,I),L=1,LA),I=1,2)
IF(IEND) GO TO 7105
GO TO 5105
79060
5100 IEND=.FALSE.
IF(L.GT.0) GO TO 5110
5105 IF(ICIL-1) 1000,1000,2000
5110 LMEAN=(L+1)/2
NMSPT=0
DO 5140 LL=1,NMEAS
IF(LD(LL).LE.0) GO TO 5140
NMSPT= NMSPT+1
NMS(NMSPT)= NOMEAS(LL)
QSUMT= QSUM(LL)
QSQT= QSQ(LL)
5120 IF(LD(LL).LE.1) GO TO 5150
QL= LD(LL)
LA=0
QBAR= QSUMT/QL
SIGMAT= DSQRT((QSQT-QSUMT*QBAR)/(QL-1.00))
TWSIG=3.00*SIGMAT
QSQT= QSQ(LL)
QSUMT= QSUM(LL)
DO 5130 LB=1,L
IF(DABS(QMEAS(LB,LL)-QBAR).LE.TWSIG) GO TO 5125
IF(QMEAS(LB,LL).GE.0.1050) GO TO 5130
QSUMT= QSUMT- QMEAS(LB,LL)
QSQT= QSQT- QMEAS(LB,LL)*QMEAS(LB,LL)
GO TO 5130
5125 LA=LA+1

```

5130 CONTINUE
IF(LA.GE.LO(LL)) GO TO 5135
LO(LL) = LA

GO TO 5120
5135 QSUM(LL)=QBAR
QSQ(LL) = SIGMAT

5140 CONTINUE
IF(TSCURR.LT.TIMSEC(LMEAN)) TDCURR=TDCURR-1.00
TSCURR=TIMSEC(LMEAN)
DATAW(1)=TDCURR
DATAW(2)=TSCURR
LA=L
L=0

GO TO 3040
5150 QSQ(LL)=0.00

GO TO 5140
6000 DMS(N)=QSUM(MINDEX)
IF(MS.EQ.2) DMS(N)= DMS(N)/COSEL
IF(MS.EQ.4) DMS(N)=DMS(N)/COSDEC
DMS(N)=DMS(N) + VALUE
DATAW(N+2)=QSUM(MINDEX)
IDATAW(N+2)=NMS(N)
IF(ELEVOK) GO TO 4000
DATAW(N+2)=0.00
IDATAW(N+2)=0
GO TO 4000

C
6100 NMSPT=1

IDATAW(3)=0
DATAW(3)=0.00
GO TO 4010

C
C
C ROUTINE TO PICK UP STATE VECTORS AND GENERATE POWER SERIES
C
C N = ARC NO.
C

C
1900 CONTINUE
BG(NC) = GHA(N) + EPOCH(N) * ROTAT
REWIND LUA
DO 1960 I=1,6
XX(I) = 0.00
ITEMP = IASTAB(N,I)
GO TO (1920,1930,1910,1940,1950,1910),ITEMP
79220
79230
79240
79250
79260
79270
79280
79290
79300
79310
79320
79330
79340


```

C          79350
C  ERROR          79360
1910  CONTINUE    79370
      WRITE (6,8) N,I,ITEMP
      GO TO 1960    79380
C          79390
C          79400
C  TOTALLY STABLE ENTERING INTO SOLN  79410
C          79420
1920  XX(I) = TSCUR(IAPNO(N,I))      79430
      GO TO 1960    79440
C          79450
C  ARC STABLE ENTERING INTO SOLN     79460
C          79470
1930  XX(I) = ASCUR(IAPNO(N,I))      79480
      GO TO 1960    79490
C          79500
C  TOTALLY STABLE NOT IN SOLN        79510
C          79520
1940  XX(I) = TS2INT(IAPNO(N,I))     79530
      GO TO 1960    79540
C          79550
C  ARC STABLE NOT IN SOLN            79560
C          79570
1950  XX(I) = AS2INT(IAPNO(N,I))     79580
1960  CONTINUE    79590
C          79600
C  STORE IN /EXTCM/                  79610
C          79620
      XP(NP) = XX(1)
      YP(NP) = XX(2)
      ZP(NP) = XX(3)
      XV(NP) = XX(4)
      YV(NP) = XX(5)
      ZV(NP) = XX(6)
      79630
      79640
      79650
      79660
      79670
      79680
      79690
C          79700
C  TJ IS EPOCH TIME (1950.0) IN SECONDS  79710
C          79720
      TJ = EPOCHD(N)*86400.00 + EPOCH(N)
      TE = TJ
      79730
      79740
C          79750
C  TZ IS INTEG START TIME
C          79760
C  TF IS INTEC STOP TIME
C          79770
      79780
      TZ = 0.00

```

TSTART = TZSEC + TZDAY * 86400.D0
TFINAL = TFSEC + TFDAY * 86400.D0

79790
79800
79810
79820
79830
79840
79850
79860
79870

C
C

IF(TSTART .GE. TJ) GO TO 1970
IF(TJ .GE. TFINAL) GO TO 1980

C
C ARC SPANS EPOCH -- MUST INTEG TWO SUBARCS

79880
79890
79900
79910
79920
79930

TF = TFINAL - TJ
CALL KICKER(2)
TF = TSTART - TJ
CALL KICKER(2)
GO TO 1990

C
C
C

ARC FOLLOWS EPOCH

1970 CONTINUE

TF = TFINAL - TJ
CALL KICKER(2)
GO TO 1990

79940
79950
79960
79970
79980
79990

C
C
C

ARC PRECEDES EPOCH

1980 CONTINUE

TF = TSTART - TJ
CALL KICKER(2)
CONTINUE

GO TO (1060,1070), IRET

80000
80010
80020
80030
80040
80050
80060
80070
80080
80090
80100
80110

END OF POWER SERIES ROUTINE

C
C
C

END

0385 CARDS

Appendix A-4
Constraints Imposed on
NAP-II Deck Setup

A-4.1 CONSTRAINTS IMPOSED BY MINITRACK PREPROCESSOR

There are constraints imposed on the NAP-II deck setup by the preprocessing program. This appendix is an attempt to outline the constraints in a concise, quick-reference form.

The Minitrack Preprocessor (Section 2.2.3) imposes an order to the stations in NAP-II (Key 1, Category 201), depending on the order the Minitrack data is preprocessed (data set 5 of Minitrack Preprocessor). The station ID's required by the NAP-II program are generated from the fifty-fifth and fifty-sixth characters of the Minitrack message format (Section 2.2.1). This code is used for the equatorial data, and the code plus 100 is used for the polar data.

Example: Station constants for Minitrack processor are in the following order:

Ft. Meyers
 Quito
 Lima
 Santiago
 Newfoundland.

The following information would be generated by the preprocessor for each station:

	Equatorial		Polar	
	Sta. ID	Sta. No.	Sta. ID	Sta. No.
Ft. Meyers	03	1	103	2
Quito	05	3	105	4
Lima	06	5	106	6
Santiago	08	7	108	8
Newfoundland	12	9	112	10

- C. Start and Stop times of the data pass Category 201 and 202
- D. End of pass control card Category 999.

A-4.2 CONSTRAINTS IMPOSED BY THE PRE-NAP PROGRAM

This program is used to modify, add, or delete NAP-II control cards.

The following are the instructions for its usage:

- | | |
|-----------|--|
| INS I1 | Inserts cards after sequence number I1. |
| DEL I1 I2 | Deletes cards between (and including) sequence numbers I1 and I2. |
| REP I1 I2 | Deletes cards between (and including) sequence numbers I1 and I2, and then inserts cards |
| MOD I1 I2 | Modifies cards between (and including) sequence numbers I1 and I2. |

Format for above four cards (A4, x, I5, 5x, I5) note that INS, DEL, REP, and MOD start in column 1 and that column 2 should be blank.

INS and REP must be followed by the cards to be inserted. The cards must be followed by a blank card to signify the end of the particular set of inserted cards.

The MOD cards must be followed by a modifying card. Columns not to be modified should be left blank.

When using the computed mid-point Minitrack data, the Category 704 cards have to be deleted from the control cards. The "704" cards should be used only when the entire data spans are used.

A-4.3 CONSTRAINTS IMPOSED ON NAP-II SETUP

A very basic assumption made when processing Minitrack data is that a good estimate of the state vector is available. This is the basis of the whole process.

The a priori sigma information should be realistically assigned with respect to the error model terms and the observed data.

When processing with the "single-data, point pen pass" data file, be sure to delete Category 704 cards that were used for the processing of the entire observed data file.

Measurement numbers (Category 701) have a limitation as to their assignment. Odd measurement numbers are reserved for cosine alpha (ℓ) measurements, and even numbers are reserved for cosine beta (m) measurements. This limitation is imposed by the Post-NAP processor.

Error model term definition cards (Category 601 cards) must be in order of totally stable, arc stable, and pass stable. There can be only one 601 card for each error model term. Duplicates inserted to override a previous 601 card are not permitted.

A-4.4 ADDITIONAL CONSTRAINTS

This section is reserved for constraints not mentioned above that have not come to light. If, in the course of reducing Minitrack data, using the procedure outlined in this report, new constraints are found, please note them in this section.