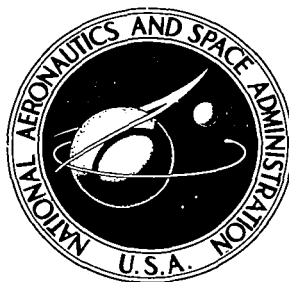


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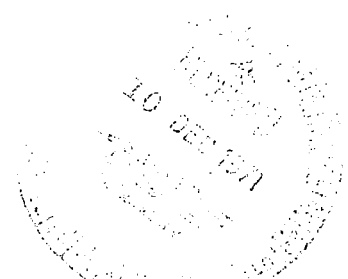
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# INVESTIGATION OF A CLAMSHELL ROLL-OUT EJECTION CONCEPT

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16. Abstract <p>The equations for the motion, forces, and couples generated by clamshells released from spinning sounding rockets in accordance with a roll-out ejection concept are presented. The application of these equations to a study of a system for the Javelin (i.e., Honest John-Nike-Nike-X248) rocket vehicle is discussed.</p> <p>The roll-out ejection concept advocated requires that each deploying clamshell be pivoted about an axis at its trailing edge located in the system sectioning plane. Clamshell despinning is a consequence of this deployment since the pivotal, i.e., roll-out, rate is in opposition to the rocket vehicle spin. The energy required by the deployment is derived largely from the rotational energy of the clamshell. Thus, the rocket vehicle will not be significantly despun by this kind of clamshell deployment.</p> <p>This ejection concept also permits a system design which makes it possible to limit clamshell angular motion to rotation about that one of its centroidal principal axes which is brought into parallelism with the rocket vehicle longitudinal axis. Also, by equalizing the moments of inertia about the other centroidal principal axes, the roll-out motion can be decoupled from any extraneous angular motion about these axes.</p>			
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## LIST OF SYMBOLS

$A, B, C, D$  = inertial parameters (slug-ft<sup>2</sup>).

$C_{x_1}, C_{x_2}, C_{x_3}$  = hinge-couple components about axes parallel to the  $x_1$ -,  $x_2$ -, and  $x_3$ -axes, respectively (ft-lb).

$C_{y_1}, C_{y_2}, C_{y_3}$  = hinge-couple components about axes parallel to the clamshell body-fixed  $y_1$ -,  $y_2$ -, and  $y_3$ -axes, respectively (ft-lb).

$C\psi, C\theta, C\phi$  = cosines of the Euler angles  $\psi, \theta,$  and  $\phi,$  respectively.

$d_1$  = clamshell hinge-axis displacement from the  $x_1$ -axis (the rocket vehicle longitudinal axis) (ft).

$d_2$  = clamshell center of mass (c.m.) displacement from the  $x_1x_2$ -plane (the system bisecting plane) before clamshell deployment (ft).

$d_3$  = clamshell c.m. displacement from the system base plane (ft).

$d_5$  = clamshell c.m. displacement from the hinge axis (ft).

$d_6$  = clamshell c.m. displacement from the  $x_2x_3$ -plane (the rocket vehicle system transverse plane containing its barycenter) (ft).

$d_7$  = clamshell c.m. displacement from the  $x_1$ -axis during deployment (ft).

$d_{7f}$  = terminal value of  $d_7$  (ft).

$F_{x_1}, F_{x_2}, F_{x_3}$  = hinge-force components directed along axes parallel to the  $x_1$ -,  $x_2$ -, and  $x_3$ -axes, respectively (lb).

$F_{y_1}, F_{y_2}, F_{y_3}$  = hinge-force components directed along axes parallel to the clamshell body-fixed  $y_1$ -,  $y_2$ -, and  $y_3$ -axes, respectively (lb).

$F_1, F_2, F_3, F_4, F_5$  = inertial forces (lb).

$$\left. \begin{aligned} J_{cy_1} &= \int_m (y_2^2 + y_3^2) dm \\ J_{cy_2} &= \int_m (y_1^2 + y_3^2) dm \end{aligned} \right\} \begin{array}{l} \text{significant elements of the clamshell inertia matrix defined in} \\ \text{terms of the clamshell body-fixed } y\text{-frame (slug-ft}^2\text{).} \end{array}$$

$$\left. \begin{aligned} J_{cy_3} &= \int_m (y_1^2 + y_2^2) dm \\ J_{cy_5} &= \int_m y_1 y_3 dm \end{aligned} \right\} \text{significant elements of the clamshell inertia matrix defined in terms of the clamshell body-fixed } y\text{-frame (slug-ft}^2\text{)}$$

$J_{vx_1}$  = rocket vehicle (minus clamshells) spin moment of inertia (moment of inertia about the  $x_1$ -axis) (slug-ft<sup>2</sup>).

$J_{z_1}, J_{z_2}, J_{z_3}$  = clamshell moments of inertia about the  $z_1$ -,  $z_2$ -, and  $z_3$ -axes, respectively (slug-ft<sup>2</sup>).

$K$  = direction cosine matrix.

$M_{y_1}, M_{y_2}, M_{y_3}$  = moments about the clamshell body-fixed  $y_1$ -,  $y_2$ -, and  $y_3$ -axes, respectively (ft-lb).

$M_{z_1}, M_{z_2}, M_{z_3}$  = moments about the clamshell body-fixed  $z_1$ -,  $z_2$ -, and  $z_3$ -axes, respectively (ft-lb).

$m$  = clamshell mass (slugs).

$\mathbf{p}$  = position vector from the origin of the  $x$ -frame to the clamshell c.m. (ft).

$R_1$  = component of the position vector from an inertial frame origin to the  $x$ -frame origin directed along the rocket vehicle body-fixed  $x_1$ -axis (ft).

$S\psi, S\theta, S\phi$  = sines of the Euler angles  $\psi, \theta$ , and  $\phi$ , respectively.

$t$  = elapsed time (s).

$t_f$  = time at the end of the clamshell deployment phase and the beginning of the free-flight phase (s).

$U, V$  = momental parameters (ft-lb).

$W_1, W_2, W_3$  = clamshell free-flight rotational rate components about the  $z_1$ -,  $z_2$ -, and  $z_3$ -axes, respectively (s<sup>-1</sup>).

$\{X_j\}$  = displacement vector for the  $j$ th point on the clamshell defined in terms of the  $X$ -frame (ft).

$\{X_{cm}\}$  = clamshell c.m. displacement vector defined in terms of the inertial  $X$ -frame (ft).

$\{z_j\}$  = displacement vector for the  $j$ th point on the clamshell defined in terms of the  $x$ -frame (the clamshell centroidal principal axis frame) (ft).

$\alpha$  = angle between the  $x_1 x_2$ -plane and the plane defined by the  $x_1$ -axis and the position vector  $\mathbf{p}$ .

$\beta$  = angle in the clamshell mass-symmetry plane between the clamshell body-fixed  $y$ -frame and the clamshell centroidal principal axis set.

$\gamma$  = clamshell roll-out angle (the angle between the  $x_1x_2$ -plane and the  $y_1y_2$ -plane).

$\eta$  = angle between the  $x_1x_2$ -plane and the plane containing both the clamshell hinge axis and clamshell c.m.

$\eta_0$  = initial value of  $\eta$ .

$\alpha_f, \gamma_f, \eta_f$  = terminal values of  $\alpha, \gamma,$  and  $\eta,$  respectively.

$\psi, \theta, \phi$  = Euler angles (see Figure 6).

$\Omega_1$  = rocket vehicle spin (rotational rate of the  $x$ -frame) ( $s^{-1}$ ).

$\Omega_{1f}$  = terminal value of  $\Omega_1$  ( $s^{-1}$ ).

$\Omega_{10}$  = initial value of  $\Omega_1$  ( $s^{-1}$ ).



# INVESTIGATION OF A CLAMSHELL ROLL-OUT EJECTION CONCEPT

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## INTRODUCTION

In this report, a roll-out ejection concept for the release of clamshells from spinning sounding rockets is developed and discussed. The primary aim is to establish the desirability of this particular concept for use with sounding rockets. It will be seen that the conditions under which the clamshells are ejected impose requirements not considered in other applications. These requirements affect chiefly the manner in which the clamshells are to be ejected.

At the present time, there are two general categories of ejectable payload-protection devices. The conceptually older and structurally simpler of these devices is the one piece nose cone. A nose cone is essentially a shell of revolution with its aft end faired and attached to the top stage of the rocket vehicle. The cone is tapered to a closed fore end. The payload is situated in the space bounded by the nose cone and the rocket vehicle. The nose cone is impelled at its ejection by springs or other means in the direction in which the rocket vehicle is pointed. Obviously, this is not attempted while the rocket vehicle is thrusting—it must occur under coasting conditions. If the rocket vehicle has a control system, it may be maneuvered so that the ejected nose cone does not present a collision hazard during a subsequent thrust phase. Unfortunately, sounding rockets do not now have this maneuvering capability. Hence, the nose cone cannot be ejected safely until the sounding rocket is in its final coast phase and at an altitude where post ejection collision is not likely to occur. Thus, the performance of a sounding rocket can be impaired by its acceleration of excess mass. In the case of the Javelin (i.e., Honest John-Nike-Nike-X248) rocket vehicle, nose cone ejection is timed to occur 120 seconds after liftoff, when the vehicle is at an altitude of about 700,000 feet. At this point in the flight, any residual X248 thrust and the drag deceleration difference between the ejected nose cone and rocket vehicle are considered to be negligible. It will be seen that this particular nose cone ejection is set for a time which occurs significantly later than is possible with clamshells. It can be seen also that, in general, nose cone ejection is troublesome when the payload is long and impossible when the payload compartment is bulbous. Guides or bumpers running the length of the payload and ejection actuators with long strokes are required in the former instance to avoid nose cone hang up. The nose cone can still be a source of trouble after it has cleared the rocket vehicle. It effectively continues to precede the

payload in the trajectory and may affect instrument readings by emitting particles and disturbing the environment in other ways.

Clamshell systems are like nose cones, largely in overall shape. Each clamshell may be considered to be a longitudinal section of a shell of revolution. The clamshells are held together by bands, clamps, and the like, or they are attached to skin sections which can be ruptured at ejection time. On ejection, each clamshell is projected away from the longitudinal axis of the rocket vehicle; that is, its movement characteristically has a component which soon carries the clamshell out of the path of the payload. Therefore, the ejected clamshells do not continue to be collision hazards after they have cleared the rocket vehicle and payload. Thus, the time at which clamshell ejection is set to occur may be made meaningful in that it is not necessary to wait until the drag has dropped practically to zero before ejection. In fact, a slight amount of drag will help to increase the longitudinal separation between the payload and ejected clamshells. Obviously, the application of rocket vehicle thrust can produce even greater separation.

Ejection can occur for the Javelin when it is at an altitude of about 300,000 feet. At this point in its flight, it is about halfway into its X248 thrust phase. Perturbations due to X248 ignition and separation have been damped out, and the dynamic pressure has dropped to negligibly low values despite the considerable increase in vehicle velocity. The shape of the dynamic pressure profile for the Javelin is exemplified by the curve in Figure 1. The X248 thrust phase occurs between the tick marks located at 56 and 97.9 s. In addition to permitting the recording of scientific data at lower altitudes than it was possible previously, clamshell ejection even at this point in the final boost phase will have a significant effect on the performance of the Javelin. Because about two thirds of the vehicle velocity at final burnout is due to the X248 thrust phase, the release of clamshells earlier in the flight can improve the vehicle's performance (see Figure 2).

Unfortunately, the conditions under which sounding rocket clamshells must operate have not been sufficiently considered in a number of designs. This situation may be partly due to the established success in the release of clamshells from nonspinning rocket vehicles, in which clamshells are disengaged and simply pitched out. It should be noted that in this case, the angular motion of each clamshell is restricted to rotation about that one of its centroidal principal axes normal to its mass symmetry plane. Hence, the motion of the clamshells during and after their deployment remains uncoupled and simple. This is not the case with clamshells pitched out from a spinning rocket vehicle. Instead, such an action causes each ejecting clamshell to rotate about all of its centroidal principal axes. The resulting complication greatly increases the extraneous tendencies of these clamshells and makes it difficult to design optimal constraints to control the clamshell motion during the deployment phase of ejection.

The extraneous tendencies should be reduced, if not eliminated, by essentially limiting clamshell angular motion to rotation about a single principal axis. This requires that each clamshell be rolled out since it is rolling to begin with. This can be done by pivoting it about an axis through either its leading or trailing edge in the clamshell system sectioning planes. Extraneous rotational tendencies may yet be induced in the clamshell by reaction to constraints utilized to develop the desired rolling motion. Thus, care must still be exercised in the design of roll-out clamshell ejection mechanisms.

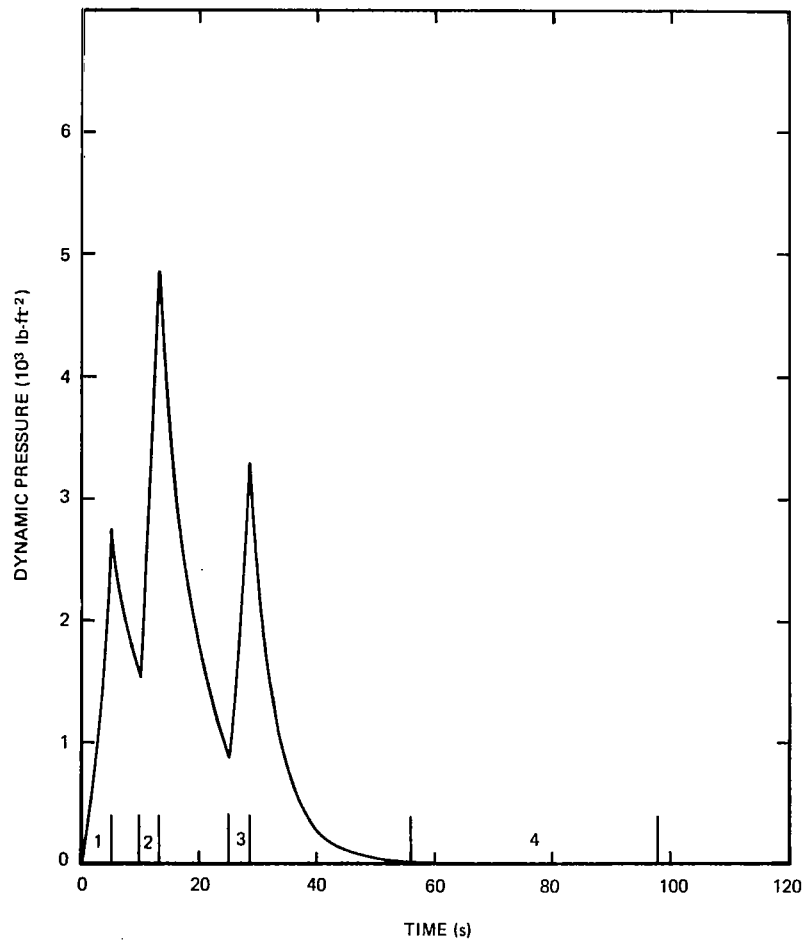


Figure 1—Dynamic pressure profile for a Javelin launched at 80° QE (quadrant elevation angle) and carrying a 120-lb gross payload.

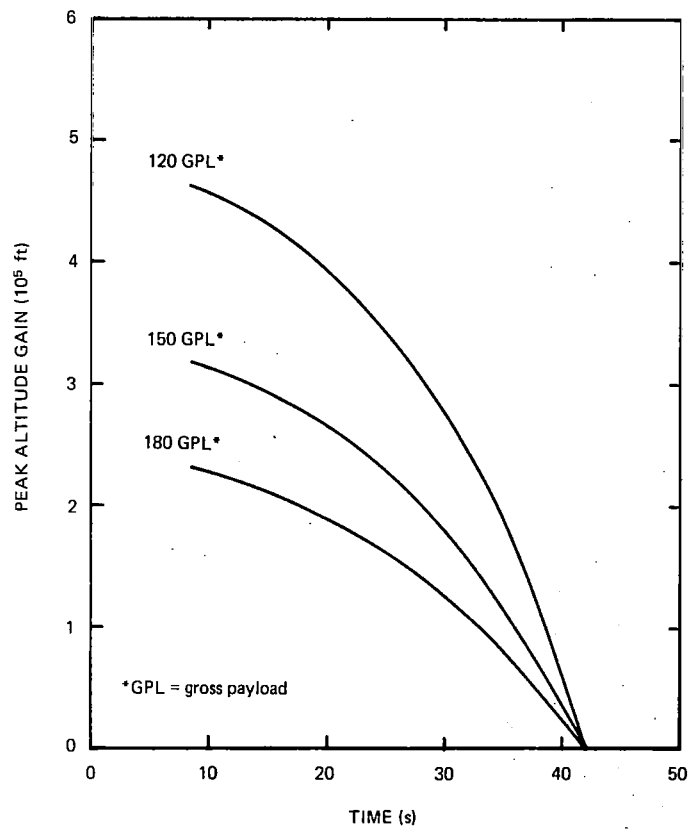


Figure 2—Effect of clamshell release time relative to X248 ignition on Javelin flight performance.

The angular momentum of a roll-out clamshell pivoted about its leading edge is increased on its deployment. This is caused by the displacement of its center of mass (c.m.) from the rocket vehicle longitudinal axis and the increase in its angular rate, which is a summation of its roll-out rate and the vehicular spin. The rocket vehicle will be despun by such clamshell deployment unless means are adopted to preclude it. This can be a troublesome endeavor since it tends to complicate the system design and increase its weight.

A clamshell pivoted about its trailing edge, on the other hand, is despun on its deployment since its pivotal, i.e., roll-out, rate is in opposition to the rocket vehicle spin. Thus, the energy for clamshell deployment can be expected to come initially from the rotational energy of the clamshell. The rocket vehicle will experience a measure of despinning after the clamshell has pivoted to a given roll-out angle. This will definitely be the case when the clamshell is totally despun, i.e., when the magnitude of the clamshell roll-out rate equals that of the rocket vehicle spin. The clamshell may be disengaged at this point in its deployment to give its free-flight motion a purely translatory character. However, in an actual flight, it may be preferable to release the clamshell earlier, i.e., at a smaller roll-out angle to reduce the extraneous torquing of the rocket vehicle during clamshell ejection. The selection of an optimum release angle is not obvious, particularly when too small an angle can result in a collision between the clamshells and the payload (this is the case with release at zero roll-out angle, i.e., instantaneous clamshell release). The effects of various system parameters must be investigated before any determination can be made with respect to this aspect or any other aspect of this problem.

### ANALYTICAL ASSUMPTIONS

The following analysis is concerned with the equations for the motion, forces, and couples generated by clamshells released from spinning sounding rockets in accordance with a roll-out ejection concept. This concept requires that each ejecting clamshell be pivoted about an axis at its trailing edge in the system bisection plane so that its pivotal, i.e., roll-out, rate is in opposition to the rocket vehicle spin. Figure 3 illustrates the ejection sequence scheme viewed head-on to a rocket vehicle with a right-hand spin.

In order to facilitate resolution of the problem, it is assumed that there is a problem symmetry which permits the characterization of the system dynamics by those of a single clamshell. Thus, the

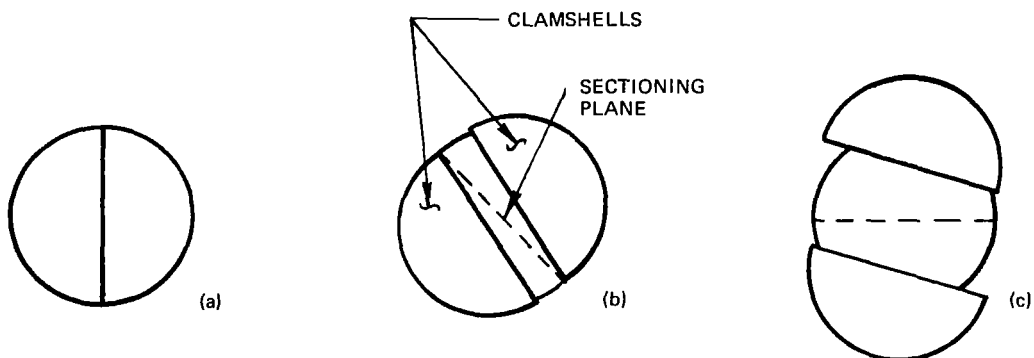


Figure 3—Trailing edge pivot type of roll-out clamshell system with right-hand vehicle spin.

clamshells are assumed to be dynamically matched, rigid bodies attached to a spinning rocket which is not coning in a significant manner when clamshell ejection is initiated. For convenience, it is assumed also that the damping and dissipative forces are negligible in comparison to the inertial forces.

Three coordinate frames are used in the analysis of the deployment phase dynamics. One of these is the  $x$ -frame, which is centered at the vehicle system barycenter and orientated so that its  $x_1$ -axis is coincident with the rocket vehicle longitudinal axis and its  $x_2$ -axis is directed in such a way that the clamshell system bisection plane is in the  $x_1 x_2$ -plane. The  $x$ -frame may be assumed to be a rocket vehicle body-fixed frame since the barycenter may be considered to be stationary during the time required by clamshell deployment. The clamshell body-fixed  $y$ -frame is centered at the clamshell c.m. and orientated so that its  $y_1$ -,  $y_2$ -, and  $y_3$ -axes parallel the  $x_1$ -,  $x_2$ -, and  $x_3$ -axes, respectively, of the  $x$ -frame before clamshell ejection. The clamshell is constrained during its deployment to maintain the parallelism between the  $x_1$  and  $y_1$  axes. The  $z$ -frame is the clamshell centroidal principal axis set. It is oriented so that its  $z_2$ -axis is normal to the clamshell mass symmetry plane and coincident with the  $y_2$ -axis of the  $y$ -frame. The clamshell may be affixed with weights to rotate the  $z_1$ - and  $z_3$ -axes and bring them into alignment with the  $y_1$ - and  $y_3$ -axes, respectively, without changing the relationship between the  $z_2$ - and  $y_2$ -axes. When this is done, the  $z$ -frame and  $y$ -frame are identical. Figure 4 illustrates the spatial relationship between the  $x$ -,  $y$ -, and  $z$ -frames.

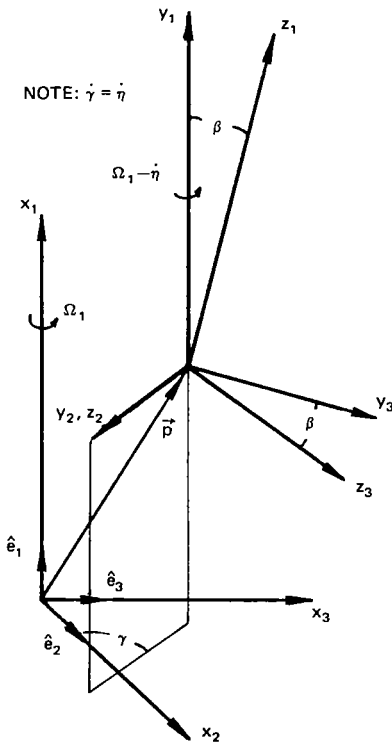


Figure 4—Coordinate frames.

## EQUATIONS FOR THE SYSTEM ANGULAR MOTION

The equations for the angular motions of the system, derived by an application of Lagrange's equation, may be written in a form suitable for digital computer solution as follows:

$$\dot{\Omega}_1 = \frac{DU - BV}{AD - BC}$$

and

$$\ddot{\eta} = \frac{AV - CU}{AD - BC},$$

where

$$A = J_{vx_1} + 2(J_{cy_1} + md_5^2),$$

$$B = -2(J_{cy_1} + md_5^2) + 2md_5d_1 \cos \eta,$$

$$C = B,$$

$$D = 2(J_{cy_1} + md_5^2),$$

$$U = -2(2m\Omega_1\dot{\eta}d_5 - m\dot{\eta}^2d_5)d_1 \sin \eta,$$

$$V = 2m\Omega_1^2d_5d_1 \sin \eta,$$

and

$$AD - BC = 2J_{vx_1}(J_{cy_1} + md_5^2) + 4md_1^2[J_{cy_1} + md_5^2(1 - \cos^2 \eta)] \neq 0.$$

## EQUATIONS FOR THE HINGE FORCES

The hinge-force components are obtained by the application of Newton's Second Law to the acceleration of the clamshell c.m. This yields

$$F_{x_1} = m\ddot{R}_1 ,$$

and

$$F_{x_2} = F_1 \sin \eta + (F_2 - F_3) \cos \eta - F_4 \sin \alpha - F_5 \cos \alpha ,$$

$$F_{x_3} = F_1 \cos \eta - (F_2 - F_3) \sin \eta + F_4 \cos \alpha - F_5 \sin \alpha ,$$

where

$$F_1 = m\ddot{\eta}d_5 ,$$

$$F_2 = m\dot{\eta}^2d_5 ,$$

$$F_3 = 2m\Omega_1\dot{\eta}d_5 ,$$

and

$$F_4 = m\dot{\Omega}_1d_7 ,$$

$$F_5 = m\Omega_1^2d_7 .$$

## EQUATIONS FOR THE HINGE COUPLES

From Figures 4 and 5, it can be shown that

$$C_{x_1} = C_{y_1} ,$$

$$C_{x_2} = C_{y_2} \cos \gamma + C_{y_3} \sin \gamma ,$$

$$C_{x_3} = C_{y_3} \cos \gamma - C_{y_2} \sin \gamma ,$$

$$F_{y_1} = F_{x_1} ,$$

and

$$F_{y_2} = F_{x_2} \cos \gamma - F_{x_3} \sin \gamma ,$$

$$F_{y_3} = F_{x_3} \cos \gamma + F_{x_2} \sin \gamma ,$$

where

$$C_{y_1} = M_{y_1} - F_{y_2}d_2 - F_{y_3}d_1 ,$$

$$C_{y_2} = M_{y_2} + F_{y_1}d_2 - F_{y_3}d_3 ,$$

$$C_{y_3} = M_{y_3} + F_{y_1}d_1 + F_{y_2}d_3 ,$$

$$M_{y_1} = M_{z_1} \cos \beta - M_{z_3} \sin \beta ,$$

and

$$M_{y_2} = M_{z_2} ,$$

$$M_{y_3} = M_{z_3} \cos \beta + M_{z_1} \sin \beta .$$

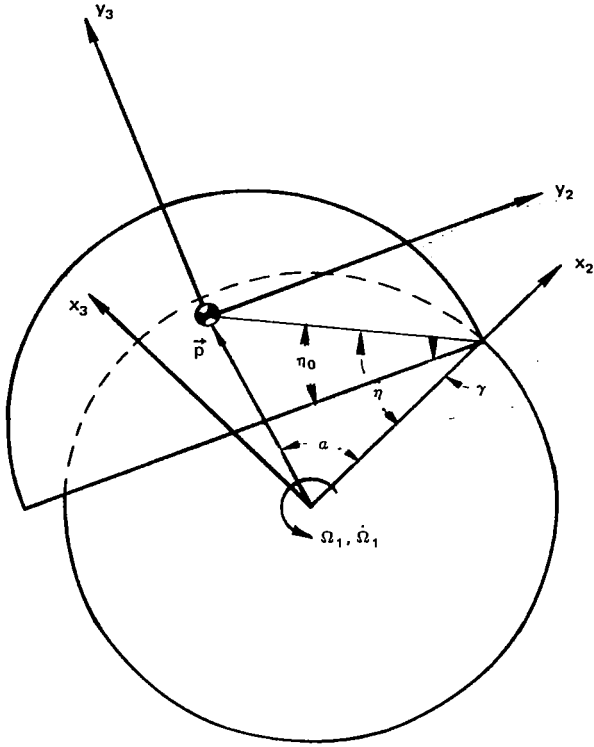


Figure 5—Deployment phase of ejection showing one ejecting clamshell.

that its  $X_1$ ,  $X_2$ , and  $X_3$ -axes parallel the  $x_1$ ,  $x_2$ , and  $x_3$ -axes of the  $x$ -frame at the instant of clamshell disengagement. This inertial frame translates at the rate established by the rocket vehicle at this time; thus,

$$\{X_j\} = K\{z_j\} + \{X_{c.m.}\},$$

where

$$K = \begin{bmatrix} C\theta C\phi & -S\theta & C\theta S\phi \\ C\psi S\theta C\phi + S\psi S\phi & C\psi C\theta & C\psi S\theta S\phi - S\psi C\phi \\ S\psi S\theta C\phi - C\psi S\phi & S\psi C\theta & S\psi S\theta S\phi + C\psi C\phi \end{bmatrix}$$

and

$$\{X_{c.m.}\} = (t - t_f) \begin{bmatrix} 0 \\ \dot{\eta}_f d_5 \sin \eta_f - \Omega_{1f} d_{7f} \sin \alpha_f \\ \dot{\eta}_f d_5 \cos \eta_f + \Omega_{1f} d_{7f} \cos \alpha_f \end{bmatrix} + \begin{bmatrix} d_6 \\ d_{7f} \cos \alpha_f \\ d_{7f} \sin \alpha_f \end{bmatrix}.$$

The square  $K$ -matrix is a direction cosine matrix based on the Euler angle system shown in Figure 6. This angular system is a variant of a system used widely by aeronautical engineers. It is utilized to

Solution of the preceding equations requires the application of Euler's equation of motion to the problem; thus,

$$M_{z_1} = J_{z_1}(\dot{\Omega}_1 - \ddot{\eta}) \cos \beta,$$

$$M_{z_2} = (J_{z_3} - J_{z_1})(\Omega_1 - \dot{\eta})^2 \cos \beta \sin \beta,$$

and

$$M_{z_3} = -J_{z_3}(\dot{\Omega}_1 - \ddot{\eta}) \sin \beta,$$

where

$$J_{z_1} = J_{cy_1} \cos^2 \beta + J_{cy_3} \sin^2 \beta - 2J_{cy_5} \cos \beta \sin \beta,$$

and

$$J_{z_2} = J_{cy_2},$$

$$J_{z_3} = J_{cy_1} \sin^2 \beta + J_{cy_3} \cos^2 \beta + 2J_{cy_5} \cos \beta \sin \beta.$$

## EQUATIONS FOR FREE FLIGHT

The free-flight displacements of the  $j$ th point on the clamshell may be expressed in terms of the  $X$ -frame, an inertial frame which is orientated so

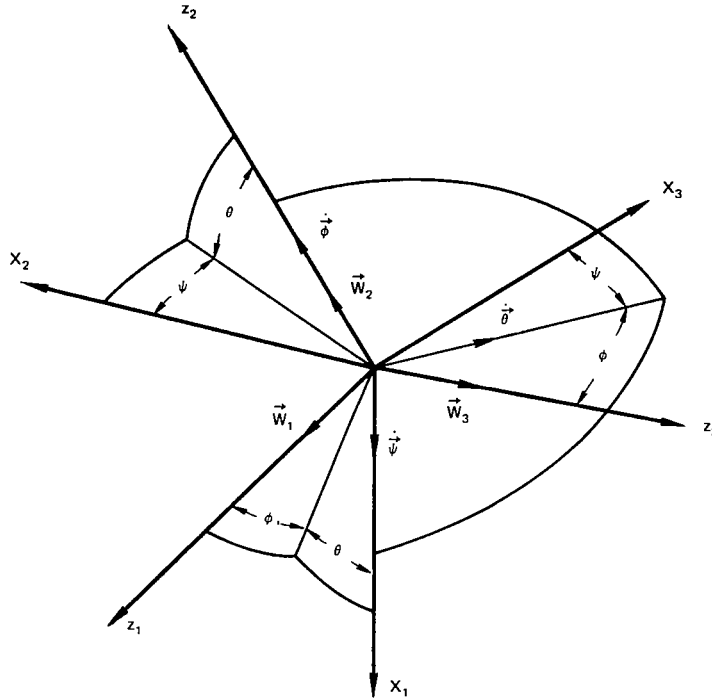


Figure 6—Euler angles and free flight coordinate systems.

simplify the determination of the initial Euler angles. From the construction in Figure 6, it can be shown that

$$\dot{\psi} = \frac{W_3 \sin \phi + W_1 \cos \phi}{\cos \theta},$$

$$\dot{\theta} = W_3 \cos \phi - W_1 \sin \phi,$$

$$\dot{\phi} = W_2 + \dot{\psi} \sin \theta,$$

$$\psi = \int^t \dot{\psi} dt - \gamma_f,$$

$$\theta = \int^t \dot{\theta} dt,$$

and

$$\phi = \int^t \dot{\phi} dt - \beta.$$

The z-frame components of the clamshell rotational rate may be obtained from Euler's equations of motion for the free flight; thus,



$$\dot{W}_1 = \frac{W_2 W_3 (J_{z_2} - J_{z_3})}{J_{z_1}},$$

$$\dot{W}_2 = \frac{W_3 W_1 (J_{z_3} - J_{z_1})}{J_{z_2}},$$

$$\dot{W}_3 = \frac{W_1 W_2 (J_{z_1} - J_{z_2})}{J_{z_3}},$$

$$W_1 = \int^t \dot{W}_1 dt + (\Omega_{1f} - \dot{\eta}_f) \cos \beta,$$

$$W_2 = \int^t \dot{W}_2 dt,$$

$$W_3 = \int^t \dot{W}_3 dt - (\Omega_{1f} - \dot{\eta}_f) \sin \beta.$$

and

## DISCUSSION

Figures 7 through 25 illustrate the results of a study of a roll-out clamshell system for the Javelin rocket vehicle. The digital computer program and a data deck utilized in this study are listed in Appendix A. Nominal system data, if the use of unaligned clamshells for which the  $\beta$ -angle is not zero is assumed, are estimated to be as follows:

$$J_{vx_1} = 7.5 \text{ slug-ft}^2,$$

$$m = 0.4 \text{ slug},$$

$$J_{cy_1} = 0.1178 \text{ slug-ft}^2,$$

$$J_{cy_2} = 0.3466 \text{ slug-ft}^2,$$

$$J_{cy_3} = 0.4200 \text{ slug-ft}^2,$$

$$J_{cy_5} = 0.03219 \text{ slug-ft}^2,$$

$$d_1 = 0.8042 \text{ ft}^2,$$

$$d_2 = 0.4286 \text{ ft}^2,$$

$$d_3 = 1.456 \text{ ft}^2,$$

$$\Omega_{10} = 9.5 \text{ rev/s},$$

$$\ddot{R}_1 = 515 \text{ ft-s}^{-2}.$$

and

When the study is applied to aligned clamshells, i.e., clamshells wherein the  $\beta$ -angle has been zeroed, the applicable clamshell parameters are changed as follows:

$$m = 0.4592 \text{ slug} ,$$

$$J_{cy_1} = 0.1656 \text{ slug-ft}^2 ,$$

$$J_{cy_2} = 0.4654 \text{ slug-ft}^2 ,$$

$$J_{cy_3} = 0.5676 \text{ slug-ft}^2 ,$$

$$J_{cy_5} = 0.0 \text{ slug-ft}^2 ,$$

$$d_2 = 0.3733 \text{ ft} ,$$

$$d_3 = 1.268 \text{ ft} .$$

and

These changes reflect the effects of alignment brought about by the attachment of two weights to each clamshell in a manner which results in minimum clamshell mass increase.

The system motion and the hinge forces and couples generated by clamshell deployment are shown in Figures 7 through 10. There appears to be no significant difference between systems using unaligned and aligned clamshells according to these figures.

It should be noted that the rocket vehicle is subject to slight spin-up followed by negligible despinning as the clamshells deploy. The individual and the total effects are of the order of a percent of the initial vehicular spin over the range of roll-out angles considered. No violation of angular momentum conservation is represented by the rocket vehicle spin-up because each clamshell is being despun as it rolls out. The vehicular spin-up signifies that the energy taken from the rotation of the clamshells is more than sufficient for their deployment. The excess energy is not large, so the spin-up is not significant. This observation applies also to the energy deficit which results in the rocket vehicle despinning at the larger roll-out angles. Thus, no special rocket vehicle despin avoidance devices are needed for the clamshell system simulated.

Reversing the rocket vehicle spin permitted a comparative study of a roll-out system with pivot axis at the clamshell leading edge. As expected, such a system subjects the rocket vehicle to greater despinning and generates hinge forces and couples of considerably larger magnitudes than the system with trailing edge pivot. These effects, illustrated in Figures 11 and 12, are attributed to the fact that the clamshells are spun up as they roll out. It will be seen that this spin-up also raises the minimum roll-out angle at which the clamshells can be safely disengaged. Thus, a roll-out system with pivot axis located at the clamshell trailing edge is preferable to a system with pivot axis at the leading edge.

It may be inferred from Figures 8 and 10 that the hinge couples are more significant to the system designer than the hinge forces. Thus, Figures 13 through 16 are included to illustrate the effects of rocket vehicle spin and longitudinal acceleration on  $C_{x_2}$  and  $C_{x_3}$ , the hinge couples which oppose the clamshell pitching and yawing tendencies, respectively. As expected, the rocket vehicle spin at the higher levels investigated produces a decidedly bad effect on  $C_{x_2}$  and  $C_{x_3}$ . On the other hand, the rocket

vehicle longitudinal acceleration tends to reduce the maximum magnitude of  $C_{x_3}$  by shifting its time trace upward. No such beneficial effect is incurred for  $C_{x_2}$  despite a similar upward shifting of its time trace. Whatever the case may be, the magnitudes of  $C_{x_2}$  and  $C_{x_3}$  indicate that serious consideration should be given to reducing the rocket vehicle spin to about a half of that presently utilized. Use of a lower rocket vehicle spin can improve the X248 motor performance in addition to moderating the design requirements of the clamshell system.

The  $X_2X_3$  projections of the near free-flight displacements of clamshells released at roll-out angles of 12.5, 15, 30, and 60 deg are shown in Figures 17 through 23. Except in Figure 19, these projections are for aligned clamshells. Since the  $X_1X_2$  and  $X_1X_3$  projections for these clamshells are straight lines, and therefore of little interest, they are not presented. Figure 19 shows that the near free-flight displacements of an unaligned clamshell under the conditions considered is not markedly different from that of an aligned clamshell. It is possible that conditions beyond the scope of this study could produce effects requiring further investigation.

Figures 17 and 20 show that roll-out clamshells can be released too soon. In each case, the clamshell rotational magnitude is too high for release at the roll-out angle shown. Obviously, clamshell release can take place safely at a lower roll-out angle with the trailing edge pivot type of system because the clamshells are subject to despinning and the offending parts are displaced farther away from the payload when disengagement occurs. The rotation of each clamshell will be near zero, and its free-flight motion thereby will be almost purely translatory when the clamshell is released at a roll-out angle of 60 deg. This effect occurs near 60 deg for the system under consideration at the various vehicle spin rates shown in Figure 24. Indeed, the angular motion of the system can be characterized by the reduced forms contained in Figure 25. This figure shows that the relationship between  $\Omega_1$  and  $\dot{\eta}$  is constant for any given roll-out angle. The locus of points in  $X$ -space through which a given part of the clamshell passes is fixed therefore by the  $\gamma$ -angle at which disengagement occurs. The vehicular spin merely affects the rate at which such a given set of points in  $X$ -space is traversed. Thus, clamshells which can be released safely at 15 deg when vehicular spin is 9.5 rev/s can also be released safely at this angle at any other positive vehicular spin if the system can bear the loads imposed upon it. That is, clamshell release for the system under consideration can be programmed for roll-out angles between 15 and 60 deg. Choice of the lower angles will be influenced by the desire to reduce unbalanced torquing of the rocket vehicle during clamshell deployment. This torquing may arise from vehicular coning motion, clamshell mismatch, and the "yo-effect" caused by nonsimultaneous release of clamshells. On the other hand, release at a higher roll-out angle is desirable because it results in the ejection of clamshells with reduced rotational motion and lowered likelihood of collision with the payload.

The system angular motions are not affected by the rocket vehicle longitudinal acceleration. The system characteristics discussed in the preceding paragraph will therefore be independent of deviations in rocket vehicle thrust. Since the various acceleration levels are normally associated with different system mass properties, it was expected that the curves in the figures discussed would reflect this fact. This mass effect, however, tends to be a minor one since it involves the interchange of a relatively small amount of energy between the rocket vehicle and the deploying clamshells.

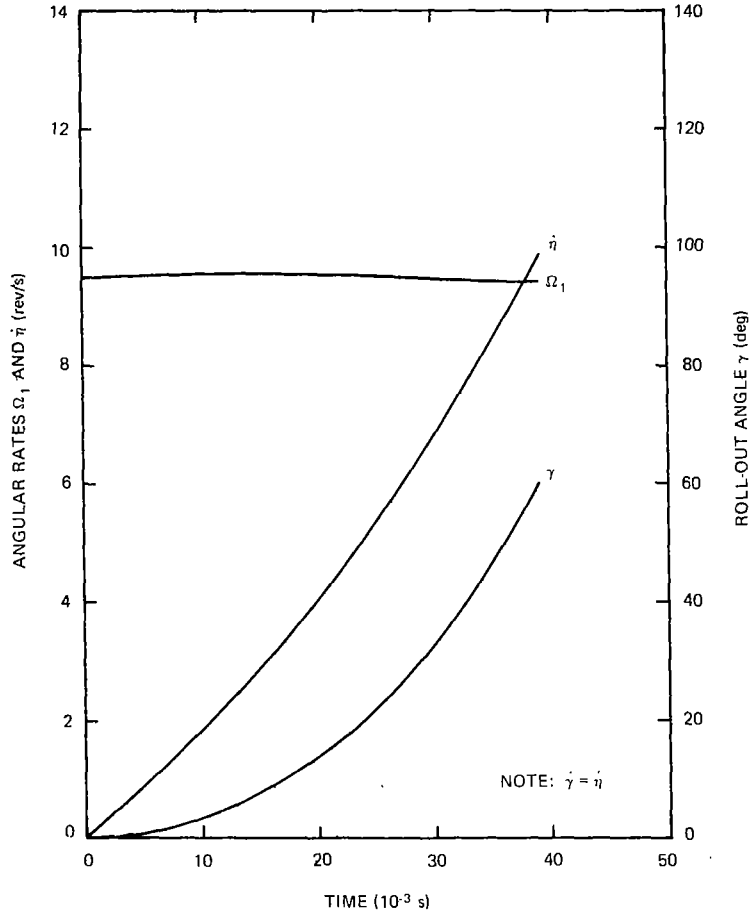


Figure 7—System motion with unaligned clamshells.

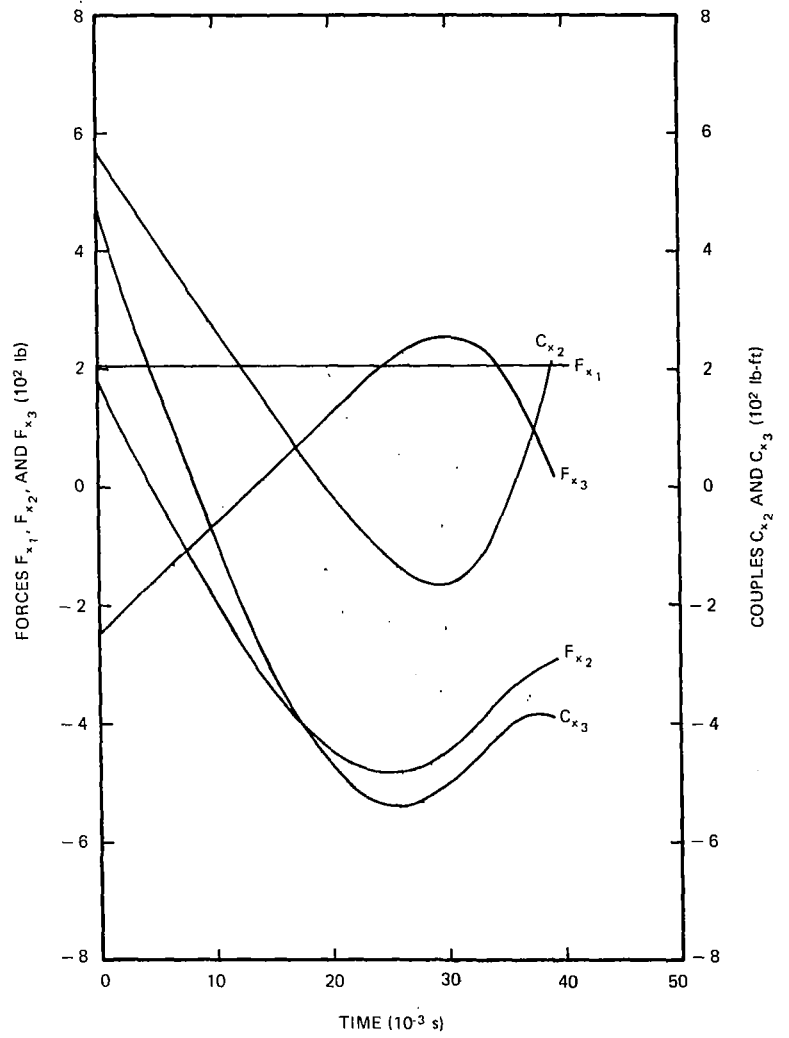


Figure 8—Forces and couples with unaligned clamshells.

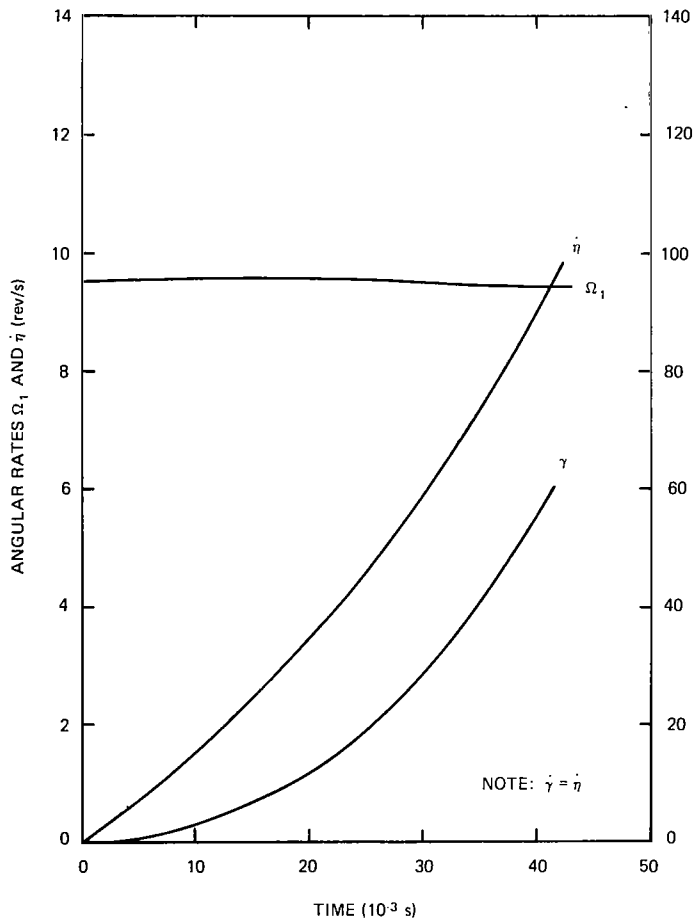


Figure 9—System motion with aligned clamshells.

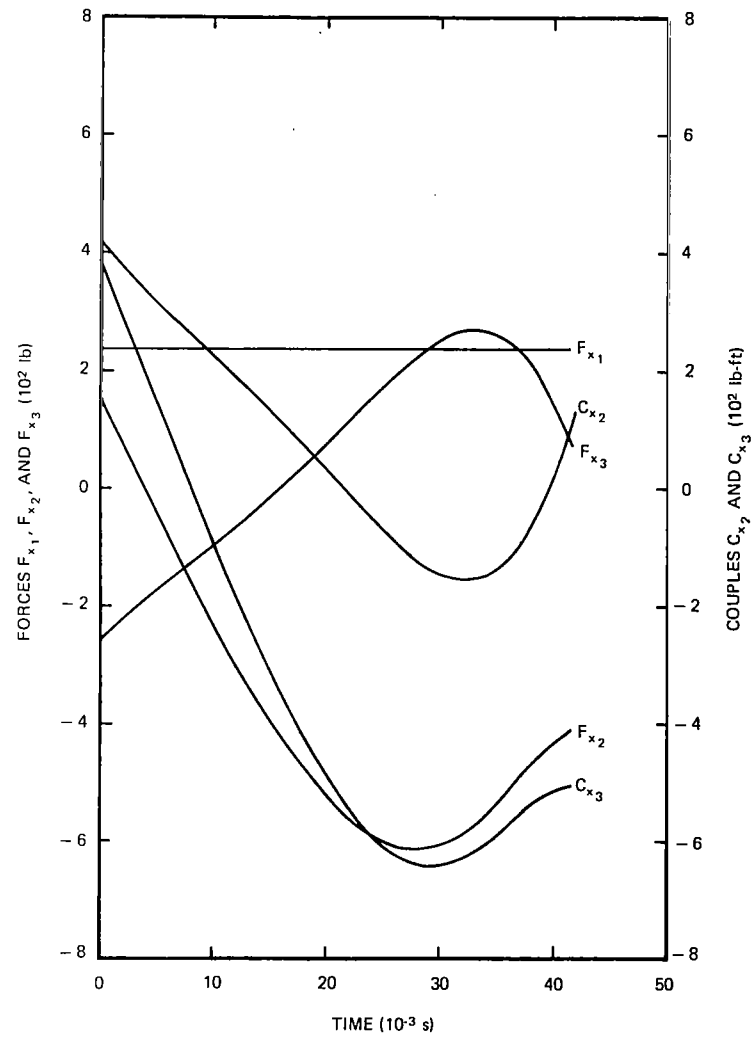


Figure 10—Forces and couples with aligned clamshells.

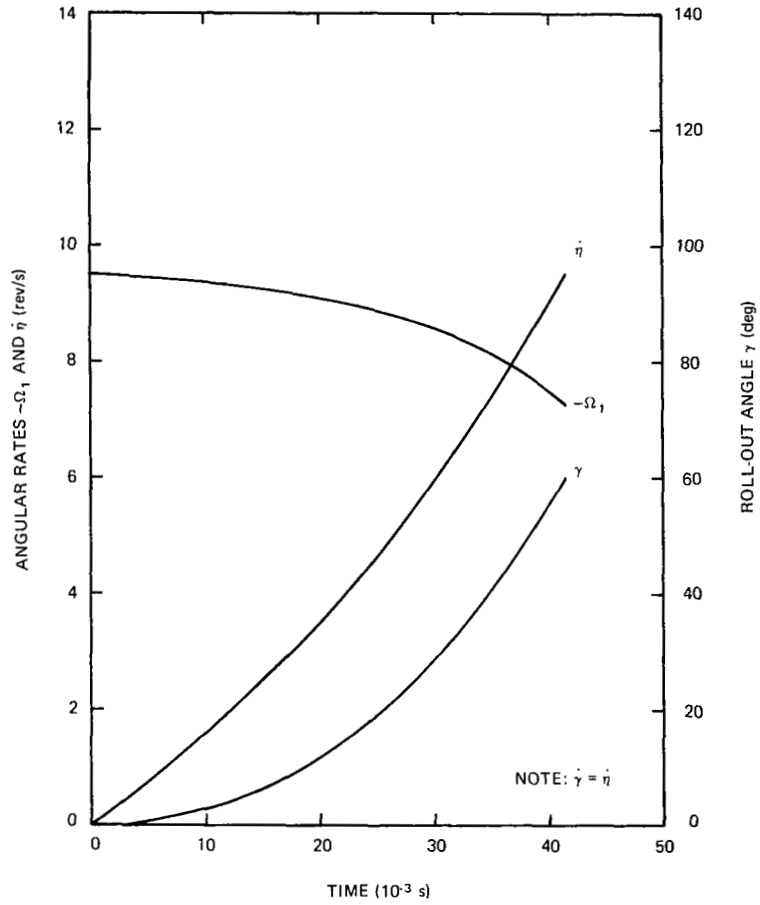


Figure 11—Effect of rocket-vehicle spin reversal on the system motion.

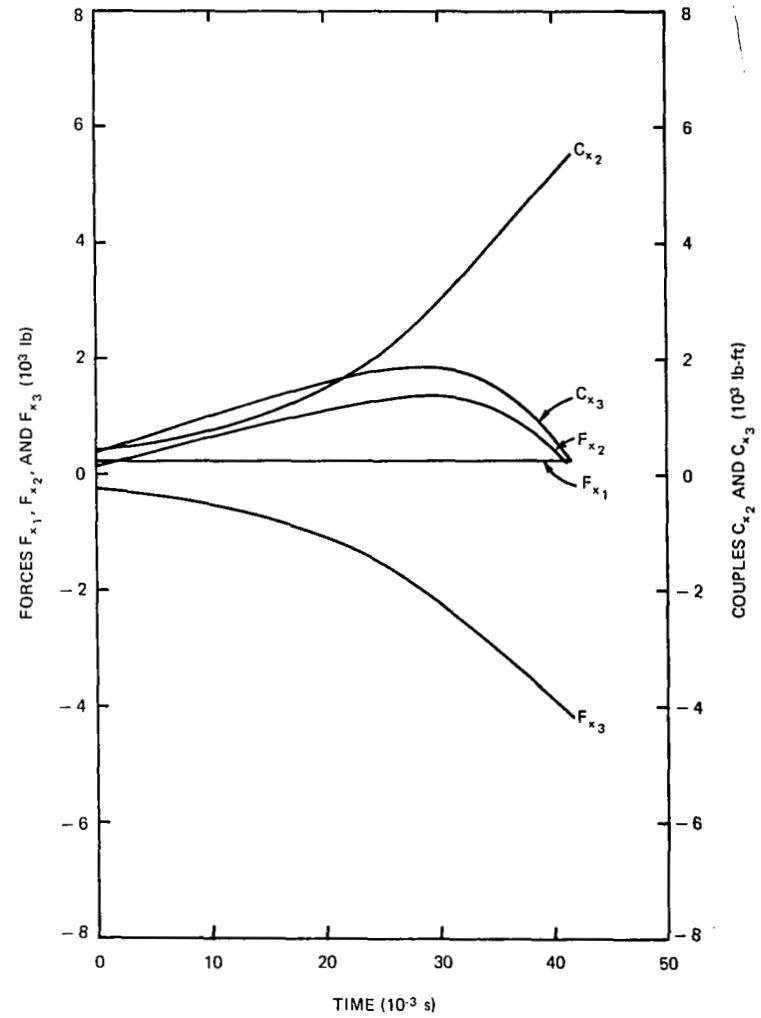


Figure 12—Effect of rocket-vehicle spin reversal on the hinge forces and couples.

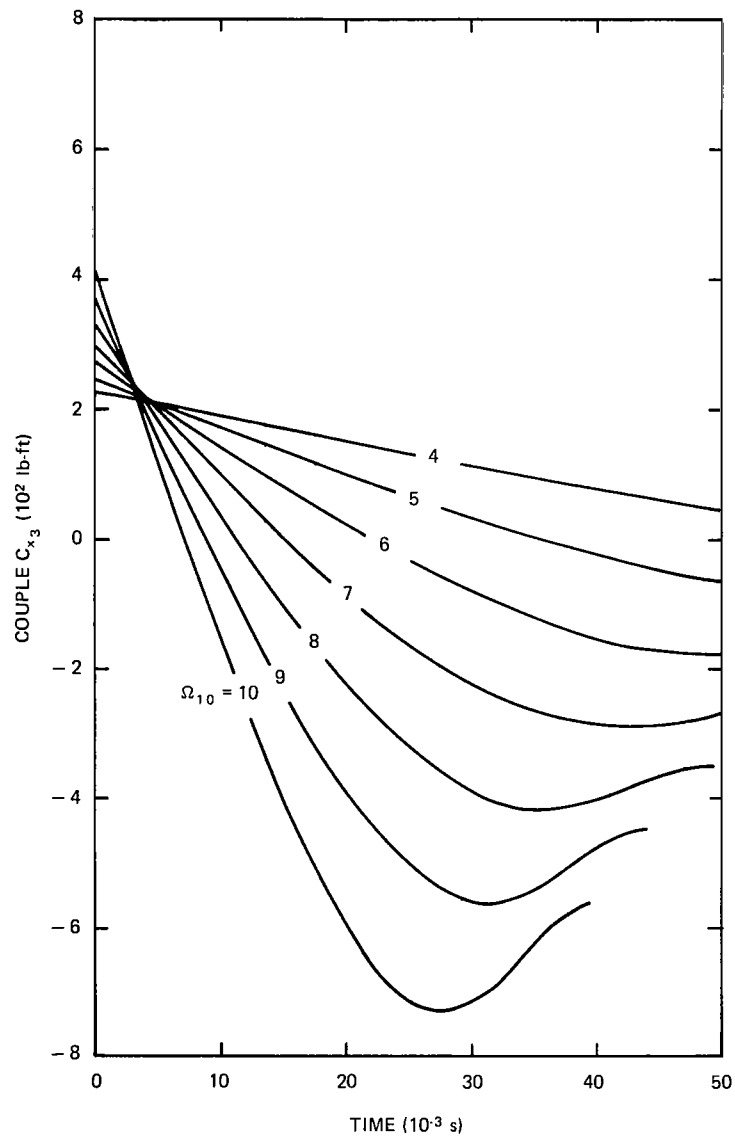


Figure 13—Effect of rocket-vehicle spin on  $C_{x3}$ .

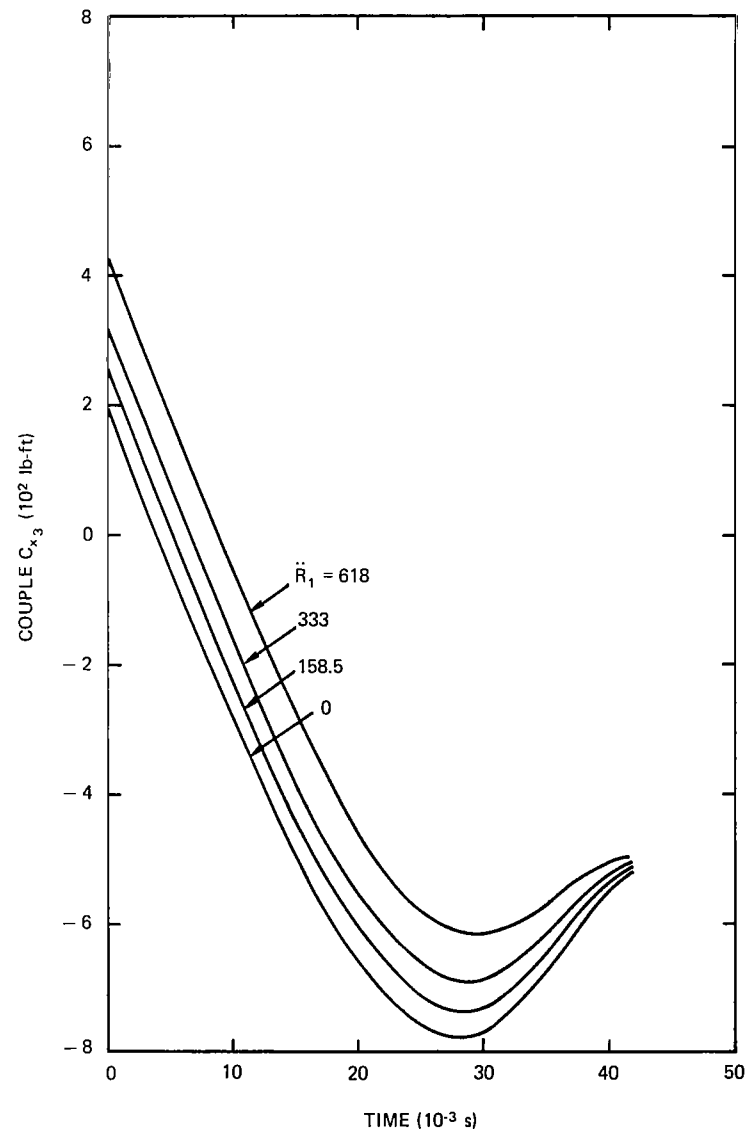


Figure 14—Effect of rocket-vehicle acceleration on  $C_{x3}$ .

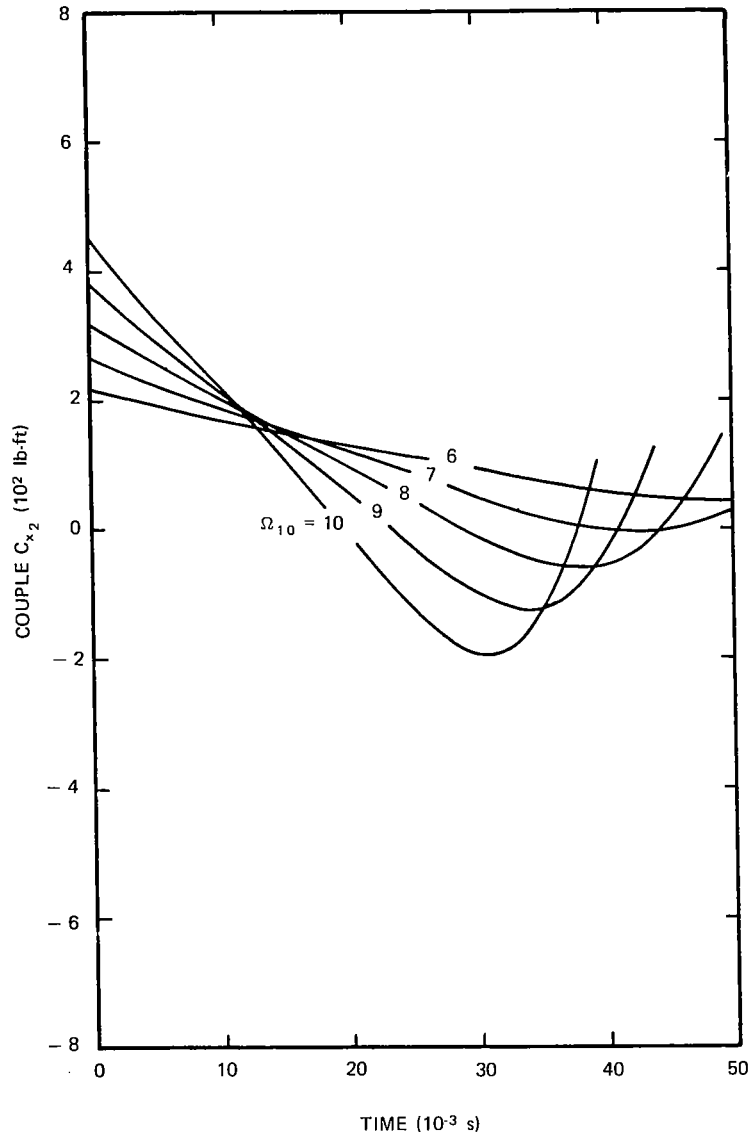


Figure 15—Effect of rocket-vehicle spin on  $C_{x_2}$ .

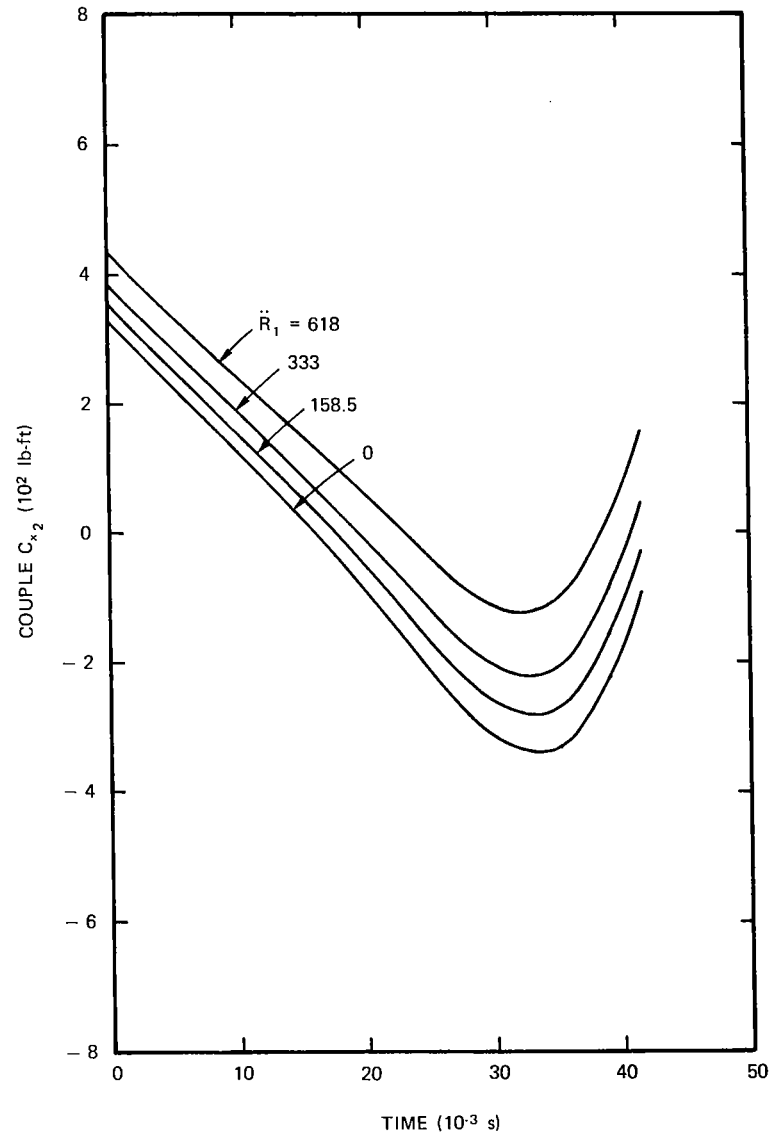


Figure 16—Effect of rocket-vehicle acceleration on  $C_{x_2}$ .



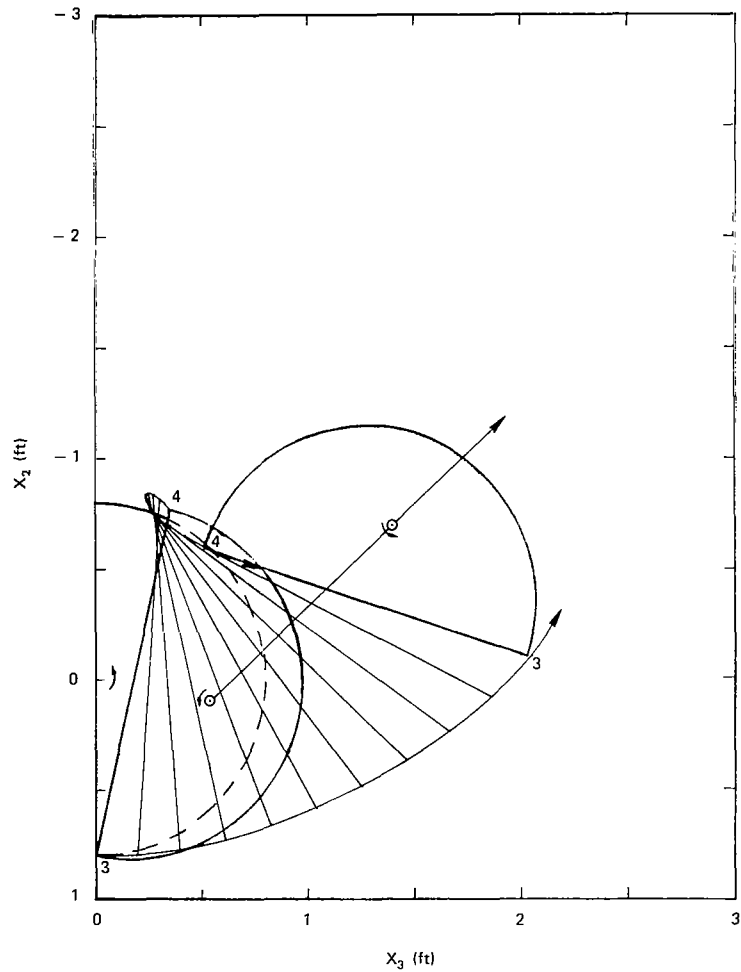


Figure 17—Near free-flight displacements of an aligned roll-out clamshell released at 12.5 deg.

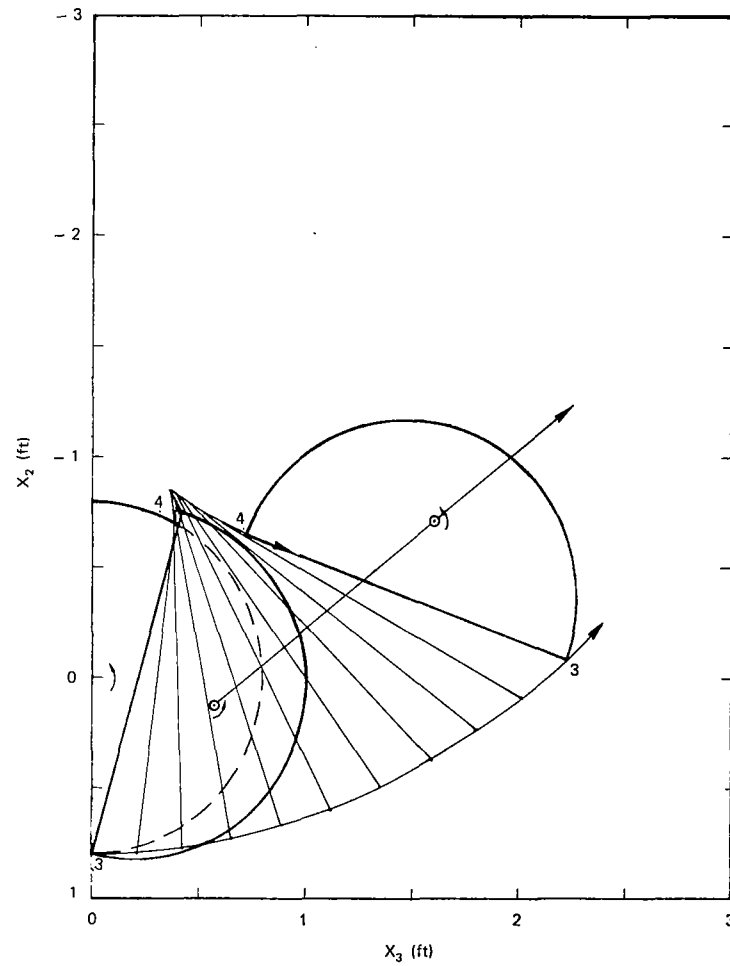


Figure 18—Near free-flight displacements of an aligned roll-out clamshell released at 15 deg.

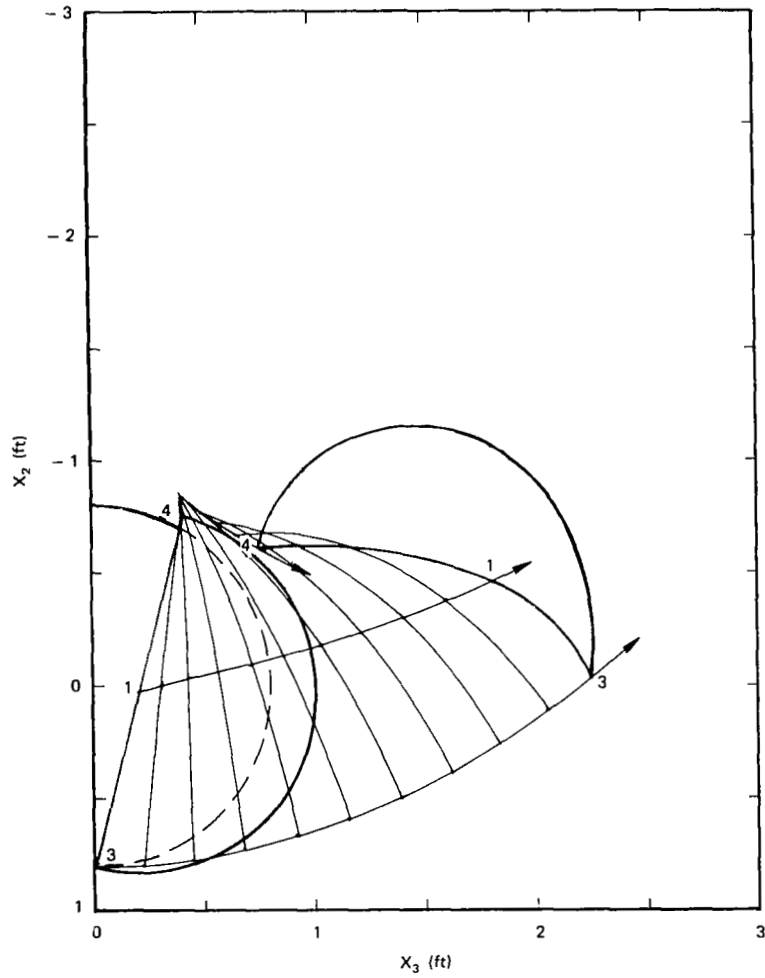


Figure 19—Near free-flight displacements of an unaligned roll-out clamshell released at 15 deg.

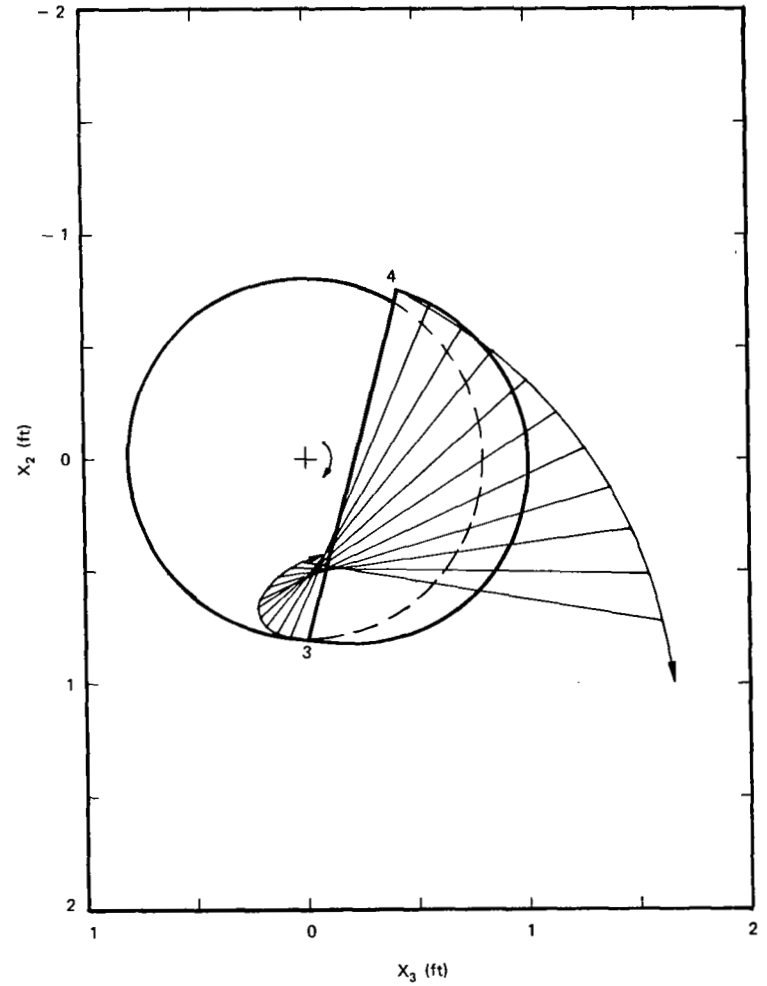


Figure 20—Effect of rocket-vehicle spin reversal on the near free-flight of an aligned clamshell released at 15 deg.

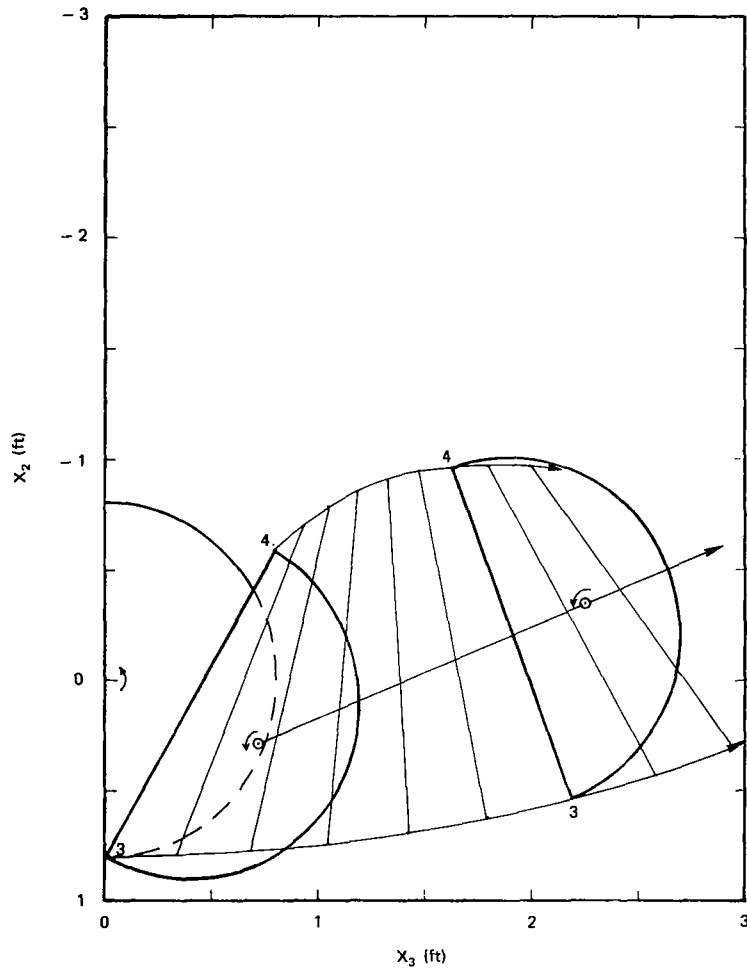


Figure 21—Near free-flight displacements of an aligned roll-out clamshell released at 30 deg.

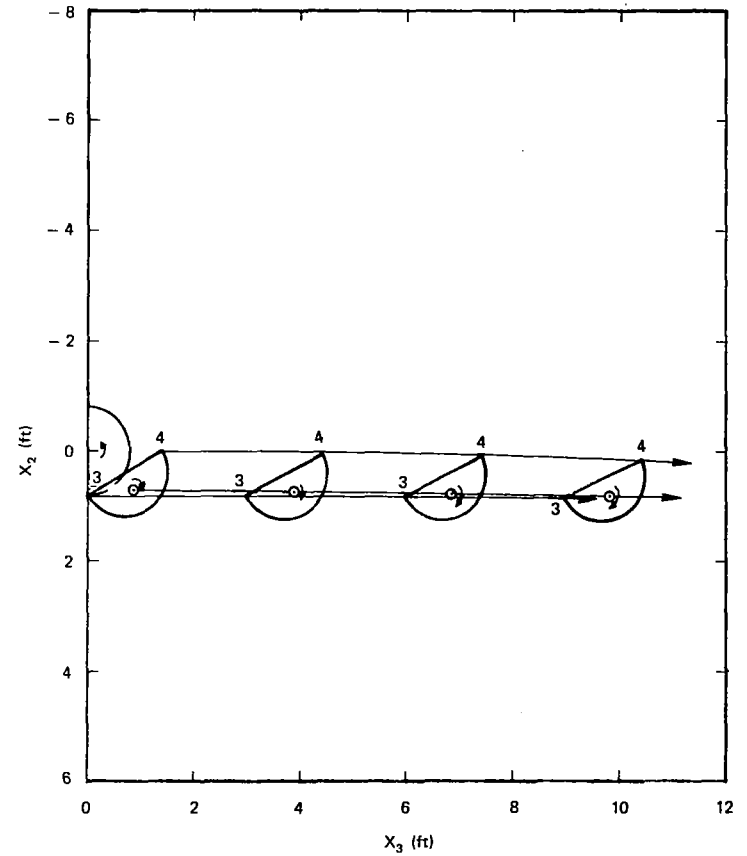


Figure 22—Near free-flight displacements of an aligned roll-out clamshell released at 60 deg.

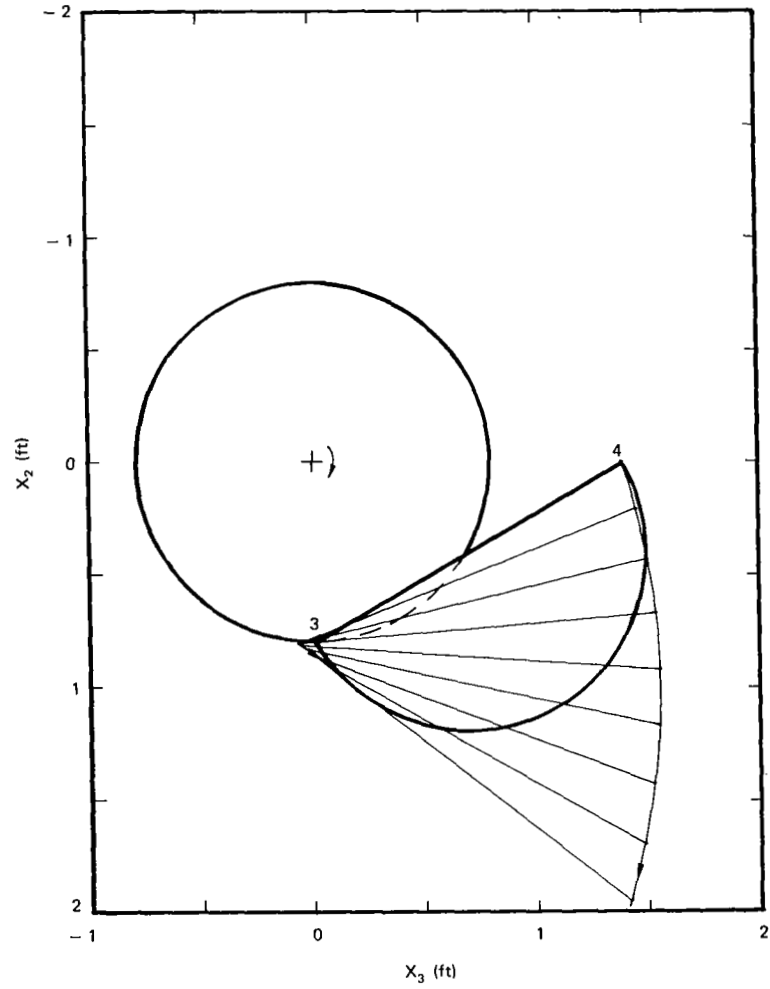


Figure 23—Effect of rocket-vehicle spin reversal on the near free-flight of an aligned clamshell released at 60 deg.

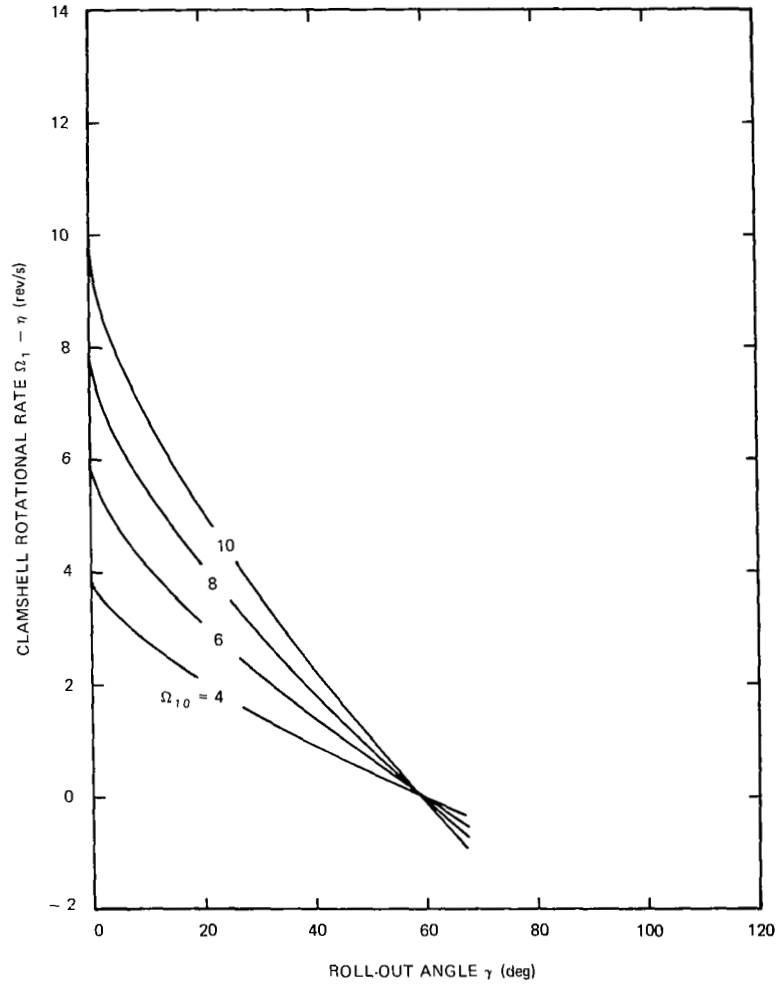


Figure 24—Clamshell rotational rate.

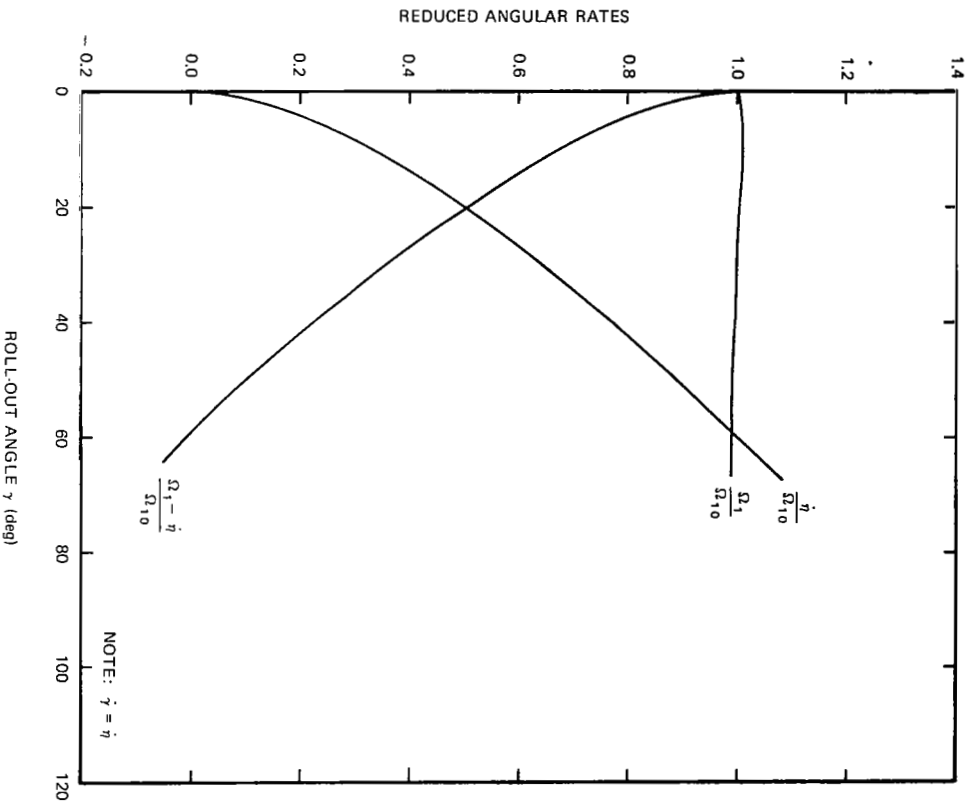


Figure 25—Angular rates for the system using aligned clamshells.

Goddard Space Flight Center  
 National Aeronautics and Space Administration  
 Greenbelt, Maryland, December 24, 1970  
 311-07-12-02-51

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Appendix A

**Source Listing of Program "ROC" and a Data Deck**

```

// EXEC FORTRAN,PARM='NAME=ROC,DECK'
//SOURCE.SYSPUNCH DD DSN=&DECK,SYSOUT=B
//SOURCEF.SYSIN DD *
C 2/21/69 - L.F.H. ROC00010
C MOD. 8/21/69 - L.F.H. ROC00020
C ROC00030
C ...MAIN PROGRAM 'ROC'... ROC00040
C PROG. ROC AND ITS SUBSIDIARY SUBPROGRAMS MAY BE UTILIZED TO STUDY ROC00050
C BOTH THE DEPLOYMENT AND THE FREE FLIGHT PHASES OF CLAMSHELL EJECTION. ROC00060
C THE TYPE OF SYSTEM THAT CAN BE STUDIED IS BASED ON A UNIQUE CLAMSHELL ROC00070
C ROLL-OUT EJECTION CONCEPT. THE FREE FLIGHT PHASE OF A GIVEN CASE IN A ROC00080
C JOB RUN MAY BE SKIPPED IF DESIRED. THE DATA LOADING IS SET SO THAT ROC00090
C THE TERMINAL CARD IN EACH LOGICAL SUBSET OF CARDS REPRESENTING A CASE ROC00100
C INPUT BE PUNCHED WITH AN INTEGER OF THE FORM 'LLLKJ' AND ADJUSTED AS ROC00110
C DESIRED BETWEEN COLUMNS 1 THROUGH 8, INCLUSIVE. IF 'J' IS ZERO, THE ROC00120
C FREE FLIGHT PHASE OF THE CASE IS SKIPPED. IF 'K' IS ZERO, THE CASE IS ROC00130
C THE LAST IN THE JOB RUN TO BE PROCESSED. THE CASE NO. IS OPTIONALLY ROC00140
C ENTERED BY PUNCHING UP TO THREE DIGITS IN 'LLL'; IF IT IS OMITTED, THE ROC00150
C CASE NO. IS EQUAL TO THE PRECEDING CASE NO. PLUS ONE. ROC00160
C L.F.H. 8/21/69. ROC00170
C ROC00180
120 FORMAT( '0',39X,'... J1 = ',I1,' ...' ) ROC00190
130 FORMAT( 80X,'RTIME = ',F8.3,' SEC.' ) ROC00200
C ROC00210
EXTERNAL SFT1,AUX1,DER1,AUX2,OUT1, ROC00220
X SET2,AUX3,DER2,AUX4,OUT2 ROC00230
C ROC00240
COMMON / LFH2 / NX(47),CBLOCK(20,220) ROC00250
REAL*8 Z(250), ROC00260
1 H,X(3),Y(8,3), ROC00270
2 DER(8,4) ROC00280
COMMON / DATA / Z,NEQ1,NEQ2,J1,J2,J3,J4,J5 ROC00290
EQUIVALENCE ROC00300
1 ( H,Z(44) ),( X(1),Z(61) ),( Y(1,1),Z(64) ), ROC00310
2 ( DER(1,1),Z(91) ) ROC00320
C ROC00330
300 CALL STIME ROC00340
CALL LOAD( Z ) ROC00350
IF( NX(20) + NX(22) .NE. 0 ) GO TO 990 ROC00360
KK = NX(9) - NX(44) ROC00370
JJ = MOD( KK,10 ) ROC00380
JK = MOD( KK,100 )/10 ROC00390
JL = MOD( KK,100000 )/100 ROC00400
IF( JL .GT. 0 ) J4 = JL ROC00410
C ROC00420
C ...1ST ( DEPLOYMENT ) PHASE... ROC00430
C ROC00440
CALL NIT1 ROC00450
CALL RK( X,Y,DER,3,H,J1,J2, ROC00460
X SET1,AUX1,DER1,AUX2,OUT1 ) ROC00470
IF( J1 .GT. 4 ) GO TO 500 ROC00480
CALL AUX1 ROC00490
CALL DER1( X,Y,DER,3,1 ) ROC00500
CALL AUX2 ROC00510
CALL OUT1( 1 ) ROC00520

```



C	IF( JJ .EQ. 0 ) GO TO 550	ROC00530
C		ROC00540
C	...2ND ( FREE FLIGHT ) PHASE...	ROC00550
C		ROC00560
	CALL NIT2	ROC00570
	CALL RKT X,Y,DER,6,H,J1,4,	ROC00580
	X SET2,AUX3,DER2,AUX4,OUT2 )	ROC00590
	IF( J1 .GT. 4 ) GO TO 500	ROC00600
	CALL AUX3	ROC00610
	CALL DER2( X,Y,DER,6,1 )	ROC00620
	CALL AUX4	ROC00630
	CALL OUT2( 1 )	ROC00640
	GO TO 550	ROC00650
C		ROC00660
	500 WRITE( 6,120 ) J1	ROC00670
	550 CALL TTIME( JTIME )	ROC00680
	RTIME = FLUAT( JTIME*26 )/1000000.	ROC00690
	WRITE( 6,130 ) RTIME	ROC00700
	IF( JK .NE. 0 ) GO TO 300	ROC00710
	GO TO 999	ROC00720
C		ROC00730
	990 IF( JK .EQ. 0 ) GO TO 999	ROC00740
	GO TO 300	ROC00750
C		ROC00760
	999 STOP	ROC00770
	END	ROC00780
C	2/22/67 - L.F.H.	LOAD0010
C	MOD. 10/23/68 - L.F.H.	LOAD0020
C		LOAD0030
	SUBROUTINE LOAD	LOAD0040
C		LOAD0050
C	...PROD. VERS...	LOAD0060
C		LOAD0070
	110 FORMAT( 20A4 )	LOAD0080
	120 FORMAT( 1X,I2,5X,20A4,2X,Z8,1X,Z8,1X,Z8 )	LOAD0090
	130 FORMAT( 15X,'...READ ERROR IN LOAD...' )	LOAD0100
C		LOAD0110
	INTEGER*2 K3,M1	LOAD0120
	COMMON / LFH2 / FWD,RD,RZ(4),	LOAD0130
	1 R1,R2,R3,R4,R5,R6,R7,R8,R9,RY(3),	LOAD0140
	2 N1,N2,N3,N4,	LOAD0150
	3 CARD(20),BLANK,	LOAD0160
	4 R30,PSW(2),K3,M1,CBLOCK(20,220)	LOAD0170
C		LOAD0180
	FWD IS NOT USED BY SUBP. LOAD OR SUBP. EDATA.	LOAD0190
	RD CONTAINS SUBP. LOAD'S SAVE AREA ADDR.	LOAD0200
	RZ'S ARE NOT USED BY SUBP. LOAD OR SUBP. EDATA.	LOAD0210
	R1 CONTAINS THE RETURN ON AN SPIE ISSUED IN SUBP. EDATA.	LOAD0220
	R2 CONTAINS A(BUST), THE SHIFTED B-ADDR. USED IN SUBP. EDATA.	LOAD0230
	R3 CONTAINS THE A(CURRENT LOAD POINT) ON EACH RETURN FROM SUBP.	LOAD0240
	EDATA.	LOAD0250
	R4 CONTAINS A(LFH2), I.E., SUBP. EDATA'S SAVE AREA ADDR.	LOAD0260
	R5 CONTAINS A(CARD), I.E., A(LFH2+88).	LOAD0270
	R6 CONTAINS A(CURRENT CARD CHARACTER IMAGE).	LOAD0280
	R7 CONTAINS A(CARD+79), I.E., A(LFH2+167).	LOAD0290



	CALL EDATA	
	GO TO ( 400,450,370 ),N1	LOAD0850
C		LOAD0860
	370 IF( N2 .EQ. 0 ) GO TO 400	LOAD0870
	IF( PSW(1) .NE. 0.0 ) PRINT 120, N2, CARD, PSW, R4	LOAD0880
	IF( PSW(1) .EQ. 0.0 ) PRINT 120, N2, CARD	LOAD0890
	400 CONTINUE	LOAD0900
	IF( K3 .LT. 1 ) GO TO 200	LOAD0910
C		LOAD0920
	450 IF( K2 .LT. J1 ) GO TO 500	LOAD0930
	470 K2 = 0	LOAD0940
	IF( K3 .EQ. 1 ) M1 = 1	LOAD0950
	500 RETURN	LOAD0960
C		LOAD0970
	600 K3 = 1	LOAD0980
	GO TO 320	LOAD0990
C		LOAD1000
	700 N4 = 32767	LOAD1010
	PRINT 130	LOAD1020
	GO TO 500	LOAD1030
	END	LOAD1040
C	2/18/69 - L.F.H.	LOAD1050
C	MOD. 7/07/69 - L.F.H.	INIT0010
C		INIT0020
	SUBROUTINE NIT1	INIT0030
C		INIT0040
C	...	INIT0050
C	...DATA INIT. FOR THE 1ST PHASE...	INIT0060
C		INIT0070
	REAL*8	INIT0080
	Z(250),	INIT0090
1	TO,HO,Q(8),	INIT0100
2	D(10),JCY(6),JZ(3),	INIT0110
3	H,ETAZ,BETA,X,Y(8),	INIT0120
4	DC(5),DS(5),	INIT0130
5	TWPI,CRTD,CDTR,PID2,PID4	INIT0140
	COMMON / DATA /	INIT0150
	Z,NEQ1,NEQ2,J1,J2,J3,J4,J5	INIT0160
	EQUIVALENCE	INIT0170
1	( TO,Z(1) ),( HO,Z(2) ),( Q(1),Z(3) ),	INIT0180
2	( D(1),Z(11) ),( JCY(1),Z(22) ),( JZ(1),Z(28) ),	INIT0190
3	( H,Z(44) ),( ETAZ,Z(46) ),( BETA,Z(47) ),	INIT0200
4	( X,Z(61) ),( Y(1),Z(64) ),	INIT0210
5	( DC(1),Z(131) ),( DS(1),Z(136) )	INIT0220
C		INIT0230
	COMMON / CONS /	INIT0240
	TWPI,CRTD,CDTR,PID2,PID4	INIT0250
C		INIT0260
	X = TO	INIT0270
	H = HO	INIT0280
	ETAZ = DATAN( D(2)/D(1) )	INIT0290
	Q(3) = ETAZ*CRTD	INIT0300
	Y(1) = Q(1)*TWPI	INIT0310
	Y(2) = Q(2)*TWPI	INIT0320
	Y(3) = ETAZ	INIT0330
	D(5) = DSQRT( D(1)**2 + D(2)**2 )	INIT0340
C		
C	...SET UP BETA AND THE PRIN. M. OF INERTIAS...	
C		

```

      IF( JCY(1) .EQ. JCY(3) ) GO TO 300
      BETA = 0.500*DATA4( 2.000*JCY(5)/( JCY(3) - JCY(1) ) )
      IF( BETA .GT. PID4 ) BETA = BETA - PID2
      IF( BETA + PID4 .LT. 0.000 ) BETA = BETA + PID2
      GO TO 310
300  BETA = 0.000
310  DC(4) = DCOS( BETA )
      DS(4) = DSIN( BETA )
      JZ(1) = JCY(1)*DC(4)**2 + JCY(3)*DS(4)**2
      1      - 2.000*JCY(5)*DC(4)*DS(4)
      JZ(2) = JCY(2)
      JZ(3) = JCY(1)*DS(4)**2 + JCY(3)*DC(4)**2
      1      + 2.000*JCY(5)*DC(4)*DS(4)
C
C 990 RETURN
      END
C 2/14/69 - L.F.H.
C MOD. 8/22/69 - L.F.H.
C
      SUBROUTINE RK( /X/,/Y/,/DER/,/NEQ/,/H/,/J1/,/JF/,
1      SETH,AUX1,DERIV,AUX2,OUT )
C
C      ...RUNGE-KUTTA 4TH ORDER INTEGRATOR...
C      FIXED STEP INTEGRATION EXCEPT FOR THE TERMINAL PROCEDURE.
C
C      X - INDEPENDENT VARIABLE.
C      Y'S - DEPENDENT VARIABLES.
C      DER'S - DERIVATIVES OF THE Y'S.
C      NEQ - NO. OF DERIVATIVE EQUATIONS.
C      H - INTEGRATION STEP SIZE.
C      J1 - BRANCHING PARAMETER SET BY SUBP. SETH FOR SUBP. RK.
C      JF - OUTPUT PRINT FREQUENCY.
C
C      SUBP. SETH - ADJUSTS H DURING THE TERMINAL INTEGRATION PROCESS AND
C      SETS J1 = 1,2,3,4, OR 5 DEPENDING ON WHETHER H IS LEFT UNCHANGED OR
C      ADJUSTED WITHOUT THE NEED TO RESET X(1) AND Y(K,1), THE INTEGRATION
C      PROCESS IS TO BE ENDED, H IS CHANGED AND THE PRECEDING INTEGRATION
C      STEP IS TO BE REPEATED WITH THE NEWER H-VALUE AND THE RESETTED X AND
C      Y-VALUES, H MUST BE CHANGED BEYOND THE MAX. ALLOWED NO. OF TIMES, OR
C      AN ABNORMAL END OF THE INTEGRATION PROCESS IS REQUIRED, RESPECTIVELY.
C      SUBP. SETH DEPENDS ON J1=0 WHENEVER SUBP. RK IS CALLED.
C      SUBP. AUX1 - COMPUTES, I.E. UPDATES, THE REQ'D DATA FOR SUBP. DERIV.
C      SUBP. DERIV - COMPUTES THE DERIV'S OF THE Y'S AT THE SUBSTEP POINTS.
C      SUBP. AUX2 - COMPUTES, I.E. UPDATES, THE ADDITIONAL DATA FOR OUTPUT.
C      SUBP. OUT - IS THE OUTPUT SUBPROGRAM.
C
C      REAL*8          X(3),Y(NEQ,3),DER(NEQ,4),H,
1      CHH,HD6
C
C      J1 = 0
C      JN = 0
C
C 400 X(2) = X(1)
      DO 410 K = 1,NEQ

```

```

INIT0350
INIT0360
INIT0370
INIT0380
INIT0390
INIT0400
INIT0410
INIT0420
INIT0430
INIT0440
INIT0450
INIT0460
INIT0470
INIT0480
INIT0490
INIT0500
RK000010
RK000020
RK000030
RK000040
RK000050
RK000060
RK000070
RK000080
RK000090
RK000100
RK000110
RK000120
RK000130
RK000140
RK000150
RK000160
RK000170
RK000180
RK000190
RK000200
RK000210
RK000220
RK000230
RK000240
RK000250
RK000260
RK000270
RK000280
RK000290
RK000300
RK000310
RK000320
RK000330
RK000340
RK000350
RK000360
RK000370
RK000380
RK000390

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410	Y(K,2) = Y(K,1)	RK000400
	IF( J1 .NE. 3 ) GO TO 415	RK000410
	IF( JN .GT. 1 .AND. MOD( JN-1,JF ) .NE. 0 ) JN = JN - 1	RK000420
C		RK000430
415	CALL SETH( X,Y,DER,NEQ,H,J1 )	RK000440
	GO TO ( 420,990,400,500,500 ),J1	RK000450
420	CONTINUE	RK000460
C		RK000470
	CALL AUX1	RK000480
	CALL DERIV( X,Y,DER,NEQ,1 )	RK000490
	IF( MOD( JN,JF ) .NE. 0 ) GO TO 425	RK000500
	CALL AUX2	RK000510
	CALL OUT( JN )	RK000520
425	CONTINUE	RK000530
C		RK000540
	CHH = 0.5D0*H	RK000550
C		RK000560
	DO 440 J = 2,4	RK000570
	IF( J .EQ. 4 ) CHH = H	RK000580
	X(1) = X(2) + CHH	RK000590
	DO 430 K = 1,NEQ	RK000600
430	Y(K,1) = Y(K,2) + CHH*DER(K,J-1)	RK000610
	CALL AUX1	RK000620
	CALL DERIV( X,Y,DER,NEQ,J )	RK000630
440	CONTINUE	RK000640
C		RK000650
	HD6 = H/6.0D0	RK000660
	X(3) = X(2)	RK000670
	DO 470 K = 1,NEQ	RK000680
	Y(K,3) = Y(K,2)	RK000690
	Y(K,1) = DER(K,1) + 2.0D0*( DER(K,2) + DER(K,3) ) + DER(K,4)	RK000700
470	Y(K,1) = Y(K,2) + HD6*Y(K,1)	RK000710
C		RK000720
	JN = JN + 1	RK000730
	GO TO 400	RK000740
C		RK000750
500	CONTINUE	RK000760
C		RK000770
990	RETURN	RK000780
	END	RK000790
C	2/14/69 - L.F.H.	1SET0010
C	MOD. 8/22/69 - L.F.H.	1SET0020
C		1SET0030
	SUBROUTINE SET1( /X/,/Y/,/DER/,/NEQ/,/H/,/J1/ )	1SET0040
C		1SET0050
C	...TERMINAL H CONTROLLER FOR THE 1ST PHASE...	1SET0060
C	X(1) AND Y(K,1) ARE RESET WHEN AN INTEG. STEP IS TO BE REPEATED.	1SET0070
C		1SET0080
	REAL*8	1SET0090
	X	7(250),
	X	YT,YEPS,
	X	FTAZ,DER(NEQ,4),
	X	H,X(NEQ),Y(NEQ,3),
	X	GAMD,TWP1,CRTD,CDTR,PID2,PID4
	COMMON / DATA /	1SET0130
	EQUIVALENCE	Z,KKK(7)
		1SET0140
		1SET0150

```

X          ( YT,Z(42) ),( YEPS,Z(43) ),      1SET0160
X          ( ETAZ,Z(46) ),( J3,KKK(5) )      1SET0170
C
COMMON / CONS /  TWPI,CRTD,CDTR,PID2,PID4    1SET0180
C
IF( J1 .EQ. 0 ) JC = 0                       1SET0190
C
...CHECK FOR TERMINAL CONDITIONS...         1SET0200
C
GAMD = ( Y(3,1) - ETAZ ) * CRTD             1SET0210
IF( GAMD .LT. 0.000 ) GO TO 500             1SFT0220
IF( DABS( ( GAMD - YT ) / YT ) .LE. YEPS ) GO TO 200 1SET0230
IF( GAMD .GT. YT ) GO TO 300               1SET0240
IF( J1 .EQ. 0 ) GO TO 100                  1SET0250
IF( Y(2,1) .LE. 0.000 .AND. DER(2,1) .LE. 0.000 ) GO TU 500 1SET0260
C
...SET J1 AS REQUIRED...                     1SET0270
C
100 J1 = 1                                   1SET0280
GO TO 990                                    1SET0290
C
200 J1 = 2                                   1SET0300
GO TO 990                                    1SET0310
C
300 JC = JC + 1                              1SET0320
IF( JC .GT. J3 ) GO TO 400                 1SET0330
IF( J1 .EQ. 0 ) GO TO 500                 1SET0340
H = 0.5D0 * H                               1SET0350
X(1) = X(3)                                 1SET0360
DO 330 K = 1,NEQ                            1SET0370
330 Y(K,1) = Y(K,3)                         1SET0380
J1 = 3                                       1SET0390
GO TO 990                                    1SET0400
C
400 J1 = 4                                   1SET0410
GO TO 990                                    1SET0420
C
500 J1 = 5                                   1SET0430
990 RETURN                                   1SET0440
END                                           1SET0450
C 2/14/69 - L.F.H.                          1SET0460
C MOD. 7/07/69 - L.F.H.                    1SET0470
C
SUBROUTINE AUX1                             1SET0480
C
...DATA UPDATER FOR THE 1ST PHASE DERIV. SUBP... 1SET0490
C
REAL*8          Z(250),                     1SET0500
1              D(10),M,JCY(6),             1SET0510
2              J VX1,GAM,ETAZ,Y(8),        1SET0520
3              DC(5),DS(5),                1SET0530
4              F(6),F23,                   1SET0540
5              QOM,QET,                     1SET0550
6              A,B,C,DD,U,V                1AUX0010
COMMON / DATA /  Z,NEQ1,NEQ2,J1,J2,J3,J4,J5 1AUX0020

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	EQUIVALENCE		1AUX0160
1	( D(1),Z(11) ),( M,Z(21) ),( JCY(1),Z(22) ),		1AUX0170
2	( J VX1,Z(31) ),( GAM,Z(32) ),( ET AZ,Z(46) ),		1AUX0180
3	( Y(1),Z(64) ),		1AUX0190
4	( DC(1),Z(131) ),( DS(1),Z(136) ),		1AUX0200
5	( F(1),Z(141) ),( F23,Z(147) )		1AUX0210
	COMMON / DBX1 / A,B,C,DD,U,V		1AUX0220
C			1AUX0230
C	DC(1) = DCOS( Y(3) )		1AUX0240
	DS(1) = DSIN( Y(3) )		1AUX0250
C			1AUX0260
	GAM = Y(3) - ET AZ		1AUX0270
	DC(2) = DCOS( GAM )		1AUX0280
	DS(2) = DSIN( GAM )		1AUX0290
C			1AUX0300
	D(7) = DSQRT( D(1)**2 + D(5)**2 - 2.000*D(5)*D(1)*DC(1) )		1AUX0310
C			1AJX0320
	F(2) = M*( Y(2)**2 )*D(5)		1AUX0330
	F(3) = 2.000*M*Y(1)*Y(2)*D(5)		1AUX0340
	F23 = F(2) - F(3)		1AUX0350
	CALL FF6		1AUX0360
C			1AUX0370
	DD = 2.000*( JCY(1) + M*( D(5)**2 ) )		1AUX0380
	A = J VX1 + 2.000*( JCY(1) + M*( D(7)**2 ) )		1AUX0390
	B = - DD + 2.000*M*D(5)*D(1)*DC(1)		1AUX0400
	C = B		1AUX0410
C			1AUX0420
	QDM = 0.000		1AUX0430
	QET = F(6)*D(1)		1AUX0440
	U = QDM + 2.000*F23*D(1)*DS(1)		1AUX0450
	V = QET + 2.000*M*( Y(1)**2 )*D(5)*D(1)*DS(1)		1AUX0460
C			1AUX0470
	990 RETURN		1AUX0480
	END		1AUX0490
C	2/14/69 - L.F.H.		1AJX0500
C			1DER0010
	SUBROUTINE DER1( X,Y,DER,NEQ,J )		1DER0020
C			1DER0030
	...DERIV. F0'S. FOR THE 1ST PHASE...		1DER0040
C			1DER0050
	REAL*8 X,Y(NEQ),DER(NEQ,4),		1DER0060
	1 A,B,C,D,U,V,DET		1DER0070
C			1DER0080
	COMMON / DBX1 / A,B,C,D,U,V		1DER0090
C			1DER0100
	DET = A*D - B*C		1DER0110
C			1DER0120
	DER(1,J) = ( D*U - B*V )/DET		1DER0130
	DER(2,J) = ( A*V - C*U )/DET		1DER0140
	DER(3,J) = Y(2)		1DER0150
C			1DER0160
	990 RETURN		1DER0170
	END		1DER0180
C	2/14/69 - L.F.H.		1DER0190
			2AUX0010

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C MOD. 7/07/69 - L.F.H.
C
C SUBROUTINE AUX2
C
C ...DATA UPDATER FOR THE 1ST PHASE OUTPUT...
C
REAL*8          Z(250),
1              D(10),M,JZ(3),
2              AX1,Y(8),DER(8),
3              DC(5),DS(5),
4              F(6),F23,
5              FX(3),FY(3),
6              MZ(3),MY(3),
7              CY(3),CX(3),
8              GAM,GAMD,TWPI,CRTD,CDTR,PID2,PID4,ZZZ
COMMON / DATA / Z,NEQ1,NEQ2,J1,J2,J3,J4,J5
EQUIVALENCE
1              ( D(1),Z(11) ),( M,Z(21) ),( JZ(1),Z(28) ),
2              ( AX1,Z(45) ),( Y(1),Z(64) ),( DER(1),Z(91) ),
3              ( DC(1),Z(131) ),( DS(1),Z(136) ),
4              ( F(1),Z(141) ),( F23,Z(147) ),
5              ( FX(1),Z(151) ),( FY(1),Z(154) ),
6              ( MZ(1),Z(161) ),( MY(1),Z(164) ),
7              ( CY(1),Z(171) ),( CX(1),Z(174) ),
COMMON / CONS / TWPI,CRTD,CDTR,PID2,PID4
C
F(1) = M*DER(2)*D(5)
F(4) = M*DER(1)*D(7)
F(5) = M*( Y(1)**2 )*D(7)
C
DC(3) = ( D(1) - D(5)*DC(1) )/D(7)
DS(3) = D(5)*DS(1)/D(7)
C
CALL FAX1
FX(1) = M*AX1
FX(2) = F(1)*DS(1) + F23*DC(1) - F(4)*DS(3)
1      - F(5)*DC(3) - F(6)*DS(2)
FX(3) = F(1)*DC(1) - F23*DS(1) + F(4)*DC(3)
1      - F(5)*DS(3) - F(6)*DC(2)
C
FY(1) = FX(1)
FY(2) = FX(2)*DC(2) - FX(3)*DS(2)
FY(3) = FX(3)*DC(2) + FX(2)*DS(2)
C
ZZZ = DER(1) - DER(2)
MZ(1) = JZ(1)*ZZZ*DC(4)
MZ(2) = ( JZ(3) - JZ(1) )*( ( Y(1) - Y(2) )**2 )*DC(4)*DS(4)
MZ(3) = - JZ(3)*ZZZ*DS(4)
C
MY(1) = MZ(1)*DC(4) - MZ(3)*DS(4)
MY(2) = MZ(2)
MY(3) = MZ(3)*DC(4) + MZ(1)*DS(4)
C
CY(1) = MY(1) - FY(2)*D(2) - FY(3)*D(1)
2AUX0020
2AUX0030
2AUX0040
2AUX0050
2AUX0060
2AUX0070
2AUX0080
2AUX0090
2AUX0100
2AUX0110
2AUX0120
2AUX0130
2AUX0140
2AUX0150
2AUX0160
2AUX0170
2AUX0180
2AUX0190
2AUX0200
2AUX0210
2AUX0220
2AUX0230
2AUX0240
2AUX0250
2AUX0260
2AUX0270
2AUX0280
2AUX0290
2AUX0300
2AUX0310
2AUX0320
2AUX0330
2AUX0340
2AUX0350
2AUX0360
2AUX0370
2AUX0380
2AUX0390
2AUX0400
2AUX0410
2AUX0420
2AUX0430
2AUX0440
2AUX0450
2AUX0460
2AUX0470
2AUX0480
2AUX0490
2AUX0500
2AUX0510
2AUX0520
2AUX0530
2AUX0540
2AUX0550
2AUX0560

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	CY(2) = MY(2) + FY(1)*D(2) - FY(3)*D(3) + F(6)*D(4)	2AUX0570
	CY(3) = MY(3) + FY(1)*D(1) + FY(2)*D(3)	2AUX0580
C		2AUX0590
	CX(1) = CY(1)	2AUX0600
	CX(2) = CY(2)*DC(2) + CY(3)*DS(2)	2AUX0610
	CX(3) = CY(3)*DC(2) - CY(2)*DS(2)	2AUX0620
C		2AUX0630
	GAMD = GAM*CRTD	2AUX0640
C		2AUX0650
	990 RETURN	2AUX0660
	END	2AUX0670
C	2/18/69 - L.F.H.	FAX00010
C		FAX00020
	SUBROUTINE FAX1	FAX00030
C		FAX00040
C	...DUMMY LONGIT. ACCELERATION SUBP...	FAX00050
C		FAX00060
	RETURN	FAX00070
	END	FAX00080
C	2/18/69 - L.F.H.	6FF00010
C	MOD. 7/07/69 - L.F.H.	6FF00020
C		6FF00030
	SUBROUTINE FF6	6FF00040
C		6FF00050
	REAL*8 Z(250),	6FF00060
X	F(6)	6FF00070
	COMMON / DATA / Z,NEQ1,NEQ2,J1,J2,J3,J4,J5	6FF00080
	EQUIVALENCE	6FF00090
X	( F(1),7(141) )	6FF00100
C		6FF00110
	300 F(6) = 0.000	6FF00120
C		6FF00130
	990 RETURN	6FF00140
	END	6FF00150
C	3/26/69 - L.F.H.	1OUT0010
C	MOD. 9/24/69 - L.F.H.	1OUT0020
C		1OUT0030
	SUBROUTINE OUT1( JJ )	1OUT0040
C		1OUT0050
C	...OUTPUT SUBP. FOR THE 1ST PHASE...	1OUT0060
C		1OUT0070
	110 FORMAT( '1' / '0',39X,'...BASE DATA...' / 1X	1OUT0080
X	/ 5X,'T0 - INITIAL TIME ( SEC ).'	1OUT0090
X	/ 5X,'H0 - INITIAL INTEGRATOR TIME STEP SIZE ( SEC ).'	1OUT0100
X	/ 5X,'Q(1)...Q(3) - INITIAL OMEGA, ETA-DOT, AND ETA '	1OUT0110
X	' ( RPS, RPS, DEG ).'	1OUT0120
X	/ 5X,'D(1)...D(8) - CLAMSHELL GEOMETRIC PARAMETERS ( FT ).'	1OUT0130
X	/ 5X,'M - CLAMSHELL MASS ( SLUG ).'	1OUT0140
X	/ 5X,'JCY(1)...JCY(6) - CLAMSHELL Y-FRAME '	1OUT0150
X	'MOMENTS AND PRODUCTS OF INERTIA ( SLUG*FT**2 ).'	1OUT0160
X	/ 5X,'JZ(1)...JZ(3) - CLAMSHELL Z-FRAME I.E. PRINCIPAL '	1OUT0170
X	'MOMENTS OF INERTIA ( SLUG*FT**2 ).'	1OUT0180
X	/ 5X,'JVX1 - CENTRAL BODY ROLL MOMENT OF INERTIA '	1OUT0190
X	' ( SLUG*FT**2 ).'	1OUT0200
X	/ 5X,'YT - TERMINAL GAMMA ( DEG ).'	1OUT0210

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X / 5X,'YEPS - TERMINAL GAMMA CONVERGENCE CRITERION ( DEG ).' 1OUT0220
X / 5X,'AX1 - SYSTEM X1 ACCELERATION ( FT/SEC**2 ).' ) 1OUT0230
115 FORMAT( '1' / '0',39X,'...BASE DATA...' ) 1OUT0240
120 FORMAT( 'OCASE NO. ',I3,5X,10A8 / 1X 1OUT0250
X / 6X,'TO,H0,Q(J)...',1P5D12.4 1OUT0260
X / 12X,'D(J)...',1P8D12.4 1OUT0270
X / 8X,'M,JCY(J)...',1P7D12.4 1OUT0280
X / 6X,'JZ(J),JVX1...',1P4D12.4 1OUT0290
X / 5X,'YT,YEPS,AX1...',1P3D12.4 ) 1OUT0300
130 FORMAT( '1' / 'OCASE NO. ',I3,5X,10A8 1OUT0310
X / 38X,'1ST PHASE OUTPUT' / 1X 1OUT0320
X / 5X,'T - ELAPSED TIME ( SEC ).' 1OUT0330
X / 5X,'GAMD - CLAMSHELL ROLL-OUT ANGLE ( DEG ).' 1OUT0340
X / 5X,'Y(3) - CLAMSHELL ETA-ANGLE ( DEG ).' 1OUT0350
X / 5X,'Y(2) - CLAMSHELL ROLL-OUT RATE ( RPS ).' 1OUT0360
X / 5X,'Y(1) - SYSTEM ROLL RATE ( RPS ).' 1OUT0370
X / 5X,'DER(2) - CLAMSHELL ROLL-OUT ACCELERATION ( RAD/SEC**2 ).' 1OUT0380
X / 5X,'DER(1) - SYSTEM ROLL ACCELERATION ( RAD/SEC**2 ).' 1OUT0390
X / 5X,'F(J) - INERTIAL AND APPLIED FORCES ( LB ).' 1OUT0400
X / 5X,'FX(J) - X-FRAME HINGE FORCE COMPONENTS ( LB ).' 1OUT0410
X / 5X,'CX(J) - X-FRAME HINGE COUPLE COMPONENTS ( FT-LB ).' 1OUT0420
X / '0' / 55X,'...' 1OUT0430
X / '0',15X,'T',9X,'GAMD',8X,'Y(3)', 1OUT0440
X 8X,'Y(2)',8X,'Y(1)',7X,'DER(2)',6X,'DER(1)' 1OUT0450
X / '0',25X,'F(1)',8X,'F(2)',8X,'F(3)', 1OUT0460
X 8X,'F(4)',8X,'F(5)',8X,'F(6)' 1OUT0470
X / '0',25X,'FX(1)',7X,'FX(2)',7X,'FX(3)', 1OUT0480
X 7X,'CX(1)',7X,'CX(2)',7X,'CX(3)' ) 1OUT0490
140 FORMAT( '1' / 'OCASE NO. ',I3,5X,10A8 1OUT0500
X / 38X,'1ST PHASE OUTPUT' ) 1OUT0510
150 FORMAT( 1X / 10X,1P7D12.4 / ( 22X,1P6D12.4 ) ) 1OUT0520
C 1OUT0530
C 1OUT0540
REAL*8 Z(250), 1OUT0550
X TO,H0,Q(3),D(8),M,JCY(6), 1OUT0560
X JZ(3),JVX1,GAMD, 1OUT0570
X YT,YEPS,AX1, 1OUT0580
X X,Y(3),DER(3),F(6),FX(3),CX(3), 1OUT0590
X TITLE(10) 1OUT0600
REAL*8 YY(3) 1OUT0610
REAL*8 TWPI,CRTO,CDTR,PID2,PID4 1OUT0620
COMMON / CONS / TWPI,CRTO,CDTR,PID2,PID4 1OUT0630
COMMON / DATA / Z,NEQ1,NEQ2,J1,J2,J3,J4,J5 1OUT0640
EQUIVALENCE 1OUT0650
X ( TO,Z(1) ),( H0,Z(2) ),( Q(1),Z(3) ), 1OUT0660
X ( D(1),Z(11) ),( M,Z(21) ),( JCY(1),Z(22) ), 1OUT0670
X ( JZ(1),Z(28) ),( JVX1,Z(31) ),( GAMD,Z(33) ), 1OUT0680
X ( YT,Z(42) ),( YEPS,Z(43) ),( AX1,Z(45) ), 1OUT0690
X ( X,Z(61) ),( Y(1),Z(64) ),( DER(1),Z(91) ), 1OUT0700
X ( F(1),Z(141) ), 1OUT0710
X ( FX(1),Z(151) ),( CX(1),Z(174) ), 1OUT0720
X ( TITLE(1),Z(241) ) 1OUT0730
C 1OUT0740
C DATA JK/ 0 /, NCASE/ 0 / 1OUT0750
C 1OUT0760

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      IF( JJ .NE. 0 ) GO TO 400
      IF( NCASE .NF. J4 ) GO TO 230
      NCASE = J4 + 1
      J4 = NCASE
      GO TO 240
230  NCASE = J4
240  IF( JK .EQ. 0 ) WRITE( 6,110 )
250  IF( JK .NE. 0 ) WRITE( 6,115 )
C
      WRITE( 6,120 )      NCASE,TITLE,
X          TO,H0,Q,
X          D,
X          M,JCY,
X          J7,JVX1,
X          YT,YEPS,AX1
300  JK = 255
C
      WRITE( 6,130 )      NCASE,TITLE
      JL = 20
C
400  IF( MOD( JL,56 ) .NE. 0 ) GO TO 500
      WRITE( 6,140 )      NCASE ,TITLE
      JL = 0
C
500  YY(1) = Y(1)/TWPI
      YY(2) = Y(2)/TWPI
      YY(3) = Y(3)*CRTD
      WRITE( 6,150 )
X          X,GAMD,YY(3),YY(2),YY(1),DER(2),DER(1),
X          F,
X          FX,CX
      JL = JL + 4
C
990  RETURN
      END
C 2/26/69 - L.F.H.
C MOD. 9/03/69 - L.F.H.
C
      SUBROUTINE NIT2
C
C          ...DATA INIT. FOR THE 2ND PHASE...
C
      REAL*8          Z(250),
X          D(10),
X          GAM,XT,
X          H,BETA,
X          XF,
X          X,Y(8),W(8),
X          DC(5),DS(5),
X          D7CA,D7SA,
X          DXCM(3),P(3,4),
X          D8M3,D1M2,Y1M2,ZZZ,
X          TWPI,CRTD,CDTR,PID2,PID4
      COMMON / DATA / Z,NEQ1,NEQ2,J1,J2,J3,J4,J5
      EQUIVALENCE
10UT0770
10UT0780
10UT0790
10UT0800
10UT0810
10UT0820
10UT0830
10UT0840
10UT0850
10UT0860
10UT0870
10UT0880
10UT0890
10UT0900
10UT0910
10UT0920
10UT0930
10UT0940
10UT0950
10UT0960
10UT0970
10UT0980
10UT0990
10UT1000
10UT1010
10UT1020
10UT1030
10UT1040
10UT1050
10UT1060
10UT1070
10UT1080
10UT1090
10UT1100
10UT1110
2NIT0010
2NIT0020
2NIT0030
2NIT0040
2NIT0050
2NIT0060
2NIT0070
2NIT0080
2NIT0090
2NIT0100
2NIT0110
2NIT0120
2NIT0130
2NIT0140
2NIT0150
2NIT0160
2NIT0170
2NIT0180
2NIT0190
2NIT0200

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X          ( D(1),Z(11) ),                2NIT0210
X          ( GAM,Z(32) ),( XT,Z(41) ),    2NIT0220
X          ( H,Z(44) ),( BETA,Z(47) ),    2NIT0230
X          ( XF,Z(51) ),                  2NIT0240
X          ( X,Z(61) ),( Y(1),W(1),Z(64) ), 2NIT0250
X          ( DC(1),Z(131) ),( DS(1),Z(136) ), 2NIT0260
X          ( D7CA,Z(141) ),( D7SA,Z(142) ), 2NIT0270
X          ( DXCM(1),Z(151) ),( P(1,1),Z(161) ) 2NIT0280
C
COMMON / CONS / TWPI,CRTD,CDTR,PID2,PID4  2NIT0290
C
EQUIVALENC ( D8M3,D1M2,Y1M2,ZZZ )       2NIT0300
C
XF = X                                     2NIT0310
C
...BODY POINT DISPLACEMENTS IN THE Z-FRAME... 2NIT0320
C
D8M3 = D(8) - D(3)                        2NIT0330
P(1,1) = D8M3*DC(4) - D(2)*DS(4)         2NIT0340
P(2,1) = 0.000                            2NIT0350
P(3,1) = - D(2)*DC(4) - D8M3*DS(4)       2NIT0360
D1M2 = D(1) - D(2)                        2NIT0370
P(1,2) = - D(3)*DC(4) + D1M2*DS(4)       2NIT0380
P(2,2) = 0.000                            2NIT0390
P(3,2) = D1M2*DC(4) + D(3)*DS(4)         2NIT0400
P(1,3) = - D(3)*DC(4) - D(2)*DS(4)       2NIT0410
P(2,3) = D(1)                             2NIT0420
P(3,3) = - D(2)*DC(4) + D(3)*DS(4)       2NIT0430
P(1,4) = P(1,3)                          2NIT0440
P(2,4) = - D(1)                          2NIT0450
P(3,4) = P(3,3)                          2NIT0460
C
...BODY C.M. DISPLACEMENT RATES...        2NIT0470
C
D7CA = D(7)*DC(3)                         2NIT0480
D7SA = D(7)*DS(3)                         2NIT0490
DXCM(2) = Y(2)*D(5)*DS(1) - Y(1)*D7SA    2NIT0500
DXCM(3) = Y(2)*D(5)*DC(1) + Y(1)*D7CA    2NIT0510
C
...INIT. BODY FIXED Z-FRAME ANGULAR RATES... 2NIT0520
C
Y1M2 = Y(1) - Y(2)                       2NIT0530
W(1) = Y1M2*DC(4)                        2NIT0540
W(2) = 0.000                              2NIT0550
W(3) = - Y1M2*DS(4)                      2NIT0560
C
...INIT. EULERIAN ANGLES...               2NIT0570
C SEE NOTES IN SUBP. DER2 AND SUBP. AUX4 ON ROTATIONAL TRANSFORMATION. 2NIT0580
C
W(4) = - GAM                              2NIT0590
W(5) = 0.000                              2NIT0600
W(6) = - BETA                             2NIT0610
C
...SET UP TIME STOP AND 'H'...           2NIT0620
C

```

	ZZZ = DABS( Y1M2 )	2NIT0760
	IF( ZZZ .LT. PID4 ) ZZZ = PID4	2NIT0770
	ZZZ = PID2/ZZZ	2NIT0780
	XT = X + ZZZ	2NIT0790
	H = ZZZ/128,000	2NIT0800
C	990 RETURN	2NIT0810
	END	2NIT0820
C	2/27/69 - L.F.H.	2NIT0830
C	MOD. 8/20/69 - L.F.H.	2SET0010
C		2SET0020
	SUBROUTINE SET2( T,W,DER,NEQ,H,J1 )	2SET0030
C		2SET0040
C	...TERMINAL H CONTROLLER FOR THE 2ND PHASE...	2SET0050
C		2SET0060
C		2SET0070
	REAL*8                  Z(250),	2SET0080
	X                        TT,H,	2SET0090
	X                        T(NEQ),W(NEQ,3),DFR(NEQ,4),	2SET0100
	X                        H1,H2	2SET0110
	COMMON / DATA /      Z,KKK(6),J5	2SET0120
	EQUIVALENCE	2SET0130
	X                        ( TT,Z(41) )	2SET0140
C		2SET0150
	IF( J1 .EQ. 0 ) JC = 0	2SET0160
C		2SET0170
	IF( J1 .EQ. 3 ) GO TO 255	2SET0180
	IF( J5 .EQ. 0 ) GO TO 250	2SET0190
	J5 = 0	2SET0200
	CALL SPIE( 0 )	2SET0210
	JC = JC + 1	2SET0220
	IF( JC .GE. 5 ) GO TO 500	2SET0230
	H1 = H	2SET0240
	H = 2.000*H	2SET0250
	T(1) = T(3)	2SET0260
	DO 200 K = 1,NEQ	2SET0270
200	W(K,1) = W(K,3)	2SET0280
	J1 = 3	2SET0290
C		2SET0300
230	IF( T(1) .EQ. TT ) GO TO 300	2SET0310
	IF( T(1) + H .LE. TT ) GO TO 990	2SET0320
	H2 = TT - T(1)	2SET0330
	JC = 0	2SET0340
	IF( J1 .EQ. 3 .AND. H1 .EQ. H2 ) GO TO 500	2SET0350
	H = H2	2SET0360
	GO TO 990	2SET0370
C		2SET0380
250	IF( JC .EQ. 0 ) GO TO 255	2SET0390
	H = H*( 0.500**JC )	2SET0400
	JC = 0	2SET0410
255	J1 = 1	2SET0420
	GO TO 230	2SET0430
C		2SET0440
300	J1 = 2	2SET0450
	GO TO 990	2SET0460
C		2SET0470

```

500 J1 = 5
990 RETURN
END
C 2/26/69 - L.F.H.
C MOD. 7/07/69 - L.F.H.
C
SUBROUTINE AUX3
C
...DATA UPDATER FOR THE 2ND PHASE DERIV. SUBP...
C
REAL*8          Z(250),
1                W(8),
2                DC(5),DS(5)
COMMON / DATA / Z,NEQ1,NEQ2,J1,J2,J3,J4,J5
EQUIVALENCE
1                ( W(1),Z(64) ),
2                ( DC(1),Z(131) ), ( DS(1),Z(136) )
C
...COSINES AND SINES OF THE EULFRIAN ANGLES...
C
DO 300 J = 1,3
DC(J) = DCOS( W(J+3) )
300 DS(J) = DSIN( W(J+3) )
C
...CHECK THE COSINE OF THE 2-ANGLE...
C
IF( DC(2) .NE. 0.000 ) GO TO 990
CALL SPIE( 1 )
J5 = 255
C
990 RETURN
END
C 2/24/69 - L.F.H.
C MOD. 7/07/69 - L.F.H.
C
SUBROUTINE DER2( T,W,DER,NEQ,J )
C
...DERIV. EQ'S. FOR THE 2ND PHASE...
C
REAL*8          T,W(NEQ),DER(NEQ,4)
REAL*8          Z(250),
1                JZ(3),DC(5),DS(5)
COMMON / DATA / Z,NEQ1,NEQ2,J1,J2,J3,J4,J5
EQUIVALENCE
1                ( JZ(1),Z(28) ), ( DC(1),Z(131) ),
2                ( DS(1),Z(136) )
C
...EULER'S EQ'S. OF MOTION FOR FREE FLIGHT...
C
DER(1,J) = W(2)*W(3)*( JZ(2) - JZ(3) )/JZ(1)
DER(2,J) = W(3)*W(1)*( JZ(3) - JZ(1) )/JZ(2)
DER(3,J) = W(1)*W(2)*( JZ(1) - JZ(2) )/JZ(3)
C
...DERIV. EQ'S. FOR EULERIAN ANGLES...
C
THE ROTATIONAL TRANSFORMATION FROM THE INERTIAL FRAME TO THE
2SET0480
2SET0490
2SET0500
3AUX0010
3AUX0020
3AUX0030
3AUX0040
3AUX0050
3AUX0060
3AUX0070
3AUX0080
3AUX0090
3AUX0100
3AUX0110
3AUX0120
3AUX0130
3AUX0140
3AUX0150
3AUX0160
3AUX0170
3AUX0180
3AUX0190
3AUX0200
3AUX0210
3AUX0220
3AUX0230
3AUX0240
3AUX0250
3AUX0260
3AUX0270
3AUX0280
3AUX0290
2DER0010
2DER0020
2DER0030
2DER0040
2DER0050
2DER0060
2DER0070
2DER0080
2DER0090
2DER0100
2DER0110
2DER0120
2DER0130
2DER0140
2DER0150
2DER0160
2DER0170
2DER0180
2DER0190
2DER0200
2DER0210
2DER0220
2DER0230

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C BODY FIXED PRINCIPAL AXIS FRAME AT THE BODY C.M. INVOLVES THREE          2DER0240
C SUCCESSIVE ROTATIONS: A ROTATION ABOUT THE 1-AXIS THROUGH THE 1-ANGLE, 2DER0250
C A ROTATION ABOUT THE 1ST INTERMEDIATE 3-AXIS THROUGH THE 2-ANGLE, AND 2DER0260
C A ROTATION ABOUT THE 2ND INTERMEDIATE 2-AXIS THROUGH THE 3-ANGLE.      2DER0270
C                                                                            2DER0280
C      DER(4,J) = ( W(3)*DS(3) + W(1)*DC(3) )/DC(2)                        2DFR0290
C      DER(5,J) = W(3)*DC(3) - W(1)*DS(3)                                2DER0300
C      DER(6,J) = W(2) + DER(4,J)*DS(2)                                   2DER0310
C                                                                            2DER0320
C 990 RETURN                                                                2DER0330
C END                                                                        2DER0340
C 2/24/69 - L.F.H.                                                         4AUX0010
C MOD. 9/03/69 - L.F.H.                                                   4AUX0020
C                                                                            4AUX0030
C      SUBROUTINE AUX4                                                       4AUX0040
C                                                                            4AUX0050
C      ...DATA UPDATER FOR THE 2ND PHASE OUTPUT...                          4AUX0060
C                                                                            4AUX0070
C      REAL*8      Z(250),                                                  4AUX0080
C      X           TF,TD,                                                  4AUX0090
C      X           T,W(8),                                                 4AUX0100
C      X           DC(5),DS(5),                                             4AUX0110
C      X           D7CA,D7SA,                                              4AJX0120
C      X           DXCM(3),XCM(3),                                         4AUX0130
C      X           P(3,4),X(3,4),                                          4AUX0140
C      X           A(3,3)                                                  4AUX0150
C      COMMON / DATA / Z,NEQ1,NEQ2,J1,J2,J3,J4,J5                        4AUX0160
C      EQUIVALENCE                                                         4AUX0170
C      X           ( TF,Z(51) ),                                           4AUX0180
C      X           ( T,Z(61) ),( W(1),Z(64) ),                             4AUX0190
C      X           ( DC(1),Z(131) ),( DS(1),Z(136) ),                     4AUX0200
C      X           ( D7CA,Z(141) ),( D7SA,Z(142) ),                       4AUX0210
C      X           ( DXCM(1),Z(151) ),( XCM(1),Z(154) ),                 4AUX0220
C      X           ( P(1,1),Z(161) ),( X(1,1),Z(201) )                   4AUX0230
C                                                                            4AUX0240
C      ...BODY C.M. DISPLACEMENTS...                                       4AUX0250
C                                                                            4AUX0260
C      XCM(1) = 0.000                                                       4AUX0270
C      TD = T - TF                                                         4AUX0280
C      XCM(2) = DXCM(2)*TD + D7CA                                          4AUX0290
C      XCM(3) = DXCM(3)*TD + D7SA                                          4AUX0300
C                                                                            4AUX0310
C      THE ROTATIONAL TRANSFORMATION FROM THE INERTIAL FRAME TO THE        4AUX0320
C BODY FIXED PRINCIPAL AXIS FRAME AT THE BODY C.M. INVOLVES THREE        4AUX0330
C SUCCESSIVE ROTATIONS: A ROTATION ABOUT THE 1-AXIS THROUGH THE 1-ANGLE, 4AUX0340
C A ROTATION ABOUT THE 1ST INTERMEDIATE 3-AXIS THROUGH THE 2-ANGLE, AND 4AUX0350
C A ROTATION ABOUT THE 2ND INTERMEDIATE 2-AXIS THROUGH THE 3-ANGLE.      4AUX0360
C      THE FOLLOWING ELEMENTS ARE COMPONENTS OF THE INVERSE OF THE TRANS- 4AUX0370
C FORMATION MATRIX FOR ROTATING THE INERTIAL FRAME INTO THE BODY FIXED 4AUX0380
C PRINCIPAL AXIS FRAME AT THE C.M. OF THE BODY.                          4AUX0390
C                                                                            4AUX0400
C      A(1,1) = DC(2)*DC(3)                                                4AUX0410
C      A(1,2) = - DS(2)                                                    4AUX0420
C      A(1,3) = DC(2)*DS(3)                                                4AUX0430
C      A(2,1) = DS(1)*DS(3) + DC(1)*DS(2)*DC(3)                         4AUX0440

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A(2,2) = DC(1)*DC(2)
A(2,3) = - DS(1)*DC(3) + DC(1)*DS(2)*DS(3)
A(3,1) = - DC(1)*DS(3) + DS(1)*DS(2)*DC(3)
A(3,2) = DS(1)*DC(2)
A(3,3) = DC(1)*DC(3) + DS(1)*DS(2)*DS(3)
C
C      ...BODY POINT DISPLACEMENTS...
C
DO 500 J = 1,4
DO 500 K = 1,3
X(K,J) = XCM(K)
DO 500 L = 1,3
500 X(K,J) = X(K,J) + A(K,L)*P(L,J)
C
990 RETURN
END
C 3/26/69 - L.F.H.
C MOD. 9/03/69 - L.F.H.
C
SUBROUTINE OUT2( JJ )
C
C      ...OUTPUT SUBP. FOR THE 2ND PHASE...
C
130 FORMAT( '1' / 'OCASE NO. ',I3,5X,10A8
X / 38X,'2ND PHASE OUTPUT' / 1X
X / 5X,'T - ELAPSED TIME ( SEC ).'
X / 5X,'XCM,YCM,ZCM - C.M. FREE FLIGHT DISPLACEMENT ( FT ).'
X / 5X,'X(J),Y(J),Z(J) - J-TH POINT FREE FLIGHT DISPLACEMENTS '
X '( FT ).'
X / '0' / 55X,'...'
X / '0',14X,'T',10X,'XCM',9X,'YCM',9X,'ZCM',
X 9X,'X(1)',8X,'Y(1)',8X,'Z(1)'
X / '0',25X,'X(2)',8X,'Y(2)',8X,'Z(2)',
X 8X,'X(3)',8X,'Y(3)',8X,'Z(3)'
X / '0',25X,'X(4)',8X,'Y(4)',8X,'Z(4)' )
140 FORMAT( '1' / 'OCASE NO. ',I3,5X,10A8
X / 38X,'2ND PHASE OUTPUT' )
150 FORMAT( '0',9X,1P7D12.4 / ( 22X,1P6D12.4 ) )
C
REAL*8      Z(250),
X           T,
X           XCM(3),X(3,4),
X           TITLE(10)
COMMON / DATA / Z,NEQ1,NEQ2,J1,J2,J3,J4,J5
EQUIVALENCE
X           ( T,Z(61) ),
X           ( XCM(1),Z(154) ),( X(1,1),Z(201) ),
X           ( TITLE(1),Z(241) ),
X           ( NCASE,J4 )
C
IF( JJ .NE. 0 ) GO TO 400
WRITE( 6,130 ) NCASE,TITLE
JL = 16
C
400 IF( MOD( JL,56 ) .NE. 0 ) GO TO 500

```

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4AUX0450
4AUX0460
4AUX0470
4AUX0480
4AUX0490
4AUX0500
4AUX0510
4AUX0520
4AUX0530
4AUX0540
4AUX0550
4AUX0560
4AUX0570
4AUX0580
4AUX0590
4AUX0600
2OUT0010
2OUT0020
2OUT0030
2OUT0040
2OUT0050
2OUT0060
2OUT0070
2OUT0080
2OUT0090
2OUT0100
2OUT0110
2OUT0120
2OUT0130
2OUT0140
2OUT0150
2OUT0160
2OUT0170
2OUT0180
2OUT0190
2OUT0200
2OUT0210
2OUT0220
2OUT0230
2OUT0240
2OUT0250
2OUT0260
2OUT0270
2OUT0280
2OUT0290
2OUT0300
2OUT0310
2OUT0320
2OUT0330
2OUT0340
2OUT0350
2OUT0360
2OUT0370
2OUT0380
2OUT0390

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```

        WRITE( 6,140 )   NCASE,TITLE
        JL = 0
C
    500 WRITE( 6,150 )   T,XCM,X
        JL = JL + 4
C
    990 RETURN
        END
/*
// EXEC ASSEMBLR,PARM='LOAD,DECK'
//SOURCE.SYSPUNCH DD DSN=&DECK,SYSOUT=
//SOURCE.SYSIN DD *
EDAT    TITLE 'EDATA-ENTRY AND INITIALIZATION SECTS.'
        PRINT DATA
* 2/22/67 - L.F.H.
* MOD. 5/15/70 - L.F.H.
        SPACE 1
*     SUBP. EDATA PROCESSES DATA CARDS 'READ' BY SUBP. LOAD AND STORES
* THE PROCESSED DATA ITEMS AS DIRECTED. CHARACTER, FULL AND DOUBLE
* WORD DECIMAL ( WHICH INCL. FULL WORD INTEGER AS WELL AS SHORT AND
* LONG REAL ), HALF WORD DECIMAL INTEGER, AND FULL WORD HEXADECIMAL
* DATA ARE PROCESSED.
*     SUBP. EDATA IS MOST EFFICIENT WHEN DIRECTED TOWARD THE LOADING OF
* BLOCKS OF STORAGE SUCH AS A COMMON AREA OR A LARGE ARRAY CONTAINING
* THE VARIOUS TYPES OF DATA REQUIRED BY A PROCESSING PROGRAM SINCE IT
* TENDS TO LOAD THE PROCESSED DATA ITEMS INTO SEQUENTIALLY HIGHER AND
* HIGHER LOCATIONS. IT MAY BE DIRECTED TO SCATTER LOAD ONLY THE RE-
* QUIRED DATA ITEMS, I.E., ALL OF THE STORAGE BLOCK NEED NOT BE LOADED.
* THE CURRENT LOAD POINT MAY BE SHIFTED AS REQ'D TO SKIP OVER SECTIONS
* OF STORAGE AT ANY TIME. THIS SHIFT IS COMPUTED RELATIVE TO THE
* INITIAL LOAD POINT.
*     CHARACTER DATA ARE STORED WITHOUT CHANGE BYTE-BY-BYTE; HENCE, THE
* CURRENT LOAD POINT CAN BE SHIFTED OFF A HALF WORD AS WELL AS A FULL
* WORD AND DOUBLE WORD BOUNDARY. IT IS ADVISABLE TO USE THE INITIAL
* LOAD POINT RESET AND SHIFT FEATURE OF SUBP. EDATA FOLLOWING THE LOAD-
* ING OF CHARACTER DATA.
*     THE LOAD POINT FOR THE FULL AND DOUBLE WORD DECIMAL DATA AS WELL
* AS THE HEXADECIMAL AND HALF WORD DECIMAL INTEGER DATA MUST BE AT THE
* APPROPRIATE BYTE BOUNDARIES.
*     SUBP. EDATA PROCESSES ITS OWN PROGRAM INTERRUPTS. IT SAVES THE
* ADDRESS OF 'THE NEXT INSTRUCTION' AND THE OLD PSW AND RESETS THE NEXT
* INSTRUCTION ADDRESS BEFORE RETURNING CONTROL TO THE CONTROL PROGRAM.
* THE CARD ERROR COLUMN NUMBER, THE CARD IMAGE, AND THE OLD PSW ARE
* PRINTED BY SUBP. LOAD.
*     SUBP. EDATA CAN DETECT CERTAIN PROCESSING ERRORS AND GENERATE THE
* CARD COLUMN NUMBER AT WHICH THE ERROR WAS DETECTED. THE LOADING OF
* ALL SUBSEQUENT DATA IS SUSPENDED, AS IT IS WHEN A PROG. INTERRUPT IS
* PROCESSED. HOWEVER, SUBSEQUENT DATA CARDS ARE CHECKED FOR ERRORS
* UNTIL A RETURN TO THE CALLER OF SUBP. LOAD IS EXECUTED. ONLY ONE
* ERROR PER CARD CAN BE DETECTED AND PROCESSED. DATA ITEMS ON A GIVEN
* CARD WHICH FOLLOW A DETECTED ERROR CANNOT BE CHECKED. SUBP. LOAD
* PRINTS THE CARD ERROR COLUMN NUMBER AND THE CARD IMAGE IN SUCH CASES.
*     FOR DETAILS ON SUBP. LOAD AND SUBP. EDATA, CALL L.F.HATAKEYAMA,
* NASA-GSFC, CODE 721, X4047.
        SPACE 1

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2OUT0400
2OUT0410
2OUT0420
2OUT0430
2OUT0440
2OUT0450
2OUT0460
2OUT0470

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EDAT0010
EDAT0020
EDAT0030
EDAT0040
EDAT0050
EDAT0060
EDAT0070
EDAT0080
EDAT0090
EDAT0100
EDAT0110
EDAT0120
EDAT0130
EDAT0140
EDAT0150
EDAT0160
EDAT0170
EDAT0180
EDAT0190
EDAT0200
EDAT0210
EDAT0220
EDAT0230
EDAT0240
EDAT0250
EDAT0260
EDAT0270
EDAT0280
EDAT0290
EDAT0300
EDAT0310
EDAT0320
EDAT0330
EDAT0340
EDAT0350
EDAT0360
EDAT0370
EDAT0380
EDAT0390
EDAT0400
EDAT0410
EDAT0420
EDAT0430

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EDATA	CSECT		EDAT0440
	SPACE	1	EDAT0450
A	EQU	10	EDAT0460
B	FQU	11	EDAT0470
C	EQU	12	EDAT0480
D	EQU	13	EDAT0490
E	EQU	14	EDAT0500
F	EQU	15	EDAT0510
	EJECT		EDAT0520
*		* * *	EDAT0530
	ENTRY	BUST	EDAT0540
	USING	*,F	EDAT0550
	B	A100	EDAT0560
	DC	CL6'5EDATA'	EDAT0570
A100	STM	E,C,12(D)	EDAT0580
	L	B,4(D)	EDAT0590
	L	A,24(B)	EDAT0600
	L	4,=A(LFH2)	EDAT0610
	ST	D,4(4)	EDAT0620
	ST	4,8(D)	EDAT0630
	LR	D,4	EDAT0640
	SPACE	1	EDAT0650
	LA	F,BUST-EDATA(F)	EDAT0660
	USING	BUST,F	EDAT0670
	B	A210	EDAT0680
*		* * * * *	EDAT0690
BUST	B	A200	EDAT0700
	DC	CL6'5BUST '	EDAT0710
A200	NI	A212+1,X'OF'	EDAT0720
	SPACE	1	EDAT0730
A210	LR	2,F	EDAT0740
	USING	BUST,2	EDAT0750
	DRUP	F	EDAT0760
	SPACE	1	EDAT0770
A212	RC	15,A300	EDAT0780
	SPACE	1	EDAT0790
	MVC	176(8,4),4(1)	EDAT0800
	MVC	9(3,1),=AL3(C110)	EDAT0810
	OI	A212+1,X'FO'	EDAT0820
	BCR	15,E	EDAT0830
*		* * * * *	EDAT0840
A300	SPIE	BUST,((1,15))	EDAT0850
	SPACE	1	EDAT0860
	STM	1,2,24(4)	EDAT0870
	CLC	82(2,4),=H'1'	EDAT0880
	BH	A400	EDAT0890
	L	3,0(A)	EDAT0900
	ST	3,172(4)	EDAT0910
	LA	5,88(4)	EDAT0920
	LA	7,79(5)	EDAT0930
	LA	8,LDB	EDAT0940
	LA	9,3	EDAT0950
	STM	1,9,24(4)	EDAT0960
	EJECT		EDAT0970
A400	LM	1,9,24(4)	EDAT0980

	LR	6,5	RESET & SAVE R6...	EDAT0990
	ST	6,44(4)	...	EDAT1000
	XC	176(8,4),176(4)	CLEAR THE 'PSW' CELLS.	EDAT1010
	XC	CL8,CL8	ZERO LOP & HOLD.	EDAT1020
	LA	A,8	SET UP RA, RB, RE, & RF...	EDAT1030
	LA	B,A402	...	EDAT1040
	LM	E,F,LOP	...	EDAT1050
	OI	A408+1,X'FO'	FNABLE THE BR. AT A408.	EDAT1060
	SPACE	1		EDAT1070
A402	CLI	0(6),C' '	COMPUTE THE LOADING OFFSET...	EDAT1080
	RE	A407	...	EDAT1090
	NI	A408+1,X'OF'	DISABLE THE BR. AT A408.	EDAT1100
	LA	B,A404	...RESET RB.	EDAT1110
A404	CLI	0(6),C'O'	...	EDAT1120
	BL	A405	...	EDAT1130
	CLI	0(6),C'9'	...	EDAT1140
	RH	C110	...	EDAT1150
	MVN	0(1,8),0(6)	...	EDAT1160
	M	E,F'10'	...	EDAT1170
	A	F,HOLD	...	EDAT1180
	B	A407	...	EDAT1190
A405	LA	B,A406	...RESET RB.	EDAT1200
A406	CLI	0(6),C' '	...	EDAT1210
	RNE	C110	...	EDAT1220
A407	LA	6,1(6)	...	EDAT1230
	RCTR	A,B		EDAT1240
	SPACE	1		EDAT1250
	CLI	0(6),C' '	CHECK THE COL. 9 CHAR.	EDAT1260
	RNE	C110		EDAT1270
	SPACE	1		EDAT1280
A408	B	A409	**	EDAT1290
	A	F,172(4)	SET UP THE CURRENT LOAD POINT...	EDAT1300
	LR	3,F	...	EDAT1310
	ST	3,32(4)	...	EDAT1320
	SPACE	1		EDAT1330
A409	SR	A,A	SET UP RA, RB, RE, RF,...	EDAT1340
	LA	B,S100	...	EDAT1350
	LA	E,4	...	EDAT1360
	LA	F,24	...	EDAT1370
	LA	6,1(6)	CHECK THE CARD COL. 10 CHAR...	EDAT1380
A410	CLC	0(1,6),0(8)	...	EDAT1390
	BE	A500(A)	BR. IF .EQ. AN ALLOWED CHAR.	EDAT1400
	LA	B,1(B)	INCR. RB.	EDAT1410
	RXLE	A,E,A410	LOOP...	EDAT1420
	B	C110		EDAT1430
	SPACE	1		EDAT1440
A500	B	BLNK	BR. OUT AS REQ'D...	EDAT1450
	B	CC	...	EDAT1460
	B	DD	...	EDAT1470
	B	HH	...	EDAT1480
	B	RRR	...	EDAT1490
	B	XX	...	EDAT1500
	TITLE	'EDATA-C DATA, BLANK AND RETURN PROC. SECTIONS'		EDAT1510
	SPACE	1		EDAT1520
*		***		EDAT1530

	SPACE 1			EDAT1540
CC	UI C102+1,X'F0'	ENABLE THE BR'S AT C102...		EDAT1550
	OI C300+1,X'F0'	...& C300.		EDAT1560
	SPACE 1			EDAT1570
C100	LA 6,1(6)	INCR., SAVE, & CHECK R6...		EDAT1580
	ST 6,44(4)	...		EDAT1590
	CR 6,7	...		EDAT1600
	RH BLNK	BR. OUT IF PAST CARD END.		EDAT1610
	CLI 0(6),X'7D'	LOOK FOR THE ' MARK...		EDAT1620
	BE C300	...BR. OUT WHEN FOUND.		EDAT1630
	SPACE 1			EDAT1640
C102	RC 15,C100	**		EDAT1650
	SPACE 1			EDAT1660
C103	C 9,72(4)	CHECK FOR PRECEDING ERRORS...		EDAT1670
	BE C100	...BR. TO AVOID DATA LOADING.		EDAT1680
	MVC 0(1,3),0(6)	MOVE A CHARACTER.		EDAT1690
	LA 3,1(3)	INCR. R3.		EDAT1700
	B C100			EDAT1710
	SPACE 1			EDAT1720
C110	SR 6,5	SET UP TROUBLE INDIC...		EDAT1730
	LA 6,1(6)	...		EDAT1740
	ST 6,76(4)	...		EDAT1750
	MVI 75(4),3	INDIC. TROUBLE.		EDAT1760
	B RR			EDAT1770
	SPACE 1			EDAT1780
C300	BC 15,C400	**		EDAT1790
	SPACE 1			EDAT1800
	CLC 0(2,6),=X'7D7D'	CHECK FOR THE '' MARK.		EDAT1810
	BNE BLNK	BR. OUT IF NOT A '' MARK.		EDAT1820
	LA 6,1(6)	INCR. R6.		EDAT1830
	ST 6,44(4)	SAVE R6.		EDAT1840
	B C103			EDAT1850
	SPACE 1			EDAT1860
C400	NI C102+1,X'OF'	DISABLE THE BR. AT C102.		EDAT1870
	NI C300+1,X'OF'	DISABLE THE BR. AT C300.		EDAT1880
	B C100			EDAT1890
	SPACE 1			EDAT1900
*	* * *			EDAT1910
	SPACE 1			EDAT1920
BLNK	MVI 79(4),0	INDIC. NO ERROR.		EDAT1930
	ST 3,32(4)	SAVE THE CURRENT LOAD PJINT.		EDAT1940
	SPACE 1			EDAT1950
RR	L 1,24(4)	RESET R1...		EDAT1960
	SPIE MF=(E,(1))	...TO RESET THE OLD P.I.E.		EDAT1970
	L 0,4(4)	RESET RD...		EDAT1980
	LM E,C,12(D)	...AND RESTORE THE OTHER R'S.		EDAT1990
	MVI 12(D),X'FF'			EDAT2000
	BCR 15,E			EDAT2010
	SPACE 1			EDAT2020
RRR	MVI 75(4),2	INDIC. RETURN.		EDAT2030
	B RR			EDAT2040
	TITLE 'EDATA-D DATA PROC. SECTION'			EDAT2050
	SPACE 1			EDAT2060
*	* * *			EDAT2070
	SPACE 1			EDAT2080

DD	SR	A,A	SET UP RA & RB...	EDAT2090
	SR	B,B	...	EDAT2100
	XC	CL16,CL16	ZERO HOP, LOP, HOLD, & EXP.	EDAT2110
	MVC	TCW,=X'4EDFFFFF'	SET UP TCW.	EDAT2120
	SPACE	2		EDAT2130
D200	LA	6,1(6)	INCR., SAVE, & CHECK R6...	EDAT2140
	ST	6,4(4)	...	EDAT2150
	CR	6,7	...	EDAT2160
	BH	D810	...BR. OUT IF PAST CARD END.	EDAT2170
	SPACE	1		EDAT2180
	CLI	0(6),C'0'	CHECK FOR NUMERICS...	EDAT2190
	BL	D500	...BR. OUT IF .LT. 0.	EDAT2200
	CLI	0(6),C'9'	...	EDAT2210
	BH	C110	...BR. TO TROUBLE IF .GT. 9.	EDAT2220
	MVN	0(1,8),0(6)	MOVE THE NUMERIC TO 'HOLD'.	EDAT2230
	LA	A,1(A)	INCR. THE DIGIT COUNT.	EDAT2240
	SPACE	1		EDAT2250
	TM	TC1,X'80'	(0,0)	EDAT2260
	BO	D220		EDAT2270
	CH	A,=H'8'	CHECK THE DIGIT COUNT...	EDAT2280
	BL	D220	...BR. AROUND IF .LT. 8.	EDAT2290
	OI	TC1,X'80'	DISCONT. THE DIGIT COUNT CHECK.	EDAT2300
	NI	TC3,X'EF'	ALLOW LONG REAL STORAGE.	EDAT2310
	NI	TC2,X'FD'	FORBID AN E IN A LONG REAL.	EDAT2320
	SPACE	1		EDAT2330
D220	TM	TC1,X'40'	(1,1)	EDAT2340
	BO	D300		EDAT2350
	LA	B,1(8)	INCR. THE FRACT. DIGIT COUNT.	EDAT2360
	SPACE	2		EDAT2370
D300	TM	TC1,X'20'	(2,0)	EDAT2380
	BO	D400		EDAT2390
	L	E,LOP	BUILD UP THE LONG PRIMITIVE...	EDAT2400
D310	LR	F,E	...	EDAT2410
	M	E,=F'10'	...	EDAT2420
	A	F,HOLD	...	EDAT2430
	TM	TC1,X'10'	(3,0)	EDAT2440
	BO	D330		EDAT2450
	ST	F,LOP	...	EDAT2460
	NI	LOP,X'03'	...	EDAT2470
	SR	E,E	...	EDAT2480
	SLDL	E,6	...	EDAT2490
	ST	E,HOLD	...	EDAT2500
	L	E,HOP	...	EDAT2510
	OI	TC1,X'10'	...'OR' BIT 3.	EDAT2520
	R	D310		EDAT2530
	FJECT			EDAT2540
D330	ST	F,HOP	...	EDAT2550
	NI	TC1,X'CF'	...ZERO BIT 3.	EDAT2560
	R	D200		EDAT2570
	SPACE	2		EDAT2580
D400	CH	A,=H'2'	CHECK THE DIGIT COUNT...	EDAT2590
	BH	C110	...BR. TO TROUBLE IF .GT. 2.	EDAT2600
	L	F,EXP	BUILD UP THE EXPONENT...	EDAT2610
	M	E,=F'10'	...	EDAT2620
	A	F,HOLD	...	EDAT2630

	ST	F,EXP	...	EDAT2640
	B	D200		EDAT2650
	SPACE	2		EDAT2660
D500	CLI	0(6),C','	CHECK FOR A COMMA...	EDAT2670
	RE	D600	...BR. OUT IF COMMA.	EDAT2680
	SPACE	1		EDAT2690
	SR	1,1		EDAT2700
	LA	C,S200	SET UP RC, RE, & RF...	EDAT2710
	LA	E,4	...	EDAT2720
	LA	F,20	...	EDAT2730
D510	CLC	0(1,6),0(C)	CHECK FOR OTHER CHARS...	EDAT2740
	RE	D700(1)	...BR. OUT AS REQ'D.	EDAT2750
	LA	C,1(C)	INCR. RC.	EDAT2760
	BXLE	1,E,D510	LOOP...	EDAT2770
	B	C110	...OR BR. TO TROUBLE.	EDAT2780
	SPACE	2		EDAT2790
D600	TM	TC1,X'08'	(4,1)	EDAT2800
	BO	INT		EDAT2810
	SPACE	1		EDAT2820
	TM	TC1,X'04'	(5,1)	EDAT2830
	BO	D620		EDAT2840
	SPACE	1		EDAT2850
	A	B,EXP	COMP. THE SCALING FACTOR...	EDAT2860
D610	NI	TC3,X'BF'	...ENABLE DOWNSCALING.	EDAT2870
	SPACE	1		EDAT2880
D611	SLL	B,3	...	EDAT2890
	ST	B,EXP	...	EDAT2900
	B	FLT		EDAT2910
	SPACE	1		EDAT2920
D620	S	B,EXP	...	EDAT2930
	RM	D630	...	EDAT2940
	B	D610	...	EDAT2950
	SPACE	1		EDAT2960
D630	LPR	B,B	...	EDAT2970
	B	D611		EDAT2980
	SPACE	2		EDAT2990
D700	B	D810	BLANK.	EDAT3000
	B	D820	.	EDAT3010
	B	D830	+	EDAT3020
	B	D840	-	EDAT3030
	B	D850	D	EDAT3040
	B	D860	E	EDAT3050
	FJECT			EDAT3060
D810	NI	TC3,X'7F'	ZERO BIT 16.	EDAT3070
	B	D600		EDAT3080
	SPACE	1		EDAT3090
D820	TM	TC1,X'02'	(6,1)	EDAT3100
	BO	D821		EDAT3110
	B	C110		EDAT3120
D821	NI	TC1,X'8D'	ALLOW FRACT. DIGIT COUNTING...	*EDAT3130
			...FORBID 2 .'S IN THE P-PART.	EDAT3140
	NI	TC2,X'6F'	FORBID + AFTER THE DEC. PT...	*EDAT3150
			...ALSO, - AFTER THE DEC. PT.	EDAT3160
D825	NI	TC1,X'F7'	ALLOW FLOATING.	EDAT3170
	B	D200		EDAT3180

	SPACE 1			EDAT3190
D830	TM TC1,X'01'	(7,0)		EDAT3200
	BO D834			EDAT3210
	TM TC2,X'80'	(8,1)		EDAT3220
	BO D832			EDAT3230
	B C110			EDAT3240
D832	NI TC2,X'6F'		FORBID TWO +'S IN THE P-PART...	*EDAT3250
			...ALSO, + & - IN THE P-PART.	EDAT3260
D833	CH A,=H'0'		CHFCK THE DIGIT COUNT...	EDAT3270
	BH C110		...BR. TO TROUBLE IF .NE. 0.	EDAT3280
	B D200			EDAT3290
	SPACE 1			EDAT3300
D834	TM TC2,X'40'	(9,1)		EDAT3310
	BO D835			EDAT3320
	B C110			EDAT3330
D835	NI TC2,X'B7'		FORBID TWO +'S IN THE E-PART...	*EDAT3340
			...ALSO, + & - IN THE E-PART.	EDAT3350
	B D833			EDAT3360
	SPACE 1			EDAT3370
D840	TM TC2,X'20'	(10,0)		EDAT3380
	BO D843			EDAT3390
	TM TC2,X'10'	(11,1)		EDAT3400
	BO D842			EDAT3410
	B C110			EDAT3420
D842	NI TC2,X'6F'		FORBID - & + IN THE P-PART...	*EDAT3430
			...ALSO, TWO -'S IN THE P-PART.	EDAT3440
	NI TC2,X'FE'		ALLOW NEG. INTEGER.	EDAT3450
	NI TC3,X'DF'		ALLOW NEG. REAL.	EDAT3460
	B D833			EDAT3470
	SPACE 1			EDAT3480
D843	TM TC2,X'08'	(12,1)		EDAT3490
	BO D844			EDAT3500
	B C110			EDAT3510
D844	NI TC1,X'FB'		ALLOW NEG. EXP.	EDAT3520
	NI TC2,X'B7'		FORBID - & + IN THE E-PART...	*EDAT3530
			...ALSO, TWO -'S IN THE E-PART.	EDAT3540
	B D833			EDAT3550
	EJECT			EDAT3560
D850	TM TC2,X'04'	(13,1)		EDAT3570
	BO D851			EDAT3580
	B C110			EDAT3590
D851	NI TC2,X'F9'		FORBID TWO D'S IN AN ITEM...	*EDAT3600
			...AND D & E IN AN ITEM.	EDAT3610
	NI TC3,X'FF'		ALLOW LONG REAL STORAGE.	EDAT3620
D852	OI TC1,X'60'		STOP THE FRACT. DIGIT COUNT...	*EDAT3630
			...AND ALLOW EXP. COMP.	EDAT3640
	OI TC1,X'01'		SET UP EXP. SIGN CHECKS...	EDAT3650
	OI TC2,X'20'		...	EDAT3660
	NI TC1,X'FD'		FORBID . IN E-PART.	EDAT3670
	SR A,A		ZERO RA.	EDAT3680
	B D825			EDAT3690
	SPACE 1			EDAT3700
D860	TM TC2,X'02'	(14,1)		EDAT3710
	BO D861			EDAT3720
	B C110			EDAT3730

D861	NI	TC2,X'F9'	FORBID TWO F'S IN AN ITEM...	*EDAT3740
			...AND E & D IN AN ITEM.	EDAT3750
	B	D852		EDAT3760
	SPACE	1		EDAT3770
INT	LM	E,F,HUP	LOAD THE LONG PRIMITIVE...	EDAT3780
	CH	E,=H'31'	...& CHECK THE H-ORDER PART.	EDAT3790
	BH	C110	...BR. TO TROUBLE IF TOO LARGE.	EDAT3800
	SLL	F,6	LINK UP THE PARTS...	EDAT3810
	SRDL	E,6	...& R-SHIFT IT ALL INTO RF.	EDAT3820
	TM	TC2,X'01'	(15,1)	EDAT3830
	BO	IN20		EDAT3840
	LNR	F,F	MAKE THE RESULT NEG., IF REQ'D.	EDAT3850
IN20	C	9,72(4)	CHECK FOR PRECEDING ERRORS...	EDAT3860
	BE	IN30	...BR. TO AVOID DATA LOADING.	EDAT3870
	ST	F,0(3)	STASH THE INTEGER WHERE REQ'D.	EDAT3880
	LA	3,4(3)	INCR. R3.	EDAT3890
	SPACE	1		EDAT3900
IN30	TM	TC3,X'80'	(16,1)	EDAT3910
	BO	DD		EDAT3920
	B	BLNK		EDAT3930
	SPACE	1		EDAT3940
FLT	LD	2,=D'0.0'	FLOAT THE LONG PRIMITIVE...	EDAT3950
	LM	A,B,HOP	...	EDAT3960
	LTR	E,A	...	EDAT3970
	BZ	FL50	...	EDAT3980
	SR	F,F	...	EDAT3990
	SRDL	E,10	...	EDAT4000
	STM	E,F,HUP	...	EDAT4010
	OI	HOP,X'4F'	...	EDAT4020
	AD	2,DWD	...	EDAT4030
FL50	LTR	B,B	...	EDAT4040
	BZ	RL10	...	EDAT4050
	SR	A,A	...	EDAT4060
	STM	A,B,HUP	...	EDAT4070
	OI	HOP,X'4E'	...	EDAT4080
	AD	2,DWD	...	EDAT4090
	EJECT			EDAT4100
	SPACE	2		EDAT4110
RL10	LTDR	2,2	CHECK THE FLOATED RESULT...	EDAT4120
	RZ	RL30	...BR. OUT TO AVOID SCALING.	EDAT4130
	L	C,EXP	...& SCALE AS REQ'D...	EDAT4140
	LTR	C,C	...	EDAT4150
	BZ	RL20	...	EDAT4160
	SPACE	1		EDAT4170
	L	1,=A(LFH3)	...	EDAT4180
	TM	TC3,X'40'	(17,1)	EDAT4190
	BO	RL15	...	EDAT4200
	SPACE	1		EDAT4210
RL11	CH	C,=H'608'	...	EDAT4220
	BL	RL13	...	EDAT4230
	SH	C,=H'600'	...	EDAT4240
	DD	2,600(1)	...	EDAT4250
	B	RL11	...	EDAT4260
RL13	DD	2,0(C,1)	...	EDAT4270
	R	RL20	...	EDAT4280



	SPACE 1			EDAT4290
RL15	CH C,=H'600'	...		EDAT4300
	RH C110	...BR. TO TROUBLE IF TOO MUCH.		EDAT4310
	MD 2,0(C,1)	...		EDAT4320
	SPACE 1			EDAT4330
RL20	TM TC3,X'20'	(18,1)		EDAT4340
	RO RL30			EDAT4350
	LNDR 2,2	MAKE IT NEG. IF REQ'D.		EDAT4360
	SPACE 1			EDAT4370
RL30	TM TC3,X'10'	(19,1)		EDAT4380
	BO RL50			EDAT4390
RL31	C 9,72(4)	CHECK FOR PRECEDING ERRORS...		EDAT4400
	RE IN30	...BR. TO AVOID DATA LOADING.		EDAT4410
	STD 2,0(3)	STASH THE L-REAL WHERE REQ'D.		EDAT4420
	LA 3,8(3)	INCR. R3.		EDAT4430
	R IN30			EDAT4440
	SPACE 2			EDAT4450
RL50	LTDR 2,2	ROUND OUT AS REQ'D...		EDAT4460
	BZ RL55	...		EDAT4470
	STD 2,DWD	...		EDAT4480
	NC HOP,=X'FF000000'	...		EDAT4490
	NC LOP,=X'80000C00'	...		EDAT4500
	AD 2,DWD	...		EDAT4510
RL55	C 9,72(4)	CHECK FOR PRECEDING ERRORS...		EDAT4520
	RE IN30	...BR. TO AVOID DATA LOADING.		EDAT4530
	STE 2,0(3)	STORE THE S-REAL WHERE REQ'D.		EDAT4540
	LA 3,4(3)	INCR. R3.		EDAT4550
	B IN30			EDAT4560
	TITLE 'EDATA-H DATA PROC. SECTION'			EDAT4570
*	* * *			EDAT4580
	SPACE 1			EDAT4590
HH	SR A,A	SET UP RA...		EDAT4600
	XC CL8,CL8	ZFRO LOP & HOLD.		EDAT4610
	OI H510+1,X'F0'	ENABLE THE BR. AT H510.		EDAT4620
	SPACE 1			EDAT4630
H200	LA 6,1(6)	INCR., SAVE, & CHECK R6...		EDAT4640
	ST 6,44(4)	...		EDAT4650
	CR 6,7	...		EDAT4660
	RH H500	...BR. OUT IF PAST CARD END.		EDAT4670
	SPACE 1			EDAT4680
	CLI 0(6),C','	CHECK THE DATA FIELD CHAR...		EDAT4690
	BL H300	...BR. OUT IF .LT. 'COMMA'.		EDAT4700
	BE H500	...BR. OUT IF .EQ. 'COMMA'.		EDAT4710
	CLI 0(6),C'0'	...		EDAT4720
	RL C110	...BR. TO TROUBLE IF .LT. 0.		EDAT4730
	CLI 0(6),C'9'	...		EDAT4740
	RH C110	...BR. TO TROUBLE IF .GT. 9.		EDAT4750
	MVN 0(1,8),0(6)	MOVE THE NUMERIC TO 'HOLD'.		EDAT4760
	LA A,1(A)	INCR. RA.		EDAT4770
	SPACE 1			EDAT4780
	L F,LOP	BUILD UP THE H-FORMATTED DATA...		EDAT4790
	M E,=F'10'	...		EDAT4800
	A F,HOLD	...		EDAT4810
	CH F,=H'32767'	...		EDAT4820
	RH C110	...BR. TO TROUBLE IF .GT. 32767.		EDAT4830

	ST	F,LOP	...	EDAT4840
	B	H200		EDAT4850
	SPACE	1		EDAT4860
H300	CLI	0(6),C' '	RECHECK THE DATA FIELD CHAR...	EDAT4870
	BE	H600	...BR. OUT IF BLANK.	EDAT4880
	CLI	0(6),C'+'	...	EDAT4890
	BE	H410	...BR. OUT IF PLUS SIGN.	EDAT4900
	CLI	0(6),C'-'	...	EDAT4910
	BE	H400	...BR. OUT IF MINUS SIGN.	EDAT4920
	R	C110	...BR. TO TROUBLE OTHERWISE.	EDAT4930
	SPACE	1		EDAT4940
H400	NI	H510+1,X'OF'	DISABLE THE BR. AT H510.	EDAT4950
H410	CH	A,=H'0'	CHECK FOR SIGN EMBEDMENT...	EDAT4960
	BH	C110	...BR. TO TROUBLE IF EMBEDDED.	EDAT4970
	B	H200		EDAT4980
	SPACE	1		EDAT4990
H500	C	9,72(4)	CHECK FOR PRECEDING ERRORS...	EDAT5000
	BE	H530	...BR. TO AVOID DATA LOADING.	EDAT5010
	LH	B,LOP+2		EDAT5020
H510	BC	15,H520	**	EDAT5030
	LNR	B,B	SET SIGN MINUS IF REQ'D.	EDAT5040
H520	STH	B,0(3)	STORE THE H-INTEGER.	EDAT5050
	LA	3,2(3)	INCR. R3.	EDAT5060
H530	BC	15,HH	**	EDAT5070
	OI	H530+1,X'F0'	ENABLE THE BR. AT H530.	EDAT5080
	B	BLNK		EDAT5090
	SPACE	1		EDAT5100
H600	NI	H530+1,X'OF'	DISABLE THE BR. AT H530.	EDAT5110
	B	H500		EDAT5120
	TITLE	'EDATA-X DATA PROC. SECTION'		EDAT5130
	SPACE	1		EDAT5140
*		* * *		EDAT5150
	SPACE	1		EDAT5160
XX	SR	A,A	ZERO RA...	EDAT5170
	XC	CL8,CL8	ZERO LOP & HOLD.	EDAT5180
	SPACE	1		EDAT5190
X200	LA	6,1(6)	INCR., SAVE, & CHECK R6...	EDAT5200
	ST	6,44(4)	...	EDAT5210
	CR	6,7	...	EDAT5220
	BH	X500	...BR. OUT IF PAST CARD END.	EDAT5230
	SPACE	1		EDAT5240
	CLI	0(6),C','	CHECK THE DATA FIELD CHAR...	EDAT5250
	BE	X400	...BR. OUT IF COMMA.	EDAT5260
	CLI	0(6),C'0'	...	EDAT5270
	BL	X300	...BR. OUT IF .LT. 0.	EDAT5280
	CLI	0(6),C'9'	...	EDAT5290
	BH	C110	...BR. TO TROUBLE IF .GT. 9.	EDAT5300
	MVN	0(1,8),0(6)	MOVE THE NUMERIC TO 'HOLD'.	EDAT5310
	L	B,HOLD	SET UP RB.	EDAT5320
	SPACE	1		EDAT5330
X220	LA	A,1(A)	INCR. & CHECK R8...	EDAT5340
	CH	A,=H'8'	...	EDAT5350
	BH	C110	...BR. TO TROUBLE IF .GT. 8.	EDAT5360
	SPACE	1		EDAT5370
	L	C,LOP	BUILD UP THE X.FORMATTED DATA...	EDAT5380

	SLL	C,4	...	EDAT5390
	OR	C,B	...	EDAT5400
	ST	C,LDP	...	EDAT5410
	R	X200	...	EDAT5420
	SPACE	1		EDAT5430
X300	CLI	0(6),C' '	RECHECK THE DATA FIELD CHAR...	EDAT5440
	RE	X500	...BR. OUT IF BLANK.	EDAT5450
	CLI	0(6),C'A'	...	EDAT5460
	BL	C110	...BR. TO TROUBLE IF .LT. 'A'.	EDAT5470
	CLI	0(6),C'F'	...	EDAT5480
	BH	C110	...BR. TO TROUBLE IF .GT. 'F'.	EDAT5490
	MVN	0(1,8),0(6)	MOVE THE NUMERIC TO 'HOLD'.	EDAT5500
	L	B,HOLD	PICK UP THE NUMERIC...	EDAT5510
	AH	B,=H'9'	...& REMOVE ITS BIAS.	EDAT5520
	R	X220		EDAT5530
	SPACE	1		EDAT5540
X400	C	9,72(4)	CHECK FOR PRECEDING ERRORS...	EDAT5550
	BE	X410	...BR. TO AVOID DATA LOADING.	EDAT5560
	SPACE	1		EDAT5570
	L	B,LDP	STASH THE DATA WHERE REQ'D...	EDAT5580
	ST	B,0(3)	...	EDAT5590
	LA	3,4(3)	INCR. R3.	EDAT5600
	SPACE	1		EDAT5610
X410	BC	15,XX	**	EDAT5620
	OI	X410+1,X'F0'	ENABLE THE BR. AT X410.	EDAT5630
	B	BLNK		EDAT5640
	SPACE	1		EDAT5650
X500	NI	X410+1,X'0F'	DISABLE THE BR. AT X410.	EDAT5660
	B	X400		EDAT5670
	TITLE	'EDATA-ERASIBLE STORAGE AND CONSTANTS.'		EDAT5680
	SPACE	1		EDAT5690
DWD	DS	OD		EDAT5700
CL16	DS	OCL16		EDAT5710
HQP	DS	F		EDAT5720
CL8	DS	OCL8		EDAT5730
LDP	DS	F		EDAT5740
HOLD	DS	OF		EDAT5750
	DS	CL3		EDAT5760
LOB	DS	C		EDAT5770
EXP	DS	F		EDAT5780
	SPACE	1		EDAT5790
TCW	DS	OF		EDAT5800
TC1	DS	C		EDAT5810
TC2	DS	C		EDAT5820
TC3	DS	C		EDAT5830
TC4	DS	C		EDAT5840
	SPACE	1		EDAT5850
S100	DC	C' '		EDAT5860
	DC	C'C'		EDAT5870
	DC	C'D'		EDAT5880
	DC	C'H'		EDAT5890
	DC	C'R'		EDAT5900
	DC	C'X'		EDAT5910
	SPACE	1		EDAT5920
S200	DC	C' '		EDAT5930

```

DC      C'..'
DC      C'+.'
DC      C'-'
DC      C'D.'
DC      C'E.'
SPACE 1
LTD RG
TITLE  'EDATA-CSECTS LFH2 AND LFH3.'
SPACE 1
*
* * * * *
*
LFH2    SPACE 1
CSECT
FWD     DS      F              +0
RD      DS      F              +4
RZ      DS      4F             +8
R1      DS      F              +24
R2      DS      F              +28
R3      DS      F              +32
R4      DS      F              +36
R5      DS      F              +40
R6      DS      F              +44
R7      DS      F              +48
R8      DS      F              +52
R9      DS      F              +56
RY      DS      3F             +60
N1      DS      F              +72
N2      DS      F              +76
N3      DS      F              +80
N4      DS      F              +84
CARD    DS      CL80           +88
BLANK   DC      CL4' '
R30     DS      F              +172
PSW     DS      2F             +176
K3      DS      2H             +184
CBLOCK  DS      4400F          +188
SPACE 1
*
* * * * *
*
LFH3    SPACE 1
CSECT
*
*
TENS    DC      D'1.0E+0,1.0E+1,1.0E+2,1.0E+3,1.0E+4,1.0E+5'
DC      D'1.0E+6,1.0E+7,1.0E+8,1.0E+9,1.0E+10'
DC      D'1.0E+11,1.0E+12,1.0E+13,1.0E+14,1.0E+15'
DC      D'1.0E+16,1.0E+17,1.0E+18,1.0E+19,1.0E+20'
EJECT
DC      D'1.0E+21,1.0E+22,1.0E+23,1.0E+24,1.0E+25'
DC      D'1.0E+26,1.0E+27,1.0E+28,1.0E+29,1.0E+30'
DC      D'1.0E+31,1.0E+32,1.0E+33,1.0E+34,1.0E+35'
DC      D'1.0E+36,1.0E+37,1.0E+38,1.0E+39,1.0E+40'
DC      D'1.0E+41,1.0E+42,1.0E+43,1.0E+44,1.0E+45'
DC      D'1.0E+46,1.0E+47,1.0E+48,1.0E+49,1.0E+50'
DC      D'1.0E+51,1.0E+52,1.0E+53,1.0E+54,1.0E+55'
DC      D'1.0E+56,1.0E+57,1.0E+58,1.0E+59,1.0E+60'
DC      D'1.0E+61,1.0E+62,1.0E+63,1.0E+64,1.0E+65'

```

```

EDAT5940
EDAT5950
EDAT5960
EDAT5970
EDAT5980
EDAT5990
EDAT6000
EDAT6010
EDAT6020
EDAT6030
EDAT6040
EDAT6050
EDAT6060
EDAT6070
EDAT6080
EDAT6090
EDAT6100
EDAT6110
EDAT6120
EDAT6130
EDAT6140
EDAT6150
EDAT6160
EDAT6170
EDAT6180
EDAT6190
EDAT6200
EDAT6210
EDAT6220
EDAT6230
EDAT6240
EDAT6250
EDAT6260
EDAT6270
EDAT6280
EDAT6290
EDAT6300
EDAT6310
EDAT6320
EDAT6330
EDAT6340
EDAT6350
EDAT6360
EDAT6370
EDAT6380
EDAT6390
EDAT6400
EDAT6410
EDAT6420
EDAT6430
EDAT6440
EDAT6450
EDAT6460
EDAT6470
EDAT6480

```

```

DC      D'1.0E+66,1.0E+67,1.0E+68,1.0E+69,1.0E+70'
DC      D'1.0E+71,1.0E+72,1.0E+73,1.0E+74,1.0E+75'
FND

```

```

EDAT6490
EDAT6500
EDAT6510

```

```

/*
// EXEC ASSEMBLR,PARM='LOAD,DECK'
//SOURCF.SYSIN DD *
SPIE    TITLE '...DIAGNOSTIC SUPPRESSOR SUBPRJGRAM...'
* 9/17/68 - L.F.H.
* MOD. 3/07/69 - L.F.H.
*
* USAGE...CALL SPIE( LDW )
*   WHERE LDW IS A PARAMETER CALLING FOR SETTING A NEW P.I.E. OR RE-
*   SETTING THE OLD P.I.E. DEPENDING ON WHETHER IT IS .GT. ZERO OR .LT.
*   ONE, RESPECTIVELY. IF THE NEW P.I.E. HAS BEEN SET, IT REMAINS IN
*   EFFECT ON SUBSEQUENT CALLS ON SPIE WITH LDW .GT. ZERO; THE OLD P.I.E.
*   IS RESET IF A SUBSEQUENT CALL ON SPIE HAS LDW .LT. ONE.
*                                     ...GOOD LUCK-L.F.H.
*
SPIE    CSECT
        ENTRY YECH,R1
        USING *,15
        R      S100
        DC     CL6'5SPIE '
SAREA  DS     18F
S100   STM   14,12,12(13)
*
        LA    12,SAREA
        ST   13,4(12)
        ST   12,8(13)
        LR   13,12
*
        BALR  2,0
        USING *,2
        DROP 15
*
        L     3,0(1)
        L     4,0(3)
        C     4,=F'1'
        BL   S300
*
        L     4,FLAG
        C     4,=F'1'
        RE   S200
        MVC  FLAG,=F'1'
*
        SPIF  YECH,((1,15))
        ST   1,R1
*
S200   L     13,4(12)
        LM   14,12,12(13)
        MVI  12(13),X'FF'
YECH   BCR   15,14
*
S300   L     4,FLAG
        C     4,=F'0'

```

```

SPIE0010
SPIE0020
SPIE0030
SPIE0040
SPIE0050
SPIE0060
SPIE0070
SPIE0080
SPIE0090
SPIE0100
SPIE0110
SPIE0120
SPIE0130
SPIE0140
SPIE0150
SPIE0160
SPIE0170
SPIE0180
SPIE0190
SPIE0200
SPIE0210
SPIE0220
SPIE0230
SPIE0240
SPIE0250
SPIE0260
SPIE0270
SPIE0280
SPIE0290
SPIE0300
SPIE0310
SPIE0320
SPIE0330
SPIE0340
SPIE0350
SPIE0360
SPIE0370
SPIE0380
SPIE0390
SPIE0400
SPIE0410
SPIE0420
SPIE0430
SPIE0440
SPIE0450
SPIE0460
SPIE0470
SPIE0480
SPIE0490

```

```

      RE      S200
      L       1,R1
      SPIE    MF=(E,(1))
      XC      FLAG,FLAG
      B       S200
*
R1      DS    F
FLAG    DC    F'0'
        LTORG
        END

/*
// EXEC ASSEMBLR,PARM='LOAD,DECK'
//SOURCE.SYSIN DD *
STIM    TITLE '...TIME INTERVAL MEASURING SUBPRDGRAM...'
* 6/14/68 - L.F.H.
* MOD. 8/30/68 - L.F.H.
*
STIME   CSECT
        ENTRY TTIME,T1
        USING *,15
        B      S100
        DC     X'05'
        DC     CL5'STIME'
S100    STM   14,12,12(13)
        LA    15,TTIME-STIME(15)
        USING TTIME,15
        NI    T102+1,X'0F'
        MVC   T2,T1
        B     T100
*
TTIME   STM   14,12,12(13)
        L     3,0(1)
        L     4,T1
        OI    T102+1,X'F0'
T100    LR    2,15
        USING TTIME,2
        DROP 15
        LA    12,SAREA
        ST    13,4(12)
        ST    12,8(13)
        LR    13,12
T102    BC    0,T200          **
*
T103    STIMER TASK,RTN,TUINTVL=T2
T105    L     13,4(12)
        LM    14,12,12(13)
        BCR   15,14
*
T200    TTIMER CANCEL
        L     4,T1
        SR    4,0
        ST    0,T1
        ST    4,0(3)
        B     T105
*
SPIE0500
SPIE0510
SPIE0520
SPIE0530
SPIE0540
SPIE0550
SPIE0560
SPIE0570
SPIE0580
SPIE0590

STIME010
STIME020
STIME030
STIME040
STIME050
STIME060
STIME070
STIME080
STIME090
STIME100
STIME110
STIME120
STIME130
STIME140
STIME150
STIME160
STIME170
STIME180
STIME190
STIME200
STIME210
STIME220
STIME230
STIME240
STIME250
STIME260
STIME270
STIME280
STIME290
STIME300
STIME310
STIME320
STIME330
STIME340
STIME350
STIME360
STIME370
STIME380
STIME390
STIME400
STIME410
STIME420

```

```

RTN      ABEND 4095,DUMP,STEP          STIME430
        EJECT                          STIME440
*                                              STIME450
T1       DC      F'138461538'          T-UNITS=60 MINUTES.  STIME460
T2       DS      F                      STIME470
SAREA    DS      18F                   STIME480
        END                               STIME490

/*
// EXEC ASSEMBLR,PARM='LOAD,DECK'
//SOURCE.SYSIN DD *
DATA     TITLE '...INITIAL DATA IN CSECTS DATA AND CONS...'
*
*     2/21/69 - L.F.H.
*     MOD. 9/03/69 - L.F.H.
*
DATA     CSECT
*
Z        DC      240D'0.0',80C' '
*
*                               ...PROGRAM CONTROL PARAMETERS...
*
NEQ1     DC      F'3'                   NO. OF 1ST PHASE DERIV. EQ'S.
NEQ2     DC      F'6'                   NO. OF 2ND PHASE DERIV. EQ'S.
J1       DC      F'0'                   BR. PARM. SET BY SUBP. SETH FOR SUBP. RK.
J2       DC      F'5'                   1ST PHASE PRINT FREQ.
J3       DC      F'5'                   H ADJUST. PARM.
J4       DC      F'0'                   CASE NO.
J5       DC      F'0'                   2ND PHASE EULERIAN POLE INDICATOR.
*
*                               ...CONVERSION CONSTANTS...
*
CONS     CSECT
TWPI     DC      D'6.2831853071795864769' 2*PI
CRTO     DC      D'57.29577951308232'    RADIANS TO DEGREES
CDTR     DC      D'1.745329251994330E-2'  DEGREES TO RADIANS
PID2     DC      D'1.570796326794897'    PI/2.0
PID4     DC      D'.7853981633974483'    PI/4.0
        END

/*
// EXEC LINKGO
//GO.SYSUDUMP DD SYSOUT=A,SPACE=(TRK,(8))
//GO.DATA5 DD *
        ...JAVELIN ROC STUDY DATA - PART 1.1...
        *****
        NOMINAL DATA WITH RELEASE AT VARYING GAMMA ANGLES.
        *****
1920     C'...JAVELIN ROC STUDY PART 1.1 - NO ALIGNMENT...'
8        D4.8828125D-4,9.5D0             H0,G1.
80       D.804167D0,.4286D0,1.456D0     D1,D2,D3.
136     D3.50333D0                       D8.
160     D.4D0,.1178D0,.3466D0,.42D0     M,JCY1,JCY2,JCY3.
192     D0D0,.03219D0,0D0               JCY4,JCY5,JCY6.
240     D7.5D0                           JVX1.
328     D6D1,5D-6                         YT,YEPS.
352     D515D0                             AX1.

```

```

DATA0010
DATA0020
DATA0030
DATA0040
DATA0050
DATA0060
DATA0070
DATA0080
DATA0090
DATA0100
DATA0110
DATA0120
DATA0130
DATA0140
DATA0150
DATA0160
DATA0170
DATA0180
DATA0190
DATA0200
DATA0210
DATA0220
DATA0230
DATA0240
DATA0250
DATA0260
DATA0270
DATA0280

```

```

JR0C0010
JR0C0020
JR0C0030
JR0C0040
JR0C0050
JR0C0060
JR0C0070
JR0C0080
JR0C0090
JR0C0100
JR0C0110
JR0C0120
JR0C0130

```







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