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(NASA-CR-163039) PRELIMINARY DESIGN DATA
PACKAGE, APPENDICES C1 AND C2 (South Coast
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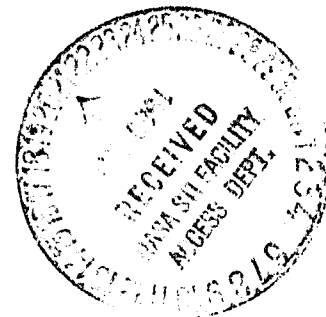
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JET PROPULSION LABORATORY
CALIFORNIA INSTITUTE OF TECHNOLOGY
PASADENA, CALIFORNIA

A P P E N D I C E S

C1 & C3

PRELIMINARY DESIGN DATA PACKAGE

PREPARED FOR:

JET PROPULSION LABORATORIES

CONTRACT NUMBER 955189

PREPARED BY:

SOUTH COAST TECHNOLOGY, INC.

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TABLE OF CONTENTS

	<u>Page</u>
APPENDICES	
C1 COMPUTER PROGRAM DOCUMENTATION	
C1.1 HYBRID2	C-1
C1.2 VSY3 & VSYS2	C-67
C1.3 CRASH	C-108
C1.4 Handling Programs	C-132
C1.5 Life Cycle Costs	C-175
C3 ENERGY AND MATERIALS	C-182

C1.1 HYBRID2

1. Program Description

HYBRID2 computes the fuel and energy consumption of a hybrid vehicle with a bi-modal control strategy over specified component driving cycles. Fuel and energy consumption are computed separately for the two modes of operation. The program also computes yearly average fuel and energy consumption using a composite driving cycle which varies as a function of daily travel.

The modelling techniques used include the following:

Heat engine - represented by a map of bsfc as a function of bmep and rpm, together with a curve of maximum torque versus rpm. The displacement of the engine for which this data is supplied is used as input; the program has provisions for scaling the data to other displacements.

Electric motor/controls - electrical input represented as a constant load plus shaft power divided by a fixed efficiency, in both driving and braking modes. Maximum (driving) and minimum (braking) torque as functions of rpm are also required.

Battery - modelled by a fractional depletion technique using the power averaged over a specified time interval rather than instantaneous power.

Engine accessory load - represented by a curve of torque required vs. system output (torque converter input) rpm. Included in these is the transmission front pump, in addition to belt-driven accessories.

Torque converter - represented by curves of speed and torque

ratios (output/input) as functions of an output speed-torque parameter equal to output speed/output torque. An input speed-torque factor, $(\text{input speed})^2 / (\text{input torque})$, at stall must also be specified.

Gearbox - represented by a set of gear ratios with different efficiencies for each ratio. Spin loss coefficients (exclusive of the front pump) may also be specified.

Differential - same treatment as gearbox.

Vehicle road load - represented by a combination of an aerodynamic load (proportional to speed squared) and tire rolling resistance. The rolling resistance coefficients can include a constant term and one which is linear with vehicle speed.

The program structure is modular, with the control strategy and shift strategies being contained in separate subroutines. A breakdown of the program routines and their functions is as follows:

1. HYBRID2 (Main Program)
 - Input of case data
 - Output
 - Numerical integration
 - Computation of yearly average fuel and energy consumption from individual driving cycle results.
2. VEHIC
 - Computation of road loads, power flow through the vehicle system up to the torque converter output.

- Computation of derivatives of all variables of integration.
3. HYREAD
 - Input of fixed, detailed component data.
 4. GRSHFT
 - Controls transmission gear ratio in accord with a pre-set shift strategy.
 5. PMOVR
 - Controls heat engine/motor power split in accord with a pre-set control strategy.
 6. TQCON
 - Computes torque converter input speed and torque given output conditions, or output torque and input speed given input torque and output speed.
 7. FILTER
 - Filters battery output power to provide a smoothed battery output power curve.
 8. INT1, INT2
 - One and two dimensional interpolation routines, respectively.

PARAMETERS		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	NRPM	—	Number of RPM's (engine)
	NMEP	—	Number of BMEP's and BSFC's
	FUELSG	g/cc	Fuel specific gravity
	DISPL	cc	Displacement
	SCALE	—	Scale factor for engine
	RPM(20)	rpm	RPM (engine)
	TQMAX(20)	ntm	Maximum torque (engine)
	BMEP(20)	bar	Brake mean effective pressure
	BSFC(20,20)	g ^{cc} /kw-hr	Brake specific fuel consumption
	NOP	—	Number of engine powers
	RPMBST	rpm	Best operating speed (engine)
	PBEST	kw	Best operating power (engine)
	PEOP(20)	kw	Engine power
	RPMEOP(20)	rpm	Optimum engine speed at specified power
	NSPMo	—	Number RPM's (motor)
	EMUM	—	Motor efficiency
	EMUG	—	Generator efficiency
	TMSKL	—	Scale factor for motor
	PINNL0	kw	No load input power (motor)
	RPMIDL	rpm	Idle speed (motor)
	RPMOPM	rpm	Best operating speed (motor)
	SPMo(20)	rpm	RPM (motor)
	TQMAX(20)	ntm	Maximum torque (motor)
	TQMIN(20)	ntm	Minimum torque (motor)
	JCVT	—	= 1 → continuously variable transmission (CVT)
	EMUCVT	—	Efficiency (CVT)
	RATUP	—	Speed up ratio (CVT)
	RATDN	—	Slowdown ratio (CVT)
	NTSP	—	Number of TSFs, TQ's and SF's
	CTCZRO	rpm ² /ntm	NI*2/NI (STALL)
	TSP(20)	rpm ² /ntm	NO/√TO (MODE 1)
	TSR2(20)	—	NO/√TO (MODE 2)
	TQR(20)	—	TO/NI
	SPR(20)	—	NO/NI
	NGEAR	—	Number of gears
	NIH	—	Number of THSET's, U/SHIFT's, and L/SH
	UPSEL	rpm	Shift up for electric operation
	DNSEL	rpm	Shift down for electric operation
	NLOCK(5)	—	Lockup (gear box)
	TRATIO(5)	—	Ratio (gear box)

PARAMETERS		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	CT2(5)	nt ^m /rpm	Spin loss coefficient (gear box)
	EMUT(5)	—	Torque efficiency (gear box)
	THSET(5)	KW	Set of powers defining shift function
	UPSHFT(5)	rpm	Upshift RPM
	DNSHFT(5)	rpm	Downshift RPM
	NDDSCH	—	Number discharge depths (battery)
	NDENS	—	Number of specific powers (battery)
	WE	KG	Battery Mass
	EBMAX	wh/KG	Energy density (battery)
	EMURG	—	Average regeneration efficiency (battery)
	EMURG2	—	Maximum regeneration efficiency (battery)
	CHGEFF	—	Recharge efficiency (battery)
	DDISCH(50)	—	Discharge depth (battery)
	CYCLES(50)	—	Cycle life (battery)
	PDENS(50)	KW	Specific power (battery)
	EDENS(50)	mJ	Specific energy (battery)
	DRATIO	—	Differential ratio
	CD1	nt ^m	Spin loss coefficient (differential)
	CD2	nt ^m /rpm	Spin loss coefficient (differential)
	EMUD	—	Torque efficiency (differential)
	RTIRE	m	Rolling radius (tire)
	CTIRE1	—	Rolling resistance coefficient (tire)
	CTIRE2	1/(kw/hr)	Rolling resistance coefficient (tire)
	NAX	—	Number speeds and torques (accessory load)
	RPMAX(50)	rpm	Speed (accessory load)
	TAX(50)	nt.m	Torque (accessory load)
	VMASS	KG	Vehicle mass
	DLI	kg.m ²	Driveline inertia
	CDA	m ²	Drag coefficient * area
	NCYCLE	—	Number of driving cycles
	NTC(3)	—	TIME, SPEDC matrix size
	NPRIC(3)	—	Output print flag for driving cycle
	NUNITS	—	Miles/hr to km/hr conversion flag
	DTC(3)	SEC	Time interval for driving cycles
	TFC(3)	SEC	Final time for driving cycles
	TIME(3,200)	SEC	Time (driving cycle)
	SPEDC(3,200)	KM/HR	Speed (driving cycle)
	NCOMP	—	DSUP, DMC, GAMMA matrix size
	DSTAV	—	Average usage

7 KAVEL
DISTANCE
DATA

PARAMETERS		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	DSUP(3)	KM	Maximum distance-driving cycle
	DNC(3)	-	Fraction of total distance
	GAMMA(30,3)	-	Driving cycle weights
	NCASE	-	Number of cases
	TEOMIN	nt.m	Minimum engine torque (mode 1)
	TEOMN2	nt.m	Minimum engine torque (mode 2)
	DBMAX	-	Battery discharge limit
	PEOMIN	KW	Heat engine minimum power
	VMAX	km/hr	Transition speed
	DTFLTR	-	low-pass filter sub-interval length

} TRAVEL
DISTRIBUTION
DATA

VARIABLES		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	A(3)	m/sec ²	Vehicle acceleration vector
	ABPI	J	Absolute value battery power
	BDBAR(30)	KW	Battery energy consumption - composite cycle
	BLIFE	KM	Battery life (expected)
	BPI	J	Battery power
	DBAR(30)	KM	Interpolated values of driving cycle distance
	DDAV	KM	Average distance on driving cycle
	DELT	SEC	Time interval size
	DEPL(3)	1/km	Battery depletion on each cycle
	DIST(3)	m	Distance on each cycle
	DLOW	KM	Minimum distance on driving cycle
	DT	SEC	Time increment
	EB	MJ	System output energy - Mode 1
	EB2	MJ	System output energy - Mode 2
	EBMAX	wh/KG	Energy density (battery)
	ECAV	MJ/KM	Yearly average energy consumption
	ECBAR(30)	MJ/KM	Composite cycles energy consumption - Mode 1
	ECBAR2(30)	MJ/KM	Composite cycles energy consumption - Mode 2
	ECH(3)	MJ/KM	Cycle heat engine energy consumption
	ECMAV(30)	MJ/KM	Composite cycles mode averaged energy consumption
	ECONS(3)	MJ/KM	Cycle energy consumption - Mode 1
	ECONS2(3)	MJ/KM	Cycle energy consumption - Mode 2
	ECSYS(3)	MJ/KM	Cycle system energy consumption
	EHFAN	MJ/KM	Yearly avg. heat engine energy consumption
	EHFBAR(30)	MJ/KM	Composite cycles heat engine energy consumption
	EK(80)	-	YDOT kinetic energy
	EKIN	MJ	Kinetic energy
	ERG(2900)	MJ	Battery specific energy
	ESYSAN	MJ/KM	Yearly average system energy consumption
	ESYSBR(30)	MJ/KM	Composite cycles system energy consumption
	FCAN	g/KM	Yearly average fuel consumption
	FCBAR(30)	g/KM	Composite cycles fuel consumption - Mode 1
	FCBAR2(30)	g/KM	Composite cycles fuel consumption - Mode 2
	FCMAV(30)	g/KM	Composite cycles mode averaged fuel consumption
	FCONS	g/KM	Cycle fuel consumption, Mode 1
	FCONS2	g/KM	Cycle fuel consumption, Mode 2
	FEAV	KM/L	Yearly averaged fuel economy
	HEEF	-	Heat engine energy fraction
	IBP(20)	-	Storage for battery power distribution

VARIABLES		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	INT1	--	Interpolation subroutine (1 dimensional)
	INT2	-	Interpolation subroutine (2 dimensional)
	ITIBP	-	Total number of cycle time iterations
	K	-	Print skip control counter
	NPRNT	-	Number of skips between successive prints
	NTIME	-	Number of TIME's and STEPS
	PBRK	KW	Braking power
	PED	KW	Engine output power
	PED2	KW	Engine output power 2
	PEOP	KW	Set of powers for optimum power drive
	PGO	KW	Regenerative output power
	PMO	KW	Motor output power
	PMO2	KW	Motor output power 2
	PMOT(2800)	W	Storage for cycle specific battery power
	PRW	KW	Renewable power
	PSO	KW	Hybrid system output power
	PSO2	KW	Hybrid system output power 2
	RANGE(30)	KM	Range for new battery discharge limit
	RFRAC(30)	-	Composite cycles fraction of total distance
	RPMTC1	rpm	Torque converter RPM - Mode 1
	RPMTC2	rpm	Torque converter RPM - Mode 2
	SPEED(20)	KM/HR	Driving speed profile
	SPENG(25)	MJ	Composite cycle specific energy - Mode 1
	SPPWR(25)	KW	Composite cycles specific power - Mode 1
	T	SEC	Time in simulation
	TIME(200)	SEC	Driving cycle time
	TTMP	SEC	Time holder
	V(L)	km/hr	Vehicle speed vector
	VAVG(3)	m/sec	Average velocity
	VBAR(25)	m/sec	Composite cycles average speed
	VMASS	kg	Effective mass of vehicle
	VMPS	m/sec	Vehicle speed
	VRECIP	sec/m	Reciprocal of avg velocity for composite cycle
	VTMP	m/sec	Velocity hold
	VTMPL	m/sec	Velocity hold
	WPAV	KW/km	Yearly average wall plug output

VARIABLES		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	Y(1)	MJ	Aerodynamic + rolling resistance energy loss
	Y(2)	MJ	Drive train energy output - Mode 1
	Y(3)	MJ	Drive train energy output - Mode 2
	Y(4)	MJ	Braking output energy
	Y(5)	MJ	System output energy - Mode 1
	Y(6)	MJ	System output energy - Mode 2
	Y(7)	MJ	Engine output energy - Mode 1
	Y(8)	MJ	Engine output energy - Mode 2
	Y(9)	MJ	Motor shaft output energy - Mode 1
	Y(10)	MJ	Motor shaft output energy - Mode 2
	Y(11)	m/sec	Velocity
	Y(12)	KM	Distance
	Y(13)	MJ	Generator output energy
	Y(14)	sec	Heat engine on time - Mode 1
	Y(15)	sec	Heat engine on time - Mode 2
	Y(16)	g	Fuel output energy - Mode 1
	Y(17)	g	Fuel output energy - Mode 2
	Y(18)	MJ	System Output energy - Mode 1
	Y(19)	MJ	System Output energy - Mode 2
	YDOT(20)	—	Runge-Kutta integration variables
	YTMP(20)	—	Runge-Kutta integration variables
	MOT	—	Number of entries in vector PMOT after Power function smoothed
	JGEAR	—	Gear Mode 1 current in m
	JGEAR2	—	Gear Mode 2 current in m
	NTM	—	Number of entries in vector PMOT
	TF	sec	Final time in simulation of cycle

VARIABLES		UNITS	DESCRIPTION	ORIGINAL PAGE IS OF POOR QUALITY
EQUATION	PROGRAM			
	BRMED	bar	Brake main pressure - Mode 1	
	BRMED2	bar	Brake main pressure - Mode 2	
	FA	nt	Aerodynamic drag force	
	FAC	nt	Acceleration force on vehicle	
	FC	g/hr	Engine fuel rate - Mode 1	
	FC2	g/hr	Engine fuel rate - Mode 2	
	FG	nt	Road grade force	
	FNET	nt	Net vehicle force	
	FR	nt	Rolling resistance force	
	PA	KW	Aerodynamic drag power	
	PD	KW	Differential output power	
	PLTC	KW	Power load on torque converter - Mode 1	
	PLTC2	KW	Power load on torque converter - Mode 2	
	PR	KW	Rolling resistance power	
	PRW	KW	Rear wheel power	
	PT	KW	Transmission output power	
	RPMD0	rpm	Differential output rpm	
	RPME0	rpm	Engine output rpm	
	RPME02	rpm	Engine output rpm - Mode 2	
	RPMS0	rpm	Hybrid system output rpm	
	RPMS02	rpm	Hybrid system output rpm - Mode 2	
	RPMT0	rpm	Transmission output rpm	
	SFC	g/kwh	Specific fuel consumption	
	TDO	nt-m	Lift-off output torque	
	TEO	nt-m	Engine output torque	
	TEO2	nt-m	Engine output torque - Mode 2	
	TLFD	nt-m	Differential torque loss	
	TLFT	nt-m	Transmission torque loss	
	TLFT2	nt-m	Transmission torque loss - Mode 2	
	TSD	nt-m	Hybrid system output torque	
	TSD2	nt-m	Hybrid system output torque - Mode 2	
	TTO	nt-m	Transmission output torque	
	HLCL	-	Gear lockup flag Mode 1	
	HLCL2	-	Gear lockup flag Mode 2	

VARIABLES		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	CC	$\text{rad}/(\text{int.ang.})$	$(\text{rad}/\text{sec}) / (1000 \text{ rpm})$
	PCDM	KW	
	PHEMAX	KW	Maximum heat engine power
	PHEMIN	KW	Minimum heat engine power
	PMMAX	KW	Maximum motor power
	PNDM	KW	Nominal power
	RPMTC	rpm	Torque converter rpm
	RPMTCN	rpm	Torque converter input rpm
	RPMTCD	rpm	Torque converter output rpm
	TACC	nt.m	Accessory output torque
	TGO	nt.m	Generator output torque
	THEMAX	nt.m	Maximum heat engine torque
	TMMAX	nt.m	Maximum motor torque
	TMMIN	nt.m	Minimum motor torque
	TMO	nt.m	Motor output torque
	TMO2	nt.m	Motor output torque 2
	TTCN	nt.m	Torque converter input torque
	TTCN1	nt.m	Torque converter input torque - Mode 1
	TTCN2	nt.m	Torque converter input torque - Mode 2
	TTCO	nt.m	Torque converter output torque
	JBRK	--	Braking (not) required flag

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VARIABLES		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	SPRAT	—	speed ratio
	TQRAT	—	torque ratio
	TSPAR	$\frac{1 \text{ in}^2}{\text{in}^2 \cdot \text{min}}$	torque speed ratio
	TSPAR2	$\frac{1 \text{ in}^2}{\text{in}^2 \cdot \text{min}}$	torque speed ratio 2

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PAGE: 1 OF 5

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FORTRAN CODING FORM

GENERAL RESEARCH CORPORATION

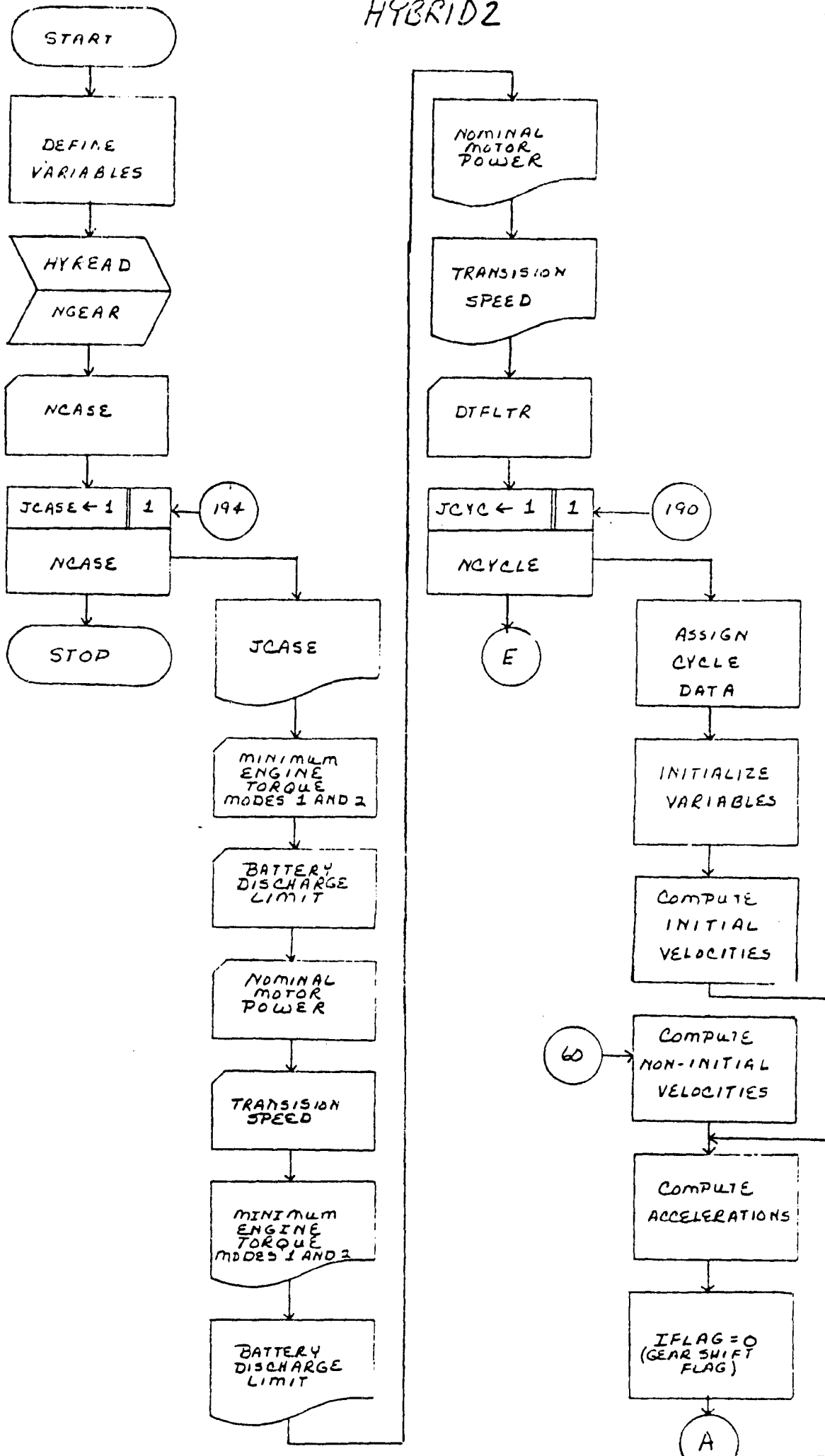
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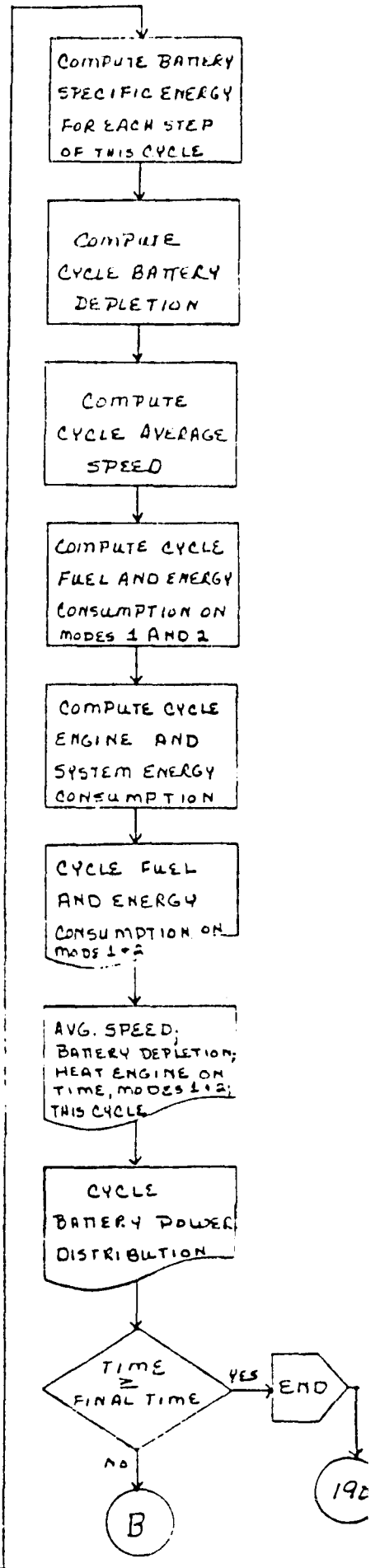
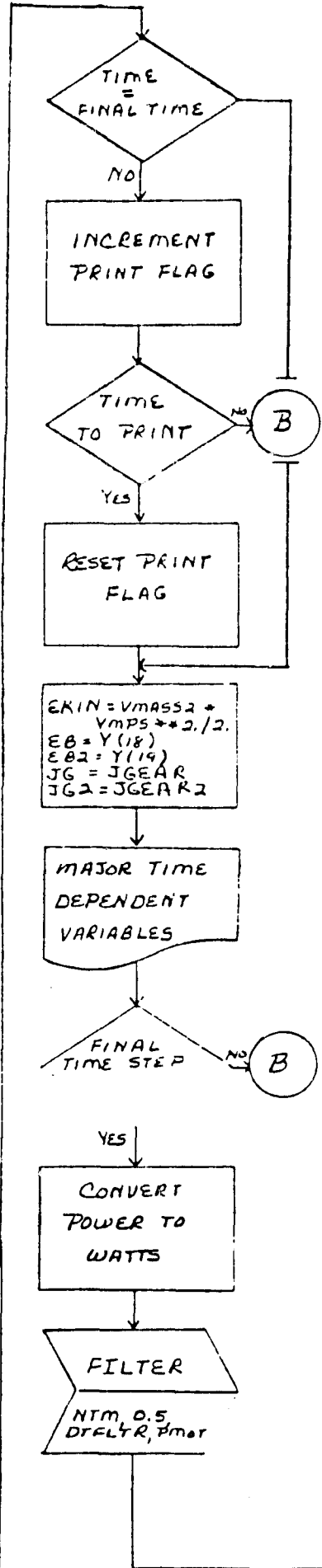
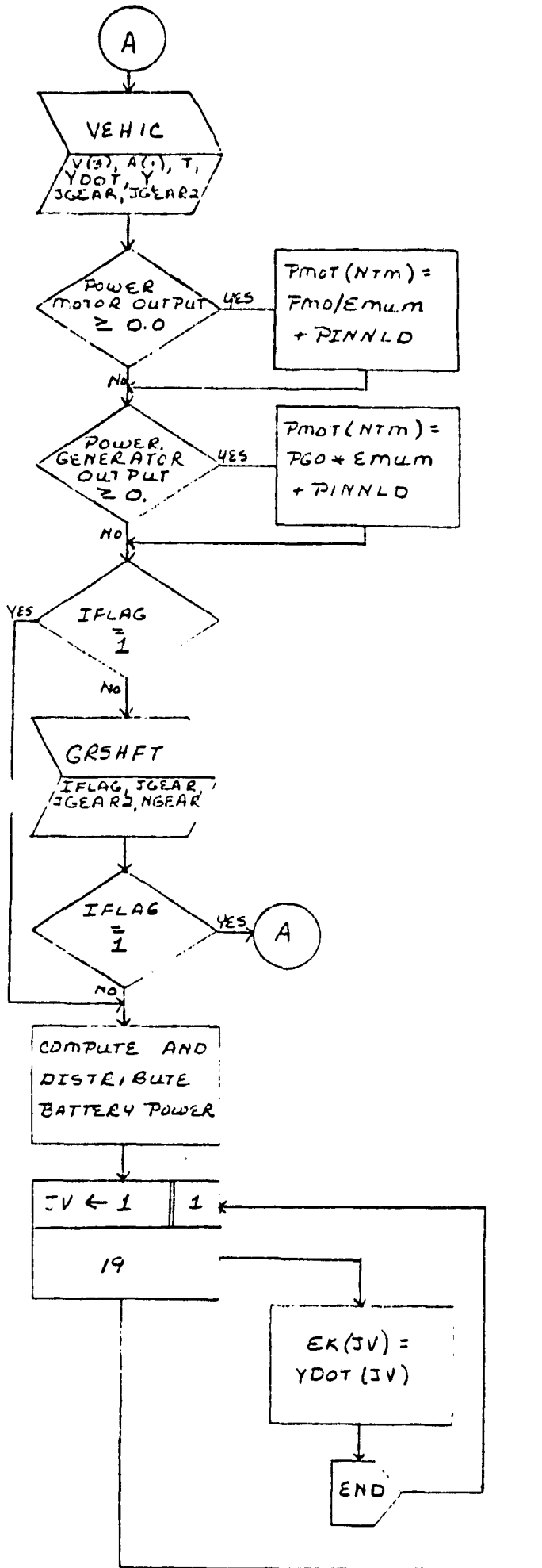
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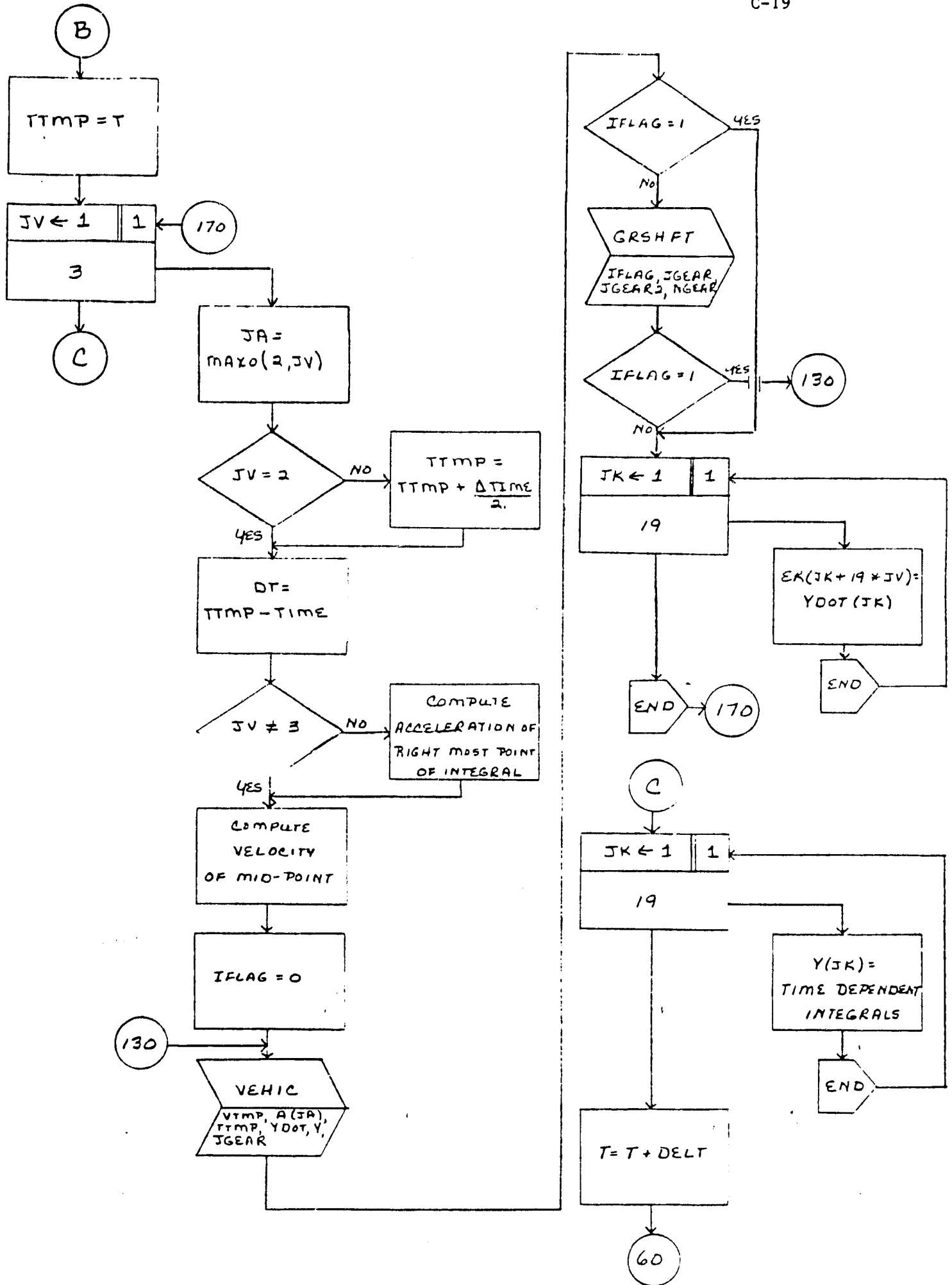
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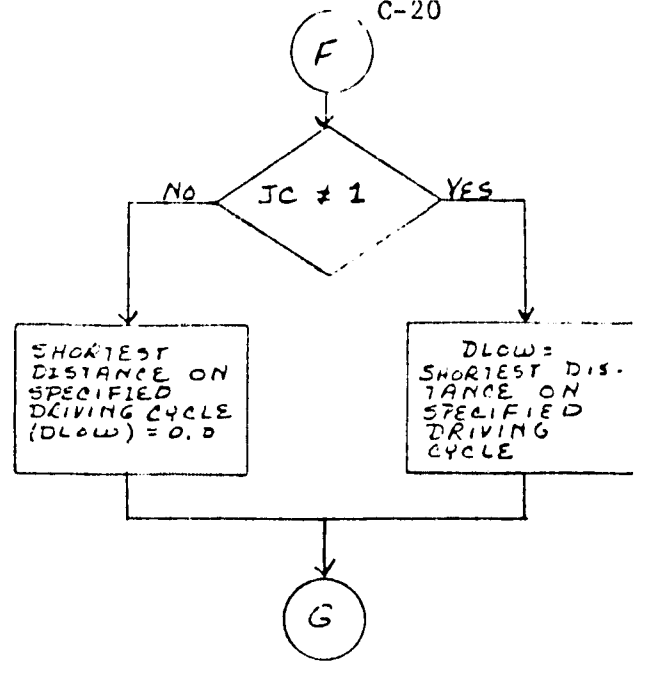
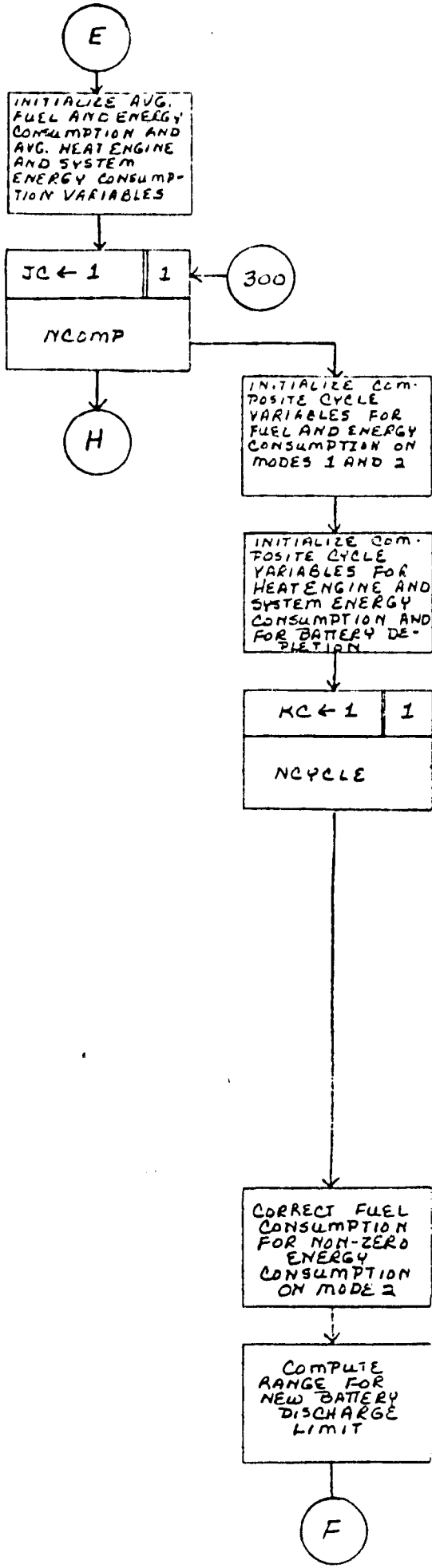
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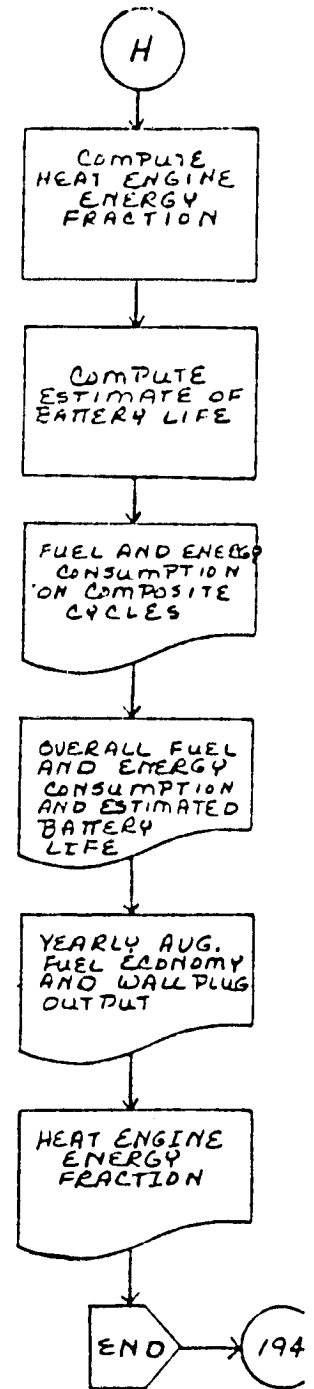
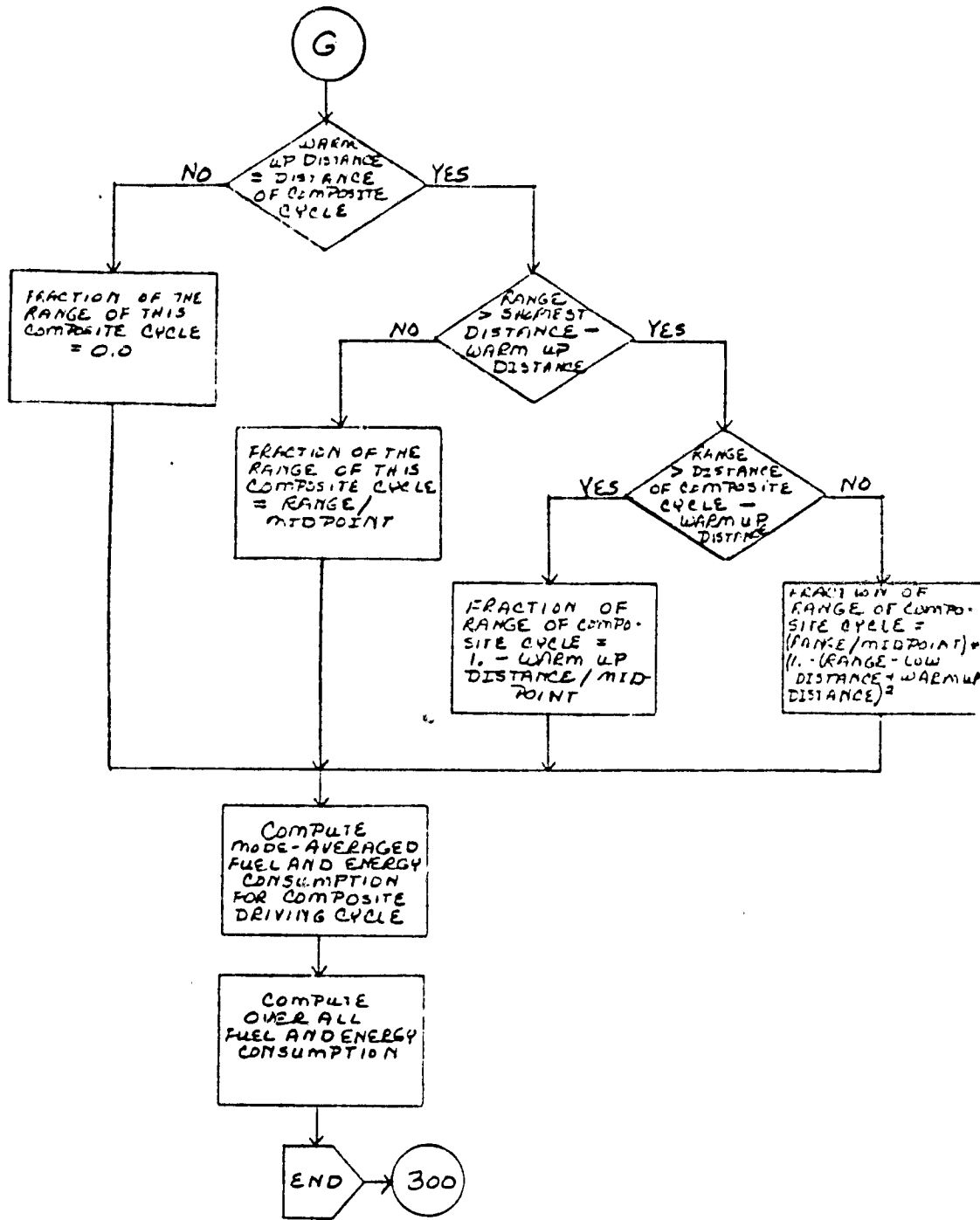
HYBRID2

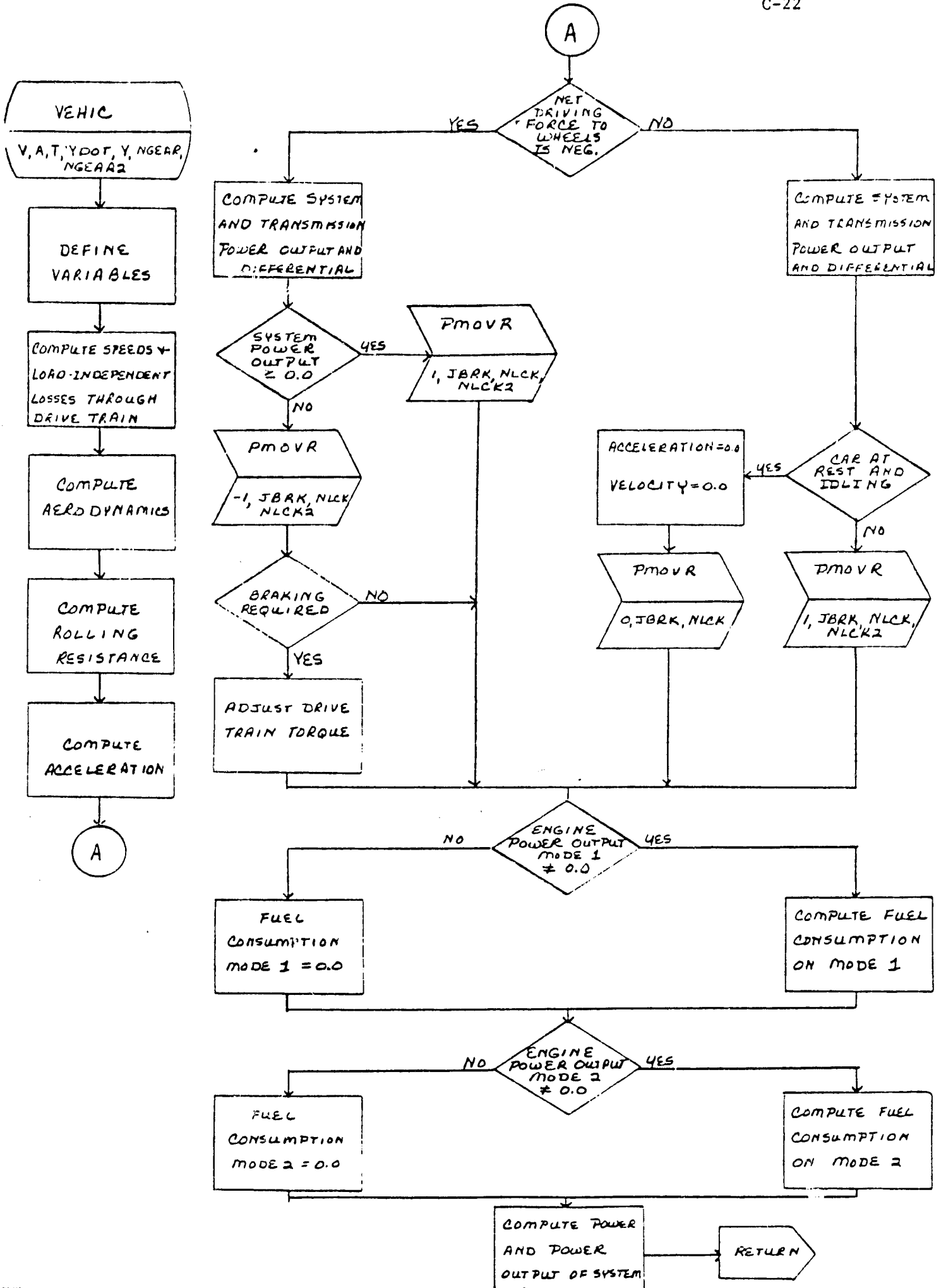


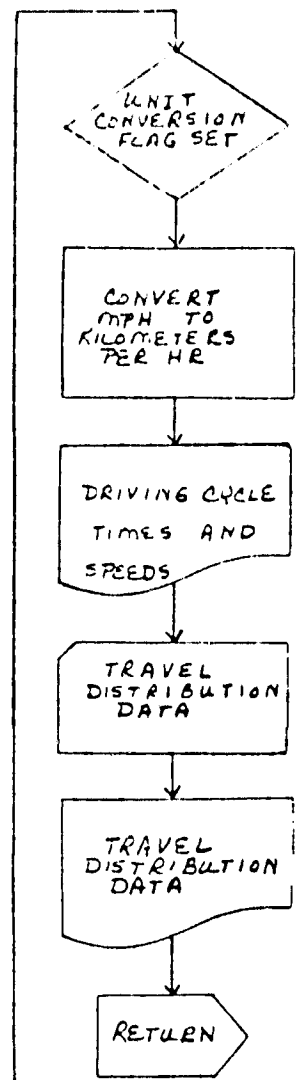
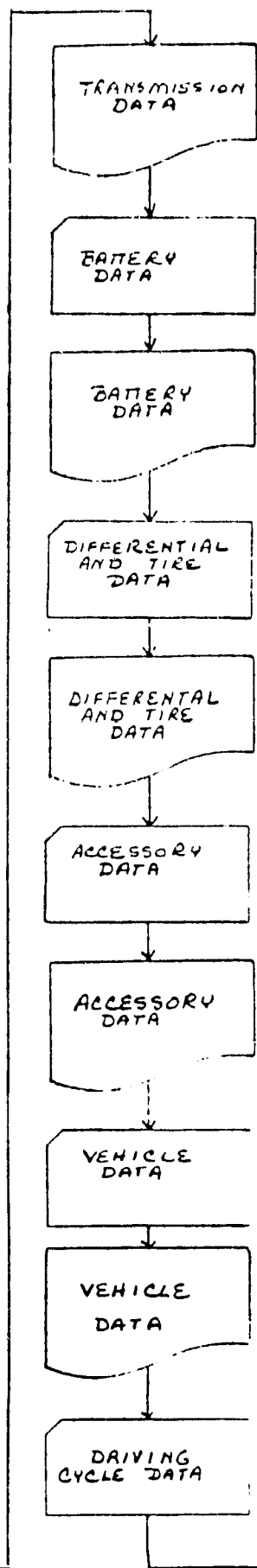
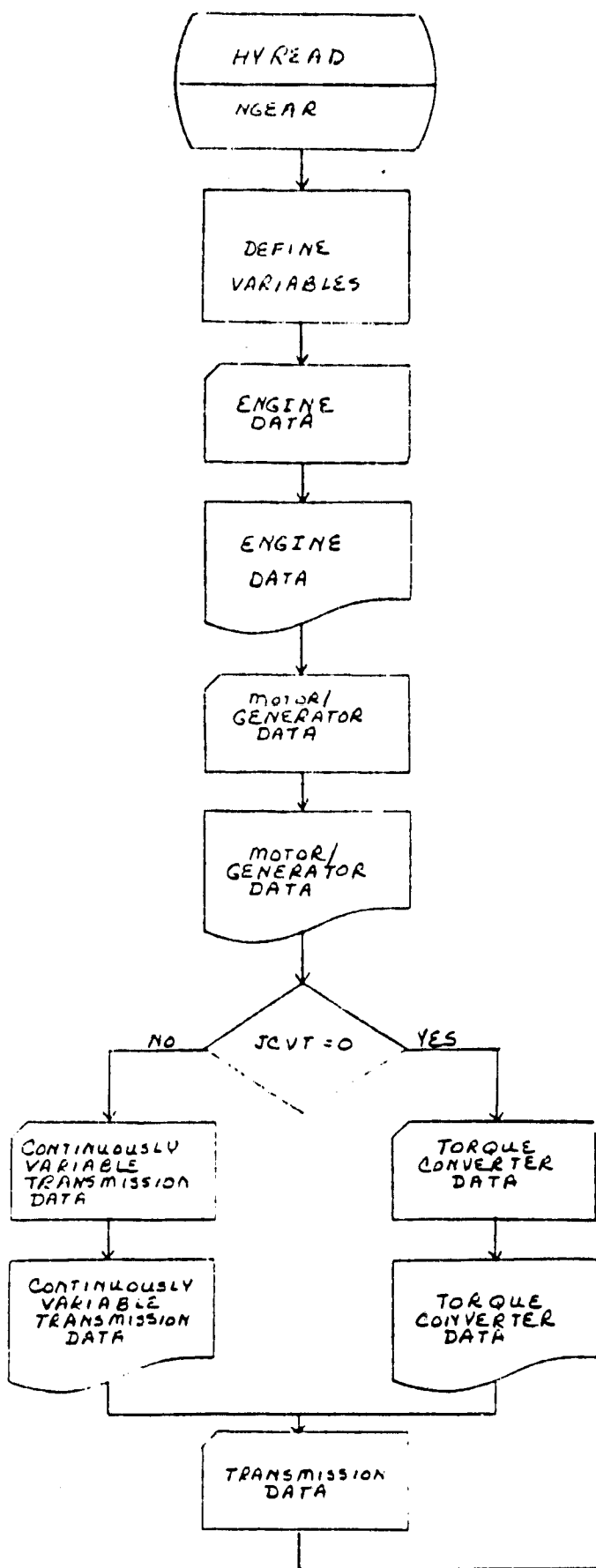


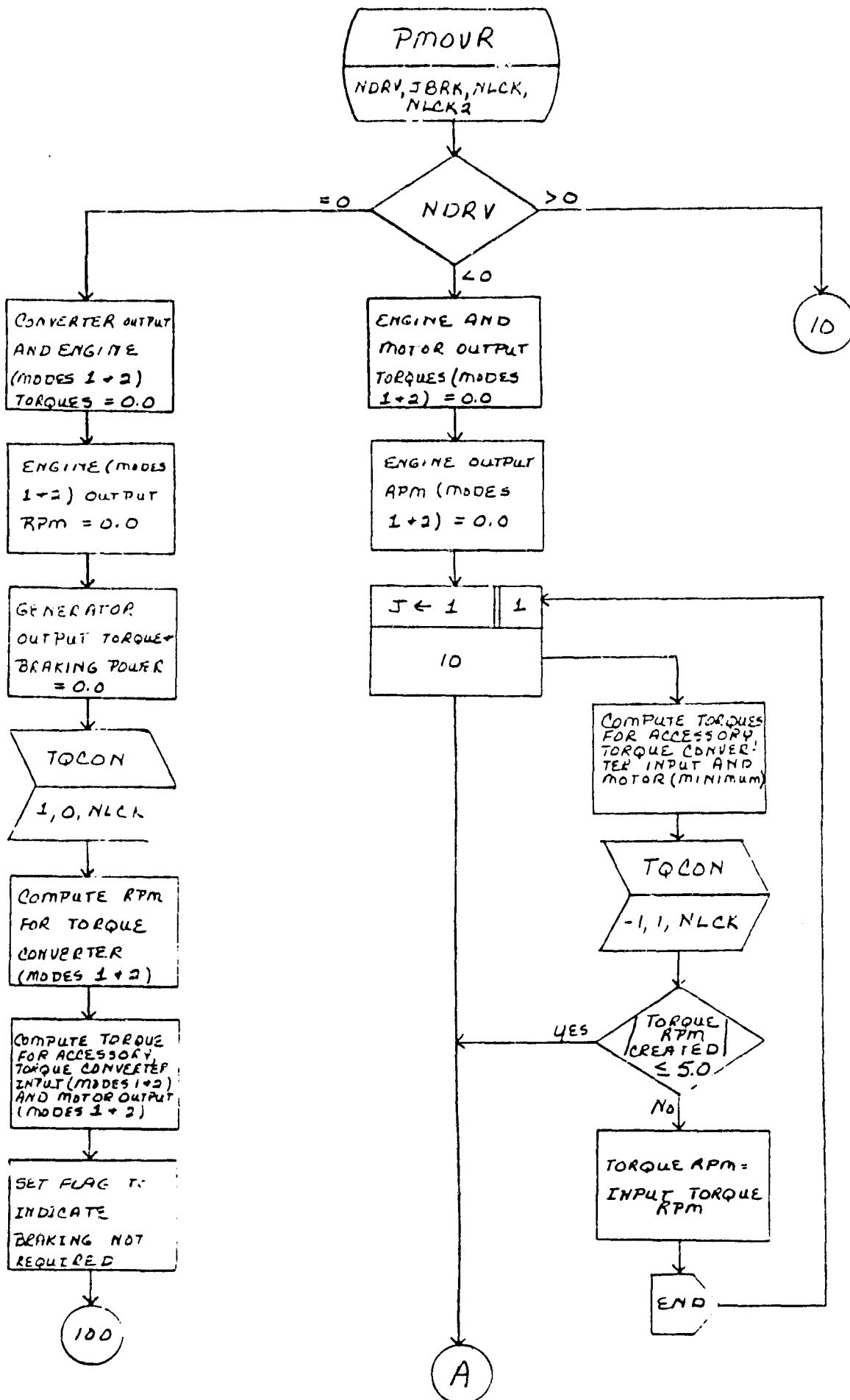


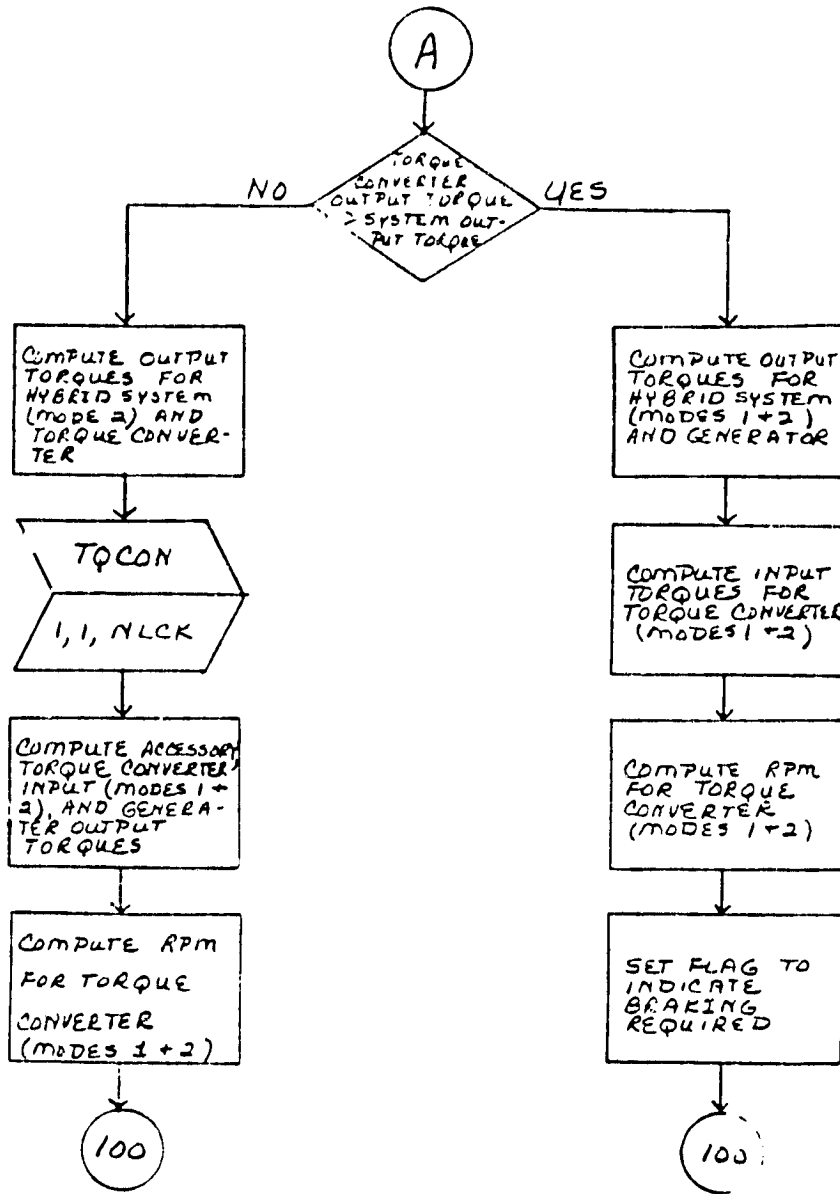


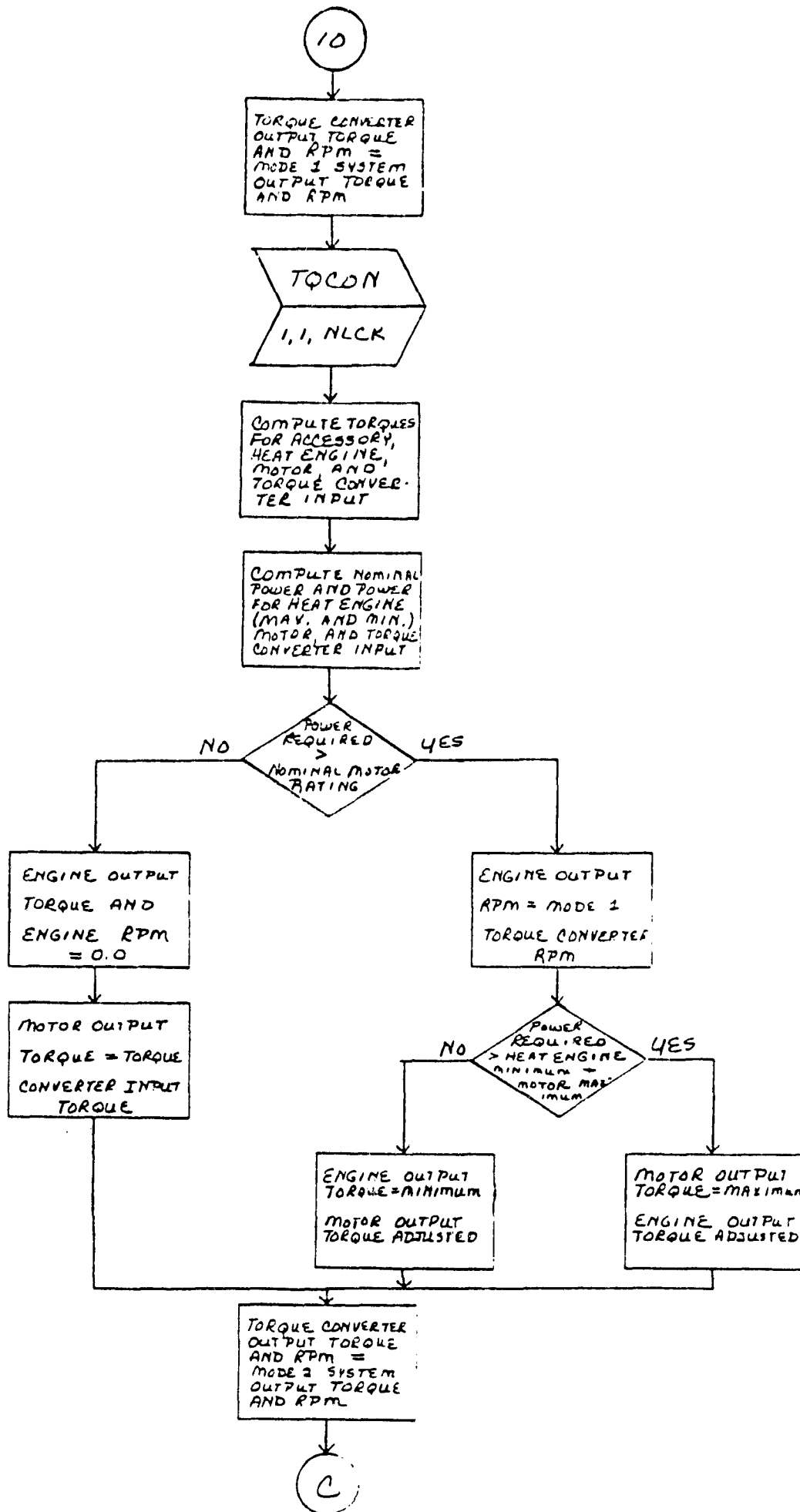


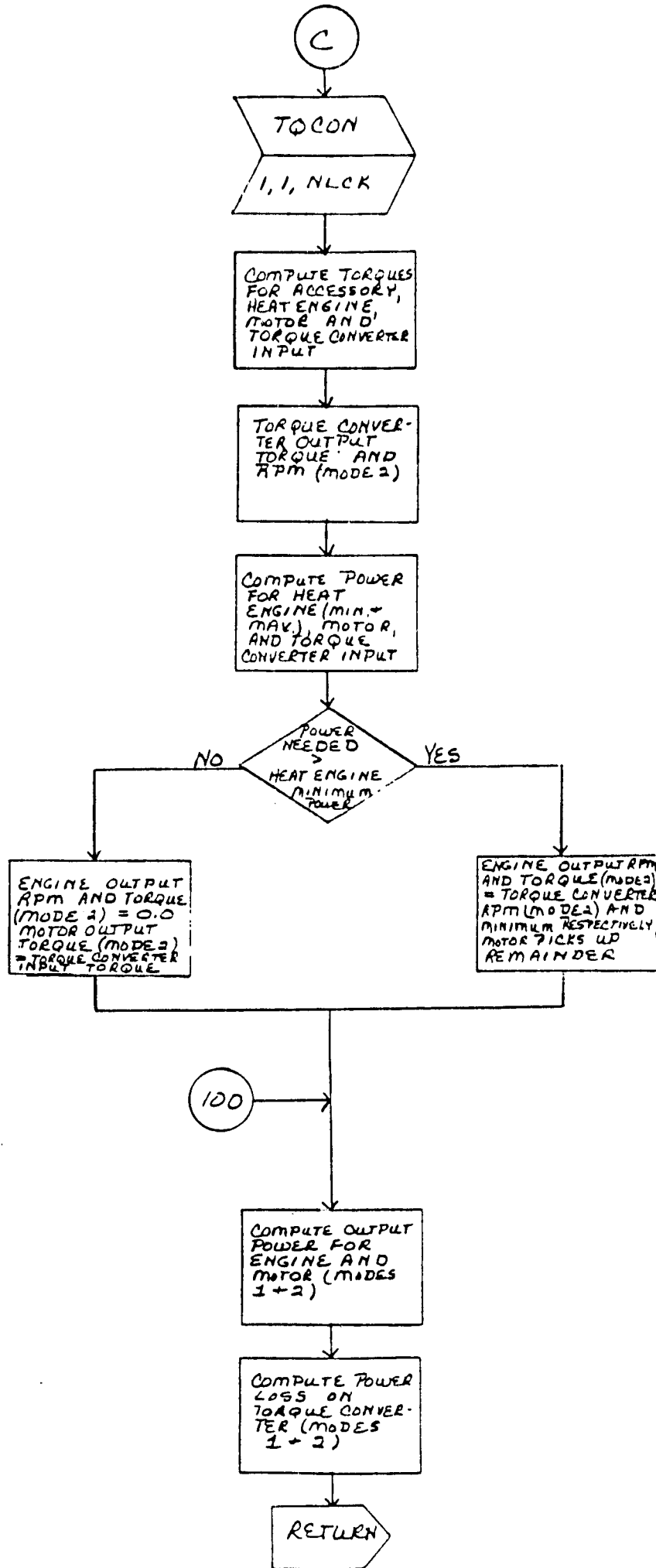


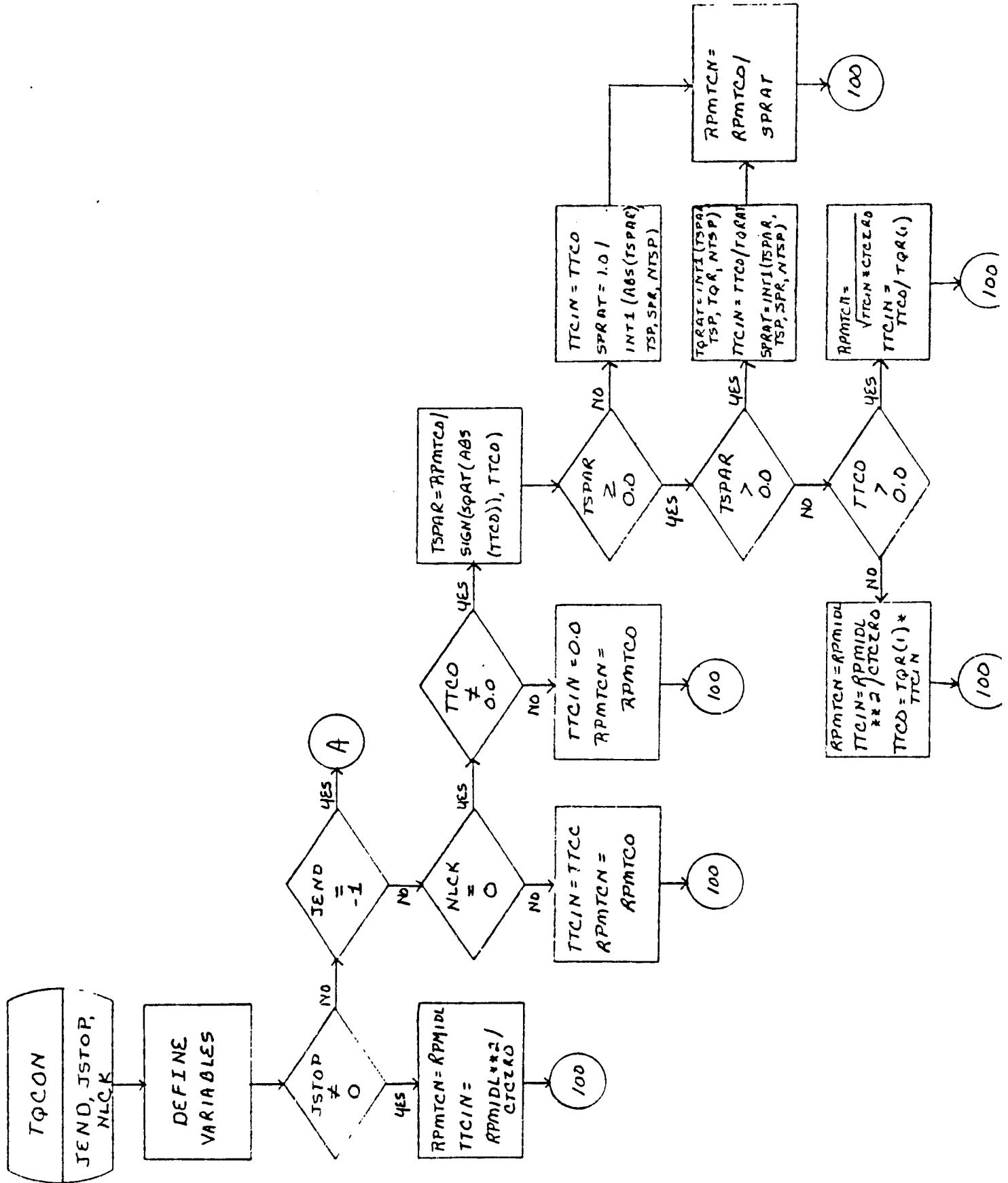


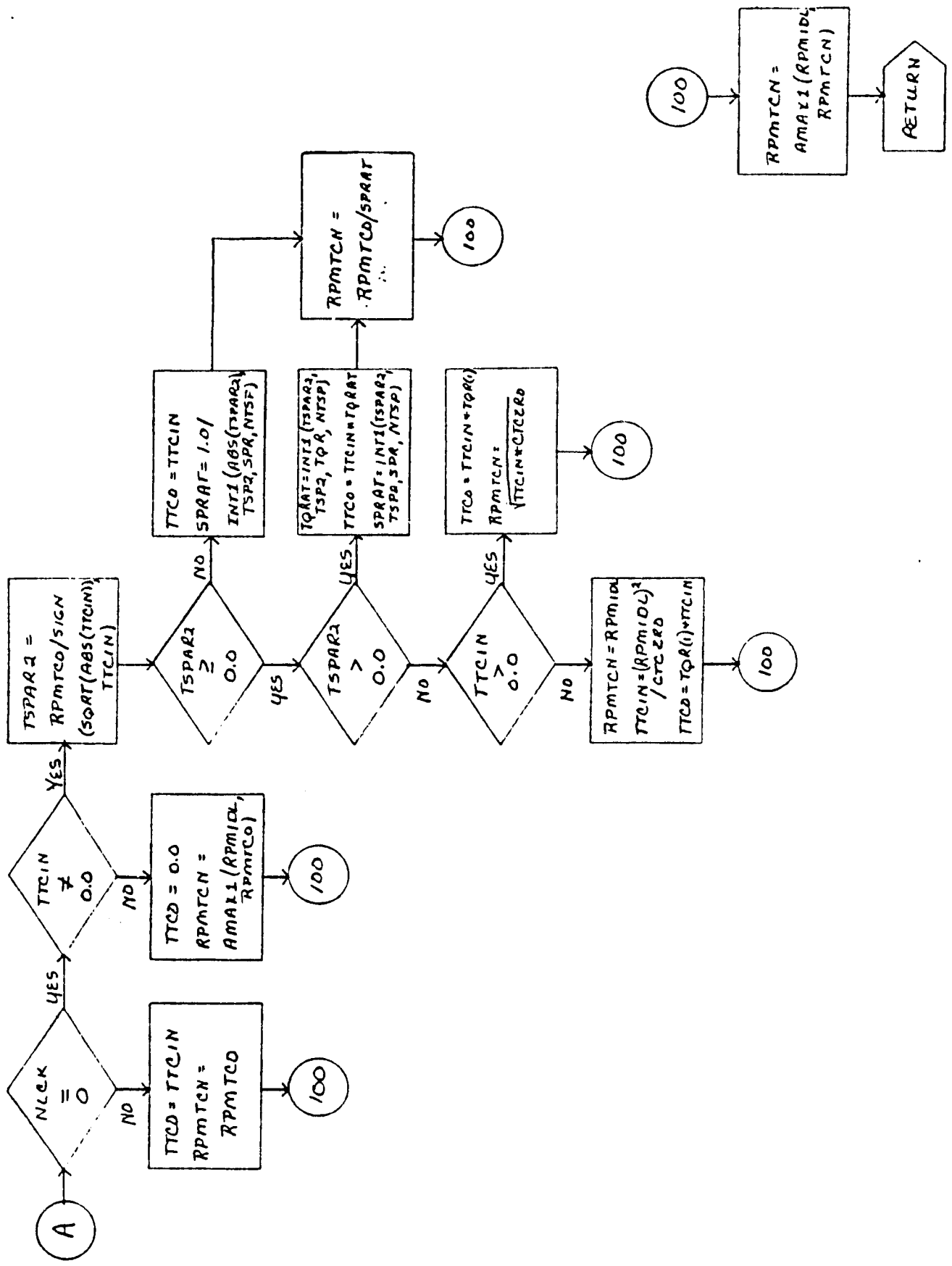


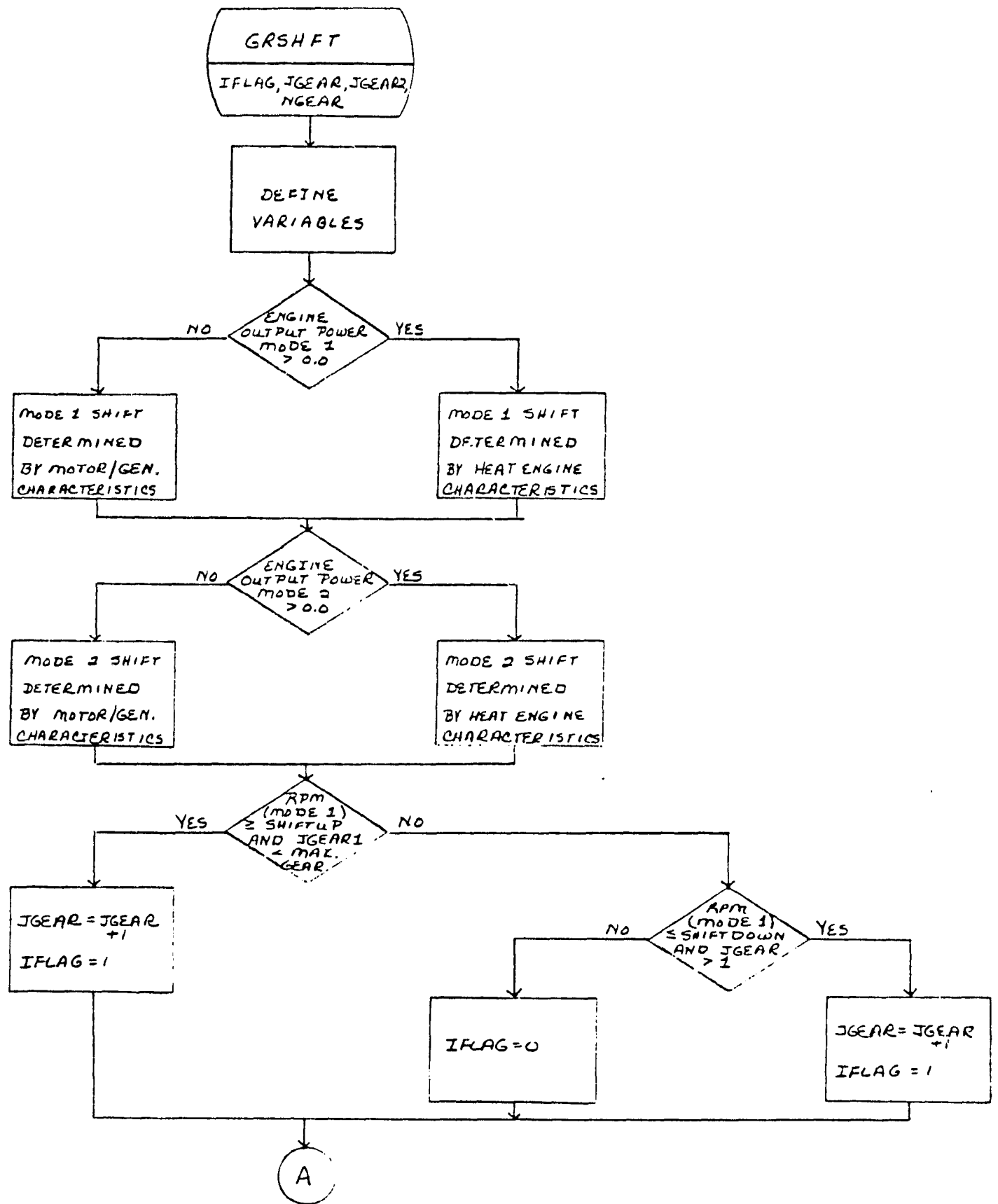


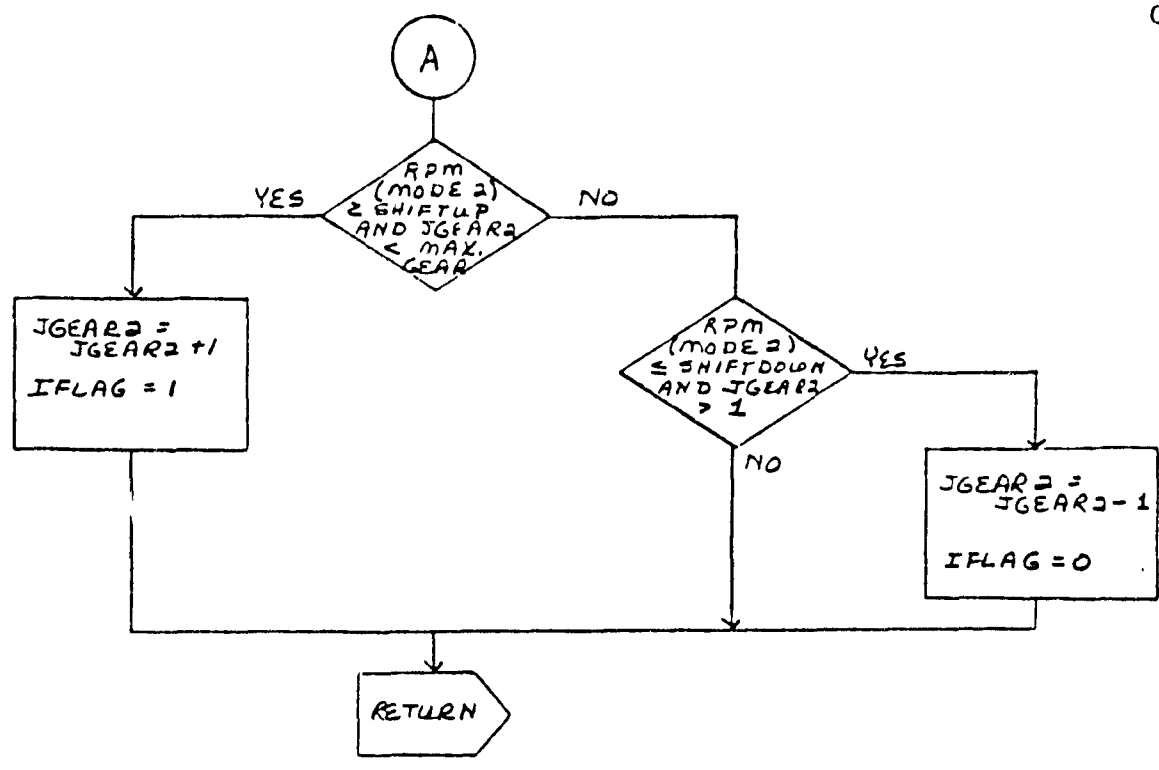


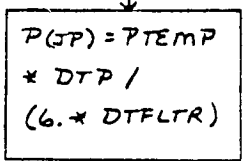
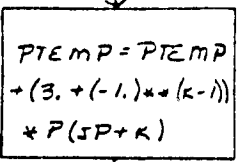
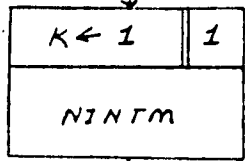
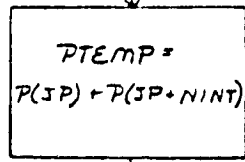
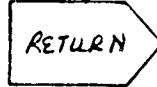
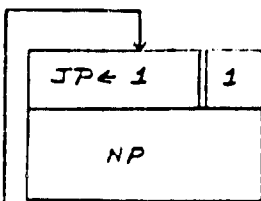
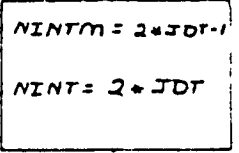
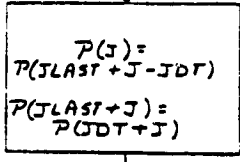
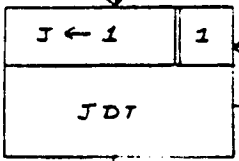
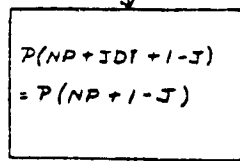
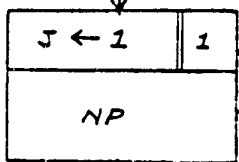
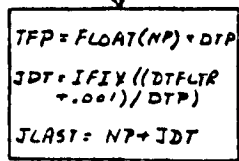
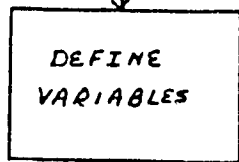
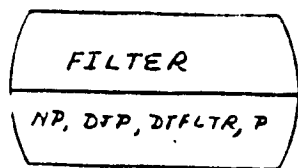


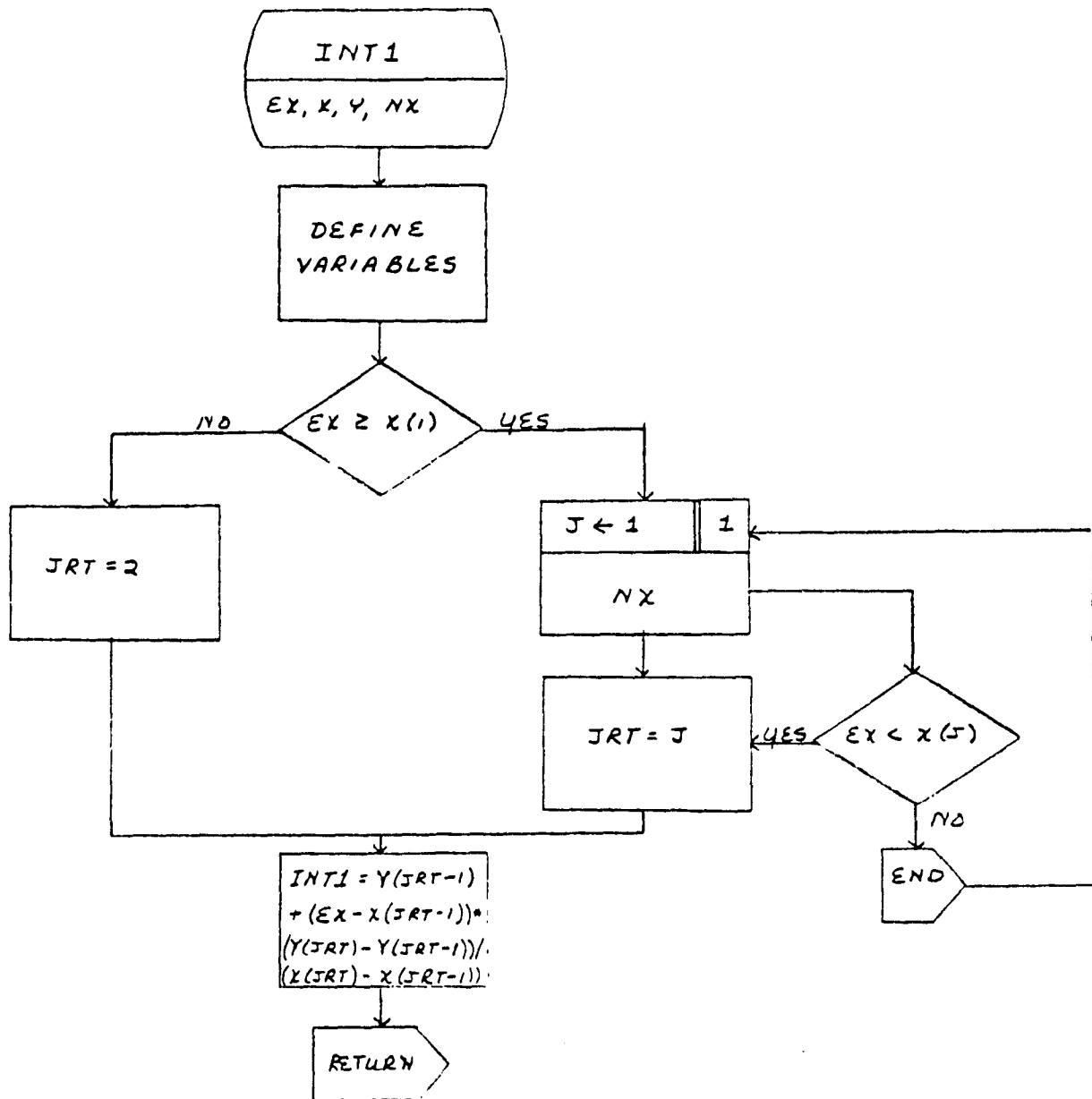


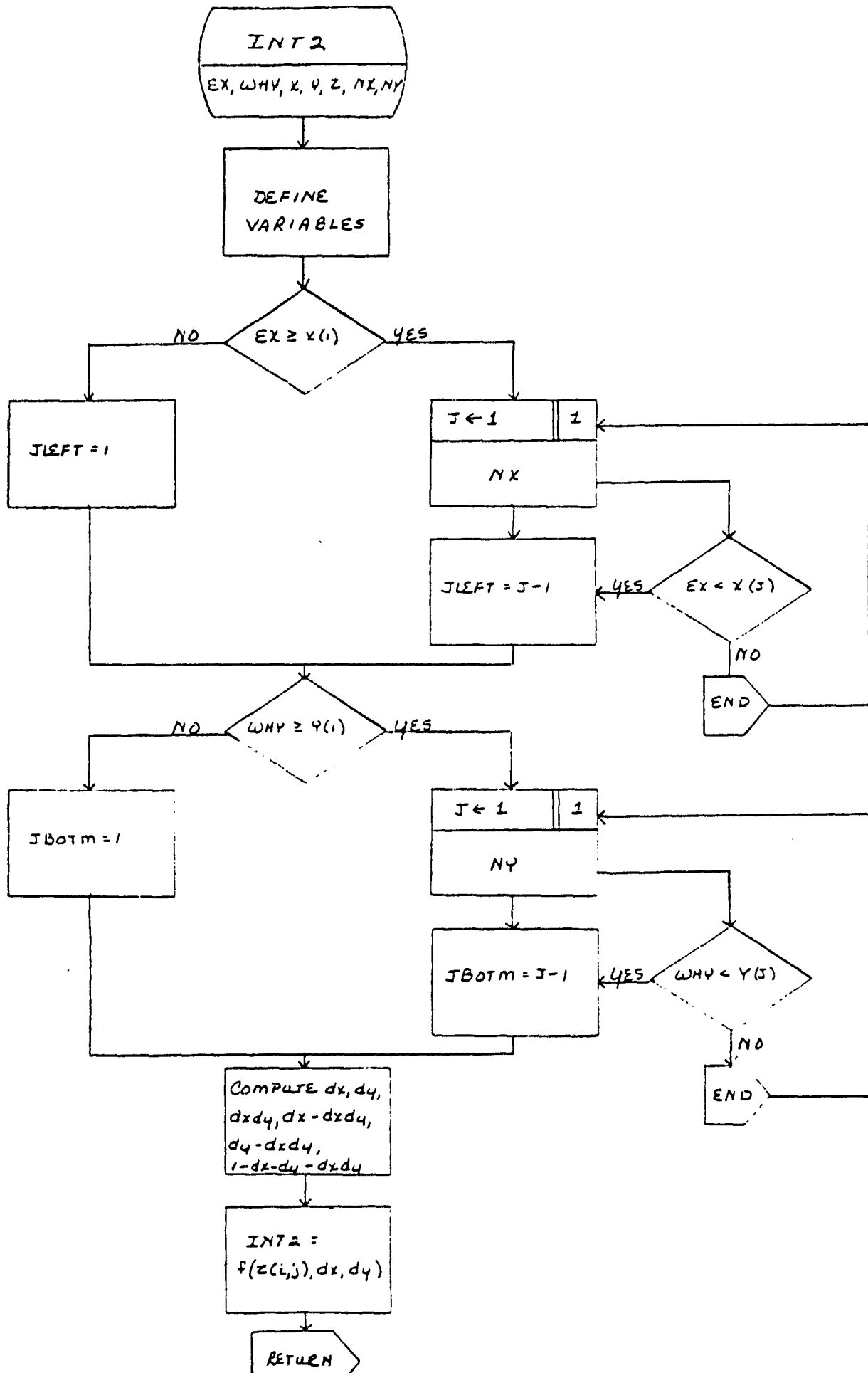












FORTRAN CODING FORM

GENERAL RESEARCH CORPORATION

PROGRAM	NAME	DATE	PAGE 2 OF 3
ROUTINE			

STATEMENT NO.	FORTRAN STATEMENT										SERIAL NUMBER	
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5	1	2	3	4	5	6	7	8	9	0	1	2
	EMUCVT	CONTINUOUSLY VARIAB	RATION	LE TRANSMISSION DATA								
		TORQUE CONVERTER DATA										
	MTSP	TSP(1)	TQR(1)	SPR(1)	TSP(MTSP)	TQR(MTSP)						
	CTGRD											
	SPR(MTSP)											
		TRANSMISSION DATA										
	NGEAR	MTH	UPSEL	PNSEL								
	NLOCK(1)	TRATIO(1)	CTA(1)	CTB(1)	EDUT(1)							
	RATIO(NGEAR)	CTA(NGEAR)	CTB(NGEAR)	EDUT(NGEAR)								
		BATTERY DATA										
		INDPENS	WIB	EBMAX	EMURG	EMURGR	CHGEFF					
	INDPCH(1)	CYCLES(1)		DISCH(NDDSCH)	CYCLES(NDDSCH)							
	PDENS(1)	EDENS(1)		PDENS(NDEMS)	EDENS(NDEMS)							
		DIFFERENTIAL AND TIRE DATA										
	DRATIO	CD1	CD2	EMUD	RTIRE	CTIRE1	CTIRE2					

FORTRAN CODING FORM

PROGRAM HYBRID2 NAME _____

ROUTINE HYREAD DATE _____

PAGE 3 OF 3

STATEMENT NO.	FORTRAN STATEMENT										SERIAL NUMBER	
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GOLETA FCRTFAN 1.3 * SEMI-AUTO PFL * (01-10-73)

PROGRAM HYBRID2

HYBRID2 MODELS OPERATION OF HYBRID VEHICLE OVER SPECIFIED DRIVE CYCLES.

DATA IN COMMON -

COMMON DISPL, FPM(20), TQMAX(20), BMEP(20), BSFC(20,20), NRPM, NMEP,
 1EMUM, EMUG, PINKLD, SPMO(20), TMOYMAX(20), TMOYMIN(20), NSPMO,
 2CTCZPO, TSP(20), TGR(20), SFR(20), TSP2(20), NTSP,
 3NLOCK(5), TRATIO(5), CT1(5), CT2(5), FMUT(5),
 4WB, FBMAX, FMURG, EMURG2,
 5DRATIO, CD1, CD2, FMUD, FTIRE, CTIRE1, CTIRE2, VMASS, DLI, CCA,
 6TFOMIN, PRMAX, RPMIDL, VMASS2, PEOMIN,
 7FUELSG, SKALE, TMSKL, NTH, NDCSCH, CHGFFF, NCYCLE, NCCMP, CSTAV,
 8NUNITS, THSFT(5), UPSHFT(5), DNSHFT(5), DDISCH(20), CYCLES(20), NTC(3
 9NFRIC(3), CTC(3), TFC(3), CSUP(30), DNC(30), DBAR(30)
 1, RPMBST, PBEFT, FEOP(20), RFMEOP(20), RPMOPM, EMUCVT, RATUP, PATDN, NOP
 2, PCENS(20), ECENS(20), NCEAS
 3, VMAX, TECMN2, UPSEL, DNSEL, DWASH, NAX, RPMAX(20), TAX(20)
 COMMON TIMO(3,200), SPECC(3,200), GAMMA(30,3)

VARIABLES IN COMMON -

COMMON FA, FR, FAC, FNET, TCC, TTC, RPMDO, RPMTC, TSC, RPMSC, RPMTCO, TTCC
 1RPMTCN, THO, TEC, THO2, TEC2, TGC, PSC, PEO, PEO2, FMC, PMO2, PGO, PRK, FC,
 2PO, PT, PRW, PLTC, THRPO, TTCIN
 3, RPMEO, RPMEO2, PLTC2, VMPS
 4, TSO2, RPMSC2, FSC2, RPMTC1, RPMTC2, RPMEP, RPMER2

REAL YOCT(20), Y(20), INT1, INT2, V(6), A(3), YTMP(20)
 REAL EK(80)
 REAL DIST(3), FCNS(3), FCNS2(3), ECONS(3), ECONS2(3)
 REAL FCBAF(30), FEPAC(30), TIME(200), SPEED(200),
 1FCBAR2(30), FCBAR(30), FCBAR2(30), FANGE(30), FCMAY(30), EOMAY(30)
 REAL SCHE(3), ECSYS(3), FHEBAR(30), ESYSPR(30)
 REAL VAUG(3)
 REAL VBAR(25), SPWR(25), SPENG(25)
 REAL PMCT(200), ERG(200), DEFL(3), RDBAR(30)
 INTEGER IEP(20)

CALL HYFEAD(NCFAP)

INPUT RUN DATA

READ 600, NCASE
 DO 194 JCASE=1, NCASE
 PRINT 925, JCASE
 READ 610, TECMIN, TECMN2, DEMAX, PEOMIN, VMAX
 PRINT 930, TECMIN, TECMN2, FBMAX, FEOMIN, VMAX
 VMAX=VMAX/3, F
 READ 610, CTFLTP
 DO 190 JCYC=1, NCYCLE
 PRINT 700
 NTIME=NTC(JCYC)
 NPONT=NPNTC(JCYC)
 DELT=DTC(JC(C))

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GOLETA FCRTFAN 1.3 * SEMI-AUTO CFL * (01-10-73)

HYST02

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000077      TF=TF0(JCYC)
000101      MCT=IFIX(TF/DELTA+2.*(DTFLTR/1.0)+1.)
      106      DO 47 J=1,NTIME
000110      TIME(J)=TIMC(JCYC,J)
000114      SPEED(J)=SPECC(JCYC,J)
000117      47 CONTINUE
000121      DO 48 J=1,MCT
000122      PMOT(J)=0.0
000123      48 CONTINUE
C
C      INITIALIZE VARIABLES OF INTEGRATION
C
000125      DO 50 J=1,20
000127      Y(J)=0.0
000130      IBP(J)=0
000131      50 CONTINUE
000133      T=0.0
000134      ITIBP=0
000135      K=NPRINT
000136      JGEAR=1
000137      JGEAR2=1
000140      NTM=0
C
C      COMPUTE VELOCITY AND ACCELERATION
C
000141      V(1)=0.0
      142      V(3)=SPEED(1)
      143      V(4)=INT1(DELTA/2.,TIME,SPEED,NTIME)
000151      V(5)=INT1(DELTA,TIME,SPEED,NTIME)
000155      V(6)=INT1(3.*DELTA/2.,TIME,SPEED,NTIME)
000163      V(2)=V(3)+V(3)-V(4)
000165      GO TO 70
000166      60 V(1)=V(3)
000170      V(3)=Y(11)
000171      V(2)=(V(1)+V(3))/2.
000174      V(4)=V(6)
000175      V(5)=INT1(T+DELTA,TIME,SPEED,NTIME)
000203      V(6)=INT1(T+3.*DELTA/2.,TIME,SPEED,NTIME)
000213      70 A(1)=(V(4)-V(2))/(3.6*DELTA)
000217      A(1)=AMIN1(A(1),9.8)
000222      A(2)=(V(5)-V(3))/(3.6*DELTA)
000226      A(2)=AMIN1(A(2),9.8)
C
C      COMPUTE VEHICLE OPERATING CONDITIONS AT MAJOR TIME POINT
C
000231      IFLAG=0
000232      80 CALL VEHIC(V(3),A(1),T,YDOT,Y,JGEAR,JGEAR2)
000241      NTM=NTM+1
000243      IF(PMO.GE.0.)PMCT(NTM)=PMO/EMUM+PINNLD
000247      IF(PGO.NE.0.)PMOT(NTM)=PGO*EMUM+PINNLD
000254      IF(IFLAG.EQ.1)GO TO 93
      256      CALL GRSHT(IFLAG,JGEAR,JGEAR2,NGEAR)
000261      IF(IFLAG.EQ.1)GO TO 80
000263      93  BPI=YDOT(18)*1000.
000265      ABPI=ABS(BPI)

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GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

HYPRIO2

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000267      DO 94 J=1,20,2
      1270      JTH=J
      1271      IF (APPI.GT.2*J-4.AND.APPI.LE.2*J) GO TO 95
000310      94 CONTINUE
000312      95 IF (RPI+2.0.GT.0.0) GO TO 96
000316      IBP(JTH+1)=IBP(JTH)+1
000320      GO TO 97
000321      96 IBP(JTH)=IBP(JTH)+1
000324      97 CONTINUE
000324      DO 98 JV=1,19
000326      EK(JV)=YDOT(JV)
000330      98 CONTINUE

C
C      TIME TO PRINT RESULTS -
C

000332      IF (T.EQ.TF) GO TO 100
000334      K=K+1
000335      IF (K.LT.NPRNT) GO TO 110
000337      K=0
000340      100 EKIN=VMASS2*VMPS**2/?
000343      ER=Y(18)
000345      FB2=Y(19)
000346      JG=JGEAR
000350      JG2=JGFAP2
000351      PRINT 710,T,Y(11),Y(12),FRW,FBRK,Y(1),Y(4),EKIN,
      1JG,RFMTC1,Y(2),Y(5),Y(7),Y(9),Y(13),Y(18),FSC,PEC,PMC,PGC,
      2JG2,FPYTC2,Y(3),Y(6),Y(8),Y(10),Y(19),FSC2,PEC2,PMO2
000451      IF (T.LT.TF) GO TO 110
000454      DIST(JCYC)=Y(12)
000456      DO 101 J=1,NTM
000457      PMOT(J)=PMOT(J)*1000.
000461      101 CONTINUE
000463      CALL F1 TFC (NTM,0.5,DTFLTR,PMOT)
000466      DO 102 J=1,NTM
000470      IF (PMOT(J).LT.0.0) GO TO 105
000472      ERG(J)=INT1 (PMOT(J)/WB,PCENS,EDENS,NDENS)
000502      ERG(J)=ERG(J)*WB
000504      GO TO 102
000505      105 ERG(J)=WB*FEMAX/EMUPG
000511      102 CONTINUE
000514      DEPL(JCYC)=2.*PMOT(1)/ERG(1)
000517      NTMS=NTM-1
000521      DO 106 J=1,NTMS
000522      DEPL(JCYC)=DEPL(JCYC)+(3.+(-1.)**(J-1))*PMOT(J+1)/ERG(J+1)
000534      106 CONTINUE
000537      DEPL(JCYC)=DEPL(JCYC)/(3.*3600.)
000541      DEPL(JCYC)=DEPL(JCYC)/DIST(JCYC)
000543      VAVG(JCYC)=DIST(JCYC)*3600./TF
000546      FCCNS(JCYC)=Y(16)/Y(12)
000550      ECCNS(JCYC)=E2/(3.6*Y(12))
      553      FCCNS2(JCYC)=Y(17)/Y(12)
      555      ECCNS2(JCYC)=E22/(3.6*Y(12))
000557      ECHE(JCYC)=Y(8)/Y(12)
000561      ECSYS(JCYC)=(Y(6)+Y(8))/Y(12)
000564      PRINT 940,Y(12),FCCNS(JCYC),FCCNS2(JCYC),ECCNS(JCYC),ECCNS2(JCYC)

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GCLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

HYBRID2

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000601      PRINT 945, VAVG(JCYC), DFPL(JCYC), Y(14), Y(15)
000615      DO 108 J=1,19
000617          ITIPP=ITIPP+IEP(J)
000621      108 CONTINUE
000623      PRINT 1020, IEP(18), IEP(16), IEP(14), IEP(12), IEP(10), IEP(8), IEP(
1 IEP(4), IEP(2), (IEP(J), J=1,19,2), ITIPP
000660      DO 109 J=1,19
000662          IEP(J)=0
000663      109 CONTINUE
000665          ITIPP=0
000666          IF(T.GE.TF) GO TO 190

```

C
C
C

INTEGRATE TO NEXT TIME STEP

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000670      110 TTMP=T
000672          DO 170 JV=1,3
000673              JA=MAX0(2,JV)
000676              IF(JV.EQ.2) GO TO 121
000677              TTMP=TTMP+DELT/2.
000702      121 DT=TTMP-T
000704              IF(JV.NE.3) GO TO 122
000706              A(3)=(V(6)-(VTMP+VTMPL)/2.)/(3.E*DELT)
000715              A(3)=AMIN1(A(3),9.8)
000720      122 VTMPL=VTMP
000722              VTMP=Y(11)+EK(11+(JV-1)*19)*CT
000731              IFLAG=0
000732      130 CALL VEHIC(VTMP, A(JA), TTMP, YDOT, Y, JGEAR, JGEAR2)
000743              IF(IFLAG.EQ.1) GO TO 160
000745              CALL GPSHFT(IFLAG, JGEAR, JGEAR2, NGEAR)
000750              IF(IFLAG.EQ.1) GO TO 130
000752      140 DO 170 JK=1,19
000754              EK(JK+19*JV)=YDOT(JK)
000761      170 CONTINUE
000765          DO 180 JK=1,19
000766              Y(JK)=Y(JK)+DELT*(EK(JK)+2.*(EK(JK+19)+EK(JK+39))+EK(JK+57))/6
000777      180 CONTINUE
001001          T=T+DELT
001002          GO TO 60
001003      190 CONTINUE
001006          FCAV=0.0
001007          ECAV=0.0
001010          FEAV=0.0
001011          ESYSAV=0.0
001012          DO 300 JC=1, NCCMP

```

C
C
C
C

COMPUTE FUEL AND ENERGY CONSUMPTION ON COMPOSITE DRIVING CYCLE
FOR MODES 1 AND 2.

```

001013      EOBAR(JC)=0.0
001014      FCBAR(JC)=0.0
001015      FCBAR2(JC)=0.0
001016      EOBARF(JC)=0.0
001017      EOBARF2(JC)=0.0
001020      ESBAR(JC)=0.0
001021      ESYSPP(JC)=0.0

```

```

001022      VRECIP=0.0
001023      DO 260 KC=1,NCYCLE
      025      VRECIP=VRECIP+GAMMA(JC,KC)/VAVG(KC)
001033      BOBAR(JC)=BOBAR(JC)+GAMMA(JC,KC)*DEPL(KC)
001040      FGBAR(JC)=FGBAR(JC)+GAMMA(JC,KC)*FCONS(KC)
001045      FGBAR2(JC)=FGBAR2(JC)+GAMMA(JC,KC)*FCONS2(KC)
001053      EGBAR(JC)=EGBAR(JC)+GAMMA(JC,KC)*ECONS(KC)
001060      EGBAR2(JC)=EGBAR2(JC)+GAMMA(JC,KC)*ECONS2(KC)
001066      FHEBAR(JC)=FHEBAR(JC)+GAMMA(JC,KC)*ECHE(KC)
001073      ESYSEB(JC)=ESYSEB(JC)+GAMMA(JC,KC)*ECSYS(KC)
001101      260 CONTINUE
001103      VBAR(JC)=1./VRECIP
001106      SPPWR(JC)=1000.*ECPAR(JC)*VBAR(JC)/WB

      C
      C      CORRECT FUEL CONSUMPTION FOR NON-ZERO ENERGY CONSUMPTION ON MODE
      C
001112      FGBAR2(JC)=(FGBAR2(JC)*EGBAR(JC)-FGBAR(JC)*EGBAR2(JC))/(EGBAR(
      1-EGBAR2(JC))

      C
      C      COMPUTE RANGE FOR NEW BATTERY DISCHARGE LIMIT
      C
001120      RANGE(JC)=DFMAX/BOBAR(JC)

      C
      C      COMPUTE FRACTION OF TOTAL DRIVING DONE ON MODE 1 FOR EACH
      C      COMPOSITE CYCLE.
      C
001123      IF(JC.NE.1)GO TO 265
      025      DLGW=0.
001126      GO TO 265
001126      265 DLGW=DSUP(JC-1)
001130      266 IF(DWARM.LE.DSUP(JC))GO TO 267
001134      RFRAC(JC)=0.
001135      GO TO 280
001135      267 IF(RANGE(JC).GT.DLGW-DWARM)GO TO 270
001143      RFRAC(JC)=RANGE(JC)/DPAF(JC)
001145      GO TO 280
001146      270 IF(RANGE(JC).GT.DSUP(JC)-DWARM)GO TO 275
001154      RFRAC(JC)=(RANGE(JC)/DPAF(JC))*(1.-(RANGE(JC)-DLGW+DWARM)**2/
      1(2.*RANGE(JC)*(DSUP(JC)-DLGW)))
001170      GO TO 280
001171      275 RFRAC(JC)=1.-DWARM/DPAF(JC)
001175      280 CONTINUE

      C
      C      COMPUTE MODE-AVERAGED FUEL AND ENERGY CONSUMPTION FOR COMPOSITE
      C      DRIVING CYCLE.
      C
001175      FCMAY(JC)=RFRAC(JC)*FGBAR(JC)+(1.-RFRAC(JC))*FGBAR2(JC)
001203      ECMAY(JC)=RFRAC(JC)*EGBAR(JC)+(1.-RFRAC(JC))*EGBAR2(JC)

      C
      C      COMPUTE OVERALL FUEL AND ENERGY CONSUMPTION.
      C
      210      FCAV=FCAV+DNC(JC)*FCMAY(JC)
001214      ECAV=ECAV+DNC(JC)*ECMAY(JC)
001217      FHEAV=FHEAV+DNC(JC)*FHEBAR(JC)
001223      ESYSAV=ESYSAV+DNC(JC)*ESYSEB(JC)

```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

HYBRID?

```

001226      FEAV=1000.*FUELSG/FCAV
      231      WPAV=ECAV/CFGEFF
      233      300 CONTINUE
C
001235      WEEF=EHEAV/ESYSAV
C
C      ESTIMATE BATTERY LIFE.
C
001237      DCAV=OBMAX
001241      BLIFE=DSTAV*INT1(DCAV,DCISCH,CYCLES,NDOSCH)
001246      PPRINT 950
001251      PRINT 960,(FCPAR(J),FCPAR2(J),ECPAR(J),RANGE(J),FCMAV(J),ECMAV(
1VBAR(J),SFPWR(J),J=1,NCCMP)
001302      PRINT 970,FCAV,ECAV,BLIFE
001314      PRINT 975,FEAV,WPAV
001324      PRINT 1010,WEEF
001332      194 CONTINUE
001335      200 STOP
C
C      FORMAT STATEMENTS
C
001337      600 FORMAT(I10,6F10.4)
001337      610 FORMAT(7F10.4)
001337      700 FORMAT(1HD,4X,4FTIME,8X,5HSPEED,5X,8HDISTANCE,4X,9HR.L.POWER,3X
18HBR.POWER,3X,10HR.L.ENERGY,3X,9HBR.ENERGY,2X,10HKIN.ENERGY/
21X,2HGN,2X,3HRPM,1X,10HD.T.ENERGY,2X,10HSYS.ENERGY,2X,10HENG.EN
3Y,4X,
1
30TOR SHAFT ENERGY,4X,10HBAT.ENERGY,3X,9HSYS.POWER,3X,9HENG.POWE
45X,17HMOTOR SHAFT POWER)
001337      710 FORMAT(1HD,2E12.4/I2,F6.0,10E12.4/I2,F6.0,4E12.4,12X,4E12.4)
001337      820 FORMAT(1H ,2E16.6)
001337      925 FORMAT(1H1,27HCONTROL PARAMETERS FOR CASE,I2)
001337      930 FORMAT(1HD,5X,20HMIN. ENGINE TORQUE =,E11.4,9H (MODE 1)
1/25X,E11.4,9H (MODE 2)/6X,20HBATT. DISCH. LIMIT =,E11.4
2/6X,21HNOMINAL MOTOR POWER =,E11.4
3/6X,18HTRANSITION SPEED =,E11.4)
001337      950 FORMAT(1HD,47HFUEL AND ENERGY CONSUMPTION ON COMPOSITE CYCLES/3
113HFUEL - MODE 1,3X,13HFUEL - MODE 2,2X,15HENERGY - MODE 1,1X,
214HRANGE - MODE 1,4X,10HFUEL - AV.,5X,12HENERGY - AV.,6X,9HAV.
3FD,5X,13HSP. POWER - 1)
001337      960 FORMAT(1H ,8E16.6)
001337      970 FORMAT(1HD,29HYEARLY AV. FUEL CONSUMPTION =,E16.6/1X,34HYEARLY
1 BATTERY ENERGY OUTPUT =,E16.6/1X,23HEXPECTED BATTERY LIFE =,E:
2)
001337      975 FORMAT(1HD,29HYEARLY AV. FUEL ECONOMY =,E16.6/1X,
129HYEARLY AV. WALL PLUG OUTPUT =,E16.6)
001337      980 FORMAT(1HD,16HCYCLE DISTANCE =,E12.4/1X,23HFUEL CONSUMPTION ON
1E 1 =,E12.4/21X,8HMODE 2 =,E12.4/1X,36HBATT. ENERGY CONSUMPTION
2 MODE 1 =,E12.4/29X,8HMODE 2 =,E12.4)
001337      1010 FORMAT(1HD,29HHEAT ENGINE ENERGY FRACTION =,E16.6)
001337      945 FORMAT(1H ,15HAVERAGE SPEED =,E12.4,1X,19HBATTERY DEPLETION =,
16,1X,21HHEAT ENGINE ON TIME =,E16.6,3H(MODE 1),1X,E16.6,8H(MODE
2)
001337      1000 FORMAT(1HD,4E12.4)
001337      1020 FORMAT(1HD,*BATTERY POWER DISTRIBUTION*,/50X,*NEGATIVE*,1X,*FO:
1VE*,/1X,
*38-34*,1X,*34-30*,1X,*30-25*,1X,*25-22*,1X,*22-19*
21X,*19-14*,1X,*14-10*,2X,*10-0*,7X,*6-2*,3X,*2-0*,2X,

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GOLETA FCRIFAN 1.3 * SEMI-AUTO OFL * (01-10-73)

HYBRID2

3*E-10*,1X,*10-14*,1X,*14-18*,1X,*18-22*,1X,*22-26*,1X,*26-30*,
4*30-34*,1X,*34-38*,1X,*TOTAL*/1(2016))
END

1337

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GOLFETA FCFTCAN 1.3 * SEMI-AUTO PFL * (01-10-73)

SUBROUTINE VFFIC(V,A,T,YDOT,Y,NGEAR,NGEAR2)

C
C
C
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C
CVEHIC COMPUTES POWER REQUIREMENTS AND LOSSES FROM SEAR WHEELS
THROUGH ENGINE

DATA IN COMMON -

000012

COMMON DISPL,RPM(20),TOMAX(20),BMEP(20),BSFC(20,20),NRPM,NMEP,
1EMUM,EMUG,FINNLD,SPMO(20),TMCMAX(20),TMCMIN(20),NSPMO,
2CTCZRO,TSP(20),TOR(20),SFR(20),TSP2(20),MTSP,
3NLCK(5),TRATIO(5),CT1(5),CT2(5),EMUT(5),
4WB,EMAX,EMURG,FMUPG2,
5DRATIO,CD1,CD2,EMUG,RTIRE,CTIRE1,CTIRE2,VMASS,OLI,CCA,
6TEOMIN,DRMAX,RPMIDL,VMASS2,PEOMIN,
7FUFLG,SKALE,THSKL,NTH,NDSCH,CHGFFF,NOYCLE,NOOMP,ESTAV,
8NUNITS,THSET(5),UPSHFT(5),DNShFT(5),DDISCH(20),CYCLES(20),ATC(1
9NPRTC(3),DTC(3),TFC(3),CSUP(30),CNC(30),DBAR(30)
1,RPMEST,PBEST,PEOP(20),RPMEO(20),RPMOPM,EMUCVT,RATUP,RATON,NO
2,PDFNS(20),EDENS(20),ADENS
3,VMAX,TEOMP2,UPSEL,DNSEL,DWARM,NAX,RPMAX(20),TAX(20)
COMMON TIMC(3,200),SPEC(3,200),GAMMA(30,3)

000012

C
C
C

VARIABLES IN COMMON -

000012

COMMON FA,FR,FAC,FNET,TDC,TTC,RPMDO,RPMTC,TSC,RPMSC,RPMTCO,TTC
1RPMTCN,TMC,TEC,TMC2,TEC2,TGC,PSC,PEO,PEO2,FMC,PMC2,PGO,PERK,FC
2PD,PT,PPW,PLTC,THPFC,TTCIN
3,RPMEO,RPMEC2,PLTC2,VMSC
4,TSC2,RPMSC2,FSC2,RPMTCO1,RPMTCO2,RPMEO,RPMEC2

000012

C
C
C
C

REAL YDOT(20),INT1,INT2

COMPUTE SPEEDS AND LOAD-INDEPENDENT LOSSES THROUGH DRIVE TRAIN

000012

VMPS=AMAX1(0.0,V/3.6)

000016

NLCK=NLCK(NGEAR)

000020

NLCK2=NLCK(NGEAR2)

000022

RPMDO=0.5492967*VMPS/RTIRE

000025

RPMTCO=RPMDO*TRATIO ←

000027

RPMSC=RPMTCO*TRATIO(NGEAR)

000031

RPMSC2=RPMTCO*TRATIO(NGEAR2)

000033

TLFD=CD1+CD2*RPMTCO

000036

TLFT=CT1(NGEAR)+CT2(NGEAR)*RPMSC

000042

TLFT2=CT1(NGEAR2)+CT2(NGEAR2)*RPMSC2

C
C
CCOMPUTE ROAD LOAD POWER REQUIREMENTS
AERODYNAMIC -

000046

FA=0.6125*CCA*VMPS**2

000051

PA=FA*VMPS/1000.

000053

YDOT(1)=PA/1000.

C
C
C

ROLLING RESISTANCE -

000054

FR=9.807*VMASS*(CTIRE1+CTIRE2*V)

000061

PR=FR*VMPS/1000.

SOLETA FORTRAN 1.3 * SFMT-AUTO PFL * (01-10-77)

VENTO

```

000063      YDCT(1)=(FA+FF)/1000.
           C
           C      ACCELERATION -
           C
000065      FAC=VMASS2*A
000067      FNET=FA+FP+FAC+FG
000073      TOC=FNET*RTIRE
000075      PRW=0.0001047197*TOC*RFMCO
000077      IF(FNET.LT.0.0)GO TO 200
           C
           C      NON-NEG. NET DRIVING FORCE TO THE WHEELS IS NEEDED
           C      DIFFERENTIAL -
           C
000100      TTO=TOC/(EMUC*DRATIO)+TLFD
           C
           C      TRANSMISSICK -
           C
000103      TSO=TTO/(EMUT(NGEAR)*TRATIO(NGEAR))+TLFT
000110      PSO=TSO*RFMSC*0.0001047197
000112      TSO2=TTO/(EMUT(NGEAR2)*TRATIO(NGEAR2))+TLFT2
000120      PSO2=TSO2*RFMSC2*0.0001047197
           C
           C      IS CAR AT REST AND IDLING -
           C
000122      IF(ABS(VMPS).LT.0.2.AND.APS(A).LT.0.1)GO TO 300
           C
           C      0134
000137      140 CALL PNCVP(1,JPRK,NLCK,NLCK2)
           C
           C      NET DRIVING FORCE AT WHEELS IS NEGATIVE
           C
000143      200 TTO=TOC*EMUC/DRATIO+TLFD
000147      TSO=TTO*EMUT(NGEAR)/TRATIO(NGEAR)+TLFT
000153      PSO=TSO*RFMSC*0.0001047197
000155      TSO2=TTO*EMUT(NGEAR2)/TRATIO(NGEAR2)+TLFT2
000162      PSO2=TSO2*RFMSC2*0.0001047197
000165      NGEAR=NGEAR2
000166      IF(PSO.GE.0.0)GO TO 210
000167      CALL PNCVP(-1,JPRK,NLCK,NLCK2)
000172      IF(JPRK.EQ.0)GO TO 400
           C
           C
000177      PSO=TSO*RFMSC*0.0001047197
000201      PSO2=PSO
000202      TTO=(TSO-TLFT)*TRATIO(NGEAR)/EMUT(NGEAR)
000206      TOC=(TTO-TLFD)*DRATIO/EMUC
000212      GO TO 400
000212      210 CALL PNCVP(1,JPRK,NLCK,NLCK2)
000215      240 GO TO 400
           C
           C      CAR IS AT REST AND IDLING
           C
000221      300 A=0.0
000222      VMPS=0.0
000223      CALL PNCVP(0,JPRK,NLCK)

```

GOLETA FCRTFAN 1.3 * SEMI-AUTO RFL * (01-10-73)

VEHIC

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OF POOR QUALITY000225
0226PSC=0.0
PSC2=0.0C
C
C

COMPUTE ENGINE FUEL RATE AND DERIVATIVES OF VARIABLES

```

000227 400 IF (PEO.NE.0.0) GO TO 410
000234    FC=0.0
000235    GO TO 420
000235 410 BRMEP=125.664*TF0/DISPL
000240    SFC=INT2 (BRMEC, BRMEF, RPM, BRMEF, BSFC, NRPM, AMEP)
000247    FC=SFC*PEO
000251 420 IF (PEO2.NE.0.0) GO TO 430
000256    FC2=0.0
000257    GO TO 440
000257 430 BRMEP2=125.664*TEO2/DISPL
000262    SFC=INT2 (BRMEC2, BRMEF2, RPM, BRMEF, BSFC, NRPM, AMEP)
000271    FC2=SFC*PEO2
000273 440 PD=TTO*RPMDC*0.0001047197
000276    PRK=PRW-PD
000300    PT=TTO*RPMTG*0.0001047197
000302    YDOT (2) = (ABS (FT-PD) + ABS (PSC-PT) + ABS (PLTG)) / 1000.
000320    YDOT (3) = (ABS (FT-PD) + ABS (PSC2-PT) + ABS (PLTG2)) / 1000.
000333    YDOT (4) = ABS (PRK) / 1000.
000335    YDOT (5) = PSC / 1000.
000337    YDOT (6) = PSC2 / 1000.
000340    YDOT (7) = PEO / 1000.
000342    YDOT (8) = PEO2 / 1000.
000344    YDOT (9) = PWC / 1000.
000345    YDOT (10) = PWC2 / 1000.
000347    YDOT (11) = A*3.6
000351    YDOT (12) = VMFS / 1000.
000353    YDOT (13) = FGC / 1000.
000354    YDOT (14) = 0.
000355    IF (PEO.EQ.0.) GO TO 442
000356    YDOT (14) = 1.
000360 442 YDOT (15) = 0.
000361    IF (PEO2.EQ.0.) GO TO 444
000362    YDOT (15) = 1.
000364 444 YDOT (16) = FC / 3600.
000366    YDOT (17) = FC2 / 3600.
000370    YDOT (18) = (PI*NLG + PWC/EMUM + FGC*FMUG*EMURG) / 1000.
000377    YDOT (19) = (PI*NLG2 + PWC2/EMULY + FGC2*EMUG*EMURG2) / 1000.
000406    RETURN
000407    END

```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

SUBROUTINE HYREAD(NCGEAR)

C
C
C
C

HYREAD INPUTS DATA FOR HYRID2

000003

DATA IN COMMON -

COMMON DISFL, RPM(20), TQMAX(20), BMEP(20), BSFC(20,20), NRPM, NMEP,
 1EMUM, EMUG, PINNLD, SPMO(20), THOMAX(20), THOMIN(20), NSFMO,
 2CTCZRO, TSP(20), TOR(20), SFR(20), TSP2(20), NTSP,
 3NLOCK(5), TRATIO(5), CT1(5), CT2(5), EMUT(5),
 4WR, EBMAX, EMURC, EMURG2,
 5DRATIO, CD1, CD2, EMUD, RTIRE, CTIRE1, CTIRE2, VMASS, DLI, CCA,
 6TECMIN, DBMAX, RPMICL, VMASS2, PEOIN,
 7FUELSG, SKALE, TMSKL, NTH, NDCSCH, CHGEFF, NCYCLE, NCCMP, DSTAV,
 8NUNITS, THSFT(5), UPSHFT(5), DNSHFT(5), DDISCH(20), CYCLES(20), NTC(
 9NPRTC(3), DTC(3), TFC(3), DSUP(30), DNC(30), DBAR(30)
 1, RPMEST, PEEST, PEO(20), RPMEO(20), RPMOPM, EMUCVT, RATUP, RATDN, NO
 2, PDENS(20), EDENS(20), NDENS
 3, VMAX, TEOPN2, UPSEL, DNSEL, DWARM, NAX, OPMAX(20), TAX(20)
 COMMON TIME(3,200), SPEC(3,200), GAMMA(30,3)

000003

C
C

VARIABLES IN COMMON -

COMMON FA, FR, FAC, FNET, TDC, TTC, RPMDO, RPMT, TSC, RFMSC, RPMTCO, TTC
 1RPMTCN, TMO, TEC, TMO2, TE02, TGO, PSC, PEO, PEO2, PFC, PFC2, PGC, PERK, FC
 2FD, PT, FPW, PLTC, THPPC, TTCIN
 3, RPHEO, RFPEC2, PLTC2, VMFS
 4, TSC2, RPMSO2, PSC2, RPMTG1, RFMTG2, PRMEP, BRMEP2

000003

C
C
C

INPUT ENGINE DATA

000003

READ 605, NRPM, NMEP, FUELSG, DISPL, SKALE

000021

READ 610, (RPM(J), TQMAX(J), J=1, NRPM), (BMEP(J), J=1, NMEP), ((BSFC(
 1, J=1, NMEP), I=1, NRPM)

000057

READ 600, NCF, RPMEST, PEEST

000071

READ 610, (PEO(J), RPMEO(J), J=1, NOP)

000106

DISPL=DISPL*SKALE

000110

PEEST=PEEST*SKALE

000111

DO 11 J=1, NRPM

000113

TQMAX(J)=SKALE*TQMAX(J)

000115

11 CONTINUE

000117

DO 12 J=1, NCF

000121

PEO(J)=PEO(J)*SKALE

000123

12 CONTINUE

000125

PRINT 600, FUELSG, DISPL

000135

PRINT 805

000141

DO 1 J=1, NRPM

000144

PRINT 910, RPM(J), TQMAX(J), BMEP(1), BSFC(J,1)

000157

PRINT 806, (BMEP(K), BSFC(J,K), K=2, NMEP)

000176

1 CONTINUE

000202

PRINT 307, RPMEST, PEEST

000211

PRINT 910, (PEO(J), RPMEO(J), J=1, NOP)

C
C
C

INPUT MOTOR/GENERATOR DATA

000226

READ 500, NSFMO, EMUM, EMUG, TMSKL, PINNLD, RPMICL, RPMOPM

000250

READ 510, (RPM(J), TQMAX(J), THOMIN(J), J=1, NSFMO)

GOLETA FCSTFAN 1.3 * SEMI-AUTO RFL * (01-10-73)

HYPERAD

```

000267      DO 2 J=1,NSEMC
      0272      TCMAX(J)=TCMAX(J)*TMSKL
      0274      TCMIN(J)=TCMIN(J)*TMSKL
000276      2 CONTINUE
000300      PRINT 911
000303      PRINT 812,FMUP,FMUG,FINNLD,RFMIDL,RPMOPM
000321      PRINT 913
000325      PRINT 914,(SPMC(J),TCMAX(J),TCMIN(J),J=1,NSEMC)

C
000344      READ 600,JCVT
C
C      JCVT=0 FOR TORQUE CONVERTOR, =1 FOR CVT
C

000352      IF(JCVT.EQ.0)GO TO 4
000354      READ 610,EMUCVT,PATUP,RATON
000366      PRINT 808,EMUCVT,PATUP,RATON
000400      GO TO 5
C      INPUT TORQUE CONVERTOR DATA
C

000402      4 READ 620,NTSP
000410      READ 610,CTCZFC,(TSP(J),TOR(J),SPR(J),J=1,NTSP)
000431      PRINT 860
000435      PRINT 865,CTCZFC
000443      PRINT 870
000447      PRINT 814,(TSP(J),TOR(J),SPR(J),J=1,NTSP)
000466      DO 3 J=1,NTSP
      3471      TSP2(J)=TSP(J)*SORT(TOR(J))
000477      3 CONTINUE
C
C      INPUT TRANSMISSION DATA
C

000502      5 READ 605,NGEAR,NTH,UPSEL,ONSSEL
000516      READ 601,(NLCK(J),TRATIO(J),CT1(J),CT2(J),EMUT(J),J=1,NGEAR)
000547      READ 610,(THSET(J),UPSHFT(J),ONSHFT(J),J=1,NTH)
000566      PRINT 840
000572      PRINT 841
000576      PRINT 842,(NLCK(J),TRATIO(J),CT1(J),CT2(J),EMUT(J),J=1,NGEAR)
000627      PRINT 844,UPSEL,ONSSEL
000637      PRINT 843
000643      PRINT 814,(THSET(J),UPSHFT(J),ONSHFT(J),J=1,NTH)
C
C      INPUT PATTERN DATA
C

000662      READ 605,NODSCH,NOENS,WE,EMAX,EMURG,EMURG2,CHGEFF
000704      READ 610,(ODSCH(J),CYCLES(J),J=1,NODSCH)
000721      READ 610,(EDENS(J),ECENS(J),J=1,NOENS)
000736      PRINT 850
000742      PRINT 855
000746      PRINT 815,WE,EMAX,EMURG,EMURG2,CHGEFF
000764      PRINT 980
      1770      PRINT 910,(ODSCH(J),CYCLES(J),J=1,NODSCH)
      1005      PRINT 925
001011      PRINT 910,(EDENS(J),ECENS(J),J=1,NOENS)
C
C      INPUT DIFFERENTIAL AND TIRE DATA

```

GCLETA FCPTFA 1.3 * SEMI-AUTO PFL * (01-10-73)

HYREAD

```

C
001026 READ 510,CRATIC,CC1,CC2,EMUD,RTIRE,CTIRE1,CTIRE2
.050 PRINT 875
001054 PRINT 885,CRATIC,CC1,CC2,EMUD,RTIRE,CTIRE1,CTIRE2

C
C INPUT ACCESSORY DATA
C
001076 READ 500,NAX
001104 READ 610,(PFMAX(J),TAX(J),J=1,NAX)
001121 PRINT 1000
001125 PRINT 910,(PFMAX(J),TAX(J),J=1,NAX)

C
C INPUT VEHICLE DATA
C
001142 READ 610,VMASS,DLI,CCA
001154 PRINT 890,VMASS,DLI,CCA
001166 VMASS2=VMASS+DLI/RTIRE**2

C
C INPUT DRIVING CYCLE DATA
C
001172 READ 620,NCYCLE
001177 PRINT 915
001203 DO 45 JC=1,NCYCLE
001206 READ 625,NTC(JC),NPRTC(JC),NUNITS,DTC(JC),TFC(JC)
001223 NT=NTC(JC)
001225 READ 610,(TIME(JC,J),SPEC(JC,J),J=1,NT)
245 IF(NUNITS.NE.1)GO TO 41

C
C CONVERT MPH TO KILOMETERS PER HOUR
C
001250 30 DO 40 J=1,NT
001252 SPEC(JC,J)=SPEC(JC,J)*1.6093
001255 40 CONTINUE
001257 41 PRINT 920
001263 PRINT 910,(TIME(JC,J),SPEC(JC,J),J=1,NT)
001303 45 CONTINUE
001307 READ 600,NCCMP,DSTAV,DWARM
001320 PRINT 990,DSTAV
001326 PRINT 995
001332 DO 320 JC=1,NCCMP
001335 READ 610,DSUF(JC),DNC(JC),(GAMMA(JC,J),J=1,NCYCLE)
001354 PRINT 915,DSUF(JC),DNC(JC),(GAMMA(JC,J),J=1,NCYCLE)
001374 320 CONTINUE
001400 PRINT 991,DWARM
001405 DBAR(1)=DSUF(1)/2.
001407 DO 46 J=2,NCCMP
001412 DBAR(J)=(DSUF(J)+DSUF(J-1))/2.
001416 46 CONTINUE
001420 RETURN

C
C FORMAT STATEMENTS
C
001420 500 FORMAT(I10,EF10.4)
001420 601 FORMAT(I10,4F10.4)
001420 605 FORMAT(2I10,5F10.4)

```

PAGE IS
 FOR QUALITY

GOLETA FCRTFA) 1.3 * SEMI-AUTO PFL * (01-10-77)

HYREAD

```

001420      F10 FORMAT(7F10.4)
001420      F20 FORMAT(7I10)
      420      E25 FORMAT(3I10,2F10.4)
001420      E00 FORMAT(1H0,11HENGINE DATA/1X,23HFUEL SPECIFIC GRAVITY =,E12.4/
      11X,14HDISPLACEMENT =,E12.4)
001420      E05 FORMAT(1H0,7X,3HRPM,9X,11HMAX. TORQUE,8X,4HMEMEP,12X,4HBSFC)
001420      E06 FORMAT(1H ,32X,2E16.6)
001420      E07 FORMAT(1H0,20HBEST OPERATING POINT - SPEED =,E12.4,6X,7HPOWER =
      1E12.4//6X,5HPOWER,8X,10HCPT. SPEED)
001420      E08 FORMAT(1H0,19HCVT CHARACTERISTICS//1X,12HEFFICIENCY =,E12.4,4X,
      11HPSPEEDUP RATIO =,E12.4,4X,16HLOWDOWN RATIO =,E12.4)
001420      E10 FORMAT(1H ,4E16.6)
001420      E11 FORMAT(1H0,20HNOTOP/GENERATOR DATA)
001420      E12 FORMAT(1H0,13HEFF.(MOTOR) =,E12.4,6X,12HEFF.(GEN.) =,E12.4,6X,
      12HNO LOAD INPUT POWER =,E12.4,6X,12HIDLE SPEED =,E12.4/1X,22H
      2 OPERATING SPEED =,E12.4)
001420      E13 FORMAT(1H0,7X,3HRPM,9X,11HMAX. TORQUE,5X,11HMIN. TORQUE)
001420      E14 FORMAT(1H ,3E16.6)
001420      E15 FORMAT(1H ,5E16.6)
001420      E40 FORMAT(1H0,12HGEARBOX DATA)
001420      P41 FORMAT(1H0,5X,7HLOCKUP-,10X,5HRATIO,10X,22HSPIN LOSS COEFFICIENT
      19X,11HTORQUE EFF.)
001420      E42 FORMAT(1H ,18,8X,4E16.6)
001420      E43 FORMAT(1H0,4X,10HENG. POWER,5X,11HUPSHIFT RPM,4X,13HDOWNSHIFT R
001420      P44 FORMAT(1H0,37HSHIFT POINTS FOR ELECTRIC OPERATION -,2E12.4)
001420      E50 FORMAT(1H0,12HBATTERY DATA)
      420      E55 FORMAT(1H0,8X,4HMASS,7X,14HENERGY DENSITY,2X,15HAV. REGEN. EFF.
      11X,15HMAX REGEN. EFF.,2X,13HRECHARGE EFF.)
001420      E60 FORMAT(1H0,21HTORQUE CONVERTOR DATA)
001420      E65 FORMAT(1H0,17HNI**2/TT(STALL) =,E16.6)
001420      E70 FORMAT(1H0,3X,11HNO/SQRT(TO),8X,5HTO/TT,11X,5HNO/NI)
001420      E75 FORMAT(1H0,12HAXLE AND TIRE DATA)
001420      E85 FORMAT(1H0,17HCTFF. RATIO =,E16.6/1X,24HSPIN LOSS COEFFICIENTS
      12E16.6/1X,13HTORQUE EFF. =,E16.6/1X,16HROLLING RADIUS =,E16.6/
      21X,33HROLLING RESISTANCE COEFFICIENTS =,2E16.6)
001420      P90 FORMAT(1H0,14HVEHICLE MASS =,E16.6,5X,19HORIVELINE INERTIA =,E
      1,5X,19H(DFAG COEF.)*AREA =,E16.6)
001420      C910 FORMAT(1H ,2E16.6)
001420      C915 FORMAT(1H0,14HDEFIVING CYCLES)
001420      C920 FORMAT(1H0,6X,4HTIME,12X,5HSPEED)
001420      C925 FORMAT(1H0,1X,14HSPECIFIC POWER,2X,15HSPECIFIC ENERGY)
001420      C980 FORMAT(1H0,1X,15HDEPTH OF DISCH.,6X,10HCYCLE LIFE)
001420      C990 FORMAT(1H0,24HTRAVEL DISTRIBUTION DATA/1X,11HAV. USAGE =,E12.4
001420      C991 FORMAT(1H0,*WARMUP DISTANCE =*,E12.4)
001420      C995 FORMAT(1H0,3X,10HMAX. DIST.,4X,15HFRACT. OF TCTAL,14X,21HORIVI
      1CYCLE WEIGHTS)
001420      1000 FORMAT(1H0,14HACCESSORY LOAD/6X,7HSPEED,11X,6HTORQUE)
001420      END

```


GOLETA FCFTFA 1.3 * SEMI-AUTO PFL * (01-10-73)

```

SUBROUTINE GCSHFT(IFLAG,JGEAR,JGFAR2,NGEAR)
C
DATA IN COMMON -
.0007 COMMON DISPL,PPM(20),TCMAX(20),PYEP(20),BSFC(20,20),NRPM,NMEP,
1EMUM,EMUG,FINALT,SFMC(20),TMCMAX(20),THOMIN(20),NSFMO,
2CTCZFO,TSP(20),TQP(20),SFR(20),TSP2(20),NTSP,
3NLCCK(5),TRATIO(5),CT1(5),CT2(5),EMUT(5),
4WB,EBMAX,EMURG,EMURG2,
5DRATIO,CD1,CD2,FMUD,RTIFE,CTIRE1,CTIRE2,VMASS,DLI,CCA,
6TEOMIN,OBMAX,RPMIDL,VMASS2,PEOMIN,
7FUELSG,SCALE,TMEXL,NTH,NDCSCH,CHGEFF,NCYCLE,NCCMP,OSTAV,
8NUNITS,THSET(5),UPSHFT(5),DNSHFT(5),DDISCH(20),CYCLES(20),NTC(
9NPRTC(3),PTC(3),TFC(3),CSUP(30),CNC(30),DBAR(30)
1,RPMBST,PREST,PEOP(20),RPMEOF(20),RPMOPM,EMUCVT,RATUP,RATDN,NO
2,PDENS(20),EDENS(20),NDENS
3,VMAX,TEOM2,UPSEL,DNSEL,CHAPM,NAX,PPMAX(20),TAX(20)
000007 COMMON TIMC(3,200),SPECC(3,200),GAMMA(30,3)
C
C VARIABLES IN COMMON -
000007 COMMON FA,FR,FAC,FNET,TCC,TTC,RPMD0,RPMT0,TS0,RPMS0,RPMT00,TTC
1RPMT0N,TMC,TEC,TM02,TE02,TG0,PSC,PE0,PE02,PMC,PM02,PG0,PERK,FC
2PD,PT,PRW,PLTC,THRPD,TTCIN
3,RPME0,RPME02,PLTC2,VMPS
4,TS02,RPMS02,PSC2,RPMT01,RPMT02,RRMEF,RRMEP2
000007 REAL INT1
C
000007 IF(PE0.GT.0.0)GO TO 5
C
C MODE 1 SHIFT DETERMINED BY MOTOR/GEN. CHARACTERISTICS
C
000011 SHFTUP=UPSEL
000012 SHFTDN=DNSEL
000013 GO TO 10
C
C MODE 1 SHIFT DETERMINED BY HEAT ENGINE CHARACTERISTICS
C
000014 5 SHFTUP=INT1(PE0,THSET,UPSHFT,NTH)
000020 SHFTDN=INT1(PE0,THSET,DNSHFT,NTH)
000024 10 IF(PE02.GT.0.0)GO TO 15
C
C MODE 2 SHIFT DETERMINED BY MOTOR/GEN. CHARACTERISTICS
C
000031 SHFTUP2=UPSEL
000032 SHFTDN2=DNSEL
000033 GO TO 20
C
C MODE 2 SHIFT DETERMINED BY HEAT ENGINE CHARACTERISTICS
C
000034 15 SHFTUP2=INT1(PE02,THSET,UPSHFT,NTH)
000040 SHFTDN2=INT1(PE02,THSET,DNSHFT,NTH)
000044 20 IF(RPMT01.GE.SHFTUP.AND.JGEAR.LT.NGEAR)GO TO 25
000044 1060 IF(RPMT01.LE.SHFTDN.AND.JGEAR.GT.1)GO TO 30
000044 1072 IFLAG=0
000072 GO TO 40
000073 20 JGEAR=JGFAR+1
000075 IFLAG=1

```

GOLETS FCPTFAN 1.3 * SEMI-AUTO PFL * (01-10-73)

GRSFT

```
000075      GO TO 40
000076      30 JGEAR=JGEAR-1
      100      IFLAG=1
000100      40 IF(RPMT02.GE.SHFUP2.AND.JGEAR2.LT.NGEAR)GO TO 45
000112      IF(RPMT02.LE.SHF0N2.AND.JGEAR2.GT.1)GO TO 50
000124      GO TO 100
000124      45 JGEAR2=JGEAR2+1
000126      IFLAG=1
000126      GO TO 100
000127      50 JGEAR2=JGEAR2-1
000131      IFLAG=1
000131      100 RETURN
000132      END
```

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OF POOR QUALITY

GOLFTA FCFTFAN 1.3 * SEMI-AUTC 9FL * (01-10-73)

```

) 0007      SUBROUTINE FMCVF (NCRV, JBRK, NLCK, NLCK2)
          COMMON DISFL, RPM(20), TCMAX(20), PMP(20), BSFC(20,20), NRPM, NMP,
          1EMUM, FMUG, FIANLC, SPMC(20), TCMAX(20), TCMIN(20), NSPMO,
          2CTCZFO, TSP(20), TOP(20), SFR(20), TSP2(20), NTSP,
          3NLCK(5), TRATIO(5), CT1(5), CT2(5), EMUT(5),
          4WR, EBMX, FMURG, FMURG2,
          5RATIO, CD1, CD2, FMUD, RTIRE, CTIRE1, CTIRE2, VMAS, DLI, CDA,
          6TECMIN, DBMAX, FPMIDL, VMAS2, PEOMIN,
          7FUELSG, SKALE, TMSKL, NTH, NDCSCH, CHGEFF, NCYCLE, NCCMP, CSTAV,
          8NUNITS, THSET(5), UPSHFT(5), DNSHFT(5), DDISCH(20), CYCLES(20), NTC(
          9NPRTC(3), CTC(3), TFC(3), CSUP(30), CNC(30), DBAP(30)
          1, RPMST, PPEST, FECP(20), FMECF(20), RPMOPM, EMUCVT, RATUP, RATON, NO
          2, PDENS(20), EDENS(20), NDENS
          3, VMAX, TEOMN2, UPSEL, DNSEL, DWARM, NAX, RPMAX(20), TAX(20)
000007      COMMON TIMC(3,200), SPEDC(3,200), GAMMA(30,3)
000007      COMMON FA, FR, FAC, FNFT, TCC, TTC, RPMDO, RPMTC, TSC, RPMSC, RPMTCO, TTC
          1RPMTCN, TMO, TEC, TMO2, TEC2, TGC, PSC, PEO, PEO2, PMC, PMC2, PGC, PERK, FC
          2PD, PT, PPW, FLTC, THRPD, TTCIN
          3, RPMEO, RPMEO2, PLTC2, VMFS
          4, TSO2, PPMSC2, FSC2, RPMTC1, RPMTC2, PRMEP, BRMEP2
000007      REAL INT1, INT2
000007      CC=0.0001047197
000010      IF(NCRV)50,80,10

```

C
C
C

SYSTEM POWER OUTPUT IS NON-NEGATIVE

```

0011      10 PBRK=0.0
000012      TGC=0.0
000013      JBRK=0
000013      TTCO=TSC
000015      RPMTCO=RPMSC
000016      CALL TOCOM(1,1,NLCK)
000020      TACC=INT1(RPMTCN, RPMAX, TAX, NAX)
000024      TTCIN=TTCIN+TACC
000025      RPMTC1=RPMTCN
000027      TTCN1=TTCIN
000030      THEMAX=INT1(RPMTCN, RPM, TCMAX, NRPM)
000034      TMMAX=INT1(RPMTCN, SPMC, TCMAX, NSPMO)
000040      PEMAX=CC*THEMAX*RPMTCN
000042      PMMAX=CC*TMMAX*RPMTCN
000044      PCOM=CC*TTCIN*RPMTCN
000046      PEMIN=CC*TECMIN*RPMTCN
000050      PNCM=AMIN1(FECMIN, PMMAX)

```

C
C
C
C
C
C

IS POWER REQUIRED MORE THAN NOMINAL MOTOR RATING

```

000054      IF(PCOM.GT.PNCM.OR.VMFS.GT.VMAX)GO TO 15

```

NO - TRACTION MOTOR HANDLES EVERYTHING

```

0070      TEQ=0.0
0071      RPMEC=0.0
000072      TMC=TTCIN
000073      GO TO 30

```

C

GOLETA FORTFAN 1.3 * SEMI-AUTO PFL * (01-10-73)

P4CV8

```

C      YES - HEAT ENGINE CUTS IN
C
0074      15 RPMSC=RPMTCC
000076      17 IF(PCOM.GT.PHEMIN+PMMAX)GO TO 20
000103      TEC=AMIN1(TTCIN,TECMIN)
000106      TMC=TTCIN-TEC
000110      GO TO 30
C
C      YES - TRACTION MOTOR AT MAX, HEAT ENGINE PICKS UP REMAINDER
C
000110      20 TEC=TTCIN-THMAX
000112      TMC=THMAX
C
C      MODE 2 CALCULATIONS
C
000113      30 TTCO=TSO2
000115      RPMTCO=RPMSCO?
000116      CALL TCCO(1,1,NLCK2)
000121      TACC=INT1(RPMTCC,RPMAX,TAX,NAX)
000125      TTCIN=TTCIN+TACC
000126      RPMTCC=RPMTCC
000130      TTCIN2=TTCIN
000131      THMAX=INT1(RPMTCC,RPMTCC,TOMAX,NRPMT)
000135      THMAX=INT1(RPMTCC,SPMC,THCMAX,NSPMO)
000141      PHEMAX=CC*THMAX*RPMTCC
000143      PMMAX=CC*THMAX*RPMTCC
00145      PCOM=CC*TTCIN*RPMTCC
000147      PHEMIN=CC*TECMIN*RPMTCC
000151      IF(PCOM.GT.PHEMIN)GO TO 40
000157      TEC2=0.0
000157      RPMSC2=0.0
000160      THO2=TTCIN
000162      GO TO 100
000162      40 RPMSC2=RPMTCC
000164      TEC2=AMIN1(THMAX,TTCIN)
000167      THO2=TTCIN-TEC2
000171      GO TO 100
C
C      SYSTEM POWER OUTPUT IS NEGATIVE
C
000171      50 TEC=0.0
000172      TEC2=0.0
000173      TMC=0.0
000174      THO2=0.0
000175      RPMSC=0.0
000176      RPMSC2=0.0
000177      RPMTCC=RPMTCC
000200      RPMTCC=RPMTCC
000201      DO 60 J=1,10
000203      THMIN=INT1(RPMTCC,SPMO,THCMIN,NSPMO)
000207      TACC=INT1(RPMTCC,RPMAX,TAX,NAX)
00213      TTCIN=THMIN-TACC
000215      CALL TCCO(-1,1,NLCK)
000221      IF(ABS(RPMTCC-RPMTCC).LE.5.0)GO TO 65
000230      RPMTCC=RPMTCC

```

GOLETA FCRTPLAN 1.3 * SEMJ-AUTO PFL * (01-10-73)

```

000231      60 CONTINUE
000233      65 IF (TTCC.GT.TSC)GO TO 70
000237      TTCC=TSO
000237      TSO2=TSO
000240      CALL TQCON(1,1,NLCK)
000242      TACC=INT1(RPMTCN,RPMAX,TAX,NAX)
000246      TTCIN=TTCIN+TACC
000247      TGC=TTCIN
000250      RPMT01=RPMTCN
000252      RPMT02=RPMTCN
000253      TTCN1=TTCIN
000254      TTCN2=TTCIN
000255      GO TO 100
000260      70 TSC=TTCC
000262      TSO2=TTCC
000263      TTCN1=TMMIN
000264      TTCN2=TMMIN
000265      TGC=TMMIN
000266      RPMT01=RPMTCN
000267      RPMT02=RPMTCN
000270      JBRK=1
000271      GO TO 100

C
C
C
000271      80 PBRK=0.0
000272      PGO=0.0
000273      TEC=0.0
000274      TEC2=0.0
000275      TTCC=0.0
000276      RPME0=0.0
000277      RPME02=0.0
000300      RPMT00=RPMSC
000301      CALL TQCON(1,0,NLCK)
000303      TACC=INT1(RPMTCN,RPMAX,TAX,NAX)
000307      TTCIN=TTCIN+TACC
000310      TMC=TTCIN
000311      TMC2=TTCIN
000312      RPMT01=RPMTCN
000314      RPMT02=RPMTCN
000315      TTCN1=TTCIN
000316      TTCN2=TTCIN
000317      JBRK=0
000322      100 PEO=CC*TEC*RPME0
000325      PEO2=CC*TEC2*RPME02
000327      PMC=CC*TMC*RPMT01
000332      PMC2=CC*TMC2*RPMT02
000334      PGO=CC*TGC*RPMT01
000337      PLTC=CC*APS(TTCN1*RPMT01-TSC*RPMS0)
000344      PLTC2=CC*APS(TTCN2*RPMT02-TSC2*RPMS02)
000351      RETURN
000351      END

```

GOLETA SCFTCAN 1.7 * SEMI-AUTO RFL * (01-10-77)

```

SUBROUTINE TORQCN (JEND, JSTOP, MLOCK)
COMMON DISPL, RPM (20), TORMAX (20), BMEP (20), PSFC (20, 20), NRRPM, NMEF,
1EMUM, EMUG, FINNLD, SPMO (20), TMCMAX (20), TMOVIN (20), NSFCO,
2CTCZRO, TSP (20), TOR (20), SFR (20), TSP2 (20), NTSP,
3MLCCK (5), TRATIO (5), CT1 (5), CT2 (5), EMUT (5),
4WB, EBMAX, EMURG, EMURG2,
5DRATIO, CD1, CD2, EMUD, RTIRF, CTIRE1, CTIRE2, VMAS, DLI, COA,
6TECHIN, DBMAX, RPMIDL, VMAS2, PECHIN,
7FUELSG, SKALE, TMSKL, NTH, NDCSCH, CHGEFF, NCYCLE, NCCMP, DSTAV,
8NUNITS, THSET (5), UPSHFT (5), DNSHFT (5), DDTSCH (20), CYCLES (20), NTC (
9NPRTC (3), CTC (3), TFC (3), CSUP (30), DNC (30), DPAR (30)
1, RPBST, PBEST, FEOP (20), RFMECF (20), RPMOPM, EMUCVT, RATUP, RATDN, NO
2, PDENS (20), EDENS (20), NDENS
3, VMAX, TEOMN2, UPSEL, DNSEL, DWARM, NAX, RPFMAX (20), TAX (20)
000006 COMMON TIMC (3, 200), SPEEDC (3, 200), GAMMA (30, 3)
000006 COMMON FA, FF, FAC, FNET, TCC, TTC, RPMDO, RPMTC, TSO, RPFSC, RPMTCO, TTC
1RPMTCN, TMC, TEC, TMO2, TEO2, TCO, PSC, PEO, FEO2, FMC, PMC2, PGO, PERK, FC
2PD, PT, PRW, PLTC, THRPC, TTCIN
3, RPFEO, RPFEC2, PLTC2, VMPS
4, TSO2, RPFSC2, PSC2, RPMTC1, RPMTC2, PRMEF, BRMEF2
000006 PEAL INT1, INT2
000006 IF (JSTOP.NE.0) GO TO 5
000007 RPMTCN=RPMIDL
000010 TTCIN=RPMIDL**2/CTCZRO
000012 GO TO 100
000012 5 IF (JEND.EQ.-1) GO TO 50
C
C HAVE OUTPUT SPEED AND OUTPUT TORQUE.
C
000014 IF (MLOCK.EQ.0) GO TO 7
000015 TTCIN=TTC
000016 RPMTCN=RPMTC
000020 GO TO 100
000020 7 IF (TTCO.NE.0.0) GO TO 10
000021 TTCIN=0.0
000022 RPMTCN=RPMTC
000024 GO TO 100
000024 10 TSPAR=RPMTCO/SIGN(SQRT(ABS(TTCO)), TTCO)
000035 IF (TSPAR.EQ.0.0) GO TO 20
000040 TTCIN=TTCO
000041 SPRAT=1.0/INT1(ABS(TSPAR), TSP, SPP, NTSP)
000047 GO TO 40
000051 20 IF (TSPAR.GT.0.0) GO TO 25
000054 IF (TTCO.GT.0.0) GO TO 25
000056 RPMTCN=RPMIDL
000057 TTCIN=RPMIDL**2/CTCZRO
000061 TTCO=TOR(1)*TTCIN
000062 GO TO 100
000063 22 TTCIN=TTCO/TCF(1)
000065 RPMTCN=SQRT(TTCIN*CTCZRO)
000071 GO TO 100
000073 25 TORAT=INT1(TSPAR, TSP, TOR, NTSP)
000077 TTCIN=TTCO/TORAT
000100 30 SPRAT=INT1(TSPAR, TSP, SPP, NTSP)
000104 40 RPMTCN=RPMTCO/SPRAT

```

GOLETA FCRTFAN 1.3 * SEMI-AUTO PFL * (01-10-73)

TQCCN

```

000106          GO TO 100
      C
      C          HAVE OUTPUT SPEED AND INPUT TORQUE
      C
000111          50 IF (NLCK.EC.0) GO TO 55
000112          TTCO=TTCIN
000114          RPMTCN=RPMTCC
000115          GO TO 100
000116          55 IF (TTCIN.NE.0.0) GO TO 60
000117          TTCO=0.0
000120          RPMTCN=AMAX1 (RPMIDL,RPMTCC)
000124          GO TO 100
000125          60 TSPAR2=RPMTCC/SIGN (SQRT (ABS (TTCIN)),TTCIN)
000136          IF (TSPAR2.GE.0.0) GO TO 70
000141          TTCO=TTCIN
000142          SPRAT=1.0/INT1 (ABS (TSPAR2),TSP2,SPR,NTSP)
000150          GO TO 30
000152          70 IF (TSPAR2.GT.0.0) GO TO 75
000155          IF (TTCIN.GT.0.0) GO TO 72
000157          RPMTCN=RPMTCL
000160          TTCIN=RPMTCL**2/CTCZRC
000161          TTCO=TGR (1)*TTCIN
000163          GO TO 100
000163          72 TTCO=TTCIN*TGR (1)
000165          RPMTCN=SQRT (TTCIN*CTCZRC)
000171          GO TO 100
      173          75 TORAT=INT1 (TSPAR2,TSP2,TGR,NTSP)
000177          TTCO=TTCIN*TORAT
000200          80 SPRAT=INT1 (TSPAR2,TSP2,SPR,NTSP)
000204          90 RPMTCN=RPMTCC/SPRAT
000206          100 RPMTCN=AMAX1 (RPMIDL,RPMTCN)
000212          RETURN
000212          END

```

000111
 000112
 000114
 000115
 000116
 000117
 000120
 000124
 000125
 000136
 000141
 000142
 000150
 000152
 000155
 000157
 000160
 000161
 000163
 000163
 000165
 000171
 173
 000177
 000200
 000204
 000206
 000212
 000212

GOLETA FORTRAN 1.3 * SEMI-AUTO PFL * (01-10-73)

SUBROUTINE FILTER(NP,DTP,DTFLTR,P)

```

C
C
000007      REAL P(2800)
000007      TFP=FLCAT(NP)*DTP
000010      JDT=IFIX((DTFLTR+0.001)/DTP)
000013      JLAST=NP+JDT
000015      DO 3 J=1,NP
000016      P(NP+JDT+1-J)=P(NP+1-J)
000022      3 CONTINUE
000024      DO 5 J=1,JDT
000025      P(J)=P(JLAST+J-JDT)
000031      P(JLAST+J)=P(JDT+J)
000035      5 CONTINUE
000037      NINTM=2*JDT-1
000040      NINT=2*JDT
000042      DO 20 JP=1,NP
000043      PTEMP=P(JP)+P(JP+NINT)
000050      DO 10 K=1,NINTM
000051      PTEMP=PTEMP+(3.+(-1.)**(K-1))*P(JP+K)
000062      10 CONTINUE
000065      P(JP)=PTEMP*DTP/(6.*DTFLTR)
000071      20 CONTINUE
000073      RETURN
000073      END

```

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GOLETA FCSTFAN 1.3 * SEMI-AUTO PFL * (G1-10-73)

```
000007      REAL FUNCTION INT1(FX,X,Y,NX)
000008      REAL X(200),Y(200)
000009      IF(EY.GE.X(1))GO TO 5
000010      JRT=7
000011      GO TO 20
000012      5 DO 10 J=1,NX
000013      IF(EX.LT.X(J))GO TO 15
000014      10 CONTINUE
000015      15 JRT=J
000016      20 INT1=Y(JRT-1)+(EX-X(JRT-1))*(Y(JRT)-Y(JRT-1))/(X(JRT)-X(JRT-1))
000017      RETURN
000018      END
```

GCLETA FCPTAN 1.3 * SEMI-AUTO SFL * (01-10-73)

REAL FUNCTION INT2(EX,WHY,X,Y,Z,NX,NY)

C
C
C
C

INT2 INTERPOLATES IN TWO VARIABLES INTERPOLATION SURFACE IS A RULED SURFACE.

```

000012 REAL X(20),Y(20),Z(20,20)
000012 IF (EX.GE.X(1))GO TO 5
000014 JLEFT=1
000015 GO TO 20
000016 5 DO 10 J=1,NX
000020 IF (EX.LT.X(J))GO TO 15
000023 10 CONTINUE
000025 15 JLEFT=J-1
000027 20 IF (WHY.GE.Y(1))GO TO 25
000032 JBOTM=1
000033 GO TO 40
000033 25 DO 30 J=1,NY
000035 IF (WHY.LT.Y(J))GO TO 35
000040 30 CONTINUE
000043 35 JBOTM=J-1
000045 40 RX=(EX-X(JLEFT))/(X(JLEFT+1)-X(JLEFT))
000052 RY=(WHY-Y(JBOTM))/(Y(JBOTM+1)-Y(JBOTM))
000056 RXRY=RX*RY
000060 W1=1.-RX-RY+FXRY
000063 W2=RY-PXRY
000065 W3=PXRY
000067 W4=PX-PXPY
INT2=W1*Z(JLEFT,JBOTM)+W2*Z(JLEFT,JBOTM+1)+W3*Z(JLEFT+1,JBOTM+
1+W4*Z(JLEFT+1,JBOTM)
000110 RETURN
000110 END

```


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4.640000E+03 9.800000E+01
 5.220000E+03 9.400000E+01
 5.800000E+03 8.800000E+01

BEST OPERATING POINT - SPEED = 3.5000E+03 POWER = 2.6800E+01

POWER OPT. SPEED
 1.070000E+01 1.500000E+03
 1.170000E+01 1.750000E+03
 1.690000E+01 2.500000E+03
 2.680000E+01 3.500000E+03
 3.440000E+01 4.500000E+03
 3.580000E+01 5.000000E+03
 3.600000E+01 6.000000E+03

MOTOR/GENERATOR DATA

EFF. (MOTOR) = 8.5000E-01 EFF. (GEN.) = 8.5000E-01 NO LOAD INPUT POWER = 1.0000E+00 IDLE SPEED = 2.0000E+02
 BEST OPERATING SPEED = 3.5000E+03

DPH	MAX. TORQUE	%IN. TORQUE
0.	6.251000E+01	0.
2.040000E+03	6.251000E+01	0.
2.050000E+03	1.250200E+02	0.
2.470000E+03	1.071600E+02	0.
1.100000E+03	8.260250E+01	-1.339500E+02
3.520000E+03	7.277950E+01	-1.339500E+02
4.000000E+03	6.386950E+01	-1.178760E+02
4.900000E+03	5.224500E+01	-9.544400E+01
5.270000E+03	4.465000E+01	-8.930000E+01
6.000000E+03	3.572000E+01	-6.427600E+01

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TORQUE CONVERTOR DATA

MI*2/TI(STALL) = 1.917000E+04

MO/SORT(TOI)	TO/TI	MO/MI
0.	2.100000E+00	0.
1.	1.393000E+01	1.000000E-01
2.	2.040000E+00	2.000000E-01
3.	1.920000E+01	3.000000E-01
4.	3.320000E+01	4.000000E-01
5.	8.980000E+01	5.000000E-01
6.	1.700000E+00	6.000000E-01
7.	7.100000E+01	7.000000E-01
8.	9.641000E+01	8.000000E-01
9.	1.100000E+02	9.000000E-01
10.	1.467000E+02	1.000000E+00
11.	1.899000E+02	1.000000E+00
12.	2.592000E+02	1.000000E+00
13.	4.109000E+02	1.000000E+00
14.	1.214000E+03	1.000000E+00

GEARBOX DATA

LOCKUP-	RATIO	SPIN LOSS COEFFICIENTS	TORQUE EFF.
0	2.450000E+00	0.	9.200000E-01
1	1.450000E+00	0.	9.200000E-01
1	1.000000E+00	0.	9.400000E-01
1	7.500000E-01	0.	9.400000E-01

SHIFT POINTS FOR ELECTRIC OPERATION = 4.5000E+03 2.4000E+03

ENG. POWER

UPSHIFT RPM	DOWNSHIFT RPM
0.	2.500000E+03
1.	1.000000E+01
2.	2.500000E+03
3.	1.300000E+03
4.	5.100000E+03
5.	1.000000E+03
6.	6.000000E+03
7.	3.500000E+03
8.	5.000000E+03
9.	3.500000E+03
10.	5.500000E+03

BATTERY DATA

MASS	ENERGY DENSITY	AV. REGEN. EFF.	MAX REGEN. EFF.	RECHARGE EFF.
2.700000E+02	4.000000E+01	7.000000E-01	9.000000E-01	5.400000E-01

DEPTH OF DISCH.

CYCLE LIFE
2.000000E-01
4.000000E-01
3.300000E+03
5.000000E-01
2.700000E+03
6.000000E-01
2.250000E+03
7.000000E-01
1.800000E+03
1.000000E-01
1.500000E+03
3.000000E-01
1.250000E+03
1.000000E+00
1.000000E+03

SPECIFIC POWER

SPECIFIC ENERGY
2.
4.600000E+01
1.500000E+02
0.

AXLE AND TYPE DATA

DIFF. RATIO = 5.120000E+00
SPIN LOSS COEFFICIENTS = 1.
TOPQUE EFF. = 9.600000E-01
ROLLING RADIUS = 3.050000E-01
0.

ROLLING RESISTANCE COEFFICIENTS = 1.00000E-02 0.

ACCESSORY LOAD

SPEED TORQUE

0. 0.
6.000000E+03 1.000000E+01

VEHICLE MASS = 2.118000E+03 DRIVELINE INERTIA = 6.600000E+00 (DRAG COEF.) * AREA = 6.720000E-01

DRIVING CYCLES

TIME SPEED

0.	0.
1.000000E+00	0.000000E+00
3.900000E+00	1.600000E+01
9.400000E+00	2.400000E+01
1.900000E+01	3.200000E+01
3.800000E+01	3.200000E+01
4.200000E+01	2.950000E+01
4.700000E+01	0.
7.200000E+01	0.

TIME SPEED

0.	0.
2.000000E+01	0.
2.600000E+01	2.715810E+01
3.100000E+01	3.637010E+01
3.700000E+01	3.218600E+01
3.900000E+01	2.365671E+01
4.330000E+01	2.542694E+01
4.640000E+01	3.653111E+01
5.020000E+01	3.653111E+01
5.460000E+01	3.413950E+01
5.960000E+01	3.942785E+01
6.020000E+01	4.135901E+01
6.720000E+01	4.900365E+01
1.146000E+02	4.900365E+01
1.123000E+02	5.198039E+01
1.150000E+02	5.133667E+01
1.246000E+02	0.
1.630000E+02	0.
1.699000E+02	3.623925E+01
1.730000E+02	4.264645E+01
1.760000E+02	3.974971E+01
1.800000E+02	4.023250E+01
1.815000E+02	4.425575E+01
1.866000E+02	2.719717E+01
1.900000E+02	3.202507E+01
1.960000E+02	5.841759E+01
2.040000E+02	7.660250E+01
2.100000E+02	7.547617E+01
2.150000E+02	7.595966E+01
2.243000E+02	8.416519E+01
2.270000E+02	9.351150E+01
2.335000E+02	8.651150E+01
2.400000E+02	9.124711E+01
2.443000E+02	9.092545E+01
2.550000E+02	8.609755E+01
2.594000E+02	8.706311E+01
2.700000E+02	9.247495E+01
2.727000E+02	9.237895E+01
2.800000E+02	9.012090E+01

5.2500E+02 0.9031E+01 1.1220E+01 1.5263E+01 5.6843E-14 5.3674E+00 4.7570E-02 0.
 2973 1.4055E+00 6.8260E+00 5.8365E+00 2.8021E+00 -2.6864E-01 3.6637E+00 1.6914E+01
 2973 1.5725E+00 6.8337E+00 7.8615E+00 2.1141E-02 3.4437E-01 1.6914E+01 1.8457E+01
 5.5000E+02 9.0107E+01 1.1053E+01 1.1271E+01 5.6843E-14 5.7055E+00 4.7570E-02 0.
 3009 1.5632E+00 7.2186E+00 5.3904E+00 2.8002E+00 -2.6864E-01 3.7785E+00 1.2490E+01
 3009 1.6508E+00 7.2263E+00 8.2934E+00 2.1141E-02 3.6937E-01 1.2490E+01 1.4071E+01
 5.7500E+02 0.3684E+01 1.2451E+01 1.1537E+01 0. 6.0134E+00 4.7570E-02 0.
 2795 1.6225E+00 7.6556E+00 5.6580E+00 2.8055E+00 -2.6864E-01 3.8098E+00 1.2785E+01
 2795 1.7099E+00 7.6630E+00 8.5664E+00 2.1141E-02 3.9437E-01 1.2785E+01 1.4140E+01
 6.0000E+02 7.7961E+01 1.3004E+01 4.0431E+00 0. 6.2724E+00 4.7570E-02 0.
 2604 1.6729E+00 7.6559E+00 5.8631E+00 2.9117E+00 -2.6864E-01 3.8657E+00 5.6635E+00
 2604 1.7612E+00 7.6633E+00 8.7990E+00 2.1141E-02 4.1937E-01 5.6635E+00 5.6635E+00
 6.2500E+02 0.5456E+01 1.3546E+01 1.9044E+01 0. 6.5220E+00 4.9527E-02 0.
 2854 1.7474E+00 8.0557E+00 6.0973E+00 3.1309E+00 -3.4387E-01 4.1344E+00 2.1148E+01
 3805 1.8460E+00 8.0633E+00 9.2597E+00 2.2184E-02 4.2742E-01 2.1148E+01 2.3675E+01
 6.5000E+02 0.8260E+01 1.4115E+01 2.3959E+01 0. 6.7999E+00 1.1675E-01 0.
 2600 1.8235E+00 8.3712E+00 6.3290E+00 3.1309E+00 -3.4387E-01 4.3265E+00 2.6550E+01
 3574 1.9974E+00 9.3789E+00 9.6743E+00 2.2184E-02 4.1304E-01 2.6550E+01 1.2631E+01
 6.7500E+02 0.4776E+01 1.4695E+01 0.7251E+00 0. 7.0873E+00 1.1675E-01 0.
 2831 1.9933E+00 8.7595E+00 6.6096E+00 3.4405E+00 -3.4387E-01 4.5101E+00 9.6688E+00
 2831 2.0740E+00 8.7672E+00 1.0101E+01 2.2184E-02 4.3884E-01 9.6688E+00 1.1068E+01
 7.0000E+02 0.6773E+01 1.5267E+01 2.0505E+01 0. 7.3659E+00 1.1675E-01 0.
 2808 1.9616E+00 9.1003E+00 6.8598E+00 3.5641E+00 -3.4387E-01 4.6884E+00 2.2723E+01
 2808 2.1403E+00 9.1088E+00 1.0475E+01 2.2194E-02 4.6304E-01 2.2723E+01 2.4109E+01
 7.2500E+02 9.1823E+01 1.5984E+01 4.4401E+00 -2.8422E-14 7.7206E+00 1.1675E-01 0.
 3067 2.0493E+00 9.5777E+00 7.1790E+00 3.7628E+00 -3.4387E-01 4.9473E+00 4.9204E+00
 3067 2.2240E+00 9.5854E+00 1.0990E+01 2.5941E-02 4.9246E-01 4.9204E+00 6.5616E+00
 7.5000E+02 4.1909E+01 1.6442E+01 -2.9110E+01 -0.8810E+00 7.9756E+00 2.0633E-01 0.
 2706 2.1114E+00 9.3851E+00 7.2053E+00 3.7628E+00 -5.2659E-01 4.0635E+00 -1.7865E+01
 2706 2.3780E+00 9.3928E+00 1.1016E+01 2.5941E-02 3.7768E-01 -1.7865E+01 0.
 7.6500E+02 -6.7287E-03 1.6589E+01 0. 0. 7.9917E+00 2.6342E-01 10.38702
 1 200 2.1319E+00 9.3189E+00 7.2053E+00 3.7630E+00 -5.8126E-01 3.5100E-01 10.6762
 1 200 2.4417E+00 9.3265E+00 1.1016E+01 2.6063E-02 3.5100E-01 0. 0.
 CYCLE DISTANCE = 1.6509E+01
 FUEL CONSUMPTION ON MODE 1 = 3.9152E+01
 MODE 2 = 6.0402E+01
 BATT. ENERGY CONSUMPTION ON MODE 1 = 0.154E-02
 MODE 2 = 5.986E-03
 AVERAGE SPEED = 7.7647E+01 BATTERY DEPLETION = 1.8114053E-02 HEAT ENGINE ON TIME = 5.930000E+02 (MODE 1) 6.740833E+02 (MODE 2)
 BATTERY POWER DISTRIBUTION

35-34	34-30	30-25	25-22	22-19	19-14	14-10	10-6	6-2	2-2	2-6	6-10	10-14	14-18	18-22	22-26	26-30	30-34	34-38	TOTAL
0	0	1	4	4	5	11	66	0	530	329	131	215	89	59	62	13	12	0	1531
NEGATIVE POSITIVE																			
FUEL AND ENERGY CONSUMPTION ON COMPOSITE CYCLES																			
FUEL - MODE 1																			
FUEL - MODE 2																			
ENERGY - MODE 1																			
ENERGY - MODE 2																			
RANGE - MODE 1																			
RANGE - MODE 2																			
AV. FUEL																			
AV. ENERGY																			
AV. SPEED																			
SP. POWER - 1																			
SP. POWER - 2																			
SP. POWER - 3																			
SP. POWER - 4																			
SP. POWER - 5																			
SP. POWER - 6																			
SP. POWER - 7																			
SP. POWER - 8																			
SP. POWER - 9																			
SP. POWER - 10																			
SP. POWER - 11																			
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SP. POWER - 17																			
SP. POWER - 18																			
SP. POWER - 19																			
SP. POWER - 20																			

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2-189489E+01	6-682517E+01	1-877184E-01	2-379863E+01	4-283931E+01	1-828279E-01	3-321721E+01	2-389339E+01
2-437829E+01	6-595765E+01	1-694077E-01	2-654085E+01	4-509388E+01	8-501416E-02	3-707505E+01	2-312541E+01
2-655128E+01	6-535931E+01	1-550447E-01	2-804051E+01	4-818455E+01	7-270766E+01	4-031820E+01	2-315231E+01
2-831791E+01	6-492168E+01	1-452841E-01	3-879763E+01	4-989084E+01	6-370040E-02	4-308138E+01	2-317524E+01
2-959243E+01	6-458824E+01	1-377501E-01	3-248313E+01	5-121445E+01	5-682480E-02	4-546387E+01	2-319581E+01
3-059864E+01	6-432544E+01	1-318324E-01	3-395036E+01	5-227242E+01	5-140533E-02	4-753392E+01	2-321222E+01
3-176502E+01	6-402241E+01	1-249748E-01	3-582556E+01	5-351660E+01	4-513546E-02	5-019816E+01	2-323428E+01
3-290171E+01	6-372878E+01	1-182937E-01	3-786307E+01	5-475026E+01	3-903992E-02	5-338832E+01	2-325826E+01
3-373503E+01	6-351392E+01	1-133935E-01	3-951119E+01	5-566992E+01	3-457982E-02	5-542828E+01	2-327767E+01
3-437231E+01	6-335031E+01	1-096465E-01	4-087159E+01	5-639339E+01	3-117565E-02	5-735980E+01	2-329372E+01
3-487539E+01	6-322135E+01	1-066877E-01	4-201399E+01	5-695333E+01	2-849256E-02	5-89871E+01	2-330719E+01
3-528298E+01	6-311787E+01	1-042940E-01	4-298588E+01	5-742021E+01	2-632367E-02	6-036828E+01	2-331889E+01
3-561923E+01	6-303196E+01	1-023352E-01	4-382389E+01	5-788877E+01	2-453422E-02	6-156190E+01	2-332857E+01
3-590188E+01	6-298016E+01	1-006533E-01	4-455339E+01	5-813801E+01	2-303272E-02	6-268149E+01	2-333721E+01
3-614243E+01	6-289950E+01	9-923844E-02	4-519389E+01	5-842004E+01	2-175500E-02	6-351561E+01	2-334478E+01
3-635006E+01	6-284619E+01	9-881630E-02	4-576214E+01	5-866509E+01	2-865433E-02	6-432310E+01	2-335151E+01
3-653103E+01	6-280096E+01	9-695445E-02	4-626782E+01	5-888816E+01	1-969663E-02	6-508623E+01	2-335749E+01
3-668984E+01	6-276896E+01	9-682103E-02	4-672125E+01	5-906982E+01	1-885554E-02	6-569367E+01	2-336287E+01

YEARLY AV. FUEL CONSUMPTION = 4-775425E+01
 YEARLY AV. BATTERY ENERGY OUTPUT = 7-361339E-02
 EXPECTED BATTERY LIFE = 1-255950E+05

YEARLY AV. FUEL ECONOMY = 1-493861E+01
 YEARLY AV. WALL PLUG OUTPUT = 1-363211E-01

HEAT ENGINE ENERGY FRACTION = 5-702510E-01

C1.2 HYBRID SYSTEM STARTUP SIMULATION PROGRAMS (VSYS & VSYS2)

1. Program Description

The programs VSYS and VSYS2 simulate the response of a hybrid system to a power demand. Initially all of the power requirements of the vehicle are being met by the electric motor under steady state conditions. The vehicle is travelling at a constant speed, the heat engine is disengaged from the drive train and is turned off.

In response to a demand for increased power output, a clutch between the engine and the motor is closed and the engine is started. The resultant torques, rpms, vehicle speed, and vehicle acceleration, are determined over time scales on the order of a second. The simulation terminates when the engine rpm reaches motor rpm.

The heat engine is modelled as a engine output torque curve that is a function of crankshaft displacement. The engine clutch is modelled as a torque curve as a function of time. Over the range of rpm's considered in the startup simulation, the motor is modelled as a straight line of motor torque versus rpm. The torque converter is modelled as two monotonic functions serving to completely determine input torque, output torque, input rpm, and output rpm, from any combination of two of these variables. The VSYS2 program version has no torque converter. The transmission has gearing, spin losses, and efficiencies. The differential has a differential ratio, spin loss, and an efficiency. The vehicle itself has aerodynamic, rolling resistance, and grade forces.

Data	Description	Units
NTHE	number of heat engine torque data points	—
HEI	heat engine inertia	kg m ²
{ THE (NTHE)	heat engine torque	nt.m
{ THETA (NTHE)	heat engine angular displacement	rev.
NTCL	number of clutch torque data points	—
{ TCL (NTCL)	clutch torque	nt.m
{ TIME (NTCL)	clutch torque engagement times	sec
CM	slope of motor torque versus r.p.m.	ntm/rpm
EMI	motor inertia	kg m ²
NTSP	number of torque converter data points	—
{ CTC2RO	(not used, kept as data convention)	—
{ TSP (NTSP)	torque - speed ratios	rpm/√ntm
{ TOR (NTSP)	torque ratios	—
{ SPR (NTSP)	speed ratios	—
NGEAR	number of gears	—
SHFTUP	upshift rpm	rpm
{ .RATIO (NGEAR)	transmission ratios	—
{ CT1 (NGEAR)	friction coefficient	nt m
{ CT2 (NGEAR)	friction coefficient	ntm/rpm
{ EMUT (NGEAR)	transmission efficiency	—
NRATIO	differential ratio	—
CD1	friction coefficient	ntm
CD2	friction coefficient	ntm/rpm
EMUD	differential efficiency	—
RTIRE	tire radius	m
CTIRE 1	friction coefficient	—
CTIRE 2	friction coefficient	1/kg ^{1/2} hr
VMACC	vehicle mass	kg
DLI	drive line inertia	kg m ²
CLF	drag coefficient * frontal area	m ²
GRAD	road gradient	—
V	vehicle speed	km/hr
ELT	run time interval for RKTTABLE	sec
TF	final time in simulation	sec
NPRNT	number of suppressed print times	—

Variables	Description	Units
JGEAR	steady state gear	—
VMPS	vehicle speed	m/sec
RPMDO	differential output r.p.m.	rpm
TLFD	differential torque loss	nt.m
RPMTO	transmission output r.p.m.	rpm
TLFT	transmission torque loss	nt.m
RPMTCO	torque converter output r.p.m.	rpm
FA	aerodynamic force	nt
FR	rolling resistance force	nt
FG	gradient force	nt
FNET ϕ	steady state net force	nt
TDO	differential output torque	nt.m
TTO	transmission output torque	nt.m
TTCO	torque converter output torque	nt.m
TSPAR	torque - speed ratio	rpm/ $\sqrt{nt.m}$
TQRAT	torque ratio	—
TTCIN	torque converter input torque	nt.m
SPRAT	speed ratio	—
RPMTCN	torque converter input rpm	rpm
TEM ϕ	steady state motor torque intercept	nt.m
K	print skip control flag	—
T	time in simulation	sec
Y(1)	angular speed of engine	rad/sec
Y(2)	angular displacement of engine	rad.
Y(3)	angular speed of motor	rad/sec.
Y(4)	speed of vehicle	m/sec.
YDOT(1)	angular acceleration of engine	rad/sec ²
YDOT(2)	angular speed of engine	rad/sec
YDOT(3)	angular acceleration of motor	rad/sec ²
YDOT(4)	acceleration of vehicle	m/sec ²
RPMHE	engine r.p.m.	rpm
RPMEM	motor r.p.m.	rpm
V	speed of vehicle	km/hr
A	acceleration of vehicle	g _{earth}
VMASS2	effective vehicle inertial mass	kg

DERIV Subroutine for VSYS

C-74

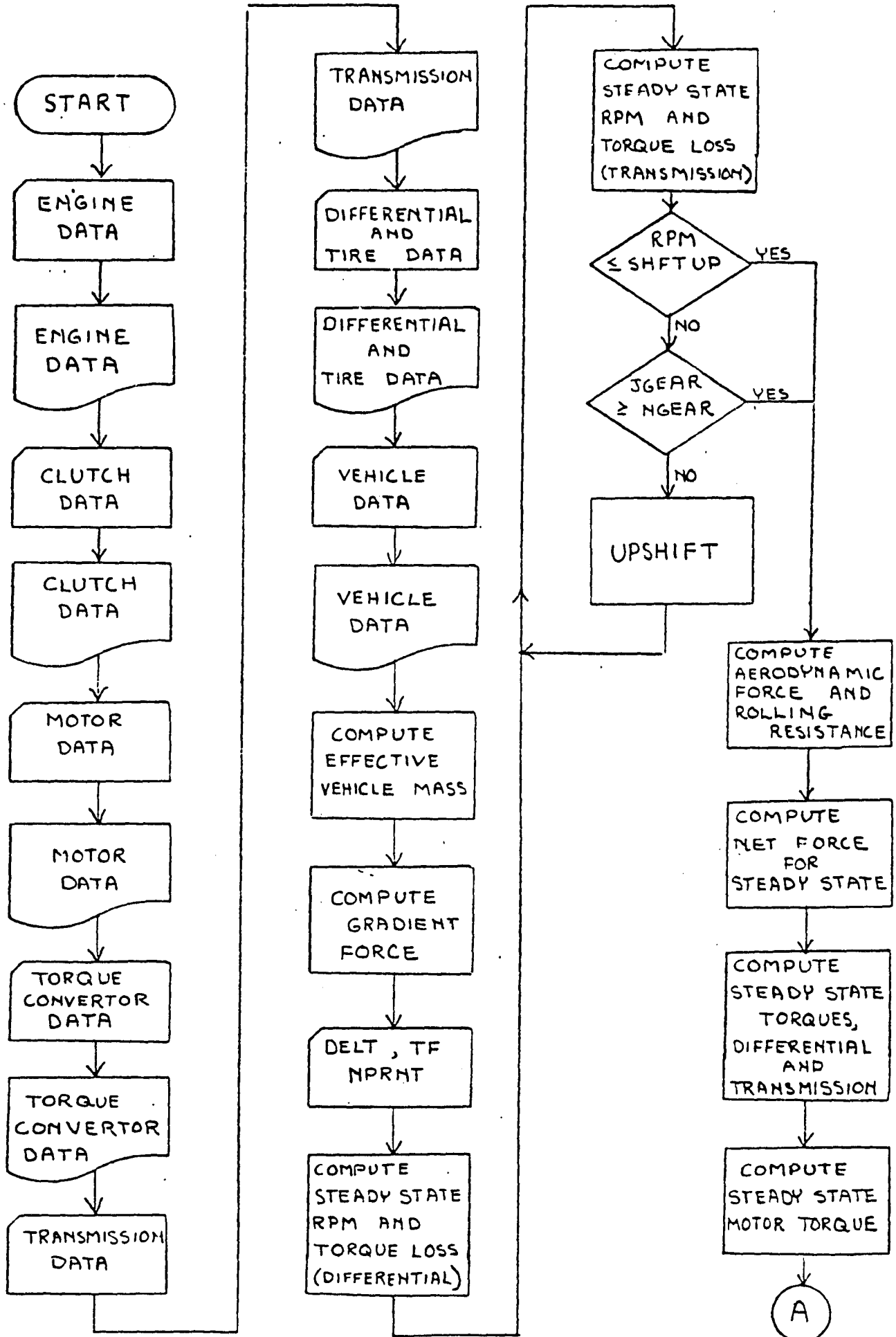
Variables	Description	Units
ICLN	clutch torque	nt m
THETAN	angular displacement of engine	rev
THEN	engine torque	nt.m
RPMDO	differential output rpm.	rpm
RPMTO	transmission output rpm.	rpm
RPMTCO	torque converter output r.p.m.	rpm
SPRAT	speed ratio	—
TSPAR	torque-speed ratio	rpm/√ftm
TQRAT	torque ratio	—
TTCO	torque converter output torque	nt m
TTCIN	torque converter input torque	nt m
TEM	motor torque	nt m
TTO	transmission output torque	nt m
TDO	differential output torque	nt m
FNET	net force on vehicle	nt
FAC	acceleration force of vehicle	nt

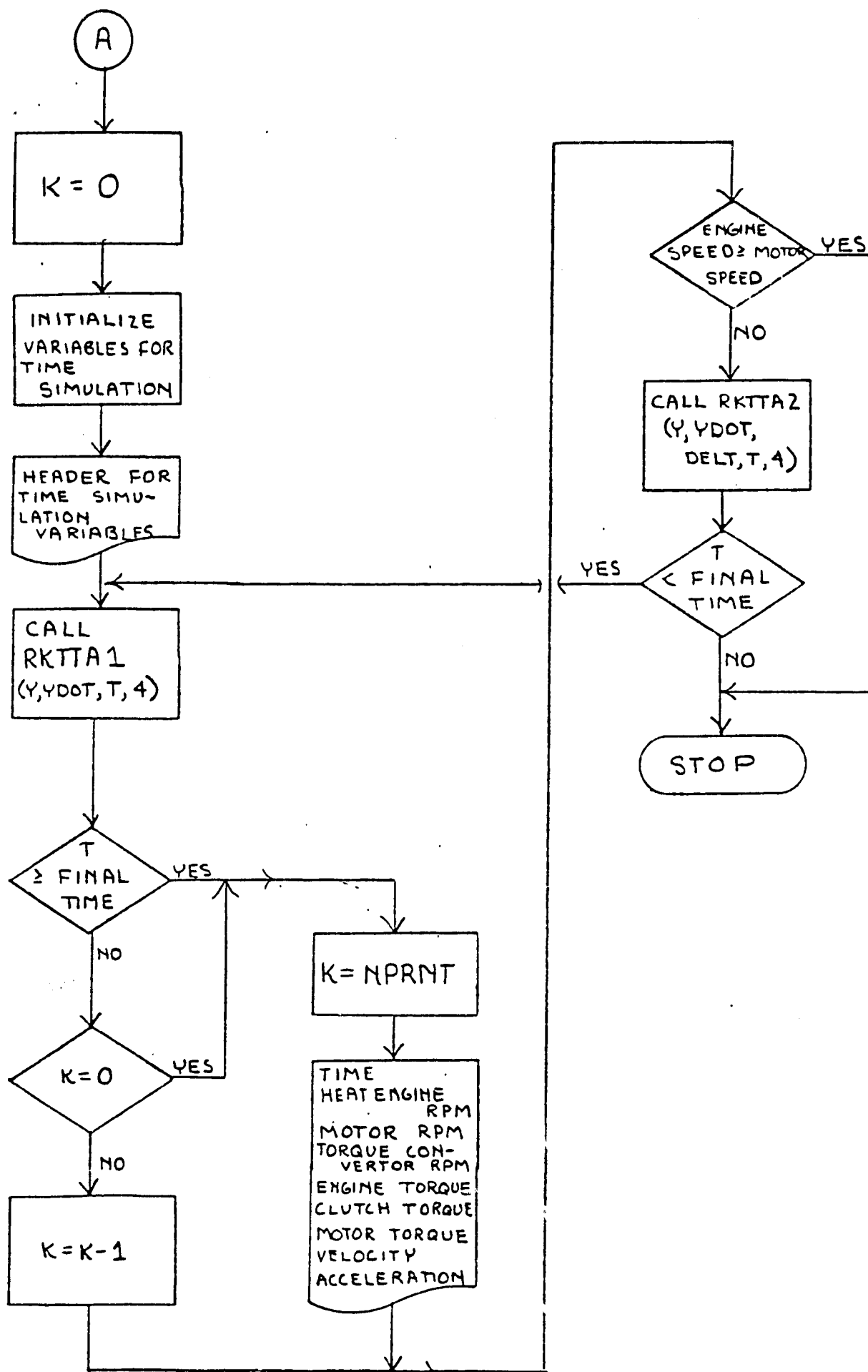
FORTRAN CODING FORM

GENERAL RESEARCH CORPORATION

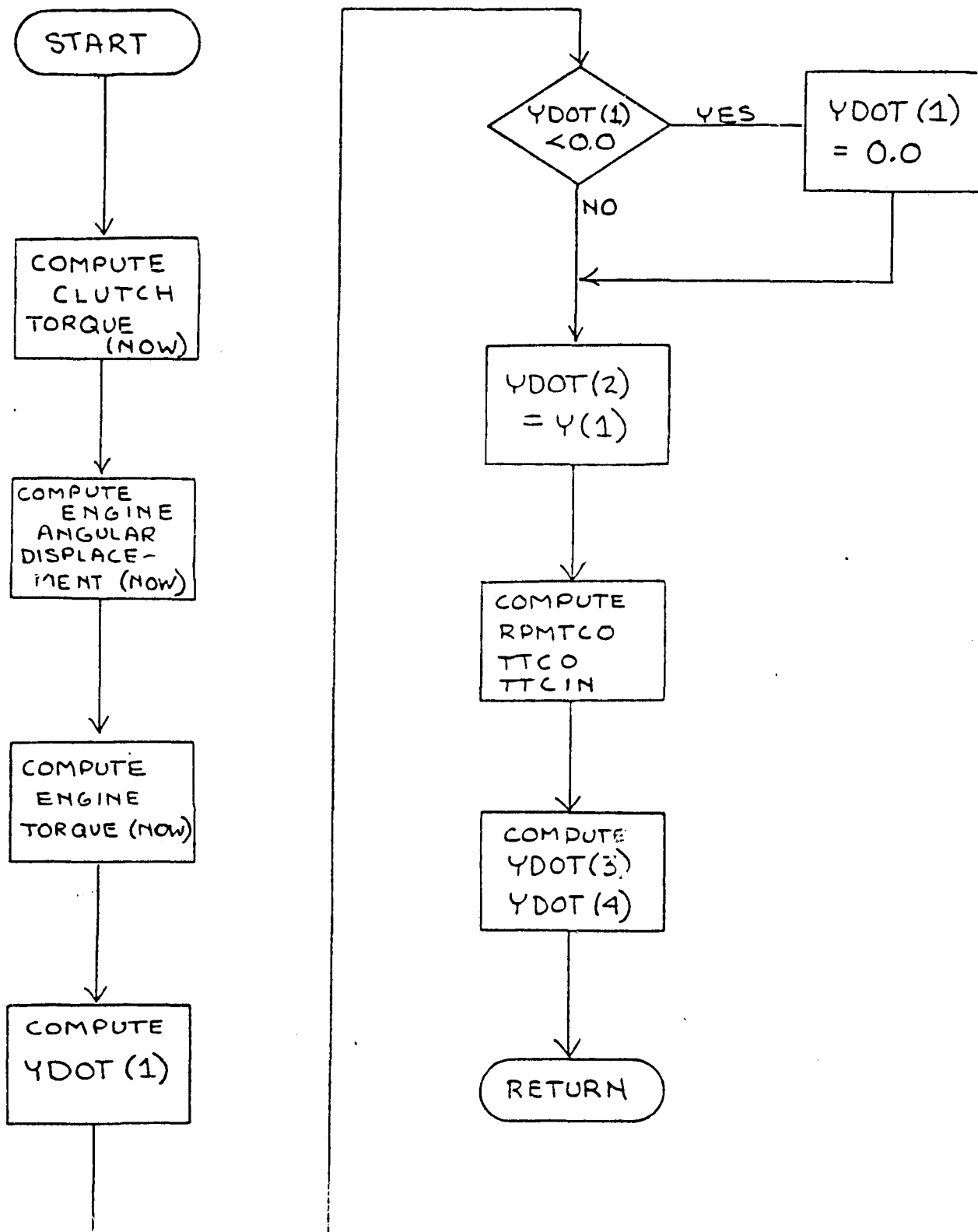
PROGRAM	NAME	PAGE	OF
VSYS		1	1
ROUTINE	DATE		
Input Format			

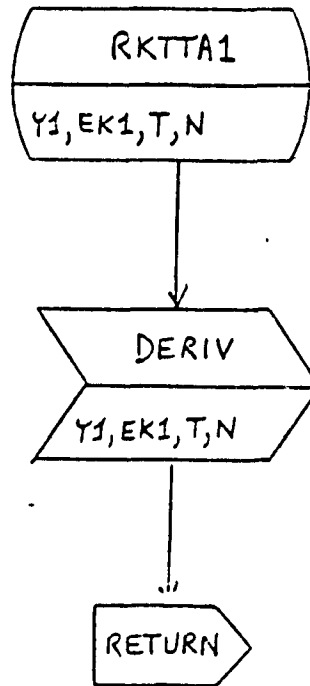
STATE- MENT NO.	FORTRAN STATEMENT										SERIAL NUMBER	
	0 ZERO 0 ALPHA 0	1 ONE 1 ALPHA 1	2 TWO 2 ALPHA 2	3 THREE 3 ALPHA 3	4 FOUR 4 ALPHA 4	5 FIVE 5 ALPHA 5	6 SIX 6 ALPHA 6	7 SEVEN 7 ALPHA 7	8 EIGHT 8 ALPHA 8	9 NINE 9 ALPHA 9		
1	NTHE	HEI										
2	THE(1)	THETA(1)	THE(NTHE)	THE TA(NTHE)						
3	NTCL											
4	TC(1)	TIME(1)	TCL(NTCL)	TIME(NTCL)						
5	CM	EMI										
6	NTSP											
7	CTC(1)	TSP(1)	TOS(1)	SPR(1)		
8	TSP(NTSP)	TOR(NTSP)	SPR(NTSP)					
9	NGEAR	SHFTUP										
10	TRATIO(1)	CT1(1)	CT2(1)	EMUT(1)		
11	...	TRATIO(NGEAR)	CT1(NGEAR)	CT2(NGEAR)	EMUT(NGEAR)							
12	DRATIO	CD1	CD2	...	EMUD	RTIRE	CTIRE1	CTIRE2				
13	VMASS	DLI	CD4	...	GRAD							
14	DELT	TF	MNPT	...								
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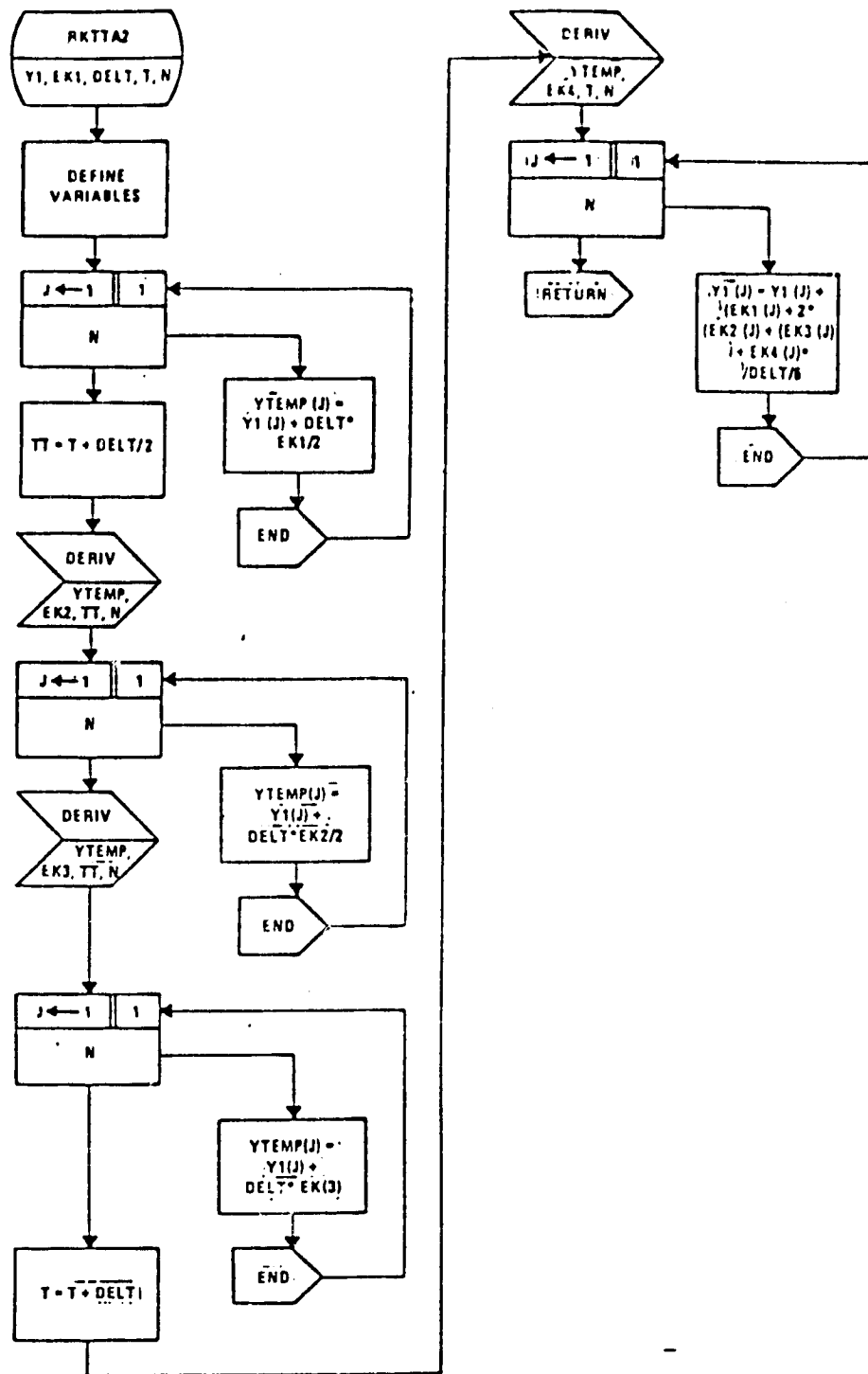


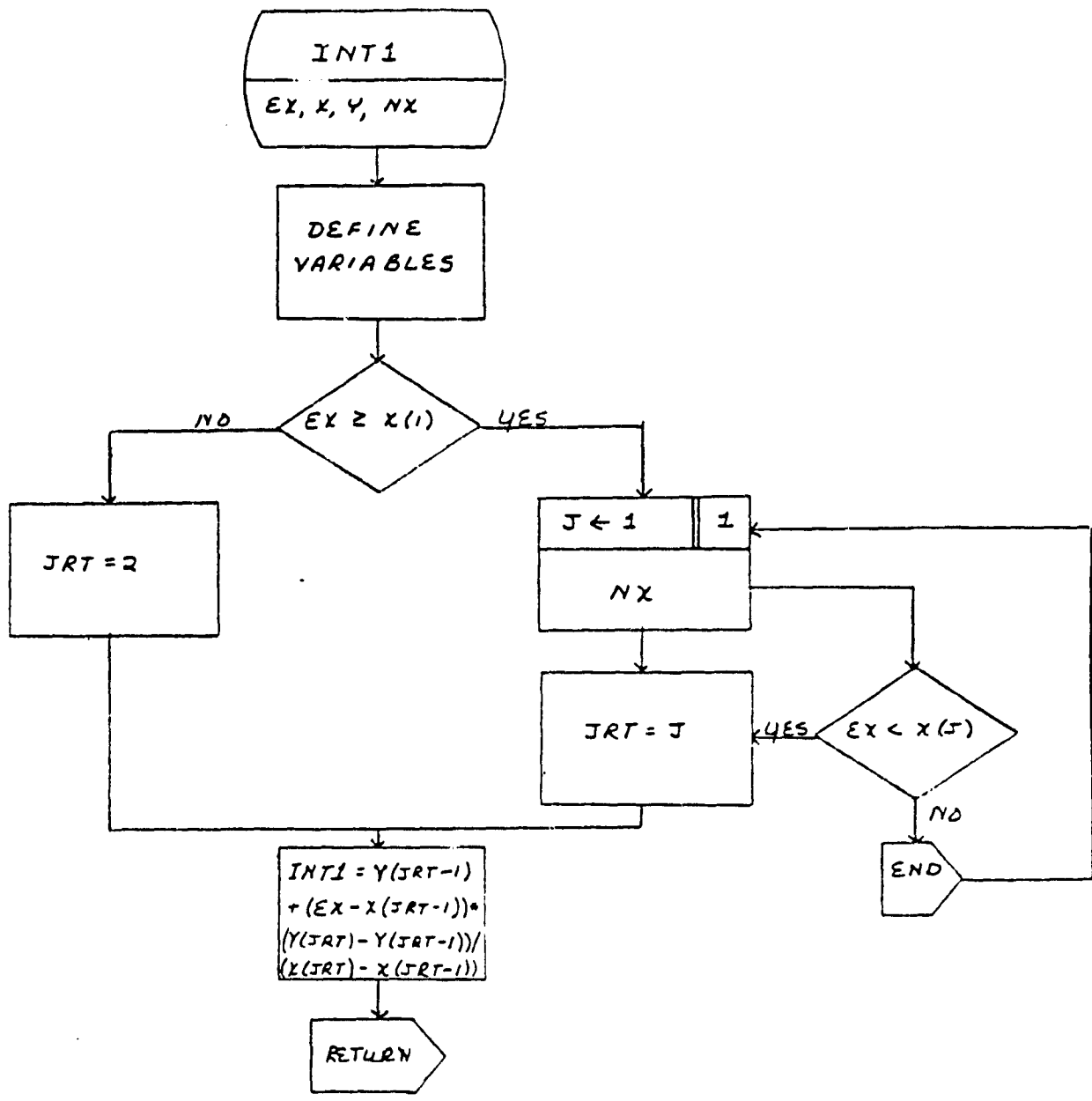


VSYS Subroutine DERIV









GOLETA FCSTPAN 1.3 * SEMI-AUTO PFL * (01-10-73)

ORIGINAL PAGE IS
OF POOR QUALITY

PROGRAM VSYS

C
C THIS PROGRAM MODELS A HYBRID VEHICLE PROPULSION SYSTEM.
C THE ELECTRIC MOTOR IS PRODUCING TORQUE UNDER STEADY STATE
C CONDITIONS AND THE HEAT ENGINE CLUTCH IS ENGAGED.

C ALL UNITS IN MKS EXCEPT
C THETA, THETAN (REVOLUTIONS)
C V, VPL (KM. PER HR.)
C A, APL (G)
C RPM00, RPMT0, RPMT00, RPMT0N (REV. PER MIN.)
C RPMHE, RPHEM (REV. PER MIN.)
C WPL, UPL (REV. PER MIN.)
C CM (NEWTON*METERS/RPM)
C CT2, CD2, SPFTUF, CTIRE2, TSP, TSPAR, COA

000003 COMMON RTIRE,CD1,CD2,DRATIC,CT1(6),CT2(6),TPATIC(6),COA,CTIRE1
1CTIRE2,VMASS,EMUD,EMUT(6),NGEAR,CLI,GRAD,CM,HEI,EMI.
2VMASS2,FG,V,JGEAR,
3TSP(20),TQR(20),SPR(20),NTSP,
4NTCL,TCL(10),TIME(10),NTHE,THE(10),THETA(10),
5VMPS,RPM00,TLFD,RPMT0,TLFT,RPMT00,FA,FR,FNET0,T00,TTC,TT00,TSP
6TORAT,TT0IN,SPRAT,RPMT0N,TEM0,THETAN,
7TCLN,THEN,TEM,FNET,FAC
000003 REAL YDOT(4),Y(4),INT1

C
C INPUT ENGINE DATA

000003 READ 640,NTHE,HEI
000013 READ 610,(THE(J),THETA(J),J=1,NTHE)
000030 PRINT 420,HEI
000036 PRINT 820,(THE(J),THETA(J),J=1,NTHE)

C
C INPUT CLUTCH DATA

000057 READ 620,NTCL
000061 READ 610,(TCL(J),TIME(J),J=1,NTCL)
000076 PRINT 400
000102 PRINT 820,(TCL(J),TIME(J),J=1,NTCL)

C
C INPUT MOTOR DATA

000117 READ 610,CM,EMI
000127 PRINT 430,CM,EMI

C
C INPUT TORQUE CONVERTOR DATA

000137 READ 620,NTSP
000145 READ 610,CTCZFO,(TSP(J),TQR(J),SPR(J),J=1,NTSP)
000166 PRINT 860
000172 PRINT 865,CTCZFO
000200 PRINT 870
000204 PRINT 814,(TSP(J),TQR(J),SPR(J),J=1,NTSP)

C
C INPUT TRANSMISSION DATA

GOLETA FORTRAN 1.3 * SEMI-AUTO PFL * (01-10-73)

VSY5

```

      C
0001223      READ 640,NGEAR,SHFTUP
      J233      READ 610,(TRATIO(J),CT1(J),CT2(J),EMUT(J),J=1,NGEAR)
000254      PRINT 840
000260      PRINT 845
000264      PRINT 810,(TRATIO(J),CT1(J),CT2(J),EMUT(J),J=1,NGEAR)
000305      PRINT 850,SHFTUP

      C
      C      INPUT DIFFERENTIAL AND TIRE DATA
      C
000313      READ 610,DRATIO,CD1,CD2,EMUD,RTIRE,CTIRE1,CTIRE2
000335      PRINT 875
000341      PRINT 880
000345      PRINT 885,DRATIO,CD1,CD2,EMUD,RTIRE,CTIRE1,CTIRE2

      C
      C      INPUT VEHICLE DATA
      C
000367      READ 610,VMASS,DLI,COA,GRAD,V
000405      PRINT 890,VMASS,DLI,COA
000417      PRINT 925,GRAD,V
000427      VMASS2=VMASS+DLI/RTIRE**2

      C
      C      GRADIENT-
      C
000432      FG=9.807*VMASS*SIN(ATAN(GRAD))

      C
      C      INPUT RUN DATA
      C
000441      READ 630,DELT,TF,NPRNT

      C
      C      COMPUTE STEADY STATE CONDITIONS
      C
000452      JGEAR=1
000453      VMPS=V/3.6
000455      RPMDO=9.5492967*VMPS/RTIRE
000457      TLFD=CD1+CD2*RPMDO
000462      RPMYC=RPMDO*DRATIO
000464      IF CONTINUE
000464      TLFT=CT1(JGEAR)+CT2(JGEAR)*RPMTC
000470      RPMTC=RPMTC+TRATIO(JGEAR)

      C
      C      UPSHIFT IF NECESSARY
      C
000472      TF((RPMTCO,LE,SHFTUP).OR.(JGEAR,GE,NGEAR))GO TO 19
000503      JGEAR=JGEAR+1
000504      GO TO 15
000505      18 CONTINUE

      C
      C      AERODYNAMIC -
      C
000505      FA=0.6125*COA*VMPS**2

      C
      C      ROLLING RESISTANCE -
      C
000510      FR=9.807*VMASS*(CTIRE1+CTIRE2*V)

```

GOLETA FCRTFAN 1.3 * SEMI-AUTO RFL * (01-10-73)

VSY5

```

C
C   ACCELERATION -
C
000514   FNET0=FA+FG+FR
000517   T00=FNET0*RTIRE

C
C   DIFFERENTIAL -
C
000521   T10=T00/(FMUC*DRATIO)+TLFC

C
C   TRANSMISSION -
C
000525   T1C0=T10/(EMUT(JGEAR)*TRATIO(JGEAR))+TLFT

C
C   HAVE OUTPUT SPEED AND OUTPUT TORQUE.
C
000532   TSPAR=RPMTCC/SQRT(ABS(T1C0))
000536   TGRAT=INT1(TSPAR,TSP,TGR,NTSP)
000542   TTCIN=T1C0/TGRAT
000544   SPRAT=INT1(TSPAR,TSP,SPR,NTSP)
000550   RPMTCN=RPMTCC/SPRAT
000552   TE40=TTCIN+CM*RPMTCN

C
C   SET INITIAL CONDITIONS
C
000555   K=0
000556   T=0.0
000557   Y(1)=0.0
000560   Y(2)=0.0
000561   Y(3)=.104719755*RPMTCN
000563   Y(4)=V/3.6
000566   PRINT 700
000571   80 CONTINUE
000571   CALL RKTTA1(Y,YDOT,T,4)
000574   IF((T.GE.TF).OR.(K.EQ.0))GO TO 107
000604   K=K-1
000605   GO TO 109
000605   107 CONTINUE
000605   K=NPRNT

C
C   TIME TO PRINT RESULTS -
C
000606   RPMHE=Y(1)/.104719755
000610   RPMEM=Y(3)/.104719755
000612   V=Y(4)*3.6
000614   A=YDOT(4)/9.807
000616   PRINT 886,T,RPMHE,RPMEM,RPMTCC,THEM,TCLN,TEM,V,A
000644   109 CONTINUE

C
C   INTEGRATE TO NEXT TIME STEP
C
000644   IF(Y(1).GE.Y(3))GO TO 190
000647   CALL RKTTA2(Y,YDOT,DELT,T,4)
000652   IF(T.LT.TF)GO TO 80
000655   190 CONTINUE

```


GOLETA FORTFAN 1.3 * SEMI-AUTO RFL * (01-10-73)

VSY5

```

000655      200 STOP
          C
          C      FORMAT STATEMENTS
          C
000657      400 FORMAT(1H0,*CLUTCH DATA*//5X,*CLUTCH TQ.*,6X,*TIME*)
000657      420 FORMAT(1H0,*ENGINE DATA*//5X,*ENGINE INERTIA =*,E16.6//
          15X,*ENGINE TQ.*,6X,*THETA*)
000657      430 FORMAT(1H0,*MOTOR DATA*//5X,*MOTOR SPEED DROOP =*,E16.6,4X,
          1*MOTOR INERTIA =*,E16.6)
000657      610 FORMAT(7F10.4)
000657      620 FORMAT(7I10)
000657      630 FORMAT(2F10.4,2I10)
000657      640 FORMAT(I10,6F10.4)
000657      700 FORMAT(1H0,4X,*TIME*, 7X,*ENGINE RPM*,3X,*MOTOR RPM*,4X,*TCO R
          16X,*ENGINE TQ.*,3X,*CLUTCH TQ.*,3X,
          2*MOTOR TQ.*,4X,*SPEED*,8X,*ACCEL.*)
000657      810 FORMAT(1H ,4E16.6)
000657      814 FORMAT(1H ,3E16.6)
000657      820 FORMAT(1H ,2E16.6)
000657      840 FORMAT(1H0,12HGEARBOX DATA)
000657      845 FORMAT(1H0,4X,10HGEAR RATIO,6X,22HSPIN LOSS COEFFICIENTS,10X
          1,*EFFICIENCY*)
000657      850 FORMAT(/T5,*UPSHIFT RPM = *,E16.6)
000657      860 FORMAT(1H0,21HTCRQUE CONVERTOR DATA)
000657      865 FORMAT(1H0,4X,17HNI**2/TI(STALL) =,E16.6)
000657      870 FORMAT(1H0,4X,11HNO/SQRT(TO),5X,FHTO/TI,11X,5HNC/NI)
000657      875 FORMAT(1H0,18HAXLE AND TIRE DATA )
000657      880 FORMAT(1H0,4X,14HFIN. DR. RATIO,2X,22HSPIN LOSS COEFFICIENTS,1
          1,*EFFICIENCY*,6X,*ROLLING RADIUS*,2X,*ROLL. RESIST. COEFFICIEN
000657      885 FORMAT(1H ,7E16.6)
000657      886 FORMAT(1H ,E12.2,9E13.4)
000657      890 FORMAT(1H0.14HVEHICLE MASS =,E16.6
          1,5X,*DRIVE LINE INERTIA = *,E16.6
          2,5X,19H(OPAG COEF.)*AREA =,F16.6)
000657      925 FORMAT(1H0,18HCYCLE GRADIENT =,E10.3,
          1*STEADY STATE SPEED =*,E10.3)
000657      END

```

GOLETA FCRTFAN 1.3 * SEMI-AUTO °FL * (01-10-73)

SUBROUTINE DEPIV(Y,YDOT,T,N)

C
C
C
C
C
CY(1) IS ENGINE SPEED
Y(2) IS ENGINE ANGULAR DISPLACEMENT
Y(3) IS MOTOR SPEED
Y(4) IS VEHICLE SPEED

000007

COMMON RTIRE,CD1,CD2,DRATIO,CT1(6),CT2(6),TRATIC(6),COA,CTIRE
1CTIRE2,VMASS,EMUD,EMUT(6),NGEAR,DLI,GRAD,CP,HEI,EMI,
2VMASS2,FG,V,JGEAR,
3TSP(20),TQR(20),SPR(20),NTSP,
4NTCL,TCL(10),TIME(10),NTHE,THE(10),THETA(10),
5VMPS,RPMDC,TLFD,RPMT0,TLFT,RPMTCO,FA,FR,FNET0,TCC,TT0,TTCO,TSI
ETORAT,TTGIN,SFRAT,RPMTGN,TEMO,THETAN,
7TCLN,THEN,TEM,FNET,FAC
REAL Y(2),YDOT(2),INT1

000007

C

000007

TCLN=INT1(T,TIME,TCL,NTCL)

000015

THETAN=Y(2)/6.2831852

000017

THEN=INT1(THETAN,THETA,THE,NTHE)

000023

YDOT(1)=(THEN+TCLN)/HEI

C
C
C

NO NEGATIVE ENGINE POTENTIAL ACCELERATION

000031

IF(YDOT(1).LT.0.0)YDOT(1)=0.0

000034

YDOT(2)=Y(1)

0036

RPMDC=9.5492967*Y(4)/RTIRE

000040

RPMTC=RPMD0*CRATIC

000042

RPMTCO=RPMTC*TRATIC(JGEAR)

000044

SPRAT=.104719755*RPMTCO/Y(3)

000047

TSPAR=INT1(SFRAT,SPR,TSF,NTSP)

000053

TORAT=INT1(SPRAT,SPR,TQR,NTSP)

000057

TTCO=(RPMTCO/TSPAR)**2.

000064

TTGIN=TTCO/TORAT

000066

TEM=TEMO-CP*Y(3)/.104719755

000074

YDOT(3)=(TEM-TCLN-TTGIN)/EMI

000101

TTC=TTCO*EMUT(JGEAR)*TRATIC(JGEAR)

000104

TDC=TT0*EMUC*CRATIC

000106

FNET=TDC/PTIRE

000110

FAC=FNET-FNET0

000112

YDOT(4)=FAC/VMASS2

000114

RETURN

000115

END

GOLETA FCFTFAN 1.3 * SEMI-AUTO PFL * (01-10-73)

```
      SUBROUTINE RKTTA1(Y1,EK1,T,N)
0007   REAL Y1(20),EK1(20)
000007 CALL DERIV(Y1,EK1,T,N)
000010 RETURN
000011 END
```

GOLETA FCFTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

```
      SUBROUTINE RKTTA2(Y1,EK1,DELT,T,N)
      REAL Y1(20),Y2(20),YTEMP(20),EK1(20),EK2(20),EK3(20),EK4(20)
      DO 50J=1,N
      YTEMP(J)=Y1(J)+DELT*EK1(J)/2.
50  CONTINUE
      TT=T+DELT/2.
      CALL DERIV(YTEMP,EK2,TT,N)
      DO 60J=1,N
      YTEMP(J)=Y1(J)+DELT*EK2(J)/2.
60  CONTINUE
      CALL DERIV(YTEMP,EK3,TT,N)
      DO 70J=1,N
      YTEMP(J)=Y1(J)+DELT*EK3(J)
70  CONTINUE
      T=T+DELT
      CALL DERIV(YTEMP,EK4,T,N)
      DO 80J=1,N
      Y1(J)=Y1(J)+(EK1(J)+2.*(EK2(J)+EK3(J))+EK4(J))*(DELT/6.)
80  CONTINUE
      RETURN
      END
```

GOLETA FORTRAN 1.3 * SEMI-AUTO PFL * (01-10-73)

```
      REAL FUNCTION INT1(EX,X,Y,NX)
      C
      C   INT1 INTERPOLATES IN ONE VARIABLE
      C
000007      REAL X(10),Y(10)
000007      IF (EX.GE.X(1))GO TO 5
000011      JRT=2
000012      GO TO 20
000013      5 DO 10 J=1,NX
000015      IF (EX.LT.X(J))GO TO 15
000020      10 CONTINUE
000022      15 JRT=J
000024      20 INT1=Y(JRT-1)+(EX-X(JRT-1))*(Y(JRT)-Y(JRT-1))/(X(JRT)-X(JRT-1))
000040      RETURN
000041      END
```

ENGINE DATA

ENGINE INERTIA = 5.250000E-02

ENGINE TC. THETA
-1.000000E+01 0.
-1.000000E+01 1.000000E+00
5.000000E+01 2.000000E+00
5.000000E+01 3.000000E+00

CLUTCH DATA

CLUTCH TO. TIME
0. 0.
1.000000E+02 1.000000E+00

MOTOR DATA

MOTOR SPEED DROOP = 4.400000E-01 MOTOR INERTIA = 1.050000E-01

TORQUE CONVERTER DATA

NI**27(IINSTALL) = 1.300000E+04

NO/SCY(TC)	TC/II	NO/ST
0.	2.100000E+00	0.
1.147000E+01	2.064000E+00	1.000000E-01
2.331000E+01	1.927000E+00	2.000000E-01
3.560000E+01	1.820000E+00	3.000000E-01
4.852000E+01	1.700000E+00	4.000000E-01
5.150000E+01	1.560000E+00	5.000000E-01
7.340000E+01	1.420000E+00	5.000000E-01
9.720000E+01	1.270000E+00	7.000000E-01
1.200000E+02	1.140000E+00	8.000000E-01
1.564000E+02	1.000000E+00	9.000000E-01
2.135000E+02	1.000000E+00	9.500000E-01
3.341000E+02	1.000000E+00	9.750000E-01
1.000000E+03	1.000000E+00	1.000000E+00

GEARBOX DATA

GEAR RATIO SPIN LOSS COEFFICIENTS EFFICIENCY

2.450000E+00	0.	9.200000E-01
1.450000E+00	0.	9.200000E-01
1.000000E+00	0.	9.400000E-01

UPSHIFT CPM = 4.000000E+03

WHEEL AND TIPT DATA

FIN. DR. RATIO SPIN LOSS COEFFICIENTS EFFICIENCY ROLLING RADIUS COLL. RESIST. COEFFICIENTS

4.100000E+00	0.	9.600000E-01	3.050000E-01	1.000000E-02	0.
--------------	----	--------------	--------------	--------------	----

VEHICLE PASS = 3.200000E+02 ROLLS PER MIN = 5.600000E+00 TORQUE LOSS COEFF = 0.700000E-01

CYCLE GEARSHIFT = 0. STEERING STABILIZER = 7.000000E+01

TIME	ENGINE RPM	TC/SCM	ENGINE TC.	CLUTCH TO.	WHEEL TO.	SPIN	ACCEL.
0.	0.	1.050000E+02	1.000000E+01	0.	2.647000E+01	7.000000E-01	-2.671000E-10
2.00E-02	0.	1.050000E+02	1.000000E+01	2.000000E+00	2.647000E+01	7.000000E-01	-6.000000E-04
4.00E-02	0.	1.050000E+02	1.000000E+01	4.000000E+00	2.647000E+01	6.000000E-01	-1.000000E-03

6.00E-02	1.6508E+01	3.6102E+03	-1.0000E+01	6.0000E+00	2.6747E+01	6.9995E+01	-1.7970E-03
0.00E-02	3.6644E+01	3.6191E+03	-1.0000E+01	6.0000E+00	2.7796E+01	6.9997E+01	-2.4949E-03
1.00E-01	3.6459E+01	3.6190E+03	-1.0000E+01	1.0000E+01	2.9662E+01	6.9995E+01	-1.1674E-03
1.20E-01	3.6474E+01	3.6189E+03	-1.0000E+01	1.2000E+01	2.9974E+01	6.9992E+01	-3.9165E-03
1.40E-01	3.6404E+01	3.6187E+03	-1.0000E+01	1.4000E+01	3.1122E+01	6.9980E+01	-6.4162E-03
1.60E-01	3.6311E+01	3.6185E+03	-1.0000E+01	1.6000E+01	3.2300E+01	6.9985E+01	-5.7111E-03
1.80E-01	3.6354E+01	3.6184E+03	-1.0000E+01	1.8000E+01	3.3512E+01	6.9989E+01	-5.5157E-03
2.00E-01	3.6395E+01	3.6183E+03	-1.0000E+01	2.0000E+01	3.4756E+01	6.9978E+01	-6.1845E-03
2.20E-01	3.6295E+01	3.6179E+03	-1.0000E+01	2.2000E+01	3.6011E+01	6.9974E+01	-6.5801E-03
2.40E-01	3.6377E+01	3.6178E+03	-1.0000E+01	2.4000E+01	3.7316E+01	6.9965E+01	-7.1144E-03
2.60E-01	3.6296E+01	3.6174E+03	-1.0000E+01	2.6000E+01	3.8671E+01	6.9962E+01	-7.6647E-03
2.80E-01	3.6205E+01	3.6171E+03	-1.0000E+01	2.8000E+01	4.0019E+01	6.9952E+01	-8.1560E-03
3.00E-01	3.6174E+01	3.6169E+03	-1.0000E+01	3.0000E+01	4.1427E+01	6.9952E+01	-8.5640E-03
3.20E-01	3.6142E+01	3.6165E+03	-1.0000E+01	3.2000E+01	4.2845E+01	6.9944E+01	-8.9405E-03
3.40E-01	3.6109E+01	3.6161E+03	-1.0000E+01	3.4000E+01	4.4289E+01	6.9939E+01	-9.3196E-03
3.60E-01	3.6075E+01	3.6158E+03	-1.0000E+01	3.6000E+01	4.5759E+01	6.9931E+01	-9.7047E-03
3.80E-01	3.6041E+01	3.6154E+03	-1.0000E+01	3.8000E+01	4.7252E+01	6.9925E+01	-1.0134E-02
4.00E-01	3.5987E+01	3.6150E+03	-1.0000E+01	4.0000E+01	4.8765E+01	6.9919E+01	-1.0542E-02
4.20E-01	3.5972E+01	3.6146E+03	-1.0000E+01	4.2000E+01	5.0309E+01	6.9911E+01	-1.0974E-02
4.40E-01	3.5937E+01	3.6142E+03	-1.0000E+01	4.4000E+01	5.1889E+01	6.9903E+01	-1.1431E-02
4.60E-01	3.5901E+01	3.6138E+03	-1.0000E+01	4.6000E+01	5.3495E+01	6.9895E+01	-1.1911E-02
4.80E-01	3.5864E+01	3.6134E+03	-1.0000E+01	4.8000E+01	5.5129E+01	6.9887E+01	-1.2413E-02
5.00E-01	3.5827E+01	3.6130E+03	-1.0000E+01	5.0000E+01	5.6795E+01	6.9879E+01	-1.2936E-02
5.20E-01	3.5790E+01	3.6125E+03	-1.0000E+01	5.2000E+01	5.8491E+01	6.9871E+01	-1.3481E-02
5.40E-01	3.5753E+01	3.6121E+03	-1.0000E+01	5.4000E+01	6.0216E+01	6.9862E+01	-1.4048E-02
5.60E-01	3.5715E+01	3.6116E+03	-1.0000E+01	5.6000E+01	6.1970E+01	6.9853E+01	-1.4637E-02
5.80E-01	3.5678E+01	3.6111E+03	-1.0000E+01	5.8000E+01	6.3753E+01	6.9844E+01	-1.5248E-02
6.00E-01	3.5640E+01	3.6107E+03	-1.0000E+01	6.0000E+01	6.5565E+01	6.9835E+01	-1.5881E-02

Data	Description	ORIGINAL PAGE IS OF POOR QUALITY Units
JTHE	number of heat engine data points	—
HEI	heat engine inertia	kg m ²
{ THE(NTHE)	heat engine torque	nt m
{ THETA(NTHE)	heat engine angular displacement	rad.
NTCL	number of clutch torque data points	—
TCL(NTCL)	clutch torque	nt m
TIME(NTCL)	clutch torque engagement times	sec.
CM	slope of motor torque versus r.p.m.	nt m/rpm
EMI	motor inertia	kg m ²
NGEAR	number of gears	—
SHFTUP	upshift rpm.	rpm
{ TRATIO(NGEAR)	transmission ratios	—
{ CT1(NGEAR)	friction coefficient	nt m
{ CT2(NGEAR)	friction coefficient	nt m/rpm
EMUT(NGEAR)	transmission efficiency	—
DRATIO	differential ratio	—
CD1	friction coefficient	nt m
CD2	friction coefficient	nt m/rpm
EMUD	differential efficiency	—
KTIRE	tire radius	m
CTIRE1	friction coefficient	—
CTIRE2	friction coefficient	—/km/hr
VMASS	vehicle mass	kg
DLI	drive line inertia	kg m ²
CDA	drag coefficient * area	m ²
GRAD	road gradient	—
V	vehicle speed	km/hr
LELT	run time interval for RKT	sec
TF	final time in simulation	sec
NPRNT	number of suppressed print times	—

Variables	Description	Units
GEAR	steady state gear	---
VMPS	vehicle speed	m/sec
RPMDO	differential output r.p.m.	rpm
TLFD	differential torque loss	nt m
RPMTO	transmission output r.p.m.	rpm
TLFT	transmission torque loss	nt m
RPMEM	motor rpm	rpm
FA	aerodynamic force	nt
FR	rolling resistance force	nt
FG	gradient force	nt
FNET ϕ	steady state net force	nt
TDO	differential output torque	nt m
TTO	transmission output torque	nt m
TSD	motor output torque	nt m
TEM ϕ	steady state motor torque intercept	nt m
VMASS2	effective vehicle vertical mass	kg
EMI2	effective motor inertia	kg m ²
K	print slip control flag	---
T	time in simulation	sec
$\dot{\gamma}(E)$	angular speed of engine	rad/sec
$\gamma(E)$	angular displacement of engine	rad
$\dot{\gamma}(S)$	angular speed of motor	rad/sec
$\dot{\gamma}DOT(1)$	angular acceleration of engine	rad/sec ²
$\dot{\gamma}DOT(2)$	angular speed of engine	rad/sec
$\dot{\gamma}DOT(3)$	angular acceleration of motor	rad/sec ²
RPMHE	engine r.p.m.	rpm
RPMEL	motor r.p.m.	rpm
V	vehicle speed	km/hr
A	vehicle acceleration	gEARTH

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DFRIV Subroutine for VSYS2

C-94

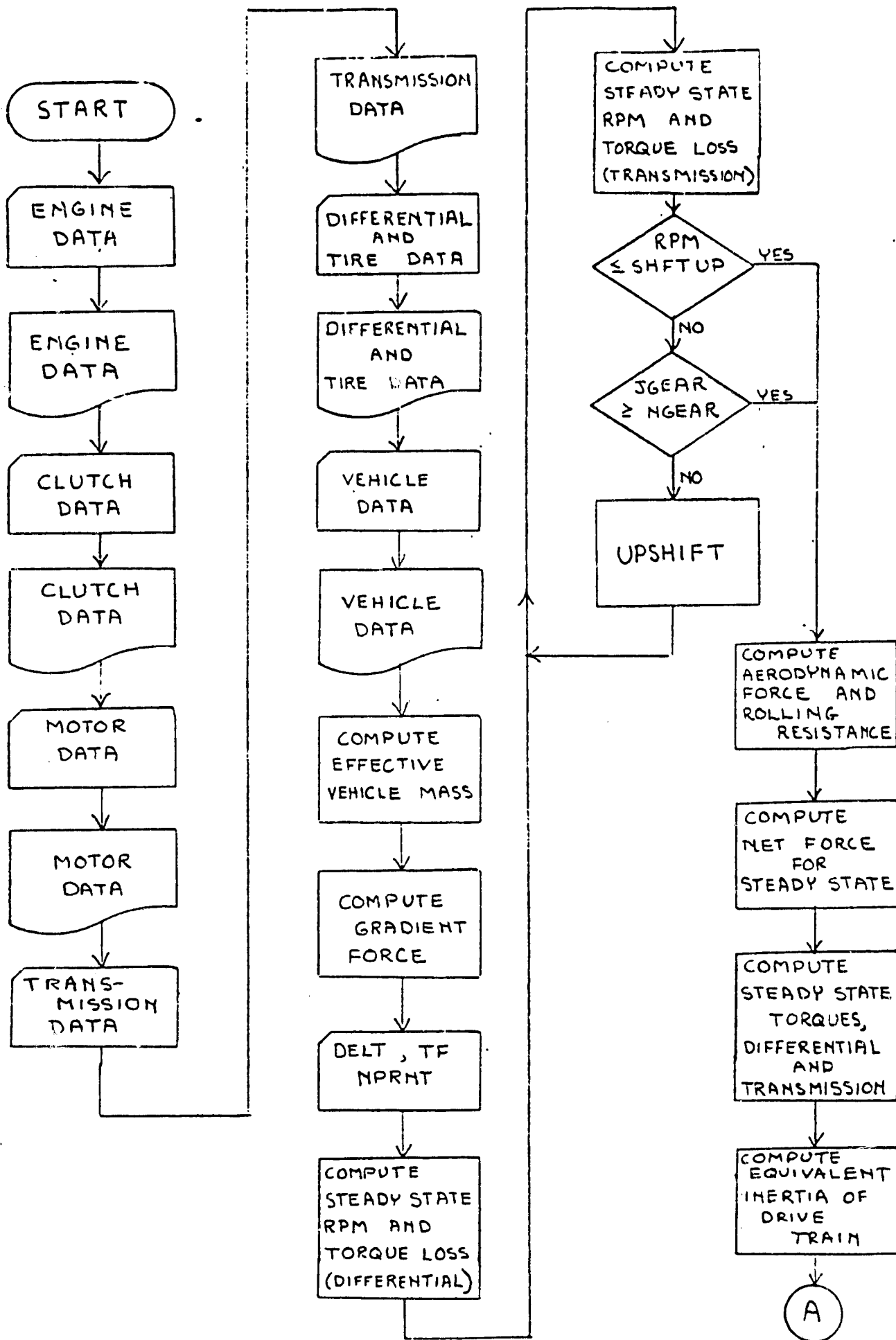
Variables	Description	Units
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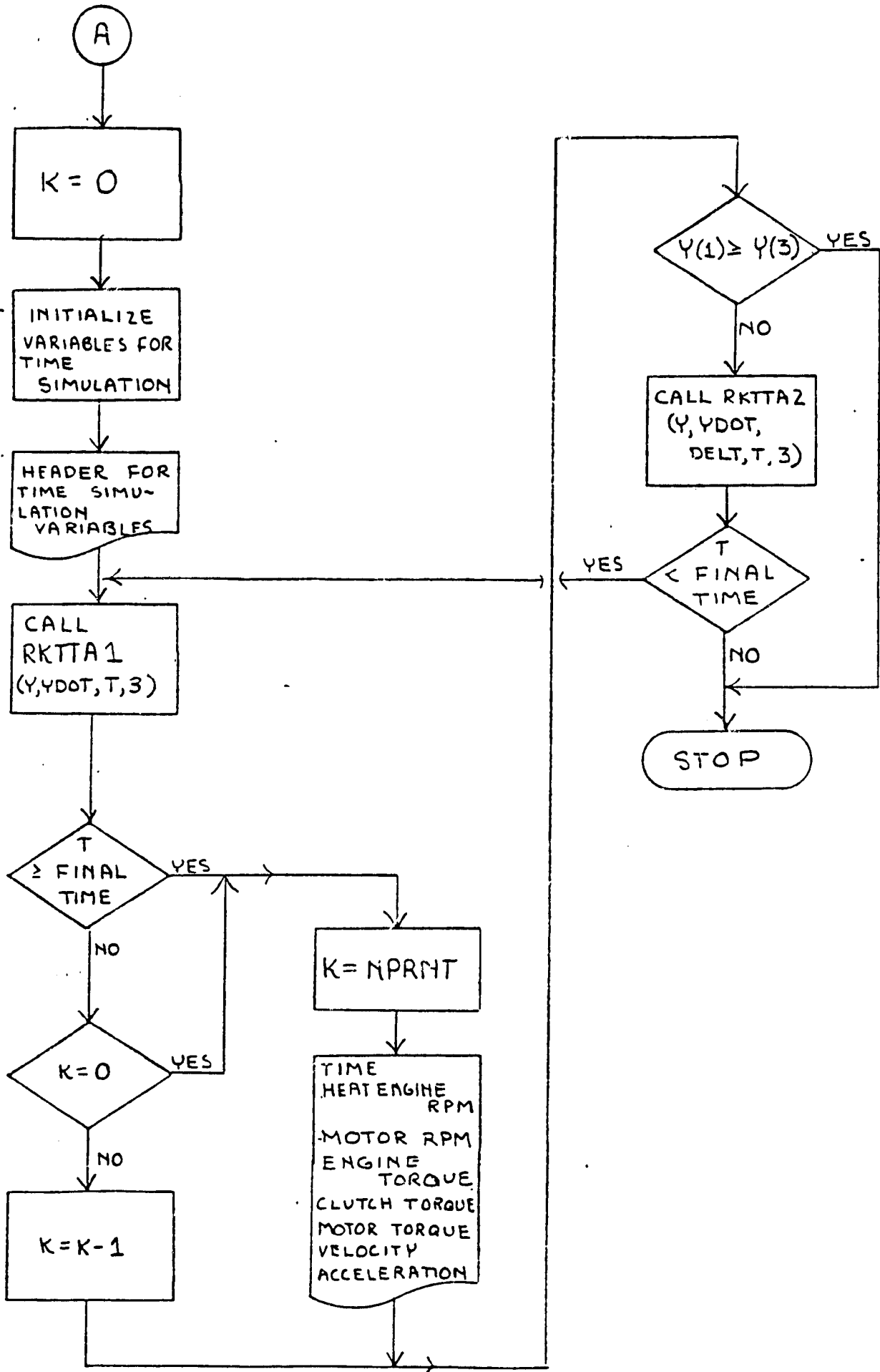
FORTRAN CODING FORM

GENERAL RESEARCH CORPORATION

PROGRAM VSYS2	NAME
ROUTINE Input for input	DATE 20 JULY 79
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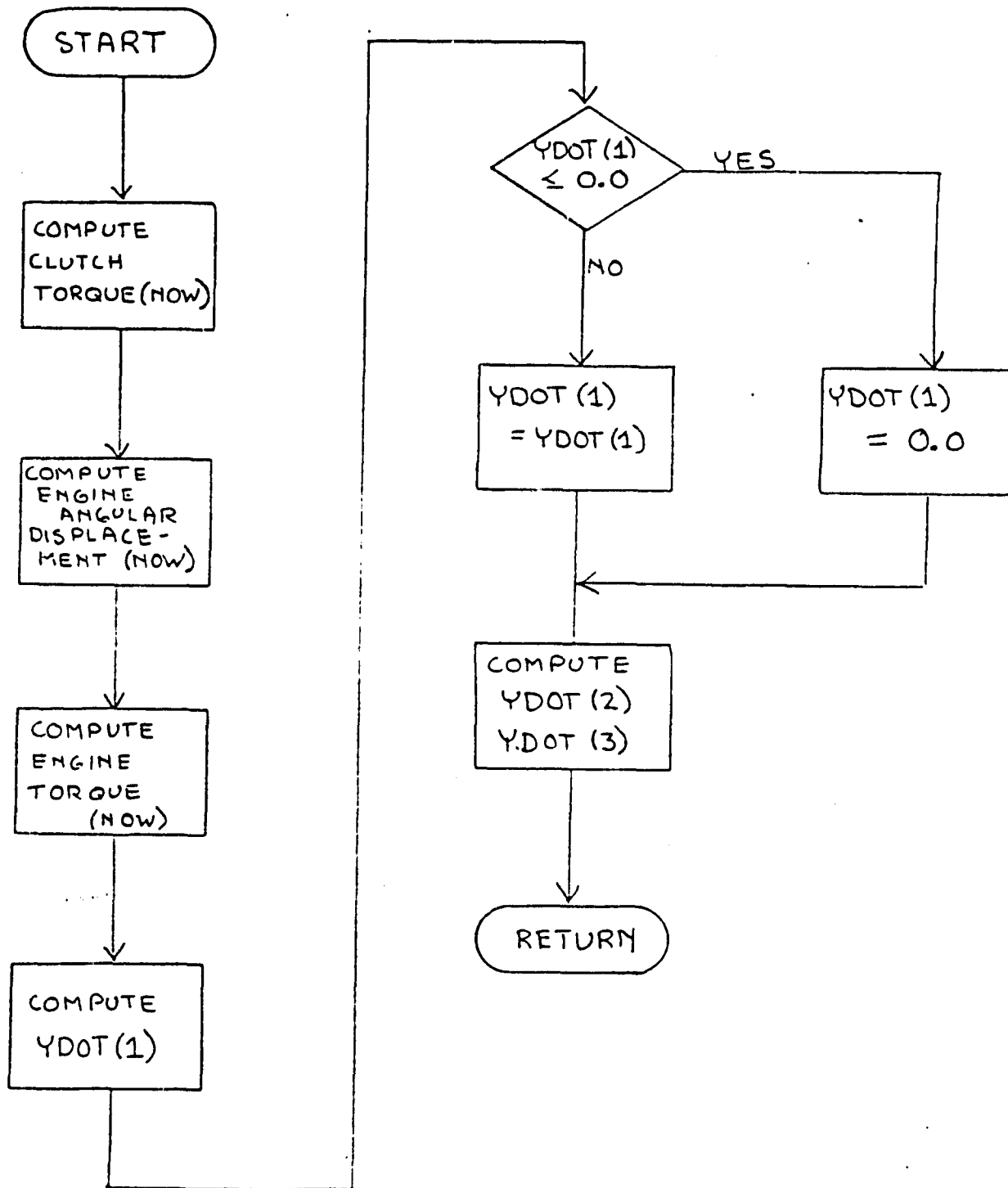
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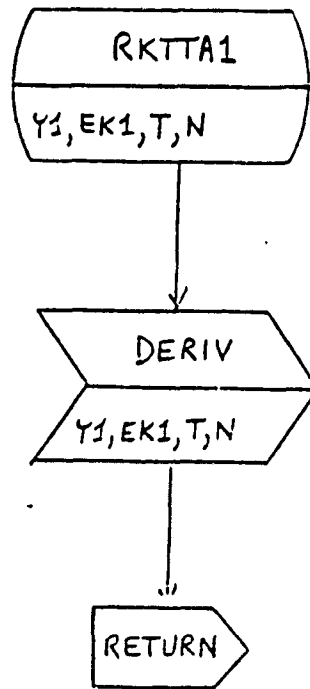


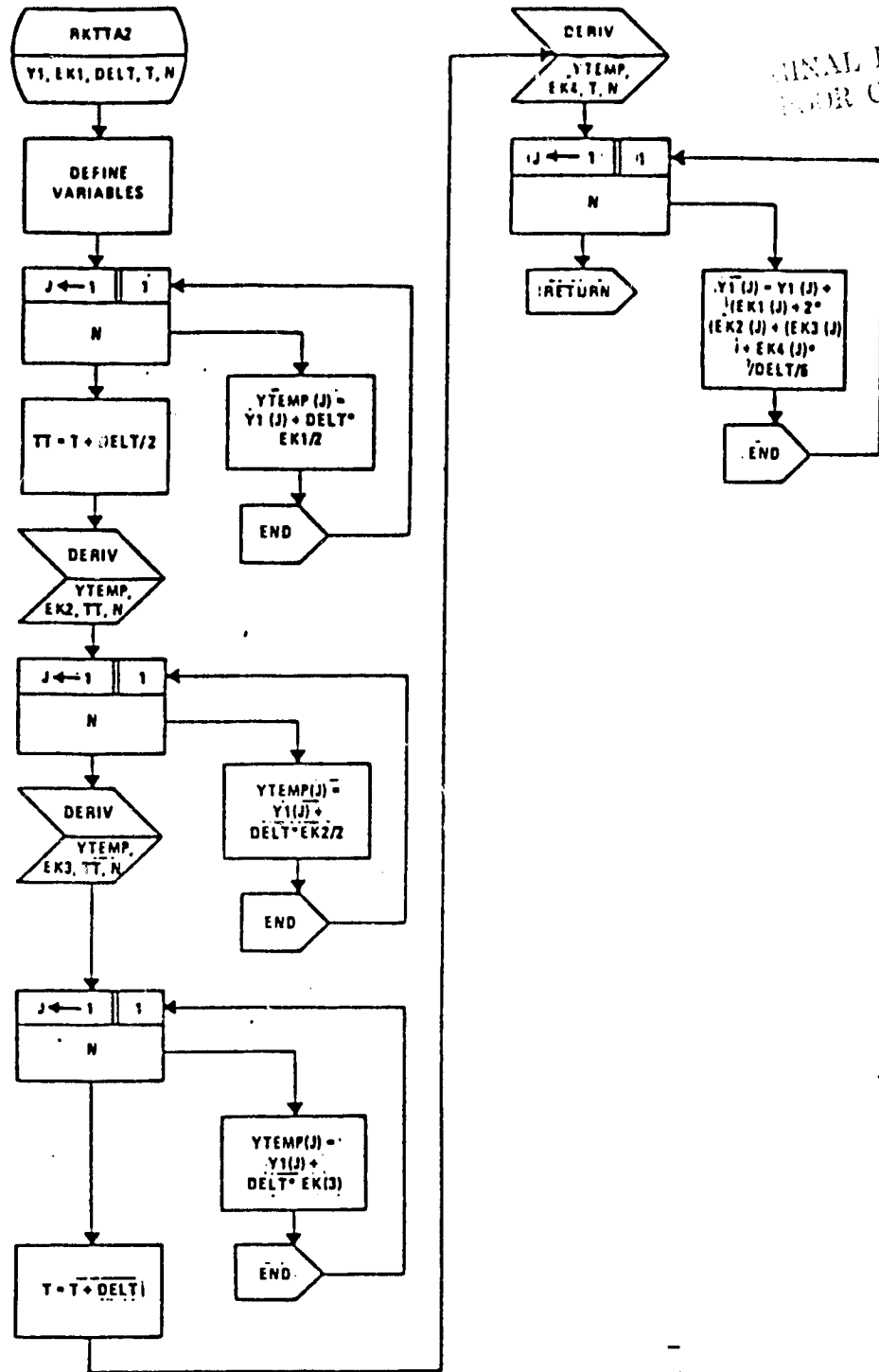


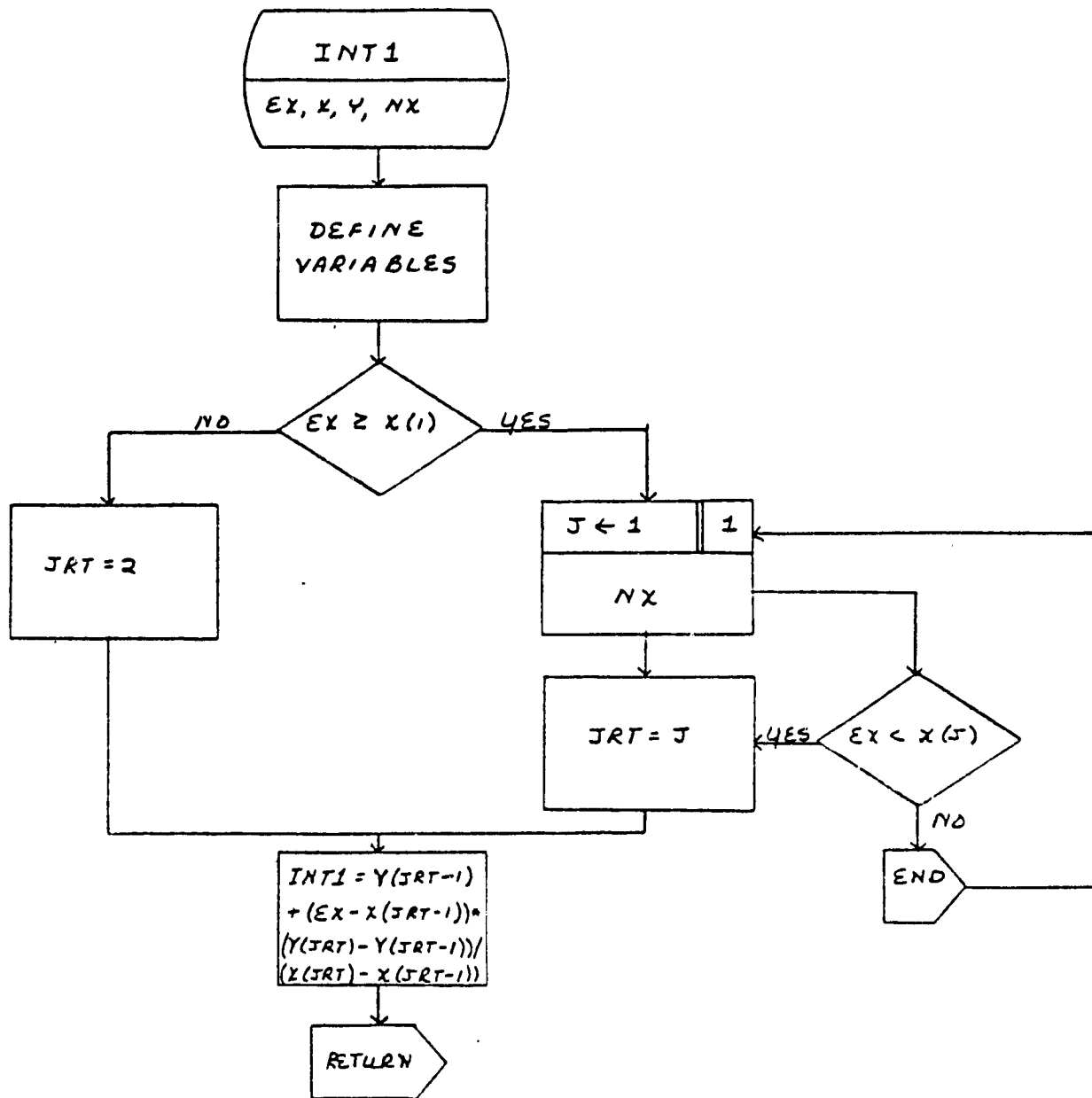
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GOLETA FORTRAN 1.3 * SEMI-AUTO 9FL * (01-10-73)

PROGRAM VSYS2

C
C THIS PROGRAM MODELS A HYBRID VEHICLE PROPULSION SYSTEM.
C THE ELECTRIC MOTOR IS PRODUCING TORQUE UNDER STEADY STATE
C CONDITIONS AND THE HEAT ENGINE CLUTCH IS ENGAGED.
C VHSYS2 VERSION HAS NO TORQUE CONVERTER.

C ALL UNITS IN MKS EXCEPT :
C THETA, THFTAN (REVOLUTIONS)
C V, VPL (KM. PER HR.)
C A, APL (G)
C RPM00, RPMTC (REV. PER MIN.)
C RPMHE, RPMEM (REV. PER MIN.)
C WPL, UPL (REV. PER MIN.)
C CM (NEWTON*METERS/PPM)
C CT2, CD2, SHFTUP, CTIPE2, TSP, TSPAR, CDA

000003 COMMON RTIPE,CD1,CD2,CRATIC,CT1(6),CT2(6),TRATIC(6),CDA,CTIRE1,
1CTIRE2,VMASS,EMUD,EMUT(6),NGEAR,DLI,GRAD,CM,HEI,EMI,
2VMASS2,FG,V,JGEAR,
3TSC,EMIZ,
4NTCL,TCL(10),TIME(10),NTPE,TPE(10),THETA(10),
5VMPS,RPMDC,TLFD,RPMTIC,TLFT,PPMTCO,FA,FR,FNET0,TDO,TTO,
6FTEM0,THETAN,
7TCLN,THEN,TEM,FNET,FAC
000003 REAL YDOT(3),Y(3),INT1

C
C INPUT ENGINE DATA

000003 READ 640,NTHE,HEI
000013 READ 610,(TPE(J),THETA(J),J=1,NTHE)
000039 PRINT 420,HEI
000036 PRINT 820,(TPE(J),THETA(J),J=1,NTHE)

C
C INPUT CLUTCH DATA

000053 READ 620,NTCL
000061 READ 610,(TCL(J),TIME(J),J=1,NTCL)
000076 PRINT 400
000102 PRINT 820,(TCL(J),TIME(J),J=1,NTCL)

C
C INPUT MOTOR DATA

000117 READ 610,CM,EMI
000127 PRINT 430,CM,EMT

C
C INPUT TRANSMISSION DATA

000137 READ 640,NGEAR,SHFTUP
000147 READ 610,(TRATIC(J),CT1(J),CT2(J),EMUT(J),J=1,NGEAR)
000170 PRINT 840
000174 PRINT 845
200 PRINT 810,(TRATIC(J),CT1(J),CT2(J),EMUT(J),J=1,NGEAR)
000221 PRINT 850,SHFTUP

C

GOLETA FCRTFAK 1.3 * SEMI-AUTO RFL * (01-10-73)

VSY52

```

)      C      INPUT DIFFERENTIAL AND TIRE DATA
      C
0227   READ 610,DRATIO,CD1,CD2,EMUD,RTIRE,CTIRE1,CTIRE2
UD0251 PRINT 875
) 000255 PRINT 880
000261 PRINT 885,DRATIO,CD1,CD2,EMUD,RTIRE,CTIRE1,CTIRE2

      C
      C      INPUT VEHICLE DATA
      C
000303 READ 610,VMASS,DLI,CDA,GRAC,V
000321 PRINT 890,VMASS,DLI,CDA
000333 PRINT 925,GRAC,V
000343 VMAS52=VMASS+DLI/RTIRE**2

      C
      C      GRADIENT-
      C
000346 FG=9.807*VMASS*SIN(ATAN(GRAC))

      C
      C      INPUT RUN DATA
      C
000355 READ 630,DELT,TF,NPRNT

      C
      C      COMPUTE STEADY STATE CONDITIONS
      C
000366 JGEAR=1
000367 VMPS=V/3.6
000371 RPMDC=9.5492967*VMPS/RTIRE
      1373 TLFD=CD1+CD2*RPMDC
      0376 RPMTC=RPMDC*DRATIO
000400 15 CONTINUE
000400 TLFT=CT1(JGEAR)+CT2(JGEAR)*RPMTC
000404 RPMEM=RPMTC*TRATIO(JGEAR)

      C
      C      UPSHIFT IF NECESSARY
      C
000406 IF((RPMEM .LE. SHFTUP).OR.(JGEAR.GE.NGEAR))GO TO 18
000417 JGEAR=JGEAR+1
000420 GO TO 15
000421 18 CONTINUE

      C
      C      AERODYNAMIC -
      C
000421 FA=0.6125*CDA*VMPS**2

      C
      C      ROLLING RESISTANCE -
      C
000424 FR=9.807*VMASS*(CTIRE1+CTIRE2*V)

      C
      C      ACCELERATION -
      C
000430 FNET0=FA+FG+FR
000433 T00=FNET0*RTIRE

      C
      C      DIFFERENTIAL -
      C

```

GOLETA FCFTFRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

VSYSP

```

000435      TTD=TD0/(EMUC*DRATIO)+TLFD
          C
          C      TRANSMISSION -
          C
000441      TSO =TTO/(EMUT(JGEAR)*TRATIO(JGEAR))+TLFT
000446      TEMO=TSO+CM*RFMEM
          C
          C      COMPUTE EQUIVALENT INERTIA OF DRIVE TRAIN
          C
000451      EMI2=EMI+(VMASS2*RTIRE**2.
          1/(EMUD*EMUT(JGEAR)*(DRATIO*TRATIO(JGEAR))**2.))
          C
          C      SET INITIAL CONDITIONS
          C
000466      K=0
000467      T=0.0
000470      Y(1)=0.0
000471      Y(2)=0.0
000472      Y(3)=.104719755*RPMEF
000475      PRINT 700
000500      80 CONTINUE
000500      CALL RKTTA1(Y,YDOT,T,3)
000503      IF((T.GE.TF).OR.(K.EQ.0))GO TO 107
000513      K=K-1
000514      GO TO 109
000514      107 CONTINUE
          9514      K=NPRINT
          C
          C      TIME TO PRINT RESULTS -
          C
000515      RPMEF=Y(1)/.104719755
000517      RPMEM=Y(3)/.104719755
000521      V=Y(3)*RTIRE*3.6/(DRATIO*TRATIO(JGEAR))
000526      A=YDOT(3)*RTIRE/(DRATIO*TRATIO(JGEAR)*9.807)
000533      PRINT 885,T,RPMEF,RPMEM,THEN,TCLN,TEM,V,A
000556      109 CONTINUE
          C
          C      INTEGRATE TO NEXT TIME STEP
          C
000556      IF(Y(1).GE.Y(3))GO TO 190
000561      CALL RKTTA2(Y,YDOT,DELTA,T,3)
000564      IF(T.LT.TF)GO TO 80
000567      190 CONTINUE
000567      200 STOP
          C
          C      FORMAT STATEMENTS
          C
000571      400 FORMAT(1H0,*CLUTCH DATA*//5X,*CLUTCH TO.*,6X,*TIME*)
000571      420 FORMAT(1H0,*ENGINE DATA*//5X,*ENGINE INERTIA =*,E16.6//
          15X,*ENGINE TO.*,6X,*THETA*)
000571      430 FORMAT(1H0,*MOTOR DATA*//5X,*MOTOR SPEED DROOP =*,E16.6,4X,
          1*MOTOR INERTIA =*,E16.6)
          571      610 FORMAT(7F10.4)
000571      620 FORMAT(7I10)
000571      630 FORMAT(2F10.4,2I10)

```

GOLETA FCPTFAN 1.3 * SEMJ-AUTO PFL * (01-10-73)

VSYST

```

000571      640 FORMAT (I10,6F10.4)
   0571      700 FORMAT (1H0,4X,*TIME*, 7X,*ENGINE RPM*,3X,*MOTOR RPM*,
      14X,*ENGINE TG.*,3X,*CLUTCH TG.*,3X,
      2*MOTOR TG.*,4X,*SPEED*,8X,*ACCEL.*)
000571      810 FORMAT (1H ,4E16.6)
000571      820 FORMAT (1H ,2E16.6)
000571      840 FORMAT (1H0,12HGGEARBOX DATA)
000571      845 FORMAT (1H0,4X,10HGGEAR RATIO,6X,22HSPIN LOSS COEFFICIENTS,10X
      1,*EFFICIENCY*)
000571      850 FORMAT (/TE,*UPSHIFT RPM = *,E16.6)
000571      875 FORMAT (1H0,18HAXLE AND TIRE DATA )
000571      880 FORMAT (1H0,4X,14HFIN. DR. RATIO,2X,22HSPIN LOSS COEFFICIENTS,10X
      1,*EFFICIENCY*,6X,*ROLLING RADIUS*,2X,*ROLL. RESIST. COEFFICIENTS
000571      885 FORMAT (1H ,7E16.6)
000571      886 FORMAT (1H ,F12.2,9E13.4)
000571      890 FORMAT (1H0,14HVEHICLE MASS =,E16.6
      1,5X,*DRIVE LINE INERTIA = *,E16.6
      2,5X,19H(DRAG COEFF.)*AREA =,E16.6)
000571      925 FORMAT (1H0,16HCYCLE GRADIENT =,E10.3,
      1*STEADY STATE SPEED =*,E10.3)
000571      END

```

GOLETA FORTFAA 1.3 * SEMI-AUTO PFL * (01-10-73)

```

          SUBROUTINE CEPIV(Y,YDOT,T,N)
C
C      Y(1) IS ENGINE SPEED
C      Y(2) IS ENGINE ANGULAR DISPLACEMENT
C      Y(3) IS MOTOR SPEED
000007      COMMON RTIME,CD1,CD2,DRATIC,CT1(6),CT2(6),TRATIO(6),CDA,CTIRE1,
1CTIRE2,VMASS,EMUD,FMUT(6),NGEAR,CLI,GRAD,CM,HEI,EMI,
2VMASS2,FG,V,JGEAR,
3TSO,EMI2,
4NTCL,TCL(10),TIME(10),NTHE,THE(10),THETA(10),
5VMPS,PPMDC,TLFD,RPMTG,TLFT,RPMTG,FA,FR,FNETD,TCD,TTO,
6TEM0,THETAN,
7TCLN,THEN,TEM,FNET,FAC
000007      REAL Y(2),YDOT(2),INT1
C
000007      TCLN=INT1(T,TIME,TCL,NTCL)
000015      THETAN=Y(2)/6.2831852
000017      THEN=INT1(THETAN,THETA,THE,NTHE)
000023      YDOT(1)=(THEN+TCLN)/HEI
C
C      NO NEGATIVE ENGINE ROTATIONAL ACCELERATION
C
000031      YDOT(1)=AMAX1(0.0,YDOT(1))
000035      YDOT(2)=Y(1)
000036      TEM=TEM0-CM*Y(3)/.104719755
   0042      YDOT(3)=(TEM-TCLN-TSO)/EMI2
   0047      RETURN
000047      END

```

GOLETA FCPTFAN 1.3 * SEMI-AUTO RFL * (01-10-73)

```

) 00007
) 0007
) 000010
) 000011

SUBROUTINE PKTTA1(Y1,EK1,T,N)
REAL Y1(20),EK1(20)
CALL DERIV(Y1,EK1,T,N)
RETURN
END
```

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GOLETA FCRTF/A 1.3 * SEMI-AUTO RFL * (01-10-73)

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) 00010      SUBROUTINE RKTTA?(Y1,EK1,DELT,T,N)
00011      REAL Y1(20),Y2(20),YTEMP(20),EK1(20),EK2(20),EK3(20),EK4(20)
00012      DO 50J=1,N
00013      YTEMP(J)=Y1(J)+DELT*EK1(J)/2.
00014      50 CONTINUE
00015      TT=T+DELT/2.
00016      CALL DERIV(YTEMP,EK2,TT,N)
00017      DO 60J=1,N
00018      YTEMP(J)=Y1(J)+DELT*EK2(J)/2.
00019      60 CONTINUE
00020      CALL DERIV(YTEMP,EK3,TT,N)
00021      DO 70J=1,N
00022      YTEMP(J)=Y1(J)+DELT*EK3(J)
00023      70 CONTINUE
00024      T=T+DELT
00025      CALL DERIV(YTEMP,EK4,T,N)
00026      DO 80J=1,N
00027      Y1(J)=Y1(J)+(EK1(J)+2.*(EK2(J)+EK3(J))+EK4(J))*(DELT/6.)
00028      80 CONTINUE
00029      RETURN
00030      END
```


GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

REAL FUNCTION INT1(EX,Y,NX)

INT1 INTERPOLATES IN ONE VARIABLE

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```
C
C
C
000007 REAL X(10),Y(10)
000007 IF(EX.GE.X(1))GO TO 5
000011 JRT=2
000012 GO TO 20
000013 5 DO 10 J=1,NX
000015 IF(EX.LT.Y(J))GO TO 15
000020 10 CONTINUE
000022 15 JRT=J
000024 20 INT1=Y(JRT-1)+(EX-X(JRT-1))*(Y(JRT)-Y(JRT-1))/(X(JRT)-X(JRT-1))
000040 RETURN
000041 END
```

ENGINE DATA

ENGINE INERTIA = 6.250000E-02
ENGINE TC.
INERTIA
-1.000000E+01
-1.000000E+01
5.500000E+00
5.000000E+00

CLUTCH DATA

CLUTCH TC.
TYPE
0.
1.000000E+02

MOTOR DATA

MOTOR SPEED SPOOP = 4.400000E-01 MOTOR INERTIA = 1.000000E-01

GEARBOX DATA

GEAR RATIO SPIN LOSS COEFFICIENTS EFFICIENCY
2.450000E+00 0. 0. 9.200000E-01
1.450000E+00 0. 0. 9.200000E-01
1.000000E+00 0. 0. 9.400000E-01

UPSHIFT PPM = 4.000000E+01

WHEEL AND TIRE DATA

FIN. CR. RATIO SPIN LOSS COEFFICIENTS ROLLING RESIST. COEFFICIENTS
4.100000E+00 0. 0. 9.600000E-01 1.000000E-02 0.

VEHICLE MASS = 2.200000E+03 DRIVE LINE INERTIA = 5.400000E+00 ROAD COEFF. ROAD = 9.700000E-01
CYCLE GRADIENT = 0. STEADY STATE SPEED = 2.0000E+01

TIME	ENGINE OCV	MOTOR OCV	ENGINE TC.	CLUTCH TC.	MOTOR TC.	SPEED	ACCEL.
0.	0.	3.6193E+01	-1.0000E+01	0.	2.4377E+01	7.0000E+01	-3.6311E-10
2.00E-02	0.	3.6192E+01	-1.0000E+01	2.0000E+00	2.4377E+01	5.0000E+01	-1.4000E-01
4.00E-02	0.	3.6191E+01	-1.0000E+01	4.0000E+00	2.4377E+01	5.0000E+01	-2.0010E-02
6.00E-02	0.	3.6190E+01	-1.0000E+01	6.0000E+00	2.4377E+01	5.0000E+01	-4.4450E-02
8.00E-02	0.	3.6189E+01	-1.0000E+01	8.0000E+00	2.4377E+01	5.0000E+01	-5.0021E-02
1.00E-01	0.	3.6188E+01	-1.0000E+01	1.0000E+01	2.4377E+01	5.0000E+01	-7.0211E-02
1.20E-01	1.0350E+00	3.6179E+01	-1.0000E+01	1.2000E+01	2.4377E+01	5.0000E+01	-9.7000E-02
1.40E-01	1.2221E+01	3.6170E+01	-1.0000E+01	1.4000E+01	2.4377E+01	5.0000E+01	-1.1720E-01
1.60E-01	2.7502E+01	3.6161E+01	-1.0000E+01	1.6000E+01	2.4377E+01	5.0000E+01	-1.1500E-02
1.80E-01	4.9923E+01	3.6152E+01	-1.0000E+01	1.8000E+01	2.4377E+01	5.0000E+01	-1.2067E-02
2.00E-01	7.5044E+01	3.6143E+01	-1.0000E+01	2.0000E+01	2.4377E+01	5.0000E+01	-1.2710E-02
2.20E-01	1.1001E+02	3.6134E+01	-1.0000E+01	2.2000E+01	2.4377E+01	5.0000E+01	-1.3410E-02
2.40E-01	1.4957E+02	3.6125E+01	-1.0000E+01	2.4000E+01	2.4377E+01	5.0000E+01	-1.4150E-02
2.60E-01	2.4758E+02	3.6116E+01	-1.0000E+01	2.6000E+01	2.4377E+01	5.0000E+01	-1.4950E-02
2.80E-01	3.7359E+02	3.6107E+01	-1.0000E+01	2.8000E+01	2.4377E+01	5.0000E+01	-1.5810E-02
3.00E-01	5.0000E+02	3.6098E+01	-1.0000E+01	3.0000E+01	2.4377E+01	5.0000E+01	-1.6730E-02
3.20E-01	6.4000E+02	3.6089E+01	-1.0000E+01	3.2000E+01	2.4377E+01	5.0000E+01	-1.7720E-02
3.40E-01	8.0000E+02	3.6080E+01	-1.0000E+01	3.4000E+01	2.4377E+01	5.0000E+01	-1.8780E-02
3.60E-01	9.9000E+02	3.6071E+01	-1.0000E+01	3.6000E+01	2.4377E+01	5.0000E+01	-2.0000E-02
3.80E-01	1.2000E+03	3.6062E+01	-1.0000E+01	3.8000E+01	2.4377E+01	5.0000E+01	-2.1390E-02
4.00E-01	1.4000E+03	3.6053E+01	-1.0000E+01	4.0000E+01	2.4377E+01	5.0000E+01	-2.2950E-02

4.60E-01	1.6425E+02	3.6077E+01	3.7900E+01	4.4000E+01	2.9755E+01	6.9744E+01	-2.9161E-02
4.60E-01	1.3111E+03	3.6050E+01	5.0000E+01	4.6000E+01	1.0232E+01	5.9744E+01	-3.0290E-02
4.80E-01	1.6095E+03	2.6044E+01	5.0000E+01	4.4000E+01	3.0720E+01	6.9721E+01	-3.1422E-02
5.00E-01	1.9120E+03	1.6037E+01	5.0000E+01	5.0000E+01	3.1242E+01	5.9692E+01	-3.2544E-02
5.20E-01	2.2207E+03	1.6024E+01	5.0000E+01	5.7000E+01	1.1771E+01	6.9674E+01	-3.3654E-02
5.40E-01	2.5354E+03	3.6012E+01	5.0000E+01	5.4000E+01	1.2723E+01	5.9651E+01	-3.4740E-02
5.60E-01	2.8563E+03	1.6000E+01	5.0000E+01	5.6000E+01	1.2850E+01	6.9624E+01	-3.5810E-02
5.80E-01	3.1832E+03	1.6000E+01	5.0000E+01	5.8000E+01	1.3474E+01	6.9600E+01	-3.6890E-02
6.00E-01	3.5163E+03	3.6077E+01	5.0000E+01	6.0000E+01	1.6175E+01	5.9574E+01	-3.7944E-02

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CI.3 CRASH SIMULATION PROGRAM (CRASH)

1. Program Description

CRASH is a program which simulates the impact response of a general non-linear spring/mass system. The masses are constrained to translation along one axis; i.e., planar or 3 dimensional translation and rotations are not simulated. The springs which interconnect the masses can be nonlinear and have different characteristics in unloading than they do in loading; i.e., they can dissipate energy in heat as well as storing it. The equation of motion of the masses are solved using a Runge-Kutta integration routine. By appropriately modelling a vehicle (or vehicles) as such a spring/mass system, the vehicle response in a barrier or vehicle-to-vehicle impact can be simulated.

A 3.2 Equations

Equation of Motion for i^{th} Mass

$$M_i \frac{d^2 x_i}{dt^2} = \sum_{j \neq i} F_{ij} - \sum_{i \neq j} F_{ji} \quad ; \quad \begin{matrix} i=1, \dots, n, \\ j=0, \dots, n \end{matrix}$$

where n is the number of masses in the system and F_{ij} is the force generated by a spring coupling mass i to mass j . The sign convention on the F_{ij} is such that $F_{ij} > 0$ if it is in a direction to accelerate mass i and decelerate mass j . See Figure A 3-1 for an example of the nomenclature and sign conventions.

Generation of Spring Forces

$$F_i = \begin{cases} f_{ij} (x_j - x_i), & \text{loading with } x_j - x_i \geq x_{sav} \\ \text{MAX} (0, f (x_{sav}) - \frac{dF}{dx} (x_{sav} - (x_j - x_i))) & , \\ & \text{unloading or loading with } x_j - x_i < x_{sav} \end{cases}$$

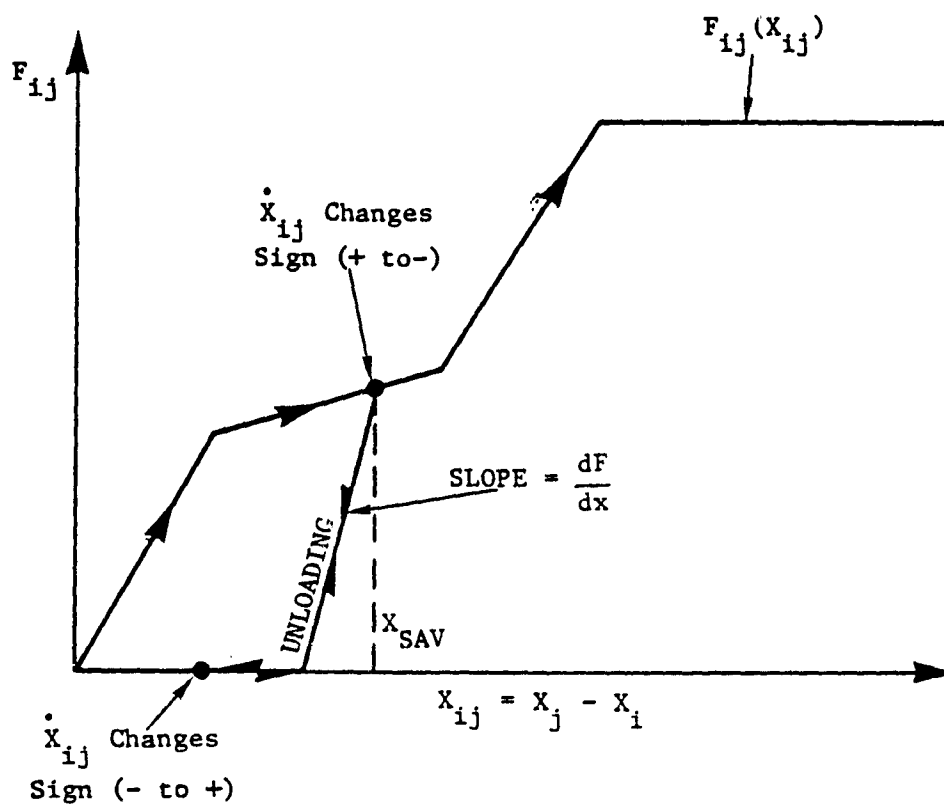


Figure A3-1 Generation of Generalized Non-Linear Spring Forces

where x_{sav} is the last value of $x_j - x_i$ at which unloading started (i.e., $\dot{x}_j - \dot{x}_i$ changed sign from positive to negative) and $\frac{dF}{dx}$ is the unloading slope. See Figure A for an illustration of how F_{ij} is generated. Note that, if there is a spring element between M_i and M_j such that the force can go negative for negative values of deflection, it is necessary to represent it as two springs. For example, the coupling between M_1 and M_2 in Figure A would be represented by two functions f_{12} and f_{21} .

CRASH

C-115

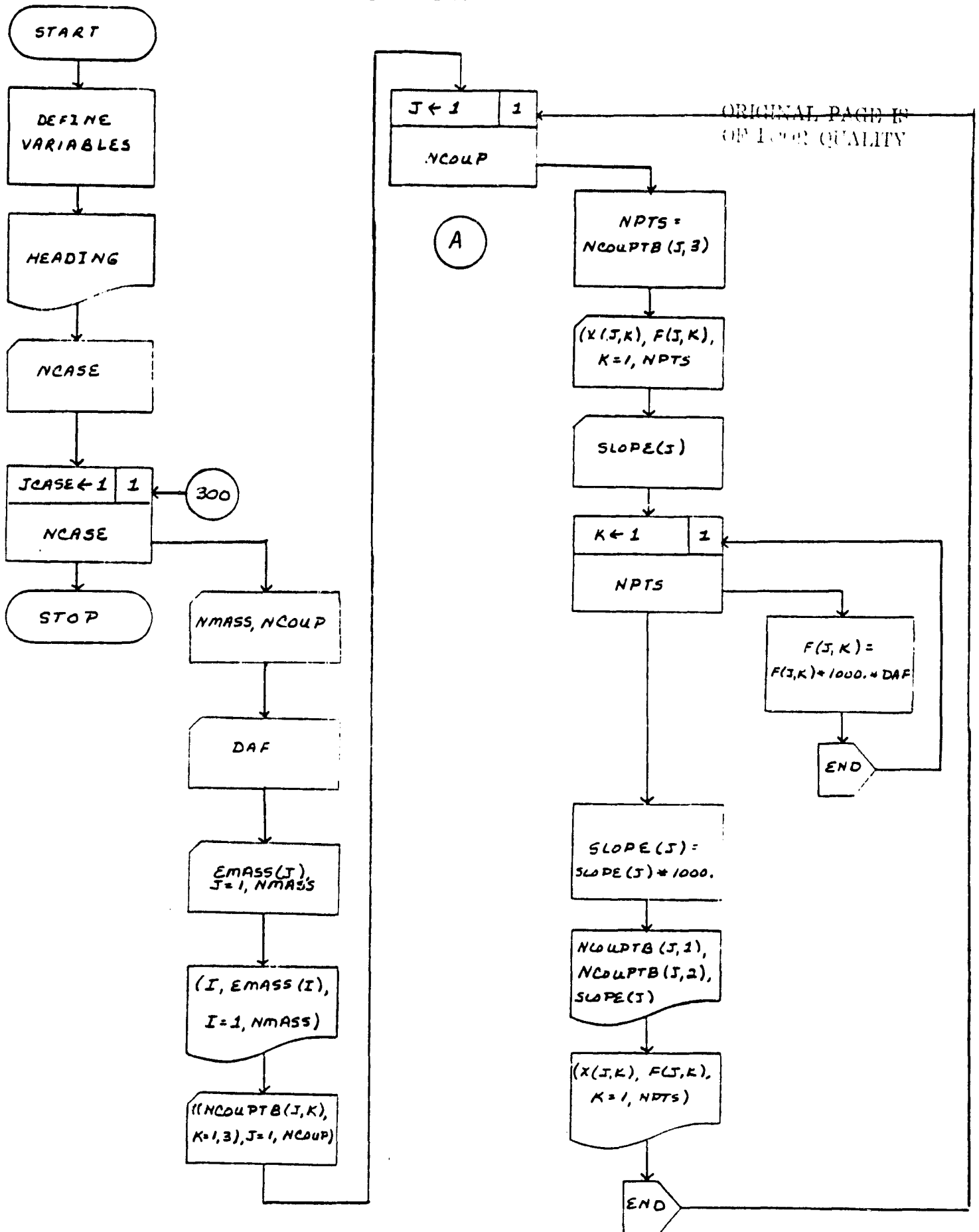
PARAMETERS		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	NCASE		NUMBER OF CASES
	NMASS		NUMBER OF MASSES
	NCOUP		NUMBER OF COUPLINGS
	DAF		DYNAMIC AMPLIFICATION FACTOR
M	EMASS(10)	KG	MASS OF ELEMENTS
	NCOUPTB(50,3)		COLUMNS 1 AND 2 CONTAIN MASS NUMBERS OF COUPLED MASSES, THIRD COLUMN CONTAINS NUMBER OF VALUES IN F AND X ARRAYS FOR SPECIFIED COUPLING
x_i	X(50,10)	M	DEFLECTION VALUES FOR EACH COUPLING
F_{ij}	F(50,10)	N/m	FORCE VALUES FOR FORCE DEFLECTION CHARACTERISTICS FOR EACH COUPLING
dF/dx	SLOPE(50)		SLOPE OF LINE ALONG WHICH UNLOADING OCCURS FOR EACH COUPLING
	TF	SEC	FINAL TIME
	DELT	SEC	TIME INCREMENT
	NPRNT		FREQUENCY OF OUTPUT PRINTING (IN RELATION TO TIME STEP)
	V0	m/sec	INITIAL VELOCITY

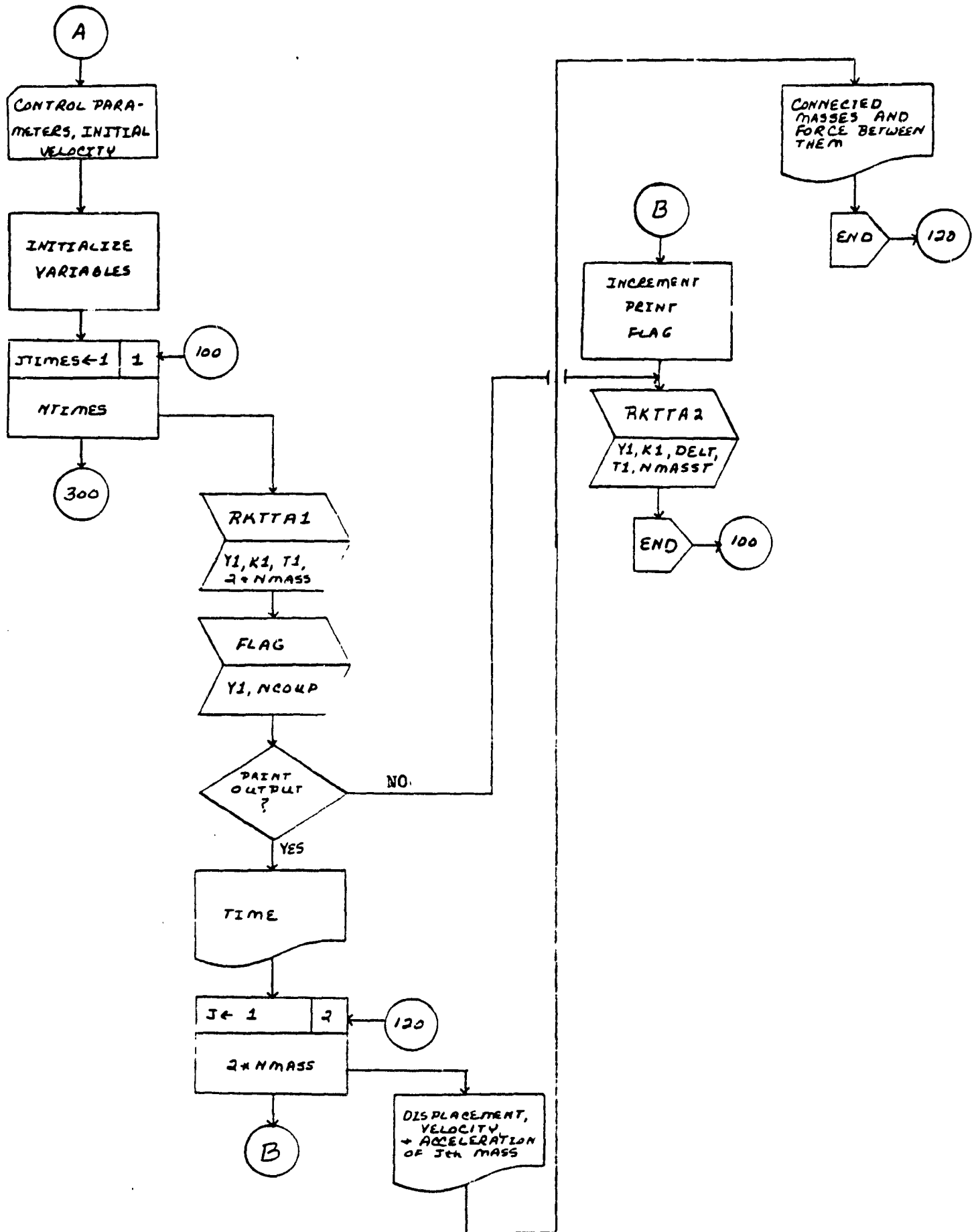
VARIABLES		UNITS	DESCRIPTION
EQUATION	PROGRAM		
$v_j - v_i$	DDELX	m/sec	INSTANTANEOUS VALUE OF VELOCITY FOR EACH COUPLING
	DELX(50)	m	INSTANTANEOUS VALUE OF DEFORMATION FOR EACH COUPLING
d^2x_i/dt^2	{DY(1,3,...19)	m/sec	VELOCITY OF MASS (1, 2, ... 10)
	{Y1(2,4,...20)	m/sec	
$f(x_{SAV})$	DY(2,4,...20)	m/sec ²	ACCELERATION OF MASS (1, 2, ... 10)
	FSAV(50)	n/m	VALUE OF FORCE AT POINT WHERE UNLOADING BEGINS
x_{SAV}	FT(50)	n/m	INSTANTANEOUS VALUE OF FORCE EXERTED FOR EACH COUPLING
	IFLAG(50)		FLAGS OCCURRENCE OF UNLOADING FOR EACH COUPLING (UNLOADING = -1, LOADING = 1)
	K1(20)		STORAGE FOR VARIABLES OF INTEGRATION
	NMASST		2 * NUMBER OF MASSES
	NTIMES		NUMBER OF TIME STEPS
	XSAV(50)	m	VALUE OF DEFORMATION AT WHICH UNLOADING BEGINS
	Y1(1,3,...19)	m	DISPLACEMENT OF MASS (1, 2, ... 10)

FORTRAN CODING FORM

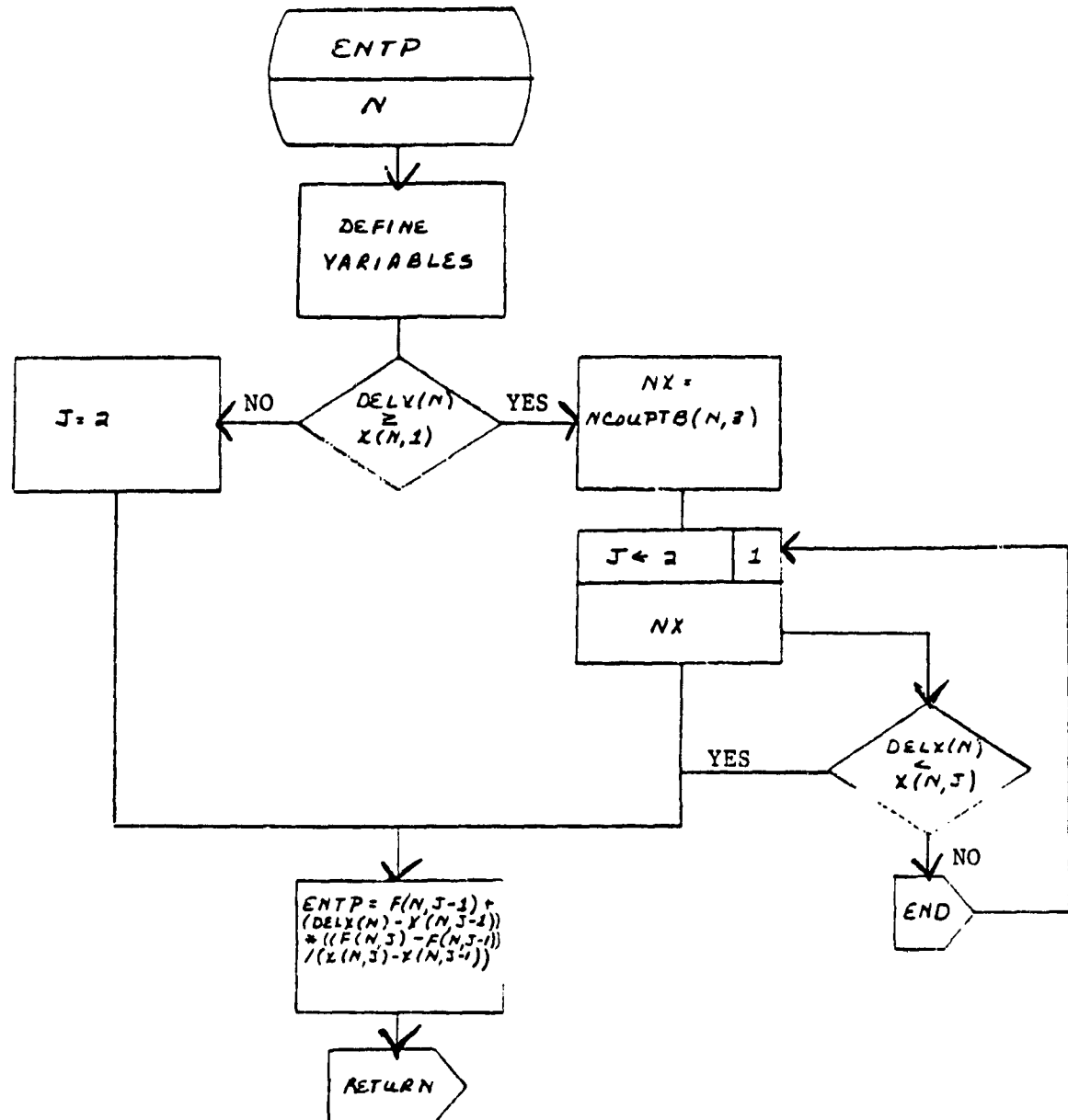
PROGRAM CRASH	NAME
ROUTINE Input Format	DATE
	PAGE OF

STATEMENT NO.	FORTRAN STATEMENT		SERIAL NUMBER
	1 = ONE I = ALPHA I	2 = TWO Z = ALPHA Z	
1	0 ZERO 0 ALPHA 0		
2	MMASS		
3	DAF		
4	EMASS(1,1)		
5	NCOUTP(1,1)		
6	X(1,1)		
7	SLOPE(1,1)		
8	TIME		
9	MPRINT		
10	Y0		
11	NPM		
12	NPMASS(1,1)		
13			
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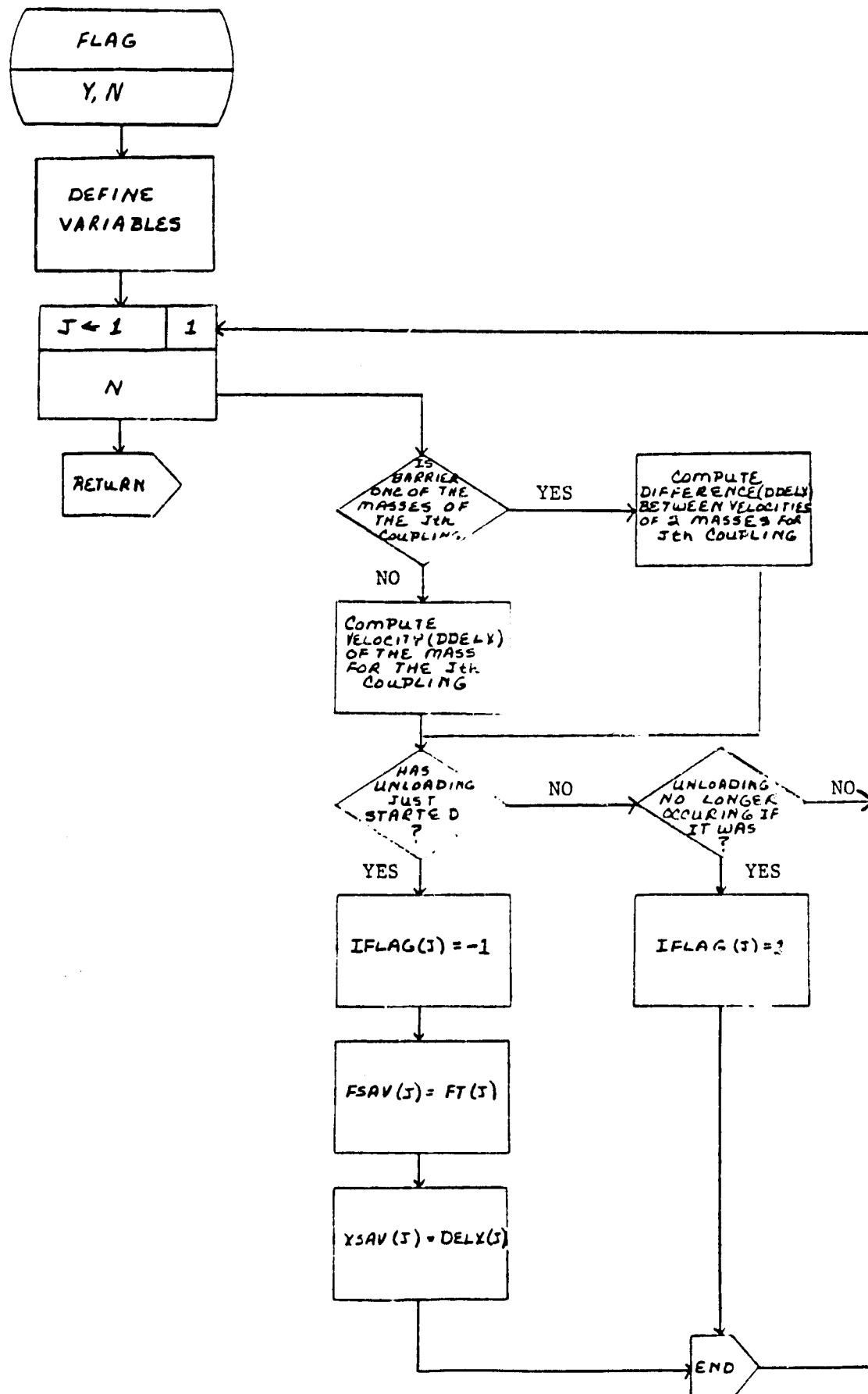




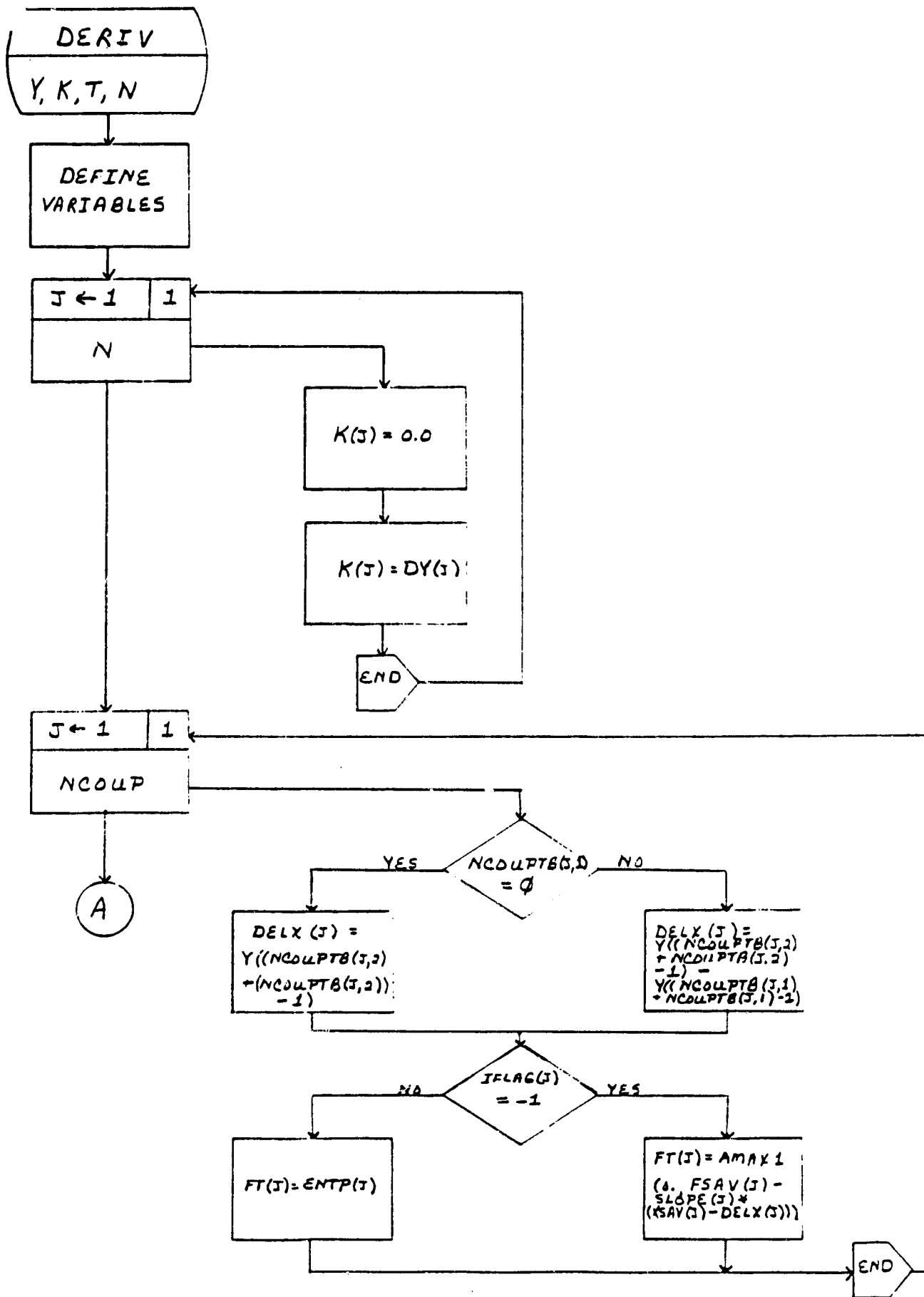
REAL FUNCTION ENTP

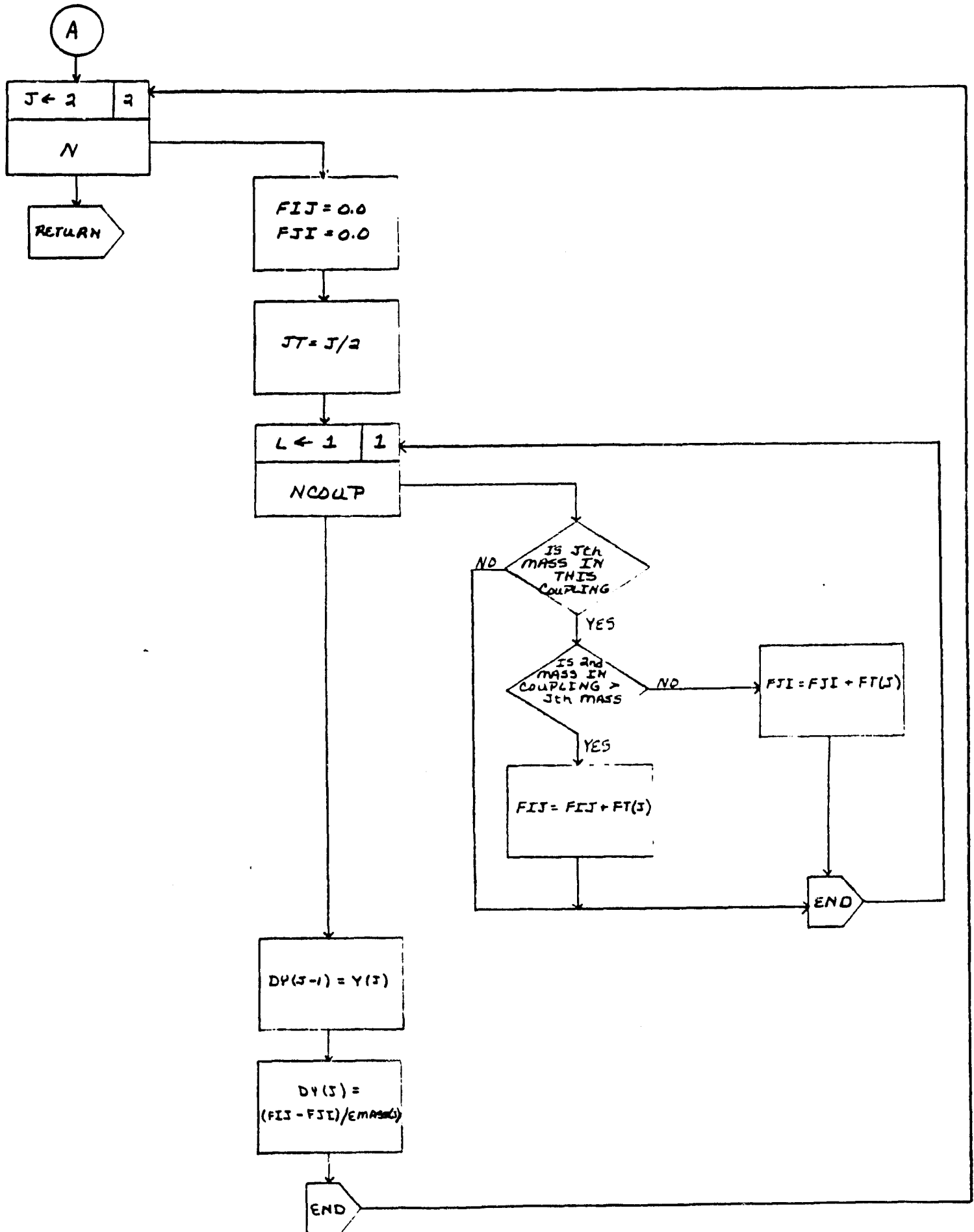


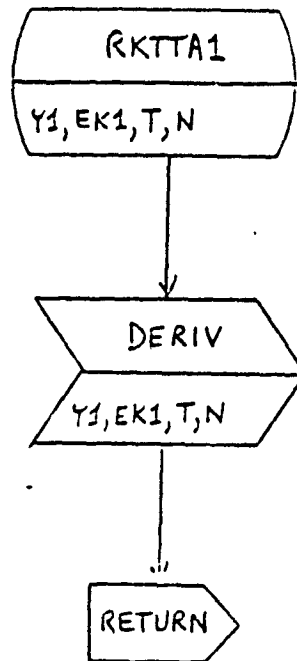
SUBROUTINE FLAG

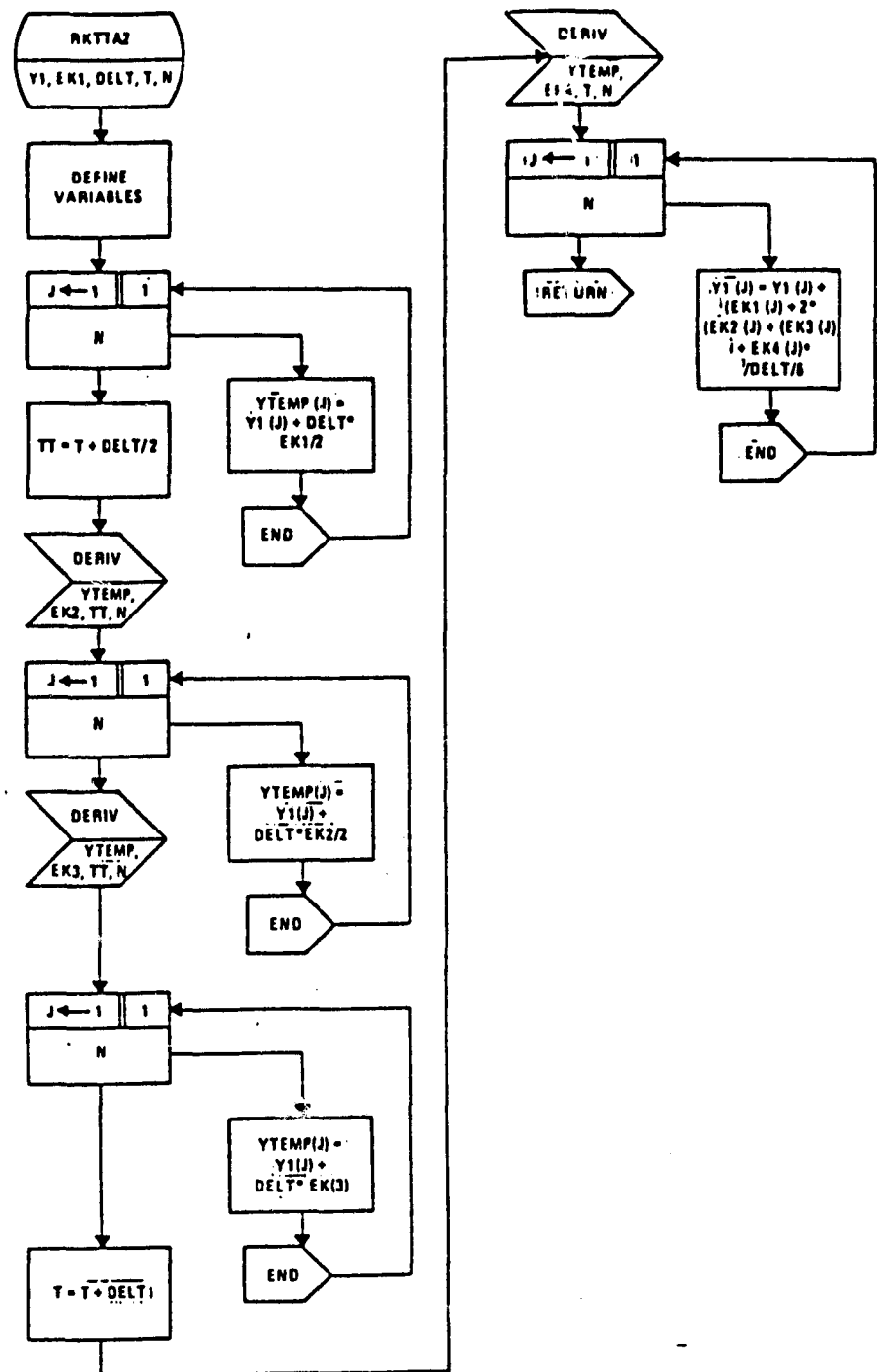


SUBROUTINE DERIV









GOLETA FCRTFAN 1.3 * SEMI-AUTO RFL * (01-10-73)

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PROGRAM CRASH

C
C CRASH SIMULATES THE BEHAVIOR OF UP TO 10 CONNECTED MASSES IN AN
C IMPACT SITUATION, CALCULATING THE DISPLACEMENT, VELOCITY, AND
C ACCELERATION OF EACH MASS AND THE FORCE EXERTED ON THE COUPLED
C MASSES.

DEFINE VARIABLES

C
C
C
C
C
C
000003 COMMON EMASS(10),F(50,10),X(50,10),FT(50),XSAV(50),FSAV(50),
1SLOPE(50),NCOUPTB(50,3),IFLAG(50),DELX(50),DY(20),NMASS,NCOUP
000003 REAL Y1(20),K1(20)
000003 REAL TPL(203),XPL(10,200),XPL1(203),DXPL(203),CDXPL(203)
000003 DIMENSION NPMASS(10),NSYMB(10)
000003 DATA NSYMB/1,2,6,7,10,12,14,11,4,26/

PRINT HEADINGS

C
C
C
000003 PRINT 500
000007 READ 400,NCASE,NPLOT
000017 IF(NPLOT.EQ.1)CALL PLOTS

CASE LOOP

C
C
C
000022 DO 300 JCASE=1,NCASE
000024 READ 400, NMASS, NCOUP
000033 READ 420,DAF
000041 READ 420,(EMASS(J), J=1,NMASS)
000054 PRINT 502
000060 PRINT 503, (I, EMASS(I), I=1,NMASS)
000074 PRINT 505
000100 READ 400, ((NCOUPTB(J,K), K=1,3), J=1,NCOUP)
000120 DO 10 J=1,NCOUP
000122 NPTS=NCOUPTB(J,3)
000124 READ 420, (X(J,K), F(J,K), K=1,NPTS)
000145 READ 420, SLOPE(J)
000153 DO 15 K=1,NPTS
000155 F(J,K)=F(J,K)*1000.*DAF
000162 15 CONTINUE
000164 SLOPE(J)=SLOPE(J)*1000
000167 PRINT 506, NCOUPTB(J,1),NCOUPTB(J,2),SLOPE(J)
000201 10 PRINT 507, (X(J,K), F(J,K), K=1,NPTS)
000225 READ 420, TF, DELT
000234 READ 400, NFRNT
000242 READ 420, VO
000250 READ 400, NPM, N3PM
000260 READ 400, (NPMASS(J), J=1,NPM)
000273 PRINT 508
000277 PRINT 509, DELT,TF,VO,NFRNT
000313 PRINT 510
000317 PRINT 515

INITIALIZE VARIABLES

C
C
C
000323 T1=0.0

```

000324      NMASS=NMASS*2
000326      NTIMES=(TF/DELTA+0.5)+1
000333      JPL=0
000334      JPRNT=0
000335      DO 20 J=1,NMASS
000336          Y1(J)=0.0
000337      20      DY(J)=0.0
000342      DO 25 J=2,NMASS,2
000344          Y1(J)=V0
000346      25      CONTINUE
000350      DO 30 J=1,NCOUP
000351          IFLAG(J)=1
000353          DELX(J)=0.0
000354          FT(J)=0.0
000355          XSAV(J)=0.0
000356      30      FSAV(J)=0.0

      C
      C      LOOP TO INTEGRATE EQUATIONS, STORE PLOT RECORDS AND SELECT
      C      RECOPOS
      C

000361      JPRNT=1
000362      DO 100 JTIMES=1,NTIMES
000363          CALL RKTTA1 (Y1,K1,T1,NMASS)
000366          CALL FLAG(Y1,NCOUP)
000370          IF(NPLOT.EQ.0)GO TO 106
000371          JPL=JPL+1
000373          TPL(JPL)=T1
000375          DO 105 K=1,NPM
000376              XPL(K,JPL)=Y1((NPMASS(K)+NPMASS(K))-1)
000404      105      CONTINUE
000406              DXPL(JPL)=Y1(N3PM+N3PM)
000411              CDXPL(JPL)=CY(N3PM+N3PM)

      C
      C      PRINT ROUTINE
      C

000414      106      IF(JPRNT.NE.JTIMES)GO TO 110
000416          PRINT 520, T1
000424          L=1
000425          DO 120 J=1,NMASS,2
000427              PRINT 525, Y1(J),Y1(J+1),DY(J+1)
000440              PRINT 540, NCOUPTB(L,1),NCOUPTB(L,2),FT(L)
000452              PRINT 550
000456      120          L=L+1
000462          IF(L.GT.NCOUP)GO TO 140
000465          DO 130 K=L,NCOUP
000466              PRINT 540, NCOUPTB(K,1),NCOUPTB(K,2),FT(K)
000477              PRINT 550
000503      130          CONTINUE
000505      140          JPRNT=JPRNT+NPRNT
000510      110          CALL RKTTA2(Y1,K1,DELTA,T1,NMASS)
000514      100      CONTINUE
000517          IF(NPLOT.EQ.0)GO TO 300

      C
      C      PLOT
      C

```

GOLETA FCRTFAN 1.3 * SEMI-AUTO RFL * (01-10-73)

CRASH

```

000520      CALL SCALE(TPL,10.0,JPL,1)
000523      CALL SCALE(CDXPL,10.0,JPL,1)
000526      CALL SCALE(CDXPL,10.0,JPL,1)
000531      CALL AXIS(0.0,0.0,0.0,4HTIME,-4,10.0,0.0,TPL(JPL+1),TPL(JPL+2),0)
000545      CALL AXIS(0.0,0.0,23HVELOCITY OF MASS ,23,10.0,90.0,
1DXPL(JPL+1),DXPL(JPL+2),0)
000561      CALL AXIS(-0.5,0.0,27HACCELERATION OF MASS ,27,10.0,90.0,
1DOXPL(JPL+1),DOXPL(JPL+2),0)
000575      CALL NUMBER(-.28,5.2,0.15,N3PM,90.0,2HI2)
000601      CALL NUMBER(-.78,5.5,0.15,N3PM,90.0,2HI2)
000605      CALL LINE(TPL,DXPL,JPL,1,5,0)
000611      CALL LINE(TPL,DOXPL,JPL,1,5,5)
000615      XAXIS=-0.5
000617      DO 200 JPM=1,NPM
000620      DO 210 LPL=1,JPL
000621      XPL1(LPL)=XPL(JPM,LPL)
000625      210 CONTINUE
000627      XAXIS=XAXIS-0.5
000631      200 CALL PLOT1(TPL,JPL,XPL1,NPMASS(JPM),NSYMB(JPM),XAXIS)
000643      CALL PLOT(15.0,0.0,-3)
000645      300 CONTINUE
000650      STOP
000652      410 FORMAT(10F10.0)
000652      400 EFORMAT(8I10)
000652      420 FORMAT(08F10.4)
000652      500 FORMAT(1H1,50X,*CRASH SIMULATION*)
000652      502 FORMAT(1H-,10X,*MASS*,10X,*WEIGHT*)
000652      509 FORMAT(1H ,12X,F10.4,7X,F10.2,8X,F10.2,14X,I2)
000652      503 FORMAT(1H ,11X,I2,9X,F10.4)
000652      505 FORMAT(1H-,10X,*COUPLING*,5X,*UNLOADING SLOPE*,5X,*DEFLECTION
1FORCE*)
000652      506 FORMAT(1H ,10X,I2,3X,I2,6X,F14.2)
000652      507 FORMAT(1H ,38X,F10.3,3X,F10.2)
000652      508 FORMAT(1H-,10X,*TIME INCREMENT*,5X,*FINAL TIME*,5X,*INITIAL VEL
1TY*,5X,*PRINT INTERVAL*)
000652      510 FORMAT(1H-,5X,4HTIME,13X,1HX,16X,2HDX,16X,3HDDX,10X,6HMASS I,5X
1MASS J,10X,21HFORCE BETWEEN I AND J)
000652      515 FORMAT(1H0)
000652      520 FORMAT(1H+,2X,E9.2)
000652      525 FORMAT(1H+,10X,3(6X,E12.4))
000652      540 FORMAT(1H+, 70X,I2,9X,I2,14X,E16.6)
000652      550 FORMAT(1H )
000652      END

```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

SUBROUTINE RKTTA1(Y1,EK1,T,N)

C
C
C
CRKTTA1 SETS EK1 EQUAL TO INITIAL CONDITIONS FOR USE IN
INTEGRATION ROUTINE

```
000007 REAL Y1(50),EK1(50)
000007 CALL DERIV(Y1,EK1,T,N)
000010 RETURN
000011 END
```

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GCLETA FCRTFAN 1.3 * SEMI-AUTO RFL * (01-10-73)

SUBROUTINE RKTTA2(Y1,EK1,DELT,T,N)

C

RKTTA2 USES RUNGE-KUTTA TECHNIQUE FOR NUMERICAL INTEGRATION.

C

```

000010 REAL Y1(50),Y2(50),YTEMP(50),EK1(50),EK2(50),EK3(50),EK4(50)
000010 DO 50J=1,N
000011 YTEMP(J)=Y1(J)+DELT*EK1(J)/2.
000017 50 CONTINUE
000022 TT=T+DELT/2.
000024 CALL DERIV(YTEMP,EK2,TT,N)
000027 DO 60J=1,N
000034 YTEMP(J)=Y1(J)+DELT*EK2(J)/2.
000041 60 CONTINUE
000045 CALL DERIV(YTEMP,EK3,TT,N)
000050 DO 70J=1,N
000055 YTEMP(J)=Y1(J)+DELT*EK3(J)
000061 70 CONTINUE
000064 T=T+DELT
000065 CALL DERIV(YTEMP,EK4,T,N)
000070 DO 80J=1,N
000075 Y1(J)=Y1(J)+(EK1(J)+2.*(EK2(J)+EK3(J))+EK4(J))*(DELT/6.)
000107 80 CONTINUE
000111 RETURN
000112 650 FORMAT(1H,8E14.6)
000112 END

```

SUBROUTINE DERIV(Y,K,T,N)

```

C
C-----
C     DERIV COMPUTES FORCE VALUES FOR EACH COUPLING AND ACCELERATION
C     EACH MASS
C
000007  COMMON EMASS(10),F(50,10),X(50,10),FT(50),XSAV(50),FSAV(50),
1SLOPE(50),NCOUPTB(50,3),IFLAG(50),DELX(50),DY(20),NMASS,NCOUPL
000007  REAL Y(20),K(20)
000007  DO 5 I=1,N
000010      K(I)=0.0
000012      5 CONTINUE
000013  DO 7 I=1,N
000015      K(I)=DY(I)
000017      7 CONTINUE
000021  DO 10 J=1,NCOUPL
000022      IF(NCOUPTB(J,1).EQ.0)GO TO 15
000024      DELX(J)=Y((NCOUPTB(J,2)+NCOUPTB(J,2))-1)-Y((NCOUPTB(J,1)+NCOUPTB(J,1))-1)
000034      GO TO 20
000035      15 DELX(J)=Y((NCOUPTB(J,2)+NCOUPTB(J,2))-1)
000043      20 IF(IFLAG(J).EQ.-1)GO TO 25
000046      FT(J)=ENTP(J)
000051      GO TO 10
000054      25 FT(J)=AMAX1(0.,FSAV(J)-SLOPE(J)*(XSAV(J)-DELX(J)))
000066      10 CONTINUE
000071  DO 30 J=2,N,2
000072      FIJ=0.0
000073      FJI=0.0
000074      JT=J/2
000075      DO 40 L=1,NCOUPL
000077      IF(NCOUPTB(L,1).NE.JT.AND.NCOUPTB(L,2).NE.JT)GO TO 40
000106      IF(NCOUPTB(L,2).GT.JT)GO TO 50
000112      FJI=FJI+FT(L)
000114      GO TO 40
000114      50 FIJ=FIJ+FT(L)
000117      40 CONTINUE
000122      DY(J-1)=Y(J)
000125      DY(J)=(FIJ-FJI)/EMASS(JT)
000131      30 CONTINUE
000133      525 FORMAT(1H ,10X,4(6X,E12.4))
000133      RETURN
000133      END

```

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GOLETA FORTRAN 1.3 * SEMI-AUTO PFL * (01-10-73)

```

SUBROUTINE FLAG(Y,N)
C
C FLAG CHECKS EACH COUPLING FOR UNLOADING
C
000005 REAL Y(20)
000006 COMMON EMASS(10),F(50,10),X(50,10),FT(50),XSAV(50),FSAV(50),
1SLOPE(50),NCCUPT9(50,3),IFLAG(50),DELX(50),DY(20),NMAST,NCOUP
000005 DO 10 J=1,N
000006 IF(NCCUPT9(J,1).EQ.0)GO TO 15
000010 DOELX=Y(NCCUPT9(J,2)+NCCUPT9(J,2))-Y(NCCUPT9(J,1)+NCCUPT9(
1 ))
000015 GO TO 18
000016 15 DOELX=Y(NCCUPT9(J,2)+NCCUPT9(J,2))
000022 18 IF(DOELX.GE.0 .OR. IFLAG(J).EQ.-1)GO TO 20
000034 IFLAG(J)=-1
000035 FSAV(J)=FT(J)
000040 XSAV(J)=DOELX(J)
000042 20 IF(DOELX(J).LE.XSAV(J))GO TO 10
000046 IFLAG(J)=1
000047 10 CONTINUE
000052 RETURN
000052 END

```

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GOLETA FCPT-AN 1.3 * SEMI-AUTO RFL * (01-10-73)

REAL FUNCTION ENTP(N)

C

C

ENTP_INTERPOLATES FORCE FOR SPECIFIED COUPLING

C

```

000003      COMMON E MASS(10),F(50,10),X(50,10),FT(50),XSAV(50),FSAV(50),
1SLOPE(50),NCOUPTB(50,3),IFLAG(50),DELX(50),DY(20),MASST,NCOUP
000003      IF (DELX(N).GE.X(N,1))GO TO 10
000006      J=2
000007      GO TO 30
000010      10 NX=NCOUPTB(N,3)
000012      DO 20 J=2,NX
000014      IF (DELX(N).LT.X(N,J))GO TO 30
000021      20 CONTINUE
000024      30 ENTP=F(N,J-1)+(DELX(N)-X(N,J-1))*((F(N,J)-F(N,J-1))/(X(N,J)-
1X(N,J-1)))
000043      RETURN
000044      ENC

```

CRASH SIMULATION

MASS WEIGHT
 1 171.000
 2 193.000
 3 411.000
 4 127.000
 5 274.000

COMPTNG UMC (KIN) SLOP
 0 1 210000.00

COMPTNG	UMC (KIN) SLOP	DEFLECTION	FORCE
0	1	0.000	0.00
		-100	85000.00
		-170	119000.00
		-175	467500.00
		-190	297500.00
		-550	297500.00
		-670	640000.00
0	2	0.000	0.00
		-430	3.00
		-360	21250.00
		-500	95300.00
0	3	0.000	0.00
		-300	3.00
		-200	1.00
		-100	17000.00
		-325	127500.00
		-350	25500.00
		-500	25500.00
		-300	10000.00
		-100	10000.00
1	2	0.000	0.00
		-300	3.00
		-300	3.00
		-300	17000.00
		-200	17000.00
2	1	0.000	0.00
		-300	3.00
		-300	3.00
		-200	17000.00
1	1	0.000	0.00
		-300	3.00
		-200	21250.00
		-200	21250.00
		-250	21250.00
		-250	51000.00
2	1	0.000	0.00
		-300	3.00
		-350	9500.00
		-270	45000.00
2	2	0.000	0.00
		-100	1.00
		-100	1.00

-120 170000.00
 -120 36000.00
 -120 0.00
 -200 0.00
 0.000 3.00
 -050 21250.00
 -150 21250.00
 -200 45700.00

1507000.00

TIME INCREMENT .0005 FINAL TIME INITIAL VELOCITY PRINT INTERVAL
 .0005 13.42 10

TIME	V	OX	ODX	MASS I	MASS J	FORCE BETWEEN I AND J
0.	0.	1.3417E+01	0.	0	1	0.
	0.	1.3417E+01	0.	0	2	0.
	0.	1.3417E+01	0.	0	3	0.
	0.	1.3417E+01	0.	1	2	0.
	0.	1.3417E+01	0.	2	1	0.
	0.	1.3417E+01	0.	1	3	0.
	0.	1.3417E+01	0.	2	3	0.
	0.	1.3417E+01	0.	2	4	0.
	0.	1.3417E+01	0.	1	5	0.
	0.	1.3417E+01	0.	3	1	0.
5.00E-13	6.4041E-02	1.2417E+01	-1.8436E+02	3	1	5.523355E+04
	6.5045E-02	1.3415E+01	-4.4521E-01	0	2	0.
	6.6049E-02	1.3335E+01	-2.7929E+01	0	3	0.
	6.7053E-02	1.3155E+01	-1.6779E+00	1	2	3.345743E+02
	6.8057E-02	1.3417E+01	-4.3304E-02	2	1	0.
	6.9061E-02	1.3417E+01	0.	1	3	2.293017E+04
	7.0065E-02	1.3417E+01	0.	2	3	0.
	7.1069E-02	1.3417E+01	0.	2	4	1.643966E+00
	7.2073E-02	1.3417E+01	0.	3	1	2.129564E+02
	7.3077E-02	1.3417E+01	0.	3	2	1.030215E+01
	7.4081E-02	1.3417E+01	0.	3	3	9.837619E+04
	7.5085E-02	1.3417E+01	0.	0	0.	0.
	7.6089E-02	1.3417E+01	0.	0	2	3.864038E+03
	7.7093E-02	1.3417E+01	0.	1	1	0.
	7.8097E-02	1.3417E+01	0.	2	3	1.188632E+05
	7.9101E-02	1.3417E+01	0.	2	4	0.
	8.0105E-02	1.3417E+01	0.	2	5	0.
	8.1109E-02	1.3417E+01	0.	1	4	6.399951E+03
	8.2113E-02	1.3417E+01	0.	3	1	3.658793E+02
	8.3117E-02	1.3417E+01	0.	3	2	3.023009E+05
	8.4121E-02	1.3417E+01	0.	0	0.	0.
	8.5125E-02	1.3417E+01	0.	0	2	0.
	8.6129E-02	1.3417E+01	0.	1	3	3.550393E+03
	8.7133E-02	1.3417E+01	0.	2	1	0.
	8.8137E-02	1.3417E+01	0.	1	3	1.451803E+05
	8.9141E-02	1.3417E+01	0.	2	0.	0.
	9.0145E-02	1.3417E+01	0.	2	5	0.
	9.1149E-02	1.3417E+01	0.	3	1	2.499293E+04
	9.2153E-02	1.3417E+01	0.	3	2	1.90723E+03
	9.3157E-02	1.3417E+01	0.	0	1	2.1711E+05
	9.4161E-02	1.3417E+01	0.	0	1	1

C1.4 HANDLING PROGRAMS (HYSIM and HYSSG)

1. Program Description

HYSIM and HYSSG are programs designed to provide a coarse indication of how changes in mass distribution, vehicle dimensions, and tire characteristics affect handling properties. HYSIM simulates the transient response of an automobile to a step in steer angle, and HYSSG computes the steady-state gain of yaw rate to steer angle as a function of forward speed. Both programs are based on a mathematical model which represents the automobile as a single mass with 3 degrees of freedom: lateral displacement, yaw and roll.

In HYSIM, the dynamics of tire force buildup are neglected, which means the front and rear tire force equations become algebraic expressions for the tire forces Y_f and Y_r . Thus, if

$$Y = \begin{pmatrix} \dot{y}_l \\ \dot{\psi} \\ \dot{\phi} \end{pmatrix} \quad \text{and} \quad Z = \begin{pmatrix} Y_f \\ Y_r \end{pmatrix}$$

the above differential equations can be written in the form

$$A\dot{Y} = BY + CZ$$

$$Z = DY + E$$

or

$$\dot{Y} = A^{-1}((B + CD)Y + CE\delta)$$

This is the form in which HYSIM solves the differential equations of motion for the vehicle.

For HYSSG, \ddot{y}_l , $\ddot{\psi}$, $\dot{\phi}$, \dot{Y}_f , and \dot{Y}_r are all set equal to zero and the steady gain of the vector Y , (and hence of its component $\dot{\psi}$, the yaw rate), to δ , is computed as follows:

$$BY = -CZ = -C(DY + E\delta), \quad \text{or} \quad \frac{1}{\delta} Y = -(B + CD)^{-1} CE$$

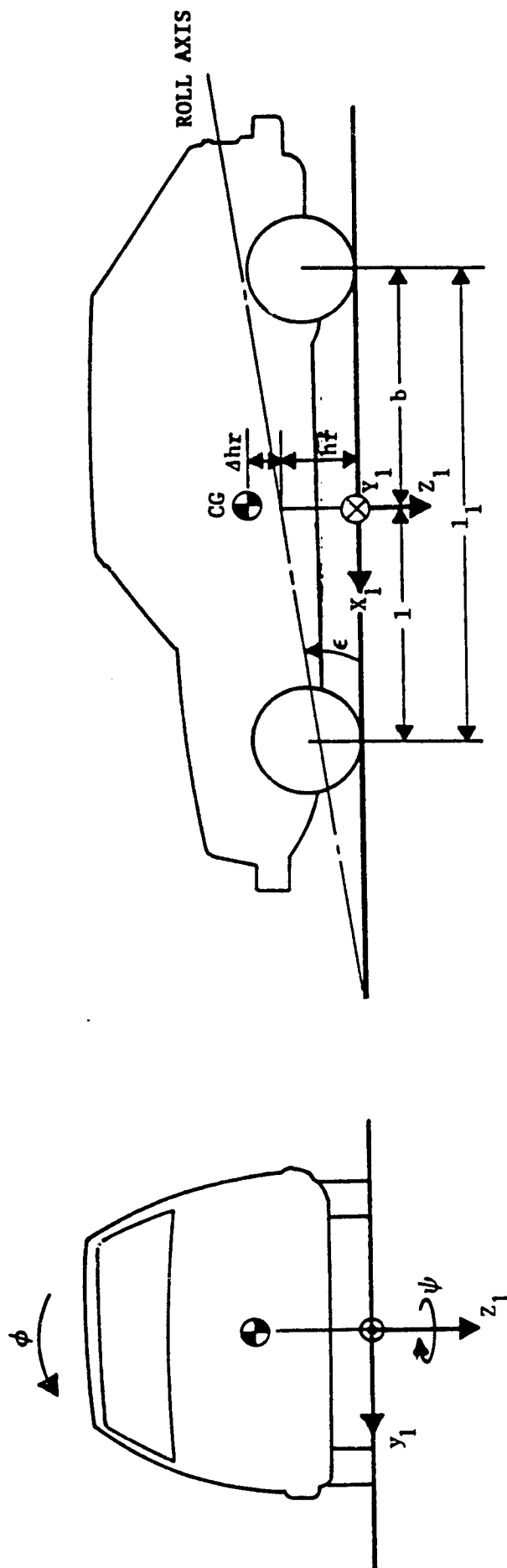


Figure A4-1 Vehicle Geometry and Coordinate Systems

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Summary of Equations for Linear, Constant-Speed Model

Lateral:

$$m_r \ddot{y}_1 + m_r \Delta h_r \ddot{\phi} = - \left(m_r + \frac{I_{ry}}{R^2} \right) \dot{x}_1 \dot{\psi} + Y_f + Y_r$$

Yaw:

$$I_{r_z} \ddot{\psi} - C_{r_{xz}} \ddot{\phi} = \frac{I_{ry}}{R^2} \dot{x}_1 \dot{y}_1 + F_A (\Delta h_r + h_r - h_a) \phi + l Y_f - b Y_r$$

Roll:

$$\begin{aligned} m_r \Delta h_r \ddot{y}_1 - C_{r_{xz}} \ddot{\psi} + (I_{r_x} + m_r \Delta h_r^2) \ddot{\phi} = \\ - m_r \Delta h_r \dot{x}_1 \dot{\psi} - (C_{\phi_f} + C_{\phi_r}) \dot{\phi} + (m_r g \Delta h_r - K_{\phi_f} - K_{\phi_r}) \phi \\ - (h_r - l e) Y_f - (h_r + b e) Y_r \end{aligned}$$

Front Tires

$$\frac{\sigma_f}{\dot{x}_1} \dot{Y}_f = - Y_f - \frac{C_{\alpha_f} Z_f}{\dot{x}_1} \dot{y}_1 - \frac{C_{\alpha_f} Z_f}{\dot{x}_1} l \dot{\psi} + C_{\alpha_f} Z_f \delta$$

Rear Tires:

$$\frac{\sigma_r}{\dot{x}_1} \dot{Y}_r = - Y_r - \frac{C_{\alpha_r} Z_r}{\dot{x}_1} \dot{y}_1 - \frac{C_{\alpha_r} Z_r}{\dot{x}_1} b \dot{\psi}$$

Miscellaneous:

$$F_A = 0.6125 C_D A \dot{x}_1^2$$

$$Z_f = \Theta_f m_r g - \frac{F_A h_A}{g}$$

$$Z_r = m_r g - Z_f$$

PARAMETERS		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	NCASE	—	NUMBER OF CASES
	NSPD	—	NUMBER OF SPEEDS
	NSTEPS	—	NUMBER OF INTEGRATION STEPS
	NPSTEP	—	PRINT FREQUENCY
	DELT	SEC	TIME INCREMENT
	SPEED(10)	KM	SPEEDS
	TM	SEC	FINAL TIME
	Y(A)	—	LATERAL VELOCITY, YAW RATE, ROLL RATE, ROLL ANGLE
M	EM	KG	MASS OF VEHICLE
I_{rx}	ENRTX	KG-M ²	MOMENTS OF INERTIA WITH RESPECT TO X, Y, AND Z AXES
I_{ry}	ENRTY	KG-M ²	
I_{rz}	ENRTZ	KG-M ²	
C_{rxz}	CYZ	KG-M ²	PRODUCT OF INERTIA WITH RESPECT TO X+Z AXES
l_1	EL1	M	WHEEL BASE LENGTH
l	EL	M	LENGTH FRONT AXLE TO CENTER OF GRAVITY
h_r	H	M	ROLL CENTER HEIGHT
Δh_r	CH	M	(CENTER OF GRAVITY - ROLL CENTER) HEIGHT
θ	THETA	—	FRACTION WT. ON FRONT WHEEL W/ STATIC CONDITIONS
ϵ	EPSLN	RAD	INCLINATION OF ROLL AXIS
R	R	M	WHEEL RADIUS
h_a	HA	M	AERO-DYNAMIC CENTER OF EFFORT
C_oA	CDA	—	DRAG COEFFICIENT * FRONTAL AREA
δ	DELTA	RAD	STEER ANGLE
C_{df}	CPF	N/RAD	ROLL DAMPING - FRONT
C_{dr}	CPR	N/RAD	ROLL DAMPING - REAR
K_{df}	EKPF	N/RAD	ROLL STIFFNESS - FRONT
K_{dr}	EKPR	N/RAD	ROLL STIFFNESS - REAR
C_{yf}	CYF	N/KAL	LATERAL FORCE - FRONT
C_{yr}	CYR	N/RAD	LATERAL FORCE - REAR
σ_f	SIGMAF	M	RELAXATION LENGTH - FRONT
σ_r	SIGMAR	M	RELAXATION LENGTH - REAR

VARIABLES		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	ACCLAT	m/sec ²	LATERAL ACCELERATION
	AINV(4,4)	-	INVERSE OF AM
	AM(4,4)	-	COEFFICIENT MATRIX
b	B	m	EL1-EL (SEE LIST OF INPUT PARAMETERS)
	BED(4,4)	-	BM-MATRIX + ED-MATRIX
	Bm(4,4)	-	COEFFICIENT MATRIX
	BMT(3,3)	-	MATRICES USED IN MATRIX INVERSION ROUTINE
	BMTT(3,3)	-	
	C(4,4)	-	AINV-MATRIX * BED-MATRIX
C _{zf}	CAFZF	N/RAD	LATERAL FORCE * LATERAL LOAD ON FRONT TIRE
C _{zr}	CARZR	N/RAD	LATERAL FORCE * LATERAL LOAD ON REAR TIRE
	DD(2,4)	-	COEFFICIENT MATRIX
	ED(4,4)	-	EE-MATRIX * UD-MATRIX
	EE(4,2)	-	COEFFICIENT MATRIX
	EF(4)	-	EE-MATRIX * F-MATRIX
m _r Δh _r	EMCH	-	MASS * (CENTER GRAVITY-ROLL CENTER) HEIGHT
	EMT(3,3)	-	MATRIX USED IN MATRIX INVERSION ROUTINE
	ENRTYR	KG-M ²	ROTATIONAL INERTIA OF WHEELS
	F(2)	-	COEFFICIENT MATRIX
F _a	FA	-	FACDEF * SPEED
0.612C _D A	FACDEF	-	0.612 * DRAG COEFFICIENT * FRONTAL AREA
g	G	N/RAD	GRAVITY
	GG(4)	-	AINV-MATRIX * EE-MATRIX
	K1(10)	-	VARIABLES OF INTEGRATION
	SUBA(3,3)	-	MATRICES USED IN MATRIX INVERSION ROUTINE
	SUBANV(3,3)	-	
	TRAN(3,3)	-	
	TRI(3,3)	-	
ẋ	XDOT	m/sec	SPEED FOR SPECIFIED SPEED LOSS
	Y1(10)	-	VARIABLES OF INTEGRATION
Z _f	ZF	KG	LATERAL LOAD ON FRONT TIRES
Z _r	ZR	KG	LATERAL LOAD ON REAR TIRES

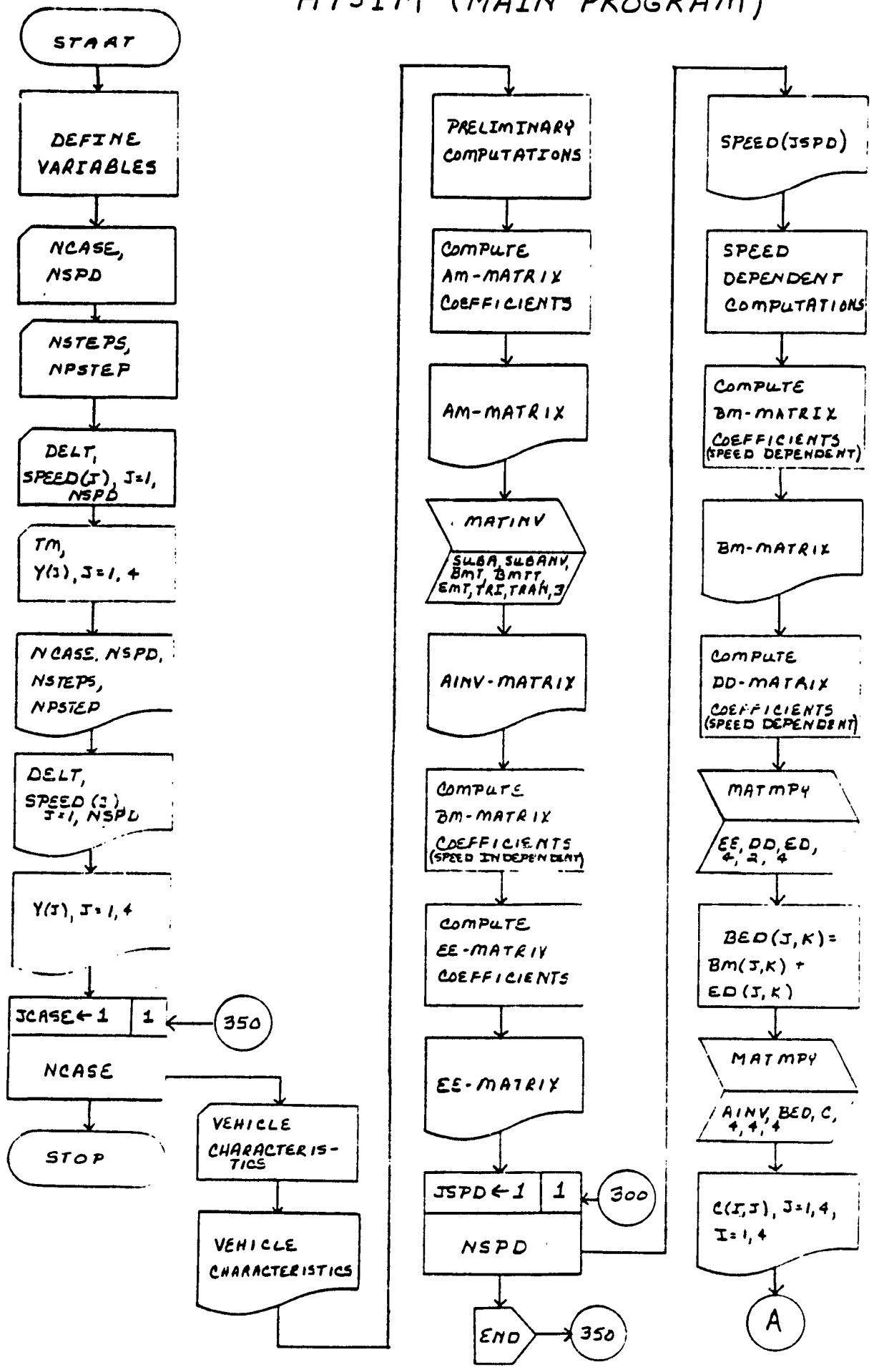
FORTRAN CODING FORM

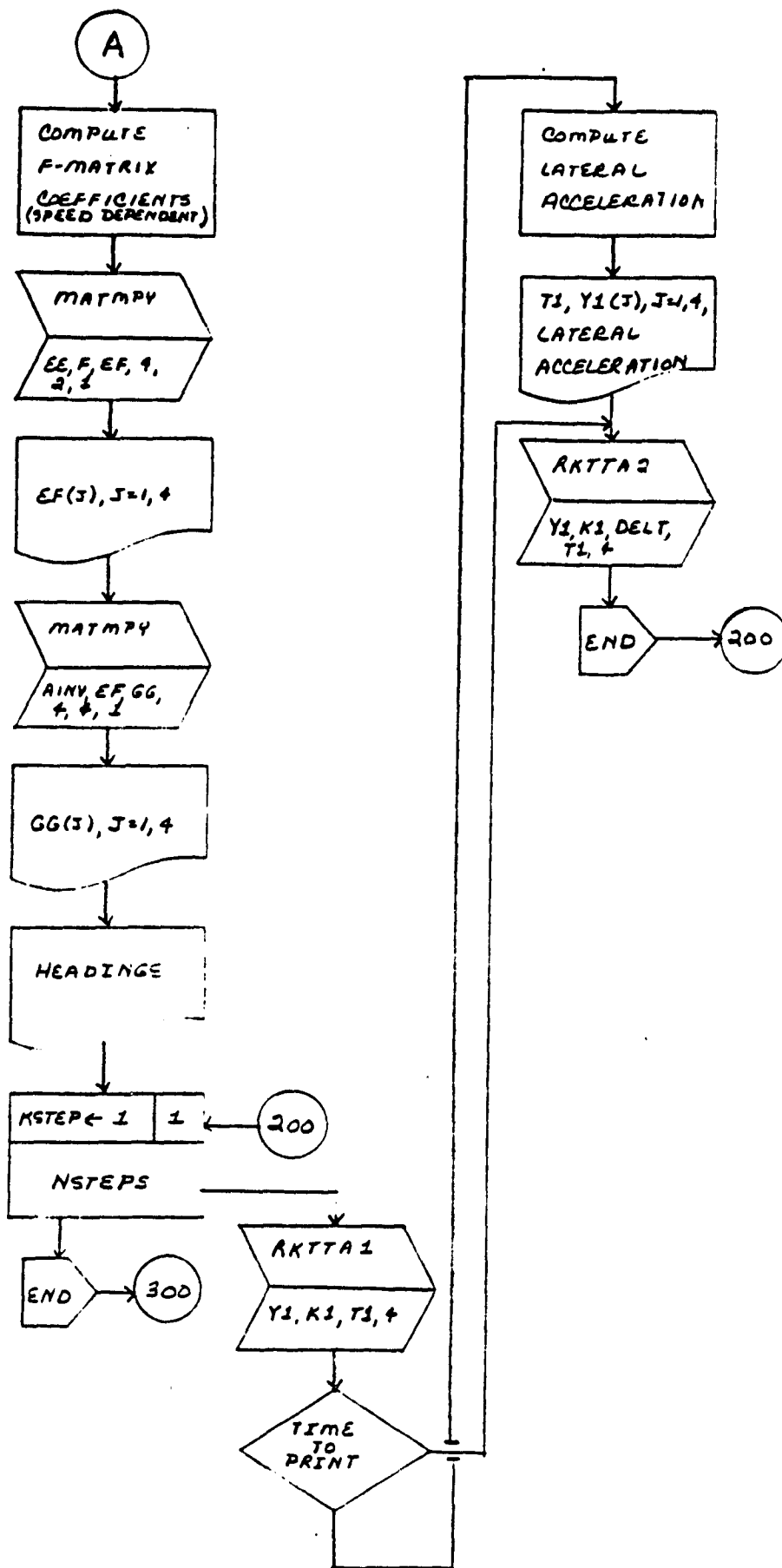
GENERAL RECORDS ARCH CORPORATION

PROGRAM HYSIM	NAME	PAGE OF
ROUTINE Input Format	DATE	

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1	M	C	A	S	E																	
2	M	S	T	E	R	S																
3	D	E	L	T																		
4	S	P	E	E	D	(1)														
5	Y	(1)																		
6	M	A	S	S	P	R	O	P	E	R	T	I	E	S								
7	E	N	R	T	X																	
8	G	O	M	E	T	R	I	C	A	L	S	P	R	O	P	E	R	T	I	E	S	
9	E	L	E																			
10	H	A																				
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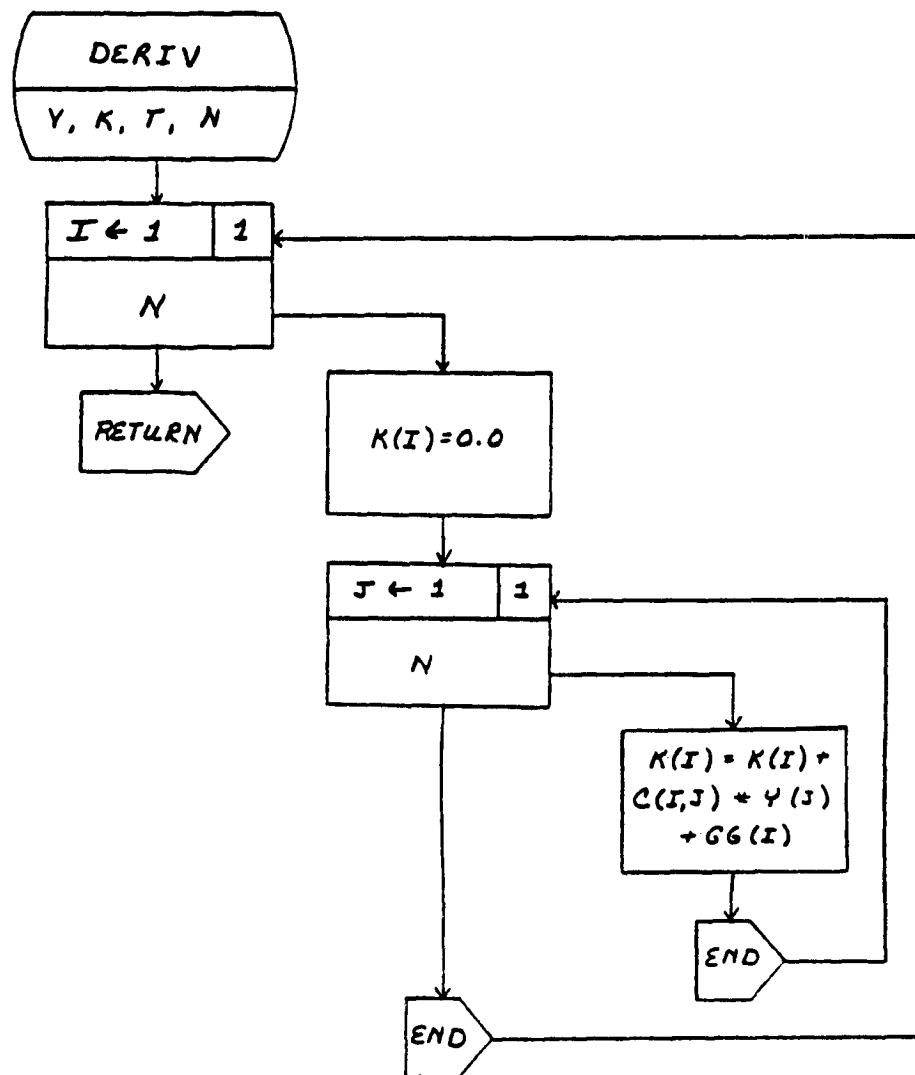
HYSIM (MAIN PROGRAM)



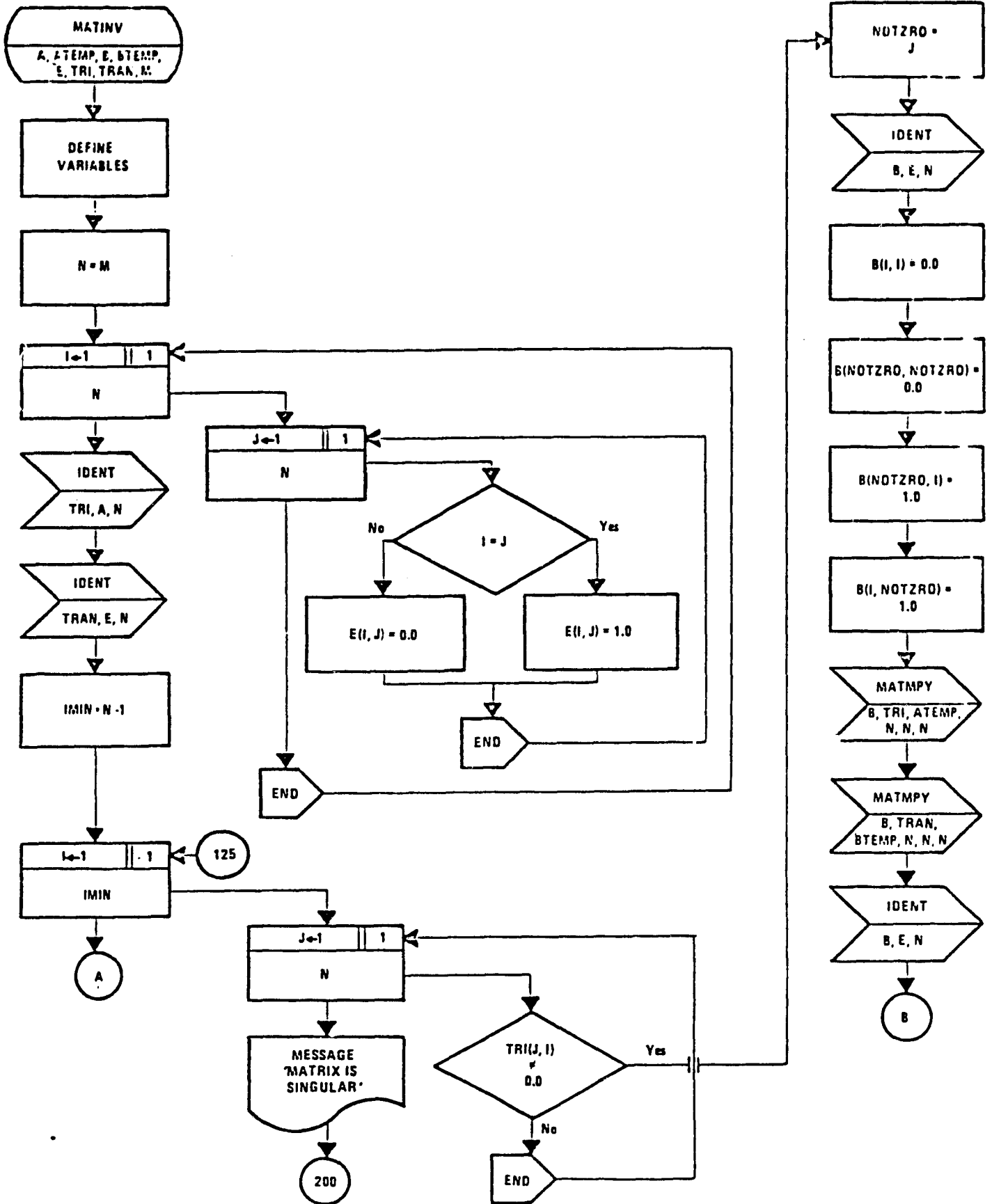


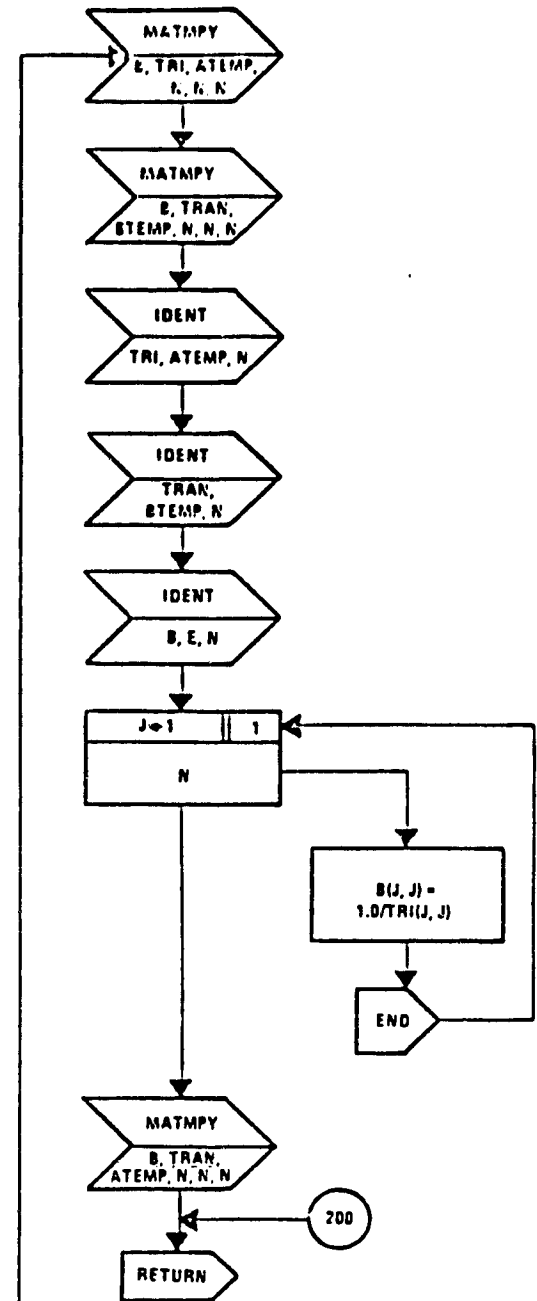
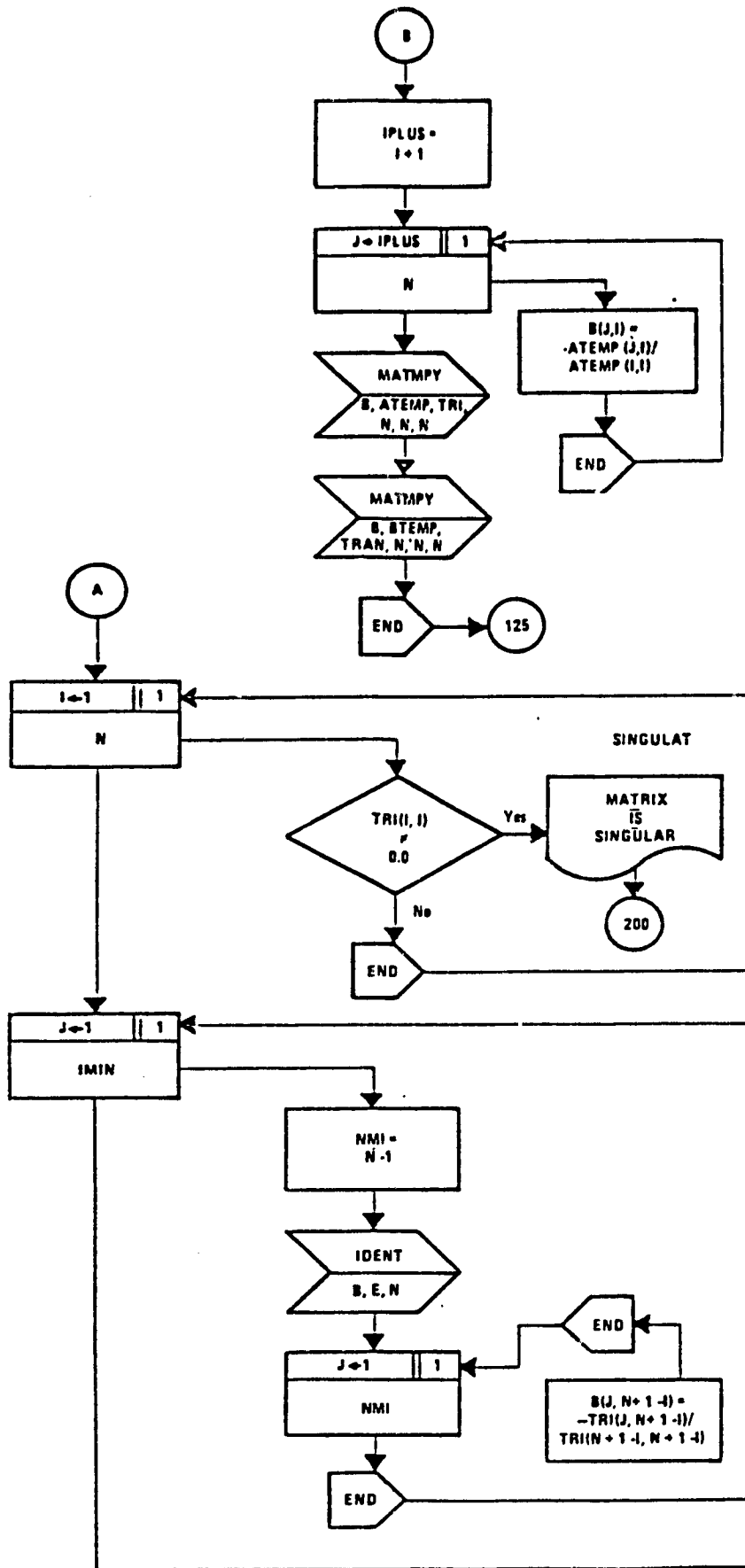
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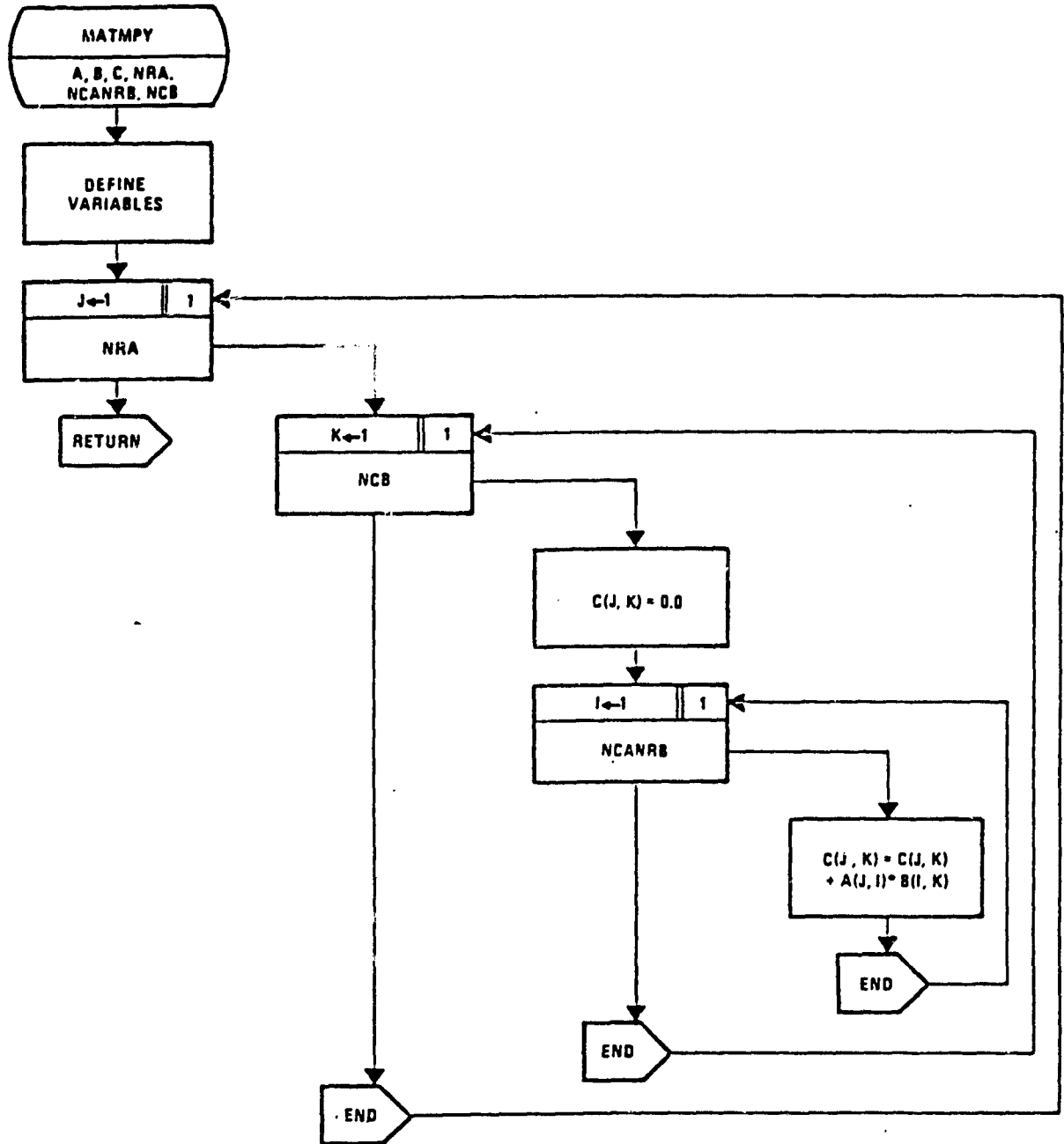


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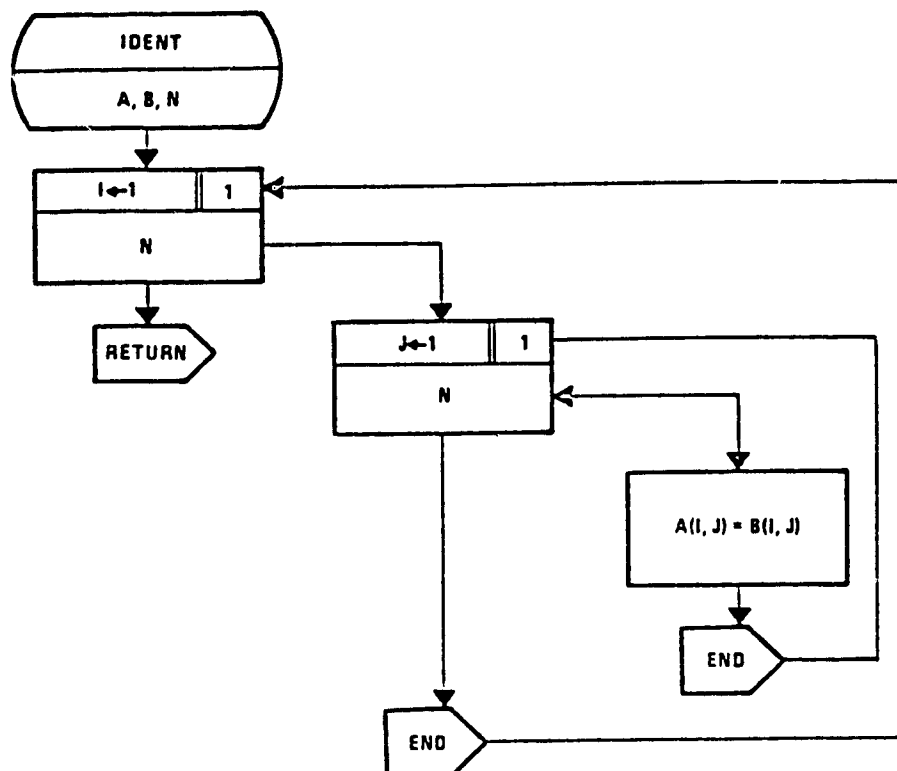


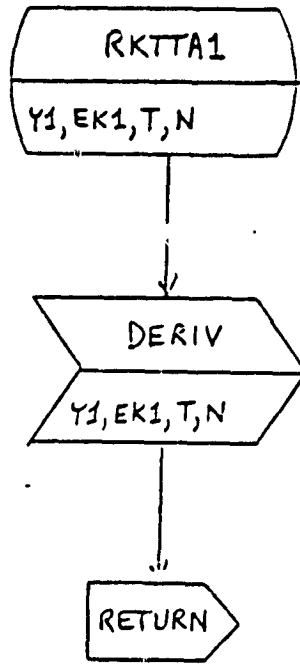


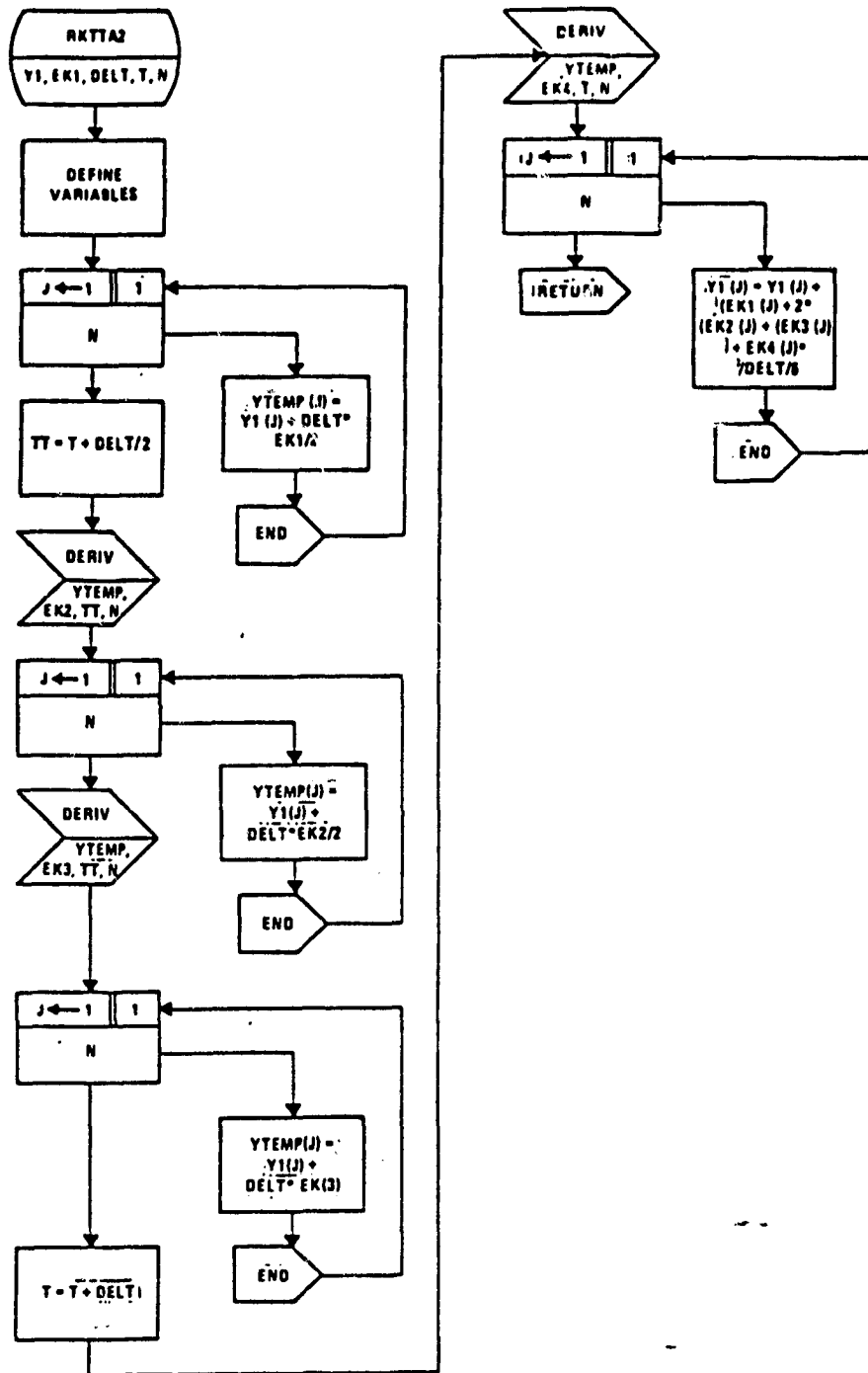
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SUBROUTINE IDENT







GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

PROGRAM HYSIM

C
C DEFINE VARIABLES
C

000003 REAL AM(4,4),RM(4,4),AINV(4,4),SUBA(3,3),SUBANV(3,3)
000003 REAL EE(4,2),OD(2,4),F(2),ED(4,4),EF(4),BED(4,4)
000003 REAL BMT(3,3),BMTT(3,3),EMT(3,3),TRI(3,3),TRAN(3,3)
000003 REAL SPEED(10)
000003 REAL Y1(10),K1(10),Y(10)
000003 COMMON C(4,4),GG(4)

C
C READ INPUT
C

000003 READ 410, NCASE, NSPD
000013 READ 410, NSTEPS, NPSTEP
000023 READ 400, DELT
000031 READ 400, (SPEED(J), J=1, NSPD)
000044 READ 400, TM, (Y(J), J=1, 4)
000060 PRINT 500
000064 PRINT 498, NCASE, NSPD, NSTEPS, NPSTEP
000100 PRINT 499, DELT, (SPEED(J), J=1, NSPD)
000115 PRINT 505
000121 PRINT 520, (Y(J), J=1, 4)
000133 PRINT 507

C
C CASE LOOP
C

000137 DO 350 JCASE=1, NCASE

C
C INPUT MASS PROPERTIES
C

000141 INPUT GEOMETRICAL PROPERTIES
000156 READ 400, EM, ENRTX, ENRTY, ENRTZ, CXZ
READ 400, EL1, EL, H, CH, THETA, EPSLN, R, HA, COA, DELTA

C
C TIRE PROPERTIES
C

000206 READ 400, CPF, CPR, EKPF, EKPR, CAF, CAR, SIGMAF, SIGMAR

C
C PRINT VEHICLE CHARACTERISTICS
C

000232 PRINT 510
000236 PRINT 520, EM, ENRTX, ENRTY, ENRTZ, CXZ
000254 PRINT 530
000260 PRINT 520, EL1, EL, H, CH, THETA, EPSLN
000300 PRINT 540
000304 PRINT 520, R, HA, COA, DELTA
000320 PRINT 550
000324 PRINT 520, CPF, CPR, EKPF, EKPR
000340 PRINT 560
000344 PRINT 520, CAF, CAR, SIGMAF, SIGMAR

C
C PRILIMINARY COMPUTATIONS
C

000360 B=EL1-EL

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HYSIM

```

000362      FACOE=0.612*COA
000364      G=9.807
000366      EMCH=EM*CH

```

```

C
C      A-MATRIX COEFFICIENTS(SPEED INDEPENDENT)
C

```

```

000370      DO 100 J=1,4
000371      DO 100 K=1,4
000372      AM(J,K)=0.0
000375      100 CONTINUE
000400      AM(1,1)=EM
000402      AM(1,3)=EMCH
000403      AM(2,2)=ENRTZ
000405      AM(2,3)=-CXZ
000406      AM(3,1)=EMCH
000407      AM(3,2)=-CXZ
000410      AM(3,3)=ENRTX+EM*CH**2
000413      AM(4,4)=1.0
000415      PRINT 570
000420      PRINT 580, ((AM(I,J),J=1,4),I=1,4)

```

```

C
C      INVERSE OF A-MATRIX
C

```

```

000436      DO 110 J=1,3
000440      DO 110 K=1,3
000441      SUFA(J,K)=AM(J,K)
000446      110 CONTINUE
000451      CALL MATINV(SURA,SUBANV,BMT,BMTT,EMT,TRI,TRAN,3)
000461      DO 120 J=1,4
000463      DO 120 K=1,4
000464      IF(J.LE.3.AND.K.LE.3)GO TO 130
000474      AINV(J,K)=0.0
000476      GO TO 120
000476      130 AINV(J,K)=SUBANV(J,K)
000503      120 CONTINUE
000507      AINV(4,4)=1.0
000511      PRINT 590
000514      PRINT 580, ((AINV(I,J),J=1,4),I=1,4)

```

```

C
C      9-MATRIX COEFFICIENTS(SPEED INDEPENDENT)
C

```

```

000532      DO 140 J=1,4
000534      DO 140 K=1,4
000535      BM(J,K)=0.0
000540      140 CONTINUE
000543      BM(3,3)=-CPF-CPR
000546      BM(3,4)=EMCH*G-EKPF-EKPR
000552      BM(4,3)=1.0

```

```

C
C      E-MATRIX COEFFICIENTS(SPEED INDEPENDENT)
C

```

```

000553      DO 150 J=1,2
000555      DO 150 K=1,4
000556      FE(J,K)=0.0
000561      150 CONTINUE

```

```

000564      EE(1,1)=1.0
000566      EE(1,2)=1.0
000567      EE(2,1)=EL
-----
000570      EE(2,2)=-B
000572      EE(3,1)=-H+EL*EPSLN
000573      EE(3,2)=-H-B*EPSLN
-----
000577      PRINT 490,((EE(I,J),J=1,2),I=1,4)

```

C
C
C

SPEED LOOP

```

000614      DO 300 JSPD=1,NSPD
000616      JPL=0
-----
000617      T1=TM
000621      DO 165 J=1,4
000622      Y1(J)=Y(J)
-----
000624      165 CONTINUE
000626      XDOT=SPEED(JSPD)
000630      PRINT 600,XDOT

```

C
C
C

SPEED DEPENDENT COMPUTATIONS

```

000635      FA=FA0EF*XDOT**2
000640      ZF=THETA*EM*G-FA*HA/EL1
000645      ZR=EM*G-ZF
-----
000647      CAFZF=CAF*ZF
000650      CARZR=CAR*ZR
00652      ENRTYR=ENSTY/R**2
00655      PRINT 610, ZF,ZR

```

C
C
C

B-MATRIX COEFFICIENTS(SPEED DEPENDENT)

```

000664      BM(1,2)=-XDOT*(EM+ENRTYR)
000667      BM(2,1)=XDOT*ENRTYR
000670      BM(2,4)=FA*(CH+H-HA)
000674      BM(3,2)=-XDOT*EMCH
000676      PRINT 620
-----
000702      PRINT 580,((BM(I,J),J=1,4),I=1,4)

```

C
C
C

D-MATRIX COEFFICIENTS(SPEED DEPENDENT)

```

000720      DO 170 J=1,4
000722      DO 170 K=1,2
000723      DD(J,K)=0.0
-----
000725      170 CONTINUE
000731      DD(1,1)=-CAFZF/XDOT
000733      DD(1,2)=-CAFZF*EL/XDOT
000735      DD(2,1)=-CARZR/XDOT
000737      DD(2,2)=CARZR*B/XDOT

```

C
C
C

COMPUTE C-MATRIX

```

000741      CALL MATM0Y(EE,DD,ED,4,2,4)
000745      DO 190 J=1,4
000747      DO 180 K=1,4
000750      CED(J,K)=BM(J,K)+ED(J,K)

```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

HYSIM

```

00757      180 CONTINUE
00763      CALL MATMPY(AINV,BED,C,4,4,4)
00767      PRINT 630
00773      PRINT 580,((C(I,J),J=1,4),I=1,4)
      C
      C      F-MATRIX COEFFICIENTS(SPEED DEPENDENT)
      C
001011     F(1)=CAFZF
001013     F(2)=0.0
      C
      C      COMPUTE GG-MATRIX
      C
001014     CALL MATMPY(EE,F,EF,4,2,1)
001020     PRINT 491,(EF(J),J=1,4)
001032     CALL MATMPY(AINV,EF,GG,4,4,1)
001036     PRINT 492,(GG(J),J=1,4)
001050     DO 160 J=1,4
001052     GG(J)=GG(J)*DELTA
001054     160 CONTINUE
001056     PRINT 492,(GG(J),J=1,4)
      C
      C      PRINT HEADINGS
      C
001067     PRINT 640
      C
      C      INTEGRATE EQUATIONS
      C
001073     KPSTEP=1
001074     DO 200 KSTEP=1,NSTEPS
001076     CALL RKTTA1(Y1,K1,T1,4)
001101     IF(KPSTEP.NE.KSTEP)GO TO 210
001103     ACCLAT=XDOT*Y1(2)+K1(1)
001106     PRINT 650,T1,(Y1(J),J=1,4),ACCLAT
001124     KPSTEP=KPSTEP+NPSTEP
001126     210 CALL RKTTA2(Y1,K1,DELT,T1,4)
001132     200 CONTINUE
001135     300 CONTINUE
001137     350 CONTINUE
001142     STOP
001144     400 FORMAT(7F10.4)
001144     410 FORMAT(2I10)
001144     498 FORMAT(1H ,4I4)
001144     499 FORMAT(1H ,10E16.6)
001144     490 FORMAT(1H ,*EE-MATRIX*/8E14.6)
001144     491 FORMAT(1H ,*EF-MATRIX*/8E14.6)
001144     492 FORMAT(1H ,*GG-MATRIX*/8E14.6)
001144     500 FORMAT(1H1,*VEHICLE CHARACTERISTICS*)
001144     505 FORMAT(1H3,*Y-VECTOR*)
001144     507 FORMAT(1H-,*FRAME*)
001144     510 FORMAT(1H0,8X,*MASS*,9X,*X-INERTIA*,7X,*Y-INERTIA*,7X,*Z-INERTIA*,
      16X,*X-Z PRODUCT*)
      1144     520 FORMAT(1H ,8E16.6)
      J1144     530 FORMAT(1H0,*GEOMETRY*/6X,*WHEELBASE*,6X,*FR. AXLE CG*,6X,*RC HE
      1HT*,5X,*CG - PC) HT.*,9X,*THETA*,11X,*EPSLN*)
001144     540 FORMAT(1H0,5X,*WHL. RAD.*,4X,*CG - AERO. LOAD*,5X,*CD AREA*,9X,

```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

HYSIM

```

1LTA*)
001144 550 FORMAT(1H0,*SUSPENSION*//10X,*ROLL DAMPING*,23X,*ROLL STIFFNESS
1X,*FRONT*,12X,*REAR*,11X,*FRONT*,12X,*REAR*)
001144 560 FORMAT(1H0,*TIRE PROPERTIES*//9X,*LATERAL FORCE*,19X,*RELAXATIO
1LENGTH*/8X,*FRONT*,12X,*REAR*,11X,*FRONT*,12X,*REAR*)
001144 570 FORMAT(1H0,*A-MATRIX*)
001144 580 FORMAT(1H ,4E14.6)
001144 590 FORMAT(1H0,*A-INVERSE MATRIX*)
001144 600 FORMAT(1H-,*SPEED =*,E14.6)
001144 610 FORMAT(1H ,*ZF =*,E14.6,5X,*ZR =*,E14.6)
001144 620 FORMAT(1H0,*B-MATRIX*)
001144 630 FORMAT(1H0,*C-MATRIX*)
001144 640 FORMAT(1HC,3X,*TIME*,6X,*Y1DOT*,7X,*PSIDOT*,6X,*PHIDOT*,7X,*PHI
16X,*LAT. ACC.*)
001144 650 FORMAT(1H ,E8.2,10E12.4)
001144 ENO

```

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OF POOR QUALITY

```

SUBROUTINE MATINV(A,ATEMP,B,BTEMP,E,TRI,TRAN,M)
C      MATINV DETERMINES THE INVERSE OF A REAL MATRIX
C      ATEMP IS THE INVERSE OF THE INPUT MATRIX A.
000013 REAL A(M,M),ATEMP(M,M),B(M,M),BTEMP(M,M),TRI(M,M),TRAN(M,M),
      1E(M,M)
000013 N=M
C      STORE THE IDENTITY MATRIX
000014 DO 20 I=1,N
000016 DO 20 J=1,N
000017 IF(I.EQ.J)GO TO 10
000023 E(I,J)=0.
000024 GO TO 20
000025 10 E(I,J)=1.
000033 20 CONTINUE
C
C      INITIALIZE TRANSFORMED AND TRANSFORMATION MATRICES
C
000040 CALL IDENT(TRI,A,N)
000043 CALL IDENT(TRAN,E,N)
C
C      TRANSFORM A-MATRIX TO UPPER TRIANGULAR FORM
C
000051 IMIN=N-1
000053 DO 125 I=1,IMIN
C      LOCATE NONZERO ELEMENT IN I-TH COLUMN
000060 DO 100 J=I,N
000061 IF(TRI(J,I).NE.0.)GO TO 110
000066 100 CONTINUE
000070 PRINT 500
000074 GO TO 200
000103 110 NOTZRO=J
000102 CALL IDENT(B,E,N)
000104 R(I,I)=C.
000114 B(NOTZRO,NOTZRO)=0.
000120 B(NOTZRO,I)=1.
000124 R(I,NOTZRO)=1.
C      GET NONZERO ELEMENT IN (I,I) LOCATION)
000127 CALL MATMPY(B,TRI,ATEMP,N,N,N)
000133 CALL MATMPY(B,TRAN,BTEMP,N,N,N)
C      GET ZEROS IN (I+1,I)-(N,I) LOCATIONS
000143 CALL IDENT(B,E,N)
000151 IPLUS=I+1
000153 DO 120 J=IPLUS,N
000163 R(J,I)=-ATEMP(J,I)/ATEMP(I,I)
000173 120 CONTINUE
000175 CALL MATMPY(B,ATEMP,TRI,N,N,N)
000201 125 CALL MATMPY(B,BTEMP,TRAN,N,N,N)
C
C      TRANSFORM A-MATRIX TO DIAGONAL FORM
C
C      CHECK DIAGONAL ELEMENTS
000217 DO 130 I=1,N
000221 IF(TRI(I,I).EQ.0.)GO TO 140
000225 130 CONTINUE
000230 GO TO 150

```


GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

MATINV

```

000233      140 WRITE(6,500)
000234      GO TO 200
000240      150 DO 170 I=1,IMIN
-----
)  C      GET ZEROS IN UPPER TRIANGLE
000242      NMI=N-I
000244      CALL IDENT(B,E,N)
-----
)  C      DO 160 J=1,NMI
000246      B(J,N+1-I)=-TRI(J,N+1-I)/TRI(N+1-I,N+1-I)
000253
000274      160 CONTINUE
-----
000277      CALL MATMPY(B,TRI,ATEMP,N,N,N)
000303      CALL MATMPY(B,TRAN,BTEMP,N,N,N)
000313      CALL IDENT(TRI,ATEMP,N)
000321      170 CALL IDENT(TRAN,BTEMP,N)
-----
)  C
)  C      NORMALIZE THE DIAGONAL ELEMENTS
)  C
000335      CALL IDENT(B,E,N)
000337      DO 180 J=1,N
000344      B(J,J)=1./TRI(J,J)
000354      180 CONTINUE
000356      CALL MATMPY(B,TRAN,ATEMP,N,N,N)
-----
000363      200 RETURN
000364      500 FORMAT(1H0,10HMATRIX IS SINGULAR)
000364      END

```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

SUBROUTINE ICENT(A,B,N)

C
C
C

IDENT EQUATES MATRICES

```
000006 REAL A(N,N),R(N,N)
000006 DO 10 I=1,N
000007 DO 10 J=1,N
000010 A(I,J)=R(I,J)
000017 10 CONTINUE
000022 RETURN
000022 END
```

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GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

SUBROUTINE MATMPY(A,B,C,NRA,NCANRB,NCB)

C

MATMPY MULTIPLIES MATRICES

C

C

```
000011 REAL A(NRA,NCANRB),B(NCANRB,NCB),C(NRA,NCB)
000011 DO 10 J=1,NRA
000012 DO 10 K=1,NCB
000013 C(J,K)=0.
000017 DO 10 I=1,NCANRB
000020 C(J,K)=C(J,K)+A(J,I)*B(I,K)
000035 10 CONTINUE
000044 RETURN
C
000044 END
```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

```
10007      SUBROUTINE RKTTA1(Y1,EK1,T,N)
000007     REAL Y1(20),EK1(20)
000010     CALL DERIV(Y1,EK1,T,N)
000011     RETURN
        END
```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

SUBROUTINE RKTTA2(Y1,EK1,DELT,T,N)

C
C
C

RKTTA2 USES RUNGE-KUTTA TECHNIQUE FOR NUMERICAL INTEGRATION

```

000010 REAL Y1(50),Y2(50),YTEMP(50),EK1(50),EK2(50),EK3(50),EK4(50)
000010 DO 50 J=1,N
-----
000011 YTEMP(J)=Y1(J)+DELT*EK1(J)/2.
000017 50 CONTINUE
000022 TT=T+DELT/2.
-----
000024 CALL DERIV(YTEMP,EK2,TT,N)
000027 DO 60 J=1,N
000034 YTEMP(J)=Y1(J)+DELT*EK2(J)/2.
-----
000041 60 CONTINUE
000045 CALL DERIV(YTEMP,EK3,TT,N)
000050 DO 70 J=1,N
000055 YTEMP(J)=Y1(J)+DELT*EK3(J)
000061 70 CONTINUE
000064 T=T+DELT
000065 CALL DERIV(YTEMP,EK4,T,N)
000070 DO 80 J=1,N
000075 Y1(J)=Y1(J)+(EK1(J)+2.*(EK2(J)+EK3(J))+EK4(J))*(DELT/6.)
-----
000107 80 CONTINUE
000111 RETURN
000112 650 FORMAT(1H ,8E14.6)
000112 END

```

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GOLETA FORTRAN 1.3 * SEMI-AUTO PFL * (01-10-73)

SUBROUTINE DERIV(Y,K,T,N)

C
C
C

DERIV SETS UP K-MATRIX FOR USE IN INTEGRATION ROUTINE

000007 COMMON C(4,4),GG(4)

000007 REAL Y(10),K(10)

000007 DO 10 I=1,4

000010 K(I)=GG(I)

000012 DO 10 J=1,4

000014 K(I)=K(I)+C(I,J)*Y(J)

000022 10 CONTINUE

000026 RETURN

000026 END

VEHICLE CHARACTERISTICS

1 3 500 5
 1.00000E-02 1.00000E+01 2.00000E+01 3.00000E+01
 Y-VECTOR 0. 0. 0. 0.

FRAME

MASS X-INERTIA Y-INERTIA Z-INERTIA X-Z PRODUCT
 1.05700E+03 0.42000E+02 5.00000E+00 4.67000E+03 5.10000E+01

GEOMETRY

MHEELBASE FR. AXLE CG RC HEIGHT (CG - RC) HT. EPSIM
 2.90000E+00 1.29000E+00 1.06000E-01 4.60000E-01 5.55000E-01 1.44000E-01
 WHL. RAD. CG - AERO. LOAD CD AREA DELTA
 3.12000E-01 5.50000E-01 1.24000E+00 2.00000E-02

SUSPENSION

ROLL DAMPING ROLL STIFFNESS
 FRONT REAR FRONT REAR
 6.90000E+03 1.35000E+03 3.19000E+04 6.70000E+03

TIRE PROPERTIES

LATERAL FORCE RELAYATION LENGTH
 FRONT REAR FRONT REAR
 9.43000E+00 9.46000E+00 2.50000E-01 2.50000E-01

A-MATRIX

1.05700E+03 0. 0.54220E+02 0.
 0. 6.07000E+03 6.10000E+01 0.
 0.54220E+02 6.10000E+01 1.21494E+03 0.
 0. 0. 0. 1.00000E+00

B-INVERSE MATRIX

7.930376E-04 6.043216E-06 -5.468145E-04 0.
 6.043216E-06 2.05225E-04 -1.488960E-05 0.
 -5.468145E-04 -1.488960E-05 1.199727E-03 0.
 0. 0. 0. 1.00000E+00

EE-MATRIX

1.00000E+00 1.00000E+00 1.23000E+00 -1.61000E+00 -2.40000E-04 -4.17800E-01 0. 0.

SPEED = 1.00000E+01

ZF = 1.003351E+04 ZR = 0.118030E+03

B-MATRIX

0. -1.909364E+04 0. 0.
 5.136423E+02 0. 0. 7.050240E+00
 0. -9.542200E+03 -6.250300E+03 -3.022266E+04
 0. 0. 1.00000E+00 0.

C-MATRIX

-1.453232E+01 -6.719015E+00 3.417531E+00 1.652624E+01
 2.321369E-01 -6.919577E+03 9.305071E-02 4.514524E-01
 1.264767E+01 -6.109063E+00 -7.429545E+00 -3.592661E+01
 0. 0. 1.00000E+00 0.

EF-MAIRIX	TIME	VIDOT	PSIDOT	PHIDOT	PHI	LAT.	ACC.
9.509020E+04	0.	4.3070E-02	0.	0.	0.	1.3597E+00	
GC-MAIRIX	1.00E-01	5.7267E-02	3.5800E-02	-2.8607E-02	-0.5186E-04	6.8674E-01	
6.79891E+01	1.50E-01	5.9726E-02	4.3898E-02	-3.9280E-02	-0.5355E-03	4.7039E-01	
GC-MAIRIX	2.00E-01	5.7522E-02	5.0940E-02	-4.0232E-02	-0.4432E-03	4.4549E-01	
1.359714E+00	3.00E-01	5.3940E-02	5.5950E-02	-4.0995E-02	-0.4739E-03	4.7894E-01	
	4.00E-01	4.9914E-02	5.9245E-02	-4.1553E-02	-1.0539E-02	5.1254E-01	
	5.00E-01	4.6050E-02	6.1567E-02	-4.1633E-02	-1.2621E-02	5.4163E-01	
	6.00E-01	4.2550E-02	6.3135E-02	-4.0966E-02	-1.4590E-02	5.6562E-01	
	7.00E-01	3.9491E-02	6.4178E-02	-3.9539E-02	-1.6787E-02	5.8516E-01	
	8.00E-01	3.6809E-02	6.4850E-02	-3.7279E-02	-1.8631E-02	6.0113E-01	
	9.00E-01	3.4740E-02	6.5291E-02	-3.4317E-02	-2.0823E-02	6.1429E-01	
	1.00E+00	3.3018E-02	6.5550E-02	-3.0812E-02	-2.2053E-02	6.2523E-01	
	1.10E+00	3.1692E-02	6.5714E-02	-2.6942E-02	-2.3490E-02	6.3437E-01	
	1.20E+00	3.0722E-02	6.5816E-02	-2.2832E-02	-2.4745E-02	6.4200E-01	
	1.30E+00	3.0067E-02	6.5865E-02	-1.8831E-02	-2.5787E-02	6.4835E-01	
	1.40E+00	2.9600E-02	6.5891E-02	-1.4902E-02	-2.6630E-02	6.5356E-01	
	1.50E+00	2.9317E-02	6.5910E-02	-1.1228E-02	-2.7282E-02	6.5778E-01	
	1.60E+00	2.9333E-02	6.5926E-02	-7.8960E-03	-2.7750E-02	6.6111E-01	
	1.70E+00	2.9680E-02	6.5947E-02	-4.9651E-03	-2.8070E-02	6.6365E-01	
	1.80E+00	3.0264E-02	6.5969E-02	-2.4662E-03	-2.8262E-02	6.6550E-01	
	1.90E+00	3.0966E-02	6.5914E-02	1.2066E-03	-2.8311E-02	6.6753E-01	
	2.00E+00	3.1763E-02	6.6043E-02	2.4200E-03	-2.8218E-02	6.6789E-01	
	2.10E+00	3.2670E-02	6.6070E-02	3.2670E-03	-2.8075E-02	6.6791E-01	
	2.20E+00	3.3709E-02	6.6105E-02	3.7828E-03	-2.7897E-02	6.6769E-01	
	2.30E+00	3.4824E-02	6.6135E-02	4.0237E-03	-2.7701E-02	6.6728E-01	
	2.40E+00	3.5930E-02	6.6163E-02	4.3373E-03	-2.7499E-02	6.6675E-01	
	2.50E+00	3.7255E-02	6.6190E-02	3.6723E-03	-2.7300E-02	6.6614E-01	
	2.60E+00	3.8745E-02	6.6214E-02	3.5744E-03	-2.7114E-02	6.6552E-01	
	2.70E+00	3.9982E-02	6.6233E-02	3.1854E-03	-2.6945E-02	6.6499E-01	
	2.80E+00	4.0955E-02	6.6250E-02	2.7419E-03	-2.6796E-02	6.6430E-01	
	2.90E+00	4.1665E-02	6.6264E-02	2.2740E-03	-2.6671E-02	6.6377E-01	
	3.00E+00	4.2112E-02	6.6274E-02	1.8095E-03	-2.6569E-02	6.6329E-01	
	3.10E+00	4.2300E-02	6.6282E-02	1.3657E-03	-2.6489E-02	6.6289E-01	
	3.20E+00	4.2300E-02	6.6291E-02	9.5819E-04	-2.6432E-02	6.6256E-01	
	3.30E+00	4.2044E-02	6.6290E-02	5.3669E-04	-2.6393E-02	6.6231E-01	
	3.40E+00	4.1595E-02	6.6291E-02	2.8700E-04	-2.6371E-02	6.6212E-01	
	3.50E+00	4.0955E-02	6.6290E-02	1.1159E-05	-2.6363E-02	6.6199E-01	
	3.60E+00	4.0150E-02	6.6288E-02	-1.1737E-04	-2.6367E-02	6.6193E-01	
	3.70E+00	3.9105E-02	6.6286E-02	-3.2201E-04	-2.6379E-02	6.6189E-01	
	3.80E+00	3.7862E-02	6.6280E-02	-4.2691E-04	-2.6398E-02	6.6190E-01	
	3.90E+00	3.6418E-02	6.6279E-02	-4.7001E-04	-2.6421E-02	6.6194E-01	
	4.00E+00	3.4777E-02	6.6273E-02	-5.1490E-04	-2.6447E-02	6.6200E-01	
	4.10E+00	3.2742E-02	6.6271E-02	-5.2000E-04	-2.6473E-02	6.6207E-01	
	4.20E+00	3.0712E-02	6.6270E-02	-4.9762E-04	-2.6499E-02	6.6215E-01	
	4.30E+00	2.8697E-02	6.6267E-02	-4.5931E-04	-2.6523E-02	6.6223E-01	
	4.40E+00	2.6664E-02	6.6264E-02	-4.1977E-04	-2.6544E-02	6.6232E-01	
	4.50E+00	2.4654E-02	6.6262E-02	-3.5110E-04	-2.6563E-02	6.6239E-01	
	4.60E+00	2.2645E-02	6.6261E-02	-2.9094E-04	-2.6579E-02	6.6246E-01	
	4.70E+00	2.0640E-02	6.6259E-02	-2.3115E-04	-2.6592E-02	6.6252E-01	
	4.80E+00	1.8638E-02	6.6258E-02	-1.7420E-04	-2.6602E-02	6.6257E-01	
	4.90E+00	1.6639E-02	6.6255E-02	-1.2193E-04	-2.6610E-02	6.6262E-01	
	5.00E+00	1.4642E-02	6.6253E-02	-7.5657E-05	-2.6615E-02	6.6265E-01	

PARAMETERS		UNITS	DESCRIPTION
EQUATION	PROGRAM		
	NCASE	—	NUMBER OF CASES
	NSPD	—	NUMBER OF SPEEDS
	SPEED(12)	m/sec	SPEEDS
M_r	EM	KG.	MASS OF VEHICLE
I_{rx}	ENRTX	KG·m ²	MOMENTS OF INERTIA WITH RESPECT TO X, Y, AND Z AXES
I_{ry}	ENRTY	KG·m ²	
I_{rz}	ENRTZ	KG·m ²	
C_{rxz}	CXZ	KG·m ²	
l_1	EL1	m	WHEEL BASE LENGTH
l	EL	m	LENGTH FRONT AXLE TO CENTER OF GRAVITY
h_r	H	m	ROLL CENTER HEIGHT
Δh_r	CH	m	(CENTER OF GRAVITY - ROLL CENTER) HEIGHT
Θ	THETA	—	FRACTION WT. ON FRONT WHEEL W/STATIC CONDITION
ϵ	EPSLN	RAD	INCLINATION OF ROLL AXIS
R	R	m	WHEEL RADIUS
h_a	HA	m	AERODYNAMIC CENTER OF EFFORT
$C_D A$	CDA	—	DRAG COEFFICIENT * FRONTAL AREA
δ	DELTA	RAD	STEER ANGLE
$C_{\phi f}$	CPF	N/RAD	ROLL DAMPING - FRONT (COEFFICIENT)
$C_{\phi r}$	CPR	N/RAD	ROLL DAMPING - REAR (COEFFICIENT)
$K_{\phi f}$	EKPR	N/RAD	ROLL STIFFNESS - FRONT (COEFFICIENT)
$K_{\phi r}$	EKPF	N/RAD	ROLL STIFFNESS - REAR (COEFFICIENT)
$C_{\phi f}$	CAF	N/RAD	LATERAL FORCE - FRONT (COEFFICIENT)
$C_{\phi r}$	CAR	N/RAD	LATERAL FORCE - REAR (COEFFICIENT)
σ_f	SIGMAF	m	RELAXATION LENGTH - FRONT
σ_r	SIGMAR	m	RELAXATION LENGTH - REAR

VARIABLES		UNITS	DESCRIPTION
EQUATION	PROGRAM		
b	B	m	ELI - EL (see list of input parameters)
	BED(4,4)	-	B _M -MATRIX + ED-MATRIX
	BEDINV(4,4)	-	INVERSE OF BED-MATRIX
	B _M (4,4)	-	COEFFICIENT MATRIX
	B _M T(4,4)	-	{ MATRICES USED IN MATRIX INVERSION ROUTINE
	B _M TT(4,4)	-	
C _{zf} Z _f	CAFZF	N/RAD	C _{zf} * Z _f
	CARZR	N/RAD	C _{zr} * Z _r
-	DD(2,4)	-	COEFFICIENT MATRIX
	ED(4,4)	-	EE-MATRIX * DD-MATRIX
	EF(4)	-	EE-MATRIX * F-MATRIX
	EE(4,2)	-	COEFFICIENT MATRIX
	EMT(4,4)	-	MATRIX USED IN MATRIX INVERSION ROUTINE
	M _r Δh _r	EMCH	-
-	ENRTYR	KG-M ²	ROTATIONAL INERTIA OF WHEELS
	F(2)	-	COEFFICIENT MATRIX
F _A	FA	-	FA * CDEF * SPEED
0.612 C _D A	FACDEF	-	0.612 * DRAG COEFFICIENT * FRONTAL AREA
g	-	N/RAD	GRAVITY
	TRAN(4,4)	-	{ MATRICES USED IN MATRIX INVERSION ROUTINE
	TRI(4,4)	-	
x _i	XDOT	m/sec	VEHICLE SPEED FOR SPECIFIED SPEED LOOP
	Y(10)	-	BEDINV-MATRIX * EF-MATRIX
	YI(10)	-	Y-MATRIX / DELTA
Z _f	ZF	KG.	LATERAL LOAD ON FRONT TIRES
Z _r	ZR	KG.	LATERAL LOAD ON REAR TIRES

UNU

GENERAL RE: RCH CORPORATION

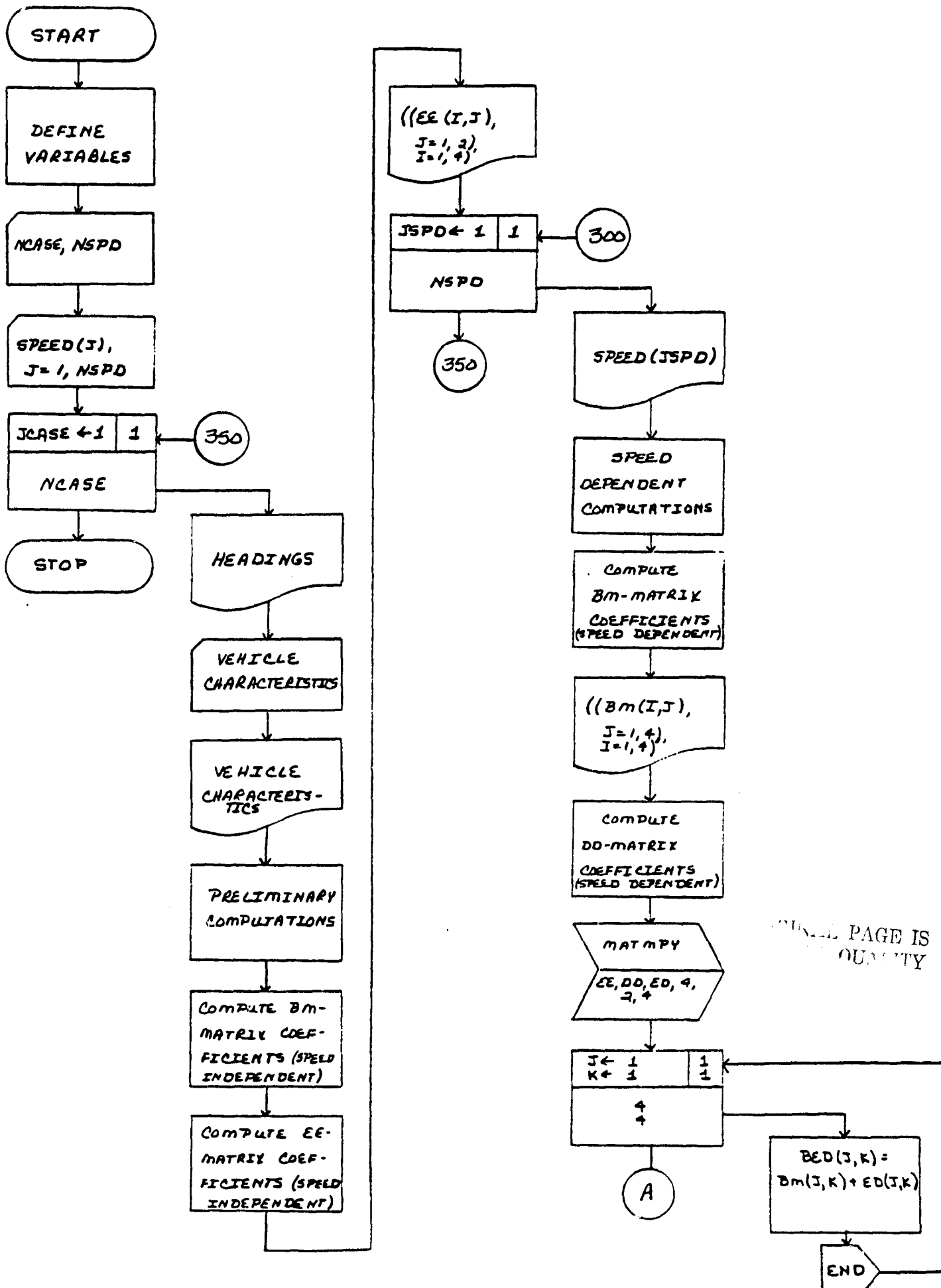
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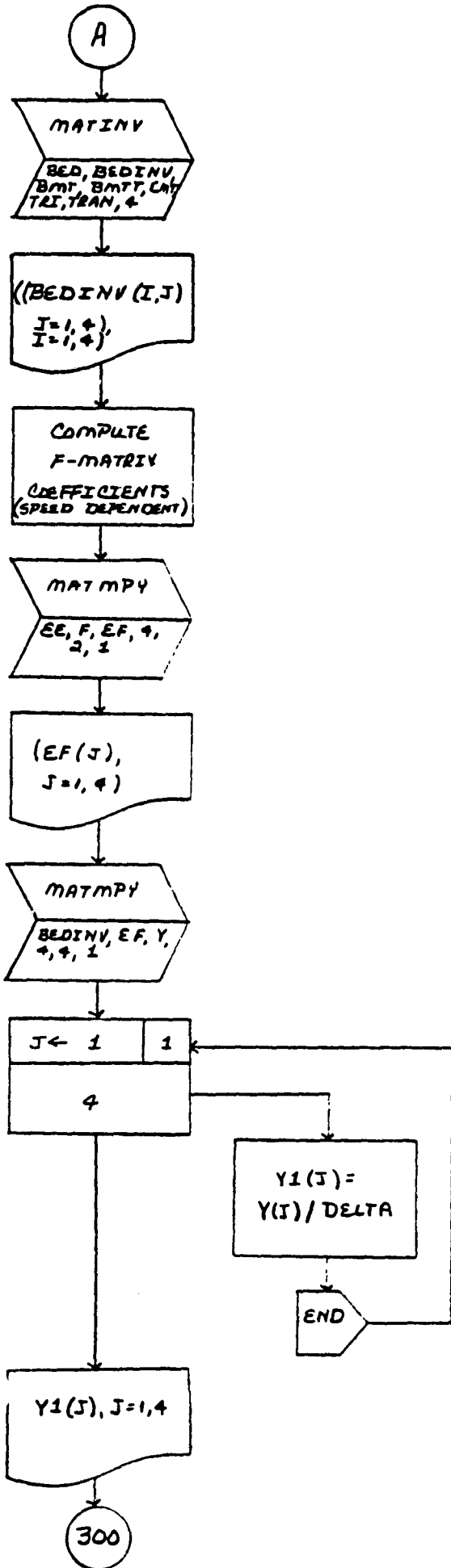
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3	M	A	S	S	P	R	O	P	R	T	I	E	S	3	
4	E	M	E	N	R	I	T	E	4	
5	G	E	O	M	E	N	T	R	I	C	N	L	P	R	O	P	E	R	T	I	E	S	5
6	E	L	I	.	E	L	6	
7	H	A	7	
8	T	I	P	E	.	P	R	O	P	E	R	T	I	E	S	8
9	S	I	G	M	A	9	
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HYSSG





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GOLETA FORTRAN 1.3 * SEMI-AUTO PFL * (01-10-73)

PROGRAM HYSSG

C
C
C

OFFLINE VARIABLES

```

000003      RFAL BM(4,4),BEDINV(4,4)
000003      RFAL EE(4,2),DD(2,4),F(2),ED(4,4),EF(4),BED(4,4)
000003      REAL BMT(4,4),BMTT(4,4),EMT(4,4),TRI(4,4),TRAN(4,4)
000003      REAL SPEED(12)
000003      REAL Y(10),Y1(10)

```

C
C
C

READ INPUT

```

000003      READ 410, NCASE, NSPD
000013      READ 400, (SPEED(J), J=1, NSPD)

```

C
C
C

CASE LOOP

```

000026      DO 350 JCASE=1, NCASE

```

C
C
C

PRINT HEADINGS

```

000030      PRINT 500
000033      PRINT 507

```

C
C
C

INPUT MASS PROPERTIES

```

000037      READ 400, EM, ENRTX, ENRTY, ENRTZ, CXZ

```

C
C
C

INPUT GEOMETRICAL PROPERTIES

```

000055      READ 400, EL1, EL, F, CH, THETA, EPSLN, R, HA, COA, DELTA

```

C
C
C

TIRE PROPERTIES

```

000105      READ 400, CPF, CPR, EKPF, EKPR, CAF, CAR, SIGMAF, SIGMAR

```

C
C
C

PRINT VEHICLE CHARACTERISTICS

```

000131      PRINT 510
000135      PRINT 520, EM, ENRTX, ENRTY, ENRTZ, CXZ
000153      PRINT 530
000157      PRINT 520, EL1, EL, H, CH, THETA, EPSLN
000177      PRINT 540
000203      PRINT 520, R, HA, COA, DELTA
000217      PRINT 550
000223      PRINT 520, CPF, CPR, EKPF, EKPR
000237      PRINT 560
000243      PRINT 520, CAF, CAR, SIGMAF, SIGMAR

```

C
C
C

PRELIMINARY COMPUTATIONS

```

000257      R=EL1-EL
000261      FACCEF=0.612*COA
000263      G=9.807
000265      EMCH=EM*CH

```

C
C

B-MATRIX COEFFICIENTS(SPEED INDEPENDENT)

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

HYSSG

```

      C
000267      DO 140 J=1,4
000270      DO 140 K=1,4
000271      BM(J,K)=0.0
000274      140 CONTINUE
000277      BM(3,3)=-CPF-CPR
000302      BM(3,4)=EMCH*G-EKPF-EKPR
000306      BM(4,3)=1.0

      C
      C      E-MATRIX COEFFICIENTS(SPEED INDEPENDENT)
      C
000307      DO 150 J=1,2
000311      DO 150 K=1,4
000312      EE(J,K)=0.0
000315      150 CONTINUE
000320      EE(1,1)=1.0
000322      EE(1,2)=1.0
000323      EE(2,1)=EL
000324      EE(2,2)=-B
000326      EE(3,1)=-H+EL*EPSLN
000331      EE(3,2)=-H-B*EPSLN
000333      PRINT 490,((EE(I,J),J=1,2),I=1,4)

      C
      C      SPEED LOOP
      C
000350      DO 300 JSPD=1,NSPD
000352      XDOT=SPEED(JSPD)
000354      PRINT 600,XDOT

      C
      C      SPEED DEPENDENT COMPUTATIONS
      C
000361      FA=FACOEF*XDOT**2
000364      ZF=THETA*EM*G-FA*HA/EL1
000371      ZR=EM*G-ZF
000373      CAFZF=CAF*ZF
000374      CARZR=CAR*ZR
000376      ENRTYR=ENRTY/R**2
000401      PRINT 610, ZF,ZR

      C
      C      B-MATRIX COEFFICIENTS(SPEED DEPENDENT)
      C
000410      BM(1,2)=-XDOT*(EM+ENRTYR)
000413      BM(2,1)=XDOT*ENRTYR
000414      BM(2,4)=FA*(CH+H-HA)
000420      BM(3,2)=-XDOT*EMCH
000422      PRINT 620
000426      PRINT 580,('BM(I,J),J=1,4),I=1,4)

      C
      C      D-MATRIX COEFFICIENTS(SPEED DEPENDENT)
      C
000444      DO 170 J=1,4
000446      DO 170 K=1,2
000447      DN(J,K)=0.0
000451      170 CONTINUE
000455      DN(1,1)=-CAFZF/XDOT

```

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GOLETA FORTRAN 1.3 * SFMI-AUTO RFL * (01-10-73)

HYSSG

```

000457      DD(1,2)=-CAFZF*EL/XDOT
000461      DD(2,1)=-CARZR/XDOT
000463      DD(2,2)=CARZR*B/XDOT
-----
C
C      COMPUTE BED INV MATRIX
C
000465      CALL MATMPY(EE,DD,ED,4,2,4)
000471      DO 180 J=1,4
000473      DO 180 K=1,4
000474      BED(J,K)=BM(J,K)+ED(J,K)
000503      180 CONTINUE
000507      CALL MATINV(BED,BEDINV,BMT,BMTT,EMT,TRI,TRAN,4)
000516      PRINT 590
000522      PRINT 580,((BEDINV(I,J),J=1,4),I=1,4)
-----
C
C      F-MATRIX COEFFICIENTS(SPEED DEPENDENT)
C
000540      F(1)=CAFZF
000542      F(2)=0.0
-----
C
C      COMPUTE Y-MATRIX
C
000543      CALL MATMPY(EE,F,EF,4,2,1)
000547      PRINT 491,(EF(J),J=1,4)
000561      DO 190 J=1,4
000563      EF(J)=EF(J)*DELTA
000565      DO 190 K=1,4
000567      BEDINV(J,K)=-BEDINV(J,K)
000572      190 CONTINUE
000575      CALL MATMPY(BEDINV,EF,Y,4,4,1)
000601      DO 200 J=1,4
000603      Y1(J)=Y(J)/DELTA
000606      200 CONTINUE
000607      PRINT 640
000613      PRINT 650,(Y1(J),J=1,4)
000625      300 CONTINUE
000630      350 CONTINUE
000632      STOP
000634      400 FORMAT(7F10.6)
000634      410 FORMAT(2I10)
000634      490 FORMAT(1HG,*,EE-MATRIX*,2(/4E14.6))
000634      491 FORMAT(1HG,*,FF-MATRIX*/2(4E14.6))
000634      500 FORMAT(1H1,*,VEHICLE CHARACTERISTICS*)
000634      507 FORMAT(1H-,*FRAME*)
000634      510 FORMAT(1H0,8X,*,MASS*,9X,*,X-INERTIA*,7X,*,Y-INERTIA*,7X,*,Z-INERTIA
16X,*,X-Z PRODUCT*)
000634      520 FORMAT(1H,*,9E16.6)
000634      530 FORMAT(1H0,*,GEOMETRY*/6X,*,WHEELBASE*,6X,*,FR. AXLE CG*,6X,*,RC H
1HT*,5X,*(CG - RC) HT.*,8X,*,THETA*,11X,*,EPSLN*)
000634      540 FORMAT(1H0,5X,*,WHL. RAD.*,4X,*,CG - AERO. LOAD*,5X,*,CD AREA*,6X,
1EER ANGLE*)
000634      550 FORMAT(1H0,*,SUSPENSION*/10X,*,ROLL DAMPING*,23X,*,ROLL STIFFNESS
1X,*,FRONT*,12X,*,REAR*,11X,*,FRONT*,12X,*,REAR*)
000634      560 FORMAT(1H0,*,TIRE PROPERTIES*/9X,*,LATERAL FORCE*,19X,*,RELAXATIC
1LENGTH*/8X,*,FRONT*,12X,*,REAR*,11X,*,FRONT*,12X,*,REAR*)

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GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

HYSSG

```
000634 580 FORMAT(1H ,4E14.6)
000634 590 FORMAT(1H0,*BED-INVERSE MATRIX*)
000634 600 FORMAT(1H-,*SPEED =*,E14.6)
000634 610 FORMAT(1H ,*ZF =*,E14.6,5X,*ZR =*,E14.6)
000634 620 FORMAT(1H0,*B-MATRIX*)
000634 640 FORMAT(1H0,4X,*Y1DOT*,7X,*PSIDOT*,6X,*PHIDOT*,7X,*PHI*)
000634 650 FORMAT(1H ,10E12.+)
000634 END
```

GOLETA FORTPAN 1.3 * SEMI-AUTO RFL * (01-10-73)

```

SUBROUTINE MATINV(A,ATEMP,B,BTEMP,E,TRI,TRAN,M)
C
C MATINV DETERMINES THE INVERSE OF A REAL MATRIX
C ATEMP IS THE INVERSE OF THE INPUT MATRIX A.
000013 REAL A(M,M),ATEMP(M,M),B(M,M),BTEMP(M,M),TRI(M,M),TRAN(M,M),
1E(M,M)
000013 N=M
C STORE THE IDENTITY MATRIX
000014 DO 20 I=1,N
000016 DO 20 J=1,N
000017 IF(I.EQ.J)GO TO 10
000020 E(I,J)=0.
000024 GO TO 20
000025 10 E(I,J)=1.
000033 20 CONTINUE
C
C INITIALIZE TRANSFORMED AND TRANSFORMATION MATRICES
C
000040 CALL IDENT(TRI,A,N)
000043 CALL IDENT(TRAN,E,N)
C
C TRANSFORM A-MATRIX TO UPPER TRIANGULAR FORM
C
000051 IMIN=N-1
000053 DO 125 I=1,IMIN
C LOCATE NONZERO ELEMENT IN I-TH COLUMN
000060 DO 100 J=I,N
000061 IF(ABS(REAL(A(J,I))) .NE. 0.)GO TO 110
000066 100 CONTINUE
000070 PRINT 500
000074 GO TO 200
000100 110 NOTZRO=J
000102 CALL IDENT(C,E,N)
000104 B(I,I)=C.
000114 R(NOTZRO,NOTZRO)=0.
000120 R(NOTZRO,I)=1.
000124 R(I,NOTZRO)=1.
C GET NONZERO ELEMENT IN (I,I) LOCATION)
000127 CALL MATMPY(B,TRI,ATEMP,N,N,N)
000133 CALL MATMPY(B,TRAN,BTEMP,N,N,N)
C GET ZERES IN (I+1,I)-(N,I) LOCATIONS
000143 CALL IDENT(B,E,N)
000151 IPLUS=I+1
000153 DO 120 J=IPLUS,N
000160 R(J,I)=-ATEMP(J,I)/ATEMP(I,I)
000173 120 CONTINUE
000176 CALL MATMPY(B,ATEMP,TRI,N,N,N)
000201 125 CALL MATMPY(B,BTEMP,TRAN,N,N,N)
C
C TRANSFORM A-MATRIX TO DIAGONAL FORM
C
C CHECK DIAGONAL ELEMENTS
002017 DO 130 I=1,N
002021 IF(ABS(REAL(A(I,I))) .EQ. 0.)GO TO 140
002025 130 CONTINUE
000230 GO TO 150

```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

MATINV

```

000230      140 WRITE(6,500)
000234      GO TO 200
000240      150 DO 170 I=1,IMIN
-----
C          GET ZEROES IN UPPER TRIANGLE
000242      NMI=N-I
000244      CALL IDENT(B,E,N)
-----
000246      DO 160 J=1,NMI
000253      B(J,N+1-I)=-TRI(J,N+1-I)/TRI(N+1-I,N+1-I)
000274      160 CONTINUE
-----
000277      CALL MATMPY(B,TRI,ATEMP,N,N,N)
000303      CALL MATMPY(B,TRAN,BTEMP,N,N,N)
000313      CALL IDENT(TRI,ATEMP,N)
-----
000321      170 CALL IDENT(TRAN,BTEMP,N)
-----
C
C          NORMALIZE THE DIAGONAL ELEMENTS
-----
C
000335      CALL IDENT(B,E,N)
000337      DO 180 J=1,N
000344      B(J,J)=1./TRI(J,J)
000354      180 CONTINUE
000356      CALL MATMPY(B,TRAN,ATEMP,N,N,N)
-----
000363      200 RETURN
000364      500 FORMAT(1H0,18HMATRIX IS SINGULAR)
000364      END
-----

```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

SUBROUTINE IDENT(A,B,N)

C

IDENT EQUATES MATRICES

C

```
000006 REAL A(N,N),B(N,N)
000006 DO 10 I=1,N
000007 DO 10 J=1,N
000010 A(I,J)=B(I,J)
000017 10 CONTINUE
000022 RETURN
000022 END
```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

SUBROUTINE MATMPY(A,B,C,NRA,NCANRB,NCB)

C

C

MATMPY MULTIPLIES MATRICES

C

```
000011 REAL A(NRA,NCANRB),B(NCANRB,NCB),C(NRA,NCB)
000011 DO 10 J=1,NRA
000012 DO 10 K=1,NCB
000013 C(J,K)=0.
000017 DO 10 I=1,NCANRB
000020 C(J,K)=C(J,K)+A(J,I)*B(I,K)
000035 10 CONTINUE
000044 RETURN
```

C

000044 END

VEHICLE CHARACTERISTICS

FRAME

PASS X-INERTIA Y-INERTIA Z-INERTIA X-Z PRODUCT
 1.857000E+03 0.420000E+02 5.000000E+00 4.879000E+03 -6.100000E+01

GEOMETRY

WHEELBASE FR. AXLE CG RC HEIGHT (CG - FC) HT. THETA EPSLN
 2.900000E+00 1.290000E+00 1.840000E-01 4.600000E-01 5.550000E-01 1.440000E-01

SUSPENSION

ROLL DAMPING REAR ROLL STIFFNESS
 FCNT FCNT REAR
 4.900000E+03 1.350000E+03 3.100000E+04 6.700000E+03

TIRE PROPERTIES

LATERAL FORCE RELAXATION LENGTH
 FCNT FCNT REAR
 9.430000E+00 9.440000E+00 2.500000E-01 2.500000E-01

EE-MATRIX

1.000000E+00 1.000000E+00 1.290000E+00 -1.410000E+10
 -2.400000E-04 -4.174000E-01 0.

SPEED = 5.000000E+00

ZF = 1.010000E+04 ZP = 4.107644E+03

Q-MATRIX

0. -9.541021E+03 0. 0.
 2.560212E+02 0. 0. 1.742560E+00
 0. -4.271100E+03 -6.250000E+03 -3.022266E+04
 0. 0. 1.000000E+00 0.

DEQ-INVERSE MATRIX

-3.060412E-05 3.064121E-06 1.727372E-10 1.117100E-06
 -1.370420E-06 -1.424785E-05 -2.444103E-10 -5.302614E-06
 -1.421865E-19 1.421055E-19 0. 1.000000E+00
 -5.049077E-06 7.471040E-06 -3.104710E-05 -2.057056E-01

SF-MATRIX

0.517634E+04 1.090775E+05 -2.044232E+01 0.

YICCY

2.2702E+00 1.7175E+09 -3.5102E-10 -1.4537E-01

SPEED = 1.000000E+01

ZF = 1.010000E+04 ZP = 4.111900E+03

R-MATRIX

0. -1.909164E+04 0. 0.
 5.136427E+02 0. 0. 7.070240E+00
 0. -0.542200E+09 -5.250000E+03 -1.222764E+04

C1.5 Life Cycle Costs

Two changes have been made in LYFECC since its summarization appeared in the report from Phase I, "Mission Analysis and Performance Specification Studies Report". First, the method of computing the discount factor now matches the one described in "Hybrid Vehicle Potential Assessment Interim Progress Report", Appendix C, Electric and Hybrid Cost Handbook, R. Left, S. Heller, Draft #5030-162, Jet Propulsion Laboratory, Pasadena, California.

The second change involves the inclusion of replacement batteries down payment. This was omitted from operating and life cycle costs in the first version of the program.

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GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

PROGRAM LYFECC

```

C
C   IFUEL CAN EQUAL 1 THRU 5 WITH THE FOLLOWING RESULTS
C   IF IFUEL=1, PETROLEUM AND ELECTRICITY ARE BOTH NOMINAL
C   IF IFUEL=2, PETROLEUM IS +30%
C   IF IFUEL=3, PETROLEUM IS -30%
C   IF IFUEL=4, ELECTRICITY IS +30%
C   IF IFUEL=5, ELECTRICITY IS -10%
C
000003   INTEGER KBR(11)
000003   REAL EKP(11),RK(11),TRCK(11),AOC(5,11),YLCC(5,11),DF(11),
1DAOC(11),DYLCC(5,11),VKT(11),PFCK(11),PFCKN(11),PFCKP(11),
1EFCK(11),EFCKN(11),EFCKP(11),TFCK(5,11),TAOC(5),AOCK(5),
1TLCC(5),ALCCK(5),TDLCC(5),DLCC(5)
C
C   PRINT HEADING
C
000003   PRINT 500
000007   READ 400,NCASE
000015   READ 400,NYEARS
000023   NYRM1=NYEARS-1
C
C   DISCOUNT FACTOR
C
000025   DO 1 J=1,NYEARS
000027   DF(J)=1./(1+.02)**(J-1)
000037   1 CONTINUE
C
C   CASE LOOP
C
000041   DO 350 JCASE=1,NCASE
000043   TK=0.
000044   BR=0.
000045   DO 5 J=1,NYEARS
000046   KBR(J)=0
000047   5 CONTINUE
C
C   INPUT
C
000051   READ 410,CV,WV,WB,PHE,PM,POP
000071   READ 410,GGPK,GOPK,EKWHPK,BOEM,BRK
000107   READ 410,(VKT(J),J=1,NYEARS),AVKT,EKT
000125   READ 410,(RK(J),J=1,NYEARS)
000140   PRINT 510
000144   PRINT 520,CV,WV,WB,PHE,PM,POP
000164   PRINT 530
000170   PRINT 520,GGPK,GOPK,EKWHPK,BRK,BOEM
C
C   MILEAGE
C
000206   FACT=EKT/AVKT
000210   DO 10 J=1,NYEARS
000212   EKP(J)=FACT*VKT(J)
000215   10 CONTINUE
C

```


C SET BATTERY REPLACEMENT FLAG

C
 000217 DO 15 J=1,NYRM1
 000220 BR=BR+EKPY(J)
 000222 TK=TK+EKPY(J)
 000224 IF(BR.LT.BRK)GO TO 15
 000227 KBR(J)=1
 000230 BR=BR-BRK
 000231 15 CONTINUE
 000234 IF(BR+EKPY(NYEARS).LE.BRK.OR.PM.EQ.0.)GO TO 18
 000245 EKPY(NYEARS)=BRK-BR
 000247 BR=BRK
 000247 GO TO 19
 000250 18 BR=BR+EKPY(NYEARS)
 000253 19 TK=TK+EKPY(NYEARS)
 000256 PRINT 533
 000261 PRINT 534
 000265 PRINT 590,(EKPY(J),J=1,11),TK

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C
 C MAINTENANCE COSTS

C
 000301 HEMC=PHE/.746*.003106+.111818
 000304 CMC=WV*.000006+.021742
 000307 EMMC=PM/.746*.001242+.037273
 000312 IF(PM.EQ.0.)EMMC=0.
 000314 BMC=WB*.000248
 000316 FMC=0.
 000317 TMCK=HEMC+CMC+EMMC+BMC+FMC

C
 C REPAIR COST

C
 000324 HERC=PHE/.746*.00497+.173939
 000327 CRC=WV*.000124+.59015
 000332 EMRC=PM/.746*.00124+.05591
 000335 IF(PM.EQ.0.)EMRC=0.
 000337 ARC=WV*.00005
 000341 TRC=(PHE+PM)/.746*.000808+.031061
 000345 TRCK=HERC+CRC+EMRC+ARC+TRC
 000352 DO 20 J=1,NYEARS
 000354 TRCKF(J)=TRCK*RKF(J)
 000357 20 CONTINUE

C
 C FUEL COST

C
 000361 IF(GGPK.EQ.0)GO TO 30
 000362 DO 25 J=1,NYEARS
 000363 PFCKN(J)=(20.90+.7479*(J-1))*GGPK
 000371 PFCKP(J)=(27.17+.9723*(J-1))*GGPK
 000377 PFCKM(J)=(14.63+.5235*(J-1))*GGPK
 000405 EFCKN(J)=(4.23+.0108*(J-1))*EKWHPK
 000413 EFCKM(J)=(3.81+.0097*(J-1))*EKWHPK
 000421 25 EFCKP(J)=(5.50+.014*(J-1))*EKWHPK
 000431 GO TO 36
 000432 30 DO 35 J=1,NYEARS
 000434 PFCKN(J)=(19.36+.6599*(J-1))*GDPK

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000442 PFCKP(J)=(25.17+.8579*(J-1))*GOPK
000450 PFCKM(J)=(13.55+.4619*(J-1))*GOPK
000456 EFCKN(J)=(4.23+.0108*(J-1))*EKWHPK
000464 EFCKM(J)=(3.81+.0097*(J-1))*EKWHPK
000472 35 EFCKP(J)=(5.50+.014*(J-1))*EKWHPK
000502 36 PRINT 540
000506 PRINT 550,HEMC,CHC,EMMC,BMC,FMC,TMCK
000526 PRINT 560
000532 PRINT 550,HERC,CRC,EMRC,ARC,TRC,TRCK
000552 PRINT 570
000556 PRINT 571
000562 PRINT 572,(PFCKN(J),J=1,11)
000574 PRINT 573,(PFCKP(J),J=1,11)
000606 PRINT 574,(PFCKM(J),J=1,11)
000620 PRINT 575,(EFCKN(J),J=1,11)
000632 PRINT 576,(EFCKP(J),J=1,11)
000644 PRINT 577,(EFCKM(J),J=1,11)
000656 DO 37 J=1,11
000660 TFCK(1,J)=PFCKN(J)+EFCKN(J)
000664 TFCK(2,J)=PFCKP(J)+EFCKP(J)
000670 TFCK(3,J)=PFCKM(J)+EFCKM(J)
000674 TFCK(4,J)=PFCKN(J)+EFCKP(J)
000700 37 TFCK(5,J)=PFCKN(J)+EFCKM(J)
000706 PRINT 578
000711 PRINT 584,(TFCK(1,J),J=1,11)

```

C
C
C

COST LOOP

```

000724 DO 300 JCOST=1,2
000726 TDCC=0.
000727 DOCK=0.
000730 DO 38 J=1,5
000731 TAOC(J)=0.
000732 AOCC(J)=0.
000733 TLCC(J)=0.
000734 ALCCCK(J)=0.
000735 TDLCC(J)=0.
000736 38 DLCCCK(J)=0.

```

C
C
C

PAYMENTS

```

000741 PV=CV*2
000743 IF(JCOST.EQ.1)PV=7646.+1.25*(CV-3823.)
000751 PV=PV+PV*.05
000754 AL=PV-PV*POP
000756 AP=(AL+AL*.065*4.)/4.

```

C
C
C

YEARLY DEPENDENT COST

```

000761 YDC1=33.+PV*.01+125.
000766 YDC2=33.+PV*.006+75.

```

C
C
C

BATTERY REPLACEMENT COST

```

000772 BRC=2.*BOEM

```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

LYFECC

```

000774      IF (JCOST.EQ.1) BRC=1.25*BOEM
000777      BRC=BRC+BRC*.05
001002      ADPBR=BRC*PDP
001003      ALBR=BRC-ADPBR
001005      APBR=(ALBR+ALBR*.065*3.)/3.
001010      PRINT 585
001014      PRINT 586
001020      PRINT 590,BRC,ALBR,APBR,BR

```

C
C
C

OPERATING COSTS

```

001034      DO 39 IFUEL=1,5
001036      AOC(IFUEL,1)=YDC1
001040      YDC=YDC1
001041      DO 40 J=2,NYEARS
001042      IF (J.GE.7) YDC=YDC2
001046      AOC(IFUEL,J)=(TMCK+TRCKF(J)+TFCK(IFUEL,J))/100.*EKPY(J)+YDC
001061      40 CONTINUE
001064      AOC(IFUEL,NYEARS)=AOC(IFUEL,NYEARS)-YDC2
001070      IF (NYEARS.LE.6) AOC(IFUEL,NYEARS)=AOC(IFUEL,NYEARS)+YDC2-YDC1
001076      DO 50 J=1,NYEARS
001100      IF (KBR(J).EQ.0) GO TO 50
001102      L=J+2
001104      DO 60 K=J,L
001105      IF (K.GT.NYEARS) GO TO 50
001110      AOC(IFUEL,J)=AOC(IFUEL,J)+ADPBR
001114      AOC(IFUEL,K)=AOC(IFUEL,K)+APBR
001120      60 CONTINUE
001122      50 TAOC(IFUEL)=TAOC(IFUEL)+AOC(IFUEL,J)
001131      39 AOCC(IFUEL)=TAOC(IFUEL)/TK

```

C
C
C

DISCOUNTED OPERATING COSTS

```

001135      DO 80 J=1,NYEARS
001137      DAOC(J)=AOC(1,J)*DF(J)
001143      80 TDOC=TDOC+DAOC(J)
001147      DOCK=TDOC/TK

```

C
C
C

LIFE CYCLE COSTS COMPONENTS

```

001151      VSV=.01*PV
001153      BSV=.5*BRC*(1.-BR/BRK)

```

C
C
C

LIFE CYCLE COSTS

```

001157      DO 85 IFUEL=1,5
001161      YLCC(IFUEL,1)=AOC(IFUEL,1)+PV*PDP
001165      YLCC(IFUEL,NYEARS)=AOC(IFUEL,NYEARS)-BSV-VSV
001174      TLCC(IFUEL)=YLCC(IFUEL,1)+YLCC(IFUEL,NYEARS)
001200      DO 90 J=2,NYRM1
001201      YLCC(IFUEL,J)=AOC(IFUEL,J)
001206      IF (J.GE.2.AND.J.LE.5) YLCC(IFUEL,J)=YLCC(IFUEL,J)+AP
001222      90 TLCC(IFUEL)=TLCC(IFUEL)+YLCC(IFUEL,J)
001231      ALCC(IFUEL)=TLCC(IFUEL)/TK

```

C

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

LYFECC

C DISCOUNTED LIFE CYCLE COSTS

C

```

001234      DO 100 J=1,NYEARS
001235      OYLCC(IFUEL,J)=YLCC(IFUEL,J)*DF(J)
001243      100  TDLCC(IFUEL)=TDLCC(IFUEL)+OYLCC(IFUEL,J)
001250      DLCCCK(IFUEL)=TDLCC(IFUEL)/TK
001252      85  CONTINUE

```

C

C

C OUTPUT

C

```

001254      PRINT 535,JCOST
001262      PRINT 588
001266      PRINT 591
001272      PRINT 590,( AOC(1,J),J=1,11),TAOC(1), AOCK(1)
001311      PRINT 595
001315      PRINT 591
001321      PRINT 590,(DAOC(J),J=1,11),TDOOC,DOCK
001337      PRINT 600
001343      PRINT 591
001347      PRINT 590,(YLCC(1,J),J=1,11),TLCC(1),ALCCCK(1)
001366      DO 120 IFUEL=1,5
001370      PRINT 610
001373      IF(IFUEL.EQ.1)GO TO 125
001375      IF(IFUEL.EQ.2)PRINT 579
001402      IF(IFUEL.EQ.3)PRINT 580
001410      IF(IFUEL.EQ.4)PRINT 581
001416      IF(IFUEL.EQ.5)PRINT 582
001424      125 PRINT 591
001430      120 PRINT 590,(OYLCC(IFUEL,J),J=1,11),TDLCC(IFUEL),DLCCCK(IFUEL)
001451      300 CONTINUE
001453      350 CONTINUE
001456      STOP
001460      400 FORMAT(7I10)
001460      405 FORMAT(1H0,10I4)
001460      410 FORMAT(7E10.4)
001460      500 FORMAT(1H1,*LIFE CYCLE COST ESTIMATION*)
001460      510 FORMAT(1H1,*VEHICLE CHARACTERISTICS*/9X,*COST*,11X,*WEIGHT*,7X
          1TTERY WT.*,3X,*HEAT ENG. RATING*,1X,*ELEC. MOTOR RATING*,2X,*X
          1N*)
001460      520 FORMAT(1H ,8E16.6)
001460      530 FORMAT(1H ,5X,*GAS LT/KM*,6X,*DIESEL LT/KM*,8X,*KWH/KM*,4X,*BA
          1Y REPLACE/KM*,4X,*BOEM*)
001460      533 FORMAT(1H0,*ANNUAL MILEAGE*)
001460      534 FORMAT(1H ,4X,*YEAR 0*,4X,*YEAR 1*,4X,*YEAR 2*,4X,*YEAR 3*,4X,
          1R 4*,4X,*YEAR 5*,4X,*YEAR 6*,4X,*YEAR 7*,4X,*YEAR 8*,4X,*YEAR
          1X,*YEAR 10*,4X,*TOTAL*)
001460      535 FORMAT(1H0,*COST CASE=*,I2)
001460      540 FORMAT(1H0,*MILEAGE DEPENDENT COSTS(CENTS/KM)*/2X,*MAINTENANCE
          15X,*HEAT ENGINE*,7X,*CHASSIS*,7X,*ELEC. MOTOR*,7X,*BATTERY*,9X
          1YWHEEL*,06X,*TOTAL*)
001460      550 FORMAT(1H ,8F15.4)
001460      560 FORMAT(1H ,1X,*REPAIR*/5X,*HEAT ENGINE*,7X,*CHASSIS*,7X,*ELEC.
          1OR*,5X,*ACCESSORIES*,5X,*TRANSMISSION*,4X,*TOTAL*)
001460      570 FORMAT(1H ,1X,*FUEL*)
001460      571 FORMAT(1H+,17X,*YEAR 0*,4X,*YEAR 1*,4X,*YEAR 2*,4X,*YEAR 3*,4X

```

GOLETA FORTRAN 1.3 * SEMI-AUTO RFL * (01-10-73)

LYFECC

```

1AR 4*,4X,*YEAR 5*,4X,*YEAR 6*,4X,*YEAR 7*,4X,*YEAR 8*,4X,*YEAR
13X,*YEAR 10*)
001460 572 FORMAT(1H ,*PETRO(NOMIN)*,1X,12F10.4)
001460 573 FORMAT(1H ,*PETRO(+30%)*,2X,12F10.4)
001460 574 FORMAT(1H ,*PETRO(-30%)*, 2X,12F10.4)
001460 575 FORMAT(1H ,*ELECT(NOMIN)*,1X,12F10.4)
001460 576 FORMAT(1H ,*ELECT(+30%)*,2X,12F10.4)
001460 577 FORMAT(1H ,*ELECT(-10%)*, 2X,12F10.4)
001460 578 FORMAT(1H ,*TOTAL*)
001460 579 FORMAT(1H+,27X,* (PETROLEUM +30%)* )
001460 580 FORMAT(1H+,27X,* (PETROLEUM -30%)* )
001460 581 FORMAT(1H+,27X,* (ELECTRICITY +30%)* )
001460 582 FORMAT(1H+,27X,* (ELECTRICITY -10%)* )
001460 584 FORMAT(1H+,13X,12F10.4)
001460 585 FORMAT(1H0,*BATTERY REPLACEMENT*)
001460 586 FORMAT(1H ,3X,*BR COST*,3X,*BR LOAN*,2X,*BR PAYMT*,1X,*MILEAGE-
IT BATTERY SET*)
001460 588 FORMAT(1H ,*ANNUAL OPERATING COSTS*)
001460 589 FORMAT(1H ,11F10.4)
001460 590 FORMAT(1H ,12F10.2,F10.5)
001460 591 FORMAT(1H ,4X,*YEAR 0*,4X,*YEAR 1*,4X,*YEAR 2*,4X,*YEAR 3*,4X,*
1R 4*,4X,*YEAR 5*,4X,*YEAR 6*,4X,*YEAR 7*,4X,*YEAR 8*,4X,*YEAR 9
1X,*YEAR 10*,4X,*TOTAL*,5X,*PER KM*)
001460 595 FORMAT(1H0,*DISCOUNTED ANNUAL OPERATING COSTS*)
001460 600 FORMAT(1H0,*LIFE CYCLE COSTS*)
001460 610 FORMAT(1H0,*DISCOUNTED LIFE CYCLE COSTS*)
01460 END

```

A P P E N D I X C 3

"ENERGY AND MATERIALS - CURRENT MODEL AUTOMOBILES"

ENERGY AND MATERIALS - CURRENT MODEL AUTOMOBILES

Materials Composition

Excellent agreement has been obtained among the several recent studies which describe the materials composition of modern automobiles. (1-5) Percentage compositions of ferrous metals, aluminum alloys, copper and copper alloys, zinc, glass, rubber, and plastics are changing slowly due to the gradual substitution of lighter materials. In any given year, however, the mass fraction of each particular material appears to be reasonably constant over a range of car weights.

Table I shows the estimated weight breakdown for automobiles as estimated by a 1975 study. (2) The same table gives the author's estimate for 1979 model cars, in the form of a rounded-off interpolation. * These estimated 1979 values will be carried forward to the manufacturing energy estimates.

Energy to Manufacture Automobiles

The investigators Hirst and Herendeen have estimated that it requires 123 million Btu to manufacture a typical American automobile. (6) This figure is similar to a value of 126 million Btu cited by Berry and Fels. (7) McGowan and Kirchoff, by contrast, calculated the manufacturing energy per car to be only 34 million Btu. (8)

* The author of this section was also a principal contributor to the materials accounting in Reference (2).

Table I - Weight Percentage Materials Composition of Automobiles

(Based on Estimates from Reference 2 for 1975, 1980;
and 1990 and an updated estimate by the author for 1979)

<u>Material</u>	Est. for <u>1975</u>	<u>Projections for</u>		Author's Est. for <u>1979</u>
		<u>1980</u>	<u>1990</u>	
Low carbon and alloy steel	61.2	56.9	54.2	60.0
Cast and malleable iron	16.2	13.6	7.9	14.0
Aluminum alloys	2.9	6.3	11.9	4.5
Copper and copper alloys	1.0	1.0	0.6	1.0
Zinc	0.8	0.4	0.3	0.6
Lead	0.7	0.8	0.7	0.8
Other metals, incl. magnesium	0.3	0.7	1.4	0.5
Rubber	4.6	5.1	5.0	5.0
Glass	2.4	2.6	2.8	2.6
Plastic	3.5	6.7	9.2	5.0
Other non-metal	<u>6.5</u>	<u>5.9</u>	<u>6.0</u>	<u>6.0</u>
Totals	100.1	100.0	100.0	100.0

Energy requirements to produce basic materials and components has not been a subject of close agreement. References differ, of course on the basis for the estimates; some include only the energy for smelting or processing, while others include the activities of mining, ore transportation, rolling and component fabrication. One must also distinguish between electrical energy and powerplant fuel consumed.

Table II identifies manufacturing energy estimates from several sources, and also sets forth the figures which will be assumed for this present task. These last figures represent our best present estimates of total energy typical for components made of each material, from mine or petroleum feed stock to finished parts. Actual total energies can vary widely with the characteristics of the ore, transportation, method of fabrication, and percentages of scrap vs. virgin materials used.

A final step is to do a trial accounting of the total energy to produce a complete automobile. We have taken as a 1979 baseline a U.S.-produced automobile of 3,620 lb. curb weight, such as the Ford LTD 4-door sedan. This is a six-passenger vehicle with a 302 CID V-8 engine and a wheelbase of 114.4 inches. The results of the energy accounting are given in Table III. A subtotal of 122.6 million Btu is the estimated energy to produce the parts from which the vehicle is assembled. To this must be added the energy to transport the components to the assembly plant, and then the energy to assemble and paint the vehicle. If subassemblies and parts equal to the car's total mass were transported an average of 100 miles, the fuel energy for truck transportation would be about 430,000 Btu. This is based on a referenced figure of 0.0176 gallon of diesel fuel per ton-mile of freight hauled. (15)

A rough estimate of energy expended at the assembly plant can be based on an assumption that about 10 kW might be expended over a ten hour period per car. This is for conveying and hoisting, welding, power tools, paint drying,

Table II - Estimates of Manufacturing and Processing Energy
for Materials and Components Used in Automobile
Production

<u>Material or Component</u>	<u>Quoted Energy, Btu /lb</u>	<u>Quoted from Reference</u>	<u>Value Used, This Study, Btu/lb</u>
Alloy Steel	22,300	(9)	
Stainless Steel	34,000	(9)	
Steel (Material Processing)	21,500	(3)	
Iron (Material Processing)	15,500	(3)	
Steel (Material Processing)	13,250	(10)	
Steel Auto Hood (Mine to formed part)	28,000	(11)	
Aluminum Hood (45% virgin mat'l)	108,300	(11)	
Aluminum - Primary (Mat'l Processing)	110,000	(3)	
Aluminum - from Scrap (Mat'l. Processing)	10,000	(3)	
Aluminum smelting (Present processes)	22,180	(12)	
Aluminum smelting (New Alcoa process)	15,350	(12)	
Alum (Total energy of metal, from 50% bauxite)	140,900	(13)	
Copper (Total energy metal, from 1.5% ore)	26,780	(13)	
Copper (Total energy metal, from 0.6% ore)	49,540	(13)	
Copper and Alloys	65,700	(9)	
Zinc Castings	45,500	(9)	45,500
Lead	14,700	(14)	15,000
Plastics	25,000	(9)	
Plastics (Incl. feed stock)	78,500	(10)	78,500
Fiber Glass-Reinforced Plastic Hood	40,100	(11)	
Fuel Value, Resin Raw Mtl.	20,000	(11)	
Rubber	37,000	(3)	37,000
Glass	13,000	(3)	13,000

(Table II continued on next page)

Table II - Continued

<u>Material or Component</u>	<u>Quoted Energy, Btu /lb</u>	<u>Quoted from Reference</u>	<u>Value Used, This Study, Btu /lb</u>
Other Materials	37,000	(3)	37,000
Stamped Steel Parts	- -	- -	28,000
Cast Iron Parts, Incl. Machining	- -	- -	20,000
Formed Aluminum Parts (45% Virgin)	- -	- -	108,000
Finished Copper and Cu Alloy Parts	- -	- -	50,000

Table III - Estimate of Manufacturing Energy for an
 Automobile of 3,620 lb Curb Weight
 (1979 Model Year 4-Door Sedan)

<u>Material, Component, or Process</u>	<u>Mass Fraction, %</u>	<u>Mass, lb</u>	<u>Specific Energy, Btu/lb</u>	<u>Total Energy, Thous. Btu</u>
Steel Components	60.0	2,172	28,000	60,816
Cast and Malleable Iron Parts	14.0	507	20,000	10,140
Aluminum Alloy Parts	4.5	163	108,000	17,604
Copper, Cu Alloy Components	1.0	36	50,000	1,800
Zinc Castings	0.6	22	45,500	1,001
Lead	0.8	29	15,000	435
Rubber	5.0	181	37,000	6,697
Glass	2.6	94	13,000	1,222
Plastic	5.0	181	78,500	14,209
Other Materials and Parts	<u>6.5</u>	<u>235</u>	<u>37,000</u>	<u>8,695</u>
Subtotals	100.0	3,620		122,619
Transportation, Parts and Subassemblies				430
Assembly Plant Energy				<u>1,140</u>
Est. Total Manufacturing Energy				124,189
(Or Approximately 124 million Btu per Car)				

and general utility supply to the plant. The electrical energy required is about 100 kWh or 341,200 Btu this is raised to 1.14 million Btu fuel energy input if the conversion of fuel to delivered electricity is 30% efficient.

Our estimate of total manufacturing energy per car is 124 million Btu. It is interesting how close this independent estimate is to the 123 million Btu calculated by Hirst and Herendeen. (6)

The energy to produce batteries is of interest from the point of view of manufacturers and owners of electric or hybrid vehicles. From estimates given by Williams in Ref. (14), we calculate that the energy to manufacture an advanced lead-acid battery will be about 15,700 Btu per lb of battery weight. Williams has identified such a battery as having a specific energy of 18 Wh/lb. It should be noted that since 15,700 Btu is the equivalent of the 4,600 Wh of energy to manufacture a pound of battery, the battery would have to undergo the equivalent of over 250 complete discharges before the cumulative stored energy would exceed the original manufacturing energy. In other words, the manufacturing energy is very significant in relationship with the total energy the battery will store over its lifetime.

THE SCRAPPING AND RECYCLING OF AUTOMOBILES:
MATERIALS AND ENERGY IMPLICATIONS

Materials Recovery

The materials composition of present and possible future automobiles was given in Table I, and is discussed in detail by References (2) and (5). Approximately ten years after the date of manufacture, cars of these compositions will appear in large numbers in the junkyards.

Ford Motor Co. investigators have stated that the motor vehicle registrations are terminated on about 9 million cars/yr at this time, and that about 90% of these are now being recycled for their metal content - primarily the ferrous metals. (5) These authors further estimate that of the available automotive scrap (in 1974), 85% of the ferrous metal was recovered. Similarly, the recycling ratios for copper, aluminum, and zinc were 62%, 53%, and 27% respectively. It may be inferred that with currently improving techniques for the separation of shredded scrap, the recycling ratios for aluminum and copper will improve. Zinc, since much of it is in the form of galvanized panels and trim, will continue to be difficult to recover.

Not much in the way of plastics is now being recycled, although in the future some economical methods of doing this may be developed. At least two alternatives are to somehow reconstitute the scrap by chemical means, or else to use the scrap plastic as fuel. The average heating value of such material is probably in the range 15,000 - 20,000 Btu /lb. A present objection to burning many plastics is the toxic nature of the combustion products.

The lead from storage batteries is eminently recyclable, and each automobile uses about three or four batteries during its lifetime. Most of the replacement batteries are salvaged in the trade-in process, as are those finally ending up in wrecking yards.

Steps in Resource Recovery

Usually the steps involved in recycling automobiles are:

1. The vehicle is transported to a local wrecking yard (dismantler).
2. A dismantler salvages parts worth reselling, which is a larger fraction in the case of late-model wrecks than for worn-out obsolete cars. In the latter instance, the tires, battery, radiator, and other easy-to-remove parts with a high scrap value are removed. Sometimes the engine and drive train are also removed at this point. The bulk is then flattened or compacted for efficient transport.
3. The bulk is shipped to a processing center, where it is either baled or shredded. Shredding is becoming the preferred technique since it results in a higher grade of ferrous scrap and allows segregation of the other materials. Many shredding plants can take engine blocks and all.
4. Recovered materials are shipped to smelters or foundries. Not all of the material finds its way back to Detroit; much of the ferrous scrap (for example) goes to regional steel mills to be turned into reinforcing bar and structural shapes.

Energy Consumption in Resource Recovery

Transportation- The average number of ton-miles of transportation is not known to us, but one scenario might be the following:

- The entire car, 3620 lb is shipped 20 miles to dismantler.
- After removing 300 lb of material, the remaining 3320 lb is forwarded to shredder, 100 miles away.
- Non-metallics and some lost metal are landfilled near the shedder; assume 2,700 lb metal to be reclaimed is shipped 500 miles further to regional smelters.

- If most of the ferrous material goes to regional steel mills, this might still leave about 1000 lb. smelted metal to be sent another 1000 miles to new users including the auto industry.

The above shipments total 1377 ton-miles. Again using a payload-specific fuel consumption of 0.0176 gal diesel fuel/ton-mile, ⁽¹⁵⁾ the aggregate transportation fuel energy would be 3.27 million Btu per recycled automobile. Other assumptions or conditions could alter this outcome appreciably.

Dismantler's Activities - Since dismantling is a labor-intensive activity, not much fuel energy is expended during this part of the process. Hoisting, flame-cutting, in-yard movements, and flattening of the hulk may consume 4 kWh per car at 20% efficiency, or a gross expenditure of 68,240 Btu per car. If 3,620 lb scrap is handled, the specific energy would be 19 Btu /lb.

Shredder - Based on conversations with the operators of shredding plants, one automobile can be shredded in 15 seconds to one minute even with engine block and drive train still in the vehicle. This is a very energy-intensive operation, since around 4000 hp is used to drive a hammer mill. Another 2000 hp or so is dedicated to segregation of the resulting scrap particles, and this process is expected to keep pace with the shredding. Our very provisional estimate, based on an assumed 20 seconds for a "car" to pass through each process and then adding 20% more energy for plant idling and overhead consumption, is 339,000 Btu per hulk.

Total Energy for Resource Recovery - The above energy elements are summed up in Table IV. The total energy for scrapping a 3620-lb passenger car and recovering an appreciable fraction of its resources is roughly estimated as 3.7 million Btu. This does not include smelting or process energy to be charged against the next use.

Table IV - Provisional Estimate of Energy Required to Recover Resources from a Junked Automobile

Basis: Original curb weight 3620 lb, and assumptions given in text. These assumed conditions are subject to wide variations.

<u>Activity</u>	<u>Energy for Activity Thous. Btu</u>
Shipping, aggregate of 1408 ton-miles	3,270
Dismantling and Flattening	68
Shredding and Sorting	<u>339</u>
Total Energy Required	3,677

(Approximately 3.7 million Btu. Does not include smelting or process energy for the next use.)

Approximate Mass Accountability:

Removed by dismantler for materials recycling - - -	200 lb *
Removed by dismantler for parts resale - - - - -	100
Metal salvaged by shredder - - - - -	2,700
Lost metal and non-metal to landfill - - - - -	<u>620</u> **
Original Curb Weight - - - - -	3,620 lb

* Includes some eventual loss such as battery case materials.

** Includes 5% loss of iron and steel, 25% loss of aluminum, and 12 lb loss of zinc.

The largest energy element by far in this total is transportation fuel. Even if this transportation component were assumed to be much less (perhaps through the economies of rail shipment, rather than by truck), it would still dominate the recycling energy requirement.

A recycling energy of almost 4 million Btu per car is to be compared with 124 million Btu to manufacture that car. While the 124 million Btu already includes the energy benefit of some scrap metal recycling, further study could reveal something of the sensitivity to ratio of recycled to virgin materials.

REFERENCES

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