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APPENDIX B

AIR EMISSION RATE CALCULATIONS

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APPENDIX B

AIR EMISSION RATE CALCULATIONS

I. MINE CONSTRUCTION

1. Drilling and Blasting - These procedures were used to estimate TSP emissions from the different shaft sinkings (i.e., main, intake air) and general underground development, and are presented under its respective heading below.

- a. Construct Mine Support Facilities - Blasting using dynamite

Emission Factor and Source: TSP-EF for emitted particles of less than or equal to 30 um; U.S. EPA (EPA, 1983) AP-42, Table 8.24-2, Blasting - Surface Coal Mining

$$\text{TSP-EF} = \frac{344(A)^{0.8}}{(D)^{1.8}(M)^{1.9}}$$

where:

A = area blasted - m²

D = hole depth - m

M = material moisture content - %

SO₂(H₂S) - 3.0 kg/t of dynamite, AP-42, Table 11.3-1

CO - 141.0 kg/t of dynamite, AP-42, Table 11.3-1

Sink Main Shaft

A = (8.5 m/2)² x 3.14 ÷ 2 = 28.36 m² (i.e., one-half of area/blast)

D = 2.12 m

M = 15%

$$\text{TSP-EF} = \frac{344(28.36)^{0.8}}{(2.12)^{1.8}(15)^{1.9}} = 7.5 \text{ kg/blast} \times 2 \text{ blasts/day} = 15.1 \text{ kg/d}$$

Process Rate:

TSP - 2 blasts/day, 30 blast days/month and 514 blast days/17 months

SO₂(CO) - 160 kg dynamite/blast

- 160 kg dynamite/h, 319 kg dynamite/d, 115 t dynamite/y

Example Calculation:

$$\text{TSP} - 514 \text{ blast days/17 months} \times 15.1 \text{ kg/day} \times \text{t}/1000 \text{ kg} = 7.8 \text{ t}/17 \text{ months}$$

$$\text{SO}_2 - 160 \text{ kg dynamite/h} \times 3.0 \text{ kg/t} \times \text{t}/1000 \text{ kg} = 0.48 \text{ kg/h}$$

$$\begin{aligned} \text{Total TSP (Sink Main Shaft)} &= 8.6 \text{ st}/17 \text{ months (1986-87)}; 6.1 \text{ st/yr (1986)} \\ \text{SO}_2 &= 0.49 \text{ t}/17 \text{ months (0.54 st}/17 \text{ months)}; \\ &0.35 \text{ t/y (0.39 st/yr)} \\ \text{CO} &= 23.1 \text{ t}/17 \text{ months (25.4 st}/17 \text{ months)}; 16.3 \\ &\text{t/y (17.9 st/yr)} \end{aligned}$$

Sink and Equip Air Intake Shaft

$$A = (6.1 \text{ m}/2)^2 \times 3.14 \div 2 = 14.6 \text{ m}^2 \text{ (i.e., one-half of area/blast)}$$

$$D = 2.12 \text{ m}$$

$$M = 15\%$$

$$\text{TSP-EF} = \frac{344(14.6)^{0.8}}{(2.12)^{1.8}(15)^{1.9}} = 4.4 \text{ kg/blast} \times 3 \text{ blasts/day} = 13.3 \text{ kg/d}$$

Process Rate:

$$\text{TSP} - 3 \text{ blasts/day, 75 blast days/month and 326 blast days}/10 \text{ months}$$

$$\begin{aligned} \text{SO}_2(\text{CO}) &- 84.4 \text{ kg/dynamite blast} \\ &- 84.4 \text{ kg/dynamite/h, 253 kg dynamite/d, 27.5 t dynamite}/10 \text{ months} \end{aligned}$$

Example Calculation:

$$\text{TSP} - 326 \text{ blast days}/10 \text{ months} \times 13.3 \text{ kg/day} \times \text{t}/1000 \text{ kg} = 4.3 \text{ t}/10 \text{ months}$$

$$\text{SO}_2 - 84.4 \text{ kg dynamite/h} \times 3.0 \text{ kg/t} \times \text{t}/1000 \text{ kg} = 0.25 \text{ kg/h}$$

$$\begin{aligned} \text{Total TSP (Air Intake Shaft)} &= 4.7 \text{ st}/10 \text{ months (1986-87)}; 2.6 \text{ st/yr (1986)} \\ \text{SO}_2 &= 0.08 \text{ t}/10 \text{ months (0.09 st}/10 \text{ months)} \\ \text{CO} &= 3.9 \text{ t}/10 \text{ months (4.3 st}/10 \text{ months)} \end{aligned}$$

Construct East Exhaust Shaft (Raise) - EER

$$A = (6.1 \text{ m}/2)^2 \times 3.14 - (2.4 \text{ m}/2)^2 \times 3.14 = 24.7 \text{ m}^2$$

$$D = 3.0 \text{ m}$$

$$M = 15\%$$

$$\text{TSP-EF} = \frac{344(14.6)^{0.8}}{(3.0)^{1.8}(15)^{1.9}} = 3.6 \text{ kg/blast} \times 3 \text{ blasts/day} = 10.8 \text{ kg/d}$$

Process Rate:

TSP - 3 blasts/day, 21 blast days/total(yr)
SO₂(CO) - 220.0 kg dynamite/blast
- 220.0 kg dynamite/h, 660 kg dynamite/d, 13.9 t
dynamite/total(yr)

Example Calculation:

TSP - 21 blast days/total x 10.8 kg/day x t/1000 kg = 0.2 t/yr
SO₂ - 220 kg dynamite/h x 3.0 kg/t x t/1000 kg = 0.66 kg/h

Total TSP (EER) = 0.3 st/yr (Construction Phase - Year 3)
SO₂ = 0.04 st/yr
CO = 2.2 st/yr

Construct West Exhaust Shaft (Raise) - WER

TSP = Same as EER

Total TSP (WER) = 0.3 st/yr (Construction Phase - Year 4)
SO₂ = 0.04 st/yr
CO = 2.2 st/yr

- b. Underground Mine Development - Use of 90% ANFO and 10% water gel for blasting rock openings of varying dimensions during shaft construction.

Emission Factors and Source:

TSP - 0.0013 kg/t (for blasting overburden and coal); From AMC* report on "Fugitive Dust Emission Factors for the Mining Industry," Appendix p. D-3 - Colorado Fugitive Emissions.

SO₂ - 1.0 kg/t of ANFO, AP-42, Table 11.3-1

NO_x - 8.0 kg/t of ANFO, AP-42, Table 11.3-1

CO - 34.0 kg/t of ANFO, AP-42, Table 11.3-1

Pb - 0.0094 kg/t of rock, AP-42, Tables 7.18-1 and 8.22-1.

*American Mining Congress

Process Rate:

<u>Year</u>	<u>Waste Rock (k-st)</u>	<u>Ore (k-st)</u>	<u>Total (k-st)</u>	<u>st/yr</u>
1986	11	-	11	0.01
1987	66	-	66	0.09
1988	763	532	1295	1.7
1989	1146	1700	2846	3.7
1990	396	2814	3210	4.2*

*See Table 4.1 - Mine (Operation) Production, 1. Initial

Peak Production Levels Expected

	<u>Hourly</u>	<u>Daily</u>	<u>Yearly</u>
Rock			
Stope	163,400 t	163,400 t	1,545,455 t
Drifts	1,793 t	5,380 t	1,041,818 t
ANFO Ratio			
Stope	0.45 kg/t	0.45 kg/t	0.45 kg/t
Drifts	1.81 kg/t	1.81 kg/t	1.81 kg/t
ANFO Total	76.8 t	83.3 t	3,107 t

Duration: As required by process rate.

Control Method and Efficiency: Residence settling and humid underground environment.

Example Calculation:

Process Rate x Emission Factor = Emission Rate

$$\begin{aligned} \text{TSP} &- 2,846,000 \text{ st/yr} \times 0.0026 \text{ lb/st} \times \text{st}/2000 \text{ lbs} = 3.7 \text{ st/yr} \\ \text{SO}_2 &- 3,107 \text{ t/yr} \times 1.0 \text{ kg/t} \times 2.2 \text{ lb/kg} \times \text{t}/1.1 \text{ st} \times \text{st}/2000 \text{ lbs} \\ &= 3.1 \text{ st/yr} \end{aligned}$$

Total TSP (Underground Mine Development) = 3.7 st/yr

SO₂ = 3.1 st/yr

NO_x = 24.9 st/yr

CO = 105.6 st/yr

Pb = 0.003 st/yr

Emitting Device: Total quantity of component air emissions will exit the mine at the east and west exhaust shafts (EER & WER). Each shaft will have two fans similar to a Joy M108-58 that will produce approximately 460,000 cfm at 900 hp each.

2. Power Generation (Construction) - The use of temporary diesel generators may be necessary for the first six months of the construction phase if transmission line electrical power is not available at the site. One 2500-kw unit will be required during these months to supply electrical power for mine shaft and mine/mill surface facilities construction. The resultant emissions from this unit were estimated as follows:

Diesel Generator

Emission Factors and Source: AP-42, Appendix - C, Internal Combustion - electric generation - diesel

TSP - 13.0 lbs/10³ gal
SO_x - 140.0 lbs/10³ gal
NO_x - 370.0 lbs/10³ gal
CO - 225.0 lbs/10³ gal
HC - 37.0 lbs/10³ gal

Process Rate: 161 gal/hr, 3,864 gal/day, and 108,192 gal/month

Duration: First six months of construction phase

Control Method and Efficiency: None

Example Calculation:

TSP - 108,192 gal/month x 13.0 lbs/10³ gal x 6 months x st/2000 lbs =
4.2 st/yr

	st/yr
TSP:	4.2
SO _x :	45.4
NO _x :	120.0
CO :	73.0
HC :	12.0

3. Mine Air Heating - Use of natural gas for direct fired mine air heating during construction. Heat content is 1000 btu/ft³.

Emission Factors and Source:

TSP - 10.0 lb/10⁶ft³, NEDS-APP.C-12/75, Nat. Gas 10-100 10⁶btu/hr
SO₂ - 0.6 lb/10⁶ft³, NEDS-APP.C-12/75, Nat. Gas 10-100 10⁶btu/hr
NO_x - 120.0 lb/10⁶ft³, NEDS-APP.C-12/75, Nat. Gas 10-100 10⁶btu/hr

CO - 20.0 lb/10⁶ft³, NEDS-APP.C-12/75, Nat. Gas 10-100 10⁶btu/hr
HC - 8.0 lb/10⁶ft³, NEDS-APP.C-12/75, Nat. Gas 10-100 10⁶btu/hr

Process Rate:

Estimated Peak Production Levels

<u>Hourly</u>	<u>Daily</u>	<u>Yearly</u>
0.0844 10 ⁶ ft ³	2.026 10 ⁶ ft ³	76.01 10 ⁶ ft ³

Duration: As required by process rate.

Control Method and Efficiency: Use of clean burning natural gas in a highly efficient direct fired furnace.

Example Calculation:

Process Rate x Emission Factor = Emission Rate

TSP:

$$0.0844 \text{ 10}^6\text{ft}^3/\text{hr} \times 10.0 \text{ lb}/10^6\text{ft}^3 = 0.84 \text{ lb/hr}$$

Emitting Device: Same as drilling and blasting

4. Mine Vehicles - Use of diesel equipment to move personnel, materials, and rock during mine construction. Diesel fuel will contain 0.4 weight percent sulfur maximum.

Emission Factors and Source:

TSP - 11.0 lb/10³ gal fuel (1.61 g/kg fuel) - page 62*
SO₂ - 31.0 lb/10³ gal fuel NEDS-off road construction equipment
NO_x - 108.5 lb/10³ gal fuel (15.9 g/kg fuel) - page 81*
CO - 1.01 lb/10³ gal fuel (0.295 g/kg fuel) - page 69*
HC - 1.97 lb/10³ gal fuel (0.289 g/kg fuel) - page 66*

*All factors were obtained from "Emission Control of a Deutz F6L-714 diesel engine, derated for underground use, by application of water/oil fuel emissions" by A. Lawson, E. W. Simmons, and M. Piatt, March 30, 1979.

Process Rate:

Peak Volumes of Diesel Fuel Used

<u>Hourly</u>	<u>Daily</u>	<u>Yearly</u>
157.8 gal	3076.7 gal	926,398 gal

Duration: As noted by process rate.

Control Method and Efficiency: Use of cleaning burning air cooled Deutz engines with a catalytic scrubber. All emission factors include control, except SO₂.

Example Calculation:

Process Rate x Emission Factor = Emission Rate

TSP:

$$0.1578 \times 10^3 \text{ gal/hr} \times 11.0 \text{ lb}/10^3 \text{ gal fuel} = 1.73 \text{ lb/hr}$$

II. MINE OPERATION

1. Drilling and Blasting - Blasting of rock using 90% ANFO and 10% water gel for production stope blasting and drift development.

a. Underground Blasting

Emission Factor and Source: AP-42, Table 8.24-2, Blasting-surface coal mining.

$$\text{TSP-EF} = \leq 30 \text{ um}$$

$$\text{TSP-EF} = \frac{344(A)^{0.8}}{(D)^{1.8}(M)^{1.9}}$$

where:

A = area blasted - m²

D = hole depth - m

M = material moisture content - %

SO₂ - 1.0 kg/t of ANFO, AP-42, Table 11.3

NO_x - 8.0 kg/t of ANFO, AP-42, Table 11.3

CO - 34.0 kg/t of ANFO, AP-42, Table 11.3

Pb - 0.00094 kg/t of rock, AP-42, Tables 7.18-1 and 8.22-1

Process Rate:

Estimated Peak Production Levels (1993)

	<u>Hourly</u>	<u>Daily</u>	<u>Yearly</u>
Rock			
Stope	163,400 t	163,400 t	3,276,000 t
Drifts	1,130 t	3,390 t	353,000 t
ANFO Ratio			
Stope	0.45 kg/t	0.45 kg/t	0.45 kg/t
Drifts	1.81 kg/t	1.81 kg/t	1.81 kg/t
ANFO Total	75.6 t	79.7 t	2,113 t

Production Stopes

A = 45 m x 20 m = 900 m²

D = 1/2 depth of stope drillhole - 60 m

M = material moisture content - 4% minimum

$$\text{TSP-EF} = \frac{344(900)^{0.8}}{(60)^{1.8}(4)^{1.9}} = 3.6 \text{ kg/blast}$$

Stope blast material weight (W) = Volume (V) x Density
 $V = 900 \text{ m}^2 \times 60 \text{ m} = 54,000 \text{ m}^3/\text{stope blast}$
 Density = 3.026 t/m^3

$$W = 54,000 \text{ m}^3/\text{stope blast} \times 3.026 \text{ t/m}^3 = 163,404 \text{ t/stope blast}$$

$$3,276,000 \text{ t/yr} \div 163,404 \text{ t/stope blast} \times 3.6 \text{ kg/blast} \times$$

$$\text{t/1000 kg} = 0.07 \text{ t/yr}$$

Development Headings

$A = 3.5 \text{ m} \times 5 \text{ m} = 17.5 \text{ m}^2$
 D = depth of heading drill hole - 3.66 m
 M = material moisture content - 4%

$$\text{TSP-EF} = \frac{344(17.5)^{0.8}}{(366)^{1.8}(4)^{1.9}} = 23.6 \text{ kg/blast}$$

$W = V \times \text{Density}$
 $V = 17.5 \text{ m}^2 \times 3.2 \text{ m} = 56 \text{ m}^3$
 Density = 3.026 t/m^3

Duration: As required by process rate.

Control Method and Efficiency: Residence settling and humid underground environment.

Example Calculation:

Process Rate x Emission Factor = Emission Rate

$$\text{SO}_2 - 75.6 \text{ t/h} \times 1.0 \text{ kg/t} = 75.6 \text{ kg/h}$$

TSP:

$$W = 56 \text{ m}^3/\text{heading blast} \times 3.026 \text{ t/m}^3 = 169.5 \text{ t/heading blast}$$

$$353,000 \text{ t/yr} \div 169.5 \text{ t/heading blast} \times 23.6 \text{ kg/heading blast} \times$$

$$\text{t/1000 kg} = 49.2 \text{ t/yr}$$

Total TSP (underground blasting) = 49.2 t/yr before gravity settling.

Underground Blasting Emissions With Gravity Settling:

Production Stopes and Development Headings - using average distances and velocities to the mine exhaust shafts (Use 350 m level stope 3-18 as a typical scheme).

Mine ventilation air stream branch velocities:

<u>Horizontal Velocity ft/minute</u>	<u>Distance ft</u>	<u>Time Minutes</u>
137	345	2.5
86	267	3.1
621	628	1.0
417	510	1.2
732	979	<u>1.3</u>

Total = 9.1 minutes (546 seconds) - (i.e. horizontal airways only) for travel time from blast area to exhaust shaft.

Emission Factor and Source: AP-42, Appendix A-1, Stone quarrying and processing - crushing

Particle Size Distribution				
<u>< 5 um</u>	<u>5 to 10 um</u>	<u>10 to 20 um</u>	<u>20 to 30 um</u>	<u>>30 um</u>
25%	25%	25%	25%	0

Settling velocity: Particle density = 3.026 t/m³

Settling height, average: 2.0 m

<u>Weight Percent</u>	<u>Particle Size (um)</u>	<u>Vertical Settling Velocity (m/sec)</u>		<u>Time (sec)</u>	=	<u>Settled Distance</u>
25%	<5	0.0036	x	546	=	1.96 m passed
25%	7.5 (5-10)	0.00637	x	546	=	3.48 m settled
25%	15 (10-20)	0.0254	x	546	=	13.87 m settled
25%	25 (20-30)	0.058	x	546	=	31.67 m settled

Determination of % Control (i.e. percent settled): Using a settling height of 2 m, all particles in the <5 um range are assumed to remain in the air stream. Therefore, 75% overall control (i.e. percent settled) is estimated for gravity settling of blasting TSP emissions.

Total TSP (underground blasting) with gravity settling estimated in the air stream from mine exhaust shafts.

49.3 t/yr x 0.25 (i.e. 1 - decimal fraction settled) = 12.3 t(13.6 st)/yr

b. Rock Handling

Handling Emissions at Stope Drawpoints and Development Headings:

Rock handling performed by LHD equipment. A maximum of 12 units in operation at any given time.

Emission Factor and Source: AP-42, Table 8.23-1, p. 8.23-4.

The use of this AP-42 section is not directly applicable because of the large size of the mined rock. However, the ore and waste rock is expected to have a moisture content of no less than 4% by weight and is considerably larger than that encountered after coarse rock crushing. Therefore, the values presented in EPA Table 8.23-1 are a conservative estimate of TSP emissions.

TSP-EF = 0.005 kg/t - Handling of high moisture rock

Process Rate: 900 t/hr, 16,000 t/day, 3,629,000 t/yr for ore and waste rock at maximum production rate.

Duration: As noted in process rate.

Control Method and Efficiency: Wetting dry piles.

Example Calculation:

TSP - 3,629,000 t/yr x 0.005 kg/t ÷ 1000 kg/t = 18.1 t/yr

Total TSP (stope drawpoints and development headings) = 18.1 t/yr before gravity settling.

Handling Emissions at Stope Drawpoints and Development Headings With Gravity Settling:

Emission Factor and Source: AP-42 Appendix A, Table A-1, p. A-3, Stone quarrying and processing - crushing

Particle Size Distribution				
<u><5 um</u>	<u>5 to 10 um</u>	<u>10 to 20 um</u>	<u>20 to 44 um</u>	<u>>44 um</u>
5%	5%	5%	10%	75%

Settling parameters and mine ventilation air stream branch velocities are the same as for the underground blasting emissions.

Weight Percent	Particle Size (um)	Vertical Settling Velocity (m/sec)		Time (sec)	Settled Distance
5%	<5	0.0036	x	546	= 1.96 m passed
5%	7.5 (5-10)	0.00637	x	546	= 3.48 m settled
5%	15 (10-20)	0.0254	x	546	= 13.87 m settled
10%	25 (20-44)	0.058	x	546	= 31.67 m settled
75%	>44	0.181	x	546	= 98.83 m settled

Determination of % Control (i.e. percent settled): Using a settling height of 2 m, all particles <5 um are assumed to settle. Therefore, 95% overall control (i.e. percent settled) is estimated for gravity settling of stope and development headings rock handling.

Total TSP (stope drawpoints and development headings) with gravity settling estimated in the air stream from the mine exhaust shafts.

$$18.1 \text{ t/yr} \times 0.05 \text{ (i.e. 1 - decimal fraction settled)} = 0.9 \text{ t(1.0 st)/yr}$$

Emissions from Handling at Orepasses and Waste Rock Passes:

Emission Factor and Source: AP-42, Table 8.23-1.

TSP-EF = 0.005 kg/t - Handling of high moisture rock

Process Rate: 900 t/hr, 16,000 t/day, 3,629,000 t/yr

Duration: As noted in process rate.

Control Method and Efficiency: Wetting if necessary.

Example Calculation:

$$\text{TSP} = 3,629,000 \text{ t/yr} \times 0.005 \text{ kg/t} \div 1000 \text{ kg/t} = 18.1 \text{ t/yr}$$

Total TSP (orepasses and waste rock passes) = 18.1 t/yr before gravity settling.

Emissions from Handling at Orepasses and Waste Rock Passes with Gravity Settling:

Mine ventilation air stream branch velocities:

<u>Horizontal Velocity ft/Minute</u>	<u>Distance ft</u>	<u>Time Minutes</u>
621	628	1.0
417	510	1.2
732	979	<u>1.3</u>

Total = 3.5 minutes (210 seconds) -
(i.e. horizontal airways only) for air travel time from load area to exhaust shaft.

Emission Factor and Source: AP-42, Appendix A, Table A-1, p. A-3, Stone quarrying and processing - crushing

Particle Size Distribution				
<u><5 um</u>	<u>5 to 10 um</u>	<u>10 to 20 um</u>	<u>20 to 44 um</u>	<u>>44 um</u>
5%	5%	5%	10%	75%

Settling parameters are the same as for the underground blasting emissions.

<u>Weight Percent</u>	<u>Particle Size (um)</u>	<u>Vertical Settling Velocity (m/sec)</u>		<u>Time (sec)</u>		<u>Settled Distance</u>
5	<5	0.0036	x	210	=	0.76 m passed
5	7.5 (5-10)	0.00637	x	210	=	1.34 m passed
5	15 (10-20)	0.0254	x	210	=	5.33 m settled
10	25 (20-44)	0.058	x	210	=	12.18 m settled
75	>44	0.181	x	210	=	38.01 m settled

Determination of % Control (i.e. percent settled) Using a settling height of 2 m, all particles >10 um are assumed to settle. Therefore, 90% overall control (i.e. percent settled) is estimated for gravity settling for rock handling at orepasses and waste rock passes.

Total TSP (orepasses and waste rock passes) with gravity settling estimated in the air stream from mine exhaust shafts.

$$18.1 \text{ t/yr} \times 0.10 \text{ (i.e. 1 - decimal fraction settled)} = 1.8 \text{ t(2.0 st)/yr}$$

Emissions from Handling - Chute to Railcar:

Emission Factor and Source: AP-42, Table 8.23-1

TSP-EF = 0.005 kg/t - Handling of high moisture ore

Process Rate: 700 t/hr, 14,000 t/day, 3,276,000 t/yr

Duration: As noted in process rate.

Control Method and Efficiency: Wetting if necessary.

Example Calculation:

$$\text{TSP} = 3,276,000 \text{ t/yr} \times 0.005 \text{ kg/t} \div 1000 \text{ kg/t} = 16.4 \text{ t/yr}$$

Total TSP (chute to railcar) = 16.4 t/yr before gravity settling.

Emissions from Handling - Chute to Railcars with Gravity Settling:

Particle size ranges are the same as for handling at orepasses and waste rock passes.

Mine ventilation air stream branch velocities:

<u>Horizontal Velocity ft/minute</u>	<u>Distance ft</u>	<u>Time Minutes</u>
285	50	0.18
285	100	0.35
1156	1235	1.07
1077	498	0.46
1268	479	0.38
1268	403	0.32
2536	160	<u>0.06</u>

Total = 2.82 minutes (169 seconds) - (i.e. horizontal airways only) for travel time from load area to exhaust shaft.

Settling parameters are the same as for the underground blasting emissions.

<u>Weight Percent</u>	<u>Particle Size (um)</u>	<u>Vertical Settling Velocity (m/sec)</u>		<u>Time (sec)</u>		<u>Settled Distance</u>
5	5	0.0036	x	169	=	0.61 m passed
5	7.5 (5-10)	0.00637	x	169	=	1.08 m passed
5	15 (10-20)	0.0254	x	169	=	4.29 m settled
10	25 (20-44)	0.058	x	169	=	9.80 m settled
75	>44	0.181	x	169	=	30.59 m settled

Determination of % Control (i.e. percent settled): Same as for handling at orepasses and waste rock passes.

Total TSP (chute to railcars) with gravity settling estimated in the air stream from mine exhaust shafts.

$$16.4 \text{ t/yr} \times 0.10 \text{ (i.e. 1 - decimal fraction settled)} = 1.6 \text{ t(1.8 st)/yr}$$

Handling from Railcars into Crusher Feed Bins:

Emission Factor and Source: AP-42, Table 8.23-1

TSP-EF = 0.005 kg/t - Handling of high moisture ore

Process Rate: 700 t/hr, 14,000 t/day, 3,276,000 t/yr

Duration: As noted in process rate.

Control Method and Efficiency: Wetting if necessary.

Example Calculation:

$$\text{TSP} - 3,276,000 \text{ t/yr} \times 0.005 \text{ kg/t} \div 1000 \text{ kg/t} = 16.4 \text{ t/yr}$$

Total TSP (railcar to crusher feed bins) = 16.4 t/yr before gravity settling.

Handling from Railcars into Crusher Feed Bins with Gravity Settling:

Particle size ranges are the same as for handling at orepasses and waste rock passes.

Mine ventilation air stream branch velocities:

<u>Horizontal Velocity ft/minutes</u>	<u>Distance ft</u>	<u>Time Minutes</u>
200	100	0.50
379	136	0.36
427	165	0.39
513	632	1.23
513	632	1.23
606	543	0.90
768	714	0.93
1609	890	0.55
1612	360	0.22
1610	242	<u>0.15</u>

Total = 6.46 minutes (387 seconds) -
(i.e. horizontal airways
only) for travel time from
loadout area to exhaust shaft.

Settling parameters are the same as for the underground blasting
emissions.

<u>Weight Percent</u>	<u>Particle Size (um)</u>	<u>Vertical Settled Velocity (m/sec)</u>		<u>Time (sec)</u>		<u>Settled Distance</u>
5	5	0.0036	x	387	=	1.39 m passed
5	7.5 (5-10)	0.00637	x	387	=	2.47 m settled
5	15 (10-20)	0.0254	x	387	=	9.83 m settled
10	25 (20-44)	0.058	x	387	=	22.45 m settled
75	>44	0.181	x	387	=	70.05 m settled

Determination of % Control (i.e. percent settled): Same as for handling
at stope drawpoints and development headings.

Total TSP (railcar to crusher feed bins) with gravity settling estimated in
the air stream from mine exhaust shafts.

$$16.4 \text{ t/yr} \times 0.05 \text{ (i.e. 1 - decimal fraction settled)} = 0.8 \text{ t(0.9 st)/yr}$$

Crusher Feed Bins to Primary Crusher:

Emission Factor and Source: AP-42, Table 8.23-1

TSP = 0.005 kg/t - Handling of high moisture rock

Process Rate: 1200 t/hr, 16,000 t/day, 3,629,000 t/yr

Duration: As noted in process rate.

Control Method and Efficiency: Wetting if necessary.

Example Calculation:

$$\text{TSP} - 3,629,000 \text{ t/yr} \times 0.005 \text{ kg/t} \div 1000 \text{ kg/t} = 18.1 \text{ t/yr}$$

Total TSP (feed bins to primary crusher) = 18.1 t/yr before gravity settling.

Crusher Feed Bins to Primary Crusher with Gravity Settling:

Particle size ranges, mine ventilation air stream branch velocities, settling parameters, and determination of % settled are the same as for handling from railcars into crusher feed bins.

Total TSP (feed bins to primary crusher) with gravity settling estimated in the air stream from mine exhaust shafts.

$$18.1 \text{ t/yr} \times 0.05 \text{ (1 - decimal fraction settled)} = 0.9 \text{ t(1.0 st)/yr}$$

Coarse Crushing to -150 mm (-6 inches):

Emission Factor and Source: AP-42, Table 8.23-1

TSP = 0.01 kg/t - Primary crushing of high moisture rock

Process Rate: 1200 t/hr, 16,000 t/day, 3,629,000 t/yr

Duration: As noted in process rate.

Control Method and Efficiency: Insertable Dust Collector, similar to DCE
Vokes Model No. DLMV 45/15 F1 - 99%
efficiency.

Example Calculation:

$$\text{TSP} - 3,629,000 \text{ t/yr} \times 0.01 \text{ kg/t} \div 1000 \text{ kg/t} \times (1-0.99) = 0.4 \text{ t(0.4 st)/yr}$$

Crusher Discharge to Picking Belt:

Emission Factor and Source: AP-42, Table 8.23-1

TSP - 0.005 kg/t - Transfer of high moisture rock

Process Rate: 1200 t/hr, 14,700 t/day, 3,629,000 t/yr

Duration: As noted in process rate.

Control Method and Efficiency: Insertable Dust Collector, similar to DCE
Vokes Model No. DLMV 45/15 F1 - 99%
efficiency.

Example Calculation:

$$\text{TSP} - 3,629,000 \text{ t/yr} \times 0.005 \text{ kg/t} \div 1000 \text{ kg/t} \times (1-0.99) = 0.2 \text{ t}(0.2 \text{ st})/\text{yr}$$

Transfer from Picking Belt to Loading Belt:

Emission Factor and Source: AP-42, Table 8.23-1

TSP - 0.005 kg/t - Transfer of high moisture rock

Process Rate: 1200 t/hr, 14,400 t/day, 3,629,000 t/yr

Duration: As noted in process rate.

Control Method and Efficiency: Insertable Dust Collector, similar to DCE
Vokes Model No. DLMV 45/15 F1 - 99%
efficiency.

Example Calculation:

$$\text{TSP} - 3,629,000 \text{ t/yr} \times 0.005 \text{ kg/t} \div 1000 \text{ kg/t} \times (1-0.99) = 0.2 \text{ t}(0.2 \text{ st})/\text{yr}$$

Transfer from Loading Belt to Hoisting Pocket:

Emission Factor and Source: AP-42, Table 8.23-1

TSP - 0.005 kg/t - Transfer of high moisture rock

Process Rate: 1200 t/hr, 14,400 t/day, 3,629,000 t/yr

Duration: As noted in process rate.

Control Method and Efficiency: Insertable Dust Collector, similar to DCE
Vokes Model No. DLMV 45/15 F1 - 99%
efficiency.

Example Calculation:

$$\text{TSP} - 3,629,000 \times 0.005 \text{ kg/t} \div 1000 \text{ kg/t} \times (1-0.99) = 0.2 \text{ t}(0.2 \text{ st})/\text{yr}$$

Transfer from Hoisting Pocket into Skip:

Emission Factor and Source: AP-42, Table 8.23-1

TSP = 0.005 kg/t - Transfer of high moisture rock

Process Rate: 1100 t/hr, 14,400 t/day, 3,629,000 t/yr

Duration: As noted in process rate.

Control Method and Efficiency: Insertable Dust Collector, similar to DCE
Vokes Model No. DLMV 45/15 F1 - 99%
efficiency.

Example Calculation:

$$\text{TSP} = 3,629,000 \text{ t/yr} \times 0.005 \text{ kg/t} \div 1000 \text{ kg/t} \times (1-0.99) = 0.2 \text{ t} \\ (0.2 \text{ st})/\text{yr}$$

TOTAL Estimated Underground Emissions

	<u>st/yr</u>
TSP =	
Blasting	13.6
Rock Handling	
Stope Drawpoints and development headings	1.0
Orepasses and waste rock passes	2.0
Chute to railcars	1.8
Railcar to crusher feed bins	0.9
Feed bins to primary crusher	1.0
Coarse crushing	0.4
Crusher discharge to picking belt	0.2
Picking belt to loading belt	0.2
Loading belt to hoisting pocket	0.2
Hoisting pocket into skip	<u>0.2</u>
Total	21.5
SO ₂ =	2.3 st/yr
NO _x =	18.6 st/yr
CO =	79.0 st/yr
Pb =	0.002 st/yr

2. Mine Air Heating - Use of natural gas (heat content 1000 BTU/SCF) for direct-fired mine air heating.

Emission Factor and Source: EPA NEDS - Source classification codes, Appendix C, p. C-5, 12/75.

TSP - 10.0 lb/10⁶ SCF (4.54 kg/10⁶ SCF)

SO_x - 0.6 lb/10⁶ SCF (0.27 kg/10⁶ SCF)

NO_x - 120.0 lb/10⁶ SCF (54.48 kg/10⁶ SCF)

CO - 20.0 lb/10⁶ SCF (9.08 kg/10⁶ SCF)

HC - 8.0 lb/10⁶ SCF (3.63 kg/10⁶ SCF)

Process Rate: 91,800 SCF/hr, 2.203 x 10⁶ SCF/day, 110.6 x 10⁶ SCF/yr

Duration: When weather conditions require.

Control Method and Efficiency: Use of natural gas.

Example Calculation:

TSP - 110.6 x 10⁶ SCF/yr x 4.54 kg/10⁶ SCF ÷ 1000 kg/t = 0.5 t (0.6 st)/yr

3. Mine Vehicles (Mobile Equipment) - Use of diesel equipment to move personnel, materials, and rock. Diesel fuel will contain 0.4 weight percent sulfur maximum.

Emission Factor and Source: "Emission control of a Deutz F6L-714 diesel engine, derated for underground use, by application of water/oil fuel emissions" by A. Lawson, E. W. Simmons, and M. Pieltt, March 30, 1979.

TSP - 11.0 lb/10³ gal (1.61 g/kg) - Lawson, et al. 1979, p. 62

SO_x - 31.0 lb/10³ gal (4.54 g/kg) - off road construction equipment from EPA NEDS

NO_x - 108.5 lb/10³ gal (15.9 g/kg) - Lawson, et al. 1979, p. 81

CO - 2.01 lb/10³ gal (0.295 g/kg) - Lawson, et al. 1979, p. 69

HC - 1.97 lb/10³ gal (0.289 g/kg) - Lawson, et al. 1979, p. 66

Process Rate: 879 l/hr, 15,841 l/day, 3,654,000 l/yr

Duration: As noted by process rate.

Control Method and Efficiency: Use of clean burning air cooled Deutz engines with a catalytic scrubber.

Example Calculation:

$$\text{TSP} - \frac{3,654,000 \text{ l/yr} \times 0.845 \text{ kg/l} \times 0.00161 \text{ kg(TSP)/kg}}{1000 \text{ kg/t}} = 5 \text{ t}(5.5 \text{ st})/\text{yr}$$

Emitting Device (Mine Operation): Total quantities of component air emissions will exit the mine at the east and west exhaust shafts (EER and WER). Each shaft will have two fans similar to a Joy M108-580D that will produce approximately 630,000 cfm at 900 hp each.

III. MINE/MILL SURFACE FACILITIES CONSTRUCTION

1. Concrete Batch Plant - Mixing of aggregate, sand, and cement for use during plant construction activities:

Emission Factor and Source: AP-42, Table 8.10-2

	<u>kg/t</u>
TSP - Transfer of sand and aggregate to elevated bins	= 0.02
Cement unloading to elevated storage silos	= 0.118
Weight hopper loading of cement, sand, and aggregate	= 0.118
Mixer loading of cement, sand, and aggregate	= 0.01
Loading of dry-batch truck	= 0.02

Process Rate: 38.3 m³/shift, 1 shift/day, 5 days/wk, 52 wks/yr

Sand and Aggregate	75.2 t/day	19,558 t/yr
Cement	<u>16.7 t/day</u>	<u>4,342 t/yr</u>
Total	91.9 t/day	23,900 t/yr

Control Method and Efficiency: Baghouse with ducting and insertable collector - 99% control efficiency, AP-42, Table 8.10-1; Other - 90% control efficiency.

Example Calculation:

$$\begin{aligned}
 \text{Yearly} & - 19,558 \text{ t/yr} \times 0.02 \text{ kg/t} \times (1-0.90) \div 1000 \text{ kg/t} = 0.04 \text{ t/yr} \\
 & 4,342 \text{ t/yr} \times 0.118 \text{ kg/t} \times (1-0.99) \div 1000 \text{ kg/t} = 0.005 \text{ t/yr} \\
 & 23,900 \text{ t/yr} \times 0.118 \text{ kg/t} \times (1-0.90) \div 1000 \text{ kg/t} = 0.282 \text{ t/yr} \\
 & 23,900 \text{ t/yr} \times 0.01 \text{ kg/t} \times (1-0.90) \div 1000 \text{ kg/t} = 0.024 \text{ t/yr} \\
 & 23,900 \text{ t/yr} \times 0.02 \text{ kg/t} \times (1-0.90) \div 1000 \text{ kg/t} = \underline{0.048 \text{ t/yr}} \\
 & \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \underline{0.399 \text{ t/yr}} \\
 & \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad (0.44 \text{ st/yr})
 \end{aligned}$$

Total Annual Estimated Emissions = 0.40 t/yr (0.44 st/yr)

2. Site Preparation

a. Mine Shafts - The surface construction activities necessary to prepare for sinking of the main mine and intake air shafts, east and west exhaust shafts (i.e. raises), and the road to the potable water supply well are the estimates provided under the heading of mine/mill surface facilities construction. The estimated TSP air emissions for the construction of these individual areas are provided below.

Emission Factor and Source: AP-42, Section 11.2.4

TSP-EF - 1.2 st/acre/month

Access road to potable water supply well with pad - outside fence

Process Rate:

$$\text{Road} - \frac{235 \text{ m} \times 6 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 0.35 \text{ acres}$$

$$\text{Pad} - \frac{(25 \text{ m}/2)^2}{4047 \text{ m}^2/\text{acre}} = 0.12 \text{ acres}$$

$$0.47 \text{ acres}$$

Access road to east exhaust shaft (EER) with pad - outside fence

Process Rate:

$$\text{Road} - \frac{135 \text{ m} \times 6 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 0.20 \text{ acres}$$

$$\text{Pad} - \frac{20 \text{ m} \times 20 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 0.10 \text{ acres}$$

$$0.30 \text{ acres}$$

Access road to west exhaust shaft (WER) with pad - outside fence

Process Rate:

$$\text{Road} - \frac{45 \text{ m} \times 6 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 0.07 \text{ acres}$$

$$\text{Pad} - \frac{20 \text{ m} \times 20 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 0.10 \text{ acres}$$

$$0.17 \text{ acres}$$

Access road to explosives magazine and pad - outside fence

Process Rate:

$$\text{Road} - \frac{88 \text{ m} \times 6 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 0.13 \text{ acres}$$

$$- \frac{527 \text{ m} \times 8 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 1.04 \text{ acres}$$

$$\text{Pad} - \frac{55 \text{ m} \times 120 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 1.63 \text{ acres}$$

$$2.80 \text{ acres}$$

Access road to preproduction ore storage pad - outside fence

Process Rate:

$$\text{Road} - \frac{240 \text{ m} \times 24 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 1.42 \text{ acres}$$

$$\text{Pad} - \frac{188 \text{ m} \times 188 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 8.73 \text{ acres}$$

$$- \frac{125 \text{ m} \times 25 \text{ m}}{4047 \text{ m}^2/\text{acre}} = 0.77 \text{ acres}$$

$$\underline{10.92 \text{ acres}}$$

$$\text{Total All} = 14.7 \text{ acres}$$

Duration: Assume all activities occur in the same month.

Control Method and Efficiency: Watering of disburbed area if necessary

Example Calculation:

$$\text{TSP} - 1.2 \text{ st/acre/month} \times 14.7 \text{ acres} = 17.6 \text{ st}$$

- b. Mine/Mill Site - Earthmoving and excavation activities will occur to clear and grade site to allow foundation work for structures and roads.

Major mine/mill surface facilities development will be completed within the first 12 months of the construction phase.

The following calculations estimate the air emissions if burning instead of mulching occurs for the tree stumps and brush accumulated from the mine/mill site construction (see also Kulibert, 1984). Burning will be on the surface in an open area.

Emission Factors and Source: AP-42, Table 2.4-2, Forest residues - unspecified.

Particulate (TSP)	NO _x	CO	HC
<u>lb/st</u>	<u>lb/st</u>	<u>lb/st</u>	<u>lb/st</u>
17	4	140	24.7

Process Rate: Total burn

Duration: 12 months

Control Method and Efficiency: None

Example Calculations: 1732 st of Forest residues for 104 acres

$$\begin{aligned} \text{TSP: } & \text{st of brush/yr} \times \text{TSP lbs/st} \times \text{st}/2000 \text{ lbs} = \\ & 1732 \text{ st/yr} \times 17 \text{ lb/st} \times \text{st}/2000 \text{ lbs} = 14.7 \text{ st/yr} \\ \text{NO}_x: & 1732 \times 4 \div 2000 = 3.5 \text{ st/yr} \\ \text{CO : } & 1732 \times 140 \div 2000 = 121.2 \text{ st/yr} \\ \text{HC : } & 1732 \times 24.7 \div 2000 = 21.4 \text{ st/yr} \end{aligned}$$

Construction Activities

Emission Factors and Source: Two emission factors are used to represent fugitive dust (TSP) emissions from site area construction activities. On-site construction activities will be represented by the general factor 1.2 st/acre/month. This general factor was not adjusted based on the site area estimated silt content of 15% from soil classification tests. However, some of the surface till will be hauled to the MWDF. Hauling emissions will be based on the following factor from AP-42 and as specified by WDNR in the September 12, 1983, letter.

Emission Factor and Source: AP-42 (i.e. May 1983), Section 11.2.1 - Unpaved roads

$$\text{TSP-EF} = k 5.9 (s/12)(S/30)^2 (w/3)^{0.7} (w/4)^{0.5} (d/365) = \text{lb/veh-mile}$$

TSP-EF = Suspended particulate emissions - lb/veh-mile

- k = Particle size multiplier - 0.8
- s = Silt content of gravel road surface material in % - 6%**
- S = Average vehicle speed - 15 mi/hr
- W = Average vehicle weight - tons(st)
- w = Average number of wheels per vehicle
- d = Dry days per year - 230 days

* The factor (S/30) is valid for a speed range of 30 to 50 mph. Below 30 mph the square of the factor is recommended (WDEQ 1979. Fugitive dust emission factors. Cheyenne, WY: Wyoming Department of Environmental Quality, Division of Air Quality. January 24 Memorandum from Charles Collins).

** The silt content (i.e. 6%) used in this calculation was as recommended by the DNR. Further, the calculations estimating the emissions are for the total year and not just the summer months.

Process Rate: 12 months.

Control Method and Efficiency: Wetting of disturbed area if necessary.

Example Calculations:

On-site construction

Site preparation completed in 12 months
Mine/mill site = 104 acres
Area disturbed/month = $104 \div 12 = 8.7$ acres

Emissions (uncontrolled) = $1.2 \text{ st/acre/month} \times 8.7 \text{ acres} \times 12 \text{ months/yr}$
= 125.3 st/yr

Emissions (controlled) = $125.3 \times 0.5^* = 62.6 \text{ st/yr}$

* Control factor for watering from AP-42, Section 11.2.4

Hauling of excavated till from mine/mill site to MWDF

Total soil material hauled:

$96,396 \text{ yd}^3 \times 2,970 \text{ lb/yd}^3 \times \text{st}/2,000 \text{ lbs} = 143,148 \text{ st}$
Assume 35 st/haul truck
Total number of trips = 4,090
Round trip miles from mine/mill site to MWDF = 4 miles
Total miles = $4,090 \text{ trips} \times 4 \text{ miles/trip} = 16,360 \text{ miles}$

$\text{TSP-EF} = (0.8)5.9(s/12)(S/30)^2(w/3)^{0.7}(w/4)^{0.5}(d/365) = \text{lb/veh-mile}$
= $(0.8)5.9(6/12)(15/30)^2(51/3)^{0.7}(6/4)^{0.5}(230/365) =$
= 3.3 lb/veh-mile

Emissions (uncontrolled) = $3.3 \text{ lb/veh-mile} \times 16,360 \text{ miles} \times \text{st}/2,000 \text{ lb}$
= 27.0 st/yr

Emissions (controlled) = $27.0 \text{ st} \times 0.15^{**} = 4.1 \text{ st/yr}$

** 85% control with chemical stabilization

Total TSP emissions from mine/mill site development including earthmoving excavation activities = 66.7 st/yr.

- c. MWDF Area - Estimates included here are for clearing the land, and surface earthwork (excavation to approximately 10 ft). The estimates use the primary emission factor from AP-42 for construction activities for project facilities. However, where deep excavation (greater than 10 ft) and major hauling of soil material within the excavated area is involved, the TSP emissions from hauling and loading and dumping of the soil material were calculated separately (i.e., in addition to the general construction emissions).

Emission Factor and Source: 1.2 st/acre/month; EPA AP-42, Section 11.2.4; Clearing and excavation (i.e., heavy construction)

Assume: Based on largest surface area disturbed in one year - Tailing Pond T1 - approximately 94 acres

Duration: 12 months (94 ÷ 12 = 7.83 acres/month)

Example Calculation:

$$\text{TSP} = 1.2 \text{ st/acre/month} \times 7.83 \text{ acres/month} \times 12 \text{ months/yr} = 112.8 \text{ st/yr}$$

- d. Access Road/Powerline Clearing and Grading - The following calculations estimate the air emissions if burning instead of mulching occurs for the tree stumps and brush accumulated from the access road/powerline construction (see also Kulibert, 1984). Burning will be on the surface in an open area.

Emission Factors and Source: AP-42, Table 2.4-2; Forest residues - unspecified

Particulate (TSP)	NO _x	CO	HC
<u>lb/st</u>	<u>lb/st</u>	<u>lb/st</u>	<u>lb/st</u>
17	4	140	24.7

Process Rate: Total burn

Duration: 12 months

Control Method and Efficiency: None

Example Calculation: 316 st of Forest residues for 37 acres

$$\text{TSP: } \text{st of brush/yr} \times \text{TSP lbs/st} \times \text{st}/2000 \text{ lbs} \\ 316 \text{ st/yr} \times 17 \text{ lb/st} \times \text{st}/2000 \text{ lbs} = 2.7 \text{ st/yr}$$

$$\text{NO}_x: 316 \times 4 \div 2000 = 0.6 \text{ st/yr}$$

$$\text{CO} : 316 \times 140 \div 2000 = 22.1 \text{ st/yr}$$

$$\text{HC} : 316 \times 24.7 \div 2000 = 3.9 \text{ st/yr}$$

Mine/Mill Site Fugitive Dust TSP Emissions from Traffic During the Construction Phase after Access Road Completion

Current estimates indicate that approximately 703 operation phase personnel will be employed by the Crandon Project. It is also assumed that there will be 1.6 employees/vehicle traveling 2.5 miles (one way) of access road to the mine/mill site. Therefore, at this rate (2 trips/day x 2.5 miles/trip x 703/1.6 employees per vehicle), approximately 2,200 vehicle miles would be traveled per day. The calculation of fugitive dust (TSP) emissions from vehicle travel is based on the most recent EPA AP-42 update (i.e. May 1983), and current estimates of employee traffic loads of 439 (703 ÷ 1.6) vehicles per day (i.e. 439 x 5 = 2195 miles/day).

Access Road

Emission Factors and Source: AP-42, Table 11.2.5-1

TSP-EF = 0.012 lb/veh-mile

Process Rate: 2195 miles/day for employee vehicles
(i.e. 439 vehicles x 5 miles/round trip)
100 miles/day for off-site delivery vehicles
(i.e. 20 vehicles x 5 miles/round trip)
Total miles traveled/day on access road =
2295 veh-miles/day

Duration: 230 dry days/yr

Control Method and Efficiency: Paving

Example Calculation:

TSP - 2295 veh-miles/day x 230 dry days/yr x 0.012 lbs/veh-mile
x st/2000 lb = 3.2 st/yr

Tailpipes

Emission Factor and Source: AP-42, Appendix D, Table D.1-19 (1987)

Process Rate: Employee vehicles - 2200 mi/day (LDV)

Duration: 350 days/yr

Control Method and Efficiency: As per EPA vehicle emission controls.

Example Calculation: Process Rate x Emission Factor = Emission Rate

$$\begin{aligned} \text{TSP: } & 2200 \text{ mi/day} \times 0.05 \text{ g/mi} \times 0.002 \text{ lbs/g} \times 350 \text{ days/yr} \times \frac{\text{st}}{2000 \text{ lbs}} \\ & = 0.04 \text{ st/yr} \\ \text{SO}_x: & 2200 \times 0.13 \text{ (Table D.1-21)} \times 0.002 \times 350 \div 2000 = 0.1 \text{ st/yr} \\ \text{NO}_x: & 2200 \times 0.40 \times 0.002 \times 350 \div 2000 = 0.3 \text{ st/yr} \\ \text{CO : } & 2200 \times 3.6 \times 0.002 \times 350 \div 2000 = 2.8 \text{ st/yr} \\ \text{HC : } & 2200 \times 0.43 \times 0.002 \times 350 \div 2000 = 0.3 \text{ st/yr} \end{aligned}$$

Emitting Device: Tailpipes of vehicles.

- e. Railroad Spur Clearing and Grading - The following calculations estimate the air emissions if burning instead of mulching occurs for the tree stumps and brush accumulated from the railroad spur construction (see also Kulibert, 1984). Burning will be on the surface in an open area.

Emission Factors and Source: AP-42, Table 2.4-2; Forest residues - unspecified

Particulate (TSP)	NO _x	CO	HC
$\frac{\text{lb/st}}{17}$	$\frac{\text{lb/st}}{4}$	$\frac{\text{lb/st}}{140}$	$\frac{\text{lb/st}}{24.7}$

Process Rate: Total burn

Duration: 12 months

Control Method and Efficiency: None

Example Calculations: 497 st of Forest residues for 45 acres

$$\begin{aligned} \text{TSP: } & \text{st of brush/yr} \times \text{TSP lbs/st} \times \frac{\text{st}}{2000 \text{ lbs}} \\ & 497 \text{ st/yr} \times 17 \text{ lbs/st} \times \frac{\text{st}}{2000 \text{ lbs}} = 4.2 \text{ st/yr} \\ \text{NO}_x: & 497 \times 4 \div 2000 = 1.0 \text{ st/yr} \\ \text{CO : } & 497 \times 140 \div 2000 = 34.8 \text{ st/yr} \\ \text{HC : } & 497 \times 24.7 \div 2000 = 6.1 \text{ st/yr} \end{aligned}$$

Diesel Locomotive - Used for on-site location and switching of railroad cars.

Emission Factors and Source: EPA - NEDS specific codes, emission factor file report, 7/23/82.

TSP - 25 lb/10³ gal

SO_x - 57 lb/10³ gal

NO_x - 370 lb/10³ gal

CO - 130 lb/10³ gal

HC - 90 lb/10³ gal

Process Rate: 5 gal/hr, 30 gal/day, 10,800 gal/yr

Duration: 2 hrs/shift, 3 shifts/day, 360 days/yr (included in process rate).

Control Method and Efficiency: None

Example Calculation:

TSP - 10,800 gal/yr x 25.0 lb/10³ gal x st/2000 lbs = 0.14 st/yr

Emission rates for the diesel locomotive are estimated to be as follows:

TSP: $\frac{\text{st/yr}}{0.14}$

SO_x: 0.3

NO_x: 2.0

CO : 0.7

HC : 0.5

h. Haul Road - Hauling of excavated till from mine/mill site to MWDF.

Emission Factors and Source: Some of the surface till will be hauled to the MWDF. Hauling emissions will be based on the following factor from AP-42.

TSP-EF (lbs/veh-mile) = k 5.9 (s/12)(S/30)²(W/3)^{0.7}(w/4)^{0.5} (d/365)

The silt content (i.e. 6%) used in this calculation was as recommended by the DNR.

Process Rate:

Total soil material hauled:

$$96,396 \text{ yd}^3 \times 2,970 \text{ lb/yd}^3 \times \text{st}/2,000 \text{ lbs} = 143,148 \text{ st}$$

Assume 35 st/haul truck

$$\text{Total number of trips} = 4,090$$

Round trip miles from mine/mill site to MWDF = 4 miles

$$\text{Total miles} = 4,090 \text{ trips} \times 4 \text{ miles/trip} = 16,360 \text{ miles}$$

$$\begin{aligned} \text{TSP-EF} &= (0.8)5.9(s/12)(S/30)^2(w/3)^{0.7}(w/4)^{0.5}(d/365) = \text{lb/veh-mile} \\ &= (0.8)5.9(6/12)(15/30)^2(51/3)^{0.7}(6/4)^{0.5}(230/365) \\ &= 3.3 \text{ lb/veh-mile} \end{aligned}$$

$$\begin{aligned} \text{Emissions (uncontrolled)} &= 3.3 \text{ lb/veh-mile} \times 16,360 \text{ miles} \times \text{st}/2,000 \text{ lb} \\ &= 27.0 \text{ st/yr} \end{aligned}$$

$$\text{Emissions (controlled)} = 27.0 \text{ st} \times 0.15^* = 4.1 \text{ st/yr}$$

* 85% control with chemical stabilization

- g. Water Discharge Pipeline - Emissions are primarily generated from general excavation, and stripping and hauling of sand and gravel.

Process Rate:

Assume:

Total construction area	= 15 acres
Pipeline distance	= 6.1 miles
Total disturbed width	= 20 ft
Sand and gravel backfill	= 3,500 yd ³
Average haul distance	= 3 miles
Pipeline construction period	= 6 months

General Construction

Emission Factor and Source: AP-42, Section 11.2.4

$$\text{TSP-EF} = 1.2 \text{ st/acre/month}$$

Process Rate:

$$\text{Area disturbed/month} = 15 \text{ acres}/6 \text{ months} = 2.5 \text{ acres/month}$$

$$\begin{aligned} \text{Emissions (uncontrolled)} &= 1.2 \text{ st/acre/month} \times 2.5 \text{ acres/month} \times 6 \text{ months} \\ &= 18.0 \text{ st} \end{aligned}$$

$$\text{Emissions (controlled)} = 18.0 \text{ st} \times 0.5^{**} = 9.0 \text{ st}$$

** 50% control with watering.

Hauling

Emission Factor and Source: AP-42

$$\begin{aligned} \text{TSP-EF} &= (0.8)5.9(15/12)(10/30)2(10/3)0.7(6/4)0.5(230/365) = \text{lb/veh-mile} \\ &= 1.2 \text{ lb/veh-mile} \end{aligned}$$

Process Rate:

$$\begin{aligned} 3,500 \text{ yd}^3 \text{ sand and gravel} \div 5 \text{ yd}^3/\text{haul} &= 700 \text{ hauls} \\ 700 \text{ hauls at 6 miles round trip/haul} &= 4,200 \text{ veh-miles} \end{aligned}$$

$$\text{Emissions (uncontrolled)} = 1.2 \times 4,200 \text{ veh-miles} \times \frac{\text{st}}{2000 \text{ lb}} = 2.5 \text{ st/yr}$$

$$\text{Emissions (controlled)} = 2.5 \text{ st/yr} \times 0.5^* = 1.3 \text{ st/yr}$$

* 50% control with watering

Total construction phase TSP emissions for the wastewater discharge pipeline are conservatively estimated to be 10.3 st/yr.

- h. In-Plant Roads - Vehicle traffic on roads within and adjacent to the main portion of the Project facilities.

Fugitive dust

Emissions of fugitive dust (TSP) from using existing gravel roads will be primarily from delivery of bentonite from the Woodlawn siding 6 miles east of the MWDF before the railroad spur is completed during 1987. Emission estimates are based on the following assumptions:

- 1) The access road and railroad will be constructed during the first 12 months of project development;
- 2) Most traffic prior to construction of the new access road will use Sand Lake road to a 1/2-mile gravel access road to the mine/mill site;
- 3) Distance from the Woodlawn siding to the MWDF is approximately 6 miles;
- 4) Construction personnel traffic during the first 12 months is estimated to be: 413 vehicles/day (i.e. 1.6 persons/vehicle and 1 mile round trip per vehicle);
- 5) Bentonite hauled during the first year would be 2,000 tons in 25 ton tractor trailers at 15 miles/hr along the 6 mile distance from the Woodlawn siding to the MWDF; and
- 6) An additional 12 service trucks and 3 equipment delivery trucks would come on-site per day (i.e. 1 mile round trip).

Fugitive dust (TSP) emissions on gravel roads are based on the following factor:

$$\text{TSP-EF} = (0.8)5.9(s/12)(s/30)^2(w/3)^{0.7}(w/4)^{0.5}(d/365)$$

Personnel traffic

Assume average vehicle weighs 1.7 tons with 4 wheels.

$$\begin{aligned}\text{TSP-EF} &= (0.8)5.9(12/12)(15/30)^2(1.75/3)^{0.7}(4/4)^{0.5}(230/365) = \\ &\text{lb/veh-mile} = 0.5 \text{ lb/veh-mile}\end{aligned}$$

$$\begin{aligned}\text{Total miles traveled} &= 413 \text{ veh-miles/day} \times 5 \text{ days/week} \times 50 \text{ weeks/yr} = \\ &103,250 \text{ veh-miles/yr}\end{aligned}$$

$$\begin{aligned}\text{Emissions (uncontrolled)} &= 103,250 \text{ veh-miles/yr} \times 0.5 \text{ lbs/veh-mile} \times \\ &\text{st/2000 lbs} = 25.8 \text{ st/yr}\end{aligned}$$

$$\text{Emissions (controlled)} = 25.8 \text{ st/yr} \times 0.15^* = 3.9 \text{ st/yr}$$

Equipment truck traffic

Assume average weight of heavy equipment trucks = 10 st
and service trucks = 5 st.

Heavy equipment truck traffic

$$3 \text{ truck miles/day} \times 5 \text{ days/week} \times 50 \text{ weeks/yr} = 750 \text{ veh-miles/yr}$$

$$\begin{aligned}\text{TSP-EF} &= (0.8)5.9(12/12)(15/3)^2(10/3)^{0.7}(18/4)^{0.5}(230/365) = \text{lb/veh-mile} \\ &= 3.7 \text{ lb/veh-mile}\end{aligned}$$

$$\begin{aligned}\text{Emissions (uncontrolled)} &= 3.7 \text{ lb/veh-mile} \times 750 \text{ veh-mile/yr} \times \text{st/2000 lbs} \\ &= 1.4 \text{ st/yr}\end{aligned}$$

$$\text{Emissions (controlled)} = 1.4 \times 0.15^* = 0.2 \text{ st/yr}$$

Service truck traffic

$$12 \text{ truck miles/day} \times 5 \text{ days/week} \times 50 \text{ weeks/yr} = 3,000 \text{ veh-miles/yr}$$

$$\begin{aligned}\text{TSP-EF} &= (0.8)5.9(1)(0.25)(5/30)^{0.7}(10/4)^{0.5}(0.6) = \text{lb/veh-mile} \\ &= 1.7 \text{ lb/veh-mile}\end{aligned}$$

$$\begin{aligned}\text{Emissions (uncontrolled)} &= 1.7 \text{ lb/veh-mile} \times 3,000 \text{ veh-mile/yr} \\ &\times \text{st/2000 lbs} = 2.6 \text{ st/yr}\end{aligned}$$

$$\text{Emissions (controlled)} = 2.6 \text{ st/yr} \times 0.15^* = 0.4 \text{ st/yr}$$

* 85% control with chemical stabilization.

Mine/Mill Site-Paved Roads

Emission Factors and Source: AP-42 (i.e. May 1983), Section 11.2.6 - Industrial Paved Roads

$$\text{TSP-EF} = k(0.09) I (4/n)(s/10)(L/1000)(W/3)^{0.7} = \text{lb/veh-mile}$$

where:

k = particle size multiplier	= 0.86
I = industrial augmentation factor	= 3.5 for LDGV = 7.0 for HDGV and HDDV
n = number of traffic lanes	= 2
s = surface material silt content (%)	= 20%
L = surface dust loading (lb/mile)	= 1000
W = average vehicle weight (tons)	= 2 st (i.e. 4000 lbs) - for light duty gasoline vehicles (LDGV) = 5 st avg. - heavy-duty gasoline vehicle (HDGV) = 15 st avg. - heavy-duty diesel vehicle (HDDV)

Process Rate:

Light Duty Gas Vehicle (LDGV)

(Pick-up Trucks)	<u>Duty</u>	<u>miles/day</u>
Assume: 20 miles/hr	Environmental	25
4 wheels	Inspections	45
W = 2 st	Security	50
230 dry days per year	Maintenance	10
	Warehouse	2.5
	Total	132.5

Heavy Duty Gas Vehicle (HDGV)

Assume: 15 miles/hr	<u>Duty</u>	<u>miles/day</u>
6 wheels	Water Truck	20
W = 5 st (average)	Trucks	6.5
230 dry days per year	Total	26.5

Heavy Duty Diesel Vehicle (HDDV)

Assume: 10 miles/hr	<u>Duty</u>	<u>miles/day</u>
6 wheels	Grader	5
W = 15 st (average)	Backhoe	0.5
230 dry days per year	60 st Crane	0.5
	10 st Crane	0.5
	Tractor/Trailer	0.5
	Forklifts	20
	Total	27.0

Control Method and Efficiency: Paving - asphalt.

Example Calculation:

$$\begin{aligned} \text{LDGV TSP-EF} &= k(0.09) I (4/n)(s/10)(L/1000)(W/3)^{0.7} = \text{lb/veh-mile} \\ &= 0.86 (0.09) 3.5 (4/2)(20/10)(1000/1000)(2/3)^{0.7} \\ &= 0.8 \text{ lb/veh-mile} \end{aligned}$$

$$\text{LDGV TSP} \quad - \quad 0.8 \text{ lb/veh-mile} \times 132.5 \text{ miles/day} \times 230 \text{ dry days/yr} \times \text{st/2000 lbs} = 12.2 \text{ st/yr}$$

$$\begin{aligned} \text{HDGV TSP-EF} &= 0.08 \times 7.0 \times 2 \times 2 \times 1 \times (5/3)^{0.7} = 3.2 \text{ lb/veh-mile} \\ \text{HDGV TSP} &\quad - \quad 3.2 \times 26.5 \times 230 \div 2000 = 9.8 \text{ st/yr} \end{aligned}$$

$$\begin{aligned} \text{HDDV TSP-EF} &= 0.08 \times 7.0 \times 2 \times 2 \times 2 \times (15/3)^{0.7} = 6.9 \text{ veh-mile} \\ \text{HDDV TSP} &\quad - \quad 6.9 \times 27 \times 230 \div 2000 = 21.4 \text{ st/yr} \end{aligned}$$

Total estimated TSP emissions = 43.4 st/yr

Gravel Roads

Emission Factors and Source: AP-42, Section 11.2.1.3

$$\text{TSP-EF} = k 5.9 (s/12)(S/30)^2(W/3)^{0.7}(w/4)^{0.5}(d/365) = \text{lb/veh-mile}$$

k = 0.8	LDGV = 132.5 miles/day
s = silt content, %	HDGV = 26.5 miles/day
S = vehicle speed, mph	HDDV = 27.0 miles/day
W = vehicle weight, st	s = 6%
w = number of tires	
d = number of dry days	

Duration: 230 dry days/yr

Control Method and Efficiency: Watering as necessary.

Example Calculations:

$$\begin{aligned} \text{LDGV TSP-EF} &= k 5.9 (s/12)(S/30)^2(W/3)^{0.7}(w/4)^{0.5}(d/365) \text{ lb/veh-mile} \\ &= (0.8) 5.9 (6/12)(20/30)^2(2/3)^{0.7}(1)^{0.5}(230/365) \\ &= 0.5 \text{ lb/veh-mile} \end{aligned}$$

$$\text{LDGV TSP} \quad - \quad 0.5 \text{ lb/veh-mile} \times 132.5 \text{ mi/day} \times 230 \text{ days/yr} \times \text{st/2000 lbs} = 7.6 \text{ st/yr}$$

$$\begin{aligned} \text{HDGV TSP-EF} &= 0.8 (5.9)(6/12)(15/30)^2(5/3)^{0.7}(6/4)^{0.5}(0.6) \\ &= 0.6 \text{ lb/veh-mile} \end{aligned}$$

$$\text{HDGV TSP} \quad - \quad 0.6 \times 26.5 \times 230 \div 2000 = 1.8 \text{ st/yr}$$

$$\begin{aligned} \text{HDDV TSP-EF} &= 0.8 (5.9)(6/12)(10/30)^2(15/3)^{0.7}(6/4)^{0.5}(0.6) \\ &= 0.5 \text{ lb/veh-mile} \end{aligned}$$

$$\text{HDDV TSP} \quad - \quad 0.5 \times 27.0 \times 230 \div 2000 = 1.9 \text{ st/yr}$$

Total estimated TSP emissions (uncontrolled) = 11.3 st/yr

Total estimated TSP emissions (controlled) = 11.3 st/yr x 0.5* = 5.7 st/yr

*50% control with watering

Total estimated TSP emissions for employee and plant operation traffic
= 49.1 st/yr

3. Construct Major Surface Facilities

- a. Fuel Transfer and Storage - Diesel fuel and gasoline will be transferred from a tank wagon to temporary storage tanks until dispensed to equipment and vehicles.

Emission Factors and Source: AP-42, Tables 4.3 and 4.4

HC/VOC	1.08000	kg/10 ³	1	Gasoline Dispensing Loss
HC/VOC	0.00259	kg/10 ³	1	Diesel Fuel Dispensing Loss
HC/VOC	0.98000	kg/10 ³	1	Gasoline Tank Loading Loss
HC/VOC	0.00236	kg/10 ³	1	Diesel Tank Loading Loss
HC/VOC	0.08400	kg/10 ³	1	Gasoline Spillage Loss
HC/VOC	0.00020	kg/10 ³	1	Diesel Spillage Loss
HC/VOC	0.01200	kg/10 ³	1	Gasoline Breathing Loss
HC/VOC	0.00029	kg/10 ³	1	Diesel Breathing Loss

Process Rate:

Peak construction levels use

	<u>Diesel</u>	<u>Gasoline</u>
Winter	22,450 1/d	530 1/d
Summer	32,850 1/d	660 1/d

Duration: Winter - 5 months (4.3 wk/month, 5 day/wk);
Summer - 7 months (4.3 wk/month, 5 day/wk)

Control Method and Efficiency: None

Example Calculation: Summation of processes

Process Rate x Emission Factor x Duration = Emission Rate

HC/VOC:

(Gasoline - Summer)

0.66 x 10 ³	1/d	x	1.080	kg/10 ³	1	=	0.710	kg/d
0.66 x 10 ³	1/d	x	0.980	kg/10 ³	1	=	0.650	kg/d
0.66 x 10 ³	1/d	x	0.084	kg/10 ³	1	=	0.080	kg/d
0.66 x 10 ³	1/d	x	0.012	kg/10 ³	1	=	0.008	kg/d

(Diesel - Summer)

$$32.85 \times 10^3 \text{ l/d} \times 0.00259 \text{ kg/10}^3 \text{ l} = 0.085 \text{ kg/d}$$

$$32.85 \times 10^3 \text{ l/d} \times 0.00236 \text{ kg/10}^3 \text{ l} = 0.078 \text{ kg/d}$$

$$32.85 \times 10^3 \text{ l/d} \times 0.00020 \text{ kg/10}^3 \text{ l} = 0.007 \text{ kg/d}$$

$$32.85 \times 10^3 \text{ l/d} \times 0.00029 \text{ kg/10}^3 \text{ l} = \underline{0.010} \text{ kg/d}$$

Total 1.608 kg/d

Emitting Device: Temporary fuel storage tanks and filling hoses.

b. Reclaim Ponds R1 and R2

Reclaim Ponds R1 and R2 are estimated to have construction activities including excavation over approximately 49.4 and 29.6 acres, respectively. Using the TSP emission factor of 1.2 st/acre from EPA AP-42 results in calculated total TSP emissions of approximately 59.3 and 36 st, respectively. Since Reclaim Pond R2 is constructed over two years, the estimated TSP emissions of 36 st are approximately 18 st/yr.

c. Tailpipe Emissions - Use of diesel fuel to power off-road equipment during construction of mine/mill site. Diesel fuel will contain 0.4 weight percent sulfur maximum.

Emission Factors and Source: EPA NEDS-National Air Data Branch (MD-14)
(Off-road construction equipment).

Diesel

TSP	-	39.35	lb/10 ³	gal	burned
SO ₂	-	31.0	lb/10 ³	gal	burned
NO _x	-	376.2	lb/10 ³	gal	burned
CO	-	112.3	lb/10 ³	gal	burned
HC/VOC	-	56.4	lb/10 ³	gal	burned

Process Rate: 2.3×10^2 gal/day

Duration: 13.5 hr/day, 5 day/wk, 4.3 wk/month, 7 month/yr

Control Method and Efficiency: None - Values are best estimate of tailpipe exit components.

Example Calculation:

Process Rate x Emission Factor = Emission Rate

$$\text{TSP} - 2.3 \times 10^2 \text{ gal/day} \times 39.35 \text{ lb/10}^3 \text{ gal} = 9.1 \text{ lb/day}$$

$$\begin{aligned} & - 9.1 \text{ lb/day} \times 5 \text{ day/wk} \times 4.3 \text{ wk/month} \times 7 \text{ months/yr} \times \text{st/2000 lbs} \\ & = 0.7 \text{ st/yr} \end{aligned}$$

Total Estimated Tailpipe Emissions, Diesel Vehicles

	<u>st/yr</u>
TSP:	0.7
SO ₂ :	0.5
NO _x :	6.5
CO :	1.9
HC/VOC:	1.0

IV. MILL/CONCENTRATOR OPERATIONS

1. Mine/Mill Surface Facilities Operation

- a. Coarse Ore Transport - During the construction and operation phases, preproduction ore will be utilized or stored on the following schedule.

<u>Year</u>	<u>Ore Handled (k-st)</u>	<u>Ore In Storage (k-st)</u>
1	-	-
2	11	9*
3	523	532
4	366	898
5	898	-

* 2 k-st (k = thousand) processed in pilot plant.

Estimates of fugitive dust (TSP) generated from various activities associated with the preproduction ore handling and storage are presented below.

Transportation emissions:

Emission Factor and Source: AP-42, Section 11.2.1.3

$$\text{TSP-EF} = k \cdot 5.9 \left(\frac{s}{12}\right) \left(\frac{S}{30}\right)^{2**} \left(\frac{W}{3}\right)^{0.7} \left(\frac{w}{4}\right)^{0.5} \left(\frac{d}{365}\right) = \text{lb/veh-mile}$$

k = particle size multiplier (AP-42)

s = silt content (%)

S = vehicle speed (mph)

W = vehicle weight (st)

w = number of vehicle tires

d = number of dry days per year

** For speeds less than 30 mph, the square of the ratio of $\left(\frac{S}{30}\right)^2$ [i.e. $\left(\frac{5}{30}\right)^2$] is used as recommended by the Wyoming Department of Environmental Quality (Fugitive dust emission factors. WDEQ, Division of Air Quality. January 24, Memorandum from Charles A. Collins, 1979).

Ore transport (Hauling)

k = 0.8

s = 6%

S = 15 mph

W = 51 st average
(33 st truck empty)

w = 6 tires

d = 230 dry days

Maximum transport year = 1990

Tons hauled in year 1990 = 898,000 st

At 35 st/haul = 25,657 hauls

Average haul distance = 1.0 mile/
round trip.

Total mile haulage in 1990 = 25,657

hauls x 1.0 veh-mile/haul = 25,657

veh-miles.

Hauling from main shaft to storage pad in 35 st dump truck.

Haul distance = to storage - 1.2 mile round trip
 from storage - 1.0 mile round trip

$$\begin{aligned} \text{TSP-EF} &= (0.8)(5.9)(s/12)(s/30)^2(w/3)^{0.7}(w/4)^{0.5}(d/365) = \text{lb/veh-mile} \\ &= (4.72)(6/12)(15/30)^2(51/3)^{0.7}(6/4)^{0.5}(230/365) \\ &= 3.3 \text{ lb/veh-mile (uncontrolled)} \end{aligned}$$

Process Rate:

Year	Volume Hauled (k-st)		No. of Hauls	Miles Traveled	Emission (tons)
	To Storage	From Storage			
1	-	-	-	-	-
2	11	2*	371	446	0.1
3	524	-	14,971	17,965	4.5
4	366	-	10,457	12,548	3.1
5	-	898	25,657	25,657	6.4

Example Calculations:

$$\begin{aligned} \text{Emissions (uncontrolled)} &= 25,657 \text{ miles} \times 3.3 \text{ lb/veh-mile} \times \text{st}/2000 \text{ lbs} \\ &= 42.3 \text{ st} \end{aligned}$$

$$\text{Emissions (controlled)} = 42.3 \text{ st} \times 0.15^{**} = 6.4 \text{ st}$$

$$\begin{aligned} \text{Emissions (controlled)} &= 3.3 \text{ lb veh-mile} \times 446 \text{ veh-miles/yr} \times \text{st}/2000 \text{ lbs} \\ &\times 0.15^{**} = 0.1 \text{ st/yr} \end{aligned}$$

* Used in pilot plant testing.

** 85% control with watering and chemical stabilization.

Loading and dumping (L&D)

Loading: Cat 988B - 7 yd³ bucket

$$\text{TSP-EF} = (0.73)(0.0018) \frac{(1.6/5)(7.2/5)(4/5)}{(4/2)^2(7/6)^{0.33}} = 0.00012 \text{ lb/ton}$$

Dumping: 35 st dump truck - 35 st ÷ 2,500 lb/yd³ × 2,000 lb/st = 28 yd³

$$\text{TSP-EF} = (0.73)(0.0018) \frac{(1.6/5)(7.2/5)(4/5)}{(4/2)^2(28/6)^{0.33}} = 0.000073 \text{ lb/st}$$

Combined (loading and dumping) emission rate = 0.000193 lb/st

Example Calculation:

$$\begin{aligned} \text{Emissions (uncontrolled)} &= 0.000193 \text{ lb/st} \times 898,000 \text{ st/yr} \times \text{st}/2000 \text{ lbs} \\ &= 0.09 \text{ (0.1) st/yr.} \end{aligned}$$

<u>Year</u>	<u>Volume Loaded and Dumped (k-st)</u>	<u>Emissions (st/yr)</u>
2	13	0.00
3	524	0.05
4	366	0.04
5	898	0.10

Wind-blown emissions:

Emission Factors and Source: Evaluation of Fugitive Dust Emissions from Mining Task 1 Report.
Identification of Fugitive Dust Sources Associated with Mining. PEDCO - Environmental Specialists, Inc., 1976. Cincinnati, Ohio.

$$\text{TSP-EF} = a I K C L V^*$$

a = Portion of total wind erosion losses measured as suspended particles (a = 0.025 for waste rock and preproduction ore)

I = Soil erodibility, tons(st)/acre/year = 38 for waste rock and preproduction ore

K = Accounts for resistance to wind erosion provided by ridges and furrows or large soil clumps in the field. Ranges from 0.5 for a field with optimum ratio of ridge height to ridge spacing, to 1.0 (no reduction) for field with smooth surface.

Assume 0.75 for storage areas and MWDF.

C = Climatic factor = 0.05 in site area

L = Unsheltered field width = 0.7

V = Vegetation cover factor. Assume unvegetated. V = 1.0

* Universal soil loss equation

Ore wind-blown emissions

Total disturbed area in 1989 = 8 acres

$$\text{TSP-EF} = a I K C L V$$

$$a = 0.025$$

$$I = 38$$

$$K = 0.75$$

$$C = 0.05$$

$$L = 0.7$$

$$V = 1.0$$

$$\text{TSP-EF} = 0.02494 \text{ st/acre/yr}$$

Example Calculation:

$$\text{Emissions (uncontrolled)} = 0.2494 \text{ st/acre/yr} \times 8 \text{ acres} = 0.2 \text{ st/yr.}$$

Preproduction Ore Crushing and Handling:

Emission Factors and Source: AP-42, Table 8.23-1

$$\begin{aligned} \text{TSP-EF} &= 0.5 \text{ lb/st} - \text{Primary Crushing} \\ &= 0.12 \text{ lb/st} - \text{Materials Handling} \end{aligned}$$

Process Rate: 440 st/hr, 5,510 st/day, 898,000 st/yr

Duration: 18 months (maximum in year 1990)

Control Method and Efficiency: Baghouse collector, 99% efficiency

Example Calculation:

$$\begin{aligned} \text{TSP} - 898,000 \text{ st/yr} \times 0.5 \text{ lb/st} \times (1-0.99) \times \text{st}/2000 \text{ lbs} &= 2.2 \text{ st/yr} \\ 898,000 \times 0.12 \times 2 \times (1-0.99) \times \text{st}/2000 \text{ lbs} &= \underline{1.1 \text{ st/yr}} \\ \text{Total} &= 3.3 \text{ st/yr} \end{aligned}$$

<u>Activity</u>	<u>TSP Emissions (st/yr)</u>
Hauling of preproduction ore	6.4
Loading and dumping of pre-production ore	0.1
Ore wind-blown emissions	0.2
Preproduction ore crushing and handling	<u>3.3</u>
	<u>10.0</u>

Total Preproduction Ore Handling (Coarse Ore Transport) Emissions

<u>Year</u>	<u>Hauling</u>	<u>L&D</u>	<u>Crushing</u>	<u>Wind-Blown</u>	<u>Total (TSP - st/yr)</u>
1	-	-	-	-	-
2	0.1	0.0	-	0.2	0.3
3	4.4	0.05	-	0.2	4.7
4	3.1	0.04	-	0.2	3.3
5	6.4	0.1	3.3	0.2	10.0

b. Fine Ore Crushing and Screening - Crushing and screening of high moisture ore

Emission Factors and Source: AP-42, Table 8.23-1

TSP-EF = 0.03 kg/t secondary and tertiary crushing
0.005 kg/t handling

Duration: 24 hr/day, 365 days/yr

Process Rate: 620 t/hr, 14,880 t/day, 3,629,000 t/yr

Control Method and Efficiency: Wet impingement scrubber - 97.9%

Example Calculation:

$$\begin{aligned} \text{TSP} &= 3,629,000 \text{ t/yr} \times 0.03 \text{ kg/t} \times 2 \text{ (crushing and screening)} \times \\ &\quad (1-0.979) \div \text{t/1000 kg} = 4.6 \text{ t/yr} \\ &= 4.6 \text{ t/yr} \times 1.1 \text{ st/t} = 5.1 \text{ st/yr} \end{aligned}$$

$$\begin{aligned} \text{TSP} &= 3,629,000 \times 0.005 \times 9 \text{ (handling)} \times (1-0.979) \div 1000 = 3.4 \text{ t/yr} \\ &= 3.4 \text{ t/yr} \times 1.1 \text{ st/yr} = 3.8 \text{ st/yr} \end{aligned}$$

Total estimated TSP emissions from crushing and screening are 8.9 st/yr.

c. Fine Ore Bin Loading and Unloading - Loading and unloading of Zn-Cu-Pb and Cu-Zn ore into and from fine ore storage bins.

Emission Factor and Source: AP-42, Table 8.23-1

TSP - Ore Handling = 0.005 kg/t

Process Rate: 620 t/hr, 14,880 t/day, 3,629,000 t/yr

Control Method and Efficiency: Wet impingement scrubber - 97.9%

Example Calculation:

$$\text{TSP} - 3,629,000 \text{ t/yr} \times 14(\text{pickup points}) \times 0.005 \text{ kg/t} \times (1-0.979) \times \text{t}/1,000 \text{ kg} = 5.3 \text{ t/yr} (5.8 \text{ st/yr})$$

- d. Concrete Batch Plant - Typical batching of concrete for miscellaneous mine/mill site applications.

Emission Factor and Source: AP-42, Table 8.10-2

	<u>kg/mt</u>
TSP - Transfer of sand and aggregate to elevated bins	= 0.02
Cement unloading to elevated storage silos	= 0.118
Weight hopper loading of cement, sand, and aggregate	= 0.118
Mixer loading of cement, sand, and aggregate	= 0.01
Loading of dry-batch truck	= 0.02

Process Rate: 38.3 m³/shift, 1 shift/day, 5 days/wk, 52 wks/yr

Sand and Aggregate	75.2 t/day	19,558 t/yr
Cement	<u>16.7 t/day</u>	<u>4,342 t/yr</u>
Total	91.9 t/day	23,900 t/yr

Control Method and Efficiency: Baghouse with ducting and insertable collector - 99% control efficiency, AP-42, Table 8.10-1; Other - 90% control efficiency

Example Calculation:

TSP (annual):

$$\begin{aligned} 19,558 \text{ t/yr} \times 0.02 \text{ kg/t} \times (1-0.90) \div 1,000 \text{ kg/t} &= 0.04 \text{ t/yr} \\ 4,342 \text{ t/yr} \times 0.118 \text{ kg/t} \times (1-0.99) \div 1,000 \text{ kg/t} &= 0.005 \text{ t/yr} \\ 23,900 \text{ t/yr} \times 0.118 \text{ kg/t} \times (1-0.90) \div 1,000 \text{ kg/t} &= 0.282 \text{ t/yr} \\ 23,900 \text{ t/yr} \times 0.01 \text{ kg/t} \times (1-0.90) \div 1,000 \text{ kg/t} &= 0.024 \text{ t/yr} \\ 23,900 \text{ t/yr} \times 0.02 \text{ kg/t} \times (1-0.90) \div 1,000 \text{ kg/t} &= \underline{0.048 \text{ t/yr}} \\ &= 0.399 \text{ t/yr} \\ &= (0.44 \text{ st/yr}) \end{aligned}$$

Total Annual Estimated Emissions = 0.40 t/yr x 1.1 st/t = 0.44 st/yr

- e. Facility Heating - Natural gas is used for three purposes in the surface facilities. They are: 1) heating the buildings, 2) water heating, and 3) water treatment (brine crystallizer). Each of these processes is described in the following under its respective heading.

Heating Buildings - Use of natural gas unit heaters. Heat content is 1000 BTU/SCF for natural gas.

Emission Factors and Source: EPA-NEDS, Appendix C, p. C-3, December 1975 - <10M BTU/hr.

TSP-EF = 10.0 lb/10⁶ SCF of natural gas

SO_x-EF = 0.6 lb/10⁶ SCF of natural gas

NO_x-EF = 120.0 lb/10⁶ SCF of natural gas

CO-EF = 17.0 lb/10⁶ SCF of natural gas

HC-EF = 3.0 lb/10⁶ SCF of natural gas

Process Rate: 17,350 SCF/hr, 416,400 SCF/day, and 33,960,000 SCF/yr of natural gas

Duration: As required by weather conditions

Control Method and Efficiency: Use of natural gas

Example Calculation:

$$\text{TSP} - (33,960,000)(10.0/1,000,000)/2000 = 0.17 \text{ st/yr}$$

Water Heating - Heating of water in the concentrator building for the process using a 42,000 BTU/hr boiler. Also, heating water in the plant services building for washrooms and showers using a 1,005,000 BTU/hr water heater.

Emission Factors and Source: Same as building heating.

Process Rate: 1,047 SCF/hr, 25,128 SCF/day, and 9,172,000 SCF/yr of natural gas.

Duration: 24 hrs/day, 365 days/yr

Control Method and Efficiency: Use of natural gas

Example Calculation:

$$\text{TSP} - (9,172,000)(10.0/1,000,000)/2000 = 0.05 \text{ st/yr}$$

Water Treatment - Use of a boiler for VCE (i.e. initial) and brine crystallization operations in the vapor compression evaporator process. Boiler will consume 14,600,000 BTU/hr of natural gas.

Emission Factors and Source: Same as for heating buildings.

Process Rate: 14,600 SCF/hr, 350,400 SCF/day, and 127,900,000 SCF/yr of natural gas

Duration: 24 hrs/day, 365 days/yr

Control Method and Efficiency: Use of natural gas

Example Calculation:

$$\text{TSP} - (127,900,000)(10.0/1,000,000)/2000 = 0.64 \text{ st/yr}$$

Total Estimated Facility Heating TSP Emissions

	<u>TSP (st/yr)</u>
Heating Buildings	0.17
Water Heating	0.05
Water Treatment	<u>0.64</u>
Total	0.86 (0.90)

- f. Fuel Transfer and Storage (Bulk Storage Facility and Service Station) - Transfer and storage of gasoline and diesel fuel (2 - 30,000 gal tanks).

Emission Factors and Source: AP-42, Table 4.3-5

$$\text{HC} - 2 \times \text{lb (lb/yr)} = 2.26 \times 10^{-2} M \left[\frac{P}{14.7-P} \right]^{0.68} D^{1.7} H^{0.51} T^{0.5} F_p C K_c$$

M = 130 (Molecular Weight of Vapor), AP-42, Table 4.3-1

P = 0.0064 psia (vapor pressure @ 60°F), AP-42, Table 4.3-1

D = 26 ft (tank diameter)

H = 6.3 ft (vapor space at 1/2 tank height)

T = 15°F (temperature variation from day to night)

F_p = 1 (paint factor), AP-42, Table 4.3-2

C = 1 (adjustment factor), AP-42, Figure 4.3-10

K_c = 1 AP-42, Table 4.3-6

Adjustment for fixed roof working loss

LW = $2.4 \times 10^{-2} M P K_h K_c$, AP-42, Table 4.3-8

Gasoline - Tank emissions, AP-42, Table 4.4-4

- 1) 0.88 kg/10³ l (filling buried tank) x 1892.5 l/d for 350 days/yr
- 2) 0.12 kg/10³ l (breathing loss) x 1892.5 l/d for 350 days/yr
- 3) 1.08 kg/10³ l (dispensing loss) x 1892.5 l/d for 350 days/yr

Diesel - Tank emissions, AP-42, Tables 4.3-1 and 4.4-4.

A direct proportion of gasoline to diesel use exists for fixed roof tank working loss and is shown below.

$$\frac{(0.0064 \text{ v.p.}) (130 \text{ mw}) \text{ Diesel}}{(5.2 \text{ v.p.}) (66 \text{ mw}) \text{ Gasoline}} = 0.0024 \text{ multiplier for 1), 2), and 3) above}$$

Process Rate: 6000 gal/day

Control Method and Efficiency: Vapor balance system for fuel loading at the storage facility and service station - 95% efficiency

Example Calculations:

$$(\text{Process Rate}) \times (\text{Emission Factor}) \times (1 - \text{Efficiency}) = \text{Emission Rate}$$

$$\text{HC: } 6000 \text{ gal/day} \times 34.1 \text{ lbs/gal/yr} \times \text{st}/2000 \text{ lbs} \times .05 = 5.1 \text{ st/yr}$$

- g. Emergency Diesel Generators - The use of 3 emergency (i.e. backup) diesel generators is required to supply electrical power in the event transmission line service is interrupted to the Project facilities. For this purpose two 2500- and one 1000-kw units will supply emergency power for the mine and for the mill facilities, respectively. These units are intended for use only in emergencies. However, to assure their ability to perform, weekly operation of each unit is necessary for a maximum of 1 hour. Also, emergency operation was estimated to be 2.5 hours per year. Total diesel fuel usage will be 192 gallons per hour per 2500-kw unit, 461 gallons per day (i.e. weekly test), and 25,125 gallons per year including the weekly and emergency operation of each unit.

Use of two 2500-kw for the mine and one 1000-kw generator for the mill for emergencies.

Emission Factors and Source: EPA, AP-42, Appendix-C, Internal combustion-electric generation-diesel, p.C-6.

TSP - 13.0 lbs/10³ gal
SO_x - 140.0 lbs/10³ gal
NO_x - 370.0 lbs/10³ gal
CO - 225.0 lbs/10³ gal
HC 37.0 lbs/10³ gal

Process Rate: 192 gal/hr, 461 gal/day, 25,125 gal/yr

Duration: Each unit will be operated a maximum of 1 hr/wk, and estimated emergency purposes are 2.5 hr/yr.

Control Method and Efficiency: None

Example Calculation:

$$\text{TSP} - 25,125 \text{ gal/yr} \times 13.0 \text{ lbs}/10^3 \text{ gal} \times \text{st}/2000 \text{ lbs} = 0.2 \text{ st/yr}$$

Total estimated emissions are as follows:

	<u>st/yr</u>
TSP:	0.2
SO _x :	1.8
NO _x :	4.7
CO :	2.8
HC :	0.5

- h. Vehicular Travel, Plant Vehicles Exhaust - The current estimated mine/mill plant operation traffic load is 186 miles/day. A conservative assumption was used in that the estimated plant operation miles traveled of 186 miles/day was equally on paved and gravel roads. The calculations, therefore, overestimate the potential TSP emissions since only portions of the miles traveled will be on either road surface.

Mine/Mill Site

Emission Factors and Source: AP-42, Appendix D, Tables D.2-10 and D.2-16 (LDGV-1990); Tables D.4-10 and D.4-15 (HDGV-1990); Tables D.5-1 and D.5-4 (HDDV-1990).

<u>LDGV (g/mi)</u>		<u>HDGV (g/mi)</u>		<u>HDDV (g/mi)</u>	
TSP-EF	0.05	TSP-EF	0.91	TSP-EF	1.3
SO ₂ -EF	0.18	SO ₂ -EF	0.36	SO ₂ -EF	2.8
NO _x -EF	2.3	NO _x -EF	11.4	NO _x -EF	18.1
CO -EF	9.8	CO -EF	117.0	CO -EF	28.7
HC -EF	1.0	HC -EF	6.0	HC -EF	4.6

Process Rate:

Light Duty Gasoline Vehicle (LDGV)

(Pick-up Trucks)	<u>Duty</u>	<u>miles/day</u>
Assume: 20 miles/hr	Environmental	25
4 wheels	Inspections	45
	Security	50
	Maintenance	10
	Warehouse	<u>2.5</u>
	Total	132.5

Heavy Duty Gasoline Vehicle (HDGV)

Assume: 15 miles/hr	<u>Duty</u>	<u>miles/day</u>
6 wheels	Water Truck	20
	Trucks	<u>6.5</u>
	Total	26.5

Heavy Duty Diesel Vehicle (HDDV)

Assume: 10 miles/hr	<u>Duty</u>	<u>miles/day</u>
6 wheels	Grader	5
	Backhoe	0.5
	60 st Crane	0.5
	10 st Crane	0.5
	Tractor/Trailer	0.5
	Forklifts	<u>20</u>
	Total	27.0

Control Method and Efficiency: As per EPA vehicle emission controls.

Example Calculation: Process Rate x Emission Factor = Emission Rate.

$$\text{LDGV TSP} - 132.5 \text{ mi/d} \times 350 \text{ d/yr} \times 0.05 \text{ g/mi} \times 0.002 \text{ lbs/g} \times \text{st}/2000 \text{ lb} = 0.002 \text{ st/yr}$$

$$\text{SO}_x - 132.5 \times 350 \times 0.18 \times 0.002 \times 0.0005 = 0.008 \text{ st/yr}$$

$$\text{NO}_x - 132.5 \times 350 \times 2.3 \times 0.002 \times 0.0005 = 0.11 \text{ st/yr}$$

$$\text{CO} - 132.5 \times 350 \times 9.8 \times 0.002 \times 0.0005 = 0.46 \text{ st/yr}$$

$$\text{HC} - 132.5 \times 350 \times 1.0 \times 0.002 \times 0.0005 = 0.05 \text{ st/yr}$$

$$\text{HDGV TSP} - 26.5 \text{ mi/d} \times 350 \text{ d/yr} \times 0.91 \text{ g/mi} \times 0.002 \text{ lbs/g} \times \text{st}/2000 \text{ lb} = 0.008 \text{ st/yr}$$

$$\text{SO}_x - 26.5 \times 350 \times 0.36 \times 0.002 \times 0.0005 = 0.003 \text{ st/yr}$$

$$\text{NO}_x - 26.5 \times 350 \times 11.4 \times 0.002 \times 0.0005 = 0.11 \text{ st/yr}$$

$$\text{CO} - 26.5 \times 350 \times 117.0 \times 0.002 \times 0.0005 = 1.09 \text{ st/yr}$$

$$\text{HC} - 26.5 \times 350 \times 6.0 \times 0.002 \times 0.0005 = 0.06 \text{ st/yr}$$

$$\text{HDDV TSP} - 27.0 \text{ mi/d} \times 350 \text{ d/yr} \times 1.3 \text{ g/mi} \times 0.002 \text{ lbs/g} \times \text{st}/2000 \text{ lbs} = 0.01 \text{ st/yr}$$

$$\text{SO}_x - 27 \times 350 \times 2.8 \times 0.002 \times 0.0005 = 0.03 \text{ st/yr}$$

$$\text{NO}_x - 27 \times 350 \times 18.1 \times 0.002 \times 0.0005 = 0.17 \text{ st/yr}$$

$$\text{CO} - 27 \times 350 \times 28.7 \times 0.002 \times 0.0005 = 0.27 \text{ st/yr}$$

$$\text{HC} - 27 \times 350 \times 4.6 \times 0.002 \times 0.0005 = 0.04 \text{ st/yr}$$

Total estimated plant vehicle exhaust emissions

TSP: 0.02 st/yr
SO_x: 0.04 st/yr
NO_x: 0.39 st/yr
CO : 1.82 st/yr
HC : 0.15 st/yr

- i. Vehicular Travel, Employee Vehicles - Current estimates indicate that approximately 703 operation phase personnel will be employed by the Crandon Project. It is also assumed that there will be 1.6 employees/vehicle traveling 2.5 miles (one way) of access road to the mine/mill site. Therefore, at this rate (2 trips/day x 2.5 miles/trip x 703/1.6 employees per vehicle), approximately 2,200 vehicle miles would be traveled per day.

Emission Factor and Source: AP-42, Appendix D, Table D.1-19 (1987)

Process Rate: Employee vehicles - 2200 mi/day (LDV).

Duration: 350 days/yr

Control Method and Efficiency: As per EPA vehicle emission controls.

Example Calculation: Process Rate x Emission Factor = Emission Rate.

TSP: 2200 mi/day x 0.05 g/mi x 0.002 lbs/g x 350 days/yr x st/2000 lbs
= 0.04 st/yr
SO_x: 2200 x 0.13 (Table D.1-21) x 0.002 x 350 ÷ 2000 = 0.1 st/yr
NO_x: 2200 x 0.40 x 0.002 x 350 ÷ 2000 = 0.3 st/yr
CO : 2200 x 3.6 x 0.002 x 350 ÷ 2000 = 2.8 st/yr
HC : 2200 x 0.43 x 0.002 x 350 ÷ 2000 = 0.3 st/yr

Emitting Device: Tailpipes of vehicles

V. MWDF CONSTRUCTION AND OPERATIONS

1. Site Preparation

MWDF Area - The surface area of construction disturbance for tailing pond T1 is estimated to be approximately 94 acres. Within this area, site preparation includes clearing the land and surface earthwork for stump removal and soil storage for reclamation (i.e. excavation to approximately 10 ft). This estimate uses the primary emission factor from AP-42 for construction activities for project facilities. However, where deep excavation (greater than 10 ft) and major hauling of soil material within the excavated area is involved, the estimated TSP emissions from hauling, and loading and dumping of the soil material were calculated separately (i.e. in addition to the surface area construction estimate).

Emission Factor and Source: AP-42, Section 11.2.4

TSP-EF = 1.2 st/acre/month.

Process Rate: Based on largest surface area disturbed in one year - Tailing Pond T1 - 94 acres.

Because many areas of the additional tailing ponds are part of the previous construction activities (i.e. common embankment sections), it was assumed that 94 acres represents the additional surface area disturbance for the other ponds. Therefore, the estimated TSP emissions of 112.8 st was used for the early construction activities for the other tailing ponds.

Duration: 12 months (94 ÷ 12 = 7.83 acres/month)

Control Method and Efficiency: Watering, if necessary.

Example Calculation:

$$\text{TSP} = 1.2 \text{ st/acre/month} \times 7.8 \text{ acres/month} \times 12 \text{ months/yr} = 112.8 \text{ st/yr}$$

2. Construct MWDF Facilities

a. Waste Rock Handling - Loading and dumping

Emission Factor and Source: AP-42, Section 11.2.3

$$\text{TSP-EF} = (k)(0.0018) \frac{(s/5)(U/5)(H/5)}{(M/2)^2(Y/6)0.33} = 1\text{b/st}$$

TSP-EF = emission factor - lb/st
 k = particle size multiplier (dimensionless) - 0.73
 s = silt content - %
 U = wind speed (mph) - 7.2 mph (Crandon Project EIR, p. 2.1-17)
 H = drop height - ft
 M = material moisture content - %
 Y = capacity of dumping device (yd³)

Process Rate: See below.

Duration: See below.

Control Method and Efficiency: None

Example Calculation:

$$\text{TSP-EF(Loading)} = (0.73)(0.0018) \frac{(1.6/5)(7.2/5)(4/5)}{(4/2)^2(7/6)^{0.33}} = 0.00012 \text{ lb/st}$$

$$\text{TSP-EF(Dumping)} = (0.73)(0.0018) \frac{(1.6/5)(7.2/5)(4/5)}{(4/2)^2(28/6)^{0.33}} = 0.000073 \text{ lb/st}$$

Combined TSP-EF = 0.000193 lb/st for loading and dumping

$$761,000 \text{ st/yr} \times 0.000193 \text{ lb/st} \times \text{st}/2000 \text{ lbs} = 0.07 \text{ st/yr}$$

<u>Year</u>	<u>Waste Rock (k-st)</u>	<u>Emissions (st/yr)**</u>
1	11	-
2	66	0.01
3	761	0.07
4	1,144	0.11
5-8	297	0.03
9-27	136	0.01

b. Hauling

Emission Factor and Source: AP-42, Section 11.2.1

$$\text{TSP-EF} = (0.8)(5.9)(s/12)(S/30)^2(W/3)^{0.7}(w/4)^{0.5}(d/365) \\ = \text{lb/veh-mile}$$

TSP-EF = suspended particulates - lb/veh-mile
 s = silt content of road material - %
 S = vehicle speed (mph)
 W = average vehicle weight - st
 w = number of wheels on vehicle
 d = dry days/year - 230

Process Rate: See below.

Duration: See below.

Control Method and Efficiency: Watering and chemical stabilization.

Example Calculation:

$$\begin{aligned} \text{TSP-EF} &= (0.8)(5.9)(6/12)(15/30)^2(51/8)^{0.7}(6/4)^{0.5}(0.63) \\ &= 3.3 \text{ lb/veh-mile} \end{aligned}$$

$$\begin{aligned} \text{Emissions (controlled)} &= 3.3 \text{ lb/veh-mile} \times 1400 \text{ veh-miles} \times \text{st}/2000 \text{ lbs} \\ &\quad \times 0.15^* \\ &= 0.35 \text{ st/yr} \end{aligned}$$

<u>Year</u>	<u>Waste Rock Hauled (k-st)</u>	<u>Miles Traveled (k)</u>	<u>Controlled Emissions (st/yr)*</u>
1	11	1.4	0.35
2	66	8.3	2.1
3	761	95.7	23.7
4	1,144	143.8	35.6
5-8	297	37.3	9.23
9-27	136	17.1	4.23

* 85% control with watering and chemical stabilization.

3. Construct Tailing Pipeline - The estimated acreage disturbed for construction of the tailings pipeline including excavation is approximately 10 acres.

Emission Factor and Source: AP-42, Section 11.2.4

$$\text{TSP-EF} = 1.2 \text{ st/acre/month}$$

Process Rate: The tailing pipeline is constructed over 2 years. Therefore, approximately 5 acres per year is the estimated acreage disturbed during construction.

Duration: 2 years

Control Method and Efficiency: Watering, if necessary.

Example Calculation:

$$\text{TSP} = 1.2 \text{ st/acre/month} \times 5 \text{ acres/yr} = 6.0 \text{ st/yr}$$

4. Construct Tailing Pond T4 - Till excavation is assumed to occur equally over two years for each pond. Other activities such as loading and dumping, and hauling of other construction soil materials (i.e. drain layer, liner) were conservatively assumed to be completed in the second year of each pond development.

a. Hauling - TSP emissions generated by hauling excavated till within the pond construction area, within the MWDF boundary, and between the mine/mill site and MWDF.

Emission Factor and Source: EPA AP-42, Section 11.2.1

$$\text{TSP-EF} = (0.8)(5.9)(s/12)(S/30)^2(w/3)^{0.7}(w/4)^{0.5}(d/365) = \text{lb/veh-mile}$$

TSP-EF = suspended particulate - lb/veh-mile

s = silt content of road material - %
 S = vehicle speed (mph)
 W = average vehicle weight - st
 w = number of wheels on vehicle
 d = dry days/year - 230

Assume: Pond with largest quantity of soil material (till) excavation - Tailing Pond T4 (i.e. average excavation is 40 ft - upper 10 ft included in emissions from site preparation). Therefore, 75% of excavated till haulage is within the pond area.

Process Rate:

<u>Source</u>	<u>s</u>	<u>S</u>	<u>w</u>	<u>W</u>	<u>d</u>	<u>Emission Factor</u> <u>lbs/veh-mile</u>	<u>Control Efficiency</u>	<u>Soil Material Moved</u> <u>k-yd³</u>	<u>Miles Traveled</u>
1. Hauling excavated till within pond	15	15	4	63	230	7.82	50% ^a	1,913 ^b	34,434
2. Bentonite/soil to pond	6	15	6	30	230	2.27	85% ^c	90 ^d	5,012
3. Underdrain to pond	6	15	6	30	230	2.27	85%	264 ^d	12,375
4. Filter mat'l to pond	6	15	6	16	230	2.27	85%	383 ^d	20,826
5. Rip-rap to pond	6	15	6	16	230	2.27	85%	237 ^d	11,109

a 50% control with watering.

b Each of the two years of construction.

c 85% control with watering and chemical stabilization.

d All in second year of T-4 construction.

Duration: Two years of construction for each pond with the development of the new storage capacity phased to coincide with disposal needs.

Control Method and Efficiency: See above - Process Rate

Example Calculation:

$$\begin{aligned} \text{TSP} &= (0.8)(5.9)(15/12)(15/30)^2(63/3)^{0.7}(4/4)^{0.5}(230/365) = \text{lb/veh-} \\ &= (4.72)(1.25)(0.25)(8.42)(1)(0.63) = 7.82 \text{ lb/veh-mile} \end{aligned}$$

$$\begin{aligned} \text{Emissions (controlled)} &= 7.82 \text{ lb/veh-mile} \times 34,434 \text{ miles} \times \text{st}/2000 \text{ lb} \\ &\quad \times 0.5^* \\ &= 67.3 \text{ st} \end{aligned}$$

* 50% control with watering.

<u>Total Estimated Emissions from Hauling</u>	<u>TSP (st/yr)</u>
1. Hauling excavated till within pond	67.3
2. Bentonite/soil to pond	0.85
3. Underdrain to pond	2.11
4. Filter material to pond	3.55
5. Rip-rap to pond	1.89
	<u>75.7</u>

b. Loading and Dumping

Emission Factor and Source: AP-42, Section 11.2.3

$$\text{TSP-EF} = (k)(0.0018) \frac{(s/5)(U/5)(H/5)}{(M/2)^2(Y/6)^{0.33}} = \text{lb/st}$$

TSP-EF = emission factor - lb/st

k = particle size multiplier (dimensionless) - 0.73

s = silt content - %

U = wind speed (mph) - 7.2 mph (Crandon Project EIR, p. 2.1-17)

H = drop height - ft

M = material moisture content - %

Y = capacity of dumping device (yd³)

Assume: Construction of Tailing Pond T-4

Process Rate:

Source	s	U	H		M	Y		Soil Material (k-st)	Emission Factor (lb/st)	
			Loading	Dumping		Loading	Dumping		Loading	Dumping
1. Till at batch plant	15	7.2	3	3	2	4.5	8	122	0.0037	0.0031
2. Underdrain	1.6	7.2	3	3	4	4.5	9.6	330	0.0001	0.00008
3. Filter	15	7.2	3	3	2	4.5	8	569	0.0037	0.0031
4. Rip-rap	1.6	7.2	3	3	4	4.5	9.6	296	0.0001	0.00008

Duration: Two years of construction for each pond, but most likely in last year only.

Control Method and Efficiency: None

Example Calculation:

$$\text{TSP-EF(Loading Till)} = (0.73)(0.0018) \frac{(15/5)(7.2/5)(3/5)}{(2/2)^2(4.5/6)0.33} = 0.0037 \text{ lb/st}$$

$$\text{Emissions (uncontrolled)} = 0.0037 \text{ lb/st} \times 82,800 \text{ yd}^3 \times 2970 \text{ lb/yd}^3 \\ \times \text{st}/2000 \text{ lb} \times \text{st}/2000 \text{ lb} = 0.23 \text{ st}$$

Total Estimated Emissions from Loading and Dumping	TSP (st/yr)	
	Loading	Dumping
1. Till at batch plant	0.23	0.19
2. Underdrain	0.017	0.013
3. Filter	1.05	0.88
4. Rip-rap	0.015	0.012

c. Wind-blown

Emission Factor and Source: Guide for Wind Erosion Control on Cropland in Great Plains States, Craig and Turelle, USDA-SCS, July 1964, in: Evaluation of fugitive dust emissions (PEDCo, 1976).

TSP-EF = aIKCLV

TSP-EF = st/acre/yr

a = total of wind erosion losses measured as suspended particulates (0.01 for ponds and storage area and 0.025 for haul roads)

I = soil erodibility factor (st/acre/yr)
(134 for ponds and storage areas and 38 for haul road)

K = surface roughness factor - 1.0

C = climate factor; 0.05 for Crandon Project site area

L = unsheltered field width; 0.7 to 1.0 for Crandon Project site area

V = vegetative cover factor - 1.0

Process Rate:

<u>Source</u>	<u>Acreage</u>	<u>Control*</u>	<u>Emission Factor</u>
Haul Road	16	0.85	0.03325 st/acre
Storage Area	20	0.85	0.0469 st/acre
Ponds	119	--	0.0469 st/acre

Duration: Two years of construction for each pond, but most likely in last year only.

Control Method and Efficiency: See above - Process Rate

Example Calculation:

$$\begin{aligned} \text{TSP} &= \text{aIKCLV} = \text{st/acre} \\ &= (0.025)(38)(1)(0.05)(0.7)(1) = 0.03325 \text{ st/acre} \\ &= 0.03325 \text{ st/acre} \times 16 \text{ acres/yr} \times 0.15^* = 0.08 \text{ st/yr} \end{aligned}$$

* 85% control with watering and chemical stabilization

<u>Total Estimated Wind-blown Emissions</u>	<u>TSP (st/yr)</u>
Haul Road	0.08
Storage area	0.14
Ponds	5.58
	<u>5.80</u>

d. Summary of Estimated MWDF Construction Emissions

Process Rate:

Activity	Vehicle Size	Mat'l Bulk Density	Round Trip Distance/ Haul	Volume of Material Moved by Area (k-yd ³)			
				T-1	T-2	T-3	T-4
Excavation	25 yd ³	2970 lb/yd ³	0.45 mi	3,068	4,652	3,750	5,100
Soil/Bentonite Mixture	12 st	2970 lb/yd ³	0.45 mi	95	99	82	90
Underdrain	12 st	2500 lb/yd ³	0.45 mi	288	296	234	264
Filter Mat'l	12 st	2900 lb/yd ³	0.45 mi	280	460	357	383
Rip-rap	12 st	2500 lb/yd ³	0.45 mi	353	318	222	237

<u>Total Estimated MWDF Construction Emissions</u>			<u>TSP (st/yr)</u>	
			<u>Year 1</u>	<u>Year 2</u>
Tailing Pond T-1 (Construction Year 3-4)	Hauling Loading and Dumping Wind-Blown		41.0	49.6
			--	1.8
			5.8	5.8
			<u>46.8</u>	<u>57.2</u>
Tailing Pond T-2 (Operation Years 4-5)	Hauling Loading and Dumping Wind-Blown		61.0	71.1
			--	2.7
			5.8	5.8
			<u>66.8</u>	<u>79.6</u>
Tailing Pond T-3 (Operation Years 11-12)	Hauling Loading and Dumping Wind-Blown		50.0	57.7
			--	2.1
			5.8	5.8
			<u>55.8</u>	<u>65.6</u>
Tailing Pond T-4 (Operation Years 17-18)	Hauling Loading and Dumping Wind-Blown		67.3	75.7
			--	2.4
			5.8	5.8
			<u>73.1</u>	<u>83.9</u>

5. Tailpipe Emissions

- a. Diesel Vehicles - Assumes all excavation and scraper equipment will use diesel fuel. Therefore, estimated miles for construction are for heavy duty diesel vehicles (HDDV).

Emission Factor and Source: AP-42, Appendix D, Tables D.5-1 and D.5-4 (HDDV-1990).

HDDV	(g/mi)
TSP-EF	= 1.3
SO _x -EF	= 2.8
NO _x -EF	= 18.1
CO -EF	= 28.7
HC -EF	= 4.6

Process Rate: 34,434 miles over two years of construction for each pond.

Duration: Two years of construction for each pond with the development of the new storage capacity phased to coincide with disposal needs.

Control Method and Efficiency: As per EPA vehicle emission controls.

Example Calculation:

Process Rate x Emission Factor = Emission Rate.

$$\text{TSP} = 34,434 \text{ mi}/2 \text{ yr} \times 1.3 \text{ g/mi} \times \text{t}/10^6 \text{ g} \times \text{st}/1.1 \text{ t} = 0.02 \text{ st/yr}$$

<u>Total Estimated Emissions for Diesel Vehicle Tailpipe Emissions</u>		<u>st/yr</u>
TSP		0.02
SO _x		0.04
NO _x		0.28
CO		0.45
HC		0.07

- b. Gasoline Vehicles - Assumes all of this activity occurs in the second year of construction.

Emission Factor and Source: AP-42, Appendix D, Tables D.2-10 and D.2-16 (LDGV-1990); Tables D.4-10 and D.4-15 (HDCV-1990).

LDGV	(g/mi)
TSP-EF	= 0.05
SO _x -EF	= 0.18
NO _x -EF	= 2.3
CO -EF	= 9.8
HC -EF	= 1.0

Process Rate: LDGV - 49,322 miles per year

Duration: Mainly during second year of construction of each pond.

Control Method and Efficiency: As per EPA vehicle emission controls.

Example Calculation:

Process Rate x Emission Factor = Emission Rate

$$\text{TSP} = 49322 \text{ mi/yr} \times 0.05 \text{ g/mi} \times \text{t}/10^6 \text{ g} \times \text{st}/1.1 \text{ t} = 0.002 \text{ st/yr}$$

<u>Total Estimated Emissions for Gasoline Vehicles</u>	<u>st/yr</u>
TSP	0.002
SO _x	0.008
NO _x	0.103
CO	0.439
HC	0.045

6. Install Liner - Soil processing and liner batch plants

a. Batch Plant

Emission Factors and Source: AP-42, Section 8.10, Concrete Batching

TSP-EF = 0.21 lb/yd³ processed

Process Rate: 102,020 yd³/yr

Duration: Not applicable

Control Method and Efficiency: Enclosed facility with air vented to filters - 90%

Example Calculation:

Emission Factor x Process Rate x Unit Conversion x Control Factor =
Annual Emission Rate

TSP = 0.2 lb/yd³ x 102,020 yd³/yr x st/2000 lb x 0.10 = 1.02 st/yr

b. Processing Plant

Emission Factors and Sources: AP-42, Section 8.19, Sand and Gravel Processing

TSP-EF = 0.1 lb/st processed

Process Rate: 139,380 st/yr

Duration: Not applicable

Control Method and Efficiency: Facility enclosed, air passed through baghouse - 99.6%

Example Calculation:

Emission Factor x Process Rate x Unit Conversion x Control
Factor = Annual Emission Rate

TSP = 0.1 lb/st x 139,380 st/yr x st/2000 lb x 0.004 = 0.028 st/yr

c. Hauling of Bentonite From Mill To Batch Plant Area

Emission Factor and Source: AP-42, Section 11.2.1

Assume 12 st tractor/trailer
Vehicle weight empty = 10 st
Vehicle weight loaded = 22 st
s = 6%
S = 15 mi/hr
W = 16 st avg.
w = 18
d = 230 days

$$\text{TSP-EF} = (0.8)(5.9)(6/12)(15/30)^2(16/3)^{0.7}(18/4)^{0.5}(0.6) = 2.4 \text{ lb/veh-mile}$$

Process Rate: 4,995 miles travelled/yr of liner material production.

Duration: Mainly during second year of construction of each pond.

Control Method and Efficiency: Watering and chemical stabilization.

Example Calculations:

$$\begin{aligned} \text{Total annual TSP emissions (uncontrolled)} &= 4,995 \text{ miles/yr} \times 2.4 \text{ lb/veh-mile} \\ &\quad \times \text{st}/2000 = 6.0 \text{ st/yr} \end{aligned}$$

$$\text{Total annual TSP emissions (controlled)} = 6.0 \text{ st/yr} \times 0.15^* = 0.9 \text{ st/yr}$$

* 85% control with chemical stabilization of haul road.

VI. Closure

Reclamation - The following calculations estimate the reclamation phase TSP air emissions. The general emission factor for TSP of 1.2 st/acre/month provided in U.S. EPA AP-42, Section 11.2.4 represents an emission rate for heavy construction activities.

- a. Reclaim Tailing Pond T1 - Earthmoving, regrading, and replanting activities will occur to develop final grades, surface water drainage patterns, and final use compatibility with the Reclamation Plan.

Emission Factors and Source: AP-42, Section 11.2.4

TSP-EF = 1.2 short tons/acre/month.

Process Rate: 24 months for 82 acres or approximately 3.4 acres/month

Duration: 24 months (Operation Years 6-7)

Control Method and Efficiency: Watering of disturbed area, if necessary

Example Calculation:

Process Rate x Emission Factor x Duration = Emission Rate

TSP = 3.4 acres/month x 1.2 st/acre/month x 12 months/yr = 49.0 st/yr

- b. Reclaim Tailing Pond T2 (partial)

Process Rate: 12 months for 54 acres or approximately 4.5 acres/month

Duration: 12 months (Operation Year 14)

Example Calculation:

TSP = 4.5 acres/month x 1.2 st/acre/month x 12 months/yr = 64.8 st/yr

- c. Reclaim Tailing Pond T3

Process Rate: 24 months for 100 acres or approximately 4.2
acres/month

Duration: 24 months (Operation Years 20-21)

Example Calculation:

$$\text{TSP} = 4.2 \text{ acres/month} \times 1.2 \text{ st/acre/month} \times 12 \text{ months/yr} = 60.5 \text{ st/yr}$$

d. Reclaim Tailing Pond T2 (remainder)

Process Rate: 18 months for 54 acres or approximately 3.0
acres/month.

Duration: 18 months (Closure (Reclamation) Years 1-2)

Example Calculation:

$$\text{TSP} = 3.0 \text{ acres/month} \times 1.2 \text{ st/acre/month} \times 12 \text{ months/yr} = 43.2 \text{ st/yr}$$

e. Reclaim Mine/Mill Site

Process Rate: 36 months for 104 acres or approximately 2.9
acres/month

Duration: 36 months (Closure (Reclamation) Years 1-4)

Example Calculation:

$$\text{TSP} = 2.9 \text{ acres/month} \times 1.2 \text{ st/acre/month} \times 12 \text{ months/yr} = 41.8 \text{ st/yr}$$

f. Reclaim Tailing Pond T4

Process Rate: 36 months for 99 acres or approximately 2.8
acres/month.

Duration: 36 months (Closure (Reclamation) Years 5-7)

Example Calculation:

$$\text{TSP} = 2.8 \text{ acres/month} \times 1.2 \text{ st/acre/month} \times 12 \text{ months/yr} = 40.3 \text{ st/yr}$$

g. Reclaim Ponds R1 and R2

Process Rate: 36 months for 75 acres or approximately 2.1 acres/month

Duration: 36 months (Closure (Reclamation) Years 3-5)

Example Calculation:

$$\text{TSP} = 2.1 \text{ acres/month} \times 1.2 \text{ st/acre/month} \times 12 \text{ months/yr} = 30.2 \text{ st/yr}$$

h. Reclaim Railroad Spur

Process Rate: 24 months for 40 acres or approximately 1.7 acres/month

Duration: 24 months (Closure Years 5-6)

Example Calculation:

$$\text{TSP} = 1.7 \text{ acres/month} \times 1.2 \text{ st/acre/month} \times 12 \text{ months/yr} = 24.5 \text{ st/yr}$$

i. Reclaim Access Road

Process Rate: 24 months for 35 acres or approximately 1.5 acres/month.

Duration: 24 months (Closure Years 6-7)

Example Calculation:

$$\text{TSP} = 1.5 \text{ acres/month} \times 1.2 \text{ st/acre/month} \times 12 \text{ months/yr} = 21.6 \text{ st/yr}$$

j. Reclamation Activities Tailpipe Emissions

Diesel Vehicles - Assumes all excavation and scraper equipment will use diesel fuel. Therefore, estimated miles for reclamation activities are for heavy duty diesel vehicles (HDDV).

Emission Factor and Source: AP-42, Appendix D, Tables D.5-1 and D.5-4 (HDDV-1990).

HDDV	(g/mi)
TSP-EF =	1.3
SO _x -EF =	2.8
NO _x -EF =	18.1
CO -FE =	28.1
HC -FE =	4.6

Process Rate: 34,434 miles over two years for reclamation of each pond.

Duration: Two years of reclamation filling, grading and cap development for each pond.

Control Method and Efficiency: As per EPA vehicle emission controls.

Example Calculation:

Process Rate x Emission Factor = Emission Rate.

$$\text{TSP} = 34,434 \text{ mi/2 yr} \times 1.3 \text{ g/mi} \times \text{t}/10^6 \text{g} \times \text{st}/1.1 \text{ t} = 0.02 \text{ st/yr}$$

Total Estimated Emissions for Diesel Vehicle Tailpipe Emissions

	<u>st/yr</u>
TSP:	0.02
SO _x :	0.04
NO _x :	0.28
CO :	0.45
HC :	0.07

Gasoline Vehicles - Assumes all of this activity occurs each year of pond reclamation.

Emission Factor and Source: AP-42, Appendix D, Tables D.2-10 and D.2-16 (LDGV-1990); Tables D.4-10 and D.4-15 (HDGV-1990).

<u>LDGV</u>	<u>(g/mi)</u>
TSP-EF =	0.05
SO _x -EF =	0.18
NO _x -EF =	2.3
CO -EF =	9.8
HC -EF =	1.0

Process Rate: LDGV - 49,322 miles per year

Duration: Mainly during second year of reclamation of each pond.

Control Method and Efficiency: As per EPA vehicle emission controls.

Example Calculation:

Process Rate x Emission Factor = Emission Rate

$$\text{TSp} = 49322 \text{ mi/yr} \times 0.05 \text{ g/mi} \times t/10^6 \times \text{st}/1.1 \text{ t} = 0.002 \text{ st/yr}$$

Total Estimated Emissions for Gasoline Vehicles Tailpipe Emissions

	<u>st/yr</u>
TSP:	0.002
SO _x :	0.008
NO _x :	0.103
CO :	0.439
HC :	0.045

APPENDIX B

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- _____. 1983. Compilation of Air Pollutant Emission Factors, Third Edition (including Supplements 1-7). AP-42. Supplements 8-14. May. Volumes I and II, Sections 1 through 7, Appendices A, B, C, D, and E. Office of Air Quality Planning and Standards. United States Environmental Protection Agency. Research Triangle Park, North Carolina.
- Kulibert, G. 1984. Personal Communication. Exxon Minerals Company Letter dated November 9, 1984. Exxon Minerals Company. Rhinelander, WI.
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- PEDCo - Environmental Specialists, Inc. 1976. Evaluation of Fugitive Dust Emissions from Mining. Task 1 Report. Identification of Fugitive Dust Sources Associated with Mining. Cincinnati, Ohi.

APPENDIX C

ISC MODEL INPUT AND OUTPUT

TABLE C-1. ISC MODEL INPUTS - ANNUAL EMISSION RATES

ISC91 (VERSION 90336)
 AN AIR QUALITY DISPERSION MODEL IN
 SECTION 3. MODELS PROPOSED SEP80 FOR 91 GUIDELINES.
 IN UNAMAP (VERSION 4) DEC 90
 SOURCE: FILE 16 ON UNAMAP MAGNETIC TAPE FROM NTIS.

*** FILE: ISCFINAA-CRAMDON TSP WITH ANNUAL EMISSION RATES ***

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CALCULATE (CONCENTRATION=1, DEPOSITION=2)
RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4)
DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1, POLAR=2)
INTERAIN ELEVATION SYSTEM (YES=1, NO=0)
CALCULATIONS ARE WRITTEN TO TAPE (YES=1, NO=0)
LIST ALL INPUT DATA (NO=0, YES=1, MET DATA ALSO=2)

COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)
WITH THE FOLLOWING TIME PERIODS:
1-HOUR (YES=1, NO=0)
2-HOUR (YES=1, NO=0)
3-HOUR (YES=1, NO=0)
4-HOUR (YES=1, NO=0)
5-HOUR (YES=1, NO=0)
8-HOUR (YES=1, NO=0)
12-HOUR (YES=1, NO=0)
24-HOUR (YES=1, NO=0)
PRINT N-DAY TABLES (YES=1, NO=0)

PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE
SPECIFIED BY ISM(7) THROUGH ISM(14):
DAILY TABLES (YES=1, NO=0)
HIGHEST 8 SECOND HIGHEST TABLES (YES=1, NO=0)
MAXIMUM 50 TABLES (YES=1, NO=0)
METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1, CARD=2)
GENERAL PROGRAM OPTION (URRAN MODE=1, USER ENTERS=2, 3)
WIND PROFILE EXPONENT VALUES (DEFAULT=1, USER ENTERS=2, 3)
VERTICAL DISPERSION RATES FOR ALL SOURCES (NO=0, YES=1)
SCALE EMISSION RATES FOR ALL SOURCES ONLY (YES=1, NO=0)
PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2, NO=1)

NUMBER OF SOURCE GROUPS (0, ALL SOURCES)
TIME PERIOD INTERVAL TO BE PRINTED (0, ALL INTERVALS)
NUMBER OF X (RANGE) GRID VALUES
NUMBER OF Y (THETA) GRID VALUES
SOURCE EMISSION RATE UNITS CONVERSION FACTOR
ENTRainment COEFFICIENT FOR STABLE ATMOSPHERE
HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED
LOGICAL DEPLETION NUMBER OF METEOROLOGICAL DATA
DEPLETION COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION
SURFACE AREA NO.
YEAR OF UPPER AIR DATA
ALLOTTED DATA STORAGE FOR THIS PROBLEM RUN
  
```

```

ISM(1) = 1
ISM(2) = 1
ISM(3) = 1
ISM(4) = 1
ISM(5) = 0
ISM(6) = 2
ISM(7) = 0
ISM(8) = 0
ISM(9) = 0
ISM(10) = 0
ISM(11) = 0
ISM(12) = 0
ISM(13) = 0
ISM(14) = 1
ISM(15) = 1
ISM(16) = 0
ISM(17) = 1
ISM(18) = 1
ISM(19) = 1
ISM(20) = 0
ISM(21) = 1
ISM(22) = 1
ISM(23) = 1
ISM(24) = 1
ISM(25) = 1
NSOURCE = 32
NGROUP = 11
IPERD = 0
NXPNTS = 0
NXPNTS = 0
NXWYD1 = 123
NXWYD2 = 10000E 07
BETA1 = 0.600
BETA2 = 0.600
ZRR = 10.00 METERS
IMET = 1
DFCAY = 0
ISSY = 14991
IUSY = 77
IUY = 14926
LIMIT = 43500 WORDS
  
```


SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 12 ***
MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** SOURCE NUMBER = 13 ***
MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** SOURCE NUMBER = 14 ***
MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 15 ***
MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,

SURFACE REFLECTION COEFFICIENT =
0.87000,0.71000,0.63000,
*** SOURCE NUMBER = 16 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000,0.71000,0.63000,
*** SOURCE NUMBER = 17 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000,0.71000,0.63000,

*** FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 18 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000,0.71000,0.63000,
*** SOURCE NUMBER = 19 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000,0.71000,0.63000,
*** SOURCE NUMBER = 20 ***
MASS FRACTION =
0.12700,0.32100,0.55200,

SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 21 ***
MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** SOURCE NUMBER = 22 ***
MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** SOURCE NUMBER = 23 ***
MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 24 ***
MASS FRACTION =

*** SOURCE NUMBER = 29 ***
 MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY(METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.63000,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 30 ***
 MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY(METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.63000,

*** SOURCE NUMBER = 31 ***
 MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY(METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.63000,

*** SOURCE NUMBER = 32 ***
 MASS FRACTION =
 0.03800, 0.098500, 0.14800, 0.16800, 0.08400, 0.07300, 0.08100, 0.07700, 0.06700, 0.07300,
 0.07200, 0.02000, 0.01000,
 SETTLING VELOCITY(METERS/SEC) =
 0.0030, 0.0200, 0.0480, 0.0960, 0.1550, 0.2300, 0.3220, 0.4300, 0.5500, 0.6900,
 0.8300, 1.0100, 1.2300,
 SURFACE REFLECTION COEFFICIENT =
 1.00000, 0.71000, 0.63000, 0.51000, 0.36000, 0.17000, 0.0 , 0.0 , 0.0 , 0.0 ,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

* SOURCE-RECEPTOR COMBINATIONS LESS THAN 100 METERS OR THREE BUILDING HEIGHTS IN DISTANCE. NO AVERAGE CONCENTRATION IS CALCULATED *

SOURCE NUMBER	RECEPTOR LOCATION RANGE (METERS) OR DIRECTION (DEGREES)	DISTANCE BETWEEN (METERS)
18	693840.0 36950.0	68.88

TABLE C-2. ISC MODEL OUTPUT - ANNUAL EMISSION RATES

*** *FILE:ISCFINAA-CPANDON TSP WITH ANNUAL EMISSION RATES* ***

* 365-DAY AVERAGE CONCENTRATION MICROGRAMS/CUBIC METER *

* FROM SOURCES:
 1, -32,
 * FOR THE DISCRETE RECEPTOR POINTS *

X	Y	CON.	X	Y	CON.	X	Y	CON.	X	Y	CON.
691000.0	390000.0	0.29486	691000.0	385000.0	0.30559	691000.0	375000.0	0.34749	691000.0	375000.0	0.34749
691500.0	390000.0	0.37513	691500.0	380000.0	0.42670	692000.0	395000.0	0.30153	692000.0	395000.0	0.30153
692000.0	390000.0	0.43292	692000.0	355000.0	0.41884	692000.0	345000.0	0.53419	692000.0	345000.0	0.53419
692500.0	390000.0	0.51292	692500.0	390000.0	0.44455	692500.0	380000.0	0.50493	692500.0	380000.0	0.50493
693000.0	390000.0	0.58064	693000.0	390000.0	0.47101	693000.0	380000.0	0.57608	693000.0	380000.0	0.57608
693500.0	390000.0	0.82771	693500.0	363000.0	1.22489	693500.0	351200.0	1.16347	693500.0	351200.0	1.16347
694000.0	390000.0	0.85231	694000.0	335000.0	1.00028	694000.0	349500.0	1.35347	694000.0	349500.0	1.35347
694500.0	390000.0	0.85985	694500.0	375200.0	1.04913	694500.0	390000.0	1.54325	694500.0	390000.0	1.54325
695000.0	390000.0	1.56536	695000.0	375200.0	0.80568	695000.0	369400.0	1.38672	695000.0	369400.0	1.38672
695500.0	390000.0	1.89100	695500.0	381500.0	0.97775	695500.0	395000.0	1.78747	695500.0	395000.0	1.78747
696000.0	390000.0	0.37721	696000.0	395000.0	0.22147	696000.0	395000.0	0.69507	696000.0	395000.0	0.69507
696500.0	390000.0	0.83351	696500.0	335000.0	1.27818	696500.0	395000.0	1.70507	696500.0	395000.0	1.70507
697000.0	390000.0	0.67719	697000.0	370000.0	0.39371	697000.0	385000.0	0.69823	697000.0	385000.0	0.69823
697500.0	390000.0	1.07753	697500.0	370000.0	1.79843	697500.0	385000.0	1.56252	697500.0	385000.0	1.56252
698000.0	390000.0	1.56953	698000.0	370000.0	0.95516	698000.0	385000.0	0.42589	698000.0	385000.0	0.42589
698500.0	390000.0	0.73738	698500.0	337400.0	0.27056	698500.0	395000.0	0.22774	698500.0	395000.0	0.22774
699000.0	390000.0	1.07238	699000.0	320000.0	1.74781	699000.0	395000.0	0.29174	699000.0	395000.0	0.29174
699500.0	390000.0	0.55519	699500.0	327600.0	0.42377	699500.0	395000.0	0.35595	699500.0	395000.0	0.35595
700000.0	390000.0	0.25169	700000.0	395000.0	0.36478	700000.0	395000.0	0.53284	700000.0	395000.0	0.53284
700500.0	390000.0	1.15285	700500.0	370000.0	1.84210	700500.0	395000.0	1.75397	700500.0	395000.0	1.75397
701000.0	390000.0	0.31122	701000.0	375000.0	1.05653	701000.0	395000.0	0.32459	701000.0	395000.0	0.32459
701500.0	390000.0	0.51355	701500.0	315000.0	0.21509	701500.0	395000.0	0.32666	701500.0	395000.0	0.32666
702000.0	390000.0	1.82287	702000.0	375200.0	1.04434	702000.0	395000.0	0.47091	702000.0	395000.0	0.47091
702500.0	390000.0	0.52937	702500.0	375200.0	3.81989	702500.0	395000.0	0.21845	702500.0	395000.0	0.21845
703000.0	390000.0	0.55434	703000.0	370000.0	1.02827	703000.0	395000.0	0.14574	703000.0	395000.0	0.14574
703500.0	390000.0	2.89971	703500.0	370000.0	2.68105	703500.0	395000.0	0.33192	703500.0	395000.0	0.33192
704000.0	390000.0	0.79569	704000.0	330200.0	0.42295	704000.0	395000.0	0.06078	704000.0	395000.0	0.06078
704500.0	390000.0	0.27982	704500.0	395000.0	0.31773	704500.0	395000.0	0.90870	704500.0	395000.0	0.90870
705000.0	390000.0	1.64350	705000.0	370000.0	1.27949	705000.0	395000.0	0.46369	705000.0	395000.0	0.46369
705500.0	390000.0	0.36865	705500.0	355200.0	0.63035	705500.0	395000.0	0.21470	705500.0	395000.0	0.21470
706000.0	390000.0	0.74947	706000.0	325000.0	0.29081	706000.0	395000.0	0.47587	706000.0	395000.0	0.47587
706500.0	390000.0	0.59072	706500.0	365000.0	0.31592	706500.0	395000.0	0.28651	706500.0	395000.0	0.28651

MAX 50
24-HR
SGROUP# 11

TABLE C-3. ISC MODEL OUTPUT - ANNUAL EMISSION RATES 50 MAXIMUM (MAX) CONCENTRATIONS

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

* 50 MAXIMUM 24-HOUR AVERAGE CONCENTRATION MICROGRAMS/CUBIC METER *

* FROM SOURCES: 1, -32*

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y (METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y (METERS) OR DIRECTION (DEGREES)
1	101.20410	1	248	694420.0	35160.0	26	19.52008	1	177	694860.0	35020.0
2	43.10016	1	300	694420.0	35160.0	27	19.07994	1	118	694420.0	35250.0
3	40.31325	1	275	694420.0	35160.0	28	19.07159	1	140	696960.0	35820.0
4	38.20253	1	129	694420.0	35160.0	29	18.46288	1	46	694860.0	35020.0
5	37.45081	1	176	694420.0	35160.0	30	18.40520	1	236	694420.0	35160.0
6	35.15314	1	130	694420.0	35160.0	31	18.34418	1	158	693350.0	36120.0
7	32.51351	1	214	694420.0	35160.0	32	17.91166	1	163	694000.0	34860.0
8	29.54734	1	256	694420.0	35160.0	33	17.91298	1	45	694420.0	35160.0
9	27.53768	1	306	694860.0	35020.0	34	17.89298	1	297	693350.0	35160.0
10	26.34236	1	316	694420.0	35160.0	35	17.80532	1	267	693350.0	35160.0
11	26.34088	1	176	694860.0	35020.0	36	17.30624	1	311	693020.0	36120.0
12	25.33609	1	115	694860.0	35020.0	37	17.20624	1	220	694420.0	35160.0
13	25.33609	1	115	694860.0	35020.0	38	17.11934	1	276	696960.0	35820.0
14	25.33609	1	115	694860.0	35020.0	39	16.98863	1	322	694420.0	35160.0
15	22.15131	1	196	694420.0	35160.0	40	16.92863	1	117	693350.0	36120.0
16	22.15131	1	196	694420.0	35160.0	41	16.81425	1	266	694860.0	35020.0
17	22.15131	1	196	694420.0	35160.0	42	16.81425	1	267	694860.0	35020.0
18	21.25767	1	119	694860.0	35020.0	43	16.68065	1	175	694420.0	35160.0
19	21.25767	1	119	694860.0	35020.0	44	16.44473	1	225	694420.0	35160.0
20	21.25767	1	119	694860.0	35020.0	45	16.42267	1	248	694860.0	35160.0
21	21.25767	1	57	694420.0	35160.0	46	16.41533	1	118	694000.0	34860.0
22	21.25767	1	364	694420.0	35160.0	47	16.32750	1	206	694420.0	35160.0
23	21.25767	1	364	694420.0	35160.0	48	16.29143	1	228	694420.0	35160.0
24	19.75574	1	319	694420.0	35160.0	49	16.25572	1	231	694420.0	35160.0
25	19.75574	1	319	694420.0	35160.0	50	16.22362	1	279	694000.0	34860.0

TABLE C-4. ISC - CALMPRO MODEL INPUTS - ANNUAL EMISSION RATES
 ISCSI (VERSION 80339)
 AN AIR QUALITY DISPERSION MODEL IN
 SECTION 3.0 MODELS PROPOSED SEP80 FOR 81 GUIDELINES.
 IN UNAMAP (VERSION 4) DISMAP
 SOURCE: FILE 16 ON UNAMAP MAGNETIC TAPE FROM NTIS.

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*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***
CALCULATE (CONCENTRATION=1,DEPOSITION=2)
RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4)
DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1,POLAR=2)
TERRAIN ELEVATIONS ARE READ (YES=1,NO=0)
CALCULATIONS ARE WRITTEN TO TAPE (YES=1,NO=0)
LIST ALL INPUT DATA (NO=0,YES=1,MET DATA ALSO=2)

COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)
WITH THE FOLLOWING TIME PERIODS:
1-HOUR (YES=1,NO=0)
2-HOUR (YES=1,NO=0)
3-HOUR (YES=1,NO=0)
4-HOUR (YES=1,NO=0)
8-HOUR (YES=1,NO=0)
12-HOUR (YES=1,NO=0)
24-HOUR (YES=1,NO=0)
PRINT *N*-DAY TABLE(S) (YES=1,NO=0)

PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE
SPECIFIED BY ISM(7) THROUGH ISM(14):
DAILY TABLES (YES=1,NO=0)
HIGHEST & SECOND HIGHEST TABLES (YES=1,NO=0)
MAXIMUM 50 TABLES (YES=1,NO=0)
METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1,CARD=2)
RURAL-URBAN OPTION (RURAL=3,URBAN MODE=1,URBAN MODE=2)
WIND PROFILE EXPONENT VALUES (DEFAULT=1,USER ENTERS=2,3)
VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULT=1,USER ENTERS=2,3)
SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES=1)
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2)
PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2,NO=1)

NUMBER OF INPUT SOURCES (=0 ALL SOURCES)
NUMBER OF SOURCE GROUPS (=0 ALL SOURCES)
TIME PERIOD INTERVAL TO BE PRINTED (=0, ALL INTERVALS)
NUMBER OF X (RANGE) GRID VALUES
NUMBER OF Y (RANGE) GRID VALUES
SOURCE EMISSION RATE UNITS
SOURCE EMISSION RATE UNITS CONVERSION FACTOR
ENTRainment COEFFICIENT FOR UNSTABLE ATMOSPHERE
ENTRainment COEFFICIENT FOR STABLE ATMOSPHERE
HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED
LOGICAL COEFFICIENT FOR METEOROLOGICAL DATA
DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION
SURFACE STATION NO.
YEAR OF SURFACE DATA
YEAR OF UPPER AIR DATA
YEAR OF UPPER AIR DATA
ALLOTTED DATA STORAGE FOR THIS PROBLEM RUN
REQUIRED DATA STORAGE FOR THIS PROBLEM RUN

ISM(1) = 1
ISM(2) = 1
ISM(3) = 1
ISM(4) = 0
ISM(5) = 0
ISM(6) = 2

ISM(7) = 0
ISM(8) = 0
ISM(9) = 0
ISM(10) = 0
ISM(11) = 0
ISM(12) = 0
ISM(13) = 0
ISM(14) = 1
ISM(15) = 1

ISM(16) = 0
ISM(17) = 1
ISM(18) = 1
ISM(19) = 1
ISM(20) = 0
ISM(21) = 1
ISM(22) = 1
ISM(23) = 0
ISM(24) = 1
ISM(25) = 1

NSOURC = 32
NPGROUP = 11
IPERD = 0
NXPNTS = 0
NXPNTS = 0
NXPNTS = 0
NXPNTS = 120000E 07
RETAL = 0.600
BETA2 = 0.600
ZRR = 10.00 METERS
IMET = 0.0
DECAY = 0
ISSY = 14991
ISSY = 177
ISSY = 14926
ISSY = 77
ISSY = 43500 WORDS
LIMIT = 17701 WORDS
  
```


SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 12 ***

MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,

SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** SOURCE NUMBER = 13 ***

MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,

SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** SOURCE NUMBER = 14 ***

MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,

SURFACE REFLECTION COEFFICIENT =
0.87000, 0.71000, 0.63000,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 15 ***

MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,

SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,
*** SOURCE NUMBER = 16 ***
MASS FRACTION =
0.1270,0.3210,0.5520,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,
*** SOURCE NUMBER = 17 ***
MASS FRACTION =
0.1270,0.3210,0.5520,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,

*** FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 18 ***
MASS FRACTION =
0.1270,0.3210,0.5520,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,
*** SOURCE NUMBER = 19 ***
MASS FRACTION =
0.1270,0.3210,0.5520,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,
*** SOURCE NUMBER = 20 ***
MASS FRACTION =
0.1270,0.3210,0.5520,

SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 21 ***
MASS FRACTION =
0.1270,0.3210,0.5520,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,

*** SOURCE NUMBER = 22 ***
MASS FRACTION =
0.1270,0.3210,0.5520,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,

*** SOURCE NUMBER = 23 ***
MASS FRACTION =
0.1270,0.3210,0.5520,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 24 ***
MASS FRACTION =

0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000,0.71000,0.63000,
*** SOURCE NUMBER = 25 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000,0.71000,0.63000,
*** SOURCE NUMBER = 26 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000,0.71000,0.63000,

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 27 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000,0.71000,0.63000,
*** SOURCE NUMBER = 28 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.87000,0.71000,0.63000,

TABLE C-4 (CONTINUED)
 FIVE HIGHEST 24-HOUR PART CONCENTRATIONS (ENDING ON JULIAN DAY, HOUR)
 (MICROGRAMS/M**3)

RECEPTOR	1	2	3	A	F
110	0.0000	0.0000	0.0000	0.0000	0.0000
120	0.0000	0.0000	0.0000	0.0000	0.0000
400	0.0000	0.0000	0.0000	0.0000	0.0000
500	0.0000	0.0000	0.0000	0.0000	0.0000
700	0.0000	0.0000	0.0000	0.0000	0.0000
800	0.0000	0.0000	0.0000	0.0000	0.0000
900	0.0000	0.0000	0.0000	0.0000	0.0000
1000	0.0000	0.0000	0.0000	0.0000	0.0000
1100	0.0000	0.0000	0.0000	0.0000	0.0000
1200	0.0000	0.0000	0.0000	0.0000	0.0000
1300	0.0000	0.0000	0.0000	0.0000	0.0000
1400	0.0000	0.0000	0.0000	0.0000	0.0000
1500	0.0000	0.0000	0.0000	0.0000	0.0000
1600	0.0000	0.0000	0.0000	0.0000	0.0000
1700	0.0000	0.0000	0.0000	0.0000	0.0000
1800	0.0000	0.0000	0.0000	0.0000	0.0000
1900	0.0000	0.0000	0.0000	0.0000	0.0000
2000	0.0000	0.0000	0.0000	0.0000	0.0000
2100	0.0000	0.0000	0.0000	0.0000	0.0000
2200	0.0000	0.0000	0.0000	0.0000	0.0000
2300	0.0000	0.0000	0.0000	0.0000	0.0000
2400	0.0000	0.0000	0.0000	0.0000	0.0000
2500	0.0000	0.0000	0.0000	0.0000	0.0000
2600	0.0000	0.0000	0.0000	0.0000	0.0000
2700	0.0000	0.0000	0.0000	0.0000	0.0000
2800	0.0000	0.0000	0.0000	0.0000	0.0000
2900	0.0000	0.0000	0.0000	0.0000	0.0000
3000	0.0000	0.0000	0.0000	0.0000	0.0000
3100	0.0000	0.0000	0.0000	0.0000	0.0000
3200	0.0000	0.0000	0.0000	0.0000	0.0000
3300	0.0000	0.0000	0.0000	0.0000	0.0000
3400	0.0000	0.0000	0.0000	0.0000	0.0000
3500	0.0000	0.0000	0.0000	0.0000	0.0000
3600	0.0000	0.0000	0.0000	0.0000	0.0000
3700	0.0000	0.0000	0.0000	0.0000	0.0000
3800	0.0000	0.0000	0.0000	0.0000	0.0000
3900	0.0000	0.0000	0.0000	0.0000	0.0000
4000	0.0000	0.0000	0.0000	0.0000	0.0000
4100	0.0000	0.0000	0.0000	0.0000	0.0000
4200	0.0000	0.0000	0.0000	0.0000	0.0000
4300	0.0000	0.0000	0.0000	0.0000	0.0000
4400	0.0000	0.0000	0.0000	0.0000	0.0000
4500	0.0000	0.0000	0.0000	0.0000	0.0000
4600	0.0000	0.0000	0.0000	0.0000	0.0000
4700	0.0000	0.0000	0.0000	0.0000	0.0000
4800	0.0000	0.0000	0.0000	0.0000	0.0000
4900	0.0000	0.0000	0.0000	0.0000	0.0000
5000	0.0000	0.0000	0.0000	0.0000	0.0000
5100	0.0000	0.0000	0.0000	0.0000	0.0000
5200	0.0000	0.0000	0.0000	0.0000	0.0000
5300	0.0000	0.0000	0.0000	0.0000	0.0000
5400	0.0000	0.0000	0.0000	0.0000	0.0000
5500	0.0000	0.0000	0.0000	0.0000	0.0000
5600	0.0000	0.0000	0.0000	0.0000	0.0000
5700	0.0000	0.0000	0.0000	0.0000	0.0000
5800	0.0000	0.0000	0.0000	0.0000	0.0000
5900	0.0000	0.0000	0.0000	0.0000	0.0000
6000	0.0000	0.0000	0.0000	0.0000	0.0000

TABLE C-4 (CONTINUED)

118	0.00	0.03	0.01C (256.24)	0.00C (300.24)	0.00C (275.24)	0.00	(0.00)	0.00	(0.00)
119	0.00	0.00	0.00C (256.24)	0.00C (300.24)	0.00C (275.24)	0.00	(0.00)	0.00	(0.00)
120	0.00	0.00	0.00C (256.24)	0.00C (300.24)	0.00C (275.24)	0.00	(0.00)	0.00	(0.00)
121	0.00	0.00	2.48C (275.24)	0.00C (300.24)	0.00C (255.24)	0.00	(0.00)	0.00	(0.00)
122	0.00	0.00	7.78C (275.24)	0.00C (300.24)	0.00C (255.24)	0.00	(0.00)	0.00	(0.00)
123	0.00	0.00	11.52C (275.24)	0.00C (300.24)	0.00C (256.24)	0.00C (248.24)	(0.00)	0.00	(0.00)

TABLE C-5. EAU CLAIRE, WISCONSIN METEOROLOGICAL DATA-CALM PERIODS

DAY	H	CALM*	P1	P2	P3	P4	P5	P6	P7	P8
1	1	1	1	1	1	1	1	1	1	1
2	1	1	1	1	1	1	1	1	1	1
3	1	1	1	1	1	1	1	1	1	1
4	1	1	1	1	1	1	1	1	1	1
5	1	1	1	1	1	1	1	1	1	1
6	1	1	1	1	1	1	1	1	1	1
7	1	1	1	1	1	1	1	1	1	1
8	1	1	1	1	1	1	1	1	1	1
9	1	1	1	1	1	1	1	1	1	1
10	1	1	1	1	1	1	1	1	1	1
11	1	1	1	1	1	1	1	1	1	1
12	1	1	1	1	1	1	1	1	1	1
13	1	1	1	1	1	1	1	1	1	1
14	1	1	1	1	1	1	1	1	1	1
15	1	1	1	1	1	1	1	1	1	1
16	1	1	1	1	1	1	1	1	1	1
17	1	1	1	1	1	1	1	1	1	1
18	1	1	1	1	1	1	1	1	1	1
19	1	1	1	1	1	1	1	1	1	1
20	1	1	1	1	1	1	1	1	1	1
21	1	1	1	1	1	1	1	1	1	1
22	1	1	1	1	1	1	1	1	1	1
23	1	1	1	1	1	1	1	1	1	1
24	1	1	1	1	1	1	1	1	1	1
25	1	1	1	1	1	1	1	1	1	1
26	1	1	1	1	1	1	1	1	1	1
27	1	1	1	1	1	1	1	1	1	1
28	1	1	1	1	1	1	1	1	1	1
29	1	1	1	1	1	1	1	1	1	1
30	1	1	1	1	1	1	1	1	1	1
31	1	1	1	1	1	1	1	1	1	1

TABLE C-5 (CONTINUED)

354	12	1	3	0	0	2	3	1																	
355	1	0	0	0	0	0	0	0																	
	TOTAL	NUMBER OF CALM HOURS																							
									1243																
	NUMBER OF 3-HR PERIODS WITH																								
	1	5	CALM HRS																						
	251	184	208																						
	NUMBER OF 24-HR PERIODS WITH																								
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	CALM HRS
	43	34	25	21	28	17	13	15	16	8	9	3	2	2	0	1	0	0	0	0	0	0	0	1	0

123 STATIONS WILL BE PROCESSED IN THIS RUN OF CALMPRO.

TABLE C-6. CALMPRO ADJUSTMENT - TSP ANNUAL AVERAGE CONCENTRATIONS - ANNUAL EMISSION RATES

RECEPTOR	RECEPTOR IDENTIFICATION	EAST COORD (USER UNITS)	NORTH COORD (USER UNITS)	ABV LOCAL GRD LVL (METERS)	RECEPTOR HT. LOCAL GRD LVL (METERS)	RECEPTOR GROUND LEVEL ELEVATION (USER MT UNITS)	DAY	AVG CONC FOR PERIOD 1-HR 1. TO DAY155-HR24. (MICROGRAMS/M**3)
1		0.00	0.00	0.00	0.00	0.00		0.00
2		0.00	0.00	0.00	0.00	0.00		0.00
3		0.00	0.00	0.00	0.00	0.00		0.00
4		0.00	0.00	0.00	0.00	0.00		0.00
5		0.00	0.00	0.00	0.00	0.00		0.00
6		0.00	0.00	0.00	0.00	0.00		0.00
7		0.00	0.00	0.00	0.00	0.00		0.00
8		0.00	0.00	0.00	0.00	0.00		0.00
9		0.00	0.00	0.00	0.00	0.00		0.00
10		0.00	0.00	0.00	0.00	0.00		0.00
11		0.00	0.00	0.00	0.00	0.00		0.00
12		0.00	0.00	0.00	0.00	0.00		0.00
13		0.00	0.00	0.00	0.00	0.00		0.00
14		0.00	0.00	0.00	0.00	0.00		0.00
15		0.00	0.00	0.00	0.00	0.00		0.00
16		0.00	0.00	0.00	0.00	0.00		0.00
17		0.00	0.00	0.00	0.00	0.00		0.00
18		0.00	0.00	0.00	0.00	0.00		0.00
19		0.00	0.00	0.00	0.00	0.00		0.00
20		0.00	0.00	0.00	0.00	0.00		0.00
21		0.00	0.00	0.00	0.00	0.00		0.00
22		0.00	0.00	0.00	0.00	0.00		0.00
23		0.00	0.00	0.00	0.00	0.00		0.00
24		0.00	0.00	0.00	0.00	0.00		0.00
25		0.00	0.00	0.00	0.00	0.00		0.00
26		0.00	0.00	0.00	0.00	0.00		0.00
27		0.00	0.00	0.00	0.00	0.00		0.00
28		0.00	0.00	0.00	0.00	0.00		0.00
29		0.00	0.00	0.00	0.00	0.00		0.00
30		0.00	0.00	0.00	0.00	0.00		0.00
31		0.00	0.00	0.00	0.00	0.00		0.00
32		0.00	0.00	0.00	0.00	0.00		0.00
33		0.00	0.00	0.00	0.00	0.00		0.00
34		0.00	0.00	0.00	0.00	0.00		0.00
35		0.00	0.00	0.00	0.00	0.00		0.00
36		0.00	0.00	0.00	0.00	0.00		0.00
37		0.00	0.00	0.00	0.00	0.00		0.00
38		0.00	0.00	0.00	0.00	0.00		0.00
39		0.00	0.00	0.00	0.00	0.00		0.00
40		0.00	0.00	0.00	0.00	0.00		0.00

TABLE C-6 (CONTINUED)

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005555110005551100000000
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111111111111111111111111

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122110111111111111111111
104104104104104104104104
122110111111111111111111

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TABLE C-7. ISC MODEL INPUTS - 24-HOUR EMISSION RATES
 IS3CCT (VERSION 80359)
 AN AIR QUALITY DISPERSION MODEL IN
 SECTION 4. MODELS PROPOSED SEP80 FOR 81 GUIDELINES.
 IN UNMAP. (VERSION 4) DISC 80
 SOURCE: FILE IS ON UNMAP MAGNETIC TAPE FROM NTIS.

*** *24HR EMISSION RATES-W/*4I 10 DAYS FROM ANNUAL 50 MAX.**

CALCULATE (CONCENTRATION=1, DEPOSITION=2)
 RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4)
 TERRAIN ELEVATIONS ARE READ (YES=1, NO=0)
 CALCULATIONS ARE WRITTEN TO TAPE (YES=1, NO=0)
 LIST ALL INPUT DATA (NO=0, YES=1, MET DATA ALSO=2)

COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)

WITH THE FOLLOWING TIME PERIODS:

- 1-HOUR (YES=1, NO=0)
- 2-HOUR (YES=1, NO=0)
- 3-HOUR (YES=1, NO=0)
- 4-HOUR (YES=1, NO=0)
- 6-HOUR (YES=1, NO=0)
- 8-HOUR (YES=1, NO=0)
- 12-HOUR (YES=1, NO=0)
- 24-HOUR (YES=1, NO=0)
- PRINT AN *DAY TABLE (S) (YES=1, NO=0)

PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE SPECIFIED BY ISW(7) THROUGH ISW(14):

- DAILY TABLES (YES=1, NO=0)
- HIGHEST & SECOND HIGHEST TABLES (YES=1, NO=0)
- MAXIMUM 50 TABLES (YES=1, NO=0)
- METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1, CARD=2)
- RURAL-URBAN OPTION (RURAL=0, URBAN=1, URBAN MODE=2)
- WIND PROFILE EXPONENT VALUES (DEFAULTS=1, USER ENTERS=2, 3)
- WIND LOGICAL POLYMERATES GRADIENT VALUES (DEFAULTS=1, USER ENTERS=2, 3)
- SCALE EMISSION RATES FOR ALL SOURCES (NO=0, YES=1)
- PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2, NO=1)

NUMBER OF INPUT SOURCES (=0 ALL SOURCES)
 NUMBER OF SOURCE GROUPS (=0 ALL INTERVALS)
 NUMBER OF PERIOD INTERVALS TO BE PRINTED (=0 ALL INTERVALS)
 NUMBER OF Y (OTHER) RECEPTORS
 NUMBER OF DISTRICT RECEPTORS
 SOURCE EMISSION RATE UNITS CONVERSION FACTOR
 ENTRANCEMENT COEFFICIENT FOR UNSTABLE ATMOSPHERE
 LOGICAL ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED
 LOGICAL UNIT NUMBER AT WHICH LOGICAL DATA
 DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPOSITION
 SURFACE STATION NO.
 YEAR AIR SURFACE DATA
 YEAR AIR UPPER AIR DATA
 LOGICAL UNIT OF CALCULATION *SAVE* TAPE
 LOGICAL UNIT OF STORAGE

ISW(1)	1
ISW(2)	1
ISW(3)	0
ISW(4)	1
ISW(5)	1
ISW(6)	2
ISW(7)	1
ISW(8)	0
ISW(9)	0
ISW(10)	0
ISW(11)	0
ISW(12)	0
ISW(13)	0
ISW(14)	0
ISW(15)	0
ISW(16)	0
ISW(17)	0
ISW(18)	0
ISW(19)	1
ISW(20)	0
ISW(21)	1
ISW(22)	1
ISW(23)	1
ISW(24)	1
ISW(25)	1
NSOURC	32
NGROUP	1
IPERD	0
NXPNTS	0
NXPNTS	0
NXPNTS	123
NXPNTS	10000E 07
BETA1	0.200
BETA2	0.600
IMETR	10.00
IMETR	1
DECAY	0.0
ISS	14991
ISY	77
IUS	14926
IUY	77
IUY	77
IYAP	12
LIMIT	43500
	WORDS

SURFACE REFLECTION COEFFICIENT =
0.97000, 0.71000, 0.63000,

*** *24HR EMISSION RATES-W/*HI 10 DAYS FROM ANNUAL 50 MAX.* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 12 ***

MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.97000, 0.71000, 0.63000,

*** SOURCE NUMBER = 13 ***

MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.97000, 0.71000, 0.63000,

*** SOURCE NUMBER = 14 ***

MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.97000, 0.71000, 0.63000,

*** *24HR EMISSION RATES-W/*HI 10 DAYS FROM ANNUAL 50 MAX.* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 15 ***

MASS FRACTION =
0.12700, 0.32100, 0.55200,
SETTLING VELOCITY(METERS/SEC) =

0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.8700, 0.7100, 0.5300,
 *** SOURCE NUMBER = 16 ***
 MASS FRACTION =
 0.1270, 0.3210, 0.5520,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.8700, 0.7100, 0.5300,
 *** SOURCE NUMBER = 17 ***
 MASS FRACTION =
 0.1270, 0.3210, 0.5520,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.8700, 0.7100, 0.5300,

*** 24HR EMISSION RATES-W/AHI 10 DAYS FROM ANNUAL 50 MAX. ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 18 ***
 MASS FRACTION =
 0.1270, 0.3210, 0.5520,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.8700, 0.7100, 0.5300,
 *** SOURCE NUMBER = 19 ***
 MASS FRACTION =
 0.1270, 0.3210, 0.5520,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.8700, 0.7100, 0.5300,
 *** SOURCE NUMBER = 20 ***
 MASS FRACTION =

0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,

*** *24HR EMISSION RATES-W/*HI 10 DAYS FROM ANNUAL 50 MAX.* **

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 21 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,

*** SOURCE NUMBER = 22 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,

*** SOURCE NUMBER = 23 ***
MASS FRACTION =
0.12700,0.32100,0.55200,
SETTLING VELOCITY(METERS/SEC) =
0.0030, 0.0200, 0.0480,
SURFACE REFLECTION COEFFICIENT =
0.8700,0.7100,0.6300,

*** *24HR EMISSION RATES-W/*HI 10 DAYS FROM ANNUAL 50 MAX.* **

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 24 ***

MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.53000,
 *** SOURCE NUMBER = 25 ***
 MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.53000,
 *** SOURCE NUMBER = 26 ***
 MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.53000,

*** *24HR EMISSION RATES-M/*HI 10 DAYS FROM ANNUAL 50 MAX.* ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 27 ***
 MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.53000,
 *** SOURCE NUMBER = 28 ***
 MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0200, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.53000,

*** SOURCE NUMBER = 29 ***
 MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0220, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.63000,

*** *24HR EMISSION RATES-W/*HI 10 DAYS FROM ANNUAL 50 MAX.* **

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 30 ***
 MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0220, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.63000,
 *** SOURCE NUMBER = 31 ***
 MASS FRACTION =
 0.12700, 0.32100, 0.55200,
 SETTLING VELOCITY (METERS/SEC) =
 0.0030, 0.0220, 0.0480,
 SURFACE REFLECTION COEFFICIENT =
 0.87000, 0.71000, 0.63000,

*** SOURCE NUMBER = 32 ***
 MASS FRACTION =
 0.03200, 0.08500, 0.14800, 0.16800, 0.08400, 0.07300, 0.08100, 0.07700, 0.06700, 0.07300,
 0.07200, 0.02800, 0.01000,
 SETTLING VELOCITY (METERS/SEC) =
 0.0300, 0.0230, 0.0480, 0.0960, 0.1550, 0.2300, 0.3220, 0.4300, 0.5500, 0.6900,
 0.8300, 1.0100, 1.2300,
 SURFACE REFLECTION COEFFICIENT =
 1.00000, 0.71000, 0.63000, 0.51000, 0.36000, 0.17000, 0.0 , 0.0 , 0.0 , 0.0 ,

*** *24HR EMISSION RATES-W/*HI 10 DAYS FROM ANNUAL 50 MAX.* **

* SOURCE-RECEPTOR COMBINATIONS LESS THAN 100 METERS OR THREE BUILDING HEIGHTS IN DISTANCE. NO AVERAGE CONCENTRATION IS CALCULATED *

TABLE C-8 (CONTINUED)

1190	0.00	1.040	0.330	130.24	0.210	176.24	0.010	214.24	0.000	256.24
1191	0.00	1.040	1.330	(214.24)	0.000	(46.24)	0.000	(130.24)	0.000	(129.24)
1200	0.00	1.040	0.770	(176.24)	0.000	(46.24)	0.000	(130.24)	0.000	(256.24)
1210	0.00	1.040	0.910	(176.24)	0.240	(129.24)	0.150	(176.24)	0.130	(275.24)
1220	0.00	1.040	0.550	(214.24)	0.600	(130.24)	0.440	(46.24)	0.440	(46.24)
1230	0.00	1.040	1.100	(214.24)	0.800	(130.24)	0.550	(256.24)	0.440	(46.24)

TABLE C-10. ISC-CALPRO MODEL OUTPUT - HIGHEST 5 DAYS NEXT TO 10 MAX

*** *FILE:ISCFINAA-CRANFON TSP WITH ANNUAL EMISSION RATES* ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION MICROGRAMS/CUBIC METER
* FROM SOURCES: 1, -32,
* FOR THE DISCRETE RECEPTOR POINTS *

	X	Y	CON.	(DAY,PER.)	X	Y	CON.	(DAY,PER.)
691000.0	3	9000.0	3.90028	(67, 1)	691000.0	385000.0	4.99101	(342, 1)
691000.0	4	94428	4.94428	(117, 1)	691500.0	395000.0	5.03723	(317, 1)
691300.0	6	13903	6.13903	(342, 1)	692000.0	380000.0	3.68045	(165, 1)
692000.0	4	00641	4.00641	(165, 1)	692000.0	355000.0	5.39876	(266, 1)
692000.0	7	51166	7.51166	(342, 1)	692000.0	395000.0	5.44452	(98, 1)
692000.0	6	57804	6.57804	(112, 1)	692500.0	390000.0	4.98966	(165, 1)
692000.0	5	05522	5.05522	(22, 1)	693000.0	380000.0	3.80254	(293, 1)
692000.0	5	15236	5.15236	(317, 1)	693000.0	380000.0	3.01356	(165, 1)
693000.0	4	12435	4.12435	(237, 1)	693000.0	365000.0	7.01338	(138, 1)
693000.0	7	63795	7.63795	(317, 1)	693020.0	357200.0	14.01438	(112, 1)
693020.0	17	30527	17.30527	(311, 1)	693000.0	349600.0	11.34248	(22, 1)
693050.0	21	08125	21.08125	(364, 1)	693000.0	335000.0	15.41970	(363, 1)
693050.0	11	24359	11.24359	(22, 1)	693000.0	38000.0	6.49951	(293, 1)
693050.0	4	46710	4.46710	(283, 1)	693360.0	36940.0	6.93750	(317, 1)
693050.0	10	05390	10.05390	(165, 1)	693350.0	36120.0	11.54088	(311, 1)
693050.0	18	76669	18.76669	(318, 1)	694000.0	390000.0	23.47004	(293, 1)
694000.0	5	39955	5.39955	(293, 1)	694000.0	369600.0	15.03043	(165, 1)
694000.0	10	37454	10.37454	(293, 1)	694000.0	345000.0	11.82588	(363, 1)
694000.0	7	30348	7.30348	(118, 1)	694000.0	325000.0	3.97357	(111, 1)
694000.0	2	68018	2.68018	(111, 1)	694500.0	385000.0	5.18974	(186, 1)
694000.0	7	39846	7.39846	(227, 1)	694500.0	375000.0	10.97342	(227, 1)
694000.0	13	27757	13.27757	(227, 1)	694500.0	385000.0	10.20410	(248, 1)
694000.0	4	29612	4.29612	(334, 1)	695000.0	370000.0	13.73863	(334, 1)
694000.0	10	10880	10.10880	(67, 1)	694840.0	374380.0	13.76233	(248, 1)
694000.0	29	34734	29.34734	(248, 1)	695000.0	330000.0	26.31408	(248, 1)
694000.0	16	42267	16.42267	(248, 1)	695000.0	320000.0	4.97864	(176, 1)
694000.0	4	67486	4.67486	(300, 1)	695000.0	375000.0	8.65343	(66, 1)
694000.0	14	84680	14.84680	(41, 1)	695500.0	337600.0	9.18639	(46, 1)
694000.0	10	05420	10.05420	(248, 1)	695500.0	327600.0	11.60905	(248, 1)
694000.0	8	36492	8.36492	(248, 1)	695500.0	385000.0	15.24727	(248, 1)
694000.0	9	07759	9.07759	(67, 1)	695820.0	378500.0	5.54838	(232, 1)
694000.0	4	25570	4.25570	(257, 1)	696000.0	370000.0	11.75045	(38, 1)
694000.0	5	37960	5.37960	(248, 1)	696000.0	315000.0	18.14358	(248, 1)
694000.0	7	00748	7.00748	(38, 1)	696500.0	370000.0	10.48105	(216, 1)
694000.0	4	42566	4.42566	(46, 1)	696500.0	315000.0	22.86405	(248, 1)
694000.0	3	30339	3.30339	(66, 1)	697000.0	385000.0	4.84764	(257, 1)

TABLE C-10. ISC-CALPRO MODEL OUTPUT - HIGHEST 5 DAYS NEXT TO 10 MAX

HIGH
24-HR
SGROUP # 11

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***
 * HIGHEST 24-HOUR AVERAGE CONCENTRATION MICROGRAMS/CUBIC METER *
 * FROM SOURCES: 1, -32,
 * FOR THE DISCRETE RECEPTOR POINTS *

X	Y	CON.	(DAY,PER.)	X	Y	CON.	(DAY,PER.)
691000.0	39000.0	3.90028	(67, 1)	691000.0	39000.0	4.99101	(342, 1)
691500.0	37500.0	4.94428	(117, 1)	691500.0	39000.0	5.03723	(317, 1)
692000.0	39000.0	6.13903	(342, 1)	692000.0	39000.0	3.66045	(165, 1)
692500.0	39000.0	4.00641	(165, 1)	692500.0	39000.0	5.379876	(67, 1)
693000.0	37500.0	7.51166	(317, 1)	693000.0	39000.0	7.44452	(266, 1)
693500.0	39000.0	6.97804	(112, 1)	693500.0	39000.0	6.98966	(98, 1)
694000.0	39000.0	5.02522	(22, 1)	694000.0	39000.0	4.87265	(165, 1)
694500.0	39000.0	5.15236	(317, 1)	694500.0	39000.0	3.80254	(293, 1)
695000.0	39000.0	4.12435	(237, 1)	695000.0	39000.0	7.01366	(165, 1)
695500.0	37500.0	4.63795	(317, 1)	695500.0	39000.0	14.01438	(138, 1)
696000.0	36120.0	7.30527	(311, 1)	696000.0	39000.0	11.34970	(112, 1)
696500.0	35320.0	21.08125	(364, 1)	696500.0	39000.0	15.41970	(22, 1)
697000.0	39000.0	11.24359	(263, 1)	697000.0	39000.0	6.85768	(363, 1)
697500.0	39000.0	4.46710	(165, 1)	697500.0	39000.0	6.49951	(237, 1)
698000.0	39000.0	19.05390	(165, 1)	698000.0	39000.0	11.93750	(317, 1)
698500.0	39000.0	19.76569	(316, 1)	698500.0	39000.0	23.64088	(317, 1)
699000.0	39000.0	5.39955	(293, 1)	699000.0	39000.0	4.47501	(273, 1)
699500.0	39000.0	17.57494	(293, 1)	699500.0	39000.0	15.03049	(165, 1)
700000.0	34860.0	3.96636	(111, 1)	700000.0	39000.0	11.82588	(363, 1)
700500.0	33500.0	2.68018	(111, 1)	700500.0	39000.0	3.97357	(111, 1)
701000.0	33500.0	7.39946	(227, 1)	701000.0	39000.0	5.18974	(186, 1)
701500.0	33500.0	13.2757	(227, 1)	701500.0	39000.0	10.57342	(237, 1)
702000.0	36098.0	4.2757	(334, 1)	702000.0	39000.0	10.20410	(237, 1)
702500.0	39000.0	10.10880	(67, 1)	702500.0	39000.0	4.73869	(334, 1)
703000.0	39000.0	29.34734	(248, 1)	703000.0	39000.0	13.76239	(248, 1)
703500.0	39000.0	16.42267	(248, 1)	703500.0	39000.0	26.34236	(248, 1)
704000.0	39000.0	4.67886	(176, 1)	704000.0	39000.0	18.31408	(248, 1)
704500.0	32500.0	4.60701	(300, 1)	704500.0	39000.0	4.97864	(166, 1)
705000.0	37020.0	4.84580	(41, 1)	705000.0	39000.0	8.97863	(66, 1)
705500.0	33220.0	18.05200	(248, 1)	705500.0	39000.0	9.15863	(46, 1)
706000.0	32240.0	10.3652	(248, 1)	706000.0	39000.0	11.620905	(248, 1)
706500.0	39500.0	4.07759	(67, 1)	706500.0	39000.0	15.24727	(248, 1)
707000.0	39500.0	9.25570	(257, 1)	707000.0	39000.0	5.34838	(38, 1)
707500.0	32250.0	5.37960	(248, 1)	707500.0	39000.0	11.75045	(38, 1)
708000.0	32250.0	7.00748	(38, 1)	708000.0	39000.0	18.14358	(248, 1)
708500.0	32260.0	4.42566	(46, 1)	708500.0	39000.0	12.85405	(248, 1)
709000.0	32950.0	3.30339	(68, 1)	709000.0	39000.0	4.84764	(257, 1)

TABLE C-11. ISC-CALPRO MODEL OUTPUT - HIGHEST 10 DAYS OF SECOND HIGHEST NEXT TO 10 MAX

2ND HIGH
24-HR
SGROUP# 11

*** *FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION RATES* ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION MICROGRAMS/CURIC METER

* FROM SOURCES:
1. -32
* FOR THE DISCRETE RECEPTOR POINTS *

X	Y	CON.	(DAY,PER.)	X	Y	CON.	(DAY,PER.)
691000.0	35000.0	3.22399	(318, 1)	691000.0	38500.0	3.74369	(318, 1)
691000.0	37500.0	3.82533	(268, 1)	691000.0	39000.0	3.72597	(258, 1)
691000.0	38000.0	3.72936	(318, 1)	692000.0	39500.0	4.67007	(164, 1)
692000.0	38000.0	3.43505	(317, 1)	692000.0	398000.0	4.56977	(318, 1)
692000.0	37500.0	3.95964	(318, 1)	692000.0	365000.0	6.51426	(311, 1)
692000.0	35500.0	4.68619	(36, 1)	692000.0	34500.0	6.95883	(364, 1)
692000.0	33500.0	3.84382	(221, 1)	692500.0	39000.0	3.57093	(164, 1)
692500.0	39000.0	4.57743	(73, 1)	693000.0	39500.0	2.90361	(237, 1)
693000.0	37500.0	3.57692	(165, 1)	693000.0	38000.0	5.21412	(164, 1)
693000.0	37500.0	3.94859	(165, 1)	693000.0	36500.0	11.41079	(116, 1)
693000.0	37500.0	17.02805	(158, 1)	693000.0	35720.0	10.75543	(127, 1)
693000.0	35200.0	11.06507	(113, 1)	693000.0	34960.0	14.13829	(264, 1)
693000.0	34500.0	8.04107	(122, 1)	693000.0	33500.0	5.45011	(279, 1)
693000.0	35000.0	4.15566	(334, 1)	693000.0	33500.0	5.52944	(346, 1)
693000.0	37500.0	7.33846	(237, 1)	693000.0	38000.0	10.86824	(78, 1)
693000.0	36500.0	17.81532	(67, 1)	693000.0	36940.0	18.34418	(158, 1)
693000.0	39500.0	2.95979	(204, 1)	693000.0	36120.0	3.76335	(204, 1)
693000.0	39500.0	4.93638	(204, 1)	693000.0	39000.0	3.00499	(293, 1)
693000.0	39860.0	17.93166	(363, 1)	693000.0	34500.0	19.19708	(279, 1)
693000.0	39500.0	7.14515	(111, 1)	693000.0	32500.0	3.90310	(118, 1)
693000.0	31500.0	2.40118	(300, 1)	693000.0	32500.0	3.90310	(118, 1)
693000.0	31800.0	6.32671	(186, 1)	693000.0	38500.0	4.85292	(227, 1)
693000.0	39580.0	12.59860	(186, 1)	693000.0	37500.0	8.21622	(186, 1)
693000.0	39500.0	3.91545	(227, 1)	693000.0	35160.0	43.12349	(46, 1)
693000.0	37500.0	9.03543	(176, 1)	693000.0	38500.0	3.72150	(186, 1)
693000.0	35720.0	2.36301	(176, 1)	693000.0	37000.0	13.49288	(67, 1)
693000.0	39740.0	7.18872	(22, 1)	693000.0	34300.0	11.12902	(46, 1)
693000.0	39500.0	4.11996	(300, 1)	693000.0	33000.0	4.76382	(275, 1)
693000.0	37020.0	3.97413	(176, 1)	693000.0	32000.0	4.76382	(300, 1)
693000.0	37020.0	14.69221	(46, 1)	693000.0	37500.0	7.26817	(232, 1)
693000.0	39240.0	5.42607	(46, 1)	693000.0	33760.0	7.96017	(214, 1)
693000.0	39500.0	4.44949	(129, 1)	693000.0	32760.0	4.14824	(129, 1)
693000.0	39500.0	3.68323	(112, 1)	693000.0	31500.0	2.71870	(275, 1)
693000.0	37500.0	8.66361	(41, 1)	693000.0	38500.0	4.57584	(299, 1)
693000.0	32250.0	3.18185	(46, 1)	693000.0	37000.0	11.34083	(257, 1)
693000.0	37500.0	6.67290	(257, 1)	693000.0	37000.0	11.34083	(257, 1)
693000.0	32260.0	3.63578	(214, 1)	693000.0	37000.0	9.95802	(129, 1)
693000.0	39500.0	2.59723	(299, 1)	693000.0	31500.0	4.59613	(46, 1)
693000.0	39500.0	2.59723	(299, 1)	693000.0	38500.0	4.43546	(41, 1)

TABLE C-12. ISC-CALPRO MODEL OUTPUT OF NEXT HIGHEST 5 DAYS TO 10 MAX - 24-HOUR EMISSION RATES
 FIVE HIGHEST 24-HOUR PART CONCENTRATIONS (ENDING ON JULIAN DAY, HOUR)
 (MICROGRAMS/M**3)

RECEPTOR	1	2	3	4	5
1	0.0200	0.0300	0.0000	0.0000	0.0000
2	0.4900	0.3400	0.0070	0.0000	0.0000
3	1.5300	0.3200	0.0000	0.0000	0.0000
4	1.7800	0.3200	0.0180	0.0000	0.0000
5	1.7300	0.3200	0.0190	0.0000	0.0000
6	1.7300	0.3200	0.0190	0.0000	0.0000
7	1.7300	0.3200	0.0190	0.0000	0.0000
8	1.7300	0.3200	0.0190	0.0000	0.0000
9	1.7300	0.3200	0.0190	0.0000	0.0000
10	1.7300	0.3200	0.0190	0.0000	0.0000
11	1.7300	0.3200	0.0190	0.0000	0.0000
12	1.7300	0.3200	0.0190	0.0000	0.0000
13	1.7300	0.3200	0.0190	0.0000	0.0000
14	1.7300	0.3200	0.0190	0.0000	0.0000
15	1.7300	0.3200	0.0190	0.0000	0.0000
16	1.7300	0.3200	0.0190	0.0000	0.0000
17	1.7300	0.3200	0.0190	0.0000	0.0000
18	1.7300	0.3200	0.0190	0.0000	0.0000
19	1.7300	0.3200	0.0190	0.0000	0.0000
20	1.7300	0.3200	0.0190	0.0000	0.0000
21	1.7300	0.3200	0.0190	0.0000	0.0000
22	1.7300	0.3200	0.0190	0.0000	0.0000
23	1.7300	0.3200	0.0190	0.0000	0.0000
24	1.7300	0.3200	0.0190	0.0000	0.0000
25	1.7300	0.3200	0.0190	0.0000	0.0000
26	1.7300	0.3200	0.0190	0.0000	0.0000
27	1.7300	0.3200	0.0190	0.0000	0.0000
28	1.7300	0.3200	0.0190	0.0000	0.0000
29	1.7300	0.3200	0.0190	0.0000	0.0000
30	1.7300	0.3200	0.0190	0.0000	0.0000
31	1.7300	0.3200	0.0190	0.0000	0.0000
32	1.7300	0.3200	0.0190	0.0000	0.0000
33	1.7300	0.3200	0.0190	0.0000	0.0000
34	1.7300	0.3200	0.0190	0.0000	0.0000
35	1.7300	0.3200	0.0190	0.0000	0.0000
36	1.7300	0.3200	0.0190	0.0000	0.0000
37	1.7300	0.3200	0.0190	0.0000	0.0000
38	1.7300	0.3200	0.0190	0.0000	0.0000
39	1.7300	0.3200	0.0190	0.0000	0.0000
40	1.7300	0.3200	0.0190	0.0000	0.0000
41	1.7300	0.3200	0.0190	0.0000	0.0000
42	1.7300	0.3200	0.0190	0.0000	0.0000
43	1.7300	0.3200	0.0190	0.0000	0.0000
44	1.7300	0.3200	0.0190	0.0000	0.0000
45	1.7300	0.3200	0.0190	0.0000	0.0000
46	1.7300	0.3200	0.0190	0.0000	0.0000
47	1.7300	0.3200	0.0190	0.0000	0.0000
48	1.7300	0.3200	0.0190	0.0000	0.0000
49	1.7300	0.3200	0.0190	0.0000	0.0000
50	1.7300	0.3200	0.0190	0.0000	0.0000
51	1.7300	0.3200	0.0190	0.0000	0.0000
52	1.7300	0.3200	0.0190	0.0000	0.0000
53	1.7300	0.3200	0.0190	0.0000	0.0000
54	1.7300	0.3200	0.0190	0.0000	0.0000
55	1.7300	0.3200	0.0190	0.0000	0.0000
56	1.7300	0.3200	0.0190	0.0000	0.0000
57	1.7300	0.3200	0.0190	0.0000	0.0000
58	1.7300	0.3200	0.0190	0.0000	0.0000
59	1.7300	0.3200	0.0190	0.0000	0.0000
60	1.7300	0.3200	0.0190	0.0000	0.0000

TABLE C-12 (CONTINUED)

1190	0.00	0.00	1.410	(40,24)	1.130	(0,24)	0.00	(0,00)	0.00	0.00	0.00	0.00	0.00
1120	0.00	0.00	1.410	(40,24)	0.200	(40,24)	0.00	(0,00)	0.00	0.00	0.00	0.00	0.00
1121	0.00	0.00	0.00	(40,24)	0.000	(0,00)	0.00	(0,00)	0.00	0.00	0.00	0.00	0.00
1122	0.00	0.00	0.00	(364,24)	0.000	(364,24)	0.00	(0,00)	0.00	0.00	0.00	0.00	0.00
1123	0.00	0.00	0.00	(364,24)	0.000	(248,24)	0.00	(0,24)	0.00	0.00	0.00	0.00	0.00

TABLE C-13 (CONTINUED)

118	0.00	0.00	1.049	(46,24)	0.450	(353,24)	0.250	(175,24)	0.070	(158,24)	0.00	(0,0)
119	0.00	0.00	1.742	(176,24)	0.470	(353,24)	0.000	(46,24)	0.000	(158,24)	0.00	(0,0)
120	0.00	0.00	0.510	(176,24)	0.150	(176,24)	0.000	(158,24)	0.000	(0,0)	0.00	(0,0)
121	0.00	0.00	0.420	(46,24)	0.140	(176,24)	0.000	(0,0)	0.000	(0,0)	0.00	(0,0)
122	0.00	0.00	0.440	(46,24)	0.350	(176,24)	0.000	(0,0)	0.000	(0,0)	0.00	(0,0)

TABLE C-14. ISC-CALPERSO MODEL OUTPUT OF TOP 6-10 DAYS OF HIGHEST, SECOND HIGHEST DAYS - 24-HOUR EMISSION RATES
 FIVE HIGHEST 24-HOUR PARTI CONCENTRATIONS (ENDING ON JULIAN DAY. HOUR)

RECEPTOR	1	2	3	4	5
1	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00
3	0.00	0.00	0.00	0.00	0.00
4	0.00	0.00	0.00	0.00	0.00
5	0.00	0.00	0.00	0.00	0.00
6	0.00	0.00	0.00	0.00	0.00
7	0.00	0.00	0.00	0.00	0.00
8	0.00	0.00	0.00	0.00	0.00
9	0.00	0.00	0.00	0.00	0.00
10	0.00	0.00	0.00	0.00	0.00
11	0.00	0.00	0.00	0.00	0.00
12	0.00	0.00	0.00	0.00	0.00
13	0.00	0.00	0.00	0.00	0.00
14	0.00	0.00	0.00	0.00	0.00
15	0.00	0.00	0.00	0.00	0.00
16	0.00	0.00	0.00	0.00	0.00
17	0.00	0.00	0.00	0.00	0.00
18	0.00	0.00	0.00	0.00	0.00
19	0.00	0.00	0.00	0.00	0.00
20	0.00	0.00	0.00	0.00	0.00
21	0.00	0.00	0.00	0.00	0.00
22	0.00	0.00	0.00	0.00	0.00
23	0.00	0.00	0.00	0.00	0.00
24	0.00	0.00	0.00	0.00	0.00
25	0.00	0.00	0.00	0.00	0.00
26	0.00	0.00	0.00	0.00	0.00
27	0.00	0.00	0.00	0.00	0.00
28	0.00	0.00	0.00	0.00	0.00
29	0.00	0.00	0.00	0.00	0.00
30	0.00	0.00	0.00	0.00	0.00
31	0.00	0.00	0.00	0.00	0.00
32	0.00	0.00	0.00	0.00	0.00
33	0.00	0.00	0.00	0.00	0.00
34	0.00	0.00	0.00	0.00	0.00
35	0.00	0.00	0.00	0.00	0.00
36	0.00	0.00	0.00	0.00	0.00
37	0.00	0.00	0.00	0.00	0.00
38	0.00	0.00	0.00	0.00	0.00
39	0.00	0.00	0.00	0.00	0.00
40	0.00	0.00	0.00	0.00	0.00
41	0.00	0.00	0.00	0.00	0.00
42	0.00	0.00	0.00	0.00	0.00
43	0.00	0.00	0.00	0.00	0.00
44	0.00	0.00	0.00	0.00	0.00
45	0.00	0.00	0.00	0.00	0.00
46	0.00	0.00	0.00	0.00	0.00
47	0.00	0.00	0.00	0.00	0.00
48	0.00	0.00	0.00	0.00	0.00
49	0.00	0.00	0.00	0.00	0.00
50	0.00	0.00	0.00	0.00	0.00
51	0.00	0.00	0.00	0.00	0.00
52	0.00	0.00	0.00	0.00	0.00
53	0.00	0.00	0.00	0.00	0.00
54	0.00	0.00	0.00	0.00	0.00
55	0.00	0.00	0.00	0.00	0.00
56	0.00	0.00	0.00	0.00	0.00
57	0.00	0.00	0.00	0.00	0.00
58	0.00	0.00	0.00	0.00	0.00
59	0.00	0.00	0.00	0.00	0.00
60	0.00	0.00	0.00	0.00	0.00
61	0.00	0.00	0.00	0.00	0.00
62	0.00	0.00	0.00	0.00	0.00
63	0.00	0.00	0.00	0.00	0.00
64	0.00	0.00	0.00	0.00	0.00
65	0.00	0.00	0.00	0.00	0.00
66	0.00	0.00	0.00	0.00	0.00
67	0.00	0.00	0.00	0.00	0.00
68	0.00	0.00	0.00	0.00	0.00
69	0.00	0.00	0.00	0.00	0.00
70	0.00	0.00	0.00	0.00	0.00
71	0.00	0.00	0.00	0.00	0.00
72	0.00	0.00	0.00	0.00	0.00
73	0.00	0.00	0.00	0.00	0.00
74	0.00	0.00	0.00	0.00	0.00
75	0.00	0.00	0.00	0.00	0.00
76	0.00	0.00	0.00	0.00	0.00
77	0.00	0.00	0.00	0.00	0.00
78	0.00	0.00	0.00	0.00	0.00
79	0.00	0.00	0.00	0.00	0.00
80	0.00	0.00	0.00	0.00	0.00
81	0.00	0.00	0.00	0.00	0.00
82	0.00	0.00	0.00	0.00	0.00
83	0.00	0.00	0.00	0.00	0.00
84	0.00	0.00	0.00	0.00	0.00
85	0.00	0.00	0.00	0.00	0.00
86	0.00	0.00	0.00	0.00	0.00
87	0.00	0.00	0.00	0.00	0.00
88	0.00	0.00	0.00	0.00	0.00
89	0.00	0.00	0.00	0.00	0.00
90	0.00	0.00	0.00	0.00	0.00
91	0.00	0.00	0.00	0.00	0.00
92	0.00	0.00	0.00	0.00	0.00
93	0.00	0.00	0.00	0.00	0.00
94	0.00	0.00	0.00	0.00	0.00
95	0.00	0.00	0.00	0.00	0.00
96	0.00	0.00	0.00	0.00	0.00
97	0.00	0.00	0.00	0.00	0.00
98	0.00	0.00	0.00	0.00	0.00
99	0.00	0.00	0.00	0.00	0.00
100	0.00	0.00	0.00	0.00	0.00

TABLE C-14 (CONTINUED)

1130	0.00	0.00	5.310	(344,24)	2.310	(276,24)	0.000	(5,24)	0.000	(3,24)	0.000	(0,0)
1131	0.00	0.00	1.070	(244,24)	0.340	(276,24)	0.000	(0,0)	0.000	(0,0)	0.000	(0,0)
1200	0.00	0.00	0.000	(276,24)	0.000	(344,24)	0.000	(0,0)	0.000	(0,0)	0.000	(0,0)
1201	0.00	0.00	0.000	(276,24)	0.000	(344,24)	0.000	(0,0)	0.000	(0,0)	0.000	(0,0)
1202	0.00	0.00	0.000	(276,24)	0.000	(344,24)	0.000	(36,24)	0.000	(0,0)	0.000	(0,0)
1203	0.00	0.00	0.000	(276,24)	0.000	(344,24)	0.000	(0,0)	0.000	(0,0)	0.000	(0,0)

TABLE C-15. ISC MODEL OUTPUT - STATIONARY SOURCES ONLY

*** * FILE:ISCFINAA-CRANDON TSP WITH ANNUAL EMISSION PATES* ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION MICROGRAMS/CUBIC METER FROM SOURCES: *
* FOR THE DISCRETE RECEPTOR POINTS *

X	Y	X	Y	CON.	(DAY,PER.)	X	Y	X	Y	CON.	(DAY,PER.)
691000.0	391000.0	691000.0	391000.0	0.98477	(67, 1)	691000.0	391000.0	691000.0	391000.0	0.98477	(318, 1)
691500.0	390000.0	691500.0	390000.0	1.46884	(117, 1)	691500.0	390000.0	691500.0	390000.0	1.46884	(258, 1)
692000.0	389000.0	692000.0	389000.0	1.213713	(165, 1)	692000.0	389000.0	692000.0	389000.0	1.213713	(165, 1)
692500.0	388000.0	692500.0	388000.0	1.411907	(112, 1)	692500.0	388000.0	692500.0	388000.0	1.411907	(199, 1)
693000.0	387000.0	693000.0	387000.0	1.55581	(122, 1)	693000.0	387000.0	693000.0	387000.0	1.55581	(98, 1)
693500.0	386000.0	693500.0	386000.0	1.87671	(144, 1)	693500.0	386000.0	693500.0	386000.0	1.87671	(164, 1)
694000.0	385000.0	694000.0	385000.0	1.205598	(199, 1)	694000.0	385000.0	694000.0	385000.0	1.205598	(293, 1)
694500.0	384000.0	694500.0	384000.0	1.715122	(165, 1)	694500.0	384000.0	694500.0	384000.0	1.715122	(138, 1)
695000.0	383000.0	695000.0	383000.0	1.99064	(311, 1)	695000.0	383000.0	695000.0	383000.0	1.99064	(121, 1)
695500.0	382000.0	695500.0	382000.0	3.60228	(364, 1)	695500.0	382000.0	695500.0	382000.0	3.60228	(92, 1)
696000.0	381000.0	696000.0	381000.0	2.07360	(122, 1)	696000.0	381000.0	696000.0	381000.0	2.07360	(323, 1)
696500.0	380000.0	696500.0	380000.0	1.34266	(283, 1)	696500.0	380000.0	696500.0	380000.0	1.34266	(323, 1)
697000.0	379000.0	697000.0	379000.0	1.73325	(307, 1)	697000.0	379000.0	697000.0	379000.0	1.73325	(144, 1)
697500.0	378000.0	697500.0	378000.0	1.241251	(293, 1)	697500.0	378000.0	697500.0	378000.0	1.241251	(199, 1)
698000.0	377000.0	698000.0	377000.0	1.36715	(253, 1)	698000.0	377000.0	698000.0	377000.0	1.36715	(235, 1)
698500.0	376000.0	698500.0	376000.0	1.11914	(236, 1)	698500.0	376000.0	698500.0	376000.0	1.11914	(235, 1)
699000.0	375000.0	699000.0	375000.0	1.92506	(111, 1)	699000.0	375000.0	699000.0	375000.0	1.92506	(145, 1)
699500.0	374000.0	699500.0	374000.0	1.45142	(153, 1)	699500.0	374000.0	699500.0	374000.0	1.45142	(300, 1)
700000.0	373000.0	700000.0	373000.0	2.23873	(227, 1)	700000.0	373000.0	700000.0	373000.0	2.23873	(227, 1)
700500.0	372000.0	700500.0	372000.0	1.07528	(227, 1)	700500.0	372000.0	700500.0	372000.0	1.07528	(227, 1)
701000.0	371000.0	701000.0	371000.0	1.67228	(157, 1)	701000.0	371000.0	701000.0	371000.0	1.67228	(292, 1)
701500.0	370000.0	701500.0	370000.0	1.60311	(196, 1)	701500.0	370000.0	701500.0	370000.0	1.60311	(232, 1)
702000.0	369000.0	702000.0	369000.0	3.73300	(248, 1)	702000.0	369000.0	702000.0	369000.0	3.73300	(232, 1)
702500.0	368000.0	702500.0	368000.0	1.46746	(176, 1)	702500.0	368000.0	702500.0	368000.0	1.46746	(248, 1)
703000.0	367000.0	703000.0	367000.0	1.60553	(141, 1)	703000.0	367000.0	703000.0	367000.0	1.60553	(176, 1)
703500.0	366000.0	703500.0	366000.0	1.18865	(231, 1)	703500.0	366000.0	703500.0	366000.0	1.18865	(66, 1)
704000.0	365000.0	704000.0	365000.0	1.87583	(248, 1)	704000.0	365000.0	704000.0	365000.0	1.87583	(248, 1)
704500.0	364000.0	704500.0	364000.0	1.95435	(267, 1)	704500.0	364000.0	704500.0	364000.0	1.95435	(232, 1)
705000.0	363000.0	705000.0	363000.0	1.48335	(231, 1)	705000.0	363000.0	705000.0	363000.0	1.48335	(32, 1)
705500.0	362000.0	705500.0	362000.0	1.87321	(36, 1)	705500.0	362000.0	705500.0	362000.0	1.87321	(248, 1)
706000.0	361000.0	706000.0	361000.0	1.12757	(42, 1)	706000.0	361000.0	706000.0	361000.0	1.12757	(183, 1)
706500.0	360000.0	706500.0	360000.0	1.865971	(41, 1)	706500.0	360000.0	706500.0	360000.0	1.865971	(323, 1)

APPENDIX D

SO₂, NO_x, CO AND HC

ANNUAL TOTAL EMISSION RATE ESTIMATES

TABLE D - 1 Schedule Associated With Project Activities During the Construction and Operation Phases and the Estimated SO₂ Air Emissions from the Proposed Sources (st/yr).

Project Activities	CONSTRUCTION				OPERATION																		
	1	2	3	4	1	2-3	4	5	6	7	8	9-11	12	13	14	15	16-17	18	19	20	21	22	
<u>Site Preparation (trees & brush)</u>																							
1. Mine Shafts																							
2. Mine/Mill Site																							
3. MAF Area																							
4. Access Road/Powerline					0.1																		
5. Railroad Spur							0.3	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
6. Haul Road							0.1	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
7. Water Discharge Pipeline																							
8. In-Plant Roads																							
9. Concrete Batch Plant																							
<u>Construct Mine Support Facilities</u>																							
1. Sink Main Shaft							0.39	0.15															
2. Sink and Equip Air Intake Shaft							0.05	0.04															
3. Construct East Exhaust Shaft																							
4. Construct West Exhaust Shaft																							
5. Power Generation							45.4	2.2	*	*													
<u>Underground Mine Development</u>																							
1. Develop Drifts and Stopes							0.007	0.07	1.4	3.1													
2. Mine Air Heating								0.02	*	*													
3. Mine Vehicles								14.4	*	*													

TABLE D - 1 (continued)

Project Activities	CONSTRUCTION				OPERATION																	
	1	2	3	4	1	2-3	4	5	6	7	8	9-11	12	13	14	15	16-17	18	19	20	21	22
<u>Construct Major Surface Facilities</u>																						
1. Construct Reclaim Pond R1																						
2. Construct Reclaim Pond R2																						
3. Mobile Sources	0.5	*	*	*	*																	
4. Construct Temporary Ore Storage Pad																						
<u>Construct MAF Facilities (Operations)</u>																						
1. Waste Rock Handling																						
a. Loading and Dumping																						
b. Hauling																						
2. Construct Tailing Pipeline																						
3. Construct Tailing Pond T1																						
4. Construct Tailing Pond T2																						
5. Reclaim Tailing Pond T1																						
6. Construct Tailing Pond T3																						
7. Reclaim Tailing Pond T2																						
8. Construct Tailing Pond T4																						
9. Reclaim Tailing Pond T3																						
10. Mobile Sources	0.05	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
11. Install Liner																						
a. Hauling of Bentonite to MAF																						

TABLE D - 2 Schedule Associated With Project Activities During the Construction and Operation Phases and the Estimated NO_x Air Emissions from the Proposed Sources (st/yr).

Project Activities	CONSTRUCTION			OPERATION																			
	1	2	3	4	1	2-3	4	5	6	7	8	9-11	12	13	14	15	16-17	18	19	20	21	22	
<u>Site Preparation (trees & brush)</u>																							
1. Mine Shafts				4.1																			
2. Mine/Mill Site																							
3. MMF Area																							
4. Access Road/Powerline		0.9	0.3	*	*																		
5. Railroad Spur		1.0	2.0	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
6. Haul Road			0.3	*	*																		
7. Water Discharge Pipeline																							
8. In-Plant Roads																							
9. Concrete Batch Plant					0.7	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
<u>Construct Mine Support Facilities</u>																							
1. Sink Main Shaft																							
2. Sink and Equip Air Intake Shaft																							
3. Construct East Exhaust Shaft																							
4. Construct West Exhaust Shaft																							
5. Power Generation																							
<u>Underground Mine Development</u>																							
1. Develop Drifts and Slopes																							
2. Mine Air Heating																							
3. Mine Vehicles																							

TABLE D - 2 (continued)

Project Activities	CONSTRUCTION				OPERATION																		
	1	2	3	4	1	2-3	4	5	6	7	8	9-11	12	13	14	15	16-17	18	19	20	21	22	
<u>Construct Major Surface Facilities</u>																							
1. Construct Reclaim Pond R1																							
2. Construct Reclaim Pond R2																							
3. Mobile Sources																							
4. Construct Temporary Ore Storage Pad																							
	6.5	*	*	*	*																		
<u>Construct MMF Facilities (Operations)</u>																							
1. Waste Rock Handling																							
a. Loading and Dumping																							
b. Hauling																							
2. Construct Tailing Pipeline																							
3. Construct Tailing Pond T1																							
4. Construct Tailing Pond T2																							
5. Reclaim Tailing Pond T1																							
6. Construct Tailing Pond T3																							
7. Reclaim Tailing Pond T2																							
8. Construct Tailing Pond T4																							
9. Reclaim Tailing Pond T3																							
10. Mobile Sources																							
11. Install Liner																							
a. Hauling of Bentonite to MMF	0.4	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*

TABLE D - 3 Schedule Associated With Project Activities During the Construction and Operation Phases and the Estimated CO Air Emissions from the Proposed Sources (at/yr).

Project Activities	CONSTRUCTION				OPERATION																		
	1	2	3	4	1	2-3	4	5	6	7	8	9-11	12	13	14	15	16-17	18	19	20	21	22	
<u>Site Preparation (trees & brush)</u>																							
1. Mine Shafts				46.2																			
2. Mine/Mill Site			75.0																				
3. MAIF Area																							
4. Access Road/Powerline				22.1																			
5. Railroad Spur			34.8	0.7	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
6. Haul Road			2.8	*	*																		
7. Water Discharge Pipeline																							
8. In-Plant Roads																							
9. Concrete Batch Plant																							
<u>Construct Mine Support Facilities</u>																							
1. Sink Main Shaft			17.9	7.5																			
2. Sink and Equip Air Intake Shaft			2.4	1.9																			
3. Construct East Exhaust Shaft																							
4. Construct West Exhaust Shaft																							
5. Power Generation			73.0	3.5	*	*																	
<u>Underground Mine Development</u>																							
1. Develop Drifts and Stopes			0.3	2.5	47.9	105.6																	
2. Mine Air Heating			0.8	*	*																		
3. Mine Vehicles			0.5	*	*																		

TABLE D - 4 Schedule Associated With Project Activities During the Construction and Operation Phases and the Estimated HC Air Emissions from the Proposed Sources (at/yr).

Project Activities	CONSTRUCTION				OPERATION																	
	1	2	3	4	1	2-3	4	5	6	7	8	9-11	12	13	14	15	16-17	18	19	20	21	22
<u>Site Preparation (trees & brush)</u>																						
1. Mine Shafts																						
2. Mine/Mill Site	25.3																					
3. MMF Area																						
4. Access Road/Powerline		4.2	0.3	*	*																	
5. Railroad Spur		6.1	0.5	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
6. Haul Road		0.3	*	*																		
7. Water Discharge Pipeline																						
8. In-Plant Roads					0.5	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
9. Concrete Batch Plant																						
<u>Construct Mine Support Facilities</u>																						
1. Sink Main Shaft																						
2. Sink and Equip Air Intake Shaft																						
3. Construct East Exhaust Shaft																						
4. Construct West Exhaust Shaft																						
5. Power Generation		12.0	0.6	*	*																	
<u>Underground Mine Development</u>																						
1. Develop Drifts and Stopes																						
2. Mine Air Heating			0.3	*	*																	
3. Mine Vehicles			0.9	*	*																	

TABLE D - 4 (continued)

Project Activities	CONSTRUCTION										OPERATION											
	1	2	3	4	1	2-3	4	5	6	7	8	9-11	12	13	14	15	16-17	18	19	20	21	22
<u>Construct Major Surface Facilities</u>																						
1. Construct Reclaim Pond R1																						
2. Construct Reclaim Pond R2																						
3. Mobile Sources																						
4. Construct Temporary Ore Storage Pad																						
	1.0	*	*	*	*																	
<u>Construct MUF Facilities (Operations)</u>																						
1. Waste Rock Handling																						
a. Loading and Dumping																						
b. Hauling																						
2. Construct Tailing Pipeline																						
3. Construct Tailing Pond T1																						
4. Construct Tailing Pond T2																						
5. Reclaim Tailing Pond T1																						
6. Construct Tailing Pond T3																						
7. Reclaim Tailing Pond T2																						
8. Construct Tailing Pond T4																						
9. Reclaim Tailing Pond T3																						
10. Mobile Sources																						
11. Install Liner																						
a. Hauling of Bentonite to MUF																						
	0.12	*	*	*	*																	

TABLE D - 4 (continued)

Project Activities	CONSTRUCTION			OPERATION																										
	1	2	3	4	1	2-3	4	5	6	7	8	9-11	12	13	14	15	16-17	18	19	20	21	22								
<u>Mine Operation (Production)</u>																														
1. Full (Total Estimated Underground Emissions)																														
a. Drilling & Blasting (Rock Handling)					0.4	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
b. Mine Air Heating					1.0	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
c. Mobile Equipment																														
<u>Mill/Concentrator Operations</u>																														
1. Facility Heating					0.3	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
2. Emergency Diesel Generators					0.5	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
3. Fuel Storage and Transfer					0.5	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
<table border="1" style="margin-left: auto; margin-right: auto;"> <tr> <th colspan="4">CLOSURE</th> </tr> <tr> <td>1</td> <td>2</td> <td>3</td> <td>4-7</td> </tr> </table>																							CLOSURE				1	2	3	4-7
CLOSURE																														
1	2	3	4-7																											
<u>Reclamation Phase</u>																														
1. Mobile Sources					1.2 ^a	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
TOTAL					49.2	4.5	*	*	8.3	*	*	*	*	*	*	*	*	*	*	*	*	*								

^aMeans previous annual estimate is used for this year.
 a Total in years 1-7 only.

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