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# LARGE AIRCRAFT COATINGS FLIGHT TESTING

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#### **EXECUTIVE SUMMARY**

The advent of the National Emission Standard for Hazardous Air Pollutants (NESHAP) and the concomitant requirements for minimal release of hazardous air pollutants have compelled the U.S. Air Force to adopt the use of paints with reduced Volatile Organic Compounds (VOCs). Self Priming Topcoat, TT-P-2756, formerly used on the exterior of the KC-135s was not performing satisfactorily with regards to adhesion, corrosion resistance, weatherability, and cleanability.

The High Performance Aerospace Coating System (HPACS) project conducted by Battelle identified four paint systems which offer improved film properties: System 23 from US Paint, System 6 from PRC-DeSoto (Courtaulds Aerospace), System 14 from Spraylat, and System 3 from Sherwin-Williams. The objective of this study was to monitor the performance of these improved systems when applied to aircraft. The Deft system from GSA, MIL-P-23377G and MIL-PRF-85285C, was used as a control. APC, urethane fluoropolymer topcoat from Deft, and applique were added to the monitoring.

Two KC-135s were painted at OC-ALC. One was coated with a system from US Paints and is based at MacDill AFB, FL; the other one had the upper surface of the left wing coated with APC (urethane fluoropolymer topcoat from Deft). Applique was applied over topcoat to areas of the right wing and a portion of the fuselage of this KC-135. It is assigned to Kadena AB, Japan. Two KC-135s were divided in the middle of the fuselage and refinished with different paint systems on each side at SM-ALC. One aircraft was coated with paint systems from Deft and PRC-DeSoto (Courtaulds); the other KC-135 was coated with paint systems from Spraylat and Sherwin-Williams. These aircraft are based at Hickam AFB, HI.

The latest inspection of the MacDill AFB test aircraft was accomplished in February, 1999. This KC-135 had logged 737.2 flight hours and 21 months environmental exposure since being painted. The aircraft had recorded 408.9 flight hours and 12 months Florida exposure between the initial and latest inspection. Visually, little corrosion and paint defects were noted. Considering the months of exposure, it is considered performing the best, although it exhibited fading and moderate chalking.

The latest inspection of the KC-135s at Hickam AFB, HI, shows the Sherwin-Williams (10 months, 328.7 flight hours) coating system to possess the best appearance, visually, followed by Deft (17 months, 612.9 flight hours), Spraylat (10 months, 328.7 flight hours), and PRC-DeSoto (Courtaulds) (17 months, 612.9 flight hours). The PRC-DeSoto (Courtaulds) system has exhibited unacceptable chalking.

The APC system (8 months) has the best appearance, but the least amount of exposure.

Preliminary data show the US Paints system to exhibit improved weatherability over the Deft control judged by the gloss and color stability as well as appearance. Limited exposure data shows Sherwin-Williams to possess improved appearance over the Deft control, but experience has shown exposure of 18 to 24 months is required to differentiate between coating systems.

Continued monitoring of these paint systems is recommended.

#### **1.0 PROJECT DESCRIPTION**

The objective of this task was to monitor the flight testing of coating systems identified by the High Performance Aerospace Coating System (HPACS) project conducted by Battelle to offer improved film properties of weatherability and cleanability. GSA coating system served as a control. APC (Advanced Performance Coating) and applique have also been included.

#### 2.0 INTRODUCTION

The reason for this project is to field-test coating systems that "exceed" current Mil-Spec coating systems. All tested coatings comply with the 1998 National Emissions Standard for Hazardous Air Pollutants (NESHAP). This project will provide a tool for ALCs to implement the best performing commercial "off the shelf" (COTS) coating system available, utilizing the results of these flights tests.

#### 3.0 BACKGROUND

TT-P-2756, Polyurethane Coating: Self Priming Topcoat coating system used formerly on the exterior moldline of the KC-135 aircraft was not meeting performance requirements over the full Programmed Depot Maintenance (PDM) cycle. The coating exhibits fading, chalking, and lack of corrosion protection.

The laboratory test and evaluation for a NESHAP compliant system with improved performance was accomplished via the HPACS contractual program managed by AFRL/MLSS. Four promising coating systems were identified by the HPACS program as being worthy for flight test consideration. The Deft coating system on the GSA contract was included to serve as a control because of its extensive use on other weapon systems. APC, a urethane fluoropolymer topcoat from Deft, was utilized on the wing of a test aircraft. Patches of paintless film (applique) from 3M was applied to portions of this test aircraft over topcoat to test the barrier properties of applique for corrosion protection. CTIO gathered other data on applique because of the opportunity. This technology is far from being implemented. The test coating systems (primer and topcoat) are tabulated below:

Vendor	HPACS	Epoxy Primer	Polyurethane Topcoat
Deft	GSA*	02-Y-40	03-GY-321
PRC-DeSoto (Courtaulds)	System 6**	513X423C/530K015/ 930K118	832G062/930G052
Sherwin-Williams	System 3	E90G203/V93V230	F93A27/V93V26/V93V1
Spraylat	System 14	EEAE 145A/B	EUBC 105B
US Paints	System 23	S9800/K8032	Awlgrip H.S.
Deft	APC (Advanced Performance Coating)	02-Y-40	99-GY-1
3M	Applique	02-Y-40	03-GY-321 + Applique

Table 1

\*Deft reformulated their MIL-P-85285 topcoat in May, 1996 to give better performance

\*\*PRC-DeSoto (Courtaulds) has added UV absorbers to their previous version topcoat to give better performance.

#### 4.0 TECHNICAL APPROACH

The coating systems were tested as drop-in replacements for MIL-P-23377G + TT-P-2756 for use on the outer moldline of KC-135 aircraft. Self Priming Topcoat (SPT) was tried and failed as a unicoat, therefore Tinker AFB and McClellan AFB started using primer (MIL-P-23377G) on selected areas of the aircraft under the SPT.

Operational test sites were selected which represent environments that are severely corrosive, marine, and receive high UV radiation. Two test aircraft were provided by Air Mobility Command (AMC); one is stationed at MacDill AFB, FL, and the other at Kadena AB, Japan. Two test aircraft were provided by Air National Guard (ANG) and are based at Hickam AFB, HI. These bases are designated as <u>severe corrosive environments</u> in T.O. 1-1-691, requiring a clear water rinse after the last flight of the day and a wash every 30 days for aircraft stationed at these locations. The AMC aircraft were coated at Tinker AFB, OK (OC-ALC) and the ANG aircraft were painted at McClellan AFB, CA (SM-ALC).

Testing was conducted as outlined in the Operational Test Plan dated August 1997, during the inspections by the CTIO team. The tests included:

TEST	REFERENCE	LOCATIONS
PATTI adhesion (modified)	ASTM D 5179	5-10 per coating system*
Pencil Hardness	ASTM D 3363	5-10 per coating system*
Wet Tape Adhesion	FTMS 141, Method 6301	5 per coating system*
Chalking (modified)	ASTM D 4214, Test Method C	5 per coating system**
Dry Film Thickness		$\cong$ 45 per aircraft***
Gloss, 60° and 85°	ASTM D 523	$\cong$ 45 per aircraft***
CIELab Color (10° observer, D65 illuminant, specular exclusive)	ASTM D 2244	≅ 45 per aircraft***

Table 2

\*Test locations, as indicated in the Aerospace Coating Service Test Technical Evaluation Team Inspection Sheet, Appendix VIII, assess fluid resistance on the belly; locations on the wings determine UV degradation. Subsequent values obtained during later inspections were from nearby locations.

\*\*Test locations on wing, as noted in Appendix VIII, measure UV degradation.

\*\*\*Test locations, as mapped in Appendix VIII, were chosen to represent different sections of the aircraft, the wings and fuselage. The locations are numbered to enable subsequent values obtained during later inspections to be near the same area.

The test plan identified three Critical Operational Issues (COIs) with attendant Measures of Effectiveness (MOE) and Measures of Performance (MOP).

The first Critical Operational Issue (COI) questions if the test coating provides equal or improved corrosion protection compared with the control coating system. In order to ensure the test coating systems show corrosion protection characteristics, the test coating systems shall be flight tested on test aircraft stationed in a severely corrosive, high UV marine environment for a minimum of 20 months. The test coating systems shall show equal or improved performance as compared to the Mil-Spec qualified Deft coating system in order to pass this COI. The Deft coating system will be used as the control coating system. The Measures of Effectiveness (MOE) are a comparison of the test coating with the control coating for corrosion protection, film integrity around fasteners, and adhesion of coating system.

The Measures of Performance (MOP) are visual inspection for corrosion and film integrity and adhesion values from the wet tape test and modified PATTI Test.

The second COI questions if the test coating offers equal or superior film performance compared with the control coating system. Per MIL-C-85285B, the specular gloss of camouflage topcoats at 60° angle of incidence shall have a reading of 5 or less. MIL-C-85285B topcoats have not been able to maintain the 5 or less reading over time and after many wash cycles. The test coating systems shall show improved performance in maintaining camouflage gloss measured at 60° and 85° over the control coating system in order to pass this COI.

The MOE includes evaluating gloss stability, cleanability and fluid resistance. The MOP uses the gloss meter and color spectrophotometer values to determine depth of change objectively and pencil hardness test to evaluate fluid resistance.

The third COI questions the appearance of the coating system compared with the control coating system. Appearance characteristics are comprised of cleanability of the coating system, color, and gloss stability of the coating system over time and after touch-up and repair, and lastly fluid resistance of the coating system. The test coating systems shall show improved performance in these areas over the control coating system in order to pass this COI.

The MOE includes evaluating the cleanability, gloss and color stability, fluid resistance and color/gloss matching of repaired areas. The MOP uses the gloss meter and color spectrophotometer values to assign numerical values relating to visual differences and pencil hardness test to evaluate fluid resistance.

Flight-testing is on going. Test aircraft are monitored at approximately 6-month intervals.

#### 5.0 TEST OBSERVATIONS

The coating application and inspections of the test aircraft are tabulated in Table 3. The values of each test and calculations of differences between the initial and subsequent tests are tabulated. Details of the laboratory test results are attached in:

Appendix I	Deft	Control
Appendix II	PRC-DeSoto (Courtaulds)	System 6
Appendix III	Sherwin-Williams	System 3
Appendix IV	Spraylat	System 14
Appendix V	US Paints	System 23
Appendix VI	Deft	APC

	ght Months Exposed urs	6 – McConnell AFB, KS 3 2 – MacDill AFB, FL 6 8 - MacDill AFB, FL 72 15 - MacDill AFB, FL		5.2 4 – Hickam AFB, HI 8.7 10 - Hickam AFB, HI	8 – Kadena AB, Japan
	Flight Hours	, 328.3 496.6 737.2	612.9	[ 145.2 328.7	ų
Inspection	Assigned	MacDill AFB, FL AMC	Hickam AFB, HI ANG	Hickam AFB, HI ANG	Kadena AB, Japan AMC
KC-135 of Paint Application and Inspection	Date Inspected	Jan. , 1998 July, 1998 February, 1999	July, 1998 January, 1999	July, 1998 January, 1999	February, 1999
	Location Painted	OC-ALC	SM-ALC	SM-ALC	OC-ALC
Summary	Date Painted	5 May 97	23-26 Sept. 1997	11-14 March 1998	29 May 1998
	Paint Vendor	US Paints	Deft-Left Side PRC-DeSoto (Courtaulds)-Right Side	Spraylat- Left Side Sherwin-Williams- Right Side	Deft Fluoropolymer Topcoat-Top Of Left Wing Applique-Top Of Right Wing And Fuselage
	Tail No.	64-14838	64-14832	59-1472	63-8040

Table 3

Large Aircraft Coatings Flight Testing

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5.1 Deft (Control) was first inspected at 10 months and 323.8 flight hours. It exhibited no chalking. The aircraft was undergoing isochronal inspection; therefore it had been washed and was in the hangar.

Witness panels had been placed on the aircraft at locations stated in Appendix I during paint application. "Initial values" had been obtained from these panels. Only small color changes were noted, showing a slightly lighter color on the wing and a slightly darker color on the fuselage. The delta L\* on the wing was 0.3 and negative 1.0 on the fuselage resulting in a delta E\* of 1.0 on both the wing and fuselage. The 60° gloss value was lower on the wing and slightly higher on the fuselage resulting in a reduced 60° gloss reading average (0.4) for the aircraft. The 85° gloss value was higher for both the wing and the fuselage, averaging 1.0 increase for the aircraft.

The modified PATTI values averaged 1764 psi on the belly and were very consistent. Modified PATTI values on the wing ranged from 1225 to 1862 psi averaging 1544 psi.

Corrosion was noted around fasteners, on the wing trailing edge, and on the doors of the front landing gear. Paint peeling was noted fasteners, engine cowling, and the leading edge.

At 17 months and 612.9 flight hours the color had changed showing the wing to be lighter and the fuselage to be very slightly darker. Comparison with the initial readings gave a delta L\* of 3.2 on the wing and negative .3 on the fuselage calculating to a delta E\* of 3.2 on the wing and .9 on the fuselage. The 60° gloss was reduced on the wing and increased slightly on the fuselage netting a slight loss of gloss (0.2). The 85° gloss was higher on both the wing and fuselage, average increase for the aircraft was 0.8 units. Chalking was moderate, rating from 5 to 8 per Photographic Reference Standard on ASTM D 659. (The higher the number the less the chalking.)

The modified PATTI test values averaged 1343 psi on the fuselage and 1493 psi on top of the wings. The values were very consistent. More details are listed in Appendix I.

Peeling was noted on the underside and leading edge of the wing, panel edges, on the sealant, and around the windshield. More details are noted in Appendix VII, Comments from Mike Sneed, OC-ALC/CRA.

5.2 PRC-DeSoto (Courtaulds) System was first inspected at 10 months and 323.8 flight hours. The chalking was moderate and rated an 8. The aircraft was undergoing isochronical inspection; therefore it had been washed and was in the hangar.

Witness panels had been placed on the aircraft at locations stated in Appendix II during paint application. Initial values were taken from these panels. Both the wing and the fuselage were lighter in color with a delta L\* of 3.4 on the wing and .9 on the fuselage resulting in a delta E\* of 3.5 on the wing and 0.9 on the fuselage. The 60° gloss was lowest of all of the test coatings and remained unchanged (1.0). The 85° gloss was slightly higher than the initial values (0.8 increase).

PATTI values for the fuselage ranged from 784 psi to 1470 psi averaging 1176 psi. The top of the wings ranged from 686 psi to 1176 psi averaging 931 psi.

Paint peeling was noted on fasteners on the leading edge and spoilers. Paint loss was noted on the leading edge of the horizontal stabilizer. Corrosion was noted on the trailing edges, fuselage, and doors of the front landing gear.

When inspected at 17 months and 612.9 flight hours, the color was even lighter with a delta  $L^*$  of 4.7 on the wing and 3.5 for the fuselage resulting in a delta  $E^*$  of 4.8 on the wing and 3.6 on the fuselage calculated from the initial color values. The 60° and 85° gloss values were slightly higher (60° - 0.4 increase, 85° - 1.1 increase). Chalking was severe, rating a 4.

Values for modified PATTI test ranged from 597 psi to 1343 psi on the fuselage averaging 1028 psi. The top of the wings ranged from 746 psi to 1194 psi averaging 888 psi. More details are explained in Appendix II.

Paint peeling was noted on the underside of the wings, on the Oklahoma Door, and around the Radome. Bare metal was apparent around the windshield and on the leading edge. More details are recorded in Appendix VII, Comments from Mike Sneed, OC-ALC/CRA.

5.3 Sherwin-Williams system was first inspected at 4 months and 145.2 flight hours. The finish exhibited no chalking. It was inspected on the flight line and the last wash was indeterminate. Hickam AFB wash rack was closed and a waiver had been requested.

Initial values that were obtained from the aircraft surface the day after the topcoat was applied utilizing the locations mapped in Appendix VIII were determined to be incorrect due to equipment malfunction. Calculations were made utilizing average readings for Fed. Standard 595B 36173. Little change in color was noted. The delta L\* on the wing was negative .83 and .45 on the fuselage computing to a delta E\* of .84 on the wing and 1.3 on the fuselage. Both the 60° and 85° gloss readings were slightly higher (0.6 unit increase for both 60° and 85° angle of incidence).

Pull values on the belly using the modified PATTI test ranged from 1274 psi to 1813 psi averaging 1519 psi. The top of the wings ranged from 1078 to 1862 psi averaging 1470 psi.

Paint loss was noted around fasteners on the aft end of the filler flap. Corrosion was seen around fasteners on the bottom of the fuselage.

At 10 months and 328.7 flight hours, little additional color change was noted. The aircraft was inspected on the flight line. The delta L\* was 1.1 on the wing and negative .45 on the fuselage; the delta E\* was 1.9 on the wing and 1.1 on the fuselage as calculated from the assumed initial values. Neither 60° nor 85° gloss values differed significantly from the initial values (60° 0.1 unit loss, 85° 0.1 gain). Chalking was moderate, ranging from 6 to 7.

PATTI pulls on the belly ranged from 697 to 746 psi averaging 713 psi. The top of the wings ranged from 1393 to 1691 psi averaging 1559 psi. More details are available in Appendix III.

Repaired areas include fasteners on upper wing, along fuselage seams, and leading edges. Peeling and cracking was noted on panel rivets, on cowling leading edges, and Beaver Tail. More details are recorded in Appendix VII, Comments from Mike Sneed, OC-ALC/CRA.

5.4 Spraylat system was first inspected at 4 months and 145.2 flight hours. No chalking was noted at that time. It was inspected on the flight line and the last wash was indeterminate. Hickam AFB wash rack was closed and a waiver had been requested.

The initial values obtained from the aircraft after painting were found to be erroneous due to equipment malfunction. Calculations were accomplished utilizing average expected color values for Fed standard 595 36173. Both the wing and the fuselage registered lighter in color with a delta L\* of .36 on the wing and .37 on the fuselage. This computed to a delta E\* of 1.1 on the wing and 1.4 on the fuselage. Both the 60° and 85° gloss values were slightly higher (60°-1.7 increase, 85°-0.6 increase).

Pull values on the belly utilizing the modified PATTI test ranged from 490 to 1078 psi averaging 865 psi. Values for the top of the wings ranged from 882 to 1421 psi averaging 1152 psi.

Paint peeling with corrosion was noted on fasteners on the wing tip. Paint was chipped below the cargo door.

At 10 months and 328.7 flight hours, little additional color change was recorded. The aircraft was inspected on the flight line. The delta L\* was .26 on the wing and negative .19 on the fuselage leading to a delta E\* of 1.8 on the wing and 1.2 on the fuselage as calculated from the assumed initial values.  $60^{\circ}$  gloss had increased 0.4 units from initial values and 85° gloss was unchanged. Chalking was moderate, ranging from 6 to 8.

Modified PATTI values for the belly ranged from 398 to 945 psi, averaging 713 psi. The top of the wings ranged from 796 to 945 psi averaging 879 psi. Greater details are available in Appendix IV.

Rework was observed on the wing, around fasteners, along fuselage seams, on the leading edge and underside of wing. Primer was showing in boom area. Paint was peeling and cracking along rivet rows and around Radome. More details are recorded in Appendix VII, Comments from Mike Sneed, OC-ALC/CRA.

5.5 US Paints system was first inspected at 8 months and 328.3 flight hours. At that time the aircraft had been assigned to McConnell AFB, KS, for six months and MacDill AFB, FL, for 2 months. Since this was the first inspection by CTIO and the aircraft had been stationed at a mild corrosion environment, the first readings were considered "initial readings". When the aircraft was transferred to MacDill AFB, FL, from McConnell AFB KS, blisters were noted on the fuselage above the horizontal stabilizer. When probed, a large (approximately 13 inches by 3 feet) area was discovered to be peeling between the primer and the chromate conversion coating.

The area was repaired. The repair was noticeable at a later date. The aircraft had been washed and was located in a hangar. The magnesium main landing gear follow-up doors exhibited moderate to severe corrosion and were later replaced by aluminum doors. There were a few spots of chipped paint in several areas around sealant and fasteners.

The next inspection 6 months and 168.3 flight hours later showed little change in color with delta L\* less than 1 for both the fuselage and the wings. The delta E\* was 1.2. The 60° gloss was lower (1.6 unit loss) and the 85° gloss was slightly higher (0.9 units). No chalking was observed.

Modified PATTI values for the belly ranged from 980 to 1274 psi averaging 1094 psi. The top of the wings ranged from 784 to 1421 psi averaging 1103 psi.

Chipped paint was observed on the leading edges of the wings and the horizontal stabilizers, along with the boom attachment points. Other areas include the engine cowlings, under the wing, and above the co-pilot window. Overall comments report most of the coating defects may be due to wear from maintenance, impact chips and broken coating around edges.

The following inspection, one year from the first "initial" inspection, showed a lighter color value with a delta L\* 2.6 on the wings and 3.3 on the fuselage calculating to a delta E\* of 2.0 on the wings and 2.3 on the fuselage, compared with the "initial" values. The 60° gloss was lower totaling a reduction of 2.8 units. The 85° gloss decreased slightly (0.4 units) from the "initial" values. Chalking was rated moderate, ranging from 6 on top of the wings to 8 under the wings.

Values on the belly for the modified PATTI test ranged from 597 to 1592 psi averaging 1055 psi. The top of the wings ranged from 1940 to 2587 averaging 2279 psi. This aircraft had accumulated a total of 737.2 flight hours since being painted, including 240.6 since the last inspection. Details are tabulated in Appendix V.

Some peeling on the leading edges and around doors and access panels was observed. More details are noted in Appendix VII, Comments from Mike Sneed, OC-ALC/CRA.

5.6 APC from Deft was first inspected at 8 months. The color was slightly darker from when initially painted, with delta L\* of negative 1.4 and delta E\* of 1.6. The 60° gloss decreased by 0.2 units and the 85° gloss increased by 1.7 units.

Modified PATTI values ranged from 1194 to 1791 psi averaging 1572 psi. Only the top of the wing was coated with APC. Greater detail is offered in Appendix VI.

Corrosion on fasteners was starting. More details are recorded in Appendix VII, Comments from Mike Sneed, OC-ALC/CRA.

5.7 The applique presented a good appearance. When it was removed, no corrosion was observed underneath, but a sticky residue remained that was difficult to dislodge. The gloss value IAW MIL-PRF-85285C was too high ( $60^\circ = 9.9$ ,  $85^\circ = 52$ ) initially, but it was not measured on the inspection trip.

5.8 Table 4 tabulates the values observed for gloss (60° and 85°) and CIEL (lightness) color data. The calculated values for delta L\* and delta E\* are also given for each inspection. The appendix for each coating system gives detailed data including individual dry film thickness readings, CIELab color readings, gloss values, and delta calculations for specific areas on the aircraft. PATTI and wet tape adhesion results, pencil hardness, chalking ratings at specific locations on the aircraft are tabulated.

		Com	partson c	lf Color a	Comparison of Color and Gloss Values of Flight Tested Systems	s Values	of Flight	Tested 5	iystems			
	1-141-1	Deff	ţ	PRC-D	PRC Desoto (Courtaulds)	atilds)		Sherwin-Williams			Sprayfat	
L' Total	19.712	49.336	51.145	48.776	144 mo 50.682	10 mo 52.576	<b>49.959</b>	<ul> <li>49.818</li> </ul>	50.182	<b>19.959</b>	<b>4 110</b> 49.644	49.947
L* Wing	49.577	49.867	52.896	48.557	52.006	53.257		49.130	51.058		49.598	50.227
L* Fuselage	49.728	48.783	49.705	48.823	49.718	52.280		50.406	49.512		49.585	49.696
∆ L* Total		-0.440	1.338		1.996	3.890		-0.141	0.223		-0.315	0.029
∆L* Wing	- <b>N</b> -	0.258	3.209		3.449	4.700		-0.829	1.099		-0.361	0.268
Δ L* Fuselage		-1.002	-0.330		0.902	3.464		0.447	-0.447		-0.374	-0.186
∆ E* Total		1.105	2.099		2.142	4.023		1.001	1.399		1.178	1.472
∆ E* Wing		0.912	3.254		3.535	4.763		0.843	1.901		1.101	1.794
∆ E* Fuselage		1.341	0.987		1.089	3.647		1.308	1.078		1.353	1.183
60 degree gloss	2.0	1.6	2.6	0.9	1.0	1.3	1.2	1.8	1.1	1.1	2.8	1.6
86 degree gloss	2.2	3.2	3.3	3.1	3.9	4.2	4.9	4.9	4.3	4.9	4.9	4.3
											- -	
		US Paints			APC							
	initial	6 mo	13 mo	initial	10 mo	17 mo						. <u> </u>
L* Total	49.689	50.509	52.822									
L* Wing	49.497	50.420	52.242	50.468	49.053							
L* Fuselage	49.702	50.379	52.653									
∆ L* Total		0.821	3.125									
AL* Wing		0.939	2.629		1.415							
∆ L* Fuselage		0.864	3.316									
∆ E* Total		1.292	2.245								-	
∆ E* Wing		1.243	2.017		1.558							
Δ E* Fuselage		1.464	2.323									
60 degree gloss	5.0	3.7	2.2	2.5	2.2							
85 degree gloss	6.2	6.9	5.8	2.7	3.9							
					Table 4	le 4						

No gloss readings (60° or 85°) were higher than specified in MIL-PRF-85285C. No wet tape failures occurred. The pencil hardness has increased on the finish from PRC-DeSoto (Courtaulds). The Spraylat system remains the softest of the finishes, but is increasing in hardness. The coating systems from Sherwin-Williams and Deft control present constant pencil hardness. The US Paint system was initially very hard and these values have remained constant. No significant changes have been noted from the modified PATTI test values.

#### 6.0 OPERATIONAL TEST AND EVALUATION TEST PLAN RESPONSE

COI-1: Do the test coating systems provide equal or improved protection against corrosion compared with control coating system?

MOE 1-1: The corrosion protection of the test coating systems shall be equal to or show an improvement over the currently used coating systems.

MOP 1-1-1: Upon visual inspection the test coated skins shall show no more exfoliation corrosion around fastener countersinks and panel edges than on the control coated skins.

Visual inspection observed no more exfoliation corrosion on any of the test aircraft than on the Deft control.

MOP 1-1-2: Upon visual inspection the test coated skins shall show no more filiform corrosion than on the control coated skins.

Visual inspection showed no more filiform corrosion on any of the test aircraft than on the Deft control.

MOE 1-2: The degree of compatibility (adhesion) of primer with the substrate and topcoat with the primer.

MOP 1-2-1: Upon visual inspection the degree of adhesion on the test side shall be equal to or better than the control side for all interfaces.

No more paint loss or peeling was observed on the test coatings than on the Deft control.

MOP 1-2-2: Modified Adhesion PATTI testing per ASTM 5179 shall measure a minimum of 1000 psi.

- Deft control All values were in excess of 1000 psi.
- PRC-DeSoto (Courtaulds) The pull values averaged 1000 psi; some pull values were less.
- Sherwin-Williams Pull values on the wing averaged 1559 psi, but pull values on the belly averaged 700 psi.
- Spraylat Pull values averaged 800 on the aircraft.

- US Paints All values but 2 were in excess of 1000, averaging the values equals over 1600.
- APC all values were over 1000, but only the top of the wing was tested, which normally gives greater values.

MOE 1-3: The integrity of the test coating system on and around upper and lower wing skin fasteners shall be equal or show an improvement over the currently used coating system.

MOP 1-3-1: Upon visual inspection and using the evaluation criteria stated in this test plan the test coating shall score an equal or higher value than the control coating.

Due to time constraints and difficulty to inspect the entire aircraft closely, the detailed rating system was not employed. In general, the integrity of the test coating systems was equal or higher than the control coating.

COI-2: Do the test coating systems provide equal or improved performance in the area of visible detection?

MOE 2-1: The gloss stability of the test coating systems shall be an improvement over the currently used coating systems.

MOP 2-1-1: Use of a portable gloss meter of 60 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

Deft control showed little gloss change, negative 0.2. Sherwin-Williams – 0.1, Spraylat and PRC-DeSoto (Courtaulds) 0.4, APC – negative 0.2, and US Paints negative 2.3. Only Sherwin-Williams showed less change in gloss and APC exhibited the same change.

MOP 2-1-2: Use of a portable gloss meter of 85 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

Deft control displayed a change of gloss equal to 0.8 units. PRC-DeSoto (Courtaulds) was higher with 1.1 and APC with 1.7. The other coating systems registered less change in gloss. Sherwin-Williams registered no change.

MOP 2-1-3: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical properties changes.

CTIO was unable to collect any chips.

MOE 2-2: The cleanability of the test coating systems shall be an improvement over the currently used systems.

MOP 2-2-1: Use of a portable gloss meter of 60 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

Deft control showed little gloss change, negative 0.2. Sherwin-Williams – 0.1, Spraylat and PRC-DeSoto (Courtaulds) 0.4, APC – negative 0.2, and US Paints negative 2.3. Only Sherwin-Williams showed less change in gloss and APC exhibited the same change.

MOP 2-2-2: Use of a portable gloss meter of 85 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

Deft control displayed a change of gloss equal to 0.8 units. PRC-DeSoto (Courtaulds) was higher with 1.1 and APC with 1.7. The other coating systems registered less change in gloss. Sherwin-Williams registered no change.

MOP 2-2-3: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical properties changes.

CTIO was unable to collect any chips.

MOE 2-3: The fluid resistance stability of the test coating systems shall be an improvement over the currently used coating systems.

MOP 2-3-1: Using the pencil hardness technique in accordance with FTMS-141, the change in hardness of the test coating shall be less than the change in hardness on the control coating.

The pencil hardness of the Deft control remained the same between the two inspections. The other test coatings remained the same or increased in hardness except one area of Sherwin-Williams exhibited one pencil hardness unit softer. The APC coating system has only been inspected once. No initial values could be obtained for any coating system.

MOP 2-3-2: Upon visual inspection the degree of adhesion on the test side shall be equal to or better than the control side for all interfaces.

No differences were recorded for adhesion differences as observed between the control coating system and the test coating systems. MOP 2-3-3: Use of a portable colorimeter in accordance with ASTM D2244 shall show a delta E ratio of test coating system to control coating system of less than 1.0 (i.e. delta E of test coating/delta E of control).

The only calculated ratio less than 1 was APC. The others ranged from 1.1 for US Paints, to 1.9 for Spraylat and PRC-DeSoto (Courtaulds), to 2.1 for Sherwin-Williams.

MOP 2-3-4: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical properties changes.

CTIO was unable to collect any chips.

COI-3 Do the test coating systems provide equal or improved appearance characteristics over the control coating system?

MOE 3-1: The cleanability of the test coating systems shall be an improvement over the currently used systems.

MOP 3-1-1: Use of a portable gloss meter of 60 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

Deft control showed little gloss change, negative 0.2. Sherwin-Williams – 0.1, Spraylat and PRC-DeSoto (Courtaulds) 0.4, APC – negative 0.2, and US Paints negative 2.3. Only Sherwin-Williams showed less change in gloss and APC exhibited the same change.

MOP 3-1-2: Use of a portable gloss meter of 85 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

Deft control displayed a change of gloss equal to 0.8 units. PRC-DeSoto (Courtaulds) was higher with 1.1 and APC with 1.7. The other coating systems registered less change in gloss. Sherwin-Williams registered no change.

MOP 3-1-3: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical properties changes.

CTIO was unable to collect any chips.

MOE 3-2 The color stability of the test coating shall be an improvement over the currently used coating system.

MOP 3-2-1: Use of a portable gloss meter of 85 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

Deft control displayed a change of gloss equal to 0.8 units. PRC-DeSoto (Courtaulds) was higher with 1.1 and APC with 1.7. The other coating systems registered less change in gloss. Sherwin-Williams registered no change.

MOP 3-2-2 Use of a black velvet cloth in accordance with ASTM D 4214, Test Method C shall show no evidence of chalking.

The APC exhibited no chalking, but it had endured the least exposure. Deft control was rated 7 as were US Paints and Spraylat. Sherwin-Williams was rated 6 and PRC-DeSoto (Courtaulds) was rated 4. (The coating systems with the higher numbers are rated the most resistance to chalking.)

MOP 3-2-3: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical properties changes.

CTIO was unable to collect any chips.

MOE 3-3: The gloss stability of the test coating system shall be an improvement over the currently used coating systems.

MOP 3-3-1: Use of a portable gloss meter of 60 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

Deft control showed little gloss change, negative 0.2. Sherwin-Williams – 0.1, Spraylat and PRC-DeSoto (Courtaulds) 0.4, APC – negative 0.2, and US Paints negative 2.3. Only Sherwin-Williams showed less change in gloss and APC exhibited the same change.

MOP 3-3-2: Use of a portable gloss meter of 85 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

Deft control displayed a change of gloss equal to 0.8 units. PRC-DeSoto (Courtaulds) was higher with 1.1 and APC with 1.7. The other coating

- systems registered less change in gloss. Sherwin-Williams registered no change.

MOP 3-3-3: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical properties changes.

CTIO was unable to collect any chips.

MOE 3-4: The fluid resistance of the test coating systems shall be an improvement over the currently used coating systems

MOP 3-4-1: Using the pencil hardness technique in accordance with FTMS-141, the change in hardness of the test coating shall be less than the change in hardness on the control coating.

The pencil hardness of the Deft control remained the same between the two inspections. The other test coatings remained the same or increased in hardness except one area of Sherwin-Williams exhibited one pencil hardness unit softer. The APC coating system has only been inspected once. No initial values could be obtained for any coating system.

MOP 3-4-2: Upon visual inspection the degree of adhesion on the test side shall be equal to or better than the control side for all interfaces.

No more paint loss or peeling was observed on the test coatings than on the Deft control.

MOP 3-4-3: Use of a portable colorimeter in accordance with ASTM D2244 shall show a delta E ratio of test coating system to control coating system of less than 1.0 (i.e. delta E of test coating/delta E of control).

The only calculated ratio less than 1 was APC. The others ranged from 1.1 for US Paints, to 1.9 for Spraylat and PRC-DeSoto (Courtaulds), to 2.1 for Sherwin-Williams.

MOP 3-4-4: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical properties changes.

CTIO was unable to collect any chips.

MOE 3-5: The The touch-up/repaired area shall an improvement relative to color and gloss over the currently used coating system.

MOP 3-5-1: Use of a portable colorimeter in accordance with ASTM D2244 shall show a delta E ratio of test coating system to control coating system of less than 1.0 (i.e. delta E of test coating/delta E of control).

CTIO was unable to obtain color readings of repaired areas and calculate values.

MOP 3-5-2: Use of a portable gloss meter of 60 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

CTIO was unable to obtain gloss readings of repaired areas and calculate values.

MOP 3-5-3: Use of a portable gloss meter of 85 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

CTIO was unable to obtain gloss readings of repaired areas and calculate values.

MOP 3-5-4: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical properties changes.

CTIO was unable to collect any chips.

#### 7.0 TEST SUMMARY

The appearance and values of the APC are excellent at this time, but it has less environmental exposure. There is no chalking and the PATTI adhesion tests are excellent. The US Paint system and Deft control exhibited similar values after the same exposure time.

The US Paint system has exhibited good exposure resistance. The aircraft has been painted for 20 months. The values obtained a year apart have shown moderate fading and little loss of 60° gloss. The aircraft had undergone 8 months exposure before inspections were initiated, but this was in a "mild corrosive environment."

Comparing all of the coating systems, they all possessed a better appearance than the other KC-135s that had been painted with TT-P-2756, Self-Priming Topcoat, at the respective bases. At this time, the APC looks excellent, but it does not have as much exposure as the other aircraft. Experience confirms that it takes 18 to 24 months exposure to obtain meaningful data to judge weathering resistance. The US Paints system was painted first and has accumulated 21 months exposure. It has exhibited moderate weatherability.

Visual observations of the KC-135s at Hickam AFB, HI, have ranked Sherwin-Williams to have the best appearance, followed by Deft control, Spraylat and PRC-DeSoto (Courtaulds). The PRC-DeSoto (Courtaulds) system has displayed unacceptable chalking.

All observed corrosion has been around fastener heads and rivets. This probably indicates the general need for a more flexible primer for larger aircraft like the KC-135. Corrosion under antennae was evident, but not coating system related.

#### 8.0 COMPARISON OF LABORATORY DATA WITH FLIGHT DATA

Laboratory testing was accomplished by Battelle for the HPACS Program for AFRL/MLSS. Table 5 summarizes data from Page 27 of the RELIABILITY AND MAINTAINABILITY IMPROVEMENT, HIGH PERFORMANCE AEROSPACE COATING SYSTEM PROGRAM. Final Report. The final overall composite desirability index conducted ranks the test coating systems in the following manner:

Category	System 3	System 6	System 14	System 23		System 17
		PRC-DeSoto (Courtaulds)	Spraylat	US Paints	Deft control	Deft TT-P- 2756 (SPT)
Survivability	.05	.01	.17	.05	.05	.03
Corrosion	.88	.93	.97	1.0	1.0	.20
Appearance	.65	.76	.59	.78	.57	.75
General	.63	.50	.56	.45	.43	.63
Flow Time	.63	.79	.79	.72	.79	.70
Composite	.59	.60	.59	.66	.53	.54

Table 5

The larger number represents greater desirability.

All of the test systems were rated high for corrosion resistance as tested, utilizing Salt Fog, Filiform, and EIS (Electrochemical Impedance Spectroscopy).

Artificial weathering data is summarized from this report, Appendix H.

Table 6 compares the laboratory test data for artificial weathering of the four systems judged to be worthy of flight testing, the GSA control and SPT (TT-P-2756):

Test		System 4	System 6	System 14	System 23	System 26	System 17
		Sherwin- Williams	PRC-DeSoto (Courtaulds)	Spraylat	US Paints	Deft control	Deft TT-P- 2756 (SPT)
Xenon Arc	ΔL*	0.2	2.1	-0.2	0.6	0.2	1.6
Weather-	ΔE*	0.3	2.0	0.3	0.6	0.2	1.6
ometer –	∆60°	-0.4	-0.8	0.0	+0.3	+0.1	-1.6
1000 hours	Δ85°	+1.0	-0.3	+0.3	+1.3	+0.3	+3.2
QUV –	$\Delta L^*$	0.8	1.5	0.2	0.1	0.5	1.6
40 Cycles	ΔΕ*	1.0	1.5	0.3	0.2	0.5	1.6
	Δ60°	-0.4	-0.7	+0.1	-0.2	+0.1	-2.3
	Δ85°	+0.4	-0.5	+0.8	0.0	+0.5	+1.3

Table 6

After 1000 hours exposure in the Xenon Arc Weatherometer (ASTM G 26), PRC-DeSoto (Courtaulds) exhibited the greatest change of color. The loss of 60° gloss was more than the other test systems in this matrix with the exception of SPT. Following 40 cycles in the QUV (ASTM G 53), PRC-DeSoto (Courtaulds) showed the greatest color difference with the exception of SPT, which is known to have poor color stability in the field. SPT also exhibited the greatest loss of gloss at 60° and the greatest increase of gloss at 85°.

The laboratory artificial weathering predicted the fading and gloss loss of the PRC-DeSoto (Courtaulds) system. The other systems tested were nearly equivalent to each other and marginally better than the GSA control and the "unacceptable" SPT.

The desirability index ranks US Paints the best overall and best appearance attribute, which seems to be the observation of this flight testing. The ranking of PRC-DeSoto (Courtaulds) next with a high appearance attribute seems at odds with artificial weathering data, but the initial appearance was very good, for both laboratory testing and when applied at the ALC. The desirability of the other test coatings were ranked nearly equal, which appears to be appropriate after flight testing.

#### 9.0 CONCLUSIONS

All of the tested paint systems have shown significantly improved weatherability over TT-P-2756, Self-Priming Topcoat. Casual observation noted that other KC-135s assigned to these same bases display a "patch work quilt" appearance.

Each coating system tested provided equal or improved protection against corrosion compared with the control coating system. The integrity of each coating system tested was equal or greater than the control coating system. The appearance of each coating system tested, with the exception of PRC-DeSoto, exhibited equal or greater stability of gloss and color than the control coating system.

US Paints system has endured the greatest exposure time of this test matrix and appears to perform better than the Deft control. Sherwin-Williams presents a better appearance than the control, but has been subjected to fewer months of exposure. Presently the Deft APC coating system offers promise, but the control performed equally with similar exposure and is known fade with additional exposure.

At this time US Paints has shown improved performance over the control. Sherwin-Williams may offer improved resistance to weathering over the Deft control and the others appear to be equal to the control at this time. Experience has shown exposure of 18 to 24 months is required to differentiate between coating systems.

Additional evaluations of these coating systems would be valuable to track weatherability as a function of time, flight hours, and missions. It is recommended that these inspections be continued at yearly intervals.

## **APPENDIX I**

**Deft Coatings** 

			KC-,	135, 1	KC-135, Tail No. 64-14832	0.64-	-1483	2	•	
			Sep-97			Jul-98			Jan-99	
Location		initial 1 *	initial *	initial L*	test	test	test L4	test	test	test
	ŀ	10170	4 070	0 746	10 550		2 257	r 50.430		7 010
	44	カーオ・カオ	-1.213	-2./10	49.725	-1.496	-3.979	0/1/20 51 770	-1.590	-3.8/0
ber	45				48.770	-1.447	-2.204	52.420	-1.600	-3.900
	46	49.675	-1.320	-3.860	48.554	-1.344	-3.315	52.790	-2.230	-3.360
ם, ו מ, ו	40				51.067	-1.594	-4.015	51.930	-1.620	-3.670
	39				50.686	-1.631	-4.129	54.000	-1.730	-3.860
	38				50.369	-1.595	4.273	53.610	-1.730	4.030
l9.	37				49.883	-1.549	4.167	53.740	-1.690	-4.050
1	36				50.199	-1.529	-4.158	53.630	-1.680	4.010
E	35				49.434	-1.422	-3.916	53.630	-1.680	4.010
Motors	49	49.922	-1.330	-3.884	48.876	-1.328	-3.608	48.730	-1.340	-3.760
	50				49.316	-1.349	-3.813	49.100	-1.310	-3.850
	32	49.828	-1.313	-3.684	49.037	-1.287	-3.720	51.870	-2.150	-3.620
	3	49.439	-1.234	-3.745	48.887	-1.319	-3.721	48.980	-1.450	-3.880
ə	8 7	10 877	700	3 7EE	10 7E1		107 C			010 0
6ej	3 4	13.024	CO7.1-			-1.532	-c	40.040 57 580	1.260	0/0.2-
əsr	41				48 509	-1 285	-3 470	49 960	-1 430	3 850
 1	30				49.142	-1.310	-3.750	49.400	-1.380	-3.870
J97	29				48.844	-1.290	-3.703	49.400	-1.380	-3.870
	28				48.463	-1.221	-3.589	48.810	-1.340	-3.950
	27	49.822	-1.289	-3.755	48.646	-1.239	-3.632	48.310	-1.280	-3.670
	47 48				48.227	-1.228	-3.044			
Average		49.712	-1.293	-3.771	49.336	-1.400	-3.713	51.145	-1.577	-3.803
Left Wing		49.577	-1.297	-3.788	49.867	-1.518	-3.734	52.896	-1.719	-3.762
Left Fuselage	Эс	49.728	-1.281	-3.735	48.783	-1.282	-3.617	49.705	-1.470	-3.847

Painted McClellan AFB, September 1997, LEFT SIDE

Initial values obtained from witness panels

Appendix I

**Deft Coatings** 

			×	(C-13	KC-135, Tail No. 64-14832	il No.	64-1	4832				
		7/98-initi	initial			1/99.	1/99-7/98			1/99-initia	nitial	
Location	delta L*	delta a*	delta b*	delta F	delta L*	delta a*	delta b*	delta E*	delta L*	defta a*	delta b*	delta E*
4	3 0.073	-0.207	0.349	0.412	2.618	-0.120	-0.503	2.669	2.691	-0.207	-0.154	2.703
•		-0.223	-0.263	0.424	2.045	-0.094	0.869	2.224	2.291	-0.317	0.606	2.391
45 45		-0.174	1.512	1.679	3.650	-0.153	-1.696	4.028	3.115	-0.327	-0.184	3.138
9:	•	-0.024	0.545	1.247	4.236	-0.886	-0.045	4.328	3.115	-0.910	0.190	3.251
, 9 1ac		-0.274	-0.155	1.427	0.863	-0.026	0.345	0.930	1.392	-0.300	0.190	1.437
ung		-0.311	-0.269	1.091	3.314	-0.099	0.269	3.326	4.325	-0.410	0.000	4.344
5	_	-0.275	-0.413	0.853	3.241	-0.135	0.243	3.253	3.935	-0.410	-0.170	3.960
	-	-0.229	-0.307	0.436	3.857	-0.141	0.117	3.861	4.065	-0.370	-0.190	4.086
36		-0.209	-0.298	0.638	3.431	-0.151	0.148	3.438	3.955	-0.360	-0.150	3.974
FLH 35	5 -0.488	-0.092	-0.032	0.498	4.196	-0.258	-0.094	4.205	3.708	-0.350	-0.126	3.727
Motors 49	9 -1.046	0.002	0.276	1.082	-0.146	-0.012	-0.152	0.211	-1.192	-0.010	0.124	1.198
50		-0.036	-0.129	0.529	-0.216	0.039	-0.037	0.223	-0.728	0.003	-0.166	0.747
С		0.026	-0.036	0.792	2.833	-0.863	0.100	2.963	-0.459	-0.837	0.064	0.957
3	0.552	-0.085	0.024	0.559	0.093	-0.131	-0.159	0.226	-0.459	-0.216	-0.135	0.525
e Ge	-1.068	-0.003	0.024	1.068	-0.114	-0.028	-0.139	0.182	-1.182	-0.031	-0.115	1.188
	.:::.								2.758	-0.371	-0.285	2.797
	_	0.004	0.285	1.344	1.451	-0.145	-0.380	1.507	0.138	-0.141	-0.095	0.219
		-0.021	0.005	0.680	0.258	-0.070	-0.120	0.293	-0.422	-0.091	-0.115	0.447
		-0.001	0.052	0.979	0.556	-0.090	-0.167	0.587	-0.422	-0.091	-0.115	0.447
28		0.068	0.166	1.371	0.347	-0.119	-0.361	0.515	-1.012	-0.051	-0.195	1.032
27	7 -1.176	0.050	0.123	1.183	-0.336	-0.041	-0.038	0.341	-1.512	0.009	0.085	1.514
4	. i											
48	-	0.061	0.711	1.747								
Average	-0.440	-0.093	0.103	0.954	1.809	-0.176	060.0-	1.965	1.338	-0.276	-0.045	2.099
Left Wing		-0.214	0.078	0.912	3.028	-0.201	-0.028	3.117	3.209	-0.401	0.015	3.254
Left Fuselage	e -1.002	0.006	0.123	1.025	0.541	-0.161	-0.145	0.760	-0.330	-0.182	-0.107	0.987

Painted McCiellan AFB, September 97, LEFT SIDE

Initial values obtained from witness panels

Appendix I

Deft Coatings

Painted McClellan AFB, September 97, LEFT SIDE

			KC.	KC-135,	Tail N	Tail No. 64-14832	<b>I-148</b>	32	,		
Location	9/97 initial DFT mils	7/98 test DFT mils	1/99 test DFT mils	9/97 initial 60 degree Gloss	7/98 test 60 degree Gloss	1/99 test 60 degree Gloss	total delta 60 degree Gloss	9/97 initial 85 degree Gloss	7/98 test 85 degree Gloss	1/99 test 85 degree Gloss	total delta 85 degree Gloss
	2         3         3         4         3	4.0 6.7 6.7 4.4 7.0 10.7 13.1 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	3.1 3.1 5.6 4.5 4.5 4.6 4.1 12.4 7.0 7 5.3 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 5.3 5.3 5.3 3.1 5.3 5.3 5.3 5.4 5.4 5.4 5.4 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6	2.6 2.5 2.5 2.6 2.6 1.7 1.7 1.7 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6	1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 2	1.4 1.4 1.5 1.5 1.5 1.9 2.6 2.4 2.1 2.4 2.1 2.4 2.4 2.4 2.4 2.4 2.4 1.6 1.6 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	0.0 0.1 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	1.9 3.3 1.5 1.6 1.9 1.9 1.9 1.9	4 7 8 7 7 8 9 8 8 8 9 7 7 8 7 8 7 8 7 8 7	4.1 4.1 3.5 3.5 3.5 3.5 3.6 3.6 3.6 3.6 3.6 3.7 2.6 2.6 2.6 2.6 2.6 3.6 3.6 3.7 2.6 4 2.6 2.6 3.7 3.6 3.7 2.6 4.0 5.3 3.7 5.6 4.0 5.6 5.7 4.0 5.7 4.0 5.7 4.0 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7	2.2 2.0 2.2 0.4 0.4 0.7 1.1 1.1 1.3 0.7 1.2 1.2 0.7 1.2 0.7 1.3 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.0 0.0 0.0
Wing	3.5	- 9.4	4.4 4.4	2.3 2.3	0. <del>1</del> . 4.	1.5 1.5	7.0- - 0.0-	2.5	3.0 3.0	0.0 4.6	0.7
Fuselage	3.4	4.0	5.2	1.8	2.1	2.2	0.5	1.7	3.5	3.0	0.9

# Appendix I

Initial values obtained from witness panels DFT = Dry Film Thickness . •

					ЧĊ Х	-135	<b></b>	135, Taih Neimber 64-14832	dimb	еr	64-1	4832						
Courtaulds – (F	Rigt	– (Right Side)					1											
	-	Fuselage	eQ4	2	Fuselage	90	6	Fuselage	901	4	Leading Edge	Edge	S	Wing Tip	┢	2 4	pper Wing 3	Upper Wing 3&4 Engines
		36/2	1/89		7/38	1/99	<b>.</b>	86/2	1/99	L.,	7/98	1/99	<b>.</b>	86/2	1/39	Ĺ	86/2	1/90
				<b>_L</b> _						<u> </u>	j,		1,		1921			ise:
Pencil Hardness			¥	L	L.	Ъ	1	L.	Ŧ	1	L.	¥		60	I		•	2H
Modified PATTI		784 psi	597 psi		1274 psi	1144 psi		1470 psi	1343 psi		1176 psi	746 psi		686 psi	1194 psi		•	995 psi
Failure Mode: AG			5 %	L		5%			15 %	L		45 %	<b>.</b>		55 🖌			45 %
٩¥			10 %	L			ł			L			<b>-</b>					
ATP	L			L			L			L			·			L		
СР	L!			I			ł			L								
ст	L		85 %	L		95 <b>%</b>	·		85 %	<b>.</b>		55 <b>%</b>	·		45 %	l		55 %
Wet Tape	L	Pass		L	Pass			Pass		I	Pasa		K	Pass		L		
								4					1					
	-	Wing Tip	đ	2	Wing			Wing		4	Wing		5	Fuselage		~		
Chalking	<u> </u>	Moderate (8")	4		Moderate (8")	4		Moderate (8*)	4	1.=	Moderate (8")	4	<u> </u>	Moderate (8")	4	<u> </u>		
Deft – (Left Side)	le)																	
	9	Fuselage	8	F	Fuselage	8	8	Fuselage	90	6	Leading Edge	Edge	ē	Wing Tip		5 6	pper Wing 1	Upper Wing 1&2 Engines
	L	7/98	1/99	L	7/98	1 00		7/98	90/5	L	1/98	4 60		7/98	1 /00	Ľ	7.00	90
		test	test		test	test		test	test		test	test		test	test		test	test
Pencil Hardness		2H	2H		2H	2H		2H+	2H		I	I		2H+	2H		•	¥
Modified PATTI		1764 psi	1293 psi	L	1764 psi	1293 psi	L	1764 psi	1443 psi	L	1862 psi	1493 psi	<b>.</b>	1225 psi	1493 psi	<b>I</b>		1493 psi
Fallure Mode: AG			5%	أسسا		20 %			15 %	L		25 %	H		20 <b>%</b>			35 %
٩P	L			L		75 %	1			L			٠			<u> </u>		
ATP	لسا			I			<b></b>			I						<u> </u>		
СР			75 %				L			L			•					
ст			20 %	L		2 <b>%</b>			85 %	L		75 %	•		* 8	L		85 <b>%</b>
Wet Tape		Pass	•	L	Pass	•	·	Pass	•		Pass	•		Pass	•	<u> </u>		•
																┝─┤		
	<u> </u>	Wing Tip	₽ P	~	Wing		<u></u> м	Wing		4	Wing	g	S	Fuselage				
Chalking		None	g		None	5		None	ω		None	8		None	Ø			
Dicht Side Cou	Ċ																	
													D A C	= Adnesion	AG = Agnesion of glue to stud of topcoat		r topcoat	
Left Side - Deft	!	•											AP	= Adhesion	AP = Adhesion of Primer to substrate	iqns c	strate	

Appendix I

\* = ASTM D 659 Photographic Reference Standard

CP = Cohesion of Primer CT = Cohesion of Topcoat

ATP = Adhesion of Topcoat to Primer

Pencil Hardness (Soft to Hard): 5b-4b-3b-2b-b-Hb-F-H-2H-3H-4H-5H-6H-7H-8H-9H

## **APPENDIX II**

Appendix II

Initial values obtained from witness panels DFT = Dry Film Thickness

			KC-1	KC-135, Tail No. 64-14832	ail No	o. 64-	1483;	8			
Location	9/97 initial DFT mils	7/98 test DFT mils	1/99 test DFT mils	9/97 initial 60 degree Gloss	7/98 test 60 degree Gloss	1/99 test 60 degree Gloss	total delta 60 degree Gloss	9/97 initial 85 degree Gloss	7/98 test 85 degree Gloss	1/99 test 85 degr <del>ee</del> Gloss	total delta 85 degree Gloss
Right Fuselage 5. 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.6 1.6 1.6 1.6 1.1 1.6 1.6	3.3. 3.3.3. 3.4.4.5. 3.4.4.5. 4.5.5.4.5. 4.5.5.4.5. 4.5.5.4.5. 4.5.5.4.5.5. 4.5.5.4.5.5. 4.5.5.5.4.5.5.5. 4.5.5.5.5	4.6 3.7 3.7 3.7 4.7 4.7 4.7 3.3 4.7 4.7 3.3 3.2 4.7 3.3 3.2 4.7 3.3 4.7 3.2 4.7 3.2 4.7 3.2 4.2 4.2 4.2 4.2 5.5 4.2 5.5 4.2 5.5 5.2 4.2 5.5 5.2 4.2 5.5 5.2 4.2 5.5 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.9 0.9 0.9 0.9 0.9 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	1.0 0.9 0.9 0.9 1.2 1.2 1.2 1.2 1.2 1.3 1.2 1.3 1.0 1.0 1.0 1.0 1.0 1.0	0.1 0.0 0.0 0.0 0.3 0.3 0.1 0.1 0.1 0.1 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	3.3 3.0 3.1 3.5 3.5 3.5 2.1 2.4	7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5	0.0444446.00 0.04446.00 0.0448.00 0.004040 0.004040 0.004040 0.004040 0.004040 0.00004040 0.00000000	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2
Average Wing Fuselage	3.9 1.6 4.2	4.6 3.9 4.2	4.0 3.6 3.5	0.0 0.0 0.0	1.0 0.9 0.8	1.3 1.6	0.4 0.1 0.7	3.1 3.3 3.1	3.9 3.2 3.2	4.2 4.5 1.4	1.1 1.2 0.1

Painted McCiellan AFB, September 97, RIGHT SIDE

**Courtaulds Paints** 

Painted McClellan AFB, September 97, RIGHT SIDE

		KC-135, Tail No. 64-14832	35, T	ail N	0.64	-148	32		
		Sep-97			Jul-98			Jan-99	
Location	initial L*	initial a*	initial b*	test L *	test a *	test b *	test L*	test a*	test b*
0				51.514	-2.031	-3.226	52.170	-1.600	-3.870
19( 4	48.557	-1.616	-4.027	51.885	-2.203	-3.774	53.310	-2.240	-2.860
ى dd				50.526	-2.014	-3.065	53.240	-2.280	-3.570
90				51.664	-2.067	-3.564	51.290	-1.990	-3.800
pni Pni				52.042	-2.150	-3.760	54.180	-2.310	-3.610
				52.385	-2.177	-3.794	53.220	-2.300	-3.690
				52.418	-2.252	-3.963	53.600	-2.300	-3.680
₽ig	<u> </u>			53.209	-2.243	-3.800	54.010	-2.300	-3.690
-	1			52.412	-2.219	-3.871	54.290	-2.270	-3.590
RH 14	4			49.007	-1.804	-3.687	53.110	-2.150	-3.700
Motors 15	5 48.617	-1.585	-4.230	50.091	-1.976	-3.853	48.870	-1.320	-3.780
19	9 48.897	-1.667	-4.106	49.201	-1.828	-3.723	52.490	-2.190	-3.590
~	8 48.830	-1.633	-4.144	48.979	-1.849	-3.843	52.930	-2.250	-3.610
•	17 48.931	-1.587	-4.108	49.718	-1.959	-3.860	53.390	-2.270	-3.500
<b>1</b> 10	0			49.102	-1.851	-3.791	53.820	-2.210	-3.520
12 12	2 48.644	-1.572	-4.159	51.309	-2.247	-3.794	50.490	-1.510	-4.070
н С				51.478	-2.213	-3.927	54.190	-2.280	-3.360
3 Jut	0 48.888	-1.566	-4.159	49.995	-1.912	-3.874	53.290	-2.190	-3.390
Rig 21		-1.535	-4.211	49.896	-1.858	-3.791	52.300	-2.140	-3.720
23	3 48.778	-1.636	-4.040	48.670	-1.778	-3.837	51.590	-1.940	-3.550
22	2 48.735	-1.671	-4.100	48.829	-1.736	-3.787	48.310	-1.280	-3.670
Average	48.776	-1.607	-4.128	50.682	-2.017	-3.742	52.576	-2.063	-3.610
Right Wing	48.557	-1.616	-4.027	52.006	-2.151	-3.646	53.257	-2.177	-3.596
Right Fuselag	48.823	-1.608	-4.128	49.718	-1.923	-3.823	52.280	-2.026	-3.598

Initial values obtained from witness panels

Painted McClellan AFB, September, 1997, RIGHT Side

			КĊ К	KC-135, Tail No. 64-14832	Tail	No.	64-14	1832				
		7/98-i	//98-initial			1/99.	1/99-7/98			1/99-initial	nitial	
Location	delta	delta	delta	deita	delta	delta	delta	delta	delta	delta	deita	deita
	<u>-</u>		'n	ů	<b>ن</b>	<b>.</b>	p,	້ພ	5	a,	<b>*</b> _	ů
ς,	2.957	-0.415	0.801	3.092	0.656	0.431	-0.644	1.015	3.613	0.016	0.157	3.616
	3.328	-0.587	0.253	3.389	1.425	-0.037	0.914	1.693	4.753	-0.624	1.167	4.934
i	1.969	-0.398	0.962	2.227	2.714	-0.266	-0.505	2.773	4.683	-0.664	0.457	4.752
ĐĐĐ	3.107	-0.451	0.463	3.174	-0.374	0.077	-0.236	0.449	2.733	-0.374	0.227	2.768
ejur iui/	3.485	-0.534	0.267	3.536	2.138	-0.160	0.150	2.149	5.623	-0.694	0.417	5.681
IS	3.828	-0.561	0.233	3.876	0.835	-0.123	0.104	0.850	4.663	-0.684	0.337	4.725
	3.861	-0.636	0.064	3.914	1.182	-0.048	0.283	1.216	5.043	-0.684	0.347	5.101
-	4.652	-0.627	0.227	4.700	0.801	-0.057	0.110	0.811	5.453	-0.684	0.337	5.506
Ŧ	3.855	-0.603	0.156	3.905	1.878	-0.051	0.281	1.900	5.733	-0.654	0.437	5.787
RH 14	0.390	-0.219	0.543	0.703	4.103	-0.346	-0.013	4.118	4.493	-0.565	0.530	4.559
Motors 15	1.474	-0.391	0.377	1.571	-1.221	0.656	0.073	1.388	0.253	0.265	0.450	0.580
19		-0.161	0.383	0.515	3.289	-0.362	0.133	3.312	3.593	-0.523	0.516	3.667
		-0.216	0.301	0.399	3.951	-0.401	0.233	3.978	4.100	-0.617	0.534	4.180
		-0.372	0.248	0.905	3.672	-0.311	0.360	3.703	4.459	-0.683	0.608	4.552
ela 6		-0.264	0.317	0.447	4.718	-0.359	0.271	4.739	4.889	-0.623	0.588	4.963
		-0.675	0.365	2.773	-0.819	0.737	-0.276	1.136	1.846	0.062	0.089	1.849
		-0.641	0.232	2.915	2.712	-0.067	0.567	2.771	5.546	-0.708	0.799	5.648
	_	-0:346	0.285	1.194	3.295	-0.278	0.484	3.342	4.402	-0.624	0.769	4.512
Вi	1.012	-0.323	0.420	1.142	2.404	-0.282	0.071	2.422	3.416	-0.605	0.491	3.504
23	-0.108	-0.142	0.203	0.270	2.920	-0.162	0.287	2.939	2.812	-0.304	0.490	2.871
·	0.094	-0.065	0.313	0.333	-0.519	0.456	0.117	0.701	-0.425	0.391	0.430	0.720
Average	1.996	-0.411	0.353	2.142	1.893	-0.045	0.132	1.898	3.890	-0.456	0.485	4.023
	3.449	-0.535	0.381	3.535	1.251	-0.026	0.051	1.429	4.700	-0.561	0.431	4.763
Right Fuselage	0.902	-0.321	0.307	1.089	2.562	-0.103	0.225	2.904	3.464	-0.423	0.531	3.647

**Courtaulds Paints** 

Appendix II

Initial values obtained from witness panels

# **APPENDIX III**

Right Fuselage         Angn wing, upper         Andree           Right Fuselage         Surface         3/88           Right Fuselage         3/11.5         3/11.5           22         21         12         3/1.5           22         5.1         3/1.5         3/1.5           23         5.1         3/1.5         3/1.5           23         5.1         11.5         3/1.5           23         5.1         3/1.5         3/1.5           23         5.1         3/1.5         3/1.5           23         5.1         5.1         4.5           23         5.1         4.5         5.1           23         5.1         4.5         5.1           23         5.1         4.5         5.1           23         5.1         4.5         5.1           5.1         5.1         5.1         5.1           5.1         5.1         5.1         5.1           5.2         5.1         5.1         5.1           5.1         5.1         5.1         5.1           5.2         5.1         5.1         5.1           5.2         5.1         5.1 <t< th=""></t<>
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Painted McClellan AFB, March 98, RIGHT SIDE

Sherwin-Williams Paints

Appendix III

DFT = Dry Film Thickness

Sherwin-Williams Paints

Painted McClellan AFB, March 1998, RIGHT SIDE

Mar-95         Jul-95 $\Gamma^*$ $a^*$ Jul-95 $\Gamma^*$ $a^*$ Jul-95 $\Gamma^*$ $a^*$ Jul-95 $49.659$ $-1.513$ $-4.086$ $48.877$ $-1.485$ $49.959$ $-1.513$ $-4.086$ $48.877$ $-1.485$ $49.959$ $-1.513$ $-4.086$ $48.903$ $-1.412$ $49.959$ $-1.445$ $49.022$ $-1.333$ $49.269$ $-1.445$ $49.9399$ $-1.445$ $49.9399$ $-1.4427$ $49.970$ $-1.445$ $49.9397$ $-1.427$ $49.870$ $49.969$ $-1.446$ $49.612$ $-1.427$ $49.870$ $49.959$ $-1.447$ $49.870$ $-1.427$ $49.870$ $49.959$ $-1.448$ $-1.427$ $49.870$ $-1.427$ $49.959$ $-1.448$ $-1.427$ $49.870$ $-1.427$ $49.959$ $-1.448$ $-1.427$ $49.870$ $-1.427$ $49.870$ $-1.422$			KC	KC-135, Tail Number 59-1472	rail Nu	Imber	59-147	2		
tion $L^*$ at initial initial $D^*$ test test at a fact of $L^*$ at a	•		Mar-98			Jul-98			Jan-99	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Location	initial 1 *	initial *		test	test	test	test 	test	test
3     49.959     -1.513     -4.086     48.877     -1.485       5     49.517     -1.445     49.517     -1.445       7     7     49.393     -1.412     49.145       9     9     49.393     -1.445     49.263     -1.445       10     11     49.269     -1.445     49.157     -1.445       11     49.269     -1.442     49.157     -1.445       11     49.269     -1.443     -1.443       12     49.927     -1.443     -1.427       13     49.927     -1.443     -1.427       14     49.041     -1.427     -1.448       15     50.149     -1.416     -1.427       16     49.870     -1.427     -1.427       13     49.927     -1.427     -1.427       13     49.870     -1.427     -1.427       14     49.870     -1.427     -1.427       12     49.870     -1.427     -1.427       13     49.870     -1.427     -1.427       20     20     49.870     -1.427       21     22     23     -1.426       22     23     -1.428     -1.426       23     49.869     -1.422    2		J	ש		Ľ	a,	<b>.</b> 0		a"	<b>p</b> "
4       49:517       -1:445         5       49:022       -1:383         6       49:033       -1:442         9       49:157       -1:445         10       49:157       -1:445         11       49:041       -1:446         14       49:041       -1:448         15       49:041       -1:448         16       49:041       -1:448         17       49:041       -1:448         18       49:041       -1:448         16       49:041       -1:448         17       49:041       -1:427         18       49:070       -1:427         13       49:070       -1:427         13       49:870       -1:427         13       49:870       -1:427         14       49:870       -1:427         13       49:870       -1:427         14       49:870       -1:427         13       49:870       -1:427         13       49:870       -1:427         14       49:870       -1:427         13       49:870       -1:427         14       49:870       -1:427		49.959	-1.513	-4.086	48.877	-1.485	-4.018	50.060	-1.670	-4.470
5     49.022     -1.383       7     7     49.389     -1.442       8     49.269     -1.442       9     49.389     -1.445       10     49.389     -1.445       11     49.041     -1.445       14     49.041     -1.445       15     49.041     -1.445       16     49.927     -1.445       17     49.927     -1.445       18     49.041     -1.445       17     49.870     -1.445       18     49.870     -1.445       17     49.870     -1.445       18     49.870     -1.427       19     49.870     -1.427       12     49.870     -1.427       13     49.870     -1.427       20     49.870     -1.427       21     49.870     -1.427       22     52.568     -1.426       23     52.568     -0.501       23     52.568     -1.427       249.59     -1.428       23     52.568     -1.427       23     52.568     -1.426       249.59     -1.428       23     52.568     -1.427       23     52.568     -1.428					49.517	-1.445	-4.003	49.640	-1.640	-4.060
7     48.903     -1.412       8     49.269     -1.444       9     49.157     -1.455       10     49.157     -1.455       11     49.041     -1.455       15     48.981     -1.440       16     49.041     -1.443       17     49.927     -1.443       18     49.027     -1.443       17     49.927     -1.443       18     49.927     -1.443       17     49.927     -1.443       18     49.927     -1.443       17     49.927     -1.443       18     49.870     -1.427       17     49.870     -1.427       18     49.870     -1.427       12     49.870     -1.427       13     49.870     -1.427       14     49.870     -1.427       13     49.870     -1.427       20     22     52.502     -0.500       21     49.870     -1.427       22     52.502     -0.501       23     -1.423     -1.422       23     -1.416     -1.422       23     -1.423     -1.422       23     -1.416     -1.422       23     -1.423	(				49.022	-1.393	-3.697	49.110	-1.630	-4.390
7         1.462           8         49.269         -1.465           9         49.157         -1.455           10         49.269         -1.440           11         49.041         -1.455           15         50.384         -1.455           16         49.041         -1.440           17         50.384         -1.423           18         49.927         -1.448           17         49.870         -1.423           18         49.970         -1.427           17         49.870         -1.427           18         49.870         -1.427           13         49.870         -1.427           20         23         49.870         -1.427           23         23         49.612         -1.423           23         25.502         -0.500         -1.423           23         49.612         -1.423         -1.423           23         49.612         -1.423         -1.423           23         49.612         -1.423         -1.423           249.69         -1.423         -1.423         -1.423           23         49.612         -1.423	908				48.903	-1.412	-4.033	48.960	-1.430	-4.290
8     49.269     -1.444       9     10     49.157     -1.455       11     49.041     -1.408       15     50.384     -1.440       16     49.041     -1.423       17     49.041     -1.423       18     49.041     -1.423       19     50.384     -1.423       11     49.870     -1.423       12     49.870     -1.427       13     49.870     -1.427       14     49.870     -1.427       12     49.870     -1.427       20     21     49.870     -1.427       21     49.870     -1.427       22     52.502     -0.500       23     52.568     -0.501       23     52.568     -0.501       23     52.568     -1.438       13     49.612     -1.422       23     52.568     -0.501       249.613     -1.428       39     -1.438       10     49.130     -1.438       13     49.818     -1.438       14     49.130     -1.438       14     49.130     -1.438       14     49.130     -1.438       14     49.130     -1.438 <th>:µr</th> <th></th> <th></th> <th></th> <th>49.399</th> <th>-1.462</th> <th>-4.123</th> <th>52.720</th> <th>-2.010</th> <th>-4.460</th>	:µr				49.399	-1.462	-4.123	52.720	-2.010	-4.460
9       49.157       -1.455         10       48.981       -1.408         11       49.041       -1.408         15       50.384       -1.416         16       50.149       -1.415         17       50.149       -1.415         18       49.870       -1.415         17       49.870       -1.427         18       49.870       -1.427         13       49.870       -1.427         20       49.870       -1.427         21       49.870       -1.427         22       49.870       -1.427         23       23       52.502       -0.500         22       52.568       -0.501         23       52.568       -0.501         23       52.568       -0.501         23       52.568       -0.501         23       52.568       -0.501         249.613       -1.423       -1.423         749.613       -1.438       -1.438         749.613       -1.438       -1.438         749.613       -1.438       -1.438         749.613       -1.438       -1.433         749.613       -1.438	าร		:		49.269	-1.444	-4.090	53.420	-2.070	-4.450
10     48.981     -1.408       11     49.041     -1.410       15     50.384     -1.423       16     50.149     -1.423       17     49.927     -1.415       18     49.927     -1.423       17     49.870     -1.423       17     49.870     -1.423       18     49.870     -1.423       17     49.870     -1.427       18     49.870     -1.427       13     49.870     -1.427       20     20     49.870     -1.427       21     49.870     -1.427       22     52.568     -0.500       23     52.568     -0.501       23     52.568     -0.501       23     52.568     -1.438       13     49.130     -1.438					49.157	-1.455	-4.070	53.940	-2.110	-4.350
11     49.041     -1.440       14     50.384     -1.415       15     50.384     -1.415       16     49.927     -1.415       17     49.870     -1.415       18     49.870     -1.427       17     49.870     -1.427       18     49.870     -1.427       17     49.870     -1.427       13     49.870     -1.427       20     21     49.870     -1.427       21     49.870     -1.427       22     52.568     -0.500       23     52.568     -0.500       23     52.568     -0.500       23     52.568     -1.438       13     49.130     -1.438					48.981	-1.408	-4.017	52.320	-1.960	-4.500
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1				49.041	-1.440	-4.097	49.350	-0.940	-2.750
15     50.149     -1.415       19     49.927     -1.415       17     49.870     -1.427       18     49.870     -1.427       12     49.870     -1.427       13     49.870     -1.427       20     49.870     -1.427       21     49.870     -1.427       23     49.612     -1.427       23     52.502     -0.500       23     52.568     -0.501       23     52.568     -1.438       13     49.659     -1.438       14     49.612     -1.427       23     52.568     -0.501       24     49.130     -1.438       13     49.659     -1.438       14     49.130     -1.438	-				50.384	-1.423	-4.077	49.130	-1.450	-4.260
19     49.927     -1.448       17     49.870     -1.427       17     49.870     -1.427       12     49.870     -1.427       13     49.870     -1.427       20     49.870     -1.427       21     49.870     -1.427       23     49.612     -1.426       23     52.568     -0.500       23     52.568     -0.501       23     50.406     -1.438					50.149	-1.415	-4.002	50.060	-1.130	-3.580
18     49.870     -1.427       17     49.870     -1.427       16     49.870     -1.427       13     49.870     -1.427       20     49.870     -1.427       21     49.870     -1.427       22     49.612     -1.427       23     52.568     -0.500       23     52.568     -0.500       249.959     -1.513     -4.086       49.130     -1.438       6     49.130     -1.438       13     49.130     -1.438	19				49.927	-1.448	-4.035	49.290	-1.440	-4.340
17     17     49.870     -1.427       16     49.870     -1.427       12     49.870     -1.427       20     49.870     -1.427       21     49.870     -1.427       23     49.612     -1.416       23     52.502     -0.500       23     52.568     -0.501       23     52.568     -0.501       23     52.568     -1.339       13     49.959     -1.513       23     52.568     -0.501       23     52.568     -0.501       23     52.568     -0.501       249.959     -1.513     -4.086     49.130       7436     49.130     -1.438	<b>.</b>							49.090	-1.550	-4.490
16 49.870 -1.427 12 49.870 -1.427 13 49.870 -1.427 20 21 49.669 -1.416 21 49.612 -1.427 23 52.502 -0.500 22 49.612 -1.428 70.501 -1.428 8elade 49.130 -1.438 ng -1.27	<b>~</b>				49.870	-1.427	-4.047	48.930	-1.500	-4.260
12 49.870 -1.427 13 49.870 -1.427 20 21 49.612 -1.416 21 23 23 49.612 -1.416 23 49.612 -1.422 52.502 -0.500 22 49.959 -1.513 -4.086 49.818 -1.339 ng 49.130 -1.438 selade	~				49.870	-1.427	-4.047	49.050	-1.420	-4.300
13     49.870     -1.427       20     49.569     -1.416       21     49.612     -1.416       23     52.502     -0.500       23     52.568     -0.501       249.959     -1.513     -4.086     49.818     -1.339       ng     49.130     -1.438     50.406     -1.777	•				49.870	-1.427	-4.047	49.630	-1.580	-4.290
20 21 21 23 23 49.612 -1.416 49.612 -1.422 52.502 -0.500 52.568 -0.501 52.568 -1.339 1.339 ng 49.130 -1.438 50.406 -1.777 50.406 -1.777	•				49.870	-1.427	-4.047	52.670	-1.990	-4.190
21 49.612 -1.422 23 52.502 -0.500 22 49.959 -1.513 -4.086 49.818 -1.339 ng 49.130 -1.438 selade -1.77					49.569	-1.416	-3.978	49.020	-1.420	-4.230
23 52.502 -0.500 22 49.959 -1.513 -4.086 49.818 -1.339 ng 49.130 -1.438 selade -1.277					49.612	-1.422	-3.878	49.000	-1.440	-4.180
22 22 52.568 -0.501 52.568 -0.501 7 49.959 -1.513 -4.086 49.818 -1.339 ng 49.130 -1.438 selade -1.227	23				52.502	-0.500	0.300	49.080	-1.360	-4.250
49.959 -1.513 -4.086 49.818 -1.339 ng 49.130 -1.438 selade -1.222					52.568	-0.501	0.251	49.360	-1.110	-3.200
49.130 -1.438 50.406 -1.222	Average	49.959	-1.513	-4.086	49.818	-1.339	-3.588	50.237	-1.564	4.157
50 406 -1 222	Right Wing				49.130	-1.438	-4.016	51.058	-1.718	-4.191
	Right Fuselage				50.406	-1.222	-3.059	49.512	-1.481	-4.173

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Painted McClellan AFB, March 98, RIGHT SIDE

					KC.	135, T	ail N	KC-135, Tail Number 59-1472	r 59-1	1472			
			7/98-initial	nitial			1/99-7/98	86/2			1/99-1	1/99-initial	
Location		Delta L*	Delta a*	Delta b*	Delta E*	Delta L*	Delta a*	Delta b*	Delta E*	Delta I *	Delta	Delta h*	Delta
	,	000,	0000		· • • •							2	ł
ŗ		-1.082	0.028	0.068	1.084	1.183	-0.185	-0.452	1.280	0.101	-0.157	-0.384	0.427
əd	4	-0.442	0.068	0.083	0.455	0.123	-0.195	-0.057	0.237	-0.319	-0.127	0.026	0.344
	ស	-0.937	0.120	0.389	1.022	0.088	-0.237	-0.693	0.738	-0.849	-0.117	-0.304	0.909
908 1 (D	g	-1.056	0.101	0.053	1.062	0.057	-0.018	-0.257	0.264	-0.999	0.083	-0.204	1.023
	1	-0.560	0.051	-0.037	0.564	3.321	-0.548	-0.337	3.383	2.761	-0.497	-0.374	2.830
	ø	-0.690	0.069	-0.004	0.693	4.151	-0.626	-0.360	4.213	3.461	-0.557	-0.364	3.524
ųß	თ	-0.802	0.058	0.016	0.804	4.783	-0.655	-0.280	4.836	3.981	-0.597	-0.264	4.034
ы. В	10	-0.978	0.105	0.069	0.986	3.339	-0.552	-0.483	3.419	2.361	-0.447	-0.414	2.438
	11	-0.918	0.073	-0.011	0.921	0.309	0.500	1.347	1.470	-0.609	0.573	1.336	1.576
RH	14	0.425	060.0	0.009	0.435	-1.254	-0.027	-0.183	1.268	-0.829	0.063	-0.174	0.849
Motors	15	0.190	0.098	0.084	0.230	-0.089	0.285	0.422	0.517	0.101	0.383	0.506	0.643
	19	-0.032	0.065	0.051	0.089	-0.637	0.008	-0.305	0.706	-0.669	0.073	-0.254	0.719
	18									-0.869	-0.037	-0.404	0.959
əɓ	17	-0.089	0.086	0.039	0.130	-0.940	-0.073	-0.213	0.967	-1.029	0.013	-0.174	1.044
ela	16	-0.089	0.086	0.039	0.130	-0.820	0.007	-0.253	0.858	-0.909	0.093	-0.214	0.938
sn	<u>1</u> 2	-0.089	0.086	0.039	0.130	-0.240	-0.153	-0.243	0.374	-0.329	-0.067	-0.204	0.393
а 1 1	13	-0.089	0.086	0.039	0.130	2.800	-0.563	-0.143	2.860	2.711	-0.477	-0.104	2.755
	20	-0.390	0.097	0.108	0.416	-0.549	-0.004	-0.252	0.604	-0.939	0.093	-0.144	0.955
	21	-0.347	0.091	0.208	0.415	-0.612	-0.018	-0.302	0.683	-0.959	0.073	-0.094	0.966
	23	2.543	1.013	4.386	5.170	-3.422	-0.860	-4.550	5.758	-0.879	0.153	-0.164	0.907
	22	2.609	1.012	4.337	5.161	-3.208	-0.609	-3.451	4.751	-0.599	0.403	0.886	1.143
Average		-0.141	0.174	0.498	1.001	0.419	-0.226	-0.552	1.959	0.223	-0.051	-0.071	1.399
Right Wing		-0.829	0.075	0.070	0.843	1.928	-0.280	-0.175	2.204	1.099	-0.205	-0.105	1.901
Right Fuselage	¢,	0.447	0.291	1.027	1.308	-0.848	-0.252	-1.079	1.951	-0.447	0.032	-0.087	1.078

Appendix III

Painted McClellan AFB, March 98

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					Ň	-135		Tail	Num	þe	r 59-	KC-135, Tail Number 59-1472						<b></b>
Sherwin-Williams	smi	- (Right	ht Si	Side)														Τ
		Fuselage	ge	2	Fuselage	ge	e	Fuselage	age	4	Upper Wing	Wing	2 Upper	Upper Wing 3&4 Engines		5 Upper	Upper Wing Tip	
· · · · ·	Ň	-	1/99	L	7/98	1/99	<b></b>	86/2	1/99	<u>I</u>	7/98	1/99	7/98	-	1/99	7/98	1/99	
			test		test	test		test	test	1	test	test	test		test	test	test	
Pencil Hardness			r			면						2H			2H	2H	거	Γ
=	121		746 psi	·-1	S.	697 psi	<u> </u>		697 psi		1862 psi	1691 psi		15:	1592 psi	1078 psi	2	<u>.</u>
Lallure Mode: Ac	4	40 %		1	5%	30 %		10 %	10 %			50 %		4	40 %	15 %		
AP			100 %			50 %	l								5 %			
A A			T				1			1								Γ
5			T		-				60 %									Γ
Ū.	<u>छ</u>	60 %	Τ		95 %	20 %	1	% 06	30 %	!	100 %	50 %		5	55 %	85 %	20 %	
wet lape		Pass	-	$\dashv$	Pass	•	$\neg$	Pass	•	$\neg$	Pass	•				Pass	•	Γ
	-	Wing Tip	┢	5	Wing		3	Wind		4	Wind	0	2	Fiteelane				T
Chalking	ž	None		Ц	None	7	1	None	9	<b>ــــ</b>	None	9	None		9	• •		•
Spraylat (Lef	(Left Side)	(e)																
	9	Fuselage	e	2	Fuselage	ge ge	8	Fuselage	age	6	Upper Wing	Wing	7 Upper \	Upper Wing 1&2 Engines		10 Upper	Upper Wing Tip	Τ
	12	2/98	1/99		7/98	1/99	L	7/98	1/99	<b>I</b>	7/98	1/99	7/98	┝	1/99	7/98	1/90	T
	te	test	test		test	test		test	test		test	test	test		test	test	taet	
Pencil Hardness	4		ß			ß	L		m	L	2B	면			개	HB	i I	Т
티	49(	490 psi   3(	398 psi		1078 psi   7	'96 psi	Ļ	1029 psi	945 psi	-	1421 psi	896 psi		94	945 psi	882 psi	796 psi	- <sub>72</sub>
Failure Mode: AG			5%			10 %		75 %	20 %	L	10 %	50 %		47	5%	5%	5%	
			85 %		45 %	35 %								2	20 %	5 %		
AIP		+																Π
CT			10 %	1.	55 %	55 %		25 %	80 %		% 06	50 %		7	75 %	% 06	95 %	Т
Wet Tape	ă —	Pass	•		Pass		<b>L</b>	Pass		L	Pass					Pass		Τ
:		Wing Tip	Ţ	 N	Wing		33	Wing	ß	4	Wing		5	Fuselage	-			Γ
Chalking	ž	None		-	None	9		None	7		None	ω	None		80			
Pencil Hardness (Soft to Hard): Right Side - Shen	Soft to kight Sid	Hard) le - Shei		4b-3 liams	5b-4b-3b-2b-b-Hb-F-H-2H-3H-4H-5H-6H-7H-8H-9H n-Williams	H-4-9-	-2H	-3H-4H-	-5H-6H-	3-H2	H6-H		4G = Adh 4P = Adh 1TP = Adl	esion of ssion of l resion of	glue to st Primer to f Topcoat	AG = Adhesion of glue to stud or topcoat AP = Adhesion of Primer to substrate ATP = Adhesion of Topcoat to Primer		
- -	Left Side - Spraylat	e - Spray	/lat					Appe	Appendix III				CP = Cohesion of Primer CT = Cohesion of Topcoat	esion of ssion of	Primer Topcoat			
												•			•			

Large Aircraft Coatings Flight Testing

### **APPENDIX IV**

**Spraylat Paints** 

Painted McClellan AFB, March 98, LEFT SIDE

					X	KC-135,	Tail	Number	er 59.	59-1472			
39       4.0       33       1.1       1.9       1.4 $-0.5$ 4.2       5.2       5.4         36       3.4       3.3       1.1       1.9       1.4 $-0.5$ 4.2       5.2       5.4         27       2.6       2.7       1.0       1.4       1.1 $-0.1$ 4.8       5.3       4.5         27       2.6       2.7       1.0       1.4       1.1 $-0.3$ 4.2       4.3       4.0         27       2.8       2.1       2.8       1.2 $-1.6$ 5.3       5.1       4.5         27       3.2       2.1       1.1       1.6       0.3       5.2       5.9       5.9       5.9         27       2.8       1.1       1.1       1.1       1.1       1.1       4.8       5.5       4.4         27       2.8       1.1       1.1       1.1       1.1       4.8       5.5       4.4         27       5.6       2.1       1.1       1.1       2.1       4.8       5.5       4.4         27       2.6       2.1       1.1       1.1       2.1       4.8       5.5       4.4	Locat	ion	1/98 initial DFT mils	7/98 test DFT mils	1/99 test DFT mils	1/98 initial 60 degree Gloss	7/98 test 60 degree Gloss	1/99 test 60 degree Gloss	total delta 60 degree Gloss	1/98 initial 85 degree Gloss	7/98 test 85 degree Gloss	1/99 test 85 degree Gloss	total delta 85 degree Gloss
35 $4.0$ $5.3$ $1.1$ $1.9$ $1.4$ $-0.3$ $4.2$ $5.3$ $5.1$ $5.2$ 2.7       2.6       2.7       1.0 $1.4$ $1.1$ $-0.3$ $4.2$ $5.3$ $5.1$ 3.8       2.8       2.0       1.2       2.8       1.1       2.0 $4.2$ $5.3$ $5.1$ $5.3$ 2.7       2.6       2.7       1.0       1.4       1.1 $-0.3$ $4.2$ $5.3$ 2.7       2.6       2.1       1.2 $-1.1$ 1.8 $0.7$ $5.2$ $5.9$ $5.1$ $5.3$ $5.1$ $4.3$ $5.3$ $5.1$ $4.3$ $5.3$ $5.1$ $4.8$ $5.5$ $5.9$ $5.1$ $6.0$ $5.7$ $6.0$ $7.0$ $5.1$ $6.0$ $7.0$ $5.1$ $6.1$ $7.0$ $5.1$ $6.5$ $5.6$ </th <th></th> <th>5</th> <th>4</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>ľ</th> <th></th> <th></th> <th></th> <th></th>		5	4						ľ				
3.6 $3.4$ $3.8$ $1.1$ $2.0$ $1.9$ $-0.1$ $4.9$ $6.0$ $2.7$ $2.6$ $2.7$ $1.0$ $1.4$ $1.1$ $-0.3$ $4.2$ $4.3$ $5.3$ $5.1$ $5.2$ $5.3$ $5.1$ $5.2$ $5.6$ <t< td=""><td></td><td>43</td><td>3.9</td><td>4.0</td><td>3.3</td><td></td><td>1.9</td><td>4.</td><td>-0.5</td><td>4.2</td><td>5.2</td><td>5.4</td><td>0.2</td></t<>		43	3.9	4.0	3.3		1.9	4.	-0.5	4.2	5.2	5.4	0.2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	) L	44	3.6	3.4	3.8	<del>.</del>	2.0	1.9	-0.1	4.9	6.0	8.0	2.0
4 $2.6$ $3.3$ $1.1$ $2.6$ $1.2$ $-1.4$ $4.8$ $5.3$ $5.1$ $2.7$ $3.2$ $2.2$ $1.2$ $1.1$ $1.8$ $0.7$ $5.2$ $5.3$ $5.1$ $4.6$ $2.8$ $3.2$ $1.2$ $1.1$ $1.8$ $0.7$ $5.2$ $5.9$ $5.1$ $3.9$ $2.9$ $3.6$ $1.1$ $1.6$ $0.3$ $5.2$ $5.9$ $5.1$ $5.2$ $5.9$ $5.1$ $5.2$ $5.9$ $5.1$ $5.1$ $5.2$ $5.9$ $5.1$ $5.2$ $5.9$ $5.1$ $7.0$ $5.1$	ədc	45	2.7	2.6	2.7	1.0	1.4		-0.3	4.2	4.3	4.0	-0.3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		46	4	2.6	3.3	1.1	2.6	1.2	-1.4	4.8	5.3	4.5	9.9 -0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		40	3.8	2.8	2.0	1.2	2.8	1.2	-1.6	5.3	5.1	4.5	-0.6
4.6 $2.8$ $3.2$ $1.2$ $2.2$ $1.9$ $-0.3$ $5.2$ $5.9$ $3.9$ $2.9$ $3.6$ $1.1$ $1.0$ $0.9$ $-0.1$ $4.8$ $5.5$ $2.7$ $2.6$ $2.6$ $1.1$ $1.0$ $0.5$ $4.6$ $5.6$ $2.7$ $2.6$ $2.6$ $1.1$ $1.0$ $0.5$ $4.8$ $5.6$ $4.2$ $5.8$ $2.3$ $1.1$ $1.0$ $2.0$ $1.0$ $5.6$ $5.6$ $116$ $10.7$ $9.6$ $1.1$ $11.2$ $2.1$ $2.1$ $5.4$ $7.0$ $6.8$ $4.4$ $5.4$ $1.4$ $5.4$ $1.7$ $2.7$ $0.9$ $5.4$ $4.0$ $5.3$ $1.0$ $1.2$ $2.7$ $0.9$ $5.4$ $4.0$ $5.6$ <td></td> <td>39</td> <td>2.7</td> <td>3.2</td> <td>2.2</td> <td>1.2</td> <td>1.1</td> <td>1.8</td> <td>0.7</td> <td>5.2</td> <td>5.9</td> <td>4.5</td> <td>-1.4</td>		39	2.7	3.2	2.2	1.2	1.1	1.8	0.7	5.2	5.9	4.5	-1.4
3.9       2.9       3.6       1.1       1.0 $0.9$ $-0.1$ 4.8       5.5         2.7       2.6       2.6       1.1       1.5       1.0 $-0.5$ 4.6       5.6       5.5         4.2       5.8       2.3       1.1       1.0       2.0       1.0       5.0       5.5       5.6	Цэ-	38	4.6	2.8	3.2	1.2	2.2	1.9	-0.3	5.2	5.9	5.9	0.0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	37	3.9	2.9	3.6	1.1	1.0	0.9	-0.1	4.8	5.5	4.2	-1.3
4.2 $5.8$ $2.3$ $1.1$ $1.0$ $2.0$ $1.0$ $5.4$ $7.0$ $5.5$ $11.6$ $10.7$ $9.6$ $1.1$ $11.2$ $2.1$ $-9.1$ $5.4$ $7.0$ $5.5$ $11.6$ $10.7$ $9.6$ $1.1$ $11.2$ $2.1$ $-9.1$ $5.4$ $7.0$ $6.4$ $5.1$ $1.2$ $4.1$ $5.5$ $1.6$ $-3.7$ $7.3$ $7.0$ $6.4$ $5.1$ $1.2$ $4.1$ $1.2$ $4.1$ $7.3$ $7.0$ $6.4$ $5.1$ $1.2$ $4.1$ $1.2$ $4.1$ $1.2$ $4.1$ $7.3$ $7.0$ $4.5$ $5.1$ $1.2$ $4.1$ $1.6$ $-2.5$ $5.4$ $4.6$ $6.6$ $4.3$ $0.9$ $1.0$ $1.1$ $2.1$ $2.5$ $5.4$ $6.6$ $5.1$ $4.0$ $5.1$ $4.0$ $5.1$ $4.0$ $5.1$ $4.0$ $5.1$ $4.0$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$		36	2.7	2.6	2.6	+	1.5	1.0	-0.5	4.6	5.6	4.2	4
11 $9.7$ $9.6$ $1.1$ $11.2$ $2.1$ $-9.1$ $5.4$ $7.0$ 11.6 $10.7$ $9.6$ $1.1$ $5.5$ $1.6$ $-3.9$ $5.1$ $6.2$ $6.8$ $4.4$ $5.4$ $1.7$ $-3.7$ $7.3$ $7.0$ $6.8$ $5.1$ $1.2$ $4.1$ $1.6$ $-3.9$ $5.1$ $6.5$ $5.8$ $4.7$ $5.1$ $1.2$ $4.1$ $1.6$ $-2.5$ $5.4$ $6.6$ $4.6$ $5.8$ $1.2$ $2.2$ $1.6$ $-2.5$ $5.4$ $6.6$ $6.6$ $4.2$ $5.8$ $1.2$ $2.2$ $0.9$ $0.6$ $3.5$ $4.0$ $5.4$ $4.0$ $3.6$ $3.5$ $4.0$ $3.5$ $4.0$ $3.5$ $4.0$ $5.1$ $4.1$ $5.1$ $1.6$ $1.6$ $1.6$ $1.3$ $5.1$ $4.7$ $5.1$ $4.7$ $5.1$ $4.7$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ <		35	4.2	5.8	2.3	÷.	1.0	2.0	1.0	5.0	5.5	4.4	-1.1
11.6       10.7       9.6       1.1 $5.5$ 1.6 $-3.9$ $5.1$ $6.2$ $6.4$ $5.1$ $5.1$ $1.2$ $4.1$ $5.4$ $1.7$ $-3.7$ $7.3$ $7.0$ $5.8$ $4.7$ $5.1$ $1.2$ $4.1$ $1.6$ $-3.9$ $5.1$ $6.2$ $5.8$ $4.7$ $1.2$ $4.5$ $5.4$ $1.7$ $-3.7$ $7.3$ $7.0$ $4.6$ $5.8$ $5.3$ $1.0$ $1.2$ $4.5$ $5.4$ $1.7$ $-3.7$ $7.0$ $4.5$ $5.8$ $5.3$ $1.0$ $1.8$ $2.7$ $0.9$ $3.5$ $4.0$ $3.5$ $4.0$ $3.5$ $4.0$ $3.5$ $4.0$ $3.5$ $4.0$ $3.5$ $4.0$ $3.5$ $4.0$ $3.5$ $4.0$ $5.4$ $4.0$ $3.5$ $4.0$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$ $5.1$	E		11	9.7	9.6	1.1	11.2	2.1	-9.1	5.4	7.0	5.6	-1.4
	Motors		11.6	10.7	9.6	1.1	5.5	1.6	-3.9	5.1	6.2	4.7	-1.5
		32	6.8	4.4	5.4	1.4	5.4	1.7	-3.7	7.3	7.0	4.6	-2.4
5.8 $4.7$ $1.2$ $4.5$ $4.5$ $5.8$ $4.7$ $1.2$ $4.5$ $5.8$ $4.7$ $1.2$ $4.5$ $5.8$ $5.3$ $1.0$ $1.8$ $2.7$ $0.9$ $3.5$ $4.0$ $4.5$ $5.8$ $5.3$ $5.3$ $5.3$ $5.3$ $5.3$ $5.3$ $5.3$ $5.3$ $5.3$ $5.3$ $5.3$ $5.3$ $5.3$ $2.7$ $0.9$ $3.5$ $4.0$ $4.5$ $5.3$ $2.7$ $0.9$ $3.5$ $4.0$ $4.5$ $5.3$ $2.7$ $0.9$ $3.5$ $4.0$ $4.5$ $5.3$ $2.7$ $0.9$ $0.6$ $1.2$ $1.6$ $0.0$ $0.1$ $1.8$ $2.7$ $5.1$ <th< td=""><td></td><td>31</td><td>6.4</td><td>5.1</td><td>5.1</td><td>1.2</td><td>4.1</td><td>1.6</td><td>-2.5</td><td>5.4</td><td>6.6</td><td>4.4</td><td>-2.2</td></th<>		31	6.4	5.1	5.1	1.2	4.1	1.6	-2.5	5.4	6.6	4.4	-2.2
4.6 $5.8$ $1.2$ $2.2$ $4.5$ $5.3$ $1.0$ $1.8$ $2.7$ $0.9$ $3.5$ $4.0$ $4.5$ $5.3$ $2.9$ $1.0$ $1.8$ $2.7$ $0.9$ $3.5$ $4.0$ $4.5$ $5.3$ $2.9$ $1.0$ $1.8$ $2.7$ $0.9$ $3.5$ $4.0$ $4.3$ $4.0$ $3.6$ $1.0$ $1.9$ $2.3$ $0.4$ $4.7$ $5.1$ $5.4$ $4.0$ $3.6$ $1.0$ $1.9$ $2.3$ $0.6$ $4.7$ $5.1$ $5.4$ $4.0$ $3.8$ $0.8$ $0.9$ $1.2$ $1.3$ $0.1$ $1.8$ $2.7$ $5.1$ $4.9$ $5.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.3$ $3.5$ <td></td> <td>34</td> <td>5.8</td> <td>4.7</td> <td></td> <td>1.2</td> <td>4.5</td> <td></td> <td></td> <td>4.8</td> <td>5.8</td> <td></td> <td></td>		34	5.8	4.7		1.2	4.5			4.8	5.8		
4.2 $5.8$ $5.3$ $1.0$ $1.8$ $2.7$ $0.9$ $3.5$ $4.0$ $4.5$ $5.3$ $2.9$ $1.0$ $1.8$ $2.7$ $0.9$ $3.5$ $4.0$ $4.3$ $4.0$ $3.6$ $1.0$ $1.9$ $2.3$ $0.4$ $4.7$ $5.1$ $5.4$ $4.0$ $4.3$ $0.9$ $1.2$ $1.3$ $0.4$ $4.7$ $5.1$ $5.4$ $4.0$ $4.3$ $0.9$ $1.2$ $1.3$ $0.1$ $1.8$ $3.2$ $3.5$ $3.5$ $4.0$ $5.4$ $4.0$ $3.8$ $0.8$ $0.9$ $1.6$ $1.3$ $0.1$ $1.8$ $4.9$ $4.4$ $3.0$ $3.5$ $0.9$ $1.6$ $1.6$ $1.6$ $1.3$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $2.1$ $1.1$	(	33	4.6	5.8		1.2	2.2			4.5	5.8		
4.5 $5.3$ $2.9$ $1.0$ $1.9$ $2.3$ $0.4$ $4.7$ $5.1$ $4.3$ $4.0$ $3.6$ $1.0$ $1.9$ $2.3$ $0.4$ $4.7$ $5.1$ $5.4$ $4.0$ $3.6$ $1.0$ $1.9$ $2.3$ $0.4$ $4.7$ $5.1$ $5.4$ $4.0$ $3.8$ $0.9$ $1.2$ $1.3$ $0.1$ $1.8$ $4.9$ $5.4$ $4.0$ $3.8$ $0.8$ $0.9$ $1.2$ $1.3$ $0.1$ $1.8$ $4.9$ $5.4$ $4.0$ $3.8$ $0.8$ $0.9$ $1.6$ $1.13$ $0.1$ $1.18$ $4.9$ $2.7$ $3.5$ $0.9$ $1.6$ $1.6$ $0.0$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $1.1$ $2.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ $3.1$ <td>əđe</td> <td>42</td> <td>4.2</td> <td>5.9</td> <td>5.3</td> <td>1.0</td> <td>1.8</td> <td>2.7</td> <td>0.9</td> <td>3.5</td> <td>4.0</td> <td>3.7</td> <td>-0.3</td>	əđe	42	4.2	5.9	5.3	1.0	1.8	2.7	0.9	3.5	4.0	3.7	-0.3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	: əs	41	4.5	5.3	2.9	1.0	1.9	2.3	0.4	4.7	5.1	3.9	-1.2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	n J	30	4.3	4.0	3.6	1.0	2.4	1.6	-0.8	3.2	3.5	2.4	-1.1
5.4       4.0       3.8       0.8       0.9       1.8       0.9       1.3         4.4       3.0       3.5       0.9       1.6       1.3       0.9       0.6       1.3         4.4       3.0       3.5       0.9       1.6       1.6       1.1       2.1       2.1       2.1       2.1       2.1       3.1       2.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       1.2       1.2       1.2       1.2       1.2       1.1       2.1       1.2       1.1       1.1       2.1       1.2       1.2       3.1       1.1       1.2       1.2       3.1       1.1       1.2       1.2       3.1       1.1       1.2       1.2       3.1       1.1       1.2       1.2       1.2       1.2       1.2       1.2       1.2       1.2       1.2       1.2       1.2       1.2       1.2       1.2       1.2       3.1       1.2       3.1       1.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3	IJ9.	29	5.4	4.0	4.3	0.9	1.2	1.3	0.1	1.8	4.9	2.8	-2.1
4.4       3.0       3.5       0.9       1.6       1.6       0.0       1.1       2.1         2.7       2.7       6.8       6.8       1.6       1.1       2.1       3.1         5.0       4.5       4.1       1.1       2.7       1.6       1.1       2.1         3.61       3.61       1.1       2.7       1.6       -1.0       4.3       5.2	7	28	5.4	4.0	3.8	0.8	0.9	1.8	0.9	0.6	1.3	1.6	0.3
2.7       6.8       3.1         2.7       1.2       1.2         5.0       4.5       4.1       1.1         3.61       3.61       1.6       -1.0       4.3       5.2		27	4.4	3.0	3.5	0.9	1.6	1.6	0.0	1.1	2.1	1.9	-0.2
2.7         1.2         1.2         1.7         1.7           5.0         4.5         4.1         1.1         2.7         1.6         -1.0         4.3         5.2           3.61		47					6.8				3.1		
5.0 4.5 4.1 1.1 2.7 1.6 -1.0 4.3 5.2 3.61		48		Î			1.2				1.7		
	Average		5.0	4.5	4.1	1.1	2.7	1.6	-1.0	4.3	5.2	4.3	-0.8
Left Fuselage	Left Win	ß	3.61										
	Left Fust	elage											

Appendix IV

**Spraylat Paints** 

Mar-96         Mar-96         Jul-96         Jul-96         Jan-96         Jan-96           Location         Initial L         "<				KC	KC-135, Tail Number 59-1472	ail Nu	mber {	59-147	2		
				Mar-98			Jul-98			Jan-99	
43 $49.959$ $-1.513$ $4.086$ $49.516$ $-1.090$ $-3.281$ $49.040$ $-0.750$ 44         44         49.124         -0.906 $49.516$ -1.090 $-3.281$ $49.610$ $-0.750$ 45         49.124         -0.906 $2.073$ $50.410$ $-0.750$ 33         49.959         -1.513         4.086 $-0.790$ $-3.661$ $-0.790$ 36         49.124         -0.906 $-3.261$ $50.410$ $-0.790$ 37         49.925         -1.1206 $-3.561$ $-1.600$ $-3.661$ $-1.020$ 36 $-1.206$ $-3.261$ $-1.206$ $-3.261$ $-1.020$ 37 $-0.920$ $-1.206$ $-3.561$ $-1.600$ $-0.900$ 36 $-1.1206$ $-3.561$ $-1.600$ $-0.900$ $-0.910$ 38 $-0.190$ $-3.561$ $-1.020$ $-3.561$ $-1.020$ 31 $-0.500$ $-1.206$ $-3.510$ $49.950$ $-1.600$ <tr< th=""><th>Locat</th><th>ion</th><th>initial I *</th><th>initial</th><th>initial</th><th>test</th><th>test</th><th>test</th><th>test</th><th>test</th><th>test</th></tr<>	Locat	ion	initial I *	initial	initial	test	test	test	test	test	test
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	500		1	a*	°*	<b>*</b> _	a*	*a	<b>.</b>	n*	<b>م</b> *
44         49.124 $0.306$ $2.073$ $50.410$ $0.570$ 66         48.800 $-1.022$ $2.561$ $49.610$ $0.780$ 66         50.235 $-1.080$ $-3.63$ $50.610$ $-1.650$ 68         50.2112 $-1.190$ $-3.563$ $50.610$ $-1.020$ 68         50.112 $-1.190$ $-3.563$ $50.610$ $-1.020$ 69 $-1.190$ $-3.563$ $50.610$ $-1.020$ 60 $-49.820$ $-1.190$ $-3.563$ $50.610$ $-1.020$ 60 $-49.820$ $-1.190$ $-3.563$ $50.210$ $-1.020$ 60 $-49.820$ $-1.166$ $-3.800$ $49.850$ $-0.900$ 61 $-1.058$ $-3.515$ $49.990$ $-0.900$ $-0.900$ 60 $-1.056$ $-1.056$ $-3.515$ $49.990$ $-0.900$ 7 $-1.058$ $-3.515$ $49.990$ $-0.900$ $-0.900$ 7 $-1.055$		43	49.959	-1.513	-4.086	49.516	-1.090	-3.228	49.040	-0.750	-1.370
	r	44				49.124	-0.906	-2.073	50.410	-0.570	-1.440
	əde	45				48.800	-1.022	-2.591	49.610	-0.790	-2.590
		40				49.235	-1.089	-3.269	49.850	-1.650	-4.500
39         50.112         -1.190         -3.563         50.610         -1.020           37         49.901         -1.206         -3.580         50.370         -1.000           36         49.602         -1.085         -3.748         50.210         -0.900           35         50         -1.085         -3.774         49.990         -0.970           35         50         50.141         -1.035         -3.276         49.990         -0.900           36         49.477         -1.033         -3.276         49.990         -0.900         -0.900           31         50         50.256         -1.146         -3.800         49.960         -0.900           31         50.256         -1.146         -3.800         49.960         -0.920           32         50.207         -1.057         -3.515         49.970         -1.650           33         50.207         -1.023         -3.515         49.970         -1.650           33         49.503         -0.927         -3.041         49.700         -0.990           41         49.902         -9.973         -3.244         49.700         -1.090           27         49.9302         -1.023 <th></th> <th>40</th> <th></th> <th></th> <th></th> <th>50.298</th> <td>-1.229</td> <td>-3.661</td> <td>51.690</td> <td>-0.840</td> <td>-2.760</td>		40				50.298	-1.229	-3.661	51.690	-0.840	-2.760
38     50.870     -1.000       37     49.991     -1.206     -3.580     50.870     -1.000       36     49.829     -1.197     -3.488     50.210     -0.900       35     49.602     -1.085     -3.274     49.990     -0.970       36     50.141     -1.030     -3.800     49.850     -0.930       31     50.141     -1.058     -3.600     49.850     -0.930       32     50.141     -1.053     -3.515     49.970     -1.480       33     50.141     -1.053     -3.515     49.970     -1.600       34     50.155     -1.057     -3.515     49.970     -1.600       33     49.900     -0.927     -3.615     49.970     -1.600       34     49.503     -0.973     -3.515     49.970     -1.650       30     49.503     -0.973     -3.224     51.140     -1.090       31     49.963     -0.517     -1.023     -3.515     49.970     -1.650       32     49.963     -0.9103     -1.148     -1.148     -1.148     -1.148       33     49.963     -0.913     -1.212     49.970     -1.650     -1.650       32     49.963     -1.1182     -3.324		90 90				50.112	-1.190	-3.563	50.610	-1.020	-2.690
37     49.829     -1.197     -3.498     50.210     -0.900       36     49.602     -1.085     -3.274     49.990     -0.970       35     49.477     -1.030     -3.276     49.9850     -0.970       49     50.141     -1.058     -3.800     49.850     -0.970       30     50.141     -1.058     -3.512     49.980     -0.920       31     50.155     -1.057     -3.512     49.980     -0.920       32     50.161     -1.057     -3.512     49.980     -0.920       33     50.207     -1.023     -3.515     49.970     -1.650       34     49.902     -0.973     -3.224     49.70     -1.090       30     50.207     -1.023     -3.214     49.70     -0.900       31     49.503     -0.973     -3.224     49.70     -0.900       32     49.503     -0.973     -3.224     49.70     -0.900       30     22     -1.162     -3.748     49.70     -0.900       31     49.503     -0.973     -3.224     49.70     -0.900       32     49.503     -0.973     -3.224     49.70     -0.900       23     49.555     -1.162     -3.71 <td< th=""><th></th><th>ထ္လိ</th><th></th><th></th><th></th><th>49.991</th><td>-1.206</td><td>-3.580</td><td>50.870</td><td>-1.000</td><td>-2.900</td></td<>		ထ္လိ				49.991	-1.206	-3.580	50.870	-1.000	-2.900
36     49.602     -1.085     -3.274     49.990     0.970       35     49.477     -1.030     -3.276     49.990     0.970       50     50.141     -1.030     -3.576     49.850     0.930       31     50.141     -1.058     -3.603     49.250     -1.480       32     50.141     -1.058     -3.663     49.250     -1.480       33     50.155     -1.057     -3.515     49.970     -1.650       33     42     50.207     -1.023     -3.515     49.970     -1.650       33     42     50.207     -1.023     -3.515     49.970     -1.650       33     42     -1.023     -3.515     49.970     -1.650       33     49.503     -0.973     -3.224     51.140     -1.090       30     49.503     -0.973     -3.224     49.100     -1.650       30     49.503     -0.973     -3.224     49.100     -1.990       21     49.960     -1.650     -1.217     49.130     -1.210       21     49.503     -0.973     -3.224     49.160     -0.990       21     49.555     -1.1022     -3.448     49.160     -0.990       21     49.555     -1	ļ97	37				49.829	-1.197	-3.498	50.210	-0.900	-2.670
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1	30 30				49.602	-1.085	-3.274	49.990	-0.970	-2.720
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		35				49.477	-1.030	-3.276	49.990	-0.970	-2.720
50         50.141         -1.058         -3.663         49.250         -1.480           31         50.155         -1.057         -3.512         49.880         -0.920           31         50.207         -1.023         -3.515         49.970         -1.650           32         50.207         -1.023         -3.515         49.970         -1.650           34         49.902         -0.927         -3.041         1.650         -1.650           34         49.902         -0.927         -3.041         1.650         -1.650           34         49.902         -0.973         -3.224         51.140         -1.090           41         49.503         -0.973         -3.224         49.500         -0.930           30         49.503         -0.973         -3.224         49.70         -1.090           30         49.503         -0.973         -3.224         49.70         -0.930           31         49.503         -1.032         -1.210         -1.210           26         -1.162         -3.331         49.160         -0.930           27         49.955         -1.137         -1.217         -1.210           49.956         -1.513<	Ξ	49				50.256	-1.146	-3.800	49.850	-0.930	-3.300
32       50.155       -1.057       -3.512       49.880       -0.920         31       50.207       -1.023       -3.515       49.970       -1.650         32       50.207       -1.023       -3.515       49.970       -1.650         33       41       49.902       -0.927       -3.041       1.650         42       49.902       -0.927       -3.041       49.970       -1.650         30       49.503       -0.973       -3.224       51.140       -1.090         41       49.503       -0.973       -3.224       51.140       -1.090         30       30       49.503       -1.032       -3.448       49.870       -0.930         22       49.382       -1.032       -3.448       49.160       -0.920         23       49.555       -1.162       -3.576       49.160       -0.920         24       49.555       -1.162       -3.514       49.160       -0.920         24       49.556       0.464       1.217       49.160       -0.920         27       49.566       0.464       1.217       49.160       -0.920         27       49.556       -1.162       -3.534       49.166	Motors	20				50.141	-1.058	-3.663	49.250	-1.480	-4.440
31       50.207       -1.023       -3.515       49.970       -1.650         34       50.207       -1.023       -3.515       49.970       -1.650         42       49.902       -0.927       -3.041       10.900       -1.650         41       49.503       -0.973       -3.224       51.140       -1.090         29       49.503       -0.973       -3.224       51.140       -1.090         20       49.503       -0.973       -3.224       51.140       -1.090         20       49.503       -0.973       -3.224       51.140       -1.090         20       49.503       -0.973       -3.224       49.260       -0.890         20       49.503       -1.032       -3.376       49.160       -1.210         21       49.555       -1.162       -3.331       49.160       -0.920         21       49.959       -1.162       -3.351       49.160       -0.920         21       49.959       -1.102       -3.254       49.160       -0.920         21       49.956       -1.102       -3.254       49.160       -0.920         21       49.956       -1.102       -3.254       49.160 <t< th=""><th></th><th>32</th><th></th><th></th><th></th><th>50.155</th><td>-1.057</td><td>-3.512</td><td>49.880</td><td>-0.920</td><td>-3.190</td></t<>		32				50.155	-1.057	-3.512	49.880	-0.920	-3.190
34       50.207       -1.023       -3.515		31				50.207	-1.023	-3.515	49.970	-1.650	-4.240
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		34				50.207	-1.023	-3.515			
	əl	33				49.902	-0.927	-3.041			
	961	42				49.503	-0.973	-3.224	51.140	-1.090	-2.980
30       30       49.382       -1.032       -3.448       49.870       -0.930         29       28       49.525       -1.162       -3.576       49.130       -1.210         27       49.525       -1.162       -3.831       49.160       -0.920         47       47.156       0.464       1.217       49.160       -0.920         48       49.059       -1.513       -4.086       49.644       -1.010       -3.584       -1.025         1       49.959       -1.513       -4.086       49.644       -1.085       -3.351       49.988       -1.025         1       49.959       -1.513       -4.086       49.598       -1.104       -3.201       50.227       -0.946         1       49.585       -0.917       -3.023       49.773       -1.087	əsi	4				49.503	-0.973	-3.224	49.260	-0.890	-2.650
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ı Fu						1 055	077 C			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	l9-	a c				200.04	200.1-	044.0	10.01	-0.850	-3.200
47     49.1/3     -1.3/4     -3.831     49.160     -0.920       47     48     0.464     1.217     49.160     -0.920       48     50.117     -1.002     -3.584     49.160     -0.920       48     50.117     -1.002     -3.584     49.988     -1.025       49.959     -1.513     -4.086     49.644     -1.085     -3.351     49.988     -1.025       1     49.598     -1.104     -3.201     50.227     -0.946       1     49.585     -0.917     -3.023     49.773     -1.087	1	2 F 7 C				10.120 1011 101	-1.102	-6.070	48.130	-1.210	-3.360
4/     47.156     0.464     1.217       48     50.117     -1.002     -3.584       49.959     -1.513     -4.086     49.644       1     49.598     -1.104     -3.201     50.227       1     -1.035     -3.023     49.773     -1.086		7				49.773	-1.374	-3.831	49.160	-0.920	-3.100
48         50.117         -1.002         -3.584         10.118         -1.025         -3.584         10.118         -1.025		47				47.156	0.464	1.217			
49.959         -1.513         -4.086         49.644         -1.085         -3.351         49.988         -1.025           1         49.598         -1.104         -3.201         50.227         -0.946           1         49.585         -0.917         -3.023         49.773         -1.087		48				50.117	-1.002	-3.584			
49.598 -1.104 -3.201 50.227 -0.946 49.585 -0.917 -3.023 49.773 -1.087	Average		49.959	-1.513	-4.086	49.644	-1.085	-3.351	49.988	-1.025	-2.991
49.585 -0.917 -3.023 49.773 -1.087	Left Wing					49.598	-1.104	-3.201	50.227	-0.946	-2.636
	Left Fusel	age				49.585	-0.917	-3.023	49.773	-1.087	-3.246

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Painted McClellan AFB, March 1998, LEFT SIDE

**Spraylat Paints** 

Painted McClellan AFB, March 98, LEFT SIDE

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				KC-'	135, 1	ail N	Tail Number 59-1472	ir 59-'	1472				
			7/98-	7/98-initial			1/99	1/99-7/98			1/99-	1/99-initial	
Location	tion	Delta L*	Delta a*	Deita <b>b</b> *	Delta E*	Delta L*	Delta a*	Delta <b>b</b> *	Delta E*	Delta L*	Deita a*	Delta b*	Delta E*
	43	-0.443	0.423	0.858	1.054	-0.476	0.340	1.858	1.948	-0.919	0.763	2.716	2.967
Ļ	44	-0.835	0.607	2.013	2.262	1.286	0.336	0.633	1.472	0.451	0.943	2.646	2.845
ıəd	45	-1.159	0.491	1.495	1.954	0.810	0.232	0.001	0.843	-0.349	0.723	1.496	1.698
e Nbi	46	-0.724	0.424	0.817	1.171	0.615	-0.561	-1.231	1.486	-0.109	-0.137	-0.414	0.449
эе, 6'	40	0.339	0.284	0.425	0.613	1.392	0.389	0.901	1.703	1.731	0.673	1.326	2.282
	39	0.153	0.323	0.523	0.633	0.498	0.170	0.873	1.019	0.651	0.493	1.396	1.617
	38	0.032	0.307	0.506	0.593	0.879	0.206	0.680	1.130	0.911	0.513	1.186	1.581
19-	37	-0.130	0.316	0.588	0.680	0.381	0.297	0.828	0.959	0.251	0.613	1.416	1.563
1	36	-0.357	0.428	0.812	0.985	0.388	0.115	0.554	0.686	0.031	0.543	1.366	1.470
	35	-0.482	0.483	0.810	1.059	0.513	0.060	0.556	0.759	0.031	0.543	1.366	1.470
гн	49	0.297	0.367	0.286	0.552	-0.406	0.216	0.500	0.679	-0.109	0.543	0.786	0.962
Motors	50	0.182	0.455	0.423	0.647	-0.891	-0.422	-0.777	1.255	-0.709	0.033	-0.354	0.793
	32	0.196	0.456	0.574	0.759	-0.275	0.137	0.322	0.445	-0.079	0.593	0.896	1.077
	31	0.248	0.456	0.571	0.772	-0.237	-0.627	-0.725	0.987	0.011	-0.137	-0.154	0.206
	34	0.248	0.490	0.571	0.792								
9	33	-0.057	0.586	1.045	1.199								
6e	42	-0.456	0.540	0.862	1.115	1.637	-0.117	0.244	1.659	1.181	0.423	1.106	1.672
əs	41	-0.456	0.540	0.862	1.115	-0.243	0.083	0.574	0.629	-0.699	0.623	1.436	1.714
nj	30												
1	29	-0.577	0.481	0.638	0.986	0.488	0.102	0.248	0.557	-0.089	0.583	0.886	1.064
•7	28	-0.434	0.351	0.510	0.756	-0.395	-0.048	0.216	0.453	-0.829	0.303	0.726	1.143
	27	-0.186	0.139	0.255	0.345	-0.613	0.454	0.731	1.057	-0.799	0.593	0.986	1.401
	47	-2.803	1.977	5.303	6.316								
	48	0.158	0.511	0.502	0.734								
Average		-0.315	0.497	0.924	1.178	0.282	0.072	0.368	1.038	0.029	0.486	1.095	1.472
Left Wing		-0.361	0.409	0.885	1.101	0.629	0.158	0.565	1.201	0.268	0.567	1.450	1.794
Left Fuselage	ge	-0.374	0.593	1.063	1.353	0.052	-0.002	0.230	0.827	-0.186	0.426	0.831	1.183

## Large Aircraft Coatings Flight Testing

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### APPENDIX V

Painted Tinker AFB, May 97, RIGHT SIDE

r	1	· · · · · · · · · · · · · · · · · · ·	1
	total delta 85 degree Gloss	3.4 3.6 3.6 3.6 5.5 5.7 4.7 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7	-0.4 -0.4 -1.2
	2/99 test 85 degree Gloss	8.8 5.7 5.7 5.6 5.6 5.5 6.1 8.8 7.3 8.6 7.3 7.3 5.8 7.3 5.8	6.2 7.0 5.6
÷	7/98 test 85 degree Gloss	9.8 11.8 11.1 7.7 6.5 6.3 8.3 8.3 8.3 8.3 8.9 6.9 6.9 6.9 6.9 8.5 8.5 8.5 8.5 8.5 8.5	7.6 8.3 7.1
38	1/98 initial 85 degree Gloss	5.7 7.9 6.5 7.0 7.0 7.3 6.1 7.5 6.1 7.5 7.5 7.5 7.5 7.5 7.5 9.1 9.1	6.7 6.8 6.8
Tail No. 64-14838	total delta 60 degree Gloss		-3.3 -2.3 4.2
No. 64	2/99 test 60 degree Gloss	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.3 2.4 2.3
Tail <b>N</b>	7/98 test 60 degree Gloss	3.2 3.2 3.3 3.3 3.3 3.3 3.4 4.9 3.3 3.0 3.5 3.5 3.5 4.9 5.0 4.0 4.0 5.1 5.0 4.9 6.1 6.1 7.0 7.0 8.4 8.4 8.4 8.4 9.7 7.0 8.4 8.4 9.7 7.0 8.4 7.0 8.4 8.4 7.0 8.4 8.4 8.4 8.4 8.4 8.4 8.4 8.4 8.4 8.4	4.0 3.3 4.5
KC-135,	1/98 initial 60 degree Gloss	4.0 4.4 4.4 7.3 4.7 7.4 4.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7	5.6 6.5 6.5
KC.	2/99 test DFT mils	33 33 33 33 33 33 34 34 35 35 35 35 35 35 35 35 35 35 35 35 35	5.3 3.8 3.3
	7/98 test DFT mils	3.6 3.6 3.6 4.7 5.0 5.7 5.0 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.2	5.4 5.6
	1/98 initial DFT mils		5.9 5.9
	Location	Right Fuselage Surface Surf	Average Wing Fuselage

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DFT = Dry Film Thickness

Appendix V

**US Paint** 

Painted Tinker AFB, May 97, LEFT SIDE

total delta 85 degree Gloss 0.0 0.1 8.0 -2.9 4.4 - 1.0 0.0 4.0 4.0 -1.6 0.0 1.2 -0.8 -1.8 0.2 -1.0 -1.6 0.5 0.5 4. 0.1 -5.1 degree Gloss 2/99 test 85 6.9 7.1 7.7 7.7 6.0 2.8 2.8 5.6 4.7 5.3 6.6 4.0 degree Gloss 7/98 test 85 6.0 10.4 9.4 5.8 5.8 6.1 7.5 5.0 6.**4** 5.8 6.3 5.3 6.2 5.7 6.9 5.0 5.2 5.0 6.4 4.3 6.4 2.9 3.3 5.6 5.3 degree Gloss 1/98 initial 85 6.4 5.3 5.8 7.9 6.0 5.6 3.9 9.8 7.6 5.0 4.2 4.8 4.5 4.5 4.5 5.9 8.9 5.7 5.7 5.4 5.4 5.1 5.1 3.4 5.2 KC-135, Tail No. 64-14838 degree Gloss total delta 60 -1.8 -1.5 -1.5 -1.6 -1.9 -2.8 -2.6 -2.8 -3.6 -2.3 -1.8 -1.5 -1.5 -1.5 -1.5 -3.6 -2.0 -2 7 -2 7 -2 7 4 -1.4 -2.4 degree Gloss 2/99 test 60 2.0 2.5 1.3 1.3 1.4 1.7 2.1 2.1 degree Gloss 7/98 test 60 3.2 3.6 3.7 2.2.6.2.4 3.9 3.1 3.5 3.5 3.7 5.0 3.7 3.1 1/98 initial 60 degree Gloss 3.8 4.6 3.8 а. 8 3.9 4.5 3.8 6.2 3.5 4.6 5.8 **6**. 5.9 4.3 5 2 5 3.1 2/99 test DFT mils 9.2 10.7 4.5 4.5 ÷. 4.0 5.5 5.6 3.6 4.0 44 7/98 test DFT mils 10.0 10.0 4.3 4.0 5.0 5.7 6.0 3.5 4.0 3.5 2.3 2.2 4.5 3.5 4.0 3.7 1/98 initial DFT mils 2.6 2.9 2.5 2.8 2.8 2.8 3.4 3.6 9 0.0 9 0.0 9 0.0 9 0.0 9 0.0 9 0.0 9 0.0 9 0.0 9 0.0 9 0.0 9 0.0 5.9 5.0 3.0 4.5 4.2 3.2 4.0 5.9 3.1 3.4 Location Wing Fuselage Average Motors Surface apelazu7 ffe Left Wing, Upper

**US Paint** 

DFT = Dry Film Thickness

Painted Tinker AFB, May 97, RIGHT SIDE

4.330 4.100 4.270 -4.510 -4.300 -4.060 4.390 4.130 4.080 4.100 4.420 -4.260 test Feb-99 -1.970 -1.980 -1.940 -1.880 -1.880 -1.920 -2.040 -2.100 -2.290 -2.030 -1.940 -1.940 **a**, test 51.700 52.300 52.720 52.880 52.100 51.940 54.260 53.180 55.210 51.940 52.730 51.440 test **\***\_\_\_ KC-135, Tail No. 64-14838 -4.220 -4.322 -4.158 -4.240 -4.183 -3.692 -3.799 -4.222 -4.386 -3.792 -3.911 -4.331 test **\***0 -1.859 -1.810 -1.846 -1.866 -1.574 Jul-98 -1.579 -1.816 -1.603 -1.692 -1.697 -1.582 -1.522 test **"** 48.319 51.465 50.096 48.614 51.458 51.613 49.904 50.674 51.517 51.653 49.254 48.757 test ٹ -3.648 -3.645 -3.806 -3.812 -3.758 -3.640 -3.744 -3.818 -3.696 -3.931 initial م\* -1.422 Jan-98 -1.368 -1.368 -1.347 -1.472 -1.375 -1.393 -1.393 -1.375 -1.350 initial a, 49.716 50.018 49.875 49.316 48.665 49.952 49.895 50.157 49.821 initial 49.331 ٹـ 10 4 5 თ S ø ດ ന ഗ ~ 4 Location RH Motors Surface Right Wing, Upper

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4.070

54.220 54.300 54.280 53.280

-4.263

-1.882

51.488

-3.628

-3.744

49.895 49.884 50.157 49.801

Q 2 33

49.844

-4.263

-1.882

51.488

-3.640 -3.652 -3.652 -3.533 3.573 -3.698

4.185

-1.764

50.960

-1.363 -1.363

20 5

apsiazu¶ trigiA

4.171 4.171

-1.789 -1.789 -1.775 -1.746

51.077

4.180

4.350 4.390 4.490

4.390 4.350

54.050

54.070

-4.337

-1.811

4.550

-2.130 -2.080 -2.090 -2.030 -2.060 -2.040 -2.010 2.080 -1.800 -2.011 -1.943 -1.961

53.790

-4.118 -4.288

-1.705 -1.780

50.673

-3.664

-1.353 -1.313 -1.375 -1.364 -1.393

49.844

œ

50.679 50.565

-3.674

4.219

52.558

-1.737

-3.755

-1.396

49.671

Right Fuselage

**Right Wing** Average

-1.731

50.294 50.388

-3.781

-1.392

49.788 49.553

50.643

51.260

-1.378 -1.375

49.803

222

-1.364

50.198

49.801

51.077

52.364

4.191

53.114

51.550

-4.153 -4.162 -4.075 4.102

53.460

-4.280 4.286

**US Paint** 

Appendix V

**US** Paint

Painted Tinker AFB, May 97, RIGHT SIDE

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ł				К С	-135,	Tail	No.	KC-135, Tail No. 64-14838	4838				
-			7/98-i	/98-initial			2/99-	2/99-7/98			2/99-i	2/99-initial	
Location	E	delta L*	delta a*	delta b*	delta E*	delta L*	delta a*	delta b*	delta E*	delta L*	delta a*	delta b*	delta E*
	3	-0.077	-0.154	-0.093	0.196	2.186	-0.418	-0.349	2.253	2.109	-0.572	-0.442	1.046
Jəd	4	-0.997	-0.211	0.004	1.019	4.561	-0.361	-0.368	4.590	3.564	-0.572	-0.364	1.621
	ŝ	-0.051	-0.350	-0.147	0.383	3.326	-0.273	-0.538	3.380	3.275	-0.623	-0.685	1.402
	G					3.343	-0.398	-0.591	3.418				
bui/	~	1.565	-0.387	-0.291	1.638	0.783	-0.081	0.092	0.793	2.348	-0.468	-0.199	1.297
	80	1.635	-0.441	-0.580	1.790	0.047	-0.064	0.306	0.316	1.682	-0.505	-0.274	0.950
μţ	o	1.742	-0.388	-0.408	1.831	0.482	-0.070	0.120	0.502	2.224	-0.458	-0.288	1.216
·	5	1.590	-0.453	-0.564	1.747	1.255	-0.074	0.222	1.277	2.845	-0.527	-0.342	1.406
	11					2.647	-0.174	0.061	2.653				
RH .	14	-0.061	-0.181	-0.518	0.552	3.084	-0.526	-0.352	3.148	3.023	-0.707	-0.870	1.202
Motors	15	0.009	-0.228	-0.496	0.546	5.306	-0.687	-0.180	5.353	5.315	-0.915	-0.676	1.930
	19	0.853	-0.342	-0.535	1.063	2.056	-0.338	-0.117	2.087	2.909	-0.680	-0.652	1.256
-	8	0.829	-0.352	-0.454	1.009	3.117	-0.425	-0.432	3.175	3.946	-0.777	-0.886	1.511
	17	0.835	-0.467	-0.614	1.137	3.371	-0.300	-0.102	3.386	4.206	-0.767	-0.716	1.650
	16	0.670	-0.436	-0.593	0.995	3.505	-0.279	-0.013	3.516	4.175	-0.715	-0.606	1.689
	12	1.604	-0.518	-0.635	1.801	2.732	-0.148	0.193	2.743	4.336	-0.666	-0.442	1.797
1.1	13	1.331	-0.489	-0.623	1.549	2.812	-0.178	0.083	2.819	4.143	-0.667	-0.540	1.713
	20	1.159	-0.401	-0.533	1.337	3.320	-0.276	-0.165	3.336	4.479	-0.677	-0.698	1.762
	21	1.276	-0.426	-0.519	1.442	2.203	-0.221	-0.219	2.225	3.479	-0.647	-0.738	1.447
- •	23	0.879	-0.425	-0.638	1.166	2.383	-0.291	-0.319	2.422	3.262	-0.716	-0.957	1.261
- 4	22	1.457	-0.397	-0.580	1.618	0.290	-0.025	-0.127	0.318	1.747	-0.422	-0.707	0.786
Average		0.855	-0.371	-0.464	1.201	2.515	-0.267	-0.133	2.558	3.319	-0.636	-0.583	1.418
Right Wing		0.772	-0.341	-0.297	1.229	2.070	-0.213	-0.116	2.131	2.578	-0.532	-0.371	1.277
Right Fuselage	age	1.089	-0.425	-0.572	1.312	2.579	-0.248	-0.122	2.603	3.668	-0.673	-0.694	1.487

Painted Tinker AFB, May 97, LEFT SIDE

		KC-	KC-135, Tail No. 64-14838	<b>Fail N</b>	lo. 64	-1483	œ		
		Jan-98			Jui-98			Feb-99	
Location	initial	initial	initial L*	test I *	test	test	test	test	test
	۔ اد	<b>ਹ</b>	2	1	R	a	Ľ	a.	9
43		-1.456	-3.990	49.037	-1.680	-4.018	50.480	-1.840	-4.120
L 44		-1.433	-3.823	48.649	-1.581	-3.858	52.110	-2.040	-4.390
•		-1.398	-3.671	49.126	-1.705	-4.159	52.170	-2.010	-4.380
	48.289	-1.299	-3.432	48.916	-1.632	-4.046	50.410	-1.810	-4.060
6 19 19		-1.459	-3.995	51.774	-1.856	-4.429	51.680	-1.880	-4.030
μn	50.312	-1.452	-4.051	51.997	-1.981	-4.229	52.690	-1.950	-4.120
38 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		-1.435	-4.012	51.614	-1.839	-4.340	53.350	-1.990	-4.140
	50.187	-1.443	-3.916	51.919	-1.872	-4.420	52.290	-1.850	-4.200
		-1.443	-3.916	51.210	-1.822	-4.404	52.220	-1.890	-4.240
35	50.125	-1.410	-3.797	51.214	-1.779	-4.397	53.800	-2.040	-4.260
LH 49	49.439	-1.335	-3.675	49.435	-1.533	-4.161	55.210	-2.290	-4.420
S	_	-1.314	-3.668	49.672	-1.632	-4.297	51.760	-1.970	-4.550
32		-1.358	-3.777	50.491	-1:677	-4.288	52.190	-1.960	-4.460
31		-1.350	-3.738	50.642	-1.742	-4.287	51.860	-1.980	4.360
34		-1.342	-3.719	51.064	-1.849	-4.378	52.670	-1.950	-4.430
93 6		-1.347	-3.639	50.817	-1.783	-4.226	51.620	-1.910	-4.440
	_	-1.370	-3.684	51.241	-1.789	-4.177	54.870	-2.210	-4.510
92		-1.387	-3.768	51.354	-1,780	-4.151	53.820	-2.170	-4.520
	-	-1.401	-3.753	51.574	-1.920	-4.469	50.510	-1.950	-4.260
- •		-1.350	-3.649	51.227	-1.882	-4.397	52.430	-1.980	4.500
<sup>28</sup> г	<u>.</u>	-1.313	-3.633	51.015	-1.814	-4.345	53.440	-2.160	-4.550
27	49.458	-1.338	-3.725	50.743	-1.790	-4.377	54.070	-2.220	-4.630
47	49.439	-1.335	-3.675	46.427	-1.275	-3.105			
48	-	-1.314	-3.668	47.848	-1.296	-3.301			
Average	49.589	-1.378	-3.766	50.375	-1.730	-4.177	52.530	-2.002	-4.344
Left Wing		-1.423	-3.860	50.546	-1.775	-4.230	52.120	-1.930	-4.194
Left Fuselage	e 49.732	-1.350	-3.702	50.370	-1.716	-4.125	52.748	-2.049	-4.466

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Appendix V

**US Paint** 

Painted Tinker AFB, May 97, LEFT SIDE

T/98-Initial         209-7/98           Location         delta				X	C-13	KC-135, Tail No. 64-14838	l No.	64-14	1838				
deta         delta         delta <th< th=""><th>·</th><th></th><th>7/98-</th><th>initial</th><th></th><th></th><th>2/99-</th><th>-7/98</th><th></th><th></th><th>2/99-i</th><th>2/99-initial</th><th></th></th<>	·		7/98-	initial			2/99-	-7/98			2/99-i	2/99-initial	
L         A         L         A         L         A         L         A         L         A         L         A         L         A         L         A         L         A         L         A         L         A         L         A         L         A         L         A         L         A         L         A         L         L         A         L         L         A         L         L         A         L         L         A         L         L         A         L         L         A         L         L         A         L         L         A         L         L         A         L         L         A         L         L         A         L <thl< th=""> <thl> <thl> <thl></thl></thl></thl></thl<>	Location	deita •	delta a*	delta 5*	delta r*	delta	delta a*	delta L*	delta 1	delta	deita	delta L+	delta
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			9	2	ш	<u>.</u>	Ð	6	ш	-	a.	<b>0</b>	Ľ
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	43	0.234	-0.224	-0.028	0.325	1.443	-0.160	-0.102	1.455	1.677	-0.384	-0.130	1.725
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	-0.061	-0.148	-0.035	0.164	3.461	-0.459	-0.532	3.532	3.400	-0.607	-0.567	3.500
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		1.310	-0.307	-0.488	1.431	3.044	-0.305	-0.221	3.067	4.354	-0.612	-0.709	4.454
1.844 $-0.397$ $-0.434$ $1.936$ $-0.024$ $0.399$ $0.411$ $1.685$ $-0.529$ $-0.178$ $1.775$ $0.693$ $0.031$ $0.109$ $0.702$ $1.566$ $-0.404$ $-0.328$ $1.650$ $1.736$ $0.164$ $1.022$ $1.732$ $-0.429$ $-0.504$ $1.854$ $0.371$ $0.022$ $0.230$ $0.432$ $1.732$ $-0.429$ $-0.504$ $1.854$ $0.371$ $0.022$ $0.432$ $1.025$ $1.023$ $-0.319$ $-0.369$ $0.1297$ $2.586$ $-0.257$ $0.533$ $2.130$ $0.170$ $-0.318$ $-0.529$ $0.712$ $1.022$ $2.130$ $0.170$ $-0.319$ $0.511$ $0.718$ $1.233$ $2.130$ $0.170$ $-0.319$ $0.511$ $0.718$ $1.233$ $2.130$ $0.170$ $0.333$ $0.725$ $2.088$ $-0.238$ $0.073$ $1.243$ $0.2616$ $0.511$ <th>93</th> <td>0.627</td> <td>-0.333</td> <td>-0.614</td> <td>0.939</td> <td>1.494</td> <td>-0.178</td> <td>-0.014</td> <td>1.505</td> <td>2.121</td> <td>-0.511</td> <td>-0.628</td> <td>2.270</td>	93	0.627	-0.333	-0.614	0.939	1.494	-0.178	-0.014	1.505	2.121	-0.511	-0.628	2.270
1.685 $-0.529$ $-0.178$ $1.775$ $0.693$ $0.031$ $0.109$ $0.702$ 1.566 $-0.404$ $-0.328$ $1.650$ $1.736$ $-0.151$ $0.200$ $1.754$ 1.732 $-0.429$ $-0.504$ $1.854$ $0.371$ $0.022$ $0.220$ $0.432$ 1.023 $-0.379$ $-0.488$ $1.195$ $1.010$ $-0.0261$ $0.137$ $2.603$ 1.023 $-0.369$ $-0.500$ $1.297$ $2.586$ $-0.251$ $2.633$ 0.0104 $-0.198$ $-0.486$ $0.525$ $5.775$ $-0.757$ $-0.253$ $2.130$ 0.0391 $-0.319$ $-0.511$ $0.718$ $1.610$ $-0.238$ $-0.777$ $1.731$ 0.170 $-0.319$ $-0.511$ $0.718$ $1.213$ $0.616$ $-0.162$ $1.610$ 0.371 $0.517$ $0.743$ $0.533$ $-0.251$ $1.731$ 0.507 $-0.549$ $0.9143$ $1.521$ $1.218$	)e1	1.844	-0.397	-0.434	1.936	-0.094	-0.024	0.399	0.411	1.750	-0.421	-0.035	1.800
1.566 $-0.404$ $-0.328$ $1.650$ $1.736$ $-0.151$ $0.200$ $1.754$ $1.732$ $-0.429$ $-0.504$ $1.854$ $0.371$ $0.022$ $0.220$ $0.432$ $1.732$ $-0.429$ $-0.504$ $1.854$ $0.371$ $0.022$ $0.220$ $0.432$ $1.023$ $-0.369$ $-0.600$ $1.297$ $2.586$ $-0.261$ $0.177$ $2.603$ $1.010$ $-0.198$ $-0.486$ $0.525$ $5.775$ $-0.757$ $-0.259$ $5.830$ $-0.004$ $-0.198$ $-0.486$ $0.525$ $5.775$ $-0.757$ $-0.259$ $5.830$ $0.170$ $-0.319$ $-0.511$ $0.712$ $1.218$ $-0.253$ $-0.172$ $1.731$ $0.616$ $-0.392$ $-0.549$ $0.9144$ $1.218$ $-0.238$ $-0.733$ $1.243$ $1.219$ $-0.507$ $-0.659$ $1.476$ $1.606$ $-0.333$ $-0.7214$ $0.841$ $1.376$ $-0.449$ $-0.587$ $1.138$ $0.803$ $-0.127$ $-0.254$ $1.813$ $1.219$ $-0.507$ $-0.659$ $1.476$ $1.606$ $-0.333$ $3.668$ $1.376$ $-0.436$ $-0.383$ $1.521$ $3.629$ $-0.421$ $-0.811$ $1.376$ $-0.436$ $-0.532$ $-0.723$ $-0.253$ $3.648$ $1.554$ $-0.393$ $-0.523$ $-0.7214$ $0.841$ $1.376$ $-0.521$ $1.138$ $-0.523$ $-0.265$ $1.649$ $1.554$ $-0.521$ $-0.733$ $-0.252$ <t< td=""><th>ung</th><td>1.685</td><td>-0.529</td><td>-0.178</td><td>1.775</td><td>0.693</td><td>0.031</td><td>0.109</td><td>0.702</td><td>2.378</td><td>-0.498</td><td>-0.069</td><td>2.431</td></t<>	ung	1.685	-0.529	-0.178	1.775	0.693	0.031	0.109	0.702	2.378	-0.498	-0.069	2.431
1.732 $-0.429$ $-0.504$ $1.854$ $0.371$ $0.022$ $0.220$ $0.432$ $1.023$ $-0.369$ $0.600$ $1.297$ $2.586$ $0.164$ $1.025$ $1.023$ $-0.369$ $0.600$ $1.297$ $2.586$ $0.137$ $2.603$ $-0.004$ $-0.198$ $0.610$ $1.297$ $2.586$ $0.253$ $5.175$ $0.757$ $2.269$ $5.830$ $0.170$ $-0.318$ $-0.511$ $0.725$ $2.775$ $-0.757$ $-0.259$ $5.830$ $0.170$ $-0.319$ $-0.511$ $0.718$ $1.699$ $-0.233$ $-0.172$ $1.731$ $0.510$ $-0.519$ $0.511$ $0.718$ $1.203$ $-0.127$ $0.2144$ $1.243$ $0.516$ $-0.332$ $-0.433$ $0.511$ $0.723$ $-0.7214$ $0.841$ $0.721$ $-0.332$ $1.752$ $2.466$ $-0.333$ $2.668$ $0.512$ $-0.430$ $-0.251$ $-0.743$ <td< td=""><th>S</th><td>1.566</td><td>-0.404</td><td>-0.328</td><td>1.650</td><td>1.736</td><td>-0.151</td><td>0.200</td><td>1.754</td><td>3.302</td><td>-0.555</td><td>-0.128</td><td>3.351</td></td<>	S	1.566	-0.404	-0.328	1.650	1.736	-0.151	0.200	1.754	3.302	-0.555	-0.128	3.351
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		1.732	-0.429	-0.504	1.854	0.371	0.022	0.220	0.432	2.103	-0.407	-0.284	2.161
1.089 $-0.369$ $-0.600$ $1.297$ $2.586$ $-0.261$ $0.137$ $2.603$ $-0.004$ $-0.198$ $-0.486$ $0.525$ $5.775$ $-0.757$ $-0.259$ $5.830$ $0.170$ $-0.318$ $-0.629$ $0.725$ $2.088$ $-0.238$ $-0.253$ $2.130$ $0.170$ $-0.319$ $-0.511$ $0.718$ $1.699$ $-0.238$ $-0.172$ $1.731$ $0.616$ $-0.319$ $-0.511$ $0.718$ $1.699$ $-0.238$ $-0.172$ $1.731$ $0.616$ $-0.392$ $-0.569$ $1.476$ $1.699$ $-0.238$ $-0.172$ $1.731$ $0.616$ $-0.392$ $-0.561$ $1.476$ $1.699$ $-0.238$ $-0.172$ $1.731$ $0.616$ $-0.392$ $-0.587$ $1.476$ $1.218$ $-0.238$ $-0.073$ $1.243$ $1.219$ $-0.507$ $-0.659$ $1.476$ $1.218$ $-0.238$ $-0.073$ $1.243$ $1.376$ $-0.419$ $-0.433$ $1.521$ $3.629$ $-0.421$ $-0.333$ $3.668$ $1.376$ $-0.419$ $-0.433$ $1.521$ $3.529$ $-0.421$ $-0.333$ $3.668$ $1.815$ $-0.519$ $-0.716$ $2.019$ $1.064$ $-0.333$ $3.668$ $1.815$ $-0.519$ $-0.716$ $2.016$ $-0.121$ $1.243$ $1.815$ $-0.519$ $-0.716$ $2.019$ $-0.232$ $-0.103$ $1.211$ $1.558$ $-0.519$ $-0.716$ $2.725$ $-0.430$ $-0.253$ $-0.768$ <tr< td=""><th></th><td>1.023</td><td>-0.379</td><td>-0.488</td><td>1.195</td><td>1.010</td><td>-0.068</td><td>0.164</td><td>1.025</td><td>2.033</td><td>-0.447</td><td>-0.324</td><td>2.107</td></tr<>		1.023	-0.379	-0.488	1.195	1.010	-0.068	0.164	1.025	2.033	-0.447	-0.324	2.107
$            \begin{array}{ c c c c c c c c c c c c c c c c c c c$	35	1.089	-0.369	-0.600	1.297	2.586	-0.261	0.137	2.603	3.675	-0.630	-0,463	3.757
		-0.004	-0.198	-0.486	0.525	5.775	-0.757	-0.259	5.830	5.771	-0.955	-0.745	5.897
		0.170	-0.318	-0.629	0.725	2.088	-0.338	-0.253	2.130	2.258	-0.656	-0.882	2.511
	32	0.391	-0.319	-0.511	0.718	1.699	-0.283	-0.172	1.731	2.090	-0.602	-0.683	2.280
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	31	0.616	-0.392	-0.549	0.914	1.218	-0.238	-0.073	1.243	1.834	-0.630	-0.622	2.037
	34	1.219	-0.507	-0.659	1.476	1.606	-0.101	-0.052	1.610	2.825	-0.608	-0.711	2.976
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		0.872	-0.436	-0.587	1.138	0.803	-0.127	-0.214	0.841	1.675	-0.563	-0.801	1.940
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		1.376	-0.419	-0.493	1.521	3.629	-0.421	-0.333	3.668	5.005	-0.840	-0.826	5.142
1.815         -0.519         -0.716         2.019         -1.064         -0.030         0.209         1.085           1.558         -0.532         -0.748         1.808         1.203         -0.098         -0.103         1.211           1.558         -0.532         -0.748         1.808         1.203         -0.098         -0.103         1.211           1.558         -0.501         -0.712         1.764         2.425         -0.346         -0.205         2.458           1.534         -0.501         -0.712         1.764         2.425         -0.346         -0.205         2.458           -3.012         0.060         0.570         3.066         3.327         -0.430         -0.253         3.364           -3.012         0.060         0.570         3.066         3.327         -0.430         -0.253         3.364           -1.654         0.018         0.367         1.694         2.332         -0.078         2.008           0.787         -0.351         -0.412         1.383         1.860         -0.232         -0.078         2.008           1.105         -0.352         -0.370         1.257         1.574         -0.155         0.078         1.649		1.664	-0.393	-0.383	1.752	2.466	-0.390	-0.369	2.524	4.130	-0.783	-0.752	4.270
1.558         -0.532         -0.748         1.808         1.203         -0.098         -0.103         1.211           1.534         -0.501         -0.712         1.764         2.425         -0.346         -0.205         2.458           1.534         -0.501         -0.712         1.764         2.425         -0.346         -0.205         2.458           -3.012         0.060         0.570         3.066         3.327         -0.430         -0.253         3.364           -3.012         0.060         0.570         3.066         3.327         -0.430         -0.253         3.364           -1.654         0.018         0.367         1.694          2.0232         -0.078         2.008           0.787         -0.351         -0.412         1.383         1.860         -0.232         -0.078         2.008           1.105         -0.352         -0.370         1.257         1.574         -0.155         0.036         1.649           0.639         -0.366         -0.423         1.615         1.731         -0.246         -0.157         1.974		1.815	-0.519	-0.716	2.019	-1.064	-0.030	0.209	1.085	0.751	-0.549	-0.507	1.059
1.534         -0.501         -0.712         1.764         2.425         -0.346         -0.205         2.458           1.285         -0.452         -0.652         1.510         3.327         -0.430         -0.253         3.364           -3.012         0.060         0.570         3.066         3.327         -0.430         -0.253         3.364           -1.654         0.018         0.367         1.694         2.426         2.0078         2.008           0.787         -0.351         -0.412         1.383         1.860         -0.232         -0.078         2.008           1.105         -0.352         -0.370         1.257         1.574         -0.155         0.036         1.649           0.639         -0.366         -0.423         1.615         1.731         -0.246         -0.157         1.974		1.558	-0.532	-0.748	1.808	1.203	-0.098	-0.103	1.211	2.761	-0.630	-0.851	2.957
1.285         -0.452         -0.652         1.510         3.327         -0.430         -0.253         3.364           -3.012         0.060         0.570         3.066         3.327         -0.430         -0.253         3.364           -1.654         0.018         0.367         1.694         2.008         2.008         1.649           0.787         -0.351         -0.412         1.383         1.860         -0.232         -0.078         2.008           1.105         -0.352         -0.370         1.257         1.574         -0.155         0.036         1.649           0.639         -0.366         -0.423         1.615         1.731         -0.246         -0.157         1.974		1.534	-0.501	-0.712	1.764	2.425	-0.346	-0.205	2.458	3.959	-0.847	-0.917	4.151
-3.012         0.060         0.570         3.066           -1.654         0.018         0.367         1.694           -1.654         0.018         0.367         1.694           0.787         -0.351         -0.412         1.383         1.860         -0.232         -0.078         2.008           1.105         -0.352         -0.370         1.257         1.574         -0.155         0.036         1.649           0.639         -0.366         -0.423         1.615         1.731         -0.246         -0.157         1.974	27	1.285	-0.452	-0.652	1.510	3.327	-0.430	-0.253	3.364	4.612	-0.882	-0.905	4.782
-1.654         0.018         0.367         1.694         2.008           0.787         -0.351         -0.412         1.383         1.860         -0.232         -0.078         2.008           1.105         -0.352         -0.370         1.257         1.574         -0.155         0.036         1.649           0.639         -0.366         -0.423         1.615         1.731         -0.246         -0.157         1.974	47	-3.012	0.060	0.570	3.066								
0.787 -0.351 -0.412 1.383 1.860 -0.232 -0.078 2.008 1.105 -0.352 -0.370 1.257 1.574 -0.155 0.036 1.649 0.639 -0.366 -0.423 1.615 1.731 -0.246 -0.157 1.974	48	-1.654	0.018	0.367	1.694								
1.105 -0.352 -0.370 1.257 1.574 -0.155 0.036 1.649 0.639 -0.366 -0.423 1.615 1.731 -0.246 -0.157 1.974	verage	0.787	-0.351	-0.412	1.383	1.860	-0.232	-0.078	2.008	2.930	-0.619	-0.570	3.071
0.639 -0.366 -0.423 1.615 1.731 -0.246 -0.157 1.974	Left Wing	1.105	-0.352	-0.370	1.257	1.574	-0.155	0.036	1.649	2.679	-0.507	-0.334	2.756
	Left Fuselage	0.639	-0.366	-0.423	1.615	1.731	-0.246	-0.157	1.974	2.964	-0.693	-0.758	3.159

Appendix V

. • KC-135, Tail Number 64-14838 Painted Tinker AFB, May 97 US Paint -- (Both Sides)

	-	Fuselage(1)		Fuselage(2)		<u>.</u>	Fuselage(1)	Fuselage(3)		Fuselage(3)	Fuselage(4)	CU	Fuselage(5)
		2/99	1/98	86/1	2/99	Ĩ	1/98 7/98	2/99	1/98	Ĺ	2/99		2/99
		Test	test	test	Test	test	•	Test	test	_	Test		Test
Pencil Hardness		HS I	2H	I	ЭН	2H	ц. —	Ë	2H Z	ЭН	SH		SH
Modified PATTI		697 psi	800 psi	1029 psi	597 psi	8	700 psi   980 psi	1582 psi	550 psi	isi 1274 psi	895 psi		8 1393 psi
Mode of Failure: AG			15 %	10 %	5%	25 %	% 20%	10 %	88		65%		50 %
٩					10 %		5%		20 %	6 10%			
ATP							· 						38
Ср		35 %			85 %	22	25 %	45 <b>%</b>			30 %		45 %
CT		65 %	85 %	<del>8</del> 0%		50 <b>%</b>	% 75%	45%		20 %	5%		5%
Wet Tape		•	•	Pass	•	Ľ	Pass	•	ŀ	Pass	•		•

		Right Top Wing Tip	p Left Top Ving	2	Right Top V	gniW qo	Left Bottom Wind			Right Top Wing	Ving	4	Right Top Wing (Fuselage)		Right Bottom Wing	2		Right Fuselage	age
	•	1/98 7/98 test test	7/98 2/99 test Test		1/98 test	7/98 test	2/99 Test		1/98 tet	7/98 test	2/99 Test	1	1/98 text	7/98	2/99 Toot	1	1/98	7/98	2/99 Taet
Chalking	1-	-		 	1	None	8		None	None	8	<b>I</b>	None	None			None	None	9
	Ŀ		- 14(1 7612									╞				1			
	_		0	7	אופשגר	nt upper wing		3	-	KIGRI UPPER WING	Buim	4	ž	Right Upper Wing	Wing	S	102 N	Right Upper W	Wing Tip
			2/99				2/99				2/99		1/98	86/2	2/99		1/98	86/2	2/99
			Test				Test				Test		test	test	Test		test	test	Test
Pencit Hardness			SH				Ĥ				Æ			윤	£	l	¥	- HS	뮰
Modified PATTI		_	2239 psi				2289 psi				2587 psi		2300 psi   1421 psi	1421 psi	2338 psi	<b>.</b>	550 psi	784 psi	1940 pel
	Ē	COLUMN REAL PROPERTY OF		ŕ				ŧ				1				1			

Pencil Hardness				He		3H		SH	£	F	НS	£
Modified PATTI		🏼 2239 psi		2289 psi		2587 psi	2300 psi	1421 psi	1 °	550 psi	784 pai	1940 p
Mode of Failure: AC	() ()	10%		40 %		15%	20 %	20 % 70 %	25 %	±0%	10%	10 %
2		80%		% 09		85%			75%	¥ 06	<b>%</b> %	8
ATP												
G							25 %	20 %			10 %	
Ö	5						55 %	10 %				
Wet Tape		•		•		-	•	Pass	•	•	Pass	•

1940 pel 10 % Ŧ

Pencil Hardness (Soft to Hard): 5b-4b-3b-2b-b-Hb-F-H-2H-3H-4H-5H-6H-7H-8H-9H (ASTM-D-3363)

Chalking: None - 8 - 6 - 4 - 2 (ASTM-D-4214)

AG = Adhesion of glue to stud or topcoat AP = Adhesion of Primer to substrate ATP = Adhesion of Topcoat to Primer CP = Cohesion of Primer CT = Cohesion of Topcoat Appendix V

Large Aircraft Coatings Flight Testing

### **APPENDIX VI**

### Deft APC/MIL-PRF-85285

Location         initial initial DFT mils         test DFT mils         initial test DFT mils         test 60 degree Gloss         60 degree Gloss         initial 60 degree Gloss         initial 85 degree Gloss         test 85 degree Gloss         degree Gloss         60 degree Gloss         initial 85 degree Gloss         test 85 degree Gloss         degree Gloss         60 degree Gloss         initial 85 degree Gloss         test degree Gloss         degree Gloss         degree Glos         degree Glos         degre			K	(C-13	5, Tai	I No.	63-80	. 40		
44       2.9       2.0       2.6       2.3         45       3.2       1.4       2.5       2.3         5       3.2       1.4       2.5       1.7         5       39       4.0       3.1       1.9       1.8       -0.1       2.0       1.7         5       39       4.0       3.1       1.9       1.0       -0.9       1.4       1.3         5       38       4.2       4.1       2.1       2.2       1.4       2.2         37       4.4       3.5       2.3       -1.2       3.9       8.5         36       5.7       4.0       3.5       2.3       -1.2       3.9       8.5         35       3.6       4.0       3.5       2.5       -1.0       3.6       2.4       -         LH       49       16.7       1.8       3.0       2.4       -       -         Left       42       4.1       2.0       1.5       2.4       2.2       -         3       2.9       1.5       0.8       -       -       -       -         9       5       2.9       2.4       1.9       1.9       - <td< th=""><th>Locatio</th><th>'n</th><th>initial DFT</th><th>test DFT</th><th>initial 60 degree</th><th>test 60 degree</th><th>60 degree</th><th>initial 85 degree</th><th>test 85 degree</th><th>delta 85 degree Gloss</th></td<>	Locatio	'n	initial DFT	test DFT	initial 60 degree	test 60 degree	60 degree	initial 85 degree	test 85 degree	delta 85 degree Gloss
LH       49       16.7       1.8       3.0       2.4         Motors       50       19.0       1.5       2.4       2.4         Left       42       4.1       2.0       1.3       2.2         3       2.9       1.5       0.8       2.2         3       2.9       1.5       0.8       2.2         3       2.9       1.5       0.8       1.9         3       2.9       2.4       1.9       1.9       1.9         3       2.9       2.4       1.9       1.9       1.9         5       2.9       2.4       1.9       1.9       1.9         5       2.9       2.4       1.9       1.9       1.7         5       2.9       2.1       2.3       2.3       2.1       1.7         6       2.2       2.1       1.7       3.6       2.3         6       2.2       2.7       2.0       1.4       1.2         9       2.7       2.0       1.4       1.2       1.7         5       11       3.0       2.1       1.5       4.0         9.0       11.0       54.0       4.0       4.0	Left Wing, Upper Surface	44 45 46 40 39 38 37 36	2.9 3.2 3.2 2.9 4.0 4.2 4.4 5.7	3.1 4.1 3.7 4.0	2.0 1.4 1.9 1.9 2.1 2.1 3.5	1.0 2.2 3.1 2.3	-0.9 0.1 1.0 -1.2	2.6 2.3 2.5 2.0 1.4 1.4 3.9 3.9	1.3 2.2 7.3 8.5	-0.3 -0.1 0.8 3.4 4.6 -1.2
Left       42       4.1       2.0       1.3       2.2         3       2.9       1.5       0.8       2.2         3       2.9       1.5       0.8       1.9         90       4       2.4       1.9       1.9       1.9         90       4       2.4       1.9       1.9       1.9         90       5       2.9       2.4       1.9       1.9         90       6       2.2       2.1       2.3       3.6         90       7       1.9       1.7       3.6       3.6         9       2.7       2.0       1.4       1.2         9       2.7       2.0       1.4       1.2         9       2.7       2.0       1.4       1.2         9       2.7       2.0       1.4       1.2         9       11       3.0       2.1       1.7       1.2         9       11       3.0       2.1       1.5       54.0         9       9.0       11.0       54.0       54.0         9       8.2       47.0       47.0       47.0         8       14       12.2       2.2										
Fuselage         41         3.0         2.4         2.2            3         2.9         1.5         0.8             9         4         2.4         1.9         1.9             9         5         2.9         2.4         1.9          1.9            9         5         2.9         2.4         1.9          2.3            9         6         2.2         2.1         2.3              9         7         1.9         1.7         3.6              9         2.7         2.0         1.4              9         2.7         2.0         1.4              10         3.3         1.7         1.2               11         3.0         2.1         1.5               10         AP*         9.0         11.0         54.0										
a)       4       2.4       1.9       1.9         b)       5       2.9       2.4       1.9         b)       6       2.2       2.1       2.3         b)       7       1.9       1.7       3.6         c)       7       1.9       1.7       3.6         c)       9       2.7       2.0       1.4         c)       9       2.7       2.0       1.4         b)       10       3.3       1.7       1.2         iiii       11       3.0       2.1       1.7         iiiii       3.0       2.1       1.7       1.2         iiiii       3.0       2.1       1.7       1.5         iiiii       3.0       2.1       1.5       54.0         iiiii       AP*       11.0       54.0       54.0         AP*       8.2       47.0       47.0       10         RH       14       12.2       2.2       3.0       10								2.2		
	Right Wing, Upper Surface	4 5 6 7 8 9 10 11 11 AP* AP*	2.4 2.9 2.2 1.9 2.3 2.7 3.3 3.0 3.0		1.9 2.4 2.1 1.7 2.1 2.0 1.7 2.1 2.1 11.0 11.0			1.9 1.9 2.3 3.6 1.7 1.4 1.2 1.7 1.5 54.0 54.0 47.0		
Motors 15   16.3   2.2     2.7   2.7										
AP* 9.5 52.9	Motors		16.3							
Right Fuselage         12         5.4         2.5         2.3           13         6.2         2.5         2.2	Fuselage	12	6.2		2.5 2.5			2.3 2.2		1.7

Painted Tinker AFB, May 98

Deft MIL-P-23377G Primer Deft MIL-PRF-85285C Topcoat

AP\* = Applique

Physical Tests

Painted Tinker AFB, May 98

				Ч Х С	135, T	ai	KC-135, Tail Number 64-8040	. 64-80	40					
APC(Left Side)														
	M	Wing Tip	2	Lift	Lift Point	3	Inboard #1 Engine		4	utboard	Outboard #2 Engine	5 Inb	Inboard #2 Engine	Engine
		1/99			1/99			1/99			1/99			1/99
		test			test		- 	test			test			test
Pencil Hardness	•	2H			HB			2H			I	•		2H
Modified PATTI	1	1692 psi		•	1194 psi		- 15	1592 psi			1592 psi	•	-	1791 psi
Failure Mode: AG		25 %			10 %		-	100 %	L		100 %			95 %
AP		40 %												
ATP														
CP			_											
CT		35 %			% 06									5%
Wet Tape	•	•		•	•		•	•	L		•		 	
												•		
Chalking		None			None			None			None			None

Left Side - Deft APC • = ASTM D 659 Photographic Reference Standard Pencil Hardness (Soft to Hard): 5b-4b-3b-2b-b-Hb-F-H-2H-3H-4H-5H-6H-7H-8H-9H

AG = Adhesion of glue to stud or topcoat AP = Adhesion of Primer to substrate ATP = Adhesion of Topcoat to Primer CP = Cohesion of Primer CT = Cohesion of Topcoat

Appendix VI

85285	
IL-PRF-4	
APC/M	
Deft	

Painted Tinker AFB, May 98

			K	2-135	KC-135, Tail No.	No.	63-8040	40	۰ ۱		
Location	no	initial L*	initial a*	initial b*	1/99 test L*	1/99 test a*	1/99 test b*	delta L*	delta a*	delta b*	deita E*
APC	43	48.977	-1.388	-3.928							
1 <del>9</del>	4 4 4 4	49.245	-1.346	-3.904							
dd <u>r</u>	6 4 9	46.748	-1.183	-3.246							
פכפ ז' f	4	50.748	-1.746	-4.487	47.720	-1.370	-3.540	-3.028	0.376	0.947	3 195
	39	49.933	-1.759	-4.529	48.880	-1.720	-4.120	-1.053	0.039	0.409	1.130
	38	49.694	-1.689	-4.428	48.350	-1.680	-3.880	-1.344	0.009	0.548	1.451
ĥ9.	37	50.801	-1.704	-4.346	49.520	-1.650	-3.670	-1.281	0.054	0.676	1.449
1	36	50.801	-1.704	-4.346	49.920	-1.620	-3.770	-0.881	0.084	0.576	1.056
	35	50.831	-1.771	-4.368	49.930	-1.680	-3.800	-0.901	0.091	0.568	1.069
н	49	49.231	-1.367	-3.927							
Motors	50	48.554	-1.295	-3.770							
Left	42	48.591	-1.300	-3.844							
Fuselage	41	49.370	-1.510	-3.685							
	e	47.738	-1.249	-3.280							
93	4	49.031	-1.397	-3.855							
u an	S	49.230	-1.316	-3.698							
Ing	9	49.164	-1.339	-3.775							
91 (	7	50.954	-1.787	-4.367							
ədd	œ	48.479	-1.265	-3.076							
'n	0	49.004	-1.282	-3.321							
'ົວເ	6	49.360	-1.307	-3.679							
ńŇ		49.146	-1.366	-3.130							
<b>1</b> 14		49.122	-1.365	-3.587							
6i)	₽₽ ₩	49.145	-1.347	-3.493			-				
Я	AP*	48.881	-1.496	-4.261							
	AP*	47.859	-1.494	-4.080							
RH	14	48.723	-1.303	-3.717							
Motors	15	48.933	-1.267	-3.665							
	AP*	49.259	-1.529	-3.872							
Fuselage	12	49.235	-1.341	-3.753							
	13	48.672	-1.339	-3.845							
Average		50.468	-1.729	-4.417	49.053	-1.620	-3.797	-1.415	0.109	0.621	1.558

Deft MIL-P-23377G Primer Deft MIL-PRF-85285C Topcoat

AP\* = Applique

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Appendix VI

Large Aircraft Coatings Flight Testing

### **APPENDIX VII**

Notes from Mr. Sneed:

### DEFT

- 1.) Worse than Courtauld's on flaps and in lesser exposed areas
- 2.) Peeling worse than on Courtauld's side
  - a.) Underside of wing
  - b.) Panel edges
  - c.) Leading edges (peeling/touchup)
  - d.) Around windshield (touched up)
- 3.) Appeared to be chalking
- 4.) Paint not sticking to sealant in a number of places

### COURTAULDS

- 1.) Peeling
  - a.) Bad underside of wings
  - b.) Oklahoma Door
  - c.) Around Radome
  - d.) Bare metal around windshield
  - e.) Leading edge fastener row, upper wing, to bare metal -- fastener's showing
  - f.) Along sealant
- 2.) Touchup -- more rework
- 3.) Chalky appearance

### SPRAYLAT

- 1.) Lot of rework near fuselage on upper wing
- 2.) More touchup around fasteners than rest of test aircraft
- 3.) Paint peeling/cracking along rivet rows and sealant
- 4.) Fuselage rework along fuselage seams
- 5.) Leading edge touchup and small amount of peeling to bare metal
- 6.) Touchup underside of wing
- 7.) Boom area under fuselage had primer showing
- 8.) Flight controls faded worse than Sherwin-Williams
- 9.) Peeling to bare metal around Radome
- 10.) Less peeling around windows than other Hickam paints

### SHERWIN-WILLIAMS

- 1.) Rework over fasteners on upper wing
- 2.) Fuel staining along front fastener row (see 1. Above)
- 3.) Some touchup on upper wing
- 4.) Spot peeled to primer on upper wing

Appendix VII

- 5.) Fuselage rework along fuselage seams
- 6.) Peeling/Cracking around and on panel rivets upper wing
- 7.) Visually better than Spraylat
- 8.) Formulated to Gunship luster
- 9.) Fasteners peeling to bare metal on Beaver Tail
- 10.) Rework spread over aircraft in general
- 11.) Leading edge touchup about the same as Spraylat side, maybe slightly more
- 12.) Cowling Leading edges peeling both to metal and primer
- 13.) Less fading and smoother surface than other aircraft

### ADVANCED PERFORMANCE COATINGS (APC)

- 1.) Noticeable color difference between GSA Topcoat
  - a.) Depending on angle of sun, appears to be darker than Deft
  - b.) Smoothest paint to the touch
- 2.) Fasteners starting to corrode center of wing
- 3.) Chipped paint in one Spot
- 4.) Very little cracking around fasteners
- 5.) Test indicate Gunship luster. It appears to have a sheen

### **US PAINT**

- 1.) Very little Radome leading edge peeling noted
- 2.) Possible touchup around pilots window
  - a.) Very hard to discern at close distance
  - b.) No peeling at time of inspection
- 3.) Typical nicks and peeling on and around doors and access panels
- 4.) Peeling to bare metal around 1 & 2 Engine cowling leading edges
  - a.) Nothing longer than 1-2 mm
- b.) Looked better than some of the Hickam aircraft
- 5.) Very little RH wing leading edge peeling
- a.) Two nicks to bare metal
- 6.) Number 3 engine cowling leading edge had no peeling
- 7.) Number 4 engine cowling leading edge had almost no peeling
- 8.) LH leading edge between number 1 and 2 engines had small amount of peeling
- 9.) LH leading edge outside of number 1 engine had some peeling
- 10.) No peeling evident on vertical and horizontal leading edges from ground view
- 11.) Sporadic touchup over aircraft fuselage
  - a.) Touchup appeared to be good match
  - b.) Low light in hanger, which may hide imperfections and chalking, makes it difficult to tell how well paint matched up
- 12.) All in all, the aircraft is in great shape for 22 months of service life
- 13.) Field units report aircraft looks better in direct sunlight than old Mil-C-85285 painted aircraft

### Appendix VII



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## Large Aircraft Coatings Flight Testing

**APPENDIX VIII** 

### KC-135 Exterior Coating System Operational Test and Evaluation Test Plan August 1997

Prepared by: Mike Spicer

**Coatings Technology Integration Office** 

Reviewed by: Maj Kevin Kuhn

**Coatings Technology Integration Office** 

Submitted by: OC-ALC/LAPEP, HQ AMC/LGBEF, HQ ANG/LGMM

Approved by: KC-135 SPD

Further dissemination only as directed by OC-ALC/LCRA (August 1997) or higher DoD authority

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### ABBREVIATIONS AND ACRONYMS

AFB	Air Force Base
AMC	Air Mobility Command
ANG	Air National Guard
COI	Critical Operational Issue
COTS	Commercial Off The Shelf
CTIO	Coatings Technology Integration Office
GSA	Government Supply
HPACS	High Performance Aerospace Coating System
HQ	Head Quarters
MAJCOM	MAJor COMmand
NCOIC	Non Commissioned Officer In Charge
NESHAP	National Emission Standards for Hazardous Air Pollutants
OC-ALC	Oklahoma City-Air Logistics Center
PDM	Programmed Depot Maintenance
QOT&E	Qualification Operational Test and Evaluation
QPL	Qualified Products List
SM-ALC	SacraMento-Air Logistics Center
SPD	Systems Program Director
Т.О.	Technical Order
UV	UltraViolet
VOC	Volatile Organic Compound

### SECTION I INTRODUCTION

**1.0 GENERAL.** Oklahoma City Air Logistics Command (OC-ALC) in conjunction with Air Mobility Command (AMC) and Air National Guard (ANG) will conduct a Qualification Operational Test and Evaluation (QOT&E) of 1998 National Emission Standards for Hazardous Air Pollutants (NESHAP) compliant coating systems in the KC-135 operational environment using a current MIL-SPEC qualified coating system as a control and select the best performing coating system to be utilized on the KC-135 fleet.

### **1.1 SYSTEM INFORMATION**

1.1.1 Background. The current TT-P-2756 coating system used on the exterior moldline of the KC-135 aircraft is not meeting performance requirements over the full Programmed Depot Maintenance (PDM) cycle. The KC-135 Systems Program Director (SPD) has directed that TT-P-2756 type material will no longer be used on KC-135 aircraft that have gone through depot and are stripped to bare metal. TT-P-2756 is a 1998 NESHAP compliant coating and as a result of this directive the depots(OC-ALC and SM-ALC) are faced with using non-NESHAP compliant coating system is tested, qualified and approved. The laboratory test and evaluation phase for an improved NESHAP compliant coating system was accomplished via the "High Performance Aerospace Coating System" (HPACS) contractual program

managed by WL/MLSS. Four promising coating systems were identified by the HPACS program as being worthy for flight test consideration.

1.1.2 Description All coating systems being tested are commercial off the shelf(COTS) products that meet 1998 NESHAP requirements. A "coating system", as referred to in this plan, is a primer and a topcoat combination. All primers being tested are a high-solids epoxy chromated primer with a VOC rating of 340 g/L or less. All topcoats being tested are a high-solids polyurethane topcoat with a VOC rating of 420 g/L or less.

Manufacturer	Primer	Topcoat	Aircraft @ Station
US Paint	S9800-K13	Awlgrip	KC-135 @ Macdill AFB, Tampa Bay Fl.
Courtaulds	513X423C/930K118/ 530K015	832G062/930G052 UV Improved*	KC-135 @ Hickham AFB, Oahu Ha.
Deft	Mil-C-23377G TI CC 02Y40	Mil-C-85285B T1 03GY321**	Same Aircraft
Pratt & Lambert Sherwin-Williams	724-500/724-501 E90G203/V93V230	785-637/785-000/ 785-118 F93A26/V93V26/V93V1	KC-135 @ Hickham AFB, Oahu Ha.
Spraylat	EEAE-154 A/B	EUBG167 A/B	Same Aircraft

The coating systems evaluated in this QOT&E are listed in the table below.

\* Courtaulds has added UV absorbers to their previous version topcoat to give better performance.

\*\* In May 96 Deft reformulated their MIL-C-85285 topcoat to give better performance.

The test coating systems are expected to provide increased performance over the TT-P-2756 in the areas of weatherability, adhesion to the substrate, cleanability, and protection against corrosion.

### **1.2 OPERATIONAL ENVIRONMENT**

1.2.1 Threat Summary Not applicable for this project

1.2.2 Operational Concept The coating systems are being tested as a drop-in replacement of TT-P-2756 for use on the outer moldlines of KC-135 aircraft. Therefore, part of this QOT&E is to check the compatibility with surface preparation materials and processes as well as spray equipment being utilized at the ALCs and field units. No major equipment changes are expected but, minor process changes could be realized

To ensure the performance of the coating systems is realized, severely corrosive, high UV, marine environments were selected as operational test sites. Also, this QOT&E project requires the normal KC-135 operating environment for testing. Special ranges, test facilities, and equipment are not required.

1.2.3 Maintenance Concept Normal touch-up and repair of the coating systems on the test aircraft by the field units will be the same procedure as for non-test aircraft, i.e. in

accordance with T.O. 1-1-8, except appropriate test coating materials will be used. Adequate quantities of test coatings will be provided when the aircraft is delivered from the ALC and upon owning unit request. Evaluation forms will be provided to the selected POC.

Some destructive testing will be performed by the engineering team when conducting a local assessment of the test coating systems. The engineering team will be responsible for repairing the destroyed coating system. The method for repair is as follows: feather the edges of the area under repair by hand sanding with 150 grit sand paper, apply a Mil-P-23377G T1 CC primer or a Mil-P-85582 T1 C2 primer using a SEMPEN applicator, allow the coating to cure 2 hours, apply a Mil-C-85285B T1 topcoat in color 36173 using a SEMPEN applicator. The SEMPEN applicator and materials in side are products of Courtaulds Aerospace. The materials in the SEMPENS are Mil Spec qualified and have been incorporated into T.O. 1-1-8.

1.2.4 Training Concept The coating system selected from this QOT&E project for use on the KC-135 fleet will undergo a battery of tests by CTIO. The tests are designed to characterize the use of the coating system under different temperatures, humidities, and spray equipment. CTIO will take the results of the tests and working with the coating system manufacturer create a users guide for that particular coating system. The users guide will define the operating window for which the coating system can be used. Suggestions and consequences for using the coating system outside of the window will also be incorporated in the users guide. The users guide can be used by painters at the ALCs and field units as a starting point for setting up their spray equipment based on their given situation. Any problems that can not be solved with the use of the users guide can be directed to CTIO.

**1.3 PROGRAM STRUCTURE** At the point in time when a coating system(s) is selected for utilization on the KC-135 fleet, CTIO will work with GSA in setting up a vehicle for the procurement of the coating system(s). Performance data, characterizing the coating system(s), obtained from the HPACS program will be used to create a Purchase Description or Specification with a qualified products list (QPL). Quality assurance testing of the material for successive batches will be tested by CTIO and stated in the Purchase Description or Specification.

### **SECTION II QOT&E OUTLINE**

### 2.0 OBJECTIVE AND CRITICAL OPERATIONAL ISSUES

The objective of this QOT&E is to conduct a flight test of NESHAP compliant coating systems with a Mil Spec coating system as a control and evaluate the performance characteristics of all coating systems per the COIs mentioned. The best performing coating system will be utilized on the KC-135 fleet.

The following COIs are derived from the Mission Need Statement, CAF/AMC/AETC/AFSOC/AFMC 812-97 (DRAFT).

Current Mil Spec coating systems(Mil-P-23377G CC, Mil-P-85285) provide adequate corrosion protection. Therefore, the test coating systems must provide equal or improved performance in the area of protection against corrosion compared to the current Mil-Spec coating system.

COI-1: Do the test coating systems provide equal or improved protection against corrosion compared with the control coating system.

The majority of the scuff sand and overcoat, and touch-up and repair activities performed at field units are a result of poor weathering and appearance characteristics of the Mil Spec coating systems. As a result, the test coating systems will have to show an improvement over the current Mil Spec coating system (Mil-P-23377G CC, Mil-P-85285).

COI-2: Do the test coating systems provide improved performance in the area of apperance.

COI-3: Do the test coating systems provide improved appearance characteristics over the control coating system.

2.1 SCOPE AND TEST CONCEPT HQ AMC is the lead organization in identifying aircraft for this QOT&E project. The three test aircraft identified are one AMC KC-135 tail number 64-14838 stationed at MacDill AFB and two ANG KC-135s, tail numbers 64-14832 and 59-1472, stationed at Hickam AFB.

The AMC KC-135 will go through PDM at OC-ALC and will be coated with a test coating system from U.S. Paint (primer S9800/K8032; topcoat Awlgrip H.S. Polyurethane) on 12 May 97.

The two ANG KC-135s will go through PDM at SM-ALC in the August/September 1997 timeframe. Tail number 64-14832 will be coated with a coating system from Courtaulds (primer 513X423C/930K118/530K015; topcoat 832G062/930G052) on the righthand side and a coating system from Deft (primer 02Y40; topcoat 03GY321) utilized as the control on the lefthand side of the aircraft. Tail number 59-1472 will be coated with a coating system from Spraylat (primer EEAE-154A; topcoat EUBG167 A/B) on the righthand side and the Pratt & Lambert (Sherwin-Williams) (primer E90G203/V93V230, topcoat F93A26/V93V26/V93V1) on the lefthand side of the aircraft.

Deft was selected as the control because of its extensive use on other weapon systems. An Application Data Sheet will be supplied to the ALC applying the coating systems and shall be completed at the time the coating systems are applied. Appendix A is a copy of the Application Data Sheet form.

Each aircraft will be evaluated after every wash cycle by the unit POC. Appendix B is a copy of the evaluation form that should be used by that field level person and sent to AMC/LGBEF, OC-ALC/LAPEP and CTIO upon completion.

On six month intervals an engineering team will conduct a local assessment of the coating systems in conjunction with local corrosion control and crew chief personnel. The engineering team will consist of engineers from the KC-135 SPD, corrosion control monitors of the participating MAJCOMs, and engineers from WL/MLSS-CTIO.

Appendix C is a copy of the evaluation form the engineering team will use to gather data to provide input to the Interim Test Event Report.

A decision point has been established 18 months from when the last KC-135 aircraft will be coated. At that point a decision between OC-ALC/LCR, OC-ALC/LAP, HQ AMC/LGM and HQ ANG/LG will be made as to the best performing coating but, the test coatings will be left on the aircraft a full PDM cycle for further evaluation.

### 2.2 PLANNING CONSIDERATIONS AND LIMITATIONS

2.2.1 Planning Considerations The ideal flight test procedure for coating systems is to apply the test coating system on one side of the test aircraft and apply the control coating system on the other side of the same test aircraft. The reasons for this paint scheme is stated in a letter issued March 1996 to all MAJCOM Corrosion Managers and authored by Gary Stevenson on behalf of WL/MLSS.

Do to circumstances out of our control, aircraft tail number 64-14838 and possibly aircraft tail number 59-1472 will not receive this paint scheme. Steps are being taken in order to ensure meaningful data will be collected from the two test aircraft.

Aircraft, tail number 64-14838 which will coated with the US Paint coating system will be stationed at MacDill AFB.

Aircraft, tail number 59-1472 which will be coated with the Spraylat coating system on one side and the Pratt & Lambert (Sherwin-Williams) coating system on the other side will be stationed at Hickham AFB. The other test aircraft, tail number 64-14832 that has the Deft coating system on one side of the aircraft will be used as the control coating system for comparing data collected from aircraft tail number 59-1472.

The variables associated with the work arounds will be noted in the reports.

2.2.1.1 Aircraft Availability The test aircraft are regularly scheduled for routine depot maintenance and will be operating in a severely corrosive, high UV marine environment. It is desired that test aircraft shall not be retired or transferred to another environment for the period of testing (a full PDM cycle).

2.2.1.2 Operational Support The respective MAJCOMs shall brief their operational field units about the QOT&E plan and their expected duties. The operational field units shall complete the evaluation forms provided, use the appropriate test coatings supplied for touch-up and repair when needed, and give the same attention to the test aircraft as would be given to any normal operating aircraft. No more, no less. A complete scuff sand and overcoat shall not be performed on the test aircraft without approval from the appropriate MAJCOM representative.

2.2.1.3 Equipment, Materials, and Processes All aspects in applying the test coatings shall be in accordance with T.O. 1-1-8 and T.O. 1-1-691.

2.2.2 Estimated Cost All coating systems will be purchased by AFMC TTO/TTP through WL/MLSS and delivered to the appropriate ALC. One gallon kit of the coating systems will accompany the respective test aircraft for touch-up and repair purposes. The ALCs will absorb any additional costs involved with the application of the test and

control coatings. In the unlikely event that catastrophic failure should occur, the appropriate MAJCOM will provide funding for the removal of test materials and the refinishing of the aircraft. Each organization participating in the evaluation of the coating systems is responsible for their TDY funding to the test site. Costs associated with test plan development, Interim and final reports, and their distribution will be absorbed by WL/MLSS-CTIO.

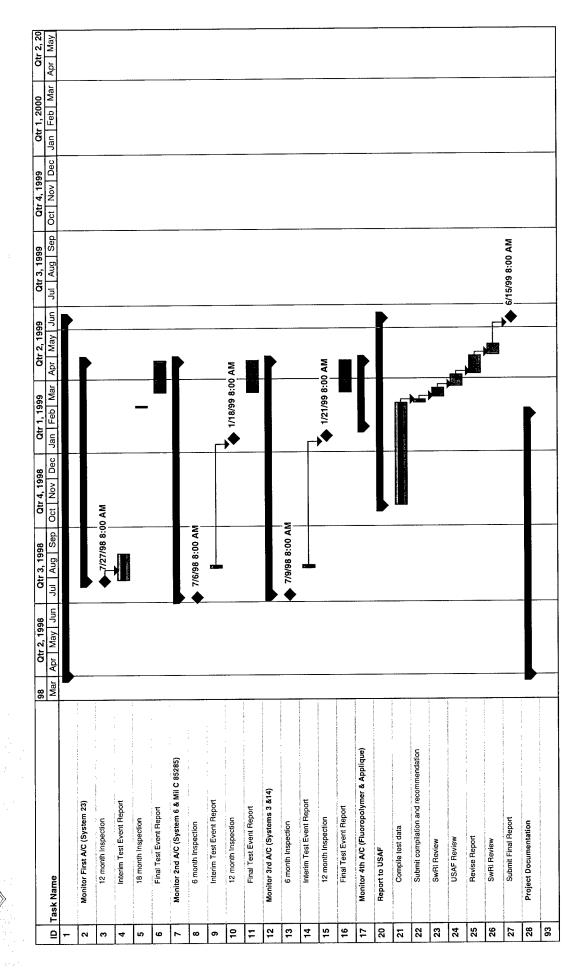
### 2.3 QOT&E SCHEDULE AND READINESS REQUIREMENTS

Ref. page 11

### SCHEDULE GOES HERE

# Jun 99 CEVV PMR

# LARGE AIRCRAFT COATING SYSTEM ZHTV98WL23 - ZHTV99CT88



CO	MOE	MOP
		MOP3-1-3: Use of a portable gloss meter of 85 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.
		MOP 3-1-4: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical property changes.
	MOE 3-2: The color stability of the test coating systems shall be an improvement over the currently used coating systems.	MOP 3-2-1: Use of a portable colorimeter in accordance with ASTM D2244 shall show a delta E ratio of test coating system to control coating system of less than 1.0 (i.e. delta E of test coating / delta E of control MOP 3-2-2: Use of a black velvet cloth in accordance with ASTM ???? shall not show evidence of chalking
		MOP 3-2-3: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical property changes. MOP 3-3-1: Use of a portable gloss meter of 60 degree geometry in
	MOE 3-3: The gloss stability of the test coating systems shall be an improvement over the currently used coating systems.	accordance with ASIM U523 shall show less change in gloss on the fest side as compared to the control side. MOP 3-3-2: Use of a portable gloss meter of 85 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.
		MOP 3-3.3: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical property changes.
	MOE 3-4: The fluid resistance stability of the test coating systems shall be an improvement over the currently used coating systems.	MOE 3-4: The fluid resistance stability of the test coating systems. MOP 3-4-1: Using the pencil hardness technique in accordance with shall be an improvement over the currently used coating FTMS-141, the change in hardness of the test coating shall be less than systems. MOP 3-4-2: Upon visual inspection the degree of adhesion on the test south interfaces and the control state for all interfaces and the
		MOP 3-4-3: Use of a portable colorimeter in accordance with ASTM D2244 shall show a delta E ratio of test coating system to control coating system of less than 1.0 (i.e. delta E of test coating / delta E of control MOP 3-4-4: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical property chances.
	MOE 3-5: The touch-up/repaired area shall show an improvment relative to color and gloss over the currently used coating system.	MOP 3-5-1: Use of a portable colorimeter in accordance with ASTM D2244 shall show a delta E ratio of test coating system to control coating system of less than 1.0 (i.e. delta E of test coating / delta E of control MOP 3-5-2: Use of a portable gloss meter of 60 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.
		MOP 3-5-3: Use of a portable gloss meter of 85 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.
		MOP 3-5-4: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and chemical property changes.

	MOF	ACM
COL 1: Do the test continue systems provide actual or	MOF 1-1: The corrosion protection of the test continue systems	MOP 1-1-1-1 (hoon visual inspection the test coated skins shall show no
improved protection against corrosion compared with the		more exfoliation corrosion around fastener countersinks and panel
control coating system?	used coating systems.	edges than on the control coated skins.
		more filliform corrosion than on the control coated skins.
	MOE 1-2: The degree of compatibility (adhesion) of primer with	MOP 1-2-1: Upon visual inspection the degree of adhesion on the test
	the substrate and topcoat with the primer.	side shall be equal to or better than the control side for all interfaces
		MOP 1-2-2: Modified Adhesion Patti testing per ASIM 51/9 shall measure a minimum of 1000 psi.
	MOE 1-3: The integrity of the test coating system on and around	
	upper and lower wing skin fasteners shall be equal or show an	
	improvment over the currently used coating system.	value than the control coating.
		MOP 1-3-2: Paint cnips from the point of failure for the fest coaling of
		control coarting shall be collected and analyzed in title laboratory to determine physical and chemical property changes
		MOP 2-1-1: Use of a portable gloss meter of 60 degree geometry in
COI-2: Do the test coating systems provide equal or	MOE 2-1: The gloss stability of the test coating systems shall be	accordance with ASTM D523 shall show less change in gloss on the test
improved performance in the area of visibile detection?	an improvement over the currently used coating systems.	side as compared to the control side.
		MUP Z-1-Z: Use of a portable gloss meter of as aegree geomeny in
		uccordance with Adim Data sharing in wress change in gross of the total side.
		MOP 2-1-3: Paint chips from the test coating and control coating shall be
		collected and analyzed in the laboratory to determine physical and
		chemical property changes. MOB 2/2/11/15/06/2/4/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/
	MOE 2-2: The cleanability of the test coating systems shall be an	MOE 2-2: The cleanability of the test coating systems shall be an with ASTM D523 shall show an increase of at least 5 percentage points
	improvment over the currently used coating systems.	over the control side.
		MOP 2-2-2: Use of a portable gloss meter of 60 degree geometry in
		accordance with ASTM D523 shall show less change in gloss on the test
		side as compared to me common side. MADD 3-23 thes of a sociable close motor of 85 chores accomptivity
		intor 2-2-3, use of a portable gloss triated of os degree geotrieny in accordance with ASTM D523 shall show less change in aloss on the test
		isconductor with routin post of the control side.
		MOP 2-2-4: Paint chips from the test coating and control coating shall be
		collected and analyzed in the laboratory to determine physical and
	MOE 2-3: The fluid resistance stability of the test coating systems	
	shall be an improvement over the currently used coating	
	systems.	the change in hardness on the control coating.
		MOP 2-3-2: Upon visual inspection the degree of adhesion on the test
		MOP2-3-3: Use of a portable colorimeter in accordance with ASTM
		D2244 shall show a delta E ratio of test coating system to control coating
		system of less than 1.0 (i.e. delta E of test coating / delta E of control
		MOP 2-3-4: Paint chips from the test coating and control coating shall be collected and analyzed in the laboratory to determine physical and
		chemical property changes.
COI-3: Do the test coating systems provide equal or improved appearance characteristics over the control	MOF 3-1: The cleanability of the test coating systems shall be an	MOP 3-1-1: Use of a 45 degree/0 degree reflectometer in accordance n with ASTM D523 shall show an increase of at least 5 percentage points
coating system?	improvment over the currently used coating systems.	over the control side.
		MOP 3-1-2: Use of a portable gloss meter of 60 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test
		side as compared to the control side.

### SECTION III METHODOLOGY

### 3.0 GENERAL

### 3.0.1 COI and MOE/MOP Matrix Ref. page 12-13

# **3.1 COI-1:** Do the test coating systems provide equal or improved protection against corrosion compared with the control coating system?

3.1.1 Scope In order to ensure the test coating systems show corrosion protection characteristics, the test coating systems shall be flight tested on test aircraft stationed in a severely corrosive, high UV marine environment for a minimum of 20 months. The test coating systems shall show equal or improved performance as compared to the Mil Spec qualified Deft coating system in order to pass this COI. The Deft coating system will be used as the control coating system.

3.1.2 Measures of Effectiveness/Performance and Evaluation Criteria

**3.1.2.1 MOE 1-1** The corrosion protection of the test coating system shall be equal to or show an improvement over the currently used coating systems

3.1.2.1.1 MOP 1-1-1 Upon visual inspection, the test coated skins shall show no more exfoliation corrosion around fastener countersinks and panel edges than on the control coated skins.

3.1.2.1.2 MOP 1-1-2 Upon visual inspection, the test coated skins shall show no more filliform corrosion than on the control side for all interfaces.

**3.1.2.2 MOE 1-2** The degree of compatibility (adhesion) of primer with the substrate and topcoat with the primer.

3.1.2.2.1 MOP 1-2-1 Upon visual inspection, the degree of adhesion on the test side shall be equal to or an improvement to the control side for all interfaces.

3.1.2.2.2 MOP 1-2-2 Using the Modified Adhesion testing per ASTM 5179, the test and control coating systems shall measure a minimum of 1000 psi. This test shall be performed on two areas of the test aircraft per coating system. The first area is the upper section of the fuselage just past the wing root. The second area is the lower section of the fuselage just past the wing root. This is a destructive test method for the coating system in the localized area. Repair of the coating system is referenced in section 1.2.3 Maintenance Concept, second paragraph.

**3.1.2.3 MOE 1-3** The integrity of the test coating system on and around upper and lower wing skin fasteners shall be equal or show improvement over the currently used coating system.

3.1.2.3.1 MOP 1-3-1 Upon visual inspection and using the evaluation criteria stated, the test coating system shall score an equal or higher value than the control coating system based on the criteria below.

No evidense of cracking or adhesion loss	4
Cracked circumferential in counter sink	3
Cracked and 1/4 moon adhesion loss around counter sink and fastener	2
Cracked and 1/2 moon adhesion loss around counter sink and fastener	1
Cracked and full moon adhesion loss around counter sink and fastener	0

**3.2 COI-2: Do the test coating systems provide improved performance in the area of visible detection?** 

3.2.1 Scope Per Mil-C-85285B the specular gloss of camouflage topcoats at 60 degrees angle of incidence shall have a reading of 5 or less. Mil-C-85285B topcoats have not been able to maintain the 5 or less reading over time and after many wash cycles. The test coating systems shall show improved performance in maintaining camouflage gloss measured at 60 degrees and 85 degrees over the control coating system in order to pass this COI.

3.2.2 Measures of Effectiveness/Performance and Evaluation Criteria

**3.2.2.1 MOE 2-1** The gloss stability of the test coating system shall be an improvement over the currently used coating systems.

3.2.2.1.1 MOP 2-1-1 Use of a portable gloss meter of 60 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

At the time when the test and control coating systems have been applied, a gloss reading shall be recorded for each coating system. On 6 month intervals, the gloss reading shall be recorded for each coating system. The delta of the test coating system shall be less than the delta of the control coating system in order to pass.

3.2.2.1.2 MOP 2-1-2 Use of a portable gloss meter of 85 degree geometry in accordance with ASTM D523 shall show less change in gloss on the test side as compared to the control side.

At the time when the test and control coating systems have been applied, a gloss reading shall be recorded for each coating system. On 6 month intervals, the gloss reading shall be recorded for each coating system. The delta of the test coating system shall be less than the delta of the control coating system in order to pass.

3.2.2.1.3 MOP 2-1-3 Paint chips from the test and control coating systems shall be collected and analyzed in the laboratory to determine physical and chemical property changes.

**3.2.2.2 MOE 2-2** The cleanability of the test coating systems shall be an improvement over the currently used coating systems.

3.2.2.2.1 MOP 2-2-1 Use of a 45 degree/0 degree reflectometer in accordance with ASTM D523 shall show an increase of at least 5 percentage points over the control side.

3.2.2.2.2 MOP 2-2-2 Same as MOP 2-1-1

3.2.2.3 MOP 2-2-3 Same as MOP 2-1-2

3.2.2.2.4 MOP 2-2-4 Same as MOP 2-1-3

**3.2.2.3 MOE 2-3** The fluid resistance stability of the test coating system shall be an improvement over the currently used coating systems.

3.2.2.3.1 MOP 2-3-1 Using the pencil hardness technique in accordance with FTMS-141, the change in hardness of the test coating shall be less than the change in hardness on the control coating.

3.2.2.3.2 MOP 2-3-3 Same as MOP 1-2-1

3.2.2.3.3 MOP 2-3-4 Same as MOP 2-1-3

**3.3 COI-3:** Do the test coating systems provide improved appearance characteristics over the control coating system?

3.3.1 Scope Appearance characteristics is comprised of cleanability of the coating system, color and gloss stability of the coating system over time and after touch-up and repair, and lastly fluid resistance of the coating system. The test coating systems shall show improved performance in these areas over the control coating system in order to pass this COI.

3.3.2 Measures of Effectiveness/Performance and Evaluation Criteria

**3.3.2.1 MOE 3-1** The cleanability of the test coating systems shall be an improvement over the currently used coating systems.

3.3.2.1.1 MOP 3-1-1 Same as MOP 2-2-1

3.3.2.1.2 MOP 3-1-2 Same as MOP 2-1-1

3.3.2.1.3 MOP 3-1-3 Same as MOP 2-1-2

3.3.2.1.4 MOP 3-1-4 Same as MOP 2-1-3

**3.3.2.2 MOE 3-2** The color stability of the test coating systems shall be an improvement over the currently used coating systems.

3.3.2.2.1 MOP 3-2-1 Same as MOP 2-3-3

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3.3.2.2.2 MOP 3-2-2 Use of a black velvet cloth in accordance with ASTM ??? shall not show evidence of chalking.

3.3.2.2.3 MOP 3-2-3 Same as MOP 2-1-3

**3.3.2.3 MOE 3-3** The gloss stability of the test coating systems shall be an improvement over the currently used coating systems.

3.3.2.3.1 MOP 3-3-1 Same as MOP 2-1-1

3.3.2.3.2 MOP 3-3-2 Same as MOP 2-1-2

3.3.2.3.3 MOP 3-3-3 Same as MOP 2-1-3

**3.3.2.4 MOE 3-4** The fluid resistance stability of the test coating systems shall be an improvement over the currently used coating systems.

3.3.2.4.1 MOP 3-4-1 Same as MOP 2-3-1

3.3.2.4.2 MOP 3-4-2 Same as MOP 1-2-1

3.3.2.4.3 MOP 3-4-3 Same as MOP 2-3-3

3.3.2.4.4 MOP 3-4-4 Same as MOP 2-1-3

**3.3.2.5 MOE 3-5** The touch-up/repaired area shall show an improvement relative to color and gloss over the currently used coating systems.

3.3.2.5.1 MOP 3-5-1 Same as MOP 2-3-3

3.3.2.5.2 MOP 3-5-2 Same as MOP 2-1-1

3.3.2.5.3 MOP 3-5-3 Same as MOP 2-1-2

3.3.2.5.4 MOP 3-5-4 Same as MOP 2-1-3

#### SECTION IV ADMINISTRATION

### **4.0 TEST MANAGEMENT**

#### 4.1 TASKING

Coatings Technology Integration Office (CTIO) shall:

1.) Develop a Test Plan for conduct of QOT&E

2.) Fund and coordinate delivery of test coating systems to ALCs

3.) Lead the engineering team in performing tests and collecting data on the test aircraft on the six month technical evaluation of the test coating systems.4.) Draft and coordinate the Interim Test Reports 30 days after the six month technical evaluations.

### OC/ALC shall:

1.) Appoint a Test Manager/Director (Donna Ballard, OC/ALC/LAPEP, (405)736-5986)

2.) Apply US Paint test coating system on KC-135 aircraft, tail number 64-14838 3.) Coordinate with SM-ALC the application of remaining test coating systems on KC-135 aircraft, tail numbers 64-14832 and 59-1472.

SM/ALC shall:

1.) Apply Deft control coating system and Courtaulds test coating system on KC-135 aircraft, tail number 64-14832.

2.) Apply Pratt & Lambert (Sherwin-Williams) test coating system and Spraylat test coating system on KC-135 aircraft, tail number 59-1472

### HQ AMC/LGBEF shall:

1.) Coordinate use of one KC-135 aircraft, tail number 64-14838

2.) Coordinate with HQ ANG/LGMM the providing of two KC-135 aircraft, tail numbers 64-14832 and 59-1472

3.) Coordinate with the field unit at MacDill AFB on responsibilities

4.) Coordinate with the field unit at Hickam AFB on responsibilities

### HQ ANG/LGMM shall:

1.) Provide two KC-135 aircraft, tail numbers 64-14832 and 59-1472

### 6<sup>th</sup> MXS/LGMF, MacDill AFB shall:

- 1.) Complete "Post Wash Evaluation Form" and send to CTIO.
- 2.) Coordinate with local bio environmental engineering office for the use of the test coating systems.
- POC: Jerry Chaplin 6<sup>th</sup> MXS/LGMF 7607 Hanger Loop Drive MacDill AFB, FL. 33621 DSN 968-7436

### 154 MXS/LGMF, Hickham AFB shall:

- 1.) Complete "Post Wash Evaluation From" and send to CTIO.
- 2.) Coordinate with local bio environmental engineering office for the use of the test coating systems.
- POC: Gary Cera MSG/E-7 154 MXS/LGMF

360 Harbor Drive, Bldg. 1055 Hickham AFB, Hi. 96853-5517 DSN

### **4.2 TRAINING REQUIREMENTS.**

Coating system manufacturers will be present to monitor the application process and instruct maintenance personnel on the application procedures.

### **4.3 SAFETY and ENVIRONMENTAL IMPACT**

All equipment and coating systems used in this test plan meet 1998 NESHAP requirements.

Material Safety Data Sheet (MSDS) for the test and control coating systems will be provided along with the materials to the using organizations.

**4.4 SECURITY** All aspects of this QOT&E project is **UNCLASSIFIED**; however, technical papers and reports generated from this project will comply with distribution statement B stated in AFI 61-204.

#### **SECTION V REPORTING**

### **5.0 REPORTS**

5.0.1 Inspection Sheets: Post Wash Evaluation Sheets will be accomplished by MacDill AFB and Hickam AFB after each wash cycle and sent to the HQ AMC/LGBEF, OC-ALC/LAPEP, and CTIO.

5.0.2 Interim Test Event Report: Interim Test Event Report will be issued by CTIO 30 days after each technical evaluation. A technical evaluation will be performed by the technical engineering team on 6 month cycles starting from when the last test aircraft is coated.

5.0.3 Final Test Report: Final Test Report will be issued by CTIO 60 days after the completion of the project.

### **5.1 BRIEFINGS**

Status briefings will be given to the CTSC on a quarterly basis by the CTIO.

### AEROSPACE COATING SERVICE TEST APPLICATION DATA SHEET

Personnel:	<b>.</b>
Depaint Method Used: (Include Manu. and Product ID of Chemicals, Dwell Times, e Describe pre-treatment steps of aircraft after depaint and prior to prime:(Include Man and Product ID of Chemicals, Mix Ratios, Dwell Times, etc.)	
Describe pre-treatment steps of aircraft after depaint and prior to prime:(Include Man and Product ID of Chemicals, Mix Ratios, Dwell Times, etc.)	
and Product ID of Chemicals, Mix Ratios, Dwell Times, etc.)	
	nu.
Describe problems experienced with pre-treatment, if any:	
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### AEROSPACE COATING SERVICE TEST APPLICATION DATA SHEET

Manufacturer Name/Product Number:         Batch Number:         Was Primer Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO         Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:         Other Comments:       Manufacturer Name/Product Number:         Batch Number:       Was Topcoat Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO         Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Humidity:       Manufacturer Name/Product Number:         Batch Number:       Manufacturer Name/Product Number:         Batch Number:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:       (min)         Temperature:       Humidity:       Manufacture:	Primer
Was Primer Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO         Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:         Other Comments:       (min)         Topcoat       Manufacturer Name/Product Number:         Batch Number:       (min) Viscosity:         Was Topcoat Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO         Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:	Manufacturer Name/Product Number:
Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:         Other Comments:       (min)         Topcoat       Manufacturer Name/Product Number:         Batch Number:       (min)         Was Topcoat Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO         Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:	Batch Number:
Time After Mixing before Spraying Begins:(min) How Long to Spray this Batch:(min) Temperature:Humidity: Other Comments: Other Comments: Topcoat Manufacturer Name/Product Number: Batch Number: Was Topcoat Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO Mixing Time:(min) Viscosity: Time After Mixing before Spraying Begins:(min) How Long to Spray this Batch:(min) Temperature:Humidity:	Was Primer Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO
How Long to Spray this Batch:	Mixing Time:(min) Viscosity:
Temperature:       Humidity:         Other Comments:	Time After Mixing before Spraying Begins:(min)
Other Comments:	How Long to Spray this Batch:(min)
Topcoat         Manufacturer Name/Product Number:         Batch Number:         Batch Number:         Was Topcoat Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO         Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:	Temperature:Humidity:
Topcoat         Manufacturer Name/Product Number:         Batch Number:         Batch Number:         Was Topcoat Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO         Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:	Other Comments:
Manufacturer Name/Product Number:         Batch Number:         Was Topcoat Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO         Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:	
Batch Number:	Topcoat
Was Topcoat Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO         Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:	Manufacturer Name/Product Number:
Mixing Time:       (min) Viscosity:         Time After Mixing before Spraying Begins:       (min)         How Long to Spray this Batch:       (min)         Temperature:       Humidity:	Batch Number:
Time After Mixing before Spraying Begins:(min)      How Long to Spray this Batch:(min)      Temperature:Humidity:	Was Topcoat Allowed to Achieve Spray Booth Temp Prior to Mixing: YES NO
How Long to Spray this Batch: (min) Temperature:Humidity:	Mixing Time:(min) Viscosity:
Temperature:Humidity:	Time After Mixing before Spraying Begins:(min)
	How Long to Spray this Batch: (min)
Other Comments:	Temperature:Humidity:
	Other Comments:

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### AEROSPACE COATING SERVICE TEST APPLICATION DATA SHEET

Painting Equipment	
Type Paint Guns (HVLP, Electrostatic, etc.):	
Manufacturer/Model of Paint Guns:	
Number of Tip and Aircap:	
Size/Type Paint Gun Heads:	
Inside Dimensions of Hoses: AirFluid	
Hose Length: AirFluid:	
Pressure Pots YES NO Plural Mix YES NO	
Auto Stirring in Cups/Pots YES NO	
Shop Air Pressure: (PSI)(CFM)	
Air Pressure (at Gun):Nozzle:	
Water/Oil Separator Installed: YES NO	

### AEROSPACE COATING SERVICE TEST CURE TIMES DATA SHEET

Tack-free Time       Hours         Cure Time Before Overcoating:       Houring         During Cure – Temperature       Humidity         Dry Film Thickness:       Mils         Appearance of Primer:       Mils         Tack-free Time:       Hours         Cure Time Before Flight:       Hours         During Cure – Temperature       Humidity         Ory Film Thickness:       Hours         During Cure – Temperature       Humidity         During Cure – Temperature       Mils         Appearance of Topcoat:       Mils	Primer			-
During Cure – Temperature Humidity   Dry Film Thickness:Mils   Appearance of Primer:   Topcoat   Tack-free Time:Hours   Cure Time Before Flight:Hours   During Cure – TemperatureHumidity   Wet Tape Test:Mils	Tack-free Time	•		_ Hours
Dry Film Thickness:Mils Appearance of Primer:Mils Topcoat Tack-free Time:Hours Cure Time Before Flight:Hours During Cure – TemperatureHumidity Wet Tape Test:Mils	Cure Time Before Overcoating:			_Hours
Appearance of Primer:   Topcoat   Tack-free Time:  Hours   Cure Time Before Flight:  Hours   During Cure – Temperature  Humidity   Wet Tape Test:  Mils	During Cure – Temperature	Humidity		<b></b>
Topcoat         Tack-free Time:      Hours         Cure Time Before Flight:      Hours         During Cure – Temperature       Humidity         Wet Tape Test:      Mils	Dry Film Thickness:		Mils	
Tack-free Time:Hours Cure Time Before Flight:Hours During Cure – TemperatureHumidity Wet Tape Test: Dry Film Thickness:Mils	Appearance of Primer:			
Cure Time Before Flight:  Hours    During Cure – Temperature  Humidity    Wet Tape Test:  Dry Film Thickness:Mils	<u>Topcoat</u>			
During Cure – Temperature Humidity   Wet Tape Test: Dry Film Thickness:Mils	Tack-free Time:			_Hours
Wet Tape Test:     Dry Film Thickness:   Mils	Cure Time Before Flight:			Hours
Dry Film Thickness:Mils	During Cure – Temperature	Humidity		
· · · · · · · · · · · · · · · · · · ·	Wet Tape Test:			
Appearance of Topcoat:	Dry Film Thickness:		Mils	
	Appearance of Topcoat:			
	• • • • • • • •			

	ant an				Gene	era	l Info	rm	ation				
Today's Date					Ai	rcr	aft Type						
Inspector	Inspector						Ta	Tail No.					
Parked in: Hange	er 🗌 o	r on F	light	Line			Tc	otal	Flight H	lours	5		· ·
					Coat	ing	z Info	rm	ation				
Painted by	<u></u>	<u></u>	*******		cation			<u> </u>	<u></u>		<u>.</u>	I	Date
Surface Preparati	on	****		-1								-1	
Primer				Mar	ufact	ure	r				Batcl	n N	lo.
Topcoat				Man	ufact	ure	r				Batch	ı N	10.
	X. Ani e San Ani	Ex	posu	re C	ondi	tio	ns thi	s F	Reportin	ig P	Perio	1	
Avg. Ground Temp.			>80° ]	F. 🗌		5	0° -80°	F. [			0° F. [		
Avg. Ground Humid	ity		> 809	_			0 % - 8		RH 🗌	_	0% RH	Ι	
Avg. Ground Light		·	Outsi				langer				xed [	]	
					Cher	nic	cal Ex	cpo	sure				
Chemica	l Type		I	Degra	ating adatio		Com	ner	its			•	
				_	erved								
	Yes	No	7	Yes	No								
Hydraulic													
Fuel													
De-Icing Fluid													
Engine Oil													
					Air	cra	aft - 1	Wa	ish				
Area Washed	-			Da		_	ash Che		a second a s	Тур	e, Mfg	g., F	Product No., Name, Mix
Exterior						1.0							
Hot Water Used: Yes	- D	• 🗌											
Other (Exhaust Track Port, etc)	cs, APU '	Track,	Gun								<u></u>		

	N	Aaintenance - Touch-U	Jp Painting		
Area Touched-Up	Date	Primer: Mil Spec /Mfg. Topcoat: Mil Spec /Mfg.	Application Method	Reason for Repair	
Wing, Upper Surface				•	
Wing, Lower Surface		·			
Wing, Leading Edge					
Fuselage, Top				· ·	
Fuselage, Sides					
Fuselage, Bottom					
Empennage					
Stabs, Vertical					
Stabs, Horizontal					
		Visual Inspect	ion		
Area	Rectanded and the	Defect	112 contraction of the	Cause	Size
					(sq. in.)
Wing, Right, Upper Su	rface	None Chip Stain Blister Chalk Sof	ten	Fluid Air Flow IImpact Unknown	
Wing, Right, Lower Su	ırface	Other	Peel I	Fluid Air Flow Impact	
	· · · ·	Other	The second se	Unknown	
Wing, Right, Leading I	Edge	None Chip Stain Blister Chalk Sof	ten I	Fluid Air Flow []Impact	
Wing, Left, Upper Sur	face	OtherOtherStain		Unknown Fluid	
		Blister Chalk Sof		Air Flow Impact Unknown	
Wing, Left, Lower Sur	face	None Chip Stain Blister Chalk Sof	ten 🔲	Fluid Air FlowImpact	
Wing, Left, Leading Ed	dge	Other None Chip Stain Blister Chalk Sof	Peel I	Unknown Fluid Air FlowImpact	<u> </u>
		Blister Chalk Sof		Unknown	
Fuselage, Right, Upper	Surface	None Chip Stain		Fluid	
	andra andra ministrational andra andra andra andra and	Blister Chalk Sof	a second at a second	Air Flow Impact	

Fuselage, Right, Lower Surface	None Chip Stain Peel	Fluid
rusciage, Rigin, Lower Burlace	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Tracelege LeC II.		
Fuselage, Left, Upper Surface	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Fuselage, Left, Lower Surface	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Empennage	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air Flow Impact
	Other	
Stabilizer, Vertical, Right Side	None Chip Stain Peel	Fluid
Statistics, vortion, right blue	Blister Chalk Soften	Air Flow Impact
Stabilizer, Vertical, Left Side		
Stabilizer, Vertical, Left Side		Fluid
		Air Flow Impact
	Other	
Stabilizer, Right Horizontal,	None Chip Stain Peel	Fluid
Upper Surface	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Stabilizer, Right Horizontal,	None Chip Stain Peel	Fluid
Lower Surface	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Stabilizer, Left Horizontal,	None Chip Stain Peel	Fluid
Upper Surface	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Stabilizer, Left Horizontal,	None Chip Stain Peel	Fluid
Lower Surface	Blister Chalk Soften	Air Flow Impact
		Unknown
#1 Engine Cowling/Intake	None Chip Stain Peel	Fluid
	Blister Chalk Soften	
	Other	Air Flow Impact
#2 Engine Cowling/Intake		
#2 Engine Cowing/Intake	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
#3 Engine Cowling/Intake	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air FlowImpact
	Other	Unknown
#4 Engine Cowling/Intake	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air Flow Impact
	Other	

verall Comm	ents				
			-		
				•	

	Gen	eral Inform	ation				
Today's Date		Aircr	aft Typ	e			
Inspector		Seria	No.				
Title of Inspector		No. o	No. of Flight Hours				
Date of Last Inspection		· · · · · · · · · · · · · · · · · · ·					
	Co	ating Informa	tion				
Painted by	Locati	on			Date		
Surface Preparation							
Primer	Manufacturer			Batch 1	<b>і</b> о.		
Topcoat	Manufacturer			Batch N	۱o.		
	Ex	posure Condit	ions				
Avg. Ground Temp.	>80° F.	50° -80° F.		<50° F.			
Avg. Ground Humidity	> 80% RH	50 % - 80% RI	I 🗌	<50% RH	]		
Avg. Ground Light	Outside	Hanger		Mixed 🗌			
		sual Inspect	ion				
Area/Tests	Location / Subst	and the second	the second s	fect	Size (sq. in.)		
Wing, Right - Upper Surface				sion			
oppor burrate		NO STEP		pping			
		(4 typ)	Blistering		· · · ·		
		6					
		Stai	ns				
		6 11		rosion			
		HI	Oth	er(Specify)			
		$\mathcal{A}$					
		11					
		dT					
		1/					
	1/0 2	1					
Wing, Right - Lower Surface			Ero	sion			
	<del></del>	7		pping			
		-(	Bli	stering			
		$\backslash \backslash$	Pee	ling			
	Stripe	$\langle \rangle$		alking			
		М	Sta	ins Tosion			
		H					
	Black				<u> </u>		
, i i i i i i i i i i i i i i i i i i i	Buick Stripe						
		> 1					
					1		
· ·		14	14 - 18 - 18 - 18 - 18 - 18 - 18 - 18 -		1		

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Wing, Left - Upper Surface       Image: Charlong Char	Area	Location / Substrate	Defect	Size (sq. in.)
Wing, Left - Lower Surface       Interface       Interface <t< td=""><td></td><td></td><td></td><td></td></t<>				
Wing, Left - Lower Surface       Erosion         Bistering       Corrosion         Bistering       Corrosion         Bistering       Corrosion         Wing, Left - Lower Surface       Erosion         Environment       Chipping         Bistering       Peeling         Chronic Specify)       Erosion         Stains       Corrosion         Stains       Corrosion         Chipping       Bistering         Peeling       Chalking         Stains       Corrosion         Other(Specify)       Other(Specify)         Stains       Corrosion         Chipping       Bistering         Peeling       Chalking         Stains       Corrosion         Other(Specify)       Other(Specify)         Fuselage, Forward Section       Erosion         Stains       Corrosion         Other(Specify)       Erosion         Stains       Corrosion         Stains       Corrosion         Chipping       Elstering         Peeling       Chalking         Stains       Corrosion		[6] [6]		
Wing, Left - Lower Surface       Image: Corrosion Corros			Blistering	_
Wing, Left - Lower Surface       Image: Chalking Stains         Bits       Corrosion         Wing, Left - Lower Surface       Image: Chalking         Bits       Chipping         Bits       Chalking         Stains       Corrosion         Other (Specify)       Image: Chalking         Bits       Chipping         Bits       Chalking         Stains       Corrosion         Other (Specify)       Image: Chalking         Fuselage, Forward Section       Image: Chalking         Fuselage, Forward Section       Image: Chalking         Stains       Corrosion         Other (Specify)       Image: Chalking         Stains       Corrosion         Chipping       Image: Chalking         Stains       Corrosion         Other (Specify)       Image: Chalking         Stains       Corrosion         Chipping       Image: Chalking         Stains       Corrosion         Chalking       Stains         Corrosion       Chipping         Stains       Corrosion				
Wing, Left - Lower Surface       Image: Stains Corrosion Other(Specify)         Wing, Left - Lower Surface       Image: Stains Corrosion Other(Specify)         Bisting       Bistering         Peeling       Chalking         Stains       Corrosion         Other(Specify)       Other(Specify)         Fuselage, Forward Section       Image: Stains         Fuselage, Forward Section       Image: Stains         Stains       Corrosion         Other(Specify)       Image: Stains         Fuselage, Forward Section       Image: Stains         Stains       Corrosion         Other(Specify)       Image: Stains		I In HI	Chalking	
Wing, Left - Lower Surface       Erosion         Birth       Erosion         Bistering       Peeling         Corrosion       Other(Specify)         Bistering       Peeling         Chalking       Stains         Corrosion       Other(Specify)         Fuselage, Forward Section       Erosion         Eng       Chalking         Bistering       Peeling         Corrosion       Other(Specify)		4		
Wing, Left - Lower Surface       Erosion         Bits       Chipping         Bits       Bits         Bits       Corrosion         Other(Specify)       Other(Specify)         Fuselage, Forward Section       Erosion         Fuselage, Forward Section       Erosion         Corrosion       Chipping         Bitstering       Peeling         Chalking       Stains         Corrosion       Chipping         Bitstering       Peeling         Chalking       Stains         Corosion       Chipping         Stains       Corosion				f
Wing, Left - Lower Surface       Erosion         Bilistering       Peeling         Chalking       Stains         Corrosion       Other(Specify)         Fuselage, Forward Section       Erosion         Fuselage, Forward Section       Erosion         Chalking       Blistering         Peeling       Corrosion         Other(Specify)       Chalking         Stains       Corrosion         Other(Specify)       Chalking         Stains       Corrosion         Other(Specify)       Chalking         Stains       Corrosion         Other(Specify)       Corrosion         Stains       Corrosion         Other(Specify)       Corrosion				
Wing, Left - Lower Surface       Erosion         Bistering       Peeling         Chalking       Stains         Corrosion       Other(Specify)         Fuselage, Forward Section       Erosion         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion         Other(Specify)       Stains         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chipping         Stains       Corrosion         Other(Specify)       Stains		V. HI	Omer(Specify)	
Wing, Left - Lower Surface       Erosion         Bistering       Peeling         Chalking       Stains         Corrosion       Other(Specify)         Fuselage, Forward Section       Erosion         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion         Other(Specify)       Stains         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chipping         Stains       Corrosion         Other(Specify)       Stains		In AT		
Wing, Left - Lower Surface       Erosion         Bistering       Peeling         Chalking       Stains         Corrosion       Other(Specify)         Fuselage, Forward Section       Erosion         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion         Other(Specify)       Stains         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chipping         Stains       Corrosion         Other(Specify)       Stains				
Wing, Left - Lower Surface       Erosion         Bistering       Peeling         Chalking       Stains         Corrosion       Other(Specify)         Fuselage, Forward Section       Erosion         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion         Other(Specify)       Stains         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chipping         Stains       Corrosion         Other(Specify)       Stains				
Wing, Left - Lower Surface       Erosion         Bistering       Peeling         Chalking       Stains         Corrosion       Other(Specify)         Fuselage, Forward Section       Erosion         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion         Other(Specify)       Stains         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chipping         Stains       Corrosion         Other(Specify)       Stains				
Wing, Left - Lower Surface       Erosion         Bitstering       Blistering         Peeling       Chalking         Stains       Corrosion         Other(Specify)       Other(Specify)         Fuselage, Forward Section       Erosion         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion         Corrosion       Corrosion         Other(Specify)       Chalking         Stains       Chipping         Stains       Chipping         Stains       Chipping         Stains       Chipping         Stains       Chipping         Stains       Corrosion         Chalking       Stains         Corrosion       Corrosion		NO STEP D		
Wing, Left - Lower Surface       Erosion         Bitstering       Blistering         Peeling       Chalking         Stains       Corrosion         Other(Specify)       Other(Specify)         Fuselage, Forward Section       Erosion         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion         Corrosion       Corrosion         Other(Specify)       Chalking         Stains       Chipping         Stains       Chipping         Stains       Chipping         Stains       Chipping         Stains       Chipping         Stains       Corrosion         Chalking       Stains         Corrosion       Corrosion		FWD (6 typ)		
Fuselage, Forward Section       Erosion         Elistering       Erosion         Chilking       Stains         Corrosion       Other(Specify)         Stains       Corrosion         Other(Specify)       Stains         Erosion       Chilpping         Blistering       Peeling         Corrosion       Corrosion         Other(Specify)       Stains         Corrosion       Chilpping         Blistering       Peeling         Chilpping       Blistering         Stains       Corrosion         Chilpping       Stains         Corrosion       Chilpping	Wing, Left - Lower Surface			
Fuselage, Forward Section       Erosion         Elistering       Erosion         Chilking       Stains         Corrosion       Other(Specify)         Stains       Corrosion         Other(Specify)       Stains         Erosion       Chilpping         Blistering       Peeling         Corrosion       Corrosion         Other(Specify)       Stains         Corrosion       Chilpping         Blistering       Peeling         Chilpping       Blistering         Stains       Corrosion         Chilpping       Stains         Corrosion       Chilpping		$\square$	Chipping	
Fuselage, Forward Section       Erosion         Chiking       Stains         Corrosion       Other(Specify)         Event       Erosion         Chipping       Blistering         Peeling       Chipping         Blistering       Peeling         Chalking       Stains         Corrosion       Chalking         Stains       Corrosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion			Blistering	
Fuselage, Forward Section       Erosion         Chilking       Stains         Corrosion       Other(Specify)         Erosion       Chipping         Blistering       Peeling         Chalking       Stains         Corrosion       Other(Specify)		Black	Peeling	
Fuselage, Forward Section       Stains         Generation       Erosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion         Other (Specify)       Corrosion		Stripe		
Fuselage, Forward Section       Corrosion         Generation       Erosion         Corrosion       Corrosion         Generation       Erosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion         Corrosion       Chipping         Stains       Corrosion         Corrosion       Corrosion			Stains	· / · · · · · · · · · · · · · · · · · ·
Birth       Other(Specify)         Fuselage, Forward Section       Erosion         Fuselage, Forward Section       Erosion         Chipping       Blistering         Peeling       Chalking         Stains       Corrosion         Charlen (Specify)       Charlen (Specify)				
Fuselage, Forward Section  Chipping  Blistering  Peeling  Chalking  Stains  Corrosion  Chipping  Stains  Corrosion  Chipping  Stains  Corrosion  Constant  Con				· · · · · · · · · · · · · · · · · · ·
Chipping       Blistering       Peeling       Chalking       Stains       Corrosion		Stripe		,
Chipping       Blistering       Peeling       Chalking       Stains       Corrosion		$r \rightarrow 1$		
Chipping       Blistering       Peeling       Chalking       Stains       Corrosion		TA		
Chipping       Blistering       Peeling       Chalking       Stains       Corrosion				·
Chipping       Blistering       Peeling       Chalking       Stains       Corrosion				
Chipping       Blistering       Peeling       Chalking       Stains       Corrosion		/ 4		
Chipping       Blistering       Peeling       Chalking       Stains       Corrosion				
Blistering       Peeling       Chalking       Stains       Corrosion	Fuselage, Forward Section			
Peeling       Chalking       Stains       Corrosion				
Chalking Stains Corrosion				
Stains Corrosion				
Stains Corrosion			Chalking	
Corrosion			Stains	
			Corrosion	
		Top View	Other(Specify)	
			· · ·	
		$\boldsymbol{C}$		
			,	
Bottom View		Bottom View		
	l			

Attea     Detect     Size (sq. in.)       Fuselage - Top Surface     Erosion     Chipping       Blistering     Peeling       Chalking     Stains       Stains     Corrosion       Other(Specify)     Other(Specify)	Area	I a setion / Only starts	D.C.	
Chipping         Blistering         Peeling         Chalking         Stains         Corrosion         Other(Specify)		Location / Substrate	Defect	Size (sq. in.)
Bistering       Pecling       Chalking       Stains       Corrosion       Other(Specify)	Fuselage - Top Surface		Erosion	
Peeling         Chalking         Stains         Corrosion         Other(Specify)			Chipping	
Chalking       Stains       Corrosion       Other(Specify)			Blistering	
Stains       Corrosion       Other(Specify)			Peeling	
Corrosion         Other(Specify)         Other(Specify)         Fuselage - Bottom Surface         Erosion         Chilking         Blistering         Peeling         Chalking         Stains         Corrosion			Chalking	
Other(Specify)       Other(Specify)       Other(Specify)       Other(Specify)       Image: Constraint of the second secon			Stains	
Fuselage - Bottom Surface     Erosion       Erosion     Chipping       Blistering     Peeling       Chalking     Stains       Corrosion     Corrosion			Corrosion	
Fuselage - Bottom Surface     Erosion       Chipping       Blistering       Peeling       Chalking       Stains       Corrosion		1	Other(Specify)	<u> </u>
Chipping Blistering Peeling Chalking Stains Corrosion				
Stains Corrosion	Fuselage - Bottom Surface		Chipping Blistering Peeling	
Corrosion			Chalking	
Corrosion Other(Specify)			Stains	· · · · · · · · · · · · · · · · · · ·
Other(Specify)			Corrosion	
			Other(Specify)	

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Area	Location / Substrate	Defect	Size (sq. in.)
Fuselage, Left Side		Erosion	· · · · · · · · · · · · · · · · · · ·
		Chipping	
		Blistering	
		Peeling	
		Chalking	
	<i>•</i>	Stains	
		Corrosion	
· · · · · · · · · · · · · · · · · · ·		Other(Specify)	
Angle of Attack Frobs	Jat Fuel : Fast Actin O	g Door	
	o D Light		
$\backslash \square$	$\langle \rangle$		
٥	$\Box \Box$		
Fuselage, Right Side		Erosion	[
		Chipping	
		Blistering	
		Peeling	
		CI. II.	
		Chalking	
		Stains	
		Stains Corrosion	
		Stains	
AC	Stars and Bars	Stains Corrosion Other(Specify)	ERGENCY, NESCUE
	Window	Stains Corrosion Other(Specify)	Angle of Attack Probe
	Window	Stains Corrosion Other(Specify)	O Angle of Attack

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Area	Location / Substrate	Defect	Size (sq. in.)
Stabilizer, Vertical Right Side		Erosion	
_		Chipping	
		Blistering	
		Peeling	
		Chalking	
		Stains	
		Corrosion	
		Other(Specify)	
Stabilizer, Vertical, Left Side		Erosion	
Submizer, Vertical, Left Side		Chipping	
	71		
		Blistering	
		Peeling	
		Chalking	
		Stains	
		Corrosion	
		Other(Specify)	· · · · · · · · · · · · · · · · · · ·
0.1111			
Stabilizer, Horizontal, Right		Erosion	
Top Surface		Chipping	
		Blistering	
· · · ;		Peeling	
		Chalking	
		Stains	
		Corrosion	
		Other(Specify)	
			· · · · · · · · · · · · · · · · · · ·
· · · · ·			
Stabilizer, Horizontal, Right		Erosion	
Bottom Surface		Chipping	
		Blistering	
		Peeling	
		Chalking	
	<b>V V</b>	Stains	
		Corrosion	······································
		Other(Specify)	
		Suici (Specify)	· · · · · · · · · · · · · · · · · · ·
	$\mathbf{X} \setminus \mathbf{I}$		
		1	

Area	Location / Substrate	Defect	Size (sq. in.)
Stabilizer, Horizontal, Left		Erosion	
Top Surface		Chipping	
		Blistering	-
		Peeling	
		Chalking	
		Stains	
		Corrosion	
		Other(Specify)	
Stabilizer, Horizontal, Left		Erosion	
Bottom Surface		Chipping	
		Blistering	
		Peeling	
		Chalking	
	$  \rangle \langle \eta$	Stains	
		Corrosion	
		Other(Specify)	

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Today's Date				-				Aircraft Type							
Inspector							Tai	Tail No.							
Parked in: Hange	r 🗌 or	on F	light	Line			Tot	al	Flight	Ho	ours				
					Coati	ng	Infor	m	ation	- 					
Painted by				Lo	cation	1					ľ	Date	;		
Surface Preparation	on										Ł				
Primer				Man	ufacti	ure	r				Batch	No.		φ <sub>αλι</sub> δας 1.,1	
Topcoat				Man	ufacti	ure	r				Batch	No.			
		Exr	osu	re Ç	ondit	tio	ns this	5 I	Report	in	g Period				
Avg. Ground Temp.			>80°		<u>.</u>	5	0° -80° F				<50⁰ F. [	]			
Avg. Ground Humid	ity			% RH		_	0 % - 80	)%	RH 🗌		<50% RH				
Avg. Ground Light			Outsi		]		langer [				Mixed 🗌	 			
	and a second				Cher	nic	al Ex	pc	osure						
Chemica	l Type		]	Degra	ating adatio erved		Comn	nei	nts						
	Yes	No		Yes	No										
Hydraulic								-							
Fuel															
De-Icing Fluid															
Engine Oil			-												
					' Air	cr	aft - V	N	ash				li Riviti		
Area Washed				Da	ate	Wa Ra		n.	- Mil Sp	ec,	Type, Mfg.	, Prod	luct No	o., Namo	e, Mix
Exterior									***						
Hot Water Used: Yes	5 🗌 No	• 🗌													
Other (Exhaust Track Port, etc)	cs, APU '	Track,	Gun						<u>,                                 </u>						

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	N - V	Agintenance - Touch-Up	Painting		Section
Area Touched-Up	Date	Primer: Mil Spec /Mfg. Topcoat: Mil Spec /Mfg.	Application Method	Reason for Repair	
Wing, Upper Surface				-	
Wing, Lower Surface					•
Wing, Leading Edge					
Fuselage, Top				•	
Fuselage, Sides					
Fuselage, Bottom					
Empennage		· · · · · · · · · · · · · · · · · · ·	. <u></u>		
Stabs, Vertical					
Stabs, Horizontal					
		Visual Inspection			
Area		Defect		Cause	Size (sq. in.)
Wing, Right, Upper Su	rface	None Chip Stain	Peel F	luíd	· · · · · · ·
		Blister Chalk Soften	A	ir Flow Impact	
Wing, Right, Lower Su	rface	None Chip Stain P		luid	
۰ ۳۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰ - ۲۰۰۰		Blister Chalk Soften	the second se	ir Flow Impact	
Wing, Right, Leading H	Edge	None Chip Stain P		luid	
· · · ·		Blister Chalk Soften		ir Flow Impact	
Wing, Left, Upper Surf	ace			luid	
		Blister Chalk Soften		ir Flow Impact	
Wing Loft Lower Surf		OtherOtherP		inknown	
Wing, Left, Lower Surf	ace	None Chip Stain P Blister Chalk Soften		luid ir FlowImpact	
		Other		nknown	
Wing, Left, Leading Ed	lge			luid	
		Blister Chalk Soften		ir Flow Impact	
Fuselage, Right, Upper	Surface	None Chip Stain P		luid	
		Blister Chalk Soften		ir Flow Impact	
الا المراجع المراجع الم المراجع المراجع المراجعة المراجع		Other		nknown	

Fuselage, Right, Lower Surface	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Fuselage, Left, Upper Surface	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Fuselage, Left, Lower Surface	None Chip Stain Peel	Fluid
6	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Empennage	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Stabilizer, Vertical, Right Side	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air Flow Impact
	Other	
Stabilizer, Vertical, Left Side	None Chip Stain Peel	
Stabilizer, Vertical, Left Side	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Stabilizer, Right Horizontal,	None Chip Stain Peel	Fluid
Upper Surface	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Stabilizer, Right Horizontal,	None Chip Stain Peel	Fluid
Lower Surface	Blister Chalk Soften	Air Flow Impact
	Other	
Stabilizer, Left Horizontal,	None Chip Stain Peel	Fluid
Upper Surface	Blister Chalk Soften	Air Flow Impact
	Other	Unknown
Stabilizer, Left Horizontal,	None Chip Stain Peel	Fluid
Lower Surface	Blister Chalk Soften	Air Flow Impact
	Other	
#1 Engine Cowling/Intake		
#1 Engine Cowing/make	None Chip Stain Peel Blister Chalk Soften	Air Flow Impact
	Other	
#2 Engine Courling(Intoles	None Chip Stain Peel	
#2 Engine Cowling/Intake		Fluid Air Flow Impact
	Blister Chalk Soften	
#2 Engine Couling from the	Other	
#3 Engine Cowling/Intake	None Chip Stain Peel	Fluid
	Blister Chalk Soften	Air Flow Impact Unknown
#4 Engine Coulies Nature	Other_OtherOtherOther_OtherOtherOther_Other_O	
#4 Engine Cowling/Intake		Fluid Air Flow Impact
	Blister Chalk Soften	
	Other	Unknown

Overall Comments				
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