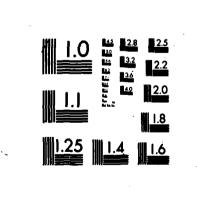
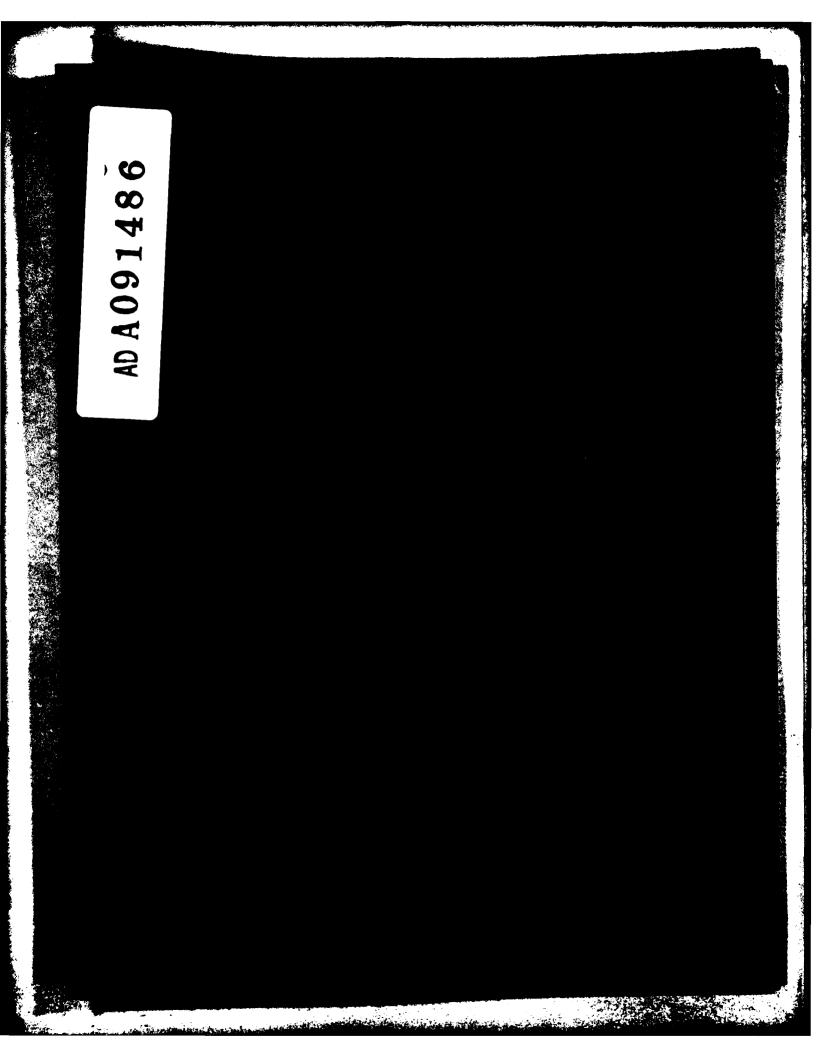


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DELAWARE RIVER BASIN

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PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams for Phase I Investigations. Copies of these guidelines may be obtained from the Office of the Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I investigation is to expeditiously identify those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigations, testing and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify the need for more detailed studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected, and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

Name of Dam: County Located: State Located: Stream: Coordinates: Newtown Dam (SCS PA 621) Bucks County Pennsylvania Newtown Creek Latitude 40° 14.7' Longitude 74° 56.0' July 1, 1980

Date of Inspection: July 1, 1980

Newtown Dam is owned by the Neshaminy Water Resources Authority and maintained by Bucks County. The dam and reservoir are used as a flood control structure for the downstream town of Newtown, Pennsylvania. The impoundment was designed by the United States Department of Agriculture, Soil Conservation Service, in 1976-77, and the structure was officially completed in 1980.

The dam and its appurtenant facilities are considered to be in good condition. The dam is classified as an "Intermediate" size structure with a "High" hazard classification, consistent with its potential in the event of failure for extensive property damage and loss of life downstream of the dam and in Chalfont, Pennsylvania.

In accordance with criteria established by Federal (OCE) Guidelines, the recommended spillway design flood for this "Intermediate" size dam and "High" hazard classification is the Probable Maximum Flood (PMF). The Soil Conservation Service designed this dam as a Class C structure, which requires that the spillway systems be designed to pass the PMF.

The hydrologic and hydraulic computations presented in Appendix D indicate that the spillway structures are capable of discharging the PMF without overtopping the embankment. Therefore, the structure is considered to have an "Adequate" spillway system.

It is recommended that, during the period required for establishment of Crownvetch, the embankment, particularly the downstream berm, be periodically checked for erosion damage.

Neshaminy Water Resources Authority has an "Operations Manual" specifying agencies responsible for operation and maintenance of Neshaminy Watershed projects completed by 1977. The manual requires updating to include Newtown Dam. The Operations Manual refers to a "Development, Operation and

Newtown Dam (SCS PA 621), NDS 1D PA 01064

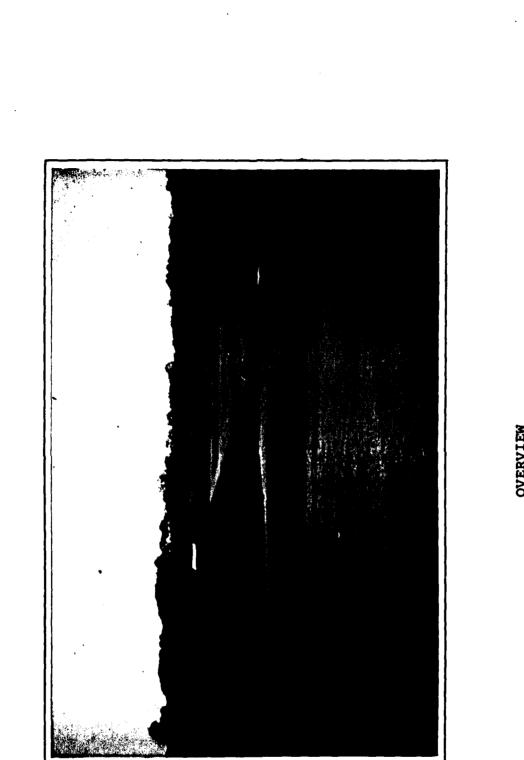
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Maintenance Manual" prepared by SCS for a maintenance inspection checklist, which should be used to insure that all items are periodically inspected and maintained in the best possible condition. It is recommended that these procedures provide for a period of observation during and following impoundment of significant quantities of water behind the embankment. These observations should include monitoring discharge from the embankment drainage system and looking for sources of uncontrolled seepage.

A warning procedure has been developed and approved by the Neshaminy Water Resources Authority. This procedure indicates that the structure should be monitored on a 24 hour basis when the severity of a forecasted storm is predicted to be near, at or above the design capacity of the structure. The procedure also includes emergency telephone numbers and areas downstream of the dam which should be notified in the event a hazardous condition develops.

Mary F. Beck, P.E. Date Pennsylvania Registration 27447E Woodward-Clyde Consultants OF MARYLAN 8 2 80 John M. Frederick, Jr., P.E. Date Maryland Registration 7301 Woodaard-Clyde Consultants John Hen APPROVED BY: PROFESSI here de 5 Sep 30 AMES W. PECK compl. Corps of Engineers Wetrict Engineer



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NEWTOWN DAM (SCS PA 621), NEWTOWN TOWNSHIP, BUCKS COUNTY, PENNSYLVANIA

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM NEWTOWN DAM (SCS PA 621) NATIONAL ID NO. PA 01064 DER NO. 9-178

SECTION 1 PROJECT INFORMATION

1.1 General.

a. <u>Authority</u>. The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.

b. <u>Purpose</u>. The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project.

Dam and Appurtenances. Newtown Dam is a 44 foot high zoned earth embankment about 850 feet long, with an emergency spillway at the left end of the embankment. The embankment contains an impervious core constructed over a cutoff trench under the dam center line. The core and cutoff trench are composed of materials classified as clayey silts and silty gravels (Zone 1), and are encompassed by more permeable materials classified as silty gravels (Zone 2). Plate 5, Appendix E, identifies a Zone 3, which is a 12 inch thick layer of topsoil or clayey silt over the entire downstream face and above the riprap on the upstream face. The upstream design slope is 3H:1V with a ten foot berm at approximately elevation 213. The downstream design slope is 2.5H:1V. Surface runoff is intercepted by a berm on the downstream face. The berm has a positive one percent slope to the right. The cutoff trench bottom width is 12 feet, and upstream and downstream slopes are 2H:1V. The upstream and downstream slopes of the relatively impervious Zone 1 core are 1H:1V. The embankment crest is 14 feet wide and has a design settled fill elevation of 239.6. Both the upstream and downstream slopes are to be protected with Crownvetch, and the crest is protected by a gravel road.

Embankment seepage is controlled by a trench drain about midway between the dam center line and the downstream

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toe. The trench drain is connected to the rock gutter at the downstream toe of the dam by a blanket drain. Embankment seepage in the vicinity of the principal spillway is to be discharged through two eight inch PVC drain pipes which outlet through the sidewalls of the impact basin. Plan and crosssection views of the dam are shown on Plates 2 through 7, Appendix E, and embankment drainage details are shown on Plate 8.

The principal spillway consists of a concrete drop inlet riser, 240 feet of 30 inch diameter reinforced concrete, steel cylinder pressure pipe, with nine anti-seep collars and an impact basin at the downstream toe. The reservoir drain located at the base of the riser has an invert elevation of 199.25, and the elevation of the riser weirs is 213.0. The outlet invert and impact basin end sill elevations are 196.0.

The emergency spillway is a trapezoidal channel excavated through rock around the left end of the embankment. The 185 foot wide channel has side slopes of 3H:1V, and the 50 foot level section (crest) is at elevation 231.9. A tributary to Newtown Creek enters the emergency spillway upstream of the control section through a channel excavated in rock, Photograph 8, Appendix C.

A 16 inch reinforced concrete pressure pipe sanitary sewer passes beneath the dam embankment, as shown on Plate 4, Appendix E. At the dam center line, the sanitary sewer is about 12 feet below the surface of the bedrock and about 10.5 feet below the dam cutoff trench. Four anti-seep collars have been constructed upstream of the dam center line around the sewer. A 12 to 16 foot thick concrete curtain wall was installed beneath the dam cutoff trench around the pipe. The sewer trench was backfilled with Zone 1 materials upstream of the center line and with Zone 2 materials downstream of the center line.

b. Location. The dam is located on Newtown Creek, a tributary to the Neshaminy Creek in Newtown Township, Bucks County, Pennsylvania. The dam is located 1.1 miles north of the center of Newtown, Pennsylvania, and is located on the USGS Quadrangle entitled "Langhorne, Pennsylvania", at coordinates N 40° 14.7' W 74° 56.0'. A regional location plan of Newtown Dam is included as Plate 1, Appendix E.

c. <u>Size Classification</u>. The dam is classified as an "Intermediate" size dam by virtue of its 44 foot height and 1,420 acre-foot total storage capacity.

d. <u>Hazard Classification</u>. A "High" hazard classification is assigned consistent with the potential for extensive property damage and loss of life along Newtown Creek downstream of the dam.

e. <u>Ownership</u>. Newtown Dam is owned by the Neshaminy Water Resources Authority. All correspondence should be sent to Mr. William Taylor, Neshaminy Water Resources Authority, Post Office Box 6, Cross Keys Office Center, 4259 Swamp Road, Doylestown, Pennsylvania 18901.

f. <u>Purpose of Dam</u>. The purpose of this dam is flood control. The structure is one of ten dams in the Neshaminy Creek Watershed that are scheduled for construction with the assistance of the United States Department of Agriculture, Soil Conservation Service (SCS). This is the eighth project of the series.

g. <u>Design and Construction History</u>. The original work plan was developed by the SCS in the late 1960's for the ten flood control sites in the Neshaminy Creek Watershed. The final design for this dam was prepared by SCS in 1976 and 1977, with the final design drawings being completed in 1977. The application to construct a flood control dam and reservoir was submitted July 21, 1977. The Report Upon the Application was prepared by the State of Pennsylvania on September 28, 1977. The project was approved by the Delaware River Basin Commission on September 28, 1977, and the permit was issued on October 3, 1977. On July 13, 1978, the contractor, Riebe Construction Company, was given notice to proceed.

The design drawings for the sanitary sewer under the dam are dated June 30, 1978. On July 20, 1978, the engineer for the Newtown Sewer Authority requested that permission for construction of the sewer under the dam be added to the dam construction permit. On August 14, the state gave permission for the sewer to be constructed under the dam.

In October 1978, the impact basin footers and floor slab were removed and replaced as a result of low concrete strength. Work on the sewer line in the right abutment began November 29, 1978, after work on the dam had shut down for the winter. The embankment was completed by November 1979, and the SCS final inspection was held on July 2, 1980.

h. Normal Operating Procedures. Reservoir outflow is controlled by the principal and emergency spillways. Under normal conditions, the pond drain gate is closed and water flows through the principal spillway over the weirs. Excess water is stored to elevation 231.9, the emergency spillway crest. Water is discharged through the emergency spillway at the left abutment only during storms with recurrence interveof once in 100 years or more.

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1.3 Pertinent Data.

A summary of pertinent data for Newtown Dam is presented as follows.

a.	Drainage Area (square miles)	3.0
b.	Discharge at Dam Site (cfs) Maximum Known Flood at Dam Site Design High Water At Top of Dam (design)	Unknown 2,092 10,967
с.	Elevation (feet above MSL) Top of Dam (design) (existing) Design High Water Emergency Spillway Crest Principal Spillway Weir Crest Pond Drain Inlet Invert Outlet Invert Downstream Toe	239.6 240.4 234.7 231.9 213.0 199.25 196.0 202.2
đ.	Reservoir (feet) Length at Normal Pool Length at Maximum Pool	1,600 4,000
e.	Storage (acre-feet) Normal Pool To Top of Dam	56 1,420
f.	Reservoir Surface Area (acres) Sediment Pool Design High Water	11 82
g.	Volume Length Maximum Height Top Width Side Slopes Upstream (design) Downstream (design) Cutoff	Zoned earth embank- ment 87,600 cubic yards 850 feet 44 feet 14 feet 3H:lV 2.5H:lV Trench beneath dam center line
	Grout Curtain	None

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h.	Principal Spillway Type	Concrete drop inlet riser with 30 inch conduit
	Reservoir Drain	Intake at base of riser
	Elevation	
	Weirs Pond Drain Inlet Invert Conduit Outlet Invert Energy Dissipator	213.0 199.25 196.0 Concrete impact ba- sin at downstream
		toe
i.	Emergency Spillway	
	Туре	Trapezoidal channel excavated through rock
	Width	185 feet
	Side Slopes	3H:1V

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SECTION 2 ENGINEERING DATA

2.1 Design.

a. <u>Data Available</u>. A summary of the available engineering data on Newtown Dam (SCS PA 621) is attached as Appendix B. Engineering data available for review are contained in a several hundred page design folder and a 35 page set of design drawings. As-built drawings are in the process of being prepared by the Soil Conservation Service (SCS) project engineer, and were available for review. The design folder and plans are located in SCS files, and as-built drawings are to be located in the Department of Environmental Resources' (DER) and the Owner's files. All of these records were prepared by the United States Department of Agriculture, Soil Conservation Service. Additional information was obtained from miscellaneous letters, correspondence and monthly construction reports in DER files.

b. <u>Design Features</u>. The principal design features of Newtown Dam are illustrated on the plans and profiles enclosed in Appendix E as Plates 2 through 13. A detailed description of the design features is also presented in Section 1.2, paragraph a, and pertinent data relative to the structure are presented in Section 1.3. In addition to the plans of the dam, Plates 14 and 16 are enclosed to show the locations of the test borings and the results of typical compaction tests performed as part of the design. Typical test boring logs are shown on Plate 15.

2.2 Construction.

Construction history is presented in Section 1.2, paragraph g. Summary construction records are located in DER files. Complete construction records are located in SCS files and were reviewed for this investigation.

2.3 Operational Data.

There are no operational records maintained. There are no minimum flow requirements for the downstream channel. There are no water level measurements or rainfall records maintained within the watershed, although the Neshaminy Water Resources Authority maintains a rain gauge at their office in Cross Keys, Doylestown, Pennsylvania.

2.4 Evaluation.

a. <u>Availability</u>. All engineering data evaluated and reproduced for this report were provided by either DER or SCS, and were supplemented by conversations and data obtained from representatives of the Neshaminy Water Resources Authority.

b. <u>Adequacy</u>. Data included in state files, supplemented with data obtained from the Neshaminy Water Resources Authority and information received from state and authority representatives, are considered adequate to evaluate the dam and appurtenant structures.

c. <u>Validity</u>. There is no reason to guestion the validity of these data.

SECTION 3 VISUAL INSPECTION

3.1 Findings.

a. <u>General</u>. Observations and comments of the field inspection team are contained in the checklist enclosed herein as Appendix A, and are summarized and evaluated as follows. In general, the dam and its appurtenant structures are considered to be in good condition. At the time of the inspection, the pond drain gate was open and stream flow was passing through the riser of the principal spillway.

b. <u>Dam</u>. The vegetation cover on the upstream and downstream faces is in fair condition. Very little Crownvetch is in evidence. The embankment was dormant seeded in the fall and reseeded again this spring. It will be another year before Crownvetch becomes abundant. Little or no damage to the embankment has occurred during the period of vegetation establishment. The crest is protected by a gravel road, Photograph 2, which is uniform with no vehicle ruts or depressions.

The vertical and horizontal alignments were checked and found to be satisfactory. The vertical alignment is shown on Sheet 5B, Appendix A. Junctions between the embankment and abutment and the embankment and spillway were judged to be in good condition, with no erosion or deterioration noted. In addition to the rock gutter at the downstream toe, a rock gutter was added to the right upstream toe above the normal pool level, and rock spoil was placed at the left upstream No seepage was observed beyond the dam toe or toe. discharging from embankment drain outlets through the impact basin sidewalls. No water was impounded in the reservoir, A ten foot wide berm, 540 feet long with a one however. percent slope, intercepts surface runoff from the downstream face of the dam and conducts it to a rock gutter along the toe. While no erosion was noted at the intersection of the berm and the downstream slope, the potential for erosion exists, particularly before the vegetation becomes well established. It is recommended that this area be inspected frequently for gullying.

c. Appurtenant Structures.

1. <u>Principal Spillway</u>. As shown on the plates, the riser is located at the upstream toe of the embankment. The exposed portions of the riser were inspected and evaluated to be in good condition with no signs of concrete deterioration, spalling or other structural deficiency or defects, Photograph

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4. An angle in the low stage trash rack is slightly bent. The impact basin at the downstream toe was inspected and found to be in good condition, Photograph 5, with no cracking or spalling of the concrete or erosion adjacent to the structure. The embankment drains outlet through the walls of the impact basin and were dry. The downstream channel was also inspected and found to be in good condition, with no significant erosion or deterioration.

2. <u>Emergency Spillway</u>. The emergency spillway at the left abutment was inspected and found to be in good condition, Photographs 6 and 7. The emergency spillway was recently seeded and mulched. A tributary to Newtown Creek enters the emergency spillway upstream of the control section, Photograph 8. The stream was dry at the time of the inspection.

d. <u>Reservoir</u>. At the time of the inspection, no water was impounded behind the embankment. The pond drain was open, permitting base flow to pass through the principal spillway. The reservoir slope in the vicinity of the right end of the dam has recently been seeded and mulched. No debris or sediment was noted in the vicinity of the riser.

Downstream Conditions, Newtown Creek downstream of e. the dam is about 14 feet wide with steep banks about 4 feet high. The left channel bank and flood plain is wooded with underbrush. The right channel bank is brush covered. A private road parallels the stream on the right bank. About 1000 feet downstream of the dam, Newtown Creek flows under State Route 532 (Dolington Road) through a 26 foot by 8.5 foot opening. About 2500 feet further downstream Newtown Creek enters the Borough of Newtown. In the next 0.6 mile are many homes and businesses subject to damage in the event of failure of About 2.8 miles downstream of the dam, Newtown Newtown Dam. Creek enters Nashaminy Creek. A "High" hazard classification is justified for this dam.

3.2 Evaluation.

Inspection of the dam and appurtenant facilities disclosed no evidence of apparent past or present movement that would indicate existing instability of the dam, principal spillway or emergency spillway. The exposed portions of the riser and impact basin were inspected, and the principal spillway is judged to be in good condition. The emergency spillway is also considered to be in good condition. The embankment is considered to be in good condition, although the vegetative cover is not firmly established. The overall condition of the dam is considered to be good.

SECTION 4 OPERATIONAL PROCEDURES

4.1 Procedures.

Operational procedures are discussed in some detail in Section 1.2. Operation of the dam does not require a dam tender. Under normal conditions the pond drain is closed and flow discharges over the riser weirs and through the 30 inch conduit at the base of the embankment. Additional excess water is then stored and discharged over the crest of the emergency spillway. There have been no large storms since the embankment was completed, and water has never flowed over the emergency spillway. Written operation and maintenance procedures used by the Neshaminy Water Resources Authority are contained in "State of Pennsylvania Watersheds and Resource Conservation and Development Operation and Maintenance Handbook for Projects Installed with Assistance from the Soil Conservation Service", and specific procedures for each site are contained in the "Operations Manual" prepared by William G. Major Associates, Inc., June 1977.

4.2 Maintenance of the Dam.

The dam is maintained by Bucks County personnel who periodically check the embankment, mow the grass and remove woody vegetation. As owner of the dam, Neshaminy Water Resources Authority monitors the maintenance performed and assists if possible.

4.3 Maintenance of Operating Facilities.

Maintenance of these facilities includes cleaning debris from the trash racks, lubricating the gate hoist and checking the structural integrity of the principal spillway system.

4.4 Warning Systems In Effect.

A draft warning procedure, dated January 1980, has been prepared by the local Civil Defense office. The draft was submitted to both the Neshaminy Water Resources Authority and the Pennsylvania Emergency Management Agency in Harrisburg for review. The warning procedures have been approved by the Neshaminy Water Resources Authority.

4.5 Evaluation.

It is judged that the current operating procedure, which does not require a dam tender, is a realistic means of operating the relatively simple control facilities at Newtown Dam.

The "Operations Manual" prepared by William G. Major Associates, Inc., summarizes the control features and the responsible agency for operation and maintenance of each project constructed by 1977 within the Neshaminy Watershed. Although the operational philosophy for a single-purpose flood control structure is contained in the manual, a "fact sheet" pertaining to Newtown Dam is required. It is important that individuals responsible for the maintenance and operation of Newtown Dam are aware of the written procedures to insure that all items are carefully inspected and maintained on a periodic basis.

SECTION 5 HYDROLOGY/HYDRAULICS

5.1 Evaluation of Features.

a. <u>Design Data</u>. The complete folder of design calculations was reviewed, and portions of this folder are presented in Appendix D.

The watershed is about 2.7 miles long and averages about 1.2 miles wide, having a total area of approximately 3.0 square miles. Elevations range from 380 in the upper reaches of the watershed to about 213, the normal pool elevation. The watershed is predominantly open/farmland, with less than 15 percent residential development. Residential development can be expected to progress rapidly within the watershed, however.

In accordance with criteria established by Federal (OCE) Guidelines, the recommended spillway design flood for this "Intermediate" size dam and "High" hazard classification is the Probable Maximum Flood (PMF). The Soil Conservation Service designed this dam as a Class C structure, which requires that the spillway systems be designed to pass the PMF.

b. <u>Experience Data</u>. There are no records of reservoir levels kept for this dam. Rainfall is measured and records are kept at the Neshaminy Water Resources Authority's office in Cross Keys, Doylestown, Pennsylvania. There are no estimates or records of previous high water levels.

c. <u>Visual Observations</u>. On the date of the inspection, there were no conditions observed that would indicate a reduced spillway capacity during an extreme event. Observations regarding the condition of the downstream channel, spillways and reservoir are located in Appendix A and are discussed in greater detail in Section 3.

d. <u>Overtopping Potential</u>. The dam was designed to pass the PMF without overtopping. The PMF inflow hydrograph and flood routing were done according to procedures in the SCS National Engineering Handbook. The flood routing was originally done by a graphical procedure. Subsequently, the flood routing was checked by the SCS computer program, TR-20, the results of which are included in Appendix D. The peak PMF inflow value computed by TR-20 is 14,853 cfs, and the combined principal and emergency spillway capacities of the reservoir at the top of the dam are 10,967 cfs. The TR-20 computer routing indicates a maximum reservoir level of 239.6 feet, the design top of dam. As the spillway systems for this dam pass the PMF without overtopping the embankment, they are considered to be "Adequate".

e. <u>Downstream Conditions</u>. Immediately downstream of the dam is a farm. The barn, which is shown on Plate 3, Appendix E, and the farm house would be damaged in the event of a dam failure. About 1,000 feet downstream of the dam Newtown Creek flows under State Route 532, through a 26 foot by 8.5 foot bridge opening. Immediately downstream of the bridge are two houses, and 2,400 feet downstream of the dam Newtown Creek enters the Borough of Newtown, where there are many more homes and businesses subject to flooding and damage in the event of failure of the dam. Therefore, a "High" hazard classification is justified for this structure.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability.

a. <u>Visual Observations</u>. Visual observations detected no evidence of existing or pending embankment instability. Upstream and downstream slopes appear stable, with no surficial slides or significant erosion. Both the upstream and downstream slopes were seeded with mixtures containing Crownvetch, which will require another year to become well established. There are no exterior signs or other evidence to indicate that the internal drainage systems were not operating properly. It is noted, however, that during this inspection the reservoir was empty, the embankment was not retaining a head of water, and the performance of the internal drainage system could not be evaluated.

Exposed portions of the principal spillway were inspected and judged to be in good condition.

b. Design and Construction Data. Design documentation is very complete as a several hundred page design folder prepared by the Soil Conservation Service (SCS) was available and reviewed for this investigation. Data included in these files are a foundation report containing permeability test results, shear strength test results and a stability analysis, structural calculations for the principal spillway and a complete set of hydrologic/hydraulic calculations. Portions of the Hydrology/Hydraulics section are presented in Appendix D. Principal features of this structure are presented in the drawings located in Appendix E.

A stability analysis of the embankment was performed by SCS using the ICES-LEASE computer program. Soil strength parameters were based on two consolidated-undrained triaxial compression test series conducted on compacted Zone 1 material and one series on compacted Zone 2 material. The foundation materials were assumed to have sufficient strength to prevent potential failure arcs from passing through the foundation. The shear strength parameters adopted for design were reviewed and judged to be conservative, based on the test results. Stability analyses using the Swedish circle method resulted in the following minimum factors of safety:

<u>Slope</u>	<u>Condition</u>	Minimum Factor of Safety
Upstream	Rapid Drawdown	1.57
Downstream	Steady Seepage	1.86

The recommended allowable factors of safety for these conditions, in accordance with Corps of Engineers EM 1110-2-1902, are 1.2 and 1.5, respectively. Therefore, it is concluded that the stability of the embankment is adequate.

c. <u>Operating Records</u>. There are no operational records for this structure.

d. <u>Post-Construction Changes</u>. There are no reports nor is there any evidence that modifications were made to this dam.

e. <u>Seismic Stability</u>. The dam is located in Seismic Zone 1. Normally it can be considered that if a dam in this zone is stable under static loading conditions, it can be assumed safe for any expected earthquake conditions. As the stability analysis resulted in a minimum factor of safety of 1.57 during rapid drawdown, the most critical loading condition, it can be assumed that seismic stability requirements are satisfied.

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SECTION 7 ASSESSMENT/REMEDIAL MEASURES

7.1 Dam Assessment.

a. <u>Evaluation</u>. Visual inspection and review of design and construction documentation indicate that the dam and appurtenant structures of Newtown Dam are in good condition.

In accordance with criteria established by Federal (OCE) Guidelines, the recommended spillway design flood for this intermediate size dam and "High" hazard classification is the Probable Maximum Flood (PMF). The Soil Conservation Service designed this dam as a Class C structure, which requires that the spillway systems be designed to pass the PMF.

The hydrologic and hydraulic computations presented in Appendix D indicate that the spillway structures are capable of discharging the PMF without overtopping the embankment. Therefore, the structure is considered to have an "Adequate" spillway system.

b. <u>Adequacy of Information</u>. The information available for this investigation was adequate to evaluate the structural and hydraulic aspects of the dam.

c. <u>Urgency</u>. It is recommended that the suggestions presented in Section 7.2 be implemented as specified.

7.2 <u>Remedial Measures</u>.

a. <u>Facilities</u>. It is recommended that, during the period required for establishment of Crownvetch, the embankment, particularly the downstream berm, be periodically checked for erosion damage.

b. Operation and Maintenance Procedures. Neshaminy Water Resources Authority has an "Operations Manual" specifying agencies responsible for operation and maintenance of Neshaminy Watershed projects completed by 1977. The manual requires updating to include Newtown Dam. The Operations Manual refers to a "Development, Operation and Maintenance Manual" prepared by SCS for a maintenance inspection checklist, which should be used to insure that all items are periodically inspected and maintained in the best possible condition. It is recommended that these procedures provide for a period of observation during and following impoundment of significant quantities of water behind the embankment. These observations should include monitoring discharge from the embankment drainage system and looking for sources of uncontrolled seepage.

A warning procedure has been developed and approved by the Neshaminy Water Resources Authority. This procedure indicates that the structure should be monitored on a 24 hour basis when the severity of a forecasted storm is predicted to be near, at or above the design capacity of the structure. The procedure also includes emergency telephone numbers and areas downstream of the dam which should be notified in the event a hazardous condition develops.

APPENDIX

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د Sheet 1 of 11	National ID # <u>PA 01064</u>	on <u>N/A</u> M.S.L.		_	site and
CHECK LIST VISUAL INSPECTION PHASE I	<i>ucks</i> Hazard Catego	Dry M.S.L. Tailwater at Time of	Raymord Lambert (Geologist) (7/14/1980)	Marry F. Beck Recorder	Mr. William Taylor. of Neshaminy Water Resources Authority was on site and provided assistance to the inspection team.
		/////200 me of Inspecti	Inspection Personnel: <u>Mary F. Beck (Hydrologist)</u> Arthur Dvinoff ^{(Geotechnical/}	Vincent McKeever (Hydrologist)	Remarks: Mr. William Taylo provided assistanc

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Sheet 1 of 11

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CONCRETE/MASONRY DAMS

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f 11 NS				She	et 2 c
Sheet 2 of 11 REMARKS OR RECOMMENDATIONS	·				
OBSERVAT IONS	N/A	N/A	N/A	N/A	N/A
VISUAL EXAMINATION OF	ANY NOTICEABLE SEEPAGE	STRUCTURE TO ABUTHENT/EMBANKMENT JUNCTIONS	DRAINS	water passages	F OURDATION

11

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CONCRETE/MASONRY DAMS

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VISUAL EXAMINATION OF	OBSERVATIONS	Sheet 3 of 11 REMARKS OR RECOMMENDATIONS
SURFACE CRACKS CONCRETE SURFACES	И/А	
STRUCTURAL CRACKING	N/A	
VERTICAL AND HORIZONTAL ALIGUMENT	N/A	
MORITH JOINTS	N/A	
CONSTRUCTION JOINTS	N/A	

Sheet 3 of 11

Sheet 4 of 11 REMARKS OR RECOMMENDATIONS **OBSERVATIONS** None observed. VISUAL EXAMINATION OF SURFACE CRACKS

EHBANKMENT

. : • •

UNUSUAL MOVEMENT OR Cracking at or beyond The toe

None observed.

sloughing or erosion of Epremicient and abuthent slopes

Crest is protected by gravel. No significant erosion was observed.

VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST

Vertical aligrment is shown on Sheet 5B of 11. Horizontal alignment is good.

RIPRAP FAILURES

Riprap is in good condition.

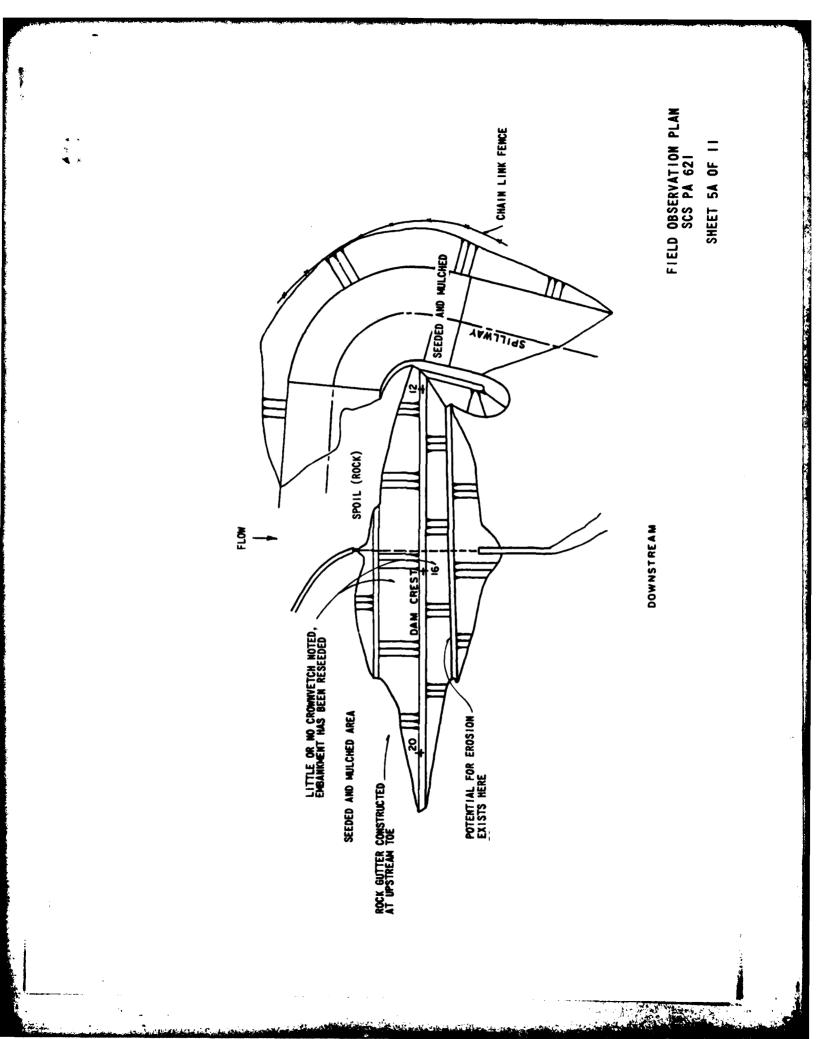
VISUAL EXMINATION OF VEGETATION	065ERVATIONS REMARKS OR RECOMMENDATIONS Upstream and downstream faces were dormant seeded and mulched in Fall, 1979 and reseeded in Spring, 1980, thus almost no Crownvetch is evident.
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLMAY AND DAM	All junctions are in good condition.
ANY NOTICEABLE SEEPAGE	None observed, reservoir dry at time of inspection.
STAFF GAGE AND RECORDER	None
DRAINS	Embankment drains outletting through impact basin walls were dru.

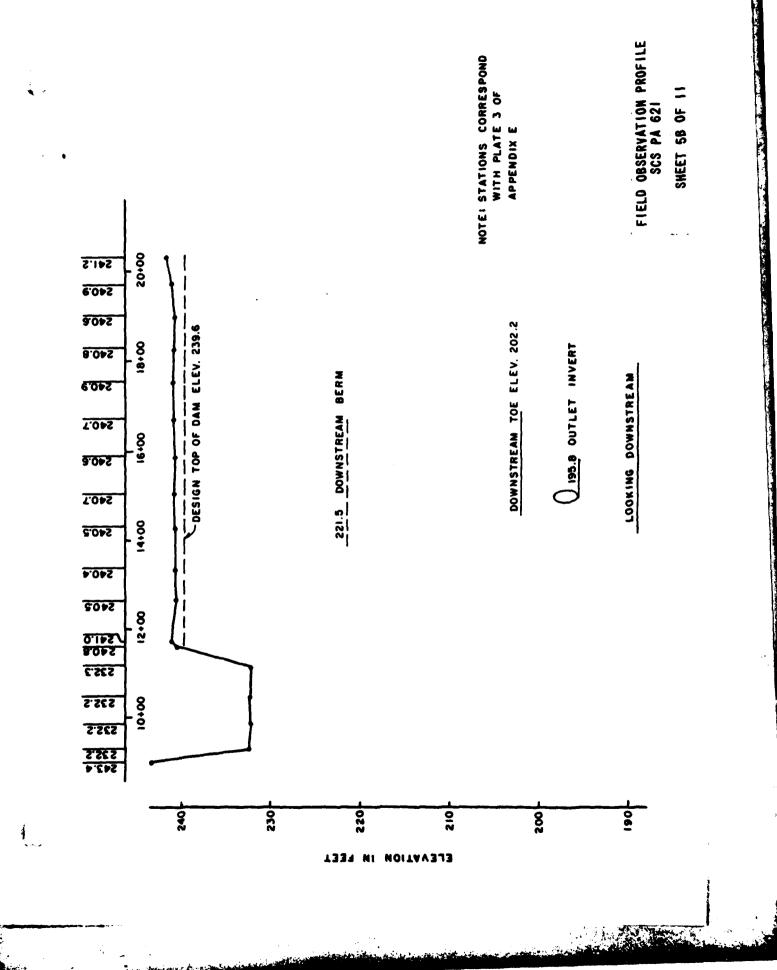
mered and the first of

Sheet 5 of 11

Contraction and the

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VISIAL EMMINTION OF CANCINE AND SALLING OF CONCINE Exposed surfaces show no signs of cracking, apalling or other concrete defects. Baposed surfaces show no signs of cracking, apalling or other concrete defects. Cool condition. OULET CHANNEL COOL condition. Cool condition. Cool condition.		PRÍNCIPAL SPILLWAY Sheet 6 of 11
Conduit through embandment not inspected. Exposed surfaces show no signs of aracking, spalling or other concrete defects. Exposed surfaces show no signs of aracking, spalling or other concrete defects. Good condition.	VISHAL EXAMINATION OF	
Exposed surfaces show no signs of cracking, galling or other concrete defects. Exposed surfaces show no signs of cracking, spalling or other concrete defects. Good condition. Sluice gate open, gate was not exercised.	CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	Conduit through embankment not inspected.
Exposed surfaces show no signs of cracking, spalling or other concrete defects. Good condition. Sluice gate open, gate was not exercised.	IMTAKE STRUCTURE	Exposed surfaces show no signs of cracking, spalling or other concrete defects.
Good condition. E Sluice gate open, gate was not exercised.	OUTLET STRUCTURE	Exposed surfaces show no signs of cracking. spalling or other concrete defects.
Sluice gate open, gate was not exercised.	OUTLET CHANNEL	
	EMERGENCY GATE	
	•	

CONCRETE MEIR Rome, the downstream edge of a 50 foot level section is the control section. APPROACH CMMIEL Good condition. A tributary to Newtown Creek enters the approach channel below the control section via a channel excavated in bedrock. DISCUMREE CHAINEL Cood condition. BRIDEE AND PIERS None.	VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
	ONCRETE MEIR	None, the downstream edge of a 50 section is the control section.	foot level
	Approach channel	Good condition. A tributary to N enters the approach channel below section via a channel excavated i	wtown Creek the control 1 bedrock.
	DISCHARGE CHA:MEL	Good condition.	
	SRIDGE AND PIERS	Rone.	

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	GATED SPILLWAY	Chant B of 11
I SUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
ONCRETE SILL	N/A	
NPROACH CHAIMEL	N/A	
DI SCHARGE CHANNEL	N/A	
BRIDGE AND PIERS	N/A	
GATES AND OPERATION EQUIPMENT	N/A	

C

INSTRUMENTATION

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VISUAL EXAMINATION	OBSERVATIONS	Sheet 9 of 11 REMARKS OR RECOMMENDATIONS
MONUMENTATION/SURVEYS	None	
OBSERVATION WELLS	None	
WEIRS	None	
PIEZOMETERS	None	
OTHER .	None	

Sheet 9 of 11

and the set of the set of the

Sheef 10 of 11	COMMENDATIONS	<i>.</i>			
	REMARKS OR RECOMMENDATIONS	Reservoir slopes are flat to moderate. The sluice gate has not been closed and the reservoir is empty.	úr area.		
		lat to moderat ed and the res	No sediment was noted in the reservoir area.		
RESERVOIR	OBSERVATIONS	slopes are f not been clos	ent was noted		
RESE	OBSERV	Reservoiı gate has	No sedime		
	IINATION OF		N		
	VISUAL EXAMINATION OF	SLOPES	SED IMENTATION		•

Sheet 10 of 11

	DOWNSTREAM CHANNEL
VISUAL EXAMINATION OF	OBSERVATIONS REMARKS OR RECOMMENDATIONS
CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)	The downstream channel is in good condition, averages 14 feet wide with 4 foot high banks on 3H:IV slopes. The banks are wooded with heavy under- brush. The left floodplain is also wooded and a farm driveway and farm is on the right floodplain.
SLOPES	The valley gradient is about 0.007.
APPROXIPATE NO. OF HOMES AND POPULATION	Immediately downstream of the dam is a farm, the barn is shown on Plate 3, Appendix E. About 1,200 feet downstream of the dam is one home subject to damage in the event of a dam failure. About 1,200 feet further downstream, Newtown Greek flows through the Borough of Newtown where there are many homes and businesses subject to damage in the event of a dam failure.

Sheet 11 of 11

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APPENDIX

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CHECK LIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I	REMARKS	"As-built" dra will be on file	Plate 1, Appendix E.	See Section 1.2 of text.	See Appendix E.	Appendix E	Appendix D	Rainfall is me at their offic
ATA ATA , OPERATION ID # <u>PA 01064</u>	Sheet 1 of	"As-built" drawings were provided for this investigation and will be on file with DER, SCS and the Owner.	ix E.	of text.				Rainfall is measured by Neshaminy Water Resources Authority at their office in Cross Keys, Doylestown, Pennsylvania.

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DESIGN REPORTS Design folder on file with DER and SCS. Design folder, see also Appendix F. Included in design folder, see also Appendix F. Included in design folder, see also Appendix F. Included in design folder, see also Appendix F. Bee discussion in Sections 5 and 6 of text. See discussion in Sections 5 and 6 of text. See discussion in Sections 5 and 6 of text. StepAge Studies UNASTRALLITY SEEPAGE STUDIES MATERIALS INVESTIGNTIONS Complete records in SCS files. LABORATOR FIELD POST-CONSTRUCTION SURVEYS OF DAM	ITEM	REMARKS
	DESIGN REPORTS	Design folder on file with DER and SCS.
	geology reports	Included in design folder, see also Appendix F.
	DESIGN CUMPUTATIONS DESIGN CUMPUTATIONS HYDROLOGY & HYDRAULICS JAM STABILITY SEEPAGE STUDIES	See discussion in Sections 5 and 6 of text.
	WATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD	Complete records in SCS files.
	OST-CONSTRUCTION SURVEYS OF DAM	A final crest profile survey was performed for "as-built" drawings.

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 Data located on SCS drawings.

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	Sheet 3 of 4
ITEM	REMARKS
MONITORING SYSTEMS	None
MODIFICATIONS	No post-construction modifications.
HIGH POOL RECURDS	None
POST COMSTRUCTION ENGINEERING STUDIES And REPORTS	None
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None
MATATE:MAICE Operat Ion Records	Neshaminy Water Resources Authority maintain these files.

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SPILLWN PLM See Appendix E for details. SECTIONS See Appendix E for details. DEFAILS See Appendix E for details. DFEMILIG See Appendix E for details. DFEMILIS See Appendix E for details. DFEMILIS See Appendix E for details. DFEMILIS See Appendix E for details. MISCELLANEOUS The following information is located in DER files. MISCELLANEOUS The following information of the Neshaminy Water Resources Authority Budmitted by the State of Pennsylvaria, Setteme 23, 1977. Basedures Authority Budmitted by the State of Pennsylvaria, Setteme 23, 1977. S. sheet set of design draxings prepared by SCS, Magust 1997. Basedures Reporte by Frederick Soluets, Project Engine SCS, August 50, 200 Also anailable from SCS were complete construction records. SCS	ITEM	REMARKS
	SPILLWAY PLAN	
	SECTIONS	See Appendix E for details.
	DETAILS	
	OPERATING EQUIPHENT PLANS & DETAILS	
		See Appendix E for details.
 "Report Upon the Application of the Neshaminy Water Resources Authority" submitted by the State of Pennsylvania, September 28, 1977. Permit issued by the State of Pennsylvania, October 3, 1977. 35 sheet set of design drawings prepared by SCS, 1976-1977. Erosion and Sediment Control Plan prepared by SCS, August 1977. Progress Reports by Frederick Schwetz, Project Engineer, SCS. Also available from SCS were complete construction records. 	MI SCELLANEOUS	The following information is located in DER files.
Pennsylvania, September 28, 1977. 2. Permit issued by the State of Pennsylvania, October 3, 1977. 3. 35 sheet set of design drawings prepared by SCS, 1976-1977. 4. Erosion and Sediment Control Plan prepared by SCS, August 1977. 5. Progress Reports by Frederick Schuetz, Project Engineer, SCS. Also available from SCS were complete construction records.		
 3. 35 sheet set of design drawings prepared by SCS, 1976-1977. 4. Erosion and Sediment Control Plan prepared by SCS, August 1977. 5. Progress Reports by Frederick Schuetz, Project Engineer, SCS. Also available from SCS were complete construction records. 		
 Erosion and Sediment Control Plan prepared by SCS, August 1977. Progress Reports by Frederick Schuetz, Project Engineer, SCS. Also available from SCS were complete construction records. 		
5. Progress Reports by Frederick Schuetz, Project Engineer, SCS. Also available from SCS were complete construction records.		
		5. Progress Reports by Frederick Schwetz, Project Engineer, SCS. Also anailable from SCS were complete construction records

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APPENDIX

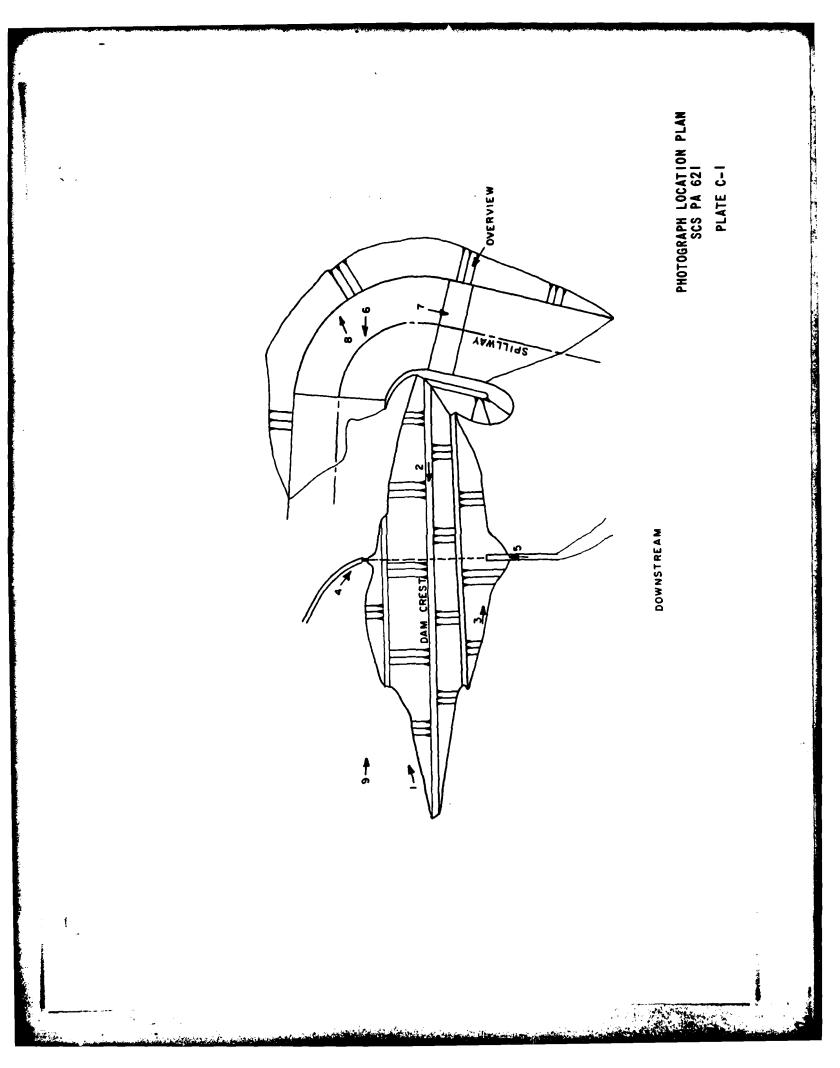
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PHOTOGRAPH NO. 1

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UPSTREAM FACE WITH ROCK GUTTER AT UPSTREAM TOE.

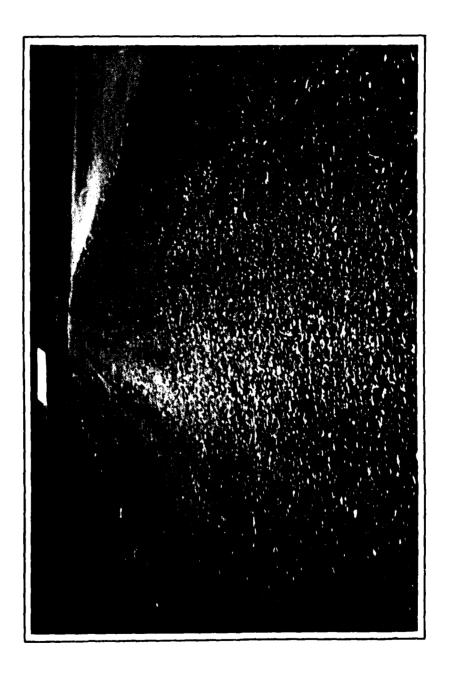
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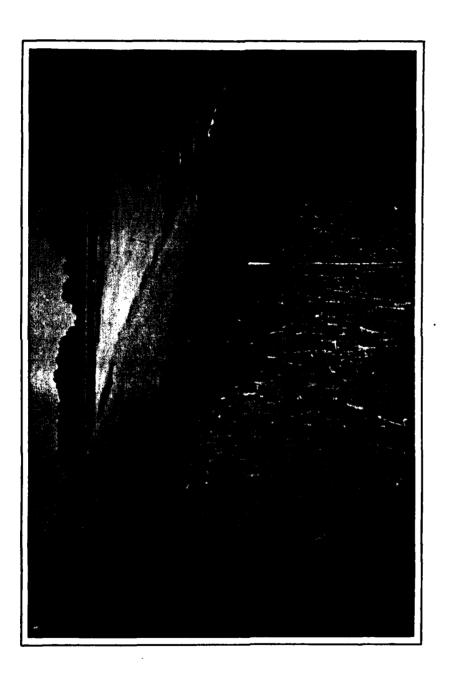


PHOTOGRAPH NO. 2

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GRAVEL ROAD PROTECTS EMBANKMENT CREST.

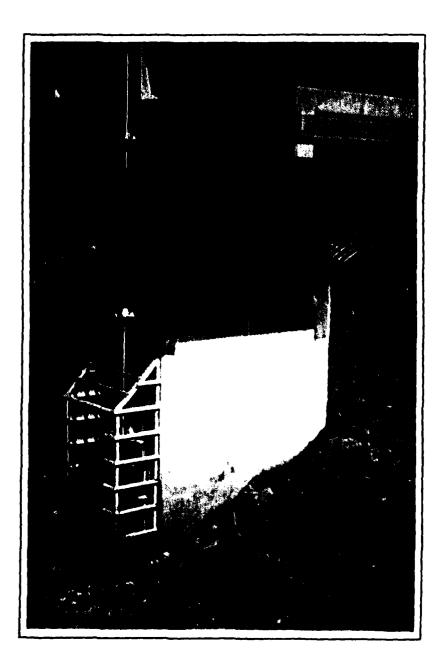
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PHOTOGRAPH NO. 3

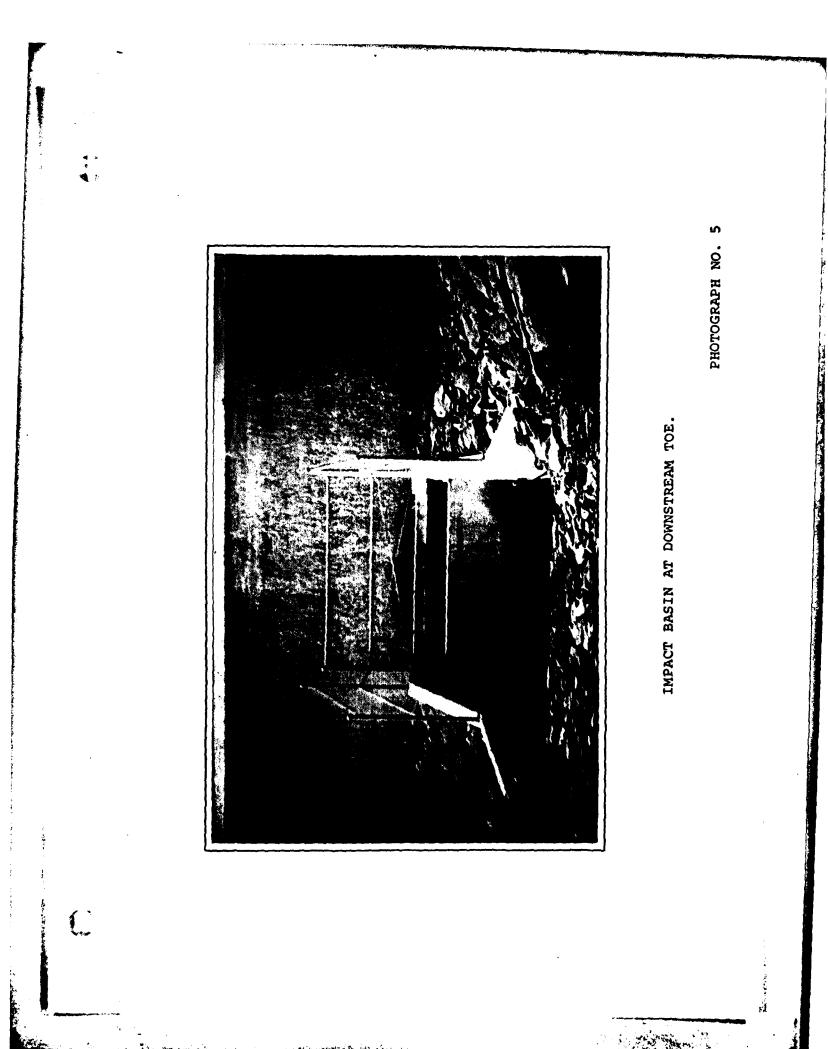
DOWNSTREAM FACE WITH ROCK GUTTER AT TOE.



PRINCIPAL SPILLWAY RISER AT UPSTREAM TOE.

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PHOTOGRAPH NO. 4



PHOTOGRAPH NO. 6

EMERGENCY SPILLWAY LOOKING UPSTREAM

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EMERGENCY SPILLWAY LOOKING DOWNSTREAM

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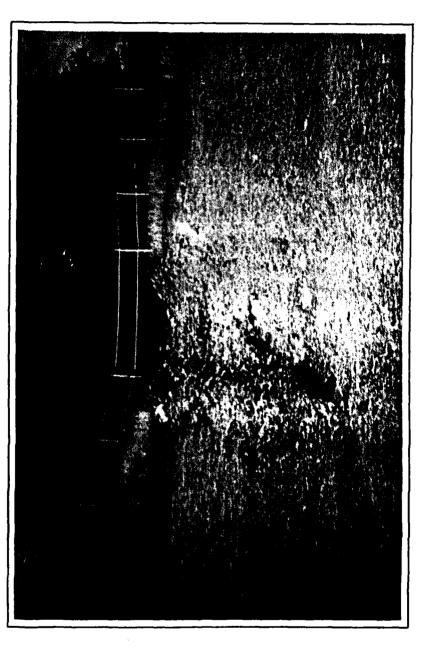


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PHOTOGRAPH NO. 8

INTERMITTENT STREAM ENTERS EMERGENCY SPILLWAY UPSTREAM OF CONTROL SECTION.

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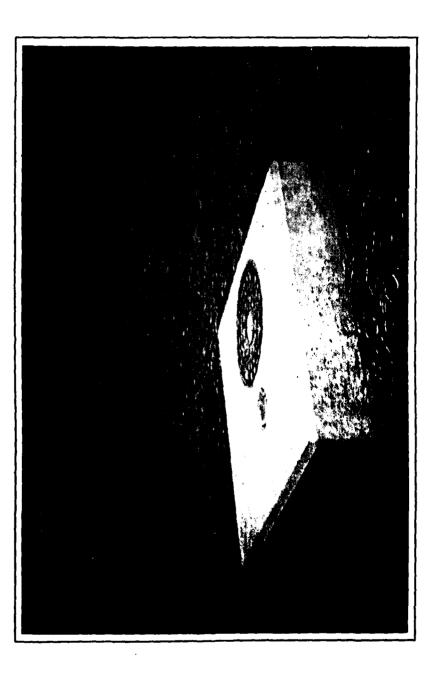
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PHOTOGRAPH NO. 9

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SANITARY SEWER MANHOLE. SEWER IS UNDER EMBANKMENT.

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TYPICAL DEVELOPMENT ADJACENT TO NEWTOWN CREEK IN NEWTOWN, PENNSYLVANIA.

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APPENDIX

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NEWTOWN DAM (SCS PA 621) CHECK LIST HYDROLOGIC AND HYDRAULIC ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: Predominantly open farm land with little residential development. ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): 213.0 feet (56 Acre-Feet). ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): 239.6 feet (1420 Acre-Feet). ELEVATION MAXIMUM DESIGN POOL: 239.6 feet. ELEVATION TOP DAM: 239.6 feet, design EMERGENCY SPILLWAY a. Elevation _____ 231.9 feet. b. Type grass lined trapezodial channel. c. Width ______ 185 feet. _____ d. Length About 650 feet. e. Location Spillover Left abutment. f. Number and Type of Gates _____ None. PRINCIPAL SPILLWAY a. Type _____ Deep inlet riser, 30 inch conduit and impact basin. b. Location _____ Dam_station 15+00, at maximum section. c. Entrance inverts _____ 213 feet. d. Exit inverts _____ 196.0 feet. e. Emergency draindown facilities Pond drain at base of riser, 199 feet. HYDROMETEOROLOGICAL GAGES: a. Type _____ None within watershed. b. Location ______ N/A c. Records N/A MAXIMUM NON-DAMAGING DISCHARGE: Not determined.

Sheet 1 of 8

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HYDROLOGIC AND HYDRAULIC BASE DATA

Sheet 2 of 8

DRAINAGE AREA: (1)3	3.04 square miles.
PROBABLE MAXIMUM PRECIPITA	ATION (PMP) 25.5 inches.
HYDROGRAPH PARAMETERS: (1)	
Runoff Curve Number	81
Time of Concentration	1.84 hour
SPILLWAY CAPACITY AT MAXIM WATER LEVEL: (1)	10,967 cfs

(1) From SCS Design Folder

Sheet 3 of 8

1. 198

Newtown Dam (SCS PA 621) Hydrology/Hydraulics

Classification (Ref.-Recommended Guidelines for Safety Inspection of Dams)

- 1. The hazard potential is rated as "High" as there would be loss of life if the dam failed.
- 2. The size classification is "Intermediate" based 1420 Acre-Feet total storage capacity and 44 feet height.
- 3. The spillway design flood, based on size and hazard classification, is the Probable Maximum Flood (PMF).

Hydrologic/Hydraulic Analysis

The complete H & H design folder was available for review. The PMF inflow hydrograph was determined according to procedures in the SCS National Engineering Handbook, Section 4 (NEH-4). The routing was done according to procedures in NEH-5 (1968, was not available for review) and, later, checked by SCS computer program, TR-20. The computer routing indicates a higher maximum water elevation than the original flood routing. As land rights were obtained before the computer routing, it was decided to increase the emergency spillway width to stay within the acquired land rights.

Orignial design parameters were checked against current information and/or criteria. The drainage area of 3.04 square miles is verified by current USGS maps.

Calculations for the PMF inflow hydrograph were based on a 6-hour rainfall of 25.5 inches and a Runoff Curve Number of 81. Rainfall criteria established for this investigation by the Corps of Engineers indicate a 26.6 inch rainfall (Ref.-Hydrometerological Report No. 33) and the use of Hop Brook factor, a point rainfall reduction factor. For a watershed of this size, the point rainfall

Sheet 4 of 8

is reduced by 20%, to 21.2 inches. Thus, the design rainfall is conservative compared to Corps of Engineers criteria. The Runoff Curve Number 81 (CN 81) is based on the hydroglogic soil group classification and expected future land use within the watershed. The future land use was based on projections of the Bucks and Montgomery Planning Commission to year 2010. Projected land use includes open, 3.5%; wooded, 9.5%; and residential and commercial 87.0%. The estimated current developed areas are less than 10% from the 1973 USGS map. The estimated future conditions are judged adequate.

The elevation-storage data was checked and found adequate. The emergency spillway discharge was checked according to current SCS criteria, TR-39. The maximum emergency spillway discharge was estimated as 10,852 cfs (see sheet 5), about the same as emergency spillway discharge used in the SCS computer routing.

The spillway is rated as "Adequate" as the spillways will pass the PMF without overtopping the embankment.

MEB DATE 7/2/80 SUBJECT. SHEET 5 OF 8 CHKD. BY REIT DATE 7/21/40 Newtown Dam Hydralogy / Hydraulics Emergency Spillway Capacity ref. SCS TR-39 bottom width = 30 ft. level section . 50 H. total length to down stream edge of level section 455 ft approach channel slope = 0.02 assume Q = 10, 552 cts estimated emergency spillway g= Q/b=10, 852/185 = 58.6cfs/ H. depth at upstream edge of level section: 5.9 H. ES-158 sheet 1 of 10 depth at entrance to appraach channel - 15.6 ft ES-158 sh. 3 of 10 velocity head at entrance to approach channel - 0. 12H. ES-159, sh. 1 at 2 total head at entrance to approach channel. elev. + water depth + velocity , head . 2240 + 15.6 + 0.12 = 259.7 ~239.6 top of the above calculations are adequate as they are within the accuracy of the charts.

· ·	PennA BuHLW Doleg-27-74	Checked	By Core	Job	NO PA-62/
	Sub, act WORK PLAN - DESI	GN CO	MPARISCN (DAMS) Sh	pet 3 of
				٠.	
	ITEM	UNIT	WORK PLAN	DESIGN	COMMENTS
	DRAINAGE AREA	SQ. MI.	3 .4	3.04	
	STORAGE CAPACITY				
	SEDIMENT (INC. AERATED)	AC. FT	69	69	
- Tel • • • • •	BENEFICIAL	AC FT			
	RETARDING	AC.FT	594	678.7	
	TOTAL	AC.FT.	663	747.7	-
	LETWEEN HIGH & LOW S.				
	SURFACE AREA				
	NORMAL POOL	ACRE			
į	GETARDING FOOL	ACRE			
	DESIGN HIGH WATER	ACRE	67	82	
	VOLUME OF FILL	CU YD.	63,100		
	TOP OF DAM ELEV	FEET	239.3	239.6	
	MAX HEIGHT OF DAM	FEET	43.3	43.6	
	EMERGENCY SPILLWAY	2.00			
	CREST ELEVATION	FEET	231.0	231.9	
	BOTTOM WIDTH	FEET	150	185.0	10 Mar
	TYPE	-		<u>s.d</u>	
	PERCENT CHANCE OF USE	• –		_/	1
	AVE. CURVE NO. COND. II	<u> </u>	<u>· 81</u>	81	<u>.</u>
	EM SP. HYDROGRAPH			• • •	
	STORM RAINFALL	IN.	10.5	10.5	A.
	STORM RUNOFF	1 N.	. 8.12	8.12	
	VELOCITY OF FLOW - V	FPS	8.3	7.58	24
	PEAK DISCHARGE RATE	- CFS	2020	2091 .	
	MAX WATER SURFACE EL	FEET	234:2	234.7	
	FREEBOARD HYDROGRAPH				
	STORM RAINFALL	JN.	26	25.5	
	STCRM RUNOFF	1 IN. 18	23.39	22.88	
	VELOCITY OF FLOW - Ve	FPS	14.2	14.79	A COMPANY AND ST
	PEAK DISCHARGE RATE	CFS	10,275	10967	a state the
	MAX. WATER SURFACE EL.	FEET	239.3	239.6	
	PRINCIPAL SPILLWAY				5.
	FISER SIZE	FT	<u> </u>	2.5 × 7.5	
	AX LOW STAGE FLOW	CFS	<u> </u>		
	ORIFICESIZE	· FT.			
	MAX HIGH STAGE FLOW	CFS	136	17.	1.44.2
1	PPE SIZENS TO	DIA	The second second	30	
	CAPACITY EQUIVALENTS	- C-			
	TOTAL SEDIMENT VOL	IN.	0.42	0.42	
	RETARDING STORAGE	1N	3.66	4.186	
	EM SPILLWAY STORAGE				· · · ·
	TO TOP OF DAM	1N	4.42	4.12	
y	0.355 OF STRUCTURE	. –		<u> </u>	
	CONSTRUCTION COSTS	ł	1		
	İ	-			
2-26-1	1 N	1 -	1		

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SHEET 7 OF 8

COMPUTATION SHEET U.S. DEPARTMENT OF AGRICULTURE SCS-ENG-522 REV. 3-69 SOIL CONSERVATION SERVICE STATE PROJECT CHECKED BY DATE Creek JOB NO. • . . 12.W • 8/27/74 A - 621 Time of Concentration (copied From planning data) SHEET 6 Slope Vel. tsec Length 10 overland Flow 2800' 2800 2.170 S Gully 7000 . 0.009 3.4 2060 CHANNel 0.01 4.5 1790 8000 6640 500 1.84 10000 A Elev \$120 17800 SimLi Soil Cover Complex (copied from planning data Future Condilions Cover sui class CN. - 7. LANC GrASS WoodTAnd 3 666 158 Public : 2.0 *>79 89 1 D 89 Commercial Residential 81.7 36.0 2941 20-42000 Res. denlint 4085 \mathcal{I} . (81.7 50. -.TT 7 40,000 81- 74 100. 8063 USP 1, 292, **3** REF - SCS DESIGN FOLDER

ENEEN STANCT ELASS E 07-19-14	3	560.38 60.75 72.48 104.07 55.27 72.48 104.07 55.41 121.58 2071.12 95.41 121.58 2071.12 95.41 121.58 2071.12 100.49 54.24 2071.12 100.49 54.24 2071.12 115.45 54.244 115.45 54.244 115.45 1201.45 111.45 113.45 1202.45 54.27.45 113.45 14502.45 54.27.45 113.45	1287-04 139104-39 10007-05 1410.76 239-01 1215 1 11494-43 12184-59 10007-45 1414.74 239-01 12-13 1 10198-98 1694-07 10021-68 1414.74 239-59 12-13 1 542-92 666.54 1786-37 920-05 234-42 4.5 0.00 0.00 1995.59 159.54 232.27 504 4.11(Cat COMPUED MP= 7.11 AT ELEV. 239-61 (5104 46 f. 1616.7 40. f. 0.73 14.1 CAL VELOCITY- 12.15 CATICAL DEPTH+ 4.59 CALIFICAL 510PE- 1.40.	1485). CFS 2953. AC-FT. 2953. AC-FT. 731. AC-FT. 10967. CFS 10114 DUAATION OF FLCM- 11.50 15,966 AC-FT PER F1. WIDTH DUAATION OF FLCM- 11.50
PA - 624 NESMANNY CHERK FREEDAAD ADUTING	¥2.000	2287.77 2287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 287.77 297.77 297.77 207.777	4.00 4.25 4.50 8.50 11.05 11.05 11.05 11.05 2.25 HOUNS CALLINE	ER SPILLMAY

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REF - SCS DESIGN FOLDER

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SHEET 8 OF 8

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APPENDIX

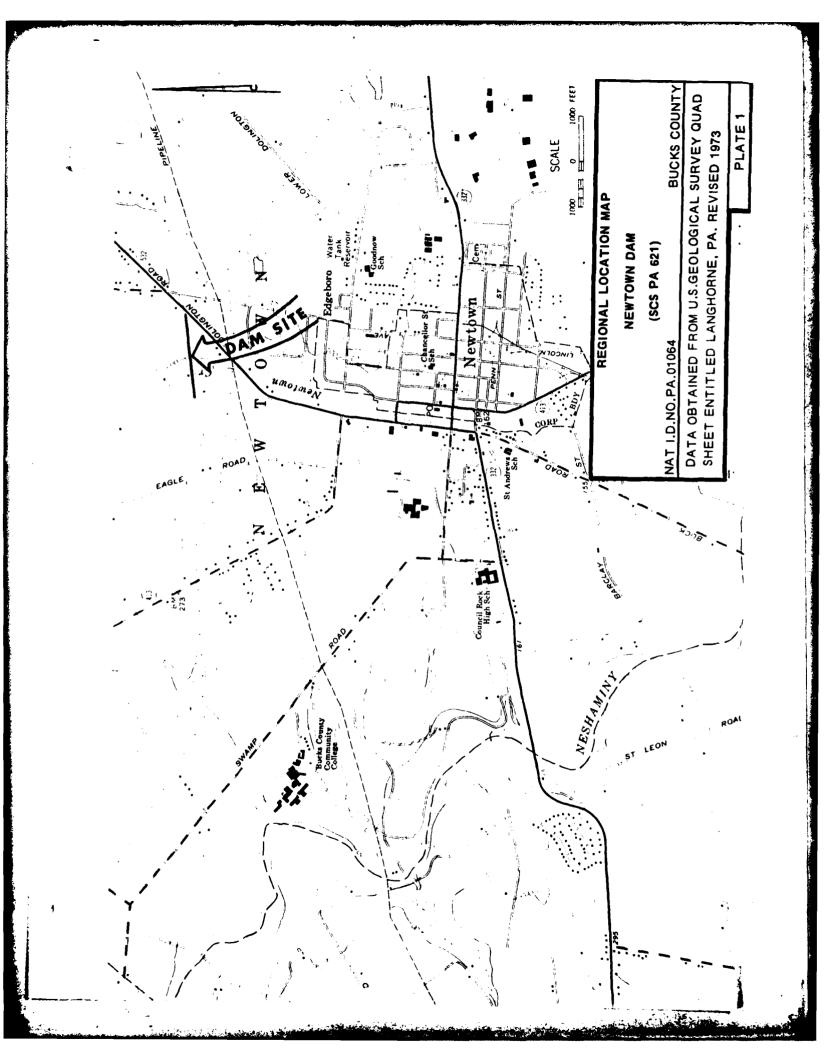
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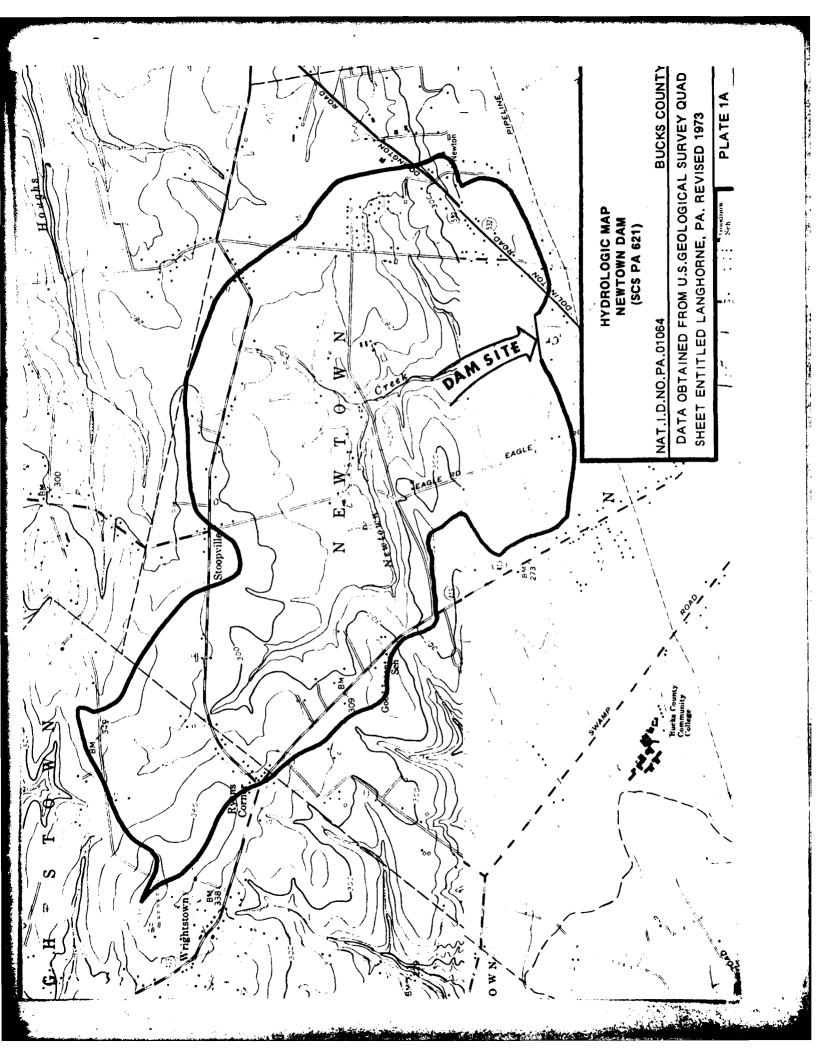
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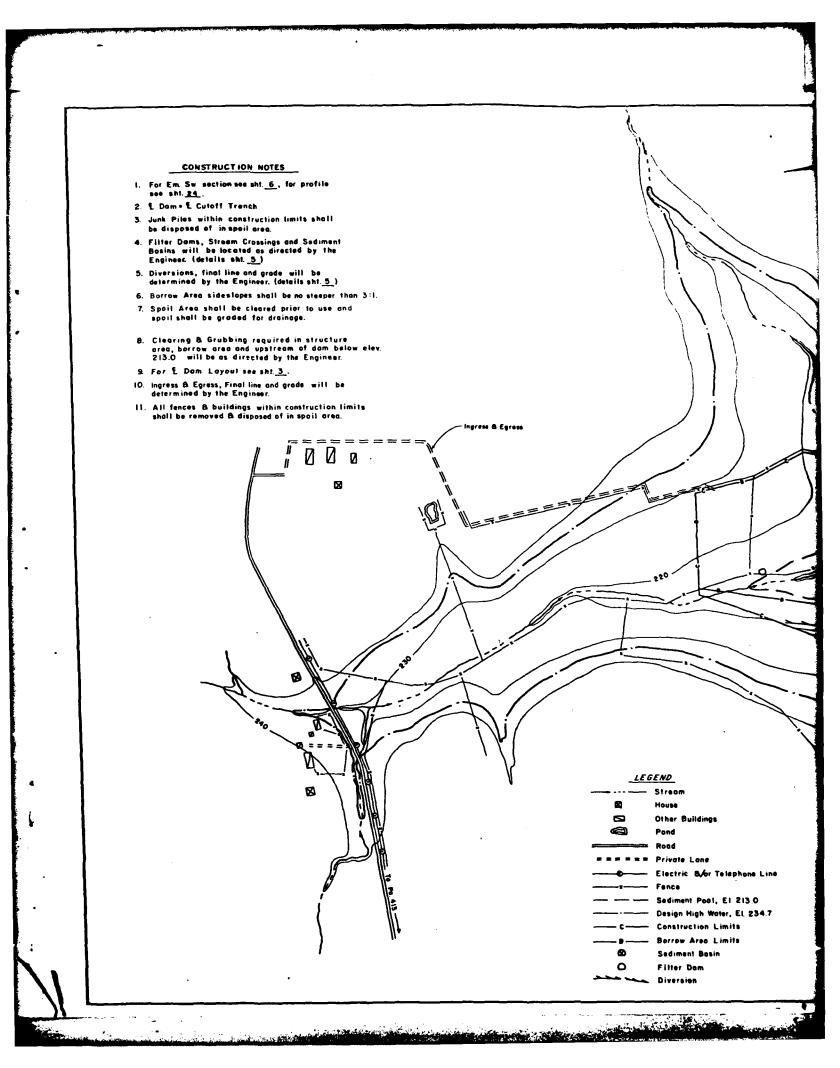
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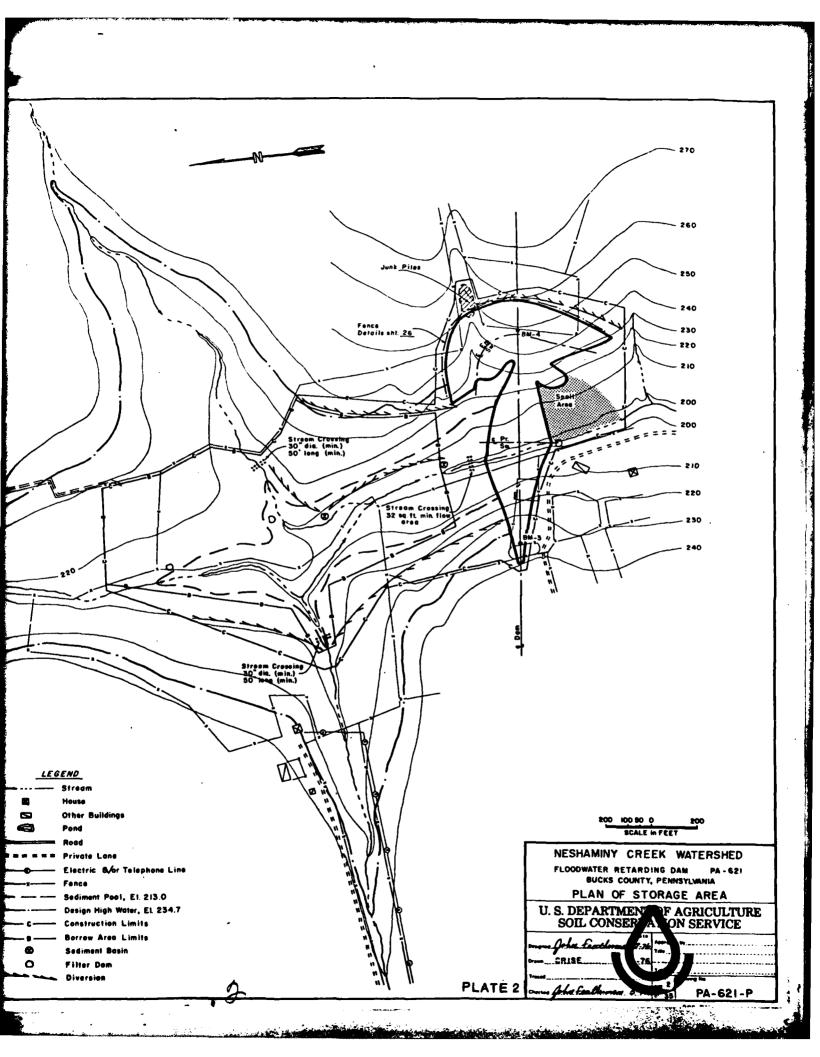
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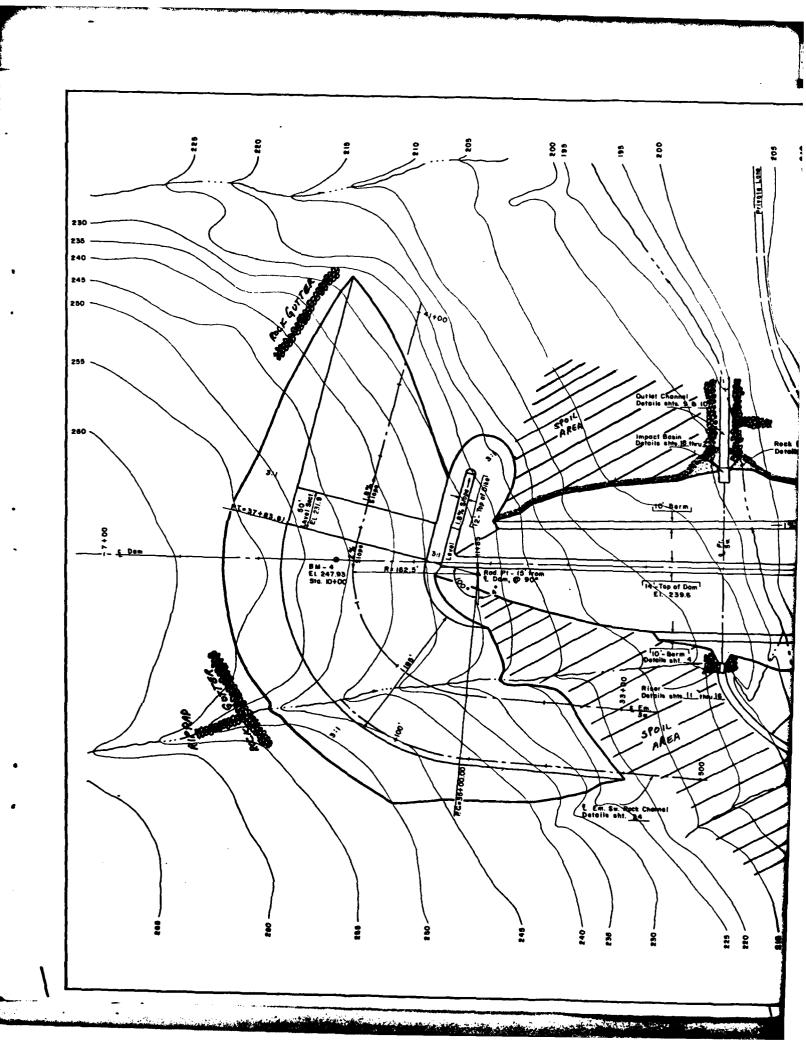
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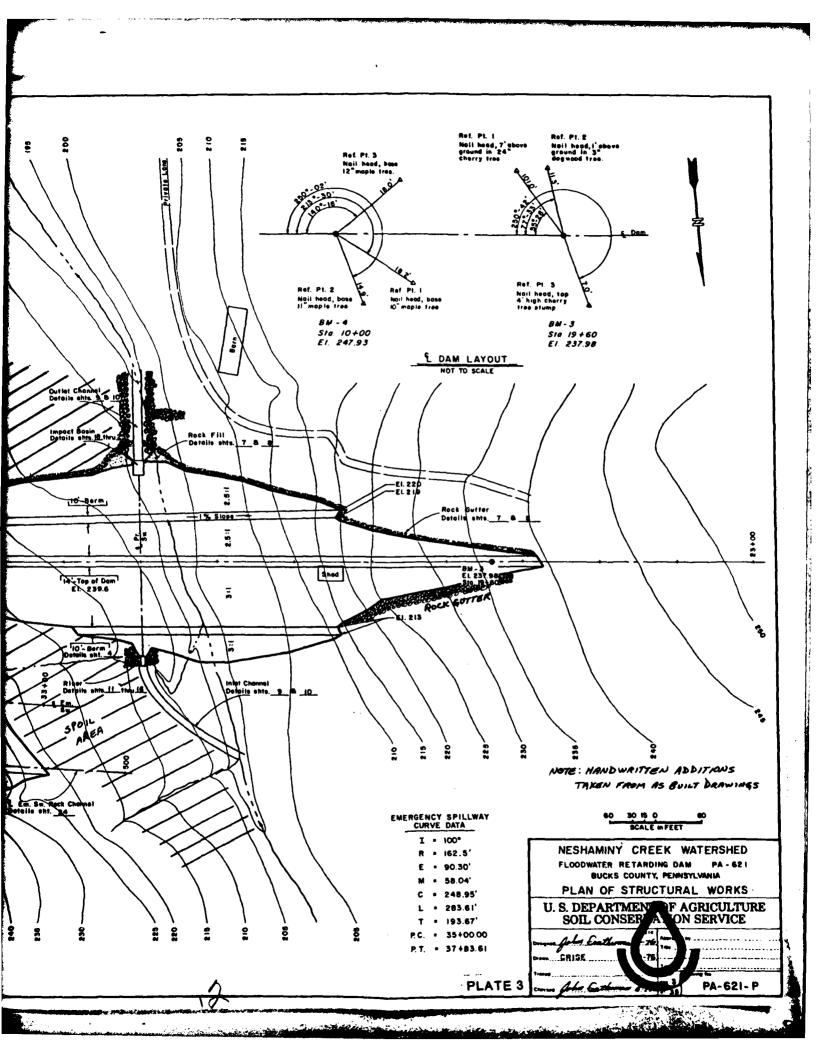


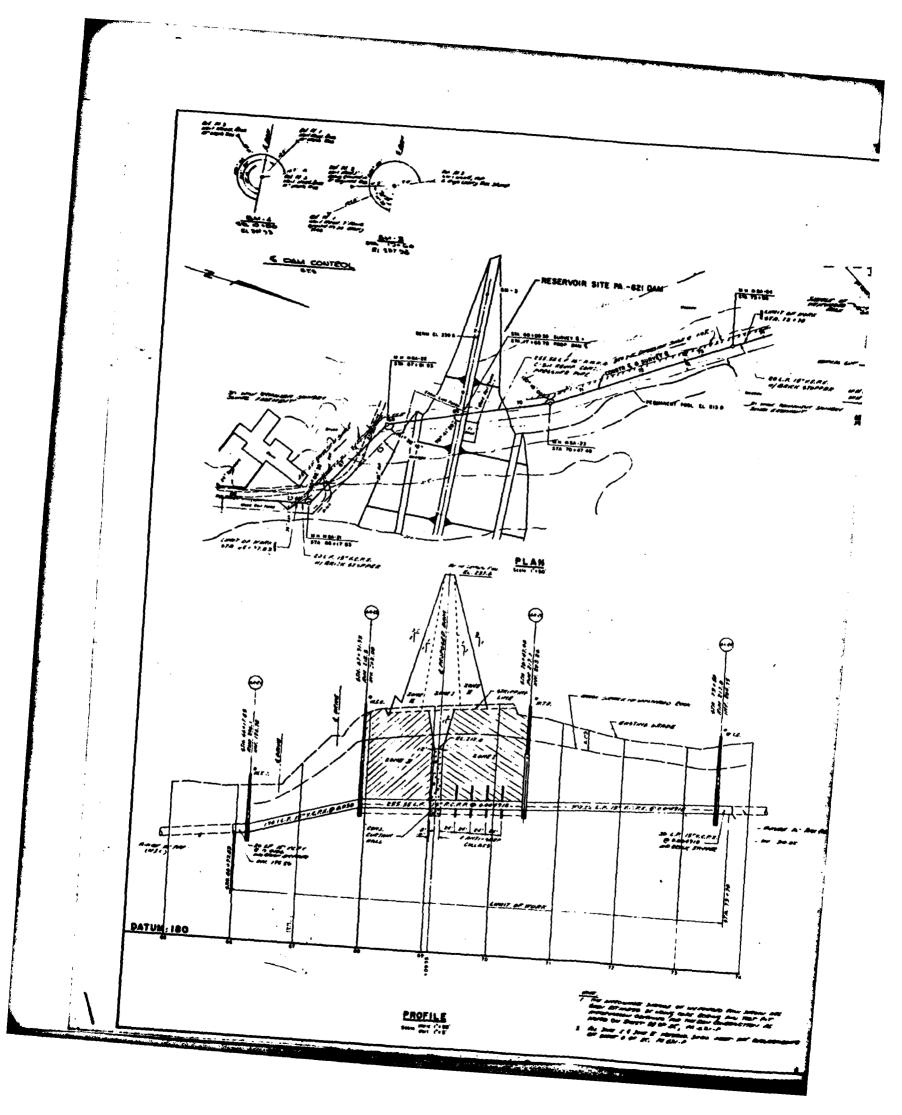


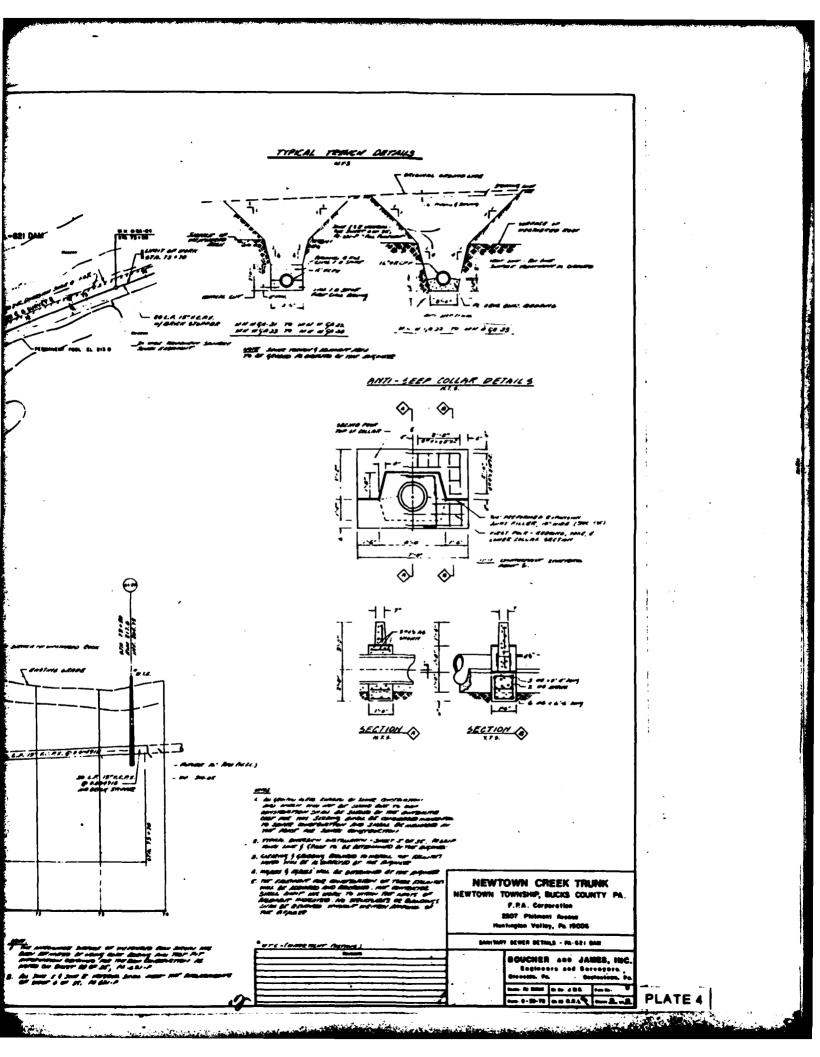


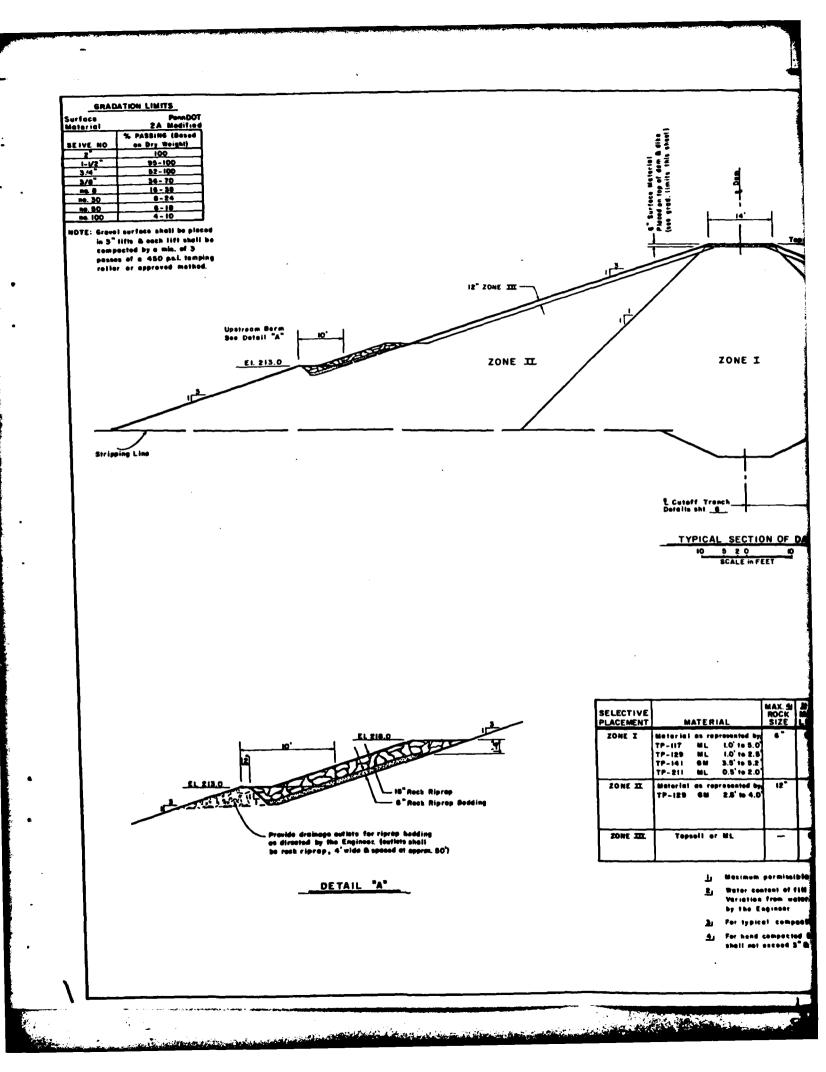


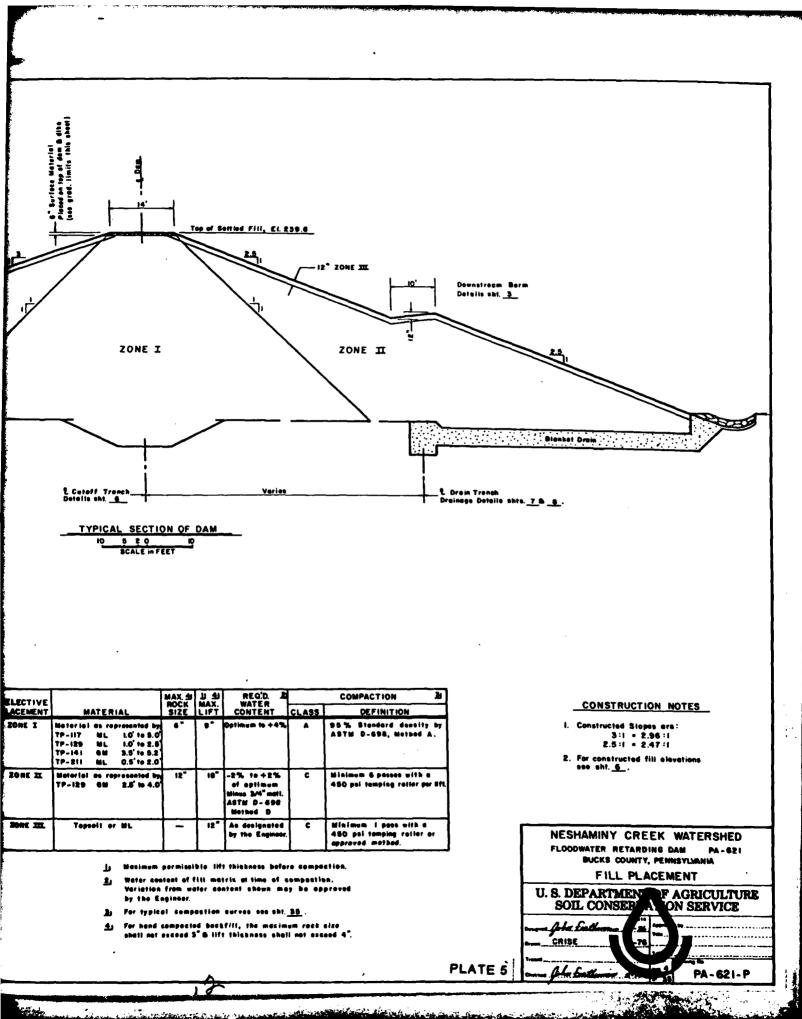




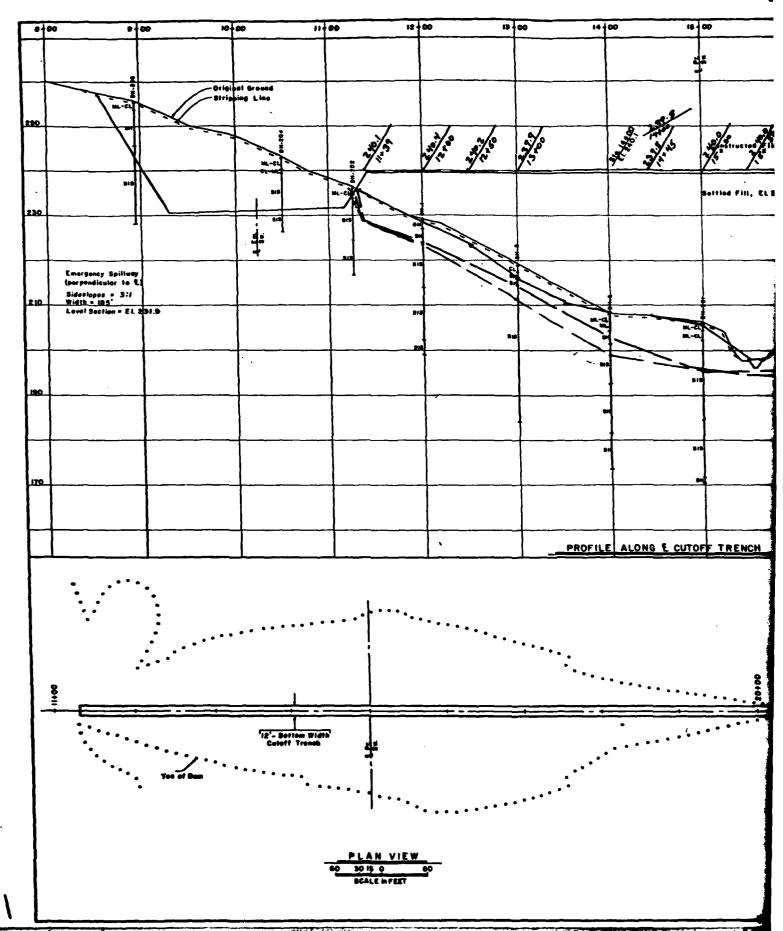


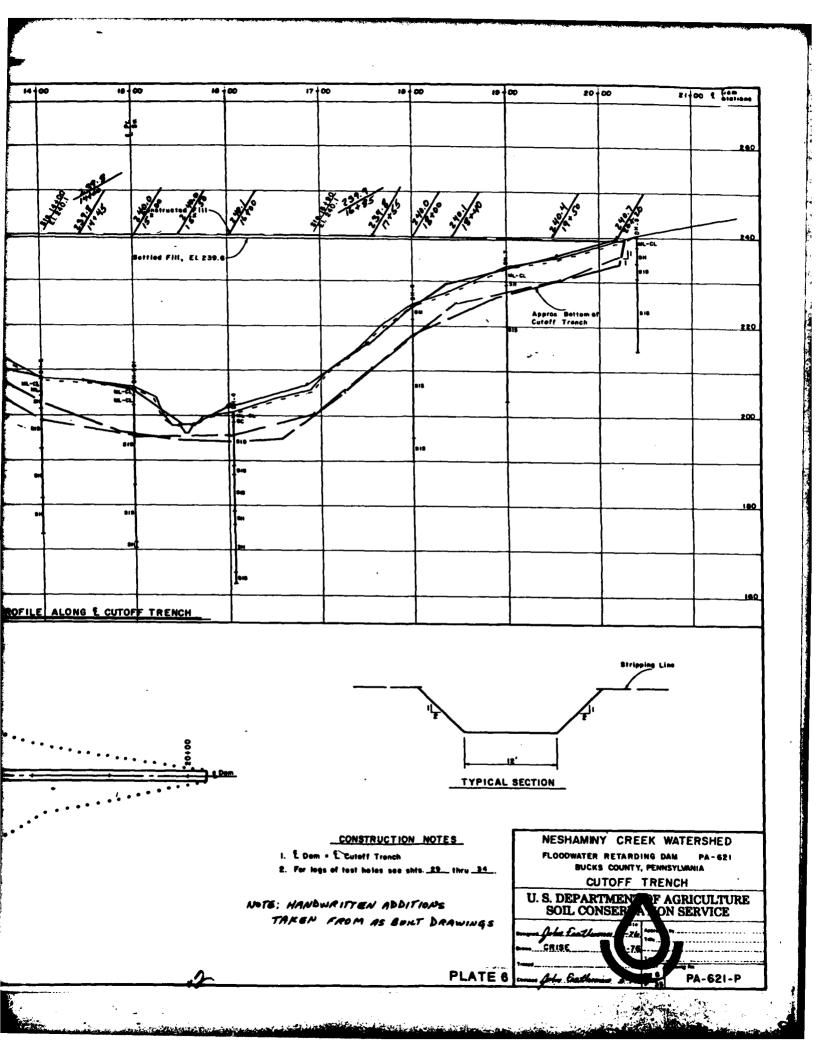


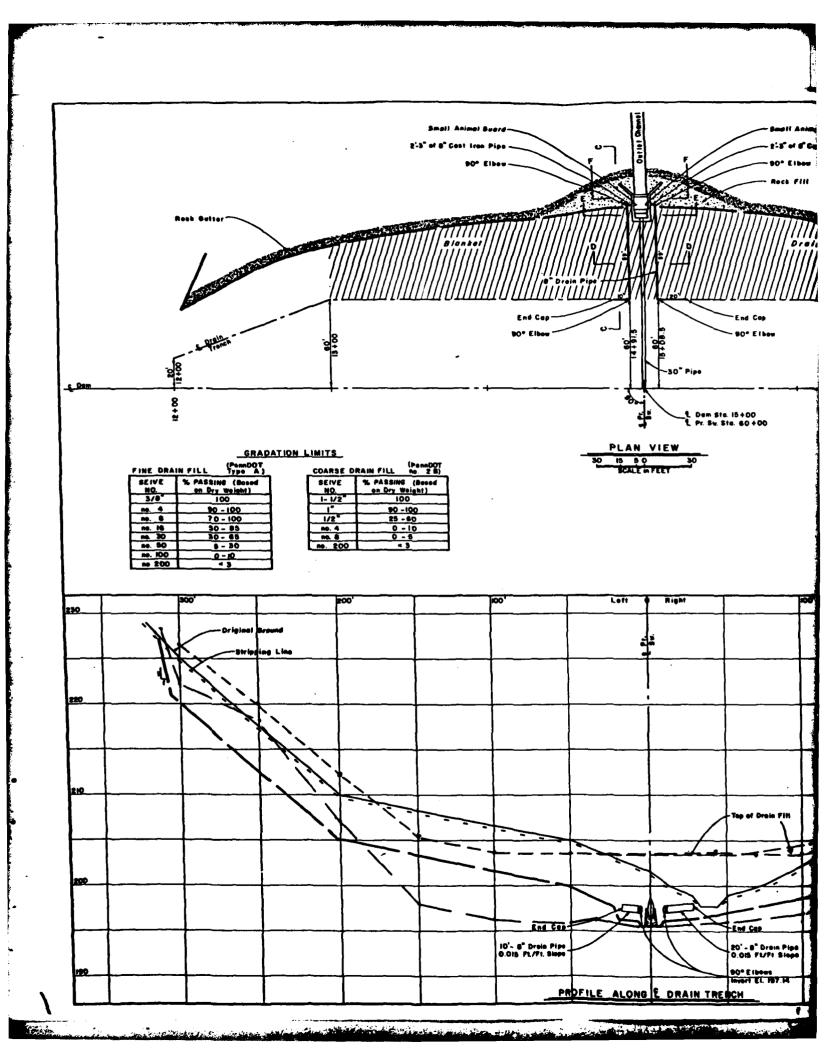


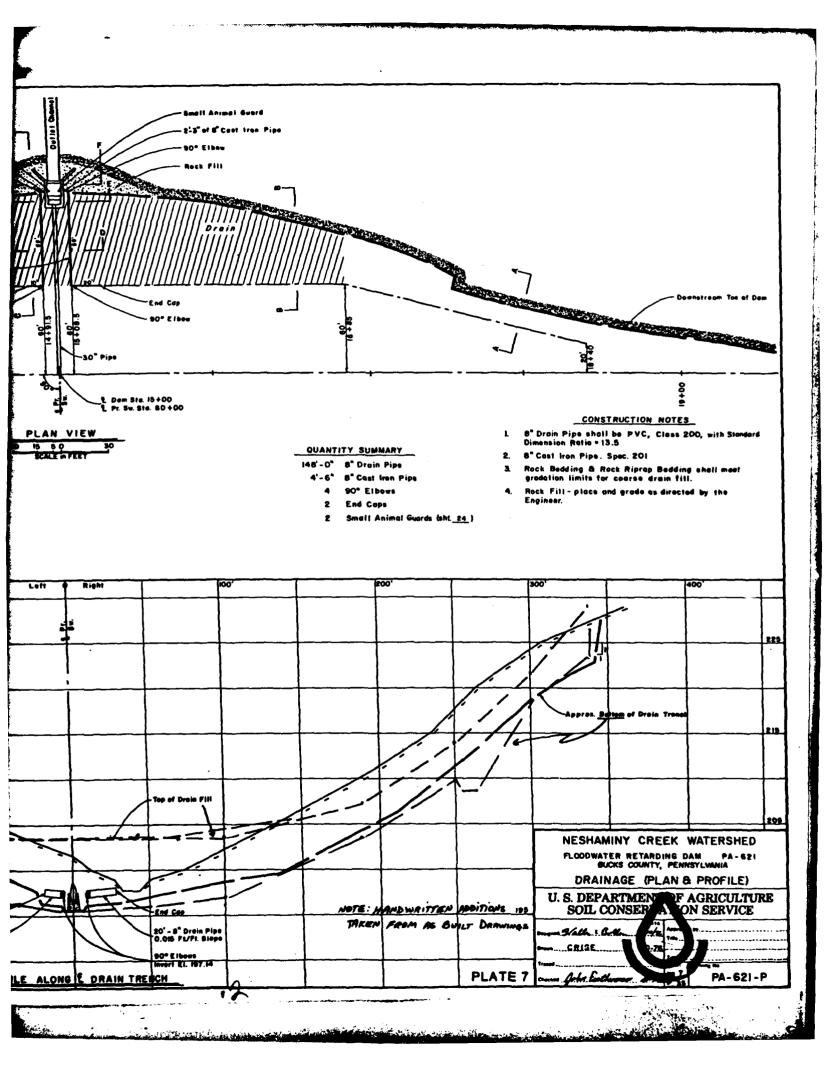


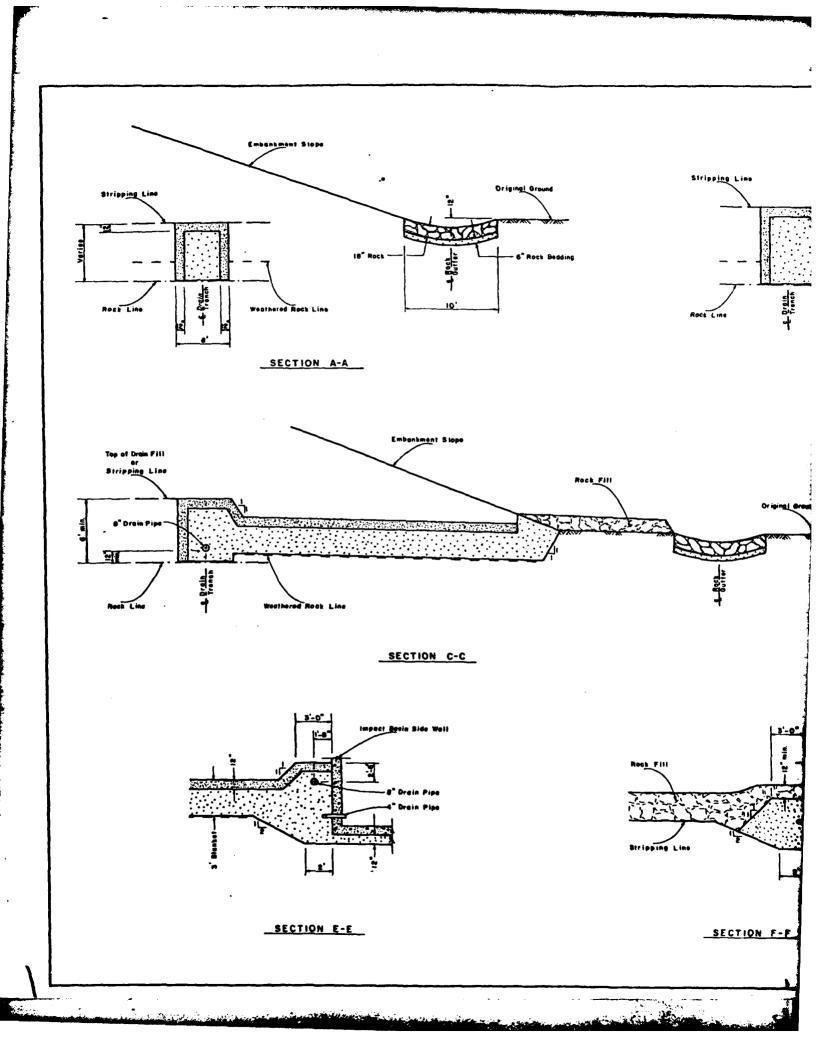
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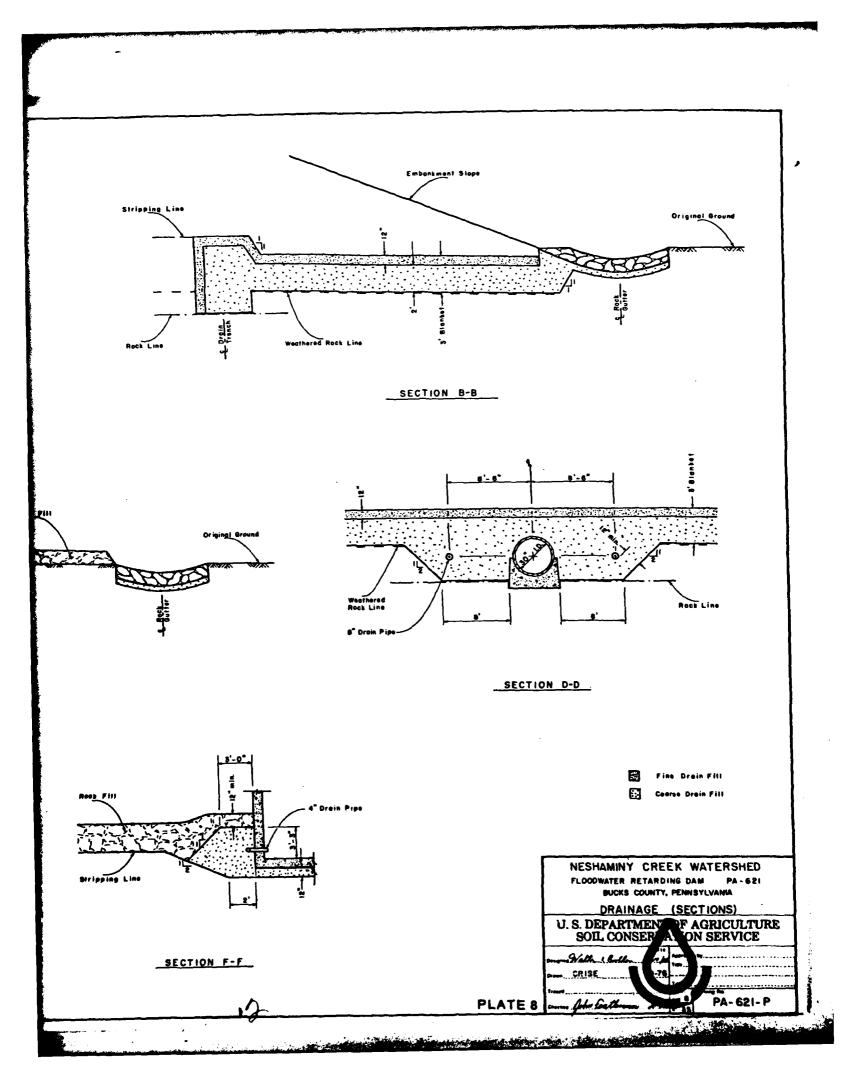


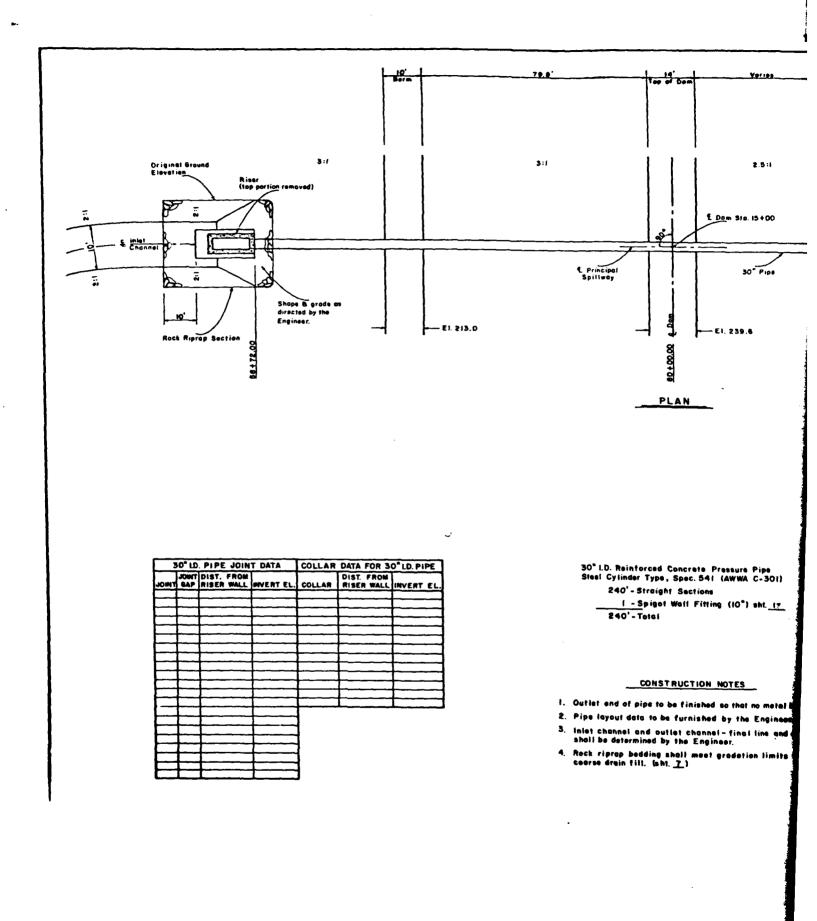


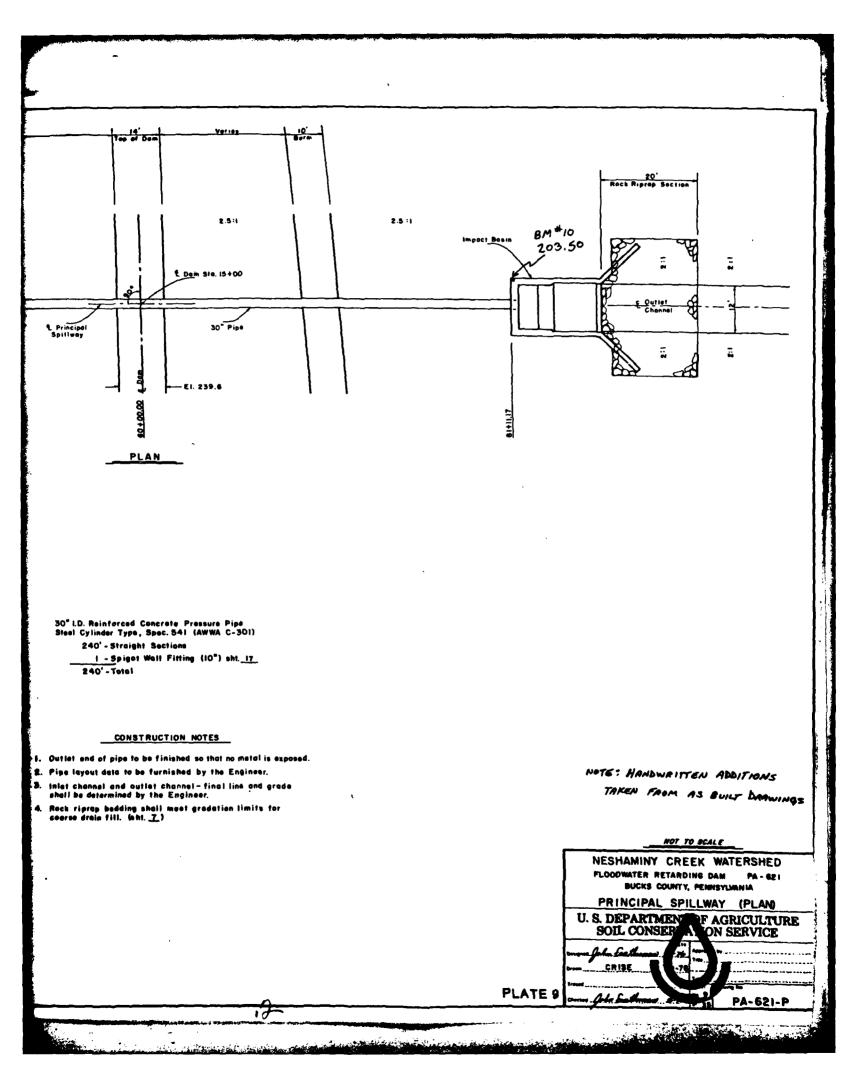


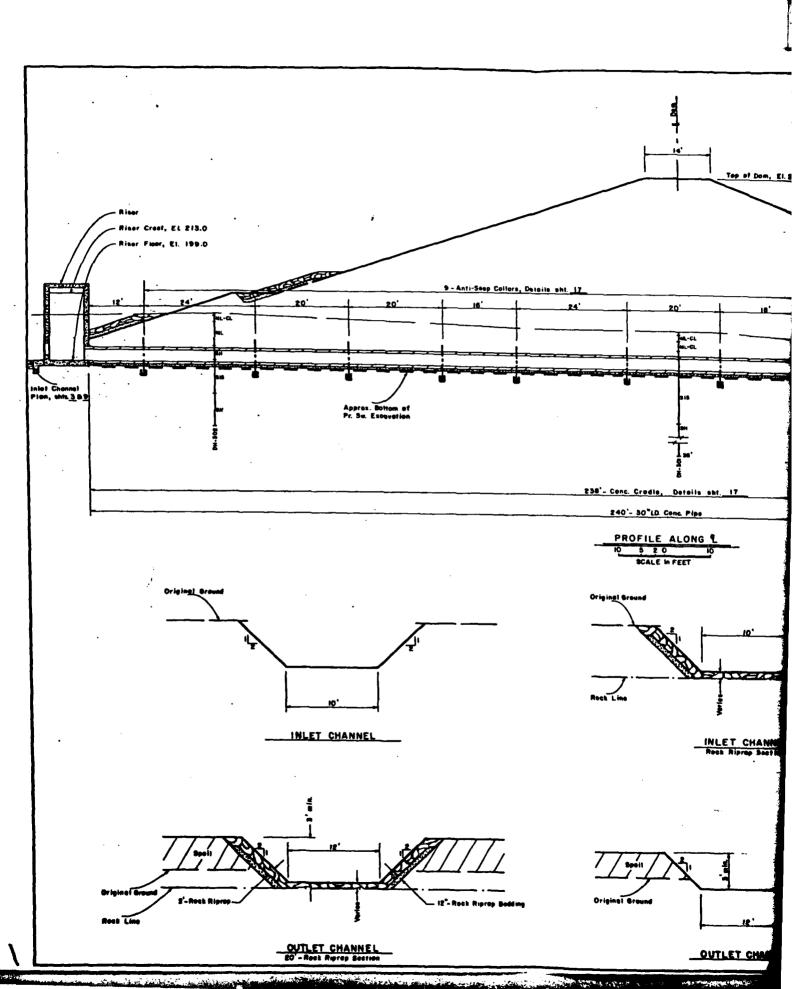


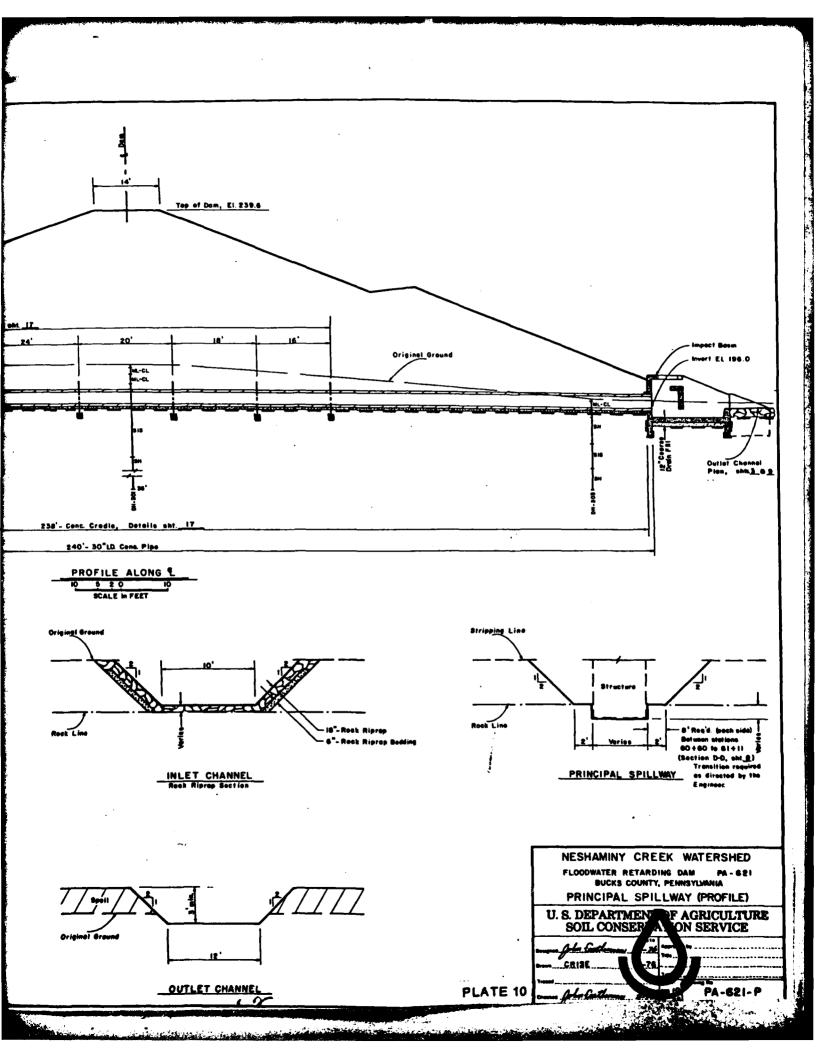


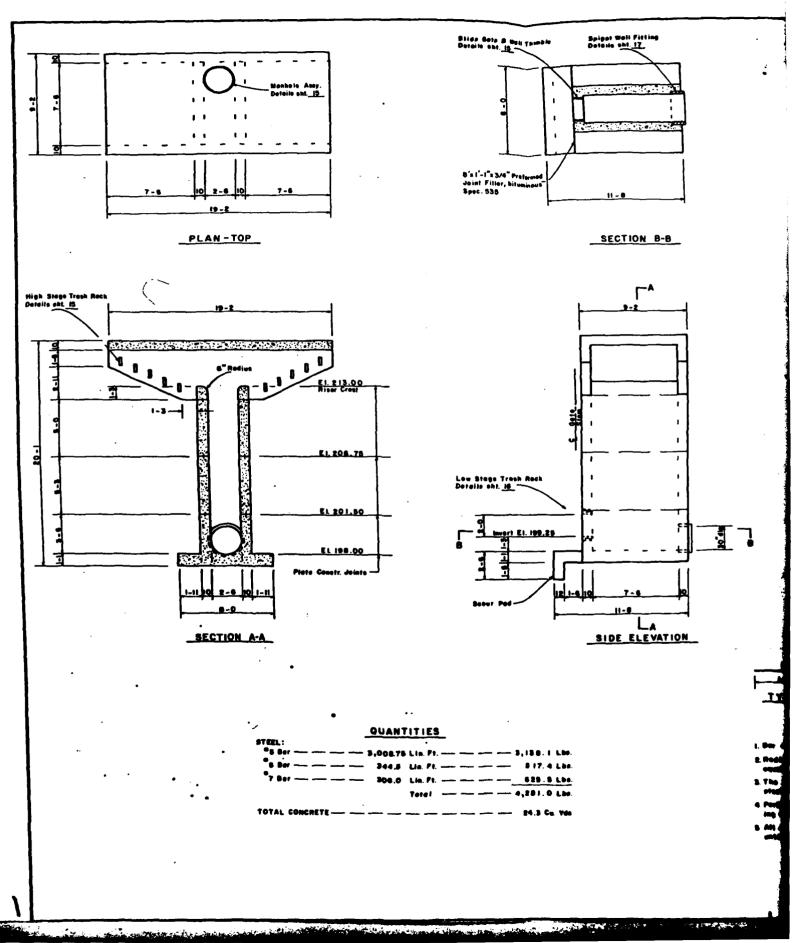


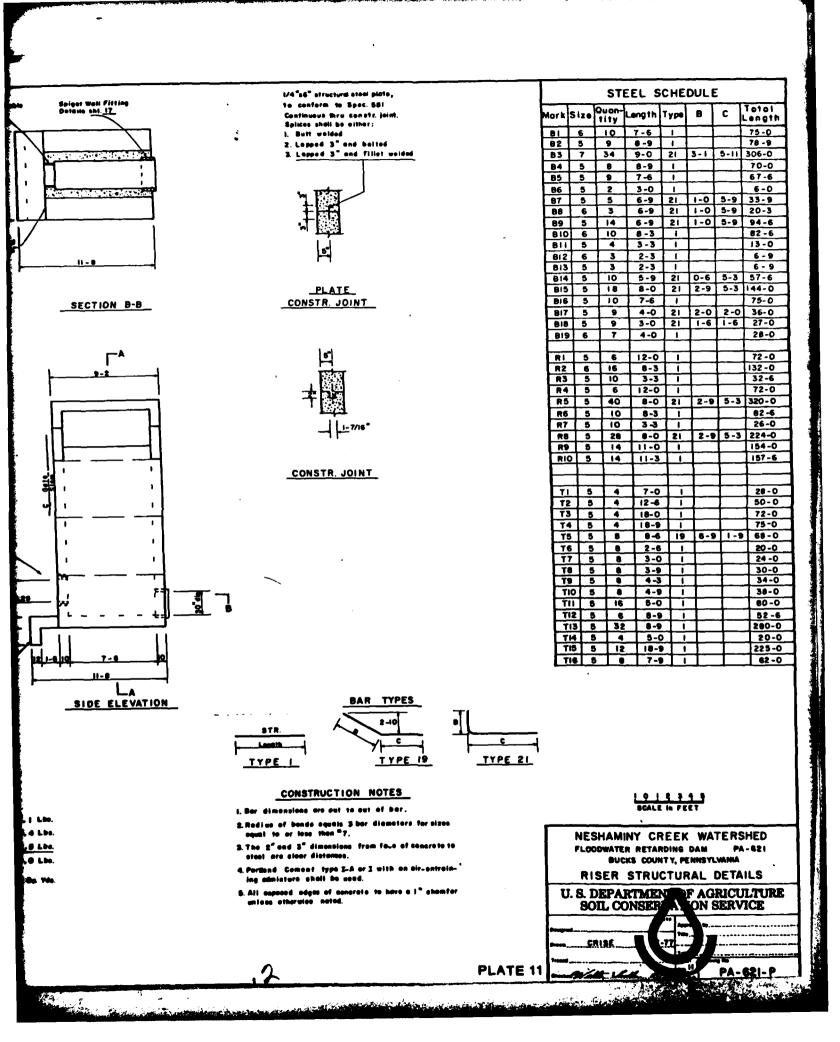


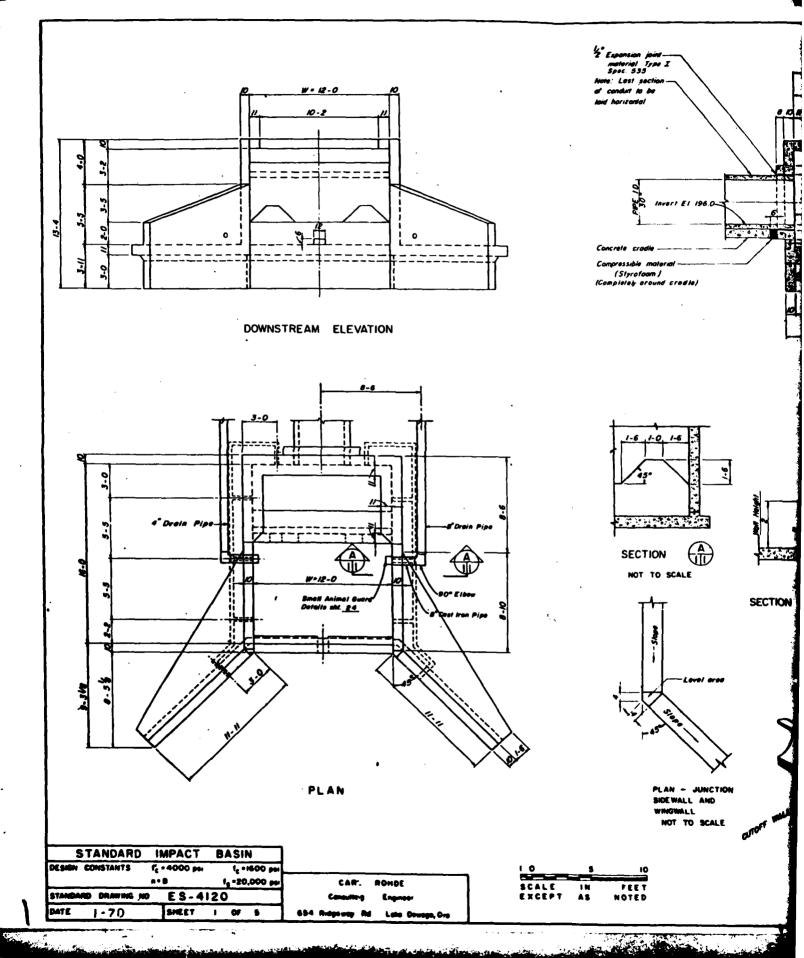




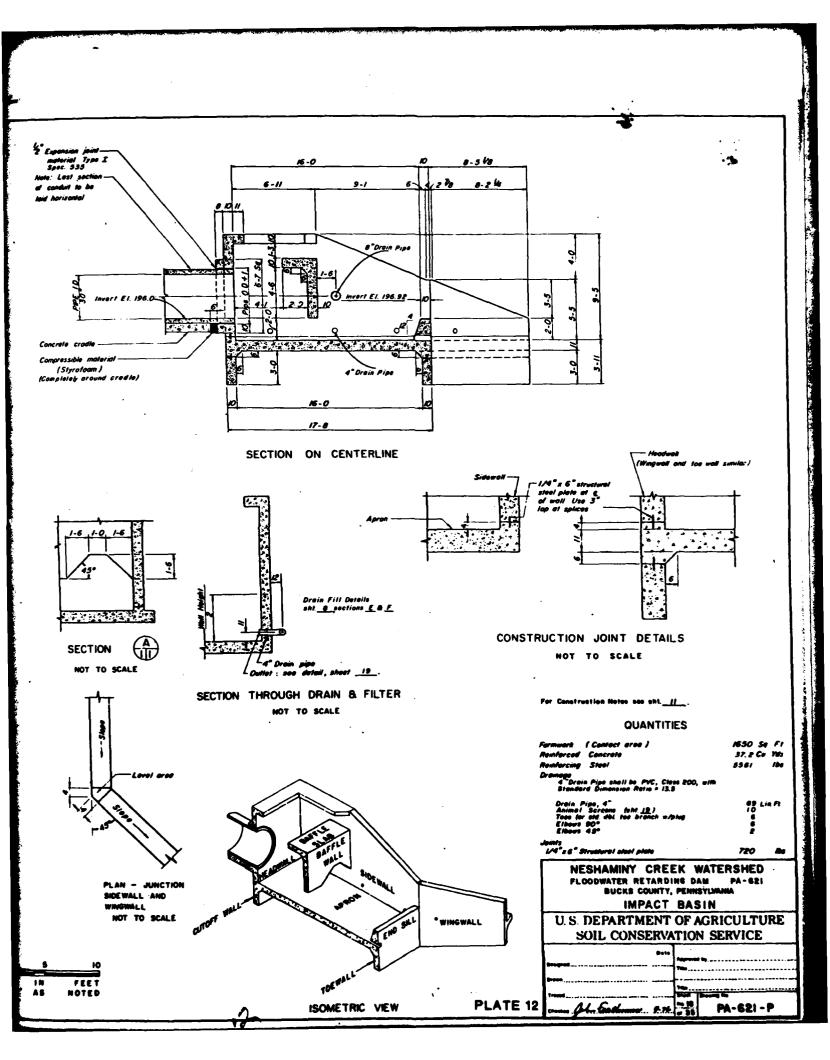


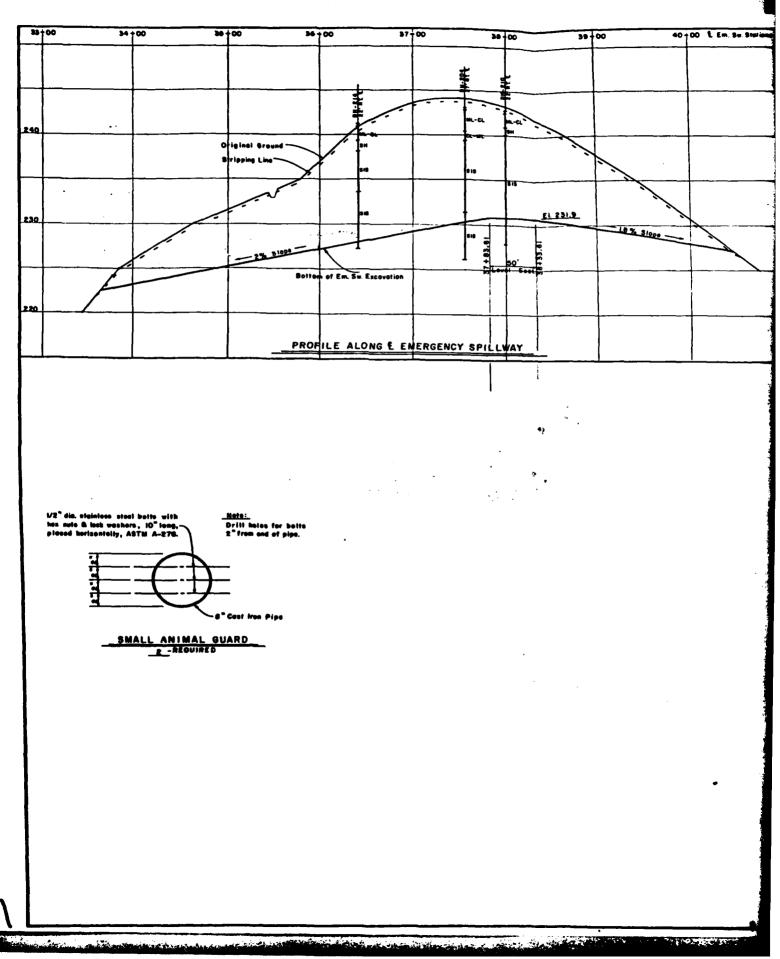






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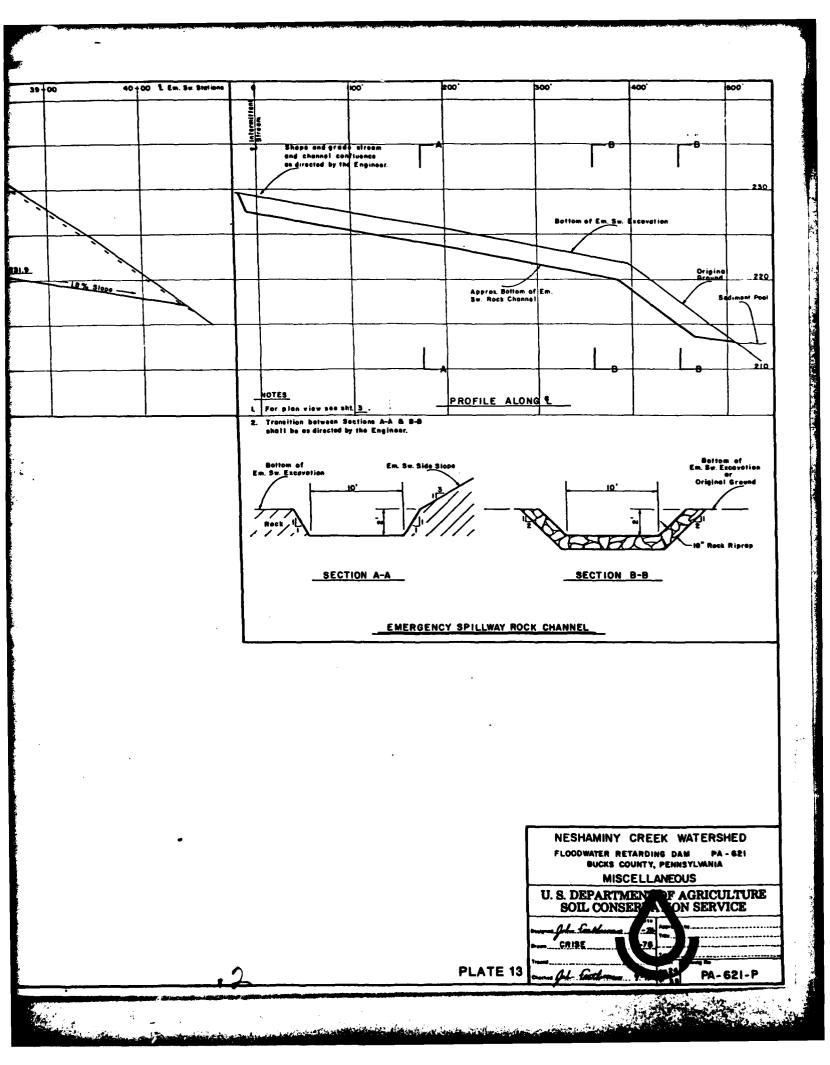


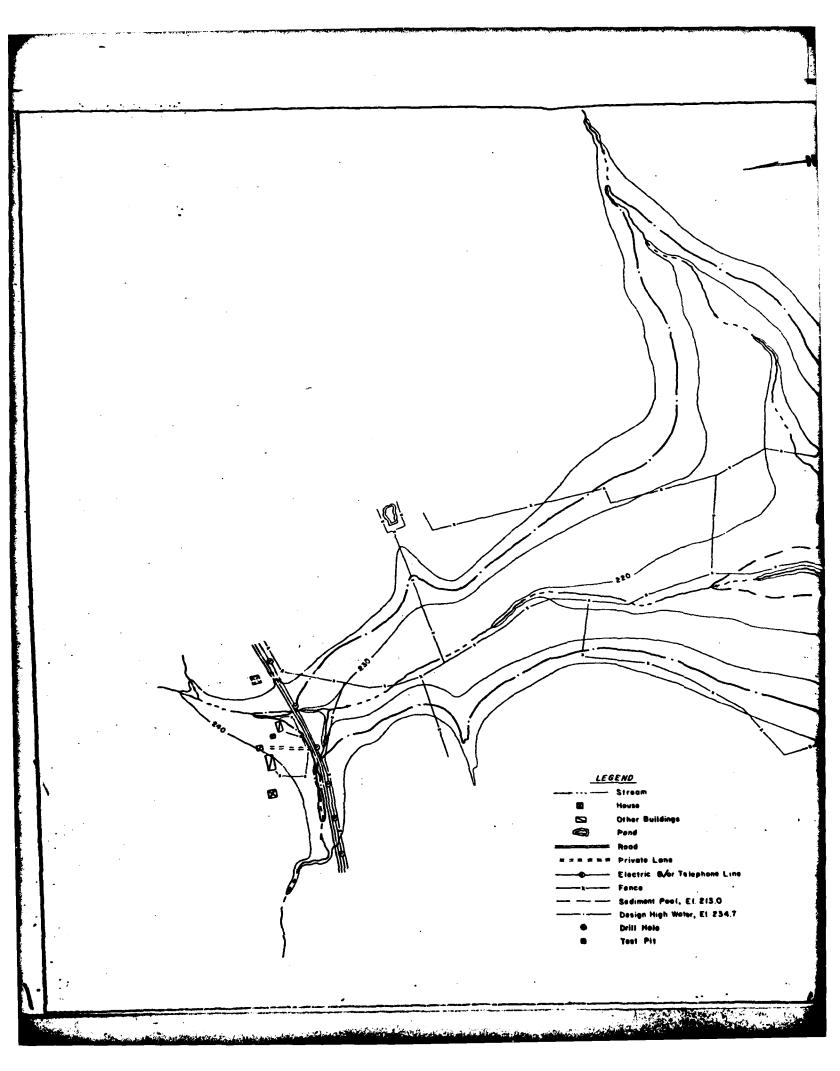


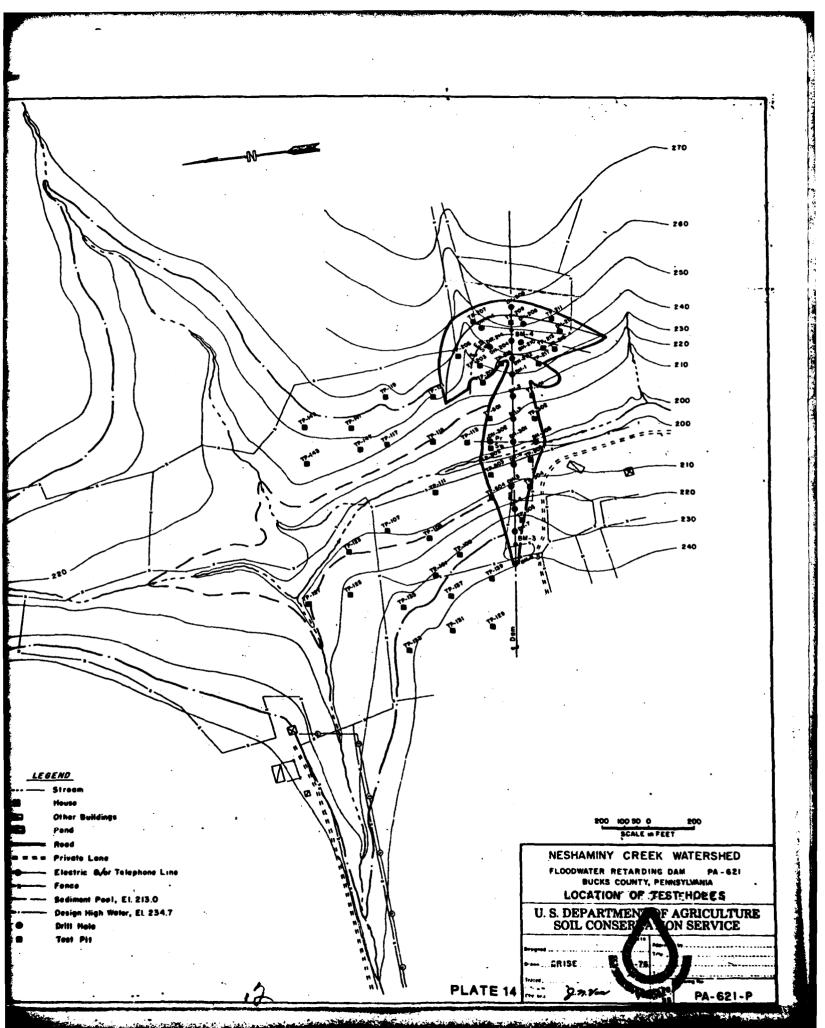
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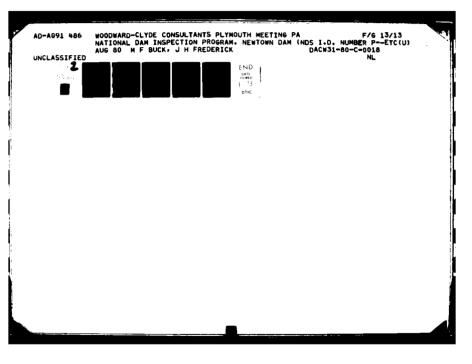


	8 841 JO	DE VAR 4-6-71 MENT: SKIP RIG										<u>CON1.8</u>	
			UNIF.									DEPTH TO	
			SOIL	STANDARD PENLY	TYPE			SAMP			22.3	25.2	50
NOLE <u>FROM</u>	0EPTN 		CLASS.	BLOWS PER 6*	BIT NSED	NQ.	TYPE	FROM FT.	T0 EI.	% 	25.2	34.0	т(54
0.0	0.4	TOP56K		1-5-17	5.87	1					•		T
0.4	2.3	GRAVEL, SILYY, RED, WEA. SHALE	GM	27-50.3	•	2	188. •	0.0 1.5	1.5	80 50	. 34.0 36.5		5
2.3 5.4	5.4 15-0	SHALE, SANDY, HARDNESS-3, RED SILTSTONE, SHALY, RED, HARDNESS-3 TO 4, VERTICAL & ANGULAR FRAC-		50/.1	TR) SPT	3	JAR	2.3	5.3 5.4	30			
		TURES TO 12,7', CL SEAMS AT 11.5 & 11.7'		•••	TRI	•		5.4	6.0	-		. ELEV.	_
5.0	26.7	SULTSTONE, SHALY, RED & GRY MOTTLED, MED. TO THICK BEDDED, BENSE, CROSSBEDDED, WEA, JOWT AT 16.8' & 13.6' WITH STAMS, MEAVY FRAC-			D IA		NX M	6.0 9.5	9.5	100		ED BY	
		TURING FROM 19.6-22.3", GRY, YHM DEDDED FROM 22.3-22.7", FROM 22.7-26.7" GRY & BANDED WITH SOME RED SHALE, ROD-57 PERCENT			:		:	12.5	35.0 19.0	100			
6.7	30.0	SILTSTONE, SHALY, THICK BEDDED, DENSE, HANDNESS-4 WITH LT. GRY			•		•	15.0 19.0	22.7	75 72			
0.0		MSTRUSIONS, (ARĜILLITE), RQD-64 PERCENT BOTTOM OF HOLE - WL (4-8-71) 5.4'			:		:	22.7	26.5 30.0	92 100	HOLE		
		•									0.0	1.5	-
		29.3. 23-00. CENTERLINE									1.5	2.5	T S
		10E VAN 4-5-73 PMENTL SKID RIG								· •	2.5	21.8	3
													5: A'
			UNIF. Soil	STANDARD PENE	TRATION TYPE			SAMP	LES				F
NOLE From	DEPTH TO	DESCRIPTION OF MATERIALS	CLASS.	PLOWS PER 6"	81T				TO	*			Ti Si
- •					USED	NQ.	TYPE			<u>NEC</u>	21.6	39.0	5
0.0 0.5	0.5 2.0	TOPSON CLAY, SILTY, 10 PERCENT SAND, TRACE OF GRAVELS, LOW PLASTIC, RED	¢L	1-2-7 17-20-33	5PT	1 2	JAR	0.0 1.5	1.5	70 70			R F
2.0	3.8	SHALE, RED, WEA., SOFT, DRY, FORMS CL WHEN MOIST + WATER STOOD IN HOL		29-50/.3	•	5	•	3.0	3.0	70 80	39.0	40.0	ء د
	5.0 35.0	SHALE BOULDER † DRALLED THADUGN; VERY SAMBY Shitstone, Shaly, Mardness-3, medium to thick bedded, red w/gry		56	TRI SPT	4	•	3.8 5.0	5.0	90	40.0		
		MOTTLING TO 10.2", VERTICAL FRACTURES FROM 6.7 TO 9.0", VERY BROKEN A 16.5", 18.0" AND 18.6", CALCITE IN ANGULAR FRACTURE AT 22.0", GRY W/	T		TRI		NXM	5.5	6.0	100			
•	•	RED FROM 30,1-35.0', SOME BANDING, ROD-66 PERCENT			•		8	6.7	6.7 12.0	100		<u>ELEV</u> ED BY;	
5.0		BOTTOM OF HOLE - #1.(4-8-71) 6.1			:		•	12.0 18.1	18.1 25.0	100 100		ING EQU	
					•			25.0	29.8	100			
		8.6. 34+00. CENTERLINE			-		-	29.0	35.0	100	HOLE		
9 <u>66E</u> 9 <u>1 11 </u> 11	HT - 101	<u>E VAN 4-2-73</u> AENT <u>1 SKID AN 3-2-</u>									FROM	TQ	0
											0.0	0.2 2.6	7
			UN IF . 50 M	STANDARD PENEL	TYPE			SAMP	LES		2.6	6.0	3
HOLE FROM	869TH T0		CLASS. SYMB.	BLOWS PER 6"	BIT <u>VSED</u>	NQ.	****		10	*	6.0	.9.3	S
							TYPE	_ <u>FI.</u> _	<u> </u>	REC.	• •		S
0.0 0.5	0.5 2.5	TOPSON SILT, CLAVEY, 10 PERCENT FINE SAND, SLIGHT PLASTIC, VERY NOIST, AED-	ML-CL	1-1-3 6-7-12	SPT +	1	JAR	0.0 1.5	1.5	80 90	9.3	25.0	S Vi
2.5	3.0	BRN SH.7, DRY,WEA. SHALE	ML	16-14-21	:	3	•	4.0	5.5	80			2
3.0	Å.9	BOULDER -DRILLED THROUGH FLAT BOULDER		14-36-37 _ 50/.h	-	4	:	5.5 7.0	7.0	70 50	25.0		B
4.0	7.0	SHALE, WEA., RED, SOVT, W/SHALE (15 PERCENT), FRAGG., DRY, WHEN WET IS LOW PLASTIC CL. 20-30 PERCENT SHALE FRAGS. FROM 6.0% 7.2*		•	TRI BIA		N N N N	7.4	8.0	80			
7.0	15.5	SILTSTONE WITH LAM MATER SMALE; RED & GRY, MARDHESS-3, THIS TO			•		•	10.6	12.1	100		DI ELEV	
		MEDIUM BEDDED, WEA. SANDSTONE, THIN BEDDED FROM 8.5' TO 9.0', VERY WEA. SMALE FROM 11.7' TO.11.9' DEOREN, WENT. FRAC. 12.9'-13.2',		•			:	12,1 13,2	13.2 15.5	100 95		ING EQUI	
		WATER ERODED VERT. JOINT FROM 13.5' TO 15.5', MED. BEDDED 13.5'- 15.5', SOME CROSS BEDDED, RQD-55 PERCENT.			:		:	15.5	19.0	100			
5.5	26.7	SNALE, SILTY, RED, MED. TO THICK BEADED, SOLID, DENSE, WITH SHALY			•		•	19.0 27.9	27.5 32.5	100 100	NOLE	DEPTH	4
		SILTSTONE STREAKS, MARDNESS-3 TO 4, 3" TO 9" PIECES, WATER ERODED JOINTS AT 23,1". A 21.3", SHALY SILTSTONE 23.0" TO 23.5", GRY, W/AED			•		•	32.5	35.0	100	FROM	<u> </u>	0
		CROSSBEDDWG FROM 23.9" TO 26.0", VERY DROKEN FROM 25.3" TO 25.8",									0.0	0.5	T
6.7	35.0	RQD-46 PERCENT. SHALE, BAY W/SHITSTONE STREAKS, THIN TO MEDIUM DEDDED, MARDHESS-3									0.5	2.0	- 1
		TO 4, SOME FRACTURING W CALCITE (THIN), VERY BROKEN AT 32.5",									.0	4.0	5
5.0		(ARGILLITE), RED SILTY SHALE FROM 34.5' TO 35.0', ROD-56 PERCENT. BOTTON OF HOLE - WL (4-9-71) 3.6'									4.0	21.4	W 5
	LEV 1	103 .0. 16+06. CENTERLINE											- 1
HEEEP	87 - JOI	VAN 4-1-71											3
		<u>ERT - Skip Alf</u>											Ri Vi
			UNIF. 10K	STANDARD PENET	TYPE			SAMP	LES		21.4	18.1	5
ILE	DEPTH		CLASS.		BIT			FROM		*	44.4		
<u>ROH.</u>		DESCAPTINE OF MATERIALS	<u>symæ.</u>	BLOWS PER 6"	USED	NQ.	TYPE		<u> </u>	_REC_			15 01
		TOPSOL SILT, CLAVEY, 10 PERCENT FINE SAND, SLIGHTLY PLASTIC, GRY-DAN	-	2-3-7	SPT	1	JAA	0.0	1.5	75			Ð
.5	1.3	SRT, CLAVET, 10 PERCENT FINE SAND, SLIGHTLT PLASTIC, SAT-BAN BRAVEL, CLAVET, RED'ORN SHALE GRAVELS 1/35 PERCENT PLASTIC FINES -	ML-CL	17-54/.3	SPT TRI	1	•	13	13	30			2
		REFUSAL AT 2.3', FINE SANDSTONE SILTSTONE, RED, WARDWESS-3, COBBLE	6C		***		NX M 9	2.8 3.6	3.6 9.0	.100	34.1	35.0	0 5
1.3 1,8		SETSTORE, SHALT, CROSS SEDDED, THIN TO MED NUM BEDDED, WATER-ERODED			•		•	9.0	14.0	100			
		DEDDING PLANES, MARDRESS-3, 5.81-6.2', THIN DEDDED, WATER ZONE, MARDNESS-2, DUE-FOUNTH INCH CLAY SEAM AT 7.8', SOFT WATER ERODED			•		•	19.5	2345	100	35.0		. DI
		SEAM AT 6.5", ONE WEN VERTICAL FRACTURE AT 8.9", SOFT WATER ERODED			•		•	29.5	36.5	100			
		ZONE FROM 8.6"-0.9", GRAY FROM 7.7", FROM 10.3" TO 12.0" SILTSTONE IS THIN BEDGED WITH SHALE STREAKS, RED TO GRAY, RQD-37 PERCENT.										- ALL SI	0 H .
	14.0	SILTSTONE, SHALT, SOLID, MARDNESS-3, 1* GRY SHALE STREAK AT 13.5',											
		GAY WARD, WATER EROOLD SEDDING PLANE AT 13.8", AQD-55 PERCENT. SILTSTONE, SHALY, RED, DENSE, HARDHESS-3, 2" VERL FRACTURED AT											
		17.0', WATER EROOCD SEAN AT 14.8', YERT, FRACTURED AT 19.8' ()* W/											
		CALCITE IN FRAC.) VERY SOLID CORE, SOME MAINLINE VERT. FRAC., RAD-65 PERCENT.											
	_												
	•												
	•	CONTINUED									1		

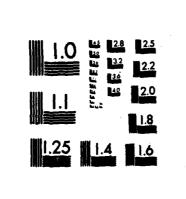
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and the second
	NOLE DEPTH	DESCRIPTION OF MATLEN	AL S									
AMPLES	EROM_TO		TE, HARDNESS-3-4, GRY W/1	RED. 1º VERT. FRAC. AT 25	11 TH 18			7' 4 28		SHALE T	0 25.21	
ROM TO %	22.3 25.2	THIN TO MED NM BEDDED	I, LIMY AT 23.51, RGD-52 PE	RCENT,								
T. FT. BLC.	25.2 34.0	THIN BEDDED, BANDED W	Y TO BROWN TO GRY (ARGILLI ITH SILTSTONE STREAKS, VEI	LT. FRAC. AT 30,3" AND 31.	0' TO 31.	3', SOFT AND BR	DKEN 31.1	RAC, FI 8' TO 3	10M 26. 2.7', Ri	9-28.8 QD-52 Pi	". ERCENT.	
.6 1.5 80 .5 2.3 50	.34.0 36.5 36.5	SILTSTONE, RED, SHALY BOTTOM OF HOLE, WL (/, DENSE, MARDNESS 3 TO 4. (4-6-71) 2.5'	SOFT WEATHERED, SHALY,20	NE AT 34.	.3', RQD-62 PERI	ENT					
.3 5.3												
5.3 5.4 30 5.4 6.0		210.7. 17+00. 9' U.S.										
1.0 9.5 100 1.5 12.5 85	LOGGED BY: DRILLING EQU	JOE VAN 4-5-71 IIPMENT <u>, skip rie -</u>	1	•								
1.5 15.0 100 5.0 19.0 75			÷		UN IF .	STANDARD PENE				SAMPLE	5	
.0 22.7 72	HOLE DEP1	н	•	,	SON CLASS.		TYPE BIT			FROM	TO	,
1.7 16.5 92 6.5 30.0 100	FROM TO	DESCRIPTION OF MATER	ALS	····	SYMB.	BLOWS PER 6'	USED	ND.	TYPE	<u>.</u>	<u>FT.</u>	R
	0.0 1.5 1.5 2.5	TOPSOIL WITH GRAVEL A SILT, CLAYEY, SLIGHT	L COBBLES PLASTIC, TRACE MOISTURE,	WEA. SHALE, CASING AT	ML-CL	2-3-4 13-19-50	5PT 5P7	1 2		0.0 1.5.	1.5 3.0	
	2.5 21.8	3.0', 10 PERCENT SANS					DIA	•	NXM	3.0	8.0	
		SEVERAL VERT. & ANGU	LAR FRAC. FROM 5.0' TO 16. ED JOINT AT 13.4' AND 17.8'	D', WORM HOLE POROSITY			•	•	• 1	14.7	14.7	- 10
SAMPLES		FROM 13.0' TO 15.3'.	AFTER 14.7' CORE PULLED SI	MALL ARTESIAN FLOW OVER			:			23.5 25.5	25.5 27.4	1(
FROM TO %		SHALY AT 21.0', ROD-4								27.4 34.5	34.5 40.0	1(
FT. FT. BEL	21.8 39.0		SHALY BANDING & CROSS-BED 25.5°, ANGULAR FRACTURING									
0.0 1.5 70 1.5 3.0 70			L 32.6' TO 33.4', RED FROM 9.0', RQD~53 PERCENT.	29.7' TO 33.6', MARDHESS-	3 70 4, 8	LED & GRY SHALY	SILTSTON	E FROM	33.6' T	10 37.0"	(Akeilit I	ne)
3.0 3.8 30 3.8 5.0	39.0 40.0 40.0		MED. BEDDED, GRY, DENSE.						•			
5.0 5.5 90	40.0		· · · · · · · · · · · · · · · · · · ·	•								
5.5 6.0	DH-8. ELEV	. 240.7". 20+40. CENTERL	INE									
6.7 12.0 100 12.0 18.1 100	LOGGED BY: Drilling Eg	JOE VAN 4-7-	<i>y</i> 1					•				
L8.1 25.0 100 25.0 29.0 100					UNIF. SON	STANDARD PEN	TRATION TYPE			SAMPL	B	
29.0 35.0 100	HOLE DE				CLASS. SYMB.	BLOWS PER 6"	BIT USED	**	TYPE	FROM FT.	T0 FT.	
	FROM T		[ML3	·								
	0.0 0.1	TOPSOIL S.R.T. CLAYEY, SLIGHT	T PLASTIC, RED, WET, 10 PE	RCENT SAND	ML-CL	1-1-1 2-9-30	SPT T	1 2	JAR 8	0.0	1.5	
SAMPLES	2.6 6.0	SHALE, SANDY, WEA.		. .		56/.5	TRI SPT	3	JAR	2.8 4.5	4.S 5.0	
FROM TO % <u>FT. FT. REC.</u>		ANGULAR FRAC. AT 7.	4', SOME FUGGY POROSITY, C .0'-9.0', GRY TO BROWN, SO	L SEAM AT B.3', SOME			TR) Dia		RXM	5.0 6.0	6.0 9.3	
0.0 1.5 80	9.3 25.	D SILTSTONE, HARDNESS	-3 TO 4 (ARGLLLITE), MEDIU	M TO THICK BEDDED, DENSE,		•			•	9.3	10.5	1
1.5 3.0 90		OIL STAM IN JOINTS A	' TO 12.3', RED, SOME GRY P T 13.2', VERT, FRAC, 18.2'	-22.8' ANGULAR JOINT AT			•		•	11.7	14.7	
4.0 5.5 80 5.5 7.0 70	25.0	23.2", RED W/GRAY, I BOTTOM OF HOLE - WL	DENSE, SOLID, FROM 21.5'-2 . (4 -9 -73) 1.4'	S', RQD+52 PERCENT.						14.7 18.2	18.2 25.0	1
7.0 7.4 50 7.4 8.0												
8,6 10,6 89 10,6 12,1 100	<u>ви-301, е</u> Logged by	LEV. 205.4. 15+00, CENTE										
12,1 13,2 100 13,2 15,5 9 5		QUIPMENT SKID RIG			UN IF	STANDARD PEN	TRATION			SAMPL	ES	
15.5 19.0 100 19.0 27.9 100	•				\$0 IL		TYPE BIT	-		FROM	TO	
27.3 32.5 100	HOLE DE	PTN DESCRIPTION OF MATE	RIALS		CLASS. <u>SYMB.</u>	BLOWS PER 6"	USED	NQ.	TYPE	_FT	<u></u>	
32.5 35.0 100						2-2-3	SPT	1	,MR	0.0	1.5	
	0.0 0. 0.5 2.	O SILT, CLAYEY, 15 PE	RCENT FINE SAND, MOIST, DR	OWN, SOME GRAVEL	ML-CL	1-3-4 7-13-37		2		1.5 3.0	3.0	
	· 2.0 4.	1.5'-2.0', ALLUV NUP 0 SULT, SLIGHT PLASTE	C. 14 PERCENT SAND, TRACE	MOISTURE, WEA. SHALE,	ML-CL		PIA			4.5	8.9	
	4.0 21	W/SHALE GRAVELS FI	ROM 3.0' TO 4.0', TAN, YELL Boulder to 4.7', cross-bed	OFD, RED TO 8.0', TO					•	8.0	9.3	
		15.0" GRY SANDED. P	ARONESS-3, THIN BEDDED, BINT ON STAINING JOINT FROM	ROKEN 13.3""13.7"			•			10.5	12.5	;
		21.4" HARDNESS=3	TO 4, THICK DEDDED, SAY & A DNE STAWING FROM 15,2*-15	ED MOTTLED,			:		:	12.5	20.0	1
		VERT, FRAC, 14.5"-	15.5", 16.5"-18.8" RED SHA	LE, HARDNESS-2 W/					:	20.0 23.5	23.5 26.5	
SAMPLES	21,4 34	SHLTY STREAKS. 1 SHALE, SILTY, MED.		N 22.4'-23.4', BRY W/			:		•	26.5	30.0 35.4	1
PROM TO %		RED & CROSS BEDDING	G (ARGILLITE), HARDHESS-3 F 1. BEBBEB, CALCAREDUS, HAR	BHESS-3. HARDNESS-4.								
FT. FT. ALC.		ABARTA SIMY SMALF	FROM 28.0'-28.8' W/ VERT. 29.2'-29.9', WITH CL SEAM	FRAC, THIN BEARER -								
0.0 1.5 75 1.5 2.3 30		29.8" THIN BEDDED /	AND SANDY, SLIGHT CALCARED	US, NARDHESS"Z PLUD,								
2.5 2.8 2.8 3.6 .100		ANE CALLS PIECE 11	.5'-33.5', THIN BEDDED, WIT .5'-34.0', AQD-43 PERCENT.		4		SHAMI		EEV H	ATED	HED	
3.6 9,0 100 9.0 14,0 100	34.1 35	RED, ROD-12 PERCE	BEDDED, HARDNESS-2, WEA.	WITH GALGITE PARTINGS,			ESHAMI					
14.0 19.5 100 19.5 2945 100	35.0	BOTTOM OF HOLE.	12 (4-12-71) 7.5'				BUCKS C				-	
29.5 36.5 100							LOGS	OF TI	EST HO	DLES	·	
	NOTE - A	LL SOR AND ROCK CLASSIF	ICATIONS WERE DETERMINED B	V VISUAL-MANUAL METHOD.		U.S. DEI	ARTN	IEN	ГOF	AGR	ICULI	rU
						SOIL	CON				RVIC	E
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MICROCOPY RESOLUTION TEST CHART • NATIONAL BUREAU OF STANDARDS-1963 A

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LEGEND

TEST HOLE NUMBERING SYSTEM

	•		
Centerline of Dam	1 ·	-	99
Borrow area	101	-	199
Emergancy spillway	201	-	299
Centerline of outlet structure	301	-	399
Stream channel	401	-	499
Relief wells	501	-	599
	60I ·	~	699
	701	~	799

UNIFIED SOIL CLASSIFICATION SYSTEM SYMBOLS

- Well groded gravels; gravel-sand mixtures GW
- GP Poorly graded gravels
- GM Silty gravels; gravel-sand-silt mixtures
- GC Clayey gravels; gravel-sand-clay mixtures
- SW Well graded sands ; sand-gravel mixtures
- SP: Poorly groded sands
- SM SC Sitty sands; sand-sitt mixtures
- Clayey sands; sand-clay mixtures
- Silts; silty, very fine sands; sandy or clayey silts ML
- CL Clays of low to medium plasticity; silty, sandy or gravelly clays
- СН Clays of high plasticity; fat clays
- MH Elastic silts; micoceous or diatomaceous silts
- OL Organic silts and organic silty clays of low plasticity
- Organic clays or silts of medium to high plasticity OH

BEDROCK SYMBOLS

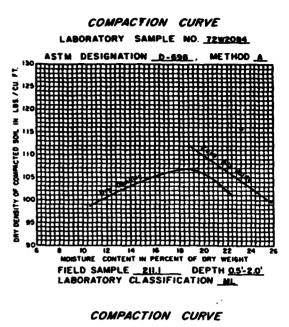
	•			
8	Basait	Sc	Schist	
Gn	Gneiss	Sh	Shale	
Gr	Granita	SiS	Siltstone	•
Ls	Limestone	. 51	Slate	
Ne	Merble	Sc	Sondstone	

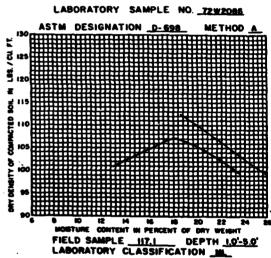
SAMPLES

- 25 Disturbed
- US Undisturbed

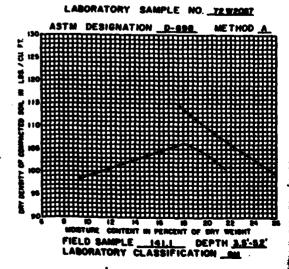
NOTE .

All soil and rock classifications were determined by visual examination, except where otherwise noted.



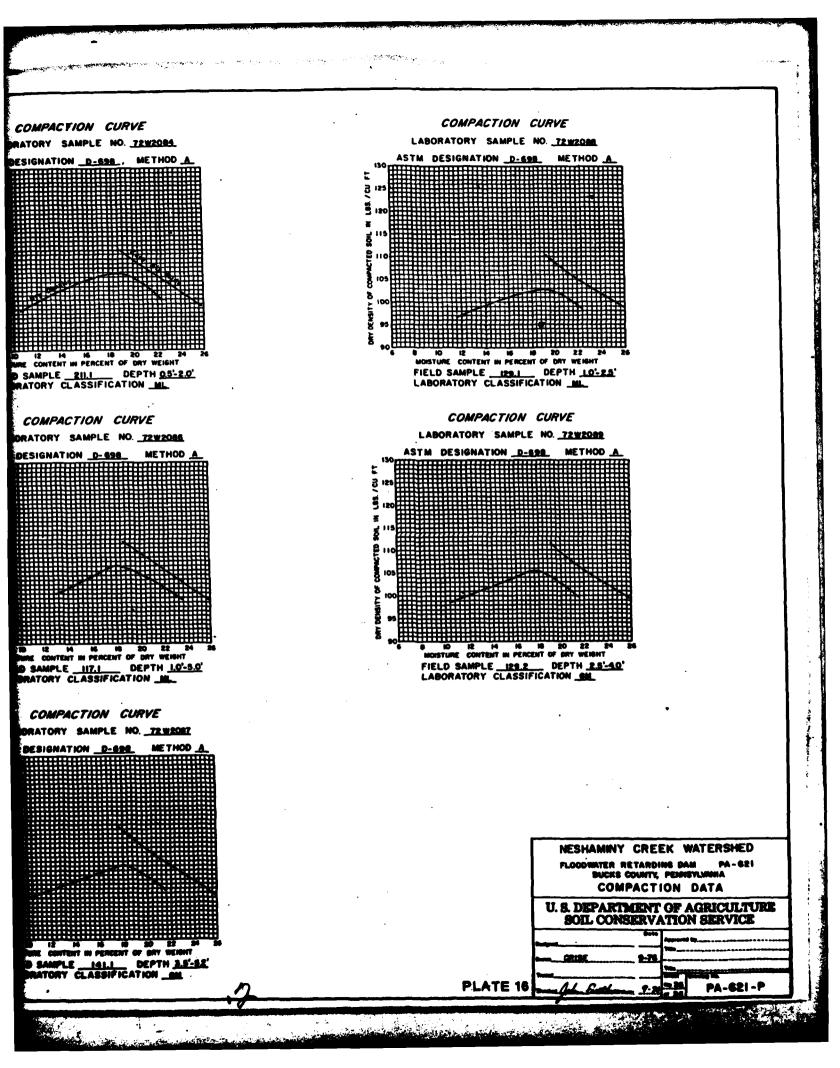






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APPENDIX

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SITE GEOLOGY NEWTOWN DAM (SCS PA 621 DAM)

1.

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SCS PA 621 Dam is located in the Triassic Lowland Section of the Piedmont Physiographic Province. As shown in Plate F-1, the site is underlain by the Stockton Formation of Triassic age. Information contained in the state files describes the bedrock as silty shale and shaly and sandy siltstone that strikes east-west and dips 10 to 20 degrees to the north. This is consistent with the observed N70°E strike and 11 degree north dip (upstream) of bedrock exposed on the left side of the emergency spillway. High angle rock jointing strikes near east-west (parallel to dam centerline) and north-south (perpendicular to dam centerline). A potential for seepage under the dam exists due to the jointed and blocky character of the bedrock.

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