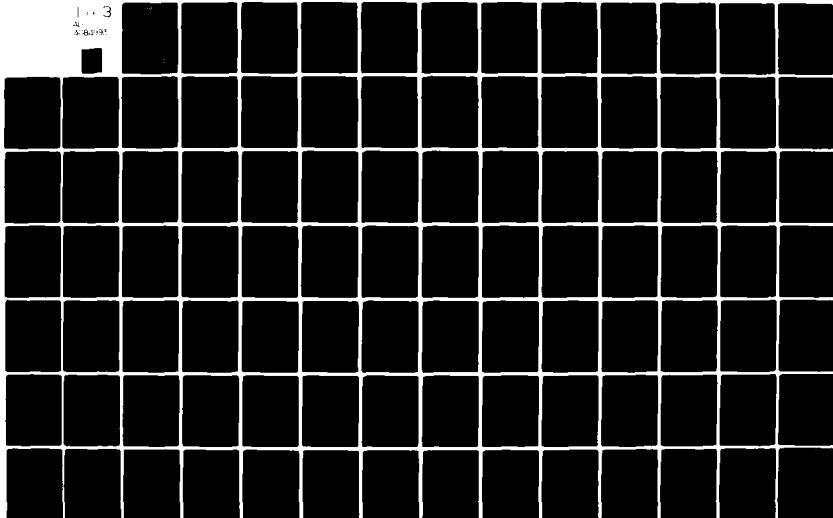
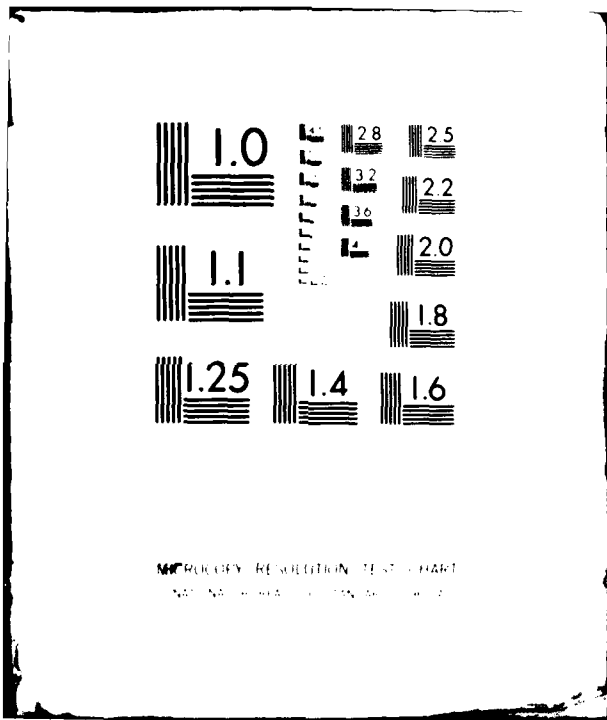


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**Volume 14A-1-Ambient Atmosphere
(Major and Minor Neutral Species
and Ionosphere)**

Science Applications, Inc.
P.O. Box 2351
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30 June 1979

Final Report for Period 1 January 1976—30 June 1979

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| 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) ROSCOE Ambient Atmospheric Model Ambient Ionospheric Model Major Neutral Species Minor Neutral Species Charged Species | | |
| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The ROSCOE-Radar ambient atmosphere model has been extensively revised to provide (a) major atmospheric properties and species densities corresponding to either a code-generated or (optional) user-specified latitude- and season- dependent temperature profile below 120-km altitude, (b) an increase from 10 to 19 minor species profiles (O, O(¹ D), O ₂ (a ¹ Δ _g), O ₃ , N(⁴ S), N(² D), N(² P), NO, NO ₂ , N ₂ O, CO ₂ , CO, CH ₄ , H ₂ O, OH, HO ₂ , H, Ar, and He), with some of them having complex dependencies on latitude (or even geographic position in the | | |

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20. ABSTRACT (Continued)

case of water below 5-km altitude), local apparent time, fractional season-year, and solar decimetric flux, (c) (optional) user-specified water-vapor profile, and (d) an ionosphere with e, O⁺, NO⁺, O₂⁺, and N₂⁺ as ionized species (>90 km).

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Conversion factors for U.S. customary
to metric (SI) units of measurement.

| To Convert From | To | Multiply By |
|--|--|----------------------------|
| angstrom | meters (m) | 1.000 000 X E -10 |
| atmosphere (normal) | kilo pascal (kPa) | 1 013 25 X E +2 |
| bar | kilo pascal (kPa) | 1.000 000 X E +2 |
| barn | meter ² (m ²) | 1.000 000 X E -28 |
| British thermal unit (thermochemical) | joule (J) | 1.054 350 X E +3 |
| calorie (thermochemical) | joule (J) | 4.184 000 |
| cal (thermochemical)/cm ² | mega joule/m ² (MJ/m ²) | 4.184 000 X E -2 |
| curie | *giga becquerel (GBq) | 3 700 000 X E +1 |
| degree (angle) | radian (rad) | 1.745 329 X E -2 |
| degree Fahrenheit | degree kelvin (K) | $T_K = (T_F + 459.67)/1.8$ |
| electron volt | joule (J) | 1.602 19 X E -19 |
| erg | joule (J) | 1.000 000 X E -7 |
| erg/second | watt (W) | 1.000 000 X E -7 |
| foot | meter (m) | 3 048 000 X E -1 |
| foot-pound-force | joule (J) | 1.355 818 |
| gallon (U.S. liquid) | meter ³ (m ³) | 3 785 412 X E -3 |
| inch | meter (m) | 2 540 000 X E -2 |
| jerk | joule (J) | 1 000 000 X E +9 |
| joule/kilogram (J/kg) (radiation dose absorbed) | Gray (Gy) | 1.000 000 |
| kilotons | terajoules | 4.183 |
| kip (1000 lbf) | newton (N) | 4.448 222 X E +3 |
| kip/inch ² (ksi) | kilo pascal (kPa) | 6 894 757 X E +3 |
| ktap | newton-second/m ² (N-s/m ²) | 1.000 000 X E +2 |
| micron | meter (m) | 1 000 000 X E -6 |
| mil | meter (m) | 2 540 000 X E -5 |
| mile (international) | meter (m) | 1 609 344 X E +3 |
| ounce | kilogram (kg) | 2 834 952 X E -2 |
| pound-force (lbs avoirdupois) | newton (N) | 4.448 222 |
| pound-force inch | newton-meter (N-m) | 1 129 848 X E -1 |
| pound-force/inch | newton/meter (N/m) | 1 751 268 X E +2 |
| pound-force/foot ² | kilo pascal (kPa) | 4 788 026 X E -2 |
| pound-force/inch ² (psi) | kilo pascal (kPa) | 6 894 757 |
| pound-mass (lbm avoirdupois) | kilogram (kg) | 4 535 924 X E -1 |
| pound-mass-foot ² (moment of inertia) | kilogram-meter ² (kg-m ²) | 4 214 011 X E -2 |
| pound-mass/foot ³ | kilogram/meter ³ (kg/m ³) | 1 601 846 X E +1 |
| rad (radiation dose absorbed) | **Gray (Gy) | 1.000 000 X E -2 |
| roentgen | coulomb/kilogram (C/kg) | 2 579 760 X E -4 |
| shake | second (s) | 1 000 000 X E -8 |
| slug | kilogram (kg) | 1 459 390 X E +1 |
| torr (mm Hg, 0° C) | kilo pascal (kPa) | 1 333 22 X E -1 |

*The becquerel (Bq) is the SI unit of radioactivity; 1 Bq = 1 event/s.

**The Gray (Gy) is the SI unit of absorbed radiation.

A more complete listing of conversions may be found in "Metric Practice Guide E 380-74," American Society for Testing and Materials.

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SECTION 1
INTRODUCTION

In this volume we describe the ROSCOE-IR model for the major and minor neutral species in the ambient atmosphere and the ionized species in the ambient ionosphere [ROSCOE Model 1]. The overall model consists of 16 subroutines of which three are major subroutines:

- a. ATMOSU provides the major neutral species and the general properties of the ambient atmosphere,
- b. SPCMIN, supplemented by Subroutines OZONE, WATER, WVOPT, and H2OSVP, provides the minor neutral species, and
- d. IONOSU provides the ambient ionized species and the general properties of the ionosphere.

The principal changes for these three routines in going from ROSCOE-Radar to ROSCOE-IR are summarized below.

The new Subroutine ATMOSU provides for:

- a. Replacement of the predetermined fit coefficients for the g/T_M profile by those derived during the initialization phase from specifying a temperature profile and a molecular weight profile.
- b. Use of a 0- to 120-km temperature profile for any latitude and season, obtained in Subroutine TEMPZH by linear interpolation of a set of latitude and season profiles based on the U.S. Standard Atmosphere Supplements, 1966 [US-66].
- c. Use of a specified universal profile of the molecular-weight function $[(M_*/M)-1] \equiv f = f_{DAY}$, independent of latitude, season, and diurnal variation. (The new f -function is specified by the DD-coefficient array for an 11th-degree polynomial.) However, the nighttime atomic oxygen profile differs from the daytime profile below 90 km and is computed from a separate fit function. The daytime atomic oxygen profile is computed from specification of temperature and molecular-weight profiles instead of being specified directly and entered as data in Subroutine SPCMIN.

- d. An option for the user to specify a temperature profile of interest to him (at altitudes $z = 0(4)120$ km) instead of using the one selected by the code as a function of latitude and season.
- e. Elimination of a pressure-correction factor employed in the original model to match the CIRA-1965 [CI-65] conditions at 120-km altitude.
- f. Season-dependent conditions at 120-km altitude (the base altitude for the high-altitude diffusion model) instead of constant conditions.
- g. An increase of the SNI array to 30 from 6.

The new Subroutine SPCMIN provides for:

- a. New altitude profiles of CO, N₂O, CH₄, H, OH, HO₂, N(²D), N(²P), and O(¹D).
- b. Revised altitude profiles of O₃, H₂O, N, N(⁴S), and NO.

The new Subroutine IONOSU provides for:

- a. Replacement of the E- and F-region generic molecular ion M⁺ by NO⁺, N₂⁺, and O₂⁺.
- b. A corresponding change in IONOU Common.

For simplicity of presentation, we have adopted a flexible definition of which species are major and which are minor. It is hoped that the meaning will always be clear to the reader in the context of the usage.

The overall inputs, some intermediate outputs, and final outputs for Model 1 are given in Table 1-1.

A flow diagram of the 16 subroutines, with their driver routine for development and test problems, is given in Figure 1-1. A brief, simplified description of the working of the 16 subroutines follows.

The Subroutine ATMOSU is initialized on a call to ATMOSU(1, 120.) to set up needed parameters and to evaluate the solar-flux-dependent Fourier coefficients used in computing the time-dependent values of τ (the variable controlling the temperature gradient at the lower boundary (120 km) of the high-altitude model) and T_{∞} (the exospheric temperature). In this call the values of the time (HL, hours), the 10.7-cm solar flux (SBAR), and the day-or-night parameter

Table 1-1. Inputs, intermediate outputs, and final outputs for major and minor neutral species and ionosphere for ambient conditions (ROSCOE Model 1).

INPUT

Initialization

Location (geographic colatitude and longitude)

Time (year, month, day, local zone time)

*Kinetic temperature profile (≤ 120 km) for latitude and season

*Moisture profile (mixing ratio, humidity, or dew-point temperature)

Operation

Altitude

SOME INTERMEDIATE OUTPUTS

Time: Universal time, Julian day number, local (apparent) time, index for day or night

Solar Properties: Solar zenith angle, solar flux at 10.7 cm

Minor Species: Fit parameters for density profiles

FINAL OUTPUTS

Neutral Species

N_2 , O_2 , O, Ar, He, CO_2 , $N(^4S)$, $N(^2D)$, $N(^2P)$, NO, NO_2 , N_2O , O_3 , $O_2(^1\Delta_g)$, $O(^1D)$, CO, CH_4 , H_2O , OH, HO_2 , H

Ionized Species (≥ 90 km)

e , O^+ , NO^+ , O_2^+ , N_2^+

Atmospheric Properties

Pressure, density, density scale height, (gas) temperature, and relative humidity

Ionospheric Properties

Electron (and N_2 vibration) temperature, effective ion-pair production rate

*Option for user specification.

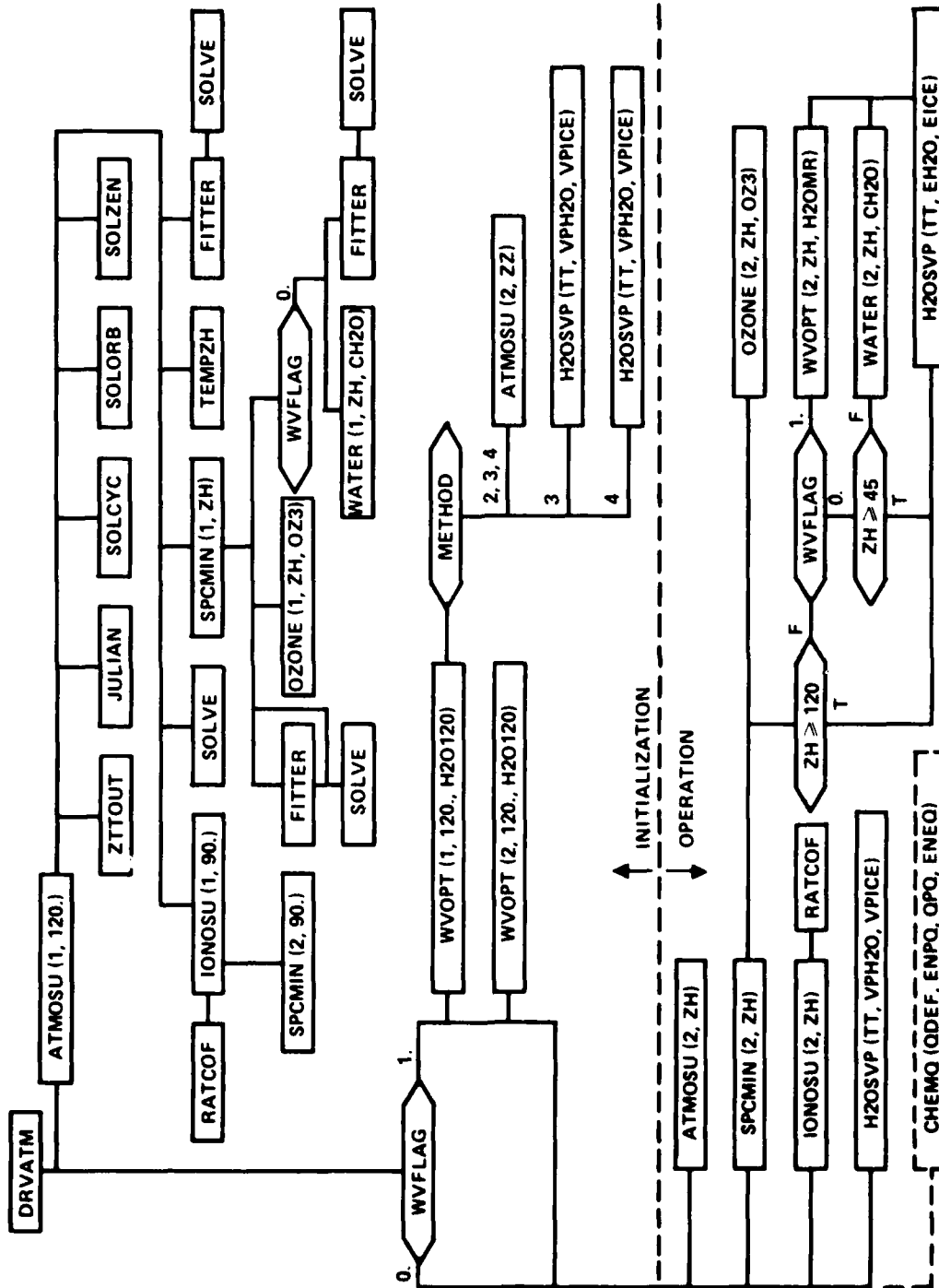


Figure 1-1. Flow diagram of Program DRVATM, Subroutines ATMOSU, SPCMIN, and IONOSU, and their auxiliary routines.

(IDORN) are determined by a series of calls from ATMOSU to five auxiliary subroutines (ZTTOUT, JULIAN, SOLCYC, SOLORB, and SOLZEN) and are passed to ATMOSU through ATMOUP Common.

The working of these five auxiliary routines is as follows:

- a. Subroutine ZTTOUT, receiving from TIME Common the input parameters year (IYRS), month (IMONS), day (IDAYS), and zone time (ZT) at east longitude PLON, returns to TIME Common the year, month, day, and mean or universal time (UT) at Greenwich.
- b. Subroutine JULIAN, called with the input parameters of year (IYRS), month (IMONS), and day (IDAYS) at north latitude PLAT, returns the Julian day number at the first of the year (YRFJ), the Julian date for vernal equinox (VEQJ), and the Julian day number on the day of interest (DAYJ) through the argument list and the fractional season-year (FYR) and the fractional summer (FST) through TIME Common.
- c. Subroutine SOLCYC, called with DAYJ, computes the average 10.7-cm solar flux (SBAR), an input to ATMOSU through ATMOUP Common.
- d. Subroutine SOLORB, called with YRFJ, VEQJ, and DAYJ and receiving UT from TIME Common, computes the Greenwich apparent time GAT, placed in TIME Common, and returns the north latitude (SOLLAT) and east longitude (SOLLON) of the subsolar point.
- e. Subroutine SOLZEN, called with SOLLAT and SOLLON and receiving PLAT, PLON, and GAT from TIME Common, returns to ATMOUP Common the solar zenith angle (CHI), the day-or-night parameter (IDORN), and the local apparent time (HL); the latter two parameters are used by ATMOSU.

The next step in the initialization of ATMOSU is to generate a fit function (with coefficient array AA) for the ratio g/T_M .

$$\frac{g}{T_M} \equiv \frac{G}{T} \frac{M}{M_*} \equiv \frac{g}{T(1+f_{\text{DAY}})} \equiv \frac{g}{T(1+f)}$$

This objective is achieved by:

- a. Developing a fit function (with coefficient array DD) by ATMOSU calling FITTER with the data-statement values of f specified in ATMOSU,

- b. Evaluating $g/[T(1+f)]$ in ATMOSU, after calling Subroutine TEMPZH to get a kinetic temperature profile, TZH(N). Subroutine TEMPZH, as directed by flag TPFLAG read by Program DRVATM and passed through ZHTEMP Common, will either (if TPFLAG = 0.0) interpolate the data base [US-66] for latitude and season or (if TPFLAG \neq 0.0) read a tabular temperature profile TZH(N) provided by the user.
- c. Calling Subroutine FITTER to obtain the coefficient-array AA.

After an initialization call from ATMOSU to SPCMIN(1,ZH), fit parameters are determined for O (nighttime only) and CO₂ and several other initializations are made; eventually, an initialization call is made to IONOSU(1,ZH). During the initialization of SPCMIN, 13 calls to FITTER and six (direct) calls to SOLVE are made to determine the fit coefficients for the day and night profiles of the minor species N, N(²D), NO, O₂(¹ Δ_g), CO, CH₄, O₃, NO₂, H₂O, H, OH, HO₂, O(¹D), and N₂O. SPCMIN also makes initializing calls to Subroutines OZONE and (if WVFLAG = 0.0) WATER. (If the user does not want the water profile provided by the code, his setting the flag WVFLAG \neq 0.0 will enable Subroutine WVOPT to read a user-provided water profile according to one of four methods specified by the flag METHOD = 1, 2, 3, 4.)

Subroutine FITTER, called from both ATMOSU and SPCMIN with values Y(I) of the dependent variable at NPTS values of the independent variable X(I), the degree NO of the polynomial used as the fitting function, an index IKIND denoting whether it is the dependent variable itself or its natural logarithm that is to be fitted, and an index ISIGN denoting negative or positive exponents in the polynomial, returns the polynomial coefficients determined by the method of least squares.

Subroutine SOLVE, called from Subroutines ATMOSU, SPCMIN, and FITTER with elements A(I,J) of a matrix of constant coefficients, returns the solutions of NO simultaneous linear algebraic equations.

The three major subroutines are ready for use after they have been initialized. On subsequent calls to ATMOSU(2,ZH), with ZH the altitude in kilometers, ATMOSU uses ATMOUP Common to return the pressure (PP), the mass density (RHO), the temperature (TT), the number densities of six species (SNI(I), I = 1,6), and the density scale height (HRHO).

On subsequent calls to SPCMIN(2,ZH), ATMOUP Common is used to return the number densities of 16 minor species (SNI(I), I = 7, 8, 13-24, 26, and 27) and the relative humidity (SNI(25)). On subsequent calls to IONOSU(2,ZH), ATMOUP Common is used to return the number densities of the five charged species (SNI(I), I = 9-11, 28, 29) and the electron (and N₂ vibration) temperature (SNI(12)) and IONOUP Common is used to return these same quantities (with different names) and the effective ion-production rate (QDEF).

Finally, another new routine for ROSCOE-IR, H2OSVP, is available to compute the saturated vapor pressure of water vapor over a plane surface of (1) water for the temperature range from 173.15 to 373.15°K (-100 to +100°C) and (2) ice for the temperature range from 173.15 to 273.15°K (-100 to 0°C). Values of zero are returned for the parameters outside the indicated temperature ranges and a message is printed if the routine is called outside the indicated range.

SECTION 2

AMBIENT ATMOSPHERE AND MAJOR NEUTRAL SPECIES

2-1 INTRODUCTION

The main subroutine for the ambient atmosphere and the major neutral species is ATMOSU. It is based on the Subroutine ATMOS originally developed by R.W. Lowen [Lo-73a] and later modified for ROSCOE-Radar [HS-75]. (The reader may refer to Lo-73a or, better, to HS-75 in which Lo-73a is reproduced with comments, revisions, and extensions.) For the manner in which ATMOSU is used in ROSCOE-IR, see Figure 2-1 for a simplified flow diagram and Table 2-1 for a summary of inputs and outputs.

2-2 THE AMBIENT ATMOSPHERE MODEL FOR ROSCOE-IR

2-2.1 Background

To understand the present model, it is useful to recall that used for ROSCOE-Radar. The ambient atmosphere model for ROSCOE-Radar [Vol. 14a] consisted of a low-altitude portion ($z < 120$ km) and a high-altitude portion ($z \geq 120$ km), appropriately joined at 120 km to provide a smooth transition. The overall model was based mainly on the CIRA-1965 [CI-65] model atmosphere, but was supplemented by use of the U.S. Standard-1962 model atmosphere since CIRA-1965 is not defined below 30-km altitude. The key to the low-altitude portion was an analytic specification of an altitude profile of the ratio g/T_M (where g is the acceleration due to gravity and T_M is the molecular-scale temperature) which permitted one to obtain the pressure (p) from an analytic integration of the hydrostatic equation [HS-75, p. 19, Equation (3)]. One then obtained the density (ρ) from the perfect gas law

$$\rho = \frac{M_*}{R} \frac{g}{T_M} \frac{p}{g} \quad (1)$$

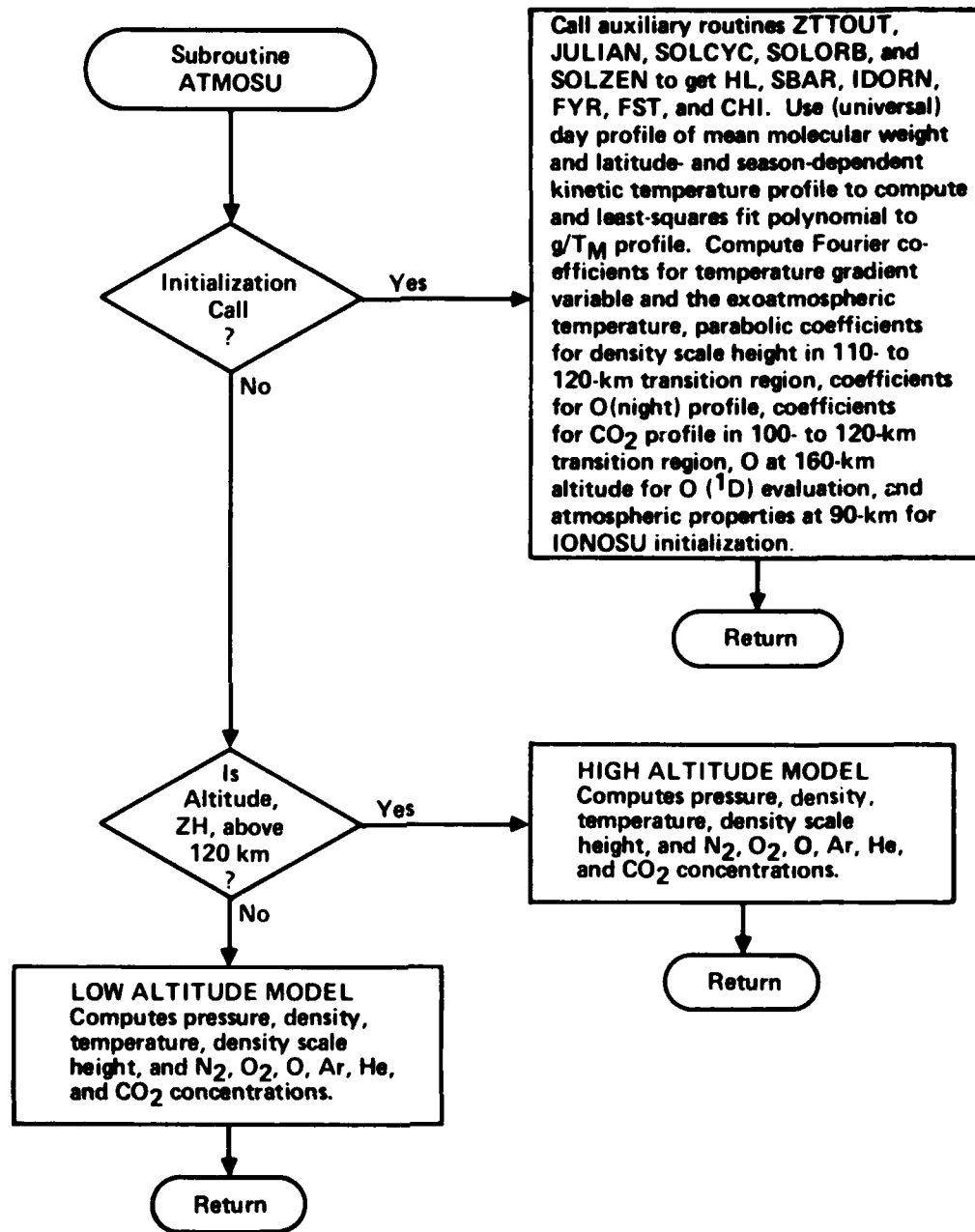


Figure 2-1. Flow diagram of Subroutine ATMOSU.

Table 2-1. Input and output variables for Subroutine
ATMOSU.

INPUT VARIABLES

Argument List

- JJ - Calculation flag
 If $\left\{ \begin{array}{l} \text{JJ} = 1: \text{ calculate initialization parameters} \\ \text{JJ} = 2: \text{ calculate atmospheric properties.} \end{array} \right.$
- ZH - Altitude of interest (km).

ALTODN Common

- ALTKM(47) - The array of altitudes at which minor species are specified as data in SPCMIN.
- ONITE(18) - The nighttime O-values specified as data in SPCMIN.
- CO2(25) - The CO₂-values specified as data in SPCMIN.

ATMOUP Common

- HL - Local time (hrs).
- SBAR - Average 10.7-cm solar flux [10^{-22} W/(m² Hz)].
- IDORN - Parameter for day or night. If COSCHI is the cosine of the zenith angle of the sun at point P, IDORN is 1 for daytime, i.e., IF(COSCHI.GE.0.0), and is -1 for nighttime, i.e., IF(COSCHI.LT.0.0).

TIME Common

- IYRS - Number of the year in the 1900's (e.g., 1974 becomes 74) at east longitude PLON.
- IMONS - Number of the month (e.g., February becomes 2) at east longitude PLON.
- IDAYS - Day of the month at east longitude PLON.
- ZT - Zone time for the 15-degree longitude interval containing PLON (decimal hours).
- PLAT - North latitude of point P (say, grid origin) (radians).
- PLON - East longitude of point P (say, grid origin).

(Continued)

Table 2-1. (Cont'd)

ZHTEMP Common

- NZHT - The number of altitudes in the ZHT array; set in SPCMIN to be 31
- TZH(31) - The kinetic temperatures at altitudes ZHT(31); provided by Subroutine TEMPZH
- ZHT(31) - The altitudes at which the kinetic temperatures are specified; set in Subroutine TEMPZH

OUTPUT VARIABLES

ALTODN Common

- S3ZOD - O density at 160-km altitude for use in evaluating $O(^1D)$ in SPCMIN

ATMOUP Common

- PP - Pressure (dynes/cm^2)
- RHO - Density (g/cm^3)
- TT - Temperature ($^{\circ}\text{K}$)
- SNI(1) - N_2 concentration ($1/\text{cm}^3$)
- SNI(2) - O_2 concentration ($1/\text{cm}^3$)
- SNI(3) - O concentration ($1/\text{cm}^3$)
- SNI(4) - Ar concentration ($1/\text{cm}^3$)
- SNI(5) - He concentration ($1/\text{cm}^3$)
- SNI(6) - CO_2 concentration ($1/\text{cm}^3$)
- HRHO - Density scale height (km)
- FEHSEQ - Fractional error in hydrostatic equilibrium

TIME Common

- RHO5KM - Mass density of dry air at 5-km altitude for use in Subroutine WATER
-

and the kinetic temperature (T) from

$$T = \frac{M}{M_*} \frac{T_M}{g} g \quad (2)$$

where M is the mean molecular weight and M_* is the value of M at sea level (28.96 g/mole). The mean molecular weight (M) was obtained from

$$\frac{M}{M_*} \equiv \frac{1}{1+f} \equiv \frac{1}{1 + M_*[O]/2L\rho} \quad (3)$$

where L is Avogadro's number, by specifying a (daytime) profile of the atomic oxygen density [O]. The species densities were obtained from the law of partial pressures and the assumption of perfect mixing. Since there was just one specification of g/T_M , the low-altitude portion of the atmosphere model was independent of latitude, season, and diurnal conditions. The high-altitude portion depended on both diurnal and solar-cycle conditions.

In planning for ROSCOE-IR, we recognized the need to account for the latitude and seasonal dependence of the atmospheric temperature below 120 km. The only data base with such information is the U.S. Standard Atmosphere Supplements-1966 [US-66]. Thus, in the ambient atmosphere model for ROSCOE-IR, we start with latitude- and season-dependent (kinetic) temperature profiles and we must ultimately obtain a latitude- and season-dependent profile of g/T_M , if we want to exploit the main structure of the atmosphere model for ROSCOE-Radar. However, there must be some other modifications. For example, $f \equiv f_{\text{Day}}$ will be prescribed and postulated not to have a latitude, season, or diurnal variation. This assumption implies:

- a. $(M/M_*)_{\text{Night}}$ will be approximated by $(M/M_*)_{\text{Day}}$, as in ROSCOE-Radar,
- b. $[O]_{\text{Day}}$ will be computed from

$$[O]_{\text{Day}} = 2 L\rho f/M_* \equiv 2 n_* f \quad (4)$$
- c. $[O]_{\text{Night}}$ will be computed directly from fit functions, as in ROSCOE-Radar.

2-2.2 Kinetic Temperature Data and Interpolation

2-2.2.1 Temperature Data

The temperature data, dependent on latitude and season but diurnally-independent, are from US-66, with locations as indicated in Table 2-2. The data are collated in Table 2-3 and plotted in Figures 2-2a through 2-2d.

Provision has been made for the user to read in his own preferred temperature profile at $z = 0(4)120$ km, accomplished by setting $TPFLAG \neq 0.0$ which enables Subroutine TEMPZH to read the desired data.

2-2.2.2 Interpolation in Latitude

The procedure for interpolating the data base is, first, to derive summer and winter tabular temperature profiles at the latitude of interest, according to the following rules:

| <u>LATBND</u> | <u>Use</u> |
|---------------|--|
| 1 | The single temperature profile for 15° latitude for both winter and summer. |
| 2,3,4,5 | The winter and summer profiles at the two boundaries of the latitude band and interpolate linearly on latitude to obtain the new winter and summer profiles. |
| 6 | The winter and summer temperature profiles for 75° latitude. |

2-2.2.3 Interpolation in Season

If $LATBND > 1$, determine the temperature profile for the calendar date of interest by linearly interpolating between January and July temperature profiles, with proper account of northern and southern hemispheres. To do this, we:

- (1) Determine a parameter F_{ST} where

F_{ST} = fraction of summer temperature to be used in the linear combination of summer- and winter-temperature profiles
= fraction of July temperature in northern latitudes.
= fraction of January temperature in southern latitudes.

F_{ST} is evaluated in Subroutine JULIAN.

Table 2-2. Location of temperature data.

| LATBND | Latitude Range | Location in US-66 for Temperature Profile at Boundary of Band |
|--------|------------------------|--|
| 1 | $0 \leq \phi < 15$ | 15°N Annual [0(4)116 km] ^a pp. 99,101 |
| 2 | $15 \leq \phi < 30$ | 15°N Annual [0(4)116 km] ^a pp. 99,101 |
| 3 | $30 \leq \phi < 45$ | 30°N {January [0(4)116 km] ^a pp. 103,105 July [0(4)116 km] ^a pp. 107,109} |
| 4 | $45 \leq \phi < 60$ | 45°N {January [0(4)116 km] ^a pp. 111,113 July [0(4)116 km] ^a pp. 115,117} |
| 5 | $60 \leq \phi < 75$ | 60°N {January [0(4)116 km] ^a pp. 123,125 July [0(4)116 km] ^a pp. 135,137} |
| 6 | $75 \leq \phi \leq 90$ | {75°N January [0(4)28 km] ^b p. 139 |
| | | {60°N January [32(4)116 km] ^a p. 125 |
| | | {75°N July [0(4)28 km] p. 145 |
| | | {60°N July [32(4)116 km] ^{a, c} p. 137 |
| | | {Same as 75 boundary} |

^a 120-km value obtained by extrapolation.

^b 0-km value changed from 249.22 to 254.0°K.
28-km value changed from 207.65 to 212.5°K.

^c 32-km value changed from 238.47 to 241.0°K.

Table 2-3. Kinetic temperature profile data from US-66.

| z km | 15°N | | 30°N | | 45°N | | 60°N | | ≈75°N | |
|---------|--------|--------|---------|--------|---------|--------|---------|--------|---------|--------|
| | Annual | July | January | July | January | July | January | July | January | July |
| 0. | 302.59 | 304.58 | 288.52 | 296.22 | 272.59 | 296.22 | 257.28 | 288.45 | 254.0 | 278.92 |
| 4. | 277.44 | 277.87 | 268.44 | 273.57 | 255.79 | 273.57 | 247.81 | 265.87 | 239.89 | 262.09 |
| 8. | 250.37 | 252.41 | 242.32 | 248.28 | 231.72 | 248.28 | 220.55 | 239.18 | 217.86 | 235.87 |
| 12. | 223.64 | 224.42 | 216.40 | 222.30 | 218.66 | 222.30 | 217.15 | 225.15 | 213.25 | 228.65 |
| 16. | 197.02 | 203.15 | 205.91 | 215.65 | 216.67 | 215.65 | 216.56 | 225.15 | 210.05 | 230.15 |
| 20. | 206.71 | 211.75 | 207.92 | 219.17 | 215.15 | 219.17 | 214.17 | 225.15 | 207.65 | 230.15 |
| 24. | 219.23 | 219.90 | 216.90 | 223.94 | 215.15 | 223.94 | 211.79 | 226.56 | 207.65 | 230.71 |
| 28. | 227.94 | 227.83 | 224.83 | 229.49 | 215.85 | 229.49 | 214.06 | 232.52 | 212.5 | 235.48 |
| 32. | 236.63 | 235.74 | 232.74 | 237.81 | 219.02 | 237.81 | 218.03 | 238.47 | 218.03 | 241.0 |
| 36. | 245.32 | 245.14 | 242.14 | 247.64 | 230.92 | 247.64 | 224.76 | 250.18 | 224.76 | 250.18 |
| 40. | 253.99 | 254.62 | 251.62 | 257.52 | 243.17 | 257.52 | 234.65 | 262.05 | 234.65 | 262.05 |
| 44. | 262.66 | 264.08 | 261.08 | 267.39 | 255.41 | 267.39 | 244.53 | 272.48 | 244.53 | 272.48 |
| 48. | 270.15 | 272.15 | 269.15 | 275.65 | 265.65 | 275.65 | 254.40 | 276.82 | 254.40 | 276.82 |
| 52. | 269.24 | 271.14 | 268.14 | 275.65 | 265.65 | 275.65 | 260.15 | 277.15 | 260.15 | 277.15 |
| 56. | 261.39 | 263.28 | 260.28 | 266.87 | 258.63 | 266.87 | 257.30 | 271.99 | 257.30 | 271.99 |
| 60. | 253.10 | 254.79 | 252.04 | 257.05 | 250.77 | 257.05 | 250.89 | 262.73 | 250.89 | 262.73 |
| 64. | 239.40 | 239.91 | 239.90 | 244.52 | 242.93 | 244.52 | 248.93 | 244.26 | 248.93 | 244.26 |
| 68. | 225.72 | 225.04 | 227.77 | 226.89 | 234.76 | 226.89 | 246.97 | 225.83 | 246.97 | 225.83 |
| 72. | 212.06 | 210.19 | 215.66 | 209.28 | 226.54 | 209.28 | 241.12 | 207.41 | 241.12 | 207.41 |
| 76. | 198.41 | 195.36 | 203.56 | 191.69 | 218.34 | 191.69 | 232.51 | 189.01 | 232.51 | 189.01 |
| 80. | 184.78 | 180.54 | 191.47 | 174.12 | 210.14 | 174.12 | 223.91 | 170.64 | 223.91 | 170.64 |
| 84. | 177.10 | 172.50 | 191.10 | 165.10 | 201.89 | 165.10 | 215.27 | 161.71 | 215.27 | 161.71 |
| 88. | 177.05 | 172.45 | 191.04 | 165.06 | 199.54 | 165.06 | 206.63 | 161.66 | 206.63 | 161.66 |
| 92. | 179.50 | 175.71 | 199.56 | 169.98 | 201.02 | 169.98 | 205.55 | 167.51 | 205.55 | 167.51 |
| 96. | 185.77 | 183.55 | 211.72 | 180.96 | 210.50 | 180.96 | 212.70 | 179.67 | 212.70 | 179.67 |
| 100. | 190.70 | 190.03 | 222.43 | 190.51 | 218.58 | 190.51 | 218.49 | 190.39 | 218.49 | 190.39 |
| 104. | 205.98 | 209.16 | 237.88 | 214.04 | 232.65 | 214.04 | 230.24 | 217.12 | 230.24 | 217.12 |
| 108. | 229.78 | 237.66 | 256.88 | 246.42 | 250.58 | 246.42 | 245.33 | 252.57 | 245.33 | 252.57 |
| 112. | 253.25 | 265.72 | 275.76 | 278.60 | 268.65 | 278.60 | 261.48 | 288.06 | 261.48 | 288.06 |
| 116. | 315.82 | 322.72 | 304.46 | 329.46 | 301.06 | 329.46 | 297.50 | 334.14 | 297.50 | 334.14 |
| 120. | 379.70 | 379.70 | 333.30 | 379.70 | 333.30 | 379.70 | 333.30 | 379.70 | 333.30 | 379.70 |

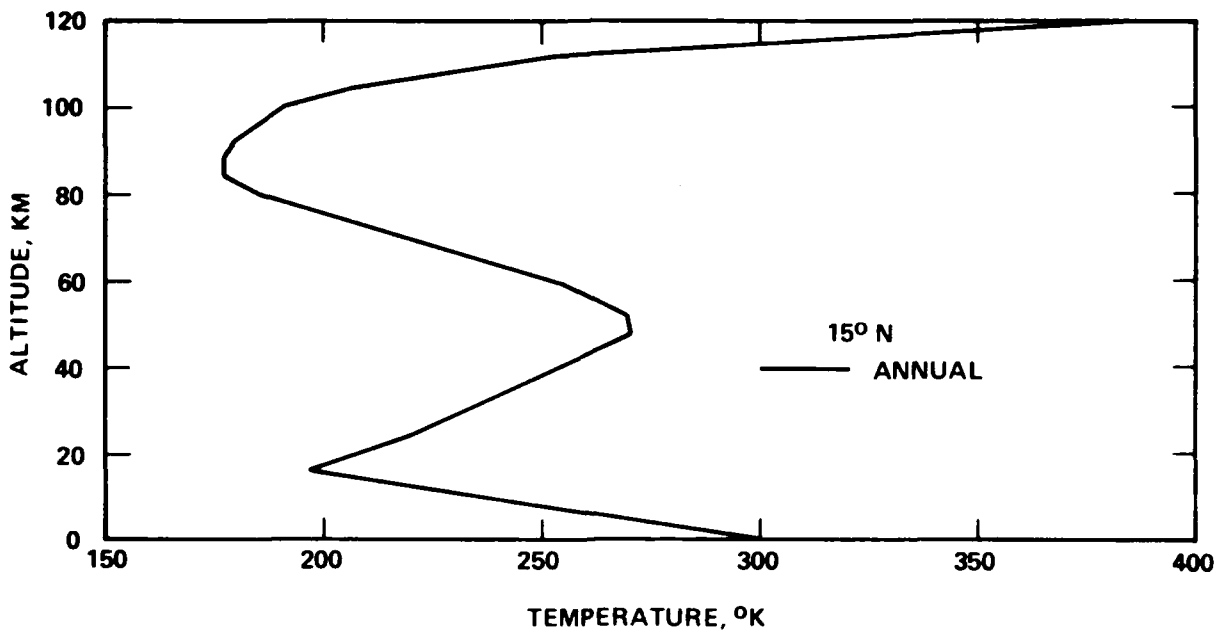


Figure 2-2a. Adopted data for temperature profile at 15°N latitude.

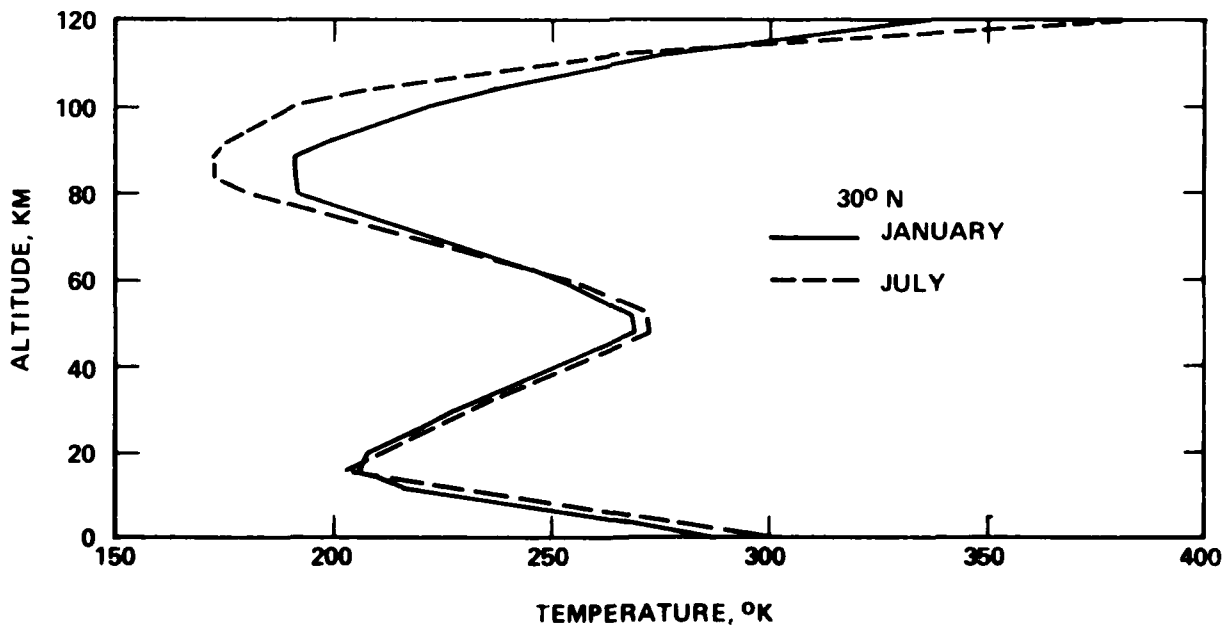


Figure 2-2b. Adopted data for temperature profile at 30°N latitude.

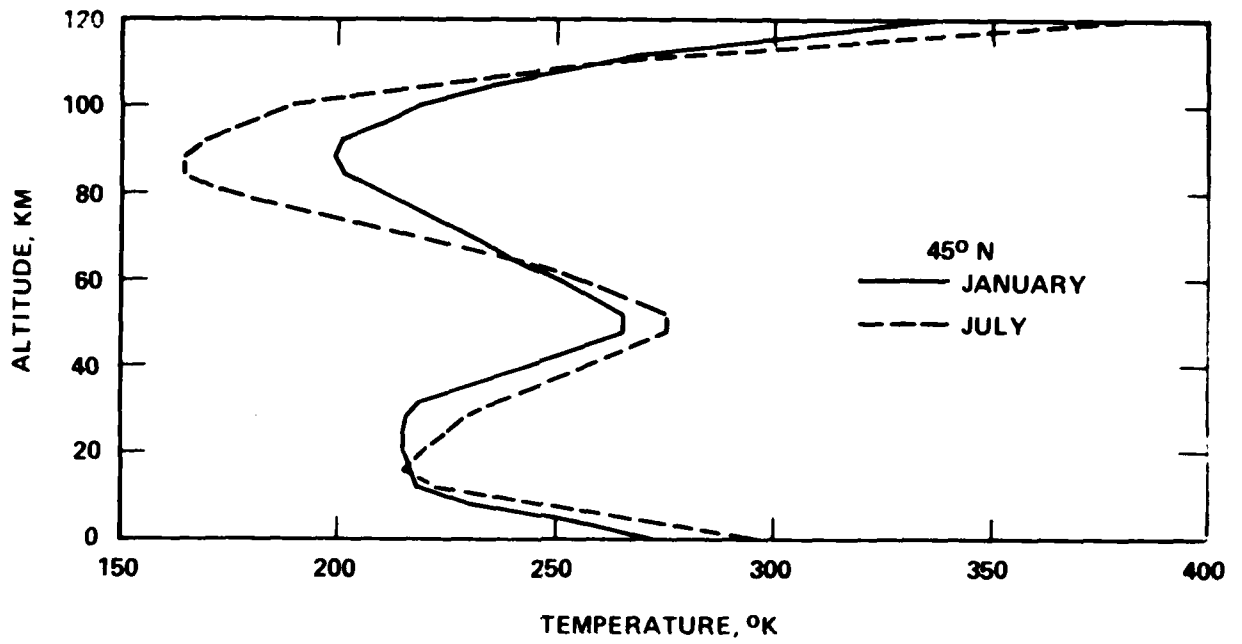


Figure 2-2c. Adopted data for temperature profile at 45°N latitude.

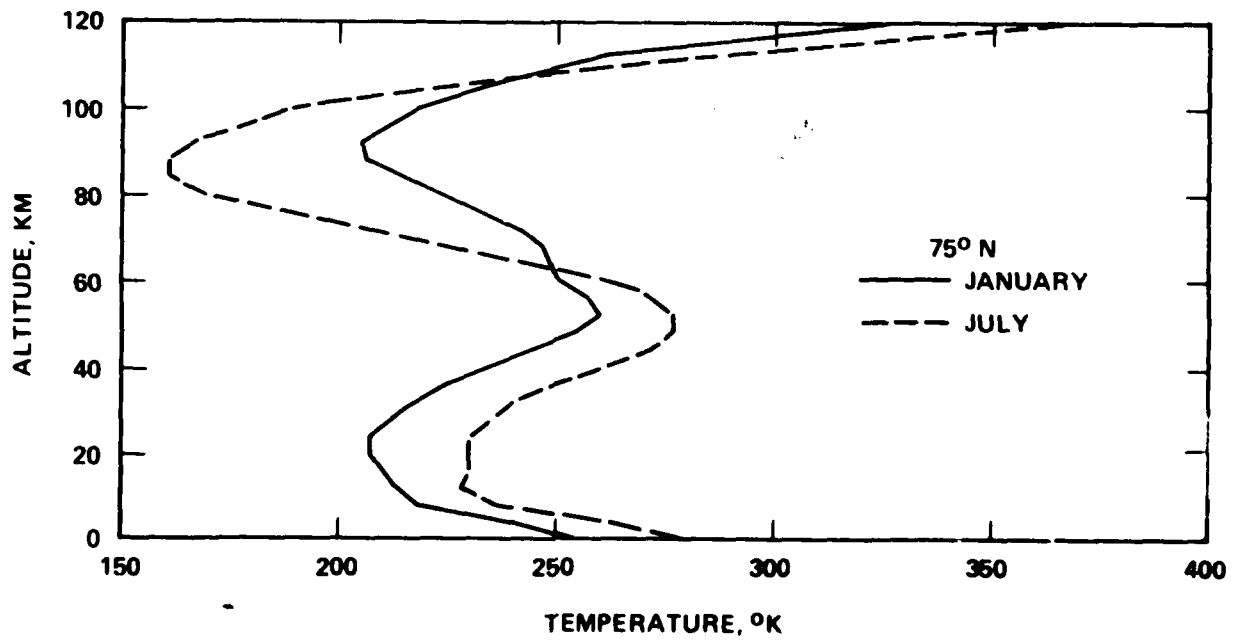


Figure 2-2d. Adopted data for temperature profile at 75°N latitude.

(2) Compute the temperature at given altitude from

$$T = F_{ST} T_{\text{summer}} + (1 - F_{ST}) T_{\text{winter}} \quad (5)$$

A test of our adopted procedure for linear seasonal interpolation is made for the 45°N latitude data where we have compared the average of the January and July values with the spring/fall value given by US-66. See Table 2-4 and Figure 2-3.

Table 2-4. Comparison of the mean of the January and July temperature profiles from US-66 with the mid-latitude spring/fall temperature profile from US-66.

| z, km | 45°N Mean ^a | Midlat. Spring/Fall ^b | z, km | 45°N Mean ^a | Midlat. Spring/Fall ^b | z, km | 45°N Mean ^a | Midlat. Spring/Fall ^b |
|-------|------------------------|----------------------------------|-------|------------------------|----------------------------------|-------|------------------------|----------------------------------|
| 0 | 284.40 | 288.15 | 44 | 261.40 | 261.40 | 88 | 182.30 | 190.54 |
| 4 | 264.68 | 262.17 | 48 | 270.65 | 270.65 | 92 | 185.50 | 191.44 |
| 8 | 240.00 | 236.22 | 52 | 270.65 | 270.65 | 96 | 195.73 | 197.77 |
| 12 | 220.48 | 216.65 | 56 | 262.75 | 263.63 | 100 | 204.54 | 202.73 |
| 16 | 216.16 | 216.65 | 60 | 253.91 | 255.77 | 104 | 223.34 | 213.02 |
| 20 | 217.16 | 216.65 | 64 | 243.72 | 243.20 | 108 | 248.50 | 226.75 |
| 24 | 219.54 | 220.56 | 68 | 230.82 | 227.53 | 112 | 273.62 | 241.09 |
| 28 | 222.67 | 224.53 | 72 | 217.91 | 214.07 | 116 | 315.26 | 298.43 |
| 32 | 228.42 | 228.49 | 76 | 205.01 | 202.34 | 120 | 356.50 | 355.19 |
| 36 | 239.28 | 239.28 | 80 | 192.13 | 190.65 | | | |
| 40 | 250.34 | 250.35 | 84 | 183.49 | 190.60 | | | |

^aAverage of January and July values.

^bUS-66, pp. 119,121.

2-2.3 Mean Molecular-Weight Profile

The mean molecular-weight profile, M , is specified by the function

$$f = \frac{M_*}{M} - 1 \quad (6a)$$

$$= \frac{M_*[O]_{\text{Day}}}{2L_0} \quad (6b)$$

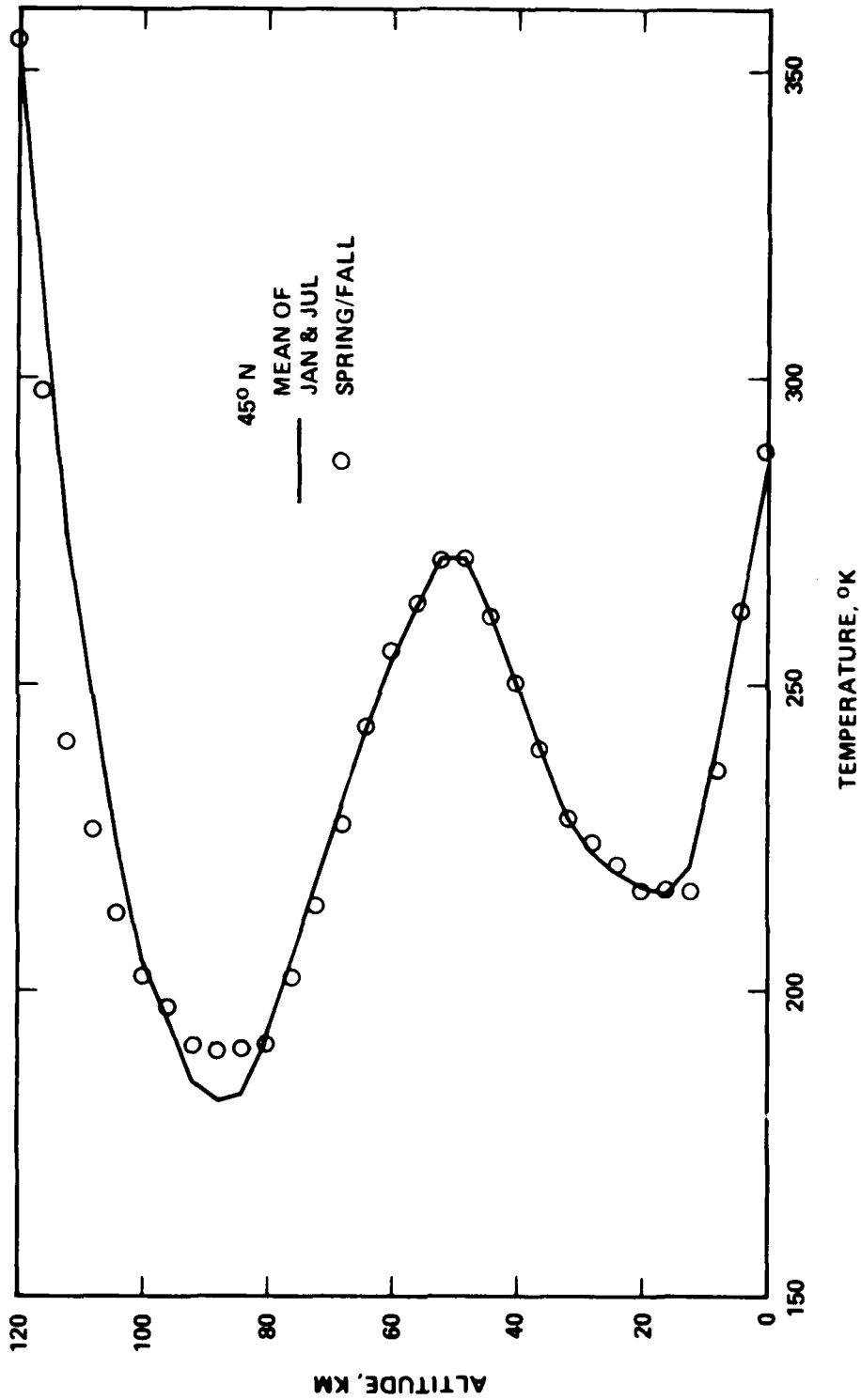


Figure 2-3. Comparison of the mean of the January and July temperature profiles from US-66 with the midlatitude spring/fall temperature profile from US-66.

taken to be independent of latitude, season, and diurnal variation. The adopted profile, given in Table 2-5 and plotted in Figure 2-4, is obtained as follows:

1. For $z = 0(4)92$ km,
 - a. Take $[O]_{\text{Day}}$ from data base for ROSCOE-Radar (set as data statement in Subroutine SPCMIN [HS-75]).
 - b. Take air density, ρ , from US-66 (pp. 119,121, Table 5.1, 45° latitude, spring/fall).
 - c. Compute f from Equation (6b).
2. For $z = 96(4)120$ km,
 - a. Take M from US-66 (p. 16, Table 2.3, spring/fall).
 - b. Compute f from Equation (6a).

2-2.4 Molecular-Scale Temperature

For the interpolated temperature profile of interest, T , and the value of $M_*/M \equiv 1 + f$ derived from the fit function for f , the molecular-scale temperature is computed from

$$\begin{aligned} T_M &= (M_*/M)T \\ &= (1 + f)T, \quad z = 0(4)120 \text{ km} \end{aligned} \quad (7)$$

2-2.5 The Ratio g/T_M

Tabular values of the ratio

$$g/T_M, \quad z = 0(4)120 \text{ km} \quad (8)$$

are computed, followed by fitting the tabular data by the 11th-degree polynomial

$$\frac{g}{T_M} = \sum_{k=0}^{11} g_k z^k, \quad 0 \leq z \leq 120 \text{ km} \quad (9)$$

Table 2-5. Molecular weight function adopted for Subroutine ATMOSU in ROSCOE-IR.

| z, km | f | z, km | f | z, km | f | z, km | f |
|-------|-----------|-------|-----------|-------|----------|-------|----------|
| 0 | 1.14(-17) | 32 | 1.59(-10) | 64 | 3.83(-6) | 96 | 1.05(-2) |
| 4 | 1.47(-16) | 36 | 1.12(-9) | 68 | 6.33(-6) | 100 | 2.40(-2) |
| 8 | 5.95(-16) | 40 | 5.90(-9) | 72 | 1.19(-5) | 104 | 3.65(-2) |
| 12 | 3.86(-15) | 44 | 2.61(-8) | 76 | 3.20(-5) | 108 | 4.78(-2) |
| 16 | 3.47(-14) | 48 | 9.14(-8) | 80 | 8.62(-5) | 112 | 5.85(-2) |
| 20 | 2.71(-13) | 52 | 2.76(-7) | 84 | 2.44(-4) | 116 | 6.82(-2) |
| 24 | 2.56(-12) | 56 | 7.24(-7) | 88 | 7.11(-4) | 120 | 7.66(-2) |
| 28 | 2.15(-11) | 60 | 1.88(-6) | 92 | 2.38(-3) | | |

2-2.6 Computation of the Major-Species Quantities

Having obtained an analytic fit function for g/T_M , one can compute the quantities for the major species almost as they are computed in HS-75, with the following exceptions:

- Pressure will be computed from Equation (3) on p. 19 of HS-75 and not by use of the pressure-correction factor on p. 21 of HS-75.
- $[O]_{\text{Day}}$, computed in HS-75 and currently from

$$[O]_{\text{Day}} = 2n_* \left(\frac{M_*}{M} - 1 \right) \equiv 2n_* f_{\text{Day}} \equiv 2n_* f \quad (10)$$

will now be latitude- and season-dependent because n_* (the total number density if no dissociation) is latitude- and season-dependent. This situation differs from that in HS-75, where $[O]_{\text{Day}}$ was input and used to help determine f .

- $[O]_{\text{Night}}$, as in HS-75, is set equal to $[O]_{\text{Day}}$ for $90 \leq z \leq 120$ km and is computed from a fit function for $z < 90$ km (see Table 4-2).

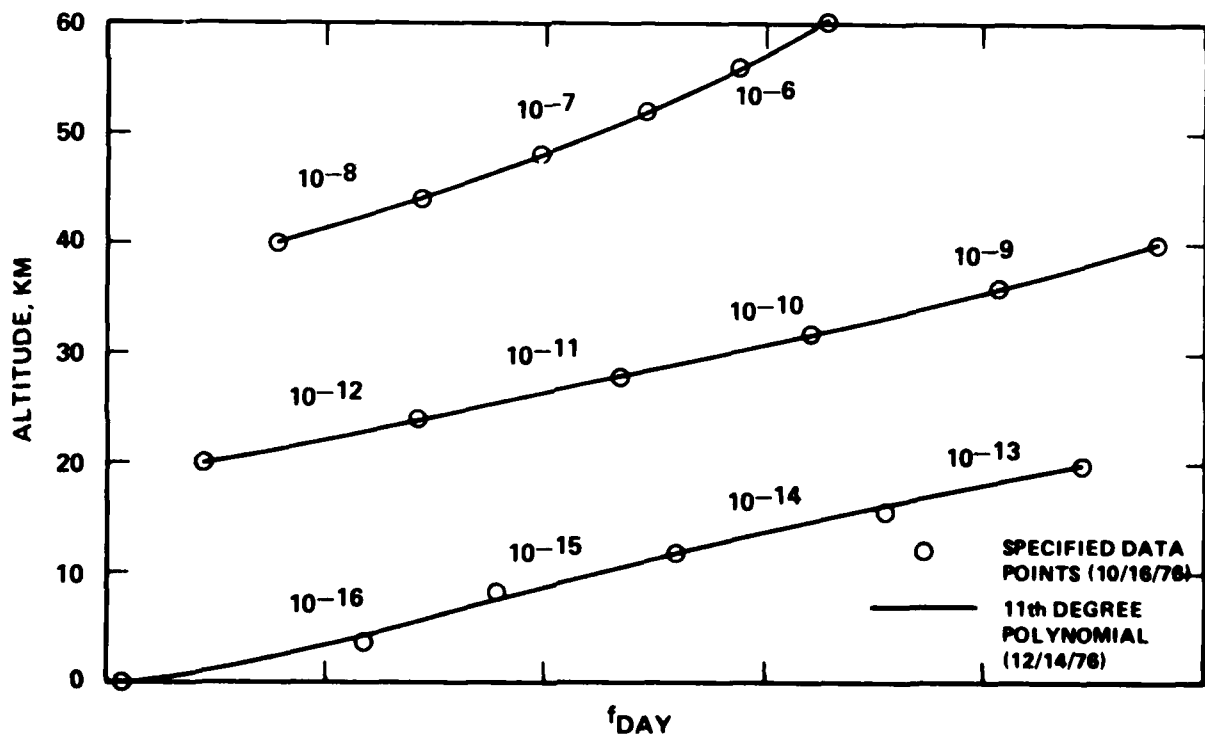
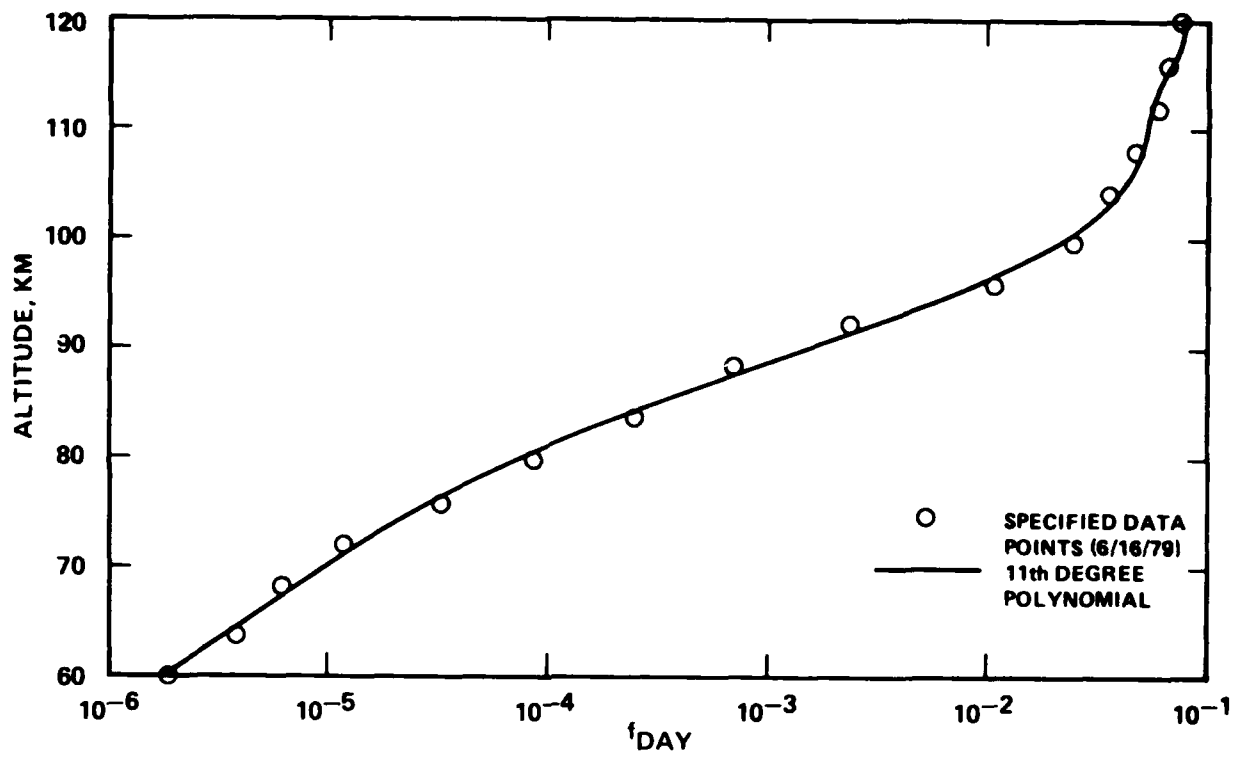


Figure 2-4. Adopted molecular-weight-function profile and fit function.

SECTION 3

AUXILIARY SUBROUTINES FOR ATMOSU AND SPCMIN

3-1 INTRODUCTION

The purpose of the five auxiliary subroutines ZTTOUT, JULIAN, SOLCYC, SOLORB, and SOLZEN is to convert inputs that are convenient for the user to the inputs required by ATMOSU, SPCMIN, and IONOSU. It is assumed the user will locate his coordinate system in space and time by stating the geographic north latitude and east longitude, the date, and zone time (based on 15-degree intervals of longitude) in a 24-hour system. These auxiliary routines determine the universal time, Julian day number, local (apparent) time, the solar zenith angle viewed from the origin, an index denoting day or night, and the 10.7-cm solar flux.

These subroutines (except ZTTOUT) had their origin in the AFWL WORRY code (where they were known as JULIAN, SOLCY, ORB, and ZSOL) and were revised when they were incorporated into the early-version ROSCOE code [LL-75]. These routines, to which ZTTOUT was added, were further revised and laden with comment cards under the contractual effort for the ROSCOE-Radar code [HS-75]. For ROSCOE-IR, most of these subroutines underwent only minor changes.

Subroutine TEMPZH, a new routine for ROSCOE-IR, determines the temperature profile used in Subroutine ATMOSU, from either a stored data base or one supplied by the user via card input.

Subroutines FITTER and SOLVE are used in providing least-squares polynomial fit functions.

3-2 SUBROUTINE ZTTOUT

Subroutine ZTTOUT converts a Gregorian calendar date (specified by stating the year in the 20th century (IYRS), the month (IMONS), and the day (IDAYS)) and zone time (ZT) at a given east longitude (PLON) to the Gregorian calendar date and mean (or universal) time (UT) at Greenwich.

For ROSCOE-IR we have corrected the computation of the zone description (ZD) when ZD should be zero and revised TIME Common.

See Table 3-1 for a summary of inputs and outputs for Subroutine ZTTOUT.

3-3 SUBROUTINE JULIAN

Subroutine JULIAN converts a Gregorian calendar date (specified by stating the year in the 20th century (IYRS), the month (IMONS), and the day (IDAYS)) to Julian day number (DAYJ) for use by Subroutine SOLORB.

In going from ROSCOE-Radar to ROSCOE-IR, we deleted the variables KYRS, KMONS, and KDAY from the argument list since these variables are now supplied through TIME Common where they are known as IYRS, IMONS, and IDAYS.

The new Subroutine JULIAN also computes, taking account of season reversal in the southern hemisphere, (1) the variable FYR, the fractional season-year, needed for the new water vapor and ozone models and (2) the variable FST, the fractional summer, needed for the seasonal interpolation between the summer and winter temperature profiles which are input as data for the revised low-altitude major-species model.

See Table 3-2 for a summary of inputs and outputs for Subroutine JULIAN.

3-4 SUBROUTINE SOLCYC

Subroutine SOLCYC computes the 10.7-cm solar flux (SBAR), an input to ATMOSU through ATMOUP Common, based on an assumed sinusoidal 11-year (or 4018-day) variation. The maximum value of 250 for SBAR, associated with Model 9 of the CIRA-65 atmosphere, has been assigned the date of 1 June 1958. The minimum value of 65 for SBAR is associated with Model 1 of the CIRA-65 atmosphere.

See Table 3-3 for a summary of inputs and outputs for Subroutine SOLCYC.

Table 3-1. Input and output variables for Subroutine ZTTOUT.

INPUT VARIABLES

Argument List

None

TIME Common

- IYRS - Number of the year in the 1900's (e.g., 1974 becomes 74) at east longitude PLON
- IMONS - Number of the month (e.g., February becomes 2) at east longitude PLON
- IDAYS - Day of the month at east longitude PLON
- ZT* - Zone time for the 15-degree longitude interval containing PLON (decimal hours)
- PLON - East longitude of point P (radians)

OUTPUT VARIABLES

Argument List

None

TIME Common

- IYRS - A possibly revised value of the input parameter, corresponding to Greenwich
- IMONS - A possibly revised value of the input parameter, corresponding to Greenwich
- IDAYS - A possibly revised value of the input parameter, corresponding to Greenwich
- UT - Universal time corresponding to the zone time ZT (decimal hours)

* A value of 24.0, treated by the code as illegal, should be input as 0.0 on the next day.

Table 3-2. Input and output variables for Subroutine JULIAN.

INPUT VARIABLES

Argument List

None

TIME Common

- IYRS - Number of the year in the 1900's (e.g., 1974 becomes 74) in the Greenwich time zone)
- IMONS - Number of the month (e.g., February becomes 2) in the Greenwich time zone
- IDAYS - Day of the month in the Greenwich time zone
- PLAT - North latitude of point P (radians)

OUTPUT VARIABLES

Argument List

- YRFJ - Julian day number (a half integer) at 0 hours UT on January 1 of the year of interest
- VEQJ - Julian date for vernal equinox
- DAYJ - Julian day number (a half integer) at 0 hours UT on the day of interest

TIME Common

- FYR - Fractional season-year, being zero on 1 January in the northern hemisphere and zero on 1 July in the southern hemisphere
 - FST - Fractional summer, being one on 1 July and zero on 1 January in the northern hemisphere and reversed in the southern hemisphere
-

Table 3-3. Input and output variables for Subroutine SOLCYC.

INPUT VARIABLES

Argument List

DAYJ - Julian day number (a half integer) at 0 hours UT on the day of interest

Common

None

OUTPUT VARIABLES

Argument List

None

ATMOUP Common

SBAR - Average 10.7-cm solar flux
[1.0E-22 W/(m² Hz)]

3-5 SUBROUTINE SOLORB

Subroutine SOLORB computes the north latitude (SOLLAT) and east longitude (SOLLON) of the apparent (actual motion) subsolar point, given the Julian day number at 0-hours UT on 1 January of the year of interest (YRFJ), the Julian date at which vernal equinox occurs (VEQJ), the Julian day number at 0-hours on the day of interest (DAYJ), and the universal time (UT).

In going from ROSCOE-Radar to ROSCOE-IR, we have defined a new variable (DELJUT) to avoid loss of significance in computing SOLLON on a small-word machine and revised the argument in the equation-of-time, consistent with its definition.

See Table 3-4 for a summary of inputs and outputs for Subroutine SOLORB.

Table 3-4. Input and output variables for Subroutine SOLORB.

INPUT VARIABLES

Argument List

- YRJF - Julian day number (a half integer) at 0 hours UT on January 1 of the year of interest
- VEQJ - Julian date for vernal equinox
- DAYJ - Julian day number (a half integer) at 0 hours UT on the day of interest

TIME Common

- UT - Universal time corresponding to zone time ZT (decimal hours)

OUTPUT VARIABLES

Argument List

- SOLLAT - North latitude of subsolar point (radians)
- SOLLON - East longitude of subsolar point (radians)

TIME Common

- GAT - Greenwich apparent time (decimal hours)
-

3-6 SUBROUTINE SOLZEN

Subroutine SOLZEN computes CHI and COSCHI, the cosine of the solar zenith angle CHI at a point P, given the geographic north latitude (PLAT) and east longitude (PLON) of the point P and the north latitude (SOLLAT) and east longitude (SOLLON) of the subsolar point. The day-or-night parameter IDORN is +1 for daytime, i.e., if $\text{COSCHI} \geq 0.0$, and is -1 for nighttime. The local apparent time (HL) is also computed from the Greenwich apparent time (GAT) and the east longitude of the point P (PLON).

See Table 3-5 for a summary of inputs and outputs for Subroutine SOLZEN.

Table 3-5. Input and output variables for Subroutine SOLZEN.

INPUT VARIABLES

Argument List

SOLLAT - North latitude of subsolar point (radians)

SOLLON - East longitude of subsolar point (radians)

TIME Common

PLAT - North latitude of point P (say, grid origin) (radians)

PLON - East longitude of point P (radians)

OUTPUT VARIABLES

Argument List

None

ATMOUP Common

IDORN - Parameter for day or night. If COSCHI is the cosine of the zenith angle of the sun at point P, IDORN is 1 for daytime, i.e., $\text{IF}(\text{COSCHI} \geq 0.0)$, and is -1 for nighttime, i.e., $\text{IF}(\text{COSCHI} < 0.0)$

HL - Local apparent time (decimal hours, e.g., 2230 hours becomes 22.50 hours)

TIME Common

CHI - Zenith angle of the sun at point P (radians)

3-7 SUBROUTINE TEMPZH

Subroutine TEMPZH determines the temperature profile (tabular, 0(4)120 km) by interpolating the data base [US-66] for latitude and season, to be used as input to the major atmospheric species model for the low-altitude range from 0- to 120-km altitude. The user may bypass the code's specification of temperature profile in the low-altitude (0- to 120-km) region by (1) requiring the driving program to set TPFLAG to a nonzero value, which is transferred to Subroutine TEMPZH through ZHTEMP Common, and (2) allowing Subroutine TEMPZH to read the user-specified profile at altitudes 0.0(4.0)120.0 km.

See Table 3-6 for a summary of inputs and outputs for Subroutine TEMPZH.

3-8 SUBROUTINE FITTER

A brief description of the operation of Subroutine FITTER is given in Section 1. A summary of inputs and outputs for Subroutine FITTER is given in Table 3-7.

3-9 SUBROUTINE SOLVE

A brief description of the operation of Subroutine SOLVE is given in Section 1. A summary of inputs and outputs for Subroutine SOLVE is given in Table 3-8.

Table 3-6. Input and output variables for Subroutine TEMPZH.

INPUT VARIABLES

Argument List

None

TIME Common

- PLAT - North latitude of point P (radians)
FST - Fraction of summer temperature profile to be used with (1.-FST) of the winter temperature profile for a given day of the year at a given latitude

ZHTEMP Common

- TPFLAG - Flag for optional treatment of temperature profile
= 0.0 normal treatment
≠ 0.0 optional treatment, allowing Subroutine TEMPZH to read the user-specified profile at altitudes $z = 0(4)120$ km

Card Input (optional)

- TZH(I), - Temperature profile specified by user at
I=1,31 altitudes $z = 0(4)120$ km

OUTPUT VARIABLES

Argument List

None

ZHTEMP Common

- TZH(I), - Temperature profile, determined by interpolation of the data base [US-66] for latitude and season, used as input to the major atmospheric species model for the low-altitude range from 0- to 120-km altitude
I=1,31
-

Table 3-7. Input and output variables for Subroutine FITTER.

INPUT VARIABLES

Argument List

- NPTS - Number of data points
- X(I) - Values of the independent variable, e.g., altitude (km)
- Y(I) - Values of the dependent variable, e.g., species concentration (cm⁻³)
- NO - Degree of polynomial to be fitted
- IKIND - Index for kind of equation to be fitted

= 1 if equation is $\ln(Y) = \sum_{n=0}^{NO} A_n X^n$

= 2 if equation is $Y = \sum_{n=0}^{NO} A_n X^n$

- ISIGN - Index for sign of exponents
- = 1 for negative exponents
- = 2 for positive exponents

Common

None

OUTPUT VARIABLES

Argument List

- Z(J) - The least-squares fit coefficients. Z(1) corresponds to A₀, Z(2) to A₁, etc.

Common

None

Table 3-8. Input and output variables for Subroutine SOLVE.

INPUT VARIABLES

Argument List

- A(I,J) - Element (I,J) of matrix of constant coefficients for NO simultaneous linear algebraic equations
- NO - The number of equations

Common

None

OUTPUT VARIABLES

Argument List

- X(K) - The least-squares fit coefficients. These are the same as the output Z(K) from FITTER.
-

SECTION 4
MINOR NEUTRAL SPECIES

4-1 SUBROUTINE SPCMIN

ROSCOE-IR requires many more neutral species than ROSCOE-Radar and an improved description of some of those included in ROSCOE-Radar.

The ROSCOE-IR high-altitude chemistry module [Volume 11-1] requires the minor neutral species O, CO₂, CO, N(⁴S), N(²D), N(²P), NO, NO₂, O₂(¹Δ_g), O₃, H, OH, HO₂, H₂O, and He (in practice, however, CO₂, CO, H₂O, and He are nonreacting species). The ROSCOE-IR low-altitude external chemistry module [Volume 11-1] requires the minor neutral species O, CO₂, N(⁴S), N(²D), NO, NO₂, O₂(¹Δ_g), O₃, H, OH, HO₂, and H₂O. (The additional species CO, CH₄, and N₂O were initially requested but they are not used.) All-altitude profiles for diurnal conditions are provided for O, CO₂, and He in Subroutine ATMOSU. Subroutine SPCMIN provides (either directly or indirectly) the profiles for the remaining species listed above.

The inputs and outputs for Subroutine SPCMIN are summarized in Table 4-1. The nature of the functions used for fitting the adopted data-base values [Volumes 14b and 14c] in various altitude ranges is given in Tables 4-2 through 4-18 for O, O(¹D), O₂(¹Δ_g), O₃, N, N(²D), N(²P), NO, NO₂, N₂O, CO₂, CO, CH₄, H₂O, OH, HO₂, and H, respectively.

4-2 OZONE

Our model for altitude profiles of the O₃ mass-mixing ratio has been specified as a function of latitude and season [My-78, Section 3]. The altitude dependence of the O₃ mass-mixing ratio ($m_R(O_3)$) is treated by using a transition boundary at 55-km altitude. Below 55 km, the model accounts for the variation of $m_R(O_3)$ with altitude, latitude, and season. The model predicts:

(text continues on p. 61)

Table 4-1. Input and output variables for Subroutine SPCMIN.

INPUT VARIABLES

Argument List

- KK - Calculation flag
 = 1, calculate initialization parameters
 = 2, calculate atmospheric properties
- ZH - Altitude of interest (km)

ATMOUP Common

- IDORN - Index for day or night
 = +1, day
 = -1, night

TIME Common

- PLAT - North latitude of point P (radians)

DATA

- ALTKM(47) - Altitudes ($z=0(5)230$ km) at which minor species densities are specified as data
- ANODAY(21) - Noontime data-base values of [NO] at altitudes $0(5)100$ km at 50° latitude
- ANONIT(21) - Midnight data-base values of [NO] at altitudes $0(5)100$ km at 50° latitude
- AN₂DDN(41) - Data-base values of the basic component ($T_7(z)$) of the $N(^2D)$ densities between 125- and 200-km altitude, augmented by 25 zeros below 125 km
- AN₄SDN(33) - Data-base values of the basic component ($T_1(z)$) of the N densities between 100- and 160-km altitude, augmented by 20 zeros below 100 km
- CH₄PCC - Factor used ($3.75369008E+16$) with total mass density (g/cm^3) to convert CH₄ mass-mixing ratio (ppmm) to molecules/ cm^3
- COMPCC - Factor used ($2.14992030E+16$) with total mass density (g/cm^3) to convert CO mass-mixing ratio (ppmm) to molecules/ cm^3
- CO₂(25) - Data-base values of [CO₂] at altitudes $0(5)120$ km

(Continued)

Table 4-1. (Cont'd)

| | |
|------------|---|
| DAHDAY(21) | - Noontime data-base values of [H] at altitudes 0(5)100 km |
| DAHMIT(21) | - Midnight data-base values of [H] at altitudes 0(5)100 km |
| DATCO(31) | - Data-base values of CO mass-mixing ratio (ppmm) at altitudes 0(5)150 km |
| DN2O(12) | - Selected values of N ₂ O volume-mixing ratio (ppbv) at altitudes 0(5)55 km |
| DOHDAY(21) | - Noontime data-base values of [OH] at altitudes 0(5)100 km |
| DOHMIT(21) | - Midnight data-base values of [OH] at altitudes 0(5)100 km |
| HO2DAY(21) | - Noontime data-base values of [HO ₂] at altitudes 0(5)100 km |
| HO2MIT(21) | - Midnight data-base values of [HO ₂] at altitudes 0(5)100 km |
| H2ODN(21) | - Data-base values of H ₂ O mass-mixing ratio (ppmm) at altitudes 20(5)120 km |
| H2OPCC | - Factor used (3.34260935E+16) with total mass density (g/cm ³) to convert H ₂ O mass-mixing ratio (ppmm) to molecules/cm ³ |
| NALTMH | - Two plus the number of altitudes (NMTH=23) between 10 and 120 km used to fit CH ₄ mass-mixing ratios |
| NALTNO | - Number of altitudes (21) between 0 and 100 km used to fit daytime NO densities at 50° latitude |
| NALTO2 | - Number of altitudes (11) between 0 and 50 km used to fit daytime O ₂ (¹ Δ _g) densities |
| NALT2D | - Number of altitudes (16) between 125 and 200 km used to fit the basic component (T ₇ (z)) of the N(² D) densities |
| NALT4S | - Number of altitudes (13) between 100 and 160 km used to fit the basic component (T ₁ (z)) of the N densities |
| NDEGNO | - Degree of the polynomial (12) used to fit the daytime NO densities between 0 and 100 km at 50° latitude |
| NDEG2D | - Degree of the polynomial (6) used to fit the basic component (T ₇ (z)) of the N(² D) densities between 125 and 200 km |

(Continued)

Table 4-1. (Cont'd)

| | |
|------------|---|
| NDEG4S | - Degree of the polynomial (5) used to fit the basic component ($T_1(z)$) of the N densities between 100 and 160 km |
| NDGH20 | - Degree of the polynomial (12) used to fit the H ₂ O mass-mixing ratio (ppmm) between 20 and 120 km |
| NDGMTH | - Degree of the polynomial (11) used to fit the CH ₄ mass-mixing ratio (ppmm) at altitudes 0(5)120 km |
| NDGNO2 | - Degree of the polynomial (12) used to fit the daytime NO ₂ densities between 0 and 160 km |
| NDGO2D | - Degree of the polynomial (10) used to fit the daytime O ₂ (¹ Δ _g) densities between 0 and 50 km |
| NKMH20 | - Number of altitudes (21) between 20 and 120 km used to fit H ₂ O mass-mixing ratios (ppmm) |
| NKMNO2 | - Number of altitudes (33) between 0 and 160 km used to fit the daytime NO ₂ densities |
| ONITE(18) | - Midnight data-base values of [O] at altitudes 0(5)85 km |
| OZ3PCC | - Factor used (1.25459271E+22) with total mass density (g/cm ³) to convert O ₃ mass-mixing ratio (kg/kg) to molecules/cm ³ |
| O1DDAY(33) | - Noontime data-base values of [O(¹ D)] at altitudes 0(5)160 km |
| O2SDGD(47) | - Noontime data-base values of [O ₂ (¹ Δ _g)] at altitudes 0(5)230 km |
| O2SDGN(47) | - Midnight data-base values of [O ₂ (¹ Δ _g)] at altitudes 0(5)230 km |
| O3DAY(26) | - Noontime data-base values of O ₃ mass-mixing ratio (ppmm) at altitudes 55(5)120 km, augmented by an assigned value at 125 km to facilitate fitting |
| O3NIT(27) | - Midnight data-base values of O ₃ mass-mixing ratio (ppmm) at altitudes 55(5)120 km, augmented by two assigned values at 125 and 130 km to facilitate fitting |
| PI | - 3.141592653590 |
| SMETH(25) | - Data-base values of CH ₄ mass-mixing ratio (ppmm) at altitudes 0(5)120 km |

(Continued)

Table 4-1. (Cont'd)

-
- SNO2D(33) - Noontime data-base values of [NO₂] at altitudes 0(5)160 km
 - SNO2N(33) - Midnight data-base values of [NO₂] at altitudes 0(5)160 km

OUTPUT VARIABLES

Argument List

None

ATMOUP Common

- SNI(7) - N concentration (1/cm³)
- SNI(8) - NO concentration (1/cm³)
- SNI(13) - O₂(¹Δ_g) concentration (1/cm³)
- SNI(14) - O₃
- SNI(15) - NO₂
- SNI(16) - H₂O
- SNI(17) - H
- SNI(18) - OH
- SNI(19) - HO₂
- SNI(20) - CO
- SNI(21) - N₂O
- SNI(22) - CH₄
- SNI(23) - N(⁴S)
- SNI(24) - N(²D)
- SNI(25) - Relative humidity, percent
- SNI(26) - O(¹D) concentration (1/cm³)
- SNI(27) - O(²P) concentration (1/cm³)



ALTODN Common

- ALTKM(47) - See input
- ONITE(18) - See input
- CO2(25) - See input (Note that the CO₂ densities from 0- to 100-km altitude are reset in Subroutine ATMOSU by using a constant volume-mixing ratio of 3.2 × 10⁻⁴.)

(Continued)

Table 4-2. Fit functions for O density profiles.

| Altitude Range, km | Description |
|------------------------------|--|
| <u>Day</u> | |
| 0 - 120 | ATMOSU low-altitude model |
| >120 | ATMOSU high-altitude model |
| <u>Night</u> ^{a, b} | |
| 0 - 60 | Constant at data-point value |
| 60 - 75 | Exponential, with slope determined by data points at 60 and 75 km |
| 75 - 85 | Exponential-like function with altitude-dependent scale height so determined that function passes through data points at 75, 80, and 85 km |
| 85 - 90 | Exponential, with slope determined by data point at 85 km and low-altitude-model value at 90 km |
| 90 - 120 | ATMOSU low-altitude model |
| >120 | ATMOSU high-altitude model |

^a My-75, Table 2-5.

^b Fits are made in Subroutine ATMOSU.

Table 4-3. Fit functions for $O(^1D)$ density profiles.^a

| Altitude Range, km | Description |
|-----------------------|--|
| | <u>Day</u> |
| 0 - 47 | Exponential-like function (lower-limited to 1.0) with altitude-dependent scale height so determined that function passes through data points at 25, 40, and 47 km |
| 47 - 80 | Exponential-like function with altitude-dependent scale height so determined that function passes through data points at 47, 65, and (assigned value of 10 at) 80 km |
| 80 - 100 | Exponential, with slope determined by data points at 80 and 100 km and passing through assigned value of 10 at 80 km |
| 100 - 120 | Exponential-like function, with altitude-dependent scale height so determined that function passes through data points at 100, 110, and 120 km |
| 120 - 160 | Exponential, with slope determined by data points at 120 and 160 km and passing through data point at 120 km |
| >160 | Proportional to O , ^b $[O(^1D)] = \{[O(^1D)]/[O]\}_{160}[O(z)]$ |
| | <u>Night</u> |
| >0 | Constant, at assigned value of 1.0 |

^a My-78, Table 9-1.

^b This procedure makes $[O(^1D)]$ dependent on the time and solar flux to the extent that $[O]$ is dependent on these parameters.

Table 4-4. Fit functions for $O_2(^1\Delta_g)$ density profiles.^a

| Altitude Range, km | Description ^b |
|-----------------------|---|
| <u>Day</u> | |
| 0 - 50 | 10th-degree polynomial (coefficients DD) to match data points at 0(5)50 km |
| 50 - 75 | Exponential, determined by data points at 50 and 75 km |
| 75 - 90 | 5th-degree polynomial, determined by data points at 75(5)90 km and derivatives of 50-to-75 km fit-function at 75 km and ≥ 90 -km function at 90 km |
| ≥ 90 | Exponential, determined by data points at 90 and 105 km |
| <u>Night</u> | |
| 0 - 70 | Constant at data-point value |
| 70 - 80 | Exponential, determined by data points at 70 and 80 km |
| 80 - 100 | 5th-degree polynomial, determined by data points at 80(5)95 km and values of daytime fit-function and its derivative at 100 km |
| >100 | Daytime fit-function |

^a My-75, Table 3-1.

^b Unchanged from HS-75, Table 14.

Table 4-5. Fit functions for O₃ mass-mixing ratio profiles.

| Altitude Range, km | Description |
|-----------------------|---|
| | <u>Day or Night</u> |
| 0 - 55 | New model, latitude- and season-dependent ^a |
| | <u>Day</u> ^b |
| 55 - 75 | 5th-degree polynomial (coefficients T03(I)), to match data points at 55(5)75 km and the (zero) derivative of the 0- to 55-km fit-function at 55 km |
| 75 - 90 | 5th-degree polynomial (coefficients U03(I)), to match data points at 75(5)90 km and derivatives of 55- to 75-km fit-function at 75 km and >90-km fit-function at 90 km |
| >90 | Exponential, determined by data points at 90 and 105 km |
| | <u>Night</u> |
| 55 - 70 | 5th-degree polynomial (coefficients V03(I)), to match data points at 55(5)70 km, the (zero) derivative of the 0- to 55-km fit-function at 55 km, and the derivative of the 70- to 75-km fit-function at 70 km |
| 70 - 75 | Exponential, determined by data points at 70 and 75 km |
| 75 - 90 | 5th-degree polynomial (coefficients W03(I)), to match data points at 75(5)90 km and derivatives of 70- to 75-km fit-function at 75 km and >90-km fit-function at 90 km |
| >90 | Exponential, determined by data points at 90 and 105 km |

^a My-78, Section 3.

^b My-75, Section 4.2 and HS-75, Table 15.

Table 4-6. Fit function for N density profiles.^a

| Altitude Range, km | Description |
|----------------------------------|--|
| <u>Day or Night</u> | |
| $z \geq 0$ | Analytic expression ^b dependent on altitude, local apparent time, latitude, fractional season-year, and solar decimetric flux. Five factors include an altitude-dependent basic factor (T_1), latitudinal factor with diurnal variation (T_2), seasonal factor ($\exp(T_3)$), diurnal factor with altitudinal and latitudinal variations ($\exp(T_4)$), and solar-flux factor (T_5) |
| <u>$T_1(z)$</u> | |
| 0 - 100 | Exponential function, passing through the fit-function value at 100 km |
| 100 - 160 | 5th-degree polynomial, determined by least squares (coefficients CC) for data points at 100(5)160 km |
| > 160 | Exponential function, passing through the fit-function value at 160 km |
| <u>$T_2(L, t)$</u> | |
| > 0 | Analytic expression dependent on latitude and local apparent time |
| <u>$T_3(f)$</u> | |
| > 0 | Analytic expression dependent on fractional season-year |
| <u>$T_4(t, z, L)$</u> | |
| > 0 | Analytic expression factorable into an expression dependent on the local apparent time and the latitude and an expression dependent on the altitude |
| <u>$T_5(F)$</u> | |
| > 0 | Analytic expression dependent on solar decimetric flux |

^a My-78, Section 12.

^b My-78, Section 12, Equations (1) through (5).

Table 4-7. Fit functions for $N(^2D)$ density profiles.^a

| Altitude Range, km | Description |
|---------------------------------------|---|
| <u>Day or Night</u> | |
| <u>>0</u> | Analytic expression ^b dependent on altitude, local apparent time, and (through a dependence on the total nitrogen atom density) on latitude, fractional season-year, and solar decimetric flux |
| <u>SNI(7) and $T_1(z)$</u> | |
| <u>>0</u> | These functions are given by the formulas for the total nitrogen atom densities |
| <u>$T_7(z)$</u> | |
| 0 - 125 | Exponential function, passing through the fit-function value at 125 km |
| 125 - 200 | 6th-degree polynomial, determined by least squares (coefficients BB) for data points at 125(5)200 km |
| >200 | Exponential function, passing through the fit-function value at 200 km |
| <u>$T_8(t)$</u> | |
| <u>>0</u> | Analytic expression dependent on the local apparent time |

^a My-78, Section 13.

^b My-78, Section 13, Equations (1) and (2).

Table 4-8. Fit functions for $N(^2P)$ density profiles.^a

| Altitude Range, km | Description |
|-----------------------|--|
| | <u>Day or Night</u> |
| 0 - 119.9 | $R_{2P2D} \equiv [N(^2P)]/[N(^2D)] = 0.01$ |
| >119.9 | $R_{2P2D} = 5.5 \times 10^{-4} P_{2P2D} e^{900/z}$ |
| | $P_{2P2D} = 0.01$ |

^a In the absence of information on the ambient density of $N(^2P)$, B.F. Myers has offered an estimate based on simplifying assumptions: (1) $[N(^2P)]$ and $[N(^2D)]$ are in steady state, (2) the production rate of $N(^2P)$ is a factor $P_{2P2D} \approx 0.01$ times that for $N(^2D)$, (3) the collisional deactivation rate of $N(^2P)$ is the same as that for $N(^2D)$, (4) the radiative decay rate of $N(^2D)$ is small compared with its collisional decay rate, (5) the altitude profile of the ratio $R_{2P2D} \equiv [N(^2P)]/[N(^2D)]$, computed by using nominal rate coefficients, can be approximated by the expression $5.5 \times 10^{-4} \times P_{2P2D} \times \exp(900/z)$ for $z \gtrsim 120$ km, at which altitude $R_{2P2D} = 0.01$.

Table 4-9. Fit functions for NO density profiles.^a

| Altitude Range, km | Description |
|---------------------------|--|
| <u>Day</u> ^b | |
| 0 - 100 | 12th-degree polynomial, determined by least squares (coefficients AA) for data points at 0(5)100 km |
| <u>Night</u> ^b | |
| 0 - 50 | Constant at data-point value of 1.0 |
| 50 - 60 | Exponential-like function (lower-limited to 1.0), with altitude-dependent scale height so determined that function passes through data points at 50, 55, and 60 km |
| 60 - 85 | Exponential, determined by data point at 60 km and daytime polynomial fit-function at 85 km |
| 85 - 100 | Daytime fit-function |
| <u>Day or Night</u> | |
| >100 | Analytic expression dependent on altitude, local apparent time, latitude, and solar decimetric flux [My-78, Section 11, Equation (6)] |

^a My-78, Section 11.

^b For both day and night, we add to the logarithm of the NO density a latitude-dependent term with an altitude-dependent coefficient. Without the latitude-dependent term, the fit functions apply to a 50° latitude. See My-78, Section 11, Equation (8).

Table 4-10. Fit functions for NO₂ density profiles.^a

| Altitude Range, km | Description ^b |
|-----------------------|---|
| <u>Day</u> | |
| 0 - 160 | 12th-degree polynomial, determined by least squares (coefficients HH) for data points at 0(5)160 km |
| >160 | Exponential, with slope determined by fit-function values at 140 and 160 km, and passing through fit-function value at 160 km |
| <u>Night</u> | |
| 0 - 55 | $[\text{NO}_2]_{\text{night}} = [\text{NO}]_{\text{day}} + [\text{NO}_2]_{\text{day}} - [\text{NO}]_{\text{night}}$ |
| 55 - 65 | Exponential, with slope determined by fit function at 55 km, and passing through data point at 65 km |
| 65 - 82 | Exponential, with slope determined by data point at 65 km and by daytime fit-function value at 82-km altitude |
| >82 | Daytime fit function |

^a My-75, Table 7-1.

^b Unchanged from HS-75, Table 16.

Table 4-11. Fit functions for N₂O volume-mixing ratio profiles^a

| Altitude Range, km | Description |
|-----------------------|--|
| | <u>Day or Night</u> ^b |
| 0 - 55 | 8th-degree polynomial, determined by least squares (coefficients CN20) for volume-mixing-ratio data-points at 0(55)55 km |
| >55 | Constant at volume-mixing ratio data-point |

^a My-78, Table 10-2.

^b This profile, obtained at high latitude, must be multiplied by a latitude-dependent factor which itself is altitude-dependent. See My-78, Section 10, Equation (2).

Table 4-12. Fit functions for CO₂ volume-mixing ratio profiles.^a

| Altitude Range, km | Description ^b |
|-----------------------|--|
| | <u>Day or Night</u> ^c |
| 0 - 100 | Constant volume-mixing ratio of 0.00032 in ATMOSU low-altitude model |
| 100 - 120 | 6th-degree polynomial, to match ATMOSU low-altitude-model value at 100 km and data points at 105(5)120 km and derivatives of low-altitude-model function at 100 km and ATMOSU high-altitude-model function at 120 km |
| >120 | ATMOSU high-altitude model |

^a My-75, Table 8-1.

^b Unchanged from HS-75, Table 10.

^c Fits are made in Subroutine ATMOSU.

Table 4-13. Fit functions for CO mass-mixing ratio profiles.^a

| Altitude Range, km | Description |
|-----------------------|--|
| <u>Day or Night</u> | |
| 0 - 150 | 13th-degree polynomial determined by least squares (coefficients EE) for data points at 0(5)150 km |
| >150 | Exponential, passing through fit function at 150 km |

^a My-78, Table 5-1.

Table 4-14. Fit functions for CH₄ mass-mixing ratio profiles.^a

| Altitude Range, km | Description |
|-----------------------|--|
| <u>Day or Night</u> | |
| 0 - 10 | Constant, at fit-function value at 10 km |
| 10 - 120 | 11th-degree polynomial, determined by least squares (coefficients FF) for data points at 10(5)120 km |
| >120 | Exponential, passing through fit function at 120 km |

^a My-78, Table 4-1.

Table 4-15. Fit functions for H₂O mass-density and mass-mixing ratio profiles.^a

| Altitude Range, km | Description |
|-----------------------|--|
| | <u>Day or Night</u> |
| 0 - 5 | Analytic fit functions for water vapor mass density (g/m ³), expressed as the sum of a mean and a seasonal term, $[H_2O] = \text{Mean}(\alpha, z) + \text{Season}(f, \alpha, z),$ where α = type of moisture region (six in total, distributed among 11 geographic regions), f = fraction of season-year, and z = altitude. |
| 5 - 14 | Interpolation between natural logarithm of mass-mixing ratio (ppmm) values at 5 and 14 km |
| 14 - 45 | Analytic fit functions for water vapor mass-mixing ratio, expressed as the sum of a mean and a seasonal term, $m_R = \text{Mean}(\text{with transition at latitude } L \approx 28^\circ \text{ for } z \approx 30 \text{ km}) + \text{Season}(f, L, z \approx 20 \text{ km})$ |
| 45 - 120 | 12th-degree polynomial for natural logarithm of mass-mixing ratio (ppmm), determined by least squares (coefficients GG) for data points at 20(5)120 km |
| >120 | Exponential, $m_R(z) = m_R(120) \exp[-0.0575(z-120)],$ where $m_R(120)$ is determined from the fit function from 45 to 120 km |

^a My-78, Section 2.

Table 4-16. Fit functions for OH density profiles.^a

| Altitude Range, km | Description |
|-----------------------|---|
| | <u>Day or Night</u> |
| 0 - 80 | 7th-degree polynomial, determined by least squares (coefficients CCOH) for data points at 0(5)80 km |
| 80 - 100 | Exponential, with slope determined by fit-function value at 80 km and passing through assigned value (60 for day and 190 for night) at 100 km |
| >100 | Analytic expression, passing through fit-function value at 100 km |

^a My-78, Table 6-1.

Table 4-17. Fit functions for HO₂ density profiles.^a

| Altitude Range, km | Description |
|-----------------------|--|
| | <u>Day or Night</u> |
| 0 - 65 | Polynomial (6th degree for day, 7th degree for night), determined by least squares (coefficients CHO ₂) for data points at 0(5)65 km |
| 65 - 75 | Exponential, with slope determined by fit-function value at 65 km and data-point value at 75 km |
| 75 - 100 | Product of two functions: (1) Exponential, with slope determined by data point values at 75 and 95 km and (2) 10 ^{F(z)} where F(z) is given by $F(z) = \begin{cases} 1.0 - 0.2 z-80 , & 75 \leq z \leq 85 \\ 0 & , z > 85 \end{cases}$ Product-function passes through data-point values at 75 and 95 km |
| >100 | Exponential, passing through fit-function value at 100 km with prescribed slope |

^a My-78, Table 7-1.

Table 4-18. Fit functions for H density profiles.^a

| Altitude Range, km | Description |
|-----------------------|---|
| <u>Day</u> | |
| 0 - 35 | Exponential (lower-limited to 1.0) with slope determined by data points at 30 and 35 km and passing through data point at 30 km |
| 35 - 40 | Exponential, with slope determined by data points at 35 and 40 km and passing through data point at 35 km |
| 40 - 86 | Exponential, with slope determined by data point at 40 and assigned value of 9.0×10^7 at 86 km and passing through data point at 40 km |
| <u>Night</u> | |
| 0 - 74 | Constant, at assigned value of 1.0 |
| 74 - 86 | Exponential-like function (lower-limited to 1.0 in range below about 74.265 km), with altitude-dependent scale height so determined that function passes through data points at 75, 80, and 86 km |
| <u>Day or Night</u> | |
| 86 - 100 | Exponential, with slope determined by data points at 86 and 100 km and passing through data point at 86 km |
| >100 | Sum of exponential and power law, adjusted to pass through data point at 100 km |

^a My-78, Table 8-1.

- (1) An increase in the total O_3 content of the atmosphere with increasing latitude,
- (2) A general increase in the maximum O_3 partial pressure with increasing latitude and an associated decrease in the altitude of the maximum,
- (3) A decrease in the O_3 partial pressure above about 24 km with increasing latitude,
- (4) A seasonal dependence the variation of which is a maximum in the altitude range between 15 and 35 km (depending on latitude), and
- (5) A variation in the seasonal maximum with changing altitude.

Above 55 km, the model accounts for the altitude and day-to-night variation of $m_R(O_3)$, but does not (explicitly) treat seasonal or geographical effects. (However, the major-species model (Section 2) uses a temperature profile that is latitude- and season-dependent; hence, there is a corresponding dependence for the total mass density and the number density of minor species, such as O_3 , specified in terms of mixing ratios.) The model does not include (small) longitudinal variations, day-to-day fluctuations, or long-term trends.

A guide to the principal features of the ozone model is given in Table 4-19. Figure 4-1 is a simplified flow chart of the operational phase of the O_3 -portion of Subroutine SPCMIN, mainly for altitudes above 55 km; the nature of the fit functions evaluated here is given in Table 4-5.

Subroutine OZONE computes the latitude and season dependence of the mass-mixing ratio of O_3 for altitudes from 0 to 55 km by evaluating Equation (14) and its supporting equations (principally, Equation (11)) in Section 3 of My-78. The inputs and outputs for Subroutine OZONE are summarized in Table 4-20.

Table 4-19. Features of ozone model [My-78].

| Subroutine | Altitude Range, km | Dependent Variable | Explicit ^a Independent Variables | | | Data Base Reference |
|--------------------|--|-----------------------------|---|--------------------|------------------|----------------------------|
| | | | Latitude | Season | Diurnal Altitude | |
| OZONE ^b | 0 > z > 55 | Mixing Ratio ^{e,f} | Yes ^c | Yes ^{c,d} | Yes | US-76, Dütsch, CIAP Mono.1 |
| SPCMIN | $\left. \begin{array}{l} 55 < z < 120 \\ z > 120 \end{array} \right\}$ | Mixing Ratio ^e | | Yes ^c | Yes | Myers [My-75] |
| | | Mixing Ratio ^e | | Yes ^c | Yes | |

^a Major-species model depends on latitude and season; conversion from mixing ratio to absolute values will reflect this dependence.

^b Subroutine OZONE is called from Subroutine SPCMIN.

^c Initialization is performed.

^d Maximum seasonal variation between 15- and 35-km altitude.

^e Subroutine SPCMIN converts from mass-mixing ratio m_R (kg O₃/kg air) to molecules/cm³ = $m_R \rho_{air} 10^{-6}/m_{O_3}$ before outputting SNI(14).

^f The form of the expression is $m_R = \text{Mean}(L,z) + \text{Season}(f,L,z)$ where L = latitude, f = fractional season-year, and z = altitude.

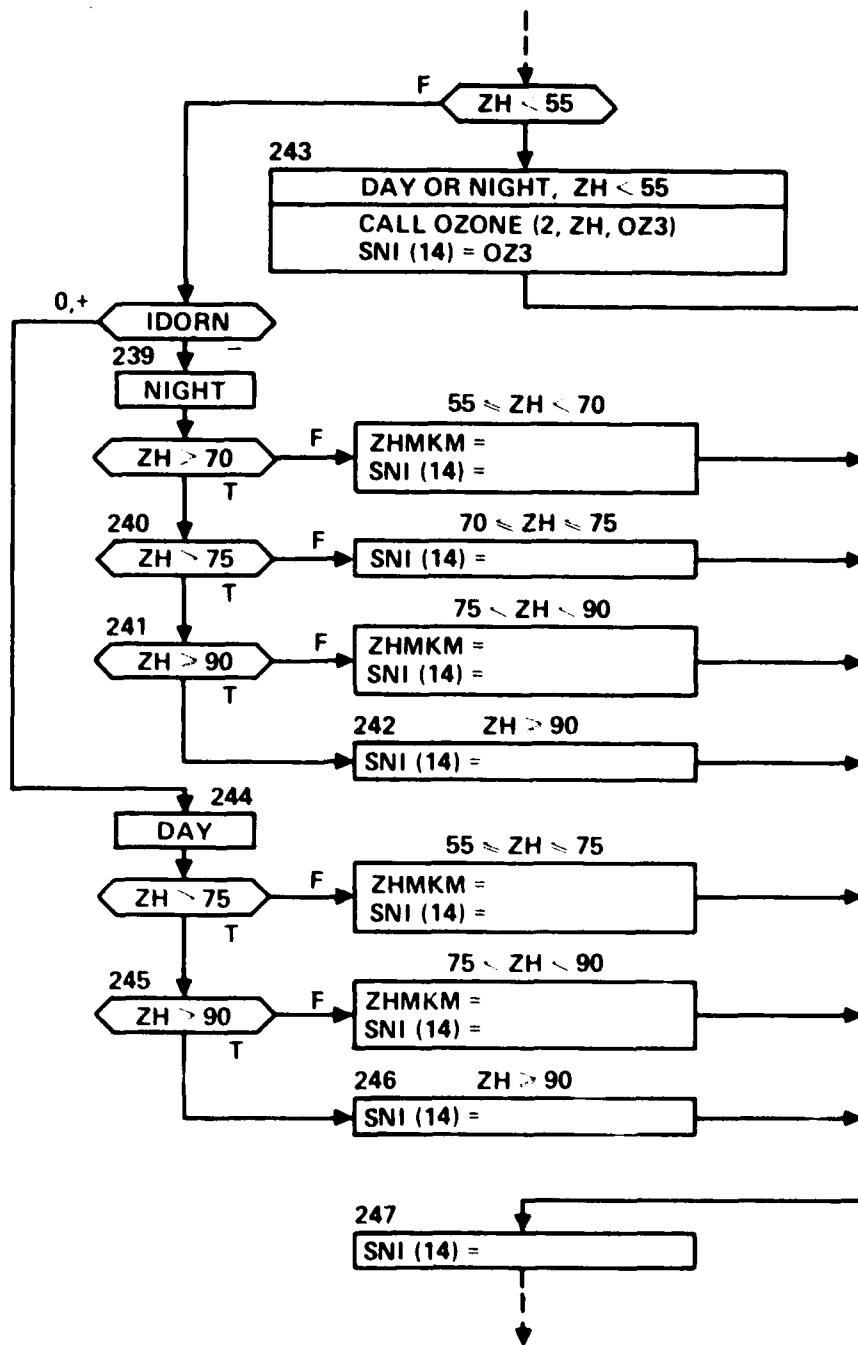


Figure 4-1. Flow chart for the O₃-portion of Subroutine SPCMIN during its operational phase.

Table 4-20. Input and output variables for Subroutine OZONE.

INPUT VARIABLES

Argument List

- KK - Calculation flag
= 1, calculate initialization parameters
= 2, calculate O₃ mass-mixing ratio for 0- to 55-km altitude
- ZKM - Altitude of interest, from 0 to 55 km

TIME Common

- PLAT - North latitude of point P (radians)
- FYR - Fractional season-year, being 0 on 1 January in northern hemisphere and on 1 July in southern hemisphere

OUTPUT VARIABLE

Argument List

- OZ3 - O₃ mass-mixing ratio at altitude ZKM (kg/kg)
-

4-3 WATER

4-3.1 The Coded Model

Our model for altitude profiles of H_2O density, as a function of latitude, longitude, and season, is given in Section 2 of My-78 and may be summarized thusly. The altitude dependence of the H_2O density is treated by using transition boundaries at 5- and 14-km altitude. For the 0- to 5-km altitude range, the Earth's surface is divided into 11 geographic zones with six types of quasi-homogeneous moisture regions (a significant reduction from the NASA data-base model having hundreds of geographic zones and 45 homogeneous moisture regions); in each region the seasonal dependence is included. For the 5- to 14-km altitude region, H_2O densities are determined by interpolating the mixing ratios at 5- and 14-km altitude. At and above 14-km altitude, we include a seasonal dependence which (1) decreases with increasing altitude and vanishes for altitudes above about 20 km, and (2) has a latitude-dependent phase shift due to the influx of water vapor from the tropical troposphere into the lower stratosphere. An associated transition region at about 30° latitude vanishes for altitudes above about 30 km where a single mixing-ratio profile obtains.

Table 4-21 summarizes the geographic regions used in modeling the 0- to 5-km altitude moisture regions. Figure 4-2 gives a simple guide to the H_2O model, with the principal features as shown in Table 4-22.

Figure 4-3 is a simplified flow chart of the operational phase of the H_2O -portion of Subroutine SPCMIN; the nature of the fit functions evaluated here is given in Table 4-15.

Subroutine WATER computes the longitude, latitude, and season dependence of water vapor for altitudes from 0 to 45 km by evaluating the equations in Section 2 of My-78. The inputs and outputs for Subroutine WATER are summarized in Table 4-23.

4-3.2 Option for User-Specified H_2O Profile

To supplement our H_2O density model, we provide to the ROSCOE user an option whereby he can input his own profile of interest. To implement this option the user inputs a value greater than 0.0 for

Table 4-21. Summary of regions used in modeling 0- to 5-km altitude moisture regions.

| Latitude Range | Number of Regions | | Latitude Distribution of Moisture Regions | | | | | | |
|----------------|-------------------|------------|---|-----|-----------|-----------|-----------|-----|--|
| | Geographic | Moisture | 0° - 30° | | 30° - 60° | | 60° - 90° | | |
| | | | Wet | Dry | Wet | Intermed. | Dry | Dry | |
| 90N - 60N | 1 | 1 | | | | | | X | |
| 60N - 30N | 4 | 3 | | | X | X | | X | |
| 30N - 30S | 3 | 2 | X | X | | | | | |
| 30S - 60S | 2 | 2 | | | X | X | | | |
| 60S - 90S | 1 | 1 | | | | | | X | |
| | | Total = 11 | | | | | | | |

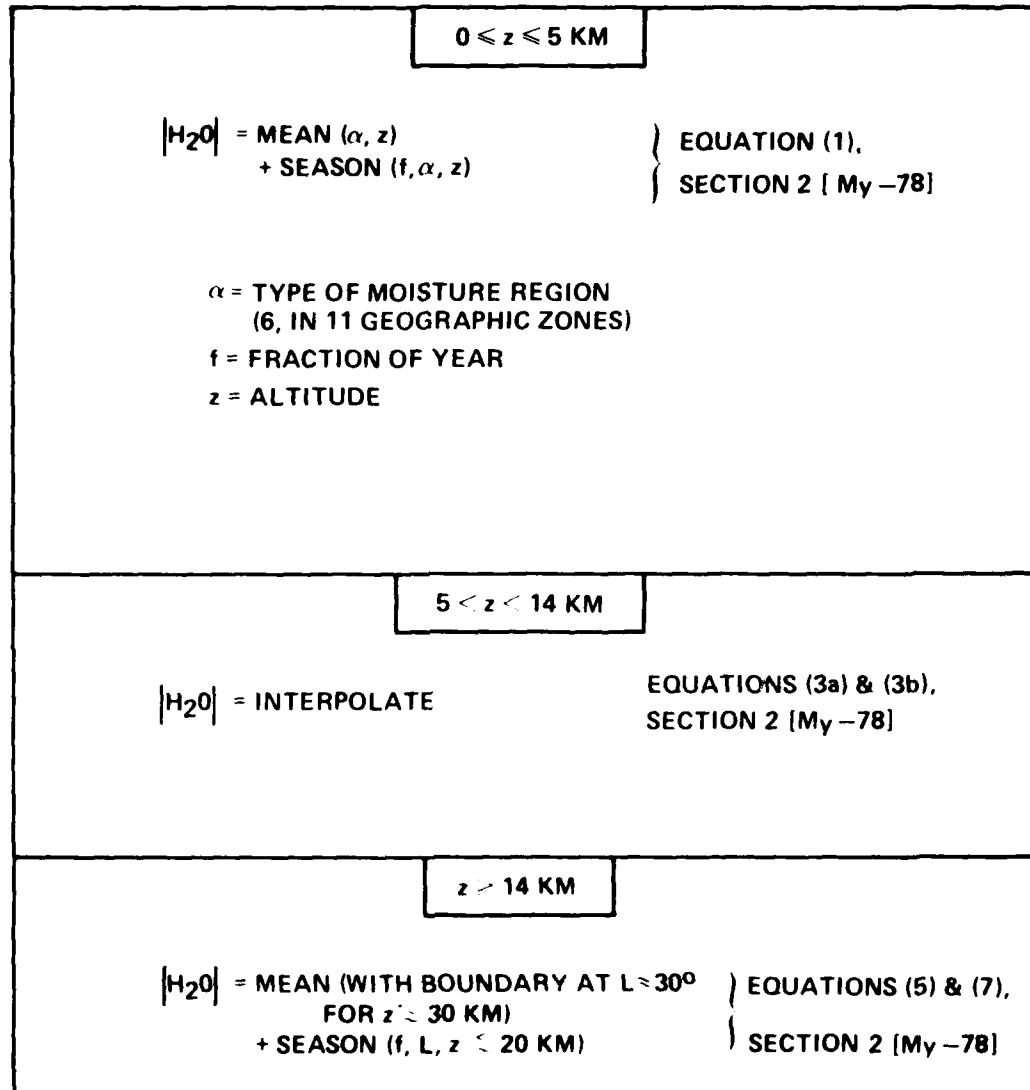


Figure 4-2. Simple guide to the H₂O model.

Table 4-22. Features of water vapor model [My-78].

| Subroutine | Altitude Range, km | Dependent Variable | Explicit ^a Independent Variables | | | Data Base Reference |
|---------------------|--------------------|----------------------------------|---|------------------|------------------|---|
| | | | Longitude | Latitude | Season | |
| WATER ^h | 0 < z < 5 | Absolute Humidity ^{b,c} | Yes ^d | Yes ^d | Yes ^d | NASA [SG-71, SF-72b] |
| | 5 < z < 14 | Mixing Ratio ^c | (yes) ^{d,e} | Yes ^d | Yes ^d | Interpolation |
| | 14 < z < 45 | Mixing Ratio ^c | Yes ^f | Yes ^g | Yes | Harries [Ha-76e] |
| SPCMIN ⁱ | 45 < z < 120 | Mixing Ratio ^c | | | Yes ^d | 45-70, Interpolation >70, Myers [My-75] |
| | z > 120 | Mixing Ratio ^c | | | Yes | Myers [My-75] |

^a Major-species model depends on latitude and season; conversion from mixing ratio to absolute values will reflect this dependence.

^b In g/m³; WATER converts to ppm = (g_{H₂O}/m³)/(g_{dry air}/cm³) before returning to SPCMIN.

^c In ppm; SPCMIN converts to molecules/cm³ = (ppm)ρ_{air}10⁻⁶/m_{H₂O} before outputting SNI(16).

^d Initialization is performed.

^e Because 5-km values used in interpolation depends on longitude.

^f Two-latitude region for z < 30 km with transition at ≈ 30° latitude.

^g Seasonal dependence for z < 20 km.

^h WATER called from SPCMIN.

ⁱ SPCMIN called from ATMOSU.

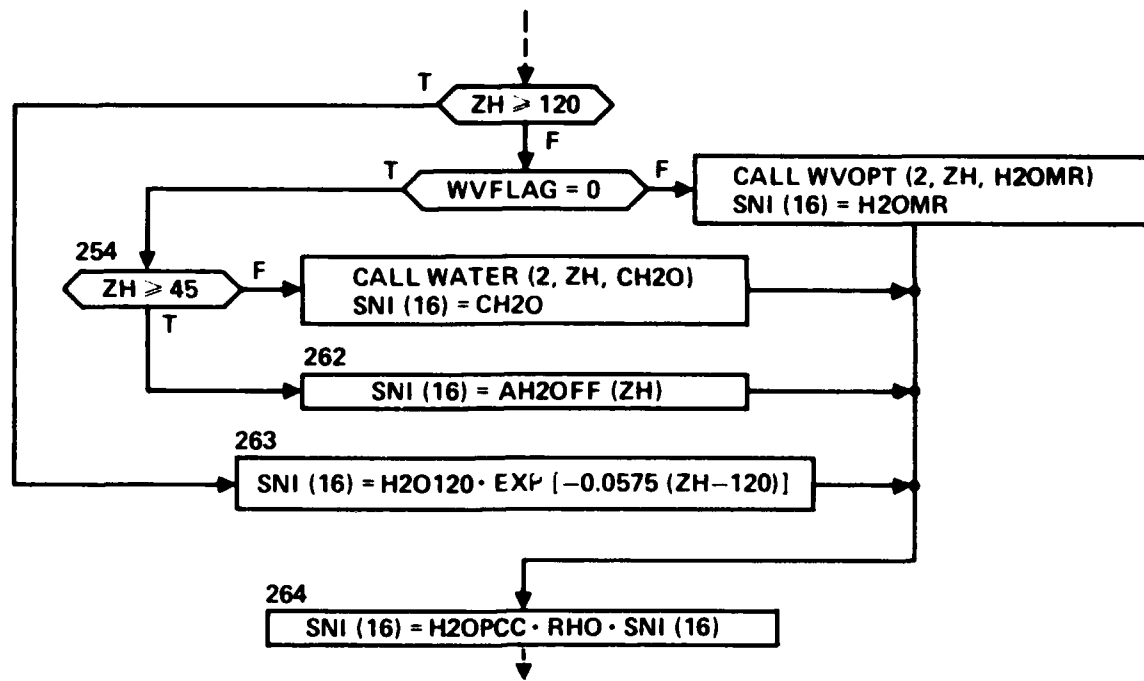


Figure 4-3. Flow chart for the H₂O-portion of Subroutine SPCMIN during its operational phase.

Table 4-23. Input and output variables for Subroutine WATER.

INPUT VARIABLES

Argument List

- KK - Calculation flag
= 1, calculate initialization parameters
= 2, calculate H₂O mass-mixing ratio for 0- to 45-km altitude
- ZH - Altitude of interest, from 0 to 45 km

ATMOUP Common

- RHO - Mass density of dry air (g/cm³)

TIME Common

- PLAT - North latitude of point P (radians)
- PLON - East longitudinal of point P (radians)
- FYR - Fractional season-year, being 0 on 1 January in northern hemisphere and on 1 July in southern hemisphere
- RH05KM - Mass density of dry air at 5-km altitude (g/cm³)

OUTPUT VARIABLE

Argument List

- H2O - Mass-mixing ratio of H₂O at altitude ZH (ppmm)
-

WVFLAG. (The normal value of 1.0 is necessary for WVFLAG so that Subroutine SPCMIN can call Subroutine WATER during the initialization phase.) For WVFLAG \neq 0.0, Subroutine WVOPT is allowed to read water data in one of four optional forms according to METHOD = 1,2,3,4, which we will discuss below. But first, it is anticipated that the user will be most interested in using his own low-altitude data over the altitude range from HH(1) = 0.0 to HH(NOP), but he must also actually read in data over the remaining higher-altitude range from HH(NOP+1) to HH(NZH) = 120.0. If the user has no personal preference for data in the higher-altitude range, he may find it convenient to use the data in a data statement in Subroutine SPCMIN, given at altitudes 20(5)120 km and in units of parts per million by mass (ppmm).

In considering what options should be available, note that Huschke [Hu-59, p. 462] states that a radiosonde measures pressure, temperature, and humidity. (Since humidity is not further specified, it could be any measure of the water-vapor content, such as absolute humidity, relative humidity, specific humidity, mixing ratio, or dew-point temperature.)

Before proceeding, we digress for the benefit of some readers to discuss various ways of expressing the water-vapor content of moist air. We have a need for some or possibly all of them and the conversion relations.

1. Water-Vapor Number Density

$$[H_2O] = H_2O \text{ molecules/cm}^3.$$

The corresponding vapor pressure at temperature T is

$$p_w = [H_2O]kT \text{ dyne/cm}^2 \quad (1a)$$

$$= 10^{-3} [H_2O]kT \text{ mb} \quad (1b)$$

2. Absolute Humidity

$$\rho_{H_2O} = (\text{grams of } H_2O) / m^3,$$

also called vapor concentration or vapor density. Note the convention of using m^{-3} and not cm^{-3} . The corresponding vapor pressure at temperature T is

$$p_w = 10^{-6} \rho_{H_2O} (g/m^3) \frac{N_A}{M_{H_2O}} kT \text{ dyne/cm}^2 \quad (2a)$$

$$= 10^{-6} \rho_{H_2O} (g/m^3) \frac{R}{M_{H_2O}} T \text{ dyne/cm}^2 \quad (2b)$$

where N_A = Avogadro's number, R = gas constant, and M_{H_2O} = molecular weight of water vapor.

3. Mass-Mixing Ratio

r_m = the dimensionless ratio of the mass of water vapor to the mass of dry air, sometimes expressed in units of parts per million by mass, i.e.,

$$r_m (\text{ppmm}) = (g_{H_2O}/m^3) / (\rho_{\text{dry air}}/\text{cm}^3) \quad (3a)$$

$$= \rho_{H_2O} (g/m^3) / \rho_{\text{dry air}} (g/cm^3) \quad (3b)$$

4. Relative Humidity

U_w = the dimensionless ratio of the actual vapor pressure (p_w) to the saturation vapor pressure (e_w), usually expressed in percent, i.e.,

$$U_w = 100 p_w / e_w \quad (4)$$

At temperatures less than 0°C, the relative humidity is evaluated with respect to water, not ice [Li-71, p. 348].

5. Dew Point (or dew-point temperature)

T_d = the temperature to which a given parcel of air must be cooled at constant pressure and constant water-vapor content in order for saturation to occur. At the dew-point temperature the saturation vapor pressure of the parcel equals the actual vapor pressure of the contained water vapor.

Since most of our H_2O modeling is done in terms of mass-mixing ratios, we decided that the general technique should be one in which the user specifies tabular data in terms of either mass-mixing

ratios or quantities from which mass-mixing ratios can be computed by the code. The options selected are:

Option 1. Mass-Mixing Ratio. The user reads in values of the water-vapor mass-mixing ratio expressed in units of parts per million by mass (ppmm). For this option no further preprocessing is required.

Option 2. Absolute Humidity. The user reads in values of the absolute humidity, ρ_{H_2O} (grams H_2O/m^3). The desired values of mass-mixing ratio are computed from Equation (3b).

Option 3. Relative Humidity. The user reads in values of the relative humidity (in percent), U_w . The desired values of mass-mixing ratio are computed from the following steps:

- a. Compute saturated vapor pressure (over water), e_w (mb), from Subroutine H2OSVP.
- b. Compute vapor pressure from

$$p_w(\text{mb}) = 0.01 U_w e_w \quad (4a)$$

- c. Compute the absolute humidity from

$$\rho_{H_2O}(\text{g/m}^3) = \frac{10^9 p_w(\text{mb})}{(R/M_{H_2O})T} \quad (2c)$$

- d. Compute the mass-mixing ratio from Equation (3b).

Option 4. Dew Point. The user reads in values of the dew-point temperature (T_d). The desired values of the mass-mixing ratio are computed from the following steps:

- a. Compute the vapor pressure ($p_w(T_d)$), which equals the saturation vapor pressure ($e_w(T_d)$) at the dew-point temperature (T_d), by using Subroutine H2OSVP.
- b. Compute the absolute humidity from Equation (2c).
- c. Compute the mass-mixing ratio from Equation (3b).

Since most of our H_2O modeling is done in terms of mass-mixing ratio r_m (ppmm), the outputs from Subroutine SPCMIN (which are independent of the value of WVFLAG) can be derived as follows:

1. Water-Vapor Number Density ($[H_2O]$, molecules/cm³)

Compute the number density

$$[H_2O] = 10^{-6} r_m(\text{ppmm}) \rho_{\text{dry air}}(\text{g/cm}^3) N_A/M_{H_2O}. \quad (5)$$

2. Relative Humidity (U_w , percent)

- a. Compute vapor pressure ($p_w(\text{mb})$), from Equation (1b).
- b. Compute saturation vapor pressure ($e_w(\text{mb})$) by using Subroutine H2OSVP.
- c. Compute relative humidity (U_w) from Equation (4).

In the above discussion we have mentioned Subroutine H2OSVP several times. This subroutine computes the saturation vapor pressure of water vapor over a plane surface of (1) water for the temperature range from 173.15 to 373.15°K (-100 to +100°C) and (2) ice for the temperature range from 173.15 to 273.15°K (-100 to 0°C). Values of zero are returned for the parameters outside the indicated temperature ranges and a message is printed if the routine is called outside the indicated range.

The formula used for the water reference is a third degree polynomial given by Wexler [We-76, Equation (16b)] as an approximation to his Equation (15) for the natural logarithm of the vapor pressure (in Pascals) of water in the range from 0 to 100°C but used here also in the extrapolated region from 0 to -100°C. The basic formula for the ice reference is that given by Goff [Go-63a, Equation (5)]. However, to simplify the computation we have fitted a sixth-degree polynomial (EWDEI) to the ratio e_w/e_i , where e_i is the saturated vapor pressure over ice as given by Goff [Go-63a, Equation (5)], and compute e_i from the expression

$$e_i = e_w/\text{EWDEI}. \quad (6)$$

The input and output variables for Subroutines WVOPT and H2OSVP are given in Tables 4-24 and 4-25.

Table 4-24. Input and output variables for Subroutine WVOPT.

INPUT VARIABLES

Argument List

- JJ - Calculation flag
= 1, initialization call
= 2, normal operation call
- HKM - Altitude of interest (km) (used only if JJ = 2)

ATMOUP Common

- RHO - Air density (g/cm^3)
- TT - Temperature ($^{\circ}\text{K}$)

VPC Common

- METHOD - Flag indicating one of four options for treatment of water vapor
= 1, data values in parts per million by mass (ppmm)
= 2, data values in absolute humidity (g/m^3)
= 3, data values in relative humidity (percent; 10 percent is input as 10., not 0.10)
= 4, data values in dew-point temperature ($^{\circ}\text{K}$)

NOTE: For METHOD = 2,3,4, the subroutine converts the first NOP values of the data into parts per million by mass, during initialization.

DATA Read In

- HH(N) - Altitude array 0.0 to 120.0 km
- WVC(N) - H₂O data using one of the four options. For N=1,NOP, data have dimensions dictated by the option used. For N=NOP+1,NZH, data have dimensions of parts per million by mass. NOP=NZH is a valid input condition.

OUTPUT VARIABLE

Argument List

- H2OMR - Water vapor content of moist air in units of parts per million by mass at altitude HKM
-

Table 4-25. Input and output variables for Subroutine H2OSVP.

INPUT VARIABLES

Argument List

TEMP - Temperature ($^{\circ}$ K)

DATA Quantities

AA(I) - Coefficients in third-degree polynomial for $\text{EH20} = e_w$, given by Wexler [We-76, Equation (16b)]

BB(I) - Coefficients in sixth degree polynomial for EWDEI used to fit the ratio $\text{EH20/EICE} = e_w/e_i$, in the range from 0 to -100° C

OUTPUT VARIABLES

Argument List

EH20 - Saturation vapor pressure over water (millibar = 1000 dyne/cm² = 100 Pascal)

EICE - Saturation vapor pressure over ice (mb)

4-4 PLOTS OF MINOR NEUTRAL SPECIES PROFILES

Comparisons of the fit-function values with the data-base values [Volumes 14c and 14b] of minor species densities are given in Figures 4-4 through 4-20. Normally, circles and triangles are used to denote the data-base values for day and night conditions, respectively. Data-base values originally specified as mixing ratios [My-78] have been converted to particle number densities here so that all profiles would be in terms of number densities. Where the day and night values do not differ, only the circles are shown. The fit-function values, obtained from the sample problems for which the output is given in Section 6, are plotted as the solid curves for daytime conditions and dashed curves for the nighttime conditions. If the daytime and nighttime values do not differ, only the solid curves are shown. For those species with dependencies on local apparent time (t), geographical position (or latitude, L), fractional seasonal-year (f), or solar decimetric flux (F), the legends normally give the specific conditions, taken from the sample problems in Section 6.

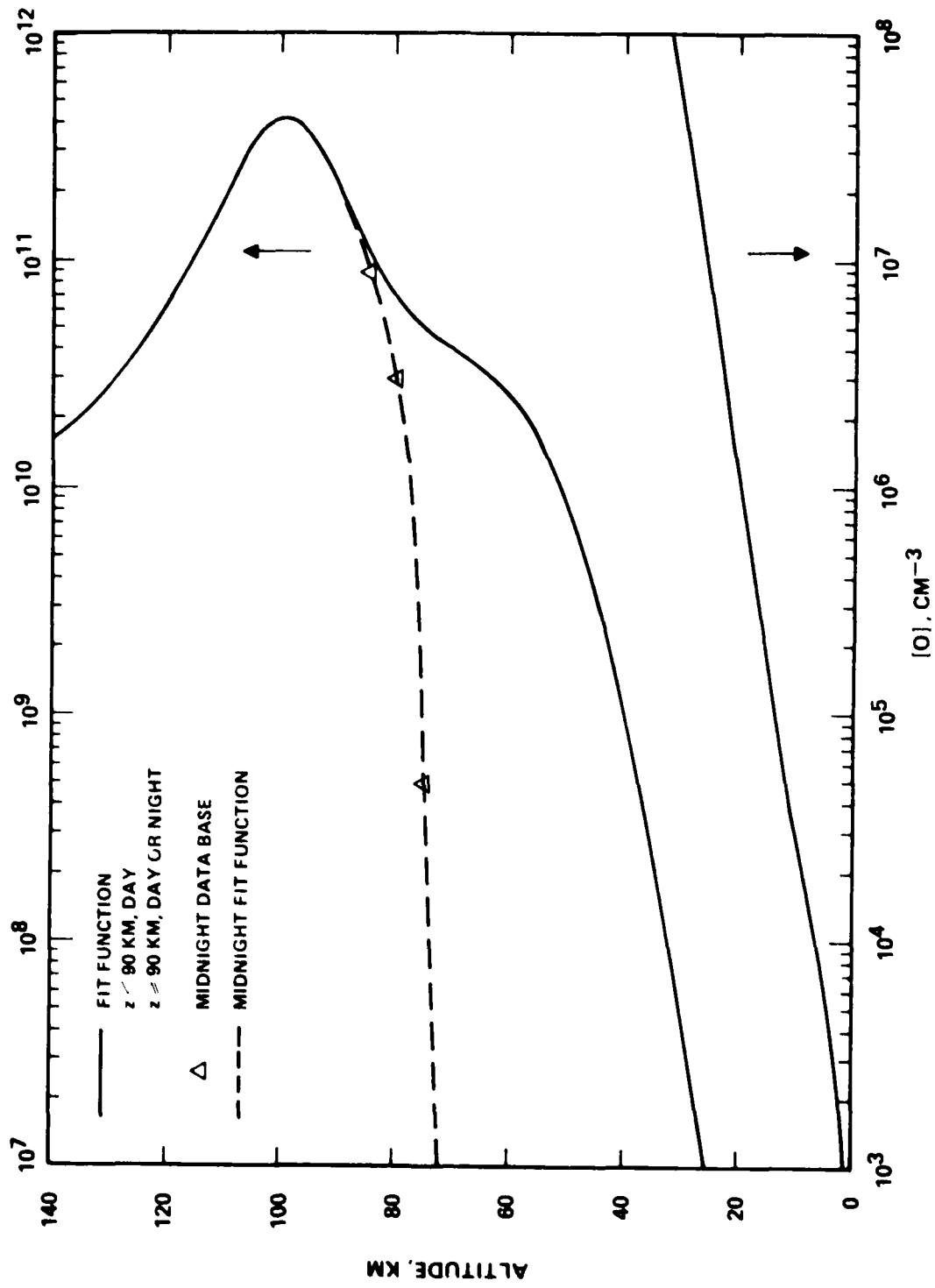


Figure 4-4. O density profile.

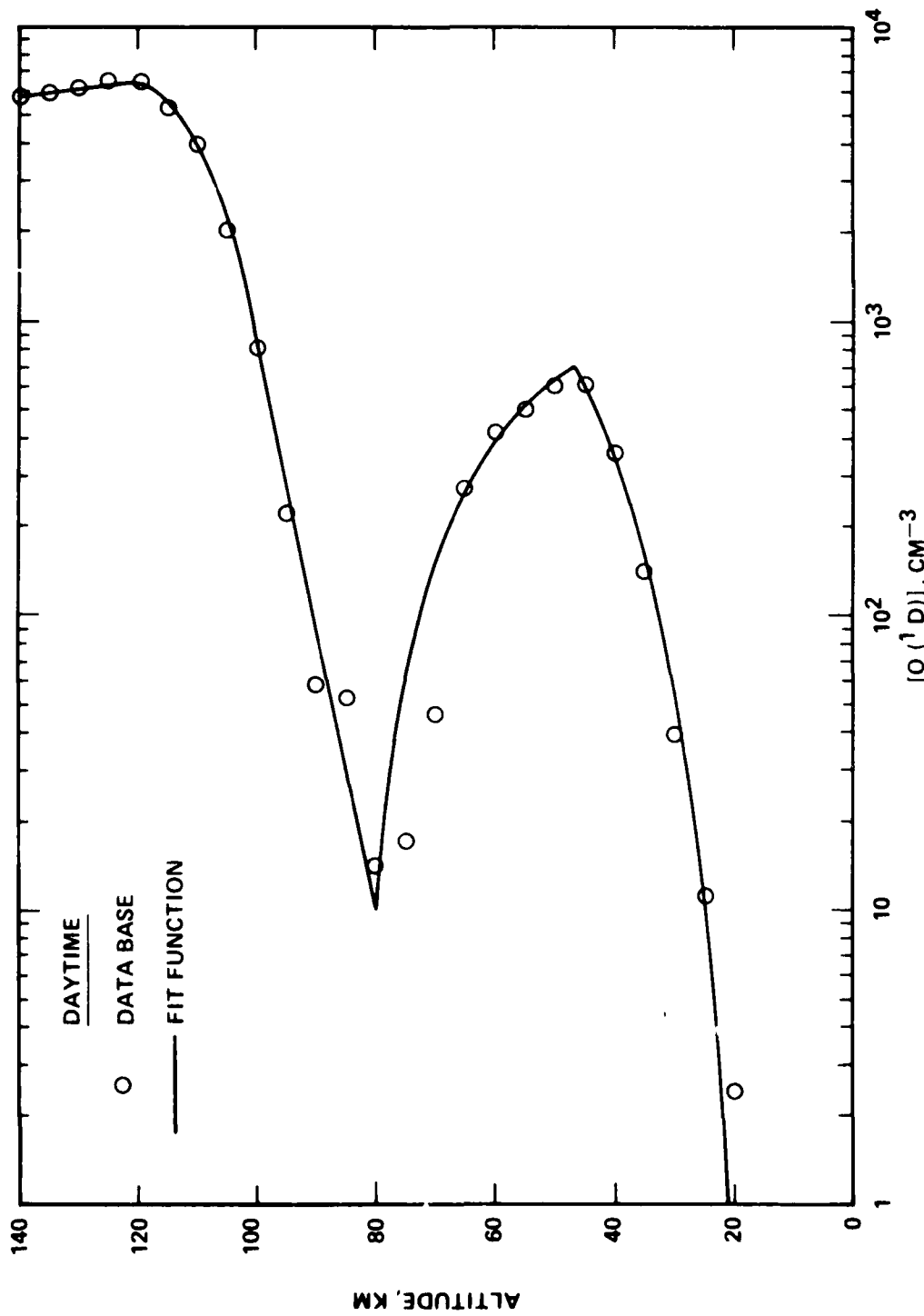


Figure 4-5. $O(^1D)$ density profile.

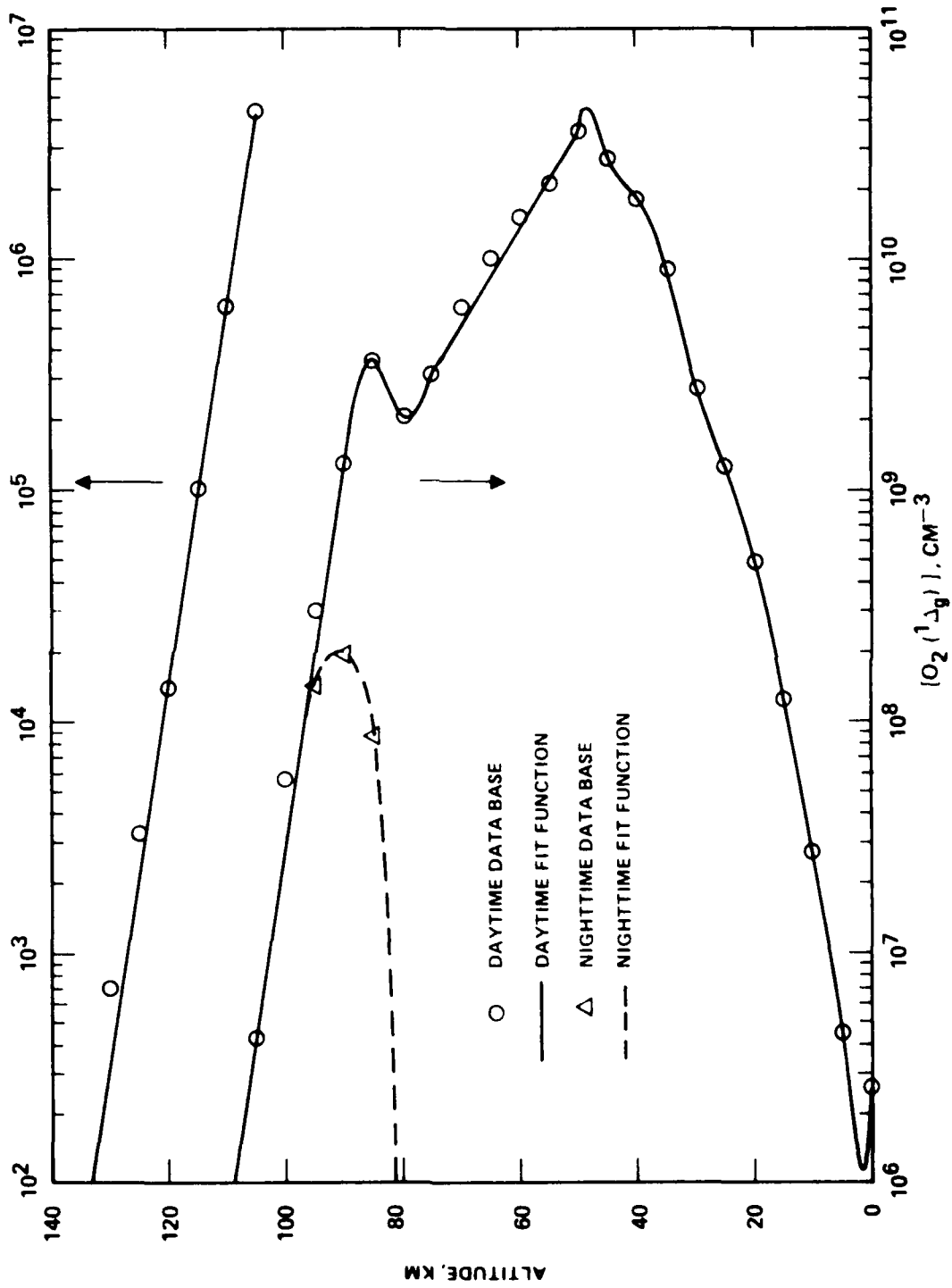


Figure 4-6. O_2 (l_g) density profile.

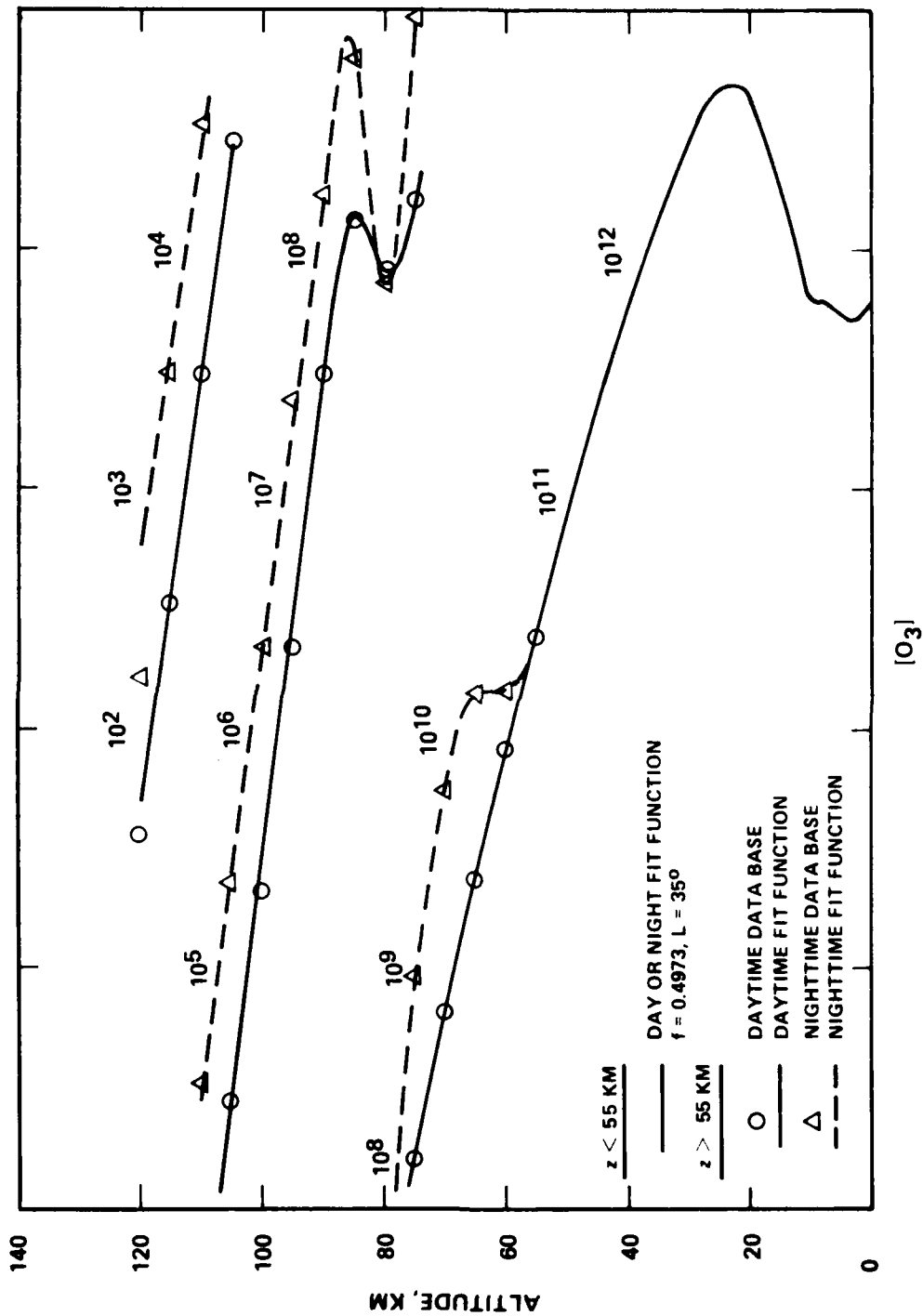


Figure 4-7. O₃ density profile.

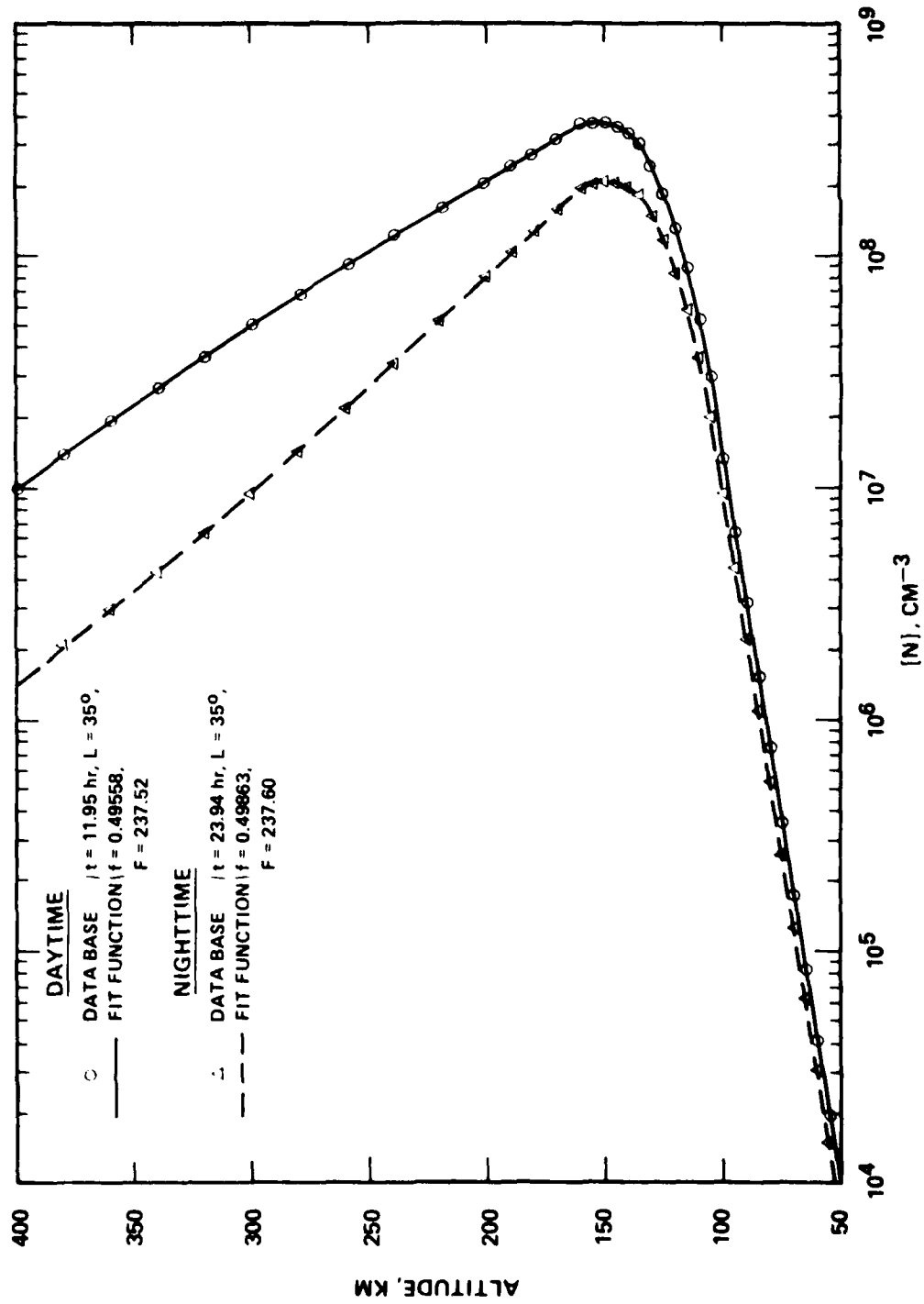


Figure 4-8. N density profile.

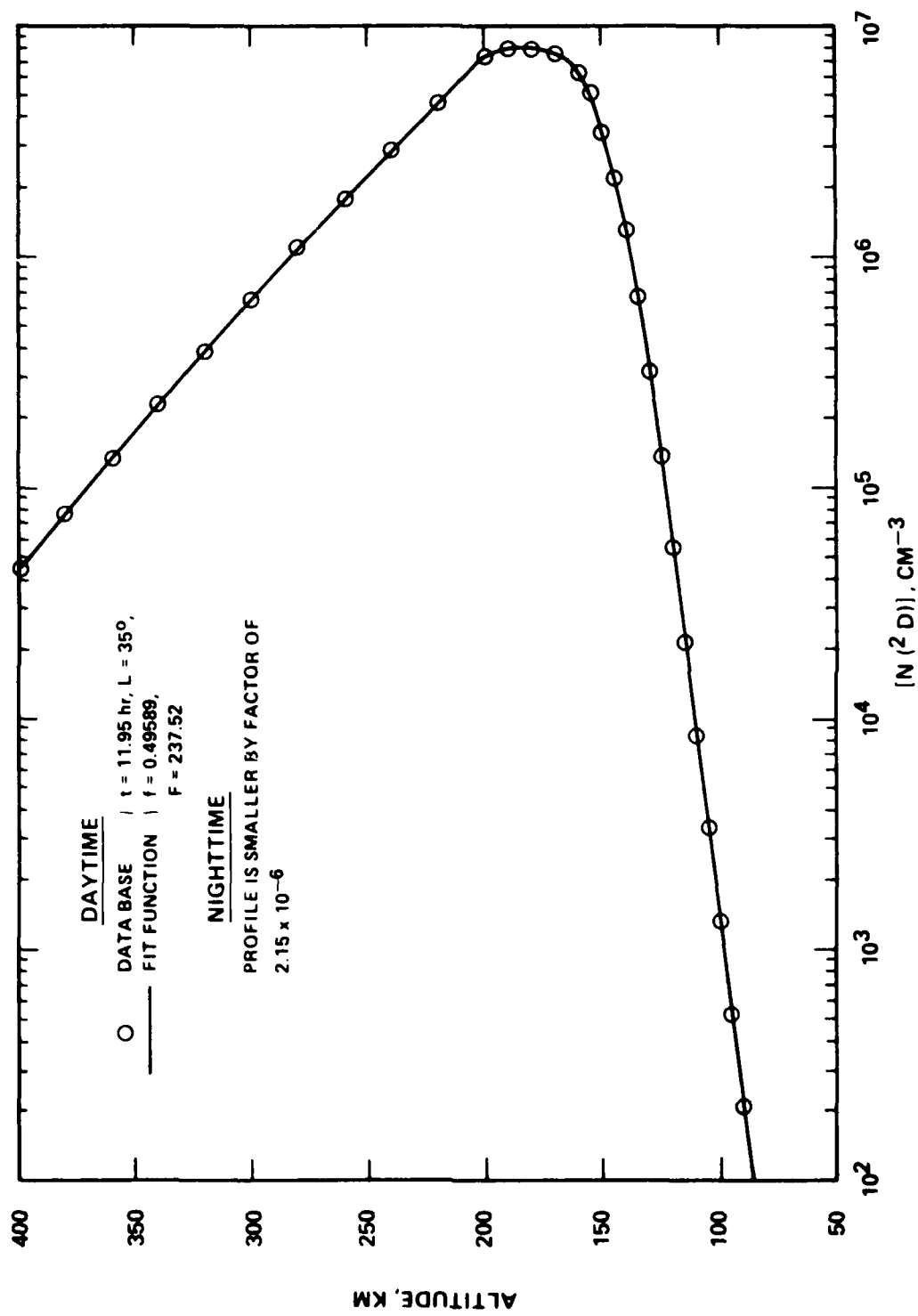


Figure 4-9. $N(2D)$ density profile.

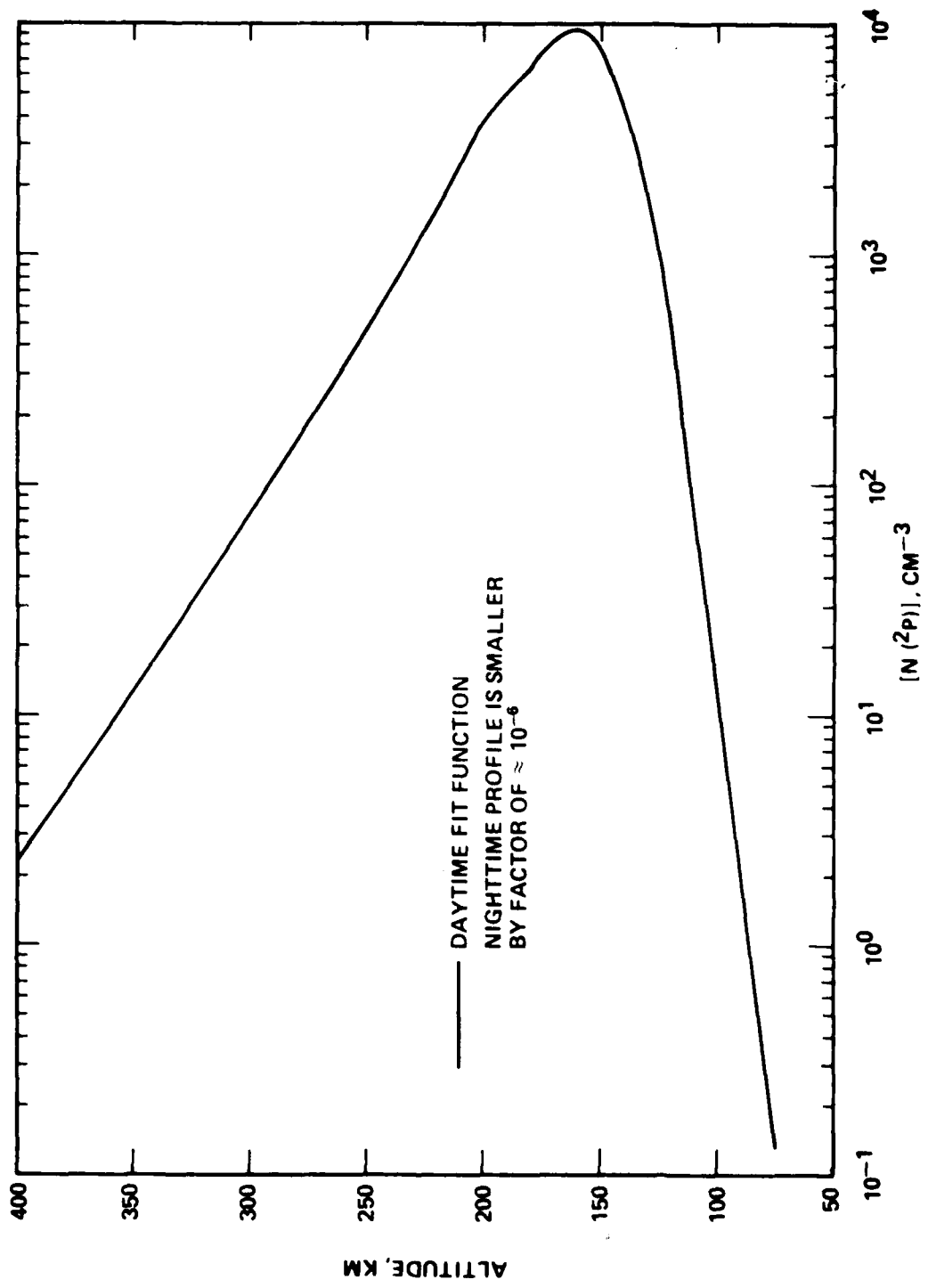


Figure 4-10. $N(2P)$ density profile.

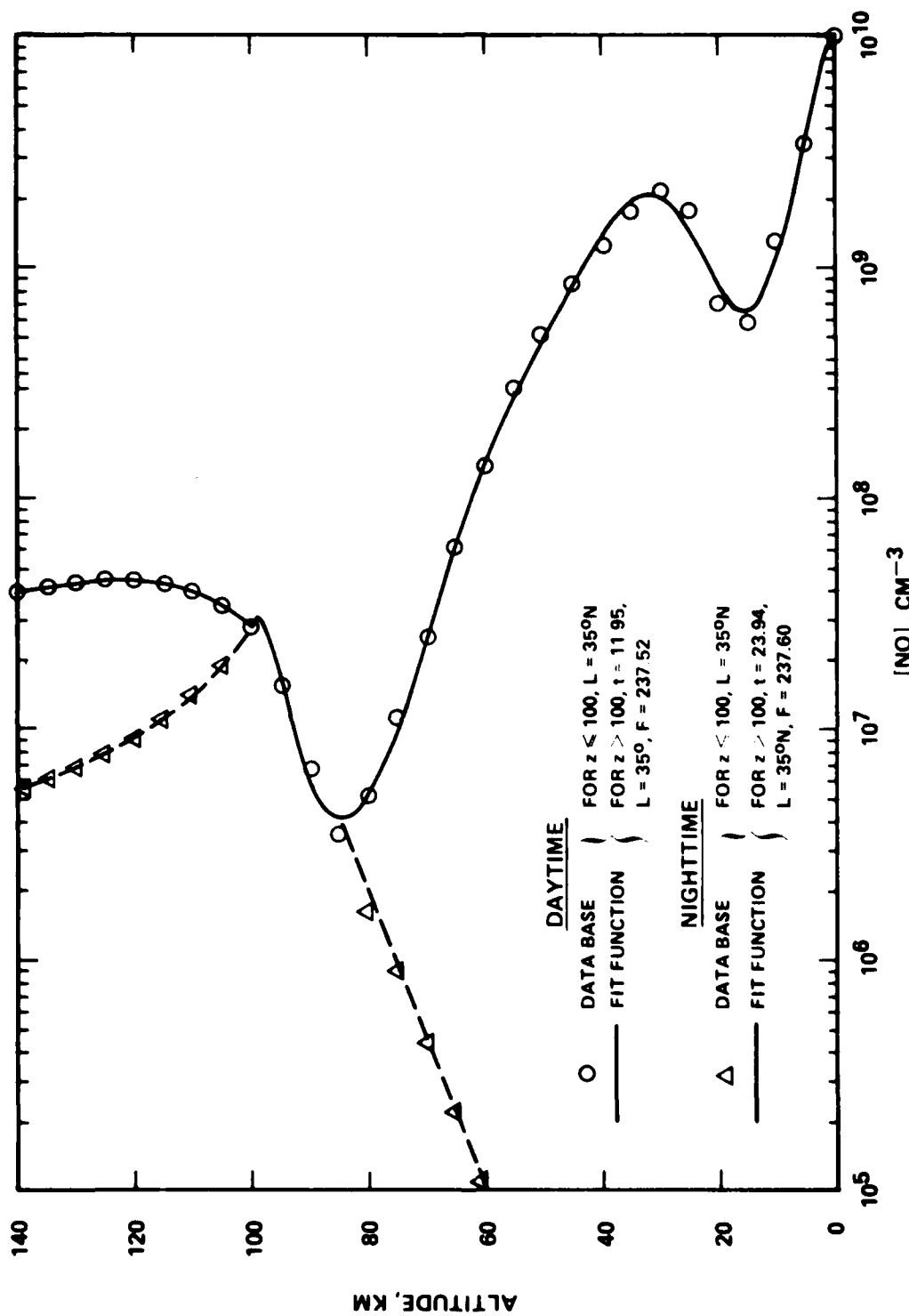


Figure 4-11. NO density profile.

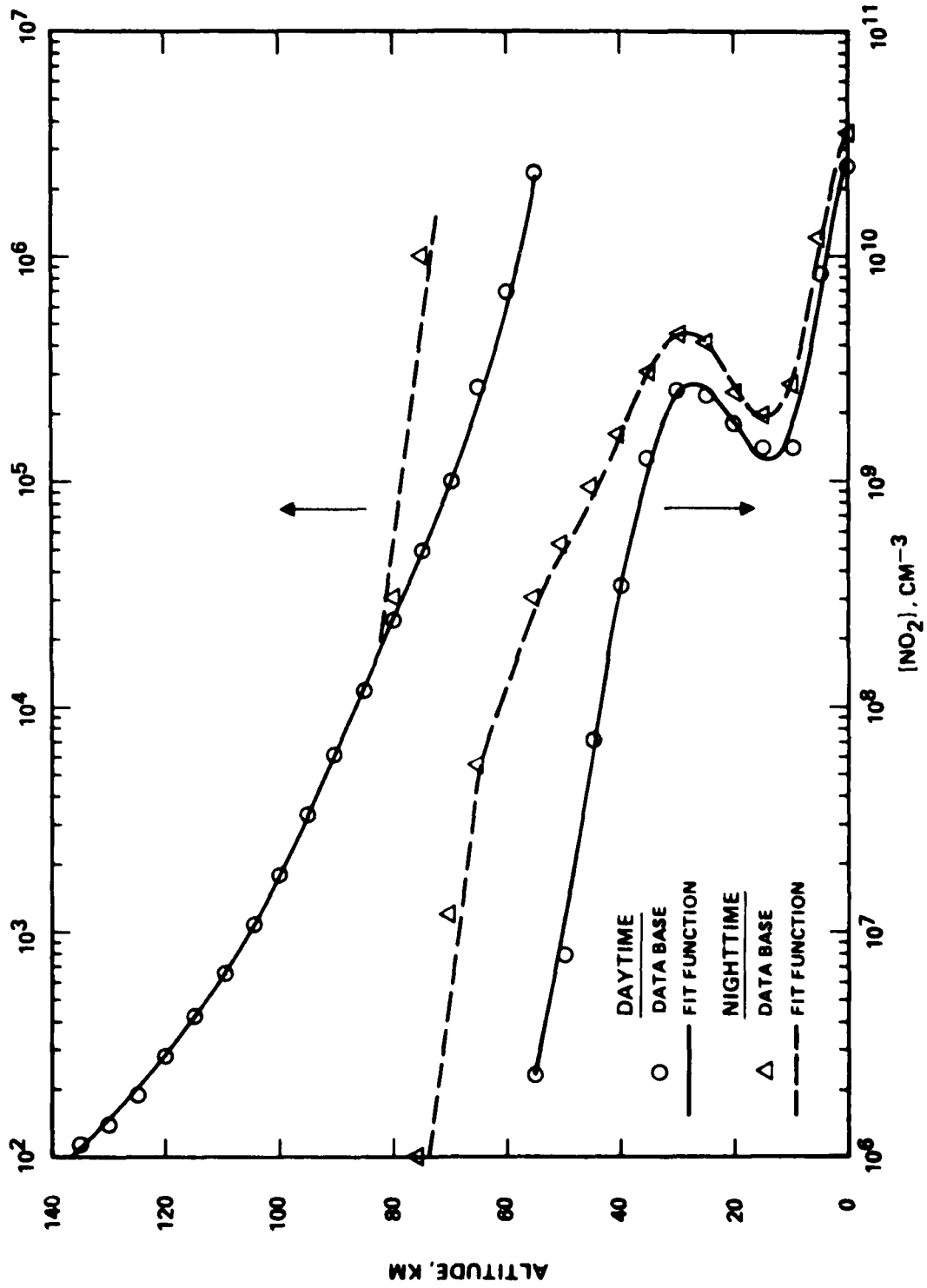


Figure 4-12. NO₂ density profile.

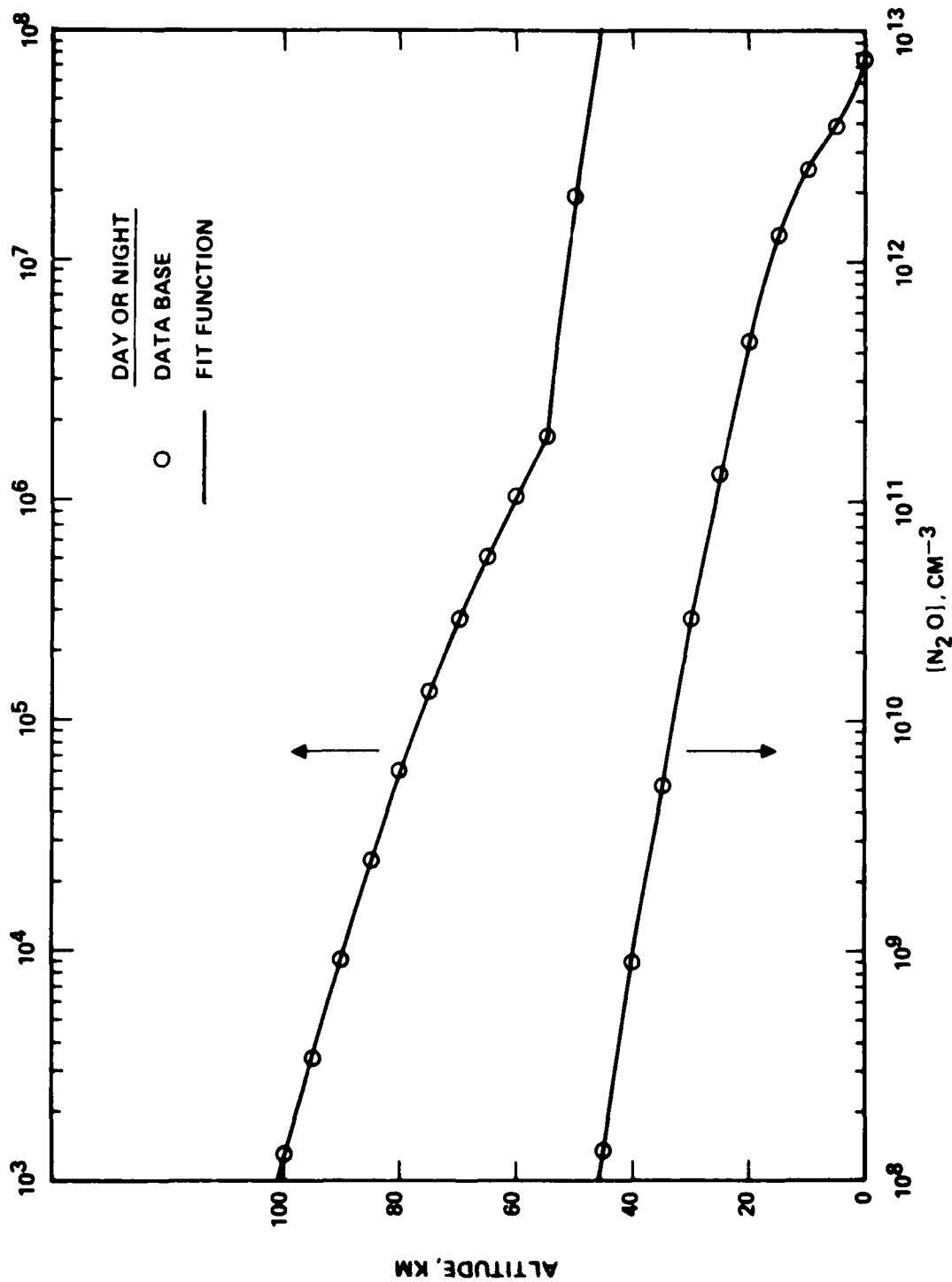


Figure 4-13. N₂O density profile.

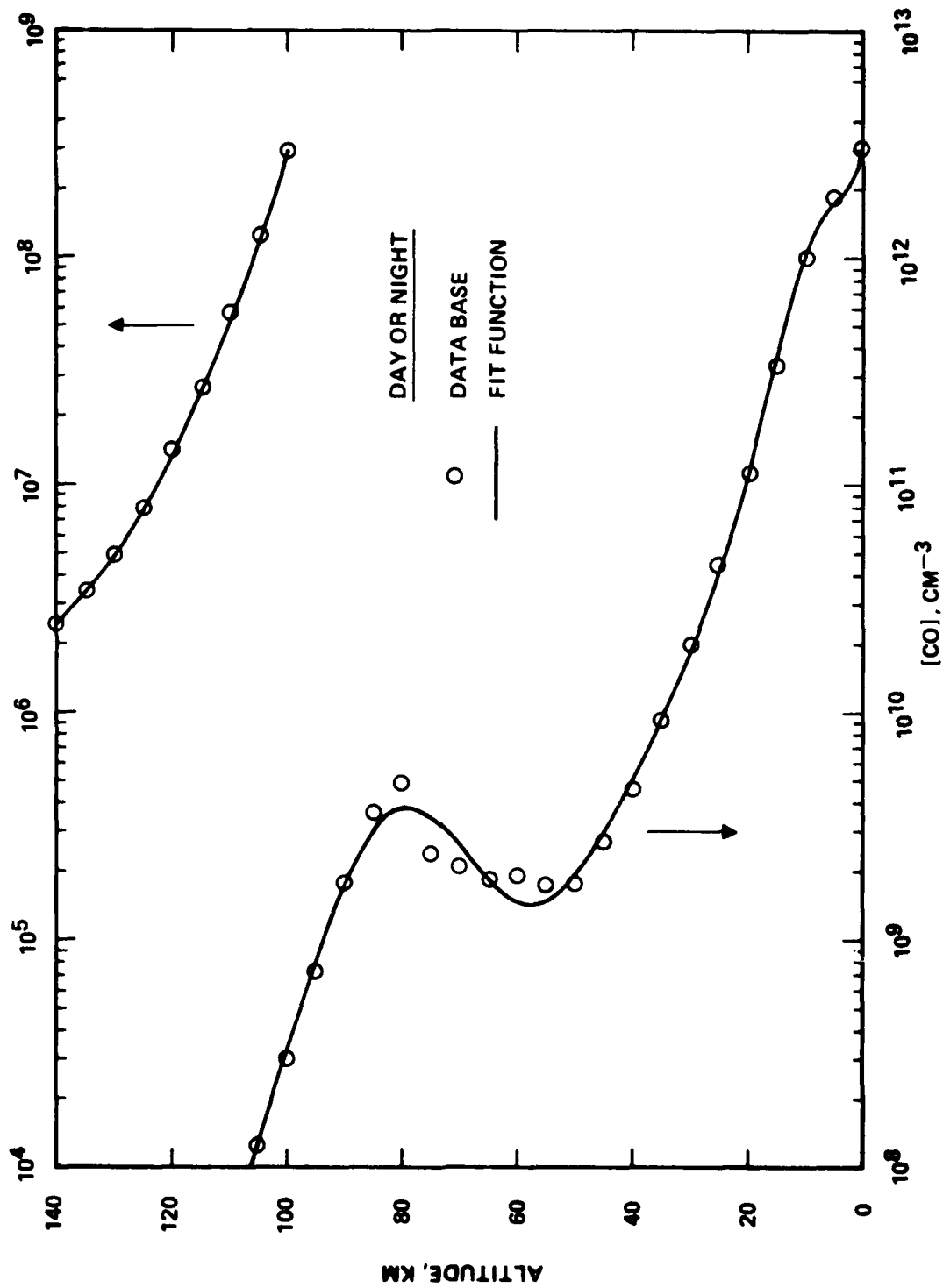


Figure 4-14. CO density profile.

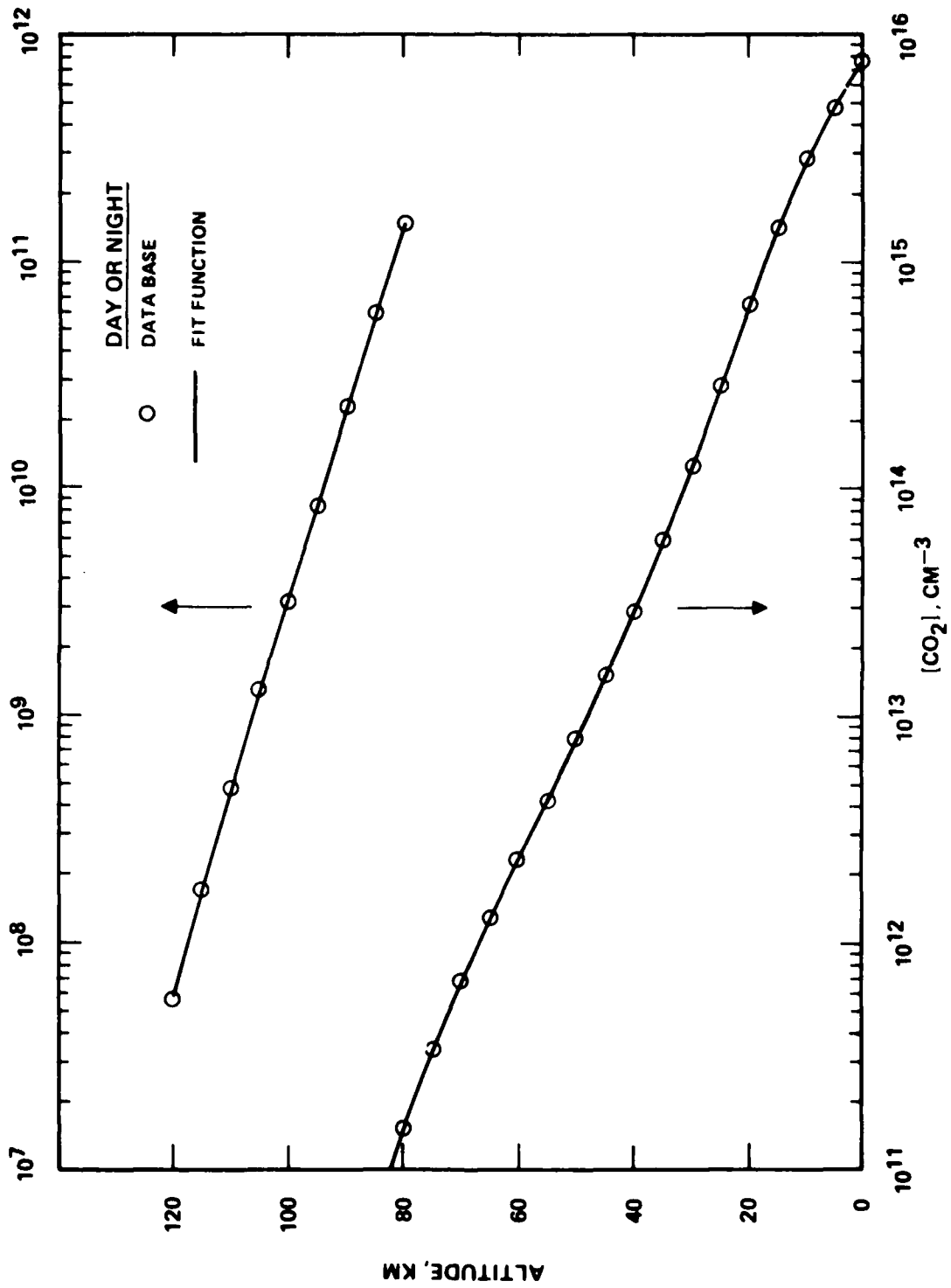


Figure 4-15. CO₂ density profile.

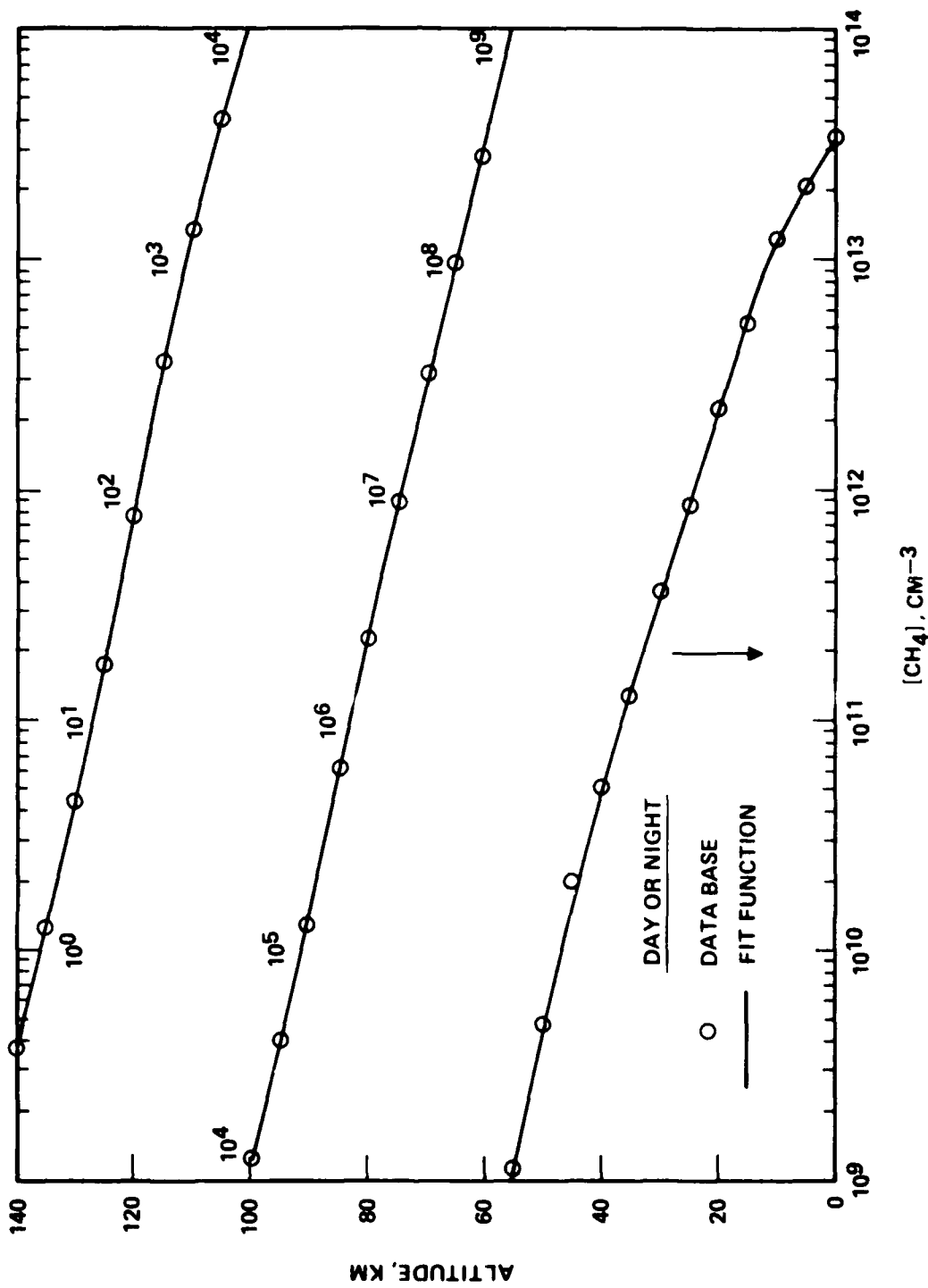
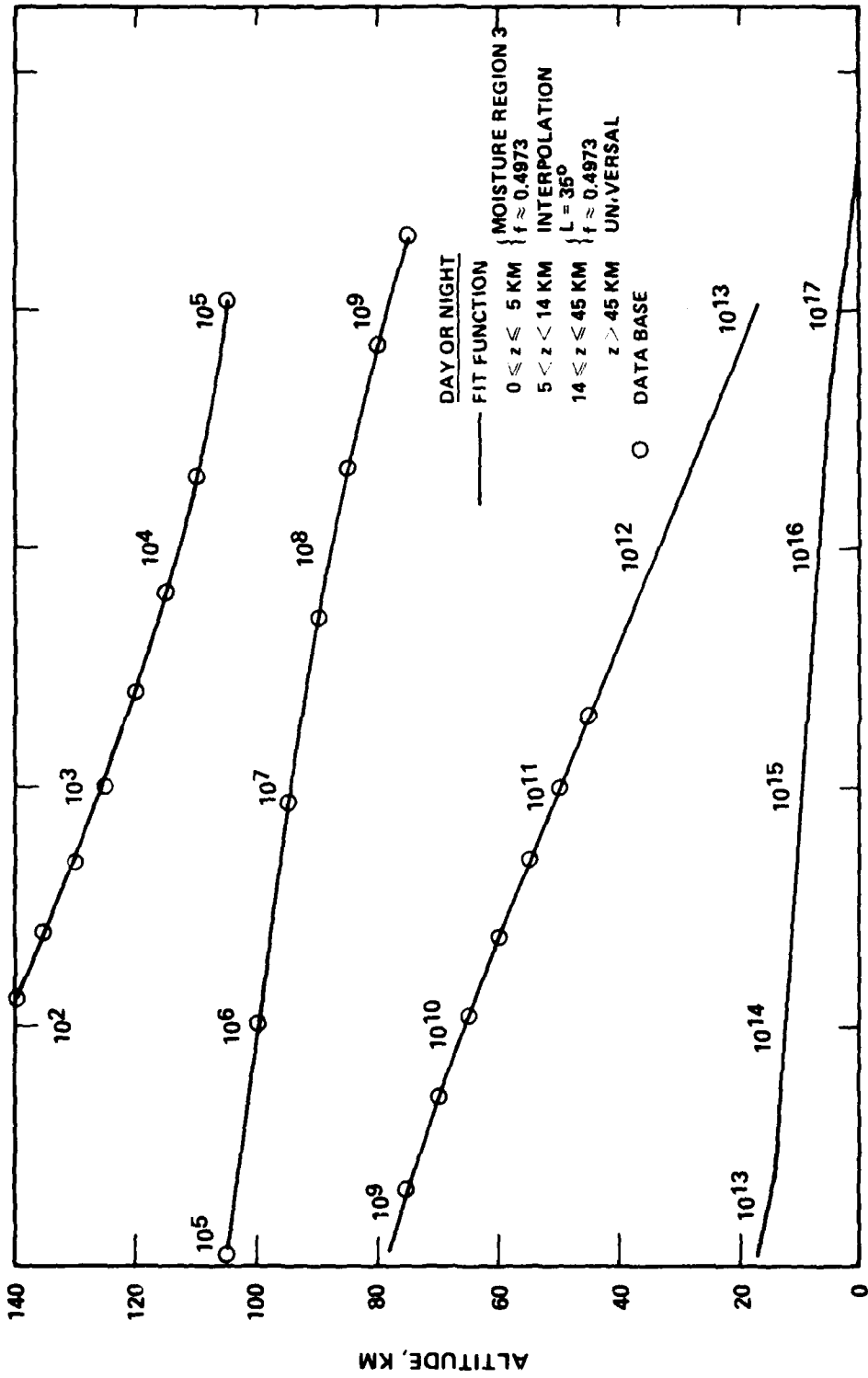


Figure 4-16. CH₄ density profile.



(H₂O). CM⁻³

Figure 4-17. H₂O density profile.

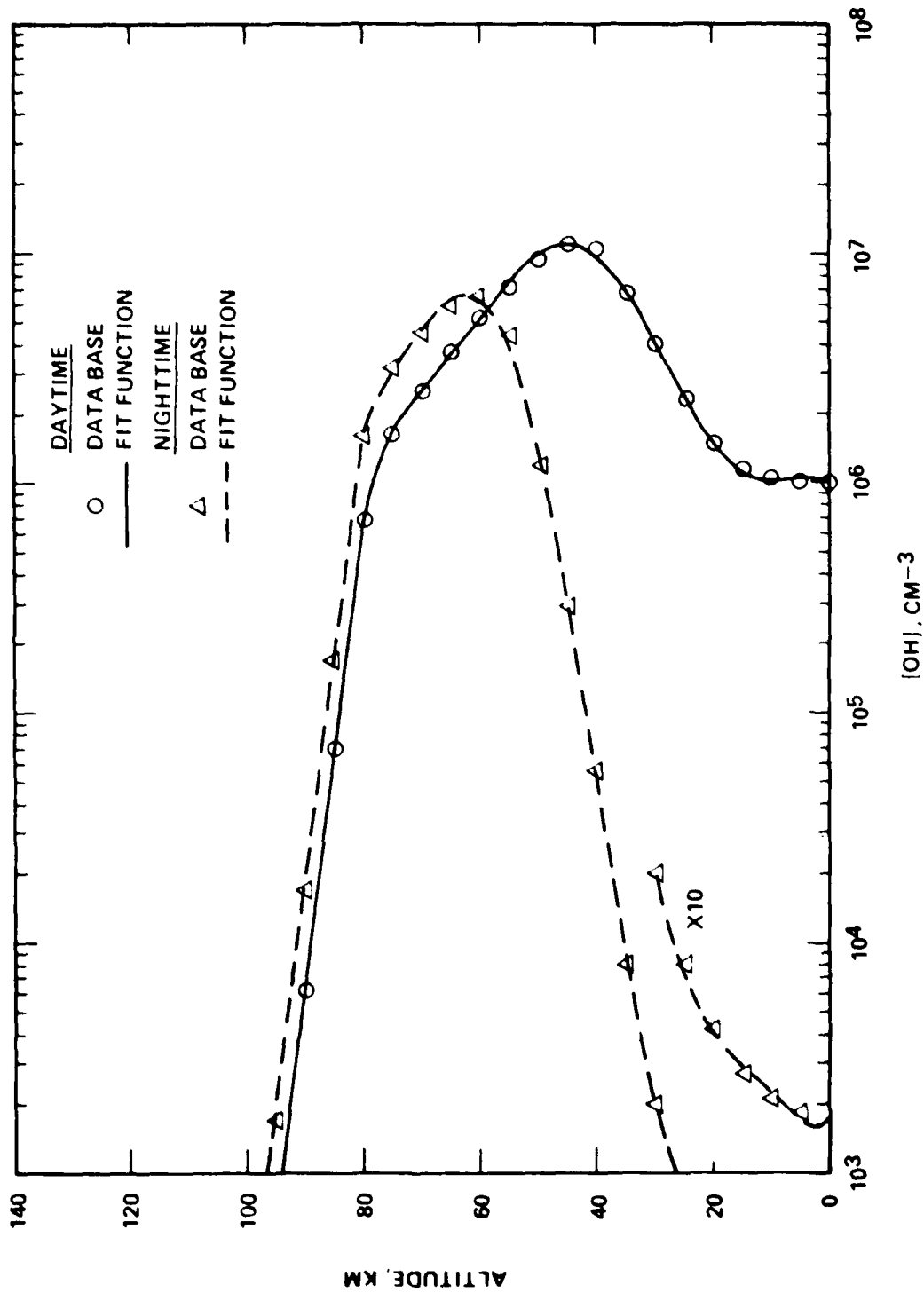


Figure 4-16. OH density profile.

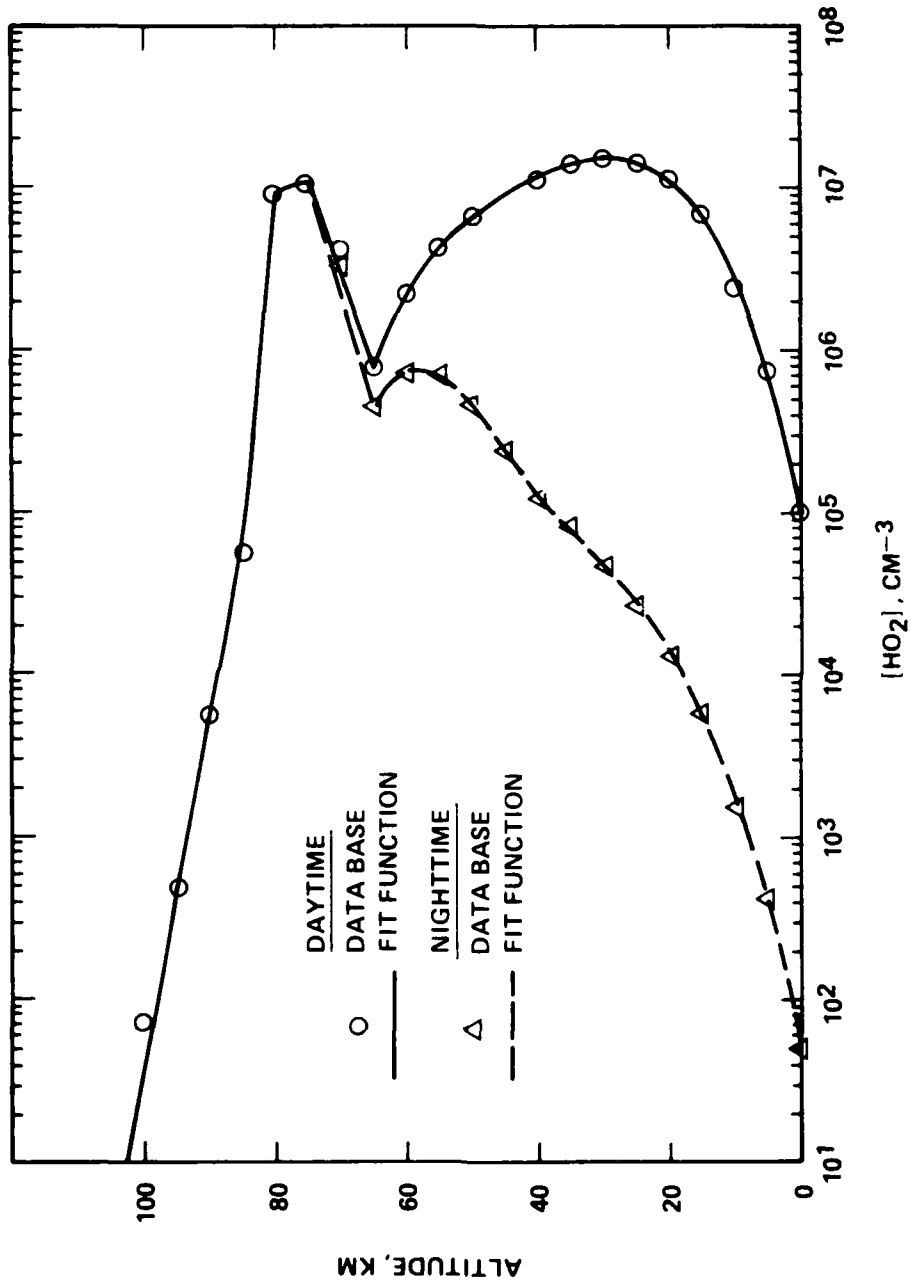


Figure 4-19. HO₂ density profile.

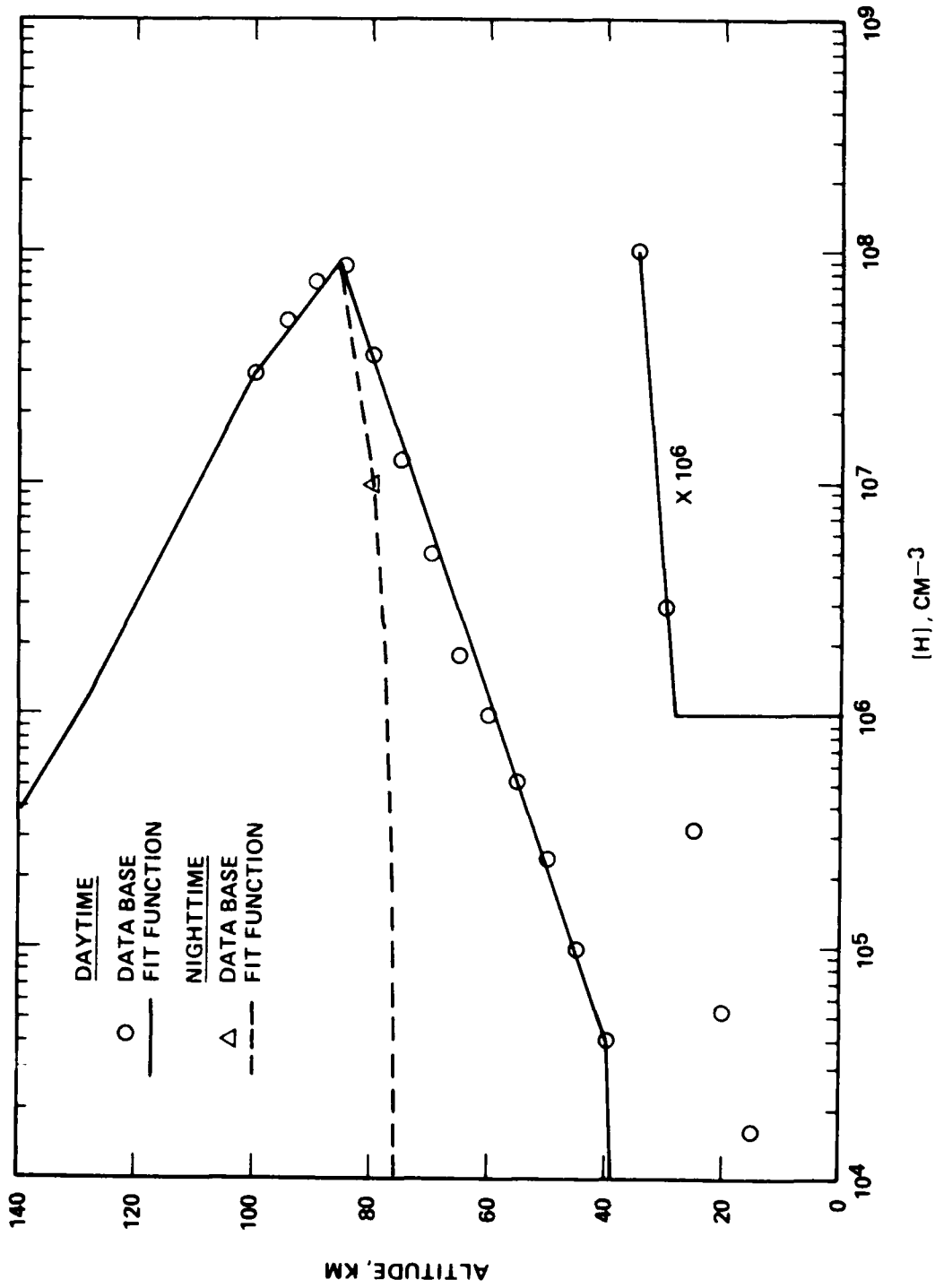


Figure 4-20. H density profile.

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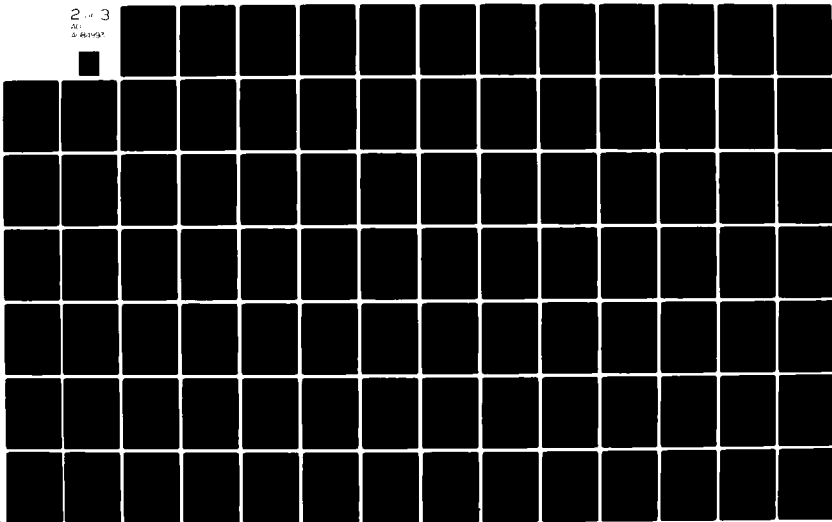
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JUN 79 D A HAMLIN, M R SCHOONOVER DNA001-76-C-0194
SAI-78-604-LJ-2A DNA-3964F-14A-1 NL

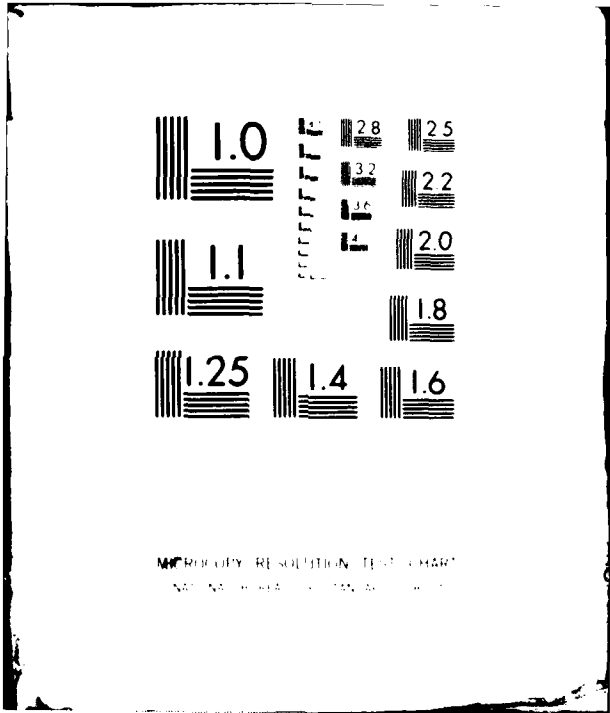
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SECTION 5

AMBIENT IONOSPHERE (SUBROUTINE IONOSU)

5-1 INTRODUCTION

Subroutine IONOSU provides the properties of the ambient ionosphere required by the chemistry modules. The quantities required for the E- and F-region ionospheric chemistry in ROSCOE-IR are obtained by a natural extension of the method used for ROSCOE-Radar (see Volume 14a, pages 67-74). The principal change is from the generic molecular ion M^+ to NO^+ , N_2^+ , and O_2^+ . There is no change in the requirements of the D-region chemistry module for ionospheric properties.

See Table 5-1 for a summary of inputs and outputs for Subroutine IONOSU.

5-2 E- AND F-REGION IONOSPHERIC PROPERTIES

The E- and F-region chemistry module requires the following quantities:

- a. q , the effective total ion-production rate that reproduces the ambient ionosphere when used with the chemistry model ($\text{cm}^{-3} \text{sec}^{-1}$)
- b. O^+ , the positive atomic-ion density (cm^{-3})
- c. NO^+ , the NO^+ molecular-ion density (cm^{-3})
- d. N_2^+ , the N_2^+ molecular-ion density (cm^{-3})
- e. O_2^+ , the O_2^+ molecular-ion density (cm^{-3})
- f. T_x , the electron (and N_2 vibration) temperature ($^{\circ}K$).

The E- and F-region ionospheric chemistry equations, which are a natural extension of the pair of equations used for ROSCOE-Radar (Volume 14a, Section 5, Equations (1) and (2)), are

Table 5-1. Input and output variables for Subroutine IONOSU.

INPUT VARIABLES

Argument List

- JJ - Calculation flag
 If { JJ=1: calculate initialization parameters
 JJ=2: calculate ionospheric properties
- ZH - Altitude of interest (km)

ATMOUP Common

- IDORN - Parameter for day or night. If COSCHI is the cosine of the zenith angle of the sun at point P, IDORN is 1 for daytime, i.e., IF(COSCHI.GE.0.0), and is -1 for nighttime, i.e., IF(COSCHI.LT.0.0)
- SNI(1) - N₂ concentration (1/cm³)
- SNI(2) - O₂ concentration (1/cm³)
- SNI(3) - O concentration (1/cm³)
- SNI(7) - N concentration (1/cm³)
- SNI(8) - NO concentration (1/cm³)
- TT - Heavy-particle temperature (°K)

ALTODN Common

- ALTKM(47)- The array of altitudes at which minor species are specified as data in SPCMIN

RATCOF Function Routine

Reaction rate coefficients for chemical reactions

DATA

- HEBOTD - Altitude below which the daytime electron density decreases exponentially and above which the logarithm of the daytime electron density increases parabolically (km)
- EBOTD - Daytime electron density at altitude HEBOTD (1/cm³)
- HF2MXD - Altitude at which the maximum daytime electron density occurs (km)

(Continued)

Table 5-1. (Cont'd)

| | |
|-----------|---|
| EF2MXD | - Daytime electron density at altitude HF2MXD (1/cm ³) |
| EDDSCH | - Scale height with which the daytime electron density decreases below altitude HEBOTD (km) |
| F2DSCH | - Scale height with which the daytime electron density decreases above altitude HF2MXD |
| HEBOTN | - Altitude below which the nighttime electron density decreases exponentially and above which the logarithm of the nighttime electron density increases sinusoidally (km) |
| EBOTN | - Nighttime electron density at altitude HEBOTN (1/cm ³) |
| HF2MXN | - Altitude at which the maximum nighttime electron density occurs (km) |
| EF2MXN | - Nighttime electron density at altitude HF2MXN (1/cm ³) |
| EDNSCH | - Scale height with which the nighttime electron density decreases below altitude HEBOTN (km) |
| F2NSCH | - Scale height with which the nighttime electron density decreases above altitude HF2MXN |
| TXT120 | - The difference between the electron temperature and the gas temperature at 120-km altitude in the ambient daytime ionosphere (°K) |
| TXT200 | - The difference between the electron temperature and the gas temperature at 200-km altitude in the ambient daytime ionosphere (°K) |
| TXT800 | - The difference between the electron temperature and the gas temperature at 800-km altitude in the ambient daytime ionosphere (°K) |
| DQDAY(18) | - The effective total ion-production rate at altitudes 0(5)85 km that reproduces the ambient daytime D-region ionosphere when used with the chemistry model (ion pairs/[cm ³ sec]) |
| DQNIT(18) | - The effective total ion-production rate at altitudes 0(5)85 km that reproduces the ambient nighttime D-region ionosphere when used with the chemistry model (ion pairs/[cm ³ sec]) |

(Continued)

Table 5-1. (Cont'd)

OUTPUT VARIABLES

ATMOUP Common

- SNI(9) - Electron concentration for $ZH \geq 90$ km ($1/\text{cm}^3$)
- SNI(10) - O^+ concentration for $ZH \geq 90$ km ($1/\text{cm}^3$)
- SNI(11) - NO^+ concentration for $ZH \geq 90$ km ($1/\text{cm}^3$)
- SNI(12) - Electron (and N_2 vibration) temperature ($^{\circ}K$)
- SNI(28) - N_2^+ concentration for $ZH \geq 90$ km ($1/\text{cm}^3$)
- SNI(29) - O_2^+ concentration for $ZH \geq 90$ km ($1/\text{cm}^3$)

IONOUP Common

- EFE - See SNI(9) above
 - EFOP - See SNI(10) above
 - EFNOP - See SNI(11) above
 - EFN2P - See SNI(28) above
 - EFO2P - See SNI(29) above
 - TX - See SNI(12) above
 - QDEF - The effective total ion-production rate that reproduces the ambient ionosphere when used with the chemistry model
-

$$[\dot{O}^+] = q_1 - \beta_{11}[O^+] - \alpha_1[O^+][e] \quad (1)$$

$$[\dot{NO}^+] = q_2 + \beta_{21}[O^+] + \beta_{23}[N_2^+] + \beta_{24}[O_2^+] - \alpha_2[NO^+][e] \quad (2)$$

$$[\dot{N}_2^+] = q_3 - \beta_{33}[N_2^+] - \alpha_3[N_2^+][e] \quad (3)$$

$$[\dot{O}_2^+] = q_4 + \beta_{41}[O^+] - \beta_{44}[O_2^+] - \alpha_4[O_2^+][e] \quad (4)$$

$$[e] = [O^+] + [NO^+] + [N_2^+] + [O_2^+] \quad (5)$$

$$q_i = \gamma_i q \quad (6a)$$

$$\sum_{i=1}^4 \gamma_i = 1 \quad (6b)$$

$$\gamma_i = A_i / \sum_{i=1}^4 A_i \quad (7)$$

$$A_1 = [O] \quad (8a)$$

$$A_2 = 2[NO] \quad (8b)$$

$$A_3 = 2[N_2] \quad (8c)$$

$$A_4 = 2[O_2] \quad (8d)$$

The assumed reactions and rate coefficients are given in Table 5-2. The rate coefficients are supplied to Subroutine IONOSU by Function RATCOF.

In the above equations, the quantities are defined as follows:

$$[O^+] = O^+ \text{ atomic-ion density (cm}^{-3}\text{)}$$

$$[NO^+] = NO^+ \text{ molecular-ion density (cm}^{-3}\text{)}$$

$$[N_2^+] = N_2^+ \text{ molecular-ion density (cm}^{-3}\text{)}$$

Table 5-2. E- and R-region ionospheric chemistry reactions and rate coefficients.

| Reaction Number | | Reaction | Rate Coefficient ^{a, b} |
|-----------------|-------|---|--|
| Here | SO-76 | | |
| 10 | -- | $O^+ \rightarrow O + h\nu$ | } ^c |
| 11 | -- | $O^+ + e + e \rightarrow O + e$ | |
| 2a | R6 | $NO^+ + e \rightarrow N(^4S) + O$ | $3.5 \times 10^{-7} (T_e/380)^{-0.5}$ |
| 2b | R5 | $NO^+ + e \rightarrow N(^2D) + O$ | $3.5 \times 10^{-7} (T_e/380)^{-0.5}$ |
| 3 | R3 | $N_2^+ + e \rightarrow N(^4S) + N(^2D)$ | $2.9 \times 10^{-7} (T_e/300)^{-0.33}$ |
| 4 | R20 | $O_2^+ + e \rightarrow O + (O^1D)$ | $2.2 \times 10^{-7} (300/T_e)^{0.9}$ |
| 5 | R2 | $O^+ + N_2 \rightarrow NO^+ + N(^4S)$ | $\begin{cases} 6 \times 10^{-13} & T_i \geq 600^\circ K \\ 6 \times 10^{-13} & (600/T_i), T_i < 600 \end{cases}$ |
| 6 | R21 | $O^+ + O_2 \rightarrow O_2^+ + O$ | $2.0 \times 10^{-11} (T_i/300)^{-0.4}$ |
| 7 | R4 | $N_2^+ + O \rightarrow NO^+ + N(^2D)$ | $2.5 \times 10^{-10} (300/T_i)^{0.44}$ |
| 8 | R8 | $O_2^+ + N(^4S) \rightarrow NO^+ + O$ | 1.8×10^{-10} |
| 9 | R9 | $O_2^+ + NO \rightarrow NO^+ + O_2$ | 6.3×10^{-10} |

^a In units of cm^3/sec for two-body reactions and cm^6/sec for three-body reactions.

^b From SO-76 (Strobel et al.) except for our reaction numbers 10 and 11 taken from BLKCHM in ROSCOE-Radar.

^c α_1 is given by: $\alpha_1 = C_{10} + C_{11}[e] + 1.5 \times 10^{-7} [e]^2/T_e^3$
 C_{10} = radiative recombination rate coefficient for the reaction $O^+ + e \rightarrow O + h\nu$
 $= 4.4 \times 10^{-12} (T_e/300)^{-0.75}$
 C_{11} = collisional-radiative recombination rate coefficient for the reaction $O^+ + e + e \rightarrow O + e$
 $= 1.2 \times 10^{-19} (T_e/300)^{-5.0}$

- $[O_2^+]$ = O_2^+ molecular-ion density (cm^{-3})
 q = total ion-production rate ($\text{cm}^{-3} \text{sec}^{-1}$)
 q_1 = O^+ -ion production rate ($\text{cm}^{-3} \text{sec}^{-1}$)
 q_2, q_3, q_4 = NO^+ -, N_2^+ -, O_2^+ -ion production rate ($\text{cm}^{-3} \text{sec}^{-1}$)
 β_{11} = $C_5[N_2] + C_6[O_2] = \beta_{21} + \beta_{41}$
 β_{21} = $C_5[N_2]$
 C_5 = ion-molecule interchange rate coefficient (cm^3/sec)
 C_6 = ion-molecule charge-exchange rate coefficient (cm^3/sec)
 β_{23} = $C_7[O]$
 β_{24} = $C_8[N] + C_9[NO]$
 β_{33} = $C_7[O] = \beta_{23}$
 β_{41} = $C_6[O_2]$
 β_{44} = $C_8[N] + C_9[NO] = \beta_{24}$
 α_1 = C_1 (corresponds to α_r in ROSCOE-Radar)
 = effective two-body collisional-radiative recombination rate coefficient for atomic ions (cm^3/sec) [KJ-74b]
 α_2 = C_2
 = dissociative recombination rate coefficient for the reaction $NO^+ + e \rightarrow \text{products}$ (cm^3/sec)
 α_3 = C_3
 = dissociative recombination rate coefficient for the reaction $N_2^+ + e \rightarrow N(^4S) + N(^2D)$ (cm^3/sec)
 α_4 = C_4
 = dissociative recombination rate coefficient for the reaction $O_2^+ + e \rightarrow O + O(^1D)$

Assume steady-state conditions. After putting Equation (6) into Equations (1) through (4), we have

$$\gamma_1 q - \beta_{11}[O^+] - \alpha_1[O^+][e] = 0 \quad (9)$$

$$\gamma_2 q + \beta_{21}[O^+] + \beta_{23}[N_2^+] + \beta_{24}[O_2^+] - \alpha_2[NO^+][e] = 0 \quad (10)$$

$$\gamma_3 q - \beta_{33}[N_2^+] - \alpha_3[N_2^+][e] = 0 \quad (11)$$

$$\gamma_4 q + \beta_{41}[O^+] - \beta_{44}[O_2^+] - \alpha_4[O_2^+][e] = 0. \quad (12)$$

By regarding $[e]$ as known, we have five equations ((5), (9), (10), (11) and (12)) in five unknowns (q , $[O^+]$, $[NO^+]$, $[N_2^+]$, and $[O_2^+]$). Rewrite Equations (9) through (12) for $[X^+][e]$ and add, followed by use of Equation (5):

$$[O^+][e] = \{\gamma_1 q - \beta_{11}[O^+]\}/\alpha_1$$

$$[NO^+][e] = \{\gamma_2 q + \beta_{21}[O^+] + \beta_{23}[N_2^+] + \beta_{24}[O_2^+]\}/\alpha_2$$

$$[N_2^+][e] = \{\gamma_3 q - \beta_{33}[N_2^+]\}/\alpha_3$$

$$[O_2^+][e] = \{\gamma_4 q + \beta_{41}[O^+] - \beta_{44}[O_2^+]\}/\alpha_4$$

$$[e]^2 = A'q + B'[O^+] + C'[N_2^+] + D'[O_2^+] \quad (13)$$

with

$$A' = \gamma_1/\alpha_1 + \gamma_2/\alpha_2 + \gamma_3/\alpha_3 + \gamma_4/\alpha_4 \quad (14a)$$

$$B' = -\beta_{11}/\alpha_1 + \beta_{21}/\alpha_2 + \beta_{41}/\alpha_4 = \beta_{21}\left(\frac{1}{\alpha_2} - \frac{1}{\alpha_1}\right) + \beta_{41}\left(\frac{1}{\alpha_4} - \frac{1}{\alpha_1}\right) \quad (14b)$$

$$C' = \beta_{23}/\alpha_2 - \beta_{33}/\alpha_3 = \beta_{23}\left(\frac{1}{\alpha_2} - \frac{1}{\alpha_3}\right) \quad (14c)$$

$$D' = \beta_{24}/\alpha_2 - \beta_{44}/\alpha_4 = \beta_{24} \left(\frac{1}{\alpha_2} - \frac{1}{\alpha_4} \right). \quad (14d)$$

Solve Equations (11) and (12) for $[N_2^+]$ and $[O_2^+]$ and put into Equation (13).

$$[N_2^+] = \gamma_3 q / \{\beta_{33} + \alpha_3 [e]\} \quad (15)$$

$$[O_2^+] = \{\gamma_4 q + \beta_{41} [O^+]\} / \{\beta_{44} + \alpha_4 [e]\} \quad (16)$$

$$\begin{aligned} [e]^2 &= A'q + B'[O^+] + C'\gamma_3 q / \{\beta_{33} + \alpha_3 [e]\} \\ &\quad + D'\{\gamma_4 q + \beta_{41} [O^+]\} / \{\beta_{44} + \alpha_4 [e]\} \\ &= (A' + C'\gamma_3 / \{\beta_{33} + \alpha_3 [e]\} + D'\gamma_4 / \{\beta_{44} + \alpha_4 [e]\})q \\ &\quad + (B' + D'\beta_{41} / \{\beta_{44} + \alpha_4 [e]\}) [O^+]. \end{aligned} \quad (17)$$

Eliminate $[O^+]$ from Equation (17) by use of $[O^+]$ from Equation (9):

$$[O^+] = \gamma_1 q / \{\beta_{11} + \alpha_1 [e]\} \quad (18)$$

$$\begin{aligned} [e]^2 &= Aq + B[O^+] \\ &= Aq + B\gamma_1 q / \{\beta_{11} + \alpha_1 [e]\} \\ &= (A + B\gamma_1 / \{\beta_{11} + \alpha_1 [e]\})q \end{aligned}$$

or

$$q = \frac{[e]^2}{A + B\gamma_1 / (\beta_{11} + \alpha_1 [e])} \quad (19)$$

with

$$A = A' + C'\gamma_3/(\beta_{33} + \alpha_3[e]) + D'\gamma_4/(\beta_{44} + \alpha_4[e]) \quad (20)$$

$$B = B' + D'\beta_{41}/(\beta_{44} + \alpha_4[e]) \quad (21)$$

Solve Equation (10) for $[\text{NO}^+]$:

$$[\text{NO}^+] = \frac{\gamma_2 q + \beta_{21}[\text{O}^+] + \beta_{23}[\text{N}_2^+] + \beta_{24}[\text{O}_2^+]}{\alpha_2[e]} \quad (22)$$

Collate Equations (19), (18), (15), (16), and (22) in the order in which they must be evaluated. Also use

$$\beta_{23} = \beta_{33}, \quad \beta_{24} = \beta_{44}.$$

$$q = \frac{[e]^2}{A + B\gamma_1/\text{FACTQ}} \quad (23)$$

$$[\text{O}^+] = \frac{\gamma_1 q}{\text{FACTQ}} \quad (24)$$

$$[\text{N}_2^+] = \frac{\gamma_3 q}{\text{A2DEN}} \quad (25)$$

$$[\text{O}_2^+] = \frac{\gamma_4 q + \beta_{41}[\text{O}^+]}{\text{A3DEN}} \quad (26)$$

$$[\text{NO}^+] = \frac{\gamma_2 q + \beta_{21}[\text{O}^+] + \beta_{23}[\text{N}_2^+] + \beta_{24}[\text{O}_2^+]}{\alpha_2[e]} \quad (27)$$

where

$$\text{FACTQ} = \beta_{11} + \alpha_1[e]$$

$$\text{A2DEN} = \beta_{33} + \alpha_3[e]$$

$$A3DEN = \beta_{24} + \alpha_4[e]$$

$$FACTA3 = D'/A3DEN$$

$$A = A' + C'\gamma_3/A2DEN + \gamma_4 FACTA3$$

$$B = B' + \beta_{41} FACTA3 .$$

In Subroutine IONOSU we use Equations (19), (18), (22), (15), and (16) to compute q , $[O^+]$, $[NO^+]$, $[N_2^+]$, and $[O_2^+]$ after prescribing analytic fits to nominal profiles of E- and F-region electron density [Ri-73, Figure 1] and electron temperature [Ev-73].

The prescribed electron-density profiles in the E- and F-region for noon and midnight conditions are shown in Figures 5-1a and 5-1b. The fit functions used to obtain these profiles are described in Table 5-3.

The prescribed electron temperature profile and the heavy-particle temperature profile in the E- and F-region for noon and midnight conditions are shown in Figure 5-2. The fit function used to obtain the electron temperature profile is described in Table 5-4.

For approximately mean solar-flux conditions, $SBAR \approx \bar{S} \approx 149 \times 10^{-22} \text{ W m}^{-2} \text{ Hz}^{-1}$, profiles of q are shown for noon and midnight conditions in Figure 5-3 and the corresponding values of $[O^+]$, $[NO^+]$, $[N_2^+]$, and $[O_2^+]$ are shown in Figures 5-1a and 5-1b.

5-3 D-REGION IONOSPHERIC PROPERTIES

The D-region chemistry requires the following quantity:

q , the effective total ion-production rate that adequately reproduces the ambient ionosphere when used with the chemistry model.

The modeling of q in the D-region (and lower) is offered with reservations; it may need to be improved if experience shows that this topic is more important than it is presently assumed to be for radar.

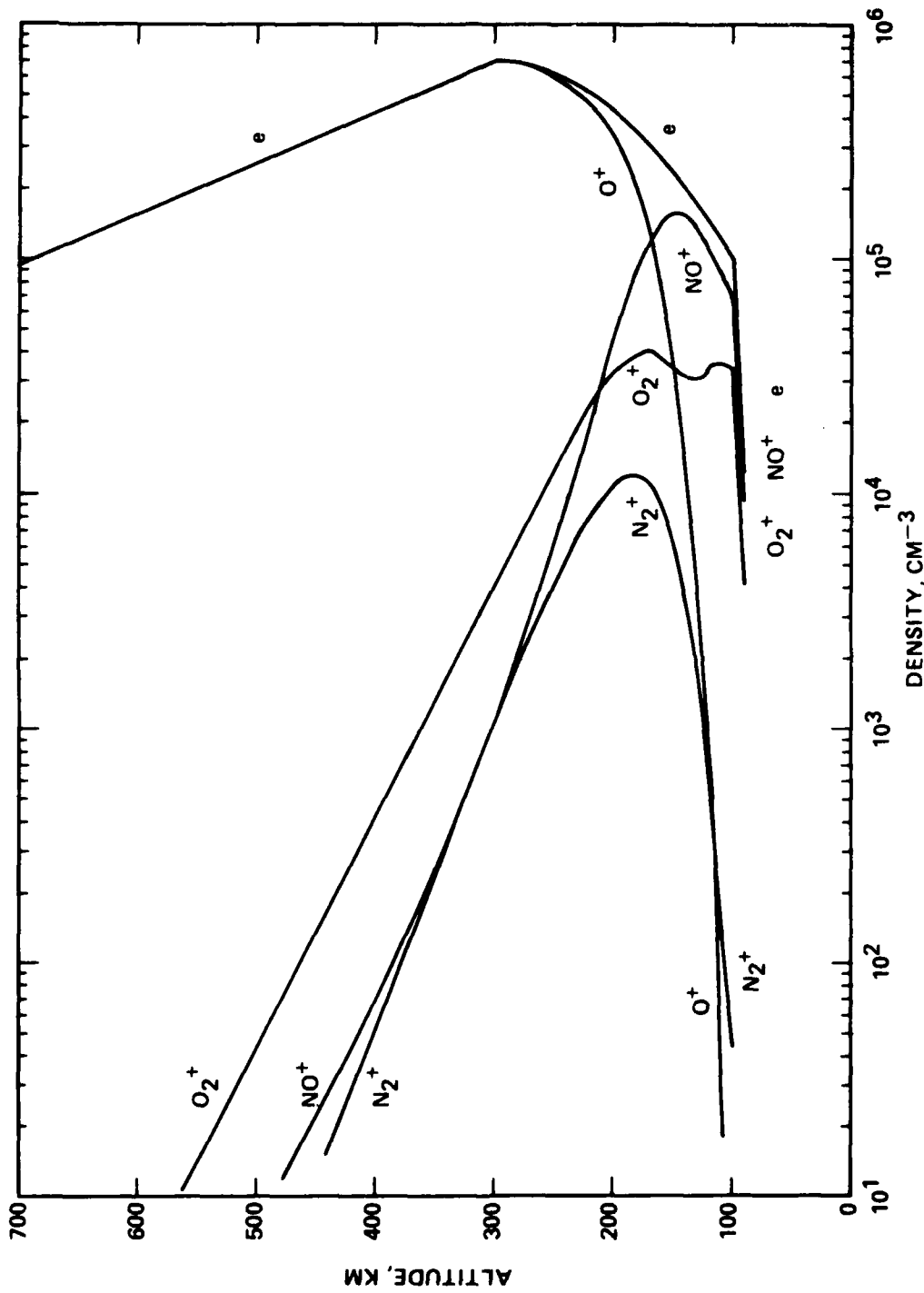


Figure 5-1a. E- and F-region ionospheric charged-species densities for noon conditions. The electron density profile is prescribed to be independent of solar-flux conditions. The atomic- (O^+) and molecular-ion (NO^+ , N_2^+ , O_2^+) densities are IONOSU-computed steady-state values for approximately average solar-flux conditions ($S \approx 149 \cdot 10^{-22} \text{ W m}^{-2} \text{ Hz}^{-1}$).

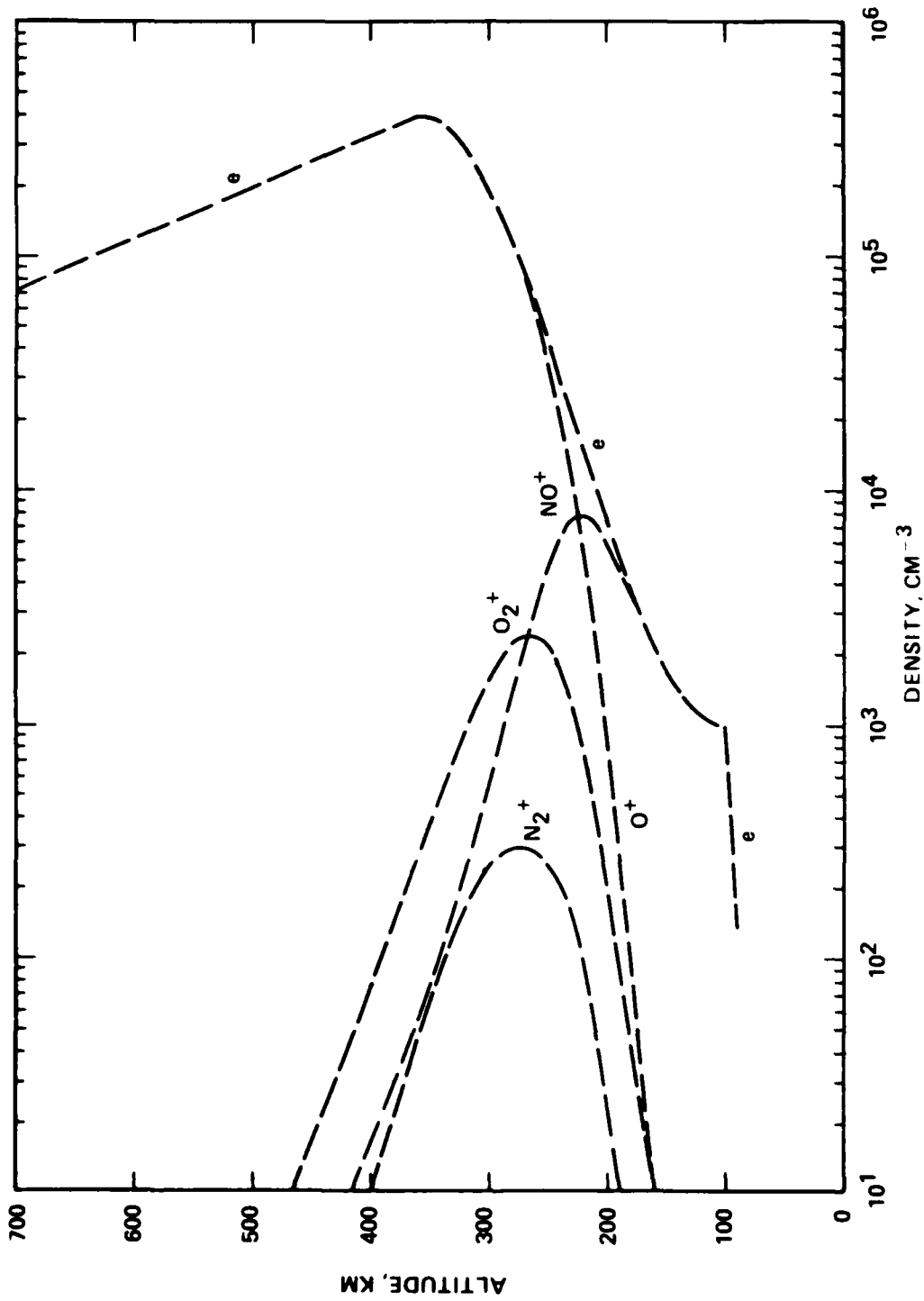


Figure 5-lb. E- and F-region ionospheric charged-species densities for midnight conditions. The electron density profile is prescribed to be independent of solar-flux conditions. The atomic- (O^+) and molecular-ion (NO^+ , N_2^+ , O_2^+) densities are IONOSU-computed steady-state values for approximately average solar-flux conditions ($\bar{S} \pm 149 \times 10^{-22} \text{ W m}^{-2} \text{ Hz}^{-1}$).

Table 5-3. Fit functions for E- and F-region electron density profiles.^a

| Altitude Range, km | Description |
|-----------------------|--|
| <u>Day</u> | |
| 90 - 100 | Exponential, determined by data-point value (EBOTD) at 100-km altitude (HEBOTD) and scale height EDDSCH |
| 100 - 300 | Parabola, determined by data-point values EBOTD and EF2MXD at altitudes HEBOTD and HF2MXD and vertical slope at altitude HF2MXD |
| >300 | Exponential, determined by data-point value (EF2MXD) at 300-km altitude (HF2MXD) and scale height F2DSCH |
| <u>Night</u> | |
| 90 - 100 | Exponential, determined by data-point value (EBOTN) at 100-km altitude (HEBOTN) and scale height EDNSCH |
| 100 - 360 | Sinusoid, determined by data-point values EBOTN and EF2MXN at altitudes HEBOTN and HF2MXN and vertical slope at the same altitudes |
| >360 | Exponential, determined by data-point value (EF2MXN) at 360-km altitude (HF2MXN) and scale height F2NSCH |

^a Based on Figure 1 in Ri-73.

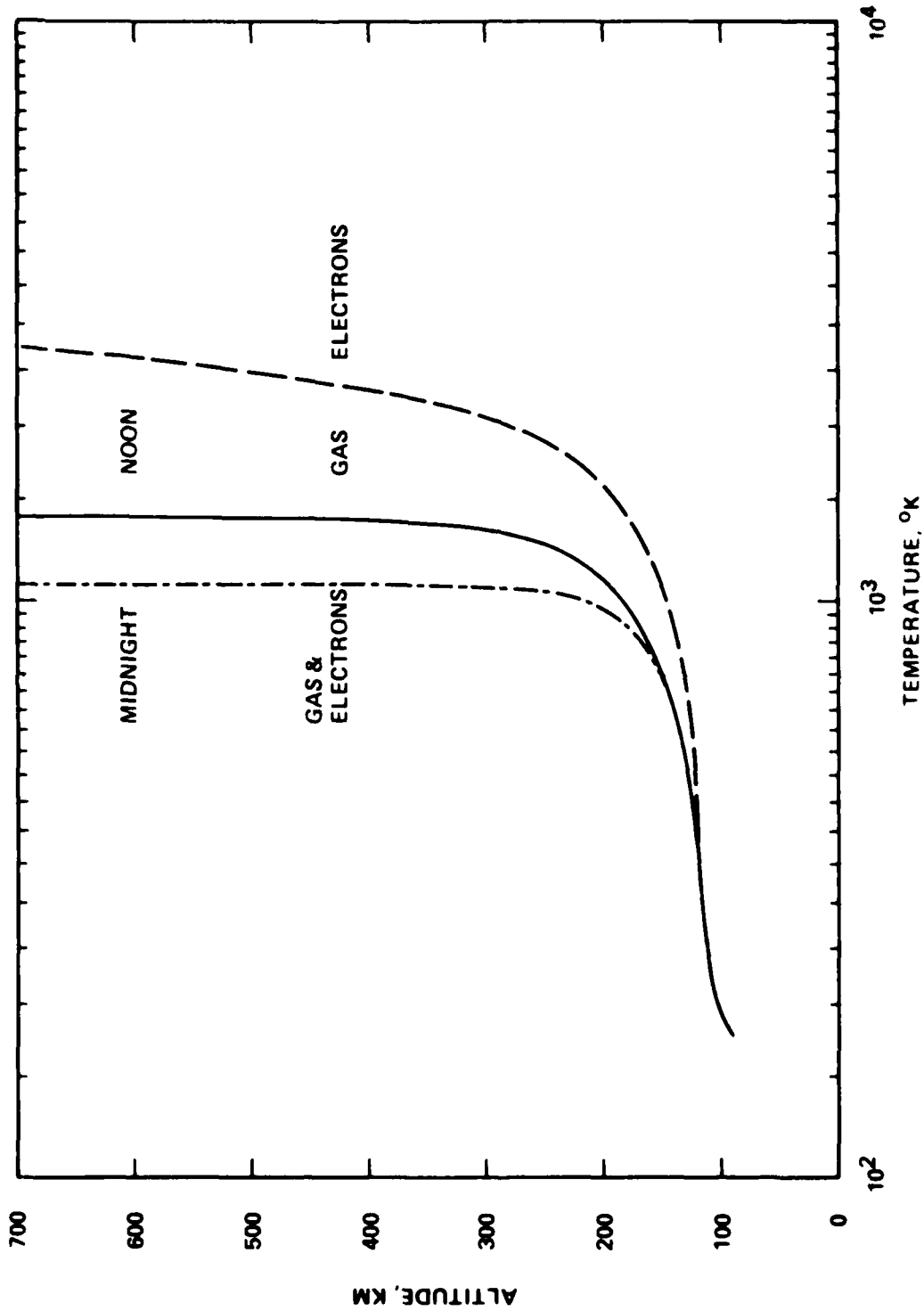


Figure 5-2. E- and F-region ionospheric temperatures. The difference between the electron and gas temperatures is prescribed to be independent of the solar-flux conditions. The absolute values shown are IONOSU-computed values for approximately average solar-flux conditions ($\bar{S} \approx 149 \times 10^{-22} \text{ W m}^{-2} \text{ Hz}^{-1}$).

Table 5-4. Fit function for electron temperature profile.

| Altitude Range, km | Description |
|-----------------------|---|
| <u>Day</u> | |
| <120 | Same as heavy-particle temperature |
| ≥120 | The difference between the electron temperature (T_x) and the gas temperature (T) is prescribed to be zero at 120-km altitude and 500°K at 200-km altitude. The parabola $T_x - T = 500[(ZH - 120)/80]^{\frac{1}{2}}$ is then used. |
| <u>Night</u> | |
| ≥0 | Same as heavy-particle temperature |

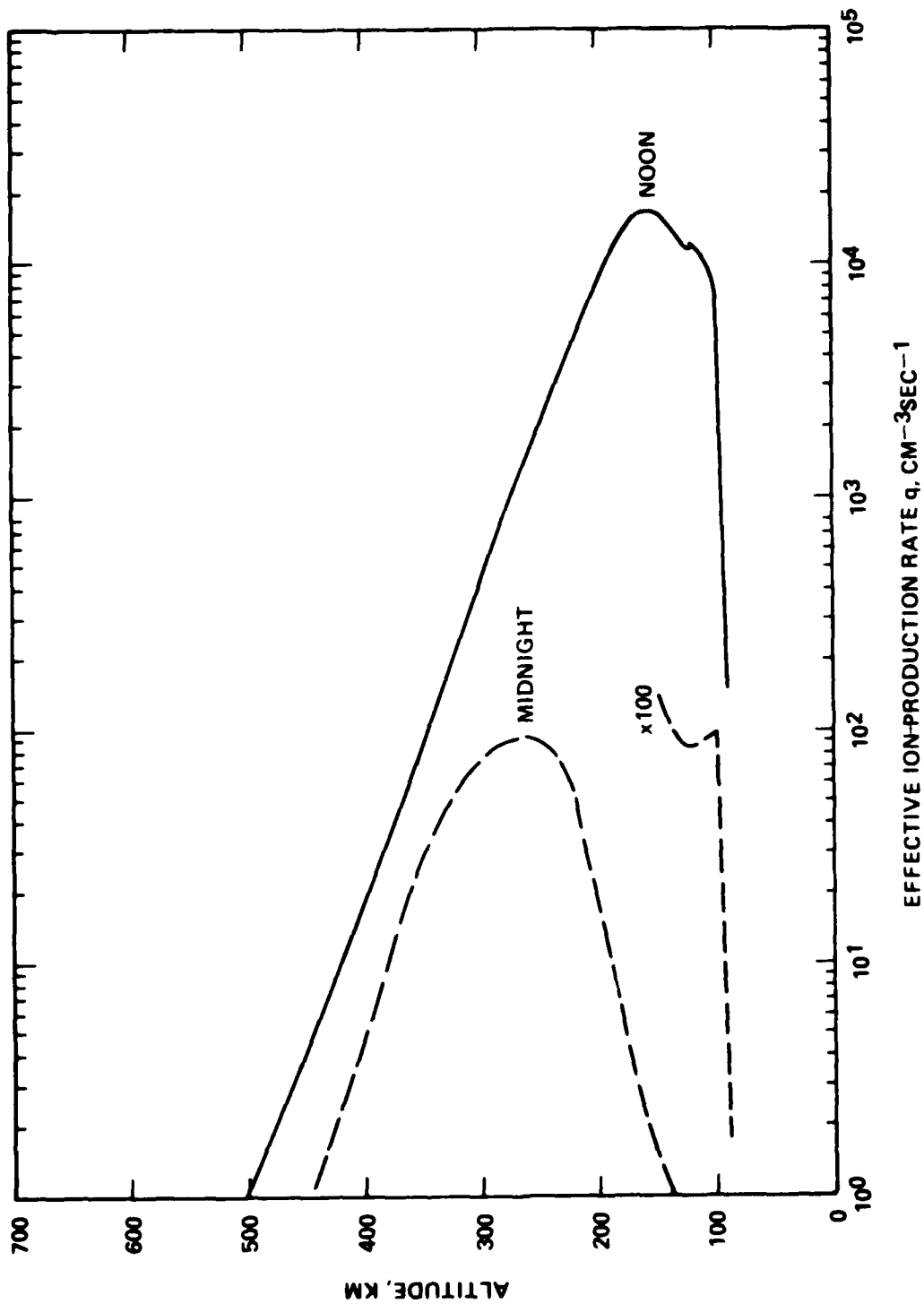


Figure 5-3. E- and F-region effective ion-production rates. The values shown are IONOSU-computed steady-state values for the prescribed electron density profiles in Figures 5-1a and 5-1b and for approximately average solar-flux conditions ($S \approx 149.19 \cdot 10^{-22} \text{ W m}^{-2} \text{ Hz}^{-1}$).

For the D region, q is determined by specifying data points at 30- and 60-km altitude and by requiring the fit function to be continuous with the value of q derived from the E- and F-region model at 90-km altitude. The fit function is extrapolated below 30-km altitude for modeling convenience and not on a physical basis.

The data adopted are based on the calculations of Webber [We-62] for the ion-production rate due to galactic cosmic rays. Webber [We-62, Figure 2] presents results in the altitude range from 30 to 90 km for two geomagnetic latitudes (50° and 70°) and for sunspot-minimum and sunspot-maximum conditions. For the geomagnetic latitude of 50° , Webber [We-62] finds $q_{\max} = 0.04$ and $q_{\min} = 0.08$ at 60-km altitude and $q_{\max} = 2.1$ and $q_{\min} = 4.5$ at 30-km altitude. We adopt solar-cycle mean values of 0.06 and 3.3 at 60- and 30-km altitude, respectively. The interested reader may also wish to consult Ra-72 (Figure 2-3) and Po-73a (Figures 2 and 3).

The profiles of q in the D and adjacent regions for noon and midnight conditions are shown in Figure 5-4. The fit functions used to obtain these profiles are described in Table 5-5.

Table 5-5. Fit functions for effective ion-production rate in D and lower regions.

| Altitude Range, km | Description |
|-----------------------|---|
| <u>Day</u> | |
| 0 - 60 | Exponential, determined by data-point values at 30- and 60-km altitude |
| 60 - 90 | Exponential, determined by data-point values at 60-km altitude and daytime value of q from E- and F-region model at 90-km altitude |
| <u>Night</u> | |
| 0 - 60 | Same as daytime |
| 60 - 90 | Exponential, determined by data-point value at 60-km altitude and nighttime value of q from E- and F-region model at 90-km altitude |

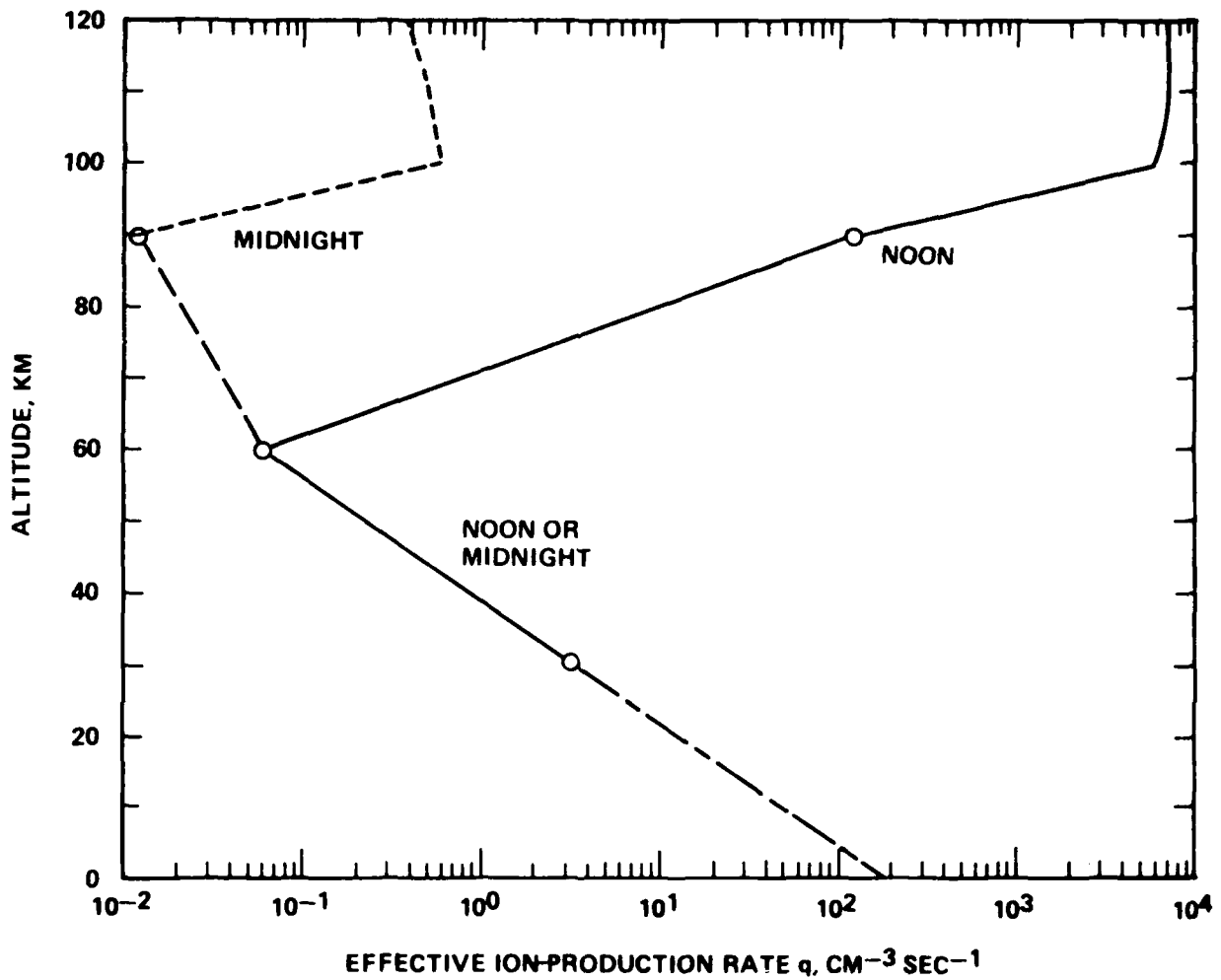


Figure 5-4. D-region effective ion-production rates. The values shown are IONOSU-computed fit functions required to pass through adopted data-base values at 30- and 60-km altitude and to join the IONOSU E- and F-region values at 90-km altitude. The extrapolation below 30-km altitude is purely for modeling convenience.

SECTION 6

PROGRAM DRVATM, LISTING OF COMPUTER PROGRAM, AND SAMPLE PROBLEM RESULTS

A driver routine (Program DRVATM) is provided to exercise the ATMOSU, SPCMIN, IONOSU, and associated routines. The required input consists of the year, month, day, zone time, geographic colatitude and longitude of the point of interest, three digital-flags relating to optional treatment of water vapor and temperature profiles, a set of test altitudes, and the number of such altitudes. Input quantities are more specifically described in Table 6-1. Program DRVATM, after reading and writing the input, first initializes the ATMOSU routine by the call ATMOSU (1,120.). The water vapor routine (WVOPT) is then initialized if WVFLAG \neq 0.0. DRVATM next loops over the test-altitude array, exercises the ATMOSU, SPCMIN, IONOSU, and H2OSVP routines for each altitude, and prints the resultant atmospheric and ionospheric property values.

A listing of the driver, ATMOSU, SPCMIN, IONOSU, their associated subroutines, and outputs from two sample problems are provided.

The quantities in the output block at each altitude are labeled in the headings. The last four entries (E, O+, M+, and N+) in row-two of the output block at each altitude (≥ 90 km) are computed by Subroutine CHEMQ and are included for comparison with the quantities E, O+, and NO+ in row-1 and N2+ and O2+ in row-4. Subroutine CHEMQ, prepared by Knapp and Jordano (see Volume 11) for use with the NRL Simple-Chemistry module developed for ROSCOE-Radar, computes steady-state ionization for the E- and F-region; it is not a part of the operational atmospheric and ionospheric module.

Table 6-1. Input quantities to Program DRVATM.

| | | |
|---------|---|--|
| NALTS | - | Number of test altitude values |
| ALTS(I) | - | Test altitude values (km) |
| IYRS | - | Number of the year in the 1900's at east longitude GLO (e.g., 1974 becomes 74) |
| IMONS | - | Number of the month at east longitude GLO (e.g., February becomes 2) |
| IDAYS | - | Day of the month at east longitude GLO |
| ZT | - | Zone time for the 15-degree longitude interval containing east longitude GLO |
| GCO | - | Geographic colatitude of grid origin or whatever reference point is desired (degrees) |
| GLO | - | Geographic east longitude of grid origin or whatever reference point is desired (degrees) |
| WVFLAG | - | Flag for optional treatment of water vapor = 0.0, normal treatment ≠ 0.0, optional treatment |
| METHOD | - | Flag indicating one of four options for treatment of water vapor = 1 data values in parts per million by mass (ppmm) = 2 data values in absolute humidity (g/m ³) = 3 data values in relative humidity (percent; 10 percent is input as 10., not 0.10) = 4 data values in dew-point temperature (°K) |
| TPFLAG | - | Flag for optional treatment of temperature profile = 0.0, normal treatment ≠ 0.0, optional treatment |

TPFLAG is transferred to Subroutine TEMPZH through ZHTEMP
Common. A nonzero value of TPFLAG allows Subroutine
TEMPZH to read the user-specified profile at altitudes
ZZ = 0.0(4.0)120.0 km.

```

PROGRAM DRVATM (INPUT,OUTPUT,TAPES=INPUT,TAP=6=OUTPUT)
C
C * * * * *
C THIS ROUTINE IS PROVIDED TO DRIVE AND TEST ATMOSP AND THE
C RELATED ROUTINES WHICH COMPUTE THE PROPERTIES OF THE
C UNDISTURBED ATMOSPHERE AND IONOSPHERE.
C * * * * *
C
C INPUT PARAMETERS
C
C   ALTS - NUMBER OF TEST-ALTITUDE VALUES
C   ALTS(I) - TEST-ALTITUDE VALUES, KM
C   IYRS - NUMBER OF THE YEAR IN THE 1900 S AT EAST
C         LONGITUDE GLO (E.G., 1974 BECOMES 74)
C   INONS - NUMBER OF THE MONTH AT EAST LONGITUDE GLO
C         (E.G., FEBRUARY BECOMES 2)
C   IOAYS - DAY OF THE MONTH AT EAST LONGITUDE GLO
C   ZT - ZONE TIME FOR THE 15-DEGREE LONGITUDE INTERVAL
C        CONTAINING EAST LONGITUDE GLO
C   GCO - GEOGRAPHIC COLATITUDE OF GRID ORIGIN OR WHATEVER
C        REFERENCE POINT IS DESIRED (DEGREES)
C   GLO - GEOGRAPHIC EAST LONGITUDE OF GRID ORIGIN OR
C        WHATEVER REFERENCE POINT IS DESIRED (DEGREES)
C   WVFLAG - FLAG FOR OPTIONAL TREATMENT OF WATER VAPOR.
C            .EQ. 0.0 NORMAL TREATMENT
C            .NE. 0.0 OPTIONAL TREATMENT
C   METHOD - FLAG INDICATING ONE OF FOUR OPTIONS, FOR
C           OPTIONAL TREATMENT OF WATER VAPOR.
C           =1 DATA VALUES IN PARTS PER MILLION BY WEIGHT
C           =2 DATA VALUES IN ABSOLUTE HUMIDITY,
C             GRAMS/METERS**3
C           =3 DATA VALUES IN RELATIVE HUMIDITY, PERCENT
C             (10 PERCENT IS INPUT AS 10. NOT 0.10)
C           =4 DATA VALUES IN DEW-POINT TEMPERATURE, DEG K
C   TPFLAG - FLAG FOR OPTIONAL TREATMENT OF TEMPERATURE
C           PROFILE.
C           .EQ. 0.0 NORMAL TREATMENT
C           .NE. 0.0 OPTIONAL TREATMENT
C           TPFLAG IS TRANSFERRED TO SUBROUTINE TEMPZH
C           THROUGH COMMON ZHTMP. A NONZERO VALUE OF TPFLAG
C           ALLOWS SUBROUTINE TEMPZH TO READ THE USER-
C           SPECIFIED PROFILE AT ALTITUDES ZZ=0.0(4.0)120. KM
C
CCC
COMMON/ATMOUP/ HL,SBAR,LDURN,PP,R40,TT,SHI(30),HRHO,PHSEQ
COMMON/IONJUP/ EPE,EPDP,EPNP,EPN2P,EPD2P,TE,WDPE
COMMON /SPECQ/ CN2,CO2,CNO,CN4S,CN2D,CO,CNP,CJP,CNE,TV,TE,TC
COMMON/PINE/ IYRS,INONS,IOAYS,ZT,PLAT,PLON,UF,CAT,PYR,FST,RHOSKM
      ,CHI
COMMON/VPC/ WVFLAG,METHOD,M23120
COMMON/ZHTMP/ WZHT,ZHTZ(3),ZHT(31),TZHZ(3),TZH(31),TPFLAG
C
CCC
DIMENSION ALTS(200)
DATA PI / 3.141592653590 /
C
C   P102 = PI/2.
C   RADDEG = PI/180.
C
C * * READ IN TEST ALTITUDES

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DRIVER 2
DRIVER 3
DRIVER 4
DRIVER 5
DRIVER 6
DRIVER 7
DRIVER 8
DRIVER 9
DRIVER 10
DRIVER 11
DRIVER 12
DRIVER 13
DRIVER 14
DRIVER 15
DRIVER 16
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DRIVER 55
DRIVER 56
DRIVER 57

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| | | | |
|------|---|--------|-----|
| C | | DRIVER | 54 |
| | READ(5,1001)MALTS | DRIVER | 55 |
| 1001 | FORMAT(I5) | DRIVER | 60 |
| | READ(5,1002)(ALTS(I),I=1,MALTS) | DRIVER | 61 |
| 1002 | FORMAT(8F10.2) | DRIVER | 62 |
| C | | DRIVER | 63 |
| C | * * READ IN YEAR,MONTH,DAY,ZONE TIME, GEOGRAPHIC CULATITUDE AND | DRIVER | 64 |
| C | * * LONGITUDE OF GRID ORIGIN. | DRIVER | 65 |
| C | | DRIVER | 65 |
| 1010 | READ(5,1003) IYRS,IMONS,IDAYS,ZT,GCO,GLO,MVFLAG,METHOD,TPFLAG | DRIVER | 67 |
| 1003 | FORMAT (J15,4E10.4,I5,E10.4) | DRIVER | 68 |
| C | CONVERT GLO TO THE CORRESPONDING POSITIVE QUANTITY, IF GLO | DRIVER | 69 |
| C | IS READ IN AS A NEGATIVE QUANTITY. | DRIVER | 70 |
| C | IF(GLO .LT. 0.0) GLO = GLO + 360. | DRIVER | 71 |
| C | A NEGATIVE VALUE OF IYRS IS USED TO TERMINATE EXAMPLES. | DRIVER | 72 |
| C | IF(IYRS.LE.0) CALL EXIT | DRIVER | 73 |
| C | | DRIVER | 74 |
| C | * * PRINT OUT INPUT VALUES | DRIVER | 75 |
| C | | DRIVER | 76 |
| | WRITE(5,2001)MALTS | DRIVER | 77 |
| 2001 | FORMAT(1H1,/,/20H TEST VALUES READ IN,/,/8H MALTS =,I5,/,/10X, | DRIVER | 78 |
| | * 3H I ,2X,11H ALTS(I),KX,/)) | DRIVER | 79 |
| | WRITE(6,2002)(I,ALTS(I),I=1,MALTS) | DRIVER | 80 |
| 2002 | FORMAT (6(2X,10,F10.2)) | DRIVER | 81 |
| | WRITE(6,2004) IYRS,IMONS,IDAYS,ZT,GCO,GLO | DRIVER | 82 |
| 2004 | FORMAT (/,/8H IYRS =I5,10H IMONS =I5,10H IDAYS =I5/ | DRIVER | 83 |
| | * 8H ZT =E12.4,14H HRS GCO =E12.4,14H DEG GLO =E12.4, | DRIVER | 84 |
| | * 4H DEG) | DRIVER | 85 |
| | WRITE(6,2007) MVFLAG,METHOD,TPFLAG | DRIVER | 86 |
| 2007 | FORMAT (8H MVFLAG=,F8.2,10X,8H METHOD=,I5,10X,8H TPFLAG=,F8.2) | DRIVER | 87 |
| C | CONVERT GCO AND GLO FROM DEGREES TO RADIANS. | DRIVER | 88 |
| | GCO = GCO*PI/180 | DRIVER | 89 |
| | GLO = GLO*PI/180 | DRIVER | 90 |
| C | IDENTIFY THE GRID ORIGIN AS THE POINT P. | DRIVER | 91 |
| | PLAT = PID2-GCO | DRIVER | 92 |
| | PLON = GLO | DRIVER | 93 |
| C | | DRIVER | 94 |
| C | * * INITIALIZE THE ATMOSU ROUTINE | DRIVER | 95 |
| C | | DRIVER | 96 |
| | WRITE(6,H020) | DRIVER | 97 |
| 0020 | FORMAT(//20H INITIALIZATION CALL,/)) | DRIVER | 98 |
| C | | DRIVER | 99 |
| | CALL ATMOSU(1,120.) | DRIVER | 100 |
| | IF(MVFLAG.EQ.0.0) GO TO 2008 | DRIVER | 101 |
| C | INITIALIZE SUBROUTINE WVOPT BY INPUTTING USER'S OPTIONAL DATA | DRIVER | 102 |
| C | FOR WATER VAPOR CONTENT, PER ONE OF FOUR METHODS. | DRIVER | 103 |
| | CALL WVOPT(1,120.,H20120) | DRIVER | 104 |
| C | GET WATER VAPOR MIXING RATIO AT 120 KM FOR USE IN | DRIVER | 105 |
| C | EXTRAPOLATING TO HIGHER ALTITUDES IN SUBROUTINE SPCMIN. | DRIVER | 106 |
| | CALL WVOPT(2,120.,H20120) | DRIVER | 107 |
| 2008 | CONTINUE | DRIVER | 108 |
| C | | DRIVER | 109 |
| | WRITE(6,2006) IYRS,IMONS,IDAYS,ZT,GCO,GLO | DRIVER | 110 |
| 2006 | FORMAT (/,/8H IYRS =I5,10H IMONS =I5,10H IDAYS =I5/ | DRIVER | 111 |
| | * 8H ZT =E12.4,14H HRS GCO =E12.4,14H RAD GLO =E12.4, | DRIVER | 112 |
| | * 4H RAD) | DRIVER | 113 |
| | WRITE(6,2005) IDURN,UT,GAT,PLAT,PLON | DRIVER | 114 |

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2005 FORMAT (//,8H IDORN =15,10H      UT =E12.4,10H      GAT =E12.4,10H      DRIVER  115
*   PLAT =E12.4,10H      PLON =E12.4)      DRIVER  116
WRITE(6,2003)HL,SWAR      DRIVER  117
2003 FORMAT (/ * HL = *P6.2 * MNS (LOCAL TIME AT GRIJ ORIGIN), SOLAR FLUX DRIVER  118
$ SWAR = *P7.2 * 1.E-22 d/(M SU MZ), * /IX, * FROM PROGRAM DRVATM (FORMAT DRIVER  119
$ 2003) * )      DRIVER  120
C      DRIVER  121
C * * LOOP OVER TEST ALTITUDES      DRIVER  122
C      DRIVER  123
WRITE(6,8002)      DRIVER  124
8002 FORMAT (1H0,129H      ALT      M2      U2      U      DRIVER  125
*   AR      HK      CO2      E      O+      MO+      DRIVER  126
*   JDEP /10X,9(5X,4H1/CC,3X),2X,10H1/(CC SEC))      DRIVER  127
WRITE(6,8003)      DRIVER  128
8003 FORMAT (1H0,9X,120H      M      NO      NO2      J2(SDC)      DRIVER  129
*   J3      M2J      E      O+      M+      DRIVER  130
*   /10X,10(5X,4H1/CC,3X))      DRIVER  131
WRITE(6,8004)      DRIVER  132
8004 FORMAT(1H0,9X,120H      PNESSURE      FENSEW      DENSITY      DEN SC HT      DRIVER  133
*   TEMP      E TEMP      H      OH      HO2      C      DRIVER  134
*   /10X,72H DYNES/CM * 2      GRAMS/CC      KM      DRIVER  135
*   DEG K      DEG K      ,4(5X,4H1/CC,3X))      DRIVER  136
WRITE(6,8006)      DRIVER  137
8006 FORMAT (1H0,9X,72H      M2O      CH4      N (4S)      N (20)      DRIVER  138
*   M (2P)      O (10)      ,2(3X,7HSAT. VP,2X),22H      N2+      U      DRIVER  139
* 2+ /10X,6(5X,4H1/CC,3X),5X,5H0ATER,8X,3HICE,3X,2:5X,4H1/CC,3X))      DRIVER  140
WRITE(6,8007)      DRIVER  141
8007 FORMAT (1H0,81X,12H REL. HUMID. /82X,12H PERCENT )      DRIVER  142
DO 50 I=1,NALTS      DRIVER  143
ZM = ALYS(I)      DRIVER  144
CALL ATMOSU(2,ZH)      DRIVER  145
CALL SPCMIN(2,ZH)      DRIVER  146
CALL IJMSU(2,ZH)      DRIVER  147
VPH2J = 0.0      DRIVER  148
VPICE = 0.0      DRIVER  149
IF( ( TT .GE. 173.15 ) .AND. ( TT .LE. 373.15 ) )      DRIVER  150
*CALL MZJSVP(TT,VPH2J,VPICE)      DRIVER  151
ZHEW = 0.0      DRIVER  152
JPO = 0.0      DRIVER  153
EMPO = 0.0      DRIVER  154
IF( ZM.LT.90. ) GO TO 45      DRIVER  155
M2 = SM1(1)      DRIVER  156
M2 = SM1(2)      DRIVER  157
CO = SM1(3)      DRIVER  158
M2J = SM1(4)      DRIVER  159
M4S = SM1(7)      DRIVER  160
M2D = 1.0      DRIVER  161
M2P = 0.0      DRIVER  162
M2J = 0.0      DRIVER  163
SEME = 0.0      DRIVER  164
TV = TK      DRIVER  165
TE = TK      DRIVER  166
TC = TT      DRIVER  167
C      SUBROUTINE CHENQ, WHICH IS NOT AN OPERATIONAL PART OF THE ATMOSU      DRIVER  168
C      PACKAGE, WAS PREPARED BY KNAPP AND JINDAVU (KJ-74,KJ-743) TO      DRIVER  169
C      COMPUTE THE STEADY-STATE IONIZATION FOR THE E- AND F-REGION.      DRIVER  170
C      ITS RESULTS FOR E,U+,M+, AND H+ IN ROW-TOU OF THE OUTPUT BLOCK      DRIVER  171

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| | | | |
|---|---|--------|-----|
| C | ARE INCLUDED FOR COMPARISON WITH THE QUANTITIES E, U+, AND W+ | DRIVER | 172 |
| C | IN MOD-ONE AND M2+ AND J2+ IN MOD-FOUR COMPUTED BY ICMDSU. | DRIVER | 173 |
| | CALL CHEMQ(JOEF,ENPQ,UPQ,ENEQ) | DRIVER | 174 |
| | 4) ENPQ = ENEQ-OPQ-ENPJ | DRIVER | 175 |
| | WRITE(5,9005) ZH,(SNI(J),J=1,6),(SNI(J),J=7,11),WUEP,SNI(7), | DRIVER | 176 |
| | SNI(8),SNI(15),SNI(13),SNI(14),SNI(16),ENEQ,UPQ, | DRIVER | 177 |
| | &MPQ,ENPQ,PP,PEHSEJ,KHU,HHU,PT,SNI(12) | DRIVER | 178 |
| | ,(SNI(J),J=17,24),SNI(27),SNI(26),VPHZJ,VPIE | DRIVER | 179 |
| | ,SNI(28),SNI(29),SNI(25) | DRIVER | 180 |
| | 9005 FORMAT (1X,0PF9.2,1P10E12.3,3(/10X,1P10E12.3)/82X,1PE12.3) | DRIVER | 181 |
| | 50 CONTINUE | DRIVER | 182 |
| C | WRITE(6,9050) | DRIVER | 184 |
| | 9050 FORMAT(/,20H END OF TEST PROBLEM) | DRIVER | 185 |
| | 10 T3 1010 | DRIVER | 186 |
| | END | DRIVER | 187 |

| SUBROUTINE ATMOSU(JJ,ZH) | | ATMOSU | 2 |
|--------------------------|---|--------|----|
| C | | ATMOSU | 3 |
| C | ATMOSU COMPUTES THE PROPERTIES OF THE UNDISTURBED ATMOSPHERE, | ATMOSU | 4 |
| C | GIVEN THE ALTITUDE ZH, AFTER ASSOCIATED SUBROUTINES COMPUTE | ATMOSU | 5 |
| C | THE LOCAL APPARENT TIME HL, SOLAR FLUX SBAR, AND DAY-OR-NIGHT | ATMOSU | 6 |
| C | PARAMETER IODRN. | ATMOSU | 7 |
| C | ATMOSU IS REVISION 13 (01/07/79) BY D. A. HANLIN AND M. R. | ATMOSU | 8 |
| C | SCHUMBERG OF ATMOS DEVELOPED BY R. W. LJWEN (SEE, AN AMBIENT | ATMOSU | 9 |
| C | ATMOSPHERE MODEL FOR MOSCIE, P. 187, VOL. 5 OF PROC. JNA 1973 | ATMOSU | 10 |
| C | ATMOSPHERIC EFFECTS SYMPOSIUM, DWA 3131-5, 5 JUNE 1973.) | ATMOSU | 11 |
| C | REVISION 02 (06/07/74) PROVIDES | ATMOSU | 12 |
| C | 1. IN HIGH-ALTITUDE MODEL, FOR USE OF GAP(120.) INSTEAD OF | ATMOSU | 13 |
| C | GAP(0.) = GZ IN COMPUTING GAM AND ZZ. | ATMOSU | 14 |
| C | 2. DENSITY SCALE HEIGHT FOR BOTH LOW- AND HIGH-ALTITUDE | ATMOSU | 15 |
| C | MODELS, WITH AN AD HOC PARABOLIC TRANSITION FROM 110- TO | ATMOSU | 16 |
| C | 120-KM ALTITUDE TO PROVIDE A CONTINUOUS DENSITY SCALE | ATMOSU | 17 |
| C | HEIGHT ACROSS THE BOUNDARY BETWEEN THE TWO MODELS. | ATMOSU | 18 |
| C | 3. ALTERED FORMULA FOR D DENSITY ON FIRST CALL AND AT LOW | ATMOSU | 19 |
| C | ALTITUDE SO AS TO USE SP-FUNCTION DIRECTLY. | ATMOSU | 20 |
| C | 4. COMMENT CARDS. | ATMOSU | 21 |
| C | REVISION 03 (10/25/74) PROVIDES | ATMOSU | 22 |
| C | 5. PROVISION FOR DAY OR NIGHT VALUES OF ATOMIC OXYGEN | ATMOSU | 23 |
| C | (OBTAINED FROM THE MINOR SPECIES SUBROUTINE SPCMIN) | ATMOSU | 24 |
| C | FOR ALTITUDES BELOW 120 KM. | ATMOSU | 25 |
| C | 6. AUTOMATED PROCEDURE FOR EVALUATING CONSTANTS IN DENSITY | ATMOSU | 26 |
| C | SCALE-HEIGHT FORMULA USED IN THE 110- TO 120-KM | ATMOSU | 27 |
| C | TRANSITION REGION. | ATMOSU | 28 |
| C | 7. PROCEDURE FOR LETTING SOLAR FLUX SBAR, AN INPUT TO | ATMOSU | 29 |
| C | ATMOSU, BE DETERMINED BY THE AUXILIARY ROUTINE SOLDFC. | ATMOSU | 30 |
| C | 8. PROCEDURE FOR LETTING THE LOCAL (APPARENT) TIME HL, | ATMOSU | 31 |
| C | AN INPUT TO ATMOSU, BE DETERMINED BY THE AUXILIARY | ATMOSU | 32 |
| C | SUBROUTINE SOLDRB. | ATMOSU | 33 |
| C | 9. PROCEDURE FOR LETTING THE DAY OR NIGHT PARAMETER IODRN | ATMOSU | 34 |
| C | BE DETERMINED BY THE AUXILIARY SUBROUTINE SOLZEM. | ATMOSU | 35 |
| C | REVISION 04 (12/08/74) PROVIDES | ATMOSU | 36 |
| C | 10. CARBON DIOXIDE AS THE SIXTH SPECIES IN ATMOSU, WITH | ATMOSU | 37 |
| C | PROFILE SPECIFIED BY B. P. MYERS ON 12/07/74. | ATMOSU | 38 |
| C | 11. EVALUATION OF DEPARTURE FROM HYDROSTATIC EQUILIBRIUM. | ATMOSU | 39 |
| C | 12. A FLAG, ZHFLAG, TO INSURE THAT SUBROUTINES IONOSU AND | ATMOSU | 40 |
| C | SPCMIN ARE CALLED AT THE SAME ALTITUDE AT WHICH ATMOSU | ATMOSU | 41 |
| C | WAS LAST CALLED. | ATMOSU | 42 |
| C | 13. DAY AND NIGHT PROFILES OF ATOMIC OXYGEN SPECIFIED BY | ATMOSU | 43 |
| C | B. P. MYERS ON 11/09/74 AND 11/23/74, RESPECTIVELY. | ATMOSU | 44 |
| C | 14. CORRECTED PROCEDURE FOR EVALUATING CONSTANTS IN DENSITY | ATMOSU | 45 |
| C | SCALE-HEIGHT FORMULA USED IN THE 110- TO 120-KM | ATMOSU | 46 |
| C | TRANSITION REGION. | ATMOSU | 47 |
| C | 15. CORRECTED CONSTANT IN LOW-ALTITUDE FORMULA FOR DENSITY | ATMOSU | 48 |
| C | SCALE HEIGHT. | ATMOSU | 49 |
| C | REVISION 05 (02/04/75) PROVIDES | ATMOSU | 50 |
| C | 16. INTERFACE WITH SPCMIN WHICH NOW COMPUTES DENSITIES OF | ATMOSU | 51 |
| C | H2O, N, NO, NO2, O2(SINGLE DELTA 3), AND O3. | ATMOSU | 52 |
| C | 17. INTERFACE WITH IONOSU WHICH NOW COMPUTES THE EFFECTIVE | ATMOSU | 53 |
| C | ION PRODUCTION RATE AT ALL ALTITUDES. | ATMOSU | 54 |
| C | REVISION 06 (04/04/75) PROVIDES | ATMOSU | 55 |
| C | 18. REVISED NIGHT PROFILE OF ATOMIC OXYGEN SPECIFIED BY | ATMOSU | 56 |
| C | B.P. MYERS ON 02/22/75 (MINOR CHANGE BELOW 60 KM). | ATMOSU | 57 |
| C | 19. REVISED DAY AND NIGHT PROFILES OF NITRIC OXIDE | ATMOSU | 58 |

| | | | | |
|---|------------------------|--|--------|-----|
| C | | | | |
| C | | SPECIFIED BY B.F. MYERS ON 04/05/75. | ATMOSU | 59 |
| C | 20. | REVISED DAY AND NIGHT PROFILES OF ATOMIC NITROGEN | ATMOSU | 60 |
| C | | SPECIFIED BY B.F. MYERS ON 04/11/75. | ATMOSU | 61 |
| C | REVISION 07 (04/24/75) | PROVIDES | ATMOSU | 62 |
| C | 21. | REVISED PROCEDURE FOR SPECIFYING AND USING DATE OF THE | ATMOSU | 63 |
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| C | * * G/TM, INTEGRAL OF G/TM, AND G. | ATMOSU | 242 |
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| | + AA(9))*AQ + AA(8))*AQ + AA(7))*AQ + AA(6))*AQ | ATMOSU | 245 |
| | + AA(5))*AQ + AA(4))*AQ + AA(3))*AQ + AA(2))*AQ + AA(1) | ATMOSU | 246 |
| C | | ATMOSU | 247 |
| | ZTMNF(AQ) = ((((((((((AA(12)/12.*AQ + AA(11)/11.*AQ | ATMOSU | 248 |
| | + AA(10)/10.*AQ + AA(9)/9.*AQ + AA(8)/8.*AQ | ATMOSU | 249 |
| | + AA(7)/7.*AQ + AA(6)/6.*AQ + AA(5)/5.*AQ | ATMOSU | 250 |
| | + AA(4)/4.*AQ + AA(3)/3.*AQ + AA(2)/2.*AQ + AA(1))*AQ | ATMOSU | 251 |
| C | | ATMOSU | 252 |
| | ZAP(BQ) = GZ/(1.0+BQ/RE)**2 | ATMOSU | 253 |
| CCC | | ATMOSU | 254 |
| C | * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE W/MSTAR DAY. | ATMOSU | 255 |
| CCC | | ATMOSU | 256 |
| | SFDAP(BQ) = EXP(((((((((((DD(13)*BQ + DD(12))*BQ + DD(11))*BQ | ATMOSU | 257 |
| | + DD(10))*BQ + DD(9))*BQ + DD(8))*BQ + DD(7))*BQ | ATMOSU | 258 |
| | + DD(6))*BQ + DD(5))*BQ + DD(4))*BQ + DD(3))*BQ | ATMOSU | 259 |
| | + DD(2))*BQ + DD(1) | ATMOSU | 260 |
| CCC | | ATMOSU | 261 |
| C | * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE DENSITY SCALE | ATMOSU | 262 |
| C | * * * HEIGHT (KM). | ATMOSU | 263 |
| CCC | | ATMOSU | 264 |
| | GKZAP(AQ) = ((((((((((AA(12)*11.*AQ + AA(11)*10.*AQ | ATMOSU | 265 |
| | + AA(10)*9.*AQ + AA(9)*8.*AQ + AA(8)*7.*AQ | ATMOSU | 266 |
| | + AA(7)*6.*AQ + AA(6)*5.*AQ + AA(5)*4.*AQ | ATMOSU | 267 |
| | + AA(4)*3.*AQ + AA(3)*2.*AQ + AA(2) | ATMOSU | 268 |
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| C | TRANSITION FUNCTION FOR THE DENSITY SCALE-HEIGHT BETWEEN | ATMOSU | 277 |
| C | THE LOW- AND HIGH-ALTITUDE MODELS. | ATMOSU | 278 |
| C | SUBSEQUENT CALLS, TO ATMOSU(2,ZH), GJ IN STATEMENT 200 | ATMOSU | 279 |
| C | HEREAFTER A LOW-ALTITUDE MODEL IS USED FOR ALTITUDES ZH | ATMOSU | 280 |
| C | LESS THAN 120 KM AND A HIGH-ALTITUDE MODEL IS USED OTHERWISE. | ATMOSU | 281 |
| CCC | | ATMOSU | 282 |
| CCC | INITIALIZATION | ATMOSU | 283 |
| CCC | | ATMOSU | 284 |
| CCC | GO TO (100,200), JJ | ATMOSU | 285 |

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| 100 | RR = SK*BICA | ATMOSU | 286 |
| | CCI = 1.0E+05*BIGMS/M ² | ATMOSU | 287 |
| C | CALL THE 5 AUXILIARY ROUTINES. | ATMOSU | 288 |
| | CALL ZFFOUT | ATMOSU | 289 |
| | CALL JLIAN(VMPJ,VEVJ,DAYJ) | ATMOSU | 290 |
| | CALL S3LCYC(DAYJ) | ATMOSU | 291 |
| | CALL S3LORB(VMPJ,VEVJ,DAYJ,SOLLAT,SULLON) | ATMOSU | 292 |
| | CALL S3LZEN(SULLAT,SJLON) | ATMOSU | 293 |
| C | CALCULATE FIT COEFFICIENTS DD(1) USED TO COMPUTE SF. | ATMOSU | 294 |
| | CALL FITTER(NZHT,ZHT,PDAY,NDEG, 1, 2, DD) | ATMOSU | 295 |
| | DD(13) = 0.0 | ATMOSU | 296 |
| C | CALL ROUTINE TO GET SEASONAL TEMPERATURE PROFILE. | ATMOSU | 297 |
| | CALL TEMPZH | ATMOSU | 298 |
| | DO 104 N=1,NZHT | ATMOSU | 299 |
| | SF = SPDAF(ZHT(N)) | ATMOSU | 300 |
| C | RESET TZN(N) TO BE THE RATIO (GDTM) OF THE ACCELERATION DUE TO | ATMOSU | 301 |
| C | GRAVITY TO THE MOLECULAR-SCALE TEMPERATURE AT ALTITUDE ZHT(N). | ATMOSU | 302 |
| | TZN(N) = GAF(ZHT(N))/((1.+SF)*TZN(N)) | ATMOSU | 303 |
| 104 | CONTINUE | ATMOSU | 304 |
| | CALL FITTER(NZHT,ZHT,TZN,11, 2, 2, AA) | ATMOSU | 305 |
| C | COMPUTE GRAV. ACCEL. G, G DIVIDED BY MOL. SCALE TEMP. TM, AND | ATMOSU | 306 |
| C | INTEGRAL OF G/TM AT 120 KM. | ATMOSU | 307 |
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| | GDTM = GDTMAF(ZH) | ATMOSU | 309 |
| | GDTMI = GDTMAF(ZH) | ATMOSU | 310 |
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| C | THE BOUNDARY CONDITIONS AT 120 KM FOR THE HIGH-ALTITUDE MODEL. | ATMOSU | 313 |
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| | RHO = 3IGMS*GDTM/RR*PP/GG | ATMOSU | 315 |
| C | CALCULATE DENSITY AT 5 KM FOR USE IN SUBROUTINE WATER. | ATMOSU | 316 |
| | PP5 = PZ*EXP(-CCI*GDTMAF(5.)) | ATMOSU | 317 |
| | RHOS5M = 3IGMS*GDTMAF(5.)/RR*PP5/GAF(5.) | ATMOSU | 318 |
| C | INITIALIZE SUBROUTINE SPCMIN | ATMOSU | 319 |
| | CALL SPCMIN(1,ZH) | ATMOSU | 320 |
| C | EVALUATE BMBMS AT 120. KM | ATMOSU | 321 |
| | SF = SPDAF(ZH) | ATMOSU | 322 |
| | BMBMS = 1.0/(1. + SF) | ATMOSU | 323 |
| | PZ = BMBMS*GG/GDTM | ATMOSU | 324 |
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| C | COMPUTE TOTAL NUMBER DENSITY, N(1/CM**3) | ATMOSU | 326 |
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| C | COMPUTE TOTAL NUMBER DENSITY IF NO DISSOCIATION, NSTAN(1/CM**3) | ATMOSU | 328 |
| | SNS = BICA*RHO/BIGMS | ATMOSU | 329 |
| C | COMPUTE DENSITIES (1/CM**3) OF N2, O2, O, AR, He, AND CO2. | ATMOSU | 330 |
| | SNIZ(1) = 0.78*SNS | ATMOSU | 331 |
| | SNIZ(2) = 1.211*SNS - SN | ATMOSU | 332 |
| | SNIZ(3) = 2.*SNS*SF | ATMOSU | 333 |
| | SNIZ(4) = 0.009*SNS | ATMOSU | 334 |
| | SNIZ(5) = 4.625E-05*SNS | ATMOSU | 335 |
| | SNIZ(6) = CO2(25) | ATMOSU | 336 |
| C | | ATMOSU | 337 |
| | ZL120 = RL+120. | ATMOSU | 338 |
| | ZGSK = GG/SK | ATMOSU | 339 |
| | CC = PI*HL/12. | ATMOSU | 340 |
| | PP = SBAK | ATMOSU | 341 |
| C | COMPUTE FOURIER COEFFICIENTS USED FOR TAU AT 120 KM. | ATMOSU | 342 |

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A(1) = +2.210150E-02 - 1.970010E-05 * FF      ATMJSU 343
A(2) = +6.712358E-03 - 1.101107E-05 * FF      ATMJSU 344
A(3) = +2.748180E-04 + 3.390522E-07 * FF      ATMJSU 345
A(4) = -5.663477E-04 + 8.669016E-07 * FF      ATMJSU 346
A(5) = -4.652258E-05 + 2.322930E-07 * FF      ATMJSU 347
A(6) = +8.984354E-05 - 1.128157E-07 * FF      ATMJSU 348
B(1) = -3.407398E-03 + 1.900959E-05 * FF      ATMJSU 349
B(2) = -5.428597E-04 + 4.101313E-06 * FF      ATMJSU 350
B(3) = -2.518983E-04 - 5.341112E-07 * FF      ATMJSU 351
B(4) = -1.380845E-04 + 2.075324E-07 * FF      ATMJSU 352
B(5) = +1.358994E-04 + 3.931811E-07 * FF      ATMJSU 353
C      COMPUTE FOURIER COEFFICIENTS USED FOR TIF.
C(1) = +5.443538E+02 + 4.328817E+00 * FF      ATMJSU 354
C(2) = -1.179819E+02 - 6.495360E-01 * FF      ATMJSU 355
C(3) = +3.115091E+01 - 4.766818E-02 * FF      ATMJSU 357
C(4) = +4.069323E+00 + 4.154692E-02 * FF      ATMJSU 358
C(5) = -6.389061E+00 + 1.415760E-02 * FF      ATMJSU 359
C(6) = +1.045482E+00 - 1.995652E-02 * FF      ATMJSU 360
S(1) = -1.138663E+01 - 7.299749E-01 * FF      ATMJSU 361
S(2) = +1.359668E+01 + 2.815729E-03 * FF      ATMJSU 362
S(3) = +9.859158E-01 + 8.138891E-02 * FF      ATMJSU 363
S(4) = +7.061132E-01 - 1.151708E-02 * FF      ATMJSU 364
S(5) = -2.925315E-01 - 4.625236E-02 * FF      ATMJSU 365
C      COMPUTE TAU (1/KM) AND TIF (DEGREES KELVIN)
TAU = A(1)      ATMJSU 367
PIF = C(1)      ATMJSU 368
DO 110 I=1,5    ATMJSU 369
PI = I          ATMJSU 370
SPI = SIN(CC*PI) ATMJSU 371
CPI = COS(CC*PI) ATMJSU 372
TAU = TAU + CPI*A(I+1) + SPI*S(I) ATMJSU 373
110 PIF = PIF + CPI*C(I+1) + SPI*S(I) ATMJSU 374
WRITE(6,8001)TIF,TAU ATMJSU 375
8001 FORMAT (/ ' TIF = *F8.3* DEG K, TAU = *1PE12.5* 1/KM, FROM SUBROUT
      SINE AT4JSU (FORMAT 8001)') ATMJSU 377
C      ATMJSU 378
C      ATMJSU 379
C      TO PROVIDE A CONTINUOUS DENSITY SCALE HEIGHT ACROSS THE
C      BOUNDARY BETWEEN THE LOW- AND HIGH-ALTITUDE MODELS, WE USE A
C      PARABOLIC TRANSITION FUNCTION, ATMJSU 380
C      HMD0 = FHR120 * ZH110**2 + SB * ZH110 + HMD110 ATMJSU 382
C      WHERE ATMJSU 381
C      HR110 = DENSITY SCALE HEIGHT AT 110 KM ATMJSU 384
C      ZH110 = ZH-110. ATMJSU 385
C      SB = APPROXIMATE DERIVATIVE OF DENSITY SCALE HEIGHT
C      AT 110-KM ALTITUDE ATMJSU 386
C      = HR1105-HR1095 ATMJSU 388
C      HR1105 = DENSITY SCALE HEIGHT AT 110.5 KM. ATMJSU 389
C      HR1095 = DENSITY SCALE HEIGHT AT 109.5 KM. ATMJSU 390
C      FHR120 = (HR120 - 10.*SB - HR110)/(120.-110.))**2 ATMJSU 391
C      IN THIS INITIALIZATION CALL WE NEED TO COMPUTE THE DENSITY
C      SCALE HEIGHT AT 120 KM, HR120, ACCORDING TO THE HIGH-ALTITUDE
C      MODEL, WHICH DEPENDS ON HL AND SHAN, AND ALSO THE DENSITY
C      SCALE HEIGHTS ACCORDING TO THE LOW-ALTITUDE MODEL AT 110 KM,
C      110.5 KM, AND 109.5 KM. ATMJSU 393
C      COMPUTE SMALL A. ATMJSU 396
C      SA = (PIF - T2)/TIF ATMJSU 397
C      COMPUTE COEFFICIENT OF M-SUB-1 IN GAMMA-SUB-1 ATMJSU 399

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ZAMT = 1.0E+05*CGSK/(T1F*TAU)
RHO = 0.0
)DRODZM = 0.0
)D 120 I=1,15
SNZSMI = SNIZ(1)*SMI(1)
ZAM = GAMT*SMI(1)
ALGANI = ALP(1) + GAM + 1.0
RHO = RHO + SNZSMI
)DRDZM = DRODZM + SNZSMI*(GAM + ALGANI*SA/(1.-SA))
120 CONTINUE
RHO120 = RHO/DRDZM/TAU
C COMPUTE DENSITY SCALE HEIGHT AT 110 KM.
GDTM = GDTMFP( 110. )
)R110 = 1.0/(CCI*GDTM
      - 2.0/(RE+110.0) - GKKZAP( 110.0 )/GDTM)
C COMPUTE DENSITY SCALE HEIGHT AT 110.5 KM.
)D1105 = GDTMFP( 110.5 )
)R1105 = 1.0/(CCI*GDTM
      - 2.0/(RE+110.5) - GKKZAP( 110.5 )/GDTM)
C COMPUTE DENSITY SCALE HEIGHT AT 109.5 KM.
)D1095 = GDTMFP( 109.5 )
)R1095 = 1.0/(CCI*GDTM
      - 2.0/(RE+109.5) - GKKZAP( 109.5 )/GDTM)
)S = )R1105-)R1095
)R120 = 0.01*()R120 - 10.*)S - )R110)
C
C AT NIGHTTIME, O DIFFERS FROM DAYTIME O ONLY BELOW ALTITUDE
C ZION(5) = 90 KM. IF( ZH.LT.ZION(1)), WHERE ZION(1) = 60 KM,
C SMI(3) = ONZI(1) = ONITE(13) = 1.1
C IF(ZH.GE.ZION(1) .AND. ZH.LT.ZION(2)), WHERE ZION(2) = 75 KM,
C SMI(3) = ONZI(2)*EXP(ZM20M*ONSMCH) WHERE
C ONZI(2) = ONITE(16) = 4.90E+08
C ZM20M = ZH-ZION(2)
C ONSMCH = ALOG(ONZI(2)/ONZI(1))/(ZION(2)-ZION(1))
C IF(ZH.GT.ZION(2) .AND. ZH.LT.ZION(4)) WHERE ZION(4) = 85 KM,
C SMI(3) = ONZI(4)*EXP(-(85.-ZH)/SZ)
C WHERE SZ IS AN ALTITUDE-DEPENDENT SCALE HEIGHT SO DETERMINED
C THAT THE FUNCTION PASSES THROUGH THE DATA POINTS AT 75, 80,
C AND 85 KM,
C SZ = S85 - (S85-S80)*(85.-ZH)/5.
C S80 = 5./ALOG( ONITE(18)/ONITE(17) )
C S85 = 2.*S80 - 10./ALOG( ONITE(18)/ONITE(16) )
C IF(ZH.GT.ZION(4) .AND. ZH.LT.ZION(5)) WHERE ZION(5) = 90 KM,
C SMI(3) = ONZI(4)*EXP(ZM40M/ONSMCH) WHERE
C ONZI(4) = ONITE(18) = 9.0E+10
C ZM40M = ZH - ZION(4)
C )NSCH = (ZION(5) - ZION(4))/ALOG( ONZI(5)/ONZI(4) )
C THE NIGHTTIME O CONSTANTS ARE NOW SET.
C ZION(1) = ALTKM(13)
C )NZI(1) = ONITE(13)
C )D 130 I=2,5
C ZION(1) = ALTKM(1+14)
C )NZI(1) = ONITE(1+14)
130 CONTINUE
)NZ = ZION(5)
C TO RESET ONZI(5) TO ITS PROPER VALUE WE NEED TO FIRST
C CALCULATE ODAYZ5...
ATMUSU 400
ATMUSU 401
ATMUSU 402
ATMUSU 403
ATMUSU 404
ATMUSU 405
ATMUSU 406
ATMUSU 407
ATMUSU 408
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| C | | ATMOSU | 457 |
| C | COMPUTE GRAV. ACCEL. G, G DIVIDED BY MOL. SCALE TEMP. TM, | ATMOSU | 458 |
| C | AND INTEGRAL OF G/TM AT ALTITUDE ZH2. | ATMOSU | 459 |
| C | | ATMOSU | 460 |
| | GG = GAF(ZH2) | ATMOSU | 461 |
| | ZDTM = GDTMFP(ZH2) | ATMOSU | 462 |
| | ZDTMI = GDTMFP(ZH2) | ATMOSU | 463 |
| C | COMPUTE PRESSURE AND DENSITY AT ALTITUDE ZH2 | ATMOSU | 464 |
| | PP = P2*EXP(-CC1*GDTMI) | ATMOSU | 465 |
| | RHO = 31GMS*GDTM/RR*PP/GG | ATMOSU | 466 |
| C | COMPUTE M/NSPAR DAY AT ALTITUDE ZH2 | ATMOSU | 467 |
| | SF = SFDAP(ZH2) | ATMOSU | 468 |
| | UMBMS = 1.0/(1. + SF) | ATMOSU | 469 |
| C | COMPUTE TOTAL NUMBER DENSITY, N(1/CM**3) AT ALTITUDE ZH2 | ATMOSU | 470 |
| | SN = BIGA/BIGMS*RHO/UMBMS | ATMOSU | 471 |
| C | COMPUTE TOTAL NUMBER DENSITY IF NO DISSOCIATION, | ATMOSU | 472 |
| C | NSPAR (1/CM**3) | ATMOSU | 473 |
| | SNS = BIGA*RHO/BIGMS | ATMOSU | 474 |
| | JDAYS = 2.*SNS*SF | ATMOSU | 475 |
| | DNZI(5) = DDAYS | ATMOSU | 476 |
| | JNSCHI = ALOG(DNZI(2)/DNZI(1))/(ZION(2)-ZION(1)) | ATMOSU | 477 |
| | S80 = 5./ALOG(UNITE(18)/UNITE(17)) | ATMOSU | 478 |
| | S85 = 2.*S80 - 10./ALOG(UNITE(18)/UNITE(16)) | ATMOSU | 479 |
| | JNSCH = (ZION(5) - ZION(4))/ALOG(DNZI(5)/DNZI(4)) | ATMOSU | 480 |
| C | | ATMOSU | 481 |
| C | TO PROVIDE A CONTINUOUS TRANSITION IN THE CO2 DENSITY BETWEEN | ATMOSU | 482 |
| C | THE ALTITUDE OF 100 KM, BELOW WHICH A CONSTANT MIXING RATIO | ATMOSU | 483 |
| C | IS ASSUMED, AND THE ALTITUDE OF 120 KM, AT WHICH THE ATMOSU | ATMOSU | 484 |
| C | HIGH-ALTITUDE MODEL (BASED ON DIFFUSIVE EQUILIBRIUM) BEGINS, | ATMOSU | 485 |
| C | WE USE THE POLYNOMIAL | ATMOSU | 486 |
| C | LOG10(SMI(6)) = SUM(XC(I)*ZMICO2**(I-1)), I=1,7 | ATMOSU | 487 |
| C | WHERE THE CONSTANTS XC(I), I=1,7, ARE DETERMINED SO THAT THE | ATMOSU | 488 |
| C | SLOPE OF ALOG10(SMI(6)) AT ZICO2(1) = 100 KM, DLGZ1Z, AND | ATMOSU | 489 |
| C | AT ZICO2(5) = 120 KM, DLGZ5Z, IS CONTINUOUS AND ALOG10(SMI(6)) | ATMOSU | 490 |
| C | EQUALS THE VALUES FOR CO2 AT ZICO2(1) = 100,105,110,115, AND | ATMOSU | 491 |
| C | 120 KM FOR I=1,5. | ATMOSU | 492 |
| C | THE CO2 CONSTANTS ARE NOW SET... | ATMOSU | 493 |
| | DD 160 I=1,5 | ATMOSU | 494 |
| | EICO2(I) = ALTKM(I+20) | ATMOSU | 495 |
| | COZZI(I) = COZ(I+20) | ATMOSU | 496 |
| 160 | CONTINUE | ATMOSU | 497 |
| C | RESET COZZI(I) TO THE VALUE OBTAINED FROM THE LOW-ALTITUDE | ATMOSU | 498 |
| C | MODEL AT ALTITUDE ZICO2(1) = 100 KM. TO DO THIS WE MUST FIRST | ATMOSU | 499 |
| C | COMPUTE GRAV. ACCEL. G, G DIVIDED BY MOL. SCALE TEMP. TM, AND | ATMOSU | 500 |
| C | INTEGRAL OF G/TM AT 100 KM. | ATMOSU | 501 |
| C | | ATMOSU | 502 |
| C | COMPUTE GRAV. ACCEL. G, G DIVIDED BY MOL. SCALE TEMP. TM, AND | ATMOSU | 503 |
| C | INTEGRAL OF G/TM AT 100 KM | ATMOSU | 504 |
| | GG = GAF(100.) | ATMOSU | 505 |
| | ZDTM = GDTMFP(100.) | ATMOSU | 506 |
| | ZDTMI = GDTMFP(100.) | ATMOSU | 507 |
| C | COMPUTE PRESSURE AND DENSITY AT 100 KM | ATMOSU | 508 |
| | PP = P2*EXP(-CC1*GDTMI) | ATMOSU | 509 |
| | RHO = BIGMS*GDTM/RR*PP/GG | ATMOSU | 510 |
| C | COMPUTE TOTAL NUMBER DENSITY IF NO DISSOCIATION, | ATMOSU | 511 |
| C | NSPAR, AT 100 KM. | ATMOSU | 512 |
| | SNS = BIGA*RHO/BIGMS | ATMOSU | 513 |

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| | COZ21(1) = 3.20E-04 * SMS | ATMOSU | 514 |
| | CC(7) = ALOG10(COZ21(1)) | ATMOSU | 515 |
| C | THE SLOPE OF ALOG10(S41(6)) AT ALTITUDE ZIC02(1) = 100 KM, | ATMOSU | 516 |
| C | DLCZ1Z, IS GIVEN BY DLCZ1Z = ALOG10(EXP(1.0))*((1./RHO) | ATMOSU | 517 |
| C | *(D(RHO)/DZ)) = ALOG10(EXP(1.0))*(-1./HRMU). | ATMOSU | 518 |
| C | COMPUTE DENSITY SCALE HEIGHT AT 100 KM. | ATMOSU | 519 |
| | HRU100 = 1.0/(CC1*G0FM | ATMOSU | 520 |
| | - 2.0/(HE+100.) - GRKZAF(100.)/G0FM) | ATMOSU | 521 |
| | DLCZ1Z = (-1.0/HRU100)*ALOG10(EXP(1.0)) | ATMOSU | 522 |
| | CC(6) = DLCZ1Z | ATMOSU | 523 |
| | DO 164 I=2,5 | ATMOSU | 524 |
| | Z11C(1) = ZIC02(1)-ZIC02(1) | ATMOSU | 525 |
| 164 | CONTINUE | ATMOSU | 526 |
| | DO 165 I=1,4 | ATMOSU | 527 |
| | Z112 = Z11C(I+1) | ATMOSU | 528 |
| | Z(1,5) = Z112*Z112 | ATMOSU | 529 |
| | DO 165 J=1,4 | ATMOSU | 530 |
| | Z(1,5-J) = Z112*D(I,6-J) | ATMOSU | 531 |
| 165 | CONTINUE | ATMOSU | 532 |
| | Z115 = Z11C(5) | ATMOSU | 533 |
| | Z(5,5) = 2.*Z115 | ATMOSU | 534 |
| | DO 170 J=1,4 | ATMOSU | 535 |
| | FJ1 = J+1 | ATMOSU | 536 |
| | Z(5,5-J) = Z115*((FJ1+1.)/FJ1)*D(5,6-J) | ATMOSU | 537 |
| 170 | CONTINUE | ATMOSU | 538 |
| | DO 175 I=1,4 | ATMOSU | 539 |
| | Z(1,5) = ALOG10(COZ21(I+1)) - XC(6)*Z11C(I+1) - XC(7) | ATMOSU | 540 |
| 175 | CONTINUE | ATMOSU | 541 |
| | DLCZ5Z = ALOG10(EXP(1.0)) *TAU*(SA+SMI(6)*GAMT)/(SA-1.0) | ATMOSU | 542 |
| | Z(5,6) = DLCZ5Z-XC(6) | ATMOSU | 543 |
| | NO = 5 | ATMOSU | 544 |
| | CALL S3LVR(D,XC,NO) | ATMOSU | 545 |
| C | | ATMOSU | 546 |
| C | COMPUTE D DENSITY AT 160 KM FOR USE IN D(10) COMPUTATION IN | ATMOSU | 547 |
| C | SUBROUTINE SPCMIN. | ATMOSU | 548 |
| | ZZ = R1120*(ALTKM(33)-120.)/(HE+ALTKM(33)) | ATMOSU | 549 |
| | ETZ = EXP(-TAU*ZZ) | ATMOSU | 550 |
| | TTDZ = (TIF-(TIF-TZ)*ETZ)/TZ | ATMOSU | 551 |
| | GAM = GAMT*SMI(3) | ATMOSU | 552 |
| | ALGAM1 = ALP(3)*GAM+1.0 | ATMOSU | 553 |
| | S3ZOD = SMI(3)*ETZ**GAM/TTDZ**ALGAM1 | ATMOSU | 554 |
| C | | ATMOSU | 555 |
| C | EVALUATE ATMOSPHERIC PROPERTIES AT 90-KM ALTITUDE PRIOR | ATMOSU | 556 |
| C | TO INITIALIZING IONOSU. | ATMOSU | 557 |
| | ZHSAVE = ZH | ATMOSU | 558 |
| | ZH = 90. | ATMOSU | 559 |
| | JUMP = 0 | ATMOSU | 560 |
| | DO TO 210 | ATMOSU | 561 |
| 177 | JUMP = 2 | ATMOSU | 562 |
| C | INITIALIZE IONOSU ROUTINE. | ATMOSU | 563 |
| | CALL IONOSU(1,24) | ATMOSU | 564 |
| | ZH = ZHSAVE | ATMOSU | 565 |
| C | SET ZHFLAG AND SPIPLG (ARBITRARY NEGATIVE VALUES) | ATMOSU | 566 |
| | SPIPLG = -20. | ATMOSU | 567 |
| | ZHFLAG = -20. | ATMOSU | 568 |
| | RETURN | ATMOSU | 569 |
| CC | | ATMOSU | 570 |

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| CC | | ATMOSU | 571 |
| 200 | CONTINUE | ATMOSU | 572 |
| | IF(ZH.EQ.ZHFLAG) RETURN | ATMOSU | 573 |
| CCC | | ATMOSU | 574 |
| C | AN ERRONEOUS CONDITION WILL OCCUR IF IONJSDR OR SPCMIN IS | ATMOSU | 575 |
| C | CALLED WITH JJ=2 AND A GIVEN VALUE OF ZH IF ATMOSU HAS NOT | ATMOSU | 576 |
| C | BEEN CALLED FIRST WITH JJ=2 AND FOR THE SAME VALUE OF ZH. | ATMOSU | 577 |
| C | THE VARIABLE ZHFLAG IS USED TO DETECT THIS CONDITION AND | ATMOSU | 578 |
| C | TO MAKE THE REQUIRED CALL TO ATMOSU. | ATMOSU | 579 |
| C | ZHFLAG IS INITIALIZED TO AN ARBITRARY NEGATIVE VALUE IN | ATMOSU | 580 |
| C | THE INITIALIZATION CALL TO ATMOSU. | ATMOSU | 581 |
| CCC | | ATMOSU | 582 |
| | ZHFLAG = ZH | ATMOSU | 583 |
| 210 | CONTINUE | ATMOSU | 584 |
| | REZHI = 1.0/(HE+ZH) | ATMOSU | 585 |
| | IF(ZH .GE. 120.) GO TO 250 | ATMOSU | 586 |
| C | | ATMOSU | 587 |
| CCCCC | LOW-ALTITUDE MODEL (ZH .LT. 120.) | ATMOSU | 588 |
| C | | ATMOSU | 589 |
| C | COMPUTE GRAV. ACCEL. AT ALTITUDE ZH, GG(CM/SEC**2). | ATMOSU | 590 |
| | GG = GAF(ZH) | ATMOSU | 591 |
| C | COMPUTE GRAV. ACCEL. DIVIDED BY MOLECULAR-SCALE TEMPERATURE. | ATMOSU | 592 |
| | GDTM = GDTMFP(ZH) | ATMOSU | 593 |
| C | COMPUTE INTEGRAL OF G/TM. | ATMOSU | 594 |
| | GDFMI = GDFMFP(ZH) | ATMOSU | 595 |
| C | COMPUTE FUNCTION NEEDED FOR DENSITY SCALE HEIGHT | ATMOSU | 596 |
| | GKZZ = GKZZAP(ZH) | ATMOSU | 597 |
| C | COMPUTE PRESSURE (DYNES/CM**2) | ATMOSU | 598 |
| | PP = PZ*EXP(-CC1*GDFMI) | ATMOSU | 599 |
| C | COMPUTE DENSITY (G/CM**3) | ATMOSU | 600 |
| | ZHD = 3IGMS*GDTM/HR*PP/GG | ATMOSU | 601 |
| C | COMPUTE DENSITY SCALE HEIGHT (KM). | ATMOSU | 602 |
| | IF(ZH .GE. 110.) GO TO 230 | ATMOSU | 603 |
| | HRHO = 1.0/(CC1*GDTM - 2.0*REZHI - GKZZ/GDTM) | ATMOSU | 604 |
| | GO TO 235 | ATMOSU | 605 |
| 230 | ZHM110 = ZH - 110. | ATMOSU | 606 |
| | HRHO = (PHR120*ZHM110 + SB)*ZHM110 + HRD110 | ATMOSU | 607 |
| C | USE FIT FUNCTION TO UNIVERSAL PROFILE OF SF FUNCTION. | ATMOSU | 608 |
| 235 | SF = SPDAF(ZH) | ATMOSU | 609 |
| | BMBMS = 1.0/(1. + SF) | ATMOSU | 610 |
| C | COMPUTE TEMPERATURE (DEG K) | ATMOSU | 611 |
| | TT = BMBMS*GG/GDTM | ATMOSU | 612 |
| C | COMPUTE NUMBER DENSITIES OF SPECIES. WE PRESCRIBE THE | ATMOSU | 613 |
| C | DAY-NIGHT DEPENDENCE OF O AND USE THE LOW-ALTITUDE MODEL TO | ATMOSU | 614 |
| C | COMPUTE THE ASSOCIATED SLIGHT DAY-NIGHT DEPENDENCE OF O2 . | ATMOSU | 615 |
| | SNS = BIGA*RHU/HIGMS | ATMOSU | 616 |
| | SN = SNS/BMBMS | ATMOSU | 617 |
| | SNI(1) = 0.78*SNS | ATMOSU | 618 |
| | SNI(2) = 1.211*SNS - SN | ATMOSU | 619 |
| | SNI(3) = 2.*SNS*SF | ATMOSU | 620 |
| | IF(IDORN.GE.0) GO TO 245 | ATMOSU | 621 |
| C | COMPUTE NIGHTTIME VALUE OF O | ATMOSU | 622 |
| | IF(ZH .GE. 90.0) GO TO 245 | ATMOSU | 623 |
| | IF(ZH - ZION(4)) 240,240,239 | ATMOSU | 624 |
| C | FIT FOR 85.0 .LT. ZH .LT. 90.0 | ATMOSU | 625 |
| 239 | ZM40H = ZH - ZION(4) | ATMOSU | 626 |
| | SNI(3) = ONZI(4)*EXP(ZM40H/ONSCN) | ATMOSU | 627 |

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| | GO TO 245 | ATMUSU | 628 |
| 240 | IF(ZH - ZION(2)) 242,242,241 | ATMUSU | 629 |
| C | PIF FOR 75.0 .LE. ZH .LE. 85.0 | ATMUSU | 630 |
| 241 | SZ = SMS - (SMS-S80)*(85.-ZH)/5. | ATMUSU | 631 |
| | SNI(3) = ONIZE(10)*EXP(-(85.-ZH)/SZ) | ATMUSU | 632 |
| | GO TO 245 | ATMUSU | 633 |
| 242 | IF(ZH-ZION(1)) 244,243,243 | ATMUSU | 634 |
| C | PIF FOR 60.0 .LE. ZH .LE. 75.0 | ATMUSU | 635 |
| 243 | ZM2OH = ZH-ZION(2) | ATMUSU | 636 |
| | SNI(3) = ONZI(2)*EXP(ZM2OH*ONSCHI) | ATMUSU | 637 |
| | GO TO 245 | ATMUSU | 638 |
| C | PIF FOR ZH .LE. 60.0 | ATMUSU | 639 |
| 244 | SNI(3) = ONZI(1) | ATMUSU | 640 |
| C | FOR ZH .GE. 90.0, USE DAY SNI(3). PROCEED WITH OTHER SPECIES. | ATMUSU | 641 |
| 245 | SNI(4) = 0.009*SMS | ATMUSU | 642 |
| | SNI(5) = 4.625E-05*SMS | ATMUSU | 643 |
| | IF(ZH.LE.100.) GO TO 246 | ATMUSU | 644 |
| | ZM1C02 = ZH-ZIC02(1) | ATMUSU | 645 |
| | SNI(5) = 10.**((((XC(1)*ZM1C02 + XC(2))*ZM1C02 + XC(3))*ZM1C02 | ATMUSU | 646 |
| | * XC(4))*ZM1C02 + XC(5))*ZM1C02 + XC(6))*ZM1C02 + XC(7)) | ATMUSU | 647 |
| | GO TO 247 | ATMUSU | 648 |
| 246 | SNI(6) = 3.20E-04 * SMS | ATMUSU | 649 |
| C | COMPUTE FRACTIONAL ERROR FROM HYDROSTATIC EQUILIBRIUM... | ATMUSU | 650 |
| C | PEUSEQ = -1.0E-05*DPPDZH/(RHO*GG) - 1.0 | ATMUSU | 651 |
| C | = -2.66709952E-12 * RR * ZH**1.833 / (BIGNS * GDTM) | ATMUSU | 652 |
| C | #HEREK 2.66709952E-12 = 1.0E-05 * 2.833 * 9.4144E-08 | ATMUSU | 653 |
| 247 | PEUSEQ = -2.66709952E-12 * RR * ZH**1.833 / (BIGNS * GDTM) | ATMUSU | 654 |
| | IF(JUMP.EQ.0) GO TO 177 | ATMUSU | 655 |
| | RETURN | ATMUSU | 656 |
| C | | ATMUSU | 657 |
| CCCCC | HIGH-ALTITUDE MODEL (ZH .GE. 120.) | ATMUSU | 658 |
| C | | ATMUSU | 659 |
| C | COMPUTE THE GEOPOTENTIAL ALTITUDE ABOVE 120 KM, ZZ(KM). | ATMUSU | 660 |
| 250 | CONTINUE | ATMUSU | 661 |
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| | DRDDZH = 0.0 | ATMUSU | 670 |
| | DPPDZH = 0.0 | ATMUSU | 671 |
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C      IF(ZH.LT.120.) TX = TT IONOSU 202
C      IF(ZH.GE.120.) TXT = SQRT( ZHM120/A ) IONOSU 203
C      WHERE IONOSU 204
C      ZHM120 = ZH-120. IONOSU 205
C      A = 80. / 500.**2 IONOSU 206
CCC IONOSU 207
C      THE REQUIRED QUANTITY FOR THE D-REGION CHEMISTRY IS OBTAINED IONOSU 208
C      AS FOLLOWS... IONOSU 209
C      DQ IS FORCED TO EQUAL THE VALUE OF EPQ AT THE BOTTOM OF THE IONOSU 210
C      GRID (90-KM) AND IS DETERMINED BY INPUT DATA AT LOWER IONOSU 211
C      ALTITUDES. IONOSU 212
C      NOTE ... QDEF = DQ OR QDEF = EPQ DEPENDING ON THE IONOSU 213
C      ALTITUDE ZM. IONOSU 214
CCC IONOSU 215
C      FOR DAYTIME... IONOSU 216
C      IONOSU 217
C      IF(ZH.LE.60.) IONOSU 218
C      DQ = UQDAY(7) * QD1307**(ZHMZ07/Z13M01) IONOSU 219
C      QD1307 = UQDAY(13)/UQDAY(7) IONOSU 220
C      ZHMZ07 = ZH-ALTK4(7) IONOSU 221
C      Z13M07 = ALTKM(13)-ALTKM(7) IONOSU 222
C      IF(60.LT.ZH .AND. ZH.LT.90.) IONOSU 223
C      DQ = UQDAY(13) * QD1913**(ZHMZ13/Z19M13) IONOSU 224
C      QD1913 = EPQZ19/DQDAY(13) IONOSU 225
C      ZHMZ13 = ZH-ALTK4(13) IONOSU 226
C      Z19M13 = ALTKM(19)-ALTK4(13) IONOSU 227
CCC IONOSU 228
C      FOR NIGHTTIME... IONOSU 229

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| C | | IOMOSU | 230 |
| C | IF(ZH.LE.60.) | IOMOSU | 231 |
| C | D2 = DQMIT(7) * QM1307**(ZHM207/Z13M07) | IOMOSU | 232 |
| C | QM1307 = DQMIT(13)/DQMIT(7) | IOMOSU | 233 |
| C | | IOMOSU | 234 |
| C | IF(60.LT.ZH .AND. ZH.LT.90.) | IOMOSU | 235 |
| C | D4 = DQMIT(13) * QM1913**(ZHMZ13/Z19M13) | IOMOSU | 236 |
| C | QM1913 = EFQZ19/DQMIT(13) | IOMOSU | 237 |
| CCC | | IOMOSU | 238 |
| |)DIMENSION GAM(4) | IOMOSU | 239 |
| |)DIMENSION DQDAY(18),DQMIT(18) | IOMOSU | 240 |
| | COMMON/ALTODN/ ALTKM(47),UNITE(18),CU2(25),S3Z00 | KUMM01 | 2 |
| | COMMON/ATMOUP/ HL,SBAR,IDURN,PP,RHO,TT,SMI(33),HWH0,FEHSE0 | KUMM02 | 2 |
| | COMMON/IUMJUP/ EFE,SFOP,EFOP,EFN2P,EFU2P,TE,QDEF | KUMM04 | 2 |
| | COMMON/ZHCHEX/ ZHFLAG,SPIPLG | KUMM09 | 2 |
| CCC | | IOMOSU | 245 |
| | DATA EBOTD,HEBUTD,EF2MXD,HP2MXD,P2DSCH,EDDSCH / 1.0E+05,1.0E+02, | IOMOSU | 246 |
| | * 7.0E+05,3.0E+02,2.0E+02,5.0 / | IOMOSU | 247 |
| | DATA EBOTN,HEBOTN,EF2MXN,HP2MXN,P2NSCH,EDNSCH / 1.0E+03,1.0E+02, | IOMOSU | 248 |
| | * 4.0E+05,3.6E+02,2.0E+02,5.0 / | IOMOSU | 249 |
| | DATA PKT120,PKT200,PKT800 / 0.0,5.0E+02,1.8E+03 / | IOMOSU | 250 |
| | DATA PI / 3.141592653590 / | IOMOSU | 251 |
| C | INTERIM VALUES 06/10/75 | IOMOSU | 252 |
| | DATA (DQDAY(I), I=1,18)/6*0.,3.3,5*0.,0.06,5*0./ | IOMOSU | 253 |
| C | INTERIM VALUES 06/10/75 | IOMOSU | 254 |
| | DATA (DQMIT(I), I=1,18)/6*0.,3.3,5*0.,0.06,5*0./ | IOMOSU | 255 |
| CCC | | IOMOSU | 256 |
| | GO TO (100,200), JJ | IOMOSU | 257 |
| C | INITIALIZATION, CALLED FROM SUBROUTINE ATMOSU DURING ITS | IOMOSU | 258 |
| C | INITIALIZATION. | IOMOSU | 259 |
| | 100 CONTINUE | IOMOSU | 260 |
| | PE02 = PI/2. | IOMOSU | 261 |
| | E2PE02 = 0.50*(HP2MXN+HEBOTN) | IOMOSU | 262 |
| | H2PE02 = 0.50*(HP2MXN-HEBOTN) | IOMOSU | 263 |
| | ALC2D1 = 0.50*ALOG10(EF2MXN/EBOTN) | IOMOSU | 264 |
| | EPEA = ALOG10(EBOTD/EF2MXD)/(HP2MXD-HEBOTD)**2 | IOMOSU | 265 |
| | A = 80. / (500.*500.) | IOMOSU | 266 |
| C | INITIALIZATION FOR D-REGION Q... | IOMOSU | 267 |
| C | COMPUTE ELECTRON TEMPERATURE AT 90-KM ALTITUDE | IOMOSU | 268 |
| | TX = TT | IOMOSU | 269 |
| | IF(1DJRN.LT.0) GO TO 150 | IOMOSU | 270 |
| C | COMPUTE DAYTIME ELECTRON DENSITY AT 90 KM | IOMOSU | 271 |
| | EPE = EBOTD * EXP((90.-HEBOTD)/EDDSCH) | IOMOSU | 272 |
| | GO TO 130 | IOMOSU | 273 |
| C | COMPUTE NIGHTTIME ELECTRON DENSITY AT 90-KM ALTITUDE | IOMOSU | 274 |
| 150 | EPE = EBOTN * EXP((90. - HEBOTN)/EDNSCH) | IOMOSU | 275 |
| 180 | ALP1 = RATCOP(10, TX) + RATCOP(11, TX)*EPE | IOMOSU | 276 |
| | + 1.5E-07*SQRT(EPE)/TX**3 | IOMOSU | 277 |
| | ALP2 = RATCOP(2, TX) | IOMOSU | 278 |
| | ALP3 = RATCOP(3, TX) | IOMOSU | 279 |
| | ALP4 = RATCOP(4, TX) | IOMOSU | 280 |
| CCC | | IOMOSU | 281 |
| C | SET SPIPLG=2.*ZH SO THAT A CALL TO SPCMIN WILL GET SMI(7) | IOMOSU | 282 |
| C | AND SMI(8). ALSO SET ZHFLAG=ZH SO THAT AN UNNECESSARY CALL | IOMOSU | 283 |
| C | WILL NOT BE MADE TO ATMJSU. THE CALL **CALL ATMJSU(2,90.)** | IOMOSU | 284 |
| C | HAS EFFECTIVELY BEEN MADE DURING THE INITIALIZATION CALL | IOMOSU | 285 |
| C | TO ATMOSU. | IOMOSU | 286 |

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| CCC | ZHFLAG = ZH | IUNUSU | 287 |
| | ZHIFLG = ZH*ZH | IUNUSU | 288 |
| | CALL SPCMIN(2,ZH) | IUNUSU | 289 |
| | BET21 = MATCOP(5,TT)*SNI(1) | IUNUSU | 290 |
| | BET23 = MATCOP(7,TT)*SNI(3) | IUNUSU | 291 |
| | BET24 = MATCOP(8,TT)*SNI(7) + MATCOP(9,TT)*SNI(8) | IUNUSU | 292 |
| | BET41 = MATCOP(6,TT)*SNI(2) | IUNUSU | 293 |
| | BET11 = BET21 + BET41 | IUNUSU | 294 |
| | A1 = SNI(3) | IUNUSU | 295 |
| | A2 = SNI(8)*2. | IUNUSU | 296 |
| | A3 = SNI(1)*2. | IUNUSU | 297 |
| | A4 = SNI(2)*2. | IUNUSU | 298 |
| | SAI = A1 + A2 + A3 + A4 | IUNUSU | 299 |
| | GAM(1) = A1/SAI | IUNUSU | 300 |
| | GAM(2) = A2/SAI | IUNUSU | 301 |
| | GAM(3) = A3/SAI | IUNUSU | 302 |
| | GAM(4) = A4/SAI | IUNUSU | 303 |
| | AP = GAM(1)/ALP1 + GAM(2)/ALP2 + GAM(3)/ALP3 + GAM(4)/ALP4 | IUNUSU | 304 |
| | 3P = BET21*(1.0/ALP2 - 1.0/ALP1) + BET41*(1.0/ALP4 - 1.0/ALP1) | IUNUSU | 305 |
| | CP = BET23*(1.0/ALP2 - 1.0/ALP3) | IUNUSU | 306 |
| | JP = BET24*(1.0/ALP2 - 1.0/ALP4) | IUNUSU | 307 |
| | A2DEN = BET23 + ALP3*EFE | IUNUSU | 308 |
| | A3DEN = BET24 + ALP4*EFE | IUNUSU | 309 |
| | FACTA3 = DP/A3DEN | IUNUSU | 310 |
| | 3IGA = AP + CP*GAM(3)/A2DEN + FACTA3*GAM(4) | IUNUSU | 311 |
| | 3IGB = 3P + FACTA3*BET41 | IUNUSU | 312 |
| | FACTQ = BET11 + ALP1*EFE | IUNUSU | 313 |
| | EPQZ19 = EFE*EFE/(3IGA + 3IGB*GAM(1)/FACTQ) | IUNUSU | 314 |
| | IF(100RN.LT.0) GO TO 190 | IUNUSU | 315 |
| | D01913 = EPQZ19/DQDAY(13) | IUNUSU | 316 |
| | D01307 = DQDAY(13)/DQDAY(7) | IUNUSU | 317 |
| | D0 TO 195 | IUNUSU | 318 |
| 190 | D01913 = EPQZ19/DQMIT(13) | IUNUSU | 319 |
| | D01307 = DQMIT(13)/DQMIT(7) | IUNUSU | 320 |
| 195 | CONTINUE | IUNUSU | 321 |
| | Z19M13 = ALTKM(19)-ALTKM(13) | IUNUSU | 322 |
| | Z13M07 = ALTKM(13)-ALTKM(7) | IUNUSU | 323 |
| | RETURN | IUNUSU | 324 |
| CC | | IUNUSU | 325 |
| CC | | IUNUSU | 326 |
| 200 | CONTINUE | IUNUSU | 327 |
| | IF(ZH.NE.ZHFLAG) CALL ATNUSU(2,ZH) | IUNUSU | 328 |
| CCC | | IUNUSU | 329 |
| C | AN ERRONEOUS CONDITION WILL OCCUR IF IUNUSU IS CALLED WITH | IUNUSU | 330 |
| C | JJ=2 AND A GIVEN VALUE OF ZH IF ATNUSU HAS NOT BEEN CALLED | IUNUSU | 331 |
| C | FIRST WITH JJ=2 AND FOR THE SAME VALUE OF ZH. | IUNUSU | 332 |
| C | THE VARIABLE ZHFLAG IS USED TO DETECT THIS CONDITION AND | IUNUSU | 333 |
| C | TO MAKE THE REQUIRED CALL TO ATNUSU. | IUNUSU | 334 |
| C | ZHFLAG IS INITIALIZED TO AN ARBITRARY NEGATIVE VALUE IN | IUNUSU | 335 |
| C | THE INITIALIZATION CALL TO ATNUSU. | IUNUSU | 336 |
| CCC | | IUNUSU | 337 |
| | IF(ZH.GE.90.) GO TO 205 | IUNUSU | 338 |
| C | SET ELECTRON TEMPERATURE FOR ZH.LT.90. | IUNUSU | 339 |
| | TK = TT | IUNUSU | 340 |
| C | Z&R) EFE, EFOP, AND EFMJLP FOR ZH.LT.90. | IUNUSU | 341 |
| | EFE = EFOP = EFMJLP = 0.0 | IUNUSU | 342 |
| | | IUNUSU | 343 |

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| C | PROCEED WITH DQ CALCULATION FOR ZH-LT.90. | 104050 | 344 |
| | IF(1DJRN.LT.0) GO TO 350 | 104050 | 345 |
| C | COMPUTE DAYTIME DQ | 104050 | 346 |
| | IF(ZH-LE.60.) GO TO 325 | 104050 | 347 |
| C | COMPUTE DAYTIME DQ FOR 60.LT.ZH-LT.90. | 104050 | 348 |
| | ZHMZ13 = ZH-ALTKM(13) | 104050 | 349 |
| | DQ = DQDAY(13) * QD1913**(ZHMZ13/Z19M13) | 104050 | 350 |
| | GO TO 385 | 104050 | 351 |
| J25 | CONTINUE | 104050 | 352 |
| C | COMPUTE DAYTIME DQ FOR ZH-LE.60. | 104050 | 353 |
| | ZHMZ07 = ZH-ALTKM(7) | 104050 | 354 |
| | DQ = DQDAY(7) * QD1307**(ZHMZ07/Z13M07) | 104050 | 355 |
| | GO TO 385 | 104050 | 356 |
| J50 | CONTINUE | 104050 | 357 |
| C | COMPUTE NIGHTTIME DQ | 104050 | 358 |
| | IF(ZH-LE.60.) GO TO 375 | 104050 | 359 |
| C | COMPUTE NIGHTTIME DQ FOR 60.LT.ZH-LT.90. | 104050 | 360 |
| | ZHMZ13 = ZH-ALTKM(13) | 104050 | 361 |
| | DQ = DQNT(13) * QN1913**(ZHMZ13/Z19M13) | 104050 | 362 |
| | GO TO 385 | 104050 | 363 |
| J75 | CONTINUE | 104050 | 364 |
| C | COMPUTE NIGHTTIME DQ FOR ZH-LE.60. | 104050 | 365 |
| | ZHMZ07 = ZH-ALTKM(7) | 104050 | 366 |
| | DQ = DQNT(7) * QN1307**(ZHMZ07/Z13M07) | 104050 | 367 |
| J85 | DOEP = DQ | 104050 | 368 |
| | SNI(9) = 0.0 | 104050 | 369 |
| | SNI(10) = 0.0 | 104050 | 370 |
| | SNI(11) = 0.0 | 104050 | 371 |
| | SNI(12) = TX | 104050 | 372 |
| | SNI(28) = 0.0 | 104050 | 373 |
| | SNI(29) = 0.0 | 104050 | 374 |
| | RETURN | 104050 | 375 |
| CCC | | 104050 | 376 |
| 205 | IF(1DJRN-LT.0) GO TO 250 | 104050 | 377 |
| CCC | | 104050 | 378 |
| C | COMPUTE DAYTIME ELECTRON DENSITY AND TEMPERATURE OF | 104050 | 379 |
| | E- AND F-REGIONS. | 104050 | 380 |
| CCC | | 104050 | 381 |
| C | ELECTRON DENSITY | 104050 | 382 |
| | IF(ZH-HEBOTD) 210,212,212 | 104050 | 383 |
| 210 | EPE = EBOTD * EXP((ZH-HEBOTD)/EDDSCH) | 104050 | 384 |
| | GO TO 220 | 104050 | 385 |
| 212 | IF(ZH-HF2MKD) 214,214,216 | 104050 | 386 |
| 214 | EPE = EF2MKD * 10.** (EPEA*(HF2MKD-ZH)**2) | 104050 | 387 |
| | GO TO 220 | 104050 | 388 |
| 216 | EPE = EF2MKD * EXP((HF2MKD-ZH)/F2DSCH) | 104050 | 389 |
| C | ELECTRON TEMPERATURE | 104050 | 390 |
| 220 | IF(ZH-120.) 222,224,224 | 104050 | 391 |
| 222 | TX = TT | 104050 | 392 |
| | GO TO 280 | 104050 | 393 |
| 224 | ZHM120 = ZH-120. | 104050 | 394 |
| | TX = TT + SQRT(ZHM120/A) | 104050 | 395 |
| | GO TO 280 | 104050 | 396 |
| CCC | | 104050 | 397 |
| C | COMPUTE NIGHTTIME ELECTRON DENSITY AND TEMPERATURE OF | 104050 | 398 |
| | E- AND F-REGIONS. | 104050 | 399 |
| CCC | | 104050 | 400 |

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| C | ELECTRON DENSITY | IOMJSU | 401 |
| | 250 IF(ZH-HERJTN) 260,262,262 | IOMJSU | 402 |
| | 260 EPE = EBUTM * EXP((ZH-HERJTN)/EDNSCH) | IOMJSU | 403 |
| | GO TO 270 | IOMJSU | 404 |
| | 262 IF(ZH-HF2MXN) 264,264,266 | IOMJSU | 405 |
| | 264 EPE = EBUTM * 10.** (ALG2D1*(1.0+SIGN(PID2*(ZH-H2PHU2)/H2MUD2))) | IOMJSU | 406 |
| | GO TO 270 | IOMJSU | 407 |
| | 266 EPE = EF2MXN * EXP((HF2MXN-ZH)/F2NSCH) | IOMJSU | 408 |
| C | ELECTRON TEMPERATURE | IOMJSU | 409 |
| | 270 TX = TT | IOMJSU | 410 |
| CCC | | IOMJSU | 411 |
| C | COMPUTE EPE, EFP, EFNOP, EFN2P, AND EFD2P | IOMJSU | 412 |
| CCC | | IOMJSU | 413 |
| C | EPE | IOMJSU | 414 |
| | 280 ALP1 = RATCOP(10, TX) + RATCOP(11, TX)*EPE | IOMJSU | 415 |
| | \$ + 1.5E-07*SQRT(EPE)/TX**3 | IOMJSU | 416 |
| | ALP2 = RATCOP(2, TX) | IOMJSU | 417 |
| | ALP3 = RATCOP(3, TX) | IOMJSU | 418 |
| | ALP4 = RATCOP(4, TX) | IOMJSU | 419 |
| | IF(ZH-NE-SPIPLG) CALL SPCMIN(2, ZH) | IOMJSU | 420 |
| CCC | | IOMJSU | 421 |
| C | AN ERRONEOUS CONDITION WILL OCCUR IF IOMJSU IS CALLED WITH | IOMJSU | 422 |
| C | JJ=2 AND A GIVEN VALUE OF ZH IF SPCMIN HAS NOT BEEN CALLED | IOMJSU | 423 |
| C | FIRST WITH JJ=2 AND FOR THE SAME VALUE OF ZH. | IOMJSU | 424 |
| C | THE VARIABLE SPIPLG IS USED TO DETECT THIS CONDITION AND | IOMJSU | 425 |
| C | TO MAKE THE REQUIRED CALL TO SPCMIN. | IOMJSU | 426 |
| CCC | | IOMJSU | 427 |
| C | THE OPTIMUM ORDER IS "CALL ATMOSU(2,ZH)" THEN | IOMJSU | 428 |
| C | "CALL SPCMIN(2,ZH)" AND THEN "CALL IOMJSU(2,ZH)". | IOMJSU | 429 |
| C | ZMPLAG AND SPIPLG WILL DETECT CALLS MADE IN ANY OTHER ORDER. | IOMJSU | 430 |
| CCC | | IOMJSU | 431 |
| C | SPIPLG IS INITIALIZED TO AN ARBITRARY NEGATIVE VALUE IN | IOMJSU | 432 |
| C | THE INITIALIZATION CALL TO ATMOSU. | IOMJSU | 433 |
| CCC | | IOMJSU | 434 |
| | BET21 = RATCOP(5, TT)*SNI(1) | IOMJSU | 435 |
| | BET23 = RATCOP(7, TT)*SNI(3) | IOMJSU | 436 |
| | BET24 = RATCOP(8, TT)*SNI(7) + RATCOP(9, TT)*SNI(8) | IOMJSU | 437 |
| | BET41 = RATCOP(6, TT)*SNI(2) | IOMJSU | 438 |
| | BET11 = BET21 + BET41 | IOMJSU | 439 |
| | A1 = SNI(3) | IOMJSU | 440 |
| | A2 = SNI(8)*2. | IOMJSU | 441 |
| | A3 = SNI(1)*2. | IOMJSU | 442 |
| | A4 = SNI(2)*2. | IOMJSU | 443 |
| | SA1 = A1 + A2 + A3 + A4 | IOMJSU | 444 |
| | GAM(1) = A1/SA1 | IOMJSU | 445 |
| | GAM(2) = A2/SA1 | IOMJSU | 446 |
| | GAM(3) = A3/SA1 | IOMJSU | 447 |
| | GAM(4) = A4/SA1 | IOMJSU | 448 |
| | BP = GAM(1)/ALP1 + GAM(2)/ALP2 + GAM(3)/ALP3 + GAM(4)/ALP4 | IOMJSU | 449 |
| | BP = BET21*(1.0/ALP2 - 1.0/ALP1) + BET41*(1.0/ALP4 - 1.0/ALP1) | IOMJSU | 450 |
| | CP = BET23*(1.0/ALP2 - 1.0/ALP3) | IOMJSU | 451 |
| | CP = BET24*(1.0/ALP2 - 1.0/ALP4) | IOMJSU | 452 |
| | A2DEN = BET23 + ALP3*EPE | IOMJSU | 453 |
| | A3DEN = BET24 + ALP4*EPE | IOMJSU | 454 |
| | FACTA3 = CP/A3DEN | IOMJSU | 455 |
| | BICA = BP + CP*GAM(3)/A2DEN + FACTA3*GAM(4) | IOMJSU | 456 |
| | BIGH = BP + FACTA3*BET41 | IOMJSU | 457 |

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| | FACTQ = BET11 + ALP1*EFE | IUNUSU | 458 |
| | EFQ = EFE*EFE/(BIGA + BIGB*GAM(1)/FACTQ) | IUNUSU | 459 |
| | ZDEF = EFQ | IUNUSU | 460 |
| C | EFDP | IUNUSU | 461 |
| | EFDP = GAM(1)*EFQ/FACTQ | IUNUSU | 462 |
| C | EFN2P, EFO2P, AND EFNOP | IUNUSU | 463 |
| | EFN2P = GAM(3)*EFQ/A2DEN | IUNUSU | 464 |
| | EFO2P = (GAM(4)*EFQ + BET41*EFDP)/A3DEN | IUNUSU | 465 |
| | EFNOP = (GAM(2)*EFQ + BET21*EFO2P + BET23*EFN2P + BET24*EFO2P) | IUNUSU | 466 |
| \$ | / (ALP2*EFE) | IUNUSU | 467 |
| | SNI(3) = EFE | IUNUSU | 468 |
| | SNI(10) = EFO2P | IUNUSU | 469 |
| | SNI(11) = EFNOP | IUNUSU | 470 |
| | SNI(12) = TX | IUNUSU | 471 |
| | SNI(28) = EFN2P | IUNUSU | 472 |
| | SNI(29) = EFO2P | IUNUSU | 473 |
| | RETURN | IUNUSU | 474 |
| | END | IUNUSU | 475 |

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| CCC | SUBROUTINE JULIAN(YRFX,VEQJ,DAYJ) | JULIAN | 2 |
| C | | JULIAN | 3 |
| C | JULIAN IS REVISION 03 (05/21/78) OF SUBROUTINE JULIAN | JULIAN | 4 |
| C | DEVELOPED FOR RJSCUE-KADAK. | JULIAN | 5 |
| C | REVISION 01 (05/04/77) PROVIDES | JULIAN | 6 |
| C | 1. CALCULATION OF (1) THE VARIABLE FYR, THE FRACTIONAL | JULIAN | 7 |
| C | SEASON-YEAR, NEEDED FOR THE NEW WATER VAPOR AND OZONE | JULIAN | 8 |
| C | MODELS AND (2) THE VARIABLE FST, THE FRACTIONAL SUMMER, | JULIAN | 9 |
| C | NEEDED FOR THE SEASONAL INTERPOLATION BETWEEN THE | JULIAN | 10 |
| C | SUMMER AND WINTER TEMPERATURE PROFILES INPUTTED AS | JULIAN | 11 |
| C | DATA FOR THE REVISED LOW-ALTITUDE MAJOR SPECIES MODEL. | JULIAN | 12 |
| C | 2. REVERSAL OF SEASONS IN SOUTHERN HEMISPHERE. | JULIAN | 13 |
| C | REVISION 02 (10/15/77) PROVIDES | JULIAN | 14 |
| C | 3. REVISED COMMENT CARDS. | JULIAN | 15 |
| C | REVISION 03 (05/21/78) PROVIDES | JULIAN | 16 |
| C | 4. DELETION OF VARIABLES KYRS, KNONS, AND KDAYS FROM THE | JULIAN | 17 |
| C | ARGUMENT LIST SINCE THESE VARIABLES ARE NOW SUPPLIED | JULIAN | 18 |
| C | THROUGH TIME COMMON WHERE THEY ARE KNOWN AS IYRS, INONS, | JULIAN | 19 |
| C | AND IDAYS. | JULIAN | 20 |
| C | 5. REVISED COMMENT CARDS. | JULIAN | 21 |
| CCC | | JULIAN | 22 |
| C | SUBROUTINE JULIAN CONVERTS A GREGORIAN DATE AT GREENWICH TO | JULIAN | 23 |
| C | JULIAN DAY NUMBER DAYJ FOR SUBROUTINE SOLORB. | JULIAN | 24 |
| C | SUBROUTINE JULIAN IS VALID FOR YEARS 1901 TO 1999 INCLUSIVE. | JULIAN | 25 |
| CCC | | JULIAN | 26 |
| C | INPUT PARAMETERS | JULIAN | 27 |
| C | TIME COMMON | JULIAN | 28 |
| C | IYRS - NUMBER OF THE YEAR IN THE 1900 S (E.G., 1974 | JULIAN | 29 |
| C | BECOMES 74), IN GREENWICH TIME ZONE. | JULIAN | 30 |
| C | INONS - NUMBER OF THE MONTH (E.G., FEBRUARY BECOMES 2), | JULIAN | 31 |
| C | IN GREENWICH TIME ZONE. | JULIAN | 32 |
| C | IDAYS - DAY OF THE MONTH, IN GREENWICH TIME ZONE. | JULIAN | 33 |
| C | PLAT - NORTH LATITUDE OF POINT P (RADIAN) | JULIAN | 34 |
| CCC | | JULIAN | 35 |
| C | OUTPUT PARAMETERS | JULIAN | 36 |
| C | ARGUMENT LIST | JULIAN | 37 |
| C | YRFX - JULIAN DAY NUMBER (A HALF INTEGER) AT 0 HRS UT | JULIAN | 38 |
| C | ON JANUARY 1 OF THE YEAR OF INTEREST. | JULIAN | 39 |
| C | VEQJ - JULIAN DATE FOR VERNAL EQUINOX. | JULIAN | 40 |
| C | DAYJ - JULIAN DAY NUMBER (A HALF INTEGER) AT 0 HRS UT | JULIAN | 41 |
| C | ON THE DAY OF INTEREST. | JULIAN | 42 |
| C | TIME COMMON | JULIAN | 43 |
| C | FYR = FRACTIONAL SEASON-YEAR | JULIAN | 44 |
| C | BEING 0 ON 1-JAN IN NORTHERN HEMISPHERE AND | JULIAN | 45 |
| C | 0 ON 1-JULY IN SOUTHERN HEMISPHERE. | JULIAN | 46 |
| C | FST = FRACTIONAL SUMMER | JULIAN | 47 |
| C | BEING 1 ON 1-JULY AND 0 ON 1-JAN IN NORTHERN | JULIAN | 48 |
| C | HEMISPHERE AND REVERSED IN SOUTHERN HEMISPHERE. | JULIAN | 49 |
| CCC | | JULIAN | 50 |
| C | DEFINITION OF DATA | JULIAN | 51 |
| C | DAYN(I) - THE CUMULATIVE NUMBER OF DAYS FROM THE BEGINNING | JULIAN | 52 |
| C | OF THE YEAR TO THE END OF THE (I-1)TH MONTH, IN | JULIAN | 53 |
| C | A NON-LEAP YEAR. | JULIAN | 54 |
| CCC | | JULIAN | 55 |
| C | DIMENSION DAYN(12) | JULIAN | 56 |
| C | COMMON/TIME/ IYRS, INONS, IDAYS, ZT, PLAT, PLON, UP, CAT, FYR, FST, RHO5KM | KUMM07 | 2 |
| C | , CHI | KUMM07 | 3 |

| | | | |
|-----|--|--------|----|
| | DATA (DAYN(1),1=1,12) / 0.,31.,59.,90.,120.,151.,181.,212., | JULIAN | 54 |
| | 243.,273.,304.,334. / | JULIAN | 55 |
| | JAYS = 10AYS | JULIAN | 60 |
| | YRS = 1YRS | JULIAN | 61 |
| CCC | | JULIAN | 62 |
| C | THE FIRST TERM FOR DAYJ IS THE JULIAN DAY NUMBER AT 0 HRS UT | JULIAN | 63 |
| C | 1900 JANUARY 1. THE THIRD TERM FOR DAYJ IS THE NUMBER OF | JULIAN | 64 |
| C | EXTRA (LEAP-YEAR) DAYS SINCE 1900 TO THE START OF THE YEAR | JULIAN | 65 |
| C | OF INTEREST. | JULIAN | 66 |
| CCC | | JULIAN | 67 |
| | DAYJ = 2415020.5 + 365.*YRS + AINT((YRS-1.)/4.) | JULIAN | 68 |
| | YRQJ = DAYJ | JULIAN | 69 |
| C | VERNAL EQUINOX OCCURS WITHIN ABOUT 7 SECONDS OF TIME AT | JULIAN | 70 |
| C | 00 HOURS ON 21 MARCH 1974, AT WHICH TIME THE JULIAN DAY | JULIAN | 71 |
| C | NUMBER IS 2442127.5 . FOR NEARBY YEARS THE JULIAN DATE FOR | JULIAN | 72 |
| C | VERNAL EQUINOX WILL BE GIVEN BY VEQJ.. | JULIAN | 73 |
| | VEQJ = 2442127.5 + 365.25*(YRS-74.) | JULIAN | 74 |
| CCC | | JULIAN | 75 |
| C | LEAP IS AN INDEX THAT EQUALS 0 FOR A LEAP YEAR AND OTHERWISE | JULIAN | 76 |
| C | EQUALS 1, 2, OR 3 . | JULIAN | 77 |
| CCC | | JULIAN | 78 |
| | LEAP = MOD(1YRS,4) | JULIAN | 79 |
| | IF(IMONS.LT.3) GO TO 1 | JULIAN | 80 |
| | IF(LEAP.EQ.0) DAYJ = DAYJ+1.0 | JULIAN | 81 |
| 1 | DAYJ = JAYJ + DAYN(IMONS) + (DAYS-1.0) | JULIAN | 82 |
| | DAYYR = 365. | JULIAN | 83 |
| | IF(LEAP.EQ.0) DAYYR = 366. | JULIAN | 84 |
| | PYR = (DAYJ-YRQJ)/DAYYR | JULIAN | 85 |
| | PST = 2.*PYR | JULIAN | 86 |
| | IF(PYR.GT.0.5) PST = 2.-PST | JULIAN | 87 |
| | IF(PLAT.GE.0.0) GO TO 2 | JULIAN | 88 |
| C | CORRECT FOR SOUTHERN HEMISPHERE | JULIAN | 89 |
| | PYR = PYR+0.50 | JULIAN | 90 |
| | IF(PYR.GT.1.0) PYR = PYR-1.0 | JULIAN | 91 |
| | PST = 1.0-PST | JULIAN | 92 |
| 2 | RETURN | JULIAN | 93 |
| | END | JULIAN | 94 |

| | | | |
|-----|--|--------|----|
| CCC | SUBROUTINE OZONE(KK,ZKM,UZ3) | OZONE | 2 |
| C | | OZONE | 3 |
| C | SUBROUTINE OZONE COMPUTES THE LATITUDE AND SEASON DEPENDENCE | OZONE | 4 |
| C | OF OZONE FOR ALTITUDES FROM 0- TO 55-KM. (FOR HIGHER ALTITUDES | OZONE | 5 |
| C | SEE SUBROUTINE SPCMIN) | OZONE | 6 |
| CCC | | OZONE | 7 |
| CCC | THIS IS A NEW ROUTINE FOR RJSOON-IR. | OZONE | 8 |
| CCC | | OZONE | 9 |
| C | INPUT PARAMETERS | OZONE | 10 |
| C | ARGUMENT LIST | OZONE | 11 |
| C | KK = CALCULATION FLAG | OZONE | 12 |
| C | = 1, CALCULATE INITIALIZATION PARAMETERS | OZONE | 13 |
| C | = 2, CALCULATE OZONE MIXING RATIO FOR 0- TO 55-KM | OZONE | 14 |
| C | ZKM = ALTITUDE OF INTEREST, FROM 0- TO 55-KM | OZONE | 15 |
| C | TIME COMMON | OZONE | 16 |
| C | PLAT = NORTH LATITUDE OF POINT (RADIANS) | OZONE | 17 |
| C | FYR = FRACTIONAL SEASON-YEAR, BEING 0 ON 1-JANUARY IN | OZONE | 18 |
| C | NORTHERN HEMISPHERE AND ON 1-JULY IN SOUTHERN | OZONE | 19 |
| C | HEMISPHERE | OZONE | 20 |
| C | OUTPUT PARAMETER | OZONE | 21 |
| C | ARGUMENT LIST | OZONE | 22 |
| C | OZ3 = MIXING RATIO OF OZONE AT ALTITUDE ZKM, IN KG/KG | OZONE | 23 |
| CCC | | OZONE | 24 |
| | COMMON/ATMOSP/ HL,SBAR,LDUMM,PP,RHO,TT,SMI(30),HKHO,PEHSEJ | KUMM02 | 2 |
| | COMMON/TIME/ IYRS,I4ONS,IDAYS,ZT,PLAT,PLJM,UF,CAT,FYR,FST,RHOSKM | KUMM07 | 2 |
| | ,CHI | KUMM07 | 3 |
| | DATA PI / 3.141592653590 / | OZONE | 27 |
| CCC | | OZONE | 28 |
| C | DO TO (100,200), KK | OZONE | 29 |
| C | INITIALIZATION, CALLED FROM SUBROUTINE SPCMIN DURING ITS | OZONE | 30 |
| C | INITIALIZATION. | OZONE | 31 |
| | 100 PI180 = PI/180. | OZONE | 32 |
| | BLL = ABS(PLAT)/PI180 | OZONE | 33 |
| | AA = 2.56E-09*(105.-BLL)*EXP(-(105.-BLL)/47.) | OZONE | 34 |
| | BB = 0.988 + 0.0136*BLL | OZONE | 35 |
| | DD = (1.837 - 0.014*BLL)*1.0E-05 | OZONE | 36 |
| | EE = 0.50/(1.0+EXP(0.077*(BLL-44.))) + 6.0E-05*BLL*BLL - 0.014 | OZONE | 37 |
| | FF = (3LL-35.)/(1.0+EXP(-0.243*(BLL-80.)))**2 | OZONE | 38 |
| | GG = 12.54 - 0.093*BLL + 0.0/(1.0+EXP(-0.318*(BLL-85.5))) | OZONE | 39 |
| | HH = 29.20 - 0.153*BLL - 0.0/(1.0+EXP(0.08*(BLL-10.))) | OZONE | 40 |
| | ALPHT = 0.20 - 6.78E-04*BLL | OZONE | 41 |
| | ZUT = (7.24E-04*BLL + 6.62E-03)*BLL + 46.9 | OZONE | 42 |
| | ALPHA = 0.235 + 0.235/(1.0+EXP(-0.0982*(BLL-37.))) | OZONE | 43 |
| | BETA = 0.55 + 0.40/(1.0+EXP(0.094*(BLL-38.))) | OZONE | 44 |
| | ZUIC = 31.0 - 0.329*BLL + 11.0/(1.0+EXP(-0.112*(BLL-74.))) | OZONE | 45 |
| | ZUIC = 37.5 - 0.193*BLL + 9.47/(1.0+EXP(-0.135*(BLL-75.))) | OZONE | 46 |
| | RETURN | OZONE | 47 |
| | 200 CONTINUE | OZONE | 48 |
| | ZKRM = 0.0 | OZONE | 49 |
| | IF((ZKM.GE.53.) .AND. (ZKM.LE.55.)) ZKRM = 1.0 | OZONE | 50 |
| | BZZ = 88*(ZKM-Z1) | OZONE | 51 |
| | IF(BZZ.GE.50.0) BZZ = 50. | OZONE | 52 |
| | SPZ = FF/(ZKM**5 + 100.) - EE*(ZKM-Z2) | OZONE | 53 |
| | IF(SPZ.GE.50.0) SPZ = 50. | OZONE | 54 |
| | ATZ = ALPHT*(ZKM-ZUT) | OZONE | 55 |
| | SMR = AA*(1.0+0.027*ZKM)/(1.0+EXP(BZZ)) + DD/(1.0+EXP(FFZ)) | OZONE | 56 |
| | SMZ = SMR/(1.0+EXP(ATZ)) | OZONE | 57 |
| | AZZ = -ALPHA*(ZKM-ZUIC) | OZONE | 58 |
| | IF(AZZ.GE.50.) AZZ = 50. | OZONE | 59 |
| | CZZ = BETA*(ZKM-ZUIC) | OZONE | 60 |
| | IF(CZZ.GE.50.) CZZ = 50. | OZONE | 61 |
| | CAPK = (1.05E-06/(1.0+EXP(AZZ))) / (1.0+EXP(CZZ)) | OZONE | 62 |
| | BZZ = 1.465*(ZKM-22.1) | OZONE | 63 |
| | FZZ = 0.70*(ZKM-13.2) | OZONE | 64 |
| | GAMMA = 60.12*(1.0/(1.0+EXP(BZZ)) + 0.655/(1.0+EXP(FZZ))) | OZONE | 65 |
| | ANGLE = (360.*FYR-GAMMA)*PI180 | OZONE | 66 |
| | JZ3T = CAPK*SIN(ANGLE) + SMR | OZONE | 67 |
| | JPSMR = 3.10E-06 - DZ3T | OZONE | 68 |
| | OZ3 = OZ3T + DPSMR*ZKRM*(0.50+SIGN(0.50,DPSMR)) | OZONE | 69 |
| | RETURN | OZONE | 70 |
| | END | OZONE | 71 |

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FUNCTION RATCOF(I,T)
RATCOF 2
C
C     FUNCTION RATCOF PROVIDES THE RATE COEFFICIENTS NEEDED FOR THE
RATCOF 3
C     S- AND F-REGION IONOSPHERE MODEL USED IN RUSCOE-IR.
RATCOF 4
C
C     THIS FUNCTION WAS PREPARED (03/01/78) FOR INTERIM USE
RATCOF 5
C     PENDING DEVELOPMENT BY G. E. TEMPU OF AN ADEQUATE EXTENSION
RATCOF 6
C     OF THE FUNCTION RATE USED IN RUSCOE-RAUAF.
RATCOF 7
C
C     INPUT PARAMETERS
RATCOF 8
C     ARGUMENT LIST
RATCOF 9
C     I - REACTION INDEX (SEE BELOW)
RATCOF 10
C     T - TEMPERATURE (DEG K)
RATCOF 11
C     = ELECTRON AND VIBRATIONAL TEMPERATURE FOR
RATCOF 12
C     REACTIONS 2, 3, 4, 10, AND 11
RATCOF 13
C     = HEAVY-PARTICLE KINETIC TEMPERATURE FOR
RATCOF 14
C     OTHER REACTIONS
RATCOF 15
C
C     OUTPUT PARAMETER
RATCOF 16
C     FUNCTION RATCOF - REACTION RATE COEFFICIENT,
RATCOF 17
C     CM**3/SEC FOR 2-BODY REACTIONS
RATCOF 18
C     CM**6/SEC FOR 3-BODY REACTIONS
RATCOF 19
C
C     REACTIONS INCLUDED...
RATCOF 20
C
C     NO.          REACTION          RATE-COEFFICIENT REFERENCE
RATCOF 21
C     .....
RATCOF 22
C     2A H0+ + E = H(4S) + U      HUANG ET AL.(1975)
RATCOF 23
C     2B H0+ + E = H(2D) + U      HUANG ET AL.(1975)
RATCOF 24
C     3 H2+ + E = H(4S) + H(2D)   BLINDI (1969)
RATCOF 25
C     4 J2+ + E = J + J(10)       WALLS AND DUNN (1974)
RATCOF 26
C     5 O+ + H2 = H0+ + H(4S)     DUNKIN ET AL.(1968)
RATCOF 27
C     6 O+ + O2 = J2+ + U         MCFARLAND ET AL.(1973)
RATCOF 28
C     7 H2+ + O = H0+ + H(2D)     MCFARLAND ET AL.(1973)
RATCOF 29
C     8 J2+ + H(4S) = H0+ + U     GOLDEN ET AL.(1966)
RATCOF 30
C     9 O2+ + H0 = H0+ + O2       FENSHFELD ET AL.(1970)
RATCOF 31
C     10 J+ + E = O + HNO         BLOCK DATA BLKCHM, RUSCOE-RAUAF.
RATCOF 32
C     11 J+ + E + E = J + E       BLOCK DATA BLKCHM, RUSCOE-RAUAF.
RATCOF 33
C     .....
RATCOF 34
C
C     FOR REACTIONS 2 THROUGH 9, RATE COEFFICIENTS ARE TAKEN
RATCOF 35
C     WITHOUT REVIEW AS PRESENTED IN SO-76 (SPICHEL ET AL., JGR
RATCOF 36
C     VOL. 81, 3745(1976)). FOR REACTIONS 10 AND 11, RATE
RATCOF 37
C     COEFFICIENTS ARE TAKEN FROM BLKCHM IN RUSCOE-RAUAF.
RATCOF 38
C
C     DIMENSION RAT(11), POW(11)
RATCOF 39
C     DATA RAT / 0.0, 7.3E-07, 2.9E-07, 2.2E-07, 5.0E-10, 2.0E-11,
RATCOF 40
C     2.5E-10, 1.8E-10, 6.3E-10, 4.4E-12, 1.2E-19 /
RATCOF 41
C     DATA POW / 0.0, 0.50, 0.33, 0.40, 0.0, 0.40, 0.44, 0.0, 0.0,
RATCOF 42
C     0.75, 5.0 /
RATCOF 43
C
C     RATCOF = RAT(I) * (300./T)**POW(I)
RATCOF 44
C     IF( I.EQ.2 ) GO TO 2
RATCOF 45
C     IF( I.EQ.5 ) GO TO 5
RATCOF 46
C     RETURN
RATCOF 47
C 2 RATCOF = RATCOF * (380./300.)**POW(2)
RATCOF 48
C     RETURN
RATCOF 49
C 5 IF( T.LT.600. ) RATCOF = RATCOF*(600./T)
RATCOF 50
C     RETURN
RATCOF 51
C     END
RATCOF 52

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| | | | |
|-----|--|--------|----|
| CCC | SUBROUTINE SOLCYC(DAYJ) | SOLCYC | 2 |
| C | | SOLCYC | 3 |
| C | SUBROUTINE SOLCYC COMPUTES THE SOLAR FLUX SBAR, AN INPUT TO | SOLCYC | 4 |
| C | ATMOSU THROUGH COMMON ATM0UP, BASED ON AN ASSUMED SINUSOIDAL | SOLCYC | 5 |
| C | 11-YR (OR 4018-DAY) VARIATION, WITH THE MAXIMUM VALUE OF 250 | SOLCYC | 6 |
| C | FOR SBAR, ASSOCIATED WITH CIRA-65 MODEL 9, OCCURRING IN | SOLCYC | 7 |
| C | 1958 JUNE 1. THE MINIMUM VALUE OF 65 FOR SBAR IS ASSOCIATED | SOLCYC | 8 |
| C | WITH CIRA-65 MODEL 1. | SOLCYC | 9 |
| CCC | | SOLCYC | 10 |
| C | REVISION 01 (03/01/78) PROVIDES... | SOLCYC | 11 |
| C | 1. REVISED ATM0UP COMMON FOR ROSCOE-12. | SOLCYC | 12 |
| CCC | | SOLCYC | 13 |
| C | INPUT PARAMETER | SOLCYC | 14 |
| C | DAYJ - JULIAN DAY NUMBER (A HALF INTEGER) AT 0 HRS UT | SOLCYC | 15 |
| C | ON THE DAY OF INTEREST. | SOLCYC | 16 |
| CCC | | SOLCYC | 17 |
| C | OUTPUT PARAMETER | SOLCYC | 18 |
| C | SBAR - AVERAGE 10.7-CM SOLAR FLUX, $1.0E-22$ W/(M**2 HZ). | SOLCYC | 19 |
| C | SBAR IS AN INPUT TO ATMOSU THROUGH COMMON ATM0UP. | SOLCYC | 20 |
| CCC | | SOLCYC | 21 |
| C | COMMON/ATM0UP/ HL,SBAR,TDURN,PP,RHO,TT,SNI(30),HNU,PHSEN | KUMMU2 | 2 |
| CCC | | SOLCYC | 23 |
| C | DEFINITION OF DATA | SOLCYC | 24 |
| C | DJ5806 - JULIAN DAY NUMBER ON 1958 JUNE 1 = 2436355.5 | SOLCYC | 25 |
| C | DATA DJ5806 / 2436355.5 / | SOLCYC | 26 |
| C | DATA PI / 3.141592653590 / | SOLCYC | 27 |
| CCC | | SOLCYC | 28 |
| C | PI2 = 2.*PI | SOLCYC | 29 |
| C | SBAR = 157.5 + 92.5*COS((DAYJ-DJ5806)*PI2/4018.) | SOLCYC | 30 |
| C | RETURN | SOLCYC | 31 |
| C | END | SOLCYC | 32 |

| | | | |
|-----|--|--------|----|
| CC: | SUBROUTINE SOLONB(YRFX,VEQJ,DAYJ,SOLLAT,SOLLON) | SOLONB | 2 |
| C | | SOLONB | 3 |
| C | SUBROUTINE SOLONB COMPUTES THE NORTH LATITUDE SOLLAT AND | SOLONB | 4 |
| C | EAST LONGITUDE SOLLON OF THE APPARENT (ACTUAL MOTION) | SOLONB | 5 |
| C | SUBSOLAR POINT, GIVEN THE JULIAN DAY NUMBER AT 0 HRS UT ON | SOLONB | 6 |
| C | JANUARY 1 OF THE YEAR OF INTEREST (YRFX), THE JULIAN DATE AT | SOLONB | 7 |
| C | WHICH VERNAL EQUINOX OCCURS (VEQJ), THE JULIAN DAY NUMBER AT | SOLONB | 8 |
| C | 0 HRS ON THE DAY OF INTEREST (DAYJ), AND THE UNIVERSAL | SOLONB | 9 |
| C | TIME (UT). | SOLONB | 10 |
| C | REVISION 02(10/15/77) PROVIDES... | SOLONB | 11 |
| C | 1. DEFINITION OF A NEW VARIABLE, DELJUT, TO AVOID LOSS OF | SOLONB | 12 |
| C | SIGNIFICANCE IN COMPUTING SOLLON ON A SMALL-WORD MACHINE. | SOLONB | 13 |
| C | 2. REVISION OF THE ARGUMENT IN THE EQUATION-OF-TIME, | SOLONB | 14 |
| C | CONSISTENT WITH ITS DEFINITION. | SOLONB | 15 |
| C | REVISION 03 (03/01/78) PROVIDES... | SOLONB | 16 |
| C | 3. REVISED TIME COMMON FOR MUSCOGEE-IR. | SOLONB | 17 |
| CCC | | SOLONB | 18 |
| C | INPUT PARAMETERS | SOLONB | 19 |
| C | YRFX - JULIAN DAY NUMBER (A HALF INTEGER) AT 0 HRS UT ON | SOLONB | 20 |
| C | JANUARY 1 OF THE YEAR OF INTEREST. | SOLONB | 21 |
| C | VEQJ - JULIAN DATE FOR VERNAL EQUINOX. | SOLONB | 22 |
| C | DAYJ - JULIAN DAY NUMBER (A HALF INTEGER) AT 0 HRS UT | SOLONB | 23 |
| C | ON THE DAY OF INTEREST. | SOLONB | 24 |
| C | UT - UNIVERSAL TIME (DECIMAL HRS). | SOLONB | 25 |
| CCC | | SOLONB | 26 |
| C | OUTPUT PARAMETERS | SOLONB | 27 |
| C | GAT - GREENWICH APPARENT TIME (DECIMAL HRS). | SOLONB | 28 |
| C | GAT IS PLACED IN COMMON TIME. | SOLONB | 29 |
| C | SOLLAT - NORTH LATITUDE OF SUBSOLAR POINT (RADIAN). | SOLONB | 30 |
| C | SOLLON - EAST LONGITUDE OF SUBSOLAR POINT (RADIAN). | SOLONB | 31 |
| CCC | | SOLONB | 32 |
| C | DEFINITIONS AND COMMENTS | SOLONB | 33 |
| C | UTD24 IS THE DECIMAL FRACTION OF DAY CORRESPONDING TO UT. | SOLONB | 34 |
| C | DAYJUT IS THE JULIAN (DECIMAL) DAY NUMBER AT UT HRS ON THE | SOLONB | 35 |
| C | DAY OF INTEREST. | SOLONB | 36 |
| C | DAYNO IS THE NUMBER OF ELAPSED (DECIMAL) DAYS SINCE THE | SOLONB | 37 |
| C | BEGINNING OF THE YEAR AT 0 HRS UT ON JANUARY 1. | SOLONB | 38 |
| C | THE QUANTITY (DAYJUT - ATNT(DAYJUT)), THE WEST LONGITUDE OF | SOLONB | 39 |
| C | THE SUBSOLAR POINT EXPRESSED AS A DECIMAL FRACTION OF 2*PI | SOLONB | 40 |
| C | RADIANS, IS SUBTRACTED FROM 1 TO OBTAIN THE FRACTIONAL EAST | SOLONB | 41 |
| C | LONGITUDE. THE FIRST TWO EXPRESSIONS FOR SOLLON ARE THE EAST | SOLONB | 42 |
| C | LONGITUDE OF THE SUBSOLAR POINT OF THE (FICTITIOUS) MEAN SUN. | SOLONB | 43 |
| C | IT IS POSSIBLE TO MAKE AN APPROXIMATE CORRECTION FOR THE | SOLONB | 44 |
| C | DIFFERENCE BETWEEN THE APPARENT (ACTUAL MOTION) SOLAR TIME | SOLONB | 45 |
| C | AND THE MEAN SOLAR TIME, KNOWN AS THE EQUATION-OF-TIME (SEE, | SOLONB | 46 |
| C | B.S., AMERICAN PRACTICAL NAVIGATOR (ORIGINALLY BY N. | SOLONB | 47 |
| C | BONDITCH), U.S. NAVY H.O. PUB. NO. 9, P. 375, OF 1962 | SOLONB | 48 |
| C | CORRECTED REPRINT EDITION, AVAILABLE FROM U.S. GOV. PRINTING | SOLONB | 49 |
| C | OFFICE). IN THE U.S.A. (IN CONTRAST TO GREAT BRITAIN) THE | SOLONB | 50 |
| C | SIGN OF THE EQUATION-OF-TIME IS CONSIDERED POSITIVE IF THE | SOLONB | 51 |
| C | TIME OF THE MERIDIAN TRANSIT BY THE SUN IS EARLIER THAN 1200 | SOLONB | 52 |
| C | HRS AND NEGATIVE IF LATER THAN 1200 HRS. (NOTE THAT A | SOLONB | 53 |
| C | MERIDIAN TRANSIT BEFORE 1200 HRS CORRESPONDS TO THE EAST | SOLONB | 54 |
| C | LONGITUDE OF THE SUN BEING SMALLER THAN THE VALUE EXPECTED | SOLONB | 55 |
| C | BASED ON A MEAN SUN.) ANNUAL EDITIONS OF THE NAUTICAL | SOLONB | 56 |
| C | ALMANAC PRIOR TO 1962 TABULATED VALUES OF THE EQUATION-OF-TIME | SOLONB | 57 |
| C | AT 12-HR INTERVALS. THESE TABULATED VALUES OF THE EQUATION-OF | SOLONB | 58 |

| | | | |
|-----|--|--------|-----|
| C | -TIME COULD BE ADDED TO THE GREENWICH MEAN TIME (OR UNIVERSAL | SOLGRH | 59 |
| C | TIME) TO OBTAIN THE GREENWICH APPARENT (OR ACTUAL MOTION) | SOLGRH | 60 |
| C | TIME. NEWER ANNUAL EDITIONS OF THE AMERICAN EPHEMERIS AND | SOLGRH | 61 |
| C | NAUTICAL ALMANAC OR THE ASTRONOMICAL EPHEMERIS DO NOT EVEN | SOLGRH | 62 |
| C | EXPLICITLY REFER TO THE TERM EQUATION-OF-TIME. INSTEAD, FOR | SOLGRH | 63 |
| C | MERIDIAN TRANSITS AND OTHER PHENOMENA THAT DEPEND ON HOUR | SOLGRH | 64 |
| C | ANGLES AND GEOGRAPHIC LOCATION, THE NEWER EDITIONS REFER NOT | SOLGRH | 65 |
| C | TO THE GREENWICH MERIDIAN AND TO UNIVERSAL TIME BUT TO A | SOLGRH | 66 |
| C | MERIDIAN 1.002738*(DELTA T) EAST OF THE GEOGRAPHIC MERIDIAN | SOLGRH | 67 |
| C | OF GREENWICH (KNOWN AS THE EPHEMERIS MERIDIAN) AND TO | SOLGRH | 68 |
| C | EPHEMERIS TIME. THE SOLAR EPHEMERIS TRANSIT, WHICH IS THE | SOLGRH | 69 |
| C | EPHEMERIS TIME AT THE INSTANT OF SOLAR TRANSIT ACROSS THE | SOLGRH | 70 |
| C | EPHEMERIS MERIDIAN, IS TABULATED AT 1-DAY INTERVALS IN THE | SOLGRH | 71 |
| C | NEWER EDITIONS. WE HAVE ADOPTED THE DEPARTURE OF THE VALUE OF | SOLGRH | 72 |
| C | THE SOLAR EPHEMERIS TRANSIT FROM 12 HR 00 MIN 00 SEC AS A | SOLGRH | 73 |
| C | CONVENIENT APPROXIMATION TO THE NEGATIVE VALUE OF THE | SOLGRH | 74 |
| C | EQUATION-OF-TIME. IN PARTICULAR, WE HAVE USED VALUES OF THE | SOLGRH | 75 |
| C | SOLAR EPHEMERIS TRANSIT FOR 1974 TABULATED IN THE 1974 EDITION | SOLGRH | 76 |
| C | OF EITHER THE ASTRONOMICAL EPHEMERIS OR THE AMERICAN EPHEMERIS | SOLGRH | 77 |
| C | AND NAUTICAL ALMANAC, AND FITTED OUR ADOPTED VALUES OF THE | SOLGRH | 78 |
| C | EQUATION-OF-TIME BY A FOUR-TERM FOURIER SERIES. WE IGNORE THE | SOLGRH | 79 |
| C | WEAK DEPENDENCE OF THE EQUATION-OF-TIME ON THE YEAR OF | SOLGRH | 80 |
| C | INTEREST. OUR FITTED EXPRESSION FOR THE EQUATION-OF-TIME IS | SOLGRH | 81 |
| C | GIVEN BY | SOLGRH | 82 |
| C | | SOLGRH | 83 |
| C | $EQT = 0.385175 \cdot \cos(P) - 3.146125 \cdot \cos(P2)$ | SOLGRH | 84 |
| C | $- 7.392635 \cdot \sin(P) - 9.536925 \cdot \sin(P2), \text{ MIN}$ | SOLGRH | 85 |
| C | | SOLGRH | 86 |
| C | WHERE | SOLGRH | 87 |
| C | $P = RADDAY \cdot (DAYJ - YRJJ)$ | SOLGRH | 88 |
| C | $P2 = 2 \cdot P$ | SOLGRH | 89 |
| C | $RADDAY = 2 \cdot \pi / 365.25 \text{ RADIANS PER DAY}$ | SOLGRH | 90 |
| C | $= 0.0172024238$ | SOLGRH | 91 |
| C | TO CONVERT FROM MINUTES OF TIME TO RADIANS OF LONGITUDE WE | SOLGRH | 92 |
| C | MUST MULTIPLY EQT BY | SOLGRH | 93 |
| C | $RADMIN = 2 \cdot \pi / 1440 \text{ RADIANS PER MINUTE}$ | SOLGRH | 94 |
| C | $= 0.00436332313$ | SOLGRH | 95 |
| C | THUS, THE EAST LONGITUDE (RADIANS) OF THE APPARENT SUN IS | SOLGRH | 96 |
| C | $SOLLON = SOLLON - RADMIN \cdot EQT$ | SOLGRH | 97 |
| C | THE NORTH LATITUDE (RADIANS) OF THE APPARENT SUN IS | SOLGRH | 98 |
| C | $SOLLAT = SLATMX \cdot \sin((DAYJUT - VEJJ) \cdot RADDAY)$ | SOLGRH | 99 |
| C | WHERE THE MAXIMUM VALUE OF THE SOLAR LATITUDE IS | SOLGRH | 100 |
| C | $SLATMX = 0.409123 \text{ RADIANS}$ | SOLGRH | 101 |
| C | | SOLGRH | 102 |
| CCC | CONJUN/TIME/ LYRS, INONS, IDAYS, ZT, PLAT, PLON, UP, CAT, FYR, FST, RHUSKM | KONM07 | 2 |
| | ,CHI | KONM07 | 3 |
| CCC | DEFINITIONS OF DATA AND CONSTANTS | SOLGRH | 104 |
| C | $P1 = 3.141592653590$ | SOLGRH | 105 |
| C | $P12 = 2 \cdot \pi$ | SOLGRH | 106 |
| C | $RADDAY = P12 / 365.25 \text{ RADIANS PER DAY IN A JULIAN YEAR}$ | SOLGRH | 107 |
| C | $= 0.0172024238$ | SOLGRH | 108 |
| C | $RADMIN = P12 / 1440 \text{ RADIANS PER MINUTE IN A DAY}$ | SOLGRH | 109 |
| C | $= 0.00436332313$ | SOLGRH | 110 |
| C | $SLATMX = \text{MAXIMUM VALUE OF SOLAR LATITUDE}$ | SOLGRH | 111 |
| C | $= 0.409123 \text{ RADIANS}$ | SOLGRH | 112 |
| C | | SOLGRH | 113 |
| CCC | | SOLGRH | 114 |

| | | | |
|------|--|--------|-----|
| DATA | PI,SLATMX / 3.141592653590, 0.409123 / | SOL024 | 115 |
| CCC | PI2 = 2.*PI | SOL026 | 116 |
| | RADDAY = PI2/365.25 | SOL028 | 117 |
| | RADMIN = PI2/1440. | SOL026 | 118 |
| | JTD24 = UT/24. | SOL028 | 119 |
| | DAYJUT = DAYJ + UTD24 | SOL028 | 120 |
| C | TO AVOID LOSS OF SIGNIFICANCE ON A SMALL-WORD MACHINE, | SOL026 | 121 |
| C | INTRODUCE A NEW VARIABLE, DELJUT. | SOL028 | 122 |
| | DELJUT = 0.50 + UTD24 | SOL028 | 123 |
| | DAYNO = DAYJUT - YRFJ | SOL028 | 124 |
| CC | SOLLJM = PI2*(1.0-DELJUT+AINY(DAYJUT)) | SOL028 | 125 |
| | SOLLJM = PI2*(1.0-DELJUT) | SOL028 | 126 |
| | IF(SOLLJM.LT.0.0) SOLLJM = SOLLJM+PI2 | SOL028 | 127 |
| | P = RADDAY*(DAYJ-YRFJ) | SOL028 | 128 |
| | P2 = 2.*P | SOL028 | 129 |
| | EQT = 0.385175* $\cos(P)$ - 3.146125* $\cos(P2)$ | SOL028 | 130 |
| | - 7.392635* $\sin(P)$ - 9.516825* $\sin(P2)$ | SOL028 | 131 |
| | ZAT = UT + EQT/60. | SOL028 | 132 |
| | SOLLJM = SOLLJM - RADMIN*EQT | SOL028 | 133 |
| | SOLLAT = SLATMX*SIN((DAYJUT-VEQJ)*RADDAY) | SOL028 | 134 |
| | RETURN | SOL028 | 135 |
| | END | SOL028 | 136 |
| | | SOL028 | 137 |

| | | |
|---|-------|----|
| SUBROUTINE SOLVE (A, X, NU) | SOLVE | 2 |
| CCC | SOLVE | 3 |
| C | SOLVE | 4 |
| C | SOLVE | 5 |
| C | SOLVE | 6 |
| C | SOLVE | 7 |
| C | SOLVE | 8 |
| CCC | SOLVE | 9 |
| CCC | SOLVE | 10 |
| CCC | SOLVE | 11 |
| C | SOLVE | 12 |
| C | SOLVE | 13 |
| C | SOLVE | 14 |
| C | SOLVE | 15 |
| C | SOLVE | 16 |
| CCC | SOLVE | 17 |
| C | SOLVE | 18 |
| C | SOLVE | 19 |
| CCC | SOLVE | 20 |
| DIMENSION A(20,21), B(20,21), X(20), LOC(20), NU(20) | SOLVE | 21 |
| KNI = NU+1 | SOLVE | 22 |
| DO 150 I=1,NU | SOLVE | 23 |
| DO 150 J=1,KNI | SOLVE | 24 |
| B(I,J) = A(I,J) | SOLVE | 25 |
| 150 CONTINUE | SOLVE | 26 |
| DO 10 N=1,NU | SOLVE | 27 |
| LOC(N) = 0 | SOLVE | 28 |
| 10 ROW(N) = 0.0 | SOLVE | 29 |
| NP = NU+1 | SOLVE | 30 |
| DO 100 I=1,NU | SOLVE | 31 |
| IP = I+1 | SOLVE | 32 |
| C-----FIND MAX ELEMENT IN I-TH COL. | SOLVE | 33 |
| AMAX = 0.0 | SOLVE | 34 |
| DO 2 K=1,NU | SOLVE | 35 |
| IF(AMAX - ABS(A(K,I))) 3,2,2 | SOLVE | 36 |
| C-----IS NEW MAX IN ROW PREVIOUSLY USED AS PIVOT. | SOLVE | 37 |
| 3 IF(NU(K)) 4,4,2 | SOLVE | 38 |
| 4 LOC(I) = K | SOLVE | 39 |
| AMAX = ABS(A(K,I)) | SOLVE | 40 |
| 2 CONTINUE | SOLVE | 41 |
| IF(AMAX) 99,99,98 | SOLVE | 42 |
| C-----MAX ELEMENT IN I-TH COL IS A(L,I) | SOLVE | 43 |
| 98 L = LOC(I) | SOLVE | 44 |
| ROW(L) = 1.0 | SOLVE | 45 |
| C-----PERFORM ELIMINATION, L IS PIVOT ROW, A(L,I) IS PIVOT ELEMENT. | SOLVE | 46 |
| DO 50 J=1,NU | SOLVE | 47 |
| IF(L=J) 6,50,6 | SOLVE | 48 |
| QF = -A(J,I)/A(L,I) | SOLVE | 49 |
| DO 40 K=IP,NU | SOLVE | 50 |
| A(J,K) = A(J,K) + QF*A(L,K) | SOLVE | 51 |
| 40 CONTINUE | SOLVE | 52 |
| 50 CONTINUE | SOLVE | 53 |
| 100 CONTINUE | SOLVE | 54 |
| DO 200 I=1,NU | SOLVE | 55 |
| I = LOC(I) | SOLVE | 56 |
| 200 X(I) = A(L,NU+1)/A(L,I) | SOLVE | 57 |
| C | SOLVE | 58 |
| WRITE(6,103) (J, X(J),J=1,NU) | SOLVE | 59 |
| C 103 | SOLVE | 60 |
| FORMAT (4(18,21,E15.8)) | SOLVE | 60 |
| RETURN | SOLVE | 61 |
| 99 WRITE(6,104) | SOLVE | 61 |
| 104 FORMAT (5X,27H NO UNIQUE SOLUTION EXISTS.) | SOLVE | 62 |
| RETURN | SOLVE | 63 |
| END | SOLVE | 64 |

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SUBROUTINE SOLZEN(SULLAT,SOLLON)
SOLZEN 2
CCC
C SUBROUTINE SOLZEN COMPUTES COSCHI, THE COSINE OF THE ZENITH
SOLZEN 3
C ANGLE OF THE SUN AT A POINT P, GIVEN THE GEOGRAPHIC NORTH
SOLZEN 4
C LATITUDE PLAT AND EAST LONGITUDE PLON OF THE POINT P AND THE
SOLZEN 5
C NORTH LATITUDE SULLAT AND EAST LONGITUDE SOLLON OF THE
SOLZEN 6
C SUBSOLAR POINT. THE DAY-NIGHT PARAMETER IDURN IS 1 FOR
SOLZEN 7
C DAYTIME, I.E., IF(COSCHI.GE.0.0), AND IS -1 FOR NIGHTTIME,
SOLZEN 8
C I.E., IF(COSCHI.LT.0.0). THE LOCAL APPARENT TIME HL
SOLZEN 9
C IS ALSO COMPUTED FROM THE GREENWICH APPARENT TIME CAT AND THE
SOLZEN 10
C LONGITUDE PLON.
SOLZEN 11
C REVISION 01 (06/07/77) PROVIDES
SOLZEN 12
C 1. SOLAR ZENITH ANGLE, CHI (RADIANS)
SOLZEN 13
C REVISION 02 (03/01/78) PROVIDES...
SOLZEN 14
C 2. REVISED ATMOSP AND TIME COMMONS FOR MUSCUE-IR.
SOLZEN 15
CCC
C INPUT PARAMETERS
SOLZEN 16
C PLAT - NORTH LATITUDE OF POINT P (RADIANS)
SOLZEN 17
C PLON - EAST LONGITUDE OF POINT P (RADIANS)
SOLZEN 18
C SULLAT - NORTH LATITUDE OF SUBSOLAR POINT (RADIANS)
SOLZEN 19
C SOLLON - EAST LONGITUDE OF SUBSOLAR POINT (RADIANS)
SOLZEN 20
CCC
C INPUT PARAMETERS
SOLZEN 21
C CHI - ZENITH ANGLE OF THE SUN AT POINT P (RADIANS)
SOLZEN 22
C IDURN - PARAMETER FOR DAY OR NIGHT. IF COSCHI IS
SOLZEN 23
C THE COSINE OF THE ZENITH ANGLE OF THE SUN AT
SOLZEN 24
C POINT P, IDURN IS 1 FOR DAYTIME, I.E.,
SOLZEN 25
C IF(COSCHI.GE.0.0), AND IS -1 FOR NIGHTTIME,
SOLZEN 26
C I.E., IF(COSCHI.LT.0.0). IDURN IS AN INPUT TO
SOLZEN 27
C ATMOSP THROUGH COMMON ATMOSP.
SOLZEN 28
C HL - LOCAL APPARENT TIME (DECIMAL HRS, E.G. 2230 HRS
SOLZEN 29
C BECOMES 22.50 HRS). HL IS AN INPUT TO ATMOSP
SOLZEN 30
C THROUGH COMMON ATMOSP.
SOLZEN 31
CCC
C COMMON/ATMOSP/ HL,SBAR,IDURN,PP,RHU,TT,SNI(30),HRHU,PHSEW
SOLZEN 32
C COMMON/TIME/ IYRS,INONS,IDAYS,ZT,PLAT,PLON,UP,CAT,PYR,PST,RHOSKM
KUMM02 2
C ,CHI
KUMM07 2
DATA PI / 3.141592653590 /
KUMM07 3
CCC
C THE FOLLOWING FORMULA IS BASED ON EQ. (1.41) OF IONOSPHERIC
SOLZEN 33
C RADIO PROPAGATION BY K. DAVIES, MRS MONOGRAPH NO, 1965
SOLZEN 34
C APRIL 1. IT MAY ALSO BE DERIVED BY APPLYING THE LAW OF
SOLZEN 35
C COSINES FOR AN OBLIQUE SPHERICAL TRIANGLE.
SOLZEN 36
C
SOLZEN 37
C COSCHI = SIN(PLAT) * SIN(SULLAT)
SOLZEN 38
C + COS(PLAT) * COS(SULLAT) * COS(PLON-SOLLON)
SOLZEN 39
C
SOLZEN 40
C CHI = ACOS( COSCHI )
SOLZEN 41
C IDURN = 1
SOLZEN 42
C IF( COSCHI.LT.0.0 ) IDURN = -IDURN
SOLZEN 43
C PI2 = 2.*PI
SOLZEN 44
C RADHR = PI/12.
SOLZEN 45
C HL = CAT - (PI2-PLON)/RADHR
SOLZEN 46
C IF( HL.LT.0.0 ) HL = HL+24.
SOLZEN 47
C RETURN
SOLZEN 48
C END
SOLZEN 49
SOLZEN 50
SOLZEN 51
SOLZEN 52
SOLZEN 53
SOLZEN 54
SOLZEN 55

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| | | | |
|-----|---|--------|----|
| CCC | SUBROUTINE SPCMIN(KK,ZH) | SPCMIN | 2 |
| C | FOR ROSCOE-RADAR (MAY 1975), | SPCMIN | 3 |
| C | THE HIGH-ALTITUDE CHEMISTRY MODULE REQUIRES THE MINOR NEUTRAL | SPCMIN | 4 |
| C | SPECIES O, CO2, N, AND NO. PROFILES FOR DAY AND NIGHT AT ALL | SPCMIN | 5 |
| C | ALTITUDES ARE PROVIDED FOR O AND CO2 IN ATMOSU. HERE IN | SPCMIN | 6 |
| C | SPCMIN WE PROVIDE PROFILES OF N AND NO. | SPCMIN | 7 |
| C | THE LOW-ALTITUDE CHEMISTRY MODULE REQUIRES, IN ADDITION TO O, | SPCMIN | 8 |
| C | CO2, N, AND NO, THE MINOR NEUTRAL SPECIES H2O, O2(SINGLET | SPCMIN | 9 |
| C | DELTA G), O3, AND NO2, ALSO PROVIDED BY SPCMIN. | SPCMIN | 10 |
| CCC | | SPCMIN | 11 |
| C | FOR ROSCOE-IR (MARCH 1978), | SPCMIN | 12 |
| C | THE CHEMISTRY-MODEL REQUIRES NEUTRAL SPECIES IN ADDITION TO | SPCMIN | 13 |
| C | THOSE INDICATED ABOVE FOR ROSCOE-RADAR. THUS, SUBROUTINE | SPCMIN | 14 |
| C | SPCMIN ADDITIONALLY PROVIDES ALTITUDE PROFILES OF CO, H2O, | SPCMIN | 15 |
| C | CH4, N, OH, HO2, N(2D), N(2P), AND O(1D), AS WELL AS REVISED | SPCMIN | 16 |
| C | PROFILES OF O3, H2O, N, N(4S), AND NO. | SPCMIN | 17 |
| C | | SPCMIN | 18 |
| C | | SPCMIN | 19 |
| C | REVISION 01 (05/08/78) PROVIDES | SPCMIN | 20 |
| C | 1. SETTING OF T03 CONSISTS IN THE NIGHTTIME O3 PROFILE. | SPCMIN | 21 |
| C | REVISION 02 (05/21/78) PROVIDES | SPCMIN | 22 |
| C | 2. DELETION OF UNUSED ARRAYS ANONZI(8), X(9), ZIM2NO(8), AND | SPCMIN | 23 |
| C | ZIMON(8). | SPCMIN | 24 |
| C | REVISION 03 (06/24/79) PROVIDES | SPCMIN | 25 |
| C | 3. REMOVAL OF SMALL DISCONTINUITY IN HO2 PROFILE AT 100 KM. | SPCMIN | 26 |
| C | 4. CONNECTION OF KEYPUNCH ERROR IN DATA FOR NIGHTTIME N DENSITY | SPCMIN | 27 |
| C | AT 80 KM (FROM 1.0E+08 TO 1.0E+07). | SPCMIN | 28 |
| C | 5. CONNECTION OF COMMENT-CARD UNITS FOR O3 MASS-MIXING-RATIO | SPCMIN | 29 |
| C | DATA. | SPCMIN | 30 |
| C | 6. LOWER LIMIT OF 1.0 FOR N DENSITY AT NIGHT BETWEEN 74 AND | SPCMIN | 31 |
| C | 75 KM. | SPCMIN | 32 |
| C | 7. CORRECTED CONVERSION OF H2O VOLUME-MIXING RATIO (PPBV) TO | SPCMIN | 33 |
| C | H2O NUMBER DENSITY (1/CM**3). | SPCMIN | 34 |
| C | 8. ABSOLUTE VALUE OF LATITUDE IN COMPUTING LATITUDE FACTOR | SPCMIN | 35 |
| C | FOR H2O. | SPCMIN | 36 |
| C | REVISION 04 (07/06/79) PROVIDES | SPCMIN | 37 |
| C | 9. CORRECTED FIT FUNCTION FOR I02 FOR 75.0 .LT. ZH .LT. 85.0 KM | SPCMIN | 38 |
| C | | SPCMIN | 39 |
| C | INPUT PARAMETERS | SPCMIN | 40 |
| C | ARGUMENT LIST | SPCMIN | 41 |
| C | KK - CALCULATION FLAG | SPCMIN | 42 |
| C | = 1, CALCULATE INITIALIZATION PARAMETERS | SPCMIN | 43 |
| C | = 2, CALCULATE ATMOSPHERIC PROPERTIES | SPCMIN | 44 |
| C | ZH - ALTITUDE OF INTEREST (KM) | SPCMIN | 45 |
| C | ATNDUP COMMON | SPCMIN | 46 |
| C | IDJMN - INDEX FOR DAY OR NIGHT | SPCMIN | 47 |
| C | = +1, DAY | SPCMIN | 48 |
| C | = -1, NIGHT | SPCMIN | 49 |
| C | SNI(I) - SPECIES DENSITIES FROM SUBROUTINE ATMOSU | SPCMIN | 50 |
| C | ATMOSPHERIC MODEL. | SPCMIN | 51 |
| C | I = 1,6 FOR N2, O2, 1, AR, He, CO2 | SPCMIN | 52 |
| C | FINE COMMON | SPCMIN | 53 |
| C | PLAT - NORTH LATITUDE OF POINT (RADIAN) | SPCMIN | 54 |
| C | ZCHECK COMMON | SPCMIN | 55 |
| C | ZBFLAG, - FLAGS USED TO DETECT AND CORRECT AN ERROROUS | SPCMIN | 56 |
| C | SPIFLG - SEQUENCE OF CALLS TO SUBROUTINES ATMOSU, SPCMIN, | SPCMIN | 57 |
| C | AND IONOSU IN THE OPERATIONAL PHASE. APPROPRIATE | SPCMIN | 58 |

| | | EXCEPTIONS ARE ALLOWED IN THE INITIALIZATION PHASE. | |
|---|--|---|------------|
| C | | | SPC41N 59 |
| C | | | SPC41N 60 |
| C | INPUT PARAMETERS | | SPC41N 61 |
| C | ATMOSP COMMON | | SPC41N 62 |
| C | SNI(7) - N | DENSITY, 1/CM**3 | SPC41N 63 |
| C | SNI(8) - NO | DENSITY, 1/CM**3 | SPC41N 64 |
| C | SNI(13) - O2(SDG) | DENSITY, 1/CM**3 | SPC41N 65 |
| C | SNI(14) - O3 | DENSITY, 1/CM**3 | SPC41N 66 |
| C | SNI(15) - NO2 | DENSITY, 1/CM**3 | SPC41N 67 |
| C | SNI(16) - H2O | DENSITY, 1/CM**3 | SPC41N 68 |
| C | SNI(17) - H | DENSITY, 1/CM**3 | SPC41N 69 |
| C | SNI(18) - OH | DENSITY, 1/CM**3 | SPC41N 70 |
| C | SNI(19) - HO2 | DENSITY, 1/CM**3 | SPC41N 71 |
| C | SNI(20) - CO | DENSITY, 1/CM**3 | SPC41N 72 |
| C | SNI(21) - H2O | DENSITY, 1/CM**3 | SPC41N 73 |
| C | SNI(22) - CH4 | DENSITY, 1/CM**3 | SPC41N 74 |
| C | SNI(23) - N(4S) | DENSITY, 1/CM**3 | SPC41N 75 |
| C | SNI(24) - N(2S) | DENSITY, 1/CM**3 | SPC41N 76 |
| C | SNI(25) - RELATIVE HUMIDITY, PERCENT | | SPC41N 77 |
| C | SNI(26) - O(1D) | DENSITY, 1/CM**3 | SPC41N 78 |
| C | SNI(27) - N(2P) | DENSITY, 1/CM**3 | SPC41N 79 |
| C | ALPDM COMMON | | SPC41N 80 |
| C | ALTKM(47) - THE ALTITUDES AT WHICH MINOR SPECIES ARE SPECIFIED AS DATA | | SPC41N 81 |
| C | ONITE(18) - THE NIGHTTIME O-VALUES SPECIFIED AS DATA | | SPC41N 82 |
| C | CO2(25) - THE CO2-VALUES SPECIFIED AS DATA | | SPC41N 83 |
| C | ZHCHEX COMMON | | SPC41N 84 |
| C | SPIPLG | | SPC41N 85 |
| C | CCC | | SPC41N 86 |
| C | DIMENSION AA(13),BB(7),CC(6),AMUNIT(21),AM4SDM(33),AM2DDM(41) | | SPC41N 87 |
| C | DIMENSION O2SDGD(47),O2SDGN(47),O3DAY(26),O3MIT(27),DD(11) | | SPC41N 88 |
| C | DIMENSION Y(6),Z(6),TOJ(6),UOJ(6),VOJ(6),WUJ(6) | | SPC41N 89 |
| C | DIMENSION H2UON(21),AMUDAY(21),GG(13),FF(12),EE(14) | | SPC41N 90 |
| C | DIMENSION DOHDAY(21),DOHMIT(21),H2O2AY(21),H2O2MIT(21),CCOH(8), | | SPC41N 91 |
| C | CHO2(8),DATCU(31),SMETH(25) | | SPC41N 92 |
| C | DIMENSION DAHDAY(21),DAHMIT(21),J1DDAY(33),DM2O(12),CM2U(9) | | SPC41N 93 |
| C | DIMENSION A(20,21) | | SPC41N 94 |
| C | DIMENSION SNO2D(33),SNO2N(33),HH(13) | | SPC41N 95 |
| C | COMMON/ALTJON/ ALTKM(47),ONITE(18),CU2(25),S3ZUO | | SPC41N 96 |
| C | COMMON/ATNJUP/ HL,SBAR,LDURN,PP,RHO,TT,SNI(33),HKKU,FEHSEQ | | KJMM01 2 |
| C | COMMON/TIME/ IYNS,INONS,IOAYS,ZT,PLAT,PLON,UT,CAT,FYR,PST,RHOSKM | | KJMM02 2 |
| C | ,CHI | | KJMM07 2 |
| C | COMMON/VPC/ WVFLAG,METHOD,AZJ120 | | KJMM09 2 |
| C | COMMON/ZHCHEX/ ZHPLAG,SPIPLG | | KJMM09 2 |
| C | CCC | | SPC41N 102 |
| C | DATA NDCGNO / 12 /, NDCG2D,NDCG4S / 6,5 / | | SPC41N 103 |
| C | DATA MALTNO / 21 /, MALT2D,MALT4S / 16,13 / | | SPC41N 104 |
| C | DATA NDCU2D,MALTU2 / 10,11 / | | SPC41N 105 |
| C | DATA NOGH2O,NKMH2O / 12,21 /, H2OPCC / 3.14260910E+16 / | | SPC41N 106 |
| C | DATA NOGMFH,MALTMH / 11,25 /, CH4PCC / 3.75369008E+16 / | | SPC41N 107 |
| C | DATA JZJPCC / 1.25459271E+22 /, OUMPCC / 2.14992030E+16 / | | SPC41N 108 |
| C | DATA PI / 3.141592653590 / | | SPC41N 109 |
| C | DATA NDCNJ2,NKMHU2 / 12,33 / | | SPC41N 110 |
| C | DATA (ALTKM(1),I=1,47) / 0.,5.,10.,15.,20.,25.,30.,35.,40.,45., | | SPC41N 111 |
| C | 50.,55.,60.,65.,70.,75.,80.,85.,90.,95., | | SPC41N 112 |
| C | 100.,105.,110.,115.,120.,125.,130.,135.,140.,145.,150.,155., | | SPC41N 113 |
| C | 160.,165.,170.,175.,180.,185.,190.,195.,200.,205.,210.,215., | | SPC41N 114 |

| | | | |
|---|--|--------|-----|
| | * 220.,225.,230. / | SPC411 | 115 |
| C | BPM VALUES 02/22/75 FJR J NIGHT | SPC411 | 116 |
| | DATA (ONIT(1),I=1,18) / 13*1.1, 2*0.0, 4.30E+00, | SPC411 | 117 |
| | 3.00E+10, 9.00E+10 / | SPC411 | 118 |
| C | BPM VALUES 12/07/74 FJR CO2 | SPC411 | 119 |
| | DATA (CO2(I),I=1,25) / 21*0.0, 1.30E+09,4.83E+08,1.70E+08, | SPC411 | 120 |
| | 5.65E+07 / | SPC411 | 121 |
| C | THE CO2 VALUES AT ALTITUDES FROM 0.0 TO 100. KM ARE RESET | SPC411 | 122 |
| C | IN SUBROUTINE APMOSU BY USING A CONSTANT MIXING-RATIO OF | SPC411 | 123 |
| C | 3.20E-04 | SPC411 | 124 |
| C | BPM VALUES 10/01/77 FJR NO DAY | SPC411 | 125 |
| | DATA (AMODAY(I),I=1,21) / 1.50E+10,3.40E+09,1.30E+09,5.80E+08, | SPC411 | 126 |
| | 7.00E+08,1.75E+09,2.10E+09,1.75E+09, | SPC411 | 127 |
| | 1.25E+09,8.50E+08,5.10E+08,3.00E+08,1.40E+08,6.40E+07,2.70E+07, | SPC411 | 128 |
| | 1.30E+07,6.20E+06,4.30E+06,8.20E+06,1.90E+07,3.40E+07 / | SPC411 | 129 |
| C | BPM VALUES 10/01/77 FJR NO NIGHT | SPC411 | 130 |
| | DATA (ANMNT(I),I=1,21) / 11*1.00E+00,1.00E+04,1.10E+05, | SPC411 | 131 |
| | 2.30E+05,4.80E+05,1.00E+06,2.00E+06, | SPC411 | 132 |
| | 4.30E+06,8.20E+06,1.70E+07,3.40E+07 / | SPC411 | 133 |
| C | BPM VALUES 11/05/77 FJR M DAY AND NIGHT N(TOTAL) | SPC411 | 134 |
| | DATA (AN4SDM(I),I=1,33) / 20*0.0,1.33E+06,2.90E+06,5.20E+06, | SPC411 | 135 |
| | 8.60E+06,1.26E+07,1.74E+07,2.26E+07, | SPC411 | 136 |
| | 2.82E+07,3.14E+07,3.30E+07,3.35E+07,3.31E+07,3.20E+07 / | SPC411 | 137 |
| C | BPM VALUES 11/26/77 FJR M DAY AND NIGHT N(2) | SPC411 | 138 |
| | DATA (AN2DDM(I),I=1,41) / 25*0.0,1.30E+04,3.00E+04,6.30E+04, | SPC411 | 139 |
| | 1.20E+05,2.00E+05,3.10E+05,4.60E+05, | SPC411 | 140 |
| | 5.50E+05,6.00E+05,6.40E+05,6.50E+05,6.50E+05,6.40E+05, | SPC411 | 141 |
| | 6.30E+05,6.10E+05,5.70E+05 / | SPC411 | 142 |
| C | BPM VALUES 01/04/75 FJR J2(SDG) DAY | SPC411 | 143 |
| | DATA (J2SDGO(I),I=1,47) / 2.60E+06,4.40E+06,2.70E+07,1.25E+08, | SPC411 | 144 |
| | 4.90E+08,1.25E+09,2.70E+09,9.00E+09, | SPC411 | 145 |
| | 1.80E+10,2.70E+10,3.50E+10,2.10E+10,1.50E+10,1.00E+10,6.10E+09, | SPC411 | 146 |
| | 3.13E+09,2.05E+09,3.60E+09,1.30E+09,3.00E+09,5.60E+07,4.30E+06, | SPC411 | 147 |
| | 6.20E+05,1.00E+05,1.40E+04,3.30E+03,7.10E+02,2.60E+02,1.00E+02, | SPC411 | 148 |
| | 4.70E+01,2.30E+01,1.20E+01,15*6.10 / | SPC411 | 149 |
| C | BPM VALUES 01/04/75 FJR J2(SDG) NIGHT | SPC411 | 150 |
| | DATA (J2SDGN(I),I=1,47) / 15*3.40,5.80E+02,1.00E+05,8.60E+07, | SPC411 | 151 |
| | 2.00E+08,1.40E+08,5.60E+07,4.30E+06, | SPC411 | 152 |
| | 6.20E+05,1.00E+05,1.40E+04,3.30E+03,7.10E+02,2.60E+02,1.00E+02, | SPC411 | 153 |
| | 4.70E+01,2.30E+01,1.20E+01,15*6.10 / | SPC411 | 154 |
| C | BPM VALUES 05/04/77 FJR O3 OZONE DAY (KG/KG) | SPC411 | 155 |
| | DATA (J3DAY(I),I=1,26) / 11*0.0,3.1E-06,1.9E-06,1.0E-06,5.3E-07, | SPC411 | 156 |
| | 2.6E-07,2.9E-07,1.2E-06,7.0E-07,1.4E-07, | SPC411 | 157 |
| | 3.6E-08,1.2E-08,3.0E-09,7.1E-10,1.5E-10,4.5E-11 / | SPC411 | 158 |
| C | BPM VALUES 05/04/77 FJR O3 OZONE NIGHT (KG/KG) | SPC411 | 159 |
| | DATA (J3NIT(I),I=1,27) / 11*0.0,3.1E-06,3.3E-06,5.9E-06,4.3E-06, | SPC411 | 160 |
| | 1.5E-06,2.6E-07,5.6E-06,4.0E-06,1.5E-06, | SPC411 | 161 |
| | 3.8E-07,9.9E-08,3.3E-08,6.5E-09,6.8E-10,1.5E-10,2.7E-11 / | SPC411 | 162 |
| C | BPM VALUES 05/04/77 FJR CO CARBON MONOXIDE (PPM) | SPC411 | 163 |
| | DATA (DATCO(I),I=1,31) / 0.12,0.12,0.11,0.072,0.054,0.048,0.048, | SPC411 | 164 |
| | 0.048,0.048,0.056,0.070,0.127,0.254, | SPC411 | 165 |
| | 0.442,0.967,2.210,10.2,18.5,24.3,26.6,29.2,30.9,32.0,32.6,33.6, | SPC411 | 166 |
| | 34.4,34.8,34.8,34.8,34.5,34.1 / | SPC411 | 167 |
| C | BPM VALUES 05/04/77 FJR CH4 METHANE (PPM) | SPC411 | 168 |
| | DATA (SMETH(I),I=1,25) / 3*0.77,0.66,0.61,0.53,0.50,0.38,0.31, | SPC411 | 169 |
| | 0.24,0.11,4.76E-2,2.12E-2,1.34E-2, | SPC411 | 170 |
| | 8.36E-3,4.80E-3,2.69E-3,1.84E-3,1.02E-3,8.77E-4,7.03E-4, | SPC411 | 171 |

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|---|---|---|--------|-----|
| | • | 5.70E-4,4.40E-4,2.55E-4,1.06E-4 / | SPCMIN | 172 |
| C | | BPM VALUES 05/34/77 FOR H2O WATER (PPM) | SPCMIN | 173 |
| | | DATA (H2OON(I),I=1,21) / 2.29,2.39,2.50,2.61,2.74,2.71,2.60, | SPCMIN | 174 |
| | | 2.36,2.10,1.80,1.51,1.25,0.98,0.76,0.46,0.21,0.066,0.018, | SPCMIN | 175 |
| | | 0.0075,0.0053,0.0040 / | SPCMIN | 176 |
| C | | BPM VALUES 07/02/77 FOR H ATOMIC HYDROGEN DAY | SPCMIN | 177 |
| | | DATA (DAHDAY(I),I=1,21) / 7.0E-03,7.6E-03,1.0E-02,1.6E-02, | SPCMIN | 178 |
| | | 5.2E-02,3.2E-01,2.9E+00,1.0E+02, | SPCMIN | 179 |
| | | 4.0E+04,1.0E+05,2.4E+05,5.1E+05,1.0E+06,1.8E+06,4.9E+06, | SPCMIN | 180 |
| | | 1.25E+07,3.5E+07,8.6E+07,7.4E+07,5.0E+07,3.0E+07 / | SPCMIN | 181 |
| C | | BPM VALUES 07/92/77 FOR H ATOMIC HYDROGEN NIGHT | SPCMIN | 182 |
| | | DATA (DANHIT(I),I=1,21) / 15*0.0,5.0E+02,1.0E+07,8.6E+07, | SPCMIN | 183 |
| | | 7.4E+07,5.0E+07,3.0E+07 / | SPCMIN | 184 |
| C | | BPM VALUES (05/02/77) FOR HYDROXYL RADICAL DAY | SPCMIN | 185 |
| | | DATA (DOMDAY(I),I=1,21) / 1.0E+06,1.0E+06,1.05E+06,1.15E+06, | SPCMIN | 186 |
| | | 1.5E+06,2.3E+06,4.0E+06,6.8E+06, | SPCMIN | 187 |
| | | 1.05E+07,1.1E+07,9.5E+06,7.2E+06,5.3E+06,3.7E+06,2.5E+06, | SPCMIN | 188 |
| | | 1.6E+06,7.0E+05,7.0E+04,6.3E+03,5.7E+02,6.7E+01 / | SPCMIN | 189 |
| C | | BPM VALUES (05/02/77) FOR HYDROXYL RADICAL NIGHT | SPCMIN | 190 |
| | | DATA (DOMNIT(I),I=1,21) / 1.7E+02,1.8E+02,2.1E+02,2.7E+02, | SPCMIN | 191 |
| | | 4.2E+02,8.1E+02,2.0E+03,8.0E+03, | SPCMIN | 192 |
| | | 5.7E+04,2.9E+05,1.2E+06,4.4E+06,6.5E+06,5.9E+06,4.5E+06, | SPCMIN | 193 |
| | | 3.2E+06,1.6E+06,1.7E+05,1.7E+04,1.7E+03,2.2E+02 / | SPCMIN | 194 |
| C | | BPM VALUES (05/02/77) FOR HYDROPEROXYL RADICAL DAY | SPCMIN | 195 |
| | | DATA (HODDAY(I),I=1,21) / 1.0E+03,7.5E+05,2.4E+06,6.9E+06, | SPCMIN | 196 |
| | | 1.15E+07,1.5E+07,1.6E+07,1.5E+07, | SPCMIN | 197 |
| | | 1.2E+07,9.1E+06,6.6E+06,4.2E+06,2.2E+06,7.9E+05,4.2E+06, | SPCMIN | 198 |
| | | 1.2E+07,9.2E+06,5.7E+04,5.7E+03,4.9E+02,7.4E+01 / | SPCMIN | 199 |
| C | | BPM VALUES (05/02/77) FOR HYDROPEROXYL RADICAL NIGHT | SPCMIN | 200 |
| | | DATA (HODNIT(I),I=1,21) / 4.9E+01,4.2E+02,1.6E+03,5.9E+03, | SPCMIN | 201 |
| | | 1.4E+04,2.7E+04,4.7E+04,8.3E+04, | SPCMIN | 202 |
| | | 1.3E+05,2.4E+05,4.6E+05,6.9E+05,7.3E+05,4.6E+05,3.5E+06, | SPCMIN | 203 |
| | | 1.2E+07,9.2E+06,5.7E+04,5.7E+03,4.9E+02,7.4E+01 / | SPCMIN | 204 |
| C | | BPM VALUES 07/02/77 FOR U(10) ATOMIC URANIUM | SPCMIN | 205 |
| | | DATA (UIODAY(I),I=1,33) / 3*1.0E-02,3.8E-01,2.4E+00,1.1E+01, | SPCMIN | 206 |
| | | 3.9E+01,1.4E+02,3.5E+02,6.0E+02, | SPCMIN | 207 |
| | | 6.0E+02,5.0E+02,4.2E+02,2.7E+02,4.6E+01,1.7E+01,1.0E+01, | SPCMIN | 208 |
| | | 5.2E+01,5.8E+01,2.2E+02,8.0E+02,2.0E+03,3.9E+03,5.2E+03, | SPCMIN | 209 |
| | | 6.4E+03,6.4E+03,6.1E+03,5.8E+03,5.5E+03,5.5E+03,5.3E+03, | SPCMIN | 210 |
| | | 5.2E+03,5.0E+03 / | SPCMIN | 211 |
| C | | BPM VALUES 07/30/77 FOR H2O (PPBV) | SPCMIN | 212 |
| | | DATA (DN2J(I),I=1,12) / 310.,260.,280.,290.,210.,120.,60.,25., | SPCMIN | 213 |
| | | 9.4,2.9,0.78,0.13 / | SPCMIN | 214 |
| C | | BPM VALUES 02/14/75 FOR NO2 DAY | SPCMIN | 215 |
| | | DATA (SNO2D(I),I=1,33) / 2.50E+10,8.30E+09,1.40E+09,1.40E+09, | SPCMIN | 216 |
| | | 1.40E+09,2.40E+09,2.50E+09,1.25E+09, | SPCMIN | 217 |
| | | 3.40E+08,7.10E+07,7.80E+06,2.70E+06,7.00E+05,2.60E+05,1.00E+05, | SPCMIN | 218 |
| | | 5.00E+04,2.40E+04,1.20E+04,6.40E+03,3.40E+03,1.80E+03,1.10E+03, | SPCMIN | 219 |
| | | 6.70E+02,4.30E+02,2.30E+02,1.90E+02,1.40E+02,1.15E+02,9.50E+01, | SPCMIN | 220 |
| | | 8.00E+01,7.00E+01,5.00E+01,4.60E+01 / | SPCMIN | 221 |
| C | | BPM VALUES 02/14/75 FOR NO2 NIGHT | SPCMIN | 222 |
| | | DATA (SNO2N(I),I=1,33) / 3.50E+10,1.20E+10,2.70E+09,2.00E+09, | SPCMIN | 223 |
| | | 2.50E+09,4.15E+09,4.55E+09,3.00E+09, | SPCMIN | 224 |
| | | 1.00E+09,9.20E+08,5.20E+08,1.00E+08,1.40E+08,5.50E+07,1.70E+07, | SPCMIN | 225 |
| | | 1.00E+06,3.00E+04,1.20E+04,6.40E+03,3.40E+03,1.80E+03,1.10E+03, | SPCMIN | 226 |
| | | 6.70E+02,4.30E+02,2.30E+02,1.90E+02,1.40E+02,1.15E+02,9.50E+01, | SPCMIN | 227 |
| | | 8.00E+01,7.00E+01,5.00E+01,4.60E+01 / | SPCMIN | 228 |

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| CCC | | SPCMIN | 227 |
| C | * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE NITRIC OXIDE IN | SPCMIN | 230 |
| C | * * * DAYTIME FOR ALTITUDES BELOW 100.0 KM | SPCMIN | 231 |
| CCC | | SPCMIN | 232 |
| | ANDDAF(BQ) = EXP(((((((((((AA(13))*BQ + AA(12))*BQ + AA(11))*BQ | SPCMIN | 233 |
| | + AA(10))*BQ + AA(9))*BQ + AA(8))*BQ + AA(7))*BQ | SPCMIN | 234 |
| | + AA(6))*BQ + AA(5))*BQ + AA(4))*BQ + AA(3))*BQ | SPCMIN | 235 |
| | + AA(2))*BQ + AA(1)) | SPCMIN | 236 |
| CCC | | SPCMIN | 237 |
| C | * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE ATOMIC NITROGEN | SPCMIN | 238 |
| C | * * * (N(TOTAL)) BETWEEN 100.0 AND 160.0 KM FOR BOTH DAY AND NIGHT. | SPCMIN | 239 |
| CCC | | SPCMIN | 240 |
| | ANN4S(BQ) = EXP((((CC(6))*BQ + CC(5))*BQ + CC(4))*BQ | SPCMIN | 241 |
| | + CC(3))*BQ + CC(2))*BQ + CC(1)) | SPCMIN | 242 |
| CCC | | SPCMIN | 243 |
| C | * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE ATOMIC NITROGEN | SPCMIN | 244 |
| C | * * * (N(2U)) BETWEEN 125. AND 200. KM FOR BOTH DAY AND NIGHT. | SPCMIN | 245 |
| CCC | | SPCMIN | 246 |
| | ANN2D(BQ) = EXP((((BB(7))*BQ + BB(6))*BQ + BB(5))*BQ | SPCMIN | 247 |
| | + BB(4))*BQ + BB(3))*BQ + BB(2))*BQ + BB(1)) | SPCMIN | 248 |
| CCC | | SPCMIN | 249 |
| C | * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE O2(1 DELTA) | SPCMIN | 250 |
| C | * * * IN DAYTIME FOR ALTITUDES BELOW 50. KM. | SPCMIN | 251 |
| CCC | | SPCMIN | 252 |
| | AOZSDP(BQ) = EXP(((((((DD(11))*BQ + DD(10))*BQ + DD(9))*BQ | SPCMIN | 253 |
| | + DD(8))*BQ + DD(7))*BQ + DD(6))*BQ + DD(5))*BQ | SPCMIN | 254 |
| | + DD(4))*BQ + DD(3))*BQ + DD(2))*BQ + DD(1)) | SPCMIN | 255 |
| CCC | | SPCMIN | 256 |
| C | * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE OJ FOR | SPCMIN | 257 |
| C | * * * ALTITUDES BELOW 150 KM. | SPCMIN | 258 |
| CCC | | SPCMIN | 259 |
| | AFCDAP(BQ) = EXP(((((((((((EE(14))*BQ + EE(13))*BQ | SPCMIN | 260 |
| | + EE(12))*BQ + EE(11))*BQ + EE(10))*BQ + EE(9))*BQ | SPCMIN | 261 |
| | + EE(8))*BQ + EE(7))*BQ + EE(6))*BQ + EE(5))*BQ | SPCMIN | 262 |
| | + EE(4))*BQ + EE(3))*BQ + EE(2))*BQ + EE(1)) | SPCMIN | 263 |
| CCC | | SPCMIN | 264 |
| C | * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE METHANE FOR | SPCMIN | 265 |
| C | * * * ALTITUDES FROM 10. KM TO 120. KM. | SPCMIN | 266 |
| CCC | | SPCMIN | 267 |
| | ICM4PF(BQ) = EXP(((((((((((FF(12))*BQ + FF(11))*BQ + FF(10))*BQ | SPCMIN | 268 |
| | + FF(9))*BQ + FF(8))*BQ + FF(7))*BQ + FF(6))*BQ | SPCMIN | 269 |
| | + FF(5))*BQ + FF(4))*BQ + FF(3))*BQ + FF(2))*BQ | SPCMIN | 270 |
| | + FF(1)) | SPCMIN | 271 |
| CCC | | SPCMIN | 272 |
| C | * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE WATER FOR | SPCMIN | 273 |
| C | * * * 45.0 .LE. ALTITUDES (KM) .LE. 120.0 KM. | SPCMIN | 274 |
| CCC | | SPCMIN | 275 |
| | ANZUPF(BQ) = EXP(((((((((((GG(13))*BQ + GG(12))*BQ + GG(11))*BQ | SPCMIN | 276 |
| | + GG(10))*BQ + GG(9))*BQ + GG(8))*BQ + GG(7))*BQ | SPCMIN | 277 |
| | + GG(6))*BQ + GG(5))*BQ + GG(4))*BQ + GG(3))*BQ | SPCMIN | 278 |
| | + GG(2))*BQ + GG(1)) | SPCMIN | 279 |
| CCC | | SPCMIN | 280 |
| C | * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE NO2 FOR | SPCMIN | 281 |
| C | * * * DAYTIME AT ALTITUDES BELOW 160. KM. | SPCMIN | 282 |
| CCC | | SPCMIN | 283 |
| | ANJ2PF(BQ) = EXP(((((((((((HH(13))*BQ + HH(12))*BQ + HH(11))*BQ | SPCMIN | 284 |
| | + HH(10))*BQ + HH(9))*BQ + HH(8))*BQ + HH(7))*BQ | SPCMIN | 285 |

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      *          * HH(6))*BQ + HH(5))*BQ + HH(4))*BQ + HH(3))*BQ          SPCMIN 286
      *          * HH(2))*BQ + HH(1))                                     SPCMIN 287
CCC
C * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE OH FOR          SPCMIN 288
C * * * DAYTIME OR NIGHTTIME FOR ALTITUDES BELOW 80. KM.                SPCMIN 289
CCC
      ADHDF( BQ ) = EXP(((((((CCOH(8))*BQ + CCOH(7))*BQ + CCOH(6))*BQ          SPCMIN 292
      *          * CCOH(5))*BQ + CCOH(4))*BQ + CCOH(3))*BQ          SPCMIN 293
      *          * CCOH(2))*BQ + CCOH(1))                               SPCMIN 294
CCC
C * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE HO2 FOR          SPCMIN 295
C * * * DAYTIME OR NIGHTTIME FOR ALTITUDES BELOW 65. KM.                SPCMIN 296
CCC
      AMZ2PF( BQ ) = EXP(((((((CH2(8))*BQ + CH2(7))*BQ + CH2(6))*BQ          SPCMIN 297
      *          * CH2(5))*BQ + CH2(4))*BQ + CH2(3))*BQ          SPCMIN 298
      *          * CH2(2))*BQ + CH2(1))                               SPCMIN 299
CCC
C * * * ARITHMETIC STATEMENT FUNCTION USED TO CALCULATE M2O AT          SPCMIN 300
C * * * ALTITUDES BELOW 55. KM.                SPCMIN 301
CCC
      AMZ0PF( BQ ) = EXP(((((((CM2O(9))*BQ + CM2O(8))*BQ + CM2O(7))*BQ          SPCMIN 302
      *          * CM2O(6))*BQ + CM2O(5))*BQ + CM2O(4))*BQ          SPCMIN 303
      *          * CM2O(3))*BQ + CM2O(2))*BQ + CM2O(1))           SPCMIN 304
CCC
      20 TO (100,200), KK          SPCMIN 305
C          INITIALIZATION, CALLED FROM SUBROUTINE ATMJSU DURING ITS          SPCMIN 306
C          INITIALIZATION.          SPCMIN 307
      100 CONTINUE          SPCMIN 308
      ALJGFR = ALJG10( EXP(1.0) )          SPCMIN 309
      PIPLAT = 180./PI*ABS( PLAT )          SPCMIN 310
C          SPCMIN 311
C          ATOMIC NITROGEN PROFILE PARAMETERS.          SPCMIN 312
C * * * TOTAL ATOMIC NITROGEN, BUT CALLED N(4S) IN CODING * * * * * N          SPCMIN 313
      H4S100 = ALTKM(21)          SPCMIN 314
      H4S160 = ALTKM(33)          SPCMIN 315
      CALL FITTER(HALT4S,ALTKM(21),AN4SDN(21),NDEG4S, 1 , 2 ,CC)          SPCMIN 316
      H4S100 = ANN4S( H4S100 )          SPCMIN 317
      H4S160 = ANN4S( H4S160 )          SPCMIN 318
      P3H4S = 0.693*SIN( (2.*PYH-0.50)*PI )          SPCMIN 319
      P5H4S = SIN( (15.*HL-141.)*PI/180. )          SPCMIN 320
      P24EXP = 1.0 + EXP(0.07*(PIPLAT-24.))          SPCMIN 321
      P2H4S = SQRT( 0.60 + (0.56 + 0.44*P5H4S)*2.87/P24EXP )          SPCMIN 322
      P75EXP = 1.0 + EXP(0.146*(PIPLAT-75.))          SPCMIN 323
      P4H4S = 1.42*P5H4S/P75EXP          SPCMIN 324
      P5H4S = 1.0 + 3.0/( 1.0 + EXP(-0.10*(SBR-134.)) )          SPCMIN 325
C          SPCMIN 326
C * * * ATOMIC NITROGEN N(20) * * * * * N(20)          SPCMIN 327
      H20125 = ALTKM(26)          SPCMIN 328
      H20200 = ALTKM(41)          SPCMIN 329
      CALL FITTER(HALT20,ALTKM(26),AN20DN(26),NDEG20, 1 , 2 ,BB)          SPCMIN 330
      H20125 = ANN20( H20125 )          SPCMIN 331
      H20200 = ANN20( H20200 )          SPCMIN 332
      P8H20Z = (1.0+EXP(-2.197*(HL-6.)))*(1.0+EXP(+2.197*(HL-18.)))          SPCMIN 333
      P8H20Z = 1.0 / P8H20Z          SPCMIN 334
      115 CONTINUE          SPCMIN 335
C          SPCMIN 336
C * * * NITRIC OXIDE PROFILE PARAMETERS * * * * * NO          SPCMIN 337

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|-----|---|--------|-----|
| C | FOR DAYTIME NO.. | SPCMIN | 343 |
| | CALL FITTER(MALTMO,ALTKM,ANUDAV,NJEGHU, 1, 2, AA) | SPCMIN | 344 |
| | HN0100 = ALTKM(21) | SPCMIN | 345 |
| | AN0100 = ALOG(ANUDAV(HN0100)) | SPCMIN | 346 |
| | CM0100 = 1.0/(1.0+EXP(-0.22*(HN0100-72.))) | SPCMIN | 347 |
| | ALOGGL = ALOG(0.375 + 0.0125*PIPLAT) | SPCMIN | 348 |
| | HN0100 = ANU100 - (1.0-CM0100)*ALOGGL | SPCMIN | 349 |
| | PHOSIM = SIN(PI*(15.*HL-105.)/180.) | SPCMIN | 350 |
| C | SET THE CURVE OF THE 10.7-CM SOLAR FLUX SBAR, SBARJ. | SPCMIN | 351 |
| | SBARJ = SBAR**J | SPCMIN | 352 |
| | A215F = 9.68 + 6.08*SBARJ/(SBARJ+5.0E+05) | SPCMIN | 353 |
| | A215FL = (A215F-CM0100)/115. | SPCMIN | 354 |
| | HN0050 = ALTKM(11) | SPCMIN | 355 |
| | HN0055 = ALTKM(12) | SPCMIN | 356 |
| | HN0060 = ALTKM(13) | SPCMIN | 357 |
| | HN0065 = ALTKM(18) | SPCMIN | 358 |
| | AN0050 = ANONIT(11) | SPCMIN | 359 |
| | AN0055 = ANONIT(12) | SPCMIN | 360 |
| | AN0060 = ANONIT(13) | SPCMIN | 361 |
| | AN0065 = ANODAF(HN0065) | SPCMIN | 362 |
| | SN0065 = 25.0/ALOG(AN0065/AN0060) | SPCMIN | 363 |
| | SN0055 = 5.0/ALOG(AN0060/AN0055) | SPCMIN | 364 |
| | SN0060 = 2.*(SN0055 - 5.0/ALOG(AN0060/AN0055)) | SPCMIN | 365 |
| C | | SPCMIN | 366 |
| C | * * * MOLECULAR OXYGEN (SINGLET DELTA G) PROFILE PARAMETERS * O2(SDG) | SPCMIN | 367 |
| | Z02090 = ALTKM(19) | SPCMIN | 368 |
| | Z02100 = ALTKM(21) | SPCMIN | 369 |
| | AO2090 = O2SDGD(19) | SPCMIN | 370 |
| | BO2090 = -ALOG(O2SDGD(22)/AO2090)/(ALTKM(22)-Z02090) | SPCMIN | 371 |
| | IF(IODRN) 142,150,150 | SPCMIN | 372 |
| 142 | Z02070 = ALTKM(15) | SPCMIN | 373 |
| | Z02080 = ALTKM(17) | SPCMIN | 374 |
| | A02070 = O2SDGD(15) | SPCMIN | 375 |
| | A02080 = O2SDGD(17) | SPCMIN | 376 |
| | BO2070 = -ALOG(A02080/A02070)/(Z02080-Z02070) | SPCMIN | 377 |
| | Z(6) = ALOG10(A02080) | SPCMIN | 378 |
| | DO 144 I=1,4 | SPCMIN | 379 |
| | Z112 = ALTKM(I+17)-Z02080 | SPCMIN | 380 |
| | A(I,5) = Z112 | SPCMIN | 381 |
| | DO 144 J=1,4 | SPCMIN | 382 |
| | A(I,5-J) = Z112*A(I,6-J) | SPCMIN | 383 |
| 144 | CONTINUE | SPCMIN | 384 |
| | Z118 = Z02100-Z02080 | SPCMIN | 385 |
| | A(5,5) = 1.0 | SPCMIN | 386 |
| | A(5,5) = -BO2090*ALJGTE | SPCMIN | 387 |
| | DO 146 J=1,4 | SPCMIN | 388 |
| | PJ = J | SPCMIN | 389 |
| | A(5,5-J) = Z118*((PJ+1.)/PJ)*A(5,6-J) | SPCMIN | 390 |
| 146 | CONTINUE | SPCMIN | 391 |
| | DO 148 I=1,3 | SPCMIN | 392 |
| | A(I,5) = ALOG10(O2SDGD(I+17)) - Z(6) | SPCMIN | 393 |
| 148 | CONTINUE | SPCMIN | 394 |
| | A(4,6) = ALOG10(AO2090*EXP(-BO2090*(Z02100-Z02090))) - Z(6) | SPCMIN | 395 |
| | NU = 5 | SPCMIN | 396 |
| | CALL SOLVE(A,Z,NU) | SPCMIN | 397 |
| | DO T) 156 | SPCMIN | 398 |
| 150 | Z02050 = ALTKM(11) | SPCMIN | 399 |

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| Z02075 = ALTKM(16) | SPCMIN | 400 |
| A02050 = U2S0GD(11) | SPCMIN | 401 |
| A02075 = U2S0GD(16) | SPCMIN | 402 |
| B02050 = -ALOG(A02075/A02050)/(Z02075-Z02050) | SPCMIN | 403 |
| CALL FITTER(MALTU2,ALTKM,U2S0GD,NDG02D, 1, 2, DU) | SPCMIN | 404 |
| F(6) = ALOG10(A02075) | SPCMIN | 405 |
| V(5) = -B02050*ALUGTE | SPCMIN | 406 |
| DO 152 I=1,3 | SPCMIN | 407 |
| Z112 = ALTKM(I+16)-Z02075 | SPCMIN | 408 |
| A(1,4) = Z112*Z112 | SPCMIN | 409 |
| A(1,5) = ALUG10(U2S0GD(I+16)) - Z112*V(5) - F(6) | SPCMIN | 410 |
| DO 152 J=1,3 | SPCMIN | 411 |
| A(1,4-J) = Z112*A(1,5-J) | SPCMIN | 412 |
| 152 CONTINUE | SPCMIN | 413 |
| Z118 = Z02090-Z02075 | SPCMIN | 414 |
| A(4,4) = 2.*Z118 | SPCMIN | 415 |
| A(4,5) = -B02090*ALUGTE - V(5) | SPCMIN | 416 |
| DO 154 J=1,3 | SPCMIN | 417 |
| PJ = J+1 | SPCMIN | 418 |
| A(4,4-J) = Z118*((PJ+1.)/PJ)*A(4,5-J) | SPCMIN | 419 |
| 154 CONTINUE | SPCMIN | 420 |
| BU = 4 | SPCMIN | 421 |
| CALL S3LVE(A,V,NO) | SPCMIN | 422 |
| 156 CONTINUE | SPCMIN | 423 |
| C | SPCMIN | 424 |
| C * * * CO (CARBON MONOXIDE) PARAMETERS * * * * * CO | SPCMIN | 425 |
| CALL FITTER(J1,ALTKM,DATCJ,13, 1, 2, KL) | SPCMIN | 426 |
| COZ150 = APCUAP(150.) | SPCMIN | 427 |
| C | SPCMIN | 428 |
| C * * * CH4 (METHANE) PARAMETERS * * * * * CH4 | SPCMIN | 429 |
| MMTH = MALTHM-2 | SPCMIN | 430 |
| CALL FITTER(MMTH,ALTKM(J),SMETH(J),NDGMTH, 1, 2, PF) | SPCMIN | 431 |
| CM4TKN = ACH4PF(10.) | SPCMIN | 432 |
| CM4120 = ACH4PF(120.) | SPCMIN | 433 |
| C | SPCMIN | 434 |
| C * * * O3 (OZONE) PARAMETERS * * * * * O3 | SPCMIN | 435 |
| C FOR DAY OR NIGHT, INITIALIZE SUBROUTINE JZONE FOR ZH .LT. 55.0 | SPCMIN | 436 |
| CALL OZJNE(1,ZH,OZ3) | SPCMIN | 437 |
| IF(IDJNM) 162,172,172 | SPCMIN | 438 |
| C START NIGHTTIME INITIALIZATION FOR ZH .GE. 55.0 KM. | SPCMIN | 439 |
| 162 Z03N55 = ALTKM(12) | SPCMIN | 440 |
| Z03D55 = Z03N55 | SPCMIN | 441 |
| C DETERMINE PARAMETERS FOR NIGHT EXPONENTIAL FOR | SPCMIN | 442 |
| C 70.0 .LT. ZH .LE. 75.0 KM. | SPCMIN | 443 |
| Z03N70 = ALTKM(15) | SPCMIN | 444 |
| Z03N75 = ALTKM(16) | SPCMIN | 445 |
| A03N70 = O3NIT(15) | SPCMIN | 446 |
| B03N70 = -ALOG(O3NIT(16)/A03N70)/(Z03N75-Z03N70) | SPCMIN | 447 |
| C DETERMINE COEFFICIENTS (V03(I) I=1,6) SU THAT SEM-LOGNBB | SPCMIN | 448 |
| C POLYNOMIAL EQUALS DATA POINTS AT 55(5)70 KM, THE (ZERO) | SPCMIN | 449 |
| C DERIVATIVE AT 55 KM OF THE FIT FUNCTION BELOW 55 KM, AND THE | SPCMIN | 450 |
| C (DISAPPEARING) DERIVATIVE AT 70 KM OF THE 70- TO 75-KM FIT | SPCMIN | 451 |
| C FUNCTION. | SPCMIN | 452 |
| V03(6) = ALOG10(O3NIT(12)) | SPCMIN | 453 |
| V03(5) = 0.0 | SPCMIN | 454 |
| DO 164 I=1,3 | SPCMIN | 455 |
| Z112 = ALTKM(I+12) - Z03N55 | SPCMIN | 456 |

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| | A(1,4) = Z112*Z112 | SPCMIN | 457 |
| | A(1,5) = ALOG10(U3MIT(1+12)) - Z112*VUJ(5) - VUJ(6) | SPCMIN | 454 |
| | DO 164 J=1,3 | SPCMIN | 459 |
| | A(1,4-J) = Z112*A(1,5-J) | SPCMIN | 460 |
| 164 | CONTINUE | SPCMIN | 461 |
| | Z118 = Z03N70-Z03N55 | SPCMIN | 462 |
| | A(4,4) = 2.*Z118 | SPCMIN | 463 |
| | A(4,5) = -803N70*ALJGTE - VUJ(5) | SPCMIN | 464 |
| | DO 166 J=1,3 | SPCMIN | 465 |
| | PJ = J+1 | SPCMIN | 466 |
| | A(4,4-J) = Z118*((PJ+1.)/PJ)*A(4,5-J) | SPCMIN | 467 |
| 165 | CONTINUE | SPCMIN | 468 |
| | NO = 4 | SPCMIN | 469 |
| | CALL SOLVE(A,VUJ,NO) | SPCMIN | 470 |
| C | DETERMINE PARAMETERS FOR NIGHT EXPONENTIAL FOR ZH .GE. 90.0 KM | SPCMIN | 471 |
| | Z03N90 = ALTKM(19) | SPCMIN | 472 |
| | U03N90 = U3MIT(19) | SPCMIN | 473 |
| | Z03N90 = -ALOG(U3MIT(22)/A03N90)/(ALTKM(22)-Z03N90) | SPCMIN | 474 |
| C | DETERMINE 5TH-DEGREE POLYNOMIAL (COEFFICIENTS W03(I) I=1,6) TO | SPCMIN | 475 |
| C | MATCH DATA POINTS AT 75(5)90 KM AND DERIVATIVES OF 70-TJ-75-KM | SPCMIN | 476 |
| C | FIT-FUNCTION AT 75 KM AND .GE. -90.0-KM FIT FUNCTION AT 90.0 KM | SPCMIN | 477 |
| | W03(6) = ALOG10(U3MIT(16)) | SPCMIN | 478 |
| | W03(5) = -803N70*ALJGTE | SPCMIN | 479 |
| | DO 168 I=1,3 | SPCMIN | 480 |
| | Z112 = ALTKM(1+16) - Z03N75 | SPCMIN | 481 |
| | A(1,4) = Z112*Z112 | SPCMIN | 482 |
| | A(1,5) = ALOG10(U3MIT(1+16)) - Z112*WUJ(5) - WUJ(6) | SPCMIN | 483 |
| | DO 168 J=1,3 | SPCMIN | 484 |
| | A(1,4-J) = Z112*A(1,5-J) | SPCMIN | 485 |
| 168 | CONTINUE | SPCMIN | 486 |
| | Z118 = Z03N90-Z03N75 | SPCMIN | 487 |
| | A(4,4) = 2.*Z118 | SPCMIN | 488 |
| | A(4,5) = -803N90*ALJGTE - WUJ(5) | SPCMIN | 489 |
| | DO 170 J=1,3 | SPCMIN | 490 |
| | PJ = J+1 | SPCMIN | 491 |
| | A(4,4-J) = Z118*((PJ+1.)/PJ)*A(4,5-J) | SPCMIN | 492 |
| 170 | CONTINUE | SPCMIN | 493 |
| | NO = 4 | SPCMIN | 494 |
| | CALL SOLVE(A,WUJ,NO) | SPCMIN | 495 |
| | GO TO 178 | SPCMIN | 496 |
| C | START DAYTIME INITIALIZATION. | SPCMIN | 497 |
| C | DETERMINE PARAMETERS FOR DAY EXPONENTIAL FOR ZH .GE. 90.0 KM. | SPCMIN | 498 |
| 172 | Z03D90 = ALTKM(19) | SPCMIN | 499 |
| | U03D90 = U3DAY(19) | SPCMIN | 500 |
| | Z03D90 = -ALOG(U3DAY(22)/A03D90)/(ALTKM(22)-Z03D90) | SPCMIN | 501 |
| C | DETERMINE 5TH-DEGREE POLYNOMIAL (COEFFICIENTS T03(I) I=1,6) TO | SPCMIN | 502 |
| C | MATCH DATA POINTS AT 55(5)75 KM AND THE (ZERO) DERIVATIVE OF | SPCMIN | 503 |
| C | THE 0-TU-55-KM FIT FUNCTION AT 55 KM. | SPCMIN | 504 |
| | Z03D55 = ALTKM(12) | SPCMIN | 505 |
| | Z03D55 = Z03D55 | SPCMIN | 506 |
| | Z03D75 = ALTKM(16) | SPCMIN | 507 |
| | T03(6) = ALOG10(U3DAY(12)) | SPCMIN | 508 |
| | T03(5) = 0.0 | SPCMIN | 509 |
| | DO 190 I=1,4 | SPCMIN | 510 |
| | Z112 = ALTKM(I+12) - Z03D55 | SPCMIN | 511 |
| | A(1,4) = Z112*Z112 | SPCMIN | 512 |
| | A(1,5) = ALOG10(U3DAY(I+12)) - Z112*TUJ(5) - TUJ(6) | SPCMIN | 513 |

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| | JD 180 J=1,3 | SPCMIN | 514 |
| | A(1,4-J) = Z112*A(1,5-J) | SPCMIN | 515 |
| 180 | CONTINUE | SPCMIN | 516 |
| | BU = 4 | SPCMIN | 517 |
| | CALL SOLVE(A,TU3,ND) | SPCMIN | 518 |
| C | DETERMINE 5TH-DEGREE POLYNOMIAL (COEFFICIENTS U03(I) I=1,6) TO | SPCMIN | 519 |
| C | DATA POINTS AT 75(5)90 KM AND DERIVATIVES OF 55-TU-75-KM FIT- | SPCMIN | 520 |
| C | FUNCTION AT 75 KM AND LOG.-90.0-KM FIT-FUNCTION AT 90.0 KM. | SPCMIN | 521 |
| | U03(6) = ALOG10(U3DAY(16)) | SPCMIN | 522 |
| | Z118 = ZU3075-Z03055 | SPCMIN | 523 |
| | U03(5) = (((5.*TU3(1))*Z118 + 4.*TU3(2))*Z118 + 3.*TU3(3))*Z118 | SPCMIN | 524 |
| | + 2.*TU3(4))*Z118 + TU3(5) | SPCMIN | 525 |
| | JD 174 I=1,3 | SPCMIN | 526 |
| | Z112 = ALTKM(I+16) - ZU3D75 | SPCMIN | 527 |
| | A(1,4) = Z112*Z112 | SPCMIN | 528 |
| | A(1,5) = ALOG10(U3DAY(I+16)) - Z112*U03(5) - U03(6) | SPCMIN | 529 |
| | JD 174 J=1,3 | SPCMIN | 530 |
| | A(1,4-J) = Z112*A(1,5-J) | SPCMIN | 531 |
| 174 | CONTINUE | SPCMIN | 532 |
| | Z118 = ZU3D90-ZU3D75 | SPCMIN | 533 |
| | A(4,4) = 2.*Z118 | SPCMIN | 534 |
| | A(4,5) = -8J3090*ALOGTE - U03(5) | SPCMIN | 535 |
| | JD 176 J=1,3 | SPCMIN | 536 |
| | FJ = J+1 | SPCMIN | 537 |
| | A(4,4-J) = Z118*((FJ+1.)/FJ)*A(4,5-J) | SPCMIN | 538 |
| 176 | CONTINUE | SPCMIN | 539 |
| | BD = 4 | SPCMIN | 540 |
| | CALL SOLVE(A,U03,ND) | SPCMIN | 541 |
| 178 | CONTINUE | SPCMIN | 542 |
| C | | SPCMIN | 543 |
| C | * * * FIT COEFFICIENTS FOR H2O (DAY AND NIGHT) * * * * * H2O | SPCMIN | 544 |
| | CALL FITFN(MKMH02,ALTKM,SMU20,MDGNO2, 1, 2, HH) | SPCMIN | 545 |
| | HNO210 = ALTKM(29) | SPCMIN | 546 |
| | HNO220 = ALTKM(33) | SPCMIN | 547 |
| | ANO2PD = ANO2PP(HNO220) | SPCMIN | 548 |
| | HNO200 = HNO210-HNO220 | SPCMIN | 549 |
| | HNO212 = ANO2PP(HNO210) / ANO2PD | SPCMIN | 550 |
| | FNO255 = ANO2PP(55.) + ANO2AP(55.) - ANO255 | SPCMIN | 551 |
| | HNO265 = SMU2M(14) | SPCMIN | 552 |
| | HNO255 = ALTKM(12) | SPCMIN | 553 |
| | HNO265 = ALTKM(14) | SPCMIN | 554 |
| | HNO20M = HNO255-HNO265 | SPCMIN | 555 |
| | HNO2FA = FNO255/HNO265 | SPCMIN | 556 |
| | ANO282 = ANO2PP(82.) | SPCMIN | 557 |
| | HNO282 = 82. | SPCMIN | 558 |
| | HNO20B = HNO265-HNO282 | SPCMIN | 559 |
| | HNO282 = ANO265/HNO282 | SPCMIN | 560 |
| C | | SPCMIN | 561 |
| C | * * * FIT COEFFICIENTS FOR WATER * * * * * H2O | SPCMIN | 562 |
| C | IF WVFLAG .NE. 0.0, USER MUST SUPPLY TABULAR WATER-VAPOR | SPCMIN | 563 |
| C | PROFILE (FROM 0.0- TO 120.0-KM ALTITUDE) WHICH IS READ BY | SPCMIN | 564 |
| C | SUBROUTINE WVOPT. IN OPERATIONAL PHASE, SUBROUTINE WVOPT | SPCMIN | 565 |
| C | PERFORMS A LOGARITHMIC INTERPOLATION TO RETURN THE H2O MASS- | SPCMIN | 566 |
| C | MIXING RATIO. | SPCMIN | 567 |
| | IF(WVFLAG.NE.0.0) GO TO 179 | SPCMIN | 568 |
| C | THIS INITIALIZATION CALL TO SUBROUTINE WATER EVALUATES THE | SPCMIN | 569 |
| C | INDEX IX FOR THE QUASI-HOMOGENEOUS MOISTURE REGION AND | SPCMIN | 570 |

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|------|--|--------|-----|
| C | EVALUATES THE LOGARITHM OF THE H2O MIXING RATIO AT 5- AND 14- | SPCMIN | 571 |
| C | KM ALTITUDES. THIS INITIALIZATION ALLOWS SUBROUTINE WATER IN | SPCMIN | 572 |
| C | THE OPERATIONAL PHASE TO OUTPUT THE H2O MIXING RATIO (PPM) | SPCMIN | 573 |
| C | FOR ZH-LT.45 KM. | SPCMIN | 574 |
| | CALL WATER(1,ZH,CH20) | SPCMIN | 575 |
| C | NOW DETERMINE THE H2O MASS-MIXING-RATIO FIT-COEFFICIENTS GG | SPCMIN | 576 |
| C | FOR THE ALTITUDE RANGE FROM 20 TO 120 KM, EVEN THOUGH THE FIT | SPCMIN | 577 |
| C | FUNCTION WILL BE USED IN THE OPERATIONAL PHASE ONLY FOR | SPCMIN | 578 |
| C | 45.LE.ZH-LT.120 KM. | SPCMIN | 579 |
| C | CALL FITTER(NKMH20,ALTKM(5),H2ODM(1),NDGH20, 1, 2,GG) | SPCMIN | 580 |
| C | THE VALUE OF THE MASS-MIXING RATIO AT 120 KM IS NEEDED FOR THE | SPCMIN | 581 |
| C | OPERATIONAL PHASE. | SPCMIN | 582 |
| | 320120 = AH2OFF(120.) | SPCMIN | 583 |
| | 179 CONTINUE | SPCMIN | 584 |
| C | | SPCMIN | 585 |
| C | * * * FIT COEFFICIENTS FOR ATOMIC HYDROGEN * * * * * H | SPCMIN | 586 |
| | H86 = 9.0E+07 | SPCMIN | 587 |
| | H100 = 3.77E+12*EXP(-0.1174*100.) + 4.07E+06*100.**(-0.7169) | SPCMIN | 588 |
| | S86100 = 14./ALOG(H86/H100) | SPCMIN | 589 |
| | IF(IDORN) 1071,1072,1072 | SPCMIN | 590 |
| 1071 | S80 = 6.0/ALOG(H86/DAHMIT(17)) | SPCMIN | 591 |
| | S85 = 2.20*(S80 - 6.0/ALOG(H86/DAHMIT(16))) | SPCMIN | 592 |
| | 20 TO 1073 | SPCMIN | 593 |
| 1072 | H30 = DAHDAY(7) | SPCMIN | 594 |
| | H35 = DAHDAY(8) | SPCMIN | 595 |
| | H40 = DAHDAY(9) | SPCMIN | 596 |
| | S3035 = 5.0/ALOG(H35/H30) | SPCMIN | 597 |
| | S3540 = 5.0/ALOG(H40/H35) | SPCMIN | 598 |
| | S4086 = 46./ALOG(H86/H40) | SPCMIN | 599 |
| 1073 | CONTINUE | SPCMIN | 600 |
| C | | SPCMIN | 601 |
| C | * * * FIT COEFFICIENTS FOR HYDROXYL RADICAL * * * * * OH | SPCMIN | 602 |
| | IF(IDORN) 181,182,182 | SPCMIN | 603 |
| 181 | AOH100 = DOHMIT(21) | SPCMIN | 604 |
| | CALL FITTER(17,ALTKM,DOHMIT, 7, 1, 2,CCOH) | SPCMIN | 605 |
| | 20 TO 184 | SPCMIN | 606 |
| 182 | AOH100 = DOHDAY(21) | SPCMIN | 607 |
| | CALL FITTER(17,ALTKM,DOHDAY, 7, 1, 2,CCOH) | SPCMIN | 608 |
| 184 | AOH080 = AOHDMF(80.) | SPCMIN | 609 |
| | 3DM080 = -ALOG(AOH100/AOH080)/(ALTKM(21)-ALTKM(17)) | SPCMIN | 610 |
| C | | SPCMIN | 611 |
| C | * * * FIT COEFFICIENTS FOR HYDROPEROXYL RADICAL * * * * * HO2 | SPCMIN | 612 |
| | IF(IDORN) 186,188,188 | SPCMIN | 613 |
| 186 | CONTINUE | SPCMIN | 614 |
| | CALL FITTER(14,ALTKM,HO2NIT, 1, 1, 2,CHU2) | SPCMIN | 615 |
| | 20 TO 190 | SPCMIN | 616 |
| 188 | CONTINUE | SPCMIN | 617 |
| | CALL FITTER(14,ALTKM,HO2DAY, 6, 1, 2,CHU2) | SPCMIN | 618 |
| | CHU2(8) = 0.0 | SPCMIN | 619 |
| 190 | AHO275 = HO2DAY(16) | SPCMIN | 620 |
| | AHO295 = HO2DAY(20) | SPCMIN | 621 |
| | AHO265 = AH2OFF(65.) | SPCMIN | 622 |
| | BHO255 = -ALOG(AHO275/AHO265)/(ALTKM(16)-ALTKM(14)) | SPCMIN | 623 |
| | BHO275 = -ALOG(AHO295/AHO275)/(ALTKM(20)-ALTKM(16)) | SPCMIN | 624 |
| | HO2100 = AHO275*EXP(-BHO275*(100. - 75.)) | SPCMIN | 625 |
| C | | SPCMIN | 626 |
| C | * * * FIT COEFFICIENTS FOR ATOMIC OXYGEN * * * * * O(10) | SPCMIN | 627 |

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| 1381 | IF(IDOWN) 1082,1081,1081 | SPCMIN | 628 |
| | JD47 = 7.0E+02 | SPCMIN | 629 |
| | JD25 = ODDAY(6) | SPCMIN | 630 |
| | JD40 = ODDAY(9) | SPCMIN | 631 |
| | JD65 = ODDAY(14) | SPCMIN | 632 |
| | JD80 = ODDAY(17) | SPCMIN | 633 |
| | JD100 = ODDAY(21) | SPCMIN | 634 |
| | JD110 = ODDAY(23) | SPCMIN | 635 |
| | JD120 = ODDAY(25) | SPCMIN | 636 |
| | JD160 = ODDAY(33) | SPCMIN | 637 |
| | SOD40 = 7.0/ALOG(OD47/OD40) | SPCMIN | 638 |
| | SOD47A = (22./15.)*(SJD40 - 7.0/ALOG(OD47/OD25)) | SPCMIN | 639 |
| | SOD65 = 18./ALOG(OD47/OD65) | SPCMIN | 640 |
| | SOD47B = (33./15.)*(SOD65 - 18./ALOG(OD47/OD80)) | SPCMIN | 641 |
| | SOD100 = 20./ALOG(OD100/OD80) | SPCMIN | 642 |
| | SOD110 = 10./ALOG(OD120/OD110) | SPCMIN | 643 |
| | SOD120 = 2.0*(SOD110 - 10./ALOG(OD120/OD100)) | SPCMIN | 644 |
| | SOD160 = 40./ALOG(OD120/OD160) | SPCMIN | 645 |
| 1382 | CONTINUE | SPCMIN | 646 |
| C | | SPCMIN | 647 |
| C | * * * FIT COEFFICIENTS FOR NITROUS OXIDE * * * * * NZU | SPCMIN | 648 |
| | CALL FITTER(12,ALTKM,ON20, 8, 1, 2, CN20) | SPCMIN | 649 |
| | IN2055 = AN20FF(55.) | SPCMIN | 650 |
| | BLEXP = 1.0/(1.0 + EXP(0.17*(PIPLAT - 23.))) | SPCMIN | 651 |
| | RETURN | SPCMIN | 652 |
| CC | | SPCMIN | 653 |
| CC | | SPCMIN | 654 |
| 200 | CONTINUE | SPCMIN | 655 |
| | IF(ZH.NE.ZHFLAG) CALL ATMOSU(2,ZH) | SPCMIN | 656 |
| CCC | | SPCMIN | 657 |
| C | AN ERRONEOUS CONDITION WILL OCCUR IF SPCMIN IS CALLED WITH | SPCMIN | 658 |
| C | KK=2 AND A GIVEN VALUE OF ZH IF ATMOSU HAS NOT BEEN CALLED | SPCMIN | 659 |
| C | FIRST WITH KK=2 AND FOR THE SAME VALUE OF ZH. | SPCMIN | 660 |
| C | THE VARIABLE ZHFLAG IS USED TO DETECT THIS CONDITION AND | SPCMIN | 661 |
| C | TO MAKE THE REQUIRED CALL TO ATMOSU. | SPCMIN | 662 |
| C | ZHFLAG IS INITIALIZED TO AN ARBITRARY NEGATIVE VALUE IN | SPCMIN | 663 |
| C | THE INITIALIZATION CALL TO ATMOSU. | SPCMIN | 664 |
| CCC | | SPCMIN | 665 |
| | IF(ZH.EQ.SPIPLG) RETURN | SPCMIN | 666 |
| CCC | | SPCMIN | 667 |
| C | AN ERRONEOUS CONDITION WILL OCCUR IF IONJSU IS CALLED WITH | SPCMIN | 668 |
| C | JJ=2 AND A GIVEN VALUE OF ZH IF SPCMIN HAS NOT BEEN CALLED | SPCMIN | 669 |
| C | FIRST WITH JJ=2 AND FOR THE SAME VALUE OF ZH. | SPCMIN | 670 |
| C | THE VARIABLE SPIPLG IS USED TO DETECT THIS CONDITION AND | SPCMIN | 671 |
| C | TO MAKE THE REQUIRED CALL TO SPCMIN. | SPCMIN | 672 |
| CCC | | SPCMIN | 673 |
| C | THE OPTIMUM ORDER IS **CALL ATMOSU(2,ZH)** THEN | SPCMIN | 674 |
| C | **CALL SPCMIN(2,ZH)** AND THEN **CALL IONJSU(2,ZH)**. | SPCMIN | 675 |
| C | ZHFLAG AND SPIPLG WILL DETECT CALLS MADE IN ANY OTHER ORDER. | SPCMIN | 676 |
| CCC | | SPCMIN | 677 |
| C | SPIPLG IS INITIALIZED TO AN ARBITRARY NEGATIVE VALUE IN | SPCMIN | 678 |
| C | THE INITIALIZATION CALL TO ATMOSU. | SPCMIN | 679 |
| CCC | | SPCMIN | 680 |
| | SPIPLG = ZH | SPCMIN | 681 |
| C | | SPCMIN | 682 |
| C | * * * COMPUTE DENSITY OF N * * * * * SNI(7)=N | SPCMIN | 683 |
| | IF(ZH.LT.W4S100) GO TO 210 | SPCMIN | 684 |

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| IF(ZH.GT.H4S160) GJ TO 212 | SPCMIN | 685 |
| FIN4SZ = ANH4S(ZH) | SPCMIN | 686 |
| GO TO 214 | SPCMIN | 687 |
| 210 FIN4SZ = A4S100*EXP(0.144*(ZH-H4S100)) | SPCMIN | 688 |
| GO TO 214 | SPCMIN | 689 |
| 212 FIN4SZ = A4S160*EXP(-0.0178*(ZH-H4S160)) | SPCMIN | 690 |
| 214 FIN4SZ = 1.0 + EXP(-0.02*(Zu-220.)) | SPCMIN | 691 |
| SNI(7) = FIN4SZ*T2H4S*EXP(T3H4S + T4H4S/T4H4SZ) * T5H4S | SPCMIN | 692 |
| C | SPCMIN | 693 |
| C * * * COMPUTE DENSITY OF EXCITED ATOMIC NITROGEN * * SNI(24)=N(20) | SPCMIN | 694 |
| IF(ZH.LT.H2D125) GJ TO 216 | SPCMIN | 695 |
| IF(ZH.GT.H2D200) GJ TO 218 | SPCMIN | 696 |
| F7H2DZ = ANH2D(ZH) | SPCMIN | 697 |
| GO TO 220 | SPCMIN | 698 |
| 216 F7H2DZ = A2D125*EXP(+0.184*(ZH-H2D125)) | SPCMIN | 699 |
| GO TO 220 | SPCMIN | 700 |
| 218 F7H2DZ = A2D200*EXP(-0.0282*(ZH-H2D200)) | SPCMIN | 701 |
| 220 SNI(24) = (SNI(7)/FIN4SZ)*F7H2DZ*T6H2DZ | SPCMIN | 702 |
| C | SPCMIN | 703 |
| C * * * COMPUTE DENSITY OF EXCITED ATOMIC NITROGEN * * SNI(27)=N(2P) | SPCMIN | 704 |
| F2P2D=ASSIGNED VALUE OF THE RATIO OF THE PRODUCTION RATE OF | SPCMIN | 705 |
| N(2P) TO THAT OF N(2D). | SPCMIN | 706 |
| F2P2D = 0.01 | SPCMIN | 707 |
| R2P2D = 0.01 | SPCMIN | 708 |
| IF(ZH.GE.119.90) R2P2D = 5.5E-04*F2P2D*EXP(900./ZH) | SPCMIN | 709 |
| SNI(27) = R2P2D*SNI(24) | SPCMIN | 710 |
| C | SPCMIN | 711 |
| C * * * COMPUTE DENSITY OF GROUND-STATE ATOMIC NITROGEN SNI(23)=N(4S) | SPCMIN | 712 |
| SNI(23) = SNI(7) - SNI(24) - SNI(27) | SPCMIN | 713 |
| C | SPCMIN | 714 |
| C * * * COMPUTE DENSITY OF NO * * * * * SNI(8)=NO | SPCMIN | 715 |
| IF(ZH.GT.HNO100) GJ TO 227 | SPCMIN | 716 |
| IF(IDJKN.GE.0) GJ TO 225 | SPCMIN | 717 |
| IF(ZH.GE.HNO085) GJ TO 225 | SPCMIN | 718 |
| CC IF GET TO THIS POINT THEN ZH.LT.85. KM AND IT IS NIGHTTIME. | SPCMIN | 719 |
| IF(ZH.GE.HNO060) GJ TO 223 | SPCMIN | 720 |
| IF(ZH.GE.HNO050) GJ TO 221 | SPCMIN | 721 |
| SNI(3) = 1.0 | SPCMIN | 722 |
| GO TO 229 | SPCMIN | 723 |
| 221 Z60MZH = HNO060-ZH | SPCMIN | 724 |
| 3DPZHD = SNO060 - 0.20*(SNO060-SNO055)*Z60MZH | SPCMIN | 725 |
| CCDFZH = 1.0 + EXP(-0.22*(ZH-72.)) | SPCMIN | 726 |
| SNI(8) = ANO060*EXP(ALUGGL/CCDFZH - Z60MZH/SJFZMJ) | SPCMIN | 727 |
| SNI(3) = AMAXI(1.0,SNI(8)) | SPCMIN | 728 |
| GO TO 229 | SPCMIN | 729 |
| 223 Z60MZH = HNO060-ZH | SPCMIN | 730 |
| CCDFZH = 1.0 + EXP(-0.22*(ZH-72.)) | SPCMIN | 731 |
| SNI(3) = ANO060*EXP(ALUGGL/CCDFZH - Z60MZH/SNO085) | SPCMIN | 732 |
| GO TO 229 | SPCMIN | 733 |
| 225 SNI(3) = ANJDAP(ZH) | SPCMIN | 734 |
| CCDFZH = 1.0 + EXP(-0.22*(ZH-72.)) | SPCMIN | 735 |
| SNI(3) = SNI(8) * EXP(ALUGGL/CCDFZH) | SPCMIN | 736 |
| GO TO 229 | SPCMIN | 737 |
| 227 ZH4100 = Z1-HNO100 | SPCMIN | 738 |
| 3DPZHD = 1.1*(1.0-EXP(-0.066*ZH4100)) | SPCMIN | 739 |
| AAZF = GNO100 + A215PL*ZH4100 | SPCMIN | 740 |
| SNI(8) = EXP(AAZF + 3DPZHD*TNUSIN + ALUGGL) | SPCMIN | 741 |

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| 229 | CONTINUE | SPCMIN | 742 |
| C | | SPCMIN | 743 |
| C | * * * * COMPUTE DENSITY OF O2(1 DELTA G) * * * * * SMI(13)=J2(SDG) | SPCMIN | 744 |
| | IF(ZH.LT.Z02100) GO TO 231 | SPCMIN | 745 |
| 230 | SMI(13) = A02090*EXP(-B02090*(ZH-Z02090)) | SPCMIN | 746 |
| | GO TO 238 | SPCMIN | 747 |
| 231 | IF(IDORN) 232,235,235 | SPCMIN | 748 |
| | NIGHTTIME O2(1 DELTA G) | SPCMIN | 749 |
| 232 | IF(ZH.GT.Z02070) GO TO 233 | SPCMIN | 750 |
| | SMI(13) = A02070 | SPCMIN | 751 |
| | GO TO 238 | SPCMIN | 752 |
| 233 | IF(ZH.GT.Z02080) GO TO 234 | SPCMIN | 753 |
| | SMI(13) = A02070*EXP(-B02070*(ZH-Z02070)) | SPCMIN | 754 |
| | GO TO 238 | SPCMIN | 755 |
| 234 | ZHMKN = ZH-Z02080 | SPCMIN | 756 |
| | SMI(13) = 10.**((((Z(1)*ZHMKN + Z(2))*ZHMKN + Z(3))*ZHMKN | SPCMIN | 757 |
| | + Z(4))*ZHMKN + Z(5))*ZHMKN + Z(6)) | SPCMIN | 758 |
| | GO TO 238 | SPCMIN | 759 |
| C | DAYTIME O2(1 DELTA G) | SPCMIN | 760 |
| 235 | IF(ZH.GE.Z02090) GO TO 236 | SPCMIN | 761 |
| | IF(ZH.GE.Z02050) GO TO 236 | SPCMIN | 762 |
| | SMI(13) = A02SDP(ZH) | SPCMIN | 763 |
| | GO TO 238 | SPCMIN | 764 |
| 236 | IF(ZH.GT.Z02075) GO TO 237 | SPCMIN | 765 |
| | SMI(13) = A02050*EXP(-B02050*(ZH-Z02050)) | SPCMIN | 766 |
| | GO TO 238 | SPCMIN | 767 |
| 237 | ZHMKN = ZH-Z02075 | SPCMIN | 768 |
| | SMI(13) = 10.**((((Y(1)*ZHMKN + Y(2))*ZHMKN + Y(3))*ZHMKN | SPCMIN | 769 |
| | + Y(4))*ZHMKN + Y(5))*ZHMKN + Y(6)) | SPCMIN | 770 |
| 238 | CONTINUE | SPCMIN | 771 |
| C | | SPCMIN | 772 |
| C | * * * * COMPUTE DENSITY OF CO (CARBON MONOXIDE) * * * * * SMI(20)=CO | SPCMIN | 773 |
| | IF(ZH.GE.150.) GO TO 2001 | SPCMIN | 774 |
| | SMI(20) = AF00AF(ZH) | SPCMIN | 775 |
| | GO TO 2002 | SPCMIN | 776 |
| 2001 | SMI(20) = CDZ150*EXP(-0.0047*(ZH-150.)) | SPCMIN | 777 |
| 2002 | SMI(20) = COMPCC*RHO*SMI(20) | SPCMIN | 778 |
| C | | SPCMIN | 779 |
| C | * * * * COMPUTE DENSITY OF CH4 (METHANE) * * * * * SMI(22)=CH4 | SPCMIN | 780 |
| C | CONVERT TO MOLECULES/CC | SPCMIN | 781 |
| C | CH4PCC = 1.0E-06 * 6.022045E+23 / 16.043 | SPCMIN | 782 |
| | IF(ZH.GE.120.) GO TO 2382 | SPCMIN | 783 |
| | IF(ZH.GT. 10.) GO TO 2381 | SPCMIN | 784 |
| | SMI(22) = CH4PCC*RHO*CH4TKM | SPCMIN | 785 |
| | GO TO 2383 | SPCMIN | 786 |
| 2381 | SMI(22) = CH4PCC*RHO*ACH4FF(ZH) | SPCMIN | 787 |
| | GO TO 2383 | SPCMIN | 788 |
| 2382 | SMI(22) = CH4PCC*RHO*CH4I20*EXP(-0.176*(ZH-120.)) | SPCMIN | 789 |
| 2383 | CONTINUE | SPCMIN | 790 |
| C | | SPCMIN | 791 |
| C | * * * * COMPUTE DENSITY OF O3 (OZONE) * * * * * SMI(14)=O3 | SPCMIN | 792 |
| | IF(ZH.LT.Z03055) GO TO 243 | SPCMIN | 793 |
| | IF(IDORN) 239,244,244 | SPCMIN | 794 |
| | NIGHTTIME O3 | SPCMIN | 795 |
| 239 | IF(ZH.GE.Z03070) GO TO 240 | SPCMIN | 796 |
| C | NIGHT 5TH-DEGREE POLYNOMIAL, 55.0 .L.E. ZH .L.F. 70.0 | SPCMIN | 797 |
| | ZHN4 = ZH-Z03055 | SPCMIN | 798 |


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      SMI(14) = 10.**((((VJ3(1)*ZHMKN + VJ3(2))*ZHMKN + VJ3(3))*ZHMKN
      * VJ3(4))*ZHMKN + VJ3(5))*ZHMKN + VJ3(6))
      GO TO 247
240 IF( ZH.GT.ZO3M75 ) GO TO 241
      NIGHT EXPONENTIAL, 70.0 .LE. ZH .LE. 75.0
      SMI(14) = A03M70*EXP(-B03M70*(ZH-ZO3M70))
      GO TO 247
241 IF( ZH.GE.ZO3M90 ) GO TO 242
      NIGHT SYN-DEGREE POLYNOMIAL, 75.0 .LT. ZH .LT. 90.0
      ZHMKN = ZH-ZO3M75
      SMI(14) = 10.**((((WJ3(1)*ZHMKN + WJ3(2))*ZHMKN + WJ3(3))*ZHMKN
      * WJ3(4))*ZHMKN + WJ3(5))*ZHMKN + WJ3(6))
      GO TO 247
242 NIGHT EXPONENTIAL, ZH .GE. 90.0 KM.
      SMI(14) = A03M90*EXP(-B03M90*(ZH-ZO3M90))
      GO TO 247
243 IF ZH.LT.55. KM, BOTH DAY AND NIGHT USE FOLLOWING.
244 CONTINUE
      CALL OZ3NK(2,ZH,OZ3)
      SMI(14) = OZ3
      GO TO 247
245 DAYTIME O3
246 IF( ZH.GT.ZO3D75 ) GO TO 245
      ZHMKN = ZH-ZO3D55
      SMI(14) = 10.**((((TJ3(1)*ZHMKN + TJ3(2))*ZHMKN + TJ3(3))*ZHMKN
      * TJ3(4))*ZHMKN + TJ3(5))*ZHMKN + TJ3(6))
      GO TO 247
247 IF( ZH.GE.ZO3D90 ) GO TO 246
      ZHMKN = ZH-ZO3D75
      SMI(14) = 10.**((((UJ3(1)*ZHMKN + UJ3(2))*ZHMKN + UJ3(3))*ZHMKN
      * UJ3(4))*ZHMKN + UJ3(5))*ZHMKN + UJ3(6))
      GO TO 247
248 DAY EXPONENTIAL, ZH .GE. 90.0 KM
249 SMI(14) = A03D90*EXP(-B03D90*(ZH-ZO3D90))
      CONVERT FROM MASS-MIXING RATIO TO NUMBER DENSITY.
247 SMI(14) = OZ3PCC*RHO*SMI(14)
      * * * * * COMPUTE DENSITY OF NO2 * * * * * SMI(15)=NO2
      IF( IDDM ) 248,252,252
      NIGHTTIME NO2
248 IF( ZH.GE.HNO255 ) GO TO 250
      SMI(15) = ANO2PF( ZH ) + ANJDAP( ZH ) - SMI(14)
      GO TO 261
250 IF( ZH.GT.HNO265 ) GO TO 251
      SMI(15) = ANO265 * RNO2PA**((ZH-HNO265)/HNO2JN)
      GO TO 261
251 IF( ZH.GT.HNO282 ) GO TO 252
      SMI(15) = ANO282 * RNO282**((ZH-HNO282)/HNO2JU)
      GO TO 261
252 DAYTIME NO2
253 IF( ZH.GT.HNO220 ) GO TO 253
      SMI(15) = ANO2PF( ZH )
      GO TO 261
253 SMI(15) = ANO2PD * RNO212**((ZH-HNO220)/HNO2JU)
261 CONTINUE
      * * * * * COMPUTE DENSITY OF H2O * * * * * SMI(16)=H2O

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SPCMIN 800
SPCMIN 801
SPCMIN 802
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SPCMIN 850
SPCMIN 851
SPCMIN 852
SPCMIN 853
SPCMIN 854
SPCMIN 855

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| IF(ZH.GE.120.) GO TO 263 | SPC41N | 856 |
| IF(MVFLAG.EQ.0.0) GO TO 254 | SPC41N | 857 |
| CALL WVDPT(2,ZH,H2OHR) | SPC41N | 858 |
| SNI(16) = H2OHR | SPC41N | 859 |
| GO TO 264 | SPC41N | 860 |
| 254 IF(ZH.GE. 45.) GO TO 262 | SPC41N | 861 |
| CALL WVDPT(2,ZH,CH2O) | SPC41N | 862 |
| SNI(16) = CH2O | SPC41N | 863 |
| GO TO 264 | SPC41N | 864 |
| 262 SNI(16) = AH2OFF(ZH) | SPC41N | 865 |
| GO TO 264 | SPC41N | 866 |
| 263 SNI(16) = H2O120*EXP(-0.0575*(ZH-120.)) | SPC41N | 867 |
| C CONVERT TO MOLECULES/CC | SPC41N | 868 |
| C H2JPCC = 1.0E-06 * 6.022045E+23 / 18.016 | SPC41N | 869 |
| 264 SNI(16) = H2OPCC*H2J*SNI(16) | SPC41N | 870 |
| C | SPC41N | 871 |
| C * * * * CALCULATE RELATIVE HUMIDITY * * * * SNI(25)=RELATIVE HUMIDITY | SPC41N | 872 |
| EH2O = 0.0 | SPC41N | 873 |
| EICE = 0.0 | SPC41N | 874 |
| IF((TT .GE. 173.15) .AND. (TT .LE. 373.15)) | SPC41N | 875 |
| *CALL H2OSVP(TT,EH2O,EICE) | SPC41N | 876 |
| SNI(25) = 0.0 | SPC41N | 877 |
| IF(EH2O.GT.0.0) SNI(25) = 1.380622E-17*TT/EH2O*SNI(16) | SPC41N | 878 |
| C | SPC41N | 879 |
| C * * * * COMPUTE DENSITY OF ATOMIC HYDROGEN H * * * * * SNI(17)=H | SPC41N | 880 |
| IF(ZH.GT.86.) GO TO 2266 | SPC41N | 881 |
| IF(IDURN) 2261,2263,2263 | SPC41N | 882 |
| 2261 IF(ZH.GE.74.) GO TO 2262 | SPC41N | 883 |
| SNI(17) = 1.0 | SPC41N | 884 |
| GO TO 2268 | SPC41N | 885 |
| 2262 SOPZ = S86 - (S86-S80)*(86.-ZH)/6. | SPC41N | 886 |
| SNI(17) = H86*EXP(-(86.-ZH)/SOPZ) | SPC41N | 887 |
| SNI(17) = AMAX1(1., SNI(17)) | SPC41N | 888 |
| GO TO 2268 | SPC41N | 889 |
| 2263 IF(ZH.GT.40.) GO TO 2265 | SPC41N | 890 |
| IF(ZH.GT.35.) GO TO 2264 | SPC41N | 891 |
| SNI(17) = H30*EXP((ZH-30.)/S3035) | SPC41N | 892 |
| SNI(17) = AMAX1(1.0,SNI(17)) | SPC41N | 893 |
| GO TO 2268 | SPC41N | 894 |
| 2264 SNI(17) = H35*EXP((ZH-35.)/S3540) | SPC41N | 895 |
| GO TO 2268 | SPC41N | 896 |
| 2265 SNI(17) = H40*EXP((ZH-40.)/S4086) | SPC41N | 897 |
| GO TO 2268 | SPC41N | 898 |
| 2266 IF(ZH.GT.100.) GO TO 2267 | SPC41N | 899 |
| SNI(17) = H86*EXP(-(ZH-86.)/S86100) | SPC41N | 900 |
| GO TO 2268 | SPC41N | 901 |
| 2267. SNI(17) = 3.77E+12*EXP(-0.1174*ZH) + 4.07E+05*ZH**(-0.7169) | SPC41N | 902 |
| 2268 CONTINUE | SPC41N | 903 |
| C | SPC41N | 904 |
| C * * * * COMPUTE DENSITY OF HYDROXYL RADICAL OH * * * * * SNI(18)=OH | SPC41N | 905 |
| IF(ZH.GE.100.) GO TO 265 | SPC41N | 906 |
| IF(ZH.GE. 80.) GO TO 260 | SPC41N | 907 |
| SNI(18) = AOHDF(ZH) | SPC41N | 908 |
| GO TO 266 | SPC41N | 909 |
| 260 SNI(18) = AOH80*EXP(-BOH80*(ZH-80.)) | SPC41N | 910 |
| GO TO 266 | SPC41N | 911 |
| 265 SNI(18) = 10. + 2.*(A3N100-10.)/(1.0+EXP(0.46*(ZH-100.))) | SPC41N | 912 |

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| 266 | CONTINUE | SPC*14 | 913 |
| C | | SPC*14 | 914 |
| C | * * * COMPUTE DENSITY HYDROPEROXYL RADICAL HO2 * * * * SNI(19)=HO2 | SPC*14 | 915 |
| | IF(ZH.GE.100.) GO TO 269 | SPC*14 | 916 |
| | IF(ZH.GE. 75.) GO TO 268 | SPC*14 | 917 |
| | IF(ZH.GE. 65.) GO TO 267 | SPC*14 | 918 |
| | SNI(19) = AMO2FF(ZH) | SPC*14 | 919 |
| | GO TO 270 | SPC*14 | 920 |
| 267 | SNI(19) = AMO265*EXP(-BHO265*(ZH-65.)) | SPC*14 | 921 |
| | GO TO 270 | SPC*14 | 922 |
| 268 | PZ75 = 1.0 | SPC*14 | 923 |
| | IF(ZH .LT. 85.0) PZ75 = 10.0** (1.0 - 0.2*ABS(ZH-80.)) | SPC*14 | 924 |
| | SNI(19) = PZ75*AMU275*EXP(-BHO275*(ZH-75.)) | SPC*14 | 925 |
| | GO TO 270 | SPC*14 | 926 |
| 269 | SNI(19) = HO2100*EXP(-0.378*(ZH-100.)) | SPC*14 | 927 |
| 270 | CONTINUE | SPC*14 | 928 |
| C | | SPC*14 | 929 |
| C | * * * COMPUTE DENSITY OF ATOMIC OXYGEN O(10) * * * * SNI(26)=O(10) | SPC*14 | 930 |
| | IF(IDOXM) 271,272,273 | SPC*14 | 931 |
| 271 | SNI(26) = 1.0 | SPC*14 | 932 |
| | GO TO 279 | SPC*14 | 933 |
| 272 | IF(ZH.GT.160.) GO TO 278 | SPC*14 | 934 |
| | IF(ZH.GT.120.) GO TO 277 | SPC*14 | 935 |
| | IF(ZH.GT.100.) GO TO 276 | SPC*14 | 936 |
| | IF(ZH.GT. 80.) GO TO 275 | SPC*14 | 937 |
| | IF(ZH.GT. 47.) GO TO 274 | SPC*14 | 938 |
| | IF(ZH.GT. 20.) GO TO 273 | SPC*14 | 939 |
| | SNI(26) = 1.0 | SPC*14 | 940 |
| | GO TO 279 | SPC*14 | 941 |
| 273 | SOPZA = SOD47A - (SOD47A-SOD43)*(47.-ZH)/7. | SPC*14 | 942 |
| | SNI(26) = OD47*EXP(-(47.-ZH)/SOPZA) | SPC*14 | 943 |
| | SNI(26) = AMAX1(1.0,SNI(26)) | SPC*14 | 944 |
| | GO TO 279 | SPC*14 | 945 |
| 274 | SOPZB = SOD47B - (SOD47B-SOD65)*(ZH-47.)/18. | SPC*14 | 946 |
| | SNI(26) = OD47*EXP(-(ZH-47.)/SOPZB) | SPC*14 | 947 |
| | GO TO 279 | SPC*14 | 948 |
| 275 | SNI(26) = OD80*EXP((ZH-80.)/SOD100) | SPC*14 | 949 |
| | GO TO 279 | SPC*14 | 950 |
| 276 | SOPZC = SOD120 - (SOD120-SOD110)*(120.-ZH)/10. | SPC*14 | 951 |
| | SNI(26) = OD120*EXP(-(120.-ZH)/SOPZC) | SPC*14 | 952 |
| | GO TO 279 | SPC*14 | 953 |
| 277 | SNI(26) = OD120*EXP(-(ZH-120.)/SOD120) | SPC*14 | 954 |
| | GO TO 279 | SPC*14 | 955 |
| 278 | SNI(26) = (OD160/S3200)*SNI(3) | SPC*14 | 956 |
| 279 | CONTINUE | SPC*14 | 957 |
| C | | SPC*14 | 958 |
| C | * * * COMPUTE DENSITY OF NITROUS OXIDE N2O * * * * * SNI(21)=N2O | SPC*14 | 959 |
| | IF(ZH.GE.55.) GO TO 280 | SPC*14 | 960 |
| | SNI(21) = AM2OFF(ZH) | SPC*14 | 961 |
| | GO TO 291 | SPC*14 | 962 |
| 280 | SNI(21) = CM2O55 | SPC*14 | 963 |
| 281 | CSHARG = 0.26*(ZH-30.) | SPC*14 | 964 |
| | COSHZ = (EXP(+CSHARG) + EXP(-CSHARG))/2. | SPC*14 | 965 |
| | SUNSMI = SNI(1) + SNI(2) + SNI(3) + SNI(4) + SNI(5) + SNI(6) | SPC*14 | 966 |
| | SNI(21) = 1.0E-09*SUNSMI*SNI(21)*(1.0 + BL*EXP*2.92/(1.0+COSHZ)) | SPC*14 | 967 |
| 299 | RETURN | SPC*14 | 968 |
| | END | SPC*14 | 969 |

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SUBROUTINE TEMPZH
TEMPZH 2
C SUBROUTINE TEMPZH DETERMINES THE TEMPERATURE PROFILE TEMPZH 3
C (TABULAR, 0(4)120 KM), BY INTERPOLATING THE DATA BASE TEMPZH 4
C (US STD 1966) FOR LATITUDE AND SEASON, TO BE USED AS INPUT TEMPZH 5
C TO THE MAJOR ATMOSPHERIC SPECIES MODEL FOR THE LOW-ALTITUDE TEMPZH 6
C RANGE FROM 0- TO 120-KM ALTITUDE. TEMPZH 7
C THE USER MAY BYPASS THE CODE'S SPECIFICATION OF TEMPERATURE TEMPZH 8
C PROFILE IN THE LOW-ALTITUDE (0 TO 120-KM) REGION BY -- TEMPZH 10
C (1) REQUIRING THE DRIVING ROUTINE TO SET TPFLAG TO A NONZERO TEMPZH 11
C VALUE, WHICH IS TRANSFERRED TO SUBROUTINE TEMPZH THROUGH TEMPZH 12
C COMMON ZHTEMP, AND (2) ALLOWING SUBROUTINE TEMPZH TO READ THE TEMPZH 13
C USER-SPECIFIED PROFILE AT ALTITUDES ZZ=0.0(4.0)120. KM . TEMPZH 14
CCC TEMPZH 15
CCC THIS IS A NEW ROUTINE FOR ROSCOE-IR. TEMPZH 16
CCC TEMPZH 17
C INPUT PARAMETERS TEMPZH 18
C TIME COMMON TEMPZH 19
C PLAT = NORTH LATITUDE OF POINT P (RADIANS) TEMPZH 20
C PST = FRACTION OF SUMMER TEMPERATURE PROFILE TO BE TEMPZH 21
C USED, WITH (1.-PST) OF THE WINTER TEMPERATURE TEMPZH 22
C PROFILE, IN DETERMINING THE TEMPERATURE PROFILE. TEMPZH 23
C FOR A GIVEN DAY OF THE YEAR AT A GIVEN LATITUDE. TEMPZH 24
C ZHTEMP COMMON TEMPZH 25
C TPFLAG = FLAG FOR OPTIONAL TREATMENT OF TEMPERATURE TEMPZH 26
C PROFILE. TEMPZH 27
C .EQ. 0.0 NORMAL TREATMENT TEMPZH 28
C .NE. 0.0 OPTIONAL TREATMENT, ALLOWING SUBROUTINE TEMPZH 29
C TEMPZH TO READ THE USER-SPECIFIED PROFILE AT TEMPZH 30
C ALTITUDES ZZ = 0.0(4.0)120. KM. TEMPZH 31
CCC TEMPZH 32
C OUTPUT PARAMETERS TEMPZH 33
C ZHTEMP COMMON TEMPZH 34
C (TZH(I),I=1,31) = TEMPERATURE PROFILE, DETERMINED BY TEMPZH 35
C INTERPOLATION OF THE DATA BASE TEMPZH 36
C (US STD 1966) FOR LATITUDE AND SEASON, TEMPZH 37
C USED AS INPUT TO THE MAJOR ATMOSPHERIC TEMPZH 38
C SPECIES MODEL FOR THE LOW-ALTITUDE TEMPZH 39
C RANGE FROM 0- TO 120-KM ALTITUDE. TEMPZH 40
CCC TEMPZH 41
COMMON/TIME/ IYRS,IMONS,IDAYS,ZT,PLAT,PLON,UT,GAT,PYR,PST,HDUSKM KMM07 2
* CHI KMM07 3
COMMON/ZHTEMP/ NZHT,ZHTZ(3),ZHT(31),TZHZ(3),TZH(31),TPFLAG KMM07 2
DIMENSION ANNUAL(31),TMPJAN(31,4),TMPJUL(31,4) TEMPZH 44
ZHT(I) ARE THE (NZHT=31) ALTITUDES AT WHICH THE TEMPERATURE TEMPZH 45
PROFILES ARE DEFINED. TEMPZH 46
DATA (ZHT(I),I=1,31) / 0.0,4.0,8.0,12.,16.,20.,24.,28.,32.,36., TEMPZH 47
40.,44.,48.,52.,56.,60.,64.,68.,72.,76., TEMPZH 48
80.,84.,88.,92.,96.,100.,104.,108.,112.,116.,120. / TEMPZH 49
ANNUAL(I), TEMPERATURES FOR 15-DEG N ANNUAL PROFILE (US-66). TEMPZH 50
DATA (ANNUAL(I),I=1,31) / 302.59,277.44,250.37,223.64,197.02, TEMPZH 51
206.71,219.23,227.94,236.63,245.32, TEMPZH 52
253.99,262.66,270.15,267.24,261.39,253.10,239.40,225.72, TEMPZH 53
212.06,198.41,184.78,177.10,177.05,179.50,185.77,190.70, TEMPZH 54
205.98,229.78,253.25,315.82,379.70 / TEMPZH 55
TMPJAN(I,1), TEMPERATURES FOR 30-DEG N JAN. PROFILE (US-66). TEMPZH 56
DATA (TMPJAN(I,1),I=1,31) / 288.52,268.44,242.32,216.40,205.91, TEMPZH 57

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| | | | |
|-----|---|--------|-----|
| | 207.92,216.90,224.83,232.74,242.14, | TEMPZH | 58 |
| | • 251.62,261.08,269.15,268.14,260.28,252.04,239.90,227.77,215.66, | TEMPZH | 59 |
| | • 203.56,191.47,191.10,191.04,199.56,211.72,222.43,237.68,256.88, | TEMPZH | 60 |
| | • 275.76,304.46,333.30 / | TEMPZH | 61 |
| C | TEMPJAN(I,2), TEMPERATURES FOR 45-DEG N JAN. PROFILE (US-66). | TEMPZH | 62 |
| | DATA (TEMPJAN(I,2),I=1,31) / 272.59,255.79,231.72,218.66,216.67, | TEMPZH | 63 |
| | • 215.15,215.15,215.85,219.02,230.92, | TEMPZH | 64 |
| | • 243.17,255.41,265.65,265.65,258.63,250.77,242.93,234.76,226.54, | TEMPZH | 65 |
| | • 218.34,210.14,201.89,199.54,201.02,210.50,218.58,232.65,250.58, | TEMPZH | 66 |
| | • 260.65,301.06,333.30 / | TEMPZH | 67 |
| C | TEMPJAN(I,3), TEMPERATURES FOR 60-DEG N JAN. PROFILE (US-66). | TEMPZH | 68 |
| | DATA (TEMPJAN(I,3),I=1,31) / 257.28,247.81,220.55,217.15,216.56, | TEMPZH | 69 |
| | • 214.17,211.79,214.06,218.03,224.76, | TEMPZH | 70 |
| | • 234.65,244.53,254.40,260.15,257.30,250.89,248.93,246.97,241.12, | TEMPZH | 71 |
| | • 232.51,223.91,215.27,206.63,205.55,212.70,218.49,230.24,245.33, | TEMPZH | 72 |
| | • 261.48,297.50,333.30 / | TEMPZH | 73 |
| C | TEMPJAN(I,4), TEMPERATURES FOR 75-DEG N JAN. PROFILE (US-66). | TEMPZH | 74 |
| | DATA (TEMPJAN(I,4),I=1,31) / 254.00,239.89,217.86,213.25,210.05, | TEMPZH | 75 |
| | • 207.65,207.65,212.50,218.03,224.76, | TEMPZH | 76 |
| | • 234.65,244.53,254.40,260.15,257.30,250.89,248.93,246.97,241.12, | TEMPZH | 77 |
| | • 232.51,223.91,215.27,206.63,205.55,212.70,218.49,230.24,245.33, | TEMPZH | 78 |
| | • 261.48,297.50,333.30 / | TEMPZH | 79 |
| C | TEMPJUL(I,1), TEMPERATURES FOR 30-DEG N JULY PROFILE (US-66). | TEMPZH | 80 |
| | DATA (TEMPJUL(I,1),I=1,31) / 304.58,277.87,252.41,224.42,203.15, | TEMPZH | 81 |
| | • 211.75,219.90,227.83,235.74,245.14, | TEMPZH | 82 |
| | • 254.62,264.08,272.15,271.14,263.28,254.79,239.91,225.04,210.19, | TEMPZH | 83 |
| | • 195.36,180.54,172.50,172.45,175.71,183.55,190.03,209.16,237.66, | TEMPZH | 84 |
| | • 265.72,322.72,379.70 / | TEMPZH | 85 |
| C | TEMPJUL(I,2), TEMPERATURES FOR 45-DEG N JULY PROFILE (US-66). | TEMPZH | 86 |
| | DATA (TEMPJUL(I,2),I=1,31) / 296.22,273.57,248.26,222.30,215.65, | TEMPZH | 87 |
| | • 219.17,223.94,229.49,237.81,247.64, | TEMPZH | 88 |
| | • 257.52,267.39,275.65,275.65,266.87,257.05,244.52,226.89,209.28, | TEMPZH | 89 |
| | • 191.69,174.12,165.10,165.06,169.98,180.96,190.51,214.04,246.42, | TEMPZH | 90 |
| | • 278.63,329.46,379.70 / | TEMPZH | 91 |
| C | TEMPJUL(I,3), TEMPERATURES FOR 60-DEG N JULY PROFILE (US-66). | TEMPZH | 92 |
| | DATA (TEMPJUL(I,3),I=1,31) / 288.45,265.87,239.18,225.15,225.15, | TEMPZH | 93 |
| | • 225.15,226.56,232.52,238.47,250.18, | TEMPZH | 94 |
| | • 262.05,272.48,276.82,277.15,271.99,262.73,244.26,225.83,207.41, | TEMPZH | 95 |
| | • 189.01,170.64,161.71,161.66,167.51,179.67,190.39,217.12,252.57, | TEMPZH | 96 |
| | • 288.06,334.14,379.70 / | TEMPZH | 97 |
| C | TEMPJUL(I,4), TEMPERATURES FOR 75-DEG N JULY PROFILE (US-66). | TEMPZH | 98 |
| | DATA (TEMPJUL(I,4),I=1,31) / 278.92,262.09,235.87,228.65,230.15, | TEMPZH | 99 |
| | • 230.15,230.71,235.48,241.00,250.18, | TEMPZH | 100 |
| | • 262.05,272.48,276.82,277.15,271.99,262.73,244.26,225.83,207.41, | TEMPZH | 101 |
| | • 189.01,170.64,161.71,161.66,167.51,179.67,190.39,217.12,252.57, | TEMPZH | 102 |
| | • 288.06,334.14,379.70 / | TEMPZH | 103 |
| | DATA PI / 3.141592653590 /, NZHT / J1 / | TEMPZH | 104 |
| CCC | | TEMPZH | 105 |
| C | IF PPFLAG HAS BEEN SET (NIN Z&ND) USER READS IN HIS OWN | TEMPZH | 106 |
| C | TEMPERATURE PROFILE AT ALTITUDES ZZ = 0.0 (4.0) 120. KM. | TEMPZH | 107 |
| CCC | | TEMPZH | 108 |
| | IF(PPFLAG.EQ.0.0) GO TO 8 | TEMPZH | 109 |
| | READ(5,101) (TZN(N),N=1,NZHT) | TEMPZH | 110 |
| 101 | FORMAT (8E10.4) | TEMPZH | 111 |
| | GO TO 99 | TEMPZH | 112 |
| 3 | PIHD = PI/180. | TEMPZH | 113 |
| C | DETERMINE INDEX, LAT&ND, OF 15-DEG LATITUDE BAND, | TEMPZH | 114 |

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|---|--|--------|-----|
| C | INCREASING POLEWARD. | TEMPZH | 115 |
| | ALAT = ABS(PLAT)/PI180 | TEMPZH | 116 |
| | LATBND = (ALAT*15.)/15. | TEMPZH | 117 |
| | IF(LATBND.GT.6) LATBND = 6 | TEMPZH | 118 |
| C | DETERMINE INDEX, IB, OF LATITUDE BOUNDARY, WITH IB=0,1,2,3,4 | TEMPZH | 119 |
| C | CORRESPONDING TO LATITUDES 15-, 30-, 45-, 60-, AND 75-DEGREES, | TEMPZH | 120 |
| C | RESPECTIVELY. | TEMPZH | 121 |
| | IB = LATBND-1 | TEMPZH | 122 |
| | IF(LATBND.EQ.6) IB = IB-1 | TEMPZH | 123 |
| C | DETERMINE FRACTIONAL VALUE OF POSITION OF INTEREST WITHIN | TEMPZH | 124 |
| C | LATITUDE BAND. | TEMPZH | 125 |
| | PLAT = ALAT/15. - FLOAT(IB) | TEMPZH | 126 |
| | PLATN1 = 1.0-PLAT | TEMPZH | 127 |
| | FSTMI = 1.0-FST | TEMPZH | 128 |
| | GO TO (11,21,31,31,31,41), LATBND | TEMPZH | 129 |
| C | DETERMINE TEMPERATURE PROFILE FOR 0- TO 15-DEG LATITUDE BAND | TEMPZH | 130 |
| C | (N) LATITUDE OR SEASONAL DEPENDENCE). | TEMPZH | 131 |
| | 11 DO 10 N=1,NZHT | TEMPZH | 132 |
| | TZH(N) = ANNUAL(N) | TEMPZH | 133 |
| | 10 CONTINUE | TEMPZH | 134 |
| | 20 TO 99 | TEMPZH | 135 |
| C | DETERMINE TEMPERATURE PROFILE FOR POSITION WITHIN 15- TO | TEMPZH | 136 |
| C | 30-DEG LATITUDE BAND (SEASONAL DEPENDENCE). | TEMPZH | 137 |
| | 21 DO 20 N=1,NZHT | TEMPZH | 138 |
| | F30 = FST*TMPJUL(N,IB) + FSTMI*TMPJAN(N,IB) | TEMPZH | 139 |
| | TZH(N) = PLATN1*ANNUAL(N) + PLAT*F30 | TEMPZH | 140 |
| | 20 CONTINUE | TEMPZH | 141 |
| | 30 TO 99 | TEMPZH | 142 |
| C | DETERMINE TEMPERATURE PROFILE FOR POSITION WITHIN 30- TO | TEMPZH | 143 |
| C | 45-DEG, 45- TO 60-DEG, OR 60- TO 75-DEG LATITUDE BAND | TEMPZH | 144 |
| C | (SEASONAL DEPENDENCE). | TEMPZH | 145 |
| | 31 DO 30 N=1,NZHT | TEMPZH | 146 |
| | FLBND = FST*TMPJUL(N,IB-1) + FSTMI*TMPJAN(N,IB-1) | TEMPZH | 147 |
| | FUBND = FST*TMPJUL(N, IB) + FSTMI*TMPJAN(N, IB) | TEMPZH | 148 |
| | TZH(N) = PLATN1*FLBND + PLAT*FUBND | TEMPZH | 149 |
| | 30 CONTINUE | TEMPZH | 150 |
| | 40 TO 99 | TEMPZH | 151 |
| C | DETERMINE TEMPERATURE PROFILE FOR 75- TO 90-DEG LATITUDE BAND | TEMPZH | 152 |
| C | (SEASONAL DEPENDENCE). | TEMPZH | 153 |
| | 41 DO 40 N=1,NZHT | TEMPZH | 154 |
| | TZH(N) = FST*TMPJUL(N,IB) + FSTMI*TMPJAN(N,IB) | TEMPZH | 155 |
| | 40 CONTINUE | TEMPZH | 156 |
| | 99 RETURN | TEMPZH | 157 |
| | END | TEMPZH | 158 |

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| | IX = 6 | WATER | 58 |
| | DO T) 122 | WATER | 59 |
| 102 | IF(DLAT.LE.125.) GO TO 104 | WATER | 60 |
| | IX = 4 | WATER | 61 |
| | DO T) 122 | WATER | 62 |
| 104 | IF(DLAT.LE.120.) GO TO 106 | WATER | 63 |
| | IX = 3 | WATER | 64 |
| | DO T) 122 | WATER | 65 |
| 105 | IF(DLAT.LT.60.) GO T) 110 | WATER | 66 |
| | IF((DLAT.GE.105.) .AND. ((DLON.GE.120.) .AND. (DLON.LE.150.))) | WATER | 67 |
| | * GO TO 108 | WATER | 68 |
| | IF((DLAT.LE.80.) .AND. ((DLON.GE.150.) .OR. (DLON.LE.50.))) | WATER | 69 |
| | * GO TO 108 | WATER | 70 |
| | IX = 1 | WATER | 71 |
| | DO T) 122 | WATER | 72 |
| 109 | IX = 2 | WATER | 73 |
| | DO T) 122 | WATER | 74 |
| 110 | IF(DLAT.LT.50.) GO TO 114 | WATER | 75 |
| | IF((DLAT.LT.55.) .AND. ((DLON.GT.235.) .AND. (DLON.LE.240.))) | WATER | 76 |
| | * GO TO 112 | WATER | 77 |
| | IX = 3 | WATER | 78 |
| | DO T) 122 | WATER | 79 |
| 112 | IX = 4 | WATER | 80 |
| | DO T) 122 | WATER | 81 |
| 114 | IF((DLON.GT.230.) .AND. (DLON.LT.255.)) GO TO 118 | WATER | 82 |
| | IF((DLAT.LT.45.) .AND. ((DLON.GE.255.) .AND. (DLON.LE.303.))) | WATER | 83 |
| | * GO TO 116 | WATER | 84 |
| | IF((DLON.GE.110.) .AND. (DLON.LE.135.)) GO TO 116 | WATER | 85 |
| | IF((DLAT.LT.40.) .AND. ((DLON.GT.30.) .AND. (DLON.LT.110.))) | WATER | 86 |
| | * GO TO 116 | WATER | 87 |
| | IX = 4 | WATER | 88 |
| | DO T) 122 | WATER | 89 |
| 116 | IX = 5 | WATER | 90 |
| | DO T) 122 | WATER | 91 |
| 118 | IF(DLAT.LT.40.) GO T) 120 | WATER | 92 |
| | IF(DLON.LE.240.) GO TO 112 | WATER | 93 |
| | IF((DLAT.LT.45.) .AND. ((DLON.GE.247.) .AND. (DLON.LT.255.))) | WATER | 94 |
| | * GO TO 112 | WATER | 95 |
| | IX = 3 | WATER | 96 |
| | DO T) 122 | WATER | 97 |
| 120 | IF(DLON.GE.247.) GO TO 116 | WATER | 99 |
| | IX = 3 | WATER | 99 |
| 122 | CONTINUE | WATER | 100 |
| CCC | | WATER | 101 |
| CCC | EVALUATE PARAMETERS AT 5- AND 14-KM ALTITUDE. | WATER | 102 |
| CCC | | WATER | 103 |
| | PVRJ60 = 160.*PVR-120. | WATER | 104 |
| | SINDAY = SIN(PVRJ60*PI180) | WATER | 105 |
| C | EVALUATE NATURAL LOG OF H2O MIXING RATIO AT 5 KM, ZMR005 | WATER | 106 |
| | ZHKM = 5.0 | WATER | 107 |
| | AA = (ALRZ(1,IX)*ZHKM + ALRZ(2,IX))*ZHKM + ALRZ(1,IX) | WATER | 108 |
| | BB = BLRZ(IX) - (0.4945 + 2.33E-04*ALAT)*ZHKM | WATER | 109 |
| | IF(IX.EQ.7 .OR. IX.EQ.5 .OR. IX.EQ.6) GO TO 126 | WATER | 110 |
| 124 | ZMR005 = EXP(AA*SINDAY*BB) | WATER | 111 |
| | ZMR005 = ALJ5(ZMR005/RHO5KM) | WATER | 112 |
| | DO T) 129 | WATER | 113 |
| 125 | RR = RR - (0.1170*%VIR-03*ALAT)*EXP(-ZHKM) | WATER | 114 |

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| | 30 TO 124 | WATER | 115 |
| C | EVALUATE NATURAL LOG OF H2O MIXING RATIO AT 14 AM, ZMR014 | WATER | 115 |
| 120 | ZHKM = 14. | WATER | 117 |
| | CC = FYR360 - 6.92*ALAT/(1.0+EXP(-0.805*(ZHKM-18.))) | WATER | 118 |
| | DD = 0.0619*ZHKM*EXP(-0.0226*ZHKM) | WATER | 119 |
| | DLBLB1 = 1.0/(1.0+EXP(0.44*(ALAT-28.))) | WATER | 120 |
| | DD = DD + 30.9*DLBLB1*EXP(-0.221*ZHKM) | WATER | 121 |
| | ZMR014 = DD*(1.0+323.*EXP(-0.448*ZHKM)*SIN(CC*PI/180)) | WATER | 122 |
| | WRITE(6,901) IX,FYR,FST | WATER | 123 |
| 901 | FORMAT (1H0,24H FROM SUBROUTINE WATER-,5H IX=,13,5X,5H FYR=, | WATER | 124 |
| | 5 P8.5,5X,5H FST=,P8.5) | WATER | 125 |
| | RETURN | WATER | 126 |
| 200 | CONTINUE | WATER | 127 |
| | IF(ZH.GE.14.) GO TO 212 | WATER | 128 |
| | IF(ZH.GE. 5.) GO TO 214 | WATER | 129 |
| | AA = (ALRZ(3,IX)*ZH + ALRZ(2,IX))*ZH + ALRZ(1,IX) | WATER | 130 |
| | BB = BLR(IX) - (0.4845 + 2.33E-04*ALAT)*ZH | WATER | 131 |
| | IF(IX.EQ.2 .OR. IX.EQ.5 .OR. IX.EQ.6) GO TO 210 | WATER | 132 |
| 200 | SMR = EXP(AA*SINDAY+BB) | WATER | 133 |
| | SMR = SMR/RND | WATER | 134 |
| | GO TO 216 | WATER | 135 |
| 210 | BB = BB - (0.1170 + 5.91E-03*ALAT)*EXP(-ZH) | WATER | 136 |
| | GO TO 200 | WATER | 137 |
| 212 | CC = FYR360 - 6.92*ALAT/(1.0+EXP(-0.805*(ZH-18.))) | WATER | 138 |
| | DD = 0.0619*ZH*EXP(-0.0226*ZH) | WATER | 139 |
| | DD = DD + 30.9*DLBLB1*EXP(-0.221*ZH) | WATER | 140 |
| | SMR = EXP(DD*(1.0+323.*EXP(-0.448*ZH)*SIN(CC*PI/180))) | WATER | 141 |
| | GO TO 216 | WATER | 142 |
| 214 | SMR = EXP(ZMR014+(ZMR005-ZMR014)*(14.-ZH)/9.) | WATER | 143 |
| 216 | W20 = SMR | WATER | 144 |
| | RETURN | WATER | 145 |
| | END | WATER | 146 |

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SUBROUTINE WVOPT(JJ,HKM,H2O4R)                                WVOPT      2
CCC                                                         WVOPT      3
C   SUBROUTINE WVOPT ALLOWS THE USER TO BYPASS THE NORMAL  WVOPT      4
C   TREATMENT (ACHIEVED BY SETTING WVFLAG=0.0) OF WATER VAPOR IN WVOPT      5
C   SUBROUTINE SPCMIN FOR THE ALTITUDE RANGE FROM 0. TO 120. KM. WVOPT      6
C   THE USER EFFECTS THE BYPASS BY READING IN WVFLAG.GT.0.0 AND WVOPT      7
C   HIS OWN DATA IN ONE OF FOUR OPTIONAL FORMS ACCORDING TO WVOPT      8
C   METHOD = 1,2,3,4. WVOPT      9
C   IT IS ANTICIPATED THAT THE USER WILL BE MOST INTERESTED IN WVOPT     10
C   USING HIS OWN LOW-ALTITUDE DATA OVER THE ALTITUDE RANGE FROM WVOPT     11
C   HH(1)=0.0 TO HH(NJP), BUT HE MUST ALSO ACTUALLY READ IN DATA WVOPT     12
C   OVER THE REMAINING HIGHER-ALTITUDE RANGE FROM HH(NOP+1) TO WVOPT     13
C   HH(NZH)=120. IF THE USER HAS NO PERSONAL PREFERENCE FOR DATA WVOPT     14
C   IN THE HIGHER-ALTITUDE RANGE, HE MAY FIND IT CONVENIENT TO WVOPT     15
C   USE THE DATA IN A DATA STATEMENT IN SUBROUTINE SPCMIN, GIVEN WVOPT     16
C   AT ALTITUDES 20(5)120 KM AND IN UNITS OF PARTS PER MILLION BY WVOPT     17
C   MASS (PPMM). WVOPT     18
CCC                                                         WVOPT     19
CCC   THIS IS A NEW ROUTINE FOR ROSCOE-IR. WVOPT     20
CCC                                                         WVOPT     21
C   INPUT PARAMETERS WVOPT     22
C   ARGUMENT LIST WVOPT     23
C       JJ - =1 FOR INITIALIZATION CALL. WVOPT     24
C           =2 NORMAL OPERATION CALL WVOPT     25
C       HKM - ALTITUDE OF INTEREST, KM (USED ONLY IF JJ=2) WVOPT     26
C   ATMOSP COMMON WVOPT     27
C       RHO - DENSITY, GRAMS/CM**3 WVOPT     28
C       TT - TEMPERATURE, DEGREES KELVIN WVOPT     29
C   VPC COMMON WVOPT     30
C       METHOD - FLAG INDICATING ONE OF FOUR OPTIONS, WVOPT     31
C           =1 DATA VALUES IN PARTS PER MILLION BY MASS WVOPT     32
C           =2 DATA VALUES IN ABSOLUTE HUMIDITY, WVOPT     33
C             GRAMS/METERS**3 WVOPT     34
C           =3 DATA VALUES IN RELATIVE HUMIDITY, PERCENT WVOPT     35
C             (10 PERCENT IS INPUT AS 10. NOT 0.10) WVOPT     36
C           =4 DATA VALUES IN DEW-POINT TEMPERATURE, DEG K WVOPT     37
C   NOTE - FOR METHOD = 2,3, OR 4 THE SUBROUTINE CONVERTS WVOPT     38
C   THE FIRST NOP VALUES OF THE DATA INTO PARTS WVOPT     39
C   PER MILLION BY MASS, DURING INITIALIZATION. WVOPT     40
C   DATA READ IN WVOPT     41
C   HH(N) - ALTITUDE ARRAY, 0.0 TO 120.0 KM WVOPT     42
C   WVC(N) - H2O DATA USING ONE OF THE FOUR OPTIONS. WVOPT     43
C   FOR N=1,NOP, DATA HAVE DIMENSIONS DICTATED BY WVOPT     44
C   THE OPTION USED. FOR N=NJP+1,NZH, DATA HAVE WVOPT     45
C   DIMENSIONS OF PARTS PER MILLION BY MASS. WVOPT     46
C   NOP = NZH IS A VALID INPUT CONDITION. WVOPT     47
C   OUTPUT PARAMETER WVOPT     48
C   ARGUMENT LIST WVOPT     49
C   H2O4R - WATER VAPOR CONTENT OF MOIST AIR IN UNITS OF WVOPT     50
C   PARTS PER MILLION BY MASS AT ALTITUDE HKM. WVOPT     51
C   WVOPT     52
CCC                                                         WVOPT     53
C   DIMENSION HH(61),WVC(61) WVOPT     54
C   COMMON/ATMOSP/ HL,S3AR,LDOWN,PP,RHO,TT,SN1(3),NRHO,PENSEQ WVOPT     55
C   COMMON/VPC/ WVFLAG,METHOD,H2O120 WVOPT     56
C   DATA CASC,ZMH2O / 8.31416781E+07,18.016 / WVOPT     57
C   20 TO (100,200), JJ WVOPT     58

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| CC | INITIALIZATION, CALLED FROM MAIN PROGRAM AFTER SUBROUTINE | WVUPT | 59 |
| CC | ATMOSU HAS BEEN INITIALIZED. | WVUPT | 60 |
| 100 | IF(METHOD) 111,111,112 | WVUPT | 61 |
| 111 | RETURN | WVUPT | 62 |
| 112 | READ(5,103) MZH,NOP | WVUPT | 63 |
| 103 | FORMAT (215) | WVUPT | 64 |
| | READ(5,105) (HH(N),WVC(N),N=1,MZd) | WVUPT | 65 |
| 105 | FORMAT (Dd10.4) | WVUPT | 66 |
| | ETH = METHJD | WVUPT | 67 |
| | GO TO (120,140,160,180), MTH | WVUPT | 68 |
| 120 | RETURN | WVUPT | 69 |
| CC | METHOD-2 INITIALIZATION. | WVUPT | 70 |
| 140 | DO 144 N=1,NOP | WVUPT | 71 |
| | ZZ = HH(N) | WVUPT | 72 |
| | CALL ATMOSU(2,ZZ) | WVUPT | 73 |
| | WVC(N) = WVC(N)/RHO | WVUPT | 74 |
| CC | WATER-VAPOR-CONTENT DATA, WVC(N) NOW EXPRESSED IN UNITS OF | WVUPT | 75 |
| CC | PARTS PER MILLION BY MASS. | WVUPT | 76 |
| 144 | CONTINUE | WVUPT | 77 |
| | DO TO 111 | WVUPT | 78 |
| CC | METHOD-3 INITIALIZATION. | WVUPT | 79 |
| 160 | RZH = GASC/ZMH2O | WVUPT | 80 |
| | DO 164 N=1,NOP | WVUPT | 81 |
| | ZZ = HH(N) | WVUPT | 82 |
| | CALL ATMOSU(2,ZZ) | WVUPT | 83 |
| | VPH2J = 0.0 | WVUPT | 84 |
| | VPICE = 0.0 | WVUPT | 85 |
| | IF((TT .GE. 173.15) .AND. (TT .LE. 373.15)) | WVUPT | 86 |
| | *CALL H2OSVP(TT,VPH2J,VPICE) | WVUPT | 87 |
| CC | DO# HAVE SATURATED VAPOR PRESSURE OVER A WATER SURFACE AT | WVUPT | 88 |
| CC | TEMPERATURE TT, VPH2O (MILLIBARS). | WVUPT | 89 |
| | WVC(N) = 1.0E+07*WVC(N)*VPH2O/(RZH*TT*MHO) | WVUPT | 90 |
| 164 | CONTINUE | WVUPT | 91 |
| | DO TO 111 | WVUPT | 92 |
| CC | METHOD-4 INITIALIZATION. | WVUPT | 93 |
| 180 | RZH = GASC/ZMH2O | WVUPT | 94 |
| | DO 184 N=1,NOP | WVUPT | 95 |
| | PD = WVC(N) | WVUPT | 96 |
| | ZZ = HH(N) | WVUPT | 97 |
| | CALL ATMOSU(2,ZZ) | WVUPT | 98 |
| | VPH2J = 0.0 | WVUPT | 99 |
| | VPICE = 0.0 | WVUPT | 100 |
| | IF((TT .GE. 173.15) .AND. (TT .LE. 373.15)) | WVUPT | 101 |
| | *CALL H2OSVP(TT,VPH2J,VPICE) | WVUPT | 102 |
| | WVC(N) = 1.0E+09*VPH2O/(RZH*TT*MHO) | WVUPT | 103 |
| 184 | CONTINUE | WVUPT | 104 |
| | DO TO 111 | WVUPT | 105 |
| CC | START LOGARITHMIC INTERPOLATION SECTION, CALLED FROM MAIN | WVUPT | 106 |
| CC | PROGRAM AT ALTITUDE HKM=120. AS PART OF THE INITIALIZATION | WVUPT | 107 |
| CC | PROCEDURE AND FROM THE H2J PORTION OF SUBROUTINE SPCMIN | WVUPT | 108 |
| CC | DURING OPERATION. | WVUPT | 109 |
| 200 | CONTINUE | WVUPT | 110 |
| | IX1 = 1 | WVUPT | 111 |
| | IX3 = MZH | WVUPT | 112 |
| 1092 | IX2 = (IX1+IX3)/2 | WVUPT | 113 |
| CC | IX1,IX2, AND IX3 ARE TRIAL INDICES USED IN THE SEARCH ROUTINE. | WVUPT | 114 |
| | IF(IX2.EQ.IX1) GO TO 1102 | WVUPT | 115 |

| | | | |
|------|---|-------|-----|
| | IF(HKM-HH(NX2)) 1094,1102,1100 | AVOPT | 116 |
| 1094 | IF(NX2-NX1-1) 1098,1096,1098 | AVOPT | 117 |
| CC | NX1 = INDEX NUMBER OF THE TABULAR ALTITUDE AT OR JUST BELOW | AVOPT | 118 |
| CC | THE ALTITUDE OF INTEREST (HKM). | AVOPT | 119 |
| 1096 | NX1 = NX1 | AVOPT | 120 |
| | GO TO 1106 | AVOPT | 121 |
| 1098 | NX3 = NX2 | AVOPT | 122 |
| | GO TO 1092 | AVOPT | 123 |
| 1100 | IF(NX3-NX2-1) 1104,1102,1104 | AVOPT | 124 |
| 1102 | NX1 = NX2 | AVOPT | 125 |
| | GO TO 1106 | AVOPT | 126 |
| 1104 | NX1 = NX2 | AVOPT | 127 |
| | GO TO 1092 | AVOPT | 128 |
| CC | ZD = FRACTIONAL DISTANCE THAT THE ALTITUDE OF INTEREST IS | AVOPT | 129 |
| CC | ABOVE THE LOWER OF THE TWO ADJACENT TABULATED ALTITUDES. | AVOPT | 130 |
| 1106 | ZD = (HKM-HH(NX1))/(HH(NX1+1)-HH(NX1)) | AVOPT | 131 |
| | H2DMR = MVC(NX1)*(MVC(NX1+1)/MVC(NX1))**ZD | AVOPT | 132 |
| | RETURN | AVOPT | 133 |
| | END | AVOPT | 134 |

| | | | |
|-----|---|--------|----|
| | SUBROUTINE ZTTOU | ZTTOU | 2 |
| CCC | | ZTTOU | 3 |
| C | SUBROUTINE ZTTOU CONVERTS A GREGORIAN CALENDAR DATE (20 TH | ZTTOU | 4 |
| C | CENTURY YEAR (YRS, MONTH (MONS, DAY (DAYS) AND ZONE TIME ZT | ZTTOU | 5 |
| C | AT EAST LONGITUDE PLON TO GREGORIAN CALENDAR DATE AND MEAN | ZTTOU | 6 |
| C | TIME UT AT GREENWICH. | ZTTOU | 7 |
| CCC | | ZTTOU | 8 |
| C | REVISION 02 (11/18/74) PROVIDES... | ZTTOU | 9 |
| C | 1. TEST FOR LEGAL INPUT DATE. | ZTTOU | 10 |
| C | REVISION 03(10/15/77) PROVIDES... | ZTTOU | 11 |
| C | 2. CORRECTED COMPUTATION OF THE ZONE DESCRIPTION, ZO, | ZTTOU | 12 |
| C | WHEN ZO SHOULD BE 0. | ZTTOU | 13 |
| C | 3. REVISED COMMENT CARDS. | ZTTOU | 14 |
| C | REVISION 04 (03/01/78) PROVIDES... | ZTTOU | 15 |
| C | 4. REVISED TIME COMMON FOR MUSCOE-IN. | ZTTOU | 16 |
| C | REVISION 05 (02/08/79) PROVIDES... | ZTTOU | 17 |
| C | 5. CONVERSION OF PLON TO THE CORRESPONDING POSITIVE | ZTTOU | 18 |
| C | QUANTITY IF INPUTTED AS A NEGATIVE QUANTITY. | ZTTOU | 19 |
| C | INPUT PARAMETERS | ZTTOU | 20 |
| C | YRS - NUMBER OF THE YEAR IN THE 1900 S (E.G., 1974 | ZTTOU | 21 |
| C | BECOMES 74), IN LOCAL TIME ZONE. | ZTTOU | 22 |
| C | MONS - NUMBER OF THE MONTH (E.G., FEBRUARY BECOMES 2), | ZTTOU | 23 |
| C | IN LOCAL TIME ZONE. | ZTTOU | 24 |
| C | DAYS - DAY OF THE MONTH, IN LOCAL TIME ZONE. | ZTTOU | 25 |
| C | ZT - ZONE TIME FOR THE 15-DEGREE LONGITUDE INTERVAL | ZTTOU | 26 |
| C | CONTAINING PLON (DECIMAL HRS) | ZTTOU | 27 |
| C | NOTE. A VALUE OF 24.0, TREATED BY THE CODE AS | ZTTOU | 28 |
| C | ILLEGAL, MUST BE INPUTTED AS 0.0 ON THE NEXT DAY. | ZTTOU | 29 |
| C | PLON - EAST LONGITUDE OF POINT P (RADIAN) | ZTTOU | 30 |
| C | (PLON MUST BE POSITIVE) | ZTTOU | 31 |
| CCC | | ZTTOU | 32 |
| C | OUTPUT PARAMETERS | ZTTOU | 33 |
| C | YRS - A POSSIBLY REVISED VALUE OF THE INPUT PARAMETER, | ZTTOU | 34 |
| C | CORRESPONDING TO GREENWICH. | ZTTOU | 35 |
| C | MONS - A POSSIBLY REVISED VALUE OF THE INPUT PARAMETER, | ZTTOU | 36 |
| C | CORRESPONDING TO GREENWICH. | ZTTOU | 37 |
| C | DAYS - A POSSIBLY REVISED VALUE OF THE INPUT PARAMETER, | ZTTOU | 38 |
| C | CORRESPONDING TO GREENWICH. | ZTTOU | 39 |
| C | UT - UNIVERSAL TIME (DECIMAL HRS) | ZTTOU | 40 |
| CCC | | ZTTOU | 41 |
| C | DEFINITION OF DATA | ZTTOU | 42 |
| C | IDAYNO(I) = DAYS IN THE I TH MONTH OF A NON-LEAP YEAR | ZTTOU | 43 |
| CCC | | ZTTOU | 44 |
| C | COMMON/TIME/ YRS,MONS,DAYS,ZT,PLAT,PLON,UT,CAT,FVR,FST,RMUSKM | KUMNO7 | 2 |
| C | ,CHI | KUMNO7 | 3 |
| C | DIMENSION IDAYNO(12) | ZTTOU | 46 |
| C | DATA (IDAYNO(1),I=1,12) / 31,28,31,30,31,30,31,31,30,31,30,31 / | ZTTOU | 47 |
| C | DATA PI / 3.141592653590 / | ZTTOU | 48 |
| CCC | | ZTTOU | 49 |
| C | CONVERSION FROM ZONE TIME ZT TO GREENWICH MEAN TIME (I.E., | ZTTOU | 50 |
| C | UNIVERSAL TIME UT) IS DONE BY FIRST FINDING THE TIME ZONE | ZTTOU | 51 |
| C | CONTAINING THE LONGITUDE PLON. | ZTTOU | 52 |
| C | N7PTS IS THE INTEGRAL NUMBER OF 7.5-DEGREE INTERVALS IN THE | ZTTOU | 53 |
| C | WESTERLY DIRECTION FROM GREENWICH TO THE LONGITUDE OF INTEREST | ZTTOU | 54 |
| C | PLON. N7PTS MAY BE 0 OR ANY INTEGER UP TO AND INCLUDING 47. | ZTTOU | 55 |
| C | HOWEVER, THE TIME-ZONE NUMBER IZONE IS 0 FOR N7PTS EQUAL TO | ZTTOU | 56 |
| C | 0 OR 47. IZONE RANGES FROM 0 TO 23. | ZTTOU | 57 |

| | | | |
|-----|---|--------|-----|
| CCC | | ZTTOUT | 58 |
| C | TEST WHETHER INPUT DATE IS LEGAL. | ZTTOUT | 59 |
| | IF(ZT.LT.0.0 .OR. ZT.GE.24.) GO TO 999 | ZTTOUT | 60 |
| | IF(IYRS.LT.1 .OR. IYRS.GT.99) GO TO 999 | ZTTOUT | 61 |
| | IF(IMONS.LT.1 .OR. IMONS.GT.12) GO TO 999 | ZTTOUT | 62 |
| C | IF YRS IS A LEAP YEAR, SET IDAYNO(2) = 29 | ZTTOUT | 63 |
| | LEAP = MOD(IYRS,4) | ZTTOUT | 64 |
| | IF(LEAP.EQ.0) IDAYNO(2) = 29 | ZTTOUT | 65 |
| | IF(IDAYS.LT.1 .OR. IDAYS.GT.IDAYNO(IMONS)) GO TO 999 | ZTTOUT | 66 |
| | PI2 = 2.*PI | ZTTOUT | 67 |
| | PID2 = PI/2. | ZTTOUT | 68 |
| | RADDEG = PI/180. | ZTTOUT | 69 |
| | IF(PLOM .LT. 0.0) PLOM = PLOM + PI2 | ZTTOUT | 70 |
| | M7PTS = (PI2-PLOM)/(7.5*RADDEG) | ZTTOUT | 71 |
| | IF(M7PTS-47) 10,20,20 | ZTTOUT | 72 |
| 10 | IZONE = (M7PTS+1)/2 | ZTTOUT | 73 |
| | GO TO 33 | ZTTOUT | 74 |
| 20 | IZONE = 24 | ZTTOUT | 75 |
| 30 | ZONE = FLOAT(IZONE) | ZTTOUT | 76 |
| CCC | | ZTTOUT | 77 |
| C | SHIFT TO CONVENTIONAL ZONE DESCRIPTION, ZD (SEE, E.G., | ZTTOUT | 78 |
| C | AMERICAN PRACTICAL NAVIGATOR (ORIGINALLY BY N. BONDITCH), | ZTTOUT | 79 |
| C | U.S. NAVY H.O. PUB. NO. 9, P.489, OF 1962 CORRECTED REPRINT | ZTTOUT | 80 |
| C | EDITION, AVAILABLE FROM U.S. GOV. PRINTING OFFICE). | ZTTOUT | 81 |
| CCC | | ZTTOUT | 82 |
| | IF(PLOM.GT.PI) GO TO 35 | ZTTOUT | 83 |
| | ZD = ZONE-24. | ZTTOUT | 84 |
| | GO TO 43 | ZTTOUT | 85 |
| 35 | ZD = ZONE | ZTTOUT | 86 |
| 40 | JT = ZT+ZD | ZTTOUT | 87 |
| C | MUST SHIFT TO NEXT DAY IF(UT.GE.24.) | ZTTOUT | 88 |
| | IF(UT.GE.24.) GO TO 50 | ZTTOUT | 89 |
| C | MUST SHIFT TO PREVIOUS DAY IF(UT.LT.0.) | ZTTOUT | 90 |
| | IF(UT.LT.0.0) GO TO 45 | ZTTOUT | 91 |
| C | NO SHIFT IS NECESSARY IF(UT.GE.0.0 .AND. UT.LT.24.) | ZTTOUT | 92 |
| | GO TO 60 | ZTTOUT | 93 |
| 45 | JT = UT+24. | ZTTOUT | 94 |
| | IDAYS = IDAYS-1 | ZTTOUT | 95 |
| C | CORRECT MONTH AND YEAR IF NECESSARY, DUE TO CHANGING THE DATE | ZTTOUT | 96 |
| C | IN CONVERTING TO UT. | ZTTOUT | 97 |
| C | CORRECT IDAYS AND IMONS IF MONTH DECREASED AT GREENWICH | ZTTOUT | 98 |
| | IF(IDAYS.GE.1) GO TO 60 | ZTTOUT | 99 |
| | IDAYS = IDAYNO(IMONS-1) | ZTTOUT | 100 |
| | IMONS = IMONS-1 | ZTTOUT | 101 |
| C | CORRECT IMONS AND IYRS IF YEAR DECREASED AT GREENWICH | ZTTOUT | 102 |
| | IF(IMONS.GE.1) GO TO 60 | ZTTOUT | 103 |
| | IMONS = 12 | ZTTOUT | 104 |
| | IYRS = IYRS-1 | ZTTOUT | 105 |
| | GO TO 60 | ZTTOUT | 106 |
| 50 | JT = UT-24. | ZTTOUT | 107 |
| | IDAYS = IDAYS+1 | ZTTOUT | 108 |
| C | CORRECT MONTH AND YEAR IF NECESSARY, DUE TO CHANGING THE DATE | ZTTOUT | 109 |
| C | IN CONVERTING TO JT. | ZTTOUT | 110 |
| C | IF YRS IS A LEAP YEAR, SET IDAYNO(2) = 29 | ZTTOUT | 111 |
| | LEAP = MOD(IYRS,4) | ZTTOUT | 112 |
| | IF(LEAP.EQ.0) IDAYNO(2) = 29 | ZTTOUT | 113 |
| C | CORRECT IDAYS AND IMONS IF MONTH INCREASED AT GREENWICH | ZTTOUT | 114 |
| | IF(IDAYS.LE.IDAYNO(IMONS)) GO TO 60 | ZTTOUT | 115 |
| | IDAYS = 1 | ZTTOUT | 116 |
| | IMONS = IMONS+1 | ZTTOUT | 117 |
| C | CORRECT IMONS AND IYRS IF YEAR INCREASED AT GREENWICH | ZTTOUT | 118 |
| | IF(IMONS.LE.12) GO TO 60 | ZTTOUT | 119 |
| | IMONS = 1 | ZTTOUT | 120 |
| | IYRS = IYRS+1 | ZTTOUT | 121 |
| 60 | RETURN | ZTTOUT | 122 |
| 999 | WRITE(6,777) | ZTTOUT | 123 |
| 777 | FORMAT (40H0 * * * ILLEGAL DATE INPUTTED * * *) | ZTTOUT | 124 |
| | CALL EXIT | ZTTOUT | 125 |
| | END | ZTTOUT | 126 |

TEST VALUES READ IN

HALTS = 107

I ALTS(I),KM

| I | 0.00 | 1.00 | 2.00 | 3.00 | 4.00 | 5.00 | 6.00 |
|-----|--------|--------|--------|--------|--------|--------|--------|
| 7 | 6.00 | 7.00 | 8.00 | 9.00 | 10.00 | 11.00 | 12.00 |
| 13 | 12.00 | 13.00 | 14.00 | 15.00 | 16.00 | 17.00 | 18.00 |
| 19 | 19.00 | 20.00 | 21.00 | 22.00 | 23.00 | 24.00 | 25.00 |
| 25 | 24.00 | 25.00 | 26.00 | 27.00 | 28.00 | 29.00 | 30.00 |
| 31 | 30.00 | 31.00 | 32.00 | 33.00 | 34.00 | 35.00 | 36.00 |
| 37 | 36.00 | 37.00 | 38.00 | 39.00 | 40.00 | 41.00 | 42.00 |
| 43 | 42.00 | 43.00 | 44.00 | 45.00 | 46.00 | 47.00 | 48.00 |
| 49 | 48.00 | 49.00 | 50.00 | 51.00 | 52.00 | 53.00 | 54.00 |
| 55 | 54.00 | 55.00 | 56.00 | 57.00 | 58.00 | 59.00 | 60.00 |
| 61 | 60.00 | 61.00 | 62.00 | 63.00 | 64.00 | 65.00 | 66.00 |
| 67 | 66.00 | 67.00 | 68.00 | 69.00 | 70.00 | 71.00 | 72.00 |
| 73 | 72.00 | 73.00 | 74.00 | 75.00 | 76.00 | 77.00 | 78.00 |
| 79 | 78.00 | 79.00 | 80.00 | 81.00 | 82.00 | 83.00 | 84.00 |
| 85 | 84.00 | 85.00 | 86.00 | 87.00 | 88.00 | 89.00 | 90.00 |
| 91 | 90.00 | 91.00 | 92.00 | 93.00 | 94.00 | 95.00 | 96.00 |
| 97 | 96.00 | 97.00 | 98.00 | 99.00 | 100.00 | 101.00 | 102.00 |
| 103 | 102.00 | 103.00 | 104.00 | 105.00 | 106.00 | 107.00 | 108.00 |
| 109 | 108.00 | 109.00 | 110.00 | 111.00 | 112.00 | 113.00 | 114.00 |
| 115 | 114.00 | 115.00 | 116.00 | 117.00 | 118.00 | 119.00 | 120.00 |
| 121 | 119.00 | 120.00 | 121.00 | 122.00 | 123.00 | 124.00 | 125.00 |
| 127 | 125.00 | 126.00 | 127.00 | 128.00 | 129.00 | 130.00 | 131.00 |
| 133 | 130.00 | 131.00 | 132.00 | 133.00 | 134.00 | 135.00 | 136.00 |
| 139 | 136.00 | 137.00 | 138.00 | 139.00 | 140.00 | 141.00 | 142.00 |
| 145 | 142.00 | 143.00 | 144.00 | 145.00 | 146.00 | 147.00 | 148.00 |
| 151 | 148.00 | 149.00 | 150.00 | 151.00 | 152.00 | 153.00 | 154.00 |
| 157 | 154.00 | 155.00 | 156.00 | 157.00 | 158.00 | 159.00 | 160.00 |
| 163 | 160.00 | 161.00 | 162.00 | 163.00 | 164.00 | 165.00 | 166.00 |
| 169 | 166.00 | 167.00 | 168.00 | 169.00 | 170.00 | 171.00 | 172.00 |
| 175 | 172.00 | 173.00 | 174.00 | 175.00 | 176.00 | 177.00 | 178.00 |
| 181 | 178.00 | 179.00 | 180.00 | 181.00 | 182.00 | 183.00 | 184.00 |

EVMS = 77 EVMS = 1 IDAYS = 1
 ZT = -1200E+02 HRS GCD = -5500E+02 DEG CLW = .2400E+01 DEG
 WFFLAG = 0.00 METHOD = 0 TFFLAG = 0.00

INITIALIZATION CALL

FROM SUBROUTINE MATCH- IX = 3 FVN = .49509 FST = .99178
 ZIF = 1040.00 DEG K, TAU = 1.41055E-02 1/KM, FROM SUBROUTINE ATMOSU (FORMAT 8001)

EVMS = 77 EVMS = 1 IDAYS = 1
 ZI = -1200E+02 HRS GCD = .7599E+00 4AU CLW = .4109E+01 MAD

IGUM = 1 IT = .2000E+02 CAT = .755E+02 PLAT = .0109E+00 PLUM = .4109E+01

| | | | | | | | | |
|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 3.72E+05 | -6.59E-05 | 5.374E-04 | 9.290E+00 | 2.457E+02 | 1.000E+00 | 1.02E+06 | 1.661E+06 | 1.354E+12 |
| 3.076E+17 | 1.539E+14 | 2.218E+01 | 5.207E-05 | 5.507E-07 | 6.491E-01 | 4.955E-01 | 0. | 0. |
| 9.00 | | | | | | | | |
| 7.300E+18 | 2.110E+18 | 2.124E+04 | 9.000E+16 | 4.675E+14 | 3.200E+15 | 0. | 0. | 5.455E+01 |
| 2.582E+01 | 1.317E+09 | 2.187E+03 | 2.045E+07 | 6.201E+11 | 1.749E+15 | 0. | 0. | 0. |
| 2.494E+05 | -1.048E-04 | 4.609E-04 | 6.719E+00 | 4.186E+02 | 1.000E+00 | 1.016E+09 | 2.125E+06 | 1.192E+12 |
| 2.776E+17 | 1.377E+13 | 2.559E+01 | 6.621E-05 | 6.621E-07 | 3.286E+01 | 2.337E-01 | 0. | 0. |
| 10.00 | | | | | | | | |
| 6.930E+18 | 1.675E+18 | 2.699E+04 | 7.996E+16 | 4.109E+14 | 2.843E+15 | 0. | 0. | 4.773E+01 |
| 2.957E+01 | 1.704E+03 | 1.780E+09 | 2.726E+07 | 6.386E+11 | 7.382E+14 | 0. | 0. | 0. |
| 2.450E+05 | -1.239E-04 | 4.273E-04 | 4.212E+00 | 2.323E+02 | 1.000E+00 | 1.015E+09 | 2.669E+06 | 1.025E+12 |
| 2.526E+17 | 1.224E+13 | 2.957E+01 | 1.960E-05 | 7.960E-07 | 1.751E-01 | 1.171E-01 | 0. | 0. |
| 11.00 | | | | | | | | |
| 6.115E+18 | 1.634E+18 | 3.986E+04 | 7.055E+16 | 3.626E+14 | 1.353E+15 | 0. | 0. | 4.176E+01 |
| 3.415E+01 | 9.039E+08 | 1.533E+09 | 3.014E+07 | 7.514E+11 | 3.129E+14 | 0. | 0. | 0. |
| 2.457E+05 | -1.442E-04 | 3.770E-04 | 7.776E+00 | 2.271E+02 | 1.000E+00 | 1.019E+06 | 3.294E+06 | 6.224E+11 |
| 2.274E+17 | 1.075E+13 | 3.415E+01 | 9.771E-05 | 9.571E-07 | 9.944E-02 | 6.316E-02 | 0. | 0. |
| 12.00 | | | | | | | | |
| 5.352E+18 | 1.430E+18 | 5.536E+04 | 6.184E+16 | 3.178E+14 | 2.199E+15 | 0. | 0. | 3.654E+01 |
| 3.955E+01 | 7.878E+08 | 1.377E+09 | 4.022E+07 | 9.434E+11 | 1.318E+14 | 0. | 0. | 0. |
| 2.112E+05 | -1.659E-04 | 3.304E-04 | 7.408E+00 | 2.272E+02 | 1.000E+00 | 1.031E+06 | 3.999E+06 | 7.118E+11 |
| 2.020E+17 | 3.281E+12 | 3.945E+01 | 1.151E-04 | 1.151E-06 | 6.076E-02 | 3.690E-02 | 0. | 0. |
| 13.00 | | | | | | | | |
| 4.652E+18 | 1.263E+18 | 7.771E+04 | 5.487E+16 | 2.768E+14 | 1.915E+15 | 0. | 0. | 3.197E+01 |
| 4.582E+01 | 7.119E+08 | 1.289E+09 | 6.509E+07 | 1.191E+12 | 5.515E+13 | 0. | 0. | 0. |
| 1.810E+05 | -1.692E-04 | 2.878E-04 | 7.100E+00 | 2.191E+02 | 1.000E+00 | 1.050E+06 | 4.778E+06 | 5.781E+11 |
| 1.768E+17 | 7.896E+12 | 4.558E+01 | 1.384E-04 | 1.384E-06 | 4.015E-02 | 2.361E-02 | 0. | 0. |
| 14.00 | | | | | | | | |
| 4.045E+18 | 1.094E+18 | 1.104E+05 | 4.667E+16 | 2.958E+14 | 1.659E+15 | 0. | 0. | 2.797E+01 |
| 5.265E+01 | 6.667E+08 | 1.253E+09 | 4.885E+07 | 1.467E+12 | 2.296E+13 | 0. | 0. | 0. |
| 1.548E+05 | -2.140E-04 | 2.494E-04 | 6.847E+00 | 2.183E+02 | 1.000E+00 | 1.078E+06 | 5.625E+06 | 4.635E+11 |
| 1.523E+17 | 6.642E+12 | 5.265E+01 | 1.664E-04 | 1.664E-06 | 2.874E-02 | 1.646E-02 | 0. | 0. |
| 15.00 | | | | | | | | |
| 3.467E+18 | 9.424E+17 | 1.585E+05 | 4.023E+16 | 2.067E+14 | 1.430E+15 | 0. | 0. | 2.447E+01 |
| 6.082E+01 | 6.462E+08 | 1.252E+09 | 1.221E+08 | 1.836E+12 | 1.739E+13 | 0. | 0. | 0. |
| 1.322E+05 | -2.408E-04 | 2.150E-04 | 6.640E+00 | 2.142E+02 | 1.000E+00 | 1.116E+06 | 6.528E+06 | 3.680E+11 |
| 1.291E+17 | 5.541E+12 | 6.082E+01 | 2.000E-04 | 2.000E-06 | 2.229E-02 | 1.251E-02 | 0. | 0. |
| 16.00 | | | | | | | | |
| 2.993E+18 | 6.097E+17 | 2.298E+05 | 3.454E+16 | 1.775E+14 | 1.228E+15 | 0. | 0. | 2.141E+01 |
| 7.076E+01 | 6.465E+08 | 1.303E+09 | 1.677E+08 | 2.242E+12 | 1.354E+13 | 0. | 0. | 0. |
| 1.124E+05 | -2.671E-04 | 1.845E-04 | 6.474E+00 | 2.128E+02 | 1.000E+00 | 1.165E+06 | 7.474E+06 | 2.900E+11 |
| 1.076E+17 | 4.596E+12 | 7.026E+01 | 2.405E-04 | 2.405E-06 | 1.867E-02 | 1.034E-02 | 0. | 0. |
| 17.00 | | | | | | | | |
| 4.561E+18 | 6.927E+17 | 3.362E+05 | 2.955E+16 | 1.516E+14 | 1.050E+15 | 0. | 0. | 1.874E+01 |
| 9.117E+01 | 5.655E+08 | 1.378E+09 | 2.684E+08 | 2.707E+12 | 1.079E+13 | 0. | 0. | 0. |
| 9.696E+04 | -2.997E-04 | 1.579E-04 | 6.142E+00 | 2.120E+02 | 1.000E+00 | 1.274E+06 | 9.448E+06 | 2.291E+11 |
| 8.810E+11 | 3.798E+12 | 8.117E+01 | 2.694E-04 | 2.694E-06 | 1.684E-02 | 9.249E-03 | 0. | 0. |
| 18.00 | | | | | | | | |
| 2.184E+18 | 5.900E+17 | 4.954E+05 | 2.526E+16 | 1.295E+14 | 8.961E+14 | 0. | 0. | 1.639E+01 |
| 9.377E+01 | 7.071E+08 | 1.483E+09 | 3.057E+08 | 3.221E+12 | 9.646E+12 | 0. | 0. | 0. |
| 6.195E+04 | -3.324E-04 | 1.247E-04 | 6.441E+00 | 2.117E+02 | 1.000E+00 | 1.302E+06 | 9.432E+06 | 1.805E+11 |
| 7.140E+11 | 3.133E+12 | 9.377E+01 | 3.477E-04 | 3.477E-06 | 1.622E-02 | 8.893E-03 | 0. | 0. |
| 19.00 | | | | | | | | |
| 1.652E+18 | 4.628E+17 | 7.341E+05 | 2.145E+16 | 1.102E+14 | 7.626E+14 | 0. | 0. | 1.434E+01 |
| 1.043E+04 | 7.581E+08 | 1.616E+09 | 3.198E+08 | 3.761E+12 | 6.010E+12 | 0. | 0. | 0. |
| 6.973E+04 | -3.673E-04 | 1.148E-04 | 6.166E+00 | 2.119E+02 | 1.000E+00 | 1.393E+06 | 1.041E+07 | 1.426E+11 |
| 5.695E+11 | 2.553E+12 | 1.883E+02 | 4.180E-04 | 4.180E-06 | 1.664E-02 | 9.130E-03 | 0. | 0. |
| 20.00 | | | | | | | | |
| 1.579E+18 | 4.473E+17 | 1.094E+06 | 1.224E+16 | 9.365E+13 | 6.480E+14 | 0. | 0. | 1.255E+01 |
| 1.251E+02 | 6.272E+08 | 1.772E+09 | 5.089E+08 | 4.245E+12 | 7.130E+12 | 0. | 0. | 0. |

| | | | | | | | | | | | |
|-------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 21.00 | 3.54E+04 | -4.05E-34 | 7.737E-05 | 6.114E+00 | 4.125E+02 | 4.125E+02 | 1.000E+00 | 1.000E+00 | 1.502E+06 | 1.135E+07 | 1.135E+11 |
| | 4.49E+01 | 2.13E-12 | 1.251E+02 | 5.026E-04 | 5.026E-06 | 1.000E+00 | 1.163E+00 | 9.937E-03 | 0. | 0. | 0. |
| | 1.340E+18 | 3.62E+17 | 1.628E+06 | 6.297E+16 | 7.948E+13 | 5.49E+14 | 0. | 0. | 0. | 0. | 1.098E+01 |
| | 4.46E+02 | 9.15E+08 | 1.944E+09 | 6.297E+06 | 4.716E+12 | 2.246E+12 | 0. | 0. | 0. | 0. | 0. |
| | 3.067E+04 | -4.45E-04 | 8.264E-05 | 6.083E+00 | 2.135E+02 | 6.13E+02 | 1.000E+00 | 1.631E+06 | 1.226E+07 | 1.226E+07 | 9.05E+10 |
| | 3.500E+11 | 1.762E+12 | 1.446E+02 | 6.944E-04 | 6.044E-06 | 1.001E+00 | 9.024E-01 | 1.138E-02 | 0. | 0. | 0. |
| 22.00 | 1.137E+18 | 3.07E+17 | 2.428E+06 | 1.112E+16 | 6.742E+13 | 4.665E+14 | 0. | 0. | 0. | 0. | 9.008E+00 |
| | 1.070E+02 | 1.020E+09 | 7.589E+08 | 7.589E+08 | 4.945E+12 | 5.414E+12 | 0. | 0. | 0. | 0. | 0. |
| | 4.324E+04 | -4.80E-04 | 7.010E-05 | 6.068E+00 | 2.149E+02 | 2.149E+02 | 1.000E+00 | 1.781E+06 | 1.310E+07 | 1.310E+07 | 7.301E+10 |
| | 2.705E+11 | 1.466E+12 | 1.678E+02 | 7.267E-04 | 7.267E-06 | 2.196E+00 | 2.408E-02 | 1.380E-02 | 0. | 0. | 0. |
| 23.00 | 9.643E+17 | 2.608E+17 | 3.616E+06 | 1.113E+16 | 5.718E+13 | 3.956E+14 | 0. | 0. | 0. | 0. | 8.406E+00 |
| | 1.929E+02 | 1.139E+09 | 2.303E+09 | 8.950E+08 | 4.985E+12 | 4.672E+12 | 0. | 0. | 0. | 0. | 0. |
| | 3.695E+04 | -5.33E-04 | 5.945E-05 | 6.071E+00 | 2.165E+02 | 2.165E+02 | 1.000E+00 | 1.958E+06 | 1.386E+07 | 1.386E+07 | 5.936E+10 |
| | 2.075E+11 | 1.213E+12 | 1.929E+02 | 8.736E-04 | 8.736E-06 | 4.045E+00 | 2.938E-02 | 1.685E-02 | 0. | 0. | 0. |
| 24.00 | 6.190E+17 | 2.213E+17 | 5.371E+06 | 9.438E+15 | 4.850E+13 | 3.356E+14 | 0. | 0. | 0. | 0. | 7.355E+00 |
| | 2.279E+02 | 1.271E+09 | 2.468E+09 | 1.339E+09 | 4.959E+12 | 4.026E+12 | 0. | 0. | 0. | 0. | 0. |
| | 3.161E+04 | -5.820E-04 | 5.043E-05 | 6.086E+00 | 2.184E+02 | 2.184E+02 | 1.000E+00 | 2.162E+06 | 1.452E+07 | 1.452E+07 | 4.672E+10 |
| | 1.581E+11 | 1.010E+12 | 2.279E+02 | 1.051E-03 | 1.051E-05 | 6.888E+00 | 3.679E-02 | 2.148E-02 | 0. | 0. | 0. |
| 25.00 | 9.943E+17 | 1.078E+17 | 7.943E+06 | 8.011E+15 | 4.117E+13 | 2.848E+14 | 0. | 0. | 0. | 0. | 6.435E+00 |
| | 2.575E+02 | 1.410E+09 | 2.597E+09 | 1.194E+09 | 4.825E+12 | 3.467E+12 | 0. | 0. | 0. | 0. | 0. |
| | 2.709E+04 | -6.134E-04 | 4.280E-05 | 6.114E+00 | 2.204E+02 | 2.204E+02 | 1.000E+00 | 2.398E+06 | 1.509E+07 | 1.509E+07 | 4.637E+10 |
| | 1.198E+11 | 8.439E+11 | 2.575E+02 | 1.263E-03 | 1.263E-05 | 1.100E+01 | 4.701E-02 | 2.801E-02 | 0. | 0. | 0. |
| 26.00 | 5.094E+17 | 1.595E+17 | 1.166E+07 | 6.005E+15 | 3.497E+13 | 2.420E+14 | 0. | 0. | 0. | 0. | 5.631E+00 |
| | 2.975E+02 | 1.552E+09 | 2.683E+09 | 1.383E+09 | 4.560E+12 | 2.986E+12 | 0. | 0. | 0. | 0. | 0. |
| | 2.325E+04 | -6.077E-04 | 3.636E-05 | 6.152E+00 | 2.277E+02 | 2.277E+02 | 1.000E+00 | 2.667E+06 | 1.554E+07 | 1.554E+07 | 3.376E+10 |
| | 9.033E+10 | 7.064E+11 | 2.975E+02 | 1.519E-03 | 1.519E-05 | 1.665E+01 | 6.095E-02 | 3.710E-02 | 0. | 0. | 0. |
| 27.00 | 5.016E+17 | 1.357E+17 | 1.707E+07 | 5.788E+15 | 2.974E+13 | 2.058E+14 | 0. | 0. | 0. | 0. | 4.927E+00 |
| | 3.437E+02 | 1.690E+09 | 2.712E+09 | 1.608E+09 | 4.195E+12 | 2.572E+12 | 0. | 0. | 0. | 0. | 0. |
| | 1.988E+04 | -7.451E-04 | 3.091E-05 | 6.199E+00 | 2.251E+02 | 2.251E+02 | 1.000E+00 | 2.972E+06 | 1.588E+07 | 1.588E+07 | 2.849E+10 |
| | 6.770E+10 | 5.925E+11 | 3.437E+02 | 1.827E-03 | 1.827E-05 | 2.411E+01 | 1.002E-01 | 4.969E-02 | 0. | 0. | 0. |
| 28.00 | 6.272E+17 | 1.156E+17 | 2.476E+07 | 4.924E+15 | 2.533E+13 | 1.753E+14 | 0. | 0. | 0. | 0. | 4.311E+00 |
| | 3.971E+02 | 1.816E+09 | 2.677E+09 | 1.897E+09 | 3.775E+12 | 2.216E+12 | 0. | 0. | 0. | 0. | 0. |
| | 1.720E+04 | -8.052E-04 | 2.634E-05 | 6.254E+00 | 2.275E+02 | 2.275E+02 | 1.000E+00 | 3.116E+06 | 1.611E+07 | 1.611E+07 | 2.925E+10 |
| | 5.049E+10 | 4.977E+11 | 3.971E+02 | 2.196E-05 | 2.196E-05 | 3.361E+01 | 1.049E-01 | 6.694E-02 | 0. | 0. | 0. |
| 29.00 | 3.643E+17 | 9.856E+16 | 3.563E+07 | 4.204E+15 | 2.160E+13 | 1.495E+14 | 0. | 0. | 0. | 0. | 3.772E+00 |
| | 4.587E+02 | 1.923E+09 | 2.577E+09 | 2.479E+09 | 3.141E+12 | 1.911E+12 | 0. | 0. | 0. | 0. | 0. |
| | 1.484E+04 | -8.689E-04 | 2.246E-05 | 6.317E+00 | 2.301E+02 | 2.301E+02 | 1.424E+00 | 3.700E+06 | 1.622E+07 | 1.622E+07 | 2.608E+10 |
| | 3.732E+10 | 4.184E+11 | 4.507E+02 | 2.641E-03 | 2.641E-05 | 4.535E+01 | 1.301E-01 | 9.036E-02 | 0. | 0. | 0. |
| 30.00 | 3.113E+17 | 8.420E+16 | 5.079E+07 | 3.591E+15 | 1.846E+13 | 1.277E+14 | 0. | 0. | 0. | 0. | 3.208E+00 |
| | 5.300E+02 | 2.005E+09 | 2.416E+09 | 2.790E+09 | 2.921E+12 | 1.649E+12 | 0. | 0. | 0. | 0. | 0. |
| | 1.282E+04 | -9.354E-04 | 1.919E-05 | 6.384E+00 | 2.327E+02 | 2.327E+02 | 2.900E+00 | 4.125E+06 | 1.622E+07 | 1.622E+07 | 1.707E+10 |
| | 2.742E+10 | 3.516E+11 | 5.400E+02 | 3.176E-03 | 3.176E-05 | 5.954E+01 | 1.814E-01 | 1.216E-01 | 0. | 0. | 0. |
| 31.00 | 2.664E+17 | 7.205E+16 | 7.177E+07 | 3.073E+15 | 1.579E+13 | 1.093E+14 | 0. | 0. | 0. | 0. | 2.887E+00 |
| | 6.123E+02 | 2.056E+09 | 2.205E+09 | 3.477E+09 | 2.531E+12 | 1.425E+12 | 0. | 0. | 0. | 0. | 0. |
| | 1.109E+04 | -1.005E-03 | 1.642E-05 | 6.457E+00 | 2.353E+02 | 2.353E+02 | 5.887E+00 | 4.500E+06 | 1.611E+07 | 1.611E+07 | 1.561E+10 |
| | 1.999E+10 | 2.954E+11 | 6.124E+02 | 3.819E-03 | 3.819E-05 | 7.628E+01 | 2.374E-01 | 1.634E-01 | 0. | 0. | 0. |
| 32.00 | 2.283E+17 | 6.177E+16 | 1.004E+08 | 2.635E+15 | 1.454E+13 | 9.486E+13 | 0. | 0. | 0. | 0. | 2.526E+00 |
| | 7.074E+02 | 2.074E+09 | 1.959E+09 | 4.389E+09 | 2.180E+12 | 1.232E+12 | 0. | 0. | 0. | 0. | 0. |

| | | | | | | | | | | | |
|-------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 32.00 | 2.610E+03 | -1.077E+03 | 1.400E+05 | 0.011E+00 | 2.379E+02 | 2.379E+02 | 2.379E+02 | 1.175E+01 | 5.094E+06 | 1.591E+07 | 1.360E+10 |
| | 1.447E+10 | 2.477E+11 | 7.074E+02 | 4.592E-03 | 4.592E-05 | 4.592E-05 | 4.592E-05 | 1.081E-01 | 2.177E-01 | 0. | 0. |
| | 1.961E+17 | 2.055E+16 | 1.492E+04 | 2.603E+15 | 1.163E+13 | 1.163E+13 | 1.163E+13 | 0. | 0. | 0. | 2.210E+00 |
| | 8.173E+02 | 2.057E+03 | 1.895E+04 | 5.575E+04 | 1.570E+12 | 1.570E+12 | 1.570E+12 | 0. | 0. | 0. | 0. |
| | 8.349E+03 | -1.152E+03 | 1.209E-05 | 0.611E+00 | 2.405E+02 | 2.405E+02 | 2.405E+02 | 2.420E+01 | 2.632E+06 | 1.563E+07 | 1.197E+10 |
| | 1.040E+10 | 2.072E+11 | 0.173E+02 | 5.522E-03 | 5.522E-05 | 5.522E-05 | 5.522E-05 | 1.969E-01 | 2.877E-01 | 0. | 0. |
| 34.00 | 1.097E+17 | 4.505E+16 | 1.910E+09 | 1.977E+15 | 1.001E+13 | 1.001E+13 | 1.001E+13 | 0. | 0. | 0. | 1.934E+00 |
| | 4.443E+02 | 2.012E+09 | 1.430E+09 | 7.063E+09 | 1.593E+12 | 1.593E+12 | 1.593E+12 | 0. | 0. | 0. | 0. |
| | 7.460E+03 | -1.211E+03 | 1.040E-05 | 0.091E+00 | 2.431E+02 | 2.431E+02 | 2.431E+02 | 4.976E+01 | 1.199E+06 | 1.527E+07 | 1.054E+10 |
| | 7.425E+09 | 1.729E+11 | 9.443E+02 | 0.040E-03 | 0.040E-05 | 0.040E-05 | 0.040E-05 | 5.063E-01 | 3.764E-01 | 0. | 0. |
| 35.00 | 1.454E+17 | 5.234E+16 | 2.594E+08 | 1.078E+15 | 8.024E+12 | 8.024E+12 | 8.024E+12 | 0. | 0. | 0. | 1.692E+00 |
| | 1.001E+03 | 1.573E+09 | 1.176E+03 | 0.743E+04 | 1.364E+12 | 1.364E+12 | 1.364E+12 | 0. | 0. | 0. | 0. |
| | 0.172E+03 | -1.312E-03 | 8.967E-06 | 0.773E+00 | 2.456E+02 | 2.456E+02 | 2.456E+02 | 1.000E+02 | 6.787E+06 | 1.484E+07 | 9.305E+09 |
| | 5.273E+09 | 1.417E+11 | 1.091E+03 | 7.855E-03 | 7.855E-05 | 7.855E-05 | 7.855E-05 | 6.393E-01 | 4.872E-01 | 0. | 0. |
| 36.00 | 1.250E+17 | 3.497E+16 | 3.489E+04 | 1.447E+15 | 7.447E+12 | 7.447E+12 | 7.447E+12 | 0. | 0. | 0. | 1.481E+00 |
| | 1.250E+03 | 1.841E+09 | 9.449E+08 | 1.084E+10 | 1.161E+12 | 1.161E+12 | 1.161E+12 | 0. | 0. | 0. | 0. |
| | 5.513E+03 | -1.595E-03 | 7.743E-06 | 0.435E+00 | 2.480E+02 | 2.480E+02 | 2.480E+02 | 3.314E+02 | 2.384E+06 | 1.436E+07 | 8.236E+09 |
| | 3.726E+09 | 1.189E+11 | 1.260E+03 | 9.002E-03 | 9.002E-05 | 9.002E-05 | 9.002E-05 | 7.985E-01 | 6.233E-01 | 0. | 0. |
| 37.00 | 1.090E+17 | 4.314E+16 | 4.647E+08 | 1.454E+15 | 6.447E+12 | 6.447E+12 | 6.447E+12 | 0. | 0. | 0. | 1.495E+00 |
| | 1.450E+03 | 1.728E+09 | 7.428E+08 | 1.293E+10 | 9.857E+11 | 9.857E+11 | 9.857E+11 | 0. | 0. | 0. | 0. |
| | 4.015E+03 | -1.481E-03 | 0.898E-06 | 0.148E+00 | 2.504E+02 | 2.504E+02 | 2.504E+02 | 1.099E+03 | 7.980E+06 | 1.384E+07 | 7.384E+09 |
| | 2.621E+09 | 9.792E+10 | 1.456E+03 | 1.155E-02 | 1.155E-04 | 1.155E-04 | 1.155E-04 | 9.861E-01 | 7.879E-01 | 0. | 0. |
| 38.00 | 9.414E+16 | 2.547E+16 | 0.127E+08 | 1.080E+15 | 5.582E+12 | 5.582E+12 | 5.582E+12 | 0. | 0. | 0. | 1.133E+00 |
| | 1.643E+03 | 1.606E+09 | 5.723E+08 | 1.494E+10 | 8.351E+11 | 8.351E+11 | 8.351E+11 | 0. | 0. | 0. | 0. |
| | 4.210E+03 | -1.570E-03 | 5.004E-06 | 7.019E+00 | 2.527E+02 | 2.527E+02 | 2.527E+02 | 3.641E+03 | 8.560E+06 | 1.328E+07 | 6.480E+09 |
| | 1.876E+09 | 0.019E+10 | 1.083E+03 | 1.388E-02 | 1.388E-04 | 1.388E-04 | 1.388E-04 | 1.204E+00 | 9.039E-01 | 0. | 0. |
| 39.00 | 0.170E+16 | 2.210E+16 | 7.999E+08 | 9.427E+14 | 4.645E+12 | 4.645E+12 | 4.645E+12 | 0. | 0. | 0. | 9.910E-01 |
| | 1.944E+03 | 1.479E+09 | 4.311E+08 | 1.068E+10 | 7.057E+11 | 7.057E+11 | 7.057E+11 | 0. | 0. | 0. | 0. |
| | 3.646E+03 | -1.062E-03 | 5.037E-06 | 7.101E+00 | 2.539E+02 | 2.539E+02 | 2.539E+02 | 1.207E+04 | 9.102E+06 | 1.271E+07 | 5.140E+09 |
| | 1.200E+09 | 6.510E+10 | 1.944E+03 | 1.670E-02 | 1.670E-04 | 1.670E-04 | 1.670E-04 | 1.453E+00 | 1.214E+00 | 0. | 0. |
| 40.00 | 7.103E+16 | 1.921E+16 | 1.034E+09 | 0.196E+14 | 4.212E+12 | 4.212E+12 | 4.212E+12 | 0. | 0. | 0. | 8.677E-01 |
| | 2.246E+03 | 1.352E+09 | 3.225E+08 | 1.011E+10 | 5.944E+11 | 5.944E+11 | 5.944E+11 | 0. | 0. | 0. | 0. |
| | 3.210E+03 | -1.768E-03 | 4.379E-06 | 7.181E+00 | 2.570E+02 | 2.570E+02 | 2.570E+02 | 4.000E+04 | 9.610E+06 | 1.212E+07 | 5.140E+09 |
| | 0.891E+08 | 5.285E+10 | 2.246E+03 | 2.008E-02 | 2.008E-04 | 2.008E-04 | 2.008E-04 | 1.734E+00 | 1.470E+00 | 0. | 0. |
| 41.00 | 6.184E+16 | 1.674E+16 | 1.425E+09 | 7.136E+14 | 3.667E+12 | 3.667E+12 | 3.667E+12 | 0. | 0. | 0. | 7.592E-01 |
| | 2.522E+03 | 1.210E+09 | 2.369E+08 | 1.928E+10 | 4.990E+11 | 4.990E+11 | 4.990E+11 | 0. | 0. | 0. | 0. |
| | 2.835E+03 | -1.852E-03 | 3.813E-06 | 7.261E+00 | 2.590E+02 | 2.590E+02 | 2.590E+02 | 4.731E+04 | 1.005E+07 | 1.152E+07 | 4.585E+09 |
| | 0.150E+08 | 4.250E+10 | 2.593E+03 | 2.415E-02 | 2.415E-04 | 2.415E-04 | 2.415E-04 | 2.044E+00 | 1.770E+00 | 0. | 0. |
| 42.00 | 5.395E+16 | 1.459E+16 | 1.681E+09 | 6.224E+14 | 3.198E+12 | 3.198E+12 | 3.198E+12 | 0. | 0. | 0. | 6.643E-01 |
| | 2.999E+03 | 1.114E+09 | 1.720E+08 | 2.940E+10 | 4.171E+11 | 4.171E+11 | 4.171E+11 | 0. | 0. | 0. | 0. |
| | 4.490E+03 | -1.950E-03 | 4.325E-06 | 7.140E+00 | 2.608E+02 | 2.608E+02 | 2.608E+02 | 5.595E+04 | 1.042E+07 | 1.092E+07 | 4.972E+09 |
| | 4.237E+08 | 3.339E+10 | 2.599E+03 | 4.704E-02 | 2.704E-04 | 2.704E-04 | 2.704E-04 | 4.595E-04 | 2.110E+00 | 0. | 0. |
| 43.00 | 4.709E+16 | 1.274E+16 | 2.112E+09 | 5.434E+14 | 2.792E+12 | 2.792E+12 | 2.792E+12 | 0. | 0. | 0. | 5.812E-01 |
| | 2.465E+03 | 1.005E+09 | 1.237E+08 | 2.177E+10 | 3.471E+11 | 3.471E+11 | 3.471E+11 | 0. | 0. | 0. | 0. |
| | 2.192E+03 | -2.050E-03 | 2.903E-06 | 7.418E+00 | 2.676E+02 | 2.676E+02 | 2.676E+02 | 6.617E+04 | 1.069E+07 | 1.032E+07 | 3.669E+09 |
| | 2.909E+08 | 2.698E+10 | 3.405E+03 | 3.492E-02 | 3.492E-04 | 3.492E-04 | 3.492E-04 | 2.743E+00 | 2.472E+00 | 0. | 0. |
| 44.00 | 4.118E+16 | 1.114E+16 | 2.030E+09 | 4.752E+14 | 2.444E+12 | 2.444E+12 | 2.444E+12 | 0. | 0. | 0. | 5.086E-01 |
| | 4.003E+03 | 9.056E+08 | 6.036E+07 | 2.361E+10 | 2.874E+11 | 2.874E+11 | 2.874E+11 | 0. | 0. | 0. | 0. |

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|-------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 45.00 | 1.570E+03 | -2.153E+01 | 2.539E+00 | 7.590E+00 | 4.200E-04 | 2.642E+02 | 7.826E+04 | 1.080E+07 | 9.735E+06 | 1.494E+09 |
| | 1.570E+03 | 4.130E+10 | 4.003E+03 | 4.200E-04 | 4.200E-04 | 5.378E+02 | 3.120E+00 | 2.857E+00 | 0. | 0. |
| | 3.606E+16 | 9.755E+15 | 3.244E+04 | 4.161E+14 | 2.118E+12 | 1.480E+13 | 0. | 0. | 0. | 4.450E-01 |
| | 4.676E+16 | 8.152E+08 | 6.280E+07 | 2.696E+10 | 2.367E+11 | 2.017E+11 | 0. | 0. | 0. | 0. |
| | 1.606E+03 | -2.257E-03 | 2.223E-06 | 7.773E+00 | 2.657E+02 | 2.657E+02 | 9.256E+04 | 1.096E+07 | 9.154E+06 | 2.967E+09 |
| | 1.358E+08 | 1.672E+10 | 4.626E+03 | 5.050E-02 | 5.050E-04 | 5.900E+02 | 3.507E+00 | 3.254E+00 | 0. | 0. |
| 46.00 | 3.164E+16 | 4.554E+15 | 3.964E+04 | 3.448E+14 | 1.875E+12 | 1.297E+13 | 0. | 0. | 0. | 1.893E-01 |
| | 5.345E+03 | 7.337E+04 | 4.450E+07 | 3.163E+10 | 1.937E+11 | 1.754E+11 | 0. | 0. | 0. | 0. |
| | 1.495E+03 | -2.362E-03 | 1.950E-06 | 7.150E+00 | 2.670E+02 | 2.670E+02 | 1.095E+05 | 1.094E+07 | 8.596E+06 | 2.683E+09 |
| | 9.249E+07 | 1.305E+10 | 3.945E+03 | 6.074E-04 | 6.074E-04 | 6.441E+02 | 3.876E+00 | 3.650E+00 | 0. | 0. |
| 47.00 | 2.777E+16 | 7.511E+15 | 4.800E+09 | 3.204E+14 | 1.946E+12 | 1.139E+13 | 0. | 0. | 0. | 1.407E-01 |
| | 6.176E+03 | 6.604E+08 | 3.151E+07 | 3.771E+10 | 1.576E+11 | 1.533E+11 | 0. | 0. | 0. | 0. |
| | 1.318E+03 | -2.468E-03 | 1.713E-06 | 7.726E+00 | 2.682E+02 | 2.682E+02 | 1.495E+05 | 1.082E+07 | 8.048E+06 | 2.437E+09 |
| | 6.269E+07 | 1.014E+10 | 6.176E+03 | 7.304E-04 | 7.304E-04 | 7.000E+02 | 4.232E+00 | 4.028E+00 | 0. | 0. |
| 48.00 | 2.441E+16 | 6.805E+15 | 3.759E+03 | 2.617E+14 | 1.447E+12 | 1.001E+13 | 0. | 0. | 0. | 2.981E-01 |
| | 7.118E+03 | 5.947E+08 | 2.234E+07 | 4.357E+10 | 1.274E+11 | 1.336E+11 | 0. | 0. | 0. | 0. |
| | 1.163E+03 | -2.575E-03 | 1.503E-06 | 7.803E+00 | 2.691E+02 | 2.691E+02 | 1.531E+05 | 1.061E+07 | 7.515E+06 | 2.226E+09 |
| | 4.234E+07 | 7.845E+09 | 7.136E+03 | 8.785E-04 | 8.785E-04 | 6.781E+02 | 4.546E+00 | 4.368E+00 | 0. | 0. |
| 49.00 | 2.149E+16 | 5.613E+15 | 6.846E+03 | 2.473E+14 | 1.274E+12 | 8.816E+12 | 0. | 0. | 0. | 2.608E-01 |
| | 8.246E+03 | 5.357E+08 | 1.588E+07 | 4.463E+10 | 1.623E+11 | 1.644E+11 | 0. | 0. | 0. | 0. |
| | 1.026E+03 | -2.662E-03 | 1.325E-06 | 7.879E+00 | 2.699E+02 | 2.699E+02 | 1.811E+05 | 1.032E+07 | 6.998E+06 | 2.046E+09 |
| | 2.852E+07 | 6.045E+09 | 8.245E+03 | 1.056E-01 | 1.056E-03 | 6.559E+02 | 4.802E+00 | 4.647E+00 | 0. | 0. |
| 50.00 | 1.894E+16 | 5.124E+15 | 8.063E+03 | 2.185E+14 | 1.123E+12 | 7.769E+12 | 0. | 0. | 0. | 2.282E-01 |
| | 9.526E+03 | 4.026E+04 | 1.134E+07 | 3.500E+10 | 8.160E+10 | 1.014E+11 | 0. | 0. | 0. | 0. |
| | 9.054E+02 | -2.780E-03 | 1.168E-06 | 7.955E+00 | 2.704E+02 | 2.704E+02 | 2.122E+05 | 9.957E+06 | 6.498E+06 | 1.894E+09 |
| | 1.933E+07 | 4.643E+09 | 9.528E+03 | 1.271E-01 | 1.271E-03 | 6.334E+02 | 4.981E+00 | 4.843E+00 | 0. | 0. |
| 51.00 | 1.671E+16 | 4.520E+15 | 9.409E+09 | 1.928E+14 | 9.909E+11 | 6.858E+12 | 0. | 0. | 0. | 1.996E-01 |
| | 1.101E+04 | 4.346E+08 | 8.145E+06 | 3.177E+10 | 6.469E+10 | 8.825E+10 | 0. | 0. | 0. | 0. |
| | 9.004E+02 | -2.896E-03 | 1.030E-06 | 8.029E+00 | 2.706E+02 | 2.706E+02 | 2.533E+05 | 9.534E+06 | 6.008E+06 | 1.767E+09 |
| | 1.454E+07 | 3.554E+09 | 1.101E+04 | 1.528E-01 | 1.528E-03 | 6.106E+02 | 5.066E+00 | 4.936E+00 | 0. | 0. |
| 52.00 | 1.476E+16 | 3.993E+15 | 1.088E+10 | 1.703E+14 | 8.753E+11 | 6.056E+12 | 0. | 0. | 0. | 1.747E-01 |
| | 1.272E+04 | 3.911E+08 | 5.893E+06 | 2.683E+10 | 5.097E+10 | 7.677E+10 | 0. | 0. | 0. | 0. |
| | 7.065E+02 | -3.001E-03 | 9.101E-07 | 8.102E+00 | 2.705E+02 | 2.705E+02 | 2.996E+05 | 9.067E+06 | 5.535E+06 | 1.662E+09 |
| | 6.076E+06 | 2.722E+09 | 1.272E+04 | 1.838E-01 | 1.838E-03 | 5.875E+02 | 5.042E+00 | 4.911E+00 | 0. | 0. |
| 53.00 | 1.305E+16 | 3.531E+15 | 1.248E+10 | 1.505E+14 | 7.741E+11 | 5.356E+12 | 0. | 0. | 0. | 1.528E-01 |
| | 1.470E+04 | 3.513E+08 | 4.308E+06 | 2.617E+10 | 3.993E+10 | 6.744E+10 | 0. | 0. | 0. | 0. |
| | 2.243E+02 | -3.104E-03 | 8.049E-07 | 8.171E+00 | 2.702E+02 | 2.702E+02 | 3.543E+05 | 8.571E+06 | 5.075E+06 | 1.578E+09 |
| | 5.072E+06 | 2.686E+09 | 1.470E+04 | 2.210E-01 | 2.210E-03 | 5.641E+02 | 4.905E+00 | 4.760E+00 | 0. | 0. |
| 54.00 | 1.156E+16 | 3.126E+15 | 1.415E+10 | 1.333E+14 | 6.853E+11 | 4.741E+12 | 0. | 0. | 0. | 1.337E-01 |
| | 1.694E+04 | 3.146E+08 | 4.166E+06 | 2.375E+10 | 3.111E+10 | 5.796E+10 | 0. | 0. | 0. | 0. |
| | 5.212E+02 | -3.205E-03 | 7.125E-07 | 6.437E+00 | 2.695E+02 | 2.695E+02 | 4.191E+05 | 8.056E+06 | 4.627E+06 | 1.512E+09 |
| | 3.039E+06 | 1.589E+09 | 1.699E+04 | 2.658E-01 | 2.658E-03 | 5.404E+02 | 4.634E-05 | 4.686E+00 | 0. | 0. |
| 55.00 | 1.024E+16 | 2.770E+15 | 1.592E+10 | 1.194E+14 | 6.972E+11 | 4.201E+12 | 0. | 0. | 0. | 1.170E-01 |
| | 1.693E+04 | 2.811E+08 | 2.355E+06 | 2.155E+10 | 2.455E+10 | 5.033E+10 | 0. | 0. | 0. | 0. |
| | 4.895E+02 | -3.303E-03 | 6.315E-07 | 4.296E+00 | 2.684E+02 | 2.684E+02 | 4.968E+05 | 7.540E+06 | 4.192E+06 | 1.464E+09 |
| | 1.703E+06 | 1.215E+09 | 1.963E+04 | 3.197E-01 | 3.197E-03 | 5.105E+02 | 4.301E+00 | 4.103E+00 | 0. | 0. |
| 56.00 | 9.041E+15 | 2.457E+15 | 1.776E+10 | 1.046E+14 | 5.345E+11 | 3.766E+12 | 0. | 0. | 0. | 1.024E-01 |
| | 2.268E+04 | 2.500E+08 | 1.770E+06 | 1.756E+10 | 2.110E+10 | 4.465E+10 | 0. | 0. | 0. | 0. |

| | | | | | | | | | | |
|-------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 57.00 | 4.292E+04 | -3.337E-04 | 5.599E-07 | 9.551E+00 | 2.670E+02 | 2.670E+02 | 5.862E+05 | 7.039E+06 | 3.770E+06 | 1.432E+09 |
| | 1.515E+06 | 9.292E+08 | 2.268E+04 | 3.046E-01 | 3.846E-03 | 4.923E+02 | 3.865E+00 | 3.636E+00 | 0. | 0. |
| | 8.05E+15 | 2.180E+15 | 1.964E+10 | 9.299E+13 | 4.772E+11 | 3.008E+12 | 0. | 0. | 0. | 4.958E-02 |
| | 2.621E+04 | 2.413E+08 | 1.440E+06 | 1.752E+10 | 1.727E+10 | 3.784E+10 | 0. | 0. | 0. | 0. |
| | 3.783E+02 | -3.487E-03 | 4.969E-07 | 8.995E+00 | 2.652E+02 | 2.652E+02 | 6.913E+05 | 6.532E+06 | 3.860E+06 | 1.415E+09 |
| | 1.344E+06 | 7.120E+06 | 2.621E+04 | 4.625E-01 | 4.625E-03 | 4.679E+02 | 3.371E+00 | 3.117E+00 | 0. | 0. |
| 58.00 | 7.156E+15 | 1.936E+15 | 2.153E+10 | 8.275E+13 | 4.243E+11 | 2.936E+12 | 0. | 0. | 0. | 7.837E-02 |
| | 3.076E+04 | 1.947E+08 | 1.074E+06 | 1.611E+10 | 1.371E+10 | 3.273E+10 | 0. | 0. | 0. | 0. |
| | 3.332E+02 | -3.572E-03 | 4.812E-07 | 6.428E+00 | 2.631E+02 | 2.631E+02 | 8.199E+05 | 6.057E+06 | 2.965E+06 | 1.414E+09 |
| | 1.193E+06 | 5.667E+08 | 3.029E+04 | 5.563E-01 | 5.563E-03 | 4.434E+02 | 2.850E+00 | 2.580E+00 | 0. | 0. |
| 59.00 | 6.356E+15 | 1.719E+15 | 2.342E+10 | 7.334E+13 | 4.769E+11 | 2.608E+12 | 0. | 0. | 0. | 6.857E-02 |
| | 4.046E+04 | 1.704E+08 | 8.043E+05 | 1.192E+10 | 1.071E+10 | 2.829E+10 | 0. | 0. | 0. | 0. |
| | 2.972E+02 | -3.652E-03 | 3.819E-07 | 8.447E+00 | 2.605E+02 | 2.605E+02 | 9.897E+05 | 5.608E+06 | 2.585E+06 | 1.427E+09 |
| | 1.660E+06 | 4.208E+08 | 3.501E+04 | 6.922E-01 | 6.922E-03 | 4.187E+02 | 2.332E+00 | 2.061E+00 | 0. | 0. |
| 60.00 | 5.647E+15 | 1.528E+15 | 2.528E+10 | 6.515E+13 | 3.348E+11 | 2.317E+12 | 0. | 0. | 0. | 6.000E-02 |
| | 4.046E+04 | 1.478E+08 | 6.375E+05 | 1.377E+10 | 8.299E+09 | 2.442E+10 | 0. | 0. | 0. | 0. |
| | 2.578E+02 | -3.726E-03 | 3.993E-07 | 8.452E+00 | 2.577E+02 | 2.577E+02 | 1.147E+06 | 5.189E+06 | 2.224E+06 | 1.455E+09 |
| | 9.418E+05 | 3.447E+08 | 4.046E+04 | 8.049E-01 | 8.049E-03 | 3.938E+02 | 1.866E+00 | 1.586E+00 | 0. | 0. |
| 61.00 | 5.016E+15 | 1.357E+15 | 2.709E+10 | 5.786E+13 | 2.974E+11 | 2.058E+12 | 0. | 0. | 0. | 7.601E-02 |
| | 4.675E+04 | 1.273E+08 | 5.031E+05 | 1.295E+10 | 6.429E+09 | 2.106E+10 | 0. | 0. | 0. | 0. |
| | 2.260E+02 | -3.794E-03 | 3.993E-07 | 8.439E+00 | 2.545E+02 | 2.545E+02 | 1.356E+06 | 4.601E+06 | 1.803E+06 | 1.497E+09 |
| | 8.364E+05 | 2.514E+08 | 4.675E+04 | 9.681E-01 | 9.681E-03 | 3.690E+02 | 1.412E+00 | 1.176E+00 | 0. | 0. |
| 62.00 | 4.455E+15 | 1.205E+15 | 2.884E+10 | 5.140E+13 | 2.641E+11 | 1.828E+12 | 0. | 0. | 0. | 2.024E-01 |
| | 5.403E+04 | 1.089E+08 | 4.045E+05 | 1.093E+10 | 4.968E+09 | 1.813E+10 | 0. | 0. | 0. | 0. |
| | 1.730E+02 | -3.912E-03 | 3.912E-07 | 8.407E+00 | 2.510E+02 | 2.510E+02 | 1.604E+06 | 4.444E+06 | 1.566E+06 | 1.555E+09 |
| | 7.427E+05 | 1.952E+08 | 5.407E+04 | 1.164E+00 | 1.164E-02 | 3.441E+02 | 1.044E+00 | 8.395E-01 | 0. | 0. |
| 63.00 | 3.954E+15 | 1.070E+15 | 3.051E+10 | 4.567E+13 | 2.344E+11 | 1.622E+12 | 0. | 0. | 0. | 1.319E-01 |
| | 6.244E+04 | 9.250E+07 | 3.287E+05 | 9.973E+09 | 3.901E+09 | 1.558E+10 | 0. | 0. | 0. | 0. |
| | 1.510E+02 | -3.961E-03 | 2.438E-07 | 8.356E+00 | 2.472E+02 | 2.472E+02 | 1.897E+06 | 4.119E+06 | 1.278E+06 | 1.628E+09 |
| | 6.592E+05 | 1.521E+08 | 6.244E+04 | 1.401E+00 | 1.401E-02 | 3.192E+02 | 7.454E-01 | 5.775E-01 | 0. | 0. |
| 64.00 | 3.506E+15 | 9.484E+14 | 3.210E+10 | 4.046E+13 | 2.079E+11 | 1.438E+12 | 0. | 0. | 0. | 1.714E-01 |
| | 7.217E+04 | 7.799E+07 | 2.697E+05 | 9.006E+09 | 3.058E+09 | 1.336E+10 | 0. | 0. | 0. | 0. |
| | 1.510E+02 | -3.961E-03 | 2.162E-07 | 8.284E+00 | 2.432E+02 | 2.432E+02 | 2.244E+06 | 3.822E+06 | 1.015E+06 | 1.717E+09 |
| | 5.845E+05 | 1.188E+08 | 7.216E+04 | 1.685E+00 | 1.685E-02 | 2.945E+02 | 5.144E-01 | 3.831E-01 | 0. | 0. |
| 65.00 | 3.105E+15 | 8.401E+14 | 3.362E+10 | 3.563E+13 | 1.841E+11 | 1.274E+12 | 0. | 0. | 0. | 2.229E-01 |
| | 8.340E+04 | 6.517E+07 | 2.235E+05 | 4.174E+09 | 2.402E+09 | 1.144E+10 | 0. | 0. | 0. | 0. |
| | 1.314E+02 | -4.006E-03 | 1.915E-07 | 8.192E+00 | 2.390E+02 | 2.390E+02 | 4.854E+06 | 3.553E+06 | 7.870E+05 | 1.822E+09 |
| | 5.177E+05 | 9.308E+07 | 8.340E+04 | 2.027E+00 | 2.027E-02 | 2.700E+02 | 3.434E-01 | 2.453E-01 | 0. | 0. |
| 66.00 | 2.746E+15 | 7.429E+14 | 3.506E+10 | 3.169E+13 | 1.629E+11 | 1.127E+12 | 0. | 0. | 0. | 2.898E-01 |
| | 9.639E+04 | 5.438E+07 | 1.868E+05 | 7.419E+09 | 1.886E+09 | 9.769E+09 | 0. | 0. | 0. | 0. |
| | 1.141E+02 | -4.047E-03 | 1.693E-07 | 8.083E+00 | 2.347E+02 | 2.347E+02 | 3.139E+06 | 3.304E+06 | 1.034E+06 | 1.943E+09 |
| | 4.579E+05 | 7.309E+07 | 9.639E+04 | 2.438E+00 | 2.438E-02 | 2.438E+02 | 2.321E-01 | 1.520E-01 | 0. | 0. |
| 67.00 | 2.425E+15 | 6.554E+14 | 3.646E+10 | 2.198E+13 | 1.438E+11 | 9.947E+11 | 0. | 0. | 0. | 3.768E-01 |
| | 1.114E+05 | 4.506E+07 | 1.574E+05 | 6.732E+09 | 1.476E+09 | 8.325E+09 | 0. | 0. | 0. | 0. |
| | 9.878E+01 | -4.082E-03 | 1.495E-07 | 7.956E+00 | 2.302E+02 | 2.302E+02 | 3.714E+06 | 3.084E+06 | 1.357E+06 | 2.079E+09 |
| | 4.042E+05 | 5.752E+07 | 1.114E+05 | 2.932E+00 | 2.932E-02 | 2.219E+02 | 1.394E-01 | 9.127E-02 | 0. | 0. |
| 68.00 | 2.136E+15 | 5.777E+14 | 3.783E+10 | 2.464E+13 | 1.266E+11 | 8.762E+11 | 0. | 0. | 0. | 4.890E-01 |
| | 1.286E+05 | 3.720E+07 | 1.336E+05 | 6.111E+09 | 1.147E+09 | 7.076E+09 | 0. | 0. | 0. | 0. |

| | | | | | | | | | | |
|-------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 69.00 | 8.339E+01 | -6.111E-03 | 1.311E+07 | 7.113E+00 | 2.750E+02 | 7.450E+02 | 4.391E+06 | 2.679E+06 | 1.764E+06 | 2.231E+09 |
| | 3.560E+05 | 4.539E+07 | 1.288E+05 | 3.528E+00 | 3.528E-02 | 1.986E+02 | 2.591E-04 | 5.331E-02 | 0. | 0. |
| | 1.477E+15 | 9.077E+14 | 3.921E+10 | 2.185E+13 | 1.113E+11 | 7.094E+11 | 0. | 0. | 0. | 6.369E-01 |
| | 1.499E+05 | 1.064E+07 | 1.141E+07 | 5.546E+04 | 8.041E+08 | 5.990E+04 | 0. | 0. | 0. | 0. |
| | 7.444E+01 | -6.141E-02 | 1.157E+07 | 1.057E+00 | 4.211E-02 | 2.111E+02 | 5.142E+06 | 2.688E+06 | 2.140E+06 | 2.596E+09 |
| | 3.129E+05 | 3.378E+07 | 1.488E+05 | 6.243E+00 | 4.241E-02 | 1.759E+02 | 3.069E-02 | 3.039E-02 | 0. | 0. |
| 70.00 | 1.645E+15 | 6.449E+14 | 6.062E+10 | 1.098E+13 | 9.754E+10 | 6.747E+11 | 0. | 0. | 0. | 4.280E-01 |
| | 1.720E+05 | 2.522E+07 | 7.008E+04 | 5.034E+04 | 6.742E+08 | 5.069E+09 | 0. | 0. | 0. | 0. |
| | 6.104E+01 | -4.166E-03 | 1.014E-07 | 7.491E+00 | 2.165E-02 | 2.165E+02 | 0.141E+06 | 2.507E+06 | 3.073E+06 | 2.571E+09 |
| | 2.742E+05 | 2.025E+07 | 1.770E+05 | 5.105E+00 | 5.105E-02 | 1.539E+02 | 2.957E-02 | 1.697E-02 | 0. | 0. |
| 71.00 | 1.437E+15 | 1.087E+14 | 4.212E+10 | 1.050E+13 | 8.520E+10 | 5.895E+11 | 0. | 0. | 0. | 1.077E+00 |
| | 1.949E+05 | 2.078E+07 | 6.471E+04 | 4.509E+04 | 5.040E+08 | 4.270E+09 | 0. | 0. | 0. | 0. |
| | 5.394E+01 | -6.180E-03 | 7.318E+08 | 6.459E+08 | 2.121E+02 | 2.121E+02 | 7.263E+06 | 2.338E+06 | 4.036E+06 | 2.755E+09 |
| | 2.395E+05 | 2.230E+07 | 1.988E+05 | 6.141E+00 | 6.141E-02 | 1.329E+02 | 1.696E-02 | 9.326E-03 | 0. | 0. |
| 72.00 | 1.251E+15 | 1.185E+14 | 6.374E+10 | 1.448E+13 | 7.419E+10 | 5.133E+11 | 0. | 0. | 0. | 1.400E+00 |
| | 2.498E+05 | 1.716E+07 | 7.348E+04 | 4.147E+04 | 3.614E+08 | 3.565E+09 | 0. | 0. | 0. | 0. |
| | 4.600E+01 | -6.210E-03 | 7.714E+08 | 7.140E+00 | 2.077E+02 | 2.077E+02 | 8.590E+06 | 2.163E+06 | 5.299E+06 | 2.942E+09 |
| | 2.086E+05 | 1.759E+07 | 2.298E+05 | 7.387E+00 | 7.387E-02 | 1.129E+02 | 9.604E-03 | 5.070E-03 | 0. | 0. |
| 73.00 | 1.046E+15 | 4.037E+14 | 4.555E+10 | 1.254E+13 | 6.438E+10 | 4.454E+11 | 0. | 0. | 0. | 1.420E+00 |
| | 2.656E+05 | 1.427E+07 | 6.307E+04 | 1.763E+04 | 2.848E+08 | 2.892E+09 | 1.016E+07 | 1.993E+06 | 6.959E+06 | 3.126E+09 |
| | 3.316E+01 | -6.211E-03 | 6.694E+08 | 6.960E+00 | 2.035E+02 | 2.035E+02 | 5.399E-03 | 2.740E-03 | 0. | 0. |
| | 1.810E+05 | 1.346E+07 | 2.656E+05 | 6.087E+00 | 6.087E-02 | 9.415E+01 | 1.560E-03 | 0. | 0. | 0. |
| 74.00 | 9.387E+14 | 2.539E+14 | 4.761E+10 | 1.938E+13 | 5.566E+10 | 3.851E+11 | 0. | 0. | 0. | 2.366E+00 |
| | 1.070E+05 | 5.594E+07 | 5.594E+04 | 3.416E+04 | 2.134E+08 | 2.498E+09 | 0. | 0. | 0. | 0. |
| | 3.213E+01 | -6.233E-03 | 5.787E+08 | 6.781E+00 | 1.744E+02 | 1.994E+02 | 1.202E+07 | 1.820E+06 | 9.138E+06 | 3.302E+09 |
| | 1.365E+05 | 1.089E+07 | 3.070E+05 | 1.063E+01 | 1.069E-01 | 7.661E+01 | 3.028E-03 | 1.481E-03 | 0. | 0. |
| 75.00 | 6.084E+14 | 4.187E+14 | 4.998E+10 | 9.328E+12 | 4.793E+10 | 3.316E+11 | 0. | 0. | 0. | 3.076E+00 |
| | 3.548E+05 | 1.077E+07 | 4.885E+04 | 1.109E+09 | 1.626E+08 | 2.072E+08 | 0. | 0. | 0. | 0. |
| | 2.798E+01 | -6.217E-03 | 4.984E+08 | 6.005E+00 | 1.955E+02 | 1.955E+02 | 1.421E+07 | 1.641E+06 | 1.200E+07 | 3.461E+09 |
| | 1.348E+05 | 8.544E+06 | 3.548E+05 | 1.286E+01 | 1.286E-01 | 6.103E+01 | 1.705E-03 | 8.056E-04 | 0. | 0. |
| 76.00 | 6.934E+14 | 1.876E+14 | 5.276E+10 | 4.601E+12 | 4.112E+10 | 2.845E+11 | 0. | 0. | 0. | 3.999E+00 |
| | 4.101E+05 | 6.541E+06 | 4.281E+04 | 2.719E+04 | 1.245E+08 | 1.711E+09 | 0. | 0. | 0. | 0. |
| | 2.352E+01 | -6.300E-03 | 4.272E+08 | 6.434E+00 | 1.919E+02 | 1.919E+02 | 1.081E+07 | 1.456E+06 | 1.147E+07 | 3.597E+09 |
| | 1.156E+05 | 6.080E+06 | 4.101E+05 | 1.547E+01 | 1.547E-01 | 4.697E+01 | 9.688E-04 | 4.435E-04 | 0. | 0. |
| 77.00 | 5.924E+14 | 1.662E+14 | 5.604E+10 | 6.636E+12 | 4.513E+10 | 2.430E+11 | 0. | 0. | 0. | 5.199E+00 |
| | 4.741E+05 | 7.449E+06 | 3.755E+04 | 2.343E+04 | 9.926E+07 | 1.405E+09 | 0. | 0. | 0. | 0. |
| | 9.876E+01 | -6.373E-03 | 3.652E+08 | 6.270E+00 | 1.885E+02 | 1.885E+02 | 1.988E+07 | 1.265E+06 | 1.097E+07 | 3.702E+09 |
| | 9.876E+04 | 5.705E+06 | 4.741E+05 | 1.063E+01 | 1.063E-01 | 3.478E+01 | 5.592E-04 | 2.487E-04 | 0. | 0. |
| 78.00 | 5.006E+14 | 1.354E+14 | 5.987E+10 | 5.016E+12 | 2.989E+10 | 2.068E+11 | 0. | 0. | 0. | 6.760E+00 |
| | 5.480E+05 | 6.475E+06 | 3.296E+04 | 2.094E+04 | 8.376E+07 | 1.164E+09 | 0. | 0. | 0. | 0. |
| | 6.403E+04 | -6.398E-03 | 3.198E+08 | 6.113E+00 | 1.853E+02 | 1.853E+02 | 2.351E+07 | 1.071E+06 | 1.049E+07 | 3.770E+09 |
| | 6.403E+04 | 4.408E+06 | 5.480E+05 | 2.740E+01 | 2.740E-01 | 2.454E+01 | 3.100E-04 | 1.429E-04 | 0. | 0. |
| 79.00 | 4.271E+14 | 1.155E+14 | 6.449E+10 | 4.785E+12 | 2.533E+10 | 1.752E+11 | 0. | 0. | 0. | 6.789E+00 |
| | 6.319E+05 | 5.747E+06 | 2.691E+04 | 1.737E+04 | 7.457E+07 | 7.316E+08 | 0. | 0. | 0. | 0. |
| | 1.373E+01 | -6.334E-03 | 2.631E+08 | 5.665E+00 | 1.824E+02 | 1.824E+02 | 2.781E+07 | 0.788E+05 | 1.003E+07 | 3.794E+09 |
| | 7.171E+04 | 3.123E+06 | 6.334E+05 | 2.695E+01 | 2.695E-01 | 1.674E+01 | 2.003E-04 | 8.474E-05 | 0. | 0. |
| 80.00 | 3.039E+14 | 7.740E+13 | 9.987E+10 | 4.159E+12 | 2.137E+10 | 1.470E+11 | 0. | 0. | 0. | 1.143E+01 |
| | 7.323E+05 | 5.144E+06 | 2.531E+04 | 2.550E+04 | 8.988E+07 | 7.512E+08 | 0. | 0. | 0. | 0. |

| | | | | | | | | | |
|--------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 93.00 | 1.117E+00 | 2.554E-01 | 4.224E+00 | 1.710E+02 | 1.730E+02 | 5.630E+07 | 2.70E+03 | 2.231E+03 | 1.287E+09 |
| | 6.14E+03 | 3.47E+04 | 4.174E+06 | 2.987E+00 | 1.386E+02 | 0. | 0. | 3.171E+00 | 5.566E+03 |
| | 3.03E+13 | 3.05E+12 | 3.06E+11 | 1.194E+09 | 1.24E+10 | 2.46E+04 | 7.65E+04 | 1.747E+04 | 5.152E+02 |
| | 4.87E+06 | 1.01E+07 | 4.39E+03 | 7.22E+06 | 1.64E+07 | 2.77E+04 | 6.31E+01 | 2.717E+04 | 6.361E+09 |
| | 3.40E-01 | 3.71E-03 | 4.76E+00 | 1.74E+02 | 1.74E+02 | 5.21E+07 | 1.70E+03 | 1.36E+03 | 1.096E+09 |
| | 3.07E+03 | 6.45E+04 | 4.82E+06 | 3.59E+00 | 1.72E+02 | 9.67E+04 | 1.830E-05 | 4.251E+00 | 6.787E+03 |
| 94.00 | 4.49E+13 | 6.55E+12 | 3.31E+11 | 1.47E+09 | 1.01E+10 | 3.01E+04 | 1.88E+02 | 2.190E+04 | 7.65E+02 |
| | 5.51E+06 | 1.27E+07 | 3.64E+03 | 4.86E+06 | 1.27E+07 | 3.35E+04 | 1.37E+02 | 3.354E+04 | 1.61E+08 |
| | 7.76E-01 | 5.87E-03 | 1.51E+00 | 1.75E+02 | 1.76E+02 | 4.82E+07 | 1.07E+03 | 8.12E+02 | 9.26E+08 |
| | 4.16E+03 | 4.94E+04 | 5.58E+06 | 4.32E+00 | 2.14E+02 | 6.51E+05 | 2.62E-05 | 5.76E+00 | 6.215E+03 |
| | 2.15E+13 | 3.21E+12 | 3.00E+11 | 1.20E+09 | 8.34E+09 | 3.67E+04 | 4.61E-02 | 2.68E+04 | 1.13E+03 |
| | 6.73E+06 | 1.62E+07 | 3.36E+03 | 1.97E+06 | 6.61E+06 | 4.11E+04 | 3.87E-02 | 4.114E+04 | 4.08E+08 |
| | 6.46E-01 | 6.09E-03 | 1.25E+00 | 5.02E+00 | 1.78E+02 | 4.46E+07 | 6.75E+02 | 4.90E+02 | 7.79E+04 |
| | 3.41E+03 | 3.60E+04 | 6.45E+06 | 5.20E+00 | 2.67E+02 | 9.69E+05 | 3.97E-05 | 7.91E+00 | 9.69E+03 |
| 95.00 | 1.66E+13 | 4.31E+12 | 3.97E+11 | 1.72E+09 | 9.88E+08 | 4.49E+04 | 1.12E-01 | 3.29E+04 | 1.69E+03 |
| | 7.46E+06 | 2.05E+07 | 2.95E+03 | 1.17E+06 | 1.77E+06 | 5.04E+04 | 9.42E-02 | 5.047E+04 | 1.07E-07 |
| | 5.48E-01 | 6.31E-03 | 1.02E+00 | 5.04E+00 | 1.80E+02 | 4.12E+07 | 4.57E+02 | 2.95E+02 | 6.51E+08 |
| | 2.80E+03 | 2.95E+04 | 7.46E+06 | 6.26E+00 | 3.33E+02 | 1.50E+07 | 6.28E-05 | 1.10E+01 | 1.19E+04 |
| 96.00 | 1.36E+13 | 3.49E+12 | 4.04E+11 | 1.57E+09 | 8.14E+08 | 5.61E+09 | 2.63E-01 | 4.037E+04 | 2.50E+03 |
| | 6.87E+06 | 2.53E+07 | 2.59E+03 | 9.04E+07 | 1.11E+08 | 3.81E+06 | 2.25E-01 | 6.189E+04 | 2.56E-07 |
| | 4.97E-01 | 6.54E-03 | 8.43E-10 | 5.04E+00 | 1.93E+02 | 1.85E+02 | 2.68E+02 | 1.784E+02 | 5.43E+08 |
| | 2.30E+03 | 2.31E+04 | 8.62E+06 | 7.54E+00 | 4.14E+02 | 2.42E+04 | 1.03E-04 | 1.55E+01 | 1.45E+04 |
| 97.00 | 1.12E+13 | 2.81E+12 | 4.54E+11 | 1.29E+09 | 6.07E+08 | 4.61E+09 | 6.09E-01 | 4.903E+04 | 3.69E+03 |
| | 9.97E+06 | 2.94E+07 | 2.28E+03 | 6.18E+07 | 6.26E+05 | 7.57E+04 | 5.26E-01 | 7.574E+04 | 6.32E-07 |
| | 3.16E-01 | 7.04E-03 | 5.71E-10 | 5.17E+00 | 1.86E+02 | 1.86E+02 | 1.68E+02 | 1.076E+02 | 4.51E+08 |
| | 1.90E+03 | 1.21E+04 | 9.97E+06 | 9.07E+00 | 5.16E+02 | 5.16E+02 | 1.76E+04 | 2.21E+04 | 1.79E+04 |
| 98.00 | 9.26E+12 | 2.24E+12 | 4.94E+11 | 1.06E+09 | 5.49E+08 | 3.80E+09 | 1.17E+00 | 5.87E+04 | 5.39E+03 |
| | 1.15E+07 | 3.06E+07 | 2.02E+03 | 4.22E+07 | 4.37E+05 | 1.620E+06 | 1.19E+00 | 9.236E+04 | 1.53E-06 |
| | 3.16E-01 | 7.04E-03 | 5.71E-10 | 5.17E+00 | 1.86E+02 | 1.86E+02 | 1.06E+02 | 6.49E+04 | 3.75E+08 |
| | 1.57E+03 | 1.44E+04 | 1.15E+07 | 1.09E+03 | 1.39E+01 | 6.42E+02 | 3.11E-04 | 3.19E+01 | 2.30E+04 |
| 100.00 | 7.46E+12 | 1.95E+12 | 4.95E+11 | 3.02E+10 | 4.534E+08 | 1.00E+05 | 4.98E+00 | 6.90E+04 | 7.79E+03 |
| | 1.31E+07 | 2.74E+07 | 1.79E+03 | 2.86E+07 | 2.72E+05 | 1.04E+06 | 2.57E+00 | 1.170E+05 | 3.68E-06 |
| | 2.67E-01 | 7.37E-03 | 4.71E-10 | 5.24E+00 | 1.934E+02 | 3.01E+07 | 6.70E+01 | 3.91E+01 | 3.11E+08 |
| | 1.08E+03 | 3.34E+03 | 1.58E+07 | 1.58E+03 | 1.58E+01 | 6.00E+02 | 5.65E-04 | 4.64E+01 | 3.08E+04 |
| 101.00 | 6.37E+12 | 1.49E+12 | 4.27E+11 | 7.29E+10 | 3.75E+08 | 2.61E+09 | 4.55E+00 | 7.10E+04 | 6.04E+03 |
| | 1.96E+07 | 3.03E+07 | 1.42E+03 | 1.94E+07 | 1.94E+05 | 6.71E+05 | 4.06E+00 | 1.150E+05 | 6.40E-06 |
| | 1.97E-01 | 8.04E-03 | 3.23E-10 | 5.18E+00 | 2.01E+02 | 2.68E+07 | 5.41E+01 | 2.684E+01 | 2.58E+08 |
| | 1.08E+03 | 3.34E+03 | 1.58E+07 | 1.58E+03 | 1.58E+01 | 2.71E+03 | 1.86E-03 | 4.93E+01 | 3.08E+04 |
| 102.00 | 5.27E+12 | 1.21E+12 | 4.11E+11 | 6.75E+10 | 3.11E+08 | 2.20E+09 | 6.77E+00 | 7.49E+04 | 9.30E+03 |
| | 1.96E+07 | 3.03E+07 | 1.42E+03 | 1.94E+07 | 1.94E+05 | 4.30E+05 | 6.10E+00 | 1.191E+05 | 1.10E-05 |
| | 1.97E-01 | 8.04E-03 | 3.23E-10 | 5.18E+00 | 2.01E+02 | 2.39E+02 | 4.74E+01 | 1.83E+01 | 2.14E+08 |
| | 7.01E+02 | 7.57E+03 | 1.86E+07 | 1.90E+03 | 1.90E+01 | 1.38E+03 | 2.95E-03 | 5.33E+01 | 3.08E+04 |
| 103.00 | 4.35E+12 | 9.66E+11 | 3.68E+11 | 5.03E+10 | 2.38E+08 | 1.66E+09 | 9.82E+00 | 7.49E+04 | 8.52E+03 |
| | 1.96E+07 | 3.03E+07 | 1.42E+03 | 9.70E+06 | 6.96E+04 | 2.77E+02 | 8.95E+00 | 1.21E+05 | 1.86E-05 |
| | 1.64E-01 | 8.41E-03 | 2.69E-10 | 4.74E+00 | 2.06E+02 | 2.17E+07 | 3.29E+01 | 1.260E+01 | 1.78E+08 |
| | 7.54E+02 | 6.17E+03 | 2.18E+07 | 2.29E+03 | 1.694E+03 | 7.86E+03 | 4.09E-03 | 5.879E+01 | 3.09E+04 |
| 104.00 | 3.64E+12 | 8.64E+11 | 3.60E+11 | 4.76E+10 | 2.15E+08 | 1.56E+09 | 1.19E+01 | 7.70E+04 | 8.16E+03 |
| | 2.52E+07 | 3.26E+07 | 1.14E+03 | 6.23E+06 | 4.43E+04 | 1.79E+05 | 1.24E+05 | 1.246E+05 | 3.12E-05 |

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SCIENCE APPLICATIONS INC LA JOLLA CA F/6 4/1
ROSCOE MANUAL, VOLUME 14A-1 - AMBIENT ATMOSPHERE (MAJOR AND MIN--ETC(U)
JUN 79 D A HAMLIN, M R SCHOONOVER DNA001-76-C-0194
SAI-78-604-LJ-2A DNA-3964F-14A-1 NL

UNCLASSIFIED

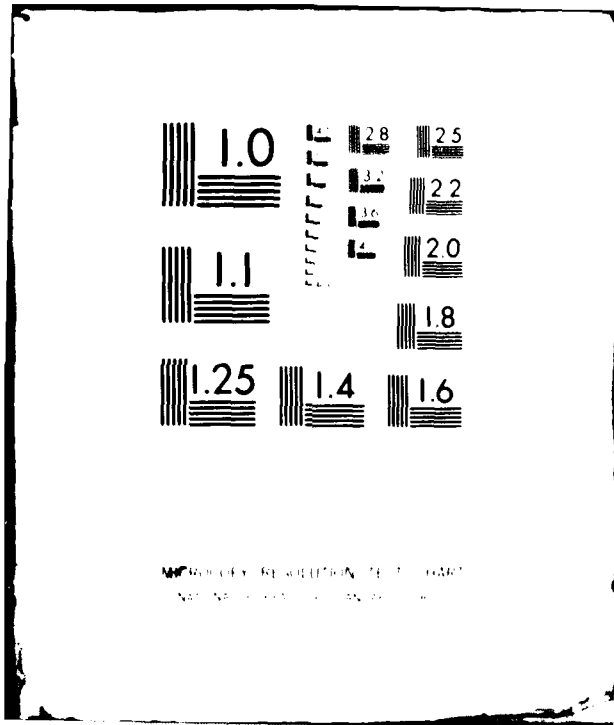
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|--------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 105.00 | 1.4175-01 | -4.810-03 | 2.245F-10 | 5.567F+00 | 2.113E+02 | 2.113E+02 | 2.113E+02 | 1.694E+07 | 2.562E+01 | 6.43E-03 | 6.546E+00 | 1.494E+08 |
| | 6.305E+02 | 5.067E+03 | 2.526E+07 | 2.760E+03 | 2.760E+01 | 2.015E+03 | 2.015E+03 | 1.544E-02 | 6.43E-03 | 6.546E+00 | 6.546E+01 | 3.092E+04 |
| | 4.908E+07 | 6.599E+11 | 3.292E+11 | 3.510E+10 | 1.807E+08 | 1.306E+09 | 1.306E+09 | 1.101E+05 | 1.720E+01 | 7.002E+04 | 7.002E+04 | 9.066E+03 |
| | 1.220E-01 | -9.243E-04 | 1.877E-10 | 5.068E+00 | 2.170E+02 | 2.170E+02 | 2.170E+02 | 1.280E+05 | 2.034E+01 | 5.817E+00 | 5.817E+00 | 5.160E-05 |
| | 5.294E+02 | 4.151E+03 | 2.906F+07 | 3.322E+03 | 3.322E+01 | 2.339E+03 | 2.339E+03 | 1.110E-02 | 1.792E-02 | 7.514E+01 | 7.514E+01 | 1.252E+08 |
| 106.00 | 2.559E+12 | 3.440E+11 | 2.963F+11 | 2.972E+10 | 1.517E+08 | 1.073E+09 | 1.073E+09 | 1.135E-08 | 2.591E+01 | 6.106E+04 | 6.106E+04 | 9.310E+03 |
| | 3.770E+07 | 3.514E+03 | 9.301F+07 | 2.318E+06 | 1.811F+04 | 7.835E+04 | 7.835E+04 | 1.316E+05 | 2.437E+01 | 1.316E+05 | 1.316E+05 | 6.437E-05 |
| | 1.076E-01 | -9.703E-03 | 1.577E-10 | 5.771E+00 | 2.231E+02 | 2.231E+02 | 2.231E+02 | 1.500E+07 | 1.679E+01 | 4.055E+00 | 4.055E+00 | 1.053E+08 |
| | 4.458E+02 | 3.195E+03 | 3.320E+07 | 3.999E+03 | 3.999E+01 | 2.662E+03 | 2.662E+03 | 6.413E-02 | 3.921E-02 | 8.681E+01 | 8.681E+01 | 3.162E+04 |
| 107.00 | 2.155E+12 | 4.512E+11 | 2.630F+11 | 2.486F+10 | 1.278E+08 | 8.812E+08 | 8.812E+08 | 1.183E+05 | 3.426E+01 | 6.311E+04 | 6.311E+04 | 9.540E+03 |
| | 3.770E+07 | 3.514E+03 | 9.301F+07 | 2.318E+06 | 1.811F+04 | 7.835E+04 | 7.835E+04 | 1.316E+05 | 2.437E+01 | 1.316E+05 | 1.316E+05 | 6.437E-05 |
| | 1.076E-01 | -9.703E-03 | 1.577E-10 | 5.771E+00 | 2.231E+02 | 2.231E+02 | 2.231E+02 | 1.500E+07 | 1.679E+01 | 4.055E+00 | 4.055E+00 | 1.053E+08 |
| | 4.458E+02 | 3.195E+03 | 3.320E+07 | 3.999E+03 | 3.999E+01 | 2.662E+03 | 2.662E+03 | 6.413E-02 | 3.921E-02 | 8.681E+01 | 8.681E+01 | 3.162E+04 |
| 108.00 | 1.821E+12 | 4.763E+11 | 2.040F+11 | 2.101E+10 | 1.080E+08 | 7.206E+08 | 7.206E+08 | 1.165E+05 | 4.454E+01 | 6.310E+04 | 6.310E+04 | 9.779E+03 |
| | 4.255E+07 | 3.741E+07 | 7.004F+02 | 1.572E+06 | 7.494E+03 | 3.689E+04 | 3.689E+04 | 1.371E+05 | 4.273E+01 | 1.390E+05 | 1.390E+05 | 2.194E-04 |
| | 7.046E-02 | -1.131E-02 | 9.516E-11 | 6.104E+00 | 2.452E+02 | 2.452E+02 | 2.452E+02 | 1.058E+07 | 1.179E+01 | 1.305E+00 | 1.305E+00 | 6.010E+07 |
| | 2.706E+02 | 1.793E+03 | 4.777E+07 | 6.977E+03 | 6.977E+01 | 3.601E+03 | 3.601E+03 | 6.221E-01 | 4.727E-01 | 1.412E+02 | 1.412E+02 | 3.123E+04 |
| 109.00 | 1.312E+12 | 2.058E+11 | 1.789F+11 | 1.781E+10 | 9.152E+07 | 5.883E+08 | 5.883E+08 | 1.187E+05 | 5.716E+01 | 6.724E+04 | 6.724E+04 | 1.000E+04 |
| | 4.255E+07 | 3.741E+07 | 7.004F+02 | 1.572E+06 | 7.494E+03 | 3.689E+04 | 3.689E+04 | 1.371E+05 | 4.273E+01 | 1.390E+05 | 1.390E+05 | 2.194E-04 |
| | 7.046E-02 | -1.131E-02 | 9.516E-11 | 6.104E+00 | 2.452E+02 | 2.452E+02 | 2.452E+02 | 1.058E+07 | 1.179E+01 | 1.305E+00 | 1.305E+00 | 6.010E+07 |
| | 2.706E+02 | 1.793E+03 | 4.777E+07 | 6.977E+03 | 6.977E+01 | 3.601E+03 | 3.601E+03 | 6.221E-01 | 4.727E-01 | 1.412E+02 | 1.412E+02 | 3.123E+04 |
| 110.00 | 1.312E+12 | 2.058E+11 | 1.789F+11 | 1.781E+10 | 9.152E+07 | 5.883E+08 | 5.883E+08 | 1.187E+05 | 5.716E+01 | 6.724E+04 | 6.724E+04 | 1.000E+04 |
| | 4.255E+07 | 3.741E+07 | 7.004F+02 | 1.572E+06 | 7.494E+03 | 3.689E+04 | 3.689E+04 | 1.371E+05 | 4.273E+01 | 1.390E+05 | 1.390E+05 | 2.194E-04 |
| | 7.046E-02 | -1.131E-02 | 9.516E-11 | 6.104E+00 | 2.452E+02 | 2.452E+02 | 2.452E+02 | 1.058E+07 | 1.179E+01 | 1.305E+00 | 1.305E+00 | 6.010E+07 |
| | 2.706E+02 | 1.793E+03 | 4.777E+07 | 6.977E+03 | 6.977E+01 | 3.601E+03 | 3.601E+03 | 6.221E-01 | 4.727E-01 | 1.412E+02 | 1.412E+02 | 3.123E+04 |
| 111.00 | 1.119E+12 | 2.242E+11 | 1.571E+11 | 1.292E+10 | 6.637E+07 | 3.916E+08 | 3.916E+08 | 5.034E-11 | 9.216E+01 | 9.147E+04 | 9.147E+04 | 1.043E+04 |
| | 5.936E+07 | 3.944E+07 | 5.881E+02 | 4.378E+05 | 2.041E+03 | 1.475E+04 | 1.475E+04 | 1.514E+05 | 9.057E+01 | 1.313E+05 | 1.313E+05 | 8.362E-04 |
| | 5.503E-02 | -1.260E-02 | 6.901E-11 | 6.342E+00 | 2.634E+02 | 2.634E+02 | 2.634E+02 | 6.397E+06 | 1.113E+01 | 6.126E-01 | 6.126E-01 | 4.697E+07 |
| | 1.969E+02 | 1.105E+03 | 5.935E+07 | 1.011E+04 | 1.011E+02 | 4.190E+03 | 4.190E+03 | 2.933E+00 | 1.118E+00 | 1.972E+02 | 1.972E+02 | 3.136E+04 |
| 112.00 | 9.575E+11 | 1.896E+11 | 1.386E+11 | 1.105F+10 | 5.677E+07 | 3.194E+08 | 3.194E+08 | 1.829E-11 | 1.169E+02 | 9.365E+04 | 9.365E+04 | 1.064E+04 |
| | 6.573E+07 | 4.063E+07 | 5.409E+02 | 2.997E+05 | 1.331E+03 | 1.161E+04 | 1.161E+04 | 1.558E+05 | 1.156E+02 | 1.557E+05 | 1.557E+05 | 1.278E-03 |
| | 4.900E-02 | -1.334E-02 | 5.903E-11 | 6.453E+00 | 2.737E+02 | 2.737E+02 | 2.737E+02 | 7.481E+06 | 1.043E+01 | 4.197E-01 | 4.197E-01 | 4.042E+07 |
| | 1.969E+02 | 1.105E+03 | 5.935E+07 | 1.011E+04 | 1.011E+02 | 4.190E+03 | 4.190E+03 | 2.933E+00 | 1.118E+00 | 1.972E+02 | 1.972E+02 | 3.136E+04 |
| 113.00 | 8.214E+11 | 1.604E+11 | 1.237E+11 | 9.578E+09 | 4.871E+07 | 2.599E+08 | 2.599E+08 | 6.912E-12 | 1.489E+02 | 9.587E+04 | 9.587E+04 | 1.084E+04 |
| | 7.249E+07 | 4.124E+07 | 4.955E+02 | 2.044F+05 | 6.717E+04 | 9.446E+03 | 9.446E+03 | 1.604E+05 | 1.473E+02 | 1.603E+05 | 1.603E+05 | 1.928E-03 |
| | 4.384E-02 | -1.413E-02 | 5.064E-11 | 6.565E+00 | 2.847E+02 | 2.847E+02 | 2.847E+02 | 6.667E+06 | 1.072E+01 | 2.876E-01 | 2.876E-01 | 3.494E+07 |
| | 1.656E+02 | 8.369E+02 | 7.297E+07 | 1.466E+04 | 1.466E+02 | 4.743E+03 | 4.743E+03 | 1.361E+01 | 0. | 2.693E+02 | 2.693E+02 | 3.142E+04 |
| 114.00 | 7.067E+11 | 1.353E+11 | 1.113F+11 | 8.154F+09 | 4.190E+07 | 2.108E+08 | 2.108E+08 | 2.728E-12 | 1.910E+02 | 9.615E+04 | 9.615E+04 | 1.194E+04 |
| | 7.962E+07 | 4.178E+07 | 4.603E+02 | 1.391E+05 | 5.719E+02 | 7.916E+03 | 7.916E+03 | 1.652E+05 | 1.677E+02 | 1.651E+05 | 1.651E+05 | 2.871E-03 |
| | 3.917E-02 | -1.501E-02 | 4.577E-11 | 6.677E+00 | 2.968E+02 | 2.968E+02 | 2.968E+02 | 5.942E+06 | 1.019E+01 | 1.971E-01 | 1.971E-01 | 3.028E+07 |
| | 1.250E+02 | 4.710E+02 | 7.961E+07 | 1.765E+04 | 1.765E+02 | 5.006E+03 | 5.006E+03 | 2.680F+01 | 0. | 3.101E+02 | 3.101E+02 | 3.142E+04 |
| 115.00 | 8.098E+11 | 1.144E+11 | 1.012F+11 | 7.036F+09 | 4.616E+07 | 1.700E+08 | 1.700E+08 | 1.126E-12 | 2.470E+02 | 1.005E+05 | 1.005E+05 | 1.123E+04 |
| | 8.717E+07 | 4.275E+07 | 4.257F+02 | 9.546E+04 | 3.763E+02 | 6.790E+03 | 6.790E+03 | 1.702E+05 | 2.404E+02 | 1.700E+05 | 1.700E+05 | 2.194E-03 |
| | 3.554E-02 | -1.596E-02 | 4.760E-11 | 6.776E+00 | 3.092E+02 | 3.092E+02 | 3.092E+02 | 5.299E+06 | 1.011E+01 | 1.351E-01 | 1.351E-01 | 2.632E+07 |
| | 1.092E+02 | 3.432E+02 | 8.714E+07 | 2.175E+04 | 2.175E+02 | 5.259E+03 | 5.259E+03 | 6.650F+13 | 0. | 3.534E+02 | 3.534E+02 | 3.135E+04 |
| 116.00 | 5.280E+11 | 9.643E+10 | 9.281E+10 | 6.092E+09 | 3.131E+07 | 1.463E+08 | 1.463E+08 | 4.650F+13 | 3.208E+02 | 1.029E+05 | 1.029E+05 | 1.142E+04 |
| | 9.510E+07 | 4.266E+07 | 3.941E+02 | 6.523E+04 | 2.465E+02 | 5.899E+03 | 5.899E+03 | 1.754E+05 | 3.102E+02 | 1.751E+05 | 1.751E+05 | 6.121E-03 |

| | | | | | | | | | | | | | | | |
|--------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 117.00 | 3.227F+02 | 1.077E-02 | 4.476E+02 | 4.255F-11 | 9.501F+07 | 9.078E+00 | 2.559E+02 | 3.227F+04 | 3.504E+03 | 4.277F+04 | 4.726E+00 | 1.007E+01 | 9.254E-02 | 3.993E+02 | 4.296E+07 |
| | 4.570E+11 | 9.14E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 | 9.545E+10 |
| | 1.071E+08 | 4.349E+07 | 3.653E+04 | 4.571E+00 | 4.571E+00 | 4.571E+00 | 4.571E+00 | 4.571E+00 | 4.571E+00 | 4.571E+00 | 4.571E+00 | 4.571E+00 | 4.571E+00 | 4.571E+00 | 4.571E+00 |
| | 2.916E-04 | -1.803E-32 | 2.830E-11 | 6.978E+00 | 6.978E+00 | 6.978E+00 | 6.978E+00 | 6.978E+00 | 6.978E+00 | 6.978E+00 | 6.978E+00 | 6.978E+00 | 6.978E+00 | 6.978E+00 | 6.978E+00 |
| | 8.266E+01 | 1.783E+02 | 1.034E+08 | 3.081E+02 | 3.081E+02 | 3.081E+02 | 3.081E+02 | 3.081E+02 | 3.081E+02 | 3.081E+02 | 3.081E+02 | 3.081E+02 | 3.081E+02 | 3.081E+02 | 3.081E+02 |
| 118.00 | 4.011E+11 | 9.714E+10 | 7.636E+10 | 4.029E+09 | 4.029E+09 | 4.029E+09 | 4.029E+09 | 4.029E+09 | 4.029E+09 | 4.029E+09 | 4.029E+09 | 4.029E+09 | 4.029E+09 | 4.029E+09 | 4.029E+09 |
| | 1.211E+08 | 4.327E+07 | 3.349E+02 | 3.046E+04 | 3.046E+04 | 3.046E+04 | 3.046E+04 | 3.046E+04 | 3.046E+04 | 3.046E+04 | 3.046E+04 | 3.046E+04 | 3.046E+04 | 3.046E+04 | 3.046E+04 |
| | 2.966E-02 | -1.722E-02 | 2.471E-11 | 7.072E+00 | 7.072E+00 | 7.072E+00 | 7.072E+00 | 7.072E+00 | 7.072E+00 | 7.072E+00 | 7.072E+00 | 7.072E+00 | 7.072E+00 | 7.072E+00 | 7.072E+00 |
| | 7.195E+01 | 1.302E+04 | 1.121E+08 | 3.710E+04 | 3.710E+04 | 3.710E+04 | 3.710E+04 | 3.710E+04 | 3.710E+04 | 3.710E+04 | 3.710E+04 | 3.710E+04 | 3.710E+04 | 3.710E+04 | 3.710E+04 |
| 119.00 | 3.531E+11 | 9.010E+10 | 7.071E+10 | 4.074E+09 | 4.074E+09 | 4.074E+09 | 4.074E+09 | 4.074E+09 | 4.074E+09 | 4.074E+09 | 4.074E+09 | 4.074E+09 | 4.074E+09 | 4.074E+09 | 4.074E+09 |
| | 1.211E+08 | 4.349E+07 | 3.146E+02 | 2.941E+04 | 2.941E+04 | 2.941E+04 | 2.941E+04 | 2.941E+04 | 2.941E+04 | 2.941E+04 | 2.941E+04 | 2.941E+04 | 2.941E+04 | 2.941E+04 | 2.941E+04 |
| | 2.466E-02 | -2.036E-02 | 2.177E-11 | 7.165E+00 | 7.165E+00 | 7.165E+00 | 7.165E+00 | 7.165E+00 | 7.165E+00 | 7.165E+00 | 7.165E+00 | 7.165E+00 | 7.165E+00 | 7.165E+00 | 7.165E+00 |
| | 6.345E+01 | 9.788E+01 | 1.213E+08 | 4.468E+04 | 4.468E+04 | 4.468E+04 | 4.468E+04 | 4.468E+04 | 4.468E+04 | 4.468E+04 | 4.468E+04 | 4.468E+04 | 4.468E+04 | 4.468E+04 | 4.468E+04 |
| 119.99 | 4.143E+11 | 9.413E+10 | 6.180E+10 | 3.627E+09 | 3.627E+09 | 3.627E+09 | 3.627E+09 | 3.627E+09 | 3.627E+09 | 3.627E+09 | 3.627E+09 | 3.627E+09 | 3.627E+09 | 3.627E+09 | 3.627E+09 |
| | 1.306E+08 | 4.363E+07 | 2.924E+02 | 1.428E+04 | 1.428E+04 | 1.428E+04 | 1.428E+04 | 1.428E+04 | 1.428E+04 | 1.428E+04 | 1.428E+04 | 1.428E+04 | 1.428E+04 | 1.428E+04 | 1.428E+04 |
| | 2.274E-02 | -2.145E-02 | 1.936E-11 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 |
| | 5.640E+01 | 7.794E+01 | 1.305E+08 | 5.370E+04 | 5.370E+04 | 5.370E+04 | 5.370E+04 | 5.370E+04 | 5.370E+04 | 5.370E+04 | 5.370E+04 | 5.370E+04 | 5.370E+04 | 5.370E+04 | 5.370E+04 |
| 120.00 | 3.140E+11 | 9.409E+10 | 6.170E+10 | 3.623E+09 | 3.623E+09 | 3.623E+09 | 3.623E+09 | 3.623E+09 | 3.623E+09 | 3.623E+09 | 3.623E+09 | 3.623E+09 | 3.623E+09 | 3.623E+09 | 3.623E+09 |
| | 1.307E+08 | 4.365E+07 | 2.922E+02 | 1.422E+04 | 1.422E+04 | 1.422E+04 | 1.422E+04 | 1.422E+04 | 1.422E+04 | 1.422E+04 | 1.422E+04 | 1.422E+04 | 1.422E+04 | 1.422E+04 | 1.422E+04 |
| | 2.274E-02 | -1.711E-05 | 1.936E-11 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 | 7.254E+00 |
| | 5.634E+01 | 7.782E+01 | 1.306E+08 | 5.380E+04 | 5.380E+04 | 5.380E+04 | 5.380E+04 | 5.380E+04 | 5.380E+04 | 5.380E+04 | 5.380E+04 | 5.380E+04 | 5.380E+04 | 5.380E+04 | 5.380E+04 |
| 121.00 | 2.744E+11 | 4.673E+10 | 5.585E+10 | 3.058E+09 | 3.058E+09 | 3.058E+09 | 3.058E+09 | 3.058E+09 | 3.058E+09 | 3.058E+09 | 3.058E+09 | 3.058E+09 | 3.058E+09 | 3.058E+09 | 3.058E+09 |
| | 1.405E+08 | 4.376E+07 | 2.714E+02 | 1.414E+04 | 1.414E+04 | 1.414E+04 | 1.414E+04 | 1.414E+04 | 1.414E+04 | 1.414E+04 | 1.414E+04 | 1.414E+04 | 1.414E+04 | 1.414E+04 | 1.414E+04 |
| | 2.102E-02 | -1.264E-05 | 1.694E-11 | 7.703E+00 | 7.703E+00 | 7.703E+00 | 7.703E+00 | 7.703E+00 | 7.703E+00 | 7.703E+00 | 7.703E+00 | 7.703E+00 | 7.703E+00 | 7.703E+00 | 7.703E+00 |
| | 4.941E+01 | 5.709E+01 | 1.404E+08 | 6.479E+04 | 6.479E+04 | 6.479E+04 | 6.479E+04 | 6.479E+04 | 6.479E+04 | 6.479E+04 | 6.479E+04 | 6.479E+04 | 6.479E+04 | 6.479E+04 | 6.479E+04 |
| 122.00 | 2.407E+11 | 4.070E+10 | 5.084E+10 | 2.806E+09 | 2.806E+09 | 2.806E+09 | 2.806E+09 | 2.806E+09 | 2.806E+09 | 2.806E+09 | 2.806E+09 | 2.806E+09 | 2.806E+09 | 2.806E+09 | 2.806E+09 |
| | 1.506E+08 | 4.382E+07 | 2.523E+02 | 6.841E+03 | 6.841E+03 | 6.841E+03 | 6.841E+03 | 6.841E+03 | 6.841E+03 | 6.841E+03 | 6.841E+03 | 6.841E+03 | 6.841E+03 | 6.841E+03 | 6.841E+03 |
| | 1.957E-02 | -1.357E-05 | 1.491E-11 | 4.151E+00 | 4.151E+00 | 4.151E+00 | 4.151E+00 | 4.151E+00 | 4.151E+00 | 4.151E+00 | 4.151E+00 | 4.151E+00 | 4.151E+00 | 4.151E+00 | 4.151E+00 |
| | 4.366E+01 | 4.220E+01 | 1.503E+08 | 7.802E+04 | 7.802E+04 | 7.802E+04 | 7.802E+04 | 7.802E+04 | 7.802E+04 | 7.802E+04 | 7.802E+04 | 7.802E+04 | 7.802E+04 | 7.802E+04 | 7.802E+04 |
| 123.00 | 2.142E+11 | 3.570E+10 | 4.652E+10 | 2.279E+09 | 2.279E+09 | 2.279E+09 | 2.279E+09 | 2.279E+09 | 2.279E+09 | 2.279E+09 | 2.279E+09 | 2.279E+09 | 2.279E+09 | 2.279E+09 | 2.279E+09 |
| | 1.610E+08 | 4.383E+07 | 2.345E+02 | 4.538E+03 | 4.538E+03 | 4.538E+03 | 4.538E+03 | 4.538E+03 | 4.538E+03 | 4.538E+03 | 4.538E+03 | 4.538E+03 | 4.538E+03 | 4.538E+03 | 4.538E+03 |
| | 1.814E-02 | -1.450E-05 | 1.325E-11 | 8.299E+00 | 8.299E+00 | 8.299E+00 | 8.299E+00 | 8.299E+00 | 8.299E+00 | 8.299E+00 | 8.299E+00 | 8.299E+00 | 8.299E+00 | 8.299E+00 | 8.299E+00 |
| | 3.883E+01 | 3.141E+01 | 1.609E+08 | 9.396E+04 | 9.396E+04 | 9.396E+04 | 9.396E+04 | 9.396E+04 | 9.396E+04 | 9.396E+04 | 9.396E+04 | 9.396E+04 | 9.396E+04 | 9.396E+04 | 9.396E+04 |
| 124.00 | 1.911E+11 | 3.152E+10 | 4.276E+10 | 1.937E+09 | 1.937E+09 | 1.937E+09 | 1.937E+09 | 1.937E+09 | 1.937E+09 | 1.937E+09 | 1.937E+09 | 1.937E+09 | 1.937E+09 | 1.937E+09 | 1.937E+09 |
| | 1.718E+08 | 4.379E+07 | 2.181E+02 | 3.101E+03 | 3.101E+03 | 3.101E+03 | 3.101E+03 | 3.101E+03 | 3.101E+03 | 3.101E+03 | 3.101E+03 | 3.101E+03 | 3.101E+03 | 3.101E+03 | 3.101E+03 |
| | 1.701E-02 | -1.544E-05 | 1.183E-11 | 9.046E+00 | 9.046E+00 | 9.046E+00 | 9.046E+00 | 9.046E+00 | 9.046E+00 | 9.046E+00 | 9.046E+00 | 9.046E+00 | 9.046E+00 | 9.046E+00 | 9.046E+00 |
| | 3.475E+01 | 2.551E+01 | 1.716E+08 | 1.132E+05 | 1.132E+05 | 1.132E+05 | 1.132E+05 | 1.132E+05 | 1.132E+05 | 1.132E+05 | 1.132E+05 | 1.132E+05 | 1.132E+05 | 1.132E+05 | 1.132E+05 |
| 125.00 | 1.713E+11 | 2.600E+10 | 3.947E+10 | 1.688E+09 | 1.688E+09 | 1.688E+09 | 1.688E+09 | 1.688E+09 | 1.688E+09 | 1.688E+09 | 1.688E+09 | 1.688E+09 | 1.688E+09 | 1.688E+09 | 1.688E+09 |
| | 1.671E+08 | 4.372E+07 | 2.079E+02 | 2.119E+03 | 2.119E+03 | 2.119E+03 | 2.119E+03 | 2.119E+03 | 2.119E+03 | 2.119E+03 | 2.119E+03 | 2.119E+03 | 2.119E+03 | 2.119E+03 | 2.119E+03 |
| | 1.595E-02 | -1.639E-05 | 1.062E-11 | 9.493E+00 | 9.493E+00 | 9.493E+00 | 9.493E+00 | 9.493E+00 | 9.493E+00 | 9.493E+00 | 9.493E+00 | 9.493E+00 | 9.493E+00 | 9.493E+00 | 9.493E+00 |
| | 3.120E+01 | 1.770E+01 | 1.826E+08 | 1.363E+05 | 1.363E+05 | 1.363E+05 | 1.363E+05 | 1.363E+05 | 1.363E+05 | 1.363E+05 | 1.363E+05 | 1.363E+05 | 1.363E+05 | 1.363E+05 | 1.363E+05 |
| 130.00 | 1.061E+11 | 1.690E+10 | 2.781E+10 | 9.188E+08 | 9.188E+08 | 9.188E+08 | 9.188E+08 | 9.188E+08 | 9.188E+08 | 9.188E+08 | 9.188E+08 | 9.188E+08 | 9.188E+08 | 9.188E+08 | 9.188E+08 |
| | 2.372E+08 | 4.241E+07 | 1.436E+02 | 3.156E+02 | 3.156E+02 | 3.156E+02 | 3.156E+02 | 3.156E+02 | 3.156E+02 | 3.156E+02 | 3.156E+02 | 3.156E+02 | 3.156E+02 | 3.156E+02 | 3.156E+02 |
| | 1.199E-02 | -2.109E-05 | 6.617E-12 | 1.172E+01 | 1.172E+01 | 1.172E+01 | 1.172E+01 | 1.172E+01 | 1.172E+01 | 1.172E+01 | 1.172E+01 | 1.172E+01 | 1.172E+01 | 1.172E+01 | 1.172E+01 |
| | 1.996E+01 | 4.575E+00 | 2.394E+08 | 3.143E+05 | 3.143E+05 | 3.143E+05 | 3.143E+05 | 3.143E+05 | 3.143E+05 | 3.143E+05 | 3.143E+05 | 3.143E+05 | 3.143E+05 | 3.143E+05 | 3.143E+05 |
| 135.00 | 7.124F+10 | 1.075E+10 | 2.085E+10 | 5.210E+08 | 5.210E+08 | 5.210E+08 | 5.210E+08 | 5.210E+08 | 5.210E+08 | 5.210E+08 | 5.210E+08 | 5.210E+08 | 5.210E+08 | 5.210E+08 | 5.210E+08 |
| | 2.947E+08 | 4.128E+07 | 1.081E+02 | 4.705E+01 | 4.705E+01 | 4.705E+01 | 4.705E+01 | 4.705E+01 | 4.705E+01 | 4.705E+01 | 4.705E+01 | 4.705E+01 | 4.705E+01 | 4.705E+01 | 4.705E+01 |

| | | | | | | | | | |
|----------|-----------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|
| 9.41E+01 | -2.27E+00 | 4.47E+12 | 1.3921E+01 | 6.007E+02 | 8.77E+02 | 6.14E+05 | 1.000E+01 | 7.03E+05 | 4.77E+04 |
| 1.34E+01 | 1.20E+00 | 2.940E+08 | 6.065E+05 | 2.340E+03 | 5.834E+03 | 0. | 0. | 2.73E+03 | 2.45E+04 |
| 5.04E+09 | 7.39E+09 | 4.631E+10 | 4.70E+08 | 1.056E+07 | 4.70E+06 | 2.01E+05 | 1.10E+04 | 1.554E+05 | 1.41E+04 |
| 3.14E+09 | 7.21E+07 | 8.997E+01 | 7.010E+00 | 3.67E+02 | 1.35E+02 | 3.471E+05 | 9.87E+03 | 3.37E+05 | 2.031E+00 |
| 7.61E+03 | -1.02E+05 | 3.206E+12 | 1.010E+01 | 7.41E+02 | 9.91E+02 | 3.921E+05 | 1.000E+01 | 1.06E+05 | 2.47E+06 |
| 9.71E+00 | 3.81E+01 | 3.37E+08 | 1.288E+06 | 4.38E+03 | 5.65E+03 | 0. | 0. | 3.894E+03 | 2.90E+04 |
| 3.72E+10 | 5.32E+09 | 1.320E+10 | 2.427E+08 | 9.84E+06 | 3.10E+06 | 2.17E+05 | 2.140E+04 | 1.60E+05 | 1.50E+04 |
| 3.72E+08 | 3.71E+07 | 8.210E+01 | 1.444E+00 | 7.04E+01 | 7.58E+01 | 3.78E+05 | 1.50E+04 | 1.63E+05 | 3.93E+00 |
| 6.35E+03 | -1.45E+05 | 2.96E+14 | 1.82E+01 | 8.18E+02 | 1.09E+03 | 2.67E+05 | 1.000E+01 | 1.68E+06 | 1.72E+06 |
| 7.31E+00 | 1.18E+01 | 3.62E+08 | 2.24E+06 | 6.13E+03 | 5.48E+03 | 0. | 0. | 5.27E+03 | 3.07E+04 |
| 2.87E+10 | 3.97E+09 | 1.094E+10 | 1.71E+08 | 8.97E+06 | 2.14E+06 | 2.34E+05 | 3.29E+04 | 1.62E+05 | 1.50E+04 |
| 3.72E+08 | 3.48E+07 | 7.40E+01 | 1.35E+01 | 1.40E+03 | 4.91E+01 | 4.07E+04 | 2.16E+04 | 3.85E+05 | 6.69E+00 |
| 5.36E+03 | -3.87E+05 | 1.84E+12 | 2.03E+01 | 8.70E+02 | 1.19E+03 | 1.96E+05 | 1.000E+01 | 2.45E+07 | 1.36E+00 |
| 5.84E+00 | 1.78E+02 | 4.68E+08 | 3.51E+06 | 7.79E+03 | 5.31E+03 | 0. | 0. | 6.85E+03 | 3.21E+04 |
| 1.60E+10 | 4.81E+09 | 7.92E+09 | 9.16E+07 | 7.90E+06 | 1.11E+06 | 2.69E+05 | 6.72E+04 | 1.56E+05 | 1.62E+04 |
| 3.64E+08 | 3.01E+07 | 4.63E+01 | 3.45E+03 | 5.96E+05 | 1.58E+01 | 4.54E+05 | 3.86E+04 | 4.16E+05 | 1.53E+01 |
| 3.98E+03 | -4.60E+05 | 1.18E+12 | 2.45E+01 | 1.01E+03 | 1.36E+03 | 1.33E+05 | 1.000E+01 | 5.53E+09 | 8.33E+05 |
| 3.69E+00 | 4.16E+03 | 3.60E+08 | 6.18E+06 | 9.42E+03 | 5.00E+03 | 0. | 0. | 1.01E+04 | 3.57E+04 |
| 1.21E+10 | 1.57E+09 | 8.05E+09 | 5.56E+07 | 7.17E+06 | 6.11E+05 | 4.07E+05 | 1.15E+05 | 1.38E+05 | 1.62E+04 |
| 3.16E+08 | 2.87E+07 | 3.33E+01 | 7.66E+05 | 2.71E+06 | 6.10E+00 | 4.83E+05 | 5.88E+04 | 4.25E+05 | 2.53E+01 |
| 3.06E+03 | -2.96E+05 | 8.11E+13 | 2.85E+01 | 1.12E+03 | 1.57E+03 | 1.10E+05 | 1.000E+01 | 1.26E+10 | 5.45E+05 |
| 2.57E+00 | 4.91E+04 | 3.09E+08 | 7.87E+06 | 8.36E+03 | 3.81E+03 | 0. | 0. | 1.31E+04 | 4.02E+04 |
| 8.57E+09 | 1.04E+09 | 4.78E+09 | 1.50E+07 | 8.57E+06 | 3.84E+05 | 3.47E+05 | 1.74E+05 | 1.15E+05 | 1.50E+04 |
| 2.74E+08 | 2.25E+07 | 2.91E+01 | 1.70E+06 | 1.30E+07 | 2.47E+00 | 4.95E+05 | 7.95E+04 | 4.16E+05 | 3.62E+01 |
| 2.42E+03 | -5.86E+05 | 5.83E+13 | 3.73E+01 | 1.21E+03 | 1.57E+03 | 1.00E+05 | 1.000E+01 | 2.88E+12 | 3.74E+05 |
| 1.87E+00 | 6.08E+05 | 2.67E+08 | 7.87E+06 | 6.42E+03 | 3.02E+03 | 0. | 0. | 1.51E+04 | 4.22E+04 |
| 6.26E+09 | 7.87E+08 | 3.89E+09 | 2.10E+07 | 6.06E+06 | 2.43E+05 | 3.88E+05 | 2.39E+05 | 9.08E+04 | 1.32E+04 |
| 2.39E+08 | 1.97E+07 | 1.71E+01 | 4.78E+08 | 6.45E+09 | 1.01E+00 | 4.92E+05 | 4.95E+04 | 3.92E+05 | 4.63E+01 |
| 1.95E+03 | -6.35E+05 | 4.35E+13 | 3.60E+01 | 1.29E+03 | 1.76E+03 | 9.53E+04 | 1.000E+01 | 6.80E+14 | 2.86E+05 |
| 1.42E+00 | 7.81E+06 | 2.31E+08 | 7.984E+06 | 5.00E+03 | 2.45E+03 | 0. | 0. | 1.60E+04 | 4.20E+04 |
| 4.70E+09 | 5.35E+08 | 3.21E+09 | 1.56E+07 | 5.68E+06 | 1.60E+05 | 4.30E+05 | 3.05E+05 | 6.93E+04 | 1.12E+04 |
| 2.08E+08 | 1.60E+07 | 1.23E+01 | 8.91E+10 | 3.29E+10 | 4.47E+01 | 4.79E+05 | 1.14E+05 | 3.69E+05 | 5.46E+01 |
| 1.60E+03 | -6.75E+05 | 3.34E+13 | 3.95E+01 | 1.37E+03 | 1.87E+03 | 9.14E+04 | 1.000E+01 | 1.50E+15 | 1.95E+05 |
| 1.10E+00 | 1.03E+06 | 2.01E+08 | 7.52E+06 | 3.72E+03 | 2.03E+03 | 0. | 0. | 1.59E+04 | 4.00E+04 |
| 4.01E+09 | 4.00E+04 | 2.32E+09 | 7.78E+06 | 5.08E+06 | 7.47E+04 | 5.12E+05 | 4.27E+05 | 3.81E+04 | 7.66E+03 |
| 1.50E+08 | 1.21E+07 | 6.35E+00 | 4.13E+13 | 9.11E+13 | 8.87E+02 | 4.36E+05 | 1.37E+05 | 2.98E+05 | 6.45E+01 |
| 1.11E+03 | -7.32E+05 | 2.09E+13 | 4.59E+01 | 1.48E+03 | 2.04E+03 | 8.52E+04 | 1.000E+01 | 7.82E+19 | 1.12E+05 |
| 7.09E+01 | 1.21E+08 | 1.54E+03 | 4.06E+06 | 1.53E+03 | 1.46E+03 | 0. | 0. | 1.37E+04 | 3.35E+04 |
| 1.77E+09 | 1.79E+08 | 1.74E+09 | 4.14E+06 | 4.64E+06 | 3.75E+04 | 5.87E+05 | 5.30E+05 | 2.05E+04 | 5.07E+03 |
| 1.16E+04 | 8.90E+06 | 3.27E+00 | 2.03E+16 | 2.67E+15 | 1.86E+02 | 3.00E+05 | 1.50E+05 | 2.36E+05 | 6.60E+01 |
| 6.61E+04 | -7.03E+05 | 1.38E+13 | 5.17E+01 | 1.57E+03 | 2.18E+03 | 8.00E+04 | 1.000E+01 | 4.07E+22 | 6.71E+04 |
| 4.87E+01 | 3.15E+10 | 1.18E+08 | 2.89E+06 | 6.76E+02 | 1.10E+03 | 0. | 0. | 1.05E+04 | 2.64E+04 |
| 1.16E+09 | 1.11E+08 | 1.49E+09 | 2.31E+06 | 4.20E+06 | 1.97E+04 | 6.47E+05 | 8.04E+05 | 1.11E+04 | 3.23E+03 |
| 9.23E+07 | 6.51E+06 | 1.69E+00 | 1.00E+19 | 8.18E+18 | 4.01E+03 | 3.38E+05 | 1.55E+05 | 1.82E+05 | 6.13E+01 |
| 5.95E+04 | -2.77E+05 | 9.81E+14 | 5.69E+01 | 1.67E+03 | 2.30E+03 | 7.58E+04 | 1.000E+01 | 2.07E+25 | 4.23E+04 |
| 4.42E+01 | 7.89E+12 | 9.05E+07 | 1.78E+06 | 3.12E+02 | 8.50E+02 | 0. | 0. | 7.53E+03 | 2.00E+04 |
| 7.85E+08 | 7.13E+07 | 1.06E+09 | 1.33E+06 | 3.99E+06 | 1.08E+04 | 8.86E+05 | 8.60E+05 | 9.210E+03 | 2.05E+03 |
| 6.92E+07 | 4.77E+06 | 8.70E+01 | 4.95E+23 | 2.58E+20 | 9.26E+04 | 2.93E+05 | 1.54E+05 | 1.39E+05 | 5.27E+01 |

| | | | | | | | | | |
|-----------|------------|-----------|-----------|-----------|-----------|------------|-----------|-----------|-----------|
| 4.495E-04 | -7.741E-03 | 6.865E-14 | 9.166E+01 | 1.688E+03 | 2.397E+03 | 7.165E+04 | 1.000E+01 | 1.105E-28 | 4.751E+04 |
| 2.501E-01 | 1.626E-13 | 6.817E+07 | 1.087E+06 | 1.487E+02 | 6.701E+02 | 0. | 0. | 5.155E+03 | 1.408E+04 |
| 300.00 | 4.053E+07 | 6.440E+04 | 7.605E+05 | 7.752E+06 | 6.088E+03 | 7.000E+05 | 6.824E+05 | 3.567E+03 | 1.281E+03 |
| 5.179E+07 | 3.431E+06 | 4.488E-01 | 2.439E-26 | 8.342E-23 | 2.140E-04 | 2.523E+05 | 1.475E+05 | 1.487E+05 | 4.246E+01 |
| 3.479E-04 | -7.592E-05 | 5.016E-14 | 6.949E+01 | 1.777E+03 | 2.476E+03 | 6.8019E+04 | 1.000E+01 | 5.758E-32 | 1.830E+04 |
| 1.870E-01 | 3.517E-15 | 5.063E+07 | 6.536E+05 | 7.221E+01 | 5.355E+02 | 0. | 0. | 3.415E+03 | 1.085E+04 |
| 320.00 | 3.754E+04 | 3.087E+07 | 6.857E+04 | 4.723E+05 | 3.471E+03 | 6.334E+05 | 6.214E+05 | 2.184E+03 | 7.228E+02 |
| 3.749E+07 | 2.555E+06 | 2.313E-01 | 1.202E-29 | 2.746E-25 | 5.047E-05 | 2.917E+05 | 1.257E+05 | 7.599E+04 | 2.961E+01 |
| 2.655E-04 | -7.506E-05 | 3.737E-14 | 6.984E+01 | 1.755E+03 | 2.545E+03 | 6.511E+04 | 1.000E+01 | 2.999E-35 | 1.241E+04 |
| 1.425E-01 | 7.754E-17 | 3.710E+07 | 3.681E+05 | 3.554E+01 | 4.325E+02 | 0. | 0. | 2.139E+03 | 7.629E+03 |
| 340.00 | 2.844E+04 | 2.072E+07 | 5.583E+04 | 4.884E+05 | 2.015E+03 | 5.731E+05 | 5.650E+05 | 1.464E+03 | 4.154E+02 |
| 2.710E+07 | 1.870E+06 | 1.193E-01 | 5.925E-33 | 9.184E-28 | 1.209E-05 | 1.630E+05 | 1.077E+05 | 5.533E+04 | 2.032E+01 |
| 2.078E-04 | -7.041E-05 | 2.827E-14 | 7.347E+01 | 1.777E+03 | 2.665E+03 | 6.234E+04 | 1.000E+01 | 1.562E-38 | 6.545E+03 |
| 1.101E-01 | 1.736E-18 | 2.688E+07 | 2.279E+05 | 1.769E+01 | 3.521E+02 | 0. | 0. | 1.336E+03 | 5.405E+03 |
| 360.00 | 1.878E+04 | 1.404E+07 | 6.574E+04 | 3.171E+06 | 1.184E+03 | 5.731E+05 | 5.130E+05 | 8.687E+02 | 2.426E+02 |
| 1.942E+07 | 1.309E+06 | 6.146E-02 | 2.920E-36 | 3.111E-30 | 1.131E+05 | 1.311E+05 | 9.371E+04 | 4.040E+04 | 1.377E+01 |
| 1.641E-04 | -6.687E-05 | 2.167E-14 | 7.688E+01 | 1.793E+03 | 2.659E+03 | 5.968E+04 | 1.000E+01 | 4.137E-42 | 5.961E+03 |
| 6.813E-02 | 3.938E-20 | 1.929E+07 | 1.326E+05 | 8.886E+00 | 2.885E+02 | 0. | 0. | 8.423E+02 | 3.646E+03 |
| 380.00 | 1.344E+04 | 3.584E+06 | 3.766E+04 | 1.106E+05 | 3.013E+06 | 4.692E+05 | 4.654E+05 | 5.633E+02 | 1.437E+02 |
| 1.482E+07 | 1.002E+06 | 3.169E-02 | 1.439E-39 | 1.066E-32 | 1.097E-07 | 1.097E+05 | 8.014E+04 | 4.956E+04 | 9.240E+00 |
| 1.305E-04 | -6.302E-05 | 1.679E-14 | 8.005E+01 | 1.806E+03 | 2.703E+03 | 5.756E+04 | 1.000E+01 | 4.234E-45 | 4.205E+03 |
| 6.807E-02 | 9.034E-22 | 1.374E+07 | 7.666E+04 | 4.503E+00 | 2.375E+02 | 0. | 0. | 5.336E+02 | 2.742E+03 |
| 400.00 | 9.866E+07 | 6.584E+06 | 6.931E+04 | 2.868E+06 | 4.199E+02 | 4.246E+05 | 4.219E+05 | 3.714E+02 | 8.616E+01 |
| 9.789E+06 | 3.332E+05 | 1.633E-02 | 7.092E-43 | 3.686E-35 | 1.784E-07 | 9.116E+04 | 6.949E+04 | 2.147E+04 | 4.000E+00 |
| 1.047E-04 | -5.901E-05 | 1.314E-14 | 8.308E+01 | 1.816E+03 | 2.751E+03 | 5.549E+04 | 1.000E+01 | 2.208E-4 | 2.996E+03 |
| 5.427E-02 | 2.093E-23 | 9.745E+06 | 4.310E+04 | 2.301E+00 | 1.964E+02 | 0. | 0. | 3.394E+02 | 1.957E+03 |
| 6.996E+07 | 4.587E+06 | 2.582E+08 | 4.370E+04 | 2.733E+06 | 4.527E+02 | 3.842E+05 | 3.82E+05 | 2.489E+02 | 5.222E+01 |
| 6.909E+06 | 3.367E+05 | 8.423E-03 | 3.495E-46 | 1.286E-37 | 4.564E-08 | 7.634E+04 | 6.042E+04 | 1.591E+04 | 4.000E+00 |
| 8.443E-05 | -5.493E-05 | 1.037E-14 | 8.596E+01 | 1.823E+03 | 2.792E+03 | 5.358E+04 | 1.000E+01 | 1.150E-51 | 2.152E+03 |
| 4.359E-02 | 4.809E-25 | 6.683E+06 | 2.528E+04 | 1.185E+00 | 1.628E+02 | 0. | 0. | 2.166E+02 | 1.396E+03 |
| 5.070E+07 | 3.154E+06 | 2.147E+08 | 2.770E+04 | 2.606E+06 | 1.530E+02 | 3.476E+05 | 3.463E+05 | 1.692E+02 | 3.196E+01 |
| 4.864E+06 | 3.928E+05 | 4.342E-03 | 1.723E-49 | 4.521E-40 | 1.232E-08 | 6.436E+04 | 5.265E+04 | 1.171E+04 | 2.693E+00 |
| 6.888E-05 | -5.080E-05 | 8.249E-15 | 8.071E+01 | 1.879E+03 | 2.892E+03 | 5.182E+04 | 1.000E+01 | 5.990E-55 | 1.550E+03 |
| 3.575E-02 | 1.151E-26 | 4.850E+06 | 1.445E+04 | 6.140E-01 | 1.354E+02 | 0. | 0. | 1.307E+02 | 9.957E+02 |
| 3.692E+07 | 2.196E+06 | 1.789E+08 | 1.764E+04 | 2.488E+06 | 9.308E+02 | 3.145E+05 | 3.136E+05 | 1.666E+02 | 1.974E+01 |
| 3.419E+06 | 2.875E+05 | 2.238E-03 | 8.990E-53 | 1.600E-42 | 2.846E-09 | 5.460E+04 | 4.597E+04 | 8.629E+03 | 1.773E+00 |
| 5.583E-05 | -6.691E-05 | 6.606E-15 | 9.134E+01 | 1.834E+03 | 2.664E+03 | 5.020E+04 | 1.000E+01 | 3.120E-58 | 1.136E+03 |
| 2.867E-02 | 7.728E-28 | 3.411E+06 | 8.252E+03 | 3.211E-01 | 1.129E+02 | 0. | 0. | 8.907E+01 | 7.100E+02 |
| 480.00 | 2.697E+07 | 1.514E+06 | 1.494E+04 | 2.372E+06 | 1.508E+02 | 2.848E+05 | 2.840E+05 | 8.136E+02 | 1.229E+01 |
| 2.401E+06 | 2.184E+05 | 1.154E-03 | 4.184E-56 | 5.700E-45 | 7.262E-10 | 4.659E+04 | 4.021E+04 | 6.372E+03 | 1.165E+00 |
| 4.573E-05 | -4.308E-05 | 5.323E-13 | 9.386E+01 | 1.837E+03 | 2.987E+03 | 4.869E+04 | 1.000E+01 | 6.331E+02 | 3.311E+02 |
| 2.344E-02 | 6.506E-30 | 2.396E+06 | 4.706E+03 | 1.688E-01 | 9.425E+01 | 0. | 0. | 5.736E+01 | 5.063E+02 |
| 500.00 | 1.975E+07 | 1.075E+06 | 1.250E+04 | 2.272E+06 | 3.491E+02 | 2.575E+05 | 2.571E+05 | 5.748E+01 | 7.715E+00 |
| 1.684E+06 | 1.540E+05 | 5.949E-04 | 2.062E-59 | 2.062E-47 | 1.863E-10 | 3.995E+04 | 3.52E+04 | 4.714E+03 | 7.643E-01 |
| 3.782E-05 | -3.942E-05 | 4.313E-13 | 9.027E+01 | 1.840E+03 | 2.929E+03 | 4.728E+04 | 1.000E+01 | 6.465E-65 | 6.145E+02 |
| 1.925E-02 | 1.560E-31 | 1.682E+06 | 2.082E+03 | 8.973E-02 | 7.885E+01 | 0. | 0. | 3.704E+01 | 3.611E+02 |
| 520.00 | 1.450E+07 | 7.578E+05 | 1.047E+04 | 4.663E+04 | 2.150E+02 | 2.310E+05 | 2.327E+05 | 4.087E+01 | 4.876E+00 |
| 1.181E+06 | 1.127E+05 | 3.067E-04 | 1.016E-62 | 7.349E-50 | 4.605E-11 | 3.441E+04 | 3.091E+04 | 3.495E+03 | 5.011E-01 |

| | | | | | | | | | |
|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|-----------|
| 4.130e-02 | -3.276e-03 | 3.512e-13 | 7.150E+01 | 1.822E+03 | 2.960E+03 | 4.597E+04 | 1.000E+01 | 4.404E+08 | 4.555E+02 |
| 1.330E-02 | 3.762E-13 | 1.177E+06 | 1.527E+03 | 4.742E-02 | 6.607E+01 | 0. | 0. | 2.398E+01 | 2.577E+02 |
| 8.278E+05 | 5.270E+05 | 8.789E+07 | 3.033E+06 | 2.079E+06 | 1.774E+11 | 2.108E+05 | 2.106E+05 | 2.975E+01 | 3.103E+00 |
| 2.575E-05 | -2.272E-05 | 1.581E+04 | 5.008E-66 | 2.658E-52 | 1.245E-11 | 2.970E+04 | 2.717E+04 | 2.597E+01 | 3.288E-01 |
| 1.315E-02 | 9.110E-35 | 8.270E+05 | 1.008E+02 | 1.843E+01 | 4.984E+03 | 4.474E+04 | 1.000E+01 | 2.247E-71 | 2.393E+02 |
| 7.013E+00 | 3.762E-05 | 7.385E+07 | 1.953E+07 | 1.990E+06 | 5.544E+01 | 0. | 0. | 1.557E+01 | 1.640E+02 |
| 5.802E+05 | 6.039E+04 | 8.149E-05 | 2.460E-69 | 9.055E-55 | 3.235E-12 | 2.580E+04 | 2.591E+04 | 1.934E+03 | 1.988E+00 |
| 1.841E-05 | -2.970E-05 | 2.362E-15 | 1.079E-02 | 1.344E+03 | 3.017E+03 | 4.359E+04 | 1.000E+01 | 1.194E-74 | 2.538E+02 |
| 1.033E-02 | 2.210E-36 | 5.797E+05 | 4.949E+02 | 1.350E-02 | 4.658E+01 | 0. | 0. | 1.014E+01 | 1.315E+02 |
| 5.019E+00 | 4.064E+02 | 6.212E+07 | 1.269E+03 | 1.905E+06 | 5.177E+00 | 1.728E+05 | 1.725E+05 | 1.545E+01 | 1.281E+00 |
| 6.062E+05 | 4.420E+04 | 4.201E-05 | 1.216E-72 | 3.520E-57 | 9.460E-13 | 2.252E+04 | 2.107E+04 | 1.443E+03 | 1.411E-01 |
| 1.786E-05 | -2.689E-05 | 1.940E-15 | 1.049E+02 | 1.845E+03 | 3.044E+03 | 4.251E+04 | 1.000E+01 | 6.231E-78 | 1.906E+02 |
| 9.114E-03 | 5.410E-38 | 4.062E+05 | 2.017E+02 | 7.312E-03 | 3.918E+01 | 0. | 0. | 6.618E+00 | 9.411E+01 |
| 4.310E+06 | 1.890E+05 | 5.232E+07 | 8.271E+02 | 1.825E+06 | 1.200E+00 | 1.562E+05 | 1.561E+05 | 1.131E+01 | 8.304E-01 |
| 2.840E+05 | 3.235E+04 | 2.160E-05 | 5.995E-76 | 1.288E-59 | 2.210E-13 | 1.969E+04 | 1.861E+04 | 1.079E+03 | 9.255E-02 |
| 1.895E-05 | -2.431E-05 | 1.613E-15 | 1.060E+02 | 1.846E+03 | 3.071E+03 | 4.149E+04 | 1.000E+01 | 3.246E-01 | 1.436E+02 |
| 7.623E-03 | 1.326E-39 | 2.547E+05 | 1.603E+02 | 3.951E-03 | 3.300E+01 | 0. | 0. | 4.334E+00 | 6.743E+01 |
| 3.198E+06 | 1.344E+05 | 4.412E+07 | 5.405E+02 | 1.749E+06 | 2.002E+00 | 1.413E+05 | 1.414E+05 | 8.314E+00 | 5.415E-01 |
| 1.995E+05 | 2.360E+04 | 1.116E-05 | 2.955E-79 | 4.730E-62 | 5.833E-14 | 1.727E+04 | 1.646E+04 | 8.087E+02 | 6.077E-02 |
| 1.254E-05 | -2.194E-05 | 1.340E-15 | 1.087E+02 | 1.847E+03 | 3.075E+03 | 4.053E+04 | 1.000E+01 | 1.691E-84 | 1.006E+02 |
| 6.392E-03 | 3.260E-41 | 1.994E+05 | 9.120E+01 | 2.142E-03 | 2.783E+01 | 0. | 0. | 2.847E+00 | 4.837E+01 |
| 2.377E+06 | 9.592E+04 | 3.724E+07 | 3.542E+02 | 1.676E+06 | 1.257E+00 | 1.279E+05 | 1.270E+05 | 8.139E+00 | 3.551E-01 |
| 1.398E+05 | 1.733E+04 | 5.755E-06 | 1.456E-02 | 1.742E-64 | 1.539E-14 | 1.520E+04 | 1.459E+04 | 6.074E+02 | 3.995E-02 |
| 1.052E-05 | -1.970E-05 | 1.110E-15 | 1.105E+02 | 1.447E+03 | 3.122E+03 | 3.981E+04 | 1.000E+01 | 8.806E-88 | 9.236E+01 |
| 5.380E-03 | 8.039E-43 | 1.397E+05 | 5.189E+01 | 1.165E-03 | 2.349E+01 | 0. | 0. | 1.877E+00 | 3.476E+01 |
| 1.770E+06 | 6.843E+04 | 3.147E+07 | 2.326E+02 | 1.607E+06 | 7.911E-01 | 1.157E+05 | 1.157E+05 | 4.550E+00 | 2.342E-01 |
| 9.792E+04 | 1.269E+04 | 4.967E-06 | 7.170E-86 | 6.435E-67 | 4.072E-15 | 1.342E+04 | 1.297E+04 | 4.572E+02 | 2.631E-02 |
| 8.905E-06 | -1.781E-05 | 9.327E-16 | 1.122E+02 | 1.847E+03 | 3.146E+03 | 3.875E+04 | 1.000E+01 | 4.587E-91 | 6.265E-01 |
| 4.518E-03 | 1.988E-44 | 9.789E+04 | 2.953E+01 | 6.350E-04 | 1.985E+01 | 0. | 0. | 1.242E+00 | 2.581E+01 |
| 1.521E+06 | 4.897E+04 | 2.662E+07 | 1.532E+02 | 1.541E+06 | 4.993E-01 | 1.047E+05 | 1.047E+05 | 3.203E+00 | 1.553E-01 |
| 6.554E+04 | 9.285E+03 | 1.530E-06 | 3.537E-89 | 2.383E-69 | 1.080E-15 | 1.189E+04 | 1.155E+04 | 2.449E+02 | 1.736E-02 |
| 7.532E-06 | -1.601E-05 | 7.815E-16 | 1.139E+02 | 1.848E+03 | 3.170E+03 | 3.793E+04 | 1.000E+01 | 2.389E-94 | 4.770E+01 |
| 3.838E-03 | 4.931E-46 | 6.656E+04 | 1.680E+01 | 3.471E-04 | 1.679E+01 | 0. | 0. | 8.246E-01 | 1.803E+01 |
| 9.870E+05 | 3.511E+04 | 2.254E+07 | 1.011E+02 | 1.478E+06 | 1.160E-01 | 9.473E+04 | 9.473E+04 | 2.523E+00 | 1.036E-01 |
| 4.806E+04 | 6.796E+03 | 7.885E-07 | 1.743E-82 | 8.647E-72 | 7.658E-17 | 1.057E+04 | 1.031E+04 | 2.607E+02 | 1.140E-02 |
| 6.388E-06 | -1.439E-05 | 6.564E-16 | 1.155E+02 | 1.848E+03 | 3.194E+03 | 3.715E+04 | 1.000E+01 | 1.244E-97 | 3.653E+01 |
| 1.254E-03 | 1.226E-47 | 4.804E+04 | 9.550E+00 | 1.901E-04 | 1.422E+01 | 0. | 0. | 5.500E-01 | 1.301E+01 |
| 7.339E+05 | 2.522E+04 | 1.910E+07 | 6.694E+01 | 1.418E+06 | 2.005E-01 | 8.572E+04 | 8.571E+04 | 1.887E+00 | 6.954E-02 |
| 3.366E+04 | 4.974E+03 | 4.065E-07 | 8.90E-96 | 3.293E-74 | 7.658E-17 | 9.435E+04 | 9.233E+03 | 1.974E+02 | 7.610E-03 |
| 5.410E-06 | -1.192E-05 | 5.526E-16 | 1.170E+02 | 1.848E+03 | 3.217E+03 | 3.641E+04 | 1.000E+01 | 6.482E-101 | 2.800E+01 |
| 2.766E-03 | 3.055E-49 | 3.365E+04 | 5.436E+00 | 1.044E-04 | 1.205E+01 | 0. | 0. | 3.685E-01 | 9.409E+00 |
| 5.540E+05 | 1.015E+04 | 1.621E+07 | 4.439E+01 | 1.361E+06 | 1.276E-01 | 8.572E+04 | 8.571E+04 | 1.414E+00 | 4.695E-02 |
| 2.958E+04 | 3.641E+03 | 2.095E-07 | 4.233E-99 | 1.228E-76 | 2.046E-17 | 9.435E+04 | 8.571E+04 | 1.998E+02 | 5.062E-03 |
| 4.624E-06 | -1.159E-05 | 9.665E-16 | 1.145E+02 | 1.848E+03 | 3.403E+03 | 3.570E+04 | 1.000E+01 | 1.37E-104 | 4.150E+01 |
| 2.358E-03 | 7.631E-51 | 2.357E+04 | 3.094E+00 | 5.742E-05 | 1.022E+01 | 0. | 0. | 2.482E-01 | 6.815E+00 |
| 4.164E+05 | 1.304E+04 | 1.376E+07 | 2.511E+01 | 1.306E+06 | 8.130E-04 | 7.010E+04 | 7.010E+04 | 1.063E+00 | 3.191E-02 |
| 1.651E+04 | 2.665E+03 | 1.080E-07 | 2.08E-102 | 4.590E-79 | 5.470E-18 | 7.608E+03 | 7.494E+03 | 1.139E+02 | 3.379E-03 |

| | | | | | | | | | | |
|---------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 760.00 | 4.254E-06 | -1.040E-05 | 3.944E-16 | 1.700E+02 | 1.848E+03 | 3.262E+04 | 3.502E+04 | 1.000E+01 | 1.759-107 | 1.655E+01 |
| | 4.014E-03 | 1.410E-52 | 1.651E+04 | 1.760E+00 | 3.164E-05 | 6.674E+00 | 0. | 0. | 1.680E-01 | 4.944E+00 |
| | 3.110E+05 | 9.457E+03 | 1.170E+07 | 1.767E+01 | 1.254E+06 | 5.202E-02 | 6.350E+04 | 6.350E+04 | 6.000E-01 | 2.181E-02 |
| | 1.177E+04 | 1.937E+03 | 5.569E+08 | 1.028-105 | 1.719E-81 | 1.470E-18 | 6.792E+03 | 6.792E+03 | 6.67E+01 | 2.265E-03 |
| | 3.317E-06 | -9.317E-06 | 3.341E-16 | 1.215E+02 | 1.848E+03 | 3.284E+03 | 3.438E+04 | 1.000E+01 | 9.160-111 | 1.277E+01 |
| | 1.725E-03 | 4.790E-54 | 1.157E+04 | 1.001E+00 | 1.746E-05 | 7.377E+00 | 0. | 0. | 1.144E-01 | 3.593E+00 |
| 800.00 | 2.359E+05 | 6.847E+04 | 4.250E+06 | 1.314E+01 | 1.204E+06 | 4.335E-02 | 5.746E+04 | 5.746E+04 | 6.035E-01 | 1.504E-02 |
| | 6.103E+03 | 1.427E+03 | 2.871E+08 | 5.068-109 | 6.42E-84 | 3.952E-19 | 6.185E+03 | 6.185E+03 | 6.617E+01 | 1.525E-03 |
| | 2.908E-06 | -8.348E-06 | 2.637E-16 | 1.279E+02 | 1.848E+03 | 3.308E+03 | 3.378E+04 | 1.000E+01 | 4.771-114 | 9.866E+00 |
| | 1.481E-03 | 1.204E-55 | 8.103E+03 | 5.697E-01 | 9.652E-06 | 6.276E+00 | 0. | 0. | 7.844E-02 | 2.616E+00 |
| 820.00 | 1.780E+05 | 4.963E+03 | 6.473E+06 | 6.794E+00 | 1.157E+06 | 2.143E-02 | 5.199E+04 | 5.199E+04 | 4.561E-01 | 1.044E-02 |
| | 5.676E+03 | 1.045E+03 | 1.460E-06 | 2.497-112 | 2.42E-86 | 1.064E-19 | 5.712E+03 | 5.662E+03 | 5.057E+01 | 1.032E-03 |
| | 4.504E-08 | -7.476E-06 | 2.413E-16 | 1.244E+02 | 1.848E+03 | 3.327E+03 | 3.317E+04 | 1.000E+01 | 2.485-117 | 7.641E+00 |
| | 1.275E-03 | 3.031E-57 | 5.676E+03 | 3.241E-01 | 5.343E-06 | 5.344E+00 | 0. | 0. | 5.413E-02 | 1.907E+00 |
| 840.00 | 1.346E+05 | 3.605E+03 | 7.221E+06 | 5.900E+00 | 1.111E+06 | 1.381E-02 | 4.704E+04 | 4.704E+04 | 3.454E-01 | 7.304E-03 |
| | 3.978E+03 | 7.647E+02 | 1.623E-09 | 1.331-115 | 9.140E-89 | 2.872E-20 | 5.251E+04 | 5.212E+04 | 3.871E+01 | 7.029E-04 |
| | 2.162E-06 | -6.622E-06 | 2.057E-16 | 1.259E+02 | 1.648E+03 | 3.346E+03 | 3.280E+04 | 1.000E+01 | 1.294-120 | 5.928E+00 |
| | 1.101E-03 | 7.647E-59 | 3.976E+03 | 1.844E-01 | 2.961E-06 | 4.535E+00 | 0. | 0. | 3.763E-02 | 1.393E+00 |
| 860.00 | 1.019E+05 | 2.622E+03 | 6.160E+06 | 3.967E+00 | 1.068E+06 | 6.918E-03 | 4.257E+04 | 4.257E+04 | 2.620E-01 | 5.152E-03 |
| | 2.785E+03 | 5.97E+02 | 3.933E-09 | 6.066-119 | 3.450E-91 | 7.766E-21 | 4.857E+03 | 4.827E+03 | 2.944E+01 | 4.816E-04 |
| | 1.871E-06 | -5.989E-06 | 1.756E-16 | 1.274E+02 | 1.848E+03 | 3.369E+03 | 3.205E+04 | 1.000E+01 | 6.743-124 | 4.608E+00 |
| | 9.531E-04 | 1.933E-60 | 2.785E+03 | 1.049E-01 | 1.643E-06 | 3.885E+00 | 0. | 0. | 2.637E-02 | 1.619E+00 |
| 880.00 | 7.724E+04 | 1.912E+03 | 5.259E+06 | 2.674E+00 | 1.077E+06 | 5.774E-03 | 3.652E+04 | 3.652E+04 | 1.991E-01 | 3.665E-03 |
| | 1.367E+02 | 4.097E+02 | 2.027E-09 | 4.990-122 | 1.304E-93 | 2.104E-21 | 4.523E+03 | 4.500E+03 | 3.221E-04 | 3.321E-04 |
| | 1.624E-06 | -5.336E-06 | 1.502E-16 | 1.489E+02 | 1.848E+03 | 3.390E+03 | 3.153E+04 | 1.000E+01 | 3.512-127 | 3.588E+00 |
| | 4.273E-04 | 4.694E-82 | 1.951E+03 | 5.969E-02 | 9.129E-07 | 3.317E+00 | 0. | 0. | 1.863E-02 | 7.676E-01 |
| 900.00 | 5.466E+04 | 1.326E+03 | 4.494E+06 | 1.606E+00 | 9.871E+05 | 3.747E-03 | 3.485E+04 | 3.485E+04 | 1.515E-01 | 2.636E-03 |
| | 1.414E-06 | -4.791E-06 | 1.286E-16 | 1.304E+02 | 1.848E+03 | 3.410E+03 | 3.102E+04 | 1.000E+01 | 1.829-130 | 2.799E+00 |
| | 7.203E-04 | 1.241E-63 | 1.368E+03 | 3.396E-02 | 5.077E-07 | 2.635E+00 | 0. | 0. | 1.327E-02 | 5.483E-01 |
| 920.00 | 4.461E+04 | 1.022E+03 | 3.844E+06 | 1.222E+00 | 9.492E+05 | 2.437E-03 | 3.153E+04 | 3.153E+04 | 1.155E-01 | 1.904E-03 |
| | 9.572E+02 | 2.195E+02 | 5.388E-10 | 7.261-129 | 1.876E-98 | 1.552E-22 | 4.005E+03 | 3.991E+03 | 1.351E+01 | 1.615E-04 |
| | 1.235E-06 | -4.283E-06 | 1.106E-16 | 1.320E+02 | 1.848E+03 | 3.430E+03 | 3.054E+04 | 1.000E+01 | 9.529-134 | 2.188E+00 |
| | 6.289E-04 | 3.155E-65 | 9.572E+02 | 1.932E-02 | 2.826E-07 | 2.424E+00 | 0. | 0. | 5.942E-03 | 4.632E-01 |
| 940.00 | 3.398E+04 | 7.482E+02 | 3.290E+06 | 4.490E-01 | 9.130E+05 | 1.656E-03 | 2.653E+04 | 2.653E+04 | 4.817E-02 | 1.391E-03 |
| | 6.705E+02 | 1.606E+02 | 2.778E-10 | 3.578-132 | 7.132-101 | 4.277E-23 | 3.609E+03 | 3.796E+03 | 1.042E+01 | 1.139E-04 |
| | 1.082E-06 | -4.827E-06 | 9.510E-17 | 1.377E+02 | 1.848E+03 | 3.449E+03 | 3.007E+04 | 1.000E+01 | 4.963-137 | 1.713E+00 |
| | 5.509E-04 | 6.034E-67 | 6.705E+02 | 1.099E-02 | 1.575E-07 | 2.075E+00 | 0. | 0. | 6.921E-03 | 2.969E-01 |
| 960.00 | 2.592E+04 | 5.494E+02 | 2.819E+06 | 5.635E-01 | 8.784E+05 | 1.039E-03 | 2.582E+04 | 2.582E+04 | 6.742E-02 | 1.028E-03 |
| | 4.937E+02 | 1.176E+02 | 1.432E-10 | 1.764-135 | 2.717-103 | 1.154E-24 | 3.646E+03 | 3.640E+03 | 6.053E+00 | 6.697E-05 |
| | 9.568E-07 | -3.418E-06 | 8.197E-17 | 1.354E+02 | 1.848E+03 | 3.469E+03 | 2.962E+04 | 1.000E+01 | 2.545-140 | 1.344E+00 |
| | 4.840E-04 | 2.049E-68 | 4.697E+02 | 6.254E-03 | 8.783E-08 | 1.778E+00 | 0. | 0. | 5.066E-03 | 2.190E-01 |
| 980.00 | 1.940E+04 | 3.046E+02 | 2.417E+06 | 3.016E-01 | 8.452E+05 | 6.804E-04 | 2.336E+04 | 2.336E+04 | 5.163E-02 | 7.630E-04 |
| | 3.470E+02 | 6.005E+01 | 7.381E-11 | 6.927-139 | 1.377-105 | 3.194E-24 | 3.519E+03 | 3.513E+03 | 6.231E+00 | 5.802E-05 |
| | 6.376E-07 | -4.051E-06 | 7.076E-17 | 1.372E+02 | 1.848E+03 | 3.486E+03 | 2.591E+04 | 1.000E+01 | 1.347-143 | 1.656E+00 |
| | 4.267E-04 | 5.216E-70 | 3.290E+02 | 3.556E-03 | 4.902E-08 | 1.525E+00 | 0. | 0. | 3.741E-03 | 1.618E-01 |
| 1000.00 | 1.515E+04 | 2.275E+02 | 2.074E+06 | 2.020E-01 | 8.135E+05 | 4.408E-04 | 2.114E+04 | 2.114E+04 | 3.959E-02 | 5.726E-04 |
| | 2.304E+02 | 6.229E+01 | 3.805E-11 | 4.784-142 | 3.966-108 | 6.641E-25 | 3.417E+03 | 3.412E+03 | 4.678E+00 | 4.191E-05 |

| | | | | | | | | | |
|-----------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 7.410E-07 | -2.72E-06 | 9.124E-17 | 1.391E+02 | 1.699E+03 | 1.507E+03 | 2.877E+04 | 1.000E+01 | 7.014-14/ | 6.221E-01 |
| 3.774E-04 | 1.341E-71 | 2.304E+02 | 2.024E-03 | 2.738E-08 | 1.308E+00 | 0. | 0. | 2.787E-03 | 1.198E-01 |
| 1040.00 | 8.307E+03 | 1.533E+06 | 1.428E-01 | 7.540E+05 | 1.919E-04 | 1.731E+04 | 1.731E+04 | 2.449E-04 | 1.404E-04 |
| | 1.131E+02 | 1.011E-11 | 1.040-148 | 5.836-113 | 6.525E-26 | 3.278E+03 | 3.275E+03 | 2.911E+00 | 2.238E-05 |
| | 5.806E-07 | -2.162E-06 | 4.612E-17 | 1.432E+02 | 1.699E+03 | 2.797E+04 | 1.000E+01 | 1.903-153 | 5.193E-01 |
| | 2.983E-04 | 6.852E-75 | 6.552E-04 | 8.562E-09 | 9.660E-01 | 0. | 0. | 1.587E-03 | 6.590E-02 |
| 1080.00 | 5.466E+03 | 8.897E+01 | 1.134E+06 | 5.805E-02 | 6.995E+05 | 1.417E+04 | 1.417E+04 | 1.389E-02 | 1.964E-04 |
| | 2.588E+01 | 1.807E+01 | 2.887E-12 | 2.577-155 | 8.062-118 | 4.970E-27 | 1.201E+03 | 1.765E+00 | 1.232E-05 |
| | 4.694E-07 | -1.713E-06 | 3.504E-17 | 1.479E+02 | 1.849E+03 | 2.722E+04 | 1.000E+01 | 5.163-160 | 3.269E-01 |
| | 2.391E-04 | 5.892E-78 | 2.121E-04 | 2.884E-09 | 7.155E-01 | 0. | 0. | 9.311E-04 | 3.649E-62 |
| 1120.00 | 3.131E+03 | 4.913E+01 | 8.430E+05 | 2.766E-02 | 6.494E+05 | 1.160E+04 | 1.160E+04 | 8.300E-03 | 1.198E-04 |
| | 2.724E+01 | 9.682E+00 | 7.144E-13 | 6.134-162 | 1.297-122 | 3.166E+03 | 3.165E+03 | 1.075E+00 | 6.975E-06 |
| | 1.817E-07 | -1.352E-06 | 2.686E-17 | 1.533E+02 | 1.849E+03 | 1.616E+03 | 1.000E+01 | 1.401-164 | 2.076E-01 |
| | 1.944E-04 | 3.957E-81 | 2.722E+01 | 8.864E-05 | 8.432E-19 | 0. | 0. | 5.610E-04 | 2.033E-02 |
| 1160.00 | 1.872E+03 | 2.730E+01 | 6.284E+05 | 1.224E-02 | 6.034E+05 | 1.672E-05 | 9.498E+03 | 4.986E-03 | 7.456E-05 |
| | 1.336E+01 | 5.187E+00 | 1.898E-13 | 1.491-168 | 1.962-127 | 2.965E-29 | 3.137E+03 | 6.587E-01 | 4.074E-06 |
| | 3.149E-07 | -1.062E-06 | 2.079E-17 | 1.594E+02 | 1.849E+03 | 1.651E+03 | 1.000E+01 | 3.800-173 | 1.332E-01 |
| | 1.804E-04 | 2.684E-84 | 1.338E+01 | 2.222E-05 | 2.655E-10 | 4.963E-01 | 0. | 1.455E-04 | 1.140E-02 |
| 1200.00 | 1.125E+03 | 1.526E+01 | 4.699E+05 | 6.424E-03 | 5.611E+05 | 7.516E-06 | 7.776E+03 | 1.011E-03 | 4.719E-05 |
| | 6.554E+00 | 2.779E+00 | 5.044E-14 | 3.621-175 | 2.999-132 | 2.325E-30 | 3.889E+03 | 4.056E-01 | 2.476E-06 |
| | 2.834E-07 | -8.499E-07 | 1.627E-17 | 1.066E+02 | 1.847E+03 | 3.686E+03 | 1.000E+01 | 1.031-179 | 8.633E-02 |
| | 1.362E-04 | 1.839E-87 | 6.554E+00 | 7.192E-06 | 8.373E-11 | 2.964E-01 | 0. | 2.166E-04 | 6.427E-03 |

END OF TEST PROGRAM

TEST VALUES HEAD IN
 BALTS = 102

| I | ALTS(I),AM | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 | 101 | 102 | 103 | 104 | 105 | 106 | 107 | 108 | 109 | 110 | 111 | 112 | 113 | 114 | 115 | 116 | 117 | 118 | 119 | 120 | 121 | 122 | 123 | 124 | 125 | 126 | 127 | 128 | 129 | 130 | 131 | 132 | 133 | 134 | 135 | 136 | 137 | 138 | 139 | 140 | 141 | 142 | 143 | 144 | 145 | 146 | 147 | 148 | 149 | 150 | 151 | 152 | 153 | 154 | 155 | 156 | 157 | 158 | 159 | 160 | 161 | 162 | 163 | 164 | 165 | 166 | 167 | 168 | 169 | 170 | 171 | 172 | 173 | 174 | 175 | 176 | 177 | 178 | 179 | 180 | 181 | 182 | |
|---|------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 1 | 0.00 | 1.00 | 2.00 | 3.00 | 4.00 | 5.00 | 6.00 | 7.00 | 8.00 | 9.00 | 10.00 | 11.00 | 12.00 | 13.00 | 14.00 | 15.00 | 16.00 | 17.00 | 18.00 | 19.00 | 20.00 | 21.00 | 22.00 | 23.00 | 24.00 | 25.00 | 26.00 | 27.00 | 28.00 | 29.00 | 30.00 | 31.00 | 32.00 | 33.00 | 34.00 | 35.00 | 36.00 | 37.00 | 38.00 | 39.00 | 40.00 | 41.00 | 42.00 | 43.00 | 44.00 | 45.00 | 46.00 | 47.00 | 48.00 | 49.00 | 50.00 | 51.00 | 52.00 | 53.00 | 54.00 | 55.00 | 56.00 | 57.00 | 58.00 | 59.00 | 60.00 | 61.00 | 62.00 | 63.00 | 64.00 | 65.00 | 66.00 | 67.00 | 68.00 | 69.00 | 70.00 | 71.00 | 72.00 | 73.00 | 74.00 | 75.00 | 76.00 | 77.00 | 78.00 | 79.00 | 80.00 | 81.00 | 82.00 | 83.00 | 84.00 | 85.00 | 86.00 | 87.00 | 88.00 | 89.00 | 90.00 | 91.00 | 92.00 | 93.00 | 94.00 | 95.00 | 96.00 | 97.00 | 98.00 | 99.00 | 100.00 | 101.00 | 102.00 | 103.00 | 104.00 | 105.00 | 106.00 | 107.00 | 108.00 | 109.00 | 110.00 | 111.00 | 112.00 | 113.00 | 114.00 | 115.00 | 116.00 | 117.00 | 118.00 | 119.00 | 120.00 | 121.00 | 122.00 | 123.00 | 124.00 | 125.00 | 126.00 | 127.00 | 128.00 | 129.00 | 130.00 | 131.00 | 132.00 | 133.00 | 134.00 | 135.00 | 136.00 | 137.00 | 138.00 | 139.00 | 140.00 | 141.00 | 142.00 | 143.00 | 144.00 | 145.00 | 146.00 | 147.00 | 148.00 | 149.00 | 150.00 | 151.00 | 152.00 | 153.00 | 154.00 | 155.00 | 156.00 | 157.00 | 158.00 | 159.00 | 160.00 | 161.00 | 162.00 | 163.00 | 164.00 | 165.00 | 166.00 | 167.00 | 168.00 | 169.00 | 170.00 | 171.00 | 172.00 | 173.00 | 174.00 | 175.00 | 176.00 | 177.00 | 178.00 | 179.00 | 180.00 | 181.00 | 182.00 |

ITRS = 79 ITHMS = 7 IDAYS = 2
 IT = 0. HMS = .5500E+02 DEG GLO = .2400E+03 DEG
 WPLAG = 0.00 METHOD = 0 TPLAG = 0.00

INITIALIZATION CALL

FROM SUBROUTINE WATER- IR = 3 FWR = .49803 PST = .99726
 TTP = 1330.012 DEG K, TAU = 2.13691E-02 1/KR, FROM SUBROUTINE ATMOSU (FUNMAT 8001)

ITRS = 79 ITHMS = 7 IDAYS = 7
 IT = 0. HMS = .9592E+00 RAD GLO = .4189E+01 RAD

IDORN = -1 UP = .H000E+01 GAP = .7343E+01 PLAT = .1109E+00 PLUM = .4189E+01

| | | | | | | | | | | | |
|-------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 45.00 | 1.974E+03 | -2.153E-03 | 5.541E-06 | 7.397E+00 | 4.643E+02 | 2.043E+02 | 1.000E+00 | 2.109E+00 | 2.866E+00 | 2.146E+05 | 2.977E+09 |
| | 1.972E+08 | 2.132E+10 | 3.030E+03 | 6.797E-08 | 6.797E-10 | 1.000E+00 | 3.128E+00 | 2.714E-04 | 0. | 0. | 0. |
| | 3.000E+16 | 3.760E+15 | 1.100E+00 | 4.160E+14 | 2.140E+12 | 1.481E+13 | 0. | 0. | 0. | 0. | 4.450E-01 |
| | 3.504E+03 | 1.000E+00 | 8.783E+08 | 3.400E+00 | 2.369E+11 | 2.018E+11 | 0. | 0. | 0. | 0. | 0. |
| | 1.694E+03 | -2.252E-03 | 2.273E-06 | 7.374E+00 | 2.656E+02 | 2.656E+02 | 1.000E+00 | 3.511E+00 | 2.363E+05 | 2.434E+05 | 2.969E+09 |
| | 1.374E+09 | 1.674E+10 | 4.504E+03 | 6.166E-06 | 8.166E-10 | 1.000E+00 | 2.109E-04 | 0. | 0. | 0. | 0. |
| 46.00 | 1.165E+16 | 3.585E+15 | 1.100E+00 | 3.652E+14 | 1.877E+12 | 1.270E+13 | 0. | 0. | 0. | 0. | 3.893E-01 |
| | 4.045E+03 | 1.000E+00 | 7.783E+08 | 3.400E+00 | 1.939E+11 | 1.760E+11 | 0. | 0. | 0. | 0. | 0. |
| | 1.436E+03 | -2.362E-03 | 1.951E-06 | 7.651E+00 | 2.671E+02 | 2.671E+02 | 1.000E+00 | 3.887E+00 | 6.130E+05 | 2.764E+05 | 2.865E+09 |
| | 9.247E+07 | 1.307E+10 | 4.045E+03 | 9.811E-08 | 9.811E-10 | 1.000E+00 | 1.670E-04 | 0. | 0. | 0. | 0. |
| 47.00 | 2.774E+16 | 7.510E+15 | 1.100E+00 | 3.670E+14 | 1.646E+12 | 1.140E+13 | 0. | 0. | 0. | 0. | 3.407E-01 |
| | 4.639E+03 | 1.000E+00 | 6.923E+08 | 3.400E+00 | 1.577E+11 | 1.533E+11 | 0. | 0. | 0. | 0. | 0. |
| | 1.319E+03 | -2.466E-03 | 1.713E-06 | 7.727E+00 | 2.622E+02 | 2.622E+02 | 1.000E+00 | 4.242E+00 | 5.682E+05 | 3.137E+05 | 2.439E+09 |
| | 6.275E+07 | 1.015E+10 | 4.669E+03 | 1.179E-07 | 1.179E-09 | 1.000E+00 | 1.340E-04 | 0. | 0. | 0. | 0. |
| 48.00 | 2.443E+16 | 6.603E+15 | 1.100E+00 | 2.919E+14 | 1.449E+12 | 1.002E+13 | 0. | 0. | 0. | 0. | 2.981E-01 |
| | 5.194E+03 | 1.000E+00 | 6.177E+08 | 3.400E+00 | 1.275E+11 | 1.336E+11 | 0. | 0. | 0. | 0. | 0. |
| | 1.164E+03 | -2.575E-03 | 1.506E-06 | 7.604E+00 | 2.622E+02 | 2.622E+02 | 1.000E+00 | 4.557E+00 | 7.707E+05 | 3.554E+05 | 2.228E+09 |
| | 4.243E+07 | 7.852E+09 | 5.389E+03 | 1.416E-07 | 1.416E-09 | 1.000E+00 | 1.091E-04 | 0. | 0. | 0. | 0. |
| 49.00 | 2.151E+16 | 5.810E+15 | 1.100E+00 | 2.482E+14 | 1.275E+12 | 8.824E+12 | 0. | 0. | 0. | 0. | 2.808E-01 |
| | 6.271E+03 | 1.000E+00 | 5.524E+08 | 3.400E+00 | 1.074E+11 | 1.165E+11 | 0. | 0. | 0. | 0. | 0. |
| | 1.026E+03 | -2.688E-03 | 1.222E-06 | 7.561E+00 | 2.622E+02 | 2.622E+02 | 1.000E+00 | 4.814E+00 | 1.024E+06 | 4.014E+05 | 2.048E+09 |
| | 2.854E+07 | 6.050E+09 | 6.221E+03 | 1.701E-07 | 1.701E-09 | 1.000E+00 | 9.021E-05 | 0. | 0. | 0. | 0. |
| 50.00 | 1.896E+16 | 5.120E+15 | 1.100E+00 | 2.187E+14 | 1.124E+12 | 7.777E+12 | 0. | 0. | 0. | 0. | 2.282E-01 |
| | 7.190E+03 | 1.000E+00 | 4.947E+08 | 3.400E+00 | 8.167E+10 | 1.015E+11 | 0. | 0. | 0. | 0. | 0. |
| | 9.072E+02 | -2.799E-03 | 1.169E-06 | 7.455E+00 | 2.704E+02 | 2.704E+02 | 1.000E+00 | 1.000E+00 | 1.449E+06 | 4.509E+05 | 1.696E+09 |
| | 1.905E+07 | 4.648E+09 | 7.180E+03 | 2.044E-07 | 2.044E-09 | 1.000E+00 | 4.993E+00 | 4.856E+00 | 0. | 0. | 0. |
| 51.00 | 1.673E+16 | 4.529E+15 | 1.100E+00 | 1.930E+14 | 9.918E+11 | 6.862E+12 | 0. | 0. | 0. | 0. | 1.996E-01 |
| | 8.286E+03 | 3.214E+03 | 4.437E+08 | 3.400E+00 | 6.475E+10 | 8.832E+10 | 0. | 0. | 0. | 0. | 0. |
| | 8.012E+02 | -2.896E-03 | 1.031E-06 | 8.030E+00 | 2.706E+02 | 2.706E+02 | 1.000E+00 | 1.736E+06 | 5.031E+05 | 1.768E+09 | 0. |
| | 1.255E+07 | 3.562E+09 | 8.286E+03 | 2.455E-07 | 2.455E-09 | 1.000E+00 | 8.501E-05 | 0. | 0. | 0. | 0. |
| 52.00 | 1.476E+16 | 3.947E+15 | 1.100E+00 | 1.705E+14 | 8.762E+11 | 6.062E+12 | 0. | 0. | 0. | 0. | 1.747E-01 |
| | 9.566E+03 | 2.941E+02 | 3.979E+08 | 3.400E+00 | 5.102E+10 | 7.684E+10 | 0. | 0. | 0. | 0. | 0. |
| | 7.076E+02 | -3.001E-03 | 9.110E-07 | 8.103E+00 | 2.706E+02 | 2.706E+02 | 1.000E+00 | 2.190E+06 | 5.565E+05 | 1.663E+09 | 0. |
| | 8.104E+06 | 2.772E+09 | 9.566E+03 | 2.950E-07 | 2.950E-09 | 1.000E+00 | 5.054E+00 | 4.924E+00 | 0. | 0. | 0. |
| 53.00 | 1.307E+16 | 3.539E+15 | 1.100E+00 | 1.506E+14 | 7.748E+11 | 5.361E+12 | 0. | 0. | 0. | 0. | 1.528E-01 |
| | 1.104E+04 | 1.364E+03 | 3.567E+08 | 3.400E+00 | 3.997E+10 | 6.818E+10 | 0. | 0. | 0. | 0. | 0. |
| | 6.249E+02 | -3.102E-03 | 8.059E-07 | 8.172E+00 | 2.702E+02 | 2.702E+02 | 1.000E+00 | 2.702E+06 | 6.088E+05 | 1.579E+09 | 0. |
| | 5.077E+06 | 2.062E+09 | 1.104E+04 | 3.543E-07 | 3.543E-09 | 1.000E+00 | 4.916E+00 | 4.772E+00 | 0. | 0. | 0. |
| 54.00 | 1.157E+16 | 3.124E+15 | 1.100E+00 | 1.335E+14 | 6.859E+11 | 4.746E+12 | 0. | 0. | 0. | 0. | 1.337E-01 |
| | 1.274E+04 | 4.206E+03 | 3.192E+08 | 3.400E+00 | 3.214E+10 | 5.804E+10 | 0. | 0. | 0. | 0. | 0. |
| | 5.316E+02 | -3.206E-03 | 7.134E+07 | 8.236E+00 | 2.692E+02 | 2.692E+02 | 1.000E+00 | 3.264E+06 | 6.576E+05 | 1.514E+09 | 0. |
| | 3.042E+06 | 1.541E+09 | 1.274E+04 | 4.257E-07 | 4.257E-09 | 1.000E+00 | 4.665E+00 | 4.497E+00 | 0. | 0. | 0. |
| 55.00 | 1.025E+16 | 2.724E+15 | 1.100E+00 | 1.143E+14 | 6.074E+11 | 4.205E+12 | 0. | 0. | 0. | 0. | 1.170E-01 |
| | 1.471E+04 | 9.242E+03 | 2.844E+08 | 3.400E+00 | 2.458E+10 | 0. | 0. | 0. | 0. | 0. | 0. |
| | 4.870E+02 | -3.303E-03 | 6.320E-07 | 8.299E+00 | 2.684E+02 | 2.684E+02 | 1.000E+00 | 4.054E+06 | 6.999E+05 | 1.466E+09 | 0. |
| | 1.710E+06 | 1.216E+09 | 1.471E+04 | 5.114E-07 | 5.114E-09 | 1.000E+00 | 4.331E-05 | 0. | 0. | 0. | 0. |
| 56.00 | 9.070E+15 | 2.459E+15 | 1.100E+00 | 1.049E+14 | 5.390E+11 | 3.729E+12 | 0. | 0. | 0. | 0. | 1.024E-01 |
| | 1.696E+04 | 1.964E+04 | 2.416E+08 | 3.400E+00 | 2.148E+10 | 4.369E+10 | 0. | 0. | 0. | 0. | 0. |

| | | | | | | | | | | | | | | | | |
|-------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 69.00 | 3.562E+05 | 5.540E+01 | 5.113E-03 | 9.479E+04 | 1.313E-07 | 1.019E+00 | 2.250E+02 | 5.544E-06 | 2.250E+02 | 1.000E+00 | 2.250E+02 | 1.000E+00 | 5.540E+01 | 5.113E-02 | 1.275E+06 | 4.234E+09 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.701E+05 | 1.701E+05 | 2.100E+13 | 7.709E+11 | 7.709E+11 | 7.709E+11 | 7.709E+11 | 7.709E+11 | 7.709E+11 | 7.709E+11 | 7.709E+11 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 8.485E+06 | 8.485E+06 | 1.409E+09 | 7.527E+09 | 7.527E+09 | 7.527E+09 | 7.527E+09 | 7.527E+09 | 7.527E+09 | 7.527E+09 | 7.527E+09 | 0. | 4.252E-02 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.159E-07 | 1.159E-07 | 7.050E+00 | 2.210E-02 | 2.210E-02 | 2.210E-02 | 2.210E-02 | 2.210E-02 | 2.210E-02 | 2.210E-02 | 2.210E-02 | 1.697E+06 | 4.399E+09 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.094E+05 | 1.094E+05 | 6.658E-06 | 6.658E-08 | 6.658E-08 | 6.658E-08 | 6.658E-08 | 6.658E-08 | 6.658E-08 | 6.658E-08 | 6.658E-08 | 3.026E-02 | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 4.455E+14 | 4.455E+14 | 1.900E+13 | 9.765E+10 | 9.765E+10 | 9.765E+10 | 9.765E+10 | 9.765E+10 | 9.765E+10 | 9.765E+10 | 9.765E+10 | 0. | 4.092E-02 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 6.311E+01 | 6.311E+01 | 3.100E+00 | 5.477E+09 | 5.477E+09 | 5.477E+09 | 5.477E+09 | 5.477E+09 | 5.477E+09 | 5.477E+09 | 5.477E+09 | 4.650E+06 | 2.575E+09 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 2.743E+05 | 2.743E+05 | 7.990E-06 | 7.990E-08 | 7.990E-08 | 7.990E-08 | 7.990E-08 | 7.990E-08 | 7.990E-08 | 7.990E-08 | 7.990E-08 | 1.688E-02 | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.439E+15 | 1.439E+15 | 1.660E+13 | 8.531E+10 | 8.531E+10 | 8.531E+10 | 8.531E+10 | 8.531E+10 | 8.531E+10 | 8.531E+10 | 8.531E+10 | 0. | 3.939E-02 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.457E+05 | 1.457E+05 | 3.372E+06 | 3.876E+09 | 3.876E+09 | 3.876E+09 | 3.876E+09 | 3.876E+09 | 3.876E+09 | 3.876E+09 | 3.876E+09 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 5.400E+01 | 5.400E+01 | 7.318E+00 | 2.120E+02 | 2.120E+02 | 2.120E+02 | 2.120E+02 | 2.120E+02 | 2.120E+02 | 2.120E+02 | 2.120E+02 | 3.257E+06 | 4.759E+09 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 2.398E+05 | 2.398E+05 | 9.604E-06 | 9.604E-08 | 9.604E-08 | 9.604E-08 | 9.604E-08 | 9.604E-08 | 9.604E-08 | 9.604E-08 | 9.604E-08 | 9.267E-03 | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.253E+15 | 1.253E+15 | 1.446E+13 | 7.429E+10 | 7.429E+10 | 7.429E+10 | 7.429E+10 | 7.429E+10 | 7.429E+10 | 7.429E+10 | 7.429E+10 | 0. | 3.791E-02 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.081E+05 | 1.081E+05 | 2.062E+01 | 2.735E+09 | 2.735E+09 | 2.735E+09 | 2.735E+09 | 2.735E+09 | 2.735E+09 | 2.735E+09 | 2.735E+09 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 4.605E+01 | 4.605E+01 | 7.140E+00 | 2.076E+02 | 2.076E+02 | 2.076E+02 | 2.076E+02 | 2.076E+02 | 2.076E+02 | 2.076E+02 | 2.076E+02 | 4.513E+06 | 2.946E+09 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 2.089E+05 | 2.089E+05 | 1.153E-05 | 1.153E-07 | 1.153E-07 | 1.153E-07 | 1.153E-07 | 1.153E-07 | 1.153E-07 | 1.153E-07 | 1.153E-07 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.047E+15 | 1.047E+15 | 1.444E+07 | 6.446E+10 | 6.446E+10 | 6.446E+10 | 6.446E+10 | 6.446E+10 | 6.446E+10 | 6.446E+10 | 6.446E+10 | 0. | 3.649E-02 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.940E+05 | 1.940E+05 | 7.448E+01 | 1.922E+09 | 1.922E+09 | 1.922E+09 | 1.922E+09 | 1.922E+09 | 1.922E+09 | 1.922E+09 | 1.922E+09 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 3.914E+01 | 3.914E+01 | 6.960E+00 | 2.034E+02 | 2.034E+02 | 2.034E+02 | 2.034E+02 | 2.034E+02 | 2.034E+02 | 2.034E+02 | 2.034E+02 | 3.625E+06 | 3.130E+09 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.812E+05 | 1.812E+05 | 1.185E-05 | 1.185E-07 | 1.185E-07 | 1.185E-07 | 1.185E-07 | 1.185E-07 | 1.185E-07 | 1.185E-07 | 1.185E-07 | 5.031E-03 | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 9.399E+14 | 9.399E+14 | 1.799E+08 | 5.573E+10 | 5.573E+10 | 5.573E+10 | 5.573E+10 | 5.573E+10 | 5.573E+10 | 5.573E+10 | 5.573E+10 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 2.718E+05 | 2.718E+05 | 2.044E+02 | 1.346E+09 | 1.346E+09 | 1.346E+09 | 1.346E+09 | 1.346E+09 | 1.346E+09 | 1.346E+09 | 1.346E+09 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.567E+05 | 1.567E+05 | 7.811E-08 | 1.993E-02 | 1.993E-02 | 1.993E-02 | 1.993E-02 | 1.993E-02 | 1.993E-02 | 1.993E-02 | 1.993E-02 | 8.662E+06 | 3.366E+09 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.091E+07 | 1.091E+07 | 1.664E-05 | 1.664E-07 | 1.664E-07 | 1.664E-07 | 1.664E-07 | 1.664E-07 | 1.664E-07 | 1.664E-07 | 1.664E-07 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 2.542E+14 | 2.542E+14 | 1.048E+12 | 4.793E+10 | 4.793E+10 | 4.793E+10 | 4.793E+10 | 4.793E+10 | 4.793E+10 | 4.793E+10 | 4.793E+10 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 4.594E+05 | 4.594E+05 | 5.811E+02 | 9.311E+08 | 9.311E+08 | 9.311E+08 | 9.311E+08 | 9.311E+08 | 9.311E+08 | 9.311E+08 | 9.311E+08 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 2.800E+01 | 2.800E+01 | 6.041E+00 | 1.955E+02 | 1.955E+02 | 1.955E+02 | 1.955E+02 | 1.955E+02 | 1.955E+02 | 1.955E+02 | 1.955E+02 | 3.313E+06 | 3.466E+09 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.349E+05 | 1.349E+05 | 1.998E-05 | 1.998E-07 | 1.998E-07 | 1.998E-07 | 1.998E-07 | 1.998E-07 | 1.998E-07 | 1.998E-07 | 1.998E-07 | 7.961E-04 | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 6.943E+14 | 6.943E+14 | 8.011E+12 | 4.117E+10 | 4.117E+10 | 4.117E+10 | 4.117E+10 | 4.117E+10 | 4.117E+10 | 4.117E+10 | 4.117E+10 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.092E+05 | 1.092E+05 | 1.011E+03 | 5.246E+08 | 5.246E+08 | 5.246E+08 | 5.246E+08 | 5.246E+08 | 5.246E+08 | 5.246E+08 | 5.246E+08 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 4.274E-03 | 4.274E-03 | 6.435E+00 | 1.915E+02 | 1.915E+02 | 1.915E+02 | 1.915E+02 | 1.915E+02 | 1.915E+02 | 1.915E+02 | 1.915E+02 | 4.376E-04 | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 8.689E+06 | 8.689E+06 | 2.400E-05 | 2.400E-07 | 2.400E-07 | 2.400E-07 | 2.400E-07 | 2.400E-07 | 2.400E-07 | 2.400E-07 | 2.400E-07 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.875E+14 | 1.875E+14 | 6.095E+09 | 3.517E+10 | 3.517E+10 | 3.517E+10 | 3.517E+10 | 3.517E+10 | 3.517E+10 | 3.517E+10 | 3.517E+10 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 2.761E+06 | 2.761E+06 | 4.565E+03 | 4.430E+08 | 4.430E+08 | 4.430E+08 | 4.430E+08 | 4.430E+08 | 4.430E+08 | 4.430E+08 | 4.430E+08 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.978E+01 | 1.978E+01 | 3.657E-04 | 1.884E+02 | 1.884E+02 | 1.884E+02 | 1.884E+02 | 1.884E+02 | 1.884E+02 | 1.884E+02 | 1.884E+02 | 2.453E+06 | 3.797E+09 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 4.043E+06 | 4.043E+06 | 1.418E+05 | 2.682E-07 | 2.682E-07 | 2.682E-07 | 2.682E-07 | 2.682E-07 | 2.682E-07 | 2.682E-07 | 2.682E-07 | 2.450E-04 | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 5.040E+14 | 5.040E+14 | 5.823E+12 | 2.992E+10 | 2.992E+10 | 2.992E+10 | 2.992E+10 | 2.992E+10 | 2.992E+10 | 2.992E+10 | 2.992E+10 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.410E+05 | 1.410E+05 | 1.277E+04 | 1.234E+08 | 1.234E+08 | 1.234E+08 | 1.234E+08 | 1.234E+08 | 1.234E+08 | 1.234E+08 | 1.234E+08 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.978E+01 | 1.978E+01 | 6.111E+00 | 1.852E+02 | 1.852E+02 | 1.852E+02 | 1.852E+02 | 1.852E+02 | 1.852E+02 | 1.852E+02 | 1.852E+02 | 1.655E+06 | 2.179E+09 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 8.412E+04 | 8.412E+04 | 3.461E-05 | 3.461E-07 | 3.461E-07 | 3.461E-07 | 3.461E-07 | 3.461E-07 | 3.461E-07 | 3.461E-07 | 3.461E-07 | 1.406E-04 | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 4.276E+14 | 4.276E+14 | 4.934E+12 | 2.535E+10 | 2.535E+10 | 2.535E+10 | 2.535E+10 | 2.535E+10 | 2.535E+10 | 2.535E+10 | 2.535E+10 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.686E+06 | 1.686E+06 | 3.574E+04 | 8.074E+07 | 8.074E+07 | 8.074E+07 | 8.074E+07 | 8.074E+07 | 8.074E+07 | 8.074E+07 | 8.074E+07 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.380E+01 | 1.380E+01 | 5.964E+00 | 1.823E+02 | 1.823E+02 | 1.823E+02 | 1.823E+02 | 1.823E+02 | 1.823E+02 | 1.823E+02 | 1.823E+02 | 1.904E+06 | 1.003E+07 |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 7.178E+04 | 7.178E+04 | 4.156E-05 | 4.156E-07 | 4.156E-07 | 4.156E-07 | 4.156E-07 | 4.156E-07 | 4.156E-07 | 4.156E-07 | 4.156E-07 | 8.321E-05 | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 1.609E+14 | 1.609E+14 | 4.164E+12 | 2.140E+10 | 2.140E+10 | 2.140E+10 | 2.140E+10 | 2.140E+10 | 2.140E+10 | 2.140E+10 | 2.140E+10 | 0. | 0. |
| | 1.079E+05 | 3.043E+14 | 3.043E+14 | 5.242E+05 | 5.242E+05 | 1.000E+05 | 7.257E+07 | 7.257E+07 | 7.257E+07 | 7.257E+07 | 7.257E+07 | 7.257E+07 | 7.257E+07 | 7.257E+07 | 0. | 0. |

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|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 1.115E+00 | -2.233E-03 | 2.283E-09 | 4.994E+00 | 1.728E+02 | 5.636E+07 | 7.764E+03 | 4.231E+03 | 1.286E+09 |
| 1.191E+03 | 6.47E+04 | 2.936E+06 | 4.484E-04 | 1.000E+00 | 0. | 0. | 3.849E-04 | 1.545E+00 |
| 93.00 | 4.031E+13 | 6.070E+12 | 3.004E+11 | 1.747E+09 | 2.466E+02 | 9.290E-07 | 2.447E+02 | 6.254E-02 |
| 3.387E+06 | 1.018E+07 | 4.398E+03 | 1.631E+08 | 4.476E+07 | 3.014E+02 | 7.658E-07 | 3.014E+02 | 5.424E-13 |
| 9.399E+01 | -5.707E-03 | 1.869E-09 | 4.992E+00 | 1.743E+02 | 5.213E+05 | 4.972E+07 | 1.346E+03 | 1.095E+09 |
| 5.073E+03 | 6.449E+04 | 3.387E+06 | 2.384E-04 | 1.000E+00 | 9.954E-04 | 1.772E-05 | 5.162E-04 | 1.871E+00 |
| 94.00 | 2.481E+13 | 6.547E+12 | 2.863E+11 | 1.471E+09 | 4.012E+02 | 2.284E-06 | 2.992E+02 | 9.287E-02 |
| 3.407E+06 | 1.275E+07 | 4.646E+03 | 1.643E+08 | 2.864E+07 | 3.631E+02 | 1.404E-06 | 3.691E+02 | 1.172E-12 |
| 7.768E-01 | -3.620E-03 | 1.530E-09 | 4.992E+00 | 1.761E+02 | 4.821E+07 | 3.185E+03 | 8.122E+02 | 9.266E+08 |
| 4.153E+03 | 4.936E+04 | 3.990E+06 | 6.483E-04 | 1.000E+00 | 4.876E-04 | 2.550E-05 | 8.598E-04 | 2.222E+00 |
| 95.00 | 2.072E+13 | 5.317E+12 | 2.345E+11 | 1.205E+09 | 4.876E-04 | 5.302E-06 | 3.653E+02 | 1.377E-01 |
| 4.506E+06 | 1.621E+07 | 3.368E+03 | 1.400E+08 | 8.602E+06 | 4.522E+02 | 4.692E-06 | 4.522E+02 | 3.455E-12 |
| 6.455E-01 | -6.090E-03 | 1.253E-09 | 5.016E+00 | 1.783E+02 | 4.450E+07 | 2.046E+03 | 4.900E+02 | 7.783E+06 |
| 3.411E+03 | 3.803E+04 | 4.550E+06 | 7.760E-04 | 1.000E+00 | 9.412E-05 | 3.652E-05 | 9.574E-04 | 2.606E+00 |
| 96.00 | 1.665E+13 | 4.312E+12 | 3.866E+11 | 9.875E+08 | 2.249E-04 | 1.34E-05 | 4.463E+02 | 2.840E-01 |
| 5.128E+06 | 2.052E+07 | 2.955E+03 | 1.127E+08 | 7.526E+06 | 4.932E+02 | 4.932E+02 | 5.543E+02 | 8.552E-12 |
| 5.374E-01 | -6.307E-03 | 1.027E-09 | 5.044E+00 | 1.807E+02 | 4.125E+07 | 1.307E-03 | 2.956E+02 | 6.310E+08 |
| 2.802E+03 | 2.950E+04 | 5.198E+06 | 9.316E-04 | 1.000E+00 | 1.461E-04 | 6.096E-05 | 1.329E-03 | 3.887E+00 |
| 97.00 | 1.367E+13 | 3.492E+12 | 1.922E+11 | 8.104E+08 | 9.878E-05 | 3.178E-05 | 5.451E+02 | 3.022E-01 |
| 5.925E+06 | 2.531E+07 | 2.598E+03 | 1.174E+08 | 7.526E+06 | 5.543E+02 | 2.718E-05 | 6.795E+02 | 2.153E-11 |
| 4.486E-01 | -6.544E-03 | 8.476E-10 | 5.077E+00 | 1.834E+02 | 3.815E+07 | 6.371E-02 | 1.784E+02 | 5.426E+08 |
| 2.385E+03 | 2.307E+04 | 5.995E+06 | 1.116E-03 | 1.000E+00 | 2.452E-04 | 1.004E-04 | 1.074E-03 | 3.889E+00 |
| 98.00 | 1.123E+13 | 2.826E+12 | 1.296E+11 | 6.661E+08 | 4.609E+09 | 7.386E-05 | 6.656E+02 | 4.471E-01 |
| 9.915E+06 | 2.244E+07 | 2.279E+03 | 6.143E+07 | 4.834E+06 | 8.332E+02 | 6.381E-05 | 8.332E+02 | 5.229E-11 |
| 3.763E-01 | -6.799E-03 | 6.926E-10 | 5.121E+00 | 1.863E+02 | 3.529E+07 | 5.362E-02 | 1.076E+02 | 4.511E+04 |
| 1.900E+03 | 1.801E+04 | 4.915E+06 | 1.343E-03 | 1.000E+00 | 1.343E-05 | 1.715E-04 | 2.667E-03 | 4.675E+00 |
| 99.00 | 9.250E+12 | 2.282E+12 | 4.136E+11 | 5.485E+08 | 3.793E+09 | 1.682E-04 | 8.122E+02 | 6.607E-01 |
| 7.976E+06 | 2.746E+07 | 3.080E+07 | 4.242E+07 | 3.110E+06 | 1.022E+03 | 1.468E-04 | 1.022E+03 | 1.305E-10 |
| 3.161E-01 | -7.075E-03 | 5.703E-10 | 5.174E+00 | 1.896E+02 | 3.264E+07 | 3.415E+02 | 6.992E+01 | 3.745E+08 |
| 1.570E+03 | 1.445E+04 | 7.976E+06 | 1.612E-03 | 1.000E+00 | 6.742E-04 | 3.027E-04 | 3.920E-03 | 6.589E+00 |
| 100.00 | 7.633E+12 | 1.848E+12 | 4.344E+11 | 4.526E+08 | 4.131E+09 | 3.744E-04 | 9.895E+02 | 9.748E-01 |
| 9.199E+06 | 2.746E+07 | 1.793E+03 | 2.866E+07 | 2.006E+06 | 1.000E+03 | 3.303E-04 | 1.253E+03 | 3.175E-10 |
| 2.668E-01 | -7.313E-03 | 4.706E-10 | 5.276E+00 | 1.932E+02 | 3.019E+07 | 2.200E+02 | 3.917E+01 | 3.107E+08 |
| 1.301E+03 | 1.157E+04 | 9.199E+06 | 1.235E-03 | 1.000E+00 | 1.191E-03 | 5.514E-04 | 5.824E-03 | 1.049E+01 |
| 101.00 | 6.314E+12 | 1.492E+12 | 4.764E+11 | 4.744E+08 | 2.612E+09 | 5.470E-04 | 9.493E+02 | 9.652E-01 |
| 1.090E+07 | 4.527E+07 | 1.594E+03 | 1.972E+07 | 1.296E+06 | 1.259E+03 | 4.676E-04 | 1.259E+03 | 5.299E-10 |
| 2.881E-01 | -7.694E-03 | 3.893E-10 | 5.306E+00 | 1.971E+02 | 2.886E+07 | 1.723E+02 | 2.684E+01 | 5.279E+08 |
| 1.040E+03 | 9.332E+03 | 1.090E+07 | 2.322E-03 | 2.322E-05 | 8.437E-07 | 1.036E-03 | 5.925E-03 | 1.094E+01 |
| 102.00 | 5.236E+12 | 1.421E+12 | 4.105E+11 | 6.042E+08 | 4.207E+09 | 7.400E-04 | 9.495E+02 | 9.559E-01 |
| 1.280E+07 | 2.337E+07 | 1.421E+03 | 1.944E+07 | 4.402E+08 | 1.267E+03 | 7.035E-04 | 1.267E+03 | 8.718E-10 |
| 1.924E-01 | -8.040E-03 | 3.228E-10 | 5.384E+00 | 2.014E+02 | 2.390E+07 | 1.297E+02 | 1.839E+01 | 2.144E+08 |
| 8.996E+02 | 7.574E+03 | 1.260E+07 | 2.768E-03 | 2.788E-05 | 4.027E-07 | 2.006E-03 | 6.152E-03 | 1.132E+01 |
| 103.00 | 4.355E+12 | 9.842E+11 | 3.878E+11 | 5.025E+08 | 1.002E+03 | 1.089E-03 | 9.495E+02 | 9.486E-01 |
| 1.491E+07 | 2.167E+07 | 1.274E+03 | 7.099E+06 | 5.461E+05 | 1.275E+03 | 9.914E-04 | 1.275E+03 | 1.416E-09 |
| 1.644E-01 | -8.411E-03 | 2.845E-10 | 5.470E+00 | 2.061E+02 | 2.172E+07 | 9.442E+01 | 1.260E+01 | 1.782E+08 |
| 7.512E+02 | 6.176E+03 | 1.491E+07 | 3.346E-03 | 3.346E-05 | 7.713E-07 | 4.610E-03 | 6.516E-03 | 1.162E+01 |
| 104.00 | 3.633E+12 | 8.028E+11 | 3.598E+11 | 4.192E+08 | 1.562E+09 | 1.484E-03 | 9.917E+02 | 9.280E-01 |
| 1.723E+07 | 2.018E+07 | 1.142E+03 | 6.203E+06 | 3.560E+05 | 1.804E+03 | 1.364E-03 | 1.285E+03 | 2.374E-09 |

| | | | | | | | | | | | | | |
|--------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|-----------|-----------|
| 105.00 | 1.411E-01 | 8.011E-03 | 2.240E-10 | 5.063E+00 | 2.112E+02 | 4.112E+02 | 4.112E+02 | 1.000E+00 | 1.517E-02 | 3.446E-04 | 0.756E+01 | 4.036E+04 | 1.091E+08 |
| | 0.290E+02 | 5.055E+03 | 1.723E+07 | 4.017E-03 | 4.017E-05 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 3.446E-04 | 3.446E-04 | 0.275E-03 | 7.033E-03 | 1.182E+01 |
| | 3.040E+12 | 6.541E+11 | 3.284E+11 | 3.508E+10 | 1.802E+04 | 1.300E+09 | 1.300E+09 | 1.300E+09 | 1.005E+03 | 1.005E+03 | 1.97E-03 | 9.935E+02 | 9.293E+01 |
| | 1.976E+07 | 1.880E+07 | 1.029E+03 | 4.300E+06 | 2.328E+05 | 1.175E+05 | 1.175E+05 | 1.175E+05 | 1.296E+03 | 1.296E+03 | 1.832E-03 | 1.296E+03 | 3.014E+09 |
| | 1.210E-01 | 9.240E-03 | 1.874E-10 | 5.662E+00 | 2.168E+02 | 2.168E+02 | 2.168E+02 | 2.168E+02 | 1.695E+07 | 1.695E+07 | 4.827E+01 | 5.917E+00 | 1.249E+08 |
| | 5.281E+02 | 4.140E+03 | 1.976E+07 | 4.821E-03 | 4.821E-05 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 3.026E-02 | 3.026E-02 | 1.762E-02 | 7.723E-03 | 1.194E+01 |
| 106.00 | 4.522E+12 | 5.425E+11 | 2.955E+11 | 2.944E+10 | 1.513E+04 | 1.074E+09 | 1.074E+09 | 1.074E+09 | 1.008E+03 | 1.008E+03 | 2.566E-03 | 9.959E+02 | 9.207E+01 |
| | 1.051E+07 | 1.769E+07 | 9.501E+02 | 2.938E+06 | 1.527E+05 | 7.614E+04 | 7.614E+04 | 7.614E+04 | 1.308E+03 | 1.308E+03 | 2.415E-03 | 1.308E+03 | 5.687E+09 |
| | 1.051E-01 | 9.700E-03 | 1.573E-10 | 5.766E+00 | 2.210E+02 | 2.210E+02 | 2.210E+02 | 2.210E+02 | 1.500E+07 | 1.500E+07 | 2.500E+01 | 4.055E+00 | 1.050E+08 |
| | 4.446E+02 | 3.386E+03 | 2.251E+07 | 5.787E-03 | 5.787E-05 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 6.226E-02 | 6.226E-02 | 3.066E-02 | 6.609E-03 | 1.194E+01 |
| 107.00 | 2.149E+12 | 4.494E+11 | 2.628E+11 | 2.480E+10 | 1.274E+08 | 4.812E+04 | 4.812E+04 | 4.812E+04 | 1.011E+03 | 1.011E+03 | 3.282E-03 | 9.984E+02 | 9.122E+01 |
| | 2.586E+07 | 1.664E+07 | 8.935E+02 | 2.008E+06 | 1.063E+05 | 5.299E+04 | 5.299E+04 | 5.299E+04 | 1.324E+03 | 1.324E+03 | 3.116E-03 | 1.324E+03 | 8.663E+09 |
| | 9.178E-02 | -1.020E-03 | 1.225E-10 | 5.076E+00 | 2.298E+02 | 2.298E+02 | 2.298E+02 | 2.298E+02 | 1.335E+07 | 1.335E+07 | 2.610E+01 | 2.778E+00 | 8.862E+07 |
| | 3.753E+02 | 2.759E+03 | 2.548E+07 | 6.945E-03 | 6.945E-05 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 1.233E-01 | 1.233E-01 | 6.698E-02 | 9.717E-03 | 1.193E+01 |
| 108.00 | 1.016E+12 | 3.752E+11 | 2.318E+11 | 2.095E+10 | 1.077E+04 | 7.206E+04 | 7.206E+04 | 7.206E+04 | 1.014E+03 | 1.014E+03 | 4.126E-03 | 1.002E+03 | 9.034E+01 |
| | 2.672E+07 | 1.570E+07 | 7.075E+02 | 1.972E+06 | 6.635E+04 | 3.678E+04 | 3.678E+04 | 3.678E+04 | 1.337E+03 | 1.337E+03 | 3.907E-03 | 1.337E+03 | 1.361E+08 |
| | 8.012E-02 | -1.073E-02 | 1.119E-10 | 5.989E+00 | 2.372E+02 | 2.372E+02 | 2.372E+02 | 2.372E+02 | 1.189E+07 | 1.189E+07 | 2.032E+01 | 1.904E+00 | 7.510E+07 |
| | 3.177E+02 | 2.332E+03 | 2.867E+07 | 8.336E-03 | 8.336E-05 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 2.555E-01 | 2.555E-01 | 2.002E-01 | 1.167E-02 | 1.181E+01 |
| 109.00 | 1.539E+12 | 3.145E+11 | 2.034E+11 | 1.776E+10 | 9.124E+07 | 5.883E+04 | 5.883E+04 | 5.883E+04 | 1.018E+03 | 1.018E+03 | 5.132E-03 | 1.006E+03 | 8.956E+01 |
| | 3.210E+07 | 1.485E+07 | 7.004E+02 | 9.376E+05 | 4.394E+04 | 2.675E+04 | 2.675E+04 | 2.675E+04 | 1.354E+03 | 1.354E+03 | 4.967E-03 | 1.354E+03 | 2.991E+08 |
| | 7.023E-02 | -1.130E-02 | 9.487E-11 | 6.104E+00 | 2.452E+02 | 2.452E+02 | 2.452E+02 | 2.452E+02 | 1.054E+07 | 1.054E+07 | 1.654E+01 | 1.305E+00 | 6.190E+07 |
| | 2.672E+02 | 1.788E+03 | 3.210E+07 | 1.000E-02 | 1.000E-04 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 6.376E-01 | 6.376E-01 | 6.689E-01 | 1.260E-02 | 1.163E+01 |
| 110.00 | 1.398E+12 | 2.648E+11 | 1.783E+11 | 1.510E+10 | 7.572E+07 | 4.800E+04 | 4.800E+04 | 4.800E+04 | 1.022E+03 | 1.022E+03 | 6.336E-03 | 1.011E+03 | 8.872E+01 |
| | 3.575E+07 | 1.409E+07 | 6.410E+02 | 6.407E+05 | 2.320E+04 | 1.934E+04 | 1.934E+04 | 1.934E+04 | 1.370E+03 | 1.370E+03 | 6.106E-03 | 1.370E+03 | 3.165E+08 |
| | 6.193E-02 | -1.193E-02 | 0.066E-11 | 6.221E+00 | 2.539E+02 | 2.539E+02 | 2.539E+02 | 2.539E+02 | 9.427E+06 | 9.427E+06 | 1.416E+01 | 8.940E-01 | 5.459E+07 |
| | 2.297E+02 | 1.414E+03 | 3.575E+07 | 1.201E-02 | 1.201E-04 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 1.346E+03 | 1.346E+03 | 1.112E+00 | 1.096E-02 | 1.130E+01 |
| 111.00 | 1.116E+12 | 2.233E+11 | 1.566E+11 | 1.407E+10 | 6.610E+07 | 3.917E+04 | 3.917E+04 | 3.917E+04 | 1.032E+03 | 1.032E+03 | 7.796E-03 | 1.016E+03 | 8.796E+01 |
| | 3.963E+07 | 1.339E+07 | 5.881E+02 | 4.378E+05 | 1.940E+04 | 1.470E+04 | 1.470E+04 | 1.470E+04 | 1.396E+03 | 1.396E+03 | 7.661E-03 | 1.396E+03 | 4.739E+08 |
| | 5.487E-02 | -1.240E-02 | 6.074E-11 | 6.348E+00 | 2.634E+02 | 2.634E+02 | 2.634E+02 | 2.634E+02 | 8.977E+06 | 8.977E+06 | 1.465E+01 | 6.126E-01 | 4.682E+07 |
| | 1.964E+02 | 1.107E+03 | 3.963E+07 | 1.401E-02 | 1.401E-04 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 2.925E+00 | 2.925E+00 | 2.657E+00 | 1.670E-02 | 1.100E+01 |
| 112.00 | 9.543E+11 | 1.890E+11 | 1.384E+11 | 1.101E+10 | 5.650E+07 | 3.194E+04 | 3.194E+04 | 3.194E+04 | 1.032E+03 | 1.032E+03 | 9.011E-03 | 1.021E+03 | 8.719E+01 |
| | 4.373E+07 | 1.270E+07 | 5.409E+02 | 2.992E+05 | 1.308E+04 | 1.157E+04 | 1.157E+04 | 1.157E+04 | 1.418E+03 | 1.418E+03 | 9.500E-03 | 1.418E+03 | 7.017E+08 |
| | 4.084E-02 | -1.334E-02 | 5.863E-11 | 6.454E+00 | 2.737E+02 | 2.737E+02 | 2.737E+02 | 2.737E+02 | 7.481E+06 | 7.481E+06 | 1.166E+01 | 1.997E-01 | 4.030E+07 |
| | 1.681E+02 | 6.437E+02 | 4.373E+07 | 1.799E-02 | 1.799E-04 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 6.094E-12 | 6.094E-12 | 6.0.0.0.0. | 1.906E-02 | 1.074E+01 |
| 113.00 | 8.180E+11 | 1.598E+11 | 1.233E+11 | 9.451E+09 | 4.454E+07 | 2.600E+04 | 2.600E+04 | 2.600E+04 | 1.032E+03 | 1.032E+03 | 1.192E-02 | 1.027E+03 | 6.644E+01 |
| | 4.807E+07 | 1.219E+07 | 4.985E+02 | 7.044E+05 | 6.717E+03 | 9.413E+03 | 9.413E+03 | 9.413E+03 | 1.432E+03 | 1.432E+03 | 1.179E-02 | 1.432E+03 | 1.027E+07 |
| | 4.267E-02 | -1.416E-02 | 5.047E-11 | 6.568E+00 | 2.847E+02 | 2.847E+02 | 2.847E+02 | 2.847E+02 | 6.667E+06 | 6.667E+06 | 2.876E+01 | 2.876E-01 | 3.481E+07 |
| | 1.045E+02 | 6.372E+02 | 4.007E+07 | 2.075E-02 | 2.075E-04 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 1.364E+06 | 1.364E+06 | 6.0.0.0.0. | 2.158E-02 | 1.036E+01 |
| 114.00 | 7.042E+11 | 1.350E+11 | 1.109E+11 | 8.176E+09 | 4.173E+07 | 2.104E+04 | 2.104E+04 | 2.104E+04 | 1.044E+03 | 1.044E+03 | 1.489E-02 | 1.036E+03 | 8.521E+01 |
| | 5.264E+07 | 1.160E+07 | 4.603E+02 | 1.137E+05 | 5.066E+03 | 7.866E+03 | 7.866E+03 | 7.866E+03 | 1.456E+03 | 1.456E+03 | 1.462E-02 | 1.456E+03 | 1.485E+07 |
| | 3.924E-02 | -1.501E-02 | 4.341E-11 | 6.681E+00 | 2.968E+02 | 2.968E+02 | 2.968E+02 | 2.968E+02 | 1.067E+06 | 1.067E+06 | 1.067E+01 | 2.158E-01 | 3.017E+07 |
| | 1.246E+02 | 4.694E+02 | 5.264E+07 | 2.490E-02 | 2.490E-04 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 2.808E+06 | 2.808E+06 | 6.0.0.0.0. | 2.421E-02 | 9.956E+00 |
| 115.00 | 6.076E+11 | 1.139E+11 | 1.008E+11 | 7.011E+09 | 3.604E+07 | 1.700E+04 | 1.700E+04 | 1.700E+04 | 1.050E+03 | 1.050E+03 | 1.877E-02 | 1.041E+03 | 8.502E+01 |
| | 5.743E+07 | 1.112E+07 | 4.571E+02 | 9.766E+04 | 3.251E+03 | 6.765E+03 | 6.765E+03 | 6.765E+03 | 1.480E+03 | 1.480E+03 | 1.830E-02 | 1.480E+03 | 2.121E+07 |
| | 3.942E-02 | -1.598E-02 | 3.746E-11 | 6.793E+00 | 3.693E+02 | 3.693E+02 | 3.693E+02 | 3.693E+02 | 5.299E+06 | 5.299E+06 | 1.062E+01 | 1.351E+01 | 2.622E+07 |
| | 1.078E+02 | 3.419E+02 | 5.743E+07 | 2.986E-02 | 2.986E-04 | 1.000E+00 | 1.000E+00 | 1.000E+00 | 6.014E-13 | 6.014E-13 | 6.0.0.0.0. | 2.699E-02 | 9.530E+00 |
| 116.00 | 5.260E+11 | 9.607E+10 | 9.246E+10 | 6.070E+09 | 3.119E+07 | 1.262E+04 | 1.262E+04 | 1.262E+04 | 1.057E+03 | 1.057E+03 | 2.380E-02 | 1.040E+03 | 8.430E+01 |
| | 6.244E+07 | 1.073E+07 | 3.941E+02 | 8.573E+04 | 2.673E+03 | 5.877E+03 | 5.877E+03 | 5.877E+03 | 1.507E+03 | 1.507E+03 | 2.301E-02 | 1.507E+03 | 2.094E+07 |

| | | | | | | | | | |
|--------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 117.00 | 4.212E-02 | -1.039E-22 | 5.244E-11 | 9.404E+00 | 4.224E+02 | 4.726E+09 | 1.037E+01 | 4.254E-02 | 4.248E+07 |
| | 9.364E+01 | 2.461E+02 | 6.244E+07 | 3.366E-02 | 3.586E-04 | 1.000E+00 | 0. | 2.967E-02 | 9.096E+00 |
| | 6.573E+11 | 6.114E+10 | 8.512E+10 | 5.276E+09 | 4.711E+07 | 1.085E+08 | 3.013E-02 | 1.056E+03 | 8.380E-01 |
| | 7.767E+07 | 1.032E+07 | 3.653E+02 | 4.457E+04 | 1.816E+03 | 5.093E+03 | 2.888E-02 | 1.534E+03 | 4.176E-07 |
| | 4.926E-02 | -1.809E-02 | 2.819E-11 | 7.013E+00 | 3.370E+02 | 3.370E+02 | 1.017E+01 | 6.341E-02 | 2.003E+07 |
| | 6.175E+01 | 1.778E+02 | 6.767E+07 | 4.303E-02 | 4.303E-04 | 1.000E+00 | 0. | 3.263E-02 | 8.666E+00 |
| 118.00 | 3.996E+11 | 6.907E+10 | 7.806E+10 | 4.011E+09 | 2.385E+07 | 8.634E+07 | 3.756E-02 | 1.065E+03 | 8.332E-01 |
| | 7.310E+07 | 9.936E+06 | 3.389E+02 | 3.046E+04 | 4.315E+03 | 1.563E+03 | 3.567E-02 | 1.563E+03 | 5.770E-07 |
| | 4.677E-02 | -1.924E-02 | 2.464E-11 | 7.122E+00 | 3.517E+02 | 3.517E+02 | 1.011E+01 | 4.345E-02 | 1.762E-07 |
| | 7.166E+01 | 1.277E+02 | 7.310E+07 | 5.163E-02 | 5.163E-04 | 1.000E+00 | 0. | 3.604E-02 | 8.257E+00 |
| 119.00 | 3.517E+11 | 5.993E+10 | 7.044E+10 | 4.058E+09 | 2.086E+07 | 6.914E+07 | 4.503E-02 | 1.074E+03 | 8.298E-01 |
| | 7.874E+07 | 9.583E+06 | 3.146E+02 | 2.081E+04 | 4.478E+03 | 1.591E+03 | 4.240E-02 | 1.591E+03 | 7.213E-07 |
| | 2.458E-02 | -2.040E-02 | 2.169E-11 | 7.229E+00 | 3.663E+02 | 3.663E+02 | 1.007E+01 | 2.977E-02 | 1.560E+07 |
| | 6.320E+01 | 9.750E+01 | 7.874E+07 | 6.195E-02 | 6.195E-04 | 1.000E+00 | 0. | 4.049E-02 | 7.894E+00 |
| 119.99 | 4.131E+11 | 2.922E+10 | 6.156E+10 | 3.013E+09 | 1.857E+07 | 5.660E+07 | 5.017E-02 | 1.083E+03 | 8.287E-01 |
| | 8.451E+07 | 9.257E+06 | 2.924E+02 | 1.428E+04 | 5.949E+02 | 2.580E+03 | 4.695E-02 | 1.620E+03 | 1.078E-06 |
| | 2.267E-02 | -1.141E-05 | 1.938E-11 | 7.334E+00 | 3.799E+02 | 4.799E+02 | 1.004E+01 | 2.040E-02 | 1.394E+07 |
| | 5.619E+01 | 7.764E+01 | 8.451E+07 | 7.432E-02 | 7.432E-04 | 1.000E+00 | 0. | 4.702E-02 | 7.686E+00 |
| 120.00 | 3.126E+11 | 5.388E+10 | 6.146E+10 | 3.609E+09 | 1.855E+07 | 5.650E+07 | 5.020E-02 | 1.081E+03 | 8.287E-01 |
| | 8.457E+07 | 9.257E+06 | 2.924E+02 | 1.428E+04 | 5.949E+02 | 2.580E+03 | 4.695E-02 | 1.620E+03 | 1.078E-06 |
| | 2.267E-02 | -1.141E-05 | 1.938E-11 | 7.334E+00 | 3.799E+02 | 4.799E+02 | 1.004E+01 | 2.040E-02 | 1.394E+07 |
| | 5.612E+01 | 7.752E+01 | 8.457E+07 | 7.432E-02 | 7.432E-04 | 1.000E+00 | 0. | 4.710E-02 | 7.686E+00 |
| 121.00 | 4.738E+11 | 4.664E+10 | 5.572E+10 | 3.051E+09 | 1.777E+07 | 4.721E+07 | 6.182E-02 | 1.094E+03 | 8.223E-01 |
| | 9.058E+07 | 8.948E+06 | 2.714E+02 | 9.719E+03 | 4.060E+02 | 1.277E+03 | 5.653E-02 | 1.656E+03 | 1.272E-06 |
| | 2.095E-02 | -1.222E-05 | 1.690E-11 | 7.797E+00 | 4.001E+02 | 4.001E+02 | 1.003E+01 | 1.398E-02 | 1.272E+07 |
| | 4.929E+01 | 5.696E+01 | 9.058E+07 | 8.917E-02 | 8.917E-04 | 1.000E+00 | 0. | 5.267E-02 | 7.267E+00 |
| 122.00 | 2.415E+11 | 4.067E+10 | 5.081E+10 | 2.604E+09 | 1.768E+07 | 3.983E+07 | 7.358E-02 | 1.104E+03 | 8.180E-01 |
| | 9.675E+07 | 8.662E+06 | 2.573E+02 | 6.641E+03 | 1.771E+03 | 1.448E+03 | 6.745E-02 | 1.692E+03 | 1.975E-06 |
| | 1.945E-02 | -1.302E-05 | 1.492E-11 | 8.258E+00 | 4.194E+02 | 4.194E+02 | 1.002E+01 | 9.580E-03 | 1.087E+07 |
| | 4.362E+01 | 4.217E+01 | 9.675E+07 | 1.070E-01 | 9.408E-04 | 1.000E+00 | 0. | 5.862E-02 | 6.962E+00 |
| 123.00 | 2.149E+11 | 3.574E+10 | 4.657E+10 | 2.404E+09 | 1.645E+07 | 3.390E+07 | 8.798E-02 | 1.115E+03 | 8.158E-01 |
| | 1.031E+06 | 8.394E+06 | 2.345E+02 | 4.348E+03 | 1.345E+02 | 1.448E+03 | 7.987E-02 | 1.728E+03 | 2.615E-06 |
| | 1.812E-02 | -1.381E-05 | 1.376E-11 | 8.719E+00 | 4.390E+02 | 4.390E+02 | 1.001E+01 | 6.564E-03 | 9.687E+06 |
| | 3.887E+01 | 3.143E+01 | 1.031E+08 | 1.284E-01 | 1.063E-03 | 1.000E+00 | 0. | 6.496E-02 | 6.867E+00 |
| 124.00 | 1.915E+11 | 3.160E+10 | 4.488E+10 | 1.941E+09 | 1.588E+07 | 2.908E+07 | 1.045E-01 | 1.127E+03 | 8.153E-01 |
| | 1.095E+08 | 8.147E+06 | 2.181E+02 | 3.101E+03 | 1.360E+02 | 1.256E+03 | 9.394E-02 | 1.764E+03 | 3.420E-06 |
| | 1.694E-02 | -1.459E-05 | 1.186E-11 | 9.178E+00 | 4.574E+02 | 4.574E+02 | 1.001E+01 | 4.494E-03 | 8.477E+06 |
| | 3.484E+01 | 2.357E+01 | 1.095E+08 | 1.540E-01 | 1.202E-03 | 1.000E+00 | 0. | 7.173E-02 | 6.460E+00 |
| 125.00 | 1.720E+11 | 2.810E+10 | 3.965E+10 | 1.694E+09 | 1.536E+07 | 2.512E+07 | 1.232E-01 | 1.139E+03 | 8.166E-01 |
| | 1.160E+08 | 7.906E+06 | 2.029E+02 | 2.119E+03 | 9.552E+01 | 1.066E+03 | 1.099E-01 | 1.800E+03 | 4.424E-06 |
| | 1.584E-02 | -1.536E-05 | 1.066E-11 | 9.035E+00 | 4.762E+02 | 4.762E+02 | 1.006E+01 | 3.082E-03 | 7.811E+06 |
| | 3.133E+01 | 1.777E+01 | 1.160E+08 | 1.847E-01 | 1.361E-03 | 1.000E+00 | 0. | 7.895E-02 | 6.220E+00 |
| 130.00 | 1.497E+11 | 1.677E+10 | 2.819E+10 | 9.269E+08 | 1.330E+07 | 1.315E+07 | 4.620E-01 | 1.209E+03 | 8.459E-01 |
| | 1.491E+08 | 6.907E+06 | 1.438E+02 | 3.158E+03 | 1.747E+01 | 5.019E+02 | 2.244E-01 | 1.991E+03 | 1.394E-05 |
| | 1.190E-02 | -1.906E-05 | 6.691E-12 | 1.190E+01 | 5.676E+02 | 5.676E+02 | 1.000E+01 | 4.656E-04 | 4.928E+06 |
| | 1.991E+01 | 4.626E+01 | 1.491E+08 | 1.174E-01 | 2.331E-03 | 1.000E+00 | 0. | 1.229E-01 | 5.454E+00 |
| 135.00 | 7.241E+10 | 1.091E+10 | 2.131E+10 | 5.593E+08 | 1.186E+07 | 7.638E+06 | 5.050E-01 | 1.296E+03 | 8.111E-01 |
| | 1.794E+08 | 6.131E+06 | 1.081E+02 | 4.705E+01 | 3.464E+00 | 2.561E+02 | 4.230E-01 | 2.204E+03 | 3.688E-05 |

| | | | | | | | | | | |
|--------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 140.00 | 9.207E-03 | -2.249E-05 | 4.552E-12 | 1.411E+01 | 9.401E+02 | 6.401E+02 | 6.144E+05 | 1.000E+01 | 7.035E-05 | 3.435E+06 |
| | 1.367E+01 | 1.305E+00 | 1.793E+04 | 8.656E-01 | 3.741E-03 | 1.000E+00 | 0. | 0. | 1.439E-01 | 5.156E+00 |
| | 5.162E+10 | 7.527E+04 | 1.681E+10 | 5.611E+06 | 1.078E+07 | 4.766E+06 | 1.409E+03 | 7.15E-01 | 1.403E+03 | 1.014E+00 |
| | 2.014E+08 | 5.506E+06 | 8.997E+01 | 7.010E+00 | 7.259E-01 | 1.362E+02 | 2.449E+03 | 7.67E-01 | 2.444E+03 | 8.316E-05 |
| | 7.482E-03 | -2.511E-05 | 3.274E-12 | 1.627E+01 | 7.096E+02 | 7.965E+02 | 3.921E+05 | 1.000E+01 | 1.063E-05 | 1.526E+06 |
| | 9.926E+00 | 3.894E-01 | 2.014E+06 | 1.634E+00 | 5.567E-03 | 1.000E+00 | 0. | 0. | 2.692E-01 | 5.282E+00 |
| 145.00 | 3.433E+10 | 5.422E+09 | 1.368E+10 | 2.448E+08 | 9.936E+06 | 3.133E+06 | 1.540E+03 | 1.611E+00 | 1.533E+03 | 1.160E+00 |
| | 2.116E+06 | 4.866E+06 | 6.210E+01 | 1.044E+00 | 1.582E-01 | 7.764E+01 | 2.733E+03 | 1.333E+00 | 2.732E+03 | 1.684E-04 |
| | 6.152E-03 | -2.623E-05 | 2.452E-12 | 1.317E+01 | 7.721E+02 | 7.721E+02 | 2.674E+05 | 1.000E+01 | 1.605E+06 | 1.768E+06 |
| | 7.502E+00 | 1.210E-01 | 2.116E+06 | 2.780E+00 | 7.585E-03 | 1.000E+00 | 0. | 0. | 3.896E-01 | 5.897E+00 |
| 150.00 | 2.936E+10 | 4.034E+09 | 1.139E+10 | 1.724E+08 | 9.264E+06 | 2.143E+06 | 1.699E+03 | 2.781E+00 | 1.609E+03 | 1.162E+00 |
| | 2.100E+08 | 4.542E+06 | 7.403E+01 | 1.556E+01 | 3.567E-01 | 4.500E+01 | 3.067E+03 | 2.241E+00 | 3.065E+03 | 3.117E-04 |
| | 5.142E-03 | -3.066E-05 | 1.894E-12 | 2.340E+01 | 8.282E+02 | 8.282E+02 | 1.959E+05 | 1.000E+01 | 2.425E-07 | 1.394E+06 |
| | 5.845E+00 | 3.877E-02 | 2.100E+08 | 4.228E+00 | 9.382E-03 | 1.000E+00 | 0. | 0. | 5.613E-01 | 7.110E+00 |
| 160.00 | 1.438E+10 | 2.400E+09 | 8.321E+09 | 9.255E+07 | 8.242E+06 | 1.093E+06 | 2.174E+03 | 0.045E+00 | 2.103E+03 | 2.000E+00 |
| | 1.946E+06 | 3.413E+06 | 4.638E+01 | 4.455E-04 | 1.735E-04 | 1.617E+01 | 3.935E+03 | 6.063E+00 | 3.929E+03 | 9.66E-04 |
| | 3.724E-03 | -3.457E-05 | 1.210E-12 | 2.425E+01 | 9.238E+02 | 9.238E+02 | 1.332E+05 | 1.000E+01 | 5.535E-09 | 4.520E+05 |
| | 3.795E+00 | 4.260E-03 | 1.946E+08 | 7.018E+00 | 1.070E-02 | 1.000E+00 | 0. | 0. | 1.167E+00 | 1.166E+01 |
| 170.00 | 1.224E+10 | 1.527E+09 | 6.375E+09 | 5.366E+07 | 7.497E+06 | 6.043E+05 | 2.743E+03 | 2.291E+01 | 2.095E+03 | 3.194E+00 |
| | 1.578E+06 | 3.231E+06 | 3.130E+01 | 7.669E-05 | 1.119E-04 | 6.194E+00 | 5.170E+03 | 1.624E+01 | 5.154E+03 | 2.408E-03 |
| | 2.793E-03 | -1.741E-05 | 8.237E-13 | 2.780E+01 | 1.001E+03 | 1.001E+03 | 1.166E+05 | 1.000E+01 | 2.763E-10 | 5.534E+05 |
| | 2.626E+00 | 4.989E-04 | 1.578E+08 | 6.113E+00 | 8.867E-03 | 1.000E+00 | 0. | 0. | 2.457E+00 | 2.346E+01 |
| 180.00 | 1.274E+10 | 1.017E+09 | 5.047E+09 | 3.793E+07 | 6.924E+06 | 3.534E+05 | 3.647E+03 | 6.508E+01 | 3.527E+03 | 5.399E+00 |
| | 1.274E+08 | 2.750E+06 | 2.911E+01 | 1.703E-06 | 6.784E-06 | 2.481E+00 | 6.939E+03 | 4.367E+01 | 6.895E+03 | 5.975E-03 |
| | 2.148E-03 | -3.934E-05 | 5.864E-13 | 3.106E+01 | 1.063E+03 | 1.063E+03 | 1.009E+05 | 1.000E+01 | 2.883E-12 | 3.759E+05 |
| | 1.900E+00 | 6.111E-05 | 1.274E+06 | 7.792E+00 | 6.360E-03 | 1.000E+00 | 0. | 0. | 5.267E+00 | 5.027E+01 |
| 190.00 | 8.103E+09 | 6.998E+08 | 4.922E+09 | 2.081E+07 | 6.464E+06 | 2.151E+05 | 4.971E+03 | 1.84E+02 | 4.662E+03 | 9.524E+00 |
| | 1.026E+08 | 2.347E+06 | 1.717E+01 | 3.780E-04 | 4.224E-07 | 1.027E+00 | 9.461E+03 | 1.178E+02 | 7.243E+03 | 1.454E-02 |
| | 1.678E-03 | -4.050E-05 | 4.312E-13 | 3.403E+01 | 1.114E+03 | 1.114E+03 | 9.539E+04 | 1.000E+01 | 6.580E-14 | 2.630E+05 |
| | 1.420E+00 | 7.732E-06 | 1.026E+08 | 7.309E+00 | 4.586E-03 | 1.000E+00 | 0. | 0. | 1.142E+01 | 1.174E+02 |
| 200.00 | 4.476E+09 | 4.936E+08 | 3.375E+09 | 1.558E+07 | 6.083E+06 | 1.349E+05 | 6.913E+03 | 5.143E+02 | 6.119E+03 | 1.713E+01 |
| | 8.240E+07 | 2.005E+06 | 1.233E+01 | 8.911E-10 | 2.704E-08 | 4.350E-01 | 1.300E+04 | 3.151E+02 | 1.268E+04 | 3.441E-02 |
| | 1.313E-03 | -4.103E-05 | 3.273E-13 | 3.673E+01 | 1.114E+03 | 1.114E+03 | 9.144E+04 | 1.000E+01 | 6.580E-14 | 2.630E+05 |
| | 1.067E+00 | 1.003E-06 | 8.240E+07 | 6.342E+00 | 3.140E-03 | 1.000E+00 | 0. | 0. | 2.463E+01 | 2.557E+02 |
| 220.00 | 2.525E+09 | 4.585E+08 | 4.382E+09 | 6.132E+06 | 5.478E+06 | 5.649E+04 | 1.394E+04 | 3.44E+03 | 9.193E+03 | 5.148E+01 |
| | 5.295E+07 | 1.466E+06 | 6.354E+00 | 4.139E-13 | 1.170E-10 | 8.270E-02 | 2.883E+04 | 1.970E+03 | 2.186E+04 | 1.620E-01 |
| | 6.729E-01 | -4.066E-05 | 1.949E-13 | 4.143E+01 | 1.214E+03 | 1.214E+03 | 8.520E+04 | 1.000E+01 | 7.823E-19 | 1.035E+05 |
| | 1.420E+00 | 1.780E-08 | 5.295E+07 | 3.310E+00 | 1.088E-03 | 1.000E+00 | 0. | 0. | 1.000E+02 | 1.196E+03 |
| 240.00 | 1.488E+09 | 1.417E+08 | 1.736E+09 | 2.918E+06 | 5.005E+06 | 2.501E+04 | 2.870E+04 | 1.547E+04 | 9.418E+03 | 1.189E+02 |
| | 3.402E+07 | 1.073E+06 | 3.276E+00 | 2.036E-16 | 5.323E-13 | 1.652E-02 | 3.847E+04 | 2.364E+03 | 3.610E+04 | 5.00E-01 |
| | 5.834E-04 | -3.834E-05 | 1.230E-13 | 4.540E+01 | 1.253E+03 | 1.253E+03 | 8.003E+04 | 1.000E+01 | 4.075E-22 | 5.947E+04 |
| | 4.382E-01 | 3.374E-10 | 3.402E+07 | 1.727E+00 | 4.039E-04 | 1.000E+00 | 0. | 0. | 2.790E+02 | 3.633E+03 |
| 260.00 | 8.994E+08 | 7.998E+07 | 1.491E+09 | 1.436E+06 | 4.614E+06 | 1.148E+04 | 5.786E+04 | 4.506E+04 | 6.101E+03 | 1.627E+02 |
| | 2.200E+07 | 7.851E+05 | 1.089E+00 | 1.004E-19 | 2.512E-15 | 3.423E-03 | 5.491E+04 | 2.33E+04 | 3.159E+04 | 9.99E-01 |
| | 4.018E-04 | -3.640E-05 | 6.466E-14 | 4.683E+01 | 1.279E+03 | 1.279E+03 | 7.556E+04 | 1.000E+01 | 2.122E-25 | 3.562E+04 |
| | 2.957E-01 | 6.437E-12 | 2.400E+07 | 9.073E-01 | 1.590E-04 | 1.000E+00 | 0. | 0. | 4.975E+02 | 6.110E+03 |
| 280.00 | 5.529E+08 | 4.603E+07 | 7.726E+08 | 7.230E+05 | 4.279E+06 | 5.395E+03 | 1.097E+05 | 9.95E+04 | 3.235E+03 | 1.877E+02 |
| | 1.439E+07 | 5.747E+05 | 8.705E-01 | 4.950E-23 | 1.218E-17 | 7.485E-04 | 2.624E+04 | 4.962E+04 | 2.660E+04 | 1.520E+00 |

| | | | | | | | | | | |
|--------|-----------|-----------|-----------|------------|-----------|-----------|-----------|-----------|------------|-----------|
| 540.00 | 9.267E-06 | 9.267E-06 | 7.715E+01 | 1.330E+03 | 1.330E+03 | 1.330E+03 | 4.597E+04 | 1.000E+01 | 4.409E-68 | 1.761E+02 |
| | 0.561E-03 | 1.454E-33 | 4.536E-04 | 1.408E-08 | 1.408E-08 | 1.408E-08 | 0. | 0. | 1.671E+00 | 2.013E+01 |
| | 1.746E-06 | 6.432E+04 | 1.986E+02 | 1.650E+06 | 6.434E-01 | 6.434E-01 | 1.676E+05 | 1.628E+05 | 2.681E+00 | 3.574E-01 |
| | 1.150E+05 | 9.457E+03 | 5.008E-66 | 3.394E-47 | 4.552E-12 | 4.552E-12 | 6.600E+04 | 6.793E+04 | 5.715E+01 | 4.032E-02 |
| | 7.265E-06 | 4.540E-06 | 1.051E-13 | 1.330E+03 | 1.330E+03 | 1.330E+03 | 4.474E+04 | 1.000E+01 | 2.297E-71 | 1.241E+02 |
| | 5.144E-03 | 3.331E-35 | 1.150E+05 | 7.509E-09 | 1.000E+00 | 1.000E+00 | 0. | 0. | 9.418E-01 | 1.240E+01 |
| 560.00 | 1.146E+06 | 1.970E+04 | 2.623E+07 | 1.749E+06 | 3.411E-01 | 3.411E-01 | 1.474E+05 | 1.471E+05 | 1.474E+00 | 2.141E-01 |
| | 8.053E+04 | 7.279E+03 | 8.149E-05 | 1.697E-49 | 1.121E-12 | 1.121E-12 | 6.297E+04 | 6.293E+04 | 3.667E+01 | 2.877E-02 |
| | 5.722E-06 | 3.809E-06 | 8.170E-16 | 1.330E+03 | 1.330E+03 | 1.330E+03 | 4.359E+04 | 1.000E+01 | 1.196E-74 | 6.780E+01 |
| | 4.051E-03 | 7.666E-37 | 8.053E+04 | 4.023E-09 | 1.000E+00 | 1.000E+00 | 0. | 0. | 5.385E-01 | 7.658E+00 |
| 580.00 | 7.541E+05 | 2.465E+04 | 2.224E+07 | 1.648E+06 | 1.725E-01 | 1.725E-01 | 1.311E+05 | 1.311E+05 | 1.311E+00 | 1.310E-01 |
| | 5.619E+04 | 5.138E+03 | 4.701E-05 | 1.068E-51 | 2.770E-13 | 2.770E-13 | 5.902E+04 | 5.899E+04 | 2.366E+01 | 2.016E-02 |
| | 4.526E-06 | 3.163E-06 | 6.378E-16 | 1.330E+03 | 1.330E+03 | 1.330E+03 | 4.251E+04 | 1.000E+01 | 6.231E-78 | 6.239E+01 |
| | 3.284E-03 | 1.771E-38 | 5.639E+04 | 2.165E-09 | 1.000E+00 | 1.000E+00 | 0. | 0. | 3.133E-01 | 4.744E+00 |
| 600.00 | 4.974E+05 | 1.532E+04 | 1.752E+07 | 1.553E+06 | 8.973E-02 | 8.973E-02 | 1.205E+05 | 1.205E+05 | 8.083E-01 | 4.209E-02 |
| | 3.949E+04 | 3.900E+03 | 2.166E-05 | 6.038E-54 | 6.872E-14 | 6.872E-14 | 5.605E+04 | 5.603E+04 | 1.534E+01 | 1.467E-02 |
| | 3.597E-06 | 2.623E-06 | 4.998E-16 | 1.330E+03 | 1.330E+03 | 1.330E+03 | 4.149E+04 | 1.000E+01 | 3.246E-81 | 4.450E+01 |
| | 2.546E-03 | 4.106E-40 | 3.949E+04 | 1.169E-09 | 1.000E+00 | 1.000E+00 | 0. | 0. | 1.861E-01 | 2.948E+00 |
| 640.00 | 3.288E+05 | 9.250E+03 | 1.383E+07 | 1.463E+06 | 4.643E-02 | 4.643E-02 | 1.090E+05 | 1.090E+05 | 5.330E-01 | 5.203E-02 |
| | 2.871E-06 | 2.871E-06 | 2.955E-79 | 3.425E-56 | 1.711E-14 | 1.711E-14 | 5.395E+04 | 5.394E+04 | 9.992E+00 | 1.091E-02 |
| | 2.012E-03 | 4.564E-42 | 4.766E+04 | 6.338E-10 | 1.000E+00 | 1.000E+00 | 0. | 0. | 1.691E-84 | 3.164E+01 |
| 640.00 | 2.179E+05 | 5.969E+03 | 1.094E+07 | 1.302E+06 | 2.454E-02 | 2.454E-02 | 9.864E+04 | 9.864E+04 | 3.526E-01 | 3.498E-02 |
| | 1.937E+04 | 2.089E+03 | 1.450E-82 | 1.950E-59 | 4.776E-15 | 4.776E-15 | 5.256E+04 | 5.256E+04 | 6.530E+00 | 6.403E-03 |
| | 2.303E-06 | 1.797E-06 | 8.506E+01 | 1.330E+03 | 1.330E+03 | 1.330E+03 | 3.961E+04 | 1.000E+01 | 8.006E-88 | 2.269E+01 |
| | 1.630E-03 | 2.234E-43 | 1.937E+04 | 3.445E-10 | 1.000E+00 | 1.000E+00 | 0. | 0. | 7.075E-02 | 1.148E+00 |
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| | 1.357E+04 | 1.529E+03 | 2.967E-06 | 1.113E-60 | 1.072E-15 | 1.072E-15 | 5.164E+04 | 5.163E+04 | 4.296E+00 | 6.456E-03 |
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