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SESAME-A SYSTEM OF EQUATIONS FOR THE SIMULATION OF AIRCRAFT IN --ETC(U)

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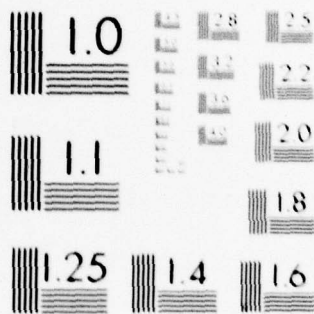
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**SESAME—A SYSTEM OF EQUATIONS
FOR THE SIMULATION OF AIRCRAFT
IN A MODULAR ENVIRONMENT.**

by

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10 B.N. Tomlinson

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1 INTRODUCTION

This Report describes a system of equations for the simulation of an aircraft's 'rigid-body' motion in real time using a digital computer. Known as SESAME - a System of Equations for the Simulation of Aircraft in a Modular Environment - it may be described as opening the door to flexible use of the simulator. Those parts of the mathematical model which are common to all aircraft, such as the equations of motion and axis transformations, have been created as a set of standard modules (written in Fortran), leaving the user to create only a small group of routines specifically to describe his aircraft. The two sets of modules are then linked together to produce a complete model program.

The simulator for which SESAME has been created changed from pure analogue to hybrid computing¹ in 1974. The computer system consists of a Xerox Sigma 8 digital computer linked to an Applied Dynamics AD4 analogue computer. This Report is concerned mainly with the digital computer aspects. In the early days of using this new computing facility, the aircraft's mathematical model, computed entirely digitally, was coded using SL1, a simulation language for solving sets of ordinary differential equations. With increasing experience and increasingly complex simulations, the single large program imposed by the SL1 language was found to be more and more inconvenient and the decision was taken to restructure the program into small, self-contained modules.

Such restructuring became feasible largely because a newly-created software package, for on-line parameter variation and inspection, provided the means to access and change, on-line, variables contained in subroutines.

Although the basic modules are themselves coded in Fortran, SL1 itself has been retained to provide the overall framework in which the modules sit. This is because SL1 provides facilities for numerical integration and for synchronisation with real-time.

The structure of the Report is as follows. After a discussion, in section 2, of the objectives to be achieved by the modular nature of SESAME, section 3 gives a brief theoretical background to the system equations, including such topics as choice of axes and definition of the equations of motion. This is followed in section 4 by an outline of how the equations to be solved are distributed among the specific routines. This is supplemented (in Appendix A) by a detailed definition of each routine and, as the ultimate specification for reference purposes, by a listing of the routines (Appendix B). Section 5 then describes the overall program structure in which the routines are embedded. Section 6 discusses how

communication among routines is achieved using the Fortran named COMMON facility, and how the user should adopt the same technique for his routines. Hybrid input/output (analogue to digital and digital to analogue conversion, and single bit discretas) is also described in section 6 in terms of what the user receives and must provide, while section 7 is a general "User's Guide", summarising what the system expects from the user, defining the set of routines and the data the user must provide, and outlining the choices the user may make regarding the atmosphere, turbulence and other features.

The Report has been written with three principal aims: to provide primary simulator users with a description of the standard computer model and an outline of how to build it into a full simulation; to provide simulator customers with an idea of how the model is formulated and what must be done to represent an individual aircraft, so that they can, if necessary, contribute to the creation of a complete simulation model; and to provide a general description of a computer model for others interested in doing something similar.

2 OBJECTIVES

Specific objectives to be achieved by the modular system of equations concern size, testing, transferability, communication and execution time, and are intended to overcome detailed weaknesses of the simulation language SL1. However, as explained later in section 5.1, SL1 is retained as the appropriate language for the overall program, containing the individual modules.

2.1 Size

A complete model program is large, often exceeding 20000 words of computer storage. If coded entirely in SL1 source language this means many lines of code. The process of translating the SL1 source code into Fortran and then compiling is slow and tedious and must be repeated in its entirety whenever a change is made at source level. The present scheme drastically cuts the size of the SL1 source program, which in itself will speed up the translation/compilation process. In addition, changes at SL1 level will be rare, since the detail of a simulation is relegated to a lower level of routine. The existence of subroutines also provides the potential ability to create overlays, in order to reduce main store occupancy.

2.2 Creation and testing

Creation and checking of modules will be easier than handling a large SL1 program since routines, such as for the generation of the aircraft's aerodynamic forces, can be defined, created and tested in isolation before being included in

the main program. Work could proceed in parallel on several routines, and be done by external users of the simulator, *ie* people who are not specialists in simulation as such.

Modifications will also be easier, since they should involve only revision of a single subroutine, its compilation and then creation of a new load module without having to repeat the SLI translation.

Using Fortran rather than SLI as the primary medium does not mean that all the useful SLI facilities, such as function generation by table look-up, must be discarded. These can still be used at the Fortran level, since each one involves a Fortran-callable subroutine or function. However, the calling sequence will, in general, be more complicated in Fortran than in SLI. SLI operators involving integration are not usable in subroutines without considerable effort.

2.3 Transferability

Having a modular structure means that simulation of a new aircraft requires only the creation of the routines specific to that aircraft. The standard parts can be picked up from libraries and special facilities, such as simulation of guidance beams, can readily be moved from simulation to simulation in subroutine form. With SLI the only way of transferring across an existing piece of code is by explicit inclusion of the source lines and punching of the necessary cards.

None of the modules includes any compromising feature which limits its employment to real-time simulation. Hence the routines described could also form the basis for a conventional digital model of aircraft dynamics for use in non-real-time studies.

2.4 Communication

A defect of the SLI language is the way most of the significant variables are lumped into one large block of labelled COMMON, the name of which is not fixed and the contents of which can change if the SLI source code is varied.

In this new system communication of variables among all the modules is achieved by using Fortran labelled COMMON, but under *user* control. This retains the advantage of using COMMON storage, that variables are conveniently accessible by any subroutine without using arguments, thus saving execution time.

2.5 Execution time

The aircraft's motion is computed by repeatedly integrating the differential equations. If a multi-pass integration technique is used, such as Runge-Kutta fourth order, there are some sections of the equations which are not part

of the dynamic loop and so need only be executed once per time step. Examples are calculation of ILS guidance and TV position signals. By having these elements as subroutines, it is easy to arrange that they are executed only as often as necessary and so save time for more important functions.

To date, aircraft model programs have been solved with only one basic loop or frame. SLI does provide a means to execute one part at a different iteration rate from another. Should circumstances arise where more than one frame time is necessary, recasting of the model program (at SLI skeleton level) will be aided by the simplicity of merely moving subroutine calls from one 'derivative' section to another, rather than blocks of code which would be necessary in a program coded completely in SLI. Communication between 'derivative' sections is also no problem when variables are in COMMON areas controlled by the user rather than by the SLI translator.

2.6 Data logging

Access to variables for data logging purposes is easy and convenient. A self-contained data logging routine can be written knowing that all variables may be accessed without special action and without run-time inefficiencies.

3 SYSTEM EQUATIONS

3.1 Choice of axes

The first requirement is to choose sets of axes in which to solve the fundamental equations of motion. In classic texts²⁻⁴ a set of axes fixed in the aircraft is generally chosen but, being a rotating frame of reference, such body axes result in the translational accelerations including angular velocity terms, as in

$$X - mg \sin \theta = m(\dot{u} + qw - rv) .$$

For efficient computer solution of the equations of motion, it is desirable to uncouple translational motion from rotational motion, a point which was made many years ago by Howe⁵ and reiterated recently⁶. This may be achieved by suitable choice of axes. Then, since rotational motion of aircraft is intrinsically more rapid than translational motion, solution of the rotational equations may be performed more frequently than the translational equations without an excessive computing load, and while maintaining overall accuracy.

Body-fixed axes still provide a natural frame for the solution of rotational equations of motion, with the advantage of constant moments of inertia. Choice

of axes therefore reduces to selecting an appropriate frame for the translational equations of motion.

So-called 'flight path axes' could be a suitable choice, with the origin at the aircraft's centre of gravity and the x axis aligned with the aircraft's velocity vector with respect to the ground. However, in the presence of winds and turbulence this introduces complications, so that, following Ref 7, the choice falls on earth-based axes.

3.2 Definition of axes

All axes systems used are orthogonal, right-handed triads.

3.2.1 Earth axes

Earth axes are an inertial frame assuming a flat, non-rotating earth. (See McFarland⁷ for the case of a spherical, rotating earth.)

The origin is at a datum point on the visual model* in use, typically at the runway threshold and on the centreline. The x-axis points northward (suffix N), the y-axis points eastward (suffix E), the xy plane being parallel to the earth's surface, and the z-axis (suffix D) points down to the centre of the earth.

3.2.2 Geometric body axes

Geometric body axes have their origin at the aircraft's centre of gravity and are located with respect to the aircraft by some geometric feature such as the longitudinal fuselage datum line. Once defined they are fixed in the aircraft. The x-axis points forward, the y-axis to starboard and the z-axis 'down'.

3.3 Aircraft attitude

Aircraft angular orientation with respect to the earth is defined⁸ by a conventional trio of Euler angles ψ , θ , ϕ . The heading angle ψ is measured from north and lies in the range $0, 360^{\circ}$; the elevation angle or pitch attitude θ is measured from the horizontal plane and lies in the range $-90, +90^{\circ}$; the roll (or bank) angle is measured from the horizontal plane and lies in the range $-180, +180^{\circ}$.

Rates of change of these angles may be related to the components of angular velocity of the aircraft by

* Outside world cues are provided by a closed-circuit TV system viewing a physical model of an appropriate terrain.

$$\left. \begin{aligned}
 \dot{\theta} &= q \cos \phi - r \sin \phi \\
 \dot{\phi} &= p + (q \sin \phi + r \cos \phi) \tan \theta = p + \dot{\psi} \sin \theta \\
 \dot{\psi} &= (q \sin \phi + r \cos \phi) \sec \theta
 \end{aligned} \right\} \quad (1)$$

and the angles themselves obtained by integration. However, a singularity occurs at $\theta = 90^\circ$. If all-attitude manoeuvring is desired, an alternative formulation of equations is necessary. No provision has yet been made for multiple rolls or turns.

3.4 Transformation from earth to body axes

Transformation of a set of variables from earth axes to body axes (or vice versa) is most conveniently achieved through the direction cosine matrix^{4,9}.

For example, the components of airspeed in body axes (u_B, v_B, w_B) are related to the components in earth axes (V_N, V_E, V_D) by

$$\left. \begin{aligned}
 u_B &= \ell_1 V_N + \ell_2 V_E + \ell_3 V_D \\
 v_B &= m_1 V_N + m_2 V_E + m_3 V_D \\
 w_B &= n_1 V_N + n_2 V_E + n_3 V_D
 \end{aligned} \right\} \quad (2)$$

where ℓ_1 etc are the direction cosines, given by

$$\left. \begin{aligned}
 \ell_1 &= S_{11} = \cos \theta \cos \psi \\
 \ell_2 &= S_{12} = \cos \theta \sin \psi \\
 \ell_3 &= S_{13} = -\sin \theta \\
 m_1 &= S_{21} = \sin \phi \sin \theta \cos \psi - \cos \phi \sin \psi \\
 m_2 &= S_{22} = \sin \phi \sin \theta \sin \psi + \cos \phi \cos \psi \\
 m_3 &= S_{23} = \sin \phi \cos \theta \\
 n_1 &= S_{31} = \cos \phi \sin \theta \cos \psi + \sin \phi \sin \psi \\
 n_2 &= S_{32} = \cos \phi \sin \theta \sin \psi - \sin \phi \cos \psi \\
 n_3 &= S_{33} = \cos \phi \cos \theta
 \end{aligned} \right\} \quad (3)$$

In matrix form, equations (2) may be written

$$\{u_B\} = S\{v_N\} \quad (4)$$

where $\{u_B\}$, $\{v_N\}$ are column matrices (after Hopkin⁴) and S , the transformation matrix, is orthogonal, its transpose S^T being the same as its inverse.

The inverse relationship, for earth axes variables in terms of body axis variables, is then given by

$$\{v_N\} = S^T\{u_B\}. \quad (5)$$

Thus, for example, the total forces (suffix T) applied in body axes (suffix X, Y, Z) may be transformed to earth axes (suffix N, E, D) by

$$\{F_{TN}\} = S^T\{F_{TX}\} \quad (6)$$

which, expanded, is

$$\left. \begin{aligned} F_{TN} &= S_{11}F_{TX} + S_{21}F_{TY} + S_{31}F_{TZ} \\ F_{TE} &= S_{12}F_{TX} + S_{22}F_{TY} + S_{32}F_{TZ} \\ F_{TD} &= S_{13}F_{TX} + S_{23}F_{TY} + S_{33}F_{TZ} \end{aligned} \right\} \quad (7)$$

Other vector components are related in the same way.

3.5 Equations of motion - translation

The components of acceleration with respect to the earth are obtained from

$$\left. \begin{aligned} \dot{v}_{KN} &= F_{TN}/m \\ \dot{v}_{KE} &= F_{TE}/m \\ \dot{v}_{KD} &= F_{TD}/m + g \end{aligned} \right\} \quad (8)$$

where the acceleration due to gravity, g , is assumed constant, and the forces F_{TN} etc in earth axes are obtained from the total forces in body axes F_{TX} , F_{TY} , F_{TZ} by the equations (7).

Integration of equations (8) yields the velocity components (v_{KN} , v_{KE} , v_{KD}) of the vehicle relative to the earth. Relative to the air mass, the velocity components of the aircraft are

$$\left. \begin{aligned} v_N &= v_{KN} - v_{WN} \\ v_E &= v_{KE} - v_{WE} \\ v_D &= v_{KD} - v_{WD} \end{aligned} \right\} \quad (9)$$

where v_{WN} , v_{WE} , v_{WD} are the components of the wind velocity relative to the ground.

The body-axes components of the velocity vector relative to the air may then be derived using equations (2) and (9), from which the velocity (or True Airspeed, TAS) is

$$v_T = \left(u_B^2 + v_B^2 + w_B^2 \right)^{\frac{1}{2}} \quad (10)$$

and equivalent airspeed is derived using the atmospheric density ratio

$$v = v_T \sigma^{\frac{1}{2}} \quad (11)$$

Angles of attack and sideslip are computed from¹⁰

$$\alpha = \tan^{-1} w_B / u_B \quad (12)$$

(α being in the range -180° , $+180^\circ$) and

$$\beta = \tan^{-1} v_B / \left(u_B^2 + v_B^2 \right)^{\frac{1}{2}} \quad (13)$$

(β being in the range -90° , $+90^\circ$ and taking the sign of v_B).

Derivatives of these angles with respect to time, needed to calculate the aerodynamic forces and moments, are created by simple difference equations. Flight path angles defining climb (γ) and track (χ) are derived from the velocity vector components relative to the ground, having first obtained the ground speed (v_K) as the horizontal component

$$v_K = \left(v_{KN}^2 + v_{KE}^2 \right)^{\frac{1}{2}} \quad (14)$$

$$\gamma = \tan^{-1} \left(-v_{KD} / v_K \right) \quad (15)$$

$$\chi = \tan^{-1} \left(v_{KE} / v_{KN} \right) \quad (16)$$

Positional coordinates x , y , h of the aircraft's centre of gravity are found by integrating the velocities

$$\left. \begin{aligned} \dot{x} &= V_{KN} \\ \dot{y} &= V_{KE} \\ \dot{h} &= -V_{KD} \end{aligned} \right\} \quad (17)$$

A block diagram of the translation equations is illustrated in Fig 1.

3.6 Equations of motion - rotation

It is assumed that the x and z body axes lie in a plane of mass symmetry so that products of inertia I_{yz} and I_{xy} are zero. Then the classical equations (Hopkin⁴, section 10.1) may be manipulated to give

$$\left. \begin{aligned} \dot{p} &= \left\{ L + \frac{I_{zx}}{I_z} N + \left[\frac{I_{zx}}{I_z} (I_z + I_x - I_y) \right] pq \right. \\ &\quad \left. + \left[(I_y - I_z) - \frac{I_{zx}^2}{I_z} \right] qr \right\} \left/ \left\{ I_x \left(1 - \frac{I_{zx}^2}{I_x I_z} \right) \right\} \right. \\ \dot{q} &= \left\{ M + I_{zx} (r^2 - p^2) + (I_z - I_x) rp \right\} / I_y \\ \dot{r} &= \left\{ N + \frac{I_{zx}}{I_x} L + \left[(I_x - I_y) + \frac{I_{zx}^2}{I_x} \right] pq \right. \\ &\quad \left. + \left[\frac{I_{zx}}{I_x} (-I_x + I_y - I_z) \right] qr \right\} \left/ \left\{ I_z \left(1 - \frac{I_{zx}^2}{I_x I_z} \right) \right\} \right. \end{aligned} \right\} \quad (18)$$

or

$$\left. \begin{aligned} \dot{p} &= CI_1 L + CI_2 N + (CI_3 p + CI_4 r) q \\ \dot{q} &= CI_5 M + CI_6 (r^2 - p^2) + CI_7 rp \\ \dot{r} &= CI_8 N + CI_2 L + (CI_9 p + CI_{10} r) q \end{aligned} \right\} \quad (19)$$

where CI_1 etc are constants evaluated during initialisation.

$$\begin{aligned}
 CI_1 &= I_z \left(I_x I_z - I_{zx}^2 \right) \\
 CI_2 &= I_{zx} \left(I_x I_z - I_{zx}^2 \right) \\
 CI_3 &= I_{zx} \left(I_x - I_y + I_z \right) \left(I_x I_z - I_{zx}^2 \right) \\
 CI_4 &= \left(I_z (I_y - I_z) - I_{zx}^2 \right) \left(I_x I_z - I_{zx}^2 \right) \\
 CI_5 &= 1/I_y \\
 CI_6 &= I_{zx}/I_y \\
 CI_7 &= (I_z - I_x)/I_y \\
 CI_8 &= I_x \left(I_x I_z - I_{zx}^2 \right) \\
 CI_9 &= \left(I_x (I_x - I_y) + I_{zx}^2 \right) \left(I_x I_z - I_{zx}^2 \right) \\
 CI_{10} &= -I_{zx} \left(I_x - I_y + I_z \right) \left(I_x I_z - I_{zx}^2 \right) .
 \end{aligned}
 \tag{20}$$

No terms are included in these equations (18) and (19) to allow for engine gyroscopic effects, but they could easily be added by the user when he provides the total moments L, M, N . It would also be straightforward to extend the equations to allow for a non-symmetric mass distribution.

Solution of the equations of rotational motion therefore consists in calculating the angular acceleration components from equations (19) given the total moments L, M, N ; integrating to obtain angular velocity components; transforming, using equations (1), to attitude rates; integrating again to attitude angles and calculating the direction cosines according to equations (3). This total process is illustrated in Fig 2.

3.7 Centre of gravity location

An aircraft's centre of gravity location is usually defined, in a fore-and-aft sense, in terms of a reference length such as the mean chord \bar{c} . Thus if the centre of gravity is quoted as being at $0.1\bar{c}$, then it is 10% of the reference chord *aft* of the origin. This convention is in a direction contrary to the normal positive sense of x , but will be retained here. The vertical location of the

centre of gravity, however, is defined as being measured in the positive z direction (*ie* downwards) from some origin.

Aerodynamic moment data may often be quoted relative to some reference centre of gravity position, so that for an actual operational centre of gravity position, some correction is necessary. This is provided for as follows. If the moment reference position of the centre of gravity is x_{cgref}, z_{cgref} and the actual centre of gravity position is x_{cg}, z_{cg} , all defined as fractions of some reference length c_{ref} then the differences are calculated as

$$\left. \begin{aligned} \Delta x_{cg} &= x_{cg} - x_{cgref} \\ \Delta z_{cg} &= z_{cg} - z_{cgref} \end{aligned} \right\} \quad (21)$$

Then differences are then available to correct aerodynamic moments to the current centre of gravity position.

3.8 Pilot position and positional rates

Given the coordinates x, y, h of the aircraft's centre of gravity, the pilot's position, needed to drive outside world displays, is obtained from

$$\left. \begin{aligned} x_{TV} &= x + (x_{pcg} \cos \theta + z_{pcg} \sin \theta) \cos \psi \\ y_{TV} &= y + (x_{pcg} \cos \theta + z_{pcg} \sin \theta) \sin \psi \\ h_{TV} &= h + (x_{pcg} \sin \theta - z_{pcg} \cos \theta) \end{aligned} \right\} \quad (22)$$

where

$$\left. \begin{aligned} x_{pcg} &= x_p + \Delta x_{cg} c_{ref} \\ z_{pcg} &= z_p - \Delta z_{cg} c_{ref} \end{aligned} \right\} \quad (23)$$

and x_p, z_p are the coordinates of the pilot's eye point, assumed to be on the aircraft centre line, and defined relative to the reference centre of gravity position.

If we put

$$\left. \begin{aligned} R_{xp} &= x_{pcg} \cos \theta + z_{pcg} \sin \theta \\ R_{hp} &= x_{pcg} \sin \theta - z_{pcg} \cos \theta \end{aligned} \right\} \quad (24)$$

then

$$\left. \begin{aligned} \dot{x}_{TV} &= \dot{x} - R_{xp} \dot{\psi} \sin \psi - R_{hp} \dot{\theta} \cos \psi \\ \dot{y}_{TV} &= \dot{y} + R_{xp} \dot{\psi} \cos \psi - R_{hp} \dot{\theta} \sin \psi \\ \dot{h}_{TV} &= \dot{h} + R_{xp} \dot{\theta} \end{aligned} \right\} \quad (25)$$

3.9 Accelerations in body axes

Linear accelerations at the aircraft's centre of gravity, at the pilot's head and elsewhere (*eg* for accelerometers) are needed.

Referred to body axes, the components (in units of *g*) of the acceleration of the aircraft's centre of gravity are

$$\left. \begin{aligned} a_{xcg} &= F_{TX}/W \\ a_{ycg} &= F_{TY}/W \\ a_{zcg} &= F_{TZ}/W \end{aligned} \right\} \quad (26)$$

These are referred to as the 'specific' accelerations and are the acceleration components that would be measured by a set of orthogonal, body-fixed, accelerometers aligned with the body axes and located at the centre of gravity of the aircraft. 'Absolute' accelerations, including the gravity components, are then

$$\begin{aligned} a_{xacg} &= a_{xcg} - \sin \theta &= a_{xcg} + S_{13} \\ a_{yacg} &= a_{ycg} + \sin \phi \cos \theta &= a_{ycg} + S_{23} \\ a_{zacg} &= a_{zcg} + \cos \phi \cos \theta &= a_{zcg} + S_{33} \end{aligned}$$

It should be remembered that a_{xacg} is not equal to \dot{u}_b because the body axis system is rotating, as explained in any text, such as Etkin³, Chapter 4.

At an arbitrary location $L(x_L, y_L, z_L)$, the components of specific acceleration are

$$\left. \begin{aligned} a_{x_L} &= a_{xcg} - \left[x_L (q^2 + r^2) - y_L (pq - \dot{r}) - z_L (pr + \dot{q}) \right] / g \\ a_{y_L} &= a_{ycg} + \left[x_L (pq + \dot{r}) - y_L (p^2 + r^2) + z_L (qr - \dot{p}) \right] / g \\ a_{z_L} &= a_{zcg} + \left[x_L (pr - \dot{q}) + y_L (qr + \dot{p}) - z_L (p^2 + q^2) \right] / g \end{aligned} \right\} \quad (27)$$

The indication of an accelerometer or a 'g' meter may then be derived from equations (27) given the location of the device. Similarly the linear acceleration components at the pilot's station (x_p, z_p) may be derived for use in driving motion systems. Further details of the accelerations computed are given in the description of the SACCBOD routine in Appendix A.

3.10 Wind, wind shear and turbulence

Wind

A datum mean wind is defined in speed and direction by V_{WKTO} and ψ_W , from which the components in earth axes are obtained as

$$\left. \begin{aligned} V_{WNLO} &= -V_{WKTO} \cos \psi_W \\ V_{WELO} &= -V_{WKTO} \sin \psi_W \end{aligned} \right\} \quad (28)$$

bearing in mind the convention that when ψ_W is zero, the wind is *from* the north. The vertical component of mean wind, V_{WDLO} , is normally assumed to be zero.

Wind shear

Wind shear is obtained as a multiplying factor f according to altitude, and the wind components at height are then

$$\left. \begin{aligned} V_{WNL} &= fV_{WNLO} \\ V_{WEL} &= fV_{WELO} \end{aligned} \right\} \quad (29)$$

This shear is effective only in magnitude, not in direction. Three choices are available: no shear ($f = 1.0$), logarithmic profile and linear profile. The initialisation process allows for actual wind at the initial height and sets up the aircraft's track to give a desired initial heading.

Turbulence

Turbulence in three orthogonal directions can be added to the components of the mean wind to give total wind components. Gust velocity components u_G, v_G, w_G are calculated by a new technique¹², based on the Statistical Discrete Gust theory of J.G. Jones¹³, which allows the intermittent character of the generated turbulence to be controlled. Scaled components of turbulence u_T, v_T, w_T are obtained by

$$\left. \begin{aligned} u_T &= u_{sig} u_G \\ v_T &= v_{sig} v_G \\ w_T &= w_{sig} w_G \end{aligned} \right\} \quad (30)$$

where u_{sig} , v_{sig} , w_{sig} are desired root-mean-square intensities. These turbulence components are considered to be along the wind, across the wind and vertical, so that the total fluctuating wind components, in earth axes, are

$$\left. \begin{aligned} V_{WN} &= V_{WNL} - (u_T \cos \psi_W - v_T \sin \psi_W) \\ V_{WE} &= V_{WEL} - (v_T \cos \psi_W + u_T \sin \psi_W) \\ V_{WD} &= V_{WDL} - w_T \end{aligned} \right\} \quad (31)$$

3.11 Properties of the atmosphere

The properties of the ICAO International Standard Atmosphere¹¹ are calculated up to a maximum height of 65616 ft by the routine SATMOS (see description of SVELOC2 in Appendix A). Given altitude, it returns the density ratio, speed of sound ratio, temperature ratio and pressure ratio for a standard day. A routine ATMOS is also available for hot days but this is not integrated into SESAME. Strictly the altitude input should be 'geopotential' but below 65616 ft it is adequate to treat geometric and geopotential altitude as interchangeable.

The user may optionally choose to use constant atmospheric properties (as in many classical studies) or else allow standard variation with altitude. A software flag KISA controls this option.

4 TECHNICAL IMPLEMENTATION

Section 3 has defined a set of equations which compose the standard processes of any aircraft simulation. These equations are distributed among a series of modules for solution by digital computer. This section briefly describes the routines and their functions. Full details of each routine are given in Appendix A and listings are given in Appendix B. In general, system routines have names beginning with S. The routines fall into four categories:

Initialisation	- SINIT, SYSCOM
Rotational motion	- SDCOS, SEULER, SACCROT
Translational motion	- SVELOC1, SALFBET, SACCLIN, SPATH, SVELOC2
Utility functions	- STV, SILS, SWIND, SACCOD, SATMOS, SCOUNT .

All the subroutines described in this Report are coded in Fortran. The particular dialect used is Xerox Extended Fortran IV, designed for the Xerox Sigma range of computers. It was not intended to use only those features of the language embodied in Standard Fortran IV and a few non-standard features have in fact been used. These include

variable names of up to 8 characters,
initialisation of COMMON variables within subroutines,
use of the NAMELIST feature (in SYSCOM only).

Conversion of the subroutines to run on another computer should, however, pose few problems.

4.1 Initialisation

Two routines (SINIT, SYSCOM) are specifically concerned with performing certain start-up, or initialisation, functions. Other initialisation functions may be performed internally in the other routines.

SINIT calculates various aircraft related constants, sets up initial height, derives initial values of atmospheric properties and initialises speeds and attitudes allowing for wind.

SYSCOM sets up communication with system variables by creating a NAMELIST table and reads 'semi-permanent' data changes from a file.

Execution of most routines during an initialisation pass is organised intrinsically by the SL1 model program (see section 5.2). Many routines may need to perform preliminary calculations. If their nature is such that they must be performed *once only* (otherwise errors will result) then a local flag must be created and the routine structured as in Fig 3a, with the flag set 'off' on entry (eg by a DATA statement). However, if there are no reasons why initial calculations should not be performed more than once there is a standard flag available in the system COMMON, JJCOMP, which takes the value 0 until the 'compute' button is pressed, and thereafter is 1. In this case the structure in Fig 3b can be used.

4.2 Rotational motion

A diagram of the information flow is shown in Fig 4. Rotational motion is calculated first, principally to provide the direction cosines required by the translational motion.

SACCROT calculates the three components of angular acceleration, in body axes, using equations (19), given total moments (supplied by the user) and inertia constants, equations (20), (calculated by SINIT).

SEULER calculates the rate of change of body attitude angles from the angular velocity components, using equations (1).

SDCOS calculates the nine direction cosines S_{ij} etc from the three attitude angles ψ, θ, ϕ using equations (3).

4.3 Translational motion

A diagram of the information flow is shown in Fig 5.

SVELOC1 derives components of velocity, relative to the air, in earth axes using equations (9) and transforms to body axes, using equations (2).

SALFBET takes the body axes velocity components and calculates $\alpha, \beta, \dot{\alpha}, \dot{\beta}$ using equations (12) and (13).

SACCLIN transforms total force components in body frame to inertial (earth) frame, using equations (7), then calculates the translational acceleration using equations (8). It may sometimes be desirable to separate the vertical from the two horizontal components so that vertical motion can be solved more frequently for better simulation of undercarriage dynamics.

SPATH calculates flight path angles from velocities in earth axes, using equations (15) and (16).

SVELOC2 calculates resultant airspeed, dynamic pressure, Mach number etc, using SATMOS for atmospheric properties. Some features are at present only valid for Mach number less than 1.0, as indicated in the routine.

4.4 Utility functions

Fig 6 shows the flow of information among the utility routines, all of which have something to do with the simulation environment, *eg* visual display, motion cues, wind etc.

STV calculates, from equations (22) to (25), positions and velocities to drive the TV visual system, and also handles the logic of belt positioning.

SILS calculates one or two segment ILS guidance beams.

SWIND controls the generation of turbulence and adds it to wind, modified by shear effects (if any).

SACCBOD calculates accelerations in body axes of the aircraft centre of gravity, from equations (26), and pilot station, accelerometers etc, from equations (27).

SATMOS calculates the properties (in ratio form) of the ICAO international standard atmosphere. It is an existing library subroutine and is not otherwise described in this Report.

A further utility routine, SCOUNT, not included in Fig 6, has nothing to do with the simulation of aircraft, but assists in the management of the calculation process, by setting an 'initialisation complete' flag, by keeping track of the sub-steps (if any) of the integration routine, and by picking up the current run number from the data logging system.

4.5 Units

With Aeronautics still retaining the use of such units as knots, it is difficult at present to make a wholehearted conversion to SI units. However, the equations set up are self-consistent so that a force in newtons acting on a mass in kilograms will produce an acceleration in m/s^2 and likewise, a force in pounds and mass in slugs will yield ft/s^2 . The routines as set up are intrinsically in the feet, pound, second system but alteration of a few conversion constants (gravity, etc) and datum values (air density, etc), would enable the whole system to work in SI units.

5 OVERALL PROGRAM STRUCTURE

5.1 Introduction

The program which provides the general framework for all the system routines is written in the simulation language SL1¹⁴.

The basic structure (Fig 7) consists of an INITIAL region, for start-up calculations, a DYNAMIC region and a TERMINAL region. (The TERMINAL region, however, has no relevance to real-time simulation.) This is a common form for continuous system simulation languages, like SL1 or CSMP. The DYNAMIC region contains one or more DERIVATIVE sections. These DERIVATIVE sections, each of which can have its own integration algorithm and step size, contain the routines which are the core of a simulation. During real-time operation, the code generated from each DERIVATIVE section is executed repetitively to produce the desired solution as a function of time. A listing of an aircraft simulation program with one DERIVATIVE section, or loop, is given in Appendix C, and corresponding flow charts of the execution sequence are shown in Fig 8. The reason for using SL1

is that two major facilities are provided by the language. These are synchronisation with real-time and a centralised integration scheme with a choice of five algorithms. Further details are contained in the Reference Manuals¹⁴⁻¹⁶ and in Ref 1.

The SLI program is translated into a series of Fortran modules. Communication is organised using Fortran labelled COMMON. To permit system COMMON to handle the main variables, however, some duplication of variables is necessary in order for SESAME routines to communicate with the integration operators.

This duplication is arranged through PROCEDURAL blocks, with the subterfuge that only those variables to be exchanged with the integration processes are contained in the argument list. Other variables thus remain invisible to the SLI translator and so may be placed in system COMMON. If they were visible to the SLI translator they would be placed in a separate COMMON area, no longer under control of the user.

For example, a PROCEDURAL block

```
PROCEDURAL (=VV)
```

```
    V = VV
```

```
END
```

picks up VV from the SLI labelled COMMON and places its value in V. In the opposite direction

```
PROCEDURAL (VVDOT=)
```

```
    VVDOT = VDOT
```

```
END
```

transfers VDOT to VVDOT, for use in the integration statement

```
VV = INTEG (VVDOT, VVIC).
```

5.2 Initialisation

In the normal course of events, the code generated by the SLI translator causes the DERIVATIVE section(s) to be executed just once at the end of INITIAL to calculate the initial values of all the derivatives. This has been augmented by explicit code (see near the 'END' of the INITIAL region in the SLI listing in Appendix C) to force these calculations to be done twice. This is necessary because routines at the end of the sequence (such as SVELOC2) produce variables, such as dynamic pressure, needed early on. Once the whole system is running, there is no problem. This slight idiosyncrasy needs to be remembered by the user. The other important point about initialisation is that at the start of a new run, a *fresh copy* of the program is loaded into main store from a disc file,

so all parameter values are restored to their datum values. However, the 'retained changes' facility (see section 7.7) permits revised parameter values to be retained from run to run.

5.3 PV100 - operator dialogue

A set of programs and routines, collectively known as the parameter variation package, exists to enable the user to interact on-line with the parameters of the simulation. The principal item is PV100, the operator dialogue routine, which provides a wider range of facilities than the 'interpreter' inherent in SL1. PV100 enables the user, on-line and during any phase of a simulation flight, to access, display and amend any variable within the scope of the model program and its subroutines. Variables may be referred to by name (the principal function of routines SYSCOM and USERCOM is to provide tables of names for use by PV100), and in addition the contents of *any* memory location may also be displayed. A display may be in alternative styles, *eg* binary, hexadecimal, integer or 'real' format. Selected changes may be 'retained' to operate for subsequent runs, otherwise the change vanishes at the end of the current run. A readable memory dump may be printed, such as all the parameters in system COMMON. There is also a facility for forcing an 'automatic hold' or freeze if a variable falls within defined limits. A description of the full facilities is given elsewhere¹⁷.

During initialisation there are four explicit calls to PV100 inserted at strategic points in the INITIAL region, as can be seen by inspection of the SL1 listing in Appendix C. These calls to PV100 are only executed if a switch (Desk Switch 1) on the simulator control desk is set on. These individual calls to PV100 may be identified by reference to the indicator ITP, as follows.

- ITP = 1 After initial conditions or retained changes have been input, but before SINIT. Enables IC values to be altered, and other changes to be inserted before the main initialisation calculations of SINIT. In particular, if the frame time is to be altered, it should be done here, using FRAMET1, DELT1 for Loop 1 and similar variables for Loop 2 (if present).
- ITP = 2 After SINIT but before the integrator IC values are actually set up.
- ITP = 3 At end of INITIAL but before analogue to digital converter (ADC) read and DERIVATIVE section(s) initialised.
- ITP = 4 After DERIVATIVE section(s) initialised and ADC read. DAC values are calculated but not yet set.

6 COMMUNICATION

6.1 Introduction

Communication among all the routines which comprise the aircraft model program is achieved by Fortran labelled COMMON. Labelled COMMON designates a block of contiguous memory locations which may be accessed by any subroutine in which the COMMON block is declared. This technique provides flexibility and also avoids the time penalty associated with using arguments in subroutine calls.

Two large blocks of labelled COMMON are employed. One, named SYSTEM, is an inherent part of the standard subroutines and contains all the state variables and other parameters common to any aircraft simulation. This is of fixed size and has its variables in predefined locations. The other, named USER, is set up, in terms of size and content, by the user to handle variables specific to his particular simulation, *eg* the aerodynamic force coefficients, engine forces etc.

6.2 System COMMON

This is defined as

```
COMMON / SYSTEM / A(1000), L(400)
```

where the array A contains real variables and L contains integer variables. An index to all the variables, in numerical and alphabetical order, is provided in Appendices D and E.

If the user wishes to pick up the current value of angle of attack (say) he needs to include in his routine

```
COMMON / SYSTEM / A(1000), L(400)
```

```
EQUIVALENCE (ALFAD , A(112))
```

and then ALFAD can be used freely in his routine. System variables must *not* be altered by the user.

6.3 User COMMON

This is defined for example as

```
COMMON / USER / B(1000), M(100)
```

where the array B is for real variables and M for integer variables. Names and sizes of these arrays are defined by the user, but the COMMON name USER must be employed. Sizes should be kept as small as possible, in order to avoid sterilising areas of core unnecessarily. However, if the size is too small, the user will have to increase it frequently, with consequent work updating *all* routines in which the COMMON statement appears.

The user will choose his own variable names and allocate space in the COMMON arrays. This will normally be done by EQUIVALENCE techniques, for flexibility. (Routines could, in fact, be created and checked in the first place without considering inter-routine communication.)

6.4 Documentation aids

A utility program has been created, called COMMLIST, to assist the user in keeping track of his variable names and locations. As he creates a variable, the user punches a card defining the variable name, its meaning and the routine in which it is calculated. This is similar to a scheme described by Bean¹⁸. The program COMMLIST can then produce an index of names in alphabetical order, of locations in numerical order or of names according to the routine in which they are created or used. A brief guide to the program COMMLIST is given in Appendix F. The lists in Appendices D and E, G and H have been produced by this program.

6.5 Access to variables at run-time

In order to be able to access his variables at run-time, to inspect and change values via PVI00¹⁷, the user must create a NAMELIST table of his variable names. This is achieved in the routine USERCOM, which must be written by the user. The bulk of this routine will be COMMON (or EQUIVALENCE) statements, referencing the variables by name. Its structure will be identical to the routine SYSCOM which does the same job for system variables. A listing of SYSCOM is included in Appendix B.

6.6 Hybrid input/output (ADC, DAC)

6.6.1 Introduction

Hybrid input/output, that is analogue to digital conversion (ADC) and digital to analogue conversion (DAC), is integrated into SESAME so that the user merely has to define entries in a set of tables incorporated in system COMMON. Conversion and scaling then occurs automatically. The general form of conversion required is of the form

$$y = ax + b$$

where a is a scale factor and b is a bias. For ADC, x would be a scaled value and y a value in 'engineering' units whereas, for DAC, x would be in engineering units and y a value scaled appropriately for output. The present implementation does not include any bias.

Data transfer in both directions employs a special piece of hardware known as the DMS12 (Direct Memory Sub System) which is a processor capable of operating in parallel with the computer's central processor. Use of this device provides for an element of parallel operation which is exploited in the software to save execution time.

Overall, the software scheme offers the user convenience - because he only has to set up data tables; flexibility - because the tables can be changed on line; and speed - because the hardware is fully exploited. The operating routines, coded in assembler, are not described in this Report.

6.6.2 Analogue to digital conversion

Analogue to digital conversion, and scaling, are executed prior to entry into the Derivative Section of the SL1 model program, where the dynamic equations are solved. The main scaling calculation performed is of the form

$$YADC(I) = ADC(NADC(I)) * AADC(I)$$

where ADC is the array of raw converted values, nominally in the range ± 1.0 , held in the SL1 labelled COMMON Z99999.

NADC is the array of ADC channel numbers

AADC is the array of scaling factors, set up by the user

YADC is the array of input values in engineering units (degrees etc) ready for use.

All 32 channels are read in raw form into the array ADC, but scaling and transfer to YADC stops when the first zero element in NADC is reached. Because of the parallel nature of the hardware (DMS12, mentioned above) scaling is begun as soon as the first raw converted value is available. Conversion of further channels then proceeds concurrently with scaling. To avoid the danger of scaling a channel before it has been converted, it is important, therefore, that ADC channels are kept in numeric order and are used, as far as possible, without large gaps. For example, to use channels 1, 3, 7, 9 is better than 1, 17, 24, 30. To use 1, 2, 3, 4 is best of all. Thus, for simplicity, $NADC(I) = I$.

The data structure being in table form allows considerable operational flexibility. For example, in the event of failure of ADC channel 2, the variable being input on this channel can be redirected to channel 9 (say) simply by repatching on the analogue computer and by changing the contents of NADC(2) from 2 to 9 via the keyboard. The scaling AADC(2) would not need to be altered. The necessary changes can all be achieved on-line and no program changes are necessary. However, the warning of the previous paragraph should not be overlooked.

At present 32 ADC channels are available and supported by software. Provision has been made for enlargement, however, by reserving 64 contiguous locations for each of the arrays AADC, YADC, NADC in the COMMON storage area.¹

The SL1 model program includes in its source code (Appendix C) a sequence of the form

```
PROCEDURAL (=ADC(1))
END
```

in order to ensure that the key driving routine Z9991 is called. No special code has to be created by the user.

The user does, of course, wish to use the result of the conversion and scaling processes, as held in YADC. To do so he may either use an element of YADC directly, as in the following example

```
CL = CLETA*YADC(7) + .....
```

or may give the element of YADC his own names via the usual EQUIVALENCE declarations *viz*

```
DIMENSION YADC(32)
EQUIVALENCE (YADC(1), A(401))
EQUIVALENCE (ETAD , YADC(7))
```

and then

```
CL = CLETA * ETAD + .....
```

To make his variable names accessible via PV100, the user could include them in subroutine USERCOM.

6.6.3 Digital to analogue conversion

Digital to analogue conversion occurs once per frame, *after* the main integration loop. The DAC software scales output variables to be in the settable range for DACs and DCUs (otherwise known as vari-DACs).

In principle, the same calculation technique is adopted as for ADC. The special difficulty for variables to be output to DACs is that they must be selected from any location in the system or user COMMON arrays (A or B) and must be routed either to proper, four-quadrant DACs (the first 32) or to two-quadrant vari-DACs (the next 16). An additional requirement is that it should be possible to set DACs from either of two loops. (This description refers for completeness to two loops. For the moment, however, only Loop 1 is operational.)

To achieve these objectives, data for four arrays must be defined by the user.

- ADAC array of scaling factors. A variable in engineering units is multiplied by the scaling factor in the appropriate element to give a result in the desired range (nominally ± 1.0).
- NADC is the array of pointers defining which variables are to be converted. The pointers may refer to the 'A' or 'B' arrays in any sequence. Distinction between the source arrays is controlled by arrays L1DAC, L2DAC below.
- L1DAC defines the source of data for each channel to be converted in Loop 1.
- L2DAC defines the source of data for each channel to be converted in Loop 2. Each element of L1DAC, L2DAC can take the value 0, 1 or 2: 1 means that the data for scaling is to be taken from array A and 2 that it comes from array B. If 0 is set, no scaling is performed.

As an example, if $NDAC(6) = 112$, $L1DAC(6) = 1$, $ADAC(6) = 0.1$ then DAC channel 6 is to be used to output, at the end of Loop 1, variable $A(112)$, *ie* ALFAD, angle of attack in degrees, scaled to ± 10.0 .

This structure provides flexibility by enabling changes to be introduced on-line. For example, by changing $NDAC(6)$ from 112 to 241 (say), and changing the scaling $ADAC(6)$ to suit, a different variable from the same array can be output on a given DAC. The source array (A or B) can also be easily changed, via L1DAC.

Operational considerations

- (1) Of the 48 DAC channels available, the first 32 are true DACs, while the rest are only two-quadrant devices. The user needs to remember this when allocating channels, so that 33-48 are only used for variables which do not change sign, *eg* airspeed. Provision has been made for expansion to 64 channels by reserving extra space for ADAC, NDAC in the COMMON area.
- (2) For those DAC channels not used, the corresponding elements of ADAC should be set to zero.
- (3) A set of default hardware addresses associated with channel numbers is defined in the table IDACAD. DAC addresses can be reassigned during initialisation.
- (4) Timing tests have given the following results:

Convert and scale 32 ADC channels	1.2 ms
Scale and convert 48 DAC channels	3.8 ms .

All channels are converted, but only those specified are scaled and stored, so that time can be saved if fewer channels are needed. 008

6.6.4 User summary of system COMMON relevant to ADC/DAC

A	301	364		401	464		501	564
	1	AADC	64		1	YADC	64	
							1	ADAC
								64

A System COMMON array (real)
 AADC* Array of scaling factors for ADC
 YADC Array of converted variables
 ADAC* Array of scaling factors for DAC

L	11	74	82	144		305	352	353	400
	1	NDAC	64	1	NADC	64	1	L1DAC	48
								1	L2DAC
									48

L System COMMON array (integer)
 NDAC* Array of pointers defining variables in 'A' array and user's 'B' array to be converted
 NADC* Array of ADC channel numbers
 L1DAC* Array of DAC source pointers for Loop 1
 L2DAC* Array of DAC source pointers for Loop 2

6.7 Hybrid input/output (discretes)

6.7.1 Introduction

Discretes are single-bit logic lines enabling on/off information to be communicated into and out of the computer. These lines are read and set automatically and so are conveniently available to the user.

6.7.2 Summary of lines available

A number of lines are available in each direction

- (a) between the digital computer (Sigma 8) and the analogue computer (AD4) and
- (b) between the digital computer and other external hardware, such as the simulator cockpits and the control desk. The numbers and types are summarised in the table below, together with the relevant driving routine.

* These items must have values supplied by the user. It is recommended that, for convenience, all such data be located in one routine, such as OUTSR, or a self-contained 'information' routine.

Type	Location	Number	Direction	Subroutine
(1) AD4 sense lines	AD4 logic patch panel	16	To Sigma 8	READSLR
(2) AD4 control lines	AD4 logic patch panel	16	From Sigma 8	SETCLR
(3) Patchable sense lines	Rack N logic patch panel	32	To Sigma 8	} READSCR
(4) Desk switches	Bay 5 of control desk	32	To Sigma 8	
(5) Relay change-overs	Rack N logic patch panel	32	To Sigma 8	} SETDSCR
			32	

The driver routines READSLR etc are themselves executed by one of two supervisor routines DSCRT1 and DSCRT2. DSCRT2 is only relevant if the model program is structured to have two iteration loops.

6.7.3 Software interface

Discrete information to be input or output is communicated via the labelled COMMON system, viz
COMMON/SYSTEM/A(1000), L(400).

The basic routines which handle the hardware are called implicitly and convert from bit patterns in 32-bit words to arrays of integers, as defined below. Each integer can take the value 0 or 1. Thus no coding or decoding (packing or unpacking) of bits is necessary by the user.

The layout of the relevant parts of L is

L	150	151	166	170	171	186	190	191	222	223	254	270	271	302
	1 ISLR 16			1 ICLR 16			1 IP 32		1 IDS 32			1 ICO 32		
	IAD4SL			IAD4CL			IDSCFL			IPCOFL				

- where ISLR(16) is the AD4 sense line array, ISLR(1) corresponding to DGS00 on the AD4 patch panel (remember the AD4 is marked in octal!)
- ICLR(16) is the AD4 control line array, ICLR(1) corresponding to DGC00 on the AD4 patch panel
- IP(32) is the array of patchable sense lines
- IDS(32) is the array of desk switches
- ICO(32) is the array of relay change-overs

IAD4SL, IAD4CL, IDSCFL, IPCOFL are flags, defined in detail in section 7.4.1 below, which control in which iteration loop, if any, the discrettes routines are executed.

All these names are defined in SYSCOM, to be accessible by PV100. For the user to obtain access to ISLR(3), for example, he will include in his routine

```
COMMON/SYSTEM/A(1000), L(400)
```

and either

```
EQUIVALENCE (ISLR(1), L(151))
```

```
DIMENSION ISLR(16)
```

or

```
EQUIVALENCE (ISLR(3), L(153))
```

The former is more general. Discrete information is then available for use in such constructs as

```
IF (ISLR(3).EQ.1) CALL XYZ
```

6.7.4 Dedicated functions

Some of these discrete lines are dedicated to certain functions within SESAME, as summarised in the following list.

<u>Line</u>	<u>Purpose</u>	<u>Routine</u>
ISLR(4)	Slew forward	STV
ISLR(5)	Slew back	STV
ICLR(16)	TV Desync	STV
IDS(1)	PV100 select	SL1
IDS(5)	TV cycle	STV
IDS(6)	X TV reset	STV
IDS(7)	Y TV reset	STV
IDS(8)	Turbulence	SWIND

7 USER'S GUIDE

7.1 What the system expects from the user

The user is required to provide the three components of total force (FTX, FTY, FTZ) and the three components of total moment (XLLTOT, XMMTOT, XNNTOT), all in body axes. Thereafter the appropriate integrations, resolutions etc occur, with the system providing back to the user all the state variables from which the forces etc are generated. Various constants must also be provided. These are described in section 7.3.

7.2 Typical user routines

The user is required to create the following set of routines, which may perform some or all of the tasks indicated.

'Input'

CONTROLS takes the raw control inputs from the pilot, applies any non-linear gearings, computes autostabiliser contributions and finishes up with the total control surface deflections, for use by the aerodynamics routines. It may also organise the computation of engine performance, including dynamics, and total thrust, momentum drag etc.

'Calculation loop'

TOTF computes aerodynamic force coefficients etc, finishing up with three components of total force from all sources.

TOTM computes aerodynamic moment coefficients etc, finishing up with three components of total moment from all sources.

'Output'

OUTSR computes miscellaneous functions, *eg* scalings of non-linear instruments, navigation and guidance and handles data logging.

'Initial'

USERCOM contains the names of all the variables the user may wish to access via PVI00, and also reads semi-permanent data changes from a file.

- * These routines are actually called at SL1 level. All are executed in a DERIVATIVE section, except USERCOM, which is executed in INITIAL.
- * All these routines are likely to be umbrella routines, in the sense that they are likely merely to organise the calling of other, more detailed, routines. For example, TOTF may call a routine to compute all ground reactions, tyre forces etc.
- * Ideally, TOTF and TOTM should be kept separate, so that they can, if necessary, be executed in different loops at different frame times.
- * Routines in the calculation loop may be executed up to four times per frame, depending on the integration technique employed, *eg* Trapezoidal, Runge-Kutta fourth order. All other routines are only executed once per frame (see section 5.4).
- * Each routine should, as far as possible, contain its own constants.
- * The method for communication of variables other than by lengthy argument lists has been described in section 6.

7.3 Data the user must provide

In addition to the primary forces and moments (FTX, XLLTOT, etc) and initial values (section 7.5), the user must provide values for a number of constants and parameters. These fall into such categories as basic data, hybrid input/output and external environment. They are described briefly below and listed in full in Appendices G and H. Typically the values will be provided by DATA statements

in appropriate subroutines (eg TOTM, TOTF), unless default values are already provided, in which case new values should be provided in the SYSCHNG file (section 7.7). Zero values should be set up if the parameter is not relevant.

Aircraft basic data

Moments of inertia	XIX, XIY, XIZ, XIZX
Centre of gravity	XCGREF, ZCGREF, ZCG
Span, wing area etc	SPAN, SWREF, STAIL, XLTAIL, CREF
Pilot location	XP, ZP
Coordinates of slip ball	X1, Y1, Z1
Coordinates of g meter	X2, Y2, Z2
Coordinates of accelerometer (AX3)	X3, Y3, Z3
Coordinates of accelerometer (AY4)	X4, Y4, Z4
Coordinates of accelerometer (AZ5)	X5, Y5, Z5

Timing

Frame time	FRAMET1, FRAMET2
Step size	DELT1, DELT2

Hybrid input/output

Scaling factors for analogue to digital conversion etc, (for full details refer to section 6.6)	AADC, ADAC L1DAC, L2DAC, NDAC, NADC
Output discretises (see section 6.7)	ICLR, ICO

External environment

Turbulence rms	USIG, VSIG, WSIG
Turbulence character	NG, SFRACG, SRDECAY
Ship speed	VSHIPKT

Additional integer parameters which can take one of several specific values and thereby select alternative functions are described in the next section.

7.4 Options available

A number of choices may be made by software flags or hardware switches. These are summarised below, with default values where relevant.

7.4.1 Software flags

(a) Variation of atmospheric properties

KISA	default 0 set in SINIT
0	constant sea level conditions at all times
1	standard atmosphere as function of current height
-1	constant properties appropriate to initial height (HIC).

FOR KISA = 1, SATMOS is called within SVELOC2 to calculate the new properties. Otherwise, constant values are set up within SINIT.

- (b) Selection of constants for TV belt in use
- | | |
|------|--------------|
| NTVB | no default |
| 1 | 700:1 model |
| 2 | 2000:1 model |
| 3 | 5000:1 model |
- (c) ILS on/off
- | | |
|-------|------------|
| LSILS | no default |
| 0 | ILS off |
| 1 | ILS on |
- (d) Type of ILS beam
- | | |
|--------|---|
| ILSFLG | no default, value obtained from XILSFLG (see section 7.5.2) |
| 1 | 3° straight beam |
| 2 | 6° straight beam |
| 3 | 6° changing to 3° at height HKINK (qv) |
- (e) Discrettes in and out (see also section 6.7)
- | | |
|--------|---|
| IAD4SL | AD4 sense lines (default 1 set in DSCRT1) |
| IAD4CL | AD4 control lines (default 1 set in DSCRT1) |
| IDSCFL | discrettes in to Sigma (default 1 set in DSCRT1) |
| IPCOFL | discrettes out from Sigma (default 0 set in DSCRT1) |
| 0 | do not execute at all |
| 1 | execute in DSCRT1, <i>ie</i> in fast loop |
| 2 | execute in DSCRT2, <i>ie</i> in slow loop (if any) |
- (f) Wind shear
- | | |
|------|-------------------------|
| ISHR | default 1, set in SINIT |
| 1 | no shear |
| 2 | logarithmic profile |
| 3 | linear profile |

The value of ISHR is obtained from XISHR set up in the Initial Conditions file.

- (g) Control of random number generation for turbulence
- | | |
|-------|---|
| LSEED | default 0, set in SWIND |
| 0 | seeds for random number generation derived from time of day |
| 1 | constant seeds employed, enabling a repeatable turbulence sequence to be obtained |

7.4.2 External switches

<u>Desk switch</u>	<u>Name</u>	<u>Purpose when set on</u>
1		Calls PVI00 during INITIAL
5	LCYCLE	TV belt cycles continually
6	LXTVIC	Resets TV x position
7	LYTVIC	Resets TV y position
8	LTURB	Turbulence
TV slew	LFWD	TV belt (and x position) moves forward at maximum rate
TV slew	LBACK	TV belt (and x position) moves backward at maximum rate

7.5 Initial conditions and initial values

7.5.1 Initial conditions

The standard SLI model embodies 12 integrations, each of which requires an initial condition. These are given in the table below as 'SLI names'. Many of these variables do not form a natural or convenient set for the user, who is more interested, for example, in specifying an initial airspeed rather than components of speed relative to the ground, or an initial angle of attack rather than pitch attitude. Hence SINIT performs various calculations to transform a user's initial values into those that the system requires.

One particular feature is that, regardless of the wind, the ground speed components are derived implicitly to satisfy the specified initial *heading* PSIDIC so that any datum wind or wind shear conditions are not revealed inadvertently to the pilot. More detail is given in the description of the SINIT routine in Appendix A.

<u>SLI names</u>	<u>Source</u>	<u>Definition</u>
VVKNIC	Calculation	Velocity comp rel to ground, north
VVKEIC	Calculation	Velocity comp rel to ground, east
VVKDIC	Calculation	Velocity comp rel to ground, down
SXIC	XIC	X position
SYIC	YIC	Y position
SHIC	HIC	Height
PPIC	PDIC, default zero	Rate of roll, body axes
QQIC	QDIC, default zero	Rate of pitch, body axes
RRIC	RDIC, default zero	Rate of yaw, body axes
PPHIC	PHIDIC, default zero	Roll attitude angle
TTHIC	Calculation	Pitch attitude angle
PPSIC	PSIDIC	Heading angle

7.5.2 Initial values

Initial values are parameters relevant to the current 'run' and are not in general true initial conditions for integration. However, those initial conditions listed above that are not calculated are obtained from a set of initial values created by the user in a file. This file is read, during the INITIAL phase, by the routine RDICFILE and its contents stored in a 20-element array (A(191) - A(210)) which is part of system COMMON.

At present only 14 elements are actually used (as defined by the value of NVALS). These are

<u>Name</u>	<u>Element</u>	<u>Definition</u>	<u>Units</u>
BETADIC	A(191)	Sideslip angle	degrees
ALFADIC	A(192)	Angle of attack	degrees
GAMDIC	A(193)	Climb angle	degrees
VKTIC	A(194)	Airspeed	knots
XIC	A(195)	X position	feet
YIC	A(196)	Y position	feet
HIC	A(197)	Height	feet
W	A(198)	Aircraft weight	pound
XCG	A(199)	Aircraft centre of gravity	fraction of ref chord
XILSFLG	A(200)	ILS flag (actually used in integer form, ILSFLG)	
XISHR	A(201)	Wind shear flag (actually used in integer form, ISHR)	
VWKTØ	A(202)	Datum wind speed	knots
PSIWD	A(203)	Wind direction	degrees
PSIDIC	A(204)	Aircraft heading	degrees
Spare	A(205) - A(210)		

Additional items could be read by increasing NVALS, eg by inputting a new value from the semi-permanent changes file (see section 7.7) read in SYSCOM.

7.6 Modification status

To keep track of the modification status of each routine, it is recommended that the user allocate an identifier per routine and assign a value to identify the version. For example, with the routine TOTF

DATA MTOTF / 1 /

to indicate version 1, or

```
DATA MTOTF / 171176/
```

to indicate the date of the current version. These values should be changed whenever the routine is modified. By placing these status identifiers in user COMMON, the current versions of each routine can be readily checked on-line.

This technique has been adopted for all the SESAME routines. The name of the version identifier is the routine name preceded by K, *eg* for routine SALFBET, the identifier is KSALFBET and contains the date in integer form. These identifiers are held in system COMMON (see Appendix E).

Identification of a new version of the executable program, or load module, is desirable. The SL1 model program has a version number (IVERSION) for its *source* code, but this is not changed if a new load module is built without changing the SL1 source. Identifying individual routines as above will help but a global load module identifier could also be created in a 'history' routine, the only purpose of which is to set a version number for the load module, *eg*

```
DATA LHARRIER / 240776 /
```

and perhaps also to include a modification history in 'comment' form.

A recent modification to the loader utility in the RBM operating system now places the date and time of load module creation into the program header. This information can be inspected from the keyboard.

7.7 Changes to parameters

It is possible to introduce lasting parameter changes into a completed and working aircraft model program without recoding.

On-line changes can be achieved from a keyboard, during any mode of a simulation, through the program PV100¹⁷. The user has the option, at the time of making the changes, of declaring that the changes be 'retained', in which case they are automatically copied into a file and read back again (by PV300) at the start of each subsequent run. These changes are initially name-orientated, but PV300 relies on absolute address so that if alternative aircraft model programs are used, the retained changes file needs to be reset.

Semi-permanent changes to a user's parameters held in USER COMMON may be achieved by creating (from cards) a file called USERCHNG which is read each time the routine USERCOM is executed. Changes to parameters in SYSTEM COMMON may be achieved by a similar process, via the file SYSCHNG. All these changes work only by parameter name, as explained in the description of SYSCOM in Appendix A.

7.8 Operational considerations

The binary versions of all SESAME routines, in relocatable form (ROM), are held in files on disc and may be incorporated when building, via OLOAD, the final executable program. To ensure that the size of user defined COMMON is correctly set up, it is essential that a user ROM containing the definition of USER COMMON be loaded *before* SDAC.

If data logging is in use, the correct run number may be obtained by inspecting the variable NRUN.

8 CONCLUSIONS

A system of equations and associated computer subroutines has been developed to make it easy to create an aircraft model program for real-time flight simulation. Several simulations have been completed and it has been found to be very useful. The objectives of the scheme have been achieved. In particular, the resulting model program is more efficient during execution in terms of time required and the modular structure has also given the desired benefits at the program development stage.

The facilities of SESAME are described as they exist at the time of publication of this Report. Extensions and enhancements may easily be added as new needs arise.

Furthermore, the routines as described in this Report are not specific either to real-time simulation or to the computer on which they have been developed. They are written in Fortran and, supplemented by appropriate integration techniques, could be used on other computers for general purpose calculations of aircraft dynamics in six degrees of freedom.

Appendix ADESCRIPTION OF INDIVIDUAL SESAME ROUTINES

<u>Section</u>	<u>Routine</u>	<u>Source file</u>	<u>Binary file (ROM)</u>
A.1	SACCBOD	SACBS	SACBR
A.2	SACCLIN	SACLS	SACLR
A.3	SACCROT	SACRS	SACRR
A.4	SALFBET	SALFS	SALFR
A.5	SCOUNT	SCNTS	SCNTR
A.6	SDCOS	SDCSS	SDCSR
A.7	SEULER	SEULS	SEULR
A.8	SILS	SILSS	SILSR
A.9	SINIT	SINTS	SINTR
A.10	SPATH	SPTHS	SPTHR
A.11	STV	STVVS	STVVR
A.12	SVELOC1	SVL1S	SVL1R
A.13	SVELOC2	SVL2S	SVL2R
A.14	SWIND	SWNDS	SWNDR
A.15	SYSKOM	SYSCS	SYSCR
A.16	DSCRT1	SCR1S	SCR1R
A.16	DSCRT2	SCR2S	SCR2R
A.17	ISDSCR	ISDCS	ISDCR

- 40
- A.1 Subroutine SACCBOD
- A.1.1 Purpose Calculates accelerations, in body axes, of aircraft centre of gravity (cg), pilot and various accelerometer locations.
- A.1.2 Call CALL SACCBOD
- A.1.3 Inputs P, Q, R
PDOT, QDOT, RDOT
RG, W
FTX, FTY, FTZ
S13, S23, S33
XP, ZP
X1, Y1, Z1; X2, Y2, Z2; X3, Y3, Z3; X4, Y4, Z4; X5, Y5, Z5
- A.1.4 Outputs AXCG, AYCG, AZCG
AXACG, AYACG, AZACG
AXP, AYP, AZP
AZAP, AZCG1
AY1, AZ2, AX3, AY4, AZ5
- A.1.5 Data required XP, ZP
X1, Y1, Z1; X2, Y2, Z2; X3, Y3, Z3; X4, Y4, Z4; X5, Y5, Z5
- A.1.6 Description (NB all accelerations in units of g) - see also section 3.9

A.1.6.1 Specific accelerations at aircraft centre of gravity (as measured by an accelerometer).

$$a_{xcg} = F_{TX}/W$$

$$a_{ycg} = F_{TY}/W$$

$$a_{zcg} = F_{TZ}/W$$

Note that in steady level flight, with $\theta = 0$, a 'normal' accelerometer at the centre of gravity registers -1 g and in a pull-up, for example, registers -1.5 g.

A.1.6.2 Absolute accelerations at aircraft centre of gravity

$$a_{xacg} = a_{xcg} + S_{13}$$

$$a_{yacg} = a_{ycg} + S_{23}$$

$$a_{zacg} = a_{zcg} + S_{33}$$

S_{13} , S_{23} , S_{33} are direction cosines, eg $S_{13} = -\sin \theta$.

A.1.6.3 Accelerations at pilot

$$a_{xp} = a_{xcg} - \left[x_p (q^2 + r^2) - z_p (pr + \dot{q}) \right] / g$$

$$a_{yp} = a_{ycg} + \left[x_p (pq + \dot{r}) + z_p (qr - \dot{p}) \right] / g$$

$$a_{zp} = a_{zcg} + \left[x_p (pr - \dot{q}) - z_p (p^2 + q^2) \right] / g$$

A.1.6.4 Absolute normal acceleration at pilot (or 'manoeuvre g' used for motion cues)

$$a_{zap} = a_{zp} + S_{33}$$

A.1.6.5 Acceleration relative to 1 g for recording

$$a_{zcg1} = a_{zcg} + 1.0$$

A.1.6.6 Acceleration for slip ball (located at x_1, y_1, z_1)

$$a_{y_1} = a_{ycg} + \left[x_1 (pq - \dot{r}) - y_1 (p^2 + r^2) + z_1 (qr - \dot{p}) \right] / g$$

A.1.6.7 Accelerations for g meter (located at x_2, y_2, z_2)

$$a_{z_2} = a_{zcg} + \left[x_2 (pr - \dot{q}) + y_2 (qr - \dot{p}) - z_2 (p^2 + q^2) \right] / g$$

A.1.6.8 Accelerations for three independent accelerometers

$$a_{x_3} = a_{xcg} - \left[x_3 (p^2 + r^2) - y_3 (pq - \dot{r}) - z_3 (pr + \dot{q}) \right] / g$$

$$a_{y_4} = a_{ycg} + \left[x_4 (pq + \dot{r}) - y_4 (p^2 + r^2) + z_4 (qr - \dot{p}) \right] / g$$

$$a_{z_5} = a_{zcg} + \left[x_5 (pr - \dot{q}) + y_5 (qr + \dot{p}) - z_5 (p^2 + q^2) \right] / g$$

A.1.7 Initialisation

Nil

A.1.8 Subroutines used

Nil

A.1.9 Remarks

008 A.1.9.1 See Etkin⁹ (Dynamics of Atmospheric Flight) pp 122-124 for derivation of acceleration at an arbitrary point.

A.1.9.2 'Flat earth' is assumed.

- A.2 Subroutine SACCLIN
- A.2.1 Purpose To compute linear accelerations in earth axes
- A.2.2 Call CALL SACCLIN
- A.2.3 Inputs FTX, FTY, FTZ
RXMASS, G
 $S_{11} - S_{33}$
- A.2.4 Outputs FTN, FTE, FTD
VKNDOT, VKEDOT, VKDDOT

A.2.5 Description

A.2.5.1 Transforms total forces in body axes (FTX, FTY, FTZ) to earth axes (FTN, FTE, FTD), using direction cosines S_{11} etc.

$$F_{TN} = S_{11}F_{TX} + S_{21}F_{TY} + S_{31}F_{TZ}$$

$$F_{TE} = S_{12}F_{TX} + S_{22}F_{TY} + S_{32}F_{TZ}$$

$$F_{TD} = S_{13}F_{TX} + S_{23}F_{TY} + S_{33}F_{TZ}$$

A.2.5.2 Calculates accelerations in earth axes

$$\dot{V}_{KN} = F_{TN}/m$$

$$\dot{V}_{KE} = F_{TE}/m$$

$$\dot{V}_{KD} = F_{TD}/m + g$$

A.2.6 Initialisation

Nil

A.2.7 Subroutines used

Nil

A.2.8 Remarks

User must supply total forces in body axes (FTX, FTY, FTZ).

A.3 Subroutine SACCROT

A.3.1 Purpose Calculates angular accelerations in body axes

A.3.2 Call CALL SACCROT

A.3.3 Inputs XLLTOT, XMMTOT, XNNTOT
P, Q, R
CI1 - CI10

A.3.4 Outputs PDOT, QDOT, RDOT

A.3.5 Description

Given total moments, angular velocity components and inertia coefficients, calculates angular acceleration components in body axes.

$$\dot{p} = CI_1L + CI_2N + CI_3pq + CI_4qr$$

$$\dot{q} = CI_5M + CI_6(r^2 - p^2) + CI_7rp$$

$$\dot{r} = CI_8N + CI_2L + CI_9pq + CI_{10}qr$$

A.3.6 Initialisation

Nil

A.3.7 Subroutines used

Nil

A.3.8 Remarks

A.3.8.1 CI1 etc are calculated in SINIT from inertia information supplied by the user.

A.3.8.2 The user must provide the total moments in body axes (XLLTOT, XMMTOT, XNNTOT).

A.3.8.3 An xz plane of symmetry is assumed.

A.4 Subroutine SALFBET

A.4.1 Purpose Calculates angles of attack and sideslip

A.4.2 Call CALL SALFBET(DT)

A.4.3 Inputs UB, VB, WB, RADTOD

A.4.4 Outputs ALFAR, ALFAD, SALFA, CALFA, ALFADOT,
BETAR, BETAD, SBETA, CBETA, BETADOT

A.4.5 Argument DT is frame time of loop in which SALFBET is used.

A.4.6 Description

A.4.6.1 Given the body axes components of airspeed, calculates α and β from (see Hopkin⁴ section 6.2)

$\alpha = \tan^{-1} WB/UB$, with α taking the sign of WB and being in the range $-\pi$ to $+\pi$.

$\beta = \tan^{-1} VB/(UB^2 + WB^2)^{1/2}$
being in the range $-\pi/2$ to $+\pi/2$, and taking the sign of VB .

A.4.6.2 Calculates the sine and cosine of α and β .

A.4.6.3 Converts α and β to degrees and stores.

A.4.6.4 Estimates the rate of change of the incidence angles ($\dot{\alpha}$ and $\dot{\beta}$) from the present and two preceding values, *eg*

$$\dot{a} = (a_2 - 4a_1 + 3a)/(2DT)$$

where DT is the time step.

A.4.7 Initialisation

During the first entry to the routine the two preceding values of α and β used in estimating $\dot{\alpha}$, $\dot{\beta}$ are set to the current values of α and β , thus making $\dot{\alpha} = \dot{\beta} = 0.0$ for two time steps after 'compute'.

A.4.8 Subroutines used

Library mathematical functions.

A.4.9 Remarks

For $UB = WB = 0.0$, $\alpha = 0.0$.

If VB is zero as well, then $\beta = 0.0$.

A.5 Subroutine SCOUNT

A.5.1 Purpose Resets pass count for derivative section

A.5.2 Call CALL SCOUNT

A.5.3 Inputs JCOMP (from COMMON 'CONTROL')

A.5.4 Outputs NCPASS, JJCOMP, NRUN

A.5.5 Description

A.5.5.1 Resets pass count NCPASS to zero. NCPASS is used in the derivative section to keep track of sub-steps of integration routine.

A.5.5.2 Picks up JCOMP from COMMON 'CONTROL' and reassigns to JJCOMP in COMMON 'SYSTEM' to enable JJCOMP to be used as an 'initialisation complete' flag. JCOMP (and hence JJCOMP) gets set to 1 once 'compute' is pressed.

A.5.5.3 Calls DLRUN to pick up current run number held in mailbox.

A.5.6 Initialisation

Nil

A.5.7 Subroutines used

DLRUN

A.5.8 Remarks

A.5.8.1 Since DLRUN accesses the foreground mailbox, any program using SCOUNT or DLRUN must be run in the foreground.

A.5.8.2 Run number is only obtained if data logging is *not* inhibited.

A.5.8.3 Because SCOUNT is not called during initialisation, the run number is not obtained until after 'compute' is pressed.

A.6 Subroutine SDCOS

A.6.1 Purpose Calculates direction cosines from Euler angles

A.6.2 Call CALL SDCOS

A.6.3 Inputs PSIR, THETAR, PHIR, RADTOD

A.6.4 Outputs PSID, THETAD, PHID,
SPSI, CPSI, STHETA, CTHETA, SPHI, CPHI

A.6.5 Description

A.6.5.1 Calculates sines and cosines of the three Euler angles

ψ - heading $0-360^{\circ}$ (or ± 180)

θ - pitch $\pm 90^{\circ}$

ϕ - bank $\pm 180^{\circ}$

A.6.5.2 Calculates nine direction cosines used in transformation from earth to body axes and vice versa (see Hopkin⁴ section 5.6).

$$\begin{aligned}
 S11 &= \cos \theta \cos \psi & &= l_1 \\
 S12 &= \cos \theta \sin \psi & &= l_2 \\
 S13 &= -\sin \theta & &= l_3 \\
 S21 &= \sin \phi \sin \theta \cos \psi - \cos \phi \sin \psi & &= m_1 \\
 S22 &= \sin \phi \sin \theta \sin \psi + \cos \phi \cos \psi & &= m_2 \\
 S23 &= \sin \phi \cos \theta & &= m_3 \\
 S31 &= \cos \phi \sin \theta \cos \psi + \sin \phi \sin \psi & &= n_1 \\
 S32 &= \cos \phi \sin \theta \sin \psi - \sin \phi \cos \psi & &= n_2 \\
 S33 &= \cos \phi \cos \theta & &= n_3
 \end{aligned}$$

A.6.5.3 Calculates $\sec \theta$ and $\tan \theta$.

A.6.5.4 Converts input angles (ψ , θ , ϕ) from radians to degrees and stores.

A.6.6 Initialisation

Nil

A.6.7 Subroutines used

Library mathematical functions, *eg* sine, cosine

A.6.8 Remarks

Makes no provision yet for $\theta = 90^\circ$, nor for large angles, *ie* multiple turns.

A.7 Subroutine SEULER

A.7.1 Purpose Calculates Euler attitude rates.

A.7.2 Call CALL SEULER

A.7.3 Inputs P, Q, R
SPHI, CPHI, TANTHT, SECTHT
RADTOD

A.7.4 Outputs PHIDT, THETDT, PSIDT
PD, QD, RD

A.7.5 Description

A.7.5.1 Calculates Euler attitude rates from body rates and Euler angles

$$\dot{\phi} = p + (q \sin \phi + r \cos \phi) \tan \theta$$

$$\dot{\theta} = q \cos \phi - r \sin \phi$$

$$\dot{\psi} = (q \sin \phi + r \cos \phi) \sec \theta$$

A.7.5.2 Converts body rates to degrees/s and stores.

A.7.6 Initialisation

Nil

A.7.7 Subroutines used

Library mathematical functions.

A.8 Subroutine SILS

A.8.1 Purpose To calculate glide slope and localiser indications for conventional instrument landing system (ILS).

A.8.2	<u>Call</u>	CALL SILS
A.8.3	<u>Inputs</u>	JJCOMP, LSILS, ILSFLG X, Y, H, RADTOD, DEGTOR
A.8.4	<u>Outputs</u>	EGS, ELOC, HSLOPE, RGS, RLOC, RKINK XGS, XLOC, YLOC, SGS, SLOC, USLOPE, BSLOPE, HKINK, CILS1, CILS2, CILS3, CILS4, XKINK
A.8.5	<u>User options</u>	
	LSILS	ILS on/off flag
	0	off, glide slope and localiser indications set to zero
	1	on
	ILSFLG	select beam type
	1	3° straight beam
	2	6° straight beam
	3	6° changing to 3° at height defined by HKINK

A.8.6 Description

A.8.6.1 If ILS is required (set by LSILS), calculates conventional angular ILS beam, with no beam noise, assuming receiver in aircraft is at centre of gravity.

A.8.6.2 If ILS is not required, glide slope and localiser indications are set to zero and no other calculations are performed.

A.8.6.3 Localiser model

Beam origin is at XLOC, YLOC. (X = 0 is at runway threshold, Y = 0 on runway centre line).

RLOC is range from transmitter.

Angular error ELOC is returned scaled to ± 1.0 , *ie* as a fraction of the defined beam width.

Beam width is \pm SLOC degrees.

A.8.6.4 Glide slope model

Glide path origin is at XGS.

RGS is range from transmitter.

HSLOPE is height of beam centre line at range RGS.

Angular error EGS is returned scaled to ± 1.0 , *ie* as a fraction of the defined beam width.

Beam width is \pm SGS degrees.

USLOPE is upper segment slope (if applicable) in degrees.

BSLOPE is lower segment slope in degrees.

For a single segment beam, USLOPE = BSLOPE.

If a 2-segment slope is used (selected by ILSFLG), the kink occurs at the defined height HKINK.

Range and position from kink (RKINK, XKINK) are derived.

A.8.7 Initialisation

A.8.7.1 During initialisation (when JJCOMP = 0) beam constants are set up according to the choice of beam defined by ILSFLG. Initialisation occurs regardless of the state of the ILS on/off flag.

A.8.8 Subroutines used

BOUND

Library mathematical routines.

A.8.9 Remarks

A.8.9.1 SILS is used by SINIT, if requested, to place the aircraft exactly on the beam as an initial condition.

A.8.9.2 If the user wishes to create his own ILS routine (or similar guidance) he could use the same name and ensure that it will interface correctly to SINIT, *ie* receive a value X and return a value HSLOPE.

A.9 Subroutine

SINIT

A.9.1 Purpose

Various initialisation calculations

A.9.2 Call

CALL SINIT

A.9.3 Inputs

XIX, XIY, XIZ, XIZX
 HIC, XIC, HSLOPE
 DENR, SPSNDR, TEMPR, PRESSR
 SPSL, RHOSL, TEMPSL, PRESSL
 VWKT \emptyset , PSIWD, SHRFAC
 PSIDIC, GAMDIC, VKTIC, BETADIC, ALFADIC
 SWREF, SPAN, W, XCG, ZCG, XCGREF, ZCGREF
 KISA, ISHR

A.9.4 Outputs

CI1 - CI10
 X
 ROOTSIG, SPSOND, RHO, TALPHA, PALPHA
 CPSIW, SPSIW, VWNL0, VWEL0, VWN, VWE, VWD
 VKNIC, VKEIC, VKDIC, VN, VE, VD, VK, VT
 THETADIC, PHIDIC
 SB2, XMASS, RXMASS, DXCG, DZCG
 PDIC, QDIC, RDIC
 RADTOD, DEGTOR, FPSTKT, XK2FPS, G, RG

A.9.5 Data to be supplied by user

SWREF, SPAN, XCGREF, ZCGREF, ZCG, XIX, XIY, XIZ, XIZX

A.9.6 User options

KISA flag to control variation of atmospheric properties
 with height
 0 sea level conditions at all times
 1 standard atmosphere
 -1 fixed values appropriate to initial height (HIC)
 ISHR wind shear selection flag (see SWIND for full
 description)

A.9.7 Description

A.9.7.1 Calculates inertia coefficients, according to equations (20)

$$\begin{aligned}
 CI0 &= 1.0 / (XIZ * XIX - XIZX * XIZX) \\
 CI1 &= XIZ * CI0 \\
 CI2 &= XIZX * CI0 \\
 CI3 &= XIZX * (XIX - XIY + XIZ) * CI0 \\
 CI4 &= (XIZ * (XIY - XIZ) - XIZX * XIZX) * CI0 \\
 CI5 &= 1.0 / XIY \\
 CI6 &= XIZX * CI5 \\
 CI7 &= (XIZ - XIX) * CI5 \\
 CI8 &= XIX * CI0 \\
 CI9 &= (XIX * (XIX - XIY) + XIZX * XIZX) * CI0 \\
 CI10 &= -XIZX * (XIX - XIY + XIZ) * CI0
 \end{aligned}$$

A.9.7.2 If HIC is set negative, calculates initial height to put aircraft exactly on ILS beam.

A.9.7.3 Sets up initial values of atmospheric properties. If KISA = 0, sets up sea level conditions. Otherwise uses SATMOS to derive properties appropriate to HIC.

A.9.7.4 Calculates local true wind components from datum wind speed

08 (V_{WKT0}) and direction (ψ_W)

$$V_{WNL\emptyset} = -V_{WKT\emptyset} \cos \psi_W$$

$$V_{WEL\emptyset} = -V_{WKT\emptyset} \sin \psi_W$$

and allows for wind shear to give initial values for V_{WN} , V_{WE} .

A.9.7.5 If initial condition is not at rest derives velocity relative to ground, and then components for IC values, given wind speed and direction, desired initial airspeed and heading. (Note that VK in this routine is resultant velocity relative to ground, whereas VK obtained in SPATH is truly the ground speed, *ie* in the horizontal plane.)

An iteration technique is used to ensure that the initial track and heading are compatible with the specified wind. The initial heading will thus not reveal to the pilot anything about the applied wind.

A.9.7.6 If initial condition *is* at rest (defined by VKTIC < 1.0) then *ground* speed is set to zero.

A.9.7.7 An initial value for θ is calculated, assuming $\emptyset = 0$, from

$$\theta = \gamma + \alpha .$$

A.9.7.8 Aircraft related constants are calculated from data supplied by the user

```

SB2      = SWREF*SPAN*SPAN
XMASS    = W/G
RXMASS   = 1.0/XMASS
DXCG     = XCG - XCGREF
DZCG     = ZCG - ZCGREF

```

A.9.7.9 Various system constants are given default values via DATA statements, as detailed below.

Default values

```

RADTOD      57.295780
DEGTOR      0.0174533
FPSTKT      0.5921053
XK2FPS      1.688889
G           32.174
RHOSL       0.0023769
SPSL        1116.45
RG          0.03108
TEMPSL      288.15
PRESSL      14.69597
DENR        1.0
SPSNDR      1.0
TEMPR       1.0
PRESSR      1.0
PDIC        0.0

```

QDIC	0.0
RDIC	0.0
PHIDIC	0.0
KISA	0
ISHR	1

A.9.7.10 A software switch is also set on (ISHRIO = 1) to enable the high speed hybrid input/output. It is communicated via labelled COMMON HSHIO.

A.9.8 Initialisation

Whole routine is for initialisation only.

A.9.9 Subroutines used

SATMOS, SILS, WSHEAR and library functions.

A.9.10 Remarks

Will not initialise correctly if initial ϕ is non-zero.

A.10 Subroutine SPATH

A.10.1 Purpose Calculates velocity over ground and flight path angles

A.10.2 Call CALL SPATH

A.10.3 Inputs VKN, VKE, VKD
RADTOD, FPSTKT

A.10.4 Outputs VK, VKKT,
PSIKR, PSIKD,
GAMMAR, GAMMAD

A.10.5 Description

A.10.5.1 Calculates velocity over ground (ground speed)

$$VK = (VKN^2 + VKE^2)^{1/2}$$

A.10.5.2 Converts VK to knots and stores.

A.10.5.3 Calculates climb angle

$$\gamma = \tan^{-1}(-VKD/VK)$$

in the range $-\pi/2$ to $+\pi/2$.

A.10.5.4 Calculates track

$$\chi (= \psi_k) = \tan^{-1}(V_{KE}/V_{KN})$$

in the range 0 to 2π .

A.10.5.5 Converts γ and χ to degrees and stores.

A.10.6 Initialisation

None

A.10.7 Subroutines used

Library mathematical functions.

A.10.8 Remarks

A.10.8.1 If $V_{KD} = V_K = 0.0$, $\gamma = 0.0$.

A.10.8.2 If $V_{KE} = V_{KN} = 0.0$, $\chi = 0.0$.

A.10.8.3 For $V_{KE} = 0.0$, $\chi = 0$ for V_{KN} positive but $\chi = 180^\circ$ for V_{KN} negative.

A.11 Subroutine STV

A.11.1 Purpose Computes TV positions and rates, and controls belt logic.

A.11.2 Call CALL STV

A.11.3 Inputs VKN, VKE, VKD, VSHIPKT, XK2FPS
X, Y, H, XIC
XP, ZP, CTHETA, STHETA, CPSI, SPSI, PSIDT, THETDT
JJCOMP, NTVB
LFWD, LBACK, LYTVIC, LXTVIC, LCYCLE

A.11.4 Outputs XTV, YTV, HTV, XIC, XIHX, XIHY
XDOTM, XDTV, YDTV, HDTV
SXPL, SXMIN, SXPLUS, SXMINUS, SYPL, SYMIN, HTVLIM,
XDTMX
IDSYNC

A.11.5 Data to be supplied by user

NTVB TV belt flag
1 700:1 model
2 2000:1 model
3 5000:1 model
VSHIPKT ship velocity, knots.

A.11.6 Description

A.11.6.1 Initialisation.

A.11.6.2 Belt slew control.

If forward slew is selected, X rate is forced to maximum positive value.

If backward slew is selected, X rate is forced to maximum negative value.

In both cases, the aircraft's position keeps in step. Positional calculations can also be referred to a ship moving at constant velocity VSHIPKT.

A.11.6.3 Integration control for X and Y (belt logic).

- (a) If Y reset is selected, Y position resets to YIC.
- (b) If X reset is selected, X position resets to XIC as originally defined in ICFILE.
- (c) If X reset is not selected, additional logic is invoked to control the belt (x):
 - * if X is not near the belt join (defined by SXMIN, SXPL - see belt diagram), the program continues to the position module.
 - * If X is near the join but 'LCYCLE' is not set, the program continues to the position module.
 - * If 'LCYCLE' is not set, the program continues to the position module.
 - * If 'LCYCLE' is set, X is forced to cycle between SXMINUS and SXPLUS. IDSYNC is set to 1 to uncouple the belt position feedback.
 - * If 'LCYCLE' is set, but the demanded X position is less than the negative cycle limit SXMINUS (as can happen if X had been previously reset), the X integrator is reset and XIC is set to SXMINUS. This will force the belt to start to move.
 - * If X is between SXMINUS and SXPLUS, the program continues to the position module.
 - * When X reaches SXPLUS, it resets to SXMINUS, before going on to the position module.

A.11.6.4 Position module - TV positions and rates in three axes (equations (22) to (25)).

- (a) Calculates pilot position, and rate of change of his position, allowing for his location away from the aircraft's centre of gravity.
- (b) If TV belt is trying to position before minimum X possible on the belt (SXMIN), or if X reset is demanded, then \dot{X}_{TV} is set to zero to stop hunting. This is not done if LCYCLE is set.
- (c) If H is above the ceiling for the model, \dot{h}_{TV} is set to zero to stop bouncing.

- (d) Limits are finally applied to x_{TV} , y_{TV} and h_{TV} to keep within model confines. These limits do not affect computed aircraft position and navigation.

A.11.7 Initialisation

A.11.7.1 During initialisation, the set of TV constants appropriate to the particular belt are selected from the array TVCON (8,3). These constants define the limit of movement as follows:

SXPL	TVCON (1, NTVB)	Maximum value of x_{TV} allowed, also determines when 'near belt join'.
SXMIN	TVCON (2, NTVB)	Minimum value of x_{TV} allowed, also determines when 'near belt join'.
SXPLUS	TVCON (3, NTVB)	} x cycles between these two values if 'cycle' mode is selected
SXMINUS	TVCON (4, NTVB)	
SYPL	TVCON (5, NTVB)	Maximum value of y_{TV} allowed
SYMIN	TVCON (6, NTVB)	Minimum value of y_{TV} allowed
HTVLIM	TVCON (7, NTVB)	Ceiling for TV height
XDTMX	TVCON (8, NTVB)	Belt velocity when slewing.

The x-related quantities are illustrated in Fig A4.

STV holds three values of each parameter in TVCON, the appropriate one being selected according to the TV belt in use. Because of this, on-line permanent changes to SXPL etc can only be achieved by changing the associated element of TVCON.

A.11.7.2 The initial value of X obtained from the IC file is stored in a temporary location (XICF) so that a demand to reset X will reset X to this value regardless of whether cycle has previously been selected.

A.11.8 Subroutines used

BOUND

A.11.9 Remarks

A.11.9.1 The array of TV constants is accessible to PV100 and so can be overwritten if new values are found to be more appropriate to the hardware. Alterations can also be made via the semi-permanent changes file (see SYSCOM).

A.11.9.2 The logical controls are set via special buttons etc on the control desk and so are hardware dependent.

LCYCLE	desk switch 5
LXTVIC	desk switch 6
LYTVIC	desk switch 7
LFWD	slew toggle patched to AD4 sense line DGS03 (line 4)
LBACK	slew toggle patched to AD4 sense line DGS04 (line 5)
IDSYNC	software flag controls AD4 control line DGC17 (line 16)

A.11.9.3 To start the aircraft at some position outside the limits of the TV model, set up XIC, YIC to suit. When the aircraft position comes within the confines of the belt, it will begin to move with the aircraft. X and Y positions can be reset using their appropriate buttons without having to reset the whole computation.

A.11.9.4 If, after a reset to some distant location, immediate movement of the belt is required, put 'X reset' off and 'cycle' on.

A.11.9.5 No provision has been made for large bank angles (>1 rev), nor for cloud or visibility control.

A.11.9.6 Successful use of this routine to drive the TV model is dependent on analogue computer circuitry incorporating position feedbacks.

A.11.9.7 Do not initialise with 'CYCLE' on if, subsequently in the run, you may want to reset X outside the confines of the belt. This is because initialisation occurs twice and so XIC is overwritten.

A.12	<u>Subroutine</u>	SVELOC1
A.12.1	<u>Purpose</u>	Calculates body axes velocity components
A.12.2	<u>Call</u>	CALL SVELOC1
A.12.3	<u>Inputs</u>	VKN, VKE, VKD VWN, VWE, VWD $S_{11} - S_{33}$
A.12.4	<u>Outputs</u>	UB, VB, WB VN, VE, VD
A.12.5	<u>Description</u>	

A.12.5.1 Given the components of velocity relative to ground (VKN, VKE, VKD) and the components of total wind speed, including turbulence (VWN, VWE, VWD), calculates components of velocity relative to the air in earth axes (VN, VE, VD), then resolves to body axes.

A.12.6 Initialisation

None

A.12.7 Subroutines used

None

A.12.8 Remarks

A.12.8.1 Assumes wind velocity component is positive in the *same* direction as the component relative to the air. Thus, for a head wind and for the aircraft on a northerly heading ($\psi = 0$), VWN is negative.

A.12.8.2 VN, VE, VD are initially calculated in SINIT.

A.13 Subroutine SVELOC2

A.13.1 Purpose Calculates total airspeed, equivalent airspeed, Mach number etc using appropriate atmospheric properties.

A.13.2 Call CALL SVELOC2

A.13.3 Inputs UB, VB, WB
H
SWREF, CREF, SPAN, SB2
KISA
FPSTKT, RHOSL, SPSL, TEMPSL, PRESSL

A.13.4 Outputs VT, VTKT, VEAS, VEASKT, XMACH
QDYN, HLFROV, QDYN, QSCREF, QSSPAN, QSB2IV
ROOTSIG, RHO, SPSOND, DENR, SPSNDR, TEMPR, PRESSR
TRATIO, ARATIO, DRATIO, PRATIO, TALPHA, PALPHA

A.13.5 Data to be supplied by user

Note that certain geometric parameters for the aircraft must be supplied by the user.

SWREF reference wing area
CREF reference chord
SPAN reference wing span
SB2 is a combination (SWREF*SPAN*SPAN) calculated in SINIT.

A.13.6 User options

The flag KISA selects the way in which atmospheric properties vary. It must only be changed in INITIAL, before SINIT is executed.

KISA = 1 standard atmosphere
 = 0 fixed values appropriate to sea level
 = -1 fixed values appropriate to initial height HIC

A.13.7 Description

A.13.7.1 Calculates total airspeed, converts to knots and stores.

$$V_T = \left(u_B^2 + v_B^2 + w_B^2 \right)^{\frac{1}{2}}$$

A.13.7.2 If the flag KISA is set to 1, obtains, for the current height, new properties (density ratio, speed of sound ratio, temperature ratio and pressure ratio) of a standard atmosphere, using the routine SATMOS.

If KISA is not set to 1, atmospheric properties are kept constant, as set up by SINIT.

A.13.7.3 Calculates properties of the atmosphere

air density	$\rho = \rho_{SL} \sigma$
speed of sound	$a = a_{SL} a_r$
ambient temperature	$T_\alpha = T_{SL} T_r$
ambient pressure	$P_\alpha = P_{SL} P_r$

A.13.7.4 Calculates equivalent airspeed, converts to knots and stores.

$$V_{EAS} = V_T \sigma^{\frac{1}{2}}$$

A.13.7.5 Calculates dynamic pressure and related terms

QDYN	$= \frac{1}{2} \rho V_T^2$
QDYNS	$= \frac{1}{2} \rho V_T^2 S_W$
QSCREF	$= \frac{1}{2} \rho V_T^2 S_{Wref}^c$
QSSPAN	$= \frac{1}{2} \rho V_T^2 S_{Wb}$
QSB21V	$= \frac{1}{2} \rho V_T (S_{Wb}^2)$

A.13.7.6 Calculates Mach number

$$M = V_T / a$$

A.13.7.7 Calculates compressible adiabatic flow relationships for Mach number < 1.0. For initialisation purposes, these ratios are given datum values of 1.0.

T _{ratio}	$= (1 + 0.2M^2)^{-1}$
a _{ratio}	$= (T_{ratio})^{\frac{1}{2}}$
ρ _{ratio}	$= (a_{ratio})^5$
P _{ratio}	$= a_{ratio} T_{ratio}$

A.13.8 Initialisation

In addition to those items mentioned above, datum values of atmospheric properties are provided in SINIT (qv).

A.13.9 Subroutines used

SATMOS

A.13.10 Remarks

Subroutine ATMOS, an alternative to SATMOS, is available to calculate atmospheric properties for hot days. It is not included as an option, however, as it is very much larger than SATMOS, the subroutine for 'standard' days.

A.14 Subroutine

SWIND

A.14.1 Purpose

Controls turbulence, wind and wind shear

A.14.2 Call

CALL SWIND

A.14.3 Inputs

H, HIC, VKTIC,
XK2FPS, FRAMET1, SFRACG, SRDECAY
VWNLØ, VWELØ, VWDLØ, CPSIW, SPSIW
USIG, VSIG, WSIG
ISHR, JJCOMP, NG, LTURB, LSEED

A.14.4 Outputs

UTURB, VTURB, WTURB
VWN, VWE, VWD
VWNL, VWEL, VWDL
SHRFAC

A.14.5 User options

LTURB

Turbulence switch

0

no turbulence calculated or output

1

turbulence calculated and output

ISHR

wind shear selection

1 (default)

no shear applied. Returns immediately with
SHRFAC = 1.0. Time overhead is minimal.

2

ARB mean shear profile (logarithmic)

3

linear shear up to 333 ft, thereafter constant

LSEED

random number seed selector

0 (default)

seeds in GUSTS routine obtained from time of day

1

constant seeds enable a repeatable turbulence sequence
to be obtained

USIG, VSIG, WSIG

rms settings for each component (never exactly achieved -
it is a random process!). Can be changed in flight.

VWKTØ

datum wind speed, true (knots)

PSIWD datum wind direction (degrees). PSIWD = 0.0 is a wind from the north. VWKTØ and PSIWD are set as initial conditions and are used by SINIT (qv) to calculate VWNLØ, CPSIW etc.

For the remaining parameters (except for VWDL) changes are only effective if applied during initialisation.

VWDL wind component in 'down' sense (default = 0.0)

SRDECAY decay parameter, should not be changed (default = 0.7)

SFRACG intermittency parameter, in range 0.0 to 0.99 (default = 0.0). Should never be set equal to 1.0. For minimum intermittency, set SFRACG = 0.0. A value of 0.7 is probably as extreme as will ever be needed. Refer to Ref 12 for discussion.

NG Controls the three gust ramp lengths used in the turbulence generation routine GUSTS¹², via

$$NGUSTS = NG * \frac{\text{Initial speed (ft/s)}}{200}$$

NGUSTS, an important parameter, required by the GUSTS routine, defines the number of gusts per second. Thus, if the initialisation speed is 200 ft/s (118 kn), NGUSTS = NG = 4 (the default value for NG) and so the shortest gust gradient distance is 200/4 = 50 ft and the longest, determined in the GUSTS subroutine, is 16 times the shortest, or 800 ft. Initialisation at speeds much below 100 kn may require NG to be increased. If the initial speed is zero, NGUSTS takes a minimum value of 1. A further limitation is that NGUSTS must be less than the repetition rate of the simulation, *eg* for a frame time of 50 ms (20 solutions/s) and NG = 4, the *maximum* initial speed must not exceed 1000 ft/s (592 kn). This constraint is checked and imposed in SWIND.

A.14.6 Description

- (a) Derives shear factor (SHRFAC) according to height, using WSHEAR subroutine.
- (b) Calculates local wind velocity components VWNL, VWEL at height, including shear effects.
- $$VWNL = VWNLØ * SHRFAC$$
- $$VWEL = VWELØ * SHRFAC$$
- VWNLØ, VWELØ are calculated in SINIT.
- (c) If turbulence is required (set by LTURB), calculates three raw components of turbulence (using GUSTS subroutine). The gust velocities obtained are scaled by nominal rms values for each component (USIG, VSIG, WSIG), set by the user, to give turbulence components UTURB, VTURB, WTURB.

- (d) If turbulence is not required, turbulence components are set to zero.
- (e) The calculated turbulence components are added to the mean wind components to provide three components of total wind (VWN, VWE, VWD) in earth axes.
- $$\begin{aligned} \text{VWN} &= \text{VWNL} - (\text{UTURB} * \text{CPSIW} - \text{VTURB} * \text{SPSIW}) \\ \text{VWE} &= \text{VWEL} - (\text{VTURB} * \text{CPSIW} + \text{UTURB} * \text{SPSIW}) \\ \text{VWD} &= \text{VWDL} - \text{WTURB} \end{aligned}$$
- (f) A flow chart is shown in Fig A9.

A.14.7 Initialisation

During initialisation, the gust generation routine GUSTS is called regardless of whether the turbulence switch LTURB is set on or off. This is necessary to perform the required preliminary calculations. However, the turbulence components returned are set to zero. GUSTS uses its own flag (IFLAG) to control initialisation, but this is tied to the system flag JJCOMP in SWIND.

A.14.8 Subroutines used

WSHEAR, GUSTS, FDC, RANDU, VSTEP, SEEDVAL
Library mathematical functions.

A.14.9 Remarks

A.14.9.1 The calculated turbulence components are added to the mean wind components, which only later become resolved into body axes. UTURB is *along* the datum wind, a positive gust increasing the wind (crudely, increasing the airspeed); VTURB is *across* the wind (a positive gust, crudely, increasing the sideslip); WTURB is *vertical*, positive up (to increase incidence).

A.14.9.2 Wind shear and attenuation of vertical turbulence with height work from altitude rather than height above local terrain.

A.14.9.3 Details of the gust generation process are contained in Ref 12.

A.14.9.4 Wind shear is only in magnitude, not in direction.

A.14.9.5 The turbulence control, LTURB, is set by a desk switch (currently number 8).

A.15 Subroutine SYSCOM

A.15.1 Purpose Sets up communication with system variables.

A.15.2 Call CALL SYSCOM

A.15.3 Inputs As set up in 'changes' file.

A.15.4 Outputs Nil

A.15.5 Description

A.15.5.1 Includes in the labelled common area SYSTEM *all* the names of system variables so that they are set up in the Namelist table.

A.15.5.2 Calls PV200 in the defined way to set up the Namelist table address. The defined way is

```

DIMENSION NAME (2)
DATA NAME/'SYSCOM'/
NAMELIST
CALL PV200(NAME)
GO TO 3
2 INPUT 101
3 CONTINUE

```

A.15.5.3 Provides for 'semi-permanent' changes to be read from a file, using the self-identified input facility

```

DATA ISYS/50/
REWIND ISYS
INPUT (ISYS)
REWIND ISYS

```

A.15.6 Initialisation

This routine is only called in the INITIAL region, so it is all initialisation.

A.15.7 Subroutines used

PV200 plus library routines. Note that to test SYSCOM in the background, a dummy PV200 should be supplied.

A.15.8 Remarks

A.15.8.1 Unit 50 used for inputting semi-permanent changes should be assigned at model load time to a file in the user's area, *eg*

```
:ASSIGN (F:50, D3, SYSCHNG)
```

A.15.8.2 Prior to running the aircraft model program, the 'changes' file should be filled with the desired changes in the form

```

X1      = 23.0
SWREF   = 560.0
*
```


The concluding asterisk (*) is essential. If no changes are required the file must contain an asterisk otherwise a run-time error occurs.

A.15.8.3 The positioning of SYSCOM means that IC values cannot be overwritten since they are read after SYSCOM is executed. However, changes introduced through SYSCOM can be altered on-line since retained changes are applied (by PV300) after SYSCOM.

- A.16 Subroutine DSCRT1/DSCRT2
- A.16.1 Purpose To control execution of routines for discrete input/output.
- A.16.2 Call CALL DSCRT1 (CALL DSCRT2)
- A.16.3 Inputs IAD4SL, IAD4CL, IDSCFL, IPCOFL
- A.16.4 Outputs By calling other routines, the arrays ISLR(16), ICLR(16), IP(32), IDS(32), ICO(32) are filled.
- A.16.5 Data to be supplied by user

Four flags must be set to control which of the basic routines, if any, is executed in which real time loop.

IAD4SL	Execution control flag for AD4 sense lines (READSLR)
IAD4CL	Execution control flag for AD4 control lines (SETCLR)
IDSCFL	Execution control flag for discrettes in to the Sigma (READSCR)
IPCOFL	Execution control flag for discrettes out from Sigma (SETDSCR)
	Each flag can take the values:
0	Do not execute
1	Execute in DSCRT1, <i>ie</i> in the fastest loop
2	Execute in DSCRT2, <i>ie</i> in the second loop.

Default values (set in DSCRT1) and typical values are

Flag	Routine	Default	Typical (possible)
IAD4SL	READSLR	1	1 (2)
IAD4CL	SETCLR	1	1 (2)
IDSCFL	READSCR	1	2
IPCOFL	SETDSCR	0	2 (1)

A.16.6 Description

Calls appropriate routines, according to flag settings. Routines which are called by DSCRT1 are not then called by DSCRT2, and *vice versa*.

A.16.7 Initialisation

Nil

A.16.8 Subroutines used

READSLR, SETCLR, READSCR, SETDSCR

A.16.9 Remarks

Execution timings are

SETCLR	0.16 ms
READSLR	0.22 ms
SETDSCR	0.34 ms
READSCR	0.87 ms
Total	<u>1.59 ms</u>

Hence a millisecond or more could be saved in the main loop by executing READSCR and SETDSCR in the second loop.

A.17 Function subroutine ISDSCR

A.17.1 Purpose To read a single specified Sigma 8 sense line

A.17.2 Call I = ISDSCR (ISET, LINE)
ISDSCR is returned with a value 0 or 1, depending on whether the specified line LINE is off or on.

A.17.3 Description

This function tests the status of an individual sense line, either from the logic patch panel in rack N (ISET = 0) or from the control desk switches (ISET = 1).

A.17.4 Initialisation

Nil

A.17.5 Subroutines used

READSCR

A.17.6 Remarks

This function is intended for use during the INITIAL region only, when time is not critical. It is not a fast routine.

Appendix B LISTING OF SESAME ROUTINES

```

1. SUBROUTINE SACCHD
2. C
3. C
4. C
5. C
6. C
7. C
8. C
9. C
10. C
11. C
12. C
13. C
14. C
15. C
16. C
17. C
18. C
19. C
20. C
21. C
22. C
23. C
24. C
25. C
26. C
27. C
28. C
29. C
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56. C
57. C
58. C
59. C
60. C
61. C
62. C
63. C
64. C
65. C
66. C
67. C
68. C
69. C
70. C
71. C
72. C
73. C
74. C
75. C

```

.....

WRITTEN BY : A.J. SPENCER

DATE : 24-02-78

DESCRIPTION : SACCHD CALCULATES ACCELERATIONS OF THE AIRCRAFT C.G. AND OF THE PILOT IN THE HOOT AREAS FOR USE BY MOTION & AUTOSTAR ETC..

.....

```

COMMON/SYSTEM/A(1000),L(400)
VERSION IDENTIFIER
DATA NSACCHD/240278/
12-R-76 SYSTEM COMMON ENLARGED
24-2-78 XP,ZP REPLACED BY XPC,ZPCG
EQUIVALENCE (NSACCHD,L(255))
*** VARIABLE OUTPUTS ***
EQUIVALENCE (XCG, #A(201)), (YCG, #A(202)), (ZCG, #A(203)),
1 (AZCG1, #A(204)), (XACG, #A(205)), (YACG, #A(206)),
2 (AZCG, #A(207)), (XAP, #A(208)), (YAP, #A(209)),
3 (AZP, #A(250)), (AZAP, #A(251)), (AY, #A(252)),
4 (AZ, #A(253)), (AX, #A(254)), (AY, #A(255)),
5 (AZ5, #A(256))
*** VARIABLE INPUTS ***
EQUIVALENCE (X1, #A(257)), (Y1, #A(258)), (Z1, #A(259)),
1 (X2, #A(260)), (Y2, #A(261)), (Z2, #A(262)),
2 (X3, #A(263)), (Y3, #A(264)), (Z3, #A(265)),
3 (X4, #A(266)), (Y4, #A(267)), (Z4, #A(268))
4 (X5, #A(269)), (Y5, #A(270)), (Z5, #A(271)),
5 (S13, #A(19)), (S23, #A(22)), (S33, #A(25)),
6 (P, #A(26)), (Q, #A(27)), (N, #A(28)),
7 (PDNT, #A(65)), (QDNT, #A(66)), (INDNT, #A(67)),
8 (XPCG, #A(280)), (ZPCG, #A(281)), (FTX, #A(136)), (FTY, #A(137)), (FTZ, #A(138))
9
**** CONSTANTS ****
EQUIVALENCE ( #A(106))
EVALUATING COMMON SUB-EXPRESSIONS
Q2 = P*P
Q2 = Q*Q
R2 = R*R
PQ = P*Q
PR = P*R
QR = Q*R
C THESE INCLUDE DIVISION BY 10'
Q2R2 = (Q2 + R2)*RG
PQD2B = (P*Q + R2)*RG
PRD2T = (P*R + Q2)*RG
PQD2T = (P*Q + R2)*RG
P2R2 = (P2 + R2)*RG
QNRD2B = (Q*R + P2)*RG
PRD2B = (P*R + Q2)*RG
QRD2T = (Q*R + P2)*RG
QNRD2T = (Q*R + P2)*RG
R4 = 1.0/R
C CALCULATING ACCELERATIONS IN 'G' UNITS
C SPECIFIC ACCNS AT AIRCRAFT C.G.
XCG = FTX*R4

```



```

76.      AYCG = FTY*HN
77.      AZCG = FTZ*HN
78.      C
79.      C ABSOLUTE ACCNS AT AIRCRAFT C.G.
80.      C
81.      AXACG = AXCG+S13
82.      AYACG = AYCG+S23
83.      AZACG = AZCG+S33
84.      C
85.      C SPECIFIC ACCNS AT PILOT
86.      C
87.      AX1 = AXCG+XPC3*Q2H2 + ZPCU*PRD1T      2*0278
88.      AYP = AYCG+XPC3*Q2H2 + ZPCU*QRPTB      2*0278
89.      AZP = AZCG+XPC3*PRD1T + ZPCG*P2Q2      2*0278
90.      C
91.      C ABSOLUTE (OR MANUEUVRE G1) ACCNS AT PILOT
92.      C
93.      AZAP = AZP+S33
94.      C
95.      C ACCNS FOR RECORDERS RELATIVE TO 1.0 0
96.      C
97.      AZCG1 = AZCG+1.0
98.      C
99.      C ACCNS FOR SLIP BALL (LOCATED AT X1,Y1,Z1)
100.     C
101.     AY1 = AYCG+X1*PRD1T+Y1*P2R2+Z1*QRPTB
102.     C
103.     C ACCNS FOR 101 METER (AT X2,Y2,Z2)
104.     C
105.     AZ2 = AZCG+X2*PRD1T+Y2*QRPTB+Z2*P2Q2
106.     C
107.     C ACCNS FOR THREE INDEPENDANT ACCELEROMETERS (FOR USE BY AUTOSTAB)
108.     C      X=ACCELEROMETER AT X3,Y3,Z3
109.     C      Y=ACCELEROMETER AT X4,Y4,Z4
110.     C      Z=ACCELEROMETER AT X5,Y5,Z5
111.     C
112.     AX3 = AXCG+X3*Q2R2+Y3*PRD1T+Z3*PRD1T
113.     AY4 = AYCG+X4*Q2H2+Y4*P2R2+Z4*QRPTB

114.     AZ5 = AZCG+X5*PRD1T+Y5*QRPTB+Z5*P2Q2
115.     RETURN
116.     END
1ASSIGN (MIS1,03,SACLS)
1FORTRAN LS,NS
EXT. FORTRAN IV, VERSION E00

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```

1.      SUBROUTINE SACCLIN
2.      C
3.      C
4.      C
5.      C      WRITTEN BY: D.OLDFIELD
6.      C      DATE:12-8-74
7.      C      DESCRIPTION: THIS SUBROUTINE CALCULATES THE TOTAL
8.      C      FORCE COMPONENTS TO THE EARTH AXES GIVEN THE
9.      C      COMPONENTS TO THE BODY AXES AND THE DIRECTION
10.     C      COSINES. THE ACCELERATION IS ALSO CALCULATED
11.     C      FROM THIS INFORMATION AND THE AIRCRAFT MASS
12.     C
13.     C
14.     C
15.     C      12-8-74      SYSTEM COMMON ENLARGED
16.     C      COMMON/SYSTEM/A(1000),L(400)
17.     C
18.     C      VERSION IDENTIFIER
19.     C
20.     C      DATA KSACCLIN/120874/
21.     C      EQUIVALENCE(KSACCLIN,L(256))
22.     C
23.     C      *** VARIABLE INPUTS ***
24.     C
25.     C      EQUIVALENCE(S11      ,A( 17)),(S12      ,A( 18)),(S13      ,A( 19)),
26.     C      1      (S21      ,A( 20)),(S22      ,A( 21)),(S23      ,A( 22)),
27.     C      2      (S31      ,A( 23)),(S32      ,A( 24)),(S33      ,A( 25)),
28.     C      3      (FTX      ,A(134)),(FTY      ,A(135)),(FTZ      ,A(136)),
29.     C      4      (RXMASS   ,A( 1))
30.     C
31.     C      *** VARIABLE OUTPUTS ***
32.     C
33.     C      EQUIVALENCE(FTN      ,A(137)),(FTE      ,A(138)),(FTD      ,A(139)),
34.     C      1      (VKDDOT   ,A(123)),(VKEDOT   ,A(1239)),(VKDDOT   ,A(1240))
35.     C
36.     C      *** CONSTANTS ***
37.     C
38.     C      EQUIVALENCE(G      ,A(145))
39.     C
40.     C      CALCULATE TOTAL FORCES TO EARTH AXES
41.     C      FTN = S11*FTX+S21*FTY+S31*FTZ
42.     C      FTE = S12*FTX+S22*FTY+S32*FTZ
43.     C      FTD = S13*FTX+S23*FTY+S33*FTZ
44.     C      CALCULATE ACCELERATION
45.     C      VKDDOT= FTN/RXMASS
46.     C      VKEDOT= FTE/RXMASS
47.     C      VKDDOT= FTD/RXMASS+G
48.     C      RETURN
49.     C      END
50.     C      IASBIGN (MISI,03,SACRS)
51.     C      IFORTNAN LB,NS
52.     C      EXT. FORTRAN IV, VERSION E00

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1.      SUBROUTINE SACCROT
2.      C
3.      C
4.      C
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34.     C
35.     C
36.     C
37.

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      WRITTEN BY : D.OLDFIELD
      DATE : 12-8-76
      DESCRIPTION : THIS SUBROUTINE CALCULATES
      THE ANGULAR ACCELERATIONS IN THE BODY
      AXES GIVEN THE TOTAL MOMENTS, ANGULAR
      VELOCITY COMPONENTS IN THE BODY AXES AND
      THE INERTIA COEFFICIENTS.

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12-8-76      SYSTEM COMMON ENLARGED
COMMON/SYSTEM/A(1000),L(400)
VERSION IDENTIFIER
DATA KSACCROT/120876/
EQUIVALENCE(KSACCROT,L(257))

```

*** VARIABLE INPUTS ***

```

EQUIVALENCE(XLLTOT ,A(131)),(XMMTOT ,A(132)),(XNNTOT ,A(133)),
1      (P ,A(26)),(Q ,A(27)),(R ,A(28)),
2      (CI1 ,A(35)),(CI2 ,A(36)),(CI3 ,A(37)),
3      (CI4 ,A(38)),(CI5 ,A(39)),(CI6 ,A(40)),
4      (CI7 ,A(41)),(CI8 ,A(42)),(CI9 ,A(43)),
5      (CI10 ,A(44))

```

*** VARIABLE OUTPUTS ***

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EQUIVALENCE(PDOT ,A(45)),(QDOT ,A(46)),(RDOT ,A(47))

```

CALCULATE ANGULAR ACCELERATIONS

```

PDOT = CI1*XLLTOT+CI2*XNNTOT+(CI3*P+CI4*R)*Q

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38.     QDOT = CI5*XMMTOT+CI6*(R*R-P*P)+CI7*R*P
39.     RDOT = CI8*XNNTOT+CI2*XLLTOT+(CI9*P+CI10*R)*Q
40.     C
41.     RETURN
42.     END

```

```

1ASSIGN (M:SI,03/SALFS)
IFORTRAN LB,NU
EXT. FORTRAN IV, VERSION E00

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```

1*      SUBROUTINE SCOUNT
2*      C
3*      C
4*      C
5*      C      *.....*
6*      C      * DESCRIPTION : THIS ROUTINE SETS PASS COUNT FOR *
7*      C      * DERIVATIVE SECTION. *
8*      C      * WRITTEN BY : B.N.TOMLINSON *
9*      C      * DATE :12-8-76 *
10*     C      * MODIFIED: 31-5-77 TO INCLUDE DLRUN *
11*     C      *.....*
12*     C
13*     C
14*     C      VERSION IDENTIFIER
15*     C
16*     C      DATA KSCOUNT/310577/
17*     C      EQUIVALENCE(KSCOUNT ,L(259))
18*     C      12-8-76      SYSTEM COMMON ENLARGED
19*     C      COMMON/SYSTEM/A(1000),L(400)
20*     C      PICK UP JCOMP (SET IN SWAIT)
21*     C      COMMON/CONTROL/JCOMP
22*     C      JCOMP = 1 AFTER COMPUTE PRESSED
23*     C
24*     C      *** VARIABLE INPUTS ***
25*     C
26*     C
27*     C      *** VARIABLE OUTPUTS ***
28*     C
29*     C      EQUIVALENCE (NRUN ,L(169))
30*     C      EQUIVALENCE(NCPASS ,L( 2)),(JJCOMP ,L( 8))
31*     C      NCPASS IS COUNT OF NUMBER OF PASSES THROUGH DERIVATIVE SECTION
32*     C      EXECUTED SO FAR IN ONE INTEGRATION STEP. SET TO ZERO IN THIS
33*     C      ROUTINE PRIOR TO DOING INTEGRATION.
34*     C      NCPASS = 0
35*     C      SET JJCOMP, IN SYSTEM COMMON, TO ENABLE STATUS TO BE
36*     C      USED, E.G. IN SILS,STV
37*     C      JJCOMP = JCOMP
38*     C      PICK UP RUN NUMBER FROM MAILBOX
39*     C      CALL DLRUN (NRUN)
40*     C      RETURN
41*     C      END
IASSIGN (MISI,03,SUCCESS)

IFORTNAN LG,NG
EXT. FORTRAN IV, VERSION E00

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1.      C
2.      C
3.      C
4.      C
5.      C
6.      C
7.      C
8.      C
9.      C
10.     C
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27.     C
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30.     C
31.     C
32.     C
33.     C
34.     C
35.     C
36.     C
37.     C

SUBROUTINE SUCMS
.....
*
* WRITTEN BY : D.ULUFIELD
* DATE : 12-8-76
* DESCRIPTION : THIS SUBROUTINE CALCULATES
* THE DIRECTION COSINES, SINES AND DEGREE
* VALUE OF THREE INPUT ANGLES IN RADIAN.
* SEC THETA AND TAN THETA ARE ALSO
* CALCULATED.
*
*.....
12-8-76 SYSTEM COMMON ENLARGED
COMMON/SYSTEM/A(1000)/L(400)

VERSION IDENTIFIER

DATA KSDCOS /120876/
EQUIVALENCE(KSDCOS ,L12601)

*** VARIABLE INPUTS ***
EQUIVALENCE(PSIR ,A( 3)),(THETA ,A( 5)),(PHIK ,A( 7))

*** VARIABLE OUTPUTS ***
EQUIVALENCE(PSID ,A( 9)),(THETA ,A( 6)),(PHID ,A( 8)),
1      (SPSI ,A( 9)),(CPSI ,A(10)),(STHETA ,A(11)),
2      (CTHETA ,A(12)),(SPHI ,A(13)),(CPHI ,A(14)),
3      (SECTHT ,A(15)),(TANTHT ,A(16)),(S11 ,A(17)),
4      (S12 ,A(18)),(S13 ,A(19)),(S21 ,A(20)),
5      (S22 ,A(21)),(S23 ,A(22)),(S31 ,A(23)),
6      (S32 ,A(24)),(S33 ,A(25))

*** CONSTANTS ***

EQUIVALENCE(RADTOD ,A(1+1))

CALCULATE SINE, COSINE AND TANGENTS
STHETA = SIN(THETA)
CTHETA = COS(THETA)
SPSI = SIN(PSIR)
CPSI = COS(PSIR)
SPHI = SIN(PHI)
CPHI = COS(PHI)

CALCULATE DIRECTION COSINES
S11 = CTHETA*CPSI
S12 = CTHETA*SPSI
S13 = -STHETA
S21 = SPHI*STHETA+CPSI*CPHI*SPSI
S22 = SPHI*STHETA*SPSI+CPHI*CPSI
S23 = SPHI*CTHETA
S31 = CPHI*STHETA+CPSI*SPHI*SPSI
S32 = CPHI*STHETA*SPSI+SPHI*CPSI
S33 = CPHI*CTHETA

CALCULATE SEC THETA AND TAN THETA
SECTHT = 1.0/CTHETA
TANTHT = STHETA/SECTHT

CALCULATE ANGLES IN DEGREES
PSID = PSIR*RADTOD
THETA = THETA*RADTOD
PHID = PHIR*RADTOD
RETURN
END
PASSIGN (M161,03,SEULS)
IFORTNAN LS,NB
EXT: FORTNAN IV, VERSION E00

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1.      SUBROUTINE SEULER
2.      C
3.      C
4.      C
5.      C
6.      C
7.      C
8.      C
9.      C
10.     C
11.     C
12.     C
13.     C      12-8-76      SYSTEM COMMON ENLARGED
14.     C      COMMON/SYSTEM/A(1000),L(400)
15.     C
16.     C      VERSION IDENTIFIER
17.     C
18.     C      DATA KSEULER /120876/
19.     C      EQUIVALENCE(KSEULER ,L(261))
20.     C
21.     C      *** VARIABLE INPUTS ***
22.     C
23.     C      EQUIVALENCE(SPHI ,A( 13)),(CPHI ,A( 14)),(SECTHT ,A( 15)),
24.     C      1      (TANTHT ,A( 16)),(P ,A( 26)),(Q ,A( 27)),
25.     C      2      (R ,A( 28))
26.     C
27.     C      *** VARIABLE OUTPUTS ***
28.     C
29.     C      EQUIVALENCE(PHIDT ,A( 29)),(THETOT ,A( 30)),(PSIDT ,A( 31)),
30.     C      1      (PD ,A( 32)),(QD ,A( 33)),(ND ,A( 34))
31.     C
32.     C      *** CONSTANTS ***
33.     C
34.     C      EQUIVALENCE(RADTOD ,A(141))
35.     C
36.     C      CALCULATE ATTITUDES
37.     C      PHIDT = P*TANTHT+(Q*SPHI+R*CPHI)

38.     C      THETOT = Q*CPHI+R*SPHI
39.     C      PSIDT = SECTHT+(Q*SPHI+R*CPHI)
40.     C      CALCULATE ANGULAR VELOCITY IN DEGREES
41.     C      PD = P/RADTOD
42.     C      QD = Q/RADTOD
43.     C      ND = R/RADTOD
44.     C
45.     C      RETURN
46.     C      END
IASSIGN (MIS1,03,BILSB)
IFORTNAN LG,NB
EXT. FORTNAN IV, VERSION E00

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287      DATA #SILS /X20574/
288      EQUIVALENCE (#SILS ,#L2627)
289      C
290      C      *** VARIABLE INPUTS ***
291      C
292      C      EQUIVALENCE (X ,#A114977), (Y ,#A115077), (Z ,#A115177)
293      C
294      C      EQUIVALENCE (ILSFLS ,#L1 ,#L2 ,#L3), (JJCDDP ,#L1 ,#L2 ,#L3), (SILS ,#L1 ,#L2 ,#L3)
295      C
296      C      *** VARIABLE OUTPUTS ***
297      C
298      C      EQUIVALENCE (SS ,#A117177), (LLOC ,#A117277), (SLOPE ,#A117377)
299      C      S      (SSS ,#A117477), (LLOC ,#A117577), (RINK ,#A117677)
300      C
301      C      *** INTERNALLY GENERATED PARAMETERS ***
302      C
303      C      EQUIVALENCE (SSS ,#A117777), (LLOC ,#A117877), (LLOC ,#A117977)
304      C      S      (SSS ,#A118077), (LLOC ,#A118177), (RINK ,#A118277)
305      C      Z      (SLOPE ,#A118377), (SLOPE ,#A118477), (RINK ,#A118577)
306      C      1      (CILS1 ,#A118677), (CILS2 ,#A118777), (CILS3 ,#A118877)
307      C      2      (CILS4 ,#A118977)
308      C
309      C      *** CONSTANTS ***
310      C
311      C      EQUIVALENCE (RADTOD ,#A114177), (DEGTOR ,#A114277)
312      C
313      C      IF (JJCDDP.EQ.0)IGR TO 99
314      C      IF (ILS.EQ.1)IGR TO 20
315      C      NO ILS REQUIRED
316      C      LGS=LLOC=0
317      C      GO TO 30
318      C      99 CONTINUE
319      C      EXECUTE ONLY IF INITIALIZATION NOT COMPLETE
320      C      GO TO 11,2,3,ILSFLS
321      C
322      C      ILSFLS
323      C      1      MAIN RUNWAY,3 DEG SLOPE
324      C      2      MAIN RUNWAY,6 DEG SLOPE
325      C      3      MAIN RUNWAY,2 SEGMENT

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76.      1 CONTINUE
77.      C 1L5 CONSTANTS FOR MAIN RUNWAY, J DEG GLIDE SLOPE
78.          XGS = 1000.0
79.          XLDC = 11000.0
80.          YLOC = 0.0
81.          SGS = 0.75
82.          WLOC = 2.0
83.          USLOPE = 3.0
84.          BSLOPE = 3.0
85.          MKINK = 0.0
86.          GO TO 10
87.      2 CONTINUE
88.      C 1L5 CONSTANTS FOR MAIN RUNWAY, 6 DEG GLIDE SLOPE
89.          XGS = 1000.0
90.          XLDC = 11000.0
91.          YLOC = 0.0
92.          SGS = 0.75
93.          WLOC = 2.0
94.          USLOPE = 6.0
95.          BSLOPE = 6.0
96.          MKINK = 0.0
97.          GO TO 10
98.      3 CONTINUE
99.      C 1L5 CONSTANTS FOR 2 SEGMENT (0/3) TO MAIN RUNWAY
100.         XGS = 1000.0
101.         XLDC = 11000.0
102.         YLOC = 0.0
103.         SGS = 0.75
104.         WLOC = 2.0
105.         USLOPE = 6.0
106.         BSLOPE = 3.0
107.         MKINK = 500.0
108.      10 CONTINUE
109.      C COLLECTIVE CONSTANTS
110.          CILS1 = RADTOD/SGS
111.          CILS2 = RADTOD/SLOC
112.          CILS3 = TAN(BSLOPE*DEGTOR)
113.          CILS4 = TAN(USLOPE*DEGTOR) - CILS3

114.          XKINK = XGS * MKINK/CILS3
115.      C MAIN ROUTINE
116.      20 CONTINUE
117.      C HERE IMMEDIATELY IF IN 'COMPUTE'
118.          MKINK = -(X - XKINK)
119.          XGS = -(X - XGS)
120.          XLDC = -(X - XLDC)
121.          WSLOPE = XGS * CILS3 * 0.5 * (RKINK + ABS(RKINK)) * CILS4
122.          SGS = ROUND(-1.0, 1.0, CILS1 * (W - WSLOPE) / XGS)
123.          SLOC = ROUND(-1.0, 1.0, CILS2 * (Y - YLOC) / XLDC)
124.      30 CONTINUE
125.          RETURN
126.          END
1ASSIGN (M1S1,03,SINTS)

IFORTNAN LB,NS
EXT. FORTRAN IV, VERSION E00

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1.      SUBROUTINE SINIT
2.      C
3.      C
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67.     C
68.     C
69.     C
70.     C
71.     C
72.     C
73.     C
74.     C
75.     C

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      * WRITTEN BY : D.OLDFIELD
      * DATE 17-10-77
      * DESCRIPTION : THIS SUBROUTINE CALCULATES
      * THE INITIAL VALUES OF THE INERTIA COEFFICIENTS
      * GIVEN IX, IY, IZ, IZX
      * THE INITIAL VALUES OF VARIABLES LISTED BELOW
      * FROM THE STATED INPUT VARIABLES FROM THE USER
      *
      * USER PROVIDED INFORMATION:-
      * BETA DIC, ALFA DIC, GAMMA DIC, VKTIC, XIC, YIC,
      * MIC, ISMR, VNKTO, PSIND, PSIDIC, SHREF, SPAN, W
      *
      * INITIAL VALUES OUTPUT:-
      * HBSLOPE, CPSIW, SPSIW, VWNLO, VWELD, SHRFAC,
      * VWN, VNE, VND, DENR, SPSONR, TEMPH, PRESSK,
      * ROOTSIG, VT, VK, VKNIC, VKEIC, VKDIC, VN, VE,
      * VD, PSDIC, THETA DIC, RADTOD, DEGTOR,
      * FPSTKT, KTOPP, D, RMOSL, SPSL, PDIC, QDIC,
      * HDIC, PHIDIC, XMASS, YXMASS, SIZ
      *
      * N=8
      * MIC NEGATIVE PLACES AIRCRAFT ON ILS BEAM
      * AT SPECIFIED RANGE XIC
      * KISA = 0 (DEFAULT) SELECTS SEA LEVEL ATMOSPHERE
      * VKTIC = 0.0 SETS SYSTEM UP FOR ZERO GROUND SPEED
      * OTHERWISE SETS UP FOR AIRSPEED (EAS) = VKTIC
      *
      * *****

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12-8-76 SYSTEM COMMON ENLARGED
17-10-77 C13 CORRECTED
8. 2.78 FLAG FOR HIGH SPEED DAC CONTROL ADDED
5.6.78 COMMON HSHID ENLARGED TO 2 WORDS
COMMON/SYSTEM/A(1000),L(400)

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38.     COMMON/HSHID/HSHID, IDUM
39.     C
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      * DATA HSHID /050678/
      * EQUIVALENCE(HSHID, L(263))
      *
      * *** INPUT VARIABLES ***
      *
      * EQUIVALENCE(XIX, A( 48)),(XIY, A( 49)),(XIZ, A( 50)),
      * 1 (XIZX, A( 51)),(ZCG, A( 98)),(XCGREF, A( 99)),
      * 2 (ZCGREF, A(100)),(SPAN, A(103)),(SHREF, A(106)),
      * 3 (HBSLOPE, A(173)),(BETA DIC, A(191)),(ALFA DIC, A(192)),
      * 4 (GAMMA DIC, A(193)),(VKTIC, A(194)),(XIC, A(195)),
      * 5 (MIC, A(197)),(XCO, A(199)),(VKNTO, A(202)),
      * 6 (PSIND, A(203)),(PSIDIC, A(204)),(SHRFAC, A(228)),
      * 7 (W, A(198))
      * EQUIVALENCE (ISMR, A( 5)),(KISA, A( 1))
      *
      * *** OUTPUT VARIABLES ***
      *
      * EQUIVALENCE(XMASS, A( 1)),(YXMASS, A( 2)),(CI1, A( 35)),
      * 1 (CI2, A( 36)),(CI3, A( 37)),(CI4, A( 38)),
      * 2 (CI5, A( 39)),(CI6, A( 40)),(CI7, A( 41)),
      * 3 (CI8, A( 42)),(CI9, A( 43)),(CI10, A( 44)),
      * 4 (VWN, A( 55)),(VNE, A( 56)),(VNO, A( 57)),
      * 5 (RMOSL, A( 79)),(SPSL, A( 80)),(DXCG, A(101)),
      * 6 (QZCG, A(102)),(SIZ, A(108)),(X, A(149)),
      * 7 (YKNIC, A(211)),(YKEIC, A(212)),(VKDIC, A(213)),
      * 8 (PHIDIC, A(214)),(THETA DIC, A(215)),
      * 9 (VH, A(217)),(VE, A(218)),(VD, A(219))
      *
      * EQUIVALENCE(PDIC, A(220)),(QDIC, A(221)),(RDIC, A(222)),
      * 1 (CPSIW, A(224)),(SPSIW, A(225)),(VWNLO, A(226)),
      * 2 (VWELD, A(227)),(RHO, A( 72)),(SPSONR, A( 73)),
      * 3 (ROOTSIG, A( 71)),(VT, A( 67)),(VK, A( 65)),
      * 4 (ALPHA, A( 88)),(PALPHA, A( 86))

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76. C          ***  CONSTANTS DERIVED  ***
77. C
78. C  EQUIVALENCE(RA)TOD ,A(141), (DEGTOR ,A(142), (FPSTKT ,A(143),
79. 1  (XK2FPS ,A(144), (Q ,A(145), (DENM ,A(178),
80. 2  (SPSNDR ,A(184), (TEMPN ,A(181), (PRESSM ,A(182),
81. 3  (TEMPSL ,A(176), (PRESSL ,A(177), (RU ,A(146))
82. C
83. C  INITIALISE CONSTANTS
84. DATA RADTOD,DEGTOR/57.295780,0.0174533/
85. DATA FPSTKT,XK2FPS/0.5921053,1.646089/
86. DATA G,RHOSL,SPSL/32.174,0.0023769,1116.45/
87. DATA RU/0.03108/
88. DATA TEMPSL,PRESSL/ZRB,15,14.69597/
89. DATA DENM,SPSNDR,TEMPR,PRESSM/1.0,1.0,1.0,1.0/
90. DATA PDIC,QDIC,MDIC,PHIDIC/0.0,0.0,0.0,0.0/
91. DATA KISA/0/
92. DATA ISHR/1/
93. C
94. C  SET FLAG FOR HIGH SPEED WYRHO OUTPUT
95. DATA IHSHO/1/
96. C
97. C  C10 = 1.0/(XIZ*XIX=XIZX=XIZX)
98. C  CALCULATE INITIAL VALUES OF INERTIA COEFFICIENTS
99. C11 = C10*XIZ
100. C12 = C10*XIZX
101. C13 = C10*(XIX=XIY=XIZI=XIZX
102. C14 = C10*(XIZ=(XIZI=XIZI=XIZX=XIZX)
103. C15 = 1.0/XIY
104. C16 = C15*XIZX
105. C17 = C15*(XIZ=XIX)
106. C18 = C10*XIX
107. C19 = C10*(XIX=XIY)*XIX=XIZX=XIZX)
108. C10 = C10*XIZX=(XIX=XIY=XIZI)
109. C
110. C  ADJUST M FOR A/C ON BEAM (M<0)
111. IF (MIC.GT.0.0) GO TO 10
112. M = XIC
113. CALL B1LS

114. MIC = HSLOPE
115. 10 CONTINUE
116. C
117. IF (KISA.EQ.0) GO TO 24
118. C  SET UP INITIAL ATMOSPHERIC VALUES
119. CALL WATMOS(MIC,DENM,SPSNDR,TEMPR,PRESSR)
120. 24 HOOTSIG = SURT(DENM)
121. WPSOVD = SPSL*SPSNDR
122. NHO = RHOSL*DENM
123. TALPHA = TEMPSL*TEMPR
124. PALPHA = PRESSL*PRESSR
125. C
126. C
127. C  CALCULATE LOCAL TRUE WIND COMPONENTS GIVEN DATUM WIND
128. C  SPEED AND DIRECTION
129. C
130. CPSI = COS(PS)ND=DEGTOR)
131. WPSI = SIN(PS)ND=DEGTOR)
132. VWNLO = -VWKT0*XK2FPS*CPSI
133. VWELO = -VWKT0*XK2FPS*SPSI
134. C  ALLOWANCE FOR WIND SKEW
135. CALL WSKW(MIC,SHR,SHR)
136. VWN = VWNLO*SHR
137. VWE = VWELO*SHR
138. VND = 0.0
139. C
140. C  SET STARTING VALUE OF TRACK EQUAL TO HEADING
141. PSIKIC = PSIDIC
142. C  AND STORE DESIRED HEADING FOR REFERENCE
143. PSIDICO = PSIDIC
144. C
145. C  CALCULATE SIN AND COS OF GAMMA
146. CUV = COS(GAMDIC=DEGTOR)
147. CUH = COS(PSIKIC=DEGTOR)
148. SUV = SIN(GAMDIC=DEGTOR)
149. SUH = SIN(PSIKIC=DEGTOR)
150. IF (VKTIC.LE.1.0) GO TO 20
151. C

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171077

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152. C      SET UP VELOCITIES FOR DESIRED AIRSPEED
153. C      AND ITERATE TO GET DESIRED HEADING
154. C INITIALISE LOOP COUNT
155. C      I = 0
156. C LOOP
157. C      30 CONTINUE
158. C      I = I + 1
159. C      CGM = CRSI(PSINDIC+VEGTOR)
160. C      SGM = SIN(PSINDIC+VEGTOR)
161. C
162. C      VT = VKTIC+K2RPS/HOBTSLU
163. C      SOLVE QUADRATIC FOR VK
164. C      B = 2*0.01(VN+CGM+VW+SGM)*CGV+VWD+SGV
165. C      C = VN+VW+VW*VW+VW*VW+VW*VW+VW*VW
166. C      VK = (-B+SQRT(B*B-4*C))/2.0
167. C      CALCULATE GROUND SPEED COMPONENTS
168. C      VKNIC = VK*CGV+CGM
169. C      VKEIC = VK*CGV+SGM
170. C      VKDIC = -VK*SGV
171. C      CALCULATE COMPONENTS OF AIRSPEED IN EARTH AXES
172. C      VN = VKNIC+VWN
173. C      VE = VKEIC+VWE
174. C      VD = VKDIC+VWD
175. C      CALCULATE INITIAL HEADING
176. C      PSIAJ = 0.0
177. C      IF (VE.EQ.0.0.AND.VN.EQ.0.0) GO TO 16
178. C      PSIAJ = ATAN2(VE,VN)*RADTOD
179. C      16 PSIDIC = PSIAJ-RETADIC
180. C      DP = PSIDIC - PSIDIC
181. C      LIMIT NUMBER OF ITERATIONS FOR SAFETY
182. C      IF (I.GE.10) GO TO 26
183. C      TEST FOR HEADING GOOD ENOUGH
184. C      IF (ABS(DP).LT.0.1) GO TO 26
185. C      PSINDIC = PSINDIC + DP
186. C      GO TO 30
187. C
188. C      SET UP VALUES FOR ZERO GROUND SPEED
189. C
190. C      20 VK = 0.0
191. C      VKNIC = 0.0
192. C      VKEIC = 0.0
193. C      VKDIC = 0.0
194. C      VN = VWN
195. C      VE = VWE
196. C      VD = VWD
197. C      VT = SQRT(VN+VN+VE+VE+VD+VD)
198. C
199. C      26 GAMD = 0.0
200. C      IF (VN.EQ.0.0.AND.VE.EQ.0.0.AND.VD.EQ.0.0) GO TO 18
201. C      GAMD = ATAN2(-VD,SQRT(VN+VN+VE+VE+VD+VD))
202. C      18 THETADIC = GAMD+ALPADIC
203. C
204. C      AIRCRAFT RELATED CONSTANTS
205. C
206. C      SB2 = SREF*SPAN*SPAN
207. C      XMASS = W/G
208. C      MXMASS = 1.0/XMASS
209. C      XCG = XCG*XCOREF
210. C      ZCG = ZCG*ZCOREF
211. C      RETURN
212. C      END
1ASSIGN (MIS1,03,SPHS)
1FORTHAN LS,NS
EXT. FORTHAN IV, VERSION EQU

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1.      SUBROUTINE SPATH
2.      C
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36.     C
37.     C

      .....
      *
      *   WRITTEN BY : D.ULUFIELD
      *   DATE : 12-8-76
      *   DESCRIPTION : THIS SUBROUTINE CALCULATES THE
      *   ANGLE OF ELEVATION AND TRACK AND THE VELOCITY
      *   OVER THE GROUND
      *
      *
      .....

12-8-76   SYSTEM COMMON ENLARGED
COMMON/SYSTEM/A(1000),L(100)

VERSION IDENTIFIER
DATA KSPATH /120876/
EQUIVALENCE(KSPATH ,L(200))

*** VARIABLE INPUTS ***
EQUIVALENCE(VKN ,A( 52)),(VKE ,A( 53)),(VKD ,A( 54))

*** VARIABLE OUTPUTS ***
EQUIVALENCE(GAMMA ,A( 61)),(GAMMA ,A( 62)),(PSIKR ,A( 63)),
1 (PSIKD ,A( 64)),(VK ,A( 65)),(VKRT ,A( 66))

*** CONSTANTS ***
EQUIVALENCE(FPSTKT ,A(103)),(RADTOD ,A(101))

      CALCULATE VELOCITY OVER GROUND
      VK = SQRT(VKN*VKN+VKE*VKE)
      VKRT = VK*FPSTKT

*** CALCULATE FLIGHT PATH ANGLES ***
INITIALISE ANGLES TO ZERO
PSIKR = 0.0
GAMMA = 0.0
      CALCULATE ANGLE OF ELEVATION
      RANGE +90 TO -90
      IF (VKD.EQ.0.0.AND.VK.EQ.0.0) GO TO 4
      GAMMA = ATAN2(-VKD,VK)
      GAMMA = GAMMA*RADTOD
      CALCULATE ANGLE OF TRACK
      RANGE 0(NORTH) TO 360
      IF (VKE.EQ.0.0.AND.VKN.EQ.0.0) GO TO 5
      PSIKR = ATAN2(VKE,VKN)
      ADJUST FOR RANGE
      IF (VKE.LT.0.0) PSIKR = 6.283185+PSIKR
5 PSIKD = PSIKR*RADTOD

      RETURN
      END
      ASSIGN (MISI,03),STVVS)

      IFORTNAN LB,MS
      EXT. FORTRAN IV, VERSION E00

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1. SUBROUTINE STV
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4. C
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25. C
26. C
27. C
28. C
29. C
30. C
31. C
32. C
33. C
34. C
35. C
36. C
37. C

      WRITTEN BY : B.N.TOMLINSON
      DATE       : 12-8-76
      REVISED   : 2-9-76 TO USE SYSTEM DISCRETES
                  6-9-76 WITH NEW TV CONSTANTS
                  FOR 700 MODEL
                  AND SHIP MOTION
                  8-9-76 HEIGHT AND BELT PROTECTION
                  9-10-76 TVCONS INCLUDED IN
                  SYSTEM COMMON AND
                  CYCLE LOGIC REVISED
      DESCRIPTION: 2-2-78 PILOT LOCATION CORRECTED
                  ALSO CALCULATES TV POSITIONS
                  N.B.
                  TVB MUST BE PROVIDED BY USER TO
                  SELECT APPROPRIATE
                  TV CONSTANTS

      LOGIC INPUTS
      BELT CYCLE      LCVLCE = 1
      BX RESET       LXTVIC = 1
      BY RESET       LYTVIC = 1
      FORWARD BLEW   LFPW  = 1
      BACKWARD BLEW LBACK = 1

      LOGIC OUTPUTS
      IDBYNC

      CONTROL OUTPUTS
      XIMX
      XIMY
      12-8-76

      SYSTEM COMMON ENLARGED
  
```

```

38. COMMON/SYSTEM/A(1000),L(400)
39. C
40. C
41. C
42. C
43. C
44. C
45. C
46. C
47. C
48. C
49. C
50. C
51. C
52. C
53. C
54. C
55. C
56. C
57. C
58. C
59. C
60. C
61. C
62. C
63. C
64. C
65. C
66. C
67. C
68. C
69. C
70. C
71. C
72. C
73. C
74. C
75. C

      VERSION IDENTIFIER

      DATA KSTV /2*0278/
      EQUIVALENCE(KSTV ,L(265))
      DIMENSION TVCON(8,3)
      DIMENSION IDS(32),ISLR(16),IP(32)

      *** VARIABLE INPUTS ***
      EQUIVALENCE(
1 (STMETA ,A(149)),(Y ,A(150)),(M ,A(151)),
2 (CPSI ,A(11)),(CTMETA ,A(12)),(SPSI ,A(152)),
3 (VKN ,A(10)),(PSIDT ,A(31)),(TNETDT ,A(30)),
4 (DXCG ,A(52)),(VKE ,A(53)),(VKD ,A(54)),
      (VSHIPRT ,A(101)),(DZCG ,A(102)),(ICREF ,A(59)),
      (VSHIPT ,A(149)),(ICREF ,A(107))
      2*0278

      EQUIVALENCE(JJCOMP ,L( 8))
      EQUIVALENCE(IDS(1) ,L(223)),(IP(1) ,L(191))
      EQUIVALENCE(LCYCLE ,IDS(5)),(LXTVIC ,IDS(6)),(LYTVIC ,IDS(7))
      EQUIVALENCE(LFPW ,ISLR(4)),(LBACK ,ISLR(5))

      *** VARIABLE OUTPUTS ***
      EQUIVALENCE(XTV ,A(152)),(YTV ,A(153)),(MTV ,A(154)),
1 (XDTV ,A(155)),(YDTV ,A(156)),(MDTV ,A(157)),
2 (XIMX ,A(159)),(XIMY ,A(160)),(XDBTM ,A(158)),
3 (XIC ,A(195)),(XPCG ,A(280)),(ZPCG ,A(281)),
4 (RXP ,A(282)),(RHP ,A(283)),(XICF ,A(284))
      2*0278
      2*0278

      EQUIVALENCE(IDSYNC ,ICLN(16))
      EQUIVALENCE(ISLR(1) ,L(151)),(ICLR(1) ,L(171))

      *** CONSTANTS ***
      EQUIVALENCE(XP ,A(109)),(ZP ,A(110)),(XK2FPS ,A(144))
  
```

```

76. C
77. EQUVALENCE(NTVB ,LI 2)
78. C
79. C *** INTERNALLY GENERATED PARAMETERS ***
80. C
81. EQUVALENCE(SXPL ,A(161)),(SXMIN ,A(162)),(SXPLUS ,A(163)),
82. 1 (SXMINUS ,A(164)),(SYPL ,A(165)),(SYMIN ,A(166)),
83. 2 (HTVLIM ,A(167)),(XDTMX ,A(168))
84. C
85. EQUVALENCE(TVCON (1,1),A(169))
86. C
87. C NTVB = 1(700)+2(2000) OR 3(5000),ACCORDING TO BELT USED
88. C
89. C SXPL = TV X TRAVEL LIMIT, POSITIVE, AND *NEAR BELT JOIN*
90. DATA TVCON(1,1),TVCON(1,2),TVCON(1,3)/ 11590.0, 33000.0, 77500.0/
91. C SXMIN = TV X TRAVEL LIMIT, NEGATIVE, AND *NEAR BELT JOIN*
92. DATA TVCON(2,1),TVCON(2,2),TVCON(2,3)/ -11590.0, -33000.0, -77500.0/
93. C SXPLUS = X CYCLE LIMIT
94. DATA TVCON(3,1),TVCON(3,2),TVCON(3,3)/ 12800.0, 34500.0, 89600.0/
95. C SXMINUS = X CYCLE LIMIT
96. DATA TVCON(4,1),TVCON(4,2),TVCON(4,3)/ -12800.0, -34500.0, -89600.0/
97. C SYPL = TV Y TRAVEL LIMIT, POSITIVE (RIGHT)
98. DATA TVCON(5,1),TVCON(5,2),TVCON(5,3)/ 2700.0, 7650.0, 54650.0/
99. C SYMIN = TV Y TRAVEL LIMIT, NEGATIVE (LEFT)
100. DATA TVCON(6,1),TVCON(6,2),TVCON(6,3)/ -2700.0, -7650.0, -54650.0/
101. C HTVLIM = CEILING FOR TV OPERATION
102. DATA TVCON(7,1),TVCON(7,2),TVCON(7,3)/ 600.0, 1480.0, 4285.7/
103. C XDTMX = TV SLEW VELOCITY
104. DATA TVCON(8,1),TVCON(8,2),TVCON(8,3)/ 389.0, 368.0, 2727.3/
105. C
106. C
107. C IF IJCOMP.EQ.1 IGO TO 5
108. C EXECUTE ONLY IF INITIALISATION NOT COMPLETE
109. SXPL = TVCON(1,NTVB)
110. SXMIN = TVCON(2,NTVB)
111. SXPLUS = TVCON(3,NTVB)
112. SXMINUS = TVCON(4,NTVB)
113. SYPL = TVCON(5,NTVB)
114. SYMIN = TVCON(6,NTVB)
115. HTVLIM = TVCON(7,NTVB)
116. XDTMX = TVCON(8,NTVB)
117. C STORE XIC FROM ICFIL FOR FUTURE USE
118. XICF = XIC
119. C ACTUAL PILOT LOCATION RELATIVE TO CG
120. XPCG = XP + DXCG*CHLF
121. ZPCG = ZP - DZCG*CHLF
122. C
123. 5 CONTINUE
124. C HERE IMMEDIATELY IF IN 'COMPUTE'
125. C
126. C *****
127. C *
128. C * SLEW
129. C *
130. C *****
131. C CHECK FOR SLEW DEMAND ON BELT UNIVE
132. C IF LFWD = 1, FORWARD SLEW AT XDTMX FT/SEC
133. IF (LFWD.EQ.0) GO TO 10
134. XDOTM = XDTMX
135. GO TO 14
136. C IF LBACK = 1, BACKWARD SLEW AT XDTMX FT/SEC
137. 10 CONTINUE
138. IF (LBACK.EQ.0) GO TO 12
139. XDOTM = -XDTMX
140. GO TO 14
141. 12 XDOTM = VKN
142. C ALLOW FOR SHIP VELOCITY
143. XDOTM = XDOTM - VSHIPKT*XR2FVS
144. 14 CONTINUE
145. C *****
146. C *
147. C * TV INTEGRATION CONTROL
148. C *
149. C *****
150. C
151. C TEST TO DETERMINE INTEGRATION STATE OF SX AND SY

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2*0278
2*0278


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152. C PUT SX AND SY IN COMPUTE, DESINE TO ZERO
153. XIMX = XIMY = 1.0
154. IUSYNC = 0
155. C IF LYTVIC = 1, SY RESETS
156. IF (LYTVIC.EQ.0) GO TO 20
157. XIMY = 0.0
158. 20 CONTINUE
159. C IF LXTVIC = 1, SX RESETS
160. IF (LXTVIC.EQ.0) GO TO 22
161. XIMX = 0.0
162. XIC = XICF
163. GO TO 24
164. C CHECK FOR TV NEAR BELT JOIN
165. 22 IF (SAXMIN.LT. X.LT.SXPLUS) GO TO 24
166. C TV NEAR BELT JOIN
167. C IF LCYCLE = 1, X COMPUTATION CYCLES BETWEEN SAXMINUS AND SXPLUS
168. IF (LCYCLE.EQ.0) GO TO 24
169. IUSYNC = 1
170. C IUSYNC = 1 TO DISCONNECT POSITION ERROR DRIVE TO TV
171. C COMMAND IMMEDIATE MOVEMENT IF A SITTING WAY OUT
172. IF (X.LT.SAXMINUS) GO TO 23
173. C WHEN SX REACHES SXPLUS, RESET SX TO SAXMINUS
174. IF (X.LT.SXPLUS) GO TO 24
175. 23 CONTINUE
176. XIMX = 0.0
177. XIC = SAXMINUS
178. 24 CONTINUE
179. C
180. C TV POSITION
181. C
182. C PILOT AT XP,ZP = NH ZP NORMALLY NEGATIVE!!! IF EYE ABOVE DATUM LINE
183. XHP = XPCG*CTHETA + ZPCG*STHETA 240278
184. RHP = XPCG*STHETA + ZPCG*CTHETA 240278
185. XTV = X + XHP*CPSI
186. YTV = Y + RHP*SPSI
187. HTV = H + RHP
188. C TV RATES
189. XDTV = XDOTH + XHP*SPSI + PSIDT + RHP*CPSI + THETDT

190. YDTV = VKE + RHP*CPSI + PSIDT + RHP*SPSI + THETDT
191. HDTV = VKD + RHP*THETDT
192. C ON LIMITS, PUT RATES TO ZERO TO KEEP TV DRIVE QUIESCENT
193. IF (LCYCLE.EQ.1) GO TO 30
194. IF ((XTV.LT.SAXMIN).OR.(LXTVIC.EQ.1)) XDTV = 0.0
195. 30 CONTINUE
196. C IF TV ABOVE CEILING, SET HDTV TO ZERO
197. IF (HTV.GT.HTVLIM) HDTV = 0.0
198. C KEEP TV POSITION WITHIN LIMITS
199. XTV = BRUND(SAXMIN,SXPL,XTV)
200. YTV = BRUND(SYMIN,SYPL,YTV)
201. HTV = BRUND(0.0,HTVLIM,HTV)
202. C
203. RETURN
204. END

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IANSION (MIS1,03,SVLIS)

IFORTNAN LS,NB
EXT: FORTNAN IV, VERSION E00

```

1.      SUBROUTINE SVELOC1
2.      C
3.      C
4.      C
5.      C
6.      C
7.      C
8.      C
9.      C
10.     C
11.     C
12.     C
13.     C
14.     C
15.     C      12-R-76      SYSTEM COMMON ENLARGED
16.     C      COMMON/SYSTEM/A(1000),L(100)
17.     C
18.     C      VERSION IDENTIFIER
19.     C
20.     C      DATA KSVELOC1/221276/
21.     C      EQUIVALENCE(KSVELOC1,L(266))
22.     C
23.     C      *** VARIABLE INPUTS ***
24.     C
25.     C      EQUIVALENCE(VKN      ,A( 52)),(VKE      ,A( 53)),(VKD      ,A( 54)),
26.     C      1      (VHN      ,A( 55)),(VHE      ,A( 56)),(VHD      ,A( 57)),
27.     C      2      (S11      ,A( 17)),(S12      ,A( 18)),(S13      ,A( 19)),
28.     C      3      (S21      ,A( 20)),(S22      ,A( 21)),(S23      ,A( 22)),
29.     C      4      (S31      ,A( 23)),(S32      ,A( 24)),(S33      ,A( 25))
30.     C
31.     C      *** VARIABLE OUTPUTS ***
32.     C
33.     C      EQUIVALENCE(UB      ,A( 58)),(VB      ,A( 59)),(WB      ,A( 60)),
34.     C      1      (VKN      ,A(217)),(VVE      ,A(218)),(VVD      ,A(219))
35.     C
36.     C      CALCULATE VELOCITY RELATIVE TO THE AIR
37.     C      VN = VKN-VHN
38.
39.     C      VE = VKE-VHE
40.     C      VD = VKD-VKD
41.     C      CALCULATE VELOCITY RELATIVE TO BODY AXES
42.     C      UB = S11*VN+S12*VE+S13*VD
43.     C      VB = S21*VN+S22*VE+S23*VD
44.     C      WB = S31*VN+S32*VE+S33*VD
45.     C      RETURN
46.     C      END
47.     C      IASSIGN (MISL,03,SVL25)
48.     C      IFORTNAN LB,NB
49.     C      EXT. FORTNAN IV, VERSION E00

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```

1* SUBROUTINE SVELCC2
2* C
3* C
4* C
5* C
6* C
7* C
8* C
9* C
10* C
11* C
12* C
13* C
14* C
15* C
16* C
17* C
18* C
19* C
20* C
21* C
22* C
23* C
24* C
25* C
26* C
27* C
28* C
29* C
30* C
31* C
32* C
33* C
34* C
35* C
36* C
37* C

.....
* WRITTEN BY : D.GLOFIELD
* DATE : 21.3.78
* DESCRIPTION : THIS SUBROUTINE CALCULATES THE
* RESULTANT AIR SPEED AND THE EQUIVALENT AIR
* SPEED, DYNAMIC PRESSURE AND HEAD.
* USING ATMOSPHERIC PROPERTIES APPROPRIATE TO
* SPECIFIED VALUE OF KISA
*
* -1 FIXED VALUES APPROPRIATE TO HIC
* 0 FIXED (SEA LEVEL) VALUES = DEFAULT
* 1 VALUES VARY WITH HEIGHT
*
.....

12=8=76 SYSTEM COMMON ENLARGED
21.3.78 TRATIO ETC GIVEN DATA VALUES
COMMON/SYSTEM/A(1000),L(1000)

VERSION IDENTIFIER

DATA KSVELCC2/210378/
EQUIVALENCE(KSVELCC2,L(267))

*** VARIABLE INPUTS ***

EQUIVALENCE(LUB ,A( 58)),(VH ,A( 59)),(WB ,A( 60)),
1 (H ,A(151)),(SREF ,A(106)),(CREP ,A(107)),
2 (SPAN ,A(103)),(SBZ ,A(108))
EQUIVALENCE(KISA ,L( 1))

*** VARIABLE OUTPUTS ***

EQUIVALENCE(VT ,A( 67)),(VTKT ,A( 68)),(VEAS ,A( 69)),

38* 1 (VEASKT ,A( 70)),(UDYN ,A(125)),(XPACH ,A( 75)),
39* 2 (NDTSIG ,A( 71)),(RHO ,A( 72)),(SPSND ,A( 73)),
40* 3 (DEPR ,A( 78)),(SPSNR ,A( 84)),(HFRHOV ,A(124)),
41* 4 (TEMPR ,A( 81)),(PRESSR ,A( 82)),(UDYNS ,A(126)),
42* 5 (USREF ,A(127)),(USSPAN ,A(128)),(USBEIV ,A(129)),
43* 6 (TRATIO ,A( 89)),(ARATIO ,A( 85)),(ORATIO ,A( 83)),
44* 7 (PRATIO ,A( 87)),(TALPHA ,A( 88)),(PALPHA ,A( 86))

*** CONSTANTS ***

EQUIVALENCE(FPSTKT ,A(143)),(RHOSL ,A( 79)),(SPSL ,A( 80)),
48* 1 (TEMPSL ,A( 76)),(PRESSL ,A( 77))

50* C
51* C
52* C
53* C
54* C
55* C
56* C
57* C
58* C
59* C
60* C
61* C
62* C
63* C
64* C
65* C
66* C
67* C
68* C
69* C
70* C
71* C
72* C
73* C
74* C
75* C

DATA TRATIO,ARATIO,ORATIO,PRATIO/991.0/
210378

*****

CALCULATE TOTAL AIR SPEED
VT = SQRT(UB*UB+VH*VH+WB*WB)
VTKT = VT*FPSTKT
SET VALUES OF NDTSIG,RHO AND SPSND
IF (KISA.NE.1) GO TO 3
CALL SATMOS(TDENS,SPSNR,TEMPR,PRESSR)
RHO = RHOSL * TDEN
SPSND = SPSL * SPSNR
NDTSIG = SQRT(DENR)
TALPHA = TEMPSL*TEMPR
PALPHA = PRESSL*PRESSR
3 CONTINUE
CALCULATE EQUIVALENT AIRSPEED
VEAS = VT*NDTSIG
VEASKT = VEAS*FPSTKT
CALCULATE DYNAMIC PRESSURE
HFRHOV = 0.5*RHO*VT
UDYN = HFRHOV*VT

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```

76.      QDYN = QDYN*SQREF
77.      USCREP = QDYN*CREP
78.      USSPAN = QDYN*SPAN
79.      USBZIV = HLFHMOV*SBZ
80.      C      CALCULATE MACH NR.
81.      XMACH = VT/SPSOND
82.      C CALCULATE COMPRESSIBLE ADIABATIC FLOW RELATIONSHIPS
83.      C MACH NUMBER < 1.0
84.      XX = 1.0 + 0.2*XMACH*XMACH
85.      C ADIABATIC STATIC/TOTAL TEMPERATURE
86.      TRATIO = 1.0/XX
87.      C ADIABATIC SPEED OF SOUND RATIO
88.      ANATIO = SQRT(TRATIO)
89.      C ADIABATIC DENSITY RATIO
90.      URATIO = ANATIO**5
91.      C ADIABATIC STATIC/TOTAL PRESSURE
92.      MRATIO = DRATIO*TRATIO
93.      RETURN
94.      END

```

1ASSIGN (MIS),OJ,SHNDS)

IFORTMAN LS,NS
EXT: FORTMAN IV, VERSION EOO

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1.      SUBROUTINE SWIND
2.      C
3.      C
4.      C
5.      C      * WRITTEN BY I B.N.TOMLINSON
6.      C      * DATE      1 20.9.76
7.      C      * REVISED  1 22.12.78 TO IMPROVE COMM'N WITH GUSTS
8.      C      *           24.02.78 VNE CORRECTED + FRACG,NGUSTS PROTECTED
9.      C      * DESCRIPTION: THIS SUBROUTINE CALCULATES TOTAL WIND
10.     C      * COMPONENTS, INCLUDING TURBULENCE AND WIND SHEAR
11.     C
12.     C
13.     C
14.     C      COMMON/SYSTEM/A(1000),L(100)
15.     C      COMMON /FRN/ AND /INITGUST/ COMMUNICATE WITH S/N GUSTS ONLY
16.     C      COMMON/FRN/FRACG,RODECAY,NGUSTS
17.     C      COMMON/INITGUST/IFLAG,ISN
18.     C      EQUIVALENCE(KSWIND ,L(268))
19.     C
20.     C      VERSION IDENTIFIER
21.     C
22.     C      DATA KSWIND/2*0278/
23.     C
24.     C      *** INPUT VARIABLES ***
25.     C
26.     C      EQUIVALENCE(M      ,A(151)),(MIC      ,A(197)),(VKTIC   ,A(194)),
27.     C      1      (VWNO    ,A(226)),(VWVELO ,A(227)),(VWNOLO ,A(223)),
28.     C      2      (CPSIN   ,A(224)),(SPSIN   ,A(225)),(FRAMET1 ,A( 92)),
29.     C      3      (USIG    ,A(235)),(VBSIG  ,A(236)),(WSIG    ,A(237)),
30.     C      4      (SFRACG  ,A(278)),(SRODECAY,A(279))
31.     C
32.     C      DIMENSION IDS(32)
33.     C      EQUIVALENCE(IISHR ,L( 5)),(IJJCOMP ,L( 8)),(ING    ,L(167)),
34.     C      1      (LTJRB  ,IDB(8)),(IDS(1) ,L(223)),(LSELD  ,L(168))
35.     C
36.     C      *** OUTPUT VARIABLES ***
37.     C

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38.      EQUIVALENCE(UTURB ,A(232)),(VTURB ,A(233)),(WTURB ,A(234)),
39.      1      (VNM ,A(25)),(VNE ,A(26)),(VND ,A(27)),
40.      2      (VNL ,A(229)),(VNL ,A(230)),(VNDL ,A(231)),
41.      3      (SHRFAC ,A(228))
42.      C
43.      C      *** CONSTANTS ***
44.      C
45.      EQUIVALENCE(KRZFPS ,A(100))
46.      C
47.      DATA NG/0/
48.      DATA VNDL/0.0/
49.      C SET UP FRAC0,RDECAY
50.      DATA BFRAC0,SRDECAY/0.0,0.7/
51.      DATA LSEED/0/
52.      C CALCULATE WIND AT HEIGHT
53.      CALL NSHEAR(ISHR,H,SHRFAC)
54.      VNL = VNL0*SHRFAC
55.      VNL = VNL0*SHRFAC
56.      C
57.      IFLAG = JJCOMP
58.      IF (JJCOMP.EQ.0) GO TO 10
59.      C INITIALISATION COMPLETE
60.      IF (ITURB.EQ.1) GO TO 20
61.      C TURBULENCE IS NOT REQUIRED
62.      GO TO 30
63.      10 CONTINUE
64.      C INITIALISATION
65.      M = HIC
66.      C PICK UP TURB PARAMETERS FROM SYSTEM VARIABLES
67.      FRAC0 = BFRAC0
68.      C CHECK ON RANGE
69.      IF (FRAC0.GT.0.99) FRAC0 = 0.99
70.      RDECAY = SRDECAY
71.      IFR = LSEED
72.      C SET UP NGUSTS ACCORDING TO INITIAL SPEED
73.      NGUSTS = NG*(VKTIC**KRZFPS/200.0)
74.      C CHECK ON RANGE
75.      IF (NGUSTS.LT.1) NGUSTS = 1
76.
77.      NMAX = 1000.0/FRAC0
78.      IF (NGUSTS.GT.NMAX) NGUSTS = NMAX
79.      20 CONTINUE
80.      C TURB IS REQUIRED
81.      CALL GUSTS(U0,V0,W0,FRAC0,M)
82.      IF (JJCOMP.EQ.0) GO TO 30
83.      C INITIALISATION IS COMPLETE,SO LET TURBULENCE OUT
84.      UTURB = UBIG*UG
85.      VTURB = VBIG*VG
86.      WTURB = WBIG*WG
87.      GO TO 40
88.      30 CONTINUE
89.      C TURBULENCE OUTPUTS SET TO ZERO (INITIALISATION,OR NOT REQUIRED)
90.      UTURB = VTURB = WTURB = 0.0
91.      40 CONTINUE
92.      C CALCULATE TOTAL WIND COMPONENTS
93.      VNM = VNL = (UTURB**CPSIN + VTURB**CPSIN)
94.      VNE = VNL = (VTURB**CPSIN + UTURB**CPSIN)
95.      VND = VNDL = WTURB
96.      C
97.      RETURN
98.      END
99.      IASIGN (MIBI,03,SYCS)
100.
101.      IFORTAN LB,NS
102.      EXT. FORTAN IV, VERSION E00

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1.      SUBROUTINE SYSOCM
2.      C
3.      C .....
4.      C
5.      C *
6.      C * WRITTEN BY : B.N.TOMLINSON *
7.      C * DATE : 24.2.78 *
8.      C * THIS ROUTINE CALLS PV200 TO PROVIDE ACCESS *
9.      C * TO SYSTEM COMMON VARIABLES *
10.     C * REVISED 12.9.76 TO INCLUDE INPUT FROM CHANGES FILE *
11.     C * 8.10.76 TVCON(8,3) ADDED *
12.     C * 29.11.76 DIMETES NAMES ADDED *
13.     C * 22.12.76 FNAME TIME VARIABLES ADDED *
14.     C * 31.5.77 NNUM ADDED *
15.     C * 18.10.77 LIDACA ETC. *
16.     C * 8. 2.78 DUMMY 'A' VARIABLES REPLACED BY ARRAYS *
17.     C * 24.2.78 LIDAC REVISED *
18.     C * .....
19.     C
20.     C
21.     C VERSION IDENTIFIER
22.     C
23.     C DATA KSYSOCM/240278/
24.     C SET UP COMMUNICATION WITH DAC HARDWARE ADDRESSES
25.     C COMMON/DACNOS/IDACAD(50)                                080278
26.     C
27.     C COMMON/SYSTEM/
28.     C X XHABS, XHABS, PSIN, PSID, THETA, THETA, PHIN, PHID, SPSI,
29.     C 1 CPSI, STHETA, CTHETA, SPIN, CPHI, SECTH, TANTH, S11(9),
30.     C 2 P, U, M, PHIUT,
31.     C 3 THETD, PSIUT, PD, QD, RD, C11(10),
32.     C 4 PDDT, UDDT, RDDT, X1X, X1Y,
33.     C 5 X1Z, X1ZX, YKN, YKE, YKD, YKN, YNE, YND, UB, VB,
34.     C 6 W, GAMMA, GAMMA, PSIKR, PSIKD, VK, VKKT, VT, VTK, VEAS,
35.     C 7 VEASKT, ROOTSIG, RMD, SPSOND, A74, XMACM, TEMPL, PRESSL, DENR, RHOSL,
36.     C 8 WPSL, TEMPR, PRESSR, DRATIO, SPINDR, ANATIO, PALPA, PHATIO, TALPA,
37.     C * * * * *
38.     C
39.     C 100
40.     C COMMON/SYSTEM/
41.     C X ZCRNF, DXCG, DZCG, SPAN, XLTAIL, STAIL, SHRF, LNEF, SBZ, XP,
42.     C 1 ZP, ALFA, ALFAD, BETAR, HETAU, A115, SALFA, CALFA, SBETA, CBETA,
43.     C 2 ALFADOT, BETADOT, A122, A123, MLFRMO, UDYM, UDYNS, QSCRF, QSSPAN,
44.     C * * * * * QSB21V,
45.     C 3 A130, XLLOT, XMMOT, XNNTOT, F1X, FTY, FTZ, F1N, F1E, F1D,
46.     C 4 A140, RAOT00, DEGTOM, FPSTKT, XKZFPS, G, NG, A147, A148, X,
47.     C 5 Y, M, XTV, YTV, MTV, XDTV, YDTV, MUIV, XDTM, X1M,
48.     C 6 X1M, SXPL, SXMIN, SXPLUS, SXMINUS, SYPL, SYNIN, MYVLM, XOTM, VSHPKT,
49.     C 7 A170, EGB, ELCC, HSLDPE, NGS, MLDC, RKINK, XGS, ALDC, YLDC,
50.     C 8 BGS, SLOC, HKINK, HSLDPE, USLDP, RKINK, C1LS1, C1LS2, C1LS3, C1LS4,
51.     C 9 A190, BETADIC, ALFADIC, GAMDIC, VKTIC, XIC, YIC, HIC, W, XG
52.     C
53.     C 200
54.     C COMMON/SYSTEM/
55.     C X X1LSFLAG, X1SHN, VKRTO, PSIN, PSIDIC, A205T210(6),
56.     C 1 VKNIC, VKEIC, VKDIC, PHIDIC, THETADIC, A216, VN, VE, VD,
57.     C 2 PDI, DDIC, MDIC, VDL0, CPSIN, SPSIN, VVNL0, VVLD, SHNAC, VVNL,
58.     C 3 VVEL, VVLD, UTUNB, VTURB, WTUNB, USIG, VSI0, HSI0, VVNDOT, VKEDOT,
59.     C 4 VKDDOT, AKCG, AYCG, AZCG, AZC41, AKACG, AYACG, AZACG, AXP, ATP,
60.     C 5 AZP, AZAP, AY1, A22, AX3, AY4, A23, X1, Y1, Z1,
61.     C 6 X2, Y2, Z2, X3, Y3, Z3, X4, Y4, Z4, X5,
62.     C 7 Y5, Z5, A27T27(16),
63.     C 8 A280T299(20)
64.     C * * * * * SFHALG, SHDECAY,
65.     C
66.     C 300
67.     C COMMON/SYSTEM/
68.     C X A300, AADC(64),
69.     C 6 TVCON(8,3),
70.     C 8 A389T399(11)
71.     C * * * * *
72.     C 400
73.     C COMMON/SYSTEM/
74.     C X A400, YADC(64),
75.     C 6 A465T499(35)
76.     C * * * * *
77.     C 500
78.     C COMMON/SYSTEM/
79.     C X A500, ADAC(64),
80.     C 6 A1565T1000

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```

76. C
77. COMMON/SYSTEM/
78. X KISA,NCPASS,NIPASS,ILSFLG,ISMR,L6,NTVB,JJCOMP,NUMD,
79. I NUMV,NDAC(64),
80. 7 KSADC,KSADC,KSDCR1,KSDCR2,KISDSCR,
81. B L80,NADC(64)
82. C 100
83. COMMON/SYSTEM/
84. 4 L145,L146,L147,LSILS,L149,
85. 5 IAD*SL,ISLR(16),
86. 6 NG,LSFEED,NRUN,
87. 7 IAD*CL,ICLR(16),
88. 8 L187,L188,L189,
89. 9 IDSCFL,IP(32)
90. C 200
91. COMMON/SYSTEM/
92. 2 IDS(32),
93. 5 KSACCBDD,KSACCLIN,KSACCR01,KSALFB&T,KSCOUNT,
94. 6 KSDCOS,KSEULEN,KSILS,K6INIT,KSPATH,KSTV,KSVELDC1,KSVELDC2,
95. C KSWIND,KSYSCOM,
96. 7 IPCDFL,ICD(32)
97. C 300
98. COMMON/SYSTEM/
99. X L303,L304,L1DAC(*8),
100. B L2DAC(*8)
101. C
102. C
103. C EQUIVALENCES = DISCRETES
104. C
105. C
106. C EQUIVALENCE(ILFND,ISLR(4)),
107. 5 (LBACK,ISLR(5))
108. C
109. C EQUIVALENCE(IDSYNC,ICLR(16))
110. C
111. C EQUIVALENCE(ICYCLE,IDS(5)),
112. 6 (LXTVIC,IS(6)),
113. 7 (LYTVIC,IDS(7))
114. B (LTJRB,IDS(8))
115. C
116. C FOR CALL TO PV200
117. DIMENSION NAME(2)
118. DATA NAME,'SYSCOM',
119. NAMELIST
120. C DEFINE INPUT UNIT FOR SYSTEM CHANGES FILE
121. DATA ISYS/50/
122. C
123. C
124. C CALL PV200(NAME)
125. GO TO 3
126. 2 INPUT(101)
127. 3 CONTINUE
128. C INPUT SEMI-PERMANENT CHANGES FROM SYSTEM INPUT FILE=UNIT ISYS
129. MEWIND ISYS
130. INPUT(11SYS)
131. MEWIND ISYS
132. RETURN
133. END
1ASSIGN (MISI,03,8CHRIS)
IFONTNAN LG,NS
EXT: FONTRAN IV, VERSION E00

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310577

2*0276
2*0278

```

1.      SUBROUTINE DSCRT1
2.      C
3.      C .....
4.      C
5.      C *   AUTHOR   : B.N.TOMLINSON
6.      C *   DATE    : 21-9-76
7.      C *   PURPOSE : THIS ROUTINE HANDLES DISCRETES IN FRAME 1.
8.      C *           THE FLAGS IAD*SL,IAD*CL,IOSCFL,IPCOFL
9.      C *           ARE SET EXTERNALLY AND DETERMINE WHICH
10.     C *           ROUTINES ARE TO BE EXECUTED
11.     C .....
12.     C
13.     C
14.     C COMMON/SYSTEM/A(1000),L(400)
15.     C
16.     C VERSION IDENTIFIER
17.     C
18.     C DATA KDSCRT1 /210976/
19.     C EQUIVALENCE(KDSCRT1 ,L( 77))
20.     C
21.     C EQUIVALENCE(IAD*SL ,L(150)),(IAD*CL ,L(170)),
22.     C 1 (IOSCFL ,L(190)),(IPCOFL ,L(270))
23.     C DATA IAD*SL,IAD*CL,IOSCFL,IPCOFL/1,1,1,0/
24.     C
25.     C IF(IAD*SL.EQ.1)CALL READSLM
26.     C IF(IAD*CL.EQ.1)CALL SETCLR
27.     C IF(IOSCFL.EQ.1)CALL READSCH
28.     C IF(IPCOFL.EQ.1)CALL SETDSCM
29.     C RETURN
30.     C END
IASSIGN (M151,D3,SCR25)

IFONTNAN LB,NS
EXT. FONTNAN Iv, VERSION EOO

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1.      SUBROUTINE DSCRT2
2.      C
3.      C .....
4.      C
5.      C *   AUTHOR   : B.N.TOMLINSON
6.      C *   DATE    : 24-8-76
7.      C *   PURPOSE : THIS ROUTINE HANDLES DISCRETES IN FRAME 2.
8.      C *           THE FLAGS IAD*SL,IAD*CL,IOSCFL,IPCOFL
9.      C *           ARE SET EXTERNALLY AND DETERMINE WHICH
10.     C *           ROUTINES ARE TO BE EXECUTED
11.     C .....
12.     C
13.     C
14.     C COMMON/SYSTEM/A(1000),L(400)
15.     C
16.     C VERSION IDENTIFIER
17.     C
18.     C DATA KDSCRT2 /240876/
19.     C EQUIVALENCE(KDSCRT2 ,L( 78))
20.     C
21.     C EQUIVALENCE(IAD*SL ,L(150)),(IAD*CL ,L(170)),
22.     C 1 (IOSCFL ,L(190)),(IPCOFL ,L(270))
23.     C
24.     C IF(IAD*SL.EQ.2)CALL READSLM
25.     C IF(IAD*CL.EQ.2)CALL SETCLR
26.     C IF(IOSCFL.EQ.2)CALL READSCH
27.     C IF(IPCOFL.EQ.2)CALL SETDSCM
28.     C RETURN
29.     C END
IASSIGN (M151,D3,IBDC5)

IFONTNAN LB,NS
EXT. FONTNAN Iv, VERSION EOO

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```

1.      FUNCTION ISDSCH(ISET,LINE)
2.      C
3.      C
4.      C
5.      C
6.      C
7.      C
8.      C
9.      C
10.     C
11.     C
12.     C
13.     C
14.     C
15.     C
16.     C
17.     C
18.     C
19.     C
20.     C
21.     DATA KISDSCH /190870/
22.     EQUIVALENCE(IKISDSCH ,L( 79))
23.     DIMENSION IP(32),IOS(32)
24.     EQUIVALENCE(ISLR(1) ,L(151)),(ICLR(1) ,L(171)),
25.     1      (IP(1) ,L(191)),(IOS(1) ,L(225)),(ICP(1) ,L(271))
26.     C
27.     CALL READSCH
28.     C
29.     ISDSCH= IP(LINE)
30.     IF(ISET.EQ.1)ISDSCH= IOS(LINE)
31.     RETURN
32.     END

```

IFIN

Appendix C
LISTING OF SL1 PROGRAM - SINGLE LOOP

```

1      PROGRAM GENERAL MODEL
2      C SET VERSION NUMBER
3          DATA IVERSION/080278/
4      C 12.8.76 SYSTEM COMMON ENLARGED
5      C 25.8.76 DISCRETES INCLUDED
6      C 5.10.76 FRAME TIME VARIABLES TIED UP
7      C 21.12.76 TOTM AND TOTF SEPARATED AND SOURCE CLEANED UP
8      C N = 2.78 SHORT NAME LIST SPECIFIED TO CUT STORAGE
9
10     CONTROL
11     MODE = REALT
12     ENDC
13     INITIAL
14
15     C DIMENSION,COMMON,DATA DECLARATIONS
16     C
17     COMMON/SYSTEM/A(1000),L(400)
18     DIMENSION RICVALS(20)
19     DATA NIPASS/1/
20     EQUIVALENCE(RICVALS(1),A(191))
21
22     C COMMUNICATION BETWEEN 'INITIAL' AND SYSTEM COMMON
23     C
24     EQUIVALENCE(VKNIC ,A(21)),(VKEIC ,A(212)),(VKDIC ,A(213)),...
25     (VIC ,A(195)),(VIC ,A(196)),(MIC ,A(197)),...
26     (PDIC ,A(220)),(QDIC ,A(221)),(RDIC ,A(222)),...
27     (PHVIC ,A(214)),(THETADIC,A(215)),(PSIDIC ,A(204)),...
28     (FRAMET1 ,A( 92)),...
29     (DEGTOR ,A(142)),(DELTA ,A( 91))
30     EQUIVALENCE(NCPASS ,L( 2)),(NIPASS ,L( 3)),(ILSFLG ,L( 4)),...
31     (ISMR ,L( 5))
32
33     C NEAL TIME PARAMETERS
34     DATA FRAMET1/50.0/
35     DATA TIMLEFT1/0.0/
36     DATA DELT1/0.050/
37     C NUMBER OF IC VALUES
38     DATA NVALS/14/
39
40     C SET UP COMMUNICATION, TO ENABLE VARIABLES IN SL1 LABELLED
41     C COMMON TO BE ACCESSED
42     C
43     DIMENSION NAME(2)
44     DATA NAME/'MODEL'/
45     NAMELIST CINT1,IALG1,JALG1,IMX,IMY,ITP,IVERSION,MODE,...
46     NS1,NVALS,SM,SY,MM,SK1L,SYIC,SMIC,T,TIMLEFT1
47     LAUNCHCALL PV200(NAME)
48     GO TO LABO
49     LABO:INPUT(101)
50     LABO:CONTINUE
51     CALL SYSCOM
52     CALL USERCOM
53
54     C CHECK ACCESS 'ON' AND INITIALISE ADA
55     CALL INTLAD
56     C READ IC CONDITIONS FROM MASTER FILE(F:1), PLACE IN SYSTEM COMMON
57     CALL RDICFILE(NVALS,RICVALS)
58     ILSFLG = RICVALS(10)
59     ISMR = RICVALS(11)
60     C *****
61     C * INPUT RETAINED CHANGES *
62     C *****
63     CALL PV300
64     C INTERPRETER
65     C *****
66     ITP = 1
67     C CALL PV100 IF DESK SWITCH 1 ON
68     IF(1SDSCH(1,1).EQ.1)CALL PV100
69
70     C STEP SIZE (FOR REAL TIME, = FRAMET1/1000.0)
71     C SL1 CALCULATES INTEGRATION STEP FROM CINT/NS.
72     C FOR USER ACCESS, GET CINT FROM DELT
73     CINT1 = DELT1
74     C INITIALISE SYSTEM FUNCTIONS.
75     CALL SINIT
76     C INTERPRETER

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77 C *****
78 C ITP = 2
79 C CALL PV100 IF DESK SWITCH 1 ON
80 C IF(IISDCR(1,1).EQ.1)CALL PV100
81 C
82 C SET UP INITIAL VALUES FOR INTEGRATIONS
83 C
84 C VVKNIC = VKNIC
85 C VVKEIC = VKEIC
86 C VVNDIC = VNDIC
87 C BVIC = VIC
88 C BYIC = YIC
89 C BVIC = VIC
90 C PPIC = PDIC+DEGTOR
91 C QQIC = QDIC+DLGTOR
92 C RRIC = RDIC+DLGTOR
93 C PPHIC = PHDIC+DEGTOR
94 C TTHIC = THETADIC+DEGTOR
95 C PPSIC = PSDIC+DEGTOR
96 C
97 C FOR CONTROL OF 'POST-INTEGRATION' CALCULATIONS,SET UP VALUE OF NIPASS TO
98 C SUIT INTEGRATION ALGORITHM (ALGOR.DEFAULT IS NIPASS=1
99 C IF(IALG1.EQ.4)NIPASS = 2
100 C IF(IALG1.EQ.5)NIPASS = 4
101 C TO ENSURE THAT SUCH 'POST-INTEGRATION' ROUTINES ARE CALLED DURING THE
102 C INITIALISATION PASS THROUGH 'Z0001'
103 C NCPASS=4
104 C
105 C INTERPRETER
106 C *****
107 C ITP = 3
108 C CALL PV100 IF DESK SWITCH 1 ON
109 C IF(IISDCR(1,1).EQ.1)CALL PV100
110 C
111 C INIT = 0
112 C INIT2:CONTINUE
113 C INIT = INIT + 1
114 C END

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```

115 C INITIALISE TWICE SO THAT 'DDYN' ETC SET UP CORRECTLY
116 C IF(INIT.EQ.1) GO TO INIT2
117 C
118 C INTERPRETER
119 C *****
120 C ITP = 4
121 C CALL PV100 IF DESK SWITCH 1 ON
122 C IF(IISDCR(1,1).EQ.1)CALL PV100
123 C
124 C START CLOCK FOR REAL TIME
125 C IF(MODE) CALL STARTC
126 C DYNAMIC
127 C
128 C ***** DYNAMIC *****
129 C
130 C IF(MODE) CALL EXITS
131 C DERIVATIVE LOOP1
132 C
133 C ***** DERIVATIVE *****
134 C
135 C
136 C *****
137 C *
138 C * SYSTEM FUNCTIONS *
139 C *
140 C *****
141 C COMMON STATEMENT TO ALLOW CONTROL PARAMETER 'MODE'
142 C TO BE ACCESSED BY THE DERIVATIVE SECTION
143 C COMMON/29980/MODE
144 C DECLARE LOGICAL MODE
145 C INTEGRATION CONTROL STATEMENTS
146 C VARIABLE T = 0.0
147 C INTERVAL CINT1 = 0.05
148 C NSTEPS NS1 = 1
149 C ALGORITHM IALG1 = 5 , JALG1 = 5
150 C NTIM1,PHAMET,IFLAG1,TIMLEFT1,1.0,1)
151 C PROCEDURAL
152 C 12-R-76 SYSTEM COMMON ENLARGED

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```

153      COMMON/SYSTEM/A(1000),L(400)
154      C
155      C      ** INPUT VARIABLES **
156      C
157      EQUIVALENCE (PHIDT ,A( 29)),(THETDT ,A( 30)),(PSIDT,A( 31)),...
158      (PDDT ,A( 45)),(I00DT ,A( 46)),(RDDT ,A( 47)),...
159      (VKNDDT ,A(238)),(VKEDDT ,A(239)),(VKDDDT,A(240)),...
160      (XIC ,A(155)),(XDDTH ,A(158)),(DELTA,A( 91)),...
161      (XIMX ,A(159)),(XINY ,A(160))
162      C
163      EQUIVALENCE (NCPASS ,L( 2)),(NIPASS ,L( 3))
164      C
165      C      ** OUTPUT VARIABLES **
166      C
167      EQUIVALENCE (PHIN ,A( 7)),(THETAR ,A( 5)),(PSIR ,A( 3)),...
168      (IP ,A( 26)),(I0 ,A( 27)),(R ,A( 28)),...
169      (VKN ,A( 52)),(VKE ,A( 53)),(VKD ,A( 54)),...
170      (X ,A(149)),(Y ,A(150)),(M ,A(151)),...
171      (TIME ,A( 96))
172      END
173      C
174      C      *****
175      C      *PRE-INTEGRAL CALLS*
176      C      *****
177      C
178      C
179      C READ AND WRITE DISCRETE LINES
180      CALL DSCR1
181      C
182      CALL SCOUNT
183      C
184      C PROCEDURAL
185      DATA IFIRST,/ /
186      IF (IFIRST.NE.1) GO TO NOTF
187      C INSERT CALLS HERE FOR ROUTINES TO BE EXECUTED AFTER ADC BUT BEFORE INTEG
188      C -RATION ,AND WHICH ARE NOT PART OF EVALUATION LOOP FOR DERIVATIVES.
189      C ONLY EXECUTE THESE ROUTINES ONCE PER FRAME
190      C 1) PRE DERIVATIVE S/R CALLS
191      C
192      CALL CONTRLS
193      C CALCULATE WIND
194      CALL SWIND
195      C
196      C RESET FLAG
197      IFIRST = 0
198      NOTF:CONTINUE
199      END
200      C
201      PROCEDURAL( = ADC(1))
202      END
203      C
204      C      *****
205      C      * ANGULAR MOTION *
206      C      *****
207      C
208      C
209      C
210      C ATTITUDE ANGLES
211      PPSI = INTEG(PPSIDT,PPSIC)
212      THET = INTEG(THETDT,THETIC)
213      PPHI = INTEG(PPHIDT,PPHIC)
214      C
215      PROCEDURAL(=PPSI,THET,PPHI)
216      C EQUATE VARIABLES
217      PSIR = PPSI
218      THETAR = THET
219      PHIR = PPHI
220      C CALCULATE DIRECTION COSINES
221      C
222      CALL SDCOS
223      C
224      END
225      C
226      PP = INTEG(PPDDT,PPIC)

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227      QQ = INTEG(QQDOT,QQIC)
228      RR = INTEG(RRDOT,RRIC)
229
230      C      PROCEDURAL(PPSIDT,TTHDT,PPHIDT,PP,QQ,RR)
231      C      EQUATE VARIABLES
232          P = PP
233          Q = QQ
234          R = RR
235      C      CALCULATE ATTITUDE RATES
236          CALL SEULER
237          PPSIDT = PSIDT
238          TTHDT = THEYDT
239          PPHIDT = PHIDT
240      END
241
242      C
243      C      *
244      C      *      LINEAR MOTION      *
245      C      *
246      C      *
247      C
248      C      VELOCITIES
249          VVKN = INTEG(VVKNDOT,VVKNIC)
250          VVKE = INTEG(VVKEDOT,VVKEIC)
251          VVKD = INTEG(VVKDDOT,VVKDIC)
252
253      C      PROCEDURAL(VVKN,VVKE,VVKD)
254      C      EQUATE VARIABLES
255          VKN = VVKN
256          VKE = VVKE
257          VKD = VVKD
258      C      CALCULATE BODY AXES VELOCITIES
259          CALL SYVELOCI
260      C      CALCULATE ALPHA AND BETA AND ASSOCIATED SINES/COSINES
261          CALL SALFBET(DELTA)
262      END
263      PROCEDURAL(HHDDOT,SYDDOT)
264      C

```



```

265      C      EQUATE VARIABLES
266          HHDDOT = -VKD
267          SYDDOT = VKE
268          SXDDOT = XDOTM
269      END
270
271      C      CALCULATE POSITIONS
272          SX = MODINT(SXDDOT,SXIC,1.0,IMX,T)
273          SY = MODINT(SYDDOT,SYIC,1.0,IMY,T)
274          HM = INTEG(HHDDOT,SHIC)
275
276      C      PROCEDURAL
277      C      USERS ROUTINES
278      C      CALCULATE TOTAL FORCES IN BODY AXES
279      C
280          CALL TOTF
281      C
282      END
283
284      C      PROCEDURAL(PPDOT,HHDDOT,RRDOT = PP,QQ,RR)
285      C      USER'S ROUTINE TO CALCULATE MOMENTS
286          CALL TOTM
287
288      C      CALCULATE ANGULAR ACCELERATIONS
289          CALL SACCROT
290      C      EQUATE VARIABLES
291          PPDOT = PDDOT
292          QQDOT = QDDOT
293          RRDOT = RDDOT
294      END
295
296      C
297      C      PROCEDURAL(VVKNDOT,VVKEDOT,VVKDDOT)
298      C      CALCULATE LINEAR ACCELERATIONS
299          CALL SACCLIN
300      C      EQUATE VARIABLES
301          VVKNDDOT = VKNDDOT
302          VVKEDDOT = VKEDDOT

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303          VKDDT = VKDDT
304      END
305      PROCEDURAL( = SX,SY,MH)
306      C          *****
307      C          *
308      C          *POST-INTEGRAL CALLS*
309      C          *
310      C          *****
311      C      *NCPASS=NCPASS*
312      C      NCPASS = COUNT OF NUMBER OF PASSES EXECUTED SO FAR IN ONE INTEGRATION STEP
313      C      NIPASS = CONSTANT,SET UP IN INITIAL,FOR NUMBER OF PASSES USED BY
314      C      INTEGRATION ROUTINE.
315      C      IF(NCPASS.LT.NIPASS)GO TO NKPASS
316      C      INSERT HERE CALLS TO 'POST-INTEGRATION' ROUTINES,TO BE EXECUTED ONLY
317      C      ONCE PER STEP.
318      C
319      C      FIRST PICK UP TIME
320      C      TIME = T
321      C      EQUATE VARIABLES
322      C      X = SX
323      C      Y = SY
324      C      H = MH
325      C      CALCULATE BODY AXES ACCELERATIONS FOR MOTION ('OUTPUT' ONLY)
326      C      CALL SACC800
327      C
328      C      CALCULATE INSTRUMENT READINGS ('OUTPUT' ONLY)
329      C      CALCULATE ILB ('OUTPUT' ONLY)
330      C      CALL SIBL
331      C
332      C      LOGIC AND POSITION FOR VFA CONTROL ('OUTPUT' ONLY)
333      C      CALL STV
334      C      EQUATE VARIABLES
335      C      SXIC = XIC
336      C      IXK = XIK
337      C      IXY = XIK
338      C      SXDOTM = XDOTM
339      C      CALCULATE EAS,MACH,DYNAMIC PRESSURE ETC.
340      C      CALL SVELOC2

341      C      CALCULATE FLIGHT PATH ANGLE
342      C      CALL SPATH
343      C
344      C      3) POST DERIVATIVE S/R CALLS
345      C
346      C      S/R 'OUTSR' HANDLES OUTPUT FUNCTIONS
347      C
348      C      CALL OUTSR
349      C
350      C      CALL SDAC
351      C
352      C      SET 'FIRST TIME' FLAG ON,READY FOR NEXT TIME ROUND
353      C      IFIRST = 1
354      C      SKPASS = CONTINUE
355      C      END
356      C
357      C      PROCEDURAL(DAC( 1),DAC( 2),DAC( 3),DAC( 4),DAC( 5),...
358      C      DAC( 6),DAC( 7),DAC( 8),DAC( 9),DAC(10),...
359      C      DAC(11),DAC(12),DAC(13),DAC(14),DAC(15),...
360      C      DAC(16),DAC(17),DAC(18),DAC(19),DAC(20),...
361      C      DAC(21),DAC(22),DAC(23),DAC(24),DAC(25),...
362      C      DAC(26),DAC(27),DAC(28),DAC(29),DAC(30),...
363      C      DAC(31),DAC(32),DAC(33),DAC(34),DAC(35),...
364      C      DAC(36),DAC(37),DAC(38),DAC(39),DAC(40),...
365      C      DAC(41),DAC(42),DAC(43),DAC(44),DAC(45),...
366      C      DAC(46),DAC(47),DAC(48)=)
367      C      END
368      C
369      C      PROCESS AUTOMATIC HOLD
370      C      CALL PV700
371      C      IF(MODE) CALL TERMINATE('AIRCRAFT')
372      C      END
373      C      END
374      C      TERMINAL
375      C      END
376      C      END

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Appendix D
INDEX TO SYSTEM COMMON, REAL VARIABLES

D.1 Numeric order

SYSTEM COMMON - REAL VARIABLES 15.3.78
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NUMERIC ORDER						
ELEMENT NO.	FONTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
1	RXMASW	1/XMASS			SINIT	SACCLIN
2	XMASS	AIRCRAFT MASS		SLUG	SINIT	SINIT
3	PSIR	HEADING ANGLE		RADIANS	DERIVATIVE	SDCOS
4	PSID	HEADING ANGLE		DEGREES	SUCOS	
5	THETAR	PITCH ATTITUDE		RADIANS	DERIVATIVE	SDCOS
6	THETAD	PITCH ATTITUDE		DEGREES	SDCOS	
7	PHIR	BANK ANGLE		RADIANS	DERIVATIVE	SDCOS
8	PHID	BANK ANGLE		DEGREES	SUCOS	
9	SPSI	SIN(PSIN)			SDCOS	STV SDCOS
10	CPSI	COS(PSIN)			SDCOS	STV SDCOS
11	STHETA	SIN(THETAR)			SDCOS	STV SDCOS
12	CTHETA	COS(THETAR)			SDCOS	STV SDCOS

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NUMERIC ORDER						
ELEMENT NO.	FONTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
13	SPHI	SIN(PHIN)			SDCOS	SEULER SDCOS
14	CPHI	COS(PHIN)			SDCOS	SEULER SDCOS
15	SECTHT	SEC(THETAR)			SDCOS	SEULER SDCOS
16	TANTHT	TAN(THETAR)			SDCOS	SEULER
17	S11	DIRECTION COSINE			SUCOS	SVELOC1 SACCLIN
18	S12	DIRECTION COSINE			SDCOS	SVELOC1 SACCLIN
19	S13	DIRECTION COSINE			SDCOS	SVELOC1 SACCLIN SACCBOD
20	S21	DIRECTION COSINE			SDCOS	SVELOC1 SACCLIN
21	S22	DIRECTION COSINE			SDCOS	SVELOC1 SACCLIN
22	S23	DIRECTION COSINE			SDCOS	SVELOC1

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ELEMENT NO.	FONTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN	
						SACCLIN SACCBOD	
23	631		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN	
24	632		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN	
25	633		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN SACCBOD	
26	P		ANG VEL,ROLL,BODY AXES	RADS/SEC	DER'TIVE	SEULER SACCR0T SACCBOD	
27	U		ANG VEL,PITCH,BODY AXES	RADS/SEC	DER'TIVE	SEULER SACCR0T SACCBOD	
28	R		ANG VEL,YAW,BODY AXES	RADS/SEC	DER'TIVE	SEULER SACCR0T SACCBOD	
29	PHIDT		ATTITUDE RATE,BANK	RAD/SEC	SEULER	DER'TIVE	
30	THETDT		ATTITUDE RATE,PITCH	RAD/SEC	SEULER	STV	

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ELEMENT NO.	FONTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN	
						DER'TIVE	
31	PSIDT		ATTITUDE RATE,HEADING	RAD/SEC	SEULER	STV DER'TIVE	
32	PD		ANG VEL,ROLL,BODY AXES	DEGS/SEC	SEULER		
33	UD		ANG VEL,PITCH,BODY AXES	DEGS/SEC	SEULER		
34	UD		ANG VEL,YAW,BODY AXES	DEGS/SEC	SEULER		
35	C11		INERTIA COEFFICIENT		SINIT	SACCR0T	
36	C12		INERTIA COEFFICIENT		SINIT	SACCR0T	
37	C13		INERTIA COEFFICIENT		SINIT	SACCR0T	
38	C14		INERTIA COEFFICIENT		SINIT	SACCR0T	
39	C15		INERTIA COEFFICIENT		SINIT	SACCR0T SINIT	
40	C16		INERTIA COEFFICIENT		SINIT	SACCR0T	
41	C17		INERTIA COEFFICIENT		SINIT	SACCR0T	
42	C18		INERTIA COEFFICIENT		SINIT	SACCR0T	
43	C19		INERTIA COEFFICIENT		SINIT	SACCR0T	

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ROYAL AIRCRAFT ESTABLISHMENT FARNBOROUGH (ENGLAND)

F/G 9/2

SESAME-A SYSTEM OF EQUATIONS FOR THE SIMULATION OF AIRCRAFT IN --ETC(U)

JAN 79 B N TOMLINSON

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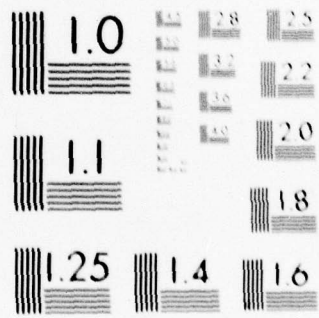
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MICROCOPY RESOLUTION TEST CHART
 NATIONAL BUREAU OF STANDARDS-1963-A

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NUMERIC ORDER							
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN	
44	CI10		INERTIA COEFFICIENT		SINIT	SACCR0T	
45	PDOT		ANGULAR ACCN. IN BODY AXES	RADS/SEC2	SACCR0T	SACCB0D	
46	QDOT		ANGULAR ACCN. IN BODY AXES	RADS/SEC2	SACCR0T	SACCB0D	
47	RDOT		ANGULAR ACCN. IN BODY AXES	RADS/SEC2	SACCR0T	SACCB0D	
48	XIX		MOMENT OF INERTIA,ROLL	SLUG FT2	USER	SINIT	
49	XIY		MOMENT OF INERTIA,PITCH	SLUG FT2	USER	SINIT	
50	XIZ		MOMENT OF INERTIA,YAW	SLUG FT2	USER	SINIT	
51	XIZX		MOMENT OF INERTIA,PRODUCT	SLUG FT2	USER	SINIT	
52	VKN		VELOCITY REL TO GROUND,NORTH	FT/SEC	DER'ITIVE	SVELOC1 SPATH STV	
53	VKE		VELOCITY REL TO GROUND,EAST	FT/SEC	DER'ITIVE	SVELOC1 SPATH STV	
54	VKD		VELOCITY REL TO GROUND,DOWN	FT/SEC	DER'ITIVE	SVELOC1 SPATH STV	

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NUMERIC ORDER							
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN	
55	VHN		VELOCITY OF WIND,NORTH	FT/SEC	SWIND	SVELOC1	
56	VHE		VELOCITY OF WIND,EAST	FT/SEC	SWIND	SVELOC1	
57	VHD		VELOCITY OF WIND,DOWN	FT/SEC	SWIND	SVELOC1	
58	UB		VEL COMP REL TO AIR,BODY AXES	FT/SEC	SVELOC1	SVELOC2 SALFBET	
59	VB		VEL COMP REL TO AIR,BODY AXES	FT/SEC	SVELOC1	SVELOC2 SALFBET	
60	WB		VEL COMP REL TO AIR,BODY AXES	FT/SEC	SVELOC1	SVELOC2 SALFBET	
61	GAMMA		FLIGHT PATH ANGLE,CLIMB	RADIANS	SPATH	SPATH	
62	GAMMAU		FLIGHT PATH ANGLE,CLIMB	DEGREES	SPATH		
63	PSIKR		FLIGHT PATH ANGLE,TRACK	RADIANS	SPATH	SPATH	
64	PSIKD		FLIGHT PATH ANGLE,TRACK	DEGREES	SPATH		
65	VK		VELOCITY RELATIVE TO GROUND	FT/SEC	SPATH	SINIT SPATH	
66	VKKT		VELOCITY RELATIVE TO GROUND	KNOTS	SPATH		

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NUMERIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
67	VT		TOTAL AIR SPEED	FT/SEC	SVELOC2	SINIT SVELOC2
68	VTKT		TOTAL AIR SPEED	KNOTS	SVELOC2	
69	VEAS		EQUIVALENT AIR SPEED	FT/SEC	SVELOC2	SVELOC2
70	VEAKT		EQUIVALENT AIR SPEED	KNOTS	SVELOC2	
71	ROOTSIG		SQRT(DENSITY RATIO)		SVELOC2	SINIT SVELOC2
72	RHO		AIR DENSITY	SLUG/FT3	SVELOC2	SVELOC2
73	SPSND		SPEED OF SOUND	FT/SEC	SVELOC2	SVELOC2
74						
75	RMACH		MACH NUMBER		SVELOC2	SVELOC2
76	TEMPBL		AIR TEMP AT SL(STANDARD DAY)	DEG. K	SINIT	SVELOC2 SINIT
77	PHESL		AMBIENT PRESSURE AT SEA LEVEL	LB/IN 2	SINIT	SVELOC2 SINIT
78	DENR		DENSITY RATIO		SINIT	SVELOC2

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NUMERIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
						SINIT
79	RHOSL		DENSITY AT SEA LEVEL	SLUG /FT3	SINIT	SVELOC2 SINIT
80	SPSL		SPEED OF SOUND AT SEA LEVEL	FT/SEC	SINIT	SVELOC2 SINIT
81	TEMPR		ATMOSPHERIC TEMP RATIO		SATMOS	SVELOC2 SINIT
82	PHESR		ATMOSPHERIC PRESSURE RATIO		SATMOS	SVELOC2 SINIT
83	DRATIO		ADIABATIC DENSITY RATIO		SVELOC2	SVELOC2
84	SPSNDH		SPEED OF SOUND RATIO		SATMOS	SVELOC2 SINIT
85	ARATIO		ADIABATIC SPEED OF SOUND RATIO		SVELOC2	SVELOC2
86	PALPHA		FREE STREAM STATIC PRESSURE	LB/IN 2	SVELOC2	
87	PRATIO		ADIABATIC STATIC/TOTAL PRESS		SVELOC2	
88	TALPHA		FREE STREAM STATIC TEMPERATURE	DEG. K	SVELOC2	
89	TRATIO		ADIABATIC STATIC/TOTAL TEMP		SVELOC2	SVELOC2

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NUMERIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
90						
91	DELT1		INTEG. STEP LENGTH NO. 1	SECS	USER	INITIAL
92	FRAMET1		FRAME TIME, LOOP 1	MSEC	USER	INITIAL SWIND
93						
94	TIME		TIME	SEC	DERIVATIVE	
95	DELT2		INTEG. STEP LENGTH NO. 2	SECS	USER	INITIAL
96	FRAMET2		FRAME TIME, LOOP 2	MSEC	USER	INITIAL
97						
98	ZCG		Z C.G. LOCATION		USER	SINIT
99	XCGMEF		X LOCATION OF REF PT		USER	SINIT
100	ZCGMEF		Z LOCATION OF REF PT		USER	SINIT
101	DXCG		DIST OF C.G. AHEAD OF M.H.C.		SINIT	STV
102	DZCG		DIST OF C.G. BELOW M.H.C.		SINIT	STV
103	SPAN		WING SPAN	FT	USER	SVELOC2

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NUMERIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
						SINIT
104	XLTAIL		TAIL ARM FROM M.H.C.	FT	USER	
105	BTAIL		TAIL PLANE AREA	FT ²	USER	
106	SWREF		WING REFERENCE AREA	FT ²	USER	SVELOC2 SINIT
107	CREF		REFERENCE CHORD	FT	USER	SVELOC2 STV
108	S02		SWREF*SPAN*SPAN	FT ⁴	SINIT	SVELOC2
109	XP		X LOC OF PILOT REL TO REFCG	FT	USER	STV
110	ZP		Z LOC OF PILOT REL TO REFCG	FT	USER	STV
111	ALFAR		ANGLE OF ATTACK	RADIANS	SALFBET	SALFBET
112	ALFAD		ANGLE OF ATTACK	DEGREES	SALFBET	
113	BETAR		ANGLE OF WIDESLIP	RADIANS	SALFBET	SALFBET
114	BETAD		ANGLE OF WIDESLIP	DEGREES	SALFBET	
115						
116	SALFA		SINE OF ALPHA		SALFBET	

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
117	CALFA		COS OF ALPHA		SALFBET	
118	SBETA		SINE OF BETA		SALFBET	
119	CBETA		COS OF BETA		SALFBET	
120	ALFADOT		RATE OF ANGLE OF ATTACK	RADS/SEC	SALFBET	
121	BETADOT		RATE OF ANGLE OF SIDESLIP	RADS/SEC	SALFBET	
122						
123						
124	MLFRMOV		0.5*RH0*VT		SVELOC2	SVELOC2
125	QDYN		DYNAMIC PRESSURE	LB/FT2	SVELOC2	SVELOC2
126	QDYNB		QDYN*SBREF	LB	SVELOC2	SVELOC2
127	QSCREF		QDYN*CHEF	LB=FT	SVELOC2	
128	QSSPAN		QDYN*SPAN	LB=FT	SVELOC2	
129	QSB2IV		MLFRMOV*SB2		SVELOC2	
130						

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
131	XLLTOT		TOTAL MOMENT, ROLL, BODY AXES	LB=FT	USER	SACCR0T
132	XMMTOT		TOTAL MOMENT, PITCH, BODY AXES	LB=FT	USER	SACCR0T
133	XNNTOT		TOTAL MOMENT, YAW, BODY AXES	LB=FT	USER	SACCR0T
134	FTX		TOTAL FORCE COMP. IN BODY AXES	LB	USER	SACCLIN SACCB0D
135	FTY		TOTAL FORCE COMP. IN BODY AXES	LB	USER	SACCLIN SACCB0D
136	FTZ		TOTAL FORCE COMP. IN BODY AXES	LB	USER	SACCLIN SACCB0D
137	FTN		TOTAL FORCE COMP IN EARTH AXES	LB	SACCLIN	SACCLIN
138	FTE		TOTAL FORCE COMP IN EARTH AXES	LB	SACCLIN	SACCLIN
139	FTD		TOTAL FORCE COMP IN EARTH AXES	LB	SACCLIN	SACCLIN
140						
141	NAOT00		CONVERSION RADIANS TO DEGREES	CONSTANT	SINIT	SDC0S SPATH SALFBET SEULER

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NUMERIC ORDER	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
						SILS SINIT
142	DEGTM		CONVERSION DEGREES TO RADIANS	CONSTANT	SINIT	SILS SINIT
143	FPSTKT		CONVERSION FT/SEC TO KNOTS	CONSTANT	SINIT	SVELOC2 SPATH
144	K4ZFPS		CONVERSION KNOTS TO FT/SEC	CONSTANT	SINIT	SWIND STV SINIT
145	G		ACCELERATION DUE TO GRAVITY	CONSTANT	SINIT	SACCLIN SINIT
146	RG		RECIPROCAL OF G		SINIT	SACCBOD
147						
148						
149	X		X POSITION OF C.G.	FT	DERIVATIVE	STV SILS
150	Y		Y POSITION OF C.G.	FT	DERIVATIVE	STV SILS
151	H		HEIGHT OF CG	FT	DERIVATIVE	SATMOS

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NUMERIC ORDER	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
						SVELOC2 STV SILS SWIND
152	XTV		X POSITION FOR TV	FT	STV	STV
153	YTV		Y POSITION FOR TV	FT	STV	STV
154	HTV		HEIGHT FOR TV	FT	STV	STV
155	XDTV		X VELOCITY FOR TV	FT/SEC	STV	
156	YDTV		Y VELOCITY FOR TV	FT/SEC	STV	
157	HDTV		H VELOCITY FOR TV	FT/SEC	STV	
158	XDOTM		RATE OF CHANGE OF A/C'S X POSN	FT/SEC	STV	DERIVATIVE STV
159	XIMX		CONTROL VAR FOR X INTEGRATION		STV	DERIVATIVE
160	XIMY		CONTROL VAR FOR Y INTEGRATION		STV	DERIVATIVE
161	BXPL		NEAR BELT JOIN POS AND LIMIT	FT	STV	STV
162	BXMIN		NEAR BELT JOIN NEG AND LIMIT	FT	STV	STV
163	BXPLUS		CYCLE LIMIT	FT	STV	STV

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
169	SKRINUS		CYCLE LIMIT	FT	STV	STV
168	SYPL		LIMIT FOR SIDEWAYS(POSITIVE)	FT	STV	STV
168	SYMIN		LIMIT FOR SIDEWAYS(NEGATIVE)	FT	STV	STV
167	HTVLIM		CEILING AND HEIGHT LIMIT	FT	STV	STV
166	XOTRX		BLEW RATE	FT/SEC	STV	STV
165	VBHIPAT		SHIP SPEED	KT	USER	STV
170						
171	ESB		GLIDE SLOPE ERROR	DEGREES	SILS	
172	ELOC		LOCALISER ERROR	DEGREES	SILS	
173	MSLOPE		HT OF ILS BEAM AT GIVEN RANGE	FT	SILS	SINIT SILS
174	MUS		RANGE FROM G/S TRANSMITTER	FT	SILS	SILS
175	MLOC		RANGE FROM LRC TRANSMITTER	FT	SILS	SILS
176	MKINK		RANGE FROM BEAM KINK	FT	SILS	SILS
177	XOS		GLIDE SLOPE ORIGIN	FT	SILS	SILS

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
178	XL0C		LOCALISER ORIGIN (X)	FT	SILS	SILS
179	YL0C		LOCALISER ORIGIN (Y)	FT	SILS	SILS
180	ESB		GLIDE SLOPE SENSITIVITY	DEGREES	SILS	SILS
181	EL0C		LOCALISER SENSITIVITY	DEGREES	SILS	SILS
182	MKINK		HEIGHT OF BEAM KINK	FT	SILS	SILS
183	MSLOPE		SLOPE OF LOWER BEAM	DEGREES	SILS	SILS
184	USLOPE		SLOPE OF UPPER BEAM	DEGREES	SILS	SILS
185	MKINK		POSITION OF BEAM KINK	FT	SILS	SILS
186	CIL01		RADTOD/SOS		SILS	SILS
187	CIL02		RADTOD/SLOC		SILS	SILS
188	CIL03		TAN(SLOPE)		SILS	SILS
189	CIL04		TAN(SLOPE)*CIL03		SILS	SILS
190						
191	BETADIC		INITIAL VALUE OF BETA	DEGREES	ICP/LE	SINIT

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
192	ALFADIC		INITIAL VALUE OF ALFA	DEGREES	ICFILE	SINIT
193	GAMDIC		INITIAL VALUE OF GAMMA	DEGREES	ICFILE	SINIT
194	VKTIC		INITIAL A/H SPEED	KNOTS	ICFILE	SINIT SWIND
195	XIC		INITIAL POSITION	FT	ICFILE	SINIT INITIAL STV
196	YIC		INITIAL POSITION	FT	ICFILE	INITIAL
197	WIC		INITIAL POSITION	FT	ICFILE	SINIT SWIND INITIAL
198	W		AIRCRAFT WEIGHT	LB	ICFILE	SINIT SACCOBO
199	XCG		X C.G. LOCATION IN AIRCRAFT		ICFILE	SINIT
200	ATLDFLAG		ILSFLAG IN 'REAL' FORM		ICFILE	INITIAL
201	XIGNR		IGNR IN 'REAL' FORM		ICFILE	INITIAL
202	VWKT0		DATUM WIND SPEED	KNOTS	ICFILE	SINIT

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
203	P8IND		DATUM WIND DIRECTION	DEGREES	ICFILE	SINIT
204	P8IOIC		INITIAL VALUE OF PSI	DEGREES	ICFILE	INITIAL SINIT
205	RIC15		SPARE			
206	RIC16		SPARE			
207	RIC17		SPARE			
208	RIC18		SPARE			
209	RIC19		SPARE			
210	RIC20		SPARE			
211	VKNIC		INIT GROUND SPEED COMP (NORTH)	FT/SEC	SINIT	INITIAL SINIT
212	VKEIC		INIT GROUND SPEED COMP (EAST)	FT/SEC	SINIT	INITIAL SINIT
213	VKDIC		INIT GROUND SPEED COMP (DOWN)	FT/SEC	SINIT	INITIAL SINIT
214	PHIDIC		INITIAL VALUE OF PHI	DEGREES	SINIT	INITIAL

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
216	THETADIC		INITIAL VALUE OF THETA	DEGREES	SINIT	INITIAL
216						
217	VN		COMP. OF TRUE AIR SPEED (NORTH)	FT/SEC	SVELOC1	SVELOC1
218	VE		COMP. OF TRUE AIR SPEED (EAST)	FT/SEC	SVELOC1	SVELOC1
219	VD		COMP. OF TRUE AIR SPEED (DOWN)	FT/SEC	SVELOC1	SVELOC1
220	PDIC		INITIAL ANGULAR RATE	RADS/SEC	SINIT	INITIAL
221	UDIC		INITIAL ANGULAR RATE	RADS/SEC	SINIT	INITIAL
222	HDIC		INITIAL ANGULAR RATE	RADS/SEC	SINIT	INITIAL
223	VNDLO		WIND VELOCITY (DOWN) AT HEIGHT	FT/SEC	SWIND	SWIND
224	CPB1W		COB (PB1W)		SINIT	SWIND SINIT
225	SPB1W		SIN (PB1W)		SINIT	SWIND SINIT
226	VHNLO		WIND VELOCITY (NORTH) AT HEIGHT	FT/SEC	SINIT	SWIND SINIT
227	VNELO		WIND VELOCITY (EAST) AT HEIGHT	FT/SEC	SINIT	SWIND

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
						SINIT
228	SWRFAC		SHEAR FACTOR		WSHEAR	SINIT SWIND
229	VHNL		MEAN WIND COMP AT HEIGHT (NTH)	FT/SEC	SWIND	SWIND
230	VHEL		MEAN WIND COMP AT HEIGHT (EAST)	FT/SEC	SWIND	SWIND
231	VHDL		MEAN WIND COMP AT HEIGHT (DOWN)	FT/SEC	SWIND	SWIND
232	UTURB		COMPONENT OF TURBULENCE	FT/SEC	SWIND	SWIND
233	VTURB		COMPONENT OF TURBULENCE	FT/SEC	SWIND	SWIND
234	WTURB		COMPONENT OF TURBULENCE	FT/SEC	SWIND	SWIND
235	USIG		RMS OF TURBULENCE	FT/SEC	USER	SWIND
236	VSIG		RMS OF TURBULENCE	FT/SEC	USER	SWIND
237	WSIG		RMS OF TURBULENCE	FT/SEC	USER	SWIND
238	VKNDOT		ACCELERATION IN EARTH AXES	FT/SEC ²	SACCLIN	DERIVATIVE
239	VKEDOT		ACCELERATION IN EARTH AXES	FT/SEC ²	SACCLIN	DERIVATIVE

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NUMERIC ORDER	ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
	241	AXCG		SPECIFIC ACCELERATION AT CG(X)	G	SACCB00	SACCB00
	242	AYCG		SPECIFIC ACCELERATION AT CG(Y)	G	SACCB00	SACCB00
	243	AZCG		SPECIFIC ACCELERATION AT CG(Z)	G	SACCB00	SACCB00
	244	AZCG1		Z ACCEL'N AT CG+REL. TO 1-0	G	SACCB00	
	245	AXACG		ABSOLUTE ACCELERATION AT CG(X)	G	SACCB00	
	246	AYACG		ABSOLUTE ACCELERATION AT CG(Y)	G	SACCB00	
	247	AZACG		ABSOLUTE ACCELERATION AT CG(Z)	G	SACCB00	
	248	AXP		SPECIFIC ACCEL'N AT PILOT (X)	G	SACCB00	
	249	AYP		SPECIFIC ACCEL'N AT PILOT (Y)	G	SACCB00	
	250	AZP		SPECIFIC ACCEL'N AT PILOT (Z)	G	SACCB00	SACCB00
	251	AZAP		ABSOLUTE ACCEL'N AT PILOT (Z)	G	SACCB00	
	252	AY1		ACCELERATION AT SLIP BALL	G	SACCB00	
	253	AZ2		ACCELERATION AT G METER	G	SACCB00	
	254	AX3		X ACCEL'N AT (X3,Y3,Z3)	G	SACCB00	

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NUMERIC ORDER	ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
	255	AY4		Y ACCEL'N AT (X4,Y4,Z4)	G	SACCB00	
	256	AZ5		Z ACCEL'N AT (X5,Y5,Z5)	G	SACCB00	
	257	X1		COORDINATES OF SLIP BALL (X1)	FT	USER	SACCB00
	258	Y1		COORDINATES OF SLIP BALL (Y1)	FT	USER	SACCB00
	259	Z1		COORDINATES OF SLIP BALL (Z1)	FT	USER	SACCB00
	260	X2		COORDINATES OF G METER (X2)	FT	USER	SACCB00
	261	Y2		COORDINATES OF G METER (Y2)	FT	USER	SACCB00
	262	Z2		COORDINATES OF G METER (Z2)	FT	USER	SACCB00
	263	X3		COORD. OF ACCELEROMETER (X3)	FT	USER	SACCB00
	264	Y3		COORD. OF ACCELEROMETER (Y3)	FT	USER	SACCB00
	265	Z3		COORD. OF ACCELEROMETER (Z3)	FT	USER	SACCB00
	266	X4		COORD. OF ACCELEROMETER (X4)	FT	USER	SACCB00
	267	Y4		COORD. OF ACCELEROMETER (Y4)	FT	USER	SACCB00
	268	Z4		COORD. OF ACCELEROMETER (Z4)	FT	USER	SACCB00

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
269	XS		COORD. OF ACCELEROMETER (AZ5)	FT	USER	SACCB00
270	YS		COORD. OF ACCELEROMETER (AZ5)	FT	USER	SACCB00
271	ZS		COORD. OF ACCELEROMETER (AZ5)	FT	USER	SACCB00
***** NOTE MISSING ELEMENT NUMBERS *****						
278	SFRACU		INTERMITTENCY FOR TURBULENCE		USER	SWIN0
279	BRDECAY		DECAY FACTOR FOR TURBULENCE		USER	SWIN0
280	APCO		X LOC OF PILOT REL TO CG		STV	STV SACCB00
281	ZPC0		Z LOC OF PILOT REL TO CG		STV	STV SACCB00
282	RAP		PILOT X RADIUS	FT	STV	STV
283	RMP		PILOT Y RADIUS	FT	STV	STV
284	XICF		EXTRA STONE FOR XIC	FT	STV	STV
***** NOTE MISSING ELEMENT NUMBERS *****						
301	AADC(1)		ARRAY OF SCALING FACTORS		USER	SADC

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
***** NOTE MISSING ELEMENT NUMBERS *****						
300	AADC(00)		ARRAY OF SCALING FACTORS		USER	SADC
300	TVCON(1,1)		ARRAY OF CONSTANTS FOR TV BELT		STV	STV
***** NOTE MISSING ELEMENT NUMBERS *****						
300	TVCON(1,3)		ARRAY OF CONSTANTS FOR TV BELT		STV	STV
***** NOTE MISSING ELEMENT NUMBERS *****						
001	YADC(1)		ARRAY OF UNSCALED INPUTS		SADC	USER
***** NOTE MISSING ELEMENT NUMBERS *****						
000	YADC(00)		ARRAY OF UNSCALED INPUTS		SADC	USER
***** NOTE MISSING ELEMENT NUMBERS *****						
001	ADAC(1)		ARRAY OF SCALING FACTORS		USER	SADC
***** NOTE MISSING ELEMENT NUMBERS *****						
000	ADAC(00)		ARRAY OF SCALING FACTORS		USER	SADC

D.2 Alphabetical order

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
301	AADC(1)		ARRAY OF SCALING FACTORS		USER	SADC
300	AADC(00)		ARRAY OF SCALING FACTORS		USER	SADC
501	ADAC(1)		ARRAY OF SCALING FACTORS		USER	SDAC
500	ADAC(00)		ARRAY OF SCALING FACTORS		USER	SDAC
112	ALFAD		ANGLE OF ATTACK	DEGREES	SALFBET	
192	ALFADIC		INITIAL VALUE OF ALFA	DEGREES	ICFILE	SINIT
120	ALFADOT		RATE OF ANGLE OF ATTACK	RADS/SEC	SALFBET	
111	ALFAN		ANGLE OF ATTACK	RADIANS	SALFBET	SALFBET
85	ARATIO		ADIABATIC SPEED OF SOUND RATIO		SVELOC2	SVELOC2
250	AX3		X ACCEL'N AT (X3,Y3,Z3)	G	SACCB00	
245	AXAC0		ABSOLUTE ACCELERATION AT C0(X)	G	SACCB00	
241	AXC0		SPECIFIC ACCELERATION AT C0(X)	G	SACCB00	SACCB00
248	AXP		SPECIFIC ACCEL'N AT PILOT (X)	G	SACCB00	
252	AY1		ACCELERATION AT SLIP WALL	G	SACCB00	

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
255	AY6		Y ACCEL'N AT (X6,Y6,Z6)	G	SACCB00	
290	AYAC0		ABSOLUTE ACCELERATION AT C0(Y)	G	SACCB00	
292	AYC0		SPECIFIC ACCELERATION AT C0(Y)	G	SACCB00	SACCB00
249	AYP		SPECIFIC ACCEL'N AT PILOT (Y)	G	SACCB00	
253	AZ2		ACCELERATION AT 0 FEET	G	SACCB00	
250	AZ5		Z ACCEL'N AT (X5,Y5,Z5)	G	SACCB00	
247	AZAC0		ABSOLUTE ACCELERATION AT C0(Z)	G	SACCB00	
251	AZAP		ABSOLUTE ACCEL'N AT PILOT (Z)	G	SACCB00	
243	AZC0		SPECIFIC ACCELERATION AT C0(Z)	G	SACCB00	SACCB00
240	AZC01		Z ACCEL'N AT C0(HEL. TO 1-0)	G	SACCB00	
250	AZP		SPECIFIC ACCEL'N AT PILOT (Z)	G	SACCB00	SACCB00
110	BETAD		ANGLE OF SIDESLIP	DEGREES	SALFBET	
191	BETADIC		INITIAL VALUE OF BETA	DEGREES	ICFILE	SINIT
121	BETADOT		RATE OF ANGLE OF SIDESLIP	RADS/SEC	SALFBET	

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
113	BETAR		ANGLE OF WIDEBLIP	RADIANS	SALFBET	SALFBET
103	BLOPE		SLOPE OF LOWER BEAM	DEGREES	SILB	SILB
117	CALFA		COS OF ALFA		SALFBET	
119	CBETA		COS OF BETA		SALFBET	
35	C11		INERTIA COEFFICIENT		SINIT	SACCR0T
36	C12		INERTIA COEFFICIENT		SINIT	SACCR0T
37	C13		INERTIA COEFFICIENT		SINIT	SACCR0T
38	C14		INERTIA COEFFICIENT		SINIT	SACCR0T
39	C15		INERTIA COEFFICIENT		SINIT	SACCR0T SINIT
40	C16		INERTIA COEFFICIENT		SINIT	SACCR0T
41	C17		INERTIA COEFFICIENT		SINIT	SACCR0T
42	C18		INERTIA COEFFICIENT		SINIT	SACCR0T
43	C19		INERTIA COEFFICIENT		SINIT	SACCR0T
44	C110		INERTIA COEFFICIENT		SINIT	SACCR0T

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
186	CILS1		RADT00/SG8		SILS	SILS
187	CILS2		RADT00/SL0L		SILS	SILS
188	CILS3		TANIBSLOPE1		SILS	SILS
189	CILS4		TANIBSLOPE1=CILS3		SILS	SILS
19	CPHI		COS(PH1)		SOCOS	SEULER SOCOS
10	CPBI		COS(PBI)		SUCOS	STV SDCOS
224	CPBIN		COS(PBIN)		SINIT	SWIND SINIT
107	CREF		REFERENCE CHORD	FT	USER	SVELOC2 STV
12	CTHETA		COS(THETA)		SOCOS	STV SDCOS
142	DEGTOR		CONVERSION DEGREES TO RADIANS	CONSTANT	SINIT	SILS SINIT
91	DELTA		INTEG. STEP LENGTH NO. 1	SECS	USER	INITIAL

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
95	DELTA2		INTEG. STEP LENGTH NO. 2	SECS	USER	INITIAL
78	DENR		DENSITY RATIO		SINIT	SVELOC2 SINIT
83	DRATIO		ADIABATIC DENSITY RATIO		SVELOC2	SVELOC2
101	DXCG		DIST OF C.G. AHEAD OF M.H.C.		SINIT	STV
102	DZCG		DIST OF C.G. BELOW M.H.C.		SINIT	STV
171	EUS		GLIDE WLOME ERROR	DEGREES	SILS	
172	ELOC		LOCALISEN ERROR	DEGREES	SILS	
143	FPBKT		CONVERSION FT/SEC TO KNOTS	CONSTANT	SINIT	SVELOC2 SPATH
92	FRAMET1		FRAME TIME, LOOP 1	MSEC	USER	INITIAL SWIND
96	FRAMET2		FRAME TIME, LOOP 2	MSEC	USER	INITIAL
139	FTD		TOTAL FORCE COMP IN EARTH AXES	LB	SACCLIN	SACCLIN
138	FTE		TOTAL FORCE COMP IN EARTH AXES	LB	SACCLIN	SACCLIN
137	FTN		TOTAL FORCE COMP IN EARTH AXES	LB	SACCLIN	SACCLIN

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
134	FTX		TOTAL FORCE COMP. IN BODY AXES	LB	USER	SACCLIN SACCBOD
135	FTY		TOTAL FORCE COMP. IN BODY AXES	LB	USER	SACCLIN SACCBOD
136	FTZ		TOTAL FORCE COMP. IN BODY AXES	LB	USER	SACCLIN SACCBOD
145	G		ACCELERATION DUE TO GRAVITY	CONSTANT	SINIT	SACCLIN SINIT
193	GAMDIC		INITIAL VALUE OF GAMMA	DEGREES	ICFILE	SINIT
62	GAMMAD		FLIGHT PATH ANGLE, CLIMB	DEGREES	SPATH	
61	GAMMAN		FLIGHT PATH ANGLE, CLIMB	RADIANS	SPATH	SPATH
151	H		HEIGHT OF CG	FT	DERIVATIVE	SATMOS SVELOC2 STV SILS SWIND
157	HDTV		H VELOCITY FOR TV	FT/SEC	STV	
197	HIC		INITIAL POSITION	FT	ICFILE	SINIT

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
						SWIND INITIAL
182	HKINK		HEIGHT OF BEAM KINK	FT	SIL8	SIL8
124	HLEFMOV		0.5*RH0*VI		SVELOC2	SVELOC2
173	HBLOPE		HT OF ILB BEAM AT GIVEN RANGE	FT	SIL8	SINIT SIL8
184	HTV		HEIGHT FOR TV	FT	STV	STV
167	HTVLIM		CEILING AND HEIGHT LIMIT	FT	STV	STV
26	P		ANG VEL, ROLL, BODY AXES	RADS/SEC	DERIVATIVE	SEULER SACCR0T SACCB00
86	PALPHA		FREE STREAM STATIC PRESSURE	LB/IN 2	SVELOC2	
32	PD		ANG VEL, ROLL, BODY AXES	DEGS/SEC	SEULER	
220	PDIC		INITIAL ANGULAR RATE	RADS/SEC	SINIT	INITIAL
48	PDDY		ANGULAR ACCN. IN BODY AXES	RADS/SEC2	SACCR0T	SACCB00
8	PHID		BANK ANGLE	DEGREES	SUC08	
214	PHIDIC		INITIAL VALUE OF PHI	DEGREES	SINIT	INITIAL

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
29	PHIDT		ATTITUDE RATE, BANK	RAD/SEC	SEULER	DERIVATIVE
7	PHIR		BANK ANGLE	RADIANS	DERIVATIVE	SUC08
87	PRATIO		ADIABATIC STATIC/TOTAL PRESS		SVELOC2	
77	PRESBL		AMBIENT PRESSURE AT SEA LEVEL	LB/IN 2	SINIT	SVELOC2 SINIT
82	PRESBR		ATMOSPHERIC PRESSURE RATIO		SATM08	SVELOC2 SINIT
4	PSID		HEADING ANGLE	DEGREES	SUC08	
204	PSIDIC		INITIAL VALUE OF PSI	DEGREES	ICFILE	INITIAL SINIT
31	PSIDT		ATTITUDE RATE, HEADING	RAD/SEC	SEULER	STV DERIVATIVE
64	PSIRD		FLIGHT PATH ANGLE, TRACK	DEGREES	SPATH	
63	PSIKR		FLIGHT PATH ANGLE, TRACK	RADIANS	SPATH	SPATH
3	PSIR		HEADING ANGLE	RADIANS	DERIVATIVE	SUC08
203	PSIND		DATUM WIND DIRECTION	DEGREES	ICFILE	SINIT

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
27	U		ANG VEL,PITCH,BODY AXES	RADS/SEC	DERIVATIVE	SEULER SACCR0T SACCR0D
33	U0		ANG VEL,PITCH,BODY AXES	D008/SEC	SEULER	
221	U0IC		INITIAL ANGULAR RATE	RADS/SEC	SINIT	INITIAL
46	U00T		ANGULAR ACCN. IN BODY AXES	RADS/SEC2	SACCR0T	SACCR0D
120	U0YN		DYNAMIC PRESSURE	LB/FT2	SVELOC2	SVELOC2
126	U0YNS		U0YN*SWNEF	LB	SVELOC2	SVELOC2
129	U00Z1V		MLFRMOV*00Z		SVELOC2	
127	U0CREF		U0YNS*CREF	LB-FT	SVELOC2	
128	U0SPAN		U0YNS*SPAN	LB-FT	SVELOC2	
28	W		ANG VEL,YAW,BODY AXES	RADS/SEC	DERIVATIVE	SEULER SACCR0T SACCR0D
141	RADT00		CONVERSION RADIANS TO DEGREES	CONSTANT	SINIT	S0C006 SPATH SALFBET

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
34	RO		ANG VEL,YAW,BODY AXES	D008/SEC	SEULER	SEULER SILS SINIT
222	ROIC		INITIAL ANGULAR RATE	RADS/SEC	SINIT	INITIAL
47	RO0T		ANGULAR ACCN. IN BODY AXES	RADS/SEC2	SACCR0T	SACCR0D
146	RO		RECIPROCAL OF G		SINIT	SACCR0D
174	RO0		RANGE FROM G/S TRANSMITTER	FT	SILS	SILS
72	RHO		AIR DENSITY	SLUG/FT3	SVELOC2	SVELOC2
79	RHOBL		DENSITY AT SEA LEVEL	SLUG /FT3	SINIT	SVELOC2 SINIT
283	RHP		PILOT W RADIUS	FT	STV	STV
205	RIC15		SPARE			
206	RIC16		SPARE			
207	RIC17		SPARE			
208	RIC18		SPARE			

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN	
209	RIC19		SPARE				
210	RIC20		SPARE				
176	RKINK		RANGE FROM BEAM KINK	FT	SILS	SILS	
175	RLOC		RANGE FROM LOC TRANSMITTER	FT	SILS	SILS	
71	ROOTSIG		SORT(DENSITY RATIO)		SVELOC2	SINIT SVELOC2	
1	RXMASS		1/XMASS		SINIT	SACCLIN	
282	RXP		PILOT X RADIUS	FT	STV	STV	
17	B11		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN	
18	B12		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN	
19	B13		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN SACCBDD	
20	B21		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN	

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN	
21	B22		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN	
22	B23		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN SACCBDD	
23	B31		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN	
24	B32		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN	
25	B33		DIRECTION COSINE		SDCOS	SVELOC1 SACCLIN SACCBDD	
116	BALFA		SINE OF ALPHA		BALFBET		
106	B02		BWREF*SPAN*SPAN	FT ⁴	SINIT	SVELOC2	
118	BUBETA		SINE OF BETA		BALFBET		
10	BECTMT		BEC(THETA)		SDCOS	SEULER SDCOS	
278	BFNACO		INTERMITTENCY FOR TURBULENCE		USER	SWIND	

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
180	BOS		GLIDE SLOPE SENSITIVITY	DEGREES	SILS	SILS
228	BHRFAC		SHEAR FACTOR		WSHEAR	SINIT SWIND
181	BLOC		LOCALISEN SENSITIVITY	DEGREES	SILS	SILS
103	SPAN		WING SPAN	FT	USER	SVELOC2 SINIT
13	SPHI		SIN(PHIN)		SUCOS	SEULER SDCOS
9	SPBI		SIN(PBIN)		SUCOS	STV SDCOS
225	SPSIN		SIN(PSIND)		SINIT	SWIND SINIT
80	SPBL		SPEED OF SOUND AT SEA LEVEL	FT/SEC	SINIT	SVELOC2 SINIT
84	SPBNDM		SPEED OF SOUND RATIO		SATMOS	SVELOC2 SINIT
73	SPBOND		SPEED OF SOUND	FT/SEC	SVELOC2	SVELOC2
279	SPDECLAY		DECAY FACTOR FOR TURBULENCE		USER	SWIND

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
105	STAIL		TAIL PLANE AREA	FT2	USER	
11	STMETA		SIN(THETA)		SUCOS	STV SDCOS
106	SHREF		WING REFERENCE AREA	FT2	USER	SVELOC2 SINIT
102	SHMIN		NEAR BELT JOIN(NEG) AND LIMIT	FT	STV	STV
104	SHMINUB		CYCLE LIMIT	FT	STV	STV
101	SHPL		NEAR BELT JOIN(POS) AND LIMIT	FT	STV	STV
103	SHPLUB		CYCLE LIMIT	FT	STV	STV
100	SHYIN		LIMIT FOR SIDWAYS(NEGATIVE)	FT	STV	STV
105	SHYPL		LIMIT FOR SIDWAYS(POSITIVE)	FT	STV	STV
88	TALPHA		FREE STREAM STATIC TEMPERATURE	DEG. K	SVELOC2	
16	TANTMT		TAN(THETA)		SUCOS	SEULER
81	TEMPR		ATMOSPHERIC TEMP RATIO		SATMOS	SVELOC2 SINIT
70	TEMPBL		AIR TEMP AT BLUNT AND DAY	DEG. K	SINIT	SVELOC2

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
						SINIT
6	THETA0		PITCH ATTITUDE	DEGREES	SOC08	
216	THETA0IC		INITIAL VALUE OF THETA	DEGREES	SINIT	INITIAL
8	THETAH		PITCH ATTITUDE	RADIANS	DERIVATIVE	SOC08
30	THETADT		ATTITUDE RATE/PITCH	RAD/SEC	BEULER	STV DERIVATIVE
94	TIME		TIME	SEC	DERIVATIVE	
89	TRATIO		ADIABATIC STATIC/TOTAL TEMP		SVELOC2	SVELOC2
366	TVCON(1,1)		ARRAY OF CONSTANTS FOR TV BELT		STV	STV
388	TVCON(8,3)		ARRAY OF CONSTANTS FOR TV BELT		STV	STV
68	UV		VEL COMP REL TO AIR/BOUY AXES	FT/SEC	SVELOC1	SVELOC2 SALFBET
236	USIU		RMS OF TURBULENCE	FT/SEC	USER	SWIND
184	USLOPE		SLOPE OF UPPER BEAM	DEGREES	SIL8	SIL8
232	UTURB		COMPONENT OF TURBULENCE	FT/SEC	SWIND	SWIND
69	VB		VEL COMP REL TO AIR/BOUY AXES	FT/SEC	SVELOC1	SVELOC2

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
						SALFBET
219	VD		COMP. OF TRUE AIR SPEED (DOWN)	FT/SEC	SVELOC1	SVELOC1
218	VE		COMP. OF TRUE AIR SPEED (EAST)	FT/SEC	SVELOC1	SVELOC1
69	VEAS		EQUIVALENT AIR SPEED	FT/SEC	SVELOC2	SVELOC2
70	VEASKT		EQUIVALENT AIR SPEED	KNOTS	SVELOC2	
65	VK		VELOCITY RELATIVE TO GROUND	FT/SEC	SPATH	SINIT SPATH
64	VKD		VELOCITY REL TO GROUND, DOWN	FT/SEC	DERIVATIVE	SVELOC1 SPATH STV
240	VKDDOT		ACCELERATION IN EARTH AXES	FT/SEC ²	SACCLIN	DERIVATIVE
213	VKDIC		INIT GROUND SPEED COMP (DOWN)	FT/SEC	SINIT	INITIAL SINIT
63	VKE		VELOCITY REL TO GROUND, EAST	FT/SEC	DERIVATIVE	SVELOC1 SPATH STV
239	VKEDOT		ACCELERATION IN EARTH AXES	FT/SEC ²	SACCLIN	DERIVATIVE
212	VKEIC		INIT GROUND SPEED COMP (EAST)	FT/SEC	SINIT	INITIAL

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
						SINIT
06	VKRT		VELOCITY RELATIVE TO GROUND	KNOTS	SPATH	
02	VKN		VELOCITY REL TO GROUND,NORTH	FT/SEC	DERIVATIVE	SVELOC1 SPATH STV
228	VKNDOT		ACCELERATION IN EARTH AXES	FT/SEC2	SACCLIN	DERIVATIVE
211	VKNIC		INIT GROUND SPEED COMP (NORTH)	FT/SEC	SINIT	INITIAL SINIT
199	VKTIC		INITIAL AIR SPEED	KNOTS	ICFILE	SINIT SINIT
217	VN		COMP. OF TRUE AIR SPEED(NORTH)	FT/SEC	SVELOC1	SVELOC1
169	VSHIPKT		SHIP SPEED	KT	USER	STV
226	VSIU		RMS OF TURBULENCE	FT/SEC	USER	SINIT
07	VT		TOTAL AIR SPEED	FT/SEC	SVELOC2	SINIT SVELOC2
08	VTRT		TOTAL AIR SPEED	KNOTS	SVELOC2	
223	VTUMB		COMPONENT OF TURBULENCE	FT/SEC	SINIT	SINIT

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
07	VWD		VELOCITY OF WIND,DOWN	FT/SEC	SINIT	SVELOC1
231	VWDL		MEAN WIND COMP AT HEIGHT(DOWN)	FT/SEC	SINIT	SINIT
223	VWDL0		WIND VELOCITY(DOWN)AT HEIGHT	FT/SEC	SINIT	SINIT
06	VWE		VELOCITY OF WIND,EAST	FT/SEC	SINIT	SVELOC1
230	VWEL		MEAN WIND COMP AT HEIGHT(EAST)	FT/SEC	SINIT	SINIT
227	VWEL0		WIND VELOCITY (EAST)AT HEIGHT	FT/SEC	SINIT	SINIT SINIT
202	VWRTO		DATUM WIND SPEED	KNOTS	ICFILE	SINIT
05	VWN		VELOCITY OF WIND,NORTH	FT/SEC	SINIT	SVELOC1
229	VWNL		MEAN WIND COMP AT HEIGHT(NTH)	FT/SEC	SINIT	SINIT
226	VWNLO		WIND VELOCITY (NORTH)AT HEIGHT	FT/SEC	SINIT	SINIT SINIT
198	W		AIRCRAFT HEIGHT	LB	ICFILE	SINIT SACCS00
00	WB		VEL COMP REL TO AIR,BODY AXES	FT/SEC	SVELOC1	SVELOC2 SALFBET

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
237	WBIG		RMS OF TUNBULENCE	FT/SEC	USER	BWIND
238	WTURB		COMPONENT OF TUNBULENCE	FT/SEC	BWIND	BWIND
149	X		X POSITION OF C.G.	FT	DERIVATIVE	STV SILS
207	X1		COORDINATES OF SLIP BALL (A1)	FT	USER	BACCROD
208	X2		COORDINATES OF U METER (A2)	FT	USER	BACCROD
209	X3		COORD. OF ACCELEROMETER (A3)	FT	USER	BACCROD
210	X4		COORD. OF ACCELEROMETER (A4)	FT	USER	BACCROD
211	X5		COORD. OF ACCELEROMETER (A5)	FT	USER	BACCROD
199	XCG		X C.G. LOCATION IN AIRCRAFT		ICFILE	SINIT
99	XCMEF		X LOCATION OF REF PT		USER	SINIT
198	XUOTH		RATE OF CHANGE OF A/C'S X POSN	FT/SEC	STV	DERIVATIVE STV
108	XOTRX		BLEW RATE	FT/SEC	STV	STV
109	XOTV		X VELOCITY FOR TV	FT/SEC	STV	

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
177	XOB		GLIDE SLOPE ORIGIN	FT	SILS	SILS
198	XIC		INITIAL POSITION	FT	ICFILE	SINIT INITIAL STV
284	XICF		EXTRA STORE FOR XIC	FT	STV	STV
199	XIMX		CONTROL VAN FOR X INTEGRATION		STV	DERIVATIVE
100	XINY		CONTROL VAN FOR Y INTEGRATION		STV	DERIVATIVE
200	XILBFLAG		ILBFLAG IN 'REAL' FORM		ICFILE	INITIAL
201	XISHR		ISHR IN 'REAL' FORM		ICFILE	INITIAL
48	XIX		MOMENT OF INERTIA/ROLL	SLUG FT ²	USER	SINIT
49	XIY		MOMENT OF INERTIA/PITCH	SLUG FT ²	USER	SINIT
50	XIZ		MOMENT OF INERTIA/YAW	SLUG FT ²	USER	SINIT
51	XIXX		MOMENT OF INERTIA/PRODUCT	SLUG FT ²	USER	SINIT
104	XK2FPB		CONVERSION KNOTS TO FT/SEC	CONSTANT	SINIT	BWIND STV SINIT

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
188	XKINR		POSITION OF BEAM KINR	FT	SILB	SILB
191	XLLTOT		TOTAL MOMENT, ROLL, BODY AXES	LB-FT	USER	SACCRBT
178	XLOC		LOCALISER ORIGIN (X)	FT	SILB	SILB
104	XLTAIL		TAIL ARM FROM M.H.C.	FT	USER	
76	XNACH		NACH NUMBER		SVELOC2	SVELOC2
2	XNASS		AIRCRAFT MASS	SLUG	SINIT	SINIT
132	XNMTOT		TOTAL MOMENT, PITCH, BODY AXES	LB-FT	USER	SACCRBT
133	XNMTOT		TOTAL MOMENT, YAW, BODY AXES	LB-FT	USER	SACCRBT
109	XP		X LOC OF PILOT REL TO NEFCG	FT	USER	STV
280	XPCB		X LOC OF PILOT REL TO CG		STV	STV SACCBOD
152	XTV		X POSITION FOR TV	FT	STV	STV
150	Y		Y POSITION OF C.G.	FT	DERIVATIVE	STV SILB
258	Y1		COORDINATES OF SLIP BALL (AY1)	FT	USER	SACCBOD

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
241	Y2		COORDINATES OF G METER (AZ2)	FT	USER	SACCBOD
244	Y3		COORD. OF ACCELEROMETER (AX3)	FT	USER	SACCBOD
247	Y4		COORD. OF ACCELEROMETER (AY4)	FT	USER	SACCBOD
270	Y5		COORD. OF ACCELEROMETER (AZ5)	FT	USER	SACCBOD
401	YADC(1)		ARRAY OF UNSCALED INPUTS		SADC	USER
404	YADC(4)		ARRAY OF UNSCALED INPUTS		SADC	USER
196	YDTV		Y VELOCITY FOR TV	FT/SEC	STV	
198	YIC		INITIAL POSITION	FT	ICFILE	INITIAL
179	YLOC		LOCALISER ORIGIN (Y)	FT	SILB	SILB
183	YTV		Y POSITION FOR TV	FT	STV	STV
259	Z1		COORDINATES OF SLIP BALL (AY1)	FT	USER	SACCBOD
262	Z2		COORDINATES OF G METER (AZ2)	FT	USER	SACCBOD
265	Z3		COORD. OF ACCELEROMETER (AX3)	FT	USER	SACCBOD
268	Z4		COORD. OF ACCELEROMETER (AY4)	FT	USER	SACCBOD

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ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
271	ZB		COORD. OF ACCELEROMETER (AZB)	FT	USER	BACC000
98	ZCG		Z C.G. LOCATION		USER	SINIT
100	ZCREF		Z LOCATION OF REF PT		USER	SINIT
110	ZP		Z LOC OF PILOT HEL TO REFCG	FT	USER	STV
281	ZPCG		Z LOC OF PILOT HEL TO CG		STV	STV BACC000

Appendix E

INDEX TO SYSTEM COMMON, INTEGER VARIABLES

E.1 Numeric order

SYSTEM COMMON - INTEGER VARIABLES 16-03-78						
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NUMERIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
1	RISA		SELECT ATMOSPHERE VARIATION		USER	SVELOCE SINIT
2	NCPASS		COUNT OF PASSES THRO DERIVATIVE		INITIAL	DERIVATIVE SCOUNT
3	NIPASS		COUNT OF PASSES TO SUIT INTEG		INITIAL	DERIVATIVE
4	ILBFLB		SELECTS ILB BEARING KILSFLB		INITIAL	SILB
5	ISHR		WIND SHEAR SHAPE (SEE RISHR)		INITIAL	SWIND SINIT
6	ISYS		UNIT NO FOR SYSTEM CHANGES		USER	SYSCOM
7	NTVS		TV BELT SELECT		USER	STV
8	JJCOMP		INITIALISATION COMPLETE FLAG		SCOUNT	SILB STV SWIND
9	NUND		NO. OF DACs TO BE SET FROM 'A'		USER	SDAC
10	NURV		NO. OF VARIACs TO BE SET FROM 'A'		USER	SDAC
11	NDAC(1)		POINTER TO VARIABLE FOR DAC 1		USER	SDAC

***** NOTE MISSING ELEMENT NUMBERS *****

SYSTEM COMMON - INTEGER VARIABLES 16-03-78						
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PAGE 2						
NUMERIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
***** NOTE MISSING ELEMENT NUMBERS *****						
74	NDAC(64)		POINTER TO VARIABLE FOR DAC 64		USER	SDAC
75	KBADC		VERSION ID - ROUTINE SADC		SADC	
76	KBDAC		VERSION ID - ROUTINE SDAC		SDAC	
77	KDSCRT1		VERSION ID - ROUTINE DSCRT1		DSCRT1	
78	KDSCRT2		VERSION ID - ROUTINE DSCRT2		DSCRT2	
79	KIBOSCR		VERSION ID - ROUTINE IBOSCR		IBOSCR	
80						
81	NADC(1)		ARRAY OF ADC CHANNEL NUMBERS		USER	SADC

***** NOTE MISSING ELEMENT NUMBERS *****

144	NADC(64)		ARRAY OF ADC CHANNEL NUMBERS		USER	SADC
145						
146						
147						

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NUMERIC ORDER	ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
	148	LSILS		CONTROLS EXECUTION OF SILS		USER	SILS
	149						
	150	IAD4SL		CONTROLS EXECUTION OF READSLR		USER	DSCRT1 DSCRT2
	151	ISLR(1)		AD4 SENSE LINE 1		READSLR	USER
***** NOTE MISSING ELEMENT NUMBERS *****							
	166	ISLR(16)		AD4 SENSE LINE 16		READSLR	USER
	167	NG		SCALE FACTOR IN NGUSTS		USER	SWIND
	168	LSEED		CONTROLS RANDOM NUMBER SEED		USER	SWIND
	169	NRUN		CURRENT RUN NO. FROM MAILBOX		SCOUNT	
	170	IAD4CL		CONTROLS EXECUTION OF SETCLR		USER	DSCRT1 DSCRT2
	171	ICLR(1)		AD4 CONTROL LINE 1		USER	SETCLR
***** NOTE MISSING ELEMENT NUMBERS *****							
	186	ICLR(16)		AD4 CONTROL LINE 16		USER	SETCLR

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NUMERIC ORDER	ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
	187						
	188						
	189						
	190	IDSCFL		CONTROLS EXECUTION OF READSCR		USER	DSCRT1 DSCRT2
	191	IP(1)		PATCHABLE DISCRETE 1 TO SIGMA		READSCR	ISDSCR
***** NOTE MISSING ELEMENT NUMBERS *****							
	222	IP(32)		PATCHABLE DISCRETE 32 TO SIGMA		READSCR	ISDSCR
	223	IDB(1)		DESK SWITCH 1 TO SIGMA		READSCR	INITIAL ISDSCR
***** NOTE MISSING ELEMENT NUMBERS *****							
	254	IDB(32)		DESK SWITCH 32 TO SIGMA		READSCR	ISDSCR
	255	KBACC00D		VERSION ID - ROUTINE SACC00D		SACC00D	
	256	KBACCLIN		VERSION ID - ROUTINE SACCLIN		SACCLIN	
	257	KBACCROT		VERSION ID - ROUTINE SACROT		SACCR0T	

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NUMERIC ORDER	ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
	258	KBALFBET		VERSION 10 - ROUTINE BALFBET		BALFBET	
	259	KBCOUNT		VERSION 10 - ROUTINE BCOUNT		BCOUNT	
	260	KSDCOS		VERSION 10 - ROUTINE SDCOS		SDCOS	
	261	KBEULER		VERSION 10 - ROUTINE BEULER		BEULER	
	262	KBILB		VERSION 10 - ROUTINE BILB		BILB	
	263	KBINIT		VERSION 10 - ROUTINE BINIT		BINIT	
	264	KSPATH		VERSION 10 - ROUTINE SPATH		SPATH	
	265	KSTV		VERSION 10 - ROUTINE STV		STV	
	266	KVELOC1		VERSION 10 - ROUTINE VELOC1		VELOC1	
	267	KVELOC2		VERSION 10 - ROUTINE VELOC2		VELOC2	
	268	KSHIND		VERSION 10 - ROUTINE SHIND		SHIND	
	269	KSYSCOM		VERSION 10 - ROUTINE SYSCOM		SYSCOM	
	270	IPCDFL		CONTROLS EXECUTION OF SETUSCR		USER	DSCRT1 DSCRT2
	271	IC011		CHANGE OVER 1 OUT OF SIGMA		USER	SETOBCR

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NUMERIC ORDER	ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
***** NOTE MISSING ELEMENT NUMBERS *****							
	302	IC012		CHANGE OVER 2 OUT OF SIGMA		USER	SETOBCR
	303						
	304						
	306	L1DAC(1)		DAC SOURCE POINTERS, LOOP1		USER	SDACN
***** NOTE MISSING ELEMENT NUMBERS *****							
	352	L1DAC(98)		DAC SOURCE POINTERS, LOOP1		USER	SDACN
	353	L2DAC(1)		DAC SOURCE POINTERS, LOOP2		USER	SDACN
***** NOTE MISSING ELEMENT NUMBERS *****							
	400	L2DAC(98)		DAC SOURCE POINTERS, LOOP2		USER	SDACN

E.2 Alphabetic order

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PAGE 1

ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
170	IAD4CL		CONTROLS EXECUTION OF SETCLR		USER	DSCRT1 DSCRT2
150	IAD4SL		CONTROLS EXECUTION OF HEADSLR		USER	DSCRT1 DSCRT2
171	ICLR(11)		AD4 CONTROL LINE 1		USER	SETCLR
186	ICLR(16)		AD4 CONTROL LINE 16		USER	SETCLR
271	ICO(11)		CHANGE OVER 1 OUT OF SIGMA		USER	SETDSCR
302	ICO(32)		CHANGE OVER 32 OUT OF SIGMA		USER	SETDSCR
223	IDB(11)		DESK SWITCH 1 TO SIGMA		READSCR	INITIAL ISDSCR
254	IDB(32)		DESK SWITCH 32 TO SIGMA		HEADSCR	ISDSCR
190	IUBCFL		CONTROLS EXECUTION OF HEADSCR		USER	DSCRT1 DSCRT2
4	ILSFLU		SELECTS ILB BEAM(SEE XILSFLG)		INITIAL	SILS
191	IP(11)		PATCHABLE DISCRETE 1 TO SIGMA		READSCR	ISDSCR
222	IP(32)		PATCHABLE DISCRETE 32 TO SIGMA		READSCR	ISDSCR

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
270	IPCDFL		CONTROLS EXECUTION OF SETDSCR		USER	DSCRT1 DSCRT2
5	ISHR		WIND SHEAR SHAPE(SEE XISHN)		INITIAL	SWIND SINIT
191	ISLR(11)		AD4 SENSE LINE 1		READSLR	USER
186	ISLR(16)		AD4 SENSE LINE 16		READSLR	USER
6	ISYS		UNIT NO FOR SYSTEM CHANGES		USER	SYSCOM
8	JJCOMP		INITIALISATION COMPLETE FLAG		SCOUNT	SILS STV SWIND
77	KDSCRT1		VERSION ID - ROUTINE DSCRT1		DSCRT1	
78	KDSCRT2		VERSION ID - ROUTINE DSCRT2		DSCRT2	
1	KISA		SELECT ATMOSPHERE VARIATION		USER	SVELOC2 SINIT
79	KISDSCR		VERSION ID - ROUTINE ISDSCR		ISDSCR	
255	KSACCB00		VERSION ID - ROUTINE SACCB00		SACCB00	
256	KSACCLIN		VERSION ID - ROUTINE SACCLIN		SACCLIN	

SYSTEM COMMON - INTEGER VARIABLES 16-03-78						
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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
257	KBACCHOT		VERSION 10 - ROUTINE SACCHOT		SACCHOT	
75	KBADC		VERSION 10 - ROUTINE SADC		SADC	
258	KBALFBET		VERSION 10 - ROUTINE SALFBET		SALFBET	
259	KSCOUNT		VERSION 10 - ROUTINE SCOUNT		SCOUNT	
76	KSDAC		VERSION 10 - ROUTINE SDAC		SDAC	
260	KSDCOS		VERSION 10 - ROUTINE SDCOS		SDCOS	
261	KSEULER		VERSION 10 - ROUTINE SEULER		SEULER	
262	KSILS		VERSION 10 - ROUTINE SILS		SILS	
263	KSINIT		VERSION 10 - ROUTINE SINIT		SINIT	
264	KSPATH		VERSION 10 - ROUTINE SPATH		SPATH	
265	KSTV		VERSION 10 - ROUTINE STV		STV	
266	KSVELOC1		VERSION 10 - ROUTINE SVELOC1		SVELOC1	
267	KSVELOC2		VERSION 10 - ROUTINE SVELOC2		SVELOC2	
268	KSHIND		VERSION 10 - ROUTINE SHIND		SHIND	

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ALPHABETIC ORDER						
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
269	KSYSCOM		VERSION 10 - ROUTINE SYSCOM		SYSCOM	
305	L1DAC(1)		DAC SOURCE POINTERS, LOOP1		USER	SDACN
352	L1DAC(48)		DAC SOURCE POINTERS, LOOP1		USER	SDACN
353	L2DAC(1)		DAC SOURCE POINTERS, LOOP2		USER	SDACN
400	L2DAC(48)		DAC SOURCE POINTERS, LOOP2		USER	SDACN
168	LSEED		CONTROLS RANDOM NUMBER SEED		USER	SHIND
148	LSILS		CONTROLS EXECUTION OF SILS		USER	SILS
81	NADC(1)		ARRAY OF ADC CHANNEL NUMBERS		USER	SADC
144	NADC(64)		ARRAY OF ADC CHANNEL NUMBERS		USER	SADC
2	NCPASS		COUNT OF PASSES THRO DERIVATIVE		INITIAL	DERIVATIVE SCOUNT
11	NDAC(1)		POINTER TO VARIABLE FOR DAC 1		USER	SDAC
74	NDAC(64)		POINTER TO VARIABLE FOR DAC 64		USER	SDAC
167	NS		SCALE FACTOR IN NSUST6		USER	SHIND
3	NIPASS		COUNT OF PASSES TO SUIT INTEG		INITIAL	DERIVATIVE

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ALPHABETIC ORDER

ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	CALCULATED IN	USED IN
109	NRUN		CURRENT RUN NO. FROM MAILBOX		SCOUNT	
7	NTVB		TV BELT SELECT		UBER	STV
9	NUMD		NO. OF DACB TO BE SET FROM 'A'		UBER	SDAC
10	NUMV		NO. OF VARIACB BE SET FROM 'A'		UBER	SDAC

Appendix F
DESCRIPTION OF PROGRAM COMMLIST

F.1 Introduction

The program COMMLIST produces an index to the variable names used in a large labelled COMMON area. A data record is prepared on cards for each variable name, giving a brief definition of the variable, its units and where it is calculated and used. A collection of such cards (which may be held on a disc file) may be sorted according to a number of criteria, of which the most important are alphabetic order of name and numeric order of element number.

For simulator purposes, two large COMMON areas are in current use, one defining system variables which are the same from simulation to simulation, *eg* height, speed and the other defining user variables which are entirely specific to the particular aircraft being simulated.

F.2 Input data

F.2.1 Main data record

Column	Purpose	Length
1 - 4	Element number	4 digits
5 - 16	Variable name	12 characters
18 - 47	Description	30 characters
49 - 58	Units	10 characters
60 - 67	Name of routine in which variable is calculated	8 characters
69 - 76	Name of routine in which variable is used	8 characters
78	Continuation indicator	1 character
	blank = no continuation	
	C = continuation .	

In general, no field delimiters are required. However, it may help human reading of data cards to insert a comma between fields. This is allowed, but is optional. The element number should be right justified in its field. A minimum of 2 data cards must be input.

F.2.2 Continuation cards

If the continuation indicator is set (C in column 78), the next card is read for additional 'used in' subroutine names. The format of this continuation card is up to 8 fields of 8 characters, separated by commas, a blank field signifying the end of the list of subroutine names and a field containing Cbbbbbbb signifying continuation on the next card.

F.3 Complete job deckF.3.1 Original data on cards

```
!JOB SIM,BARRY LIST COMMON VARIABLES
!ATTEND
!COMMLIST
    Title card
    Selection card
    Data cards
!EOD
!FIN
```

F.3.2 Original data on disc file

It is assumed data cards have been copied to a file by :COPY

```
!JOB SIM,BARRY LIST COMMON VARIABLES
!ATTEND
!ASSIGN (F:100,DC,RCOMMON)
!COMMLIST
    Title card
    Selection card
    Additional data cards (optional)
!EOD
!FIN
```

F.3.3 Remarks

Note, in example section F.3.2 above, that although the main input file is taken to be a disc file, data can still be read from the card reader in the same run. This enables additional data cards to be added to and merged with the main file, thus avoiding the need to recreate the main file for every small change in data.

Note also that if original data is on cards only, as in example section F.3.1, device 100 does *not* need to be assigned to the card reader.

!EOD is essential.

F.3.4 Title card

The 80 characters on this card are printed out as a heading on each page of the output listing exactly as they appear on the card. This enables the user to identify the nature of the information being listed. If the contents of the title card are centred on the card, they will be centred on the listing page.

F.3.5 Selection of listing options

Options are specified on a selection card, containing up to 20 words of 4 characters. The options are

Abbb	Alphabetic order of variable name
Dbbb	Data listed as stored
Nbbb	Numeric order according to element number
CbbbbSSSSSSSS	Lists all variables calculated in subroutine SSSSSSSS
UbbbbSSSSSSSS	Lists all variables used in subroutine SSSSSSSS
Xbbb	Read next card for additional instructions.

The blanks (b = blank) are essential. There are no field separators.

As many options as desired may be specified. If they will not fit on one selection card, continuation is indicated by the X option.

F.4 Output listings

The output listing reproduces the input information spaced out for better legibility. An extra column labelled 'quantity' is left blank for the insertion of mathematical symbols associated with the variable.

For the alphabetical option, all blank records (*ie* those with only an element number) are ignored and not printed.

For the numeric option, a warning message is output when an unused element number is encountered.

For options C and U the 'calculated in' or 'used in' columns are omitted, as appropriate.

In the early stages of building a COMMON list, it is worth including data cards containing only an element number. These will be listed by the numeric option and enable details of new variables to be written in on the listing.

Appendices D, E, G and H were produced by the COMMLIST program.

F.5 Arrays

It is recommended that the first and last elements of an array are included as data items, in order to make it clear in the listings which items in the complete list are genuinely unused. COMMLIST will handle arrays of more than one dimension, provided that an element, *eg* X(12,10) can be fitted into the allowable 12 characters. If this recommendation is adopted, the user will find the warning message 'NOTE MISSING ELEMENT NUMBERS' interspersed between the first and last elements in the numeric order listing.

F.6 Operational considerationsF.6.1 Devices used

DCB	Device	Purpose
100	defaults to card reader	data file
101	console TTY	opening message (!!COMMLIST)
105	card reader	title card
105	card reader	selection (control) cards
105	card reader	extra data
108	line printer	all listings

F.6.2 Messages

F.6.2.1 !!COMMLIST

This message on the console teletype announces the start of execution of COMMLIST.

F.6.2.2 *** NOTE MISSING ELEMENT NUMBERS ***

This is a warning message to draw attention to gaps in the sequence of element numbers.

F.6.2.3 COMMLIST ABORTED - TOO MANY INPUT RECORDS

This message is output on the teletype when too many input records have been read. It is repeated on device 108, supplemented by the last record read.

F.7 Limits on data

This program uses many (23) arrays to hold the input information. These arrays are dimensioned at present to cater for 500 input data cards. However, since the DO loops are in the range 1 to 1000, the number of input data cards could be increased to 1000 by altering the DIMENSION statements in the program and by increasing JMAX, the limit on the number of records read. Any increase will greatly enlarge the core store needed to run the program, so should not be made unless really necessary. This present limit of 500 applies, of course, to individual variable names, so the program will cope with a user array of 2000 or more locations if many constituents are themselves large arrays, for which it is adequate to include only the first and last elements, as already discussed.

F.8 Location of system COMMON

The raw data for system COMMON variables are held in files on the DC area of the disc. Real variables are in file DC, RCOMMON and integer variables in file DC, ICOMMON. An index listing may therefore be made at any time using the technique of section F.3.2, with the job card

!ASSIGN (F:100,DC,RCOMMON)

or

!ASSIGN (F:100,DC,ICOMMON)

included as required.

Appendix G

INDEX TO SYSTEM DATA TO BE PROVIDED BY THE USER, REAL VARIABLES

CALCULATED IN USER		SYSTEM COMMON - REAL VARIABLES 15.3-78			PAGE 1
ELEMENT NO.	FORTTRAN NAME	QUANTITY	DESCRIPTION	UNITS	USED IN
98	XIX		MOMENT OF INERTIA,ROLL	SLUG FT2	SINIT
99	XIV		MOMENT OF INERTIA,PITCH	SLUG FT2	SINIT
90	XIZ		MOMENT OF INERTIA,YAW	SLUG FT2	SINIT
91	XIZX		MOMENT OF INERTIA,PRODUCT	SLUG FT2	SINIT
91	DELTA1		INTEG. STEP LENGTH NO. 1	SECS	INITIAL
92	FRAMET1		FRAME TIME,LOOP 1	MSEC	INITIAL SWIND
95	DELTA2		INTEG. STEP LENGTH NO. 2	SECS	INITIAL
96	FRAMET2		FRAME TIME,LOOP 2	MSEC	INITIAL
98	ZCG		Z C.G. LOCATION		SINIT
99	XCOREF		X LOCATION OF REF PT		SINIT
100	ZCOREF		Z LOCATION OF REF PT		SINIT
103	SPAN		WING SPAN	FT	SVELOC2 SINIT
104	XLTAIL		TAIL ARM FROM M.R.C.	FT	

CALCULATED IN USER		SYSTEM COMMON - REAL VARIABLES 15.3-78			PAGE 2
ELEMENT NO.	FORTTRAN NAME	QUANTITY	DESCRIPTION	UNITS	USED IN
105	BTAIL		TAIL PLANE AREA	FT2	
106	SWREF		WING REFERENCE AREA	FT2	SVELOC2 SINIT
107	CREP		REFERENCE CHORD	FT	SVELOC2 STV
109	XP		X LOC OF PILOT REL TO REFCG	FT	STV
110	ZP		Z LOC OF PILOT REL TO REFCG	FT	STV
131	XLLOT		TOTAL MOMENT,ROLL,BODY AXES	LB-FT	SACCR0T
132	XMMTOT		TOTAL MOMENT,PITCH,BODY AXES	LB-FT	SACCR0T
133	XMMTOT		TOTAL MOMENT,YAW,BODY AXES	LB-FT	SACCR0T
134	FTX		TOTAL FORCE COMP. IN BODY AXES	LB	SACCLIN SACCB00
135	FTY		TOTAL FORCE COMP. IN BODY AXES	LB	SACCLIN SACCB00
136	FTZ		TOTAL FORCE COMP. IN BODY AXES	LB	SACCLIN SACCB00
139	VSWIPKT		SHIP SPEED	KT	STV

CALCULATED IN USER		SYSTEM COMMON - REAL VARIABLES 15.3.78			PAGE 3
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	USED IN
235	UB10		RMS OF TURBULENCE	FT/SEC	SWIND
236	VB10		RMS OF TURBULENCE	FT/SEC	SWIND
237	WB10		RMS OF TURBULENCE	FT/SEC	SWIND
257	X1		COORDINATES OF BLIP BALL (AY1)	FT	SACCB00
258	Y1		COORDINATES OF BLIP BALL (AY1)	FT	SACCB00
259	Z1		COORDINATES OF BLIP BALL (AY1)	FT	SACCB00
260	X2		COORDINATES OF G METER (AZ2)	FT	SACCB00
261	Y2		COORDINATES OF G METER (AZ2)	FT	SACCB00
262	Z2		COORDINATES OF G METER (AZ2)	FT	SACCB00
263	X3		COORD. OF ACCELEROMETER (AX3)	FT	SACCB00
264	Y3		COORD. OF ACCELEROMETER (AX3)	FT	SACCB00
265	Z3		COORD. OF ACCELEROMETER (AX3)	FT	SACCB00
266	X4		COORD. OF ACCELEROMETER (AY4)	FT	SACCB00
267	Y4		COORD. OF ACCELEROMETER (AY4)	FT	SACCB00

CALCULATED IN USER		SYSTEM COMMON - REAL VARIABLES 15.3.78			PAGE 4
ELEMENT NO.	FORTRAN NAME	QUANTITY	DESCRIPTION	UNITS	USED IN
268	Z4		COORD. OF ACCELEROMETER (AY4)	FT	SACCB00
269	X5		COORD. OF ACCELEROMETER (AZ5)	FT	SACCB00
270	Y5		COORD. OF ACCELEROMETER (AZ5)	FT	SACCB00
271	Z5		COORD. OF ACCELEROMETER (AZ5)	FT	SACCB00
278	BFRACT		INTERMITTENCY FOR TURBULENCE		SWIND
279	BRDECAY		DECAY FACTOR FOR TURBULENCE		SWIND
301	AADC(1)		ARRAY OF SCALING FACTORS		SADC
364	AADC(64)		ARRAY OF SCALING FACTORS		SADC
501	ADAC(1)		ARRAY OF SCALING FACTORS		SDAC
564	ADAC(64)		ARRAY OF SCALING FACTORS		SDAC

STOP 0
IFIN

Appendix H
INDEX TO SYSTEM DATA TO BE PROVIDED BY THE USER, INTEGER VARIABLES

SYSTEM COMMON - INTEGER VARIABLES 16-03-78

10:50 MAR 13, '79

PAGE 1

CALCULATED IN USER		QUANTITY	DESCRIPTION	UNITS	USED IN
ELEMENT NO.	FORTRAN NAME				
1	KISA		SELECT ATMOSPHERE VARIATION		SVLOC2 SINIT
6	ISYS		UNIT NO FOR SYSTEM CHANGES		SYSCOM
7	NTVS		TV BELT SELECT		STV
9	NUMD		NO. OF DACS TO BE SET FROM 'A'		SDAC
10	NUMV		NO. OF VARIADACS BE SET FROM 'A'		SDAC
11	NDAC(1)		POINTER TO VARIABLE FOR DAC 1		SDAC
74	NDAC(64)		POINTER TO VARIABLE FOR DAC 64		SDAC
81	NADC(1)		ARRAY OF ADC CHANNEL NUMBERS		SADC
104	NADC(64)		ARRAY OF ADC CHANNEL NUMBERS		SADC
148	LSILS		CONTROLS EXECUTION OF SILS		SILS
180	JAD4SL		CONTROLS EXECUTION OF HEADSLR		DSCRT1 DSCRT2
167	NS		SCALE FACTOR IN NGUSTS		SWIND
168	LSEED		CONTROLS RANDOM NUMBER SEED		SWIND

SYSTEM COMMON - INTEGER VARIABLES 16-03-78

10:50 MAR 13, '79

PAGE 2

CALCULATED IN USER		QUANTITY	DESCRIPTION	UNITS	USED IN
ELEMENT NO.	FORTRAN NAME				
170	JAD4CL		CONTROLS EXECUTION OF SETCLR		DSCRT1 DSCRT2
171	ICLR(1)		AD4 CONTROL LINE 1		SETCLR
186	ICLR(16)		AD4 CONTROL LINE 16		SETCLR
190	IDSCFL		CONTROLS EXECUTION OF REAUSCR		DSCRT1 DSCRT2
270	IPCDFL		CONTROLS EXECUTION OF SETUSCR		DSCRT1 DSCRT2
271	IC(1)		CHANGE OVEN 1 OUT OF SIGMA		SETUSCR
302	IC(32)		CHANGE OVEN 32 OUT OF SIGMA		SETUSCR
305	L1DAC(1)		DAC SOURCE POINTERS, LOOP1		SDACN
302	L1DAC(48)		DAC SOURCE POINTERS, LOOP1		SDACN
303	L2DAC(1)		DAC SOURCE POINTERS, LOOP2		SDACN
400	L2DAC(48)		DAC SOURCE POINTERS, LOOP2		SDACN

*STOP 0
IFIN

LIST OF SYMBOLS

a	speed of sound
a_x, a_y, a_z	accelerations along x, y, z body axes
b	reference wing span
\bar{c}	mean chord
c_{ref}	reference chord
CI_1 etc	inertia constants
f	shear factor
F_{TN}, F_{TE}, F_{TD}	applied forces in earth axes
F_{TX}, F_{TY}, F_{TZ}	applied forces in body axes
g	acceleration due to gravity
h	height of centre of gravity
I_x, I_y, I_z, I_{zx}	moments of inertia
L, M, N	total moments
M	Mach number
l_1, l_2, l_3, m_1, n_1 , etc	direction cosines
m	aircraft mass
P	atmospheric pressure
p, q, r	angular velocity components
R_{hp}	vertical distance of pilot's eye above centre of gravity
R_{xp}	horizontal distance of pilot's eye from centre of gravity
S_{ij}	direction cosines ($S_{11} = l_1$ etc)
S	transformation matrix
S_w	reference wing area
T	atmospheric temperature
u, v, w	velocity components
V	equivalent airspeed
V_K	ground speed
V_T	true airspeed
V_N, V_E, V_D	components of airspeed in earth axes (north, east, down)
V_{KN}, V_{KE}, V_{KD}	components of velocity relative to earth
V_{WN}, V_{WE}, V_{WD}	components of total wind velocity relative to earth
$V_{WNL\emptyset}, V_{WEL\emptyset}, V_{WDL\emptyset}$	components of datum mean wind speed in earth axes
$V_{WKT\emptyset}$	datum mean wind speed
$V_{WNL}, V_{WEL}, V_{WDL}$	components of mean wind speed at height
W	aircraft weight
X	force along x-axis
x, y, z	positional coordinates

LIST OF SYMBOLS (concluded)

x_p, z_p	coordinates of pilot's eye point, relative to reference centre of gravity
x_{pcg}, z_{pcg}	coordinates of pilot's eye point, relative to actual centre of gravity
$\Delta x_{cg}, \Delta z_{cg}$	centre of gravity displacements from reference position
α	angle of attack
β	angle of sideslip
γ	climb angle
θ	pitch attitude
ρ	air density
σ	atmospheric density ratio
ϕ	bank angle
χ	track angle
ψ	heading angle
ψ_w	wind direction

Suffices

a	absolute
B	body axes
cg	at, or of, the centre of gravity
G	gusts
L	at arbitrary location
p	pilot
r	ratio
SIG	rms
SL	sea level
T	turbulence
TV	television (for outside world display)
α	ambient

A dot over a variable denotes differentiation with respect to time.

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Fig 1

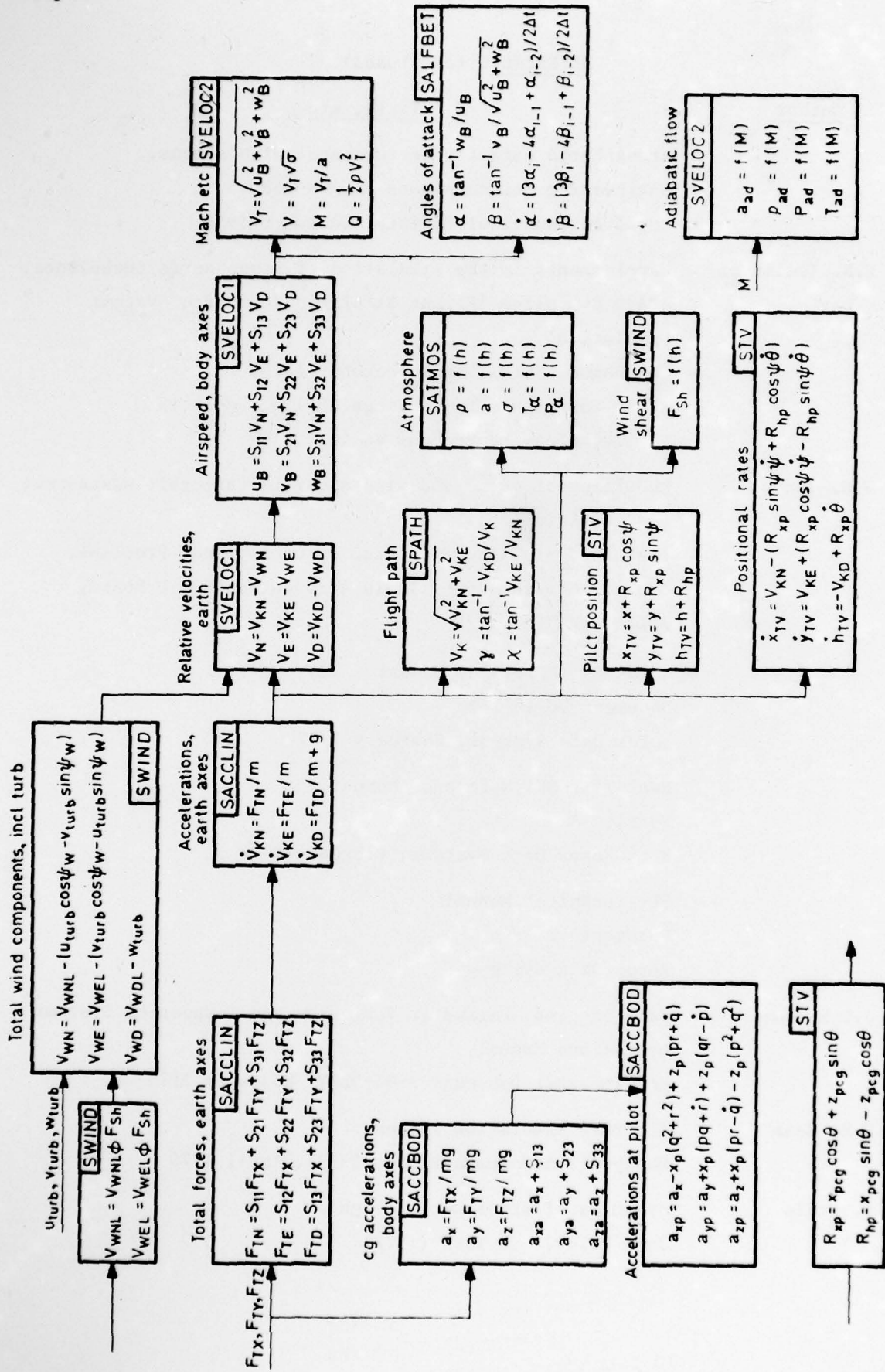


Fig 1 Block diagram of translational equations

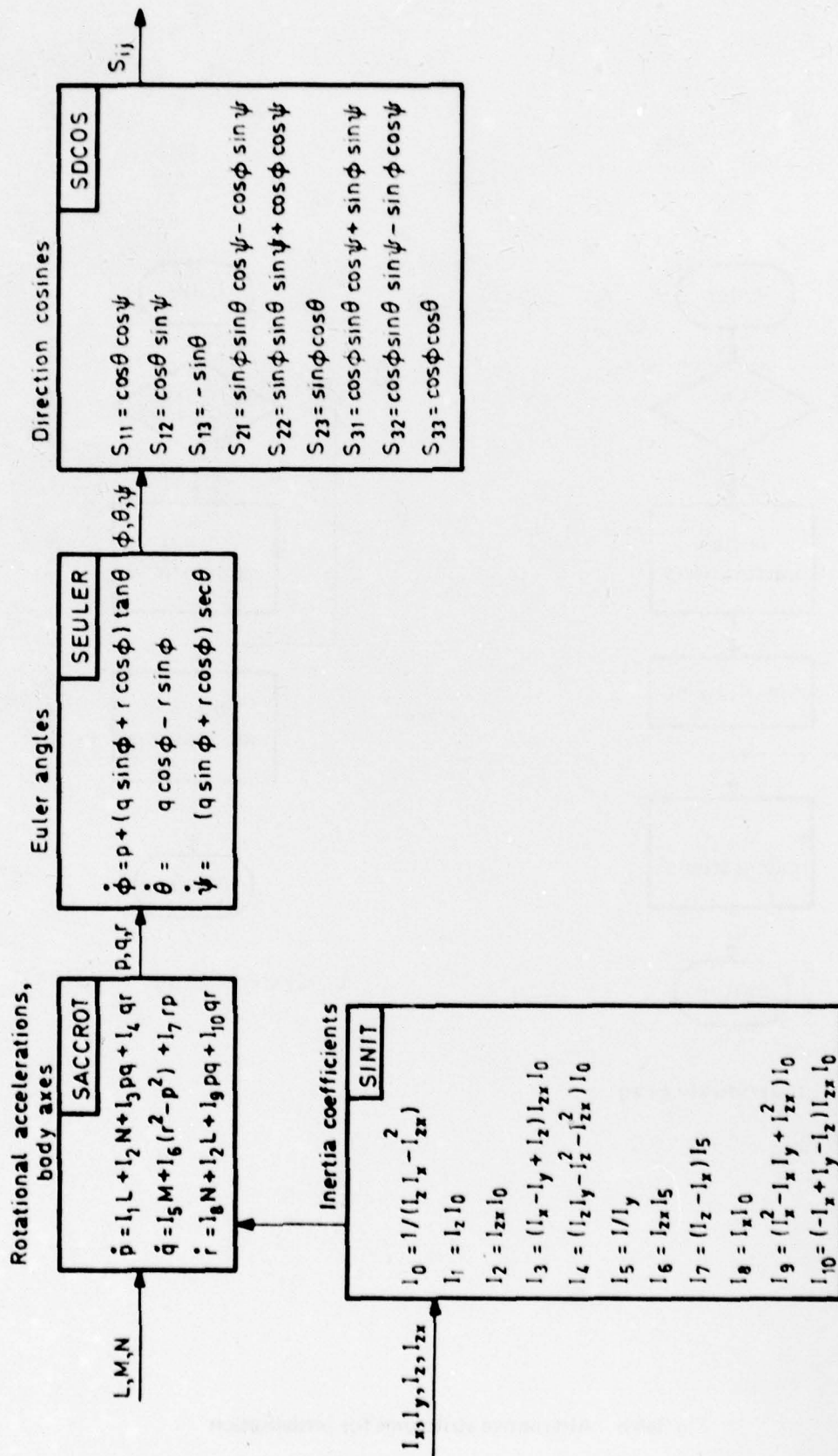
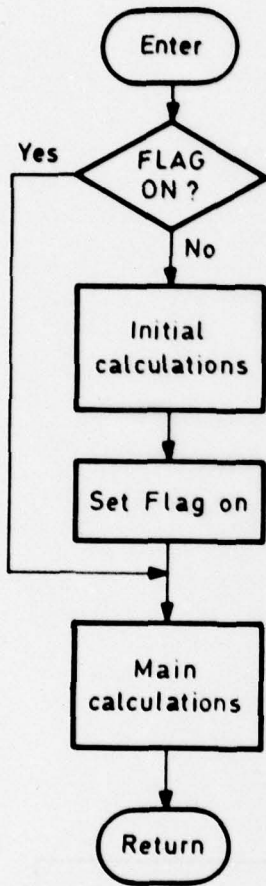
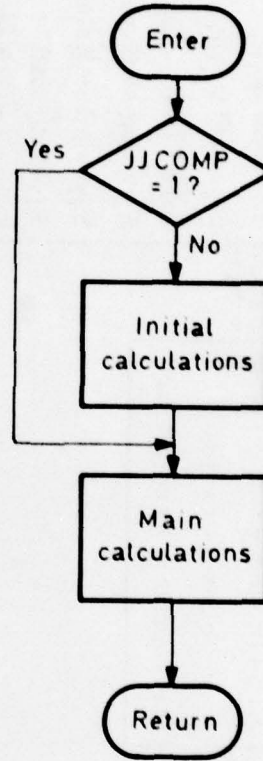


Fig 2 Block diagram of rotational equations

Fig 3a&b



a Individual Flag



b System Flag, JJCOMP

Fig 3a&b Alternative structures for initialisation

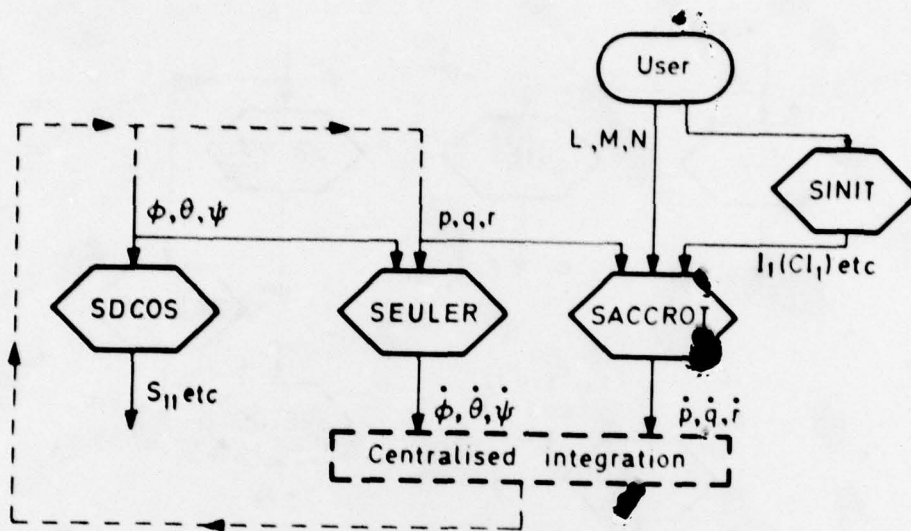


Fig 4 Information flow - rotational motion

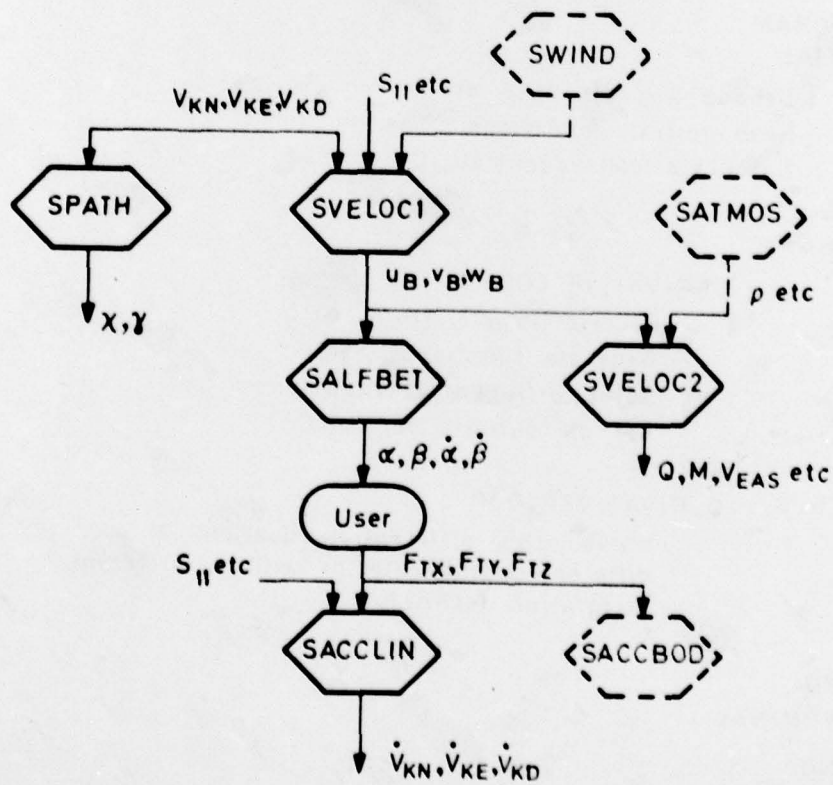


Fig 5 Information flow - translational motion

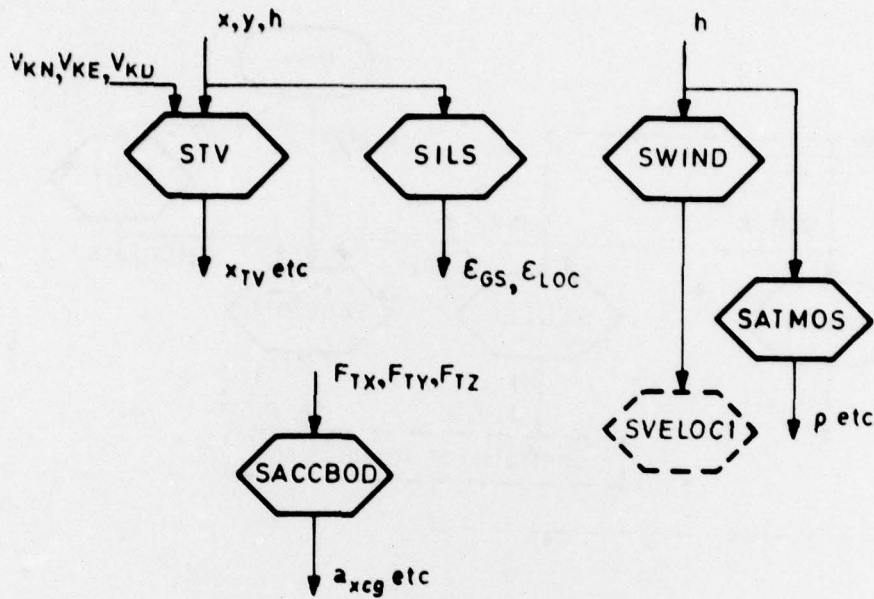


Fig 6 Information flow – utilities

PROGRAM
INITIAL

Set up aircraft data etc
Read initial conditions
Calculate consequential ICs

END
DYNAMIC

DERIVATIVE LOOP 1

Receive inputs from ADC
Generate functions
Solve differential equations
Set up outputs for DAC

END

DERIVATIVE LOOP 2

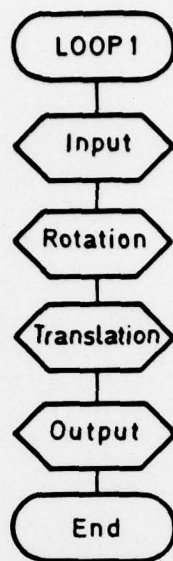
Solve other differential equations at a
different frame rate or with a different
integration technique

END

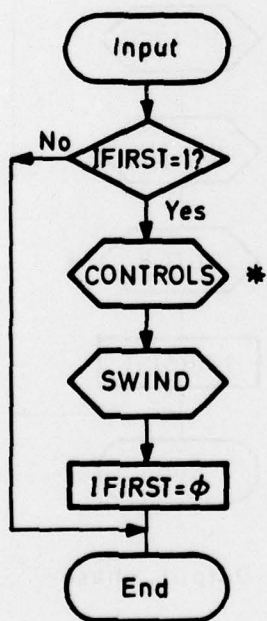
END
TERMINAL

END
END

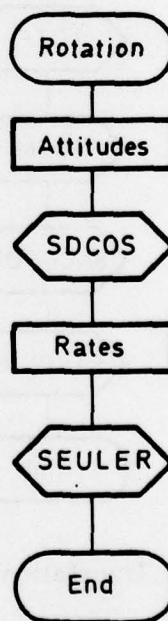
Fig 7 SL1 model program structure



a Phases of calculation



b Input phase

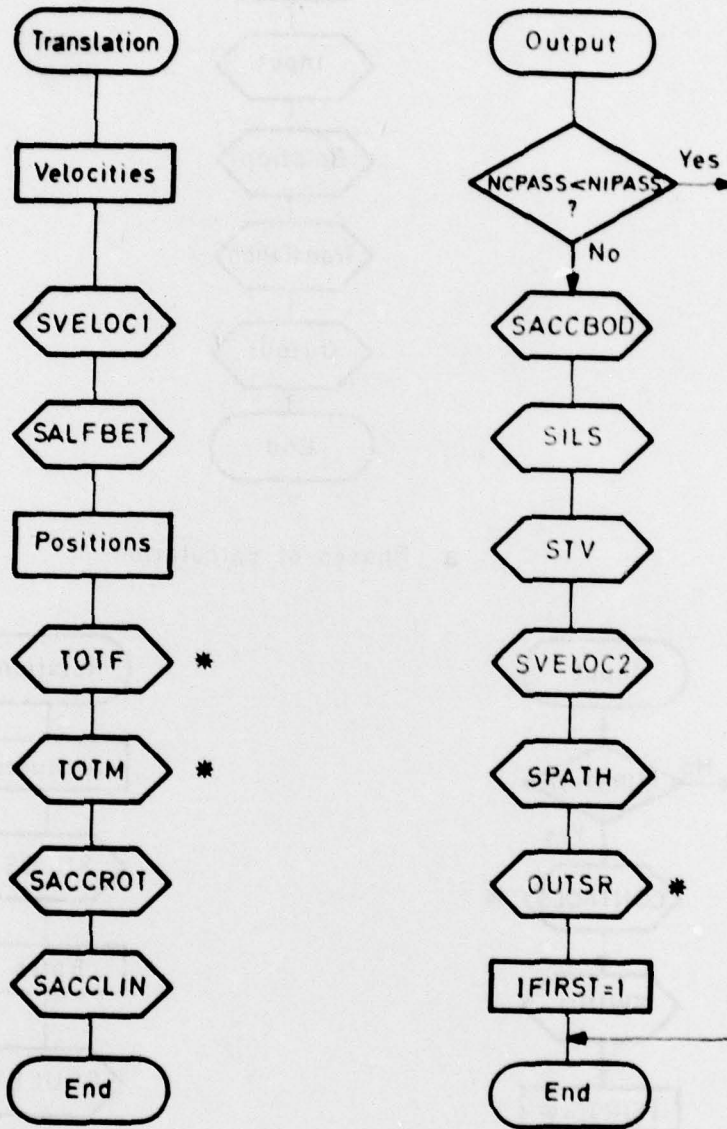


c Rotation phase

* Indicates routine to be supplied by User

Fig 8a-c Execution sequence, single loop

Fig 8d&e



d Translation phase

e Output phase

* Indicates routine to be supplied by User

Fig 8d&e Execution sequence, single loop

Fig A1

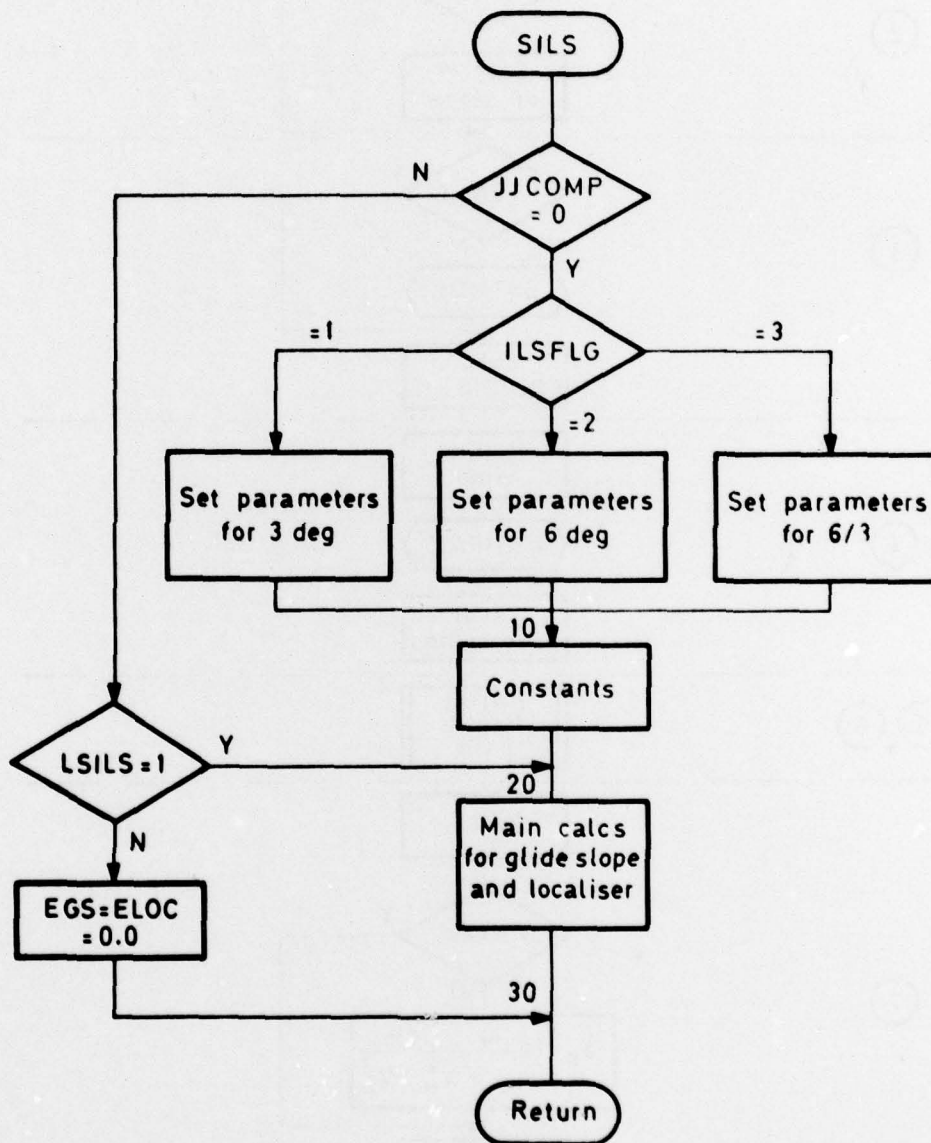


Fig A1 Flow diagram for SILS subroutine

Fig A2

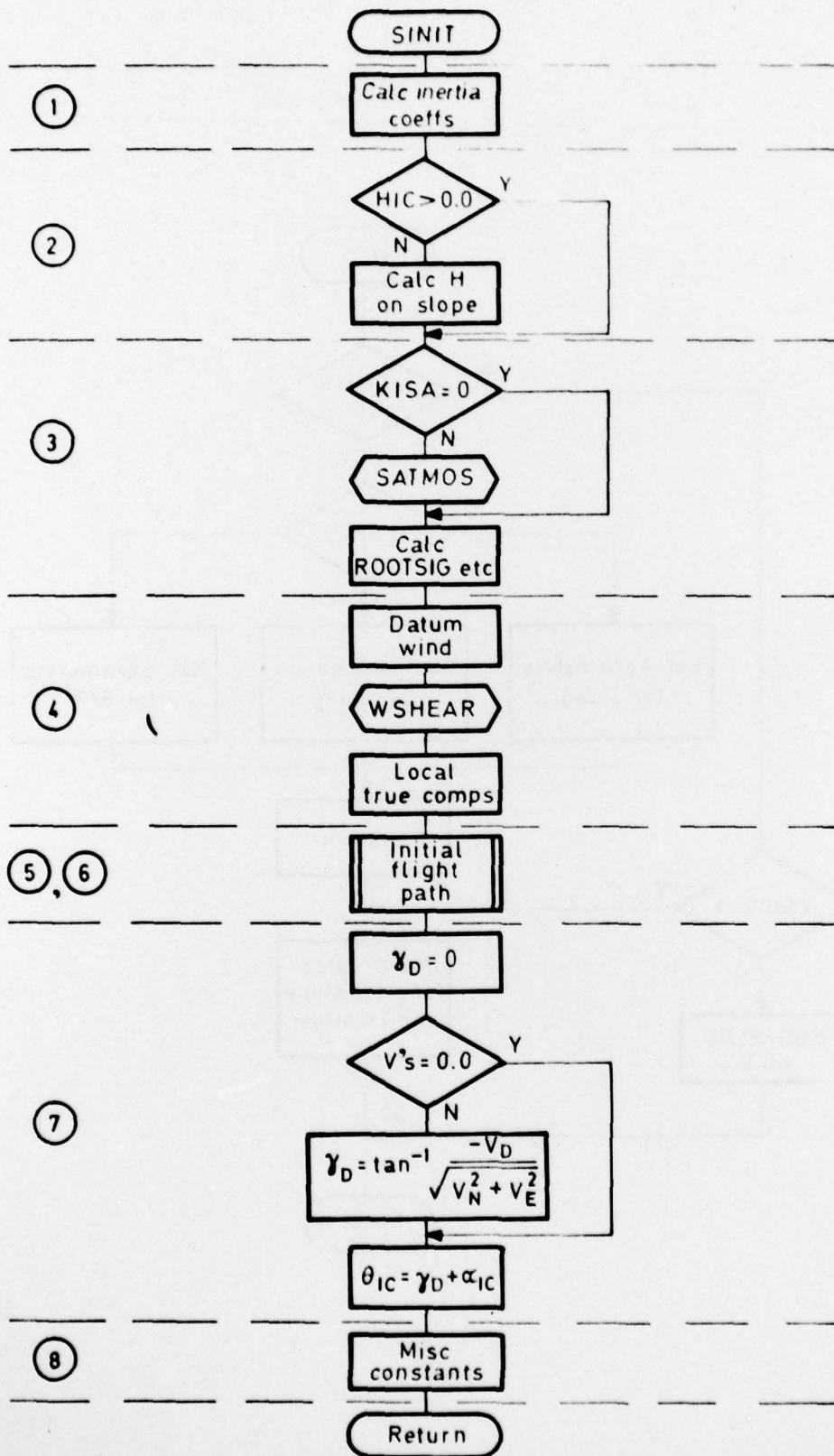


Fig A2 Flow diagram for SINIT subroutine

Fig A3

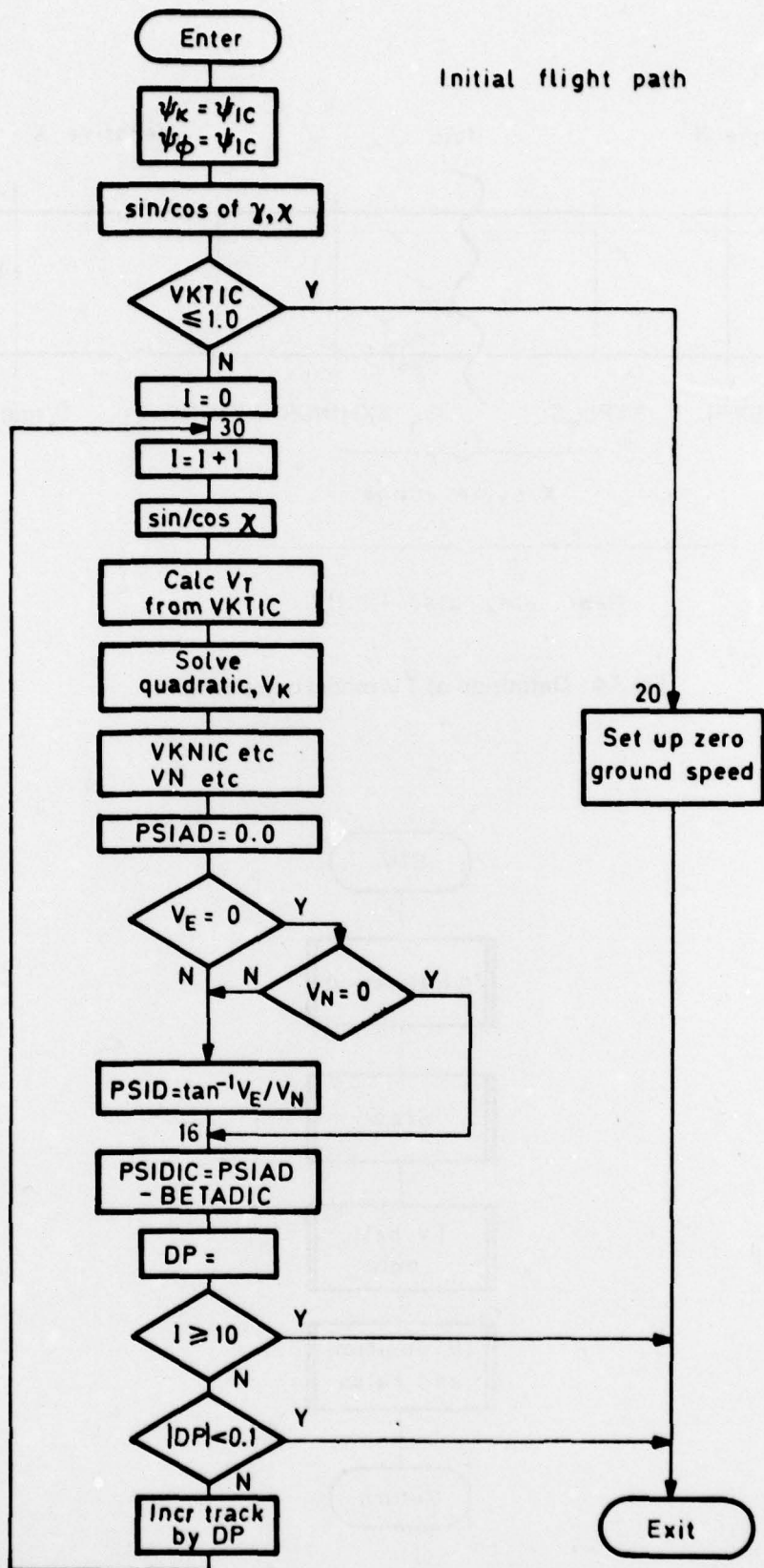


Fig A3 Flow diagram for 'initial flight path' phase of SINIT

Figs A4 & A5

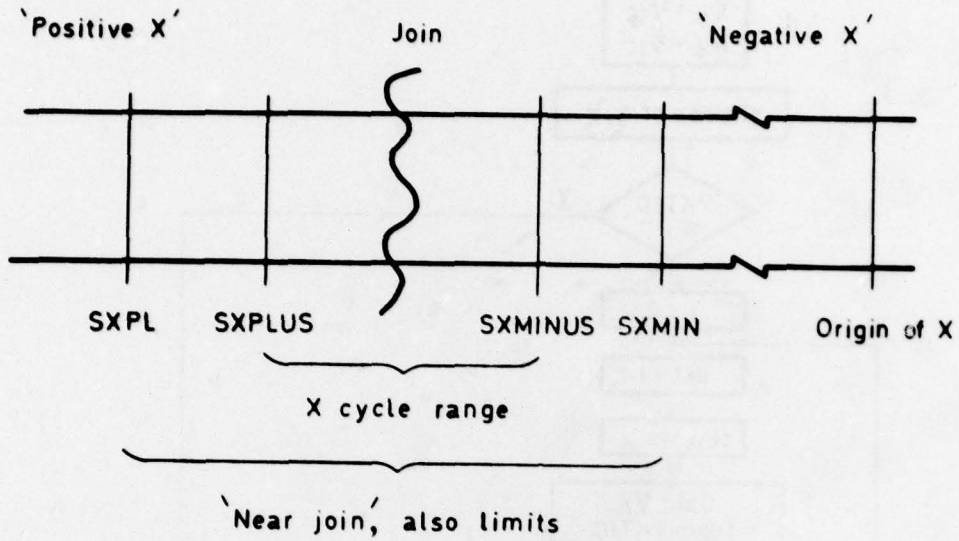


Fig A4 Definition of TV model belt positions

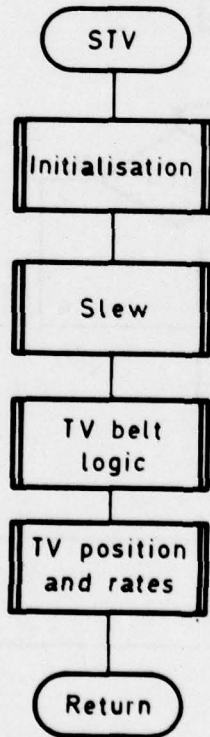


Fig A5 Overall flow diagram of STV subroutine

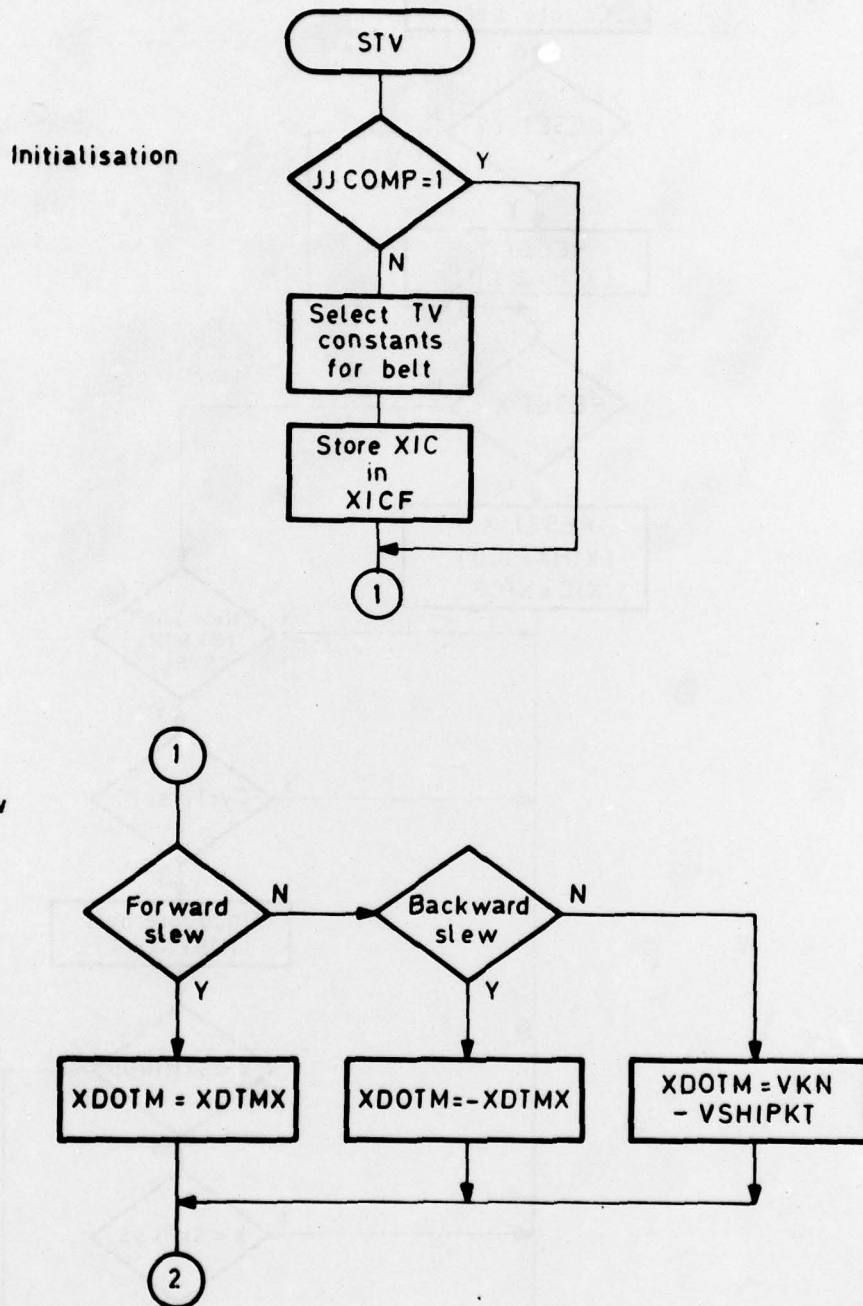


Fig A6 Flow diagrams of 'initialisation' and 'slew' phase of STV subroutine

Fig A7

TV belt logic

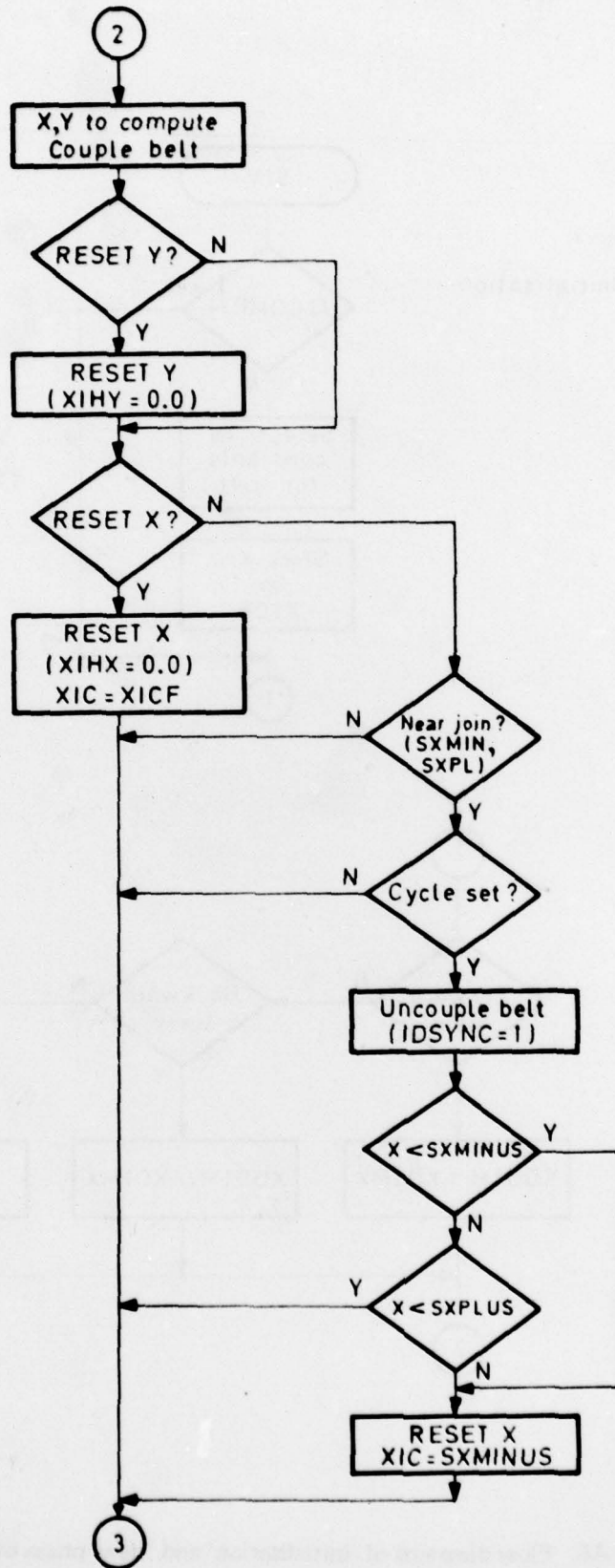


Fig A7 Flow diagram of TV belt logic in STV subroutine

TV position and rates

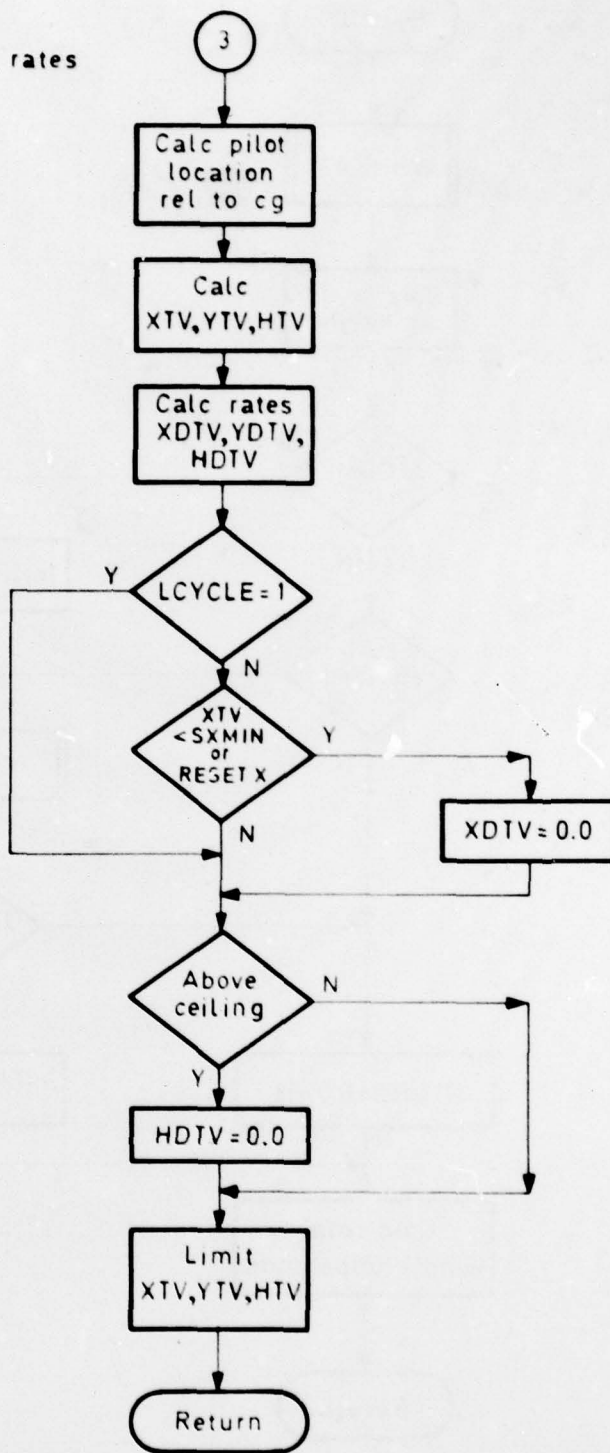


Fig A8 Flow diagram of TV position and rate control, STV subroutine

Fig A9

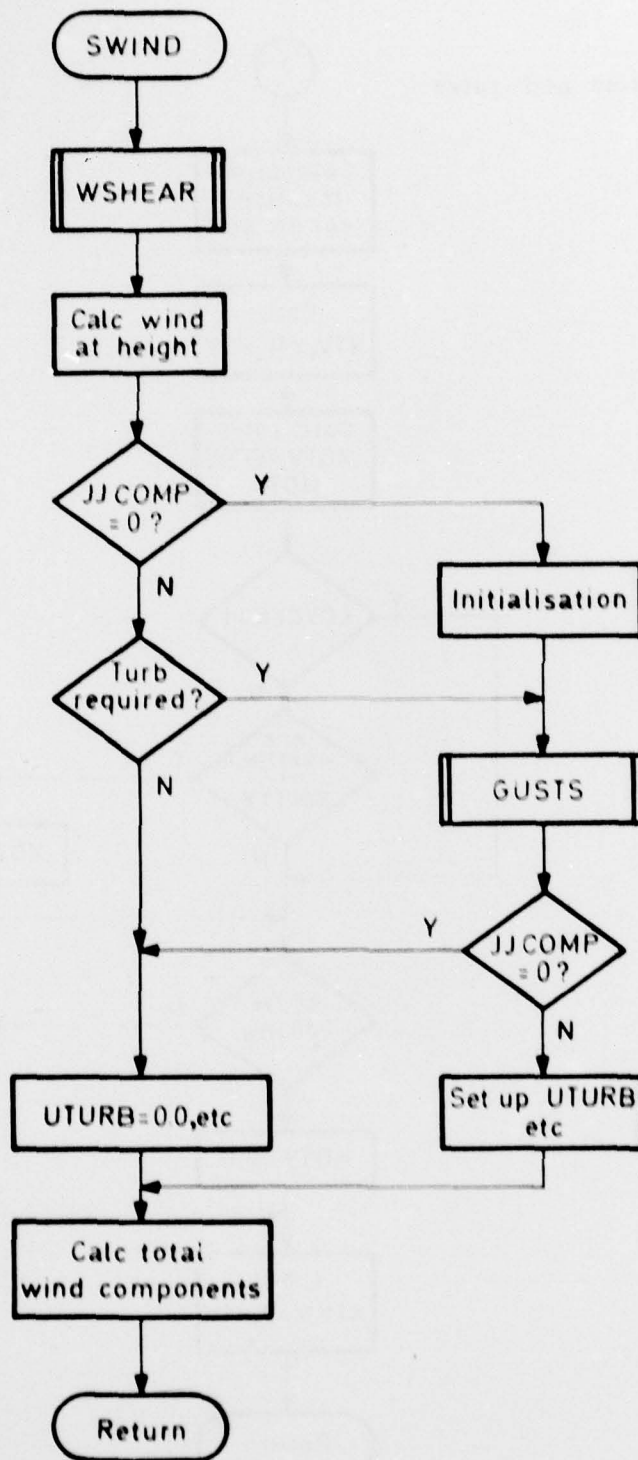


Fig A9 Flow chart of SWIND subroutine

REPORT DOCUMENTATION PAGE

Overall security classification of this page

UNCLASSIFIED

As far as possible this page should contain only unclassified information. If it is necessary to enter classified information, the box above must be marked to indicate the classification, e.g. Restricted, Confidential or Secret.

1. DRIC Reference (to be added by DRIC)	2. Originator's Reference RAE TR 79008	3. Agency Reference N/A	4. Report Security Classification/Marking UNCLASSIFIED
5. DRIC Code for Originator 7673000W	6. Originator (Corporate Author) Name and Location Royal Aircraft Establishment, Farnborough, Hants, UK		
5a. Sponsoring Agency's Code N/A	6a. Sponsoring Agency (Contract Authority) Name and Location N/A		
7. Title SESAME - A system of equations for the simulation of aircraft in a modular environment			
7a. (For Translations) Title in Foreign Language			
7b. (For Conference Papers) Title, Place and Date of Conference			
8. Author 1. Surname, Initials Tomlinson, B.N.	9a. Author 2	9b. Authors 3, 4	10. Date January 1979 Pages 149 Refs. 19
11. Contract Number N/A	12. Period N/A	13. Project	14. Other Reference Nos. FS 91
15. Distribution statement (a) Controlled by - Head of Flight Systems Department, RAE (b) Special limitations (if any) -			
16. Descriptors (Keywords) (Descriptors marked * are selected from TEST) Simulation. Mathematical modelling. Software. Computer programs			
17. Abstract A system of equations has been developed for the simulation of an aircraft's motion in real time using a digital computer. Those parts of the mathematical model common to all aircraft have been created as a set of Fortran subroutines, leaving the user to create only a small group of routines specifically to describe his aircraft. The equations employed are defined and the computer implementation described in detail. The Report can be used as a handbook and "user guide" but as the routines described are not specific to real-time simulation they could be used as a basis for a general mathematical model of an aircraft for use on any computer which supports Fortran.			

FS910/1