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LOCKHEED-GEORGIA CO MARIETTA

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THE GENERATION, RADIATION AND PREDICTION OF SUPERSONIC JET NOIS--ETC(U)

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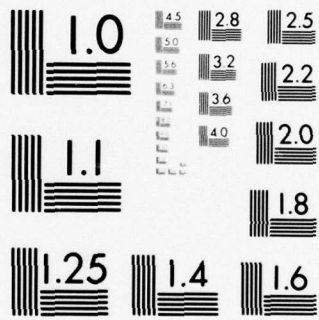
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AFAPL-TR-78-85  
Volume II

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**THE GENERATION, RADIATION AND PREDICTION  
OF SUPERSONIC JET NOISE  
VOLUME II - APPENDIX-COMPUTER PROGRAM LISTING**

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*LOCKHEED-GEORGIA COMPANY  
MARIETTA, GEORGIA 30063*

OCTOBER 1978

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FINAL REPORT FOR PERIOD 1 DECEMBER 1975 - 1 SEPTEMBER 1978

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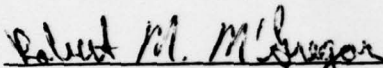
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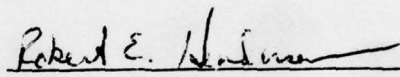
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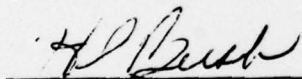
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This appendix volume presents a complete listing of the unified jet noise prediction computer program (UNIJET), developed to predict the total noise from a subsonic or supersonic jet under static conditions. In addition, a listing of the computer program (called INTEG) to predict absolute turbulent mixing noise levels at 90° to the jet axis, using laser velocimeter turbulence measurements, is also given. A detailed description of these two programs in the form of a user's guide is given in the main volume of this report.		

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```

*DECK UNIMAIN
PROGRAM UNIMAIN(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,TAPE2)
C .....
C *
C * UNIFIED JET NOISE PREDICTION PROGRAM *
C * ----- *
C *
C * PACKAGE A = NOISE FROM LARGE-SCALE TURBULENCE STRUCTURE *
C * PACKAGE B = TURBULENT MIXING NOISE *
C * PACKAGE C = SHOCK ASSOCIATED NOISE *
C *
C * OPNO = OPTION NUMBER *
C *
C * OPNO 1 = A *
C * OPNO 2 = B *
C * OPNO 3 = C *
C * OPNO 4 = A, B, AND A+B *
C * OPNO 5 = B, C, AND B+C *
C * OPNO 6 = A, C, AND A+C *
C * OPNO 7 = A, B, C, AND A+B+C *
C *
C * BOPNO 1 = HIGH-FREQUENCY LILLEY EQUATION SOLUTION *
C * BOPNO 2 = NUMERIC LILLEY EQUATION SOLUTION *
C .....
C DIMENSION TM(20),FREQ(30)
C DIMENSION SPLA(30),SPLB(30),SPLC(30),SPLT(30)
C DIMENSION SPLLS(30,20)
C DIMENSION SPLM(33,12)
C DIMENSION THDOCT(33)
C
C INTEGER TP,OPNO,BOPNO
C INTEGER OPPE
C REAL MJ
C
C INTEGER OC
C REAL K0,K1,L0,L1,MC
C
C DATA IC,OC/2HIC,2H /
C
C DATA NU /1/
C
C DATA THDOCT /
C 1 50. , 63. , 80. , 100. , 125. , 160. , 200. ,
C 2 250. , 315. , 400. , 500. , 630. , 800. , 1000. ,
C 3 1250. , 1600. , 2000. , 2500. , 3150. , 4000. , 5000. ,
C 4 6300. , 8000. , 10000. , 12500. , 16000. , 20000. , 25000. ,
C 5 31500. , 40000. , 50000. , 63000. , 80000. /
C WRITE EXPLANATIONS FOR FAILURES
C
C CALL DATE (DATED)
C CALL TIME (TIMED)
C WRITE (6,640) DATED,TIMED
C
C WRITE (6,650)
C
C WRITE (6,660)

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A 10
A 20
A 30
A 40
A 50
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A 400
A 410
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A 530
A 540
A 550
A 560
A 570
A 580

```



C		A 590
C	NOVEMBER 15 77. PREDICTION FOR VJ/A0 GT 1 INSIDE CONE OF	A 600
C	SILENCE(IC) ALLOWED	A 610
C		A 620
	WRITE (6,670)	A 630*
C		A 640
C	NOVEMBER 15 77. PREDICTION FOR VJ/A0 GT 1 INSIDE CONE OF	A 650
C	SILENCE(IC) ALLOWED	A 660
C		A 670
	WRITE (6,680)	A 680*
C		A 690
C	READ STATEMENTS	A 700
C		A 710
	READ (5,690) DIA,R	A 720*
	DFT=DIA/12.0	A 730
	ROD=R/DFT	A 740
C		A 750
C	NFREQ = 0 INPUT STARTING 1/3 O.B. NUMBER IN ISTART AND	A 760
C	ENDING 1/3 O.B. NUMBER IN ISTOP	A 770
C	NO FREQUENCIES ARE READ IN .	A 780
C	NFREQ NE 0 NFREQ IS THE NUMBER OF FREQUENCIES TO BE READ IN	A 790
C	ISTART AND ISTOP ARE NOT USED.	A 800
C		A 810
	READ (5,700) NANG,NFREQ,ISTART,ISTOP	A 820*
C		A 830
	IF (NFREQ,EQ.0) GO TO 10	A 840
	READ (5,690) (FREQ(I),I=1,NFREQ)	A 850*
	GO TO 30	A 860
C		A 870
	10 NFREQ=(ISTOP-ISTART)+1	A 880
	J=ISTART-1	A 890
	DO 20 I=1,NFREQ	A 900
	J=J+1	A 910
	20 FREQ(I)=THDOCT(J)	A 920
	30 CONTINUE	A 930
C		A 940
	READ (5,690) (TM(J),J=1,NANG)	A 950*
C		A 960
C		A 970
	READ (5,700) NS	A 980*
	READ (5,690) C,K0,K1,BC	A 990*
C		A1000
C	READ JET OPERATING CONDITIONS AND CALCULATE ALL BASIC PARAMETERS	A1010
C	*	A1020
C	* OPPE 0 = FLOW PARAMETERS INPUT ARE P0,T0F,VJA0,TJTO	A1030
C	* OPPE 1 = FLOW PARAMETERS INPUT ARE P0,T0F,PRG,TRF	A1040
C	*	A1050
C		A1060
	READ (5,700) OPNO,OPPER,ICODE,IFLG,BOPNO,ISS,IOPT,ILWR	A1070*
	IF (OPNO,EQ.2.OR,OPNO,EQ.4.OR,OPNO,EQ.5.OR,OPNO,EQ.7) CALL SELECT	A1080S
	1(NU,ISS)	A1090
	40 READ (5,700) TP	A1100*
C		A1110
C		A1120
	IF (TP,EQ.0) GO TO 630	A1130
C		A1140
	IF (OPPER,EQ.1) GO TO 50	A1150
	READ (5,690) P0,T0F,VJA0,TJTO	A1160*
	GO TO 60	A1170



50	READ (5,690) P0,T0F,PRG,TRF	A1180*
60	CONTINUE	A1190
	IF (IOPT.EQ.2) READ (5,690) RSW	A1200*
	IF (IOPT.EQ.3) READ (5,690) RSW,ALTB,BLTB	A1210*
C		A1220
C		A1230
	ICOMP=1	A1240
	IF (ICODE.EQ.0) GO TO 100	A1250
	IF (ICODE.EQ.2) GO TO 90	A1260
	READ (5,700) IVEL,IANG,INCANG	A1270*
	ICOMP=0	A1280
	IF (IVEL.EQ.0.OR.ISTART.EQ.0.OR.OPPER.EQ.0) ICOMP=1	A1290
	IF (ICOMP.EQ.1) GO TO 100	A1300
	REWIND 2	A1310*
	DO 80 IV=1,IVEL	A1320
	DO 70 J=1,12	A1330
	READ (2,710) (SPLM(I,J),I=7,30)	A1340*
70	CONTINUE	A1350
80	CONTINUE	A1360
	IOFF=ISTART-1	A1370
	GO TO 100	A1380
C		A1390
90	IOFF=ISTART-1	A1400
	ICOMP=0	A1410
	IANG=1	A1420
	INCANG=1	A1430
	READ (5,710) ((SPLM(I,J),I=7,30),J=1,NANG)	A1440*
C		A1450
100	CONTINUE	A1460
C		A1470
C	CLEAR MAIN ARRAY OF SPLS FROM LARGE SCALE NOISE PREDICTION	A1480
C		A1490
	DO 110 J=1,20	A1500
	DO 110 I=1,30	A1510
110	SPLLS(I,J)=1.0	A1520
C		A1530
	CALL CALPER (VJAO,TJTO,P0,T0F,TRF,PRG,TRK,TRTO,PRP0,PRGA,DJDO,MJ,A	A1540S
	10,VJ,GAMA,OPPER)	A1550
C		A1560
	IF (MJ.LE.1.0) GO TO 120	A1570
C		A1580
	BETA=SQRT(MJ*MJ-1.0)	A1590
	L0=K0*DIA*BETA	A1600
	L1=K1*DIA*BETA	A1610
	MC=C*VJAO	A1620
	VC=C*VJ	A1630
C		A1640
C	WRITE JET OPERATING CONDITIONS AND ALL BASIC PARAMETERS	A1650
C		A1660
120	WRITE (6,720) TP,OPNO,PRG,P0,TRF,T0F,GAMA	A1670*
C		A1680
	WRITE (6,730) PRP0,TRTO,TJTO,DJDO,VJAO,MJ,VJ	A1690*
C		A1700
	WRITE (6,740) DIA,R,ROD	A1710*
C		A1720
	IF (IOPT.GT.1) WRITE (6,750) RSW	A1730*
	IF (IOPT.EQ.3) WRITE (6,760) ALTB,BLTB	A1740*
	IF (OPNO.EQ.3) GO TO 130	A1750
	IF (OPNO.EQ.5) GO TO 130	A1760

	IF (OPNO, EQ. 6) GO TO 130	A1770
	IF (OPNO, EQ. 7) GO TO 130	A1780
	GO TO 140	A1790
C	130 WRITE (6, 770) C, K0, K1, NS	A1800
C		A1810*
C	IF (MJ, LE, 1.0) GO TO 140	A1820
C		A1830
C	WRITE (6, 780) BETA, VC, MC, L0, L1	A1840
C		A1850*
C	140 CONTINUE	A1860
C		A1870
C	BEGIN ANGLE LOOP	A1880
C		A1890
C	JJ=IANG-INCANG	A1900
	DO 620 J=1, NANG	A1910
	ZM=TM(J)/57.2957795	A1920
	JJ=JJ+INCANG	A1930
C		A1940
C	COMPUTE PACKAGE A IF OPTION NUMBER IS 1, 4, 6, OR 7	A1950
C		A1960
C	IF (OPNO, EQ. 1) GO TO 150	A1970
	IF (OPNO, EQ. 4) GO TO 150	A1980
	IF (OPNO, EQ. 6) GO TO 150	A1990
	IF (OPNO, EQ. 7) GO TO 150	A2000
	GO TO 220	A2010
C		A2020
C	150 CONTINUE	A2030
C		A2040
C	PACKAGE A -- NOISE FROM LARGE-SCALE TURBULENCE STRUCTURE*****	A2050
C		A2060
C	IF (ICOMP, EQ. 1) GO TO 160	A2070
	WRITE (6, 790) TM(J)	A2080
	GO TO 170	A2090*
	160 WRITE (6, 800) TM(J)	A2100
C		A2110*
C	BEGIN FREQUENCY LOOP (PACKAGE A)	A2120
C		A2130
C	170 SUMDIF=0.0	A2140
	IH=IOFF	A2150
	NF=0	A2160
C		A2170
C	DO 210 I=1, NFREQ	A2180
C		A2190
C	IF (J, NE, 1) GO TO 180	A2200
	F=FREQ(I)	A2210
C		A2220
C		A2230
C	STRNO=F*DFT/VJ	A2240
	CALL LSMAIN (VJA0, TJT0, GAMA, DFT, VJ, F, I, NANG, TM, IFLG, SPLLS)	A2250
	180 SPLA(I)=SPLLS(I, J)	A2260S
C		A2270
C	IF (ICOMP, EQ. 1) GO TO 200	A2280
	IH=IH+1	A2290
	SPLDIF=SPLA(I)-SPLM(IH, JJ)	A2300
	IF (SPLM(IH, JJ), LE, 10.0, OR, SPLA(I), LE, 10.0) SPLDIF=9999999.9	A2310
	IF (SPLM(IH, JJ), LE, 10.0, OR, SPLA(I), LE, 10.0) GO TO 190	A2320
	SUMDIF=SUMDIF+SPLDIF**2	A2330
	NF=NF+1	A2340
		A2350

C		A2360
C	WRITE PREDICTED VALUES (PACKAGE A)	A2370
C		A2380
	190 WRITE (6,810) FREQ(I),SPLA(I),SPLM(IH,JJ),SPLDIF,SUMDIF	A2390*
	GO TO 210	A2400
	200 WRITE (6,820) FREQ(I),SPLA(I)	A2410*
C		A2420
	210 CONTINUE	A2430
	IF (ICOMP,EQ,1) GO TO 220	A2440
	STDEV=0.0	A2450
	IF (NF.GT,0) STDEV=SQRT(SUMDIF/NF)	A2460
	WRITE (6,830) STDEV	A2470*
C		A2480
C	COMPUTE PACKAGE B IF OPTION NUMBER IS 2, 4, 5, OR 7	A2490
C		A2500
	220 IF (OPNO,EQ,2) GO TO 230	A2510
	IF (OPNO,EQ,4) GO TO 230	A2520
	IF (OPNO,EQ,5) GO TO 230	A2530
	IF (OPNO,EQ,7) GO TO 230	A2540
	GO TO 290	A2550
C		A2560
	230 CONTINUE	A2570
C		A2580
C	PACKAGE B -- TURBULENT MIXING NOISE*****	A2590
C		A2600
	WRITE (6,840) BOPNO	A2610*
	IF (ISS,EQ,1) WRITE (6,850)	A2620*
	IF (NU,EQ,3) WRITE (6,860)	A2630*
	IF (ICOMP,EQ,1) GO TO 240	A2640
	WRITE (6,870) TM(J)	A2650*
	GO TO 250	A2660
	240 WRITE (6,880) TM(J)	A2670*
C		A2680
C	BEGIN FREQUENCY LOOP (PACKAGE B)	A2690
C		A2700
	250 SUMDIF=0.0	A2710
	IH=IOFF	A2720
	NF=0	A2730
C		A2740
	DO 280 I=1,NFREQ	A2750
C		A2760
	CALL MXNOISE (NU,ILWR,OPNO,BOPNO,IOPT,ROD,DFT,TOF,A0,VJ,VJA0,TJTO,	A2770S
	1I,FREQ,S,ZM,SM,RSW,ALTB,BLTB,SPLB,SPLPD,SPLPQ,IND)	A2780
C		A2790
	IF (ICOMP,EQ,1) GO TO 270	A2800
	IH=IH+1	A2810
	SPLDIF=SPLB(I)-SPLM(IH,JJ)	A2820
	IF (SPLM(IH,JJ).LE,10.0.OR.SPLB(I).LE,15.0) SPLDIF=9999999.9	A2830
	IF (SPLM(IH,JJ).LE,10.0.OR.SPLB(I).LE,15.0) GO TO 260	A2840
	SUMDIF=SUMDIF+SPLDIF**2	A2850
	NF=NF+1	A2860
	260 WRITE (6,890) FREQ(I),S,SM,SPLPQ,SPLPD,SPLB(I),IND,SPLM(IH,JJ),SPL	A2870*
	DIF,SUMDIF	A2880
	GO TO 280	A2890
	270 WRITE (6,900) FREQ(I),S,SM,SPLPQ,SPLPD,SPLB(I),IND	A2900*
C		A2910
	280 CONTINUE	A2920
C		A2930
	IF (ICOMP,EQ,1) GO TO 290	A2940



	STDEV=0.0	A2950
	IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A2960
	WRITE (6,910) STDEV	A2970*
C	COMPUTE PACKAGE C 'F OPTION NUMBER IS 3, 5, 6, OR 7	A2980
C		A2990
	290 IF (OPNO,EQ.3) GO TO 300	A3000
	IF (OPNO,EQ.5) GO TO 300	A3010
	IF (OPNO,EQ.6) GO TO 300	A3020
	IF (OPNO,EQ.7) GO TO 300	A3030
	GO TO 370	A3040
		A3050
C	300 CONTINUE	A3060
C		A3070
C	PACKAGE C -- SHOCK ASSOCIATED NOISE*****	A3080
C		A3090
	IF (MJ.LE.1.0) GO TO 310	A3100
C		A3110
	DF=(1.0-(MC*COS(ZM)))	A3120
	WORK2=((L1*DF)/(VC*12.0))	A3130
C		A3140
	310 WRITE (6,920) TM(J)	A3150*
	IF (ICOMP,EQ.1) GO TO 320	A3160
	WRITE (6,930)	A3170*
	GO TO 330	A3180
	320 WRITE (6,940)	A3190*
C		A3200
C	BEGIN FREQUENCY LOOP (PACKAGE C)	A3210
C		A3220
	330 SUMDIF=0.0	A3230
	IH=IOFF	A3240
	NF=0	A3250
	DO 360 I=1,NFREQ	A3260
C		A3270
	CALL SANOISE (BETA,TJTO,ROD,BC,DFT,A0,NFREQ,FREQ,I,J,TM,L0,MJ,DF,W	A3280S
	1ORK2,NS,SPLC,HXX,HYY,CYY,A3,A2)	A3290
C		A3300
C	WRITE PREDICTED VALUES (PACKAGE C)	A3310
C		A3320
	IF (ICOMP,EQ.1) GO TO 350	A3330
	IH=IH+1	A3340
	SPLDIF=SPLC(I)-SPLM(IH,JJ)	A3350
	IF (SPLM(IH,JJ).LE.10.0.OR.SPLC(I).LE.10.0) SPLDIF=9999999.9	A3360
	IF (SPLM(IH,JJ).LE.10.0.OR.SPLC(I).LE.10.0) GO TO 340	A3370
	SUMDIF=SUMDIF+SPLDIF**2	A3380
	NF=NF+1	A3390
	340 WRITE (6,950) FREQ(I),HXX,HYY,CYY,A3,A2,SPLC(I),SPLM(IH,JJ),SPLDIF	A3400*
	1,SUMDIF	A3410
	GO TO 360	A3420
	350 WRITE (6,960) FREQ(I),HXX,HYY,CYY,A3,A2,SPLC(I)	A3430*
C		A3440
	360 CONTINUE	A3450
C		A3460
	IF (ICOMP,EQ.1) GO TO 370	A3470
	STDEV=0.0	A3480
	IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A3490
	WRITE (6,970) STDEV	A3500*
	370 CONTINUE	A3510
C		A3520
C	THE FOLLOWING FOUR SECTIONS COMPUTE THE TOTAL NOISE*****	A3530

C	**FOR OPTION NUMBERS 4, 5, 6, AND 7, RESPECTIVELY*****	A3540
C		A3550
	IF (OPNO.EQ.1) GO TO 620	A3560
	IF (OPNO.EQ.2) GO TO 620	A3570
	IF (OPNO.EQ.3) GO TO 620	A3580
	IF (OPNO.EQ.4) GO TO 380	A3590
	IF (OPNO.EQ.5) GO TO 440	A3600
	IF (OPNO.EQ.6) GO TO 520	A3610
	IF (OPNO.EQ.7) GO TO 540	A3620
C		A3630
C	COMPUTATION FOR OPTION 4 -- TOTAL NOISE = A+B	A3640
C		A3650
	380 WRITE (6,980) TM(J)	A3660*
	IF (ICOMP.EQ.0) WRITE (6,990)	A3670*
	IF (ICOMP.EQ.1) WRITE (6,1000)	A3680*
C		A3690
	SUMDIF=0.0	A3700
	IH=IOFF	A3710
	NF=0	A3720
C		A3730
	DO 430 I=1,NFREQ	A3740
	SPLT(I)=10.0*ALOG10(10.0**((SPLA(I)/10.0)+10.0**((SPLB(I)/10.0)))	A3750
	IF (ICOMP.EQ.1) GO TO 420	A3760
	IH=IH+1	A3770
	SPLDIF=SPLT(I)-SPLM(IH,JJ)	A3780
	IF (SPLM(IH,JJ).LE.10.0) GO TO 390	A3790
	IF (SPLT(I).LE.15.0) GO TO 390	A3800
	GO TO 400	A3810
	390 SPLDIF=9999999.9	A3820
	GO TO 410	A3830
	400 CONTINUE	A3840
	SUMDIF=SUMDIF+SPLDIF**2	A3850
	NF=NF+1	A3860
	410 WRITE (6,1010) FREQ(I),SPLA(I),SPLB(I),SPLT(I),SPLM(IH,JJ),SPLDIF,	A3870*
	1SUMDIF	A3880
	GO TO 430	A3890
	420 WRITE (6,1020) FREQ(I),SPLA(I),SPLB(I),SPLT(I)	A3900*
	430 CONTINUE	A3910
C		A3920
	IF (ICOMP.EQ.1) GO TO 620	A3930
	STDEV=0.0	A3940
	IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A3950
	WRITE (6,1030) STDEV	A3960*
	GO TO 620	A3970
C		A3980
C	COMPUTATION FOR OPTION 5 -- TOTAL NOISE = B+C	A3990
C		A4000
	440 WRITE (6,1040) TM(J)	A4010*
	IF (ICOMP.EQ.1) GO TO 450	A4020
	WRITE (6,1050)	A4030*
	GO TO 460	A4040
	450 WRITE (6,1060)	A4050*
C		A4060
	460 CONTINUE	A4070
	SUMDIF=0.0	A4080
	IH=IOFF	A4090
	NF=0	A4100
	DO 510 I=1,NFREQ	A4110
	SPLT(I)=10.0*ALOG10(10.0**((SPLB(I)/10.0)+10.0**((SPLC(I)/10.0)))	A4120

IF (ICOMP.EQ.1) GO TO 500	A4130
IH=IH+1	A4140
SPLDIF=SPLT(I)-SPLM(IH,JJ)	A4150
IF (SPLM(IH,JJ).LE.10.0) GO TO 470	A4160
IF (SPLB(I).LE.15.0) GO TO 470	A4170
IF (SPLC(I).LT.10.0) GO TO 470	A4180
GO TO 480	A4190
470 SPLDIF=9999999.9	A4200
GO TO 490	A4210
480 CONTINUE	A4220
SUMDIF=SUMDIF+SPLDIF**2	A4230
NF=NF+1	A4240
490 WRITE (6,1070) FREQ(I),SPLB(I),SPLC(I),SPLT(I),SPLM(IH,JJ),SPLDIF,	A4250*
1SUMDIF	A4260
GO TO 510	A4270
500 CONTINUE	A4280
WRITE (6,1080) FREQ(I),SPLB(I),SPLC(I),SPLT(I)	A4290*
510 CONTINUE	A4300
C	A4310
IF (ICOMP.EQ.1) GO TO 620	A4320
STDEV=0.0	A4330
IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A4340
WRITE (6,1090) STDEV	A4350*
GO TO 620	A4360
C	A4370
C	A4380
COMPUTATION FOR OPTION 6 -- TOTAL NOISE = A+C	A4390
C	A4400*
520 WRITE (6,1100) TM(J)	A4410
C	A4420
DO 530 I=1,NFREQ	A4430
SPLT(I)=10.0*ALOG10(10.0**((SPLA(I)/10.0)+10.0**((SPLC(I)/10.0))	A4440*
WRITE (6,1110) FREQ(I),SPLA(I),SPLC(I),SPLT(I)	A4450
530 CONTINUE	A4460
C	A4470
GO TO 620	A4480
C	A4490
C	A4500
COMPUTATION FOR OPTION 7 -- TOTAL NOISE = A+B+C	A4510*
C	A4520
540 WRITE (6,1120) TM(J)	A4530*
IF (ICOMP.EQ.1) GO TO 550	A4540
WRITE (6,1130)	A4550*
GO TO 560	A4560
550 WRITE (6,1140)	A4570
560 CONTINUE	A4580
C	A4590
SUMDIF=0.0	A4600
IH=IOFF	A4610
NF=0	A4620
DO 610 I=1,NFREQ	A4630
SPLT(I)=10.0*ALOG10(10.0**((SPLA(I)/10.0)+10.0**((SPLB(I)/10.0)+10.0	A4640
1**((SPLC(I)/10.0))	A4650
IF (ICOMP.EQ.1) GO TO 600	A4660
IH=IH+1	A4670
SPLDIF=SPLT(I)-SPLM(IH,JJ)	A4680
IF (SPLM(IH,JJ).LE.10.0) GO TO 570	A4690
IF ((SPLA(I).LE.10.0.AND.SPLB(I).LE.15.0).OR.SPLC(I).LE.10.0) GO TO 5	A4700
170	A4710
GO TO 580	
570 SPLDIF=9999999.9	



GO TO 590	A4720
580 SUMDIF=SUMDIF+SPLDIF**2	A4730
NF=NF+1	A4740
590 WRITE (6,1150) FREQ(I),SPLA(I),SPLB(I),SPLC(I),SPLT(I),SPLM(IH,JJ)	A4750*
1,SPLDIF,SUM	A4760
GO TO 610	A4770
600 CONTINUE	A4780
WRITE (6,1160) FREQ(I),SPLA(I),SPLB(I),SPLC(I),SPLT(I)	A4790*
610 CONTINUE	A4800
C	A4810
IF (ICOMP.EQ.1) GO TO 620	A4820
STDEV=0.0	A4830
IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A4840
WRITE (6,1170) STDEV	A4850*
GO TO 620	A4860
C	A4870
C	A4880
END ANGLE LOOP	A4890
C	A4900
620 CONTINUE	A4910
GO TO 40	A4920
630 STOP	A4930
C	A4940
640 FORMAT (1H1,10X,"DATE ",1A10,10X,"TIME ",1A10,//)	A4950
650 FORMAT (2X,"***LARGE SCALE NOISE FAILURES ARE INDICATED BY THE ","	A4960
1FOLLOWING***",//5X,"SPLA=1.0 STABILITY CALCULATIONS FAILED TO CO	A4970
2NVERGE",/5X,"SPLA=2.0 LARGE SCALE NOISE AT THIS JET VELOCITY IS N	A4980
3EGLECTED ",/5X,"SPLA=3.0 LARGE SCALE NOISE AT THIS ANGLE IS NEGLE	A4990
4CTED",/5X,"SPLA=4.0 LARGE SCALE NOISE AT THIS FREQUENCY IS NEGLE	A5000
5TED",/5X,"SPLA=5.0 SEARCH FOR STARTING VALUES GIVES SINGULAR MAT	A5010
6RIX",////)	A5020
660 FORMAT (2X,"***TURBULENT MIXING NOISE (BOPNO 1) FAILURES ARE INDIC	A5030
ATED BY THE FOLLOWING***",//5X,"SPLB=1.0 VELOCITY PROFILE GRADIENT	A5040
2T IS NOT AVAILABLE",/5X,"SPLB=2.0 SM IS OUTSIDE THE RANGE OF SOURCE	A5050
3CE DATA",/5X,"SPLB=3.0 SOURCE DIRECTIVITY EXPRESSION IS LESS THAN	A5060
4 ZERO",/5X,"SPLB=4.0 NUMBER OF ITERATIONS EXCEEDS 50",/5X,"SPLB=5	A5070
5.0 SM GOES NEGATIVE IN ITERATION ROUTINE",/5X,"SPLB=6.0 ARGUMENT	A5080
6 X IN DECAY FACTOR IS NEGATIVE",/5X,"SPLB=7.0 RADIATION ANGLE IS	A5090
7LESS THAN 30.0 DEGREES",/5X,"SPLB=8.0 TURBULENT MIXING NOISE AT T	A5100
8HIS ANGLE AND JET ","VELOCITY IS NEGLECTED",////)	A5110
670 FORMAT (2X,"***TURBULENT MIXING NOISE (BOPNO 2) FAILURES ARE INDIC	A5120
ATED BY THE FOLLOWING***",//5X,"SPLB=2.0 SM IS OUTSIDE THE RANGE	A5130
2OF SOURCE DATA",/5X,"SPLB=3.0 SOURCE DIRECTIVITY EXPRESSION IS LE	A5140
3SS THAN ZERO",/5X,"SPLB=4.0 NUMBER OF ITERATIONS EXCEEDS 50",/5X,	A5150
4"SPLB=5.0 SM GOES NEGATIVE IN ITERATION ROUTINE",/5X,"SPLB=8.0 T	A5160
5URBULENT MIXING NOISE AT THIS ANGLE AND JET ","VELOCITY IS NEGLECT	A5170
6ED",/5X,"SPLB=9.0 CRITICAL LAYER RADIUS TOO SMALL",/5X,"SPLB=10	A5180
7.0 BESSEL FUNCTION FAILURE",/5X,"SPLB=11.0 SOURCE AND CRITICAL	A5190
8LAYER RADIUS COINCIDE",////)	A5200
680 FORMAT (2X,"***SHOCK ASSOCIATED NOISE FAILURES ARE INDICATED BY TH	A5210
1E FOLLOWING***",//5X,"SPLC=1.0 MJ IS LESS THAN 1.0",/5X,"SPLC=2.0	A5220
2 SIGMA IS OUTSIDE THE RANGE OF MASTER SPECTRA",/5X,"SPLC=3.0 SHO	A5230
3CK NOISE CONTRIBUTION AT THIS ANGLE AND JET"," TEMPERATURE"/15X,"C	A5240
4AN BE (AND IS) NEGLECTED")	A5250
690 FORMAT (8F10.0)	A5260
700 FORMAT (16I5)	A5270
710 FORMAT (12F6.1)	A5280
720 FORMAT (1H1,//////17X,40H***** UNIFIED JET NOISE PREDICTION *****	A5290
1///32X,10HTEST POINT,14,///31X,13HOPTION NUMBER,13,///5X,20HRESERV	A5300
2OIR PRESSURE =,F6.2,28H PSI, ATMOSPHERIC PRESSURE =,F6.2,4H PSI,/1	

3X,23HRESERVOIR TEMPERATURE =,F7.1,29H DEG.F, CHAMBER TEMPERATURE = A5310  
 4,F7.1,3H DEG.F,/31X,7HGAMMA =,F5.2) A5320  
 730 FORMAT (//10X,22HPRESSURE RATIO PR/P0 =,F6.3,/10X,25HTEMPERATURE R A5330  
 ATIO TR/T0 =,F6.3,/10X,36HJET STATIC TEMPERATURE RATIO TJ/T0 =,F6. A5340  
 23,/10X,25HJET DENSITY RATIO DJ/D0 =,F6.3,/10X,26HJET VELOCITY RATI A5350  
 30 VJ/A0 =,F6.3,/10X,20HJET MACH NUMBER MJ =,F6.3,/10X,17HJET VELOC A5360  
 4ITY VJ =,F7.1,4H FPS) A5370  
 740 FORMAT (//10X,17HNOZZLE DIAMETER =,F6.2,7H INCHES,/10X,21HMICROPHO A5380  
 NE DISTANCE =,F6.2,5H FEET,/10X,5HR/D =,F6.2) A5390  
 750 FORMAT (//,10X,"TURBULENCE INTENSITY RADIAL HALF WIDTH = ",E13.6) A5400  
 760 FORMAT (10X,"RADIAL COHERENCE LENGTH SCALE COEFFICIENTS (A,B) = ", A5410  
 1E13.6," , ",E13.6) A5420  
 770 FORMAT (///10X,37H\*\*SHOCK ASSOCIATED NOISE PARAMETERS\*\*,///10X,3HC A5430  
 1 =,F5.2,5X,4HK0 =,F5.2,5X,4HK1 =,F5.2,/10X,21HNUMBER OF SHOCKS NS A5440  
 2=,I3) A5450  
 780 FORMAT (//10X,6HBETA =,F6.3,/10X,29HEDDY CONVECTION VELOCITY VC =, A5460  
 1F7.1,4H FPS,/10X,32HEDDY CONVECTION MACH NUMBER MC =,F6.3,/10X,30H A5470  
 2AVERAGE SHOCK CELL LENGTH L0 =,F7.3,7H INCHES,/10X,28HFIRST SHOCK A5480  
 3CELL LENGTH L1 =,F7.3,7H INCHES) A5490  
 790 FORMAT (1H1,////,5X,"NOISE FROM LARGE-SCALE TURBULENCE ","STRUCT A5500  
 URE",////,5X,"OBSERVER ANGLE =",F7.2," DEGREES",///,1X,3X,"FREQ(HZ) A5510  
 2",4X,"SPLA(DB)",16X,"SPLM(DB)",4X,"DIFF",9X,"SUM",/) A5520  
 800 FORMAT (1H1,////,5X,"NOISE FROM LARGE-SCALE TURBULENCE STRUCTURE" A5530  
 1,///,5X,16HOBSERVER ANGLE =,F7.2,8H DEGREES,///,1X,3X,"FREQ(HZ)",4X, A5540  
 2"SPLA(DB)"/) A5550  
 810 FORMAT (2X,2F10.1,14X,2(4X,F6.1),2X,F12.1) A5560  
 820 FORMAT (2X,F10.1,F10.1) A5570  
 830 FORMAT (//,40X,"STANDARD DEVIATION = ",F7.2) A5580  
 840 FORMAT (1H1,////,5X,"TURBULENT MIXING NOISE (BOPNO =",I2,"") A5590  
 850 FORMAT (/,T2,"\*\*\* ALTERNATIVE AXIAL SOURCE LOCATION MODEL ","UTILI A5600  
 IZED \*\*\*) A5610  
 860 FORMAT (/,T2,"\*\*\* DISPLACEMENT SOURCE MODEL \*\*\*) A5620  
 870 FORMAT (///,5X,"OBSERVER ANGLE =",F7.2," DEGREES",///,1X,3X,"FREQ( A5630  
 1HZ)",4X,"FD/VJ",6X,"SM",5X,"SPLPQ(DB)",1X,"SPLPD(DB)",2X,"SPLB(DB) A5640  
 2",16X,"SPLM(DB)",4X,"DIFF",9X,"SUM",/) A5650  
 880 FORMAT (///,5X,16HOBSERVER ANGLE =,F7.2,8H DEGREES,///,1X,3X,"FREQ( A5660  
 1HZ)",4X,"FD/VJ",6X,"SM",5X,"SPLPQ(DB)",1X,"SPLPD(DB)",2X,"SPLB(DB) A5670  
 2"/) A5680  
 890 FORMAT (1X,F10.1,2F10.3,3F10.1,2X,A2,10X,2(4X,F6.1),2X,F12.1) A5690  
 900 FORMAT (1X,F10.1,2F10.3,3F10.1,2X,A2) A5700  
 910 FORMAT (//,74X,"STANDARD DEVIATION = ",F7.2) A5710  
 920 FORMAT (1H1,////,5X,"SHOCK ASSOCIATED NOISE",///,5X,16HOBSERVER AN A5720  
 IGLE =,F7.2,8H DEGREES,///) A5730  
 930 FORMAT (1X,3X,"FREQ(HZ)",3X,"SIGMA",3X,"H0(DB)",3X,"C1",3X,"ANS3(D A5740  
 1B)",3X,"ANS2(DB)",5X,"SPLC(DB)",16X,"SPLM(DB)",4X,"DIFF",9X,"SUM", A5750  
 2/) A5760  
 940 FORMAT (1X,3X,"FREQ(HZ)",3X,"SIGMA",3X,"H0(DB)",3X,"C1",3X,"ANS3(D A5770  
 1B)",3X,"ANS2(DB)",5X,"SPLC(DB)"/) A5780  
 950 FORMAT (2X,F10.1,3X,F5.2,3X,F6.1,2X,F4.2,2X,F7.1,4X,F7.1,5X,F7.1,1 A5790  
 15X,2(4X,F6.1),2X,F12.1) A5800  
 960 FORMAT (2X,F10.1,3X,F5.2,3X,F6.1,2X,F4.2,2X,F7.1,4X,F7.1,5X,F7.1) A5810  
 970 FORMAT (//,85X,"STANDARD DEVIATION = ",F7.2) A5820  
 980 FORMAT (1H1,////,5X,"TOTAL NOISE",///,5X,16HOBSERVER ANGLE =,F7.2, A5830  
 18H DEGREES,///) A5840  
 990 FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLA(DB)",2X,"SPLB(DB)",2X,"SPLT(DB)" A5850  
 1,19X,"SPLM(DB)",19X,"DIFF",13X,"SUMDIFF",/) A5860  
 1000 FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLA(DB)",2X,"SPLB(DB)",2X,"SPLT(DB)" A5870  
 1,/) A5880  
 1010 FORMAT (2X,4F10.1,19X,F10.1,14X,F6.1,8X,F12.1) A5890



1020	FORMAT (2X,4F10.1)	A5900
1030	FORMAT (//,T79,"STANDARD DEVIATION = ",F6.1)	A5910
1040	FORMAT (1H1,//////5X,"TOTAL NOISE",///5X,16HOBSEVER ANGLE =,F7.2, 18H DEGREES,///)	A5920
1050	FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLB(DB)",2X,"SPLC(DB)",2X,"SPLT(DB)" 1,16X,"SPLM(DB)",4X,"DIFF",9X,"SUM",/)	A5930
1060	FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLB(DB)",2X,"SPLC(DB)",2X,"SPLT(DB)" 1/)	A5940
1070	FORMAT (2X,4F10.1,16X,2(4X,F6.1),2X,F12.1)	A5950
1080	FORMAT (2X,4F10.1)	A5960
1090	FORMAT (//,T64,"STANDARD DEVIATION = ",F6.1)	A5970
1100	FORMAT (1H1,//////5X,"TOTAL NOISE",///5X,16HOBSEVER ANGLE =,F7.2, 18H DEGREES,///1X,4X,"FREQ(HZ)",3X,"SPLA(DB)",2X,"SPLC(DB)",2X,"SPL 2T(DB)"/)	A5980
1110	FORMAT (2X,4F10.1)	A5990
1120	FORMAT (1H1,//////5X,"TOTAL NOISE",///5X,16HOBSEVER ANGLE =,F7.2, 18H DEGREES,///)	A6000
1130	FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLA(DB)",2X,"SPLB(DB)",2X,"SPLC(DB)" 1,2X,"SPLT(DB)",16X,"SPLM(DB)",4X,"DIFF",9X,"SUM",/)	A6010
1140	FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLA(DB)",2X,"SPLB(DB)",2X,"SPLC(DB)" 1,2X,"SPLT(DB)"/)	A6020
1150	FORMAT (2X,5F10.1,15X,2(4X,F6.1),2X,F12.1)	A6030
1160	FORMAT (2X,5F10.1)	A6040
1170	FORMAT (//,T71,"STANDARD DEVIATION = ",F6.1)	A6050
	END	A6060
		A6070
		A6080
		A6090
		A6100
		A6110
		A6120
		A6130
		A6140-

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*DECK CALPER
SUBROUTINE CALPER (VJAO,TJTO,P0,T0F,TRF,PRG,TRK,TRTO,PRP0,PRGA,DJD
10,MJ,A0,VJ,GAMA,OPPER)
REAL MJ
INTEGER OPFER
DIMENSION GAM(11)
IF (OPPER.EQ.1) GO TO 30
C
C
C
CALCULATIONS FROM INPUT OF TJTO,VJAO,T0F,AND P0
TRK=5./9.*(T0F+460.0)*TJTO
TOK=(5.0*(T0F+460.0))/9.0
GAMA0=1.421-(TOK/11800.0)*(EXP(-ABS(TOK-450.0)/200.0)/80.0)
IF (TOK.LE.290.0) GAMA0=1.402
A0=SQRT(GAMA0*1716.8*(T0F+460.0))
TJK=TJTO*TOK
GAMAJ=1.421-(TJK/11800.0)*(EXP(-ABS(TJK-450.0)/200.0)/80.0)
IF (TJK.LE.290.0) GAMAJ=1.402
GJGO=GAMAJ/GAMA0
MJ=VJAO/SQRT(GJGO*TJTO)
VJ=VJAO*A0
DJDO=1.0/TJTO
GAM(1)=0.0
DO 10 I=2,11
GAM(I)=1.421-(TRK/11800.0)*(EXP(-ABS(TRK-450.0)/200.0)/80.0)
IF (TRK.LE.290.0) GAM(I)=1.402
PRGA=1.0*((GAM(I)-1.0)/2.0*MJ**2)
PRP0=PRGA*((GAM(I)/(GAM(I)-1.0))
TRTO=TJTO*PRGA
TRK=5./9.*(T0F+460.0)*TRTO
PRG=(PRP0-1.0)*P0
TRF=TRTO*(T0F+460.0)-460.0
DIFF=ABS(GAM(I)-GAM(I-1))
JJ=I
IF (DIFF.LE.0.0001) GO TO 20
10 CONTINUE
WRITE (6,40)
STOP 100
20 GAMA=GAM(JJ)
RETURN
C
C
C
CALCULATIONS FROM INPUT OF P0,T0F,PRG, AND TRF
30 PRP0=(PRG/P0)+1.0
TRTO=(TRF+460.0)/(T0F+460.0)
TRK=(5.0*(TRF+460.0))/9.0
GAMA=1.421-(TRK/11800.0)*(EXP(-ABS(TRK-450.0)/200.0)/80.0)
IF (TRK.LE.290.0) GAMA=1.402
PRGA=PRP0*((GAMA-1.0)/GAMA)
MJ=SQRT((2.0/(GAMA-1.0))*(PRGA-1.0))
TJTO=TRTO/PRGA
DJDO=1.0/TJTO
TOK=(5.0*(T0F+460.0))/9.0
GAMA0=1.421-(TOK/11800.0)*(EXP(-ABS(TOK-450.0)/200.0)/80.0)
IF (TOK.LE.290.0) GAMA0=1.402
A0=SQRT(GAMA0*1716.8*(T0F+460.0))
TJK=TJTO*TOK
GAMAJ=1.421-(TJK/11800.0)*(EXP(-ABS(TJK-450.0)/200.0)/80.0)
IF (TJK.LE.290.0) GAMAJ=1.402

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GJG0=GAMAJ/GAMA0  
VJA0=MJ\*SQRT(GJG0\*TJT0)  
VJ=VJA0\*A0  
RETURN

B 590  
B 600  
B 610  
B 620  
B 630  
B 640  
B 650  
B 660-

C

40 FORMAT (///,IX,"\*\*\*\* THE GAMA ITERATION FAILED TO CONVERGE ", "AFT  
IER 10 TRIES. COMPUTATION STOPPED - CHECK INPUT. \*\*\*\*")  
END

*DECK	LSMAIN	C	10
	SUBROUTINE LSMAIN (VJA,TJT,GAMA,DFT,VJ,F,I,NANG,TH,IFN,SPLLS)	C	20
C		C	30
C	THIS PROGRAM IS AN INTERMEDIATE STEP BETWEEN UNIMAIN AND	C	40
C	LSNOISE TO HANDLE INITIALIZATION AND ERROR PROCESSING	C	50
		C	60
	DIMENSION TM(20),PTHETA(20),PDB(20),SPLLS(30,20)	C	70
	COMPLEX ALPHA,OKDB	C	80
	REAL MACH2,MLS	C	90
	INTEGER GAMMA	C	100
	COMMON/INFO/ALPHA,OMEGA,MACH2,TJT0,NORD,GM1,OKDB,IFLG,VJA0	C	110
	TJT0=TJT	C	120
	VJA0=VJA	C	130
	IFLG=IFN	C	140
	B0=0.05	C	150
	GAMMA=8	C	160
	INF=0	C	170
	RADNF=0.	C	180
	RSTART=0.	C	190
	XLAST=0.	C	200
	FREQ=F	C	210
	IEROR=0	C	220
	SN=F*DFT/VJ	C	230
	MLS=17.2*ALOG10(10.0*SN)	C	240
	CLS=74.13*SN**(-0.136)	C	250
	CAL=MLS*10.0*ALOG10(VJA0)*CLS	C	260
	IF (VJA0.LT.1.15) GO TO 20	C	270
	IF (SN.LT.0.1.OR.SN.GT.0.5) GO TO 40	C	280S
	CALL LSNOIS (FREQ,TH,NANG,GAMA,DFT,VJ,B0,GAMMA,INF,RADNF,XLAST,RST	C	290
	IART,PTHETA,PDB,IEROR)	C	300
	IF (IEROR.EQ.1) RETURN	C	310
	IF (IEROR.EQ.2) GO TO 60	C	320
	DO 10 J=1,NANG	C	330
	SPLLS(I,J)=PDB(J)*CAL	C	340
	IF (TM(J).LT.15.0.OR.TM(J).GT.45.0) SPLLS(I,J)=3.0	C	350
10	CONTINUE	C	360
	RETURN	C	370
20	DO 30 J=1,NANG	C	380
30	SPLLS(I,J)=2.0	C	390
	RETURN	C	400
40	DO 50 J=1,NANG	C	410
50	SPLLS(I,J)=4.0	C	420
	RETURN	C	430
60	DO 70 J=1,NANG	C	440
70	SPLLS(I,J)=5.0	C	450
	RETURN	C	460-
	END		



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*DECK LSNOISE
SUBROUTINE LSNOIS (FREQ,TM,NANG,GAMA,DFT,VJ,B0,GAMMA,INF,RADNF,XLA D 10
1ST,RSTART,PTHETA,PDB,IEROR) D 20
DIMENSION TM(NANG),PTHETA(NANG),PDB(NANG) D 30
***** D 40
C * D 50
C * THIS PROGRAM DETERMINES THE GROWTH OF PRESSURE * D 60
C * FLUCTUATIONS IN A DIVERGING, COMPRESSIBLE * D 70
C * AXISYMMETRIC JET. * D 80
C * D 90
***** D 100
COMPLEX PY(3),Y(3),DY(3),P(3),Q(3),ACON(130),BB(130),ALPHA D 110
COMPLEX BB4,CSTEP,LIM(6),RADC,RAD,DIR(6) D 120
COMPLEX UVAL,DUVAL,CVAL,LAMDAM,LAMDAP,ETAC D 130
COMPLEX RHO,DRHO,AC,PP,DPP,ADAT(100),CDAT(100) D 140
COMPLEX DUDS,D2UDRS,DRDS,D2RDRS D 150
COMPLEX HSUM(2,3,2),ISUM(2,2),DUMH(3),DUM,DUM1,L1,L2 D 160
COMPLEX DKDB D 170
COMPLEX ARG,H01,H02,H11,H12,I0,I1 D 180
COMPLEX E0,E1,E2,E3,A2,A4 D 190
REAL MACH2 D 200
INTEGER GAMMA D 210
DIMENSION SDAT(100) D 220
COMMON/INFO/ALPHA,OMEGA,MACH2,TJTO,NORD,GM1,DKDB,IFLG,VJAO D 230
COMMON/SPR/HTHETA,S,KEY1,UCENT,DUDDS,BETA1,BETA2,IFUNC D 240
COMMON/DECAY/ ID,SD D 250
SMIN1=2.5E-4 D 260
SMAX1=.05 D 270
ERMIN=.1 D 280
ERMAX=.14 D 290
ERMIN=.1 D 300
ERMAX=.14 D 310
PI=3.14159265 D 320
A=.693147 D 330
STRNO=FREQ*DFT/VJ D 340
NTT=0 D 350
ID=0 D 360
SD=1000. D 370
C D 380
C SET UP CONDITIONS FOR STABILITY CALCULATION D 390
C D 400
C STARTING RADIUS D 410
RST1=0.05 D 420
C FINISHING RADIUS D 430
RFIN=4. D 440
C DIMENSIONS OF COMPLEX CONTOUR DEFORMATION D 450
ETA11=0.5 D 460
ETA21=0.5 D 470
C NUMBER OF THICKNESSES TO BE CALCULATED D 480
NLIM=70 D 490
C 3* VARIATION IN PERCENTAGE FOR WAVENUMBER GUESSES D 500
PERCR=0.005 D 510
PERCI=0.005 D 520
C THICKNESS STEP SIZE D 530
DS=0.005/STRNO D 540
C STARTING THICKNESS FOR BOUNDARY LAYER D 550
S=0.05-DS D 560
C SET UP CALCULATED VALUE OF MODENUMBER D 570
NORD=1 D 580

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	AN=FLOAT(NORD)	D 590
	GM1=GAMA-1	D 600
	MACH2=VJA0*VJA0	D 610
	NORD1=NORD*1	D 620
10	S=S*DS	D 630
C		D 640
C	ADJUST MINIMUM AND MAXIMUM STEP SIZES TO THE LOCAL WIDTH	D 650
C		D 660
	SMIN=SMIN1*S	D 670
	SMAX=SMAX1*S	D 680
	IF (SMIN.GT.SMIN1) SMIN=SMIN1	D 690
	IF (SMAX.LT.SMAX1) SMAX=SMAX1	D 700
	ETA1=ETA11*S	D 710
	ETA2=ETA21*S	D 720
C		D 730
C	CALCULATE THE LOCAL POTENTIAL CORE RADIUS	D 740
C	OR THE CENTERLINE VELOCITY	D 750
C		D 760
	KEY1=3	D 770
	BETA1=0.	D 780
	BETA2=0.	D 790
	UCENT=1.	D 800
	RAD=CMPLX(-.0125,0.)	D 810
	DO 20 I=1,161	D 820
	RAD=RAD*.025	D 830
	CALL UEVAL (RAD,UVAL,DUVAL,DUDS,D2UDRS,RHO,DRHO,DRDS,D2RDRS)	D 840
	VAL=REAL(RHO*UVAL*UVAL)	D 850
	BETA1=BETA1+VAL*.025	D 860
	BETA2=BETA2+VAL*REAL(RAD)*.025	D 870
	IF (ABS(VAL).LT.1.E-5) GO TO 30	D 880
20	CONTINUE	D 890
C		D 900
C	CALCULATION OF THE POTENTIAL CORE RADIUS	D 910
C		D 920
30	VAL=S*S*((TJT0*BETA1)**2-2.*TJT0*BETA2)+1.	D 930
	IF (VAL) 70,40,40	D 940
40	VAL=-S*BETA1*TJT0+SQRT(VAL)	D 950
	IF (VAL) 70,50,50	D 960
50	HTHETA=VAL	D 970
	KEY1=1	D 980
	IF (HTHETA.LT.RST1) GO TO 60	D 990
	RST=HTHETA*.1E-10	D1000
	GO TO 150	D1010
60	RST=RST1	D1020
	GO TO 150	D1030
C		D1040
C	CALCULATION OF THE CENTERLINE VELOCITY	D1050
C		D1060
70	KEY1=4	D1070
80	BETA2=0.	D1080
	RAD=CMPLX(-.0125,0.)	D1090
	USAVE=UCENT	D1100
	DO 90 I=1,161	D1110
	RAD=RAD*.025	D1120
	CALL UEVAL (RAD,UVAL,DUVAL,DUDS,D2UDRS,RHO,DRHO,DRDS,D2RDRS)	D1130
	VAL=REAL(RHO*UVAL*UVAL)	D1140
	BETA2=BETA2+VAL*REAL(RAD)*.025	D1150
	IF (ABS(VAL).LT.1.E-5) GO TO 100	D1160
90	CONTINUE	D1170

100	UCENT=1./SQRT(2.*TJT0*BETA2)/S	D1180
	IF (ABS(UCENT-USAVE).LT.1.E-4) GO TO 110	D1190
	GO TO 80	D1200
C		D1210
C	CALCULATION OF RATE OF CHANGE OF CENTERLINE VELOCITY	D1220
C	WITH LOCAL THICKNESS	D1230
C		D1240
110	AA=GM1*MACH2/2.	D1250
	BA=(1.-TJT0-AA)	D1260
	AK=SQRT(BA*BA+4.*AA)	D1270
	IF (VJA0.LT.1.E-10) GO TO 120	D1280
	DUCDS=-((AA*UCENT+BA)*UCENT-1.)*(ALOG(ABS((AA*UCENT+BA)*UCENT-1.)))	D1290
	1-BA*ALOG(ABS((2.*AA*UCENT+BA-AK)*(BA+AK)/(2.*AA*UCENT+BA+AK)/(BA-A	D1300
	2K)))/AK)/UCENT/S/AA	D1310
	GO TO 140	D1320
120	BA=1.-TJT0	D1330
	IF (ABS(BA).LT.1.E-10) GO TO 130	D1340
	DUCDS=2.*(1.-BA*UCENT)*(BA*UCENT+ALOG(ABS(1.-BA*UCENT)))/S/UCENT/B	D1350
	1A/BA	D1360
	GO TO 140	D1370
130	DUCDS=-UCENT/S	D1380
140	KEY1=2	D1390
	GO TO 160	D1400
150	YMAX=RFIN*S*HMHETA	D1410
	GO TO 170	D1420
160	YMAX=RFIN*S	D1430
170	CONTINUE	D1440
C		D1450
C	READ IN OR INTERPOLATE FOR THE GUESSED VALES OF ALPHA	D1460
C		D1470
	IF (NTT.EQ.NLIM) GO TO 710	D1480
	IF (NTT.EQ.0) GO TO 190	D1490
	ALPHA=ALPHA+DKDB*DS	D1500
C		D1510
C	CONVERGENCE SEARCH FOR DAMPED SUPERSONIC WAVE	D1520
C		D1530
	IF (AIMAG(ALPHA).LT.0.) GO TO 180	D1540
	IF ((OMEGA/REAL(ALPHA)).LT.(1./VJA0)) GO TO 180	D1550
	ID=1	D1560
	SD=S-DS	D1570
	GO TO 710	D1580
180	ACON(1)=ALPHA	D1590
	ACON(2)=CMPLX((1.-PERCR)*REAL(ALPHA),(1.-PERCI)*AIMAG(ALPHA))	D1600
	ACON(3)=CMPLX((1.+PERCR)*REAL(ALPHA),(1.+PERCI)*AIMAG(ALPHA))	D1610
	NT=3	D1620
	GO TO 200	D1630
C		D1640
C	DETERMINE THE STARTING VALUES FROM TABULATION	D1650
C		D1660
190	CALL ASTART (VJA0,STRNO,TJT0,ALPHA,NORD,IEROR)	D1670S
	IF (IEROR.NE.2) GO TO 180	D1680
	RETURN	D1690
C		D1700
C	CALCULATE STROUHAL NUMBER AND RADIAN FREQUENCY	D1710
C		D1720
200	STRNO=FREQ*DFT/VJ	D1730
	OMEGA=STRNO*PI	D1740
	IF (IFLG.EQ.0) GO TO 210	D1750



	WRITE (6,740) NORD,VJA0,TJT0,STRNO,OMEGA,S	D1760*
210	IF (KEY1,EQ.2) GO TO 220	D1770
	IF (IFLG,EQ.0) GO TO 230	D1780
	WRITE (6,750) HTHETA	D1790*
	GO TO 230	D1800
220	IF (IFLG,EQ.0) GO TO 230	D1810
	WRITE (6,760) UCENT	D1820*
C		D1830
C	BEGIN THE INTEGRATION AND CALCULATE THE	D1840
C	STARTING VECTORS	D1850
C		D1860
230	KK=0	D1870
	IFUNC=1	D1880
	IF (IFLG,EQ.0) GO TO 240	D1890
	WRITE (6,830) BETA1,BETA2	D1900*
240	KK=KK+1	D1910
	ALPHA=ACON(KK)	D1920
C		D1930
C	IF KEY1 = 2 THE STARTING VECTORS ARE OBTAINED FROM A	D1940
C	SERIES SOLUTION	D1950
C		D1960
250	IF (KEY1,EQ.2) GO TO 290	D1970
	LAMDAM=CSQRT(ALPHA*ALPHA-MACH2*(ALPHA-OMEGA)*(ALPHA-OMEGA)/TJT0)	D1980
	DO 260 I=1,3	D1990
260	Y(I)=(0.,0.)	D2000
	Y(1)=CMPLX(RST,0.)	D2010
	ARG=LAMDAM*Y(1)	D2020
	PHI=ATAN2(AIMAG(ARG),REAL(ARG))	D2030
	IF (PHI,GT.=PI.AND,PHI,LE.PI/2.) GO TO 270	D2040
	ARG=ARG*(0.,-1.)	D2050
	CALL NCBRTS (ARG,H01,H02,NORD,0)	D2060S
	CALL NCBRTS (ARG,H11,H12,NORD1,0)	D2070S
	I0=CEXP((0.,1.)*AN*PI/2.)*H01	D2080
	I1=CEXP((0.,1.)*(AN+1.)*PI/2.)*H11	D2090
	GO TO 280	D2100
270	ARG=ARG*(0.,1.)	D2110
	CALL NCBRTS (ARG,H01,H02,NORD,0)	D2120S
	CALL NCBRTS (ARG,H11,H12,NORD1,0)	D2130S
	I0=CEXP((0.,-1.)*AN*PI/2.)*H01	D2140
	I1=CEXP((0.,-1.)*(AN+1.)*PI/2.)*H11	D2150
280	Y(2)=I0	D2160
	Y(3)=AN*I0/Y(1)+LAMDAM*I1	D2170
	GO TO 300	D2180
C		D2190
C	SERIES SOLUTION FOR THE STARTING VECTORS	D2200
C		D2210
290	RHO=1./(1.-(1.-TJT0)*UCENT+0.5*GM1*MACH2*UCENT*(1.-UCENT))	D2220
	DRHO=-UCENT*RHO/RHO*(1.-TJT0-0.5*GM1*MACH2*(1.-2.*UCENT))	D2230
	D2RDR2=2.*DRHO*DRHO/RHO-DRHO*GM1*MACH2*RHO*RHO*UCENT*UCENT	D2240
	DUM=ALPHA*UCENT-OMEGA	D2250
	E0=(MACH2*DUM*DUM*RHO-ALPHA*ALPHA)	D2260
	E1=(4.*ALPHA*UCENT/DUM-2.*DRHO/RHO)*A/S/S	D2270
	E2=MACH2*DUM*(DUM*DRHO-2.*ALPHA*UCENT*RHO)*A/S/S	D2280
	E3=(4.*ALPHA*UCENT*OMEGA/DUM/DUM-2.*(D2RDR2-DRHO*DRHO/RHO)/RHO)*A*	D2290
	1A/S**4	D2300
	A2=-((E0+AN*E1)/4.)/(AN+1.)	D2310
	A4=-((E2+AN*E3+A2*(E0+(AN+2.)*E1))/8.)/(AN+2.)	D2320
	Y(1)=CMPLX(RST1,0.)	D2330
	Y(2)=Y(1)**NORD*(1.+Y(1)*Y(1)*(A2+A4*Y(1)*Y(1)))	D2340



	Y(J)=Y(1)**(NORD-1)*(AN*Y(1)*Y(1)**((AN*2.)*A2*(AN*4.)*A4*Y(1)*Y(1	D2350
	1))	D2360
300	M=3	D2370
C		D2380
C	IF IFUNC = 1. EIGENVALUE IS BEING CALCULATED	D2390
C	IF IFUNC = 2. DALPHA/DS IS BEING CALCULATED FROM THE	D2400
C	SOLVABILITY CONDITION	D2410
C		D2420
	IF (IFUNC.EQ.1) GO TO 320	D2430
	IF (KEY1.EQ.2) GO TO 310	D2440
	DUM=ALPHA-OMEGA	D2450
	MSUM(1,1,1)=(0.,0.)	D2460
	MSUM(2,1,1)=2.*(ALPHA-MACH2*DUM/TJT0)*Y(1)*Y(2)*Y(2)/DUM/DUM	D2470
	ISUM(1,1)=(0.,0.)	D2480
	ISUM(2,1)=(ALPHA-MACH2*DUM/TJT0)*Y(1)*Y(1)*(I0*I0-I1*I1-2.*AN*I0*I	D2490
	1/LAMDAM/Y(1))/DUM/DUM*TJT0	D2500
	GO TO 320	D2510
310	CALL UEVAL (Y(1),UVAL,DUVAL,DUDS,D2UDRS,RHO,DRHO,DRDS,D2RDRS)	D2520S
	DUM=ALPHA*UVAL-OMEGA	D2530
	MSUM(1,1,1)=(((D2RDRS-DRHO*DRDS/RHO)/RHO/RHO+2.*ALPHA*(D2UDRS-ALPH	D2540
	1A*DUVAL*DUDS/DUM)/RHO/DUM)*Y(3)/DUM/DUM-2.*MACH2*(DRDS/RHO*ALPHA*D	D2550
	2UDS/DUM)*Y(2))*Y(2)*Y(1)	D2560
	MSUM(2,1,1)=2.*(ALPHA-MACH2*DUM*RHO*UVAL)*Y(1)*Y(2)*Y(2)/DUM/DUM-2	D2570
	1.*OMEGA*DUVAL*Y(3)*Y(2)*Y(1)/DUM**4/RHO	D2580
	ISUM(1,1)=(0.,0.)	D2590
	ISUM(2,1)=(0.,0.)	D2600
320	INT=0	D2610
C		D2620
C	DETERMINE THE CONTOUR OF INTEGRATION=	D2630
C	LOCATE THE CRITICAL POINT	D2640
C		D2650
	IND=0	D2660
	DO 330 I=1,3	D2670
330	DIR(I)=(1.,0.)	D2680
	DO 340 I=4,6	D2690
340	DIR(I)=(-1.,0.)	D2700
	CVAL=OMEGA/ALPHA	D2710
	ETAC=CSQRT(-CLOG(CVAL/UCENT)/A)	D2720
	IF (KEY1.EQ.2) GO TO 350	D2730
	RADC=ETAC*S*HTheta	D2740
	GO TO 360	D2750
350	RADC=ETAC*S	D2760
360	IF (REAL(RADC).GT.(2.*RST1)) GO TO 370	D2770
	RST1=RST1/2.	D2780
	GO TO 250	D2790
370	TEMP1=AIMAG(RADC)*SIGN(ETA2,AIMAG(RADC))*SIGN(1.,-AIMAG(CVAL))	D2800
C		D2810
C	DECIDE WHETHER NECESSARY TO INTEGRATE AROUND	D2820
C	THE CRITICAL POINT	D2830
C		D2840
	IF (ABS(AIMAG(RADC)).GT.ETA2.AND.AIMAG(CVAL).GT.0.) GO TO 380	D2850
	DIR(2)=CMPLX(0.,SIGN(1.,TEMP1))	D2860
	DIR(5)=DIR(2)	D2870
C		D2880
C	DEFINE THE LIMITS OF THE CONTOUR INTEGRATION	D2890
C		D2900
	LIM(1)=CMPLX(REAL(RADC)-ETA1,0.)	D2910
	LIM(2)=CMPLX(REAL(RADC)-ETA1,TEMP1)	D2920
	LIM(5)=CMPLX(REAL(RADC)+ETA1,TEMP1)	D2930

LIM(4)=CMPLX(REAL(RADC)*ETA,0.)	D2940
LIM(3)=CMPLX(REAL(RADC),TEMP1)	D2950
LIM(6)=LIM(3)	D2960
IF (REAL(LIM(1)).GT.REAL(Y(1))) GO TO 400	D2970
LIM(1)=Y(1)	D2980
LIM(2)=CMPLX(REAL(Y(1)),AIMAG(LIM(2)))	D2990
IF (IFLG.EQ.0) GO TO 400	D3000
IF (IFUNC.EQ.2) WRITE (6,840) (LIM(I),I=1,6)	D3010*
GO TO 400	D3020
380 DO 390 I=1,6	D3030
390 LIM(I)=CMPLX(REAL(RADC),0.)	D3040
400 CONTINUE	D3050
C	D3060
C	D3070
C	D3080
PERFORM THE INTEGRATION	D3090
IWR=0	D3100
ISTEP=1	D3110
CSTEP=(0.,0.)	D3120
INT=0	D3130
K=1	D3140
H=SMIN*10.	D3150
IFL=1	D3160
410 PY(1)=Y(1)	D3170
PY(2)=Y(2)	D3180
PY(3)=Y(3)	D3190
420 IF (H.LT.SMIN) H=SMIN	D3200
IF (H.GT.SMAX) H=SMAX	D3210
IF (CABS(Y(1)-LIM(ISTEP)).GT.H) GO TO 430	D3220
H=CABS(Y(1)-LIM(ISTEP))	D3230
IF (IFL.EQ.1) IFL=2	D3240
IF (IFL.EQ.3) IFL=4	D3250
430 CSTEP=ABS(H)*DIR(ISTEP)	D3260S
CALL PJMRUN (M,CSTEP,Y,DY,P,Q,ERRES)	D3270
IND=IND+1	D3280
IF (ERRES.LT.ERMIN) GO TO 450	D3290
IF (ERRES.LT.ERMAX) GO TO 460	D3300
IF (H.LE.SMIN) GO TO 440	D3310
H=0.8*H	D3320
Y(1)=PY(1)	D3330
Y(2)=PY(2)	D3340
Y(3)=PY(3)	D3350
IF (IFL.EQ.2) IFL=1	D3360
IF (IFL.EQ.4) IFL=3	D3370
GO TO 420	D3380
440 IWR=1	D3390
GO TO 460	D3400
450 H=1.25*H	D3410
460 IF (IFUNC.EQ.1) GO TO 500	D3420
C	D3430
C	D3440
C	D3450S
CALCULATE INTEGRALS TO FIND DALPHA/DS	D3460
CALL UEVAL (Y(1),UVAL,DUVAL,DUDS,D2UDRS,RHO,DRHO,DRDS,D2RDRS)	D3470
DUM=ALPHA*UVAL-OMEGA	D3480
DUM1=Y(1)*Y(2)/DUM/DUM/RHO	D3490
J=2	D3500
IF (INT.EQ.1) J=3	D3510
HSUM(1,J,K)=DUM1*((D2RDRS/RHO-DRHO*DRDS/RHO/RHO+2.*ALPHA*(D2UDRS/D	D3520
1UM-ALPHA*DUVAL*DUDS/DUM/DUM))*Y(3)-2.*MACH2*DUM*(DUM*DRDS*ALPHA*RH	
20*DUDS)*Y(2))	

	HSUM(2,J,K)=DUM1*2.*(ALPHA=MACH2*DUM*RHO*UVAL)*Y(2)-OMEGA*DUVAL*Y	D3530
	1(3)/DUM/DUM)	D3540
	IF (J,EQ,3) GO TO 470	D3550
	L1=CSTEP	D3560
	IF (K,EQ,2) L1=-L1	D3570
	INT=1	D3580
	GO TO 500	D3590
470	L2=CSTEP	D3600
	IF (K,EQ,2) L2=-L2	D3610
	DO 490 J=1,2	D3620
	DO 480 I=1,3	D3630
480	DUMH(I)=HSUM(J,I,K)	D3640
	DUM1=ISUM(J,K)	D3650
	CALL INTEG (DUMH,DUM1,L1,L2)	D3660S
	ISUM(J,K)=DUM1	D3670
490	HSUM(J,1,K)=HSUM(J,3,K)	D3680
	INT=0	D3690
500	GO TO (410,510,410,550), IFL	D3700
510	Y(1)=LIM(ISTEP)	D3710
	IF (IFUNC,EQ,1) GO TO 530	D3720
	IF (INT,EQ,0) GO TO 530	D3730
	DO 520 I=1,2	D3740
	ISUM(I,1)=ISUM(I,1)+0.5*L1*(HSUM(I,1,1)+HSUM(I,2,1))	D3750
520	HSUM(I,1,1)=HSUM(I,2,1)	D3760
	INT=0	D3770
	GO TO 530	D3780
530	ISTEP=ISTEP+1	D3790
	IF (ISTEP,GT,3) GO TO 540	D3800
	IF (CABS(Y(1)-LIM(ISTEP)).LT,.1,E-10) GO TO 510	D3810
	IFL=1	D3820
	GO TO 410	D3830
C		D3840
C	STORE FUNCTION AND DERIVATIVE FOR MATCHING LATER	D3850
C		D3860
540	PP=Y(2)	D3870
	DPP=Y(3)	D3880
	GO TO 580	D3890
550	Y(1)=LIM(ISTEP)	D3900
	IF (IFUNC,EQ,1) GO TO 570	D3910
	IF (INT,EQ,0) GO TO 570	D3920
	DO 560 I=1,2	D3930
	ISUM(I,2)=ISUM(I,2)+0.5*L1*(HSUM(I,1,2)+HSUM(I,2,2))	D3940
560	HSUM(I,1,2)=HSUM(I,2,2)	D3950
	INT=0	D3960
570	ISTEP=ISTEP+1	D3970
	IF (ISTEP,GT,6) GO TO 600	D3980
	IF (CABS(Y(1)-LIM(ISTEP)).LT,.1,E-20) GO TO 550	D3990
	IFL=3	D4000
	GO TO 410	D4010
C		D4020
C	STARTING CONDITIONS OUTSIDE THE JET	D4030
C		D4040
580	Y(1)=CMPLX(YMAX,0.)	D4050
	LAMDAP=CSQRT(MACH2*OMEGA*OMEGA-ALPHA*ALPHA)	D4060
	IF (AIMAG(LAMDAP).GT,0.) GO TO 590	D4070
	LAMDAP=-LAMDAP	D4080
590	ARG=LAMDAP*Y(1)	D4090
	CALL NCBRTS (ARG,H01,H02,NORD,1)	D4100S
	CALL NCBRTS (ARG,H11,H12,NORD1,1)	D4110S

Y(2)=H01	D4120
Y(3)=AN*H01/YMAX-LAMDAP*H11	D4130
IFL=3	D4140
IF (IFUNC, EQ.1) GO TO 410	D4150
MSUM(1,1,2)=(0.,0.)	D4160
MSUM(2,1,2)=2.*ALPHA*Y(1)*Y(2)*Y(2)/OMEGA/OMEGA	D4170
ISUM(1,2)=(0.,0.)	D4180
ISUM(2,2)=-ALPHA*Y(1)*Y(1)*(H01*H01+H11*H11-2.*AN*H01*H11/LAMDAP/Y	D4190
1(1))/OMEGA/OMEGA	D4200
INT=0	D4210
K=2	D4220
GO TO 410	D4230
C	D4240
C	D4250
C	D4260
600 BB4=Y(3)*PP-Y(2)*DpP	D4270
AC=Y(2)/PP	D4280
IF (IFUNC, EQ.1) GO TO 620	D4290
IF (IFLG, EQ.0) GO TO 610	D4300
WRITE (6,810) AC	D4310*
C	D4320
C	D4330
C	D4340
610 ISUM(1,1)=AC*AC*ISUM(1,1)+ISUM(1,2)	D4350
ISUM(2,1)=AC*AC*ISUM(2,1)+ISUM(2,2)	D4360
DKDB=-ISUM(1,1)/ISUM(2,1)	D4370
IF (IFLG, EQ.0) GO TO 10	D4380
WRITE (6,820) DKDB	D4390*
GO TO 10	D4400
620 BB(KK)=BB4	D4410
IF (IFLG, EQ.0) GO TO 630	D4420
WRITE (6,770) IND, ACON(KK), BB(KK)	D4430*
630 IF (KK, LT. NT) GO TO 240	D4440
C	D4450
C	D4460
C	D4470
CALL LAGRAN (KK, ACON, ALPHA, BB)	D4480S
IF (NTT, EQ.0) ALPHA=CMPLX(REAL(ALPHA), -ABS(AIMAG(ALPHA)))	D4490
ACON(KK+1)=ALPHA	D4500
IF (ABS(REAL(ACON(KK+1))), LT. 1.E-5) GO TO 640	D4510
IF (ABS(1.-REAL(ACON(KK))/REAL(ACON(KK+1))), GT. 0.005) GO TO 680	D4520
GO TO 650	D4530
640 WRITE (6,850)	D4540*
650 IF (ABS(AIMAG(ACON(KK+1))), LT. 1.E-5) GO TO 660	D4550
IF (ABS(1.-AIMAG(ACON(KK))/AIMAG(ACON(KK+1))), GT. 0.005) GO TO 680	D4560
GO TO 670	D4570
660 WRITE (6,860)	D4580*
GO TO 690	D4590
670 CONTINUE	D4600
GO TO 690	D4610
680 IF (KK, LT. 15) GO TO 240	D4620
IEROR=1	D4630
RETURN	D4640
690 IF (IFLG, EQ.0) GO TO 700	D4650
WRITE (6,780) ALPHA	D4660*
700 NTT=NTT+1	D4670
ADAT(NTT)=ALPHA	D4680
SDAT(NTT)=S	D4690
CDAT(NTT)=AC	D4700



IFUNC=2	D4710
GO TO 240	D4720
710 CONTINUE	D4730
IF (IFLG.EQ.0) GO TO 730	D4740
WRITE (6,790) VJAO	D4750*
DO 720 I=1,NTT	D4760
720 WRITE (6,800) SDAT(I),ADAT(I),CDAT(I)	D4770*
730 CONTINUE	D4780
CALL DIRECT (ADAT,NTT,DS,TH,NANG,BO,GAMMA,INF,RADNF,XLAST,RSTART,P	D4790S
1THETA,PDB)	D4800
RETURN	D4810
C	D4820
740 FORMAT (1H1,10X,"INVISCID AXISYMMETRIC JET STABILITY CALCULATION"/	D4830
111X,"*****"/22X,"MODE N	D4840
2UMBER = ",I1//22X,"MACH NUMBER = ",F10.4//22X,"TEMPERATURE RATIO =	D4850
3 ",F10.4//22X,"STROUHAL NUMBER = ",F10.4//22X,"FREQUENCY = ",F10.4	D4860
4//22X,"THICKNESS = ",F10.4//)	D4870
750 FORMAT (22X,"POTENTIAL CORE RADIUS = ",F10.4//)	D4880
760 FORMAT (22X,"JET CENTERLINE VELOCITY = ",F10.4//)	D4890
770 FORMAT (1X,15,4X,"ALPHA = ",2E11.5,2X,"GIVES B4 = ",2E11.5/)	D4900
780 FORMAT (21X,"WAVENUMBER = ",2F14.9//)	D4910
790 FORMAT (1H1,30X,"MACHNO = ",F10.4//3X,"THICKNESS",15X,"ALPHA",25X	D4920
1,"C"//)	D4930
800 FORMAT (1X,E11.5,4(2E11.5))	D4940
810 FORMAT (30X,"C = ",2F14.9/)	D4950
820 FORMAT (25X,"DK/DS = ",2E12.5//)	D4960
830 FORMAT (1X,"BETA1 = ",F10.5,5X,"BETA2 = ",F10.5//)	D4970
840 FORMAT (1X,4(1X,2E14.7))	D4980
850 FORMAT (1X,"REAL PART OF ALPHA TOO SMALL FOR CONVERGENCE TEST"/)	D4990
860 FORMAT (1X,"IMAGINARY PART OF ALPHA TOO SMALL FOR CONVERGENCE ", "T	D5000
EST, ITERATIONS COMPLETED"/)	D5010
END	D5020-

```

*DECK PJMRUN
SUBROUTINE PJMRUN (M,H,Y,DY,P,Q,ERRES)
  COMPLEX Y(M),DY(M),P(M),Q(M),RR(8),H
  DO 10 I=1,M
10  Q(I)=(0.,0.)
    DY(1)=(1.,0.)
    DO 20 I=2,M
20  DY(I)=(0.,0.)
    CALL DERY (M,Y,DY)
    DO 30 I=1,M
    P(I)=H*DY(I)*0.5
    RR(I)=(P(I)-Q(I)+Y(I))-Y(I)
    Y(I)=Y(I)+RR(I)
30  Q(I)=(3.*Q(I))-P(I)+(3.*RR(I))
    CALL DERY (M,Y,DY)
    DO 40 I=1,M
    P(I)=H*DY(I)
    RR(I)=((P(I)-Q(I))*0.5+Y(I))-Y(I)
    Y(I)=Y(I)+RR(I)
40  Q(I)=(3.*P(I))-(2.*Q(I))-(6.*RR(I))
    CALL DERY (M,Y,DY)
    ERRES=0.
    DO 60 I=1,M
    IF (CABS(P(I)-Q(I)).LT.1.E-20) GO TO 50
    E=CABS(((H*DY(I))-P(I))/(P(I)-Q(I)))
    IF (E.GT.ERRES) ERRES=E
50  P(I)=H*DY(I)-0.5*P(I)
    RR(I)=(P(I)+Y(I))-Y(I)
    Y(I)=Y(I)+RR(I)
60  Q(I)=Q(I)+6.*(P(I)-RR(I))
    CALL DERY (M,Y,DY)
    DO 70 I=1,M
    P(I)=(-4.*P(I)+H*DY(I)+Q(I))/6.
    RR(I)=(P(I)+Y(I))-Y(I)
    Y(I)=Y(I)+RR(I)
70  Q(I)=RR(I)-P(I)
    RETURN
  END

```

```

E 10
E 20
E 30
E 40
E 50
E 60
E 70
E 80S
E 90
E 100
E 110
E 120
E 130
E 140S
E 150
E 160
E 170
E 180
E 190
E 200S
E 210
E 220
E 230
E 240
E 250
E 260
E 270
E 280
E 290
E 300S
E 310
E 320
E 330
E 340
E 350
E 360
E 370-

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•DECK DERY	
SUBROUTINE DERY (M,Y,DY)	F 10
COMPLEX Y(M),DY(M),ALPHA,UVAL,DUVAL,RHO,DRHO	F 20
COMPLEX DUDS,D2UDRS,DRDS,D2RDRS,DUM	F 30
COMPLEX DKDB	F 40
REAL MACH2	F 50
COMMON/INFO/ALPHA,OMEGA,MACH2,TJTO,NORD,GM1,DKDB,IFLG,VJAO	F 60
COMMON/SPR/HTHETA,S,KEY1,UCENT,UCDS,BETA1,BETA2,IFUNC	F 70
AN=NORD	F 80
CALL UEVAL (Y(1),UVAL,DUVAL,DUDS,D2UDRS,RHO,DRHO,DRDS,D2RDRS)	F 90
DUM=ALPHA*UVAL-OMEGA	F 100
DY(2)=Y(3)	F 110
DY(3)=(DRHO/RHO+2.*ALPHA*DUVAL/DUM-1./Y(1))*Y(3)+(ALPHA*ALPHA-MACH	F 120
12*DUM*DUM*RHO*AN*AN/Y(1)/Y(1))*Y(2)	F 130
RETURN	F 140
END	F 150-





•DECK LAGRAN		
SUBROUTINE LAGRAN (NUM,C,CVAL,B4)		H 10
COMPLEX C(10),B4(10),CVAL,CONT,CMIN		H 20
DO 20 JJ=1,2		H 30
N=NUM-JJ		H 40
CMIN=B4(N)		H 50
JN=N		H 60
DO 10 I=1,N		H 70
K=NUM-I-JJ+1		H 80
IF (CABS(CMIN),LE,CABS(B4(K))) GO TO 10		H 90
JN=K		H 100
CMIN=B4(K)		H 110
10 CONTINUE		H 120
IF (JN,EQ,N) GO TO 20		H 130
B4(JN)=B4(N)		H 140
B4(N)=CMIN		H 150
CMIN=C(N)		H 160
C(N)=C(JN)		H 170
C(JN)=CMIN		H 180
20 CONTINUE		H 190
CVAL=(0.,0.)		H 200
DO 40 J=N,NUM		H 210
CONT=(1.,0.)		H 220
DO 30 I=N,NUM		H 230
IF (I,EQ,J) GO TO 30		H 240
CONT=CONT*(B4(I)/(B4(J)-B4(I)))		H 250
30 CONTINUE		H 260
40 CVAL=CVAL+C(J)*CONT		H 270
RETURN		H 280
END		H 290-

*DECK NCBRTS		I 10
SUBROUTINE NCBRTS (Z,B1,B2,N,M)		I 20
COMPLEX Z,M1(50),M2(50),B1,B2		I 30
IF (M.EQ.0) GO TO 20		I 40
IF (N.EQ.0.OR.N.EQ.1) GO TO 20		I 50S
CALL CBRTS (Z,M1(1),M2(1),0,1)		I 60S
CALL CBRTS (Z,M1(2),M2(2),1,1)		I 70
NP1=N+1		I 80
DO 10 J=3,NP1		I 90
M1(J)=2.*(J-2)*M1(J-1)/Z-M1(J-2)		I 100
10 M2(J)=2.*(J-2)*M2(J-1)/Z-M2(J-2)		I 110
B1=M1(NP1)		I 120
B2=M2(NP1)		I 130
RETURN		I 140S
20 CALL CBRTS (Z,B1,B2,N,M)		I 150
RETURN		I 160-
END		

•DECK CERTS		
SUBROUTINE CBRTS (Z,H1,H2,N,M)		J 10
DIMENSION AJ(1000)		J 20
COMPLEX Z,CON,F2,SUM,AJN,AYN,FCT,FCD,H1,H2		J 30
AN=N		J 40
R=CABS(Z)		J 50
IF (R.GT.6.6) GO TO 60		J 60
IF (R.GE..1E-30) GO TO 10		J 70
THETA=0.		J 80
GO TO 20		J 90
10 THETA=ATAN2(AIMAG(Z),REAL(Z))		J 100
20 CONTINUE		J 110
THN=AN*THETA		J 120
CON=CMPLX(COS(THN),SIN(THN))		J 130
F1=-1.		J 140
F2=CMPLX((COS(2.*THETA)-1.),SIN(2.*THETA))		J 150
F3=R/2.		J 160
FAC=1.		J 170
LIM=29-N		J 180
CALL BSSLS (R,AJ,29,IERR)		J 190S
SUM=CMPLX(AJ(N+1),0.)		J 200
FCD=F1*F2*F3		J 210
FCT=(1.,0.)		J 220
DO 30 K=1,LIM		J 230
L=N+K+1		J 240
FAC=K*FAC		J 250
FCT=FCT*FCD		J 260
AJ(L)=AJ(L)/FAC		J 270
30 SUM=SUM+FCT*AJ(L)		J 280
IN=LIM+1		J 290
KN=LIM+11		J 300
DO 40 I=IN,KN		J 310
FAC=I*FAC		J 320
L=I+N		J 330
CALL BELS (R,Y,L)		J 340S
FCT=FCT*FCD		J 350
Y=Y/FAC		J 360
40 SUM=SUM+FCT*Y		J 370
AJN=CON*SUM		J 380
CALL BELZ (Z,AJN,AYN,N)		J 390S
IF (M,NE.0) GO TO 50		J 400
H1=AJN		J 410
H2=AYN		J 420
RETURN		J 430
50 H1=AJN*(0.,1.)*AYN		J 440
H2=AJN*(0.,1.)*AYN		J 450
RETURN		J 460
60 CONTINUE		J 470
CALL HAN (Z,H1,H2,N)		J 480S
IF (M,NE.0) GO TO 70		J 490
H1=(H1+H2)/2.		J 500
H2=(0.,-.5)*(H1-H2)		J 510
70 RETURN		J 520
END		J 530-

•DECK BSSLS	
SUBROUTINE BSSLS (X,F,N,IERR)	K 10
DIMENSION F(1)	K 20
IERR=0	K 30
NMAX=30	K 40
IF (N,LE,NMAX) GO TO 10	K 50
IERR=1	K 60
RETURN	K 70
10 MX=X	K 80
NPP=3*MX+12+10*(IABS(N-1)/10)	K 90
IF (IFIX(X).GT.N) NPP=IFIX(3.*X+12.)	K 100
IF (MOD(NPP,2).EQ.0) NPP=NPP+1	K 110
DO 20 I=1,NPP	K 120
20 F(I)=0.	K 130
IF (X,GE,.1E-34) GO TO 30	K 140
F(1)=1.	K 150
RETURN	K 160
30 IF (X,GE,.14E0) GO TO 80	K 170
Z=X/2.	K 180
F(1)=1.	K 190
LPP=NPP-1	K 200
DO 40 K=1,LPP	K 210
40 F(K+1)=F(K)*Z	K 220
FAC2=-Z*Z	K 230
FAC1=1.	K 240
DO 70 I=1,NPP	K 250
NORD=I-1	K 260
IF (I,EQ,1) GO TO 50	K 270
FAC1=FAC1/FLOAT(NORD)	K 280
50 VAL=FAC1	K 290
SUM=FAC1	K 300
DO 60 J=2,20	K 310
L=J+NORD-1	K 320
K=J-1	K 330
VAL=VAL*FAC2/FLOAT(L*K)	K 340
IF (ABS(VAL).LT.1.E-20) GO TO 70	K 350
60 SUM=SUM+VAL	K 360
70 F(I)=F(I)*SUM	K 370
RETURN	K 380
80 NP=NPP+1	K 390
NPR=NPP-1	K 400
F(NP-1)=.1E-34	K 410
F(NP)=0.	K 420
DO 90 I=1,NPR	K 430
NP=NPP-I	K 440
XN=NP	K 450
90 F(NP)=2.*XN/X*F(NP+1)-F(NP+2)	K 460
XN=F(1)	K 470
DO 100 I=3,NPP,2	K 480
100 XN=2.*F(I)+XN	K 490
XN=1./XN	K 500
DO 110 I=1,NPP	K 510
F(I)=XN*F(I)	K 520
110 CONTINUE	K 530
RETURN	K 540
END	K 550-



*DECK BELS	L 10
SUBROUTINE BELS (X,Y,N)	L 20
AN=N	L 30
FN=1.	L 40
DO 10 I=1,N	L 50
AI=I	L 60
10 FN=FN*AI	L 70
C=(.5*X)**2	L 80
CN=(.5*X)**N/FN	L 90
F=C/(AN+1.)	L 100
AJ=2.	L 110
D=1.	L 120
FN1=1.-F	L 130
20 F=F*C/((AN+AJ)*AJ)	L 140
FN1=FN1+D*F	L 150
AJ=AJ+1.	L 160
D=-D	L 170
IF (ABS(F/FN1)-1.E-10) 30,30,20	L 180
30 Y=FN1*CN	L 190
RETURN	L 200
END	

•DECK BELZ	
SUBROUTINE BELZ (X,Y,XY,N)	M 10
COMPLEX X,Y,XY,SM,CXF,CCN,CC,CF,CFN1,CFN3,CHA,XI	M 20
CHA=(.5,0.)	M 30
AN=N	M 40
IF (CABS(X).GE..1E-30) GO TO 10	M 50
PH=0.	M 60
GO TO 20	M 70
10 PH=ATAN2(AIMAG(X),REAL(X))	M 80
20 CONTINUE	M 90
XI=(0.,1.)	M 100
R=CABS(X)	M 110
FN=1.	M 120
FM=0.	M 130
FQ=0.	M 140
SM=(0.,0.)	M 150
IF (N) 30,60,30	M 160
30 DO 40 I=1,N	M 170
AI=I	M 180
FM=FM+1./AI	M 190
40 FN=FN*AI	M 200
CXF=CHA*CHA*X*X	M 210
CCN=(CHA*X)**(-N)/FN	M 220
FS=FN/AN	M 230
GS=1.	M 240
DO 50 I=1,N	M 250
AI=I	M 260
SM=SM+CCN*FS/GS	M 270
CCN=CCN*CXF	M 280
GS=GS*AI	M 290
IF (N.EQ.I) GO TO 50	M 300
FS=FS/(AN-AI)	M 310
50 CONTINUE	M 320
60 CC=CHA*CHA*X*X	M 330
CCN=(CHA*X)**N	M 340
CCN=CCN/FN	M 350
CF=CC/(AN+1.)	M 360
AJ=2.	M 370
D=1.	M 380
CFN1=1.-CF	M 390
CFN3=CMPLX(FM,0.)	M 400
FQ=FQ+1./(AJ-1.)	M 410
FM=FM+1./(AN+AJ-1.)	M 420
FP=FM+FQ	M 430
CFN3=CFN3-CF*FP	M 440
70 CF=CF*CC/((AN+AJ)*AJ)	M 450
CFN1=CFN1+D*CF	M 460
FQ=FQ+1./AJ	M 470
FM=FM+1./(AN+AJ)	M 480
FP=FM+FQ	M 490
CFN3=CFN3+D*CF*FP	M 500
AJ=AJ+1.	M 510
D=-D	M 520
IF (CABS(CF/CFN1)-1.E-10) 80,80,70	M 530
80 XY=(2.*(1.5772156649*(ALOG(R/2.)*XI*PH))*Y-SM-CFN3*CCN)/3.141592653	M 540
159	M 550
RETURN	M 560
END	M 570-

*DECK HAN		N 10
SUBROUTINE HAN (Z,H1,H2,N)		N 20
COMPLEX Z,H1,H2,SETI,SP,X,CP,CP1		N 30
PI=3.14159265359		N 40
AN=N		N 50
IF (CABS(Z).GE..1E-30) GO TO 10		N 60
PH=0.		N 70
GO TO 20		N 80
10 PH=ATAN2(AIMAG(Z),REAL(Z))		N 90
20 CONTINUE		N 100
R=CABS(Z)		N 110
S1=EXP(-1.*AIMAG(Z))/SQRT(.5*PI*R)		N 120
SIGMA1=2.*REAL(Z)/PI-AN-.5-PH/PI		N 130
SETI=CEXP(.5*(0.,1.)*PI*SIGMA1)		N 140
SP=(1.,0.)		N 150
CP=SP		N 160
CP1=CP		N 170
X=-2.*Z*(0.,1.)		N 180
C1=1.		N 190
30 CP=CP*(4.*AN*AN-C1*C1)/(C1*4.*X)		N 200
C1=C1+2.		N 210
SP=SP*CP		N 220
IF (CABS(CP)-CABS(CP1)) 40,50,50		N 230
40 CP1=CP		N 240
GO TO 30		N 250
50 SP=SP-CP		N 260
H1=S1*SETI*SP		N 270
S1=EXP(AIMAG(Z))/SQRT(.5*PI*R)		N 280
SIGMA1=-2.*REAL(Z)/PI+AN+.5-PH/PI		N 290
SETI=CEXP(.5*(0.,1.)*PI*SIGMA1)		N 300
SP=(1.,0.)		N 310
X=2.*Z*(0.,1.)		N 320
CP=SP		N 330
CP1=CP		N 340
C1=1.		N 350
60 CP=CP*(4.*AN*AN-C1*C1)/(C1*4.*X)		N 360
C1=C1+2.		N 370
SP=SP*CP		N 380
IF (CABS(CP)-CABS(CP1)) 70,80,80		N 390
70 CP1=CP		N 400
GO TO 60		N 410
80 SP=SP-CP		N 420
H2=S1*SETI*SP		N 430
RETURN		N 440-
END		

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•DECK INTEG
SUBROUTINE INTEG (H,SUM,L1,L2)
COMPLEX H(3),SUM,L1,L2
SUM=SUM+(L1*L2)*(H(1)*L2*(2.*L1-L2)+H(2)*(L1*L2)**2+H(3)*L1*(2.*L2
1-L1))/L1/L2/6.
RETURN
END
0 10
0 20
0 30
0 40
0 50
0 60-

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*DECK DIRECT
SUBROUTINE DIRECT (ADAT,NTT,DB,TM,NANG,B0,GAMMA,INF,RADNF,XLAST,RS P 10
1TART,PTHETA,PDB) P 20
DIMENSION TM(NANG),PTHETA(NANG),PDB(NANG) P 30
COMPLEX Y(4),DY(4),P(4),Q(4),XSAVE,PY(4) P 40
COMPLEX ALPHA,DKDB,ADAT(1),AVAL,DUM P 50
COMPLEX XVAL(1025),W(1025),W1(1025),BN(1025),CWAVE,CONT P 60
COMPLEX H01,H02 P 70
REAL NFDB(1025,10) P 80
INTEGER GAMMA P 90
REAL MJ,MACH2,KAPPA,M20 P 100
COMMON/DATA/KAPPA,EPSI,POTB,IFLAG P 110
COMMON/INFO/ALPHA,OMEGA,MACH2,TJT0,NORD,GM1,DKDB,IFLG,VJAO P 120
ERMIN=0.1 P 130
ERMAX=0.14 P 140
PI=3.14159 P 150
FCT=57.2958 P 160
MJ=VJAO/SQRT(TJT0) P 170
IF (MJ.GT.2.) GO TO 10 P 180
SIGMA=10.7/(1.-.1163*MJ*MJ) P 190
GO TO 20 P 200
10 SIGMA=19.4*SQRT(MJ-0.9418) P 210
20 EPSI=1.2658/SIGMA P 220
DELX=0.5/OMEGA P 230
IF (IFLG.EQ.0) GO TO 30 P 240
WRITE (6,680) NORD,VJAO,TJT0,EPSI,GAMMA P 250
C P 260
C CALCULATION OF WIDTH AT END OF POTENTIAL CORE P 270
C P 280
30 M20=MACH2*OMEGA*OMEGA P 290
A=0.2*MACH2 P 300
B=(1.-TJT0-A) P 310
IF (A.LT.1.E-10) GO TO 40 P 320
AK=SQRT(B*B+4.*A) P 330
POTB=-1.38629*A/(ALOG(ABS(A+B-1.))-B*ALOG(ABS((2.*A+B-AK)*(B+AK)/
12.*A+B+AK)/(B-AK))))/AK)/TJT0 P 340
POTB=SQRT(POTB) P 350
GO TO 60 P 370
40 IF (ABS(B).LT.1.E-10) GO TO 50 P 380
POTB=-.693147*B*B/(B+ALOG(ABS(1.-B)))/TJT0 P 390
POTB=SQRT(POTB) P 400
GO TO 70 P 410
50 POTB=1.17741 P 420
GO TO 80 P 430
C P 440
C CALCULATION OF THE EDDY VISCOSITY CONSTANT P 450
C P 460
60 RHOB=1./(1.-0.5*B-0.25*A) P 470
KAPPA=(1./A-1/(B+A)*ALOG(ABS(A+B-1.)))-(B*B+2.*A*A*B)*ALOG(ABS((2.*A
1+B-AK)*(B+AK)/(2.*A+B+AK)/(B-AK)))/AK)/2./A)*2.88539/RHOB P 480
GO TO 90 P 500
70 RHOB=1./(1.-0.5*B) P 510
KAPPA=(0.5*TJT0*ALOG(TJT0)/B/B)*2.88539/B/RHOB P 520
GO TO 90 P 530
80 KAPPA=POTB/2.07944 P 540
90 IFLAG=1 P 550
C P 560
C CALCULATION OF STARTING CONDITIONS P 570
C P 580

```

	Y(1)=(0.,0.)	P 590
	Y(2)=80	P 600
	Y(3)=(1.,0.)	P 610
	Y(4)=(1.,0.)	P 620
	B=REAL(Y(2))	P 630
	UC=REAL(Y(3))	P 640
	X=REAL(Y(1))	P 650
	DBDX=EPSI	P 660
C		P 670
C	CALCULATE INTEGRAND FOR FOURIER TRANSFORM	P 680
		P 690
	XVAL(1)=Y(4)	P 700
	IF (NORD.EQ.0) GO TO 110	P 710
	CALL COEFF (ADAT,NIT,B,AVAL,DB)	P 720
	DUM=CSQRT(MACH2*OMEGA*OMEGA-AVAL*AVAL)	P 730
	IF (AIMAG(DUM).GT.0.) GO TO 100	P 740
	DUM=-DUM	P 750
100	DUM=DUM**NORD	P 760
	XVAL(1)=XVAL(1)/DUM	P 770
110	CONTINUE	P 780
	AMP=CABS(XVAL(1))	P 790
	IF (ABS(AIMAG(XVAL(1))).LT.1.E-20) GO TO 120	P 800
	IF (ABS(REAL(XVAL(1))).LT.1.E-20) GO TO 130	P 810
	PHASE=ATAN2(AIMAG(XVAL(1)),REAL(XVAL(1)))*FCT	P 820
	GO TO 140	P 830
120	PHASE=0.	P 840
130	PHASE=90.*SIGN(1.,AIMAG(XVAL(1)))	P 850
140	IF (IFLG.EQ.0) GO TO 150	P 860
	WRITE (6,690) X,B,DBDX,UC,XVAL(1),AMP,PHASE	P 870
C		P 880
C	BEGIN INTEGRATION	P 890
		P 900
150	N=2**GAMMA	P 910
	ISTEP=1	P 920
	H=DELX	P 930
	SMAX=H	P 940
	SMIN=H/1000.	P 950
	XSAVE=Y(1)	P 960
160	IFL=1	P 970
	XSTOP=REAL(XSAVE)*DELX	P 980
	ISTEP=ISTEP+1	P 990
	IF (ISTEP.GE.(N+2)) GO TO 310	P1000
170	DO 180 I=1,4	P1010
180	PY(I)=Y(I)	P1020
190	IF (H.LT.SMIN) H=SMIN	P1030
	IF (H.GT.SMAX) H=SMAX	P1040
	IF (CABS(Y(1)-XSTOP).GT.H) GO TO 200	P1050
	H=CABS(Y(1)-XSTOP)	P1060
	IFL=2	P1070
200	CALL RUNREL (4,H,Y,DY,P,0,ERRES,ADAT,NTT,DB)	P1080
	IND=IND+1	P1090
	IF (ERRES.LT.ERMIN) GO TO 230	P1100
	IF (ERRES.LT.ERMAX) GO TO 240	P1110
	IF (H.LE.SMIN) GO TO 220	P1120
	H=0.8*H	P1130
	DO 210 I=1,4	P1140
210	Y(I)=PY(I)	P1150
	IFL=1	P1160
	GO TO 190	P1170

220	IWR=1	P1180
	GO TO 240	P1190
230	H=1.25*H	P1200
240	IF (IFL, EQ, 1) GO TO 170	P1210
	X=REAL(Y(1))	P1220
	B=REAL(Y(2))	P1230
	UC=REAL(Y(3))	P1240
	DBDX=REAL(DY(2))	P1250
C		P1260
C		P1270
C	CALCULATE INTEGRAND FOR FOURIER TRANSFORM	P1280
	XVAL(ISTEP)=Y(4)	P1290
	IF (NORD, EQ, 0) GO TO 260	P1300
	CALL COEFF (ADAT, NIT, B, AVAL, DB)	P1310S
	DUM=CSQRT(MACH2*OMEGA*OMEGA-AVAL*AVAL)	P1320
	IF (AIMAG(DUM), GT, 0.) GO TO 250	P1330
	DUM=-DUM	P1340
250	DUM=CSQRT(DUM)	P1350
	XVAL(ISTEP)=XVAL(ISTEP)/DUM	P1360
260	CONTINUE	P1370
	AMP=CABS(XVAL(ISTEP))	P1380
	IF (ABS(AIMAG(XVAL(ISTEP))), LT, 1.E-20) GO TO 270	P1390
	IF (ABS(REAL(XVAL(ISTEP))), LT, 1.E-20) GO TO 280	P1400
	PHASE=ATAN2(AIMAG(XVAL(ISTEP)), REAL(XVAL(ISTEP)))*FCT	P1410
	GO TO 290	P1420
270	PHASE=0.	P1430
	GO TO 290	P1440
280	PHASE=90.*SIGN(1., AIMAG(XVAL(ISTEP)))	P1450
290	IF (IFLG, EQ, 0) GO TO 300	P1460
	WRITE (6, 690) X, B, DBDX, UC, XVAL(ISTEP), AMP, PHASE	P1470*
300	XSAVE=Y(1)	P1480
	GO TO 160	P1490
310	IF (IFLG, EQ, 0) GO TO 320	P1500
	WRITE (6, 700) IWR, IND	P1510*
C		P1520
C		P1530
C	PERFORM FOURIER TRANSFORM	P1540
320	IGAM=GAMMA+1	P1550
	INUM=2**IGAM	P1560
	N1=N+1	P1570
	N2=N+2	P1580
	DO 360 I=N2, INUM	P1590
	J=I-INUM-1	P1600
	X=FLOAT(J)*DEL X	P1610
	DUM=(0., 1.)*ADAT(1)*X	P1620
	IF (CABS(DUM), GT, 30.) GO TO 330	P1630
	XVAL(I)=XVAL(I)*CEXP(DUM)	P1640
	GO TO 340	P1650
330	XVAL(I)=(0., 0.)	P1660
340	IF (NORD, EQ, 0) GO TO 360	P1670
	DUM=CSQRT(M20-ADAT(1)*ADAT(1))	P1680
	IF (AIMAG(DUM), GT, 0.) GO TO 350	P1690
	DUM=-DUM	P1700
350	DUM=DUM**NORD	P1710
	XVAL(I)=XVAL(I)/DUM	P1720
360	CONTINUE	P1730
	CALL FFT (IGAM, INUM, XVAL, W)	P1740S
	DO 370 I=1, INUM	P1750
370	XVAL(I)=XVAL(I)*DEL X/2./PI	P1760

	DELW=2.*PI/DELX/INUM	P1770
	IF (IFLG.EQ.0) GO TO 380	P1780
	WRITE (6,710)	P1790*
C		P1800
C	CALCULATION OF B(K)	P1810
C		P1820
	380 DO 440 I=1,INUM	P1830
	IF (I,GE,N) GO TO 390	P1840
	KK=I+N1	P1850
	W(KK)=DELW*(I-N)	P1860
	GO TO 400	P1870
	390 KK=I-N+1	P1880
	W(KK)=DELW*(I-N)	P1890
	400 BN(KK)=XVAL(KK)	P1900
	AMP=CABS(BN(KK))	P1910
	IF (ABS(AIMAG(BN(KK))),LT.1.E-20) GO TO 410	P1920
	IF (ABS(REAL(BN(KK))),LT.1.E-20) GO TO 420	P1930
	PHASE=ATAN2(AIMAG(BN(KK)),REAL(BN(KK)))*FCT	P1940
	GO TO 430	P1950
	410 PHASE=0.	P1960
	GO TO 430	P1970
	420 PHASE=90.*SIGN(1.,AIMAG(BN(KK)))	P1980
	430 WAVEN=REAL(W(KK))	P1990
	IF (IFLG.EQ.0) GO TO 440	P2000
	WRITE (6,720) WAVEN,BN(KK),AMP,PHASE	P2010*
	440 CONTINUE	P2020
	INP1=INUM+1	P2030
	XVAL(INP1)=XVAL(1)	P2040
	W(INP1)=W(1)	P2050
	BN(INP1)=BN(1)	P2060
C		P2070
C		P2080
C	CALCULATION OF FAR FIELD DIRECTIVITY PATTERN	P2090
		P2100
	IF (IFLG.EQ.0) GO TO 450	P2110*
	WRITE (6,730)	P2120
	450 DO 550 M=1,NANG	P2130
	ANGLE=TM(M)/FCT	P2140
	COST=COS(ANGLE)	P2150
	WAVEN=OMEGA*VJA0*COST	P2160
	IF (WAVEN.LT.0.) GO TO 460	P2170
	IVAL=IFIX(WAVEN/DELW-.001)+1	P2180
	IF (IVAL.LT.3) IVAL=3	P2190
	IF (IVAL.GT.(N-1)) IVAL=N-1	P2200
	GO TO 470	P2210
	460 IVAL=IFIX(WAVEN/DELW-.001)+INP1	P2220
	IF (IVAL.LT.(N2+2)) IVAL=N2+2	P2230
	IF (IVAL.GT.(INP1-2)) IVAL=INP1-2	P2240
	470 IM2=IVAL-2	P2250
	IP2=IVAL+2	P2260
	CWAVE=(0.,0.)	P2270
	DO 490 J=IM2,IP2	P2280
	CONT=(1.,0.)	P2290
	DO 480 KJ=IM2,IP2	P2300
	IF (J,EQ,KJ) GO TO 480	P2310
	CONT=CONT*(WAVEN-W(KJ))/(W(J)-W(KJ))	P2320
	480 CONTINUE	P2330
	490 CWAVE=CWAVE+BN(J)*CONT	P2340
	IF (NORD.EQ.0) GO TO 520	P2350
	IF (ABS(ANGLE),LT.1.E-20) GO TO 500	



	VAL=(SQRT(M20-WAVEN*WAVEN))*NORD	P2360
	GO TO 510	P2370
500	VAL=0.	P2380
510	CWAVE=CWAVE*VAL	P2390
520	PTHETA(M)=2.*REAL(CWAVE*CONJG(CWAVE))	P2400
	ANGLE=ANGLE*FCT	P2410
	IF (PTHETA(M).LT.1.E-20) GO TO 530	P2420
	PDB(M)=10.*ALOG10(PTHETA(M))	P2430
	GO TO 540	P2440
530	PDB(M)=0.	P2450
540	IF (IFLG.EQ.0) GO TO 550	P2460
	WRITE (6,740) ANGLE,PTHETA(M),PDB(M)	P2470*
550	CONTINUE	P2480
	IF (INF.EQ.0) GO TO 670	P2490
C		P2500
C		P2510
C	CALCULATION OF NEAR FIELD SOUND PRESSURE LEVEL CONTOURS	P2520
	IF (NORD.EQ.0) GO TO 580	P2530
	DO 570 I=1,INUM	P2540
	DUM=CSQRT(M20-W(I)*W(I))	P2550
	IF (ABS(AIMAG(DUM)).LT.1.E-10) GO TO 560	P2560
	IF (AIMAG(DUM).GT.0.) GO TO 570	P2570
	DUM=-DUM	P2580
	GO TO 570	P2590
560	IF (REAL(DUM).LT.0.) DUM=-DUM	P2600
570	BN(I)=BN(I)*DUM**NORD	P2610
580	DO 650 I=1,INF	P2620
	RAD=RSTART*FLOAT(I)*RADNF	P2630
	DO 610 J=1,INUM	P2640
	DUM=CSQRT(M20-W(J)*W(J))	P2650
	IF (ABS(AIMAG(DUM)).LT.1.E-10) GO TO 590	P2660
	IF (AIMAG(DUM).GT.0.) GO TO 600	P2670
	DUM=-DUM	P2680
	GO TO 600	P2690
590	IF (REAL(DUM).LT.0.) DUM=-DUM	P2700
600	DUM=DUM*RAD	P2710
	CALL NCBRTS (DUM,H01,H02,NORD,1)	P2720S
610	XVAL(J)=BN(J)*H01	P2730
	DO 620 J=1,INUM	P2740
620	XVAL(J)=XVAL(J)*SQRT(RAD)	P2750
	CALL FFT (IGAM,INUM,XVAL,W1)	P2760S
	DO 630 J=1,INUM	P2770
630	XVAL(J)=XVAL(J)*DEWL	P2780
	DO 640 J=2,N	P2790
	K=J*N	P2800
640	NFDB(J,I)=10.*ALOG10(0.5*REAL(XVAL(K)*CONJG(XVAL(K)))/RAD)	P2810
650	NFDB(1,I)=10.*ALOG10(0.5*REAL(XVAL(1)*CONJG(XVAL(1)))/RAD)	P2820
	WRITE (6,750) RADNF	P2830*
	DO 660 J=1,N	P2840
	K=N-J*2	P2850
	IF (J.EQ.1) K=1	P2860
	X=DELX*FLOAT(J-1)	P2870
	IF (X.GT.XLAST) GO TO 660	P2880
	WRITE (6,760) X,(NFDB(K,I),I=1,INF)	P2890*
660	CONTINUE	P2900
670	RETURN	P2910
C		P2920
680	FORMAT (1H1,28X,"VARIATION OF FOURIER TRANSFORM INTEGRAND"/29X,40H	P2930
	1*****//28X,"MODE NUMBER ",I1/2	P2940

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28X,"MACH NUMBER = ",F10.4/23X,"TEMPERATURE RATIO = ",F10.4/32X,"EP P2950
3SILON = ",F10.4/34X,"GAMMA " ,I2//4X,"AXIAL",3X,"THICKNESS", P2960
44X,"DBDX",3X,"CENTERLINE",2X,"FOURIER TRANSFORM",7X,"AMPLITUDE",2X P2970
5,"PHASE"/3X,"DISTANCE",22X,"VELOCITY",2X,"INTEGRAND, G(S)"/) P2980
690 FORMAT (1X,4F10.4,2E12.4,2X,2F10.4) P2990
700 FORMAT (//1X,"IWR = ",I1,2X,"IND = ",I5//) P3000
710 FORMAT (1H1,25X,"WAVENUMBER SPECTRUM, B(K)"/26X,25H***** P3010
1*****//1X,"WAVENUMBER",4X,"WAVENUMBER SPECTRUM",6X,"AMPLITUDE P3020
2",2X,"PHASE"/21X,"B(K)"/) P3030
720 FORMAT (1X,F10.4,2X,2E12.4,2X,2F10.4) P3040
730 FORMAT (1H1,20X,"FAR-FIELD DIRECTIVITY"/21X,21H***** P3050
1**//9X,"ANGLE",10X,"PTHETA",11X,"P DB"/) P3060
740 FORMAT (6X,F10.4,5X,E12.5,5X,F10.4) P3070
750 FORMAT (1H1,20X,"NEAR FIELD SOUND PRESSURE LEVEL CONTOURS"/21X,40H P3080
1*****//35X,"RADIAL SPACING = ", P3090
2F5.2," RADII"/) P3100
760 FORMAT (1X,F10.4,5X,13F8.2) P3110
END P3120-

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*DECK RUNREL
SUBROUTINE RUNREL (M,H,Y,DY,P,Q,ERRES,ADAT,NTT,DB)
COMPLEX Y(M),DY(M),P(M),Q(M),RR(4)
COMPLEX ADAT(1)
10 DO 20 I=1,M
20 Q(I)=(0.,0.)
DY(1)=(1.,0.)
DO 30 I=2,M
30 DY(I)=(0.,0.)
CALL DERY1 (M,Y,DY,ADAT,NTT,DB)
DO 40 I=1,M
P(I)=H*DY(I)*.5
RR(I)=(P(I)-Q(I)+Y(I))-Y(I)
Y(I)=Y(I)+RR(I)
40 Q(I)=(3.*Q(I))-P(I)+(3.*RR(I))
CALL DERY1 (M,Y,DY,ADAT,NTT,DB)
DO 50 I=1,M
P(I)=H*DY(I)
RR(I)=((P(I)-Q(I))*5+Y(I))-Y(I)
Y(I)=Y(I)+RR(I)
50 Q(I)=(3.*P(I))-(2.*Q(I))-(6.*RR(I))
CALL DERY1 (M,Y,DY,ADAT,NTT,DB)
ERRES=0.
DO 70 I=1,M
IF (CABS(P(I)-Q(I)).LT.1.E-20) GO TO 60
E=CABS((H*DY(I))-P(I))/(P(I)-Q(I))
IF (E.GT.ERRES) ERRES=E
60 P(I)=H*DY(I)-.5*P(I)
RR(I)=(P(I)+Y(I))-Y(I)
Y(I)=Y(I)+RR(I)
70 Q(I)=Q(I)+6.*(P(I)-RR(I))
CALL DERY1 (M,Y,DY,ADAT,NTT,DB)
DO 80 I=1,M
P(I)=(-4.*P(I)+H*DY(I)+Q(I))/6.
RR(I)=(P(I)+Y(I))-Y(I)
Y(I)=Y(I)+RR(I)
80 Q(I)=RR(I)-P(I)
RETURN
END

```

```

Q 10
Q 20
Q 30
Q 40
Q 50
Q 60
Q 70
Q 80
Q 90$
Q 100
Q 110
Q 120
Q 130
Q 140
Q 150$
Q 160
Q 170
Q 180
Q 190
Q 200
Q 210$
Q 220
Q 230
Q 240
Q 250
Q 260
Q 270
Q 280
Q 290
Q 300
Q 310$
Q 320
Q 330
Q 340
Q 350
Q 360
Q 370
Q 380-

```





*DECK COEFF	
SUBROUTINE COEFF (A,NG,S,AVAL,DB)	S 10
COMPLEX A(1),AVAL,A1,A2,A3	S 20
I=IFIX((S-0.05)/DB)	S 30
IF (I.EQ.1) I=2	S 40
IF (I.EQ.NG) I=NG-1	S 50
IF (I.GT.NG) GO TO 10	S 60
DS=S-0.05-(I-1)*DB	S 70
A1=(A(I-1)-2.*A(I)+A(I+1))/2./DB/DB	S 80
A2=(4.*A(I)-3.*A(I-1)-A(I+1))/2./DB	S 90
A3=A(I-1)	S 100
AVAL=DS*(A1*DS+A2)+A3	S 110
10 RETURN	S 120
END	S 130-



```
*DECK ISOL
FUNCTION ISOL(IOUT,IGAM,K)
  IB=2**(IGAM-IOUT)
  IW=IB,AND,K
  IF (IW.EQ.0) GO TO 10
  ISOL=K
  RETURN
10 ISOL=K+IB
  RETURN
  END
```

```
U 10
U 20
U 30
U 40
U 50
U 60
U 70
U 80
U 90-
```

•DECK	IMOVE		
	FUNCTION	IMOVE(IOUT,IGAM,K)	
	I2=1		V 10
	IG=IGAM-1		V 20
	DO 10 I=1,IG		V 30
	10 I2=I2+2**I		V 40
	I1=K.AND.I2		V 50
	I3=IGAM-IOUT		V 60
	I4=SHIFT(I1,-I3)		V 70
	I1=COMPL(I2)		V 80
	I3=I1.AND.K		V 90
	I1=I3.OR.I4		V 100
	IMOVE=IREV(IGAM,I1)		V 110
	RETURN		V 120
	END		V 130
			V 140-



```
•DECK IDASH  
FUNCTION IDASH(IOUT,IGAM,K)  
IB=2** (IGAM-IOUT)  
IA=COMPL(IB)  
IDASH=K.AND.IA  
RETURN  
END
```

```
W 10  
W 20  
W 30  
W 40  
W 50  
W 60-
```

```

•DECK IREV
FUNCTION IREV(M,II)
  I2=1
  NG=M-1
  DO 10 I=1,NG
10  I2=I2+2**I
    I1=I1.AND.I2
    I3=I1.AND.1525258
    I4=SHIFT(I3,1)
    I3=I1.AND.1252528
    I5=SHIFT(I3,-1)
    I3=I4.OR.I5
    I4=I3.AND.314638
    I5=SHIFT(I4,2)
    I6=I3.AND.1463148
    I3=SHIFT(I6,-2)
    I4=I3.OR.I5
    I3=I4.AND.74178
    I5=SHIFT(I3,4)
    I3=I4.AND.1703608
    I6=SHIFT(I3,-4)
    I4=I5.OR.I6
    I3=I4.AND.3778
    I5=SHIFT(I3,8)
    I3=I4.AND.1774008
    I6=SHIFT(I3,-8)
    I4=I5.OR.I6
    IM=16-M
    IF (IM.EQ.0) GO TO 20
    I5=SHIFT(I4,-IM)
    GO TO 30
20  I5=I4
30  I3=COMPL(I2)
    I4=I3.AND.I1
    IREV=I5.OR.I4
  RETURN
  END

```

```

X 10
X 20
X 30
X 40
X 50
X 60
X 70
X 80
X 90
X 100
X 110
X 120
X 130
X 140
X 150
X 160
X 170
X 180
X 190
X 200
X 210
X 220
X 230
X 240
X 250
X 260
X 270
X 280
X 290
X 300
X 310
X 320
X 330
X 340
X 350
X 360-

```

•DECK	ASTART		Y 10
	SUBROUTINE	ASTART (VJA0,STRNO,TJT0,ALPHA,NORD,IEROR)	Y 20
		COMPLEX ALPHA,ASTAR0(4,3,8),ASTAR1(4,3,8),A(7,7),B(7)	Y 30
		COMPLEX ALSTAR(4,3,8)	Y 40
		COMMON/ADATA/ASTAR0,ASTAR1	Y 50
C			Y 60
C		LOCATE CLOSEST VALUE IN STARTING VALUE MATRIX	Y 70
		IF (STRNO,LE,0.065) I=1	Y 80
		IF (STRNO,LE,0.2,AND,STRNO,GT,0.065) I=2	Y 90
		IF (STRNO,LE,0.4,AND,STRNO,GT,0.2) I=3	Y 100
		IF (STRNO,GT,0.4) I=4	Y 110
		IF (TJT0,LE,1.63) J=1	Y 120
		IF (TJT0,LE,2.56,AND,TJT0,GT,1.63) J=2	Y 130
		IF (TJT0,GT,2.56) J=3	Y 140
		K=IFIX((VJA0-0.5)/0.25)+1	Y 150
		IKEY=I	Y 160
		JKEY=J	Y 170
		IF (NORD,EQ,0) GO TO 20	Y 180
		DO 10 II=1,4	Y 190
		DO 10 JJ=1,3	Y 200
		DO 10 KK=1,8	Y 210
10		ALSTAR(II,JJ,KK)=ASTAR1(II,JJ,KK)	Y 220
		GO TO 40	Y 230
20		DO 30 II=1,4	Y 240
		DO 30 JJ=1,3	Y 250
		DO 30 KK=1,8	Y 260
30		ALSTAR(II,JJ,KK)=ASTAR0(II,JJ,KK)	Y 270
C			Y 280
C		CALCULATE STARTING VALUE MATRIX	Y 290
		DO 90 IFL=1,7	Y 300
		IF (IFL,EQ,1) GO TO 80	Y 310
		IF (IFL,LT,4) GO TO 60	Y 320
		IF (IFL,LT,6) GO TO 70	Y 330
		IF (IFL,EQ,6) GO TO 50	Y 340
		K=K+2	Y 350
		GO TO 80	Y 360
50		K=K-1	Y 370
		IF (K,EQ,0) K=2	Y 380
		IF (K,EQ,7) K=K-1	Y 390
		I=IKEY	Y 400
		GO TO 80	Y 410
60		J=J+1	Y 420
		IF (J,EQ,4) J=1	Y 430
		GO TO 80	Y 440
70		J=JKEY	Y 450
		I=I+1	Y 460
		IF (I,EQ,5) I=2	Y 470
80		IF (I,EQ,1) S1=0.03	Y 480
		IF (I,EQ,2) S1=0.1	Y 490
		IF (I,EQ,3) S1=0.3	Y 500
		IF (I,EQ,4) S1=0.5	Y 510
		IF (J,EQ,1) T1=1.0	Y 520
		IF (J,EQ,2) T1=2.273	Y 530
		IF (J,EQ,3) T1=2.857	Y 540
		AM1=0.5*(K-1)*0.25	Y 550
		A(IFL,1)=(1.,0.)	Y 560
		A(IFL,2)=S1	Y 570
			Y 580

	A(IFL,3)=S1*S1	Y 590
	A(IFL,4)=T1	Y 600
	A(IFL,5)=T1*T1	Y 610
	A(IFL,6)=AM1	Y 620
	A(IFL,7)=AM1*AM1	Y 630
	90 B(IFL)=ALSTAR(I,J,K)	Y 640
C		Y 650
C	CALL FOR SOLUTION OF SIMULTANEOUS EQUATIONS	Y 660
C		Y 670
	CALL SIMQ (A,B,7,KS)	Y 680S
	IF (KS,EQ.0) GO TO 100	Y 690
	IEROR=2	Y 700
	RETURN	Y 710
C		Y 720
C	CALCULATE STARTING VALUE	Y 730
C		Y 740
	100 ALPHA=B(1)*B(2)*STRNO*B(3)*STRNO*STRNO*B(4)*TJT0*B(5)*TJT0*TJT0*B(	Y 750
	16)*VJA0*B(7)*VJA0*VJA0	Y 760
	RETURN	Y 770
	END	Y 780-



```
•DECK ISEQ  
SUBROUTINE ISEQ (I)  
GO TO (10,10,20), I  
10 I=I+1  
RETURN  
20 I=1  
RETURN  
END
```

```
Z 10  
Z 20  
Z 30  
Z 40  
Z 50  
Z 60  
Z 70
```

*DECK SIMQ		AA 10
SUBROUTINE SIMQ (A,B,N,KS)		AA 20
COMPLEX A(1),B(1),BIGA,SAVE		AA 30
C	FORWARD SOLUTION	AA 40
C		AA 50
C	TOL=0.0	AA 60
	KS=0	AA 70
	JJ=-N	AA 80
	DO 80 J=1,N	AA 90
	JY=J+1	AA 100
	JJ=JJ+N+1	AA 110
	BIGA=(0.,0.)	AA 120
	IT=JJ-J	AA 130
	DO 20 I=J,N	AA 140
C		AA 150
C	SEARCH FOR MAXIMUM COEFFICIENT IN COLUMN	AA 160
C		AA 170
	IJ=IT+I	AA 180
	IF (CABS(BIGA)-CABS(A(IJ))) 10,20,20	AA 190
	10 BIGA=A(IJ)	AA 200
	IMAX=I	AA 210
	20 CONTINUE	AA 220
C		AA 230
C	TEST FOR PIVOT LESS THAN TOLERANCE (SINGULAR MATRIX)	AA 240
C		AA 250
	IF (CABS(BIGA)-TOL) 30,30,40	AA 260
	30 KS=1	AA 270
	RETURN	AA 280
C		AA 290
C	INTERCHANGE ROWS IF NECESSARY	AA 300
C		AA 310
	40 I1=J+N*(J-2)	AA 320
	IT=IMAX-J	AA 330
	DO 50 K=J,N	AA 340
	I1=I1+N	AA 350
	I2=I1-IT	AA 360
	SAVE=A(I1)	AA 370
	A(I1)=A(I2)	AA 380
	A(I2)=SAVE	AA 390
C		AA 400
C	DIVIDE EQUATION BY LEADING COEFFICIENT	AA 410
C		AA 420
	50 A(I1)=A(I1)/BIGA	AA 430
	SAVE=B(IMAX)	AA 440
	B(IMAX)=B(J)	AA 450
	B(J)=SAVE/BIGA	AA 460
C		AA 470
C	ELIMINATE NEXT VARIABLE	AA 480
C		AA 490
	IF (J=N) 60,90,60	AA 500
	60 IOS=N*(J-1)	AA 510
	DO 80 IX=JY,N	AA 520
	IXJ=IOS+IX	AA 530
	IT=J-IX	AA 540
	DO 70 JX=JY,N	AA 550
	IXJX=N*(JX-1)+IX	AA 560
	JJX=IXJX+IT	AA 570
	70 A(IXJX)=A(IXJX)-(A(IXJ)*A(JJX))	AA 580

	80	B(IX)=B(IX)-(B(J)*A(IXJ))	AA 590
C			AA 600
C		BACK SOLUTION	AA 610
C			AA 620
	90	NY=N-1	AA 630
		IT=N*N	AA 640
		DO 100 J=1,NY	AA 650
		IA=IT-J	AA 660
		IB=N-J	AA 670
		IC=N	AA 680
		DO 100 K=1,J	AA 690
		B(IB)=B(IB)-A(IA)*B(IC)	AA 700
		IA=IA-N	AA 710
	100	IC=IC-1	AA 720
		RETURN	AA 730
		END	AA 740-

•DECK BLKLS:

BLOCK DATA LSN

COMPLEX ASTAR0(4,3,8),ASTAR1(4,3,8)	AB 10
COMMON /ADATA/ ASTAR0,ASTAR1	AB 20
DATA (((ASTAR0(I,J,K),I=1,4),J=1,3),K=1,4) /	AB 30
1 (.09358,-.00988),(.3018,-1.0835),(.8303,-.5622),(1.4941,-1.3801),	AB 40
2 (.09268,-.0147),(.2843,-.1235),(.5727,-.83452),(1.5899,-2.4995),	AB 50
3 (.09227,-.0165),(.2762,-.1375),(.4225,-.8857),(1.6951,-2.8943),	AB 60
4 (.09370,-.0104),(.3045,-.0895),(.8813,-.6111),(1.6631,-1.3868),	AB 70
5 (.09282,-.0155),(.2885,-.1312),(.6531,-.9349),(1.7001,-2.3972),	AB 80
6 (.09258,-.0173),(.2806,-.1450),(.4920,-1.0286),(1.7864,-2.8183),	AB 90
7 (.09432,-.0110),(.3118,-.0943),(.9654,-.6463),(1.8513,-1.3641),	AB 100
8 (.09385,-.0163),(.2965,-.1402),(.7901,-1.0089),(1.8762,-2.2768),	AB 110
9 (.09340,-.0183),(.2895,-.1538),(.6586,-1.1550),(1.9302,-2.7002),	AB 120
0 (.09584,-.0109),(.3230,-.0957),(1.0682,-.6527),(2.0507,-1.3039),	AB 130
1 (.09555,-.0164),(.3085,-.1443),(.9465,-1.0326),(2.0944,-2.1508),	AB 140
2 (.09528,-.0183),(.3018,-.1593),(.8603,-1.1941),(2.1292,-2.5534) /	AB 150
DATA (((ASTAR0(I,J,K),I=1,4),J=1,3),K=5,8) /	AB 160
1 (.09622,-.0102),(.3345,-.0945),(1.1765,-.6259),(2.2561,-1.1935),	AB 170
2 (.09638,-.0156),(.3225,-.1450),(1.0996,-1.0170),(2.3324,-2.0077),	AB 180
3 (.09628,-.0175),(.3162,-.1618),(1.0434,-1.1779),(2.3664,-2.3866),	AB 190
4 (.09656,-.00982),(.3425,-1.0907),(1.2791,-.5613),(2.455,-1.0065),	AB 200
5 (.09696,-.0150),(.3355,-.1430),(1.2449,-.9702),(2.5775,-1.8286),	AB 210
6 (.09700,-.0170),(.3300,-.1610),(1.2092,-1.1304),(2.6217,-2.1918),	AB 220
7 (.09678,-.00947),(.3488,-.0855),(1.3532,-.4552),(2.5695,-0.6875),	AB 230
8 (.09733,-.0145),(.3472,-.1371),(1.3808,-.8920),(2.8178,-1.5880),	AB 240
9 (.09744,-.0165),(.3432,-.1585),(1.3623,-1.0552),(2.8803,-1.9492),	AB 250
0 (.09790,-.00917),(.3540,-.0790),(1.3646,-.3370),(2.7500,0.0000),	AB 260
1 (.09765,-.0141),(.3578,-.1318),(1.4992,-.7761),(3.0192,-1.2388),	AB 270
2 (.09782,-.0160),(.3568,-.1525),(1.5013,-.9476),(3.1223,-1.6252) /	AB 280
DATA (((ASTAR1(I,J,K),I=1,4),J=1,3),K=1,4) /	AB 290
1 (.1013,-.0930),(.353,-.291),(1.0606,-.7823),(1.7405,-1.3550),	AB 300
2 (.1071,-.1403),(.388,-.427),(1.0934,-1.1439),(1.6609,-2.1340),	AB 310
3 (.1095,-.1573),(.402,-.475),(1.0913,-1.2721),(1.5279,-2.5331),	AB 320
4 (.1015,-.0930),(.357,-.293),(1.0949,-.7973),(1.8407,-1.3815),	AB 330
5 (.1074,-.1405),(.393,-.431),(1.1354,-1.1581),(1.8220,-2.1505),	AB 340
6 (.1098,-.1576),(.407,-.477),(1.1359,-1.2871),(1.7537,-2.5379),	AB 350
7 (.1018,-.0933),(.363,-.297),(1.1461,-.8100),(1.9793,-1.3880),	AB 360
8 (.1078,-.1408),(.401,-.435),(1.1952,-1.1708),(2.0182,-2.1410),	AB 370
9 (.1103,-.1581),(.414,-.479),(1.1990,-1.3006),(1.9946,-2.5056),	AB 380
0 (.1022,-.0938),(.372,-.301),(1.2134,-.8131),(2.1455,-1.3590),	AB 390
1 (.1083,-.1414),(.410,-.437),(1.2715,-1.1754),(2.2342,-2.0963),	AB 400
2 (.1110,-.1585),(.424,-.482),(1.2790,-1.3067),(2.2422,-2.4416) /	AB 410
DATA (((ASTAR1(I,J,K),I=1,4),J=1,3),K=5,8) /	AB 420
1 (.1027,-.0943),(.381,-.304),(1.2928,-.7999),(2.3276,-1.2818),	AB 430
2 (.1090,-.1420),(.421,-.439),(1.3611,-1.1669),(2.4613,-2.0123),	AB 440
3 (.1117,-.1590),(.436,-.484),(1.3730,-1.3005),(2.4945,-2.3437),	AB 450
4 (.1032,-.0948),(.393,-.307),(1.3790,-.7646),(2.5121,-1.1393),	AB 460
5 (.1099,-.1426),(.434,-.441),(1.4604,-1.1414),(2.6935,-1.8810),	AB 470
6 (.1126,-.1596),(.451,-.486),(1.4774,-1.2776),(2.7490,-2.2042),	AB 480
7 (.1040,-.0953),(.407,-.306),(1.4639,-.7010),(2.6612,-0.8973),	AB 490
8 (.1109,-.1431),(.450,-.441),(1.5657,-1.0942),(2.9228,-1.6878),	AB 500
9 (.1138,-.1603),(.467,-.485),(1.5886,-1.2345),(3.0011,-2.0110),	AB 510
0 (.1049,-.0956),(.422,-.303),(1.5320,-.6039),(2.6335,-0.5950),	AB 520
1 (.1122,-.1438),(.468,-.437),(1.6713,-1.0205),(3.1281,-1.4037),	AB 530
2 (.1151,-.1611),(.484,-.482),(1.7025,-1.1668),(3.2391,-1.7421) /	AB 540
END	AB 550
	AB 560-



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*DECK MXNOISE
SUBROUTINE MXNOISE (NU,ILWR,OPNO,BOPNO,IOPT,ROD,DFT,TOF,A0,VJ,VJA0 AC 10
1,TJT0,I,FREQ,S,ZM,SM,RSW,ALTB,BLTB,SPLB,SPLPD,SPLPG,IND) AC 20
DIMENSION SPLB(1),FREQ(1),SMD(28) AC 30
DIMENSION T1(6) AC 40
REAL KS,KZRZ,LH,LHM AC 50
INTEGER OC,BOPNO,OPNO AC 60
C AC 70
COMMON/ONE/ SPLNQ(28),CQ(28),SPLND(28),CD(28),UCLUJ(28),SD(28,6) AC 80
COMMON/ELEVEN/X(7) AC 90
COMMON/TWELVE/DEC(7) AC 100
C AC 110
C AC 120
DATA IC,OC,IT/2HIC,2H ,2HIT/ AC 130
DATA T1/0.98,1.77,2.209,3.330,0.0,0.0/ AC 140
C AC 150
IND=OC AC 160
TM=ZM*57.2957795 AC 170
IF (OPNO.EQ.2.OR.OPNO.EQ.5) GO TO 10 AC 180
S=FREQ(I)*DFT/VJ AC 190
SM=0.0 AC 200
IF ((TM.LE.45.0.AND.VJA0.GE.1.15).AND.(S.GE.0.1.AND.S.LE.0.5)) GO AC 210
1 TO 410 AC 220
C AC 230
THIS LOOP CALCULATES SMD FOR A GIVEN TJT0 AC 240
FOR ALL 16 VALUES OF SM (PACKAGE B) AC 250
C AC 260
C AC 270
10 DO 60 N=1,28 AC 280
IF (TJT0.GE.0.98.AND.TJT0.LE.3.33) GO TO 20 AC 280
IF (TJT0.LT.T1(1)) SMD(N)=SD(N,1)-(T1(1)-TJT0)*(SD(N,2)-SD(N,1))/( AC 290
T1(2)-T1(1)) AC 300
IF (TJT0.GT.T1(4)) SMD(N)=SD(N,4) AC 310
IF (SMD(N).LT.0.0) SMD(N)=0.0 AC 330
GO TO 60 AC 340
20 J=2 AC 350
30 IF (TJT0-T1(J)) 50,50,40 AC 360
40 J=J+1 AC 370
GO TO 30 AC 380
50 SMD(N)=SD(N,J)+(T1(J)-TJT0)*(SD(N,J-1)-SD(N,J))/(T1(J)-T1(J-1)) AC 390
60 CONTINUE AC 400
C AC 410
THIS SECTION ITERATES TO FIND SM ASSOCIATED WITH THE REQUIRED S AC 420
C AC 430
ICOUNT=0 AC 440
SO=FREQ(I)*DFT/VJ AC 450
SM1=0.01 AC 460
SM=SM1 AC 470
CALL DOPPLE (NU,SM,Z,TS,GS,DS,DM,S,TZ,EI,ETAI,RODA,ROD,ZM,TOF,VJA0 AC 480S
1,TJT0,GAMA) AC 490
S1=S AC 500
SM2=0.63 AC 510
SM=SM2 AC 520
CALL DOPPLE (NU,SM,Z,TS,GS,DS,DM,S,TZ,EI,ETAI,RODA,ROD,ZM,TOF,VJA0 AC 530S
1,TJT0,GAMA) AC 540
S2=S AC 550
SME=SM1*(SO-S1)*(SM2-SM1)/(S2-S1) AC 560
SM=SME AC 570
IF (SM.LT.0.0) GO TO 380 AC 580

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	CALL DOPPLE (NU,SM,Z,TS,GS,DS,DM,S,TZ,EI,ETAI,RODA,ROD,ZM,TOF,VJAO	AC 5905
	1,TJTO,GAMA)	AC 600
	SOE=S	AC 610
	IF (ABS(SOE-SO),LE,0.001) GO TO 80	AC 620
70	SM1=SM2	AC 630
	SM2=SME	AC 640
	S1=S2	AC 650
	S2=SOE	AC 660
	SME=SM1*(SO-S1)*(SM2-SM1)/(S2-S1)	AC 670
	SM=SME	AC 680
	IF (SM,LT,0.0) GO TO 380	AC 690
	CALL DOPPLE (NU,SM,Z,TS,GS,DS,DM,S,TZ,EI,ETAI,RODA,ROD,ZM,TOF,VJAO	AC 7005
	1,TJTO,GAMA)	AC 710
	SOE=S	AC 720
	ICOUNT=ICOUNT+1	AC 730
	IF (ABS(SOE-SO),LE,0.001) GO TO 80	AC 740
	IF (ICOUNT,EQ,50) GO TO 370	AC 750
	GO TO 70	AC 760
C		AC 770
C	THIS SECTION INTERPOLATES VALUES OF SMD,SPLNQ,SPLND,CQ,CD	AC 780
C		AC 790
80	SM=SME	AC 800
	S=SOE	AC 810
	SM1000=SM*1000.0	AC 820
	Y=ALOG10(SM1000)	AC 830
	XX=10.0*Y-14	AC 840
	IF (XX,GT,28) GO TO 350	AC 850
	IF (XX,LT,1.0) GO TO 350	AC 860
	JX=XX	AC 870
	J1=JX+1	AC 880
	EX=XX-JX	AC 890
	SMDI=SMD(JX)+EX*(SMD(J1)-SMD(JX))	AC 900
	SPLNQI=SPLNQ(JX)+EX*(SPLNQ(J1)-SPLNQ(JX))	AC 910
	SPLNQI=SPLNQI-20.0*ALOG10(RODA/72.0)	AC 920
	SPLNDI=SPLND(JX)+EX*(SPLND(J1)-SPLND(JX))	AC 930
	SPLNDI=SPLNDI-20.0*ALOG10(RODA/72.0)	AC 940
	CQI=CQ(JX)+EX*(CQ(J1)-CQ(JX))	AC 950
	CDI=CD(JX)+EX*(CD(J1)-CD(JX))	AC 960
		AC 970
	IF (BOPNO,EQ,1) GO TO 100	AC 980
	IF (BOPNO,EQ,2) GO TO 90	AC 990
C		AC1000
90	PI=3.141593	AC1010
	KZRZ=PI*FREQ(I)*DFT/A0	AC1020
	DELRAD=(SMDI*VJAO)/(DM*KZRZ)	AC1030
	UCLUJI=UCLUJ(JX)+EX*(UCLUJ(J1)-UCLUJ(JX))	AC1040
	UICZ=VJAO	AC1050
	IF (DELRAD,GT,1.818535) UICZ=VJAO*UCLUJI	AC1060
	ETAIN=ETAI	AC1070
	IF (DELRAD,GT,1.818535) ETAIN=ETAI/UCLUJI	AC1080
	GM=(GAMA-1.0)/2.0	AC1090
	TITZ=1.0-GM*UICZ*UICZ+(TS-1.0-GM*ETAIN*ETAIN*UICZ*UICZ)/ETAIN	AC1100
	GO TO 100	AC1110
C		AC1120
100	KS=(DS*DS)/(TS*GS)-(COS(Z)*COS(Z))	AC1130
	DSP2=DS*DS*0.06*0.06*VJAO*VJAO*COS(Z)*COS(Z)	AC1140
	IND=OC	AC1150
	IF (KS,LT,0.0) GO TO 170	AC1160
C		AC1170

C	**PREDICTION OUTSIDE CONE OF SILENCE**	AC1180
C		AC1190
C	QUADRUPOLE CONTRIBUTION	AC1200
C		AC1210
	LH=80.0*ALOG10(VJA0)	AC1220
	CA=-10.0*(2*NU*3)*ALOG10(DM)	AC1230
	IF (BOPNO,EQ.1) GO TO 110	AC1240
	IF (BOPNO,EQ.2) GO TO 120	AC1250
110	FF=10.0*ALOG10(DS**4*DSP2*(NU-2))-30.0*ALOG10(TS)-20.0*ALOG10(GS)	AC1260
	ZZ=1.0*(CQI*(TS*TS)*(GS*GS)*((1.0/DS)**4)*((COS(Z))**4))	AC1270
	GO TO 130	AC1280
120	CALL LILLEY (NU,IOPT,6,DELRAD,UICZ,TITZ,GAMA,KZRZ,TZ,ETAIN,RSW,ALT	AC1290S
	IB,BLTS,ILWR,FPM,FPD,FPQ,IERL)	AC1300
	IF (IERL,NE.0) GO TO 420	AC1310
	FF=FPQ	AC1320
	ZZ=1.0*CQI*10.0*((FPM-FPQ)/10.0)*COS(Z)**4	AC1330
	GO TO 130	AC1340
130	IF (ZZ,LE.0.0) GO TO 360	AC1350
	DIRECT=10.0*ALOG10(ZZ)	AC1360
	SPLPQ=SPLNQI*LH*CA*FF*DIRECT	AC1370
C		AC1380
C	DIPOLE CONTRIBUTION	AC1390
C		AC1400
	LH=60.0*ALOG10(VJA0)	AC1410
	RTS=1.0/TS	AC1420
	TEMPS=10.0*ALOG10((1.0-RTS)*(1.0-RTS))	AC1430
	CA=-10.0*(2*NU*1)*ALOG10(DM)	AC1440
	IF (BOPNO,EQ.1) GO TO 140	AC1450
	IF (BOPNO,EQ.2) GO TO 150	AC1460
140	FF=10.0*ALOG10(DS*DS*DSP2*(NU-2))-20.0*ALOG10(TS)-10.0*ALOG10(GS)	AC1470
	ZZ=1.0*(CDI*TS*GS*((1.0/DS)**2)*((COS(Z))**2))	AC1480
	GO TO 160	AC1490
150	FF=FPD	AC1500
	ZZ=1.0*CDI*10.0*((FPM-FPD)/10.0)*COS(Z)**2	AC1510
	GO TO 160	AC1520
160	IF (ZZ,LE.0.0) GO TO 360	AC1530
	DIRECT=10.0*ALOG10(ZZ)	AC1540
	SPLPD=SPLNDI*LH*TEMPS*CA*FF*DIRECT	AC1550
C		AC1560
	GO TO 330	AC1570
C		AC1580
C	**PREDICTION INSIDE CONE OF SILENCE**	AC1590
C		AC1600
170	CONTINUE	AC1610
	IND=IC	AC1620
	TZ=Z*57.2957795	AC1630
	IF (TZ,LT.30.0,AND,BOPNO,EQ.1) GO TO 400	AC1640
C		AC1650
	IF (BOPNO,EQ.1) GO TO 180	AC1660
	IF (BOPNO,EQ.2) GO TO 260	AC1670
C		AC1680
C	CALCULATION OF UT/US AND TRANSITION POINT TEMPERATURE RATIO TT	AC1690
C		AC1700
180	ONE=2.0*ETAI*VJA0/COS(Z)+TS-1.0*ETAI*ETAI*VJA0*VJA0*VJA0*0.2	AC1710
	TWO=1.2*ETAI*ETAI*VJA0*VJA0	AC1720
	THREE=(SIN(Z)/COS(Z))**2	AC1730
	FOUR=ONE*ONE-4.0*TWO*THREE	AC1740
	IF (FOUR,LT.0.0) GO TO 190	AC1750
	UTUS=(ONE-SQRT(FOUR))/(2.0*TWO)	AC1760



	GO TO 200	AC1770
190	UTUS=100.0	AC1780
200	CONTINUE	AC1790
C		AC1800
	TT=((1.0/COS(Z))-(VJA0*UTUS*ETAI))**2	AC1810
C		AC1820
C	CALCULATION OF EXPONENTIAL DECAY	AC1830
C		AC1840
	PHI=UTUS*ETAI	AC1850
	DE=((TJT0-1.0)/TT)*(2.0*VJA0/(SQRT(TT)))+(0.2*VJA0*VJA0*(1.0-2.0*P	AC1860
	HI)/TT)	AC1870
	GPHI=GPT(PHI)	AC1880
	IF (GPHI.EQ.0.0) GO TO 340	AC1890
	DEN=-1.0*GPHI*COS(Z)*COS(Z)*DE	AC1900
C		AC1910
	Q=(SQRT(ABS(KS)))**3	AC1920
	Y=(4.0*Q)/(3.0*DEN)	AC1930
	AA3=Y*SMDI*VJA0/DM	AC1940
	IF (AA3.GE.0.6) GO TO 240	AC1950
	IND=IT	AC1960
	IF (AA3.LT.0.0) GO TO 390	AC1970
	II=2	AC1980
210	IF (AA3-X(II)) 230,230,220	AC1990
220	II=II+1	AC2000
	IF (II.GT.7) GO TO 240	AC2010
	GO TO 210	AC2020
230	QQ=DEC(II)+((X(II)-AA3)/(X(II)-X(II-1)))*(DEC(II-1)-DEC(II))	AC2030
	GO TO 250	AC2040
240	QQ=0.39152*EXP(-AA3)/(SQRT(3.0*AA3+1.0))	AC2050
250	DECAY=10.0*ALOG10(QQ)	AC2060
	GO TO 260	AC2070
C		AC2080
C	QUADRUPOLE CONTRIBUTION	AC2090
C		AC2100
260	LH=80.0*ALOG10(VJA0)	AC2110
	CA=-10.0*(2*NU+3)*ALOG10(DM)	AC2120
	IF (BOPNO.EQ.1) GO TO 270	AC2130
	IF (BOPNO.EQ.2) GO TO 280	AC2140
270	CONTINUE	AC2150
	P1=ABS(KS)*COS(Z)*COS(Z)	AC2160
	FFF=10.0*ALOG10(DSP2**(NU-2)*P1*P1/TS)	AC2170
	FFI=FFF*DECAY	AC2180
	ZZ=P1/(COS(Z)*COS(Z))	AC2190
	YY=1.0+CQI/(ZZ*ZZ)	AC2200
	GO TO 290	AC2210
280	CALL LILLEY (NU,IOPT,6,DELRAD,UICZ,TITZ,GAMA,KZRZ,TZ,ETAIN,RSW,ALT	AC2220S
	1B,BLTB,ILWR,FPM,FPD,FPQ,IERL)	AC2230
	IF (IERL.NE.0) GO TO 420	AC2240
	FFI=FPQ	AC2250
	YY=1.0+CQI*10.0**((FPM-FPQ)/10.0)*COS(Z)**4	AC2260
	GO TO 290	AC2270
290	IF (YY.LE.0.0) GO TO 360	AC2280
	DIRECI=10.0*ALOG10(YY)	AC2290
	SPLPQ=SPLNQI*LH+CA*FFI*DIRECI	AC2300
C		AC2310
C	DIPOLE CONTRIBUTION	AC2320
C		AC2330
	LHM=60.0*ALOG10(VJA0)	AC2340
	RTS=1.0/TS	AC2350



	TEMP2=10.0*ALOG10((1.0-RTS)*(1.0-RTS))	AC2360
	CAH=-10.0*(2*NU+1)*ALOG10(DH)	AC2370
	IF (BOPNO,EQ.1) GO TO 300	AC2380
	IF (BOPNO,EQ.2) GO TO 310	AC2390
300	FF=10.0*ALOG10(DSP2**(NU-2)*P1/TS)	AC2400
	FFH=FF+DECAY	AC2410
	YYH=1.0*CDI/ZZ	AC2420
	GO TO 320	AC2430
310	FFH=FPD	AC2440
	YYH=1.0*CDI*10.0**((FPM-FPD)/10.0)*COS(Z)**2	AC2450
	GO TO 320	AC2460
320	IF (YYH,LE.0.0) GO TO 360	AC2470
	DIRH=10.0*ALOG10(YYH)	AC2480
	SPLPD=SPLNDI+LHM+TEMP2+CAH+FFH+DIRH	AC2490
C		AC2500
C	**ADDITION OF QUADRUPOLE AND DIPOLE CONTRIBUTIONS**	AC2510
C		AC2520
330	SPLB(I)=10.0*ALOG10(10.0**((SPLPQ/10.0)+10.0**((SPLPD/10.0)))	AC2530
	GO TO 430	AC2540
C		AC2550
C	FAILURE CODE STATEMENTS (PACKAGE B)	AC2560
C		AC2570
340	SPLB(I)=1.0	AC2580
	SPLPQ=0.0	AC2590
	SPLPD=0.0	AC2600
	GO TO 430	AC2610
C		AC2620
350	SPLB(I)=2.0	AC2630
	SPLPQ=0.0	AC2640
	SPLPD=0.0	AC2650
	GO TO 430	AC2660
C		AC2670
360	SPLB(I)=3.0	AC2680
	SPLPQ=0.0	AC2690
	SPLPD=0.0	AC2700
	GO TO 430	AC2710
C		AC2720
370	SPLB(I)=4.0	AC2730
	SPLPQ=0.0	AC2740
	SPLPD=0.0	AC2750
	GO TO 430	AC2760
C		AC2770
380	SPLB(I)=5.0	AC2780
	SPLPQ=0.0	AC2790
	SPLPD=0.0	AC2800
	GO TO 430	AC2810
C		AC2820
390	SPLB(I)=6.0	AC2830
	SPLPQ=0.0	AC2840
	SPLPD=0.0	AC2850
	GO TO 430	AC2860
C		AC2870
400	SPLB(I)=7.0	AC2880
	SPLPQ=0.0	AC2890
	SPLPD=0.0	AC2900
	GO TO 430	AC2910
C		AC2920
410	SPLB(I)=8.0	AC2930
	SPLPQ=0.0	AC2940

```
SPLPD=0.0
GO TO 430
420 CONTINUE
SPLB(I)=FLOAT(IERL)
SPLPQ=0.0
SPLPD=0.0
430 CONTINUE
RETURN
END
```

```
AC2950
AC2960
AC2970
AC2980
AC2990
AC3000
AC3010
AC3020
AC3030-
```

```

*DECK SELECT
SUBROUTINE SELECT (NU,ISS)
C
  DIMENSION IRD(8),SM(28),DELRAD(28,6)
  DIMENSION IWRT(8)
  COMMON/FOUR/ A(16)
  COMMON/FIVE/ B(16)
  COMMON/SIX/ C(16)
  COMMON/SEVEN/ D(16)
  COMMON/EIGHT/ E(16)
  COMMON/NINE/ F(16)
  COMMON/THIRTN/ R(16)
  COMMON/EIGHTY/ T1(16),SD(16,6)
C
  COMMON/FOUR1/ A1(28)
  COMMON/FIVE1/ R1(28)
  COMMON/SIX1/ C1(28)
  COMMON/SEVEN1/ D1(28)
  COMMON/EIGHT1/ E1(28)
  COMMON/NINE1/ F1(28)
  COMMON/THIRTN1/ R1(28)
  COMMON/EIGHTY1/ SD1(28,6),SDT1(28,6)
C
  COMMON/ONE/ SPLNQ(28),CQ(28),SPLND(28),CD(28),UCLUJ(28),XSD(28,6)
C
  COMMON/TWO/ ETA(28),XE(28)
  DATA PI / 3.141593 /
  DATA SM / 0.0316,0.04,0.05,0.063,0.08,0.1,0.125,0.16,0.2,0.25,
1 0.316,0.4,0.5,0.63,0.8,1.0,1.25,1.6,2.0,2.5,3.16,4.0,5.0,
2 6.3,8.0,10.0,12.5,16.0 /
C
  ICOUNT=0
C
  IF (NU.EQ.3) GO TO 40
C
  DO 10 N=1,28
  ETA(N)=A1(N)
  SPLNQ(N)=B1(N)
  CQ(N)=C1(N)
  SPLND(N)=D1(N)
  XE(N)=E1(N)
  CD(N)=F1(N)
  UCLUJ(N)=R1(N)
10 CONTINUE
  DO 30 I=1,4
  DO 30 N=1,28
  IF (ISS.EQ.1) GO TO 20
  XSD(N,I)=SD1(N,I)
  GO TO 30
20 XSD(N,I)=SDT1(N,I)
30 CONTINUE
  GO TO 90
C
40 CONTINUE
  DO 60 N=1,28
  IF (N.LT.6.OR.N.GT.21) GO TO 50
  ETA(N)=A(N-5)
  SPLNQ(N)=B(N-5)
  CQ(N)=C(N-5)

```

```

AD 10
AD 20
AD 30
AD 40
AD 50
AD 60
AD 70
AD 80
AD 90
AD 100
AD 110
AD 120
AD 130
AD 140
AD 150
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AD 170
AD 180
AD 190
AD 200
AD 210
AD 220
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AD 240
AD 250
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AD 270
AD 280
AD 290
AD 300
AD 310
AD 320
AD 330
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AD 350
AD 360
AD 370
AD 380
AD 390
AD 400
AD 410
AD 420
AD 430
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AD 460
AD 470
AD 480
AD 490
AD 500
AD 510
AD 520
AD 530
AD 540
AD 550
AD 560
AD 570
AD 580

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	SPLND(N)=D(N-5)	AD 590
	XE(N)=E(N-5)	AD 600
	CD(N)=F(N-5)	AD 610
	UCLUJ(N)=R(N-5)	AD 620
	GO TO 60	AD 630
50	CONTINUE	AD 640
	ETA(N)=0.0	AD 650
	SPLNQ(N)=0.0	AD 660
	CQ(N)=0.0	AD 670
	SPLND(N)=0.0	AD 680
	XE(N)=0.0	AD 690
	CD(N)=0.0	AD 700
	UCLUJ(N)=1.0	AD 710
60	CONTINUE	AD 720
	DO 80 I=1,4	AD 730
	DO 80 N=1,28	AD 740
	IF (N.LT.6.OR.N.GT.21) GO TO 70	AD 750
	XSD(N,I)=SD(N-5,I)	AD 760
	GO TO 80	AD 770
70	XSD(N,I)=0.0	AD 780
80	CONTINUE	AD 790
		AD 800
C		AD 810
90	CONTINUE	AD 820
	IF (ISS.EQ.0.OR.ISS.EQ.1) GO TO 150	AD 830*
	READ (5,200) (IRD(I),I=1,8)	AD 840
	DO 100 I=1,8	AD 850
	IF (IRD(I).EQ.0) GO TO 100	AD 860
	ICOUNT=ICOUNT+1	AD 870
	IWRT(ICOUNT)=I	AD 880
100	CONTINUE	AD 890*
	IF (IRD(1).EQ.1) READ (5,210) (SPLNQ(N),N=1,28)	AD 900*
	IF (IRD(2).EQ.1) READ (5,210) (CQ(N),N=1,28)	AD 910*
	IF (IRD(3).EQ.1) READ (5,210) (SPLND(N),N=1,28)	AD 920*
	IF (IRD(4).EQ.1) READ (5,210) (CD(N),N=1,28)	AD 930*
	IF (IRD(5).EQ.1) READ (5,210) (ETA(N),N=1,28)	AD 940*
	IF (IRD(6).EQ.1) READ (5,210) (XE(N),N=1,28)	AD 950*
	IF (IRD(7).EQ.1) READ (5,210) (UCLUJ(N),N=1,28)	AD 955
	IF (IRD(8).EQ.0) GO TO 150	AD 960
	DO 120 JJ=1,4	AD 970*
	IF (IRD(8).EQ.1) READ (5,210) (DELRAD(N,JJ),N=1,28)	AD 980
	DO 110 N=1,28	AD 990
	XSD(N,JJ)=PI*SM(N)*DELRAD(N,JJ)	AD1000
110	CONTINUE	AD1010
120	CONTINUE	AD1020
	IF (IRD(8).NE.2) GO TO 150	AD1030
	DO 130 N=1,28	AD1040
	XSRJ=2.0/SQRT(0.021*SM(N)*SM(N)+0.057*SM(N))	AD1050
	DELRAD(N,1)=XSRJ/7.616559	AD1060
	IF (XSRJ.GT.13.85) DELRAD(N,1)=(1.0+0.55*(XSRJ-13.85)/(26.0-13.85)	AD1070
	1)*1.818535	AD1080
130	CONTINUE	AD1090
	FAC1=0.98**0.25	AD1100
	FAC2=1.77**0.25	AD1110
	FAC3=2.209**0.25	AD1120
	FAC4=3.330**0.25	AD1130
	DO 140 N=1,28	AD1140
	DELRAD(N,2)=DELRAD(N,1)*FAC2	AD1150
	XSD(N,2)=PI*SM(N)*DELRAD(N,2)	AD1160
	DELRAD(N,3)=DELRAD(N,1)*FAC3	



	XSD(N,3)=PI*SM(N)*DELRAD(N,3)	AD1170
	DELRAD(N,4)=DELRAD(N,1)*FAC4	AD1180
	XSD(N,4)=PI*SM(N)*DELRAD(N,4)	AD1190
	DELRAD(N,1)=DELRAD(N,1)*FAC1	AD1200
	XSD(N,1)=PI*SM(N)*DELRAD(N,1)	AD1210
140	CONTINUE	AD1220
150	CONTINUE	AD1230
	IF (IRD(8),NE,0) GO TO 170	AD1240
	DO 160 JJ=1,4	AD1250
	DO 160 N=1,28	AD1260
	DELRAD(N, JJ)=XSD(N, JJ)/(PI*SM(N))	AD1270
160	CONTINUE	AD1280
170	CONTINUE	AD1290
	WRITE (6,220)	AD1300*
	IF (ICOUNT.EQ.0) WRITE (6,230)	AD1310*
	IF (ICOUNT.GT.0) WRITE (6,240) (IWRT(I),I=1,ICOUNT)	AD1320*
	IF (IRD(8),EQ.2) WRITE (6,250)	AD1330*
	WRITE (6,260) (SM(N),N=1,14)	AD1340*
	WRITE (6,270) (SPLNQ(N),N=1,14)	AD1350*
	WRITE (6,280) (CQ(N),N=1,14)	AD1360*
	WRITE (6,290) (SPLND(N),N=1,14)	AD1370*
	WRITE (6,300) (CD(N),N=1,14)	AD1380*
	WRITE (6,310) (ETA(N),N=1,14)	AD1390*
	WRITE (6,320) (XE(N),N=1,14)	AD1400*
	WRITE (6,330) (UCLUJ(N),N=1,14)	AD1410*
	DO 180 JJ=1,4	AD1420
	WRITE (6,340) (DELRAD(N, JJ),N=1,14)	AD1430*
180	CONTINUE	AD1440
	WRITE (6,350) (SM(N),N=15,28)	AD1450*
	WRITE (6,270) (SPLNQ(N),N=15,28)	AD1460*
	WRITE (6,280) (CQ(N),N=15,28)	AD1470*
	WRITE (6,290) (SPLND(N),N=15,28)	AD1480*
	WRITE (6,300) (CD(N),N=15,28)	AD1490*
	WRITE (6,310) (ETA(N),N=15,28)	AD1500*
	WRITE (6,320) (XE(N),N=15,28)	AD1510*
	WRITE (6,330) (UCLUJ(N),N=15,28)	AD1520*
	DO 190 JJ=1,4	AD1530
	WRITE (6,340) (DELRAD(N, JJ),N=15,28)	AD1540*
190	CONTINUE	AD1550
	RETURN	AD1560
C		AD1570
200	FORMAT (16I5)	AD1580
210	FORMAT (8F10.1)	AD1590
220	FORMAT (1H1,44X,"MIXING NOISE SOURCE AND MEAN FLOW CONSTANTS")	AD1600
230	FORMAT (/,52X,"* STANDARD DATA VALUES USED *")	AD1610
240	FORMAT (/,44X,"USER INPUT VALUES FOR PARAMETERS",8(1X,I1))	AD1620
250	FORMAT (1X,"SOURCE LOCATION MODEL USED , WITH SIGMA = 13.5 , ", "TO 1 CALCULATE DELTA/RJ",/,1X,"(TJ/T0)**0.25 DEPENDENCE ", "ASSUMED , A 2T STANDARD TEMPERATURES 0.98,1.77,2.209,3.33")	AD1630 AD1640 AD1650
260	FORMAT (///,1X,"SM",7X,14F7.3)	AD1660
270	FORMAT (/,1X,"SPLQ",5X,14F7.2)	AD1670
280	FORMAT (/,1X,"AXWTQ",4X,14F7.2)	AD1680
290	FORMAT (/,1X,"SPLD",5X,14F7.2)	AD1690
300	FORMAT (/,1X,"AXWTD",4X,14F7.2)	AD1700
310	FORMAT (/,1X,"VS/VJ",4X,14F7.2)	AD1710
320	FORMAT (/,1X,"VC/VJ",4X,14F7.2)	AD1720
330	FORMAT (/,1X,"VMAX/VJ",2X,14F7.2,/) )	AD1730
340	FORMAT (1X,"DELTA/RJ",1X,14F7.2)	AD1740
350	FORMAT (///,1X,"SM",7X,14F7.2)	AD1750
	END	AD1760-

*DECK	DOPPLER	AE	10
	SUBROUTINE DOPPLE (NU,SM,Z,TS,GS,DS,DM,S,TZ,EI,ETAI,RODA,ROD,ZM,TO	AE	20
	IF,VJA0,TJT0,G)	AE	30
	COMMON/TWO/ETA(28),E(28)	AE	40
C		AE	50
C	CALCULATION OF DM AND S*****	AE	60
C		AE	70
C	EI=INTERPOLATED E	AE	80
C	ETAI=INTERPOLATED ETA	AE	90
C	A=ALPHA	AE	100
C	B=BETA	AE	110
C	GS=GAMMA RATIO GS/G0	AE	120
C	TS=SOURCE TEMPERATURE RATIO TS/T0	AE	130
C		AE	140
	IF (NU,NE.3) GO TO 30	AE	150
	IF (SM,LT.3.16) GO TO 10	AE	160
	EI=0.6	AE	170
	ETAI=0.6	AE	180
	GO TO 70	AE	190
10	IF (SM,GT.0.1) GO TO 20	AE	200
	EI=0.8	AE	210
	ETAI=0.5	AE	220
	GO TO 70	AE	230
20	SM1000=SM*1000	AE	240
	Y=ALOG10(SM1000)	AE	250
	X=10.0*Y-14.0	AE	260
	GO TO 60	AE	270
30	IF (SM,LT.16.0) GO TO 40	AE	280
	EI=0.6	AE	290
	ETAI=0.6	AE	300
	GO TO 70	AE	310
40	IF (SM,GT.0.0316) GO TO 50	AE	320
	EI=1.0	AE	330
	ETAI=0.3	AE	340
	GO TO 70	AE	350
50	SM1000=SM*1000	AE	360
	Y=ALOG10(SM1000)	AE	370
	X=10.0*Y-14.0	AE	380
60	CONTINUE	AE	390
	JX=X	AE	400
	J1=JX+1	AE	410
	EX=X-JX	AE	420
	EI=E(JX)+EX*(E(J1)-E(JX))	AE	430
	ETAI=ETA(JX)+EX*(ETA(J1)-ETA(JX))	AE	440
C	CALCULATION OF RADIATION ANGLE TZ(DEGREES)	AE	450
C		AE	460
70	POS=1.0/SQRT(0.057*SM+0.021*SM*SM)	AE	470
	RODA=SQRT(ROD*ROD+POS*POS-2.0*ROD*POS*COS(ZM))	AE	480
	XX=(ROD*ROD+RODA*RODA-POS*POS)/(2.0*ROD*RODA)	AE	490
	AA=SQRT(1.0-XX*XX)	AE	500
	W=ATAN2(AA,XX)	AE	510
	Z=W*ZM	AE	520
	TZ=Z*57.2957795	AE	530
C		AE	540
C	CALCULATION OF GAMMAS	AE	550
C		AE	560
	D=0.073	AE	570
	TSM=1.0*(0.6*(TJT0-1.0))+(VJA0*VJA0*(0.6-0.6*0.6)*0.2)	AE	580

```

IF (TSM.LT.0.999) D=0.034
TS=1.0*(TSM-1.0)/((0.98*D/(SM*SM))**.25)
TOC=((TUR-32.0)*5.0)/9.0
TOK=TOC+273.0
T=TS*TOK
G0=1.421-(TOK/11800.0)*(EXP(-ABS(TOK-450.0)/200.0)/80.0)
IF (TOK.LE.290.0) G0=1.402
G=1.421-(T/11800.0)*(EXP(-ABS(T-450.0)/200.0)/80.0)
IF (T.LE.290.0) G=1.402
GS=G/G0
C
A=0.2*TS**.2
IF (NU.EQ.3) A=0.2*TS**.6
B=0.55*TS**.2
IF (NU.EQ.3) B=0.4*TS**.2
DS=1.0-ETA1*VJA0*COS(Z)
DC=1.0-EI*VJA0*COS(Z)
C
C
C
CALCULATION OF MODIFIED DOPPLER FACTOR DM AND STROUHAL NUMBER S
C
C
C
*** A NEGATIVE SQUARE ROOT ARGUMENT ERROR CAN OCCUR IN THE NEXT
STATEMENT, FOR EXAMPLE, AT HIGH TEMPERATURES. THIS PROBLEM DOES
NOT ARISE IF DM IS GIVEN BY
C
C
DM=SQRT(DC*DC+B*B*VJA0*VJA0*COS(Z)*COS(Z)
1 +A*A*VJA0*VJA0*ABS(DS*DS/(TS*GS)-COS(Z)*COS(Z)))
C
C
THIS REVISED DEFINITION OF DM WAS SUGGESTED BY THE INVESTIGATION
INTO TRANSVERSE NONCOMPACTNESS EFFECTS WITH NUMERICAL LILLEY
EQUATION SOLUTIONS, DESCRIBED IN SECTION 2.1.5.2. HOWEVER THE
SHEAR LAYER THICKNESS PARAMETER SHOULD BE FIRST RE-OPTIMISED, WITH
THE REVISED DM, BEFORE THIS CHANGE IS CONSIDERED FOR GENERAL
PREDICTION PURPOSES.
C
C
DM=SQRT(DC*DC+B*B*VJA0*VJA0*COS(Z)*COS(Z)+A*A*VJA0*VJA0*(DS*DS/(TS
1*GS)-COS(Z)*COS(Z)))
S=SM/DM
RETURN
END

```

```

AE 590
AE 600
AE 610
AE 620
AE 630
AE 640
AE 650
AE 660
AE 670
AE 680
AE 690
AE 700
AE 710
AE 720
AE 730
AE 740
AE 750
AE 760
AE 770
AE 780
AE 790
AE 800
AE 810
AE 820
AE 830-

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•DECK	GPT		
	FUNCTION	GPT(PHI)	AF 10
C			AF 20
C		THIS FUNCTION CALCULATES THE GRADIENT OF VELOCITY PROFILE*****	AF 30
C			AF 40
	DATA	RPI,PI/1.7724539,3.141593/	AF 50
	IF	(PHI.LT.0.0.OR.PHI.GT.1.0) GO TO 10	AF 60
		GPT=0.0	AF 70
	IF	(PHI.LT.0.0001.OR.PHI.GT.0.9999) RETURN	AF 80
		X=0.0	AF 90
	DO	10 I=1,20	AF 100
		DEL=0.5*(1.0-ERF(RPI*X))-PHI	AF 110
		DELP=-EXP(-X*X*PI)	AF 120
		DIF=DEL/DELP	AF 130
		X=X-DIF	AF 140
	IF	(ABS(DIF).LT.0.0001) GO TO 20	AF 150
10	CONTINUE		AF 160
	STOP	7	AF 170
20	CONTINUE		AF 180
	GPT=DELP		AF 190
	RETURN		AF 200
	END		AF 210-







	DIMENSION D(50),ID(50)	AG1180
	COMMON/FOURTN/US(24)	AG1190
	REAL KZRZ	AG1200
	IERL=0	AG1210
	GO TO (10,60,70), IOPT	AG1220
	10 CONTINUE	AG1230
C		AG1240
C	FIND NEAREST STANDARD SOURCE RADIAL POSITION	AG1250
	DO 20 I=1,24	AG1260
	ISRL=I	AG1270
	IF (ETAIN.GT.US(I)) GO TO 30	AG1280
20	CONTINUE	AG1290
30	CONTINUE	AG1300
	CALL DSETUP (NU,IOPT,IW,DELRAD,UICZ,TITZ,GAMMA,KZRZ,THETZ,ISRL,ETA	AG1310S
	IIN,RSW,ALTB,BLTB,D,ID,ILWR)	AG1320
	CALL SUB2 (D,ID)	AG1330S
	FPM=D(31)	AG1340
	FPD=D(32)	AG1350
	FPQ=D(33)	AG1360
	IF (ISRL.LE.1) GO TO 40	AG1370
	FACL=(ETAIN-US(ISRL-1))/(US(ISRL)-US(ISRL-1))	AG1380
	FPM=D(41)+(FPM-D(41))*FACL	AG1390
	FPD=D(42)+(FPD-D(42))*FACL	AG1400
	FPQ=D(43)+(FPQ-D(43))*FACL	AG1410
40	CONTINUE	AG1420
	IERL=ID(41)	AG1430
	IF (ILWR.EQ.0) GO TO 50	AG1440
	WRITE (IW,90) IERL,FPM,FPD,FPQ	AG1450*
50	CONTINUE	AG1460
	RETURN	AG1470
60	CONTINUE	AG1480
70	CONTINUE	AG1490
	ISRL=0	AG1500
	CALL DSETUP (NU,IOPT,IW,DELRAD,UICZ,TITZ,GAMMA,KZRZ,THETZ,ISRL,ETA	AG1510S
	IIN,RSW,ALTB,BLTB,D,ID,ILWR)	AG1520
	CALL SUB2 (D,ID)	AG1530S
	FPM=D(36)	AG1540
	FPD=D(37)	AG1550
	FPQ=D(38)	AG1560
	IERL=ID(41)	AG1570
	IF (ILWR.EQ.0) GO TO 80	AG1580
	WRITE (IW,90) IERL,FPM,FPD,FPQ	AG1590*
80	CONTINUE	AG1600
	RETURN	AG1610
C		AG1620
90	FORMAT (1X,I5,3E13,6)	AG1630
	END	AG1640-

```

*DECK DSETUP
SUBROUTINE DSETUP (NU,IOPT,IV,DELRAD,UICZ,TITZ,GAMMA,KZRZ,THETZ,IS AM 10
JRL,ETAIN,RSW,ALTB,BLTB,D,ID,ILWR) AM 20
REAL KZRZ AM 30
DIMENSION D(1),ID(1) AM 40
DATA RTPI / 2.506628 / AM 50
ITEST=0 AM 60
PI=3.141593 AM 70
X1=7.616559*DELRAD AM 80
IF (X1.GT.13.85) X1=13.85*(DELRAD/1.818535-1.0)*(26.0-13.85)/0.55 AM 90
ANG=THETZ*PI/180.0 AM 100
IF (DELRAD.LE.0.0.OR,DELRAD.GT.9.0) GO TO 70 AM 110
IF (UICZ.LT.0.0.OR,UICZ.GT.3.0) GO TO 70 AM 120
IF (TITZ.LE.0.0.OR,TITZ.GT.9.0) GO TO 70 AM 130
IF (GAMMA.LT.1.0.OR,GAMMA.GT.1.5) GO TO 70 AM 140
IF (KZRZ.LE.0.0.OR,KZRZ.GT.20.0) STOP 1 AM 150
IF (THETZ.LE.0.0.OR,THETZ.GE.180.) STOP 1 AM 160
D(1)=0.02*X1/8.0 AM 170
D(2)=.001 AM 180
D(3)=0.0 AM 190
D(4)=0.02 AM 200
D(5)=0.0 AM 210
D(6)=0.12*X1/8.0 AM 220
D(7)=.005 AM 230
D(8)=GAMMA AM 240
D(9)=0.0 AM 250
D(10)=0.0 AM 260
IF (IOPT.EQ.1) GO TO 20 AM 270
RTEST=0.5*X1*RSW/0.832554 AM 280
IF (RTEST.LT.D(1)) ITEST=1 AM 290
IF (RTEST.LT.D(1)) GO TO 20 AM 300
D(9)=RSW AM 310
RS=0.0 AM 320
IF (ETAIN.LT.0.0001.OR,ETAIN.GT.0.9999) GO TO 10 AM 330
IF (DELRAD.LE.1.818535) RS=1.0*DELRAD*(SQRT(ABS(ALOG(-GPT(ETAIN)))) AM 340
1)+0.022*13.5/SQRT(PI)) AM 350
IF (DELRAD.GT.1.818535) RS=DELRAD*SQRT(2.0*EXP(-1.0)*ABS(ALOG(ETAI AM 360
N))) AM 370
10 CONTINUE AM 380
RSC=(RS-1.0)/X1 AM 390
D(10)=RSC AM 400
20 CONTINUE AM 410
D(11)=KZRZ AM 420
D(12)=UICZ AM 430
D(13)=TITZ AM 440
D(14)=COS(ANG) AM 450
D(15)=SIN(ANG) AM 460
D(16)=X1 AM 470
D(17)=0.0 AM 480
D(18)=0.0 AM 490
D(19)=0.0 AM 500
D(20)=0.0 AM 510
D(21)=1.0 AM 520
D(22)=1.0 AM 530
D(23)=0.0 AM 540
D(24)=0.0 AM 550
D(25)=0.0 AM 560
D(26)=0.0 AM 570
GO TO (30,40,50), IOPT AM 580

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30	CONTINUE	AH 590	
	D(26)=0.0	AH 600	
	GO TO 60	AH 610	
40	CONTINUE	AH 620	
	D(26)=0.0	AH 630	
	IF (D(1).GE.10.0*0.5*X1*D(9)/0.832554) ITEST=1	AH 640	
	IF (D(1).GE.10.0*0.5*X1*D(9)/0.832554) GO TO 60	AH 650	
	D(26)=D(1)	AH 660	
	GO TO 60	AH 670	
50	CONTINUE	AH 680	
	SLTB=(ALTB*X1+BLTB)/RTPI	AH 690	
	IF (SLTB.LT.D(1)) ITEST=1	AH 700	
	IF (SLTB.LT.D(1)) GO TO 60	AH 710	
	D(26)=SLTB	AH 720	
60	CONTINUE	AH 730	
	ID(1)=5	AH 740	
	ID(2)=IW	AH 750	
	ID(3)=1	AH 760	
	ID(4)=NU	AH 770	
	ID(5)=0	AH 780	
	ID(6)=0	AH 790	
	ID(7)=1	AH 800	
	ID(8)=0	AH 810	
	ID(9)=0	AH 820	
	ID(10)=12	AH 830	
	ID(11)=0	AH 840	
	ID(12)=0	AH 850	
	ID(13)=0	AH 860	
	ID(14)=0	AH 870	
	ID(15)=0	AH 880	
	ID(16)=82	AH 890	
	ID(17)=ISRL	AH 900	
	ID(18)=0	AH 910	
	ID(25)=0	AH 920	
	ID(26)=ILWR	AH 930	
	IF (IOPT.EQ.2.OR.IOPT.EQ.3.AND.ITEST.EQ.0) ID(25)=1	AH 940	
	IF (ITEST.NE.0) WRITE (IW,80) RSW,ALTB,BLTB	AH 950*	
	RETURN	AH 960	
70	CONTINUE	AH 970	
	WRITE (IW,90) DELRAD,UICZ,TITZ,GAMMA	AH 980*	
	STOP	AH 990	
		AH1000	
C	80	FORMAT (1X,"RSW,ALTB,BLTB",3E13.6,"TOO SMALL.OPTION 1 ASSUMED")	AH1010
	90	FORMAT (1X,"FLOW PARAMETERS OUTSIDE ALLOWED RANGE",4E13.6)	AH1020
		END	AH1030-

*DECK SUB2		
	SUBROUTINE SUB2 (D, ID)	AI 10
	EXTERNAL FCT, AFCT, OUTP	AI 20
	DIMENSION D(1), ID(1)	AI 30
	DIMENSION PRMT(8), Y(4), DERY(4), AUX(16,4), A(4,4), XOS(40), AMP(3)	AI 40
	DIMENSION APLUG(3), IER(2), TIJ(7,40), YMI(450,5), TX(7)	AI 50
	DIMENSION PRS(40), PQ(40), PD(40)	AI 60
	DIMENSION PA(40)	AI 70
	COMPLEX CMLX, CSORT	AI 80
	COMPLEX JSR, CAMP(2), BET1, BET2, STP1, STP2, RADM, BCNS, RPRES	AI 90
	COMPLEX KRO, KR0, BCWS, CPLUG(2), TRN, TRRN	AI 100
	COMPLEX ST1(40), BE1(40), BET1D	AI 110
	COMPLEX ST2(40), BE2(40), BET2D	AI 120
	COMPLEX TRFN, TFFN	AI 130
	COMPLEX SAV	AI 140
	REAL KW, M, M1, KWS	AI 150
	COMMON YPU(450,5)	AI 160
C	YPU IN OUTP, RADCSO	AI 170
C	NMP BELOW IS MAX FIRST DIMENSION	AI 180
C	NMP IN YMI ABOVE	AI 190
	COMMON/CI/ IR, IW, NOUT, ICHECK	AI 200
	COMMON/BJ/ M, KW, CANG, PI, BV, CV, TJR, G	AI 210
	COMMON/CRIT/ ICC, RC, XMC(16), XTC(16), YCR	AI 220
	COMMON/BN/ NCEO, NCJ, NUT	AI 230
	COMMON/ER/ IERX	AI 240
C	*** FIX STEP SIZE MOD	AI 250
	COMMON/FIX/ JFIXSS	AI 260
	COMMON/ FJET/ IFJ, FJUT, FJTT, FJRT, FJBV, FJCV	AI 270
	COMMON/BUG/ IDBUG	AI 280
	COMMON/STYPE/ MTYPE	AI 290
	COMMON /SRDCSD/ SAV(450)	AI 300
	EQUIVALENCE (YPU(1,1), YMI(1,1))	AI 310
	NDIM=4	AI 320
	ICC=3	AI 330
	NMP=450	AI 340
	PI=3.141593	AI 350
	TEMP=.25	AI 360
	JSR=(0.,1.)	AI 370
	DO 10 JJ=1,8	AI 380
10	PRMT(JJ)=0.	AI 390
	DO 20 I=1,16	AI 400
20	AUX(I,1)=0.0	AI 410
C		AI 420
	PRMT(3)=-D(1)	AI 430
	PRMT(4)=D(2)	AI 440
	PRMT(7)=D(3)	AI 450
	DFC=D(4)	AI 460
	ROX=D(5)	AI 470
	RC=D(6)	AI 480
	ECON=D(7)	AI 490
	G=D(8)	AI 500
	RSW=D(9)	AI 510
	RSC=D(10)	AI 520
	KW=D(11)	AI 530
	M=D(12)	AI 540
	TJR=D(13)	AI 550
	CANG=D(14)	AI 560
	SANG=D(15)	AI 570
	X1=D(16)	AI 580

BV=D(17)	AI 590
TCOR=D(18)	AI 600
DCOR=D(19)	AI 610
FJUT=D(20)	AI 620
FJTT=D(21)	AI 630
FJRT=D(22)	AI 640
FJBV=D(23)	AI 650
FJCV=D(24)	AI 660
FJFF=D(25)	AI 670
IW=ID(2)	AI 680
NGEO=ID(3)	AI 690
MTYPS=ID(4)	AI 700
NUT=ID(5)	AI 710
IERX=ID(6)	AI 720
IHX=ID(7)	AI 730
IWB=ID(8)	AI 740
JFIXSS=ID(9)	AI 750
JCC=ID(10)	AI 760
ISG=ID(11)	AI 770
IDBUG=ID(12)	AI 780
NSLOX=ID(13)	AI 790
NSLO=ID(14)	AI 800
NCJN=ID(15)	AI 810
NCJM=ID(16)	AI 820
ISRL=ID(17)	AI 830
IFJ=ID(18)	AI 840
IO=ID(26)	AI 850
IF (PRMT(3),EQ,0,0) RETURN	AI 860
NCJMX=NCJM+1	AI 870
NCJNX=NCJN+1	AI 880
	AI 890
	AI 900
CALL AXIAL (X1,BV,CV)	AI 910S
	AI 920
	AI 930
SET UP RADIAL SOURCE LOCATIONS IF REQUIRED	AI 940
IF (NSLOX.GT.0) GO TO 40	AI 950
CALL SLOC (DFC,X1,BV,CV,G,XOS,NSLO)	AI 960S
IF (ISRL.LE.0) GO TO 30	AI 970
IF (CV,EQ,0,0) NSLO=ISRL	AI 980
IF (CV,NE,0,0) NSLO=ISRL+NSLO-24	AI 990
30 CONTINUE	AI1000
40 CONTINUE	AI1010
	AI1020
	AI1030
	AI1040
FJPC=(1.-FJUT)*(1.-FJUT)/FJTT	AI1050
ROI=0.	AI1060
XVS=DFC	AI1070
FJSW=0	AI1080
DO 80 IVS=1,1000	AI1090
RO=XVS	AI1100S
CALL VELT (XVS,M,TJR,BV,CV,G,XMC,XTC,3)	AI1110
IF (IVS,EQ,1) M1=XMC(1)	AI1120
IF (IVS,EQ,1) T1=XTC(1)	AI1130
IF (IO,EQ,0) GO TO 50	AI1140*
IF (NUT,GT,0) WRITE (IW,460) XVS,(XMC(I),I=1,3),(XTC(I),I=1,3)	AI1150
50 CONTINUE	AI1160
IF (XMC(1),GE,.99) GO TO 70	AI1170
TPRO=(1.-XMC(1))*(1.-XMC(1))/XTC(1)	

	IF (FJ3W,NE,0,OR,IFJ,EQ,0) GO TO 60	A11180
	IF (ABS(TPRO-FJPC),LT,1,E-04) ROI=XVS	A11190
	IF (ABS(TPRO-FJPC),LT,1,E-04) FJSW=1	A11200
60	CONTINUE	A11210
	IF (ABS(TPRO-1.),LT,.1E-03) GO TO 90	A11220
70	CONTINUE	A11230
	XVS=XVS+FJRT*DFC	A11240
80	CONTINUE	A11250
90	CONTINUE	A11260
	IF (M,EQ,0,0,AND,TJR,EQ,1,) RO=ROX	A11270
	IF (XOS(1),LT,DFC) DFC=XOS(1)*PRMT(3)/2048.	A11280
	IF (XOS(NSLO),GT,RO) RO=XOS(NSLO)-PRMT(3)/2048.	A11290
	RO=DFC+IFIX(RO/PRMT(3))*PRMT(3)	A11300
	IF (ROX,NE,0,,AND,ROX,GT,XOS(NSLO)) ROI=ROX	A11310
	IF (IFJ,EQ,0,AND,ROI,NE,0,) RO=ROI	A11320
	IF (IFJ,EQ,0,AND,ROI,EQ,0,) ROI=RO	A11330
	IF (IO,EQ,0) GO TO 100	A11340
	IF (NUT,GT,0) WRITE (IW,440) X1,DFC,ROI,RO,RC	A11350*
100	CONTINUE	A11360
C		A11370
C		A11380
	XKW2=KW*KW	A11390
	ICC=2	A11400
	DO 120 MS=1,NSLO	A11410
	CALL VELT (XOS(MS),M,TJR,BV,CV,G,AMP,APLUG,ICC)	A11420S
	PRS(MS)=1.-AMP(1)*CANG	A11430
	ID(41)=0	A11440
	IF (ABS(PRS(MS)),LT,1,E-30) ID(41)=11	A11450
	IF (ABS(PRS(MS)),LT,1,E-30) GO TO 420	A11460
	PRS(MS)=PRS(MS)*PRS(MS)/APLUG(1)	A11470
	PQ(MS)=(CANG*CANG-PRS(MS))*KW*KW	A11480
	PD(MS)=-APLUG(2)/APLUG(1)-2.*AMP(2)*CANG/(1.-AMP(1)*CANG)	A11490
	PA(MS)=-APLUG(2)/APLUG(1)	A11500
	IF (ISG,EQ,1) PA(MS)=0.0	A11510
	IF (ISG,EQ,1) PD(MS)=0.	A11520
	IF (IO,EQ,0) GO TO 110	A11530
	IF (NUT,GT,0) WRITE (IW,440) XOS(MS),AMP(1),APLUG(1),PRS(MS),PQ(MS)	A11540*
	1),PD(MS)	A11550
110	CONTINUE	A11560
120	CONTINUE	A11570
C		A11580
C		A11590
	ICC=3	A11600
	YCR=0.	A11610
	ICRIT=0	A11620
	CTEST=1.-M1*CANG	A11630
	IF (CTEST,GT,0,0) GO TO 140	A11640
	ICRIT=1	A11650
	YCR=1.	A11660
	CALL CRIT (YCR,M,TJR,BV,CV,G,CANG)	A11670S
	ICC=JCC	A11680
	CALL VELT (YCR,M,TJR,BV,CV,G,XMC,XTC,ICC)	A11690S
	ICC=3	A11700
	IF (IO,EQ,0) GO TO 130	A11710
	IF (NUT,GT,0) WRITE (IW,440) YCR,(XMC(KI),KI=1,JCC)	A11720*
	IF (NUT,GT,0) WRITE (IW,440) YCR,(XTC(KI),KI=1,JCC)	A11730*
130	CONTINUE	A11740
	ID(41)=0	A11750
	IF (YCR,LT,(DFC-PRMT(3)*RC)) ID(41)=9	A11760



	IF (YCR,LT.(DFC-PRMT(3)*RC)) GO TO 420	AI1770
160	CONTINUE	AI1780
C		AI1790
C		AI1800
	KRO=CMPLX(KW*SANG,0.0)	AI1810
	DUM=CTEST*CTEST/T1-CANG*CANG	AI1820
	KRD=CMPLX(KW*KW*DUM,0.0)	AI1830
	KRD=CSQRT(KRD)	AI1840
	IF (DUM,LT.0.0) KRD=-KRD	AI1850
	IF (NCJNX,GT.1) GO TO 160	AI1860
	DO 150 NTS=1,7	AI1870
	DO 150 MS=1,NSLO	AI1880
150	TIJ(NTS,MS)=0.	AI1890
160	CONTINUE	AI1900
	MXOS=1	AI1910
C		AI1920
C		AI1930
	DO 370 NCJX=NCJNX,NCJMX	AI1940
	ICHECK=0	AI1950
	NCJ=NCJX-1	AI1960
	SCALE=10.**(-NCJ)	AI1970
C		AI1980
C		AI1990
	BCWS=(0.0,0.0)	AI2000
	IF (NGEO,EQ.1) GO TO 170	AI2010
	RADM=-JSR*KRO	AI2020
	BCNS=JSR*KRD	AI2030
	BCWS=(0.,0.)	AI2040
C	ORIGIN AT EDGE OF SINGLE SHEAR LAYER	AI2050
	RPRES=-1./(2.*JSR*KRO)	AI2060
	IERDS=0	AI2070
	GO TO 180	AI2080
170	CONTINUE	AI2090
	CALL RABC (NCJ,RO,DFC,KRO,KRD,RADM,BCNS,BCWS,RPRES,IERDS)	AI2100S
180	CONTINUE	AI2110
	DUM=T1/(CTEST*CTEST)	AI2120
	BCNS=DUM*BCNS	AI2130
	BCWS=DUM*BCWS	AI2140
	IF (IO,EQ.0) GO TO 190	AI2150
	IF (NUT,GT.0) WRITE (IW,440) KRO,KRD,BCWS,RADM,BCNS,RPRES	AI2160*
190	CONTINUE	AI2170
	ID(41)=0	AI2180
	IF (IERDS,NE.0) ID(41)=10	AI2190
	IF (IERDS,NE.0) GO TO 420	AI2200
C		AI2210
C		AI2220
	NOUT=0	AI2230
C	WRONSK = REMOVED	AI2240
	PRMT(3)=-PRMT(3)	AI2250
	PRMT(1)=DFC	AI2260
	PRMT(2)=ROI	AI2270
	IF (ICRIT,EQ.0) GO TO 200	AI2280
	IF (PRMT(2),GT.(YCR-RC)) PRMT(2)=YCR-RC	AI2290
200	CONTINUE	AI2300
	PRMT(6)=XOS(MXOS)-2.*PRMT(3)	AI2310
	IF (MXOS,EQ.1) PRMT(6)=DFC	AI2320
	PRMT(8)=XOS(NSLO)+2.*PRMT(3)	AI2330
	CALL IDERY (DERY,TEMP,NDIM,PRMT,ICC)	AI2340S
	Y(1)=SCALE	AI2350

	Y(2)=0.	AI2360
	Y(3)=REAL(BCNS)*Y(1)	AI2370
	Y(4)=0.	AI2380
C	EXTRA MOD NEEDED HERE IF 2-D JET CASE TO BE INCLUDED	AI2390
	IF (NGEO.EQ.0) Y(4)=AIMAG(BCNS)*Y(1)	AI2400
C	USE NEXT CARD FOR COMPLEX ANGLES	AI2410
C	Y(4)=AIMAG(BCNS)	AI2420
	CALL HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A,XCU)	AI2430S
	IF (IHLF.GE.11) STOP 2	AI2440
	IF (NOUT.GT.NMP) STOP 3	AI2450
	IF (ICRIT.EQ.0) GO TO 240	AI2460
C		AI2470
C		AI2480
	DO 210 IZ=1,NDIM	AI2490
210	Y(IZ)=Y(IZ)+DERY(IZ)*(PRMT(2)-XCU)	AI2500
	CALL TRANS (Y,ST2,NDIM)	AI2510S
	IF (NOUT.GT.0) NOUT=NOUT-1	AI2520
	PRMT(1)=-PI	AI2530
	PRMT(2)=0.	AI2540
	PRMT(3)=PRMT(3)/(RC*2.**IHX)	AI2550
	PRMT(3)=PRMT(3)*PI	AI2560
	DO 220 IZ=1,NDIM	AI2570
220	DERY(IZ)=TEMP	AI2580
	ICC=JCC	AI2590
	CALL HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A,XCU)	AI2600S
	IF (IHLF.GE.11) STOP 2	AI2610
	IF (NOUT.GT.NMP) STOP 3	AI2620
	DO 230 IZ=1,NDIM	AI2630
230	Y(IZ)=Y(IZ)-DERY(IZ)*XCU	AI2640
	CALL TRANS (Y,BE2,NDIM)	AI2650S
C		AI2660
C		AI2670
	ICC=3	AI2680
	PRMT(3)=RC*PRMT(3)*2.**IHX	AI2690
	PRMT(3)=PRMT(3)/PI	AI2700
	IF (NOUT.GT.0) NOUT=NOUT-1	AI2710
C		AI2720
C		AI2730
	PRMT(1)=YCR-RC	AI2740
C	WRONSK	AI2750
	PRMT(2)=ROI	AI2760
	PRMT(6)=XOS(MXOS)-2.*PRMT(3)	AI2770
	IF (PRMT(1).GT.PRMT(2)) PRMT(2)=PRMT(1)+PRMT(3)	AI2780
	CALL IDERY (DERY,TEMP,NDIM,PRMT,ICC)	AI2790S
	CALL HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A,XCU)	AI2800S
	IF (IHLF.GE.11) STOP 2	AI2810
240	CONTINUE	AI2820
	NOUTM=NOUT	AI2830
	IF (NOUTM.GT.NMP) STOP 5	AI2840
	IF (IO.EQ.0) GO TO 250	AI2850
	IF (NUT.GT.0) WRITE (IW,450) NCJ,MXOS,NOUTP,NOUTM,ICHECK	AI2860*
250	CONTINUE	AI2870
C		AI2880
C		AI2890
	IF (IFJ.EQ.0) GO TO 260	AI2900
	PRMT(1)=XCU	AI2910
	PRMT(2)=RO	AI2920
	PRMT(3)=PRMT(3)*FIX(FJRT+FJFF)	AI2930
	PRMT(8)=0.	AI2940

	CALL IDERY (DERY,TEMP,NDIM,PRMT,ICC)	AI2950S
	CALL HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A,XCU)	AI2960S
	IF (IHLF,GE,11) STOP 2	AI2970
	PRMT(3)=PRMT(3)/IFIX(FJRT+FJFF)	AI2980
260	CONTINUE	AI2990
C		AI3000
C		AI3010
	NOUT=0	AI3020
	PRMT(3)=-PRMT(3)	AI3030
	DO 290 MS=MXOS,NSLO	AI3040
	STEST=10.	AI3050
	DO 270 ISE=1,NOUTM	AI3060
	XTEST=ABS(YMI(ISE,1)-XOS(MS))	AI3070
	IF (XTEST,GT,STEST) GO TO 280	AI3080
	STEST=XTEST	AI3090
	MMI=ISE	AI3100
270	CONTINUE	AI3110
280	CONTINUE	AI3120
	IF (XOS(MS),LT,YMI(MMI,1)) MMI=MMI-1	AI3130
	STP2=CMPLX(YMI(MMI,2),YMI(MMI,3))	AI3140
	XINTP=(XOS(MS)-YMI(MMI,1))/(YMI(MMI+1,1)-YMI(MMI,1))	AI3150
	STP2=(1.-XINTP)*STP2+XINTP*CMPLX(YMI(MMI+1,2),YMI(MMI+1,3))	AI3160
	ST2(MS)=STP2	AI3170
	BE1(MS)=(1.-XINTP)*SAV(MMI)+XINTP*SAV(MMI+1)	AI3180
	BET2=CMPLX(YMI(MMI,4),YMI(MMI,5))	AI3190
	BET2D=CMPLX(YMI(MMI+1,4),YMI(MMI+1,5))	AI3200
	BET2=(1.-XINTP)*BET2+XINTP*BET2D	AI3210
	BE2(MS)=BET2/ST2(MS)	AI3220
290	CONTINUE	AI3230
C		AI3240
C		AI3250
	XN4=FLOAT(NCJ)	AI3260
	XN4=XN4*XN4*XN4*XN4	AI3270
	NCON=7*(MXOS-1)	AI3280
C	WRONSK	AI3290
	DO 300 IZ=1,4	AI3300
	Y(IZ)=Y(IZ)+DERY(IZ)*(RO-XCU)	AI3310
300	CONTINUE	AI3320
	CALL WRCAL (NGEO,Y,RADM,RPRES,CAMP(1))	AI3330S
C	CALCULATE RADIAL/AZIMUTHAL COHERENCE AND RADIAL	AI3340
C	SOURCE DISTRIBUTION EFFECTS FOR THIS AZIMUTHAL MODE	AI3350
	IFLAG=0	AI3360
	IF (ID(25),GT,0) CALL RADCSO (IFLAG,NCJ,CAMP(1),D,ID,NOUTM,BV,CV)	AI3370S
C		AI3380
C		AI3390
	DO 340 MS=MXOS,NSLO	AI3400
	XAV=XOS(MS)	AI3410
C	EXTRA MOD NEEDED HERE IF 2-D JET CASE TO BE INCLUDED	AI3420
	IF (NGEO,EQ,0) XAV=1.	AI3430
	CAMP(2)=ST2(MS)*CAMP(1)	AI3440
C	THIS RESTRICTS FREQ. TO GT. 10, E-14	AI3450
C	IF (ALOG10(CABS(CAMP(2)))-NCJ,LT,-30.) CAMP(2)=(0.,0.)	AI3460
	RCAMP=ABS(REAL(CAMP(2)))	AI3470
	AICAMP=ABS(AIMAG(CAMP(2)))	AI3480
	IF (IO,EQ,0) GO TO 310	AI3490
	IF (RCAMP,LT,1.E-30,AND,AICAMP,LT,1.E-30) WRITE (IW,440) CAMP(2)	AI3500*
310	CONTINUE	AI3510
	IF (RCAMP,LT,1.E-30,AND,AICAMP,LT,1.E-30) CAMP(2)=(0.,0.)	AI3520
	XAV2=XAV*XAV	AI3530

	XAV3=XAV*XAV2	AI3540
	XAV4=XAV2*XAV2	AI3550
	TRN=BE2(MS)*PRS(MS)/XAV	AI3560
C	EXTRA MOD NEEDED HERE IF 2-D JET CASE TO BE INCLUDED	AI3570
	TRRN=PQ(MS)+NCJ*NCJ/XAV2+TRN*(PD(MS)-NGEO/XAV)	AI3580
	IF (MTYPS,EQ.1) TRRN=PQ(MS)+NCJ*NCJ/XAV2+TRN*(PA(MS)-NGEO/XAV)	AI3590
	IF (MTYPS,EQ.3) GO TO 320	AI3600
C		AI3610
C	EXTRA INFO. FOR MTYPS,NE,3	AI3620
C	ICC=3	AI3630
	CALL VELT (XOS(MS),M,TJR,BV,CV,G,AMP,APLUG,ICC)	AI3640
	AMP(1)=1.-AMP(1)*CANG	AI3650S
	ST1(MS)=-CANG*AMP(2)/BE1(MS)	AI3660
	IF (ISG,EQ.1) ST1(MS)=(0.0,0.0)	AI3670
	IF (ISG,EQ.1) AMP(2)=0.	AI3680
	AMP(3)=-CANG*AMP(3)/AMP(1)	AI3690
	IF (ISG,EQ.1) AMP(3)=0.	AI3700
320	CONTINUE	AI3710
C		AI3720
C		AI3730
	TRC=CABS(TRN)	AI3740
	IF (MTYPS,EQ.1) TRC=CABS(TRN+ST1(MS))	AI3750
	TRC=TRC*TRC	AI3760
	TRRC=CABS(TRRN)	AI3770
	TRRC=TRRC*TRRC	AI3780
	TRR=2.*REAL(TRN)	AI3790
	TRFN=(TRN-1./XAV)/XAV	AI3800
	IF (MTYPS,EQ.1) TRFN=(TRN+ST1(MS)-1.0/XAV)/XAV	AI3810
	TRFC=CABS(TRFN)	AI3820
	TRFC=TRFC*TRFC	AI3830
	TFFN=(TRN-NCJ*NCJ/XAV)/XAV	AI3840
	TFFC=CABS(TFFN)	AI3850
	TFFC=TFFC*TFFC	AI3860
	CN=CABS(CAMP(2))	AI3870
	CN=CN*CN	AI3880
	IF (NCJ,GT.0) CN=2.*CN	AI3940
	TX(1)=CN	AI3950
	TX(2)=TRC*CN	AI3960
	TX(3)=TRRC*CN	AI3970
C	EXTRA MOD NEEDED HERE IF 2-D JET CASE TO BE INCLUDED	AI3980
	IF (NGEO,EQ.0) GO TO 330	AI3990
	TX(4)=NCJ*NCJ*CN/XAV2	AI4000
	TX(5)=NCJ*NCJ*TRFC*CN	AI4010
	TX(6)=TFFC*CN	AI4020
	TX(7)=CABS(TRN)*CABS(TRN)*CN	AI4030
330	CONTINUE	AI4040
	CALL TCON (MS,NCJX,NCJNX,TIJ,TX,ECON,NCON,MXOS)	AI4050S
	IF (NCON,EQ.7*NSLO) GO TO 380	AI4060
340	CONTINUE	AI4070
C		AI4080
C		AI4090
	IF (IFIX(PRMT(7)),EQ.0) GO TO 370	AI4100
	IF (IO,EQ.0) GO TO 360	AI4110
	DO 350 MS=1,NSLO	AI4120



	WRITE (IW,440) (TIJ(NTS,MS),NTS=1,7)	AI4130*
350	CONTINUE	AI4140
360	CONTINUE	AI4150
370	CONTINUE	AI4160
C		AI4170
C		AI4180
380	CONTINUE	AI4190
	TX(1)=0.0	AI4200
	SIPD=0.0	AI4210
	TISO=0.0	AI4220
	DO 410 MS=1,NSLO	AI4230
C	SAVE TX(1),SIPD,TISO FOR INTERPOLATION IN S.R. LILLEY	AI4240
	D(41)=TX(1)	AI4250
	D(42)=SIPD	AI4260
	D(43)=TISO	AI4270
	CALL TSIGN (MS,TIJ)	AI4280S
	TX(1)=10.*ALOG10(TIJ(1,MS))	AI4290
	TX(2)=10.*ALOG10(TIJ(2,MS)/(1.5*XKW2))	AI4300
	TX(3)=10.*ALOG10(TIJ(3,MS)/(1.375*XKW2*XKW2))	AI4310
C	EXTRA MOD NEEDED HERE IF 2-D JET CASE TO BE INCLUDED	AI4320
	IF (NGEO,EQ.0) GO TO 390	AI4330
	TX(4)=10.*ALOG10(TIJ(4,MS)/(1.5*XKW2))	AI4340
	TX(5)=10.*ALOG10(TIJ(5,MS)/(1.125*XKW2*XKW2))	AI4350
	TX(6)=10.*ALOG10(TIJ(6,MS)/(1.375*XKW2*XKW2))	AI4360
	TX(7)=10.0*ALOG10(TIJ(7,MS)/(0.5*XKW2))	
390	CONTINUE	AI4370
	TISO=TIJ(3,MS)+TIJ(6,MS)+2.*TIJ(5,MS)	AI4380
	TISO=TISO*XKW2*XKW2*(CANG**4)*TIJ(1,MS)+2.*XKW2*CANG*CANG*(TIJ(2,MS)+TIJ(4,MS))	AI4390
	TISO=10.*ALOG10(TISO/(XKW2*XKW2))	AI4400
	TISO=TISO+TCOR	AI4410
	SIPD=TIJ(7,MS)+TIJ(4,MS)+XKW2*CANG*CANG*TIJ(1,MS)	AI4420
	SIPD=10.*ALOG10(SIPD/XKW2)	AI4430
	SIPD=SIPD+DCOR	AI4440
	ICC=1	AI4450
	SMACH=1.	AI4460
	IF (M,NE.0.) SMACH=M	AI4470
	CALL VELT (XOS(MS),SMACH,TJR,BV,CV,G,AMP,APLUG,ICC)	AI4480
C	VEL. AND TEMP. MUST BE LESS THAN 10. SOURCE POS. LESS THAN 99.	AI4490S
	IF (IO,EQ.0) GO TO 400	AI4500
	WRITE (IW,430) XOS(MS),AMP(1),APLUG(1),(TX(NTS),NTS=1,7),TISO,SIPD	AI4510
400	CONTINUE	AI4520*
C	JAN76	AI4530
410	CONTINUE	AI4540
	D(31)=TX(1)	AI4550
	D(32)=SIPD	AI4560
	D(33)=TISO	AI4570
C		AI4580
C		AI4590
C	OBTAIN NON-COMPACT FLOW FACTORS	AI4600
	IFLAG=1	AI4610
	IF (ID(25),GT.0) CALL RADCSO (IFLAG,NCJ,CAMP(1),D,ID,NOUTH,BV,CV)	AI4620
C		AI4630S
C		AI4640
C		AI4650
420	CONTINUE	AI4660
	RETURN	AI4670
C		AI4680
430	FORMAT (1X,F8.4,2F7.4,9F7.2)	AI4690
440	FORMAT (1X,6E13.6)	AI4700
450	FORMAT (1X,3HNCJ,5I5)	AI4710
460	FORMAT (1X,7E11.4)	AI4720
	END	AI4730-

```
•DECK AXIAL
SUBROUTINE AXIAL (X1,BV,CV)
IF (X1.GT.13.85) GO TO 10
BV=X1/13.5
CV=-.022*X1
GO TO 20
10 CONTINUE
BV=1.0*(X1-13.85)*0.55/(26.0-13.85)
BV=BV*1.559874
CV=0.
20 CONTINUE
RETURN
END
```

```
AJ 10
AJ 20
AJ 30
AJ 40
AJ 50
AJ 60
AJ 70
AJ 80
AJ 90
AJ 100
AJ 110
AJ 120-
```

•DECK SLOC	
SUBROUTINE SLOC (XS,X1,BV,CV,G,XOS,NSLO)	AK 10
DIMENSION XOS(1)	AK 20
DIMENSION U(40)	AK 30
DATA U(1),U(2),U(3),U(4),U(5),U(6),U(7),U(8),U(9),U(10),U(11),	AK 40
1U(12),U(13),U(14),U(15),U(16),U(17),U(18),U(19),U(20),U(21),U(22),	AK 50
2  U(23),U(24)/.99,.98199,.968865,.9481,.91859,.87741,.82377,	AK 60
3  .757455,.67936,.67,.66295,.6,.591905,.5,.408098,.3206435,	AK 70
4  .2425485,.1762325,.1225905,.081409,.051541,.0311374,.0180080,	AK 80
5  .01/	AK 90
IF (CV.EQ.0.) GO TO 70	AK 100
IF (X1.GT.8.01) GO TO 40	AK 110
RMDEL=1.+0.022*X1-.12185*X1	AK 120
XOS(1)=2.*XS	AK 130
RDEL=(RMDEL-XOS(1))/9.	AK 140
DO 10 IDEL=1,9	AK 150
XOS(IDEL+1)=XOS(IDEL)+RDEL	AK 160
10 CONTINUE	AK 170
RDEL=.2437*X1/20.	AK 180
DO 20 IDEL=10,17	AK 190
XOS(IDEL+1)=XOS(IDEL)+RDEL	AK 200
20 CONTINUE	AK 210
XOS(19)=1.-.001007875*X1	AK 220
XOS(20)=1.	AK 230
XOS(21)=1.+0.00872375*X1	AK 240
XOS(22)=XOS(18)+RDEL	AK 250
DO 30 IDEL=22,32	AK 260
XOS(IDEL+1)=XOS(IDEL)+RDEL	AK 270
30 CONTINUE	AK 280
NSLO=33	AK 290
RETURN	AK 300
40 CONTINUE	AK 310
XOS(1)=2.0*XS	AK 320
RDEL=0.2437*X1/20.0	AK 330
NMAX=(1.0+0.022*X1-XOS(1))/RDEL	AK 340
XOS(NMAX+5)=1.0+0.022*X1	AK 350
XOS(2)=XOS(NMAX+5)-NMAX*RDEL	AK 360
NDUM=NMAX-1	AK 370
DO 50 IDUM=2,NDUM	AK 380
XOS(IDUM+1)=XOS(IDUM)+RDEL	AK 390
50 CONTINUE	AK 400
XOS(NMAX+1)=1.0-0.001007875*X1	AK 410
XOS(NMAX+2)=1.0	AK 420
XOS(NMAX+3)=1.0+0.00872375*X1	AK 430
XOS(NMAX+4)=XOS(NMAX)+RDEL	AK 440
NDMIN=NMAX+5	AK 450
NDMAX=NMAX+14	AK 460
DO 60 IDUM=NDMIN,NDMAX	AK 470
XOS(IDUM+1)=XOS(IDUM)+RDEL	AK 480
60 CONTINUE	AK 490
NSLO=NMAX+15	AK 500
RETURN	AK 510
70 CONTINUE	AK 520
NSLO=24	AK 530
DO 80 I=1,NSLO	AK 540
XOS(I)=BV*SQRT(ALOG(1./U(I)))	AK 550
IF (XOS(I).LE.XS) XOS(I)=1.1*XS	AK 560
80 CONTINUE	AK 570
RETURN	AK 580
END	AK 590

*DECK VELT		AL 10
SUBROUTINE VELT (X,M,TJR,BV,CV,G,XMC,XTC,ICC)		AL 20
DIMENSION XMC(1)		AL 30
DIMENSION XTC(1)		AL 40
COMMON/ FJET/IFJ,FJUT,FJTT,FJRT,FJBV,FJCV		AL 50
REAL M		AL 60
DATA SPI/1.7724538/		AL 70
VRT=0.0		AL 80
GMM=(G-1.)/2.		AL 90
TJX=TJR-FJTT+GMM*(M-FJUT)*(M-FJUT)		AL 100
FJTJX=FJTT-(1.-GMM*FJUT*FJUT)		AL 110
IF (CV.EQ.0.) GO TO 180		AL 120
C		AL 130
XN=(ABS(X)-1.*CV)/BV		AL 140
IF (XN.GT.10.) GO TO 10		AL 150
IF (XN.LT.-10.) GO TO 70		AL 160
VR=0.5*(1.-ERF(XN))		AL 170
XMC(1)=(M-FJUT)*VR		AL 180
XTC(1)=FJTT-GMM*XMC(1)*XMC(1)+VR*TJX		AL 190
IF (ICC.EQ.1.AND.IFJ.EQ.0) RETURN		AL 200
IF (IFJ.EQ.0) GO TO 90		AL 210
GO TO 30		AL 220
C		AL 230
10 DO 20 I=1,ICC		AL 240
XTC(I)=0.		AL 250
20 XMC(I)=0.0		AL 260
XTC(I)=1.		AL 270
IF (IFJ.EQ.0) GO TO 60		AL 280
C		AL 290
30 CONTINUE		AL 300
XX=(ABS(X)/FJRT-1.*FJCV)/FJBV		AL 310
IF (XX.GT.10.) GO TO 60		AL 320
IF (XX.LT.-10.) GO TO 50		AL 330
VRT=0.5*(1.-ERF(XX))		AL 340
XMC(1)=FJUT*VRT*XMC(1)		AL 350
IF (XTC(1).EQ.1.0) XTC(1)=1.0-GMM*XMC(1)*XMC(1)+VRT*FJTJX		AL 360
40 CONTINUE		AL 370
IF (ICC.EQ.1) GO TO 60		AL 380
IF (XN.GT.10..AND.CV.NE.0.) GO TO 60		AL 390
IF (XN.GT.4..AND.CV.EQ.0.) GO TO 60		AL 400
IF (CV.EQ.0.) GO TO 210		AL 410
GO TO 90		AL 420
C		AL 430
50 CONTINUE		AL 440
XMC(1)=FJUT*XMC(1)		AL 450
IF (XTC(1).EQ.1.0) XTC(1)=FJTT		AL 460
VRT=1.		AL 470
GO TO 40		AL 480
60 CONTINUE		AL 490
RETURN		AL 500
C		AL 510
70 XMC(1)=M		AL 520
XTC(1)=TJR		AL 530
IF (ICC.EQ.1) RETURN		AL 540
C		AL 550
		AL 560
		AL 570
		AL 580



	DO 80 I=2,ICC	AL 590
	XTC(I)=0.	AL 600
	80 XMC(I)=0.0	AL 610
	RETURN	AL 620
C		AL 630
C		AL 640
	90 CONTINUE	AL 650
	XMC(1)=VR	AL 660
	XMC(2)=1.	AL 670
	IF (ICC.GT.2) XMC(3)=2.*XN	AL 680
	N=ICC-1	AL 690
	IF (N=2) 120,120,100	AL 700
	100 DO 110 I=3,N	AL 710
	110 XMC(I+1)=2.*XN*XMC(I)-2.*(I-2)*XMC(I-1)	AL 720
	120 EP=EXP(-XN*XN)	AL 730
	FACT=EP/SPI	AL 740
	DO 130 I=2,ICC	AL 750
	FACT=-FACT/BV	AL 760
	130 XMC(I)=FACT*XMC(I)	AL 770
C	FORM DER. OF VEL. RATIO	AL 780
	DO 150 ND=2,ICC	AL 790
	XTC(ND)=0.	AL 800
	AFAC=1.	AL 810
	DO 140 NDR=1,ND	AL 820
	INDR=ND-NDR+1	AL 830
	XTC(ND)=XTC(ND)+AFAC*XMC(INDR)*XMC(NDR)	AL 840
	AFAC=AFAC*(ND-NDR)/NDR	AL 850
	140 CONTINUE	AL 860
	150 CONTINUE	AL 870
	DO 160 ND=2,ICC	AL 880
	XTC(ND)=-GMM*(M-FJUT)*(M-FJUT)*XTC(ND)+XMC(ND)*TJX	AL 890
	160 CONTINUE	AL 900
	DO 170 I=1,ICC	AL 910
	XMC(I)=(M-FJUT)*XMC(I)	AL 920
	170 CONTINUE	AL 930
	XMC(1)=FJUT*VRT*XMC(1)	AL 940
C	FJ GRADIENTS NOT INCLUDED	AL 950
	RETURN	AL 960
C		AL 970
C		AL 980
	180 CONTINUE	AL 990
	XN=X/BV	AL1000
	IF (XN.GT.4.) GO TO 190	AL1010
	VR=EXP(-XN*XN)	AL1020
	XMC(1)=(M-FJUT)*VR	AL1030
	XTC(1)=FJUT-GMM*XMC(1)*XMC(1)+VR*TJX	AL1040
	IF (ICC.EQ.1.AND. IFJ.EQ.0) RETURN	AL1050
	IF (IFJ.EQ.0) GO TO 210	AL1060
	GO TO 30	AL1070
C		AL1080
C		AL1090
	190 DO 200 I=1,ICC	AL1100
	XTC(I)=0.	AL1110
	200 XMC(I)=0.	AL1120
	XTC(1)=1.	AL1130
	IF (IFJ.EQ.0) RETURN	AL1140
	GO TO 30	AL1150
C		AL1160
C		AL1170

210	CONTINUE	AL1180
	XMC(1)=1.	AL1190
	XMC(2)=2.*XN	AL1200
	IF (ICC-2) 240,240,220	AL1210
220	DO 230 I=3,ICC	AL1220
230	XMC(I)=2.*XN*XMC(I-1)-2.*(I-2)*XMC(I-2)	AL1230
240	FACT=VR	AL1240
	DO 250 I=1,ICC	AL1250
	XMC(I)=FACT*XMC(I)	AL1260
250	FACT=-FACT/BV	AL1270
	DO 270 ND=2,ICC	AL1280
	XTC(ND)=0.	AL1290
	AFAC=1.	AL1300
	DO 260 NDR=1,ND	AL1310
	INDR=ND-NDR+1	AL1320
	XTC(ND)=XTC(ND)+AFAC*XMC(INDR)*XMC(NDR)	AL1330
	AFAC=AFAC*(ND-NDR)/NDR	AL1340
260	CONTINUE	AL1350
270	CONTINUE	AL1360
	DO 280 ND=2,ICC	AL1370
	XTC(ND)=-GMM*(M-FJUT)*(M-FJUT)*XTC(ND)+XMC(ND)*TJX	AL1380
280	CONTINUE	AL1390
	DO 290 I=1,ICC	AL1400
	XMC(I)=(M-FJUT)*XMC(I)	AL1410
290	CONTINUE	AL1420
	XMC(1)=FJUT*VRT+XMC(1)	AL1430
C	FJ GRADIENTS NOT INCLUDED	AL1440
	RETURN	AL1450
	END	AL1460-

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*DECK ERF
      FUNCTION ERF(XN)
C      ERROR FUNCTION RATIONAL APPROXIMATION 7.1.27 OF NBS(ABRAMOWITZ)
      DATA SPI,A1,A2,A3,A4/1.7724538,.278393,.230389,.000972,.078108/
      XA=ABS(XN)
      X1=XA
      X2=XA*X1
      X3=XA*X2
      X4=XA*X3
      XRF=1.+A1*X1+A2*X2+A3*X3+A4*X4
      ERF=1.-1./(XRF*XRF*XRF*XRF)
      IF (XN.LT.0.) ERF=-ERF
      RETURN
      END
      AM 10
      AM 20
      AM 30
      AM 40
      AM 50
      AM 60
      AM 70
      AM 80
      AM 90
      AM 100
      AM 110
      AM 120
      AM 130-

```

*DECK CRIT	
SUBROUTINE CRIT (Y,M,TJR,BV,CV,G,CANG)	AN 10
DIMENSION YMC(3)	AN 20
DIMENSION YTC(3)	AN 30
ICC=3	AN 40
DO 10 N=1,10	AN 50
CALL VELT (Y,M,TJR,BV,CV,G,YMC,YTC,ICC)	AN 60\$
YX=Y*(1.-YMC(1)*CANG)/(YMC(2)*CANG)	AN 70
IF (ABS((YX-Y)/YX).LT..001) GO TO 20	AN 80
Y=YX	AN 90
10 CONTINUE	AN 100
Y=0.	AN 110
20 RETURN	AN 120
END	AN 130-



*DECK RABC	
SUBROUTINE RABC (N,RO,DFC,KRO,KRD,RADM,BCNS,BCWS,RPRES,IERDS)	AO 10
COMPLEX CMLX	AO 20
COMPLEX J,HND,JND	AO 30
COMPLEX KRO,KRD,RADM,BCNS,BCWS,RPRES	AO 40
COMPLEX Z,BJ,Y	AO 50
COMMON/ER/ IERX	AO 60
COMMON/BUG/ IDBUG	AO 70
IERDS=0	AO 80
J=(0.,1.)	AO 90
Z=RO*KRO	AO 100
D=.001	AO 110
CALL CBESL1 (Z,N,BJ,D,IERDS)	AO 120\$
IF (IERDS.NE.0) RETURN	AO 130
CALL CBESL2 (Z,N,Y,IERDS)	AO 140\$
IF (IERDS.NE.0) RETURN	AO 150
RPRES=BJ-J*Y	AO 160
CALL CBESL1 (Z,N+1,BJ,D,IERDS)	AO 170\$
IF (IERDS.NE.0) RETURN	AO 180
CALL CBESL2 (Z,N+1,Y,IERDS)	AO 190\$
IF (IERDS.NE.0) RETURN	AO 200
HND=-(BJ-J*Y)*N*RPRES/Z	AO 210
RADM=Z*HND/RPRES	AO 220
Z=DFC*KRD	AO 230
IF (FLOAT(N+1).GT.250.*CABS(Z*Z)) GO TO 10	AO 240
CALL CBESL1 (Z,N,BJ,D,IERDS)	AO 250\$
IF (IERDS.NE.0) RETURN	AO 260
BCNS=BJ	AO 270
CALL CBESL1 (Z,N+1,BJ,D,IERDS)	AO 280\$
IF (IERDS.NE.0) RETURN	AO 290
JND=-BJ*N*BCNS/Z	AO 300
BCNS=Z*JND/BCNS	AO 310
RETURN	AO 320
10 BCNS=N-Z*Z/(2.*(N+1))	AO 330
RETURN	AO 340
END	AO 350-

```

*DECK CBESL1
C *****
C BESSEL FUNCTION OF COMPLEX VARIABLES *
C *****
C
SUBROUTINE CBESL1 (CX,N,CBJ,D,IER)
COMPLEX CX,CALPHA,CBJ,CFM1,CBPREV,CFM,CBMK,CS
COMMON/BUG/ IDBUG
IF (IDBUG,EQ.1) WRITE (6,80)
CBJ=(0.,0.)
IF (N.LT.0) IER=1
IF (N.LT.0) RETURN
X=CABS(CX)
Y=AIMAG(CX)
IF (X.EQ.0.0.AND.Y.EQ.0.0) IER=2
IF (X.EQ.0.0.AND.Y.EQ.0.0) RETURN
IF (X.LE.15.) NTEST=20.+10.*X-X**2/3.
IF (X.LE.15.) GO TO 10
NTEST=90.+X/2.
10 IF (N.GE.NTEST) IER=4
IF (N.GE.NTEST) RETURN
IER=0
N1=N+1
CBPREV=(0.,0.)
IF (X.LT.5.) MA=X+6.
IF (X.LT.5.) GO TO 20
MA=1.4*X+60./X
20 MB=N+X/4+2
MZERO=MAX0(MA,MB)
MMAX=NTEST
IF (MZERO.GE.MMAX-2) MMAX=MZERO+3
DO 70 M=MZERO,MMAX,3
CFM1=(1.E-28,1.E-28)
CFM=(0.,0.)
CALPHA=(0.,0.)
IF (M.EQ.(M/2)*2) JT=-1
IF (M.EQ.(M/2)*2) GO TO 30
JT=1
30 M2=M-2
DO 60 K=1,M2
MK=M-K
CBMK=2.*MK*CFM1/CX-CFM
CFM=CFM1
CFM1=CBMK
IF (MK-N-1) 50,40,50
40 CBJ=CBMK
50 JT=-JT
CS=1+JT
60 CALPHA=CALPHA+CBMK*CS
CBMK=2.*CFM1/CX-CFM
IF (N.EQ.0) CBJ=CBMK
CALPHA=CALPHA+CBMK
CBJ=CBJ/CALPHA
ACBJ=CABS(CBJ)
ER1=(REAL(CBJ)-REAL(CBPREV))/ACBJ
ER2=(AIMAG(CBJ)-AIMAG(CBPREV))/ACBJ
C ER1 = (REAL(CBJ) - REAL(CBPREV)) / REAL(CBJ)
C ER2 = (AIMAG(CBJ) - AIMAG(CBPREV)) / AIMAG(CBJ)
IF (ABS(ER1).GT.D) GO TO 70
IF (ABS(ER2).GT.D) GO TO 70
RETURN
70 CBPREV=CBJ
IER=3
RETURN
C
80 FORMAT (1X,4HCBE1)
END

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```

AP 10
AP 20
AP 30
AP 40
AP 50
AP 60
AP 70
AP 80*
AP 90
AP 100
AP 110
AP 120
AP 130
AP 140
AP 150
AP 160
AP 170
AP 180
AP 190
AP 200
AP 210
AP 220
AP 230
AP 240
AP 250
AP 260
AP 270
AP 280
AP 290
AP 300
AP 310
AP 320
AP 330
AP 340
AP 350
AP 360
AP 370
AP 380
AP 390
AP 400
AP 410
AP 420
AP 430
AP 440
AP 450
AP 460
AP 470
AP 480
AP 490
AP 500
AP 510
AP 520
AP 530
AP 540
AP 550
AP 560
AP 570
AP 580
AP 590
AP 600
AP 610
AP 620
AP 630
AP 640
AP 650
AP 660-

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*DECK CBESL2
C ..... AQ 10
C   C B E S L 2 ..... AQ 20
C ..... AQ 30
C ..... AQ 40
SUBROUTINE CBESL2 (X,N,BY,IER) AQ 50
C   COMPLEX CSQRT,CSIN,CCOS,CLOG AQ 60
      COMPLEX T, P0, Q0, P1, Q1, A, B, Y0, Y1, XX, X2, TERM, AQ 70
1   TS, YA, YB, YC AQ 80
      COMPLEX X, BY AQ 90
      COMMON/BUG/ IDBUG AQ 100
      IF (IDBUG,EQ,1) WRITE (6,200) AQ 110*
      IF (N) 180,10,10 AQ 120
10  IER=0 AQ 130
      IF (CABS(X)) 190,190,20 AQ 140
20  P1=3.141592653 AQ 150
      IF (CABS(X)-4.) 40,40,30 AQ 160
30  T=4./X AQ 170
      IF (IDBUG,EQ,1) WRITE (6,200) AQ 180*
      P0=.3989422793 AQ 190
      Q0=-.0124669441 AQ 200
      P1=.3989422819 AQ 210
      Q1=.0374008364 AQ 220
      A=T*T AQ 230
      B=A AQ 240
      P0=P0-.0017530620*A AQ 250
      Q0=Q0+.0004564324*A AQ 260
      P1=P1+.0029218256*A AQ 270
      Q1=Q1-.00063904*A AQ 280
      A=A*A AQ 290
      P0=P0+.00017343*A AQ 300
      Q0=Q0-.0000869791*A AQ 310
      P1=P1-.000223203*A AQ 320
      Q1=Q1+.0001064741*A AQ 330
      A=A*B AQ 340
      P0=P0-.0000487613*A AQ 350
      Q0=Q0+.0000342468*A AQ 360
      P1=P1+.0000580759*A AQ 370
      Q1=Q1-.0000398708*A AQ 380
      A=A*B AQ 390
      P0=P0+.0000173565*A AQ 400
      Q0=Q0-.0000142078*A AQ 410
      P1=P1-.000020092*A AQ 420
      Q1=Q1+.00001622*A AQ 430
      A=A*B AQ 440
      P0=P0-.0000037043*A AQ 450
      Q0=Q0+.0000032312*A AQ 460
      P1=P1+.0000042414*A AQ 470
      Q1=Q1-.0000036594*A AQ 480
      A=SQRT(2.*PI) AQ 490
      B=4.*A AQ 500
      P0=A*P0 AQ 510
      Q0=B*Q0/X AQ 520
      P1=A*P1 AQ 530
      Q1=B*Q1/X AQ 540
      A=X-PI/4. AQ 550
      B=CSQRT(2./(PI*X)) AQ 560
      Y0=B*(P0*CSIN(A)+Q0*CCOS(A)) AQ 570
      Y1=B*(-P1*CCOS(A)+Q1*CSIN(A)) AQ 580

```

IF (IDBUG.EQ.1) WRITE (6,200)	AQ 590*
GO TO 90	AQ 600
40 XX=X/2.	AQ 610
X2=XX*XX	AQ 620
T=CLOG(XX)+.5772156649	AQ 630
SUM=0.	AQ 640
TERM=T	AQ 650
Y0=T	AQ 660
DO 70 L=1,15	AQ 670
IF (L-1) 50,60,50	AQ 680
50 SUM=SUM+1./FLOAT(L-1)	AQ 690
60 FL=L	AQ 700
TS=T-SUM	AQ 710
TERM=(TERM*(-X2)/FL**2)*(1.-1./(FL*TS))	AQ 720
70 Y0=Y0+TERM	AQ 730
TERM=XX*(T-.5)	AQ 740
SUM=0.	AQ 750
Y1=TERM	AQ 760
DO 80 L=2,16	AQ 770
SUM=SUM+1./FLOAT(L-1)	AQ 780
FL=L	AQ 790
FL1=FL-1.	AQ 800
TS=T-SUM	AQ 810
TERM=(TERM*(-X2)/(FL1*FL))*((TS-.5/FL)/(TS+.5/FL))	AQ 820
80 Y1=Y1+TERM	AQ 830
PI2=2./PI	AQ 840
Y0=PI2*Y0	AQ 850
Y1=-PI2/X+PI2*Y1	AQ 860
90 IF (N-1) 100,100,130	AQ 870
100 IF (N) 110,120,110	AQ 880
110 BY=Y1	AQ 890
GO TO 170	AQ 900
120 BY=Y0	AQ 910
GO TO 170	AQ 920
130 YA=Y0	AQ 930
YB=Y1	AQ 940
K=1	AQ 950
140 T=FLOAT(2*K)/X	AQ 960
YC=T*YB-YA	AQ 970
K=K+1	AQ 980
IF (K=N) 150,160,150	AQ 990
150 YA=YB	AQ1000
YB=YC	AQ1010
GO TO 140	AQ1020
160 BY=YC	AQ1030
170 RETURN	AQ1040
180 IER=1	AQ1050
RETURN	AQ1060
190 IER=2	AQ1070
RETURN	AQ1080
	AQ1090
	AQ1100
C 200 FORMAT (1X,4HCBE2)	AQ1110-
END	



AD-A064 685

LOCKHEED-GEORGIA CO MARIETTA  
THE GENERATION, RADIATION AND PREDICTION OF SUPERSONIC JET NOIS--ETC(U)  
OCT 78 B J TESTER, P J MORRIS, H K TANNA F33615-76-C-2021  
LG78ER0262-VOL-2 AFAPL-TR-78-85-VOL-2 NL

F/G 20/1

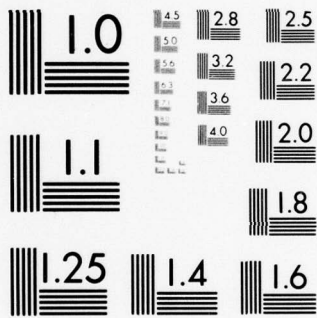
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2 OF 2

AD A064 685



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DDC



MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

•DECK IDERY	
SUBROUTINE IDERY (DERY,TEMP,NDIM,PRMT,ICC)	AR 10
DIMENSION DERY(1),PRMT(1)	AR 20
DO 10 I=1,NDIM	AR 30
DERY(I)=TEMP	AR 40
10 CONTINUE	AR 50
ICC=3	AR 60
IF (IFIX(PRMT(7)).EQ.0) ICC=1	AR 70
RETURN	AR 80
END	AR 90-

*DECK HPCL		A 10
SUBROUTINE HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A,X)		A 20
DIMENSION PRMT(1),Y(1),DERY(1),AUX(16,1),A(1),BT(6)		A 30
GO TO 40		A 40
C		A 40
C THIS PART OF SUBROUTINE HPCL COMPUTES THE RIGHT HAND SIDE DERY OF		A 50
C THE GIVEN SYSTEM OF LINEAR DIFFERENTIAL EQUATIONS.		A 60
10 CALL AFCT (X,A,Y)		A 70S
CALL FCT (X,DERY)		A 80S
DO 30 M=1,NDIM		A 90
LL=M-NDIM		A 100
HS=0.		A 110
DO 20 L=1,NDIM		A 120
LL=LL+NDIM		A 130
20 HS=HS+A(LL)*Y(L)		A 140
30 DERY(M)=HS+DERY(M)		A 150
GO TO (90,420,440,460,190,260,290,560,600,750,770,320), ISW2		A 160
C		A 170
C POSSIBLE BREAK-POINT FOR LINKAGE		A 180
C		A 190
40 N=1		A 200
IJ=1		A 210
IHLF=0		A 220
X=PRMT(1)		A 230
H=PRMT(3)		A 240
PRMT(5)=0.		A 250
DO 50 I=1,NDIM		A 260
AUX(16,I)=0.		A 270
AUX(15,I)=DERY(I)		A 280
50 AUX(1,I)=Y(I)		A 290
IF (H*(PRMT(2)-X)) 70,60,80		A 300
C		A 310
C ERROR RETURNS		A 320
60 IHLF=12		A 330
GO TO 80		A 340
70 IHLF=13		A 350
C		A 360
C COMPUTATION OF DERY FOR STARTING VALUES		A 370
80 ISW2=1		A 380
GO TO 10		A 390
C		A 400
C RECORDING OF STARTING VALUES		A 410
90 CALL OUTP (X,Y,DERY,IHLF,NDIM,PRMT)		A 420S
IF (PRMT(5)) 110,100,110		A 430
100 IF (IHLF) 120,120,110		A 440
110 RETURN		A 450
120 DO 130 I=1,NDIM		A 460
130 AUX(8,I)=DERY(I)		A 470
C		A 480
C COMPUTATION OF AUX(2,I)		A 490
ISW1=1		A 500
GO TO 400		A 510
C		A 520
140 X=X+H		A 530
DO 150 I=1,NDIM		A 540
150 AUX(2,I)=Y(I)		A 550
C		A 560
C INCREMENT H IS TESTED BY MEANS OF BISECTION		A 570
160 IHLF=IHLF+1		A 580



	X=X+H	A 590
	DO 170 I=1,NDIM	A 600
170	AUX(4,I)=AUX(2,I)	A 610
	H=.5*H	A 620
	N=1	A 630
	ISW1=2	A 640
	GO TO 400	A 650
C		A 660
180	X=X+H	A 670
	ISW2=5	A 680
	GO TO 10	A 690
190	N=2	A 700
	DO 200 I=1,NDIM	A 710
	AUX(2,I)=Y(I)	A 720
200	AUX(9,I)=DERY(I)	A 730
	ISW1=3	A 740
	GO TO 400	A 750
C		A 760
C	COMPUTATION OF TEST VALUE DELT	A 770
210	DELT=0.	A 780
	DO 220 I=1,NDIM	A 790
C	118 DELT=DELT+AUX(15,I)*ABS(Y(I)-AUX(4,I))	A 800
	IF (Y(I).EQ.0.0) GO TO 220	A 810
	DELT=DELT+AUX(15,I)*ABS((Y(I)-AUX(4,I))/Y(I))	A 820
220	CONTINUE	A 830
	DELT=.06666667*DELT	A 840
	IF (ABS(DELT)-PRMT(4)) 250,250,230	A 850
230	IF (IMLF-10) 160,240,240	A 860
C		A 870
C	NO SATISFACTORY ACCURACY AFTER 10 BISECTIONS. ERROR MESSAGE.	A 880
240	IMLF=11	A 890
	X=X+H	A 900
	GO TO 80	A 910
C		A 920
C	SATISFACTORY ACCURACY AFTER LESS THAN 11 BISECTIONS	A 930
250	X=X+H	A 940
	ISW2=6	A 950
	GO TO 10	A 960
260	DO 270 I=1,NDIM	A 970
	AUX(3,I)=Y(I)	A 980
270	AUX(10,I)=DERY(I)	A 990
	N=3	A1000
	ISW1=4	A1010
	GO TO 400	A1020
C		A1030
280	N=1	A1040
	X=X+H	A1050
	ISW2=7	A1060
	GO TO 10	A1070
290	X=PRMT(1)	A1080
	DO 300 I=1,NDIM	A1090
	AUX(11,I)=DERY(I)	A1100
300	Y(I)=AUX(1,I)+H*(.375*AUX(8,I)+.7916667*AUX(9,I)-.2083333*AUX(10,I)	A1110
	1)+.04166667*DERY(I))	A1120
310	X=X+H	A1130
	N=N+1	A1140
	ISW2=12	A1150
	GO TO 10	A1160
320	CALL OUTP (X,Y,DERY,IMLF,NDIM,PRMT)	A1170S

	IF (PRMT(5)) 110,330,110	A1180
330	IF (N=4) 340,480,480	A1190
340	DO 350 I=1,NDIM	A1200
	AUX(N,I)=Y(I)	A1210
350	AUX(N+7,I)=DERY(I)	A1220
	IF (N=3) 360,380,480	A1230
C		A1240
360	DO 370 I=1,NDIM	A1250
	DELT=AUX(9,I)+AUX(9,I)	A1260
	DELT=DELT*DELT	A1270
370	Y(I)=AUX(1,I)+.3333333*H*(AUX(8,I)+DELT*AUX(10,I))	A1280
	GO TO 310	A1290
C		A1300
380	DO 390 I=1,NDIM	A1310
	DELT=AUX(9,I)+AUX(10,I)	A1320
	DELT=DELT*DELT*DELT	A1330
390	Y(I)=AUX(1,I)+.375*H*(AUX(8,I)+DELT*AUX(11,I))	A1340
	GO TO 310	A1350
C		A1360
C	THE FOLLOWING PART OF SUBROUTINE HPCL COMPUTES BY MEANS OF	A1370
C	RUNGE-KUTTA METHOD STARTING VALUES FOR THE NOT SELF-STARTING	A1380
C	PREDICTOR-CORRECTOR METHOD.	A1390
400	Z=X	A1400
	DO 410 I=1,NDIM	A1410
	XX=H*AUX(N+7,I)	A1420
	AUX(5,I)=XX	A1430
410	Y(I)=AUX(N,I)+.4*XX	A1440
C	XX IS AN AUXILIARY STORAGE LOCATION	A1450
C		A1460
	X=Z+.4*H	A1470
	ISW2=2	A1480
	GO TO 10	A1490
420	DO 430 I=1,NDIM	A1500
	XX=H*DERY(I)	A1510
	AUX(6,I)=XX	A1520
430	Y(I)=AUX(N,I)+.2969776*AUX(5,I)+.1587596*XX	A1530
C		A1540
	X=Z+.4557372*H	A1550
	ISW2=3	A1560
	GO TO 10	A1570
440	DO 450 I=1,NDIM	A1580
	XX=H*DERY(I)	A1590
	AUX(7,I)=XX	A1600
450	Y(I)=AUX(N,I)+.2181004*AUX(5,I)-3.050965*AUX(6,I)+3.832865*XX	A1610
C		A1620
	X=Z+H	A1630
	ISW2=4	A1640
	GO TO 10	A1650
460	DO 470 I=1,NDIM	A1660
470	Y(I)=AUX(N,I)+.1747603*AUX(5,I)-.5514807*AUX(6,I)+1.205536*AUX(7,I)	A1670
	+1.1711848*H*DERY(I)	A1680
	X=Z	A1690
	GO TO (140,180,210,280), ISW1	A1700
C		A1710
C	POSSIBLE BREAK-POINT FOR LINKAGE	A1720
C		A1730
C	STARTING VALUES ARE COMPUTED.	A1740
C	NOW START HAMMINGS MODIFIED PREDICTOR-CORRECTOR METHOD.	A1750
480	ISTEP=3	A1760

490	IF (N=8) 520,500,520	A1770
C		A1780
C	N=8 CAUSES THE ROWS OF AUX TO CHANGE THEIR STORAGE LOCATIONS	A1790
500	DO 510 N=2,7	A1800
	DO 510 I=1,NDIM	A1810
	AUX(N-1,I)=AUX(N,I)	A1820
510	AUX(N+6,I)=AUX(N+7,I)	A1830
	N=7	A1840
C		A1850
C	N LESS THAN 8 CAUSES N+1 TO GET N	A1860
520	N=N+1	A1870
C		A1880
C	COMPUTATION OF NEXT VECTOR Y	A1890
	DO 530 I=1,NDIM	A1900
	AUX(N-1,I)=Y(I)	A1910
530	AUX(N+6,I)=DERY(I)	A1920
	X=X+H	A1930
540	ISTEP=ISTEP+1	A1940
	DO 550 I=1,NDIM	A1950
	DELT=AUX(N-4,I)+1.333333*H*(AUX(N+6,I)+AUX(N+6,I)-AUX(N+5,I)+AUX(N	A1960
	1+4,I)+AUX(N+4,I))	A1970
	Y(I)=DELT-.9256198*AUX(16,I)	A1980
550	AUX(16,I)=DELT	A1990
C	PREDICTOR IS NOW GENERATED IN ROW 16 OF AUX, MODIFIED PREDICTOR	A2000
C	IS GENERATED IN Y. DELT MEANS AN AUXILIARY STORAGE.	A2010
	ISW2=8	A2020
	GO TO 10	A2030
C	DERIVATIVE OF MODIFIED PREDICTOR IS GENERATED IN DERY	A2040
C		A2050
560	DO 570 I=1,NDIM	A2060
	DELT=.125*(9.*AUX(N-1,I)-AUX(N-3,I)+3.*H*(DERY(I)+AUX(N+6,I)+AUX(N	A2070
	1+6,I)-AUX(N+5,I))	A2080
	AUX(16,I)=AUX(16,I)-DELT	A2090
570	Y(I)=DELT+.07438017*AUX(16,I)	A2100
C		A2110
C	TEST WHETHER H MUST BE HALVED OR DOUBLED	A2120
	DELT=0.	A2130
	DO 580 I=1,NDIM	A2140
	IF (Y(I).EQ.0,0) GO TO 580	A2150
C	310 DELT=DELT+AUX(15,I)*ABS(AUX(16,I))	A2160
	DELT=DELT+AUX(15,I)*ABS(AUX(16,I)/Y(I))	A2170
580	CONTINUE	A2180
	IF (ABS(DELT)-PRMT(4)) 590,720,720	A2190
C		A2200
C	H MUST NOT BE HALVED. THAT MEANS Y(I) ARE GOOD.	A2210
590	ISW2=9	A2220
	GO TO 10	A2230
600	CALL OUTP (X,Y,DERY,IHLF,NDIM,PRMT)	A2240
	IF (PRMT(5)) 620,610,620	A2250
610	IF (IHLF-11) 630,620,620	A2260
620	RETURN	A2270
630	IF (H*(X-PRMT(2))) 640,620,620	A2280
640	IF (ABS(X-PRMT(2))-1*ABS(H)) 620,650,650	A2290
650	IF (ABS(DELT)-.02*PRMT(4)) 660,660,490	A2300
C		A2310
C		A2320
C	H COULD BE DOUBLED IF ALL NECESSARY PRECEEDING VALUES ARE	A2330
C	AVAILABLE	A2340
660	IF (IHLF) 490,490,670	A2350



670	IF (N-7) 490,680,680	A2360
680	IF (ISTEP=4) 490,690,690	A2370
690	IMOD=ISTEP/2	A2380
	IF (ISTEP-IMOD-IMOD) 490,700,490	A2390
700	H=H+H	A2400
	IHLF=IHLF-1	A2410
	ISTEP=0	A2420
	DO 710 I=1,NDIM	A2430
	AUX(N-1,I)=AUX(N-2,I)	A2440
	AUX(N-2,I)=AUX(N-4,I)	A2450
	AUX(N-3,I)=AUX(N-6,I)	A2460
	AUX(N+6,I)=AUX(N+5,I)	A2470
	AUX(N+5,I)=AUX(N+3,I)	A2480
	AUX(N+4,I)=AUX(N+1,I)	A2490
	DELT=AUX(N+6,I)+AUX(N+5,I)	A2500
	DELT=DELT+DELT+DELT	A2510
710	AUX(16,I)=8.962963*(Y(I)-AUX(N-3,I))-3.361111*H*(DERY(I)+DELT+AUX(N+4,I))	A2520
	GO TO 490	A2530
		A2540
		A2550
C		A2560
C	H MUST BE HALVED	A2570
720	IHLF=IHLF+1	A2580
	IF (IHLF-10) 730,730,590	A2590
730	H=.5*H	A2600
	ISTEP=0	A2610
	DO 740 I=1,NDIM	A2620
	Y(I)=.00390625*(80.*AUX(N-1,I)+135.*AUX(N-2,I)+40.*AUX(N-3,I)+AUX(N-4,I))-0.1171875*(AUX(N+6,I)-6.*AUX(N+5,I)-AUX(N+4,I))*H	A2630
	AUX(N-4,I)=.00390625*(12.*AUX(N-1,I)+135.*AUX(N-2,I)+108.*AUX(N-3,I)+AUX(N-4,I))-0.234375*(AUX(N+6,I)+18.*AUX(N+5,I)-9.*AUX(N+4,I))*2H	A2640
	AUX(N-3,I)=AUX(N-2,I)	A2650
740	AUX(N+4,I)=AUX(N+5,I)	A2660
	DEL=X-H	A2670
	X=DEL-(H+H)	A2680
	ISW2=10	A2690
	GO TO 10	A2700
750	DO 760 I=1,NDIM	A2710
	AUX(N-2,I)=Y(I)	A2720
	AUX(N+5,I)=DERY(I)	A2730
760	Y(I)=AUX(N-4,I)	A2740
	X=X-(H+H)	A2750
	ISW2=11	A2760
	GO TO 10	A2770
770	X=DEL	A2780
	DO 780 I=1,NDIM	A2790
	DELT=AUX(N+5,I)+AUX(N+4,I)	A2800
	DELT=DELT+DELT+DELT	A2810
	AUX(16,I)=8.962963*(AUX(N-1,I)-Y(I))-3.361111*H*(AUX(N+6,I)+DELT+DERY(I))	A2820
780	AUX(N+3,I)=DERY(I)	A2830
	GO TO 540	A2840
	END	A2850
		A2860
		A2870
		A2880
		A2890-



```

•DECK AFCT
SUBROUTINE AFCT (X,A,Y)
DIMENSION A(1),Y(1)
      COMPLEX ACF,BCF,CCF,DCF
DO 10 I=1,16
10 A(I)=0.0
CALL COEF (X,ACF,BCF,CCF,DCF)
A(3)=REAL (ACF)
A(3)=-A(3)
A(8)=A(3)
A(9)=REAL (BCF)
A(14)=A(9)
A(10)=AIMAG (BCF)
A(13)=-A(10)
A(7)=AIMAG (ACF)
A(4)=-A(7)
RETURN
END

```

```

B 10
B 20
B 30
B 40
B 50
B 60$
B 70
B 80
B 90
B 100
B 110
B 120
B 130
B 140
B 150
B 160
B 170-

```

```
*DECK FCT
SUBROUTINE FCT (X,F)
DIMENSION F(1)
F(1)=0.
F(2)=0.
F(3)=0.
F(4)=0.
RETURN
END
```

```
C 10
C 20
C 30
C 40
C 50
C 60
C 70
C 80-
```

•DECK	OUTP		
	SUBROUTINE	OUTP (X,Y,DERY,IHLF,NDIM,PRMT)	D 10
		DIMENSION Y(1),DERY(1),PRMT(1)	D 20
		COMMON YPU(450,5)	D 30
		COMPLEX ZDUM,SAVF,SAVFM	D 40
		COMPLEX SAV	D 50
		COMMON/CRIT/ ICC,RC,XMC(16),XTC(16),YCR	D 60
		COMMON/SF/ SAVF	D 70
		COMMON/STYPE/ MTYPS	D 80
		COMMON/CI/ IR,IW,NOUT,ICHECK	D 90
		COMMON/BJ/ M,KW,CANG,PI,BV,CV,TJR,G	D 100
		COMMON/JB/ M1,M1D,M1DD,TR,TRD,TRDD	D 110
		COMMON/BN/ NCEO,NCJ,NUT	D 120
		COMMON /SRDCSD/ SAV(450)	D 130
		REAL M,KW,M1,M1D,M1DD	D 140
		XDUM=X	D 150
		IF (ICC.GT.3) XDUM=YCR*RC*COS(X)	D 160
		IF (XDUM.LT.PRMT(6).OR.XDUM.GT.PRMT(8)) GO TO 20	D 170
		NOUT=NOUT+1	D 180
		IF (NOUT.GT.450) WRITE (IW,50) X	D 190*
		IF (NOUT.GT.450) RETURN	D 200
		IF (ICC.GT.3) GO TO 30	D 210
		YPU(NOUT,1)=X	D 220
		DO 10 I=1,NDIM	D 230
10		YPU(NOUT,I+1)=Y(I)*(1.0-M1*CANG)**(MTYPS-3)	D 240
		SAV(NOUT)=SAVF	D 250
20		CONTINUE	D 260
		IF (IFIX(PRMT(7)).EQ.0) RETURN	D 270
		IF (NOUT.GT.450) WRITE (6,40) X	D 280*
		WRITE (IW,50) X,Y(I),Y(3),M1,M1D,TR,TRD,IHLF	D 290*
		RETURN	D 300
30		CONTINUE	D 310
		SAVFM=SAVF**(3-MTYPS)	D 320
		YPU(NOUT,1)=XDUM	D 330
		ZDUM=CMPLX(Y(1),Y(2))/SAVFM	D 340
		YPU(NOUT,2)=REAL(ZDUM)	D 350
		YPU(NOUT,3)=AIMAG(ZDUM)	D 360
		ZDUM=CMPLX(Y(3),Y(4))/SAVFM	D 370
		YPU(NOUT,4)=REAL(ZDUM)	D 380
		YPU(NOUT,5)=AIMAG(ZDUM)	D 390
		SAV(NOUT)=SAVF	D 400
		GO TO 20	D 410
			D 420
C	40	FORMAT (1X,"STORAGE OVERFLOW - TRY LARGER STEP SIZE. X = ",E13.6)	D 430
	50	FORMAT (1X,7E11.4,I1)	D 440
		END	D 450-

*DECK	COEF		
	SUBROUTINE	COEF (X,ACF,BCF,CCF,DCF)	E 10
C	CHECK	FOR 2-D CASE	E 20
	REAL	M,KW,M1,MID,MIDD	E 30
	COMMON	/CI/ IR,IW,NOUT,ICHECK	E 40
	COMMON	/BJ/ M,KW,CANG,PI,BV,CV,TJR,G	E 50
	COMMON	/JB/ M1,MID,MIDD,TR,TRD,TRDD	E 60
	COMMON	/CRIT/ICC,RC,XMC(16),XTC(16),YCR	E 70
	COMMON	/BN/ NCEO,NCJ,NUT	E 80
	COMMON	/SF/ SAVF	E 90
	COMPLEX	SAVF	E 100
	COMPLEX	CMPLX,CEXP	E 110
	COMPLEX	ACF,BCF,CCF,DCF,ZERO,FAC,J,WUN,MPHI,CXJJ	E 120
	COMPLEX	MPHIX	E 130
	COMPLEX	TPHI,TPHIX,CSIG	E 140
	DIMENSION	YMC(3)	E 150
	DIMENSION	YTC(3)	E 160
	ZERO	=(0.0,0.0)	E 170
	J	=(0.0,1.0)	E 180
	WUN	=(1.0,0.0)	E 190
	IF	(ICC.GT.3) GO TO 20	E 200
	CALL	VELT (X,M,TJR,BV,CV,G,YMC,YTC,ICC)	E 210
	M1	=YMC(1)	E 220
	TR	=YTC(1)	E 230
	IF	(ICC.EQ.1) GO TO 10	E 240
	IF	(X.LT.0.) YMC(2)=-YMC(2)	E 250
	IF	(X.LT.0.) YTC(2)=-YTC(2)	E 260
	MID	=YMC(2)	E 270
	TRD	=YTC(2)	E 280
	MIDD	=YMC(3)	E 290
	TRDD	=YTC(3)	E 300
10	CONTINUE		E 310
	V	=1.0-M1*CANG	E 320
	SAVF	=CMPLX(V,0.0)	E 330
	P	=V*V/TR	E 340
	ACF	=CMPLX(KW*KW*(P-CANG*CANG)/P,0.0)	E 350
	IF	(NCEO.GT.0) ACF=X*ACF-NCJ*NCJ/(X*P)	E 360
	BCF	=CMPLX(P,0.0)	E 370
	IF	(NCEO.GT.0) BCF=BCF/X	E 380
	CCF	=ZERO	E 390
	DCF	=ZERO	E 400
	RETURN		E 410
20	CONTINUE		E 420
	MPHI	=ZERO	E 430
	TPHI	=ZERO	E 440
	MPHIX	=ZERO	E 450
	TPHIX	=ZERO	E 460
	CSIG	=RC*CEXP(J*X)	E 470
	CXJJ	=WUN	E 480
	FAC	=WUN	E 490
	DO	40 JJ=1,ICC	E 500
	MPHI	=MPHI+XMC(JJ)*FAC/CXJJ	E 510
	TPHI	=TPHI+XTC(JJ)*FAC/CXJJ	E 520
	IF	(CABS((MPHI-MPHIX)/MPHI).GT..0001) GO TO 30	E 530
	IF	(CABS((TPHI-TPHIX)/TPHI).LT..0001) GO TO 50	E 540
30	CONTINUE		E 550
	MPHIX	=MPHI	E 560
	TPHIX	=TPHI	E 570
	FAC	=FAC*CSIG	E 580



	XJJ=JJ	E 590
	CXJJ=CMPLX(XJJ,0.0)*CXJJ	E 600
40	CONTINUE	E 610
	STOP 7	E 620
50	CONTINUE	E 630
	FAC=WUN-MPHI*CANG	E 640
	SAVF=FAC	E 650
	FAC=FAC*FAC/TPHI	E 660
	ACF=J*CSIG*KW*KW*(WUN-CANG*CANG/FAC)	E 670
	IF (NGEO.EQ.1) ACF=(YCR*CSIG)*ACF-NCJ*NCJ/(FAC*(YCR*CSIG))*J*CSIG	E 680
	BCF=J*CSIG*FAC	E 690
	IF (NGEO.EQ.1) BCF=BCF/(YCR*CSIG)	E 700
	CCF=ZERO	E 710
	DCF=ZERO	E 720
	IF (JJ.EQ.ICC) ICHECK=1	E 730
C	WRITE(IW,400) MPHI,TPHI,ACF,JJ,ICC	E 740
C	400 FORMAT(1X,6E13.6/1X,2I5)	E 750
	M1=REAL(MPHI)	E 760
	TR=REAL(TPHI)	E 770
	M1D=XMC(2)	E 780
	TRD=XTC(2)	E 790
	M1DD=XMC(3)	E 800
	TRDD=XTC(3)	E 810
	RETURN	E 820
	END	E 830-

```
•DECK TRANS
  SUBROUTINE TRANS (ST2,Y,NDIM)
    DIMENSION ST2(1),Y(1)
    DO 10 I=1,NDIM
      Y(I)=ST2(I)
10 CONTINUE
  RETURN
  END
```

```
F 10
F 20
F 30
F 40
F 50
F 60
F 70-
```

```

•DECK WRCAL
SUBROUTINE WRCAL (NGEO,Y,RADM,RPRES,FWRONS)      G 10
  COMPLEX CMLX                                  G 20
  COMPLEX RADM,RPRES,FWRONS ,WRONSK             G 30
  DIMENSION Y(1)                                G 40
  PI=3.141593                                    G 50
  WRONSK=(1.,0.)                                 G 60
  IF (NGEO.EQ.1) WRONSK=CMLX(0.,-2./PI)         G 70
  FWRONS=(CMLX(Y(1),Y(2))*RADM-CMLX(Y(3),Y(4)))*RPRES G 80
  FWRONS=WRONSK/FWRONS                           G 90
  RETURN                                          G 100
  END                                             G 110-

```

*DECK TCON		
SUBROUTINE TCON (MS,NCJX,NCJNX,TIJ,TX,ECON,NCON,MXOS)		H 10
DIMENSION TIJ(7,1),TX(1)		H 20
IF (NCJX.EQ.NCJNX) GO TO 20		H 30
IF (NCJX.LT.3) GO TO 20		H 40
ICT=0		H 50
DO 10 I=1,7		H 60
IF (TIJ(I,MS).EQ.0.) GO TO 10		H 70
IF (TX(I)/TIJ(I,MS).LT.ECON) NCON=NCON+1		H 80
IF (TX(I)/TIJ(I,MS).LT.ECON/100.) ICT=ICT+1		H 90
10 CONTINUE		H 100
IF (ICT.EQ.7) MXOS=MXOS+1		H 110
20 DO 30 I=1,7		H 120
TIJ(I,MS)=TIJ(I,MS)+TX(I)		H 130
30 CONTINUE		H 140
RETURN		H 150
END		H 160-



*DECK	TSIGN	
	SUBROUTINE	TSIGN (MS, TIJ)
		DIMENSION
		TIJ(6,1)
		COMMON/CI/
		IR, IW, NOUT, ICHECK
	DO	20 I=1,6
	IF	(TIJ(I,MS).GT.0.) GO TO 10
	WRITE	(IW,30) I, TIJ(I,MS)
		TIJ(I,MS)=-TIJ(I,MS)
	IF	(TIJ(I,MS).EQ.0.) TIJ(I,MS)=1.
10	CONTINUE	
20	CONTINUE	
	RETURN	
C		
30	FORMAT	(1X,13H**SOURCE TYPE,I5,2HIS,E13.6)
	END	

I 10  
I 20  
I 30  
I 40  
I 50  
I 60\*  
I 70  
I 80  
I 90  
I 100  
I 110  
I 120  
I 130  
I 140-

*DECK RADCSO		J	10
SUBROUTINE RADCSO (IFLAG,NCJ,WINV,D, ID,NOUTM,BV,CV)		J	20
DIMENSION D(1),ID(1),XM(2),XT(2),SLTB(5),A(5,7),TIJ(7,5)		J	30
DIMENSION SSIM(5),SSID(5),SSIQ(5)		J	40
COMPLEX C(450,7)		J	50
COMPLEX WINV,TRRN,RES		J	60
COMPLEX SAV		J	70
REAL M,KW		J	80
COMMON YPU(450,5)		J	90
COMMON /SRDCSD/ SAV(450)		J	100
COMMON/PSD/ RC,BLTB,CVD		J	110
C	RPI=1.772424	J	120
	CVD=CV	J	130
	G=D(8)	J	140
	RSW=D(9)	J	150
	RSC=D(10)	J	160
	KW=D(11)	J	170
	XKW2=KW*KW	J	180
	M=D(12)	J	190
	TJR=D(13)	J	200
	CANG=D(14)	J	210
	X1=D(16)	J	220
	TCOR=D(18)	J	230
	DCOR=D(19)	J	240
C		J	250
	IW=ID(2)	J	260
	NGEO=ID(3)	J	270
	MTYPS=ID(4)	J	280
	IWB=ID(8)	J	290
	NCL=ID(25)	J	300
	IO=ID(26)	J	310
C	GO AND FORM SIO,SID IF THIS IS FINAL CALL	J	320
	IF (IFLAG.GT.0) GO TO 70	J	330
	DO 10 IT=1,NCL	J	340
C	SLTB(IT)=D(IT+24)*X1	J	350
	SLTB(IT)=D(IT+25)	J	360
10	CONTINUE	J	370
	AWINV=CABS(WINV)	J	380
	RC=RSC*X1+1.0	J	390
	R99=BV*SQRT(ALOG(1.0/0.99))	J	400
	IF (CV.EQ.0.0.AND.RC.LT.R99) RC=R99	J	410
	IF (RC.LE.2.0*D(4)) RC=2.0*D(4)	J	420
	BLTB=0.5*X1*RSW/0.832554611	J	430
	IF (BLTB.LE.0.0) RETURN	J	440
	RCB=RC/BLTB	J	450
	REF=BLTB*BLTB/2.0*(EXP(-RCB*RCB)+RCB*RPI*(1.0+ERF(RCB)))	J	460
	ICC=1	J	470
	CALL VELT (RC,M,TJR,BV,CV,G, XM,XT,ICC)	J	480
	XKAPS2=(1.0-XM(1)*CANG)*(1.0-XM(1)*CANG)/XT(1)-CANG*CANG	J	490
	XKAPS2=ABS(XKAPS2)	J	500
	IF (NCJ,NE,0) GO TO 30	J	510
	DO 20 IT=1,5	J	520
	DO 20 JS=1,7	J	530
20	TIJ(JS,IT)=0.0	J	540
30	CONTINUE	J	550
C	SET UP CNAB FOR ALL SOURCE TYPES	J	560
	ICC=2	J	570
	DO 40 I=1,NOUTM	J	580

R=YPU(I,1)	J 590
CALL VELT (R,M,TJR,BV,CV,G,XM,XT,ICC)	J 600S
PRS=1.0-XM(1)*CANG	J 610
PRS=PRS*PRS/XT(1)	J 620
PQ=(CANG*CANG-PRS)*KW*KW	J 630
PD=-XT(2)/XT(1)-2.0*XM(2)*CANG/(1.0-XM(1)*CANG)	J 640
C(I,1)=CMPLX(YPU(I,2),YPU(I,3))	J 650
C(I,2)=CMPLX(YPU(I,4),YPU(I,5))	J 660
C(I,2)=C(I,2)*PRS/R	J 670
TRRN=(PQ*NCJ*NCJ/(R*R))*C(I,1)+(PD-NGEO/R)*C(I,2)	J 680
C(I,3)=TRRN-(MTYPS-3)*XM(2)*CANG/(1.0-XM(1)*CANG)*C(I,2)	J 690
C(I,4)=NCJ*C(I,1)/R	J 700
C(I,6)=(C(I,2)-NCJ*NCJ*C(I,1)/R)/R	J 710
C(I,7)=C(I,2)	
C(I,2)=C(I,2)-XM(2)*CANG*C(I,1)/SAV(I)	J 720
C(I,5)=NCJ*(C(I,2)-C(I,1)/R)/R	J 730
40 CONTINUE	J 740
DO 60 IT=1,NCL	J 750
IF (SLTB(IT),LT.D(1),OR,BLTB,LT.D(1)) GO TO 60	J 760
DO 50 JS=1,7	J 770
CALL INTRAP (NCJ,YPU(1,1),C(1,JS),NOUTM,SLTB(IT),RES,IERS)	J 780S
IF (CABS(RES),LE.0,0) RES=(1.E-99,0,0)	J 790
C(IT,JS)=RES	J 800
C(IT,JS)=C(IT,JS)*AWINV*AWINV	J 810
ARG=KW*SLTB(IT)/2.0	J 820
IF (SLTB(IT),LT,BLTB/10,0) ARG=0.0	J 830
C(IT,JS)=EXP(ARG*ARG*XKAPS2)*C(IT,JS)	J 840
C(IT,JS)=C(IT,JS)/(REF*SLTB(IT)*SLTB(IT)/2.0)	J 850
TIJ(JS,IT)=TIJ(JS,IT)+CABS(C(IT,JS))	J 860
IF (NCJ,NE,0) TIJ(JS,IT)=TIJ(JS,IT)+CABS(C(IT,JS))	J 870
50 CONTINUE	J 880
SIM=10.0*ALOG10(CABS(C(IT,1)))	J 890
IF (NCJ,EQ,0) SSIM(IT)=SIM	J 900
SIM=SIM-SSIM(IT)	J 910
SID=CABS(C(IT,7))+CABS(C(IT,4))+XKW2*CANG*CANG*CABS(C(IT,1))	J 920
SID=10.0*ALOG10(SID/XKW2)	J 930
IF (NCJ,EQ,0) SSID(IT)=SID	J 940
SID=SID-SSID(IT)	J 950
SIQ=CABS(C(IT,3))+CABS(C(IT,6))+2.0*CABS(C(IT,5))	J 960
SIQ=SIQ*XKW2*XKW2*CANG**4+CABS(C(IT,1))+2.0*CANG**2*XKW2*(CABS(C(I	J 970
IT,2))+CABS(C(IT,4)))	J 980
SIQ=10.0*ALOG10(SIQ/(XKW2*XKW2))	J 990
IF (NCJ,EQ,0) SSIQ(IT)=SIQ	J1000
SIQ=SIQ-SSIQ(IT)	J1010
IF (IO,EQ,0) GO TO 60	J1020
IF (IWB,NE,0) WRITE (IW,100) IERS,SLTB(IT),(TIJ(JS,IT)+JS=1,7),SIM	J1030*
1,SID,SIQ,NCJ	J1040
60 CONTINUE	J1050
GO TO 90	J1060
70 CONTINUE	J1070
DO 80 IT=1,NCL	J1080
IF (SLTB(IT),LT.D(1),OR,BLTB,LT.D(1)) GO TO 80	J1090
A(IT,1)=10.0*ALOG10(TIJ(1,IT))	J1100
A(IT,2)=10.0*ALOG10(TIJ(2,IT)/(0.5*XKW2))	J1110
A(IT,3)=10.0*ALOG10(TIJ(3,IT)/(0.375*XKW2*XKW2))	J1120
A(IT,4)=10.0*ALOG10(TIJ(4,IT)/(0.5*XKW2))	J1130
A(IT,5)=10.0*ALOG10(TIJ(5,IT)/(0.125*XKW2*XKW2))	J1140
A(IT,6)=10.0*ALOG10(TIJ(6,IT)/(0.375*XKW2*XKW2))	J1150
A(IT,7)=10.0*ALOG10(TIJ(7,IT)/(0.5*XKW2))	
SIQ=TIJ(3,IT)+TIJ(6,IT)+2.0*TIJ(5,IT)	J1160
SIQ=SIQ*XKW2*XKW2*(CANG**4)+TIJ(1,IT)+2.0*CANG*CANG*XKW2*(TIJ(2,IT	J1170

1)*TIJ(4,IT)	J1180
SIQ=10.0*ALOG10(SIQ/(XKW2*XKW2))	J1190
SIQ=SIQ*TCOR	J1200
SID=TIJ(7,IT)+TIJ(4,IT)*XKW2*CANG*CANG*TIJ(1,IT)	J1210
SID=10.0*ALOG10(SID/XKW2)	J1220
SID=SID*DCOR	J1230
IF (IO.EQ.0) GO TO 80	J1240
IF (IWB.NE.0) WRITE (IW,110) SLTB(IT),(A(IT,JS),JS=1,7),SIQ,SID	J1250
80 CONTINUE	J1260
D(36)=A(IT,1)	J1270
D(37)=SID	J1280
D(38)=SIQ	J1290
90 CONTINUE	J1300
RETURN	J1310
C	J1320
100 FORMAT (1X,I1.11F11.4,I5)	J1330
110 FORMAT (1X,F3.4,14X,9F7.2)	J1340
END	J1350



*DECK	INTRAP	
	SUBROUTINE INTRAP (NCJ,R,CNAB,NOUTM,SLTB,RES,IERS)	K 10
	COMMON/PSD/ RC,BLTB,CVD	K 20
	DIMENSION R(1)	K 30
	COMPLEX CNAB(1),YIN(450),YOUT(450),RES	K 40
	IERS=0	K 50
	RMIN=RC-1.96*BLTB*1.414	K 60
	RMAX=RC+1.96*BLTB*1.414	K 70
	SLTB2=SLTB*SLTB/2.0	K 80
	IZC=0	K 90
	IF (SLTB.LT,BLTB/10.0) IZC=1	K 100
	DO 40 JOUT=1,NOUTM	K 110
	RFIX=R(JOUT)	K 120
	YOUT(JOUT)=(0.0,0.0)	K 130
	IF (RFIX.LT,RMIN.OR,RFIX.GT,RMAX) GO TO 40	K 140
	RFB=RFIX/SLTB	K 150
	IF (IZC.EQ,0) GO TO 10	K 160
	YIN(NOUTM)=CNAB(JOUT)*SRPSD(RFIX)*SLTB2	K 170
	GO TO 30	K 180
10	CONTINUE	K 190
	DO 20 JIN=1,NOUTM	K 200
	YIN(JIN)=(0.0,0.0)	K 210
	RVAR=R(JIN)	K 220
	IF (RVAR.LT,RMIN.OR,RVAR.GT,RMAX) GO TO 20	K 230
	RVB=RVAR/SLTB	K 240
	ARG=2.0*RFB*RVB	K 250
	DR2=(RVB-RFB)*(RVB-RFB)	K 260
C	-675.84,X.741.67 FOR EXP(X) ON CDC 7600	K 270
	IF (DR2.GT,3.84) GO TO 20	K 280
	CALL BESI (ARG,NCJ,ANS,IER)	K 290\$
	IF (IER.NE,0) IERS=1	K 300
	YIN(JIN)=RVAR*CNAB(JIN)*SRPSD(RVAR)*ANS*EXP(-DR2)	K 310
20	CONTINUE	K 320
	CALL QTFG (R,YIN,YIN,NOUTM)	K 330\$
30	CONTINUE	K 340
	YOUT(JOUT)=RFIX*CONJG(CNAB(JOUT))*SRPSU(RFIX)*YIN(NOUTM)	K 350
40	CONTINUE	K 360
	CALL QTFG (R,YOUT,YOUT,NOUTM)	K 370\$
	RES=YOUT(NOUTM)	K 380
	RETURN	K 390
	END	K 400-

```
•DECK SRPSD
      FUNCTION SRPSD(R)
      COMMON/PSD/ RC,BLTB,CVD
      SRPSD=0.0
      DR=(R-RC)/BLTB
      DR2=DR*DR
      IF (DR2.GT.78.0) GO TO 10
      SRPSD=EXP(-DR2/2.0)
10 CONTINUE
      RETURN
      END
```

```
L 10
L 20
L 30
L 40
L 50
L 60
L 70
L 80
L 90
L 100-
```

```

*DECK BESI
SUBROUTINE BESI (X,N,BI,IER)
C BESI MODIFIED TO COMPUTE EXP(-X)*ORIGINAL
IER=0
BI=1.0
IF (N) 210,20,10
10 IF (X) 220,40,40
20 IF (X) 220,30,40
30 RETURN
40 TOL=1.0E-2
IF (X-12.0) 60,60,50
50 IF (X-FLOAT(N)) 60,60,170
60 XX=X/2.0
TERM=1.0
IF (N) 100,100,70
70 DO 90 I=1,N
FI=I
IF (ABS(TERM)-1.0E-68) 80,90,90
80 IER=3
BI=0.0
RETURN
90 TERM=TERM*XX/FI
100 BI=TERM
XX=XX*XX
DO 120 K=1,1000
C IF (ABS(TERM) - ABS(BI*TOL)) 100,100,80
IF (ABS(TERM)-ABS(BI*TOL)) 130,130,110
C 80 FK=K*(N+K)
110 FK=FLOAT(K)*FLOAT(N+K)
TERM=TERM*(XX/FK)
120 BI=BI*TERM
IER=5
GO TO 160
130 CONTINUE
IF (X-170.0) 150,150,140
140 IER=4
GO TO 160
150 BI=EXP(-X)*BI
160 RETURN
170 FN=4*N*N
C IF (X-170.0) 115,111,111
C 111 IER=4
C RETURN
XX=1.0/(8.0*X)
TERM=1.0
BI=1.0
DO 190 K=1,30
IF (ABS(TERM)-ABS(TOL*BI)) 200,200,180
180 FK=(2*K-1)**2
TERM=TERM*XX*(FK-FN)/FLOAT(K)
190 BI=BI*TERM
GO TO 60
200 PI=3.141592653
C BI=BI*EXP(X)/SQRT(2.0*PI*X)
BI=BI/SQRT(2.0*PI*X)
GO TO 160
210 IER=1
GO TO 160
220 IER=2
GO TO 160
END
M 10
M 20
M 30
M 40
M 50
M 60
M 70
M 80
M 90
M 100
M 110
M 120
M 130
M 140
M 150
M 160
M 170
M 180
M 190
M 200
M 210
M 220
M 230
M 240
M 250
M 260
M 270
M 280
M 290
M 300
M 310
M 320
M 330
M 340
M 350
M 360
M 370
M 380
M 390
M 400
M 410
M 420
M 430
M 440
M 450
M 460
M 470
M 480
M 490
M 500
M 510
M 520
M 530
M 540
M 550
M 560
M 570
M 580
M 590
M 600-

```

*DECK QTFG		
C	.....	N 10
C	SUBROUTINE QTFG	N 20
C		N 30
C	PURPOSE	N 40
C	TO COMPUTE THE VECTOR OF INTEGRAL VALUES FOR A GIVEN	N 50
C	GENERAL TABLE OF ARGUMENT AND FUNCTION VALUES.	N 60
C		N 70
C	DESCRIPTION IS ON PAGE 86 OF IBM-SSP MANUAL	N 80
C		N 90
C	.....	N 100
C	SUBROUTINE QTFG (X,Y,Z,NDIM)	N 110
C		N 120
C	DIMENSION X(1)	N 130
C	COMPLEX Y(1),Z(1),SUM1,SUM2	N 140
C		N 150
C	SUM2=0.0	N 160
C	IF (NDIM-1) 40,30,i0	N 170
C		N 180
C	INTEGRATION LOOP	N 190
C	DO 20 I=2,NDIM	N 200
10	SUM1=SUM2	N 210
	SUM2=SUM2+.5*(X(I)-X(I-1))*(Y(I)+Y(I-1))	N 220
20	Z(I-1)=SUM1	N 230
30	Z(NDIM)=SUM2	N 240
40	RETURN	N 250
	END	N 260
		N 270-



```

*DECK BLKTMN
      BLOCK DATA TMN
C
C      INPUT DATA*****
C      A=ETA (SM)
C      B=SPLNQ (SM)
C      C=CQ (SM)
C      D=SPLND (SM)
C      E=E (SM)
C      F=CD (SM)
C      H=ARGUMENT X IN EXPONENTIAL DECAY FACTOR
C      P=EXPONENTIAL DECAY FACTOR DEC(X) FOR ARGUMENT X
C
C      R=RATIO OF CENTER-LINE VELOCITY TO JET EXIT VELOCITY AT EACH
C      STROUHAL NUMBER
C      U=RATIO OF MEAN VELOCITY TO CENTER-LINE VELOCITY AT EACH
C      STANDARD SOURCE POSITION
C
C      COMMON/FOUR/A (16)
C      COMMON/FIVE/B (16)
C      COMMON/SIX/C (16)
C      COMMON/SEVEN/D (16)
C      COMMON/EIGHT/E (16)
C      COMMON/NINE/F (16)
C      COMMON/ELEVEN/H (7)
C      COMMON/TWELVE/P (7)
C
C      COMMON/FOUR1/ A1 (28)
C      COMMON /FIVE1/ B1 (28)
C      COMMON /SIX1/ C1 (28)
C      COMMON /SEVEN1/ D1 (28)
C      COMMON /EIGHT1/ E1 (28)
C      COMMON /NINE1/ F1 (28)
C      COMMON /EIGHTY1/ SD1 (28,6),SDT1 (28,6)
C
C      COMMON/THIRTN1/ R1 (28)
C      COMMON/THIRTN/R (16)
C      COMMON/FOURTN/U (24)
C
C      COMMON/EIGHTY/T1 (6),SD (16,6)
C
C      DATA (T1(I),I=1,4) / 0.980, 1.770, 2.209, 3.330 /
C      DATA ((SD(N,K),N=1,16),K=1,4) / 0.67,0.80,0.95,1.18,1.31,1.70,
1 2.00,2.30,2.62,2.92,3.23,3.50,3.75,4.00,4.25,4.45,0.67,0.80,
2 0.95,1.18,1.43,1.70,2.00,2.30,2.70,3.10,3.40,3.80,4.18,4.50,
3 4.80,5.15,0.67,0.80,0.95,1.15,1.50,1.90,2.30,2.72,3.14,3.55,
4 3.95,4.38,4.75,5.12,5.40,5.60,0.67,0.80,0.95,1.20,1.55,2.00,
5 2.50,2.90,3.45,3.90,4.35,4.75,5.10,5.35,5.60,5.80 /
C
C      DATA ((SDT1(N,I),N=1,28),I=1,4) /
10.01,0.01,0.01,0.01,0.01,0.01,0.05,0.13,0.30,0.52,0.80,1.05,1.30,
21.50,1.75,1.90,2.05,2.18,2.30,2.40,2.50,2.60,2.69,2.79,2.89,2.96,
33.03,3.09,
40.08,0.09,0.11,0.12,0.15,0.23,0.32,0.45,0.65,0.90,1.20,1.50,1.80,
52.10,2.35,2.55,2.70,2.90,3.03,3.17,3.30,3.43,3.55,3.67,3.79,3.89,
63.98,4.06,
70.20,0.22,0.25,0.28,0.31,0.39,0.53,0.70,0.95,1.25,1.60,1.95,2.25,
82.55,2.85,3.05,3.30,3.50,3.70,3.90,4.06,4.23,4.39,4.56,4.71,4.84,
0 10
0 20
0 30
0 40
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	94.94,5.04.	0 590
	\$0.25,0.28,0.32,0.36,0.45,0.57,0.75,0.95,1.25,1.60,2.00,2.35,2.70.	0 600
	\$3.00,3.30,3.60,3.85,4.10,4.30,4.50,4.70,4.80,5.10,5.24,5.42,5.56.	0 610
	\$5.68,5.80/	0 620
C		0 630
	DATA ((SD1(N,I),N=1,28),I=1,4)/	0 640
	1 0.11,0.14,0.18,0.23,0.31,0.45,0.65,0.85,1.10,1.35,1.60,1.85,2.20.	0 650
	2 2.55,3.00,3.30,3.60,3.85,4.10,4.45,4.75,5.10,5.32,5.53,5.71,5.86.	0 660
	3 5.99,6.11.	0 670
	4 0.11,0.14,0.18,0.23,0.31,0.45,0.65,0.85,1.10,1.35,1.60,1.85,2.25.	0 680
	5 2.70,3.15,3.50,3.95,4.30,4.70,5.00,5.30,5.58,5.82,6.04,6.24,6.41.	0 690
	6 6.55,6.68.	0 700
	7 0.11,0.14,0.18,0.25,0.35,0.50,0.70,0.95,1.25,1.55,1.90,2.25,2.75.	0 710
	8 3.25,3.75,4.20,4.60,5.00,5.35,5.65,5.95,6.26,6.53,6.78,7.01,7.19.	0 720
	9 7.35,7.50.	0 730
	\$ 0.11,0.14,0.18,0.25,0.35,0.50,0.77,1.10,1.50,1.85,2.25,2.75,3.25.	0 740
	\$ 3.80,4.30,4.75,5.20,5.55,5.85,6.13,6.40,6.74,7.03,7.29,7.54,7.74.	0 750
	\$ 7.91,8.07 /	0 760
C		0 770
	DATA A(1),A(2),A(3),A(4),A(5),A(6),A(7),A(8),A(9),A(10),A(11),	0 780
	1 A(12),A(13),A(14),A(15),A(16)/0.5,0.52,0.54,0.56,0.57,0.58,0.585.	0 790
	2 0.59,0.595,0.598,0.6,0.6,0.6,0.6,0.6,0.6/	0 800
C		0 810
	DATA A1/ 0.32,0.36,0.40,0.44,0.47,0.5,0.52,0.54,0.56,0.57,0.58,	0 820
	1 0.585,0.59,0.595,0.598,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,	0 830
	2 0.6,0.6,0.6 /	0 840
C		0 850
	DATA B(1),B(2),B(3),B(4),B(5),B(6),B(7),B(8),B(9),B(10),B(11),	0 860
	1 B(12),B(13),B(14),B(15),B(16)/81.5,83.5,85.2,86.9,88.2,89.4,90.4.	0 870
	2 91.2,91.8,92.1,92.2,92.2,92.1,92.0,91.9,91.6/	0 880
C		0 890
	DATA B1/ 70.5,73.5,75.5,78.0,79.9,81.5,83.1,84.6,86.2,87.7,89.0.	0 900
	1 90.0,90.7,91.3,91.8,92.1,92.1,92.0,91.9,91.7,91.4,90.8,90.3,	0 910
	2 89.7,89.2,88.6,88.1,87.5 /	0 920
C		0 930
	DATA C(1),C(2),C(3),C(4),C(5),C(6),C(7),C(8),C(9),C(10),C(11),	0 940
	1 C(12),C(13),C(14),C(15),C(16)/0.75,0.75,0.75,1.1,1.0,1.0,1.0,1.1.	0 950
	2 0.75,0.5,0.3,0.1,0.0,-0.2,-0.4,-0.5/	0 960
C		0 970
	DATA C1/ 7.0,5.0,4.0,3.0,3.0,2.3,1.5,1.0,1.0,1.2,1.2,1.0,0.9,0.7.	0 980
	1 0.6,0.3,0.1,0.0,-0.15,-0.25,-0.4,-0.4,-0.5,-0.55,-0.6,-0.65,	0 990
	2 -0.7,-0.7 /	01000
C		01010
	DATA D(1),D(2),D(3),D(4),D(5),D(6),D(7),D(8),D(9),D(10),D(11),	01020
	1 D(12),D(13),D(14),D(15),D(16)/93.2,95.3,97.0,98.4,99.4,100.1,	01030
	2 100.7,100.9,100.9,100.8,100.6,100.1,99.5,98.7,97.8,96.9/	01040
C		01050
	DATA D1/ 82.0,84.4,86.6,88.8,91.0,93.1,95.2,97.0,98.3,99.4,100.1.	01060
	1 100.6,101.0,101.1,101.0,100.6,100.0,99.3,98.5,97.6,96.6,95.8,	01070
	2 94.9,94.0,93.0,92.0,91.0,90.0 /	01080
C		01090
	DATA E(1),E(2),E(3),E(4),E(5),E(6),E(7),E(8),E(9),E(10),E(11),	01100
	1 E(12),E(13),E(14),E(15),E(16)/0.8,0.77,0.75,0.7,0.68,0.66,0.63,	01110
	2 0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6/	01120
C		01130
	DATA E1/ 1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,0.9,0.8,0.73,0.68,0.65,	01140
	1 0.63,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6 /	01150
C		01160
	DATA F(1),F(2),F(3),F(4),F(5),F(6),F(7),F(8),F(9),F(10),F(11),	01170

	1 F(12),F(13),F(14),F(15),F(16)/2.3,2.0,1.5,1.3,1.0,0.8,0.6,0.5,	01180
	2 0.3,0.1,-0.15,-0.2,-0.35,-0.4,-0.4,-0.4/	01190
C		01200
	DATA F1/ 15.0,10.0,10.0,7.5,6.0,4.5,3.0,1.7,1.3,1.0,0.8,0.6,0.3,	01210
	1 0.2,0.0,-0.15,-0.2,-0.3,-0.3,-0.4,-0.4,-0.5,-0.55,-0.6,-0.62,	01220
	2 -0.62,-0.65,-0.7 /	01230
C		01240
	DATA H(1),H(2),H(3),H(4),H(5),H(6),H(7)/0.0,0.1,0.2,0.3,0.4,0.5,	01250
	1 0.6/	01260
C		01270
	DATA P(1),P(2),P(3),P(4),P(5),P(6),P(7)/1.0,0.59,0.4,0.28,0.2,	01280
	1 0.158,0.128/	01290
C		01300
	DATA R/ 0.58,0.65,0.74,0.82,0.9,0.95,0.99,1.0,1.0,1.0,1.0,1.0,1.0,	01310
	1 1.0,1.0,1.0 /	01320
C		01330
	DATA R1 / 0.32,0.36,0.4,0.46,0.52,0.58,0.65,0.74,0.82,0.90,0.96,	01340
	1 1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,	01350
	2 1.0,1.0 /	01360
C		01370
	DATA U(1),U(2),U(3),U(4),U(5),U(6),U(7),U(8),U(9),U(10),U(11),	01380
	1 U(12),U(13),U(14),U(15),U(16),U(17),U(18),U(19),U(20),U(21),	01390
	2 U(22),U(23),U(24)/0.99,0.98199,0.968865,0.9481,0.91859,0.87741,	01400
	3 0.82377,0.757455,0.67936,0.67,0.66295,0.6,0.591905,0.5,0.408098,	01410
	4 0.3206435,0.2425485,0.1762325,0.1225905,0.081409,0.051541,	01420
	5 0.0311374,0.018008,0.01/	01430
C		01440
	END	01450-



*DECK	SANOISE	P	10
	SUBROUTINE SANOISE (BETA,TJTO,ROD,BC,DFT,A0,NFREQ,FREQ,I,J,TM,L0,M	P	20
	1J,DF,WORK2,NS,SPLC,HXX,HYY,CYY,A3,A2)	P	30
	DIMENSION TM(20),FREQ(20),SPLC(30),HVX(30),HVV(30),CVX(30),	P	40
	1 CVY(30),ANS3DB(30)	P	50
	COMMON / THIRTY / HX(20)	P	60
	COMMON / FORTY / HY(20)	P	70
	COMMON / FIFTY / CX(20)	P	80
	COMMON / SIXTY / CY(20)	P	90
	REAL MJ,K0,K1,L0,L1,MC	P	100
	IF (J,NE,1,OR,I,NE,1) GO TO 50	P	110
C		P	120
C	CALCULATION OF OASPLC (PACKAGE C)	P	130
C		P	140
	IF (BETA.GT.1.0) GO TO 20	P	150
	IF (TJTO.LT.0.9) GO TO 10	P	160
	ANS1DB=(40.0*ALOG10(BETA))-(20.0*ALOG10(ROD))	P	170
	OASPLC=157.5+ANS1DB	P	180
	GO TO 40	P	190
10	ANS1DB=(40.0*ALOG10(BETA))-(20.0*ALOG10(ROD))	P	200
	OASPLC=155.5+ANS1DB	P	210
	GO TO 40	P	220
20	IF (TJTO.LT.0.9) GO TO 30	P	230
	ANS1DB=(20.0*ALOG10(BETA))-(20.0*ALOG10(ROD))	P	240
	OASPLC=157.5+ANS1DB	P	250
	GO TO 40	P	260
30	ANS1DB=(10.0*ALOG10(BETA))-(20.0*ALOG10(ROD))	P	270
	OASPLC=155.5+ANS1DB	P	280
	GO TO 40	P	290
40	CONTINUE	P	300
50	IF (J,NE,1) GO TO 70	P	310
C		P	320
C	CALCULATION OF ANS3DB AND INTERPOLATED VALUES OF H0 AND C1	P	330
C	FOR ALL SPECIFIED FREQUENCIES (PACKAGE C)	P	340
C		P	350
	WORK1=((6.2832*RC*DFT*BETA)/A0)	P	360
	HVX(I)=((6.283*FREQ(I)*L0)/(12.0*A0))	P	370
	CVX(I)=HVX(I)	P	380
	IF (HVX(I).LT.0.2) GO TO 60	P	390
	IF (HVX(I).GT.70.0) GO TO 60	P	400S
	CALL LAGRNG (HX,HY,20,HVX(I),HVV(I))	P	410
	IF (TJTO.LT.0.9) HVY(I)=HVV(I)-2.0	P	420S
	CALL LAGRNG (CX,CY,20,CVX(I),CVY(I))	P	430
	ANS3DB(I)=10.0*ALOG10(WORK1*FREQ(I))	P	440
60	CONTINUE	P	450
70	CONTINUE	P	460
	IF (MJ,LE.1.0) GO TO 110	P	470
C		P	480
C	SHOCK NOISE CONTRIBUTION CAN BE AND IS NEGLECTED	P	490
C	FOR THE FOLLOWING CONDITIONS #	P	500
C	(1) TJTO LESS THAN 0.9 AND TM(J) LESS THAN 50 DEG.	P	510
C	(2) TJTO GREATER THAN 0.9 AND TM(J) LESS THAN 30 DEG.	P	520
C		P	530
	IF (TJTO.LT.0.9.AND.TM(J).LT.50.0.OR.TJTO.GE.0.9.AND.TM(J).LT.30.0	P	540
	1) GO TO 120	P	550
C		P	560
	IF (HVX(I).LT.0.2) GO TO 100	P	570
	IF (HVX(I).GT.70.0) GO TO 100	P	580
C		P	580



WC=6.283*FREQ(I)	P 590
IIEND=NS-1	P 600
SUMI=0.0	P 610
DO 90 II=1,IIEND	P 620
CI2=CVY(I)**(II+1)	P 630
ISEND=NS-II	P 640
SUMS=0.0	P 650
DO 80 ISN=1,ISEND	P 660
IS=ISN-1	P 670
QIS=WORK2*II*(1.0-(0.06*(IS+((II+1.0)/2.0))))	P 680
QCOS=COS(QIS*WC)	P 690
QSIN=SIN((QIS*WC*BC)/2.0)	P 700
WORK3=(QCOS*QSIN)/QIS	P 710
SUMS=SUMS+WORK3	P 720
80 CONTINUE	P 730
WORK4=CI2*SUMS	P 740
SUMI=SUMI+WORK4	P 750
90 CONTINUE	P 760
C	P 770
WORK5=(4.0*SUMI)/(NS*BC*WC)	P 780
ANS2=1.0*WORK5	P 790
ANS2DB=10.0*ALOG10(ABS(ANS2))	P 800
C	P 810
SPL=HVY(I)+ANS1DB+ANS3DB(I)+ANS2DB	P 820
SPLC(I)=SPL	P 830
HXX=HVX(I)	P 840
HYY=HVY(I)	P 850
CYY=CVY(I)	P 860
A3=ANS3DB(I)	P 870
A2=ANS2DB	P 880
GO TO 130	P 890
C	P 900
C	P 910
C	P 920
100 HYY=0.0	P 930
HXX=HVX(I)	P 940
CYY=0.0	P 950
A3=0.0	P 960
A2=0.0	P 970
SPLC(I)=2.0	P 980
GO TO 130	P 990
C	P1000
110 HXX=0.0	P1010
HYY=0.0	P1020
CYY=0.0	P1030
A3=0.0	P1040
A2=0.0	P1050
SPLC(I)=1.0	P1060
GO TO 130	P1070
C	P1080
120 HXX=0.0	P1090
HYY=0.0	P1100
CYY=0.0	P1110
A3=0.0	P1120
A2=0.0	P1130
SPLC(I)=3.0	P1140
GO TO 130	P1150
130 RETURN	P1160
END	P1170-

•DECK LAGRNG		
SUBROUTINE LAGRNG (X,Y,N,VALX,VALY)		Q 10
C		Q 20
C THIS SUBROUTINE CONDUCTS LAGRANGIAN INTERPOLATION*****		Q 30
C		Q 40
C X=X-COORDINATES OF H0 OR C1 MASTER INPUT SPECTRUM		Q 50
C Y=Y-COORDINATES OF H0 OR C1 MASTER INPUT SPECTRUM		Q 60
C N=NUMBER OF POINTS DESCRIBING H0 OR C1 MASTER INPUT SPECTRUM		Q 70
C VALX=ARGUMENT SIGMA		Q 80
C VALY=INTERPOLATED VALUE OF H0 OR C1 AT ARGUMENT SIGMA		Q 90
C		Q 100
C DIMENSION X(20),Y(20)		Q 110
C		Q 120
N1=N-1		Q 130
DO 10 I=2,N1		Q 140
IF (VALX.LE.X(I)) GO TO 20		Q 150
10 CONTINUE		Q 160
I=N1		Q 170
20 IS1=I-1		Q 180
IS2=I+1		Q 190
VALY=0.0		Q 200
DO 40 I=IS1,IS2		Q 210
P=1.0		Q 220
DO 30 J=IS1,IS2		Q 230
IF (I.EQ.J) GO TO 30		Q 240
A=(VALX-X(J))/(X(I)-X(J))		Q 250
P=P*A		Q 260
30 CONTINUE		Q 270
B=P*Y(I)		Q 280
VALY=VALY+B		Q 290
40 CONTINUE		Q 300
RETURN		Q 310
END		Q 320-

•DECK	BLKSAN	
	BLOCK DATA SAN	R 10
C		R 20
C	INPUT DATA*****	R 30
C		R 40
C	HX=ARGUMENT SIGMA IN SOURCE STRENGTH SPECTRUM	R 50
C	HY=SOURCE STRENGTH H0(SIGMA) FOR ARGUMENT SIGMA	R 60
C	CX=ARGUMENT SIGMA IN CORRELATION COEFFICIENT SPECTRUM	R 70
C	CY=CORRELATION COEFFICIENT C1(SIGMA) FOR ARGUMENT SIGMA	R 80
C		R 90
	COMMON/THIRTY/HX(20)	R 100
	COMMON/FORTY/HY(20)	R 110
	COMMON/FIFTY/CX(20)	R 120
	COMMON/SIXTY/CY(20)	R 130
C		R 140
	DATA HX/ 0.2,0.3,0.4,0.7,1.0,1.5,2.0,3.0,3.5,4.0,4.5,5.0,6.0,7.0,	R 150
	1 8.0,10.0,20.0,40.0,68.0,70.0 /	R 160
C		R 170
	DATA HY/ 116.0,121.6,125.5,132.5,137.7,142.7,145.7,148.5,149.1,	R 180
	1 149.2,149.1,148.8,147.9,146.7,145.7,143.7,137.4,130.5,125.4,	R 190
	2 125.2 /	R 200
C		R 210
	DATA CX/ 0.2,0.3,0.4,0.7,1.0,1.5,2.0,3.0,3.5,4.0,4.5,5.0,6.0,7.0,	R 220
	1 8.0,10.0,20.0,40.0,68.0,70.0 /	R 230
C		R 240
	DATA CY/ 0.70,0.71,0.71,0.72,0.73,0.74,0.74,0.71,0.69,0.67,0.64,	R 250
	1 0.62,0.58,0.54,0.50,0.45,0.28,0.12,0.02,0.02 /	R 260
C		R 270
	END	R 280-

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*DECK INTEG
PROGRAM INTEG(INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT)          S 10
EXTERNAL FCT,FCD,FQA6                                          S 20
REAL I1,I2,K                                                    S 30
REAL MJ                                                         S 40
DIMENSION W(24),FREQ(24),WI1(24),WI2(24),XU(24),XX(21),ENT1(21), S 50
1 ENT2(21),DBU(24),OBD(24),DB(24)                               S 60
2 ,SN(24),SPLM(24),IL(3)                                       S 70
COMMON/CON/ A0,VJ,XC,K,A1,B1,C1,A2,B2,C2,D2,A3,B3,RJ,WP,        S 80
1 A4,A5,XLIMIT,INTFLG                                          S 90
PI=3.141593                                                    S 100
C
C READ INPUT CONSTANTS                                         S 110
C                                                                S 120
C                                                                S 130
READ (5,140) RUNNO                                             S 140*
READ (5,170) (FREQ(I),I=1,24)                                  S 150*
10 READ (5,140) TP                                             S 160*
IF (TP.LT.1.0) GO TO 130                                       S 170
READ (5,180) (SPLM(I),I=1,24)                                  S 180*
READ (5,160) IOUT                                              S 190*
READ (5,160) INTFLG                                           S 200*
READ (5,140) MJ                                               S 210*
READ (5,140) VJF                                              S 220*
READ (5,140) XC                                               S 230*
READ (5,140) T0F                                             S 240*
READ (5,150) K                                               S 250*
READ (5,140) A1                                               S 260*
READ (5,140) B1                                               S 270*
READ (5,140) C1                                               S 280*
READ (5,150) A2                                               S 290*
READ (5,150) B2                                               S 300*
READ (5,140) C2                                               S 310*
READ (5,150) D2                                               S 320*
READ (5,150) A3                                               S 330*
READ (5,150) B3                                               S 340*
READ (5,150) A4                                               S 350*
READ (5,150) A5                                               S 360*
READ (5,150) XLIMIT                                           S 370*
READ (5,140) RJ                                               S 380*
READ (5,140) R                                               S 390*
READ (5,150) PAMB                                             S 400*
C                                                                S 410
A0F=49.02*SQRT(T0F+.459.67)                                    S 420
PAMB=PAMB*6894.7572                                           S 430
VJ=VJF*12.0                                                  S 440
AJ=VJ/MJ                                                      S 450
A0=A0F*12.0                                                  S 460
XC=XC*2.0*RJ*(4.3+1.1*MJ*MJ)                                  S 470
VJA0=VJ/A0                                                    S 480
TJT0=(AJ/A0)**2                                              S 490
THETA=90.0                                                    S 500
C                                                                S 510
K=K/(0.63*AJ*2.0*MJ*(1.1+0.9*MJ))                             S 520
C BEGIN FREQUENCY LOOP                                         S 530
C                                                                S 540
XLOWER=0.0                                                    S 550
XUPER2=1.0/XC                                                 S 560
TURB=0.6667*0.179*MJ**(-.1028)                               S 570
CONST=20.0*ALOG10(1.4*PAMB/2.0E-5)-20.0*ALOG10(R)+10.0*ALOG10(0.23) S 580

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116)	40.0*ALOG10(VJ/A0* $TURB/A0$ )-10.0*ALOG10(64.0*PI* $SQRT(PI)$ )+10.0*	S 590
2	ALOG10(2.0)	S 600
	DO 80 I=1,24	S 610
	W(I)=2.0*PI*FREQ(I)	S 620
	SN(I)=FREQ(I)*2.0*RJ/VJ	S 630
	WP=W(I)	S 640
	XMAX=5.99402199/(FREQ(I)*K)	S 650
	IF (INTFLG.EQ.1) GO TO 20	S 660
	IF (XC.LT.XMAX) GO TO 20	S 670
	XUPPER=XMAX	S 680
	CALL QA6 (FQA6,I1)	S 690S
	GO TO 30	S 700
20	XUPPER=XC	S 710
	CALL DQG32 (XLOWER,XUPPER,FCT,I1)	S 720S
30	XU(I)=XUPPER	S 730
	W1(I)=I1*W(I)**5*(1.0/ $SQRT(C1)$ )	S 740
	W1(I)=W1(I)* $SQRT(PI)$ /2.0	S 750
	IF (W1(I).GT.0.0) GO TO 40	S 760
	DBU(I)=0.0	S 770
	GO TO 50	S 780
40	DBU(I)=10.0*ALOG10(W1(I))	S 790
50	CALL DQG32 (XLOWER,XUPER2,FCD,I2)	S 800S
	W12(I)=I2*W(I)**5/(2.0*C2)	S 810
	W12(I)=W12(I)/4.0	S 820
	IF (W12(I).GT.0.0) GO TO 60	S 830
	DBD(I)=0.0	S 840
	GO TO 70	S 850
60	DBD(I)=10.0*ALOG10(W12(I))	S 860
70	DB(I)=10.0*ALOG10(10.0**((DBU(I)/10.0)+10.0**((DBD(I)/10.0)))	S 870
	DBU(I)=DBU(I)+CONST	S 880
	DBD(I)=DBD(I)+CONST	S 890
	DB(I)=DB(I)+CONST	S 900
80	CONTINUE	S 910
	WRITE (6,190) INTFLG,MJ,T0F,A0,VJF,XC,RJ,A1,A2,B1,B2,C1,C2,K,D2,A3	S 920*
	1,B3,A4,A5,R,PAMB,XLIMIT	S 930
	DO 90 I=1,24	S 940
	WRITE (6,200) FREQ(I),SN(I),DBU(I),DBD(I),DB(I)	S 950*
90	CONTINUE	S 960
	IF (IOUT.EQ.0) GO TO 120	S 970
	WRITE (6,210)	S 980*
	ENT2(I)=0.0	S 990
	DO 110 I=1,24	S1000
	WP=W(I)	S1010
	WRITE (6,220) FREQ(I),W(I)	S1020*
	DO 100 J=1,21	S1030
	XX(J)= $FLOAT(J-1)$	S1040
	ENT1(J)=FCT(XX(J))*W(I)**5*(1.0/ $SQRT(C1)$ )	S1050
	IF (J.EQ.1) GO TO 100	S1060
	ENT2(J)=FCD(1.0/XX(J))*W(I)**5/(2.0*C2)/XX(J)**2	S1070
100	CONTINUE	S1080
	WRITE (6,230) XX(1),ENT1(1)	S1090*
	WRITE (6,230) (XX(J),ENT1(J),ENT2(J),J=2,21)	S1100*
110	CONTINUE	S1110
120	CONTINUE	S1120
C		S1130
C	RETURN FOR NEXT COMPUTATION	S1140
C		S1150
C	GO TO 10	S1160
		S1170

130 STOP	S1180
C	S1190
FORMAT STATEMENTS	S1200
C	S1210
C	S1220
C	S1230
140 FORMAT (F15.1)	S1240
150 FORMAT (E10.4)	S1250
160 FORMAT (I1)	S1260
170 FORMAT (8F10.1)	S1270
180 FORMAT (12F6.1)	S1280
190 FORMAT (1H1,T8,"INPUT PARAMETERS FOR INTEGRATION ARE -",//,T2,"INT	S1290
1FLG = ",I2,//T5,"MJ = ",E15.8,T40,"T0 = ",E15.8,//,T5,"A0 = ",E15.	S1300
28,T40,"VJ = ",E15.8,//,T5,"XC = ",E15.8,T40,"RJ = ",E15.8,//,T5,"A	S1310
31 = ",E15.8,T40,"A2 = ",E15.8,//,T5,"B1 = ",E15.8,T40,"B2 = ",E15.	S1320
48,//,T5,"C1 = ",E15.8,T40,"C2 = ",E15.8,//,T5," K = ",E15.8,T40,"D	S1330
52 = ",E15.8,//,T5,"A3 = ",E15.8,T40,"B3 = ",E15.8,//,T5,"A4 = ",E1	S1340
65.8,T40,"A5 = ",E15.8,//,T5," R = ",E15.8,T40,"P0 = ",E15.8,//,T5,	S1350
7"XLIMIT = ",F6.2,////,T2,"FREQUENCY",T18,"SN",T29,"DBU",T40,"DBD",	S1360
8T51,"DB",//)	S1370
200 FORMAT (T3,F8.2,T15,F7.3,3(4X,F7.2))	S1380
210 FORMAT (1H1,T24,"VALUES OF INTEGRAND FOR VARIOUS VALUES OF X",/)	S1390
220 FORMAT (/5X,"FREQUENCY = ",F8.2,5X,"OMEGA = ",E15.7,//,T15,"X",T2	S1400
18,"INTEGRAND 1",T48,"INTEGRAND 2",/)	S1410
230 FORMAT (11X,F10.6,5X,E15.7,5X,E15.7)	S1420-
END	

*DECK FCT	
FUNCTION FCT(X)	T 10
REAL L1,LT,K	T 20
COMMON/CON/ A0,VJ,XC,K,A1,B1,C1,A2,B2,C2,D2,A3,B3,RJ,WP,	T 30
1 A4,A5,XLIMIT,INTFLG	T 40
DATA PI,RTP / 3.141593,0.797885 /	T 50
R12=RJ	T 60
IF (X.LE.XLIMIT) GO TO 10	T 70
L1=A1*X+B1	T 80
LT=A3*X+B3	T 90
GO TO 20	T 100
10 L1=A4*X	T 110
LT=A5*X	T 120
20 CONTINUE	T 130
D1=1.0	T 140
T0=K*X*D1	T 150
IF (INTFLG.EQ.1) GO TO 50	T 160
PART1=R12*X*L1*LT**2*T0	T 170
PART=- (WP*T0) / 8.0	T 180
IF (PART.LT.147.5.AND.PART.GT.-146.5) GO TO 30	T 190
PART2=0.0	T 200
GO TO 40	T 210
30 PART2=EXP(PART)	T 220
40 FCT=PART1*PART2*EXP(-.0016*X*X)	T 230
RETURN	T 240
50 PART1=R12*X*L1*LT**2*T0	T 250
PART=- (L1*WP)**2/(8.0*PI*0.63*0.63*VJ*VJ)	T 260
IF (PART.LT.147.5.AND.PART.GT.-146.5) GO TO 60	T 270
PART2=0.0	T 280
GO TO 70	T 290
60 PART2=EXP(PART)	T 300
70 PART3=RTP*PI/4.0/(1.0+(WP*T0)**2/4.0)**1.5	T 310
FCT=PART1*PART2*PART3*EXP(-.0016*X*X)	T 320
RETURN	T 330
END	T 340-

*DECK QG10	
SUBROUTINE QG10 (XL,XU,FCT,Y)	U 10
A=0.5*(XU+XL)	U 20
B=XU-XL	U 30
C=0.4869533*B	U 40
Y=0.03333567*(FCT(A+C)+FCT(A-C))	U 50
C=0.4325317*B	U 60
Y=Y+0.07472567*(FCT(A+C)+FCT(A-C))	U 70
C=0.3397048*B	U 80
Y=Y+0.1095432*(FCT(A+C)+FCT(A-C))	U 90
C=0.2166977*B	U 100
Y=Y+0.1346334*(FCT(A+C)+FCT(A-C))	U 110
C=0.07443717*B	U 120
Y=B*(Y+0.1477621*(FCT(A+C)+FCT(A-C)))	U 130
RETURN	U 140
END	U 150-



*DECK FQA6	
FUNCTION FQA6(XP)	V 10
REAL L1,LT,K	V 20
COMMON/CON/ A0,VJ,XC,K,A1,B1,C1,A2,B2,C2,D2,A3,B3,RJ,WP,	V 30
1 A4,A5,XLIMIT,INTFLG	V 40
X=SQRT(8.0*XP/(WP**2*K**2))	V 50
R12=RJ	V 60
IF (X.LE.XLIMIT) GO TO 10	V 70
L1=A1*X*B1	V 80
LT=A3*X*B3	V 90
GO TO 20	V 100
10 L1=A4*X	V 110
LT=A5*X	V 120
20 CONTINUE	V 130
T0=K*X	V 140
PART1=SQRT(XP)*R12*L1*LT*LT*T0	V 150
PART2=(WP**2*K**2)/4.0	V 160
FQA6=PART1/PART2*EXP(-.0016*X*X)	V 170
RETURN	V 180
END	V 190-

```
*DECK QA6
SUBROUTINE QA6 (FCT,Y)
X=15.12996
Y=.5317103E-6*FCT(X)
X=9.124248
Y=Y+.0001714737*FCT(X)
X=5.196153
Y=Y+.007810781*FCT(X)
X=2.552590
Y=Y+.1032160*FCT(X)
X=.8983028
Y=Y+.5209846*FCT(X)
X=.09874701
Y=Y+1.140270*FCT(X)
RETURN
END
```

```
W 10
W 20
W 30
W 40
W 50
W 60
W 70
W 80
W 90
W 100
W 110
W 120
W 130
W 140
W 150-
```

•DECK FCD	
FUNCTION FCD(X)	X 10
REAL L2,LT,K	X 20
COMMON/CON/ A0,VJ,XC,K,A1,B1,C1,A2,B2,C2,D2,A3,B3,RJ,WP,	X 30
1 A4,A5,XLIMIT,INTFLG	X 40
DATA PI,RTP / 3.141593,0.797885 /	X 50
L2=(A2/X+B2)**D2	X 60
LT=(A3/X+B3)**D2	X 70
T0=K/X	X 80
IF (INTFLG.EQ.1) GO TO 30	X 90
PART1=L2*LT*LT*XC**4*EXP(-.0016*XC*XC)*T0	X 100
PART=- (WP*T0)**2/8.0	X 110
IF (PART.LT.147.5.AND.PART.GT.-146.5) GO TO 10	X 120
PART2=0.0	X 130
GO TO 20	X 140
10 PART2=EXP(PART)	X 150
20 FCD=PART1*PART2	X 160
RETURN	X 170
30 PART1=L2*LT**2*XC**4*EXP(-.0016*XC*XC)*T0	X 180
VC=0.63*VJ	X 190
PART=- (L2*WP)**2/(8.0*PI*VC*VC)	X 200
IF (PART.LT.147.5.AND.PART.GT.-146.5) GO TO 40	X 210
PART2=0.0	X 220
GO TO 50	X 230
40 PART2=EXP(PART)	X 240
50 PART3=RTP*PI/4.0/(1.0+(WP*T0)**2/4.0)**1.5	X 250
FCD=PART1*PART2*PART3	X 260
RETURN	X 270
END	X 280-

*DECK DQG32	
SUBROUTINE DQG32 (XL,XU,FCT,Y)	Y 10
A=.5*(XU+XL)	Y 20
B=XU-XL	Y 30
C=.49863193092474078*B	Y 40
Y=.003509305004735048*(FCT(A+C)+FCT(A-C))	Y 50
C=.4928057557726341*B	Y 60
Y=.008137197365452835*(FCT(A+C)+FCT(A-C))	Y 70
C=.48238112779375322*B	Y 80
Y=.012696032654631030*(FCT(A+C)+FCT(A-C))	Y 90
C=.46745303796886984*B	Y 100
Y=.017136931456510717*(FCT(A+C)+FCT(A-C))	Y 110
C=.44816057788302606*B	Y 120
Y=.021417949011113340*(FCT(A+C)+FCT(A-C))	Y 130
C=.42468380686628499*B	Y 140
Y=.025499029631188088*(FCT(A+C)+FCT(A-C))	Y 150
C=.39724189798397120*B	Y 160
Y=.029342046739267774*(FCT(A+C)+FCT(A-C))	Y 170
C=.36609105937014484*B	Y 180
Y=.032911111388180923*(FCT(A+C)+FCT(A-C))	Y 190
C=.33152213346510760*B	Y 200
Y=.036172897054424253*(FCT(A+C)+FCT(A-C))	Y 210
C=.29385787862038116*B	Y 220
Y=.039096947893535153*(FCT(A+C)+FCT(A-C))	Y 230
C=.25344995446611470*B	Y 240
Y=.041655962113473378*(FCT(A+C)+FCT(A-C))	Y 250
C=.21067563806531767*B	Y 260
Y=.043826046502201906*(FCT(A+C)+FCT(A-C))	Y 270
C=.16593430114106382*B	Y 280
Y=.045586939347881942*(FCT(A+C)+FCT(A-C))	Y 290
C=.11964368112606854*B	Y 300
Y=.046922199540402283*(FCT(A+C)+FCT(A-C))	Y 310
C=.07223598079139825*B	Y 320
Y=.047819360039637430*(FCT(A+C)+FCT(A-C))	Y 330
C=.024153832843869158*B	Y 340
Y=B*(Y+.048270044257363900*(FCT(A+C)+FCT(A-C)))	Y 350
RETURN	Y 360
END	Y 370-