

AD-A063 476 NAVAL WEAPONS CENTER CHINA LAKE CALIF F/G 9/2
NAVAL WEAPONS CENTER VERSION OF THE ATMOSPHERIC TRANSMITTANCE C--ETC(U)
MAR 77 W M CORNETTE

UNCLASSIFIED

NWC-TM-3107

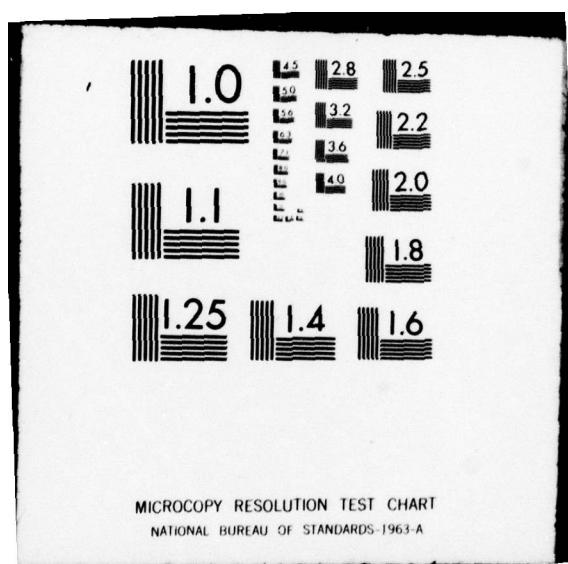
SIDEP-E095-0410

NL

OF
AD
AD-A063-476



END
DATE
FILMED
3-79
DOC



DDC FILE COPY

AD A063476

95-0410

106259

NWC Technical Memorandum 3107

LEVEL II

⑥
NAVAL WEAPONS CENTER
VERSION OF THE ATMOSPHERIC
TRANSMITTANCE COMPUTER CODE LOWTRAN:
USER'S MANUAL AND PROGRAM LISTING.

⑩ by
Dr. William M. Cornette
Weapons Systems Analysis Division
Systems Development Department

⑪ MAR 1977

⑫ 65p.

⑬ NWC-TM-3107

⑭ GIDEP ⑮ E095-0410

DDC
JAN 19 1979
V A

Approved for public release; distribution unlimited.
This is an informal report of the Naval Weapons Center
and is not part of the permanent records of the Department
of Defense.

NAVAL WEAPONS CENTER
China Lake, California 93555

78 11 28 110
403 019 LB 1
2

MAY 25 1978

NR

GOVERNMENT-INDUSTRY DATA EXCHANGE PROGRAM

GENERAL DOCUMENT SUMMARY SHEET

1 OF 1

1. ACCESS NUMBER E095-0410		2. COMPONENT/PART NAME PER GIDEP SUBJECT THESAURUS Computers, Program, NOC	
3. APPLICATION Engineering		4. MFR NOTIFICATION <input type="checkbox"/> NOTIFIED <input checked="" type="checkbox"/> NOT APPLICABLE	
6. ORIGINATOR'S DOCUMENT TITLE NWC Version of the Atmospheric Transmittance Computer Code LOWTRAN: User's Manual & Program Listing		5. DOCUMENT ISSUE (Month/Year) March 1977	
8. ORIGINATOR'S DOCUMENT NUMBER NWC TM 3107		9. ORIGINATOR'S PART NAME/IDENTIFICATION NWC/LOWTRAN	
10. DOCUMENT (SUPERSEDED) (SUPPLEMENTS) ACCESS NO. None		11. ENVIRONMENTAL EXPOSURE CODES None	
12. MANUFACTURER None		13. MANUFACTURER PART NUMBER None	
14. INDUSTRY/GOVERNMENT STANDARD NUMBER None			

15. OUTLINE, TABLE OF CONTENTS, SUMMARY, OR EQUIVALENT DESCRIPTION

LOWTRAN is a FORTRAN computer program, developed at the U.S. Air Force Geophysics Laboratory (AFGL), which calculates the transmittance of the earth's atmosphere in the spectral region from 0.25 to 28.57 μ m with 20 cm $^{-1}$ spectral resolution on a linear wavenumber scale. A choice of six atmospheric models covering seasonal and latitudinal variations from sea level to 100 km are available, in addition to a capability of allowing the user to input atmospheric profile or meteorological parameters of his own choosing. The program includes four aerosol models and permits either hazy or clear haze condition to be selected, in addition to the capability of selecting a particular visibility of the user's choosing. The model accounts for molecular absorption, molecular scattering, and aerosol extinction, plus atmospheric refraction and earth's curvature effects.

In examining AFGL's version of LOWTRAN (hereafter referred to AFGL/LOWTRAN), the author became aware that it would be possible to redesign the program without changing the basic methodology. This redesign achieves two goals: (a) a significant decrease in program size and hence computer time; and (b) a more structured program flow. The first goal is critical for repeated uses of the program or if the program is to be incorporated into a weapon/sensor system's simulation. The second goal is tied to the first one in that a smooth, structured logic flow usually improves computer time. Moreover, a structured program is easier to understand, to use, and, when necessary, to modify and update.

This report documents the updated code, in addition to including some corrections which have been brought to the author's attention.

78 11 28 110

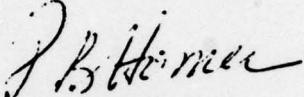
16. KEY WORDS FOR INDEXING NWC/LOWTRAN; FORTRAN; Program Listing; Atmospheric Transmittance; Input/Output		17. GIDEP REPRESENTATIVE M. H. Sloan	18. PARTICIPANT ACTIVITY AND CODE Naval Weapons Center, China Lake, CA (X7)
---	--	--	---

NWC TM 3107

FOREWORD

This technical memorandum contains a brief description and program listing of the atmospheric transmittance computer code NWC/LOWTRAN. The computer code development has been supported by a contract with Naval Air Systems Command (AIR-503E).

This document has been prepared primarily as an interim presentation of timely information. Although care has been taken in the preparation of the technical material presented, the results herein are to be considered as preliminary in nature.



P. B. HOMER
Head, Weapons Systems Analysis Division
Systems Development Department
28 March 1977

NWC TM 3107, published by Code 317, 50 copies.

CONTENTS

FOREWORD	1
INTRODUCTION	3
BACKGROUND	3
BASIC STRUCTURE	4
INPUT/OUTPUT	5
PORTABILITY	12
PROGRAM LISTING	13
MAJOR SYMBOLS AND DEFINITIONS	58
CONCLUSIONS	62
REFERENCES & BIBLIOGRAPHY	63

FIGURES:

1. Sample Output for NWC/LOWTRAN	8
--	---

ACCESSION NO.	
STP	DATE RECEIVED
SVC	DATE SERIALIZED
SEARCHED	
INDEXED	
FILED	
RT	
BOOK, BULLETIN/AVAILABILITY CODE	
ON	AVAIL. FOR BORROWING
A	

INTRODUCTION

LOWTRAN is a FORTRAN computer program, developed at the U.S. Air Force Geophysics Laboratory (AFGL), which calculates the transmittance of the earth's atmosphere in the spectral region from 0.25 to $28.57\mu\text{m}$ (350 to $40,000\text{ cm}^{-1}$) with 20 cm^{-1} spectral resolution on a linear wave-number scale. A choice of six atmospheric models (tropical, midlatitude summer and winter, subarctic summer and winter, and the U.S. 1962 standard atmosphere) covering seasonal and latitudinal variations from sea level to 100 km are available, in addition to a capability of allowing the user to input atmospheric profile or meteorological parameters of his own choosing. The program includes four aerosol models (average continental, urban, rural, and maritime) and permits either hazy (5-km visibility) or clear (23-km visibility) haze condition to be selected, in addition to the capability of selecting a particular visibility of the user's choosing. The model accounts for molecular absorption, molecular scattering, and aerosol extinction, plus atmospheric refraction and earth's curvature effects.

LOWTRAN is presently the best available method for predicting atmospheric transmittance and, as such, should be incorporated in simulations and studies of electro-optic weapon/sensor systems performance. One advantage of LOWTRAN is that AFGL is continually improving and upgrading the computer code. For further documentation on LOWTRAN and its limitations, see Refs. 1-5, 11, and 14.

BACKGROUND

In examining AFGL's version of LOWTRAN (hereafter referred to AFGL/LOWTRAN), the author became aware that it would be possible to redesign the program without changing the basic methodology. This re-design achieves two goals:

- a. a significant decrease in program size and hence computer time; and
- b. a more structured program flow.

The first goal is critical for repeated uses of the program or if the program is to be incorporated into a weapon/sensor systems simulation. The second goal is tied to the first one in that a smooth, structured logic flow usually improves computer time. Moreover, a structured program is easier to understand, to use, and, when necessary, to modify and update.

The author re-designed AFGL/LOWTRAN and produced the computer code NWC/LOWTRAN. It should be emphasized that NWC/LOWTRAN does not attempt to modify the methodology or the algorithm used in AFGL/LOWTRAN in any way whatsoever. The only difference between the two versions is in the computer coding of the algorithm. In fact, where possible, NWC/LOWTRAN uses the same variable names and statement labels as AFGL/LOWTRAN III (ref. 8). This was done to assist comparison between the two codes. The author recently received the modifications to LOWTRAN III necessary to upgrade it to LOWTRAN IIIB status (Ref. 4). These changes have been implemented into NWC/LOWTRAN (Ref. 15). This report documents the updated code, in addition to some corrections which have been brought to the author's attention (e.g., Refs. 9, 10, 14, and 16).

The author would particularly like to thank Mr. T. J. Smith of the Naval Weapons Center and Dr. A. Goroch of the Naval Environmental Prediction Research Facility for indicating several errors. In addition, the author would appreciate having any additional corrections to LOWTRAN brought to his attention at the following address:

Commander (Code 3173)
Attn: Dr. William M. Cornette
Naval Weapons Center
China Lake CA 93555

Comm. Telephone (714) 939-3551
Autovon 245-3551

BASIC STRUCTURE

The NWC/LOWTRAN computer code consists of four modules:

- (1) the main program;
- (2) the subroutine POINT, which computes the mean refractive index above and below a given altitude and interpolates exponentially to determine the equivalent absorber amounts at that altitude;
- (3) the subroutine ANGL, which calculates the initial zenith angle taking into account refraction effects; and
- (4) a BLOCK DATA module, which inputs the spectral and transmittance data.

NWC TM 3107

The number of executable statements contained in each module are:

Main program	405
Subroutine POINT	26
Subroutine ANGL	217
BLOCK DATA	0
TOTAL	648

This is a reduction by over 200 lines of executable computer code from AFGL/LOWTRAN (Ref. 15).

The actual run time for execution time of NWC/LOWTRAN is dependent upon the number of levels used in the geometry, whether the subroutine ANGL is called, and the width and resolution of the spectral band. However, the execution time for the sample output in Figure 1 (shown later in this report) was approximately 470 milliseconds.

INPUT/OUTPUT

The basic inputs to NWC/LOWTRAN are only four cards:

Card 1: MODEL, IAERO, IHAZE, JP, IM, M1, M2, M3, ML, RO, VIS
----- FORMAT (9I3,3X,2F10.3)

MODEL selects one of the following model atmospheres:

MODEL = 0 for a horizontal path when meteorological data is used. Instead of card 2, read altitude (km), pressure (mb), temperature (deg C), dew point temperature (deg C), relative humidity (%), water vapor density (gm. m^{-3}), ozone density (gm. m^{-3}), visibility (km), and range (km).
----- FORMAT (3F10.3,2F5.2,2(1PE10.3),2(OPF10.3)).

MODEL = 1 specifies a tropical atmosphere.
MODEL = 2 specifies a midlatitude summer atmosphere.
MODEL = 3 specifies a midlatitude winter atmosphere.
MODEL = 4 specifies a sub-arctic summer atmosphere.
MODEL = 5 specifies a sub-arctic winter atmosphere.
MODEL = 6 specifies the 1962 U.S. Standard atmosphere.
MODEL = 7 for a new model atmosphere (e.g. radiosonde data).
Read between cards 1 and 2, altitude (km), pressure (mb), temperature (deg C), dew point temperature (deg C), relative humidity (%), water vapor density (gm. m^{-3}), ozone density (gm. m^{-3}), and aerosol density (cm^{-3}).

NWC TM 3107

----- FORMAT (3F10.3,2FS.2,2(1PE10.31,2(OPE10.3)).

Note that either dew point temperature, relative humidity, or water vapor density can be used.

IAERO selects the type of aerosol attenuation:

IAERO = 1 specifies an average continental aerosol model.

IAERO = 2 specifies a rural aerosol model.

IAERO = 3 specifies an urban aerosol model.

IAERO = 4 specifies a maritime aerosol model.

IHAZE selects the degree of aerosol attenuation:

If IHAZE = 0 no aerosol scattering is computed.

If IHAZE = 1 and VIS is non-zero, then aerosol attenuation for the visible range is used.

If IHAZE = 1 or 2 and VIS is zero, then aerosol attenuation for 23 km and 5 km visible ranges, respectively, is used.

JP selects the print option:

JP = 0 for normal operation.

JP = 1 to suppress the printing of the transmittance table.

IM determines when radiosonde data is to be read in:

IM = 0 for normal operation or when subsequent calculations are to be run with MODEL = 7.

IM = 1 for reading in radiosonde data initially for MODEL = 7.

M1, M2, and M3 are used to change temperature, H₂O, and O₃ altitude profiles, respectively, to another model value.

ML is the number of levels of radiosonde data for MODEL = 7.

RO is the input value for the radius of the earth. If RO = 0.0, then the program uses stored values.

VIS is the visual range at sea level (km).

Card 2: I = TYPE, LEN, H1, H2, ANGLE, RANGE, BETA---FORMAT (2I3,4X,5F10.3)

ITYPE indicates the type of atmospheric path:

ITYPE = 1, corresponds to a horizontal (constant pressure) path. Read H1 and RANGE.

NWC TM 3107

ITYPE = 2, vertical or slant path between two altitudes.
Read H1 and two other geometric parameters (e.g., H2
and ANGLE).
ITYPE = 3, vertical or slant path to space.
Read H1 and ANGLE.

LEN selects the type of ray path to be used:

LEN = 0 for normal operation of the program which selects the
shorter path when applicable.
LEN = 1 to select the longer path when applicable.

H1 = observer altitude (km)
H2 = source altitude (km)
ANGLE = zenith angle at H1 (degrees)
RANGE = path length (km)
BETA = earth center angle (degrees)

Card 3: V1, V2, DV-----FORMAT (3F10.3)

V1 = initial frequency (wavenumber (cm⁻¹)) value
V2 = final frequency (wavenumber (cm⁻¹)) value
DV = frequency intervals at which transmittance is printed
Note: V1, V2, and DV must be integral multiples of 5 cm⁻¹

Card 4: IXY-----FORMAT (I3)

IXY is the cycling indicator:

IXY = 0 to end data
IXY = 1 for new card 3 only
IXY = 2 to continue data
IXY = 3 for new card 2 only
IXY = 4 for new card 1 only

A sample output is shown in Figure 1.

NWC TM 3107

SUB-ARCTIC (60 DEG. LAT.) WINTER MODELS ATMOSPHERE

CONTINENTAL AEROSOL MODEL

HAZE MODEL = 23.0 KM VISUAL RANGE AT SEA LEVEL

H1 = 2.500 KM. H2 = 8.500 KM. ANGLE = 65.0000 GEOM. RANGE = 14.17 KM. BETA = .11547 DEG

SLANT PATH BETWEEN ALTITUDES H1 AND H2 WHERE H1 = 2.500 KM H2 = 8.500 KM. ZENITH ANGLE = 65.000 DEGREES

FREQUENCY RANGE VI = 2350.0 CM⁻¹ TO V2 = 2450.0 CM⁻¹ FOR DV = 5.0 CM⁻¹ (4.08 - 4.26 MICRONS)

FIGURE 1. Sample Output for NWC/LOWTRAN.

NWC TM 3107

HORIZONTAL PROFILES		1.062+00	1.000+00	1.913-03	2.853-04	2.900-02	3.052+02
-	0	1.233-01	1.067+00	6.633-04	6.633-04	6.633-04	6.633-04
1	0	1.091-01	6.834-03	6.651-01	6.144-04	9.239-01	4.399-01
2	0	7.629-02	6.936-01	5.197-01	4.114-04	9.193-01	1.699-01
3	0	4.918-02	5.538-01	4.099-01	2.422-04	7.254-01	7.975-02
4	0	2.647-02	4.484-01	1.729-03	3.177-01	1.101-04	6.458-01
5	0	1.153-02	3.648-01	1.717-03	2.504-01	3.801-05	5.773-01
6	0	5.027-03	2.950-01	1.700-03	1.961-01	1.376-05	5.145-01
7	0	2.457-03	2.372-01	2.335-03	1.525-01	6.006-06	4.571-01
8	0	4.423-04	1.692-01	2.802-03	1.175-01	8.156-07	4.043-01
9	0	2.955-04	1.470-01	4.693-03	8.799-02	5.326-07	3.512-01
10	0	1.680-04	1.117-01	6.611-03	6.428-02	2.898-07	3.002-01
11	0	1.008-04	8.490-02	8.279-03	4.697-02	1.681-07	2.566-01
12	0	5.984-05	6.446-02	1.045-02	3.429-02	9.673-08	2.192-01
13	0	3.598-05	4.901-02	1.072-02	2.307-02	5.637-08	1.875-01
14	0	1.736-05	3.725-02	1.050-02	1.832-02	2.639-02	1.603-01
15	0	1.145-05	2.829-02	1.127-02	1.338-02	1.832-02	1.785-01
16	0	0.386-06	2.159-02	1.173-02	9.820-03	1.229-08	1.174-01
17	0	6.371-06	1.642-02	1.101-02	7.184-03	9.194-09	1.005-01
18	0	4.946-06	1.253-02	1.035-02	5.273-03	7.033-09	8.615-02
19	0	2.019-06	9.538-03	9.406-03	3.859-03	5.918-09	7.375-02
20	0	3.357-06	7.260-03	8.245-03	2.824-03	4.657-09	6.315-02
21	0	3.301-06	3.301-06	5.151-03	7.049-03	2.062-03	4.571-09
22	0	2.863-06	4.189-03	6.099-03	1.506-03	3.942-03	5.399-02
23	0	2.629-06	3.180-03	5.238-03	1.099-03	3.624-09	5.194-02
24	0	2.533-06	2.413-03	4.115-03	8.012-04	3.528-09	3.372-02
25	0	2.451-06	1.629-03	3.432-03	5.836-04	3.481-09	2.880-02
26	0	2.309-07	4.420-07	1.166-03	1.153-04	8.463-10	2.627-03
27	0	6.381-07	5.216-04	2.348-05	1.113-10	5.705-03	1.273-02
28	0	9.587-08	1.096-04	5.216-04	2.348-05	2.082-04	4.293-03
29	0	1.879-08	2.784-05	1.710-04	4.924-06	2.001-11	2.577-03
30	0	4.317-09	7.615-06	4.056-05	1.123-06	4.311-12	1.215-03
31	0	7.692-10	2.221-06	1.018-05	2.757-07	7.221-13	5.947-04
32	0	1.604-12	2.291-08	7.112-08	1.474-09	1.118-15	4.407-05
33	0	1.499-16	5.397-12	5.175-12	1.041-13	6.038-20	3.852-07

FIGURE 1. Sample Output for NWC/LOWTRAN. (contd)

11

NWC TM 3107

VERTICAL PROFILES														
		PSI	PHI	BETA	THETA	RANGE								
3	2.5	7.305-02	7.319-01	2.059-03	5.441-01	3.778-04	9.126-01	1.502-01	2.318-03	-0.0000	115.0097	.0097	65.0000	
3	3.0	1.597-01	1.912+00	6.159-03	1.394+00	7.741-04	2.532+00	2.895-01	7.173-03	.0022	115.0267	.0267	64.9326	
3	3.5	2.022-01	2.970+00	1.023-02	2.062+00	9.343-04	3.976+00	3.764-01	1.225-02	.0048	115.0434	.0434	64.9759	
3	4.0	2.207-01	3.646+00	1.426-02	2.587+00	9.906-04	5.264+00	4.398-01	1.754-02	.0071	115.0603	.0603	64.9589	
3	4.5	2.292-01	4.272+00	1.899-02	2.996+00	6.409+00	4.908-01	2.407-02	.0092	115.0775	.0775	.0867	64.9418	
3	5.0	2.320-01	4.773+00	2.503-02	3.313+00	1.019-03	7.424+00	5.406-01	3.289-02	.0112	115.0947	.0947	.1059	64.9245
3	5.5	2.324-01	4.982+00	2.880-02	3.442+00	1.020-03	7.684+00	5.657-01	3.863-02	.0126	115.1029	.1029	.1155	64.9067
ESTIMATED TANGENT ALTITUDE =		.000 KM												
EQUIVALENT SEA LEVEL ABSORBER AMOUNTS														
WATER VAPOUR		CO ₂ ETC.	OZONE	NITROGEN	H ₂ O (CONT)	AEROSOL	OZONE(U-V)							
GM CM-2		KM	ATM CM	KM	GM CM-2	KM	ATM CM							
M(1-0) =		2.324-01	4.982+00	2.880-02	3.442+00	1.020-03	7.684+00							

FIGURE 1. Sample Output for NWC/LOWTRAN. (contd)

NWC TM 3107

INTEGRATED ABSORPTION		AEROSOL ABS		AEROSOL TRANSMISSION		H2O CONT. TRANSMISSION		N2 CONT. TRANSMISSION		OZONE TRANSMISSION		CO2+ TRANSMISSION		H2O		TOTAL MICRONS		WAVELENGTH CM-1		
2330	4.2553	.0000	.9964	.0000	.9969	.0000	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2335	4.2463	.0000	.9964	.0000	.9969	.0000	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2340	4.2373	.0000	.9964	.0000	.9969	.0000	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2345	4.2283	.0000	.9964	.0000	.9969	.0000	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2350	4.2194	.0000	.9964	.0000	.9969	.0000	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2355	4.2105	.0000	.9964	.0000	.9969	.0000	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2360	4.2017	.0014	.9964	.0000	.9969	.0002	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2365	4.1929	.0271	.9964	.0000	.9969	.0405	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2370	4.1841	.1125	.9964	.0000	.9969	.1691	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2375	4.1754	.2543	.9964	.0000	.9969	.3851	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2380	4.1667	.4524	.9964	.0000	.9969	.6836	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2385	4.1580	.7500	.9964	.0000	.9969	.8774	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2390	4.1494	.6612	.9964	.0000	.9969	.9859	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2395	4.1408	.6721	.9964	.0000	.9969	.9918	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2400	4.1322	.6823	.9964	.0000	.9969	.9971	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2405	4.1237	.6966	.9964	.0000	.9969	.9912	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2410	4.1152	.6919	.9964	.0000	.9969	.9738	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2415	4.1068	.6988	.9964	.0000	.9969	.9688	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2420	4.0984	.7038	.9964	.0000	.9969	.9660	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2425	4.0900	.7129	.9964	.0000	.9969	.9641	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	
2430	4.0816	.7254	.9964	.0000	.9969	.9633	.9972	.0000	.9973	.0000	.9975	.0000	.9976	.0000	.9977	.0000	.9978	.0000	.9979	

FIGURE 1. Sample Output for NMC/LOWTRAN. (cont'd)

PORATABILITY

During the development of the NWC/LOWTRAN computer code, it was attempted to use a highly portable subset of ANSI FORTRAN (Ref. 12). To facilitate this, the PFORT verifier developed by Bell Telephone Laboratories (Ref. 13) has been used to check the portability of the computer code.

To the best of the author's knowledge, the only areas where difficulties may arise in using NWC/LOWTRAN with compilers and machines other than Univac compilers and computers, are as follows:

- (i) The program uses the Univac library routines ACOS (arccosine), ASIN (arcsine), and TAN (tangent); if not available on the desired machine (e.g., on Honeywell Series 32 computers) or if another name is used (e.g., ARCOS and ARSIN on the IBM 360 series computers), some changes will be necessary.
- (ii) The values for the input/output units on the Univac 1110 are 5 for the card reader and 6 for the line printer; these values are input to the program in the BLOCK DATA module for easy accessibility.
- (iii) Due to the large arrays used in NWC/LOWTRAN, much of the data in the BLOCK DATA module are assigned by DATA statements to an array name, or part of an array through an implicit DO; this feature may create certain difficulties on some compilers.

If anyone experiences any problems using NWC/LOWTRAN due to compiler or machine incompatibilities, the author would greatly appreciate being notified.

NAVAL WEAPONS CENTER MODIFICATION
OF AFOL LOWTRAN 3B

REVISION DATE 28 MARCH 1977

PROGRAM LONTRAN 3B CALCULATES THE TRANSMITTANCE OF THE ATMOSPHERE FROM 350 CM⁻¹ TO 40000 CM⁻¹ (0.25 TO 26.57 MICRONS) IN 25 CM⁻¹ SPECIAL RESOLUTION ON A LINEAR WAVE NUMBER SCALE. REFRACTION AND EARTH'S CURVATURE EFFECTS ARE INCLUDED. THE ATMOSPHERE IS LAYERED IN ONE KILOMETER INTERVALS. BETWEN GROUND LEVEL AND 25 KM., 5 KM. INTERVALS TO 30 KM.; A THEN KM. INTERVAL TO 70 KM., AND A THIRTY KM. INTERVAL TO 100 KM.

PROGRAM ACTIVATED BY SUBMISSION OF FOUR CARD SEQUENCE -

CARD 1 - MODEL, IAERO, IMAZE, JP, IM, MI, M2, M3, ML, RO, VIS
FORMAT(13,3X,21)

1-2 3 5 6 7 8 9 10-12 13 15 16 17 18 19 20 21 22 23 24 25

270
 280 MODEL SELECTS ONE OF THE FOLLOWING MODEL ATMOSPHERE.
 MODEL = 0 FOR HORIZ. PATH WHEN METEOROL. DATA USED -
 INSTEAD OF CARD 2, READ M1, P(MB), T(VIDEO C), DEM PT, TEMP
 (VIDEO C), REL. HUMIDITY(PERCENT), H2O DENSITY 10M, H-31,03
 DENSITY (10M, H-31), RANGE(1KM)
 DENSITY FORMAT(10.3-2F5.2-2(1PE10.3).0PF10.3).
 MODEL = 1 SPECIFIES A TROPICAL ATMOSPHERE.
 MODEL = 2 SPECIFIES A MIDLATITUDE SUMMER ATMOSPHERE.
 MODEL = 3 SPECIFIES A MIDLATITUDE WINTER ATMOSPHERE.
 MODEL = 4 SPECIFIES A SUB-ARCTIC SUMMER ATMOSPHERE.
 MODEL = 5 SPECIFIES A SUB-ARCTIC WINTER ATMOSPHERE.
 MODEL = 6 SPECIFIES A 1962 US STANDARD ATMOSPHERE.
 MODEL = 7 FOR NEW MODEL ATMOSONDE DATA.
 READ BETWEEN CARDS 1 AND 2, ALTITUDE(1KM), P
 DEM PT, TEMP(VIDEO C), REL. HUMIDITY(PERCENT), H2O DENSITY
 (10M, H-31), 03 DENSITY(10M, H-31), AEROSOL NO. DENSITY(CH-3)
 FORMATTED(3F10.3-2F5.2-2(1PE10.3).2(0PF10.3).
 NOTE - EITHER DEM PT, TEMP., REL. HUM. . OR H2O DENSITY
 CAN BE USED.

IAERO SELECTS THE TYPE OF AEROSOL ATTENUATION
 IAERO = 1 SPECIFIES AN AVERAGE CONTINENTAL AEROSOL MODEL.
 IAERO = 2 SPECIFIES A RURAL AEROSOL MODEL.
 IAERO = 3 SPECIFIES AN URBAN AEROSOL MODEL.
 IAERO = 4 SPECIFIES A MARITIME AEROSOL MODEL.

IMAZE SELECTS THE DEGREE OF AEROSOL ATTENUATION
 IF IMAZE=0 NO AEROSOL SCATTERING IS COMPUTED.
 IF IMAZE = 1 AND VIS IS NOT-ZERO, THEN AEROSOL ATTENUATION
 FOR THE VISIBLE RANGE IS USED.
 IF IMAZE = 1 OR 2 AND VIS IS ZERO, THEN AEROSOL ATTENUATION
 FOR 23 KM AND 5 KM VISIBLE RANGES, RESPECTIVELY,
 IS USED.

JP SELECTS THE PRINT OPTION
 JP = 0 FOR NORMAL OPERATION.
 JP = 1 TO SUPPRESS THE PRINTING OF THE TRANSMITTANCE TABLE.

IM DETERMINES WHEN RADIOSONDE DATA IS TO BE READ IN
 IM = 0 FOR NORMAL OPERATION.
 IM = 1 FOR INITIALIZING RADIOSONDE OR METEOROLOGICAL
 DATA.

M1, M2, AND M3 ARE USED TO CHANGE TEMP., H2O, AND O3 ALTITUDE
 PROFILES, RESPECTIVELY, TO ANOTHER MODEL VALUE.

ML IS THE NUMBER OF LEVELS OF RADIOSONDE DATA FOR MODEL = 7.

R0 IS THE INPUT VALUE FOR THE RADIUS OF THE EARTH. IF R0 IS
 ZERO THEN THE PROGRAM USES STORED VALUES.

VIS IS THE VISUAL RANGE AT SEA LEVEL (KM)

CARD 2- ITYPE,LEN,M1,M2,ANGLE,RANGE,BETA---FORMAT(2I3.0,X,9P10.3) * OLOH03100
 OLOH08200
 OLOH03000

TYPE INDICATES THE TYPE OF ATMOSPHERIC PATH

```

ITYPE = 1. CORRESPONDS TO A HORIZONTAL (CONSTANT PRESSURE)
PATH. READ MI AND RANGE.
ITYPE = 2. VERTICAL OR SLANT PATH BETWEEN TWO ALTITUDES.
READ MI AND TWO OTHER GEOMETRIC PARAMETERS (E.O., M2 AND
ANGLE).
ITYPE = 3. VERTICAL OR SLANT PATH TO SPACE.
READ MI AND ANGLE.

LEN SELLECTS THE TYPE OF RAY PATH TO BE USED
LEN = 0 FOR NORMAL OPERATION OF THE PROGRAM WHICH SELLECTS
THE SHORTER PATH WHEN APPLICABLE.
LEN = 1 TO SELLECT THE LONGER PATH WHEN APPLICABLE.

MI      = OBSERVER ALTITUDE (KM)
M2      = SOURCE ALTITUDE (KM)
ANGLE   = ZENITH ANGLE AT MI (DEGREES)
RANGE   = PATH LENGTH (KM)
BETA    = EARTH CENTRE ANGLE (DEGREES)

CARD 3- VI.V2.DV-----FORMAT(3F10.3)-----

VI = INITIAL FREQUENCY (WAVENUMBER CM-1) INTEGER VALUE
V2 = FINAL FREQUENCY (WAVENUMBER CM-1) INTEGER VALUE
DV = FREQUENCY INTERVALS AT WHICH TRANSMITTANCE IS PRINTED
NOTE - DV MUST BE A MULTIPLE OF 5 CM-1

CARD 4- IXV-----FORMAT(13)-----

IXV IS THE CYCLING INDICATOR:
IXV = 0 TO END DATA
IXV = 1 FOR NEW CARD 3 ONLY
IXV = 2 TO CONTINUE DATA
IXV = 3 FOR NEW CARD 2 ONLY
IXV = 4 FOR NEW CARD 1 ONLY (PLUS RADIOSONDE OR
METEOROLOGICAL DATA, IF DESIRED)

LOCAL CKZERO
COMMON /LOWTRN/ IATH,NL,M21(34),M22(34),P17,34,T(7,34),
               C1(17,34),M01(4),VX1(4),TR(67),FO(67),CI(2580),
               C2(1975),C3(540),C4(133),CS(115),C7(4,45),CA(1,45),CB(1,10),
               EM1(0,34),M,M1,M2,M3,RE,CM,CO,PI,CA,REALTH(7,2(34)),IN,IR
DIMENSION TX(10),VH(10),E(10),AM21(34),AM22(34),M(10),
          CKZERO(VARI)=ABS(VARI),LT,1,E=20
IXY=2
IP=1
NL1=NL-1
DO 200 ITER=1,10000
  IF (IXY.LE.0.OR.IXY.GE.5) GO TO 200
  IF (IXY.EQ.1) GO TO 107
  IF (IXY.EQ.3) GO TO 105
  IF (IXY.EQ.5) GO TO 103
  IF (IXY.EQ.7) GO TO 101
  IF (IXY.EQ.9) GO TO 100
  IF (IXY.EQ.11) GO TO 99
  IF (IXY.EQ.13) GO TO 98
  IF (IXY.EQ.15) GO TO 97
  IF (IXY.EQ.17) GO TO 96
  IF (IXY.EQ.19) GO TO 95
  IF (IXY.EQ.21) GO TO 94
  IF (IXY.EQ.23) GO TO 93
  IF (IXY.EQ.25) GO TO 92
  IF (IXY.EQ.27) GO TO 91
  IF (IXY.EQ.29) GO TO 90
  IF (IXY.EQ.31) GO TO 89
  IF (IXY.EQ.33) GO TO 88
  IF (IXY.EQ.35) GO TO 87
  IF (IXY.EQ.37) GO TO 86
  IF (IXY.EQ.39) GO TO 85
  IF (IXY.EQ.41) GO TO 84
  IF (IXY.EQ.43) GO TO 83
  IF (IXY.EQ.45) GO TO 82
  IF (IXY.EQ.47) GO TO 81
  IF (IXY.EQ.49) GO TO 80
  IF (IXY.EQ.51) GO TO 79
  IF (IXY.EQ.53) GO TO 78
  IF (IXY.EQ.55) GO TO 77
  IF (IXY.EQ.57) GO TO 76
  IF (IXY.EQ.59) GO TO 75
  IF (IXY.EQ.61) GO TO 74
  IF (IXY.EQ.63) GO TO 73
  IF (IXY.EQ.65) GO TO 72
  IF (IXY.EQ.67) GO TO 71
  IF (IXY.EQ.69) GO TO 70
  IF (IXY.EQ.71) GO TO 69
  IF (IXY.EQ.73) GO TO 68
  IF (IXY.EQ.75) GO TO 67
  IF (IXY.EQ.77) GO TO 66
  IF (IXY.EQ.79) GO TO 65
  IF (IXY.EQ.81) GO TO 64
  IF (IXY.EQ.83) GO TO 63
  IF (IXY.EQ.85) GO TO 62
  IF (IXY.EQ.87) GO TO 61
  IF (IXY.EQ.89) GO TO 60
  IF (IXY.EQ.91) GO TO 59
  IF (IXY.EQ.93) GO TO 58
  IF (IXY.EQ.95) GO TO 57
  IF (IXY.EQ.97) GO TO 56
  IF (IXY.EQ.99) GO TO 55
  IF (IXY.EQ.101) GO TO 54
  IF (IXY.EQ.103) GO TO 53
  IF (IXY.EQ.105) GO TO 52
  IF (IXY.EQ.107) GO TO 51
  IF (IXY.EQ.109) GO TO 50
  IF (IXY.EQ.111) GO TO 49
  IF (IXY.EQ.113) GO TO 48
  IF (IXY.EQ.115) GO TO 47
  IF (IXY.EQ.117) GO TO 46
  IF (IXY.EQ.119) GO TO 45
  IF (IXY.EQ.121) GO TO 44
  IF (IXY.EQ.123) GO TO 43
  IF (IXY.EQ.125) GO TO 42
  IF (IXY.EQ.127) GO TO 41
  IF (IXY.EQ.129) GO TO 40
  IF (IXY.EQ.131) GO TO 39
  IF (IXY.EQ.133) GO TO 38
  IF (IXY.EQ.135) GO TO 37
  IF (IXY.EQ.137) GO TO 36
  IF (IXY.EQ.139) GO TO 35
  IF (IXY.EQ.141) GO TO 34
  IF (IXY.EQ.143) GO TO 33
  IF (IXY.EQ.145) GO TO 32
  IF (IXY.EQ.147) GO TO 31
  IF (IXY.EQ.149) GO TO 30
  IF (IXY.EQ.151) GO TO 29
  IF (IXY.EQ.153) GO TO 28
  IF (IXY.EQ.155) GO TO 27
  IF (IXY.EQ.157) GO TO 26
  IF (IXY.EQ.159) GO TO 25
  IF (IXY.EQ.161) GO TO 24
  IF (IXY.EQ.163) GO TO 23
  IF (IXY.EQ.165) GO TO 22
  IF (IXY.EQ.167) GO TO 21
  IF (IXY.EQ.169) GO TO 20
  IF (IXY.EQ.171) GO TO 19
  IF (IXY.EQ.173) GO TO 18
  IF (IXY.EQ.175) GO TO 17
  IF (IXY.EQ.177) GO TO 16
  IF (IXY.EQ.179) GO TO 15
  IF (IXY.EQ.181) GO TO 14
  IF (IXY.EQ.183) GO TO 13
  IF (IXY.EQ.185) GO TO 12
  IF (IXY.EQ.187) GO TO 11
  IF (IXY.EQ.189) GO TO 10
  IF (IXY.EQ.191) GO TO 9
  IF (IXY.EQ.193) GO TO 8
  IF (IXY.EQ.195) GO TO 7
  IF (IXY.EQ.197) GO TO 6
  IF (IXY.EQ.199) GO TO 5
  IF (IXY.EQ.201) GO TO 4
  IF (IXY.EQ.203) GO TO 3
  IF (IXY.EQ.205) GO TO 2
  IF (IXY.EQ.207) GO TO 1
  IF (IXY.EQ.209) GO TO 0
  IF (IXY.EQ.211) GO TO -1
  IF (IXY.EQ.213) GO TO -2
  IF (IXY.EQ.215) GO TO -3
  IF (IXY.EQ.217) GO TO -4
  IF (IXY.EQ.219) GO TO -5
  IF (IXY.EQ.221) GO TO -6
  IF (IXY.EQ.223) GO TO -7
  IF (IXY.EQ.225) GO TO -8
  IF (IXY.EQ.227) GO TO -9
  IF (IXY.EQ.229) GO TO -10
  IF (IXY.EQ.231) GO TO -11
  IF (IXY.EQ.233) GO TO -12
  IF (IXY.EQ.235) GO TO -13
  IF (IXY.EQ.237) GO TO -14
  IF (IXY.EQ.239) GO TO -15
  IF (IXY.EQ.241) GO TO -16
  IF (IXY.EQ.243) GO TO -17
  IF (IXY.EQ.245) GO TO -18
  IF (IXY.EQ.247) GO TO -19
  IF (IXY.EQ.249) GO TO -20
  IF (IXY.EQ.251) GO TO -21
  IF (IXY.EQ.253) GO TO -22
  IF (IXY.EQ.255) GO TO -23
  IF (IXY.EQ.257) GO TO -24
  IF (IXY.EQ.259) GO TO -25
  IF (IXY.EQ.261) GO TO -26
  IF (IXY.EQ.263) GO TO -27
  IF (IXY.EQ.265) GO TO -28
  IF (IXY.EQ.267) GO TO -29
  IF (IXY.EQ.269) GO TO -30
  IF (IXY.EQ.271) GO TO -31
  IF (IXY.EQ.273) GO TO -32
  IF (IXY.EQ.275) GO TO -33
  IF (IXY.EQ.277) GO TO -34
  IF (IXY.EQ.279) GO TO -35
  IF (IXY.EQ.281) GO TO -36
  IF (IXY.EQ.283) GO TO -37
  IF (IXY.EQ.285) GO TO -38
  IF (IXY.EQ.287) GO TO -39
  IF (IXY.EQ.289) GO TO -40
  IF (IXY.EQ.291) GO TO -41
  IF (IXY.EQ.293) GO TO -42
  IF (IXY.EQ.295) GO TO -43
  IF (IXY.EQ.297) GO TO -44
  IF (IXY.EQ.299) GO TO -45
  IF (IXY.EQ.301) GO TO -46
  IF (IXY.EQ.303) GO TO -47
  IF (IXY.EQ.305) GO TO -48
  IF (IXY.EQ.307) GO TO -49
  IF (IXY.EQ.309) GO TO -50
  IF (IXY.EQ.311) GO TO -51
  IF (IXY.EQ.313) GO TO -52
  IF (IXY.EQ.315) GO TO -53
  IF (IXY.EQ.317) GO TO -54
  IF (IXY.EQ.319) GO TO -55
  IF (IXY.EQ.321) GO TO -56
  IF (IXY.EQ.323) GO TO -57
  IF (IXY.EQ.325) GO TO -58
  IF (IXY.EQ.327) GO TO -59
  IF (IXY.EQ.329) GO TO -60
  IF (IXY.EQ.331) GO TO -61
  IF (IXY.EQ.333) GO TO -62
  IF (IXY.EQ.335) GO TO -63
  IF (IXY.EQ.337) GO TO -64
  IF (IXY.EQ.339) GO TO -65
  IF (IXY.EQ.341) GO TO -66
  IF (IXY.EQ.343) GO TO -67
  IF (IXY.EQ.345) GO TO -68
  IF (IXY.EQ.347) GO TO -69
  IF (IXY.EQ.349) GO TO -70
  IF (IXY.EQ.351) GO TO -71
  IF (IXY.EQ.353) GO TO -72
  IF (IXY.EQ.355) GO TO -73
  IF (IXY.EQ.357) GO TO -74
  IF (IXY.EQ.359) GO TO -75
  IF (IXY.EQ.361) GO TO -76
  IF (IXY.EQ.363) GO TO -77
  IF (IXY.EQ.365) GO TO -78
  IF (IXY.EQ.367) GO TO -79
  IF (IXY.EQ.369) GO TO -80
  IF (IXY.EQ.371) GO TO -81
  IF (IXY.EQ.373) GO TO -82
  IF (IXY.EQ.375) GO TO -83
  IF (IXY.EQ.377) GO TO -84
  IF (IXY.EQ.379) GO TO -85
  IF (IXY.EQ.381) GO TO -86
  IF (IXY.EQ.383) GO TO -87
  IF (IXY.EQ.385) GO TO -88
  IF (IXY.EQ.387) GO TO -89
  IF (IXY.EQ.389) GO TO -90
  IF (IXY.EQ.391) GO TO -91
  IF (IXY.EQ.393) GO TO -92
  IF (IXY.EQ.395) GO TO -93
  IF (IXY.EQ.397) GO TO -94
  IF (IXY.EQ.399) GO TO -95
  IF (IXY.EQ.401) GO TO -96
  IF (IXY.EQ.403) GO TO -97
  IF (IXY.EQ.405) GO TO -98
  IF (IXY.EQ.407) GO TO -99
  IF (IXY.EQ.409) GO TO -100
  IF (IXY.EQ.411) GO TO -101
  IF (IXY.EQ.413) GO TO -102
  IF (IXY.EQ.415) GO TO -103
  IF (IXY.EQ.417) GO TO -104
  IF (IXY.EQ.419) GO TO -105
  IF (IXY.EQ.421) GO TO -106
  IF (IXY.EQ.423) GO TO -107
  IF (IXY.EQ.425) GO TO -108
  IF (IXY.EQ.427) GO TO -109
  IF (IXY.EQ.429) GO TO -110
  IF (IXY.EQ.431) GO TO -111
  IF (IXY.EQ.433) GO TO -112
  IF (IXY.EQ.435) GO TO -113
  IF (IXY.EQ.437) GO TO -114
  IF (IXY.EQ.439) GO TO -115
  IF (IXY.EQ.441) GO TO -116
  IF (IXY.EQ.443) GO TO -117
  IF (IXY.EQ.445) GO TO -118
  IF (IXY.EQ.447) GO TO -119
  IF (IXY.EQ.449) GO TO -120
  IF (IXY.EQ.451) GO TO -121
  IF (IXY.EQ.453) GO TO -122
  IF (IXY.EQ.455) GO TO -123
  IF (IXY.EQ.457) GO TO -124
  IF (IXY.EQ.459) GO TO -125
  IF (IXY.EQ.461) GO TO -126
  IF (IXY.EQ.463) GO TO -127
  IF (IXY.EQ.465) GO TO -128
  IF (IXY.EQ.467) GO TO -129
  IF (IXY.EQ.469) GO TO -130
  IF (IXY.EQ.471) GO TO -131
  IF (IXY.EQ.473) GO TO -132
  IF (IXY.EQ.475) GO TO -133
  IF (IXY.EQ.477) GO TO -134
  IF (IXY.EQ.479) GO TO -135
  IF (IXY.EQ.481) GO TO -136
  IF (IXY.EQ.483) GO TO -137
  IF (IXY.EQ.485) GO TO -138
  IF (IXY.EQ.487) GO TO -139
  IF (IXY.EQ.489) GO TO -140
  IF (IXY.EQ.491) GO TO -141
  IF (IXY.EQ.493) GO TO -142
  IF (IXY.EQ.495) GO TO -143
  IF (IXY.EQ.497) GO TO -144
  IF (IXY.EQ.499) GO TO -145
  IF (IXY.EQ.501) GO TO -146
  IF (IXY.EQ.503) GO TO -147
  IF (IXY.EQ.505) GO TO -148
  IF (IXY.EQ.507) GO TO -149
  IF (IXY.EQ.509) GO TO -150
  IF (IXY.EQ.511) GO TO -151
  IF (IXY.EQ.513) GO TO -152
  IF (IXY.EQ.515) GO TO -153
  IF (IXY.EQ.517) GO TO -154
  IF (IXY.EQ.519) GO TO -155
  IF (IXY.EQ.521) GO TO -156
  IF (IXY.EQ.523) GO TO -157
  IF (IXY.EQ.525) GO TO -158
  IF (IXY.EQ.527) GO TO -159
  IF (IXY.EQ.529) GO TO -160
  IF (IXY.EQ.531) GO TO -161
  IF (IXY.EQ.533) GO TO -162
  IF (IXY.EQ.535) GO TO -163
  IF (IXY.EQ.537) GO TO -164
  IF (IXY.EQ.539) GO TO -165
  IF (IXY.EQ.541) GO TO -166
  IF (IXY.EQ.543) GO TO -167
  IF (IXY.EQ.545) GO TO -168
  IF (IXY.EQ.547) GO TO -169
  IF (IXY.EQ.549) GO TO -170
  IF (IXY.EQ.551) GO TO -171
  IF (IXY.EQ.553) GO TO -172
  IF (IXY.EQ.555) GO TO -173
  IF (IXY.EQ.557) GO TO -174
  IF (IXY.EQ.559) GO TO -175
  IF (IXY.EQ.561) GO TO -176
  IF (IXY.EQ.563) GO TO -177
  IF (IXY.EQ.565) GO TO -178
  IF (IXY.EQ.567) GO TO -179
  IF (IXY.EQ.569) GO TO -180
  IF (IXY.EQ.571) GO TO -181
  IF (IXY.EQ.573) GO TO -182
  IF (IXY.EQ.575) GO TO -183
  IF (IXY.EQ.577) GO TO -184
  IF (IXY.EQ.579) GO TO -185
  IF (IXY.EQ.581) GO TO -186
  IF (IXY.EQ.583) GO TO -187
  IF (IXY.EQ.585) GO TO -188
  IF (IXY.EQ.587) GO TO -189
  IF (IXY.EQ.589) GO TO -190
  IF (IXY.EQ.591) GO TO -191
  IF (IXY.EQ.593) GO TO -192
  IF (IXY.EQ.595) GO TO -193
  IF (IXY.EQ.597) GO TO -194
  IF (IXY.EQ.599) GO TO -195
  IF (IXY.EQ.601) GO TO -196
  IF (IXY.EQ.603) GO TO -197
  IF (IXY.EQ.605) GO TO -198
  IF (IXY.EQ.607) GO TO -199
  IF (IXY.EQ.609) GO TO -200
  IF (IXY.EQ.611) GO TO -201
  IF (IXY.EQ.613) GO TO -202
  IF (IXY.EQ.615) GO TO -203
  IF (IXY.EQ.617) GO TO -204
  IF (IXY.EQ.619) GO TO -205
  IF (IXY.EQ.621) GO TO -206
  IF (IXY.EQ.623) GO TO -207
  IF (IXY.EQ.625) GO TO -208
  IF (IXY.EQ.627) GO TO -209
  IF (IXY.EQ.629) GO TO -210
  IF (IXY.EQ.631) GO TO -211
  IF (IXY.EQ.633) GO TO -212
  IF (IXY.EQ.635) GO TO -213
  IF (IXY.EQ.637) GO TO -214
  IF (IXY.EQ.639) GO TO -215
  IF (IXY.EQ.641) GO TO -216
  IF (IXY.EQ.643) GO TO -217
  IF (IXY.EQ.645) GO TO -218
  IF (IXY.EQ.647) GO TO -219
  IF (IXY.EQ.649) GO TO -220
  IF (IXY.EQ.651) GO TO -221
  IF (IXY.EQ.653) GO TO -222
  IF (IXY.EQ.655) GO TO -223
  IF (IXY.EQ.657) GO TO -224
  IF (IXY.EQ.659) GO TO -225
  IF (IXY.EQ.661) GO TO -226
  IF (IXY.EQ.663) GO TO -227
  IF (IXY.EQ.665) GO TO -228
  IF (IXY.EQ.667) GO TO -229
  IF (IXY.EQ.669) GO TO -230
  IF (IXY.EQ.671) GO TO -231
  IF (IXY.EQ.673) GO TO -232
  IF (IXY.EQ.675) GO TO -233
  IF (IXY.EQ.677) GO TO -234
  IF (IXY.EQ.679) GO TO -235
  IF (IXY.EQ.681) GO TO -236
  IF (IXY.EQ.683) GO TO -237
  IF (IXY.EQ.685) GO TO -238
  IF (IXY.EQ.687) GO TO -239
  IF (IXY.EQ.689) GO TO -240
  IF (IXY.EQ.691) GO TO -241
  IF (IXY.EQ.693) GO TO -242
  IF (IXY.EQ.695) GO TO -243
  IF (IXY.EQ.697) GO TO -244
  IF (IXY.EQ.699) GO TO -245
  IF (IXY.EQ.701) GO TO -246
  IF (IXY.EQ.703) GO TO -247
  IF (IXY.EQ.705) GO TO -248
  IF (IXY.EQ.707) GO TO -249
  IF (IXY.EQ.709) GO TO -250
  IF (IXY.EQ.711) GO TO -251
  IF (IXY.EQ.713) GO TO -252
  IF (IXY.EQ.715) GO TO -253
  IF (IXY.EQ.717) GO TO -254
  IF (IXY.EQ.719) GO TO -255
  IF (IXY.EQ.721) GO TO -256
  IF (IXY.EQ.723) GO TO -257
  IF (IXY.EQ.725) GO TO -258
  IF (IXY.EQ.727) GO TO -259
  IF (IXY.EQ.729) GO TO -260
  IF (IXY.EQ.731) GO TO -261
  IF (IXY.EQ.733) GO TO -262
  IF (IXY.EQ.735) GO TO -263
  IF (IXY.EQ.737) GO TO -264
  IF (IXY.EQ.739) GO TO -265
  IF (IXY.EQ.741) GO TO -266
  IF (IXY.EQ.743) GO TO -267
  IF (IXY.EQ.745) GO TO -268
  IF (IXY.EQ.747) GO TO -269
  IF (IXY.EQ.749) GO TO -270
  IF (IXY.EQ.751) GO TO -271
  IF (IXY.EQ.753) GO TO -272
  IF (IXY.EQ.755) GO TO -273
  IF (IXY.EQ.757) GO TO -274
  IF (IXY.EQ.759) GO TO -275
  IF (IXY.EQ.761) GO TO -276
  IF (IXY.EQ.763) GO TO -277
  IF (IXY.EQ.765) GO TO -278
  IF (IXY.EQ.767) GO TO -279
  IF (IXY.EQ.769) GO TO -280
  IF (IXY.EQ.771) GO TO -281
  IF (IXY.EQ.773) GO TO -282
  IF (IXY.EQ.775) GO TO -283
  IF (IXY.EQ.777) GO TO -284
  IF (IXY.EQ.779) GO TO -285
  IF (IXY.EQ.781) GO TO -286
  IF (IXY.EQ.783) GO TO -287
  IF (IXY.EQ.785) GO TO -288
  IF (IXY.EQ.787) GO TO -289
  IF (IXY.EQ.789) GO TO -290
  IF (IXY.EQ.791) GO TO -291
  IF (IXY.EQ.793) GO TO -292
  IF (IXY.EQ.795) GO TO -293
  IF (IXY.EQ.797) GO TO -294
  IF (IXY.EQ.799) GO TO -295
  IF (IXY.EQ.801) GO TO -296
  IF (IXY.EQ.803) GO TO -297
  IF (IXY.EQ.805) GO TO -298
  IF (IXY.EQ.807) GO TO -299
  IF (IXY.EQ.809) GO TO -300
  IF (IXY.EQ.811) GO TO -301
  IF (IXY.EQ.813) GO TO -302
  IF (IXY.EQ.815) GO TO -303
  IF (IXY.EQ.817) GO TO -304
  IF (IXY.EQ.819) GO TO -305
  IF (IXY.EQ.821) GO TO -306
  IF (IXY.EQ.823) GO TO -307
  IF (IXY.EQ.825) GO TO -308
  IF (IXY.EQ.827) GO TO -309
  IF (IXY.EQ.829) GO TO -310
  IF (IXY.EQ.831) GO TO -311
  IF (IXY.EQ.833) GO TO -312
  IF (IXY.EQ.835) GO TO -313
  IF (IXY.EQ.837) GO TO -314
  IF (IXY.EQ.839) GO TO -315
  IF (IXY.EQ.841) GO TO -316
  IF (IXY.EQ.843) GO TO -317
  IF (IXY.EQ.845) GO TO -318
  IF (IXY.EQ.847) GO TO -319
  IF (IXY.EQ.849) GO TO -320
  IF (IXY.EQ.851) GO TO -321
  IF (IXY.EQ.853) GO TO -322
  IF (IXY.EQ.855) GO TO -323
  IF (IXY.EQ.857) GO TO -324
  IF (IXY.EQ.859) GO TO -325
  IF (IXY.EQ.861) GO TO -326
  IF (IXY.EQ.863) GO TO -327
  IF (IXY.EQ.865) GO TO -328
  IF (IXY.EQ.867) GO TO -329
  IF (IXY.EQ.869) GO TO -330
  IF (IXY.EQ.871) GO TO -331
  IF (IXY.EQ.873) GO TO -332
  IF (IXY.EQ.875) GO TO -333
  IF (IXY.EQ.877) GO TO -334
  IF (IXY.EQ.879) GO TO -335
  IF (IXY.EQ.881) GO TO -336
  IF (IXY.EQ.883) GO TO -337
  IF (IXY.EQ.885) GO TO -338
  IF (IXY.EQ.887) GO TO -339
  IF (IXY.EQ.889) GO TO -340
  IF (IXY.EQ.891) GO TO -341
  IF (IXY.EQ.893) GO TO -342
  IF (IXY.EQ.895) GO TO -343
  IF (IXY.EQ.897) GO TO -344
  IF (IXY.EQ.899) GO TO -345
  IF (IXY.EQ.901) GO TO -346
  IF (IXY.EQ.903) GO TO -347
  IF (IXY.EQ.905) GO TO -348
  IF (IXY.EQ.907) GO TO -349
  IF (IXY.EQ.909) GO TO -350
  IF (IXY.EQ.911) GO TO -351
  IF (IXY.EQ.913) GO TO -352
  IF (IXY.EQ.915) GO TO -353
  IF (IXY.EQ.917) GO TO -354
  IF (IXY.EQ.919) GO TO -355
  IF (IXY.EQ.921) GO TO -356
  IF (IXY.EQ.923) GO TO -357
  IF (IXY.EQ.925) GO TO -358
  IF (IXY.EQ.927) GO TO -359
  IF (IXY.EQ.929) GO TO -360
  IF (IXY.EQ.931) GO TO -361
  IF (IXY.EQ.933) GO TO -362
  IF (IXY.EQ.935) GO TO -363
  IF (IXY.EQ.937) GO TO -364
  IF (IXY.EQ.939) GO TO -365
  IF (IXY.EQ.941) GO TO -366
  IF (IXY.EQ.943) GO TO -367
  IF (IXY.EQ.945) GO TO -368
  IF (IXY.EQ.947) GO TO -369
  IF (IXY.EQ.949) GO TO -370
  IF (IXY.EQ.951) GO TO -371
  IF (IXY.EQ.953) GO TO -372
  IF (IXY.EQ.955) GO TO -373
  IF (IXY.EQ.957) GO TO -374
  IF (IXY.EQ.959) GO TO -375
  IF (IXY.EQ.961) GO TO -376
  IF (IXY.EQ.963) GO TO -377
  IF (IXY.EQ.965) GO TO -378
  IF (IXY.EQ.967) GO TO -379
  IF (IXY.EQ.969) GO TO -380
  IF (IXY.EQ.971) GO TO -381
  IF (IXY.EQ.973) GO TO -382
  IF (IXY.EQ.975) GO TO -383
  IF (IXY.EQ.977) GO TO -384
  IF (IXY.EQ.979) GO TO -385
  IF (IXY.EQ.981) GO TO -386
  IF (IXY.EQ.983) GO TO -387
  IF (IXY.EQ.985) GO TO -388
  IF (IXY.EQ.987) GO TO -389
  IF (IXY.EQ.989) GO TO -390
  IF (IXY.EQ.991) GO TO -391
  IF (IXY.EQ.993) GO TO -392
  IF (IXY.EQ.995) GO TO -393
  IF (IXY.EQ.997) GO TO -394
  IF (IXY.EQ.999) GO TO -395
  IF (IXY.EQ.1001) GO TO -396
  IF (IXY.EQ.1003) GO TO -397
  IF (IXY.EQ.1005) GO TO -398
  IF (IXY.EQ.1007) GO TO -399
  IF (IXY.EQ.1009) GO TO -400
  IF (IXY.EQ.1011) GO TO -401
  IF (IXY.EQ.1013) GO TO -402
  IF (IXY.EQ.1015) GO TO -403
  IF (IXY.EQ.1017) GO TO -404
  IF (IXY.EQ.1019) GO TO -405
  IF (IXY.EQ.1021) GO TO -406
  IF (IXY.EQ.1023) GO TO -407
  IF (IXY.EQ.1025) GO TO -408
  IF (IXY.EQ.1027) GO TO -409
  IF (IXY.EQ.1029) GO TO -410
  IF (IXY.EQ.1031) GO TO -411
  IF (IXY.EQ.1033) GO TO -412
  IF (IXY.EQ.1035) GO TO -413
  IF (IXY.EQ.1037) GO TO -414
  IF (IXY.EQ.1039) GO TO -415
  IF (IXY.EQ.1041) GO TO -416
  IF (IXY.EQ.1043) GO TO -417
  IF (IXY.EQ.1045) GO TO -418
  IF (IXY.EQ.1047) GO TO -419
  IF (IXY.EQ.1049) GO TO -420
  IF (IXY.EQ.1051) GO TO -421
  IF (IXY.EQ.1053) GO TO -422
  IF (IXY.EQ.1055) GO TO -423
  IF (IXY.EQ.1057) GO TO -424
  IF (IXY.EQ.1059) GO TO -425
  IF (IXY.EQ.1061) GO TO -426
  IF (IXY.EQ.1063) GO TO -427
  IF (IXY.EQ.1065) GO TO -428
  IF (IXY.EQ.1067) GO TO -429
  IF (IXY.EQ.1069) GO TO -430
  IF (IXY.EQ.1071) GO TO -431
  IF (IXY.EQ.1073) GO TO -432
  IF (IXY.EQ.1075) GO TO -433
  IF (IXY.EQ.1077) GO TO -434
  IF (IXY.EQ.1079) GO TO -435
  IF (IXY.EQ.1081) GO TO -436
  IF (IXY.EQ.1083) GO TO -437
  IF (IXY.EQ.1085) GO TO -438
  IF (IXY.EQ.1087) GO TO -439
  IF (IXY.EQ.1089) GO TO -440
  IF (IXY.EQ.1091) GO TO -441
  IF (IXY.EQ.1093) GO TO -442
  IF (IXY.EQ.1095) GO TO -443
  IF (IXY.EQ.1097) GO TO -444
  IF (IXY.EQ.1099) GO TO -445
  IF (IXY.EQ.1101) GO TO -446
  IF (IXY.EQ.1103) GO TO -447
  IF (IXY.EQ.1105) GO TO -448
  IF (IXY.EQ.1107) GO TO -449
  IF (IXY.EQ.1109) GO TO -450
  IF (IXY.EQ.1111) GO TO -451
  IF (IXY.EQ.1113) GO TO -452
  IF (IXY.EQ.1115) GO TO -453
  IF (IXY.EQ.1117) GO TO -454
  IF (IXY.EQ.1119) GO TO -455
  IF (IXY.EQ.1121) GO TO -456
  IF (IXY.EQ.1123) GO TO -457
  IF (IXY.EQ.1125) GO TO -458
  IF (IXY.EQ.1127) GO TO -459
  IF (IXY.EQ.1129) GO TO -460
  IF (IXY.EQ.1131) GO TO -461
  IF (IXY.EQ.1133) GO TO -462
  IF (IXY.EQ.1135) GO TO -463
  IF (IXY.EQ.1137) GO TO -464
  IF (IXY.EQ.1139) GO TO -465
  IF (IXY.EQ.1141) GO TO -466
  IF (IXY.EQ.1143) GO
```

```

00137 IF (MODEL.EQ.1) WRITE((IM,400)
IF (MODEL.EQ.2) WRITE((IM,411)
IF (MODEL.EQ.3) WRITE((IM,412)
IF (MODEL.EQ.4) WRITE((IM,413)
IF (MODEL.EQ.5) WRITE((IM,414)
IF (MODEL.EQ.6) WRITE((IM,415)
IF (IM1.NE.0) WRITE((IM,444) H1
IF (M2.NE.0) WRITE((IM,445) H2
IF (M3.NE.0) WRITE((IM,446) M3
IF (IAERO.EQ.1) WRITE((IM,471)
IF (IAERO.EQ.2) WRITE((IM,472)
IF (IAERO.EQ.3) WRITE((IM,473)
IF (IMAZE.EQ.1) AND (CKZERO(IM)) VIS=23.
IF (IMAZE.EQ.2) AND (CKZERO(IM)) VIS=5.
IF (NOT CKZERO(VIS)) WRITE((IM,417) VIS
IF (VIS.QT=0.0) AND (VIS.LT.0) WRITE((IM,442)
IF (MODEL.EQ.0) N=7
IF (MODEL.NE.0) H=MODEL
IF (MODEL.EQ.0) NLP=1
IF (MODEL.NE.0) AND (MODEL.NE.7) NLP=NL
IF (MODEL.EQ.7) NLP=MAX0(NL,1)
IF (ML.DT.NL) WRITE((IM,451) ML,NL
IF (ML.DT.NL) STOP
C
C      READ IN RADIOSONDE (MODEL = 7) OR METEOROLOGICAL (MODEL = 0) DATA
C
C      00 101 1 = 1 NL
C      IF (H.NE.7) AMZ1(1)=MZ1(1)
C      IF (H.NE.7) AMZ2(1)=MZ2(1)
C      IF (H.NE.7) Z(1)=20(1)
C      CONTINUE
C      IF (NOT CKZERO(H)) RE=REARTH(H)
C      IF (H.NE.7) OR 1M.EQ.0) GO TO 104
C
C      00 103 K = 1.NLP
C      IF (MODEL.EQ.0) READ(IR,429) 2(K),P(7,K),THP,DP,RH,MH(7,K).
C      MD17(K),RANOE
C      IF (MODEL.EQ.7) READ(IR,429) 2(K),P(7,K),THP,DP,RH,MH(7,K).
C      MD17(K),AMZ1(K)
C      IF (MODEL.EQ.0) AMZ2(K)=0.0
C      IF (MODEL.EQ.0) H1=2(K)
C      DO 102 I = 1, NL
C      IF (2(I,K).GT.20(1)) / (20(J+1)-20(J))
C      FAC=(2(I,K)-20(J))/ (20(J+1)-20(J))
C      T17(K)=THP*273.15
C      IF (M1.NE.0) T17(K)=T(M1,J)* (T(M1,J+1)/T(M1,J))**FAC
C      IF (NOT CKZERO(RH)) TT=273.15/T(K)
C      IF (NOT CKZERO(DP)) TT=273.15/(T(K)*DP)
C      IF (CKZERO(MH(7,K))) MH(7,K)=EXP((18.9766-10.8595*TT-2.43882
C      *TT+2)*TT
C      IF (NOT CKZERO(RH)) MH(7,K)=0.01*RH*MH(7,K)
C
C      00 104 H1=0. MH(7,K)=MH(M2,J)*(MH(M2,J+1)/MH(M2,J))**FAC
C      IF (M3.NE.0) MH(7,K)=MH(M3,J)*(MH(M3,J+1)/MH(M3,J))**FAC
C      IF (CKZERO(MH(2(K)))) MH22(K)=MH22(J+1)/MH22(J)**FAC
C
C      00 105
C      00 106
C      00 107
C      00 108
C      00 109
C      00 110
C      00 111
C      00 112
C      00 113
C      00 114
C      00 115
C      00 116
C      00 117
C      00 118
C      00 119
C      00 120
C      00 121
C      00 122
C      00 123
C      00 124
C      00 125
C      00 126
C      00 127
C      00 128
C      00 129
C      00 130
C      00 131
C      00 132
C      00 133
C      00 134
C      00 135
C      00 136
C      00 137
C      00 138
C      00 139
C      00 140
C      00 141
C      00 142
C      00 143
C      00 144
C      00 145
C      00 146
C      00 147
C      00 148
C      00 149
C      00 150
C      00 151
C      00 152
C      00 153
C      00 154
C      00 155
C      00 156
C      00 157
C      00 158
C      00 159
C      00 160
C      00 161
C      00 162
C      00 163
C      00 164
C      00 165
C      00 166
C      00 167
C      00 168
C      00 169
C      00 170
C      00 171
C      00 172
C      00 173
C      00 174
C      00 175
C      00 176
C      00 177
C      00 178
C      00 179
C      00 180
C      00 181
C      00 182
C      00 183
C      00 184
C      00 185
C      00 186
C      00 187
C      00 188
C      00 189
C      00 190
C      00 191
C      00 192
C      00 193
C      00 194
C      00 195
C      00 196
C      00 197
C      00 198
C      00 199
C      00 200
C      00 201
C      00 202
C      00 203
C      00 204
C      00 205
C      00 206
C      00 207
C      00 208
C      00 209
C      00 210
C      00 211
C      00 212
C      00 213
C      00 214
C      00 215
C      00 216
C      00 217
C      00 218
C      00 219
C      00 220
C      00 221
C      00 222
C      00 223
C      00 224
C      00 225
C      00 226
C      00 227
C      00 228
C      00 229
C      00 230
C      00 231
C      00 232
C      00 233
C      00 234
C      00 235
C      00 236
C      00 237
C      00 238
C      00 239
C      00 240
C      00 241
C      00 242
C      00 243
C      00 244
C      00 245
C      00 246
C      00 247
C      00 248
C      00 249
C      00 250
C      00 251
C      00 252
C      00 253
C      00 254
C      00 255
C      00 256
C      00 257
C      00 258
C      00 259
C      00 260
C      00 261
C      00 262
C      00 263
C      00 264
C      00 265
C      00 266
C      00 267
C      00 268
C      00 269
C      00 270
C      00 271
C      00 272
C      00 273
C      00 274
C      00 275
C      00 276
C      00 277
C      00 278
C      00 279
C      00 280
C      00 281
C      00 282
C      00 283
C      00 284
C      00 285
C      00 286
C      00 287
C      00 288
C      00 289
C      00 290
C      00 291
C      00 292
C      00 293
C      00 294
C      00 295
C      00 296
C      00 297
C      00 298
C      00 299
C      00 300
C      00 301
C      00 302
C      00 303
C      00 304
C      00 305
C      00 306
C      00 307
C      00 308
C      00 309
C      00 310
C      00 311
C      00 312
C      00 313
C      00 314
C      00 315
C      00 316
C      00 317
C      00 318
C      00 319
C      00 320
C      00 321
C      00 322
C      00 323
C      00 324
C      00 325
C      00 326
C      00 327
C      00 328
C      00 329
C      00 330
C      00 331
C      00 332
C      00 333
C      00 334
C      00 335
C      00 336
C      00 337
C      00 338
C      00 339
C      00 340
C      00 341
C      00 342
C      00 343
C      00 344
C      00 345
C      00 346
C      00 347
C      00 348
C      00 349
C      00 350
C      00 351
C      00 352
C      00 353
C      00 354
C      00 355
C      00 356
C      00 357
C      00 358
C      00 359
C      00 360
C      00 361
C      00 362
C      00 363
C      00 364
C      00 365
C      00 366
C      00 367
C      00 368
C      00 369
C      00 370
C      00 371
C      00 372
C      00 373
C      00 374
C      00 375
C      00 376
C      00 377
C      00 378
C      00 379
C      00 380
C      00 381
C      00 382
C      00 383
C      00 384
C      00 385
C      00 386
C      00 387
C      00 388
C      00 389
C      00 390
C      00 391
C      00 392
C      00 393
C      00 394
C      00 395
C      00 396
C      00 397
C      00 398
C      00 399
C      00 400

```



```

255 100 CONTINUE
  IF (I1IND.EQ.11) CALL ANGL (H1, MS, ANGLE, BETA, LEN, NLP)
  L0H2550
  L0H2560
  L0H2570
  L0H2580
  L0H2590
  L0H2600
  L0H2610
  L0H2620
  L0H2630
  L0H2640
  L0H2650
  L0H2660
  L0H2670
  L0H2680
  L0H2690
  L0H2700
  L0H2710
  L0H2720
  L0H2730
  L0H2740
  L0H2750
  L0H2760
  L0H2770
  L0H2780
  L0H2790
  L0H2800
  L0H2810
  L0H2820
  L0H2830
  L0H2840
  L0H2850
  L0H2860
  L0H2870
  L0H2880
  L0H2890
  L0H2900
  L0H2910
  L0H2920
  L0H2930
  L0H2940
  L0H2950
  L0H2960
  L0H2970
  L0H2980
  L0H2990
  L0H3000
  L0H3010
  L0H3020
  L0H3030
  L0H3040
  L0H3050
  L0H3060
  L0H3070
  L0H3080
  L0H3090
  L0H3100
  L0H3110

256 256*
  IF (I1IND.EQ.11) GO TO 110
  IF (J.P.EQ.0) WRITE (IN, *271)
  IF (ITYPE.EQ.11) GO TO 1100
  DO 109 K = 1,10
    VNIK1=0.0
    BETA=0.0
    SR=0.0
  109 261*
  262*
  263*
  264*
  265*
  266*
  267*
  268*
  269*
  270*
  271*
  272*
  273*
  274*
  275*
  276*
  277*
  278*
  279*
  280*
  281*
  282*
  283*
  284*
  285*
  286*
  287*
  288*
  289*
  290*
  291*
  292*
  293*
  294*
  295*
  296*
  297*
  298*
  299*
  300*
  301*
  302*
  303*
  304*
  305*
  306*
  307*
  308*
  309*
  310*
  311*
  312*

C***  NON DEFINE CONSTANT PRESSURE PATH QUANTITIES EH(1-8)
C
  SPHI=SIN(ANGLE*CA)
  RI=(RE+H1)*SPHI
  IF (H1.LE.Z*(NLP)) GO TO 110
  X=(RE+Z*(NLP))/(RE+H1)
  IF (SPHI.OT.X) HMIN=RI-RE
  IF (SPHI.OT.X) WRITE (IN, *33) HMIN
  IF (SPHI.OT.X) GO TO 209
  H1=Z*(NLP)
  J1=NLP
  SPHI=SPHI/X
  ANGLE=180.-ASIN(SPHI)/CA
  CONTINUE
  RI=(RE+H1)*SPHI
  CONTINUE
  DO 112 I = 1, NLP
    PS=PI*(H1/1013.0
    TS=273.15/T(H1,I)
    TS=296.0/273.15)*TS
    X=PS*TS
    PT=PS*QT(TS)
    D=0.1*WH(M2,I)
    PPH=q .56E-6*T(H1,I)*WH(M2,I)
    IF (CKZERO(VIS)) HAZE=1.E+38
    IF (NOT CKZERO(VIS)) HAZE=119.*((AHZ2(I))-AHZ1(I))/VIS.
    AM2(I,I)=5.0*AM2(I,I)/23.0/18.
    EM(I,I)=D*PT*0.9
    EM(I2,I)=X*PT*0.9
    EM(3,I)=46.667*WH(M3,I)*PT*0.9
    EM(4,I)=0.8*PT*X
    EM(5,I)=D*(PPH*EXP(16.08*(TSI-1.0))+0.002*(PS-PPH))
    EM(6,I)=X
    EM(7,I)=3.5338E-4*AMAX1(HAZE,0.0)
    EM(8,I)=46.667*WH(M3,I)
    EM(9,I)=0.0
    EM(10,I)=D*(0.12*PS+0.88*PPH)*EXP(16.58*(TSI-1.0))
    REF=CO*(H1,I)/T(H1,I)-q .56E-6*CH*WH(M2,I)*T(H1,I)
    IF (I.EQ.0) NLP=GO TO 111
    PPH=q .56E-6*T(H1,I)*REF+CO*(H1,I)/T(H1,I)-PPH*CH
    EM(9,I)=0.56E-6*REF+CO*(H1,I)/T(H1,I)-PPH*CH
    IF (I1IND.EQ.0.OR.JP.EQ.0) WRITE (IN, *35), 1.2(I),
      (ENIK,I),K=1,10).REF
    CONTINUE
    IF (H1.GE.211) J1=1
    EM(9,I)=EM(9,I)+1.0
    CONTINUE
  
```

```

312*      IF (MODEL.NE.0) CALL POINT (MH,YNI,J1,NP1,E,IP)
313*      IF (ITYPE.EQ.19) TXI=0
314*      IF (ITYPE.EQ.11) GO TO 47
315*      C**** DOWNHARD TRAJECTORY
316*      C
317*      IF (ANGLE.LE.90.) GO TO 19
318*      K2=0
319*      IF (NP1.EQ.1) J1=J1-1
320*      J2=J1+1
321*      JP1=J1+1
322*      IF ((MH2.OF.Z(J1+1)).OR.CKZERO(MH2-MH1)).OR.(NP1.EQ.1).AND.
323*          M2.OE.Z(J1+1)) GO TO 30
324*      CALL POINT (MH2,YNI,J2,NP2,M,IP)
325*      TX2=N(9)
326*      IF (MH2.LT.MH1) MH2
327*      IF (J1.EQ.J2) TX2=TX1+YNI-EH(9,N)
328*      IF (MH2.OF.MH1) TX1=TX2
329*      IF ((J1.EQ.J2).AND.M2.LT.MH1) YNI=TX2
330*      AD=(RE+MH)*SPHI*YNI
331*      IF (MH2.OE.MH1) YNI=YNI
332*      DO 31 I = 1,J1
333*      MHIN=AD/EH(9,1)-RE
334*      IF ((I.EQ.J1) MHIN=AD/YNI-RE
335*      IF (MHIN.LE.2(I+1)) GO TO 32
336*      CONTINUE
337*      X=MHIN
338*      IF (MHIN.LE.0.001) GO TO 34
339*      CALL POINT (MHIN,YN,JMIN,NP,TX,IP)
340*      TX3=TX(9)
341*      IF (J2.EQ.JMIN.OR.J1.EQ.JMIN) TX3=YNI+TX(9)-EH(9,N)
342*      IF ((J1.EQ.JMIN AND MH2.OE.MH1) GO TO 33
343*      MHIN=AD/TX3-RE
344*      IF (ABS(X-MHIN).GT.0.0001) GO TO 32
345*      IF ((J1.EQ.JMIN AND MH2.OE.MH1) YNI=TX3
346*      IF ((J2.EQ.JMIN AND J1.NE.J2) YNI=TX3
347*      IF (MH2.OE.MH1) TX2=TX3
348*      IF (MH2.OE.MH1) J2=JMIN
349*      IF (MH2.OE.MH1 OR MH2.LT.MHMIN) MHMIN
350*      WRITE(IW,436) MHIN
351*      IF (MH2.LT.MHMIN) WRITE(IW,440) MHMIN
352*      GO TO 35
353*      C
354*      WRITE(IW,436) MHIN
355*      IF (MH2.LT.MH1) GO TO 35
356*      IF (ITYPE.EQ.3.OR.M2.OE.MH1) WRITE(IW,437)
357*      ITYPE=2
358*      TX2=EH(9,1)
359*      JMIN=0
360*      J2=1
361*      M2=0.0
362*      H=0.0
363*      C**** NOW DEFINE VERTICAL PATH QUANTITIES YMIN-B
364*      C
365*      IF (JP.EQ.0) WRITE(IW,420)
366*      GO 135 ITES = 1.10000
367*      C
368*      C
369*      C
370*      C
371*      C
372*      C
373*      C
374*      C
375*      C
376*      C
377*      C
378*      C
379*      C
380*      C
381*      C
382*      C
383*      C
384*      C
385*      C
386*      C
387*      C
388*      C
389*      C
390*      C
391*      C
392*      C
393*      C
394*      C
395*      C
396*      C
397*      C
398*      C
399*      C
400*      C
401*      C
402*      C
403*      C
404*      C
405*      C
406*      C
407*      C
408*      C
409*      C
410*      C
411*      C
412*      C
413*      C
414*      C
415*      C
416*      C
417*      C
418*      C
419*      C
420*      C
421*      C
422*      C
423*      C
424*      C
425*      C
426*      C
427*      C
428*      C
429*      C
430*      C
431*      C
432*      C
433*      C
434*      C
435*      C
436*      C
437*      C
438*      C
439*      C
440*      C
441*      C
442*      C
443*      C
444*      C
445*      C
446*      C
447*      C
448*      C
449*      C
450*      C
451*      C
452*      C
453*      C
454*      C
455*      C
456*      C
457*      C
458*      C
459*      C
460*      C
461*      C
462*      C
463*      C
464*      C
465*      C
466*      C
467*      C
468*      C
469*      C
470*      C
471*      C
472*      C
473*      C
474*      C
475*      C
476*      C
477*      C
478*      C
479*      C
480*      C
481*      C
482*      C
483*      C
484*      C
485*      C
486*      C
487*      C
488*      C
489*      C
490*      C
491*      C
492*      C
493*      C
494*      C
495*      C
496*      C
497*      C
498*      C
499*      C
500*      C
501*      C
502*      C
503*      C
504*      C
505*      C
506*      C
507*      C
508*      C
509*      C
510*      C
511*      C
512*      C
513*      C
514*      C
515*      C
516*      C
517*      C
518*      C
519*      C
520*      C
521*      C
522*      C
523*      C
524*      C
525*      C
526*      C
527*      C
528*      C
529*      C
530*      C
531*      C
532*      C
533*      C
534*      C
535*      C
536*      C
537*      C
538*      C
539*      C
540*      C
541*      C
542*      C
543*      C
544*      C
545*      C
546*      C
547*      C
548*      C
549*      C
550*      C
551*      C
552*      C
553*      C
554*      C
555*      C
556*      C
557*      C
558*      C
559*      C
560*      C
561*      C
562*      C
563*      C
564*      C
565*      C
566*      C
567*      C
568*      C
569*      C
570*      C
571*      C
572*      C
573*      C
574*      C
575*      C
576*      C
577*      C
578*      C
579*      C
580*      C
581*      C
582*      C
583*      C
584*      C
585*      C
586*      C
587*      C
588*      C
589*      C
590*      C
591*      C
592*      C
593*      C
594*      C
595*      C
596*      C
597*      C
598*      C
599*      C
600*      C
601*      C
602*      C
603*      C
604*      C
605*      C
606*      C
607*      C
608*      C
609*      C
610*      C
611*      C
612*      C
613*      C
614*      C
615*      C
616*      C
617*      C
618*      C
619*      C
620*      C
621*      C
622*      C
623*      C
624*      C
625*      C
626*      C
627*      C
628*      C
629*      C
630*      C
631*      C
632*      C
633*      C
634*      C
635*      C
636*      C
637*      C
638*      C
639*      C
640*      C
641*      C
642*      C
643*      C
644*      C
645*      C
646*      C
647*      C
648*      C
649*      C
650*      C
651*      C
652*      C
653*      C
654*      C
655*      C
656*      C
657*      C
658*      C
659*      C
660*      C
661*      C
662*      C
663*      C
664*      C
665*      C
666*      C
667*      C
668*      C
669*      C
670*      C
671*      C
672*      C
673*      C
674*      C
675*      C
676*      C
677*      C
678*      C
679*      C
680*      C
681*      C
682*      C
683*      C
684*      C
685*      C
686*      C
687*      C
688*      C
689*      C
690*      C
691*      C
692*      C
693*      C
694*      C
695*      C
696*      C
697*      C
698*      C
699*      C
700*      C
701*      C
702*      C
703*      C
704*      C
705*      C
706*      C
707*      C
708*      C
709*      C
710*      C
711*      C
712*      C
713*      C
714*      C
715*      C
716*      C
717*      C
718*      C
719*      C
720*      C
721*      C
722*      C
723*      C
724*      C
725*      C
726*      C
727*      C
728*      C
729*      C
730*      C
731*      C
732*      C
733*      C
734*      C
735*      C
736*      C
737*      C
738*      C
739*      C
740*      C
741*      C
742*      C
743*      C
744*      C
745*      C
746*      C
747*      C
748*      C
749*      C
750*      C
751*      C
752*      C
753*      C
754*      C
755*      C
756*      C
757*      C
758*      C
759*      C
760*      C
761*      C
762*      C
763*      C
764*      C
765*      C
766*      C
767*      C
768*      C
769*      C
770*      C
771*      C
772*      C
773*      C
774*      C
775*      C
776*      C
777*      C
778*      C
779*      C
780*      C
781*      C
782*      C
783*      C
784*      C
785*      C
786*      C
787*      C
788*      C
789*      C
790*      C
791*      C
792*      C
793*      C
794*      C
795*      C
796*      C
797*      C
798*      C
799*      C
800*      C
801*      C
802*      C
803*      C
804*      C
805*      C
806*      C
807*      C
808*      C
809*      C
810*      C
811*      C
812*      C
813*      C
814*      C
815*      C
816*      C
817*      C
818*      C
819*      C
820*      C
821*      C
822*      C
823*      C
824*      C
825*      C
826*      C
827*      C
828*      C
829*      C
830*      C
831*      C
832*      C
833*      C
834*      C
835*      C
836*      C
837*      C
838*      C
839*      C
840*      C
841*      C
842*      C
843*      C
844*      C
845*      C
846*      C
847*      C
848*      C
849*      C
850*      C
851*      C
852*      C
853*      C
854*      C
855*      C
856*      C
857*      C
858*      C
859*      C
860*      C
861*      C
862*      C
863*      C
864*      C
865*      C
866*      C
867*      C
868*      C
869*      C
870*      C
871*      C
872*      C
873*      C
874*      C
875*      C
876*      C
877*      C
878*      C
879*      C
880*      C
881*      C
882*      C
883*      C
884*      C
885*      C
886*      C
887*      C
888*      C
889*      C
890*      C
891*      C
892*      C
893*      C
894*      C
895*      C
896*      C
897*      C
898*      C
899*      C
900*      C
901*      C
902*      C
903*      C
904*      C
905*      C
906*      C
907*      C
908*      C
909*      C
910*      C
911*      C
912*      C
913*      C
914*      C
915*      C
916*      C
917*      C
918*      C
919*      C
920*      C
921*      C
922*      C
923*      C
924*      C
925*      C
926*      C
927*      C
928*      C
929*      C
930*      C
931*      C
932*      C
933*      C
934*      C
935*      C
936*      C
937*      C
938*      C
939*      C
940*      C
941*      C
942*      C
943*      C
944*      C
945*      C
946*      C
947*      C
948*      C
949*      C
950*      C
951*      C
952*      C
953*      C
954*      C
955*      C
956*      C
957*      C
958*      C
959*      C
960*      C
961*      C
962*      C
963*      C
964*      C
965*      C
966*      C
967*      C
968*      C
969*      C
970*      C
971*      C
972*      C
973*      C
974*      C
975*      C
976*      C
977*      C
978*      C
979*      C
980*      C
981*      C
982*      C
983*      C
984*      C
985*      C
986*      C
987*      C
988*      C
989*      C
990*      C
991*      C
992*      C
993*      C
994*      C
995*      C
996*      C
997*      C
998*      C
999*      C

```

```

      IF (K2.EQ.0) REF=YN2
      IF (K2.EQ.1) REF=YH2
      XI=H1
      J+JP+1
      CONTINUE
      JPJ-1
      X2=2*J1
      IF ((J1.EQ.0).AND.(K2.EQ.0)) X2=H
      IF ((J1.EQ.JMIN.AND.K2.EQ.1)) X2=HM1H
      HM=(IRE+XI)*SPHI-RE
      IF (HM.NT.2*(J1).AND.HM.NT.0*J1) X2=HM
      AX=(IRE+XI)/(IRE+X2)
      DS=XI-X2
      ALP=90.0
      THET=ASIN(SPM1)/CA
      SALP=RX*SPHI
      IF ((A3S(X2-HM).NT.1.E-9)) ALP=ASIN(SALP)/CA
      BET=ALP-THEt
      IF (SPH1.NT.1.E-10) DS=(RC*X2)*SIN(BET*CA)/SPH1
      THETA=100.-THEt
      THETA=SET+SET
      PSI=GET-ALP-ANGLE+180.
      SR=SR+DS
      DO 39 K = 1,10
      AJ=ENIK(J,1)
      BJ=ENIK(J+1)
      IF ((J.EQ.J1) .AND. (BJ-E(K)) .LT. 0.0) AJ=H(K)
      IF ((J.EQ.J2) .AND. (AJ-E(K)) .LT. 0.0) AJ=H(K)
      IF ((J.EQ.JMIN) .AND. (AJ-E(K)) .LT. 1.E-3) AJ=TX(K)
      IF ((J.EQ.JMIN) .AND. (ABS((H2-M1).LT.1.E-3)) AJ=TX(K)
      IF (K2.NE.0 .AND. J.EQ.J2) BJ=H(K)
      IF (K2.NE.0 .AND. J.EQ.JMIN) AJ=X(K)
      IF (CKZERO(AJ,BJ).OR.CKZERO(BJ,J) .EV.0.0
      IF (CKZERO(AJ,BJ).EV.0)
      IF (.NOT.CKZERO(AJ).AND..NOT.CKZERO(BJ)) .EV.DS.(AJ-BJ)/ALOG(AJ/BJ)
      VHK1VH(K)+EV
      CONTINUE
      IF (LJ.PEQ.0) WRITE(LIM,435) J,XI,(VNL(L),L=1,8),PSI,ALP.
      IF (BETA.THTA.SR
      IF ((J.EQ.J2) .AND. (H2.EQ.M1)) GO TO 45
      IF ((J.EQ.JMIN) .AND. (K2.EQ.J1)) GO TO 45
      IF (J.NE.-1) RN=REF/EM10.J-11
      IF ((J.EQ.J2+1) RN=REF/TX2
      IF ((J.EQ.J2) .AND. (K2.EQ.0)) RN=REF/YN2
      IF ((J.EQ.JMIN+1) .AND. (K2.EQ.1)) RN=REF/TX3
      IF ((SALP.OE.RN) RN=1.0
      SPHI=SPH1.RN
      REF=EM10.J1
      IF ((J.EQ.J2+1) .AND. K2.EQ.0) REF=TZ2
      XI=X2
      IF (J1.NE.1 .AND. (J1.NE.J2.OR.K2.NE.0)) GO TO 30
      IF (ILEN.LE.0.0) GO TO 47
      IF (ILEN.EQ.0) WRITE(LN,430)
      IF (ILEN.EQ.0) GO TO 47
      IF (ILEN.EQ.0) GO TO 47
      WRITE(LM,439)

```

```

1 IF (ABS(X1-MININ).LE.0.001) GO TO 47
20
21 H=MMIN
22 JP1=J2+1
23 IF (NP2.EQ.1) JP1=JP1-1
24 B=BETA
25 PH=180.-ASIN(SPH1)/CA
26 TS=SR
27 PS=PSI
28 DO 42 K = 1,10
29   E(K)=VM(K)
30   BETA=2.*BETA-B
31   PSI=2.*PSI-PS
32   SR=2.*SR-SR-15
33 CONTINUE
34
35 C    LONG PATH TAKEN
36
37 C    PHI=PH
38   DO 44 K = 1,10
39     VM(K)=2.*VM(K)-E(K)
40   GO TO 47
41
42 C    CONTINUE
43   DO 46 K = 1,10
44     VM(K)=2.*VM(K)
45   BETA=2.*BETA
46   SR=2.*SR
47   IF (CKZERO(M2-M1)) GO TO 47
48   RN=TX1/RN1
49   SPHI=SIN(ANGLE*CA)
50   IF (SPHI.LT.RN) SPHI=SPHI/RN
51
52 C    UPWARD TRAJECTORY
53
54 C    10
55 C    CONTINUE
56 C    11
57 C    12
58 C    13
59 C    14
60 C    15
61 C    16
62 C    17
63 C    18
64 C    19
65 C    20
66 C    21
67 C    22
68 C    23
69 C    24
70 C    25
71 C    26
72 C    27
73 C    28
74 C    29
75 C    30
76 C    31
77 C    32
78 C    33
79 C    34
80 C    35
81 C    36
82 C    37
83 C    38
84 C    39
85 C    40
86 C    41
87 C    42
88 C    43
89 C    44
90 C    45
91 C    46
92 C    47
93 C    48
94 C    49
95 C    50
96 C    51
97 C    52
98 C    53
99 C    54
100 C    55
101 C    56
102 C    57
103 C    58
104 C    59
105 C    60
106 C    61
107 C    62
108 C    63
109 C    64
110 C    65
111 C    66
112 C    67
113 C    68
114 C    69
115 C    70
116 C    71
117 C    72
118 C    73
119 C    74
120 C    75
121 C    76
122 C    77
123 C    78
124 C    79
125 C    80
126 C    81
127 C    82
128 C    83
129 C    84
130 C    85
131 C    86
132 C    87
133 C    88
134 C    89
135 C    90
136 C    91
137 C    92
138 C    93
139 C    94
140 C    95
141 C    96
142 C    97
143 C    98
144 C    99
145 C    100
146 C    101
147 C    102
148 C    103
149 C    104
150 C    105
151 C    106
152 C    107
153 C    108
154 C    109
155 C    110
156 C    111
157 C    112
158 C    113
159 C    114
160 C    115
161 C    116
162 C    117
163 C    118
164 C    119
165 C    120
166 C    121
167 C    122
168 C    123
169 C    124
170 C    125
171 C    126
172 C    127
173 C    128
174 C    129
175 C    130
176 C    131
177 C    132
178 C    133
179 C    134
180 C    135
181 C    136
182 C    137
183 C    138
184 C    139
185 C    140
186 C    141
187 C    142
188 C    143
189 C    144
190 C    145
191 C    146
192 C    147
193 C    148
194 C    149
195 C    150
196 C    151
197 C    152
198 C    153
199 C    154
200 C    155
201 C    156
202 C    157
203 C    158
204 C    159
205 C    160
206 C    161
207 C    162
208 C    163
209 C    164
210 C    165
211 C    166
212 C    167
213 C    168
214 C    169
215 C    170
216 C    171
217 C    172
218 C    173
219 C    174
220 C    175
221 C    176
222 C    177
223 C    178
224 C    179
225 C    180
226 C    181
227 C    182
228 C    183
229 C    184
230 C    185
231 C    186
232 C    187
233 C    188
234 C    189
235 C    190
236 C    191
237 C    192
238 C    193
239 C    194
240 C    195
241 C    196
242 C    197
243 C    198
244 C    199
245 C    200
246 C    201
247 C    202
248 C    203
249 C    204
250 C    205
251 C    206
252 C    207
253 C    208
254 C    209
255 C    210
256 C    211
257 C    212
258 C    213
259 C    214
260 C    215
261 C    216
262 C    217
263 C    218
264 C    219
265 C    220
266 C    221
267 C    222
268 C    223
269 C    224
270 C    225
271 C    226
272 C    227
273 C    228
274 C    229
275 C    230
276 C    231
277 C    232
278 C    233
279 C    234
280 C    235
281 C    236
282 C    237
283 C    238
284 C    239
285 C    240
286 C    241
287 C    242
288 C    243
289 C    244
290 C    245
291 C    246
292 C    247
293 C    248
294 C    249
295 C    250
296 C    251
297 C    252
298 C    253
299 C    254
300 C    255
301 C    256
302 C    257
303 C    258
304 C    259
305 C    260
306 C    261
307 C    262
308 C    263
309 C    264
310 C    265
311 C    266
312 C    267
313 C    268
314 C    269
315 C    270
316 C    271
317 C    272
318 C    273
319 C    274
320 C    275
321 C    276
322 C    277
323 C    278
324 C    279
325 C    280
326 C    281
327 C    282
328 C    283
329 C    284
330 C    285
331 C    286
332 C    287
333 C    288
334 C    289
335 C    290
336 C    291
337 C    292
338 C    293
339 C    294
340 C    295
341 C    296
342 C    297
343 C    298
344 C    299
345 C    300
346 C    301
347 C    302
348 C    303
349 C    304
350 C    305
351 C    306
352 C    307
353 C    308
354 C    309
355 C    310
356 C    311
357 C    312
358 C    313
359 C    314
360 C    315
361 C    316
362 C    317
363 C    318
364 C    319
365 C    320
366 C    321
367 C    322
368 C    323
369 C    324
370 C    325
371 C    326
372 C    327
373 C    328
374 C    329
375 C    330
376 C    331
377 C    332
378 C    333
379 C    334
380 C    335
381 C    336
382 C    337
383 C    338
384 C    339
385 C    340
386 C    341
387 C    342
388 C    343
389 C    344
390 C    345
391 C    346
392 C    347
393 C    348
394 C    349
395 C    350
396 C    351
397 C    352
398 C    353
399 C    354
400 C    355
401 C    356
402 C    357
403 C    358
404 C    359
405 C    360
406 C    361
407 C    362
408 C    363
409 C    364
410 C    365
411 C    366
412 C    367
413 C    368
414 C    369
415 C    370
416 C    371
417 C    372
418 C    373
419 C    374
420 C    375
421 C    376
422 C    377
423 C    378
424 C    379
425 C    380
426 C    381
427 C    382
428 C    383
429 C    384
430 C    385
431 C    386
432 C    387
433 C    388
434 C    389
435 C    390
436 C    391
437 C    392
438 C    393
439 C    394
440 C    395
441 C    396
442 C    397
443 C    398
444 C    399
445 C    400
446 C    401
447 C    402
448 C    403
449 C    404
450 C    405
451 C    406
452 C    407
453 C    408
454 C    409
455 C    410
456 C    411
457 C    412
458 C    413
459 C    414
460 C    415
461 C    416
462 C    417
463 C    418
464 C    419
465 C    420
466 C    421
467 C    422
468 C    423
469 C    424
470 C    425
471 C    426
472 C    427
473 C    428
474 C    429
475 C    430
476 C    431
477 C    432
478 C    433
479 C    434
480 C    435
481 C    436
482 C    437
483 C    438
484 C    439
485 C    440
486 C    441
487 C    442
488 C    443
489 C    444
490 C    445
491 C    446
492 C    447
493 C    448
494 C    449
495 C    450
496 C    451
497 C    452
498 C    453
499 C    454
500 C    455
501 C    456
502 C    457
503 C    458
504 C    459
505 C    460
506 C    461
507 C    462
508 C    463
509 C    464
510 C    465
511 C    466
512 C    467
513 C    468
514 C    469
515 C    470
516 C    471
517 C    472
518 C    473
519 C    474
520 C    475
521 C    476
522 C    477
523 C    478
524 C    479
525 C    480
526 C    481
527 C    482
528 C    483
529 C    484
530 C    485
531 C    486
532 C    487
533 C    488
534 C    489
535 C    490
536 C    491
537 C    492
538 C    493
539 C    494
540 C    495
541 C    496
542 C    497
543 C    498
544 C    499
545 C    500
546 C    501
547 C    502
548 C    503
549 C    504
550 C    505
551 C    506
552 C    507
553 C    508
554 C    509
555 C    510
556 C    511
557 C    512
558 C    513
559 C    514
560 C    515
561 C    516
562 C    517
563 C    518
564 C    519
565 C    520
566 C    521
567 C    522
568 C    523
569 C    524
570 C    525
571 C    526
572 C    527
573 C    528
574 C    529
575 C    530
576 C    531
577 C    532
578 C    533
579 C    534
580 C    535
581 C    536
582 C    537
583 C    538
584 C    539
585 C    540
586 C    541
587 C    542
588 C    543
589 C    544
590 C    545
591 C    546
592 C    547
593 C    548
594 C    549
595 C    550
596 C    551
597 C    552
598 C    553
599 C    554
600 C    555
601 C    556
602 C    557
603 C    558
604 C    559
605 C    560
606 C    561
607 C    562
608 C    563
609 C    564
610 C    565
611 C    566
612 C    567
613 C    568
614 C    569
615 C    570
616 C    571
617 C    572
618 C    573
619 C    574
620 C    575
621 C    576
622 C    577
623 C    578
624 C    579
625 C    580
626 C    581
627 C    582
628 C    583
629 C    584
630 C    585
631 C    586
632 C    587
633 C    588
634 C    589
635 C    590
636 C    591
637 C    592
638 C    593
639 C    594
640 C    595
641 C    596
642 C    597
643 C    598
644 C    599
645 C    600
646 C    601
647 C    602
648 C    603
649 C    604
650 C    605
651 C    606
652 C    607
653 C    608
654 C    609
655 C    610
656 C    611
657 C    612
658 C    613
659 C    614
660 C    615
661 C    616
662 C    617
663 C    618
664 C    619
665 C    620
666 C    621
667 C    622
668 C    623
669 C    624
670 C    625
671 C    626
672 C    627
673 C    628
674 C    629
675 C    630
676 C    631
677 C    632
678 C    633
679 C    634
680 C    635
681 C    636
682 C    637
683 C    638
684 C    639
685 C    640
686 C    641
687 C    642
688 C    643
689 C    644
690 C    645
691 C    646
692 C    647
693 C    648
694 C    649
695 C    650
696 C    651
697 C    652
698 C    653
699 C    654
700 C    655
701 C    656
702 C    657
703 C    658
704 C    659
705 C    660
706 C    661
707 C    662
708 C    663
709 C    664
710 C    665
711 C    666
712 C    667
713 C    668
714 C    669
715 C    670
716 C    671
717 C    672
718 C    673
719 C    674
720 C    675
721 C    676
722 C    677
723 C    678
724 C    679
725 C    680
726 C    681
727 C    682
728 C    683
729 C    684
730 C    685
731 C    686
732 C    687
733 C    688
734 C    689
735 C    690
736 C    691
737 C    692
738 C    693
739 C    694
740 C    695
741 C    696
742 C    697
743 C    698
744 C    699
745 C    700
746 C    701
747 C    702
748 C    703
749 C    704
750 C    705
751 C    706
752 C    707
753 C    708
754 C    709
755 C    710
756 C    711
757 C    712
758 C    713
759 C    714
760 C    715
761 C    716
762 C    717
763 C    718
764 C    719
765 C    720
766 C    721
767 C    722
768 C    723
769 C    724
770 C    725
771 C    726
772 C    727
773 C    728
774 C    729
775 C    730
776 C    731
777 C    732
778 C    733
779 C    734
780 C    735
781 C    736
782 C    737
783 C    738
784 C    739
785 C    740
786 C    741
787 C    742
788 C    743
789 C    744
790 C    745
791 C    746
792 C    747
793 C    748
794 C    749
795 C    750
796 C    751
797 C    752
798 C    753
799 C    754
800 C    755
801 C    756
802 C    757
803 C    758
804 C    759
805 C    760
806 C    761
807 C    762
808 C    763
809 C    764
810 C    765
811 C    766
812 C    767
813 C    768
814 C    769
815 C    770
816 C    771
817 C    772
818 C    773
819 C    774
820 C    775
821 C    776
822 C    777
823 C    778
824 C    779
825 C    780
826 C    781
827 C    782
828 C    783
829 C    784
830 C    785
831 C    786
832 C    787
833 C    788
834 C    789
835 C    790
836 C    791
837 C    792
838 C    793
839 C    794
840 C    795
841 C    796
842 C    797
843 C    798
844 C    799
845 C    800
846 C    801
847 C    802
848 C    803
849 C    804
850 C    805
851 C    806
852 C    807
853 C    808
854 C    809
855 C    810
856 C    811
857 C    812
858 C    813
859 C    814
860 C    815
861 C    816
862 C    817
863 C    818
864 C    819
865 C    820
866 C    821
867 C    822
868 C    823
869 C    824
870 C    825
871 C    826
872 C    827
873 C    828
874 C    829
875 C    830
876 C    831
877 C    832
878 C    833
879 C    834
880 C    835
881 C    836
882 C    837
883 C    838
884 C    839
885 C    840
886 C    841
887 C    842
888 C    843
889 C    844
890 C    845
891 C    846
892 C    847
893 C    848
894 C    849
895 C    850
896 C    851
897 C    852
898 C    853
899 C    854
900 C    855
901 C    856
902 C    857
903 C    858
904 C    859
905 C    860
906 C    861
907 C    862
908 C    863
909 C    864
910 C    865
911 C    866
912 C    867
913 C    868
914 C    869
915 C    870
916 C    871
917 C    872
918 C    873
919 C    874
920 C    875
921 C    876
922 C    877
923 C    878
924 C    879
925 C    880
926 C    881
927 C    882
928 C    883
929 C    884
930 C    885
931 C    886
932 C    887
933 C    888
934 C    889
935 C    890
936 C    891
937 C    892
938 C    893
939 C    894
940 C    895
941 C    896
942 C    897
943 C    898
944 C    899
945 C    900
946 C    901
947 C    902
948 C    903
949 C    904
950 C    905
951 C    906
952 C    907
953 C    908
954 C    909
955 C    910
956 C    911
957 C    912
958 C    913
959 C    914
960 C    915
961 C    916
962 C    917
963 C    918
964 C    919
965 C    920
966 C    921
967 C    922
968 C    923
969 C    924
970 C    925
971 C    926
972 C    927
973 C    928
974 C    929
975 C    930
976 C    931
977 C    932
978 C    933
979 C    934
980 C    935
981 C    936
982 C    937
983 C    938
984 C    939
985 C    940
986 C    941
987 C    942
988 C    943
989 C    944
990 C    945
991 C    946
992 C    947
993 C    948
994 C    949
995 C    950
996 C    951
997 C    952
998 C    953
999 C    954
1000 C    955
1001 C    956
1002 C    957
1003 C    958
1004 C    959
1005 C    960
1006 C    961
1007 C    962
1008 C    963
1009 C    964
1010 C    965
1011 C    966
1012 C    967
1013 C    968
1014 C    969
1015 C    970
1016 C    971
1017 C    972
1018 C    973
1019 C    974
1020 C    975
1021 C    976
1022 C    977
1023 C    978
1024 C    979
1025 C    980
1026 C    981
1027 C    982
1028 C    983
1029 C    984
1030 C    985
1031 C    986
1032 C    987
1033 C    988
1034 C    989
1035 C    990
1036 C    991
1037 C    992
1038 C    993
1039 C    994
1040 C    995
1041 C    996
1042 C    997
1043 C    998
1044 C    999
1045 C    1000
1046 C    1001
1047 C    1002
1048 C    1003
1049 C    1004
1050 C    1005
1051 C    1006
1052 C    1007
1053 C    1008
1054 C    1009
1055 C    1010
1056 C    1011
1057 C    1012
1058 C    1013
1059 C    1014
1060 C    1015
1061 C    1016
1062 C    1017
1063 C    1018
1064 C    1019
1065 C    1020
1066 C    1021
1067 C    1022
1068 C    1023
1069 C    1024
1070 C    1025
1071 C    1026
1072 C    1027
1073 C    1028
1074 C    1029
1075 C    1030
1076 C    1031
1077 C    1032
1078 C    1033
1079 C    1034
1080 C    1035
1081 C    1036
1082 C    1037
1083 C    1038
1084 C    1039
1085 C    1040
1086 C    1041
1087 C    1042
1088 C    1043
1089 C    1044
1090 C    1045
1091 C    1046
1092 C    1047
1093 C    1048
1094 C    1049
1095 C    1050
1096 C    1051
1097 C    1052
1098 C    1053
1099 C    1054
1100 C    1055
1101 C    1056
1102 C    1057
1103 C    1058
1104 C    1059
1105 C    1060
1106 C    1061
1107 C    1062
1108 C    1063
1109 C    1064
1110 C    1065
1111 C    1066
1112 C    1067
1113 C    1068
1114 C    1069
1115 C    1070
1116 C    1071
1117 C    1072
1118 C    1073
1119 C    1074
1120 C    1075
1121 C    1076
1122 C    1077
1123 C    1078
1124 C    1079
1125 C    1080
1126 C    1081
1127 C    1082
1128 C    1083
1129 C    1084
1130 C    1085
1131 C    1086
1132 C    1087
1133 C    1088
1134 C    1089
1135 C    1090
1136 C    1091
1137 C    1092
1138 C    1093
1139 C    1094
1140 C    1
```


K*(IV-575)/5*
 IF (IV.OE. 350. AND. IV.LT.12800).OR.
 (IV.OE.13400.AND. IV.LE.14500))
 HS1=ALO010(MAX1(M(11,1,OE-201)+C(11))
 IF (IV.LT. 350. OR. IV.OE.12800).AND.
 (IV.LT.13400.OR. IV.OE.14500)) HS1=FW(11)-1.0
 IF (IV.OE. 300. AND. IV.LT.8060).OR.
 (IV.01.12970.AND. IV.LT.3190))
 HS2=ALO010(M(2),1,OE-20)+C2(J)
 IF ((IV.LT. 500. OR. IV.OE.8060).AND.
 (IV.LE.12970.OR. IV.OE.13190)). HS2=FW(11)-1.0
 IF (IV.OE. 575. AND. IV.LE. 3270)
 HS3=ALO010(MAX1(M(3),1,OE-20)+C3(K))
 IF ((IV.LT.575.OR. IV.OE. 3270). HS3=F(01))-1.0
 NS1=0
 NS2=0
 NS3=0
 DO 202 L = 1,67
 IF (HS1.FW(L)) NS1=L
 IF (HS2.GE.FW(L)) NS2=L
 IF (HS3.GE.FO(L)) NS3=L
 CONTINUE
 202
 C***** WATER VAPOUR
 C
 IF (NS1.EQ.0) TX(1)=1.0
 IF (NS1.GT.0.AND.NS2.LT.67) TX(1)=TR(NS1+1)+
 (TR(NS1)-TR(NS1+1))*(FW(NS1+1)-NS2)/(FW(NS1+1)-FW(NS1))
 IF (NS1.EQ.67) TX(1)=0.0
 C***** UNIFORMLY MIXED GASES
 C
 IF (NS2.EQ.0) TX(2)=1.0
 IF (NS2.GT.0.AND.NS2.LT.67) TX(2)=TR(NS2+1)+
 (TR(NS2)-TR(NS2+1))*(FW(NS2+1)-NS2)/(FW(NS2+1)-FW(NS2))
 IF (NS2.EQ.67) TX(2)=0.0
 C
 OZONE
 C
 IF (NS3.EQ.0) TX(3)=1.0
 IF (NS3.GT.0.AND.NS3.LT.67) TX(3)=TR(NS3+1)+
 (TR(NS3)-TR(NS3+1))*(FO(NS3+1)-NS3)/(FO(NS3+1)-FO(NS3))
 IF (NS3.EQ.67) TX(3)=0.0
 C***** NITROGEN CONTINUUM
 C
 K*(IV-2080)/5*
 IF (IV.LT.2000.OR.IV.OE.2740) TX(4)=C4(K)*W(4)
 IF (IV.OE. 2000.AND. IV.LT. 2740) TX(4)=C4(K)*W(4)
 C***** WATER VAPOUR CONTINUUM
 C
 X1=FLOAT(IV-2350)/50.0+1.0
 NM=IFIX(X1)
 TX(NM)=0.0
 C***** 10 MICRON REGION
 C

```

597*   C      IF ((IV.OE. = 870.AND.IV.LE. 1390) TX(9)=14.18+55570.0*
      C      EXP(-7.87E-3*FLOAT((IV)))+W(9);
      C      * MICRON REGION
      C      IF ((IV.OE. 2350.AND.IV.LE.3000) TX(9)=(C5(NH)+(X1-FLOAT(NH));
      C      * +(C5(NH+1)-C5(NH)));
      C      * W(10);
      C      * MOLECULAR SCATTERING
      C      IF ((IV.LT. 2740) TX(9)=0.0
      C      IF ((IV.OE. 2740.AND.IV.LE.3000)
      C      * TX(9)=9.807E-20*(FLOAT((IV))+0.0117)*W(9);
      C      * AEROSOL EXTINCTION
      C      ML=10000./FLOAT((IV))
      C      XX=0.0
      C      YY=0.0
      C      TX(7)=0.0
      C      TX(10)=0.0
      C      IF ((IAZAE.E0.0) 00 TO 204
      NS=0
      DO 203 L=1,94
      IF ((ML .EQ. VXAERO(L)) NS=L
      IF (NS .EQ. 0) AND. MS .LT. 492 XX=C7 ((AERO,NS+1)-
      C7 ((AERO,NS)-C7 ((AERO,NS+1)-(VXAERO,NS+1))-ML)/
      (VXAERO(NS+1)-VXAERO,NS+1)
      IF (NS .EQ. 0) AND. MS .LT. 492 YY=C7 ((AERO,NS+1)-
      (C7 ((AERO,NS)-C7 ((AERO,NS+1)-(VXAERO,NS+1))-ML)/
      (VXAERO,NS+1)-(VXAERO,NS+1))
      CONTINUE
      TX(7)=XX+(17)
      TX(10)=YY+ML;
      TX(10)=YY+ML;
      C      * UV OZONE
      C      IF ((IV.OE. 13000.AND.IV.LE. 23400) XI=FLOAT((IV-13000)/200)+I.
      C      IF ((IV.OE. 27500.AND.IV.LE.50000) XI=FLOAT((IV-27500)/500)+B7.
      C      * XI(X1)+1
      C      IF ((IV.OE. 11000.AND.IV.LE. 23400).OR.
      C      * ((IV.OE. 27500.AND.IV.LE.50000).
      C      * TX(9)=W(9)+(C8(N)+((XI-FLOAT(N))+C8(N-1)))
      C      * TX(9).OR. IV.LT.13000.OR. IV.OE. 23400).AND.
      C      * IV.LT.27500.OR.IV.OE. 50000).TX(9)=0.0
      TX(9)=0.0
      IF ((IV.OE. 2080.AND.IV.LT. 27400 TX(9)=TX(9)+TX(9))
      IF ((IV.OE. 870.AND.IV.LT. 3000 TX(9)=TX(9)+TX(9))
      IF ((IV.OE. 2740.AND.IV.LT.50000) TX(9)=TX(9)+TX(9))
      TX(9)=TX(9)+(X(7))
      IF ((IV.OE. 13000.AND.IV.LE. 23400).OR.
      * ((IV.OE. 27500.AND.IV.LE.50000).TX(9)=TX(9)+TX(9))
      DO 205 L=4,10
      TX(10)=EXP(-TX(L))
      TX(10)=1.0-TX(10)
      203

```

```

      TX(1)=TX((1)*TX(2)); TX(3)=TX(1)
      IF (IV,0C,13000, AND IV,LL,30000) TX(3)=TX(0)
      IF (UP,EO,3) TX(0)=TX(1)
      AB=1.0-TX(0)
      IF (IV,EO,IV1, OR, IV,EO,IV2) AB=0.5-AB
      SUM=SUM+AB*FLOAT(IV1)
      IF (UP,EO,0, AND, IABS(MOD(IV,50-IDV)),EQ,0) WHITE((IV,425),LOH6600)
      IF (UP,EO,0) WHITE(IV,423) IV,ML,TX(0),(TX(L),LP1,7),TX(10),LOH6610
      SUM
      AB=1.0-SUM/FLOAT(IV2-IV1)
      WRITE(1M,424) IV1,IV2,SUM,AB
      READ(LR,400) IXY
      CONTINUE
      400 FORMAT(9I3,3X,2F10.3)
      405 FORMAT(2I3,4X,2F10.3)
      406 FORMAT(10X,29H HORIZONTAL PATH, ALTITUDE = F7.3,13H KM, RANGE = LOH67400
      407 FORMAT(10X,29H SLANT PATH BETWEEN ALTITUDES M1 AND M2 WHERE M1 =LOH67500
      408 FORMAT(10X,5IM SLANT PATH BETWEEN ALTITUDES M1 AND M2 WHERE M1 =F7.3,8H DEGREES, M2 =F7.3,8H DEGREES, LOH67700
      409 FORMAT(10X,40H SLANT PATH TO SPACE FROM ALTITUDE M1 = F7.3,18H LOH67800
      410 FORMAT(1M,10X,4IM TROPICAL (115 DEG. LAT.) MODEL ATMOSPHERE) LOH6800
      411 FORMAT(1M,10X,5IM MIDLATITUDE (45 DEG. LAT.) SUMMER MODEL ATMOSPHERE) LOH68200
      412 FORMAT(1M,10X,5IM MIDLATITUDE (45 DEG. LAT.) WINTER MODEL ATMOSPHERE) LOH68300
      413 FORMAT(1M,10X,5IM SUB-ARCTIC (60 DEG. LAT.) SUMMER MODEL ATMOSPHERE) LOH68500
      414 FORMAT(1M,10X,5IM SUB-ARCTIC (60 DEG. LAT.) WINTER MODEL ATMOSPHERE) LOH68700
      415 FORMAT(1M,10X,36W 1962 U.S. STANDARD ATMOSPHERE MODEL) LOH68900
      417 FORMAT(10X,14H HAZE MODEL = F5.1,29H KM VISUAL RANGE AT SEA LEVEL) LOH6900
      418 FORMAT(10X,22H FREQUENCY RANGE VI = F7.1,14H CM-1 TO V2 = F7.1, LOH69200
      419 *15H CM-1 FOR DV = F6.1,9H CM-1 (F6.2,9H MICRONS),//,LOH69300
      420 FORMAT(10X,38H EQUIVALENT SEA LEVEL ABSORBER AMOUNTS //21X,110HATL0H69400
      421 *ER VAPOUR CO2 ETC. OZONE NITROGEN (CONT) H2O (CONT) LOH69500
      422 *MOL SCAT AEROSOL OZONE (U-V)/24X,7HOM CM-2,10X,2HMM, LOH69600
      423 *10X,5HATM CM-10X,2HMM,9X,7HOM CM-2,10X,2HMM,13X,2HMM,10X,5HATM CM-1,LOH69700
      424 FORMAT(1M,1//10X,2H VERTICAL PROFILES .63X,3MPS1,4X,3MPH1,6X, LOH69800
      425 *HIGETA,4X,13HTHETA RANGE) LOH69900
      426 FORMAT(10X,10H M11-B) *BLIPEN,31/74X,1PE14,3/, LOW70000
      427 FORMAT(10X,10X,32H FREQ WAVELENGTH TOTAL M20,5X,4HC02*,5X, LOW70100
      428 *84HOZONE M2 CONT MOL SCAT AEROSOL AEROSOL INTEGRATE LOW70200
      429 *D /1X,14W CM-1 MICRONS,814X,5MTRANS) ,4X,20H ABS ABSORPTION J,LOW70300
      430 FORMAT(10X,16,10H,4,F12.2) LOW70400
      421 *FORMAT(1//27H INTEGRATED ABSORPTION FROM .15,4H 10 .15,8H CH-1 - . LOW70500
      422 *F10,2,26H, AVERAGE TRANSMITTANCE = F8,4, LOW70600
      423 FORMAT(1//20X,42HAKSOIL SCATTERING NOT COMPUTED. IMAGE = 01, LOW70700
      424 FORMAT(1M,1//10X,20H HORIZONTAL PROFILES) LOW70800
      425 FORMAT(10X,8H MI) *F7.3,10H KM, M2 *F7.3,13H KM, ANGLE = . LOW70900
      426 *F8,4,14H GEOM. RANGE = F7.2,12H KM, BETA = ,F8,5,4H DEG, LOW71000

```

```

FORMAT(10.3,2F9.2)(IPE10.3),OPPF10.3) LOW71100
    7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*
    01722    01722    01722    01722    01722    01722    01722    01722    01722    01722
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      F7.2, 0M  MS. T   *      F5.1, 1.18H C. DEW PT. TEMP = *      FS.1, 1.19H C. REL. HUM. LOW71300
    *101TY = *      F5.1, 1.21H PCT. H2O DENSITY = *      IPE9.2, 7M GM.H-3/10X.17M OZOLLOW71400
    *NE DENSITY = *      IPE9.2, 17M GM.H-3. RANGE = *      F10.3, 3M KM) LOW71500
    *      FORM169H TRAJECTORY MISSES EARTH ATMOSPHERE. CLOSEST DISTANCE OFLOW71600
    *      APPROACH IS .F10.7/19H END OF CALCULATION! LOW71700
    01723    01723    01723    01723    01723    01723    01723    01723    01723    01723
    7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORM10X.1M .F6.1, 1(IPE10.3) LOW71800
    01724    01724    01724    01724    01724    01724    01724    01724    01724    01724
    7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORM113.F8.1, 8(IPE10.3).4(OPF9.4).F8.1) LOW71900
    01725    01725    01725    01725    01725    01725    01725    01725    01725    01725
    7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*   7120*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT164H PATH INTERSECTS EARTH - PATH CHANGED TO TYPE 2 WITH H2 LOW72000
    01726    01726    01726    01726    01726    01726    01726    01726    01726    01726
    7200*   7200*   7200*   7200*   7200*   7200*   7200*   7200*   7200*   7200*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT185H CHOICE OF TWO PATHS FOR THIS CASE - SHORTER PATH TAKEN LOW72200
    01727    01727    01727    01727    01727    01727    01727    01727    01727    01727
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FOR LONGER PATH SET LEN = 1) LOW72400
    01728    01728    01728    01728    01728    01728    01728    01728    01728    01728
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT185H CHOICE OF TWO PATHS FOR THIS CASE - LONGER PATH TAKEN. LOW72500
    01729    01729    01729    01729    01729    01729    01729    01729    01729    01729
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FOR SHORTER PATH SET LEN = 0) LOW72600
    01730    01730    01730    01730    01730    01730    01730    01730    01730    01730
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT70H H2 WAS SET LESS THAN MMIN AND HAS BEEN RESET EQUAL TO ML0W72700
    01731    01731    01731    01731    01731    01731    01731    01731    01731    01731
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      'MIN I.E., H2 = .F 10.3) LOW72800
    01732    01732    01732    01732    01732    01732    01732    01732    01732    01732
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT124H MODEL ATMOSPHERE NO. 7/23M Z (KMH) P (MB) LOW72900
    01733    01733    01733    01733    01733    01733    01733    01733    01733    01733
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      HEIGHT (C) DEW PT RH H20(GM H-3) 031GM H-3) NO. DEN.) LOW73000
    01734    01734    01734    01734    01734    01734    01734    01734    01734    01734
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT181H FO0 CONDITIONS MAY EXIST AT SEA LEVEL FOR THIS VISUAL LOW73100
    01735    01735    01735    01735    01735    01735    01735    01735    01735    01735
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      RANGE/93M IF SO THEN ASSUME THE TRANSMITTANCE DUE TO FO0 IS GIVEN LOW73200
    01736    01736    01736    01736    01736    01736    01736    01736    01736    01736
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      'BY THE TRANSMITTANCE AT 0.95 MICRONS! LOW73300
    01737    01737    01737    01737    01737    01737    01737    01737    01737    01737
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT11/5X.2B(HESTIMATED TANGENT ALTITUDE = .F 10.3, 3M KM//) LOW73400
    01738    01738    01738    01738    01738    01738    01738    01738    01738    01738
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT15X.%INHUMATE TEMPERATURE PROFILE FOR MODEL ATMOSPHERE .15) LOW73500
    01739    01739    01739    01739    01739    01739    01739    01739    01739    01739
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT15X.%INHUMATE VAPOR PROFILE FOR MODEL ATMOSPHERE .15) LOW73600
    01740    01740    01740    01740    01740    01740    01740    01740    01740    01740
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT15X.%INHUMATE OZONE PROFILE FOR MODEL ATMOSPHERE .15) LOW73700
    01741    01741    01741    01741    01741    01741    01741    01741    01741    01741
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT1/10X.2B(H CONTINENTAL AEROSOL MODEL) LOW73800
    01742    01742    01742    01742    01742    01742    01742    01742    01742    01742
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT1/10X.2B(H RURAL AEROSOL MODEL) LOW73900
    01743    01743    01743    01743    01743    01743    01743    01743    01743    01743
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT1/10X.2B(H URBAN AEROSOL MODEL) LOW74000
    01744    01744    01744    01744    01744    01744    01744    01744    01744    01744
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT1/10X.2B(H MARITIME AEROSOL MODEL) LOW74100
    01745    01745    01745    01745    01745    01745    01745    01745    01745    01745
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      FORMAT10H 15) INPUT LEVELS EXCEEDS MODEL LIMIT OF . LOW74200
    01746    01746    01746    01746    01746    01746    01746    01746    01746    01746
    7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*   7220*
    *30      *30      *30      *30      *30      *30      *30      *30      *30      *30
    *      END

```

END OF COMPIRATION: NO DIAGNOSTICS.

NWC TM 3107

CENTRAL POINT 009403

SUBROUTINE **POINT** CENTRE POINT 800703

STORAGE USED: COOK11, 000000; DATA10, 000000; BLANK COMMON12, 000000
COMMON BLOCKS:

LOMTRN 013730
0303

EXTERNAL REFERENCES (CLOCK. NAME)	8001	8005	8009	8007
XPARA				
WHDUS				
M1023				
WF8835				

卷之三

[P.D.] 11. - 2000 - N - 101, 11) Tinted Emulsion

SUBROUTINE POINT (X,YN,N,MP,TX,IP)
 PNT00100
 PNT00200
 PNT00300
 PNT00500
 PNT00700
 PNT00900
 PNT01000
 PNT01100
 PNT01200
 PNT01300
 PNT01400
 PNT01600
 PNT01700
 PNT01800

SUBROUTINE POINT COMPUTES THE MEAN REFRACTIVE INDEX ABOVE AND
 BELOW A GIVEN ALTITUDE AND INTERPOLATES EXPONENTIALLY TO DETER-
 MINE THE EQUIVALENT ABSORBER AMOUNTS AT THAT ALTITUDE.
 X - REAL VARIABLE REPRESENTING THE ALTITUDE (KMI) (INPUT).
 YN - REAL VARIABLE REPRESENTING THE MEAN REFRACTIVITY BELOW X
 (IN-UNITS) (OUTPUT).
 N - INTEGER VARIABLE REPRESENTING THE ATMOSPHERIC LEVEL AT
 OR BELOW X (OUTPUT).
 MP - INTEGER VARIABLE (OUTPUT).
 NIP=1 IF X COINCIDES WITH Z(N).
 NIP=0 IF X DOES NOT COINCIDE WITH Z(N).
 TX - REAL VECTOR OF LENGTH 10
 TX(1-10) ARE ABSORBER AMOUNTS PER KM AT.
 TX(1-10) ARE ABSORBER AMOUNTS PER KM AT.

A horizontal row of small, dark circular marks or dots, likely representing a barcode or a series of data points.

NWC TM 3107

**END OF COMPLICATIONS,
NO DIAGNOSTICS.**

SUBROUTINE ANOL ENTRY POINT 00232
 STORAGE USED: CODE(11) 000203; DATA(0) 000204; BLANK COMMONS; 000000
 COMMON BLOCKS:
 6603 LOMTRN 019738

EXTERNAL REFERENCES (BLOCK, NAME)

STORAGE	ASSIGNMENT	1-BLOCK, TYPE, RELATIVE LOCATION, NAME
6601	POINT	000621 11L
6603	ACOS	0001 000776 12L
6605	COS	0001 000680 17L
6607	SIN	0001 001771 23L
6610	ATAN	0001 000166 'L
6611	TAN	0001 000205 SL
6612	ASIN	0001 000415 ALP
6613	AL00	0000 R 000027 BET1
6614	NWDUS	0000 R 000050 C
6615	M1028	0003 001771 C2
6616	MERR38	0003 014760 CB

STORAGE ASSIGNMENT 1-BLOCK, TYPE, RELATIVE LOCATION, NAME

STORAGE	ASSIGNMENT	1-BLOCK, TYPE, RELATIVE LOCATION, NAME
6601	POINT	0001 000776 12L
6603	ACOS	0001 000680 17L
6605	COS	0001 001203 18L
6607	SIN	0001 002117 26L
6610	ATAN	0000 000100 401F
6611	TAN	0001 000233 6L
6612	ASIN	0000 R 000021 AN0
6613	AL00	0000 R 000030 BET2
6614	NWDUS	0003 015660 CO
6615	M1028	0003 013764 C4
6616	MERR38	0000 R 000071 DB1
6617	SET	0003 R 015126 EH
6618	SET	0003 R 000060 FB
6619	SET	0003 R 002532 FO
6620	SET	0003 000000 IATM
6621	SET	0003 - 015734 IN
6622	SET	0003 015052 HL
6623	SET	0003 00001 NL
6624	SET	0003 R 015561 PI
6625	SET	0000 R 000046 RN
6626	SET	0000 R 000017 THET
6627	SET	0003 000076 TN1
6628	SET	0003 000065 TX3
6629	SET	0000 R 000034 XMIN
6630	SET	0003 R 000053 YN2
6631	SET	0000 R 000051 YH1
6632	SET	0000 R 000043 YH2
6633	SET	0000 R 000042 YH3
6634	SET	0000 R 000041 YH4
6635	SET	0000 R 000040 YH5
6636	SET	0000 R 000039 YH6
6637	SET	0000 R 000038 YH7
6638	SET	0000 R 000037 YH8
6639	SET	0000 R 000036 YH9
6640	SET	0000 R 000035 YH10
6641	SET	0000 R 000034 YH11
6642	SET	0000 R 000033 YH12
6643	SET	0000 R 000032 YH13
6644	SET	0000 R 000031 YH14
6645	SET	0000 R 000030 YH15
6646	SET	0000 R 000029 YH16
6647	SET	0000 R 000028 YH17
6648	SET	0000 R 000027 YH18
6649	SET	0000 R 000026 YH19
6650	SET	0000 R 000025 YH20

SUBROUTINE ANGL (M1,M2,ANGLE,BETA,LEN,PL)

```

C      THIS SUBROUTINE CALCULATES THE INITIAL ZENITH ANGLE TAKING INTO
C      ACCOUNT EARTH CURVATURE AND ATMOSPHERIC REFRACTION EFFECTS.
C      THE REFRACTIVE INDEX IS ASSUMED TO BE CONSTANT IN A GIVEN LAYER.
C      FOR GREATER ACCURACY INCREASE THE NUMBER OF LEVELS IN THE MODEL
C      ATMOSPHERE. THIS SUBROUTINE CAN BE REMOVED FROM THE PROGRAM
C      IF IT IS NOT NEEDED.
C
C      M1,M2 - REAL VARIABLE REPRESENTING THE ALTITUDES (KM) (INPUT).
C      ANGLE - REAL VARIABLE REPRESENTING THE ZENITH ANGLE (RADIAN)
C              (OUTPUT).
C      BETA - REAL VARIABLE REPRESENTING THE EARTH CENTER ANGLE (RADIAN)
C              (INPUT).
C      LEN - INTEGER VARIABLE REPRESENTING THE TYPE OF PATH (INPUT).
C              LEN = 0 IMPLIES THE SHORTER PATH WHERE APPLICABLE.
C              LEN = 1 IMPLIES THE LONGER PATH WHERE APPLICABLE.
C      PL - INTEGER VARIABLE REPRESENTING THE NUMBER OF LAYERS IN THE
C          ATMOSPHERE (INPUT).

C      REFERENCES - CORNETTE AND SHILANTA. NWC TM 2965
C      MODULES CALLED - POINT
C      COMMON BLOCKS USED - LOWTRN
C      REVISION DATE 19 NOVEMBER 1976
C
C      LOGICAL CKZERO
C      COMMON /LOWTRN/ IATH,ML,M21(34),M22(34),P(7,34),T(7,34),
C      M1(7,34),M2(7,34),VX(14,49),TR(67),PN(67),CI(2560),
C      C2(1575),C3(340),C4(133),CS(119),C7(14,49),CB(102),
C      EH(10,34),M,ML,M2,REE,CH,CO,P1,CA,NEARTH(7),Z(134),IM,IR
C      DIMENSION TX(10)
C
C      CKZERO(VARI)=ABS(VARI).LT.1.E-20
C
C      IP=99
C      X1=RE+M1
C      X2=RE+M2
C      LEN=0
C      BETA=BETA*CA
C      IF ((CKZERO(BETA)) .NE. ACOS(X2/X1))
C          TANO=(X2*SIN(BETA))/(X2-COS(BETA))-X1
C      THET=ATAN(TANO)
C      IF (THET.LT.0.0) THET=THET+PI
C      SPHI=SIN(THET);
C      ANG=THET/CA
C      TN=THET
C      TH=TH-0.9*CA
C      DO 101 ITER = 1,10
C
C      AN000100
C      AN000200
C      AN000300
C      AN000400
C      AN000500
C      AN000600
C      AN000700
C      AN000800
C      AN000900
C      AN001000
C      AN001100
C      AN001200
C      AN001300
C      AN001400
C      AN001500
C      AN001600
C      AN001700
C      AN001800
C      AN001900
C      AN002000
C      AN002100
C      AN002200
C      AN002300
C      AN002400
C      AN002500
C      AN002600
C      AN002700
C      AN002800
C      AN002900
C      AN003000
C      AN003100
C      AN003200
C      AN003300
C      AN003400
C      AN003500
C      AN003600
C      AN003700
C      AN003800
C      AN003900
C      AN004000
C      AN004100
C      AN004200
C      AN004300
C      AN004400
C      AN004500
C      AN004600
C      AN004700
C      AN004800
C      AN004900
C      AN005000
C      AN005100
C      AN005200
C      AN005300
C      AN005400
C      AN005500
C      AN005600
C      AN005700
C      AN005800
C      AN005900
C      AN006000
C
C      101
C
C      34

```

```

370
00131 ANGLE=THET
00132 P0T=0.0
00133 S1=0.0
00134 C1=0.0
00135 S2=0.0
00136 C2=0.0
00137 P0T2=0.0
00138 P0T3=0.0
00139 P0T4=0.0
00140 IF (BETA.LE.0.0) GO TO 2
00141 IF (2.*THET-P1.OF.1.E-9) GO TO 9
00142 IF (IP.EQ.100) GO TO 6
00143 XMIN=X2*COS(BETA)-RE
00144 IF (XMIN.LT.HI) GO TO 8
00145 IF (XMIN.GE.HI) GO TO 4
00146 HMIN=H2
00147 H2=HI
00148 H1=MMIN
00149 ANGLE=SPHI
00150 SPHI=1.0
00151 ANG=ANGLE/CA
00152 IP=100
00153 CALL POINT (HI,YN,J1,NP,TX,IP)
00154 TXI=TX(J1)
00155 CALL POINT (H2,YN,J2,NP,TX,IP)
00156 IF (NP.EQ.1) J2=J2-1
00157 IF (J1.EQ.J2) TXI=TXI+YN-EM(J1,J1)
00158 CONTINUE
00159 XI=RE+HI
00160 P0T=-TAN(THET)
00161 DU 7 J = J1,J2
00162 IF (J NE. J2) X2=RE+Z(J+1)
00163 IF (J.EQ.J2) X2=RE+H2
00164 SAL=XP(SPHI/X2
00165 ALP=ASIN(SALP)
00166 RN=EM(J+1)/EM(J,J)
00167 IF (J+1).EQ.J2) RN=YN/EM(J,J)
00168 IF (J.EQ.J1) RN=EM(J9,J+1)/TXI
00169 IF (J.J1).EQ.J2.AND.J.EQ.J1, RN=YN/TXI
00170 FBT=FB+TAN(THET)-TAN(ALP)
00171 D1=B1*THET-ALP
00172 THI=THET/CA
00173 C=ALP/CA
00174 IF (CKZERO(X2-(RE+H2))) C=PI-ALP
00175 IF ((SAL).GE.RN) RN=1.
00176 THET=ASIN(SPHI)
00177 XI=X2
00178 CONTINUE
00179 IF (BETALE.0.0) THET=C
00180 IF (BETA.LE.0.0) GO TO 28
00181 GO TO 28
00182 TANO=TANO
00183 ANGLE=PI-ANGLE
00184 TN=ANGLE
00185 ANO=ANGLE/CA

```

```

115
116 IF (MM1.LE.0.0) GO TO 3
117 CONTINUE
118 IP=101
119 CALL POINT (M1,YN1,J1,NP1,TX,IP)
120 TX1=TX(1)
121 TX1=TX(1)
122 IF (NP1.EQ.1) J1=J1-1
123 J2=ML
124 IF (M2.GE.M1) GO TO 13
125 CALL POINT (M2,YN2,J2,NP2,TX,IP)
126 TX2=TX(1)
127 IF (J1.EQ.J2) X2=RE+HE
128 IF (J1.EQ.J1) X1=RE+HE
129 IF (J1.EQ.J2) X2=RE+HE
130 SALP=XI*SPHI/X2
131 MM1=XI*SPHI-RE
132 IF (SALP.LE.-1.0) GO TO 11
133 IF (MM1.GT.M2) GO TO 10
134 ALP=ASIN(SALP)
135 THET=ASIN(SALP)
136 BET=ALP-THET
137 BET=SE1-BET
138 FB=TA(1)
139 FB=FB-TAN(THET)
140 IF (J1.NE.J1) FB=FB+FB
141 FB1=FB1+FB
142 TH1=THET/CA
143 BE=BET/CA
144 AL=AL/CA
145 IF (CKZERO(X2-RE+HE)) C=PI-ALP
146 REF=EM(9,J1)
147 IF (J1.EQ.-J1) REF=YNI
148 IF (J1.EQ.J2) REF=TX2
149 IF (J1.EQ.1) GO TO 12
150 MM1=EM(0,J1)/EM(0,J-1)
151 MM1=YNI/EM(0,J-1)
152 MM1=REF/TX2
153 IF (J1.EQ.J2+1) MM1=REF/YN2
154 IF (J1.EQ.J2) MM1=REF/YN2
155 IF (SALP.GE.RN) MM1=1.
156 SPHI=SALP*RN
157 IF (12(J1).LE.M2) GO TO 12
158 CONTINUE
159 X1=RE
160 IF (ABS(Z(J1)-M2).GE.1.0E-10.OR.J.EQ.1) GO TO 14
161 J1=J1-1
162 X1=RE+Z(J1)
163 IF (J1.EQ.J1) X1=RE+HE
164 IF (J1.EQ.J2) X1=RE+HE
165 MM1=XI*SPH-RE
166 IF (MM1.LE.0.0) BI=BETI
167 IF (MM1.LE.0.0) LEN=0
168 IF (MM1.LE.0.0) FBT=FB1
169 IF (MM1.LE.0.0) FB=FB1
170 IF (MM1.LE.0.0) GO TO 26

```

```

171*      IF (Z(J)).LT.HMINI GO TO 10
172*      REF=EM10,J1
173*      IF (J.EQ.J2) REF=YN
174*      SAL=XP1*SAL1/X2
175*      ALP=ASIN(SALP)
176*      THET=ASIN(SPH1)
177*      BET=ALP-THET
178*      FB=TAN(ALP)-TAN(THET)
179*      FBZ2=F012+FB
180*      BET2=BET2+BET
181*      BRIN=BET1+BET2
182*      AL=ALP/CA
183*      TH1=THE1/CA
184*      RN=REF/EM10,J-1)
185*      IF (SALP.GE.RN) RN=1.0
186*      SPHI=SALP*RN
187*      GO TO 13
188*      TX3=YH1+TX1(B1)-EM10,J1)
189*      YH1=X3
190*      IF (ABS(HM2-2*(J+1)).LE.1.0E-9) YH1=TX1(B1)
191*      IF (ABS(HM1-2*(J+1)).LE.1.0E-9) YH1=TX1(B1)
192*      GO TO 19
193*      IP=102
194*      CALL POINT (HM1N,YH1,J2,NP,TX,IP)
195*      TX3=TX1(B1)
196*      IF (J.EQ.J1.AND.HM2.GE.M1) GO TO 17
197*      IF (J.EQ.J1.OR.J.EQ.J2) TX3=YH2+TX1(B1)-EM10,J1)
198*      IF (HM1N.GT.M2) TX3=TX1(B1)
199*      JF (J.EQ.J1.AND.HMIN.GT.M2) GO TO 17
200*      RN=REF/TX3
201*      IF (SALP.GE.RN) RN=1.
202*      SPHI=SALP*RN
203*      X1=SPHI-RE
204*      DIF=ABS(HMIN-X1)
205*      HMIN=X
206*      IF (DIF.GT.1.0E-9) GO TO 18
207*      X2=RE+MMIN
208*      MMIN=X
209*      IF (CKZERO(RNN)) FBT3=-TAN(THET)
210*      IF (CKZERO(RNN)) GO TO 20
211*      ONK=(TX3-1.0)*ALOG((TX3-1.0)/(REF-1.0)+(X2-X1))
212*      FBT3=-TAN(THET)*(1.0-1.0/(1.0+TX3/X2+DNX1))
213*      BET=0.5*PI-TMET
214*      BET1=GET1-BET
215*      GET2=GET2+GET
216*      BRIN=GET1+BET2
217*      IF (HM2.GE.M1) GO TO 23
218*      BET=GET1+2.*BET2
219*      GO TO 20
220*      003=ABS(SIGNIN-BETA1)
221*      002=BE1-CETA
222*      001=BE1A-BET1
223*      IF ((DB3.GT.0.01.OR.DB3.GE.0.02).AND.002.GT.0.001) B1=BET1
224*      IF ((DB3.GT.0.01.OR.DB3.GE.0.02).AND.002.LT.0.001) LENO
225*      IF ((DB3.GT.0.01.OR.DB3.GE.0.02).AND.002.GT.0.001) FBT=FBT1
226*      IF ((DB3.GT.0.01.OR.DB3.GE.0.02).AND.002.LT.0.001) DB2.GT.0.001
227*      IF ((DB3.LE.0.01.OR.DB2.LE.0.01).AND.003.LE.0.01) B1=BET1+BET2
228*      IF ((DB3.LE.0.01.OR.DB2.LE.0.01).AND.003.LE.0.01) FBT=FBT1+FBT2+
229*      FBT3
230*      GO TO 20
231*      003=ABS(SIGNIN-BETA1)
232*      002=BE1-CETA
233*      001=BE1A-BET1
234*      IF ((DB3.GT.0.01.OR.DB3.GE.0.02).AND.002.GT.0.001) B1=BET1
235*      IF ((DB3.GT.0.01.OR.DB3.GE.0.02).AND.002.LT.0.001) LENO
236*      IF ((DB3.GT.0.01.OR.DB3.GE.0.02).AND.002.GT.0.001) FBT=FBT1
237*      IF ((DB3.GT.0.01.OR.DB2.LE.0.01).AND.003.LE.0.01) B1=BET1+BET2
238*      IF ((DB3.LE.0.01.OR.DB2.LE.0.01).AND.003.LE.0.01) FBT=FBT1+FBT2+
239*      FBT3
240*      GO TO 20

```

NWC TM 3107

```

IF (DB3 .NE. DB2 .AND. DB2 .LE. DB1) D1=DET
IF (DB3 .NE. DB2 .AND. DB2 .LE. DB1) LEN=1
IF (DB3 .NE. DB2 .AND. DB2 .LE. DB1) FST=FST1+2.0*(FST2+FST3)
00 TO 26
B1=2.0*BET1+8C71
LEN=1
FST=2.0*(FST1+FST2+FST3)
WRITE(1M,401) J,B1,FST,FST1,FST2,FST3,TX1,YN1
IF (CKZERO(M2-M1)) GO TO 28
J=103
IF (INP1.EQ.11) J1=J1+1
SPHI=SPH1*ANOLE
IF ((Z1(J+1)).LE.M2) CALL POINTINT2,YN,M,NP,TX,IP1
IF ((Z1(J+1)).LE.M2) J2=J1+1
RN=TX1/FTH1
IF (SPHI.OE.RN) RN=1.
IF (SPHI-SPH1/RN) RN=1.
SPHI=SPH1/RN
THET=ASIN(SPHI)
00 TO 5
THET-ANGLE*(BETA-B1)/(1.+FST/TANB)
051-01/CA
B-BET1/CA
TH1=THET/CA
MR1=THET1A(.404) B1=0.08*FST1 TH1I=TANO
IF (THET1I.OV.) THET1I=0.0
THE1=THET1/CA
MR1=THET1A(.404) BET1I=0.0*FST1
THE1=THET1/CA
MR1=THET1A(.405) TH1I=TH1I
SPHI=SPH1*(THET1)
TANG=TAN(THET1)
IF ((A3$BETA-B1).LT.1.1.E-7.OR.ABS(Angle-THE1).LT.1.E-7) GO TO 28
CONTINUE
THET=ANGLE*THET1/2.
28 ANGLE=THET/CA
IF ((BETA.LE.0.01) MI=H2
WRITE(1M,.001) ANOLE,ITER
RETURN

C
401 FORMAT (10,IPE16.7,0.0PF13.0)
404 FORMAT (14H TOTAL BETA = ,IPE14.8,0PF19.8,7H FST = ,IPE14.8,0H
        *ET = ,0PF14.6,8H TANO = ,F10.8,15H TOTAL RANGE = ,F10.11
        405 FORMAT (SF12.6)
406 FORMAT (8X/15HZEMITH ANGLE = ,F7.3,93H DEGREES - RECOMPUTED FROM SIAN
        407 FORMAT (14H LITERATION,13,1H)
END

```

END OF COMPILATION!

NO DIAGNOSTICS.

NWC TM 3107

```

***** OUTPUT DEVICE NUMBER
C   DATA      IN /8/
C
C   *** THE VALUE FOR PI
C   DATA      PI /3.14159265358979/
C
C   *** THE CONVERSION FROM DEGREES TO RADIANS.
C   DATA      CA /0.017453292519943/
C
C   *** THE MEAN RADIUS OF THE EARTH (INTERNATIONAL SPHEROID) IN KM.
C   DATA      REBAR /6371.289315/
C
C   *** THE POLAR RADIUS OF THE EARTH (INTERNATIONAL SPHEROID) IN KM.
C   DATA      REPOL /6356.911948/
C
C   *** THE EQUATORIAL RADIUS OF THE EARTH (INTERNATIONAL SPHEROID) IN KM.
C   DATA      REEQU /6378.388000/
C
C   *** VALUES OF THE RADIUS OF THE EARTH FOR THE MODEL ATMOSPHERES IN KM.
C   DATA      REARTH(1) /6376.951637/
C   DATA      REARTH(2) /6367.659029/
C   DATA      REARTH(3) /6387.659029/
C   DATA      REARTH(4) /6362.287754/
C   DATA      REARTH(5) /6362.287754/
C   DATA      REARTH(6) /6367.659029/
C   DATA      REARTH(7) /6371.299315/
C
C   *** NUMBER OF TYPES OF MODEL ATMOSPHERES
C   DATA      IATH /8/
C
C   *** NUMBER OF LEVELS IN MODEL ATMOSPHERE DATA
C   DATA      NL /30/
C
C   *** HAZE MODEL: 23 KM. VISIBLE RANGE
C
C   DATA      M21 /2.830E+03 1.293E+03 5.373E+02 2.297E+02
C   DATA      1.193E+02 0.892E+01 0.341E+01 0.893E+01 0.6073E+01 0.5822E+01
C   DATA      0.5.879E+01 0.5.320E+01 0.5.589E+01 0.5.159E+01 0.5.032E+01 0.4.747E+01
C   DATA      0.4.514E+01 0.4.460E+01 0.4.317E+01 0.2.689E+01 0.1.689E+01 0.1.935E+01
C   DATA      0.1.456E+01 0.1.114E+01 0.0.831E+00 0.7.343E+00 0.2.239E+00 0.0.893E+01
C   DATA      0.1.351E-01 0.1.079E-02 0.5.553E-05 0.1.970E-08 0.0.000E+00/
C
C   *** HAZE MODEL: 5 KM. VISIBLE RANGE
C
C   DATA      M22 /1.379E+04 0.334E+03 1.845E+03 0.3.735E+02
C   DATA      0.2.454E+02 0.892E+01 0.341E+01 0.893E+01 0.6.073E+01 0.5.822E+01

```

00137 00* * 5.679E+01 5.320E+01 5.589E+01 5.159E+01 5.552E+01 5.797E+01. DAT0800
 00137 00* * 4.514E+01 4.00E+01 4.317E+01 4.317E+01 4.336E+01 4.193E+01. DAT0900
 00137 01* * 4.456E+01 4.00E+01 4.317E+01 4.317E+01 4.336E+01 4.193E+01. DAT0910
 00137 02* * 1.951E-01 4.00E+01 4.14E+01 4.831E+00 7.434E+00 2.299E+00 5.892E+01. DAT0920
 00137 03* * 0.000E+00 4.00E+01 4.00E+01 4.00E+01 4.00E+01 4.00E+00 0.000E+00. DAT0930
 C ALTITUDE (KM.) AT LEVEL I
 00137 94* C DATA 20 / 0.0 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0. DAT0940
 00137 95* C DATA 9.0 10.0 11.0 12.0 13.0 14.0 15.0 16.0 17.0 18.0. DAT0950
 00137 96* C DATA 21.0 22.0 23.0 24.0 25.0 26.0 27.0 28.0 29.0 30.0. DAT0960
 00137 97* C DATA 100.0 9999.0 / DAT0970
 00137 98* C C *** PRESSURE (MB.) AT LEVEL I FOR THE MODEL ATMOSPHERES
 00137 99* C C ***
 00137 100* C DATA 7.150E+02 6.330E+02 5.590E+02 4.920E+02 4.320E+02 3.780E+02. DAT1000
 00137 101* C DATA 3.290E+02 2.860E+02 2.470E+02 2.130E+02 1.820E+02 1.580E+02. DAT1010
 00137 102* C DATA 1.320E+02 1.110E+02 9.370E+01 7.890E+01 6.660E+01 5.650E+01. DAT1020
 00137 103* C DATA 4.800E+01 4.090E+01 3.500E+01 3.000E+01 2.570E+01 2.220E+01. DAT1030
 00137 104* C DATA 0.000E+00 3.050E+00 1.590E+00 8.540E-01 3.790E-02 3.000E-04. DAT1040
 00137 105* C DATA 0.000E+00 / DAT1050
 00137 106* C DATA 7.100E+02 6.280E+02 5.540E+02 4.870E+02 4.260E+02 3.720E+02. DAT1060
 00137 107* C DATA 3.240E+02 2.810E+02 2.430E+02 2.090E+02 1.790E+02 1.530E+02. DAT1070
 00137 108* C DATA 1.300E+02 1.100E+02 9.500E+01 7.920E+01 6.930E+01 5.950E+01. DAT1080
 00137 109* C DATA 4.900E+01 4.370E+01 3.330E+00 1.760E+00 9.510E-01 6.710E-02 3.000E-04. DAT1090
 00137 110* C DATA 0.000E+00 / DAT1100
 00137 111* C DATA 7.040E+02 6.081E+02 5.313E+02 4.627E+02 4.016E+02 3.473E+02. DAT1110
 00137 112* C DATA 3.200E+02 2.568E+02 2.199E+02 1.882E+02 1.610E+02 1.378E+02. DAT1120
 00137 113* C DATA 1.250E+02 1.007E+02 8.610E+01 7.350E+01 6.280E+01 5.370E+01. DAT1130
 00137 114* C DATA 4.580E+01 3.910E+01 3.340E+01 2.880E+01 2.430E+01 2.110E+01. DAT1140
 00137 115* C DATA 1.180E+00 2.530E+00 1.290E+00 6.820E-01 4.670E-02 3.000E-04. DAT1150
 00137 116* C DATA 0.000E+00 / DAT1160
 00137 117* C DATA 7.000E+02 6.081E+02 5.313E+02 4.627E+02 4.016E+02 3.473E+02. DAT1170
 00137 118* C DATA 3.107E+02 2.677E+02 2.300E+02 1.977E+02 1.700E+02 1.460E+02. DAT1180
 00137 119* C DATA 1.250E+02 1.007E+02 8.610E+01 7.350E+01 6.280E+01 5.370E+01. DAT1190
 00137 120* C DATA 4.580E+01 3.910E+01 3.340E+01 2.880E+01 2.430E+01 2.110E+01. DAT1200
 00137 121* C DATA 1.180E+00 2.530E+00 1.290E+00 6.820E-01 4.670E-02 3.000E-04. DAT1210
 00137 122* C DATA 0.000E+00 / DAT1220
 00137 123* C DATA 7.000E+02 6.081E+02 5.313E+02 4.627E+02 4.016E+02 3.473E+02. DAT1230
 00137 124* C DATA 3.107E+02 2.677E+02 2.300E+02 1.977E+02 1.700E+02 1.460E+02. DAT1240
 00137 125* C DATA 1.250E+02 1.007E+02 8.610E+01 7.350E+01 6.280E+01 5.370E+01. DAT1250
 00137 126* C DATA 4.580E+01 3.910E+01 3.340E+01 2.880E+01 2.430E+01 2.110E+01. DAT1260
 00137 127* C DATA 1.180E+00 2.530E+00 1.290E+00 6.820E-01 4.670E-02 3.000E-04. DAT1270
 00137 128* C DATA 0.000E+00 / DAT1280
 00137 129* C DATA 7.000E+02 6.081E+02 5.313E+02 4.627E+02 4.016E+02 3.473E+02. DAT1290
 00137 130* C DATA 3.107E+02 2.677E+02 2.300E+02 1.977E+02 1.700E+02 1.460E+02. DAT1300
 00137 131* C DATA 1.250E+02 1.007E+02 8.610E+01 7.350E+01 6.280E+01 5.370E+01. DAT1310
 00137 132* C DATA 4.580E+01 3.910E+01 3.340E+01 2.880E+01 2.430E+01 2.110E+01. DAT1320
 00137 133* C DATA 1.180E+00 2.530E+00 1.290E+00 6.820E-01 4.670E-02 3.000E-04. DAT1330
 00137 134* C DATA 0.000E+00 / DAT1340
 00137 135* C DATA 7.012E+02 6.168E+02 5.405E+02 4.722E+02 4.111E+02 3.585E+02. DAT1350
 00137 136* C DATA 3.080E+02 2.850E+02 2.087E+02 1.977E+02 1.510E+02 1.291E+02. DAT1360
 00137 137* C DATA 1.211E+02 1.035E+02 8.650E+01 7.350E+01 6.280E+01 5.370E+01. DAT1370
 00137 138* C DATA 4.729E+01 4.047E+01 3.467E+01 3.109E+01 2.845E+01 2.548E+01. DAT1380
 00137 139* C DATA 9.765E+00 2.871E+00 1.491E+00 7.978E-01 5.920E-02 3.008E-04. DAT1390
 00137 140* C DATA 0.000E+00 / DAT1400
 00137 141* C DATA 7.012E+02 6.168E+02 5.405E+02 4.722E+02 4.111E+02 3.585E+02. DAT1410
 00137 142* C DATA 3.080E+02 2.850E+02 2.087E+02 1.977E+02 1.510E+02 1.291E+02. DAT1420
 00137 143* C DATA 1.211E+02 1.035E+02 8.650E+01 7.350E+01 6.280E+01 5.370E+01. DAT1430
 00137 144* C DATA 4.729E+01 4.047E+01 3.467E+01 3.109E+01 2.845E+01 2.548E+01. DAT1440
 00137 145* C DATA 9.765E+00 2.871E+00 1.491E+00 7.978E-01 5.920E-02 3.008E-04. DAT1450

C *** TEMPERATURE (K) AT LEVEL 1 FOR THE MODEL ATMOSPHERES
 C DATA (T(1,1), I=1,3W) / 300.0, 294.0, 288.0, 287.0, 277.0,
 C DAT14700
 C DAT14800
 C DAT14900
 C DAT15000
 C DAT15100
 C DAT15200
 C DAT15300
 C DAT15400
 C DAT15500
 C DAT15600
 C DAT15700
 C DAT15800
 C DAT15900
 C DAT16000
 C DAT16100
 C DAT16200
 C DAT16300
 C DAT16400
 C DAT16500
 C DAT16600
 C DAT16700
 C DAT16800
 C DAT16900
 C DAT17000
 C DAT17100
 C DAT17200
 C *** WATER VAPOR DENSITY (GM.M-3) AT LEVEL 1 FOR THE MODEL ATMOSPHERES
 C DATA (WM(1,1), I=1,3W) / 1.9E+01, 1.3E+01, 9.3E+00,
 C DAT17300
 C DAT17400
 C DAT17500
 C DAT17600
 C DAT17700
 C DAT17800
 C DAT17900
 C DAT18000
 C DAT18100
 C DAT18200
 C DAT18300
 C DAT18400
 C DAT18500
 C DAT18600
 C DAT18700
 C DAT18800
 C DAT18900
 C DAT19000
 C DAT19100
 C DAT19200
 C DAT19300
 C DAT19400
 C DAT19500
 C DAT19600
 C DAT19700
 C DAT19800
 C DAT19900
 C DAT20000
 C DAT20100
 C DAT20200
 C DAT20300
 C DAT20400
 C DAT20500

NWC TM 3107

• 6.0E-04 8.7E-04 3.8E-04 1.1E-04 4.3E-05 1.8E-05 6.3E-06.

• 1.4E-07 1.0E-09 0.0E+00 / 1.0E+00 0.0E+00 / 1.0E+00 0.0E+00 /

• DATA (MH(6,1,1=1,3)= / 9.9E+00 4.2E+00 2.8E+00 5.4E+05.

• 1.8E+00 1.1E+00 0.6E+01 3.8E+01 0.12 1E-01 1.2E-01 4.8E-01.

• 1.8E-02 0.2E-03 3.7E-03 1.8E-03 0.4E-04 7.2E-04 6.1E-04.

• 5.2E-04 3.E-04 4.4E-04 4.4E-04 4.4E-04 5.2E-04 5.7E-04.

• 6.1E-04 0.6E-04 3.8E-04 1.6E-04 1.6E-04 6.7E-05 1.2E-05.

• 1.3E-07 1.1E-09 0.0E+00 /

DATA20300

DATA20400

DATA20500

DATA20600

DATA20700

DATA20800

DATA20900

DATA21000

DATA21100

DATA21200

DATA21300

DATA21400

DATA21500

DATA21600

DATA21700

DATA21800

DATA21900

DATA22000

DATA22100

DATA22200

DATA22300

DATA22400

DATA22500

DATA22600

DATA22700

DATA22800

DATA22900

DATA23000

DATA23100

DATA23200

DATA23300

DATA23400

DATA23500

DATA23600

DATA23700

DATA23800

DATA23900

DATA24000

DATA24100

DATA24200

DATA24300

DATA24400

DATA24500

DATA24600

DATA24700

DATA24800

DATA24900

DATA25000

DATA25100

DATA25200

DATA25300

DATA25400

DATA25500

DATA25600

DATA25700

DATA25800

DATA25900

DATA26000

DATA26100

DATA26200

DATA26300

DATA26400

DATA26500

DATA26600

DATA26700

DATA26800

DATA26900

DATA27000

DATA27100

DATA27200

DATA27300

DATA27400

DATA27500

DATA27600

DATA27700

DATA27800

DATA27900

DATA28000

DATA28100

DATA28200

DATA28300

DATA28400

DATA28500

DATA28600

DATA28700

DATA28800

DATA28900

DATA29000

DATA29100

DATA29200

DATA29300

DATA29400

DATA29500

DATA29600

DATA29700

DATA29800

DATA29900

DATA20000

C *** OZONE DENSITY (GM.M-3) AT LEVEL 1 FOR THE MODEL ATMOSPHERES

DATA (M0(1,1,1=1,3)= / 9.9E+00 4.2E+00 2.8E+00 5.4E+05.

• 9.1E-05 1.7E-05 4.3E-05 4.3E-05 3.9E-05 4.3E-05 3.9E-05.

• 3.9E-05 4.1E-05 4.3E-05 4.3E-05 4.3E-05 4.3E-05 4.3E-05.

• 6.9E-05 9.0E-05 1.4E-04 1.8E-04 2.4E-04 2.8E-04 3.2E-04.

• 3.4E-04 3.4E-04 2.4E-04 2.4E-04 2.4E-04 2.4E-04 2.4E-04.

• 0.6E+00 4.3E-11 0.0E+00 /

DATA (M0(2,1,1=1,3)= / 9.9E+00 5.6E+00 6.0E+00 6.0E+00.

• 6.2E-05 6.6E-05 6.9E-05 7.5E-05 7.9E-05 8.6E-05.

• 2.4E-04 2.6E-04 3.2E-04 3.4E-04 3.6E-04 3.8E-04 3.9E-04.

• 3.2E-04 3.0E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(3,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(4,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(5,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(6,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(7,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(8,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(9,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(10,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(11,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(12,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(13,1,1=1,3)= / 9.9E+00 5.6E+00 5.6E+00 5.6E+00.

• 5.6E-05 5.9E-05 6.2E-05 6.5E-05 6.8E-05 7.1E-05.

• 1.6E-04 2.1E-04 2.6E-04 3.0E-04 3.2E-04 3.4E-04 3.6E-04.

• 3.8E-04 4.1E-04 4.3E-04 4.5E-04 4.7E-04 4.9E-04 5.1E-04.

• 3.6E-04 3.4E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04 2.6E-04.

• 0.6E-05 4.3E-11 0.0E+00 /

DATA (M0(14,1,1=1,3)= / 9.9E+00 5.6E

NWC TM 3107

NWC TM 3107

NWC TM 3107

NWC TM 3107

SPECTRAL DATA: UNIFORMLY MIXED GASES

DATA	(C2(1), I=1-180)
-4.25	-3.70
-3.20	-2.75
-1.90	-1.73
-1.51	-1.29
-1.11	-0.81
-0.51	-0.51
-0.30	-0.30
-0.60	-0.22
-0.49	-0.49
-0.76	-0.76
-1.26	-1.26
-1.56	-1.56
-1.20	-1.20
-1.00	-1.00
-1.90	-1.90
-3.12	-3.12
-3.37	-3.37
-1.76	-1.76
-1.81	-1.81
-2.08	-2.08
-2.23	-2.23
-2.36	-2.36
-2.56	-2.56
-2.71	-2.71
-2.72	-2.72
-2.90	-2.90
-3.12	-3.12
-3.18	-3.18
-3.56	-3.56
-3.66	-3.66
-3.86	-3.86
-3.96	-3.96
-3.99	-3.99
-3.99	-3.99
-2.52	-2.52
-2.52	-2.52
-2.73	-2.73
-2.86	-2.86
-2.01	-2.01
-2.17	-2.17
-1.77	-1.77
-1.63	-1.63
-1.47	-1.47

NWC TM 3107

NWC TM 3107

NWC TM 3107

SPECTRAL DATA: OZONE

C *** SPECTRAL DATA: N2 CONTINUUM

0.01719 0.01690 0.01577 0.01500 0.01454 0.01367 0.01341.
 0.01269 0.01250 0.01235 0.01231 0.01237 0.01232 0.01233
 0.01249 0.01193 /

 C *** MARITIME AEROSOL MODEL
 C DATA (C7A11,1,-1,-1,-1)
 C /0.19376 0.18391 0.17637 0.16815 0.16065 0.15800 0.15278.
 C 0.14855 0.14497 0.13915 0.12825 0.11962 0.11160.
 C 0.10644 0.09893 0.09340 0.07573 0.06413 0.05932 0.05191.
 C 0.04383 0.02239 0.00316 0.00619 0.00456 0.00282 C.03871.
 C 0.03584 0.03344 0.02466 0.02729 0.02819 0.03378 0.03677.
 C 0.04014 0.04205 0.03368 0.04295 0.04291 0.03525.
 C 0.03166 0.02641 /

 C *** SPECTRAL DATA: AEROSOL ABSORPTION
 C *** AVERAGE CONTINENTAL AEROSOL MODEL
 C DATA (C7A11,1,-1,-1,-1)
 C /0.09530 0.09560 0.09580 0.09600 0.09610 0.09610.
 C 0.09814 0.10120 0.10480 0.10920 0.10348 0.10369 0.10369.
 C 0.00487 0.00232 0.00222 0.00171 0.00143 0.00154 0.00148.
 C 0.00295 0.00360 0.00423 0.00620 0.00504 0.00702 0.01160.
 C 0.01180 0.01310 0.01430 0.00937 0.00698 0.00549 0.00439.
 C 0.00366 0.00464 0.00691 0.00607 0.00506 0.00507 0.00565.
 C 0.00562 0.00561 /

 C *** RURAL AEROSOL MODEL
 C DATA (C7A12,11,-1,-1,-1)
 C /0.07845 0.03681 0.02110 0.01317 0.01114 0.01095 0.00966.
 C 0.01050 0.00750 0.00933 0.00750 0.00437 0.00493 0.00568.
 C 0.00250 0.00214 0.00232 0.00321 0.00388 0.00462 0.00749.
 C 0.00617 0.00807 0.01254 0.01128 0.01209 0.01378 0.0005.
 C 0.00832 0.00810 0.00860 0.00570 0.00535 0.00516 0.00523.
 C 0.00538 0.00834 0.00696 0.00767 0.00767 0.00767 0.00767.
 C 0.00749 0.00761 /

 C *** URBAN AEROSOL MODEL
 C DATA (C7A13,11,-1,-1,-1)
 C /0.08805 0.05331 0.03938 0.03011 0.02640 0.02498 0.02160.
 C 0.02050 0.01905 0.01948 0.01272 0.00999 0.00920 0.00917.
 C 0.00622 0.00589 0.00563 0.00575 0.00608 0.00649 0.00654.
 C 0.00729 0.00834 0.01253 0.01141 0.01207 0.01344 0.01028.
 C 0.00879 0.00858 0.00743 0.00616 0.00612 0.00587 0.00589.
 C 0.00595 0.00837 0.00714 0.00770 0.00689 0.00759 0.00751.
 C 0.00729 0.00730 /

 C *** MARITIME AEROSOL MODEL
 C DATA (C7A14,11,-1,-1,-1)
 C /0.01667 0.00710 0.00383 0.00223 0.00183 0.00178 0.00193.
 C 0.00169 0.00191 0.00200 0.00161 0.00243 0.00369 0.00619.
 C 0.00711 0.00298 0.00374 0.00629 0.00551 0.02321 0.01019.
 C 0.00893 0.01071 0.01190 0.01202 0.01218 0.01216 0.01098.

0.01072, 0.01073, 0.01108, 0.01144, 0.01178, 0.02531, 0.02765,
 0.03035, 0.03198, 0.03195, 0.03196, 0.02976, 0.02734, 0.02462,
 0.02218, 0.01915/

C *** SPECTRAL DATA: OZONE - UV AND VISIBLE
 C DATA CB / 9, 30E-03, 8, 00E-03, 1, 07E-02, 1, 10E-02, 1, 27E-02, DAT94400
 C DAT94500
 C DAT94600
 C DAT94700
 C DAT94800
 C DAT94900
 C DAT95000
 C DAT95100
 C DAT95200
 C DAT95300
 C DAT95400
 C DAT95500
 C DAT95600
 C DAT95700
 C DAT95800
 C DAT95900
 C DAT96000
 C DAT96100
 C DAT96200
 C DAT96300
 C DAT96400
 C DAT96500

1.71E-02, 2.00E-02, 2.75E-02, 3.07E-02, 3.84E-02, 4.78E-02, 5.87E-02, DAT95000
 6.54E-02, 7.62E-02, 9.15E-02, 1.00E-01, 1.09E-01, 1.20E-01, 1.28E-01, DAT95100
 1.12E-01, 1.11E-01, 1.16E-01, 1.19E-01, 1.23E-01, 1.26E-02, 1.30E-02, DAT95200
 3.82E-02, 2.94E-02, 2.98E-02, 1.98E-02, 1.86E-02, 1.81E-02, 1.68E-02, DAT95300
 9.24E-02, 8.28E-02, 7.97E-02, 7.07E-02, 6.98E-02, 6.56E-02, 4.77E-02, DAT95400
 1.17E-02, 7.70E-03, 6.10E-03, 8.30E-03, 8.10E-03, 3.70E-03, 3.20E-03, DAT95500
 3.10E-03, 2.95E-03, 1.98E-03, 1.40E-03, 8.25E-04, 2.50E-04, 0.00E-04, DAT95600
 0.00E-04, 0.00E-04, 5.65E-04, 2.00E-03, 7.35E-03, 2.03E-02, 0.98E-02, DAT95700
 1.19E-01, 2.46E-01, 3.18E-01, 1.02E-00, 1.95E-00, 3.79E-00, 6.65E-00, DAT95800
 1.24E-01, 2.20E-01, 3.67E-01, 5.93E-01, 8.50E-01, 1.26E-02, 1.68E-02, DAT95900
 2.06E+02, 2.42E+02, 2.71E+02, 2.91E+02, 3.02E+02, 3.03E+02, 3.04E+02, DAT96000
 2.77E+02, 2.54E+02, 2.26E+02, 1.96E+02, 1.68E+02, 1.44E+02, 1.17E+02, DAT96100
 9.75E+01, 7.65E+01, 1.0NE+01, 9.62E+01, 3.46E+01, 2.52E+01, 0.00E+01, DAT96200
 1.57E+01, 1.20E+01, 1.00E+01, 8.00E+00, 6.30E+00, 4.80E+00, DAT96300
 0.00E+00, 0.00E+00, 0.00E+00, 0.00E+00, 0.00E+00, DAT96400
 0.00E+00, 0.00E+00, 0.00E+00, 0.00E+00, 0.00E+00, DAT96500

END OF COMPILED: NO DIAGNOSTICS.

IN LONTRAN.MAIN
IN LONTRAN.BLOCKDATA
LIB LONTRAN.
END

ADDRESS LIMITS 001000 085015
000000 0E4136
STARTING ADDRESS 015554

SEGMENT SHAING	001000 025014	040000 064136
NSWTC5/FOR59		
NMBLK5/FOR59		
NIRHDS/FOR59		
NHDFS/FOR59		
NBDC15/FOR59		
NFTCH5/FOR59		
NFTVS/FOR59		
NCNTS/FOR59		
NCLOSS/FOR59		
NHBLK8/FOR59		
NGS12/FOR59		
NUPDAS/FOR59		
NWF03/FOR59		
NIGERS/FOR59		
NOTINS/FOR59A		
NINIMS/FOR59A		
NINPTS/FOR59A		
NFHTS/FOR59		
NFCMS/FOR59A		
NTARS/FOR59A		
TAN OTANS/FOR59		
ALDS/FOR59		
ATANS/FOR59		
ASINCOS/FOR59.		
SQRT8/FOR59		
SINCOS3/FOR59		
EING/FOR59		
NEXPBS/FOR59		
NETOPS/FOR59A		
NOUFS/FOR59A		
NIEHS/FOR59		
NIBUFFS/FOR59		
GOMAC (COMMONBLOCK)		
MINTAS/FOR59A		
POINT		
LONTRAN		

NWC TM 3107

gross earnings. Level 72-0

MAJOR SYMBOLS AND DEFINITIONS

AB	Absorption at frequency V; also average transmittance
AHZ1, AHZ2	Aerosol number density
AJ	Equivalent absorber amount per km at level J
ALP	Angle of arrival at adjacent level
ANGLE	Input zenith angle (degrees)
BET	Angle subtended at the earth's center as path traverses adjacent levels
BETA	Total angle subtended by path at earth's center
BJ	Equivalent absorber amount per km at level J + 1
CA	Conversion factor from degrees to radians
CO	Wavelength dependent coefficient used in refractive index expression
CW	Wavelength dependent coefficient used in refractive index expression
C1	Log absorption coefficient for water vapor
C2	Log absorption coefficient for uniformly mixed gases
C3	Log absorption coefficient for ozone
C4	Absorption coefficient for nitrogen ($\sim 4\mu\text{m}$)
C5	Absorption coefficient for water vapor continuum ($\sim 4\mu\text{m}$)
C6	Extinction coefficient for molecular scattering
C7	Extinction coefficient for aerosol models
C7A	Aerosol absorption coefficient
C8	Absorption coefficient for ozone (UV and visible regions)
D	Water vapor amount (pr. cm/km) at level I
DP	Dew point temperature ($^{\circ}\text{C}$)
DS	Path length from level I to Level I + 1
DV	Wavenumber increment at which transmittance is calculated
DZ	Height increment from level I to level I + 1
E(K)	Equivalent absorber amounts per km at height H1
EH(1,I)	Equivalent absorber amount per km for water vapor at level Z(I)
EH(2,I)	Equivalent absorber amount per km for carbon dioxide, etc. at level Z(I)
EH(3,I)	Equivalent absorber amount per km for ozone at level Z(I)
EH(4,I)	Equivalent absorber amount per km for nitrogen at level Z(I)
EH(5,I)	Equivalent absorber amount per km for water vapor continuum at level Z(I)
EH(6,I)	Equivalent absorber amount per km for molecular scattering at level Z(I)
EH(7,I)	Equivalent absorber amount per km for aerosol extinction at level Z(I)
EH(8,I)	Equivalent absorber amount per km for ozone (UV and visible) at level Z(I)
EH(9,I)	Mean refractive index of layer above level Z(I)

NWC TM 3107

EV	Integrated absorber amount from level I to level I+1
FAC	Factor for exponential and linear interpolation
FO	Transmission function logarithmic absorber amount scale for ozone
FW	Transmission function logarithmic absorber amount scale for water vapor and the uniformly mixed gases
H	Altitude (km)
H1	Initial altitude (km)
H2	Final altitude (km)
HAZE	Aerosol number density (no. cm^{-3})
HM	Estimated tangent height (km)
HMIN	Minimum altitude of path trajectory (km)
HZ1	Aerosol number density (no. cm^{-3}), for 23 km visual range
HZ2	Aerosol number density (no. cm^{-3}) for 5 km visual range
I	Running integer used as altitude (level) indicator
IAERO	Indicator for type of aerosol model
IATM	Number of levels in model atmosphere
IDV	Frequency increment (cm^{-1})
IFIND	Indicator for using subroutine ANGL
IHAZE	Aerosol model indicator
IM	Parameter used when reading in a new atmospheric model
IP	Indicator for using subroutine POINT to calculate refractive index only (IP = 0) or equivalent absorber amounts also (IP ≠ 0).
IR	Card printer number
ITER, ITES	Iteration counters
ITYPE	Indicator for type of atmospheric path
IV	Frequency at which transmittance is calculated
IV1	Starting frequency
IV2	Last frequency
IW	Line printer number
IXY	Parameter for terminating program and cycling indicator
J	Running integer for altitude identification
JMIN	Altitude indicator for minimum height of path
JP	Print option parameter
J1	Level indicator for altitude H1
J2	Level indicator for altitude H2
K	Absorber indicator, K = 1, 2, 3, etc., corresponds to water vapor, uniformly mixed gases, ozone, etc., respectively
K2	Cycling parameter for downward looking paths
L	Frequency indicator for ozone transmittance calculation
LEN	Parameter used for defining longest of two paths
M	Integer used to identify required model atmosphere
ML	Number of levels in radiosonde data input (MODEL - 7)
MODEL	Integer used to identify required model atmosphere

NWC TM 3107

M1	Integer for selecting temperature altitude profile for (M=M1)
M2	Integer for selecting water vapor altitude profile for (M=M2)
M3	Integer for selecting ozone altitude profile for (M=M3)
N	Indicator for level below given input altitude used in POINT subroutine
NL,NLP	Number of levels in model atmosphere data
NP	Indicator for determining whether H1 or H2 coincide with levels in the model atmosphere
NP1	Value of NP for altitude H1
NP2	Value of NP for altitude H2
NS1,NS2,NS3	Counters corresponding to WS1, WS2, WS3
P(M,I)	Pressure (mb) at level I for model atmosphere M
PHI	Angle of arrival at H2
PI	3.141592654, that is π
PPW	Partial pressure of water vapor (in atmospheres)
PS	Total pressure in atmospheres
PSI	Angular deviation of path from initial direction
PT	Product of total pressure (atm) and the square root of $273/T(M,I)$
RANGE	Path length (km)
RE,REARTH	Earth radius (km)
REF	Refractive index of air at level I
RH	Relative humidity (%)
RN	Ratio of refractive indices of air above and below a given level
RX	Ratio of earth center distances between adjacent levels
RO	Earth radius (km) read in as input (=RE)
R1	The product of the sine of the initial zenith angle and the earth center distance to starting altitude
SALP	Sine of angle of arrival at adjacent level
SPHI	Sine of the local zenith angle at a given level
SR	Slant range (km)
SUM	Accumulated integrated absorption
T(M,I)	Temperature (K) for model atmosphere M at level I
THET	Zenith angle at a given level (in radians)
THETA	Zenith angle at a given level (in degrees)
TMP	Ambient temperature ($^{\circ}$ C)
TR	Transmittance scales for transmission functions
TS	Ratio of standard temperature (273.15K) to temperature at level I
TS1	Ratio of 296.0K to temperature at level I
TT	Ratio $273.15/(TMP + 273.15)$
TX(K)	Equivalent absorber amounts per km at a given altitude obtained from POINT; also transmittance values at a given wavelength for each absorber type (K = 1, 8)
TX(9)	Total transmittance at frequency IV
TX(10)	Absorption due to aerosol only at frequency IV

NWC TM 3107

TX1	Refractive index of layer above initial altitude H1
TX2	Refractive index of layer above final altitude H2
TX3	Refractive index of layer above minimum altitude HMIN
VH(K)	Integral of the equivalent absorber amounts from H1 to level I
VIS	Visual range (km) at sea level
VX	Wavelength at which aerosol coefficients are read in (μm)
V1	Initial frequency for transmittance calculation, cm^{-1}
V2	Final frequency for transmittance calculation, cm^{-1}
W(K)	Total equivalent absorber amount for entire path
WH(M, I)	Water vapor density for atmospheric model M at level I (gm m^{-3})
WL, WL1, WL2	Wavelength in microns
WO(M, I)	Ozone density for atmospheric model M at level I (gm m^{-3})
WS1	Transmission function scaling factor for water vapor at given wavelength
WS2	Transmission function scaling factor for carbon dioxide, etc., at given wavelength
WS3	Transmission function scaling factor for ozone at given wavelength
X	Input height to POINT subroutine
XI	Wavenumber interpolation parameter
XX	Wavenumber identification parameter for UV ozone transmittance calculation
X1	Earth center distance of level I
X2	Earth center distance of level I + 1
YN	Refractive index of layer <u>below</u> input height from POINT subroutine
YN1	Refractive index of layer below initial altitude III
YN2	Refractive index of layer below final altitude H2
YY	Aerosol absorption coefficient at frequency V
Z(I), ZO(I)	Altitude at level I in km

NWC TM 3107

CONCLUSIONS

LOWTRAN is, in the author's opinion, the best available computer code for analyzing atmospheric transmittance effects on electro-optical systems. As such, it should be used in the evaluation of all electro-optic type sensors. With the release of LOWTRAN IIIB, several previously valid criticisms have been accounted for; in addition, the U.S. Air Force Geophysics Laboratory continues to improve and upgrade the existing code.

The author would appreciate being notified of any difficulties or problems that arise when using NWC/LOWTRAN. Also, any assistance that may be required, either in using the existing code or in modifying the code for use in a simulation, can be obtained by contacting the author.

REFERENCES & BIBLIOGRAPHY

1. Institute for Defense Analyses, Infrared Continuum Absorption by Atmospheric Water Vapor in the 8-12 μm Window by Robert E. Roberts, Lucien M. Biberman, and John E. A. Selby. Paper P-1184, dtd Apr 1976. Also in Applied Optics (1976).
2. Air Force Geophysics Laboratory, Atmospheric Transmittance from 28.5 μm : Computer Code LOWTRAN 2 by J. E. A. Selby and R. M. McClatchey, AFCRL-TR-72-0745, dtd 29 Dec 1972.
3. . Atmospheric Transmittance from 0.25 to 28.5 μm : Computer Code LOWTRAN III by J. E. A. Selby and R. A. McClatchey, AFCRL-TR-75-0255, dtd 7 May 1975.
4. . Computer Code Update to LOWTRAN IIIB (Working Papers) by J. E. A. Selby and R. A. McClatchey (received by author on 24 Sept 1976).
5. . Optical Properties of the Atmosphere (third edition) by R. A. McClatchey, et al., AFCRL-TR-72-0497, dtd 24 Aug 1972.
6. . AFCRL Atmospheric Absorption Line Parameters Compilations by R. A. McClatchey, et al., AFCRL-TR-73-0096, dtd 26 Jan 1973.
7. . Atmospheric Attenuation of Laser Radiation from 0.76 to 31.25 μm by R. A. McClatchey and J. E. A. Selby, AFCRL-TR-74-0003, dtd 3 Jan 1974.
8. Naval Weapons Center, Naval Weapons Center (Code 407) Reprogrammed Version of U.S. Air Force Geophysics Laboratory Computer Code LOWTRAN III by William M. Cornette. NWC Reg. Memo 4073-19-74, dtd 27 Apr 1976.
9. . Errata to NWC/LOWTRAN 3 Computer Code by William M. Cornette. NWC Reg. Memo 4073-31-76, dtd 18 Jun 1976.
10. . Correction to AFGL/LOWTRAN 3 and NWC/LOWTRAN 3 Computer Codes by William M. Cornette. NWC Reg. Memo 4073-42-76, dtd 12 Aug 1976.
11. . EO Weapon System Meteorology: Parameters and Instrumentation by Alexis Shlanta. NWC Technical Memo 2856, dtd Aug 1976.
12. American National Standards Institute, Inc., FORTRAN, ANSI-X3.9 - 1966, 7 Mar 1966.

NWC TM 3107

13. Bell Telephone Laboratories, The PPORT Verifier, by B. G. Ryder and A. D. Hall. Computing Science Technical Report No. 12, dtd Jul 1975.
14. Naval Weapons Center, Notification of Problem Areas in LOWTRAN III and LOWTRAN IIIB Computer Codes by William M. Cornette. NWC Reg. Memo 3173-51-76, dtd 3 November 1976.
15. . Availability of Atmospheric Transmittance Computer Code LOWTRAN IIIB at the Naval Weapons Center by William M. Cornette and Alexis Shlanta. NWC TM 2965, Nov 1976.
16. . Errata to Naval Weapons Center Version of the Atmospheric Transmittance Computer Code LOWTRAN IIIB. Serial ltr. #7917, dtd 20 December 1976.