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AEROSPACE SYSTEMS INC BURLINGTON MASS
ROTOR WAKE EFFECTS ON HUB/PYLON FLOW. VOLUME II. PROGRAM SHAPES--ETC(U)
MAY 78 P 500H00, R B NOLL, L MORINO, N D HAMM DAAJ02-75-C-0041

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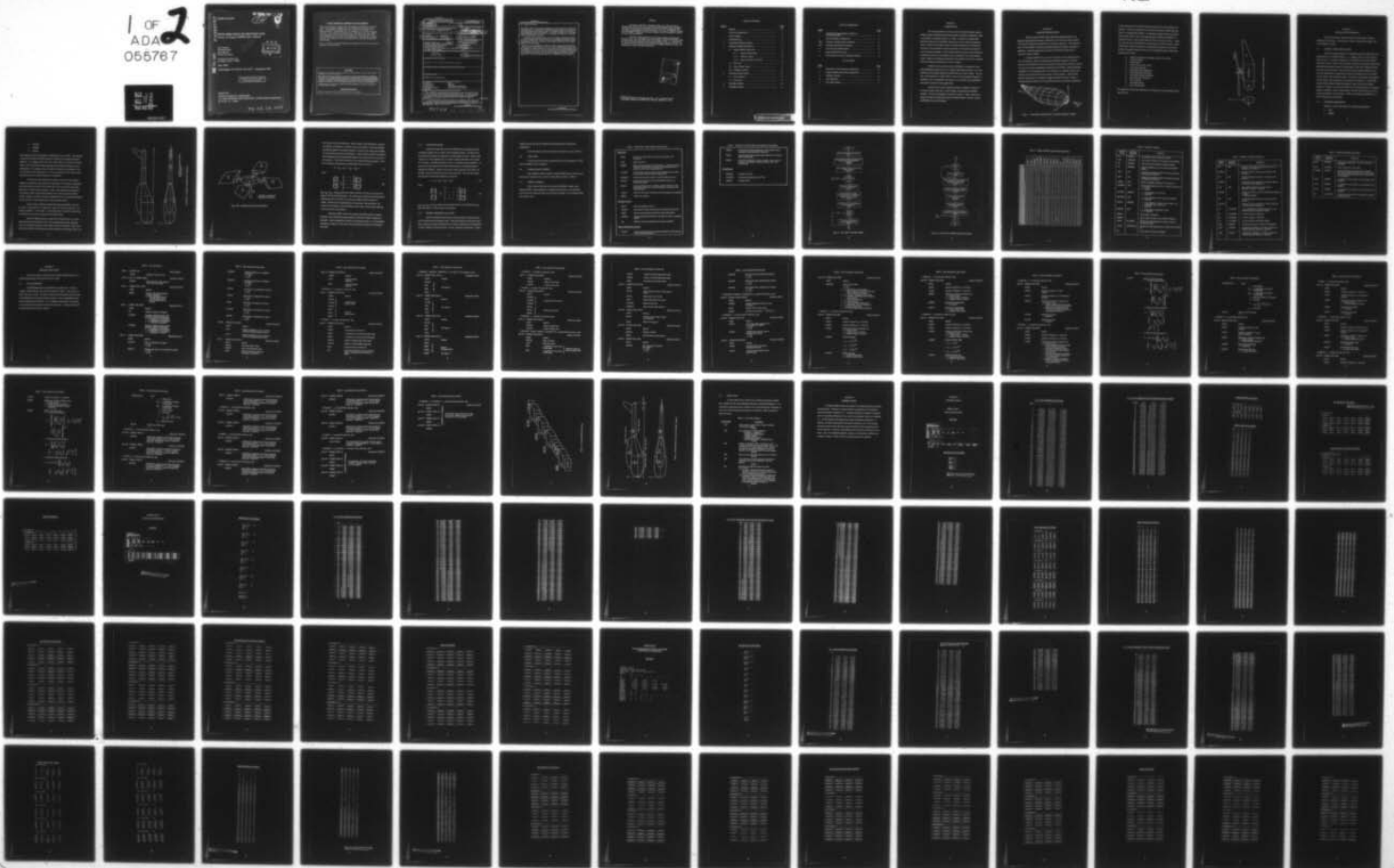
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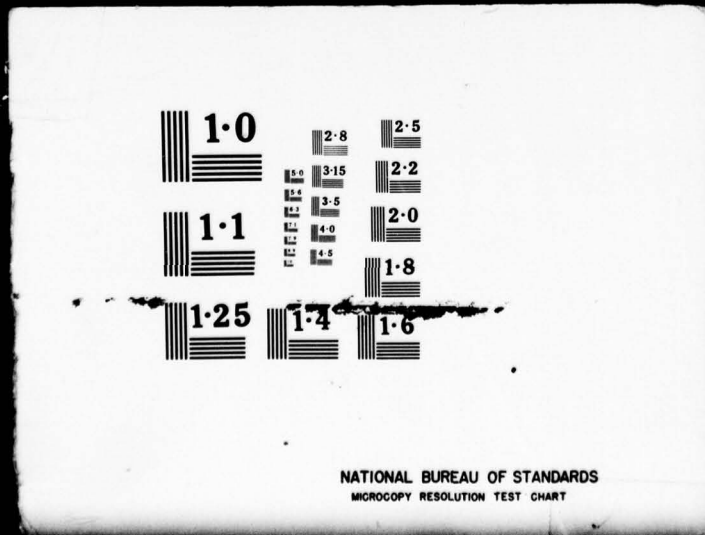
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ROTOR WAKE EFFECTS ON HUB/PYLON FLOW
Volume II, Program SHAPES User's Manual

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AD 55921



Aerospace Systems, Inc.
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May 1978

Final Report for Period June 1975 - September 1977

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Prepared for
APPLIED TECHNOLOGY LABORATORY
U. S. ARMY RESEARCH AND TECHNOLOGY LABORATORIES (AVRADCOM)
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APPLIED TECHNOLOGY LABORATORY POSITION STATEMENT

This report presents a method for determining aerodynamic characteristics of helicopter shapes under the influence of the main rotor wake. The method is considered to be worthy of publication for dissemination of information and the stimulation of further related research. The reader is cautioned that this method does not predict flow separation as the title would imply, nor does the rotor wake fully impinge upon the body of the helicopter. The method is useful, however, as a design tool in determining rotor-fuselage aerodynamic interference.

Mr. F. A. Raitch of the Aeromechanics Technical Area served as project engineer for this effort.

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19 REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER	
USARTL-TR-78-1B			
4. TITLE (and Subtitle)	5. TYPE OF REPORT & PERIOD COVERED		9
ROTOR WAKE EFFECTS ON HUB/PYLON FLOW. Volume II, Program SHAPES User's Manual.	Final Report, June 1975 - September 1975		
7. AUTHOR(s)	14	6. PERFORMING ORGANIZATION REPORT NUMBER	
Paul/Soohee, Richard B./Noll, Luigi/Morino Norman D./Ham		AST-TR-76-38 Volume II - Vol - 2	
5. PERFORMING ORGANIZATION NAME AND ADDRESS	15	8. CONTRACT OR GRANT NUMBER(s)	
Aerospace Systems, Inc. Burlington, Massachusetts 01803		DAAJ02-75-C-0041	
11. CONTROLLING OFFICE NAME AND ADDRESS	16	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
Applied Technology Laboratory U.S. Army Research & Technology Labs (AVRADCOM) Fort Eustis, Virginia 23604		62209A 1F262209AH76 00 087 EK	
14. MONITORING AGENCY NAME & ADDRESS (If different from Controlling Office)	11	12. REPORT DATE	
12 294p.		May 1978	
		13. NUMBER OF PAGES	
		190	
		15. SECURITY CLASS. (of this report)	
		Unclassified	
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
16. DISTRIBUTION STATEMENT (of this Report)			
Approved for public release; distribution unlimited.			
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)			
18. SUPPLEMENTARY NOTES			
Volume II of a two-volume report.			
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)			
Helicopter	Rotors		
Hub/Pylon Flow	Separation		
Induced Drag	Finite Element Aerodynamics		
Potential Aerodynamics	Aerodynamic Computer Program		
Rotor Wake			
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)			
An investigation has been conducted to demonstrate the use of the Green's function method to study rotor wake effects on helicopter hub/pylon flow. This report consists of two volumes which document the theoretical formulation and the use of the digital computer program SHAPES (Subsonic Helicopter Aerodynamics Program with Effects of Separation).			
Volume I presents the theoretical formulation and corresponding numerical procedure for the study of incompressible potential aerodynamics with separated flow. While the			

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20. Abstract (Continued)

formulation is valid for fully unsteady aerodynamics, this report is mainly concerned with rotor aerodynamics. A potential flow aerodynamic program, SHAPES, with suitable rotor wake representation was developed to predict the separation characteristics of arbitrary three-dimensional helicopter configurations. In particular, the effect of the rotor blade wake, blade shank wake, and hub wake in the separation of the flow over a lifting helicopter in forward flight is analyzed.

The present method has potential application in the design of helicopters because it provides an analytical capability which can be used to develop low-drag profile as well as to explore problem areas. Extensive numerical results obtained from Program SHAPES demonstrated the flexibility and accuracy of the method. These results are in excellent agreement with existing data.

Volume II, The User's Manual, describes the structure and use of Program SHAPES. SHAPES is written in FORTRAN IV for operation on the CDC 6600 digital computer system at the Applied Technology Laboratory, U.S. Army Research and Technology Laboratories (AVRADCOM), Fort Eustis, VA. The User's Manual (Volume II) contains detailed information for preparing an input data deck and interpreting the computed data; a discussion of various subroutines, flow charts, common storage and definition of FORTRAN variables; sample cases to illustrate the program output; and a FORTRAN listing of the program.

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PREFACE

This report, prepared by Aerospace Systems, Inc. (ASI), Burlington, Massachusetts, for the U.S. Army under Contract DAAJ02-75-C-0041, documents the results of research performed during the period June 1975 to September 1977. The study was sponsored by the Eustis Directorate, U.S. Army Air Mobility Research and Development Laboratory,* Fort Eustis, Virginia, with Mr. Frederick A. Raitch serving as Technical Monitor.

The effort was directed by Mr. John Zvara, President and Technical Director of ASI. Mr. Paul Soohoo served as Principal Technical Staff Member under the supervision of Mr. Richard B. Noll, Vice President of ASI. Dr. Luigi Morino, Director of Computational Continuum-Mechanics Program at Boston University, and Dr. Norman D. Ham, Director of the V/STOL Technology Laboratory at MIT, contributed to the study as Principal Consultants.

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SECTION 1 INTRODUCTION

This volume describes the structure and use of a digital computer program, SHAPES, Subsonic Helicopter Aerodynamic Program with Effects of Separation, which was developed by Aerospace Systems, Inc. (ASI), to analyze the incompressible potential aerodynamics of helicopter configuration with rotor wakes and separation effects. Volume 1 of this report contains a complete description of the theoretical formulation and corresponding numerical procedure for the aerodynamic method for use in the computer program. It also includes extensive numerical results showing the flexibility and accuracy of the method as well as comparison with several existing results. Proper use of SHAPES is predicated on the assumption that the user is familiar with the techniques and limitations set forth in Volume 1.

SHAPES is written almost entirely in FORTRAN IV for operation on the CDC 6600 digital computer system at the Applied Technology Laboratory, U.S. Army Research and Technology Laboratories (AVRADCOM), Fort Eustis, Virginia. The program was developed with a highly modular structure for ease of program checkout, to simplify the user's understanding of the program, and to facilitate any modifications that might be required for future applications.

Sections 2 and 3 contain programming details of SHAPES: functions of the various routines, flow charts, common storage, and definition of FORTRAN variables. The use of the program is presented in Section 4. Sample cases are presented in Section 5 to illustrate the output of Program SHAPES. Section 6 contains the FORTRAN listing of the program.

SECTION 2

COMPUTER PROGRAM SHAPES

Computer program SOUSSA (Steady Oscillatory Unsteady Subsonic and Supersonic Aerodynamics) discussed in Subsection 2.2 of Volume I has been modified to include rotor dynamics and separation from hub/pylon components. The revised program is called SHAPES, for Subsonic Helicopter Aerodynamic Program with Effects of Separation. Geometry preprocessor for single-rotor helicopter configurations is included in Program SHAPES.

In Program SHAPES the user need not be familiar with the aerodynamic portion of the program, unlike other sophisticated aerodynamic programs in which the choice for the combination of various aerodynamic functions (sources, doublets, vortices) is an art which requires considerable understanding of the method. Another advantage of SHAPES is that the paneling used for the aerodynamics is completely arbitrary and, therefore, may coincide with the one used for structural analysis. A typical finite element representation of a helicopter fuselage configuration is shown in Figure 1. The aerodynamic paneling can be accomplished manually by inputting the coordinates

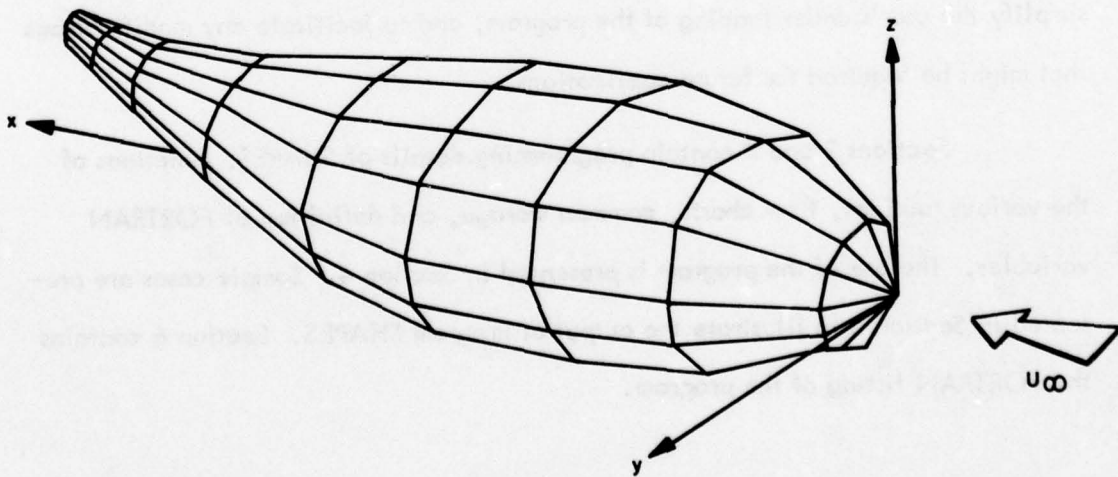


Figure 1. Finite Element Representation of Arbitrary Helicopter Fuselage.

of the corner points of all selected aerodynamic panels or by using a geometry preprocessor. A geometry preprocessor for conventional helicopter configurations (see Figure 2) is incorporated in SHAPES. The fuselage is assumed to have an elliptical center section with the nose and tail approximated by elliptical paraboloids. An ellipsoidal element is used to approximate the rotor hub and pylon sections. In addition, the rotor shaft and blade shank are represented by cylindrical sections. Given the helicopter configuration geometry, the preprocessor computes the corner point locations of required aerodynamic panels for the complete helicopter configuration.

Required inputs include:

- Shape and dimensions of fuselage, pylon, shaft, and hub
- Number of blades
- Rotor diameter
- Extent of root cutout or shank
- Cross-section of shank
- Rotor blade airfoil designation
- Rotor blade chord distribution
- Rotor blade thickness distribution
- Rotor blade twist distribution
- Rotor tip speed
- Freestream velocity
- Rotor wake geometry

This capability eliminates the requirement for the selection of the aerodynamic paneling by the user.

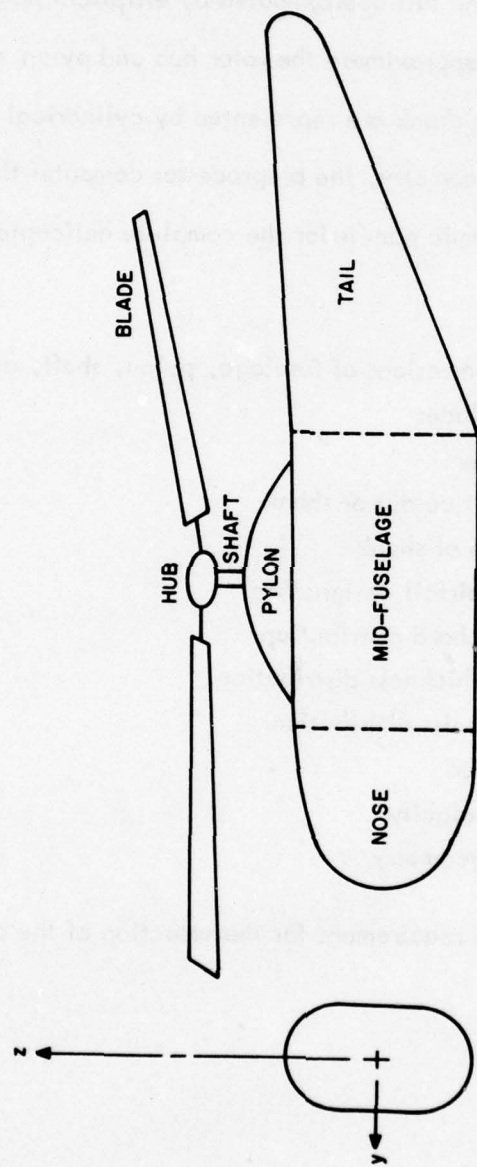


Figure 2. Typical Helicopter Configuration.

SECTION 3

PROGRAM SHAPES DESCRIPTION

This section contains a brief description of the organization of Program SHAPES and its subroutines, a flow diagram, a table of common block storage, and a list of FORTRAN variables.

3.1 PROGRAM SHAPES ORGANIZATION

The present computer program for incompressible potential aerodynamics with separated flow for a complete helicopter, i.e., fuselage, pylon, and rotor, contains three main parts: (1) geometric preprocessor, (2) coefficient matrix, and (3) pressure distribution and force. Based on data provided, the geometric preprocessor automatically generates the aerodynamic panels for the helicopter as well as the numbering and location of the panel corner points in the reference Cartesian (global) coordinate system. The matrix coefficients are determined by evaluating the doublet and source integrals over the surface of the aerodynamic panels. This yields N simultaneous linear equations with N unknown velocity potentials at the centroids of N elements. A standard IBM subroutine GELG (Gaussian elimination method) is used to solve for the unknown potentials. To obtain a continuous distribution for the velocity potential, an averaging scheme is introduced. Hence, the perturbation velocities and the pressure at the centroid of each element can be evaluated. Finally, the aerodynamic coefficients, i.e., lift and induced drag, are computed.

3.1.1 GEOMETRIC PREPROCESSOR

Presently, five main subroutines form the geometric preprocessor:

- DATA
- PREPRO

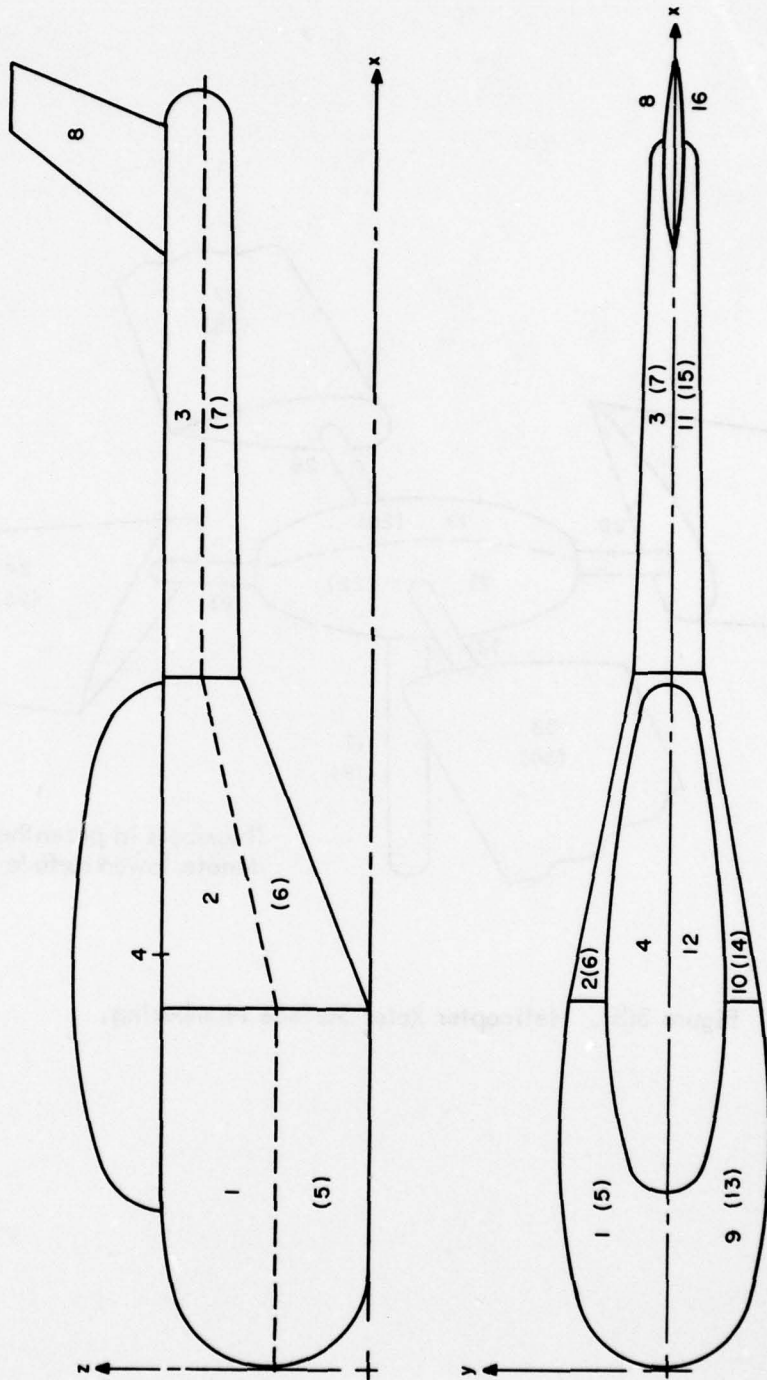
- COODPT
- GEOMET
- VEC123

Basic geometric inputs of the problem are defined by the user in DATA. This subroutine automatically generates the global subsurface numbering of the complete helicopter geometry; i.e., fuselage, pylon, shaft, hub, shank, blade, and vertical tail sections. Figure 3 shows the subsurface global numbering for the helicopter fuselage and rotor configurations. One important input for DATA is the number of the elements in the x and y directions for each subsurface, IS. This input controls the total number of aerodynamic panels used to model the geometry of the problem.

The variation of the element sizes (uniform or nonuniform finite element breakup) is another basic input parameter to the program. In the present investigation, particular attention must be paid to the flow field in the vicinity of the rotor shaft, pylon, hub, and upper fuselage elements. Hence, small elements are prescribed for the hub/pylon region, whereas larger elements can be used on the lower fuselage section. Moreover, the local curvilinear coordinates ξ and η are automatically defined so that the normal to each surface panel is always directed outward.

Finally, DATA automatically defines the parameter KWAKES, which has the value 1 if the subsurface, IS, generates a wake and a value of 0 otherwise. For example, KWAKES = 1 on the pylon. A vortex-layer wake is assumed to emanate from the separation point and this is represented as a doublet layer.

Subroutine PREPRO generates a nodal function NOFCT (IXY, IS), which relates the local nodal numbering, IXY, with the required global nodal numbering. Next, the Cartesian coordinates of these nodes is obtained by COODPT. Basic inputs required for COODPT are the shape and overall dimensions of the fuselage, pylon, and



(Numbers in parentheses denote lower surface.)

Figure 3(a). Helicopter Fuselage Surface Numbering.

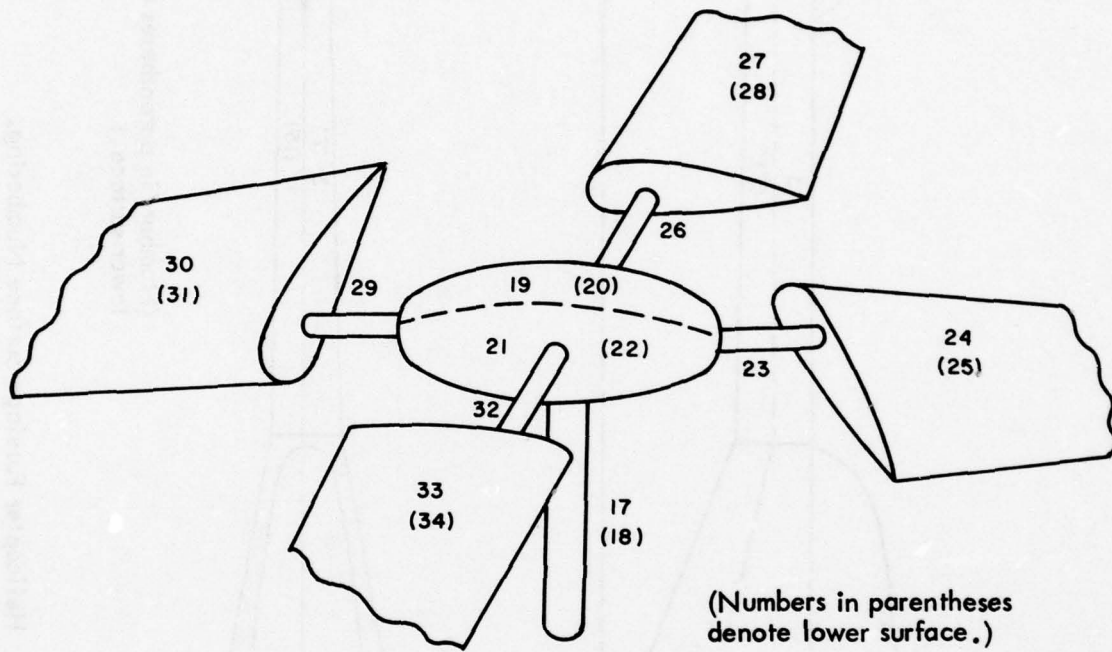


Figure 3(b). Helicopter Rotor Surface Numbering.

hub sections, blade-twist distribution, blade thickness, chord distribution, number of rotor blades, rotor diameter, and extent of root cutout (shank). Subroutine GEOMET automatically generates a parameter NODE as a function of the corner point ICORNR for each aerodynamic panel of the helicopter. Finally, VEC123 completes the geometry of the aerodynamic panel (hyperboloidal element) that contains the four corner points of the element. This results in continuity of the complete helicopter geometry. Note that the equation that represents a hyperboloidal element is given by

$$\bar{P} = \bar{P}_0 + \bar{P}_1 \xi + \bar{P}_2 \eta + \bar{P}_3 \xi \eta \quad (1)$$

where

$$\begin{Bmatrix} \bar{P}_0 \\ \bar{P}_1 \\ \bar{P}_2 \\ \bar{P}_3 \end{Bmatrix} = \frac{1}{4} \begin{bmatrix} 1 & 1 & 1 & 1 \\ 1 & 1 & -1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & -1 & 1 \end{bmatrix} \begin{Bmatrix} \bar{P}_{pp} \\ \bar{P}_{pm} \\ \bar{P}_{mp} \\ \bar{P}_{mm} \end{Bmatrix} \quad (2)$$

\bar{P}_{pp} , \bar{P}_{pm} , \bar{P}_{mp} , and \bar{P}_{mm} denote the Cartesian location of the four corner points and \bar{P}_0 gives the centroid of the element. This subroutine also performs the Prandtl-Glauert transformation and the rotation of the axis due to angle of attack and angle of sideslip. PRINTA writes the specifications of the problem, node coordinates, the centroid of each element, nodal numbering for each surface, and the nodal numbering of the corner points of the element.

Subroutine CHECK verifies if the maximum permissible number of elements along the x and y directions on each subsurface and the total number of elements are exceeded. Several compatibility conditions exist between the data. If an incompatible relationship is present, an error code will be printed and the execution of the program terminated.

3.1.2 COEFFICIENT MATRIX

Subroutine COEFF forms the matrix coefficients by evaluating the source and doublet integrals over the surface of the aerodynamic panels. The effect of the rotor wake and the presence of separation are automatically included. COEFF yields a system of N linear equations with N unknown velocity potentials at the centroid of N elements. SOLUTN calls GELG to solve N simultaneous linear equations. To obtain the velocity potential at the node of each element, an averaging scheme is employed by AVERAG. Using the value of the velocity potential at the nodes, PHI provides a continuous distribution of the velocity potential. Note that the equation that represents this continuous distribution is given by

$$\varphi = \varphi_0 + \varphi_1 \xi + \varphi_2 \eta + \varphi_3 \xi \eta \quad (3)$$

where

$$\begin{Bmatrix} \varphi_0 \\ \varphi_1 \\ \varphi_2 \\ \varphi_3 \end{Bmatrix} = \frac{1}{4} \begin{bmatrix} 1 & 1 & 1 & 1 \\ 1 & 1 & -1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & -1 & 1 \end{bmatrix} \begin{Bmatrix} \varphi_{pp} \\ \varphi_{pm} \\ \varphi_{mp} \\ \varphi_{mm} \end{Bmatrix} \quad (4)$$

φ_{pp} , φ_{pm} , φ_{mp} , and φ_{mm} denote the velocity potential at the nodal points and φ_0 gives the value of φ at the centroid of the element.

3.1.3 PRESSURE DISTRIBUTION AND FORCE

VELXYZ evaluates the perturbation velocity (Cartesian coordinate system) at the centroid of each aerodynamic panel. Subroutine CPLINR uses Bernoulli's equation to compute the pressure distribution at the centroid. PRINTB writes the distribution of sources, doublets, velocity potential, velocity, and pressure distribution. Finally,

FORCE evaluates the total lift coefficient and induced drag on the helicopter configuration.

A brief description of the main program and subroutines is given in Table 1.

3.2 FLOW CHART

In order to provide a general understanding of the overall program, the flow chart for SHAPES is shown in Figure 4.

3.3 COMMON BLOCK STORAGE

Most FORTRAN-related variables in Program SHAPES used by more than one subroutine are organized into a number of common blocks as shown in Table 2.

3.4 FORTRAN VARIABLES

Table 3 presents definitions of all principal FORTRAN variables used in Program SHAPES. Where appropriate, mathematical definitions are also indicated. The units of each variable are those used internally by SHAPES, and occasionally differ from the input units.

Table 1. Description of Main Program and Subroutines.

<u>Preprocessor</u>	
MAIN	Controls the logical flow of information supplied by the subroutines.
DATA	Reads input data.
PREPRO	Defines nodal numbering for the helicopter. (The surface of the helicopter configuration is divided into 34 subsurfaces with a maximum of four rotor blades permitted.)
COODPT	Defines and/or reads in the Cartesian coordinates of the nodes on the surface of the helicopter configuration.
GEOMET	Defines the four nodal corners for each aerodynamic panel.
VEC123	Defines the equation of each hyperboloidal surface (i.e., aerodynamic panel).
PRINTA	Writes specification of the problem, nodal numbering for the helicopter configuration, nodal coordinates, and the centroid of the elements.
CHECK	Verifies if the maximum defined in the main program is exceeded.
DEBUG	Writes error message.
<u>Coefficient Matrix</u>	
COEFF	Forms the coefficient matrix.
SOLUTN	Calls GELG to obtain the perturbation aerodynamic potential.
GELG	Solves system of general equations by Gauss elimination.
AVERAG	Obtains potential distribution at the nodes by using an averaging scheme.
PHI	Defines a continuous distribution of velocity potential.
<u>Pressure Distribution and Force</u>	
VELXYZ	Evaluates the velocity (perturbation) distribution at the centroid of each aerodynamic panel.

Table 1. Description of Main Program and Subroutines (Concluded).

CPLINR	Evaluates the pressure distribution at the centroid of each aerodynamic panel (Bernoulli's equation).
FORCE	Evaluates the lift and induced drag coefficients on the helicopter configuration.
PRINTB	Writes the distribution of source, doublet, wake, velocity potential, perturbation velocities, pressure, lift, and induced drag.
<u>Miscellaneous</u>	
ASINH(X)	Evaluates $\sinh^{-1}(X)$.
ATANP(X)	Evaluates principal part of $\tan^{-1}(X)$.
LOG(X)	Evaluates $\ln(X)$.

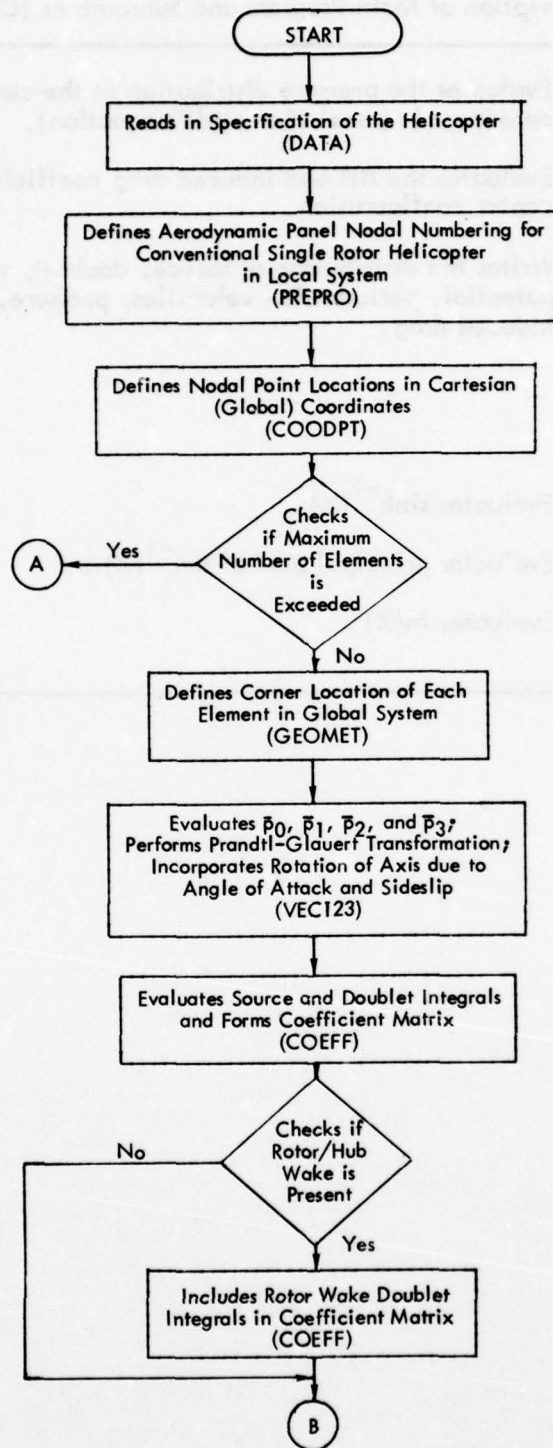


Figure 4. Flow Chart for SHAPES Program.

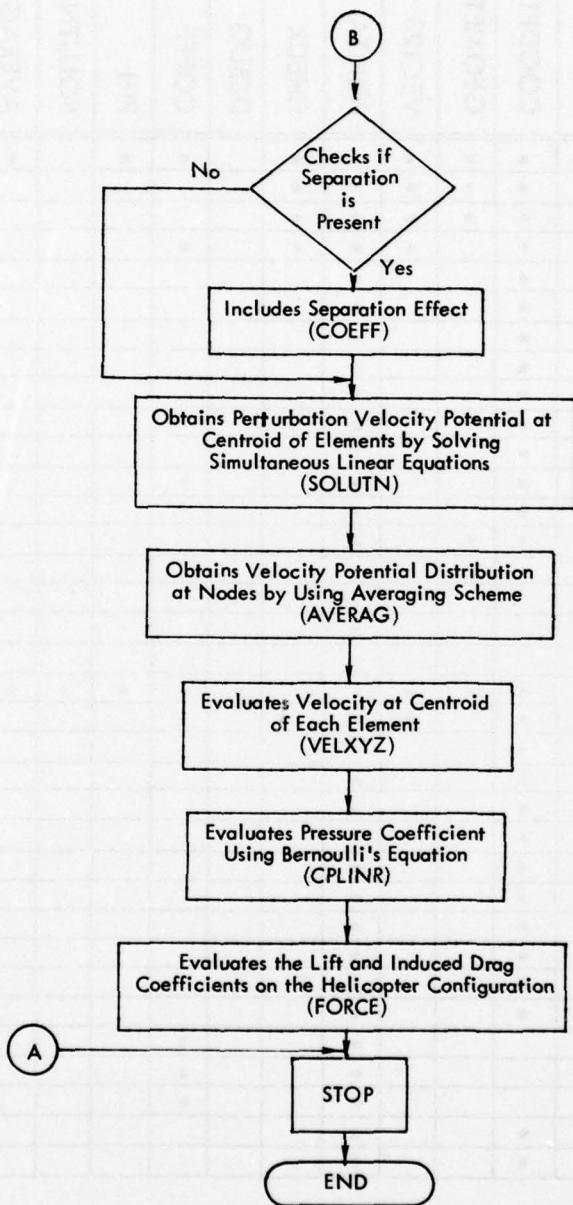


Figure 4. Flow Chart for SHAPES Program (Concluded).

Table 2. Program SHAPES Common Block Organization.

	MAIN	DATA	PREPRO	COORDPT	GEOMET	VEC123	PRINTA	CHECK	DEBUG	COEFF	PHI	SOLUTN	AVERAG	VELXYZ	CPLINR	FORCE	PRINTB
ZZZ1	*	*	*	*	*	*	*	*		*	*		*	*	*	*	*
ZZZ2	*	*	*	*	*	*	*	*									*
ZZZ3	*	*	*	*	*	*	*	*									*
ZZZ4	*	*		*		*	*	*		*						*	*
ZZZ5	*	*		*			*										*
ZZZ6	*	*		*			*										*
ZZZ7	*	*		*			*										*
ZZZ8	*	*		*			*										*
ZZZ9	*	*		*			*										*
ZZZ10	*	*		*			*										*
ZZZ11	*	*		*			*										*
ZZZ12	*	*		*			*			*							*
ZZZ13	*	*		*			*										*
ZZZ14	*	*		*	*		*										*
ZZZ15	*	*		*			*										*
ZZZ16	*	*					*										*
ZZZ17	*	*					*										*
ZZZ18	*	*					*										*
ZZZ19	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
ZZZ20	*	*		*		*	*			*							*
ZZZ21	*	*	*	*			*										*
ZZZ22	*	*		*			*										*
ZZZ23	*	*		*			*										*
ZZZ24	*	*		*			*										*
ZZZ25	*	*		*			*										*
ZZZ26	*	*		*			*										*
ZZZ27	*	*		*			*										*
ZZZ28	*	*		*			*										*
ZZZ29	*	*		*			*										*
ZZZ30	*	*		*			*										*
ZZZ31	*	*					*			*							*
ZZZ32	*	*					*			*							*
ZZZ33	*	*					*			*							*
ZZZ34	*	*		*			*										*
ZZZ35	*	*		*			*										*

Table 3. FORTRAN Variables.

Variable Name	Maximum Dimension	Definition
AA	(NESQ)	A coefficient matrix (stored columnwise).
AVG	(NNODE)	The number of elements surrounding the node INODE.
BC	(NELEM)	Downwash on the centroid of IELEMth element.
CP	(NELEM)	Pressure coefficient at the centroid of the IELEMth element.
HCSI	(11)	Defines the normalized nodal line locations along the x direction for surface IS.
HETA	(11)	Defines the normalized nodal line locations along the y direction for surface IS.
ISFACE	(NS)	Defines the global numbering of the surface IS.
KNORML	(NS)	Indicates the direction of the unit normal on surface IS. = 1 outward = -1 inward
KROTOR	(NELEM)	= 1 if the element is on the rotor = 0 otherwise
KROTORS	(NS)	= 1 if the subsurface is part of the rotor assembly = 0 otherwise
KWAKE	(NELEM)	= 1 if the element is in contact with a wake, i.e., rotor blade, hub, pylon, etc. = 0 otherwise
KWAKES	(NS)	= 1 if the surface IS generates a wake = 0 if otherwise
NELEM		Total number of elements.
NNODE		Total number of nodes on the surfaces considered.
NODE	(4,NELEM)	Defines the nodal numbering at the four corners of the element IELEM.
NOFCT	(NXYMP,34)	Defines the nodal numbering of the nodes on the surface IS.
NS		Total number of surfaces considered.

Table 3. FORTRAN Variables (Continued).

Variable Name	Maximum Dimension	Definition
NT	(34)	Subtotal of the number of elements up to, but not including, the surface IS.
NTMAX		Maximum number of elements permissible on the helicopter.
NX	(34)	Number of elements along the x direction of the surface IS.
NXMAX		Maximum number of elements permissible along the x direction on any subsurface.
NXY	(34)	Total number of elements on the surface IS [NXY(IS) = NX(IS) * NY(IS)]
NXYMP		Defines the maximum number of elements permitted on a surface = NXMAX*NYMAX
NY	(34)	Number of elements along the y-direction of the surface IS.
NYMAX		Maximum number of elements permissible along the y direction on any subsurface.
PC	(3,NELEM)	x,y,z coordinates of centroid of elements in the reference Cartesian coordinate system.
P1	(3,NELEM)	A vector along the ξ direction.
P2	(3,NELEM)	A vector along the η direction.
P3	(3,NELEM)	A vector normal to the element IELEM.
PHIC	(NELEM)	Velocity potential at the center of the element.
PHI1	(NELEM)	Interpolation coefficient - the local variation of velocity potential along the ξ direction.
PHI2	(NELEM)	Interpolation coefficient - the local variation of velocity potential along the η direction.

Table 3. FORTRAN Variables (Concluded).

Variable Name	Maximum Dimension	Definition
PH13	(NELEM)	Interpolation coefficient - the local variation of downwash.
SOR	(NNODE)	Velocity potential at the nodes.
SOURCE	(NELEM)	Source distributions at the centroids of elements. After calling subroutine GELG, this variable stores the velocity potential distributions at the centroids of the elements.
VELX	(NELEM)	x component of the velocity at the centroids of the elements.
VELY	(NELEM)	y component of the velocity at the centroids of the elements.
VELZ	(NELEM)	z component of the velocity at the centroids of the elements.
XK	(3,NNODE)	Coordinates of the nodes in the reference Cartesian coordinate system.

SECTION 4

PROGRAM SHAPES USAGE

This section contains a description of the Program SHAPES data input including program options and a description of error codes.

4.1 INPUT DESCRIPTION

All SHAPES data input is accomplished via punched cards. The input variables, required formats, and options are presented in Table 4. Some inputs may require more than one card. The number of input data cards required varies from case to case depending on the type of problem considered. Several compatibility conditions exist among some of the data. If an incompatible relationship is encountered, an error code will be printed and the execution terminated. A typical data setup for running multiple cases is shown in Figure 5.

Table 4. Input Description.

Data 1:	FORMAT (I5)	(Main Program)
	NCASE	Number of cases to be run
Data 2, 3, and 4:	FORMAT (20A4)	(Subroutine DATA)
	GG(20)	Name, location, date, description of job, and remarks
Data 5:	FORMAT (2A4, 10I5)	(Subroutine DATA)
	GG(2)	Remarks
	KREAD	Control code for the definition of nodal coordinates = 0 the coordinates will be defined automatically = 1 the coordinates will be read in
Data 6:	FORMAT (2A4, 10I5)	(Subroutine DATA)
	GG(2)	Remarks
	NS	Number of surfaces considered
	KSYMMY	Symmetry condition between left- and right-hand side of helicopter = -1 if geometry is antisymmetric = 0 if geometry has no symmetry = 1 if geometry is symmetric
	KSYMMZ	Symmetry condition between upper and lower surfaces of helicopter = -1 if geometry is antisymmetric = 0 if geometry has no symmetry = 1 if geometry is symmetric
Data 7:	FORMAT (2A4, 10I5)	(Subroutine DATA)
	GG(2)	Remarks
	NPYLON	Pylon is considered for analysis = 1 yes = 0 no
	NBODY1	Fuselage nose section is considered for analysis = 1 yes = 0 no

Table 4. Input Description (Continued).

NBODY2	Fuselage midsection is considered for analysis = 1 yes = 0 no
NBODY3	Fuselage tail section is considered for analysis = 1 yes = 0 no
NVTAIL	Vertical tail is considered for analysis = 1 yes = 0 no
NSHAFT	Rotor shaft is considered for analysis = 1 yes = 0 no
NHUB	Rotor hub is considered for analysis = 1 yes = 0 no
NSHANK	Blade shank is considered for analysis = 1 yes = 0 no
NBLADE	Rotor blade is considered for analysis = 1 yes = 0 no
Data 8:	FORMAT (2A4,10I5) (Subroutine DATA)
GG(2)	Remarks
KPYL1	Number of elements in the x direction of the mid-fuselage before the pylon
KPYL2	Number of elements in the x direction of the mid-fuselage after the pylon
Data 9:	FORMAT (2A4,7F8.3) (Subroutine DATA)
GG(2)	Remarks
UMACH	Freestream Mach number
OMEGA	Rotor rotational speed (rpm)
AREA	Reference area for evaluating aerodynamic coefficient

Table 4. Input Description (Continued).

Data 10: FORMAT (2A4,7F8.3) (Subroutine DATA)

GG(2)	Remarks
ALFA	Angle of attack (degrees)
BETA	Angle of sideslip (degrees)

If NPYLON = 1, use Data 11; otherwise, skip.

Data 11: FORMAT (2A4,7F8.3) (Subroutine DATA)

GG(2)	Remarks
XPYCTR	Coordinates of pylon's center
YPYCTR	
ZPYCTR	
RXPYL	Radii of pylon section
RYPYL	
RZPYL	

If NVTAIL = 1, use Data 12; otherwise, skip.

Data 12: FORMAT (2A4,7F8.3) (Subroutine DATA)

GG(2)	Remarks
VSPAN	Span length of vertical tail
XLEZV	x coordinate of vertical tail leading edge
XTEZV	x coordinate of vertical tail trailing edge
TANLEV	Tangent of leading edge sweep angle
TANTEV	Tangent of trailing edge sweep angle
TAUV	Thickness ratio of vertical tail
ZPV	Height of root chord of vertical tail with respect to global Cartesian coordinate system

Table 4. Input Description (Continued).

If $(N\text{BODY1} + N\text{BODY2} + N\text{BODY3}) \neq 0$, use DATA 13-16; otherwise, skip.

Data 13: FORMAT (2A4, 7F8.3) (Subroutine DATA)

GG(2)	Remarks
XNOSE	} See Figure 6
XBD1	
XBD2	
XTAIL	

Data 14: FORMAT (2A4, 7F8.3) (Subroutine DATA)

GG(2)	Remarks
YNOSE	} See Figure 6
YBD1	
YBD2	
YTAIL	

Data 15: FORMAT (2A4, 7F8.3) (Subroutine DATA)

GG(2)	Remarks
ZNOSE	} See Figure 6
ZBD1	
ZBD2	
ZTAIL	

Data 16: FORMAT (2A4, 7F8.3) (Subroutine DATA)

GG(2)	Remarks
RYBD1	} Radii of fuselage section See Figure 6
RZBD1	
RYBD2	
RZBD2	

Table 4. Input Description (Continued).

If NSHAFT = 1, use Data 17; otherwise, skip.

Data 17: FORMAT (2A4,7F8.3) (Subroutine DATA)

GG(2)	Remarks
RSHAFT	Radius of rotor shaft
LSHAFT	Length of rotor shaft

If NHUB = 1, use Data 18; otherwise, skip.

Data 18: FORMAT (2A4,7F8.3) (Subroutine DATA)

GG(2)	Remarks
XHUBCR	} Coordinates of hub center
YHUBCR	
ZHUBCR	
RXHUB	} Radii of hub section
RYHUB	
RZHUB	

If NSHANK = 1, use Data 19; otherwise, skip.

Data 19: FORMAT (2A4,7F8.3) (Subroutine DATA)

GG(2)	Remarks
RSHANK	Radius of blade shank
LSHANK	Length of blade shank

If (NSHAFT + NHUB + NSHANK + NBLADE) \neq 0, use Data 20-23; otherwise, skip.

Data 20: FORMAT (2A4,7F8.3) (Subroutine DATA)

GG(2)	Remarks	
RROTOR	Blade tip radius	
YCUT	Blade root cutout	
XBLE	x coordinate of root chord leading edge	} Reference blade at azimuth angle of 90°
XBTE	x coordinate of root chord trailing edge	

Table 4. Input Description (Continued).

	TANBLE	Tangent of leading edge sweep angle	
	TANBTE	Tangent of trailing edge sweep angle	
	TAUBL	Thickness ratio of blade airfoil	
Data 21:	FORMAT (2A4,7F8.3)		(Subroutine DATA)
	GG(2)	Remarks	
	THET75	Blade collective pitch at three-quarter radius	
	THET1C	Blade lateral cyclic pitch	
	THET1S	Blade longitudinal cyclic pitch	
	CONING	Blade coning angle	
	AZIMUTH	Blade azimuth angle (degrees)	
Data 22:	FORMAT (2A4,7F8.3)		(Subroutine DATA)
	GG(2)	Remarks	
	RPITCH	Collective pitch angle at blade root (degrees)	
	TWIST	Blade twist (degrees)	
Data 23:	FORMAT (2A4,10I5)		(Subroutine DATA)
	GG(2)	Remarks	
	KBLADE	Number of blades	
	ITWIST	Defines blade twist distribution	
Data 24:	FORMAT (2A4,10I5)		(Subroutine DATA)
	GG(2)	Remarks	
	NWAKPY	Flow separation considered for analysis = 1 yes = 0 no	

Table 4. Input Description (Continued).

NWAKHB	Rotor hub wake is generated for analysis = 1 yes = 0 no
NWAKSK	Blade shank wake is generated for analysis = 1 yes = 0 no
NWAKBL	Rotor blade wake is generated for analysis = 1 yes = 0 no

If (NWAKHB + NWAKSK + NWAKBL) \neq 0, use Data 25; otherwise, skip.

Data 25: FORMAT (2A4,15,2F8.3) (Subroutine DATA)

GG(2)	Remarks
NSPIRAL	Number of elements along one rotor wake spiral
SPIRAL	Number of rotor wake spirals
UWAKE	Induced rotor velocity = $\sqrt{1/2 C_T} \Omega R$

If NWAKPY = 1, use Data 26-27; otherwise, skip.

Data 26: FORMAT (2A4,10I5) (Subroutine DATA)

GG(2)	Remarks
NSTAG	Vortex layer from separation line is considered for analysis = 1 yes = 0 no
NVORT	Isolated vortex (branch wake) is considered for analysis = 1 yes = 0 no

Data 27: FORMAT (2A4,7F8.3) (Subroutine DATA)

GG(2)	Remarks
CSTAG	Intensity of the vortex layer from separation line
CVORT	Intensity of the isolated vortex (branch wake)

Table 4. Input Description (Continued).

Data 28: FORMAT (2A4,10I5) (Subroutine DATA)

GG(2)	Remarks
KPRINT(I)	Output control code
	= 1 yes
	= 0 no
	I = 1 specification of the problem
	I = 2 nodal numbering of surfaces and corner nodal numbering of elements
	I = 3 Cartesian coordinates of the nodes
	I = 4 Cartesian coordinates of the centroids of the element
	I = 5 coefficient matrix AA
	I = 6 source integrals
	I = 7 velocity potential distributions
	I = 8 perturbation velocity distributions
	I = 9 pressure coefficients
	I = 10 lift and induced drag coefficients

If NBODY1 = 1, use Data 29; otherwise, skip.

Data 29: FORMAT (2A4,10I5) (Subroutine DATA)

GG(2)	Remarks
NX(KS)	Number of elements in x direction
NY(KS)	Number of elements in y direction
KNSELE	Define the variation of element size
	= 0 define by input
	= 1 uniform along x direction
	= 2 quadratic along x direction
KNSSHP	Defines nose shape
	= 1; $r = R [\xi]^{1/2}$
	= 2; $r = R [\xi]^{1/3}$
	= 3; $r = R [\xi]^{1/4}$
KNSTYP	Defines nose type
	= 1 circular cross section
	= 2 elliptical cross section

Table 4. Input Description (Continued).

If NBODY2 = 1, use Data 30; otherwise, skip.

Data 30: FORMAT (2A4,10I5) (Subroutine DATA)

GG(2)	Remarks
NX(KS)	Number of elements in x direction
NY(KS)	Number of elements in y direction
KBDELE	Defines the variation of element size = 0 define by input = 1 uniform along x direction = 2 quadratic along x direction
KBDSHP	Defines the fuselage shape = 1 cylindrical
KBDTYP	Defines the fuselage type = 1 circular cross section = 2 elliptical cross section

If NBODY3 = 1, use Data 31; otherwise, skip.

Data 31: FORMAT (2A4,10I5) (Subroutine DATA)

GG(2)	Remarks
NX(KS)	Number of elements in x direction
NY(KS)	Number of elements in y direction
KTNELE	Defines the variation of element size = 0 define by input = 1 uniform along x direction = 2 quadratic along x direction
KTNSHP	Defines aft-body shape = 1; $r = R\sqrt{\xi}$ = 2; $r = R[\xi]^{1/3}$ = 3; $r = R[\xi]^{1/4}$
KTNTYP	Defines aft-body type = 1 circular cross section = 2 elliptical cross section

Table 4. Input Description (Continued).

If NPYLON = 1, use Data 32; otherwise, skip.

Data 32: FORMAT (2A4,10I5) (Subroutine DATA)

GG(2)	Remarks
NX(KS)	Number of elements in radial direction
NY(KS)	Number of elements in circumferential direction
KPYELE	Defines the variation of element size = 0 define by input = 1 uniform element distribution along radial and circumferential direction = 2 quadratic along radial direction with uniform element distribution in circumferential direction
KPYSHP	Defines pylon shape = 1 elliptical
KPYTYP	Defines pylon type = 1 elliptical

If NVTAIL = 1, use Data 33; otherwise, skip.

Data 33: FORMAT (2A4,10I5) (Subroutine DATA)

GG(2)	Remarks
NX(KS)	Number of elements in x direction
NY(KS)	Number of elements in y direction
KVTELE	Defines the variation of element size = 0 define by input = 1 uniform element distribution along axial and spanwise direction = 2 nonuniform (quadratic) element distribution along axial and spanwise direction = 3 quadratic along spanwise direction with uniform element distribution in axial direction = 4 quadratic along axial direction with uniform element distribution in spanwise direction

Table 4. Input Description (Continued).

KVTSHP

Defines vertical tail shape
 = 1 circular biconvex airfoil

$$Z = \pm \left\{ \left[\frac{\left(\frac{c}{2}\right)^2 + \tau_{\max}^2}{2 \tau_{\max}} \right]^2 - \left[X - \frac{X_{LE} + X_{TE}}{2} \right]^2 - \left[\frac{\left(\frac{c}{2}\right)^2 - \tau_{\max}^2}{2 \tau_{\max}} \right] \right\}^{1/2}$$

= 2 define by following equation

$$Z = \pm \tau \left\{ \sqrt{\frac{X}{X_{TE} - X_{LE}}} \left(1 - \frac{X}{X_{TE} - X_{LE}} \right) \sqrt{1 - \frac{Y}{S}} \right\}$$

= 3 define by following equation

$$Z = \pm (4\tau) (2C_o) \left\{ \left(\frac{X}{X_{TE} - X_{LE}} \right) \left(1 - \frac{X}{X_{TE} - X_{LE}} \right) \sqrt{1 - \frac{Y}{S}} \right\}$$

Table 4. Input Description (Continued).

KVTSHP (Cont.)

where

c = chord length

X_{LE} = x components of sectional leading edge

X_{TE} = x components of sectional trailing edge

y = spanwise location of the section

S = half span

$$\bar{\tau} = \tau_{\max} \left(\frac{3}{4} \sqrt{3} \right) (2 C_o)$$

C_o = root chord

KVTYP

Define vertical tail type
= 1

If NSHAFT = 1, use Data 34; otherwise, skip.

Data 34: FORMAT (2A4,10I5)

(Subroutine DATA)

GG(2)

Remarks

NX(KS)

Number of elements in shaft direction

NY(KS)

Number of elements in circumferential direction

KSHELE

Defines the variation of element size
= 0 define by input
= 1 uniform element distribution

KSHSHP

Defines rotor shaft shape
= 1 cylindrical

KSHTYP

Defines rotor shaft type
= 1 circular cross section

Table 4. Input Description (Continued).

If NHUB = 1, use Data 35; otherwise, skip.

Data 35: FORMAT (2A4,10I5) (Subroutine DATA)

GG(2)	Remarks
NX(KS)	Number of elements in x direction
NY(KS)	Number of elements in circumferential direction
KHBELE	Defines the variation of element size = 0 define by input = 1 uniform element distribution
KHBSHP	Defines rotor hub shape = 1 elliptical
KHB TYP	Defines rotor hub type = 1 elliptical

If NSHANK = 1, use Data 36; otherwise, skip.

Data 36: FORMAT (2A4,10I5) (Subroutine DATA)

GG(2)	Remarks
NX(KS)	Number of elements in shank direction
NY(KS)	Number of elements in circumferential direction
KSKELE	Defines the variation of element size = 0 define by input = 1 uniform element distribution
KSKSHP	Defines blade shank shape = 1 cylindrical
KSK TYP	Defines blade shank type = 1 circular cross section

If NBLADE = 1, use Data 37; otherwise, skip.

Data 37: FORMAT (2A4,10I5) (Subroutine DATA)

GG(2)	Remarks
NX(KS)	Number of elements in x direction

Table 4. Input Description (Continued).

NY(KS)	Number of elements in y direction
KBLELE	Defines the variation of element size = 0 define by input = 1 uniform element distribution = 2 nonuniform (quadratic) element distribution
KBLSHP	Defines rotor blade shape = 1 circular biconvex airfoil

$$Z = \pm \left\{ \begin{array}{l} \left[\frac{\left(\frac{c}{2}\right)^2 + \tau_{\max}^2}{2 \tau_{\max}} \right]^2 - \left[X - \frac{X_{LE} + X_{TE}}{2} \right]^2 \\ - \frac{\left(\frac{c}{2}\right)^2 - \tau_{\max}^2}{2 \tau_{\max}} \end{array} \right\}^{1/2}$$

= 2 define by following equation

$$Z = \pm \tau \left\{ \begin{array}{l} \sqrt{\left(\frac{X}{X_{TE} - X_{LE}}\right)} \\ \left(1 - \frac{X}{X_{TE} - X_{LE}}\right) \sqrt{1 - \frac{r}{R}} \end{array} \right\}$$

= 3 define by following equation

$$Z = \pm (4\tau) (2 C_o) \left\{ \begin{array}{l} \left(\frac{X}{X_{TE} - X_{LE}}\right) \\ \left(1 - \frac{X}{X_{TE} - X_{LE}}\right) \sqrt{1 - \frac{r}{R}} \end{array} \right\}$$

Table 4. Input Description (Continued).

KBLSHP (Cont.)

where

c = blade chord

X_{LE} = x components of blade leading edge

X_{TE} = x components of blade trailing edge

r = radial location

R = rotor radius

$$\bar{\tau} = \tau_{\max} \left(\frac{3}{4} \sqrt{3} \right) (2 C_o)$$

C_o = blade root chord

KBLTYP

Defines rotor blade type
= 1

If NPYLON = 1, use Data 38-39; otherwise, skip.

Data 38: FORMAT (10F8.3)

(Subroutine COODPT)

HCSI(IX)

Normalized x direction nodal line coordinates
[Note that HCSI(IX), IX = 1, NXP is implied with NXP denoting the number of nodal lines along the x direction]

Data 39: FORMAT (10F8.3)

(Subroutine COODPT)

HETA(IY)

Normalized y direction nodal line coordinates
[Note that HETA(IY), = 1, NYP is implied with NYP denoting the number of nodal lines along the y direction]

If NVTAIL = 1, use Data 40-41; otherwise, skip.

Data 40: FORMAT (10F8.3)

(Subroutine COODPT)

HCSI(IX)

Normalized x direction nodal line coordinates
[Note that HCSI(IX), IX = 1, NXP is implied with NXP denoting the number of nodal lines along the x direction]

Table 4. Input Description (Continued).

Data 41: FORMAT (10F8.3) (Subroutine COODPT)

HETA(IY) Normalized y direction nodal line coordinates
 [Note that HETA(IY), IY = 1, NYP is implied
 with NYP denoting the number of nodal lines
 along the y direction]

If NSHAFT = 1, use Data 42-43; otherwise, skip.

Data 42: FORMAT (10F8.3) (Subroutine COODPT)

HCSI(IX) Normalized x direction nodal line coordinates
 [Note that HCSI(IX), IX = 1, NXP is implied
 with NXP denoting the number of nodal lines
 along the x direction]

Data 43: FORMAT (10F8.3) (Subroutine COODPT)

HETA(IY) Normalized y direction nodal line coordinates
 [Note that HETA(IY), IY = 1, NYP is implied
 with NYP denoting the number of nodal lines
 along the y direction]

If NHUB = 1, use Data 44-45; otherwise, skip.

Data 44: FORMAT (10F8.3) (Subroutine COODPT)

HCSI(IX) Normalized x direction nodal line coordinates
 [Note that HCSI(IX), IX = 1, NXP is implied
 with NXP denoting the number of nodal lines
 along the x direction]

Data 45: FORMAT (10F8.3) (Subroutine COODPT)

HETA(IY) Normalized y direction nodal line coordinates
 [Note that HETA(IY), IY = 1, NYP is implied
 with NYP denoting the number of nodal lines
 along the y direction]

If NSHANK = 1, use Data 46-47; otherwise, skip.

Data 46: FORMAT (10F8.3) (Subroutine COODPT)

HCSI(IX) Normalized x direction nodal line coordinates
 [Note that HCSI(IX), IX = 1, NXP is implied
 with NXP denoting the number of nodal lines
 along the x direction]

Table 4. Input Description (Continued).

Data 47: FORMAT (10F8.3) (Subroutine COODPT)

HETA(IY) Normalized y direction nodal line coordinates
 [Note that HETA(IY), IY = 1, NYP is implied
 with NYP denoting the number of nodal lines
 along the y direction]

If NBLADE = 1, use Data 48-49; otherwise, skip.

Data 48: FORMAT (10F8.3) (Subroutine COODPT)

HCSI(IX) Normalized x direction nodal line coordinates
 [Note that HCSI(IX), IX = 1, NXP is implied
 with NXP denoting the number of nodal lines
 along the x direction]

Data 49: FORMAT (10F8.3) (Subroutine COODPT)

HETA(IY) Normalized y direction nodal line coordinates
 [Note that HETA(IY), IY = 1, NYP is implied
 with NYP denoting the number of nodal lines
 along the y direction]

If KREAD = 1, use Data 50; otherwise, skip.

Data 50: FORMAT (3E12.4) (Subroutine COODPT)

XK(K,INODE) The nodal coordinates in global Cartesian system
 [Note that (XK(K,INODE), K = 1,3), INODE = 1,
 NNODE) is implied]

If NWAKPY = 1 and NSTAG = 1, use Data 51-54; otherwise, skip.

Data 51: FORMAT (3E12.4) (Subroutine COODPT)

YPP(K)

Data 52: FORMAT (3E12.4)

YPM(K)

Data 53: FORMAT (3E12.4)

YMP(K)

Data 54: FORMAT (3E12.4)

YMM(K)

The separation wake nodal coordinates
 in global Cartesian system [Note that
 K=1,3 is implied]

Table 4. Input Description (Concluded).

If NWAKPY = 1 and NVORT = 1, use Data 55-58; otherwise, skip.

Data 55: FORMAT (3E12.4)	}	(Subroutine COEFF)
YPP(K)		
Data 56: FORMAT (3E12.4)		
YPM(K)		
Data 57: FORMAT (3E12.4)	}	The isolated vortex branch wake nodal coordinates in global Cartesian system [Note that K=1,3 is implied]
YMP(K)		
Data 58: FORMAT (3E12.4)		
YMM(K)		

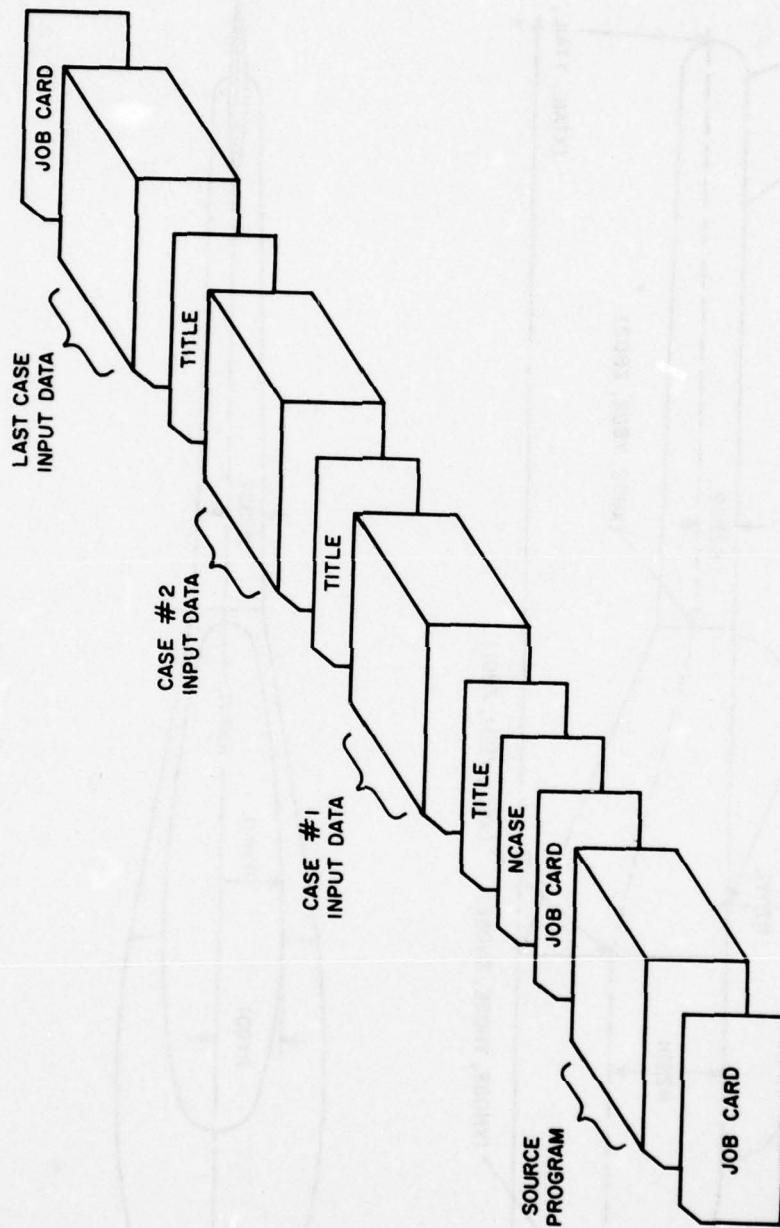


Figure 5. Program SHAPES Data Setup.

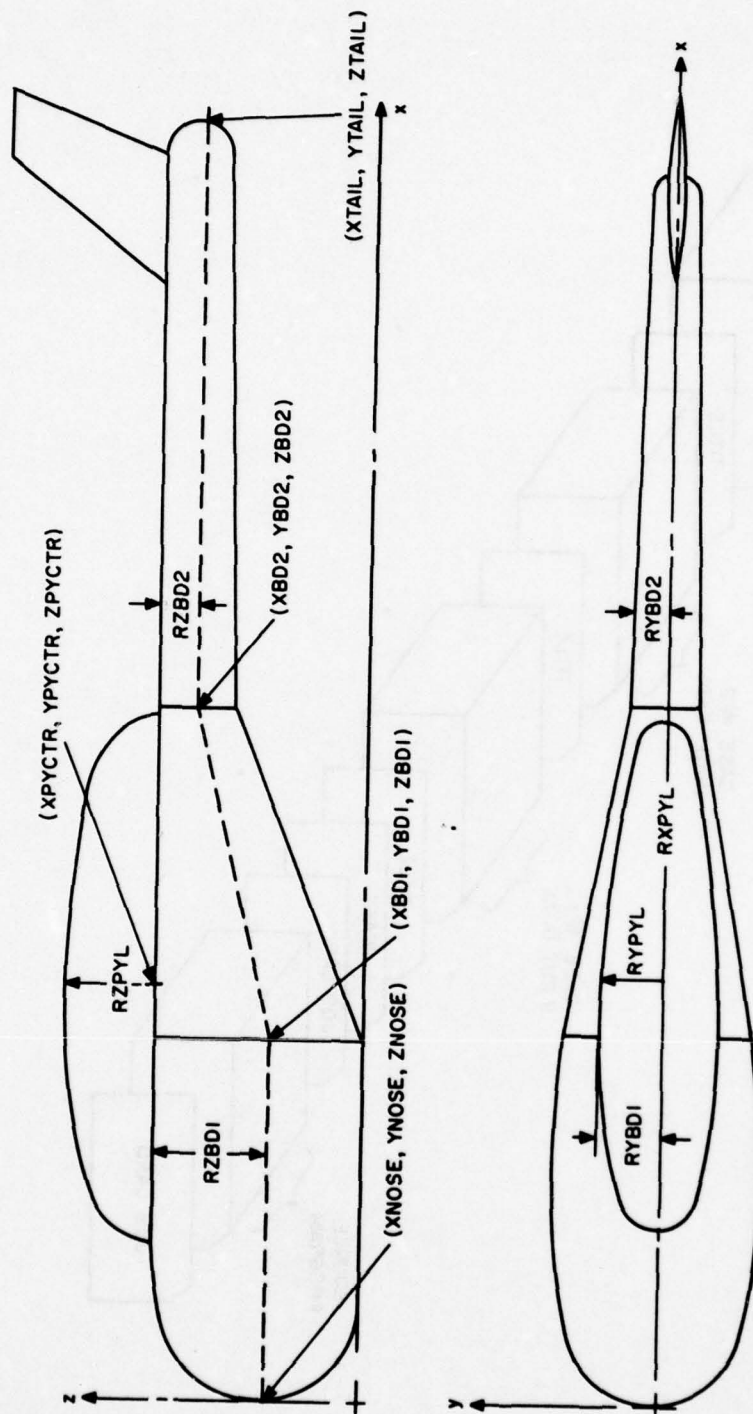


Figure 6. Basic Geometric Inputs for Helicopter Fuselage.

4.2 ERROR CODES

To insure proper data are read in and to minimize unnecessary computer time, SHAPES contains several debugging statements at specified checkpoints. If an inconsistency among input data or violation of the input specification is detected, an error code will be printed and the computer run terminated. Table 5 summarizes these error codes.

Table 5. Error Codes Summary.

<u>Code Number</u>	<u>Description</u>
100	Mach number is greater than 1 (Present SOUSSA is a subsonic program) (DATA)
200	$NS \neq (NPYLON + NVTAIL)*MULTY + (NBODY1 + NBODY2 + (NBODY3)*MULT*MULTY + (NSHAFT*MULTY + (NHUB*MULT*MULTY* + KBLADE*(NSHANK + NBLADE*MULT)$ (DATA)
300	Number of elements in the x direction of a sub-surface exceeds the maximum permissible value. This is limited by the storage capacity of the computer. The user has the option of changing the value of NXMAX and NYMAX defined in the main program. (DATA)
400	Same as code number 300 except for the y direction. (DATA)
500	Total number of elements required for analysis exceeds the maximum limit specified in the main program. (DATA)
IER	IBM subroutine GELG provides error code = 0 no error = 1 no result is obtained because the number of equations is less than 1 or the pivoting element at any elimination step equals 0 = N warning is indicated because of a possible loss of significant figures at elimination step N+1 where the pivoting element is less than equal to the specified tolerance times the magnitude of the greatest element of matrix A (DATA)

SECTION 5

PROGRAM OUTPUT

In Program SHAPES several output options are available and these are briefly summarized here. The amount of output required to be printed out is controlled by Data 28, described in Subsection 4.1. Among the information available is the specification of the problem defined by the user and the basic geometric inputs to the problem, i.e., overall dimensions and shapes used to model a helicopter configuration. In addition, the nodal numbering of the aerodynamic breakup as well as the Cartesian coordinate location of the nodal points and the centroid of each aerodynamic panel can be requested. Furthermore, the coefficient matrix and source distribution can be output. Also, the perturbation potential, velocity, and the pressure coefficient are available as outputs. Finally, the lift and induced drag can be requested.

SECTION 6
PROGRAM LISTING

SAMPLE CASE 1:
SINGLE-BLADE ROTOR

Data Input

```

3
PROGRAM SHAPES
HUB PYLON FLOW SEPARATION
SINGLE ROTOR BLADE PROFILE
NREAD 0
0 0 0 0 0 0 0 0 0 0 1
00 0 0 0 0 0 0 0 0 0 1
000 0 0 0 0 0 0 0 0 0 1
UMACH 0.000 395.030
ALFA 0.000 1.000
SOFD 17.000 2.310 0.000 1.000 0.000 0.300 0.000
TWTZ 0.000 0.000 0.000 1.000 0.000 0.000 0.000
NPITCH 10.000 0.000
KBLADE 1 1
NWARC 0 0 0 1
SPIAL 10 1.000 20.000
KPRINT 1 1 1 1 0 1 1 1 1 1
NPROT 3 7 2 1 1
DATA
MELEN = 02
IS= 1 NV= 3 NY= 7 NYV= 21 ISFACE= 1 NT= 0 KNOPPL= 1 KNAKES= 1 KROTORS= 1
IS= 2 NV= 3 NY= 7 NYV= 21 ISFACE= 2 NT= 21 KNURML= -1 KNAKES= 1 KROTORS= 1
PREPDS
NWCDE = 06

```

Specifications of the Problem

```

FOR PRT 124
ND= 3
NT= 7

FOR SPT 20
NS= 3
NV= 7

MELEN= 02
KPRINT= 1
KPRINT= 2

```

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X, Y, and Z Coordinates of the Nodes

NODE=	X	Y	Z
1	0.00000	2.33000	0.00000
2	.12025	2.33000	-.01163
3	.47803	2.33000	-.06234
4	1.06448	2.33000	-.19941
5	0.00000	6.35469	0.00000
6	.12025	6.35469	-.01163
7	.47803	6.35469	-.06234
8	1.06448	6.35469	-.19941
9	0.00000	9.76020	0.00000
10	.12025	9.76020	-.01163
11	.47803	9.76020	-.06234
12	1.06448	9.76020	-.19941
13	0.00000	12.54553	0.00000
14	.12025	12.54553	-.01163
15	.47803	12.54553	-.06234
16	1.06448	12.54553	-.19941
17	0.00000	14.71367	0.00000
18	.12025	14.71367	-.01163
19	.47803	14.71367	-.06234
20	1.06448	14.71367	-.19941
21	0.00000	16.26163	0.00000
22	.12025	16.26163	-.01163
23	.47803	16.26163	-.06234
24	1.06448	16.26163	-.19941
25	0.00000	17.19041	0.00000
26	.12025	17.19041	-.01163
27	.47803	17.19041	-.06234
28	1.06448	17.19041	-.19941
29	0.00000	17.50000	0.00000
30	.11028	17.50000	-.02216
31	.47310	17.50000	-.06862
32	1.06448	17.50000	-.19941
33	.11630	2.33000	-.03269
34	.46818	2.33000	-.11491
35	.11630	6.35469	-.03269
36	.46818	6.35469	-.11491
37	.11630	9.76020	-.03269
38	.46818	9.76020	-.11491
39	.11630	12.54553	-.03269
40	.46818	12.54553	-.11491
41	.11630	14.71367	-.03269
42	.46818	14.71367	-.11491
43	.11630	16.26163	-.03269
44	.46818	16.26163	-.11491
45	.11630	17.19041	-.03269
46	.46818	17.19041	-.11491

X, Y, and Z Coordinates of the Centroid of Aerodynamic Panels

ELEM=	XPC	YPC	ZPC
1	.06012	4.34235	-.00581
2	.29914	4.34235	-.03698
3	.77126	4.34235	-.13087
4	.06012	8.05745	-.00581
5	.29914	8.05745	-.03698
6	.77126	8.05745	-.13087
7	.06012	11.15337	-.00581
8	.29914	11.15337	-.03698
9	.77126	11.15337	-.13087
10	.06012	13.63010	-.00581
11	.29914	13.63010	-.03698
12	.77126	13.63010	-.13087
13	.06012	15.48765	-.00581
14	.29914	15.48765	-.03698
15	.77126	15.48765	-.13087
16	.06012	16.72602	-.00581
17	.29914	16.72602	-.03698
18	.77126	16.72602	-.13087
19	.05963	17.34520	-.00845
20	.29741	17.34520	-.04619
21	.77003	17.34520	-.13744
22	.05815	4.34235	-.01634
23	.29224	4.34235	-.07380
24	.76633	4.34235	-.15716
25	.05815	8.05745	-.01634
26	.29224	8.05745	-.07380
27	.76633	8.05745	-.15716
28	.05815	11.15337	-.01634
29	.29224	11.15337	-.07380
30	.76633	11.15337	-.15716
31	.05815	13.63010	-.01634
32	.29224	13.63010	-.07380
33	.76633	13.63010	-.15716
34	.05815	15.48765	-.01634
35	.29224	15.48765	-.07380
36	.76633	15.48765	-.15716
37	.05815	16.72602	-.01634
38	.29224	16.72602	-.07380
39	.76633	16.72602	-.15716
40	.05864	17.34520	-.01371
41	.29397	17.34520	-.06459
42	.76756	17.34520	-.15059

Nodal Numbering for Surfaces

FOR SURFACE 24							
1	5	9	13	17	21	25	29
2	6	10	14	18	22	26	30
3	7	11	15	19	23	27	31
4	8	12	16	20	24	28	32

FOR SURFACE 25							
1	5	9	13	17	21	25	29
33	35	37	39	41	43	45	30
34	36	38	40	42	44	46	31
4	8	12	16	20	24	28	32

Nodal Numbering for Elements

ELEM	++	+-	-+	--
1	6	2	5	1
2	7	3	6	2
3	8	4	7	3
4	10	6	3	5
5	11	7	10	6
6	12	8	11	7
7	14	10	13	9
8	15	11	14	10
9	16	12	15	11
10	18	14	17	13
11	19	15	18	14
12	20	16	19	15
13	22	18	21	17
14	23	19	22	18
15	24	20	23	19
16	26	22	25	21
17	27	23	26	22
18	28	24	27	23
19	30	26	29	25
20	31	27	30	26
21	32	28	31	27
22	33	35	1	5
23	34	36	3	35
24	4	8	34	36
25	35	37	5	9
26	36	38	35	37
27	8	12	36	38
28	37	39	9	13
29	38	40	27	39
30	12	16	38	40
31	39	41	13	17
32	40	42	39	41
33	16	20	40	42
34	41	43	17	21
35	42	44	41	43
36	20	24	42	44
37	43	45	21	25
38	44	46	43	45
39	24	28	44	46
40	45	50	25	29
41	46	31	45	30
42	28	32	46	31

The Distribution of the Source

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THE DISTRIBUTION OF SOURCE

FOR SUBSURFACE 24						
-0.5455E+01	-0.98095E+01	-0.13011E+02	-0.16471E+02	-0.10312E+02	-0.10733E+02	-0.10910E+02
-0.27403E+01	-0.62637E+01	-0.14607E+01	-0.77902E+01	-0.67406E+01	-0.88877E+01	-0.53715E+01
0.40619E+01	0.91102E+01	0.12643E+02	0.15465E+02	0.17400E+02	0.17995E+02	0.32096E+01
FOR SUBSURFACE 25						
-0.6686E+01	-0.10991E+02	-0.15012E+02	-0.16247E+02	-0.26509E+02	-0.21201E+02	-0.11707E+02
-0.64065E+01	-0.85095E+01	-0.11727E+02	-0.14336E+02	-0.16200E+02	-0.17000E+02	-0.97150E+01
0.33064E+01	0.30461E+01	0.72062E+01	0.11639E+02	0.11950E+02	0.12013E+02	0.61040E+01

The Distribution of the Velocity Potential

THE DISTRIBUTION OF THE VELOCITY POTENTIAL

FOR SUBSURFACE 24						
0.57703E+02	0.12070E+03	0.13220E+03	0.13100E+03	0.12223E+03	0.16029E+03	0.94956E+02
0.11366E+03	0.14807E+03	0.15739E+03	0.16143E+03	0.15467E+03	0.13902E+03	0.11436E+03
0.11917E+03	0.19291E+03	0.17375E+03	0.18060E+03	0.17500E+03	0.15953E+03	0.12810E+03
FOR SUBSURFACE 25						
0.6197E+02	0.64167E+02	0.59452E+02	0.47274E+02	0.29003E+02	0.10253E+02	0.27677E+02
0.49022E+02	0.40460E+02	0.39531E+02	0.23127E+02	0.34100E+01	0.62300E+01	0.10610E+02
0.44051E+02	0.42059E+02	0.30273E+02	0.10092E+02	0.70572E+01	0.13457E+02	0.61021E+01

Pressure Distribution

THE DISTRIBUTION OF CP						
FOR SUBSURFACE 24						
-.00766E+00	-.13091E+01	-.14902E+01	-.25306E+01	-.30028E+01	-.20658E+01	-.43030E+01
-.12650E+01	-.19535E+00	-.20234E+00	-.36062E+00	-.41152E+00	-.30549E+00	-.21216E+00
.22533E+00	.35270E+00	.51106E+00	.65003E+00	.73322E+00	.69717E+00	.20360E+00
FOR SUBSURFACE 25						
.02564E+00	.12750E+01	.10370E+01	.23371E+01	.26643E+01	.25063E+01	.52100E+01
.01057E+01	.13220E+00	.19753E+00	.25337E+00	.27727E+00	.24046E+00	.07001E+01
-.26629E+00	-.30151E+00	-.16490E+00	-.69930E+00	-.79643E+00	-.76640E+00	-.35074E+00

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SAMPLE CASE 2:
XH-51A HELICOPTER ROTOR

Data Input

```

PROGRAM SHAPES
RHO FT/LB FLOW SEPARATION
FOUR BLADED HELICOPTER ROTOR
KREAD 0
*
*
***
UNACP 0.000 399.137
ALFA 0.000 0.000
ROTOR 17.500 2.530
THETYS 0.000 0.000 0.000 1.065 0.000 0.000 0.000 .000
RPITCH 10.000 7.000
KBLADE 0 1
NHART 0 0 0 1
SPIRAL 10 3.000 30.000
RPRINT 1 1 1 1 0 1 1 1 1 1
NROTOR 0 0 2 1 1

DATA

HELEN # 200

IS= 1 NX= 0 NY= 0 NXY= 25 ISPACE= 1 NY= 0 KNORML= 1 KWAKES= 1 KROTCS= 1
IS= 2 NX= 0 NY= 0 NXY= 25 ISPACE= 2 NY= 25 KNORML= -1 KWAKES= 1 KROTCS= 1
IS= 3 NX= 0 NY= 0 NXY= 25 ISPACE= 3 NY= 50 KNORML= 1 KWAKES= 1 KROTCS= 1
IS= 4 NX= 0 NY= 0 NXY= 25 ISPACE= 4 NY= 75 KNORML= -1 KWAKES= 1 KROTCS= 1
IS= 5 NX= 0 NY= 0 NXY= 25 ISPACE= 5 NY= 100 KNORML= 1 KWAKES= 1 KROTCS= 1
IS= 6 NX= 0 NY= 0 NXY= 25 ISPACE= 6 NY= 125 KNORML= -1 KWAKES= 1 KROTCS= 1
IS= 7 NX= 0 NY= 0 NXY= 25 ISPACE= 7 NY= 150 KNORML= 1 KWAKES= 1 KROTCS= 1
IS= 8 NX= 0 NY= 0 NXY= 25 ISPACE= 8 NY= 175 KNORML= -1 KWAKES= 1 KROTCS= 1

PREPRO
MODE= 220

```

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Specifications of the Problem

FOR PART 24
NX= 5
NY= 5

FOR PART 25
NX= 5
NY= 5

FOR PART 27
NX= 5
NY= 5

FOR PART 28
NX= 5
NY= 5

FOR PART 30
NX= 5
NY= 5

FOR PART 31
NX= 5
NY= 5

FOR PART 33
NX= 5
NY= 5

FOR PART 34
NX= 5
NY= 5

NELEM=200

KSYMMY= 0
KSYMMZ= 0

X, Y, and Z Coordinates of the Nodes

NOCE=	X	Y	Z
1	0.00000	2.33000	0.00000
2	.04335	2.33000	-.00388
3	.17300	2.33000	-.01758
4	.38781	2.33000	-.04726
5	.68587	2.33000	-.10309
6	1.06448	2.33000	-.19941
7	0.00000	7.79120	0.00000
8	.04335	7.79120	-.00388
9	.17300	7.79120	-.01758
10	.38781	7.79120	-.04726
11	.68587	7.79120	-.10309
12	1.06448	7.79120	-.19941
13	0.00000	12.03880	0.00000
14	.04335	12.03880	-.00388
15	.17300	12.03880	-.01758
16	.38781	12.03880	-.04726
17	.68587	12.03880	-.10309
18	1.06448	12.03880	-.19941
19	0.00000	15.07280	0.00000
20	.04335	15.07280	-.00388
21	.17300	15.07280	-.01758
22	.38781	15.07280	-.04726
23	.68587	15.07280	-.10309
24	1.06448	15.07280	-.19941
25	0.00000	16.89320	0.00000
26	.04335	16.89320	-.00388
27	.17300	16.89320	-.01758
28	.38781	16.89320	-.04726
29	.68587	16.89320	-.10309
30	1.06448	16.89320	-.19941
31	0.00000	17.50000	0.00000
32	.04258	17.50000	-.00798
33	.17032	17.50000	-.03190
34	.38321	17.50000	-.07179
35	.68127	17.50000	-.12762
36	1.06448	17.50000	-.19941
37	.04131	2.33000	-.01207
38	.16763	2.33000	-.04623
39	.37862	2.33000	-.09632
40	.67667	2.33000	-.15215
41	.04181	7.79120	-.01207
42	.16763	7.79120	-.04623
43	.37862	7.79120	-.09632
44	.67667	7.79120	-.15215
45	.04181	12.03880	-.01207
46	.16763	12.03880	-.04623
47	.37862	12.03880	-.09632
48	.67667	12.03880	-.15215
49	.04181	15.07280	-.01207
50	.16763	15.07280	-.04623
51	.37862	15.07280	-.09632
52	.67667	15.07280	-.15215
53	.04181	16.89320	-.01207
54	.16763	16.89320	-.04623
55	.37862	16.89320	-.09632
56	.67667	16.89320	-.15215
57	-2.33000	.00000	0.00000
58	-2.33000	.04335	-.00388
59	-2.33000	.17300	-.01758
60	-2.33000	.38781	-.04726
61	-2.33000	.68587	-.10309
62	-2.33000	1.06448	-.19941
63	-7.79120	.00000	0.00000
64	-7.79120	.04335	-.00388
65	-7.79120	.17300	-.01758
66	-7.79120	.38781	-.04726

67	-7.79120	.68587	-.10309
68	-7.79120	1.06448	-.19941
69	-12.03880	.00000	0.00000
70	-12.03880	.04335	-.00388
71	-12.03880	.17300	-.01758
72	-12.03880	.38781	-.04726
73	-12.03880	.68587	-.10309
74	-12.03880	1.06448	-.19941
75	-15.07280	.00000	0.00000
76	-15.07280	.04335	-.00388
77	-15.07280	.17300	-.01758
78	-15.07280	.38781	-.04726
79	-15.07280	.68587	-.10309
80	-15.07280	1.06448	-.19941
81	-16.89320	.00000	0.00000
82	-16.89320	.04335	-.00388
83	-16.89320	.17300	-.01758
84	-16.89320	.38781	-.04726
85	-16.89320	.68587	-.10309
86	-16.89320	1.06448	-.19941
87	-17.50000	.00000	0.00000
88	-17.50000	.04258	-.00798
89	-17.50000	.17032	-.03190
90	-17.50000	.38321	-.07179
91	-17.50000	.68127	-.12762
92	-17.50000	1.06448	-.19941
93	-2.33000	.04131	-.01207
94	-2.33000	.16763	-.04623
95	-2.33000	.37862	-.09632
96	-2.33000	.67667	-.15215
97	-7.79120	.04181	-.01207
98	-7.79120	.16763	-.04623
99	-7.79120	.37862	-.09632
100	-7.79120	.67667	-.15215
101	-12.03880	.04181	-.01207
102	-12.03880	.16763	-.04623
103	-12.03880	.37862	-.09632
104	-12.03880	.67667	-.15215
105	-15.07280	.04181	-.01207
106	-15.07280	.16763	-.04623
107	-15.07280	.37862	-.09632
108	-15.07280	.67667	-.15215
109	-16.89320	.04181	-.01207
110	-16.89320	.16763	-.04623
111	-16.89320	.37862	-.09632
112	-16.89320	.67667	-.15215
113	-.00000	-2.33000	0.00000
114	-.04335	-2.33000	-.00388
115	-.17300	-2.33000	-.01758
116	-.38781	-2.33000	-.04726
117	-.68587	-2.33000	-.10309
118	-1.06448	-2.33000	-.19941
119	-.00000	-7.79120	0.00000
120	-.04335	-7.79120	-.00388
121	-.17300	-7.79120	-.01758
122	-.38781	-7.79120	-.04726
123	-.68587	-7.79120	-.10309
124	-1.06448	-7.79120	-.19941
125	-.00000	-12.03880	0.00000
126	-.04335	-12.03880	-.00388
127	-.17300	-12.03880	-.01758
128	-.38781	-12.03880	-.04726
129	-.68587	-12.03880	-.10309
130	-1.06448	-12.03880	-.19941
131	-.00000	-15.07280	0.00000
132	-.04335	-15.07280	-.00388
133	-.17300	-15.07280	-.01758
134	-.38781	-15.07280	-.04726
135	-.68587	-15.07280	-.10309
136	-1.06448	-15.07280	-.19941
137	-.00000	-16.89320	0.00000
138	-.04335	-16.89320	-.00388
139	-.17300	-16.89320	-.01758
140	-.38781	-16.89320	-.04726

141	-.63587	-13.89320	-.10309
142	-1.06448	-16.89320	-.19941
143	-.00000	-17.50000	0.00000
144	-.04253	-17.50000	-.00792
145	-.17032	-17.50000	-.03190
146	-.38321	-17.50000	-.07179
147	-.68127	-17.50000	-.12762
148	-1.06448	-17.50000	-.19941
149	-.04181	-2.33000	-.01207
150	-.16763	-2.33000	-.04623
151	-.37862	-2.33000	-.09632
152	-.67667	-2.33000	-.15215
153	-.04181	-7.79120	-.01207
154	-.16763	-7.79120	-.04623
155	-.37862	-7.79120	-.09632
156	-.67667	-7.79120	-.15215
157	-.04181	-12.03880	-.01207
158	-.16763	-12.03880	-.04623
159	-.37862	-12.03880	-.09632
160	-.67667	-12.03880	-.15215
161	-.04181	-15.07280	-.01207
162	-.16763	-15.07280	-.04623
163	-.37862	-15.07280	-.09632
164	-.67667	-15.07280	-.15215
165	-.04181	-16.89320	-.01207
166	-.16763	-16.89320	-.04623
167	-.37862	-16.89320	-.09632
168	-.67667	-16.89320	-.15215
169	2.33000	-.00000	0.00000
170	2.33000	-.04335	-.00388
171	2.33000	-.17300	-.01752
172	2.33000	-.38781	-.04722
173	2.33000	-.68587	-.10309
174	2.33000	-1.06448	-.19941
175	7.79120	-.00000	0.00000
176	7.79120	-.04335	-.00388
177	7.79120	-.17300	-.01752
178	7.79120	-.38781	-.04722
179	7.79120	-.68587	-.10309
180	7.79120	-1.06448	-.19941
181	12.03880	-.00000	0.00000
182	12.03880	-.04335	-.00388
183	12.03880	-.17300	-.01752
184	12.03880	-.38781	-.04722
185	12.03880	-.68587	-.10309
186	12.03880	-1.06448	-.19941
187	15.07280	-.00000	0.00000
188	15.07280	-.04335	-.00388
189	15.07280	-.17300	-.01752
190	15.07280	-.38781	-.04722
191	15.07280	-.68587	-.10309
192	15.07280	-1.06448	-.19941
193	16.89320	-.00000	0.00000
194	16.89320	-.04335	-.00388
195	16.89320	-.17300	-.01752
196	16.89320	-.38781	-.04722
197	16.89320	-.68587	-.10309
198	16.89320	-1.06448	-.19941
199	17.50000	-.00000	0.00000
200	17.50000	-.04258	-.00792
201	17.50000	-.17032	-.03190
202	17.50000	-.38321	-.07179
203	17.50000	-.68127	-.12762
204	17.50000	-1.06448	-.19941
205	2.33000	-.04181	-.01207
206	2.33000	-.16763	-.04623
207	2.33000	-.37862	-.09632
208	2.33000	-.67667	-.15215
209	7.79120	-.04181	-.01207
210	7.79120	-.16763	-.04623
211	7.79120	-.37862	-.09632
212	7.79120	-.67667	-.15215
213	12.03880	-.04181	-.01207
214	12.03880	-.16763	-.04623

215	12.03880	-.37862	-.09632
216	12.03880	-.67667	-.15215
217	15.07280	-.04131	-.01207
218	15.07280	-.16753	-.04623
219	15.07280	-.37862	-.09632
220	15.07280	-.67667	-.15215
221	16.89320	-.04131	-.01207
222	16.89320	-.16753	-.04623
223	16.89320	-.37862	-.09632
224	16.89320	-.67667	-.15215

X, Y, and Z Coordinates of the Centroid of Aerodynamic Panels

ELEM#	XPC	YPC	ZPC
1	.02167	5.06060	-.00194
2	.10817	5.06060	-.01073
3	.28041	5.06060	-.03242
4	.53684	5.06060	-.07517
5	.87517	5.06060	-.15125
6	.02167	9.91500	-.00194
7	.10817	9.91500	-.01073
8	.28041	9.91500	-.03242
9	.53684	9.91500	-.07517
10	.87517	9.91500	-.15125
11	.02167	13.55580	-.00194
12	.10817	13.55580	-.01073
13	.28041	13.55580	-.03242
14	.53684	13.55580	-.07517
15	.87517	13.55580	-.15125
16	.02167	15.98300	-.00194
17	.10817	15.98300	-.01073
18	.28041	15.98300	-.03242
19	.53684	15.98300	-.07517
20	.87517	15.98300	-.15125
21	.02148	17.19660	-.00296
22	.10731	17.19660	-.01934
23	.27859	17.19660	-.04213
24	.53454	17.19660	-.08744
25	.87403	17.19660	-.15738
26	.02091	5.06060	-.00604
27	.10472	5.06060	-.02915
28	.27313	5.06060	-.07127
29	.52765	5.06060	-.12423
30	.87058	5.06060	-.17578
31	.02091	9.91500	-.00604
32	.10472	9.91500	-.02915
33	.27313	9.91500	-.07127
34	.52765	9.91500	-.12423
35	.87058	9.91500	-.17578
36	.02091	13.55580	-.00604
37	.10472	13.55580	-.02915
38	.27313	13.55580	-.07127
39	.52765	13.55580	-.12423
40	.87058	13.55580	-.17578
41	.02091	15.98300	-.00604
42	.10472	15.98300	-.02915
43	.27313	15.98300	-.07127
44	.52765	15.98300	-.12423
45	.87058	15.98300	-.17578
46	.02110	17.19660	-.00901
47	.10559	17.19660	-.02455
48	.27455	17.19660	-.06156
49	.52994	17.19660	-.11197
50	.87173	17.19660	-.16964
51	-5.06060	.02167	-.00194
52	-5.06060	.10817	-.01073
53	-5.06060	.28041	-.03242
54	-5.06060	.53684	-.07517
55	-5.06060	.87517	-.15125
56	-9.91500	.02167	-.00194
57	-9.91500	.10817	-.01073
58	-9.91500	.28041	-.03242
59	-9.91500	.53684	-.07517
60	-9.91500	.87517	-.15125
61	-13.55580	.02167	-.00194
62	-13.55580	.10817	-.01073
63	-13.55580	.28041	-.03242
64	-13.55580	.53684	-.07517
65	-13.55580	.87517	-.15125
66	-15.98300	.02167	-.00194
67	-15.98300	.10817	-.01073
68	-15.98300	.28041	-.03242
69	-15.98300	.53684	-.07517
70	-15.98300	.87517	-.15125

71	-17.19660	.02148	-.00296
72	-17.19660	.10731	-.01934
73	-17.19660	.27859	-.04213
74	-17.19660	.53454	-.08744
75	-17.19660	.87403	-.15738
76	-5.06060	.02091	-.00604
77	-5.06060	.10472	-.02915
78	-5.06060	.27313	-.07127
79	-5.06060	.52765	-.12423
80	-5.06060	.87058	-.17578
81	-9.91500	.02091	-.00604
82	-9.91500	.10472	-.02915
83	-9.91500	.27313	-.07127
84	-9.91500	.52765	-.12423
85	-9.91500	.87058	-.17578
86	-13.55580	.02091	-.00604
87	-13.55580	.10472	-.02915
88	-13.55580	.27313	-.07127
89	-13.55580	.52765	-.12423
90	-13.55580	.87058	-.17578
91	-15.98300	.02091	-.00604
92	-15.98300	.10472	-.02915
93	-15.98300	.27313	-.07127
94	-15.98300	.52765	-.12423
95	-15.98300	.87058	-.17578
96	-17.19660	.02113	-.00501
97	-17.19660	.10559	-.02455
98	-17.19660	.27495	-.06156
99	-17.19660	.52994	-.11197
100	-17.19660	.87173	-.16964
101	-.02167	-5.06060	-.00194
102	-.10517	-9.06060	-.01073
103	-.28041	-5.06060	-.03242
104	-.53684	-9.06060	-.07917
105	-.87517	-5.06060	-.15125
106	-.02167	-9.91500	-.00194
107	-.10817	-9.91500	-.01073
108	-.28041	-9.91500	-.03242
109	-.53684	-9.91500	-.07917
110	-.87517	-9.91500	-.15125
111	-.02167	-13.55580	-.00194
112	-.10817	-13.55580	-.01073
113	-.28041	-13.55580	-.03242
114	-.53684	-13.55580	-.07917
115	-.87517	-13.55580	-.15125
116	-.02167	-15.98300	-.00194
117	-.10817	-15.98300	-.01073
118	-.28041	-15.98300	-.03242
119	-.53684	-15.98300	-.07917
120	-.87517	-15.98300	-.15125
121	-.02148	-17.19660	-.00296
122	-.10731	-17.19660	-.01934
123	-.27859	-17.19660	-.04213
124	-.53454	-17.19660	-.08744
125	-.87403	-17.19660	-.15738
126	-.02091	-5.06060	-.00604
127	-.10472	-5.06060	-.02915
128	-.27313	-5.06060	-.07127
129	-.52765	-5.06060	-.12423
130	-.87058	-5.06060	-.17578
131	-.02091	-9.91500	-.00604
132	-.10472	-9.91500	-.02915
133	-.27313	-9.91500	-.07127
134	-.52765	-9.91500	-.12423
135	-.87058	-9.91500	-.17578
136	-.02091	-13.55580	-.00604
137	-.10472	-13.55580	-.02915
138	-.27313	-13.55580	-.07127
139	-.52765	-13.55580	-.12423
140	-.87058	-13.55580	-.17578
141	-.02091	-15.98300	-.00604
142	-.10472	-15.98300	-.02915
143	-.27313	-15.98300	-.07127

144	-.52765	-15.98300	-.12423
145	-.87058	-15.98300	-.17578
146	-.02110	-17.19660	-.00501
147	-.10559	-17.19660	-.02455
148	-.27495	-17.19660	-.06156
149	-.52994	-17.19660	-.11197
150	-.87173	-17.19660	-.16964
151	5.06060	-.02167	-.00194
152	5.06060	-.10817	-.01073
153	5.06060	-.29041	-.03242
154	5.06060	-.53684	-.07517
155	5.06060	-.87517	-.15125
156	9.91500	-.02167	-.00194
157	9.91500	-.10817	-.01073
158	9.91500	-.29041	-.03242
159	9.91500	-.53684	-.07517
160	9.91500	-.87517	-.15125
161	13.55580	-.02167	-.00194
162	13.55580	-.10817	-.01073
163	13.55580	-.29041	-.03242
164	13.55580	-.53684	-.07517
165	13.55580	-.87517	-.15125
166	15.98300	-.02167	-.00194
167	15.98300	-.10817	-.01073
168	15.98300	-.29041	-.03242
169	15.98300	-.53684	-.07517
170	15.98300	-.87517	-.15125
171	17.19660	-.02148	-.00296
172	17.19660	-.10731	-.01536
173	17.19660	-.27859	-.04213
174	17.19660	-.53454	-.08744
175	17.19660	-.87403	-.15738
176	5.06060	-.02091	-.00604
177	5.06060	-.10472	-.02915
178	5.06060	-.27313	-.07127
179	5.06060	-.52765	-.12423
180	5.06060	-.87058	-.17578
181	9.91500	-.02091	-.00604
182	9.91500	-.10472	-.02915
183	9.91500	-.27313	-.07127
184	9.91500	-.52765	-.12423
185	9.91500	-.87058	-.17578
186	13.55580	-.02091	-.00604
187	13.55580	-.10472	-.02915
188	13.55580	-.27313	-.07127
189	13.55580	-.52765	-.12423
190	13.55580	-.87058	-.17578
191	15.98300	-.02091	-.00604
192	15.98300	-.10472	-.02915
193	15.98300	-.27313	-.07127
194	15.98300	-.52765	-.12423
195	15.98300	-.87058	-.17578
196	17.19660	-.02110	-.00501
197	17.19660	-.10559	-.02455
198	17.19660	-.27495	-.06156
199	17.19660	-.52994	-.11197
200	17.19660	-.87173	-.16964

Nodal Numbering for Surfaces

FOR SURFACE		24			
1	7	13	19	25	31
2	8	14	20	26	32
3	9	15	21	27	33
4	10	16	22	28	34
5	11	17	23	29	35
6	12	18	24	30	36

FOR SURFACE		25			
1	7	13	19	25	31
37	41	45	49	53	57
38	42	46	50	54	58
39	43	47	51	55	59
40	44	48	52	56	60
6	12	18	24	30	36

FOR SURFACE		27			
57	63	69	75	81	87
58	64	70	76	82	88
59	65	71	77	83	89
60	66	72	78	84	90
61	67	73	79	85	91
62	68	74	80	86	92

FOR SURFACE		28			
57	63	69	75	81	87
93	97	101	105	109	113
94	98	102	106	110	114
95	99	103	107	111	115
96	100	104	108	112	116
62	68	74	80	86	92

FOR SURFACE		30			
113	119	125	131	137	143
114	120	126	132	138	144
115	121	127	133	139	145
116	122	128	134	140	146
117	123	129	135	141	147
118	124	130	136	142	148

FOR SURFACE		31			
113	119	125	131	137	143
149	153	157	161	165	169
150	154	158	162	166	170
151	155	159	163	167	171
152	156	160	164	168	172
118	124	130	136	142	148

FOR SURFACE		33			
169	175	181	187	193	199
170	176	182	188	194	200
171	177	183	189	195	201
172	178	184	190	196	202
173	179	185	191	197	203
174	180	186	192	198	204

FOR SURFACE		34			
169	175	181	187	193	199
205	209	213	217	221	225
206	210	214	218	222	226
207	211	215	219	223	227
208	212	216	220	224	228
174	180	186	192	198	204

Nodal Numbering for Elements

ELEM	++	+-	-+	--
1	8	2	7	1
2	9	3	8	2
3	10	4	9	3
4	11	5	10	4
5	12	6	11	5
6	14	8	13	7
7	15	9	14	8
8	15	10	15	9
9	17	11	16	10
10	18	12	17	11
11	20	14	19	13
12	21	15	20	14
13	22	16	21	15
14	23	17	22	16
15	24	18	23	17
16	26	20	25	19
17	27	21	26	20
18	28	22	27	21
19	29	23	28	22
20	30	24	29	23
21	32	26	31	25
22	33	27	32	26
23	34	28	33	27
24	35	29	34	28
25	36	30	35	29
26	37	41	1	7
27	38	42	37	41
28	39	43	38	42
29	40	44	39	43
30	6	12	40	44
31	41	45	7	13
32	42	46	41	45
33	43	47	42	46
34	44	48	43	47
35	12	18	44	48
36	45	49	13	19
37	46	51	45	49
38	47	51	46	50
39	48	52	47	51
40	18	24	48	52
41	49	53	19	25
42	50	54	49	53
43	51	55	50	54
44	52	56	51	55
45	24	30	52	56
46	53	32	25	31
47	54	33	53	32
48	55	34	54	33
49	56	35	55	34
50	30	36	56	35
51	64	58	63	57
52	65	59	64	58
53	66	60	65	59
54	67	61	66	60
55	68	62	67	61
56	70	64	69	63
57	71	65	70	64
58	72	66	71	65
59	73	67	72	66
60	74	68	73	67
61	76	70	75	69
62	77	71	76	70
63	78	72	77	71
64	79	73	78	72
65	80	74	79	73
66	82	76	81	75
67	83	77	82	76
68	84	78	83	77

69	85	79	84	78
70	86	80	85	79
71	86	82	87	81
72	89	83	88	82
73	90	84	89	83
74	91	85	90	84
75	92	86	91	85
76	93	87	92	86
77	94	88	93	87
78	95	89	94	88
79	96	90	95	89
80	97	91	96	90
81	97	101	63	69
82	98	102	97	101
83	99	103	98	102
84	100	104	99	103
85	68	74	100	104
86	101	105	69	75
87	102	106	101	105
88	103	107	102	106
89	104	108	103	107
90	74	80	104	108
91	105	109	75	81
92	106	110	105	109
93	107	111	106	110
94	108	112	107	111
95	80	86	108	112
96	109	88	81	87
97	110	89	109	88
98	111	90	110	89
99	112	91	111	90
100	86	92	112	91
101	120	114	119	113
102	121	115	120	114
103	122	116	121	115
104	123	117	122	116
105	124	118	123	117
106	126	120	125	119
107	127	121	126	120
108	128	122	127	121
109	129	123	128	122
110	130	124	129	123
111	132	126	131	125
112	133	127	132	126
113	134	128	133	127
114	135	129	134	128
115	136	130	135	129
116	138	132	137	131
117	139	133	138	132
118	140	134	139	133
119	141	135	140	134
120	142	136	141	135
121	144	138	143	137
122	145	139	144	138
123	146	140	145	139
124	147	141	146	140
125	148	142	147	141
126	149	143	148	142
127	150	144	149	143
128	151	145	150	144
129	152	146	151	145
130	118	124	152	146
131	153	147	153	147
132	154	148	154	148
133	155	149	155	149
134	156	150	156	150
135	124	130	156	160
136	157	151	157	151
137	158	152	158	152
138	159	153	159	153
139	160	154	160	154
140	130	136	160	164
141	161	155	161	155

142	162	166	161	165
143	163	167	162	166
144	164	168	163	167
145	136	142	164	168
146	165	144	137	143
147	166	145	165	144
148	167	146	166	145
149	168	147	167	146
150	142	148	168	147
151	176	170	175	169
152	177	171	176	170
153	178	172	177	171
154	179	173	178	172
155	180	174	179	173
156	182	176	181	175
157	183	177	182	176
158	184	178	183	177
159	185	179	184	178
160	186	180	185	179
161	188	182	187	181
162	189	183	188	182
163	190	184	189	183
164	191	185	190	184
165	192	186	191	185
166	194	188	193	187
167	195	189	194	188
168	196	190	195	189
169	197	191	196	190
170	198	192	197	191
171	200	194	199	193
172	201	195	200	194
173	202	196	201	195
174	203	197	202	196
175	204	198	203	197
176	205	199	204	198
177	206	210	205	209
178	207	211	206	210
179	208	212	207	211
180	174	180	208	212
181	209	213	175	181
182	210	214	209	213
183	211	215	210	214
184	212	216	211	215
185	180	186	212	216
186	213	217	181	187
187	214	218	213	217
188	215	219	214	218
189	216	220	215	219
190	186	192	216	220
191	217	221	187	193
192	218	222	217	221
193	219	223	218	222
194	220	224	219	223
195	192	198	220	224
196	221	200	193	199
197	222	201	221	200
198	223	202	222	201
199	224	203	223	202
200	198	204	224	203

The Distribution of the Source

FOR SUBSURFACE 24				
-.67898E+01	-.12965E+02	-.17601E+02	-.20237E+02	-.11351E+02
-.64984E+01	-.12450E+02	-.16917E+02	-.19516E+02	-.10964E+02
-.36705E+01	-.69826E+01	-.94592E+01	-.10879E+02	-.62031E+01
.20676E+01	.40148E+01	.54635E+01	.63976E+01	.33652E+01
.76145E+01	.14806E+02	.20137E+02	.23241E+02	.12750E+02
FOR SUBSURFACE 25				
-.70504E+01	-.13521E+02	-.18387E+02	-.21175E+02	-.11844E+02
-.75670E+01	-.14784E+02	-.20220E+02	-.23463E+02	-.13102E+02
-.59701E+01	-.11792E+02	-.16203E+02	-.18950E+02	-.10664E+02
-.85895E+00	-.20238E+01	-.29820E+01	-.37337E+01	-.22639E+01
.60343E+01	.11586E+02	.15663E+02	.17933E+02	.98657E+01
FOR SUBSURFACE 27				
-.67898E+01	-.12965E+02	-.17601E+02	-.20237E+02	-.11351E+02
-.64984E+01	-.12450E+02	-.16917E+02	-.19516E+02	-.10964E+02
-.36705E+01	-.69826E+01	-.94592E+01	-.10879E+02	-.62031E+01
.20676E+01	.40148E+01	.54635E+01	.63976E+01	.33652E+01
.76145E+01	.14806E+02	.20137E+02	.23241E+02	.12750E+02
FOR SUBSURFACE 28				
-.70504E+01	-.13521E+02	-.18387E+02	-.21175E+02	-.11844E+02
-.75670E+01	-.14784E+02	-.20220E+02	-.23463E+02	-.13102E+02
-.59701E+01	-.11792E+02	-.16203E+02	-.18950E+02	-.10664E+02
-.85895E+00	-.20238E+01	-.29820E+01	-.37337E+01	-.22639E+01
.60343E+01	.11586E+02	.15663E+02	.17933E+02	.98657E+01

FDR SUBSURFACE 30

-.67898E+01	-.12965E+02	-.17601E+02	-.20237E+02	-.11351E+02
-.64984E+01	-.12450E+02	-.16917E+02	-.19516E+02	-.10964E+02
-.36705E+01	-.69526E+01	-.94592E+01	-.10879E+02	-.62031E+01
.20676E+01	.40148E+01	.54635E+01	.63976E+01	.33652E+01
.76145E+01	.14806E+02	.20137E+02	.23241E+02	.12750E+02

FDR SUBSURFACE 31

-.70504E+01	-.13521E+02	-.18387E+02	-.21175E+02	-.11844E+02
-.75670E+01	-.14784E+02	-.20220E+02	-.23463E+02	-.13102E+02
-.59701E+01	-.11792E+02	-.16203E+02	-.18950E+02	-.10664E+02
-.85895E+00	-.20238E+01	-.29820E+01	-.37337E+01	-.22639E+01
.60343E+01	.11586E+02	.15663E+02	.17933E+02	.98657E+01

FDR SUBSURFACE 33

-.67898E+01	-.12965E+02	-.17601E+02	-.20237E+02	-.11351E+02
-.64984E+01	-.12450E+02	-.16917E+02	-.19516E+02	-.10964E+02
-.36705E+01	-.69526E+01	-.94592E+01	-.10879E+02	-.62031E+01
.20676E+01	.40148E+01	.54635E+01	.63976E+01	.33652E+01
.76145E+01	.14806E+02	.20137E+02	.23241E+02	.12750E+02

FDR SUBSURFACE 34

-.70504E+01	-.13521E+02	-.18387E+02	-.21175E+02	-.11844E+02
-.75670E+01	-.14784E+02	-.20220E+02	-.23463E+02	-.13102E+02
-.59701E+01	-.11792E+02	-.16203E+02	-.18950E+02	-.10664E+02
-.85895E+00	-.20238E+01	-.29820E+01	-.37337E+01	-.22639E+01
.60343E+01	.11586E+02	.15663E+02	.17933E+02	.98657E+01

The Distribution of the Velocity Potential

FOR SUBSURFACE 24				
.17602E+03	.20640E+03	.20732E+03	.18068E+03	.15468E+03
.17886E+03	.21339E+03	.21798E+03	.19379E+03	.16714E+03
.18380E+03	.22322E+03	.23153E+03	.20961E+03	.17963E+03
.18929E+03	.23356E+03	.24566E+03	.22568E+03	.18934E+03
.18643E+03	.23073E+03	.24566E+03	.22257E+03	.18346E+03
FOR SUBSURFACE 25				
.16041E+03	.17883E+03	.17098E+03	.13619E+03	.11212E+03
.15183E+03	.16619E+03	.15586E+03	.11874E+03	.95408E+02
.14952E+03	.15728E+03	.14563E+03	.10694E+03	.82754E+02
.14380E+03	.15562E+03	.14404E+03	.10571E+03	.78885E+02
.14135E+03	.15756E+03	.14451E+03	.10988E+03	.82064E+02
FOR SUBSURFACE 27				
.17602E+03	.20640E+03	.20732E+03	.18068E+03	.15468E+03
.17886E+03	.21339E+03	.21798E+03	.19379E+03	.16714E+03
.18380E+03	.22322E+03	.23153E+03	.20961E+03	.17963E+03
.18929E+03	.23356E+03	.24566E+03	.22568E+03	.18934E+03
.18643E+03	.23073E+03	.24566E+03	.22257E+03	.18346E+03
FOR SUBSURFACE 28				
.16041E+03	.17883E+03	.17098E+03	.13619E+03	.11212E+03
.15183E+03	.16619E+03	.15586E+03	.11874E+03	.95408E+02
.14952E+03	.15728E+03	.14563E+03	.10694E+03	.82754E+02
.14380E+03	.15562E+03	.14404E+03	.10571E+03	.78885E+02
.14135E+03	.15756E+03	.14451E+03	.10988E+03	.82064E+02

FOR SURFACE 30

.17602E+03	.20641E+03	.20732E+03	.18068E+03	.15468E+03
.17886E+03	.21339E+03	.21798E+03	.19379E+03	.16714E+03
.18380E+03	.22322E+03	.23153E+03	.20961E+03	.17963E+03
.18929E+03	.23356E+03	.24566E+03	.22568E+03	.18934E+03
.18643E+03	.23073E+03	.24566E+03	.22257E+03	.18346E+03

FOR SUBSURFACE 31

.16041E+03	.17883E+03	.17098E+03	.13619E+03	.11212E+03
.15183E+03	.16619E+03	.15586E+03	.11874E+03	.95400E+02
.14552E+03	.15728E+03	.14563E+03	.10694E+03	.82754E+02
.14380E+03	.15562E+03	.14404E+03	.10571E+03	.78885E+02
.14135E+03	.15756E+03	.14451E+03	.10988E+03	.82064E+02

FOR SURFACE 33

.17602E+03	.20540E+03	.20732E+03	.18068E+03	.15468E+03
.17886E+03	.21339E+03	.21798E+03	.19379E+03	.16714E+03
.18380E+03	.22322E+03	.23153E+03	.20961E+03	.17963E+03
.18929E+03	.23356E+03	.24566E+03	.22568E+03	.18934E+03
.18643E+03	.23073E+03	.24566E+03	.22257E+03	.18346E+03

FOR SUBSURFACE 34

.16041E+03	.17883E+03	.17098E+03	.13619E+03	.11212E+03
.15183E+03	.16619E+03	.15586E+03	.11874E+03	.95400E+02
.14552E+03	.15728E+03	.14563E+03	.10694E+03	.82754E+02
.14380E+03	.15562E+03	.14404E+03	.10571E+03	.78885E+02
.14135E+03	.15756E+03	.14451E+03	.10988E+03	.82064E+02

Pressure Distribution

FOR SUBSURFACE 24				
-.10193E+01	-.18540E+01	-.29055E+01	-.36553E+01	-.18860E+01
-.15173E+00	-.30130E+00	-.48997E+00	-.60060E+00	-.28944E+00
-.11633E+00	-.21550E+00	-.33475E+00	-.38244E+00	-.21574E+00
-.24355E-01	-.61409E-01	-.10789E+00	-.10601E+00	-.65347E-01
.27068E+00	.45045E+00	.66623E+00	.79997E+00	.41744E+00
FOR SUBSURFACE 25				
.12332E+01	.20739E+01	.30870E+01	.38080E+01	.21446E+01
.24289E+00	.37140E+00	.51221E+00	.61583E+00	.35977E+00
.77155E-01	.11078E+00	.14419E+00	.17862E+00	.82484E-01
.19756E-01	.92388E-02	-.29301E-02	-.11323E-01	-.10274E-01
-.25524E+00	-.45014E+00	-.64576E+00	-.82444E+00	-.41975E+00
FOR SUBSURFACE 27				
-.22063E+00	-.66035E+00	-.12827E+01	-.17903E+01	-.10721E+01
-.24219E-01	-.94383E-01	-.22389E+00	-.33037E+00	-.39245E+00
-.14865E-01	-.60488E-01	-.15311E+00	-.22746E+00	-.42499E+00
-.69449E-02	-.19498E-02	-.51913E-01	-.99233E-01	-.39249E+00
.71613E-01	.17953E+00	.28145E+00	.32919E+00	-.22828E-01
FOR SUBSURFACE 28				
.28237E+00	.75515E+00	.13274E+01	.17690E+01	.10734E+01
.58637E-01	.13832E+00	.19970E+00	.26258E+00	.29788E+00
.20845E-01	.40475E-01	.37636E-01	.31767E-01	.21774E+00
.81468E-02	.36365E-02	-.26761E-01	-.60218E-01	.19615E+00
-.50783E-01	-.15666E+00	-.31931E+00	-.44820E+00	-.14959E+00

FOR SUBSURFACE 30				
.56203E+00	.51296E+00	.36899E+00	.16555E+00	.16322E-01
.03759E+01	.83474E-01	.62199E-01	.26930E+01	.99953E-03
.64417E-01	.59976E-01	.42390E-01	.16581E-01	-.31805E-02
.14005E-01	.17769E-01	.13933E-01	.32679E-02	-.10356E-01
-.14844E+00	-.12360E+00	-.89126E-01	-.38927E-01	-.14940E-01
FOR SUBSURFACE 31				
-.67996E+00	-.57377E+00	-.39208E+00	-.17259E+00	-.18741E-01
-.13386E+00	-.10274E+00	-.89213E-01	-.28222E-01	-.24223E-02
-.42457E-01	-.30642E-01	-.18754E-01	-.89582E-02	.20596E-02
-.10723E-01	-.25429E-02	-.47929E-03	-.11078E-02	.61449E-02
.14121E+00	.12492E+00	.86005E-01	.34585E-01	.65353E-02
FOR SUBSURFACE 33				
-.23663E+00	-.68066E+00	-.12939E+01	-.16995E+01	-.79758E+00
-.43758E-01	-.12314E+00	-.20396E+00	-.24330E+00	.10400E+00
-.37047E-01	-.95035E-01	-.13926E+00	-.13840E+00	.20607E+00
-.17294E-01	-.41695E-01	-.42407E-01	-.35046E-02	.31679E+00
.50636E-01	.14732E+00	.29965E+00	.43185E+00	.42533E+00
FOR SUBSURFACE 34				
.27089E+00	.74493E+00	.13675E+01	.18664E+01	.10525E+01
.50350E-01	.13253E+00	.24729E+00	.34503E+00	.59768E-01
.13853E-01	.39664E-01	.87800E-01	.13789E+00	-.13319E+00
.88585E-03	.30078E-02	.23352E-01	.47707E-01	-.20028E+00
-.63241E-01	-.16356E+00	-.28045E+00	-.34170E+00	-.26362E+00

SAMPLE CASE 3:

BO-105 FUSELAGE (NO PYLON, NO ROTOR)
WITH EFFECTS OF SEPARATION

Data Input

```

3
PROGRAM SHAPES
HUB PYLON FLOW SEPARATION
FUSELAGE - WITH SEPARATION EFFECTS
KREAD      0
*          12      0      0
**         0      1      1      1      0      0      0      0      0
***        0      0
UAMCH      .204      0.000      -0.000
ALFA       0.000      0.000
NBODY      0.000      12.000      38.000      41.000
NBODY      0.000      0.000      0.000      0.000
NBODY      0.000      0.000      0.000      0.000
NBODY      7.250      5.250      7.250      8.250
NWAKE      1      0      0      0
NPYLON     1      1
CSTAG      -20.000      1.000
KPRINT     1      1      1      1      0      1      1      1      1      1
NBODY1     4      4      2      1      1
NBODY2     4      4      1      1      1
NBODY3     4      4      2      1      1
    
```

Specifications of the Problem

FOR PART 1
NX= 4
NY= 4

FOR PART 2
NX= 4
NY= 4

FOR PART 3
NX= 4
NY= 4

FOR PART 5
NX= 4
NY= 4

FOR PART 6
NX= 4
NY= 4

FOR PART 7
NX= 4
NY= 4

FOR PART 9
NX= 4
NY= 4

FOR PART 10
NX= 4
NY= 4

FOR PART 11
NX= 4
NY= 4

FOR PART 13
NX= 4
NY= 4

FOR PART 14
NX= 4
NY= 4

FOR PART 15
NX= 4
NY= 4

NELEM=132

KSMMY= 0
KSMMZ= 0

X, Y, and Z Coordinates of the Nodes

NOCE =	X	Y	Z
1	0.0000	0.0000	0.0000
2	.7500	-0.0000	2.0625
3	3.0000	-0.0000	-4.1250
4	6.7500	-0.0000	1.1875
5	12.0000	0.0000	8.2500
6	6.7500	.5333	1.9050
7	3.0000	1.3672	3.8110
8	6.7500	2.0808	5.7165
9	12.0000	2.7745	7.6220
10	.7500	1.2513	1.4534
11	3.0000	2.5632	2.5162
12	6.7500	3.8449	-4.3752
13	12.0000	5.1262	5.8333
14	.7500	1.3743	.7892
15	3.0000	3.3496	1.5747
16	6.7500	5.0239	2.3675
17	12.0000	6.5983	3.1571
18	.7500	1.8125	0.0000
19	3.0000	3.5250	0.0000
20	6.7500	5.4375	0.0000
21	12.0000	7.2500	0.0000
22	18.5000	-0.0000	8.2500
23	25.0000	-0.0000	5.2500
24	31.5000	-0.0000	2.2500
25	38.0000	-0.0000	0.0000
26	18.5000	2.7745	7.1220
27	25.0000	2.7745	7.1220
28	31.5000	2.7745	7.1220
29	38.0000	2.7745	7.1220
30	18.5000	5.1262	5.8333
31	25.0000	5.1262	5.8333
32	31.5000	5.1262	5.8333
33	38.0000	5.1262	5.8333
34	18.5000	6.5983	3.1571
35	25.0000	6.5983	3.1571
36	31.5000	6.5983	3.1571
37	38.0000	6.5983	3.1571
38	18.5000	7.2500	0.0000
39	25.0000	7.2500	0.0000
40	31.5000	7.2500	0.0000
41	38.0000	7.2500	0.0000
42	39.3125	-0.0000	8.1875
43	-0.2500	-0.0000	-4.1250
44	40.3125	-0.0000	2.0625
45	-1.0000	0.0000	0.0000
46	39.3125	2.0808	5.7165
47	40.2500	1.3672	3.8110
48	40.4125	.5333	1.9050
49	39.3125	3.8449	-4.3752
50	-0.2500	2.5632	2.5162
51	40.3125	1.2513	1.4534
52	39.3125	5.0239	2.3675
53	40.2500	3.3496	1.5747
54	-0.3125	1.6743	.7892
55	39.3125	5.4375	0.0000
56	40.2500	3.5250	0.0000
57	40.3125	1.8125	0.0000
58	.7500	-0.0000	-2.0625
59	3.0000	-0.0000	-4.1250
60	6.7500	-0.0000	-6.1875
61	12.0000	-0.0000	-8.2500
62	.7500	.5333	-1.9050
63	3.0000	1.3672	-3.8110
64	6.7500	2.0808	-5.7165
65	12.0000	2.7745	-7.6220
66	.7500	1.2513	-1.4534
67	3.0000	2.5632	-2.5162
68	6.7500	3.8449	-4.3752

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69	12.00000	3.12552	-5.63363
70	.75000	1.57163	-7.74928
71	3.00000	3.34905	-1.77357
72	6.75000	5.02359	-2.36765
73	12.00000	6.59913	-3.15714
74	18.50000	-0.00000	-3.25000
75	25.00000	-0.00000	-3.25000
76	31.50000	-0.00000	-3.25000
77	38.00000	0.00000	-3.25000
78	44.50000	2.77445	-7.62201
79	51.00000	2.77445	-7.62201
80	57.50000	2.77445	-7.62201
81	64.00000	2.77445	-7.62201
82	70.50000	5.12552	-5.83363
83	77.00000	5.12552	-5.83363
84	83.50000	5.12552	-5.83363
85	90.00000	3.12552	-5.63363
86	96.50000	3.34913	-3.15714
87	103.00000	3.34913	-3.15714
88	109.50000	3.34913	-3.15714
89	116.00000	3.34913	-3.15714
90	122.50000	-0.00000	-0.15750
91	129.00000	-0.00000	-0.12500
92	135.50000	-0.00000	-2.05250
93	142.00000	2.35114	-5.71550
94	148.50000	1.33723	-3.81100
95	155.00000	3.34913	-1.93550
96	161.50000	3.34913	-4.37522
97	168.00000	2.56326	-2.91582
98	174.50000	1.25163	-1.45841
99	181.00000	5.12359	-2.36785
100	187.50000	3.34906	-1.57857
101	194.00000	1.57453	-0.78928
102	200.50000	-0.63361	1.95550
103	207.00000	-1.32723	3.61100
104	213.50000	-2.00000	5.71650
105	220.00000	-2.77445	7.62201
106	226.50000	-1.25163	1.45841
107	233.00000	-2.56326	2.91582
108	239.50000	-3.34909	4.37522
109	246.00000	-5.12552	5.83363
110	252.50000	-1.57453	0.79250
111	259.00000	-3.34906	1.57857
112	265.50000	-5.02359	2.36765
113	272.00000	-6.59913	3.15714
114	278.50000	-1.51250	0.00000
115	285.00000	-3.62500	0.00000
116	291.50000	-5.43750	0.00000
117	298.00000	-7.25000	0.00000
118	304.50000	-2.77445	7.62201
119	311.00000	-2.77445	7.62201
120	317.50000	-2.77445	7.62201
121	324.00000	-2.77445	7.62201
122	330.50000	-5.12552	5.83363
123	337.00000	-5.12552	5.83363
124	343.50000	-5.12552	5.83363
125	350.00000	-5.12552	5.83363
126	356.50000	-6.59913	3.15714
127	363.00000	-6.59913	3.15714
128	369.50000	-6.59913	3.15714
129	376.00000	-6.59913	3.15714
130	382.50000	-7.25000	0.00000
131	389.00000	-7.25000	0.00000
132	395.50000	-7.25000	0.00000
133	402.00000	-7.25000	0.00000
134	408.50000	-2.05114	5.71550
135	415.00000	-1.33723	3.81100
136	421.50000	-0.63361	1.95550
137	428.00000	-3.34919	4.37522
138	434.50000	-2.56326	2.91582
139	441.00000	-1.25163	1.45841
140	447.50000	-3.34909	2.37522

141	-0.25000	-3.34906	1.57057
142	-0.81250	-1.57493	.78928
143	39.31250	-3.43710	0.00000
144	-0.25000	-3.32510	1.00000
145	40.81250	-1.31210	0.00000
146	.75000	-.53361	-1.40550
147	3.00000	-1.38723	-3.61100
148	6.75000	-2.09034	-5.71650
149	12.00000	-2.77445	-7.82201
150	.75000	-1.25163	-1.45841
151	3.00000	-2.55326	-2.41682
152	6.75000	-3.34639	-4.37522
153	12.00000	-3.12362	-5.63363
154	.75000	-1.57453	-.78928
155	3.00000	-3.34906	-1.57057
156	6.75000	-4.02359	-2.36789
157	12.00000	-5.59813	-3.15714
158	18.00000	-2.77445	-7.82201
159	24.00000	-2.77445	-7.82201
160	31.50000	-2.77445	-7.82201
161	38.00000	-2.77445	-7.82201
162	44.50000	-3.12362	-5.63363
163	24.00000	-3.12362	-5.63363
164	31.50000	-3.12362	-5.63363
165	38.00000	-3.12362	-5.63363
166	44.50000	-3.59813	-3.15714
167	24.00000	-3.59813	-3.15714
168	31.50000	-3.59813	-3.15714
169	38.00000	-3.59813	-3.15714
170	39.31250	-2.30004	-0.71056
171	40.62500	-1.35723	-3.01100
172	40.81250	-.53361	-1.40550
173	40.31250	-3.04429	-4.37522
174	-0.25000	-2.55326	-2.41682
175	-0.81250	-1.25163	-1.45841
176	39.31250	-3.02359	-2.36789
177	40.25000	-3.34906	-1.57057
178	-0.81250	-1.57453	-.78928

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X, Y, and Z Coordinates of the Centroid of Aerodynamic Panels

ELEM#	XPC	YPC	ZPC
1	.30306	.17340	.33200
2	1.91528	.52021	2.97800
3	4.97972	.35702	4.35000
4	9.57538	1.21382	6.94400
5	.38306	.73904	.84000
6	1.91528	1.111-3	2.52203
7	4.97972	2.45905	4.20403
8	9.57538	3.79581	5.88603
9	.38306	.73904	.84000
10	1.91528	2.21712	1.68577
11	4.97972	3.55321	2.80912
12	9.57538	4.88930	3.93345
13	.38306	.87175	.19722
14	1.91528	2.01527	.59196
15	4.97972	3.35179	.98661
16	9.57538	4.68831	1.38125
17	15.57758	1.38723	7.93600
18	22.21721	1.38723	7.93600
19	28.85683	1.38723	7.93600
20	35.49646	1.38723	7.93600
21	15.57758	3.35049	6.72702
22	22.21721	3.35049	6.72702
23	28.85683	3.35049	6.72702
24	35.49646	3.35049	6.72702
25	15.57758	5.31233	4.49539
26	22.21721	5.31233	4.49539
27	28.85683	5.31233	4.49539
28	35.49646	5.31233	4.49539
29	15.57758	6.37406	1.57857
30	22.21721	6.37406	1.57857
31	28.85683	6.37406	1.57857
32	35.49646	6.37406	1.57857
33	39.48662	1.21382	3.94400
34	40.63578	.35702	.96000
35	41.78495	.52021	2.97800
36	41.78495	.17340	.33200
37	39.48662	3.79581	5.88603
38	40.63578	2.45905	4.20403
39	41.78495	1.111-3	2.52203
40	41.78495	.73904	.84000
41	39.48662	5.17320	3.93345
42	40.63578	3.55321	2.80912
43	41.78495	2.21712	1.68577
44	41.78495	.73904	.84000
45	39.48662	5.11231	1.38125
46	40.63578	4.35049	.98661
47	41.78495	2.01527	.59196
48	41.78495	.87175	.19722
49	.38306	.17340	-.99200
50	1.91528	.52021	-2.97600
51	4.97972	.35702	-4.35000
52	9.57538	1.21382	-6.94400
53	.38306	1.45381	-.34000
54	1.91528	1.481-3	-2.52203
55	4.97972	2.45905	-4.20403
56	9.57538	3.79581	-5.88603
57	.38306	.73904	-.84000
58	1.91528	2.21712	-1.68577
59	4.97972	3.55321	-2.80912
60	9.57538	4.88930	-3.93345
61	.38306	.87175	-.19722
62	1.91528	2.01527	-.59196
63	4.97972	3.35179	-.98661
64	9.57538	4.68831	-1.38125

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65	15.57758	1.33723	-7.93600
66	22.21721	1.38723	-7.93600
67	28.85683	1.38723	-7.93600
68	35.49646	1.38723	-7.93600
69	15.57758	3.95049	-6.72782
70	22.21721	3.95049	-6.72782
71	28.85683	3.95049	-6.72782
72	35.49646	3.95049	-6.72782
73	15.57758	5.31233	-4.49538
74	22.21721	5.31233	-4.49538
75	28.85683	5.31233	-4.49538
76	35.49646	5.31233	-4.49538
77	15.57758	6.97406	-1.57857
78	22.21721	6.97406	-1.57857
79	28.85683	6.97406	-1.57857
80	35.49646	6.97406	-1.57857
81	39.48662	1.21352	-5.99400
82	-0.63578	3.3732	-4.96000
83	41.40190	5.2021	-2.97000
84	41.78495	1.734	-3.92000
85	39.48662	3.4503	-3.62000
86	40.63578	2.4590	-4.20400
87	41.40190	1.8143	-2.92253
88	41.78495	1.3331	-3.84093
89	39.48662	3.1732	-3.93343
90	40.63578	3.0352	-2.60902
91	41.40190	2.21712	-1.63517
92	41.78495	1.7301	-3.01192
93	39.48662	3.1231	-1.35123
94	40.63578	4.3787	-3.98601
95	41.40190	2.61527	-3.51155
96	41.78495	1.7175	-1.13732
97	38306	-1.1340	3.99200
98	1.91528	-2.21712	2.97000
99	4.97972	-3.9702	4.96000
100	9.57538	-4.10231	6.94400
101	13.306	-4.3351	8.04000
102	19.91528	-4.4143	2.82293
103	24.97972	-2.4130	3.20400
104	9.57538	-3.4563	3.36604
105	38306	-2.7904	3.5142
106	1.91528	-2.21712	1.63517
107	4.97972	-3.9702	2.97000
108	9.57538	-4.1732	3.93345
109	38306	-0.8717	1.9732
110	1.91528	-2.21527	3.5145
111	4.97972	-4.3787	3.98601
112	9.57538	-4.10231	1.35125
113	15.57758	-1.38723	7.93610
114	22.21721	-1.38723	7.93600
115	28.85683	-1.38723	7.93600
116	35.49646	-1.38723	7.93600
117	15.57758	-3.95049	6.72782
118	22.21721	-3.95049	6.72782
119	28.85683	-3.95049	6.72782
120	35.49646	-3.95049	6.72782
121	15.57758	-5.31233	4.49538
122	22.21721	-5.31233	4.49538
123	28.85683	-5.31233	4.49538
124	35.49646	-5.31233	4.49538
125	15.57758	-6.97406	1.57857
126	22.21721	-6.97406	1.57857
127	28.85683	-6.97406	1.57857
128	35.49646	-6.97406	1.57857
129	39.48662	-1.21352	5.99400
130	40.63578	-3.3732	4.96000
131	41.40190	-5.2021	2.97000
132	41.78495	-1.734	3.92000
133	39.48662	-3.4503	3.62000
134	40.63578	-2.4590	4.20400
135	41.40190	-1.8143	2.92253

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136	41.78495	-4.4331	.34058
137	39.48662	-5.17323	3.933-6
138	41.63973	-3.33920	2.30982
139	-1.4-190	-2.21712	1.86577
140	41.78495	-4.73904	.86152
141	39.48662	-5.10231	1.36125
142	40.63578	-4.33874	.55561
143	41.40190	-2.51527	.55155
144	41.78495	-3.37175	.19732
145	.36306	-1.17340	-4.33240
146	1.91528	-5.2021	-2.97600
147	4.97972	-4.05702	-4.33000
148	9.57638	-1.21352	-5.94400
149	.36306	-4.63351	-4.04053
150	1.91528	-1.48143	-2.52253
151	4.97972	-2.43355	-4.20455
152	9.57638	-3.45558	-5.38684
153	.36306	-4.73904	-4.56152
154	1.91528	-2.21712	-1.66577
155	4.97972	-3.09520	-2.80982
156	9.57638	-5.17323	-3.93345
157	.36306	-3.7175	-1.3732
158	1.91528	-2.51527	-4.56155
159	4.97972	-4.35873	-4.94661
160	9.57638	-6.10231	-1.36125
161	15.57758	-1.33723	-7.93600
162	22.21721	-1.33723	-7.93600
163	28.85683	-1.33723	-7.93600
164	35.49646	-1.33723	-7.93600
165	42.13609	-3.95049	-6.72782
166	22.21721	-3.95049	-6.72782
167	28.85683	-3.95049	-6.72782
168	35.49646	-3.95049	-6.72782
169	42.13609	-5.91233	-4.49533
170	22.21721	-5.91233	-4.49533
171	28.85683	-5.91233	-4.49533
172	35.49646	-5.91233	-4.49533
173	42.13609	-6.37405	-1.57857
174	22.21721	-6.37405	-1.57857
175	28.85683	-6.37405	-1.57857
176	35.49646	-6.37405	-1.57857
177	42.13609	-1.21352	-5.94400
178	40.63578	-1.17340	-4.97600
179	-1.4-190	-2.21712	-2.30982
180	41.78495	-4.73904	.86152
181	39.48662	-5.10231	1.36125
182	40.63578	-4.33874	.55561
183	41.40190	-2.51527	.55155
184	41.78495	-3.37175	.19732
185	39.48662	-4.17323	3.93345
186	-0.63578	-3.09520	-2.80982
187	41.40190	-2.21712	-1.66577
188	-1.74495	-4.73904	-4.56152
189	39.48662	-5.10231	-1.36125
190	-0.63578	-4.33874	.55561
191	-1.4-190	-2.51527	-4.56155
192	41.78495	-3.7175	-1.3732

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Nodal Numbering for Surfaces

FOR SURFACE 1

1	1	1	1	1
2	6	10	14	18
3	7	11	15	19
4	8	12	16	20
5	9	13	17	21

FOR SURFACE 2

5	9	13	17	21
22	26	30	34	38
23	27	31	35	39
24	28	32	36	40
25	29	33	37	41

FOR SURFACE 3

25	29	33	37	41
42	46	50	54	58
43	47	51	55	59
44	48	52	56	60
45	49	53	57	61

FOR SURFACE 5

1	1	1	1	1
58	62	66	70	74
59	63	67	71	75
60	64	68	72	76
61	65	69	73	77

FOR SURFACE 6

61	65	69	73	77
74	78	82	86	90
75	79	83	87	91
76	80	84	88	92
77	81	85	89	93

FOR SURFACE 7

77	81	85	89	93
90	93	96	99	102
91	94	97	100	103
92	95	98	101	104
93	96	99	102	105

FOR SURFACE 9

1	1	1	1	1
2	102	106	110	114
3	103	107	111	115
4	104	108	112	116
5	105	109	113	117

FOR SURFACE 10

5	105	109	113	117
22	118	122	126	130
23	119	123	127	131
24	120	124	128	132
25	121	125	129	133

FOR SURFACE 11

29	121	125	129	133
42	134	137	140	143
43	135	138	141	144
44	136	139	142	145
45	45	45	45	45

FOR SURFACE 13

1	1	1	1	1
58	146	150	154	114
59	147	151	155	115
60	148	152	156	116
61	149	153	157	117

FOR SURFACE 14

61	149	153	157	117
74	158	162	166	130
75	159	163	167	131
76	160	164	168	132
77	161	165	169	133

FOR SURFACE 15

77	161	165	169	133
90	170	173	175	143
91	171	174	177	144
92	172	175	178	145
45	45	45	45	45

Nodal Numbering for Elements

ELEM	++	+-	-+	--
1	1	2	1	1
2	7	3	5	2
3	4	4	7	3
4	5	7	5	4
5	10	6	1	1
6	11	7	11	6
7	12	8	11	7
8	13	9	12	8
9	14	10	1	1
10	15	11	14	10
11	15	12	15	11
12	17	13	16	12
13	18	14	1	1
14	19	15	19	14
15	20	16	19	15
16	21	17	20	16
17	23	22	3	3
18	27	23	25	22
19	28	24	27	23
20	29	25	28	24
21	30	26	13	9
22	31	27	30	26
23	32	28	31	27
24	33	29	32	28
25	34	30	17	13
26	35	31	34	30
27	36	32	35	31
28	37	33	36	32
29	38	34	37	33
30	39	35	38	34
31	40	36	39	35
32	41	37	40	36
33	42	42	29	25
34	47	43	40	42
35	48	44	41	43
36	49	45	42	44
37	49	46	33	23
38	50	47	43	46
39	51	48	44	47
40	52	49	51	48
41	52	50	37	33
42	53	51	38	49
43	54	51	33	20
44	55	52	34	51
45	56	52	41	37
46	56	53	35	32
47	57	54	36	38
48	58	55	37	44
49	58	56	1	1
50	59	57	39	42
51	60	58	39	43
52	61	59	60	54
53	62	60	1	1
54	63	61	62	56
55	64	62	53	47
56	65	63	64	48
57	66	70	1	1
58	67	71	65	70
59	68	72	37	71
60	69	73	38	72
61	70	18	1	1
62	71	19	70	18
63	72	20	71	19
64	73	21	72	20

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65	74	78	81	85
66	75	79	74	79
67	75	80	75	79
68	77	81	75	80
69	78	82	82	89
70	79	83	78	82
71	80	84	79	83
72	81	85	80	84
73	82	86	81	85
74	83	87	82	86
75	84	88	83	87
76	85	89	84	88
77	86	90	85	89
78	87	91	86	90
79	88	92	87	91
80	89	93	88	92
81	90	94	89	93
82	91	95	90	94
83	92	96	91	95
84	93	97	92	96
85	94	98	93	97
86	95	99	94	98
87	96	100	95	99
88	97	101	96	100
89	98	102	97	101
90	99	103	98	102
91	100	104	99	103
92	101	105	100	104
93	102	106	101	105
94	103	107	102	106
95	104	108	103	107
96	105	109	104	108
97	106	110	105	109
98	107	111	106	110
99	108	112	107	111
100	109	113	108	112
101	110	114	109	113
102	111	115	110	114
103	112	116	111	115
104	113	117	112	116
105	114	118	113	117
106	115	119	114	118
107	116	120	115	119
108	117	121	116	120
109	118	122	117	121
110	119	123	118	122
111	120	124	119	123
112	121	125	120	124
113	122	126	121	125
114	123	127	122	126
115	124	128	123	127
116	125	129	124	128
117	126	130	125	129
118	127	131	126	130
119	128	132	127	131
120	129	133	128	132

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129	42	134	25	121
130	43	135	42	134
131	44	136	43	135
132	45	45	44	136
133	134	137	121	122
134	135	138	136	137
135	136	139	135	138
136	45	45	136	139
137	137	140	125	129
138	138	141	137	140
139	139	142	138	141
140	45	45	139	142
141	140	143	121	133
142	141	144	140	143
143	142	145	141	144
144	45	45	142	145
145	146	148	1	1
146	147	149	146	147
147	148	150	147	148
148	149	151	148	149
149	150	152	1	1
150	151	153	150	151
151	152	154	151	152
152	153	155	152	153
153	154	156	1	1
154	155	157	154	155
155	156	158	155	156
156	157	159	156	157
157	158	160	1	1
158	159	161	158	159
159	160	162	159	160
160	161	163	160	161
161	162	164	161	162
162	163	165	162	163
163	164	166	163	164
164	165	167	164	165
165	166	168	165	166
166	167	169	166	167
167	168	170	167	168
168	169	171	168	169
169	170	172	169	170
170	171	173	170	171
171	172	174	171	172
172	173	175	172	173
173	174	176	173	174
174	175	177	174	175
175	176	178	175	176
176	177	179	176	177
177	178	180	177	178
178	179	181	178	179
179	180	182	179	180
180	181	183	180	181
181	182	184	181	182
182	183	185	182	183
183	184	186	183	184
184	185	187	184	185
185	186	188	185	186
186	187	189	186	187
187	188	190	187	188
188	189	191	188	189
189	190	192	189	190
190	191	193	190	191
191	192	194	191	192
192	193	195	192	193

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The Distribution of the Source

FOR SUBSURFACE 1

- .11944E+04	- .11943E+04	- .11941E+04	- .11940E+04
- .11322E+04	- .11317E+04	- .11309E+04	- .11304E+04
- .10005E+04	- .99997E+03	- .99827E+03	- .99730E+03
- .75270E+03	- .75175E+03	- .75051E+03	- .74969E+03

FOR SUBSURFACE 2

- .29311E+03	- .29549E+03	- .29875E+03	- .30098E+03
- .41211E+02	- .41335E+02	- .41983E+02	- .42293E+02
.18265E+03	.18456E+03	.18757E+03	.18973E+03
.50453E+03	.51193E+03	.51987E+03	.52610E+03

FOR SUBSURFACE 3

.10697E+04	.10742E+04	.10819E+04	.10848E+04
.13099E+04	.13115E+04	.13137E+04	.13153E+04
.14415E+04	.14419E+04	.14425E+04	.14431E+04
.15021E+04	.15022E+04	.15022E+04	.15023E+04

FOR SUBSURFACE 5

- .11944E+04	- .11943E+04	- .11941E+04	- .11940E+04
- .11322E+04	- .11317E+04	- .11309E+04	- .11304E+04
- .10005E+04	- .99997E+03	- .99827E+03	- .99730E+03
- .75270E+03	- .75175E+03	- .75051E+03	- .74969E+03

FOR SUBSURFACE 6

- .29311E+03	- .29549E+03	- .29875E+03	- .30398E+03
- .41211E+02	- .41535E+02	- .41983E+02	- .42293E+02
.18245E+03	.18436E+03	.18757E+03	.18973E+03
.50453E+03	.51033E+03	.51987E+03	.52610E+03

FOR SUBSURFACE 7

.10697E+04	.10742E+04	.10805E+04	.10848E+04
.13099E+04	.13115E+04	.13137E+04	.13153E+04
.14415E+04	.14419E+04	.14426E+04	.14431E+04
.15021E+04	.15022E+04	.15022E+04	.15023E+04

FOR SUBSURFACE 9

- .11944E+04	- .11943E+04	- .11941E+04	- .11940E+04
- .11322E+04	- .11317E+04	- .11309E+04	- .11304E+04
- .10005E+04	- .99957E+03	- .99827E+03	- .99738E+03
- .75270E+03	- .75175E+03	- .75051E+03	- .74909E+03

FOR SUBSURFACE 10

- .29311E+03	- .29549E+03	- .29875E+03	- .30398E+03
- .41211E+02	- .41535E+02	- .41983E+02	- .42293E+02
.18245E+03	.18436E+03	.18757E+03	.18973E+03
.50453E+03	.51033E+03	.51987E+03	.52610E+03

FOR SUBSURFACE 11

.10697E+04	.10742E+04	.10805E+04	.10840E+04
.13099E+04	.13115E+04	.13137E+04	.13153E+04
.14415E+04	.14419E+04	.14426E+04	.14431E+04
.15021E+04	.15022E+04	.15022E+04	.15023E+04

FOR SUBSURFACE 13

-.11944E+04	-.11343E+04	-.11941E+04	-.11940E+04
-.11322E+04	-.11317E+04	-.11309E+04	-.11304E+04
-.10055E+04	-.93937E+03	-.49827E+03	-.93738E+03
-.75270E+03	-.75175E+03	-.75051E+03	-.74969E+03

FOR SUBSURFACE 14

-.29311E+03	-.29549E+03	-.29875E+03	-.30098E+03
-.41211E+02	-.41335E+02	-.41983E+02	-.42293E+02
.18245E+03	.18455E+03	.18757E+03	.18973E+03
.50453E+03	.51133E+03	.51987E+03	.52510E+03

FOR SUBSURFACE 15

.10697E+04	.10742E+04	.10805E+04	.10840E+04
.13099E+04	.13115E+04	.13137E+04	.13153E+04
.14415E+04	.14419E+04	.14426E+04	.14431E+04
.15021E+04	.15022E+04	.15022E+04	.15023E+04

The Distribution of the Velocity Potential

FOR SUBSURFACE 1			
- .67872E+03	- .67879E+03	- .67892E+03	- .67915E+03
- .64670E+03	- .64671E+03	- .64690E+03	- .64750E+03
- .58307E+03	- .58329E+03	- .58396E+03	- .58536E+03
- .45087E+03	- .45151E+03	- .45303E+03	- .45560E+03
FOR SUBSURFACE 2			
- .12407E+03	- .12732E+03	- .13420E+03	- .14102E+03
- .11810E+02	- .15937E+02	- .22830E+02	- .31136E+02
.78425E+02	.72959E+02	.63175E+02	.51499E+02
.21893E+03	.21115E+03	.19549E+03	.17049E+03
FOR SUBSURFACE 3			
.76572E+03	.75131E+03	.72782E+03	.70411E+03
.90653E+03	.89511E+03	.87721E+03	.85861E+03
.96299E+03	.95337E+03	.94101E+03	.92914E+03
.96505E+03	.96313E+03	.95990E+03	.95621E+03
FOR SUBSURFACE 5			
- .68045E+03	- .68025E+03	- .67989E+03	- .67949E+03
- .65243E+03	- .65137E+03	- .65018E+03	- .64874E+03
- .59367E+03	- .59226E+03	- .58995E+03	- .58746E+03
- .46828E+03	- .46526E+03	- .46289E+03	- .45906E+03

FOR SUBSURFACE 6

$-.15193E+03$	$-.15151E+03$	$-.14998E+03$	$-.14894E+03$
$-.52254E+02$	$-.50019E+02$	$-.45609E+02$	$-.33118E+02$
$.18535E+02$	$.22224E+02$	$.29785E+02$	$.33300E+02$
$.12757E+03$	$.13228E+03$	$.14625E+03$	$.15155E+03$

FOR SUBSURFACE 7

$.65944E+03$	$.65364E+03$	$.67205E+03$	$.68527E+03$
$.82571E+03$	$.82937E+03$	$.83416E+03$	$.84398E+03$
$.90704E+03$	$.90935E+03$	$.91333E+03$	$.91267E+03$
$.94695E+03$	$.94735E+03$	$.94991E+03$	$.95274E+03$

FOR SUBSURFACE 9

$-.67872E+03$	$-.67378E+03$	$-.67692E+03$	$-.67918E+03$
$-.64670E+03$	$-.64671E+03$	$-.64694E+03$	$-.64760E+03$
$-.56307E+03$	$-.56328E+03$	$-.56396E+03$	$-.56536E+03$
$-.45887E+03$	$-.45181E+03$	$-.45303E+03$	$-.45560E+03$

FOR SUBSURFACE 10

$-.12407E+03$	$-.12732E+03$	$-.13424E+03$	$-.14102E+03$
$-.11810E+02$	$-.15337E+02$	$-.22830E+02$	$-.31136E+02$
$.78425E+02$	$.72953E+02$	$.63175E+02$	$.51699E+02$
$.21893E+03$	$.21019E+03$	$.19549E+03$	$.17849E+03$

FOR SUBSURFACE 11

.76572E+03	.75131E+03	.72782E+03	.70411E+03
.90653E+03	.89511E+03	.87721E+03	.85361E+03
.96298E+03	.95357E+03	.94101E+03	.92914E+03
.96503E+03	.95313E+03	.95950E+03	.95621E+03

FOR SUBSURFACE 13

-.68049E+03	-.53025E+03	-.67985E+03	-.67349E+03
-.65243E+03	-.65157E+03	-.65016E+03	-.64374E+03
-.59367E+03	-.53226E+03	-.58995E+03	-.53746E+03
-.46828E+03	-.46626E+03	-.46229E+03	-.45906E+03

FOR SUBSURFACE 14

-.15193E+03	-.15151E+03	-.14998E+03	-.14654E+03
-.52254E+02	-.31133E+02	-.45609E+02	-.33116E+02
.18535E+02	.22424E+02	.29785E+02	.39340E+02
.12757E+03	.13429E+03	.14625E+03	.16155E+03

FOR SUBSURFACE 15

.65948E+03	.65334E+03	.67205E+03	.63527E+03
.82571E+03	.82837E+03	.83416E+03	.84398E+03
.90764E+03	.91135E+03	.91303E+03	.91367E+03
.94696E+03	.94795E+03	.94991E+03	.95274E+03

Pressure Distribution

FOR SUBSURFACE 1			
.61577E+00	.10273E+01	.11106E+01	.11420E+01
.66014E+00	-.10644E+00	-.10991E+00	-.11134E+00
-.17570E+00	-.17734E+00	-.17959E+00	-.18145E+00
-.32859E+00	-.32903E+00	-.32882E+00	-.32753E+00
FOR SUBSURFACE 2			
-.28964E+00	-.28751E+00	-.28430E+00	-.28075E+00
-.13356E+00	-.13243E+00	-.13023E+00	-.12704E+00
-.15172E+00	-.14859E+00	-.14413E+00	-.13851E+00
-.45281E+00	-.44751E+00	-.43959E+00	-.43215E+00
FOR SUBSURFACE 3			
-.69056E+00	-.72971E+00	-.77607E+00	-.80326E+00
-.16853E+00	-.15559E+00	-.21161E+00	-.23123E+00
-.36355E-01	-.45608E-01	-.58911E-01	-.71382E-01
.28684E-02	.19030E-03	-.34147E-02	-.67867E-02
FOR SUBSURFACE 5			
.96689E+00	.10318E+01	.11214E+01	.11330E+01
-.94236E-01	-.98972E-01	-.10516E+00	-.10972E+00
-.16570E+00	-.16370E+00	-.17483E+00	-.17870E+00
-.31676E+00	-.31937E+00	-.32244E+00	-.32543E+00

FOR SUBSURFACE 6

-.27501E+00	-.27525E+00	-.27607E+00	-.27787E+00
-.11324E+00	-.11536E+00	-.11895E+00	-.12311E+00
-.11960E+00	-.12233E+00	-.12702E+00	-.13266E+00
-.42368E+00	-.42395E+00	-.42460E+00	-.42726E+00

FOR SUBSURFACE 7

-.70167E+00	-.7325E+00	-.77709E+00	-.80523E+00
-.20899E+00	-.21340E+00	-.23233E+00	-.23817E+00
-.69518E-01	-.72507E-01	-.76396E-01	-.76379E-01
-.11631E-01	-.11501E-01	-.10677E-01	-.93713E-02

FOR SUBSURFACE 9

.61577E+00	.52275E+01	.11156E+01	.11820E+01
.66014E+00	-.10544E+00	-.10991E+00	-.11134E+00
-.17570E+00	-.17794E+00	-.17959E+00	-.19045E+00
-.32859E+00	-.32903E+00	-.32882E+00	-.32753E+00

FOR SUBSURFACE 10

-.28964E+00	-.29751E+00	-.28430E+00	-.29075E+00
-.13356E+00	-.13243E+00	-.13023E+00	-.12704E+00
-.15172E+00	-.14399E+00	-.14413E+00	-.13651E+00
-.45281E+00	-.44751E+00	-.43959E+00	-.43215E+00

FOR SUBSURFACE 11

-.69056E+00	-.72371E+00	-.77507E+00	-.80526E+00
-.16858E+00	-.18538E+00	-.21101E+00	-.23123E+00
-.30355E-01	-.43501E-01	-.58911E-01	-.79362E-01
.28684E-02	.19090E-03	-.34147E-02	-.67367E-02

FOR SUBSURFACE 13

.96689E+00	.10318E+01	.11214E+01	.11630E+01
-.94236E-01	-.98472E-01	-.10516E+00	-.10972E+00
-.16570E+00	-.16970E+00	-.17483E+00	-.17070E+00
-.31676E+00	-.31937E+00	-.32266E+00	-.32543E+00

FOR SUBSURFACE 14

-.27501E+00	-.27525E+00	-.27607E+00	-.27787E+00
-.11324E+00	-.11536E+00	-.11895E+00	-.12311E+00
-.11960E+00	-.12233E+00	-.12702E+00	-.13266E+00
-.42368E+00	-.42395E+00	-.42480E+00	-.42726E+00

FOR SUBSURFACE 15

-.70167E+00	-.73428E+00	-.77709E+00	-.83423E+00
-.21099E+01	-.21941E+01	-.23233E+01	-.25517E+01
-.69518E-01	-.72907E-01	-.76396E-01	-.75379E-01
-.11431E-01	-.11401E-01	-.11877E-01	-.93713E-02

AD-A055 767

AEROSPACE SYSTEMS INC BURLINGTON MASS

F/G 20/4

ROTOR WAKE EFFECTS ON HUB/PYLON FLOW. VOLUME II. PROGRAM SHAPES--ETC(U)

MAY 78 P 500H00, R B NOLL, L MORINO, N D HAMM DAAJ02-75-C-0041

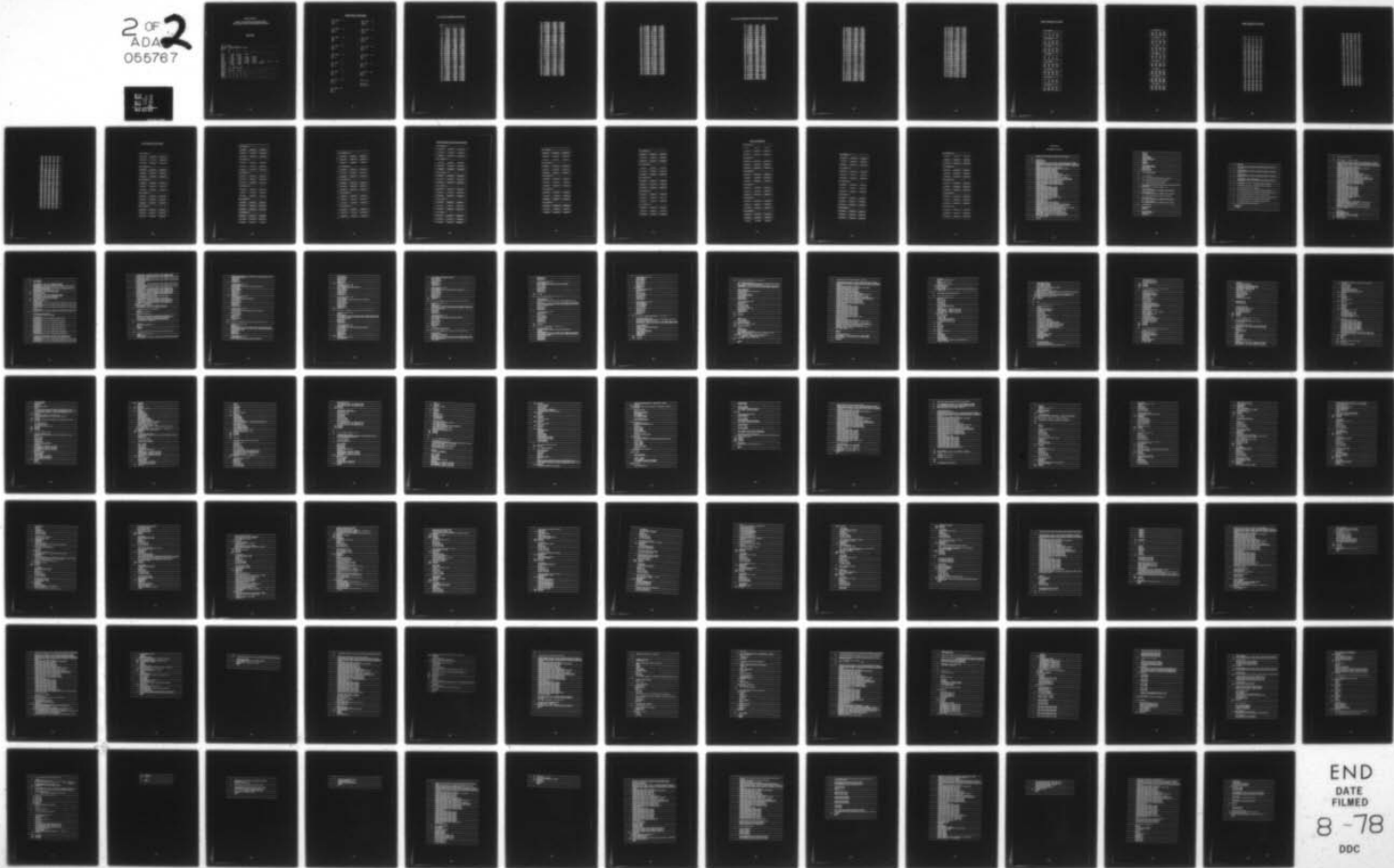
UNCLASSIFIED

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2 OF 2
ADA
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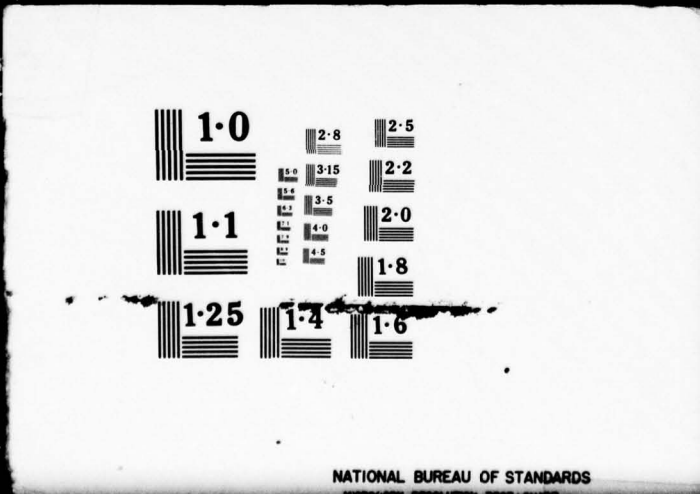


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NATIONAL BUREAU OF STANDARDS

SAMPLE CASE 4:
 MODEL 1 HELICOPTER CONFIGURATION
 WITH ROTOR WAKE AND SEPARATION EFFECTS

Data Input

```

1
PROGRAM SHAPES
HUB PYLON FLOW SEPARATION
FUSELAGE - SINGLE ROTOR (TWO BLADES)
KREAD 0
*      16      0      0
**     0      1      1      1      0      0      0      0      1
***    0      0
-----
UMAC1   .047  3600.000  -0.000
ALFA    0.000   0.000
NBOJY   1.000   9.000   18.000   36.000
NBOJY   0.000   0.000   0.000   0.000
NBOJY   0.000   0.000   0.000   0.000
NBOJY   1.450   3.250   1.450   2.900
ROTOR   20.000   8.040   11.550   15.050   0.000   0.000   .121
IHEI75  0.000   0.000   0.000   0.000   90.000
RPITCH  0.000   0.000
KBLADE  2      1
NWAKE   1      0      0      1
SPIRAL  18   3.000  450.000
-----
NPYLON  1      1
CSIAG   -60.000   1.000
KPRINT  1      1      1      1      0      1      1      1      1      1
NBOJY   3      3      2      1      1
NBOJY   3      3      1      1      1
NBOJY   3      3      2      1      1
NROTOR  3      3      2      1      1
-----

```

Specifications of the Problem

FOR PART 1
NX= 3
NY= 3

FOR PART 13
NX= 3
NY= 3

FOR PART 2
NX= 3
NY= 3

FOR PART 14
NX= 3
NY= 3

FOR PART 3
NX= 3
NY= 3

FOR PART 15
NX= 3
NY= 3

FOR PART 5
NX= 3
NY= 3

FOR PART 24
NX= 3
NY= 3

FOR PART 6
NX= 3
NY= 3

FOR PART 25
NX= 3
NY= 3

FOR PART 7
NX= 3
NY= 3

FOR PART 27
NX= 3
NY= 3

FOR PART 9
NX= 3
NY= 3

FOR PART 28
NX= 3
NY= 3

FOR PART 10
NX= 3
NY= 3

NELEM=144
KSYM= 0
KSYMZ= 0

FOR PART 11
NX= 3
NY= 3

X, Y, and Z Coordinates of the Nodes

NODE*	X	Y	Z
1	0.00000	0.00000	0.00000
2	1.00000	-0.00000	1.00333
3	4.00000	-0.00000	2.16667
4	3.00000	.00000	3.25000
5	1.00000	.24167	.93819
6	4.00000	.48333	1.07639
7	3.00000	.72500	2.01458
8	1.00000	.41858	.54167
9	4.00000	.83716	1.00333
10	3.00000	1.25574	1.62500
11	1.00000	.48333	-0.00000
12	4.00000	.96667	-0.00000
13	3.00000	1.45000	-0.00000
14	12.00000	-0.00000	3.13333
15	15.00000	-0.00000	3.01667
16	19.00000	.00000	2.90000
17	12.00000	.72500	2.71355
18	15.00000	.72500	2.61251
19	19.00000	.72500	2.51147
20	12.00000	1.25574	1.56667
21	15.00000	1.25574	1.50033
22	18.00000	1.25574	1.45000
23	12.00000	1.45000	-0.00000
24	15.00000	1.45000	-0.00000
25	18.00000	1.45000	-0.00000
26	24.00000	-0.00000	1.93333
27	34.00000	-0.00000	.96667
28	36.00000	0.00000	0.00000
29	28.00000	.48333	1.67432
30	34.00000	.24167	.83716
31	29.00000	.83716	.96667
32	34.00000	.41858	.48333
33	28.00000	.96667	-0.00000
34	34.00000	.48333	-0.00000
35	1.00000	-0.00000	-1.00333
36	4.00000	-0.00000	-2.16667
37	9.00000	.00000	-3.25000
38	1.00000	.24167	-.93819
39	4.00000	.48333	-1.07639
40	9.00000	.72500	-2.01458
41	1.00000	.41858	-.54167
42	4.00000	.83716	-1.00333
43	3.00000	1.25574	-1.62500
44	12.00000	-0.00000	-3.13333
45	15.00000	-0.00000	-3.01667
46	19.00000	.00000	-2.90000
47	12.00000	.72500	-2.71355
48	15.00000	.72500	-2.61251

49	15.00000	.72500	-2.51147
50	12.00000	1.25574	-1.56667
51	15.00000	1.25574	-1.50033
52	19.00000	1.25574	-1.45000
53	29.00000	-.00000	-1.93333
54	34.00000	-.00000	-.96667
55	29.00000	.48333	-1.67432
56	34.00000	.24167	-.83716
57	29.00000	.83716	-.96667
58	34.00000	.41858	-.48333
59	1.00000	-.24167	.93819
60	4.00000	-.48333	1.87639
61	9.00000	-.72500	2.81458
62	1.00000	-.41858	.54167
63	4.00000	-.83716	1.08333
64	9.00000	-1.25574	1.62500
65	1.00000	-.48333	-.00000
66	4.00000	-.96667	-.00000
67	9.00000	-1.45000	-.00000
68	12.00000	-.72500	2.71355
69	15.00000	-.72500	2.61251
70	18.00000	-.72500	2.51147
71	12.00000	-1.25574	1.56667
72	15.00000	-1.25574	1.50033
73	19.00000	-1.25574	1.45000
74	12.00000	-1.45000	-.00000
75	15.00000	-1.45000	-.00000
76	19.00000	-1.45000	-.00000
77	29.00000	-.48333	1.67432
78	34.00000	-.24167	.83716
79	29.00000	-.83716	.96667
80	34.00000	-.41858	.48333
81	29.00000	-.96667	-.00000
82	34.00000	-.48333	-.00000
83	1.00000	-.24167	-.93819
84	4.00000	-.48333	-1.87639
85	9.00000	-.72500	-2.81458
86	1.00000	-.41858	-.54167
87	4.00000	-.83716	-1.08333
88	9.00000	-1.25574	-1.62500
89	12.00000	-.72500	-2.71355
90	15.00000	-.72500	-2.61251
91	18.00000	-.72500	-2.51147
92	12.00000	-1.25574	-1.56667
93	15.00000	-1.25574	-1.50033
94	19.00000	-1.25574	-1.45000
95	29.00000	-.48333	-1.67432
96	34.00000	-.24167	-.83716
97	29.00000	-.83716	-.96667

99	74.00000	-4.4858	-4.48333
99	11.55000	3.75000	6.67000
100	11.93889	3.75000	6.70462
101	13.10556	3.75000	6.75642
102	15.05000	3.75000	6.67000
103	11.55000	12.77778	6.67000
104	11.93889	12.77778	6.70462
105	13.10556	12.77778	6.75642
106	15.05000	12.77778	6.67000
107	11.55000	18.19444	6.67000
108	11.93889	18.19444	6.70462
109	13.10556	18.19444	6.75642
110	15.05000	18.19444	6.67000
111	11.55000	20.00000	6.67000
112	11.93889	20.00000	6.67000
113	13.10556	20.00000	6.67000
114	15.05000	20.00000	6.67000
115	11.93889	3.75000	6.63538
116	13.10556	3.75000	6.58358
117	11.93889	12.77778	6.63538
118	13.10556	12.77778	6.58358
119	11.93889	18.19444	6.63538
120	13.10556	18.19444	6.58358
121	-11.55000	-3.75000	6.67000
122	-11.93889	-3.75000	6.70462
123	-13.10556	-3.75000	6.75642
124	-15.05000	-3.75000	6.67000
125	-11.95000	-12.77778	6.67000
126	-11.93889	-12.77778	6.70462
127	-13.10556	-12.77778	6.75642
128	-15.05000	-12.77778	6.67000
129	-11.55000	-18.19444	6.67000
130	-11.93889	-18.19444	6.70462
131	-13.10556	-18.19444	6.75642
132	-15.05000	-18.19444	6.67000
133	-11.55000	-20.00000	6.67000
134	-11.93889	-20.00000	6.67000
135	-13.10556	-20.00000	6.67000
136	-15.05000	-20.00000	6.67000
137	-11.93889	-3.75000	6.63538
138	-13.10556	-3.75000	6.58358
139	-11.93889	-12.77778	6.63538
140	-13.10556	-12.77778	6.58358
141	-11.93889	-18.19444	6.63538
142	-13.10556	-18.19444	6.58358

X, Y, and Z Coordinates of the Centroid of Aerodynamic Panels

ELEM#	XPC	YPC	ZPC
1	.50055	.06042	.50538
2	2.50277	.18125	1.51615
3	6.50719	.30208	2.52691
4	.50055	.16506	.36997
5	2.50277	.49518	1.10390
6	6.50719	.82531	1.84983
7	.50055	.22548	.13542
8	2.50277	.67643	.40625
9	6.50719	1.12739	.67708
10	10.51162	.36250	2.97787
11	13.51494	.36250	2.86901
12	16.51825	.36250	2.76016
13	10.51162	.99037	2.17995
14	13.51494	.99037	2.10026
15	16.51825	.99037	2.02058
16	10.51162	1.35287	.79792
17	13.51494	1.35287	.76875
18	16.51825	1.35287	.73958
19	23.02545	.30208	2.25478
20	31.03438	.18125	1.35287
21	35.03872	.06042	.45096
22	23.02545	.82531	1.65061
23	31.03438	.49518	.99037
24	35.03872	.16506	.33012
25	23.02545	1.12739	.60417
26	31.03438	.67643	.36250
27	35.03872	.22548	.12083
28	.50055	.06042	-.50538
29	2.50277	.18125	-1.51615
30	6.50719	.30208	-2.52691
31	.50055	.16506	-.36997
32	2.50277	.49518	-1.10390
33	6.50719	.82531	-1.84983
34	.50055	.22548	-.13542
35	2.50277	.67643	-.40625
36	6.50719	1.12739	-.67708
37	10.51162	.36250	-2.97787
38	13.51494	.36250	-2.86901
39	16.51825	.36250	-2.76016
40	10.51162	.99037	-2.17995
41	13.51494	.99037	-2.10026
42	16.51825	.99037	-2.02058
43	10.51162	1.35287	-.79792
44	13.51494	1.35287	-.76875
45	16.51825	1.35287	-.73958
46	23.02545	.30208	-2.25478
47	31.03438	.18125	-1.35287
48	35.03872	.06042	-.45096
49	23.02545	.82531	-1.65061

50	31.03430	.49518	-.99037
51	35.03872	.16506	-.33012
52	23.02545	1.12739	-.60417
53	31.03430	.67643	-.36250
54	35.03872	.22548	-.12083
55	.50055	-.06042	-.50538
56	2.50277	-.18125	1.51615
57	6.50719	-.30208	2.52691
58	.50055	-.16506	.36997
59	2.50277	-.49518	1.10990
60	6.50719	-.82531	1.84983
61	.50055	-.22548	.13542
62	2.50277	-.67643	.40625
63	6.50719	-1.12739	.67708
64	10.51162	-.36250	2.97787
65	13.51494	-.36250	2.86901
66	16.51825	-.36250	2.76016
67	19.51162	-.99037	2.17995
68	13.51494	-.99037	2.18026
69	16.51825	-.99037	2.82058
70	10.51162	-1.35297	.79792
71	13.51494	-1.35297	.76875
72	16.51825	-1.35297	.73958
73	23.02545	-.30208	2.25678
74	31.03430	-.18125	1.35287
75	35.03872	-.06042	.45096
76	23.02545	-.82531	1.65061
77	31.03430	-.49518	.99037
78	35.03872	-.16506	.33012
79	23.02545	-1.12739	-.60417
80	31.03430	-.67643	.36250
81	35.03872	-.22548	-.12083
82	.50055	-.06042	-.50538
83	2.50277	-.18125	-1.51615
84	6.50719	-.30208	-2.52691
85	.50055	-.16506	-.36997
86	2.50277	-.49518	-1.10990
87	6.50719	-.82531	-1.84983
88	.50055	-.22548	-.13542
89	2.50277	-.67643	-.40625
90	6.50719	-1.12739	-.67708
91	10.51162	-.36250	-2.97787
92	13.51494	-.36250	-2.86901
93	16.51825	-.36250	-2.76016
94	10.51162	-.99037	-2.17995
95	13.51494	-.99037	-2.18026
96	16.51825	-.99037	-2.82058
97	10.51162	-1.35297	-.79792
98	13.51494	-1.35297	-.76875

49	16.11925	-1.35287	-0.73358
100	23.12945	-0.30208	-2.25479
101	11.11430	-0.18125	-1.35287
102	35.13872	-0.06042	-0.45096
103	21.02545	-0.82531	-1.65061
104	31.03430	-0.49518	-0.99037
105	19.03872	-0.16506	-0.33012
106	23.02945	-1.12739	-0.60417
107	31.03430	-0.67663	-0.36250
108	35.03872	-0.22548	-0.12083
109	11.75744	8.26389	6.68731
110	12.53608	8.26389	6.73052
111	14.19335	8.26389	6.71321
112	11.75744	15.48611	6.68731
113	12.53608	15.48611	6.73052
114	14.09335	15.48611	6.71321
115	11.75744	19.09722	6.67866
116	12.53608	19.09722	6.70026
117	14.19335	19.09722	6.69161
118	11.75744	8.26389	6.65269
119	12.53608	8.26389	6.60344
120	14.19335	8.26389	6.62679
121	11.75744	15.48611	6.65269
122	12.53608	15.48611	6.60948
123	14.09335	15.48611	6.62679
124	11.75744	19.09722	6.66134
125	12.53608	19.09722	6.63974
126	14.19335	19.09722	6.64839
127	-11.75744	-8.26389	6.68731
128	-12.53608	-8.26389	6.73052
129	-14.09335	-8.26389	6.71321
130	-11.75744	-15.48611	6.68731
131	-12.53608	-15.48611	6.73052
132	-14.09335	-15.48611	6.71321
133	-11.75744	-19.09722	6.67866
134	-12.53608	-19.09722	6.70026
135	-14.09335	-19.09722	6.69161
136	-11.75744	-8.26389	6.65269
137	-12.53608	-8.26389	6.60344
138	-14.09335	-8.26389	6.62679
139	-11.75744	-15.48611	6.65269
140	-12.53608	-15.48611	6.60948
141	-14.09335	-15.48611	6.62679
142	-11.75744	-19.09722	6.66134
143	-12.53608	-19.09722	6.63974
144	-14.09335	-19.09722	6.64839

Nodal Numbering for Surfaces

FOR SURFACE 1			
1	1	1	1
2	5	8	11
3	6	9	12
4	7	10	13

FOR SURFACE 2			
4	7	10	13
14	17	20	23
15	18	21	24
16	19	22	25

FOR SURFACE 3			
16	19	22	25
26	29	31	33
27	30	32	34
23	28	28	28

FOR SURFACE 5			
1	1	1	1
35	38	41	11
36	39	42	12
37	40	43	13

FOR SURFACE 6			
37	40	43	13
44	47	50	23
45	48	51	24
46	49	52	25

FOR SURFACE 7			
46	49	52	25
53	55	57	33
54	56	58	34
23	28	28	28

FOR SURFACE 9			
1	1	1	1
2	59	62	65
3	60	63	66
4	61	64	67

FOR SURFACE 10			
4	61	64	67
14	68	71	74
15	69	72	75
16	70	73	76

FOR SURFACE 11			
16	70	73	76
26	77	79	81
27	78	80	82
28	28	28	28

FOR SURFACE 13			
1	1	1	1
75	83	86	89
36	84	87	86
37	85	88	87

FOR SURFACE 14			
37	95	88	67
44	69	92	74
45	90	93	79
46	91	94	76

FOR SURFACE 15			
46	91	94	76
53	95	97	81
54	96	98	82
28	28	28	28

FOR SURFACE 24			
99	103	107	111
109	104	108	112
101	105	109	113
102	106	110	114

FOR SURFACE 25			
99	107	107	111
115	117	119	112
116	118	120	113
102	106	110	114

FOR SURFACE 27			
121	125	129	133
122	126	130	134
123	127	131	135
124	128	132	136

FOR SURFACE 28			
121	125	129	133
137	139	141	134
138	140	142	135
124	128	132	136

Nodal Numbering for Elements

ELEM	++	+-	-+	--
1	5	2	1	1
2	6	3	5	2
3	7	4	6	3
4	8	5	1	1
5	9	6	8	5
6	10	7	9	6
7	11	8	1	1
8	12	9	11	8
9	13	10	12	9
10	17	14	7	4
11	18	15	17	14
12	19	16	18	15
13	20	17	18	7
14	21	18	20	17
15	22	19	21	18
16	23	20	13	10
17	24	21	23	20
18	25	22	24	21
19	26	23	19	16
20	27	27	29	26
21	28	28	30	27
22	31	29	22	19
23	32	30	31	29
24	28	28	32	30
25	33	31	25	22
26	34	32	33	31
27	28	28	34	32
28	35	38	1	1
29	36	39	35	38
30	37	40	36	39
31	38	41	1	1
32	39	42	38	41
33	40	43	39	42
34	41	11	1	1
35	42	12	41	11
36	43	13	42	12
37	44	47	37	40
38	45	48	44	47
39	46	49	45	48
40	47	50	40	43
41	48	51	47	50
42	49	52	48	51
43	50	23	43	13
44	51	24	50	23
45	52	25	51	24
46	53	55	46	49
47	54	56	53	55
48	28	28	54	56

49	55	57	49	52
50	56	58	55	57
51	28	28	56	58
52	57	33	52	29
53	58	34	57	33
54	28	28	58	34
55	2	59	1	1
56	9	60	2	59
57	4	61	3	60
58	59	62	1	1
59	60	63	59	62
60	61	64	60	63
61	52	65	1	1
62	63	66	62	65
63	64	67	63	66
64	14	68	4	61
65	15	69	14	68
66	16	70	15	69
67	68	71	61	66
68	69	72	68	71
69	70	73	69	72
70	71	74	64	67
71	72	75	71	74
72	73	76	72	75
73	26	77	16	70
74	27	78	26	77
75	28	28	27	78
76	77	79	70	73
77	78	80	77	79
79	28	28	78	80
79	79	81	73	76
80	80	82	79	81
81	28	28	80	82
82	33	35	1	1
83	34	36	83	35
84	35	37	84	36
85	86	83	1	1
86	37	84	86	83
87	88	85	87	84
88	69	86	1	1
89	66	87	65	86
90	67	88	66	87
91	88	86	85	87
92	30	49	89	44
93	41	46	90	45
94	32	89	88	85
95	43	90	92	88
96	94	91	93	90

97	74	92	67	88
98	75	93	74	92
99	76	94	75	93
100	95	53	91	46
101	46	54	95	53
102	26	28	96	54
103	97	95	94	91
104	98	96	97	95
105	28	28	98	96
106	81	97	76	94
107	82	98	81	97
108	24	28	82	98
109	105	100	103	99
110	109	101	104	100
111	106	102	105	101
112	108	104	107	103
113	109	105	108	104
114	110	106	109	105
115	112	108	111	107
116	113	109	112	108
117	114	110	113	109
118	115	111	99	103
119	116	112	115	117
120	102	106	116	118
121	117	119	103	107
122	118	120	117	119
123	106	110	118	120
124	119	112	107	111
125	120	113	119	112
126	110	114	120	113
127	126	122	125	121
128	127	123	126	122
129	128	124	127	123
130	130	126	129	125
131	131	127	130	126
132	132	128	131	127
133	133	130	133	129
134	135	131	134	130
135	136	132	135	131
136	137	139	121	125
137	138	140	137	139
138	124	128	138	140
139	139	141	125	129
140	140	142	139	141
141	128	132	140	142
142	141	134	129	133
143	142	135	141	134
144	132	136	142	135

The Distribution of the Source

FOR SURFACE 1

- .897355E+02	- .89462E+02	- .89131E+02
---------------	--------------	--------------

- .84277E+02	- .84701E+02	- .84595E+02
--------------	--------------	--------------

- .74571E+02	- .74639E+02	- .74282E+02
--------------	--------------	--------------

FOR SURFACE 2

- .47538E+02	- .49261E+02	- .4883E+02
--------------	--------------	-------------

- .27588E+02	- .28720E+02	- .30053E+02
--------------	--------------	--------------

- .11036E+02	- .11957E+02	- .14521E+02
--------------	--------------	--------------

FOR SURFACE 3

. 75639E+01	. 69589E+01	. 54540E+01
-------------	-------------	-------------

. 13015E+02	. 13476E+02	. 12748E+02
-------------	-------------	-------------

. 16507E+02	. 16315E+02	. 15939E+02
-------------	-------------	-------------

FOR SURFACE 4

- .89556E+02	- .89430E+02	- .89141E+02
--------------	--------------	--------------

- .84723E+02	- .84573E+02	- .84537E+02
--------------	--------------	--------------

- .72623E+02	- .72787E+02	- .73400E+02
--------------	--------------	--------------

FOR SURFACE 5

- .42652E+02	- .44604E+02	- .47102E+02
--------------	--------------	--------------

- .29142E+02	- .29856E+02	- .30445E+02
--------------	--------------	--------------

- .18342E+02	- .17929E+02	- .16805E+02
--------------	--------------	--------------

FOR SUBSURFACE 7

.10734E+01 .20296E+01 .35994E+01

.10713E+02 .11148E+02 .11893E+02

.19377E+02 .15562E+02 .15663E+02

FOR SUBSURFACE 9

-.39783E+02 -.89429E+02 -.89089E+02

-.94614E+02 -.84210E+02 -.84007E+02

-.73682E+02 -.72497E+02 -.71870E+02

FOR SUBSURFACE 10

-.46084E+02 -.46123E+02 -.46406E+02

-.27711E+02 -.29855E+02 -.30431E+02

-.12367E+02 -.14895E+02 -.17301E+02

FOR SUBSURFACE 11

.70612E+01 .56619E+01 .38513E+01

.13799E+02 .13237E+02 .12415E+02

.16318E+02 .16263E+02 .15863E+02

FOR SUBSURFACE 13

-.89829E+02 -.89462E+02 -.89188E+02

-.84522E+02 -.84266E+02 -.84043E+02

-.72382E+02 -.71951E+02 -.71744E+02

FOR SUBSURFACE 14

-.42942E+02 -.44183E+02 -.45755E+02

-.29117E+02 -.30135E+02 -.30047E+02

-.18788E+02 -.19842E+02 -.18739E+02

FOR SUBSURFACE 15

.74244E+00 .10670E+01 .21650E+01

.10617E+02 .10890E+02 .11551E+02

.15596E+02 .15506E+02 .15569E+02

FOR SUBSURFACE 24

- .78755E+03 -.70861E+03 -.62415E+03

-.26141E+03 -.48756E+03 -.61629E+03

.23480E+03 .48777E+03 -.42148E+02

FOR SUBSURFACE 25

-.38756E+03 -.70861E+03 -.62415E+03

-.26143E+03 -.48756E+03 -.61628E+03

.23479E+03 .48777E+03 -.42148E+02

FOR SUBSURFACE 27

-.37486E+03 -.69827E+03 -.61925E+03

-.25512E+03 -.48144E+03 -.61353E+03

.22337E+03 .39747E+03 -.48037E+02

FOR SUBSURFACE 28

-.37646E+03 -.69828E+03 -.61925E+03

-.25517E+03 -.48144E+03 -.61351E+03

.22396E+03 .39747E+03 -.48039E+02

The Distribution of the Velocity Potential

FOR SURFACE 1		
- .46059E+02	- .45837E+02	- .45642E+02
- .43106E+02	- .43535E+02	- .43832E+02
- .38208E+02	- .39314E+02	- .39935E+02
FOR SURFACE 2		
- .20751E+02	- .23836E+02	- .25509E+02
- .96652E+01	- .11712E+02	- .15051E+02
.59479E+01	.58202E+01	.19665E+01
FOR SURFACE 3		
- 1.0816E+03	- .10755E+03	- .81939E+02
- .50172E+03	- .35268E+03	- .23162E+03
- .28712E+03	- .26498E+03	- .23473E+03
FOR SURFACE 4		
- .46449E+02	- .46133E+02	- .45735E+02
- .44569E+02	- .44338E+02	- .44107E+02
- .40463E+02	- .40151E+02	- .40099E+02
FOR SURFACE 5		
- .24928E+02	- .25525E+02	- .25893E+02
- .20842E+02	- .20185E+02	- .18347E+02
- .17573E+02	- .14880E+02	- .10502E+02
FOR SURFACE 6		
- .46017E+02	- .51944E+02	- .68332E+02
- .11498E+03	- .12897E+03	- .16636E+03
- .17639E+03	- .18723E+03	- .20720E+03

FOR SURFACE 9

-.46016E+02 -.45697E+02 -.45455E+02

- .42909E+02 -.42573E+02 -.42661E+02

- .36572E+02 -.35876E+02 -.36314E+02

FOR SURFACE 10

- .18557E+02 -.19743E+02 - .22044E+02

-.96158E+01 -.12030E+02 -.15513E+02

.41598E+01 .20712E+01 -.17663E+01

FOR SUBSURFACE 11

-.10339E+03 -.10960E+03 -.84478E+02

-.50095E+03 -.35233E+03 -.23248E+03

-.28715E+03 -.26507E+03 -.23491E+03

FOR SUBSURFACE 13

-.46401E+02 -.45972E+02 -.45552E+02

-.44297E+02 -.43636E+02 -.43068E+02

-.39852E+02 -.38630E+02 -.37418E+02

FOR SURFACE 14

-.24641E+02 -.24636E+02 -.23897E+02

-.21848E+02 -.20633E+02 -.18778E+02

- .18526E+02 -.16667E+02 -.13421E+02

FOR SUBSURFACE 15

-.46536E+02 -.53573E+02 -.62687E+02

- .11372E+03 -.12969E+03 -.16475E+03

-.17643E+03 -.18733E+03 -.20732E+03

FOR SUBSURFACE 24

-.19908E+03 -.36608E+03 -.31439E+03

-.13719E+03 -.26042E+03 -.31484E+03

.13121E+03 .22146E+03 -.16031E+02

FOR SUBSURFACE 25

- 20791E+03 -.36731E+03 -.31523E+03

-.14058E+03 -.26242E+03 -.31620E+03

.12759E+03 .21921E+03 -.17558E+02

FOR SUBSURFACE 27

-.19781E+03 -.36264E+03 -.31327E+03

-.13848E+03 -.25951E+03 -.31511E+03

.11989E+03 .21306E+03 -.21094E+02

FOR SUBSURFACE 28

-.19725E+03 -.36280E+03 -.31348E+03

-.13844E+03 -.25976E+03 -.31532E+03

.11955E+03 .21280E+03 -.21302E+02

Pressure Distribution

FOR SUBSURFACE 1		
.16013E+01	.12411E+01	.13861E+01
.47196E+00	-.37578E-01	- .35702E-01
-.75173E-01	-.71136E-01	-.69669E-01
FOR SUBSURFACE 2		
-.17921E+00	-.17405E+00	- .15750E+00
-.16858E+00	-.18174E+00	-.15948E+00
.62716E+00	.56760E+00	.43009E+00
FOR SUBSURFACE 3		
.91196E+00	.75819E+00	.48350E+00
.73212E+00	.86923E+00	.57373E+00
-.15981E+01	.89266E-01	.15728E+00
FOR SUBSURFACE 5		
.92646E+00	.12525E+01	.13879E+01
- .35608E-01	-.38367E-01	- .36135E-01
-.70646E-01	-.70751E-01	-.69485E-01
FOR SUBSURFACE 6		
-.12449E+00	-.12867E+00	-.13996E+00
-.48501E-01	-.68291E-01	-.10844E+00
.17148E+00	.28746E+00	.28982E+00
FOR SUBSURFACE 7		
.18616E+00	.21073E+00	.38861E+00
.38819E+00	.34409E+00	.48358E+00
.11380E+01	.73242E+00	.39221E+00

FOR SUBSURFACE 9

.17426E+01 .12271E+01 .13669E+01

.45739E+00 -.59901E-01 -.55051E-01

-.89829E-01 -.83759E-01 -.77312E-01

FOR SUBSURFACE 10

-.16883E+00 -.15273E+00 -.13613E+00

-.14938E+00 -.13943E+00 -.11648E+00

.52823E+00 .57705E+00 .44364E+00

FOR SUBSURFACE 11

.31436E+00 .75143E+00 .47793E+00

.72772E+00 .86170E+00 .56648E+00

-.15614E+01 .81267E-01 .15059E+00

FOR SUBSURFACE 13

.91495E+00 .12334E+01 .13684E+01

-.44118E-01 -.52038E-01 -.52583E-01

-.74145E-01 -.75231E-01 -.74789E-01

FOR SUBSURFACE 14

-.11879E+00 -.11990E+00 -.12045E+00

-.43102E-01 -.50677E-01 -.77182E-01

.17265E+00 .21433E+00 .30116E+00

FOR SUBSURFACE 15

.18181E+00	.20744E+00	.29630E+00
.37629E+00	.33818E+00	.39673E+00
.11291E+01	.72403E+00	.38526E+00

FOR SUBSURFACE 24

-.24559E+03	-.41632E+03	-.15649E+03
-.40284E+03	-.87233E+03	-.90483E+03
-.17987E+03	-.47176E+03	-.66969E+03

FOR SUBSURFACE 25

-.23212E+03	-.39809E+03	-.14613E+03
-.40121E+03	-.86989E+03	-.90090E+03
-.18310E+03	-.47636E+03	-.67019E+03

FOR SUBSURFACE 27

-.22548E+03	-.39161E+03	-.14203E+03
-.37732E+03	-.83780E+03	-.87557E+03
-.16408E+03	-.45538E+03	-.65340E+03

FOR SUBSURFACE 28

-.22492E+03	-.38923E+03	-.14061E+03
-.37728E+03	-.83759E+03	-.87504E+03
-.16944E+03	-.45653E+03	-.65346E+03

SECTION 6
PROGRAM LISTING

```

PROGRAM MAIN(INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT)
C
C
C      NS(MAX)=34
C      NELEH(MAX)=400
C      NMODE(MAX)=350
COMMON/ZZZ1/NX(34),NY(34),NX1(34),KSY1M1,KSYMMZ,NSYMH1,NSYMHZ
COMMON/ZZZ2/NSFX,NSBODY,NS,NT(34),TSEAF(34),KNORML(34),KNAKES(34)
COMMON/ZZZ3/NPYLON,NBODY1,NBODY2,NBODY3,NVTAIL,NSHAFT,NHUB,NSHANK,
1  NBLADE
COMMON/ZZZ4/UMACH,OMEGA,ALFA,ABETA,AREA
COMMON/ZZZ5/YDYCT1,YDYCT2,ZDYCT1,RXBY1,RBYV1,RZBY1
COMMON/ZZZ6/XNOSE,XBD1,X3D2,XTAIL
COMMON/ZZZ7/YNOSE,YBD1,Y3D2,YTAIL
COMMON/ZZZ8/ZNOSE,ZBD1,Z3D2,ZTAIL
COMMON/ZZZ9/ZYBD1,RZBD1,ZYBD2,RZBD2
COMMON/ZZZ10/RSHAFT,LSHAF1,RSHANK,LSHANK
COMMON/ZZZ11/XMUSCR,YMUSCR,ZMUSCR,XMUS,RYMUS,RZMUS
COMMON/ZZZ12/RROTOR,BCHRD,TAUBL,ALFA3
COMMON/ZZZ13/TMET1,TMET2,TMET3,CONING,AZIMUTH
COMMON/ZZZ14/KBLADE,TANEB,TANTEB,XBLE,X3TE,KROTOR(34)
COMMON/ZZZ15/MSRAN,XLEZ1,XLEZ2,TANLE1,TANTE1,TAU,ZVTAIL
COMMON/ZZZ16/NWAKPY,NWAK1B,NWAKSK,NWAKB
COMMON/ZZZ17/WAKPY,WAK1B,WAKSK,WAKB
COMMON/ZZZ18/WANGPY,WANG1B,WANGSK,WANGB
COMMON/ZZZ19/KPRINT(10),KREAD,KWRITE,KREAD
COMMON/ZZZ20/PI
COMMON/ZZZ21/KPY1,KPY2
COMMON/ZZZ22/KNSELE,KNSS1P,KNSTYP
COMMON/ZZZ23/KRDELE,KRDS1P,KRO1YP
COMMON/ZZZ24/KTNELE,KTNS1P,KTNTYP
COMMON/ZZZ25/KPYELE,KPVS1P,KPYTYP
COMMON/ZZZ26/KVTELE,KVTS1P,KVTTYP
COMMON/ZZZ27/KSMELE,KSMSHP,KSHTYP
COMMON/ZZZ28/KHBELE,KHBSHP,KHBTYP
COMMON/ZZZ29/KSKELE,KSIS1P,KSXTYP
COMMON/ZZZ30/KBLELE,KBLS1P,KBLTYP
COMMON/ZZZ31/NSTAG,NVORT,NSPTRAL,SPTRAL
COMMON/ZZZ32/CSTAG,CVORT
COMMON/ZZZ33/UMAKE
COMMON/ZZZ34/YCUT
COMMON/ZZZ35/TMIST,RTMIST,TMIST
COMMON/ZZZ36/XCTR,YCTR,ZCTR,RX,RY,RZ
COMMON/ZZZ37/MSRAN,XLEZ1,XLEZ2,TANLE1,TANTE1,TAU,ZP
DIMENSION VELY(250),VELZ(250),PHI3(250),KROTOR(250)
DIMENSION CP(250),VELX(250),CG(2),AVG(250)
DIMENSION PC(3,250),P1(3,250),P2(3,250),P3(3,250),K(3,250)
DIMENSION KWAKE(250),MODE(4,250),NOECT(40,34)
DIMENSION PHIC(250),PHI1(250),PHI2(250),BC(250)
DIMENSION AA(62500),SOUCF(250),S2(250)
EQUIVALENCE (AA(1),PHIC(1)),(AA(401),PHI1(1))
EQUIVALENCE (AA(401),PHI2(1)),(AA(1201),PHI3(1))
EQUIVALENCE (AA(1601),V_X(1)),(AA(1201),VELY(1))
EQUIVALENCE (AA(2401),V_Z(1)),(AA(2801),CP(1))
REAL LSHAFT,LSHANK
C
NREAD=9

```

```

NWRITE=6
NXMAX=6
NYMAX=6
NTHAX=600
NXMAXP=NXMAX+1
NYMAXP=NYMAX+1
NXYMP=NXMAXP*NYMAXP
NSTAG=0
NVORT=0
NSPIRAL=0
NNAKBL=0
C
READ(NREAD,2) NCASE
WRITE(NWRITE,2) NCASE
2 FORMAT(10I5)
3 FORMAT(10F8,3)
4 FORMAT(2A4,2I5)
C
DO 999 ICASE=1,NCASE
C
C CALL DATA(MELEM)
C
C CALL PREPRO(MNODE,NXYMP,NOFCT,MELEM,NTHAX)
C
C CALL COORD(MELEM,NXYMP,NOFCT,XK,MNODE)
C
C CALL CHECK(MELEM,NXMAX,NYMAX,NTHAX)
C
C CALL GEOMET(MELEM,NXYMP,NOFCT,MNODE,XK,MNODE,KMAKE,KROR)
WRITE(6,60)
60 FORMAT(10X,'--- MATN FRM GEOMAT ---')
C
IF(KPRINT(1).EQ.1)
1 CALL PRINTA(MELEM,NXYMP,XK,MNODE,PC,NOFCT,MNODE,1)
C
IF(KPRINT(2).EQ.1)
1CALL PRINTA(MELEM,NXYMP,XK,MNODE,PC,NOFCT,MNODE,2)
C
CALL VEC123(MELEM,MNODE,PC,P1,P2,P3,XK,MNODE)
C
IF(KPRINT(3).EQ.1)
1CALL PRINTA(MELEM,NXYMP,XK,MNODE,PC,NOFCT,MNODE,3)
C
IF(KPRINT(4).EQ.1)
1CALL PRINTA(MELEM,NXYMP,XK,MNODE,PC,NOFCT,MNODE,4)
C
MESQ=MELEM/2
C
DO 6 NN=1,MESQ
AA(NN)=0.0
6 CONTINUE
C
DO 0 I=1,MELEM
NNN=I+(I-1)*MELEM
SOURCE(I)=0.0
AA(NNN)=1.0

```

```

9 CONTINUE
C
CALL COEFF(NELEM,PC,NNODE,XK,NODE,KWAKE,NESQ,AA,SOURCE,BC,
1 KROTOR,1)
C
IF(MSTAG.NE.0)
1 CALL COEFF(NELEM,PC,NNODE,XK,NODE,KWAKE,NESQ,AA,SOURCE,BC,
2 KROTOR,2)
C
IF(MVORT.NE.0)
1 CALL COEFF(NELEM,PC,NNODE,XK,NODE,KWAKE,NESQ,AA,SOURCE,BC,
2 KROTOR,3)
C
IF(NBLADE.EQ.1.AND.NMACBL.NE.0)
1 CALL COEFF(NELEM,PC,NNODE,XK,NODE,KWAKE,NESQ,AA,SOURCE,BC,
2 KROTOR,4)
C
IF(KPRINT(5).EQ.1)CALL :2INTB(NELEM,NESQ,AA,SOURCE,1)
C
IF(KPRINT(6).EQ.1)CALL :2INTB(NELEM,NESQ,AA,SOURCE,2)
C
CALL SOLUTM(NELEM,NESQ,1A,SOURCE)
C
IF(KPRINT(7).EQ.1)CALL :2INTB(NELEM,NESQ,AA,SOURCE,3)
C
CALL AVERAG(SOURCE,SOR,22,NELEM,NODE,NOEFT,MYXMP,NNODE,AVG)
C
CALL RMT(SOR,NNODE,NODE,2MTC,RMT1,RMT2,RMT3,NELEM)
C
CALL VELXYZ(VELX,VELY,VELZ,RMT1,RMT2,RMT3,PC,R1,R2,R3,NELEM)
C
CALL CPTMRCR(VELX,VELY,VELZ,RMT3,NELEM,PC,KROTOR)
C
IF(KPRINT(8).EQ.1)CALL :2INTB(NELEM,NESQ,AA,CP,A)
C
CALL FCRCE(NNODE,XK,NELE4,NODE,C2)
C
999 CONTINUE
1000 STOP
END

```



```

C
SUBROUTINE DATA(MFILEM)
C
C
C DATE CREATED : MARCH 31, 1975
C
COMMON/ZZZ1/IX(34),NY(34),NXY(34),KSYMNY,KSYMHZ,NSYMHY,NSYMHZ
COMMON/ZZZ2/NSFX,NSBODY,NS,NT(34),TSEACE(34),KNORM(34),KNAKES(34)
COMMON/ZZZ3/NPYLON,NBODY1,NBODY2,NBODY3,NVTAIL,NSHAFT,NHUB,NSHANK,
1 NBLADE
COMMON/ZZZ4/UMACH,OMEGA,ALFA,ABETA
COMMON/ZZZ5/YBYCTR,YBYCTR,ZBYCTR,RYBYL,ZBYL,RZBYL
COMMON/ZZZ6/INOSE,XB01,XB02,XTAIL
COMMON/ZZZ7/YNOSE,YB01,YB02,YTAIL
COMMON/ZZZ8/ZNOSE,ZB01,ZB02,ZTAIL
COMMON/ZZZ9/RBY01,RZB01,RYB02,RZB02
COMMON/ZZZ10/RSHAFT,LSHAFT,RSHANK,LSHANK
COMMON/ZZZ11/YMUBCR,YMUBCR,ZMUBCR,RXMUB,YMUB,RZMUB
COMMON/ZZZ12/RROTOR,BCH RD,TAUBL,ALFA3
COMMON/ZZZ13/TMET75,TMET1C,TMET5,CONING,AZMUTH
COMMON/ZZZ14/KBLADE,TAN EB,TANTEB,XBLE,X9TE,KROTORS(34)
COMMON/ZZZ15/MSPAN,XLEZV,XTEZV,TANLEV,TANTEV,TAU,ZYTAIL
COMMON/ZZZ16/NWAKPY,NWAK1B,NWAKSK,NWAKBL
COMMON/ZZZ17/WAKPY,WAK1B,WAKSK,WAKBL
COMMON/ZZZ18/WANGPY,WANG1B,WANGSK,WANGBL
COMMON/ZZZ19/KPRINT(18),NREAD,NWRITE,KREAD
COMMON/ZZZ20/PI
COMMON/ZZZ21/KRY1,KRY2
COMMON/ZZZ22/KNSELE,KNSE1P,KNSTYP
COMMON/ZZZ23/KBELE,KBE1P,KBTYP
COMMON/ZZZ24/KNELE,KNSE1P,KNTYP
COMMON/ZZZ25/KRYELE,KRYS1P,KRYTYP
COMMON/ZZZ26/KVTELE,KVTS1P,KVTYP
COMMON/ZZZ27/KSELE,KSE1P,KSTYP
COMMON/ZZZ28/KHBELE,KHBSHP,KHBTYP
COMMON/ZZZ29/KSKELE,KSK1P,KSKTYP
COMMON/ZZZ30/KBLELE,KBL1P,KBLTYP
COMMON/ZZZ31/NSTAG,NVORT,NSPIRAL,SPTRAL
COMMON/ZZZ32/CSTAG,CVORT
COMMON/ZZZ33/VCUT
COMMON/ZZZ33/UWAKE
COMMON/ZZZ34/YCTR,YCTR,ZCTR,RY,RZ
COMMON/ZZZ35/HSPAN,XLEZV,XTEZV,TANLEH,TANTEH,TAUH,ZP
COMMON/ZZZ35/TMIST,RTMIST,TMIST
DIMENSION AC1ORD(20),WNP(2),WNP1(2),WNP2(2),WNP3(2)
DIMENSION GG(20),KSEACE(20)
DIMENSION TCHORD(10),TAKIS(10),VCHORD(10),VAXIS(10)
REAL LSHAFT,LSHANK
C
NSFX= 8
DO 18 I=1,3
READ(NREAD,18) GG
19 WRITE(NWRITE,20)GG
READ(NREAD,18) GG(1),GG(2),KREAD
WRITE(NWRITE,20)GG(1),GG(2),KREAD
18 FORMAT(28A4)
20 FORMAT(1X,28A4)

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```

C
C USE KSYMMY=0
C USE KSYMMZ=0
READ(NREAD,18) GG(1),GG(2),NS,KSYMMY,KSYMMZ
WRITE(NWRITE,28)GG(1),GG(2),NS,KSYMMY,KSYMMZ
READ(NREAD,18) GG(1),GG(2),NPYLON,NBODY1,NBODY2,NBODY3,NVTAIL,
1 NSHAFT,NHUB,NSHANK,NBLADE
WRITE(NWRITE,28)GG(1),GG(2),NPYLON,NBODY1,NBODY2,NBODY3,NVTAIL,
1 NSHAFT,NHUB,NSHANK,NBLADE
READ(NREAD,18) GG(1),G(2),KPYL1,KPYL2
WRITE(NWRITE,28)GG(1),G(2),KPYL1,KPYL2
18 FORMAT(2A4,10I5)
28 FORMAT(1X,2A4,10I5)
READ(NREAD,12) GG(1),GG(2),UMACH,OMEGA,AREA
WRITE(NWRITE,22)GG(1),GG(2),UMACH,OMEGA,AREA
READ(NREAD,12) GG(1),GG(2),ALFA,ABETA
WRITE(NWRITE,22)GG(1),G(2),ALFA,ABETA
12 FORMAT(2A4,7F8.3)
22 FORMAT(1X,2A4,7E10.3)
IF(NPYLON.EQ.1)
1READ(NREAD,12) GG(1),G(2),XRYCTR,YRYCTR,ZRYCTR,XPY1,RPY1,RZY1
IF(NPYLON.EQ.1)
1WRITE(NWRITE,22)GG(1),G(2),XRYCTR,YRYCTR,ZRYCTR,XPY1,RPY1,RZY1
IF(NVTAIL.EQ.1)
1READ(NREAD,12) GG(1),G(2),WSPAN,XLEZV,XTEZV,TANLEV,TANTEV,TAUV
2,ZPV
TE(NVTAIL.EQ.1)
1WRITE(NWRITE,22) GG(1),GG(2),WSPAN,XLEZV,XTEZV,TANLEV,TANTEV,TAUV
2,ZPV
C
NTBD=NBODY1+NBODY2+NBODY3
NROTOR=NSHAFT+NHUB+NSHANK+NBLADE
C
IF(NTBD.NE.0)
1READ(NREAD,12)GG(1),GG(2),XNOSE,Y801,Y802,XTAIL
IF(NTBD.NE.0)
1WRITE(NWRITE,22)GG(1),GG(2),XNOSE,Y801,Y802,XTAIL
IF(NT80.NE.0)
1READ(NREAD,12) GG(1),G(2),YNOSE,Y801,Y802,XTAIL
IF(NT80.NE.0)
1WRITE(NWRITE,22)GG(1),G(2),YNOSE,Y801,Y802,XTAIL
IF(NT80.NE.0)
1READ(NREAD,12) GG(1),G(2),ZNOSE,Z801,Z802,ZTAIL
IF(NT80.NE.0)
1WRITE(NWRITE,22)GG(1),G(2),ZNOSE,Z801,Z802,ZTAIL
IF(NT801.NE.0)
1READ(NREAD,12) GG(1),GG(2),RY801,RZ801,RY802,RZ802
IF(NT80.NE.0)
1WRITE(NWRITE,22)GG(1),G(2),RY801,RZ801,RY802,RZ802
C
TE(NSHAFT.EQ.1)READ(NREAD,12) GG(1),GG(2),RSHAFT,LSHAFT
IF(NSHAFT.EQ.1)WRITE(NWRITE,22)GG(1),GG(2),RSHAFT,LSHAFT
TE(NHUB.EQ.1)
1READ(NREAD,12)GG(1),GG(2),XHUBCR,YHUBCR,ZHUBCR,RXHUB,RYHUB,RZHUB
TE(NHUB.EQ.1)
1WRITE(NWRITE,22)GG(1),GG(2),XHUBCR,YHUBCR,ZHUBCR,RXHUB,RYHUB,RZHUB

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IF(NSHANK.EQ.1) READ(NREAD,12)GG(1),GG(2),RSHANK,LSHANK
IF(NSHANK.EQ.1)WRITE(NWRITE,22)GG(1),GG(2),RSHANK,LSHANK
IF(NBLADE.EQ.1) READ(NREAD,12) GG(1),GG(2),RROTOR,YCUT,XBLE,XBTE,
1 TANLE,TANBE,TAU9L
IF(NBLADE.EQ.1)WRITE(NWRITE,22)GG(1),GG(2),RROTOR,YCUT,XBLE,XBTE,
1 TANLE,TANBE,TAU9L
TANLEB=TANLE
TANLEB=TANBE
IF(NBLADE.EQ.1) READ(NREAD,12)GG(1),GG(2),THET75,THET1C,THET1S,
1 CONINC,AZIMUTH
IF(NBLADE.EQ.1)WRITE(NWRITE,22)GG(1),GG(2),THET75,THET1C,THET1S,
1 CONINC,AZIMUTH
IF(NBLADE.EQ.1) READ(NREAD,12)GG(1),GG(2),RPITCH,TWIST
IF(NBLADE.EQ.1)WRITE(NWRITE,22)GG(1),GG(2),RPITCH,TWIST
IF(NBLADE.EQ.1) READ(NREAD,18)GG(1),GG(2),KBLADE,ITWIST
IF(NBLADE.EQ.1)WRITE(NWRITE,22)GG(1),GG(2),KBLADE,ITWIST
READ(NREAD,13) GG(1),G(2),NWKPY,NWKMP,NWAKSK,NWAKBL
WRITE(NWRITE,22)GG(1),G(2),NWKPY,NWKMP,NWAKSK,NWAKBL
IF((NWKMB+NWAKSK+NWAKB).NE.0)
1 READ(NREAD,16) GG(1),GG(2),NSPIRAL,SPIRAL,UNAKE
IF((NWKMB+NWAKSK+NWAKB).NE.0)
1 WRITE(NWRITE,26)GG(1),GG(2),NSPIRAL,SPIRAL,UNAKE
IF(NWKPY.EQ.1) READ(NREAD,18)GG(1),GG(2),NSTAG,NVORT
IF(NWKPY.EQ.1)WRITE(NWRITE,28)GG(1),GG(2),NSTAG,NVORT
IF(NWKPY.EQ.1) READ(NREAD,12)GG(1),GG(2),CSTAG,CVORT
IF(NWKPY.EQ.1)WRITE(NWRITE,22)GG(1),GG(2),CSTAG,CVORT
16 FORMAT( 2A,15,2F8.3)
26 FORMAT(1X,2A,15,2F8.3)
READ(NREAD,19) GG(1),G(2),(KPRINT(K),K=1,10)
WRITE(NWRITE,28)GG(1),G(2),(KPRINT(K),K=1,10)

C
IF(UNACH.EQ.1) CALL DEBUG(100)
MULTY=1
IF(KSYMMX.EQ.0)MULTY=2
MULT=1
IF(KSYMMZ.EQ.0)MULT=2
MS=0
IF(NYBD.NE.0)MS=MS+(NB00V1+NB00V2+NB00V3)*MULT
IF(NPYLON.NE.0.OR.NVTAL.NE.0)MS=MS+(NPYLON+NVTAL)*MULT
IF(NMUB.NE.0)MS=MS+NSIC*MULT+NMMUB*MULT
IF(NROTOR.NE.0)MS=MS+3*LADE*(NSHANK+NBLADE)*MULT
IF(MS.NE.0) CALL DEBUG(200)

P C D
REFLEN=1.
BETA=SQRT(LABS(UNACH**2-1.))
KS=0
NSBODY=0
NSBOT=0

P C D
***** NOSE *****
C
IF(NBODY1.EQ.0)GO TO 100
KS=KS+1
NSBODY=NSBODY+1
READ(NREAD,18) GG(1),G(2),NX(KS),NY(KS),KNSELE,KNSSH,KNSTYP

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WRITE (NWRITE, 28) GG(1), GG(2), NX(KS), NY(KS), KNSELE, KNSSHP, KNSTYP
NXY(KS)=NX(KS)*NY(KS)
ISFACE(KS)=1
KNORHL(KS)=1
KWAKES(KS)=0
KROTORS(KS)=0
3
IF(KSYMNY.NE.0) GO TO 170
NSBODY=NSBODY+1
JS=KS+(NBODY1+NBODY2+NBODY3)*MULT+NPYLON+NVTAIL
NX(JS)=NX(KS)
NY(JS)=NY(KS)
NXY(JS)=NXY(KS)
ISFACE(JS)=0
KWAKES(JS)=0
KNORHL(JS)=1
KROTORS(JS)=0
170
CONTINUE
IF(KSYMZ.NE.0) GO TO 199
NSBODY=NSBODY+1
KSL=KS+NBODY1+NBODY2+NBODY3)*MULT+NPYLON
NX(KSL)=NX(KS)
NY(KSL)=NY(KS)
NXY(KSL)=NXY(KS)
ISFACE(KSL)=5
KWAKES(KSL)=0
KNORHL(KSL)=1
KROTORS(KSL)=0
C
IF(KSYMNY.NE.0) GO TO 199
NSBODY=NSBODY+1
JSL=KSL+(NBODY1+NBODY2+NBODY3)*MULT+NPYLON+NVTAIL
NX(JSL)=NX(KS)
NY(JSL)=NY(KS)
NXY(JSL)=NXY(KS)
ISFACE(JSL)=13
KWAKES(JSL)=0
KNORHL(JSL)=1
KROTORS(JSL)=0
199
CONTINUE
C
C ----- FUSLAGE -----
C
IF(NBODY2.EQ.0) GO TO 299
KS=KS+1
NSBODY=NSBODY+1
READ (NREAD, 18) GG(1), GG(2), NX(KS), NY(KS), KBOLE, KBO SHP, KBO TYP
WRITE (NWRITE, 28) GG(1), GG(2), NX(KS), NY(KS), KBOLE, KBO SHP, KBO TYP
NXY(KS)=NX(KS)*NY(KS)
ISFACE(KS)=2
KNORHL(KS)=1
KROTORS(KS)=0
KWAKES(KS)=0
C
IF(KSYMNY.NE.0) GO TO 271
NSBODY=NSBODY+1
JS=KS+(NBODY1+NBODY2+NBODY3)*MULT+NPYLON+NVTAIL

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NX(JS)=NX(KS)
NY(JS)=NY(KS)
NXY(JS)=NXY(KS)
ISFACE(JS)=10
KMAKES(JS)=0
KNORML(JS)=1
KROTORS(JS)=0
270 CONTINUE
IF(KSYHMZ.NE.0)GO TO 299
NSBODY=NSBODY+1
KSL=KS+NBODY1+NBODY2+NBODY3+NPYLON
NX(KSL)=NX(KS)
NY(KSL)=NY(KS)
NXY(KSL)=NXY(KS)
ISFACE(KSL)=5
KMAKES(KSL)=0
KNORML(KSL)=-1
KROTORS(KSL)=0
C
IF(KSYHMY.NE.0)GO TO 299
NSBODY=NSBODY+1
JSL=KSL+(NBODY1+NBODY2+NBODY3)*MULT+NPYLON+NVTTAI
NX(JSL)=NX(KS)
NY(JSL)=NY(KS)
NXY(JSL)=NXY(KS)
ISFACE(JSL)=10
KMAKES(JSL)=0
KNORML(JSL)=1
KROTORS(JSL)=0
280 CONTINUE
C
C ----- AFT=30DY -----
C
IF(NBODY3.EQ.0)GO TO 300
KS=KS+1
NSBODY=NSBODY+1
READ(NREAD,10) GG(1),GG(2),NX(KS),NY(KS),KTNELE,KTNSHP,KTNTYP
WRITE(NWRITE,20)GG(1),GG(2),NX(KS),NY(KS),KTNELE,KTNSHP,KTNTYP
NXY(KS)=NX(KS)*NY(KS)
ISFACE(KS)=3
KNORML(KS)=1
KMAKES(KS)=0
KROTORS(KS)=0
C
IF(KSYHMY.NE.0)GO TO 370
NSBODY=NSBODY+1
JS=KS+(NBODY1+NBODY2+NBODY3)*MULT+NPYLON+NVTTAIL
NX(JS)=NX(KS)
NY(JS)=NY(KS)
NXY(JS)=NXY(KS)
ISFACE(JS)=11
KMAKES(JS)=0
KNORML(JS)=-1
KROTORS(JS)=0
370 CONTINUE
IF(KSYHMZ.NE.0)GO TO 300
NSBODY=NSBODY+1

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```

KSL=KS+N800Y1+N800Y2+N800Y3+NPYLON
NX(KSL)=NX(KS)
NY(KSL)=NY(KS)
NXY(KSL)=NXY(KS)
ISFACE(KSL)=7
KWAKES(KSL)=0
KNORML(KSL)=-1
KROTORS(KSL)=0
C
IF(KSYM*NY.NE.0)GO TO 199
NSBODY=NSBODY+1
JSL=KSL*(N800Y1+N800Y2+N800Y3)*MULT+NPYLON+NVTAIL
NX(JSL)=NX(KS)
NY(JSL)=NY(KS)
NXY(JSL)=NXY(KS)
ISFACE(JSL)=15
KWAKES(JSL)=0
KNORML(JSL)=-1
KROTORS(JSL)=0
199 CONTINUE
C
----- BYLON -----
C
IF(NBYLON.EQ.0)GO TO 499
KS=KS+1
NSBODY=NSBODY+1
READ(NREAD,18) GG(1),GG(2),NX(KS),NY(KS),KPYELE,KPYSHR,KPYTYP
WRITE(NWRITE,28)GG(1),GG(2),NX(KS),NY(KS),KPYELE,KPYSHR,KPYTYP
NXY(KS)=NX(KS)*NY(KS)
ISFACE(KS)=4
KNORML(KS)=1
KWAKES(KS)=1
KROTORS(KS)=0
C
IF(KSYM*NY.NE.0)GO TO 499
NSBODY=NSBODY+1
JS=KS+(N800Y1+N800Y2+N800Y3)*MULT+NPYLON+NVTAIL
NX(JS)=NX(KS)
NY(JS)=NY(KS)
NXY(JS)=NXY(KS)
ISFACE(JS)=12
KWAKES(JS)=1
KNORML(JS)=-1
KROTORS(JS)=0
499 CONTINUE
C
N800YS=N800Y1+N800Y2+N800Y3
C
----- VERTICAL TAIL -----
C
NSBODY=NSBODY+1
IF(NVTAIL.EQ.0)GO TO 599
KS=N800YS*MULT+NPYLON+1
READ(NREAD,18) GG(1),GG(2),NX(KS),NY(KS),KVTELE,KVTSMP,KVTYP
WRITE(NWRITE,28)GG(1),GG(2),NX(KS),NY(KS),KVTELE,KVTSMP,KVTYP
NXY(KS)=NX(KS)*NY(KS)
ISFACE(KS)=8

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KNORML(KS)=-1
KMAKES(KS)=1
KROTORS(KS)=0
C
IF(KSYMMY.NE.0)GO TO 599
NSBODY=NSBODY+1
JS=KS+(NBODY1+NBODY2+NBODY3)*MULT+NPLYON+NVTAIL
NX(JS)=NX(KS)
NY(JS)=NY(KS)
NXY(JS)=NXY(KS)
ISFACE(JS)=16
KMAKES(JS)=1
KNORML(JS)=+1
KROTORS(JS)=0
C
599 CONTINUE
C
----- ROTOR SHAFT -----
C
IF(NSHAFT.EQ.0)GO TO 699
NSBODY=NSBODY+1
KS=(NBODY1+NBODY2+NBODY3)*MULT+MULT*(NPLYON+NVTAIL)*MULT
KS=KS+1
READ(NREAD,13) GG(1),GG(2),NX(KS),NY(KS),KSBELE,KHSHP,KSTYP
WRITE(NWRITE,28)GG(1),GG(2),NX(KS),NY(KS),KSBELE,KHSHP,KSTYP
NXY(KS)=NX(KS)*NY(KS)
ISFACE(KS)=17
KNORML(KS)=1
KMAKES(KS)=0
KROTORS(KS)=1
C
IF(KSYMMY.NE.0)GO TO 699
NSBODY=NSBODY+1
JS=KS+1
NX(JS)=NX(KS)
NY(JS)=NY(KS)
NXY(JS)=NXY(KS)
ISFACE(JS)=18
KMAKES(JS)=0
KNORML(JS)=+1
KROTORS(JS)=1
C
699 CONTINUE
C
----- ROTOR HUB -----
C
IF(NHUB.EQ.0)GO TO 799
KS=NBODY1+NBODY2+NBODY3+MULT*(NPLYON+NVTAIL+NSHAFT)*MULT
KS=KS+1
NSBODY=NSBODY+1
READ(NREAD,13) GG(1),GG(2),NX(KS),NY(KS),KSBELE,KHSHP,KSTYP
WRITE(NWRITE,28)GG(1),GG(2),NX(KS),NY(KS),KSBELE,KHSHP,KSTYP
NXY(KS)=NX(KS)*NY(KS)
ISFACE(KS)=19
KNORML(KS)=1
KMAKES(KS)=1
KROTORS(KS)=1

```

```

C
IF(KSYMZY.NE.0)GO TO 778
NSBODY=NSBODY+1
JS=KS+NHUB*MULT
NX(JS)=NX(KS)
NY(JS)=NY(KS)
NXY(JS)=NXY(KS)
ISFACE(JS)=21
KNAKES(JS)=1
KNORML(JS)=-1
KROTORS(JS)=1
778 CONTINUE
IF(KSYMZY.NE.0)GO TO 793
NSBODY=NSBODY+1
KSL=KS+1
NX(KSL)=NX(KS)
NY(KSL)=NY(KS)
NXY(KSL)=NXY(KS)
ISFACE(KSL)=20
KNAKES(KSL)=1
KNORML(KSL)=-1
KROTORS(KSL)=1
2
IF(KSYMZY.NE.0)GO TO 793
NSBODY=NSBODY+1
JSL=JS+NHUB*MULT
JSL=KSL+NHUB*MULT
NX(JSL)=NX(KS)
NY(JSL)=NY(KS)
NXY(JSL)=NXY(KS)
ISFACE(JSL)=22
KNAKES(JSL)=1
KNORML(JSL)=1
KROTORS(JSL)=1
799 CONTINUE
C
C ----- ROTOR BLADE SHANK -----
C
IF(NSHANK.EQ.0)GO TO 899
KS=(NBODY1+NBODY2+NBODY3)*MULT+MULT*(NBVLONANNTAIL)*MULT+
INSHAF*MULT+NHUB*MULT+JLTY+1
READ(NREAD,4) GG(1),GG(2),NX(KS),NY(KS),KSKELE,KSXSHP,KSXTYP
WRITE(NWRITE,2)GG(1),GG(2),NX(KS),NY(KS),KSKELE,KSXSHP,KSXTYP
C
DO 810 K=1,KBLADE
NSBODY=NSBODY+1
KSS=KS+(K-1)*(NSHANK+NB.4DE*MULT)
NX(KSS)=NX(KS)
NY(KSS)=NY(KS)
NXY(KSS)=NXY(KS)+NY(KS)
ISFACE(KSS)=23+(K-1)*3
KNORML(KSS)=1
KNAKES(KSS)=1
KROTORS(KSS)=1
810 CONTINUE
C
899 CONTINUE

```



```

C ----- ROTOR BLAD -----
C
IF (NBLADE.EQ.0) GO TO 99
KS= (NBDY1+NBDY2+NBDY3)*MULT*MULTY+(NPYLON+NVTAIL)*MULTY+
1 NSHAFTMULTYANNUBBMIN*TMULTYANSHANK*1
READ(NREAD,10) GG(1),G(2),NX(KS),NY(KS),KBLELE,K3LSMP,KBLTYP
WRITE(NWRITE,20)GG(1),G(2),NX(KS),NY(KS),KBLELE,K3LSMP,KBLTYP
C
DO 918 K=1,KBLADE
NSBODY=NSBODY+1
KSS=KS+(K-1)*NSHAFTMULTYANNUBBMIN*TMULTYANSHANK*1
NX(KSS)=NX(KS)
NY(KSS)=NY(KS)
NXY(KSS)=NX(KS)*NY(KS)
ISFACE(KSS)=2*(K-1)*3
KNORML(KSS)=1
KMAKES(KSS)=1
KROTORS(KSS)=1
C
IF (KSYMHZ.NE.0) GO TO 919
NSBODY=NSBODY+1
KSSL=KSS+1
NX(KSSL)=NX(KSS)
NY(KSSL)=NY(KSS)
NXY(KSSL)=NXY(KSS)
ISFACE(KSSL)=25*(K-1)*3
KMAKES(KSSL)=1
KNORML(KSSL)=-1
KROTORS(KSSL)=1
918 CONTINUE
C
999 CONTINUE
C
NELEN=0
WRITE(6,8002)
DO 1000 IS=1,NS
1000 NELEN=NELEN+NXY(IS)
WRITE(6,8001)NELEN
8001 FORMAT(//5X,'NELEN = ',I5/)
C
8002 FORMAT(//10X,'#DATA')
C
NSBTOT=0
DO 1100 IS=1,NS
NT(IS)=NSBTOT
NSBTOT=NSBTOT+NXY(IS)+NY(IS)
WRITE(6,8003) IS,NX(IS),YF(IS),NXY(IS),ISFACE(IS),NT(IS),
1 KNORML(IS),KMAKES(IS)
8003 FORMAT (5X,'IS= ',IS,2X,'NX= ',IS,2X,'NY= ',IS,
1 ' NXY= ',IS, ' ISFACE= ',IS, ' NT= ',IS,
2 ' KNORML= ',IS, ' KMAKES= ',IS)
1100 CONTINUE
C
RETURN
END

```



```

C
SUBROUTINE COORDT (NLELE, NXYMP, NOFCT, XK, NNODE)
C
COMMON/ZZZ1/NX(34), NY(34), NXY(34), KSYNM1, KSYNM2, NSYNM1, NSYNM2
COMMON/ZZZ2/NSFX, NSBODY, NS, NT(34), ISFACE(34), KNORML(34), KMAKES(34)
COMMON/ZZZ3/RBY10, RBODY1, RBODY2, RBODY3, RVTAIL, RSMAPT, RHUB, RSHANK
1 NBLADE
COMMON/ZZZ4/UMACM, OMEGA, ALFA, ABETA
COMMON/ZZZ5/KPYCTR, YPYCTR, ZPYCTR, RXPYL, RYPYL, RZPYL
COMMON/ZZZ6/KNOSE, X001, X302, XTAIL
COMMON/ZZZ7/YNOSE, Y001, Y302, YTAIL
COMMON/ZZZ8/ZNOSE, Z001, Z302, ZTAIL
COMMON/ZZZ9/RY001, RZ001, RY002, RZ002
COMMON/ZZZ10/RSMAPT, LSHAPT, RSHANK, LSHANK
COMMON/ZZZ11/XHUBCR, YHUBCR, ZHUBCR, RXHUB, RYHUB, RZHUB
COMMON/ZZZ12/RROTOR, BCOROT, TAUBL, ALFAR
COMMON/ZZZ13/TMET75, THET1C, THET1S, CONING, AZIMUTH
COMMON/ZZZ14/KBLADE, TANLE, TANTE, KBL1, YRTE, KROTORS(34)
COMMON/ZZZ15/VSPAN, XLEZV, XTEZV, TANLE, TANTE, TAVV, ZVTAIL
COMMON/ZZZ16/MAKPY, MAK1B, MAKSK, MAKKB
COMMON/ZZZ17/WAKLPY, WAK1B, WAKLSK, WAKLB
COMMON/ZZZ18/WANGPY, WANG1B, WANGSK, WANGB
COMMON/ZZZ19/KPRINT(10), NREAD, NWRITE, KREAD
COMMON/ZZZ20/RT
COMMON/ZZZ21/KPY1, KPY2
COMMON/ZZZ22/KNSFL, KNSS1P, KNSTYP
COMMON/ZZZ23/KBDELE, K0S1P, K0TYP
COMMON/ZZZ24/KTMELE, KTS1P, KTTYP
COMMON/ZZZ25/KPYELE, KPS1P, KPTYP
COMMON/ZZZ26/KVTELE, KVS1P, KVTYP
COMMON/ZZZ27/KSHELE, KSH1P, KSHYP
COMMON/ZZZ28/KHBELE, KHS1P, KHTYP
COMMON/ZZZ29/KSKELE, KSK1P, KSKYP
COMMON/ZZZ30/KBLELE, KBL1P, KBLYP
COMMON/ZZZ31/NSTAG, NVORT, NSPIRAL, SPIRAL
COMMON/ZZZ32/UMAKE
COMMON/ZZZ33/YCUT
COMMON/ZZZ34/XCTR, YCTR, ZCTR, RX, RY, RZ
COMMON/ZZZ35/HSPAN, XLEZ1, XTEZ1, TANLEH, TANTEH, TAVH, ZP
COMMON/ZZZ36/TIMST, RTTCH, TIMST
DIMENSION AC4ORD(20), WNP(2), WNP1(2), WNP2(2), WNP3(2)
DIMENSION XVT, NNODE, NOFCT(NXYMP, 34), CC(20), KSFAC(34)
DIMENSION DFPP(2), DFPM(2), DFMP(2), DFHM(2)
DIMENSION MCHORD(11), MAXIS(11), MCHORD1(11), MAXIS1(11)
DIMENSION HCSI(11), HETA(11)
REAL LSMAPT, LSHANK
C
NSX=34
KREAD=0
C
IF (KREAD.EQ.0) GO TO 9
READ (NREAD, 15) ((XK(K, I NODE), K=1, 3), I NODE=1, NNODE)
WRITE (NWRITE, 25) ((XK(K, I NODE), K=1, 3), I NODE=1, NNODE)
FORMAT (3E12, A)
GO TO 900
9
CONTINUE
C

```

```

REFLEN=1.
BETA=SQRT(ABS(UIMACH**2-1.))
MULT=1
IF(KSYMMZ.EQ.0)MULT=2
MULTY=1
IF(KSYMMY.EQ.0)MULTY=2
15 FORMAT(10F8.3)
25 FORMAT(1X,10F8.3)
PI=3.14159265
300 FORMAT(2X,A15.8,I5,2X,A15.8,I5,2X,A15.8,I5,2X,A15.8,I5,2X,
1 *NOFACT=*,I5)
C
C
KFACE=NSOBY1+NSOBY2+NSOBY3+NRYLON
C
C
C
C
IF(NRYLON.EQ.0)GO TO 10.
KS=KFACE
DXX=1./NX(KS)
DYY=1./NY(KS)
NXP=NX(KS)+1
NYP=NY(KS)+1
LPYELE=KPYELE
IF(LPYELE.NE.0) GO TO 102
IF(KPYELE.NE.0) GO TO 102
LPYELE=1
READ(NREAD,15) (HCSI(IX),IX=1,NXP)
WRITE(NWRITE,25) (HCSI(IX),IX=1,NXP)
READ(NREAD,15) (META(IY),IY=1,NYP)
WRITE(NWRITE,25) (META(IY),IY=1,NYP)
102 CONTINUE
DO 110 IX=1,NXP
DO 110 IY=1,NYP
XX=(IX-1)*DX
YY=(IY-1)*DY
IF(KPYELE.EQ.0) XX=HCSI(IX)
IF(KPYELE.EQ.0) YY=META(IY)
GO TO(131,132,133),LPYELE
131 CONTINUE
CSI=XX
ETA=YY
GO TO 113
132 CONTINUE
CSI=XX*XX
ETA=YY
133 CONTINUE
CSI=1./(1.-XX)**2
ETA=YY
113 CONTINUE
THETA=PI*ETA
RX=CSI/RXPVL
RY=CSI/RYPVL
YB=RX*CBOS(THETA)
YB=RY*SIN(THETA)
ZB=RZBYL*SQRT(1.-(YB/RXPVL)**2-(YB/RYPVL)**2)
IXY=IX+(IY-1)*NXP

```

```

      INODE=NOFCT(IXY,KS)
      XK(1,INODE)=X8+XPYCTR
      XK(2,INODE)=Y8+YPYCTR
      XK(3,INODE)=Z8+ZPYCTR
      WRITE(6,140)IX,IV,IXY,CSI,ETA,INJDE
      WRITE(6,141)THETA,2X,RY
      WRITE(6,142)X8,Y8,Z8
      WRITE(6,143)(XK(I,INODE),I=1,3)
140  FORMAT(10X,'IX=',I5,2X,'IV=',I5,2X,'IXY=',I5,2X,'CSI=',E12.6,2X,
141  'ETA=',E12.6,2X,'INODE=',I5)
141  FORMAT(10X,'THETA=',E12.6,2X,'RX=',E12.6,2X,'RY=',E12.6)
142  FORMAT(10X,'X8=',E12.6,2X,'Y8=',E12.6,2X,'Z8=',E12.6)
143  FORMAT(10X,'XK=',3(E12.6,2X))
113  CONTINUE
199  CONTINUE
C
C
C      KS=8
C
C
C      =====NOSE=====
C
      IF(NBODY1.EQ.8)GO TO 500
      KS=KS+1
      DO 500 I=BODY1+1,MULT
      IF(I=BODY1.EQ.1)SIGNZ=+1
      IF(I=BODY1.EQ.2)SIGNZ=-1
      NXP=NX(KS)+1
      NY=NY(KS)+1
      DX=1./NX(KS)
      TINC=8.58RT/NY(KS)
      DO 550 IX=1,NXP
      YX=(IX-1)*DX
      IF(KNSELE.EQ.1)CSI=YX
      IF(KNSELE.EQ.2)CSI=YX*DX
      X=XNOSE+(XBD1-XNOSE)*CSI
      IF(KNSSMP.EQ.1)RRY=RYBD1*SQR(CSI)
      IF(KNSSMP.EQ.1)RRZ=RZBD1*SQR(CSI)
      IF(KNSSMP.EQ.2)RRY=RYBD1*(CSI)**.333333
      IF(KNSSMP.EQ.2)RRZ=RZBD1*(CSI)**.333333
      IF(KNSSMP.EQ.3)RRY=RYBD1*(CSI)**.25
      IF(KNSSMP.EQ.3)RRZ=RZBD1*(CSI)**.25
      DO 550 IY=1,NYP
      THET=(IY-1)*TINC
      THETA=(AB.58RT-THET)
      ETA=COS(THETA)
      YV=RRY*ETA
      ZZ=SIGNZ*RRZ*SIN(THETA)
      DELZ=(ZBD1-ZNOSE)
      DOWNZ=DELZ-DELZ*CSI
      ZZ=ZZ+DOWNZ
C
C
      IXY=IX+(IY-1)*NYP
      IF(I=BODY1.EQ.1)IS=KS
      IF(I=BODY1.EQ.2)IS=KS+KPCF
      WRITE(6,140)IX,IV,IXY,CSI,ETA,NOFCT(IXY,IS)

```



```

WRITE(6,142)X,YY,ZZ
XK(1,NOFCT(IXY,IS))=X
XK(2,NOFCT(IXY,IS))=YY
XK(3,NOFCT(IXY,IS))=ZZ
550 CONTINUE
598 CONTINUE
599 CONTINUE
C -----BODY-----
C
IF(NBODY2.EQ.8)GO TO 69
KS=KS+1
DO 698 IBODY2=1,MULT
IF(IBODY2.EQ.1)SIGNZ=+1.
IF(IBODY2.EQ.2)SIGNZ=-1.
NXP=NX(KS)+1
NYP=NY(KS)+1
TINCR=8.6881/NY(KS)
DXX=1./NX(KS)
DO 631 IY=1,NXP
XXX=(IX-1)*DXX
IF(KBDELE.EQ.1)CSI=XXX
IF(KBDELE.EQ.2)CSI=XXX*(X
R1=RZ01+(RZ02-RZ01)*CSI
R2=RZ01+(RZ02-RZ01)*CSI
DELZ=RZ02-RZ01
ZZZ=DELZ*CSI
XY=XB01+(XB02-XB01)*CSI
DO 631 IY=1,NYP
THETA=(8.6881*(IX-1)*TINCR)
YY=R1*COS(THETA)
ZZ=SIGNZ*R2*STN(THETA)
ZZ=ZZ+ZZZ+Z01
IXY=IX+(IX-1)*NXP
IF(IBODY2.EQ.1)IS=KS
IF(IBODY2.EQ.2)IS=KS+KRODE
XK(1,NOFCT(IXY,IS))=XX
XK(2,NOFCT(IXY,IS))=YY
XK(3,NOFCT(IXY,IS))=ZZ
531 CONTINUE
698 CONTINUE
699 CONTINUE
C -----TAIL NOSE-----
C
IF(NBODY3.EQ.8)GO TO 899
KS=KS+1
DO 898 IBODY3=1,MULT
IF(IBODY3.EQ.1)SIGNZ=+1.
IF(IBODY3.EQ.2)SIGNZ=-1.
NXP=NX(KS)+1
NYP=NY(KS)+1
DXX=1./NX(KS)
TINCR=8.5*PI/NY(KS)
DO 878 IY=1,NXP
XX=(IX-1)*DXX

```



```

XX=1.-XX
IF(KYNELE.EQ.1)CSI=XX
IF(KYNELE.EQ.2)CSI=XX*XX
IF(KYNSMP.EQ.1)RRZ=RZBD2*SQRT(CSI)
IF(KYNSMP.EQ.2)RRZ=RZBD2*CSI
IF(KYNSMP.EQ.2)RRZ=RZBD2*CSI
CSI=1.-CSI
X=XBD2+(XTAIL-XBD2)*CSI
DO 388 IY=1,NYP
THETA=(IY-1)*TINCR
THETA=(.485921-TMET)
ETA=COS(THETA)
YY=RRY*ETA
ZZ=SIGNZ*RRZ*SIN(THETA)
C
DELZ=ZTATI-ZBD2
DOWNZ=DELZ*CSI
ZZ=ZZ+DOWNZ+ZBD2
C
IXY=IX+(IY-1)*NXP
IF(IBODY3.EQ.1)IS=KS
IF(IBODY3.EQ.2)IS=KS+KFACE
XK(1,NOFCT(IXY,IS))=X
XK(2,NOFCT(IXY,IS))=YY
XK(3,NOFCT(IXY,IS))=ZZ
858 CONTINUE
888 CONTINUE
899 CONTINUE
C
----- VERTICAL TAIL -----
C
IF(NVTAIL.EQ.0)GO TO 399
KS=(NBDY1+NBDY2+NBDY3)*MULI+NDYLOM+1
DO 398 IYTL=1,1
C
IF(KVTTYE.EQ.1)GO TO 3178
READ(NREAD,15) GG(1),GG(2),WNPP,WNPB,WNXP,WNNM
WRITE(NWRITE,25)GG(1),GG(2),WNPP,WNPB,WNXP,WNNM
3178 CONTINUE
SIGNZ=+1.
TAILL=NWSPAN-2.*8
TAILWD=TAILLN/2.
PLE=8.
RTE=8.
DXX=1./NY(KS)
DYY=1./NY(KS)
NXP=NY(KS)+1
NYP=NY(KS)+1
LVTELE=KVTELE
IF(LVTELE.NE.0)GO TO 3130
LVTELE=1
READ(NREAD,15) GG(1),GG(2),(HCSI(IX),IX=1,NXP)
WRITE(NWRITE,25)GG(1),GG(2),(HCSI(IX),IX=1,NXP)
READ(NREAD,15) GG(1),GG(2),(HETA(IY),IY=1,NYP)

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WRITE (NWRITE, 25) GG(1), GG(2), (META(IY), IY=1, NYP)
3108 CONTINUE
DO 318 IX=1, NXP
DO 318 IY=1, NYP
XX=(IX-1)*DX
YY=(IY-1)*DY
IF (KVTELE.EQ. 0) XX=HCSI(I, X)
IF (KVTELE.EQ. 0) YY=META(I, Y)
GO TO (3131, 3132, 3133, 3134), LVTELE
3131 CONTINUE
CSI=XX
ETA=YY
GO TO 313
3132 CONTINUE
CSI=XX*XX
ETA=(1.-YY)*2
GO TO 313
3133 CONTINUE
CSI=XX
ETA=(1.-YY)*2
GO TO 313
3134 CONTINUE
CSI=XX*XX
ETA=YY
313 CONTINUE
C
IF (KVTTYP.EQ. 1) GO TO 3133
Y=TAILWO*ETA
XLE=XLEZV+TANLEW*(Y-RLD)
XTE=XTEZV+TANTEV*(Y-RTE)
VCHORD(IY)=XTE-XLE
VAXIS(IY)=XLE+VCHORD(IY)*0.5
Y=XLE+(XTE-XLE)*CSY
C
3139 CONTINUE
IF (KVTTYP.EQ. 2) GO TO 313
X1=(WNP(1)-WNM(1))*CSI+WNM(1)
Y1=(WNP(2)-WNM(2))*CSI+WNM(2)
X2=(WNP(1)-WNM(1))*CSI+WNM(1)
Y2=(WNP(2)-WNM(2))*CSI+WNM(2)
X3=(WNP(1)-WNM(1))*ETA+WNM(1)
Y3=(WNP(2)-WNM(2))*ETA+WNM(2)
X4=(WNP(1)-WNM(1))*ETA+WNM(1)
Y4=(WNP(2)-WNM(2))*ETA+WNM(2)
DET=(X1-X2)*(Y3-Y4)-(X3-X4)*(Y1-Y2)
IF (DET.EQ. 0.) GO TO 3147
X=(X1-X2)*(X4*Y3-X3*Y4)-(X3-X4)*(X2*Y1-X1*Y2)/DET
Y=(Y1-Y2)*(X4*Y3-X3*Y4)-(Y3-Y4)*(X2*Y1-X1*Y2)/DET
GO TO 3149
3147 CONTINUE
XXXX
Y=Y4
3149 CONTINUE
C
GO TO (3151, 3152, 3153), /TSMB
3151 CONTINUE
C
FOR CIRCULAR BICONVEX

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```

C
XC=0.5*(XLE+XTE)
PL=0.5*(XTE-XLE)
M=TAU*VSPAN
ATAU=2.*M
ETACR=1.-ATAU/VSPAN
XXC=X-XC
Z=0.
IF(M.EQ.0..OR.IY.EQ.NYP..OR.IX.EQ.1..OR.IX.EQ.NXP)GO TO 315
Z=SIGNZ*(SQRT((PL*VPLAMP+1)/(2.*M+1)+2.-XXC**2)-(PL*VPLAMP)/(2.*M))
IF(ETA.GE.ETACR)Z=Z*SQRT(1.-((ETA-ETACR)*VSPAN/ATAU)**2)
GO TO 315
3152 CONTINUE
TAUBAR=TAU*0.75*SQRT(1.-XTEZY-XLEZY)
Z=SIGNZ*TAUBAR*SQRT(CSD*(1.-CSI)*SQRT(1.-ETA**2))
GO TO 315
3193 CONTINUE
Z=SIGNZ*TAU*(XTEZY-XLEZY)*SQRT(1.-CSI)*SQRT(1.-ETA**2)
315 CONTINUE
C
IXY=IX+(IY-1)*NXP
XK(1,NOFCT(IY,KS))=Z
XK(2,NOFCT(IY,KS))=Z
XK(3,NOFCT(IY,KS))=V*VTAU
318 CONTINUE
398 CONTINUE
399 CONTINUE
C
----- SHAFT -----
C
IF(NSHAFT.EQ.0)GO TO 299
KS=(NBDY1+N30DY2+NBDY3)*MULT*MULTY*(NBY1 ON*NVTAU)*MULTY
KS=KS+1
DXX=1./NX(KS)
DYY=1./NY(KS)
NYP=NX(KS)+1
NYP=NY(KS)+1
LSHELE=KSHELE
IF(LSHELE.NE.0)GO TO 211
IF(LSHELE.NE.0)GO TO 201
LSHELE=1
READ(MREAD,15) (MCSI(IY),IY=1,NYP)
WRITE(MWRITE,25) (MCSI(IY),IY=1,NXP)
READ(MREAD,15) (META(IY),IY=1,NYP)
WRITE(MWRITE,25) (META(IY),IY=1,NXP)
201 CONTINUE
DO 210 IX=1,NXP
DO 210 IY=1,NYP
XX=(IX-1)*DXX
YY=(IY-1)*DYY
IF(KSHELE.EQ.0) XX=MCSI(IX)
IF(KSHELE.EQ.0) YY=META(IY)
GO TO (231,232,233),LSHELE
231 CONTINUE
CSI=XX
FY=YY
GO TO 213

```

```

232 CONTINUE
CST=XXYY
ETA=YY
GO TO 213
233 CONTINUE
CST=1./1.-XX/1.883
ETA=YY
217 CONTINUE
THETA=PI*ETA
R=RSNAFT
XB=R*COS(THETA)
YB=RSIN(THETA)
ZB=CSI*LSHAFT
IXY=IX+(IY-1)*NXP
INODE=NOFCT(IXY,KS)
KK(1,INODE)=XB*XPYCTR
KK(2,INODE)=YB*YPYCTR
KK(3,INODE)=ZB*ZPCTR*LSHAFT-ZOARTR/L
WRITE(6,61)KS,IX,IY,IXY,INODE
WRITE(6,62)XB,YB,ZB
WRITE(6,63)(KK(L,INODE),L=1,3)
61 FORMAT(10X,KS=*,IS=*,(XB,IS=*,YB=*,IS=*,ZY=*,IS=*,
1 * INODE=*,IS)
62 FORMAT(10X,KB=*,E12.6,*,YB=*,E12.6,*,ZB=*,E12.6)
63 FORMAT(10X,*,KK=*,3(E12.6,2X))
218 CONTINUE
299 CONTINUE
C
IF(NHUB.EQ.0) GO TO 499
KS=(NBOOY1+NBOOY2+NBOOY3)*MULT*NULTVA*(NBYLONANNAT1)*NULTVA
1 NSHAFT*NULTY
KS=KS+1
DO 498 INULT=1,MULT
C
IF(INULT.EQ.1) SIGNZ=1
IF(INULT.EQ.2) SIGNZ=-1
C
DXX=1./NX(KS)
DYY=1./NY(KS)
NXP=NX(KS)+1
NYP=NY(KS)+1
LHBELE=KHBELE
IF(LHBELE.NE.0) GO TO 400
LHBELE=1
READ(NREAD,15) (HCST(I),IY=1,NXP)
WRITE(NWRITE,25) (HCST(IY),IY=1,NXP)
READ(NREAD,15) (META(IY),IY=1,NYP)
WRITE(NWRITE,25) (META(IY),IY=1,NYP)
400 CONTINUE
DO 410 IY=1,NXP
DO 420 IY=1,NYP
XX=(IY-1)*DXX
YY=(IY-1)*DYY
IF(KHBELE.EQ.0) XX=HCST(IY)
IF(KHBELE.EQ.0) YY=META(IY)
GO TO (431,432,433),LHBELE
431 CONTINUE

```



```

      CSI=XX
      ETABYY
      GO TO 413
432  CONTINUE
      CSI=XX*XX
      ETABYY
      GO TO 413
447  CONTINUE
      CSI=1.-(1.-XX)**2
      ETABYY
413  CONTINUE
      THETA=PI*ETA
      RX=CSI*RXHUB
      RY=CSI*RYHUB
      X0=RX*COS(THETA)
      Y0=RY*STH(THETA)
      Z0=SIGNZ*PRZMJB*SQRT(1.-X0/RXPYL)**2-(Y0/RYPYL)**2)
      IXV=IX+(IY-1)*NXP
      IS=KS+(IMULT-1)
      INODE=NOFCT(IXV,IS)
      XK(1,INODE)=X0+XHUBCR
      XK(2,INODE)=Y0+YHUBCR
      XK(3,INODE)=Z0+ZHUBCR
      WRITE(6,61)IS,IX,IY,IXV,INODE
      WRITE(6,62)X0,Y0,Z0
      WRITE(6,63)XK(1,INODE),X1,3)
418  CONTINUE
498  CONTINUE
499  CONTINUE
C
C
900  CONTINUE
C
      NSS=(NBODY1+NBODY2+NBODY3)*MULTANRYLON
      I+NVTAIL
      DO 910 IS=1,NSS
      JS=IS+NSS
      NXP=NX(IS)+1
      NYP=NY(IS)+1
      DO 910 IX=1,NXP
      DO 910 IY=1,NYP
      IXV=IX+(IY-1)*NXP
      XK(1,NOFCT(IXV,JS))=XK(1,NOFCT(IXV,IS))
      XK(2,NOFCT(IXV,JS))=-XK(2,NOFCT(IXV,IS))
      XK(3,NOFCT(IXV,JS))=XK(3,NOFCT(IXV,IS))
      WRITE(6,56)IXV,IS
54  FORMAT(10X,'IXY=',IS,2X,'IS=',IS)
310  CONTINUE
C
      IF(MSHAFT.EQ.8) GO TO 911
      IS=NSS*MULTY+1
      JS=IS+1
      NXP=NX(IS)+1
      NYP=NY(JS)+1
      DO 912 IX=1,NXP
      DO 912 IY=1,NYP
      IXV=IX+(IY-1)*NXP

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```

WRITE (6,54) IX, IS
XK(1,NOFCT(IX,JS))=XK(1,NOFCT(IX,IS))
XK(2,NOFCT(IX,JS))=-XK(2,NOFCT(IX,IS))
XK(3,NOFCT(IX,JS))=XK(3,NOFCT(IX,IS))
912 CONTINUE
913 CONTINUE
C
IF (NMUR.EQ.8) GO TO 913
IS1=NSS*MULTY+NSHAFT*MULTY+1
IS2=IS1+1
DO 914 IS=IS1,IS2
  JS=IS*MULTY
  NXP=NX(IS)+1
  NY=NXY(IS)+1
DO 915 IX=1,NXP
DO 916 IY=1,NYP
  IX=IX+(IY-1)*NXP
  WRITE (6,54) IX, IS
  XK(1,NOFCT(IX,JS))=XK(1,NOFCT(IX,IS))
  XK(2,NOFCT(IX,JS))=-XK(2,NOFCT(IX,IS))
  XK(3,NOFCT(IX,JS))=XK(3,NOFCT(IX,IS))
915 CONTINUE
914 CONTINUE
913 CONTINUE
C
C
C
C
----- BLADE SHANK -----
C
IF (NSHANK.EQ.8) GO TO 700
KS=(NBODY1+NBODY2+NBODY3)*MULT*MULTY+(NPYLOM+NVTAIL)*MULTY+
1-NMUR*MULT*MULTY+NSHAFT*MULTY+1
DO 700 IB=1,KBLADE
C
IF (IB.EQ.1) SIGNY=1.
IF (IB.EQ.2) SIGNY=-1.
C
DXX=1./NY(KS)
DYY=1./NY(KS)
NXP=NX(KS)+1
NYP=NY(KS)+1
LSKELE=KSKELE
IF (LSKELE.NE.8) GO TO 700
LSKELE=1
READ (NREAD,15) (MCSI(IX);IX=1,NXP)
WRITE (NWRITE,25) (MCSI(IY-1),IY=1,NYP)
READ (NREAD,15) (META(IY);IY=1,NYP)
WRITE (NWRITE,25) (META(IY),IY=1,NYP)
700 CONTINUE
DO 710 IY=1,NYP
DO 710 IX=1,NXP
  YY=(IY-1)*DYY
IF (KSKELE.EQ.8) XX=MCSI IX)
IF (KSKELE.EQ.8) YY=META(IY)
710 CONTINUE
CSI=XX

```

```

ETA=YY
GO TO 713
732 CONTINUE
CSI=1.-(1.-XX)***
ETA=YY
GO TO 713
733 CONTINUE
CSI=XX**X
ETA=YY
713 CONTINUE
THETA=2.*PI*ETA
R=RSNAK
X0=R*COS(THETA)
Z0=R*STN(THETA)
Y0=CSI*LSHANK
C
IXY=IX+(IY-1)*NXP
IS=KS*(IB-1)*(NBLADE*MULT+NSHANK)
INODE=NOFCT(IXY, IS)
XX(1, INODE)=XUBCR*X0
XX(2, INODE)=SIGN*(YHUBCR+RYHUB+LSHANK-Y0)
XX(3, INODE)=ZUBCR*Z0
WRITE(6,61) IS, IX, IY, IXV, INODE
WRITE(6,62) X0, Y0, Z0
WRITE(6,63) (XX(L, INODE), L=1,3)
718 CONTINUE
798 CONTINUE
799 CONTINUE
C
C
C
C
C ----- ROTOR BLADE -----
C
IF(NBLADE.EQ.0) GO TO 1039
KKS=(NBOV1+NBOV2+NBOV3)*MULT*TY+(NRY1+DNHNTAT1)*MULTY
I +NSHAFT*MULTY+NHUB*MUL*MULTY+NSHANK
DO 1098 IB=1, KBLADE
KS=KKS+1+(IB-1)*(NBLADE*MULT+NSHANK)
DO 1097 IMLT=1, MULT
WRITE(6,55) IB, IMLT, IXV, IS, X, Y, Z
C
SIGNV=1.
IF(IMULT.EQ.1) SIGNZ=1.
IF(IMULT.EQ.2) SIGNZ=-1.
C
OXX=1./NX(KS)
OYY=1./NY(KS)
NXP=NX(KS)+1
NYP=NY(KS)+1
LBLELE=KBLELE
IF(LBLELE.NE.0) GO TO 1099
LBLELE=1
READ(NREAD, 15) (HCST(IY), IY=1, NYP)
WRITE(NWRITE, 25) (HCST(IX), IX=1, NXP)
READ(NREAD, 15) (HETA(IY), IY=1, NYP)
WRITE(NWRITE, 25) (HETA(IY), IY=1, NYP)

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```

1000 CONTINUE
DO 1010 IX=1,NXP
DO 1010 IY=1,NYP
XX=(IX-1)*DXX
YY=(IY-1)*DYY
IF(KBLELE.EQ.0) XX=MCST*IX
IF(KBLELE.EQ.0) YY=META(IY)
GO TO (1031,1032,1033,1034),LBLELE
1031 CONTINUE
CSI=XX
ETA=YY
GO TO 1013
1032 CONTINUE
CSI=XX*XX
ETA=1.-(1.-YY)**2
GO TO 1013
1033 CONTINUE
CSI=XX
ETA=1.-(1.-YY)**2
GO TO 1013
1034 CONTINUE
CSI=XX*XX
ETA=YY
1013 CONTINUE
BCMORD=XBTE-XBLE
XLEZ=XBLE
XTEZ=XBTE
TANBLE=TANLE3
TANBTE=TANBTE3
SPAN=2.*RROTOR
Y=(RROTOR-YCJT)*ETA+YCUT
XLE=XLEZ+TANBLE*(Y-YCUT)
XTE=XTEZ+TANBTE*(Y-YCUT)
FCMORD=XTE-XLE
X=XLE+FCMORD*CSI
C
C
GO TO (1051,1052,1053),C31SMP
1051 CONTINUE
C
C FOR CIRCULAR BICONVEX
C
XC=0.5*(XLE+XTE)
PL=0.5*(XTE-XLE)
TAUBL=.050
TAU=TAUBL
H=TAU*PL
ATAU=2.*H
ETACR=1.-ATAU/SPAN
XCY=X-C
Z=0.
IF(N.EQ.0..OR.IY.EQ.NYP..OR.IX.EQ.1..OR.IX.EQ.NXP)GO TO 115
Z=SIGNZ*(SQRT(((PL*PL+H*H)/(2.*H))**2-XC**2)-(PL*PL-H*H)/(2.*H))
IF(ETA.GE.ETACR)Z=Z*SQRT(1.-((ETA-ETACR)*SPAN/ATAU)**2)
GO TO 115
1052 CONTINUE
TAUBAR=TAU*.75*SQRT(3.)*(XTEZ-XLEZ)

```



```

Z=SIGNZ*TAUBAR*SQRT(CSI)*(1.-CSI)*SQRT(1.-ETA**2)
GO TO 115
1053 CONTINUE
Z=SIGNZ*TAUBAR*(XTEZ-XLIZ)*CST*(1.-CSI)*SQRT(1.-ETA**2)
115 CONTINUE
C
IXY=IX+(IY-1)*NXP
IS=KS
IF (IMULT.EQ.2) IS=KS+1
INODE=NOECT(IY,IS)
XK(1,INODE)=X
XK(2,INODE)=Z*STGMV
XK(3,INODE)=Z*ZHUBCR
C
AZIN=AZINUT*PI/180.
GO TO (301,302),I*TWIST
C
301 CONTINUE
PITCHR=RPITCH*PI/180.
PITCHT=(RPITCH+TWIST)*PI/180.
X1=VCUT
X2=RROTOR
XX=XK(1,INODE)
YY=XK(2,INODE)
ZZ=XK(3,INODE)
C1=(YY-X2)/(X1-X2)
C2=(YY-X1)/(X2-X1)
DX=X2-X1
PITCH=C1*PITCHR+C2*PITCHT
GO TO 303
302 CONTINUE
PITCHR=RPITCH*PI/180.
PIT75=(THET75+THET1C*COB(AZIN)+THET1S*SIN(AZIN))*PI/180.
X1=VCUT
X2=.75*RROTOR
XX=XK(1,INODE)
YY=XK(2,INODE)
ZZ=XK(3,INODE)
C1=(YY-X2)/(X1-X2)
C2=(YY-X1)/(X2-X1)
DX=X2-X1
PITCH=C1*PITCHR+C2*PIT75
C
303 CONTINUE
C
C BLADE TWIST
C
COSPIT=COS(PITCH)
SINBIT=SIN(PITCH)
C
XK1=XK(1,INODE)
XK3=XK(3,INODE)
XK(1,INODE)=XK1*COB(PIT)+XK3*SINBIT
XK(3,INODE)=-XK1*SINBIT+XK3*COB(PIT)
C
C CONING ANGLE
C
CONE=CONING*PI/180.

```

```

COSC=COS(CONE)
SINC=SIN(CONE)
C
XK2=XK(2,INODE)
XK3=XK(3,INODE)
XK(2,INODE)=XK2*COSC-XK3*SINC
XK(3,INODE)=XK2*SINC+XK3*COSC
C
C AZIMUTH
C
HZIM=(AZIMUTH-90.)*PI/180.
COSMZ=COS(HZIM)
SINMZ=SIN(HZIM)
C
XK1=XK(1,INODE)
XK2=XK(2,INODE)
XK(1,INODE)=XK1*COSMZ-XK2*SINMZ
XK(2,INODE)=XK1*SINMZ+XK2*COSMZ
C
ANG=2.*PI/KBLADE
ANGR=ANG*(IB-1)
C
XK1=XK(1,INODE)
XK2=XK(2,INODE)
C
XK(1,INODE)=XK1*COS(ANGR)-XK2*SIN(ANGR)
XK(2,INODE)=XK1*SIN(ANGR)+XK2*COS(ANGR)
C
WRITE(6,55)IB,IMULT,IXY,IS,X,Y,Z
55 FORMAT(18X,2I8,2I5,2X,1MULT=,I5,2X,2IXY=,I5,2X,2IS=,I5,2X,
1 *XYZ=*,3(E12.6,2X))
1818 CONTINUE
1897 CONTINUE
1898 CONTINUE
1899 CONTINUE
C
WRITE(6,60)
60 FORMAT(18X,==== END OF COORD ==)
C
RETURN
END

```

```

C
SUBROUTINE CHECK (NELEM, NYMAX, NYMAX, NYMAX)
COMMON /ZZZ1/ NX (34), NY (34), NXY (34), KSYMHY, KSYMHZ, NSYMHY, NSYMHZ
COMMON /ZZZ2/ NSFX, NSBODY, NS, NT (34), TSPACE (34), KNORM (34), KMAKES (34)
COMMON /ZZZ3/ NPYLON, NBODY1, NBODY2, NBODY3, NVTAIL, NSHAFT, NMUB, NSHANK,
1 NBLADE
COMMON /ZZZ4/ JMACH, OMEGA, ALFA, ABETA
COMMON /ZZZ5/ XPYCTR, YPYCTR, ZPYCTR, RXYL, ZYPL, RZPYL
COMMON /ZZZ6/ XNOSE, XBD1, ZBD2, XTAL
COMMON /ZZZ7/ YNOSE, YBD1, ZBD2, YTAL
COMMON /ZZZ8/ ZNOSE, ZBD1, ZBD2, ZTAL
COMMON /ZZZ9/ RYBD1, ZYBD1, ZYBD2, RZBD2
COMMON /ZZZ10/ RSHAFT, LSHFT, RSHANK, LSHANK
COMMON /ZZZ11/ XHUBCR, YHUBCR, ZHUBCR, RYHUB, ZYHUB, RZHUB
COMMON /ZZZ12/ RROTOR, BCHRD, TAUBL, ALFA
COMMON /ZZZ13/ IMETZ, IMETC, IMETS, CONING, AZIMUTH
COMMON /ZZZ14/ KBLADE, TANTEB, TANTE9, XBLE, X3TE, KRATORS (34)
COMMON /ZZZ15/ XSRAN, XLEZ, XTEZ, TANLEV, TANTEV, TAU, ZVTAL
COMMON /ZZZ16/ NNAKPY, NNAK1B, NNAKSK, NNAKBL
COMMON /ZZZ17/ NAKLRY, NAK1B, NAKLSK, NAKLB
COMMON /ZZZ18/ NANGPY, NAN1B, NANGSK, NANGBL
COMMON /ZZZ19/ KPRINT (18), NREAD, NWRITE, KREAD
COMMON /ZZZ20/ PI
COMMON /ZZZ21/ KPY1, KPY2
COMMON /ZZZ22/ KNSELE, KNST4P, KNSTYP
COMMON /ZZZ23/ KBLELE, KBL4P, KBLTYP
COMMON /ZZZ24/ KTNELE, KTN4P, KTNTP
COMMON /ZZZ25/ KPYELE, KPY4P, KPYTYP
COMMON /ZZZ26/ KYTELE, KVT4P, KVTYP
COMMON /ZZZ27/ KSMELE, KSM4P, KSMTP
COMMON /ZZZ28/ KHBELE, KH84P, KH8TP
COMMON /ZZZ29/ KSKLE, KSK4P, KSKTP
COMMON /ZZZ30/ KBLELE, KBL4P, KBLTYP
COMMON /ZZZ31/ NSTAG, NVORT, NSPTRAL, SPTRAL
REAL LSHAFT, LSHANK
C
DO 100 IS=1, NS
IF (NX (IS).GT. NYMAX) CALL DEBUG (300)
IF (NY (IS).GT. NYMAX) CALL DEBUG (300)
100 CONTINUE
IF (NELEM.GT. NYMAX) CALL DEBUG (500)
WRITE (6, 60)
60 FORMAT (10X, '--- END OF CHECK --- ')
RETURN
END

```

```

C
SUBROUTINE PREPRO(MODE,NXYMP,NOFCT,NELM,NTHAKE)
C
C THIS SUBROUTINE FUNCTIONED AS A PRE-PROCESSOR. ON RETURN,
C THE CO-ORDINATES OF NODES IN THE GLOBAL NUMBERING SYSTEM
C WILL BE RE-CONSTRUCTED TO GIVE CO-ORDINATES IN THE LOCAL
C NUMBERING SYSTEM FOR INDIVIDUAL SURFACES.
C
C
INTEGER DP,RA,RP,MM
DIMENSION NOFCT(NXYMP,3)
COMMON/ZZZ1/NX(34),NY(34),NZ(34),KSYM1,KSYM2,NSYMM1,NSYMM2
COMMON/ZZZ2/ISFX,NSBODY,IS,NT(34),ISFACE(34),KNORML(34),KNAKES(34)
COMMON/ZZZ3/NBYLON,NBODY1,NBODY2,NBODY3,NXTAIL,NSMAFT,NMUB,NSMANK,
1 NBLADE
COMMON/ZZZ4/OMEGA,ALFA,ABETA
COMMON/ZZZ5/KPYCTR,YPYCTR,ZPYCTR,RXPYL,RYPYL,RZPYL
COMMON/ZZZ6/YNOSE,YB01,Y302,YTAIL
COMMON/ZZZ7/YNOSE,YB01,Y302,YTAIL
COMMON/ZZZ8/ZNOSE,ZB01,Z302,ZTAIL
COMMON/ZZZ9/RYP01,RZB01,RYP02,RZB02
COMMON/ZZZ10/RSMAFT,LSMAFT,RSMAK,LSMAK
COMMON/ZZZ11/XHUBCR,YHUBCR,ZHUBCR,RXHUB,RXHUB,RZ4UB
COMMON/ZZZ12/RROTOR,RCM1D,TAUBL,ALFA
COMMON/ZZZ13/THET75,THET1C,THET1S,CONING,AZINHUT
COMMON/ZZZ14/KBLADE,TAN1B,TAN1E,XBL1,X2E,KROTORS(34)
COMMON/ZZZ15/VSPAN,XLEZV,XTEZV,TANLEV,TANTEV,TAU,ZVTAIL
COMMON/ZZZ16/NMAKPY,NMAK1B,NMAKSK,NMAKBL
COMMON/ZZZ17/MAKPY,MAK1B,MAKLSK,MAKBL
COMMON/ZZZ18/MANGPY,MANG1B,MANGSK,MANGBL
COMMON/ZZZ19/KPRINT(10),VREAD,NWRITE,KREAD
COMMON/ZZZ20/PT
COMMON/ZZZ21/KPYL1,KPYL2
COMMON/ZZZ22/KNSELE,KNSE1P,KNSTYP
COMMON/ZZZ23/KBDELE,KBDE1P,KB0TYP
COMMON/ZZZ24/KTMELE,KTME1P,KTNTYP
COMMON/ZZZ25/KPYELE,KPY1P,KPYTYP
COMMON/ZZZ26/KVTELE,KVT1P,KVTTYP
COMMON/ZZZ27/KSHELE,KSHE1P,KSHTYP
COMMON/ZZZ28/KMBELE,KMB1P,KBSTYP
COMMON/ZZZ29/KSKELE,KSKE1P,KSKTYP
COMMON/ZZZ30/KBLELE,KBL1P,KBLTYP
COMMON/ZZZ31/NSTAG,NVORT,NSPIRAL,SPIRAL
C
C
C DO 24 I=1,NS
C24 WRITE(6,234)NX(I),NY(I),NZ(I),KNORML(I),ISFACE(I)
CC
MULT=1
IF(KSYM2.EQ.0)MULT=2
MULTY=1
IF(KSYM1.EQ.0)MULTY=2
CC
CC
CC
NTBODY=NBODY1+NBODY2+NBODY3

```



```

CC      NNODEX=0
      NNODEU=0
      IF (NTBODY.EQ.0) GO TO 17
      NNODEX=1
      DO 28 I=1,NTBODY
      28 NNODEX=NNODEX+NX(I)
      18 CONTINUE
CC      IF (NTBODY.NE.0)
      1 NNODEU=NNODEU+NNODEX*(NY(NTBODY)+1) - (NTBODY-1)*NY(NTBODY)
CC
CC      NNODEX=NUMBER OF NODES ALONG AIRCRAFT CENTERLINE
CC
CC      NNODEU=NUMBER OF NODES ON UPPER RHS FUSELAGE BODY
CC
CC
      IS=0
      NNODES=0
      NLAST=0
C
      IF (NBODY1.EQ.0) GO TO 99
      IS=ISA1
      NXP=NX(IS)+1
      NYP=NY(IS)+1
      DO 88 IY=1,NYP
      DO 88 IX=1,NXP
      IXY=IX+(IY-1)*NXP
C
      IF (IX.EQ.1.AND.IY.GT.1) GO TO 85
      NNODES=NNODES+1
      85 CONTINUE
      INODE=NNODES
      IF (IX.EQ.1) INODE=1
      NOECT (IXY, IS) = INODE
      88 CONTINUE
      99 CONTINUE
C
      NLAST=NNODES
      IF (NBODY2.EQ.0) GO TO 199
      IS=ISA1
      NXP=NX(IS)+1
      NYP=NY(IS)+1
      DO 188 IY=1,NYP
      DO 188 IX=1,NXP
      IXY=IX+(IY-1)*NXP
C
      IF (IX.EQ.1) GO TO 185
      NNODES=NNODES+1
      185 CONTINUE
      INODE=NNODES
      IF (IX.EQ.1) INODE=(NX(1)+1)+(IY-1)*NX(1)
      NOECT (IXY, IS) = INODE
      188 CONTINUE
      199 CONTINUE
C

```

```

NLAST=NODE0
IF(MR0NY3.EQ.8)GO TO 299
IS=IS+1
NXP=NY(IS)+1
NYP=NY(IS)+1
DO 288 IX=1,NXP
DO 288 IX=1,NXP
IXY=IX+(IX-1)*NYP
C
IF(IX.EQ.1)GO TO 285
IF(IX.EQ.NXP.AND.IY.GT.1)GO TO 295
NODE0=NODE0+1
285 CONTINUE
INODE=NODE0
IF(IX.EQ.1)INODE=
1 NX(1)*(NY(1)+1)+1+
2 NX(2)*(IX-1)*NX(2)
IF(IY.EQ.NYP)INODE=
1 NX(1)*(NY(1)+1)+1+
2 NX(2)*(NY(2)+1)+
3 NX(3)
NOECT(IXY,IS)=INODE
288 CONTINUE
299 CONTINUE
C
NLAST=NODE0
C
IF(MR0YL0.EQ.8)GO TO 399
IS=IS+1
NXP=NY(IS)+1
NYP=NY(IS)+1
DO 388 IX=1,NXP
DO 388 IX=1,NXP
IXY=IX+(IX-1)*NYP
C
IF(IX.EQ.1.AND.IY.GT.1)GO TO 385
IF(IX.EQ.NXP)GO TO 385
NODE0=NODE0+1
385 CONTINUE
INODE=NODE0
IF(IX.EQ.1)INODE=
1 NLAST+1
IF(IX.EQ.NXP)INODE= NX(1)*(NY(1)+1)+1+NYP-(IX-1)
NOECT(IXY,IS)=INODE
388 CONTINUE
399 CONTINUE
NLAST=NODE0
C
IF(KSYMHZ.NE.8)GO TO 499
IF(MR0DY1.EQ.8)GO TO 499
IS=IS+1
NXP=NY(IS)+1
NYP=NY(IS)+1
DO 488 IX=1,NXP
DO 488 IX=1,NXP
IXY=IX+(IX-1)*NYP
C

```

```

IF (IX.EQ.1) GO TO 485
IF (IY.EQ.NYP) GO TO 445
NODE0=NODE0+1
445 CONTINUE
INODE=NODE0
IF (IX.EQ.1) INODE=1
IF (IX.NE.1.AND.IY.EQ.NYP) INODE=
1 NX(1)+NY(1)+IX
NOFCT (IXY,IS) = INODE
448 CONTINUE
499 CONTINUE
C
NLAST=NODE0
C
IF (KSYMHZ.NE.0) GO TO 503
IF (NBODY2.EQ.0) GO TO 509

IS=IS+1
NXP=NX (IS) +1
NYP=NY (IS) +1
DO 588 IY=1,NYP
DO 588 IX=1,NXP
IXY=IX+(IY-1)*NXP
C
IF (IX.EQ.1) GO TO 585
IF (IY.EQ.NYP) GO TO 545
NODE0=NODE0+1
545 CONTINUE
INODE=NODE0
IF (IX.EQ.1.AND.IY.NE.NY) INODE=
1 NLAST-NX(1)*(NY(1)-2)-(NX(1)-1)-1+(IY-1)*NX(1)
IF (IX.EQ.1.AND.IY.EQ.NY) INODE=
1 NX(1)*(NY(1)+1)+1
IF (IY.EQ.NYP.AND.IY.NE.1) INODE=
1 NX(1)*(NY(1)+1)+1+
2 NX(2)+NY(2)-1+IX
NOFCT (IXY,IS) = INODE
548 CONTINUE
599 CONTINUE
C
NLAST=NODE0
IF (KSYMHZ.NE.0) GO TO 603
IF (NBODY3.EQ.0) GO TO 609
IS=IS+1
NXP=NX (IS) +1
NYP=NY (IS) +1
DO 688 IY=1,NYP
DO 688 IX=1,NXP
IXY=IX+(IY-1)*NXP
C
IF (IX.EQ.1) GO TO 685
IF (IY.EQ.NYP) GO TO 645
IF (IX.EQ.NXP) GO TO 685
NODE0=NODE0+1
645 CONTINUE
INODE=NODE0
IF (IX.EQ.1.AND.IY.NE.NY) INODE=

```

```

1 NLAST-NX(2)*(NY(2)-2)-(IX(2)-1)-1+(IY-1)*NX(2)
IF(IY.EQ.NXP.AND.(IX.NE.1.OR.IX.NE.NXP))INODE=
1 NX(1)*(NY(1)+1)+1
2 NX(2)*(NY(2)+1)+1
3 (NX(3)-1)*NY(3)+1+(IX-1)
IF(IY.EQ.NXP)INODE=
1 NX(1)*(NY(1)+1)+1+
2 NX(2)*(NY(2)+1)+
3 NX(3)
IF(IY.EQ.1.AND.IY.EQ.NXP)INODE=
1 NX(1)*(NY(1)+1)+1+NX(2)*(NY(2)+1)
NOFCT(IX,IS)=INODE
688 CONTINUE
699 CONTINUE
C
NLAET=NODE8
NODE7=NLAET
IF(NVITAIL.EQ.8)GO TO 78
IS=IS+1
NXP=NX(IS)+1
NYP=NY(IS)+1
DO 788 IX=1,NXP
DO 788 IX=1,NXP
IXY=IX+(IY-1)*NXP
C
NODE8=NODE8+1
INODE=NODE8+NLAET
NOFCT(IX,IS)=INODE
788 CONTINUE
799 CONTINUE
C
NLAET=NODE8
IF(KSYHMY.NE.0) GO TO 833
IF(NBODY1.EQ.8)GO TO 89
IS=IS+1
NXP=NX(IS)+1
NYP=NY(IS)+1
DO 888 IX=1,NXP
DO 888 IX=1,NXP
IXY=IX+(IY-1)*NXP
C
IF(IY.EQ.1) GO TO 845
IF(IY.EQ.1) GO TO 885
NODE8=NODE8+1
885 CONTINUE
INODE=NODE8
IF(IX.EQ.1)INODE=1
IF(IY.EQ.1)INODE=IX
NOFCT(IX,IS)=INODE
888 CONTINUE
899 CONTINUE
C
NLAET=NODE8
IF(KSYHMY.NE.8) GO TO 933
IF(NBODY2.EQ.8)GO TO 999
IS=IS+1
NXP=NX(IS)+1

```



```

NYP=NY(IS)+1
KPYL1=1
KPYL2=2
K1=KPYL1+2
K2=K1+NX(4)-2
DO 988 IY=1,NYP
DO 988 IX=1,NXP
IXY=IX+(IY-1)*NXP

C
IF(MPYLON.NE.0) GO TO 951
IF(IX.EQ.1) GO TO 985
IF(IY.EQ.1) GO TO 985
NODE0=NODE0+1
985 CONTINUE
INODE=NODE0
IF(IX.EQ.1) INODE=
1 NLAST-NX(1)*(NY(1)-1)-(NX(1)-1)-1+(IY-1)*NX(1)
IF(IY.EQ.1) INODE=
2 NX(1)*(NY(1)+1)+1+(IX-1)
IF(IX.EQ.1.AND.IY.EQ.1) INODE=
1 NX(1)+1
GO TO 949
950 CONTINUE
IF(IY.EQ.1) GO TO 951
IF(IY.EQ.1.AND.(IX.LT.M.OR.IX.GT.K2)) GO TO 951
NODE0=NODE0+1
951 CONTINUE
INODE=NODE0
IF(IX.EQ.1) INODE=NLAST-NX(1)*(NY(1)-1)-(NX(1)-1)-1+(IY-1)*NX(1)
IF(IX.EQ.1.AND.(IX.LT.M.OR.IX.GT.K2)) INODE=
1 NX(1)*(NY(1)+1)+1+(IX-1)
IF(IX.EQ.1.AND.IY.EQ.1) INODE=NX(1)+1
949 CONTINUE
NOECT(IY,IS)=INODE
988 CONTINUE
989 CONTINUE

C
NLAST=NODE0
IF(KSYMMY.NE.0) GO TO 1039
IF(MBOCY3.EQ.0) GO TO 1021
IS=IS+1
NYP=NY(IS)+1
DO 1088 IY=1,NYP
DO 1088 IX=1,NXP
IXY=IX+(IY-1)*NXP

C
IF(IY.EQ.1) GO TO 1085
IF(IY.EQ.1) GO TO 1085
IF(IY.EQ.NYP) GO TO 1085
NODE0=NODE0+1
1085 CONTINUE
INODE=NODE0
IF(IX.EQ.1) INODE=
1 NLAST-NX(2)*(NY(2)-1)+(IY-2)*NX(2)
IF(IY.EQ.1) INODE=
1 NX(1)*(NY(1)+1)+1+NX(2)*(NY(2)+1)+(IX-1)

```

```

IF(IX.EQ.1.AND.IY.EQ.1)INODE=
1 NX(1)*(NY(1)+1)+NX(2)
IF(IX.EQ.NXP)INODE=
1 NX(1)+NY(1)+1+1
2 NX(2)*(NY(2)+1)+NX(3)
MOECT(IY,IS)=INODE
1080 CONTINUE
1090 CONTINUE
C
NLAST=NODE0
IF(KSYMHY.NE.0) GO TO 1139
IF(NPYLON.EQ.0)GO TO 1193
IS=IS+1
NXP=NY(IS)+1
NYP=NY(IS)+1
DO 1188 IY=1,NYP
DO 1180 IX=1,NXP
IYI=IY+(IY-1)*NXP
C
IF(IY.EQ.1)GO TO 1185
IF(IX.EQ.1.OR.(IX.EQ.NXP))GO TO 1185
IF(IY.EQ.NYP)GO TO 1185
NODE0=NODE0+1
1185 CONTINUE
INODE=NODE0
IF(IY.EQ.1)INODE=NODE0+1
IF(IX.EQ.1)INODE=NODE0+1
IF(IY.EQ.NYP.AND.IX.NE.1)INODE=NODE0+1+(NXP-2)*(NYP-1)+1+(IY-2)
IF(IX.EQ.NXP)INODE=NLAST-(NX(3)-1)*NY(3)-NX(2)*NY(2)+1-(IY-1)
IF(IY.EQ.1.AND.IX.EQ.NXP)INODE=NX(1)*(NY(1)+1)+1+NX(2)+1
IF(IY.EQ.NYP.AND.IX.EQ.NXP)INODE=NX(1)*(NY(1)+1)+1+1
MOECT(IY,IS)=INODE
1180 CONTINUE
1190 CONTINUE
C
NLAST=NODE0
IF(KSYMHZ.NE.0) GO TO 1239
IF(NBODY1.EQ.0)GO TO 1293
IS=IS+1
NXP=NY(IS)+1
NYP=NY(IS)+1
DO 1288 IY=1,NYP
DO 1280 IX=1,NXP
IYI=IY+(IY-1)*NXP
C
IF(IY.EQ.1)GO TO 1285
IF(IX.EQ.1)GO TO 1285
IF(IY.EQ.NYP)GO TO 1285
NODE0=NODE0+1
1285 CONTINUE
INODE=NODE0
RSS=0
IF(NPYLON.EQ.0)PSS=1.
IF(RSS.EQ.1)GO TO 1298
IF(IX.EQ.1)INODE=1
IF(IY.NE.1.AND.IY.EQ.1)INODE=
1 NODE0+

```

```

2 (NX(4)-1)*(NY(4)+1)+IX
IF (IX.NE.1.AND.IY.EQ.NY2) INODE=NLAST-
1 NX(4)*(NY(4)-1)-(NX(3)-1)*NY(3)-
2 NX(2)*NY(2)+NX(1)*(IX-1)
GO TO 1250
1290 CONTINUE
IF (IX.EQ.1) INODE=1
IF (IX.NE.1.AND.IY.EQ.1) INODE=
1 NODEU+(IX-1)
IF (IX.NE.1.AND.IY.EQ.NY2) INODE=
1 NODEU+NX(1)*NY(1)+NX(2)*Y(2)+(NX(3)-1)*NY(3)+
2 NY(1)*NY(1)+1*(IX-1)
1250 CONTINUE
NODET(IY,IS)=INODE
1280 CONTINUE
1290 CONTINUE
C
NLAST=NODEB
IF (KSYMHZ.NE.0) GO TO 1393
IF (MBOY2.EQ.0) GO TO 1333
IS=IS+1
NXP=NY (IS)+1
NYP=NY (IS)+1
DO 1380 IY=1,NYP
DO 1380 IX=1,NXP
IXY=IX+(IY-1)*NXP
C
IF (IY.EQ.1) GO TO 1385
IF (IX.EQ.1) GO TO 1385
IF (IY.EQ.NYP) GO TO 1385
NODEB=NODEB+1
1385 CONTINUE
INODE=NODEB
PSS=0.
IF (NPYLON.EQ.0) PSS=1.
IF (PSS.EQ.1) GO TO 1390
IF (IX.EQ.1.AND.(IY.NE.1.OR.IY.NE.NYP)) INODE=
1 NLAST-NX(1)*(NY(1)-1)+IX(2)*NY(1)
IF (IX.EQ.1.AND.IY.EQ.1) INODE=
1 NODEU+NX(1)+1*(NY(1)+1)+1*(IX(1))
IF (IX.GT.1.AND.IY.EQ.1) INODE=
1 NODEU+NX(1)+1*(NY(1)+1)+1*(IX(1))
2 NX(1)*NY(1)+(IX-1)
IF (IX.EQ.1.AND.IY.EQ.NY2) INODE=
1 NLAST-NX(1)*(NY(1)-1)+IX(4)*(NY(4)-1)-
2 (NY(3)-1)*NY(3)+NX(2)*NY(3)
IF (IX.GT.1.AND.IY.EQ.NY2) INODE=
1 NLAST-NX(1)*(NY(1)-1)-
2 (NX(4)-1)*(NY(4)-1)-(NX(3)-1)*NY(3)-
3 NX(2)+IX(1)
GO TO 1350
1390 CONTINUE
IF (IX.EQ.1.AND.(IY.NE.1.OR.IY.NE.NYP)) INODE=
1 NLAST-NX(1)*(NY(1)-1)+1*(IX(2)+1)*NY(1)
2 +NX(1)
IF (IX.EQ.1.AND.IY.EQ.1) INODE=
1 NODEU+NX(1)

```

```

IF(IY.EQ.1.AND.IX.NE.1)INODE=
1 NODEU+NX(1)*NY(1)+IX-1
IF(IX.EQ.1.AND.IY.EQ.NY) INODE=
1 NLAST-NX(1)*NY(1)-1+IX(1)-1+NY(1)-NX(1)*NY(1)
IF(IX.NE.1.AND.IY.EQ.NY)INODE=
1 NLAST-NX(1)*NY(1)-1+IX(1)-1+NY(1)-NX(1)+IX-1
1350 CONTINUE
NOECT(IY,IS)=INODE
1360 CONTINUE
1380 CONTINUE
NLA=NODE0
IF(NBODY3.EQ.0)GO TO 1422
IS=IS+1
NXP=NX(IS)+1
NYP=NY(IS)+1
DO 1460 IX=1,NXP
DO 1480 IY=1,NYP
IYY=IY+(IY-1)*NXP
C
IF(IY.EQ.1)GO TO 1485
IF(IY.EQ.1)GO TO 1485
IF(IY.EQ.NYP)GO TO 1485
IF(IX.EQ.NXP)GO TO 1485
NODE0=NODE0+1
1485 CONTINUE
INODE=NODE0
PSS=0.
IF(NBYLON.EQ.0)PSS=1.
IF(PSS.EQ.1)GO TO 1490
IF(IY.EQ.1)INODE=NLA=
1 NX(2)+(IY-2)*NX(2)
IF(IX.EQ.1.AND.IY.EQ.1)INODE=
1 NODEU+(NX(4)-1)*(NY(4)+1)+1+
2 NX(1)*NY(1)+NX(2)
IF(IX.NE.1.AND.IY.EQ.1)INODE=
1 NODEU+(NX(1)-1)*(NY(1)+1)+1+NX(1)*NY(1)
2 NX(2)*NY(2)+(IX-1)
IF(IY.EQ.NYP.AND.IX.EQ.1)INODE=
1 NLAST-NX(2)*(NY(2)-1)+IX(1)*(NY(1)-1)-
2 (NX(1)-1)*(NY(1)-1)+NX(1)*NY(1)
3 +NX(3)
IF(IY.EQ.NYP.AND.IX.NE.1)INODE=
1 NLAST-NX(2)*(NY(2)-1)+IX(1)*(NY(1)-1)-
2 (NX(1)-1)*(NY(1)-1)+NX(1)*NY(1)+IX-1
IF(IX.EQ.NXP)INODE=
1 NX(1)*(NY(1)+1)+NX(2)*NY(2)+1+NX(3)+1
GO TO 1450
1490 CONTINUE
IF(IY.EQ.1)INODE=
1 NODEU+NX(1)*NY(1)+NX(2)*NY(2)+IX-1
IF(IY.EQ.NYP)INODE=
1 NLAST-NX(2)*(NY(2)-1)+IX(1)*(NY(1)-1)-NX(1)+IX
IF(IX.EQ.NXP)INODE=
1 NODEU+(NX(1)+1)*NY(1)
IF(IX.EQ.1)INODE=
1 NLAST-NX(2)-(NX(2)-1)-1+(IY-2)*NX(2)
2 +NX(2)

```



```

IF(IX.EQ.1.AND.IY.EQ.1)INODE=
1 NODEU+NX(1)+NY(1)+NX(2)
IF(IX.EQ.1.AND.IY.EQ.NYP)INODE=
1 NLAST-NX(2)+NY(2)+1-NX(1)+NY(1)-1-NX(3)+NY(3)
1458 CONTINUE
NOFCT(IY,IS)=INODE
1468 CONTINUE
1499 CONTINUE
NLASt=NODE0
IF(INVTAL.EQ.0)GO TO 1503
IS=IS+1
NXP=NX(IS)+1
NYP=NY(IS)+1
DO 1548 IY=1,NYP
DO 1588 IX=1,NXP
IXY=IX+(IY-1)*NXP
C
IF(IY.EQ.1.OR.IY.EQ.NYP)GO TO 1585
IF(IY.EQ.NYP)GO TO 1585
NODE0=NODE0+1
1585 CONTINUE
INODE=NODE0
IF(IX.EQ.1)INODE=
1 NODET+(IY-1)*NX(1)+1
IF(IX.EQ.NXP)INODE=
1 NODET+1+NX(1)+(IY-1)*NX(1)+1
IF(IY.EQ.NYP)INODE=
1 NODET+NX(1)+1+NY(1)+1
NOFCT(IY,IS)=INODE
1588 CONTINUE
1599 CONTINUE
C
NLASt=NODE0
NBOdy=NODE0
IF(INSHAFT.EQ.0)GO TO 1633
IS=IS+1
NXP=NX(IS)+1
NYP=NY(IS)+1
DO 1688 IY=1,NYP
DO 1688 IX=1,NXP
IXY=IX+(IY-1)*NXP
C
NODE0=NODE0+1
INODE=NODE0
NOFCT(IY,IS)=INODE
1688 CONTINUE
1699 CONTINUE
C
NLASt=NODE0
IF(KSYHMY.EQ.0)GO TO 1739
IF(INSHAFT.EQ.0)GO TO 1739
IS=IS+1
NXP=NX(IS)+1
NYP=NY(IS)+1
DO 1788 IY=1,NYP
DO 1788 IX=1,NXP
IXY=IX+(IY-1)*NXP

```

```

C
IF (IY.EQ.1.OR.IY.EQ.NXP) GO TO 1735
NODE8=NODE8+1
1735 CONTINUE
INODE=NODE8
IF (IY.EQ.1) INODE=
1 NBODY+IX
IF (IY.EQ.NXP) INODE=
1 NBODY+(NX(IS)+1)*NY(IS)+IX
NOFCT (IXY, IS) = INODE
1780 CONTINUE
1790 CONTINUE
C
MLAST=NODE8
IF (NHUB.EQ.8) GO TO 1899
IS=IS+1
NXP=NX (IS)+1
NYP=NY (IS)+1
DO 1880 IY=1, NYP
DO 1880 IX=1, NXP
IXY=IX+(IY-1)*NXP
C
IF (IX.EQ.1.AND.IY.GT.1) GO TO 1885
NODE8=NODE8+1
1885 CONTINUE
INODE=NODE8
IF (IX.EQ.1) INODE=MLAST+1
NOFCT (IXY, IS) = INODE
1888 CONTINUE
1890 CONTINUE
C
MLAST=NODE8
IF (KSYMMZ.NE.8) GO TO 1939
IF (NHUB.EQ.8) GO TO 1930
IS=IS+1
NXP=NX (IS)+1
NYP=NY (IS)+1
DO 1920 IY=1, NYP
DO 1920 IX=1, NXP
IXY=IX+(IY-1)*NXP
C
IF (IY.EQ.1.AND.IY.GT.1) GO TO 1985
IF (IX.EQ.NXP) GO TO 1985
NODE8=NODE8+1
1985 CONTINUE
INODE=NODE8
IF (IX.EQ.1) INODE=NBODY+
1 (NY (IS)+1)*(NY (IS)+1)
2 (NX (IS)+1)*(NY (IS)-1)
3 NY (IS)* (NY (IS)+1)
IF (IX.EQ.NXP) INODE=NBODY+
1 (NX (IS)+1)*(NY (IS)+1)
2 (NX (IS)+1)*(NY (IS)-1)
3 (NY (IS)+1)*(IY-1)*NX (IS)
NOFCT (IXY, IS) = INODE
1988 CONTINUE
1999 CONTINUE

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C
  NLAST=NODE8
  IF(KSYMHV.NE.0) GO TO 2199
  IF(NHUB.EQ.8) GO TO 2888
  IS=IS+1
  NXP=NX(IS)+1
  NYP=NY(IS)+1
  DO 2888 IY=1,NYP
  DO 2888 IX=1,NXP
  IXY=IX+(IY-1)*NXP

C
  IF(IY.EQ.1) GO TO 2888
  IF(IY.EQ.1.OR.IY.EQ.NYP) GO TO 2885
  NODE8=NODE8+1
2885 CONTINUE
  INODE=NODE8
  IF(IX.EQ.1) INODE=NBODY+
  1 (NX(15)+1)*(NY(15)+1)+
  2 (NX(16)+1)*(NY(16)-1)+
  3 1
  IF(IY.EQ.1.AND.IX.NE.1) INODE=
  1 NBODY+(NX(15)+1)*(NY(15)+1)+
  2 (NX(16)+1)*(NY(16)-1)+
  3 IY
  IF(IY.EQ.NYP.AND.IX.NE.1) INODE=
  1 NBODY+(NX(15)+1)*(NY(15)+1)+
  2 (NX(16)+1)*(NY(16)-1)+
  3 NY(17)+NY(17)+1
  NOFCT(IXY,IS)=INODE
2888 CONTINUE
2899 CONTINUE
C
  NLAST=NODE8
  IF(KSYMHV.NE.0) GO TO 2199
  IF(NHUB.EQ.6) GO TO 2199
  IS=IS+1
  NXP=NX(IS)+1
  NYP=NY(IS)+1
  DO 2180 IY=1,NYP
  DO 2180 IX=1,NXP
  IXY=IX+(IY-1)*NXP

C
  IF(IX.EQ.1) GO TO 2185
  IF(IY.EQ.1.OR.IY.EQ.NYP) GO TO 2185
  IF(IX.EQ.NXP) GO TO 2185
  NODE8=NODE8+1
2185 CONTINUE
  INODE=NODE8
  IF(IX.EQ.1) INODE=NBODY+
  1 (NX(15)+1)*(NY(15)+1)+
  2 (NX(16)+1)*(NY(16)-1)+
  3 NY(17)+NY(17)+1
  4 1
  IF(IY.EQ.1.AND.IX.NE.1) INODE=NBODY+
  1 (NX(15)+1)*(NY(15)+1)+
  2 (NX(16)+1)*(NY(16)-1)+
  3 NX(17)*(NY(17)+1)+1

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4 IX
IF (IY .EQ. NYP .AND. IX .NE. 1) INODE=NBODY+
1 (NX(15)+1)*(NY(15)+1)+
2 (NX(16)+1)*(NY(16)-1)+
3 NX(17)*(NY(17)+1)+1+
4 (NX(18)-1)*NY(18)+IX
IF (IX .EQ. NXP) INODE=NBODY+
1 (NX(15)+1)*(NY(15)+1)+
2 (NX(16)+1)*(NY(16)-1)+
3 NX(17)*(NY(17)+1)+1+
4 (NX(18)-1)*(NY(18)+1)+1+
5 NX(19)*(IY-3)*NX(19)
IF (IX .EQ. NXP .AND. IY .EQ. NYP) INODE=
1 NBODY+
2 (NX(15)+1)*(NY(15)+1)+
3 (NX(16)+1)*(NY(16)-1)+
4 NX(17)*(NY(17)+1)+1
IF (IY .EQ. NYP .AND. IY .EQ. 1) INODE=
1 NBODY+
2 (NX(15)+1)*(NY(15)+1)+
3 (NX(16)+1)*(NY(16)-1)+NX(17)
4 1
NOFCT (IXY, IS) = INODE
2198 CONTINUE
2199 CONTINUE
C
NLAST=NODE0
IF (NLSMANK .EQ. 8) GO TO 2222
IS=IS+1
NXP=NY (IS)+1
NYP=NY (IS)+1
DO 2288 IY=1, NYP
DO 2288 IX=1, NXP
IXY=IX+(IY-1)*NXP
C
IF (IY .EQ. NYP) GO TO 2285
NODE0=NODE0+1
2285 CONTINUE
INODE=NODE0
IF (IY .EQ. NYP) INODE=NLAST+IY
NOFCT (IXY, IS) = INODE
2288 CONTINUE
2299 CONTINUE
C
NLAST=NODE0
IF (NBLADE .EQ. 8) GO TO 2303
IS=IS+1
NXP=NY (IS)+1
NYP=NY (IS)+1
DO 2388 IY=1, NYP
DO 2388 IX=1, NXP
IXY=IX+(IY-1)*NXP
C
NODE0=NODE0+1
INODE=NODE0
NOFCT (IXY, IS) = INODE
2388 CONTINUE

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2399 CONTINUE
C
NLAST=NODE0
IF(KSYNTHZ.NE.0) GO TO 2439
IF(NBLADE.EQ.0) GO TO 2439
IS=IS+1
NXP=NX(IS)+1
NYP=NY(IS)+1
DO 2480 IY=1,NYP
DO 2488 IX=1,NXP
IXY=IX+(IY-1)*NXP
C
IF(IX.EQ.1.OR.IX.EQ.NXP) GO TO 2485
IF(IY.EQ.NYP) GO TO 2485
NODE0=NODE0+1
2485 CONTINUE
INODE=NODE0
IF(IY.EQ.1) INODE=
1 NLAST-NXP*NYP+(IY-1)*NXP
1 +1
IF(IX.EQ.NXP) INODE=NLAST-NXP*NYP+1+(IY-1)*NXP*NX(IS)
IF(IY.EQ.NYP) INODE=NLAST-NXP+IX
NOFCT(IXY,IS)=INODE
2488 CONTINUE
2499 CONTINUE
C
NLAST=NODE0
NTEMP=NODE0
IF(NSHANK.EQ.0) GO TO 2533
IS=IS+1
NXP=NX(IS)+1
NYP=NY(IS)+1
DO 2580 IY=1,NYP
DO 2588 IX=1,NXP
IXY=IX+(IY-1)*NXP
C
IF(IY.EQ.NYP) GO TO 2585
NODE0=NODE0+1
CC
2585 CONTINUE
INODE=NODE0
IF(IY.EQ.NYP) INODE=NLAST+IX
NOFCT(IXY,IS)=INODE
2588 CONTINUE
2599 CONTINUE
C
NLAST=NODE0
IF(NBLADE.EQ.0) GO TO 2633
IS=IS+1
NXP=NX(IS)+1
NYP=NY(IS)+1
DO 2680 IY=1,NYP
DO 2688 IX=1,NXP
IXY=IX+(IY-1)*NXP
C
NODE0=NODE0+1
INODE=NODE0

```

```

NOFCT (IXY, IS) = INODE
2688 CONTINUE
2699 CONTINUE
C
NLAST=NODE0
IF (INBLADE.EQ.0) GO TO 2723
IS=IS+1
NXP=NX (IS) + 1
NYP=NY (IS) + 1
DO 2788 IX=1, NXP
DO 2788 IX=1, NXP
IXY=IX+(IX-1)*NXP
C
IF (IX.EQ.1.OR.IX.EQ.NXP) GO TO 2785
IF (IY.EQ.NYP) GO TO 2785
NODE0=NODE0+1
2785 CONTINUE
INODE=NODE0
IF (IX.EQ.1) INODE=NLAST-NXP*NYP+(IY-1)*NXP
1 * 1
IF (IX.EQ.NXP) INODE=NLAST-NXP*NYP+1+(IY-1)*NXP+NX (IS)
IF (IY.EQ.NYP) INODE=NLAST-NXP*IX
NOFCT (IXY, IS) = INODE
2788 CONTINUE
2799 CONTINUE
NLAST=NODE0
NODE=NLAST
CC
CC
C
IF (KSYMHY.EQ.0) NSYMHY=1
IF (KSYMHY.NE.0) NSYMHY=2
IF (KSYMHZ.EQ.0) NSYMHZ=1
IF (KSYMHZ.NE.0) NSYMHZ=2
C
NNODE=NODE0
WRITE (6,4000)
4000 FORMAT (//18X,6HPREPRO)
WRITE (6,4001) NNODE
4001 FORMAT (5X,6NNODE=,15)
DO 100 IS=1, NS
NXP=NX (IS) + 1
NYP=NY (IS) + 1
DO 100 IX=1, NXP
IXY=IX+(IX-1)*NXP
WRITE (6,200) IS, IX, IY, IXY, NOFCT (IXY, IS)
100 CONTINUE
200 FORMAT (2X, *IS=*, IS, 2X, *IX=*, IS, 2X, *IY=*, IS, 2X, *IXY=*, IS, 2X,
1 *NOFCT=*, IS)
RETURN
END

```

```

SUBROUTINE GEOMET (NELEM, NXYMP, NOFCT, NODE, XK, NTNODE, KWAKE, KROTOR)
C
C
COMMON/ZZZ1/XY(34), NY(34), NXY(34), KSYMMY, KSYMMZ, NSYMMY, NSYMMZ
COMMON/ZZZ2/NSFX, NSBODY, NS, NT(34), ISFACE(34), KNORHL(34), KWAKES(34)
COMMON/ZZZ3/NRYLON, NBOOY1, NBOOY2, NBOOY3, NYTAIL, NSHAFT, NHUB, NSMANK,
1 NBLADE
COMMON/ZZZ4/CIMACH, OMEGA, ALFA, ABETA
COMMON/ZZZ5/KPYCTR, YPYCTR, ZPYCTR, RXPYL, RYPYL, RZPYL
COMMON/ZZZ6/XNOSE, XBD1, XBD2, XTATI
COMMON/ZZZ7/YNOSE, YBD1, YBD2, YTAIL
COMMON/ZZZ8/ZNOSE, ZBD1, ZBD2, ZTATI
COMMON/ZZZ9/RYBD1, RZBD1, RYBD2, RZBD2
COMMON/ZZZ10/RSHAFT, LSHAFT, RSHANK, LSHANK
COMMON/ZZZ11/XHUBCR, YHUBCR, ZHUBCR, RXHUB, RYHUB, RZHUB
COMMON/ZZZ12/KROTOR, BCMD10, TAUBL, ALFA0
COMMON/ZZZ13/THET75, THET1C, THET1S, CONING, AZIMUTH
COMMON/ZZZ14/KBLADE, TAM1B, TANTB, XBLE, YBLE, KROTOR(34)
COMMON/ZZZ15/VSPAN, XLEZV, XTEZV, TANLEV, TANTEV, TAU, ZVTAIL
COMMON/ZZZ16/MMAKPY, MMAC1B, MMAKSK, MMAKBL
COMMON/ZZZ17/MAKLPY, MAK1B, MAKLSK, MAKBL
COMMON/ZZZ18/MANGPY, MANG1B, MANGSK, MANGBL
COMMON/ZZZ19/KPRINT(10), NREAD, NWRITE, KREAD
COMMON/ZZZ20/RT
COMMON/ZZZ21/KPY1, KPY2
COMMON/ZZZ22/KNSELE, KNSS1B, KNSTYP
COMMON/ZZZ23/KBOELE, KBOS1P, KBOTYP
COMMON/ZZZ24/KINELE, KINS1B, KINTYP
COMMON/ZZZ25/KPYELE, KPYS1P, KPYYTP
COMMON/ZZZ26/KVTELE, KVTS1B, KVTTYTP
COMMON/ZZZ27/KSHELE, KSHS1P, KSHTYP
COMMON/ZZZ28/KMBELE, KMBS1P, KMBTYP
COMMON/ZZZ29/KSKELE, KSKS1P, KSKTYP
COMMON/ZZZ30/KBLELE, KBL11P, KBLTYP
COMMON/ZZZ31/NSTAG, NVORT, NSPIRAL, SPIRAL
DIMENSION KROTOR(NELEM)
DIMENSION XK(3, NTNODE), JFCT(NXYMP, 34), KWAKE(NELEM), NODE(4, NELEM)
REAL LSHAFT, LSHANK
C
C
NSH=NS
NMALE=NELEM
DO 1999 IS=1, NSH
ISFIX=ISFACE(IS)
NXX=NX(IS)
NXP=NXX+1
NYY=NY(IS)
DO 999 IX=1, NXP
DO 999 IY=1, NYY
C
C
IELEM=IX*NXY(IS)+IY-1)+NT(IS)
IF(KNORHL(IS).EQ.-1)GO TO 986
C
C
-- --
++ ++
C

```

```

IXMM=IX
IXPM=IX+1
IXMP=IX
IXPD=IX+1
IYMM=IY
IYPM=IY
IYPP=IY+1
IYPD=IY+1
C
GO TO 987
986 CONTINUE
C
-- --
** **
C
IYMM=IY
IXMP=IX
IXPD=IX+1
IXPM=IX+1
IYMM=IY+1
IYMP=IY
IYPD=IY
IYPM=IY+1
987 CONTINUE
C
IXYPP=IXPP+(IYPP-1)*NXP
IXYPN=IXPN+(IYPM-1)*NXP
IYYPD=IXPD+(IYMD-1)*NXP
IXYMH=IXMM+(IYMH-1)*NXP
C
NODE(1,IELEM)=NOFCT(IXY=1,IS)
NODE(2,IELEM)=NOFCT(IXY=2,IS)
NODE(3,IELEM)=NOFCT(IXY=3,IS)
NODE(4,IELEM)=NOFCT(IXY=4,IS)
KNAKE(IELEM)=0
KROTOR(IELEM)=0
IF(KNAKES(IS).GT.0.AND..X.EQ.NXX)KNAKE(IELEM)=1
IF(KROTOR(IS).NE.0)KRFOR(IELEM)=1
WRITE(6,50)IS,IELEM,NODE(1,IELEM),NODE(2,IELEM),NODE(3,IELEM),
1 NODE(4,IELEM),KNAKE(IELEM),KROTOR(IELEM)
50 FORMAT(5X,'IS=',I5,2X,'IELEM=',I5,2X,'NODE1=',I5,2X,'NODE2=',I5,
1 2X,'NODE3=',I5,2X,'NODE4=',I5,2X,'KNAKE=',I5,2X,'KROTOR=',I5)
C
999 CONTINUE
1999 CONTINUE
C
WRITE(6,60)
60 FORMAT(10X,'==== END OF ICOMET ====')
RETURN
END

```



```

C
SUBROUTINE WEC123 (NELEM, NODE, RC, P1, P2, P3, XK, NNODE)
COMMON /ZZZ1 / NX (36), NY (36), NXY (36), KSYM1, KSYM2, NSYMM1, NSYMM2
COMMON /ZZZ2 / NSFX, NSBODY, NS, NT (36), ISFACE (36), KNORM (36), KMAKES (36)
COMMON /ZZZ3 / NPYLON, NBODY1, NBODY2, NBODY3, NVTAIL, NSHAFT, NHUB, NSHANK,
1 NBLADE
COMMON /ZZZ4 / UNACH, OMEGA, ALFA, ABETA
COMMON /ZZZ5 / XPYCTB, YBYCT2, ZBYCTB, RXPVI, RYBVI, RZBVI
COMMON /ZZZ6 / XNOSE, XBD1, XBD2, XTAIL
COMMON /ZZZ7 / YNOSE, YBD1, YBD2, YTAIL
COMMON /ZZZ8 / ZNOSE, ZBD1, ZBD2, ZTAIL
COMMON /ZZZ9 / XBD1, RZBD1, YBD2, RZBD2
COMMON /ZZZ10 / RSHAFT, LSHAF, RSHANK, LSHANK
COMMON /ZZZ11 / XHUBCR, YHUBCR, ZHUBCR, RXHUB, RYHUB, RZHUB
COMMON /ZZZ12 / RROTOR, RCHORD, TAUBL, ALFA9
COMMON /ZZZ13 / TME1S, TME1C, TME1S, CONINC, AZIMUTH
COMMON /ZZZ14 / KBLADE, TANEB, TANTEB, XBLE, XSTE, KROTORS (36)
COMMON /ZZZ15 / NSPAN, XLEZ, XTEZ, TANL, TANR, TANTEV, TAU, ZVTAIL
COMMON /ZZZ16 / NMAKPY, NMAK1B, NMAKSK, NMAKBL
COMMON /ZZZ17 / NMAKLPY, NMAK1B, NMAKSK, NMAKBL
COMMON /ZZZ18 / WANGPY, WANG1B, WANGSK, WANGBL
COMMON /ZZZ19 / KPRINT (10), NREAD, NWRITE, KREAD
COMMON /ZZZ20 / PI
COMMON /ZZZ21 / KPY1, KPY3
COMMON /ZZZ22 / KNSELE, KNSE1P, KNSTYP
COMMON /ZZZ23 / KBDELE, KBDS1P, KBOTYP
COMMON /ZZZ24 / KTHELE, KTNS1P, KTHYTP
COMMON /ZZZ25 / KPVELE, KPVS1P, KPVTYP
COMMON /ZZZ26 / KVTELE, KVTS1P, KVTTYTP
COMMON /ZZZ27 / KSSELE, KSSE1P, KSSTYP
COMMON /ZZZ28 / KHBELE, KHBS1P, KHSTYP
COMMON /ZZZ29 / KSKELE, KSKE1P, KSKTYP
COMMON /ZZZ30 / KBLELE, KBL1P, KBLTYP
COMMON /ZZZ31 / NSTAG, NVORT, NSPRAL, SPTRAL
DIMENSION XK (3, NNODE), NODE (4, NELEM)
DIMENSION RC (3, NELEM), R1 (3, NELEM), R2 (3, NELEM), R3 (3, NELEM)
REAL LSHAFT, LSHANK
C
ALFAR=ALFA*3.14159/180.
SINALF=SIN(ALFAR)
COSALF=COS(ALFAR)
BETA=SQRT (ABS (1.-UNACH*UNACH))
C
BET=ABETA*3.14159/180.
SINBET=SIN(BET)
COSBET=COS(BET)
C
DO 100 INODE=1, NNODE
XK1=XK (1, INODE)
XK3=XK (3, INODE)
XK (1, INODE)=(XK1*COSALF+XK3*SINALF)/BETA
XK (3, INODE)=(XK1*SINALF+XK3*COSALF)
WRITE (6, 61) INODE, XK1, XK3
61 FORMAT (10X, 'INODE=', I5, 'XK1=', F16.6, 'XK3=', F16.6)
100 CONTINUE
DO 101 INODE=1, NNODE
XK1=XK (1, INODE)

```

```
KK2=KK(2,INODE)
KK(1,INODE)=KK1*COSBET+K2*SINBET
KK(2,INODE)=-KK1*SINBET+K2*COSBET
101 CONTINUE
DO 200 IELEM=1,NELEM
DO 199 K=1,3
YPP=KK(K,NODE(1,IELEM))
YPM=KK(K,NODE(2,IELEM))
YMP=KK(K,NODE(3,IELEM))
YMH=KK(K,NODE(4,IELEM))
PC(K,IELEM)=(YPP+YPM+YMP+YMH)/4.
P1(K,IELEM)=(YPP+YPM-YMP-YMH)/4.
P2(K,IELEM)=(YPP-YPM+YMP-YMH)/4.
P3(K,IELEM)=(YPP-YPM-YMP+YMH)/4.
C
199 CONTINUE
200 CONTINUE
C
WRITE(6,60)
60 FORMAT(10X,'==== END OF VEC 123 ===')
RETURN
END
```

```

C      000000000 SUBROUTINE PRINTA 00000000000000000000000000000000000000000
C
SUBROUTINE PRINTA(NELEM, NXYP, XK, NNODE, PC, NOFCT, NODE, NPRINT)
COMMON/ZZZ1/NX(34), NY(34), NXV(34), KSYM1, KSYM2, KSYM3, KSYM4, KSYM5, KSYM6, KSYM7, KSYM8
COMMON/ZZZ2/NSFX, NSBODY, NS, NT(34), ISFACE(34), KNORML(34), KNAKES(34)
COMMON/ZZZ3/NRYLON, NBD1, NBD2, NBD3, NVTAIL, NSHAFT, NHUB, NSHANK,
1 NBLADE
COMMON/ZZZ4/OMEGA, ALFA, ABETA
COMMON/ZZZ5/KPYCTR, YPYCTR, ZPYCTR, RXPYL, RYPYL, RZPYL
COMMON/ZZZ6/XNOSE, YB01, X302, XTATL
COMMON/ZZZ7/YNOSE, YB01, Y302, YTATL
COMMON/ZZZ8/ZNOSE, ZB01, Z302, ZTATL
COMMON/ZZZ9/RB01, RB01, RB02, RB02, RZ302
COMMON/ZZZ10/LSHAFT, LSHANK, RSHAFT, RSHANK, LSHANK
COMMON/ZZZ11/XHUBCR, YHUBCR, ZHUBCR, RXHUB, RYHUB, RZHUB
COMMON/ZZZ12/RROTOR, RCHORD, TAUBL, ALFA
COMMON/ZZZ13/THET75, THET1C, THET1S, CONING, AZIMUTH
COMMON/ZZZ14/KBLADE, TANLE, TANGTE, XBLE, XBLE, KROTOR(34)
COMMON/ZZZ15/VSPAN, XLEZV, XTEZV, TANLEY, TANTEV, TAU, ZVTAIL
COMMON/ZZZ16/MAKPY, MAK4B, MAK5K, MAK6B
COMMON/ZZZ17/MAKPY, MAK4B, MAK5K, MAK6B
COMMON/ZZZ18/MANGPY, MAN4B, MANGSK, MANG6B
COMMON/ZZZ19/KPRINT(10), KREAD, NWRITE, KREAD
COMMON/ZZZ20/P
COMMON/ZZZ21/KPY1, KPY2
COMMON/ZZZ22/KNSELE, KNS4P, KNS5P
COMMON/ZZZ23/KBDELE, KB04P, KB05P
COMMON/ZZZ24/KXBLE, KX4B, KX5B
COMMON/ZZZ25/KPYELE, KP4P, KP5P
COMMON/ZZZ26/KVTELE, KV4B, KV5B
COMMON/ZZZ27/KSKELE, KS4P, KS5P
COMMON/ZZZ28/KBLELE, KB4B, KB5B
COMMON/ZZZ29/KSKELE, KS4P, KS5P
COMMON/ZZZ30/KBLELE, KB4B, KB5B
COMMON/ZZZ31/NSTAG, NVORT, NSPIRAL, SPIRAL
DIMENSION PC(3, NELEM), XK(3, NNODE), NOFCT(NXYP, 34), NODE(4, NELEM)
REAL LSHAFT, LSHANK
C
      GO TO (1,2,3,4), NPRINT
      CONTINUE
      WRITE(NWRITE, 110)
110  FORMAT(//2X, 'SPECIFICATIONS OF THE PROBLEM')
      DO 112 II=1, NS
      IF(NXY(IT), EQ, DIGNO TO 112)
      WRITE(NWRITE, 113) ISFACE: II)
      WRITE(NWRITE, 114) NX(IT), NY(IT)
112  CONTINUE
113  FORMAT(//2X, 'FOR PART 2: ')
      WRITE(NWRITE, 115) NELEM, CSYM1, KSYM2, REFLN, SPAN, TAU,
      1 ALFA, ALFABC, OMEGA, TZZZ
114  FORMAT(2X, 'NK= ', I2, /2X, 'NY= ', I2)
115  FORMAT(//2X, 'NELEM= ', I3, /2X, 'CSYM1= ', I2, /2X, 'KSYM2= ', I2, /
1 2X, 'REFERENCE LENGTH = ', F6.2/2X, 'SPAN = ', F6.2/
1 2X, 'RING THICKNESS= ', F7.3/2X, 'ALFA = ', F7.3/2X, 'ALFABC = ', F7.3//
1 2X, 'OMEGA NUMBER = ', F7.3/2X, 'TZZZ= ', I5//)
      WRITE(NWRITE, 116) TANGLE, TANGTE, CHORD, R
116  FORMAT(2X, 'TANGLE= ', F6.2/2X, 'TANGTE= ', F6.2/2X, 'CHORD = ', F6.2

```

```

1 //2X,*RADIUS =*,F6.2)
  RETURN
2 CONTINUE
  WRITE(NWRITE,222)
222 FORMAT(//4X,*MODE=*,4X,*K=,10X,*Y=,10X,*Z=//)
  DO 2210 I=1,NMODE
2210 WRITE(NWRITE,221)INODE,(K(K,INODE),K=1,3)
221  FORMAT(4X,I4,3(1X,F10.5))
220 CONTINUE
  RETURN
3 CONTINUE
  WRITE(NWRITE,340)
340 FORMAT(///1X,*ELEM=*,4X,*XPC=.7X,*YPC=.7X,*ZPC=)
  DO 345 I=1,NELEM
345  WRITE(NWRITE,345)I,(PC(K,I),K=1,3)
345  FORMAT(1X,I3,12F10.5)
  RETURN
4 CONTINUE
  WRITE(NWRITE,41)
41  FORMAT(//5X,*MODAL NUMBERING FOR SURFACES=//)
  DO 44 IS=1,NS
  NXE=NX(IS)+1
  NYE=NY(IS)+1
  NXYP=NXE*NYE
  WRITE(NWRITE,46)ISFACE(.5)
  DO 44 IX=1,NXP
  WRITE(NWRITE,45)(NOFCT('XY,IS),IXY=IX,NXYP,NXP)
44  CONTINUE
45  FORMAT(11I6)
46  FORMAT(//5X,*FOR SURFACE =,IS/)
  WRITE(NWRITE,47)
47  FORMAT(//5X,*MODAL NUMBERING FOR ELEMENTS=//)
  WRITE(NWRITE,49)
  DO 48 IELEM=1,NELEM
48  WRITE(NWRITE,45)IELEM,(NODE(ICORNR,IELEM),ICORNR=1,4)
49  FORMAT(//2X,*ELEM=,4X,*K=,4X,*Y=,4X,*Z=//)
  RETURN
  END

```



```
##### SUBROUTINE JEBUG #####  
C  
C  
SUBROUTINE JEBUG(K)  
COMMON/ZZZ19/KPRINT(10),NREAD,NWRITE,KREAD  
WRITE(NWRITE,11)  
1 FORMAT(/2X," ERROR CODE = ",I5/)  
RETURN  
END
```

```

C
C
C
SUBROUTINE PRINTB(NELEM, NESQ, AA, SOURCE, NPRINT)
COMMON/ZZZ1/XY(3), NY(3), NXY(3), KSYM1, KSYM2, NSYMY, NSYMY2
COMMON/ZZZ2/NSFX, NSBODY, YS, NT(34), ISFACE(34), KNORML(34), KNAKES(34)
COMMON/ZZZ3/NRYLOM, NBOOY1, NBOOY2, NBOOY3, NYTAIL, NSHAFT, NMUB, NSHANK,
1 NBLADE
COMMON/ZZZ4/UMACH, JMEGA, ALFA, ABETA
COMMON/ZZZ5/XPYCTR, YPYCTR, ZPYCTR, RXPYLR, RYPYLR, RZPYLR
COMMON/ZZZ6/XNOSE, YB01, Y3D2, YTAIL
COMMON/ZZZ7/YNOSE, YB01, Y3D2, YTAIL
COMMON/ZZZ8/ZNOSE, ZB01, Z3D2, ZTAIL
COMMON/ZZZ9/RB01, RB02, RB03, RB04
COMMON/ZZZ10/RSHAFT, LSHAFT, RSHANK, LSHANK
COMMON/ZZZ11/XHUBCR, YHUBCR, ZHUBCR, RXHUB, RYHUB, RZHUB
COMMON/ZZZ12/RROTQR, RCMGRD, TAUBL, ALFA3
COMMON/ZZZ13/THET75, THET1C, THET1S, CONANG, AZIMUTH
COMMON/ZZZ14/KBLADE, XAMB, YANTEB, XBLE, X3TE, KROTORS(34)
COMMON/ZZZ15/VSPAN, XLEZV, XTEZV, TANLEV, TANTEV, TAU, ZVAIL
COMMON/ZZZ16/HAKRY, HAK4B, HAKSK, HAKBL
COMMON/ZZZ17/HAKPY, HAK4B, HAKSK, HAKBL
COMMON/ZZZ18/HANGRY, HANG4B, HANGSK, HANGBL
COMMON/ZZZ19/KPRINT(10), VREAD, NWRITE, KREAD
COMMON/ZZZ20/PI
COMMON/ZZZ21/KPY1, KPY2
COMMON/ZZZ22/KSLELE, KMS4B, KMSYP
COMMON/ZZZ23/KBDELE, K904P, KBOTYP
COMMON/ZZZ24/KTNELE, KTN4B, KNTYP
COMMON/ZZZ25/KPYELE, KPYS4P, KPITYP
COMMON/ZZZ26/KVTELE, KVT4B, KVITYP
COMMON/ZZZ27/KSHELE, KSHS4P, KSHTYP
COMMON/ZZZ28/KMBELE, KMBS4B, KMBTYP
COMMON/ZZZ29/KSKELE, KSKS4P, KSKTYP
COMMON/ZZZ30/KBLELE, KBL4B, KBLTYP
COMMON/ZZZ31/NSTAG, NVORT, NSPIRAL, SPIRAL
C
DIMENSION SOURCE(NELEM), IA(NESQ)
DIMENSION ABSVAL(100), FISEAN(100)
REAL LSHAFT, LSHANK
NXY(3)=NY(3)
GO TO(1,2,3,4,5), NPRINT
1 CONTINUE
WRITE(NWRITE, 110)
110 FORMAT(//2X, 'DISTRIBUTION OF AA(I, J)')
DO 11 I=1, NELEM
WRITE(NWRITE, 111) I
111 FORMAT(2X, 'INDEX =', I2)
WRITE(NWRITE, 112)(AA(K), K=N1, N2, NELEM)
112 FORMAT(1X, 8E15.6)
11 CONTINUE
RETURN
2 CONTINUE
WRITE(NWRITE, 221)

```

```

221 FORMAT(///2X,*THE DISTRIBUTION OF SOURCE*)
225 CONTINUE
NSBTOT=0
DO 229 IS=1,NS
WRITE(NWRITE,223)ISFACE(IS)
223 FORMAT(//5X,*FOR SUBSURFACE*IS)
IND=NSBTOT
NSBTOT=NSBTOT+NX(IS)*NY(IS)
IFIN=NSBTOT
NXX=NX(IS)
DO 226 IX=1,NXX
WRITE(NWRITE,228)
IF(NPRINT.GE.5.AND.(IX.EQ.NXX))GO TO 226
IND=IND+1
WRITE(NWRITE,227)(SOURC(KK),KK=IND,IFIN,NXX)
226 CONTINUE
227 FORMAT(1X,8E15.5)
228 FORMAT(//)
229 CONTINUE
RETURN
3 CONTINUE
WRITE(NWRITE,330)
330 FORMAT(///2X,*THE DISTRIBUTION OF THE VELOCITY POTENTIAL*)
GO TO 225
4 CONTINUE
WRITE(NWRITE,440)
440 FORMAT(///2X,*THE DISTRIBUTION OF CP*)
GO TO 225
5 CONTINUE
RETURN
END

```

```

C
C
C
SUBROUTINE S3LUTH(NLEEM, NESQ, AA, SOURCE)
C
COMMON/ZZZ1/XY(TA), NY(TA), NY(TB), KSYM1, KSYM2, NSYMY, NSYMZ
COMMON/ZZZ2/NSFX, NSBODY, VS, NT(34), ISFACE(34), KNORML(34), KMAKES(34)
COMMON/ZZZ3/XPYLOM, MBOY1, MBOY2, MBOY3, NYTAIL, NSHAFT, NHUB, NSHANK,
1 NBLADE
COMMON/ZZZ4/MACH, OMEGA, ALFA, ABETA
COMMON/ZZZ5/XPYCTR, YPYCTR, ZPYCTR, RXPYL, RYPYL, RZPYL
COMMON/ZZZ6/XNOSE, YB01, ZB02, XTATL
COMMON/ZZZ7/YNOSE, YB01, YB02, YTAIL
COMMON/ZZZ8/ZNOSE, ZB01, ZB02, ZTATL
COMMON/ZZZ9/RYP01, RZB01, RYB02, RZB02
COMMON/ZZZ10/RSHAFT, LSHAFT, RSHANK, LSHANK
COMMON/ZZZ11/XHUBCR, YHUBCR, ZHUBCR, RXHUB, RYHUB, RZHU3
COMMON/ZZZ12/PROTOR, BCH, TD, TAUBL, ALFA2
COMMON/ZZZ13/THET75, THET1C, THET1S, CONING, AZIMUTH
COMMON/ZZZ14/KBLADE, TAN, EB, TANTEB, XBLE, XSTE, KROTORS(TA)
COMMON/ZZZ15/VSPAN, XLEZV, XTEZV, TANLEV, TANFEV, TAU, ZVTAIL
COMMON/ZZZ16/MKAPY, MKAB, MKASK, MKAKB
COMMON/ZZZ17/MKLPY, MKHB, MKLSK, MKLBL
COMMON/ZZZ18/MANGRY, MANGAB, MANGSK, MANGB
COMMON/ZZZ19/KPRINT(10), IREAD, NWRITE, KREAD
COMMON/ZZZ20/PT
COMMON/ZZZ21/KPY1, KPY2
COMMON/ZZZ22/KSELE, KMS4P, KMSY2
COMMON/ZZZ23/KBDELE, KBDS4P, KBOTY2
COMMON/ZZZ24/KTMELE, KMS4P, KMTY2
COMMON/ZZZ25/KPYELE, KPS4P, KPYTY2
COMMON/ZZZ26/KVTELE, KVS4P, KVTY2
COMMON/ZZZ27/KSHELE, KMS4P, KSHTY2
COMMON/ZZZ28/KHBELE, KMS4P, KMHTY2
COMMON/ZZZ29/KSKELE, KKS4P, KSKTY2
COMMON/ZZZ30/KBLELE, KBL4P, KBLTY2
COMMON/ZZZ31/NSTAG, NVOR, NSPIRAL, SPIRAL
DIMENSION AA(NESQ), SOURCE(NLEEM)
REAL LSHAFT, LSHANK
C
IF(KPRINT(5).EQ.1)CALL PRINTB(NLEEM, NESQ, AA, SOURCE, 1)
IF(KPRINT(6).EQ.1)CALL PRINTB(NLEEM, NESQ, AA, SOURCE, 2)
TOL=0.001
CALL CGCELG(SOURCE, AA, NLEEM, 1, TOL, IER)
C
IF(IER.NE.0)WRITE(NWRITE, 100)IER
C
100 FORMAT('//////', I0, ' IER = ', I0, '//////')
IF(KPRINT(7).EQ.1)CALL PRINTB(NLEEM, NESQ, AA, SOURCE, 3)
RETURN
END

```



```

C
C      SUBROUTINE CGEELG(R,A,M,N,EPS,IER)
C
C
C
C      DIMENSION A(1),R(1)
C      YFIM)23,23,1
C
C      SEARCH FOR GREATEST ELEMENT IN MATRIX A
1 IER=0
  PIV=0
  MM=N*M
  MM=N*M
  DO 3 L=1,MM
    Y88=ABS(A(L))
    IF(Y88-PIV)3,3,2
  2 PIV=Y88
  3 CONTINUE
  TOL=EPS*PIV
  A(I) IS PIVOT ELEMENT. PIV CONTAINS THE ABSOLUTE VALUE OF A(I).
C
C
C      START ELIMINATION LOOP
  LST=1
  DO 17 K=1,M
C
C      TEST ON SINGULARITY
  IER)M)23,23,A
  4 IF(IER)7,5,7
  5 IF(PIV-TOL)6,6,7
  6 IER=K-1
  7 PIV=1./A(I)
  J=(I-1)/M
  I=I-1
  J=J+1-K
  I+K IS ROW-INDEX, J+K C LUNN-INDEX OF PIVOT ELEMENT
C
C      PIVOT ROW REDUCTION AND ROW INTERCHANGE IN RIGHT HAND SIDE R
  DO 8 L=K,MM,N
    LL=L+1
    TB=PIV*R(LL)
    R(LL)=R(L)
  8 R(L)=TB
C
C      IS ELIMINATION TERMINATED?
  IER)M)19,18,18
C
C      COLUMN INTERCHANGE IN MATRIX A
  9 LEND=LST+M-K
  I)12,12,18
  10 II=J*M
  DO 11 L=LST,LEND
    TB=A(L)
    LL=L+1
    A(L)=A(LL)
  11

```

```

11 A(LL)=TB
C
C ROW INTERCHANGE AND PIVOT ROW REDUCTION IN MATRIX A
12 DO 13 L=LST,MM,M
LL=L+1
TB=PIVIAA(LL)
A(LL)=A(L)
13 A(L)=TB
C
C SAVE COLUMN INTERCHANGE INFORMATION
A(LST)=J
C
C ELEMENT REDUCTION AND NEXT PIVOT SEARCH
PIV=0
LST=LST+1
J=0
DO 16 II=LST,LEND
PIV=A(II)
IST=II+M
14 IS=1
DO 15 L=IST,MM,M
LL=L+1
A(L)=A(L)+PIV*A(LL)
TB=A(LL)
IF(TBB-PIV)15,15,1+
15 PIV=TB
I=L
15 CONTINUE
DO 16 L=K,MM,M
LL=L+1
16 R(LL)=R(LL)+PIV*R(L)
17 LST=LST+M
C
C END OF ELIMINATION LOOP
C
C
C BACK SUBSTITUTION AND BACK INTERCHANGE
18 IF(M-1)23,22,19
19 I=MM+1
LST=M+1
DO 21 I=2,M
II=LST-I
IST=IST-LST
L=IST-M
1+ALL)+.5
DO 21 J=II,MM,M
TB=R(J)
LL=J
DO 20 K=IST,MM,M
LL=LL+1
20 TB=TB-A(K)*R(LL)
K=J+L
R(J)=R(K)
21 R(K)=TB
22 RETURN
C
C
C ERROR RETURN
23 IER=-1
RETURN
END

```



```

DIMENSION PCJ(3)
REAL L, SMAET, L, SMANK
C
DO 100 I=1, N1, N2, N3, N4, N5, N6, N7, N8, N9, N10, N11, N12, N13, N14, N15, N16, N17, N18, N19, N20, N21, N22, N23, N24, N25, N26, N27, N28, N29, N30, N31, N32, N33, N34, N35, N36, N37, N38, N39, N40, N41, N42, N43, N44, N45, N46, N47, N48, N49, N50, N51, N52, N53, N54, N55, N56, N57, N58, N59, N60, N61, N62, N63, N64, N65, N66, N67, N68, N69, N70, N71, N72, N73, N74, N75, N76, N77, N78, N79, N80, N81, N82, N83, N84, N85, N86, N87, N88, N89, N90, N91, N92, N93, N94, N95, N96, N97, N98, N99, N100
C
DO 100 I=1, N1, N2, N3, N4, N5, N6, N7, N8, N9, N10, N11, N12, N13, N14, N15, N16, N17, N18, N19, N20, N21, N22, N23, N24, N25, N26, N27, N28, N29, N30, N31, N32, N33, N34, N35, N36, N37, N38, N39, N40, N41, N42, N43, N44, N45, N46, N47, N48, N49, N50, N51, N52, N53, N54, N55, N56, N57, N58, N59, N60, N61, N62, N63, N64, N65, N66, N67, N68, N69, N70, N71, N72, N73, N74, N75, N76, N77, N78, N79, N80, N81, N82, N83, N84, N85, N86, N87, N88, N89, N90, N91, N92, N93, N94, N95, N96, N97, N98, N99, N100
C
IF (UMACH .GT. 1) CALL DEBIG (A00)
BETA=SQRT(1.-UMACH**2)
C
C
C
C
SIGMPT(1)=1.0
C
CONST=48.5/3.14159
C
C
KOUNT=0
DO 100 I=1, NELEM
C
KSPIRAL=1
LSPIRAL=1
IF (ICHECK .EQ. 4) KSPIRAL=SPIRAL
IF (ICHECK .EQ. 4) LSPIRAL=NSPIRAL
DO 100 ISD=1, KSPIRAL
DO 100 NSP=1, LSPIRAL
C
GO TO (100, 200, 300, 400), ICHECK
C
100 CONTINUE
C
DO 94 K=1, 3
YPP(K)=XK(K, NODE(1, J))
YPM(K)=XK(K, NODE(2, J))
YMP(K)=XK(K, NODE(3, J))
YMM(K)=XK(K, NODE(4, J))
PCJ(K)=PC(K, J)
34 CONTINUE
GO TO 500
200 CONTINUE
NSTAG=1
IF (KOUNT .EQ. 1) RETURN
READ (NREAD, 201) (YPP(K), K=1, 3)
WRITE (NWRITE, 202) (YPP(K), K=1, 3)
READ (NREAD, 201) (YPM(K), K=1, 3)
WRITE (NWRITE, 202) (YPM(K), K=1, 3)
READ (NREAD, 201) (YMP(K), K=1, 3)
WRITE (NWRITE, 202) (YMP(K), K=1, 3)
READ (NREAD, 201) (YMM(K), K=1, 3)
WRITE (NWRITE, 202) (YMM(K), K=1, 3)
DO 205 K=1, 3
205 PCJ(K)=(YPP(K)+YPM(K)+YMP(K)+YMM(K))/4.

```



```

KOUNT=1
GO TO 500
300 CONTINUE
C
NWRITE=1
IF (KOUNT.EQ.1) RETURN
READ(NREAD,201) (YBP(K),K=1,3)
WRITE(NWRITE,202) (YPP(K),K=1,3)
READ(NREAD,201) (YPM(K),K=1,3)
WRITE(NWRITE,202) (YPM(K),K=1,3)
READ(NREAD,201) (YMR(K),K=1,3)
WRITE(NWRITE,202) (YMR(K),K=1,3)
READ(NREAD,201) (YMH(K),K=1,3)
WRITE(NWRITE,202) (YMH(K),K=1,3)
DO 305 K=1,3
305 PCJ(K)=(YPP(K)+YPM(K)+YMR(K)+YMH(K))/4.
KOUNT=1
201 FORMAT(10F8.3)
202 FORMAT(1X,10F8.3)
GO TO 500
400 CONTINUE
C
NSPIRAL=1
IF (KMAKE(J).EQ.0) GO TO 100
IF (KROTOR(J).EQ.0) GO TO 100
DO 400 K=1,3
YPP(K)=XK(K,NODE(1,J))
YPM(K)=XK(K,NODE(2,J))
YMR(K)=XK(K,NODE(3,J))
YMH(K)=XK(K,NODE(4,J))
400 CONTINUE
C
RATIO=UMAKE/JMEGA
RATIO=RATIO*50./(2.*PI)
RATIO=-1.*RATIO
FACTOR=2.*PI/NSPIRAL
DO 100 ISP=1,ISPIRAL
DO 100 NSP=1,NSPIRAL
IMAKE=NSP+(ISP-1)*NSPIRAL
C
THETA1=(IMAKE-1)*FACTOR
THETA2=IMAKE*FACTOR
C
SIN1=SIN(THETA1)
COS1=COS(THETA1)
C
SIN2=SIN(THETA2)
COS2=COS(THETA2)
C
YBP2=YBP(1)*COS2+YBP(2)*SIN2
YPP2=-YPP(1)*SIN2+YPP(2)*COS2
C
XMP1=YPP(1)*COS1+YPP(2)*SIN1
YMR1=YBP(1)*SIN1+YBP(2)*COS1
C
YMH1=YPM(1)*COS1+YPM(2)*SIN1
YMH1=-YPM(1)*SIN1+YPM(2)*COS1
C
XPH2=YPM(1)*COS2+YPM(2)*SIN2

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YPM2=-YPM(1)*SIN2+YPM(2)*COS2
C
RPP2=SQRT(XPP2*XPP2+YPP2*YPP2)
RMP1=SQRT(XMP1*XMP1+YMP1*YMP1)
RHM1=SQRT(XHM1*XHM1+YHM1*YHM1)
RPM2=SQRT(XPM2*XPM2+YPM2*YPM2)
C
IF(NSP-CT,1) GO TO 503
C
ZP=0.0
ZPP2=ZP+RATIO*THETA2*RP2/RROTOR
ZMP1=ZP+RATIO*THETA1*RM1/RROTOR
ZHM1=ZP+RATIO*THETA1*RHM1/RROTOR
ZPM2=ZP+RATIO*THETA2*RP2/RROTOR
GO TO 504
503 CONTINUE
ZPP2=ZP+RATIO*(THETA2-FACTOR)+RATIO*FACTOR*RP2/RROTOR
ZMP1=ZP+RATIO*(THETA1-FACTOR)+RATIO*FACTOR*RM1/RROTOR
ZHM1=ZP+RATIO*(THETA1-FACTOR)+RATIO*FACTOR*RHM1/RROTOR
ZPM2=ZP+RATIO*(THETA2-FACTOR)+RATIO*FACTOR*RP2/RROTOR
504 CONTINUE
C
YPP(1)=XPP2
YPP(2)=YPP2
YPP(3)=ZPP2
C
YPM(1)=XPM2
YPM(2)=YPM2
YPM(3)=ZPM2
C
YMP(1)=XMP1
YMP(2)=YMP1
YMP(3)=ZMP1
C
YHM(1)=XHM1
YHM(2)=YHM1
YHM(3)=ZHM1
C
IF(ZPP2.LT.(ZBD1+RZBD1+ZPYL))GO TO 100
IF(ZPM2.LT.(ZBD1+RZBD1+ZPYL)) GO TO 100
C
DO 505 K=1,3
505 PCJ(K)=(YPP(K)+YPM(K)+YMP(K)+YHM(K))/4.
C
500 CONTINUE
C
DO 1002 K=1,3
AA1(K,1)=0.5*(YPP(K)-YMP(K))
AA1(K,2)=0.5*(YPM(K)-YHM(K))
AA2(K,1)=0.5*(YPP(K)-YPM(K))
AA2(K,2)=0.5*(YMP(K)-YHM(K))
A1(K,1)=AA1(K,1)
A1(K,2)=AA1(K,2)
A2(K,1)=AA2(K,1)
A2(K,2)=AA2(K,2)
1002 CONTINUE

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```

DO 1003 L=1,2
A1A1(L)=DOTPRD(A1(1,L),A1(2,L),A1(3,L),A1(1,L),A1(2,L),A1(3,L))
1003 A2A2(L)=DOTPRD(A2(1,L),A2(2,L),A2(3,L),A2(1,L),A2(2,L),A2(3,L))
C
DO 1004 K=1,3
IF(A1A1(1).EQ.0.)A1(K,0)=A1(K,2)
IF(A1A1(2).EQ.0.)A1(K,0)=A1(K,1)
IF(A2A2(1).EQ.0.)A2(K,1)=A2(K,2)
IF(A2A2(2).EQ.0.)A2(K,0)=A2(K,1)
1004 CONTINUE
C
DO 1005 L=1,2
A1A1(L)=DOTPRD(A1(1,L),A1(2,L),A1(3,L),A1(1,L),A1(2,L),A1(3,L))
1005 A2A2(L)=DOTPRD(A2(1,L),A2(2,L),A2(3,L),A2(1,L),A2(2,L),A2(3,L))
C
DO 1007 L=1,2
DO 1007 M=1,2
1007 A1A2(L,M)=DOTPRD(A1(1,L),A1(2,L),A1(3,L),A2(1,M),A2(2,M),A2(3,M))
C
A1CRA2(1)=SQRT(A1A1(2)*A2A2(1)-A1A2(2,1)**2)
A1CRA2(2)=SQRT(A1A1(1)*A2A2(1)-A1A2(1,1)**2)
A1CRA2(3)=SQRT(A1A1(1)*A2A2(2)-A1A2(1,2)**2)
A1CRA2(4)=SQRT(A1A1(2)*A2A2(2)-A1A2(2,2)**2)
C
DO 1008 K=1,3
AVA1(K)=0.5*(A1(K,1)+A1(K,2))
1008 AVA2(K)=0.5*(A2(K,1)+A2(K,2))
C
YNORM(1)=AVA1(2)*AVA2(3)-AVA1(3)*AVA2(2)
YNORM(2)=AVA1(3)*AVA2(1)-AVA1(1)*AVA2(3)
YNORM(3)=AVA1(1)*AVA2(2)-AVA1(2)*AVA2(1)
C
SN(1)=YNORM(1)/BETA
SN(2)=YNORM(2)
SN(3)=YNORM(3)
ASN=SQRT(SN(1)**2+SN(2)**2+SN(3)**2)
AYN=SQRT(YNORM(1)**2+YNORM(2)**2+YNORM(3)**2)
DO 1010 K=1,3
UN(K)=YNORM(K)/AYN
SNUM(K)=SN(K)/ASN
1010 CONTINUE
C
DO 178 I=1,NELEM
C
DO 168 ISYMHV=1,NSYMHV
DO 168 ISYHMZ=1,NSYHMZ
SIGNPT(2)=3.-2*ISYMHV
SIGNPT(3)=3.-2*ISYHMZ
C
DO 1102 K=1,3
1102 PZ(K)=PC(K)-PC(K,I)*SIGNPT(K)
QDOTUN=DOTPRD(UN(1),UN(2),UN(3),PZ(1),PZ(2),PZ(3))
C
DO 1110 K=1,3
Q(K,1)=YBN(K)-PC(K,I)*SIGNPT(K)
Q(K,2)=YPP(K)-PC(K,I)*SIGNPT(K)

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Q(K,3)=YMP(K)-PC(K,1)*SI GMPT(K)
Q(K,4)=YHM(K)-PC(K,1)*SI GMPT(K)
1110 CONTINUE
DO 1111 K=1,3
Q(K,1)=0.5*(Q(K,1)+Q(K,2))
Q(K,2)=0.5*(Q(K,2)+Q(K,3))
Q(K,3)=0.5*(Q(K,3)+Q(K,4))
Q(K,4)=0.5*(Q(K,4)+Q(K,1))
1111 CONTINUE
C
DO 1112 K=1,3
KP1=K+1
KP2=K+2
IF (KP1.GT.3) KP1=KP1-3
IF (KP2.GT.3) KP2=KP2-3
QMCRA1(K,1)=QM(KP1,2)*A1(KP2,1)-QM(KP2,2)*A1(KP1,1)
QMCRA1(K,2)=QM(KP1,4)*A1(KP2,2)-QM(KP2,4)*A1(KP1,2)
QMCRA2(K,1)=QM(KP1,1)*A2(KP2,1)-QM(KP2,1)*A2(KP1,1)
QMCRA2(K,2)=QM(KP1,3)*A2(KP2,2)-QM(KP2,3)*A2(KP1,2)
1112 CONTINUE
C
RC=SQRT(DOTPR0(PZ(1),PZ(2),PZ(3),PZ(1),PZ(2),PZ(3)))
C
DO 155 ICORN2=1,4
GO TO (5502,5504,5506,5508),ICORN2
5502 CONTINUE
SIGN12=-1.
ICSI=1
IETA=2
GO TO 5510
5504 CONTINUE
SIGN12=+1.
ICSI=1
IETA=1
GO TO 5510
5506 CONTINUE
SIGN12=-1.
ICSI=2
IETA=1
GO TO 5510
5508 CONTINUE
SIGN12=+1.
ICSI=2
IETA=2
5510 CONTINUE
C
DO 5520 K=1,3
QV(K)=Q(K,ICORN2)
A1V(K)=A1(K,IETA)
A2V(K)=A2(K,ICSI)
QCRA1(K)=QMCRA1(K,IETA)
QCRA2(K)=QMCRA2(K,ICSI)
5520 CONTINUE
C
QQ=SQRT(DOTPR0(QV(1),QV(2),QV(3),QV(1),QV(2),QV(3)))
C
CALL LOG(ICORN2,QQ,QV,A1V,QCRA1,ALOG1,1)

```



```

C
CALL LOG1(CORN2,QQ,QV,A*Y,QCRA2,ALOG2,2)
C
TANP=8.
IF(QDOTUN.EQ.0.)GO TO 530
HNUMER=DOTPR2(QCRA1(1),QCRA1(2),QCRA1(3),QCRA2(1),QCRA2(2),
1 QCRA2(3))
DENOM=QQ*QDOTUN*A1CRA2(I)*QNR1
IF(DENOM.NE.0.)TANP=ATANP(HNUMER,DENOM)
550 CONTINUE
C
COEFF1=DOTPR1(UN(1),UN(2),UN(3),QCRA1(1),QCRA1(2),QCRA1(3))
COEFF2=DOTPR2(UN(1),UN(2),UN(3),QCRA2(1),QCRA2(2),QCRA2(3))
C
SRCINT=-CONST*SIGN12*
1 (=COEFF1*ALOG1+COEFF2*ALOG2-QDOTUN*TANP)
C
GO TO (801,802,803,804),ICHECK
801 CONC=1.0
GO TO 850
802 CONC=CSTAG
GO TO 850
803 CONC=CVORT
GO TO 850
804 CONC=1.0
850 CONTINUE
DBTINT=-CONST*SIGN12*TA,P*CONC
-
SGNINT=1.
C
NNN=I+(J-1)*NELEM
C
AA(NNN)=AA(NNN)-SGNINT*JBTINT
C
C
IF(ICHECK.NE.1)GO TO 600
UFREE=UNACH*1117.
OMEGAX=8.
OMEGAY=0.
OMEGAZ=OMEGA*2.*PI/60.
RX=PC(1,J)
RY=PC(2,J)
RZ=PC(3,J)
BCX=XPROJ(OMEGAX,OMEGAY,OMEGAZ,RX,RY,RZ)
BCY=YPROJ(OMEGAX,OMEGAY,OMEGAZ,RX,RY,RZ)
BCZ=ZPROJ(OMEGAX,OMEGAY,OMEGAZ,RX,RY,RZ)
BCR=DOTPRO(BCX,BCY,BCZ,JN(1),UN(2),UN(3))
IF(KROTOR(J).EQ.0)BCR=
BCB=-1.*UFREE*UN(1)
BC(J)=BCB+BCR
SOURCE(I)=SOURCE(I)+SGNINT*SRCINT* BC(J)
600 CONTINUE
C
150 CONTINUE
155 CONTINUE
160 CONTINUE

```

170 CONTINUE
180 CONTINUE
C
C
RETURN
END

```

C
C
SUBROUTINE L3G(ICORNR,Q,QV,AV,QCRAV,ALOG,ICORR)
DIMENSION QV(3)
DIMENSION AV(3),QCRAV(3)
C
DOTPRO(X1,Y1,Z1,X2,Y2,Z2)=X1*X2+Y1*Y2+Z1*Z2
C
AVAV=DOTPRO(AV(1),AV(2),AV(3),AV(1),AV(2),AV(3))
QQAV=DOTPRO(QV(1),QV(2),QV(3),AV(1),AV(2),AV(3))
QXA=SQRT(DOTPRO(QCRAV(1),QCRAV(2),QCRAV(3),
                QCRAV(1),QCRAV(2),QCRAV(3)))
ALOG=ASINH(QQAV/QXA)/SQRT(AVAV)
RETURN
END

```

PC

```
FUNCTION ATANP (NUMER, DENOM)  
ADENOM=ABS (DENOM)  
ATANP=ATAN2 (NUMER, ADENOM)  
IF (DENOM < 0.) ATANP=ATANP  
RETURN  
END
```


C
C

```
SUBROUTINE AVERAG(SOURCE, SOR, PC, NELEM, NODE, NOFCT, NKYMF, NNODE,  
1, AVG)  
DIMENSION SOURCE(NELEM), SOR(NNODE), AVG(NNODE), PC(3, NELEM)  
DIMENSION NODE(4, NELEM), NOFCT(NKYM, 3)  
COMMON/ZZZ1/NX(34), NY(34), NXY(34), KSYMMY, KSYMMZ, NSYMMY, NSYMMZ  
COMMON/ZZZ2/NSFX, NSBODY, NS, NT(34), TSPACE(34), KNORM(34), KNAKES(34)  
COMMON/ZZZ3/NPYLON, NBODY1, NBODY2, NBODY3, NVTAIL, NSHAFT, NNUB, NSHANK,  
1, NBLADE  
COMMON/ZZZ4/OMEGA, ALFA, ABETA  
COMMON/ZZZ5/YRYCTR, YRYCZ, ZRYCTR, ZRYL, ZRYL, ZRYL, ZRYL  
COMMON/ZZZ6/XNOSE, XBD1, XBD2, XTAIL  
COMMON/ZZZ7/YNOSE, YBD1, YBD2, YTAIL  
COMMON/ZZZ8/ZNOSE, ZBD1, ZBD2, ZTAIL  
COMMON/ZZZ9/RVBD1, RVBD1, RVBD2, RVBD2  
COMMON/ZZZ10/RSHAFT, LSHAFT, RSHANK, LSHANK  
COMMON/ZZZ11/XHUBC1, XHUBC2, ZHUBC1, ZHUBC2, RYHUB, RYHUB, RZHUB  
COMMON/ZZZ12/RROTOR, BCHORD, TAUBL, ALFA  
COMMON/ZZZ13/TMETZ, TMETC, TMETIS, CONING, AZIMUTH  
COMMON/ZZZ14/KBLADE, TAMB, TANTEB, XBLE, XBTE, KROTORS(34)  
COMMON/ZZZ15/NSRAN, XLEZ, XTEZ, TANLEV, TANTEV, TAU, ZNTAIL  
COMMON/ZZZ16/HNAKPY, HNAK1B, HNAKSK, HNAKBL  
COMMON/ZZZ17/HAKLBY, HAK1B, HAKLSK, HAKLB  
COMMON/ZZZ18/HANGPY, HAN1B, HANGSK, HANGBL  
COMMON/ZZZ19/KPRINT(10), VREAD, NWRITE, KREAD  
COMMON/ZZZ20/PI  
COMMON/ZZZ21/KPY1, KPY2  
COMMON/ZZZ22/KNSELE, KNST1P, KNSTYP  
COMMON/ZZZ23/KQDELE, KQDS1B, KQDTP  
COMMON/ZZZ24/KTNELE, KTNS1P, KTNTYP  
COMMON/ZZZ25/KPYELE, KPYSP, KPYTYP  
COMMON/ZZZ26/KVTELE, KVTS1P, KVTTYP  
COMMON/ZZZ27/KSMELE, KSM1B, KSMTP  
COMMON/ZZZ28/KHBELE, KHBS1P, KHBTYP  
COMMON/ZZZ29/KSKELE, KSK1B, KSKTYP  
COMMON/ZZZ30/KBLELE, KBL1P, KBLTYP  
COMMON/ZZZ31/HSTAG, HWORD, MSPTRAL, SPTRAL  
INTEGER PH, PP  
REAL LSHAFT, LSHANK
```

C

```
DO 98 I=NODE+1, NNODE  
AVG(I, NODE) = 0.  
SOR(I, NODE) = 0.  
98  
DO 100 IELEM=1, NELEM  
PP=NODE(1, IELEM)  
PH=NODE(2, IELEM)  
NB=NODE(3, IELEM)  
HM=NODE(4, IELEM)  
SOR(PP) = SOR(PP) + SOURCE(IELEM)  
SOR(PH) = SOR(PH) + SOURCE(IELEM)  
SOR(NB) = SOR(NB) + SOURCE(IELEM)  
SOR(HM) = SOR(HM) + SOURCE(IELEM)  
AVG(PP) = AVG(PP) + 1.  
AVG(PH) = AVG(PH) + 1.  
AVG(NB) = AVG(NB) + 1.  
AVG(HM) = AVG(HM) + 1.
```

```
100 CONTINUE  
DO 110 INODE=1,NNODE  
110 SOR(INODE)=SOR(INODE)/AVG(INODE)  
100 CONTINUE  
SOR(1)=0.0  
SOR(2)=0.0  
RETURN  
END
```

C

```

SUBROUTINE PH1(SOR,NNODE,MODE,PHIC,PH1,PHI2,NELEM)
DIMENSION SOR(NNODE),PHIC(NELEM),PH1(NELEM),PHI2(NELEM)
DIMENSION PH1Y(NELEM)
DIMENSION NODE(4,NELEM)
COMMON/ZZZ1/NX(34),NY(34),NZ(34),KSYMMY,KSYMMZ,NSYMMY,NSYMMZ
COMMON/ZZZ2/NSFX,NSBODY,YS,NT(34),ISFACE(34),KNORML(34),KNAKES(34)
COMMON/ZZZ3/NBYLON,NBODY1,NBODY2,NBODY3,NBTAIL,NSHAFT,NHUB,NSHANK
1 NBLADE
COMMON/ZZZ4/OMEGA,ALFA,ABETA
COMMON/ZZZ5/XPYCTR,YPYCTR,ZPYCTR,XPYVL,RPYVL,RZPYL
COMMON/ZZZ6/XNOSE,YB01,ZB02,XTAIL
COMMON/ZZZ7/YNOSE,YB01,ZB02,XTAIL
COMMON/ZZZ8/ZNOSE,ZB01,ZB02,ZTAIL
COMMON/ZZZ9/RB01,RZB01,RB02,RZB02
COMMON/ZZZ10/RSHAFT,LSHAFT,RSHANK,LSHANK
COMMON/ZZZ11/XHUBCR,YHUBCR,ZHUBCR,RXHUB,RXHUB3,RZHU3
COMMON/ZZZ12/RROT03,RCM3D,TAU03,ALFA3
COMMON/ZZZ13/TMET5,THE1C,THE1S,CONING,AZIMUTH
COMMON/ZZZ14/KBLADE,TAN3B,TAN3E,XBL3,Y3TE,KROTORS(34)
COMMON/ZZZ15/VSPAN,XLEZV,XTEZV,TANLEV,TANTEV,TAU,ZVTAIL
COMMON/ZZZ16/NNAKRY,NNAK4B,NNAKSK,NNAKBL
COMMON/ZZZ17/WAKLPY,WAK4B,WAKLSK,WAKLBL
COMMON/ZZZ18/WANGRY,WAN4B,WANGSK,WANGBL
COMMON/ZZZ19/KPRINT(10),VREAD,NWRITE,KREAD
COMMON/ZZZ20/RT
COMMON/ZZZ21/KPY1,KPY2
COMMON/ZZZ22/KNSLE1,KNS4B,KNSTY2
COMMON/ZZZ23/KBDELE,KNS4P,KB0TY2
COMMON/ZZZ24/KKNELE,KNS4B,KNTTY2
COMMON/ZZZ25/KPYELE,KPY4P,KPYTY2
COMMON/ZZZ26/KKTELE,KNS4B,KNTTY2
COMMON/ZZZ27/KSHELE,KNS4P,KSHTY2
COMMON/ZZZ28/KKBELE,KNS4B,KMBTY2
COMMON/ZZZ29/KSKELE,KSK4P,KSKTY2
COMMON/ZZZ30/KBLELE,KBL4B,KBLTY2
COMMON/ZZZ31/NSTAG,NVORT,NSPIRAL,SPIRAL
INTEGER RM,R2
REAL LSHAFT,LSHANK
DO 701 IELEM=1,NELEM
PP=NODE(1,IELEM)
RM=NODE(2,IELEM)
NP=NODE(3,IELEM)
NN=NODE(4,IELEM)
PHIC(IELEM)=(SOR(PP)+SO2(PN)+SOR(NP)+SOR(NN))/4.
PH1(IELEM)=(SOR(PP)+SOR(RM)+SOR(NP)+SOR(NN))/4.
PHI2(IELEM)=(SOR(PP)-SO2(PN)+SOR(NP)-SOR(NN))/4.
PH1Y(IELEM)=(SOR(PP)-SOR(RM)+SOR(NP)+SOR(NN))/4.
701 CONTINUE
WRITE(6,719)
719 FORMAT(//6X,'ELEM',9X,'PHIC',11X,
10BM1,9X,2BM12,9X,2BM13)
DO 720 IELEM=1,NELEM
720 WRITE(6,721)IELEM,PHIC(IELEM),PH1(IELEM),PHI2(IELEM),PH1Y(IELEM)
721 FORMAT(5X,I6,9X,6E15.5)
RETURN
END

```

```

C
SUBROUTINE VELXYZ(VELX,VELY,VELZ,PHI1,PHI2,PHI3,PC,P1,P2,P3,
1 NELEM)
DIMENSION VELX(NELEM),PHI1(NELEM),PHI2(NELEM)
DIMENSION PHI(3(NELEM))
DIMENSION VEY(NELEM),VZ(NELEM)
DIMENSION PC(3,NELEM),P1(3,NELEM),P2(3,NELEM),P3(3,NELEM)
COMMON/ZZZ1/XX(3),YY(3),ZZ(3),KSYMMY,KSYMMZ,NSYMMY,NSYMMZ
COMMON/ZZZ2/NSFX,NSBODY,VS,NT(3),ISFACE(3),KNORHL(3),KNAKES(3)
COMMON/ZZZ3/RYLON,NBODY1,NBODY2,NBODY3,NVTAIL,NSHAFT,NHUB,NSHANK,
1 NBLADE
COMMON/ZZZ4/OMEGA,ALFA,ABETA
COMMON/ZZZ5/XPYCTR,YPYCTR,ZPYCTR,RXPVL,RYPYL,RZPYL
COMMON/ZZZ6/XNOSE,YBD1,ZBD2,YTAIL
COMMON/ZZZ7/YNOSE,YBD1,ZBD2,YTAIL
COMMON/ZZZ8/ZNOSE,ZBD1,ZBD2,ZTAIL
COMMON/ZZZ9/RYBD1,RZBD1,RYBD2,RZBD2
COMMON/ZZZ10/RSHAFT,LSHAFT,RSHANK,LSHANK
COMMON/ZZZ11/XHUBCR,YHUBCR,ZHUBCR,RXHUB,RYHUB,RZHUB
COMMON/ZZZ12/PROTOR,BCMD,TAUBL,ALFA
COMMON/ZZZ13/THET75,THET1C,THET1S,COS,NG,AZIMUTH
COMMON/ZZZ14/KBLADE,TAN,EB,TANTEB,KBLE,XRTE,KROTORS(3)
COMMON/ZZZ15/VSPAN,XLEZV,XTEZV,TANLEV,TANTEV,TAU,ZVTAIL
COMMON/ZZZ16/NMAKRY,NMAC,NS,NMAKSK,NMAKBL
COMMON/ZZZ17/WAKLRY,WAK,NS,WAKLSK,WAKLBL
COMMON/ZZZ18/WANGRY,WAN,NS,WANGSK,WANGBL
COMMON/ZZZ19/KPRINT(10),VREAD,NWRITE,KREAD
COMMON/ZZZ20/PI
COMMON/ZZZ21/KPY1,KPY2
COMMON/ZZZ22/KNSLE,KNS,KB,KNSTYB
COMMON/ZZZ23/KBDELE,KBS,KB,KBOTYP
COMMON/ZZZ24/KTNELE,KTR,KB,KTNTYP
COMMON/ZZZ25/KPYELE,KPY,KB,KPYTYP
COMMON/ZZZ26/KVTELE,KVT,KB,KVTYP
COMMON/ZZZ27/KSHELE,KSH,KB,KSHTYP
COMMON/ZZZ28/KMBELE,KMB,KB,KMBTYP
COMMON/ZZZ29/KSKELE,KSK,KB,KSKTYP
COMMON/ZZZ30/KBLELE,KBL,KB,KBLTYP
COMMON/ZZZ31/NSTAG,NVORT,NSPIRAL,SPIRAL

C
DOTPRO(X1,X2,X3,Y1,Y2,Y3)=X1*Y1+X2*Y2+X3*Y3
VECPRX(D1,D2,D3,E1,E2,E3)=D1*E1+D2*E2+D3*E3
VECPRY(D1,D2,D3,E1,E2,E3)=D3*E1-D1*E3
VECPRZ(D1,D2,D3,E1,E2,E3)=D1*E2-D2*E1

C
DO 888 JELEM=1,NELEM

C
A1XC=P1(1,JELEM)
A1YC=P1(2,JELEM)
A1ZC=P1(3,JELEM)
A2XC=P2(1,JELEM)
A2YC=P2(2,JELEM)
A2ZC=P2(3,JELEM)

A1XA2X=VECPRX(A1XC,A1YC,A1ZC,A2XC,A2YC,A2ZC)
A1XA2Y=VECPRY(A1XC,A1YC,A1ZC,A2XC,A2YC,A2ZC)
A1XA2Z=VECPRZ(A1XC,A1YC,A1ZC,A2XC,A2YC,A2ZC)

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C      A1XA2S=DOTPRO(A1XA2Y,A1XA2Y,A1XA2Z,A1XA2Y,A1XA2Y,A1XA2Z)
      A1XA2A=SQRT(A1XA2S)
C      A1A1=DOTPRO(A1XC,A1YC,A1ZC,A1XC,A1YC,A1ZC)
      A1A2=DOTPRO(A1XC,A1YC,A1ZC,A2XC,A2YC,A2ZC)
      A2A2=DOTPRO(A2XC,A2YC,A2ZC,A2XC,A2YC,A2ZC)
C      A11=A2A2/A1XA2S
      A12=A1A2/A1XA2S
      A21=A12
      A22=A1A1/A1XA1S
C      UNORMX=A1XA2Y/A1XA2A
      UNORMY=A1XA2Y/A1XA2A
      UNORMZ=A1XA2Z/A1XA2A
C      A1XU=A11*A1YC+A12*A2XC
      A1YU=A11*A1YC+A12*A2YC
      A1ZU=A11*A1ZC+A12*A2ZC
C      A2XU=A21*A1YC+A22*A2XC
      A2YU=A21*A1YC+A22*A2YC
      A2ZU=A21*A1ZC+A22*A2ZC
C      A3XU=UNORMX
      A3YU=UNORMY
      A3ZU=UNORMZ
C      VEL Y (JELEM)=PHI1(JELEM)*A1YU+PHI2(JELEM)*A2YU
      VEL Z (JELEM)=PHI1(JELEM)*A1ZU+PHI2(JELEM)*A2ZU+PHI3(JELEM)*A3ZU
800  CONTINUE
      RETURN
      END

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SUBROUTINE CPLINR(CP,VE,X,VELY,VELZ,PHIC,NELEM,PC,KROTOR)
DIMENSION CP(NELEM),VELX(NELEM),PHIC(NELEM)
DIMENSION VE,Y(NELEM),VE,Z(NELEM)
DIMENSION PC(3,NELEM),KROTOR(NELEM)
COMMON/ZZZ1/NX(34),NY(34),NXY(34),KSYM1,KSYM2,NSYMMY,NSYMMZ
COMMON/ZZZ2/NSEY,NSBODY,NS,NT(34),ISEACE(34),KNORM(34),KNAKES(34)
COMMON/ZZZ3/NPYLON,NBODY1,NBODY2,NBODY3,NVTAIL,NSHAFT,NHUB,NSHANK,
1 NBLADE
COMMON/ZZZ4/JMACH,OMEGA,ALFA,ABETA
COMMON/ZZZ5/XPYCTR,YPYCTR,ZPYCTR,XPYV1,YPYV1,ZPYV1
COMMON/ZZZ6/KNOSE,XB01,ZB02,XTAIL
COMMON/ZZZ7/XNOSE,YB01,ZB02,YTAIL
COMMON/ZZZ8/ZNOSE,ZB01,ZB02,ZTAIL
COMMON/ZZZ9/RX01,RZ01,ZY02,RZ02
COMMON/ZZZ10/RSHAFT,LSM,T,RSMANK,LSHANK
COMMON/ZZZ11/XHUBC2,ZHUBC2,ZHUBC2,RXMUB,ZYMUB,ZZHUB3
COMMON/ZZZ12/RROTOR,BCHORD,TAUBL,ALFA9
COMMON/ZZZ13/TMETZS,TMETLC,TMETLS,COMING,AZMUTH
COMMON/ZZZ14/KBLADE,TAN.EB,TANTE3,XBLE,XBTE,KROTORS(34)
COMMON/ZZZ15/NSPAN,XL,ZL,YTEZV,TAN.EV,TANTEV,TAU,ZVTAIL
COMMON/ZZZ16/NHAKPY,NHAK1B,NHAKSK,NHAKBL
COMMON/ZZZ17/HAKPY,HAK1B,HAKLSK,HAKLBL
COMMON/ZZZ18/WANGPY,WAN1B,WANGSK,WANGBL
COMMON/ZZZ19/KROTOR(10),KREAD,NWRITE,KREAD
COMMON/ZZZ20/PI
COMMON/ZZZ21/KPY1,KPY2
COMMON/ZZZ22/KNSELE,KNSS4P,KNSTYP
COMMON/ZZZ23/KBDELE,KBS4P,KBDTY2
COMMON/ZZZ24/KTNELE,KTNSHP,KTNTY2
COMMON/ZZZ25/KRYELE,KRS4P,KRYTY2
COMMON/ZZZ26/KVTELE,KVTS4P,KVTY2
COMMON/ZZZ27/KSHELE,KS4P,KSHTY2
COMMON/ZZZ28/KHBELE,KHS4P,KHBTY2
COMMON/ZZZ29/KSKELE,KS4P,KSHTY2
COMMON/ZZZ30/KBLELE,KBS4P,KBLTY2
COMMON/ZZZ31/NSIAC,NVORT,NSIRAI,SIRAI
DOTPRO(X1,Y1,Z1,X2,Y2,Z2)=X1*X2+Y1*Y2+Z1*Z2
XPROY(OX,OY,OZ,EX,EY,EZ)=OX*EY-EZ*OX
XPROZ(OX,OY,OZ,EX,EY,EZ)=OX*EY-EZ*OY
BETAZA=ABS(1.-UMACH**2)
BETA=SQRT(BETAZA)
UFREE=UMACH**1.117
OMEGAY=0.
OMEGAZ=OMEGA
OMEGAZ=OMEGAZ**2.*PI/68.
IF(UMACH.EQ.0) UFREE=OMEGA**2.*PI**KROTOR/68.
DO 900 IELEM=1,NELEM
RX=PC(1,IELEM)
RY=PC(2,IELEM)
RZ=PC(3,IELEM)
VX=VELX(IELEM)
VY=VELY(IELEM)
VZ=VELZ(IELEM)
CPB=(1.-2.*UFREE*VX-(VX*VX+VY*VY+VZ*VZ))/(UFREE*UFREE)
CPB=(-2.*UFREE*VX)/(UFREE*UFREE)

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CRX=XPROX(OMEGAX,OMEGAY,JMEGAZ,RX,RY,RZ)
CRY=XPROY(OMEGAX,OMEGAY,JMEGAZ,RX,RY,RZ)
CRZ=XPROZ(OMEGAX,OMEGAY,JMEGAZ,RX,RY,RZ)
CPR=DOTPR(CRX,CRY,CRZ,X,Y,Z)
CPR=CPR*2./(JFREE*UFREE)
IF(KROTOR/IELEM).EQ.0)C22=0.
CP(IELEM)=CPR+CPR
300 CONTINUE
RETURN
END
```

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SUBROUTINE FJRCE(NNODE,XX,NELEM,NODE,CP)
DIMENSION A1(3),A2(3),XC(3,NNODE),NODE(4,NELEM),PC(3),CP(NELEM)
COMMON/ZZZ1/XX(34),NY(34),NXY(34),KSY:MY,KSYMZ,NSYMMY,NSYMMZ
COMMON/ZZZ2/NSFY,NSBODY,YS,XT(34),ISPACE(34),KNORML(34),KNAKES(34)
COMMON/ZZZ3/VPYLN,NBODY1,NBODY2,NBODY3,NVTAIL,NSHAFT,NHUB,NSHANK,
      NBLADE
COMMON/ZZZ4/UMACH,OMEGA,ALFA,ABETA
COMMON/ZZZ5/XPYCTR,XPYCTR,ZPYCTR,XPYVL,XPYVL,RZPYL
COMMON/ZZZ6/XNOSE,XB01,X3D2,XTAIL
COMMON/ZZZ7/XNOSE,YB01,Y3D2,YTAIL
COMMON/ZZZ8/ZNOSE,ZB01,Z3D2,ZTAIL
COMMON/ZZZ9/RVBD1,ZVB01,RVB02,RVB02
COMMON/ZZZ10/RSHAFT,LSHAFT,RSHANK,LSHANK
COMMON/ZZZ11/XHUBCR,YHUBCR,ZHUBCR,XYHUB,XYHUB,RZYHUB
COMMON/ZZZ12/ROTOR,BCHRD,TAUBL,ALFA3
COMMON/ZZZ13/THET2,THET1C,THET1S,COSINC,AZTMUTH
COMMON/ZZZ14/KBLADE,TAN:EB,TANTEB,XBLE,X9TE,KROTOR(34)
COMMON/ZZZ15/VSRAV,YLEZY,YTEZY,TANLEY,TANTEN,TAU,ZNTAIL
COMMON/ZZZ16/NWAKPY,NWAK1B,NWAKSK,NWAKB
COMMON/ZZZ17/WAKPY,WAK1B,WAKSK,WAK1B
COMMON/ZZZ18/WANGPY,WANG1B,WANGSK,WANGBL
COMMON/ZZZ19/KPRINT(10),KREAD,KWRITE,KREAD
COMMON/ZZZ20/PI
COMMON/ZZZ21/KPY1,KPY2
COMMON/ZZZ22/KNSELE,KNSS1P,KNSTYP
COMMON/ZZZ23/KBLELE,KNS1P,KNTYP
COMMON/ZZZ24/KTNELE,KTNS1P,KTNTYP
COMMON/ZZZ25/KVTELE,KVTS1P,KVTTYP
COMMON/ZZZ26/KVTELE,KVTS1P,KVTTYP
COMMON/ZZZ27/KSNELE,KSNS1P,KSNTYP
COMMON/ZZZ28/KHBELE,KHBS1P,KHBTYP
COMMON/ZZZ29/KSKELE,KSNS1P,KSNTYP
COMMON/ZZZ30/K9LELE,KBL1P,K9LTYP
COMMON/ZZZ31/INSTAG,NVORT,NSPRAL,SPRAL
INTEGER PP,PH,HP,M4
C
DOTPR0(X1,Y1,Z1,X2,Y2,Z2)=X1*X2+Y1*Y2+Z1*Z2
XPROX(IX,DY,JZ,EX,EY,EZ)=DY*EZ-DZ*EY
XPROY(IX,DY,JZ,EX,EY,EZ)=DZ*EX-DX*EZ
XPROZ(IX,DY,JZ,EX,EY,EZ)=DX*EY-DY*EX
C
BETA=SQRT(1.-UMACH*UMACH)
MULT=1
MULTZ=1
IF(KSYMZ.NE.0) MULTZ=2
IF(KSYMMY.NE.0) MULT=2
CLIFT=0.0
CDRAG=0.0
CH=0.0
DO 100 J=1,NELEM
PP=NODE(1,J)
PH=NODE(2,J)
HP=NODE(3,J)
MH=NODE(4,J)
DO 200 K=1,3
YPP=XX(K,PP)
YPH=XX(K,PH)

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YMP=XK(K,MP)
YMM=XK(K,MM)
A1(K)=(YPP+YPM-YMP-YMM)/4.
A2(K)=(YRP+YRM-YMP-YMM)/4.
PC(K)=(YPP+YPM+YMP+YMM)/4.
200 CONTINUE
A1(1)=A1(1)*BETA
A2(1)=A2(1)*BETA
PC(1)=PC(1)*BETA
C
A1X2X=XPROX(A1(1),A1(2),A1(3),A2(1),A2(2),A2(3))
A1X2Y=XPROY(A1(1),A1(2),A1(3),A2(1),A2(2),A2(3))
A1X2Z=XPROZ(A1(1),A1(2),A1(3),A2(1),A2(2),A2(3))
C
DELL=A1X2Z
CLIFT=CLIFT+.5*CP(J)*DELL*MULT*MULTZ
C
DELD=A1X2Y
CDRAG=CDRAG+.5*CP(J)*DELD*MULT*MULTZ
C
100 CONTINUE
C
AREA=1.
C
CLIFT=CLIFT/AREA
CDRAG=CDRAG/AREA
C
WRITE (NWRITE,100)CLIFT
300 FORMAT (//10X,'LIFT COEFFICIENT =',E12.6)
WRITE (NWRITE,101)CDRAG
301 FORMAT (//10X,'DRAG (INDUCED) COEFFICIENT =',E12.6)
RETURN
END

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