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Results of in-situ meteorological measurements and aerosol particle size distribution samplings are also reported.

#### FOREWORD

The data contained in this report are preliminary and presented here in the interest of rapid dissemination. Further refinements in data processing may lead to minor revisions.

For detailed discussion on particular aspects of the material contained herein the following personnel may be consulted:

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Aerosol Extinction Measurements	A. Guttman, J. A. Curcio
Fourier Transform Spectroscopy	K. M. Haught, S. T. Hanley
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Basic Meteorological Data	D. H. Garcia
Aerosol Particle Spectrometry	G. L. Trusty

Dr. J. A. Dowling was Project Officer and responsible for overail coordination of this project.

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#### ABSTRACT

Atmospheric transmission measurements were carried out at Cape Canaveral Air Force Station during the spring of 1977 by means of the NkL Infrared Mobile Optical Radiation Laboratory (IMORL). Reduced data resulting from this effort are presented in this report for five laser wavelength regions (HeNe, Nd-YAG, DF, CO, CO<sub>2</sub>). Typical high-resolution ( $\Delta \omega = .08 \text{ cm}^{-1}$ ) transmission spectra included in this report were derived on the basis of Fourier transform spectroscopy. An extensive set of aerosol scattering coefficient data is reported for 15 visible wavelengths and is based on Koschmieder type measurements of contrast of distant targets. Results of extensive monitoring of HDO path concentration with a Gas Filter Correlation Spectrometer (GFCS) show an abundance ratio significantly lower than is commonly reported in the literature. Results of in-situ meteorological measurements and aerosol particle size distribution samplings are also reported.

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#### DATA COMPENDIUM FOR ATMOSPHERIC LASER PROPAGATION STUDIES CONDUCTED AT CAPE CANAVERAL, FLORIDA, FEBRUARY-MAY 1977

#### 1. INTRODUCTION

During the months of February through May 1977, the Infrared Mobile Optical Radiation Lab (IMORL) of NRL was operated at the Cape Canaveral Air Force Station (CCAFS) in Florida to conduct an extensive series of atmospheric transmission experiments. A principal objective of these experiments was to obtain precisely calibrated high-resolution atmospheric transmission spectra in the  $3-5 \,\mu$ m and  $8-14 \,\mu$ m atmospheric windows suitable for rigorous comparisons to computer models. Absolute transmission calibration of the FTS spectra is obtained by means of extinction measurements at several laser frequencies performed with minimal time offset from the FTS measurements. Emission spectra of the laser sources operated multi-line is used to generate accurate frequency calibrations of the atmospheric transmission spectra using the well known positions of the several laser lines used in the experiments.

A secondary objective of the CCAFS experiments was the evaluation of the effects of absolute humidity variations and the influence of aerosol scattering on the atmospheric extinction of several infrared laser lines in the above spectral regions.

A detailed description of the IMORL instrumentation may be found in Ref. 1. Experiments were conducted over a 5.1-km. overwater path, shown in Fig. 3.1 as Path 3. Atmospheric extinction and spectroscopic data were collected with the following apparatus:

(1) HeNe, Nd-YAG, DF, CO, and CO<sub>2</sub> lasers

- (2) Fourier Transform Spectrometer (FTS)
- (3) Gas Filtci Correlation Spectrometer (GFCS)
- (4) Bandpass filtered telephotometer operating at 14 wavelengths and optical pyrometer at two wavelengths
- (5) Aerosol particle spectrometer
- (6) Nephelometer operating at three wavelengths
- (7) Basic meteorological measurement apparatus

New additions to the IMORL system which were used extensively for the first time include a short wavelength CO laser, the FTS, the GFCS and the filtered telephotometer.

Presented in this report are the data gathered during the three month period with all the above instrumentation except the nephelometer. Data processing for the latter was not completed in time to be included here. A summary of laser extinction, FTS, GFCS, absolute humidity and visibility data is given in Table 1.1.

Note: Manuscript submitted September 8, 1977.

The laser beam extinction data are presented in Section 2. Section 3 contains a complete listing of all visible extinction data derived on the basis of telephotometric and pyrometric contrast measurements. Samples of the high resolution atmospheric absorption spectra obtained with the SMI are shown graphically in Section 4. Results of the GFCS measurement yielding HDO/H<sub>2</sub>O abundance ratios are contained in Section 5, while Section 6 includes selected data from the on-site meteorological stations, including aerosol spectrometer measurements.

It should be noted that all times, unless otherwise noted, refer to local civil time, which was EST for the months of Feb-April and EDT for May.

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#### 2. LASER EXTINCTION MEASUREMENT DATA

This section contains data from line-by-line laser extinction measurements made at Cape Canaveral Air Force Station in the spring of 1977. Transmissions were measured for helium-neon, neodymium-YAG, deuterium fluoride, carbon monoxide, and carbon dioxide laser sources along a 5.1-km overwater path from February through May of 1977. An elaborate scheme has been worked out to correct for short- and longterm drifts to achieve overall accuracies which are typically better than 5%. A detailed discussion of the measurement procedure can be found in the paper by Dowling et al<sup>1</sup>.

The columns appearing in Tables 2.0 to 2.4 include data given as day, month, and year. The months are designated by a single letter with F, M, A, and Y corresponding to February, March, April and May respectively. The time is given on a 24-hour clock. "Run Code" denotes short-path normalization measurements by 0, 1, 2, 7, 8, or 9, long-path transmission by 3. 4, 5, or 6. The short-path normalizations are used for computer reduction and do not appear on the final tables. Line ID denotes a particular line of given laser source. A six digit alpha numeric code for line ID was used to designate a particular laser operating line and in some cases the detector used for the measurements according to the following scheme:

LASER CODE	LINE ID	LASER/LINE	(µm)	DETECTOR
0	P00-S1	HeNe	0.6328	Si diode
1	P11 <b>-</b> SI	Nd-YAG	1.06	Si diode
1	P11-IN	Nd-YAG	1.06	InSb diode (77K)
3	P02-08	$DF/(2 \rightarrow 1 P_8 line)$	3.8007	InSb diode (77K)
4	P05-09	CO/(5→4 P <sub>9</sub> line)	4.9923	InSb diode (77K)
5	P10-20	$C0_2/00^{\circ}1 \rightarrow 10^{\circ}0$ band (P <sub>20</sub> line)	10.5910	GeAu PC (77K)
5	R02-20	CO <sub>2</sub> /00 <sup>°</sup> 1→02 <sup>°</sup> 0 band (R <sub>20</sub> line)	9.2714	GeAu PC (77K)

"Mob" and "Stat Gain" refer to precision gain settings used on detector preamplifiers for a single measurement. "Trans" is the actual transmission over the 5.1-km path corrected for detector efficiency and optical-train transmission. "Ex Coef." is the corresponding extinction coefficient for the measured transmission at a single line and is expressed in units of km<sup>-1</sup>. The optical-train efficiency is treated as a linear variable between two bracketing zero-path calibrations. For He-Ne and Nd-YAG, a single table summarizes all measurements in each case.

For DF, CO, and  $CO_2$ , one table per day is used due to the large number of individual lines involved.

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#### 3. AEROSOL EXCTINCTION MEASUREMENTS 3.1 SPECTROPHOTOMETRIC DATA

Contrast reduction experiments based on the Koschmieder theory were performed along the three paths shown in Fig. 3.1. Path 3, which is identical with that used for the laser beam experiments. Path 2, with a range of 2.57km, is nearly parallel to the beach with a portion of it running over water but displaced not more than about 100 m from the shore. The short path, No. 1, has a length of 1.28 km and runs entirely over land, with a maximum perpendicular distance of about 100 m inland from the shore. As may be seen from the geometry these three paths represent a convenient means for probing gradients perpendicular to the shore. The light-measuring apparatus was placed at the convergence of the three paths, in close proximity to the laser receiving station situated on the beach in a large semitrailer van. Passive "black" targets defined the termination points at the far ends of the paths.

For any particular path, of length R, an apparent contrast ratio,  $C_p$ , is defined such that

$$C_{R} = \frac{N_{h} - N_{b}}{N_{h}} = 1 - \frac{\int_{0}^{R} N(r) dr}{\int_{0}^{\infty} N(r) dr},$$
 (3-1)

where N and N represent the apparent radiance of the black target at the end of the path, and the radiance of the horizon sky adjacent to the target, respectively. For daylight operation in the visible region of the spectrum these radiances represent predominantly scattered solar radiation. Thus the radiance integrand, N(r), in Eq. (3.1)refers to the total volume scattering by atmospheric particles into the observation direction resulting from illumination of the volume in all directions.

If one neglects the effects of earth's curvature and assumes homogeneity of scatterersand uniformity of illumination along the effective range of the path, the well-known Koschmieder analysis predicts an exponential decay of  $C_R$  with range, i.e.,

$$C_{R}(\lambda) = e^{-\sigma} \lambda^{R}$$
, (2)

where  $\sigma_\lambda$  refers to the monochromatic scattering coefficient at wavelength  $\lambda$ , and the contrast ratio appears as a wavelength dependent function.

The quantity  $C_R$  was measured with a spectrally filtered telephotometer. Fourteen wavelengths were defined by bandpass interference filters which were used in sequence to observe black targets along the three paths shown in Fig. 3.1.

The resulting data are presented in Table 3.1 and shown graphically in Figs. 3.2, 3.3 and 2.4.

Fig. 3.5 shows the effect of wind speed on the nature of the spectra and on the gradients across the shore line.

#### 3.2 PYROMETRIC DATA

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The attenuation coefficient at 0.5568 and 0.6500 µm was determined visually by means of a telepyrometer. This is an optical pyrometer which has been modified by the addition of a telephoto lens. The attenuation coefficient was determined by measuring the radiance of a suitable black target and also the radiance of the adjacent horizon sky. These radiances are then applied to the Koschmieder relationship, which relates luminance to attenuation (see Sec. 3.1). In this simplified form the target is black and the measurement is made in a spectral region of minimal absorption, so that the observed attenuation is caused by molecular and aerosol scattering. In practice the apparent spectral brightness temperature of the target and horizon sky is determined by the optical pyrometer. From the known blackbody spectral radiance as a function of temperature, the attenuation coefficient is determined from the Koschmieder relationship, Equation (3-1). Four optical path lengths, of 3.10, 4.61, 5.08 and 7.47 km were used for these measurements. A small structure located near the laser transmitter site, Figure 3.1 was used for the 3.1 and 5.08 km paths with the pyrometer located near the aerosol sampling station and receiver site respectively. For the 4.61 and 7.47 km paths tree lines located near the shore line served as black targets with the pyrometer located at the laser transmitter site.

Table 3.2 gives the complete set of data in terms of three basic parameters, namely, path transmittance, extinction coefficient, and meteorological range (VIS.).

#### 4. HIGH-RESOLUTION FTS MEASUREMENTS

The high-resolution atmospheric transmission measurements were made with an IDAC Model 1000 Fourier transform interferomete spectrometer (FTS) system. A description of the FTS system and of its installation in the IMORE receiver trailer appears elsew -re<sup>1</sup> and will not be repeated here.

For the 1977 Cape Canaveral experiments the interferometer was operated in two distinct modes, depending upon the spectral region being investigated.

For work in the 3  $\mu$ m to 5  $\mu$ m atmospheric window, the interferometer was configured with a CaF<sub>2</sub> beamsplitter and an InSb deter or. Inteferograms of a graybody source in the IMORL transmitter traiter (5 km distant) were sampled at 128 K equally spaced points over a total optical retardation of 8 cm. To reduce noise levels in the resulting computed spectra, 100 interferometer scans were typically co-added prior to calculating the Fourier transform. The sampling process generally required about fifteen minutes.

For work in the 10  $\mu$ m region, the FTS system was used with a KBr beamsplitter and a HgCdTe detector. The 8 cm optical retardation vas retained, but the sampling was reduced to 64 K (equally spaced) points. Because the background radiation in this region is proportionately larger, separate "no-source" scans were also recorded. These reference interferograms provide data on the spectral distribution of the atmospheric background radiation, which must be separated from the graybody spectra before attempting an absolute transmission normalization. (To date, initial efforts to affect this separation by simply differencing the two types of interferogram prior to computing the Fourier transform have not proved satisfactory.)

Examples of spectra obtained with the FTS system are presented in Figures 4.1, 4.2, and 4.3. These spectra (chosen to cover a wide range of water vapor pressures) also incorporate preliminary transmission normalizations, based on the laser absolute transmission measurements. Care must be exercised when interpreting the "flat top" features seen in these spectra in regions of low transmission. The current software used by the FTS system does not correctly compute the ratio of a long-path spectrum to a short-path background spectrum when both the numerator and the denominator are small. In such cases, however, the atmospheric transmission at five kilometers is small (less chan 5%). A description of the laser measurements is presented in Section 2 of this report, and the techniques used to obtain a preliminary normalization have been presented in several earlier reports<sup>2</sup>,<sup>3</sup>,<sup>4</sup>.

Finally, development is currently nearing completion of a new series of computer programs designed to standardize the transmission normalization of sampled atmospheric spectra. These programs directly

process spectra from the magnetic tapes written by the FTS data aystem, and produce both graphical and digital magnetic tape output. It is expected the remainder of the high-resolution, laser-calibrated spectra from the Florida experiments should be available within two months.

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#### 5. GAS FILTER CORRELATION SPECTROMETER MEASUREMENTS

The atmospheric abundance of the molecular species HDO was measured with a gas filter correlation spectrometer (CFCS) during field measurements at the Patuxent Naval Air Station in November of 1976 and at Cape Canaveral Air Force Station (CCAFS) in the spring of 1977. This device is described in Jetail in reference (1). Data taken during the CCAFS experiment are plotted in Figures 5.1-5.23. Each plot presents a complete set of data taken during one day. HDO abundances determined by the GFCS are indicated by the symbol G. Also shown in Figures 5.1-5.23 are HDO abundances determined from local dew-point measurements using the widely accepted value of 0.03% for the HDO/H2O abundance ratio and the measured air temperature. Dewpoint measurements were performed at the transmitter, receiver and mid-point locations along the measurement path shown in Figure 3.1. The HDO abundances (expressed as molecules/cm/cm) derived from them are indicated by the symbols T, R, and M respectively in Figures 5.1-5.23.

Earlier GFCS data taken during the Patuxent NAS experiment are plotted in Figure 5.24 as water vapor partial pressure (using the 0.03% abundance ratio) against local time for several  $d_{eff}$ .

#### 6. METEOROLOGICAL MEASUREMENTS

#### 6.1 BASIC METEOROLOGICAL DATA

Three independent systems were used during the atmospheric transmission experiments to monitor and record the meteorological conditions at the two ends of the 5.1-km path and at a point approximately midway. One system was located in the office trailer van next to the transmitter van; another identical system was located in the mobile receiver trailer van and was operational during long-path measurements. A third, similar system was situated in the mobile meteorological van at the path halfway point.

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These systems include the following meteorological sensors: an automatically balancing EG&G Model 110S-M dew-point hygrometer to measure atmospheric temperature and dew point; a Yellow Springs Instruments Company Model 2014 barometric-pressure transducer; an Eppley Laboratory No. 8-48 Black and White Pyranometer to measure global (total sun and sky) radiation; a Thornthwaite Associates Model 912 sensitive-cup ane-mometer to measure wind speed at the path ends; a Young Gill Model 35003 propeller Vane to measure wind speed and horizontal wind direction at the midpoint; and a Young bivane to measure horizontal and vertical wind direction at each path end.

Analog voltages from each meteorological sensor are processed by a Monitor Labs 7200 data-acquisition system at each path end and by a Particle Measuring Systems data-acquisition system at the midpoint location. The outputs are digitally recorded on magnetic tape for subsequent reduction at NRL.

Table 6.1.1 lists the available meteorological data for the period 23 February through 25 May 1977 at the three monitoring eites: transmitter T, mobile met van M, and receiver/spectrometer, S. Air temperature AT is in degrees Celsius; the partial pressure of water vapor PPH<sub>2</sub>O is in torr; barometeric pressure BP is  $i_1$  millibars; global/solar radiation SR is in watts per square meter; wind speed WS is in meters per second; and horizontal wind direction WDH is in degrees clockwise from magnetic north. Blank spaces in this table indicate unavailability of data for that time for a particular sensor due to operational difficulties in the field; lack of an entry for any system at the approximate half-hour mark indicates nonexistence of data at that time or failure in processing system tape for that day or time of day. Each entry in this table is a 6-minute average terminating at the time indicated.

Figure 6.1.1 shows an example of the variation in air temperature and partial pressure of water vapor observed at the three monitoring sites during a particular day (15 March 1977).

#### 6.2 PARTICLE SPECTROMETRY

The Laser/Aerosol Interaction Section of the Optical Radiation Branch provided, for the first three months of the 1977 Florida experiment, measurements of aerosol distributions and readings from one set of meteorological instruments. The data from the aerosol measurements are provided here in Table 6.2.1. The meteorological measurements were presented above in Section 6.1 (location M).

The equipment used for obtaining the aerosol size distributions included two optical particle spectrometer probes and a buffer memory manufactured by Particle Measuring Systems. The Active Scattering Aerosol Spectrometer Probe (ASASP) monitors particles from 0.1  $\mu$ m radius to 2.0  $\mu$ m radius with a sample volume flow rate of 0.11 cm<sup>3</sup>/sec. The High Volume Classical Aerosol Spectrometer Probe (HVCASP) monitors particles from 1.0  $\mu$ m to 15  $\mu$ m radius with a sample volume flow rate of 49 cm<sup>3</sup>/sec.

Sampling occurs on a one-second basis in the system as configured. These data are recorded on a 9-track computer compatible magnetic tape which is later reduced to the desired averaging times. For the work in Florida six-minute averages were chosen as giving acceptable counting statistics while minimizing the time-slew which might degrade the resolution of any major, abrupt aerosol density fluctuations.

For the purposes of this compendium, the resultant six-minute averages are given only on the half hour as shown in Table 6.2.1. Presented there are aerosol size distributions in the form of particle density  $(\Delta N/\Delta R)$  as a function of particle radius (R). The density is found from the average number of counts per second in a bin divided by the sample volume flow rate divided by the width of the sampling bin ( $\Delta R$ ) which has its center at radius R. The entries for the first seven bin locaticus are obtained from the ASASP; the remaining fifteen are obtained from the HVCASP.

The relatively large gap between the bins with centers at 0.33  $\mu$ m and 1.22  $\mu$ m is the result of an inherent double-valued response function in the ASASP which arises because a single frequency light (a HeNe laser) i, used as the illuminating source. Because the simple approach as Jescribed above for obtaining  $\Delta N/\Delta R$  gives structure which is nonexistant in the actual distribution in that particular region, the results obtained from those bins have been omitted.

The extinction coefficients which are calculated from these distributions will be presented in a later report with a detailed analysis.

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visibility (km) 24.3 11.9 0.01 42.3 35.0 20.0 20.0 19.5 14.0 10.0 18.0 21.0 : : : : z : r YF1 ррН<sub>2</sub>0 (Torr) 13.6 12.8 7 0 13.1 16.0 15.0 16.0 16.5 14.6 11.7 5.8 9.2 : = : 2 ĩ : = GFCS GFCS ł >: ł ł ≍ × ł ł ł × ł Code\* 211 211 111 112 111 132 132 111 111 111 111 111 111 111 ł ł ! -Ξ 0-7800 0-7300 800-3200 0-7600 0-3900 1600-3200 1800-3200 1800-3200 1800-3200 1800-3200 800-3200 1800-3200 1800-3200 1800-3200 1800-3200 FTS FTS Spectral Interval (cm<sup>-1</sup>) ł ł ł + 1335 1155-1600 1050 1300 Time 1530 1840 1610 1700 1820 1240 1250 1250 1210 1225 1300 1310 ł ł ł # Lines Measured 50 65 70 ł 75 11 ł 1 67 5 ł 21 68 1 76 Ł 87 81 ł LASER HeNe, DF, CO<sub>2</sub> heNe,DF, CO<sub>2</sub> HeNe, CO<sub>2</sub> HeNe, CO<sub>2</sub> i'eNe, CO<sub>2</sub> Lasers °2 : : ł DF : : 1 = = ļ 1430-1610 1420-1830 0950-1450 1045-1250 1030-1615 1530-1800 1130-1430 1000-1618 1150-1540 1125-1700 0091-0600 1025-1530 Time ł ł ł ; ł Pathlength (m) 5080 3 : : = = 2 : = ÷ : ŧ = : : : = : Date 2-23 20 11 12 25 : 26 28 : = 3-2 ~ \$

TABLE 1.1.5 1977 CCAI'S EXPERIMENT SUMMARY

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			LASEI	-		FTS		GFCS	¥	1
1	Pathiength (m)	Tine	Lasers	# Lines Measured	Time	FTS Spectral Interval (cm <sup>-1</sup> )	Code *	GFCS	ррИ <sub>2</sub> 0 (Тогг)	visibility (km)
1	=	1000-1715	=	156	1320- 1415	+	132	×	7.0	24.5
	2	0830-1430	=	70	1110- 140	+	032 132	×	12.5	25.0
	50	1340-1450	•	17	1520	+	232	;	16.6	19.0
	:	1020-1450	1	53	:	ł	ł	ł	ł	1
ION	_									
	:	1	ł	1	1545	800-3200	132	1	15.0	30.5
	÷	ł	ł	ţ	1545	0-3900	132	ł	z	•
	Ŧ	;	ł	ł	1545	0-1900	132	ł	:	=
	:	1000-1630	HeNe, DF, CO_2	138	1305	1800-3200	111	:	17.5	25.0
	:		ł		1320	1800-6600	111	1	:	z
	5080	1400-1600	HeNe, DF	27	1245	1800-6600	111	×	18.0	<u>30.0</u>
	Ŧ	ł	;	ł	1245	0-7800	111	×	=	:
	:	1000-1600	н <b>.че, DF.</b> Со, сл <sub>2</sub>	88	1310	1800-3200	111	×	18.0	20.0
	÷			ł	1330	1800-3200	111	×	2	÷
	Ŧ				1635	806-3200	132	×	:	-
	÷	579-1960	HeNe,YAG, DF,CO <sub>2</sub>	138	1345	800-3200	132	×	18.5	29.8

TABLE 1.1. 1977 CCAFS EXPERIMENT SUPPLARY

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had a bir a way to be and the Philips. "A fibra way of the Philips have " d the two sta

			LASE	~		SLA		5735	5	
Date	Pathlength (m)	Time	Lasers	# Lines Measured	Time	FTS Spectral Interval (cm <sup>-1</sup> )	Code*	GFCS	ррИ <sub>2</sub> 0 (Тогг)	visibility (km)
4-2	ŧ	1	ł	1	1345	0-3900	132	×	=	=
	5080	1	ł	ł	1400	800-3200	132	×	18.5	29.8
	:	ł	ł	1	1400	0-3900	132	×	:	=
4-4	:	0915-1630	HeNe,YAG, DF, CO <sub>2</sub>	180	1235	800-3200	132	×	18.0	21.0
	:	1	ł	ł	1255	800-1400	132	×	=	=
		1	ł	8	1310	E00-1600	032	×	1	£
		ł	8	1	1310	0-3900	032	×	z	=
4-5	-	1045-1545	HeNe,YAG, DF, CO_2	72	1350- 1425	+	132	×	10.5	50.0
4-6	50	0930-1650	-	129	1230	800-3200	132	ł	7.0	60.0
	-	1	ł	ł	1245	800-3200	132	ł	=	=
4-7	:	0940-1430	HeNe,YAG, DF, CO <sub>2</sub>	66	1245	1800-3200	111	1	6.8	53.0
		ł		ł					=	=
3RD SESSION	_									
5-13	50	1500-1700	DF, CO	6	1	ł	ł	ł	;	1
14	-	1030-1745	HeNe,YAG, DF,CO,CO_2	130	1140	1800-3200	311	ł	12.8	ł
	:	ł	;	ł	1240	1800-6600	311	i	12.4	1
	:	;	ł	I	1300	1800-3200	311	ł	:	ł

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SUPPAARY
EXPERIMENT
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			IASE			FTS FTS		GFCS	WE	1	COMMENTS
Pat	thlength (n)	Tipe	Lasers	+ Lines Measured	Time	Spectral Interval (cm <sup>-1</sup> )	Code *	GFCS	ppH <sub>2</sub> 0 (Torr)	visibility (km)	
	5080	6121-0560	HeNe,YAG, Co, Co <sub>2</sub>	244	1	1	1	×	15.0	26.0	
	-	1000-1500	=	123	ł	;	1	×	14.5	25.0	
	=	1100-1545	HeNe, YAG, DF	26	1120	1800-6600	311	×	14.0	28.0	
	:	ł	1	:	1350	1800-6600	311	×	14.5	:	
	=	1	;	;	1415	1800-6600	311	×	14.5	:	
	Ŧ	0630-1410	HeNe,YAG DF	42	1015	1800-3263	311	×	16.5	18.0	
	:	ł	ł	;	1245	1800-3200	311	×	:	2	
	:	ł	ł	ł	1300	1800-3200	311	×	:	÷	
	:	ł	:	;	1420	1800-3200	311	×	÷	÷	
	:	0900-1615	HeNe,YAG DF,CO,CO <sub>2</sub>	84	0160	1800-6600	111	×	18.0	46.0	
	=	1	:	1	1115	2000-2050	116	×	18.0	-	O laser scans on FTS
	:	ł	;	ł	1215	2000-2050	116	×	18.0	=	
	:	ł	ł	:	1310	800-3200	311	×	17.0	-	
	:			i	1330	1800-6600	311	×	17.0	-	
	:	;	1	i	1645	1800-6600	311	×	18.0	:	
	:	0845-1515	HeNe,Y4G DF, CO <sub>2</sub>	90	0060	1800-3200	311	×	20.0	32.0	
	:	:	;	ł	1145	1800-3200	311	×	:	÷	
	:	1	;	ł	1210	1800-3200	311	×	:	:	
	:	;	ł	r I	1535	1800-3200	311	×	:	:	

TABLE 1.1. 1977 CCAFS EXPERIMENT SUMMARY

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CONTENTS					ulti-l'ar DF laser on FTS		
	visibility (km)	27.0	:	:	i I	ł	1
ME	ррН <sub>2</sub> 0 (Torr)	20.0	:	20.0	•	ł	ł
GLCS	GFCS	×	×	×	ł	Ļ	:
	Code *	I	311	311	116	311	311
FTS	FIS Spectral Interval (cm <sup>-1</sup> )	1800-6600	1800-6600	1800-6600	1800-3200	1800-6600	1800-3200
	Tîme	0955	1155	1215	1050	1430	1445
ER	# Lines Measured	51	;	ł	109	Ĩ	:
IAS	l.asers	HeNe,YAG DF, CO <sub>2</sub>	ł	ł	HeNe,YAG DF,CO2	1	ł
1	Time	<b>3845-1345</b>	ł	ł	1950-1500	:	ł
	Pathlength (m)	5080	:	=	50	:	Ŧ
	Date	5-25			26		

NOTES:

- + several interferrograms recorded and stored but not yet transformed
  - FTS measurement code \*
    - lst digit: source

- 0 = no source 1 = transmitter greybody 2 = receiver greybody 3 = glober (transmitter) 9 = as specified in comments

2nd digit: beamsplitter

- 1 = CaF<sub>2</sub> 2 = Quartz 3 = KBr

.rd digit: detector

1 = InSb (SBRC) 2 = HgCdTe (ADL) 3 = HgCdTe (TI)

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THELE	2.6 OF	LINE BY L	INE LASEN	EXTINCTION	on measurem	ENTS FOR HE	NE LASER	SOURCE
DATE	THE	RUN CODE	LOSER	LINE ID	MOR GAIN	STAT CAIN	TRONS	EX COFF
	1 (1)2		BRODA			STRE GRAD	Innito	
		_	-		-	_		
J2M77	253	3	3	P00-51	0	0	0.747	0.057
9_11/7	954	3	2	P00-51	0	0	0.757	0.054
9 11 i i	1111	2	6	P90-51	U U	r R	0.718	0.055
329977 99M77	1215	ి సి	5	100-51	ย	0	0.646	0.025
32177	937 470	377	0	P00-51	1	8	0.534	0.123
53M72	939	2	8	P00-51	1	8	0.529	0,124
1507	9.13	3	ด้	P00-S1	1	0 A	0.320	A 121
nSi477	925	ž	ñ	PAA-SI	i	Ä	8.521	0.127
381-77	947	3	ē	P00-S1	ī	ดั	A.533	0.123
U8M77	1356	4	ě	P00-51	ø	õ	0.597	0.101
38M77	1358	4	0	P00-S1	Ð	0	0.579	0.107
04M77	1446	3	0	P00-S1	8	Ø	0.456	0.153
19M77	1155	3	0	P00-SI	2	2	0.154	0.365
11M77	1356	3	õ	P00-SI	2	2	0.314	ð.226
11.377	1449	3	0	P00-51	2	2	0.282	0.247
12077	1407	3	N N	P00-51	2	2	0.429	0.165
12010	1565	57	0	P00-51	ž	2	0.430	0.165
13007	1511	37	0	P00-51	5	ź	0.209	0.152
01077	1439	3	о Я	P00-51	5	4	0.302	6 199
62977	1151	7	ñ	P00-S1	5	5	0.505	Ø 129
92877	1235	4	õ	P00-51	2	ž	0.513	0.128
02477	1314	5	Ğ	P00-SI	ž	ž	0.546	0.118
0 °77	1429	6	0	F00-S1	2	2	0.565	0.111
92A77	1502	6	0	P00-S1	2	2	0.581	0.106
0-iH77	1052	3	0	P00-S1	2	2	0.512	0.131
J4877	1133	4	0	P00-51	2	2	0.548	0.117
04477	1451	3	5	P00-51	á	5	0.407	0.170
64H77 67572	1000	4	อื่	P00-51	22	22	0.304	0.107
05472	1456	2	Ä	PHAST	5	2	0.541	0.076
95877	1527	4	ĕ	P00-S1	ž	ž	8.738	0.061
15777	1243	3	ō	P90-SI	2	ž	0.673	0.076
10977	1444	4	0	P00-SI	1	1	0.557	0.114
16477	1530	5	0	P00-S1	1	1	0.559	0.114
17Y77	1233	3	0	P00-S1	2	Ş	0.497	0.137
201/77	1438	3	0	P00-51	2	2	0.582	0.107
21977	1130	3	ดั	POU-SI	2	2	0.428	0.166
211/77	1207	4	0	P00-51	5	Š	0.436	0.162
211/77	1323	5	6	P00-51	22	20	0.420	0.105
22022	1236	Å	Ä	P00-51	5	2	0.405	0.113
24077	1435	5	ă	P00-S1	2	2	0.728	0.062
23177	1602	ĕ	ă	P09-S1	2	2	0.790	0.046
24777	1039	3	ē	P00-S1	ž	ž	0.716	0.065
24477	1119	4	0	P00-SI	2	Ž	0.730	0.062
24777	1329	5	0	F00-SI	2	2	0.661	0.081
24777	1409	6	0	P00-S1	5	2	0.730	0.062
24777	1503	6	ğ	F00-SI	Z	Z	0.720	0.064
25477	847	3	0	P00-51	2	2	0.526	0.125
234(1	930 1000	4	ย ผ	700-51 700-51	5	4	0.642	0.000
25777	1143	ĕ	ĕ	P00-51	2	ź	0.615	0.095
		-	-		-	-		

TABLE	5.1 OF	LINE BY L	the loser	EXTINCTIO	n Measurem	ents for ND	yg laser	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EN COEF
02077	1154	3	١	P11-51	Ň	2	0.683	0.075
02n77	1528	5	1	P11-51	3	2 - Z	0.662	0.001
QZATT	1212	ų.	1	P11=51	2	Ę	0.677	n.076
92977	1435	6	1	PHISI	1	2 2	0.671	0.070
USA77	1262	ų	į	F11-51	Ś	č	6.639	0.087
UGHEF	1216	U S	l.	F 1 1* 10	3	9	0.051	0.090
100H/7	1245	8	1	611-61	3	27	0.031	0.000
States -	1024	3	1	111-01	6	16 74	9.00M	0,102
0.49441.1 Defici	和后上] 皆用此了	4 2	1	111-41	5	ية. 1	0.267	9,107
0.40.62	1670	Å	1	011-21	5	е ,ч	0.418	8,171
9-02-	រត់នើ	Ä	1	P11-51	3	5	0.369	ñ. 195
ยรื่อ	1466	*	i	Pil-Št	2	3	0.747	0.057
85677	1528	ä	i	Pii-Si	2	, Č	0.799	0.044
05477	1537	5	i	PII-IN	2	2	0.830	0.036
16177	12.16	3	i	111-51	5	ē	0.896	0.021
161.00	149	à	i	P11-51	ĩ	Ĩ	0.793	0.045
16171	1533	5	i i	Piinst	1	1	0.773	0,050
17425	1235	3	1	P11-91	S	2	0.658	0.082
20177	1440	2	1	P11-51	2	2	0.764	0.055
30125	1538	3	1	P11-51	3	2	0.790	0.049
21177	1133	3	1	P11-51	2	2	0.710	0.067
5144	1500	ન	1	P11-51	ş	2	0.696	0.071
211/22	1331	÷,	1	<u> </u>	2	1 i i	0.653	0.972
21VT5	1401	b.	1	<u>F11-S1</u>	2	2	0.641	0.087
52112	1139	3	1	P11-SI	e .	2	0.701	0.048
	1525	નુ	1	F11-51	4	Ϋ́,	0.558	0.034
	1423	5	1	F11-51	ų.	r i	9.143	6.663
6 4 6 6 6	1684	Ď	1	11-51			17. L 34 AL 1988	0.001
64177	14.26	3	ļ	P11~51	S.	s,	9.123	0,000
5. 14 V F F	1113	*1 6	1	111-21	2.	5	0,100	
54111	1211	4 5	1	111-24	Ś	1	0.754 0.754	1. 1655 0. 666
2 10 11	1883.1	2 2	1	111-31 Bilact	*:	5	0 716	0.000
294777 380477	1 2 2 2 4 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4	3	1	144734	3	5 7	0.110	8.895
63111	946			811-81	5	4 <u>.</u> 3	6 ***1	0.661
122311 301099	1010	54 b.	4	343744	i,	5	6 7 6 1	6.661

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TAELE	5.2 OF	LINE BY L	INE LASER	EXTINCTIO	on measurem	ents for df	LASER	SOURCE
PATE	TIME	FUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
03M77	1429	3	3	P02-08	4	3	0.478	0.144
33177	1431	3	3	P02-07	4	3	0.323	0.221
231177	1432	зк Х	2	P02-95	ŝ	4	0.468	0.143
3 31177	1.436	ž	š	P01-07	š	4	0.477	0.145
031177	1437	5	3	P01-06	5	4	0.375	0.191
03177	1439	5	3	P01-07	5	4	0.472	0.147
03001 03007	1441	3	3	PA2-A5	ŝ	2	0.255	0.204
93M77	1445	ŝ	3	P02-07	5	3	0.315	0.226
03M77	14.14	3	3	P02-08	4	3	0.459	0.152
0211/7	1445	3	3	P02-10	4	3	0.347	0.207
1131177	1448	ž	š	P02-10	š	4	0.338	8.210
C3M77	1450	3	3	F02-08	5	4	0.439	0.161
03477	1452	3	3	P02-07	é	4	0.318	0.224
03007 03M27	1455	210	3	P02-05	6	4	0.454	0.154
33177	1456	3	5	P01-07	Š	4	0.453	0.154
93H77	1458	3	3	P01-96	6	5	0.360	0.280
93472	1409	<u> ১</u>	37	P01-07 P31-38	5	4	0.460	0.152
031177	1501	č	3	P02-J5	Š	4	0.240	0.164
J3177	.563	3	3	P02-07	5	3	0.302	0.234
93,477	1544	5	3	P02~08	4	3	0.431	0.165
33°h -	1535	24	2	F02-10 F02-12	4	35	0.327 0 494	0.218
13M-7	.508	ž	ŝ	F02-10	4	3	0.303	0.233
251177	1268	3	3	P02-98	4	3	0.379	0.190
(10) <b>(00)</b>		-	_		_	_		
68M77 00M77	1132	3	3	P02-08	3	3	0.627	0.091
USM27	1136	33	3	P02-05	4	3	0.4/5	0.145
08M77	1138	3		P01-08	5	4	0.438	0.161
904177 39M75	1140	37	3	P01-07	4	4	0.623	0.092
08M77	1143	3	3	P01-05	ŝ	5	0.536	0.122
08M27	1145	3	3	P01-06	ē	Š	0.418	8.179
0.0M77 0.0M77	1146	3		P02-05	ភ្ន	5	0.627	0.691
09M77	1149	3	3	P02-07	4	4	0.487	0.140
13M77	1150	3	3	P02-10	4	3	0.460	0.152
051177 000077	1152	3	3	P02-12	4	4	0.581	0.166
3.4177	1154	3	3	P02-08	3	37	0.618	0.152
C9M77	1431	4	3	P02-98	ž	3	0.642	0.086
381177	1434	4	3	P02-07	4	3	0.510	0.132
19M27	1433	4	5	PU2-05 PO1-29	3 5	3	0.652	0.084
03M77	1479	4	13	P01-07	4	4	0.655	0.085
78M77	1440	4	3	F01-06	5	4	0.582	0.106
P8677 69627	1441	4	57	P01-07 P01-09	5	4	0.640	0.087
03M77	1443	4	3	P02-05	4	4	0.623	8.103
772480	144	4	3	P02-07	4	3	0.517	0.129
08017	1446	4	3	P02-03	3	3	0.609	9.097
35m77	1440	4	3	P02-12	4	3	0.402	0.155 0.182
<u>98477</u>	1-1-19	-4	3	P02-10	4	3	0.433	0.164
30247	1450	4	3	P02-08	0	3	0.614	0.095

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TABLE	2.2 OF	LINE BY L	INE LASER	EXTINCTIO	n measurem	ENTS FOR DF	LASER	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GRIN	STAT GAIN	TRANS	EX COEF
891777 9531777 9531777 9531777 9531777 9531777 9531777 9531777 9531777 9531777 9531777 9531777 9531777 9531777 9531777 9531777 9531777 95317777 95317777 95317777 95317777 95317777 95317777 953177777 9531777777777777777777777777777777777777	1618 1621 1621 1622 1622 1622 1622 1622	លាលាលសាសសាលាលាលាក	លកម្មភាពសម្ពាលស្រុកស្រុ	P82-08 F02-05 P01-05 P01-07 P01-07 P01-07 P01-07 P02-03 P02-10 P02-10 P02-12 P02-10 P02-10 P02-10 P02-10	<u>ង</u> ៨សមាម៨សសសសត សមាជ	<b>Გ</b> Ა Ო Ა Ა Ა Ა Ა Ა Ა Ა Ა Ა Ა Ა Ა Ა Ა Ა Ა	C.540 0.385 0.5377 0.585 0.585 0.585 0.576 0.576 0.576 0.594 0.594 0.594 0.591	0.113 6.187 0.201 0.105 0.141 0.194 0.194 0.194 0.194 0.194 0.194 0.195 0.194 0.194 0.194 0.195 0.194 0.194 0.194
11177777777777777777777777777777777777	1129 11337 11337 11337 113446 115546 11551 11551 15515 15512 15522 15522 15522	мерикимининининининини	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	P02-08 P02-05 P01-07 P01-07 P01-07 P022-10 P022-10 P022-10 P022-10 P022-10 P022-00 P022-00 P022-00 P001-08 P0022-00 P001-08 P001-08 P002-08 P001-08 P002-08 P002-08 P002-08 P002-08 P002-08 P002-08 P002-08 P002-08 P002-08 P002-08 P002-08 P002-08 P001-08 P002-08 P001-08 P002-08 P001-08 P001-08 P002-08 P001-08 P002-08 P002-08 P001-08 P002-08 P001-08 P001-08 P002-08 P001-08 P002-08 P001-08 P002-08 P001-08 P002-08 P001-08 P001-08 P002-08 P001-08 P001-08 P002-08 P001-08 P001-08 P002-08 P001-08 P002-08 P001-08 P001-08 P002-08 P001-08 P002-08 P001-08 P001-08 P002-08 P001-08 P002-08 P001-08 P002-08 P001-08 P002-08 P0000-08 P002-08 P002-08 P002-08 P002-08 P002-08 P002-08 P	444r0rrw444074+440r0r00000	๚๚๚๛๛๛๚๚๚๚๚๚๚๛๛๛๛๚๚๚	$\begin{array}{c} 9.358\\ 9.358\\ 0.379\\ 0.382\\ 0.478\\ 0.382\\ 0.474\\ 0.382\\ 0.474\\ 0.303\\ 0.473\\ 0.312\\ 0.312\\ 0.312\\ 0.343\\ 0.312\\ 0.343\\ 0.343\\ 0.343\\ 0.343\\ 0.343\\ 0.343\\ 0.343\\ 0.449\\ 0.343\\ 0.345\\ 0.244\\ 0.229\\ 0.345\\ 0.2445\\ 0.245\\ 0.445\\ 0.255\\ 0.255\\ 0$	0.201 0.161 0.1840 0.21684 0.21684 0.22363 0.2269 0.2269 0.21699 0.21489 0.21499 0.21489 0.21489 0.21489 0.21489 0.21489 0.21489 0.21489 0.21489 0.21489 0.21489 0.214990 0.2149900000000000000000000000000000000000
200777 1200777 1200777 1200777 1200777 1200777 1200777 1200777 1200777 12007777 12007777	1522 1522 1522 1522 1522 1522 1522 1522	<b>ជាយលាយសាលសាសសាស</b> សាស	លះកម្មលេខាល់លាលសាល	P02-09 P02-07 P01-05 P01-07 P01-07 P01-07 P01-08 P02-05 F02-05 F02-08 P02-08 P02-10 P02-10 P02-10 P02-10	444207025104443	4 ๒ ๒ ๒ ๒ <b>๛ ๛ ๛ ๛ ๛</b> ๛ ๛ ๛	0.525 0.327 0.497 0.249 0.532 0.541 0.248 0.519 0.523 0.518 0.398 0.593 0.598 0.593 0.401 0.596	0.126 2.219 0.137 0.272 0.123 0.128 0.127 0.128 0.134 0.134 0.133

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TABLE	2.2 OF	LINE BY L	INE LASE	R EXTINCTIO	on measurem	ENTS FOR DF	LASER	SOURCE
PATE	TIME	RUN CODE	LASEX	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
44747777777777777777777777777777777777	1110 1111 1112 1116 1116 1116 1116 1123 1126 1127 1126 1127 1126 1127	សសាលាថា សោសលាមាសាស	ស្រុកស្រុកស្រុកស្រុកស្រុកស្រុកស្រុកស្រុក	P02-08 P02-07 P02-05 P01-08 P01-06 P01-07 F01-08 F02-05 P02-08 P02-08 P02-08 P02-10 F02-10 P02-10 P02-08	NM70000NN7.57MN7	н ь тими ритории прии	0.693 0.594 0.541 0.666 0.604 0.527 0.674 0.527 0.507 0.507 0.507 0.507 0.702	0 072 0.102 0.030 0.120 0.079 0.098 0.081 0.125 0.077 0.111 0.066 0.133 0.087 0.133 0.087 0.159
154777 1546777 1546777 1546777 154777 154777 154777 154777 154777 154777 154777	1811 1013 1014 1015 1016 1017 1018 1019 1021 1025 1025 1026 1029	ୠୠୠୠୠୠୠୠୠୠୠୠୠୠ	๚๛๚๛๚๛๚๛๚๚๚	P02-08 P02-05 P01-07 P01-07 P01-07 P01-07 P01-07 P02-08 P02-08 P02-08 P02-10 P02-10 P02-10 P02-10 P02-10	ស្រុកភ្លេសភ្លេសក្នុងស្រុកស្រុក	មានសាលាសាសាសាសាសាសាសា	0.710 0.536 0.678 0.475 0.582 0.582 0.475 0.547 0.542 0.547 0.542 0.516 0.517 0.647	0.067 0.122 0.076 0.075 0.075 0.078 0.078 0.078 0.080 0.080 0.129 0.029 0.025
	14822 1414 14156 14167 14167 14167 14167 14167 14420 14225 14225 14225 14225 14225 14225 14225 14225 14225 14225 14225 14256 144566 14456 1446 144	ะ เป็นประเทศ (14) (14) (14) (14) (14) (14) (14) (14)	ଏକାରାଜାକାର୍ଯ୍ୟ କାର୍ଯ୍ୟ କାର୍ଯ୍ୟ କାର୍ଯ୍ୟ କାର୍ଯ୍ୟ କାର୍ଯ୍ୟ କାର୍ଯ୍ୟ କାର୍ଯ୍ୟ	P02-08 P02-07 P01-08 P01-08 P01-06 P01-07 P01-08 P02-07 P02-07 P02-07 P02-10 P02-10 P02-10 P02-10 P02-10	Ŧ <b>₽₽₽</b> ₽₽₽₽₽	<b>พตชุมของว่อตุดตุดภู</b>	0.634 0.399 0.6420 0.6280 0.6280 0.6280 0.6280 0.6285 0.6885 0.6855 0.4855 0.4855 0.4855 0.4855 0.4855 0.4855	6.0889 6.0887 6.0845 6.0845 6.0845 6.0845 6.0845 6.0845 6.0845 6.0845 6.085 6.085 6.195 6.195 6.195 6.195

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ÐA	777 mm	OF LINE	BY LINE I	LASER EXTIN	CTION MEAS	IDEMELIAN			
24	TIP	TE RUN C	ode las	SER LINE	ID MOR CO	MERENIS F(	DR DF	LAS	SER SOURCE
01	121 779	3 7		-	IND GA	IN STAT	GAIN	TRANS	E.K COEF
014 014 014 014 014 014 0147 0147 0147 0	121       1221       1222       1222       1222       1222       1222       1222       1222       1222       1222       1222       1222       1222       1222       1222       1222       1223       1356       1401       1402       1410       1411       1412       1412       1412       1412       1412       1420       1421	90000000000000000000000000000000000000	មាលមុសលល់ស្រុសស្វស្វស្វស្វស្វស្វស្វស្វស្វស្វស្វស្វស្វ	P02-0 P01-0 P01-0 P01-0 P01-0 P02-1 P02-1 P02-1 P02-1 P02-00 P02-00 P01-00 P01-00 P01-00 P01-00 P01-00 P01-00 P02-00 P01-00 P02-10 P02-10 P02-00 P02-00 P02-00 P01-00 P02-00 P002-00 P00 P	3667674555547445767785545; 4&4	<b>₵</b> ₱₥₥₥₥₥₽₱₽₽₽₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩		8.416671 6416671 8.6512161 8.653512564 8.653512564 8.5565366 8.5565366 8.556643 8.556643 8.556643 8.556643 8.556643 8.56644 8.566444 8.566444 8.566444 8.566444 8.566444 8.566444 8.566444 8.566444 8.5664444 8.5664444 8.5664444 8.56644444 8.56644444444444444444444	0.078 0.121 0.000 0.231 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.088 0.129 0.129 0.129 0.129 0.129 0.129 0.129 0.138 0.083 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.075 0.085 0.085 0.075 0.0750 0.0750000000000
U2A77 U2A777 U2A77 U2A77 U2A77 U2A77 U2A77 U2A77 U2A77 U2A77 U2A77 U2A77 U2A77	1209 1209 1211 1212 1214 1214 1214 1214 1214 121	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	ษณิษณฑณษณษณศณฑฑ๗๗๗๗๗๗๗๗๗๗๗๗๗๗๗๗๛๗ 	P02-03 P02-05 P01-08 P01-02 P01-02 P01-02 P01-02 P02-05 P02-05 P02-08 P02-08 P02-08 P02-08 P02-08 P01-06 P02-08 P01-06 P02-08 P01-06 P02-08 P01-06 P02-08 P01-08 P02-08 P01-08 P02-08 P01-08 P02-08 P02-08 P01-08 P02-	444%~%~~~%5555~~545%598%%%%5655~~44	<b>₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩</b>	0.7.4(.3.6577537347,263347275354762755755745275575575575575575575575575575575575575	55 669590023188873747	0.298 0.060 6.153 0.856 0.208 9.078 0.110 0.064 0.056 0.211 0.062 0.107 0.058 0.107 0.058 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.136 0.059 0.134 0.139 0.134 0.139 0.134 0.139 0.134 0.139 0.134 0.139 0.134 0.139 0.134 0.

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TABLE	5.2 OF	LINE BY L	INE LASER	EXTINCTION	on measurem	ENTS FOR DF	LASER	SOURCE
DATE	TIME	RUN CODE	Laser	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
00000000000000000000000000000000000000	$\begin{array}{c} 1151\\ 1153\\ 1155\\ 1155\\ 1156\\ 1156\\ 1159\\ 1201\\ 1204\\ 1206\\ 1206\\ 1206\\ 1405\\ 1408\\ 1412\\ 1408\\ 1412\\ 1423\\ 1425\\ 1425\\ 1425\\ 1429\\ 1425\\ 1429\\ 1425\\ 1429$ 1429\\ 1429\\ 1429 1429\\ 1429 1429 1429\\ 1429 142	июююююююююююеаааааааааааааа	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	$\begin{array}{c} 987\\ -876\\ $	<b>ฯ</b> ฯ ฯ ฯ ๛ ๛ ๛ ๛ ๛ ๛ ๛ ๛ ๛ ๛ ๛ ๛ ๛ ๛ ๛ ๛	<b>ਲ਼ਲ਼ਲ਼ਲ਼ਲ਼ਲ਼ਲ਼ਲ਼ਲ਼ਲ਼</b> ੑੑਲ਼ਲ਼ੑੑਲ਼ਖ਼ਖ਼ਲ਼ਲ਼ੑੑੑੑੑੵਲ਼ਲ਼ਲ਼ੑੑਲ਼ੑਲ਼ੑੑਲ਼ੑ	0.6726 0.68766844906175866442446988731080017774	0.099 0.093 0.093 0.0943 0.103 0.103 0.153 0.153 0.153 0.1137 0.161 0.161 0.161 0.1206 0.1206 0.1229 0.1232 0.1235 0.1235 0.1235 0.1235 0.1235 0.1351 0.1351 0.1804
05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77 05A77	154 <b>0</b> 1541 1543 1544 1545 1546 1548 1549 1550	ผสผสสสส	ณณณณณณณ ม ม ม ม ม ม ม ม ม ม ม ม ม ม ม ม	P02-08 P02-07 P02-05 P01-08 P01-08 P01-06 P02-08 P02-10 P02-12 P02-38	りりたくなくなりたり	470004704	0.834 0.613 0.819 0.546 0.784 0.585 0.231 0.617 0.757 0.814	0.036 0.096 0.839 0.118 0.074 0.074 0.036 0.094 0.054 0.040
2077 2077 2077 2077 2077 2077 2077 2077	1502 1504 1508 1508 1512 1512 1514 1516 1520	มพลสสสสส	88888888888 88888888888	P02-08 P02-07 P01-08 P01-08 P01-07 P01-06 P02-08 P02-10 P02-12 P02-08	<b>ਲ਼ਲ਼ਲ਼</b> ੑੑੑ <i>๛</i> ੑੑ <i></i>	<b>พฤษษณฑ</b> ณษณฑ	0.558 0.588 0.540 0.296 0.441 0.549 0.441 0.549 0.425 0.425 0.549	0.114 0.185 0.238 0.121 0.160 0.117 0.167 0.114 0.118

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					MEGSHEEM	ENTS FOR DF	LASER SC	JURCE
TABLE	2.2 OF	LINE BY L	INE LASER	EXTINCTIO	MOR GAIN	STAT GAIN	TRANS E	× COEF
DATE 2147777 2147777 2147777 2147777 2147777 2147777 2147777 2147777 2147777 2147777 2147777 21477777 21477777 21477777 2147777777777	TIME 1146 1147 1149 1151 1153 1156 1159 1201 1203 1349 1342 1344 7 1344 7 1354 7 1352 7 1354	BUN CODE 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	LASER 333333333333333333333333333333333333	LINE 10 P02-08 P02-07 P01-07 P01-07 P02-08 P02-08 P02-08 P02-08 P02-08 P02-08 P02-08 P02-08 P02-08 P02-08 P01-07 P02-08 P01-07 P02-08 P01-07 P02-08 P02-12 P02-12 P02-12 P02-12 P02-12 P02-12 P02-12 P02-12 P02-12 P02-12 P02-12 P02-08	555764444464444664	សលលាលជាងសាលាលាល សាលាលាល សាលាលាកាតា សាលាលាលាល	0.382       0.32695       0.33842       0.33891       0.6691       0.64655       0.6529       0.6685       0.6686       0.6638       0.616	0.188 0.263 0.263 0.209 0.073 0.072 9.149 0.071 0.124 0.074 0.074 0.074 0.074 0.074 0.069 0.161 0.082 0.217 0.200 0.100 0.151 0.103 0.095
	1221 1222 1223 1222 1223 1222 1223 1222 1223 1224 1227 1224 1227 1224 1227 1224 1227 1244 144 144 144 1477 144 1477 144 1477 144 1477 144 1477 144 1477 144 14777 144 14777 144 14777 144 14777 144 14777 144 147777 144 147777 144 147777 144 1477777 144 1477777 144 14777777 144 14777777 144 147777777777	33333333333333555555555555555555555555	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	P02-08 P02-05 P01-08 P01-08 P01-08 P01-08 P02-01 P02-0 P02-0 P02-0 P02-0 P02-0 P01-6 P01-6 P01-6 P01-6 P01-6 P01-7 P02- P01-7 P02- P02- P02- P02-	47476744644757674464	លហាមសេសមាលមេង សាល់សាសសាល	0.673 0.439 0.527 0.527 0.527 0.556 0.456 0.567 0.567 0.567 0.568 0.416 0.517 0.513 0.5513 0.643 0.643 0.643 0.645	0.161 0.076 0.219 0.084 0.138 0.079 0.135 0.090 0.079 0.082 0.171 0.082 0.171 0.0224 0.075 0.130 0.089 0.137 0.086 0.092
	4477 14 4477 11 44777 1 44777 1 44777 1 24777 1 24777 2 24777 2 2477777 2 24777 2 247777 2 247777777777	047     3       0452     3       053     3       057     3       059     3       1003     3       1102     3       1103     1344       13443     1346       13445     1346       1345     1355       1355     1355       1355     1356	333999999999999999999999999999999999999	P02- P02- P01 P01 P01 P01 P01 P01 P02 P02 P02 P02 P02 P02 P02 P02 P02 P02	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	33478735377	0.335 0.352 0.542 0.542 0.542 0.542 0.542 0.5540000000000	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

TABLE	2.2 OF	LINE BY L	INE LASER	EXTINCTIO	on measurem	ents for df	LASE	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
25777 25777 25777 25777 25777 25777 25777 25777	1036 1035 1036 1133 1134 1136 1139 1140		*****	P02-08 P02-07 P02-05 P01-06 P02-08 P02-12 P02-10 P02-08	ちちゅうぶっちち	4 4 4 4 4 5 4 4 5 4 4	0.590 0.370 0.339 J.448 0.536 0.589 0.468 0.587	0.103 0.194 0.211 0.157 0.104 0.103 0.148 0.104
TABLE	2.3 OF	LINE BY L	INE LASER	EXTINCTI	on measurem	ents for co	LASEI	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
16 <b>777</b> 16777 16777 16777	1620 1631 1636 1640	<b>3</b> 33 33 3	4 4 4	P05-09 P04-10 P04-09 P04-08	2 12 12 2	8 9 9	0.035 0.046 0.191 0 106	0.654 0.601 0.323 0.319
17 <b>Y77</b> 17 <b>Y77</b> 17 <b>Y77</b> 17 <b>Y77</b> 17 <b>Y77</b> 17 <b>Y77</b> 17 <b>Y77</b>	1247 1250 1254 1259 1301 1302 1303	<b>ស</b> .226.06.016	4 4 4 4 4 4 4	P04-09 P04-11 P05-11 P04-10 P04-10 P04-09 P04-08	8 8 8 8 8 8 8 8 8 8 8	<b>~~~~</b> ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	0.004 0.007 0.004 0.010 0.010 0.047 0.048	1.091 0.957 1.078 0.899 0.899 0.597 0.593
23Y77 23Y77 23Y77 23Y77	1148 1150 1156 1200	3333	4444	P04-09 P04-08 P04-10 P05-09	12 12 12	9 9 9	0.113 0.121 0.021 0.015	8.425 0.413 8.759 0.818

TABLE	2.4 OF	LINE BY L	INE LASER	EXTINCTIO	n measureme	ENTS FOR CO2	LASER	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
00000000000000000000000000000000000000	1119 1120 1121 1123 1125 1127 1128 1130 1134 1139 1139 1139 1142 1143 1145 1146 1151 1158 1203 1204	นผนผนผนผนผนผสสสสสสสสสส	ໞໞຑຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬ	P10-20 P10-30 P10-38 P10-14 P10-06 R10-20 R10-20 R10-22 R10-22 R10-22 P02-20 P02-22 P02-32 P02-23 R02-08 R02-08 R02-08	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	222322222211111111111111111111111111111	0.5673 0.6644 0.535122 0.6665 0.6665 0.66619 0.66619 0.6625 0.6625 0.6625 0.6425 0.6425 0.5356 0.6425 0.5356 0.5236 0.5536 0.55566 0.55566 0.55566 0.55566 0.55566 0	0.111 0.096 0.068 0.122 0.106 0.081 0.094 0.558 0.087 0.167 0.090 0.181 0.159 0.181 0.121 0.202 0.162 0.129 0.282 0.137 0.121
081777 081777 081777 081777 081777 081777 081777 081777 081777 081777 081777 081777 081777 081777 081777 081777 081777 081777	$\begin{array}{c} 1018\\ 1019\\ 1029\\ 1022\\ 1024\\ 1025\\ 1026\\ 1026\\ 1026\\ 1026\\ 1026\\ 1026\\ 1026\\ 1026\\ 1026\\ 1026\\ 1026\\ 1026\\ 1026\\ 1044\\ 1046\\ 1046\\ 1046\\ 1046\\ 1046\\ 1050\\$	๛๛๛๛๛๛๛๛๛๛๛	សសសសភាសភាសភាសភាសភាសភាសភាសភាភាភាភាភាភាភា	P10-20 P10-26 P10-30 P10-14 P10-10 P10-06 R10-20 R10-28 R10-28 R10-28 R10-28 P02-26 P02-26 P02-26 P02-26 P02-20 R02-20 R02-28 R02-28 R02-28 R02-28 R02-28 R02-28 R02-28	~~~~®©©©©©©©©¶¶¶©©©©©	<b>ଡ଼ୢୄୢୠଡ଼ଡ଼ୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄୄ</b>	0.389 0.417 0.251 0.374 0.393 0.4450 0.113 0.4460 0.241 0.241 0.241 0.241 0.241 0.241 0.240 0.340 0.2404 0.2402 0.2404 0.2402	0.184 0.171 0.162 0.270 0.192 0.182 0.188 0.144 0.426 0.426 0.278 0.2111 0.225 0.2111 0.274 0.246 0.205 0.180 0.428 0.178
091777 091777 091777 091777 0917777 0991777 09917777 09917777 09917777 09917777 09917777 09917777 09917777 09917777 099177777 099177777	1512 1513 1515 1517 1519 1520 1521 1522 1524 1525 1526 1527 1536 1537 1538 1541 1552 1553 1554	<u>พพพพพตตตตตตตตตตต</u> ต	ຑຉຬຉຑຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬ	P10-29 P10-30 P10-38 P10-14 P10-10 P10-06 R10-20 R10-20 R10-20 R10-20 P02-20 P02-22 P02-14 P02-20 P02-20 P02-20 R02-20 R02-20 R02-20 R02-20 R02-20 R02-20 R02-20 R02-20 R02-20 R02-20 R02-20 R02-20 R02-20 R02-20 R02-20 P0	77798887857655555557F	<b>ᲣᲣᲣᲑᲢᲢᲢᲢ</b> ᲑᲑ ᲑᲔᲝᲪᲪᲐᲓᲓᲐᲓ	0.313 0.343 0.343 0.357 0.364 0.311 0.359 0.413 0.0075 0.444 0.265 0.287 0.203 0.203 0.274 0.335 0.2720 0.3720	0.227 0.203 0.201 0.197 0.228 0.219 0.200 0.219 0.200 0.191 0.322 0.086 0.259 0.244 0.211 0.312 0.278 0.278 0.278 0.253 0.214 0.510 0.251
TABLE	2.4 OF	LINE BY L	INE LASER	EXTINCTIO	n measurem	ENTS FOR CO2	LASER	SOURCE
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DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
10477 10477 10477 10477 10477 10477 10477 10477 10477 10477 10477 10477 10477 10477 10477 10477 10477 10477 10477	1349 13554 13556 13559 14896 14496 14413 14426 14445 14448 14452 14448 14526 14448 14526	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	ໞໞໞໞໞຑຨຑຨຬຨຬຨຬຨຬຨຬ	P10-29 P10-30 P10-20 P10-20 P10-20 P10-10 P10-06 R10-20 R10-20 R10-20 R10-20 R10-20 R10-20 R10-20 P02-20 P02-20 P02-20 P02-20 P02-20		๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	$\begin{array}{c} \textbf{8.188} \\ \textbf{0.214} \\ \textbf{0.203} \\ \textbf{0.203} \\ \textbf{0.169} \\ \textbf{0.206} \\ \textbf{0.169} \\ \textbf{0.206} \\ \textbf{0.206} \\ \textbf{0.206} \\ \textbf{0.236} \\ \textbf{0.2361} \\ \textbf{0.2361} \\ \textbf{0.168} \\ \textbf{0.2361} \\ \textbf{0.168} \\ \textbf{0.168} \\ \textbf{0.168} \\ \textbf{0.1432} \\ \textbf{0.143} \\ \textbf{0.143} \end{array}$	0.326 0.301 0.307 0.311 0.503 0.347 0.325 0.309 0.4496 0.2884 0.2884 0.2884 0.3337 0.3488 0.3348 0.3388 0.3388 0.3388 0.3388 0.3388 0.3388 0.3388 0.3388 0.3388
11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77 11M77	1486 1412 1414 1415 1418 1418 1419 1421 1428 1428 1428 1430 1431 1433 1434 1435 1444 1445 1446	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	ຎຎຎຒຎຎຎຎຎຎຎຎຎຎຎຎ	F10-20 F10-20 F10-20 F10-30 F10-38 F10-38 F10-14 F10-10 F10-28 R10-28 R10-28 R10-28 R10-28 R10-28 R10-28 R02-28 F02-32	118899888687655664484	<b>ព</b> ្រសសសម្ភាណពាក់ កំណូលិស្តាលក្មស្នាល	0.142 0.147 0.158 0.167 0.161 0.161 0.144 0.152 0.375 0.072 0.183 0.208 0.208 0.245 0.250 0.239 0.239	0.381 0.3760 0.3556 0.3556 0.3569 0.3569 0.3558 0.31915 0.3325 0.3325 0.33274 0.3305 0.3356 0.3356 0.3357 0.35777 0.35777 0.35777 0.35777 0.357777 0.35777777777777777777777777777777777777
12177 12177 12177 12177 12177 12177 12177 12177 12177 12177 12177 12177 12177 12177 12177	1428 14231 1432 14334 14334 14446 144469 14453 14455 14555 14555 14555 14555 14555	าตนตลอนและเพราะเพราะ	<b>ຎຑຑຑຑຑຑຑຑຑຑຑຑຑຑຑຑຑຑ</b>	P10-20 P10-30 P10-38 P10-38 P10-38 P10-38 P10-38 R10-22 R10-22 R10-22 P002-34 P002-34 P002-34 P002-34 P002-34 P002-32 P002-32 P002-32 P002-32 P002-30 P002-32 P002-30 P00-30 P00-30 P100-30 P002-30 P0	<b>֎֎֎֎֎֎֎֎֎ՠՠՠՠՠՠՠ</b>	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	0.482 0.5143 0.524 0.524 0.574 0.574 0.574 0.574 0.574 0.681 0.217 0.681 0.259 0.6217 0.598 0.596 0.596 0.596 0.596 0.598 0.595 0.59	8.142 8.130 8.119 9.126 9.126 9.109 0.063 0.075 0.293 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.085 0.067 0.085 0.067 0.085 0.067 0.0720 0.0720 0.0720000000000

TABLE	2.4 OF	LINE BY L	INE LASER	EXTINCTIO	MEASUREM	ENTS FOR CO2	LASER	SOURCE
DATE	TIME	RUN CODE	LASER	LINE 1D	MOB GAIN	STAT GAIN	TEANS	EX COEF
11111111111111111111111111111111111111	$\begin{array}{c} 1150\\ 1151\\ 1155\\ 1155\\ 1155\\ 1155\\ 0122\\ 020\\ 022$	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	ໟໟຨຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬຬ	$\begin{array}{l} P10-26\\ P10-38\\ P10-38\\$	๛๛๛๛๛๛ <mark>๛</mark> ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	<b>ຑຑຑຆຎຑຑ</b> ຎຑຑຑຑຑຑຑຑຌຆ <b>ຬຬຆຑຑຑຑຌຌຌຌຌຌຌຌຌຌຌຌຌຌຌຌຌຌຌຌຌຌ</b>	9.5.6.5.4.6.3.3.5.4.3.5.4.1.9.4.8.5.4.7.6.7.3.8.1.7.5.6.7.2.9.8.5.0.9.4.1.3.4.4.5.5.4.4.5.5.6.7.2.9.8.5.0.9.4.1.3.4.4.5.5.4.4.5.5.6.7.2.9.8.5.0.9.4.1.3.4.4.5.5.4.4.5.5.4.4.5.5.6.7.2.9.8.5.0.9.4.1.3.4.4.5.5.4.7.6.7.3.8.1.7.5.6.7.2.9.8.5.0.9.4.1.3.4.4.5.5.4.7.6.7.3.8.1.7.5.6.7.2.9.8.5.0.9.4.1.3.4.4.5.5.4.7.6.7.3.8.1.7.5.6.7.2.9.8.5.0.9.4.1.3.4.4.5.5.4.7.6.7.3.8.1.7.5.6.7.2.9.8.5.0.9.4.1.3.4.4.5.5.4.7.6.7.3.8.1.7.5.6.7.2.9.8.5.0.9.4.1.3.4.6.6.6.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	$\begin{array}{c} \textbf{0.1399} \\ \textbf{0.14990} \\ \textbf{0.1459} \\ \textbf{0.1459} \\ \textbf{0.1459} \\ \textbf{0.1459} \\ \textbf{0.1459} \\ \textbf{0.1424} \\ \textbf{0.1453} \\ \textbf{0.1424} \\ \textbf{0.1423} \\ \textbf{0.1424} $
15M777 15M777 15M777 15M777 15M777 15M777 15M777 15M777 15M777 15M777 15M777 15M777 15M777 15M777 15M777 15M777	906789 9089 911244 9129911299 911299 911299 91224 9228 9224 9228 933124 933324 933324	<b>สสลดเสลตลอดส</b> ดเลสส	ຑຬຑຬຑຬຑຬຑຬຑຬຑຬຑຬຑຬ	P10-20 P10-26 P10-33 P10-33 P10-14 P10-10 F10-06 R10-34 R10-28 R10-28 R10-28 R10-28 R10-20 P02-20 P02-20 P02-20 R02-20 R02-20 R02-20 R02-20	87776000020000000000000	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	0.3405 3405 0.4459 0.45590000000000000000000000000000000000	8.193 8.177 8.1761 0.214 0.214 8.187 9.172 1.006 0.152 0.1664 0.255 0.2664 0.255 0.2664 0.255 0.2665 0.2550 0.25550 0.25550 0.25550000000000

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TABLE	2.4 OF	LINE BY L	INE LASER	EXTINCTIO	n Measurem	ENTS FOR CO2	LASER	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	ex coef
01477 01477 01477 01477 01477 01477 01477 01477 01477 01477 01477 01477 01477 01477 01477 01477 01477	1450 14551 14522 14553 14555 14555 14502 1508 15086 15086 15086 15086 15089 1511	444474 14474444444444	សមានសមានសម្លានក្នុងសមាន ក្លាយក្លានក្លាយក្លាយក្លាយក្លាយក្លាយក្លាយក្លាយក្លាយ	P10-20 P10-30 P10-38 P10-14 P10-10 P10-06 R10-34 R10-26 R10-34 R10-26 P02-20 P02-20 P02-226 P02-22 P02-214 P02-20 R02-28 R02-28 R02-28 R02-28	10 13399888797769666666 106	๚๚๛๚๛๛๚ <u>๛</u> ๛๛๛๛๛	$\begin{array}{c} 0.121\\ 0.138\\ 0.138\\ 0.146\\ 0.138\\ 0.146\\ 0.138\\ 0.146\\ 0.158\\ 0.194\\ 0.175\\ 0.154\\ 0.154\\ 0.160\\ 0.178\\ 0.160\\ 0.133\\ 0.219\\ 0.202\\ 0.$	<b>0.4190</b> <b>0.33876</b> <b>0.33876</b> <b>0.33760</b> <b>0.335200</b> <b>0.3535200</b> <b>0.3535200</b> <b>0.35353500</b> <b>0.35353500</b> <b>0.35353500</b> <b>0.35353500</b> <b>0.35353500</b> <b>0.35353500</b> <b>0.35353500</b> <b>0.35353500</b> <b>0.35353500</b> <b>0.35353500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535500</b> <b>0.3535900</b> <b>0.3535900</b> <b>0.3535900</b> <b>0.3535900</b> <b>0.3535900</b> <b>0.35359000</b> <b>0.35359000000000000000000000000000000000</b>
020777 020777 020777 020777 020777 020777 020777 0207777 0207777 0207777 0207777 02077777 020777777 02077777777	$\begin{array}{c} 1249\\ 1250\\ 1251\\ 1252\\ 1255\\ 1255\\ 1255\\ 1255\\ 1255\\ 1255\\ 1255\\ 1255\\ 1255\\ 1255\\ 1255\\ 1255\\ 1306\\ 1308\\ 1438\\ 1438\\ 14438\\ 14448\\ 1445\\ 14458\\ 1455\\ 15$	ми	ស្រសាសសាលាសាសាសាសាសាសាសាសាលាក្នុងសាលាក្នុងសាលាក្នុងសាលាក្នុងសាលាក្នុងសាលាក្នុងសាលាក្នុងសាលាក្នុងសាលាក្នុងសា	260 210-23 2	൭ൕൕൕൕൕൕൕ൹൹൹൹ൕൕൕൕൕൕൕ൹൹൹൹൹൹൹൹ൕൕൕൕൕൕൕൕൕൕൕ	សលាលជាជាលាកស្នាលាក្នុងជាក្មស្នាលលោកសាលាលាលក្មាណកាលកាលកាលកាលកាលកាលកាលកាលកាលកាលកាលកាលកាលក	0.126 0.12648 0.12648 0.12648 0.12648 0.1265 0.00000 0.00000 0.000000	5660326292845983552295348009271772718806867923 488614885648845983523542748526835836431644108667923 4886148856455373388287724452683564355535838435 90000001100000000000000000000000000000

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TAPLE	2.4 OF	LINE BY L	INE LASER	EXTINCTIO	n measurem	ENTS FOR CO2	LASER	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EX COEF
34477	1107	3	5	P10-20	8	5	8.131	0.397
04A77	1100	3	5	P10-30	8	5	0.140	0.368
8-4977	1110	3	5	P10-38	8	5	0.154	0.365
04877	1110	3	5	P10-14	8	5	0.132	0.395
04477	1113	3	รี	P10-06	8	รั	0.175	0.341
0-1477	1113	3	5	R10-34	, é	4	0.222	0.294
04977 94977	1113	NC N	5	R10-20 R10-28	12	1	0.000	0.313
94877	1119	ž	š	110-12	ě	4	0.056	0.563
94477	1120	2	5	R10-06	ê	5	0.173	0.343
04477 04877	1123	3	5	P02-26	5	ž	0.210	0.305
04H77	1124	3	Š	P02-32	ŝ	Ž	0.228	0.289
04877 04077	1125	3	54	FU2-14 P02-08	5	22	8.161	8.357
U4A77	1127	3	Š	R02-20	š	ž	0.224	0.292
04077	1129	3	5	R02-28	4	2	0.261	0.262
04877	1130	3	5	R02-08	4	2	0.024	0.271
04077	1582	4	ŝ	P10-38	10	7	0.143	0.379
84877 94027	1586	<b>ब</b> त	5	P10-30 P10-26	9	6	0.142	0.381
04A77	1509	4	รี	P10-20	š	ě	0.120	0.413
34477	1512	्यू	5	F18-14	9	5	0.123	0.489
94A77	1514	4	5	P10-06	8	5	0.136	0.350
94977	1517	4	5	P10-20	8	5	0.121	0.413
04077	1519	4	2	R10-06 R10-12	8	5	0.162 0.052	0.355
94677	1528	4	š	R10-28	17	4	0.186	0.328
94977	1530	4	5	R18-34	7	4	0.197	0.318
04477	1534	4	5	P02-32	7		0.120	0.311
04077	1549	4	5	P02-26	6	3	0.185	0.330
94877	1551	4	25	P02-20 P02-14	6	3	0.172 0.145	8.344
84977	1555	4	ŝ	P02-08	ē	3	0.183	0.332
04077	1558	4	5	R02-08	6 0	3	9.212	0.303
04A77	1682	4	รั	R02-08	6	3	0.204	0.310
84977	1605	4	5	R02-14	9	3	0.019	0.771
04477	1618	4	5	R02-28	5	ź	0.191	0.323
04477	1615	4	5	F10-20	8	5	0.110	0.431
35077	1500	5	F	D10-00	٥	~		<b>0</b>
95A77	1503	33	5	P10-26	8	6	0.387 0.456	0.185 0.154
05A77	1584	3	5	P10-30	8	Ğ	0.491	0.145
05H77 05A77	1505	3	5	P10-38 P10-14	87	7	0.517	C.129
05A77	1507	3	š	Pið-ið	7	6	0.413	0.160
95877	1508	37	5	P10-06	7	6	0.510	0.132
<b>85A77</b>	1510	ž	ž	R10-20	12	4	0.004	0.115
USA77	1512	3	5	R10-28	6	5	0.508	0.132
05A77	1514	23	5	R10-12 R10-06	7	5	0.253	0.268
95677	1516	3	5	P02-20	5	Š	0.367	0.196
05877	1517	33	5	P02-26 P02-22	5	3	0.391	0.183
05477	<b>i</b> 5i9	š	รั	P02-14	é	4	0.450	0.163
05A77 05077	1520	37	5	P02-08	6	4	0.336	0.213
05A77	1523	3	5	R02-20	5	उ	0.391 0.457	0.184
USA77	1524	3	5	R82-14	é	3	0.125	0.406
1 C. 1996 C. F.	1 7 7 7	•	-	ALC: N THE REAL PROPERTY AND A	<b>W</b> .	1		

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TABLE	2.4 OF	LINE BY L	INE LASE	R EXTINCTION	on measurem	ENTS FOR CO2	LASEF	SOURCE
DATE	TIME	RUN CODE	LASER	LINE ID	MOB GAIN	STAT GAIN	TRANS	EM COEF
16777 16777 16777 16777 16777 16777 16777 16777 16777 16777 16777 16777 16777	1458 1500 1501 1506 1515 1516 1517 1520 1522 1522 1525	เมณณณณณณณณณ เม	รรรรรรรรรรรรรร	$\begin{array}{c} P10-20\\ P10-30\\ P10-38\\ >10-10\\ R10-34\\ R10-12\\ P02-32\\ P02-32\\ P02-20\\ R02-20\\ R02-20\\ R02-28\\ R02-28\\ R02-28\\ R02-28\\ R02-28\\ R02-20\\ P10-20\\ P10-20\\ \end{array}$	78887955644848	๛๛๛๛๛๛๛๚๚๛๛๛	0.213 0.253 0.259 0.230 0.297 0.296 0.266 0.160 0.183 0.258 0.308 0.258 0.308 0.211 0.211	0.302 0.269 0.267 0.287 0.458 0.359 0.359 0.359 0.359 0.331 0.259 0.331 0.230 0.334 0.230 0.2354
17477 17477 17477 17477 17477 17477 17477 17477 17477 17477 17477 17477 17477 17477 17477	1451 1501 1504 1508 1513 1529 1535 1552 1559 1607 1611 1612 1614 1620 1627	88888888888888888888888888888888888888	ໞຑຑຑຑຑຑຑຑຑຑຑຑຑ	P10-20 P10-38 P10-30 P10-20 R10-12 R10-20 R10-34 P02-32 P02-32 P02-08 R02-08 R02-08 R02-20 R02-20 R02-20	88 19 8772765558547	587655454 <b>MBMBM</b> 80	0.208 0.248 0.210 0.229 0.229 0.210 0.229 0.305 0.305 0.305 0.305 0.305 0.308 0.308 0.308 0.308 0.308 0.308 0.308 0.320 0.271 0.320 0.2219	0.307 0.264 0.272 0.305 0.2881 1.235 0.3491 0.255 0.319 0.255 0.319 0.255 0.252 0.2257 0.227
244777 244777 244777 244777 244777 244777 244777 244777 244777 244777 244777 244777 244777 244777	1429 1434 1435 1437 1438 1449 1454 1455 1456 1456 1456 1458 1458 1458	88888888888888888888888888888888888888	ຑຑຑຑຑຑຑຑຑຑຑຑຑຑ	P10-20 P10-30 P10-38 P10-20 P10-10 R10-34 R10-34 R10-22 R10-12 P02-32 P02-32 R02-28 R02-28 R02-28 R02-28	១១១១១១ឧ <b>ខា្លទទទ</b> ទភភភភភ	<b>ภภภภภภภ 4 4 ภ</b> พพงงงง	0.084 0.098 0.180 0.084 0.084 0.142 0.071 0.142 0.071 0.142 0.071 0.142 0.071 0.151 0.151 0.151 0.151 0.194 0.178	0.483 0.453 0.445 0.485 0.485 0.487 0.381 0.517 0.687 0.358 0.418 0.369 0.326 0.326 0.321 0.338
255777 255777 255777 255777 255777 255777 255777 255777 255777 255777 255777 255777 255777 255777 255777 255777 255777 255777	857 859 900 900 911 914 912 922 923 924 922 922 922 922 922 922	๛๛๛๛๛๛๛๛๛๛๛	ໞຑຑຬຬຨຎຬຑຠຑຑຑຑຑ	P10-20 P10-30 P10-38 P10-20 P10-38 P10-38 P10-38 P10-38 P10-38 R10-12 P02-34 R10-12 P02-34 R02-28 R02-28 R02-28 R02-28	10 10 10 10 10 10 10 10 10 10 10 10 10 1	00007700077001 01000	0.063 0.077 0.099 0.115 0.117 0.108 0.126 0.126 0.140 0.140 0.181 0.237 0.181 0.237 0.181	0.539 9.515 0.501 0.422 0.419 0.435 0.339 0.342 0.3384 0.3384 0.3350 0.3381 0.3534 0.3350 0.3381 0.3281 0.3281

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Table 3.1. Aerosol extinction coefficients derived on the basis of contrast attenuation measurements at the Cape Canaveral shore (see Fig. 3.1 for path definition).

0.246

0.101

174 PATH MAVE LENGTH LENGTH (RM3 (MTCMDN) 3820 EXTENCTEMN THEF L\*CAL 77#t 45 MAH 77 33 MAH 77 38 MAH 77 31 MAH 77 31 MAH 77 35 MAH 73 35 MAH 73 33 MAH 77 33 MAH 77 33 MAH 77 PATH WAVE EXTENCTION LENGTH LENGTH (DEFF. CKH3 CHTCHON3 C/RH3 DATE (/.\*) 1500 1550 1517 1.08 0.4010 0.4010 0.4158 1.0H 0. 140 0.118 17 MAK 17 17 MAH 77 17 MAH 77 17 MAK 17 17 MAK 17 17 MAK 17 17 MAK 17 18 MAK 17 19 MAK 17 MAK 17 1540 1504 1520 1547 1507 1524 1544 1510 1529 1514 1514 0.415M 0.4500 0.5050 0.5164 0.5200 0.5461 0.5770 0.5461 0.5770 0.4200 0.4200 0.4200 0.4200 0.612M 0.612M 100/ 5.08 4.0H 1101 0.4050 0.174 4.0A 5.08 0.118 0.4010 0.180 \*.0+ \*.0+ \*.0H 104# 4.08 0.4100 0.4480 0.5050 0.5144 0.5200 -0.298 0.289 0.289 ii 11 12 MAN 37 1.08 1.08 1.05 0.171 1010 1012 1015 1015 1039 1045 1017 1041 13 MAW 77 13 MAW 77 14 MAW 77 13 MAW 77 11 0.101 1.08 1.08 0.245 0.245 0.245 0.346 0.345 0.365 0.365 0.285 0.142 -08 -08 -08 0.14+ 4.08 0.1461 1.0# 5.0# 5.0# 0.166 0.544A 0.6500 0.6200 0.6228 1.0# 0.166 1554 1500 1517 1504 1504 1504 1520 1542 1045 0.140 0.140 0.140 1-0# 1-0# 0.6443 0.4050 0.4158 0.111 1107 4.08 5.08 5.08 7.51 7.51 0.41) 0.41) 0.420 0.198 0.6124 0.6441 7.6441 7.4050 0.4050 0.146 0.146 0.146 0.214 0.226 0.4100 1007 12 MAH 77 12 MAH 77 12 MAH 77 0.1010 11 MAN 77 1011 1048 1010 1016 1042 1014 0.408 2.51 2.51 2.51 2.51 2.51 2.51 2.51 1507 1574 1544 1510 1529 1538 1514 1549 1549 1541 1511 1540 0.4050 0.458 0.450 0.4888 0.5050 0.5145 0.5200 0.5461 0.5770 12 MAR 17 13 MAR 17 14 MAR 17 14 MAR 17 15 MAR 17 15 MAR 17 16 MAR 17 17 MAR 17 18 MAR 17 19 MAR 17 0.219 0.212 0.146 0.204 0.204 0.204 0.5200 0. 176 0. 194 0. 194 0. 198 0.5461 0.5770 0.5770 11 MAN 12 MAN 13 MAN 11 MAN 13 MAN 17 2.57 2.57 2.57 2.57 2.57 1.28 1.28 1.28 0.4894 0.4000 0.4200 P.4324 P.4324 P.4324 11111 0.198 0.470 0.470 0.198 0.411 0.426 1019 0.214 1011 D.247 D.247 D.235 0.5846 0.6000 31 MAH 21 MAH 21 MAH \*\* MAN 77 MAN 77 MAN 77 MAN 77 MAN 77 1045 1020 1106 1057 1110 0.40.0 0.4010 0.4010 0.4118 0.4158 0.4580 0.644 0.6328 0.6328 0.6328 0.6328 0.240 0.212 0.242 0.242 11 1.28 1.28 1.28 1.28 1.28 1.28 1.28 3340 1504 1520 1542 1507 1524 1564 1564 MAN 22 MAN 22 MAN 22 MAN 22 MAN 22 MAN 22 11 0.641 0.4880 0.5050 0.5145 0.5200 0.4461 0.5270 0.5886 0.4441 1007 0.102 1.28 1.28 1.28 0.678 0.678 0.674 0.4050 0.4050 0.4358 0.268 0.274 0.274 11 1013 104# 1010 1036 1052 1055 1055 1055 1055 1055 1041 1041 1045 7030 0.424 0.641 0.647 0.877 0.824 0.607 0.647 \*\*\* \*\*\* \*\*\* \*\*\* 0.4500 0.4880 0.5050 11 0.246 11 ii ii 11 11 1510 1524 1514 1514 1558 0.7446 0.4000 0.4200 0.4328 0.4328 0.5050 0.5145 0.5200 0.5461 0.5770 0.5846 ;;; ;;; ;;; 11 11 17 MAH 37 17 MAH 37 0.748 0.4941 17 PAN 17 PAN 17 PAN 17 0.011 0.6000 0.6200 0.6328 0.6328 0.274 0.26H 17 MAH 17 12 MAH 17 12 MAH 72 12 MAH 72 17 MAH 77 1020

12

10%7

1.28

0.6943

3

Table 3.1.( continued )

91AC	L PCAL TIN	L PATH E LENGTH	WAVE LENGTH	EXTINCTION					
		(KH) (	PICPONS	LOFFF.	DATE	4.00	AL PATH	NAME	
14 MAR 1	17 847			(/			ME LENGTH	LENGTH EXTINCT	Ľ
24 HAR 7	7 931	5.08	0.4050	0.144			<pre>{KH}</pre>	(RICROW) COEFF.	•
14 MAR 7	7 907	2+08	0.4050	0.140	24 HAR	77 16		(/(4)	)
14 MAR 7	7 920	2.08	4.4 358	0.134	14 HAR	17 14	5+08	0.4050	
AN MAR 7	7 152	5.04	2.4500	0.140	14 MAR	77 154	5-08	0.4050 0.157	<u>/</u>
IN MAR 2	1 910		2+4880	0.114	14 HAR	17 150	5-08	0.4358 0.153	
34 HAR 1	922	5.00	.5050	0.121	14 HAN	77 167	\$ 5+08	0.4500	1
14 748 71	856	5.08	1+5145	0.125	14 MAR	77 154	5-08	0.4880 0.12	
14	912	5.04	-2200	9.114	14 MAN	17 155	-08	0.5050	
14 848 77	925	5.00	-5461	0.171	24 ####	17 151	2.08	0-5145 0 110	
14 14 14	900	5.04	.5770	0.133	LA HAR I	17 154	2-08	0.5200	
14 144 77	915	5.00	+5896	0-129	14 HAR 7	7 1541	- 08	0.5461 0.135	
14 848 55	917	5.04	- 6000	0-136	19 748 7	7 1534	2.08	0.5770 0.175	
A BAR SS	703	5-08	• 6 2 0 0	0.125	14 MAN 7	7 1604	2.08	0-5#96 0-143	
14	933	5-04	6328	0.121	LA MAR 7	7 1547	2.08	0-5896 0-147	
14 man 35	928	5.00	6328	0-140	24 148 7	7 1548	74.08	0.6000 0.151	
14 MAR ST	938	5.00	6943	0.155	LA MAR Y	1 1537	7-08	0.6200 0.140	
14 HAN 33	847	2.57	6943	0.157	19 HAR 71	1400	2+08	0.6328 0.143	
14 848 33	930	2.57 .	4050	0.150	14 HAR 11	1608	7+08	0.6943 0.176	
14 RAH 12	907	2.57 0	9050	0.162	IN MAR YY	1525	7.08 (	0.6943 0.207	
14 848 33	920	2.57	7338	0.150	14 14 77	1602	2 6 7 1	-4050 0-192	
14	#52	2.57	->00	9-156	14 48 77	1540	2 8 7	-4050 0.184	
14 MAN 22	910	2.57	000	0.133	14 488 97	1552	2.61	4358 0.142	
14 840 77	\$55	2.57 0	920	0.150	14 MAR 77	1529		-4500 0-192	
14 BAR /2	856	2.57 0.0	243	0.150	14 848 77	1542	2.57 0	4880 0.212	
14 MAR 33	712	2.57 0.5	441	0.139	14 944 55	1555	2.57	-5050 0.128	
14 MAR 77	725	2.47 0.5	770	0.150	14 848 33	1532	2.57	-5145 0-112	
14 848 77	100	2.57 0.6		0.174	14 848 55	1545	2.57	-5200 0.150	
14 HAR 77	715	2.57 0.6	000 (	-156	14 844 35	1557	2.57	3461 0.150	
14 MAR 77	717	2.57 0.4	200	-180	14 848 33	1534	2.57	5770 0-156	
14 HAN 77	903	2.57 0.6		-168	14 RAN 13	1405	2.57	2876 0.199	
24 868 77	¥ 14	2.57 0.61	128	-162	14 948 77	1547	2.57 .	3876 0.192	
14 MAH 77	728	2.57 0.69	4.2	•174	14 848 22	1548	2.57 .	0.205	
14 HAH 77	737	2.57 0.69	43 0	• 205	14 848 72	15 37	2.57 0.	6778 0.199	
14 HAR 77	897	1.28 0.40	50 0	-212	14 MAR 37	1600	2.57 0	69.28 0.226	
14 MAH 77	907	1.28 0.40	So a	174	14 PAR 77	1607	2.57 0.	0.186	
14 HAR 77	930	1.28 0.43	58	1 /4	14 HAR 77	1525	1.28 0.4	0.247	
14 HAH 77	852	1-28 0-45	00 0	107	14 MAR 17	1001	1-28 0.4	0.279	
14 MAR 77	910	-28 0.48	10 0	124	14 HAR 77	1540	1.28 0.4	15.0 0.312	
14 MAR 77	122	-26 0.505	0 0.	144	14 MAR 77	1352	1.25 0.4	500 0.302	
24 HAR 77	854	-28 0.514	5 0.	144	14 HAR 77	1579	1.28 0.4	880 0.373	
14 HAR 77	122	-28 0.520	0 0.	1 7 7	14 MAR 77	1665	1.28 0.5	050 0.214	
14 MAH 77	925	-28 0.546	1 0.	136	24 MAR 17	1533	1.28 0.5	45 0.214	
14 HAH 77	900	. 0.577	9 0.1	150	14 RAN 77	2545	1.28 0.5:	200 0.105	
14 MAK 77	915		6 0.1	34	14 MAR 77	1582	1.28 0.50	61 0 175	
	117 1	0.6001	0.1	46	14 MAH 77	1514	1.28 0.57	70 0.235	
	903 1	0.620(	0.1	36	14 HAR 77	1547	1-28 0.58	96 0 143	
	935	0.6321	0.1	74	14 MAR 77	1544	78 0.60	00 0 000	
· · ··································	228 1	0-6324	0.1	74	14 MAR 77	1517		00 0.274	
· · ## 77	976	28 0.6943	0.1	55	14 MAP 77	1606		28 0.270	
	••	··· V.0443	· · ·	65	24 RAR 27	1600	. 63 0.63	28 0.747	
			-		14 PAK 77	1604	64	0.214	
						I	+28 0.694	3 0.252	
								71	

Table 3.1.(continued)

		C.C.A.C.	PAIN	WAVE	EXTINCTION		1.00.41			
UAI	t	A I NE	LENGTI	4 LFNGTH	COFFE.	DATA	LOUME	PATH	WAVE	EXTINCTION
			(88)	CHICRONY	(///	UNIT	1 I ME	LENGTH	LENGTH	COEFF.
			• • •		(/=)			(K#)	CHICKON	67883
1 47	R 77	94.0	* **							
1 42	8 77	1071	2.00	0.4050	0.373	2 APR 77	839	5.04		
1 49		1051	2.08	0.4050	0.361	2 APR 77	924	5 00	0.4070	0.214
		1005	5.08	0.4358	0.327	2 APR 77		7.08	0.9050	0.214
1 47		1018	5.08	0.4500	0.307	2 APH 73	878	5-08	0+4354	0-192
1 40	F 77	953	5.08	0.4880	0.265		914	5.08	0.4500	0.192
1 AP	K 77	1005	5.04	3.5050	0 233	2 MP# 11	843	5.08	0.4880	0.158
1 AP	# 77	1021	6		0.213	2 MPR 77	100	5.08	0.5050	0.143
1 47	8 77	966		0+2145	0.265	2 APR 77	917	5.08	0.5145	
1 47	8 77	1010	2.00	0.5200	0.281	2 APH 77	844	5.08	0 5 300	V+128
1 40		1010	2+00	0.5461	0.237	2 APH 77	904	5 0.0	0.5200	0.190
1		1023	>-08	0.5770	0.237	2 499 77		2.08	V.3461	0.146
		777	5.08	0.5896	0.231	2 499 77	717	2.08	0.5770	0.146
1 471		1013	5.08	0.6000	0.244	2 484 33	0.20	5.08	0.5896	0.130
1 AP	1 77	1015	5.08	0-6200	0.207	2 AFR 77	907	5.08	0.6000	0.134
1 API	1 77	1002	5.08	0.4328	0.201	2 474 11	911	5.08	0.6200	0.134
1 471	1 77	1036	5.08	0 4330	V.201	2 APR 77	854	5.08	0.6328	0.123
1 AP1	1 77	1027		0.000	0.218	2 APK 77	928	5.08	0.6328	0.120
1 APP	1 77	1037	7.00	0.0793	0+218	2 APR 77	972	5.08	0.4943	0.130
1 47	77	1031	2.04	0+6943	0-218	2 APH 77	930	5 04	0.0743	0+1 34
1 484		748	2.57	0.4050	0.408	2 478 77		3.08	0.0441	0.138
		1032	2.57	0.4050	0.408	2 488 77	• > •	2.71	0.4050	0.254
1 479	11	1005	2.57	0.4358	0.398	2 484 77	729	2.57	0.4050	0.254
L APP	177	1018	2.57	0-4500	0.357		858	2.57	0.4358	0.233
1 AP4	177	953	2.57	0.4880	0.370	2 474 11	914	2.57	0.4500	0.240
1 дрн	177	100	2.57	0 5054	4.315	2 APR 77	843	2.57	0.4880	0.199
1 APR	77	1021	3 67	0 - 70 70	0.311	Z APH 77	990	2.57	0.5050	0.312
1 APR	77		2	0.2147	0.328	2 AP# 77	917	2.57	0 5145	0.212
1 49.8		777	2.57	0.5200	0.30Z	2 APK 77			V-7147	0.205
1 400		1010	2.57	0.5461	0.311	2 498 77		2.71	0.5200	0,199
1 474		1023	2.57	0.5770	0.319	2 488 77	704	2+21	4.5461	0.212
L AFR		759	2.57	0.5896	0.128	2 APH 33	717	2.57	0.5770	0.212
1 479	11	1013	2.57	0.45.40	0.311	3 49 5 47	420	2.57	0.5896	0.205
1 47#	77	1015	2.57	0-6200	0.284	2 454 77	907	2.57	0.6090	0.219
-1 APR	77	1002	2.57	0.4728	0.200	2 APR 17	911	2.57	0.6700	0.199
1 APR	77	1035	2.67	0.0320	V. 3V2	2 APR 77	854	2.57	0.4328	0.100
1 APR	77	1027	3 63	0.0328	0.311	2 AP# 77	928	2.57	0.4330	0.177
1 401	77	1074	(+)(	0+6943	0.311	2 APK 77	973		V-0328	0.219
1 400	77	1030	2.51	0.6943	0.328	2 AP# 77	936	2+71	0.0443	0.219
1		798	•24	0.4050	0.511	2 AP# 77		2	0.2793	0.219
		10.5	1.28	0.4050	0.526	2 APR 77		Lozo	0+4057	0.313
1 APR	11	1005	1.28	0.4358	0.496	2 444 13	878	1.28	0+4358	0.268
J APR	11	1018	1.20	0.4500	0.453		714	1.20	0.4500	0.290
I APR	77	953	1.28	0.4880	0 373	2 APR 77	843	1.28	0.4880	0.225
1 APP	77	1608	1.28	0.5050	0.373	2 AP# 77	900	1.28	0.5050	0.226
1 APK	77	1021	1 20	0.7070	0.399	2 APR 77	917	1.28	0.5145	0 344
1 APR	17		1.20	0.7197	0.399	2 APH 77	844	1.24	6 6 206	0.240
1 40-	77	1010	1.20	V-5200	0.361	2 AP# 77	904	1.20	- 7CUU	4.277
1	**	1010	1.28	0.5461	0.373	2 APR 77			U+7961	V-246
1 48-		1023	1.28	0.5770	0.386	2 494 22	717	1+20	9.5770	0.246
A	11	959	1.28	0.5896	0.399	2 488 24	870	1.28	0.5896	0.246
1 APR	77	1013	1.28	0. 6000	0.309	C =FR []	707	1.28	0-6000	0.246
1 APR	77	1015	1.24	8.6200	0.300	2 899 77	911	1.28	0.6200	0.225
1 APR	77	1002	1.20	6.4178	V. J. 77	2 APR 77	854	1.28	0.4328	0.235
1 APR	77	1034	1 34		V+ 377	2 AP# 77	922	1.28	0.6941	
1 428	77	1417		W+0325	0.386		-			***71
1 APR	77	1027	1-20	0.6943	0.399					
	• •	1937	1.28	0.6943	0.412					

Table 3.1.( continued )

	LOCAL	PATH	WAVE	EXTINCTION		LOCAL	PATH	MAVE	EXTINCTION
DATE	T I HE	LENGTH	LENGTH	COEFF.	DATE	TIME	LENGTH	FRACTH	CALEC.
		(K#)	CATCHON	} (/K#)			(K4)	(HICRON)	(/KH)
4 APP 77	846	5.08	0.4050	0.245	5 478 /7	960			
4 APR 77	977	5.08	0.4050	0.258	5 APN 77	1010	2.08	0.4070	0.204
4 APK 77	905	5.08	0.4358	0.226	5 APR 77	1027	7.08	9-9050	9.212
4 APR 77	918	5.08	0.4500	0.224	5 APR 77	1010	7.08	0.9178	0.187
4 478 77	84.9	5 00	0 4840	0.100	5 499 73	1020	7.45	0.4500	0.176
4 APR 77	907	5 00	0.4000	0 190	5 ADH 77	778	5.00	0.4880	0+185
4 488 77	977	5400	0.5030	0.170	5 484 33	1012	5.08	0.5050	0.176
A APR 77	713	7400	0.5147	0.190	5 400 33	1022	5.00	0.5145	0.146
4 APR 77		5.00	0.7200	0.170	5 499 77	1000	5.08	0-5700	0-162
4 498 77	907	5.00	0.7401	0.170	5 454 77	1014	5.08	0.3.51	0.176
A APH 77	722		0.5770	0.190	5 498 77	1029	5.08	0.57 0	0.196
A APR 77	700	5.08	0.3070	0.100	5 454 33	1003	5.00	0-589	0.185
4 488 33	912	5+08	0.6000	0+196	5 APR 11	1016	2.09	0-6900	0.207
4 APR 77	910	5.08	0.6200	0.171	7 AP# //	1017	5-08	0-6200	0.185
A ARR 77	903	5.08	0.6328	0.100	5 AFR 11	1006	5.08	0.6328	0.140
A APH 11		2.00	0-6328	0.176	5 AF# 11	1034	5.08	0.6328	0-190
A 888 77	7/0	2.08	0.6943	0.171	2 AF# 77	1026	5-00	0.6943	0.212
4 444 11	332	5.08	9.6741	9-176	5 AFK 11	950	2.57	0.4050	0.352
4 APK //	846	2.57	0.4050	0.246	5 AP# 77	1028	2.57	0-4050	0-366
4 400 37	428	2.51	0-4050	0.286	5 APR 77	1010	2.57	0.4358	0.357
4 NPX 11	705	2.57	0.4 158	9.286	5 AFR 77	1920	2.57	0.4500	0.34T
4 474 77	918	2.57	0.4500	0.270	5 APR 17	958	2.57	0-4880	0-320
4 474 77	849	2.51	0-4480	0.233	5 APR	1012	7.57	0.5050	0.338
-	401	2.57	0.5050	Q-247	5 APK 74	1022	2.57	0.5:45	0.408
A APR 17	920	2.57	0.5145	0.233	5 APR 77	1000	2.57	0.5200	0-357
	856	2.57	8-5200	0.219	5 AP# 77	1014	2.57	0-5461	0.408
4 APR 77	909	2.57	0.5461	0-240	5 APR 77	1024	2.57	0.5770	C.431
4 APR 77	922	2.57	0.5770	0.247	5 APH 77	1003	2.57	0-5896	0.387
4 AP# 77	900	2.57	0.5896	0.240	5 APR 77	1016	2.57	0-6000	0-456
4 APR 77	912	2.57	0-6000	0-240	5 APR 77	1017	2.57	0.6200	0.495
4 APR 71	916	2,57	0.9590	0.233	5 APR 77	1006	2.57	0.6328	0.431
4 AP# 77	903	2.57	0.6328	0.233	5 APH 77	1026	2.57	0-6943	0.495
4 APR 77	458	2.57	0.6328	0.240	5 AP# 77	950	1.28	0-4050	0.412
4 APR 77	926	2.57	0.6943	0.247	5 APK 77	1010	1.20	0.4358	0.325
4 APR 77	936	2.57	9.6943	0-210	5 APR 77	1020	1.28	0-4500	0.257
4 APH 77	846	1.28	0.4050	0.399	5 AP# 77	958	1.78	0.4880	0.247
4 APR 77	905	1.28	0.4358	0.373	5 APK 77	1012	1.28	0.5050	0.412
4 APN 77	849	1.28	0.4880	0.313	5 AP# 77	1072	1.28	0-5145	0.337
4 APR 77	918	1.28	0-4500	0.361	5 APR 77	1000	1.28	3-5200	6. 399
4 APR 77	907	1.28	0.5050	0.337	5 APR 77	1014	1.28	0.5461	0.386
4 APH 77	920	1.28	0.5145	0.301	5 AP# 77	1074	1.26	0.5770	0.279
4 AP# 17	856	1.28	8-5200	0.279	5 APK 77	1003	1.28	0.5876	0.439
4 AP# 77	909	1.28	0.5461	0.301	5 AP# 77	1016	1.28	0.6000	0.481
4 #F# 77	922	1.28	0.5770	0.325	5 APR 77	1017	1.25	0.6200	0.361
4 2PR 77	900	1.28	0.5896	0-313	5 APH 77	1006	1.28	0-6328	0.349
4 APR 77	912	1.28	0.6900	0.337	5 APR 27	1026	1.28	0.6941	0.439
4 APR 77	916	1.28	0+6200	0.325					
4 AP# 77	903	1.28	0.6328	0.313					
4 878 77	976	1.24	0.4943	0.361					

LATENCE IM

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Table 3.1. (continued)

						LOCAL	PATH N	AVE CA	CFF.
			MANE F	<b>XTINCTION</b>		TTHE L	ENGTH LE	NGIN CO	2 M M 1
	LOCAL	PATH	BATE C	CREFF.	UNIC		(KH) (HI	CKON) (	/***/
	11#E	LENGTH	LENGIN						
DALC		(K#)	(HJC#ON)	(76.47			c 04 0.	4050 0	201
		••••			13 HAY 77	917	2.90	4868 0	.231
			0.4050	0.162	13 BAY 77	1023	5.00 0	4600 0	. 190
A APR 77	759	7.00	0 4050	0,162	13 MAY 77	1001	5.06 9	.4700	1 24
6 APR 77	835	5.08	4 4 3 6 8	0.121		422	5.08 0	.4880	146
4 APX 77	812	5.05	0.4320	0.125	13 887 77	1074	5.08 0	.4660	
4 488 77	124	5.08	0.4700	0 114	13 MAY //		5.08 0	.5050	9-173
	753	5.08	0.4880		13 MAY 77	940	E 08 0	.5145	0,144
6 APR 11	808	5.08	0.5050	0.101	13 RAY 77	1007	- AA A	5200	a.1?1
6 RPR //		6.08	0.5145	0.10/	13 NAY 77	930	3.00	5461	0.133
6 APR 77	020		0.5700	0.101	13 MAY 77	951	5-08		0.125
6 APH 77	754	7.00	0.5461	0.114	12 BAY 77	1012	5-08 4		0.125
A AP# 77	815	5.00	A \$770	0.101		035	5.08 (	.5846	4 1 1 1
A APX 77	639	5.08	0.2110	0.101	13 MAT 17	854	5.08	0.6000	0.177
4 APE 77	809	5.05	0.3770	0.111	13 HAT 77		5.08	0.6200	0-122
	819	5.08	0.0000		13 RAT (1	7,0	K.04	0.6328	0-101
	821	5.06	0.6200	0.104	13 BAY 77	936	5 08	4358	0.190
6 APK //		5.08	0.6328	0.041	13 HAY 77	943	7.00	A 4500	0.125
6 APR 77	601	6.08	0.6943	0.104	13 NAV 77	1014	5.08	A 4943	0.121
6 APR 71	833	7.00	0.4050	0.162	13 BAY 77	1012	5.08	0.0742	0.286
6 APH 31	750	(	0.4050	0.156	13 BAY 77	917	2.57	0.4070	0.286
A APR 71	1 8'2	2.74	A 4 16	0.144	17 10 17	1022	2.57	0.4070	0.100
A APR 7	7 812	2.5	0.4370	0.139	13 881 17	442	2.57	0.4358	0.212
	2 824	2.51	0.450	0.174	13 MAY 11	743	2.57	0.4500	0.240
	7 753	2-5	2 0.498	9 9-120	13 HAV 77	1001	3.57	0.4880	0.212
6 MPH 1		2.5	7 0.505	0 0.120	\$3 HAY 77	922	2.57	0.4880	0.226
6 APH 7	7 505	2.5	7 0.514	\$ 0.117	13 HAV 77	1026	2.31	0 5050	0.212
6 APR 7	7 824		1 0.520	0 0.117	13 RAY 77	946	2.51		0.212
6 APR 7	7 75	2	. 0.546	0.133	43 BAY 77	1005	2.51	8+3147	0 247
A APR 7	17 115	5 (•]		0.128	13 10 77	930	2.57	0.5200	0 174
A APP 1	17 830	0 Z."		0.128	13 MAT 11	951	2.57	0.5461	0.174
	7 10	0 2.5	7 0.505	0 134	13 MAY //		2.57	0.5770	9+1 **
0 MPH -	22 81	g 2.9	7 0.600	0 117	13 MAY 7	1000	2.57	0.5896	0-102
0 85		3 2.9	57 0.626	10 0.11	13 HAY 7	432	5 67	0.6000	0.180
0		Ā 2.1	57 0.63	24 0.120	13 MAY 71			A 4200	0.168
6 APR		3 2.9	57 0.69	63 0.144	13 WAY 71	r 950	2.51	1 . 18	0.156
6 47*	11 12		28 0.40	50 0.290	13 BAY 7	7 938	2.57		0.192
6 APR	יו וו	<b>u</b>		50 0.279	13 HAY 7	7 1014	2.57	(	0.199
A APN	11 13	15 1.		58 0.214	13 HAY 7	1012	2.57	0.6443	4 149
6 APT	77 81	12 1.	CO 4.43	0.204	L3 441 7	7 917	1.28	0.4070	0.368
A	77 82	24 1.	28 0.92	0.174	33 #44 /	1020	1.78	0.4050	0.377
4 499	11 1	53 1.	28 0.47	0.114	13 MAY 7	1 1050	1.28	0.4358	0.214
	17 2	08 1.	28 0+50	30 014	13 HAT 7	1 443	1.74	0.4500	0.349
6		2 1.	.28 0.51	47 0+10	13 MAY 1	7 1001	1.20	0.4880	0.279
6	-11 - 1	ka 1.	20 0-5	500 0°13	13 MAY 1	17 927		A 4880	0.325
6 APP		10 1	28 0-54	101 0-16	13 HAY 1	17 102	1.28	0.4044	0.225
6 AP#	17 1	12 1		776 0.18	4 13 847	17 944	5 1+2 <b>8</b>	0.5050	0.268
6 APH	77 8	130 L	-20 0.5	0.19	4 12	77 100	5 1.28	0.3147	0 744
6 AP#	77 1	100 1	• CB	0.17	4 15	77 61	0 1.28	0.5200	W. 144
	1 1	119 1	.28 V.b	200 0-17	4 13 HAY	71 <b>7</b> 2	1 1.74	0.5461	0.214
		B21 1	.28 4-6	200 0 11	13 HAY		1.20	0.5996	0.204
		AN4 1	.28 0.6	328 0417	13 MAY	77 93	7 1.00	0.5770	0.194
6 API		1 22	.78 0.6	943 Q.24	13 HAT	77 100	1.10	0 4000	0.225
6 871	. 77				13 847	17 95	4 1.20	A 4200	0.184
					13 847	17 95	in 1-24	, <b>U</b> .02UV	0.145
						77 01	18 1-21	0.6328	0 301
					13 441	10	4 1.21	0.6500	0.301
					13 #44	11 10	1.2	6 Q.4943	j ¥.515
					13 MAY	77 10			

Table 3.1.(continued)

	LACAL	PATH	MAVE	EXTENCTEMN		L "CAL	PATH	WAVE	EXTINCTION
DATE	TIPE	LENCTH	LENGTH	CREFF.	DATE	A I NE	LENGTH	LENGTH	CØEFF.
		(##)	(HICHON)	(/##)			(K#)	(HICRON)	(/K4)
				A 5.73	14 MAY 77		2.57	0.4500	0.155
14 84 77		5.00	0 4050	0 463	14 847 27		2.67	0.4943	0.174
44 844 77	+10	7.V8	0 4050	0.417	14 MAY 77	75)	1.78	0.4850	0.497
14		7.00		0 40 7	14 887 77	805	1.78	0.4050	0.557
		2.00	0.4050	0.402	14 847 77	830	1.28	0.4050	0.526
14 444 17	415	7.08	0.4040	0.326	14 844 77		1	0.4060	0.611
14 447 77	873		0.4930	4 348	14 844 77		1.2	0.4050	0.474
20 54 77	404	2.00	0.4740	A 100	14 844 77	153	1 28	0.4358	0.474
34 844 33	34.3		4 6464	0 402	14 PAY 77	804	1.24	0.4500	0.361
14 -41 17		7400	0.5050	6.118	14 RAY 77	244	1.74	0.4880	0.361
14		7400	0 6 6 6 6	0.208	14 844 77	75.2	1.24	0.5050	0.467
14 847 77		5.08	0.7030	0.265	14 987 77		1.21	0.5950	0.373
14 887 77	904		A 6146	0.237	14 847 77	A 14	1.24	0.5050	0.349
14 847 17		5 5 5	0 6200	0.244	14 987 77	455	1.28	0.5050	0.301
14 849 77		5.04	0.5441	0.212	14 947 77	904	1.71	0.5145	0.467
14 RAY 77	-04	5.04	0.5770	0.190	14 947 77	846	1.28	0.5200	0.325
14 MAY 77	848	5.44	0.5896	0.218	14 MAY 77	858	1.28	0.5461	0.257
14 847 77	900		0.6000	0.1#5	14 MAY 77	904	1.24	0.5770	0.235
14 887 77	902	5.08	0.6200	0.164	14 PAY 77	848	1.20	0.5896	0.279
14 847 77	758	5.04	0.6324	0.251	24 #47 77	900	1-28	0.6000	0.215
· 14 947 77	#11	5.08	0.6178	0.274	14 HAY 77	902	1.78	4.6700	0.279
14 #47 77	#76	5.08	0.4328	0.196	14 MAY 77	758	1.28	0.6328	0.313
14 HAY 77	851	5.08	0.4328	0.140	14 MAY 77	811	1-28	0.6124	0.279
14 #47 77	916	5.08	0.4328	0.166	14 HAY 77	\$ 36	1.78	0.632#	0.268
14 HAY 77	#03	5.01	0.6400	0.244	14 HAY 77	451	1.28	0.6328	0.247
14 PAT 17		5.06	0.4500	0.224	14 MAY 77	917	1.28	0,432#	0.214
14 PAY 77	878	4.08	0.6500	0.140	14 PAT 77	<b>#</b> # 3	1.28	0.6500	0-313
14 PAY 77	913	4.00	0.6400	4.157	14 MAY 77	411	1-74	0.6500	0.268
14 MAY 77	411	<.08	0.4941	0.162	15 MAY 37	8 3 <b>8</b>	1.20	0.4590	0.268
14 PAY 27	752	2.57	0.4050	0.5 5	14 MAY 77	913	1.28	0.4500	0.214
14 MAY 77	805	2.47	0.4850	0.441	14 "47 77	411	1-28	0.694 1	0.235
, 14 MAY 77	0,8	7.47	0.4050	0.44					
14 #41 77	842	2.57	0.1050	0.411					
34 MAY 77	414	2.57	0.4050	0.357					
14 462 77	1853	2.57	0.4158	0.357					
14 #47 77	904	2.51	0.4500	0.319					
14 <b>FAV 77</b>	844	2.57	0.4880	0.302					
14 PAY 77	752	5.57	0.5050	0.376					
14 PAY 77	805	2.57	0.5050	0.330					
24 407 77	8.34	2.57	0.5050	0.302					
24 PAY 77	855	2.57	0.5050	9.270					
14 MAY 77	906	2.57	0.7141	9.77*					
14 -44 77	846	2.57	9.5790	0.270					
	858	2.21	0.7401	0.213					
14 -#4 77	40.8	<u></u>	9.5//0						
1	546		U-3046	0.211					
14	700	()	0.4200	0.197					
14 843 33	792 78 -	2475	0.4375	0.242					
14	#14 #14	7 67	0.4378	0.226					
14 -BAY 77	# 24	2.11	0.4178	8.219					
14 MAY 13	# 7 <b>#</b> ## 2	2.41	-1-4328	0.199					
14 HAY 73	# 7 L	2.57	0.6328	0.196					
14 847 22	80.1	2.57	0.4500	0.247					
14 847 77	411	2.47	0.4500	0.214					
14 843 97	-11		0.4500	1.205					

Table 3.1. (continued)

		LOCAL	PATH	WAVE	EXTINCTION		LOCAL	PATH	WAVE	EXTINCTION
DATE		1 I #E	LENGTH	LENGTH	COFFF.	DAIL	TIME	LENGTH	LENGTH	C SEFF.
			(K#)	(RICRON)	(/K#)			(##)	CHICKON	(/K#)
14 MAY	17	933	5.00	0.4050	0.338	16 MAY 77	1041	5.08	0-4050	0.258
14 HAY	77	1000	5.08	0.4050	0.317	16 RAY 77	1055	5.08	A-4358	0 231
14 MAY	11	944	5.08	0.4358	0.207	16 MAY 77	1107	5.08	0.4500	0 221
14 MAY	77	952	5.08	0.4500	0.265	16 HAY 77	7044	5.08	0.4881	0.201
14 947	71	936	5.08	0.4880	0.196	16 MAY 77	1058	5.00	0.5050	0.185
14 HAY	11	945	5.05	0.5050	0.218	16 BAY 77	1110	5 08	0 6146	0 100
14 884	17	954	5.08	0.5145	0.212	16 847 77	1044	5.08	0.5200	0.164
14 MAY	17	938	5.08	0.5200	0.207	16 MAY 77	1100	5.08	0.5441	0.171
14 MAY	77	947	5-08	0.5461	0.185	16 MAY 77	1112	5.08	0.5770	0.165
14 787	11	956	5.08	0.5770	0-100	16 MAY 77	1049	5.08	0.5896	0.162
14 MAY	77	940	5-04	9-5896	0-166	16 RAY 77	1103	5.08	0.4000	0.153
14 MAY	77	949	5.08	9.6800	9.162	16 847 77	1105	5 00	0 4 300	
14 PAY	17	951	5.00	0.6700	0.153	16 MAY 77	1052	5 00	0.0200	0.174
14 MAY	77	942	5-08	6.4328	0.153	16 884 77	1117	5.08	0.4500	0.140
14 987	17	1005	5.08	0.4328	0.153	IA HAT ST	1115	5 08	0.0700	0.163
14	77	1000	5.08	0.6500	0.153	16 887 77	1041	2.00	0.0743	0.177
14 MAY	77	958	5.08	0-6943	0.144	16 PAY 77	1121	2 67	0 4050	0 211
14 847	77	433	2.57	0.4050	0.407	16 HAY 77	1055	2 6 7	A 4350	0.311
14 447	17	1002	7.57	0.4050	0.386	16 HAY 77	1107	2 . 71	0 4500	0.278
14 HAV	77	944	2.57	0.4358	A. 311	16 BAY 77	1044	2 67	0.4900	0.2.0
14 RAY	17	952	2.57	0.4500	0.328	14 844 77	1054		0.0000	0.240
14 947	11	9 16	2.57	0.4580	0.247	16 844 77	1110	2471	0+2020	0.240
14 PAY	17	945	2.52	0.5050	0 270	14 PAY 77	1044	24.77	0.5200	0.277
14 PAY	17	954	2.57	0.5145	0 247	16 RAY 77	1100	2 67	0 644	0.214
14 447	11	938	2.57	0.5200	0.276	16 PAY 77	1112	2 67	0 6770	0.224
14 847	77	947	2.57	0.5461	0.226	16 BAY 71	1049	2 67	0 5894	0.220
14 844	11	956	2.57	0.5770	0.240	16 RAY 77	1103	2	0.1070	0 326
14 MAY	77	940	2.57	0.5896	0.199	16 MAY 77	1105	7.57	0 4200	0.100
14 844	17	949	7.57	0.6000	0.219	16 MAY 77	1052	2 67	0 4330	0.199
14 PAY	77	951	2.57	0.6200	0.219	16 MAY 77	1117	2 67	0.0727	0 212
14 MAY	77	942	2.57	0.4328	0.174	16 RAY 77	1115	2.67	0 4 94 3	0.212
14 MAY	77	1004	2.57	0.6329	0.229	16 847 77	1174	2.57	0.4947	0 21 0
14 HAY	77	1000	2.57	0.4500	0.212	16 MAY 77	1041	1.28	0 4850	0 144
14 944	77	958	2.57	0.4943	0.233	16 RAY 77	1121	1 20	0.4050	A 360
14 PAT	77	933	1.28	8-4050	0.399	16 PAY 77	1055	1.28	0.4358	0.349
14 HAY	77	100	1.7	9.4050	0.439	16 847 77	1107	1.78	0.4500	0.349
14 MAY	77	944	1.28	0.4358	0.337	16 BAY 77	1044	1.78	0.4900	0 301
14 HAY	77	952	1.28	0.4500	0.325	16 BAY 77	1050	1.70	0.4000	0.301
14	77	936	1.71	0.4550	0.279	16 847 77	1110	1.70	0.3030	0.301
14 HAV	77	945	1.78	9.5050	0.301	16 HAV 77	1046	1.78	0.5200	0.390
14 887	77	954	1.28	0.5145	0.246	16 BAY 77	1100	1.20	0 5441	0.248
14 .847	77	938	1.78	0.5200	0.246	16 HAY 77	1112	1.29	0 \$770	0.268
14 MAY	77	947	1.28	0.5461	0.235	16 MAY 77	1049	1.78	0 6494	4.767
14 MAY	77	954	1.28	0.5770	0.215	16 MAY 77	1107	1.74	0.6000	0.257
14 PAY	77	940	1.21	0.5496	0.225	16 PAY 77	1105	1.74	0.6200	0.244
14 MAY	77	949	1.24	0.4000	0.225	16 847 77	1052	1.20	0.6128	0.267
14 444	n	951	1.78	0.6700	0.214	16 947 77	1117	1.2#	0.6500	0.248
14 844	77	942	1.28	0.4128	0.704	16 MAY 77	1115	1.76	0_6943	0.301
14 MAY	11	1005	1.28	0.6328	9-325	16 RAY 77	1174	1.7	0.4943	0.301
14 HAY	77	1000	1.28	0.6500	0.268					<b>~</b> • JUI
14 847	17	958	1.24	0 4843	A 248					

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Table 3.1. (continued)

DAYE	11.04	I CHCY	SAAF 1	XIINCTIAN		LACAL	PATH	MAVE	
	11-6	L+NG1	H LENGTH	COEFF.	DATE	TINE	I ENCTH		CALINCII.
		(KH)	(MIC#ON)	(/KN)			2000	LENGIH	CHEFF.
							(	(410408)	(/K#)
10 -44 77	1210	5.08	0.4050	0.273	17 444 22				
16 447 77	1247	5.08	0.4050	0.258	17 844 33	1221	5.08	0.4050	0.417
16 MAY 77	1271	5.08	0.4358	0 744	17 848 25	1235	5.08	0_4050	0.402
16 PAY 77	1232	5.08	0.4500		11	1232	5.08	0+4358	0.361
16 MAY 77	1212	5.00	0 4000	0.231	17 MAY 77	1243	5.05	0.4560	0.341
16 #84 77	1222	6 6 6	0.4880	0-201	17 MAY 33	1023	5.08	0.4880	0 227
16 PAY 77	1276	2408	4-2020	0.196	17 NAV 77	1234	5.08	0 6060	0.327
16 889 72	1233	1.08	0-2145	0-190	17 MAY 77	1245	5.04	0 6146	0.321
14 844 33	1214	5.04	0.5200	0-196	17 RAY 77	1025	5 04	4 5 3 6 6	0.307
14 545 45	1276	5.08	0.5461	0.189	17 NAV 22	1224	2.00	0.5200	0.317
10 PAT 77	1237	5-08	0+5770	0.196	17 BAY 33	1230	7.08	0.5461	0.298
10 PAY 77	1216	5.08	0.5896	0.176	17 843 33	1290	5.08	9-5110	0.289
16 MAY 77	122#	5.08	0.6000	0 100		1021	5.08	0-5896	0.289
16 PAV 77	1230	5.08	0-6700	0.170		1238	5.08	0.6000	0.289
16 MAY 77	1218	5.00	0.0200	V-270	17 987 77	1241	5.08	0.6200	0.265
16 MAY 77	1247	6 00	9+0320	8.178	17 444 77	1229	5.08	0.6328	0.765
16 PAY 77	1242		0.0328	0.180	17 MAY 37	1252	5.00	0.4500	
16 849 77	1246	2+08	9+6500	0.176	ST MAY 77	1250	5.00	0 4943	0.273
16 844 77	1240	5+08	0+6943	9.196	17 MAY 77	1221	2 67	0 4060	0.289
14 848 93	1210	2.57	9.4050	0.328	17 547 77	1256	2.51	0.4450	0.524
LO MAY II	1246	2.57	0_4050	0.311	17 844 33	1239	2.77	0-4050	9.468
10 MAY 77	1221	2.57	0.4358	0.311	17 844 33	1272	2.57	0.4358	0.468
10 MAY 77	1232	2.57	0.4500	0.302	17 844 34	1243	2.57	0.4500	0.450
16 PAY 77	1212	2.57	0.4580	0 242	17	1223	2.57	0.4860	0.420
16 MAY 77	1223	2.57	0.5050	0.334	17 987 77	1274	2.57	0.5050	0.470
16 MAY 77	1235	2 63	445430	0-218	11 487 27	1245	2.57	0.5145	0.40.0
16 MAY 77	1214	2 6 7 6	4+2142	0-270	17 444 77	1225	2.57	9-5700	0.431
16 HAY 77	1 7 9 4	2	0.5200	0.254	17 844 77	1236	2.57	0-5441	
16 WAY 77	1233	(.)(	0.5461	9.278	17 MAV 77	1248	2.57	3 \$770	0.720
14 844 73	1236	2.51	9.5770	0.278	17 MAY 77	1 2 2 7		4.3770	0-348
14 848 85	1210	2.57	Q.5896	0.262	17 BAY 77	1234	24.27	0.3876	0.431
14	1228	2.57	9-6960	0.278	ST 844 77	1 2 3 8	2.71	0.6000	0-420
16 MAY 77	1230	2.57	0-6200	0-247	17 844 33	1271	2.51	0.6200	9.387
10 MAY 77	1218	2.57	0.6328	0.247	17 845 55	162-	2.57	0.6328	0_408
16 MAY 77	1248	2.57	0.6328	0 242	AT THE IT	1252	2.57	0.6500	0.387
16 MAY 77	1242	7.57	0.4943	0 3 70	LT MAY 77	1250	2.57	0.6941	0.39#
16 MAY 77	1210	1.28	0 4050	0.270	17 PAY 77	1221	1.28	0.4050	0.659
16 MAY 77	1245	1.28	0 4050	4.377	17 #44 17	1254	1.28	0.4050	0.441
16 PAY 77	1271	1	047020	0.412	17 MAY 77	1232	1.78	0.4358	0.441
16 MAY 77	1212	1.28	0+4358	9-386	17 MAY 77	1243	1.71	0.4500	0.041
16 844 77	1212	1+50	9-4880	0-325	17 MAY 77	1223	1 1 4	0. 470 g	0.771
14 848 33	1232	1.24	9.4500	0.386	17 MAY 77	1224	4.4	0.9680	0.573
10 441 77	1223	1-58	0.5050	0.337	17 BAY 73	1234	1+20	0.5050	0.526
Le HAY II	1235	1.28	0.5145	0.313	17 844 11	1277	1+28	0.5145	0.511
16 MAY 77	1214	1-28	0.5700	0.301	ST BAY SS	1225	1.28	0.5200	0.526
16 MAY 77	1226	1.21	0.5461	8 376		1236	1.28	0.5461	0.511
16 MAY 77	1237	1.28	0.5770	N 267	11 MAT 77	1248	1.28	0.5770	0.494
16 MAY 77	1216	1.2#	A 6994	**367	17 MAY 77	1227	1.28	0.5896	0.557
16 MAY 77	1228	1 10	**7578	9+313	17 MAY 77	1238	1.24	0.6000	0.511
16 HAY 73	1220	1.20	0.6000	0.325	17 MAY 77	1241	1.74	0.6200	
16 WAY 72	1238	1.00	0.6200	0.325	17 MAY 77	1229	1.24	A 4124	W+ 7 70
14 844 75		1.26	U-632N	0.301	17 847 72	1250	2.74	0 4043	4.711
14	1247	1.28	0.6328	0.313	17 MAY 77	1363	1460	W.0793	U-476
10 HAT //	1242	1.28	0.6500	0.301		1676	1.28	0-6500	8-467
TO ANA 13	1240	1.28	0-6943	0.349					

Table 3.1. (continued)

	e cet		WAVE	EXTINCTION					
DALF	1186	LENGTH	I EFACTH	CAFEE	DATE	LUCAL	PATH	HAVE	EXTINCTION
		CKNN			UAIE	TIPE	LENGTH	LENGTH	COFFF.
			(41(-04)	1/8-)			(K#)	(MICRON)	C/KH3
18 #44 77	1000								
18 847 77	1040	2.08	0.4050	0.361	19 MAY 77	1122	5.08	0 4050	
18 844 33	1040	5.08	9-4050	0+361	29 MAY 77	1220	5 05	0.4030	0.417
18 844 33	1003	5-08	0-4350	0.327	19 HAY 77	1 4 1 0		0-9030	0+417
A	1005	5.08	0.4500	0.317	19 847 77	1107	00	0-4358	0.373
18 MAY 77	1007	5.08	0.4580	0.273	18 843 33	1207	2.04	0-4500	0.338
18 844 77	1010	5-08	0.5000	0 373	10 000 00	1125	5-08	0-4580	0.317
10 MAY 77	1012	5.04	0.5145	0.213	14 787 77	1141	5.08	0.5050	0.241
18 MAY Y7	1013	5.08	0 6200	0.221	17 MAY 77	1214	5.08	0-5145	0.289
18 MAY 77	1014	5.04	0.5100	0.231	14 MAY 77	1130	5.0R	0.5200	0.273
18 447 77	1010		4.3401	0+231	19 MAY 77	1144	5.08	0.5441	0.246
18 847 77	1014	5+08	0.5770	0+196	19 HAY 77	1216	5.08	0.5770	0.203
18 847 33	1020	5.00	0.5896	0-196	19 MAY 77	1132	5 04	0.7770	0.203
TR NAW WW	1030	5-08	0.6000	0-145	19 MAY 77	1148	5.00	0.7096	0-237
10 -41 77	1032	5-08	0-6200	0-140	14 HAY 77	1161	7-08	0.6000	0.251
14 -44 11	1034	5-08	0-6328	0.196	19 843 77	1171		0-6700	0.224
10 -44 11	1036	5.08	0.6500	0.140		1133	<b>5.08</b>	0-6328	0.212
18 PAY 77	1030	5.08	0.4943	0.100		1215	5.08	0.4500	0-224
18 MAY 77	1000	2.57	0.4050	0 400	19 887 77	1215	5-08	0-6943	0.231
18 MAY 77	1040	2.57	0 4050	0.408	17 HAY 77	1155	2.57	0-4050	0.468
18 PAY 77	1003	2.57	0.4070	0.451	19 MAY 77	1220	2.57	0.4050	0.468
18 MAY 77	1005	3 6 7	V 4 7 3 7 8	0+378	19 864 77	1139	2.57	0.4358	0.420
18 PAY 77	1007	2031	0.4500	0+376	19 RAY 77	1207	7.57	0.4500	0 449
18 844 97	1007	2.51	0.4080	0.338	19 MAY 77	1125	2.57	0 4880	0.408
18 844 44	1010	2+57	0.5050	0.319	19 844 77	1141	2.57	0.000	0.380
10	1012	2.57	0.5145	0.311	19 HAV 77	1218	2 6 7	0.5050	0.376
14 MAY //	1013	2.57	8.5200	0.302	19 844 77	1110	2.71	0+5145	0.376
18 -81 77	1016	2.57	0.5461	0.311	19 RAY 77	1144	2.31	0.5200	0 - 35 7
10 MAY 77	1016	2.57	0.5770	0.270	18 844 77	1144	2.51	0.5461	0.357
18 HAY 77	1026	2.57	0.5844	A 111		1216	2.57	0.5770	0.357
18 MAY 77	1030	2.51	0.6000	0 2 3 4	17 -41 77	1135	2.57	0-5496	0.338
18 MAY 77	1032	2.17	0.4300	V.224	17 487 77	1148	2,57	0-6000	0.318
18 MAY 77	10 14	2.57	0 4370	4.234	14 MAY 77	1151	2,57	0.6200	0.302
18 947 77	1036	7 67	0.0120	4.202	19 PAY 77	£135	2.57	0-6328	0.286
18 #49 .7	10.70	2431	0.0700	0.262	19 #AV 77	1215	2.52	0.6500	A 110
18 884 77	1000	2+71	0.6943	0.262	19 MAY /7	1212	2.57	0.4943	0.320
18	1000	1.28	0.4050	0.481	19 #AY 7	1172	1.24	0 4040	0.378
TH MAY TY	1040	1.50	0.4050	0.467	19 MAY 77	1220	1 78	0.4050	0.807
	1003	1.28	0.4358	0.481	19 #44 77	1111	1 20	0.4070	0.041
10 -81 11	1005	1-58	0-4500	0.439	19 847 77	1207	1.2	0.4358	0-526
10 HAY 77	1007	1.78	0.4880	0.399	19 844 77	1207	1.28	0.4500	0.557
18 MAY 77	1010	1.28	0.5050	0.412		1125	1.28	0-4880	0.467
L# PAY 77	1012	1-28	0.5145	0.384	17 - 47 //	1141	1.28	0.5050	0.453
L# #4¥ 77 -	1013	1.78	0.5200	0 4 30	17 787 77	1218	1.78	0.5145	0.496
LB MAY 77	1016	1.20	0.5441	0 4 3 8	14 PAY 77	1130	1.20	0-5200	0.439
18 MAY 77	1018	1.20	0 6330	0.937	19 844 77	1144	1.28	0.5461	0.419
8 MAY 77	1076	1 70	0.7170	V+349	19 HAY 77	1216	1.28	0.5770	0 447
8 HAY 72	1030	1.20	U-5796	0.337	19 WAY 77	1132	1.21	0.5896	0.101
8 841 77	1070	1.7	v.6000	0.279	14 MAY 77	1148	1.24	0.4000	4.377
	1032	1.28	8.6200	0.325	19 MAY 77	1151	3 78	0 4 3 A A	V. 426
	1034	1-28	0.6124	0.349	19 MAY 77	1114	1 34	V-0/WU	V. 380
	1036	1.28	0.6500	0.349	19 947 72	1218	1.25	0.4320	0.373
	1035	1.28	0.694 3	0.394	19 947 77	1313	1.20	V+0500	0.439
					AF	1616	1.20	0.6943	0.481

#### Table 3.1. (continued)

	1.00.41	BATH		****		LOCAL	PATH	WAVE	EXTINCTION
DATE	1195	LENGTH	I FRGTH	COFFF.	DAIL	TT#E	LENGTH	LENGTH	COEFF.
0-10		(##)	(RTC=ON)	(/##>			(K#)	(HICRON)	(/K#)
70 MAY 77	863	5.08	0.4050	0.349	20 949 77	1322	5.08	0.4050	0.241
20 444 71	979	5.08	0.4050	0.273	20 444 77	1 355	<.08	0.4050	0.265
20 MAY 77	901	5.08	0.4358	0.265	20 HAY 77	1335	5.08	0.4358	0.258
20 HAY 77	915	5-08	0.4500	0.237	20 484 77	1346	<.08	0-4500	0.265
20 PAY 77	847	5.08	0.4880	0.244	20 #47 77	1376	5.08	0.4880	0.237
20 #44 77	930	5.08	0.4880	0.207	20 MAY 77	1317	5.05	0.5050	0.244
20 #44 77	904	5.08	0.5050	0.218	20 MAY 77	1348	5.08	0.5145	0.237
20 844 77	916	5.09	0.5145	0.190	20 MAY 71	1328	<.0A	0.5200	0-274
20 #47 77	852	5.08	0.5200	9.219	20 MAY 77	1339	5.05	0.5461	0-244
20 #44 77	907	5.08	0.5461	0.185	20 MAY 77	1 350	5-0A	0.5770	0.251
20 MAY 77	970	5.08	0.5770	0.171	20 MAY 77	1330	5.08	0,5846	0.218
20 MAY 77	855	5.08	0.5896	0.185	20 MAY 77	1341	5-00	0.000	4.231
20 MAY 77	910	5.00	0.6000	0.171	20 44 77	1 34 3	5-08	0.6700	0.21
20 MAY 77	911	5.08	0.6200	0.149	20 444 77	1392	5.08	0.0320	0.274
20 PAY 77	858	5.08	0.6329	0.166	20 441 11	1400	5-0"	0-6328	0.211
28 444 77	858	5.05	0.6354	0.144	20 - 47 27	1 3 - 1	7.08	0.07-1	0.277
20 444 11	976	5.08	0.6500	0.140		1366	24.77	0.4050	0.347
20 MAY 77	921	•	0.6943	0.144	20 847 77	1 3 70	2.57	0.4359	0.338
20 MAY 77	843	5 - S	0.4050	0.371	20 044 77	1 344	2.57	3.4500	0.338
20 PRV 77	928	2.57	0.4050	0.947	20 847 77	1 2 7 4	2.57	0.4580	0.319
20 887 77	901	- <u>{</u>	0.4458	0.347	20 847 77	1 1 1 1	2.57	0.5050	0.311
20	417	2.51	0.4500	0.347	28 #44 77	1 148	2.57	0.5145	0.311
20 - 44 - 77	347		0.4780	0.300	28 447 77	1320	2.57	0.5200	0.311
20 847 77	431	2+37	0.4040	0 347	28 444 11	1 3 3 9	2.57	0.5461	0.319
20 441 77	014	3 67	0.5145	0.262	28 847 77	1 350	2.57	0.5770	0.319
20 844 77	910	2 4 7	0.5700	0.311	20 MAY 77	1310	2.57	0.5896	0.319
20 841 77	407	5 67	0.5441	0 378	20 PAY TT	1341	2.57	0.6000	0.318
20 841 77	920	2.51	0.5770	0.242	20 MAY 17	1343	2.57	0.6200	0.311
20 4/ 77	855	2.57	0.5896	0.294	20 MAY 17	1332	2.57	G.6328	0.319
20 PAY 77	910	2.57	0.4000	0.294	20 MAT 77	1359	2,57	0.6324	0.319
20 847 77	911	2.57	0.6200	0.247	20 MAY 77	1351	2.57	0.6943	1.371
20 #47 77	858	2.57	0.6328	0.254	20 MAY Y7	1 3 2 2	1.20	0.4050	0.453
20 MAY 77	9 15	2.57	8569.0	0.219	20 444 17	1357	1.28	0.4050	0.481
20 844 77	976	2.57	0.6500	0.240	20 MAY 37	1335	1.28	0.4358	0.453
20 PAY 72	921	2.57	0.6947	0.212	20 MAY 77	1 346	1.28	0,4500	0.467
20 MAY 77	#43	1.20	0.4050	0.467	20 444 77	1326	1,20	0.4880	0.412
20 MAY 77	927	1.28	0.4050	0.526	20 PAY 77	1337	1.28	0-5050	0.420
20 884 77	901	1.28	0-4358	0.542	20 PAY 11	1 398	1.78	0.7147	0.477
20 444 77	915	1.28	0.4500	0.481	20 441 77	1328	1.78	0.5441	0.399
20 MAY 77	847	1.24	0.4880	0.313		1337	1.00	0 6170	0.453
20 444 77	933	1.28	0.4000	0.434	20 -41 11	1330	1,20	0.5494	0.467
20 484 77	904	1.28	0.5050	4.711	20 -44 77	1 3 10	1 28	0.4000	0.447
20 - 44 77	916	1.78	0.7147	4.470	30 847 77	2 2 4 2	1.28	0.6700	0.453
20 444 11	852	1.20	0.5200	0.40	20 844 77	1112	1.78	0.4328	0.439
20 -87 //	907	1.10	0.5720	0.412	20 881 77	158	1.28	0.4328	0.453
20 949 37	7/4	1.78	0.5984	0.4 6	20 #47 21	31	1.2	0.6943	0.576
20 847 77	10	1.78	0.4000	0.496	••				
26 444 77	911	1.78	9.6200	0 . 19					
20 847 77		1.78	0.6328	0.453					
20 847 22	914	1.28	0.6328	0.346					
20 447 77	926	1.78	0.6500	0.396					
20 847 71			0 4843	0 384					



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Fig. 3.5. EFFECT OF WIND SPEED ON EXTINCTION COEFFICIENT SPECTRA NEAR THE CAPE CANAVERAL, FLORIDA SHORELINE.

#### Table 3.2. Aerosol extinction coefficients and visibility derived from pyrometer measurements.

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DATE	LOCAL	RANGE	λ	TRANS-	EXTINC.	VIS.
(y.m.d)	TIME	<u>(km)</u>	<u>(µ)</u>	MITTANC	<u>E (km<sup>-1</sup>)</u>	<u>(km)</u>
19999911121112222222222222222222222222		771077171717117717171710710710701101017107710710	<b>8888888888888888888888888888888888888</b>	75527734277771925025726288154718150430741616104235950180938/ 38745946550584492220263927429319664503598958387443499412722 **********************************	00000000000000000000000000000000000000	943912984019642554153375102121315 11112211212145434350245745443434

(y.m.d)TIME(km)( $\mu$ )MITTANCE (km <sup>-1</sup> )(km)77 030210405.080.55680.6850.07452.77 030211365.080.55680.5430.12032.77 030211504.610.55680.5700.18221.77 030211523.100.55680.4570.10637.77 030212007.470.55680.4570.0844.6.77 030216104.610.55680.5750.0754.2.77 030216107.470.55680.5750.0754.2.77 030216107.470.55680.5180.16221.77 03038523.100.55680.4610.15220.77 03038523.100.55680.24990.38910.77 0303132523.100.55680.24990.38910.77 0303132527.470.55680.24990.38910.77 0303132527.470.55680.1360.26713.77 0303132527.470.55680.1360.26713.77 0303140577.470.55680.1360.1200.26777 0303142257.470.55680.1360.1200.26777 03045.080.55680.1300.1200.26777 03045.080.55680.1300.1200.26777 030414225 <th>(y.m.d)TIME(km)(<math>\mu</math>)MITTANCE(km<sup>-1</sup>)77 030210405.080.55680.6850.07477 030211365.080.55680.5430.12077 030211504.610.55680.5430.12177 030211505.080.55680.5700.18277 030211505.080.55680.57500.18277 030216105.5680.55680.5640.10677 030216105.5680.55680.5640.18577 030216105.5680.55680.55750.02577 030216123.100.55680.55680.14377 03038523.100.55680.4240.14377 030313255.080.55680.24300.125377 0303132577.470.55680.24300.126177 0303132577.470.55680.13600.325377 0303132577.470.55680.1200.26777 030314277.470.55680.1200.26777 030415277.470.55680.1200.26777 03045.080.55680.1300.26777 030415207.470.55680.3300.1207030415207.470.55680.3310.26777 030415207.470.55680.1200.26777 030410005.080.5568</th>	(y.m.d)TIME(km)( $\mu$ )MITTANCE(km <sup>-1</sup> )77 030210405.080.55680.6850.07477 030211365.080.55680.5430.12077 030211504.610.55680.5430.12177 030211505.080.55680.5700.18277 030211505.080.55680.57500.18277 030216105.5680.55680.5640.10677 030216105.5680.55680.5640.18577 030216105.5680.55680.55750.02577 030216123.100.55680.55680.14377 03038523.100.55680.4240.14377 030313255.080.55680.24300.125377 0303132577.470.55680.24300.126177 0303132577.470.55680.13600.325377 0303132577.470.55680.1200.26777 030314277.470.55680.1200.26777 030415277.470.55680.1200.26777 03045.080.55680.1300.26777 030415207.470.55680.3300.1207030415207.470.55680.3310.26777 030415207.470.55680.1200.26777 030410005.080.5568
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Fig. 5.1 INTEGRATED HDD CONCENTRATION (MOLECULES CHACH) FOR 5.12 KM PATH, 3-MAR-77, CCAFS PATH TEMP. 15 DEG C. M-MOBILE MET STATION.T-TRANSMITTER MET.R-RECEIVER MET.G-GFCS

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Fig. 5.2 INTEGRATED HD0 CONCENTRATION (MOLECULES CM CM) FOR 5.12 KM PATH, 4-MAR-77, CCAFS PATH TEMP. 19 DEG C, M-MOBILE MET STATION, T-TRANSMITTER MET, R-RECEIVER MET.G-GFCS

TIME IN HOURS



Fig. 5.3 INTEGRATED HDD CONCENTRATION(MOLECULES/CM/CM) FOR 5.12 KM PATH, 7-MAR-77, CCAFS PATH TEMP. 24 DEG C. M-MOBILE MET STATION, T-TRANSMITTER MET, R-RECEIVER MET, G-GFCS

TIME IN HOURS



Fig. 5.4 INTEGRATED HD0 CONCENTRATION MOLECULES (M. C.M.) FOR 5.12 EM PATH. 8-MAR-TT. CCAES PATH TEMP. 21 DEG C. N-MOBILE MET STATION.T-TENNISMITTER NET.R-RECEIVER MET.G-3FC:

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Fig. 5.6 INTEGRATED HDD CONCENTRATION (MOLECULES/CM/CM) FOR 5.12 KM PATH, 10-MAR-77, CCAFS PATH TEMP, 18 DEG C, M-MOBILE MET STATION, T-TRANSMITTER MET, R-RECEIVER MET, G-GFCS

TIME IN HOURS



Fig. 5.7 INTEGRATED HD0 CONCENTRATION(MOLECULES/CM/CM) FOR 5.12 KM PATH, 11-MAR-77, CCAFS PATH TEMP. 19 DEG C, M-MOBILE MET STATION,T-TRANSMITTER MET,R-RECEIVER MET,G-GFCS

TIME IN HOURS



Fig. 5.8 INTEGRATED HDO CONCENTRATION (MOLECULES/CM/CM) FOR 5.12 KM PATH, 12-MAR-77, CCAFS PATH TEMP. 20 DEG C, M-MOBILE MET STATION, T-TEANSMITTER MET, R-RECEIVER MET, G-GFCS

TIME IN HOURS



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Fig. 5.9 INTEGRATED HDO CONCENTRATION (MOLECULES/CM/CM) FOR 5.12 KM PATH, 14-MAR-77, CCAFS PATH TEMP. 23 DEG C, M-MOBILE MET STATION.T-TRANSMITTER MET.R-RECEIVER MET.G-GFCE

TIME IN HOURS



Fig. 5.10 INTEGRATED HDD CONCENTRATION (MOLECULES/CM/CM) FOR 5.12 KM PATH, 15-MAR-77, CCAFS PATH TEMP, 28 DEG C. M-MOBILE MET STATION T-TRANSMITTER MET B-RECEIVER MET C.CECC

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Fig. 5.11 INTEGRATED HDD CONCENTRATION (MOLECULES/CM/CM) FOR 5.12 KM PATH, 31-MAR-77, CCAFS PATH TEMP, 22 DEG C. M-MOBILE MET STATION, T-TRANSMITTER MET, R-RECEIVER MET, G-GFCS

TIME IN HOURS



Fig. 5.12 INTEGRATED HDD CONCENTRATION (MOLECULES/CH/CM) FOR 5.12 KM PATH, 1-APR-77, CCAFE PATH TEMP, 23 DEG C, M-MOBILE MET STATION, T-TRANSMITTER MET, R-RECEIVER MET.G-GFC:





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Fig. 5.14 INTEGRATED HDG CONCENTRATION CMOLECULEUSCH CMOLEGNER SUB AM TATHO ANAFORD CONFU PATH TEMP. 24 DEG COMOMOBILE MET STATIONOT-TRANSMITTER.MEDUS PROBABLE MET, G-GFCS

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a that we the most  Fig. 5.15 INTEGRAVED HDG CONCENTRATION (MOLECULES (CM CM) FOR 5.12 KM PHTH, 5-GER OT, CCHES, PATH TEMES 24 DEG C. M-MOBILE MET STATION.T-TENNEMITTER MET/R-RECEIVER MET/G-GEOS



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Fig. 5.16 INTEGRATED ADD CONCENTRATION MOLECULES CHORED FOR 5.12 KM PATH. 16-MAY-77. COMP. PATH TEMP. 25 DEG C. M-NOBILE NET STATION TOTAMISMITTER MET R-RECEIVER MET.G. OFC.



Fig. 5.17 INTEGRATED HD0 CONCENTRATION (MOLECULES (CM, CM) FOR 5.12 KM PATH, 17-MH)-TT, CCHES PATH TEMP. 25 DEG C, M-MOBILE MET STATION T-TRANSMITTER MET, R-PECEIVEP MET G-SFCS

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Fig. 5.20 INTEGRATED HDD CONCENTRATION (MOLECULE: CH CM) FOF S. 2 KM FATH (21-MAX-77), CCAPS PATH TEMP2 26 DEG C (M-MOBILE MET STATION T-TEAMSMITTED MET F RECEIVED MET G-GFC)

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Fig. 5.21 INTEGRATED HD0 CONCENTRATION HOLECULES ON OMA POP 5.12 PM PATH 23-MAY-TT COAF PATH TEMPS 26 DEG C. H-MOBILE MET 1.4TION T-TEMNEMITTEP MET P-RECEIVER MET G-GECI

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Fig. 5.22 INTEGENTED ADA CONCENTRATIONS MOLECULE. ON THE FOR FOR FOR FULL HATH, 24-MAY-TT, CONTE PATH TEME, 28 DEG C. M-MOBILE MET STHTION T-JEHO MITTEP MET F-PECEIVEP MET G-SPOS

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Fig. 5.23 INTEGRATED HDD CONCENTRATION (MOLECULES (CH. CH.) FOR 5.12 FM PHTH. 25-MHY-T.) CCHES PATH TEME. 30 DEG C. M-MOBILE MET STHTION, T-TRHUMMITTEP MET, E-PECEIDLE MET, G-GECS

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					(DEG)	(TORR)	Ê	( 4848 )	(# 150 #)		(056)	
23	FEB	17	1430	F	18.2	13.29	84.9	1018.1	0.37	4.2		
23	FE8	11	1500	-	19.1	13.46	81.4	1017.9	0.37	3 <b>.</b> 7		
23	FLB	11	1530	F	18.6	13.53	84.4	1017.6	0.37	4.9		
23	FE8	17	1600	-	18.4	13.49	85.2	1017.3	0.37	5.6		
23	FE8	17	1630	-	17.8	13.29	87.2	1016.9	0.37	8.2		
23	FE8	77	1700	F	17.5	13.15	87.6	1016.8	0.37	8.2		
23	FE 8	11	1730	►	17.5	13.14	87.7	1016.7	0.37	7.4		
25	FEA	11	1100	T	18.0	9.38	60.6	1019.4	0.36	2.1	179	
25	FER	17	1130	-	16.7	10.07	70.6	1019.6	0.36	1.6	211	
25	FE B	11	1200	⊢	16.3	10.24	74.0	1019.4	0.36	5 • 5	105	
25	FEP	77	1230	►	17.4	10.33	69.4	1019.1	0.36	0.7	148	
25	FEB	17	1300	-	17.3	10.30	69.5	1018.6	0.36	1.4	130	
25	FER	11	1330	-	17.4	10.59	71.1	1018.3	0.36	1.7	129	
25	FEP	17	1400	<b></b>	17.5	10.91	72.3	1018.1	0.36	2•2	142	
25	FEB	77	1430	-	17.6	11.39	75.5	1017.9	0.65	1.9	153	
25	FE B	11	1500	-	17.7	11.66	77.1	1017.8	16*0	2.1	163	
25	FEB	22	1530		17.9	11.84	77.3	1017.5	0.81	2.1	162	
25	FER	11	1600	┢	17.9	12.39	80.7	1017.4	0.68	1.6	185	
25	Ft B	17	1,30	-	17.8	12.51	82.0	1017.3	0.53	1.7	189	
25	FEB	11	1700	<b>þ</b>	17.9	12.61	81.9	1017.3	0.38	1.3	209	
25	FER	17	1730	⊢	17.7	12.86	84.6	1017.2	0.22	1.1	222	
25	FE B	17	1 80 0	F	17.6	12.61	83.5	1017.4	0.07	1.0	235	
26	FEB	11	1030		18.5	14.16	88.9	1017.9	• 6• 0	1.7	121	
26	FE8	77	1100	-	18.5	14.15	88.5	1017.9	1.02	1.5	98	
26	FE B	11	1130	+	20.0	14.71	83.7	1017.9	1.07	1.5	114	
26	FER	17	1200	-	18.9	14.61	89.5	1017.6	1.11	1.8	16	
26	FEB	17	1230	-	19.4	14.92	88.6	1017.2	1.13	1.8	92	
26	FE3	11	1300	-	19.2	14.89	89.2	1016.7	1.12	2.3	89	
26	FEB	11	1330	-	19.6	15.11	88.7	1016.3	1.08	3.0	106	

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26	FE 8	77	1400	۲	20.0	14.92	85.0	1016.1	1.03	3.4	118
26	FE 8	11	1430		19.9	14.94	85.6	1015.7	0.95	4.1	114
26	FE8	11	1500	<b>}</b>	19.8	15.18	87.7	1015.3	0.86	4.2	115
26	FE 8	11	1530	<b>þ.</b> .	19.8	15.35	88.8	1015.3	0.74	<b>4</b> • 5	116
26	FER	11	1600	<b>p</b> -1	19.6	15.45	90.3	1015.3	0.61	4.6	116
26	FEB	11	1630	-	19.5	15.51	91.3	1015.3	0.44	3 <b>.</b> 8	113
26	F.E. 8	17	1700	•	19.4	15.56	92.4	1015.2	0.28	4.3	114
28	FE 8	11	1203	F	13.8	8.97	76.0	1018.2	0.55	4 • 4	315
28	r F F	Li	1233	+-	14.1	8.04	66.7	1018.0	0.45	3.7	258
8 Z	FE8	11	1303	Ŧ	13.3	7.17	62.9	1017.4	0.25	3.9	283
28	FEP	22	1333	¥	13.1	7.00	62.1	1016.8	0.20	<b>4</b> • 3	288
28	FE8	11	1400	æ	14.0	5.91	49.4	1020.8	0.29	6•0	43
<b>2</b> 8	FE 8	11	1407	-	14.1	7.06	58.6	1016.5	0.55	4.1	241
28	E E E E E	₩ <b>₩</b> { #	1430	7	14.0	6.07	509	1020.8	0.22	0.9	76
28	FEB	77	1431	-4	13.6	6.77	58.2	1016.2	0.28	3.4	165
28	FE B	11	1501	¥	13.9	6.27	52.8	1016.6	0.32	3.0	187
8 2	FEB	11	1531	-	14.2	7.38	60.7	1016.6	0.29	3•2	227
\$ ≥	FrB	17	1601		14.4	6.22	50.7	1016.6	0.31	2.9	172
82	FE B	11	1631	Ŧ	14.3	6.33	51.8	1016.9	0.26	3•3	213
28	FEB	11	1011	L	14.1	6.46	53.7	1017.0	0.08	2.7	247
0) 22	F.E.B	77	1731	-	14.2	5.96	49°2	1017.1	0.03	2.4	215
28	FL B	11	1801	<b>}</b>	14.4	6.27	51.1	1017.6	0.01	2.4	256
-1	MAR	11	1100	æ	15.1	4.61	35.9	1027.3	1.07	1.3	259
-	M A N	77	1102	<b>-</b>	15.1	4.86	37.9	1022.8	1.06	5.5	141
-,	MAR	17	1130	5	15.1	4.73	37.0	1027.3	1.14	1.3	275
	MAR	77	1200	X	15.1	4.58	35.6	1027.3	1.19	1.3	272
<b>, -1</b>	MAR	77	1230	Ŧ	15.5	4.42	33.6	1027.2	1.21	1.1	261
٦	MAP	11	1300	<b>*</b>	14.8	4.48	35.6	1021.8	1.18	5.8	194
-	M A R	11	1330	t-	14.7	4.26	34.1	1021.6	1.16	5.8	144

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1											
UAT	HINDH	YEAR	JWII	STTE	AT	PPH20	I	89	SR	SH SH	HOH VULUV
					10101	( 1044 )	( 9 )				(UEG)
-	4 <b>4</b> 4	11	1400	Ŧ	14.6	4.21	33.9	1021.3	1.10	5.3	104
	MAK	77	1430		14.7	4 4 4 4	35.5	1021.1	1.03	5.5	207
7	MAK	17	1500	-	14.8	4.72	37.4	1020.9	<b>96</b> 0	<b>6 • </b>	176
y and	4 V W	11	1530	-	14.6	4.91	38.7	1020.7	0.82	4.6	83
-	MAR	77	1600	-	14.6	4.21	33.9	1020.7	0.69	4.5	75
~	MAK	77	1630	►	14.6	4.41	35.5	1020.7	0.54	4.1	15
2	MAR	77	006	X	13.9	6.09	51.2	1027.8	0.60	0.5	323
~	MAR	77	930	▶	15.8	5.49	40.9	1023.4	0.73	2.8	270
~	N A K	77	930	æ	16.0	5.28	38.7	1027.8	0 - 7 4	0.6	126
2	AAM	77	1000	-	16.6	10.4	35.1	1023.5	0.85	3.6	67
~	MAR	11	1000	¥C.	16.9	5.35	37.2	1028.5	0.85	0.5	256
2	M X X	11	1030	-	16.8	4 • 6 4	32.5	1923.7	0.95	3.7	117
~	<b>3 4 5</b>	17	1030	x	18.1	5.28	34.0	1028.5	0.96	0.7	44
2	XQM	17	1100	►	17.2	5.22	35.4	1023.6	1.03	3.5	87
2	MAK	17	1100	£	18.2	5,45	34.8	1023 .5	1.05	0.8	31
2	M A R	17	1130	۲	16.9	4 . 85	33.5	1.223.7	1.09	4.0	131
2	MAR	77	1130	Z	16.3	5.42	34.5	:028.5	1.11	6°0	31
~	MAK	17	1200	⊢	16.9	5.55	30.5	1023.6	1.12	4.6	01-
2	A A R	11	1200	•	16.1	5.90	37.8	1024.5	0.98	6.0	24
2	200	17	1230	<b>b</b>	36.5	6.61	47.1	1023.3	1.18	5.1	79
2	MAR	11	1230	Ŧ				1028.5	1.19	1.0	23
~	na r	27	1305		16.4	6. RD	48.7	1022.9	1.01	3.9	173
2	<b>第一日</b> 第二日 第二日	11	1300	<b>X</b>	17.4	6.08	40.8	1028.2	0.99	0.9	36
2	? .₹ ₩.	11	1330	-	16.7	7.61	53.4	1022.7	1.10	3.7	36
~	MAR	17	1330	X	18.2	6.76	43.2	1027.9	1.13	0.9	35
~	3 <b>d</b> H	17	1400	+	17.0	7.92	54.8	1022.2	1.06	3.8	66
~	MAR	17	1400	¥	17.6	7.31	48.4	1027.3	1.08	0.8	04
2	MAR	17	1430	F	16.7	7.99	56.0	1022.0	0.99	3.9	4
~	MAR	17	1430	T	17.9	7.55	49.1	1027.0	1.01	0.8	29

JAY	HINDU	YEAR	IHE	SITE	AT	DCHdd	на	80	58	2	HOM
				1	(DEC)	(TORR)	:	(MBAR)	CH DS/H)	(W/S)	(DEG)
~	2 <b>4</b> F	17	1500	Ħ				1027.0	0.91	0.8	37
2	MAR	17	1530	T	17.8	7.92	52.0	1026.4	0.79	0.7	32
m	3 <b>4</b> 8	11	1000	•	17.7	11.67	77.2	1020.8	0.49	4.5	96
m	1 A R	77	1000	æ	17.5	11.73	78.4	1025.0	0.62	0.8	109
m	AAR	17	1030	-	17.8	11.83	77.4	1020.9	0.88	3.9	66
m	N A R	11	1030	T	14.1	9.01	74.6	1025.1	0.70	0.7	112
'n	1 0 X	11	1100	-	17.5	12.45	82.9	1021.1	0.69	2•5	100
m	M A R	77	1100	X	17.6	12.36	82.0	1025.3	0.51	••0	126
<b>ا</b> ل	XDM	77	1130	►	18.2	12.74	81.6	1020.9	0.89	2.3	81
m	AAM	11	1130	Ħ	17.9	12.73	83.0	1025.1	0.73	4.0	100
m	MAR	77	1200	+	18.0	12.57	81.3	1020.3	0.79	4.2	92
m	X A E	17	1200	æ	17.8	12.68	83.2	1024.5	0.09	0.5	107
m	4 9 F	11	1230	►	17.9	12.79	83 <b>.</b> 3	1020.0	1.09	3.6	96
m	MAR	77	1230	<b>X</b> .	17.9	12.77	83.3	1024.5	0.68	0.7	117
ſ	NAK	17	1300	<b></b>	17.9	13.17	85.9	1019.4	1.07	2.7	89
'n	2 <b>4</b> 8	11	1300	æ	17.7	13.11	86.6	1023.9	0.45	0.5	115
m	N A R	11	1330	-4	19.0	13.39	81.1	1019.2	1.10	1.8	104
m	AAR	11	1330	æ	18.5	13.40	83.8	1023.1	1.17	4.0	105
m	a a a	11	1400	-	19.6	13.23	82.2	1019.1	1.04	1.6	46
m	MAR	11	1430	<b>p</b>	18.6	13.47	84.0	1018.4	10.97	3•2	103
m	N A K	11	1500	-	18.3	13.24	84.1	1018.3	0.88	3.8	46
4	A R	17	006	æ	18.0	14.62	7.49	1019.7	0.59	0.9	169
4	MAR	17	930	x	18.1	14.61	93.9	1019.8	0.72	1.0	165
4	X V II	17	1000	Ħ	18.6	14.86	92.7	1019.8	0.85	1.2	159
•	241	17	1100	¥	18.8	14.96	91.8	1020.6	0.67	1.0	158
4	2 4 2	11	1130	Ħ	19.2	15.10	90.5	1020.7	1.04	1.0	155
4	***	11	1200	X	19.3	15.21	90.7	1020.4	0.80	1.2	150
4		11	1230	×	19.3	15.42	92.0	1020.6	0.57	1.3	149
4	N N N	77	1300	٩	19.5	15.50	1.16	1020.1	1.07	1.3	148

UAT	HINDU	YFAR	TIME	CTTC	A T	00U00	20	00	20	5	
				1170	(DEG)	(TORR)		CHBAR)	CH CS M)	CH/S)	CDEG)
							× •				
4	MAR	17	1330	X	19.6	15.59	91.0	1019.7	1.13	1.6	150
4	2 <b>4</b> 2	77	1400	æ	19.8	15.58	96.0	1019-6	1.02		155
4	MAR	77	1430	æ	19.8	15.59	90.3	1019-4	46-0	1.3	121
4	MAR	11	1500	æ	19.9	15.67	90.1	1018.7	0-86		151
4	MAR	77	1530	æ	19.9	15.72	<b>5°06</b>	1018.4	0.17	5.1	153
<b>**</b>	MAR	77	006	s	22.3	17.24	85.4	1017.9	7.4.7	) ) )	221
~	MAR	11	930	5	23.5	17.35	79.8	1018-0	2.19		228
~	MAR	17	1000	\$	24.5	17.35	75.4	1018-0	2.19		212
~	MAR	11	1030	s	25.4	17.30	71.1	1018.0	2.19		276
~	NAR NAR	17	1100	s	26.6	17.20	65.9	1018.0	2.19		248
~	MAR	17	1130	S	27.6	16.94	61.0	1018.0	2.19		247
	KAR	11	1200	S	27.9	16.62	59.1	1017.8	2.19		266
~	MAR	11	1230	s	28.1	16.69	58.6	1017.6	2.19		267
•••	MAR	77	1300	Ś	28.0	16.36	57.6	1017.3	2.19		278
-	MAR	11	1330	s	19.8	13.21	76.4	1017.8	2.19		8
~	MAR	11	1400	S	18.2	13.06	83.4	1017.8	2.19		12
~	MAK	11	1430	Ś	17.2	12.56	85.6	1017.9	2.19		
-	MAR	11	1500	S	16.4	12.26	87.6	1019-1	2.19		α
	MAR	17	1530	S	16.1	11.90	86.8	1018.3	2.19		4
~	MAR	11	1600	s	15.9	11.79	87.2	1018.4	2.19		~ ~
~	MAR	11	1630	s	15.6	11.84	89.0	1018.6	2.19		) ( ) (
-	MAR	11	1700	s	15.3	11.70	90.2	1019.5	2.19		
œ	MAR	77	006	s	18.2	21.9	58.6				4 J
æ	MAR	11	930	S	20.0	9.84	56.2				
30	MAR	22	1000	┣	19.8	9.99	57.7	1021.9	0.85	3.3	77
σ	MAR	77	1000	×	17.0	11.60	80.0	1028.1	0.25	0.5	70
30	MAR	11	1000	s	20.5	9.54	52.7	     	] )	1 9 9	•
σ	X M H	17	1030	-	18.4	11.20	70.8	1024.3	0.25	4.4	60
σ	NAR	11	1030	X	17.5	11.21	75.1	1028.4	0.63	1.0	11

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YAC	HINDE	YFAR	TIME	STTF	Δ Τ	DCHOO	Нα	d R	9 ×	2	
			) ;	) • •	(DEG)	(TORR)	5	CHBAR)	CH DS/N)	(M/S)	CDEG
30	MAR	17	1030	s	20.7	9•36	51.0				
ኖ	MAR	17	1100	-	18.5	11.50	72.0	1024.0	0.72	4 • 4	49
ን	MAR	17	1100	x	17.6	11.05	73.3	1028.7	0 • 60	1.1	78
6	NAK	77	1130	F	19.1	11.06	66.9	1023.7	0.50	4.0	5.5
σ	MAR	17	1130	E	19.0	10.59	64.5	1028.3	0.71	1.3	69
σ	MAR	11	1200		19.8	11.13	64.3	1023.5	0.89	4 . 4	57
σ	MAR	77	1200	X	18.7	10.68	66.3	1028.3	1.26	1.2	77
ø	MAR	11	1230	F	20.2	11.00	62.2	1023.3	1.24	4.0	52
თ	MAR	77	1230	æ	19.2	10.51	63.0	1027.9	1.21	1.3	76
ა	MAR	17	1300	►	20.5	11.77	65.1	1022.7	1.18	5.0	63
	MAR	77	1300	<b>X</b>	18.8	11.45	70.5	1027.2	1.19	1.1	15
δ	MAR	77	1330		19.2	11.92	71.4	1022.3	1.00	4.4	67
¢.	MAR	11	1330	S.	18.5	11.69	73.1	1027.0	1.10	0.8	81
σ	MAR	77	1400	-	18.7	11.96	74.2	1022.0	1.01	3.8	12
σ	AAM	17	14:00	-	19.6	11.93	70.0	1021.8	0.92	<b>4</b> • 3	66
ን	AAR	77	1500	-	20.0	11.14	63.7	1021.3	0.75	3•5	57
σ	d V M	77	1530	-	19.4	11.45	67.8	1021.2	0~66	3•3	68
σ	MAR	77	1600	-	19.6	10.98	64.2	1021.0	0.49	3.4	63
6	MAR	11	1757	S	18.8	12.21	75.1	1024.0	0.10	0.0	59
10	X Y M	17	006	x	17.5	13.51	90.3	1021.7	0.27	0.6	46
10	MAP	17	930	æ	17.9	13.58	88.4	1021.5	0.67	0.7	96
10	XAX	17	1000	æ	18.1	13.50	87.1	1021.7	0.34	0.8	110
10	0 <b>0 0</b>	27	1003	r	18.9	14.43	88.0	1020.9	0.31	3.7	112
10	NAR N	77	1030	æ	18.1	13.68	87.8	1022.0	0.27	1.0	104
5	MAR	22	1033	Ś	19.2	14.41	86.5	1020.9	0.27	4.4	104
10	201	11	1100	×	18.1	13.75	88.5	1021.8	0.29	0.8	111
101	AAR	77	1103	S	19.1	14.43	87.1	1020.9	0.40	4.0	112
10	XAM	77	1130	X.	17.9	13.73	89.3	1021.8	0.51	0.6	113
10	MAR	17	1133	r	19.4	14.62	85.8	1020.8	0.66	2.3	118

فرحاكم معاليهم والمعادية وسيلاكمه

DAY	HINDH	YEAR	JWIT	SITE	AT	PPH26	Нα	<b>B</b> P	SR	SH	HQM
					(DEG)	(TORR)	(\$)	(MBAR)	CHISQ M)	(W/S)	(DEG)
1 C	MAR	77	1200	æ	18.1	13.76	88.2	1021.4	0.51	<b>*</b> • 0	108
10	M A R	11	1203	s	19.9	14.75	84.8	1020.7	0.66	1.9	111
10	MAR	11	1230	X	18.1	13.76	88.5	1021.2	0.39	0.3	104
10	MAR	17	1233	s	19.7	14.67	85.1	1020.4	0.46	1.5	104
10	MAR	11	1303	s	20.5	14.58	80.ó	1020.0	0.62	1.8	6 9 9
10	MAR	77	1333	S	20.3	14.39	80.5	1019.8	0.43	2.0	82
10	TAR	11	1400	►	18.9	14.45	88.4	1016.5	0.15	2•5	65
10	4 A R	77	1403	s	19.9	14.27	82.1	1019.3	0.35	2.2	8 () 8
10	MAR	17	1430	۲	19.9	14.64	83.8	1016.3	0.12	2.4	61
10	NAK	57	1433	S	20.0	14.36	82.1	1019.2	0.34	2.2	62
10	2 N N N	77	1503	s	20.4	14.65	81.8	1019.3	0.19	1.0	49
10	MAR	77	1533	S	20.6	15.03	82.6	1019.4	0.31	1.0	58
	MAR	11	930	£	18.6	15.41	96.3	1021.3	0.32	0.1	156
11	MAR	77	1000	Æ	19.0	15.68	95.2	1021.6	0.35	0.1	112
11	MAR	17	1030	£	19.1	15.71	95.1	1021.8	0.54	0.3	87
11	MAK	77	1100	£	19.5	16.03	94.1	1022.1	1.07	0•3	117
11	AAR	17	1133	S	22.3	15.85	78.3	1020.9	0.71	3.5	0
11	MAR	77	1203	s	22.1	16.29	81.5	1020.9	0.61	0.1	0
11	MAR	11	1233	S	21.7	16.42	84.5	1020.4	1.04	0.1	0
11	MAR	77	1303	S	22.9	16.52	78.8	1020.0	1.03	0.1	16
11	X V R	11	1333	Ś	22.9	16.73	80.0	1019.7	0.74	0.1	98
11	MAR	77	1403	S	22.9	16.69	7.97	1019.6	0.96	0.1	102
11	AAR	11	1433	S	22.2	16.83	83.8	1019.1	06.0	0.1	118
11	MAR	17	1503	S	23.2	16.92	79.5	1019.0	0.96	0.1	101
11	MAR	17	1533	S	23.3	16.83	78.6	1018.8	0.69	0.1	<b>86</b>
11	MAR	11	1603	s	23.5	16.83	77.3	1019.0	0.65	0.1	78
11	MAR	17	1633	S	22.8	16.60	79.8	1018.9	0.22	0.0	92
12	MAR	11	006	£	19.1	15.26	92.3	1021.1	0.52	0.6	120
12	AAR	17	930	-	19.3	15.46	92.2	1017.7	0.61	2 <b>.</b> 8	108

1 2 1	H I N C W	VEAD	T T MC	<b>677</b> 0	÷ •		20	0	25	5	
-				2110							
					( ) ] ( )		3				10201
12	MAR	11	930	8	19.2	15.29	91.6	1021.4	0.58	0.6	125
12	388	11	1000	-	19.4	15.53	91.9	1017.8	0.71	2.6	115
12	5 <b>1 1</b> 1	77	1000	Æ	19.4	15.36	91.2	1021.4	0.73	0.6	138
12	MAR	17	1030	-	19.8	15.75	91.2	1017.8	0.86	2.5	113
12	1 1 1 1 1 1	11	1030	T	19.5	15.43	91.0	1021.4	0.80	0.5	141
12	MAK	77	1100	×	19.8	15.64	90.3	1021.4	1.06	4.0	149
12	MAR	11	1129	\$	23.6	16.67	76.3	1020.4	1.14		145
12	MAR	11	1130	F	19.8	15.88	91.8	1017.7	1.05	1.8	121
12	MAR	77	1130	X	20.0	15.72	89.9	1021.2	1.06	0 <b>.</b> 4	147
12	MAR	77	1159	S	24.1	16.94	75.4	1920.1	1.16		147
12	AAK	11	1200	+	20.3	16.11	90.5	101 /.2	1.06	1.7	119
12	X A H	11	1200	æ	0.1	15.82	6.98	1021.1	1.08	0.4	147
12	MAR	77	1229	S	24.5	17.09	74.2	1019.9	1.25		149
12	XAX	11	1230	►	20.5	16.15	89.4	1017.0	1.17	1.1	119
12	X M H	77	1230	æ	20.5	15.98	88.5	1020.6	0.99	4.0	154
12	MAR	11	1259	S	24.1	17.05	75.5	1019.3	1.13		140
12	X A E	11	1300	<b>_</b>	20.3	16.31	91.4	1016.7	1.10	1.7	130
12	2 <b>4</b> 8	77	1300	æ	20.6	16.13	88.8	1020.3	1.12	0•3	148
12	MAR	17	1329	5	24.3	17.20	75.4	1019.0	1.08		140
12	Xei	11	1330	•	20.3	16.44	91.9	1016.4	1.01	1.6	127
12		77	1330	X	20.7	16.26	88.7	1020.0	0.88	0.3	137
12	MAR	17	1359	S	23.7	17.07	77.8	1018.2	1.16	0.0	135
<b>1</b> 2	MAR	77	1400	►	20.3	16.58	92.7	1015.6	1.04	3.1	127
12	2 <b>4 4</b>	77	1400	π	20.5	16.42	90.8	1019.5	1.08	0.7	133
12	MAR	17	1429	S	24.4	17.30	75.5	1017.8	1.07		141
12	X D I	11	1430	+	20.5	16.88	93.2	1015.2	1.01	3.2	136
12	1 <b>4</b> 1	17	1430	×	20.6	16.65	91.4	1019.1	1.04	0.6	141
12	MAR	11	1459	ŝ	24.4	17.33	75.4	1017-6	0.93		149
77	1 1 1	17	1500	<del>}</del>	20.4	16.77	93.2	1015.0	0.90	3.1	138

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فالفاقية والمتعالمة والمحالية والمحالية والمتعالية والمتلك والمتحال والمتحال والمتحالية والمحال والمحال والمعال والمحالية والمحال

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AY	HINDW	YEAR	TIME	SITE	AT	PPH20	Ha	BP (MRAD)	SR CUISO NO	HS (H/S)	KDFG)
12	MAR	77	1500	æ	20.7	16.70	91.3	1018.6	0.91	0.7	151
ΪŻ	N A K	11	1529	5	24.4	17.39	75.7	1017.6	0.86		145
12	AAR	17	1530	X	20.6	16.66	91.4	1013.6	0.81	0.6	Utl
12	MAR	LĹ	1559	S	23.6	17.28	79.3	1017.2	0.73		133
12	MAR	11	1600	æ	20.5	16.62	92.1	1018.2	0.70	0.7	136
2	MAR	77	1630	æ	20.5	16.67	91.9	1018.0	0.53	0.7	126
12	MAR	77	1700	×	20.5	16.65	92.0	1018.0	0.41	0.8	133
14	AAK	17	930	X	22.9	8.92	42.6	1019.2	0.75	0.5	201
14	MAR	11	1000	*	23.0	8.03	38.2	1015.6	0.93	2.7	70
14	MAR	17	1000	£	23.4	7.58	35.1	1019.2	0.89	0.7	44
14	MAR	11	1028	S	26.5	9.62	37.1	1018.4	1.01		49
14	MAR	22	1030	•	23.4	6.83	31.5	1015.7	1.92	2.8	25
14	PAR	77	1030	T	23.9	6.24	28.0	1019.3	0.99	0.5	50
14	XDM	17	1100	-	23.6	6.66	30 . 4	1015.7	1.10	2 • 8	28
14	51 A 15	17	1100	£	24.4	5.67	24.7	1019.2	1.07	0.7	45
14	MAR	77	1130	-	23.7	6.50	29.6	1015.7	1.17	3•6	42
14	XAN	17	1130	æ	24.4	5.30	23.1	1019.2	1.14	1.0	28
14	<b>4 4 4</b>	11	1200	~	23.3	6.59	30.6	1015.4	1.21	4.2	61
14	MAR	17	1200	æ	24.6	5.49	23.7	1019.2	1.19	1.0	40
47	MAK	17	1230	►	23.6	7.16	32.8	1015.2	1.23	3•3	50
14	244	77	1230	æ	24.4	6.06	26.4	1019.0	1.21	0.9	27
14	NAR	17	1258	s	26.0	7.06	27.9	1017.6	1.26		42
14	X D L	Li	1300	►	23.1	7.39	34.8	1015.0	1.23	3.9	111
14	NAK	22	1300	¥	24.3	6.27	27.5	1018.9	1.20	1.0	30
14	N A R	77	1330	-	23.4	7.29	33.9	1014.7	1.20	3.9	61
4	A A M	77	1330	3	24.3	6.19	27.1	1018.4	1.17	0.9	66
14	X M H	77	1400	+	23.4	7.63	35.3	1014.4	1.14	3•5	55
24	MAR	17	1400	æ	24.7	6.43	27.5	1018.1	1.12	0 • B	ري د
14	MAR	22	1430		23.5	8.12	37.4	1014.1	1.06	3 <b>.</b> 3	4

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2				     	1		:	4		•	
1 4 1		TEAK		SLIE	AT (DEG)	CTORR)	H¥ E	BP (MRAR)	CH DSCH)		(DEG)
								•		<b>k</b> 	<b>1</b>
14	MAR	11	1430	#	24.2	6.45	28.4	1017.6	1.05	6•0	24
14	a a a	11	1458	Ś	26.5	6.93	26.7	1016.7	1.11		39
14	MAK	11	1500	+	22.8	8.28	39.9	1014.0	0.98	3.4	30
14	M A R	17	1500	X	24.2	6.18	27.3	1017.6	0.95	0.8	56
14	MAR	11	1530	►	22.4	8.15	40.1	1014.1	0.87	3.0	31
14	MAR	17	1530	X	23.8	6.07	27.5	1017.5	0.83	0.8	33
14	5 A K	11	1558	\$	24.8	9.13	39.0	1016.1	0.74		58
14	X N M	11	1600	يعو	22.6	8.02	39.0	1013.8	0.74	2.6	28
14	AAR	17	1600	Ŧ	23.5	6.29	29.0	1017.2	0.69	0.9	46
14	MAR	17	1628	s	23.7	9.34	42.4	1016.0	0.52		66
14	A A R	11	1630	t	22.2	8.54	42.4	1013.5	0.60	2.4	34
4	X M K	77	1630	X	23.0	6.44	30.6	1016.8	0.55	0.9	51
44	MAR	11	1658	Ś	23.1	10.29	48.4	1016.0	0.43		66
14	MAR	11	1700	+	21.9	8.53	43.2	1013.4	0.45	2.4	24
14	MAR	77	1700	×	22.6	6.59	32.0	1016.7	0 * * 0	0.8	46
14	MAR	77	1730	æ	21.9	6.71	34.0	1016.7	0.23	0.8	
15	MAK	11	859	S	23.5	11.96	55.0	1018.3	0.37		3 û 6
15	XDN	17	006	×	21.4	9.48	49.6	1019.2	0.67	0.6	308
15	MAR	11	929	S	24.8	10.95	46.7	1018.6	0.64	0,1	311
15	d 9 W	11	930	-	22.8	9.68	46.5	1015.7	0.84	2.4	306
15	MAR	77	930	T	22.5	9.18	44.8	1019.5	0.80	0.5	303
15	MAR	17	959	S	25.8	10.92	43.9	1018.7	0.87	0.1	282
15	2 G M	11	1000	-	23.5	8.91	41.2	1015.7	6.96	2.6	279
l 5	X A K	77	1000	×	23.6	8.50	38.9	1019.4	6.0	0.3	296
57	MAR	11	1029	Ś	27.2	10.67	39.4	1018.7	1.0.1	0.1	270
15	MAR	11	1030	-	21.8	11.82	60.4	1015.8	1.06	1.3	133
15	M A K	27	1030	s:	24.4	8.98	39.3	1019.5	1.03	0.3	293
15	MAR	11	1059	Ś	28.2	10.36	36.2	1018.6	1.13	0.2	119
15	AAM	17	1100	-	23.2	11.96	51 <b>.</b> Ŗ	1015.7	1.14	2.8	20

والمتحم ومراوحة فالمتحمد المتحادين فيالتمارية والمتحمد المتحمد المحمد والمحمد والمحمد والمحمد والمحمد وسيلاتهم

UAY	HINDW	YEAR	TIME	SITE	AT	PPH20	ня	ВP	SR	٨S	HUM
					(DEC)	(TORR)	(1)	( AB B N)	(HISQ K)	(W/S)	(DEC)
15	MAR	77	1100	x	20.9	12.95	10.01	1019.5	1.12	0.7	128
15	MAR	11	1129	S	22.4	13.52	66.5	1019.6	1.22	C•2	101
41	RAK	77	1130	<b>F</b>	23.1	11.05	52.1	1015.7	1.21	2 <b>•</b> 3	26
15	MAR	11	1130	X	21.7	12.51	64.3	1019.5	1.18	0.8	128
15	244	22	1200	+	23.5	10.01	46.0	1015.7	1.24	3•2	73
15	RAK	77	1200	X	26.1	10.05	39.7	1019.5	1.21	0.7	37
15	XAM	11	1230	-	24.2	9.44	41.6	1015.6	1.24		68
15	MAR	22	1300	-	23.9	8.75	39.2	1015.3	1.23	5	42
15	MAR	11	1330	-	23.8	8.66	39.3	1014.9	1.19	3 • 5	27
15	MAR	11	1430	<b>}</b>	23.4	8.70	40.3	1014.4	1.05	3•0	<b>۴</b>
15	7 Q M	11	1500	-	23.7	8.81	40.0	1014.1	0.95	2.1	42
16	2 A M	77	1000	Ŧ	21.3	16.58	87.5	1015~2	0.93	2.0	218
16	MAR	11	1030	+	23.8	16.88	76.2	1015.3	1.04	2.4	283
16	NAK	17	1100	<b>.</b>	24.7	16.91	72.6	1015.1	0.70	2.4	236
16	NAK	17	1130		21.3	16.79	88 <b>.</b> 3	1014.9	1,22	3 • 3	78
16	MAR	77	1200	F	21.8	17.17	87.9	1014.9	0.96	3.5	41
16	2 <b>4 4</b>	17	1230	►	22.2	17.02	84.6	1014.7	1.04	3.0	75
16	X 4 1	77	1300	⊢	23.5	16.69	77.0	1014.2	0.71	2.5	38
16	MAR	11	1330	-	23.6	16.78	76.6	1014.2	1.00	2.6	45
30	NAK	17	930	-4	21.9	17.61	89.2	1020.0	0.96	2.0	143
06	X M	11	1000	-	21.7	17.27	88.9	1020.1	1.04	2.4	161
30	MAR	17	1030	-	21.9	17.19	87.3	1020.3	1.02	2.0	157
30	2 <b>4</b> 1	77	1100	-	22.3	17.37	86.1	1019.9	1.01	2.6	126
30	X A H	11	1130	F	22.8	17.09	82.0	1019.6	1.25	2.6	120
30	MAR	17	1200	⊢	23.0	17.39	82.5	1019.4	1.28	3•0	120
30	XQX	17	1230	-	22.7	17.26	83.2	1018.9	1.36	4.4	131
30	X V R	17	1300	+	22.6	17.59	85.3	1018.3	1.19	5.8	132
30	X d M	17	1330	-	22.7	17.55	84.9	1018.1	1.01	5.4	135
<b>1</b>	n a c	17	906	æ	22.6	16.46	79.8	1023.1	0.43		

MONIH YEAR TIME SITE	YEAR TIME SITE	TIME SITE	SITE		AT CDEG)	PPH20 (TGRR)	кн (2)	BP (MBAR)	SR CW/SQ M)	WS (M/S)	HOH CDEG
MAR 77 930 M 2	77 930 N 2	930 M 2	N N	2	3.8	16.07	72.6	1023.3	0.92		
MAR 77 1000 H 24	77 1000 H 24	1000 H 24	<b>x</b>	~	6.	15.57	66.0	1023.3	0.81	0.5	15
MAR 77 1030 H 25	77 1030 H 25	1030 H 25	# 25	5	0.	15.12	63.7	1023.8	0.32	0 . 9	239
MAR 77 110C H 25	77 110C H 25	110C H 25	H 25	5	• 5	15.62	64.0	1023.7	1.20	0.7	280
MAR 77 1130 M 26	77 1130 H 26	1130 m 26	<b>H</b> 26	26		15.35	60.6	1023.2	1.24	0.5	259
MAR 77 1200 M 25	77 1200 M 25	1200 M 25	M 25	25	4	16.19	66.4	1023.0	1.17	0.7	183
MAR 77 1229 5 29.	77 1229 S 29.	1229 S 29.	S 29.	29	8	17.28	54.9	1021.3	1.16	2.8	188
MAR 77 1230 H 24.	77 1230 H 24.	1230 H 24.	<b>E</b> 24.	24	2	17.49	77.1	1022.6	1.31	0.7	166
MAK 77 1259 5 28.	77 1259 5 28.	1259 5 28.	s 28.	28.	0	19.50	65.1	1020.5	1.19	3.7	147
MAR 77 1300 M 23.	77 1300 M 23.	1300 H 23.	M 23.	23.	8	18.09	81.7	1022.0	1.35	1.0	154
MAR 77 1329 5 26.	77 1329 5 26.	1329 5 26.	S 26.	26.	6	18.37	69.1	1019.8	0.84	4.1	159
MAR 77 1330 M 23.	77 1330 M 23.	1330 H 23.	H 23.	23.	ŝ	18.20	83.8	1021.5	1.00	0.9	158
MAK 77 1359 S 27.	77 1359 S 27.(	1359 S 27.(	S 27.(	27.(	~	18.34	68.4	1019.6	1.01	3.7	152
MAR 77 1400 M 23.6	77 1400 M 23.6	1400 M 23.6	m 23.6	23.6		18.02	82.6	1021.0	0.92	6.0	159
MAK 77 1429 S 26.5	i7 1429 S 26.5	1429 S 26.5	S 26.5	26.5		18.34	70.5	1019.1	0.95	4.6	154
MAR 77 1430 T 23.7	77 1430 T 23.1	1430 T 23.7	T 23.7	23.1	•	18.44	83.9	1015.1	0.77	<b>6 .</b> 8	128
MAP 77 1430 M 23.	77 1430 M 23.	1430 M 23.	M 23.	23.	5	18.29	84.0	1020.3	10.97	1.0	150
MAR 77 1459 5 26.	77 1459 S 26.	1459 S 26.	S 26.	26.	ŝ	18.37	71.4	1018.1	1.05	4.8	155
MAH 77 1500 T 23.	77 1500 T 23.	1500 T 23.	T 23.	23.	9	18.60	84.8	1015.7	0.92	5.0	129
MAR 77 1500 M 23.	77 1500 M 23.	1500 M 23.	<b>m</b> 23.	23.	4	19.33	84.9	1019.5	0.89	1.0	153
MAK 77 1529 5 26.	77 1529 S 26.	1529 S 26.	S 26.	26.	0	18.28	72.6	1017.9	0.50	4.7	155
HAK 77 1530 T 23.	77 1530 T 23.	1530 T 23.	T 23.	23.		18.61	5885	1015.3	0.55	<b>4</b> • 8	124
HAR 77 1530 M 23.3	77 1530 M 23.3	1530 M 23.3	M 23.3	23.	~	17.79	82.9	1019.3	0.44	1.1	162
MAR 77 1600 T 23.3	77 1600 T 23.3	1600 T 23.3	T 23.3	23.3	~	18.52	86.2	1014.9	0.59	<b>6 - 8</b>	130
APR 77 900 M 21.4	77 900 M 21.4	900 M 21.4	M 21.4	21.4		17.26	<b>90.4</b>	1020.8	0.57	4.0	178
APR 77 930 M 22.	77 930 M 22.	930 M 22.	m 22.	22.	0	17.34	87.6	1021.4	0.73	4.0	178
APK 77 1000 H 22.	77 1000 M 22.	1000 H 22.	<b>H</b> 22.	22.	+	17.59	86.7	1021.4	1.04	0.6	168
APK 77 1029 5 26.4	77 1029 5 26.	1029 S 26.	S 26.	26.		18.85	73.1	1020.3	0.65	3.0	153
APR 7- 1030 T 22.	7" 1030 T 22.	1030 T 22.	T 22.	22.	و	17.98	87.6	1017.8	1.04	2.8	131

- - -----فلاشل كمتعلقة فكمتر كسما يشغل

1							:	4	ļ		
A A O		YEAR	JH I L	SITE	AT (DEG)	PPH20 (TORR)	H 2 (2)	BP (MBAR)	SR (H/SQ H)	WS (W/S)	UDH CDEG)
-	APR	17	1030	I	22.6	17.64	85.9	1021.3	10.07	0.6	157
-	APR	11	1059	S	26.1	18.76	73.8	1020.2	1.00	3.4	161
	パンス	77	1100	+	22.7	17.41	84.0	1017.6	1.08	3•0	128
~	4 P R	11	1100	æ	22.6	17.80	86.6	1021.2	1.13	0.7	152
-	APR	11	1129	S	26.0	19.01	75.2	1020.4	0.94	2.1	142
-	APK	17	1130	⊢	22.3	18.00	89.4	1017.6	1.10	2.4	156
-	APR	17	1130	x	22.7	17.68	85.3	1021.2	1.24	0.6	152
	APR	11	1159	s	25.0	18.92	79.5	1020.1	1.15	2.3	113
-	APK	17	1200	-	23.1	17.93	84.8	1017.5	1.15	2.4	120
1	APR	11	1200	æ	23.0	17.55	83•3	1021.2	1.24	0.5	134
-4	APR	77	1229	Ś	24.6	18,14	78.4	1019.8	1.17	2.8	110
-	APR	11	1230	⊢	23.6	17.74	81.0	1017.1	1.17	2•5	93
7	APR	11	1230	æ	23.2	17.13	80.2	1020.9	1.25	0.6	111
-	APR	17	1259	s	24.8	17.98	76.7	1019.4	1.19	3.1	98
-1	APR	17	1300	-	23.4	17.70	81.9	1016.5	1.20	3.1	92
-	APR	22	1300	Z	23.5	17.44	80.4	1020.5	1.23	0•6	100
-	APR	17	1329	Ś	24.5	18.10	78.4	1018.8	1.10	3•5	102
	APR	77	1330	-	23.6	17.67	80.6	1016.0	1.09	3•2	63
7	APR	11	1330	T	23.5	17.32	80.0	1020.0	1.19	0.6	103
-	APH	11	1359	S	24.5	18.25	1.91	1018.2	1.07	3.7	123
	APR	11	1400	+	24.4	18.39	80.1	1015.5	1.06	4.2	111
r4	APR	11	1400	T	23.5	17.92	82.4	1019.4	1.13	0.7	124
7	APR	11	1429	S	24.7	19.92	80.9	1017.9	0.97	3•6	118
-	APR	77	1430	•	23.8	18.90	85.7	1015.2	0.99	<b>0 •  4</b>	121
-	APR	11	1430	2	23.2	18.17	85.1	1019.1	1.06	0.8	131
1	APR	17	1459	s	26.0	18.87	74.7	1017.5	0.89	4.1	140
-	APR	77	1500		23.9	19.09	85.7	1014.9	0.85	4.6	124
-	AVR	77	1500	æ	23.3	18.31	85.3	1018.5	0.99	0.9	144
-	APR	11	1529	S	25.8	19.99	76.3	1017.3	0.79	<b>4</b> . 3	138
2			1		1		:	1	1		
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	HINDE	TEAR	T I ME	SITE	AT (DEG)	PPH20 (TORR)	HE CE	8P (48AR)	CH SE M)	(M/S)	0101 101
-	APK	77	1530	-	23.8	18.97	85.8	1014.8	0.77	<b>4</b> . 8	132
-	APR	17	1530	T	23.4	18.34	85.0	1018.1	0.83	0.8	136
-	APR	17	1559	S	26.3	19.37	75.5	1017.2	0.67	4.4	147
-	APR	11	1600	<b>}</b>	23.7	19.42	88.4	1014.7	0.66	4.4	127
N	APR	17	930	-	22.2	17.58	87.5	1018.4	0.77	3.4	152
2	APR	11	933	S	25.4	18.44	75.6	1021.3	0.75	3.2	149
~	APR	17	1000	-	22.3	17.79	87.9	1018.4	10.97	3.1	159
~	APR	17	1003	S	25.7	18.46	74.3	1021.3	0.89	3.2	149
2	Ark	11	1030	-	22.5	17.87	87.4	1018.4	1.03	3.9	160
2	APR	11	1033	v	25.8	18.44	74.0	1021.3	1.02	3.7	160
~	APR	77	1100	⊷	22.7	18.26	58.2	1019.4	1.10	3.7	150
2	APK	11	1103	\$	25.8	18.64	74.6	1021.3	1.09	3.6	149
2	APR	11	1130	+	23.0	18.53	88.1	1018.1	1.15	3•6	143
2	APK	77	1133	Ś	26.0	18.90	75.0	1020.9	1.12	3•3	152
~	APR	17	1200	⊢	23.4	18.45	85.6	1018.0	1.19	4.7	142
~	APR	11	1203	s	24.1	18.80	74.2	1020.7	1.19	3.8	148
2	APK	11	1230	⊢	23.7	18.62	84.5	1017.8	1.21	<b>4 .</b> 8	136
2	APR	77	1233	S	26.1	18.87	74.3	1020.4	1.19	4 • 2	149
~	APR	11	1300	-	23.7	18.57	84.4	1017.3	1.19	5.1	123
2	APK	17	1303	S	25.8	18.83	75.7	1020.1	1.21	4.6	138
2	AVR	77	1330	•	23.9	18.62	83.6	1016.9	1.11	5.2	122
N	APR	17	1333	Ś	26.3	18.90	7,6;	1019.7	1.17	4 • 4	147
2	APK	77	1400	-	23.9	18.67	83.8	1016.6	1.06	<b>4</b> .9	124
2	APR	17	1403	S	26.2	18.73	73.2	1019.3	1.09	4.8	142
~	APR	11	1430	-	24.2	19.12	84.6	1016.3	\$6*0	4.9	120
~	APK	17	1433	S	26.1	18.94	74.6	1018.8	0.98	6.4	139
2	APR	77	1500	►	24.0	18.77	84.0	1015.8	0.87	6.2	131
2	8 P Q	77	1503	S	26.3	18.73	72.9	1018.5	0.93	5.8	149
2	APR	27	1530	-	24.0	18.80	83.9	1015.7	0.78	6.2	135

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South Contraction of the State

VAU	HINDH	YEAR	TIME	SITE	AT 1000	DCHOO	НИ	9.0 1 1 1 1	SR 201	SH	HOH
					(DEG)	(ICKR)	Ê	( HBAR )		(4/2)	CDEC)
2	APK	77	1533	Ś	26.2	18.60	72.8	1018.3	0.83	5.9	150
2	APK	11	1600	-	24.0	19.84	84.0	1015.7	0.66	6.2	: 35
2	APR	77	1630	<b></b>	23.9	18.96	85.0	1015.6	0.51	6.4	136
4	APR	11	929	Ś	24.6	18.57	79.9	1016.0	0.78	6.1	169
4	APR	17	930	×	22.2	17.80	88.5	1016.8	0.91	1.3	169
4	APR	77	959	S	24.8	18.62	79.1	1016.0	0.96	6.1	166
4	APR	17	1000	⊢	22.9	18.19	87.0	4.6101	1.01	7.4	156
4	APK	17	1000	X	22.5	17.79	80	1016.9	1.02	1.3	167
4	APR	77	1029	S	24.8	18.55	78.9	1015.9	1.04	6.9	164
4	APR	17	1030	+	23.1	18.24	86.1	1013.2	1.10	7.3	154
4	APK	77	1030	Ħ	22.7	17.92	86.3	1016.6	1.12	1.4	163
*	APR	17	1059	S	24.9	18.55	78.4	1015.5	1.11	6.8	160
4	APK	11	1100	+	23.2	18.30	85.8	1013.0	1 0 1	7.2	147
4	APR	77	1100	æ	22.9	17.96	85 <b>.</b> 8	1016.3	1.18	1.3	160
4	APR	77	1129	S	25.0	18.41	7.75	1015.2	1.17	7.0	161
4	Ark	17	1130	+	23.3	19.18	84.6	1012.7	1.22	7.7	148
4	B P G	11	1130	W	23.0	17.80	84.6	1016.1	1.23	1.4	162
4	APR	17	1159	S	25.1	18.50	77.2	1014.8	1.16	7.3	159
4	AFR	77	1200	►	23.5	18.30	84.1	1012.4	1.26	8.2	148
4	APR	11	1200	T	23.2	16.7.	84.1	1215.8	1.29	1.6	159
4	APR	77	1229	S	25.0	18.78	; 8 <b>.</b> 9	1014.3	1.24	8.1	161
4	A T K	17	1230	<b>p</b>	23.5	18.53	85.1	1011.9	1.24	9.6	147
4	APR	77	1230	X	23.3	18.23	94.9	1015.1	0.30	1.7	159
4	APR	17	1259	S	25.0	18.80	19.0	1013.8	1.23	7.7	161
4	Arr	11	1300	-	23.6	18.56	85.1	1011.4	1.24	9.1	148
4	21 d 8	17	1300	æ	23.3	18.21	85.0	1014.6	1.25	1.6	163
4	APR	77	1329	S	25.0	18.78	78.8	1013.1	1.19	9•3	162
4	APW	17	1330	-	23.7	18.59	84.8	1010.9	1.21	10.1	149
4	APR	17	1330	X	23.3	19.24	84.8	1013.9	1.21	1.8	162

وماغف فبرخانه أسفوهم فلانته بشكميه سا

~ ちょうぶつ ちまだ しまれん

V A U	HANGE	YEAR	J#I1	SITE	AT	PPH20	Hav	9.0	SR	N S	HON
					( 930)	(TORK)		( H B A R )	CH/SQ H)		CDEG
4	AVK	77	1359	5	25.3	18.85	78.1	1012.7	1.08	8.9	164
4	APR	77	1430	-	23.7	18.54	84.4	1010.4	1.15	6.6	151
4	APR	11	1400	æ	23.4	18.20	84.4	1013.4	1.16	1.8	162
4	Ark	11	1429	S	25.5	18.80	76.7	1012.2	1.07	8.2	165
*	APR	11	1430	<b>*</b>	23.8	18.45	83.6	1009.9	1.05	9•6	149
4	APR	11	1430	X	23.4	13.06	83.7	1013.1	1.08	1.7	163
4	APR	11	1459	S	25.4	18.67	76.5	1011.7	7 6 . 0	8.7	164
4	APR	11	1500	-	23.8	18.51	83.8	1009.5	0.90	9.8	153
4	APR	11	1500	æ	23.4	18.04	83.5	1012.8	1.01	1.8	164
4	APR	11	1529	S	25.2	18.67	77.4	1011.5	0.77	9.2	162
4	APR	17	1530	æ	23.4	18.18	83.9	1012.3	0.84	1.9	162
ŝ	APR	17	930	-	24.4	17.85	78.0	1009.7	0.84	12.1	184
ŝ	APR	77	1003	S	28.2	17.51	61.0	•		9.3	
Ś	APR	17	1033	s	29.6	17.01	54.6			8.4	
Ś	APR	17	1103	S	30.3	15.94	49.3			8•3	
ŝ	<b>A</b> P K	11	1133	S	31.5	16.00	46.2	1013.0	1.00	9.3	233
ŝ	<b>A</b> P R	77	1203	S	31.1	15.17	44.8	1013.0	0.46	10.4	237
\$	APR	77	1233	S	30.8	15.01	45.1	1012.9	0.50	9.2	275
ŝ	APK	17	1303	S	25.7	14.40	58.1	1013.8	1.06	7.5	293
Ś	APR	17	1333	S	24.9	13.88	58.9	1014.3	0.36	5.3	292
ŝ	APR	11	1403	S	د <b>4.</b> 2	12.33	54.3	1014.2	0.81	6.8	296
ŝ	AVR	17	1433	S	25.4	12.21	50.3	1014.1	0.92	5.6	281
ŝ	APR	17	1503	S	<b>5</b> •2	10.83	44.9	1013.8	0.43	6•3	260
5	APR	17	1533	s	24.9	16*6	41.9	1013.7	0.52	4.9	267
v	AFR	17	1100	►	18.3	7.14	45.4	1023.2	0.95	5.0	230
•	APR	17	1130	-	18.0	6.95	45.0	1023.1	0.97	<b>8 • 4</b>	193
9	A P K	77	1200	+	17.9	6.96	45.2	1023.0	1.23	5.3	145
9	APK	11	1230	•	18.0	7.03	45.4	1022.8	0.98	5.2	276
9	APR	77	1400	•	18.0	7.01	45.2	1022.4	1.15	5.2	90

UAY	HINDE	YEAR	TME	SITE	AT CDFG)	PPH20	RH (2)	BP (MRAR)	SR CH/SQ M)	WS W	NDH CDEG)
							r A				
•	APR	11	1430	۰.	17.9	6.97	45.4	1022.1	1.02	<b>4 • 5</b>	153
9	A P R	11	1500	-	18.0	7.07	45.7	1021.9	0.99	4.8	66
9	APK	11	1530	-	18.0	5.97	45 °2	1021.7	0.87	4.2	52
9	APR	77	1600	-	17.8	6.84	44.7	1021.6	0.76	4.0	16
Ŷ	APR	17	1630	-	17.6	7.20	47.9	1021.6	0.59	4.1	62
~	APK	11	1000	+	21.4	6.51	34.2		0.89		
~	APR	17	1030	-	21.2	7.16	37.9		1.00		
~	APK	17	1100	-					1.08		
~	APK	17	1130	-					1.13		
~	APR	11	1200	-					1.17		
~	4 d K	11	1230	-4					1.20		
7	AI	17	1300	-					1.19		
~	a q a	17	1330	+					1.15		
~	APK	17	1400	•					1.10		
~	APR	17	1430	+					1.01		
16	Y A Y	17	1429	Ś	25.4	14.47	59.4	982.1	1.26	4.5	123
16	MAY	77	1459	s	25.3	15.36	63.3	981.1	1.20	5•5	104
16	MAY	77	1529	s	25.4	15.57	64.1	978.4	1.10	5.4	104
16	MAY	11	1559	S	25.4	15.47	63 <b>.</b> 5	976.4	1.04	5.0	106
16	N A Y	11	1629	s	25.5	15.32	62.6	976.3	0.92	5.2	104
16	X A Y	11	1659	s	25.6	15.32	62.3	974.3	0.80	4.8	104
17	444	17	1000	S	25.6	18.01	73.1	1024.7	0.81	<b>6 • 3</b>	76
17	1 A V	77	1030	r	25.6	18.16	6°£1	1024.9	0.65	5.0	80
11	Y A M	77	1100	S	25.7	18.25	73.7	984.5	1.07	5 • 2	73
17	MA Y	11	1130	s	25.5	17.46	4.11	919.5	1.15	6.0	11
17	Y A M	77	1200	s	25.4	17.22	70.6	978.4	1.22	5.7	75
11	MAY	77	1230	S	25.4	17.03	69.9	978.8	1.27	6.1	
11	N A Y	11	1,000	S	25.5	16.79	68.7	916.7	1.31	5 . 4	6,8
17	* 4 #	77	1330	Ś	25.4	16.23	66.6	974.9	1.32	5 • 1	r **

**द ीक** %7}^

مندومه فترك والأكاميرة فكالأوريب أعدالا الالاستسامة فالايس والايس والموس ومعادة والمرابع معادله والمناطق ومالغان وملقاته ومطلوبها وملاحك بنعار ويخاسب يتر

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UAY	HINDH	YEAR	TIME	SITE	AT (DFG)	PPH20 (TORR)	АН ( 2 )	BP (MBAR)	SR (W/SO M)	45 (M/S)	UEG)
17	MAY	77	1400	S	25.7	16.29	65.9	974.2	1.31	5.0	70
17	Y A M	11	1430	S	25.5	16.13	65.7	973.1	1.30	5•3	76
17	Y D M	17	1500	s	25.6	16.13	65.4	972.9	1.24	5.2	75
17	MAY	17	1530	s	25.7	15.71	63.4	973.1	1.18	4.8	72
17	ΥΔM	11	1600	S	25.9	15.40	61.6	973.4	1.07	4 • 5	75
17	1 A M	77	1630	Ś	26.1	15.51	61.1	1.179	0.93	4.7	61
11	MAY	17	1700	S	26.1	15.89	62.5	973.6	0.80	4.5	61
18	Y A M	11	928	5	25.8	15.53	62.3	1022.7	0.69	2.4	70
18	TAM	77	958	Ś	26.0	15.55	61.6	1022.9	0.89	2.7	88
18	447	77	1028	5	26.0	15.45	61.2	1023.1	0.71	3•3	79
Я М	Y D M	11	1058	S	26.2	15.69	61.6	1023.2	1.11	3.2	88
18	NAY	77	1128	\$	26.3	15.53	60.4	1023.3	1.18	3.0	69
20	YAM	77	1003	5	27.0	14.71	55.0	1019.5	0.82	2.8	106
26	Y A M	11	1033	S	27.1	14.65	54.4	1019.6	0.96	3•5	16
20	MAY	77	1103	Ś	27.4	14.43	52.7	1019.8	1.06	2.7	104
20	MAY	11	1133	S	27.6	14.10	50.8	1019.9	1.16	3.0	98
25	M A Y	11	1203	\$	27.5	13.82	50.1	1019.9	1.24	4.7	92
20	N A M	11	1233	5	21	14.18	52.6	1019.8	1.28	5.3	έu
20	NAY	77	1303	5	26.9	14.23	53.6	1019.8	1.31	6.4	£6
20	MAY	77	1333	5	26.7	14.67	55.9	1019.5	1.33	6.2	06
20	447	17	1403	Ś	26.7	14.78	56.1	1019.7	1.29	3.1	84
20	MAY	11	1433	S	26.6	14.96	56.9	1019.5	1.22	3.5	61
20	YAM	11	1503	Ś	26.8	14.90	56.4	1019.6	1.18	3•2	87
20	Y M Y	11	1533	s	26.8	14.92	56.6	1019.4	1.09	3•5	89
20	Y A M	11	1603	S	26.8	15.20	57.6	1019.0	1.03	3.8	88
21	YAM	11	1031	S	26.0	16.11	63.7	1019.4	0.98	5.2	96
21	ADW	17	1101	Ś	26.2	16.36	64.2	1019.6	1.07	4.7	40
21	YAN	11	1131	Ś	26.2	16.17	63.3	1020.1	1.16	5.2	86
21	A A M	11	1201	S	26.3	16.38	63.9	1020.2	1.22	5.0	95

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ն<mark>երնել,</mark> անհան հետուրել մուս էրուսել դուսել ծենել։ «Երջեն հուրել ենելու է ենել

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MAY   77   1231   5   26.3   16.57   63.5   960.8   1.20     MAY   77   1301   5   26.2   16.57   64.1   1019.9   1.20     MAY   77   1401   5   26.2   16.57   64.1   1019.9   1.20     MAY   77   1401   5   26.2   16.57   67.4   1019.9   0.58   3.3     MAY   77   1501   5   26.2   16.65   65.5   1019.9   0.58   3.3     MAY   77   1501   5   26.5   18.16   65.5   1016.1   0.96   3.3<	►	HINDW	YEAR	TIME	SITE	AT (DEG)	РРН20 (такк)	HR (X)	вр (мчдр)	SR (H/SQ H)	HS (H/S)	HDH CDEG
MAY   77   1301   5   26.2   16.50   64.7   1019.9   1.20   4.4     MAY   77   1401   5   26.3   16.67   67.4   1019.9   0.58   3.3     MAY   77   1401   5   26.3   16.67   67.4   1019.9   0.58   3.3     MAY   77   1501   5   26.5   18.16   65.5   1019.9   0.58   3.3     MAY   77   1501   5   26.5   18.16   65.5   1016.5   0.56   3.3     MAY   77   1033   5   27.7   18.21   65.5   1016.1   0.35   3.3     MAY   77   1033   5   27.7   18.21   65.5   1016.1   0.36   3.3     MAY   77   1133   5   25.5   17.70   72.4   1016.6   0.46   1.6     MAY   77   1203   5   25.6   17.761   61.5   1016.4   1.05   4.4     MAY   77   1203   5   1016.		4 A M	77	1231	ŝ	26.3	16.27	63.5	960.8	1.28	4•3	106
MAY   77   1331   5   26.3   16.48   64.1   1019.9   1.48   4.6     MAY   77   1501   5   25.8   16.77   67.4   1019.9   0.58   3.3     MAY   77   1501   5   26.7   16.62   65.7   1019.9   0.58   3.3     MAY   77   1033   5   27.7   165.5   1016.1   0.36   3.3   3.8     MAY   77   1033   5   27.7   18.21   65.5   1016.1   0.36   3.3   3.2     MAY   77   11033   5   27.3   177   1015.1   0.35   1.7   7     MAY   77   11033   5   27.3   177   1015.1   0.35   1.4   4.3     MAY   77   11033   5   25.9   17.701   10.5   1.005   1.015   1.4   4.4     MAY   77   1203   5   25.0   17.701   1015.6   1.015   1.4   4.4     MAY   77   1203		A A M	77	1301	Ś	26.2	16.50	64.7	1019.9	1.20	4 - 4	108
MAY   77   1401   5   25.8   16.77   67.4   1019.5   0.58   3.8     MAY   77   1431   5   26.7   16.77   67.4   1019.5   0.691   3.8     MAY   77   1601   5   26.7   16.75   65.5   1016.5   0.91   3.2     MAY   77   1033   5   26.6   17.72   65.5   1016.5   0.95   3.0   3.6     MAY   77   11033   5   27.3   17.72   65.5   1016.5   0.31   1.6   3.0     MAY   77   1133   5   25.5   17.77   65.5   1016.5   0.31   1.6   7     MAY   77   1203   5   25.7   17.76   65.5   1016.5   1.02   66.5   1.7   7   1.02   7   1.6   7   1.6   7   1.6   7   1.4   1.7   1.6   1.7   1.6   7   1.1   1.7   1.6   1.7   1.6   1.7   1.6   1.7   1.1   1.7 <td></td> <th></th> <td>11</td> <td>1331</td> <td>S</td> <td>26.3</td> <td>16.48</td> <td>64.1</td> <td>1019.9</td> <td>1.48</td> <td>4.6</td> <td>104</td>			11	1331	S	26.3	16.48	64.1	1019.9	1.48	4.6	104
MAY   77   1431   5   26.7   16.62   65.7   1019.5   1.29   3.0     MAY   77   1501   5   26.7   16.62   65.5   1016.1   0.91   3.2     MAY   77   1003   5   26.7   16.62   65.5   1016.1   0.91   3.2     MAY   77   1003   5   27.3   17.77   65.5   1016.1   0.35   1.7   1.7     MAY   77   1103   5   28.1   17.77   65.5   1016.1   0.35   1.7   1.7     MAY   77   1133   5   25.5   17.70   72.4   1016.1   0.35   1.7   1.7     MAY   77   1203   5   25.5   17.70   72.4   1016.1   0.35   1.6   1.7     MAY   77   1203   5   25.5   17.70   72.4   1016.1   0.35   1.6   1.7   1.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0		YAM	77	1401	S	25.8	16.77	67.4	1019.9	0.58	<b>3</b> •8	69
MAY   77   1501   5   26.7   16.75   63.7   1016.1   0.36   3.3   2     MAY   77   1033   5   27.3   17.72   65.5   1016.1   0.35   1.7   1     MAY   77   1033   5   27.3   17.72   65.5   1016.1   0.35   1.7   1     MAY   77   1133   5   25.5   17.70   71.6   1016.4   1.02   8.4   2.0   2   2   2   2   1   1.6   1   1.7   1.7   1.7   1.4   1.7   1.0   3<		A A M	77	1431	S	26.2	16.62	65.2	1019.8	0.91	3•2	62
MAY   77   933   5   76.6   18.16   69.4   1016.5   0.66   3.3   3     MAY   77   1003   5   27.7   18.21   65.5   1016.1   0.84   2.0   5     MAY   77   1103   5   27.3   17.72   65.5   1016.4   1.02   4.4     MAY   77   1133   5   259.5   17.70   72.4   1016.4   1.02   4.4     MAY   77   1203   5   25.5   17.70   72.4   1016.4   1.02   4.4     MAY   77   1203   5   256.9   17.54   67.3   1016.4   1.02   4.4     MAY   77   1303   5   26.6   17.54   67.3   1015.5   1.10   2.6   1.7     MAY   77   1303   5   26.6   17.54   67.3   1015.6   1.6   4.6     MAY   77   1303   5   26.1   17.96   72.4   1016.1   1.6   4.6     MAY   77		<b>7 8 8</b>	17	1501	S	26.7	16.75	63.7	1019.5	1.29	3•0	8 0 8 0
MAY   77   1003   5   27.7   18.21   65.5   1016.1   0.84   2.0   2     MAY   77   1103   5   27.3   17.72   65.2   1016.1   0.35   1.7     MAY   77   1103   5   25.5   17.77   65.2   1016.4   1.02   5   1.7     MAY   77   1203   5   25.5   17.70   72.4   1016.4   1.02   4.4     MAY   77   1203   5   25.5   17.94   77.6   1016.4   1.02   4.4     MAY   77   1333   5   26.6   17.96   77.6   1015.5   1.10   2.6     MAY   77   1333   5   26.6   17.96   77.9   1015.5   1.10   2.6     MAY   77   1503   5   26.1   17.96   77.9   1015.5   1.10   2.6     MAY   77   1503   5   26.1   17.96   77.9   1015.5   1.16   3.6     MAY   77   1603		Y A M	11	933	S	26.6	18.16	69.4	1016.5	0.66	3•3	261
MAY   77   1033   5   27.3   17.72   65.2   1016.1   0.35   1.7     MAY   77   1103   5   28.1   17.61   61.9   1016.1   0.35   1.7     MAY   77   1103   5   28.1   17.61   61.9   1016.1   0.35   1.7     MAY   77   11203   5   25.5   17.70   72.4   1016.1   0.31   1.6     MAY   77   1203   5   25.5   17.796   72.4   1016.1   0.46   1.7     MAY   77   1303   5   26.6   17.56   67.3   1015.5   1.10   2.6     MAY   77   1333   5   26.4   17.56   67.3   1015.5   1.46   3.4     MAY   77   1433   5   26.4   17.56   70.8   968.1   1.73   4.6     MAY   77   1503   5   26.1   17.96   72.8   971.1   1.10   2.6     MAY   77   1603   5   70.3 </td <td></td> <th>YAM</th> <td>11</td> <td>1003</td> <td>s</td> <td>27.7</td> <td>18.21</td> <td>65.5</td> <td>1016.1</td> <td>0.84</td> <td>2 • 0</td> <td>231</td>		YAM	11	1003	s	27.7	18.21	65.5	1016.1	0.84	2 • 0	231
MAY   77   1103   5   28.1   17.61   61.9   1015.9   0.31   1.6     MAY   77   1133   5   25.5   17.70   72.4   1016.4   1.02   4.4     MAY   77   1233   5   25.5   17.70   72.4   1016.4   1.02   4.4     MAY   77   1233   5   25.5   17.79   72.4   1016.4   1.02   4.4     MAY   77   1303   5   26.6   17.441   65.6   1015.5   1.10   2.6     MAY   77   1303   5   26.6   17.451   65.6   1015.5   1.10   2.6     MAY   77   1403   5   26.6   17.451   67.2   967.7   1.38   4.6     MAY   77   1503   5   26.6   18.71   77.9   9015.5   1.10   2.6     MAY   77   1603   5   26.3   18.71   77.9   971.1   1.13   4.6     MAY   77   1603   5   26.3<		N A Y	11	1033	Ś	27.3	17.72	65.2	1016.1	0.35	1.7	22
MAY   77   1133   5   55.5   17.70   72.4   1016.4   1.02   4.4     MAY   77   1203   5   25.9   17.94   71.6   1016.4   1.48   4.3     MAY   77   1203   5   25.9   17.94   71.6   1016.4   1.48   4.3     MAY   77   1203   5   26.9   17.96   72.3   1016.1   0.46   1.7     MAY   77   1333   5   26.6   17.54   67.3   1015.5   1.10   2.6     MAY   77   1333   5   26.6   17.56   0.46   1.7   8.3     MAY   77   1403   5   26.6   17.96   70.8   968%   1.10   2.6     MAY   77   1503   5   26.1   17.96   70.8   968%   1.133   4.6     MAY   77   1503   5   26.1   17.96   70.8   971.1   1.133   4.6     MAY   77   1603   5   21.10   72.9		YAY	17	1103	s	28.1	17.61	61.9	1015.9	0.31	1.6	108
MV   77   1203   5   25.9   17.94   71.6   1016.1   0.44   1.7     MV   77   1233   5   25.7   17.96   72.3   1016.1   0.44   1.7     MV   77   1233   5   26.9   17.41   65.6   1015.6   0.46   1.7     MV   77   1333   5   26.6   17.554   67.3   1015.5   1.10   2.6     MV   77   1403   5   26.6   17.554   67.3   1015.5   1.10   2.6     MV   77   1603   5   26.1   17.96   70.8   968.1   1.38   4.6     MV   77   1503   5   26.1   17.96   70.8   968.1   1.13   3.5     MV   77   1503   5   26.1   17.96   72.7   967.7   1.39   4.6     MV   77   1603   5   26.3   18.71   77.9   1016.4   0.67   2.6     MV   77   1603   5   26.3   <		Y A M	11	1133	S	25.5	17.70	72.4	1016.4	1.02	4.4	19
MAY   77   1233   5   55.7   17.96   72.3   1016.1   0.44   1.7     MAY   77   1303   5   26.9   17.54   65.6   1015.6   0.46   1.7     MAY   77   1303   5   26.6   17.554   67.3   1015.5   1.10   2.6     MAY   77   1403   5   26.6   17.564   67.3   1015.5   1.10   2.6     MAY   77   1433   5   26.6   17.564   67.3   1015.5   1.10   2.6     MAY   77   1503   5   26.1   17.96   70.8   968.1   1.38   4.6     MAY   77   1503   5   26.0   18.70   72.9   967.77   1.38   4.6     MAY   77   1603   5   26.3   18.71   77.9   971.1   1.13   3.5     MAY   77   1603   5   27.3   21.20   77.9   1014.7   1.013   3.5     MAY   77   901   5   27.3<		¥ 8 M	17	1203	S	25.9	17.94	71.6	1016.4	1.48	4.3	83
MAY   77   1303   5   26.9   17.41   65.6   1015.5   1.10   2.6     MAY   77   1333   5   26.6   17.55   67.3   1015.5   1.10   2.6     MAY   77   1403   5   26.6   17.55   67.3   1015.5   1.10   2.6     MAY   77   1403   5   26.6   17.50   67.6   1015.5   1.46   3.4     MAY   77   1503   5   26.1   17.96   70.8   968.1   1.33   4.6     MAY   77   1503   5   26.1   18.79   72.2   967.7   1.33   4.6     MAY   77   1503   5   26.0   18.71   72.9   971.1   1.13   3.5     MAY   77   1603   5   26.3   18.71   77.9   1016.3   0.67   4.0     MAY   77   1603   5   21.25   77.9   1016.1   1.13   3.5     MAY   77   931   77.9   1016.6   0.67<		Y A M	11	1233	s	25.7	17.96	72.3	1016.1	0.44	1.5	125
MAY   77   1333   5   26.6   17.54   67.3   1015.5   1.46   3.4     MAY   77   1403   5   26.4   17.61   68.2   1015.5   1.46   3.4     MAY   77   1403   5   26.4   17.61   68.2   1015.5   1.46   3.4     MAY   77   1503   5   26.1   19.28   72.2   967.7   1.39   4.6   3.4     MAY   77   1503   5   26.0   18.59   73.0   971.1   1.13   3.5     MAY   77   1603   5   26.3   18.71   77.9   1014.7   1.13   3.5     MAY   77   1603   5   26.3   18.71   77.9   1014.7   1.13   3.5     MAY   77   1603   5   26.3   18.71   77.9   1016.9   0.21   2.2     MAY   77   1831   5   21.25   77.9   1016.9   0.7   1.05   3.8     MAY   77   931   5		A D M	22	1303	s	26.9	17.41	65.6	1015.6	0-46	1.7	132
MAY   77   1403   5   26.4   17.61   68.2   1015.5   1.46   3.4     MAY   77   1433   5   26.1   17.96   70.8   968.1   1.38   4.8     MAY   77   1503   5   26.1   18.79   70.8   967.7   1.38   4.6     MAY   77   1503   5   26.1   18.79   72.7   967.7   1.39   4.6     MAY   77   1503   5   26.0   18.39   72.0   971.1   1.13   3.5     MAY   77   1603   5   26.5   18.71   77.9   1014.7   1.13   3.5     MAY   77   1603   5   26.3   18.71   77.9   1014.7   1.05   3.8     MAY   77   1603   5   26.3   18.71   77.9   1016.9   0.21   2.2     MAY   77   901   5   27.3   71.9   1016.9   0.73   1.7     MAY   77   1931   5   26.5   76.5		Y A M	17	1333	Ś	26.6	17.54	67.3	1015.5	1.10	2.6	113
MAY   77   1433   5   26.1   17.96   70.8   968.1   1.38   4.8     MAY   77   1503   5   26.1   19.28   72.7   967.7   1.39   4.6     MAY   77   1503   5   26.1   19.28   72.7   967.7   1.39   4.6     MAY   77   1503   5   26.0   18.39   72.7   967.7   1.39   4.6     MAY   77   1503   5   26.0   18.71   77.9   971.1   1.13   3.5     MAY   77   1603   5   26.3   18.71   77.9   1014.7   1.05   3.8     MAY   77   901   5   27.3   21.10   82.1   1016.9   0.73   1.7     MAY   77   931   5   77.9   1016.6   0.73   1.7   1.05   3.8     MAY   77   931   5   27.2   20.57   76.0   960.9   1.16   3.7     MAY   77   1131   5   26.5   <		Y A M	77	1403	s	26.4	17.61	68.2	1015.5	1.46	3.4	87
MAY   77   1503   5   26.1   19.28   72.7   967.7   1.39   4.6     MAY   77   1503   5   26.0   18.39   73.0   971.3   0.67   4.6     MAY   77   1533   5   26.0   18.39   73.0   971.1   1.13   3.5     MAY   77   1533   5   26.3   18.71   77.9   971.1   1.13   3.5     MAY   77   1603   5   26.3   18.71   77.9   1014.7   1.13   3.5     MAY   77   931   5   26.3   18.71   77.9   1016.8   6.55   2.2     MAY   77   931   5   28.1   21.25   77.9   1016.8   6.55   2.6     MAY   77   1911   5   27.2   20.52   76.0   1016.69   0.73   1.7   1.7     MAY   77   1101   5   27.2   20.52   76.5   1017.1   1.27   3.8     MAY   77   1201   5		YAM	11	1433	Ś	26.1	17.96	70.8	968.1	1.38	<b>4 .</b> 8	80
MAY   77   1533   5   26.0   18.39   73.0   971.3   0.67   4.0     MAY   77   1603   5   26.2   18.55   72.8   971.1   1.13   3.5     MAY   77   1603   5   26.3   18.71   77.9   1014.7   1.05   3.8     MAY   77   1603   5   26.3   18.71   77.9   1016.4   1.13   3.5     MAY   77   1831   5   26.3   21.10   82.1   1016.4   0.21   2.2   2.2     MAY   77   901   5   27.3   21.25   77.9   1016.6   0.73   1.7   1.05   3.8     MAY   77   931   5   27.2   20.52   76.0   1016.9   0.73   1.7		N A M	11	1503	S	26.1	19.28	72.2	967.7	1.30	4.6	15
MAY   T7   1603   5   26.2   18.55   72.8   971.1   1.13   3.5     MAY   77   1633   5   26.3   18.71   77.9   1014.7   1.05   3.8     MAY   77   1633   5   26.3   18.71   77.9   1014.7   1.05   3.8     MAY   77   831   5   26.3   18.71   77.9   1016.4   0.21   2.2     MAY   77   901   5   27.3   21.25   77.9   1016.9   0.21   2.2     MAY   77   931   5   28.1   21.25   77.9   1016.9   0.73   1.7   1.7   1.7     MAY   77   1301   5   27.2   20.52   76.5   1017.1   1.29   3.3   1.7   1.17   1.7		Y D M	77	1533	s	26.0	18.39	73.0	971.3	0.67	4.0	82
MAY   77   1633   5   26.3   18.71   72.9   1014.7   1.05   3.8     MAY   77   831   5   26.3   21.10   82.1   1016.8   0.21   2.2     MAY   77   901   5   27.3   21.10   82.1   1016.8   0.21   2.2     MAY   77   901   5   27.3   21.25   77.9   1016.9   0.73   1.7     MAY   77   931   5   28.1   21.25   77.9   1016.9   0.73   1.7     MAY   77   931   5   28.1   21.33   75.0   1016.9   0.73   1.7     MAY   77   1101   5   27.2   20.52   76.5   1017.1   1.29   3.8     MAY   77   1201   5   26.4   20.27   76.5   1017.2   1.47   4.3     MAY   77   1231   5   26.5   20.27   78.1   76.5   10.3   1.45   4.3     MAY   77   1201   5		Y A M	17	1603	S	26•2	18.55	72.8	971.1	1.13	3.5	8
MAY   77   831   5   26.3   21.10   82.1   1016.8   0.21   2.2     MAY   77   901   5   27.3   21.25   77.9   1016.8   6.55   2.4     MAY   77   901   5   27.3   21.25   77.9   1016.9   0.73   1.7     MAY   77   931   5   28.1   21.33   75.0   1016.9   0.73   1.7     MAY   77   1301   5   28.1   21.33   75.0   1017.1   1.16   3.3     MAY   77   1131   5   26.9   20.32   76.5   1017.1   1.29   3.8     MAY   77   1201   5   26.8   20.20   76.5   1017.2   1.37   3.1     MAY   77   1231   5   26.5   20.27   78.1   960.3   1.45   4.3     MAY   77   1201   5   26.5   20.27   78.1   960.3   1.45   4.3		Y A M	17	1633	S	26.3	18.71	72.9	1014.7	1.05	3 <b>•</b> 8	90
MAY   77   901   5   27.3   21.25   77.9   1016.8   6.55   2.4   1     MAY   77   931   5   28.1   21.33   75.0   1016.9   0.78   1.7     MAY   77   931   5   28.1   21.33   75.0   1016.9   0.78   1.7     MAY   77   1101   5   27.2   20.52   76.0   960.9   1.16   3.3     MAY   77   1131   5   26.9   20.32   76.5   1017.1   1.29   3.8     MAY   77   1201   5   26.8   20.29   76.5   1017.2   1.37   3.1     MAY   77   1231   5   26.7   20.07   76.5   1017.2   1.45   4.3   1     MAY   77   1201   5   26.5   20.27   78.1   960.3   1.45   4.3   1		¥ 4 ¥	17	831	\$	26.3	21.10	82.1	1016.3	0.21	2•2	188
MAY   77   931   5   28.1   21.33   75.0   1016.9   0.73   1.7     MAY   77   1101   5   27.2   20.52   76.0   960.9   1.16   3.3     MAY   77   1101   5   27.2   20.52   76.0   960.9   1.16   3.3     MAY   77   1131   5   26.9   20.32   76.5   1017.1   1.29   3.8     MAY   77   1201   5   26.8   20.29   76.6   1017.2   1.37   3.1     MAY   77   1231   5   26.7   20.07   76.5   1017.2   1.472   4.3     MAY   77   1231   5   26.5   20.27   78.1   960.3   1.455   4.3   1		MAY	11	106	Ś	27.3	21.25	P. 77.9	1016.8	G • 5 F	2.4	168
MAY   77   1101   5   27.2   20.52   76.0   960.9   1.16   3.3   1     MAY   77   1131   5   26.9   20.32   76.5   1017.1   1.29   3.8   1     MAY   77   1201   5   26.9   20.32   76.6   1017.2   1.29   3.8   1     MAY   77   1201   5   26.6   20.29   76.6   1017.2   1.37   3.1   1     MAY   77   1231   5   26.7   20.07   76.5   1017.2   1.472   4.3   1     MAY   77   1231   5   26.5   20.27   78.1   960.3   1.455   4.3   1		¥ 8 M	11	931	S	28.1	21.33	75.0	1016.9	6 - 1 3 0	1.7	168
MAY   77   1131   S   26.9   20.32   76.5   1017.1   1.29   3.8   1     MAY   77   1201   5   26.8   20.29   76.8   1017.2   1.37   3.1   1     MAY   77   1201   5   26.8   20.29   76.8   1017.2   1.37   3.1   1     MAY   77   1231   5   26.7   20.07   76.5   1017.2   1.42   4.3   1     MAY   77   1201   5   26.5   20.27   78.1   960.3   1.45   4.3   1		T A F	77	1011	Ś	27.2	20.52	76.0	960.9	1.16	3•3	127
MAY 77 1201 5 26.8 20.29 76.8 1017.2 1.37 3.1 1 MAY 77 1231 5 26.7 20.07 76.5 1017.2 1.42 4.3 1 MAY 77 1301 5 26.5 20.27 78.1 960.3 1.45 4.3 1		MAY	11	1131	S	26.9	20.32	76.5	1017.1	1.29	3.8	125
MAY 77 1231 5 26.7 20.07 76.5 1017.2 1.42 4.3 1 MAY 77 1301 5 26.5 20.27 78.1 960.3 1.45 4.3 1		YAM	11	1201	S	26.8	20.29	76.8	1017.2	1.37	3.1	124
MAY 77 1301 S 26.5 20.27 78.1 960.3 1.45 4.3 1		Y A M	17	1231	r	26.7	20.07	76.5	1017.2	1.42	4.3	122
		A A M	17	1301	S	26.5	20.27	78.1	960.3	1.45	<b>4</b> • 3	119

A STATE OF A

UAY	HINDW	YEAR	TIME	SITE	AT (deg)	PPH20 (Torr)	RH (F)	BP (MBAR)	SR (W/SQ M)	WS CH/S)	HDH CDEG
24	Y A M	77	1331	Ś	26.4	20.57	79.8	467.4	1 . 4 2		114
24	AAM	17	1401	S	26.4	20.59	79.6	1016.9			711
24	A A M	17	1431	ŝ	26.5	20.89	80.5	1016-6			 
24	MAY	11	1501	S	26.8	20.94	79.1	1016-0	1.46	5.7	
24	AA	11	1532	s	26.7	21.10	80 • 2	1015.9	1.19		2 4 F
25	7 A M	11	903	S	27.8	20.89	7.21	1015.1	0.54	2.6	212
25	A A M	77	933	S	28.9	20.12	67.4	1015.1	0.73		228
25	MAY	11	1003	S	30.0	19.97	62.8	1015.2	0.90	2.6	247
5	A A M	11	1033	s	31.5	18.57	53.7	1014.9	1.00	1.5	238
\$ 2	Y A K	27	1103	s	32.4	17.30	47.6	1015.0	1.12	1.7	219
5 i N	X A K	17	1133	S	30.5	20.07	61.2	1015.0	1.24	3.3	145
22	× × ⊨	11	1203	S	29.9	20.77	65.8	1014.8	1.33	3.9	152





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				NRL	APTO	ູ້	S 1.	E C	able Distr	6.2 -1 hu	.l tion	Me	2086	eme	nts			
			Part	1c1	e Dei	nsit		1/00	(mn/:	87 (	Pa	ırti	cle	Rad	tus (I	(m		
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8 7 6 1	17 1400	1.532 ]	3 3.975	20	2.585 2.585	55	5 • 4 6 E 5 • 4 6 E	12	3.43E 4.03E	10	1.726 3.56ë	22	1.50E	55	-01-01-01-01-01-01-01-01-01-01-01-01-01-	1.076-01	1.946-0 2.226-0	2.936-03
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-Seratod Child Social Section States Table 6.2.1 (Continued) Aerosol Size Distribution Measurements

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1 MAR		1100	5.976-04 7.165-04 4.736-04	6.57E-ù4 5.37E-u4 1.79t-04 1.79t-04	6.576-04 3.536-04 7.986-04 5.976-05	2.93E-04 1.19E-04 1.19E-04 1.79E-04	1.19E-04 4.19E-04 0.00E 00 5.97E-05	5.97E-05 5.97E-05 5.97E-03 0.00E 03	0.00E 00 0.00E 00 0.00E 00 0.00E 00	1.796-04 5.976-05 0.006 00 0.006 00	1.196-04 0.006 00 0.006 00 0.006 00	0.00E 00 0.00E 00 0.00E 00 0.00E 00	0.006 00 0.006 00 0.006 00
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2 2 1 1 1	> >	11200 11200 11200 11200 11200 12200 12200 12200 12200 12200 12200	7. 316-92 9.886-02 9.746-02 1.996-01 1.096-01 1.076-01 1.120-01 1.396-61	3.866-02 4.406-02 2.776-02 5.716-02 5.796-02 5.796-02 5.816-02 5.816-02 6.975-62	1.756-02 1.896-02 1.266-02 2.256-02 2.3356-02 2.3359-02 2.176-02 2.716-02 2.716-02 3.156-02	5.472-03 8.352-03 4.896-03 9.916-03 9.666-03 9.375-03 1.026-03 1.236-02	3.3466-03 2.4466-03 1.6676-03 3.4466-03 3.4466-03 3.6466-03 3.6466-03 3.6466-03 3.646-03 3.646-03 3.646-03 3.646-03 3.646-03	1.676-03 1.256-93 1.076-03 1.376-03 2.266-93 2.666-93 2.665-03 2.665-03 2.665-03 2.665-03	1.196-04 8.956-04 4.786-04 5.376-04 9.556-04 1.326-03 1.256-03 1.076-03	2.39E-04 4.78E-04 2.98E-04 2.98E-04 2.98E-04 5.97E-04 5.97E-04 7.16E-04 7.16E-04	2,986-04 1.196-04 1.796-04 1.196-04 4.186-04 4.186-04 5.576-04 5.976-04	L. 796-04 L. 196-04 L. 196-04 O. 006 00 2. 986-04 2. 986-04 5. 976-05 1. 796-04 5. 976-05	0.006 A° 5.976-U° 5.976-U° 5.976-05 1.196-04 1.196-04 1.196-04 2.976-05 5.976-04
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9 MAR	1	1030	1.41E-21 7.192-22 8.505-02	7.585-02 4.235-02 5.295-02	3.87E-02 1.95E-02 2.71E-62	1.416-92 9.736-03 1.406-02	6.86E-03 5.32E-03 5.37E-03	4.006-0] 2.266-03 2.866-03	2.33E-03 2.26E-03 2.39E-03	1.37E-03 1.25E-03 1.37E-03	8.36E-04 2.39E-04 5.97E-04	2.396-04 2.986-04 7.766-04	1.19E-04 1.79E-04 1.79E-04

Table 6.2.1 (Continued) NRL Aerorol Size Distribution Measurements

	4.07	1.526-01 1.556-01 1.586-01 2.166-01 2.566-01	2.43E-01 2.655E-01 1.31E-01 2.32E-01 1.55E-01 1.55E-01 2.32E-01 2.32E-01	8.176-01 9.046-01 5.406-01 3.246-01	$\begin{array}{c} 2 & 5 & 5 \\ 1 & 1 & 5 & 5 \\ 1 & 1 & 5 & 5 \\ 1 & 1 & 5 & 5 \\ 1 & 1 & 5 & 5 \\ 1 & 1 & 5 & 5 \\ 1 & 1 & 5 & 5 \\ 1 & 1 & 1 & 5 & 5 \\ 1 & 1 & 1 & 5 & 5 \\ 1 & 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1$	2.446-03 2.446-0300-03 2.446-03 2.446-03 2.446-03 2.446-03 2.446-0
	3.12	5.766-01 5.526-01 5.657-01 7.516-01 8.766-01	8.226-01 8.526-01 7.916-01 7.916-01 5.636-01 8.356-01 8.356-01 8.366-01	3.026 00 3.466 00 1.946 30 1.166 00	7.32E-01 5.42E-01 5.42E-01 4.94E-01 4.54E-01 4.54E-01 5.54E-01 3.45E-01 3.4	1.796-02 2.226-02 2.226-02 2.726-02 1.486-02 2.176-02 2.176-02 2.176-02 2.166-02 1.456-02 1.456-02 2.116-02 1.456-02 1.456-02 1.456-02 2.116-02 1.456-02 1.456-02 2.110-02 1.456-02 1.456-02 2.110-02 1.456-02 1.456-02 2.110-02 1.456-02 2.456-02 1.456-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.466-02 2.460-02 2.400-02 2.460-0200-02 2.460-02 2.460-02 2.460-02 2.460-02 2.460-0
(Ei	2.17	1.796 00 1.586 00 1.6586 00 1.9566 00 1.956 00 2.006 00	2.224 00 2.385 00 1.466 00 2.166 00 2.166 00 2.166 00 2.516 00 2.516 00 2.516 00 2.516 00	6.93E 00 8.54E 00 5.33E 00 3.34E 00	1	2.836.01 3.496.01 3.496.01 3.496.01 3.496.01 3.496.01 3.496.01 3.496.01 3.496.01 3.966.01 3.966.01 3.966.01 3.966.01
dius (,	1.22	5.19E 00 4.52E 00 4.11E 00 5.22E 00 5.20E 00	1.086 01 9.746 00 6.266 00 9.256 00 9.256 00 8.046 00 9.426 00 1.296 01 1.296 01	2.296 01 3.216 01 1.976 01 1.356 01	5-296 5-296 5-296 5-296 5-296 5-296 5-206	1.86F 00 2.95F 00 2.95F 00 2.95F 00 2.95F 00 2.95F 00 2.95F 00 2.51F 00 2.51F 00 2.51F 00 2.51F 00
icle Ra	66.0	9.255 01 8.825 01 8.975 01 8.976 01 8.696 01 1.106 02	4.42E 02 4.15E 02 3.32E 02 4.15E 02 3.35E 02 3.35E 02 4.37E 02 4.37E 02	2.186 02 3.906 92 2.655 02 1.915 02	4.055 01 4.056 01 4.056 01 4.076 01 5.286 01 5.296 0100000000000000000000000000000000000	1.776 01 3.776 01 1.776 01 1.476 01 3.056 01 3.056 01 1.776 01 1.7
s. Part	0.23	9. 396 C1 1. 236 C2 7. 346 91 1. 546 91 1. 546 02	7.406 92 5.066 92 5.066 92 4.076 92 4.176 92 4.146 92 4.146 92 4.146 92 4.146 92	3.516 02 4.546 92 2.555 02 2.335 02	4.066 01 4.096 01 4.096 01 4.096 01 7.996 01 7.996 01 7.996 01 4.697 01 4.697 01 4.697 01 1.466	1.165 01 1.266 01 1.2676 01 2.276 01 2.276 01 1.276 01 1.276 01 1.276 01 2.276 01 2.276 01 2.276 01 2.276 01 2.276 01
c/nm) v	0.26	2.296 02 2.546 02 2.296 02 3.776 02 3.536 02	1.216 03 1.116 03 8.466 02 1.076 7] 8.596 02 9.596 02 9.466 02 1.236 03 1.236 03 1.236 03	5.17E 02 5.40E 02 4.69E 02 3.94E 02	6.975 01 7.095 02 1.095 02 1.095 02 1.095 02 1.095 02 1.045 02 1.046 02 0.006 01 1.015 02 1.016 02 1.016 02 1.016 02 1.016 02 1.016 02 1.016 02 1.016 02 1.016 02 1.016 02 2.356 02 2.556 02 2.5	2.446 01 2.456 01 2.456 01 2.456 01 2.456 01 2.456 01 2.456 01 2.456 01 2.456 01 3.416 010000000000000000000000000000000000
ty (1/c	9.22	4.20E 32 4.49E 62 4.11E 02 5.89E 02 5.89E 32	2.456 03 1.626 03 1.516 03 1.5	P.17E 02 1.35E 03 7.86E 02 7.51ë 32	2.535 02 2.555 02 2.555 02 1.556 02 1.566 02 1.566 02 1.556 02 2.556 02 2.5	2.5245 01 2.5256 01 2.5266 01 2.5566 01 2.5566 01 2.52166 01 2.5216 01000000
e Densi	6.19	1.416 03 4.706 43 1.446 53 1.446 93 1.866 93 2.236 93	5.37c J 4.49c J 3.94c J 3.94c J 4.63c J 4.63c J 3.97c J 3.97c J 3.97c J 3.97c J 3.97c J	2.345 93 4.311 03 4.375 03 1.905 03	6.916 02 6.916 02 6.916 02 6.926	1. 12 32 14.195 32 5.995 31 5.995 31 5.995 31 5.995 31 5.555 31 7.9916 31 7.9916 31 7.9916 31 7.115 31 7.115 31
Partic1(	9.15	1.646 93 1.728 95 1.566 63 2.2828 03 2.168 03	5.20E 03 4.26E 03 3.69E 03 4.37E 03 4.37E 03 4.37E 03 4.11E 03 4.11E 03 3.71E 03 3.71E 03	2.415 03 5.695 v3 2.655 03 2.055 03	6.346 02 55.496 02 55.496 02 55.696 02 55.696 02 55.696 02 10.096 02 10.166	1.046 02 1.196 02 8.906 02 9.296 01 9.296 01 9.466 01 7.5466 01 7.5466 01 7.5466 01 7.5466 01 5.466 01 5.466 01 5.466 01
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NRL Aerosol Size Distribution Measurements Particle Density (1/cc/µm) vs. Particle Radius (µm)

57 14.52 )E-04 2.98E-04	9E-04 2.39E-04 BE-04 5.97E-05 9E-04 0.00E 00 9E-04 1.19E-04	85-04 4.185-04 66-04 5.975-04 86-04 1.796-04 85-04 7.166-04 11.166-04 11.166-04 15-03 7.166-04 15-03 9.555-04	8E-03 4.23E-03 8E-03 4.23E-03 8E-03 4.23E-03 1E-03 2.33E-03 7E-03 1.25E-03	E-04 2.98E-04 E-04 1.79E-04 EE-04 1.79E-04 EE-04 1.79E-04 EE-04 1.79E-04 EE-04 1.19E-04 EE-04 2.98E-04 EE-04 2.98E-04 EE-04 1.19E-04 EE-04 1.19E-04 EE-04 EE-04 1.19E-04 EE-04 1.19E-04 EE	35     0
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Table 6.2.1 (Continued) NRL Aerosol Size Distribution Measurements

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