

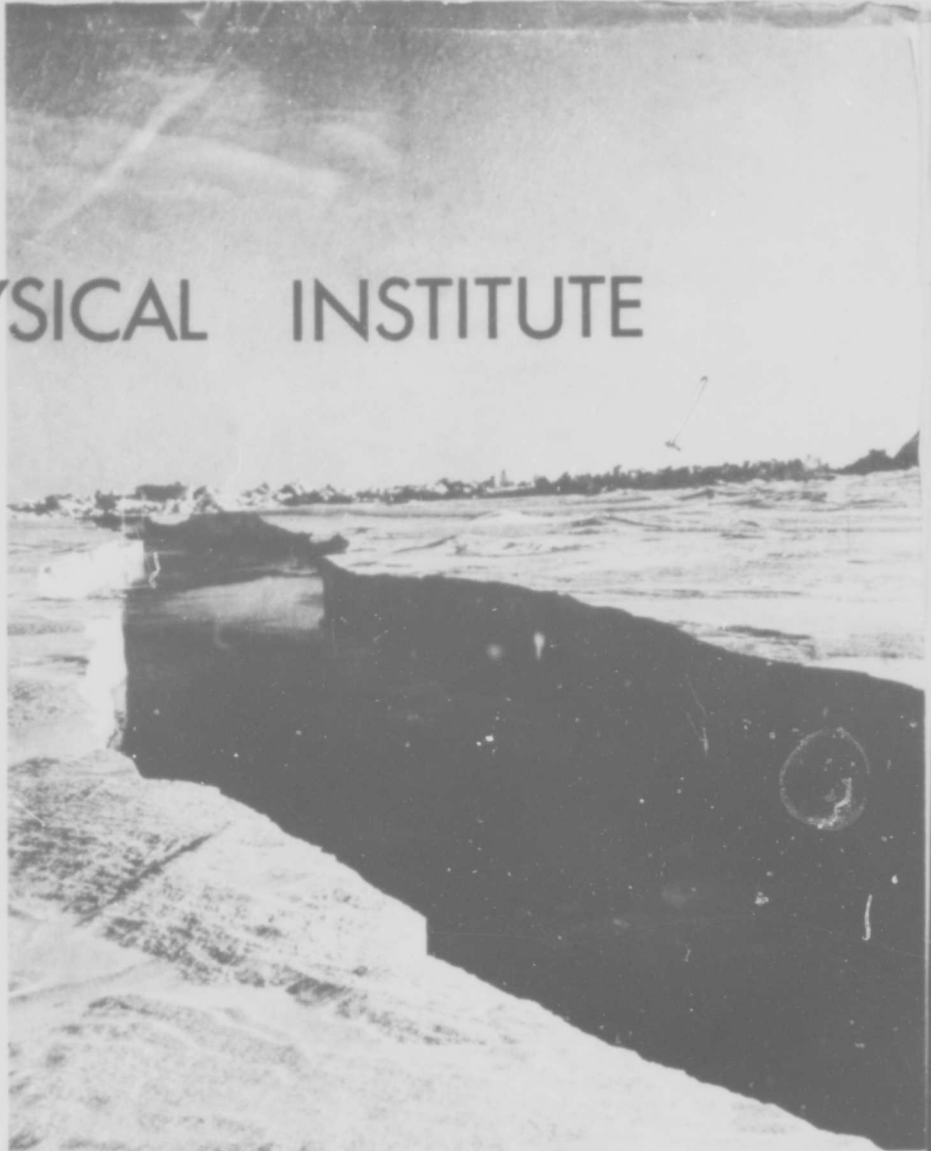
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SEA ICE STRENGTH

by

H. R. PEYTON

December 1966

FINAL REPORT

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UNIVERSITY OF ALASKA

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Principal Investigator:

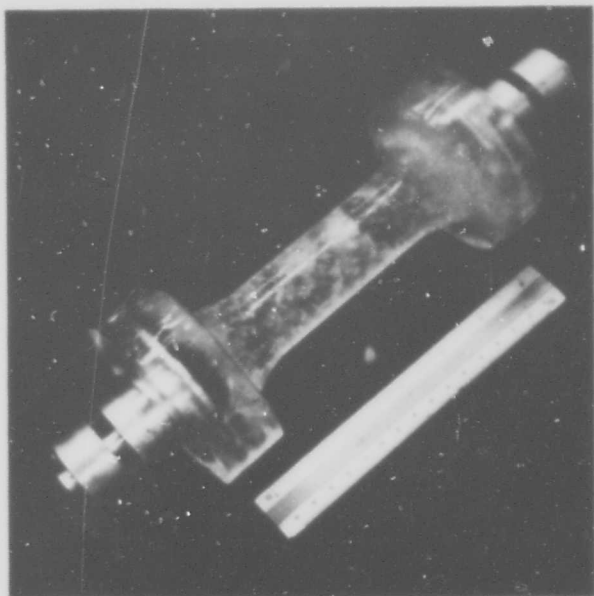
H. R. Peyton

Approved by:

K. B. Mather :

K. B. Mather
Director

SEA ICE STRENGTH



This tension test specimen is one of the types used in this research for the determination of the mechanical properties of sea ice.



Application of research findings was made in the design of this offshore oil drilling platform in Cook Inlet, Alaska. It has provisions for 32 wells with 8 through each 14.5 foot diameter leg. Eleven such platforms are in various stages of completion.

Abstract

This report contains the results from a study of the mechanical and structural properties of sea ice; the study commenced in 1958 and was completed in late 1965. Most of the experimental work is based upon stress-strain tests in both direct compression and direct tension. Approximately 3800 of these tests were made.

Those parameters anticipated to have significant effect upon strength were measured: temperature, salinity, rate of loading, crystal size, crystallographic orientation, history of the ice and depth in the ice sheet. All of these are found to be significant except that the history factor itself tended to be determined by the other parameters.

The analysis was accomplished primarily by the testing of models by linear multiple regression. The models selected yield good results with multiple correlation coefficients between 0.70 and 0.98 over a range of petrofabric types.

Sea ice is shown to be complex and its description requires five classifications of petrofabric types, each of which exhibit somewhat different characteristics. The load rate proved to be a highly significant parameter in both strength and stiffness in most cases. Ice failing in tension is somewhat less sensitive to load rate than is ice in compression.

The interrelated effects of salinity and temperature were studied using the brine volume concept. This study yielded positive confirmation of the brine volume concept, evidence of solid salt reinforcement, and evidence of failure plane selectivity to bypass strongly reinforced planes. These aspects pertain to both tension and compression failure modes.

Depth in the ice sheet is shown to be a strength factor when related to each of three parameters; rate of loading, brine volume and solid salt reinforcement.

Additional work accomplished in conjunction with construction of large offshore oil drilling platforms had provided significant information concerning oscillatory failure of sea ice in compression and strength reduction at very high load rates. The ice failure force oscillation is an ice property and is not primarily a function of the response of the structure. The amplitude of oscillation is large and at a frequency in the range of most space frame structures. The failing ice may cause forced resonant vibration in structures, and the forces are large enough to resonantly vibrate structure weighing several thousand tons.

Preface

The work accomplished under the Office of Naval Research Arctic Project is covered in Chapters 1-9. Chapter 10 is included as additional work which grew directly from that supported by ONR. This additional work is a practical application of sea ice mechanics to the design and construction of offshore drilling platforms in Cook Inlet, Alaska. At the present time there are eleven such platforms in various stages of design, construction, or operation. A representative structure costs 10 million dollars exclusive of well drilling expenses, contains 2500 tons of steel, and provides conduits for drilling 32 wells.

Acknowledgements

Several individuals have been of considerable assistance in the execution of the work. Mr. Stephen Nathanson spent four years at Barrow, Alaska during the field portion of the work, and his work was instrumental in the development of test procedures and their execution. Mr. Chia Yao Yuan performed many exacting tests at Barrow, and his meticulous attention to detail, even in difficult situations, is reflected in the high quality data acquired. Mr. Phillip Johnson was active on the analysis of data and presentation of results during that portion of the project. His diligence, study and ideas are greatly appreciated. Mr. Frank Komin accomplished much of the detailed work in Cook Inlet. The quality and detail of this portion is in great part due to his efforts. Support and encouragement by the U.S. Army Cold Region Research and Engineering Laboratory and the help of Dr. Andrew Assur is greatly appreciated as is that of the Navy Civil Engineering Laboratory and Mr. Earl Moser.

The work was supported by the Geography Branch of the Office of Naval Research and was further supported by the Office of Naval Research through the Arctic Research Laboratory. The support of Dr. Max Brewer, Director, Arctic Research Laboratory is gratefully acknowledged. Partial support was furnished by the State of Alaska. That portion of the work accomplished in Cook Inlet was supported by Shell Oil Company as operator for itself, Standard Oil Company of California and Atlantic-Richfield Oil Company. The support of these companies and the subsequent release of a portion of the results is greatly appreciated.

Without the active support and participation of my wife, Patricia, and children, Linda and Paul, the work would not have been possible. Particular gratitude is expressed for those years in which they lived and worked at Barrow.

TABLE OF CONTENTS

	Page
ABSTRACT	4
PREFACE	5
ACKNOWLEDGEMENTS	6
LIST OF TABLES	12
LIST OF FIGURES	14
LIST OF EXHIBITS	17
I. INTRODUCTION	19
1.1 GENERAL PROPERTIES, A REVIEW	19
1.1.1 <u>Basic Properties of Ice</u>	19
1.1.2 <u>Physical Properties of Sea Ice</u>	20
1.1.3 <u>Mechanical Properties of Sea Ice</u>	21
1.2 RESEARCH OBJECTIVES	21
1.2.1 <u>The Need to Identify Mechanical Properties</u>	21
1.2.2 <u>Parameters which Apparently Govern Mechanical Properties</u>	21
1.3 EXPERIMENTS	22
1.3.1 <u>Experimental Design</u>	22
1.3.2 <u>Expected Experimental Results</u>	22
1.3.3 <u>Experiments Accomplished</u>	22
1.4 PREVIEW OF RESULTS	23
1.4.1 <u>Early Results</u>	23
1.4.2 <u>Load Rate Effect</u>	23
1.4.3 <u>Effect of Brine Volume</u>	23
1.4.4 <u>Solid Salt Effect</u>	24
1.4.5 <u>Failure Mechanisms</u>	24
1.4.6 <u>Additional Considerations</u>	24
1.5 CLOSURE	24
II. EXPERIMENTS	27
2.1 LOCATION	27
2.2 PETROFABRICS: CRYSTAL SIZE, SHAPE AND ORIENTATION	27
2.3 MEASUREMENTS OF PARAMETERS	27
2.3.1 <u>Temperature</u>	27
2.3.2 <u>Rate of Loading</u>	27
2.3.3 <u>Salinity</u>	27
2.3.4 <u>Ice Type Classifications</u>	28

2.3.5	<u>Crystal Orientation</u>	28
2.3.6	<u>Age and History Factors</u>	28
2.4	SAMPLING	28
2.5	MECHANICAL PROPERTIES	
2.5.1	<u>Compression Stress-Strain Tests</u>	28
2.5.2	<u>Tension Stress-Strain Tests</u>	29
2.5.3	<u>Compression and Tension Creep</u>	30
2.6	DATA REDUCTION	30
2.6.1	<u>Field Calculations</u>	30
2.6.2	<u>Refined Data Reductions</u>	30
III.	EARLY RESULTS	35
3.1	GENERAL	35
3.2	ICE FORMS	35
3.2.1	<u>Classification</u>	35
3.2.2	<u>Bottom Ice</u>	35
3.3	STRENGTH	39
3.3.1	<u>Rate of Loading</u>	39
3.3.2	<u>Temperature</u>	40
3.3.3	<u>Crystal Orientation</u>	40
3.4	GENERAL RESULTS	40
IV.	DATA ANALYSIS	43
4.1	INTRODUCTION	43
4.2	EXAMPLE OF BASIC TECHNIQUE	43
4.3	DISPERSION MEASURED IN NATURAL LOGARITHMS	44
4.4	SIMPLE INTERRELATIONSHIPS	45
V.	LOAD RATE EFFECTS	47
5.1	INTRODUCTION	47
5.2	RATE OF LOADING EFFECT, COMPRESSION	47
5.2.1	<u>Initial Analysis</u>	47
5.2.2	<u>Factors That Control the Rate Power</u>	47
5.2.3	<u>Rate Power for a Single Type-Orientation Group</u>	47
5.2.4	<u>Developing General Rate Functions</u>	48
5.2.5	<u>Testing the General Rate Functions</u>	50
5.2.6	<u>The Orientation and Type Function of Rate Power</u>	51
5.2.7	<u>Characteristics of Strate</u>	52
5.3	RATE OF LOADING EFFECT, TENSION	53

5.3.1	<u>Initial Analysis</u>	53
5.3.2	<u>Factors that Control Rate Exponent</u>	55
5.3.3	<u>Rate Exponent for a Single Type-Orientation Group</u>	56
5.3.4	<u>Developing General Rate Functions</u>	57
5.3.5	<u>Testing the General Rate Function</u>	58
5.4	RATE OF LOADING EFFECT; TENSION AND COMPRESSION COMPARISONS	59
5.5	SUMMARY	60
VI.	BRINE AND SOLID SALT EFFECTS - CENTER ICE - ONE INCH DEPTH	63
6.1	INTRODUCTION	63
6.1.1	<u>Sea Ice Formation</u>	63
6.1.2	<u>Current Knowledge of General Physical Properties</u>	64
6.2	BRINE SOLIDIFICATION	68
6.2.1	<u>Examination of the Strate of Center Ice</u>	68
6.2.2	<u>Geometric Model for Ice-Salty Ice-Brine System</u>	72
6.2.3	<u>Sea Ice Phases and Strate of Center Ice</u>	76
6.2.4	<u>Quantitative Aspects of Salt Deposits</u>	77
6.2.5	<u>Effect of Brine Channel Shape and Salt</u>	80
6.2.6	<u>Qualitative Aspects of Salt</u>	82
6.2.7	<u>A Combined Salt Function</u>	83
6.3	FAILURE TYPES	88
6.4	REEVALUATION OF PUBLISHED DATA	88
6.4.1	<u>Assur's Ring Tensile Data</u>	88
6.4.2	<u>Graystone and Langleben</u>	89
6.5	CONCLUSIONS	90
VII.	GENERAL FUNCTION FOR STRENGTH, CENTER ICE, ALL DEPTHS	93
7.1	INTRODUCTION	93
7.2	CENTER ICE DATA, COMPRESSION	93
7.3	A GENERAL STRENGTH FUNCTION FOR 1 INCH CENTER ICE	94
7.4	THE BRINE FUNCTION, LIQUID AND SOLID	95
7.4.1	<u>General</u>	95
7.4.2	<u>Slope of Brine Volume Function</u>	100
7.4.3	<u>Salt Reinforcement</u>	101
7.5	TESTING, ADJUSTING, AND EVALUATING THE COMPLETE STRENGTH FUNCTION	103
7.6	INTEGRATED COMPRESSIVE STRENGTH OF AN ICE SHEET, CENTER ICE, HORIZONTAL LOADING	105

7.7	CONCLUSIONS	108
VIII.	STRENGTH FUNCTIONS, BOTTOM ICE	111
8.1	INTRODUCTION	111
8.2	AVERAGE STRENGTH	111
8.3	ELASTICITY	112
	8.3.1 <u>General</u>	112
	8.3.2 <u>Elasticity at Various Orientations</u>	113
8.4	TENSILE STRATE FUNCTIONS OF 90-00, 90-45, AND 90-00 ORIENTATIONS	114
8.5	COMPRESSIVE STRENGTH FUNCTIONS OF 90-00, 90-45 AND 90-00 ORIENTATIONS	116
	8.5.1 <u>Strate Functions</u>	116
	8.5.2 <u>Solid Salt Reinforcement Functions</u>	117
8.6	TESTING THE STRENGTH FUNCTIONS	120
	8.6.1 <u>Plotback Check</u>	120
IX.	BRINE-BASAL PLANE	125
9.1	INTRODUCTION	125
9.2	BRINE-BASAL PLANE CHARACTERISTICS	125
	9.2.1 <u>Necessary Conditions</u>	125
	9.2.2 <u>Mechanical Properties in the Brine-Basal Plane</u>	126
	9.2.3 <u>Rate Functions in the Brine-Basal Plane</u>	130
	9.2.4 <u>Brine Volume and Salt Reinforcement in the Brine-Basal Plane</u>	130
9.3	SUMMARY AND CONCLUSIONS	131
X.	APPLICATION	135
10.1	INTRODUCTION	135
	10.1.1 <u>The Problem</u>	135
	10.1.2 <u>Status of Knowledge</u>	135
10.2	INITIAL OBSERVATIONS	136
10.3	ICE THICKNESS PREDICTIONS	136
10.4	RAFTING	136
10.5	ICE STRENGTH	138
	10.5.1 <u>Mode of Failure</u>	138
	10.5.2 <u>Ice Strength Testing, 1962-63</u>	138
	10.5.3 <u>Ice Strength Testing, 1963-64</u>	140
	10.5.4 <u>Ice Strength Testing, 1964-65</u>	140
10.6	LATERAL ICE FORCES ON PILING	140

10.6.1	<u>Field Measurements</u>	140
10.6.2	<u>Laboratory Measurements</u>	142

LIST OF TABLES

Table 3.1	Sea Ice Crystal Orientation	38
Table 5.1	Compression Data Groups	48
Table 5.2	Average Rate Power, Compression	48
Table 5.3	Values of Type and Orientation Variable, Compression	49
Table 5.4	Rate Function Statistics, Horizontal Loading, Compression	49
Table 5.5	Rate Function Statistics, Vertical Loading, Compression	50
Table 5.6	Values of Strate, Compression	52
Table 5.7	Average Rate Function, Compression	53
Table 5.8	Tension Data Eliminated	54
Table 5.9	Inventory of Useable Tests	54
Table 5.10	Tension Data Groups	55
Table 5.11	Weak Data Eliminated	56
Table 5.12	Rate Exponent for Tension Singto	57
Table 5.13	Fitting Tension Rotvar	58
Table 5.14	Study of Coefficient of Variation of Strength and Strate	58
Table 5.15	Strength and Strate Values	59
Table 5.16	Average Rate Functions	60
Table 6.1	Quantities of Precipitated Solid Salt at Various Temperatures	64
Table 6.2	Quantitative Data for 1 o/oo Sea Ice	78
Table 6.3	Relative Brine Volume of 8 o/oo Ice at Various Temperatures	80
Table 6.4	Qualitative Aspects of Sodium Sulfate Deposits	82
Table 6.5	Variables used in the General Strength Equation	87
Table 6.6	Representative Values for Sodium Sulfate Reinforcement	87
Table 7.1	Inventory of Center Compression Data	94
Table 7.2	Average Strate and $(1-v^{1/2})$	95
Table 7.3	Average Salinity at Different Depths	98
Table 7.4	Idealized Brine Volume and $(1-v^{1/2})$, 1°C	98
Table 7.5	Anchor Points and Least Squares Slopes	100
Table 7.6	Slope of Brine Volume Functions	100
Table 7.7	Average Values of Salt Depth Reinforcement and $S:\sigma_r/s$	102

Table 7.8	Average Values of q and Standard Deviation; $\sigma_q/S.D.$	102
Table 7.9	Values of K for Each Depth	103
Table 7.10	Relationship of K and Depth	103
Table 7.11	Comparative Statistical Information, $K=f(\text{depth})$	104
Table 7.12	Plotback Statistical Information, $K=10,000$	105
Table 7.13	Integrated Center Ice Sheet Strengths, lbs/ inch width	108
Table 8.1	Tensile and Compressive Strength at Standard Conditions at Different Orientations	112
Table 8.2	Values of E , Tension and Compression	113
Table 8.3	Values of E at Different Orientations	114
Table 8.4	Average Tensile Strate	114
Table 8.5	Average Compressive Strate	116
Table 8.6	Calculation of Salt Reinforcement	117
Table 8.7	Salt Reinforcement Data	118
Table 8.8	Statistical Tests of Strength Functions	120
Table 9.1	Estimated-Measured Strength for Odd Orientations	128
Table 9.2	Values of Type and Orientation Variable at Several Orientations	130
Table 9.3	Rate Functions at Standard Conditions	130
Table 9.4	Equation Data for Groups Loaded on the Brine Plane	131
Table 9.5	Orientation vs Mechanical Properties	131

LIST OF FIGURES

		Page	
Figure	2.1	Representative Stress-Strain Test, Compression	31
Figure	2.2	Tension Test Specimen with Loading Heads Attached	31
Figure	2.3	Tension Test Loading Heads	31
Figure	2.4	Complete Tension Test Set Up	31
Figure	2.5	Representative Stress-Strain Test, Tension	32
Figure	2.6	Representative Creep Test, Compression	32
Figure	2.7	Representative Creep Test, Tension	32
Figure	2.8	Stress-Strain Test Rate of Loading	32
Figure	2.9	Stress-Strain Test Modulus of Elasticity	33
Figure	3.1	Petrofabric Profiles	33
Figure	3.2	Bottom Thin Sections	33
Figure	3.3	Preferentiation of Bottom Ice C-Axis, All C-Axis Horizontal, Preferentiation in Horizontal Plane	33
Figure	3.4	Crack Effect on C-Axis Orientation Sea Ice, Eison Lagoon	41
Figure	3.5	Specimen Orientation Nomenclature	41
Figure	3.6	Rate of Loading Effect on Strength New Sea Ice, Compression, 50"-60" Depth	41
Figure	3.7	Comparative Strength and Load Rate Effects Compression	41
Figure	3.8	Comparative Strength and Load Rate Effects Tension	42
Figure	3.9	Creep Rate, Compression	42
Figure	6.1	Block Diagram of Assurs' Elliptical Model	65
Figure	6.2	Plan View of Elliptical Model	66
Figure	6.3	Indication of Solid Salt Reinforcement Center Ice One Inch Depth	70
Figure	6.4	Plan View of Sea Ice Model with Deposited Solid Salts	72
Figure	6.5	Diagram of Ice Strength and Superimposed Salt Reinforcement	74
Figure	6.6	Orientation of Compressive Forces on Sea Ice	75
Figure	6.7	Relative Brine Volume	79
Figure	6.8	Ions Lost to Salts	79
Figure	6.9	Salt Volume	79
Figure	6.10	Associated Ice Volume	79
Figure	6.11	Salt Volume	81

Figure	6.12	Sali Area	81
Figure	6.13	Amount of Solid Salt Reinforcement	81
Figure	6.14	Sali Quality Function	84
Figure	6.15	Solid Salt Volume, Ratios to Sali and Relative Solid Salt Volume	84
Figure	6.16	Salt-Water Rates in Brine	84
Figure	6.17	Sali-Brine Ratio	84
Figure	6.18	Plot of Calculated Strength versus Measured Strength	86
Figure	6.19	Pattern of Failure Types Center Ice, Compression	91
Figure	6.20	Evidence of Brine Reinforcement Ring Tensile Test After Assur	91
Figure	6.21	Sodium Sulfate Salt Reinforcement Ring Tensile Tests After Assur	91
Figure	6.22	Sodium Sulfate and Sodium Chloride Salt Reinforcement, Ring Tensile After Assur	91
Figure	7.1	Salt Effects with Depth Center Ice, Compression	97
Figure	7.2A	Strate at Depth, -1° and -2°C Center Ice	97
Figure	7.2B	Strate at Depth, -5°C Center Ice	97
Figure	7.2C	Strate at Depth, -10°C and -21°C Center Ice	97
Figure	7.3	Salt Effects With Depth, Center Ice With Solid Salts	99
Figure	7.4	Slope of Brine Volume Function Versus Depth	99
Figure	7.5	Salty Ice Quality at Various Depths	99
Figure	7.6	Values of Coefficient K at Various Depths	99
Figure	7.7	Brine Volume Function at Various Depths Liquid Brine Only	107
Figure	7.8	Idealized Solid Salt Reinforcement at Various Depths	107
Figure	7.9	Idealized Solid Salt Reinforcement at Various Temperatures	107
Figure	7.10	Idealized Function for Strate	107
Figure	7.11	Strength Profiles Center Ice	109
Figure	8.1	Sea Ice Strength at Various Orientations under Standard Conditions	115
Figure	8.2	Tensile and Compressive Strength under Standard Conditions	115
Figure	8.3	Modulus of Elasticity of Various Orientations under Standard Conditions	115
Figure	8.4	Strate, Brine Volume, and Orientation Relationship Bottom Ice, Tension	115

Figure 8.5	Strate, Brine Volume, and Orientation Relationship Bottom Ice, Compression	119
Figure 8.6	Solid Salt Reinforcement, Bottom Ice, Compression	119
Figure 8.7	Solid Salt Reinforcement Function	119
Figure 8.8	Plotback of 90-00 Tension Tests	119
Figure 8.9	Plotback of 90-45 Tension Tests	121
Figure 8.10	Plotback of 90-90 Tension Tests	121
Figure 8.11	Plotback of 90-00 Compression Tests	121
Figure 8.12	Plotback of 90-45 Compression Tests	121
Figure 8.13	Plotback of 90-90 Compression Tests	124
Figure 9.1	Force On a Specimen, Small θ	127
Figure 9.2	Force Diagram, Large θ	127
Figure 9.3	Force On a Specimen, Large θ	127
Figure 9.4	Force Diagram, Small θ	127
Figure 9.5	Brine-Basal Plane Function	129
Figure 9.6	Strength Orientation Relationship	129
Figure 9.7	Rate Function-Orientation Relationship	129
Figure 9.8	Strate Values for Bottom Ice Loaded on the Brine-Basal Plane	129
Figure 10.1	Cook Inlet	137
Figure 10.2	Wind at Middleground Shoal Platform A	137
Figure 10.3	Wind and Waves which Commonly Occur in Summer In Cook Inlet	137
Figure 10.4	Common Winter Ice Cover in Cook Inlet	137
Figure 10.5	Rafting of Thin Ice Floes	139
Figure 10.6	Ice Failure Against Platform I	139
Figure 10.7	Ice Failure Against Platform II	139
Figure 10.8	Ice Failure Against Platform III	139
Figure 10.9	Detailed Ice Failure I	141
Figure 10.10	Detailed Ice Failure II	141
Figure 10.11	Detailed Ice Failure III	141
Figure 10.12	Failure Stress-Load Rate, Field, Sample Cook Inlet Ice	141
Figure 10.13	Test Pile Installation	143
Figure 10.14	Test Pile Force Records, Oscillator Force, Case J	143
Figure 10.15	Ratcheting Failure MGS A, 29 December 1964, Gage 33-A	143

LIST OF EXHIBITS

	Page
Exhibit 1.1	References 147
Exhibit 1.2	Data Code 153
Exhibit 1.2.1	Data Summary, Compression 154
Exhibit 1.2.2	Data Summary, Tension 167
Exhibit 5.1	Ratio Constant and Rate Power 173
Exhibit 5.2	Data Groups, Compression 173
Exhibit 5.3	Rate Power at Various Depths and Temperatures, Center Ice 173
Exhibit 5.4	Evaluation of Strate Two, Compression 174
Exhibit 5.5	Rate and Orientation Variable, Compression 174
Exhibit 5.6	Strength and Strate at Various Orientations, Bottom Ice, Compression 174
Exhibit 5.7	Statistical Analysis of Strate 175
Exhibit 5.8	Tension Rate Power 175
Exhibit 5.9	Strate and Strength, Individual Data Groupings 176
Exhibit 5.10	Strate and Strength, Larger Groupings 177
Exhibit 6.1	Code for Data 178
Exhibit 6.2	Compression Data, Center Ice 180
Exhibit 7.1A	Plotback, 1 Inch Center Ice, Compression 182
Exhibit 7.1B	Plotback, 4 Inch Center Ice, Compression 182
Exhibit 7.1C	Plotback, 7 Inch Center Ice, Compression 182
Exhibit 7.1D	Plotback, 11 Inch Center Ice, Compression 182
Exhibit 7.1E	Plotback, 17 Inch Center Ice, Compression 183
Exhibit 7.1F	Plotback, 18-21 Inch Center Ice, Compression 183
Exhibit 7.1G	Plotback, 25-29 Inch Center Ice, Compression 183
Exhibit 7.1H	Plotback, 32-36 Inch Center Ice, Compression 183
Exhibit 7.2	Brine Volume Strength Function 184
Exhibit 7.3	Matrix of $1-v^{1/2}$ 184
Exhibit 7.4	Salt Reinforcement Matrix 184
Exhibit 7.5	Strate Matrix 184
Exhibit 7.6	Temperature Matrix 184
Exhibit 7.7	Rate Power Matrix 184
Exhibit 7.8	Rate Function for Warm Ice 185
Exhibit 7.9	Rate Function for Medium Ice 185
Exhibit 7.10	Rate Function for Cold Ice 185

Exhibit 7.11	General Brine Volume Functions	185
Exhibit 7.12	Brine Volume Strength Functions	186
Exhibit 7.13	Salt Reinforcement	186
Exhibit 7.14	Strate	186
Exhibit 7.15	Strength of Warm Ice	187
Exhibit 7.16	Strength of Medium Ice	187
Exhibit 7.17	Strength of Cold Ice	187
Exhibit A	Time-Stress-Strain Data	A-1

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Page	Paragraph	Line	Change	To
19	1.1.1	32	allure	failure
20		9	anistropic	anisotropic
23		6	anistrotropic	anisotropic
23	1.4.3	5	particuularly	particularly
27	2.3.1	7	analysis	analysis;
28	2.5.1	7	prove	provide
35	3.2.2	1	cause	caused
39	6	3	prbability	probability
43	4.2	9	reasonabl	reasonable
43	Eq. 4.4		In	In σ
45		14	perencent	percent
45	4.4	2	independ	independent
62	last	3	varability	variability
67		3	adequte	adequate
77	4	2	deom	with
83	6.2.7	4	s	σ_s
129	Figure 9.7		Tension	Compression
129	Figure 9.7		Compression	Tension
142	3	1	structurla	structural
146	1	3	varying	varying temperature
146	2	10	through	though
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	several locations		crystaline	crystalline
			crystalographic	crystallographic
			colinear	collinear

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Chapter I

INTRODUCTION

1.1 GENERAL PROPERTIES, A REVIEW

1.1.1 Basic Properties of Ice. Pure ice is a crystalline material, and its properties can be rather well described by the parameters which have been used in the description of most other crystalline materials. The general topic of this research is that of ice strength and a description of strength based on physical properties.

The most important physical property of pure ice in the context of this investigation is that of ice crystal type which occurs at pressures and temperatures within range found in nature on the earth's surface. This type is a simple hexagonal crystal and is one in which the atomic spacing and bond strength vary greatly within the crystal (1).

A useful analog model of the ice crystal is that of a stack of plastic plates between which are sandwiched layers of stiff grease. The hexagonal pattern is in the plane of the plastic sheets and represents the plane of greatest atomic bond strength. The crystal axis perpendicular to the plates is the optic or C-axis.

The stacked plate analogy is particularly useful in visualizing the effects of temperature, rate of load application and direction of load application on deformation and strength.

The temperature effect can be envisioned with the model observed at temperatures of -100°C and $+100^{\circ}\text{C}$. At the colder temperature, the plastic plates are brittle and exhibit elastic properties. The grease layers also act elastically with little evidence of viscous behavior. At the warmer temperatures, both layers exhibit strong viscous behavior with the grease layers being nearly liquid.

It is seen that temperature influences the amount and rate of deformation due to loading. The rate of load application is also seen to have a strong influence on the amount of deformation that would occur prior to fracture of the crystal. The sensitivity to rate of load application is particularly evident when the load is applied in a manner such that shear stresses force the plastic plates to slide over each other. Very slow rates of loading result in large deformations prior to failure and afford the opportunity for fracture at small total loads. On the other hand, extremely rapid loading rates result in small deformations, by the time the total stress has reached a large value, and fracture occurs. Generally, the slow loading rates result in relatively viscous deformation and low failure strengths. Rapid loading rates result in relatively elastic deformation and high failure strengths.

The model clearly indicates the strong influence of the direction of load application on deformation and failure strength. The greatest deformation and least strength obviously occurs if the plates slide

over each other; deformation along the basal plane of the crystal. Greater strength and less deformation occurs if the force is applied perpendicular to the basal plane or parallel to the basal plane.

The characteristics of single ice crystals as described here in analog form have been studied in some detail by Nakaya (2) and others (3,4). The viscous and elastic properties associated with temperature, load rate, and direction of loading have been partially evaluated by these investigators, and single ice crystals have been shown to be quite **anisotropic with respect to strength and deformation**. Additional work is required, however, for a clear understanding of basic mechanisms.

Polycrystalline ice can be formed to provide a homogeneous mass consisting of a great number of small crystals which are randomly oriented with respect to their c-axes. Such ice behaves isotropically but nevertheless exhibits strong sensitivity to temperature with respect to the relative importance of both viscous and elastic deformation. The most interesting work accomplished in this area has been performed by Jellenick and Brill (5). Their results indicate a great increase in viscous behavior with warm temperatures and a large increase in rate of deformation and total deformation with both increasing temperature and applied load. The values they obtained are not of particular importance here, but it is important to note that they found polycrystalline, pure ice to simultaneously deform viscously and elastically at those temperatures which can reasonably be expected in nature. Such a result is expected for a material near the melting point, and all naturally occurring ice is relatively near the melting point when compared with most other crystalline materials. Considerable research is now being directed toward the understanding of properties of materials at high temperatures, but most of this work tends to be of little value in the study of sea ice.

1.1.2 Physical Properties of Sea Ice. In sea ice, discrete volumes of entrapped brine are found within a matrix of pure ice. The brine is entrapped during the growth process because the growth rate of pure ice exceeds the downward convection rate of enriched brines at the growth face. Numerous investigators have studied this entrapment process and it is very well established that the brines are truly entrapped rather than being incorporated within ice crystals (6). It can be seen that the amount of entrapped brine is a function of the growth velocity. Some details of this process are described in Chapter 6.

The entrapped brines have a profound influence on the physical make-up of sea ice. The most important characteristic is the presence of liquid brine within the sea ice matrix at all temperatures and times. The ice crystal analog model can be expanded to include sea ice by incorporating large bubbles of antifreeze, or brine, in some of the grease layers. It is possible to freeze all of the brine, but with very few exceptions this does not occur in nature. The quantity of liquid brine, the chemical composition of the brine, the chemical composition of sea ice solids, and the internal geometry of sea ice crystals, each exhibit considerable variation with temperature. A complete description of these complex relationships with temperatures and salinity is given in Chapter 6.

The entrapped brines drain out of the pure ice matrix at warm temperatures. This knowledge is ancient as evidenced by the fact that Eskimos have used old sea ice to provide a supply of potable water. The amount of entrapped liquid brine is then also a function of age as well as growth velocity and temperature.

1.1.3 Mechanical Properties of Sea Ice. The addition of antifreeze along some basal planes of the ice crystal analog completes the mechanical property analog for sea ice. The strength and resistance to deformation is substantially reduced along basal planes due to the lack of strength and the low viscosity of the antifreeze.

Several investigators have studied sea ice strength by numerous experimental methods including direct compression, bending, and ring tensile tests. A great many tests have well established the effect of liquid brine on ice strength. The best single work is that of Assur and his development of a brine volume concept based upon results of ring tensile tests. Assur's work is reviewed in detail in Chapter 6.

The ring tensile test has been most extensively used, and these tests have provided the data upon which most detailed analytical work has been based (7). The test consists of machining a right circular cylinder of ice which is then loaded on its sides with the specimen splitting from end to end. The test is quite similar to tension tests performed on portland cement concrete cylinders. It will be noted that deformation measurements of such load tests would be very difficult to achieve, and no provision can be made for careful measurement of direction of load application with respect to crystal orientation. The latter provision is not necessary if the material is found to be homogeneous, but it will be shown in Chapter 3 that sea ice is not homogeneous. For this type of specimen and loading, the rate of load application is not a discrete value throughout the test specimen because the stresses vary both radially and rotationally about the cylinder axis.

The bending tests also measure tensile strength, but they do not yield good results for detailed evaluation of rate of loading, direction of local application and deformation.

Very little detailed work has been accomplished in evaluating compressive strength characteristics (8).

Deformation measurements of sea ice are very limited. Elastic deformation properties, however, have been studied by means of seismic methods which should correspond to extremely high rates of load application (9).

1.2 RESEARCH OBJECTIVES

1.2.1 The Need to Identify Mechanical Properties. The structural analyses of sea ice structures, for example floating ice sheets, require knowledge of two mechanical properties. The first is the deformation characteristics; viscosity and elastic modulus. If the ice is cold and the load rate is large, the structure can be analyzed by assuming ice

to behave elastically. If the ice is warm and the rate of loading is slow or the load is constant, the ice can be assumed to behave viscously. Intermediate cases of load rates and temperatures require visco-elastic solutions. In all cases, the stress-deformation-time relationship must be known.

The second required property is the strength. After the structural analysis is accomplished, it is possible to determine how much force can be applied to the structure provided the ice strength is known and predictable. It is noted that the force required to fail the structure is of interest from two aspects. The first is concerned with the load which can be supported by an ice structure. The second is concerned with the load an ice structure may impart to an obstacle in its path.

1.2.2 Parameters which Apparently Govern Mechanical Properties. The more obvious parameters which would be expected to govern the mechanical properties of sea ice include temperature, salinity and rate of load application. The direction of load application relative to that of crystal orientation is also important if the sea ice is not homogeneous, thus the crystallographic characteristics of the ice should be significant. The possibility should be considered that certain factors associated with the chemical composition of sea ice with partially frozen brine.

1.3 EXPERIMENTS

1.3.1 Experimental Design. Measurements of crystal size, shape, and degree of randomness in orientation are required. These measurements are quite effectively made by standard thin section techniques using a universal stage (10). Salinity determination is a well-standardized process.

The mechanical properties are best determined by stress-strain tests in direct compression or direct tension over selected ranges of load rate and temperature. The load rate must be over a large range from zero upward. The zero load rate actually prescribes a creep test at constant load. The temperature range of importance is from the melting temperature to at least -20°C and preferably to -30°C .

Stress-strain tests are desired for representative types of sea ice and for numerous directions of loading if the ice is inhomogeneous or anisotropic.

1.3.2 Expected Experimental Results. Physical property measurements coupled with the stress-strain test measurements should provide data to describe deformation and strength in terms of physical properties, rate of loading, and direction of loading. It is anticipated that these descriptions would be complex. Previous work by other investigators has shown the description of strength to be quite complicated even with fewer parameters than are considered here.

1.3.3 Experiments Accomplished. Stress-strain and creep tests in both direct tension and direct compression are developed. The details of

experiments are described in Chapter 2. Also described in that chapter are the series of experiments and measurements required to describe the physical properties of sea ice.

The experiments were all performed as outlined in the section on experimental design, however, sea ice was found to possess a broad spectrum of crystallographic types and to exhibit more anisotropic behavior than had been anticipated. As the experimental program progressed, the range of experiments accomplished had to be reduced and did not include all of the combinations desired by the experimental design. Additionally, it was found that the mechanical properties varied in some subtle fashion with depth in the ice sheet, and depth then became another parameter of the study. Equipment limitations restricted the desired ranges of loading rate and temperature.

1.4 PREVIEW OF RESULTS

1.4.1 Early Results. The amount of data collected was quite large, and detailed analysis has not been completed on all of it. Chapter 3 is a report of many results which could be determined without recourse to detailed analysis. These early results are, in large part, plots of raw data which show the very strong dependence of the more important parameters. In that chapter is shown the extremely anisotropic behavior of the deformation and strength of sea ice. Five sea ice classifications were found to be required in order to describe the great variability of sea ice types. The ranges of strength and deformation are shown to be enormous even within the somewhat restricted experimental limits which were used.

Later chapters indicate the complexity encountered in developing descriptions of strength and deformation, and this paper does not incorporate an analysis of all the data which were collected, but rather covers a detailed analysis of certain portions of the experimental results.

1.4.2 Load Rate Effect. The parameters of ice type, direction of loading, temperature, and salinity are all shown in Chapter 3 to be significant. Each of these parameters, however, were prescribed to be measured at nearly discrete values by the manner in which the experiments were accomplished. The data could then be sorted on the basis of these parameters. The remaining parameter of most importance, based on evaluation of raw data, is rate of load application. Load rates were not determined at discrete values, but varied over a continuous spectrum. This parameter was then the first to be considered in the detailed analysis. Chapter 5 contains the detailed analysis of rate of loading with respect to the other variables, and the results of Chapter 5 show widely varying significance of load rate on strength.

1.4.3 Effect of Brine Volume. The next parameter selected for study was the one interrelated with temperature and salinity which describes the amount of liquid brine, or brine volume, in the system.

Very early analysis of the brine volume effect proved to be complex, and for this reason, a small portion of the data of particularly good quality was selected for first analysis. The first analysis is

reported in Chapter 6 and is concerned with the compressive strength of one ice type at a single depth in the ice sheet. The analysis is then expanded in Chapter 7 to cover this particular ice type for compressive strengths over the entire depth within which this ice type was found to occur.

The brine volume-strength analysis for both tensile and compressive strengths as well as some analysis of deformation characteristics is further extended in Chapter 8 to cover a second ice type.

1.4.4 Solid Salt Effect. As the brine in sea ice becomes colder, a continual precipitation of solid salts occurs. Analysis of the data indicates the possibility that these deposited solid salts reinforce sea ice in certain directions of compression loading. Such reinforcement was not found in the analysis of tension tests. The analysis of the effects due to solid salts is described in conjunction with the descriptions of brine volume effects because the two effects are intimately interrelated. The first description of solid salt reinforcement is in Chapter 6 and continues through Chapter 9.

1.4.5 Failure Mechanisms. The data revealed the possibility of solid salt reinforcement only in some of the ice types and loading directions. The reason for this apparent inconsistency is pursued in Chapter 9 in which the possibility is considered of a shift in failure plane from a reinforced to a non-reinforced one. The failure plane shift concept is shown to have some merit, but not all questions are satisfactorily resolved.

1.4.6 Additional Considerations. The investigator was afforded the opportunity to do further experimental work beyond that previously described here. Some of the results of this additional work are described in Chapter 10. It is of particular significance that the range in the rate of load application used in Chapters 2 - 9, and which was afforded by the stress-strain apparatus, does not allow accurate evaluation of the load rate effect at very high load rates. Also of significance is a preliminary evaluation of a pulsating ice failure which is found to occur when an ice sheet fails in edge loaded compression.

1.5 CLOSURE

The large amount of experimental data acquired under this project has been only partially analyzed. Those complete portions of the analysis constitute a description of the strength of some types of sea ice in terms of physical properties, rate and direction of loading, and depth within the ice sheet.

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Chapter 2

EXPERIMENTS

2.1 LOCATION

All experimental work by the University of Alaska, supported by the Office of Naval Research Geography Branch, was accomplished at the Arctic Research Laboratory at Barrow, Alaska. Two eight by twelve foot portable food storage refrigeration units were enclosed in an insulated structure and modified for temperature-controlled laboratories. Within these laboratories were installed all ice testing equipment including a three-cell triaxial shear machine which provided adequate loading capabilities within budgetary limitations.

2.2 PETROFABRICS; CRYSTAL SIZE, SHAPE AND ORIENTATION

All measurements of petrofabrics were made by use of polarized light and a large universal stage patterned after the smaller Rigsby Stage (1). Thin sections were prepared from each sample to provide petrofabric profiles which correlated with strength specimens. Additionally, petrofabric profiles were obtained from several locations in the Arctic Ocean and others in the vicinity of Barrow, Alaska.

2.3 MEASUREMENTS OF PARAMETERS

2.3.1 Temperature. Temperature measurements were made with calibrated thermistors located at various locations including several in temperature controlled laboratories with one thermistor at each test cell location and within a few inches of the test specimen.

With all other parameters held constant, the test temperature was varied through the range to be expected in Nature. Distinct temperature points were used to allow easier analysis those most frequently used were -2° , -5° , -10° , and -21°C . Two effects on mechanical properties are expected to result from temperature differences. The first and probably most significant for sea ice is the brine volume or volume of liquid phase contained interstitially in the ice matrix. The second is the effect on the crystalline ice material.

2.3.2 Rate of Loading. The rate at which load is applied to ice affects the maximum strength and the apparent stiffness or apparent modulus of elasticity. With all other parameters held constant, the ice was tested in a series of discrete load rates. These rates varied from 20 psi/min to several thousand psi/min.

2.3.3 Salinity. Chlorinity was determined for each test specimen for most of the testing program. During the first tests a titration technique was used and later a conductivity apparatus was calibrated and used. The conductivity method proved to be accurate and much more rapid than the titration method. Salinity is calculated from chlorinity values, and brine volume is calculated from temperature and salinity values.

2.3.4 Ice Type Classification. The ice type classifications are described in the next chapter. Usually classification of samples was not a difficult problem because the ice proved sufficiently uniform in large enough volumes to obtain several test specimens with very similar petrofabrics.

2.3.5 Crystal Orientation. Where applicable, crystal orientation was prescribed for each test specimen. An example is one ice type with collinear preferred c-axis orientation and foliation perpendicular to the c-axis. The test specimen could then be cut from a sample in any crystallographic orientation. Four orientations were generally used:

- a. the specimen oriented vertically in the ice sheet and perpendicular to the c-axis,
- b. the specimen oriented horizontally in the ice sheet and at 0° to the c-axis,
- c. horizontal and 45° to the c-axis, and
- d. horizontal and 90° to the c-axis.

2.3.6 Age and History Factors. When possible, a given type of ice was sampled several times between its formation and summer thaw. One sample of very old polar pack ice which was obtained in the summer of 1962 had a very similar petrofabric to one found in newly formed ice and thus allowed a good examination of long term age effects.

2.4 SAMPLING

It was determined early in the testing program that small core samples had many disadvantages, therefore, most sampling consisted of sawing out large samples of approximately two cubic feet. The ice varies considerably in many properties with depth; therefore, consistently similar specimens could be obtained only from the same depth. Sampling was performed to allow the preparation of many specimens from the same depth, thus providing minimum petrofabric and salinity differences between individual specimens.

2.5 MECHANICAL PROPERTIES

Four general types of tests were run; compressive stress-strain, tensile stress-strain, compressive creep and tensile creep. These test types were selected because of the large amount of useful information which can be extracted and because of the ease with which such results can be mathematically incorporated into structural analysis calculation procedures. There were 3762 sea ice tests and 305 single crystal tests.

2.5.1 Compression Stress-Strain Tests. The field sample was slabbed to provide sizes which could be handled with a band saw. Specimen blanks approximately 2" x 2" x 3" were prepared. These blanks were turned to cylindrical shape 1.4" in diameter on a metal working lathe and trimmed to 2.6" long. The ends were then trued to parallel smooth surfaces perpendicular to the cylinder axis.

A loading apparatus was devised and constructed to prove axial loading. The specimen was placed in the apparatus, and two dial indicators were set to measure deformation while loading proceeded. The load was measured

with a proving ring and time was recorded to allow calculation of load rate. The data indicated on the moving dials were all simultaneously recorded photographically and were later transcribed from film onto computation sheets. Figure 2.1 shows the plotted stress-strain curve for a representative test.

From the stress-strain curve many mechanical properties can be determined:

- a. Modulus of elasticity or stiffness (apparent)
- b. The maximum stress attained or "maximum strength".
- c. The stress at time of rupture or "ultimate strength".
- d. The energy required for failure.

In addition to the plotting of the curve, the rate of loading and modulus of elasticity were calculated in a rather crude fashion to allow modest interpretation and analysis in the field. Continual checks were made to insure measurement accuracy of all parameters. During the time of field data acquisition, the interrelationships were plotted and followed to ascertain, in a rough fashion, the effects of the various parameters.

2.5.2 Tension Stress-Strain Tests. The problems encountered in the development of a satisfactory direct tension test for ice were formidable and required extensive work. Suitable equipment and procedures were not productively used until January 1962. Some 900 tension tests were run subsequent to that date and constituted the major effort of the final field season.

Several systems of direct tension equipment and procedure were tried, and each in turn proved to be inadequate but pointed the way to improvement. Following is a brief description of the final design. Many aspects of this design were dictated by local Barrow problems; availability of material, skilled shop personnel and tools for investigator use. Therefore, certain promising avenues could not be pursued and the final product is a compromise.

The device is essentially a pair of aluminum end fixtures between which a test section of sea ice is welded and then pulled in tension to failure. Problems encountered in welding the sea ice to aluminum with distilled water dictated an intermediate thickness of distilled water ice.

The problems of preventing bending and torsional stresses from occurring in the test section demanded three degrees of articulation of the end fixture. This in itself is not difficult to provide when precise deformation measurements are not required, but the combination of end articulation and deformation measurement provided a multitude of difficulties. Figure 2.2 shows a test specimen prior to placement in the testing machine.

The aluminum end fixture is shown in Figure 2.3. The upper view is an exploded view showing the component parts and the lower view shows the assembled fixture.

The complete test set up is shown in Figure 2.4. The test specimen as shown in Figure 2.2 is set on knife edges in the loading frame and

subsequently an extensometer with dial indicators was placed in position to measure deformation.

The deformation measurements were made from the ends of brass capped pins which can be seen in Figure 2.3. These pins were carefully greased for their entire length except for the notched end which was incorporated in the weld. Thus the pin was fixed only at the end of the sea ice specimen and transferred sea ice deformation through the test heads to a point where the deformation could be measured.

Several types of deformation measuring devices were evaluated, but the only type which produced acceptable results was the dial indicator. Reasonably precise stress-strain data required deformation measurements of 0.00001 inch. Dial indicators of 0.0001 inch were available and were sufficiently sensitive to allow interpretation of 0.00001 inch movements if extreme care was exercised. This art was developed to a high degree using photographic collimation techniques. Figure 2.5 shows a representative stress-strain curve from tension test #1943. Data acquisition and reduction was quite similar to that for compression tests.

The preparation of tension specimens proved to be difficult and time consuming initially. Considerable improvements were made in procedures such that preparation time was cut from 5 hours to 20 minutes per successful specimen.

2.5.3 Compression and Tension Creep. After the development of reliable stress-strain apparatus, additional equipment was constructed to determine creep behavior in both tension and compression. These tests did not require a testing machine because only constant load was applied to the specimen, thus two tension creep cells and five compression creep cells were operated continuously after their fabrication was completed. The time durations of many of the creep tests were several days; therefore, the number of creep tests is quite small. Figures 2.6 and 2.7 show representative creep curves for compressive and tensile creep, respectively.

2.6 DATA REDUCTION

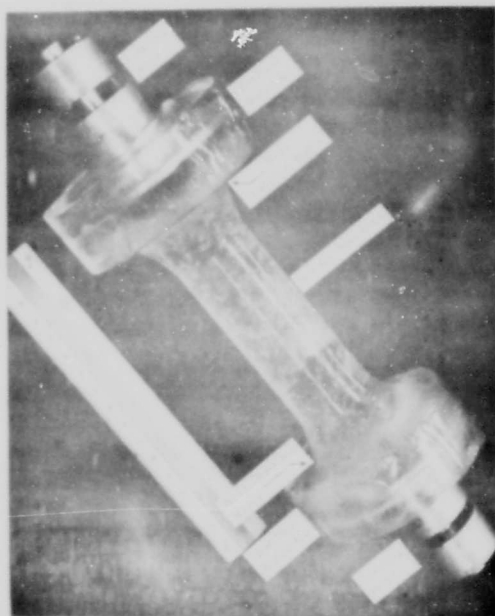
2.6.1 Field Calculations. All data acquired were reduced in the field such that stress-strain or creep curves could be plotted. Late in the project, April 1962, the University of Alaska IBM 1620 computer was used to assist in field calculations.

The field calculations were carried to a point of assuring reliable results. This required considerable summarization of data to enable observation of general relationships and patterns of behavior of the numerous parameters.

2.6.2 Refined Data Reductions. It was determined during the winter of 1962-1963, after leaving Barrow, that the field data were more sensitive to the rate of loading than had been determined by field calculations. It was further determined that the rate of loading and modulus of elasticity values could then be considerably refined by using a more complex and exacting calculation procedure than would have been reasonable in the field.

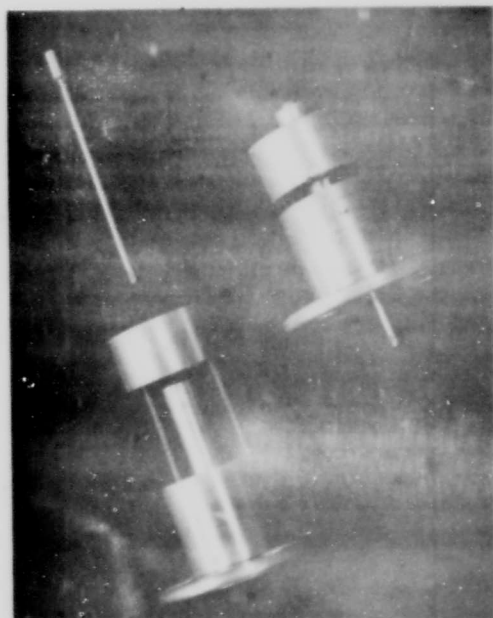


Figure 2.1



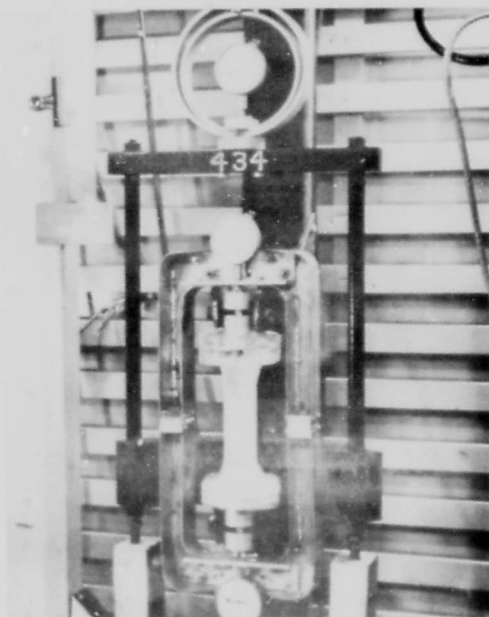
Tension Test Specimen with Loading Straws Attached.

Figure 2.2



Tension Test Loading Ready.

Figure 2.3



Complete Tension Test Set Up.

Figure 2.4

Representative Stress-Strain Test
Tension



Figure 2.5

Representative Creep Test
Compression

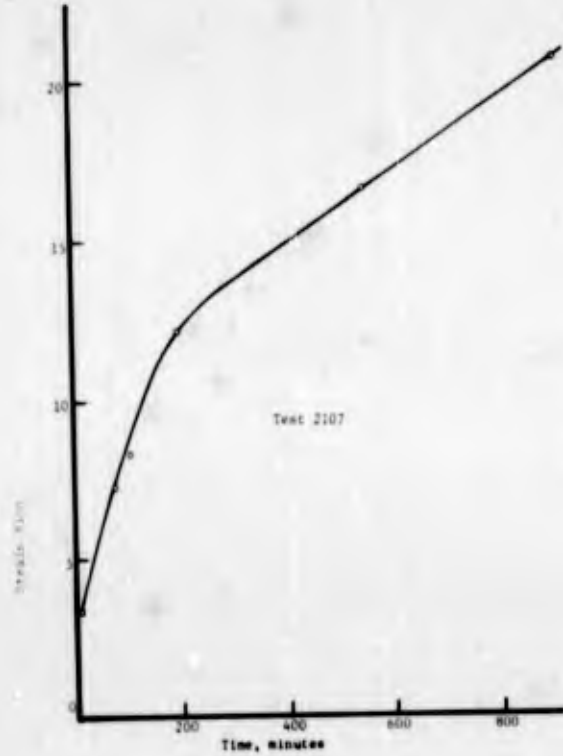


Figure 2.6

Representative Creep Test
Tension

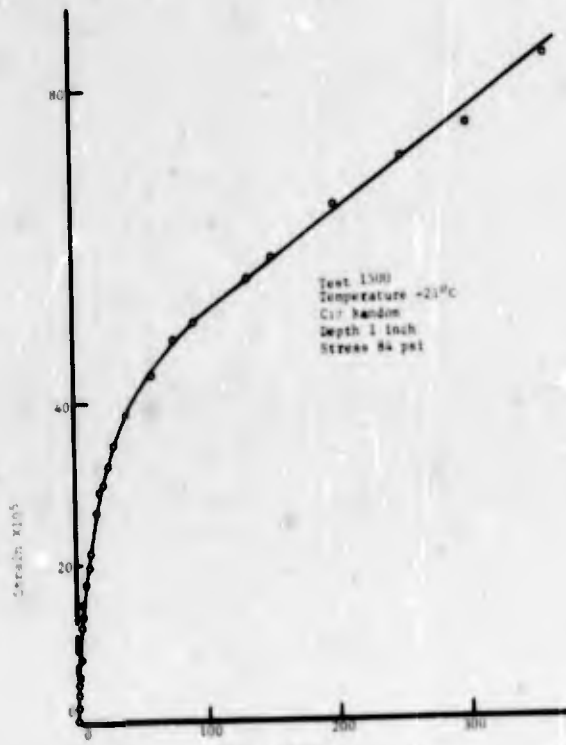


Figure 2.7

Stress-Strain Test
Rate of Loading

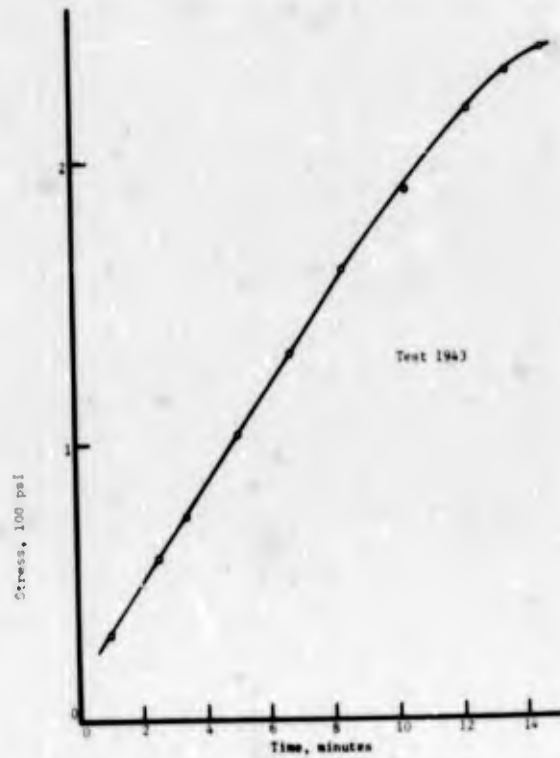


Figure 2.8

The rate of loading calculation necessitated the plotting of stress vs. time for all stress-strain tests and the fitting of a linear curve through the data. The results were much more consistent than those of the crude field calculations. An example is shown in Figure 2.8.

The modulus of elasticity or Young's modulus of ice is actually a misnomer but is used for lack of a better term. Ice is a viscoelastic material, therefore, the slope of the stress-strain curve is time dependent. Nevertheless the apparent stiffness modulus of the material at varying load rates is a most important material property and must be known for structural analysis of ice structures by elastic methods.

For field calculations an arbitrary definition of stiffness was established which allowed adequate monitoring of data as they were acquired. When detailed analysis was initiated, inconsistencies indicated that a more reliable definition of stiffness was needed. This new definition was established and new stiffness calculations were accomplished for all stress-strain tests. The first segment of all stress-strain curves were plotted to large scale as shown in Figure 2.9. The resulting value of modulus of elasticity shows substantial improvement over the field calculations with the new stiffness definition based on a secant modulus from the origin to one third the average ultimate strength of the replicate tests. The number of identical tests was usually five for compression and three for tension.

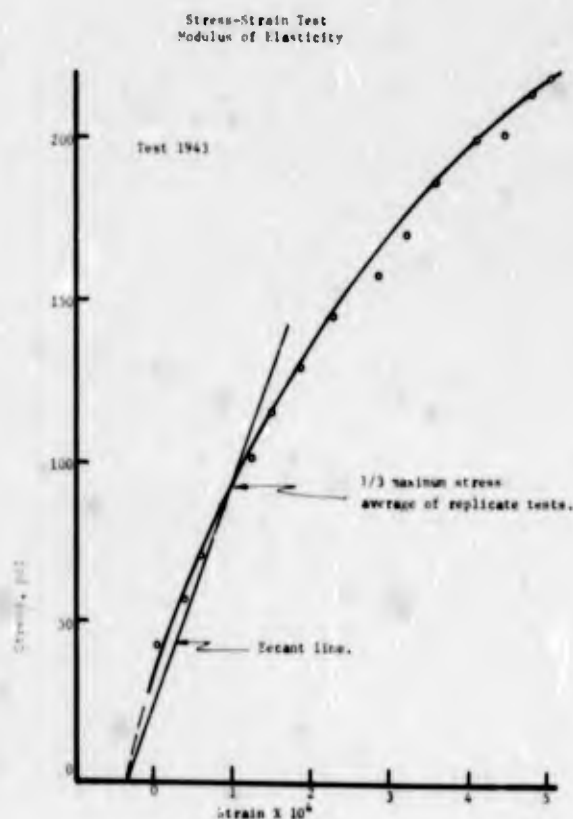


Figure 2.9

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Chapter 3

EARLY RESULTS

3.1 GENERAL

This chapter contains an outline of gross observations and general trends which are presented prior to discussion of the detailed findings.

3.2 ICE FORMS

Several structures of ice have been found, and each has been tested through portions of the spectra of other parameters.

Most of the ice tested was near-shore, first-year sea ice, obtained a few hundred yards offshore at Barrow, Alaska. One sample of summer polar ice was obtained about 200 miles north of Barrow.

The ice forms are here classified primarily on the basis of crystal structure in terms of size, shape, and orientation, and on the basis of chlorinity.

3.2.1 Classifications.

Fine-grained. This crystal type exhibits random orientation in all directions with a grain size of about 1 mm. The chlorinity tends to be the highest of the ice types with a value around $5\frac{1}{2}^{\circ}/\text{oo}$ (parts per thousand). This ice type was found extensively more than 10 inches below the surface only during one of three years' sampling and is generally found near the surface of the ice sheet. During one season it was found in an area that had been exposed to rather heavy winds during the initial formation of ice crystals on the water surface. This fine-grained slush ice had a chlorinity of 6.7 to $7.3^{\circ}/\text{oo}$.

Medium-grained. This type has a vertical c-axis with a grain size of about 1 mm by 2 mm by 4 mm long. The medium grain has been found in the top 10 inches of the ice sheet. The chlorinity tends to be around $5^{\circ}/\text{oo}$.

Center ice. This type is characterized by a horizontal c-axis having random orientation in the horizontal plane. It is generally found from the surface to a 40-inch depth. The grain size is in the order of 6 mm by 12 mm by 24 mm with the platelets stacked 6 mm thick. The chlorinity tends to be around $3^{\circ}/\text{oo}$.

Bottom ice. This structure has been found 20 inches or more below the ice surface and is characterized by a horizontal c-axis and a strongly preferred c-axis in the horizontal plane. The grains are similar in shape to the center ice but increase in size with depth to about 20 mm by 40 mm by 80 mm at a 72-inch depth. The chlorinity varies from about $2^{\circ}/\text{oo}$ to $0.1^{\circ}/\text{oo}$ as found with old polar ice from the central Arctic Ocean.

Both fine grained and center ice have been described previously (1, 2). Profiles of ice studied are shown in Figure 3.1.

3.2.2 Bottom ice. Considerable interest is caused by the mere presence of bottom ice, its extent and mechanism of formation. The initial discovery of the petrofabric was made in seasonally grown ice in the

immediate Barrow vicinity and was sampled by a SIPRE corer. The crystal size was too large to prove colinear, horizontal orientation, so the sampling procedure was changed to large block sampling cut with a chain saw.

The first indication of the extent of bottom ice formation was shown by a 10 foot square sample taken in March of 1962 from the 5 foot thick seasonal ice at Barrow. It was found that the very strongly azimuth preferential was uniform and colinear over the entire section. This indicated that the extent of bottom ice was large with respect to ice sheet thickness. If bottom ice is indeed a general feature of Arctic Ocean sea ice, problems can be expected to be encountered due to the anisotropic behavior of the ice sheet since orientation affects strength.

No detailed petrofabric data were taken of this sample, but the colinear orientation was so dramatic that specimens could be cut at any angle to the c-axis by direct visual measurement of angle based on platelet orientation seen in reflected light without magnification. Many of the tests with special load-c-axis orientations for bottom ice were on specimens from this large sample. Results shown in later chapters clearly show the anisotropic behavior due to colinear orientation.

The presence of extensive bottom ice in seasonal ice was determined during a two week field trip in April, 1963. Seven large samples of seasonal ice were obtained from broadly spaced locations in the Beaufort and Chuckchi Seas. These sample locations were between $148^{\circ}\text{W } 74^{\circ} 0'\text{N}$ and $176^{\circ}\text{W } 72^{\circ} 30'\text{N}$. All ice at depths below 36 inches was found to be "bottom ice". Four of approximately 250 thin sections are shown in Figure 3.2, showing the general "bottom ice" petrofabric. These four thin sections are parallel to the plane of the ice sheet and are from two corners of a one foot square sample section from depths of 48 and 59 inches of the same sample, #2. Virtually all crystals in these two sections have their c-axes horizontal $\pm 2^{\circ}$, i.e. in the plane of the photograph. The arrows indicate the envelope of azimuth directions of the c-axis for all crystals in the section. It can be seen in this case that all crystals are lined up within 40° over a much larger area than that of one thin section. Many individual thin sections have an envelope of azimuth orientation of less than the 25° shown. Figure 3.3 shows histograms of four samples from the following locations:

Sample No.	Location
2	Elson Lagoon, Barrow
5	$176^{\circ}\text{W } 72^{\circ}30'\text{N}$
7	$148^{\circ}\text{W } 74^{\circ}0'\text{N}$
8	$148^{\circ}\text{W } 74^{\circ}0'\text{N}$

Sample 8 was from the middle of a refrozen lead several hundred feet wide and shows the colinear orientation preferential at the surface.

These data were acquired by removing a single ice block of the full thickness of the floe by use of a long chain saw. The cross sectional shape of the sample was approximately one foot square, and one inch thick horizontal cross sectional slabs were taken at each foot of thickness from the top plus one at two inches below the surface and one at two inches from the bottom. Additionally, a full length vertical profile sample

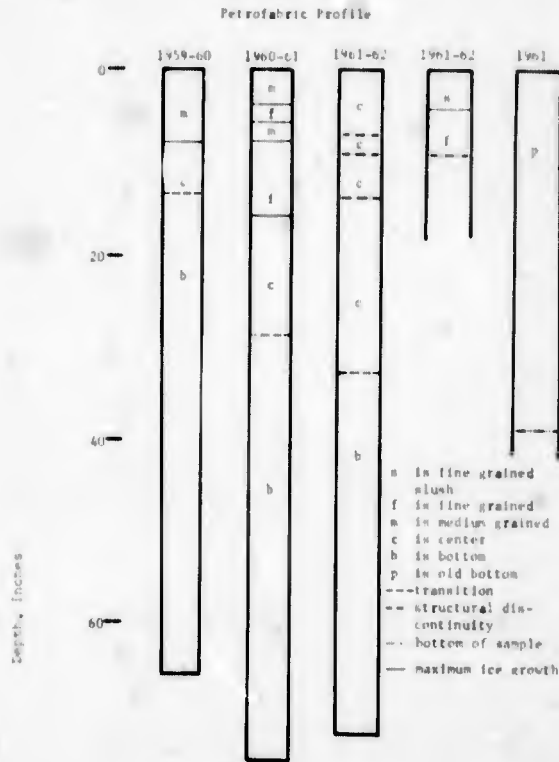
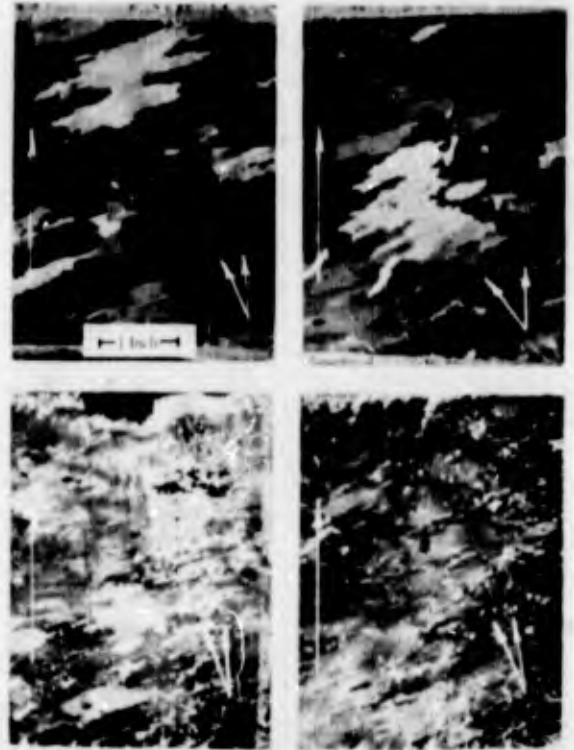


Figure 3.1



Bottom Ice Thin Sections. Upper and Lower Pictures from 48 and 59 Inch Depths Respectively.

Figure 3.2

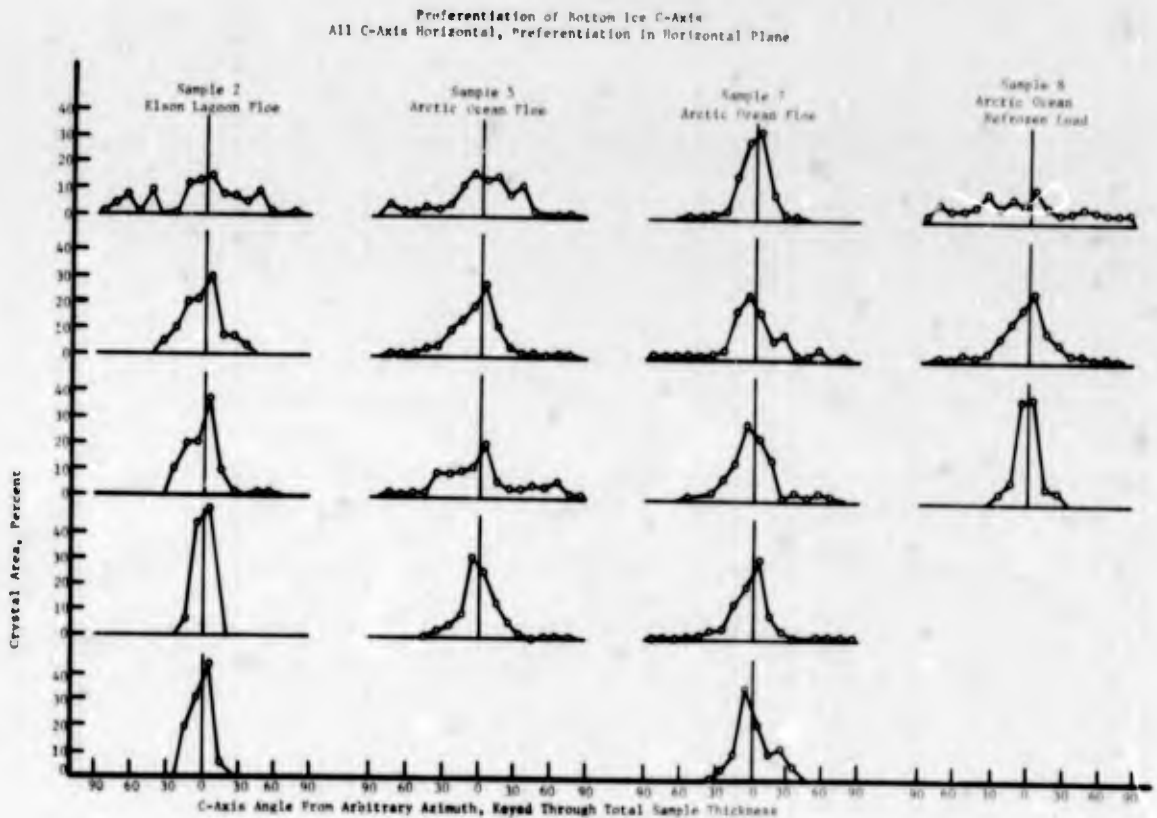


Figure 3.3

slab one inch thick was removed. The slabs were keyed for relative position from the block, covered with polyethylene, packed in insulated boxes and returned to the Barrow laboratory within a few hours.

Four thin sections each four inches square, were prepared from each horizontal slab. One thin section was cut from each corner and was keyed for position relative to the original ice block. The histograms shown in Figure 3.3 results from the four thin sections, and therefore are representative of the complete foot square sample.

Table 3.1 includes the statistical information from the four representative locations. The other samples showed similar results, but the photographic negatives were accidentally destroyed before prints could be made.

Table 3.1
Sea Ice Crystal Orientation

Sample	Depth, inches	Mean angle from arbitrary datum	Maximum spread in orientation angle;	Standard deviation of orientation angle;
2	12	+2.38°	170°	37.0°
	24	-2.18	80	16.4
	36	-1.60	90	14.1
	48	-0.70	30	6.2
	56	-1.37	40	8.6
3	12	-1.39	180	32.2
	24	-3.13	180	23.3
	36	+4.58	180	37.3
	45	+1.69	130	16.2
7	12	-2.69°	80	17.3
	24	-0.17	180	26.6
	36	-0.66	130	19.1
	48	-1.31	180	25.4
	56	+3.01	80	15.2
8	2	-4.44	180	42.7
	12	-0.92	180	23.0
	22	0.00	120	9.9

On the basis of these samples, it appears that bottom ice is indeed a general Arctic feature and anisotropic behavior of the gross ice sheet can be expected. This may shed some light on the extreme variability of the ring tensile test and various loading tests in which the petrofabric and crystal orientation are not considered to be parameters.

The "azimuth" of the colinear orientation does not change significantly with depth in the floe; therefore, the mechanism of its formation can not be dependent on a driving force which has geodetically oriented flux lines such as a magnetic field or an ocean current. The floes in the ocean are constantly in rotational motion, but the colinear orientation remains fixed relative to the ice floe, not to the earth.

One hypothesis which agrees with the evidence obtained thus far is based upon the existence of strain fields associated with polygonal cracking of the ice sheet due to thermal shrinkage. Two observations point in this direction. The first is the lack of bottom ice in upper portions of the ice sheet which grew before thermal cracking occurred. The thermally induced strain field is undefined vectorially before cracking occurs. Bottom ice is a general petrofabric feature in those portions of the ice sheet which were formed after thermal cracking and thus after the thermally induced strain field became vectorially defined.

The second observation is the large horizontal extent of the collinearity relative to the transition thickness through which the ice type changes from center ice to bottom ice, i.e. horizontal and random in that plane to horizontal and colinear in that plane. This evidence precludes simple crystal growth selectivity through such thin transition layers.

Other hypotheses include the effect of lateral heat flow due to cracks, but the large volumes and consistent occurrence of bottom ice makes this somewhat suspect. The ice is formed well below the bottom of any crack and also occurs in crack free areas.

Also to be considered is the crystal form in liquids near their freezing points. This is virtually impossible to measure at this time in the field.

Following the first hypothesis, a series of cracks was exposed in Elson Lagoon near Barrow, and samples containing a crack were removed. The median of the azimuths was then determined relative to the crack azimuth by visual inspection of the thin section on the universal stage. This is a crude technique and is subject to fairly high error, but the alternative of determining orientations of individual crystals could not be accomplished in the time available.

The results are shown in Figure 3.4. There the colinear c-axis azimuths can be seen to follow the crack azimuth very well except in areas where many cracks intersect. The statistical results show very high probability of parallel azimuths of crack and c-axis.

These data do not prove any of the hypotheses, but tend to disprove the lateral heat flow concept because 1) the thermal cracks contained split crystals, thus had been formed after the crystal and 2) the lateral heat flow to an open crack should be very nearly normal to the crack and the confusion in orientation near intersecting cracks should not be as severe as the data show.

3.3 STRENGTH

The strength to be discussed is the maximum strength achieved in unconfined compression and tension.

3.3.1 Rate of Loading. Rate of stress application has been increased from constant load. The actual rates achieved depend on the forms of ice and equipment limitations. The upper limit of loading rates tended to be 3000 pounds per square inch per minute for compression and 100

psi per minute for tension. The constant load tests involved loading by three methods. The first is by direct load of hanging weights, the second by a load amplifying knife edge lever system and the third, by maintaining a constant load by a screw jack through a proving ring. The rates of loading were obtained by the use of a motor driven variable speed transmission which in turn drove a screw jack. The load was measured by proving rings.

3.3.2 Temperature. The temperature effect has been followed through the various ice structures at temperatures which could be expected in the ice. Additional temperature ranges have been studied in some cases, but the generally used temperatures were -2° , -5° , -10° and -20°C . This provided two temperatures above and below that at which sodium sulfate begins to precipitate.

3.3.3 Crystal Orientation. The notation for direction of loading and crystal orientation for all of the data is as follows. σ is the notation for the applied stress vector, Z is the vertical direction and C is the c-axis direction. The notation $\sigma : Z$, $\sigma : C$ gives rather complete information with $\sigma : Z = 90^{\circ}$ being a specimen orientated horizontally and $\sigma : Z = 0^{\circ}$ being a vertical specimen. $\sigma : C = 0^{\circ}$ indicates the load applied parallel to the c-axis and $\sigma : C = 90^{\circ}$ is perpendicular to the c-axis. The details of notation are shown in Figure 3.5 for the specific case of bottom ice where $C : Z = 90^{\circ}$.

3.4 GENERAL RESULTS

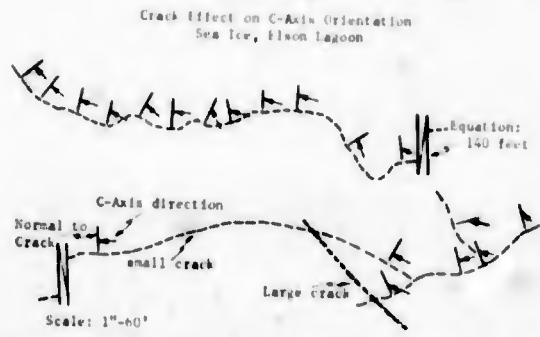
The results shown here are indicative of the general trends which will be discussed in detail in following chapters. Only a small part of the data were used for these preliminary studies but are representative of the total data in a general way.

Compressive strengths are shown in Figure 3.6 for four orientations. Both the grain size and chlorinity change with depth in the ice sheets, and the depth of this particular group of data is noted. The chlorinity at this depth was 2.1‰. The strength is significantly higher for $\sigma : Z = 0^{\circ}$, $\sigma : C = 90^{\circ}$ than for $\sigma : Z = 90^{\circ}$, $\sigma : C = 90^{\circ}$.

This relationship has been observed for all bottom ice tested. A composite picture of compressive strength relationships between ice structures is shown in Figure 3.7. These curves represent the closest representations $\sigma : C$ angle possible ($\sigma : Z = 90^{\circ}$, $\sigma : C = 90^{\circ}$ or random) for the various ice types and within similar orientations. There is shown a strong chlorinity-strength relationship with the exception of the medium grain and center ice. The curve of pure ice single-crystal strength is the upper limit of the envelope of the single crystal data.

Tension results for summer pack ice are shown in Figure 3.8. As expected, the scatter is proportionally greater than for the compression tests. The effect of variable brine volume has not yet been determined.

The creep rate shown in Figure 3.9 is the minimum slope of a strain-time curve. In general, for creep rates of less than 1 in./in./min $\times 10^{-5}$,



Sample Number	Crack Azimuth, Degrees	C-axis Azimuth, Degrees	Difference, (n) Degrees
1	75	69	6
2	62	62	0
3	39	42	-3
4	39	52	-13
5	54	62	-8
6	26	10	-4
7	49	88	-39
8	15	37	-22
9	26	38	-12
10	31	41	-10
11	76	88	-12
12	17	46	-29
13	25	26	-1
14	50	53	-3
15	0	55	-55
16	96	34	60
17	11	24	-13
18	1	34	-33
19	7	61	-54
		Ave	Std Dev
All Tests		12.9	24.1
All Tests except #7		11.5	22.0
All Tests except #7 & 14-19		10.8	9.4

Figure 3.4

Specimen Orientation Nomenclature

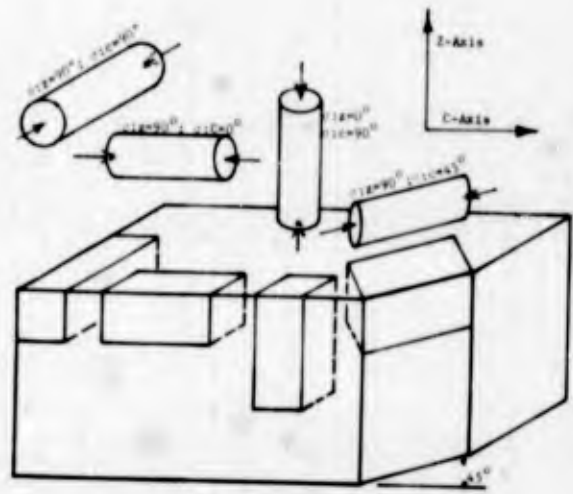


Figure 3.5

Rate of Loading Effect on Strength
New Sea Ice, Compression, 50"-10" Depth

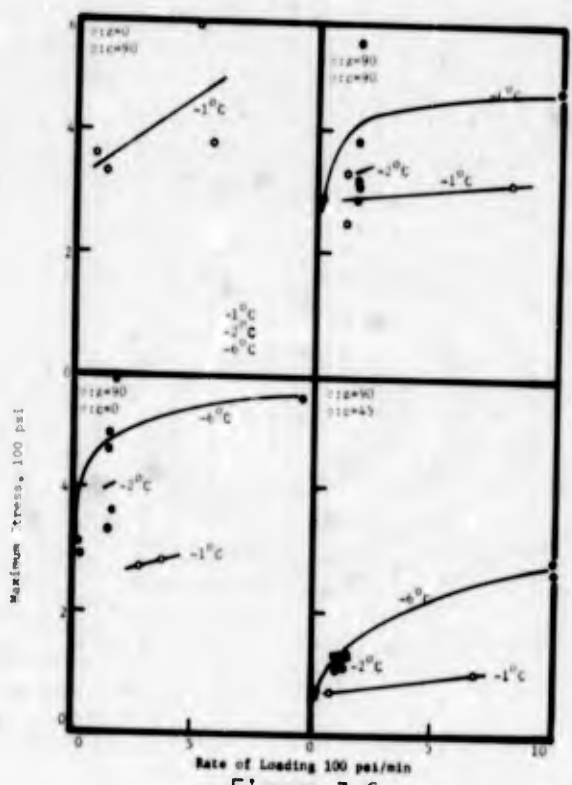


Figure 3.6

Comparative Strength and Load Rate Effects
Compression

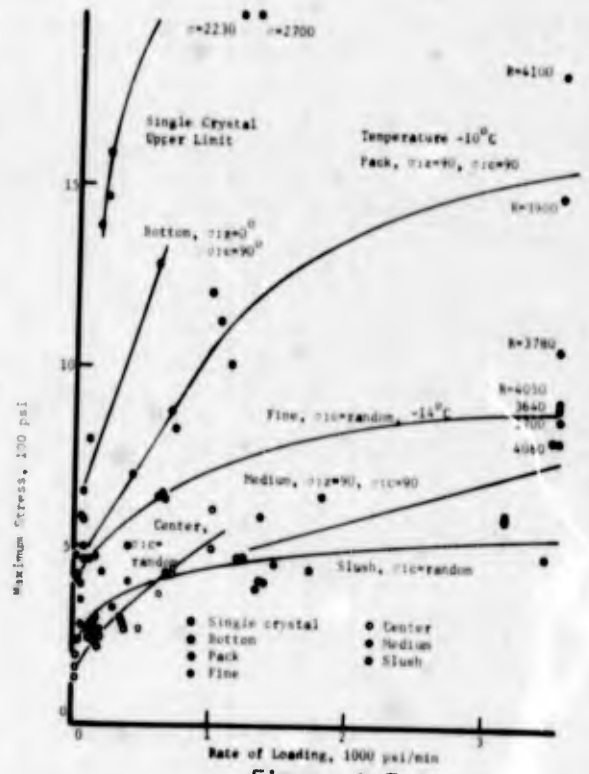


Figure 3.7

the rates do not become greater than this minimum with increasing time. For greater creep rates than $1 \text{ in./in./min} \times 10^{-5}$, the creep rates reach a minimum and then becomes increasingly greater with increasing time, ending with a disruptive failure. These particular curves are for bottom ice undergoing slow thawing and also at -6°C .

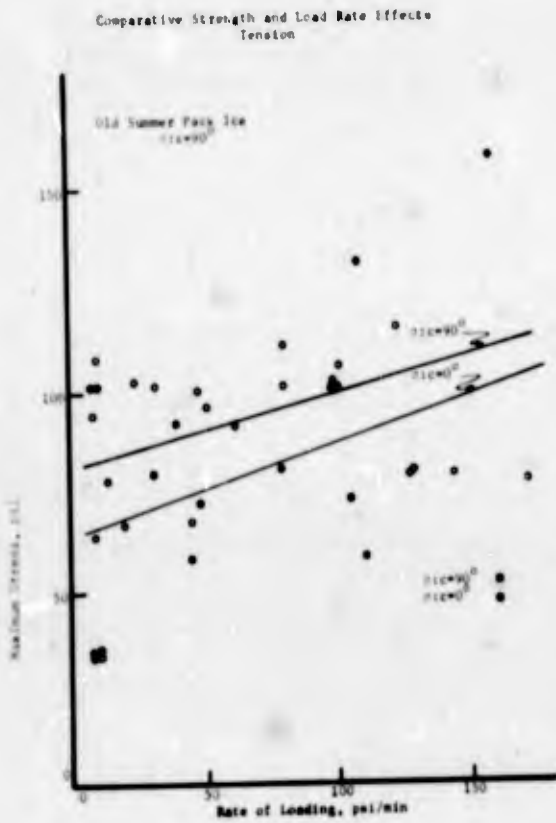


Figure 3.8

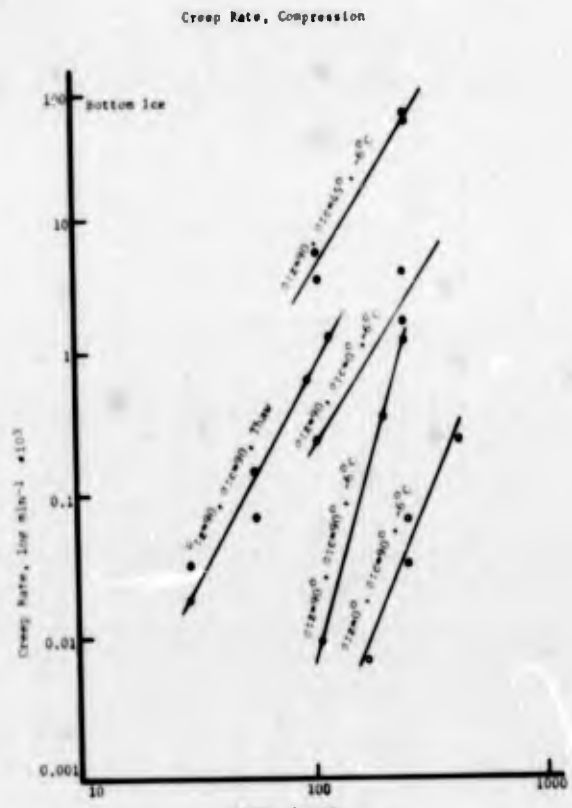


Figure 3.9

Chapter 4

DATA ANALYSIS

4.1 INTRODUCTION

The general form of the equation for the strength of sea ice was assumed to be

$$\sigma = [a][f(x_1)][f(x_2)] \dots [f(x_n)] \quad 4.1$$

where any $f(x_i)$ could be established depending upon the physical or chemical mechanism being considered. The specific independent variable x_i was assumed to affect strength according to some reasonable physical law, and a function was selected to describe the mechanism. The function was then statistically tested to check validity.

4.2 EXAMPLE OF BASIC TECHNIQUE

The compression strength depends very critically upon the rate of loading and so this was selected as the first parameter to study. Certain other variables were important, but the data could be sorted to provide groups for which those specific parameters were constant within the group: petro-fabric type, crystal orientation, age of ice, and degree of spring time disintegration. Other variables were not sortable in a systematic way because of inter-relationships among them which were probably complex in nature: temperature, salinity, brine volume, and depth in the ice sheet.

A reasonable fitting function was selected for load-rate (R), temperature (T), salinity (S), brine volume (V) and depth (D) which yielded the set of equations for n groups of data,

$$\begin{aligned} \sigma_1 &= [a_1][f_1(R)][f_1(T)][f_1(S)][f_1(V)][f_1(D)] \\ \sigma_2 &= [a_2][f_2(R)][f_2(T)][f_2(S)][f_2(V)][f_2(D)] \\ \sigma_n &= [a_n][f_n(R)][f_n(T)][f_n(S)][f_n(V)][f_n(D)] \end{aligned} \quad 4.2$$

It was reasoned that variability due to all independent parameters except load rate (R) can be reasonably well extracted by linear multiple regression techniques on equations of the form,

$$\ln \sigma = \ln a + \ln [f(R)]^r + \ln [f(T)]^t \dots \quad 4.3$$

yielding a , r , t ... and whereupon the values of the load rate function can be evaluated by

$$\ln [f(R)]^r = \ln \sigma - \ln a - \ln [f(T)]^t \dots \quad 4.4$$

The load-rate function then can be studied in detail. When one is satisfied with its evaluation, the variability of strength due to load-rate can be extracted from strength values by

$$\sigma_a = \frac{\sigma}{f(R)} = [a][f(T)][f(S)][f(V)][f(D)] \quad 4.5$$

where σ_a is now defined Strate.

Each succeeding parameter or group of inter-related parameters then can be studied in turn, and each individual parametric function can be statistically evaluated in relation to the entire equation.

4.3 DISPERSION MEASURED IN NATURAL LOGARITHMS

Many of the calculations are in units of natural logs so the log values are often more readily available than antilogs. Because of the excessive computer cost of conversion from logs to antilogs, it is desirable to have a measure of the relative variation of the actual numbers when performing a statistical analysis of the natural logs. With caution, the standard deviation of the natural logs can be used. The mathematical relationship is as follows:

\bar{x} = average of data

s = standard deviation of data

cv = coefficient of variation of data

$\overline{\ln x}$ = average of logarithms of data

S = standard deviation of logarithms of data

1. Assuming

$$(\bar{x}+s) - (\bar{x}-s) \approx e^{\overline{\ln x} + S} - e^{\overline{\ln x} - S} \quad 4.6$$

$$2s \approx e^{\overline{\ln x}} e^S - \frac{e^{\overline{\ln x}}}{e^S} \quad 4.7$$

by definition, $s = (cv)(\bar{x})$

$$(2)(cv)(\bar{x}) \approx e^{\overline{\ln x}} (e^S - \frac{1}{e^S}) \quad 4.8$$

2. If the data have reasonable dispersion,

$$\bar{x} \approx e^{\overline{\ln x}}$$

$$2cv \approx e^S - \frac{1}{e^S} \quad 4.9$$

3. Where S is less than 0.20

$$e^S \approx 1 + S \quad \text{and} \quad \frac{1}{e^S} \approx 1 - S$$

$$2cv \approx (1 + S) - (1 - S) \quad 4.10$$

$$cv \approx S$$

4.11

A later data review indicates that this relation is very good for values of S up to 0.17. Apparently assumptions 1 and 2 cause scatter and assumption 3 causes a systematic error at S values higher than .17. The standard deviation of the log values becomes larger than the coefficient of variation of the actual numbers; however, the standard deviation of the log values can be used as a guide to perhaps 0.30 or more. It is possible to calculate and remove the systematic error.

$$e^x = 1 + x + \frac{x^2}{2!} + \frac{x^3}{3!} + \frac{x^4}{4!} + \dots + \frac{x^n}{n!} \quad 4.12$$

$$e^x - e^{-x} = 2x + \frac{2x^3}{3!} + \frac{2x^5}{5!} + \dots \quad 4.13$$

If x is small, the first two terms are adequate. Equation 4.12 becomes

$$cv \approx S + \frac{S^3}{6} \quad 4.14$$

and the systematic error is $S^3/6$. The relative error is $\frac{S^3/6}{S}$

or $S^2/6$. When $S = 0.40$, the relative error is only about three percent.

4.4 SIMPLE INTERRELATIONSHIPS

Early analysis demonstrated that interrelations exist between rate of loading and other independent variables, particularly temperature. The multiple regressions for determining broad functional relationships was

$$\text{Strength} = A(\text{Depth})^d (\text{Salinity})^s (\text{Temp})^t (\text{Rate} + 50)^r \dots$$

This equation will handle most simple interrelationships on the basis of the following:

$$\begin{aligned} \text{Strength} &= A(\text{Depth})^d (\text{Temp})^t (\text{Rate})^r (\text{Temp} \times \text{Rate})^m \\ \text{Strength} &= A(\text{Depth})^d (\text{Temp})^t (\text{Rate})^r (\text{Temp})^m (\text{Rate})^m \\ \text{Strength} &= A(\text{Depth})^d (\text{Temp})^{t+m} (\text{Rate})^{r+m} \end{aligned}$$

The regression, in solving for A , d , $t+m$, etc., automatically sorts out the simple interrelationships and assigns variation in the dependent variable in the most simple manner.

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Chapter 5

LOAD RATE EFFECTS

5.1 INTRODUCTION

The data were grouped according to tension, compression, petrofabric, crystal orientation, degree of spring-time disintegration and experimental precision. These groups were then analyzed as outlined in Chapter 4 with respect to rate of loading.

5.2 RATE OF LOADING EFFECT, COMPRESSION

5.2.1 Initial Analysis. The best fitting rate function was determined to be of the form $(\text{Rate} + \text{Constant})^r$, and the constant was found to vary between 25 and 100 psi/min by solving the regression equation

$$\text{Strength} = A(\text{Depth})^d (\text{Salinity})^s (\text{Temp})^t (\text{Rate} + \text{Const})^r \quad 5.1$$

The rate exponents, r , generally ranged from .15 to .50 and tended to group for ice of the same type and orientation. The fit using this equation tended to be satisfactory for most of the data with multiple regression coefficients up to and beyond .90.

It was then found that the rate constant, Const ; and rate exponent, r , were related within petrofabrics and orientation families, but were otherwise variable. See Exhibit 5.1.

Exhibit 5.1 of this report shows, in addition to the r - Const curves, the curves of the multiple regression coefficient, R , versus Const . The rate exponent curves show a fine family relationship but the curves for the multiple regression coefficient fail to show a definite pattern. The best-fitting Const was studied thoroughly, and were found to vary from less than -20 to greater than 100 in a generally random way with an average value being perhaps 10 or 20.

Because Const is rather random, and because the average Const is relatively small, a Const of zero will be used for the time being. Any further study of it is deferred until creep information is considered.

5.2.2 Factors Controlling the Rate Exponent. The combination of ice type-crystal orientation define both the ice used and how it is loaded in strength testing. Basic sorting of the data is, first by crystal type, and secondly, by orientation with each group consisting of a single type and orientation. Since there are frequent references in the balance of this paper to ice of a single type and orientation, this will be abbreviated to singto. Analysis demonstrated that different singto not only had different strengths but they had different rate functions. Study of the center ice demonstrated that rate exponent, r , varied with depth and temperature.

5.2.3 Rate Exponent for a Single Type-Orientation Group(Singto). Once it had been determined that temperature and depth controls r , the ice in each compression singto was sorted into groups with essentially single depths

and temperatures. The effect of ice age was ignored but pack ice was kept separate from other ice. The total number of groups, total number of samples represented, the groups used, and samples used for each singto are shown as follows:

Table 5.1

Compression Data Groups

ICE	TOTAL GROUPS	TOTAL SAMPLES	GROUPS USED	SAMPLES USED
<u>Horizontal</u>				
Fine	4	68	4	68
Med 90-90	6	196	5	174
Center	18	611	14	566
Bot 90-00	9	274	8	265
Bot 90-45	8	234	7	221
Bot 90-90	7	232	7	232
Total Horizontal	53	1615	45	1526
<u>Vertical</u>				
Med 00-90	2	32	2	32
Bot 00-90	10	274	8	242
Total Vertical	12	306	10	274

About 93% of the data were used.

Exhibit 5.2 is a listing of the data developed. It shows the identification of each singto, number of samples, average $\ln(\text{depth})$, average $\ln(\text{temp})$, average $\ln(\text{salinity})$, and the fitted rate exponent, r , from a regression of the data. Ignore for the moment the column $\ln(\text{rotvar} \times e)$. The starred data were eliminated because of an atypical rate exponent. Comments on Exhibit 5.2 show the apparent reasons for this atypical behavior. Exhibit 5.3 shows a center ice rate exponent plotted against $\ln(\text{depth})$ and $\ln(\text{temperature})$.

5.2.4 Developing General Rate Functions. The average rate exponent for the different singto were approximately as shown in Table 5.2.

Table 5.2
Average Rate Exp., Compression

	ICE	AVERAGE RATE EXPONENT
Horizontal	Fine	.14
	Med 90-90	.20
	Center	.22
	Bot 90-00	.20
	Bot 90-45	.40
	Bot 90-90	.25
Vertical	Med 00-00	.20
	Bot 00-90	.17

The fine, medium, and center ice all falls within the same general depth range and the bottom ice is also within a general depth range. It is obvious that the rate exponent is a function

of type and orientation as well as depth and temperature. A new variable, Rotvar, for Rate Orientation and Type Variable, was introduced and a rate exponent equation was assumed.

$$r = A(\text{Depth})^m (\text{Temp})^n (\text{Rotvar}) \quad 5.2$$

The center ice was selected as the primary ice from which to work and it was assigned a Rotvar value of 1.00. Each other horizontal singto was compared to the center ice by fitting values of Rotvar. The values are shown in Table 5.3

Table 5.3

Values of Type and Orientation Variable, Compression

ICE	ROTVAR
Fine	.55
Med 90-90	.79
Center	1.00
Bot 90-00	.60
Bot 90-45	1.26
Bot 90-90	.79

When the horizontal data groups were analysed by weighted regression, 45 data groups and 1526 samples yielded the following equation:

$$r_h = .166(\text{Depth})^{.138} (\text{Temp})^{.09} (\text{Rotvar}) \quad 5.3$$

where the subscript h represents horizontal specimens, depth is in inches and temperature in °C, r being used in the equation,

$$\text{Strength} = A(\text{Depth})^d (\text{Salinity})^s (\text{Temp})^t (\text{Rate})^r$$

This completes the development for the general rate function for horizontal ice which has the statistical description given in Table 5.4.

Table 5.4

Rate Function Statistics, Horizontal Loading, Compression
(Performed on Logarithms of Variables)

Constant Term		-2.79503		
R Squared		.84123		
R (Multiple correlation coefficient)		.91719		
Standard Error		.121		
Ind Var	Regr Coef	Std Error	Part Cor Coef	†
Depth	.13766	.00239	.62202	57.584
Temp	.09016	.00361	.26480	24.947
Rotvar	.97850	.01240	.82352	78.869

The same procedure was used with the vertical ice. However, there were only two slings, one of which was a very weak group. It was found that the Rotvar function was not important for the data available and the general rate function for 10 data groups and 274 samples is

$$r_v = .316(\text{Depth})^{-.123} (\text{Temp})^{-.096} \quad 5.4$$

where v indicates vertical specimens, depth is in inches and temperature in °C.

The statistical information is given in Table 5.5

Table 5.5

Rate Function Statistics, Vertical Loading, Compression
(Performed on Logarithm of Variables)

Constant Term		-1.15012		
R Squared		.40271		
R		.63459		
Standard Error		.108		
Ind Var	Regr Coef	Std Error	Part Cor Coef	t
Depth	-.12281	.01085	-.56286	-11.316
Temp	-.09640	.00899	-.53301	-10.716

5.2.5 Testing the General Rate Functions. The general rate functions for compressive strength were tested by the method outlined below to determine how well they fit the data.

1. Dividing the strength by the rate function removes the variation due to rate and only the variation due to other factors remains.
2. STRATE ONE is defined as the strength divided by the best-fitting rate function from equation 5.1.
3. STRATE TWO is defined as the strength divided by the general rate function.
4. The general rate function fit can be determined by comparing the dispersion of STRATE ONE to that of STRATE TWO for each data group. The coefficient of variation was used as the measure of dispersion.
5. If the coefficient of variation for STRATE TWO is not greatly different from that for STRATE ONE for the individual data groups, it can be concluded that the derived general rate function has survived a rather rigorous test.

Exhibit 5.4 lists for each data group the number of observations, the mean, standard deviation, and coefficients of variation for each STRATE ONE and STRATE TWO. The tests for the general rate functions are that (1) the average value of STRATE TWO should be very close to that of STRATE ONE, and that (2) the coefficient of variation of STRATE TWO should also be very close to that of STRATE ONE. All data, including the groups eliminated earlier, were processed.

In examining Exhibit 5.4, which represents horizontal ice, it is seen that 36 of the 53 groups have coefficients of variation for STRATE

TWO smaller than for STRATE ONE. These particularly good fits are in the fine ice, center ice, and bottom 90-90 ice. In the medium 90-90, bottom 90-00 and 90-45 ice, the coefficients of variations for STRATE TWO are usually larger than those for STRATE ONE.

Since coefficient of variation is affected by differences in size of either the standard deviation or the average value, it is considered that a difference in coefficient of variation of about 0.0050 is smallest for which it can be said that the differences should be examined. Using this criterion, the coefficients of variation of STRATE TWO are found to be too large for the following ice groups.

ICE	NUMBER
Fine	0 of 4
Med 90-90	2 of 6
Center	0 of 19
Bot 90-00	2 of 9
Bot 90-45	2 of 8
Bot 90-90	0 of 7

It would seem that the horizontal general rate function fits the fine, center and bottom 90-90 ice very well but there is some question about the other three singto.

The medium 90-90 ice indicates that the rate exponent decreases with increasing depth which is contrary to the general rate function being used for horizontal ice. However, three data groups are of early ice and the fourth is at the melting temperature so the data are not generally good.

The bottom 90-00 groups that do not fit well are small and one is at the melting temperature. The remaining data groups fit quite well for the bottom 90-00 ice. The two bottom 90-90 groups are also small. One is warm and has a very low range of rate. It seems reasonable to conclude that the general rate function for horizontal ice fits the data adequately well.

5.2.6 The Orientation and Type Function of Rate Exp. Rotvar is the orientation and type function of the rate exponent, r , and it is a simple multiplying variable that ranges from .55 to 1.26 in the equations.

$$r = A(\text{Depth})^d (\text{Temp})^{\dagger} (\text{Rotvar})$$

Exhibit 5.5 is a plot of Rotvar versus average STRATE TWO for the different horizontal singto. This plot indicates a good curvilinear relationship between the two groups. A least squares parabolic fit yields the equation

$$\text{Rotvar} = .709 + .443 (\text{Strate Two}) - .088 (\text{Strate Two})^2 \quad 5.5$$

with a standard deviation of .036. When this equation is differentiated and the derivative set equal to zero, it yields a maximum Rotvar of 1.27 at a STRATE TWO value of 2.5. These values are very close to those values for 90-45 ice and possibly indicates that 90-45 ice represents a limiting

case of the general load rate functions. The physical significance of this point should be pursued. Each STRATE TWO mean contains some error due to experimental variability and additional variability due to undefined functions of temperature, brine volume, depth and perhaps other variables. The different singto, however, have been tested at temperatures and brine volume of roughly the same average values and ranges, so this relationship should not be completely discounted.

Table 5.6 shows the values of Rotvar and STRATE TWO for horizontal singto and indicates an inverse relationship between Rotvar and STRATE TWO. This relationship is probably the result of the number of crystal boundaries and Inter-platelet brine planes which are oriented in the plane of maximum principal shear. The greater the number of boundaries and brine planes, the more viscous the bulk properties might be expected to be. One reason for this is the lesser ice area and the higher local shear stress in ice which bridges the brine plane and possibly the crystal boundaries. A second reason is the probable orientation of the bridging ice basal plane, being parallel to the brine plane.

Table 5.6

Values of Strate, Compression

ORIENTATION	ROTVAR	STRATE TWO AVERAGE
Bot 90-45	1.26	2.87
Center	1.00	4.28
Med 90-90	.79	4.95
Bot 90-90	.79	4.90
Bot 90-90	.60	5.47
Fine	.55	5.34

5.2.7 Characteristics of Strate. Strate should have less variation than does strength because the variability due to rate has been removed. Some problems exist in measuring the change in variation.

The calculations were made in logarithms and it is more convenient to use the log values that are available.

$$\text{If } \ln(\text{strength}) = i \pm j$$

$$\text{Strength} = e^{i \pm j} = e^i e^{\pm j}$$

where i is the average and j is the standard deviation of $\ln(\text{strength})$. The value of e^j seems to be the most useful measure of variability of strength.

Table 5.7

Average Rate Function, Compression

ICE	\bar{j} STRENGTH	\bar{j} STRATE	CHANGE \bar{j}	PERCENT CHANGE	AVERAGE F(RATE)
Fine	1.99	1.35	.64	65	1.97
Med 90-90	1.56	1.56	.10	15	3.50
Center	2.03	1.66	.37	36	4.31
Bot 90-00	1.73	1.42	.31	43	3.48
Bot 90-45	2.17	1.39	.78	66	11.9
Bot 90-90	1.84	1.38	.46	55	4.46
Med 00-90	1.53	1.53	.00	00	3.26
Bot 00-90	1.91	1.69	.22	24	2.79
All Comp	2.28	2.68	-.40	-31	4.25

In examining the data contained in Table 5.7 it is seen that all ice except the suspect medium 90-90 ice shows substantially higher values of \bar{j} for strength than for strate. The bottom 00-90 ice, which is the strongest and least rate sensitive, had the least variation removed. The bottom 90-45 ice, which is the most rate sensitive, had the greatest variation removed.

Since
$$\text{Strate} = \text{Strength}/(f(\text{Rate}))$$

$$f(\text{Rate}) = \text{Strength}/\text{Strate}$$

and a useful comparison may be made by setting

$$\text{Average } f(\text{Rate}) = \text{Average Strength}/\text{Average Strate}.$$

Table 5.7 lists the average $f(\text{Rate})$ for the different singto. The variation within each singto is reduced, but at the same time, the spread between the different singto is increased as compared to the value for strength. Exhibit 5.6 shows average strength and average strate versus orientation for the bottom ice.

5.3 RATE OF LOADING EFFECT, TENSION

5.3.1 Initial Analysis. For the tensile strength testing, a series of direct tension testing apparatus was developed. An improved model was adopted with test 880 and the final model was adopted with test 1446.2. The data have been classified according to the apparatus used. Data prior to test 880 are classified as "very early" and are not used, data from 880 to 1446.2 are classified as "early" and are used but considered questionable. Data continuing from 1446.2 on are classified as "late" data and are considered to be generally good. The early and late data were kept separated in this analysis.

The tension data fall into four failure types; good test, weld failure, head failure, and no failure. Obviously, in the analysis of maximum

strength, only the good tests can be used. For some tests, no rate information is available and these data cannot be used in an analysis of the effect of rate on strength.

A total of 1054 tests were available and those which were eliminated are shown in Table 5.8.

Table 5.8
Tension Data Eliminated

Type Tests Removed	No. Removed
Very early tests	139
Weld Failure	54
Head Failure	38
No Failure	11
No Rate Information	35

The 777 tests remaining were sorted by ice type, orientation, and early or late. Table 5.9 shows the inventory of tests.

Table 5.9
Inventory of Useable Tests

<u>Ice Type</u>	<u>Ice Orientation</u>	<u>Early</u>	<u>Late</u>	<u>Total</u>
<u>Major Groups</u>				
Fine	90-11(Random)	26	--	26
Medium	90-90	9	12	21
Center	90-11(Random)	32	155	187
Bottom	00-90	--	100	100
Bottom	90-00	23	144	137
Bottom	90-45	11	92	103
Bottom	90-90	26	124	150
<u>Minor Groups</u>				
Bottom	22-90	--	6	6
Bottom	67-90	--	6	6
Bottom	90-22	1	6	7
Bottom	90-67	--	6	5
Bottom	45-90	--	29	29
Total		<u>128</u>	<u>649</u>	<u>777</u>
Total, Major Groups		127	597	724

The minor groups shown are essentially based on strength information at a single depth, temperature, and rate of loading. They cannot be used in determining the rate function. The data remaining for analysis are the 724 tests of the seven major type and orientation groups. In compressive strength, the factors that controlled the rate function had proved to be ice type, ice orientation, depth, and temperature.

The 724 remaining tension tests, which were already sorted by type and orientation were further sorted into groups with limited temperature and ice depth ranges and also with the early data kept separate from the late data. Table 5.10 shows the number of data groups for each single ice type and orientation (singto).

Table 5.10

Tension Data Groups

<u>Singto</u>	<u>Early Groups Data</u>		<u>Late Groups Data</u>		<u>Total Groups Data</u>	
Fine	2	26	0	0	2	26
Medium	1	9	1	12	2	21
Center 90-11	2	32	11	155	13	187
Bottom 00-90	0	0	7	100	7	100
Bottom 90-00	1	23	7	114	8	137
Bottom 90-45	1	11	7	92	8	103
Bottom 90-90	1	26	7	124	8	150
Total	8	127	40	597	48	724

The average size of the individual data group is 15 tests. The largest number of tests and largest number of groups are from the center ice.

5.3.2 Factors that Control Rate Exponent. The analysis for the general rate function for tensile strength is quite similar to that used for compressive strength. Some difference arises due to the nature of the tension test and to improved analytical procedure.

Three factors affected the results as compared to those for compression results.

1. Tensile strength proved to be less dependent upon the rate of loading than did compressive strength.
2. Tensile strength data have much more scatter than compressive strength data.
3. The number of tests per group (average of 15) was relatively small.

As a result, the pattern of rate effect on tensile strength was much less clear than the pattern observed in the compressive study.

A few tests with low strength, particularly at high loading rates, were found, and because tension tests are particularly sensitive to flaws, it is possible that these involved flawed specimens. It was decided to eliminate the obviously weak specimens, and 26 tests were eliminated as shown in Table 5.11. Later testing under a different study, as reported in Chapter 10, has shown a strength reduction at very high load rates, much higher than those reported here.

Table 5.11

Weak Data Eliminated

Singto	Initial Data	Eliminated Data
Fine 90-11	26	0
Medium 90-90	21	0
Center 90-11	187	10
Bottom 00-90	100	9
Bottom 90-00	137	2
Bottom 90-45	103	0
Bottom 90-90	<u>150</u>	<u>5</u>
Total	724	26

In no case were more than three tests removed from a group.

Exhibit 5.8 lists the information developed showing identification of the individual groups, the number of tests per group, the averages of the natural logs of strength, depth, temperature and rate, the standard deviation of the natural log of rate, the rate exponent and the Student's *t* for the rate exponent value.

5.3.3 Rate Exponent for a Single Type and Orientation Group. When the rate exponent values, *r*, had been obtained for the individual groups, it was necessary to combine them to see if they would fit an equation of the form

$$r = A(\text{Depth})^m (\text{Temperature})^n \quad 5.6$$

Two problems developed; the first was scatter in rate exponent within the singto due to the small number of tests per group and the scatter inherent in the tension data; the second was the need for weighting the data groups.

No means was found for handling negative values of exponents in a regression analysis and it was necessary to partly ignore the data groups with a negative rate exponent. Forty six groups now remained, three with negative rate exp. values and 672 remaining useable tests.

Weighting of the data was required because:

1. Each data group represented different numbers of observations,
2. The range of rate for the different groups varied greatly, and
3. The significance of the rate exponent value for the different groups, as measured by *t*-test, varied.

An arbitrary weighting formula was adopted:

$$\text{Weight for the group} = (\text{No. of obs}) (\text{range}) (t^{1/2}) \quad 5.7$$

Obviously, the number of observations is a direct component of a weighting formula. The range is because the data group with the greater range of load rate should give a better indication of the rate function. The range was defined as $\ln(\text{Rate})$ plus the standard deviation of $\ln(\text{Rate})$. It had been observed that the relationship between the square root of Student's t and significance defined in percentile values is approximately linear in the normal range of t . This is the basis for using $t^{1/2}$ in the weighting formula.

A weighted multiple regression was used to fit a data group with the equation:

$$r = A(\text{Depth})^a (\text{Temperature})^b (\text{Rotvar}) \quad 5.8$$

where Rotvar is a constant for each singto which allows all singto to be grouped as in the analysis of compression data. Table 5.12 shows the results obtained for each singto and the multiple correlation coefficient.

Table 5.12

Rate Exp. for Tension Singto

<u>Singto</u>	<u>Groups</u>	<u>Av r</u>	<u>A</u>	<u>a</u>	<u>b</u>	<u>R</u>
Center	13	.053	.054	-.142	.065	.387
Bottom 00-90	6	.036	.012	.319	-.078	.380
Bottom 90-00	6	.040	large	-1.919	-.448	.886
Bottom 90-45	8	.109	.613	-.382	-.165	.660
Bottom 90-90	8	.048	.554	-.628	-.050	.268

The analysis is continued similar to that for compression.

5.3.4 Developing General Rate Functions. Rotvar (Rate Orientation and Type Variable) again is a multiplying function in the rate exponent. It is designed to be a constant for each singto. Center ice, which has the most data, the largest number of data groups, and the greatest range in depth, was assigned a Rotvar value of 1.00 in the same manner as with the analysis of compression data. All other singto must then have Rotvar fitted so they may be grouped with center ice.

The final fit for the horizontal rate function is

$$r_h = .082(\text{Depth})^{.295} (\text{Temperature})^{.064} (\text{Rotvar}) \quad 5.9$$

with the Rotvar values shown in Table 5.13. R, the multiple correlation coefficient, is 0.74.

Table 5.13
Fitting Tension Rotvar

<u>Singto</u>	<u>Rotvar</u>
Medium	4.48
Center	1.00
Bottom 90-00	1.82
Bottom 90-45	4.48
Bottom 90-90	2.12

For the vertical (bottom 00-90) ice, the rate exponent is

$$r_v = .012(\text{Depth})^{.319} (\text{Temperature})^{-.078} \quad 5.10$$

5.3.5 Testing the General Rate Function. Strate, the strength function with the rate effect removed, is obtained by dividing strength by the rate function. The compression rate analysis had shown that weaker ice had a larger rate function; and therefore, strate for the weaker ice was proportionately smaller than for the stronger ice. As a result, the relative variation for strate was greater than that for strength when all of the data were grouped, even though the rate function had been responsible for much of the variation in the data. It was expected that tension data might show the same phenomena, and statistical analyses were made on the small data groups for a true indication of the result of removing the rate effect.

Exhibit 5.9 shows the sums, raw cross products, averages, standard deviations and coefficients of variation for the individual data groups for both strength and strate. Exhibit 5.10 shows the same information for combinations of data, by singto and larger groupings. Table 5.14 summarizes the information in the Exhibits by showing selected information regarding the coefficients of variation of the groups. The basic test is whether the coefficient of variation for strate is less than that for strength; if so, part of the variation in the strength data is accounted for by the rate function.

Table 5.14

Study of Coefficient of Variation for Strength and Strate

<u>Singto</u>	<u>All Groups</u>	<u>Late Groups</u>	<u>Ratio of Coefficients of Variation</u> <u>Strate/Strength</u>	
			<u>All</u>	<u>Late</u>
	<u>Improved/total</u>	<u>Improved/total</u>		
Medium	2/2	1/1	1.516	.886*
Center	12/13	11/11	.878	.848
Bottom 90-00	7/8	6/7	1.00	1.01
Bottom 90-45	8/8	7/7	.844	.862
Bottom 90-90	6/8	5/7	.972	.955
All Horiz	35/39	30/33	1.092	1.103
Bottom 00-90	4/7	4/7	1.036	1.036
All Tension	39/46	34/40	1.133	

*one group only

The coefficient of variation for strate is decreased for 35 of the 39 data groups and 30 of the 33 groups of late data. This decrease indicates that the extraction of the rate function dependence has indeed been successful in removing some of the variation in the data.

The ratio of the coefficients of variation of strate to that of strength for a singto and also for a larger group indicates an improvement in the variation in the entire group if the ratio is less than one. The center and bottom 90-45 ice show a relatively large improvement indicating that rate does account for a substantial portion of the variation of these data. The bottom 90-90 shows a smaller improvement and the bottom 90-00 is not affected. The horizontal data, when grouped show that the relative variation is greater in strate than in strength. This result is identical to that discovered in analysis of the compression data. The vertical data also show an increase in relative variation.

5.4 RATE OF LOADING EFFECT: TENSION AND COMPRESSION COMPARISONS

It is desirable to examine the average values of strength and strate for the different singto for both tension and compression. The study of the medium ice is limited by the small number of tests, particularly in tension, but the other data should provide good comparative values. Table 5.15 shows the average strength and strate values in compression and tension as well as some comparative results.

Table 5.15

Strength and Strate Values

Singto	Compression			Tension			Comp/Tension	
	Strength	Strate	Ratio	Strength	Strate	Ratio	Strength	Strate
Med 90-90	493	140	3.50	94.4	35.0	2.70	5.22	4.00
Center	313	72	4.31	96.3	74.5	1.29	3.25	0.97
Bot 90-00	822	237	3.48	114.2	92.3	1.24	7.20	2.57
Bot 90-45	210	17	11.9	100.2	56.2	1.78	2.10	0.30
Bot 90-90	600	134	4.46	156.8	120.6	1.30	3.19	1.11
All Horiz	405	90	4.52	116.3	85.7	1.36	3.48	1.05
Bot 00-90	985	354	2.79	261.7	216.8	1.21	3.76	1.63
All Data	465	109	4.25	129.6	98.7	1.31	3.59	1.10

The ratio of strength/strate is also the average function of rate for the singto. It is apparent that the rate function is extremely important in compressive strength with an average value for all horizontal data of about 4.52. In tension, the equivalent value is only 1.36 showing that rate is much less important in tensile strength.

All compressive strengths are much greater than tensile strengths for the same singto. The compressive and tensile strate values, however, are roughly equivalent with a compressive-strate/tensile-strate ratio for all horizontal data of 1.05. The individual singto behave differently however. The weaker, more rate-sensitive, singto (bottom 90-45 and center) is weaker in compressive strate than in tensile strate; the stronger, less rate sensitive singto remain stronger in compressive strate than in tensile strate.

Table 5.16 is a listing in ascending order of compressive rate functions for the various singto, their compressive and tensile average rate functions, and the ratio of compressive to tensile average rate functions.

Table 5.16

Average Rate Functions

Singto	Average f(rate)		Ratio Comp/Tens
	Comp.	Tension	
Bot 00-90	2.79	1.21	1.30
Bot 90-00	3.48	1.24	2.81
Center	4.31	1.29	3.34
Bot 90-90	4.46	1.30	3.43
Bot 90-45	11.9	1.78	6.69
All Horiz	4.52	1.36	3.32

The singto ranking for average tensile rate functions is the same as for compressive rate function, but the compressive rate functions increase more rapidly than do those for tension.

5.5 SUMMARY

5.5.1 Conclusions

1. The strength of sea ice increases as the rate of loading increases, within the load rate range of these experiments.
2. The data studied indicate that general rate functions can be written for both horizontal and vertical strength.
3. The variables that affect the rate function are depth, temperature, orientation and ice types.
4. The rate function included in the equation

$$\text{Strength} = (\text{Rate} + \text{Constant})^r \text{ --- (All other effects)}$$

has been adopted; however, the constant seems rather random. An average value of 10 or 20 psi/minute was found but with wide scatter and no defineable pattern. This constant is important only at low load rates where the effect of creep may enter. Since creep is not being studied at this time, a rate constant of zero is used.

5. The general rate functions are of the form $(\text{Rate})^r$, and following are the empirical expressions for r.

Compression

Horizontal

$$r_{ch} = 0.166(\text{Depth})^{0.138}(\text{Temp})^{0.09}(\text{Rotvar})$$

	<u>Ice</u>	<u>Rotvar</u>
Fine	90-11(Random)	0.55
Medium	90-90	0.79
Center	90-11(Random)	1.00
Bottom	90-00	0.60
Bottom	90-45	1.26
Bottom	90-90	0.79

Vertical (Bottom 00-90)

$$r_{cv} = 0.316(\text{Depth})^{-.123}(\text{Temp})^{-0.096}$$

Tension

Horizontal

$$r_{th} = 0.082(\text{Depth})^{-0.295}(\text{Temp})^{-0.064}(\text{Rotvar})$$

	<u>Ice</u>	<u>Rotvar</u>
Medium	90-90	4.48
Center	90-11(Random)	1.00
Bottom	90-00	1.82
Bottom	90-45	4.48
Bottom	90-90	2.12

Vertical (Bottom 00-90)

$$r_{tv} = 0.012(\text{Depth})^{0.319}(\text{Temp})^{-0.078}$$

- Depth is in inches, temperatures in °C and rate in psi/minute.
- It is not known why depth and temperature affect the rate function. It is interesting that sign reversal between horizontal and vertical rate functions are opposite for tension and compression.
 - A. For almost all of the small groups of data, the relative variation of strate is less than that for strength.
B. When all data of a single type and orientation of ice are grouped, the relative variation of strate is less than that for strength only if the ice is fairly rate-sensitive. For ice not rate sensitive, the relative variation of strate is greater than that for strength.
C. When all data are grouped, the relative variation of strate is greater than that for strength.
 - While the average rate function in compression has a value of about 4.52, the average rate function in tension is approximately 1.35. Compressive strength is several times as sensitive to rate as is tensile strength.
 - The average compressive strength (horizontal only) is about 3.5 times as great as the average compressive strate. However, the average compressive strate is only about 1.05 times as great as the tensile strate. The conclusion is that the gross difference

In compressive and tensile strength is due to the large effect of rate in compression.

11. In examining the individual ice type and orientation groups, it is found that some of the weaker types and orientations are weaker in compressive strate than in tensile strate. The stronger types and orientations maintain a stronger compressive than tensile strate. The effect of ice type and orientation is extremely important in strate.

Later it may be possible to refine the results obtained in this analysis and express them in a less empirical manner. The achievement thus far is the development of general rate functions. The general rate functions for horizontal forces appear to fit the data well with the exception of medium 90-90 ice. Enough sample types, orientations and depths were available to yield results in which confidence can be accepted. The vertically oriented ice data were sharply limited in number of samples, types, and orientations; the results are then much more tentative than for the horizontally oriented ice.

The measurement of variation of strength and strate is not entirely satisfactory. A better measure could be obtained by a statistical analysis of the antilog values. The value of e^j does provide a measure of variability, but this type of measure is questionable as to the precision which it can provide.

Chapter 6

BRINE AND SOLID SALT EFFECTS - CENTER ICE - ONE INCH DEPTH

6.1 INTRODUCTION

6.1.1 Sea Ice Formation. The freezing of sea water is rather complex because the sea water is a dilute solution of several salts. The salts depress the freezing point below the freezing temperature of fresh water, and when freezing begins, pure water ice is formed and the excluded salts become segregated in the liquid brine. Part of the enriched brine drains away from the growth boundary of the ice, but part is trapped in the ice structure and gives sea ice a net salinity. The ice and its entrapped brine cool as the ice sheet thickens. With the lowering of the temperature, the salt in the brine begins to precipitate and is incorporated into the solid ice structure. Sea ice thus has three major phases:

1. Pure water ice.
2. Liquid brine of varying concentration.
3. Solid salts of several types.

Ringer (1) investigated the freezing of sea water and established the order and temperature at which salts precipitate. Nelson and Thompson (4) confirmed Ringer's conclusions. Assur (7) developed a complete phase table at intervals of two degrees over the range 0°C to -54°C for standard sea ice (sea ice with a salinity of 34.325 per mil) showing:

1. Ions in solution
2. Water
3. Solid salt
4. Ice

Assur's table was used for the phase studies in this report.

Table 6.1 gives information concerning precipitated salts from Assur's phase table at the three points of -22°, -36° and -54°C. The table shows the individual salts which precipitate in sea ice, the temperatures at which they begin to precipitate, the quantity (in gm/kg of sea water) which has precipitated at the three temperatures and the ratio of individual salts to the total precipitated salts expressed in per cent.

Table 6.1

Quantities of Precipitated Solid Salts at Various Temperatures.

Salt	Precip. Temp. °C	-22°C		-36°C		-54°C	
		gm/kg	%	gm/kg	%	gm/kg	%
$\text{CaCO}_3 \cdot 6\text{H}_2\text{O}$	-2.2	0.243	2.8	0.314	0.6	0.319	0.5
$\text{Na}_2\text{SO}_4 \cdot 10\text{H}_2\text{O}$	-8.2	8.171	94.5	8.883	18.8	8.883	14.0
$\text{MgCl}_2 \cdot 8\text{H}_2\text{O}$	-18.0	0.235	2.7	1.579	3.3	2.284	3.6
$\text{NaCl} \cdot 2\text{H}_2\text{O}$	-22.9	0.000	0.0	36.492	77.2	38.034	59.8
KCl	-36.8	0.000	0.0	0.000	0.0	0.725	1.1
$\text{MgCl}_2 \cdot 12\text{H}_2\text{O}$	-43.2	0.000	0.0	0.000	0.0	13.275	20.9
Unk. Salts		0.000	0.0	0.046	0.1	0.061	0.1
Total		8.649		47.314		63.576	

Of the 34.325 grams of ions in one liter of standard sea water at 0°C, 1.040 grams remain in solution at -54°C. The 33.285 grams not remaining in solution are in the 63.576 grams of solid salts shown in Table 1, mostly as hydrates.

The lower surface of sea ice remains at the freezing point of the sea water (-1.8°C) while the upper surface temperature is controlled by the air temperature, wind, and snow cover. Temperatures in the Arctic do not get extremely low and the sea ice normally has a cover of snow; therefore, extremely low sea ice temperatures do not normally occur. Only sodium sulfate and sodium chloride salts seem important in sea ice because the calcium carbonate is present only in trace quantities and $\text{MgCl}_2 \cdot 8\text{H}_2\text{O}$, which begins to precipitate at -18°C, has deposited only small quantities at -22.9°C where large quantities of sodium chloride begin to precipitate. The other salts, such as potassium chloride, may never precipitate in Nature except in isolated instances.

6.1.2 Current Knowledge of General Physical Properties. Weeks (8) describes ice formed, while there was still wave motion, in the top sheet as small crystals with vertical crystallographic axes except that the crystals have been disarranged and tilted by the wave action. The amount of wave action governs the degree of disarrangement. Below the initial ice sheet, the crystals grow downward and change orientation to a horizontal c-axis. The crystals are composed of small platelets normal to the c-axis and the brine and air trapped in the ice is distributed in the individual ice crystals between the platelets of pure ice. During the freezing process, the platelets are first completely separated by layers of brine and form a skeletal layer of 1-2 cm thickness. As the freezing continues, ice bridges begin to connect the platelets and the ice begins to have some strength.

Anderson and Weeks (5) have shown that the cylinders of brine between the ice platelets are either circular or elliptical in horizontal section and often extend vertically entirely through the ice sheet. When sea ice fails in tension or flexure, it breaks primarily along the brine cells parallel to the small platelets, because the liquid brine reduces the effective cross-sectional area of the ice and because the brine cell geometry produces stress concentrations. Two geometric models were developed by Weeks and Anderson, one with round brine channels and one with brine channels of constant width. The reduced cross-section and stress concentration were incorporated in equations for strength with the effective cross section reduction expressed in terms of brine volume, the ratio of liquid brine volume to total volume.

Anderson and Weeks also reported that solid salts would exist at temperatures below the eutectic points of the various constituents, but they believed that the solid salts would affect strength only after sodium chloride began to precipitate. They limited their analysis to warm ice but concluded that solid salts would act as binders rather than stress concentrators in very cold sea ice because others reported that the very cold sea ice could have strengths higher than lake ice.

Assur (7) discussed and further developed a description of the properties of sea ice. He developed the geometric model with brine channels with elliptical cross sections. This model is the most useful that has been developed. Figure 6.1 is a block diagram of it showing the vertical brine channels, ice platelets, and bridging ice. The three axes are the crystal axis, brine axis and zenith axis. (Assur used a growth axis pointed down rather than the zenith axis up.)

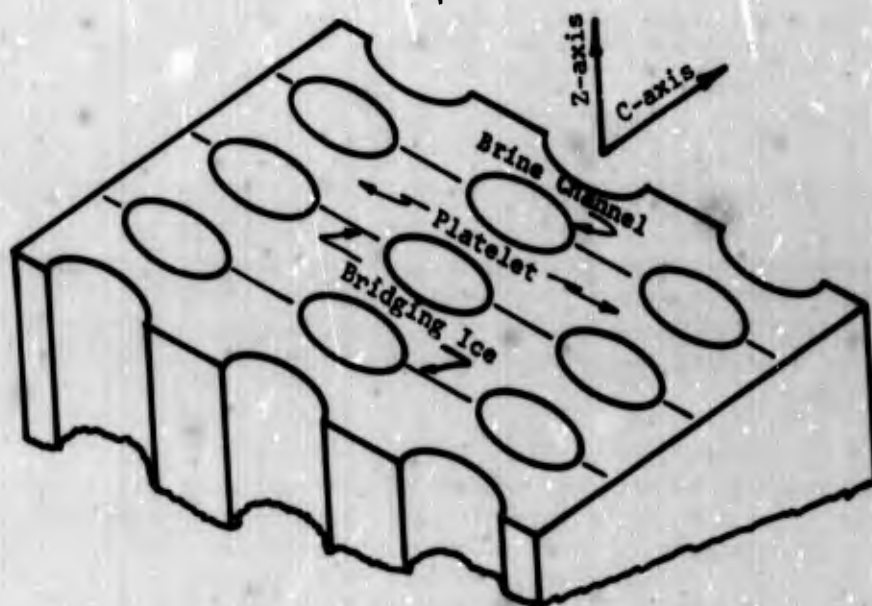


Figure 6.1 Block diagram of Assur's elliptical model.

Figure 6.2 Plan view of elliptical model.

Figure 6.2 is a plan view of Assur's elliptical model.

The geometry of the elliptical model is easily developed. The ratio of the major to minor axis is,

$$e = r_b / r_a, \quad 6.1$$

The cross-sectional area of an ellipse is,

$$F = \pi r_a r_b = \pi r_b^2 / e \quad 6.2$$

The relative brine volume in a unit thickness is

$$v = \pi r_b^2 / e a_o b_o \quad 6.3$$

The relative brine area in the brine plane (Z-B plane) is

$$F_g = \frac{2r_b}{b_o} = \sqrt{\frac{4a_o b_o e v}{\pi b_o^2}} = \sqrt{\frac{4a_o e v}{\pi b_o}} \quad 6.4$$

The strength in the brine plane is

$$\sigma = \sigma_o (1 - F_g) = \sigma_o \left(1 - \sqrt{\frac{4a_o e v}{\pi b_o}}\right) \quad 6.5$$

where σ is the ice strength of the specimen and σ_o is the basic strength of the bridging ice, including stress concentration effects. Equation 6.5 is equivalent to Assur's Equation 22 except that physical values are used instead of dimensionless relationships and that the brine channels are un-interrupted and extend through the model. This strength relationship is intended to be representative for strength in the brine plane in tension, shear, and compression.

Assur studied the ring tensile strength of 327 specimens and found he could show a linear relationship between the average strength of data groups and $v^{1/2}$ for those data without precipitated salts (v = brine volume expressed as a ratio of brine volume to total volume). However, he found the specimens with solid salts were stronger and concluded that the solid salts reinforced the ice. Precipitation of solid sodium sulfate decahydrate caused an abrupt increase in strength of one-third and precipitation of sodium chloride dihydrate caused a rapid, but smooth, increase in strength. Assur

hypothesized that when failure occurred in the plane of the brine channels, the brine channels acted as stress concentrators but that a relatively thin layer of solid salts was adequate reinforcement to reduce stresses in the pure ice. When strength increased rapidly with precipitation of sodium chloride, the failure in the brine plane probably occurred first in the bridging ice rather than in the reinforced brine channels. The strength of cold ice with large quantities of sodium chloride dihydrate was found to be more than twice or perhaps even three times the strength of natural fresh water ice. Assur also commented that it is possible to assume that salt inclusions increase strength by reducing crack propagation.

Weeks (9) studied salt ice (NaCl ice) as simplified ice suitable for laboratory studies. His laboratory-grown ice at the 30.5" depth (13, Fig. 1) appears to have had crystals with the c-axis horizontal but randomly oriented. He found the ring tensile strength of solid salt-free ice between -5° and -21.2°C to be a linear function of $v^{1/2}$ and not affected by the temperature of the pure ice platelets. For ice containing solid sodium chloride (below -21.2°C) the ring tensile strength was independent of both the temperature of the sample and the volume of solid salt present in the ice. Weeks reasoned that if the brine pockets were filled with salt with strength equal to or greater than the ice matrix, the failure would occur in the matrix and the strength measured would be that of the ice in the matrix.

Weeks also found the ratio of stress concentration in salt ice to that in fresh water ice to be about 1.20, implying that roughly the same stress concentration exists in fresh water ice as in salt ice. The salt ice that Weeks produced was fundamentally different from sea ice because it had a single eutectic point of -21.2°C . At that temperature, all of the brine crystallizes and the system goes directly from a brine-ice system to a solid salt-ice system. On the basis of his studies of salt ice, Weeks reexamined Assur's data and hypotheses and suggested that:

1. The strength of very cold sea ice may approach but will not exceed the strength of fresh water ice.
2. The sodium sulfate decahydrate either does not reinforce the sea ice or makes it about 20 per cent stronger. The correct alternative cannot be decided from the data.
3. The crystallization of $\text{NaCl}\cdot 2\text{H}_2\text{O}$ and possibly $\text{Na}_2\text{SO}_4\cdot 10\text{H}_2\text{O}$ might reinforce the brine pockets and create one or two discontinuities in sea ice strength at unique temperatures at which critical amounts of reinforcing salt have been deposited.

Brown (10) experimented with in-place cantilever tests of sea ice strength at Wales, Alaska, in 1958 and 1959 and at Thule in 1961. He concluded that his data did not indicate any sudden increase in flexural strength caused by precipitation of sodium sulfate decahydrate. He reasoned that any increase in flexural strength due to the precipitation of salts should be gradual since the salts are coming out of solution gradually as temperature decreases.

Graystone and Langleben (11) experimented with ring tensile tests on sea ice during the winter of 1960. They found from their data from specimens not having solid salts, when adjusted for temperature and sorted into groups with small ranges of $v^{1/2}$, that ring tensile strength was linear with

$v^{1/2}$. They found that their data of specimens with solid sodium sulfate fits this same linear expression and suggests that the solid salts do not have a reinforcing effect, perhaps remaining in suspension rather than being incorporated into the solid structure.

The sea ice described in this report has been classified as in Chapter 4:

1. Fine-grained, at or near the surface, with the crystals having a random orientation in all directions, Chlorinity is high.
2. Medium-grained, at or near the surface, with a vertical c-axis and with larger grains.
3. Center ice, found from at or near the surface to a depth which is usually less than two feet. The c-axis is horizontal but is random in that plane.
4. Bottom ice, found from the lower boundary of the center ice to the bottom of the ice sheet. This type has a horizontal c-axis with the direction preferred.

Pack ice more than one year old has been found to be essentially of the bottom ice type but with greatly reduced salinity.

6.2 BRINE SOLIDIFICATION

6.2.1 Examination of the Strate of Center Ice. Most investigators, using ring tensile tests, have found sea ice strength to be a linear function of $v^{1/2}$ and, except for Assur, have not reported solid salt effects. The analysis herein has shown that temperature has a limited effect on the rate function. Except to account for this dependence, the analysis will proceed on the basis used by others with the primary effects of temperature and salinity controlling brine volume and any secondary effects being identified after the brine volume function has been defined.

The largest single grouping of data of this study consists of compression tests made on center ice in early winter 1961-1962 after the testing equipment and techniques had been perfected but before the ice sheet had frozen deep enough to supply bottom ice. These center ice data proved extremely useful in finding the rate function, so it was also investigated to see the effects of brine volume on Strate, the definition of Strate being strength divided by the load rate function.

Figure 6.3 contains a plot of strate versus $(1-v^{1/2})$ for 148 center ice specimens at a depth, of one inch; 82 of the specimens were ice without solid salts and 66 contained solid sodium sulfate. The specimens were 2.5 inches long, 1.4 inches in diameter, and were tested in direct compression. This plate shows:

1. The center ice exhibits a uniform behavior making it possible to use it for further analysis.
2. The Strate for center ice without solid salts is linear with $(1-v^{1/2})$.
3. Ice with solid salts is much stronger than the Strate-brine volume relationship can explain, so the excess strength must be due to salt reinforcement.

Assur (7) suspected that sodium sulfate reinforced ring tensile specimens. Figure 6.3 shows that sodium sulfate strongly reinforces center ice in compression

The ice crystals of the center ice are small (on the order of one-fourth inch in horizontal dimensions) so that a test specimen with a diameter of 1.4 inches contains a substantial number of crystals in each cross section. If the orientation of the crystals is random enough, the center ice can be a relatively homogenous material at the macro scale. Apparently this is the explanation for the uniform behavior of this ice.

Equations 6.1 to 6.5 were developed for the study of failure in the brine plane. Center ice failure must be mainly in the brine planes of the crystals but with some platelets edge-loaded or loaded from the flat side. It appears that the center ice failure system cannot be identified but perhaps can be considered analogous to failure in the brine plane.

The least squares line on Figure 6.3 is for the ice without solid salts. Its equation is

$$\sigma_a = -34.44 + 191.12 (1-v)^{1/2} \quad 6.8$$

where σ_a is Strate. It can be put in the form of equation 6.5 in the following manner:

$$\begin{aligned} \sigma_a &= A + B(1-v)^{1/2} \\ \sigma_a &= A + B - Bv^{1/2} \\ \sigma_a &= (A + B) \left(1 - \frac{B}{A+B} v^{1/2}\right) \end{aligned}$$

The basic strength of the "bridging" ice is:

$$\sigma_o = A + B = 156.68 \quad 6.9$$

A geometric constant for center ice without solid salts is

$$C_o = \frac{B}{A+B} = 1.22 \quad 6.10$$

The equation for the least squares line rewritten is

$$\sigma_a = 156.68 (1-1.22v)^{1/2} \quad 6.11$$

with a standard deviation of 17.94 and correlation coefficient, R, of 0.78.

Exhibit 6.1 is a listing of the data used in this analysis and plotted on Figure 6.3. Exhibit 6.2 explains the code used in Exhibit 6.1.

The reinforcement effect of the solid sodium sulfate makes it necessary to examine these salt deposits geometrically, quantitatively and qualitatively.

Indication of Solid Salt Reinforcement
Center Ice, One Inch Depth

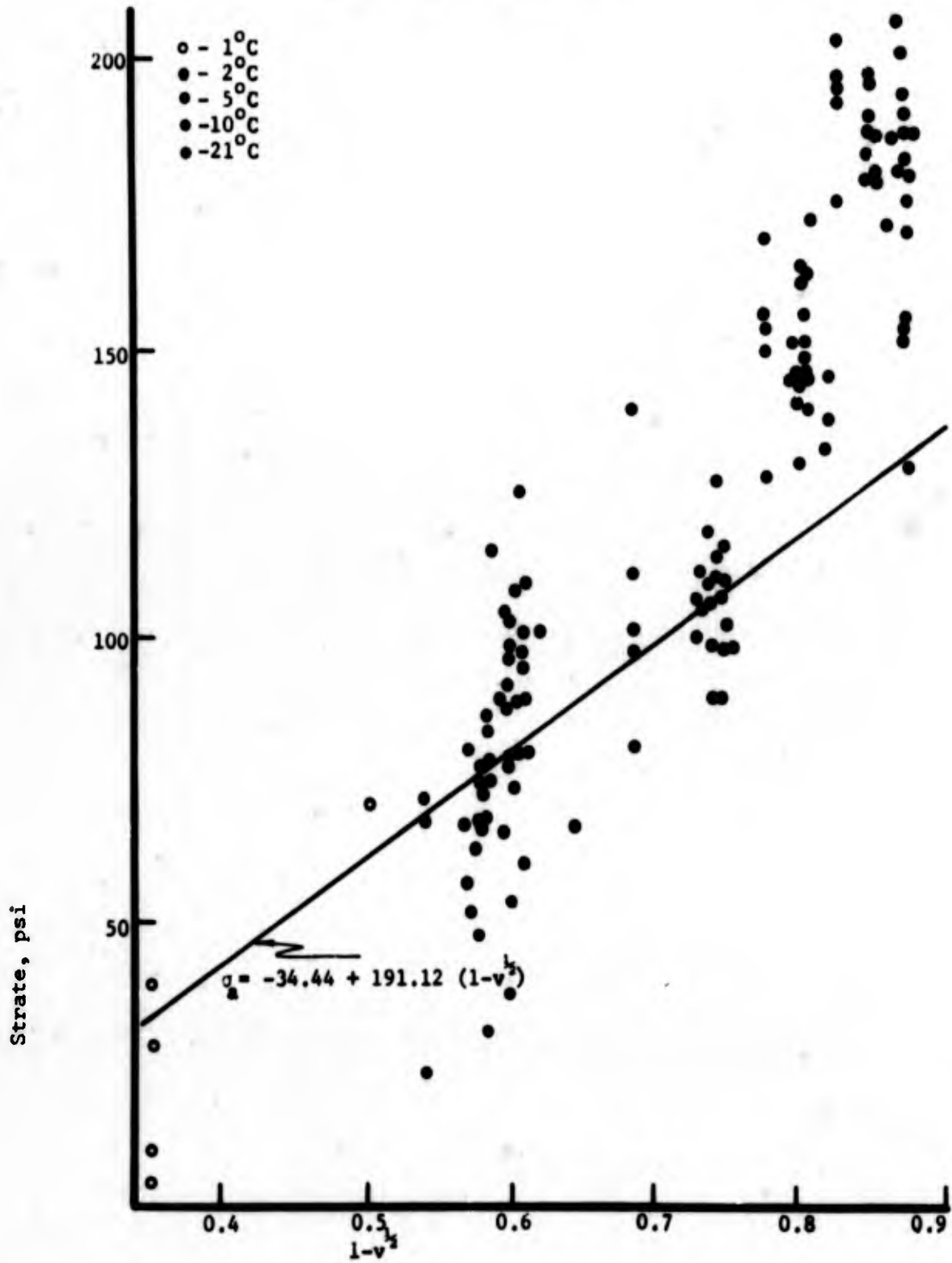


Figure 6.3

Terms and Symbols:

In general, the terms and symbols used in this report are those used by Assur (7) with the necessary additional terms and symbols.

- Alce - Ice deposited in association with solid salts.
 Sall - Salty ice - the combination of solid salts and alce.
 Strate - Ice strength with the rate function removed. psi.
- B-axis - Brine axis.
 C-axis - crystal axis.
 G-axis - Assur's growth axis.
 Z-axis - Zenith axis.
- F - Average cross sectional area of a brine channel.
 F_a - Effective ice area in the brine plane. Relative.
 F_c - Salty ice (sall) area in brine plane. Relative.
 F_d - Cross sectional area of brine and sall. Relative.
 F_e - Sall and brine area in the brine plane. Relative.
 F_g - Brine area in the brine plane. Relative.
 G - Geometric constant for failure in brine plane.
 G_a - Geometric constant for failure in the C-Z plane.
 G_c - Geometric constant for failure in the center ice.
 S - Relative solid salt volume.
 Q - Quality of sall. Ratio of solid salt volume/sall volume.
 T - Temperature, °C. Always measured from 0°C down regardless of sign.
- a_o - Platelet spacing.
 b_o - Brine channel spacing in the brine plane.
 d - Delta or incremental value.
 r_a - Minor radius of the brine channel.
 r_b - Major radius of the brine channel.
 r_c - Minor radius of the sall deposit.
 r_d - Major radius of the sall deposit.
 v - Relative brine volume.
 v_a - Relative brine and sall volume.
 v_b - Relative sall volume.
 v_o - Brine volume at zero strength.
 v_s - Relative volume of solid salts.
- ϵ - Ratio of brine pocket radii.
 ϵ_l - Ratio of sall pocket radii.
 σ - Measured or raw strength. psi.
 σ_a - Strate. psi.
 σ_c - Calculated strength. psi.
 σ_o - Basic strate of bridging ice. psi.
 σ_r - Strate reinforcement of sall. psi.
 σ_s - Sall reinforcement of strate in sall. psi.
 σ_t - Basic strate of ice in the C-Z plane. psi.

6.2.2 Geometric Model for Ice-Salty Ice-Brine System. The geometric models developed in the past (5,7) have been for ice-brine systems. Salt reinforcement makes it necessary to develop a more complete model that includes the solid salts. Assur's phase information, to be developed in more detail in the following sections, indicates that ice is forming at the same time the solid salts are precipitating. The ice that forms in association with solid salts has been called alce (associated ice). The combination of alce and solid salts has been called sali (salty ice).

The brine channel size, at the time the solid sodium sulfate begins to precipitate, is quite small: in the order of 0.03 mm in diameter. The ice obviously forms on the sides of the brine channel walls and the apparent salt reinforcement indicates that the solid salts must also be deposited there. The exact structure and composition of sali is unknown.

The elliptical model shown in Figures 6.1 and 6.2 serves as the basis for further model development. Figure 6.4 shows a plan view of the model with sali deposited on the inner walls of the brine channels.

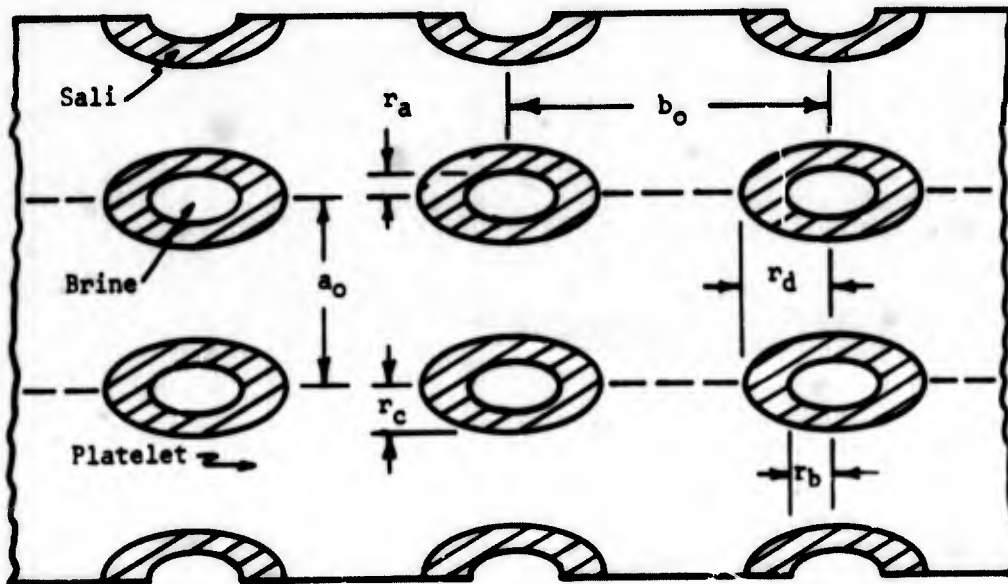


Figure 6.4. Plan view of sea ice model with deposited solid salts.

The radii of the brine channels are still r_a and r_b . Two new radii, r_c and r_d are defined as the outer limits of the sali and correspond to the boundaries of the brine channels at -8.2°C , when sali begins to precipitate.

Defining

$$\epsilon_1 = \frac{r_d}{r_c}$$

The cross-sectional area of salt and brine in one brine channel,

$$F_d = \pi r_c r_d = \frac{\pi r_d^2}{\epsilon_1}; \quad 6.13$$

The relative volume of salt and brine,

$$v_a = \frac{\pi r_d^2}{\epsilon_1 a_o b_o}; \quad 6.14$$

In the brine plane the total area of brine and salt is

$$F_e = \frac{2r_d}{b_o} = \sqrt{\frac{4\epsilon_1 a_o}{\pi b_o}} \sqrt{v_a}; \quad 6.15$$

Thus the area of salt in the brine plane is

$$F_c = F_e - F_g = \sqrt{\frac{4a_o}{\pi b_o}} \left[\sqrt{\epsilon_1 v_a} - \sqrt{\epsilon v} \right] \quad 6.16$$

If $\epsilon_1 = \epsilon$, eq. 6.16 becomes

$$F_c = \sqrt{\frac{4a_o \epsilon}{\pi b_o}} \left[\sqrt{v_a} - \sqrt{v} \right] \quad 6.17$$

The salt is considered to have two strength functions. The first is the strength of the ice and is defined by equation 6.5. The second strength function to be superimposed on the first is due to salt reinforcement.

$$\sigma_r = \sigma_s \sqrt{\frac{4a_o}{\pi b_o}} \left[\sqrt{\epsilon_1 v_a} - \sqrt{\epsilon v} \right] \quad 6.18$$

where σ_r is the salt reinforcement for the specimen and σ_s is the reinforcement strength of the salt. This is a strength function describing sea ice composed of brine, salt and pure water ice.

$$\sigma_a = \sigma_o \left[1 - \sqrt{\frac{4a_o \epsilon}{\pi b_o}} \sqrt{v} \right] + \sigma_s \left[\sqrt{\frac{4a_o}{\pi b_o}} \left(\sqrt{\epsilon_1 v_a} - \sqrt{v} \right) \right] \quad 6.19$$

If the brine channel shape remains constant, $\frac{\sigma_a}{\sigma_o}$ becomes

$$\frac{\sigma_a}{\sigma_o} = \left[1 - \sqrt{\frac{4a_o \epsilon}{\pi b_o}} \sqrt{v} \right] + \frac{\sigma_s}{\sigma_o} \left[\sqrt{\frac{4a_o \epsilon}{\pi b_o}} \left(\sqrt{v_a} - \sqrt{v} \right) \right] \quad 6.20$$

Figure 6.5 shows the strength relationship as compared to brine volume. The strength of the ice increases with the brine volume function to a temperature of 8.2°C. At that temperature the solid salts begin to precipitate and reinforce the ice; then the strength follows the steeper curved line which is the sum of ice strength and salt reinforcement.

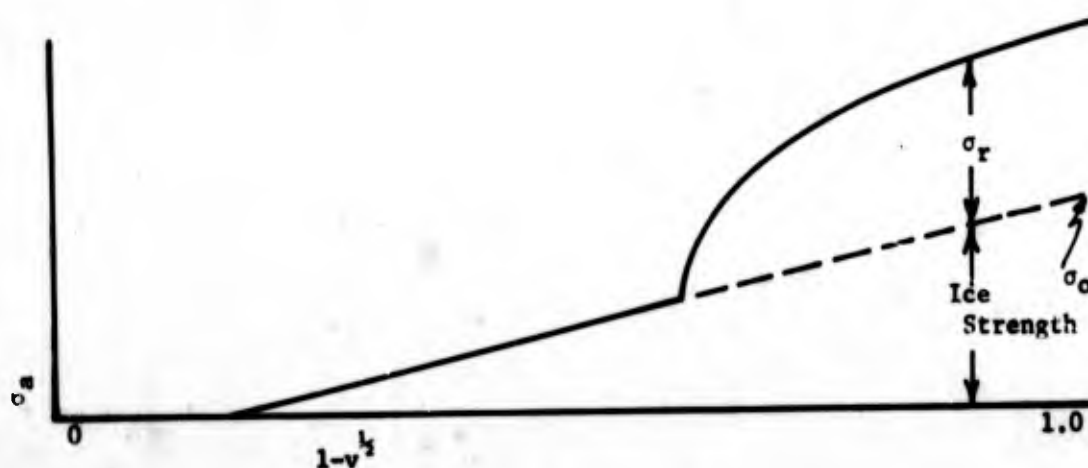


Figure 6.5. Diagram of ice strength and superimposed salt reinforcement.

Defining a geometric factor for ellipses

$$G = \sqrt{\frac{4ab_0c}{\pi b_0}} \quad 6.21$$

and a salt area function

$$S = \sqrt{v_a} - \sqrt{v} \quad 6.22$$

equation 20 becomes

$$\sigma_a = \sigma_0 [1 - G \sqrt{v}] + \sigma_s GS \quad 6.23$$

If there is no solid salt, S is zero and equation 6.23 becomes equation 6.5. G , the geometric factor, contains three variables, a_0 , b_0 and c . If any of these change, G changes and the strength should change. Differentiating equation 6.23,

$$\frac{d\sigma_a}{dG} = -\sigma_0 \sqrt{v} + S \sigma_s \quad 6.24$$

It has been reported (13,14) that an increase in platelet thickness reduces the strength of the ice. Equation 6.24 shows that this would be true for an ice-brine system but if salt is present an additional effect occurs which is opposite in sign. The net result depends on several factors.

The strength functions that have been derived are based on the concept of failure in the brine plane. Sea ice may also fail in other planes. Figure 6.6 shows orientation of forces on a block of ice.

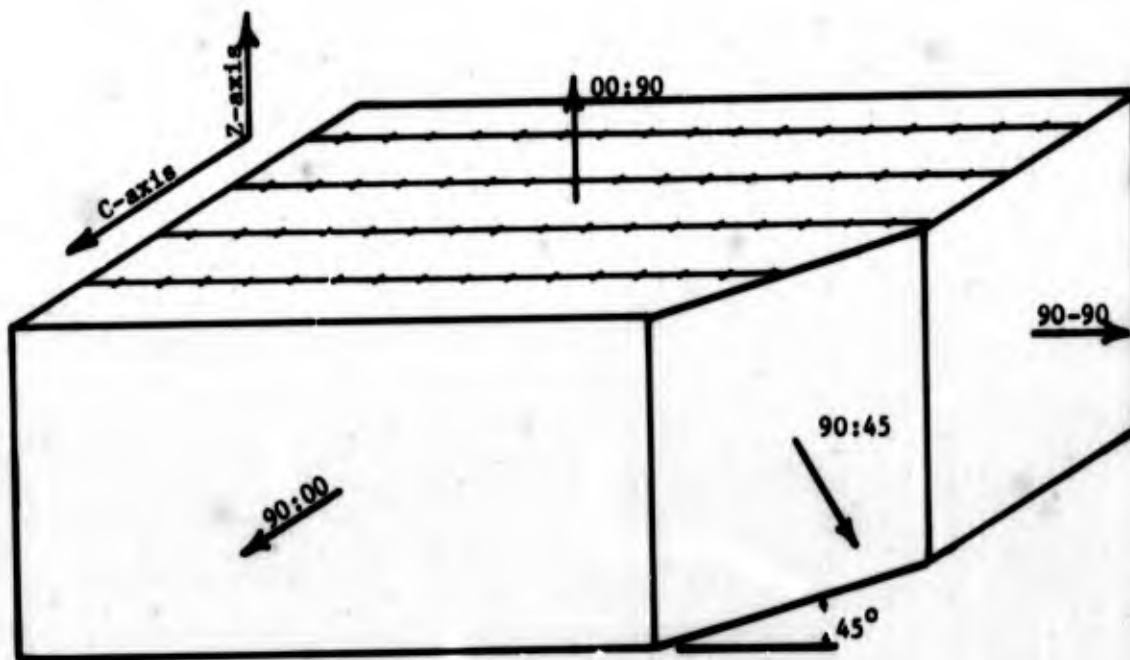


Figure 6.6. Orientation of compressive forces on sea ice.

Tensile forces are shown but compressive forces could be easily shown by reversing the directions of the force vectors. In general, the ice fails across the platelets by crushing, shear, or tension. Ice with 90-45 orientation fails in shear along the brine plane and 90-00 ice in tension tends to fail by tensile separation of the bridging ice in the brine plane. The c-z plane is geometrically representative of cross-platelet failure planes.

The equations for strength in the c-z plane can be developed in a manner similar to that used for brine plane failure. For a brine-ice system

$$\sigma_a = \sigma_t \left[1 - \sqrt{\frac{4b_o}{\pi a_o}} \sqrt{v} \right] \quad 6.25$$

where σ_t is the transverse strength of the actual ice in the plane of failure. For a brine-salt-ice system

$$\sigma_a = \sigma_t \left[1 - \sqrt{\frac{4b_o}{\pi a_o \epsilon}} \sqrt{v} \right] + \sigma_s \left[\sqrt{\frac{4b_o}{\pi a_o \epsilon_1}} \left(\sqrt{\frac{v_a}{\epsilon_1}} - \sqrt{\frac{v}{\epsilon}} \right) \right] \quad 6.26$$

If ϵ_1 equals ϵ this becomes

$$\sigma_a = \sigma_t \left[1 - \sqrt{\frac{4b_o}{\pi a_o \epsilon}} \sqrt{v} \right] + \sigma_s \left[\sqrt{\frac{4b_o}{\pi a_o \epsilon}} \left(\sqrt{v_a} - \sqrt{v} \right) \right] \quad 6.27$$

If a new geometric factor is defined for failure in the c-z plane

$$G_a = \sqrt{\frac{4b_o}{\pi a_o \epsilon}} \quad 6.28$$

Equation 6.27 becomes

$$\sigma_a = \sigma_t (1 - G_a \sqrt{v}) + \sigma_s G_a S \quad 6.29$$

If equation 6.29 is differentiated with respect to G_a

$$\frac{d\sigma_a}{dG_a} = -\sigma_t \sqrt{v} + S\sigma_s \quad 6.30$$

This differential is similar in form to equation 6.24. However, if G and G_a are examined, it is seen that

$$G = \frac{4}{\pi} \frac{1}{G_a},$$

so that changing one of the parameters, such as the platelet thickness, a_o , increases one geometric factor while reducing the other and increases one strength while reducing the other.

Equations 6.25 - 6.30 for cross-platelet failure may be valid in tension and shear. They can not be used universally in compression because the ice platelet when loaded on their edges, exhibit column failure of the platelets at high brine volume values as was seen in failed specimens.

The equations developed for the strength of salt-reinforced ice strength could be extended to include a second form of salt (such as sodium chloride salt) by adding another element similar to the one for sodium sulfate salt.

6.2.3 Sea Ice Phases and Strate of Center Ice. A study of the various aspects of sea ice phases was made using Assur's phase and brine volume results (7) as source information while at the same time an effort was made to relate the phase information to the center ice strength. The study was intended to be as complete as possible, and the final values

desired were the relative volumes of the various components of sea ice and the relationships between these components. Calculations were made for two degree temperature increments from zero to -54°C .

Assur's phase information was considered accurate to the second phase and the third phase was carried as a computational convenience. Three significant numbers were used for brine volume calculations. The values generated in this study are estimated to have accuracy of two phases for standard sea ice and three or four for sea ice of 1 o/oo salinity. An average sea ice density of 0.926 gm/cc was used although density varies somewhat with temperature and salinity (3). Molecular weights and most specific gravities were obtained from the Handbook of Chemistry and Physics, 40th Edition, but the effect of temperature on the specific gravities of the various salts is unknown and was not considered.

Assur, in constructing his table, calculated brine volume for sea ice with a salinity of 1 o/oo so that the brine volume for ice of any salinity could be obtained by multiplying the table value by the salinity. This procedure was followed for the various relative volumes.

After the phase information was developed, curves were fitted to the various important relationships deemed an expression of the form:

$$Y = A + B (X)^N \quad 6.31$$

by solving first for the best-fitting N and then solving by least squares for A and B.

6.2.4 Quantitative Aspects of Salt Deposits. While values have been generated in the phase studies to -54°C , the data ranges from -1° to -21°C and this study is primarily concerned with that temperature range. All temperatures used are positive in sign while measuring temperatures below 0°C . Table 6.2 shows the important quantitative information obtained from the source data and developed in the phase studies for ice of 1 o/oo salinity to a temperature of -22°C .

Table 6.2

Quantitative Data for 1 o/oo Salinity Sea Ice.

Temp °C	Ions gm/l	v cc/l	v _s cc/l	Δ v _s cc/l	Alce cc/l	Δ Alce cc/l	Sali cc/l	Δ Sali cc/l	S Rel.
0	.000	1000.00	.000	.000	0.000	0.000	0.000	0.000	.0000
-2	.001	24.00	.000	.000	0.000	0.000	0.000	0.000	.0000
-4	.001	12.40	.000	.000	0.000	0.000	0.000	0.000	.0000
-6	.002	8.60	.001	.000	0.000	0.000	0.000	0.000	.0000
-8	.002	6.67	.001	.000	0.000	0.000	0.000	0.000	.0000
-10	.050	5.35	.075	.074	1.037	1.037	1.113	1.111	.0071
-12	.073	4.82	.112	.036	1.773	.735	1.885	.771	.0124
-14	.083	4.33	.127	.015	2.290	.517	2.418	.532	.0163
-16	.090	3.95	.137	.010	2.687	.396	2.825	.406	.0194
-18	.095	3.65	.145	.007	3.018	.331	3.163	.338	.0221
-20	.099	3.38	.151	.006	3.312	.294	3.464	.300	.0245
-22	.102	3.14	.158	.006	3.566	.254	3.724	.260	.0268

The curves that have been fitted to the cumulative values in Table 6.2 and their standard errors are:

Curve	S. E.	
Salt used = $0.926 - \text{salt shown} = 0.109 - 17.98/T^{2.48}$.001	6.32
$v = 1.03 + 45.80/T$.07	6.33
$v_s = 0.168 - 26.53/T^{2.46}$.002	6.34
$\text{Alce} = 6.55 - 32.28/T^{.767}$.017	6.35
$\text{Sali} = 6.60 - 35.26/T^{.808}$.009	6.36
$S = 0.082 - 0.180/T^{.381}$.0001	6.37

The units in the equations are identical with those in Table 6.2. The brine volume data used for curve fitting ranged from -2° to -22°C. All other curves are for the range from -10° to -22°C and can probably be extrapolated to -8.2° and -22.9°. Ions used, v, v_s, alce, and sali for any salinity can be calculated by multiplying by the salinity in o/oo. Values for S for any salinity can be calculated by multiplying the table value by the square root of the salinity in o/oo.

Figures 6.7 through 6.12 show curves of the different quantitative functions versus temperature with both cumulative and incremental values plotted on the same graph. All cumulative curves, except brine volume, show that the incremental rate decreases with the lower temperatures. The incremental values have a minor aberration at -12° because the incremental value used for -10° is for the range from -8.2° to -10° rather than -2.0°C.

Relative Brine Volume

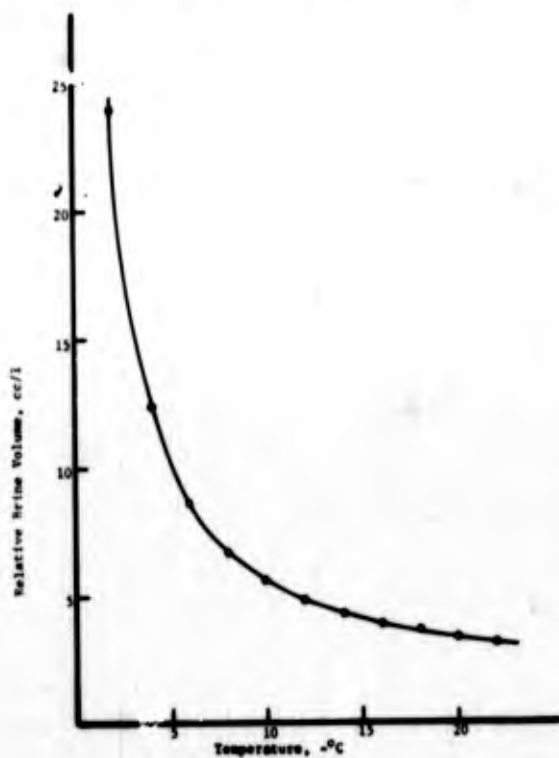


Figure 6.7

Ions Lost to Salts

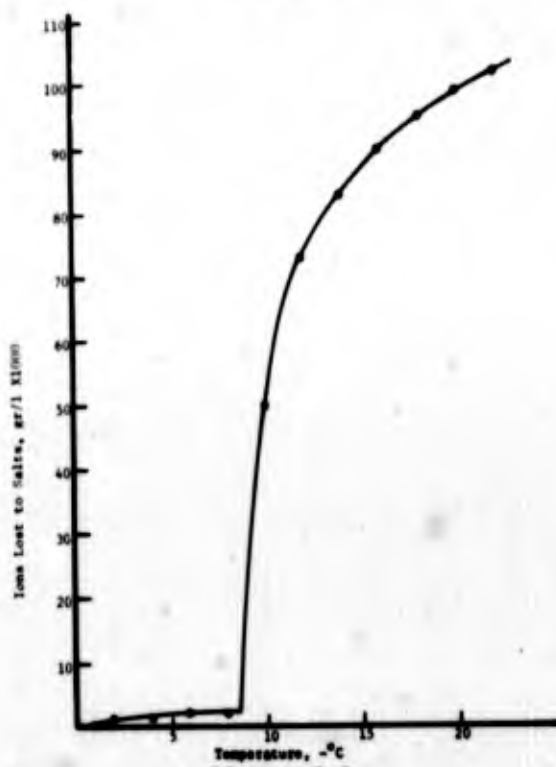


Figure 6.8

Salt Volume

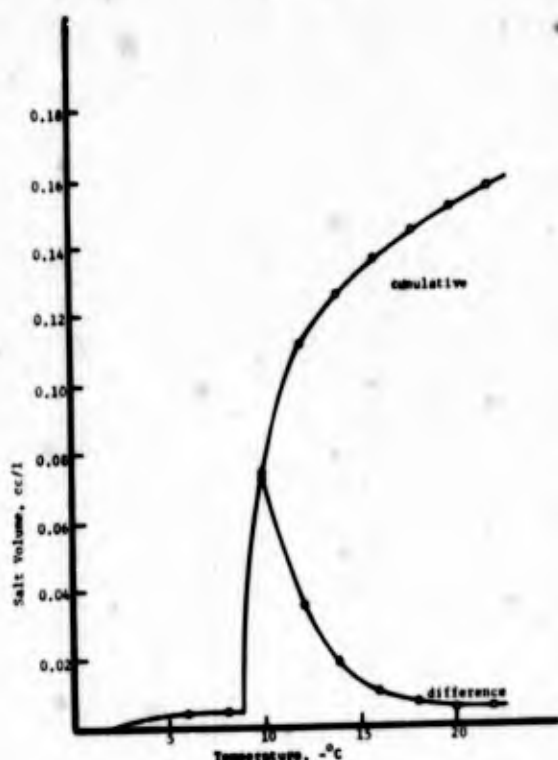


Figure 6.9

Associated Ice Volume

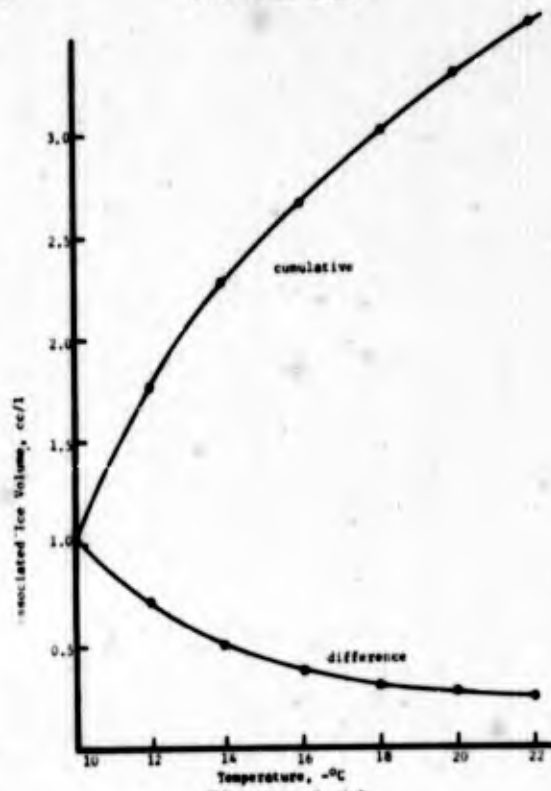


Figure 6.10

Salt area function of size center ice, σ_r , the salt reinforcement for the center ice being examined, can be determined by using the following relationship derived from equation 6.23:

$$\sigma_r = \sigma_a - \sigma_o (1-G \sqrt{v}) \quad 6.38$$

σ_r was calculated for each specimen with solid salts and was then plotted against S , the salt area function in the brine plane, in Figure 6.13. This figure shows:

1. σ_r increases with increasing S , and
2. This reinforcement, which must pass through the origin, is not linear with S .

Figure 6.13 shows the Strate of the center ice to be linear with $(1-v)^{1/2}$ if no solid salts are present. S is a similar area function, and the salt reinforcement should logically be linear with it. The lack of linearity indicates that there must be one or more additional salt functions affecting salt reinforcement. The factors which may be involved are:

1. Change in shape of the brine channels.
2. Change in the proportion of salts in the salt (quality changes).
3. Change in failure mode or location.

6.2.5 Effect of Brine Channel Shape on Salt Reinforcement. It has been reported (5) that as the brine channels become colder and smaller they tend to become rounder. If the brine channel shape changes, the true equation for σ_r is

$$\sigma_r = \sigma_o G_d [\sqrt{v_a \epsilon_1} - \sqrt{v \epsilon}] \quad 6.40$$

where G_d is the geometric factor, G , but excluding the shape factor, ϵ .

Figure 6.13 shows that the change in shape between -1° and -5°C cannot be extreme or the linearity between strate and $(1-v)^{1/2}$ would be affected. Some change in shape can be accepted as negligible because changes in the square root of ϵ are small; thus Strate would not be significantly sensitive to changes in shape.

If the brine channels do change from ellipses to circles, the change would probably be fairly uniform with decreasing brine volume. Table 6.3 shows the relative brine volume of 8 o/oo ice at various temperatures.

Table 6.3

Relative Brine Volume of 8 o/oo Ice at Various Temperatures.

Temperature, °C	v
-1.	.402
-2.	.192
-5.	.082
-8.2	.052
-10.	.044
-15.	.033
-21.	.026

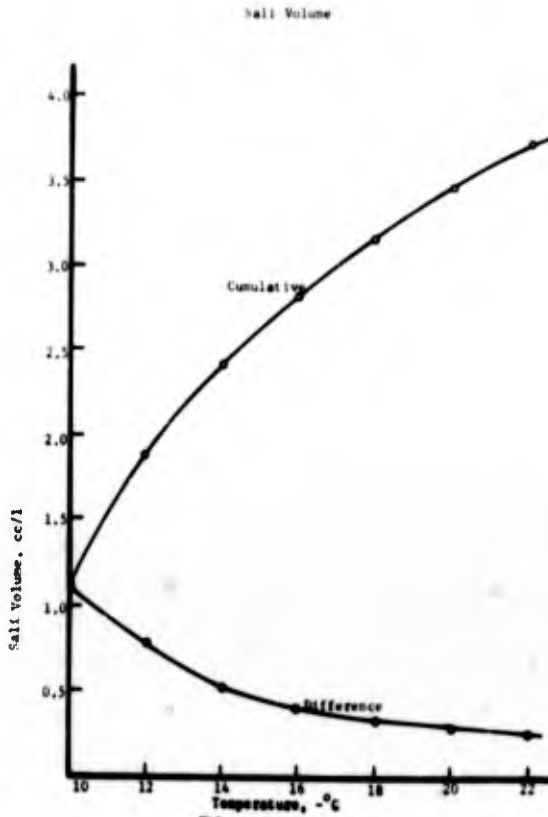


Figure 6.11

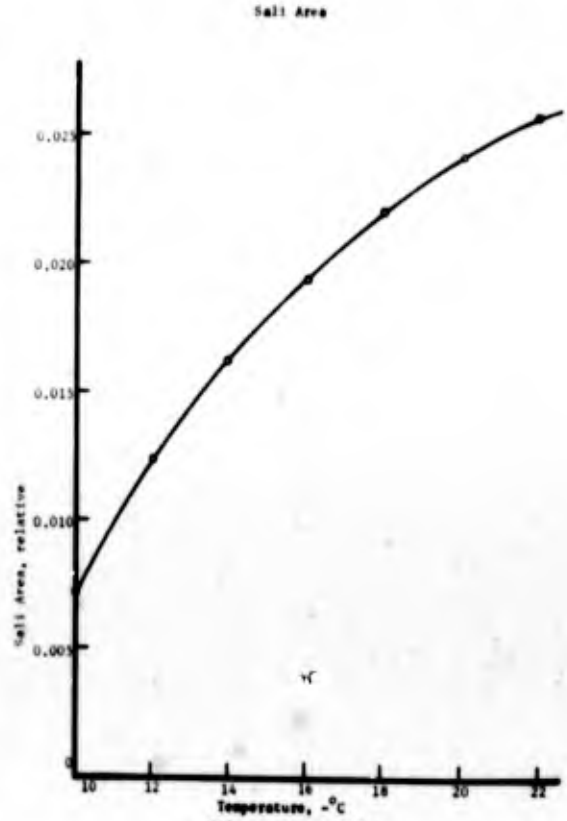


Figure 6.12

Amount of Solid Salt Reinforcement

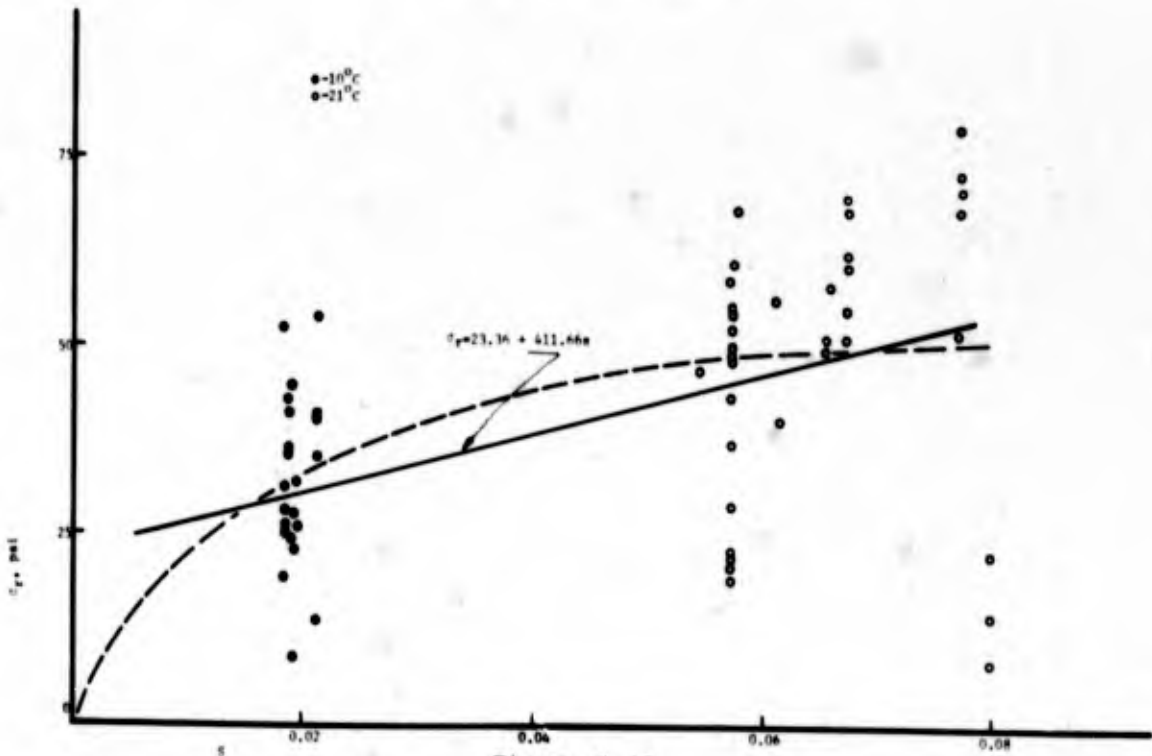


Figure 6.13

Most of the brine volume change occurs at warm temperatures, and the change between -10° and -21° is so small that any gross change in brine channel shape between the two temperatures is highly improbable. The brine channels probably do change shape as the brine volume becomes small but this alone cannot explain the curvilinear relationship between σ_r and S .

6.2.6 Qualitative Aspects of Sali. The two qualitative aspects of sali are:

1. The salt or salts contained in the sali, and
2. The quality or relative amounts of salt at any radius within an annular ring of sali.

The salts precipitated in sea ice were identified by the freezing of sea water in a closed system with subsequent examination the salts which precipitated in the bottom of the container (4). It has not been conclusively decided that the same salts precipitate inside the brine channels nor that they are incorporated in the sali.

The quality or amount of salts in the sali can be measured in several ways:

1. Weight of salts/weight of sali.
2. Volume of salts/volume of sali.
3. Moles of ions lost from the brine/moles of water lost from the brine.

The volume ratio appears best because the model employs volumes, and salt reinforcement is apparently a physical phenomenon which depends on volumes. This approach allows analysis of effective strengths over effective cross sectional areas of the failure plane. Specific weights for the salts have been used in these phase studies with the assumptions that any thermal volume changes are small and that any error in specific weight is constant.

Table 6.4 shows some of the qualitative aspects of sodium sulfate sali. Q , the quality function, is the ratio of salt volume to sali volume.

Table 6.4

Qualitative Aspects of Sodium Sulfate Deposits.

Temp	Cum. Q	ΔQ	Δ Salts/ H_2O (moles)	Sali/Brine (volumes)
-8°	.000	.000	.0000	0.000
-10	.068	.066	.0053	0.201
-12	.059	.046	.0042	0.391
-14	.052	.029	.0027	0.558
-16	.048	.025	.0022	0.715
-18	.045	.021	.0019	0.866
-20	.043	.021	.0021	1.024
-22	.042	.024	.0024	1.186

<u>Curve</u>	<u>S. E.</u>	
$Q = 0.034 + 2.707/T^{1.90}$.00043	6.40
$Q = 0.145 - 0.237 S^{.229}$.00075	6.41
$\Delta \text{ moles Salts}/\text{H}_2\text{O} = 0.00176 + 30.60/T^{3.86}$.00032	6.42
$\text{Salt}/\text{Brine} = -0.892 + 0.174 T^{.80}$.0074	6.43

Table 6.6 shows the ratio of moles of salts to H₂O to be very small; in the order of 0.2 to 0.5 per cent. Q, the ratio, salt volume/salt volume, is in the order of five per cent. Furthermore, Q begins at 0.084 (extrapolating equation 6.41 to a temperature of -8.2°C) when sodium sulfate precipitation begins and then continuously decrease with lowering temperature. The incremental values of Q show a minimum around -19° and a moderate increase at lower temperatures due to the precipitation of a small quantity of MgCl₂·8H₂O.

Equation 6.42, the relationship between Q and S, shows that quality drops continuously with increasing S for constant salinity. This is important to consider in evaluating the sketched, non-linear curve in Figure 6.13.

Figure 6.14 indicates Q as a function of temperature, Figure 6.15 indicates the relationship between Q and S for 1 o/oo sea ice, and Figure 6.16 indicates the molecular ratio of salts to water. Table 6.4 and Figure 6.17 indicate the ratio of salt volume to brine volume.

The salt quality factor meets the requirement of a parameter necessary to explain the curvilinear relationship between σ_r and S in Figure 6.13. If the solid salt reinforces the salt, it is reasonable to expect some direct relationship between the amount of salt and the amount of reinforcement. The salt quality for sodium sulfate salt begins at 0.084 and drops fairly rapidly to a value of about 0.021. This loss in quality may explain the declining incremental salt reinforcement with decreasing temperature.

6.2.7 A Combined Salt Function. If salt reinforcement depends on both S (the salt geometric function) and Q (the salt quality function) a combined salt function must be used. The simplest form is found by expressing σ_s in terms of Q.

$$\sigma_s = KQ^e \quad 6.44$$

K is a constant, e is a fitting exponent, and Q is the cumulative quality function. The equation for salt reinforcement is

$$\sigma_r = GS\sigma_s = GSKQ^e. \quad 6.45$$

Since σ_r is determined from experimental data and G and S are either known

Salt Quality Function

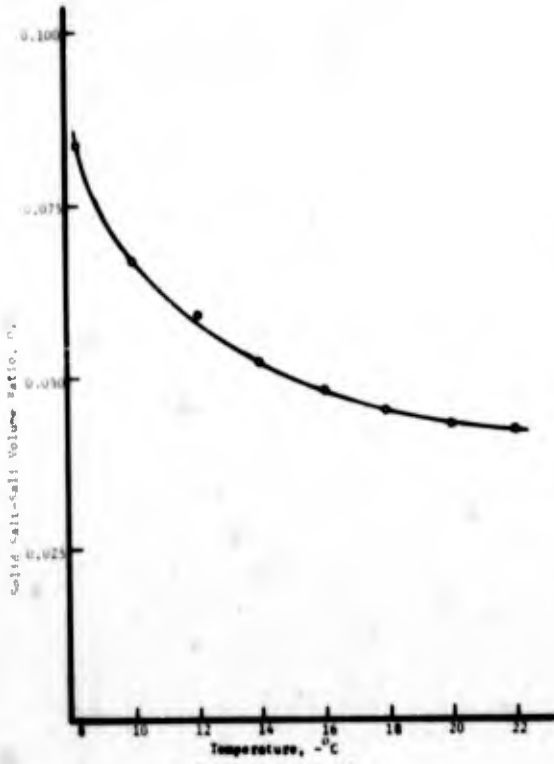


Figure 6.14

Solid Salt Volume, Ratios to Salt and Relative Solid Salt Volume

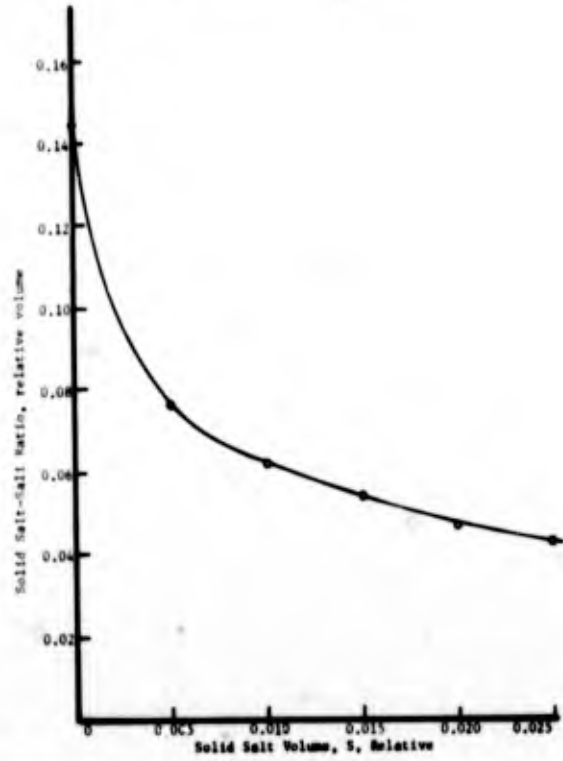


Figure 6.15

Salt-Water Ratio in Brine

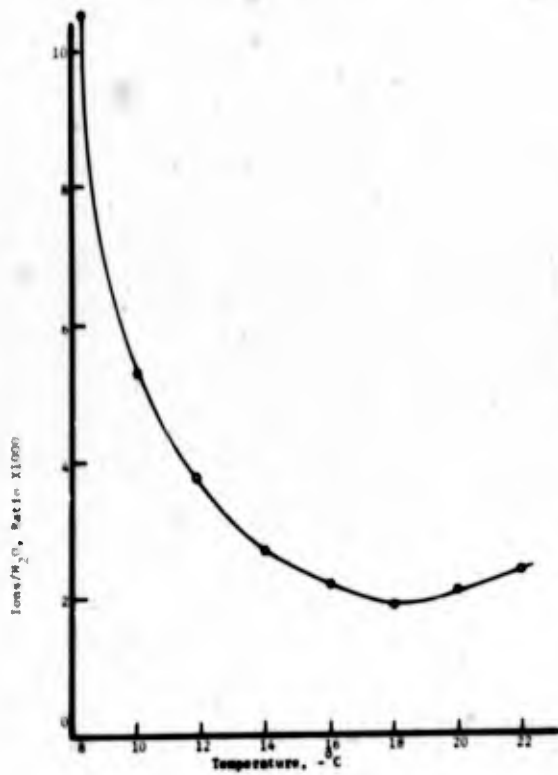


Figure 6.16

Salt-Brine Ratio

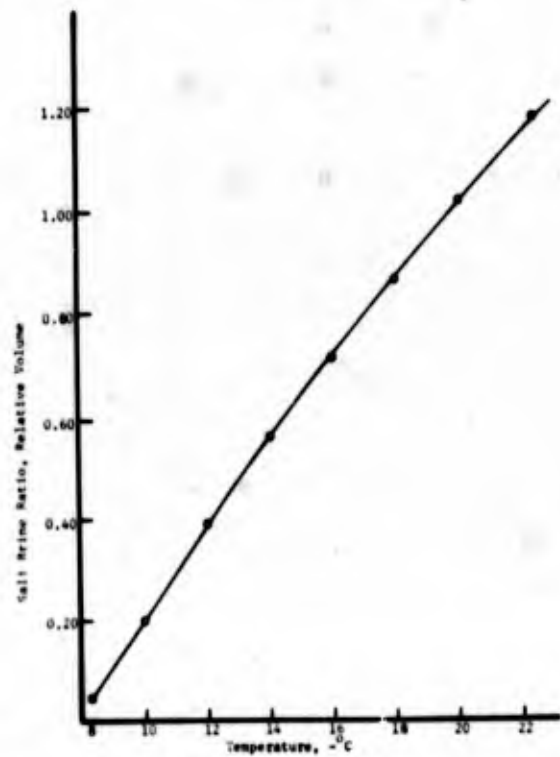


Figure 6.17

or can be calculated, the equation can be altered to

$$\frac{\sigma_r}{GS} = KQ^a \quad 6.46$$

For the data under study, Q and σ_r/GS were calculated for each experimental test. The mean values obtained for -10° and -21° were

Temp	Q	σ_r/GS
-	0.0	0.0
-10.	0.0680	1200.
-21.	0.0423	650

The equation fitted to these points is

$$\sigma_s = 39,400 Q^{1.3} \quad 6.47$$

The salt reinforcement function then becomes

$$\sigma_r = 39,400 GSQ^{1.3} \quad 6.48$$

and the overall fitting equation for the data being examined is

$$\sigma = \text{Rate}^r [156.68(1-1.22v^{1/2}) + 39,400 (1.22) S Q^{1.3}] \quad 6.49$$

Figure 6.18 shows calculated strength versus measured strength using equation 6.49. The least squares line has the equation

$$\sigma_c = 22.69 + .98 \sigma$$

with a standard deviation of 73.18 and correlation coefficient of 0.973. This fit is highly satisfactory although it might be possible to rework the constants and find a slightly better fit. Further refinement is not justified because the overall function is as precise as the data.

Equation 6.23 using the combined salt function for salt reinforcement is

$$\sigma = \text{Rate}^r [\sigma_0 (1-Gv^{1/2}) + KGSQ^{1.3}] \quad 6.50$$

The variables such as v , S and Q in this equation are combinations of the original independent variables measured for each test specimen. Assuming,

1. a_0 is a function of depth in a generalized growth rate expression.
2. b_0 is a constant controlled by ice formation parameters.
3. c is controlled by temperature,

the independent variables and their importances can be evaluated. Table 6.5 shows the independent variables and the elements in equation 6.51 to which they contribute. If the element appears twice in the equation, a double score is shown. An indication of the range of the variable is also given.

Plot of Calculated Strength versus Measured Strength

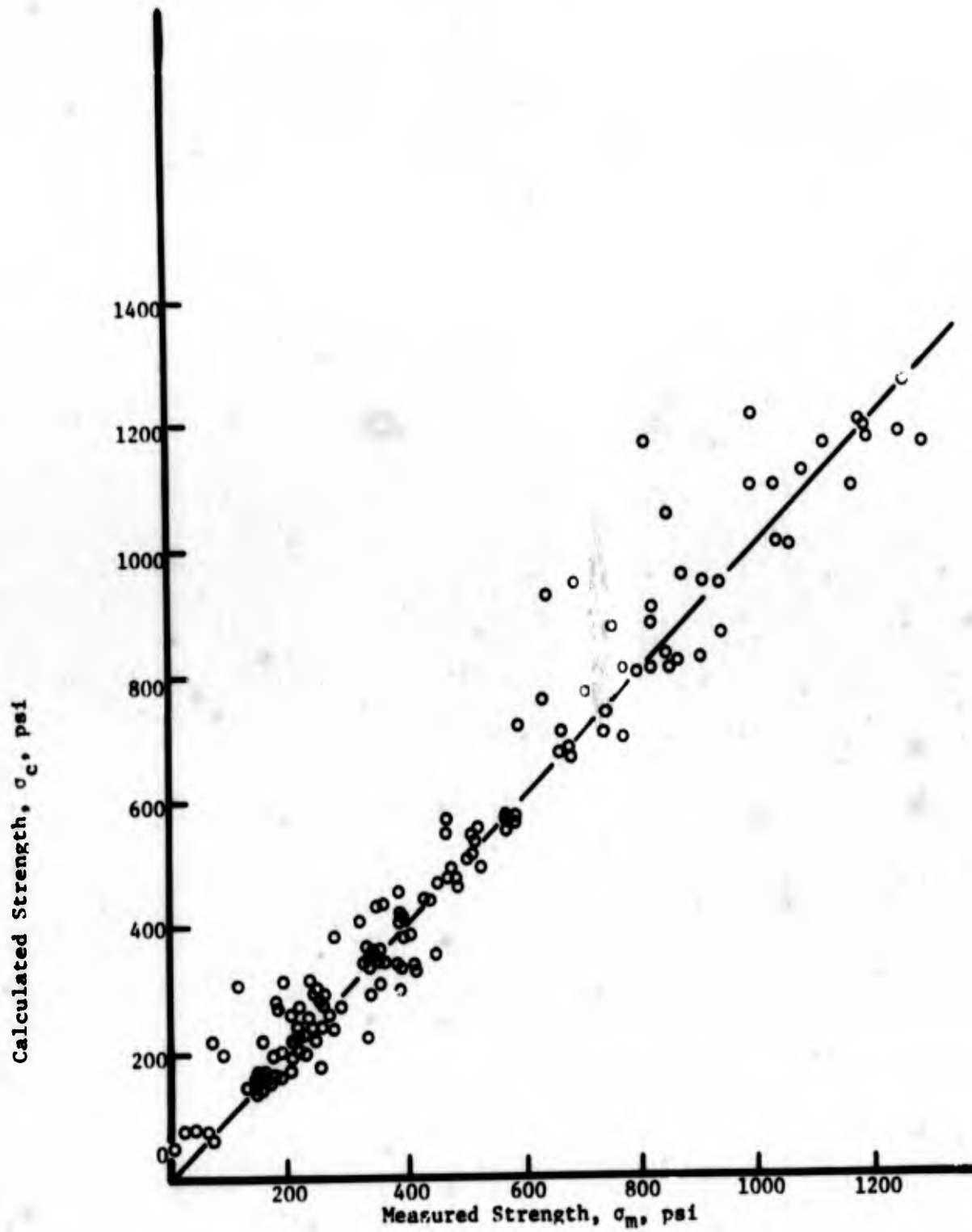


Figure 6.18

Table 6.5

Variables Used in the General Strength Equation.

	<u>Rate</u>	<u>G</u>	<u>v</u>	<u>S</u>	<u>Q</u>	<u>Total</u>	<u>Range</u>
Rate	x					1	Great
Depth	x	xx				3	Great
Temperature	x	xx	x	x	x	6	Medium
Salinity			x	x		2	Small

Temperature is seen to be involved in all elements in equation 6.51, depth in three, salinity in two and rate in one. The range in rate is the greatest and that of salinity the smallest. In order of descending importance, these variables rank in the order:

Rate
Temperature
Depth
Salinity

Some concept of the value for σ_s , the salt reinforcement effect for sodium sulfate, can be obtained from equation 6.48. Table 6.6 shows values of σ_s and the ratio σ_s/σ_0 for the ice under study. σ_s represents the bulk salt strength at the unique temperatures shown.

Table 6.6

Representative Values for Sodium Sulfate Reinforcement

<u>Temp °C</u>	<u>Q</u>	<u>σ_s</u> (psi)	<u>σ_s/σ_0</u>
-8.2	0.084 (max)	1575	10.
-12.0	0.059	980	6.2
-22.0	0.042(min)	640	4.1

The salt reinforcement in the center ice is extremely important as shown in Table 6.6 and Figure 6.3.

The combined function for salt reinforcement developed in this section is plausible and convenient. It was developed as one possible explanation of the data and is based entirely on parameters which have been developed by the application of phase information to the center ice under study. However, Figure 6.13 defines the curve of salt reinforcement only by data at two points other than the origin. The continuous curve which has been assumed has not been proved, and the combined function for salt reinforcement presented here is only a suggested function which fits the data very well and which is based upon a reasonable physical model.

6.3 FAILURE TYPES

The failure type was recorded during testing as a piece of available information which may later be of value. Exhibit 6.1 lists the failure type for each test and Exhibit 6.2 explains their coding. Some simplifications were made in the classifications for this analysis:

1. "Bulge" failure was considered to be plastic failure, and
2. "Tensile" and "shear" failures were lumped together because those failures initially classified as "tensile" failure were later found to actually be shear failures.

Figure 6.19 indicates that failure type is apparently controlled by loading rate and temperature with a change in pattern when solid salt begins to deposit. The solid salts have two effects:

1. The plastic failure type ceases, and
2. The upper limit of the failures without visible deformation abruptly jumps to a higher load rate.

Loading rate, temperature, and solid salts seem to govern the failure pattern. These parameters also govern strength.

6.4 REEVALUATION OF PUBLISHED DATA

6.4.1 Assur's Ring Tensile Data. Assur (7) used 327 ring tensile tests from various sources in an effort to define the tensile strength of sea ice. The tests are grouped into narrow ranges of salinity and further subdivided into narrow ranges of brine volume. Strength values were adjusted to a common temperature of -10°C to remove any temperature effect. Group averages with about nine tests per group were used for strength and brine volume data points. He found that strength at constant temperature was linear with the square root of salinity and therefore with the square root of brine volume. Precipitation of solid salts at low temperatures affected tensile strength and Assur interpreted the data as indicating a relatively thin layer of sodium sulfate which abruptly increased strength by one-third with no further reinforcement effect. Solid sodium chloride also produced a rapid increase in strength.

Assur's work is extremely important because he was the first to report the influence of solid salts on the strength of ice. His work has been the basis for further study of solid salts and their effects.

Weeks (9) studied salt ice (NaCl ice) and found that tensile strength was linear with $v^{1/2}$ and continuous. He re-evaluated Assur's data and, considering only the ice without solid sodium chloride, showed the plot of strength is linear with $v^{1/2}$. He fitted two lines to the data, one to the data without solid salts and the other to that data plus that with solid sodium sulfate. He was unable to determine the correct curve but concluded

that sodium sulfate probably did not reinforce the ice.

Assur's results have been reworked in this study because it is the only large group of sea ice tension data available with enough information to be treated in the same manner as the compression center ice data of the study. The information available for the individual groups is:

1. Number of tests in the group.
2. Average temperature.
3. Average salinity.
4. Average square root of brine volume.
5. Average strength.

Type, orientation, rate of loading and depth are not published.

The relationship between strength and $(1-v)^{1/2}$ for the without solid salts data is:

$$\text{Strength} = 19.73(1-2.37v^{1/2}) \text{ kg/cm}^2 \quad 6.51$$

σ_0 from equation 6.51 is 280.6 psi. Three groups with solid sodium sulfate fall below the least squares line for salt-free ice and were discarded. They were also discarded by Weeks. The brine volume effect was removed using equation 6.39 and the salt reinforcement was found for all ice with solid salts as shown in Figure 20. Figure 6.21 shows the relationship between σ_r and S , the salt area function, for the remaining sodium sulfate ice. The equation for the least squares fit is

$$\sigma_v = 0.31 + 35.97 S \text{ kg/cm}^2 \quad 6.52$$

The sodium sulfate reinforcement is less than that found for the center ice in compression, but it is still almost twice the basic ice strength. Figure 6.22 shows the effect of both the retained sodium sulfate ice and the sodium chloride ice, and the sodium chloride reinforcement is obviously large.

This analysis of Assur's data shows that the functions developed for analysis of compression data for center ice can be used to demonstrate both sodium sulfate and sodium chloride reinforcement in the tensile strength of sea ice. Assur's data do not contradict the findings of analysis herein of compression data, but rather they show an excellent and only available, picture of possible sodium chloride reinforcement.

6.4.2 Graystone and Langleben. Graystone and Langleben (11) also report ring tensile data which appear to show sodium sulfate reinforcement. The information published is not adequate to be reworked in the manner that Assur's results were reworked, but the inference of salt reinforcement exists.

6.5 CONCLUSIONS

The main conclusions reached in this study of salt deposits are the following:

1. Center ice behaves in a consistent manner making it suitable for analysis.
2. The strength of the center ice in compression is linear with $(1-v)^{1/2}$ but the slope of the curve changes abruptly with the initial precipitation of sodium sulfate.
3. Precipitation of solid sodium sulfate may result in strong reinforcement.
4. Sodium sulfate is precipitated in association with the formation of a large amount of new ice. This combination of solid salt and associated ice (called salt) is four to ten times as strong as salt-free ice. The reinforcement can be tentatively explained in terms of the area of salt in the failure plane and the relative volume of solid salts in the salt.
5. The mechanism by which solid salts may reinforce ice is not known. Two possibilities are that the salt crystals destroy the alignment of planes of weakness or that they inhibit crack propagation.
6. Little is known about solid salts in sea ice. This subject requires more study.
7. The primary parameters affecting the strength of sea ice in compression are:
 - A. Ice type and orientation
 - B. Rate of loading
 - C. Brine volume
 - D. Salt volume and quality
 - E. Plate thickness
 - F. Brine channel shape.Some of these parameters can be expressed in simpler variables such as temperature and salinity.
8. The strength function of sea ice is probably continuous. Discontinuities are not evident in the data.
9. An examination of the published data of others suggests sodium sulfate reinforcement and sodium chloride reinforcement is also apparent in Assur's results.

Pattern of Failure Types
Center Ice, Compression

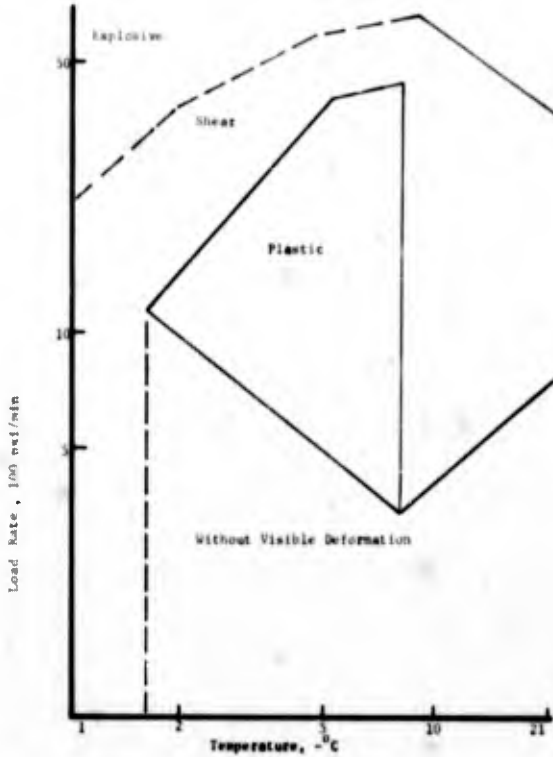


Figure 6.19

Sodium Sulfate and Sodium Chloride Salt Reinforcement
Pine Tensile Tests After Ansur

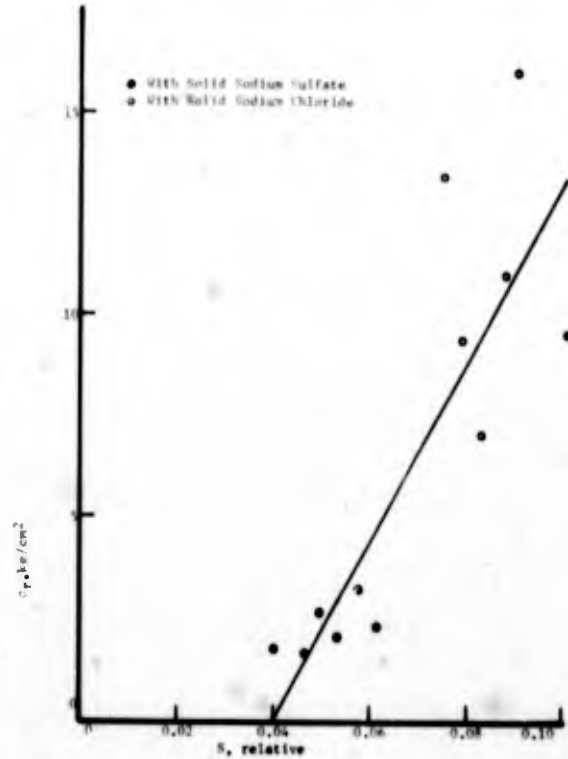


Figure 6.20

Sodium Sulfate Salt Reinforcement
Ring Tensile Tests After Ansur

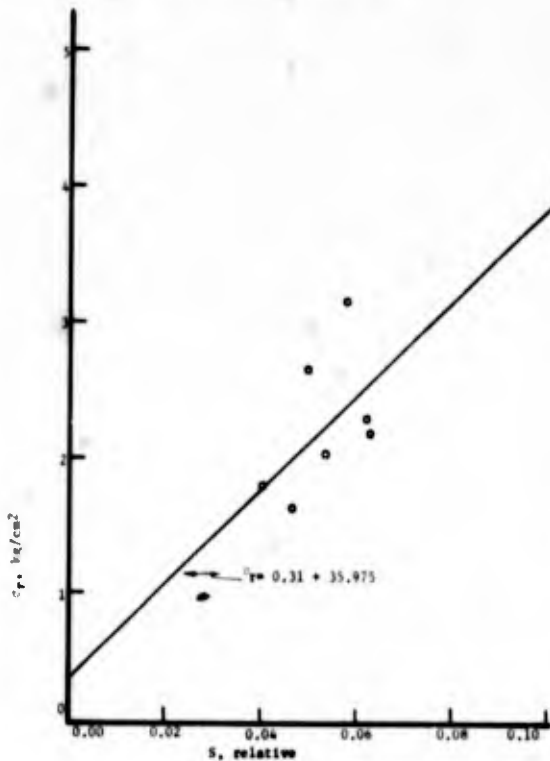


Figure 6.21

Evidence of Brine Reinforcement,
Ring Tensile Test After Ansur

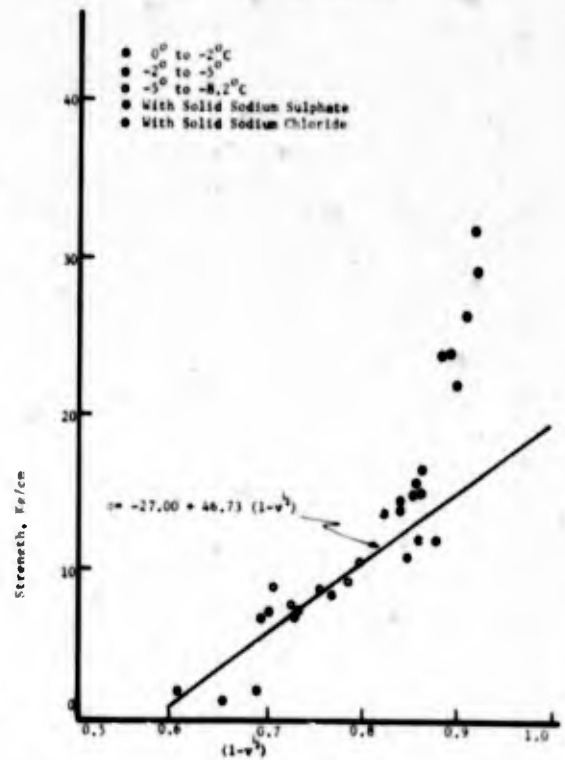


Figure 6.22

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Chapter 7

GENERAL FUNCTION FOR COMPRESSIVE STRENGTH OF
CENTER ICE AT ALL DEPTHS

7.1 INTRODUCTION

A general function for the compressive strength of center ice of varying depth is of the form

$$\text{Strength} = f(\text{rate}) [f(\text{brine volume} + \text{salt reinforcement})]$$

and fits the data available with a correlation coefficient greater than 0.93. The strength of this ice of a single type and orientation can be expressed in terms of four primary variables; rate, temperature, depth and salinity.

The rate function was obtained in Chapter 5, and its value increases with rate, depth, and negative temperature.

The brine volume-strength function is controlled by depth, geometry of the brine channels, and brine volume. If the ice is very warm, strength is controlled by brine volume. When the ice is colder, strength is controlled by both brine volume and depth. The equations which have been developed do not explain the effect of depth on the brine volume function. Several questions have been raised which cannot be answered by the center ice data because of the limited range of depth within which the center ice petrofabric was found to occur.

Center ice shows salt reinforcement from solid sodium sulfate decahydrate at all depths, and the salt reinforcement is proportional to the amount of salty ice in the failure plane and the quality of the salty ice. For some unknown reason, the salt reinforcement decreases with depth, but the reinforcement is a significant portion of the strength of colder ice. The strength of the salty ice fraction is several times the strength of ice without salt.

It is possible to use the functions developed in this chapter to integrate the compressive strength of sheets of center ice if the ice is warmer than -22.9°C , the mode of failure is the same as for the test specimens, and the thickness, rate of loading, salinity and thermal regime are known. The strength of a 40-inch thick sheet varies from 6.2 to 37.9 kips per horizontal inch of sheet depending on loading rate and thermal regime. The average horizontal compression strength through the 40-inch thickness is 155 to 950 psi.

7.2 CENTER ICE DATA, COMPRESSION

The center ice compression data is the largest single group which was obtained. This ice has proved to be the best group of data for initial analysis because of the high quality of data, quite uniform ice behavior, and because the bottom ice can be considered a special case of center ice with the crystal axes aligned. Results of analysis on center ice have been shown to be good

In Chapter 6, in which the strength of center ice at a depth of 1" was described.

Table 7.1 is an inventory of the numbers of tests by depth and temperature of all center ice tests. There were 598 tests remaining after 13 tests at 4 inches and -10°C were discarded because they were abnormally weak.

Table 7.1
Inventory of Center Compression Tests

Temp, $^{\circ}\text{C}$	DEPTH, INCHES								Total
	1	4	7	11	17	18-21	25-29	32-36	
1	6	10	7	4				7	34
2	50	73	4		24			6	157
5	25	16	4	14	22				81
6								5	5
10	32	48	34	17	27	11	11		180
14, 14.3						18	6		24
<u>20, 21</u>	<u>42</u>	<u>62</u>	<u>3</u>	<u>—</u>	<u>23</u>	<u>—</u>	<u>—</u>	<u>—</u>	<u>130</u>
Total	155	209	52	35	96	29	17	18	611

7.3 A GENERAL STRENGTH FUNCTION FOR 1 INCH CENTER ICE

An overall equation for compressive strength was developed for one inch center ice as follows:

$$\text{Strength} = f(\text{rate})[f(\text{brine volume} + \text{salt reinforcement})] \quad 7.1$$

$$\text{Strate} = \frac{\text{Strength}}{f(\text{rate})} = f(\text{brine volume} + \text{salt reinforcement}) \quad 7.2$$

$$\text{where,} \quad f(\text{rate})_{\text{cent. ice}} = \text{Rate}^{(.166 \text{ Depth} \cdot 1.38 \text{ Temp} \cdot 0.09)} \quad 7.3$$

$$f(\text{brine volume}) = \sigma_0 (1 - G v^{1/2}) \quad 7.4$$

$$\text{Salt reinforcement} = G S K Q^e \quad 7.5$$

where

σ_0 = the basic strength of the ice

G = a geometric factor

v = relative brine volume

S = relative area of salty ice in the brine plane

K = a fitting constant

Q = quality of salty ice = ratio of solid salts/salty ice

σ = strength

σ_a = strate
 σ_r = salt reinforcement
 σ_s = reinforcement value of the salty ice (unit reinforcement)
 σ_m = measured strength
 σ_c = calculated strength
 Fra = function of rate
 Fbv = function of brine volume
 e = a fitting exponent

The general equation of interest in this analysis is

$$\text{Strate} = \sigma_o (1 - G v^{1/2}) + G S K Q^e$$

Q, S and v have been calculated directly from Assur's phase information. In the study of 1" ice, values were obtained for σ_o and G while studying the brine volume function, and values were obtained for K and e while studying salt reinforcement. The objective of this chapter, assuming this general equation to be suitable, is to find more general values of σ_o , G, K and e as functions of depth.

7.4 THE BRINE FUNCTION, LIQUID AND SOLID

7.4.1 General. In Chapter 6, a linear relationship was observed between the strate of center ice and $(1-v^{1/2})$ in the warmer ice before solid salt precipitation. All 1", 4" and 7" depth specimens have tests at -1, -2, and -5°C, and these three temperatures are adequate to show linearity. The deeper depth test groups do not have three temperatures in the non-solid salt temperature range, and linearity cannot be proved for these depths but is assumed to be true because of the behavior of tests from 1", 4" and 7" depths.

Average values of strate and $(1-v^{1/2})$ were calculated for each single-temperature, single-depth group of tests. Table 7.2 is a listing of these values and Figure 7.1 shows the values with only the main depths and temperatures being considered.

Table 7.2
Average Strate and $(1-v^{1/2})$
 $(1-v^{1/2})/\text{Strate}$

Temp	Depth				
	1"	4"	7"	11"	17"
-1°	.3792/28.4	.4167/32.1	.4338/40.4	.5049/39.8	
-2°	.5933/79.2	.6363/58.7	.5436/43.5		.6664/49.4
-5°	.7321/106.0	.7527/72.5	.7843/49.8	.7772/39.2	.7848/48.9
-10°	.7962/150.2	.8203/85.7	.8347/86.6	.8081/90.9	.8481/52.2
-21°	.8580/178.9	.8713/110.3	.8791/85.7		.8778/74.0

These test groups retain all variability not explained by the general rate function and include any errors; sampling, experimental or analytical. With this in mind, the broad picture outlined in Figure 6.1 exhibits the following qualities in a general sense.

1. For constant depth, the slope of the line decreases as the depth increases.
2. The constant depth curves all appear to originate in the same general region where strate is between 30 and 40 and $(1-v^{1/2})$ is between .35 and .50
3. Salt reinforcement is apparent for all depths.
4. The function, $(1-v^{1/2})$, increases with increasing depth for the same temperature, thus salinity decreases with depth.
5. There is no indication that the relationship between strate and $(1-v^{1/2})$ is not linear in the temperature range without solid salts.
6. The slope of the lines of constant temperature vary. The line for -1° ice is positive and shows strate increasing with increasing depth and increasing $(1-v^{1/2})$. At colder temperatures, the slopes become strongly negative, thus suggesting that brine volume controls strate in warm ice but that depth controls at colder temperatures.

Figure 7.2 shows strate versus depth for the -2° , -5° , -10° and -21° ice. The -2° and -5° lines show a curvilinear relationship between strate and depth with the 17 inch ice apparently being abnormally strong. The -10° line shows a strate-depth relationship apparently to exist but it is not simple and smooth, and the 17 inch ice appears to be abnormally weak and does not show salt reinforcement at -10° as it does at other depths. The -21° line is smooth with the 17" ice again showing less brine reinforcement than might be expected.

A set of fitting functions can be determined for the non-solid salt (salt free) ice temperature range. Some idealization will be required because of anomalous data, but the final results will show this to be reasonable.

Anchor points; brine volume versus depth, -1°C : Figure 7.3 shows average strate versus average $(1-v^{1/2})$ for the ice without salt reinforcement. These values indicate that it is possible to describe the family of lines by first defining an anchor point at a temperature of -1° in terms of brine volume and strate at -1° and then describing the slope of the line in terms of depth.

The first need is to determine a salinity function in terms of depth. Table 7.3 shows the average salinities for the data at each depth for the center ice.

Salt Effects with Depth
Center Ice, Compression

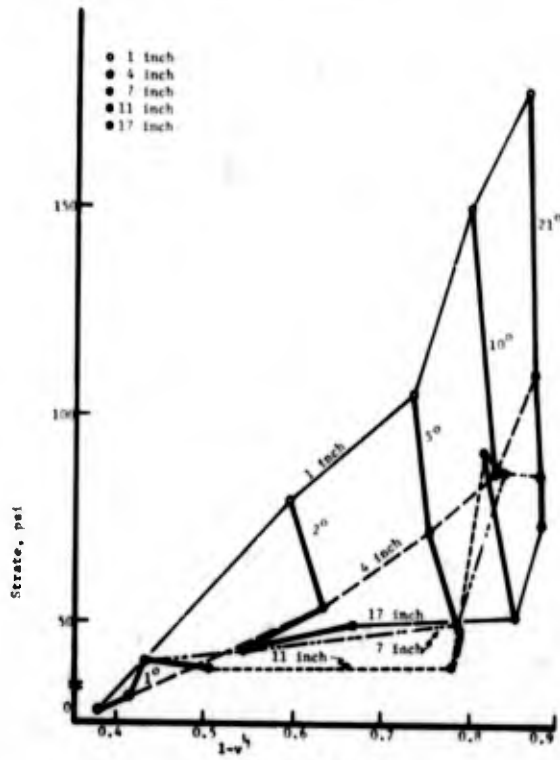


Figure 7.1

Strate at Depth, -10° and -21°
Center Ice

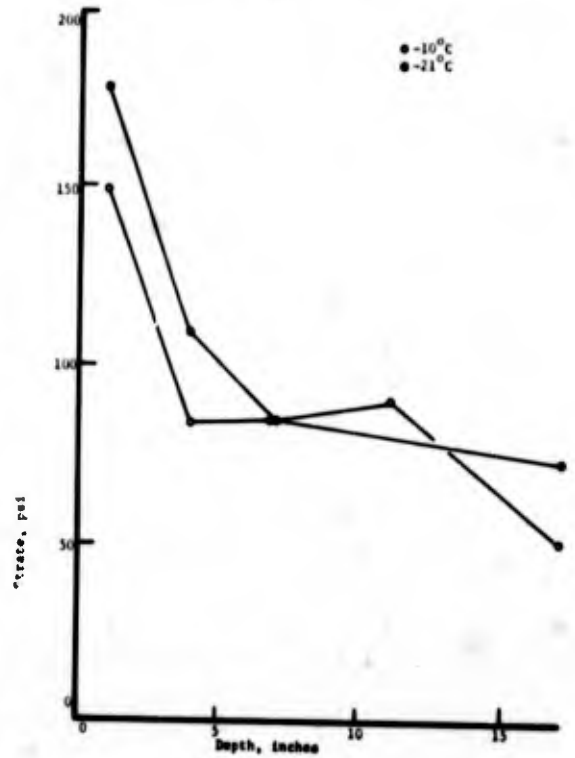


Figure 7.2A

Strate at Depth, -5°
Center Ice

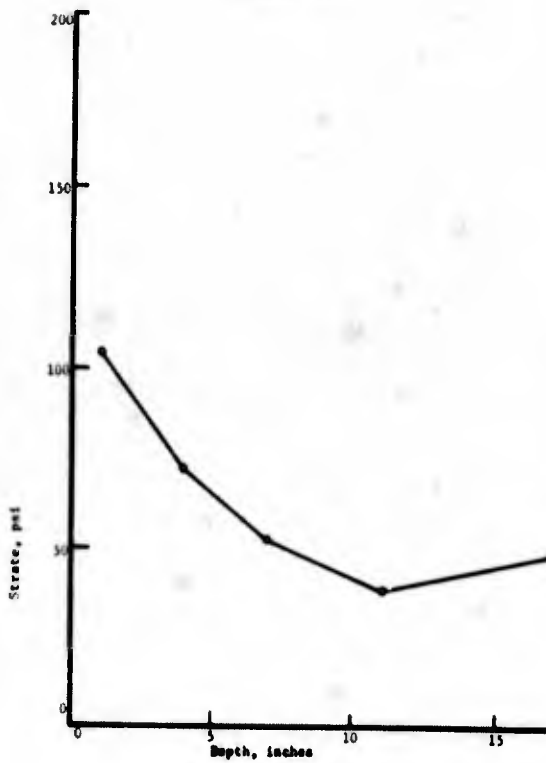


Figure 7.2B

Strate at Depth, -1° and -2° C
Center Ice

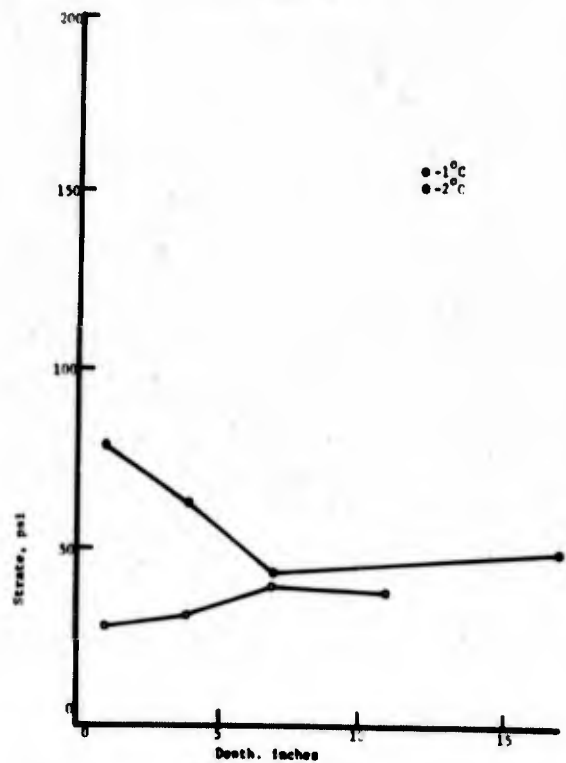


Figure 7.2C

Table 7.3

Average Salinity at Different Depths

Depth	Average Salinity o/oo
1"	7.25
4"	5.80
7"	5.40
11"	5.94
17"	4.59

The salinity, except for the 11" depth, fits a line:

$$\text{Salinity} = 7.25 - 0.95 \ln(\text{Depth}) \quad 7.6$$

Analysis in Chapter 6 indicated a brine-volume function for sea ice with a salinity of 1 o/oo.

$$\text{Brine Volume} = 1.03 + 45.80/T \quad 7.7$$

Brine volume can be found for any salinity by multiplying the results of equation 7.7 by the salinity in o/oo. Table 7.4 shows the values of brine volume and $(1-v)^{1/2}$ for various depths based on salinity from equation 7.6 for -1°C .

Table 7.4

Idealized Brine Volume and $(1-v)^{1/2}$, -1°C .

Depth	Brine Volume, v	$1-v^{1/2}$
1"	.339	.4173
2	.308	.4444
3	.290	.4608
4	.278	.4728
6	.260	.4902
9	.241	.5083
13	.226	.5252
19	.209	.5433
28	.191	.5626
42	.173	.5827

This depth - $(1-v)^{1/2}$ relationship can be fitted to the following equation:

$$(1-v)^{1/2}_{-1^\circ} = .177 + .243 \text{ Depth}^{.138} \quad 7.8$$

The equation of the least squares line for strate is

$$\text{strate}_{-1^\circ} = -1.75 + 84.9 (1-v)^{1/2}_{-1^\circ} \quad 7.9$$

Salt Effects With Depth,
Center Ice With Solid Salt

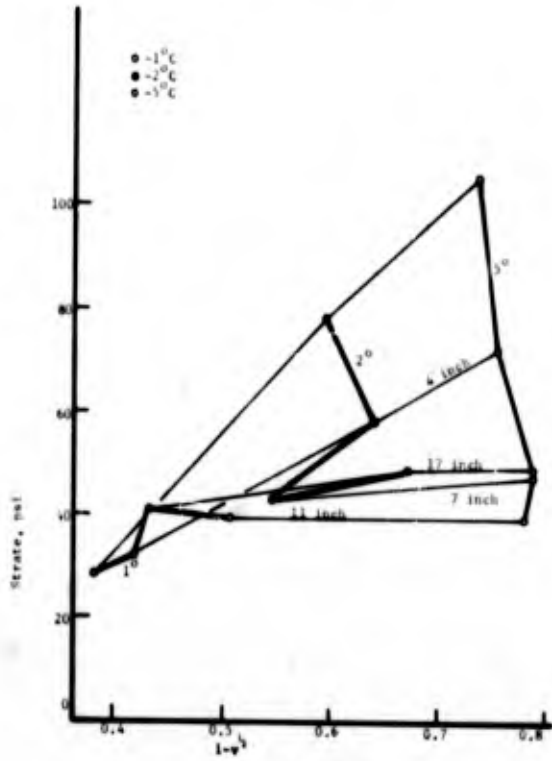


Figure 7.3

Values of Coefficient K at Various Depths

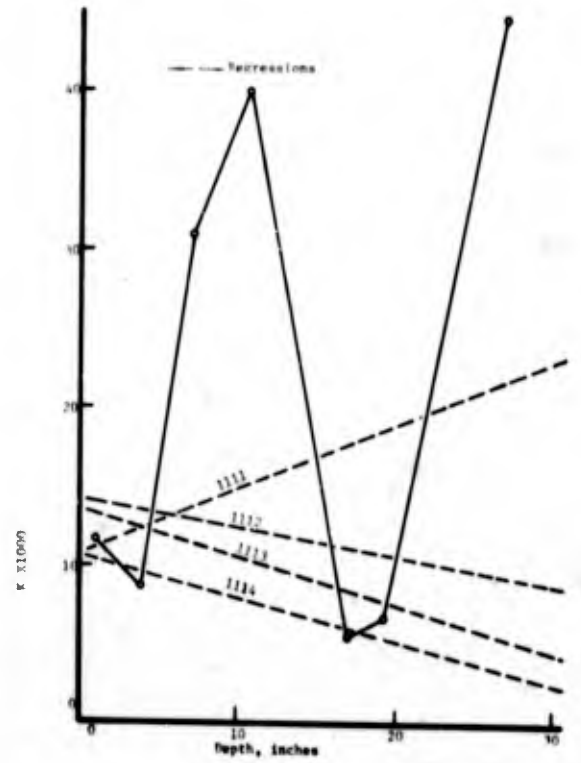


Figure 7.4

Salty Ice Quality at Various Depths

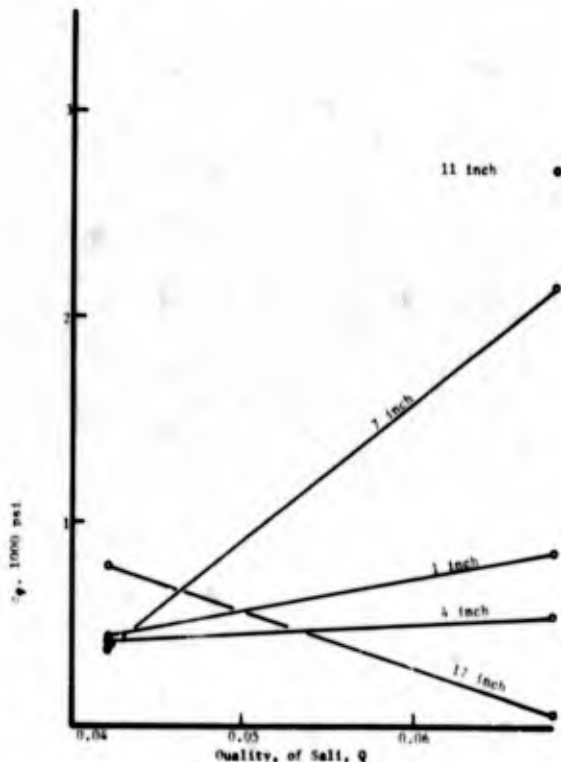


Figure 7.5

Slope of Brine Volume
Function Versus Depth

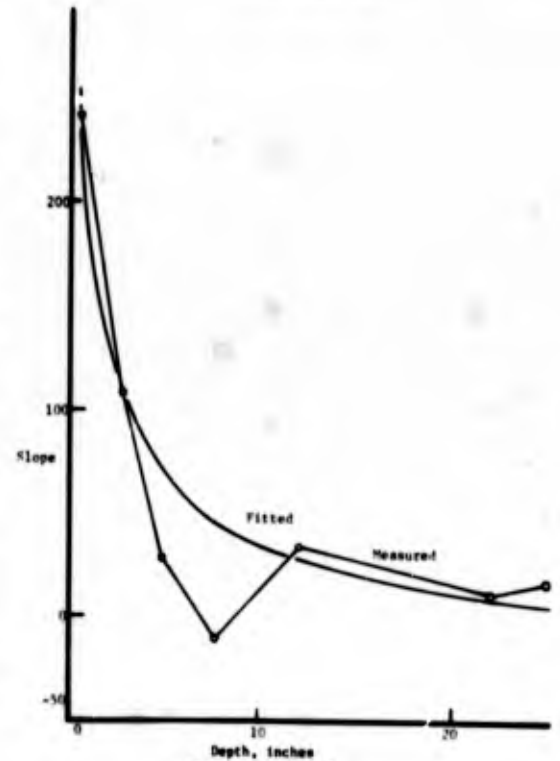


Figure 7.6

With a least squares line forced through the origin, the equation becomes

$$\text{Strate } -1_0 = 81 (1-v)^{1/2} \quad 7.10$$

Using equation 7.10, an anchor point for each constant temperature curve can be based on the -1° curve and defined in terms of depth.

$$X_0 = 0.177 + 0.243 \text{ Depth}^{0.138} \quad 7.11$$

$$Y_0 = 81 X_0 \quad 7.12$$

7.4.2 Slope of Brine Volume Function. A least squares line was fitted between the anchor point for a particular depth and the -2° and -5° data for that depth. The slope of this least squares line represents the brine volume function for that depth based on the anchor point. Table 7.5 shows the various depths, number of observations, anchor points, and slope of the least squares line through the anchor points.

Table 7.5

Anchor Points and Least Squares Slopes

Depth	Obs	X_0	Y_0	Slope
1"	81	.42	34.0	242.7
4	99	.47	38.0	124.3
7	15	.50	40.5	27.9
11	18	.52	42.1	-11.0
17	46	.54	43.7	27.5
32	8	.59	47.8	9.9
36	10	.60	48.6	14.9

Figure 7.6 shows slope versus depth. A regression, analysis weighted by number of observations, between slope and depth yielded equation 7.13.

$$\text{Slope} = -61. + 309.4/\text{Depth}^{.443} \quad 7.13$$

Table 7.6 shows the measured slopes, the calculated slopes, and the differences.

Table 7.6

Slope of Brine Volume Functions (units = 1/Inch)

Depth	Measured Slope	Fitted Slope	Difference
1"	242.7	248.3	-7.6
4	124.3	106.6	17.7
7	27.9	70.1	-42.2
11	-11.0	45.7	-56.7
17	27.5	27.4	.1
32	9.9	4.5	4.4
36	14.9	2.1	12.8

The 7 and 11 inch data have the poorest fit but both are for small numbers of data, the general fit seems good.

For any calculated strength, an equation can be written as follows:

$$Y - Y_0 = M (X - X_0), \quad 7.14$$

where M is the slope of the line and (X_0, Y_0) is the anchor point. This equation can also be written in the form:

$$Y = Y_0 - M X_0 + M X \quad 7.15$$

which is of the form:

$$Y = A + BX$$

where X is $(1-v)^{1/2}$
 $A = Y_0 - M X_0$

It was shown in Chapter 6 that

$$\sigma_a = \sigma_0 (1-Gv)^{1/2}$$

where $\sigma_0 = A + B$
 $G = B/(A+B)$

In the existing situation

$$\sigma_0 = A + M = Y_0 - M X_0 + M \quad 7.16$$

$$G = M/\sigma_0 \quad 7.17$$

$$\text{Brine volume function} = \sigma_0 (1-Gv)^{1/2} \quad 7.18$$

$$\text{where } X_0 = 0.177 + 0.243 \text{ Depth}^{0.138}$$

$$Y_0 = 81 X_0$$

$$M = -61 + 309.4/\text{Depth}^{0.443}$$

7.4.3 Salt Reinforcement. Chapter 5 showed the effect of salt reinforcement on 1" center Ice and the reinforcement is described by equation 7.19.

$$v_r = G S K Q^e, \quad 7.19$$

where

G is the geometric factor determined in the brine function study.

S is the salty ice (sali) area in the brine plane.

K is a fitting coefficient.

Q is the quality of salty ice (sali).

e is a fitting exponent.

Figure 7.1 shows solid salt reinforcement to be found in all center ice studies; therefore a general approach may be followed.

$$\sigma_r = \sigma_a - (\text{liquid brine volume function}) \quad 7.20$$

σ_r was calculated for each test with solid salts and average values of σ_r for each depth and temperature are shown in Table 7.7. S, the salt area function, is also shown in the table.

Table 7.7

Average Values of Salt Reinforcement and S: σ_r/S
Depth

Temp °C	1	4	7	11	17
-10	9.23/.0205	10.3/.0172	23.0/.0157	35.7/.0184	0.25/.0145
-21	36.1/.0638	27.8/.0578	18.8/.0543		21.3/.0548

Of the elements in equation 7.19, σ_r , G, S, and Q are either measured or defined models. The unknowns are K and e. A new strength function is defined and used to describe additional geometric and phase information.

$$\sigma_q = \frac{\sigma_r}{GS} = K Q^e \quad 7.21$$

The value of σ_q for each test was calculated, and the average values with the standard deviation for each depth and temperature are shown in Table 7.8 accompanied by the value of Q for that temperature.

Table 7.8

Average Values of σ_q and Standard Deviation; $\sigma_q/S.D.$
Depth

Temp °C	1"	4"	7"	11"	17"	Q
-10	848/410	524/583	2145/1842	2700/881	64/2382	.0680
-21	431/203	424/218	374/311		793/752	.0423

Figure 7.5 shows σ_q versus Q for the various depths. It is obvious that no precise salt reinforcement function is possible. The scatter inherent in the rate and brine volume functions have been carried into the salt reinforcement function. In the analysis of the center 1" ice, it was found that e, the exponent of Q, was about 1.3 for the best fit. In this analysis it appears that a value of e of 1.0 will be satisfactory. The remaining unknown is K, with equation 7.21 becoming

$$\sigma_q = K Q \quad 7.22$$

The best fitting value of K for each depth was determined by

$$K = \frac{\sum Q \sigma_q}{\sum Q^2}$$

Table 7.9

Values of K for Each Depth			
Depth	Number of Observations	K	Standard Deviation
1"	63	11,595	302
4"	97	8,547	390
7"	32	30,675	1777
11"	17	39,712	881
17"	50	5,352	1862
18-21"	29	6,475	682
25-29"	17	44,400	2345

Figure 7.4 shows K as a depth function with the number of observations for each depth shown. K exhibits great variation; however, the high values are all for small groups of observations and the larger groups tend to show a pattern. A series of weighted, linear regressions were made of the Depth-K values with the weighting factor being the number of observations.

Table 7.10

Relationships of K and Depth						
Regression No	Data used	Number of Observations	\bar{Y}	A	B	R
1111	All	305	14,513	10,926	401	.258
1112	Less 25-29	288	12,748	14,265	-193	-.128
1113	Less 25-29, 11	271	11,057	13,518	-321	-.288
1114	Less 25-29, 11, 7	239	8,430	10,624	-283	-.896

The only significant relationship between K and depth is found in Regression 1114 with a correlation coefficient of 0.9 for the equation

$$K = 10624 - 283(\text{Depth}) \quad 7.24$$

If the depth function in K proves to not be significant, an alternate would be to use a constant value of about 10,000. This completes the definition of equation 7.1 and the general strength function for center ice is now ready for testing and evaluation.

7.5 TESTING, ADJUSTING, AND EVALUATING THE COMPLETE STRENGTH FUNCTION

The general expression for the compressive strength of center ice is

$$\text{Strength} = \text{Rate}^r [\sigma_0 (1 - G v^{1/2}) + G S K Q] \quad 7.25$$

with the following values for the individual components of equation 7.25.

$$r = 0.166 \text{ Depth} \quad 0.138 \quad 0.09 \text{ Temp}$$

$$\sigma_o = Y_o - M X_o + M$$

$$Y_o = 81 X_o$$

$$X_o = 0.177 + 0.243 \text{ Depth}^{0.138}$$

$$M = -61 + 309.4/\text{Depth}^{.443}$$

$$G = m/\sigma_o$$

$$S = (SV+BV)^{1/2} - (BV)^{1/2} = Sa1^{1/2} (.082 - .180/T^{.381})$$

$$v = Sa1(1.03 + 45.8/T)$$

$$Sa1 = 7.25 - .95 \ln(\text{Depth})$$

$$K = 10600 - 280 \text{ Depth}$$

$$Q = .034 + 2.707/T^{1.90}$$

Strength was calculated for each individual test using equation 7.25. These values were compared with the measured value and two regressions were made, each on the calculated strength in terms of the measured strength. The first by a general least squares fit and the second with a least squares fit forced through the origin. These results are shown in Exhibit 7.1 and in Table 7.11.

Table 7.11

Comparative Statistical Information, $K = f(\text{Depth})$

Depth	- Least Squares Line - - -			Line Through Origin			
	Number of Observations	A	B	Stand. Dev.	R	Slope	Stand. Dev.
1"	155	.35	.98	91.7	.958	1.041	93.8
4	196	.10	1.00	69.1	.965	1.023	96.3
7	52	.75	.72	94.4	.861	.872	102.1
11	35	142	.52	91.6	.822	.787	120.7
17	96	84	.74	92.4	.892	.908	103.3
18-21	29	67	.79	58.8	.888	.952	63.8
25-29	17	51	.67	42.1	.910	.813	46.4
32-36	18	74	.61	22.5	.865	.976	33.3
All	598	.33	.92	92.4	.934	.984	94.2

The information shown in Table 7.11 indicates the general expression fits well. The equation was adjusted by changing K to a constant value of 10,000 and ignoring the depth effect.

Table 7.12

Plotback Statistical Information, $K = 10,000$

Depth	Number of Observations	- Least Squares Line - - -		Stand. Dev.	Line Through Origin		Stand. Dev.
		A	B		R	Slope	
1"	155	36	.98	91.0	.958	1.035	93.2
4"	196	7	1.02	70.1	.965	1.034	70.2
7"	52	73	.74	97.2	.861	.889	104.3
11"	35	137	.55	89.7	.841	.809	117.8
17"	96	76	.80	96.9	.897	.951	105.4
18-21"	29	65	.86	58.4	.905	1.022	63.1
25-29"	17	54	.70	40.9	.919	.842	45.8
32-36"	18	74	.61	22.5	.865	.976	33.3
All	598	33	.93	90.9	.937	.997	92.7

The slope of the single curve from the origin through all of the data is very close to 1.00. The correlation coefficient for this line is .934 which is satisfactory.

Exhibit 7.2 shows the value of the brine volume-strength function in tabular form for each degree from -1°C to -22°C , and for 7 depths. Exhibit 7.3 shows the value of $(1-v^{1/2})$ for the same temperatures and depth. Figure 7.7 shows the brine volume-strength function versus $(1-v^{1/2})$ for the different depths and is the model derived from the data shown in Figures 7.1 and 7.3.

The salt reinforcement for constant temperatures and depth groups is shown in Exhibit 7.4, and Figure 7.8 shows salt reinforcement as a function of depth for three temperatures and Figure 7.9 shows salt reinforcement versus temperature.

Strate, the sum of the brine volume strength function and the salt reinforcement, is shown for the same depths and temperatures in Exhibit 7.5, and Figure 7.10 shows strate versus temperature for constant depths. The brine volume strength function and the salt reinforcement are apparent in this figure, and the reduction of both components with increasing depth is also apparent.

7.6 INTEGRATED COMPRESSIVE STRENGTH OF AN ICE SHEET, CENTER ICE, HORIZONTAL LOADING.

The practical problem of a moving ice sheet impinging on an obstacle such as a piling is one of timely concern. It is known that the mode of failure in such a circumstance can be direct compression; therefore, the net strength through the sheet thickness can be integrated from the information developed for center ice. A natural ice sheet normally exists with a roughly linear temperature gradient; about -2°C throughout during summer melt and with upper surface temperature about -20°C during cold winter periods.

All the parameters of strength thus far studied, load rate, salinity, brine volume and brine reinforcement, vary both with temperature and depth. The limitations of integrating the sheet strength with the information thus far developed are as follows.

1. The entire sheet need be composed of center ice,
2. The ice may not be colder than -22.9°C which is the initial precipitation temperature of sodium chloride dihydrate, and has not been studied,
3. The mode of failure must be the same as for the specimens tested, and
4. The accuracy of the model.

With these limitations in mind, three example integrations are performed for an ice sheet 40 inches thick as follows:

1. The temperature is held constant at -2°C thus reflecting a summer condition. (Warm regime)
2. A linear temperature gradient is established with -22°C at the upper surface and -2°C at the lower surface thus reflecting a cold period. (Medium regime)
3. A linear temperature gradient is established with -22°C at the upper surface and -12°C at the lower surface simulating the center ice upper layer of an 80 inch thick ice sheet during a cold winter period. (Cold regime)
4. Load rates of 100, 300, 1000, and 5000 psi/min are used with each temperature profile yielding 12 integrations.
5. The integration is performed by finite summation of one inch increments.

Exhibit 7.6 shows the temperatures for the three thermal regimes at the top of each increment, Exhibit 7.7 shows the values of rate exponent for each inch for each thermal regime, Exhibits 7.8, 7.9 and 7.10 show the rate functions, (Rate) r , for the warm, medium, and cold thermal regimes at the four different loading rates. The rate function increases with increasing temperature, increasing depth, and increasing rate, and it ranges in value from about 2 to about 19. This is a multiplying function and shows the rate function to be highly important.

Exhibit 7.11 indicates the general brine volume functions, X_0 , Y_0 , B (or M), σ_0 , G , and salinity at various depths, and Exhibit 7.12 shows the brine volume-strength functions (in psi) for the three thermal regimes at each inch of depth. The latter is sensitive to both depth and temperature near the surface but approaches a constant value which is independent of depth or temperature at deeper depths.

The salt reinforcement values are shown in Exhibit 7.13 for the three thermal regimes. The difference in reinforcement between the medium and cold ice is small, thus indicating the results of the solid salt quality function.

Exhibit 7.14 shows strate, the brine volume strength function, and the salt reinforcement values. Strate decreases rapidly with depth in the upper levels because both the brine volume strength function and the salt reinforcement exhibit this characteristic. For the ice under study, strate varies from about 45 to 240 depending on depth and temperature. In Exhibits

Brine Volume Function at Various Depths
Liquid Brine Only

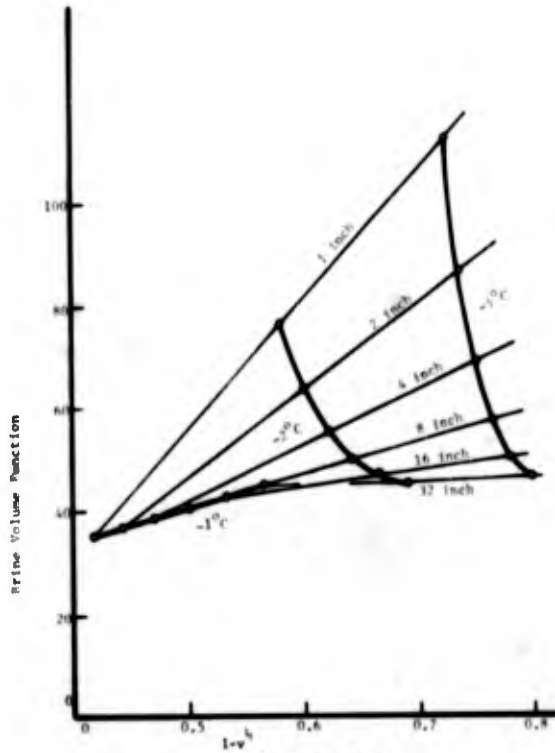


Figure 7.7

Idealized Function for Strate

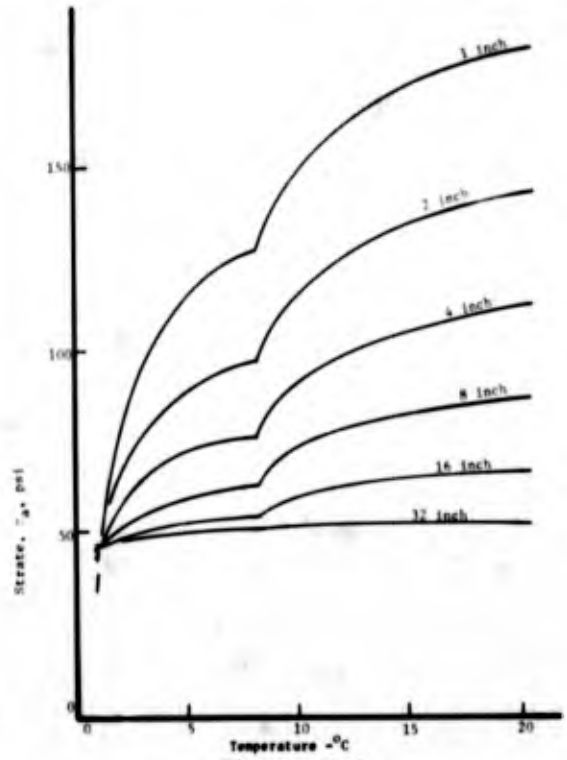


Figure 7.8

Idealized Solid Salt Reinforcement at Various Temperatures

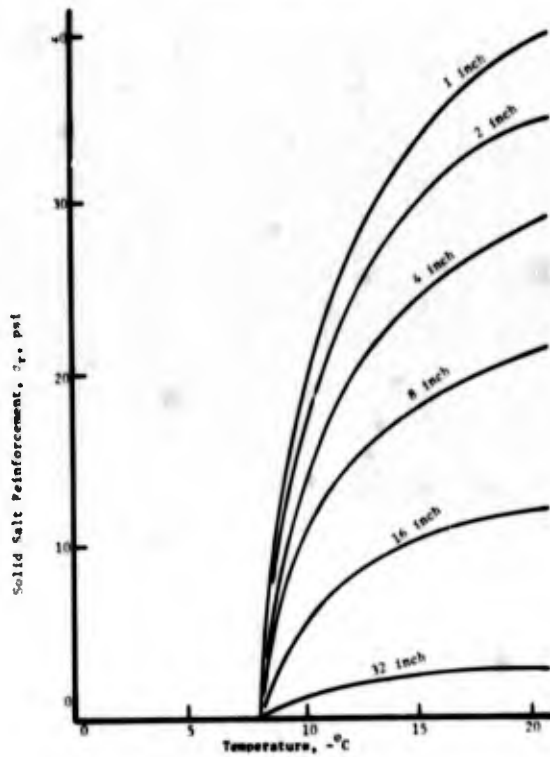


Figure 7.9

Idealized Solid Salt Reinforcement at Various Depths

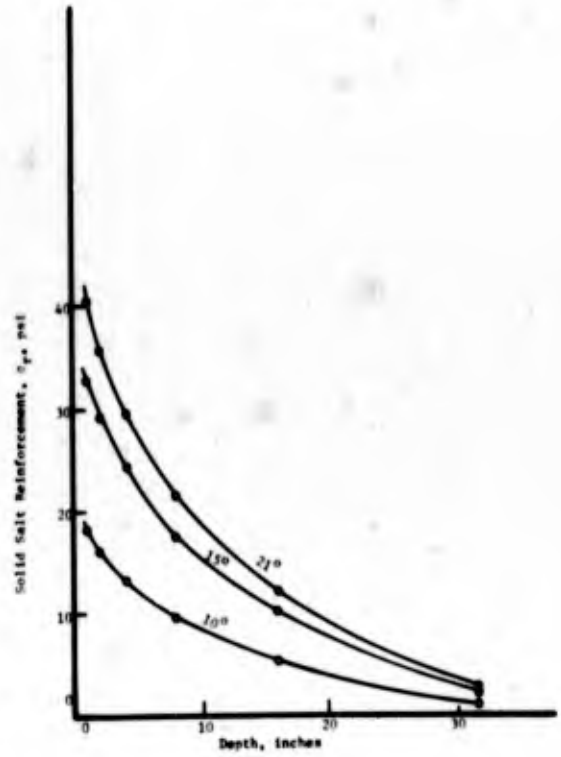


Figure 7.10

7.15, 7.16 and 7.17 are shown the strengths (strate times the rate function) of warm, medium, and cold ice respectively at the four different loading rates. Also shown are the totals or integrated strengths and the average strengths. The integrated strengths for the different rate-thermal regime combinations are shown in Table 7.13. Strength varies from about 145 to 1300 psi.

Table 7.13

Integrated Center Ice Sheet Strengths, lbs/inch of width
Thickness of 40"

Rate, psi/min	Warm	Medium	Cold
100	6,400	10,500	11,400
300	8,500	14,500	15,900
1,000	11,700	20,600	23,000
5,000	17,800	33,100	37,900

The medium and cold ice sheets are substantially stronger than the warm ice sheets, and the cold ice is somewhat stronger than the medium ice. Increasing rate from 100 to 5,000 psi/minute increases the strength by three times.

Figure 7.11 indicates the strength-depth relationship for a rate of 1,000 psi/minute for the three thermal regimes. In general, the warm ice strength is almost constant with depth because the brine volume-strength function decreases with depth but the rate function increases. The medium and cold ice have appreciable strength gradients with depth due to overriding effects of brine volume and solid salt reinforcement.

7.7 CONCLUSIONS

1. The general compressive strength function has been developed for all horizontally loaded center ice which inherently has horizontal crystal orientation but random orientation in the horizontal plane. The geometric variables used were based on bottom ice which is similar to center ice but has collinearly oriented crystals in the horizontal plane. Center ice can then be expected to behave somewhat as bottom ice if bottom ice properties were integrated in orientation about the horizontal plane. These geometric variables have shown to fit the data very well, but further refinements must await detailed analysis of bottom ice.
2. Center ice from varying depths in the ice sheet has a systematic pattern, thus making it possible to develop a general strength function with a correlation coefficient of 0.93 for 598 specimens with variation of temperature from -1° to -21°C and depths from 1 to 36 inches.
3. The general strength function is

$$\text{Strength} = f(\text{Load Rate})[f(\text{brine volume} + \text{solid salt reinforcement})]$$

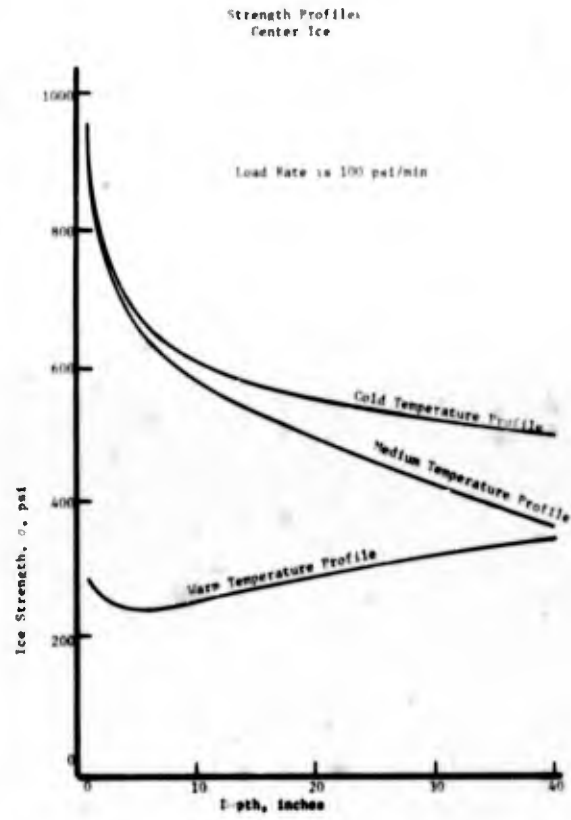


Figure 7.11

4. The function of load rate is

$$(\text{Load Rate})^{0.166} \text{Depth}^{0.136} \text{Temp}^{0.09} = f(\text{Rate})$$

5. The brine volume function is complicated. The greatest strength attenuation is due to liquid brine occurring with warm temperature near the ice sheet surface. The value of the function becomes much less with depth for all temperatures although it remains linear with strate for a particular depth. The details are expressed in equation 7.18. The reason for the attenuation of the brine volume effect with depth is not yet clear. The most intriguing speculation concerns platelet widths increasing with depth and the possibility of a shift in brine plane failures through the bridging ice to interior platelet ice. The failure plane shift is tentatively considered in Chapter 9. It is interesting to note here that such a shift does not negate the solid salt reinforcement concept, but rather enhances it for two reasons: 1) the solid salt reinforced ice is most probably stronger than interior platelet ice and 2) the reinforced brine channels may well inhibit crack propagation and increase the platelet ice's net rupture strength. Thus, the strength in the brine plane may exceed the strength in the platelet plane, and further, the strength in the platelet plane may be enhanced because of inhibition of crack propagation from platelet to platelet. Certain other speculations can be made about variability of brine channel shape, brine plane contaminates between channels, stress concentration, crystal lattice dislocations, and surface energy, but no clear evidence can be discerned.
6. All center ice indicates strong reinforcement due to precipitated sodium sulfate decahydrate. The reinforcement for a single depth is proportional to the salty quantity but the effect decreases with depth. This reinforcement is a significant factor in the strength of colder ice thus implying that salty ice is several times stronger than salt-free ice. Although intriguing, no definitive data are yet available for describing the mechanism of reinforcement.
7. The six primary variables which govern strength are ice type, orientation, load rate, temperature, depth and salinity.
8. The strength functions developed in this chapter are limited to ice warmer than -22.9°C and having direct compression failure.
9. The equations for center ice strength allow integration through a thickness up to 40 inches. Reasonable average strengths range between 155 to 955 pounds per square inch for reasonable field conditions and for failure modes in direct compression.

Chapter 8

STRENGTH FUNCTIONS, BOTTOM ICE

8.1 INTRODUCTION

General load rate functions were developed in Chapter 5 for each ice petro-fabric type and orientation. The development of this chapter is the determination of functions for brine volume and solid salt reinforcement for bottom ice by methods described in Chapters 6 and 7. The amount of data collected was very large; therefore, the orientation effect was closely studied with the data selected from a single depth and load rate.

8.2 AVERAGE STRENGTH

Tensile and compressive strengths are affected by the rate of loading, thus standard rates of loading were established and a calculation was made to determine the most probable strength at that rate for each orientation. The standard rates which were selected are 200 psi/min for tension and 460 psi/min for compression. The most probable strength values for each orientation were then obtained as follows:

1. For the main orientations (00-90, 90-00, 90-45 and 90-90), for which rate functions have been established, a group of 6 to 12 tests was selected with rates near the standard. Strate for the group was averaged and the appropriate rate function was applied to find the most probable strength.
2. For other orientations (22 1/2-90, 45-90, 67 1/2-90, 90-22 1/2, and 90-67 1/2) the tests were generally grouped near the standard rates. A linear regression of strength versus rate was calculated, and the strength was adjusted to reflect its value at the standard rate by use of the regression equation. This value was examined to ensure that it was typical. Sparsity of data in these orientations precluded development of a general rate function of high confidence.

Without a suitable general rate function, value of strate could not be determined with a high level of statistical significance. It is for this reason that the analysis in this chapter is made in terms of strength at the fixed value of load rate. Table 8.1 shows, for each orientation, the number of tests, strength at the standard rate, and standard deviation of the strength for both tension and compression. Figure 8.1 shows strength versus orientation in one configuration and Figure 8.2 indicates the same information in another configuration.

Table 8.1

Tensile and Compressive Strength at Standard Conditions
for Different Orientations.

Orientation	Tension			Compression		
	Number of Observations	Strength (Rate=200)	Stdev.	Number of Observations	Strength (Rate=460)	Stdev.
00-90	9	284	68	12	1260	175
22 1/2-90	6	169	19	9	638	150
45-90	4	192	15	12	790	250
67 1/2-90	6	132	22	7	348	40
90-90	8	153	25	8	612	115
90-67 1/2	5	151	25	8	329	82
90-45	8	110	27	6	259	145
90-22 1/2	6	109	8	8	356	70
90-00	9	132	13	8	1020	210

It is interesting and important to note that Figures 8.1 and 8.2 indicate the same pattern of strength versus orientation in compression as in tension. The fact that tension and compression strength patterns are similar reinforces the probability that each is roughly correct.

The quadrant from the b-axis to the c-axis is the zone containing the brine-basal failure plane and it will be studied in the greatest detail. The character of the strength-orientation function, the extreme variation in strength, and the known structure of the ice in this quadrant suggest that the strength and other mechanical properties of the brine-basal plane can be defined and is worthy of tentative analysis.

8.3 ELASTICITY

8.3.1 General. E, the modulus of elasticity, or Young's modulus, is defined by the slope of the stress-strain curve. In determining E for individual data, a stress-strain plot was made and the average strength for a group of similar data was determined if the plot showed substantial curvature. A secant slope was then obtained between a point of zero stress and a point equal to 1/3 the average maximum failure stress of repeated tests.

Tests were sorted by type, orientation and sampling date, and it was observed that E was strongly dependent on rate of loading. Table 8.2 indicates the E dependence of the various parameters including the best-fitting rate exponent, Exp , in the equation as determined by regression,

$$E = \text{Rate}^{Exp} (\text{All other functions}).$$

Table 8.2

Orient	Tension or Compression	No. of data	Rate Exp.	t-test	Correlation Coefficient		
					Multiple	With Strength	With Rate
00-90	T	65	.02	0.9	.39	.21	.13
90-00	T	53	.13	2.9	.56	.34	.38
90-45	T	58	.40	9.6	.84	.72	.71
90-90	T	67	.09	2.6	.44	.03	.30
00-90	C	113	.20	8.8	.74	.74	.58
90-00	C	105	.27	7.6	.71	.64	.56
90-45	C	95	.46	14.5	.84	.71	.79
90-90	C	114	.32	8.8	.72	.76	.62

The information presented in Table 8.2 is not intended to be definitive. It is presented to indicate some of the characteristics of E, shown by the tests, but without detailed analysis. This information shows generally:

1. The pattern of E versus rate is very similar to that for strength.
 - A. The E-rate relationship is curvilinear.
 - B. The exponent in compression is larger than the exponent in tension.
 - C. The pattern of exponents versus orientation is similar to that for strength.
2. The multiple correlation coefficients are all significant and are highly significant in most cases.
3. Partial correlation coefficients between E and strength and between E and rate are found to be significant in most cases.

It is important to remember that this is average information, and the modulus of elasticity has not been studied in detail.

8.3.2 Elasticity at Various Orientations. The data which have been studied for strength for different orientations were also subjected to a cursory examination of modulus of elasticity. For the different groups of tests, E has been determined by fitting a least squares line for E versus rate and then finding E for the standard rates of 200 and 460 psi/min for tension and compression respectively. Table 8.3 shows these values of E for the different orientations, and Figure 8.3 shows E versus orientation.

Table 8.3

Values of E at different orientations.

Orientation	E in compression Rate = 460 psi/min	E in tension Rate = 200 psi/min
00-90	2.47×10^5	10.23×10^5
22 1/2-90	.72 "	8.54 "
45-90	1.54 "	8.73 "
67 1/2-90	.56 "	6.22 "
90-90	1.75 "	7.90 "
90-67 1/2	1.13 "	4.76 "
90-45	.93 "	4.19 "
90-22 1/2	.58 "	4.27 "
90-00	1.30 "	8.11 "

Two points are important:

1. The modulus of elasticity for tension is approximately 5 times greater than that for compression.
2. The modulus of elasticity-orientation plot shows the same shape as that for strength-orientation.

The E orientation pattern in the brine-basal plane shows the same deep, broad valley as the strength-orientation. This reinforces further the confidence in the general strength-orientation pattern in the brine-basal plane shown by the data under study. It also suggests that the same sort of orientation relationship can be used to define the value of E in the brine-basal plane.

8.4 TENSILE STRATE FUNCTIONS OF 90-00, 90-45 AND 90-90 ORIENTATIONS

Strate has been defined as the strength with the rate function removed and Table 8.4 shows the average tensile strate and $(1-v^{1/2})$ for 44 inch depth ice for the three orientations, 90-00, 90-45 and 90-90 for temperatures of -2, -5, -10, and -21°C.

Table 8.4
Average Tensile Strate

Temp	90-00			90-45			90-90		
	Number of Obs.	Strate	$1-v^{1/2}$	Number Obs.	Strate	$1-v^{1/2}$	Number Obs.	Strate	$1-v^{1/2}$
-2°	20	78.4	.6512	15	53.3	.6568	16	108.2	.6703
-5	22	104.1	.7696	12	61.8	.7720	23	125.6	.7820
-10	8	112.8	.8355	11	72.4	.8421	20	150.0	.8328
-21	12	121.2	.8726	14	70.7	.8781	14	145.2	.8790

It is immediately obvious that no salt reinforcement is shown by the data. Furthermore, while the data appear approximately linear with $(1-v^{1/2})$, it is not sufficiently sensitive to changes in $(1-v^{1/2})$ to allow fitting of the general model.

Sea Ice Strength at Various Orientations under Standard Conditions

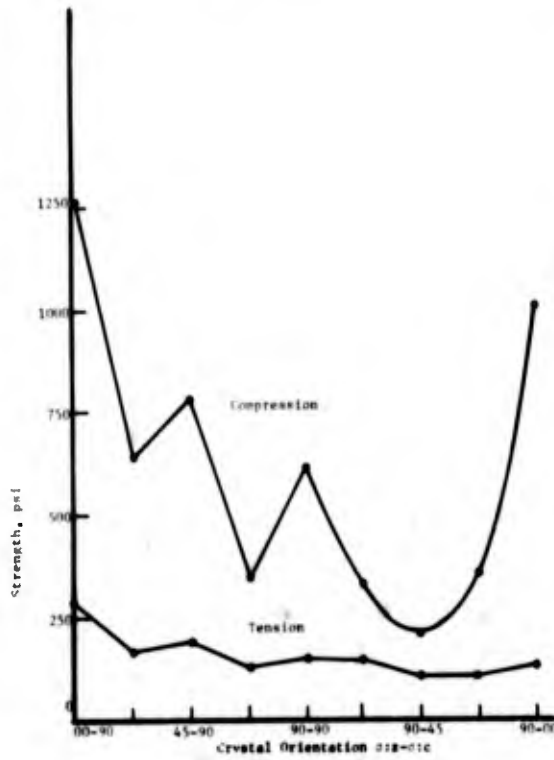


Figure 8.1

Tensile and Compressive Strength under Standard Conditions

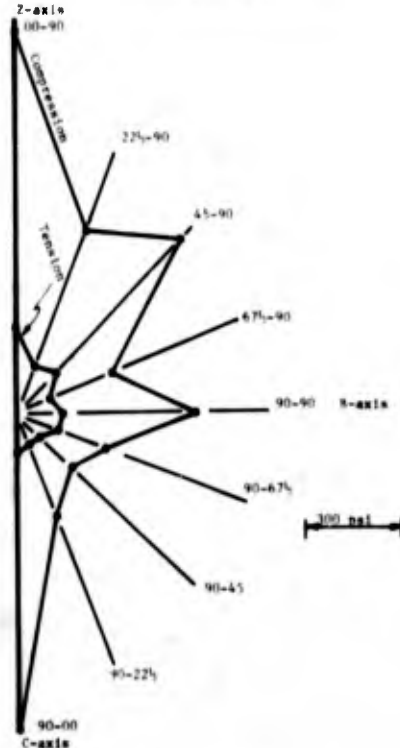


Figure 8.2

Modulus of Elasticity at Various Orientations under Standard Conditions

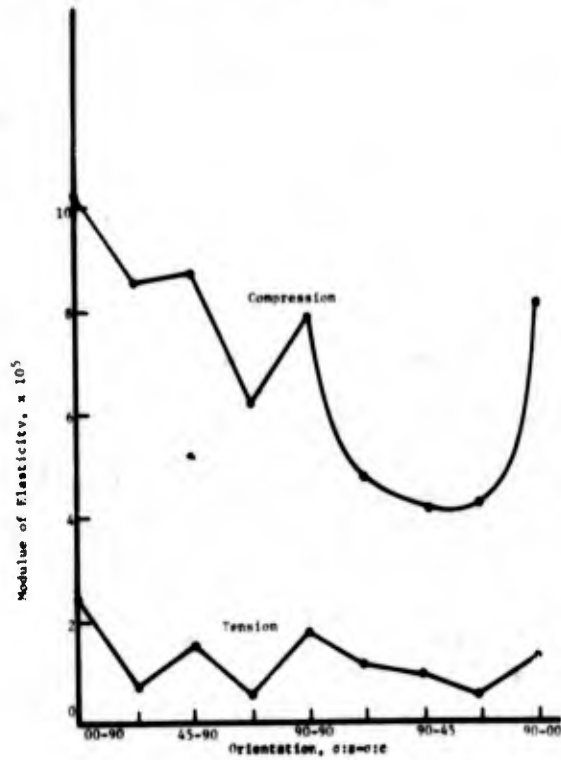


Figure 8.3

Strate, Brine Volume, and Orientation Relationship Bottom Ice, Tension

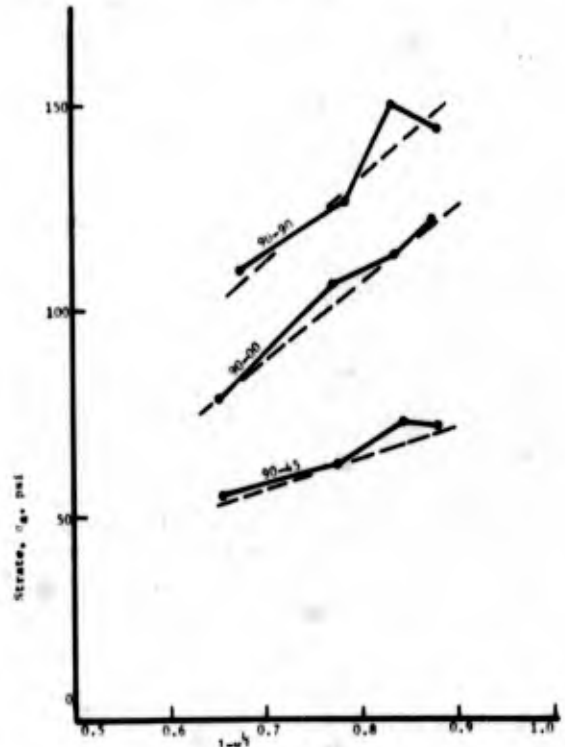


Figure 8.4

linear equations using the average values and weighted for number of observations are:

Orient	Equation	$(1-v^{1/2})$ intercept	
90-00	$\sigma_a = -46.4 + 193.0 (1-v^{1/2})$.240	8.1
90-45	$\sigma_a = -3.4 + 86.2 (1-v^{1/2})$.040	8.2
90-90	$\sigma_a = -31.9 + 207.8 (1-v^{1/2})$.154	8.3

and in standard form,

Orient	Equation	
90-00	$\sigma_a = 146.6 (1-1.32v^{1/2})$	8.6
90-45	$\sigma_a = 82.8 (1-1.04v^{1/2})$	8.5
90-90	$\sigma_a = 175.8 (1-1.18v^{1/2})$	8.6

These provide the strate functions needed to describe the tensile strength of sea ice at 44 inches of depth.

8.5 COMPRESSIVE STRENGTH FUNCTIONS OF 90-00, 90-45 AND 90-90 ORIENTATIONS.

8.5.1 Strate Functions. Table 8.5 and Figure 8.5 show the average compressive strate and $(1-v^{1/2})$ for 44 inch ice for the three orientations, 90-00, 90-45 and 90-90 for temperatures of -2, -5, -10, and -21°C.

Table 8.5

Average Compressive Strate

Temp °C	Number of Obs.	90-00 Strate	$1-v^{1/2}$	Number of Obs.	90-45 Strate	$1-v^{1/2}$	90-90 Obs.	Strate	$1-v^{1/2}$
-2	59	212.2	.682	45	14.09	.682	66	91.65	.700
-5	65	245.7	.800	47	17.22	.790	82	110.4	.802
-10	36	341.0	.832	34	17.07	.836	37	148.3	.839
-21	28	351.1	.881	24	22.33	.877	29	198.1	.881

Figure 8.5 demonstrates that the strength of 90-45 ice in compression, as in tension, shows no salt reinforcement and is relatively insensitive to changes in brine volume. On the other hand, the strength of 90-00 and 90-90 orientations in compression show a greater sensitivity to changes in brine volume function and also show strong salt reinforcement. The shape of the brine volume function for the 90-00 and 90-90 orientations can not be determined because only two temperatures, -2° and -5°, are available, in the non-solid salt temperature range. The brine volume function is assumed to be linear.

Linear equations fitting the above data and weighted for the number of observations are shown on the following page.

Orient	Temps	Equation	$(1-v^{1/2})$	Intercept
90-00	All	$\sigma_a = -256.0 + 671.2 (1-v^{1/2})$.381	8.7
90-00	2,5	$\sigma_a = 18.58 + 283.9 (1-v^{1/2})$	-.065	8.8
90-45	All	$\sigma_a = -8.62 + 32.82 (1-v^{1/2})$.263	8.9
90-90	All	$\sigma_a = -253.5 + 478.0 (1-v^{1/2})$.530	8.10
90-90	2,5	$\sigma_a = -37.0 + 183.8 (1-v^{1/2})$.201	8.11

Also shown are the linear brine volume equations in standard form.

Orient	Temps	Equation	
90-00	2,5	$\sigma_a = 302.5 (1-.938v^{1/2})$	8.12
90-45	All	$\sigma_a = 24.2 (1-1.36v^{1/2})$	8.13
90-90	2,5	$\sigma_a = 146.8 (1-1.25v^{1/2})$	8.14

The 90-45 ice shows no salt reinforcement and equation 8.13 completes the description of the strength of 90-45 compression ice at 44". A salt reinforcement term is required for the other two orientations.

8.5.2 Solid Salt Reinforcement Functions. Solid salt reinforcement is described as in Chapter 6.

$$\sigma_r = \sigma_a - \sigma_o (1-Gv^{1/2}) \quad 8.15$$

σ_r is salt reinforcement, and σ_o and G are the constants in equations 8.12 and 8.14. Table 8.6 shows the calculation of σ_r for the 90-00 and 90-90 ice at -10 and -21°C.

Table 8.6

Calculation of Salt Reinforcement.

Orient	Temp °C	Number of Observations	$1-v^{1/2}$	meas	calc	$\sigma_r = \sigma_m - \sigma_c$
90-00	-10	36	.832	341.0	254.8	86.2
90-00	-21	28	.881	351.1	268.7	82.4
90-90	-10	37	.839	148.3	117.2	31.1
90-90	-21	29	.881	198.1	124.9	73.2

As for center ice,

$$S = (S_{all} + v)^{1/2} - v^{1/2} \quad 8.16$$

where S_{all} is the relative quantity of solid salts and associated ice (salty ice). An equation has been developed for S for the temperature range, -8.2° to -22.9°C.

$$S = (\text{Salinity})^{1/2} (.082 - .180/\text{Temp}^{.381}) \quad 8.17$$

For the data under consideration, average S is 0.0154 at -10°C and 0.055 at -21°C, the details of which are shown in Figure 8.6.

In the study of salt reinforcement of center ice, the general function developed for salt reinforcement was

$$\sigma_r = G S K Q^e \quad 8.18$$

where G is the geometric constant found in determining the brine volume function, S has been defined, Q is a quality function for salty ice, e is the fitting exponent for Q, and K is a fitting constant. σ_r is calculated from equation 8.15, S is calculated from equation 8.17, and Q can be calculated from

$$Q = .034 + 2.707/T^{1.90} \quad 8.19$$

and from equation 8.18

$$\frac{\sigma_r}{GS} = K Q^e \quad 8.20$$

Table 8.7 shows the different values involved in equation 8.20 for the 90-00 and 90-90 compressive data.

Table 8.7

Salt Reinforcement Data

Orient	Number of Observations	Temp	σ_r	G	S	σ_r/GS	Q
90-00	36	-10°	86.2	.938	.015	6.20	.068
90-00	28	-21	82.4	.938	.055	1600	.052
90-90	37	-10	3.1	1.25	.015	1600	.068
90-90	29	-21	73.2	1.25	.055	1060	.042

Figure 8.7 gives the salt reinforcement data of Table 8.7 with a third point at the origin for each orientation. The relationship is linear for the 90-90 data, and e can be taken as 1. Using a weighted least squares line through the origin, K is approximately 250,000, but it was later necessary to adjust this to 30,000 when the functions were tested. The salt reinforcement for 90-90 compression is

$$\sigma_{r_{90-90 c}} = 30,000 G S Q \quad 8.21$$

For the 90-00 salt reinforcement, an equation can be fitted using a value of e of 2.5, but this increases the value of K by several times. Another approach is suggested by Figure 8.8 which shows the salt reinforcement to be constant at approximately 85 psi, and this approach will be used because of its simplicity.

Stress, Brine Volume, and Orientation Relationships
Bottom Ice, Compression

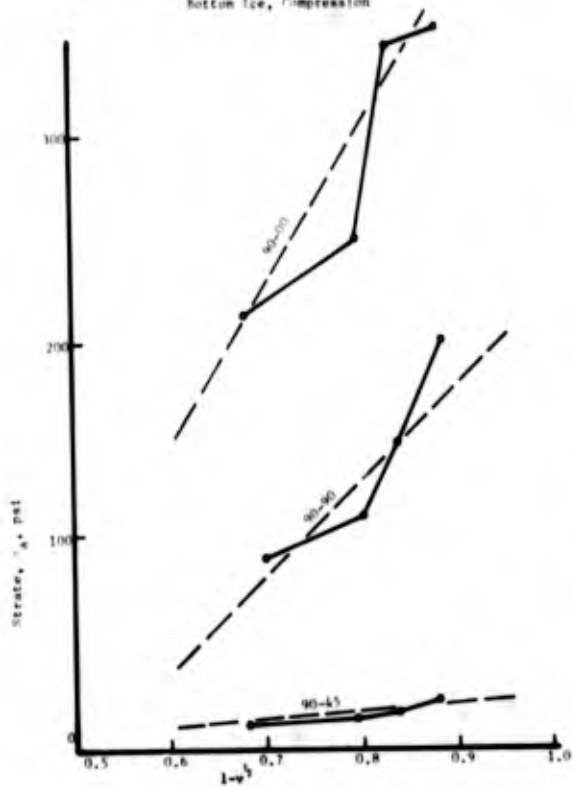


Figure 8.5

Plotback of 90-00 Tension Tests

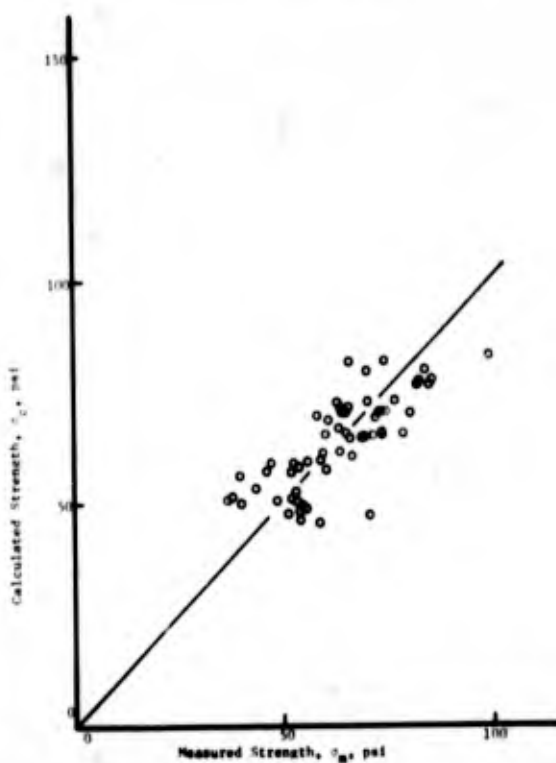


Figure 8.6

Solid Salt Reinforcement Function

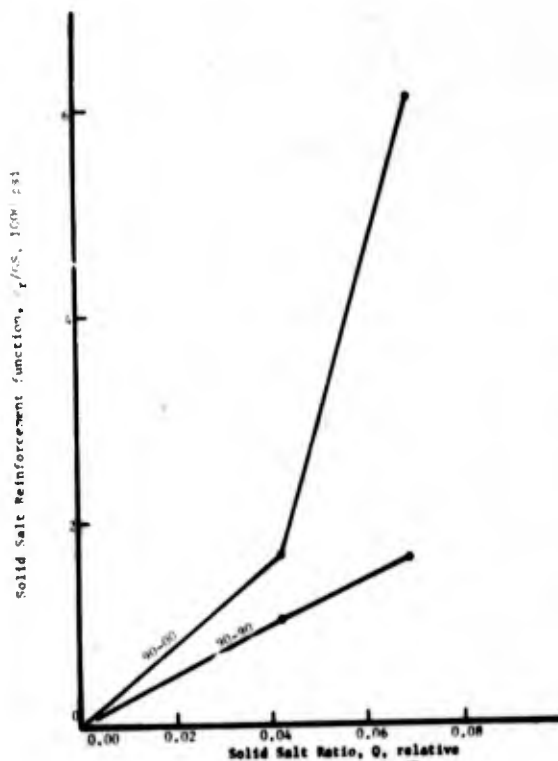


Figure 8.7

Solid Salt Reinforcement, Bottom Ice, Compression

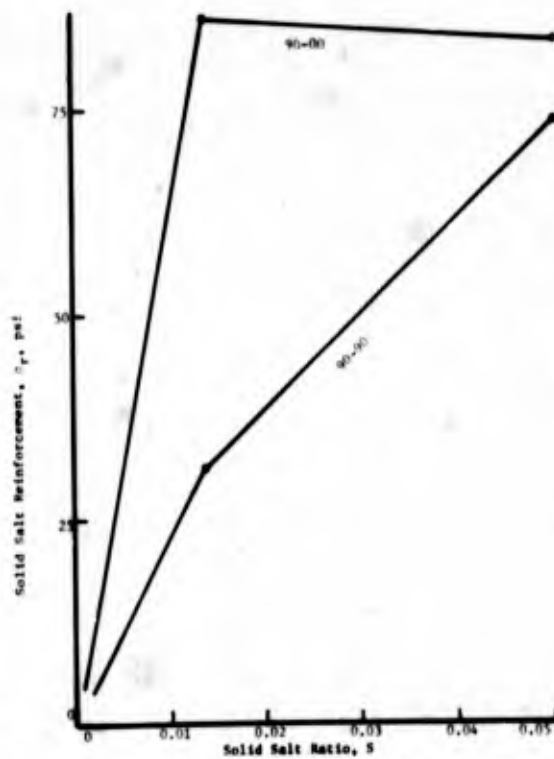


Figure 8.8

8.6 TESTING THE STRENGTH FUNCTIONS

8.6.1 Plotback Check. Plotback of the calculated value versus the measured value was used for the strength functions that were developed in the preceding two sections for strength at 90-00, 90-45 and 90-90 orientations in both tension and compression. Figures 8.8 to 8.13 show the calculated strength-measured strength using the following equations:

Fig.	Orient	Tension or Compression	Equation	
8	90-00	T	$= f(\text{rate}) (146.6(1-1.32v^{1/2}))$	8.22
9	90-45	T	$= f(\text{rate}) (82.8(1-1.04v^{1/2}))$	8.23
10	90-90	T	$= f(\text{rate}) (175.8(1-1.18v^{1/2}))$	8.24
11	90-00	C	$= f(\text{rate})(302.5(1-.938v^{1/2})+85.)*$	8.25
12	90-45	C	$= f(\text{rate}) (24.2(1-1.36v^{1/2}))$	8.26
13	90-90	C	$= f(\text{rate})(146.8(1-1.25v^{1/2})+30,000 G S O)*$	8.27

*Salt reinforcement only below -8.2°C.

Five statistical tests are used to determine the fit of the plotback and thus the fit of the equations, the results of which are shown in Table 8.8

1. The average residual.
2. The least squares slope from the origin through the data.
3. The standard deviation of the residuals.
4. The correlation coefficient.
5. The coefficient of variation.

Table 8.8

Statistical Tests of Strength Functions.

Data	Number of Observations	Average σ_m	Slope	R	Residuals, psi		Coeff. of Variation
					Avg.	Stdev	
90-00 T	62	124.7	.985	.73	-.13	17.8	.143
90-45 T	52	115.0	.978	.77	.10	17.2	.150
90-90 T	73	172.9	.961	.53	.01	35.7	.206
All Tens	187	140.8	.971	.62	-.01	26.0	.185
90-00 C	188	1039.	.968	.86	- 11.	273.	.263
90-45 C	150	323.	.980	.95	- 2.9	85.4	.264
90-90 C	214	771.	.963	.93	4.0	185.	.240
All Comp	552	740.	.967	.90	- 2.8	201.	.272
All Data	739	589.	.967	.90	- 2.1	174.	.296

The average residuals are negligible indicating that the average calculated strength is close to the average measured strength. The slope,

Plotback of 90-45 Tension Tests

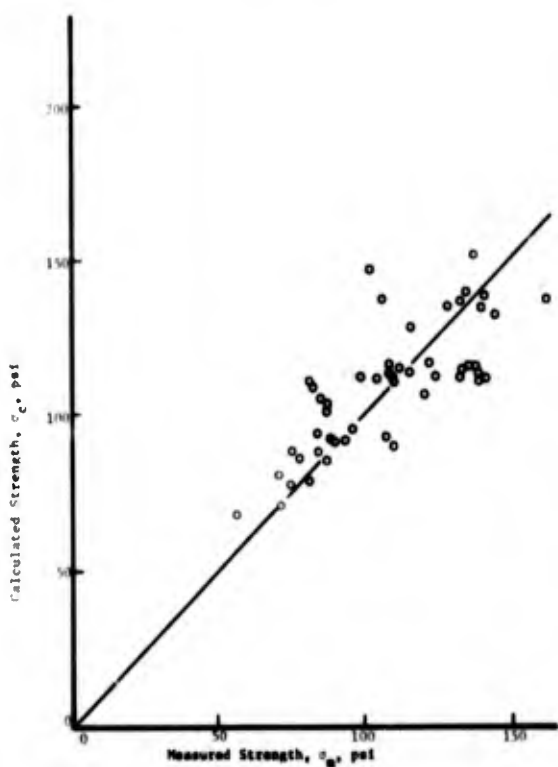


Figure 8.9

Plotback, 90-90 Tension Tests

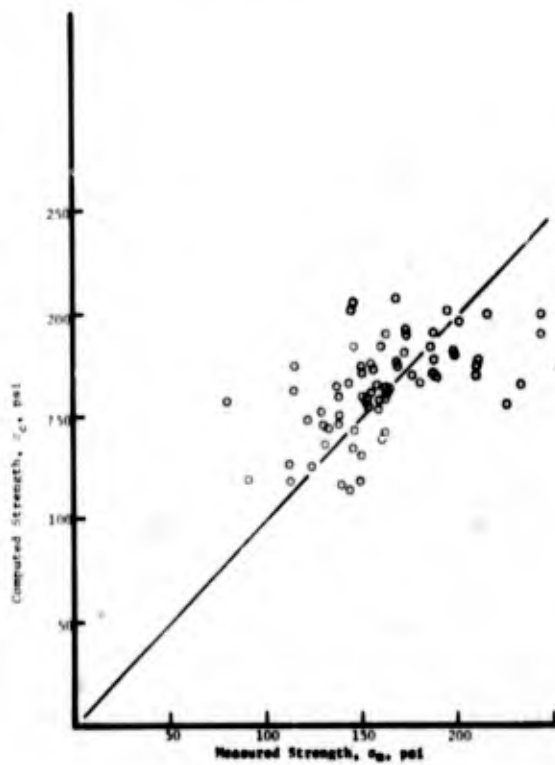


Figure 8.10

Plotback of 90-00 Compression Tests

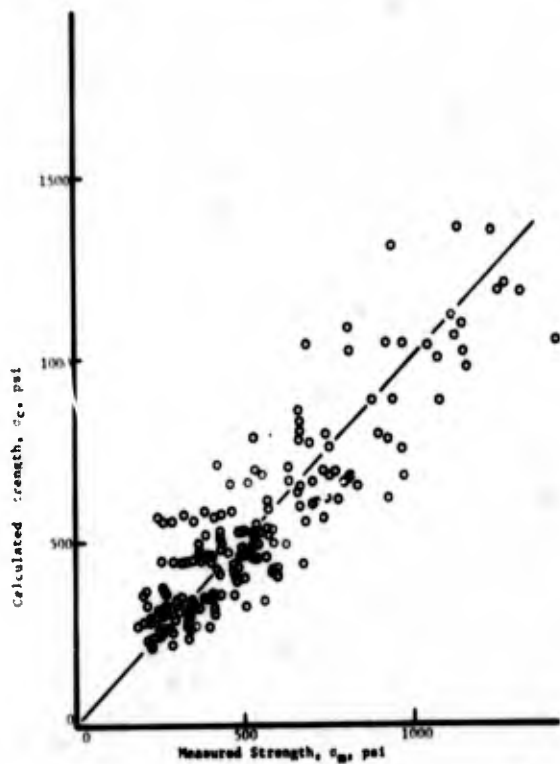


Figure 8.11

Plotback of 90-45 Compression Tests

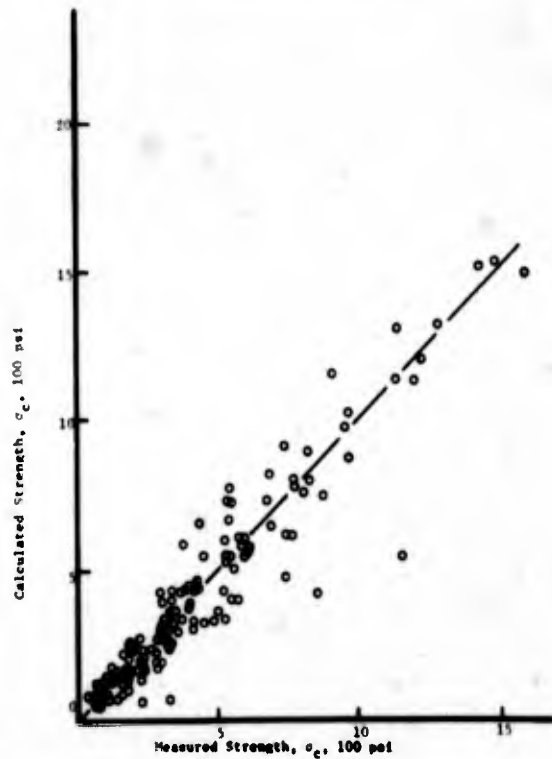


Figure 8.12

which is calculated by least squares shows an average value of approximately .97 with a systematic grouping of all data about that value. This indicates that all calculated values should be increased by approximately 3 percent to yield the best least squares fit; however, this small systematic error is ignored because the functions are probably as accurate as the data.

The correlation coefficients vary between 0.53 and 0.77 for tension and between 0.86 and 0.95 for compression. This is highly satisfactory. The coefficients of variation show a standard deviation in tension of 15 to 20 percent of the average value of measured strength. The compression data show the standard deviation of the residuals is approximately 25 percent of the average value of measured strength; however, while the compression data show a higher coefficient of variation, it also shows a higher correlation coefficient, and this apparent anomaly results from the different distributions and ranges of the data. The tension data are relatively insensitive to rate, and the range of rate was smaller than for compression. On the other hand, the compressive strength is much more sensitive to load rate and the range of the load rate is much greater. Consequently, the range of the compression data is much greater than the tension data. The tension data occur in a group removed from the origin by a discrete amount and have a fairly uniform density over a limited range. The result of this distribution gives relatively high average values which in turn yields a low coefficient of variation. The compression data, however, extends from near the origin for a relatively great range with high density near the origin, and decreases in density at the higher strengths. This gives average values that are relatively low and a correspondingly high coefficient of variation. The great range makes possible a high correlation coefficient.

The plotback plot and statistical analysis generate the following comments:

90-00 Tension. Figure 8.6

The data appear to be well centered on the line of perfect agreement. Because of the weak rate function, the data for the different temperatures are grouped separately, and the range for an individual temperature is small. This explains both the correlation coefficient (.73) and the coefficient of variation (.143). The fitting function is satisfactory.

90-45 Tension. Figure 8.9

These data also appear to be well centered on the line of perfect agreement. Because of the stronger rate effect, the data for the different temperatures overlap, and those for a single temperature have considerably more range than for 90-00 tension. The correlation coefficient is relatively large (.77) because of the increased data ranges.

90-90 Tension. Figure 8.10

This group of tests has the smallest correlation coefficient (.53) and the largest coefficient of variation (.206) of any tension group. It is relatively insensitive to load-rate, with the data grouped by temperature; however, the plot shows a general curve for the data as a whole. The reason for this is two-fold:

1. The data for each temperature tend to show a substantial scatter, and

2. The function used is a compromise because the -10° data show a substantial strength increase over that expected from the strath- $(1-v^{1/2})$ relation for -2° and -5° . This suggests solid salt reinforcement. The strength for -21° , however, drops to an approximately linear relationship with the -2° and -5° data, thus making the solid salt reinforcement concept questionable.

The -2° data falls on the line of perfect agreement. The -5° data falls somewhat above it. The -10° data falls below it and the -21° data falls above it. The correlation coefficient is sufficiently large to show a moderate correlation.

90-00 Compression. Figure 8.11

This pattern is fairly typical of the compression data groups. Because of rate sensitivity and range, the data for different temperatures overlap extensively, and for each temperature there is enough range in strength values to demonstrate a linear pattern. The correlation coefficient (.86) is quite good, but the standard deviation of the residuals (273.) and the coefficient of variation (.263) are both high. The function includes a constant salt reinforcement value, and it is obvious that salt reinforcement must be considered for this orientation. If the density of the data were more uniform, the coefficient of variation would be somewhat smaller.

90-45 Compression. Figure 8.12

Most of the comments regarding the 90-00 compression apply here, but the correlation coefficient is higher (.95), the differential density is more marked, and the overlap of the data for different temperatures is greater. The coefficient of variation (.264) is the same as for the 90-00 data and the fit for each temperature seems adequately centered and linear. Since no salt reinforcement is involved in the calculated strength, it appears certain that this orientation has insignificant salt reinforcement. These data and those for 90-45 tension show that the 90-45 ice is more consistent in performance than all other orientations studied.

90-90 Compression. Figure 8.13

The comments regarding the 90-00 and 90-45 compression data generally apply to this ice. The correlation (.93) is almost as good as the 90-45 data but the coefficient of variation (.272) is the greatest of any data group studied. Differential data density is seen to be much of the reason. The different temperatures overlap at the lower strengths; however, this function contains a salt reinforcement element which drives the -10° and -21° data into somewhat exclusive zones. Both the -10° and -21° data seem satisfactorily linear and these data, like the 90-00, appear to define a linear envelope indicating either random scatter or a second order effect not yet identified.

All Tension.

Statistical information has been calculated for groups of all tension, all compression, and all tests. In general, the All Tension grouping shows values that are approximately average for the three groups. The

All Compression.

This grouping shows an overall correlation coefficient of .90 but a relatively high coefficient of variation (.272) due to differential data density. The average residual is essentially zero and the least squares slope through the origin is .97. The poorest results were obtained from the 90-00 data.

All Data.

Because the compression data is approximately 3 times as numerous as the tension data, this shows primarily the results of the compression analysis. The data show a correlation coefficient of .90, a high coefficient of variation (.290), an essentially zero average residual, and a slope by least squares through the origin of about .97. Since tension strength is much weaker than compression, the effect of differential density noted in the compression data is intensified in this grouping of all 739 data.

It is concluded that the strength models and the functions derived therefrom express the behavior quite well and are considered adequate for the further analysis in Chapter 9.

Plotback of 90-90 Compression Tests

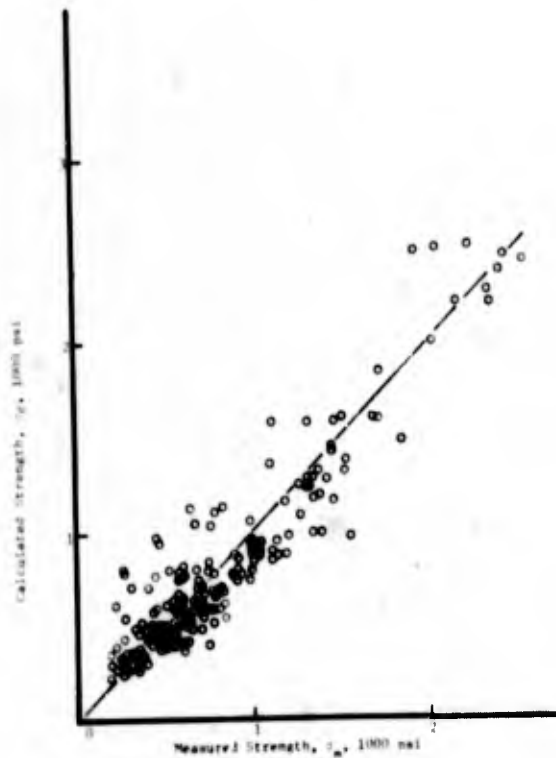


Figure 8.13

Chapter 9

BRINE PLANE - BASAL PLANE FAILURE

9.1 INTRODUCTION

The extremely low strength and stiffness of ice subjected to basal plane shear stress is well known and has been intensively investigated in fresh ice, single and polycrystalline. Substantial evidence has been found in this study for proposing that sea ice properties are sometimes dictated by basal plane characteristics of ice within platelets rather than by the parallel brine plane with its liquid brine and solid salts. These effects were not discernable in center ice, but became quite clear in observations of certain bottom ice properties.

Should basal plane failure be significant, several properties should be apparent, but before proceeding to such a list, the following considerations are put forth.

A shift from brine plane failure to basal plane failure could occur at warmer temperatures and would be difficult to ascertain without data over many small increments of temperature. Such data do not exist, but this type of shift is quite unlikely because of very low areas of bridging ice in the brine plane near the melting point. Ice specimen failures under these conditions in the laboratory have resulted in considerable delamination of crystals. This was not generally found in specimens with high shear stresses in the brine-basal plane, but was found with edge loading of the platelets.

Nothing is known about the crystal orientation of the bridging ice; at least sufficient detail is not available to allow a definitive strength analysis. It is conceivable that bridging ice is not a continuation of platelet ice, but the presentation which follows will consider only the continuation concept.

9.2 BRINE - BASAL PLANE CHARACTERISTICS

9.2.1 Necessary Conditions. Two parallel planes will be considered. The first is the brine plane including the total interplatelet brine at -1.8°C , the solids that form from this liquid, and the ice bridging from platelet to platelet at -1.8°C . The second is the basal plane within the fresh ice platelet.

Brine-plane failure requires several elements:

1. A linear relation between σ and $(1-v)^{1/2}$ with σ sensitive to v .
2. A reasonable value of v_0 , perhaps in the order of .5 to .65.
3. Salt reinforcement. All solid salts are deposited in the brine plane, therefore, salt reinforcement indicates that failure occurs either in the brine plane or in a failure plane cutting the brine plane.

Basal plane failure characteristics to be expected would include:

1. A rather limited relationship between strength and brine volume. Brine volume would probably be of some effect until enough ice had formed to provide a continuous platelet structure through the specimen. Beyond that point, the strength should remain approximately constant except for the direct temperature effect on the platelet structure strength.
2. Relatively high creep rates at cold temperatures.
3. No salt reinforcement.

9.2.2 Mechanical Properties in the Brine-Basal Plane. The behavior of the 90-45 ice in both tension and compression suggests a basal plane failure in the ice platelets between brine planes. This question is left open for the present and a general function for either the brine or basal plane or both can be developed without definitely identifying the specific plane involved.

Figure 9.1 shows a specimen with unit cross-sectional area loaded with an axial force $\sigma \cdot AB$ and a crystal axis at an angle θ with σ . The brine-basal plane of weakness cuts the specimen at EF perpendicular to the c-axis. Figure 9.2 shows a force diagram of the upper part of the specimen with the internal forces $\sigma_n \cdot EF$, and $\sigma_s \cdot EF$.

$$\sigma_n \cdot EF = \sigma \cdot AB \cdot \cos \theta \quad 9.1$$

$$\sigma_s \cdot EF = \sigma \cdot AB \cdot \sin \theta \quad 9.2$$

However, $AB/EF = \cos \theta$, and equations 9.1 and 9.2 can be written

$$\sigma_n = \sigma \cos^2 \theta \quad 9.3$$

$$\sigma_s = \sigma \sin \theta \cos \theta \quad 9.4$$

or

$$\sigma = \sigma_n / \cos^2 \theta \quad 9.5$$

$$\sigma = \sigma_s / \sin \theta \cos \theta \quad 9.6$$

Figures 9.3 and 9.4 show the situation when θ approaches 90° and it can be shown,

$$\sigma_e CD = \sigma AB \sin \theta \quad 9.7$$

$$\sigma_e = \sigma \sin^2 \theta \quad 9.8$$

$$\sigma = \sigma_e / \sin^2 \theta \quad 9.9$$

Equations 9.5, 9.6 and 9.9 yield ultimate strength values based on three modes of failure in the b-c-axis plane. The most important strength function here is that for shear in the brine-basal plane. Equation 9.4, where σ_s is the shear strength in the brine-basal plane, can be solved for σ_s for the 90-45 data. Since $\sin \theta \cos \theta$ is 0.5 for $\theta = 45^\circ$,

$$\sigma_s = 0.5 \sigma_{90-45} \quad 9.10$$

Force On a Specimen
Small θ



Figure 9.1

Force Diagram
Small θ



Figure 9.2

Force On a Specimen
Large θ

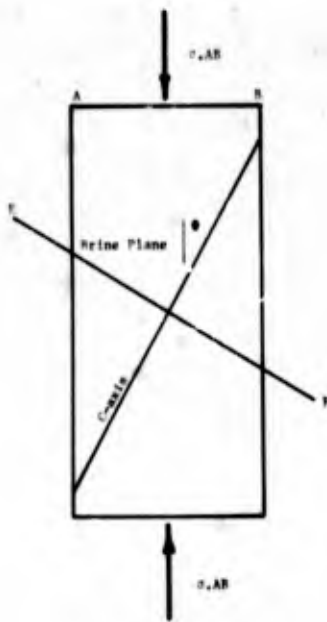


Figure 9.3

Force Diagram
Large θ



Figure 9.4

Figure 9.5 shows the function $\frac{1}{\sin \theta \cos \theta}$ which becomes infinite if θ is 0° or 90° and attain a value of 2.0 for $\theta = 45^\circ$. This function forms a broad, deep valley similar to the apparent shape of the strength function.

The function is valid at angles greater than 0° less than 90° . Near 0° and 90° the lack of information prevents definition of the shape of the curve from data. Two possibilities present themselves:

1. If 90-00 and 90-90 orientations have unique modes of failure based on the frontal and edge loading of the platelet structure, equations 9.5 and 9.9 would begin to govern as the angle between load and the c-axis departed from 0° and 90° .
2. If sea ice acts as a granular or amorphous material when loaded on these two axes, the strength should remain approximately constant until another mode of failure controls strength.

Figure 8.6 shows strength versus orientation with both options 1 and 2 under the standard conditions outlined in Chapter 8. The scale factor used for the central part of the function is obtained using equation 9.10 which yields 129.5 psi in compression and 55 psi in tension. At both ends of the curve, strength is

$$\sigma_n = 90-00 \text{ strength} \quad 9.11$$

$$\sigma_e = 90-90 \text{ strength} \quad 9.12$$

By definition, the 90-00, 90-45 and 90-90 strength values are on the curve. The 90-22 1/2 and 90-67 1/2 values are the only ones available for testing the curves and these strengths are shown in Table 9.1 and Figure 9.6. Three values fit rather nicely but the 90-22 1/2 strength in tension is lower than it should be. The fit is sufficiently satisfactory to indicate that the strength-orientation relation is a good first approximation for the data available.

Table 9.1

Estimated-Measured Strength Values for Odd Orientations

Orientation	Tensile Strength		Compressive Strength	
	Estimated	Measured	Estimated	Measured
90-67 1/2	151	156	329	366
90-22 1/2	109	156	356	366

The shape of the curve is undefined between $0^\circ - 22 \frac{1}{2}^\circ$ and $67 \frac{1}{2}^\circ - 90^\circ$. Evidence from tests of laboratory grown single, fresh, ice crystals indicates the strength to be very sensitive to θ near 0° and 90° . The sea ice tests did not show such high sensitivity, but the expected true shape of the curves are shown dotted. Certain additional effects would be expected from experimental error due to lateral restraints at specimen ends and end interference with brine plane and platelet continuity.

Brine-Basal Plane Function

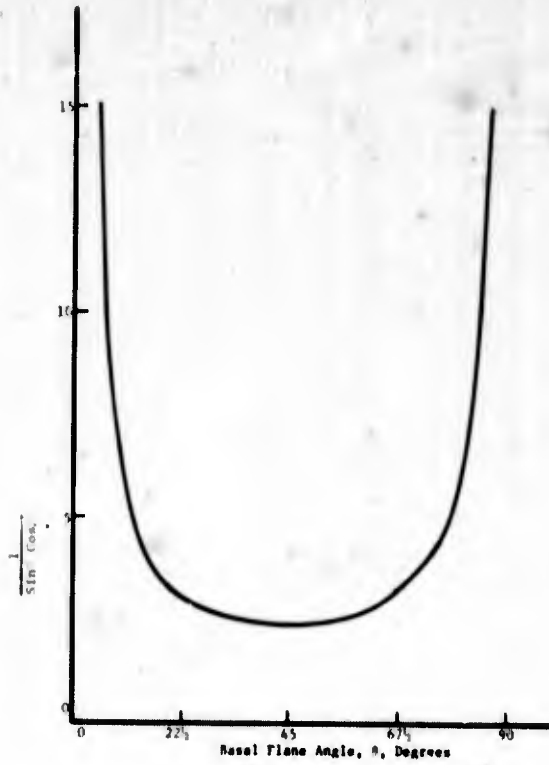


Figure 9.5

Strength Orientation Relationship

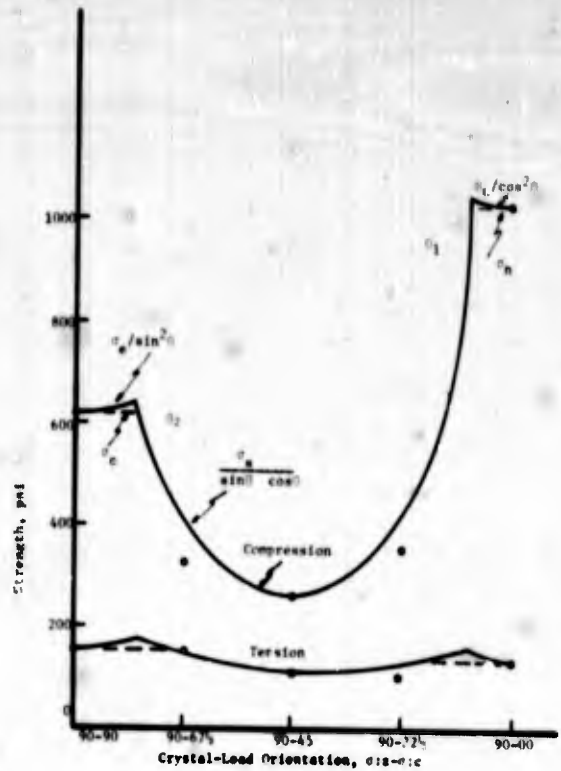


Figure 9.6

Rate Function-Orientation Relationship

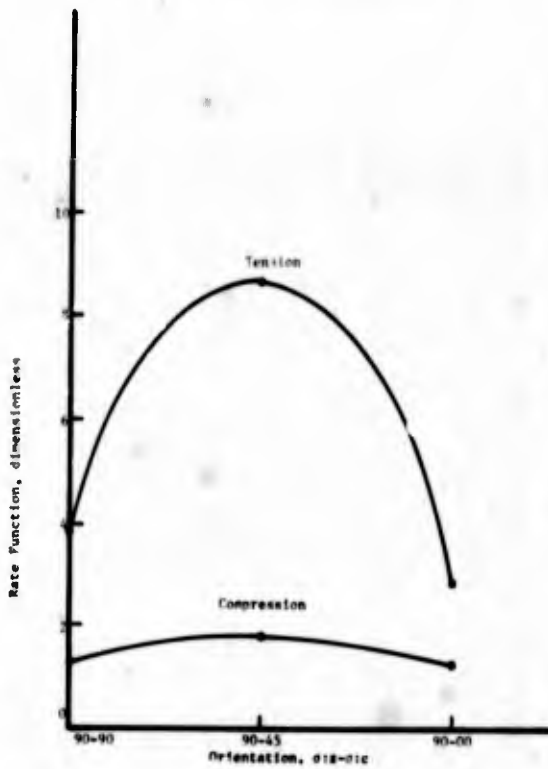


Figure 9.7

Stress Values for Bottom Ice Loaded on the Brine-Basal Plane

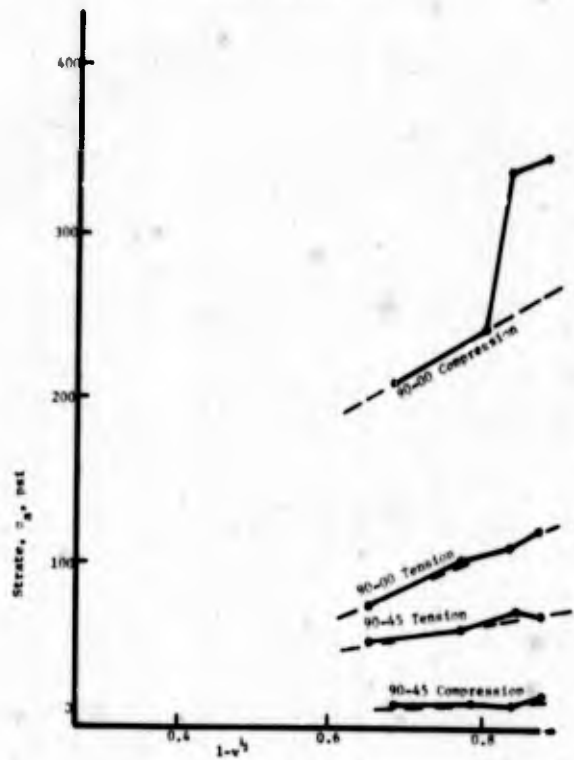


Figure 9.8

9.2.3 Rate Functions in the Brine-Basal Plane. The rate functions for tensile and compressive strength were developed in Chapter 4 with the general approach

$$\text{Strength} = f(\text{rate}) \times (\text{All other functions})$$

where

$$f(\text{rate}) = \text{Rate}^r$$

The exponent, r , is empirically fitted to the compression strength data in the horizontal plane:

$$r_{\text{comp}_h} = 0.166 \text{ Depth}^{.138} \text{ Temperature}^{.09} \text{ Rotvar}_c \quad 9.12$$

and, for tensile strength

$$r = .082 \text{ Depth}^{-.195} \text{ Temperature}^{-.064} \text{ Rotvar}_t \quad 9.13$$

Rotvar is the Rate Orientation and Type Variable empirically fitted for the different orientations and types. Table 9.2 shows the values of Rotvar for bottom ice.

Table 9.2

Values of Type and Orientation Variable for Several Orientations

Orientation	Rotvar _{comp.}	Rotvar _{tens.}
90-00	.60	1.82
90-45	1.26	4.48
90-90	.79	2.12

The $f(\text{rate})$ is shown in Table 9.3 and Figure 9.7 for tension and compression for 44 inch ice at -5° at rates of 200 psi/min for tension and 460 psi/min for compression.

Table 9.3

Rate Functions for Standard Conditions.

Orientation	Compression		Tension	
	r	$f(\text{rate})$	r	$f(\text{rate})$
90-00	.194	2.79	.0445	1.266
90-45	.407	8.60	.109	1.78
90-90	.255	3.86	.052	1.32

Comparison of Figure 9.7 with Figures 8.1 and 8.3 indicates that, in the basal plane, an inverse relation exists between the rate function and both strength and modulus of elasticity.

9.2.4 Brine Volume and Salt Reinforcement in the Brine-Basal Plane. Four data groups represent direct loads on the brine-basal plane. The 90-00 data is loaded directly on the basal plane in either tension or compression. The 90-45 data is loaded at 45° to the brine-basal plane

and exerts the maximum shear force combined with either a tensile or compressive force. Tables 8.4 and 8.5 show the values of strate and $(1-v)^{1/2}$ for this data at the temperatures available. Equations for the brine volume functions have been developed in the form

$$\sigma_a = \sigma_o (1-Gv)^{1/2}$$

Table 9.4 shows the values of σ_o , G, and v_o for the four groups, and Figure 9.8 shows strate versus $(1-v)^{1/2}$.

Table 9.4

Equation Data for Groups Loaded on the Brine Plane

Orient	σ_o	G	v_o
90-00	146.6	1.32	.634
90-45	82.8	1.04	.040
90-00	302.5	.938	1.134
90-45	24.2	1.36	.543

9.3 SUMMARY AND CONCLUSIONS

Analysis of all details which have been outlined has not been accomplished and some gaps occur in Table 9.5 which summarizes details of the mechanical properties of bottom ice of various load orientations.

Table 9.5

Orientation vs Mechanical Properties

	Compression				
	90-00	90-22 1/2	90-45	90-67 1/2	90-90
$\bar{\sigma}$, psi	1020	356	259	329	612
Ex 10^{-5} , psi	1.30	0.58	0.93	1.13	1.75
Strate, psi	246		17		110
Rotvar	0.60		1.26		0.75
Rate Exponent	0.19		0.14		0.26
f(rate)	2.8		8.6		3.9
σ_o , psi	303		24		147
G	0.94		1.3		1.4
v_o	1.1		0.54		0.62
Salt Reinforcement	yes		no		yes

Orientation vs Mechanical Properties

	Tension				
$\bar{\sigma}$, psi	132	109	110	141	143
$\text{Ex}10^{-5}$, psi	8.11	4.27	4.10	4.76	7.90
Strate, psi	104		62		126
Rotvar	1.82		4.48		2.12
Rate Exponent	0.04		0.11		0.05
f(rate)	1.3		1.8		1.3
σ_0 , psi	147		83		176
G	1.3		1.0		1.2
v_0	0.58		0.90		0.71
Salt Reinforcement	no		no		no

The evidence clearly indicates that compression at 90-45 and tension at 90-45 and 90-00 exhibit characteristics of failure outside the brine plane, at least for temperature colder than -10°C . Behavior at warmer temperatures is quite different from that for 90-90 orientation, but the differences could be equally ascribed to brine plane failure or as basal plane failure.

The 90-22 1/2 orientation seems adequate to force basal plane failure, but information is inadequate to make further analysis at this time. The 90-67 1/2 orientation is strongly affected by mechanical and geometrical constraints on the ends of specimens; therefore, these data would yield erroneous results.

The 90-00 compression curve shows obvious solid salt reinforcement and that failure must be influenced by the brine plane. The three groups remaining for examination are the 90-00 tension data and the 90-45 data in both compression and tension. The 90-00 tension data show:

1. There is no apparent salt reinforcement.
2. For the four different temperatures, strate is apparently fairly linear with $(1-v)^{1/2}$.
3. $v_0 = .63$ is reasonable.

Table 8.3 and Figure 8.3 show the 90-00 tension ice to be relatively stiff and the stress-strain curves for the individual data show an almost linear relationship curve from the origin to the point of failure with only small load rates and warm ice showing significant curvature. The tensile strength of 90-00 ice is only 20% stronger than that of 90-45 ice. This has been shown in Figure 8.1. The rate function compared with that for 90-45 tension ice is small with tension Rotvar values respectively of 1.82 and 4.48.

Inspection of the 90-00 tension data indicates no salt reinforcement. In addition, the four data points are quite linear with $(1-v)^{1/2}$, thus reinforcing the validity of this function. Finally a v_0 of .63 is a reasonable value. It seems; therefore, that all criteria for brine plane failure are met with the possible exception of salt reinforcement.

The 90-45 tension data indicates some similarities to the 90-00 tension data. There is no salt reinforcement and there is apparently a linear relationship with $(1-v)^{1/2}$. σ_0 is about 83 psi compared with 147 for the 90-00 ice. The slope is relatively flat with a G value of 1.04 and an $(1-v)^{1/2}$ intercept of .04. In this case, the requirement for a reasonable v_0 value is not met.

The 90-45 compression data shows no salt reinforcement, it is fairly linear with $(1-v)^{1/2}$, and it has a reasonable value for v_0 . However, this ice is very weak with a σ_0 of .3 that for 90-45 tension. Since σ_0 is in terms of strata, it is necessary to calculate a rate function to compare strengths. Using a rate of 500 psi/min, a depth of 44 inches and a temperature of -5° , the rate functions for tension and compression are 2.68 and 12.4 respectively. In this representative case, the ratio of compression to tension rate functions is 4.64, thus the compressive strength for this ice is greater than for tension.

The evidence is not entirely satisfactory to explain the occurrence of solid salt reinforcement in some orientations but not in others. There is, however, enough evidence to demonstrate the possibility of failure plane shift from the brine plane to the basal plane within platelets at cold temperatures when the brine plane strength may be strongly reinforced with solid salts.

It should be noted that no solid salt reinforcement has been indicated by tension tests on bottom ice. The question of possible solid salt reinforcement as reported by Assur has not been verified by the direct tension tests of bottom ice used in this study.

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Chapter 10

APPLICATION

10.1 INTRODUCTION

Direct application of the work shown in the preceding chapters was made on a specific project from 1963 through 1965; determination of ice loads, design, fabrication, erection and performance testing of a large offshore oil drilling platform in Cook Inlet, Alaska. The analysis in Chapters 4 through 9 were not completed, and parts had not yet been initiated. Early analysis had given considerable insight to the engineering properties of sea ice, and intuitive reasoning could be used with discretion. It should be noted here that the time requirement for establishing the design conditions in a new environment was very short. For example, specially manufactured steel for the future structure was ordered less than six months after the project was conceived and three months after the author began work on the design conditions. The tone of this chapter, therefore, is quite different from that of preceding chapters which were in a research instead of design atmosphere.

The actual study was accomplished in a different manner than outlined here. Actually, the work resulted in a set of four reports, each a substantial refinement of the other. This chapter will contain only those portions which show the end product and the method of achieving it. Work which was exploratory and was later refined will be deleted in the interest of clarity and brevity. Further, much of the detailed work has yet to be released from proprietary status.

10.1.1 The Problem. The problem is rather simple to state: "What will be the forces imposed by ice on an offshore oil drilling platform in Cook Inlet, Alaska?" There is some experience concerning lateral loads on piling or structures by ice in rivers and in some other situations. The extrapolation of this experience to the Cook Inlet is, however, not practical because of the different parametric factors that are known to occur in Cook Inlet. These include high tides, large tidal velocities, high mineral content in the form of soil particles in the water, and considerable mixing of fresh river water with sea water. No previous work has been done in attempting to describe the ice conditions in Cook Inlet.

10.1.2 Status of Knowledge. The description of lateral loads on structures due to ice is an empirical relationship, and the literature contains certain empirical expressions describing these lateral forces on such structures as bridge piers located in rivers. Mechanical properties of ice are highly variable thus leading to different failure modes and great differences in strength. Extensive differences in heat transfer result in large differences in ice growth rates, even in locations with similar ambient weather conditions. Therefore, it is impossible to closely predict lateral loads on a specific structure in a specific location without first determining for the specific ice the expected thickness, the strength of that ice, and the failure mode exhibited when such ice impinges upon a structure. Of necessity, then, an empirical ad hoc experimental approach must be followed if answers are to be found in reasonable time.

10.2 INITIAL OBSERVATIONS

Cook Inlet. Cook Inlet, Alaska, assumed considerable engineering importance after the discovery of offshore oil in the summer of 1962. The Inlet is one of the most difficult in the world in which to work because of 35 foot tides and six knot tidal velocities. The high latitude of 62° results in strong Coriolis forces, so this coupled with the Inlet geometry causes considerable cross currents at both ebb and flood tides. The water is quite turbulent through its entire depth and has a high silt suspension content which makes it virtually opaque. The water depths are variable from 135 feet to -35 feet, based on mean low tide, resulting in frequent choppy wave action, extensive mud flats and three to four foot tidal bores. The general distribution of atmospheric air pressures coupled with the geometry of surrounding mountains and valleys allows full gales to frequently occur and the attendant water waves have heights of about 30 feet. Katabatic winds are very strong in the Turnagain and Knik Arm vicinities. The influx of fresh water from numerous rivers is highly variable from summer to winter resulting in an attendant variability in salinity in the Inlet.

These factors alone make Cook Inlet a difficult place in which to work, but the climate is sufficiently cold in the winter to also create a sea ice cover of up to 3.5 feet. This ice forms in floes of up to two miles in diameter which move up and down the Inlet with the six knot tide and travel distances in the order of 25 miles per tide.

The study of this ice is the topic of this chapter. The general characteristics of the Inlet are shown in Figures 10.1 through 10.4.

10.3 ICE THICKNESS PREDICTIONS

The thickness of the sea ice in Cook Inlet is derived from two mechanisms. The first is the growth thickness and the second is the mechanical stacking or rafting. The analysis of growth of sea ice in Cook Inlet has proved to be an interesting problem. Many factors are contributing to the growth and decay of the ice sheet, and fundamental information of the oceanographic and weather parameters of the Inlet area are too meager to allow competent analysis from first principles at the present time. Therefore, the analysis prior to construction of the first offshore drilling platform was subject to wide limits of confidence.

10.4 RAFTING

At the time of maximum ice growth in the Inlet and at the time of sampling for strength measurements, thickness determinations were made of several floes during 1963-64. They were quite uniform in thickness of about twelve inches. At this time, general observations were made concerning the occurrence of rafting, and it was determined, and is shown in Figure 10.5, that the majority of the rafting occurs when the ice is quite thin and generally does not appreciably affect ice thickness. However, it will be noted that some small areas of rafting do indeed occur which can double the thickness of the ice sheet. Several locations were observed in which the one foot thick ice sheet had rafted with its full thickness, thereby resulting in a two foot thick ice sheet. It will be noted, however, that not only

the fact that the ice sheet doubles in thickness is important, but also of significance, is the horizontal extent of such thickening. The field determination of rafting effects is complex because a search must be conducted for the maximum rafting effects. This is a population sampling program which requires a large number of observations.

10.5 ICE STRENGTH

10.5.1 Mode of Failure. The most important observation made during the first winter of the study was the mode of failure of the ice when impinging upon a temporary exploratory drilling platform. Figures 10.6, 7 and 8 show the general features of the failure type. At the time these pictures were taken, the tidal movement was into the Inlet, or a flood tide. The "A" arrows in all figures indicate the platform orientation with the "A" arrow indicating "up Inlet" toward Anchorage.

It can be observed that the failure mode of the ice is direct compression. No significant tension cracking of the ice floes occurred, and the total volume of ice impinging upon a single platform piling is crushed into very small pieces. Figures 10.9, 10 and 11 show this failure in detail. Figure 10 shows in particular the ice being reduced to small particle size.

Figures 10.6, 7, and 8 show that orientation of the platform relative to the direction of general ice movement is of little significance in reducing ice forces on the platform due to forces imposed by floes, be they rafted or not. This can be observed particularly in Figure 10.7 in which the "trailing" piling might have been expected to receive substantial force reduction. Piling No. 3 in Figure 10.7 can be observed to be offset about one piling diameter and is apparently receiving negligible force reduction due to the path cut by piling No. 1. This compression failure mode makes the utilization of ice cutters of questionable value.

Also to be observed from Figures 10.6, 7 and 8, is the type of path cut through the floes. The platform is obviously a restriction to the movement of individual floes. The configuration and point of contact of upstream floes with the particular floe which is being extruded past the platform results in differing path shapes. In Figure 10.6 it can be seen that a curvilinear path is being generated, probably dictated by the floe immediately upstream from the one being cut. Figure 10.7 shows a large floe moving past the platform in which no major floes are obvious upstream and the path generated is straight. Figure 10.8 again shows a curvilinear path. The upstream conditions at the time of the photograph are unknown.

10.5.2 Ice Strength Testing, 1962-63. Mid-Inlet ice was sampled at Middle-ground Shoals immediately after the maximum ice growth conditions occurred during the winter of 1962-63. The only major ice-growing weather occurred during the first week of February and sampling was done on 7 February when the ice was thickest. Five samples were collected and salinity profiles were determined for each sample. Eighty-two compression and tension tests were made from the ice collected.



Rafting of Thin Ice Flows. F indicates Rafted Section.

Figure 10.5



Ice Failure Against Platform, I, Note the Double Thick Rafted Section and the Small Flow Size.

Figure 10.6



Ice Failure Against Platform II, Note the Double Thick Rafted Section and the Compression Failure on all Four Legs.

Figure 10.7



Ice Failure Against Platform, III, Note the Curvilinear Path and Nature of Flow Splitting which does not Reduce Platform Loads.

Figure 10.8

10.5.3 Ice Strength Testing, 1963-64. Two favorable ice growing periods occurred during the winter, mid-January and mid-February. The January period provided the best ice and five samples were studied in detail. One sample, number 6, was collected during March for detailed study. All samples were collected to correlate with unique test pile (see 10.6) data. The first day of test pile data collection produced the most important bit of record for the season. On this day, 22 January, ice was sampled, numbers 4 and 5, which appeared to best match this record.

The samples were collected, flown directly to Anchorage by helicopter and stored in a deepfreeze until tested. Compression tests, salinity tests and crystallographic thin sections were run on each of the six samples.

10.5.4 Ice Strength Testing, 1964-65. Six large field samples were collected, and direct compression strengths were determined over a range of load rates and temperatures. Five samples (1-5) were collected in conjunction with force measurements on MGS-A, the completed structure. Previous test pile results indicated loads or forces at high load rates to be about one-half of those at low load rates. The results of the load rate-strength data show this clearly in Figure 10.12. The dotted line denotes Arctic sea ice properties as determined from slower load rates. It should be noted that the actual strength of this particular ice is much lower than average for Cook Inlet ice and the temperature effect is very slight, due to the low salinities (less than 2 parts per thousand). There were three ice growth periods during the winter, and these samples were taken on 16 and 20 February, during the third growth period. Onsite observations and impressions indicated the highest ice strengths during the first period, with the second and third periods producing increasingly weaker ice.

10.6 LATERAL ICE FORCES ON PILING

10.6.1 Field Measurements. A test pile was erected on the temporary drilling platform previously shown. Figure 10.13 shows the test pile for this project at the right side of the figure. It was a 36 inch diameter, 20 foot long cylinder supported as a simple beam. The lower hinge was a piece of 3/4 inch plate which also served to support the pile vertically. The upper end was unsupported either vertically or horizontally except by a 300,000 pound load cell and adequate rigging to prevent its being pushed over.

The second test pile shown in Figure 10.13, erected by others, is of cantilever design. It was totally collapsed by ice forces before useful data could be acquired from it. The simple beam test pile facility was destroyed when the entire platform failed and disappeared in December 1964.

Several interesting factors were observed. First, and most important, is that the largest ice forces occurred when the ice velocity was very slow or zero. The action seen in Figure 10.14, Case J, occurred with a change in velocity of from 3 or 4 miles per hour to zero. In Figure 10.14, the trace runs from left to right and from top to bottom. Starting with the upper left corner (Point C), the ice velocity is high but slowing-down by point D. This slowing resulted from the breaking away of a large chunk of the ice floe which had already passed the platform and thus ceased pulling the floe past the platform. From point E to F on the



Detailed Ice Failure I, Note the Bern of Broken Ice on Each Side of Path.

Figure 10.9



Detailed Ice Failure II, Note the Small Size of Crushed Ice.

Figure 10.10



Detailed Ice Failure III, Note the Rolling Bern of Broken Ice.

Figure 10.11

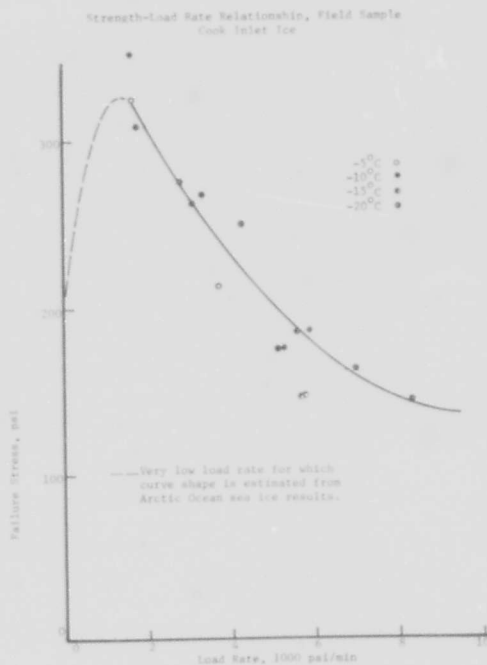


Figure 10.12

record is the slowing of the floe to a complete stop at about point F. Very little motion or ice breakage occurred between points B-A and F. This slow ratcheting failure is characteristic of all the low velocity failure experienced during the winter. This floe seemed to be uniform in thickness over its entire area.

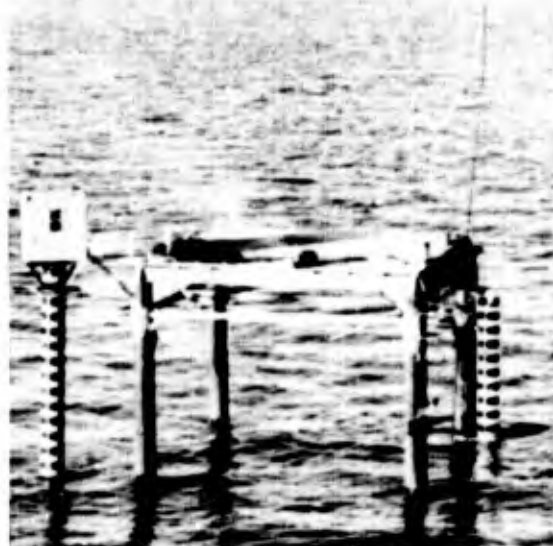
Slow, ratcheting failure was also experienced by small floes which were held against the test pile by currents which were insufficient to fail the ice. If this floe were struck by another, a substantial amount of ratcheting failure occurred until eventually, enough ice was backed up-stream to provide adequate force to increase the velocity. Then the forces were reduced.

This mode of ice failure produces severest structural loading and occurs with very small rates of loading. The actual rate of loading for this type of failure has not been measured, but it is believed that the failure occurs at velocities between virtually zero and 50 feet per minute. Normal high velocity failures may be as high as 600 feet per minute. The ratcheting failure appears to occur only at low ice temperatures and has been recorded only twice, once in early 1964 on the test pile at MGST 1 and once in late 1964 on MGS-A. The replotted MGS-A record is shown in Figure 10.15. Reasonably accurate values for resonant structural frequency were available for MGS-A, but not for MGST-1. The MGS-A ratcheting ice failure frequency and the resonant structural frequency are nearly identical at 1.2 cycles per second. This is very important if the mechanism is forced, poorly damped, resonant vibration caused by an oscillatory failure of the ice which happens to occur at the same frequency as the resonant structural frequency. Laboratory studies, reported below, indicate the vibrations to be forced, but that damping is too great to allow significant amplification.

A 2:1 ratio of ratcheting induced forces to high velocity induced forces is a consistent value found in results of direct compression tests, test pile data, MGS-A data and laboratory pile loading data. The ratio is thus found both in static and dynamic situations and clearly shows this to be a load rate effect of the ice rather than resonant amplification of structural stresses.

10.6.2 Oscillatory Forces.

1. Laboratory Measurements. The experimental set up is shown in Figure 10.16. The ice was frozen in place with the tank and associated equipment in a cold lab. The full ice sheet was cut into four smaller pieces which could be forced past the pile by the variable speed drive equipment. Each small "floe" was failed at a very slow velocity for half its length and then at the highest velocity which the equipment was capable of producing for the second half. The forces were determined by SR-4 strain gage measurements of the cantilevered, fixed end, one inch diameter pile. Various test sections were mounted at the top of the pile; single piles of 1/4, 1/2, 1 and 2 inch diameters and double piles of the identical diameters and variable spacing.
2. Data Evaluation. Precision measurement of the ice thickness was impractical; therefore, all forces are related to those of a one inch diameter pile at high velocity failure. This base run was



Test Pile Installation. The Test Pile used is on the Right and is a Simple Beam

Figure 10.13



Test Pile Force Records, Oscillograph Case J.

Figure 10.14

Ratcheting Failure
MIS A, 29 December, 1964
Case 31-A

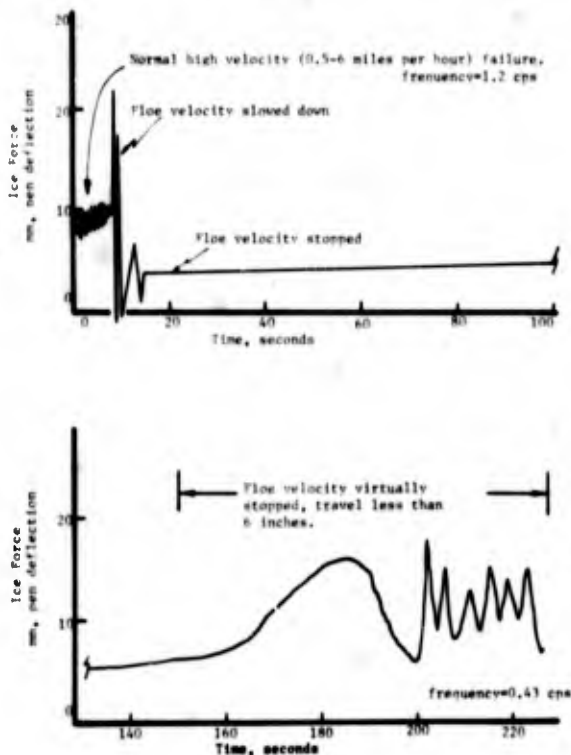


Figure 10.15

Experimental Equipment
Laboratory Pile Study

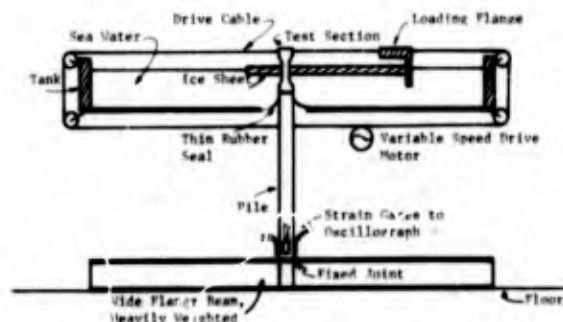


Figure 10.16

made on each new tank of ice and provided adequate references for force and stress values.

The ice was not identical from day to day; therefore, the ratio of the failure stress at high velocity to that at low velocity is more meaningful than either of the absolute values.

3. Loading Rate. The loading rate effect was clearly shown by experiments and was very similar to the effects observed on the platforms and to those of the direct compression tests in the laboratory. This feature is shown in Figure 10.17 by the decreasing ratio of the ice failure stress for high load rate (σ_f) to the failure stress for low load rate (σ_s). The 2:1 ratio of low velocity to high velocity failure was reproduced and substantiated similar results by other methods of measurement.
4. Superstructure Mass Effect. This parameter was studied by adding weights to the top of the pile test section. The results are shown in Figure 10.18. These tests were run only on the one inch diameter section only and are shown for the slow velocity failure as a failure stress ratio using the unweighted one inch test section (σ_s) as 100%. There is no appreciable effect within the range of the experiments.

There is a slight reduction in failure stress with increased superstructure weight, but the effect is very small. The range of superstructure masses used would be equivalent to the deck weights of MGS-A which range from zero to approximately 5000 tons. Therefore, the deckmass parameter has a negligible effect on ice failure stress at the slow velocities within the scope of these tests. This result should be studied further with particular emphasis on low ice temperatures (σ_s) where ratcheting failure has been observed in the field.

5. Vibration. The results concerning oscillating ice forces and structural vibration are shown in Figure 10.19. The most severe restraint of the present design criteria is that of ratcheting ice failure which occurs frequently at very low ice velocities. The slow speed experimental tests duplicated the ratcheting failure for all pile sizes and spacings and were easily induced. All of the data in Figure 10.19 are of the ratcheting type and it is easily seen that the frequency of this type failure is not matched to the resonant frequency of the structure but rather is a characteristic of the ice. It will be further noted that the frequency associated with the laboratory grown ice is approximately 5 cycles per second with the spread in data decreasing with increased "deck mass". It is doubtful that the decrease in data spread is due to decreasing resonant frequency per se, but rather is apparently dependent on the structural mass, structural time response, and ice failure force relationships. The difference between the experimental value of approximately 5 cps as compared with approximately 1 cps for the prototypes is most probably due to the differences in the ice. It was not possible to

Load Rate Effect Laboratory Experiments
Single 1" Diameter Leg

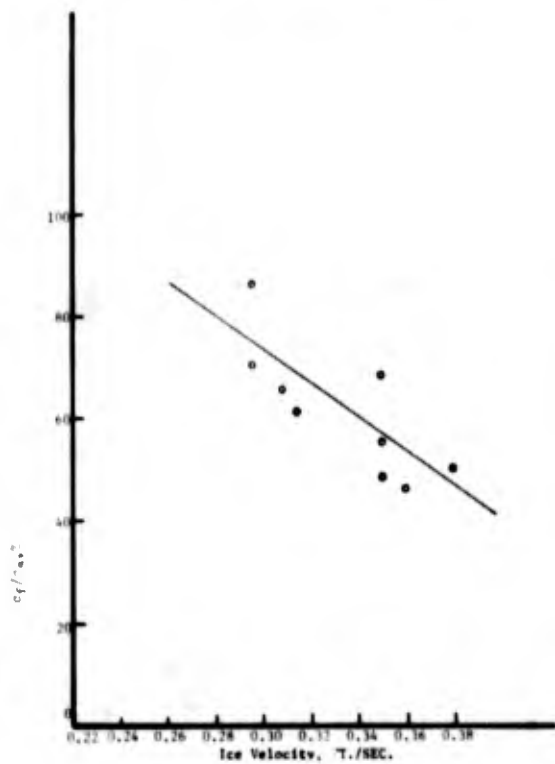


Figure 10.17

Resonant Frequency of Structure and Oscillating Ice Force Frequency
Slow Velocity, Ratcheting Type Failure

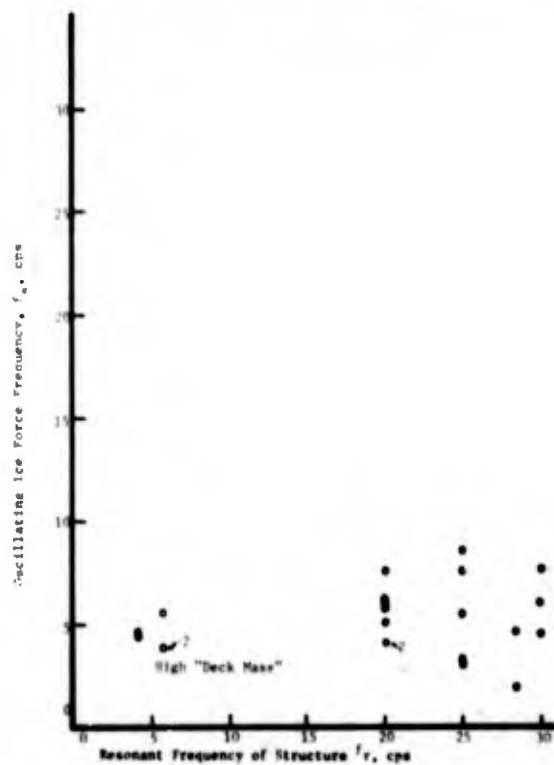


Figure 10.18

Structural Mass Effect, 1" Diameter Leg,
Ice Force Factor

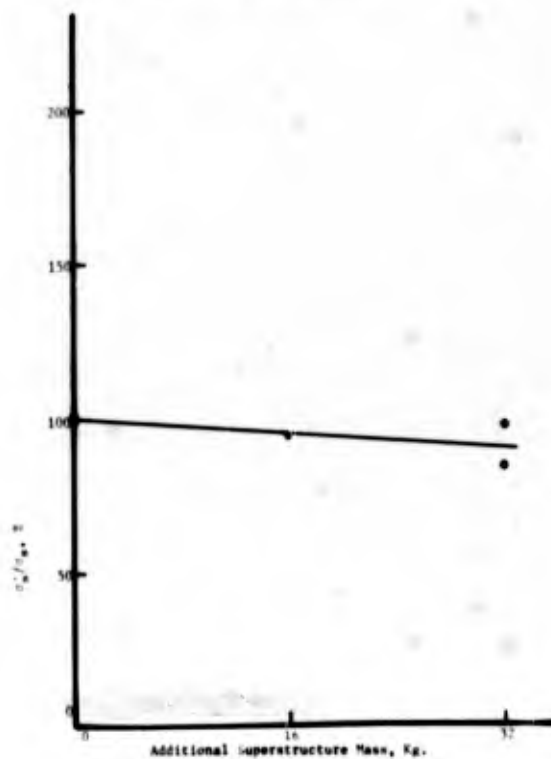


Figure 10.19

experiment with lower ice temperatures, but it should be expected that there is a frequency-temperature relationship due to the large changes in ice properties with varying temperature. It should be noted that earlier the ratcheting frequency was speculated to be generated by the resonant frequency of the structure; this must now be seriously questioned. The two data records from prototypes showing ratcheting failure frequencies which were nearly equal to the structural resonant frequencies could now be considered coincidence. It is of considerable importance, however, to be aware of the high probability of the ratcheting failure's matching the structural resonant frequency.

There does exist a possibility for forced, damped, resonant vibration of platforms at a time of very large ice forces. This, of course, is not a trivial matter. The degree of damping to be expected is variable between structures and is probably most dependent upon structural deflection in the water and water displacement per cycle. The extent to which damping is accurately included in the two prototype records is not known. None of the experimental data show the characteristic forced resonant vibration amplification, through the experimental device had far less damping than the prototypes. All evidence, thus far indicates the damping to be great, and the amplification due to forced vibration is insignificant. The 2:1 ratio of low to high speed failure stresses is further substantiation of the validity of a load rate function concept as seen in Figure 10.12.

EXHIBITS

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EXHIBIT 1.2

DATA CODE

The data shown in Exhibit 1.2.1 is a summary of values calculated from the experimental data shown in Exhibit A. This summary includes the mechanical properties of failure strength and stiffness, the test parameters of temperature and load rate, and many physical properties of the ice.

A specimen of the data is shown below. The decimal is omitted in the data and immediately below each "word" in the specimen below is the word number.

12250	26390	11	8080	11	531	210	10000	8230	5400	Word
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)			Word Number
1	0	0	2	1	4	1	0			Decimal place

Word Meaning

- 1 Identification number.
2 bcdeeff

b = date of collection

- 2 1 Nov-31 Dec
3 1 Jan-31 Apr
4 1 May-15 May
5 16 May-31 May
6 1 June-15 June
7 16 June-1 Aug
8 1 Aug-31 Oct

c = location of collection

- 1 100 yards of theater
2 1 mile off ACS
3 100 miles north of Barrow
4 200 miles north of Barrow
5 100-150 yards north of theater, 1961
6 300 yards north of theater

d = crystal type code

- 1 fine
2 medium
3 center
4 bottom
5 pack

ee - angle between sigma and zenith, 0° to 90°
ff - angle between sigma and c-axis, 0° to 90°
"11" indicates randomness

Word Meaning

- 3 ghhlj

g = failure type

<u>Code</u>	<u>Tension meaning</u>	<u>Compression meaning</u>
1	good test	no visible deformation
2	weld failure	tensile failure

3	head failure	head failure
4	no failure	plastic failure
5	not used	no information
6	"	bad test
7	"	bulge failure
8	"	explosive failure
9	"	ring around specimen

hh - age of sample at time of test, days.

\overline{II} - depth from top of ice to center of specimen, inches.

\overline{I} - type of test, "1" is compression, "2" is tension

- 4 Chlorinity o/oo
- 5 Temperature -°C.
- 6 Modulus of Elasticity, psi x 10⁵.
- 7 Failure Strength, psi.
- 8 Rate of Loading, psi/min.

EXHIBIT 1-1 COMPRESSION DATA, REDUCED

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
0009.0	.3120000	.500081	4.54	18.9	10.00	405.00	
0010.0	.3120000	.500081	5.34	16.8	35.00	413.00	
0011.0	.3120000	.500081	4.18	16.3	89.00	410.00	
0012.0	.3120000	.500081	5.11	16.8	88.00	509.00	
0014.0	.3120000	.502081	4.44	18.9	79.00	540.00	
0015.0	.3120000	.502081	4.71	18.9	560.00	785.00	
0017.0	.3120000	.500081	5.09	21.0	82.00	461.00	
0019.0	.3120000	.500081	5.22	21.0	590.00	889.00	
0020.0	.3120000	.500081	4.07	21.0	30.00	436.00	
0021.0	.3120000	.500081	4.72	21.0	700.00	886.00	
0022.0	.3120000	.501031	4.49	21.0	260.00	892.00	
0027.0	.3120000	.501081	6.70	21.0	1230.00	894.00	
0030.0	.3120000	.501081	4.57	14.0	2200.00	742.00	
0041.0	.3120000	.500081	4.00	10.0	80.00	747.00	
7042.0	.3120000	.500081	4.05	10.0	510.00	628.00	
7043.0	.3120000	.500081	4.21	10.0	1320.00	831.00	
7044.0	.3120000	.500081	3.60	10.0	250.00	445.00	
0046.0	.3130000	.500081	4.77	10.0	300.00	457.00	
0047.0	.3130000	.500081	3.76	18.9	470.00	872.00	
0050.0	.3130000	.500081	3.46	18.9	2200.00	582.00	
0051.0	.3130000	.500081	3.78	18.9	470.00	920.00	
0057.0	.3130000	.501081	3.89	21.0	510.00	551.00	
0058.0	.3130000	.501081	5.32	21.0	85.00	953.00	
0059.0	.3130000	.501081	4.54	21.0	34.00	929.00	
0060.0	.3140000	.500481	2.23	14.3	71.00	1270.00	
0061.0	.3140000	.500481	2.27	14.3	860.00	1040.00	
0062.0	.3140000	.500481	2.46	14.3	93.00	544.00	
0063.0	.3140000	.500481	2.52	14.3	560.00	1003.00	
0064.0	.3140000	.500481	2.33	14.3	990.00	1007.00	
0065.0	.3140000	.500481	2.61	14.3	91.00	806.00	
0066.0	.3140000	.500481	2.30	14.3	95.00	800.00	
0071.0	.3140000	.500481	2.41	10.0	87.00	1330.00	
0072.0	.3140000	.500481	2.19	10.0	610.00	578.00	
0073.0	.3140000	.500481	1.92	10.0	48.00	738.00	
0077.0	.3140000	.500681	2.72	6.00	94.00	1143.00	
0078.0	.3140000	.500681	2.96	6.00	600.00	795.00	
0079.0	.3140000	.501681	1.94	6.00		120.00	01.10000
0081.0	.3149000	.500481	1.86	6.00	120.00	850000	475.00
0084.0	.3149000	.500681	1.82	6.00	82.00	500000	105.00
0085.0	.3149000	.500681	1.82	6.00	970.00	8.60000	733.00
0086.0	.3149000	.500681	1.99	6.00	920.00	6.20000	958.00
0087.0	.3149000	.500681	1.99	6.00	660.00	1.40000	240.00
0088.0	.3149000	.500681	1.99	6.00	1000.00		917.00
0089.0	.3149000	.500681	4.06	14.3	93.00	455.00	
0097.0	.3130000	.500081	4.36	14.3	540.00	741.00	
0098.0	.3130000	.500081	4.36	14.3	93.00	476.00	
0099.0	.3130000	.500081	3.87	14.3	157.00	622.00	
0103.0	.3130000	.501081	3.97	14.3	157.00	6.20000	477.00
0104.0	.3130000	.501081	14.3	150.00		1.00000	338.00
0105.0	.3130000	.501081	4.80	14.3	134.00	1.30000	514.00
0107.0	.3130000	.501081	14.3	165.00			917.00
7108.0	.3130000	.500081	5.28	14.3	1060.00	1.40000	530.00
0109.0	.3134545	.500081	5.78	14.3	800.00	1.90000	376.00
0119.0	.3225011	.500081	1.00	14.3	520.00		667.00
7110.0	.3120000	.500081	5.28	14.3	1000.00		494.00
0120.0	.3229000	.500081	0.70	14.3	88.00	1.10000	416.00
0121.0	.3229000	.500081	0.70	14.3	480.00		262.00
0122.0	.3220000	.500081	0.70	14.3	480.00		403.00
0123.0	.3249000	.501681	1.15	14.3	740.00		227.00
0126.0	.3249000	.501681	1.15	14.0	125.00		587.00
0128.0	.4120000	.500081	5.13	14.3	245.00		680.00
0131.0	.4120000	.501081	6.56	14.3	580.00	1.50000	756.00
0132.0	.4129000	.501081	4.89	14.3	930.00	1.80000	676.00
0134.0	.4130000	.500081	4.43	14.3	1000.00		388.00
0136.0	.4139000	.500081	4.43	14.3	143.00		470.00
0139.0	.4130611	.502081	3.29	16.9	45.00		429.00
0149.0	.4139000	.500081	4.54	6.00	680.00		375.00
0151.0	.4139000	.500081	3.30	6.00	825.00	1.20000	608.00
0197.0	.5149000	.500681	2.49	6.00	840.00	1.00000	599.00
0199.0	.5149000	.500681	2.49	6.00	910.00	1.40000	274.00
0161.0	.5149045	.500681	2.49	6.00	870.00	2.10000	1345.00
0166.0	.5140000	.500681	2.93	6.00	1060.00	7.30000	303.00
0196.0	.5120000	.500081	3.98	2.00	470.00		9.20000
0197.0	.5120000	.500081	3.98	2.00	940.00	1.00000	598.00
0198.0	.5120000	.500081	3.98	2.00	880.00	1.00000	147.00
0199.0	.5120000	.500081	2.36	2.00	440.00	2.30000	410.00
0200.0	.5120000	.500081	2.36	2.00	735.00	1.90000	118.00
0201.0	.5129000	.500081	2.36	2.00	295.00	1.50000	229.00
0202.0	.5129000	.500081	2.36	2.00	785.00	2.00000	886.00
0203.0	.5120000	.500081	2.36	2.00	880.00	1.90000	168.00
0204.0	.5129000	.500081	2.36	2.00	550.00		743.00
0207.0	.5140000	.500681	2.90	2.00	530.00		1.40000
0208.0	.5140000	.500681	2.90	2.00	980.00		738.00
0209.0	.5140000	.500681	2.90	2.00	520.00		2.60000
0210.0	.5140000	.500681	2.90	2.00	960.00		231.00
0211.0	.5149000	.501681	2.13	2.00	740.00	1.90000	469.00
0212.0	.5149000	.501681	2.13	2.00	740.00	1.90000	163.00
0213.0	.5149045	.501681	2.13	2.00	740.00	1.40000	146.00
0214.0	.5149000	.500681	2.19	2.00	175.00		340000
0215.0	.5149000	.501681	2.19	2.00	120.00		800000
0216.0	.5140045	.501681	2.19	2.00	160.00		4.40000
0217.0	.5140090	.501681	1.68	2.00	184.00		650000
0219.0	.5149000	.501681	2.50	2.00	680.00		340000
7220.0	.5149000	.502681	2.50	2.00	600.00		190000
0221.0	.5149045	.502681	2.50	2.00	450.00		477.00
0222.0	.5140090	.501161	1.21	1.00	530.00		413.00
0223.0	.5140090	.501161	1.21	1.00	510.00		1.50000
0224.0	.5140090	.501101	1.21	1.00	740.00		1.50000
0225.0	.5140090	.501141	1.21	1.00	1060.00		.760000
0226.0	.5140090	.502141	1.21	1.00	184.00		1.20000
0228.0	.5149000	.502121	2.44	1.00	580.00		1.60000
0229.0	.5149045	.502121	2.44	1.00	140.00		4.50000
0230.0	.5149090	.502121	2.44	1.00	140.00		4.50000
0231.0	.5149000	.502121	2.64	1.00	170.00		2.20000
0232.0	.5149045	.502121	2.64	1.00	33.00		1.20000
0233.0	.5140090	.501601	2.58	1.00	560.00		587.00
0234.0	.5140090	.501601	2.58	1.00	870.00		1.00000
0235.0	.5149090	.501601	2.58	1.00	960.00		1.20000
0236.0	.5149000	.501601	2.58	1.00	680.00		.710000
0237.0	.5149045	.502601	2.58	1.00	675.00		.280000
0238.0	.5149090	.501501	2.74	1.00	132.00		.460000
0239.0	.5149000	.501501	2.74	1.00	140.00		.380000
0240.0	.5149045	.501501	2.74	1.00	130.00		.160000
0241.0	.5149090	.503121	2.50	1.00	480.00		.340000
0242.0	.5140090	.501501	.872	1.00	95.00		166.00
0243.0	.5140090	.501501	.872	1.00	110.00		340000
0244.0	.5140090	.501501	.872	1.00	110.00		2.00000
0245.0	.5140000	.503121	.250	1.00	660.00		.930000
0246.0	.5149045	.503121	.250	1.00	660.00		.340000
0247.0	.5149090	.504121	.250	1.00	111.00		.390000
0248.0	.5149000	.504121	.250	1.00	140.00		1.00000
0249.0	.5149045	.504121	.250	1.00	180.00		1.00000
0250.0	.5140090	.501081	.050	2.00	520.00		577.00
0251.0	.5140090	.502081	.050	2.00	1040.00		680.00
0252.0	.5140090	.501081	.050	2.00	83.00		288.00
0253.0	.5140090	.501081	.050	2.00	560.00		499.00
0254.0	.5140090	.502081	.050	2.00	920.00		312.00
0255.0	.5140090	.501081	.050	2.00	520.00		225.00
0256.0	.5140090	.501081	.050	2.00	540.00		532.00
0257.0	.5140090	.501081	.050	2.00	1120.00		600.00
0258.0	.5140090	.500081	.050	2.00	41.00		341.00
0259.0	.5140090	.502181	.050	2.00	53.00		295.00
0260.0	.5140090	.502181	.050	2.00	580.00		702.00
0261.0	.5140090	.502181	.050	2.00	1080.00		620.00
0262.0	.5140090	.503181	.050	2.00	620.00		441.00
0263.0	.5140090	.503181	.050	2.00	480.00		379.00
0264.0	.5140090	.503181	.050	2.00	1020.00		530.00
0265.0	.5140090	.503181	.050	2.00	480.00		371.00
0266.0	.5140090	.502181	.050	2.00	540.00		488.00
0267.0	.5140090	.502181	.050	2.00	950.00		400.00
0268.0	.5140090	.505081	.400	10.0	40.00		322.00
0269.0	.5140090	.504681	.400	10.0	330.00		453.00
0270.0	.5140090	.505081	.400	10.0	1040.00		734.00
0271.0	.5140090	.505081	.400	10.0	46.00		229.00
0272.0	.5140090	.505081					

EXHIBIT 1-1 COMPRESSION DATA, REDUCED

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
0009.0	.2120000	.500081	4.54	16.9	30.00	405.00	
0010.0	.2120000	.500081	5.39	16.8	35.00	413.00	
0011.0	.2120000	.500081	4.18	16.3	29.00	410.00	
0012.0	.2120000	.500081	5.11	16.8	28.00	509.00	
0014.0	.3120000	.502081	4.44	18.7	79.00	540.00	
0015.0	.3120000	.502081	4.71	18.9	98.00	785.00	
0017.0	.3120000	.500081	5.09	21.0	82.00	461.00	
0018.0	.3120000	.500081	5.22	21.0	99.00	889.00	
0020.0	.3120000	.500081	4.07	21.0	30.00	436.00	
0021.0	.3120000	.500081	4.72	21.0	70.00	886.00	
0023.0	.3120000	.501081	4.49	21.0	260.00	692.00	
0027.0	.3120000	.501081	6.70	21.0	123.00	894.00	
0030.0	.3120000	.501081	4.57	14.0	220.00	742.00	
0041.0	.3120000	.500081	4.00	10.0	81.00	347.00	
0042.0	.3120000	.500081	4.85	10.0	510.00	628.00	
0045.0	.3120000	.500081	4.21	10.0	132.00	831.00	
0046.0	.3130000	.500081	3.60	10.0	250.00	445.00	
0047.0	.3130000	.500081	4.77	10.0	36.00	457.00	
0050.0	.3130000	.500081	3.46	18.9	220.00	872.00	
0051.0	.3130000	.500081	3.76	18.9	470.00	582.00	
0057.0	.3130000	.501081	3.39	21.0	510.00	920.00	
0058.0	.3130000	.501081	3.39	21.0	85.00	551.00	
0059.0	.3130000	.501081	4.44	21.0	34.00	553.00	
0060.0	.3140000	.500481	2.23	14.3	71.00	929.00	
0061.0	.3140000	.500481	2.27	14.3	660.00	1270.00	
0062.0	.3140000	.500481	7.46	14.3	93.00	1040.00	
0063.0	.3140000	.500481	2.52	14.3	560.00	544.00	
0064.0	.3140000	.500481	2.33	14.3	990.00	1063.00	
0065.0	.3140000	.500481	2.63	14.3	91.00	1074.00	
0066.0	.3140000	.500481	2.30	14.3	55.00	808.00	
0071.0	.3140000	.500481	2.41	10.0	67.00	800.00	
0072.0	.3140000	.500481	2.19	10.0	610.00	1330.00	
0073.0	.3140000	.500481	1.92	10.0	48.00	576.00	
0077.0	.3140000	.500601	2.72	6.00	94.00	738.00	
0078.0	.3140000	.500601	2.96	6.00	600.00	1143.00	
0079.0	.3140000	.501601	1.94	6.00		795.00	
0083.0	.3149000	.500601	1.86	6.00	120.00	51.1000	329.00
0084.0	.3149000	.500601	1.86	6.00	130.00	860000	475.00
0085.0	.3149000	.500601	1.86	6.00	82.00	500000	105.00
0086.0	.3149000	.500601	1.99	6.00	970.00	8.60000	733.00
0087.0	.3149000	.500601	1.99	6.00	920.00	6.28000	950.00
0088.0	.3149000	.500601	1.99	6.00	660.00	1.40000	240.00
0089.0	.3140000	.500601	1.99	6.00	100.00		917.00
0097.0	.3130000	.500081	4.06	14.3	93.00		455.00
0098.0	.3130000	.500081	4.26	14.3	540.00		741.00
0099.0	.3130000	.500081	3.87	14.3	93.00		476.00
0101.0	.3130000	.501081	3.97	14.3	157.00		622.00
0104.0	.3139000	.501081	1.43	150.00		6.20000	477.00
0105.0	.3139000	.501081	4.80	14.3	134.00	1.00000	338.00
0107.0	.3139000	.501081	1.43	165.00		1.70000	514.00
0108.0	.3139000	.500081	5.28	14.3	106.00		917.00
0109.0	.314545	.500081	5.28	14.3	600.00	1.40000	530.00
0119.0	.3220011	.500081	1.00	14.3	520.00	1.90000	376.00
0110.0	.3129000	.500081	5.28	14.3	100.00		667.00
0120.0	.3220000	.500081	0.70	14.3	88.00		494.00
0121.0	.3229000	.500081	0.70	14.3	89.00	1.10000	416.00
0122.0	.3220000	.500081	0.70	14.3	480.00		262.00
0125.0	.3249000	.501601	1.15	14.3	740.00		403.00
0126.0	.3249000	.501601	1.15	14.0	125.00		227.00
0128.0	.4120000	.500081	5.13	14.3	245.00		587.00
0131.0	.4120000	.501081	5.56	14.3	580.00		680.00
0132.0	.4129000	.501081	5.56	14.3	1030.00	1.50000	750.00
0134.0	.4130000	.501081	4.89	14.3	930.00	1.80000	676.00
0136.0	.4139000	.500081	4.43	14.3	143.00	.710000	388.00
0139.0	.4130011	.502081	1.29	14.3	45.00		470.00
0149.0	.4139000	.500081	4.54	6.00	480.00		429.00
0151.0	.4139000	.500081	5.40	6.00	825.00	1.20000	375.00
0157.0	.5149000	.500601	2.49	6.00	840.00	1.00000	608.00
0159.0	.5149000	.500601	2.49	6.00	910.00	1.40000	559.00
0161.0	.5149000	.500601	2.49	6.00	870.00	2.10000	278.00
0166.0	.5140000	.500601	2.93	6.00	160.00	7.30000	1345.00
0196.0	.5120000	.500081	3.98	2.00	470.00		303.00
0197.0	.5120000	.500081	3.98	2.00	540.00	9.20000	741.00
0198.0	.5120000	.500081	3.98	2.00	890.00	1.00000	598.00
0199.0	.5120000	.500081	2.36	2.00	440.00	.230000	147.00
0200.0	.5120000	.500081	2.36	2.00	735.00	1.90000	410.00
0201.0	.5129000	.500081	2.36	2.00	295.00	.150000	116.00
0202.0	.5129000	.500081	2.36	2.00	765.00	2.00000	225.00
0203.0	.5120000	.500081	2.36	2.00	880.00	1.50000	866.00
0204.0	.5129000	.500081	2.36	2.00	550.00	.190000	168.00
0207.0	.5140000	.500601	2.90	2.00	530.00		743.00
0208.0	.5140000	.500601	2.90	2.00	980.00	1.40000	1013.00
0209.0	.5140000	.500601	2.90	2.00	520.00		739.00
0210.0	.5140000	.500601	2.90	2.00	960.00	2.60000	901.00
0211.0	.6149000	.501601	2.13	2.00	600.00		231.00
0212.0	.6149000	.501601	2.13	2.00	740.00	1.90000	489.00
0213.0	.6149000	.501601	2.13	2.00	740.00	1.90000	163.00
0214.0	.6149000	.500601	2.19	2.00	175.00	1.40000	146.00
0215.0	.6149000	.501601	2.19	2.00	120.00	.340000	118.00
0216.0	.6140000	.501601	2.19	2.00	160.00	.600000	109.00
0217.0	.6140000	.501601	1.68	2.00	184.00	4.40000	765.00
0219.0	.6149000	.501601	2.50	2.00	680.00	.650000	650.00
0220.0	.6149000	.502601	2.50	2.00	600.00	.340000	499.00
0221.0	.6149000	.502601	2.50	2.00	460.00	.190000	153.00
0222.0	.6140000	.501141	1.21	1.00	530.00		477.00
0223.0	.6140000	.501141	1.21	1.00	510.00		413.00
0224.0	.6140000	.501141	1.21	1.00	740.00	1.60000	411.00
0225.0	.6140000	.501141	1.21	1.00	1060.00	.760000	492.00
0226.0	.6140000	.502141	1.21	1.00	184.00		245.00
0228.0	.6149000	.501121	2.64	1.00	580.00	.690000	204.00
0229.0	.6149000	.501121	2.64	1.00	580.00	.160000	143.00
0230.0	.6149000	.502121	2.64	1.00	140.00	.450000	79.00
0231.0	.6149000	.502121	2.64	1.00	120.00	.220000	92.00
0232.0	.6149000	.502121	2.64	1.00	330.00	.120000	47.00
0233.0	.6140000	.501601	2.58	1.00	660.00		587.00
0234.0	.6140000	.501601	2.58	1.00	870.00	1.00000	385.00
0235.0	.6149000	.501601	2.58	1.00	960.00	1.20000	429.00
0236.0	.6149000	.501601	2.58	1.00	880.00	.710000	293.00
0237.0	.6149000	.502601	2.58	1.00	675.00	.280000	103.00
0238.0	.7149000	.501501	7.40	1.00	132.00	.460000	256.00
0239.0	.7149000	.501501	7.40	1.00	140.00	.380000	267.00
0240.0	.7149000	.501501	7.40	1.00	130.00	.160000	71.00
0244.0	.7149000	.503121	2.50	1.00	480.00	.740000	166.00
0242.0	.7140000	.501501	8.70	1.00	95.00		370.00
0241.0	.7140000	.501501	8.70	1.00	110.00	.340000	330.00
0245.0	.7149000	.503121	2.50	1.00	660.00	2.30000	198.00
0246.0	.7149000	.503121	2.50	1.00	940.00	.930000	150.00
0247.0	.7149000	.504121	2.50	1.00	111.00	.340000	289.00
0248.0	.7149000	.504121	2.50	1.00	1.00	.390000	315.00
0249.0	.7149000	.504121	2.50	1.00	5.00	1.00000	111.00
0250.0	.7140000	.501081	0.50	2.00	1.00		577.00
0251.0	.7140000	.502081	0.50	2.00	16.00		680.00
0252.0	.7140000	.501081	0.50	2.00	83.00		288.00
0253.0	.7140000	.501081	0.50	2.00	560.00		499.00
0254.0	.7140000	.502081	0.50	2.00	920.00		312.00
0255.0	.7140000	.501081	0.50	2.00	52.00		225.00
0256.0	.7140000	.501081	0.50	2.00	540.00		532.00
0257.0	.7140000	.501081	0.50	2.00	112.00		600.00
0258.0	.7140000	.500081	0.50	2.00	41.00		341.00
0259.0	.7140000	.502181	0.50	2.00	53.00		295.00
0260.0	.7140000	.502181	0.50	2.00	550.00		702.00
0261.0	.7140000	.502181	0.50	2.00	108.00		623.00
0262.0	.7140000	.503181	0.50	2.00	62.00		441.00
0263.0	.7140000	.503181	0.50	2.00	480.00		379.00
0264.0	.7140000	.503181	0.50	2.00	102.00		530.00
0265.0	.7140000	.503181	0.50	2.00	46.00		371.00
0266.0	.7140000	.502181	0.50	2.00	560.00		408.00
0267.0	.7140000	.502181	0.50	2.00	950.00		400.00
0268.0	.7140000	.505081	0.50	10.0	40.00		322.00
0269.0	.7140000	.504081	0.50	10.0	330.00		453.00
0270.0	.7140000	.505081	0.50	10.0	164.00		754.00
0271.0	.7140000	.505081	0.50	10.0	46.00		22

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
0322.0	7149045	500181	1.30	1.20	170.0	230000	153.00
0323.0	7149045	500181	1.30	1.00	99.00	332000	260.00
0324.0	7149045	500181	1.30	1.00	78.00	336000	321.00
0325.0	7149045	500181	1.30	1.00	38.00	450000	89.00
0326.0	7149045	500181	1.10	2.00	300.0	1.00000	437.00
0327.0	7149045	500181	1.10	2.00	190.0	4.10000	610.00
0328.0	7149045	500181	1.10	2.00	71.00	900000	103.00
0329.0	7149045	500181	1.10	2.00	190.0	1.00000	570.00
0330.0	7149045	500181	1.10	2.00	330.0	2.40000	575.00
0331.0	7149045	500181	1.10	2.00	139.0	1.00000	242.00
0332.0	7149045	500181	1.10	2.00	210.0	2.50000	770.00
0333.0	7149045	500181	1.10	2.00	150.0	1.30000	345.00
0334.0	7149045	500181	1.10	2.00	179.0	0.98000	617.00
0335.0	7149045	500181	1.10	2.00	187.0	1.30000	539.00
0336.0	7149045	500181	1.10	2.00	110.0	0.70000	220.00
0337.0	7149045	500181	1.10	2.00	300.0	2.00000	1030.00
0338.0	7149045	500181	1.10	2.00	290.0	0.70000	611.00
0339.0	7149045	500181	1.10	2.00	114.0	1.70000	250.00
0340.0	7149045	500181	1.10	2.00	105.0	1.20000	353.00
0341.0	7149045	500181	1.10	2.00	320.0	3.30000	616.00
0342.0	7149045	500181	1.10	2.00	100.0	0.80000	142.00
0343.0	7149045	500181	1.10	2.00	0.00	0.50000	150.00
0344.0	7149045	500181	1.10	2.00	0.00	0.83000	181.00
0345.0	7149045	500181	1.10	2.00	140.0	0.90000	611.00
0346.0	7149045	500181	1.10	2.00	110.0	0.49000	340.00
0347.0	7149045	500181	1.10	2.00	88.0	0.84000	124.00
0348.0	7149045	500181	1.10	2.00	68.0	0.95000	86.00
0349.0	7149045	500181	1.10	2.00	145.0	1.70000	486.00
0350.0	7149045	500181	1.10	2.00	100.0	0.29000	63.00
0351.0	7149045	500181	1.10	2.00	89.0	0.57000	57.00
0352.0	7149045	500181	1.10	2.00	163.0	0.20000	135.00
0353.0	7149045	500181	1.10	2.00	160.0	0.56000	192.00
0354.0	7149045	500181	1.10	2.00	140.0	1.10000	255.00
0355.0	7149045	500181	1.10	2.00	130.0	0.53000	364.00
0356.0	7149045	500181	1.10	2.00	49.0	0.50000	90.00
0357.0	7149045	500181	1.10	2.00	62.0	0.56000	59.00
0358.0	7149045	500181	1.10	2.00	115.0	0.29000	55.00
0359.0	7149045	500181	1.10	2.00	101.0	0.48000	210.00
0360.0	7149045	500181	1.10	2.00	138.0	0.51000	302.00
0361.0	7149045	500181	1.10	2.00	93.0	0.27000	263.00
0362.0	7149045	500181	1.10	2.00	132.0	1.70000	486.00
0363.0	7149045	500181	1.10	2.00	100.0	1.20000	339.00
0364.0	7149045	500181	1.10	2.00	167.0	0.62000	670.00
0365.0	7149045	500181	1.10	2.00	0.00	0.468.00	468.00
0366.0	7149045	500181	1.10	2.00	98.0	0.39000	362.00
0367.0	7149045	500181	1.10	2.00	137.0	0.60000	500.00
0368.0	7149045	500181	1.10	2.00	78.0	0.27000	177.00
0369.0	7149045	500181	1.10	2.00	97.0	0.42000	158.00
0370.0	7149045	500181	1.10	2.00	106.0	0.36000	223.00
0371.0	7149045	500181	1.10	2.00	110.0	0.64000	349.00
0372.0	7149045	500181	1.10	2.00	145.0	0.72000	551.00
0373.0	7149045	500181	1.10	2.00	140.0	0.60000	395.00
0374.0	7149045	500181	1.10	2.00	150.0	0.72000	543.00
0375.0	7149045	500181	1.10	2.00	110.0	0.37000	408.00
0376.0	7149045	500181	1.10	2.00	91.0	0.30000	197.00
0377.0	7149045	500181	1.10	2.00	117.0	0.41000	431.00
0378.0	7149045	500181	1.10	2.00	145.0	0.72000	373.00
0379.0	7149045	500181	1.10	2.00	104.0	0.58000	293.00
0380.0	7149045	500181	1.10	2.00	152.0	0.72000	529.00
0381.0	7149045	500181	1.10	2.00	6.00	0.20000	668.00
0382.0	7149045	500181	1.10	2.00	140.0	1.10000	212.00
0383.0	7149045	500181	1.10	2.00	200.0	3.40000	275.00
0384.0	7149045	500181	1.10	2.00	176.0	3.16.00	316.00
0385.0	7149045	500181	1.10	2.00	153.0	2.30000	322.00
0386.0	7149045	500181	1.10	2.00	105.0	0.81000	292.00
0387.0	7149045	500181	1.10	2.00	137.0	0.58000	387.00
0388.0	7149045	500181	1.10	2.00	147.0	0.97000	582.00
0389.0	7149045	500181	1.10	2.00	150.0	0.71000	408.00
0390.0	7149045	500181	1.10	2.00	393.0	9.30000	947.00
0391.0	7149045	500181	1.10	2.00	650.0	1018.00	1018.00
0392.0	7149045	500181	1.10	2.00	620.0	1105.00	1105.00
0393.0	7149045	500181	1.10	2.00	560.0	3.10000	1033.00
0394.0	7149045	500181	1.10	2.00	300.0	4.60000	603.00
0395.0	7149045	500181	1.10	2.00	385.0	5.50000	820.00
0396.0	7149045	500181	1.10	2.00	650.0	5.50000	1033.00
0397.0	7149045	500181	1.10	2.00	157.0	3.40000	460.00
0398.0	7149045	500181	1.10	2.00	415.0	9.30000	932.00
0399.0	7149045	500181	1.10	2.00	760.0	3.20000	818.00
0400.0	7149045	500181	1.10	2.00	190.0	2.00000	665.00
0401.0	7149045	500181	1.10	2.00	400.0	4.00.00	603.00
0402.0	7149045	500181	1.10	2.00	530.0	4.20000	694.00
0403.0	7149045	500181	1.10	2.00	170.0	3.10000	420.00
0404.0	7149045	500181	1.10	2.00	180.0	6.70000	549.00
0405.0	7149045	500181	1.10	2.00	162.0	6.30000	468.00
0406.0	7149045	500181	1.10	2.00	163.0	3.10000	545.00
0407.0	7149045	500181	1.10	2.00	4.01	9.00.00	499.00
0408.0	7149045	500181	1.10	2.00	100.0	504.00	504.00
0409.0	7149045	500181	1.10	2.00	100.0	516.00	516.00
0410.0	7149045	500181	1.10	2.00	970.0	513.00	513.00
0411.0	7149045	500181	1.10	2.00	1.75	9.00.00	611.00
0412.0	7149045	500181	1.10	2.00	1130.0	740.00	740.00
0413.0	7149045	500181	1.10	2.00	1200.0	736.00	736.00
0414.0	7149045	500181	1.10	2.00	1100.0	643.00	643.00
0415.0	7149045	500181	1.10	2.00	1.43	2.00000	370.00
0416.0	7149045	500181	1.10	2.00	1.60.00	1.40000	513.00
0417.0	7149045	500181	1.10	2.00	1.50.00	1.60000	559.00
0418.0	7149045	500181	1.10	2.00	1.60.00	1.10000	269.00
0419.0	7149045	500181	1.10	2.00	1.40.00	1.10000	412.00
0420.0	7149045	500181	1.10	2.00	1.31.00	1.00000	459.00

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
0428.0	2329090	500041	6.58	14.3	153.0	970000	273.00
0429.0	2329090	500041	6.58	14.3	264.0	400000	236.00
0430.0	2329090	500041	6.58	14.3	153.0	710000	193.00
0431.0	2329090	500041	6.58	14.3	134.0	590000	226.00
0432.0	2329090	500041	6.06	14.3	337.0	1.80000	380.00
0433.0	2329090	500041	6.06	14.3	345.0	1.80000	350.00
0434.0	2329090	500041	6.06	14.3	320.0	1.30000	197.00
0435.0	2329090	500041	6.06	14.3	410.0	4.20000	461.00
0436.0	2329090	500041	6.06	14.3	280.0	6.30000	249.00
0437.0	2329090	500041	6.06	14.3	140.0	1.00000	367.00
0438.0	2329090	500041	6.06	14.3	840.0	2.20000	380.00
0439.0	2329090	500041	6.06	14.3	810.0	4.20000	340.00
0440.0	2329090	500041	6.06	14.3	480.0	370.00	370.00
0441.0	2329090	500041	6.06	14.3	840.0	2.20000	367.00
0442.0	2329090	500041	5.17	14.3	530.0	625.00	625.00
0443.0	2329090	500041	5.17	14.3	510.0	537.00	537.00
0444.0	2329090	500041	5.17	14.3	640.0	7.70000	534.00
0445.0	2329090	500041	5.17	14.3	610.0	9.30000	630.00
0446.0	2329090	500041	5.87	14.3	120.0	2.20000	111.00
0447.0	2329090	500041	5.87	14.3	270.0	3.60000	126.00
0448.0	2329090	500041	5.87	14.3	410.0	1.80000	270.00
0449.0	2329090	500041	5.87	14.3	750.0	3.80000	237.00
0450.0	2329090	500041	5.87	14.3	560.0	3.60000	928.00
0451.0	2329090	500041	5.87	14.3	1540.0	2.10000	323.00
0452.0	2329090	500041	5.77	14.3	160.0	1.80000	245.00
0453.0	2329090	500041	5.77	14.3	210.0	1.70000	462.00
0454.0	2329090	500041	5.77	14.3	140.0	1.70000	365.00
0455.0	2329090	500041	5.77	14.3	495.0	3.70000	476.00
0456.0	2329090	500041	5.77	14.3	360.0	1.70000	640.00
0457.0	2329090	500041	5.77	14.3	530.0	1.20000	525.00
0458.0	2329090	500041	5.77	14.3	360.0	3.40000	555.00
0459.0	2329090	500041	4.92	14.3	640.0	3.40000	683.00
0460.0	2329090	500041	4.92	14.3	640.0	1129.00	1129.00
0461.0	2329090	500041	4.92	14.3	640.0	123.00	123.00
0462.0	2329090	500041	4.92	14.3	161.0	1.30000	325.00
0463.0	2329090	500041	4.92	14.3	610.0		

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG	ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
0616.0	3329090	500041	4.21	21.0	2180.	3.60000	1119.0	0751.0	3339011	500171	4.68	14.3	1000.	3.10000	538.00
0620.0	3329090	500041	5.23	21.0	1950.	3.00000	965.00	0752.0	3339011	500211	4.49	14.3	1000.	2.45000	685.00
0622.0	3329090	500041	5.23	21.0	2250.	4.20000	1213.0	0753.0	3339011	500171	4.68	14.3	1100.	2.10000	482.00
0624.0	3329090	500041	5.23	21.0	2000.	2.70000	947.00	0754.0	3339011	500211	4.49	14.3	880.0	2.30000	450.00
0626.0	3329090	500041	3.62	21.0	640.0	2.30000	810.00	0755.0	3339011	500181	4.68	14.3	980.0	1.90000	428.00
0628.0	3329090	500041	3.62	21.0	630.0	2.70000	773.00	0756.0	3339011	500211	4.49	14.3	990.0	2.30000	516.00
0629.0	3329090	500041	3.62	21.0	700.0	2.30000	940.00	0757.0	3339011	500171	4.68	14.3	1000.	2.60000	499.00
0630.0	3329090	500041	3.62	21.0	700.0	2.10000	740.00	0762.0	4329090	501021	2.53	14.3	170.0	3.20000	688.00
0631.0	3329090	500041	5.51	21.0	693.0	3.00000	910.00	0763.0	4329090	501021	2.53	14.3	170.0	1.60000	665.00
0632.0	3329090	500041	5.51	21.0	770.0	4.00000	750.00	0764.0	4329090	501021	2.53	14.3	155.0	1.50000	465.00
0633.0	3329090	500041	5.51	21.0	695.0	2.90000	846.00	0765.0	4329090	501021	2.53	14.3	137.0	1.42000	472.00
0634.0	3329090	500041	5.51	21.0	590.0	2.40000	832.00	0766.0	4329090	501021	2.53	14.3	143.0	1.45000	414.00
0636.0	3329090	500041	4.91	21.0	264.0	2.60000	683.00	0767.0	4329090	501021	2.53	14.3	161.0	2.50000	455.00
0637.0	3329090	500041	4.91	21.0	249.0	2.70000	618.00	0768.0	4329090	501021	2.53	14.3	160.0	1.50000	432.00
0639.0	3329090	500041	4.91	21.0	260.0	3.40000	601.00	0769.0	4329090	502021	2.53	14.3	161.0	1.65000	450.00
0640.0	3329090	500041	4.91	21.0	260.0	2.40000	582.00	0770.0	4329090	502021	2.53	14.3	157.0	1.90000	432.00
0642.0	3329090	500041	3.33	21.0	260.0	2.40000	874.00	0771.0	4319011	501101	5.25	14.3	159.0	2.40000	502.00
0643.0	3329090	500041	3.33	21.0	260.0	3.00000	633.00	0772.0	4319011	502101	5.25	14.3	160.0	2.20000	550.00
0645.0	3329090	500041	3.33	21.0	260.0	1.90000	611.00	0773.0	4319011	502101	5.25	14.3	150.0	2.40000	482.00
0647.0	3329090	500041	3.33	21.0	255.0	3.10000	561.00	0774.0	4319011	502101	5.25	14.3	153.0	1.60000	470.00
0650.0	3329090	500041	3.33	21.0	235.0	1.40000	687.00	0775.0	4319011	502141	5.25	14.3	162.0	2.15000	433.00
0651.0	3329090	500041	3.60	21.0	650.0	2.70000	663.00	0776.0	4319011	502141	5.25	14.3	158.0	2.30000	478.00
0652.0	3329090	500041	3.60	21.0	750.0	4.70000	964.00	0777.0	4319011	502141	5.25	14.3	160.0	2.40000	811.00
0653.0	3329090	500041	3.60	21.0	730.0	4.60000	672.00	0778.0	4319011	502141	5.25	14.3	157.0	2.30000	477.00
0654.0	3329090	500041	3.60	21.0	730.0	3.80000	895.00	0779.0	4319011	503141	5.25	14.3	155.0	1.80000	479.00
0655.0	3329090	500041	3.60	21.0	640.0	2.10000	503.00	0780.0	4319011	503101	5.25	14.3	157.0	1.90000	803.00
0656.0	3329090	500041	2.51	21.0	200.0	2.60000	487.00	0781.0	4339011	503201	4.45	14.3	152.0	1.45000	275.00
0657.0	3329090	500041	2.51	21.0	220.0	3.40000	863.00	0782.0	4339011	503201	4.45	14.3	160.0	1.30000	317.00
0658.0	3329090	500041	2.90	21.0	230.0	3.40000	701.00	0783.0	4339011	503201	4.45	14.3	156.0	1.40000	288.00
0659.0	3319011	500041	5.80	20.0	225.0	2.70000	529.00	0784.0	4339011	503181	4.68	14.3	158.0	1.10000	273.00
0660.0	3329090	500021	2.90	20.0	250.0	3.10000	720.00	0785.0	4339011	503181	4.68	14.3	158.0	1.60000	270.00
0661.0	3319011	500041	5.80	20.0	230.0	2.60000	546.00	0786.0	4339011	503181	4.68	14.3	146.0	1.70000	314.00
0662.0	3329090	500021	3.39	21.0	235.0	2.40000	543.00	0787.0	4339011	506251	2.24	14.3	150.0	1.80000	344.00
0663.0	3319011	500041	4.96	20.0	215.0	2.60000	550.00	0788.0	4339011	506251	2.24	14.3	146.0	2.35000	386.00
0664.0	3329090	500021	3.39	21.0	140.0	2.90000	694.00	0789.0	4339011	506271	2.24	14.3	163.0	2.50000	408.00
0665.0	3319011	500041	4.96	21.0	120.0	1.40000	533.00	0790.0	4339011	507271	2.24	14.3	158.0	3.80000	360.00
0666.0	3329090	500021	2.93	21.0	130.0	4.00000	761.00	0791.0	4339011	507271	2.24	14.3	158.0	2.60000	432.00
0667.0	3319011	500041	5.25	21.0	110.0	1.80000	529.00	0792.0	4339011	507271	2.24	14.3	153.0	1.70000	292.00
0668.0	3329090	500021	2.93	21.0	260.0	7.00000	268.00	0793.0	4329090	507021	2.64	14.3	320.0	1.40000	330.00
0669.0	3319011	500041	5.25	20.0	150.0	1.40000	412.00	0794.0	4329090	507021	2.64	14.3	340.0	1.60000	350.00
0670.0	3329090	501021	2.93	21.0	160.0	1.40000	6328.00	0795.0	4329090	507021	2.64	14.3	55.00	1.20000	349.00
0671.0	3319011	501041	5.25	21.0	140.0	1.40000	412.00	0796.0	4329090	507021	2.64	14.3	66.00	1.80000	418.00
0672.0	3329090	500021	2.53	21.0	270.0	1.20000	424.00	0797.0	4329090	507021	2.64	14.3	120.0	3.80000	821.00
0673.0	3319011	500041	4.95	21.0	280.0	1.30000	477.00	0798.0	4329090	507021	2.64	14.3	120.0	4.40000	830.00
0674.0	3329090	501021	2.53	21.0	290.0	2.70000	618.00	0799.0	4329090	508021	2.64	14.3	52.00	1.90000	368.00
0675.0	3329090	500021	2.53	21.0	210.0	3.30000	1145.00	0800.0	4319011	508121	5.24	14.3	370.0	2.50000	413.00
0676.0	3319011	500041	5.10	21.0	190.0	3.20000	910.00	0801.0	4319011	508121	5.24	14.3	120.0	3.10000	818.00
0677.0	3329090	500021	2.53	21.0	220.0	4.20000	1220.00	0802.0	4319011	508121	5.24	14.3	470.0	3.30000	538.00
0678.0	3319011	500041	5.10	21.0	190.0	3.30000	895.00	0803.0	4319011	508121	5.24	14.3	240.0	2.25000	434.00
0679.0	3329090	500021	2.53	21.0	205.0	4.00000	1463.00	0804.0	4319011	508121	5.24	14.3	56.00	1.70000	491.00
0681.0	3324545	500031	3.82	21.0	290.0	1.00000	295.00	0805.0	4319011	508121	5.24	14.3	31.00	1.40000	387.00
0682.0	3324545	500031	3.82	20.0	158.0	1.20000	453.00	0806.0	4319011	509121	5.24	14.3	110.0	4.20000	672.00
0683.0	3324545	500031	3.82	20.0	180.0	3.60000	824.00	0808.0	4339011	505191	4.44	14.3	106.0	3.20000	583.00
0684.0	3324545	501031	3.82	20.0	190.0	3.70000	800.00	0809.0	4339011	509191	4.49	14.3	25.00	4.20000	185.00
0685.0	3324545	501031	3.82	14.3	180.0	2.80000	671.00	0810.0	4339011	509191	4.49	14.3	107.0	1.20000	545.00
0686.0	3320000	500031	3.82	14.3	190.0	2.90000	835.00	0811.0	4339011	509191	4.49	14.3	270.0	1.70000	190.00
0687.0	3320000	500031	3.82	14.3	290.0	1.50000	383.00	0812.0	4339011	509191	4.49	14.3	52.00	4.40000	238.00
0688.0	3320000	501031	3.82	14.3	190.0	3.30000	816.00	0813.0	4339011	510191	4.49	14.3	54.00	1.70000	227.00
0689.0	3319090	500041	5.10	21.0	100.0	3.20000	740.00	0814.0	4339011	510191	4.49	14.3	102.0	2.20000	531.00
0690.0	3329090	500021	2.53	14.3	162.0	2.50000	581.00	0815.0	4339011	501291	2.24	10.0	160.0	1.30000	238.00
0691.0	3329090	500021	2.53	14.3	150.0	1.90000	468.00	0816.0	4339011	501291	2.24	10.0	165.0	1.20000	247.00
0691.0	3329090	500021	2.53	14.3	165.0	1.00000	723.00	0817.0	4339011	501291	2.24	10.0	167.0	1.10000	263.00
0695.0	3319011	500041	5.10	14.3	160.0	1.00000	662.00	0818.0	4339011	501291	2.24	10.0	169.0	1.10000	282.00
0696.0	3329090	500021	2.53	14.3	300.0	2.00000	450.00	0819.0	4339011	501291	2.24	10.0	170.0	1.70000	273.00
0697.0	3329090	500021	2.53	14.3	150.0	2.00000	634.00	0820.0	4339011	501291	2.24	10.0	110.0	2.10000	485.00
0698.0	3329090	500021	2.53	14.3	150.0	1.30000	395.00	0821.0	4339011	501291	2.24	10.0	28.00	4.67000	156.00
0700.0	3319011	500041	5.10	14.3	150.0	1.56000	476.00	0822.0	4339011	502291	2.24	10.0	102.0	2.30000	550.00
0701.0	3319011	500041	5.10	14.3	150.0	1.30000	460.00	0823.0	4339011	502291	2.24	10.0	176.0	2.30000	622.00
0702.0	3329090	500021	2.53	14.3	150.0	2.00000	542.00	0824.0	4339011	502291	2.24	10.0	250.0	2.90000	129.00
0703.0	3329090	500021	2.53	14.3	160.0	1.56000	504.00	0825.0							

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
0861.0	5349090	518681	2.25	1.00	150.0	600000	319.00
0862.0	5349090	518681	2.25	1.00	25.00	440000	185.00
0863.0	5349090	518681	2.25	1.00	770.0	900000	414.00
0864.0	5349090	518681	2.25	1.00	152.0	740000	421.00
0865.0	5349090	518681	2.25	1.00	24.00	440000	254.00
0866.0	5349090	518681	2.25	1.00	970.0	1.250000	488.00
0867.0	5349090	518681	2.25	1.00	153.0	700000	327.00
0868.0	5349090	518681	2.25	1.00	21.00	270000	196.00
0869.0	5349090	518681	2.25	1.00	80.00	610000	445.00
0870.0	5349090	522581	2.25	2.00	168.0	1.280000	583.00
0871.0	5349090	522581	2.25	2.00	165.0	950000	364.00
0872.0	5349090	522581	2.25	2.00	163.0	1.030000	384.00
0873.0	5349090	522581	2.25	2.00	113.0	930000	297.00
0874.0	5349090	522581	2.25	2.00	120.0	950000	113.00
0875.0	5349090	522581	2.25	2.00	155.0	690000	330.00
0876.0	5349090	522581	2.25	2.00	117.0	1.170000	136.00
0877.0	5349090	522581	2.25	2.00	170.0	930000	314.00
0878.0	5349090	522581	2.25	2.00	6.00	1.100000	299.00
0879.0	5349090	522581	2.25	2.00	29.00	1.600000	479.00
0880.0	5349090	522581	2.25	2.00	1.90	1.600000	79.00
0881.0	5349090	522581	2.25	2.00	170.0	1.090000	559.00
0882.0	5349090	522581	2.25	2.00	152.0	880000	466.00
0883.0	5349090	522581	2.25	2.00	22.00	930000	313.00
0884.0	5349090	522581	2.25	2.00	98.00	1.650000	560.00
0885.0	5349090	522581	2.25	2.00	151.0	830000	500.00
0886.0	5349090	522581	2.25	2.00	26.00	940000	285.00
0887.0	5349090	522581	2.25	2.00	100.0	1.600000	601.00
0888.0	5349090	522581	2.25	2.00	151.0	980000	400.00
0889.0	5349090	522581	2.25	2.00	154.0	970000	344.00
0890.0	5349090	522581	2.25	2.00	23.00	680000	231.00
0891.0	5349090	522581	2.25	2.00	98.00	1.300000	541.00
0892.0	5349090	522581	2.25	2.00	120.0	500000	131.00
0893.0	5349090	522581	2.25	2.00	20.00	400000	291.00
0894.0	5349090	522581	2.25	2.00	15.00	300000	62.0000
0895.0	5349090	522581	2.25	2.00	99.00	600000	271.00
0896.0	5349090	522581	2.25	2.00	38.00	800000	279.40
0897.0	5349090	522581	2.25	2.00	51.00	570000	366.20
0898.0	5349090	522581	2.25	2.00	51.00	1.350000	349.70
0899.0	5349090	522581	2.25	2.00	61.00	3.900000	349.70
0900.0	5349090	522581	2.25	2.00	95.00	580000	386.00
0901.0	5349090	522581	2.25	2.00	104.00	4.800000	386.00
0902.0	5349090	522581	2.25	2.00	350.00	950000	446.00
0903.0	5349090	522581	2.25	2.00	350.00	1.020000	423.00
0904.0	5349090	522581	2.25	2.00	387.00	1.210000	523.00
0905.0	5349090	522581	2.25	2.00	770.00	1.400000	833.00
0906.0	5349090	522581	2.25	2.00	725.00	1.250000	377.00
0907.0	5349090	522581	2.25	2.00	61.00	1.440000	388.00
0908.0	5349090	522581	2.25	2.00	77.00	1.100000	596.00
0909.0	5349090	522581	2.25	2.00	39.00	1.000000	451.00
0910.0	5349090	522581	2.25	2.00	13.00	0.300000	217.00
0911.0	5349090	522581	2.25	2.00	50.00	640000	401.00
0912.0	5349090	522581	2.25	2.00	34.00	640000	285.00
0913.0	5349090	522581	2.25	2.00	80.00	1.180000	781.00
0914.0	5349090	522581	2.25	2.00	100.00	2.350000	1189.00
0915.0	5349090	522581	2.25	2.00	110.00	3.700000	1218.00
0916.0	5349090	522581	2.25	2.00	110.00	6.200000	1130.00
0917.0	5349090	522581	2.25	2.00	59.00	6.800000	652.00
0918.0	5349090	522581	2.25	2.00	71.00	3.500000	495.00
0919.0	5349090	522581	2.25	2.00	44.00	4.800000	88.0000
0920.0	5349090	522581	2.25	2.00	130.00	8.900000	157.00
0921.0	5349090	522581	2.25	2.00	280.00	1.130000	207.00
0922.0	5349090	522581	2.25	2.00	700.00	8.100000	223.00
0923.0	5349090	522581	2.25	2.00	11.00	300000	372.00
0924.0	5349090	522581	2.25	2.00	180.00	1.600000	427.00
0925.0	5349090	522581	2.25	2.00	395.00	4.000000	990.00
0926.0	5349090	522581	2.25	2.00	12.00	475.00	
0927.0	5349090	522581	2.25	2.00	460.00	4.000000	1490.00
0928.0	5349090	522581	2.25	2.00	13.00	3.000000	63.0000
0929.0	5349090	522581	2.25	2.00	320.00	1.950000	533.00
0930.0	5349090	522581	2.25	2.00	419.00	2.750000	707.00
0931.0	5349090	522581	2.25	2.00	27.00	2.600000	247.00
0932.0	5349090	522581	2.25	2.00	575.00	2.400000	605.00
0933.0	5349090	522581	2.25	2.00	380.00	4.800000	989.00
0934.0	5349090	522581	2.25	2.00	84.00	3.000000	343.00
0935.0	5349090	522581	2.25	2.00	41.00	1.900000	321.00
0936.0	5349090	522581	2.25	2.00	62.00	2.000000	592.00
0937.0	5349090	522581	2.25	2.00	300.00	3.900000	896.00
0938.0	5349090	522581	2.25	2.00	41.00	2.200000	317.00
0939.0	5349090	522581	2.25	2.00	35.00	5.600000	85.0000
0940.0	5349090	522581	2.25	2.00	13.00	1.100000	73.0000
0941.0	5349090	522581	2.25	2.00	210.00	5.000000	308.00
0942.0	5349090	522581	2.25	2.00	1.00	3.900000	896.00
0943.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0944.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0945.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0946.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0947.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0948.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0949.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0950.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0951.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0952.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0953.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0954.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0955.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0956.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0957.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0958.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0959.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0960.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0961.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0962.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0963.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0964.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0965.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0966.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0967.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0968.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0969.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0970.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0971.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0972.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0973.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0974.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0975.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0976.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0977.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0978.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0979.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0980.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0981.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0982.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0983.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0984.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0985.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0986.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0987.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0988.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0989.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0990.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0991.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0992.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0993.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0994.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0995.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0996.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0997.0	5349090	522581	2.25	2.00	4.85	2.00	680.00
0998.0	5349090	522581	2.25	2.00	4.85	2.00	680.00

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
1224.0	2639011	304041	3.41	21.0	330.0	2.10000	862.00
1225.0	2639011	304041	3.41	21.0	340.0	1.00000	823.00
1226.0	2639011	309011	3.41	21.0	285.0	1.80000	700.00
1227.0	2639011	309011	3.41	21.0	440.0	4.50000	327.00
1229.0	2639011	309071	2.46	21.0	51.000	1.10000	207.00
1230.0	2639011	309071	2.46	21.0	219.0	2.40000	730.00
1231.0	2639011	309071	2.46	21.0	540.0	1.65000	1100.00
1232.0	8449045	399151	2.10	21.0	545.0	2.70000	812.00
1233.0	8449045	399151	2.10	21.0	294.0	2.80000	767.00
1235.0	8449045	399151	2.10	21.0	939.0	1.80000	575.00
1236.0	8449045	399151	2.10	21.0	320.0	3.20000	260.00
1239.0	2519011	318041	3.41	21.0	64.000	0.90000	384.00
1240.0	2519011	318041	3.41	21.0	150.000	0.90000	480.00
1241.0	2519011	318041	3.41	21.0	920.000	1.70000	650.00
1242.0	2519011	318041	3.41	21.0	58.000	2.45000	910.00
1244.0	2639011	306041	3.41	1.00	21.000	0.02000	40.000
1245.0	2639011	306041	3.41	1.00	41.000	1.20000	80.000
1246.0	2639011	306041	3.41	1.00	130.000	1.60000	84.000
1247.0	2639011	307041	3.41	1.00	24.000	0.09100	106.000
1248.0	2639011	307041	3.41	1.00	730.000	1.90000	99.000
1249.0	2639011	307041	3.41	1.00	940.000	1.00000	90.000
1250.0	2639011	307071	2.46	1.00	16.000	0.07500	84.000
1251.0	2639011	307071	2.46	1.00	130.000	2.29000	245.00
1252.0	2639011	307071	2.46	1.00	170.000	1.20000	116.00
1254.0	2639011	308111	2.45	1.00	11.000	3.30000	52.000
1255.0	2639011	308111	2.45	1.00	71.000	0.92000	124.00
1256.0	2639011	308111	2.45	1.00	620.000	5.00000	237.00
1257.0	2639011	308111	2.45	1.00	613.000	1.30000	140.00
1261.0	2639011	309011	2.45	1.00	210.000	0.93000	245.00
1266.0	2519011	312041	6.66	5.00	52.000	0.80000	161.00
1267.0	2519011	312041	6.66	5.00	115.000	3.80000	188.00
1268.0	2519011	312041	6.66	5.00	560.000	2.00000	204.00
1270.0	2519011	312071	6.66	5.00	39.000	2.00000	220.00
1271.0	2519011	312071	6.66	5.00	540.000	4.50000	304.00
1272.0	2519011	312071	6.66	5.00	340.000	2.50000	291.00
1273.0	2519011	312011	6.66	5.00	44.000	5.00000	168.00
1274.0	2519011	312011	6.66	5.00	787.000	1.10000	270.00
1275.0	2519011	312011	6.66	5.00	351.000	1.20000	236.00
1276.0	2639011	312011	5.26	5.00	48.000	5.50000	230.00
1277.0	2639011	312011	5.26	5.00	124.000	5.70000	238.00
1278.0	2639011	312011	5.26	5.00	660.000	0.80000	341.00
1279.0	2639011	312011	5.26	5.00	250.000	1.10000	351.00
1280.0	2639011	312011	5.26	5.00	280.000	1.90000	706.00
1283.0	2639011	313041	3.59	5.00	44.000	6.00000	160.00
1284.0	2639011	313041	3.59	5.00	140.000	6.30000	202.00
1285.0	2639011	313041	3.59	5.00	720.000	9.00000	278.00
1286.0	2639011	313041	3.59	5.00	509.000	1.30000	348.00
1289.0	2639011	313071	2.50	5.00	24.000	4.70000	103.00
1290.0	2639011	313071	2.50	5.00	170.000	1.10000	183.00
1291.0	2639011	313071	2.50	5.00	630.000	1.30000	289.00
1292.0	2639011	313071	2.50	5.00	430.000	2.50000	351.00
1294.0	2639011	313041	3.59	5.00	62.000	6.90000	162.00
1295.0	2639011	313041	3.59	5.00	165.000	1.40000	235.00
1296.0	2639011	313041	3.59	5.00	304.000	1.50000	259.00
1297.0	2639011	313041	3.59	5.00	245.000	1.80000	445.00
1299.0	2639011	314071	2.40	5.00	14.000	1.20000	79.000
1300.0	2639011	314071	2.40	5.00	80.000	3.30000	98.000
1301.0	2639011	314071	2.40	5.00	520.000	5.50000	140.00
1302.0	2639011	314071	2.40	5.00	600.000	0.24000	243.00
1304.0	2639011	314111	2.67	5.00	46.000	1.30000	79.000
1309.0	2639011	314111	2.67	5.00	150.000	1.20000	150.00
1306.0	2639011	314111	2.67	5.00	240.000	7.15000	210.00
1307.0	2639011	314111	2.67	5.00	640.000	1.90000	320.00
1308.0	2639011	314111	2.67	5.00	170.000	3.50000	205.00
1309.0	2639011	314111	2.67	5.00	475.000	0.85000	260.00
1311.0	2639011	314111	2.67	5.00	58.000	0.80000	79.000
1312.0	2639011	314111	2.67	5.00	950.000	1.40000	183.00
1313.0	2639011	314111	2.67	5.00	2620.000	2.20000	445.00
1314.0	2639011	314111	2.67	5.00	4000.000	2.80000	447.00
1316.0	2639011	314111	2.67	5.00	180.000	2.00000	149.00
1317.0	2639011	314111	2.67	5.00	730.000	1.72000	235.00
1318.0	2639011	314111	2.67	5.00	2250.000	1.30000	244.00
1319.0	2639011	314111	2.67	5.00	6100.000	1.79000	350.00
1325.0	2639011	310111	4.94	10.0	66.000	1.10000	346.00
1326.0	2639011	310111	4.94	10.0	110.000	2.29000	396.00
1327.0	2639011	311011	4.74	10.0	275.000	2.05000	392.00
1328.0	2639011	311011	4.94	10.0	1400.000	1.10000	670.00
1329.0	2639011	311011	4.94	10.0	2150.000	1.45000	780.00
1330.0	2639011	311011	4.94	10.0	5100.000	1.60000	854.00
1331.0	2639011	311041	3.42	10.0	67.000	0.84000	256.00
1332.0	2639011	311041	3.42	10.0	157.000	1.40000	316.00
1333.0	2639011	311041	3.42	10.0	373.000	1.00000	335.00
1334.0	2639011	311041	3.42	10.0	300.000	3.10000	450.00
1335.0	2639011	311041	3.42	10.0	1400.000	0.80000	564.00
1336.0	2639011	311041	3.42	10.0	3000.000	0.84000	679.00
1337.0	2639011	311041	3.42	10.0	5200.000	1.30000	781.00
1338.0	2639011	311041	3.42	10.0	8800.000	1.20000	479.00
1339.0	2639011	311071	2.37	10.0	74.000	0.95000	220.00
1340.0	2639011	311071	2.37	10.0	185.000	1.20000	359.00
1341.0	2639011	311071	2.37	10.0	420.000	3.30000	299.00
1342.0	2639011	311071	2.37	10.0	790.000	0.77000	618.00
1343.0	2639011	311071	2.37	10.0	1950.000	0.80000	496.00
1344.0	2639011	311071	2.37	10.0	2790.000	0.50000	387.00
1345.0	2639011	311011	3.70	10.0	52.000	0.57000	261.00
1346.0	2639011	311011	3.70	10.0	170.000	0.82000	338.00
1347.0	2639011	311011	3.70	10.0	290.000	0.47000	394.00
1348.0	2639011	311011	3.70	10.0	980.000	1.10000	734.00
1349.0	2639011	311011	3.70	10.0	2730.000	2.05000	831.00
1350.0	2639011	311011	3.70	10.0	5400.000	1.50000	912.00
1351.0	2639011	311011	3.70	10.0	6600.000	0.83000	236.00

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
1352.0	2639011	311011	3.70	10.0	170.000	1.00000	451.00
1353.0	2639011	311011	3.70	10.0	420.000	1.40000	459.00
1354.0	2639011	311011	3.70	10.0	1100.000	2.70000	829.00
1355.0	2639011	311011	3.70	10.0	2500.000	0.85000	810.00
1356.0	2639011	311011	3.70	10.0	5150.000	1.75000	952.00
1357.0	2639011	311011	3.70	10.0	75.000	0.68000	289.00
1358.0	2639011	311011	3.70	10.0	120.000	0.60000	320.00
1359.0	2639011	311011	3.70	10.0	121.000	0.95000	190.00
1360.0	2639011	311011	3.70	10.0	540.000	0.40000	559.00
1361.0	2639011	311011	3.70	10.0	170.000	1.90000	711.00
1362.0	2639011	311011	3.70	10.0	3600.000	2.00000	870.00
1363.0	2629090	106171	3.84	10.0	75.000	0.48000	338.00
1364.0	2629090	106171	3.84	10.0	100.000	0.61000	358.00
1365.0	2629090	106171	3.84	10.0	170.000	1.00000	360.00
1366.0	2629090	106171	3.84	10.0	330.000	0.70000	429.00
1367.0	2629090	106171	3.84	10.0	750.000	0.42000	610.00
1368.0	2629090	106171	3.84	10.0	140.000	1.40000	861.00
1369.0	2629090	106171	3.84	10.0	250.000	0.35000	732.00
1370.0	2629090	106171	3.84	10.0	480.000	0.48000	837.00
1371.0	2629090	106171	3.84	10.0	75.000	0.70000	388.00
1372.0	2629090	106171	3.84	10.0	124.000	0.75000	423.00
1373.0	2629090	106171	3.84	10.0	700.000	1.60000	500.00
1374.0	2629090	106171	3.84	10.0	950.000	0.92000	570.00
1375.0	2629090	106171	3.84	10.0	2500.000	1.00000	700.00
1376.0	2629090	106171	3.84	10.0	5000.000	0.70000	650.00
1377.0	2629090	106171	3.84	10.0	1200.000	1.00000	261.00
1378.0	2629090	106171	3.84	10.0	62.000	0.25000	410.00
1379.0	2629090	106171	3.84	10.0	700.000	1.00000	500.00
1380.0	2629090	106171	3.84	10.0			840.00
1381.0	2629090	106171	3.84	10.0	390.000	3.30000	737.00
1382.0	2629090	106171	3.84	10.0	5490.000	2.30000	918.00
1383.0	2629090	106171	3.84	10.0	80.000	0.88000	340.00</

ID	CODE 1	CODE 2	CML	TEMP	RATE	MODULUS	STRENG
1504.0	.2629090	.167171	2.68	21.0	235.0	1.70000	667.00
1505.0	.2629090	.167171	2.68	21.0	1100.0	2.10000	949.00
1506.0	.2629090	.167171	2.68	21.0	2300.0	2.20000	1028.00
1507.0	.2629090	.167171	2.68	21.0	9800.0	1.80000	1163.00
1508.0	.2629090	.167171	2.68	21.0	400.0	1.70000	798.00
1514.0	.2629090	.553261	1.95	21.0	94.00	.250000	378.00
1515.0	.2629090	.553261	1.95	21.0	190.0	.920000	497.00
1516.0	.2629090	.553261	1.95	21.0	670.0	1.870000	656.00
1517.0	.2629090	.553261	1.95	21.0	2000.0	1.000000	860.00
1518.0	.2629090	.553261	1.95	21.0	5800.0	1.030000	1054.00
1519.0	.3639011	.118171	2.64	21.0	68.00	.780000	394.00
1520.0	.3639011	.118171	2.64	21.0	700.0	.900000	489.00
1521.0	.3639011	.118171	2.64	21.0	540.0	.590000	723.00
1522.0	.3639011	.118171	2.64	21.0	1800.0	.780000	910.00
1523.0	.3639011	.118171	2.64	21.0	6300.0	1.190000	1132.00
1530.0	.2629090	.163171	2.68	1.00	48.00	.280000	188.00
1531.0	.2629090	.553171	2.68	1.00	24.00	.080000	127.00
1532.0	.2629090	.463171	2.68	1.00	510.0	1.280000	240.00
1533.0	.2629090	.463171	2.68	1.00	1600.0	.440000	350.00
1534.0	.2629090	.863171	2.68	1.00	2900.0	.320000	424.00
1535.0	.2629090	.863171	2.68	1.00	47.00	.270000	331.00
1536.0	.2629090	.863171	2.68	1.00	49.00	.090000	112.00
1537.0	.2629090	.863171	2.68	1.00	1400.0	.019000	175.00
1538.0	.2629090	.864171	2.67	1.00			98.0000
1539.0	.2629090	.565261	1.95	1.00	38.00	.038000	160.00
1540.0	.2629090	.565261	1.95	1.00	72.50	.200000	120.00
1541.0	.2629090	.565261	1.95	1.00			97.0000
1542.0	.2629090	.167171	2.68	1.00	120.0	.600000	295.00
1543.0	.2629090	.467171	2.68	1.00	880.0	.540000	460.00
1544.0	.2629090	.567171	2.68	1.00	3800.0	.400000	440.00
1545.0	.2629090	.567261	1.95	1.00	91.00	.150000	151.00
1546.0	.2629090	.567261	1.95	1.00	341.0	.120000	132.00
1547.0	.2629090	.668261	1.95	1.00	4400.0	1.440000	465.00
1548.0	.2629090	.668261	1.95	1.00	742.0	1.660000	338.00
1549.0	.3639011	.134171	2.55	2.00	145.0	.480000	205.00
1550.0	.3639011	.134171	2.55	2.00	261.0	.250000	207.00
1551.0	.3639011	.334171	2.75	2.00	1320.0	.600000	163.00
1552.0	.3639011	.334171	2.50	2.00	4450.0	2.400000	409.00
1553.0	.3639011	.134171	2.52	2.00	176.0	1.200000	241.00
1555.0	.3639011	.134171	2.48	2.00	300.0	.270000	228.00
1556.0	.3639011	.334171	2.48	2.00	850.0	.720000	243.00
1557.0	.3639011	.334171	2.78	2.00	2600.0	.440000	316.00
1558.0	.3639011	.134171	2.69	2.00	25.00	.078000	139.00
1559.0	.3639011	.134171	2.70	2.00	61.00	.530000	183.00
1560.0	.3639011	.135041	2.65	2.00	44.00	.190000	121.00
1561.0	.3639011	.135041	2.78	2.00	24.00	.240000	125.00
1562.0	.3639011	.135041	2.95	2.00	157.0	2.000000	169.00
1563.0	.3639011	.335041	2.58	2.00	34.00	.680000	161.00
1564.0	.3639011	.135041	2.60	2.00	400.0	1.100000	184.00
1565.0	.3639011	.135041	2.80	2.00	54.00	.540000	150.00
1566.0	.3639011	.135041	2.88	2.00	1250.0	1.060000	199.00
1567.0	.3639011	.335041	3.08	2.00	700.0	.430000	171.00
1568.0	.3639011	.335041	3.33	2.00	3650.0	.230000	171.00
1569.0	.3639011	.335041	3.10	2.00	3700.0	.900000	220.00
1573.0	.3639011	.135011	3.60	2.00	47.00	.250000	141.00
1574.0	.3639011	.135011	3.65	2.00	174.0	.140000	90.0000
1575.0	.3639011	.336011	2.85	2.00	3700.0	.610000	276.00
1578.0	.3639011	.101011	3.67	2.00	35.00	.290000	169.00
1579.0	.3639011	.141011	3.45	2.00	33.00	.270000	152.00
1580.0	.3639011	.101011	4.00	2.00	32.00	.210000	142.00
1581.0	.3639011	.101011	4.05	2.00	68.00	.650000	161.00
1582.0	.3639011	.101011	4.00	2.00	85.00	.620000	142.00
1583.0	.3639011	.101011	3.98	2.00	90.00	.620000	161.00
1584.0	.3639011	.101011	4.12	2.00	220.0	.140000	172.00
1585.0	.3639011	.101011	3.66	2.00	314.0	.380000	214.00
1586.0	.3639011	.101011	3.63	2.00	340.0	.590000	216.00
1587.0	.3639011	.401011	4.20	2.00	1100.0	.330000	268.00
1588.0	.3639011	.401011	3.95	2.00	1400.0	.860000	268.00
1589.0	.3639011	.401011	3.95	2.00	1200.0	.380000	291.00
1590.0	.3639011	.301011	4.30	2.00	2100.0	.240000	252.00
1591.0	.3639011	.301011	4.07	2.00	3000.0	.860000	190.00
1592.0	.3639011	.301011	4.26	2.00	3800.0	1.200000	237.00
1594.0	.3639011	.102011	3.70	2.00	36.00	.210000	142.00
1595.0	.3639011	.102011	4.05	2.00	45.00	.640000	131.00
1596.0	.3639011	.102011	4.00	2.00	74.00	.180000	152.00
1597.0	.3639011	.503011	3.40	2.00	280.0	.340000	159.00
1598.0	.3639011	.103011	3.76	2.00	840.0	.470000	206.00
1599.0	.3639011	.303011	4.79	2.00	700.0	.040000	71.0000
1600.0	.3639011	.304011	4.00	2.00	2600.0	.590000	117.00
1601.0	.3639011	.303011	3.65	2.00	1200.0	.180000	180.00
1602.0	.3639011	.303011	4.13	2.00	1400.0	.190000	217.00
1603.0	.3639011	.303011	4.20	2.00	1900.0	.590000	180.00
1604.0	.3639011	.102041	2.73	2.00	4300.0	.627000	113.00
1605.0	.3639011	.102041	2.55	2.00	42.00	.260000	161.00
1606.0	.3639011	.103041	2.50	2.00	124.0	.590000	131.00
1607.0	.3639011	.103041	2.55	2.00	118.0	.940000	132.00
1608.0	.3639011	.103041	2.83	2.00	330.0	.640000	204.00
1609.0	.3639011	.403041	2.97	2.00	320.0	.900000	220.00
1610.0	.3639011	.403041	2.75	2.00	900.0	.940000	260.00
1611.0	.3639011	.403041	2.50	2.00	980.0	.320000	296.00
1612.0	.3639011	.403041	2.70	2.00	2900.0	.630000	331.00
1613.0	.3639011	.303041	2.70	2.00	3200.0	.760000	349.00
1614.0	.3639011	.104041	2.48	2.00	32.00	.390000	110.00
1615.0	.3639011	.104041	2.90	2.00	28.00	.160000	150.00
1616.0	.3639011	.104041	2.78	2.00	51.00	.100000	130.00
1617.0	.3639011	.104041	2.57	2.00	190.0	.470000	185.00
1618.0	.3639011	.104041	2.61	2.00	390.0	.330000	259.00
1619.0	.3639011	.104041	2.73	2.00	250.0	.140000	192.00
1620.0	.3639011	.404041	2.50	2.00	970.0	.970000	295.00
1621.0	.3639011	.204041	2.75	2.00	720.0	.610000	280.00

ID	CODE 1	CODE 2	CML	TEMP	RATE	MODULUS	STRENG
1622.0	.3639011	.204041	2.55	2.00	3950.0	.530000	424.00
1623.0	.3639011	.304041	2.56	2.00	3900.0	.600000	272.00
1631.0	.3639011	.103041	2.75	2.00	37.00	.140000	157.00
1632.0	.3639011	.103041	2.63	2.00	150.0	1.100000	205.00
1633.0	.3639011	.403041	2.61	2.00	940.0	.910000	285.00
1634.0	.3639011	.303041	2.70	2.00	1350.0	.870000	385.00
1635.0	.3639011	.403041	3.03	2.00	2400.0	.600000	343.00
1636.0	.3639011	.403041	2.60	2.00	2900.0	.750000	380.00
1637.0	.3639011	.303041	2.05	2.00	2400.0	.410000	417.00
1638.0	.3639011	.303041	2.86	2.00	2660.0	.169000	361.00
1639.0	.3639011	.303041	2.55	2.00	2400.0	.750000	430.00
1640.0	.3639011	.303041	2.23	2.00	5400.0	1.070000	470.00
1641.0	.3639011	.303041	2.77	2.00	3050.0	1.600000	383.00
1643.0	.3639011	.103041	2.12	2.00	520.0	.740000	262.00
1644.0	.3639011	.303041	2.50	2.00	3100.0	.350000	340.00
1649.0	.3640090	.107441	2.78	2.00	68.00	.420000	597.00
1650.0	.3640090	.107441	2.47	2.00	61.00	.630000	173.00
1651.0	.3640090	.107441	2.55	2.00	110.0	1.680000	756.00
1652.0	.3640090	.107441	2.40	2.00	170.0	1.300000	882.00
1653.0	.3640090	.107441	2.50	2.00	217.0	1.720000	951.00
1654.0	.3640090	.107441	2.50	2.00	220.0	1.000000	890.00
1655.0	.3640090	.308441	2.55	2.00	590.0	1.370000	1433.00
1656.0	.3640090	.108441	2.66	2.00	730.0	2.500000	1170.00
1657.0	.3640090	.108441	2.63	2.00	675.0	3.000000	1102.00
1658.0	.3640090	.808441	2.55	2.00	1500.0	2.200000	1458.00
1659.0	.3640090	.808441	2.53	2.00	240.0	2.800000	1457.00
1660.0	.3640090	.808441	2.55	2.00	2400.0	2.900000	1550.00
1661.0	.3640090	.808441	2.60	2.00	5900.0	3.500000	1775.00
1662.0	.3640090	.808441	2.53	2.00	5800.0	3.030000	1565.00
1663.0	.3640090	.808441	2.68	2.00	5600.0	1.600000	989.00
1664.0	.3640090	.808441	2.48	2.00	5900.0	3.800000	1797.00
1665.0	.3640090	.808441	2.60	2.00	3800.0	1.540000	974.00
1666.0	.3640090	.808441	2.55	2.00	4700.0		1615.00
1667.0	.3640090	.908441	2.70	2.00	2300.0	2.600000	1330.00
1668.0	.3640090	.108441	2.75	2.00	280.0	2.20	

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
1796.0	.3649045	.201441	2.73	10.0	140.0	1.42000	350.00
1797.0	.3649045	.201441	2.86	10.0	112.0	.750000	340.00
1798.0	.3649045	.201441	3.02	10.0	130.0	.600000	417.00
1799.0	.3649045	.201441	2.40	10.0	440.0	1.82000	588.00
1800.0	.3649045	.201441	4.56	10.0	420.0	1.60000	614.00
1801.0	.3649045	.201441	3.55	10.0	400.0	1.20000	543.00
1803.0	.3649090	.302441	2.64	10.0	110.0	1.56000	1098.00
1804.0	.3649090	.302441	2.44	10.0	108.0	1.37000	915.00
1805.0	.3649090	.302441	3.04	10.0	98.00	.840000	1191.00
1806.0	.3649090	.302441	2.15	10.0	240.0	.950000	1221.00
1807.0	.3649090	.302441	3.16	10.0	240.0	.900000	924.00
1809.0	.3649090	.302441	3.66	10.0	630.0	1.40000	1604.00
1810.0	.3649090	.302441	3.21	10.0	666.0	1.24000	1627.00
1811.0	.3649090	.302441	3.61	10.0	650.0	1.20000	1355.00
1812.0	.3649090	.302441	3.50	10.0	270.0	2.10000	2008.00
1813.0	.3649090	.302441	2.35	10.0	250.0	2.04000	1999.00
1814.0	.3649090	.302441	3.00	10.0	230.0	1.23000	1635.00
1815.0	.3649090	.302441	3.25	10.0			1855.00
1816.0	.3649090	.302441	3.25	10.0	700.0	1.81000	2235.00
1817.0	.3649090	.302441	3.25	10.0	690.0	1.60000	2612.00
1823.1	.3649045	.102441	3.25	5.00	30.00	1.40000	46.000
1828.0	.3649045	.102441	3.63	5.00	36.00	1.80000	78.000
1829.0	.3649045	.102441	3.65	5.00	73.00	.670000	82.000
1830.0	.3649045	.102441	4.19	5.00	280.0	.610000	164.000
1831.0	.3649045	.102441	4.27	5.00	340.0	.590000	180.000
1833.0	.3649045	.102441	2.95	5.00	260.0	.820000	460.000
1835.0	.3649045	.102441	3.02	5.00	440.0	1.10000	609.000
1841.0	.3649090	.402441	3.30	5.00	97.00	.890000	432.000
1842.0	.3649090	.402441	2.86	5.00	65.00	1.00000	329.000
1843.0	.3649090	.402441	2.29	5.00	480.0	1.08000	564.000
1844.0	.3649090	.402441	2.95	5.00	680.0	2.70000	700.000
1845.0	.3649090	.402441	2.80	5.00	460.0	.450000	565.000
1846.0	.3649090	.402441	3.10	5.00	76.00	.500000	356.000
1847.0	.3649090	.402441	2.35	5.00	180.0	1.40000	900.000
1848.0	.3649090	.402441	2.46	5.00	165.0	1.50000	802.000
1849.0	.3649090	.402441	2.58	5.00			816.000
1851.0	.3649090	.402441	2.83	5.00	540.0	1.20000	460.000
1852.0	.3649090	.402441	2.97	5.00	480.0	.480000	576.000
1855.0	.3649090	.402441	2.28	5.00	95.00	1.58000	1027.000
1856.0	.3649090	.402441	2.66	5.00	95.00	1.00000	657.000
1857.0	.3649090	.402441	2.35	5.00	160.0	1.20000	642.000
1858.0	.3649090	.402441	2.65	5.00	570.0	1.60000	900.000
1859.0	.3649090	.402441	1.88	5.00	570.0	1.40000	782.000
1860.0	.3649090	.402441	3.41	5.00	700.0	2.30000	1144.300
1861.0	.3649090	.402441	3.25	5.00	650.0	3.30000	1790.000
1862.0	.3649090	.402441	3.25	5.00	650.0	3.00000	1989.000
1863.0	.3649090	.402441	3.25	5.00	750.0	2.60000	2042.000
1867.0	.3649090	.402441	3.20	5.00	660.0	1.68000	1363.000
1868.0	.3649090	.402441	2.75	5.00	100.0	2.20000	1400.000
1869.0	.3649090	.402441	3.17	5.00	680.0	1.76000	1222.000
1877.0	.3649045	.107441	2.90	5.00	56.00	1.70000	78.000
1879.0	.3649045	.107441	3.48	5.00	110.0	.260000	119.000
1880.0	.3649045	.107441	3.00	5.00	114.0	.500000	120.000
1881.0	.3649045	.107441	2.83	5.00	27.00	.800000	168.000
1882.0	.3649045	.107441	2.90	5.00	100.0	1.10000	331.000
1883.0	.3649045	.107441	2.68	5.00	975.0	1.20000	290.000
1884.0	.3649045	.107441	2.60	5.00	750.0	1.30000	323.000
1885.0	.3649045	.107441	2.60	5.00	300.0	1.19000	431.000
1886.0	.3649045	.107441	2.60	5.00	330.0	2.27000	413.000
1887.0	.3649045	.107441	2.60	5.00	260.0	.710000	421.000
1888.0	.3649045	.107441	2.85	5.00	360.0	1.40000	460.000
1894.0	.3649090	.308441	2.60	5.00	130.0	.350000	93.000
1895.0	.3649090	.308441	2.98	5.00	240.0	.960000	799.000
1896.0	.3649090	.308441	2.80	5.00	220.0	1.30000	900.000
1897.0	.3649090	.308441	3.25	5.00	180.0	1.23000	1014.000
1898.0	.3649090	.308441	3.25	5.00	200.0	2.64000	961.000
1899.0	.3649090	.308441	3.03	5.00	140.0	1.35000	702.000
1900.0	.3649090	.308441	3.31	5.00	370.0	1.70000	1100.000
1901.0	.3649090	.308441	3.00	5.00	390.0	1.32000	1383.000
1902.0	.3649090	.308441	3.00	5.00	380.0	2.66000	1363.000
1903.0	.3649090	.308441	2.80	5.00	310.0	3.50000	735.000
1904.0	.3649090	.308441	2.75	5.00	540.0	2.50000	1283.000
1905.0	.3649090	.308441	3.00	5.00	600.0	6.40000	1403.000
1908.0	.3649090	.109441	2.90	5.00	200.0	1.10000	360.000
1909.0	.3649090	.109441	3.03	5.00	180.0	.990000	425.000
1910.0	.3649090	.109441	3.05	5.00	170.0	.880000	351.000
1911.0	.3649090	.109441	3.01	5.00	150.0	1.50000	715.000
1912.0	.3649090	.109441	3.15	5.00	320.0	1.39000	900.000
1913.0	.3649090	.109441	3.13	5.00	380.0	1.86000	738.000
1914.0	.3649090	.109441	2.88	5.00	410.0	1.85000	1132.000
1915.0	.3649090	.109441	3.10	5.00	510.0	1.27000	1050.000
1924.0	.3649090	.311441	2.48	5.00	265.0	.490000	1309.000
1925.0	.3649090	.311441	2.55	5.00	110.0	.860000	1181.000
1926.0	.3649090	.311441	2.80	5.00	235.0	2.04000	860.000
1927.0	.3649090	.311441	3.14	5.00	280.0	1.40000	932.000
1928.0	.3649090	.311441	3.13	5.00	750.0	2.60000	1463.000
1929.0	.3649090	.311441	3.00	5.00	720.0	1.47000	1225.000
1930.0	.3649090	.311441	3.00	5.00	1277.0	.870000	1260.000
1931.0	.3649090	.311441	2.85	5.00	1800.0	2.52000	1579.000
1932.0	.3649090	.311441	2.85	5.00	1950.0	2.33000	1490.000
1933.0	.3649090	.311441	3.00	5.00	4450.0	4.42000	1461.000
1934.0	.3649090	.311441	3.00	5.00	4430.0	4.34000	1988.000
1961.0	.3649000	.118441	2.42	2.00	120.0	.970000	481.000
1962.0	.3649000	.118441	2.80	2.00	85.00	.350000	432.000
1963.0	.3649000	.118441	3.30	2.00	120.0	1.13000	475.000
1964.0	.3649000	.118441	2.85	2.00	160.0	.910000	494.000
1965.0	.3649000	.118441	2.70	2.00	170.0	1.10000	630.000
1967.0	.3649000	.118441	2.63	2.00	1500.0	1.62000	975.000
1968.0	.3649000	.118441	2.58	2.00	410.0	.360000	677.000
1969.0	.3649000	.118441	2.90	2.00	540.0	.490000	981.000

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
1970.0	.3649000	.319441	2.50	2.00	190.0	2.99000	808.000
1971.0	.3649000	.319441	2.26	2.00	150.0	2.16000	922.000
1972.0	.3649000	.319441	2.90	2.00	180.0	2.30000	1163.000
1973.0	.3649000	.319441	2.80	2.00	385.0	2.23000	989.000
1974.0	.3649000	.319441	2.95	2.00	370.0	1.97000	1011.000
1975.0	.3649000	.319441	2.61	2.00	260.0	3.00000	976.000
1976.0	.3649000	.319441	3.03	2.00	530.0	1.97000	953.000
1977.0	.3649000	.319441	3.20	2.00	500.0	1.53000	769.000
1978.0	.3649000	.319441	2.93	2.00	560.0	2.20000	1200.000
1990.0	.3649000	.220441	3.00	2.00	86.00	1.60000	413.000
1991.0	.3649000	.220441	2.65	2.00	103.0	3.20000	550.000
1992.0	.3649000	.220441	3.00	2.00	110.0	1.22000	467.000
1993.0	.3649000	.220441	2.84	2.00	430.0	1.70000	467.000
1994.0	.3649000	.220441	3.06	2.00	620.0	2.30000	677.000
1995.0	.3649090	.120441	2.32	2.00	78.00	1.10000	256.000
1996.0	.3649090	.120441	2.98	2.00	49.00	1.40000	207.000
1997.0	.3649090	.120441	2.61	2.00	76.00	.400000	253.000
1998.0	.3649090	.120441	2.50	2.00	135.0	.800000	293.000
1999.0	.3649090	.120441	2.65	2.00	127.0	.530000	251.000
2000.0	.3649090	.120441	2.65	2.00	150.0	.920000	295.000
2001.0	.3649090	.121441	3.48	2.00	570.0	1.77000	522.000
2014.0	.3649090	.121441	2.31	2.00	560.0	1.26000	470.000
2015.0	.3649090	.121441	2.78	2.00	580.0	2.10000	472.000
2016.0	.3649090	.121441	2.50	2.00	1400.0	.470000	693.000
2017.0	.3649090	.121441	2.05	2.00	1400.0	1.10000	412.000
2018.0	.3649090	.121441	2.80	2.00	1600.0	.740000	700.000
2019.0	.3649090	.321441	2.80	2.00	1400.0	1.10000	412.000
2020.0	.3649090	.221441	3.15	2.00	500.0	1.42000	627.000
2021.0	.3649090	.221441	3.25	2.00	510.0	2.48000	754.000
2022.0	.3649090	.221441	2.53	2.00	570.0	2.34000	564.000
2025.0	.3649045	.121441	2.15	2.00	190.0	.050000	53.000
2026.0	.3649045	.121441	2.96	2.00	350.0	.200000	43.000
2027.0	.3649045	.121441	2.93	2.00	71.00	.210000	57.000
2028.0	.3649045	.121441	2.18				

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
2138.0	.3639011	.702041	2.97	10.0		1.60000	707.00
2147.0	.3639011	.103041	2.51	10.0	126.0	1.80000	187.00
2148.0	.3639011	.103041	2.66	10.0	58.00	2.00000	137.00
2149.0	.3639011	.103041	3.00	10.0	74.00	5.10000	171.00
2150.0	.3639011	.103041	3.00	10.0	180.00	6.70000	177.00
2151.0	.3639011	.103041	3.00	10.0	140.00	5.30000	242.00
2152.0	.3639011	.103041	3.00	10.0	160.00	7.50000	185.00
2153.0	.3639011	.103041	3.00	10.0	140.00	1.28000	261.00
2154.0	.3639011	.103041	3.00	10.0	140.00	6.90000	262.00
2155.0	.3639011	.103041	3.00	10.0	520.00	1.14000	339.00
2156.0	.3639011	.103041	3.00	10.0		1.58000	426.00
2157.0	.3639011	.103041	3.00	5.00	1000.	4.90000	336.00
2158.0	.3639011	.103041	3.00	5.00	1900.	2.57000	395.00
2159.0	.2639011	.703041	3.00	5.00	4400.	2.77000	540.00
2160.0	.2639011	.703041	3.00	5.00	5000.	1.66000	519.00
2161.0	.3639011	.703041	3.00	5.00	5250.	3.07000	527.00
2162.0	.3639011	.703041	3.00	5.00	2900.	7.10000	496.00
2163.0	.3639011	.703041	3.00	5.00	3200.	1.10000	456.00
2164.0	.3639011	.703041	3.00	5.00	2100.	5.90000	402.00
2176.0	.3639011	.104011	3.41	5.00	96.00	5.10000	234.00
2177.0	.3639011	.104011	3.45	5.00	39.00	1.40000	210.00
2178.0	.3639011	.104011	3.29	5.00	64.00	3.50000	212.00
2179.0	.3639011	.104011	3.50	5.00	48.00	2.60000	221.00
2180.0	.3639011	.104011	3.60	5.00	220.00	3.90000	244.00
2181.0	.3639011	.104011	3.61	5.00	182.00	7.20000	260.00
2182.0	.3639011	.104011	3.30	5.00	140.00	4.70000	256.00
2183.0	.3639011	.104011	3.41	5.00	190.00	1.00000	241.00
2184.0	.3639011	.104011	3.48	5.00	390.00	5.80000	387.00
2185.0	.3639011	.104011	3.65	5.00	490.00	8.00000	347.00
2186.0	.3639011	.704011	3.45	5.00	1100.	1.00000	389.00
2187.0	.3639011	.704011	3.65	5.00	1140.	2.00000	394.00
2188.0	.3639011	.704011	3.46	5.00	1500.	8.60000	433.00
2189.0	.3639011	.204011	3.38	5.00	5900.	2.00000	590.00
2190.0	.3639011	.204011	3.50	5.00	5600.	3.60000	573.00
2191.0	.3639011	.204011	3.40	5.00	4600.	3.50000	470.00
2192.0	.3639011	.504011	3.43	5.00	4150.	1.80000	520.00
2193.0	.3639011	.704011	3.48	5.00	3400.	1.30000	506.00
2194.0	.3639011	.104011	3.81	5.00	4500.	8.60000	335.00
2195.0	.3639011	.704011	3.69	5.00	3000.	1.20000	533.00
2209.0	.3639011	.105041	3.10	2.00	51.00	2.70000	119.00
2210.0	.3639011	.105041	3.11	2.00	65.00	5.80000	129.00
2211.0	.3639011	.105041	2.84	2.00	41.00	2.70000	135.00
2212.0	.3639011	.105041	2.80	2.00	85.00	2.45000	175.00
2213.0	.3639011	.105041	2.50	2.00	64.00	1.90000	137.00
2214.0	.3639011	.105041	2.82	2.00	100.00	2.60000	157.00
2215.0	.3639011	.105041	2.90	2.00	66.00	2.90000	133.00
2216.0	.3639011	.105041	2.90	2.00	350.00	2.90000	225.00
2217.0	.3639011	.105041	2.88	2.00	375.00	5.80000	210.00
2218.0	.3639011	.105041	2.92	2.00	310.00	2.45000	203.00
2219.0	.3639011	.705041	2.70	2.00	870.00	3.50000	285.00
2220.0	.3639011	.505041	3.10	2.00	1400.	1.30000	217.00
2221.0	.3639011	.705041	2.92	2.00	1800.	5.70000	313.00
2222.0	.3639011	.705041	2.78	2.00	3300.	7.00000	268.00
2223.0	.3639011	.705041	3.32	2.00	4900.	2.10000	284.00
2224.0	.3639011	.705041	2.94	2.00	3300.	6.50000	253.00
2225.0	.3639011	.705041	2.79	2.00	3150.	1.50000	214.00
2226.0	.3639011	.705041	3.20	2.00	2700.	9.00000	305.00
2227.0	.3639011	.705041	3.14	2.00	1750.	7.30000	191.00
2228.0	.3639011	.505041	2.97	2.00	400.00	8.00000	256.00
2231.0	.3649000	.129441	2.70	2.00	640.00	1.30000	660.00
2232.0	.3649000	.729441	2.79	2.00	590.00	1.10000	653.00
2244.0	.3639011	.107011	3.52	2.00	68.00	1.50000	203.00
2245.0	.3639011	.107011	3.58	2.00	52.00	6.20000	174.00
2246.0	.3639011	.107011	3.58	2.00	47.00	3.30000	190.00
2247.0	.3639011	.107011	3.51	2.00	36.00	2.20000	177.00
2248.0	.3639011	.107011	3.88	2.00	97.00	4.60000	254.00
2249.0	.3639011	.107011	3.79	2.00	150.00	6.00000	207.00
2250.0	.3639011	.107011	3.52	2.00	180.00	6.20000	217.00
2251.0	.3639011	.107011	3.48	2.00	150.00	7.10000	189.00
2252.0	.3639011	.107011	3.92	2.00	320.00	3.20000	338.00
2253.0	.3639011	.107011	3.57	2.00	450.00	8.80000	277.00
2254.0	.3639011	.107011	3.60	2.00	470.00	8.00000	257.00
2255.0	.3639011	.107011	3.64	2.00	1400.	1.10000	341.00
2256.0	.3639011	.707011	3.50	2.00	1600.	1.60000	390.00
2257.0	.3639011	.707011	3.30	2.00	1500.	7.80000	356.00
2258.0	.3639011	.807011	3.58	2.00	4200.	1.30000	454.00
2259.0	.3639011	.807011	3.76	2.00	4100.	1.50000	369.00
2260.7	.3639011	.207011	3.76	2.00	3200.	1.30000	417.00
2261.0	.3639011	.207011	3.65	2.00	3600.	1.50000	417.00
2262.0	.3639011	.207011	3.49	2.00	2900.	8.00000	394.00
2263.0	.3639011	.207011	3.50	2.00	2900.	1.50000	392.00
2278.0	.3639011	.109011	3.56	21.00	100.00	2.00000	480.00
2279.0	.3639011	.109011	3.56	21.00	91.00	1.00000	474.00
2280.0	.3639011	.109011	2.72	21.00	78.00	1.60000	493.00
2281.0	.3639011	.109011	2.72	21.00	63.00	4.60000	441.00
2282.0	.3639011	.109011	2.72	21.00	210.00	1.40000	573.00
2283.0	.3639011	.109011	2.72	21.00	200.00	1.00000	474.00
2284.0	.3639011	.109011	2.72	21.00	190.00	1.07000	575.00
2286.0	.3639011	.109011	2.72	21.00	650.00	2.60000	750.00
2287.0	.3639011	.109011	2.72	21.00	580.00	2.24000	599.00
2288.0	.3639011	.109011	2.72	21.00	740.00	1.45000	636.00
2289.0	.3639011	.209011	2.72	21.00	2000.	2.20000	950.00
2290.0	.3639011	.209011	2.72	21.00	1410.	6.00100	759.00
2291.0	.3639011	.209011	2.72	21.00	2060.	1.10000	923.00
2292.0	.3639011	.809011	2.72	21.00	3.00000	1183.00	
2293.0	.3639011	.809011	2.72	21.00	6100.	2.08000	1192.00
2294.0	.3639011	.809011	2.72	21.00	6400.	2.00000	1003.00
2295.0	.3639011	.209011	2.72	21.00	3400.	3.80000	860.00
2296.0	.3639011	.209011	2.72	21.00	4100.	1.60000	1040.00
2297.0	.3639011	.209011	2.72	21.00	4100.	6.00000	1003.00

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
2310.0	.3639011	.510041	2.58	21.00	51.00	2.90000	314.00
2311.0	.3639011	.510041	2.30	21.00	76.00	6.20000	301.00
2312.0	.3639011	.510041	2.40	21.00	55.00	7.65000	380.00
2313.0	.3639011	.510041	2.58	21.00	68.00	5.60000	302.00
2314.0	.3639011	.510041	2.58	21.00	190.00	1.60000	313.00
2315.0	.3639011	.510041	2.58	21.00	130.00	2.80000	332.00
2316.0	.3639011	.510041	2.58	21.00	180.00	9.00000	323.00
2317.0	.3639011	.510041	2.58	21.00	182.00	1.30000	320.00
2318.0	.3639011	.510041	2.58	21.00	700.00	1.80000	478.00
2319.0	.3639011	.510041	2.58	21.00	560.00	7.00000	484.00
2320.0	.3639011	.510041	2.58	21.00	700.00	1.30000	516.00
2321.0	.3639011	.510041	2.58	21.00	1850.	1.50000	533.00
2322.0	.3639011	.510041	2.58	21.00	1600.	1.10000	719.00
2323.0	.3639011	.510041	2.58	21.00	1900.	1.40000	643.00
2324.0	.3639011	.510041	2.58	21.00	5700.	2.60000	907.00
2325.0	.3639011	.510041	2.58	21.00	5900.	1.95000	913.00
2326.0	.3639011	.510041	2.58	21.00	5800.	2.10000	1026.00
2327.0	.3639011	.510041	2.58	21.00	3700.	1.42000	883.00
2328.0	.3639011	.510041	2.58	21.00	3650.	1.30000	828.00
2329.0	.3639011	.510041	2.58	21.00	3950.	1.30000	749.00
2329.0	.3639011	.103171	2.74	21.00	83.00	1.00000	197.00
2343.0	.3639011	.103171	2.24	21.00	97.00	1.30000	258.00
2344.0	.3639011	.103171	2.41	21.00	64.00	8.00000	187.00
2345.0	.3639011	.103171	2.30	21.00	97.00	1.03000	242.00
2346.0	.3639011	.303171	2.38	21.00	175.00	1.75000	530.00
2347.0	.3639011	.303171	2.58	21.00	170.00	1.00000	456.00
2348.0	.3639011	.303171	2.47	21.00	174.00	8.30000	372.00
2349.0	.3639011	.303171	2.50	21.00	180.00	1.18000	447.00
2350.0	.3639011	.303171	2.57	21.00	610.00	1.40000	529.00
2351.0	.3639011	.103171	2.32	21.00	510.00	6.30000	353.00
2352.0	.3639011	.103171	2.65	21.00	330.00	1.10000	378.00
2353.0	.3639011	.303171	2.62	21.00	180.00	1.10000	544.00
2354.0	.3639011	.303171	2.59	21.00	650.	1.10000	712.00
2355.0	.3639011	.703171	2.64	21.00	2100.	2.70000	713.00
2356							

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
2459.0	.3639011	.110171	2.39	10.0	185.0	2.08000	229.00
2460.0	.3639011	.110171	1.94	10.0	700.0	1.70000	379.00
2461.0	.3639011	.110171	1.99	10.0	660.0	1.44000	350.00
2462.0	.3639011	.410171	2.09	10.0	650.0	.60000	604.00
2463.0	.3639011	.110171	2.26	10.0	590.0	1.30000	348.00
2464.0	.3639011	.410171	2.31	10.0	2000.0	1.80000	652.00
2465.0	.3639011	.410171	2.32	10.0	1800.0	1.36000	594.00
2466.0	.3639011	.410171	2.35	10.0	2000.0	1.64000	470.00
2467.0	.3639011	.410171	2.00	10.0	4900.0	2.56000	727.00
2468.0	.3639011	.410171	2.45	10.0	5800.0	2.10000	635.00
2469.0	.3639011	.410171	2.26	10.0	6600.0	5.00000	988.00
2470.0	.3639011	.110171	2.58	10.0	4200.0	1.56000	529.00
2471.0	.3639011	.410171	1.88	10.0	3500.0	1.30000	864.00
2472.0	.3639011	.110171	1.89	10.0	4100.0	2.65000	539.00
2473.0	.3639011	.110171	2.76	10.0	130.0	.61000	213.00
2485.0	.3639011	.111171	2.49	10.0	41.00	.17000	55.000
2486.0	.3639011	.111171	2.48	10.0	73.00	.48000	104.00
2487.0	.3639011	.111171	2.42	10.0	58.00	.77000	94.000
2488.0	.3639011	.611171	2.25	10.0	74.00	.60000	163.00
2489.0	.3639011	.111171	2.40	10.0	144.0	.94000	118.00
2490.0	.3639011	.111171	2.59	2.00	81.00	.24000	137.00
2491.0	.3639011	.111171	2.50	2.00	66.00		130.00
2492.0	.3639011	.611171	2.46	2.00	93.00	.23000	222.00
2493.0	.3639011	.611171	2.47	2.00	104.0	.55000	166.00
2494.0	.3639011	.611171	2.68	2.00	290.0	.29000	173.00
2495.0	.3639011	.611171	2.79	2.00	353.0	.37000	222.00
2496.0	.3639011	.611171	2.65	2.00	183.0	1.31000	293.00
2497.0	.3639011	.611171	2.48	2.00	1400.0	.79000	446.00
2498.0	.3639011	.611171	2.49	2.00	2000.0	1.30000	364.00
2499.0	.3639011	.311171	2.77	2.00	6900.0	.80000	390.00
9500.0	.3639011	.311171	2.48	2.00	5650.0	1.05000	333.00
2501.0	.3639011	.411171	2.33	2.00	6050.0	2.50000	317.00
2502.0	.3639011	.411171	2.43	2.00	2650.0	.70000	475.00
2503.0	.3639011	.411171	2.31	2.00	4300.0	2.14000	385.00
2519.0	.4649000	.205441	2.24	21.0	110.0	2.04000	1024.0
2520.0	.4649000	.205441	2.10	21.0	59.00	1.04000	1043.0
2521.0	.4649000	.205441	2.35	21.0	110.0	2.00000	1103.0
2522.0	.4649000	.205441	2.47	21.0	110.0	2.00000	1017.0
2523.0	.4649000	.305441	2.41	21.0	270.0	3.54000	1277.0
2524.0	.4649000	.305441	2.41	21.0	215.0	1.29000	1284.0
2525.0	.4649000	.405441	2.81	21.0	87.00		1054.0
2526.0	.4649000	.205441	2.68	21.0	235.0	2.19000	1112.0
2527.0	.4649000	.405441	2.49	21.0	680.0	1.10000	1343.0
2528.0	.4649000	.805441	2.49	21.0	620.0	1.07000	1873.0
2529.0	.4649000	.805441	2.49	21.0	730.0	1.43000	1776.0
2530.0	.4649000	.805441	2.49	21.0	770.0	3.62000	1437.0
2531.0	.4649000	.805441	2.58	21.0	7500.0	2.86000	1530.0
2532.0	.4649000	.805441	2.63	21.0	2800.0	3.62100	2980.0
2533.0	.4649000	.805441	2.59	21.0	7500.0	2.44600	1833.0
2534.0	.4649000	.805441	2.27	21.0	2600.0	2.88000	1776.0
2535.0	.4649000	.805441	2.38	21.0	2500.0	2.90000	2025.0
2536.0	.4649000	.805441	2.06	21.0	2500.0	2.94000	1876.0
2537.0	.4649000	.805441	2.56	21.0	4700.0	2.06000	2570.0
2538.0	.4649000	.805441	2.77	21.0	5300.0	.35300	2470.0
2539.0	.4649000	.106441	2.50	21.0	67.00	.85000	183.00
2540.0	.4649000	.106441	2.27	21.0	73.00	.75000	184.00
2541.0	.4649000	.106441	2.60	21.0	47.00	.56.000	174.00
2542.0	.4649000	.106441	2.58	21.0	150.0	.81000	260.00
2543.0	.4649000	.106441	2.58	21.0	170.0	1.00000	245.00
2544.0	.4649000	.106441	2.38	21.0	127.0	.55000	220.00
2545.0	.4649000	.106441	2.56	21.0	510.0	.60000	583.00
2546.0	.4649000	.106441	2.40	21.0	470.0	.78000	413.00
2547.0	.4649000	.106441	2.75	21.0	630.0	1.70000	412.00
2548.0	.4649000	.306441	2.68	21.0	6800.0	2.80000	1148.0
2549.0	.4649000	.206441	2.28	21.0	6800.0	3.00000	1197.0
2550.0	.4649000	.406441	2.78	21.0	6700.0	2.80000	1278.0
2551.0	.4649000	.306441	2.49	21.0	2100.0	3.10000	772.00
2552.0	.4649000	.306441	2.49	21.0	1500.0	1.50000	647.00
2553.0	.4649000	.306441	2.34	21.0	1500.0	1.00000	697.00
2554.0	.4649000	.406441	2.58	21.0	5000.0	4.10000	912.00
2555.0	.4649000	.806441	2.49	21.0	3700.0	2.50000	917.00
2556.0	.4649000	.806441	2.68	21.0	3700.0	2.10000	968.00
2557.0	.4649000	.806441	2.55	21.0	74.00	.88000	226.00
2558.0	.4649000	.806441	2.57	21.0	80.00	3.00000	793.00
2559.0	.4649000	.207441	2.57	21.0	91.00	2.70000	702.00
2560.0	.4649000	.207441	2.57	21.0	90.00	1.40000	764.00
2561.0	.4649000	.207441	2.20	21.0	70.00	1.80000	663.00
2562.0	.4649000	.207441	2.29	21.0	250.0	2.90000	1040.0
2563.0	.4649000	.207441	2.82	21.0	240.0	2.70000	997.00
2564.0	.4649000	.207441	2.67	21.0	210.0	.94000	1047.0
2565.0	.4649000	.207441	2.30	21.0	240.0	3.00000	1004.0
2566.0	.4649000	.207441	2.67	21.0	210.0	.94000	1047.0
2567.0	.4649000	.207441	2.38	21.0	760.0	2.80000	1263.0
2568.0	.4649000	.207441	2.10	21.0	770.0	2.40000	1266.0
2569.0	.4649000	.507441	2.04	21.0	360.0	3.19000	1315.0
2570.0	.4649000	.507441	2.15	21.0	780.0	3.19000	2030.0
2571.0	.4649000	.807441	2.72	21.0	2600.0	3.10000	2438.0
2572.0	.4649000	.807441	2.58	21.0	2500.0	2.90000	1735.0
2573.0	.4649000	.807441	2.12	21.0	6500.0	4.30000	2412.0
2574.0	.4649000	.807441	2.62	21.0	7200.0	4.00000	2451.0
2575.0	.4649000	.807441	2.42	21.0	7250.0	5.00000	2058.0
2576.0	.4649000	.807441	2.62	21.0	5350.0	4.60000	2353.0
2577.0	.4649000	.807441	2.15	21.0	5100.0	4.00000	2178.0
2578.0	.4649000	.807441	2.55	21.0	4800.0	4.10000	2366.0
2579.0	.4649000	.309441	2.51	10.0	110.0	2.34000	704.00
2580.0	.4649000	.309441	2.71	10.0	102.0	2.36000	953.00
2581.0	.4649000	.209441	3.10	10.0	87.00	2.20000	629.00
2582.0	.4649000	.209441	2.60	10.0	190.0	1.56000	939.00
2583.0	.4649000	.309441	3.20	10.0	203.0	1.00000	953.00
2584.0	.4649000	.209441	2.81	10.0	212.0	2.13000	1097.0
2636.0	.4649000	.309441	2.90	10.0	680.0	4.31000	1570.0
2637.0	.4649000	.309441	2.84	10.0	740.0	4.16000	1427.0
2638.0	.4649000	.309441	2.90	10.0	670.0	5.12000	1827.0
2639.0	.4649000	.809441	2.78	10.0	870.0	2.80000	1457.0
2640.0	.4649000	.809441	2.69	10.0	2400.0	4.07000	1493.0
2641.0	.4649000	.809441	2.81	10.0	2400.0	2.92000	2084.0
2642.0	.4649000	.809441	2.73	10.0	7400.0	7.30000	2153.0
2643.0	.4649000	.809441	2.90	10.0	6900.0	4.27000	2218.0
2644.0	.4649000	.809441	2.01	10.0	720.0	8.30000	2530.0
2645.0	.4649000	.809441	2.84	10.0	4500.0	4.62000	2720.0
2646.0	.4649000	.809441	2.80	10.0	3900.0	4.99000	2241.0
2647.0	.4649000	.809441	2.80	10.0	4750.0	4.81000	2227.0
2650.0	.4649000	.509441	2.47	10.0	2800.0	1.10000	1283.0
2651.0	.4649000	.312441	2.80	10.0	91.00	1.59000	475.00
2652.0	.4649000	.312441	2.69	10.0	61.00	.56000	349.00
2653.0	.4649000	.312441	2.81	10.0	81.00	.75000	462.00
2654.0	.4649000	.312441	2.70	10.0	86.00	2.20000	398.00
2655.0	.4649000	.312441	2.31	10.0	210.0	1.10000	585.00
2656.0	.4649000	.312441	2.70	10.0	185.0	1.10000	598.00
2657.0	.4649000	.912441	2.61	10.0	170.0	.88000	682.00
2658.0	.4649000	.512441	2.40	10.0	154.0	.62000	689.00
2659.0	.4649000	.312441	2.41	10.0	730.0	3.39000	1004.0
2660.0	.4649000	.312441	2.40	10.0	720.0	3.02000	890.00
2661.0	.4649000	.312441	2.69	10.0	680.0	1.81000	1018.0
2662.0	.4649000	.312441	2.76	10.0	690.0	3.00000	911.00
2663.0	.4649000	.312441	2.10	10.0	350.0	5.00000	1305.0
2664.0	.4649000	.312441	2.61	10.0	2400.0	4.83000	1307.0
2665.0	.4649000	.212441	2.58	10.0	2150.0	4.50000	1383.0
2666.0	.4649000	.312441	2.71	10.0	650.0	4.22000	1517.0
2667.0	.4649000	.312441	2.63	10.0	610.0	3.89000	1471.0
2668.0	.4649000	.312441	2.76	10.0	610.0	3.06000	1305.0
2669.0	.4649000	.312441	2.43	10.0	610.0	4.67000	1104.0
2670.0	.4649000	.812441	2.43	10.0	4900.0	3.33000	1847.0
2671.0	.4649000	.312441	2.68	10.0	3600.0	.97000	1097.0
2672.0	.4649000	.312441	2.90	10.0	4400.0	2.57000	1443.0
2673.0	.4649000	.312441	2.60	10.0	4300.0	3.34000	1457.0
2688.0							

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG	ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
2812.0	.4649090	.316441	2.71	5.00	63.00	.640000	348.00	2973.0	.4640090	.822441	2.40	2.00	6150.	3.15000	1600.0
2813.0	.4649090	.316441	2.58	5.00	195.00	1.130000	622.00	2974.0	.4640090	.822441	2.15	2.00	5600.	2.60000	1611.0
2814.0	.4649090	.316441	2.21	5.00	190.00	1.800000	568.00	2975.0	.4640090	.822441	2.45	2.00	6400.	6.00000	1600.0
2815.0	.4649090	.316441	2.78	5.00	190.00	2.100000	469.00	2976.0	.4640090	.323441	2.68	10.0	115.0	2.91000	1306.0
2816.0	.4649090	.316441	2.09	5.00	162.00	.570000	411.00	2977.0	.4640090	.323441	3.08	10.0	130.0	1.91000	1283.0
2817.0	.4649090	.316441	2.30	5.00	750.00	2.940000	792.00	2978.0	.4640090	.223441	3.10	10.0	66.00	1.36000	1363.0
2818.0	.4649090	.316441	2.06	5.00	700.00	.800000	547.00	2979.0	.4640090	.323441	2.97	10.0	159.0	3.60000	1227.0
2819.0	.4649090	.316441	2.64	5.00	750.00	2.350000	647.00	2980.0	.4640090	.323441	2.49	10.0	240.0	2.18000	1630.0
2820.0	.4649090	.316441	2.20	5.00	730.00	2.300000	590.00	2981.0	.4640090	.323441	2.61	10.0	220.0	2.80000	1420.0
2821.0	.4649090	.316441	2.13	5.00	2000.	3.130000	885.00	2982.0	.4640090	.323441	3.10	10.0	220.0	5.29000	1348.0
2822.0	.4649090	.316441	2.06	5.00	2000.	2.100000	903.00	2983.0	.4640090	.323441	2.71	10.0	210.0	1.34000	1112.0
2823.0	.4649090	.316441	2.20	5.00	1750.	2.400000	674.00	2984.0	.4640090	.823441	2.69	10.0	810.0	4.16000	2090.0
2824.0	.4649090	.316441	2.30	5.00	2100.	1.670000	882.00	2985.0	.4640090	.823441	2.48	10.0	720.0	2.31000	1727.0
2825.0	.4649090	.316441	2.71	5.00	5500.	2.490000	979.00	2986.0	.4640090	.823441	2.68	10.0	800.0	4.71000	2079.0
2826.0	.4649090	.316441	2.88	5.00	6150.	3.350000	1564.00	2987.0	.4640090	.823441	2.60	10.0	2700.	3.40000	2157.0
2827.0	.4649090	.316441	2.37	5.00	2540.	.650000	983.00	2988.0	.4640090	.823441	2.41	10.0	2500.	3.60000	2597.0
2828.0	.4649090	.316441	2.80	5.00	3800.	2.080000	1110.00	2989.0	.4640090	.823441	2.68	10.0	2600.	7.00000	2333.0
2829.0	.4649090	.316441	2.81	5.00	4100.	3.400000	1179.00	2990.0	.4640090	.823441	2.71	10.0	4600.	7.00000	2333.0
2830.0	.4649090	.316441	2.50	5.00	4000.	1.610000	1104.00	2991.0	.4640090	.823441	2.40	10.0	4800.	4.39000	1054.0
2831.0	.4649090	.316441	2.72	5.00	5500.	1.960000	1126.00	2992.0	.4640090	.823441	2.55	10.0	4900.	3.85000	2729.0
2832.0	.4649090	.316441	2.47	5.00	5900.	3.400000	1386.00	2993.0	.4640090	.823441	2.60	10.0	5500.	4.07000	2990.0
2833.0	.4649090	.317441	2.23	2.00	59.00	.350000	643.00	2994.0	.4640090	.123441	2.68	10.0	6150.	3.95000	2670.0
2834.0	.4649090	.317441	2.49	2.00	45.00	1.700000	439.00	2995.0	.4640090	.823441	2.50	10.0	6700.	3.63000	2823.0
2841.0	.4649090	.317441	2.40	2.00	48.00	2.200000	436.00	3022.0	.4640090	.124441	2.42	5.00	150.0	3.83000	1113.0
2842.0	.4649090	.317441	2.39	2.00	43.00	.305000	538.00	3023.0	.4640090	.124441	2.49	5.00	110.0	1.67000	983.00
2843.0	.4649090	.317441	2.58	2.00	150.00	.570000	539.00	3024.0	.4640090	.124441	2.30	5.00	140.0	1.00000	903.00
2855.0	.4649090	.917441	2.40	2.00	140.00	.620000	682.00	3025.0	.4640090	.124441	2.40	5.00	128.0	1.62000	1054.0
2856.0	.4649090	.917441	2.36	2.00	148.00	.730000	759.00	3026.0	.4640090	.124441	2.40	5.00	240.0	4.00000	1111.0
2857.0	.4649090	.917441	2.80	2.00	140.00	.710000	658.00	3027.0	.4640090	.124441	2.50	5.00	120.0	1.163.00	1163.0
2858.0	.4649090	.917441	2.70	2.00	650.00	1.360000	757.00	3028.0	.4640090	.124441	2.38	5.00	210.0	2.19000	1088.0
2859.0	.4649090	.317441	2.61	2.00	540.00	1.520000	625.00	3029.0	.4640090	.124441	2.18	5.00	224.0	2.44000	1005.0
2860.0	.4649090	.917441	2.67	2.00	640.00	1.260000	750.00	3030.0	.4640090	.124441	2.49	5.00	785.0	2.66000	1442.0
2861.0	.4649090	.317441	2.60	2.00	2300.	1.960000	927.00	3031.0	.4640090	.124441	2.33	5.00	750.0	2.68000	1393.0
2862.0	.4649090	.317441	2.69	2.00	1900.	2.290000	896.00	3032.0	.4640090	.124441	2.33	5.00	870.0	2.30000	1307.0
2863.0	.4649090	.317441	2.78	2.00	1900.	1.770000	911.00	3033.0	.4640090	.324441	2.28	5.00	710.0	4.30000	1364.0
2864.0	.4649090	.317441	2.75	2.00	4000.	1.580000	975.00	3034.0	.4640090	.224441	2.47	5.00	2500.	2.98000	1533.0
2865.0	.4649090	.317441	2.59	2.00	3700.	1.650000	875.00	3035.0	.4640090	.824441	2.80	5.00	2800.	5.20000	2400.0
2866.0	.4649090	.917441	2.49	2.00	3000.	1.150000	1010.00	3036.0	.4640090	.824441	2.32	5.00	2200.	2.41000	1713.0
2867.0	.4649090	.917441	2.63	2.00	4900.	2.090000	1018.00	3037.0	.4640090	.824441	2.57	5.00	5350.	2.26000	989.00
2870.0	.4649090	.317441	2.90	2.00	5800.	1.720000	1124.00	3038.0	.4640090	.824441	2.80	5.00	4550.	3.37000	2253.0
2885.0	.4649045	.319441	2.78	2.00	34.00	.100000		3039.0	.4640090	.824441	2.27	5.00	4200.	3.02000	1775.0
2886.0	.4649045	.319441	2.61	2.00	20.00	.061000		3040.0	.4640090	.824441	2.10	5.00	7200.	3.77000	2093.0
2887.0	.4649045	.319441	2.59	2.00	6.00	.053000		3041.0	.4640090	.824441	2.19	5.00	6400.	3.95000	2016.0
2888.0	.4649045	.319441	2.59	2.00	42.00	.038000		3042.0	.4640090	.824441	2.76	5.00	7200.	4.68000	2392.0
2889.0	.4649045	.319441	2.46	2.00	37.00	.057000		3043.0	.4640090	.824441	2.29	5.00	4100.	4.83000	1734.0
2890.0	.4649045	.319441	2.85	2.00	130.00	.076000		3044.0	.4640090	.824441	2.68	21.0	120.0	1.90000	1484.0
2891.0	.4649045	.319441	2.67	2.00		.088000		3045.0	.4640090	.824441	2.76	21.0	110.0	1.90000	1320.0
2892.0	.4649045	.319441	2.50	2.00	45.00	.042000		3046.0	.4640090	.224441	2.75	21.0	110.0	4.33000	1997.0
2893.0	.4649045	.319441	2.67	2.00	200.00	.051000		3047.0	.4640090	.424441	2.78	21.0	104.0	3.00000	1373.0
2894.0	.4649045	.319441	2.35	2.00	400.00	.070000		3048.0	.4640090	.424441	2.58	21.0	230.0	5.90000	1957.0
2895.0	.4649045	.319441	2.66	2.00	390.00	.150000		3049.0	.4640090	.124441	2.81	21.0	230.0	3.40000	1731.0
2896.0	.4649045	.319441	2.75	2.00	780.00	.523000	226.00	3050.0	.4640090	.324441	2.70	21.0	190.0	2.30000	1663.0
2897.0	.4649045	.319441	2.60	2.00	1200.	.920000	258.00	3052.0	.4640090	.826441	2.75	21.0	850.0	5.04000	2745.0
2898.0	.4649045	.319441	2.53	2.00	1500.	1.300000	250.00	3053.0	.4640090	.826441	2.72	21.0	750.0	4.35000	2534.0
2899.0	.4649045	.319441	2.67	2.00	2900.	1.000000	352.00	3054.0	.4640090	.826441	2.73	21.0	800.0	4.03000	2246.0
2900.0	.4649045	.319441	2.49	2.00	3000.	1.400000	387.00	3055.0	.4640090	.826441	2.40	21.0	710.0	3.62000	2252.0
2901.0	.4649045	.319441	2.70	2.00	3250.	1.300000	419.00	3056.0	.4640090	.826441	2.69	21.0	27.00	4.11000	3119.0
2902.0	.4649045	.319441	2.80	2.00	5600.	3.200000	447.00	3057.0	.4640090	.826441	2.62	21.0	2650.	3.23000	3119.0
2903.0	.4649045	.319441	2.67	2.00	5400.	1.800000	431.00	3058.0	.4640090	.826441	2.35	21.0	2700.	6.30000	3119.0
2904.0	.4649045	.319441	2.78	2.00	4200.	2.000000	394.00	3059.0	.4640090	.826441	2.57	21.0	5400.	5.40000	3125.0
2905.0	.4649045	.319441	2.75	2.00	4900.	1.300000	676.00	3060.0	.4640090	.826441	2.10	21.0	5400.	4.60000	3317.0
2920.0	.4649090	.120441	2.53	2.00	58.00	.095000	185.00	3061.0	.4640090	.826441	2.70	21.0	5400.	5.04000	3527.0
2921.0	.4649090	.120441	2.74	2.00	76.00	.340000	279.00	3062.0	.4640090	.826441	2.39	21.0	7100.	4.00000	3088.0
2922.0	.4649090	.120441	2.28	2.00	91.00	.570000	341.00	3063.0	.4640090	.826441	2.60	21.0	7300.	6.70000	3673.0
2923.0	.4649090	.120441	2.00	2.00	61.00	.800000	411.00	3064.0	.4640090	.826441	2.55	21.0	6750.	8.77000	3033.0
2924.0	.4649090	.321441	2.50	2.00	145.00	1.100000	210.00	3064.1	.4640090	.826441	2.60	21.0	7300.	4.53000	2220.0
2925.0	.4649090	.221441	2.61	2.00	200.00	3.100000	387.00	3065.0	.4640090	.826441	2.70	21.0	7500.	6.08000	3900.0
2926.0	.4649090	.221441	2.70	2.00	135.00	.900000	355.00	3067.0	.4649090	.129531	3.10	5.00	96.00	1.80000	530.00
2927.0	.4649090	.221441	2.70	2.00	125.00	.820000	198.00	3068.0	.4649090	.129531	2.80	5.00	79.00	3.20000	575.00
2928.0	.4649090	.321441	2.33	2.00	420.00	.940000	432.00	3069.0	.4649090	.129531	3.08	5.00	70.00	.680000	410.00
2929.0	.46490														

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG	ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
3134.0	.4649000	.830531	2.98	5.00	5700.	2.99000	1444.0	3319.0	.4644590	.137441	2.59	5.00	49.00	.350000	426.00
3135.0	.4649000	.830531	2.10	5.00	4000.	1.94000	932.00	3320.0	.4644590	.137441	2.89	5.00	170.00	.810000	543.00
3136.0	.4649000	.230531	2.87	5.00	4300.	2.11000	1370.00	3321.0	.4644590	.137441	2.51	5.00	150.00	.950000	522.00
3137.0	.4649000	.230531	2.33	5.00	3300.	4.20000	845.00	3322.0	.4644590	.137441	2.51	5.00	160.00	1.390000	494.00
3152.0	.4649045	.131531	2.80	5.00	4000.		36.000	3323.0	.4644590	.137441	2.72	5.00	640.00	1.980000	710.00
3153.0	.4649045	.131531	2.80	5.00	56.00	.410000	69.000	3324.0	.4644590	.137441	2.59	5.00	730.00	3.200000	1202.00
3154.0	.4649045	.131531	2.80	5.00	36.00	.110000	36.000	3325.0	.4644590	.137441	2.75	5.00	590.00	1.250000	746.00
3155.0	.4649045	.131531	2.86	5.00	86.00	.590000	77.000	3326.0	.4644590	.137441	2.60	5.00	1650.	1.540000	926.00
3156.0	.4649045	.131531	2.40	5.00	79.00		50.000	3327.0	.4644590	.237441	2.80	5.00	1900.	.780000	1153.00
3157.0	.4649045	.131531	2.01	5.00	130.00	.800000	105.000	3328.0	.4644590	.337441	2.50	5.00	2100.	2.300000	1124.00
3158.0	.4649045	.131531	2.80	5.00	127.00	.650000	74.000	3329.0	.4644590	.237441	2.61	5.00	4590.	2.730000	1376.00
3159.0	.4649045	.131531	2.01	5.00	440.00	1.060000	162.000	3330.0	.4644590	.337441	2.78	5.00			1420.00
3160.0	.4649045	.131531	2.90	5.00	437.00	.970000	157.000	3331.0	.4644590	.837441	2.57	5.00	4400.	2.660000	1318.00
3161.0	.4649045	.131531	2.01	5.00	460.00	1.340000	169.000	3332.0	.4644590	.837441	2.75	5.00	5600.	2.260000	1410.00
3162.0	.4649045	.131531	2.80	5.00	445.00	.630000	173.000	3333.0	.4644590	.837441	2.72	5.00	5000.	1.600000	1410.00
3163.0	.4649045	.131531	2.95	5.00	1300.	1.300000	272.000	3334.0	.4644590	.837441	2.72	5.00	6800.	2.760000	1406.00
3164.0	.4649045	.131531	2.92	5.00	1700.	1.660000	297.000	3356.0	.4642290	.338441	2.59	5.00	6800.	2.140000	768.00
3165.0	.4649045	.131531	2.80	5.00	1300.	.590000	293.000	3357.0	.4642290	.138441	2.50	5.00	5900.	.860000	466.00
3166.0	.4649045	.131531	2.80	5.00	4150.	2.300000	345.000	3358.0	.4642290	.338441	2.60	5.00	4700.	.600000	970.00
3167.0	.4649045	.131531	2.80	5.00	3900.	2.910000	373.000	3359.0	.4642290	.138441	2.50	5.00	6400.	1.800000	795.00
3168.0	.4649045	.131531	2.80	5.00	4000.	1.700000	354.000	3360.0	.4642290	.138441	2.50	5.00	3700.	.370000	536.00
3169.0	.4649045	.131531	2.07	5.00	5100.	2.900000	469.000	3361.0	.4642290	.138441	2.61	5.00	5200.	.590000	499.00
3170.0	.4649045	.131531	2.00	5.00	5100.	2.100000	432.000	3362.0	.4642290	.138441	2.68	5.00	5600.	1.840000	793.00
3171.0	.4649045	.131531	2.88	5.00	4200.	1.900000	387.000	3363.0	.4642290	.138441	2.90	5.00	6200.	2.000000	761.00
3172.0	.4649045	.631531	3.06	5.00	4600.	3.500000	500.000	3364.0	.4642290	.138441	2.61	5.00	6200.	1.600000	696.00
3186.0	.4640090	.133531	2.99	5.00	104.00	2.600000	630.000	3365.0	.4646790	.138441	2.49	5.00	4800.	.990000	392.00
3187.0	.4640090	.133531	2.90	5.00	92.00	1.900000	465.000	3366.0	.4646790	.138441	2.89	5.00	6100.	.250000	342.00
3188.0	.4640090	.133531	2.91	5.00	71.00	.590000	364.000	3367.0	.4646790	.138441	2.99	5.00	4800.	.430000	273.00
3189.0	.4640090	.133531	2.39	5.00	188.00	2.400000	594.000	3368.0	.4646790	.138441	2.89	5.00	3600.	.280000	336.00
3190.0	.4640090	.133531	2.59	5.00	92.00	1.560000	564.000	3369.0	.4646790	.138441	2.75	5.00	2900.	1.500000	361.00
3191.0	.4640090	.133531	2.79	5.00	250.00	2.430000	664.000	3370.0	.4646790	.138441	2.58	5.00	4400.	.850000	351.00
3192.0	.4640090	.333531	2.60	5.00	740.00	2.560000	856.000	3371.0	.4646790	.138441	2.78	5.00	4400.	.510000	390.00
3193.0	.4640090	.133531	2.88	5.00	190.00	1.720000	629.000	3372.0	.4646790	.138441	2.86	5.00	5300.	.560000	349.00
3194.0	.4640090	.333531	2.79	5.00	660.00	2.470000	704.000	3385.0	.4649067	.140441	2.60	5.00	4700.	1.300000	386.00
3195.0	.4640090	.133531	2.79	5.00	600.00	2.710000	778.000	3386.0	.4649067	.140441	2.61	5.00	3500.	.260000	389.00
3196.0	.4640090	.333531	2.58	5.00	720.00	3.040000	994.000	3387.0	.4649067	.140441	2.60	5.00	2500.	.250000	250.00
3197.0	.4640090	.833531	2.83	5.00	2400.	2.720000	1255.000	3388.0	.4649067	.140441	2.70	5.00	3800.	1.400000	245.00
3198.0	.4640090	.833531	2.68	5.00	2300.	4.400000	1263.000	3389.0	.4649067	.140441	2.52	5.00	4300.	.830000	406.00
3199.0	.4640090	.833531	2.51	5.00	2200.	3.500000	1233.000	3390.0	.4649067	.140441	2.52	5.00	4200.	.750000	229.00
3200.0	.4640090	.833531	2.80	5.00	4500.	5.800000	1348.000	3391.0	.4649067	.140441	2.44	5.00	5900.	1.300000	337.00
3201.0	.4640090	.833531	2.68	5.00	4500.	3.000000	1427.000	3392.0	.4649067	.140441	2.58	5.00	3940.	.800000	203.00
3202.0	.4640090	.833531	2.68	5.00	4000.	3.850000	1374.000	3393.0	.4649022	.140441	2.60	5.00	4500.	.510000	356.00
3203.0	.4640090	.833531	2.80	5.00	6100.	3.180000	1573.000	3394.0	.4649022	.340441	2.61	5.00	4900.	.740000	317.00
3204.0	.4640090	.833531	2.90	5.00	6400.	4.200000	2095.000	3395.0	.4649022	.340441	2.73	5.00	4400.	.700000	280.00
3205.0	.4640090	.833531	2.50	5.00	6300.	2.880000	1384.000	3396.0	.4649022	.140441	2.62	5.00	4600.	1.100000	309.00
3206.0	.4640090	.833531	2.98	5.00	6300.	4.000000	1586.000	3397.0	.4649022	.140441	2.58	5.00	5200.	.250000	308.00
3207.0	.4640090	.833531	2.58	5.00	4150.	3.500000	1356.000	3398.0	.4649022	.140441	2.68	5.00	4300.	.350000	455.00
3234.0	.4640090	.434531	2.90	2.00	680.00	2.900000	642.000	3399.0	.4649022	.140441	2.70	5.00	4700.	.670000	341.00
3235.0	.4640090	.134531	2.65	2.00	690.00	2.480000	520.000	3400.0	.4649022	.940441	2.70	5.00	4300.	.330000	465.00
3236.0	.4640090	.434531	3.20	2.00	660.00	2.100000	545.000	3401.0	.4649090	.102441	1.68	5.00	9400.	1.600000	305.10
3237.0	.4640090	.134531	3.10	2.00	667.00	1.700000	532.000	3402.0	.4649090	.102441	1.85	5.00	8000.	.710000	278.90
3238.0	.4640090	.134531	2.80	2.00	660.00	1.620000	557.000	3403.0	.4649090	.102441	1.66	5.00	5400.	.260000	249.60
3239.0	.4640090	.134531	2.69	2.00	640.00	1.300000	643.000	3404.0	.4649090	.102441	1.67	5.00	9500.	.830000	190.20
3240.0	.4640090	.134531	3.19	2.00	615.00	1.500000	544.000	3405.0	.4649090	.102441	1.54	5.00	1760.	1.700000	501.00
3241.0	.4640090	.134531	3.08	2.00	645.00	1.600000	585.000	3406.0	.4649090	.102441	1.25	5.00	1800.	1.090000	348.70
3242.0	.4649045	.134531	2.80	2.00	370.00	.284000	94.000	3407.0	.4649090	.102441	1.47	5.00	1920.	1.690000	471.00
3243.0	.4649045	.134531	2.70	2.00	310.00	.630000	99.000	3408.0	.4649090	.102441	1.63	5.00	1700.	1.500000	473.10
3244.0	.4649045	.134531	2.66	2.00	360.00	.372000	101.000	3409.0	.4649090	.102441	1.44	5.00	7600.	3.700000	611.00
3245.0	.4649045	.134531	2.61	2.00	400.00	.750000	132.000	3410.0	.4649090	.102441	1.85	5.00	5800.	.880000	428.60
3246.0	.4649045	.134531	2.70	2.00	280.00	.360000	93.000	3411.0	.4649090	.102441	1.90	5.00	7000.	2.700000	580.80
3247.0	.4649045	.134531	2.50	2.00	372.00	.570000	125.000	3412.0	.4649090	.102441	1.51	5.00	8900.	1.900000	647.10
3248.0	.4649045	.134531	2.15	2.00	312.00	.250000	89.000	3413.0	.4649090	.402441	1.29	5.00	1500.	1.100000	583.30
3249.0	.4649045	.134531	2.05	2.00	328.00	.600000	133.000	3414.0	.4649090	.502441	1.24	5.00	1600.	1.050000	573.30
3262.0	.4649090	.135531	2.83	2.00	550.00	1.400000	493.000	3415.0	.4649090	.402441	1.48	5.00	1400.	1.560000	969.20
3263.0	.4649090	.135531	2.20	2.00	530.00	1.900000	512.000	3416.0	.4649090	.802441	1.43	5.00	5900.	2.700000	750.40
3264.0	.4649090	.135531	2.30	2.00	670.00	3.400000	577.000	3417.0	.4649090	.802441	1.64	5.00	4900.	2.500000	1347.00
3265.0	.4649090	.135531	2.68	2.00	610.00	1.000000	484.000	3418.0	.4649090	.802441	1.76	5.00	4500.	2.890000	1194.20
3266.0	.4649090	.135531	3.05	2.00	620.00	2.580000	540.000	3419.0	.4649090	.802441	1.71	5.00	6950.	6.000000	1290.20
3267.0	.4649090	.135531	2.89	2.00	490.00	.750000	374.000	3420.0	.4649090	.802441	1.71	5.00	7700.	2.630000	637.60
3268.0	.4649090	.135531	2.78	2.0											

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
3473.0	.6649045	.105441	1.78	5.00	84.00	.700000	64.100
3474.0	.6649045	.105441	1.69	5.00	44.00	.330000	75.200
3479.0	.6649045	.105441	1.55	5.00	170.00	.550000	89.500
3480.0	.6649045	.105441	2.10	5.00		.200000	51.500
3481.0	.6649045	.105441	1.50	5.00	85.00	.350000	91.100
3482.0	.6649045	.105441	1.73	5.00	87.00	.220000	46.700
3483.0	.6649045	.105441	1.39	5.00	450.00	1.140000	168.000
3484.0	.6649045	.105441	1.48	5.00	360.00	.660000	137.800
3485.0	.6649045	.105441	1.54	5.00	420.00	1.200000	138.600
3486.0	.6649045	.105441	1.55	5.00	350.00	.410000	153.700
3487.0	.6649045	.105441	1.47	5.00	1500.00	1.900000	310.600
3488.0	.6649045	.105441	1.80	5.00	1200.00	.880000	259.100
3489.0	.6649045	.105441	1.52	5.00	1400.00	1.100000	299.500
3490.0	.6649045	.105441	1.39	5.00	1300.00	.890000	225.800
3491.0	.6649045	.105441	1.68	5.00	3100.00	1.530000	418.800
3492.0	.6649045	.105441	1.52	5.00	2850.00	.820000	294.800
3493.0	.6649045	.105441	1.79	5.00	4000.00	1.500000	340.700
3494.0	.6649045	.105441	1.77	5.00	5100.00	1.640000	422.600
3495.0	.6649045	.105441	1.84	5.00	4100.00	2.050000	427.900
3496.0	.6649045	.105441	2.04	5.00	5300.00	2.400000	433.900
3525.0	.6649090	.306441	1.57	5.00	128.00	1.680000	742.800
3526.0	.6649090	.306441	1.54	5.00	96.00	1.200000	599.700
3527.0	.6649090	.306441	1.47	5.00	130.00	2.400000	780.600
3528.0	.6649090	.306441	1.61	5.00	105.00	1.530000	750.600
3529.0	.6649090	.306441	1.75	5.00	700.00	3.250000	1197.600
3530.0	.6649090	.306441	1.45	5.00	600.00	2.000000	939.600
3532.0	.6649090	.306441	2.04	5.00	700.00	3.000000	969.200
3533.0	.6649090	.306441	1.64	5.00	685.00	2.030000	975.900
3534.0	.6649090	.306441	1.35	5.00	600.00	3.740000	1157.800
3535.0	.6649090	.306441	1.37	5.00	700.00	3.520000	832.200
3536.0	.6649090	.306441	1.36	5.00	5200.00	2.860000	584.600
3537.0	.6649090	.306441	1.34	5.00	5500.00	4.260000	164.744
3538.0	.6649090	.306441	1.44	5.00	5400.00	3.500000	1857.800
3539.0	.6649090	.306441	1.70	5.00	110.00	2.580000	1489.600
3540.0	.6649090	.306441	1.72	5.00	95.00	1.840000	878.700
3541.0	.6649090	.306441	1.70	5.00	66.00	.410000	806.300
3542.0	.6649090	.306441	1.68	5.00	120.00	3.000000	930.000
3543.0	.6649090	.306441	1.70	5.00	740.00	2.080000	1456.100
3544.0	.6649090	.306441	1.70	5.00	740.00	3.240000	1615.800
3545.0	.6649090	.306441	1.70	5.00	740.00	2.500000	1281.500
3546.0	.6649090	.306441	1.70	5.00	730.00	3.700000	1531.600
3547.0	.6649090	.306441	1.70	5.00	700.00	3.100000	1246.600
3548.0	.6649090	.306441	1.64	5.00	730.00	4.300000	1857.800
3549.0	.6649090	.306441	1.77	5.00	7200.00	4.400000	1993.000
3550.0	.6649090	.306441	1.70	5.00	7900.00	5.530000	2398.300
3551.0	.6649090	.306441	1.74	5.00	6100.00	1.700000	1032.200
3552.0	.6649090	.306441	1.56	5.00	189.00	1.700000	831.500
3553.0	.6649090	.306441	1.53	5.00	170.00	.900000	569.800
3554.0	.6649090	.306441	1.52	5.00	130.00	.920000	747.400
3555.0	.6649090	.306441	1.62	5.00	195.00	1.200000	519.300
3556.0	.6649090	.306441	1.49	5.00	200.00	4.800000	1376.100
3557.0	.6649090	.306441	1.48	5.00	2700.00	11.000000	1829.300
3558.0	.6649090	.306441	1.84	5.00	2500.00	2.280000	1128.500
3559.0	.6649090	.306441	1.50	5.00	2200.00	3.700000	1268.400
3560.0	.6649090	.306441	1.49	5.00	5700.00	3.700000	1448.800
3561.0	.6649090	.306441	1.30	5.00	4300.00	3.030000	1477.900
3562.0	.6649090	.306441	1.74	5.00	4400.00	7.700000	1871.400
3563.0	.6649090	.306441	1.52	5.00	4100.00	3.980000	1724.400
3564.0	.6649090	.306441	1.74	5.00	196.00	1.400000	1076.500
3565.0	.6649090	.306441	1.89	5.00	200.00	2.500000	1011.400
3567.0	.6649090	.306441	1.99	5.00	190.00	1.900000	984.000
3568.0	.6649090	.306441	1.51	5.00	2500.00	3.200000	1898.400
3569.0	.6649090	.306441	1.92	5.00	2500.00	3.400000	1682.400
3570.0	.6649090	.306441	1.50	5.00	2400.00	5.700000	1633.300
3571.0	.6649090	.306441	1.70	5.00	2300.00	3.180000	1703.500
3572.0	.6649090	.306441	1.92	5.00	3700.00	1.900000	2020.000
3573.0	.6649090	.306441	1.69	5.00	4000.00	4.420000	2202.400
3574.0	.6649090	.306441	2.19	5.00	5000.00	3.790000	1993.000
3575.0	.6649090	.306441	1.71	5.00	4800.00	4.300000	2026.700
3602.0	.6644590	.308441	1.41	5.00	570.00	1.820000	546.900
3603.0	.6644590	.308441	1.36	5.00	440.00	1.040000	339.200
3604.0	.6644590	.308441	1.34	5.00	590.00	1.240000	621.500
3605.0	.6644590	.308441	1.35	5.00	640.00	3.200000	546.900
3606.0	.6644590	.308441	1.67	5.00	600.00	1.350000	601.900
3607.0	.6644590	.308441	1.71	5.00	570.00	2.000000	685.600
3608.0	.6644590	.308441	1.63	5.00	560.00	1.600000	697.600
3609.0	.6644590	.308441	1.83	5.00	640.00	2.200000	681.100
3610.0	.6644590	.308441	1.70	5.00	670.00	1.910000	781.900
3611.0	.6644590	.308441	1.79	5.00	690.00	3.200000	745.900
3612.0	.6644590	.308441	1.86	5.00	520.00	1.350000	562.700
3613.0	.6644590	.308441	1.61	5.00	720.00	2.160000	885.600
3614.0	.6644590	.308441	1.62	5.00	490.00	2.200000	910.000
3615.0	.6644590	.308441	1.70	5.00	660.00	2.300000	743.600
3616.0	.6644590	.308441	1.74	5.00	712.00	3.000000	989.200
3628.0	.6649000	.309441	1.34	5.00	520.00	1.190000	561.200
3630.0	.6649000	.309441	1.38	5.00	480.00	.810000	592.900
3631.0	.6649000	.309441	1.34	5.00	546.00	1.800000	664.500
3632.0	.6649000	.309441	2.02	5.00	180.00	1.300000	213.900
3633.0	.6649000	.309441	1.56	5.00	190.00	1.190000	249.600
3634.0	.6649000	.309441	1.40	5.00	140.00	.690000	216.300
3635.0	.6649000	.309441	1.44	5.00	174.00	1.400000	403.700
3636.0	.6649000	.309441	1.63	5.00	380.00	.720000	364.500
3637.0	.6649000	.309441	1.98	5.00	630.00	.900000	560.500
3638.0	.6649000	.309441	1.67	5.00	480.00	1.000000	261.500
3639.0	.6649000	.309441	1.80	5.00	570.00	2.300000	415.100
3640.0	.6649000	.309441	1.46	5.00	1700.00	1.260000	432.400
3641.0	.6649000	.309441	1.45	5.00	1650.00	1.700000	607.200
3642.0	.6649000	.309441	1.59	5.00	1700.00	1.830000	433.900
3643.0	.6649000	.309441	1.62	5.00	1700.00		261.500
3644.0	.6649000	.309441	1.71	5.00	6000.00	3.400000	860.000

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
3645.0	.6649090	.309441	1.61	5.00	5400.00	3.970000	971.500
3646.0	.6649090	.309441	1.60	5.00			277.300
3647.0	.6649090	.309441	1.49	5.00			277.300
3648.0	.6649045	.111441	1.61	2.00	94.00	.670000	64.900
3649.0	.6649045	.111441	2.29	2.00	86.00	.380000	54.600
3648.0	.6649045	.111441	1.93	2.00	113.00	.390000	57.000
3669.0	.6649045	.111441	1.90	2.00	97.00	.290000	49.900
3670.0	.6649045	.111441	2.27	2.00	109.00	.350000	61.800
3671.0	.6649045	.111441	1.93	2.00	63.00	.130000	41.200
3672.0	.6649045	.111441	2.27	2.00	390.00	1.400000	103.300
3673.0	.6649045	.111441	2.60	2.00	360.00	.790000	71.300
3674.0	.6649045	.111441	1.70	2.00	365.00	.700000	103.000
3675.0	.6649045	.111441	1.67	2.00	334.00	.650000	138.800
3676.0	.6649045	.111441	2.04	2.00	300.00	.500000	95.100
3677.0	.6649045	.111441	2.70	2.00	180.00	.760000	220.300
3678.0	.6649045	.111441	1.86	2.00	135.00	1.600000	230.600
3679.0	.6649045	.111441	2.80	2.00	130.00	.900000	174.300
3680.0	.6649045	.111441	2.08	2.00	100.00	.590000	151.500
3681.0	.6649045	.111441	2.10	2.00	235.00	.740000	265.400
3682.0	.6649045	.111441	2.08	2.00	260.00	1.400000	237.700
3683.0	.6649045	.111441	2.70	2.00	190.00	1.300000	225.000
3684.0	.6649045	.111441	2.19	2.00	320.00	.620000	252.800
3685.0	.6649045	.111441	2.08	2.00	380.00	1.300000	255.100
3686.0	.6649045	.111441	2.01	2.00	510.00	1.290000	332.800
3687.0	.6649045	.111441	1.60	2.00	400.00	1.700000	263.100
3688.0	.6649045	.111441	1.88	2.00	350.00	1.030000	233.700
3706.0	.6649090	.112441	1.52	2.00	97.00	.880000	178.300
3707.0	.6649090	.112441	1.80	2.00	90.00	.460000	233.700
3708.0	.6649090	.112441	1.43	2.00	118.00	1.300000	235.300
3709.0	.6649090	.112441	1.80	2.00	79.00	.380000	221.900
3710.0	.6649090	.112441	1.37	2.00	140.00	.700000	217.900

EXHIBIT 1-2 TENSION DATA, REDUCED

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
0141.0	.4129090	.14082	4.41	14.3	86.00	138.00	
0143.0	.4129090	.14082	3.82	14.3	180.00	105.00	
0144.0	.4129090	.14082	3.82	14.3	90.00	74.0000	
0145.0	.4129090	.14082	3.82	14.3	140.00	93.0000	
0146.0	.4129090	.14082	3.82	14.3	160.00	97.0000	
0147.0	.4129090	.14082	3.82	14.3	130.00	76.0000	
0154.0	.5149045	.140602	2.69	6.00	170.00	87.5000	
0155.0	.5149045	.140602	2.29	6.00	190.00	81.0000	
0156.0	.5149045	.140602	2.29	6.00	170.00	106.0000	
0163.0	.5149045	.140602	2.37	6.00	130.00	87.0000	
0164.0	.5149045	.140602	2.37	6.00	140.00	53.5000	
0165.0	.5149045	.140602	2.37	6.00	190.00	104.0000	
0176.0	.5149045	.140602	2.53	6.00	270.00	33.5000	
0177.0	.5149045	.140602	2.53	6.00	160.00	50.0000	
0178.0	.5149045	.140602	2.53	6.20	280.00	92.0000	
0179.0	.5149045	.140602	1.86	6.00	250.00	75.0000	
0180.0	.5149045	.140602	1.86	6.00	230.00	97.0000	
0181.0	.5149045	.140602	1.86	6.00	261.00	116.0000	
0185.0	.5149045	.140602	2.37	6.00	140.00	92.0000	
0186.0	.5149045	.140602	2.37	6.00	160.00	147.0000	
0195.0	.5130090	.140082	2.85	2.00	520.00	308.0000	
0418.0	.2329090	.140062	3.25	4.00	420.00	2.150000	72.1000
0419.0	.2329090	.140062	5.66	14.3	330.00	2.500000	95.3000
0435.0	.2329090	.140062	6.06	14.3	290.00	2.100000	51.0000
0438.0	.2329090	.140062	6.06	14.3	400.00	2.100000	30.8000
0442.0	.2329090	.140062	6.00	14.3	320.00	44.0000	
0445.0	.2329090	.140062	5.17	14.3	140.00	1.800000	41.9000
0450.0	.2329090	.140062	5.17	14.3	160.00	3.300000	44.2000
0451.0	.2329090	.140062	5.17	14.3	120.00	2.000000	45.9000
0455.0	.2329090	.140062	5.87	14.3	45.00	1.900000	47.8000
0456.0	.2329090	.140062	5.87	14.3	49.00	3.800000	64.9000
0464.0	.2329090	.140082	5.77	14.3	47.00	2.400000	98.9000
0471.0	.2329090	.140082	6.17	14.3	49.00	3.500000	111.3000
0474.0	.2329090	.140082	6.17	14.3	130.00	2.700000	100.5000
0479.0	.2329090	.140082	4.92	14.3	48.00	3.200000	120.6000
0480.0	.2329090	.140082	4.92	14.3	46.00	1.800000	60.3000
0482.0	.2329090	.140072	4.92	14.3	46.00	1.900000	45.5000
0486.0	.2329090	.140072	4.84	14.3	110.00	3.100000	77.6000
0489.0	.2329090	.140072	4.84	14.3	110.00	3.800000	110.4000
0491.0	.2329090	.140072	4.84	14.3	110.00	3.800000	46.9000
0494.0	.2339011	.140182	2.98	10.0	47.00	1.700000	48.9000
0500.0	.2339011	.140182	2.98	10.0	44.00	2.100000	76.7000
0501.0	.2339011	.140182	2.98	10.0	51.00	3.200000	63.0000
0502.0	.2339011	.140182	2.98	10.0	75.00	3.100000	59.0000
0503.0	.2339011	.140182	2.70	10.0	89.00		83.8000
0507.0	.2339011	.140182	2.70	10.0	43.00	1.300000	51.9000
0511.0	.2339011	.140182	2.70	10.0	48.00	1.000000	77.1000
0515.0	.3349045	.140282	2.44	6.00	45.00		73.0000
0516.0	.3349045	.140282	2.44	6.00	47.00		92.0000
0517.0	.3349045	.140282	2.44	6.00	45.00		106.0000
0518.0	.3349045	.140282	2.44	6.00	45.00		55.0000
0519.0	.3349045	.140282	2.44	6.00	44.00		71.0000
0520.0	.3349045	.140282	2.44	6.00	45.00		77.0000
0521.0	.3349045	.140282	2.44	6.00	44.00		71.0000
0522.0	.3349045	.140282	2.44	6.00	47.00		78.0000
0523.0	.3349045	.140282	2.44	6.00	46.00		70.0000
0524.0	.3349045	.140282	2.44	6.00	39.00		80.0000
0525.0	.3349045	.140282	2.41	6.00	38.00		74.0000
0525.1	.3349045	.140282	2.41	6.00	40.00		78.0000
0526.0	.3349045	.140282	2.41	6.00	37.00		59.0000
0527.0	.3349045	.140282	2.41	6.00	36.00	2.400000	74.0000
0528.0	.3349045	.140282	2.41	6.00	40.00	2.300000	97.4000
0529.0	.3349045	.140282	2.41	6.00	39.00	2.500000	72.0000
0530.0	.3349045	.140282	2.56	14.3	47.00	3.200000	66.0000
0531.0	.3349045	.140282	2.56	14.3	47.00	2.900000	69.0000
0532.0	.3349045	.140282	2.56	14.3	48.00	1.700000	66.0000
0533.0	.3349045	.140282	2.56	14.3	46.00	1.500000	55.0000
0534.0	.3349045	.140282	2.84	14.3	46.00	3.200000	81.0000
0535.0	.3349045	.140282	2.84	14.3	47.00	1.200000	83.0000
0536.0	.3349045	.140282	2.84	14.3	44.00	1.500000	70.0000
0537.0	.3349045	.140282	2.84	14.3	44.00	1.900000	89.3000
0538.0	.3349045	.140282	2.84	14.3	44.00	1.800000	57.0000
0539.0	.3349045	.140282	2.85	14.3	44.00	1.500000	29.0000
0540.0	.3349045	.140282	2.85	14.3	46.00	1.700000	107.7000
0541.0	.3349045	.140282	2.85	14.3	42.00	1.300000	64.0000
0542.0	.3349045	.140282	3.16	14.3	38.00	1.900000	75.0000
0543.0	.3349045	.140282	3.16	14.3	40.00	1.700000	84.0000
0544.0	.3349045	.140282	3.16	14.3	37.00	1.600000	59.0000
0545.0	.3349045	.140282	3.16	14.3	40.00	1.700000	78.0000
0546.0	.3349045	.140282	2.39	14.3	44.00	1.900000	79.0000
0547.0	.3349045	.140282	2.39	14.3	38.00	1.800000	73.0000
0548.0	.3349045	.140282	2.39	14.3	36.00	1.900000	64.0000
0549.0	.3349045	.140282	2.90	4.00	46.00	1.900000	83.0000
0550.0	.3349045	.140282	2.90	4.00	51.00	1.600000	81.0000
0551.0	.3349045	.140282	2.62	4.00	48.00	1.800000	50.0000
0552.0	.3349045	.140282	2.62	4.00	48.00	2.200000	113.0000
0553.0	.3349045	.140282	2.62	4.00	46.00	1.200000	38.0000
0554.0	.3349045	.140282	2.62	4.00	33.00	1.100000	32.0000
0555.0	.3349045	.140282	2.90	4.00	46.00	1.200000	36.0000
0556.0	.3349045	.140282	2.90	4.00	44.00	1.200000	38.0000
0557.0	.3349045	.140282	2.90	4.00	44.00	1.300000	69.2000
0558.0	.3349045	.140282	2.91	4.00	43.00	1.900000	39.0000
0559.0	.3349045	.140282	2.91	4.00	44.00	1.200000	46.0000
0560.0	.3349045	.140282	2.91	4.00	49.00	1.300000	69.0000
0561.0	.3349045	.140282	2.93	4.00	41.00	2.500000	80.0000
0562.0	.3349045	.140282	2.93	4.00	39.00	1.800000	73.0000
0563.0	.3349045	.140282	2.93	4.00	52.00	2.000000	95.0000
0564.0	.3349045	.140282	3.30	4.00	33.00	1.300000	49.0000
0565.0	.3349045	.140422	3.30	4.00	53.00	2.000000	42.0000
0566.0	.3349045	.140422	3.30	4.00	32.00	1.700000	87.0000
0567.0	.3349045	.140422	2.57	4.00	32.00	1.200000	33.5000
0568.0	.3349045	.140422	2.57	4.00	31.00	1.500000	45.0000
0569.0	.3349045	.140422	2.57	4.00	31.00	1.400000	62.0000
0617.0	.3329090	.140042	5.23	21.0	430.00	5.700000	117.4000
0618.0	.3329090	.140042	5.23	21.0	390.00	4.500000	146.0000
0619.0	.3329090	.140042	5.23	21.0	400.00	3.800000	94.4000
0621.0	.3329090	.140042	5.23	21.0	410.00	3.500000	115.0000
0623.0	.3329090	.140042	5.23	21.0	440.00	4.700000	134.0000
0625.0	.3329090	.140042	3.62	21.0	150.00	6.700000	138.0000
0627.0	.3329090	.140042	3.62	21.0	140.00	6.800000	127.0000
0637.0	.3329090	.140042	4.91	21.0	130.00	4.100000	132.0000
0638.0	.3329090	.140042	4.91	21.0	140.00	5.100000	50.0000
0641.0	.3329090	.140042	3.33	21.0	95.00	6.600000	149.0000
0644.0	.3329090	.140042	3.33	21.0	97.00	2.800000	125.0000
0646.0	.3329090	.140042	3.33	21.0	96.00	5.400000	80.0000
0648.0	.3329090	.140042	3.33	21.0	97.00	4.000000	134.0000
0649.0	.3329090	.140042	3.33	21.0	96.00	4.300000	113.0000
0689.0	.3319011	.140042	5.10	14.3	26.00		78.0000
0692.0	.3319011	.140042	5.10	14.3	40.00		93.8000
0694.0	.3319011	.140042	5.10	14.3	40.00	3.000000	93.8000
0699.0	.3319011	.140042	5.10	14.3	43.00		83.8000
0706.0	.3319011	.140042	4.33	14.3	41.00		99.0000
0707.0	.3319011	.140042	4.33	14.3	44.00		93.8000
0708.0	.3319011	.140042	4.33	14.3	210.00		125.8000
0739.0	.3319011	.140042	4.33	14.3	180.00		110.5000
0714.0	.3319011	.140042	4.33	14.3	230.00		127.3000
0720.0	.3319011	.140042	4.33	14.3	7.6000		124.2000
0725.0	.3319011	.140042	4.33	14.3	12.0000		181.5000
0725.0	.3319011	.140042	4.33	14.3	10.0000		146.5000
0727.0	.3319011	.140042	3.88	14.3	14.0000		97.0000
0727.1	.3319011	.140042	4.33	14.3	270.00		130.5000
0729.0	.3319011	.140042	3.88	14.3	280.00		126.8000
0733.0	.3329090	.140022	2.64	14.3	330.00		131.2000
0734.0	.3329090	.140022	2.64	14.3	310.00		159.4000
0735.0	.3329090	.140022	2.64	14.3	280.00		105.0000
0736.0	.3329090	.140022	2.64	14.3	310.00		101.5000
0758.0	.3319011	.140042	5.25	14.3	77.00		

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
7961.0	.8449000	.147122	.230	10.0	33.00	2.90000	91.300
0963.0	.8449000	.147122	.230	10.0	32.00		80.300
0964.0	.8449000	.147122	.230	10.0	64.00		92.000
0965.0	.8449000	.147122	.230	10.0	66.00		106.10
0966.0	.8449000	.248122	.230	10.0	28.00	3.30000	68.300
0967.0	.8449000	.151122	.230	10.0	33.00	3.50000	101.000
0970.0	.8449000	.151122	.230	10.0	24.00	2.80000	67.500
0972.0	.8449000	.151122	.230	10.0	93.00	7.30000	100.200
0973.0	.8449000	.151122	.230	10.0	89.00	2.10000	73.200
0975.0	.8449000	.151122	.230	10.0	46.00	1.40000	59.300
0977.0	.8449000	.160092	.230	10.0			64.300
0979.0	.8449000	.160092	.230	10.0	130.0	4.30000	73.600
0980.0	.8449000	.160092	.230	10.0	130.0	3.70000	65.300
0984.0	.8449000	.161062	.230	10.0	140.0	4.80000	80.000
0985.0	.8449000	.161062	.230	10.0	150.0		77.800
0987.0	.8449000	.161062	.230	10.0	150.0	4.30000	62.000
0990.0	.8449000	.162062	.230	10.0	9.500	2.00000	79.100
0992.0	.8449000	.162062	.230	10.0	10.00	1.60000	37.600
0994.0	.8449000	.162062	.230	10.0	9.200	2.80000	65.300
0996.0	.8449000	.162062	.230	10.0	50.00	11.00000	92.500
0998.0	.8449000	.164062	.230	10.0	9.300	1.80000	36.200
1001.0	.8449000	.164062	.230	10.0	9.300	4.80000	34.600
1002.0	.8449000	.164062	.230	10.0	9.000	1.00000	35.800
1007.0	.8449000	.165202	.210	10.0			92.700
1009.0	.8449000	.165202	.210	10.0	150.0	7.80000	115.600
1010.0	.8449000	.165202	.210	10.0	130.0	10.30000	78.400
1011.0	.8449000	.166202	.210	10.0	10.00	5.40000	95.500
1014.0	.8449000	.166202	.210	10.0	9.500	8.00000	107.900
1015.1	.8449000	.266202	.210	10.0	9.900	8.60000	119.000
1015.2	.8449000	.167202	.210	10.0	10.00	8.60000	109.000
1017.0	.8449000	.168202	.210	10.0	10.00	2.80000	102.800
1019.0	.8449000	.168202	.210	10.0	140.0	4.80000	130.700
1021.0	.8449000	.267252	.270	10.0	8.600	4.20000	62.600
1021.1	.8449000	.167252	.270	10.0	9.000		102.200
1023.0	.8449000	.267252	.270	10.0	7.200	0.70000	64.000
1023.1	.8449000	.168252	.270	10.0	7.600	0.70000	59.900
1024.0	.8449000	.268252	.270	10.0	31.00	3.80000	74.100
1024.1	.8449000	.268252	.270	10.0	28.00	2.80000	48.600
1024.2	.8449000	.169252	.270	10.0	27.00	2.30000	79.800
1025.0	.8449000	.268252	.270	10.0	56.00	3.00000	71.000
1025.1	.8449000	.268252	.270	10.0	56.00	3.30000	61.400
1025.2	.8449000	.169252	.270	10.0	61.00	4.50000	92.800
1026.0	.8449000	.368252	.270	10.0	33.00	4.00000	51.500
1026.1	.8449000	.271252	.270	10.0	170.0	7.60000	133.800
1035.0	.8449000	.369252	.270	10.0	140.0	7.60000	133.800
1035.1	.8449000	.170252	.270	10.0	5.900	11.00000	158.000
1036.0	.8449000	.271252	.270	1.000	5.900	11.00000	158.000
1036.1	.8449000	.272252	.270	1.000	11.000	9.30000	119.000
1040.0	.8449000	.272252	.270	1.000	88.000	8.70000	85.300
1040.1	.8449000	.372252	.270	1.000	58.000	4.60000	79.100
1040.2	.8449000	.274252	.270	1.000	31.000	8.00000	111.000
1040.3	.8449000	.174252	.270	1.000			139.000
1042.0	.8449000	.273282	.190	1.000	150.0	5.80000	128.600
1042.1	.8449000	.273282	.190	1.000	130.0	6.50000	95.700
1042.2	.8449000	.374282	.190	1.000	150.0	9.10000	104.000
1042.3	.8449000	.175282	.190	1.000			139.000
1057.0	.8449000	.175282	.190	1.000	6.600	1.60000	78.700
1058.0	.8449000	.176282	.190	1.000	57.000	5.00000	106.000
1059.0	.8449000	.176282	.190	1.000	120.00	4.60000	102.000
1061.0	.8449000	.276282	.190	1.000	7.000	0.90000	58.600
1061.1	.8449000	.178282	.190	1.000			68.000
1062.0	.8449000	.278282	.190	1.000	50.000	1.10000	68.700
1062.1	.8449000	.178282	.190	1.000			95.000
1063.0	.8449000	.178282	.190	1.000	110.0	2.70000	80.400
1071.0	.8449000	.179322	.160	1.000	6.500	0.870000	52.600
1075.0	.8449000	.179322	.160	1.000	120.00	6.70000	84.200
1078.0	.8449000	.180282	.190	3.000	8.500	1.50000	57.200
1082.0	.8449000	.180282	.190	3.000	130.00	5.10000	74.000
1149.0	.2639011	.103012	6.870	10.0	3.700	2.50000	34.000
1150.0	.2639011	.103042	5.880	10.0	3.900	1.50000	34.000
1152.0	.2639011	.103012	6.870	10.0	51.00	2.80000	15.700
1124.0	.2619011	.103042	5.880	10.0	130.0	7.90000	74.100
1155.0	.2619011	.107072	4.880	10.0	100.0	3.90000	51.600
1156.0	.2619011	.107012	6.880	10.0	130.0	2.50000	59.000
1159.0	.2519011	.109042	6.600	10.0	9.000	2.4.0000	71.200
1162.0	.2639011	.107042	5.300	10.0	57.00	2.30000	40.000
1163.0	.2619011	.109072	4.880	10.0	81.00	2.50000	43.200
1164.0	.2639011	.102042	5.300	10.0	14.00	1.40000	27.000
1165.0	.2639011	.102042	5.300	10.0	150.0	1.40000	22.900
1166.0	.2639011	.102072	4.800	10.0	75.00	3.40000	57.000
1167.0	.2639011	.103072	4.800	2.000	68.00	2.70000	40.800
1175.0	.2639011	.103072	4.800	2.000	12.00	1.30000	28.900
1178.0	.2639011	.103042	5.300	2.000	72.00	1.80000	49.000
1180.0	.2639011	.104042	5.300	2.000	13.00	1.60000	19.000
1182.0	.2639011	.104072	4.800	2.000	4.600	1.40000	41.900
1181.0	.2639011	.104042	5.300	2.000	5.000	0.820000	31.300
1188.0	.2519011	.113042	5.800	2.000	100.00	3.50000	52.900
1192.0	.2519011	.113042	5.800	2.000	27.00	1.40000	55.600
1174.0	.2519011	.113072	5.800	2.000	15.00	1.50000	97.000
1195.0	.2519011	.113012	5.800	2.000	23.00	1.80000	69.000
1199.0	.2519011	.114072	6.600	1.000	25.00	3.30000	45.800
1205.0	.2519011	.114012	6.600	1.000			70.000
1206.0	.2519011	.114012	6.600	1.000	79.00	0.830000	30.000
1211.0	.2519011	.115072	5.800	1.000	20.00	0.940000	16.100
1212.0	.2639011	.107012	4.850	1.000	12.00		21.800
1217.0	.2639011	.109042	4.850	20.00	16.00	3.00000	80.000
1221.0	.2639011	.104012	5.310	20.00			80.800
1228.0	.2639011	.104072	2.460	20.00	75.00	4.50000	76.000
1232.0	.2639011	.105042	3.461	21.00	15.00	5.40000	58.200
1237.0	.8449000	.299152	.210	10.0	130.0		87.000

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
1237.1	.8449000	.199152	.210	20.0	120.00	2.00000	97.300
1238.0	.8449000	.299152	.210	21.0	6.500	2.00000	67.100
1238.1	.8449000	.299152	.210	1.000	4.000	1.60000	27.000
1253.0	.2639011	.104042	3.461	1.000	6.500	1.90000	27.400
1254.0	.2639011	.108072	2.460	1.000			27.400
1260.0	.2639011	.102072	2.460	1.000	68.00	2.20000	38.400
1262.0	.2639011	.109042	3.461	1.000	69.00	2.10000	32.200
1263.0	.2639011	.109112	2.850	1.000	9.300	3.00000	20.500
1264.0	.2639011	.109112	2.850	1.000			43.300
1282.0	.2619011	.103012	5.260	5.000	56.00	1.80000	39.600
1287.0	.2639011	.103042	3.590	5.000	5.800	2.60000	54.700
1288.0	.2639011	.103042	3.590	5.000	69.00	2.40000	50.500
1291.0	.2639011	.103012	5.260	5.000	5.000	1.40000	44.700
1298.0	.2639011	.104072	2.500	5.000	5.000	1.50000	64.400
1301.0	.2639011	.204072	2.500	5.000	85.00	4.50000	66.600
1303.1	.2639011	.204072	2.500	5.000	68.00	4.80000	59.900
1303.2	.2639011	.105072	2.500	5.000	72.00	3.00000	65.200
1310.0	.2639011	.104042	3.460	5.000	16.00	2.40000	67.300
1315.0	.2639011	.104042	3.590	5.000	87.00	2.40000	52.200
1322.0	.2639011	.109112	2.670	5.000	5.000	1.00000	55.100
1323.0	.2639011	.109112	2.670	5.000	62.00		53.200
1446.0	.2629090	.127172	3.880	10.0	21.00	5.70000	65.000
1447.0	.2629090	.128172	3.880	10.0	140.00	5.70000	67.000
1448.0	.2629090	.128172	3.880	10.0	190.00	8.40000	106.000
1449.0	.2629090	.128172	3.880	10.0	390.00	7.60000	126.600
1450.0	.2629090	.129172	3.880	10.0	930.00	8.70000	134.000
1454.0	.2639011	.130012	4.490	20.0	590.00	7.10000	122.000
1455.0	.2639011	.130012	4.490	21.0	0.200	4.80000	103.000
1456.0	.2639011	.132012	4.490	21.0	270.00	6.00000	127.000
1457.0	.2639011	.132012	4.490	21.0	680.00	8.20000	185.000
1458.0	.2639011	.136012	4.490	21.0	110.00	7.10000	117.000
1465.0	.2639011	.136012	4.490	21.0	120.00	0.7.20000	101.000
1470.0	.2639011	.339012	4.490	21.0	420.00	8.20000	117.000
1486.0	.3639011	.105012	3.880	21.0	26.00	6.90000	96.000
1487.0	.3639011	.106012	3.880	21.0	700.00	3.30000	111.000
1487.1	.3639011	.106012	3.8				

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
1918.0	.3649090	.119442	3.15	5.00	24.00	8.90000	169.30
1919.0	.3649090	.119442	2.35	5.00	1300.	9.30000	207.50
1920.0	.3649090	.119442	3.10	5.00	980.0	10.0000	219.50
1921.0	.3649090	.119442	2.35	5.00	1300.	7.20000	213.50
1940.0	.3640090	.112442	2.80	5.00	17.00	5.10000	189.70
1940.1	.3640090	.112442	2.70	5.00			235.50
1941.0	.3640090	.112442	2.80	5.00			208.50
1941.1	.3640090	.112442	2.80	5.00	41.00	20.0000	230.90
1942.0	.3640090	.112442	2.91	5.00			118.70
1942.1	.3640090	.112442	2.91	5.00	30.00	14.0000	214.00
1942.2	.3640090	.112442	2.91	5.00			202.90
1943.0	.3640090	.112442	2.92	5.00	18.00	5.00000	245.50
1943.1	.3640090	.112442	2.92	5.00	35.00	4.30000	260.00
1944.0	.3640090	.112442	2.92	5.00	1700.	8.30000	255.50
1945.0	.3640090	.112442	2.95	5.00	1000.	18.0000	252.80
1946.0	.3640090	.112442	2.95	5.00			228.20
1946.1	.3640090	.112442	2.95	5.00	1700.	17.0000	298.60
1947.0	.3640090	.112442	2.95	5.00	1800.	9.50000	239.00
1947.1	.3640090	.112442	2.95	5.00	1700.	9.30000	254.00
1948.0	.3649000	.114442	2.95	5.00	26.00	6.80000	131.30
1949.0	.3649000	.114442	3.15	5.00	24.00	6.50000	109.00
1950.0	.3649000	.114442	2.55	5.00	21.00	5.80000	117.30
1951.0	.3649000	.114442	3.20	5.00	1000.	9.30000	141.40
1952.0	.3649000	.114442	3.23	5.00	1300.	9.40000	159.30
1953.0	.3649000	.114442	2.63	5.00	1500.	13.0000	123.50
1954.0	.3649000	.114442	3.00	5.00	1900.	10.0000	141.70
1955.0	.3649000	.114442	3.16	5.00	1900.	10.0000	129.20
1956.0	.3649000	.114442	2.55	5.00	1700.	9.10000	124.30
1979.0	.3649000	.118442	2.55	2.00	35.00	6.30000	78.900
1980.0	.3649000	.118442	2.20	2.00	42.00	6.70000	85.500
1981.0	.3649000	.118442	2.95	2.00	28.00	6.00000	106.30
1982.0	.3649000	.119442	3.25	2.00	890.0	19.0000	104.80
1983.0	.3649000	.119442	3.34	2.00	640.0	2.40000	96.400
1984.0	.3649000	.119442	3.45	2.00	620.0	8.70000	104.60
1985.0	.3649000	.119442	3.16	2.00	1500.	11.0000	109.30
1986.0	.3649000	.119442	3.35	2.00	140.0	12.0000	100.60
1987.0	.3649000	.119442	3.44	2.00	1600.	6.90000	139.00
2001.0	.3649090	.119442	2.60	2.00	330.0	4.10000	53.300
2002.0	.3649090	.119442	2.80	2.00	1200.	8.00000	138.50
2003.0	.3649090	.119442	2.80	2.00	1200.	11.8000	135.50
2004.0	.3649090	.119442	2.80	2.00	33.00		180.50
2005.0	.3649090	.119442	2.80	2.00	29.00	5.60000	95.000
2006.0	.3649090	.120442	2.80	2.00	20.00	4.50000	145.00
2007.0	.3649090	.120442	2.65	2.00	17.00	3.60000	117.50
2008.0	.3649090	.120442	2.90	2.00	940.0		113.10
2009.0	.3649090	.120442	2.50	2.00	1100.	5.70000	89.000
2010.0	.3649045	.120442	2.80	2.00	960.0	4.10000	127.50
2012.0	.3649045	.120442	2.70	2.00	1100.	5.10000	144.50
2013.0	.3649045	.120442	3.18	2.00	1100.	5.40000	65.500
2038.0	.3649045	.121442	2.60	2.00	1500.	1.90000	74.800
2039.0	.3649045	.121442	2.35	2.00	1500.	2.30000	74.600
2040.0	.3649045	.121442	2.80	2.00	1500.	9.50000	71.000
2041.0	.3649045	.121442	3.11	2.00	990.0	5.20000	127.00
2042.0	.3649045	.121442	2.80	2.00	1100.	4.30000	120.00
2043.0	.3649045	.121442	2.90	2.00	1200.	5.10000	145.00
2044.0	.3649045	.121442	3.10	2.00	1200.	4.40000	145.20
2054.0	.3649090	.122442	2.80	2.10	47.00	7.50000	185.30
2055.0	.3649090	.122442	2.83	2.10	41.00	8.50000	198.30
2056.0	.3649090	.122442	2.15	2.10	51.00	9.10000	157.30
2057.0	.3649090	.122442	2.83	2.10	2000.	17.0000	151.60
2058.0	.3649090	.122442	2.70	2.10	2600.	17.0000	152.80
2059.0	.3649090	.122442	2.70	2.10	3400.	10.0000	175.00
2069.0	.3649000	.122442	2.80	2.10	2200.	8.50000	148.00
2070.0	.3649000	.122442	2.80	2.10	2200.	2.80000	144.60
2071.0	.3649000	.122442	2.60	2.10	2300.	6.80000	126.30
2072.0	.3649000	.122442	2.80	2.10	1300.	15.0000	197.00
2073.0	.3649000	.122442	3.35	2.10	1500.	9.10000	130.30
2074.0	.3649000	.122442	2.60	2.10	1200.	9.30000	147.00
2081.0	.3649045	.122442	2.32	2.10	1700.	3.20000	102.70
2082.0	.3649045	.122442	2.70	2.10	2600.	3.70000	100.50
2084.0	.3649045	.122442	2.70	2.10	2000.	7.00000	106.00
2085.0	.3649045	.122442	2.70	2.10	2800.	9.40000	144.00
2109.0	.3639011	.104012	4.15	10.00	1400.	5.10000	110.30
2110.0	.3639011	.101012	4.26	10.00	1800.	4.20000	98.500
2111.0	.3639011	.101012	3.85	10.00	1700.	3.70000	97.200
2112.0	.3639011	.101012	3.98	10.00	940.0	4.80000	123.60
2113.0	.3639011	.101012	3.79	10.00	675.0	7.70000	138.80
2114.0	.3639011	.101012	3.76	10.00	795.0	6.00000	119.20
2115.0	.3639011	.101012	3.88	10.00	140.0	5.50000	117.60
2139.0	.3639011	.102042	3.30	10.00	1500.	1.80000	91.300
2140.0	.3639011	.102042	3.26	10.00	1300.	2.60000	104.70
2141.0	.3639011	.102042	2.90	10.00	1300.	2.20000	90.000
2142.0	.3639011	.102042	2.80	10.00	950.0	6.80000	138.00
2143.0	.3639011	.102042	2.87	10.00	810.0	6.10000	121.50
2144.0	.3639011	.102042	3.20	10.00	800.0	8.30000	128.00
2145.0	.3639011	.102042	3.00	10.00	150.0	4.80000	108.30
2146.0	.3639011	.102042	3.00	10.00	150.0	5.60000	124.80
2167.0	.3639011	.103042	3.00	5.00	1300.		93.500
2168.0	.3639011	.103042	3.00	5.00	1400.		94.300
2169.0	.3639011	.103042	3.00	5.00	1300.	6.40000	92.000
2170.0	.3639011	.103042	3.00	5.00	800.0		95.000
2171.0	.3639011	.103042	3.00	5.00	810.0	8.00000	148.70
2172.0	.3639011	.103042	3.05	5.00	760.0	5.90000	120.30
2173.0	.3639011	.103042	3.00	5.00	130.0	6.30000	91.200
2174.0	.3639011	.103042	3.00	5.00	910.0	4.80000	77.600
2175.0	.3639011	.103042	3.00	5.00	630.0	5.10000	104.80
2196.0	.3639011	.104012	3.35	5.00	1300.	2.00000	91.200
2197.0	.3639011	.104012	3.88	5.00	1400.	2.90000	79.500
2198.0	.3639011	.104012	3.71	5.00	1500.	1.90000	76.800
2199.0	.3639011	.104012	3.55	5.00	760.0	6.30000	104.80

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
2200.0	.3639011	.104012	3.55	5.00			109.00
2201.0	.3639011	.104012	3.55	5.00	1000.		97.000
2202.0	.3639011	.104012	3.47	5.00			104.80
2203.0	.3639011	.104012	3.85	5.00			93.100
2204.0	.3639011	.104012	3.60	5.00	120.0	1.70000	97.000
2205.0	.3649045	.124442	2.69	5.00	160.0	4.10000	73.200
2205.1	.3649045	.124442	2.69	2.00	140.0	3.20000	68.500
2206.0	.3649045	.124442	3.51	5.00	1200.	6.80000	143.50
2233.0	.3639011	.105042	3.19	2.00	150.0		65.000
2234.0	.3639011	.105042	3.41	2.00	160.0	1.40000	64.100
2235.0	.3639011	.105042	2.90	2.00	130.0	2.40000	86.400
2236.0	.3639011	.105042	3.19	2.00	700.0	10.0000	79.200
2237.0	.3639011	.105042	3.09	2.00			86.400
2238.0	.3639011	.105042	3.10	2.00	770.0	9.80000	59.800
2238.1	.3639011	.107062	3.10	2.00	700.0	12.0000	86.300
2239.0	.3639011	.105042	2.92	2.00	110.0	5.90000	77.400
2240.0	.3639011	.105042	2.98	2.00	130.0		86.400
2241.0	.3639011	.105042	2.90	2.00	120.0	7.30000	91.800
2242.0	.3639011	.105042	2.92	2.00	100.0		77.400
2243.0	.3639011	.105042	2.47	2.00	110.0	3.60000	81.000
2244.0	.3639011	.107012	3.65	2.00	110.0	2.10000	78.500
2245.0	.3639011	.107012	3.40	2.00	130.0	1.50000	58.700
2265.0	.3639011	.107012	3.66	2.00	120.0		51.500
2267.0	.3639011	.107012	3.73	2.00	130.0	2.50000	77.400
2268.0	.3639011	.107012	3.31	2.00	410.0	7.70000	97.900
2269.0	.3639011	.107012	3.31	2.00	430.0		92.700
2270.0	.3639011	.107012	3.31	2.00	470.0	5.50000	105.10
2271.0	.3639011	.107012	3.49	2.00	430.0	7.00000	98.700
2272.0	.3639011	.107012	3.70	2.00			97.900
2273.0	.3639011	.107012	3.56	2.00	110.0	2.30000	83.600
2274.0	.3639011	.107012	3.36	2.00	110.0	2.80000	87.500
2275.0	.3639011	.107012	3.43	2.00			67.500
2298.0	.3639011	.109012	2.98	2.10	180.0	6.40000	97.000
2299.0	.3639011	.109012	3.19	2.10	190.0	5.30000	94.300
2300.0	.3639011	.109012	2.80	2.10	190.0	4.80000	98.700
2301.0	.3639011	.109012	2.72	2.10	170.0	4.30000	129.90
2302.0	.3639011	.109012	2.30	2.10	960.0		133.40
2303.0	.3639011	.109012	2.39	2.10	1100.</		

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
2487.0	.4649011	.111172	2.71	10.0	140.0	5.00000	91.000
2488.0	.4649011	.111172	2.74	10.0	120.0	4.60000	66.200
2489.0	.4649011	.111172	2.54	2.00	9.500	2.00000	72.7000
2490.0	.4649011	.111172	2.51	2.00	10.000	9.80000	57.0000
2491.0	.4649011	.111172	2.64	2.00	9.600	8.70000	44.6000
2492.0	.4649011	.111172	2.64	2.00	9.000	1.10000	65.0000
2493.0	.4649011	.111172	2.31	2.00	71.000	4.30000	57.0000
2494.0	.4649011	.111172	2.77	2.00	71.000	5.90000	47.0000
2495.0	.4649011	.111172	2.59	2.00	71.000	6.20000	51.0000
2496.0	.4649011	.111172	2.56	2.00	63.000	4.70000	62.0000
2497.0	.4649011	.111172	2.53	2.00	56.000	4.10000	60.0000
2498.0	.4649011	.111172	2.47	2.00	100.000	3.30000	67.200
2499.0	.4649011	.111172	2.58	3.00	150.000	3.00000	98.0000
2500.0	.4649011	.111172	2.62	2.00	100.000	3.50000	80.0000
2501.0	.4649011	.111172	2.75	2.00	100.000	4.60000	77.0000
2502.0	.4649000	.115442	2.68	21.00	21.000	6.00000	146.000
2503.0	.4649000	.115442	2.10	21.00	21.000	75.0000	124.93
2504.0	.4649000	.115442	2.38	21.00	19.000	129.000	114.50
2505.0	.4649000	.115442	2.27	21.00	17.000	118.000	142.70
2506.0	.4649000	.115442	2.69	21.00	17.000	7.90000	167.50
2507.0	.4649000	.115442	2.68	21.00	17.000	10.0000	162.30
2508.0	.4649000	.115442	2.68	21.00	21.000	8.80000	126.50
2509.0	.4649000	.115442	2.67	21.00	12.000	2.70000	85.0000
2510.0	.4649000	.115442	2.41	21.00	11.000	2.40000	88.0000
2511.0	.4649000	.115442	2.41	21.00	17.000	2.40000	92.6000
2512.0	.4649000	.115442	2.68	21.00	18.000	3.70000	94.1000
2513.0	.4649000	.115442	2.68	21.00	14.000	4.70000	141.000
2514.0	.4649000	.115442	2.45	21.00	10.000	6.80000	169.70
2515.0	.4649000	.115442	2.55	21.00	10.000	6.50000	138.90
2516.0	.4649000	.115442	2.67	21.00	10.000	8.00000	110.80
2517.0	.4649000	.115442	2.51	21.00	15.000	5.20000	113.20
2518.0	.4649000	.115442	2.42	21.00	15.000	4.50000	164.10
2519.0	.4649000	.115442	2.55	21.00	16.000	6.10000	141.40
2520.0	.4649000	.115442	2.28	21.00	16.000	5.30000	141.40
2521.0	.4649000	.115442	2.69	21.00	15.000	10.6000	106.90
2522.0	.4649000	.115442	2.38	21.00	19.000	2.50000	244.60
2523.0	.4649000	.115442	2.45	21.00	22.000	2.60000	149.80
2524.0	.4649000	.115442	2.45	21.00	15.000	5.80000	165.20
2525.0	.4649000	.115442	2.15	21.00	15.000	10.0000	226.00
2526.0	.4649000	.115442	2.49	21.00	13.000	10.0000	274.30
2527.0	.4649000	.115442	2.38	21.00	11.000	11.0000	204.30
2528.0	.4649000	.115442	2.33	21.00	12.000	188.80	
2529.0	.4649000	.115442	2.53	21.00	12.000	12.0000	255.70
2530.0	.4649000	.115442	2.53	21.00	12.000	77.4000	
2531.0	.4649000	.115442	2.18	21.00	18.000	9.00000	151.70
2532.0	.4649000	.115442	2.01	21.00	18.000	14.0000	195.00
2533.0	.4649000	.115442	2.34	21.00	18.000	8.40000	213.60
2534.0	.4649000	.115442	2.69	21.00	18.000	12.0000	119.50
2535.0	.4649000	.115442	2.73	10.00	12.000	14.7000	
2536.0	.4649000	.115442	2.81	10.00	12.000	6.40000	82.5000
2537.0	.4649000	.115442	2.59	10.00	12.000	11.0000	128.20
2538.0	.4649000	.115442	2.67	10.00	11.000	9.60000	166.50
2539.0	.4649000	.115442	2.55	10.00	8.000	10.0000	168.80
2540.0	.4649000	.115442	2.93	10.00	8.000	13.0000	118.50
2541.0	.4649000	.115442	2.71	10.00	8.000	14.0000	139.60
2542.0	.4649000	.115442	2.80	10.00	14.000	11.0000	116.30
2543.0	.4649000	.115442	2.72	10.00	15.000	14.0000	139.60
2544.0	.4649000	.115442	2.88	10.00	15.000	11.0000	178.80
2545.0	.4649000	.115442	2.98	10.00	14.000	8.30000	166.90
2546.0	.4649000	.115442	2.66	10.00	20.000	9.20000	169.80
2547.0	.4649000	.115442	2.49	10.00	20.000	7.70000	160.80
2548.0	.4649000	.115442	2.77	10.00	20.000	148.90	
2549.0	.4649000	.115442	2.77	10.00	20.000	10.0000	68.0000
2550.0	.4649000	.115442	2.83	10.00	6.000	9.20000	196.60
2551.0	.4649000	.115442	2.50	10.00	11.000	10.0000	181.70
2552.0	.4649000	.115442	2.77	10.00	11.000	11.0000	170.40
2553.0	.4649000	.115442	2.77	10.00	21.000	6.30000	162.90
2554.0	.4649000	.115442	2.55	10.00	8.000	9.40000	181.70
2555.0	.4649000	.115442	2.61	10.00	11.000	9.00000	266.00
2556.0	.4649000	.115442	2.91	10.00	20.000	12.0000	177.50
2557.0	.4649000	.115442	2.87	10.00	21.000	12.0000	177.50
2558.0	.4649000	.115442	2.78	10.00	20.000	6.50000	177.50
2559.0	.4649000	.115442	2.67	10.00	19.000	9.00000	220.40
2560.0	.4649000	.115442	2.56	10.00	12.000	6.90000	147.10
2561.0	.4649000	.115442	2.40	10.00	8.000	5.80000	146.10
2562.0	.4649000	.115442	2.45	10.00	9.000	8.00000	135.10
2563.0	.4649000	.115442	2.80	10.00	8.000	8.60000	151.50
2564.0	.4649000	.115442	2.79	10.00	17.000	5.50000	139.20
2565.0	.4649000	.115442	2.50	10.00	15.000	4.90000	168.00
2566.0	.4649000	.115442	2.50	10.00	16.000	3.70000	115.00
2567.0	.4649000	.115442	2.58	10.00	15.000	5.50000	109.20
2568.0	.4649000	.115442	2.54	10.00	12.000	1.40000	80.9000
2569.0	.4649000	.115442	2.35	10.00	12.000	1.60000	90.9000
2570.0	.4649000	.115442	2.51	10.00	12.000	1.80000	87.9000
2571.0	.4649000	.115442	2.64	10.00	13.000	5.80000	129.10
2572.0	.4649000	.115442	2.58	10.00	15.000	6.30000	118.80
2573.0	.4649000	.115442	2.99	5.00	11.000	8.00000	116.30
2574.0	.4649000	.115442	2.59	5.00	13.000	6.80000	125.40
2575.0	.4649000	.115442	2.30	5.00	13.000	4.50000	102.60
2576.0	.4649000	.115442	2.30	5.00	13.000	6.80000	120.40
2577.0	.4649000	.115442	2.80	5.00	7.500	10.0000	128.60
2578.0	.4649000	.115442	2.80	5.00	9.000	13.0000	128.60
2579.0	.4649000	.115442	2.73	5.00	9.000	6.40000	114.30
2580.0	.4649000	.115442	3.00	5.00	8.000	9.80000	155.30
2581.0	.4649000	.115442	2.74	5.00	15.000	6.10000	135.90
2582.0	.4649000	.115442	2.94	5.00	15.000	7.40000	145.50
2583.0	.4649000	.115442	2.78	5.00	15.000	7.00000	136.80
2584.0	.4649000	.115442	2.85	5.00	15.000	7.10000	145.50

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
2759.0	.4649045	.115442	2.67	5.00	75.000	6.20000	164.20
2760.0	.4649045	.115442	2.70	5.00	100.000	6.80000	120.90
2761.0	.4649045	.115442	2.75	5.00	100.000	5.70000	136.80
2762.0	.4649045	.115442	2.50	5.00	87.000	4.80000	124.00
2763.0	.4649045	.115442	2.47	5.00	150.000	4.70000	91.200
2764.0	.4649045	.115442	2.10	5.00	140.000	3.70000	88.900
2765.0	.4649045	.115442	2.61	5.00	150.000	3.70000	91.200
2766.0	.4649045	.115442	2.65	5.00	140.000	3.70000	91.200
2767.0	.4649045	.115442	2.72	5.00	140.000	3.70000	91.200
2768.0	.4649045	.115442	2.71	5.00	110.000	3.20000	77.500
2769.0	.4649045	.115442	2.64	5.00	130.000	3.30000	84.400
2770.0	.4649045	.115442	2.73	5.00	81.000	6.10000	132.30
2771.0	.4649045	.115442	2.74	5.00	81.000	6.10000	132.30
2772.0	.4649045	.115442	2.23	5.00	110.000	13.00000	181.70
2773.0	.4649099	.116442	2.23	5.00	110.000	9.30000	229.40
2774.0	.4649099	.116442	2.59	5.00	110.000	7.70000	203.50
2775.0	.4649099	.116442	2.33	5.00	110.000	9.80000	119.10
2776.0	.4649099	.116442	2.09	5.00	40.000	9.80000	189.40
2777.0	.4649099	.116442	2.70	5.00	41.000	9.80000	169.80
2778.0	.4649099	.116442	3.08	5.00	130.000	9.70000	169.80
2779.0	.4649099	.116442	2.23	5.00	37.000	7.50000	157.90
2780.0	.4649099	.116442	2.23	5.00	120.000	7.30000	119.10
2781.0	.4649099	.116442	2.33	5.00	170.000	8.50000	163.80
2782.0	.4649099	.116442	2.16	5.00	120.000	10.00000	169.80
2783.0	.4649099	.116442	2.19	5.00	120.000	4.20000	143.10
2784.0	.4649099	.116442	2.67	5.00	80.000	8.70000	169.80
2785.0	.4649099	.116442	2.60	5.00	87.000	7.70000	144.20
2786.0	.4649099	.116442	2.38	5.00	80.000	8.00000	126.90
2787.0	.4649099	.116442	2.06	5.00	80.000	6.70000	134.30
2788.0	.4649099	.116442	2.70	5.00	80.000	4.10000	105.90
2789.0	.4649099	.116442	2.60	5.00	80.000	3.70000	107.20
2790.0	.4649099	.116442	2.64	5.00	80.000	4.20000	115.60
2791.0	.4649099	.116442	2.54	5.00	80.000	4.20000	105.10
2792.0	.4649099	.116442	2.57	5.00	80.000	9.30000	105.10
2793.0	.46490						

ID	CODE 1	CODE 2	CHL	TEMP RATE	MODULUS	STRENG	ID	CODE 1	CODE 2	CHL	TEMP RATE	MODULUS	STRENG		
3016.0	.4640090	.124442	2.50	5.00	290.0	9.10000	379.80	3286.0	.4644590	.136442	2.88	5.00	200.0	10.0000	202.90
3017.0	.4640090	.124442	2.74	5.00	36.00	12.0000	297.50	3288.0	.4644590	.136442	2.79	5.00	1500.	13.0000	197.80
3018.0	.4640090	.124442	2.26	5.00	40.00	13.0000	240.00	3289.0	.4644590	.136442	2.70	5.00	1500.	11.0000	266.00
3019.0	.4640090	.124442	2.60	5.00	32.00	9.50000	244.30	3290.0	.4644590	.136442	3.10	5.00	1300.	9.80000	233.80
3020.0	.4640090	.124442	2.29	5.00	36.00	11.0000	203.20	3335.0	.4644590	.137442	2.60	5.00	1300.	9.50000	180.60
3021.0	.4640090	.124442	2.33	5.00	32.00	08.90000	195.00	3336.0	.4644590	.137442	2.79	5.00	1300.	9.60000	226.50
3066.0	.4640090	.126442	2.79	21.0	42.00	9.70000	409.30	3337.0	.4644590	.137442	2.65	5.00	420.0	15.0000	170.80
3067.0	.4640090	.226442	2.81	21.0	38.00		203.40	3338.0	.4644590	.137442	2.69	5.00	400.0	10.0000	226.60
3068.0	.4640090	.126442	2.48	21.0	40.00	8.20000	326.70	3339.0	.4644590	.137442	2.79	5.00	420.0	11.0000	187.80
3069.0	.4640090	.126442	2.81	21.0	42.00	7.90000	320.70	3340.0	.4644590	.137442	2.95	5.00	61.00	9.00000	157.00
3070.0	.4640090	.126442	2.80	21.0	38.00	13.0000	379.70	3341.0	.4644590	.137442	2.79	5.00	77.00	8.70000	178.70
3071.0	.4640090	.126442	2.76	21.0	38.00	9.10000	321.90	3342.0	.4644590	.137442	2.79	5.00	72.00	7.30000	193.80
3072.0	.4640090	.126442	2.76	21.0	41.00	6.60000	345.20	3343.0	.4644590	.237442	2.69	5.00			65.200
3073.0	.4640090	.126442	2.81	21.0	400.0	9.30000	382.10	3344.0	.4642290	.137442	2.79	5.00	210.0	5.20000	177.30
3074.0	.4640090	.126442	2.32	21.0	1300.	11.0000	249.00	3345.0	.4642290	.138442	2.88	5.00	220.0	6.50000	223.30
3075.0	.4640090	.126442	2.81	21.0	2200.	14.0000	463.90	3346.0	.4642290	.138442	2.72	5.00	200.0	14.0000	164.20
3076.0	.4640090	.126442	2.50	21.0	2500.	12.0000	249.00	3347.0	.4642290	.138442	2.81	5.00	210.0	7.80000	197.70
3077.0	.4640090	.126442	2.62	21.0	2500.	11.0000	271.20	3348.0	.4642290	.138442	2.65	5.00	210.0	6.50000	197.00
3078.0	.4640090	.126442	2.55	21.0	44.00		783.50	3349.0	.4642290	.138442	2.66	5.00	200.0	5.80000	152.40
3079.0	.4640090	.126442	2.76	21.0	170.0	11.0000	357.50	3350.0	.4646790	.138442	2.78	5.00	223.0	5.60000	141.20
3080.0	.4640090	.126442	2.21	21.0	2700.	11.0000	351.30	3351.0	.4646790	.138442	2.90	5.00	223.0	4.70000	154.30
3081.0	.4640090	.126442	2.55	21.0	42.00		751.00	3352.0	.4646790	.138442	2.90	5.00	210.0	5.10000	130.00
3106.0	.4649090	.129532	2.49	5.00	24.00	7.60000	119.10	3353.0	.4646790	.138442	2.81	5.00	200.0	7.20000	163.50
3107.0	.4649090	.129532	2.69	5.00	24.00	15.0000	150.10	3354.0	.4646790	.138442	2.96	5.00	200.0	5.80000	105.10
3108.0	.4649090	.129532	2.46	5.00	21.00	11.0000	134.60	3355.0	.4646790	.138442	2.70	5.00	210.0	6.90000	130.70
3109.0	.4649090	.129532	3.18	5.00	23.00	12.0000	150.70	3373.0	.4649067	.140442	2.37	5.00	200.0	6.70000	162.90
3110.0	.4649090	.129532	3.20	5.00	200.0	11.0000	113.20	3374.0	.4649067	.140442	2.46	5.00	210.0	5.40000	161.60
3111.0	.4649090	.129532	2.49	5.00	200.0	9.00000	134.00	3375.0	.4649067	.140442	2.80	5.00	210.0	3.10000	130.00
3112.0	.4649090	.129532	3.05	5.00	180.0	9.30000	129.90	3376.0	.4649067	.140442	2.39	5.00	210.0	3.00000	106.50
3113.0	.4649090	.129532	2.79	5.00	180.0	9.50000	187.70	3377.0	.4649067	.140442	2.60	5.00	180.0	5.10000	179.00
3114.0	.4649090	.129532	3.15	5.00	110.0	10.0000	160.80	3379.0	.4649067	.140442	2.46	5.00	180.0	3.80000	112.30
3115.0	.4649090	.129532	2.85	5.00	700.0	8.20000	140.00	3380.0	.4649067	.140442	2.46	5.00	180.0	4.70000	111.60
3116.0	.4649090	.129532	2.86	5.00	1100.	7.40000	178.70	3381.0	.4649067	.140442	2.90	5.00	180.0	4.10000	95.900
3117.0	.4649090	.129532	2.57	5.00	1100.	7.40000	190.60	3382.0	.4649067	.140442	2.40	5.00	200.0	4.90000	115.60
3118.0	.4649090	.129532	2.49	5.00	1100.	7.80000	148.90	3383.0	.4649067	.140442	2.40	5.00	200.0	4.00000	107.70
3140.0	.4649090	.130532	3.13	5.00	800.0		86.500	3384.0	.4649067	.140442	2.90	5.00	190.0	4.90000	112.30
3141.0	.4649090	.130532	3.19	5.00	800.0	7.10000	127.70	3423.0	.4649090	.102442	1.59	5.00	120.0	11.0000	139.60
3142.0	.4649090	.130532	2.70	5.00	920.0	6.30000	77.500	3424.0	.4649090	.102442	1.90	5.00	120.0	4.70000	90.400
3143.0	.4649090	.130532	3.00	5.00	600.0	5.30000	51.600	3425.0	.4649090	.102442	1.54	5.00	140.0	8.90000	132.40
3144.0	.4649090	.130532	2.73	5.00	140.0	5.80000	79.800	3426.0	.4649090	.102442	1.75	5.00	140.0	7.30000	126.10
3145.0	.4649090	.130532	2.32	5.00	140.0	5.80000	104.10	3427.0	.4649090	.102442	1.85	5.00	150.0	11.140	
3146.0	.4649090	.130532	3.19	5.00	140.0	6.40000	129.10	3428.0	.4649090	.102442	1.66	5.00	140.0	9.10000	96.600
3147.0	.4649090	.130532	2.41	5.00	140.0	6.40000	68.400	3429.0	.4649090	.102442	1.64	5.00	160.0	9.60000	133.70
3148.0	.4649090	.130532	2.73	5.00	120.0	5.50000	130.00	3432.0	.4649090	.102442	2.08	5.00			111.40
3149.0	.4649090	.130532	2.46	5.00	900.0	11.0000	108.90	3433.0	.4649090	.104442	1.70	5.00	800.0	10.0000	101.90
3150.0	.4649090	.130532	2.86	5.00	13.00		119.90	3434.0	.4649090	.104442	1.47	5.00	940.0	13.0000	76.800
3151.0	.4649090	.130532	3.10	5.00	1300.	6.60000	107.20	3435.0	.4649090	.104442	1.44	5.00	900.0	6.70000	45.600
3173.0	.4649045	.131532	2.80	5.00	1000.	6.50000	114.70	3436.0	.4649090	.104442	1.87	5.00	870.0	8.80000	159.60
3174.0	.4649045	.131532	2.80	5.00	1100.	6.60000	102.60	3437.0	.4649090	.104442	1.63	5.00	990.0	11.0000	163.70
3175.0	.4649045	.131532	2.98	5.00	930.0	5.90000	91.200	3438.0	.4649090	.104442	1.48	5.00	120.0	6.70000	148.20
3176.0	.4649045	.131532	2.87	5.00	980.0	6.20000	132.30	3439.0	.4649090	.104442	1.70	5.00	150.0	4.20000	134.50
3177.0	.4649045	.131532	2.87	5.00	130.0	2.60000	96.700	3465.0	.4649090	.104442	1.46	5.00	120.0	6.20000	99.100
3178.0	.4649045	.131532	2.85	5.00	130.0	2.40000	87.100	3466.0	.4649090	.104442	1.68	5.00	120.0	14.0000	120.50
3179.0	.4649045	.131532	2.91	5.00	140.0	3.40000	102.60	3467.0	.4649090	.104442	1.60	5.00	120.0	9.60000	127.50
3180.0	.4649045	.131532	2.83	5.00	140.0	3.60000	84.400	3468.0	.4649090	.104442	1.48	5.00	140.0	13.0000	85.900
3181.0	.4649045	.131532	2.40	5.00	140.0	2.50000	72.000	3469.0	.4649090	.104442	1.59	5.00	93.00	10.0000	100.20
3182.0	.4649045	.131532	2.87	5.00	170.0	1.40000	70.700	3470.0	.4649090	.104442	1.27	5.00	180.0	4.80000	75.000
3183.0	.4649045	.131532	2.87	5.00	140.0	8.30000	70.700	3498.0	.4649090	.105442	1.81	5.00	200.0	7.70000	96.000
3184.0	.4649045	.131532	3.10	5.00	110.0	1.40000	63.800	3499.0	.4649090	.105442	1.50	5.00	200.0	4.2000	42.700
3185.0	.4649045	.131532	2.85	5.00	1100.	1.30000	119.50	3500.0	.4649090	.105442	1.45	5.00	1400.	11.0000	100.60
3208.0	.4640090	.133532	2.62	5.00	18.00	14.0000	204.50	3501.0	.4649090	.105442	1.63	5.00	1400.	6.50000	85.100
3209.0	.4640090	.133532	2.79	5.00	35.00	6.70000	190.90	3502.0	.4649090	.105442	1.63	5.00	1400.	6.00000	78.200
3210.0	.4640090	.133532	2.50	5.00	36.00	11.0000	190.90	3503.0	.4649090	.105442	1.58	5.00	1400.	12.0000	74.500
3211.0	.4640090	.133532	2.97	5.00	31.00		150.00	3504.0	.4649090	.105442	1.80	5.00	820.0	7.70000	111.90
3212.0	.4640090	.133532	2.50	5.00	270.0	12.0000	190.90	3505.0	.4649090	.105442	1.80	5.00	760.0	8.60000	104.90
3213.0	.4640090	.133532	2.58	5.00	260.0	7.50000	249.10	3506.0	.4649090	.105442	1.75	5.00	820.0	7.60000	93.300
3214.0	.4640090	.133532	3.02	5.00	270.0	14.0000	159.10	3507.0	.4649090	.105442	1.70	5.00	740.0	12.0000	113.50
3215.0	.4640090	.133532	2.63	5.00	280.0	9.10000	195.50	3508.0	.4649090	.105442	1.47	5.00	720.0	23.0000	98.300
3216.0	.4640090	.133532	2.78	5.00			159.00	3509.0	.4649090	.105442	1.50	5.00	570.0	73.800	
3217.0	.4640090	.133532	2.88	5.00	1800.	12.0000	140.90	3510.0	.4649045	.106442	1.63	5.00	1700.	620000	66.900
3218.0	.4640090	.133532	2.66	5.00	1										

ID	CODE 1	CODE 2	CHL	TEMP	RATE	MODULUS	STRENG
3596.0	.6649090	.118402	1.81	5.00	41.00	11.0000	167.40
3598.0	.6649090	.118402	1.86	5.00	17.00	16.0000	234.40
3599.0	.6649091	.118402	1.92	5.00	18.00	16.0000	252.80
3600.0	.6649093	.118402	1.91	5.00	19.00	16.0000	252.80
3611.0	.6649092	.118402	1.78	5.00	18.00	14.0000	237.90
3617.0	.6649090	.118402	1.81	5.00	21.00	14.0000	149.70
3618.0	.6649090	.118402	1.78	5.00	22.00	8.0000	111.60
3619.0	.6649090	.118402	1.88	5.00	14.00	11.0000	123.60
3620.0	.6649090	.118402	1.71	5.00	21.00	10.0000	164.20
3621.0	.6649090	.118402	1.50	5.00	22.00	10.0000	68.910
3622.0	.6649090	.118402	1.70	5.00	21.00	9.5000	147.10
3623.0	.6649090	.118402	2.17	5.00	22.00	5.1000	75.500
3624.0	.6649090	.118402	1.99	5.00	21.00	7.3000	216.80
3625.0	.6649090	.118402	1.81	5.00	24.00	8.0000	167.20
3626.0	.6649090	.118402	1.89	5.00	20.00	8.0000	121.60
3627.0	.6649090	.118402	2.25	5.00	21.00	11.0000	75.500
3628.0	.6649045	.111442	2.10	2.00	19.00	1.4000	63.000
3629.0	.6649045	.111442	2.36	2.00	17.00	1.6000	66.900
3630.0	.6649045	.111442	2.36	2.00	15.00	1.9000	58.800
3631.0	.6649045	.111442	1.98	2.00	18.00	1.1000	55.400
3632.0	.6649045	.111442	2.65	2.00	17.00	1.2000	52.800
3633.0	.6649045	.111442	1.93	2.00	17.00	1.4000	71.000
3634.0	.6649045	.111442	2.11	2.00	13.00	2.5000	80.300
3635.0	.6649045	.111442	2.32	2.00	12.00	2.8000	55.900
3636.0	.6649045	.111442	2.48	2.00	14.00	2.7000	90.800
3637.0	.6649045	.111442	1.99	2.00	11.00	4.1000	74.800
3638.0	.6649045	.111442	1.80	2.00	8.00	4.2000	74.800
3639.0	.6649045	.111442	2.31	2.00	9.10	5.2000	91.600
3640.0	.6649045	.111442	2.35	2.00	7.50	6.1000	86.100
3641.0	.6649045	.111442	2.30	2.00	8.00	4.7000	84.000
3642.0	.6649045	.111442	1.80	2.00	11.00	4.1000	77.700
3643.0	.6649045	.111442	2.34	2.00	12.00	3.1000	42.800
3644.0	.6649000	.112442	1.30	2.00	27.00	2.4000	98.500
3645.0	.6649000	.112442	1.16	2.00	28.00	5.3000	79.400
3646.0	.6649000	.112442	1.80	2.00	30.00		118.20
3647.0	.6649000	.112442	1.43	2.00	19.00	7.7000	78.800
3648.0	.6649000	.112442	1.39	2.00	24.00	6.5000	130.00
3649.0	.6649000	.112442	1.50	2.00	19.00	8.4000	82.100
3650.0	.6649000	.112442	1.80	2.00	21.00	7.6000	99.200
3651.0	.6649000	.112442	1.70	2.00	11.00	6.8000	131.30
3652.0	.6649000	.112442	1.56	2.00	12.00	6.5000	78.800
3653.0	.6649000	.112442	1.34	2.00	11.00	6.5000	134.60
3654.0	.6649000	.112442	1.17	2.00	31.00	1.7000	97.200
3655.0	.6649000	.112442	1.14	2.00	30.00	4.8800	104.90
3656.0	.6649000	.112442	1.14	2.00	34.00	8.8000	95.900
3657.0	.6649000	.112442	1.14	2.00	34.00	6.3000	97.800
3658.0	.6649000	.112442	1.25	2.00	27.00	8.8000	116.90
3659.0	.6649000	.112442	1.18	2.00	20.00	8.8000	78.100
3660.0	.6649000	.112442	1.14	2.00	19.00	5.9000	78.800
3661.0	.6649000	.112442	1.23	2.00	20.00	6.6000	78.800
3662.0	.6649000	.112442	1.16	2.00	19.00	6.2000	105.10
3663.0	.6649000	.112442	1.24	2.00	21.00	7.1000	79.400
3664.0	.6649000	.112442	1.16	2.00	82.00	12.0000	111.60
3665.0	.6649000	.112442	1.13	2.00	10.00	22.0000	90.600
3666.0	.6649000	.112442	1.04	2.00	12.00	12.0000	130.00
3667.0	.6649000	.112442	1.24	2.00	12.00	23.0000	158.30

Rate Constant and Rate Power

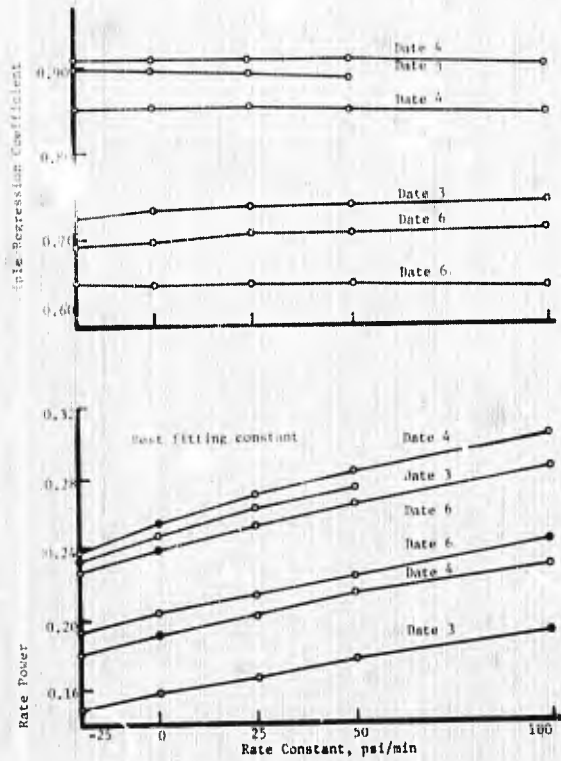


Exhibit 5.1

Rate Power at Various Depth and Temperatures, Center Ice

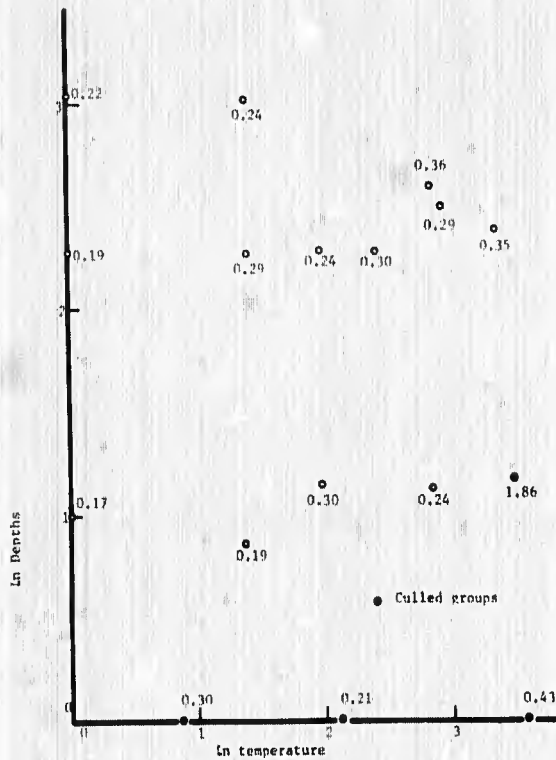


Exhibit 5.3

EXHIBIT 5.2

DATA GROUPS, COMPRESSION, ALL VALUES IN HUNDRETHS

ID	NOBS	RPOW	LN DEP	LN TEM	LN SAL	LN ROTVAR	X E
HORIZONTAL SPECIMENS							
CFAREV	9	10	111	161	249	40	
CFB	19	15	97	249	228	40	
CFC	15	16	139	302	231	40	
CFD	25	14	247	266	222	40	
CM79A	22	42	139	209	198		• EARLY DATE
CM99H	71	20	113	266	192	76	
CM99C	40	25	120	304	187	76	
CM99D	17	20	298		147	76	
CM99E	35	17	303	230	177	76	
CM99F	11	21	303	304	143	76	
CRP A	16	30	87		201	100	• -1 C
CRP B	75	17		100	193	100	
CRP C1	32	19		230	211	100	
CRP C2	42	22		304	180	100	
CRP D	89	19	138	86	171	100	
CRP E1	48	29	139	230	187	100	
CRP E2	62	24	139	304	163	100	
CRP F	11	21	211		179	100	• -1 C
CRP G	8	23	195	115	184	100	
CRP H	37	24	195	236	158	100	
CRP I	14	30	240	161	158	100	
CRP J	17	30	240	230	190	100	
CRP K	46	24	283	113	152	100	
CRP L RV	50	36	283	264	147	100	
CRP M	29	29	294	252	192	100	
CRP N	7	43	358		140	100	• SMALL GROUP
CRP O	11	86	350	115	140	100	• -1 C
CRP P	17	35	333	242	140	100	
CB90AREV	8	22	334		114	48	
CB90B	9	15	218	230	-88		
CB90C	12	24	327	230	113	48	
CB90DREV	44	16	378	69	159	48	
CB90E	102	19	379	184	143	48	
CB90F	27	19	378	304	151	48	
CB90GREV	28	22	414	27	72	48	
CB90HREV	23	20	397	165	154	48	
CB90I	21	20	428	230	102	48	
CB94AREV	45	44	378	69	143	123	
CB94BREV	59	39	379	161	144	123	
CB94C	34	42	378	230	158	123	
CB94D	24	43	378	334	153	123	
CB94E	13	20	401	64	148		• -1.2 C
CB94FREV	19	45	397	161	155	123	
CB94GREV	25	33	428	18	-97	123	
CB94H	15	39	428	216	-99	123	
CB99AREV	52	25	378	69	141	73	
CB99BREV	42	25	378	161	155	73	
CB99C	37	28	378	230	155	73	
CB99D	29	26	378	304	151	73	
CB99EREV	27	22	397	134	161	73	
CB99F	26	22	428	16	126	73	
CB99G	19	28	428	230	100	73	
VERTICAL ICE							
CM00A	16	21	208	275	218	2	
CM00B	16	19	188	181	136	2	
CB09A	49	18	378	69	155	1	
CB09B1	24	17	369	161	115	1	
CB09B2	60	17	378	161	136	1	
CB09C	32	20	378	230	164	1	
CB09D	22	12	378	304	155	1	
CB09E1	8	18	397	69	167	1	
CB09E2	22	28	397	161	160	1	• VERY EARLY
CB09F	10	9	387	255	143	1	
CB09GREV	29	18	428	69	-131	1	
CB09H	18	14	428	230	-32	1	
• CULLED DATA GROUPS							

EXHIBIT 5.4
EVALUATION OF STRATE TWO, COMPRESSION

ID	NOB	RPOW	AV	SD	CV	AV	SD	CV
			***STRATE 2**			---STRATE 1---		
			x100	x10E4	x10E4	x100	x10E4	x10E4
HORIZONTAL SPECIMENS								
FINE ICE								
CFAREV	9	10	470	1504	319	483	1593	330
CFE	19	15	535	2252	421	522	2770	520
CFE	15	16	558	2014	161	549	1034	188
CFD	25	14	562	1058	195	553	1008	182
MEDIUM ICE								
CM99A	22	42	488	3948	808	304	3324	1092 1
CM99B	71	20	501	3876	773	497	3592	723 2
CM99C	40	25	540	2088	386	510	1887	369
CM99D	17	20	445	3686	846	432	3562	830 3
CM99E	25	17	463	2437	526	507	1905	375
CM99F	11	21	494	1766	357	524	1144	218
CENTER ICE								
CRP A	16	30	671	7570	2354	270	7189	2666 4
CRP B	75	17	664	3141	708	448	3399	758 5
CRP C1	32	19	487	2727	560	493	2731	554
CRP C2	42	22	518	1185	228	513	1192	232
CRP D	89	19	408	2671	654	422	2878	682
CRP E1	48	29	412	2412	559	401	2290	570
CRP F2	62	24	468	1621	346	480	1596	332
CRP F	11	21	366	2652	724	370	2706	732 6
CRP G	8	23	383	1674	447	386	2064	535
CRP H	37	24	441	3148	763	454	3409	750
CRP I	14	30	364	2649	728	338	2583	765 7
CRP J	17	30	450	1225	272	436	1161	266
CRP K	46	24	386	2802	726	401	2917	727 8
CRPL1	27	40	390	3571	916	320	3004	921 9
CRPL2	23	29	427	2773	649	442	2740	619
CRP M	29	29	407	1567	385	415	1848	445
CRP N	7	43	375	3466	923	310	2998	965 10
CRP O	11	86	386	1193	308			11
CRP P	17	35	410	1824	445	394	1914	486
BOTTOM ICE								
CB90AREV	8	22	539	1348	250	497	613	123
CB90B	9	15	510	3134	608	516	2863	555
CB90C	12	24	540	2283	422	509	2073	407
CB90DREV	44	16	545	1812	332	554	1796	324
CB90E	102	19	560	3077	549	562	3279	582
CB90F	27	19	587	1851	315	604	1832	303
CB90GREV	28	22	510	3266	640	485	3083	635
CB90HREV	23	20	544	2600	477	541	2517	485
CB90I	21	20	507	3147	620	516	3236	627
CB94AREV	45	44	269	2594	964	218	2270	1041 12
CB94BREV	59	39	291	4089	1405	294	4093	1391 13
CB94C	34	42	291	1515	520	291	1515	520
CB94D	24	43	318	1772	557	331	1726	521
CB94E	13	20	256	1984	773	357	1838	514 14
CB94FREV	19	46	258	1866	723	222	1651	745
CB94GREV	25	33	309	2218	718	335	2385	711 15
CB94H	15	39	286	1754	613	319	1366	429
CB99AREV	52	25	461	2255	489	444	2175	490
CB99BREV	42	25	488	1941	398	482	1935	401
CB99C	37	28	509	1540	302	494	1486	301
CB99D	29	26	539	1071	198	549	1022	186
CB99EREV	27	22	496	2221	447	512	2683	524
CB99F	26	22	466	3203	687	471	3249	690
CB99G	19	28	487	2421	496	485	2411	497
VERTICAL SPECIMENS								
MEDIUM ICE								
CM00A	16	21	539	3385	628	508	3233	636
CM00B	16	19	519	4848	934	505	4442	879
BOTTOM ICE								
CR09A	49	18	570	2184	383	574	2183	380
CR09B1	24	17	610	1845	302	610	1845	302
CR09B2	60	17	596	2685	450	596	2685	450
CR09C	32	20	640	1649	257	612	1444	235
CR09D	22	12	679	2288	336	698	2283	327
CR09E1	8	18	513	836	162	518	835	161
CR09E2	22	28	569	2111	371	493	1170	237
CR09F	10	9	600	2872	479	633	2772	437
CR09GREV	29	18	501	3096	617	505	3102	614
CR09H	18	14	535	4942	923	546	4939	904

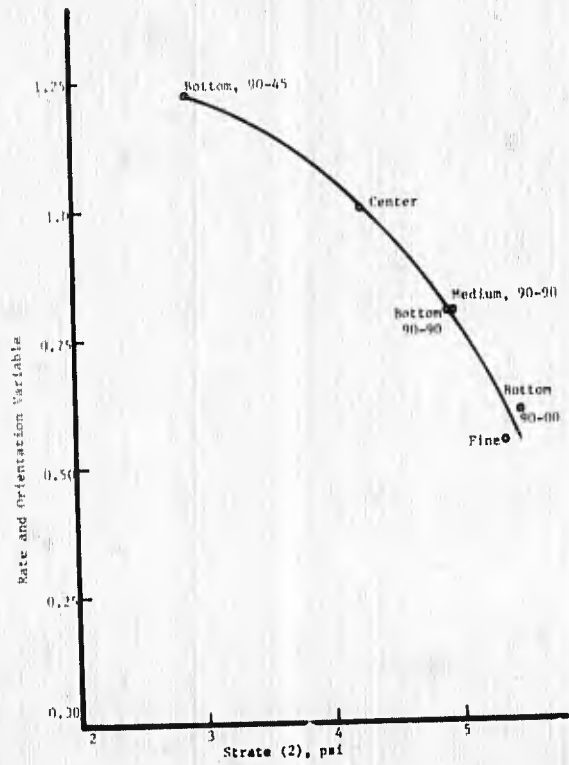


Exhibit 5.5

Strength and Strate at Various Orientations
Bottom Ice, Compression

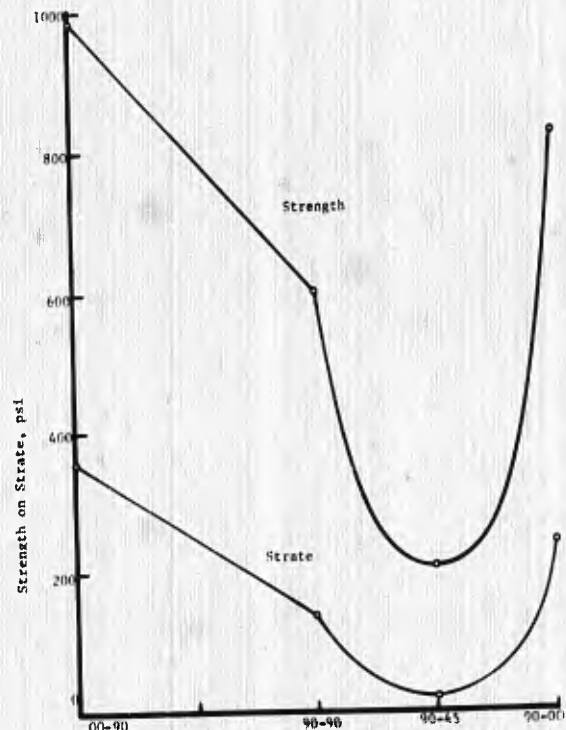


Exhibit 5.6

EXHIBIT 5.7

STATISTICAL ANALYSIS OF LN(STRENGTH) AND STRATE

ID	NOBS	AV LN	AV	STDEV	ESTDEV	COFVAR
HORIZONTAL ICE						
FINE 90-11 ICE						
STRENGTH	71	6.0199	411	.6882	1.99	.1143
STRATE	68	5.3409	2.9	.3042	1.35	.0569
DIFF		.6790	1.97	.3840	1.47	
MEDIUM 90-90 ICE						
STRENGTH	203	6.2036	493	.5089	1.66	.0820
STRATE	196	4.9489	141	.4424	1.56	.0893
DIFF		1.2547	3.50	.0665	1.07	
CENTER 90-11 ICE						
STRENGTH	606	5.7464	313	.7085	2.03	.1232
STRATE	611	4.7828	72	.5053	1.66	.1179
DIFF		1.4636	4.31	.2032	1.22	
BOTTOM 90-00 ICE						
STRENGTH	246	6.7174	822	.5505	1.73	.0620
STRATE	274	5.4666	237	.3547	1.42	.0648
DIFF		1.2468	3.48	.1958	1.21	
BOTTOM 90-45 ICE						
STRENGTH	269	5.3421	210	.7776	2.17	.1445
STRATE	234	2.8658	17	.3260	1.39	.1137
DIFF		2.4763	11.9	.4516	1.57	
BOTTOM 90-90 ICE						
STRENGTH	308	6.3947	600	.6085	1.84	.0951
STRATE	232	4.8984	134	.3255	1.38	.0664
DIFF		1.4963	4.46	.2830	1.32	
ALL HORIZONTAL ICE						
STRENGTH	1703	6.0054	405	.7949	2.21	.1325
STRATE	1615	4.4992	90	.8857	2.42	.1969
DIFF		1.5062	4.52	-.0908	.91	
VERTICAL ICE						
MEDIUM 00-00 ICE						
STRENGTH	33	6.2349	510	.4271	1.53	.0685
STRATE	32	5.0518	156	.4365	1.54	.0864
DIFF		1.1831	3.26	-.0094	.99	
BOTTOM 00-90 ICE						
STRENGTH	306	6.8956	985	.6483	1.91	.0940
STRATE	274	5.8688	354	.5234	1.69	.0891
DIFF		1.0268	2.79	.1249	1.13	
ALL VERTICAL ICE						
STRENGTH	339	6.8313	927	.6601	1.93	.0966
STRATE	307	5.7646	117	.6586	1.93	.1142
DIFF		1.0667	2.90	.0015	1.00	
ALL ICE						
STRENGTH	2042	6.1425	465	.8274	2.28	.1347
STRATE	1922	4.6954	109	.9861	2.68	.2100
DIFF		1.4471	4.25	-.1587	.85	

EXHIBIT 5.8

TENSION RATE POWER

ID	NOBS	STR	DEP	T	RATE	STDEVR	RPOW	T
RNTF1	11	3.945	1.212	1.089	3.715	.962	-.117	.70
RNTF2	15	4.585	2.079	1.352	5.439	.681	-.035	.15
RNTM1	9	4.343	.693	1.792	5.147	1.040	.162	1.43
RNTM2	12	4.612	2.904	2.343	6.016	1.114	.178	3.35
RNTC1	21	3.686	1.493	.964	2.763	1.188	.042	.95
RNTC2A	9	3.873	1.419	2.539	3.043	1.322	.124	1.44
RNTC3A	13	4.434	0.000	.693	4.916	1.803	.107	2.85
RNTC4	22	4.414	1.405	.693	4.499	2.011	.026	2.24
RNTC5A	12	4.198	2.833	.693	4.272	1.946	.033	1.53
RNTC6A	14	4.582	.792	1.609	4.667	1.951	.030	3.04
RNTC7	9	4.347	2.833	1.609	4.242	2.002	.033	2.64
RNTC8	16	4.732	.780	2.303	4.938	1.903	.069	6.39
RNTC9	10	4.469	2.833	2.303	4.603	1.940	.066	1.92
RNTC10	7	4.734	1.386	2.939	4.853	1.642	.102	2.76
RNTC11	23	4.720	.000	3.042	5.268	1.564	.045	2.89
RNTC12	12	4.667	1.386	3.045	4.869	1.670	.063	3.88
RNTC13A	9	4.567	2.833	3.045	4.690	1.751	.036	2.12
RNT091A	16	5.476	3.784	.693	5.442	1.839	.043	2.75
RNT092	17	5.596	3.784	1.609	5.494	1.691	.028	1.05
RNT093A	13	5.272	3.956	1.327	4.965	1.258	.034	1.24
RNT094	10	5.453	3.689	1.609	5.568	1.792	.032	1.80
RNT095	11	5.403	3.784	1.609	5.473	1.729	.038	1.20
RNT096	12	5.711	3.784	2.303	5.315	1.749	-.023	.59
RNT097A	12	5.873	3.784	3.045	5.278	1.555	.038	1.83
RNT901	23	4.304	2.986	1.821	3.543	.968	.166	3.43
RNT902	21	4.575	3.784	.693	4.844	1.677	-.021	1.03
RNT903	12	4.640	3.784	.693	5.210	1.512	.057	1.40
RNT904	22	4.858	3.784	1.609	4.947	1.699	.032	2.22
RNT905A	15	4.552	3.970	1.365	4.613	1.532	-.064	1.92
RNT906	18	4.509	3.784	1.609	4.731	1.603	.063	1.66
RNT907	11	4.953	3.784	2.303	4.986	1.815	.029	.79
RNT908	13	4.975	3.784	3.045	4.802	1.853	.020	.79
RNT941	11	4.244	3.365	1.263	3.736	1.304	.136	5.80
RNT942	15	4.613	3.784	.693	5.668	1.583	.138	3.70
RNT943	13	4.250	3.784	.693	5.107	1.591	.090	2.11
RNT944	12	4.673	3.784	1.609	5.132	1.776	.134	5.72
RNT945	15	4.344	4.970	1.365	5.291	1.614	.107	3.94
RNT946	12	4.466	3.784	1.609	4.940	1.534	.090	3.29
RNT947	11	4.822	3.784	2.303	5.243	1.606	.118	5.20
RNT948	14	4.778	3.784	3.045	5.349	1.913	.079	3.42
RNT991	26	4.547	2.639	2.175	3.872	1.102	.096	2.31
RNT992A	18	4.940	3.784	.693	4.836	1.838	.017	.84
RNT993A	9	4.640	3.784	.693	5.019	1.640	.075	1.47
RNT994	23	5.092	3.784	1.609	5.234	1.500	.064	3.23
RNT995	18	4.962	3.970	1.355	5.198	1.373	.044	1.77
RNT996A	12	4.824	3.784	1.609	4.622	1.628	.037	1.15
RNT997	21	5.240	3.784	2.303	5.387	1.691	.071	2.47
RNT998	18	5.145	3.784	3.045	5.330	1.935	.019	.50

EXHIBIT 5.9

STRATE AND STRENGTH, INDIVIDUAL DATA GROUPINGS

STRATE	STRENGTH								
RNTM1	009								
181.88	726.50	SUM							
3925.99	62197.25	CROSS PRODUCT							
20.2389	81.7277	AVERAGE							
5.5941	22.5073	STANDARD DEVIATION							
.2768	.2788	COEFF OF VARIATION							
RNTM2	012	RNTC10	007	RNT907	011	RNT901	026	RNT903A	013
552.78	1255.20	643.54	804.90	1774.77	1574.30	1941.74	2547.20	2060.91	2493.20
26862.22	140106.26	59866.20	94575.63	150516.56	238007.09	154956.45	247283.88	332317.88	485832.34
46.0654	124.5833	91.9351	114.9857	115.8883	143.1181	74.6845	97.9615	158.5318	191.7846
11.1922	28.6898	10.8124	18.3649	16.8595	21.6751	19.9340	26.6652	21.5972	25.2899
.2628	.2743	.1176	.1597	.1440	.1514	.2669	.2722	.1362	.1318
RNTC1	021	RNTC11	023	RNT908	013	RNT92A	018	RNT904	010
770.76	892.90	1819.05	2602.20	1566.23	1901.10	1958.71	2543.80	1935.59	2144.80
31742.60	42266.89	146026.78	299623.18	192048.56	283827.83	218741.54	367061.68	177605.29	556547.20
36.7332	42.9195	79.1286	113.1391	120.4793	146.2384	108.8173	141.4222	193.5590	234.4890
11.1394	14.6315	9.5724	15.3926	16.7086	22.0111	18.1489	21.0567	18.1171	22.9455
.3579	.3441	.1209	.1360	.1386	.1545	.1667	.1492	.0936	.0978
RNT92A	009	RNTC12	012	RNT941	011	RNT903A	009	RNT905	011
399.67	458.40	103.12	1287.80	488.98	789.20	720.80	952.10	2037.66	2471.30
19705.60	26012.48	89043.97	140575.14	22151.60	59628.58	59596.03	105025.19	187106.82	568033.59
44.4106	50.9333	85.8436	107.3166	44.2709	71.7454	80.0893	105.7888	185.2419	224.6636
15.5679	18.2544	7.4738	14.6868	7.6977	17.34.8	15.2775	21.1937	11.0590	35.8083
.3503	.3583	.0870	.1368	.1738	.2417	.1907	.2192	.1676	.1593
RNTC3A	013	RNTC13A	009	RNT947	015	RNT994	023	RNT906	012
760.00	1175.40	761.75	875.30	799.58	1560.40	2890.20	3802.70	3111.63	3705.10
46121.74	106619.56	65609.22	87003.47	43871.20	172123.6	370273.75	648747.97	844174.33	1186057.0E 07
58.4616	87.3538	84.6395	97.2555	53.3055	104.0266	125.6612	165.3347	259.3025	306.7583
11.8701	24.8671	11.9083	15.3120	9.6455	26.4573	17.9599	30.1732	58.2477	61.8430
.2030	.2846	.1406	.1574	.1771	.2543	.1429	.1824	.2246	.2002
RNTC4	022	RNT901	023	RNT941	013	RNT995	018	RNT97A	012
1450.19	1829.60	1483.70	1808.10	514.56	933.30	2008.44	2601.30	3630.88	4297.90
96797.12	154141.22	105623.20	156880.63	20971.23	69882.29	228568.57	384958.29	1111875.6	1563363.2
65.9178	83.1634	64.5089	78.6130	39.5815	71.7923	111.5805	144.5166	302.5739	358.1583
7.5705	9.7224	21.2248	25.8847	7.0953	15.6879	16.2058	23.0435	34.7243	46.7434
.1146	.1169	.3290	.3292	.1792	.2157	.1452	.1594	.1147	.1355
RNTC5A	012	RNT902	021	RNT944	012	RNT996A	012	RNT91A	016
688.33	809.30	1650.39	2061.80	741.94	1327.90	1194.70	1516.10	21.1713	32.3632
40215.76	55850.93	133933.58	207211.54	46679.13	156775.05	121964.87	196885.05	.1084	.1343
57.3613	67.4416	78.5920	98.1849	61.8288	110.6583	99.5588	126.3418		
8.1567	10.7486	14.5420	15.4629	8.5570	29.8965	16.5729	22.0298		
.1421	.1593	.1850	.1574	.1383	.2701	.1664	.1743		
RNTC6A	014	RNT903	012	RNT945	015	RNT997	021	RNT902	017
1050.84	1386.10	987.95	1265.80	707.62	1247.00	3130.60	4104.60	40.7390	50.8492
80938.32	141344.97	83724.43	118950.90	36419.24	116449.76	493561.74	856664.96	.1811	.1859
75.0605	99.0071	82.3278	105.4833	47.1749	83.1333	149.0766	195.4571		
12.5915	17.7832	14.7277	22.2151	14.7288	30.2184	36.6478	52.1495		
.1677	.1796	.1788	.2106	.3122	.3634	.2458	.2668		
RNTC7	009	RNT904	022	RNT946	012	RNT998	017	RNT904	010
608.39	699.30	2290.13	2850.70	615.44	1060.00	2323.79	2985.30	18.1171	22.9455
41325.88	54955.19	240811.14	373825.47	31985.20	96098.32	338111.21	557131.23	.0936	.0978
67.5991	77.7000	104.0968	129.5772	51.2872	88.3333	136.6940	175.6058		
4.9881	8.8004	10.7255	14.5398	6.1837	14.9696	35.7612	45.3424		
.0737	.1132	.1030	.1122	.1205	.1694	.2616	.2582		
RNTC8	016	RNT905A	015	RNT947	011	RNT91A	016	RNT905	011
1175.15	1832.00	1207.96	1457.20	796.20	1392.10	3124.24	3853.70	31.0590	35.8083
119063.00	212236.02	103616.48	148429.32	58199.11	182092.59	616778.40	943898.41	.1676	.1593
85.9469	114.5000	80.5312	97.1466	72.3826	126.5545	195.2650	240.8562		
7.6281	15.2140	21.2759	22.1475	7.5329	24.3228	21.1713	32.3632		
.0887	.1328	.2641	.2279	.1040	.1921	.1084	.1343		
RNTC9	010	RNT906	018	RNT948	014	RNT92	017	RNT906	012
765.84	892.20	1357.96	1679.40	990.71	1697.70	3823.61	4648.50	58.2477	61.8430
60790.55	83528.10	106414.26	163604.88	71511.13	213962.73	886558.75	13124616	.2246	.2002
76.5847	89.2200	75.4426	93.3000	70.7650	121.2642	224.9188	273.4411		
15.4165	20.8859	15.2729	20.1711	10.3901	24.9497	40.7390	50.8492		
.2013	.2340	.2024	.2161	.1468	.2057	.1811	.1859		

EXHIBIT 5.1

STRATE AND STRENGTH, SINGTO AND LARGER GROUPINGS

STRENGTH	STRATE	STRENGTH/STRATE		STRENGTH	STRATE	STRENGTH/STRATE
LL TENSION				ALL BOTTOM 90-00		
671			NO. OF DATA	135		
86960.50	66225.06	1.31	SUMS	14598.40	11819.09	1.23
144704.17	8918692.30	1.62	CROSS PRODUCTS	1702739.70	1116688.20	1.52
129.598	98.696	1.313	AVERAGES	108.136	87.548	1.235
69.1146	59.6324	1.1590	STD. DEVIATION	30.4350	24.7285	1.2307
.5332	.6042	.8826	COEFF. OF VARIATION	.2814	.2824	.9964
ALL HORIZONTAL TENSION				LATE BOTTOM 90-00		
580				112		
63146.00	46500.54	1.35		12790.30	10335.39	1.23
7856226.80	4362275.20	1.80		1545859.00	1011065.00	1.52
108.872	80.173	1.357		114.199	92.200	1.237
41.1696	31.0951	1.2479		27.7079	22.7228	1.2193
.3781	.4127	.9160		.2426	.2462	.9853
ALL LATE HORIZONTAL				ALL BOTTOM 90-45		
481				103		
55923.90	41235.54	1.35		10007.60	5653.03	1.77
7241477.10	4024169.60	1.79		1067012.40	331787.84	3.21
116.265	85.728	1.356		97.161	54.883	1.770
39.2490	31.9209	1.2295		30.4641	14.5279	2.0969
.3375	.3723	.9066		.3135	.2647	1.1845
MEDIUM				LATE BOTTOM 90-45		
21				92		
1981.50	734.66	2.69		9210.40	5166.05	1.78
203003.51	30768.21	6.59		1007383.80	309636.24	3.25
94.357	34.983	2.697		100.200	56.152	1.784
28.3150	15.9169	1.7789		30.3278	14.6566	2.0692
.3000	.4549	.6595		.3026	.2610	1.1596
ALL CENTER				ALL BOTTOM 90-90		
177				144		
15305.60	12124.73	1.27		21052.90	16169.03	1.30
1499712.80	897246.74	1.67		3383758.30	1985784.10	1.70
87.602	68.501	1.278		146.200	112.284	1.302
28.3431	19.4654	1.4560		46.2442	34.5040	1.3402
.3235	.2841	1.1385		.3163	.3072	1.0293
ALL LATE CENTER				LATE BOTTOM 90-90		
147				118		
14154.30	10954.10	1.29		18505.90	14227.24	1.30
1431453.40	845778.54	1.69		3116474.40	1830827.70	1.70
96.287	74.517	1.292		156.829	120.569	1.300
21.6712	14.2204	1.5239		42.7875	31.4128	1.3621
.2250	.1908	1.1793		.2728	.2605	1.0471
BOTTOM 00-90						
91						
23814.50	19724.52	1.20				
6614190.00	4556417.10	1.45				
261.697	216.752	1.207				
65.1483	55.8836	1.1657				
.2489	.2578	.9655				

EXHIBIT 4.1

COMPRESSION DATA WITH SALT PROPERTIES, CENTER ICE

ID	A	B	CHL	T	STRATE	SV	IV	E	STR	RATE	ES	
11980	2639011	50611	485	10	141610	4171	0	5829	80	60	9	4
12130	2639011	50711	485	10	145119	4171	0	5829	700	700	40	38
12140	2639011	50711	485	10	145560	4171	0	5829	400	620	125	28
12150	2639011	50711	485	10	232662	4171	0	5829	620	420	150	15
12160	2639011	50711	485	10	225576	4171	0	5829	600	230	230	9
12600	2639011	40911	285	10	426364	2451	3	7549	9300	2450	2100	71
11950	2639011	50511	485	20	426960	2104	3	7806	7100	2170	630	71
11970	2639011	50611	485	20	420967	2104	0	7496	19000	2070	680	67
15730	3639011	12511	360	20	428444	1562	0	8438	2500	1410	47	72
15740	3639011	13611	365	20	161099	1584	0	8416	1400	900	174	47
15750	3639011	13611	365	20	420458	1584	0	8764	6100	2760	3700	67
15780	3639011	10111	367	20	451737	1592	0	8408	2900	1690	35	91
15790	3639011	10111	395	20	642149	1714	0	8286	2700	1520	33	83
15800	3639011	10111	400	20	435871	1736	0	8264	2100	1470	32	78
15810	3639011	10111	405	20	435444	1757	0	8247	6500	1610	68	77
15820	3639011	10111	400	20	419043	1736	0	8264	8800	1420	85	66
15830	3639011	10111	398	20	430616	1727	0	8271	4200	1610	90	74
15840	3639011	10111	412	20	421826	1788	0	8212	1400	1720	220	67
15850	3639011	10111	366	20	437541	1588	0	8412	3800	2140	314	79
15860	3639011	10111	363	20	437104	1575	0	8425	5500	2160	340	79
15870	3639011	40111	420	20	438447	1822	0	8178	3300	2680	1100	80
15880	3639011	40111	395	20	431262	1714	0	8286	8600	2600	1400	74
15890	3639011	40111	395	20	445102	1714	0	8286	3800	2910	1200	85
15900	3639011	30111	430	20	427151	1866	0	8134	2400	2520	2100	67
15910	3639011	30111	407	20	486766	1766	0	8234	8600	1900	3000	47
15920	3639011	10111	426	20	404747	1840	0	8152	12000	2370	3800	57
15940	3639011	10311	370	20	433844	1605	0	8395	2100	1420	36	76
15950	3639011	10211	455	20	421037	1757	0	8243	6400	1310	45	67
15960	3639011	10211	400	20	424234	1736	0	8264	1800	1520	74	72
15970	3639011	50311	440	20	459812	1475	0	8525	3400	1590	280	60
15980	3639011	10311	376	20	416782	1631	0	8369	4700	2060	840	64
15990	3639011	30311	475	20	413404	2078	0	7922	400	710	700	22
16000	3639011	30411	400	20	404746	1736	0	8264	5500	1170	2600	30
16010	3639011	30311	365	20	437145	1584	0	8416	1800	1800	1200	53
16020	3639011	30311	417	20	413184	1792	0	8208	1500	2170	1400	62
16030	3639011	30311	420	20	393701	1822	0	8178	5900	1800	1500	51
22440	3639011	10711	352	20	458625	1527	0	8473	15000	2030	68	98
22450	3639011	10711	358	20	447832	1553	0	8447	6200	1740	52	88
22460	3639011	10711	358	20	458370	1553	0	8447	3500	1900	47	97
22470	3639011	10711	351	20	455877	1523	0	8477	2200	1770	36	95
22480	3639011	10711	388	20	434018	1683	0	8317	4600	2540	97	115
22490	3639011	10711	370	20	446947	1605	0	8395	6000	2070	150	87
22500	3639011	10711	352	20	444823	1527	0	8473	6200	2170	180	88
22510	3639011	10711	348	20	437849	1510	0	8490	7100	1890	150	79
22520	3639011	10711	352	20	482926	1527	0	8473	3200	3380	320	123
22530	3639011	10711	367	20	456771	1592	0	8408	8800	2770	460	96
22540	3639011	10711	360	20	446806	1562	0	8438	8000	2570	470	69
22550	3639011	10711	364	20	458182	1579	0	8421	11000	3410	1400	97
22560	3639011	10711	350	20	469508	1519	0	8481	16000	3900	1600	109
22570	3639011	10711	330	20	461496	1432	0	8568	7800	3560	1500	100
22580	3639011	10711	358	20	468076	1553	0	8447	7800	4540	4200	107
22590	3639011	10711	376	20	447761	1631	0	8369	15000	3690	4100	88
22600	3639011	10711	376	20	464260	1631	0	8369	13000	4170	3200	103
22610	3639011	10711	365	20	462231	1584	0	8416	15000	4170	3600	101
22620	3639011	10711	349	20	460289	1514	0	8485	8000	3940	2900	99
22630	3639011	10711	350	20	460378	1519	0	8481	15000	3920	2800	99
12760	2639011	102611	526	50	471380	978	0	9022	5500	2300	48	111
12770	2639011	102611	526	50	457656	978	0	9022	5700	2380	120	97
12780	2639011	402611	526	50	461723	978	0	9022	800	3410	660	101
12790	2639011	402611	526	50	439696	978	0	9022	11000	3510	2500	81
12800	2639011	302611	526	50	494490	978	0	9022	19000	7060	5600	140
21760	3639011	104011	391	50	460136	727	0	9273	5100	2340	96	99
21770	3639011	104011	345	50	456654	641	0	9359	1400	2100	18	106
21780	3639011	104011	329	50	457848	611	0	9389	3400	2120	64	97
21790	3639011	104011	350	50	467385	651	0	9349	2400	2210	48	107
21800	3639011	104011	360	50	448805	669	0	9331	3900	2440	220	88
21810	3639011	104011	361	50	458704	671	0	9329	7200	2600	182	98
21820	3639011	104011	330	50	462063	613	0	9387	4700	2560	140	101
21830	3639011	104011	341	50	450311	634	0	9366	10000	2410	190	90
21840	3639011	104011	348	50	484220	647	0	9353	5800	3870	390	126
21850	3639011	104011	365	50	469039	678	0	9322	8000	3470	490	108
21860	3639011	704011	365	50	465735	678	0	9322	10000	3890	1100	104
21870	3639011	704011	365	50	465944	678	0	9322	20000	3940	1140	105
21880	3639011	704011	346	50	470248	643	0	9357	8600	4330	1500	110
21890	3639011	204011	338	50	475565	626	0	9372	20000	5900	5900	116
21900	3639011	204011	350	50	473617	651	0	9349	36000	5730	5600	113
21910	3639011	204011	340	50	457482	632	0	9368	3500	4700	4600	97
21920	3639011	504011	343	50	469518	637	0	9363	18000	5200	4150	109
21930	3639011	704011	378	50	470518	703	0	9297	13000	5060	3400	110
21940	3639011	104011	381	50	467113	708	0	9292	8600	3350	450	106
21950	3639011	704011	365	50	478056	678	0	9322	12000	5330	3600	119
13250	2639011	101011	494	100	501212	492	99	9408	11000	3460	66	150
13260	2639011	101011	494	100	504537	492	99	9408	2500	3960	110	155
13270	2639011	101011	474	100	485276	492	99	9408	2000	3920	275	128
13280	2639011	501011	494	100	501464	492	99	9408	11000	6700	1800	150
13290	2639011	501011	494	100	513127	492	99	9408	14500	7800	2150	159
13300	2639011	501011	444	100	504993	492	99	9408	16000	8540	5100	156
13560	2639011	806111	370	100	515659	368	74	9557	17500	9520	5150	171
20900	3639011	101011	386	100	502091	384	77	9538	3700	3590	76	151
20910	3639011	101011	375	100	493852	373	75	9551	43000	3340	80	139
20920	3639011	101011	419	100	497015	417	84	9498	3200	3430	78	144

20930	3639011	101011	386	100	509666	384	77	9538	2100	4090	100	163
20940	3639011	101011	404	100	485027	402	81	9516	7800	3670	200	127
20950	3639011	101011	407	100	495292	405	81	9513	8700	3890	160	141
20960	3639011	201011	385	100	498374	383	77	9539	13200	5130	550	146
20970	3639011	201011	406	100	498805	404	81	9514	10200	5310	640	146
20980	3639011	201011	388	100	508552	386	78	9535	11000	5740	580	161
20990	3639011	201011	353	100	510212	351	74	9529	16900	7430	1950	164
21000	3639011	201011	383	100	509109	381	77	9541	12900	6870	1700	156
21010	3639011	201011	384	100	499664	382	77	9540	24800	6720	2000	147
21020	3639011	201011	413	100	501397	411	83	9504	16500	7910	3900	150
21160	3639011	501011	385	100	499575	383	77	9539	31400	8300	5800	147
21170	3639011	201011	400	100	496657	398	80	9521	23500	8320	6800	143
21190	3639011	201011	390	100	505059	388	78	9534	17000	8020	3700	156
21200	3639011	201011	385	100	497464	383	77	9539	12100	7150	3050	144
12250	2639011	808011	531	210	488337	515	347	9337	10000	8230	5400	132
12260	2639011	309011	531	210	452706	515	347	9337	18000	7000	2050	138
12270	2639011	509011	531	210	498435	515	347	9337	45000	3270	44	146
14600	2639011	936011	494	210	517738	293	323	9383	14000	4540	83	177
14610	2639011	536011	494	210	532308	293	323	9383	18000	9110	1100	205
14620	2639011	136011	494	210	528221	293	323	9383	27000	8740	1100	196
14630	2639011	836011	494	210	529168	293	323	9383	27000	12570	5900	198
14660	2639011	336011	494	210	526678	293	323	9383	22900	10500	2800	193
14710	2639011	304011	480	210	524964	226	248	9525	10000	8290	1000	190
14720	2639011	304011	480	210	528752	226	248	9525	21000	8610	1000	197
14730	2639011	104011	480	210	524062	226	248	9525	17300	4900	85	190
14740	2639011	804011	480	210	529632	226	248	9525	19000	10710	2700	199
14750	2639011	804011	480	210	519665	226	248	9525	24000	11300	5500	180
14760	2639011	104011	480	210	521704	226	248	9525	22000	5180	128	184
14770	2639011	104011	480	210	525457	226	248	9525	14000	5910	200	191
14780	2639011	104011	480	210	525532	226	248	9525	13800	5400	410	191
22780	3639011	109011	456	210	519340	211	233	9555	20800	4800	100	180
22790	3639011	109011	456	210	520090	211	233	9555	10800	4740	91	181
22800	3639011	109011	472	210	527702	161	178	9660	16000	4930	78	195
22810	3639011	109011	472	210	520782	161	178	9660	4600	4410	63	182
22820	3639011	109011	472	210	521255	161	178	9660	14000	5730	210	183
22830	3639011	109011	472	210	503326	161	178	9660	12000	4740	205	153
22840	3639011	109011	472	210	523734	161	178	9660	3070	5750	190	188
22860	3639011	109011	472	210	524120	161	178	9660	26000	7500	650	188
22870	3639011	109011	472	210	504065	161	178	9660	22400	5990	580	154
22880	3639011	109011	472	210	504872	161	178	9660	14500	6360	740	155
22890	3639011	209011	472	210	523832	161	178	9660	22000	9500	2000	188
22900	3639011	209011	472	210	508228	161	178	9660	6000	7590	1410	162
22910	3639011	209011	472	210	520220	161	178	9660	11000	9230	2060	181
22930	3639011	609011	472	210	522785	161	178	9660	20800	11920	6100	186
22940	3639011	609011	472	210	504499	161	178	9660	20000	10030	6400	155
22950	3639011	209011	472	210	502583	161	178	9660	38000	8600	3400	152
22960	3639011	209011	472	210	517602	161	178	9660	16000	10400	4100	176
22970	3639011	209011	472	210	513979	161	178	9660	6000	10030	4100	170
23120	3639011	814011	310	210	523806	184	203	9612	27000	12000	6000	188
24080	3639011	214011	256	210	488821	152	167	9680	9100	6490	1900	130
24100	3639011	214011	315	210	514829	187	206	9606	26300	8860	2200	172
24110	3639011	814011	290	210	533662	172	190	9637	34700	13000	5500	207
24140	3639011	814011	362	210	523811	215	237	9547	17800	12690	7800	188
24160	3639011	814011	271	210	526074	161	177	9661	36400	12050	5500	192
24170	3639011	814011	248	210	520316	147	162	9690	0	10900	4500	181
24180	3639011	814011	277	210	530842	164	181	9654	12500	11810	4000	202

EXHIBIT 6.2

CODE FOR DATA

The data shown in Exhibit 6.1 is the data at a relatively advanced stage of analysis. Besides the original data, rate of loading, and modulus of elasticity, it contains brine volume, solid salt volume, ice volume, str.ate, and the natural log of str.ate.

A specimen of the data is shown below. The decimal is omitted in the data and immediately below each "word" in the specimen below is the word number.

12250	26390	11	8080	11	531	210	488337	315	347	9337	10000	8230	5400	132
(1)	(2)	(3)	(4)	(5)	(6)		(7)	(8)	(9)	(10)	(11)	(12)	(13)	
1	0	0	2	1	5		4	4	4	4	1	0	0	

Word Meaning

Word Number
Decimal Place

- 1 Identification number.
2 bcdeeff

b = date of collection

- 2 1 Nov-31 Dec
3 1 Jan-31 Apr
4 1 May-15 May
5 16 May-31 May
6 1 June-15 June
7 16 June-1 Aug
8 1 Aug-31 Oct

c = location of collection

- 1 100 yards of theater
2 1 mile off ACS
3 100 miles north of Barrow
4 200 miles north of Barrow
5 100-150 yards north of theater, 1961
6 300 yards north of theater

d = crystal type code

- 1 fine
2 medium
3 center
4 bottom
5 pack

ee - angle between sigma and zenith, 0° to 90°
ff - angle between sigma and c-axis, 0° to 90°
"11" indicates randomness

Word Meaning

- 3 ghhiij

g = failure typeCodeTension meaningCompression meaning

- 1
2

good test
weld failure

no visible deformation
tensile failure

3	head failure	head failure
4	no failure	plastic failure
5	not used	no information
6	"	bad test
7	"	bulge failure
8	"	explosive failure
9	"	ring around specimen

hh - age of sample at time of test, days.

\bar{ii} - depth from top of ice to center of specimen, inches.

\bar{J} - type of test, "1" is compression, "2" is tension

- 4 Chlorinity, o/oo
- 5 Temperature, -°C.
- 6 Natural log of Strate
- 7 Brine volume, relative
- 8 Solid salt volume, relative
- 9 Ice volume, relative
- 10 Modulus of Elasticity, $\text{psi} \times 10^5$.
- 11 Strength, psi.
- 12 Rate of loading, psi/min.
- 13 Strate.

Plotback
1 Inch Center Ice, Compression

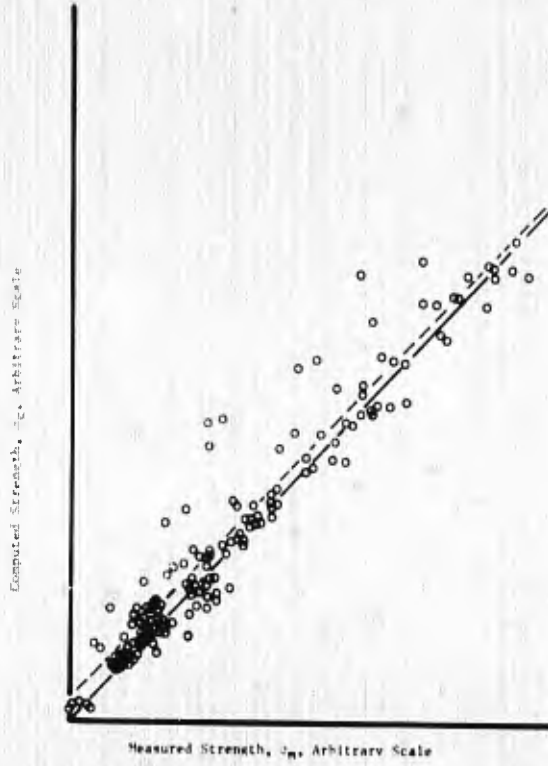


Exhibit 7.1A

Plotback,
4 Inch Center Ice, Compression

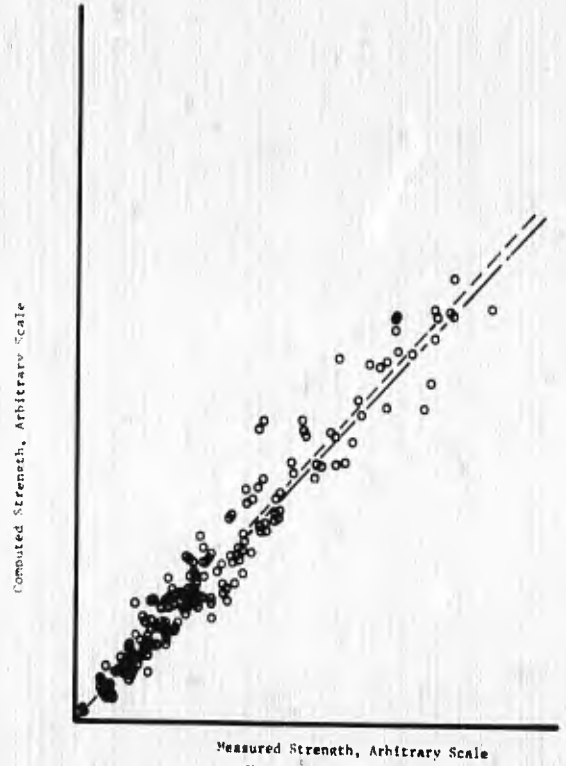


Exhibit 7.1B

Plotback, 7 Inch Center Ice
Compression

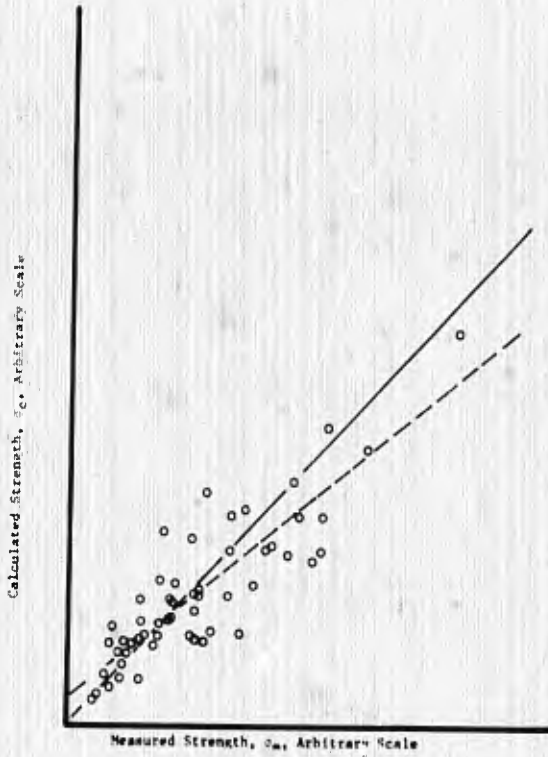


Exhibit 7.1C

Plotback, 11 Inch Center Ice,
Compression

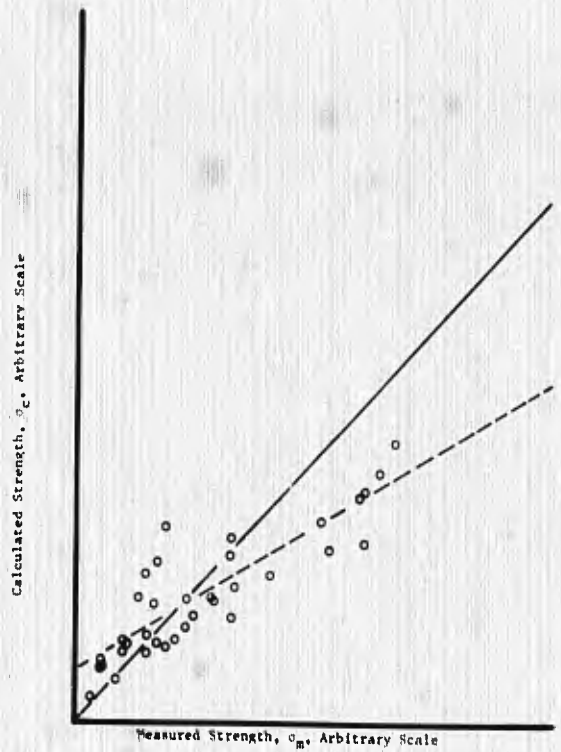


Exhibit 7.1D

Plotback, 17 Inch Center Ice
Compression

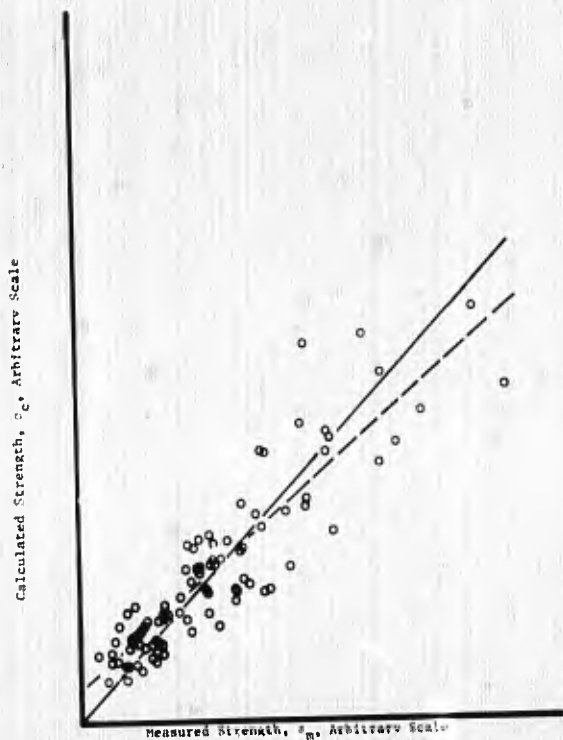


Exhibit 7.1F

Plotback, 32-36 Inch Center Ice,
Compression

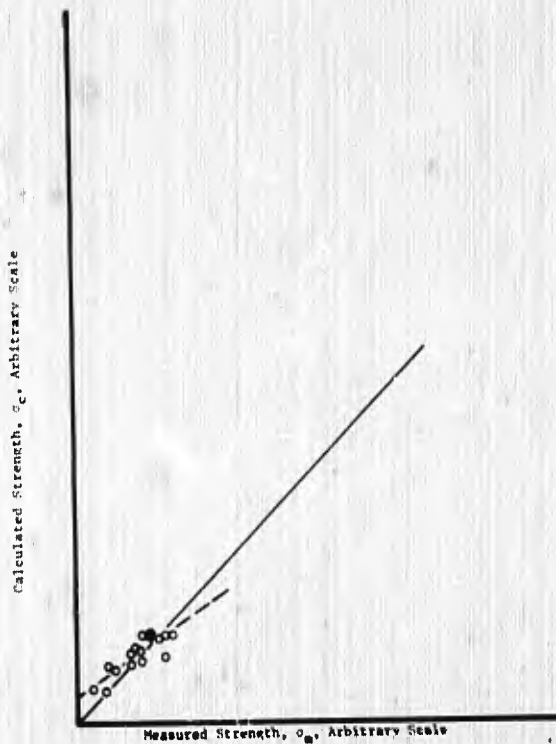


Exhibit 7.1E

Plotback, 25-29 Inch Center Ice
Compression

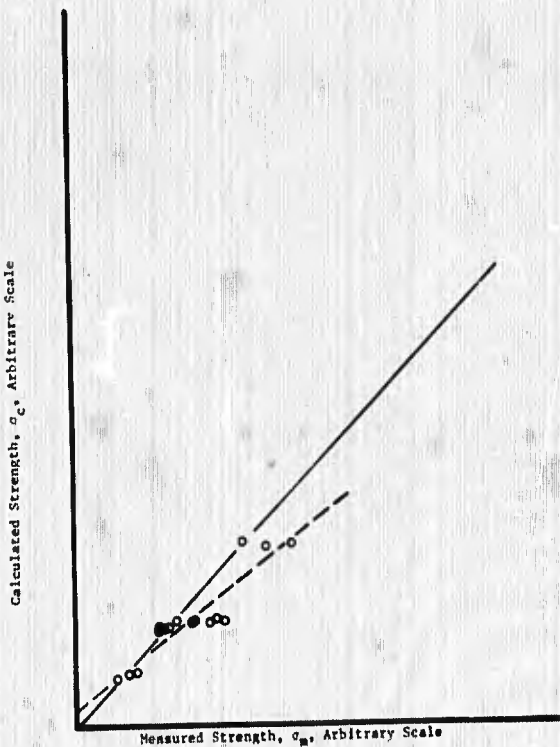


Exhibit 7.1G

Plotback, 18-21 Inch Center Ice,
Compression

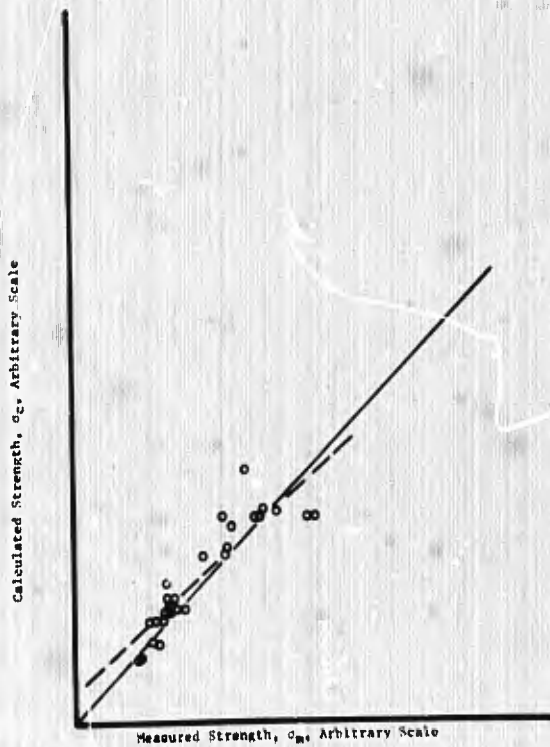


Exhibit 7.1H

EXHIBIT 7.2 BRINE VOLUME STRENGTH FUNCTION

TEMP	1.	2.	4.	DEPTH 8.	16.	32.	40.
1	34.8	36.8	38.6	40.4	42.5	44.9	45.8
2	76.1	63.2	54.6	49.2	46.4	45.6	45.7
3	94.2	74.8	61.6	53.1	48.2	45.9	45.7
4	104.8	81.6	65.7	55.4	49.2	46.1	45.7
5	112.0	86.2	68.5	56.9	49.9	46.2	45.7
6	117.3	89.5	70.5	58.0	50.4	46.3	45.7
7	121.3	92.1	72.1	58.9	50.7	46.4	45.7
8	124.6	94.2	73.4	59.6	51.1	46.5	45.6
9	127.2	95.9	74.4	60.1	51.3	46.5	45.6
10	129.5	97.3	75.3	60.6	51.5	46.5	45.6
11	131.3	98.5	76.1	61.0	51.7	46.6	45.6
12	133.0	99.6	76.6	61.4	51.9	46.6	45.6
13	134.4	100.5	77.2	61.7	52.0	46.6	45.6
14	135.7	101.3	77.7	62.0	52.1	46.6	45.6
15	136.5	102.0	78.1	62.2	52.2	46.7	45.6
16	137.8	102.7	78.5	62.4	52.3	46.7	45.6
17	138.7	103.3	78.8	62.6	52.4	46.7	45.6
18	139.6	103.8	79.2	62.8	52.5	46.7	45.6
19	140.3	104.3	79.5	62.9	52.5	46.7	45.6
20	141.0	104.7	79.7	63.1	52.6	46.7	45.6
21	141.6	105.1	80.0	63.2	52.7	46.7	45.6
22	142.2	105.5	80.2	63.4	52.7	46.8	45.6

EXHIBIT 7.6

TEMPERATURE MATRIX

DEPTH	WARM	MEDIUM	COLD
1	2.00	22.00	22.00
2	2.00	21.50	21.75
3	2.00	21.00	21.50
4	2.00	20.50	21.25
5	2.00	20.00	21.00
6	2.00	19.50	20.75
7	2.00	19.00	20.50
8	2.00	18.50	20.25
9	2.00	18.00	20.00
10	2.00	17.50	19.75
11	2.00	17.00	19.50
12	2.00	16.50	19.25
13	2.00	16.00	19.00
14	2.00	15.50	18.75
15	2.00	15.00	18.50
16	2.00	14.50	18.25
17	2.00	14.00	18.00
18	2.00	13.50	17.75
19	2.00	13.00	17.50
20	2.00	12.50	17.25
21	2.00	12.00	17.00
22	2.00	11.50	16.75
23	2.00	11.00	16.50
24	2.00	10.50	16.25
25	2.00	10.00	16.00
26	2.00	9.50	15.75
27	2.00	9.00	15.50
28	2.00	8.50	15.25
29	2.00	8.00	15.00
30	2.00	7.50	14.75
31	2.00	7.00	14.50
32	2.00	6.50	14.25
33	2.00	6.00	14.00
34	2.00	5.50	13.75
35	2.00	5.00	13.50
36	2.00	4.50	13.25
37	2.00	4.00	13.00
38	2.00	3.50	12.75
39	2.00	3.00	12.50
40	2.00	2.50	12.25

EXHIBIT 7.3 11-ROOT BRINE VOLUME MATRIX

TEMP	1.	2.	4.	DEPTH 8.	16.	32.	40.
1	.6173	.6444	.6728	.6930	.6950	.6694	.6811
2	.5934	.6028	.6237	.6447	.6676	.6922	.7006
3	.6562	.6722	.6890	.7068	.7257	.7460	.7529
4	.6992	.7131	.7278	.7434	.7599	.7777	.7837
5	.7281	.7408	.7541	.7681	.7831	.7991	.8046
6	.7493	.7610	.7732	.7862	.8000	.8148	.8198
7	.7646	.7765	.7880	.8001	.8130	.8268	.8315
8	.7786	.7889	.7998	.8112	.8234	.8364	.8409
9	.7893	.7991	.8094	.8203	.8319	.8443	.8486
10	.7983	.8077	.8175	.8279	.8390	.8509	.8550
11	.8059	.8149	.8244	.8344	.8451	.8566	.8605
12	.8125	.8212	.8304	.8401	.8504	.8615	.8652
13	.8183	.8267	.8356	.8450	.8550	.8657	.8694
14	.8234	.8316	.8402	.8493	.8590	.8695	.8730
15	.8279	.8359	.8443	.8532	.8627	.8728	.8763
16	.8320	.8398	.8480	.8567	.8659	.8758	.8792
17	.8356	.8433	.8513	.8598	.8688	.8785	.8818
18	.8390	.8465	.8543	.8626	.8715	.8810	.8842
19	.8420	.8494	.8571	.8652	.8739	.8833	.8864
20	.8448	.8520	.8596	.8676	.8762	.8853	.8884
21	.8474	.8545	.8619	.8698	.8782	.8872	.8903
22	.8497	.8567	.8641	.8718	.8801	.8890	.8920

EXHIBIT 7.7

RATE POWER MATRIX

DEPTH	WARM	MEDIUM	COLD
1	.160	.199	.199
2	.186	.231	.231
3	.200	.247	.248
4	.210	.258	.259
5	.217	.267	.268
6	.223	.274	.275
7	.228	.280	.282
8	.233	.285	.287
9	.237	.289	.292
10	.241	.293	.296
11	.244	.296	.300
12	.247	.299	.303
13	.250	.301	.306
14	.253	.304	.309
15	.255	.306	.312
16	.257	.308	.314
17	.260	.309	.317
18	.262	.311	.319
19	.264	.312	.321
20	.266	.313	.323
21	.268	.314	.324
22	.269	.315	.326
23	.271	.316	.328
24	.273	.317	.329
25	.274	.317	.331
26	.276	.317	.332
27	.277	.317	.333
28	.279	.317	.335
29	.280	.317	.337
30	.281	.317	.337
31	.283	.316	.338
32	.284	.316	.339
33	.285	.315	.340
34	.286	.314	.341
35	.288	.312	.342
36	.289	.311	.342
37	.290	.308	.343
38	.291	.306	.344
39	.292	.303	.344
40	.293	.299	.345

EXHIBIT 7.4 SALT REINFORCEMENT FUNCTION

TEMP	1.	2.	4.	DEPTH 8.	16.	32.	40.
1	.0	.0	.0	.0	.0	.0	.0
2	.0	.0	.0	.0	.0	.0	.0
3	.0	.0	.0	.0	.0	.0	.0
4	.0	.0	.0	.0	.0	.0	.0
5	.0	.0	.0	.0	.0	.0	.0
6	.0	.0	.0	.0	.0	.0	.0
7	.0	.0	.0	.0	.0	.0	.0
8	.0	.0	.0	.0	.0	.0	.0
9	11.4	10.1	8.4	6.1	3.4	.7	-.0
10	18.0	16.0	13.2	9.7	5.4	1.1	-.1
11	22.7	20.2	16.7	12.2	6.9	1.4	-.1
12	26.3	23.3	19.3	14.1	7.9	1.6	-.1
13	29.0	25.7	21.3	15.5	8.8	1.8	-.2
14	31.2	27.7	22.9	16.7	9.4	1.9	-.2
15	33.0	29.3	24.3	17.7	10.0	2.1	-.2
16	34.6	30.7	25.4	18.6	10.5	2.2	-.2
17	36.0	31.9	26.4	19.3	10.9	2.2	-.2
18	37.2	33.0	27.3	20.0	11.2	2.3	-.2
19	38.3	34.0	28.1	20.6	11.6	2.4	-.2
20	39.3	34.9	28.9	21.1	11.9	2.5	-.2
21	40.3	35.7	29.6	21.6	12.2	2.5	-.2
22	41.1	36.5	30.2	22.1	12.4	2.6	-.2

EXHIBIT 7.5 STRATE OF ICE SHEET

TEMP	1.	2.	4.	DEPTH 8.	16.	32.	40.
1	34.8	36.8	38.6	40.4	42.5	44.9	45.8
2	76.1	63.2	54.6	49.2	46.4	45.6	45.7
3	94.2	74.8	61.6	53.1	48.2	45.9	45.7
4	104.8	81.6	65.7	55.4	48.2	46.1	45.7
5	112.0	86.2	68.5	56.9	49.9	46.2	45.7
6	117.3	89.5	70.5	58.0	50.4	46.3	45.7
7	121.3	92.1	72.1	58.9	50.7	46.4	45.7
8	124.6	94.2	73.4	59.6	51.1	46.5	45.6
9	127.2	95.9	74.4	60.1	51.3	46.5	45.6
10	129.5	97.3	75.3	60.6	51.5	46.5	45.6
11	131.3	98.5	76.1	61.0	51.7	46.6	45.6
12	133.0	99.6	76.6	61.4	51.9	46.6	45.6
13	134.4	100.5	77.2	61.7	52.0	46.6	45.6
14	135.7	101.3	77.7	62.0	52.1	46.6	45.6
15	136.5	102.0	78.1	62.2	52.2	46.7	45.6
16	137.8	102.7	78.5	62.4	52.3	46.7	45.6
17	138.7	103.3	78.8	62.6	52.4	46.7	45.6
18	139.6	103.8	79.2	62.8	52.5	46.7	45.6
19	140.3	104.3	79.5	62.9	52.5	46.7	45.6
20	141.0	104.7	79.7	63.1	52.6	46.7	45.6
21	141.6	105.1	80.0	63.2	52.7	46.7	45.6
22	142.2	105.5	80.2	63.4	52.7	46.8	45.6

EXHIBIT 7.8

RATE FUNCTION FOR WARM ICE

DEPTH	100	300	1000	5000
1	2.094	2.498	3.031	3.925
2	2.364	2.903	3.635	4.910
3	2.517	3.138	3.994	5.516
4	2.630	3.313	4.266	5.982
5	2.721	3.456	4.490	6.372
6	2.799	3.578	4.684	6.712
7	2.867	3.686	4.856	7.017
8	2.928	3.784	5.011	7.295
9	2.983	3.872	5.154	7.552
10	3.034	3.954	5.286	7.792
11	3.081	4.031	5.410	8.018
12	3.126	4.102	5.527	8.231
13	3.167	4.170	5.637	8.435
14	3.206	4.234	5.742	8.629
15	3.244	4.295	5.843	8.815
16	3.279	4.353	5.939	8.994
17	3.313	4.409	6.031	9.167
18	3.346	4.463	6.120	9.334
19	3.377	4.515	6.206	9.496
20	3.407	4.564	6.289	9.653
21	3.436	4.613	6.370	9.806
22	3.464	4.659	6.448	9.955
23	3.491	4.705	6.524	10.100
24	3.518	4.747	6.598	10.242
25	3.543	4.792	6.670	10.380
26	3.568	4.833	6.741	10.515
27	3.592	4.874	6.810	10.648
28	3.616	4.914	6.877	10.778
29	3.639	4.953	6.943	10.905
30	3.662	4.991	7.007	11.030
31	3.684	5.028	7.071	11.153
32	3.705	5.064	7.133	11.274
33	3.726	5.100	7.193	11.392
34	3.747	5.135	7.253	11.509
35	3.767	5.169	7.312	11.624
36	3.787	5.203	7.370	11.737
37	3.806	5.236	7.426	11.849
38	3.825	5.268	7.482	11.959
39	3.844	5.300	7.537	12.067
40	3.862	5.332	7.591	12.174

EXHIBIT 7.10

RATE FUNCTION FOR COLD ICE

DEPTH	100	300	1000	5000
1	2.503	3.115	3.960	5.457
2	2.905	3.747	4.952	7.190
3	3.137	4.171	5.557	8.286
4	3.308	4.401	6.017	9.141
5	3.446	4.629	6.398	9.859
6	3.563	4.825	6.726	10.487
7	3.665	4.996	7.017	11.049
8	3.756	5.150	7.275	11.560
9	3.837	5.289	7.518	12.030
10	3.912	5.417	7.739	12.466
11	3.981	5.535	7.943	12.874
12	4.044	5.645	8.134	13.256
13	4.103	5.747	8.313	13.617
14	4.159	5.843	8.482	13.958
15	4.210	5.933	8.641	14.282
16	4.259	6.019	8.791	14.589
17	4.305	6.099	8.934	14.882
18	4.349	6.176	9.070	15.161
19	4.390	6.248	9.199	15.428
20	4.429	6.317	9.322	15.683
21	4.466	6.383	9.439	15.926
22	4.501	6.445	9.551	16.160
23	4.535	6.505	9.658	16.383
24	4.567	6.561	9.761	16.597
25	4.597	6.616	9.858	16.802
26	4.626	6.667	9.951	16.998
27	4.654	6.716	10.040	17.185
28	4.680	6.762	10.125	17.365
29	4.705	6.808	10.206	17.537
30	4.729	6.851	10.284	17.701
31	4.751	6.891	10.358	17.857
32	4.773	6.930	10.428	18.007
33	4.793	6.966	10.495	18.149
34	4.812	7.001	10.558	18.285
35	4.831	7.034	10.618	18.413
36	4.848	7.065	10.675	18.535
37	4.864	7.095	10.729	18.650
38	4.879	7.122	10.780	18.759
39	4.894	7.148	10.827	18.861
40	4.907	7.172	10.872	18.956

EXHIBIT 7.9

RATE FUNCTION FOR MEDIUM ICE

DEPTH	100	300	1000	5000
1	2.503	3.115	3.960	5.457
2	2.902	3.742	4.944	7.175
3	3.129	4.108	5.536	8.249
4	3.295	4.380	5.982	9.076
5	3.427	4.598	6.346	9.761
6	3.538	4.783	6.655	10.351
7	3.633	4.942	6.925	10.870
8	3.716	5.082	7.163	11.333
9	3.789	5.207	7.377	11.751
10	3.855	5.319	7.569	12.131
11	3.914	5.420	7.744	12.476
12	3.967	5.512	7.903	12.793
13	4.015	5.595	8.047	13.082
14	4.059	5.670	8.179	13.347
15	4.099	5.739	8.299	13.589
16	4.135	5.801	8.408	13.809
17	4.167	5.858	8.507	14.010
18	4.196	5.908	8.596	14.191
19	4.222	5.953	8.676	14.353
20	4.245	5.993	8.746	14.496
21	4.265	6.028	8.808	14.622
22	4.282	6.058	8.860	14.730
23	4.296	6.083	8.904	14.821
24	4.307	6.102	8.940	14.894
25	4.316	6.118	8.967	14.948
26	4.321	6.128	8.984	14.985
27	4.324	6.132	8.993	15.003
28	4.324	6.132	8.993	15.002
29	4.321	6.126	8.982	14.980
30	4.314	6.115	8.961	14.938
31	4.304	6.097	8.930	14.873
32	4.290	6.072	8.887	14.784
33	4.272	6.041	8.831	14.670
34	4.249	6.001	8.761	14.527
35	4.222	5.953	8.676	14.353
36	4.188	5.895	8.573	14.143
37	4.148	5.825	8.449	13.893
38	4.100	5.741	8.302	13.594
39	4.041	5.639	8.125	13.237
40	3.970	5.516	7.910	12.807

EXHIBIT 7.11

GENERAL BRINE VOLUME FUNCTIONS

DEPTH	X0	Y0	B	SIGD	G	SAL
.5	.389	31.56	359.60	251.04	1.432	7.908
1.5	.424	34.38	197.53	148.06	1.334	6.864
2.5	.442	35.84	145.17	116.77	1.243	6.379
3.5	.455	36.86	116.62	100.40	1.161	6.059
4.5	.464	37.66	97.90	90.04	1.087	5.821
5.5	.473	38.31	84.39	82.78	1.019	5.630
6.5	.479	38.87	74.02	77.37	.956	5.471
7.5	.486	39.36	65.72	73.14	.898	5.335
8.5	.491	39.80	58.89	69.75	.844	5.216
9.5	.496	40.19	53.12	66.95	.793	5.111
10.5	.500	40.55	48.17	64.41	.745	5.016
11.5	.504	40.88	43.86	62.61	.700	4.929
12.5	.508	41.19	40.06	60.88	.658	4.850
13.5	.512	41.48	36.67	59.37	.617	4.777
14.5	.515	41.75	33.63	58.04	.579	4.709
15.5	.518	42.00	30.87	56.86	.542	4.646
16.5	.521	42.24	28.36	55.81	.508	4.586
17.5	.524	42.47	26.06	54.87	.475	4.530
18.5	.527	42.68	23.94	54.01	.443	4.478
19.5	.529	42.89	21.99	53.24	.413	4.428
20.5	.532	43.09	20.17	52.53	.384	4.380
21.5	.534	43.28	18.47	51.88	.356	4.335
22.5	.536	43.46	16.89	51.29	.329	4.292
23.5	.538	43.63	15.40	50.74	.303	4.250
24.5	.540	43.80	14.01	50.24	.278	4.211
25.5	.542	43.97	12.69	49.77	.255	4.173
26.5	.544	44.12	11.44	49.34	.232	4.136
27.5	.546	44.28	10.26	48.93	.209	4.101
28.5	.548	44.43	9.14	48.56	.188	4.067
29.5	.550	44.57	8.08	48.21	.167	4.034
30.5	.552	44.71	7.07	47.88	.147	4.003
31.5	.553	44.84	6.10	47.57	.128	3.972
32.5	.555	44.98	5.18	47.28	.109	3.942
33.5	.556	45.10	4.30	47.01	.091	3.914
34.5	.558	45.23	3.45	46.76	.073	3.886
35.5	.559	45.35	2.64	46.52	.056	3.858
36.5	.561	45.47	1.86	46.29	.040	3.832
37.5	.562	45.59	1.11	46.08	.024	3.806
38.5	.564	45.70	.39	45.87	.008	3.781
39.5	.565	45.81	-.29	45.68	-.006	3.757

EXHIBIT 7.12

LINE VOLUME STRENGTH FUNCTIONS

DEPTH	WARM	MEDIUM	COLD
1	94.607	194.633	194.633
2	68.006	118.972	119.085
3	60.051	95.996	96.161
4	55.998	84.006	84.205
5	53.504	76.435	76.660
6	51.809	71.147	71.393
7	50.585	67.214	67.478
8	49.663	64.160	64.438
9	48.947	61.713	62.004
10	48.378	59.705	60.008
11	47.919	58.026	58.339
12	47.544	56.602	56.923
13	47.233	55.377	55.707
14	46.974	54.314	54.650
15	46.756	53.383	53.725
16	46.573	52.561	52.909
17	46.418	51.832	52.184
18	46.287	51.180	51.536
19	46.175	50.596	50.955
20	46.081	50.069	50.431
21	46.002	49.594	49.956
22	45.934	49.162	49.526
23	45.878	48.770	49.133
24	45.832	48.413	48.775
25	45.793	48.088	48.447
26	45.763	47.790	48.146
27	45.738	47.519	47.870
28	45.720	47.270	47.616
29	45.706	47.044	47.381
30	45.697	46.837	47.165
31	45.692	46.650	46.965
32	45.691	46.480	46.781
33	45.693	46.327	46.610
34	45.698	46.191	46.453
35	45.706	46.072	46.307
36	45.716	45.970	46.172
37	45.728	45.881	46.047
38	45.743	45.821	45.932
39	45.759	45.780	45.826
40	45.777	45.768	45.728

EXHIBIT 7.13

SALT REINFORCEMENT

DEPTH	WARM	MEDIUM	COLD
1	.000	44.531	44.531
2	.000	32.240	32.441
3	.000	33.981	34.353
4	.000	30.592	31.113
5	.000	27.734	28.390
6	.000	25.251	26.030
7	.000	23.053	23.944
8	.000	21.080	22.076
9	.000	19.292	20.386
10	.000	17.660	18.846
11	.000	16.160	17.434
12	.000	14.774	16.133
13	.000	13.489	14.929
14	.000	12.291	13.811
15	.000	11.172	12.770
16	.000	10.122	11.798
17	.000	9.133	10.889
18	.000	8.201	10.037
19	.000	7.317	9.237
20	.000	6.478	8.485
21	.000	5.678	7.777
22	.000	4.912	7.110
23	.000	4.177	6.481
24	.000	3.467	5.887
25	.000	2.780	5.326
26	.000	2.109	4.796
27	.000	1.452	4.296
28	.000	.804	3.823
29	.000	.007	3.376
30	.000	.000	2.954
31	.000	.000	2.556
32	.000	.000	2.180
33	.000	.000	1.826
34	.000	.000	1.494
35	.000	.000	1.181
36	.000	.000	.889
37	.000	.000	.615
38	.000	.000	.361
39	.000	.000	.126
40	.000	.000	-.090

EXHIBIT 7.14

STRATE VALUES

DEPTH	WARM	MEDIUM	COLD
1	94.607	239.164	239.164
2	68.006	157.213	157.527
3	60.051	129.978	130.514
4	55.998	114.598	115.310
5	53.504	104.169	105.051
6	51.809	96.399	97.423
7	50.585	90.267	91.427
8	49.663	85.240	86.515
9	48.947	81.006	82.391
10	48.378	77.365	78.854
11	47.919	74.187	75.774
12	47.544	71.376	73.056
13	47.233	68.865	70.636
14	46.974	66.605	68.462
15	46.756	64.555	66.496
16	46.573	62.683	64.708
17	46.418	60.965	63.074
18	46.287	59.381	61.574
19	46.175	57.914	60.192
20	46.081	56.548	58.916
21	46.002	55.272	57.734
22	45.934	54.075	56.636
23	45.878	52.948	55.614
24	45.832	51.881	54.662
25	45.793	50.868	53.774
26	45.763	49.900	52.943
27	45.738	48.971	52.166
28	45.720	48.075	51.439
29	45.706	47.204	50.758
30	45.697	46.337	50.120
31	45.692	46.450	49.522
32	45.691	46.480	48.962
33	45.693	46.327	48.437
34	45.698	46.191	47.947
35	45.706	46.072	47.489
36	45.716	45.970	47.061
37	45.728	45.886	46.663
38	45.743	45.821	46.294
39	45.759	45.780	45.952
40	45.777	45.768	45.637

EXHIBIT 7.15

WARM ICE STRENGTH

DEPTH	100	300	1000	5000
1	198.180	236.412	286.832	371.415
2	160.789	197.428	247.235	333.976
3	151.192	188.448	239.899	331.263
4	147.310	185.542	238.926	335.018
5	145.637	184.934	240.278	340.957
6	145.046	185.424	242.692	347.784
7	145.060	186.507	245.647	354.984
8	145.440	187.935	248.890	362.321
9	146.052	189.570	252.288	369.678
10	146.817	191.334	255.763	376.993
11	147.687	193.177	259.272	384.231
12	148.627	195.068	262.784	391.377
13	149.616	196.985	266.284	398.421
14	150.638	198.911	269.758	405.361
15	151.683	200.846	273.201	412.195
16	152.741	202.773	276.609	418.925
17	153.808	204.691	279.977	425.555
18	154.878	206.596	283.306	432.087
19	155.949	208.487	286.554	438.524
20	157.018	210.360	289.841	444.871
21	158.083	212.217	293.048	451.130
22	159.142	214.054	296.216	457.305
23	160.196	215.874	299.345	463.401
24	161.242	217.674	302.436	469.419
25	162.281	219.455	305.490	475.363
26	163.311	221.218	308.508	481.236
27	164.333	222.962	311.491	487.040
28	165.346	224.688	314.444	492.779
29	166.350	226.396	317.357	498.455
30	167.346	228.086	320.242	504.070
31	168.333	229.758	323.095	509.627
32	169.311	231.414	325.919	515.127
33	170.280	233.053	328.714	520.573
34	171.240	234.676	331.480	525.966
35	172.192	236.283	334.219	531.309
36	173.135	237.874	336.931	536.603
37	174.070	239.451	339.618	541.849
38	174.996	241.012	342.279	547.050
39	175.915	242.559	344.916	552.206
40	176.825	244.092	347.530	557.319
SUMS	6408.111	8524.248	11669.371	17793.785
AVERAGE	160.202	213.106	291.734	444.844

EXHIBIT 7.17

OLD ICE STRENGTH

DEPTH	100	300	1000	5000
1	596.665	745.156	847.169	1305.246
2	457.721	542.354	780.230	1132.713
3	409.466	517.874	725.272	1081.538
4	381.518	507.545	693.941	1054.194
5	362.059	486.381	672.155	1035.799
6	347.167	470.104	655.354	1021.757
7	335.105	456.836	641.572	1010.183
8	324.965	445.603	629.810	1000.171
9	316.218	435.844	619.447	991.242
10	308.529	427.205	610.282	983.081
11	301.675	419.450	601.945	975.545
12	295.448	412.416	594.294	968.506
13	289.883	405.982	587.247	961.887
14	284.744	400.060	580.708	955.632
15	280.014	394.659	574.610	949.700
16	275.642	389.486	568.903	944.001
17	271.583	384.736	563.566	938.689
18	267.804	380.293	558.504	933.564
19	264.276	376.128	553.749	928.671
20	260.974	372.214	549.259	923.992
21	257.878	368.531	545.011	919.526
22	254.971	365.061	540.989	915.261
23	252.237	361.786	537.176	911.183
24	249.663	358.694	533.564	907.284
25	247.238	355.772	530.135	903.516
26	244.951	353.009	526.882	899.942
27	242.794	350.397	523.795	896.527
28	240.759	347.925	520.865	893.266
29	238.838	345.588	518.087	890.154
30	237.026	343.378	515.452	887.187
31	235.317	341.290	512.956	884.363
32	233.706	339.319	510.594	881.678
33	232.190	337.460	508.362	879.121
34	230.764	335.709	506.256	876.720
35	229.426	334.064	504.274	874.444
36	228.172	332.521	502.414	872.304
37	227.002	331.080	500.674	870.301
38	225.912	329.738	499.054	868.438
39	224.903	328.495	497.555	866.717
40	223.974	327.351	496.177	865.143
S	11391.247	15225.436	23136.334	37659.202
R	284.781	48.135	575.458	946.480

EXHIBIT 7.16

MEDIUM ICE STRENGTH

DEPTH	100	300	1000	5000
1	592.665	745.156	847.169	1305.246
2	456.301	588.367	777.379	1128.136
3	406.800	534.161	719.676	1072.287
4	377.673	501.967	685.622	1040.150
5	357.081	479.074	661.119	1016.864
6	341.090	461.095	641.605	97.564
7	327.956	446.146	625.112	981.224
8	316.764	433.248	610.623	966.090
9	306.980	421.832	597.594	951.954
10	298.265	411.540	585.674	938.528
11	290.392	402.132	574.590	925.629
12	283.197	393.437	564.099	913.133
13	276.563	385.431	554.226	900.981
14	270.398	377.717	544.816	889.014
15	264.632	370.519	535.794	877.265
16	259.206	363.677	527.058	865.658
17	254.073	357.138	518.676	854.146
18	249.193	350.859	510.480	842.690
19	244.531	344.795	502.469	831.248
20	240.055	338.924	494.604	819.778
21	235.738	333.200	486.866	808.232
22	231.554	327.597	479.158	796.584
23	227.478	322.085	471.503	784.765
24	223.467	316.633	463.843	772.731
25	219.557	311.212	456.149	760.425
26	215.665	305.792	448.350	747.785
27	211.787	300.361	440.432	734.745
28	207.901	294.827	432.341	721.234
29	203.286	289.225	422.581	704.763
30	202.084	286.419	419.753	699.651
31	200.802	284.443	416.906	693.856
32	199.425	282.275	413.081	687.208
33	197.936	279.887	409.136	679.564
34	196.314	277.243	404.712	671.054
35	194.534	274.302	399.736	661.274
36	192.564	271.008	394.116	650.187
37	190.361	267.294	387.734	637.502
38	187.876	263.065	380.429	622.929
39	185.028	258.189	371.977	606.037
40	181.754	252.473	362.045	586.190
SUMS	10524.920	14503.553	20638.887	33144.709
AVERAGE	263.123	362.588	515.972	828.617

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EXHIBIT A

TIME-STRAIN-STRESS DATA

Tensile stress-strain test

Tensile creep tests

Compressive stress-strain test

Compressive creep tests

TIME-STRAIN-STRESS DATA

This exhibit contains the detailed data from stress-strain and creep tests. The column headings have the following meaning:

Time

This is the clock time which was photographically recorded simultaneously with measurements of load and deformation. Time is generally expressed in the data as hours, minutes, and hundredths of minutes. The format of the six digit number (123456) is hours in digits 1 and 2, minutes in digits 3 and 4, and hundredths of minutes in digits 5 and 6. In some cases, digits 5 and 6 represent seconds, and these cases are noted. Some creep tests have time durations greater than 99 hours. In these cases the leading 100's of hours digit has been ignored.

Strain

Strain is calculated from the raw deformation measurements and is expressed as a dimensionless number. The number is listed as strain $\times 10^5$. Exceptions to the exponent 5 are noted.

Stress

Compression: Stress is calculated from the raw data load measurements and is expressed in pounds per square inch. The number listed is stress $\times 10^0$. Exceptions to the exponent 0 are noted.

Tension: Stress is expressed in pounds per square inch and the number listed is stress $\times 10^1$. Exceptions to the exponent 1 are noted.

Test number

A test identification number precedes the set of time-strain-stress data for each test

The tension tests are the first test listed and start on page A 4. These are then followed by the compression tests which begin with test 1 and continue through the remainder of Exhibit A.

Some tension tests were re-run because of weld or head failures. Data for the original run and each re-run are listed.

Explanatory Notes.

1. Strain data expressed as strain $\times 10^5$.
2. Strain data expressed as strain $\times 10^4$.
3. Strain data expressed as strain $\times 10^6$.
4. Stress data expressed as stress $\times 10^0$.
5. Stress data expressed as stress $\times 10^1$.
6. Not used.
7. The last two time digits represent seconds.

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
0141			0141			0141			0141			0141		
SEE NOTES 2,4,7			0141			0141			0141			0141		
101903	0	0	093040	0	0	0165			205911	94	83	167538	237	652
101910	13	8	093044	13	11	091751	0	0	205914	104	92	167539	279	726
101919	49	13	093047	24	20	091801	0	0	205918	117	100	167542	320	807
101926	74	19	093050	40	26	091808	3	2	205920	131	104	167543	350	875
101928	102	28	093054	53	33	091811	8	8	205925	167	103	167545	366	953
101940	140	36	093057	64	39	091814	13	17	205929	193	105	0435		
101947	167	45	093100	77	47	091817	20	26	205932	226	97	SEE NOTE 7		
101952	188	53	093103	88	57	091820	27	35	205936	238	108	150400	0	0
101957	204	62	093106	100	67	091823	33	44	205939	116	106	150403	0	6
102001	218	71	093107	116	76	091825	37	52	0185			150405	0	22
102006	233	82	0148			091828	42	61	SEE NOTES 2,4,7			150410	0	23
102012	250	94	SEE NOTES 2,4,7			091831	42	71	090539	0	0	150415	24	60
102016	265	105	100921	0	0	091834	46	81	090600	0	0	150417	32	108
102021	310	109	100929	20	56	091837	53	91	090609			150419	84	134
102027	322	110	100935	16	36	091840	59	101	090617	1	3	150421	93	208
102032	392	86	100940	50	56	0176			090621	10	11	150422	100	212
102040	404	112	100946	64	76	SEE NOTES 2,4,7			090625	25	19	150426	100	212
102044	420	138				204633	0	0	090628	36	26	150428	100	212
0142			0154			204702	1	0	090631	46	36	150432	128	296
SEE NOTES 2,4,7			SEE NOTES 2,4,7			204710	1	2	090634	55	43	150433	144	338
133220	0	0	213035	0	0	204713	8	8	090637	63	51	150434	180	382
133319	70	34	213039	10	11	204716	16	17	090640	76	58	150436	236	445
133332	150	53	213042	20	19	204719	23	20	090644	84	65	150437	236	510
133340	181	68	213045	27	27	204723	33	33	090647	97	71	0438		
133609	185	67	213047	33	36	0177			090649	109	77	169290	0	0
140403	188	67	213050	39	43	0178			090653	123	84	169296	0	0
150800	195	67	213053	46	51	SEE NOTES 2,4,7			090659	92	92	169280	0	33
155115	196	68	213056	54	59	214846	0	0	0186			169281	36	77
170000	200	68	213059	62	67	214859	0	0	SEE NOTES 2,4,7			169282	48	114
180800	203	68	213102	70	76	214904	0	1	195252	0	0	169283	76	156
190000	204	69	213105	78	84	214910	2	2	195304	0	0	169284	96	201
201500	207	68				214914	9	8	195308	1	1	169285	168	250
210000	208	67	0154			214917	17	17	195312	8	7	169286	172	299
222200	209	67	SEE NOTES 2,4,7			214922	42	18	195315	17	16	169287	208	339
244000	213	68	201508	0	0	214928	71	25	195318	25	24	169288		
080700	225	68	201516	0	0	214931	83	29	195321	35	32	0442		
081013	357		201545	1	1	214934	96	33	195324	46	41	167725	0	0
0143			201548	3	4	214937	109	37	195327	56	50	162724	0	18
SEE NOTES 2,4,7			201552	13	11	0178			195330	51	50	162731	0	55
100902	27	0	201554	21	19	0178			195333	59	68	162732	0	97
100700	28	0	201557	33	27	SEE NOTES 2,4,7			195336	67	77	162734	0	147
100717	0	20	201600	38	34	094218	0	0	195338	72	86	162735	8	184
100732	70	36	201604	40	44	094232	0	1	195341	79	94	162736	16	233
100738	89	51	201607	50	54	094240	0	2	195345	88	105	162737	40	271
100742	100	63	201610	67	64	094242	10	8	195348	96	115	162738	44	303
100746	109	77	201614	78	74	094246	20	17	195351	103	123	162739	56	137
100750	131	81				094249	29	25	195355	113	140	162740	60	369
100754	139	94	0155			094252	35	32	195358	121	156	162741	60	409
100759	147	105	SEE NOTES 2,4,7			094255	43	42	195402	147	147	162742	52	449
0144			213305	0	0	094258	50	51	0190			162743	48	484
SEE NOTES 2,4,7			213308	9	8	094259	57	60	SEE NOTES 2,4,7			0449		
214502	0	0	213311	16	17	094304	65	69	140110	0	0	150002	0	0
214519	27	18	213314	25	27	094307	72	77	140119	5	9	150005	0	28
214529	69	34	213317	30	37	094310	78	85	140133	7	37	150006	29	104
214542	135	51	213320	37	47	094313	92	92	140139	16	84	150008	42	171
214548	160	62	213323	44	57	0179			140142	24	105	150007	129	245
214554	190	70	213326	45	66	SEE NOTES 2,4,7			140149	34	176	150007	167	325
214556	190	74	213329	58	75	092147	0	0	140154	43	221	150008	213	402
0145			213332	81	81	092201	0	0	140200	54	268	0450		
SEE NOTES 2,4,7			0156			092211	3	3	140207	70	302	162077	0	0
213730	0	0	SEE NOTES 2,4,7			092214	8	10	140211	87	308	162080	4	47
213736	13	17	235045	0	0	092217	16	18	140214	118	279	162080	33	144
213740	27	26	235103	0	0	092224	25	27	140217	260	240	162081	62	225
213746	57	35	235106	17	7	092226	38	44	0418			162081	100	309
213750	71	45	235110	29	17	092229	45	54	162082	158	394	0451		
213754	84	56	235113	33	27	092234	52	62	155825	0	0	175200	0	0
213757	97	66	235116	35	34	092237	57	70	155829	33	30	175202	8	11
213800	108	76	235120	42	44	092234	57	70	155832	37	37	175202	8	11
213804	117	85	235123	54	51	092237	57	75	155835	63	111	175203	8	44
213807	126	93	235125	58	59	0180			155836	67	144	175203	37	123
0145B			235128	63	67	SEE NOTES 2,4,7			155837	67	188	175204	70	174
SEE NOTES 2,4,7			235131	79	75	101420			155838	83	250	175204	100	226
192108	0	0	235134	83	84	101430	0	0	155839	104	302	175205	133	281
192113	11	9	235137	92	92	101434	3	2	155840	108	340	175205	166	333
192116	22	20	235140	100	100	101439	3	3	155842	142	397	175206	195	403
192119	33	29				101443	10	11	155843	171	443	175206	220	459
192123	50	41	0163			101446	17	21	155844	204	510	0455		
192128	65	55	SEE NOTES 2,4,7			101449	25	30	155846	238	598	152050	0	0
192132	78	66	211659	0	0	101452	30	41	155848	271	675	152133	4	9
192135	97	75	211707	3	3	101455	38	50	155849	271	675	152145	4	46
192139	128	84	211712	13	10	101458	38	60	0419			152157	12	76
192143	162	91	211716	28	21	101501	38	70	SEE NOTE 7			152164	16	107
192352	728		211720	46	31	101504	38	70	167501	0	0	152173	64	143
192404	728		211726	75	40	101507	38	87	167504	0	16	152187	104	

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
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170458	437	918	143205	20	167	153563		726
170459	508	1005	143220	95	234	153569		726
	532	1003	143235	128	301	153576		726
0479			143243	140	335	0516		
015560	0	0	143250	160	368	000045	0	0
015640	0	30	143258	172	402	000076		170
015660	12	98	143265	196	435	000147		500
015676	32	167	143273	212	469	000237		420
015691	56	236	143277	216	489	0518		
015705	76	302	143280	224	506	140073	0	0
015720		368	143288	244	539	140115		170
015727		398	143295	252	573	140188		500
015735	120	445	143303	264	604	0517		
015746	128	502	143311	284	637	113158	0	0
015760	152	566	143317	300	670	113201		170
015767	160	571	143325	320	703	113274		500
015774	184	639	143333	352	737	113392		1060
015781	200	671		408	767	0519		
015793	216	735	0501			153850	0	0
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015825	312	872	160375	4	34	153964		500
015840	344	938	160390	24	101	154092		709
015847	360	971	160405	44	171	0520		
015862	384	1042	160420	64	238	172164	0	0
015877	56	1104	160440	104	335	172202		170
015885	472	1141	160444	128	369	172275		500
015900	540	1206	160453	144	402	172345		770
0480			160465	180	469	0521		
154540	0	0	160478	216	536	114815	0	0
154555	16	33	160485	232	570	114857		170
154572	60	100	160490	260	603	114933		500
154588	120	167		264	630	114978		713
154602	184	234	0502			0522		
154617	232	301	172825	0	0	000030	0	0
154632	280	368	172829	28	67	000067		170
154653	308	469	172830	32	97	000149		500
154668	320	536	172830	36	121	000194		780
154682	396	603	172830	52	151	0525		
0482			172831	56	174	131132	0	0
173725	0	0	172831	72	208	131136		190
173746	36	45	172831	72	191	131149		680
173764	72	113	172832	92	278	131150		740
173780	108	187	172833	104	315	0525		
173795	132	247	172833	116	345	152177	0	0
173810	172	314	172834	132	379	152181		170
173825	212	392	172834	144	409	152194		690
173840	248	455	172835	160	452	152196		780
0486			172835	180	486	0523		
132477	0	0	172835	192	519	164615	0	0
132481	64	170	172836	204	553	164654		170
132482	64	234	172836	224	590	164726		500
132482	92	316	172836		588	164770		703
132483	112	375	0503			0524		
132483	136	455	112752	0	0	180900	0	0
132484	176	519	112753	0	20	180910		180
132484	196	586	112754	4	117	180918		510
132485	248	656	112755	8	161	180923		680
132485	280	732	112755	20	223	180926		803
0489			112756	24	302	0526		
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151802	8	56	112758	40	429	171810		190
151803	16	125	112758	40	499	171819		500
151804	36	202	112759	48	556	171822		590
151805	64	261	112760	56	610	171823		590
151805	88	328	112760	80	684	0527		
151806	112	392	112761	84	762	190803	0	0
151806	140	462	112762	104	824	190805		12
151807	172	526		112	838	190807		30
151807	232	599	0507			190809		63
151808	300	695	134375	0	0	190811		96
151808	332	764	134410	12	39	190813		133
151809	412	831	134432	52	134	190814		171
151809	448	898	134448	76	201	190815		200
151810	496	983	134462	124	268	190817		234
151810	552	1047	134478	172	335	190818		258
151811			134493	240	402	190819		271
0491			134500	264	436	190820		300
165550	0	0	134510	288	469	190821		317
165551	0	37	134517	312	503	190822		342
165552	4	97		352	519	190823		367
165553	12	186	0511			190824		396
165553	32	251	151000	0	0	0528		
165554	40	312	151030	4	34	204651		
165554	60	375	151047	20	99	204653		4
0494			151062	60	168	204654		12
131150	0	0	151077	124	238	204656		54
131230	8	44	151105	184	302	204658		88
131245	40	107	151120	256	369	204660		125
131260	80	178	151125	328	436	204661		158
131275	120	245	151132	396	503	204663		204
131290	160	312	151140	432	536	204665		242
131303	196	379	151153	492	603	204667		272
131310	216	409	151160	524	640	204668		321
131316	260	442	151168	556	670	204669		354
131324	296	476	151175	548	704	204670		392
0500			151190	540	771	204671		421
143150	0	0	0515			204672		450
143172	12	33	153411	0	0	204673		475
			153452			170	204674	526

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
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204677			151837	354	420	151817	254	410
0529			151847	413	470	151819	296	470
095652			151857	471	520	151820	317	500
095653		33	0536			151821	358	540
095655	29	104	181142			151822	375	570
095656	46	174	181159	17	33	151823	388	606
095658	83	240	181171	46	84	151824	429	640
095660	121	308	181193	83	134	151825	463	686
095661	163	370	181195	121	184	151826	463	720
095663	204	435	181205	158	240	151827	483	776
095665	246	505	181216	192	290	151828	546	840
095666	275	544	181227	225	335	0544		
095666	300	592	181235	254	370	170604		
095667	325		181242	283	400	170605		42
095668	379	680	181249	312	435	170606		105
095670	420		181255	338	470	170607		167
0530			0537			170610		220
131477			170220			170611		258
131485	21	33	170233	13	33	170612		318
131502	29	100	170250	42	100	170613		351
131519	63	170	170266	79	170	170615		404
131534	83	234	170280	116	234	170616		455
131548	104	300	170294	158	300	170617		502
131562	113	368	170310	200	370	170618		545
131577	146	435	170320	229	415	170619		590
131591	167	500	170332	263	470	0545		
131605	187	565	170345	292	520	201282		
131621	229	636	170355	325	570	201283		49
0531			170365	342	600	201285		114
140691			0538			201286		170
140700	8	33	091424			201287		234
140715	21	100	091433	17	33	201290		300
140731	25	167	091444	46	84	201291		368
140746	63	234	091458	83	134	201303		780
140760	63	300	091465	104	167	114977		
140773	104	370	091473	125	204	114980		40
140781	104	410	091480	142	234	114981		104
140800	129	500	091487	163	270	114983		176
140813	146	570	091494	188	304	114984		234
140820	146	600	091500	208	335	114986		306
140828	154	636	091507	225	370	114987		368
140836	179	670	0539			114990		438
140842			114927			0547		
0532			114940	21	33	133179		
160186			114952	50	84	133196	452	733
160196	13	32	114963	83	134	0548		
160205	29	65	114975	121	190	152122		
160213	50	99	114985	154	240	152139	326	642
160221	67	132	114995	188	290	0549		
160229	92	166	115005			152667	539	830
160236	108	199	0540			0550		
160244	130	233	132186			172904		
160250	150	266	132204	21	33	173069	554	810
160257	171	301	132220	63	100	0551		
160263	196	335	132236	96	170	133735		
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TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS			
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		700	151708	110	610	131844	92	400	215860	260	940	000083	804	154390	66	167	
0558			151710	150	680	131849	105	480	215873	280	1000	0714		154410	84	234	
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154056			151718			131869	172	740	215921	390	1280	0720		154480	188	504	
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170037			170015	0	70	131885	215	950	0649			001061	670	171315	104	70	
170180	912	689	170016	30	120	131890	222	1010	083510	0	0	001821	1242	171332	96	130	
0561			170017	60	170	131897	234	1080	083603	0	30	0723		171347	92	200	
143808			170018	60	230	131903	238	1120	083611	0	70	000000		171362	116	270	
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170415	116	358	170034	220	820	163655	60	200	083720	170	670	000000	0	201540	202	200	
170429	385	950	170035	260	890	163660	70	270	083732	200	740	000285	228	201560	206	270	
0564			170037	290	950	163665	80	340	083744	210	800	000782	912	201580	222	400	
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143280			0623			0641			083793	350	1070	000086	1305	201652	288	600	
143291	282	427	181053	0	0	130560	0	0	083804	1130		0729		201663		670	
0566			181055	0	60	130595	0	70	0649			000000		0915			
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163050	466	870	181058	10	160	130620	10	200	151789	0	50	000073	1093	084601	26	30	
0567			181059	36	210	130634	20	270	151805	20	121	0733		084610	32	70	
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182579	100	590	133728	0	0	130854	250	1470	222614	44	402	143383	0	084757	192	700	
182580	110	630	133740	10	80	130867		1490	222630	184	469	143395	6	11	084765	196	740
182581	120	670	133746	10	150	0644			222644	244	526	143405	5	18	0916		0
182583	120	720	133751	20	220	151954	0	0	222657	272	570	143416	12	27	134621		0
182584	130	770	133755	30	280	151965	40	50	222668	312	610	143428	13	36	134634	2	30
182585	130	810	133760	50	350	151979	68	120	222682	412	663	143440	8	46	134648	0	70
182587	140	860	133765	50	410	151990	92	190	222691	456	698	143452	17	55	134657	6	100
182588	170	940	133770	60	480	152003	120	260	222709	692	767	143464	25	64	134667	6	130
182590	190	1010	133774	70	560	152015	138	320	222725	992	836	143475	24	73	134674	16	170
182593	210	1080	133778	80	620	152029	160	400	222741	1072	901	143487	23	82	134681	26	200
182595	240	1140	133783	90	680	152044	192	490	222751	1140	938	143498	21	91	134689	30	230
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140634	0	70	133802	150	960	152110	320	860	090776	112	151	0759		134727	42	470	
140636	4	120	133805	160	1040	152122	336	930	090788	196	201	SEE NOTES 1,4		134736	52	540	
140637	12	180	133810	170	1080	152134	368	990	090804	320	288	190000	0	0	134744	56	600
140638	16	240	133815	190	1150	152145	400	1060	090820	512	335	190062	17	2	134751	66	670
140640	20	300	133820	210	1220	152158	420	1130	090838	712	402	190072	15	9	134765	88	740
140641	30	350	133825	230	1290	152171	448	1200	090848	912	442	190084	32	18	134780	94	800
140643	30	400	133830	250	1350	152181		1250	090855	972	469	190097	39	28	0917		
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140647	50	610	144827	10	0	165221	20	70	090904	1660	637	190135	21	55	171275	50	70
140649	60	680	144835	0	60	165235	40	130	090920	1712	737	190149	63	64	171284	56	100
140650	70	750	144840	10	140	165247	40	200	090938	1784	804	190157	68	68	171291	66	130
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0919			165565	134	70	195205	176	380	103326	10	60	091739	44	730	113365	80	270
210723	0	0	165572	170	100	195207	214	420	103370	60	120	091741	50	800	113378	100	340
210735	26	30	165583	246	140	195209	238	460	103394	90	180	091742	70	880	113390	130	400
210744	54	70	165590	266	170	195210	262	500	103408	120	210	091745	114	950	113403	160	470
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10758	52	130	165613	434	240	195214	326	590	103434	150	350	0936			113430	260	600
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210780	130	230	165647	864	340	101300		0	103471	220	530	114549		120	0943		
210788	158	270	165660	1120	370	101352		20	103483	240	580	114550		180	154985	00	0
210795	190	300	165673	1360	400	101366		20	103497	262	660	114552		230	155000	20	70
210804	236	340	0923			101378		40	103511	320	730	114554		290	155014	20	110
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210840	448	470	081761		17	101400		80	103544	420	880	114556		410	155041	50	270
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210876			081780		46	101426		80	114559			114560		530	155068	140	400
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114440	76	70	081810		138	101464		140	114564			114564		720	0944		
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114463	136	180	081840		282	101500		220	114568			152320	66	220	104235		200
114471	154	220			320	101511		240	114569			152321	86	280	104240		270
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114488	204	290	194351		8	101536		280	114571			152327	106	390	140807		0
114495	238	320	194352		14	104373		0	114572			152328	122	450	140833		0
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154178	266	720	194366		162	104597		180	114585			114929		120	140865		0
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162591	150	540	114730	59	34	132737	40	161	050152	28	263	133137	30	403	053041	46	188
162592	164	600	114745	58	66	132748	68	208	050159	28	300	133142	10	460	053074	60	270
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162596	196	740	114763	49	155	132764	72	307	050178	38	397	133149	64	551	053144	104	284
162597	210	800	114776	47	212	132779	76	359	050191	72	444	133151	74	595	053177	127	313
162599	224	869	114793	44	285	132788	80	410	050202	82	532	133155	84	643	053218	156	348
0950			114812	48	357	132799	88	477	050214	112	602	133158	84	672	053257	184	385
092530	00	0	114835	55	429	132809	92	545	050225	118	667	133161	100	749	053290	220	418
092500	30	70	114855	68	501	132820	120	612	050236	132	735	133164	100	800	053329	256	454
092504	10	130	114876	76	573	132830	142	580	050247	148	801	133167		799	053367	298	487
092506	00	200	114893	70	646	132840	240	749	050257	178	867	0966			053402	332	519
092509	20	270	114911	69	718	132851	340	824	050270	200	934	132900	0	0	053438	376	553
092592	40	340	114931	98	790	132860	402	882	050281		1000	133001	0	2	053473	420	547
092595	54	400	114949	98	862	0965			050291			133007	7	28	053503	458	621
092598	90	470	114967	135	942	080817	0	0	0973			133011	7	91	0966		
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092607	130	670	090365	50	10	080862	2	121	083680	18	63	133023	30	306	114976	0	46
092609	150	740	090385	50	43	080876	4	171	083687	24	100	133026	37	324	114983	4	82
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092614	190	870	090418	70	144	080901	14	306	083702	68	169	133036	46	475	114992	0	151
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195952	1080		193541	28	10	081016		987	0975			163123	0	113	115061	66	583
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161090	0		193796	854	837	161082	192	539	172919	314	408	163168	196	782	161821	40	47
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171895	21	114	0961			175273			172958	668	668	012963	12	15	161957	28	181
171921	78	268	185100	0	0	175291	4	39	173046	14320		012988	16	33	161992	34	213
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171991	99	695	185163	2	117	175326	22	157	0979			013064	44	100	162105	130	311
172019	120	754	185181	32	180	175351	48	231	045600	0	0	013078	56	135	162150	168	347
172045	134	883	185192	28	217	175376	74	315	045700	2	0	013137	70	170			
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084820	0	0	185227	48	336	175421	126	474	045715	0	36	013145	124	264	161821	4	46
084850	101	26	185237	52	371	175445	166	551	045730	2	99	013183	156	302	161865	8	80
084860	101	59	185255	114	421	175466	192	627	045734	4	152	013222	182	335	161892	14	114
084871	117	89	185265	124	455	175487	228	709	045739	6	209	013260	210	366	161926	30	146
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084892	115	157	185292	158	538	175517	296	827	045746	8	271	013294	244	402	161992	52	212
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084925	126	257	185333	268	672	175549	344	945	045756	46	432	013370	310	468	162106	154	310
084935	122	291	185342	298	705	175558	372	983	045760	60	480	013399	362	500	162130	178	366
084946	124	324	185353	346	744	175568	390	1024	045763	66	527	013347	390	534	1051		
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085011	176	525	185383	458	839	042911	0	0	045776	112	712	013650	528	634	173518	10	41
085033	207	594	185393	538	872	042930	4	9	045781		736	013685	584	670	173565	38	81
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042833	104	713	161897	855	144639	96	422	035975	10	87	152203	2	0	041743	64	530	
042836	112	752	161930	908	144697	110	473	035984	18	120	152222	8	75	041815	68	565	
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35	251	1467	0373	128	1014	17	218	1765	000000	0	132	000000	0	165
44	311	1849	0418	162	1112	3118			000145	26	270	000000	0	133
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11																			

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1593			000029	42	532	000441	2855	666	000009	144	660	070011	159	1131	000012	23	656
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000007	46	1060	000058	97	1116	000047	23	125	000000	0	161	000004	17	310	000003	7	185
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000007	36	855	000022	2	534	000039	40	168	000009	117	473	3745			000007	35	596
000010	65	1212	000028	20	653	000060	68	212	000011	157	644	000000	0		000008	52	778
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000016	138	2128	000007	2	191	000128	285	337	000007	10	126	000053	26	340	000013	121	1415
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000006	19	645	000036	68	782	000342	3040	551	000031	234	419	000158	100	668	100900		
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000031	10	349	3623			000072	110	212	000160	8	526	000051	19	335	1230	330	288
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000003	4	382	000010	31	398	000000	0	100	000191	112	532	000076	-33	233	SEE NOTES 2,7		
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000016	161	2344	000052	146	1249	000043	253	502	000051	210	328	000236	14	659	1130	160	377
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000007	14	705	000081	224	1775	000000	0	112	000226	225	854	3749			1404	453	333
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000011	53	1340	000098	288	2031	000009	27	168	000335	187	1182	000008	0	197	1600	697	274
000013	63	1687	3625			000015	53	254	3694			000013	0	262	1700	825	239
000015	102	2019	000000	0	158	000028	153	421	000000	0	165	000027	2	394	0003		
000017	131	2310	000011	13	195	000034	236	504	000006	2	197	000027	28	526	SEE NOTES 2,7		
3600			000018	28	333	000041	393	593	000009	17	266	000033	35	656	151600		
000000	0	212	000025	48	459	000047	468	673	000017	31	398	000039	66	783	1615	7	73
000004	2	366	000032	60	591	000053	631	756	000023	55	528	000046	85	920	1630	17	151
000006	19	604	000038	75	714	3655			00003C	87	656	000052	121	1056	1700	48	245
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000011	104	1529	000060	133	1051	000017	68	211	000000	0	171	000007	2	203	1830	219	269
000014	131	1847	000067	146	1307	000025	110	296	000005	8	198	000010	19	264	1900	284	258
000015	161	2082	000077	193	1511	000035	212	419	000009	14	269	000013	26	333	1930	345	249
000017	191	2366	000087	237	1711	000042	327	502	000016	38	397	000018	38	398	2000	402	235
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000007	70	953	000012	28	332	000019	95	337	000048	182	1120	000000	0	180	SEE NOTES 2,7		
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TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS			
1505	35	261	5700	196	611	1615	399	629	3000	89	317	211700	114	174	0248	193	742
1515	44	303	5800	220	600	1630	527	518	3200	107	368	240200	123	174	0255	308	618
1525	53	339	5900	271	371	1645	670	374	3400	126	410	310800	135	174	120301	460	455
1540	80	368	170100	319	350	1700	794	294	3600	149	431	311000	144	174	0314	496	205
1600	115	379	0300	366	330	1735	877	222	3800	178	434	331600	150	174	0329	496	133
1615	144	371	0500	400	333	1802	906	206	4000	212	404	353900	155	174	0359	1063	113
1630	179	371	0700	451	324	0016			4200	235	368	354000	135	0	0011		
1700	236	358	0900	494	322	SEE NOTES 2,7			4330	246	321	360500	134	0	SEE NOTES 2,7		
1750	293	354	1100	535	318	101506	0		4700	267	280	361700	133	0	113857	51	200
1800	354	351	1300	578	314	1855	40	117	4900	275	266	0026			4100	57	200
1900	471	353	0011			4020	48	117	5100	283	252	SEE NOTES 2,7			4500	66	200
2000	576	363	SEE NOTES 2,7			110557	51	117	5800	295	222	112506	0		120000	76	200
2100	716	307	120203			120010	54	117	170207	300	208	2515	8	61	3500	89	200
2200	846	257	0300	14	67	133010	57	117	1100	308	191	2535	37	249	111801	101	200
0006			0400	29	155	143000	59	117	0021			2635	76	324	141700	114	200
SEE NOTES 2,7			0500	47	235	145500	60	117	SEE NOTES 2,7			2653	86	332	152200	130	200
104400			0600	68	316	165553	62	117	151502			2653	86	332	165600	148	200
4500	2	18	0700	94	374	191735	63	117	SEE NOTES 2,7			2653	86	332	190000	166	200
4515	9	40	0800	130	410	205705	65	117	151502			112740	110	335	205700	176	200
4530	16	61	0900	182	408	211023	69	117	1614	13	117	2850	146	336	213900	197	200
4600	23	105	1000	241	386	215025	70	117	1620	20	185	2930	168	336	064500	246	200
4630	32	148	1100	304	359	235730	72	117	1625	25	243	3025	201	337	092200	260	200
4700	41	190	1200	366	332	070037	79	117	1631	29	268	3120	290	335	105800	273	200
4730	50	230	1300	423	317	074745	79	117	1757	40	295	3200	373	337	110000	293	0
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4900	82	338	1500	538	293	111805	82	117	1915	57	390	3315	425	335	135500	251	0
5000	113	405	1600	594	284	112235	83	0	2112	73	460	3350	557	293	0032		
5100	158	427	1700	651	272	113055	80	0	2212	104	507	3405	704	224	SEE NOTES 2,7		
5200	217	428	1800	708	258	115910	84	0	2302	143	741	0027			200357	0	0
5300	250	417	0012			115910	84	0	2450	251	886	SEE NOTES 2,7			200423	22	72
5400	348	376	0017			133022	87	0	2637	359	845	103057			0637	33	133
5600	478	336	141700			SEE NOTES 2,7			2508	472	351	3104	10	122	0533	45	199
5800	605	295	1730	4	6	183700			2918	872	203	3111	20	218	0518	50	199
0007			1800	15	36	3800	9	70	0022			3115	21	308	0652	56	199
SEE NOTES 2,7			1900	38	116	3900	26	155	SEE NOTES 2,7			3120	44	411	1200	65	199
103400			2000	52	204	4000	43	236	111200	0		3126	41	497	2500	75	200
3630	7	37	2100	70	293	4100	60	317	1630	55	235	3129	52	570	211000	94	201
3645	15	90	2200	99	375	4200	81	385	1700	58	235	3133	63	652	220400	110	199
3500	28	152	2300	113	447	4300	105	433	1800	60	235	3137	75	723	2813	115	199
3515	37	211	2400	146	496	4400	136	460	2000	64	235	3142	99	810	232553	129	201
3530	50	282	2500	195	509	4500	168	461	2500	69	235	3147	112	855	0033		
3545	60	366	2600	262	474	4600	205	444	3500	77	235	3151	150	888	SEE NOTES 2,7		
3600	75	410	2700	334	429	4700	241	420	5000	85	235	3155	186	894	143600	0	
3615	87	463	2800	408	387	4800	272	398	121500	94	235	3159	239	893	3620	10	85
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3645	130	551	3000	538	338	5100	412	381	131400	107	235	3207	708	758	3636	26	234
3700	159	571	3100	602	314	5300	484	356	141000	119	235	0028			3655	37	303
3715	196	575	3200	666	293	5600	567	343	151200	141	235	SEE NOTES 2,7			3728	44	301
3730	246	554	0013			5700	662	321	165700	168	235	160500	0		3800	52	301
3745	304	514	SEE NOTES 2,7			0018			183300	173	235	0650	112	174	3842	58	303
3800	357	483	151330			SEE NOTES 2,7			205300	190	235	0735	118	174	3950	66	300
3830	470	404	151552	33	81	163300			240400	209	235	1000	126	174	4422	83	302
3850	541	348	1600	39	81	3314	2	37	024500	224	235	2000	136	174	4800	78	304
0008			4303	40	81	3124	24	104	131000	278	235	5600	151	174	150412	134	302
SEE NOTES 2,7			170019	42	81	3332	36	181	1025	260	0	180400	166	174	2300	171	302
103500			5445	42	81	3143	43	263	2500	257	0	200700	183	174	5236	219	302
3511	4	78	185535	43	81	3355	54	412	190600	255	0	215700	204	174	162546	265	303
3520	14	159	201325	44	81	3405	61	511	163100	255	0	240300	215	174	170418	327	302
3530	24	252	211654	45	81	3414	61	597	0023			265100	228	174	2005	350	302
3541	35	366	222608	46	81	3427	60	724	SEE NOTES 2,7			265700	251	174	2100	375	6
3550	46	457	230105	46	81	3445	115	647	182000	0		385200	285	174	0034		
3600	58	541	241334	48	81	3450	150	889	2015	8	44	391000	288	174	SEE NOTES 2,7		
3612	78	631	045245	48	81	3502	187	889	2030	21	102	391214	238	0	153800	0	
3623	120	699	121736	50	81	3510	239	858	2045	32	160	394400	235	0	4200	41	160
3633	211	704	085542	50	81	3517	329	751	2100	42	222	430800	231	0	4600	46	160
0009			090742	51	81	3526	449	98	2130	61	350	0029			160800	58	150
SEE NOTES 2,7			090842	52	81	3540	720	140	2200	81	480	SEE NOTES 2,7			4000	66	160
110500			091022	41		3555	804	145	2230	105	585	131154			180900	80	160
0600	7	24	0014			0019			2300	136	657	1205	14	73	200300	93	160
0700	13	54	SEE NOTES 2,7			SEE NOTES 2,7			2322	169	689	1213	28	140	223700	107	160
0800	20	84	102903			154115	0		2345	221	692	1220	41	207	233500	151	160
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1000	32	143	3100	36	131	2313	41	235	2430	368	583	1245	75	295	090500	192	160
1100	46	201	3200	53	207	2400	42	235	2500	515	400	1255	80	296	131100	250	160
1300	63	254	3300	70	287	3000	51	235	2527	672	207	1328	96	294	133300	240	0
1500	81	303	3400	88	363	4500	58	235	2547	733	174	1419	114	295	135200	240	0
1700	102	343	3500	109	435	102100	70	235	0024			1524	132	295	165100	239	0
1900	126	376	3600	133	496	4830	76	235	SEE NOTES 2,7			1621	146	295	0035		
2100	156	397	3700	165	530	111845	83	235	131355	0	351	1809	166	295	SEE NOTES 2,7		
2300	191	405	3800	213	540	5800	91	235	131417	0	408	2001	187	296	183102	0	
2500	233	405	3900	277	505	131900	107	235	1432	17	498	2154	207	295	183116	21	103
2700	254	401	4000	348	456	141700	116	235	1452	26	512	2400	228	296	3121	27	151
2900	296																

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS				
0739	44	342	1700	434	2	2023	703	110	1645	99	770	233430	152	240	SEE NOTES 2,7			
140822	71	405	2600	430	2	2024	789	91	1650	125	840	243300	159	240	192100			
0844	80	409	5400	429	2	0046	SEE NOTES 2,7	0	1655	166	472	013748	166	240	2116	3	5	
140907	91	413	0041	SEE NOTES 2,7	0	172400	12	37	1700	227	852	023700	172	240	2200	12	60	
141000	111	407	203700	0	0	2815	12	37	0051	SEE NOTES 2,7	0	024318	143	0	2317	28	151	
1050	129	407	3732	12	35	2827	22	85	092202	0	0	025400	140	0	2523	42	240	
1210	163	405	3830	33	118	2841	36	150	2350	2	3	033400	138	0	2558	46	277	
1330	201	405	3902	45	164	2850	45	188	2406	20	48	104400	136	0	2656	53	350	
1430	234	406	4000	67	239	2900	53	231	2422	36	117	0056	SEE NOTES 2,7	0	2755	63	431	
1520	270	407	4032	80	276	2910	61	271	2432	45	167	143206	3307	3	84	2800	69	489
1620	314	403	4101	96	304	2921	74	317	2452	59	257	3325	31	149	2857	74	526	
1709	359	405	4200	134	345	2931	88	360	2511	75	342	3343	58	320	3353	81	557	
1753	405	403	4253	179	347	2947	106	406	2534	95	432	3430	72	322	3430	87	609	
1824	448	407	4330	233	314	3004	134	438	2600	125	521	3518	79	321	3500	90	653	
1924	538	404	4400	271	289	3016	160	445	2620	148	566	3713	93	320	3600	99	740	
2009	634	403	4500	343	254	3025	186	479	2630	164	590	4010	108	320	3652	108	816	
2031	718	407	4600	409	234	3037	230	414	2647	199	582	4434	123	320	3700	120	862	
2045	795	372	4700	470	224	3047	272	378	2703	243	562	4916	137	320	3900	138	924	
2105	920	291	4800	538	217	3058	316	341	2720	293	489	5925	147	319	3952	173	929	
0037	SEE NOTES 2,7	0	0042	SEE NOTES 2,7	0	3113	368	306	2747	388	434	151230	196	319	4030	262	821	
105435	0	0	185456	17	78	3131	430	271	2808	464	379	2455	233	321	0061	SEE NOTES 2,7	0	
110525	72	240	5506	35	153	3149	486	254	2842	583	308	3646	287	320	134100	0	0	
0801	76	240	5516	49	228	3204	529	241	2908	661	276	5227	365	320	4623	12	10	
1000	79	240	5534	60	302	0047	SEE NOTES 2,7	0	0052	SEE NOTES 2,7	0	160616	445	320	4653	22	106	
1700	86	240	5547	74	385	200300	1	0	141000	0	0	1915	535	320	4709	32	271	
1800	88	240	5554	89	480	201000	1	0	1017	5	16	2800	622	322	4725	40	448	
4100	104	240	5601	106	541	1100	10	28	1038	29	84	3600	729	324	4741	46	626	
5600	110	240	5609	121	584	1200	17	61	1055	45	163	4200	852	323	4756	51	782	
130300	131	240	5615	146	617	1400	34	136	1153	53	161	4455	950	323	4812	60	1088	
141000	147	240	5619	167	628	1500	42	172	1335	59	162	4625	927	0	4828	67	1217	
154406	163	240	5625	203	624	1530	46	190	2742	74	161	5600	927	0	4847	74	1217	
193200	197	240	5632	280	569	1600	50	205	150027	86	161	182000	927	0	4853	74	1218	
221800	213	240	5642	352	480	1700	58	243	165420	105	161	0057	SEE NOTES 2,7	0	4920	81	1204	
2100	227	240	5709	559	318	1730	62	261	202558	126	161	134400	0	0	5145	575	323	
240300	242	240	5732	685	263	1800	62	275	220047	134	161	4410	11	84	5205	664	333	
0510	201	0	5804	917	175	1830	71	292	011208	146	161	4420	24	193	5222	698	283	
380300	194	0	5834	1019	120	1900	75	304	3043	123	2	4434	37	313	5245	726	230	
0038	SEE NOTES 2,7	0	5900	1050	98	2000	84	333	1300	126	2	4454	61	491	0062	SEE NOTES 2,7	0	
101152	11	68	0043	2200	103	381	2100	94	358	3043	123	2	4500	65	507	154700	0	0
1210	14	151	182200	22	137	2300	115	403	2200	103	381	5123	89	639	4400	15	94	
1230	36	247	2210	36	227	2400	126	421	150500	0	0	5132	98	562	4900	29	108	
1253	39	249	2217	57	320	2500	139	432	0518	12	8	5143	107	665	5000	40	279	
101500	48	247	2224	65	320	2600	153	444	0532	27	107	5151	116	743	5100	48	374	
1900	54	247	2248	84	320	2700	169	453	0547	62	259	5200	130	825	5200	58	470	
2900	63	251	2400	84	320	2800	186	457	150609	62	464	5212	146	877	5300	65	575	
112100	82	251	2400	104	322	3030	235	457	0633	77	463	5222	162	920	5400	74	661	
122700	96	245	2900	128	320	3515	342	417	0719	91	463	5227	172	911	5500	82	744	
133400	107	249	3200	150	320	4100	475	362	0813	106	464	5240	187	873	5600	91	817	
153200	125	251	3700	182	320	5009	690	280	0909	121	463	5253	217	808	5700	108	881	
200600	161	249	4100	209	320	0048	SEE NOTES 2,7	0	1105	144	465	5310	267	695	5745	130	891	
243900	186	251	4709	252	320	110159	19	44	1400	194	461	5328	361	494	5806	156	1040	
244100	161	0	4800	257	320	0122	9	44	1620	253	463	5400	265	313	5831	184	996	
011500	158	0	5200	286	320	0130	16	80	1711	285	463	0058	SEE NOTES 2,7	0	5855	260	714	
082400	157	0	5800	330	318	0147	29	159	1814	335	463	151100	0	0	5910	349	538	
0039	SEE NOTES 2,7	0	190400	380	318	0136	21	107	1900	383	464	1200	15	43	5935	494	272	
101400	17	69	0800	418	320	0233	37	159	1948	448	464	1300	34	150	0063	SEE NOTES 2,7	0	
1417	33	290	1400	483	320	0500	45	159	2110	640	463	1400	52	232	165453	0	0	
1443	41	393	1500	449	0	1000	54	159	2134	749	460	1500	70	309	5510	18	105	
1455	50	403	192408	442	0	3310	70	159	2150	867	428	1600	88	378	5520	29	192	
101553	68	403	0044	SEE NOTES 2,7	0	124800	95	159	SEE NOTES 2,7	0	1700	109	440	5530	43	295		
1720	83	401	133600	3611	21	108	141900	118	159	110800	0	1800	132	497	5544	54	421	
2100	104	401	3611	37	209	160019	139	159	0900	2	7	1900	155	533	5555	62	531	
2700	126	401	3618	50	296	196411	180	159	0915	29	144	2000	179	551	5857	88	544	
3700	152	401	3624	66	400	213830	198	159	0925	45	240	2055	183	544	0064	SEE NOTES 2,7	0	
5600	190	403	3630	82	400	220955	205	161	0940	61	401	2100	216	544	092603	0	0	
112800	236	401	3642	82	400	321053	186	2	1000	69	399	2200	259	538	2641	18	394	
5600	276	401	3706	104	400	0049	SEE NOTES 2,7	0	1025	76	401	2300	313	497	2649	30	528	
122400	315	399	3722	118	400	184755	0	0	1139	90	401	2400	374	439	2707	36	659	
131100	398	403	3847	214	399	4812	11	66	1317	103	401	2500	445	383	2718	43	772	
140400	438	403	3914	268	396	4825	31	200	1900	136	399	2600	522	330	2726	49	845	
145200	492	403	3936	322	398	4840	51	345	2500	175	398	2700	507	295	2735	61	931	
151800	522	401	3950	375	399	4853	70	479	3139	224	401	2800	648	269	2768	96	1013	
155900	572	399	4012	472	398	4902	78	478	3430	273	400	0059	SEE NOTES 2,7	0	2752	178	916	
165800	636	401	4020	523	397	4917	88	479	3600	311	402	4000	12	42	0065	SEE NOTES 2,7	0	
174900	700	401	4037	675	384	5015	125	481	3800	383	399	4200	25	117	193000	0	0	
175300	678	0	4140	751	4	5031												

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
0066			4800	109	515	204000	107	239	010017	133	166	270917	157	920	211727	521	246
SEE NOTES 2,7			4900	121	607	214300	111	239	011500	113	3	220924	190	950	211734	621	246
214900	0	0	4930	127	646	233802	118	239	073627	112	3	220931	238	950	211740	724	246
3100	15	82	5000	135	680	014107	128	240	073847	131	164	220937	312	850	211752	937	246
3300	33	178	5100	149	750	025907	138	241	104248	143	163	220942	709	409	211759	1078	246
3500	47	271	5200	174	799	030145	118		142505	156	163	220955	732	487	211807	1261	246
3700	56	373	5230	201	800	031800	117		154347	162	166	0000			0093		
3900	65	480	5300	202	877	080700	117		154843	140	0	SEE NOTES 2,7			SEE NOTES 2,7		
220000	69	535	5320	448	355	0077			0083			223900	0	0	214046	0	0
0200	79	638	5345	552	195	SEE NOTES 2,7			SEE NOTES 2,7			223916	6	25	214100	0	0
0300	83	683	5400	343	157	190705	0	0	185700	0	0	223921	16	100	214117	8	17
0500	96	764	0072			0802	15	46	185900	0	2	223926	30	152	214130	14	101
0600	106	789	SEE NOTES 2,7			0900	41	135	190100	4	34	223930	46	200	214152	28	246
0700	124	806	192400	0	0	1000	61	239	190200	20	107	223935	69	232	214405	35	246
0828	139	805	2407	12	71	1100	75	326	190230	33	162	223939	96	235	215827	47	246
0900	169	766	2418	28	168	1200	92	420	190300	51	232	223945	140	240	220433	54	247
0928	255	612	2427	37	260	1300	106	520	190330	70	289	223951	178	208	221020	71	246
0949	340	642	2437	43	346	1400	122	619	190400	96	321	224000	242	175	223925	88	246
1032	452	248	2446	51	435	1500	141	704	190430	132	329	224008	293	159	224850	96	246
1100	532	201	2455	58	524	1548	170	738	190456	169	312	224020	376	143	231006	120	246
1300	599	189	2464	66	608	1602	190	729	190530	232	291	224035	477	134	232368	143	246
0067			2503	66	608	1620	237	670	190600	278	214	224049	567	127	233445	170	246
SEE NOTES 2,7			2511	70	692	1634	284	588	190630	321	192	224115	746	120	236400	215	246
091810	0	0	2527	82	851	1648	368	436	190700	361	188	224147	938	112	235400	268	247
3024	23	173	2534	85	930	1723	494	255	190730	400	177	224218	1130	110	235900	310	246
3040	40	264	2542	91	1007	1800	561	203	190800	439	172	224248	1326	104	240406	363	246
3050	48	355	2550	96	1070	0078			190830	480	171	224301	1381	103	240945	429	246
3907	61	528	2600	105	1144	SEE NOTES 2,7			190900	514	171	224314	1485	100	0094		
3917	69	637	2609	116	1216	204000	0	0	0084			0089			SEE NOTES 2,7		
3927	77	723	2618	132	1265	204025	40	167	SEE NOTES 2,7			SEE NOTES 2,7			032320	0	0
3934	83	785	2623	166	1279	204046	62	345	194000	0	0	241300	0	0	093330	14	103
3942	90	856	2628	205	595	204105	76	525	194200	26	111	241328	1	0	094500	16	103
3950	101	937	0073			204121	89	694	194330	40	195	241333	14	55	110800	25	103
4000	121	1000	SEE NOTES 2,7			204138	102	849	194400	64	275	241340	29	125	130430	36	103
4007	152	1014	165700	0	0	204154	115	890	194418	68	299	241346	42	212	190300	55	103
0068			5900	26	68	204212	133	1007	194500	101	382	241352	53	295	171400	99	103
SEE NOTES 2,7			170000	49	165	204228	166	1123	194530	128	429	241357	63	375	174300	123	103
151600	0	0	0300	69	263	204235			194600	158	450	241402	71	451	180000	164	103
1625	52	186	0500	88	357	204307			194630	191	472	241407	77	531	182100	184	103
1648	86	390	0700	111	447	0079			194700	232	475	241411	86	631	183900	233	103
1717	93	392	0900	138	529	SEE NOTES 2,7			194730	268	454	241415	92	684	185400	281	103
1828	98	392	1000	153	562	213100	0	0	194817	335	422	241420	101	756	190600	296	103
2013	110	392	1130	171	578	213300	21	84	194900	396	403	241425	110	818	191800	329	103
2043	121	392	1138	190	574	213404	31	319	195000	479	388	241430	127	891	193100	370	103
2115	143	392	1200	205	558	213500	46	411	195330	748	316	241434	144	925	0095		
162009	321	392	1300	255	484	213600	61	503	0085			241437	144	889	SEE NOTES 2,7		
2308	528	390	1400	324	398	214003	74	587	SEE NOTES 2,7			241442	262	614	220830	0	0
2328	572	390	1500	390	337	214200	88	677	205200	0	0	241445	306	531	220945	45	103
2347	622	394	1700	489	268	214501	109	784	205300	14	56	241515	520	361	221000	60	103
2410	691	381	1900	571	234	214705	138	795	205330	38	97	0090			221019	68	103
0069			2509	792	201	214800	274	985	205400	70	105	SEE NOTES 2,7			221034	81	103
SEE NOTES 2,7			0074			214900	391	255	205430	114	105	161220	0	0	221100	101	103
191600	0	0	SEE NOTES 2,7			215011	428	234	205500	154	105	161308	0	1	221115	117	103
1624	29	117	132200	0	0	0080			205530	194	101	161316	3	18	221200	163	103
1637	54	240	2210	23	61	SEE NOTES 2,7			205600	232	95	161321	7	35	221230	199	103
1709	59	241	2221	46	138	152500	0	0	205630	273	89	161340	20	104	221300	241	103
2000	64	240	2233	67	235	152515	17	59	205700	311	86	161405	37	249	221330	287	103
3806	78	241	2335	78	237	152527	37	162	205730	348	82	161600	53	250	221400	337	103
214850	94	284	2633	84	237	152536	48	236	205800	388	81	161619	64	249	221500	392	103
231500	98	239	3900	102	239	152700	55	237	205830	426	80	162520	90	249	221530	452	103
014900	108	240	5200	110	237	153105	61	238	205900	468	77	162902	107	249	221530	519	103
051608	118	240	140600	121	239	155000	73	239	205930	502	75	163158	127	247	221600	586	103
101545	145	241	3000	155	237	162745	92	238	210000	540	73	163358	147	249	221630	666	103
5045	150	241	3830	179	237	164145	108	240	210033	582	73	163649	187	249	221700	734	103
114822	161	241	4500	215	237	165200	135	237	210100	618	73	163834	229	250	221730	807	103
131291	196	240	5035	278	237	165723	154	238	210130	654	71	163953	267	249	221800	880	103
3352	213	241	5300	333	237	170407	192	239	210150	677	71	164042	307	249	0096		
140255	246	241	5500	396	240	181400	287	239	0086			164125	367	247	SEE NOTES 2,7		
2217	296	241	5700	481	237	171830	370	238	214400	0	0	164155	388	249	094515	0	0
5045	395	241	5900	601	238	172200	454	238	214406	11	65	164236	467	249	094645	27	103
150543	455	241	0075			172500	536	237	214410	19	143	0091			095000	58	103
3040	554	241	SEE NOTES 2,7			172800	634	242	214415	28	221	SEE NOTES 2,7			095800	58	103
5046	632	242	162200	0	0	173011	720	238	214420	36	303	201600	0	0	101045	89	103
162030	763	241	2222	39	122	0081			214425	48	386	201611	8	2	102400	127	103
2300	794	241	2250	90	403	SEE NOTES 2,7			214430	63	477	201618	18	169	103445	216	103
0070			2335	102	402	182935	22	161	214435	69	552	201622	35	247	110645	253	103
SEE NOTES 2,7			2500	113	402	182951	36	307	214439	79	613	201737	52	247	111545	280	103
204745	0	0	2700	124	404	183001	43	401	214443	96	692	201845	72	247	113850	360	103
4812	18	71	3000	145	401	183045	50	461	214450	123	733	201926	80	247	114700	378	103
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TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
220153	0	0	5230	3	10	2720	19	16	3933	57	246	3035	154	491	284	132	322
220159	7	14	5310	12	59	2727	30	83	3935	68	246	3055	193	472	2853	377	305
220204	18	74	5332	20	116	2732	41	153	4315	88	246	3116	255	424	2902	430	291
220220	37	173	5400	32	186	2737	52	225	4715	109	246	0121			2910	489	281
220230	54	264	5430	44	266	2743	64	310	5813	150	246	SEE NOTES 2,7			2922	562	271
220241	69	349	5500	58	346	2750	82	392	0A0808	181	246	205945	0	1	2945	705	258
220251	80	423	5530	71	426	2756	101	468	2029	222	246	210004	0	0	3004	819	250
220300	89	528	5630	100	576	2805	134	531	3047	268	246	0017	1	6	3016	891	246
220310	102	613	5600	185	509	2810	161	539	4116	314	246	0032	4	18	0126		
220322	123	698	5700	125	615	2815	186	531	5319	380	246	0044	5	26	SEE NOTES 2,7		
220326	134	720	5720	145	631	2821	239	468	090855	464	246	0056	7	35	153000	0	0
220332	160	741	5735	167	624	2830	304	393	0115			0105	9	41	3106	3	3
220337	191	741	5800	207	560	2838	371	354	SEE NOTES 2,7			0120	12	51	3253	10	62
220343	240	718	5830	264	461	2848	439	321	092400	0		0132	15	60	3650	51	124
220350	314	614	5900	314	394	2868	510	298	2430	10	102	0155	21	77	3716	49	180
220356	384	528	110000	398	322	2909	564	283	2700	14	102	0220	29	93	3735	65	204
220412	516	351	0010	407	314	0110			100900	32	102	0243	31	110	3756	48	223
220428	552	248	0104			SEE NOTES 2,7			122700	50	102	0307	36	128	3814	107	227
220455	575	191	SEE NOTES 2,7			193245	0	0	173200	68	102	0330	40	162	3833	143	226
0099			122903	0	0	3303	2	9	230000	78	102	0353	45	196	3847	146	225
SEE NOTES 2,7			2943	13	53	3310	14	114	114200	104	102	0417	49	231	3854	165	220
222055	0	0	3015	22	137	3315	23	201	144600	108	102	0545	56	265	3920	203	212
222913	6	5	3100	40	252	3320	36	288	171100	113	102	0515	64	299	3967	242	205
223014	42	76	3140	57	320	3325	46	368	1232	55	100	0547	76	333	4014	279	194
223116	67	174	3200	77	383	3330	61	444	3000	91	100	0624	91	367	4047	320	187
223215	78	265	3230	99	428	3336	78	522	230300	92	100	0709	119	400	4115	357	181
223316	1	351	3250	117	460	3341	97	589	080350	92	100	0753	157		4144	376	175
223425	142	441	3301	125	470	3350	133	663	0116			0818	193	414	4242	472	167
223516	180	476	3400	197	477	3358	176	677	SEE NOTES 2,7			0915	292	381	4361	549	164
223529	196	474	3430	240	453	3403	213	684	103200	0		1114	508	294	4511	654	162
223600	251	426	3500	280	428	3409	261	590	3300	16	102	0122			4640	780	162
223635	325	351	3600	363	396	3416	331	484	111600	36	102	SEE NOTES 2,7			4810	895	162
223700	372	312	3635	409	381	3421	373	443	132900	54	102	214547	0	0	0127		
223730	417	280	3700	440	371	3425	409	409	162700	70	102	4610	13		SEE NOTES 2,7		
223800	461	257	3730	480	365	3434	469	371	191500	83	102	4616	19		132450	0	0
223835	510	239	3800	517	357	3441	515	348	224030	104	102	4621	37		2502	0	3
223907	551	232	0105			0111			081043	139	102	4627	62		2520	9	85
223945	596	222	SEE NOTES 2,7			0117			1230	126	0	4635	92		2545	23	248
0100			142745	0	0	200445	0	0	5300	123	100	4640	110		2607	35	248
SEE NOTES 2,7			2800	0	0	0700	0	0	0117			4644	134		2621	50	248
135247	4	0	2820	5	32	0707	10	38	SEE NOTES 2,7			4652	206		3057	69	248
5310	4	20	2900	26	137	0713	20	103	101855	0	0	4700	262		3330	86	249
5322	22	128	2932	45	209	0718	30	181	1918	12	102	4705	47		3922	124	247
5334	40	238	3000	68	270	0723	42	266	2530	31	102	0123			4308	164	247
5415	48	238	3030	95	316	0729	60	348	3400	38	102	SEE NOTES 2,7			4517	203	248
5545	57	239	3100	128	334	0735	72	424	120500	57	102	121147	0	0	4630	219	247
140300	73	240	3130	171	338	0741	96	503	161900	76	102	1218	1	2	4734	280	247
2240	93	240	3203	220	327	0746	115	535	220600	90	102	1345	16	101	4811	309	249
5023	114	239	3218	241	309	0755	180	539	082400	112	102	1520	37	244	4853	350	247
151828	131	240	3230	261	303	0800	224	481	2515	102	0	1630	53	244	4923	383	249
4622	151	239	3300	273	283	0805	272	424	2400	87	0	1740	70	244	4951	420	248
165352	198	238	3330	274	268	0810	313	385	112200	83	0	1900	95	244	5019	458	248
181704	248	239	3401	274	258	0818	372	308	0118			2025	127	244	5106	533	248
191211	305	240	3500	470	243	0112			SEE NOTES 2,7			2320	208	244	5250	609	249
5044	329	240	3532	530	237	SEE NOTES 2,7			151400	0	0	2525	206	244	0128		
205133	376	239	3600	542	234	205357	0	0	1458	0	0	2650	356	244	SEE NOTES 2,7		
215045	420	238	3615	589	229	5402	0	0	1505	7	42	2733	396	244	181600	0	0
222122	439	238	3700	644	218	5410	6	51	1519	169	15	2803	425	244	1816	1	8
0101			3713	666	218	5417	17	109	0119			2940	540	244	1840	31	82
SEE NOTES 2,7			0107			5423	29	246	SEE NOTES 2,7			3035	608	245	1705	58	177
091718	0	0	SEE NOTES 2,7			5451	44	247	162952	0		3100	644	245	1732	86	285
1727	5	19	155046	0	0	5535	57	247	2958	0	0	3150	712	244	1750	100	358
1802	61	310	5100	0	0	5634	67	247	3004	6	14	3240	782	245	1812	121	447
1844	95	398	5118	2	23	210046	87	247	3008	11	28	3340	874	244	1835	165	535
1916	118	398	5200	18	120	0415	108	247	3013	18	42	3445	973	244	1900	188	587
1930	127	399	5230	31	199	0945	128	246	3017	22	57	3600	1085	244	1909	219	587
1951	145	398	5300	45	285	1530	146	247	3020	26	70	3730	1166	125	1915	245	574
2017	164	396	5400	77	428	2030	165	247	3025	28	84	4605	1228	0	1925	286	533
2035	181	396	5430	99	487	3200	202	247	3028	31	98	0124			1935	358	446
2050	198	398	5518	152	514	4616	238	247	3031	33	112	SEE NOTES 2,7			1947	431	357
2121	243	395	5534	173	514	5900	280	247	3037	38	142	141900	0	0	2000	508	266
2143	288	395	5600	213	464	220400	313	247	3042	42	186	2100	56	68	2015	598	177
2200	332	397	5700	304	375	1700	350	247	3050	48	249	2205	73	144	2035	681	137
2211	377	401	5731	348	348	2750	394	247	3055	54	279	2300	83	245	2052	736	121
2223	434	387	5801	385	334	3545	425	246	3103	61	322	3300	95	245	0129		
2231	502	370	5830	422	327	0113			3113	81	376	163600	120	245	SEE NOTES 2,7		
2235	561	313	5900	458	319	SEE NOTES 2,7			0120			220915	152	245	184200	0	0
0102			0108			233443	0	0	SEE NOTES 2,7			083740	198	245	4212	11	0
SEE NOTES 2,7			SEE NOTES 2,7			3500	0	3	192148	0	0	101800	207	245	4307	4	0
103200	0	0	165548	0	0	3513	11	82	2200	0	0	140200	227	245	4315	41	16
3222	19	240	5600	0	0	3528	31	245	2204	1	2	204800	268	246	4335	114	323
3500	75	240	5612	18	158	3628	46	245	2214	1	5	4830	255	0	4365	148	460
4100	91	241	5624	37	372	3815	57	245	2218	2							

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS			
5220	45	427	5209	53	160	4904	260	102	151600	140	102	5200	3	25	5137	356	
5225	100	513	5238	58	189	4955	276	102	165100	159	102	5205	13	92	0170		
5230	120	574	5255	69	232	110700	288	102	180037	176	102	5208	20	138	SEE NOTES 2,7		
5245	193	618	5315	81	271	5630	313	102	205400	214	102	5212	30	193	132000	0	0
5251	243	568	5330	92	298	130000	320	102	220000	228	102	5215	43	235	2030	47	248
5300	313	647	5340	141	348	140700	327	102	241557	258	102	5219	58	262	2500	83	248
5310	385	627	5350	183	364	150800	338	102	081600	380	102	5222	79	274	2800	107	242
5321	468	592	5365	254	291	171900	346	102	3502	386	102	5227	108	278	3115	153	248
5340	586	597	5375	310	261	185000	356	102	4900	380		5238	194	249	3300	203	249
5352	660	597	5382	350	249	200700	365	102	092200	380		5249	267	225	3452	261	248
5406	737	596	5390	406	233	211100	370	102	2342	380		5301	362	209	3509	379	261
0131			5406	466	231	2734	367	0	0157			5312	412	200	3532	466	248
SEE NOTES 2,7			5490	504	224	3000	332	0	SEE NOTES 2,7			5325	498	189	3552	515	249
100530	0	0	0136			4000	330	0	144350	0	0	5337	575	188	3604	572	233
0601	0	0	SEE NOTES 2,7			075700	323	0	4402	1	0	5356	691	177	3615	670	242
0615	23	84	185452	0	0	083400	322	0	4406	10	55	5408	765	178	3633	710	251
0626	39	183	5503	0	7	0149			4410	23	122	5421	864	172	3648	813	246
0635	51	273	5642	17	75	SEE NOTES 2,7			4415	33	171	5438	959	169	3702	918	240
0645	64	365	5719	36	160	190850	0	0	4420	44	242	5504	1114	166	3730	1154	243
0655	78	452	5745	51	230	0900	0	0	4425	58	319	0162			3746	1304	244
0705	92	539	5817	71	301	0905	6	25	4429	72	392	194950	0	0	3800	1436	242
0715	116	626	5900	103	374	0910	16	58	4432	78	434	5202	10	8	3811	1504	249
0730	168	680	5916	120	388	0915	25	97	4435	87	485	5208	33	25	3822	1584	242
0734	195	676	190000	180	374	0925	41	174	4439	100	539	5212	40	73	3848	1691	242
0740	238	653	10	195	361	0929	48	210	4441	110	588	5215	44	121	0171		
0743	278	606	50	263	305	0938	68	283	4446	130	608	5219	56	185	SEE NOTES 2,7		
0747	327	535	0114	303	277	0943	79	319	4449	160	589	5223	70	229	145745	0	0
0751	407	598	0215	383	243	0948	93	350	4451	208	479	5229	93	266	5759	35	242
0754	516	214	0315	463	238	0954	110	387	4456	264	359	5232	156	266	5815	46	242
0802	592	127	0419	543	230	1007	159	429	4500	305	300	5242	183	262	5837	62	242
0806	678	100	0453	588	229	1013	189	429	4507	367	188	5251	243	229	5925	84	250
0814	683	92	0535	643	222	1017	218	418	4514	424	138	5302	310	207	150005	119	248
0132			0137			1022	264	372	0158			5319	407	192	0182	142	242
SEE NOTES 2,7			SEE NOTES 2,7			1031	358	283	SEE NOTES 2,7			5333	500	185	0203	181	246
120539	0	0	125121	0	0	1034	431	229	0401	0	0	5347	590	175	0243	223	241
0608	0	15	5200	3	7	0150			0404	10	42	5402	681	164	0313	258	232
0615	12	96	5213	22	102	SEE NOTES 2,7			0410	15	100	0166			0335	301	244
0621	27	185	5221	30	166	194751	0	0	0414	23	166	SEE NOTES 2,7			0403	377	249
0627	40	265	5229	35	251	4800	0	1	0418	32	240	160145	0	0	0421	453	244
0631	52	346	5249	42	244	4815	31	93	0421	35	244	0203	0	2	0172		
0636	64	427	5350	54	247	4823	44	158	0425	47	341	0207	5	59	SEE NOTES 2,7		
0641	79	510	5603	73	242	4834	64	241	0429	57	393	0215	18	177	155845	0	0
0646	88	574	5750	88	246	4904	87	241	0432	67	439	0222	33	297	5905	46	240
0651	105	653	5910	108	246	4940	106	243	0435	77	481	0230	47	456	5931	71	240
0658	131	725	130100	143	243	5020	124	243	0440	85	535	0240	63	647	5953	88	240
0705	161	754	0600	183	243	5058	143	243	0446	107	587	0248	77	795	160015	102	240
0709	189	755	0930	223	245	5136	160	241	0450	126	612	0257	92	939	0040	116	240
0713	229	702	1530	291	243	5256	215	217	0454	151	612	0309	110	1155	0175	159	240
0720	304	570	1900	361	244	5312	249	243	0457	183	573	0167			0224	172	240
0725	372	460	1700	431	249	5352	294	224	0503	265	439	SEE NOTES 2,7			0353	209	243
0735	464	364	1900	527	244	5510	362	243	0512	360	316	190518			0459	253	243
0746	545	320	2100	652	245	5642	420	243	0520	419	250	0530	0	0	0600	297	250
0802	657	288	2135	635	5715	482	243	0526	462	231	0534	7	44	0542	330	244	
0133			0138			5733	552	240	0159			0548	37	245	0548	370	245
SEE NOTES 2,7			0139			5755	613	239	131945	0	0	0558	96	398	0607	75	550
135413	0	0	092445	0	0	0151			2000	0	0	0615	84	663	0615	84	663
140020	0	6	2900	0	16	SEE NOTES 2,7			2005	9	48	0621	100	778	0632	120	923
46	38	16	2910	7	67	210249	0	0	2009	18	105	0642	144	1067	0654	193	1183
47	43	62	2518	14	134	0300	1	13	2014	30	177	0658	222	1136	0700	246	926
52	51	134	2525	18	245	0307	15	91	2018	40	227	0700	246	926	0160		
56	58	207	2848	30	244	0313	35	194	2022	49	278	0700	246	926	SEE NOTES 2,7		
0100	65	270	105200	57	246	0319	57	270	2025	58	330	0700	246	926	162545	0	0
0106	78	365	162900	97	241	0328	94	350	2029	68	383	0700	246	926	2600	0	0
0111	87	442	205859	122	243	0333	117	588	2032	79	429	0700	246	926	2639	21	111
0116	100	523	235800	134	242	0338	150	375	2037	96	483	0700	246	926	2705	43	254
0120	112	595	074034	170	241	0344	191	372	2042	114	525	0700	246	926	175200	82	242
0126	128	675	102800	187	244	0355	280	311	2047	138	561	182000	97	234	20200	140	249
0132	143	748	3030	173	0411	388	270	2051	166	599	204500	184	249	205900	214	242	
0139	166	818	4100	173	0425	484	249	2100	219	566	209900	250	246	211300	250	246	
0147	196	880	113500	172	0442	594	240	2106	285	483	212400	292	249	212400	292	249	
0153	227	896	0139			0500	711	231	2115	377	352	213000	329	249	213000	329	249
0157	261	884	SEE NOTES 2,7			0518	824	223	2125	467	252	214000	301	214000	301		
0203	319	803	183945	0		0540	977	216	2146	620	178	223000	301	223000	301		
0211	415	618	4003	0	1	0152			0160			0149			SEE NOTES 2,7		
0226	585	366	4022	2	11	SEE NOTES 2,7			133620	0	0	0149			175600	0	0
0238	680	299	4040	7	23	231232	0	0	3633	15	0	0149			5708	58	232
0252	766	281	4055	11	33	1241	9	66	3639	49	3	0149			5714	92	251
0134			4124	19	52	1251	23	155	3643	57	61	0149			5719	127	255
SEE NOTES 2,7			4150	23	71	1305	28	155	3647	66	114	0149					

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS			
0420	98	252	0700	131	102	2945	99	303	154940	395	160	23110	116	571	094719	62	163
0423	115	252	1000	150	102	2948	124	290	154957	519	140	23122	135	671	094723	72	163
0427	117	248	1300	169	102	2953	185	228	0203			121132	185	743	094727	121	152
0432	173	252	1530	189	102	3004	274	155	SEE NOTES 2,7			0208			094730	208	163
0437	213	256	1710	208	102	3040	498	90	170916	0	0	SEE NOTES 2,7			094733	285	174
0441	249	256	2030	247	102	0197			170920	7	39	013711	0	0	094803	159	127
0445	287	256	2300	288	102	SEE NOTES 2,7			170925	20	80	013705	0	60	094816	440	119
0451	361	232	2515	323	102	203939	0	0	170928	31	121	013711	11	127	094827	517	111
0457	401	248	2730	363	102	3954	0	153	170932	41	164	013718	29	206	094838	593	107
0500	445	264	2930	401	102	3959	27	211	170935	47	204	013721	38	253	094851	673	103
0504	490	281	3131	438	102	4007	31	249	170940	59	252	013726	48	130	094857	719	101
0508	538	252	3330	478	102	4006	36	296	170944	70	324	013730	57	400	094909	745	98
0512	482		3500	518	102	4010	40	355	170949	84	416	013735	68	486	094920	841	95
0187			3730	594	102	4013	45	409	170954	96	485	013740	80	567	094926	900	95
SEE NOTES 2,7			3930	669	102	4016	47	448	170959	107	599	013738	91	633	094938	938	95
133340	0	0	3950	492		4020	53	515	171004	118	637	013751	137	746	094951	1053	93
3400	70	102	4710	627		4023	57	521	171012	135	741	013756	120	819	095006	1093	93
3442	47	102	0189			4026	60	605	171020	164	849	013802	134	887	095009	1170	91
3506	66	102	SEE NOTES 2,7			4030	66	656	171024	180	866	013810	161	966	0214		
3525	85	102	212800	0	0	4037	579	741	171028	218	818	013818	198	1013	SEE NOTES 2,7		
3545	108	102	2805	13	16	0198			171032	257	0	013822	225	1000	102248	0	0
3600	124	102	2809	29	36	SEE NOTES 2,7			0204			SEE NOTES 2,7			102300	0	0
3618	143	102	2814	44	58	225045	0	0	SEE NOTES 2,7			SEE NOTES 2,7			102340	0	0
3645	181	102	2818	51	67	5052	11	41	184137	0	0	101145	0	0	102365	2	11
3708	219	102	2910	51	68	5057	26	90	184137	12	44	101202	0	0	102400	9	54
3735	42	102	4010	55	68	5104	49	169	184142	30	90	101207	9	20	102417	14	95
3755	297	102	0190			5111	67	250	184148	64	127	101212	20	57	102439	33	131
3815	335	102	SEE NOTES 2,7			5117	82	329	184158	80	160	101224	38	154	102506	107	146
3837	378	102	021700	0	0	5121	94	395	184209	188	168	101233	52	245	102565	130	144
3853	412	102	1715	15	20	5125	104	451	184228	320	155	101244	68	334	102624	188	127
3910	450	102	1732	32	40	5130	121	457	184243	424	147	101254	81	423	102702	204	115
3950	543	102	2000	32	40	5135	141	566	184257	520	138	101303	94	512	102756	283	103
4030	637	102	2500	35	40	5140	167	598	184313	620	132	101313	109	598	102785	342	90
4105	739	102	3000	36	40	5143	193	566	184317	648	131	101324	126	683	102845	437	45
4135	835	102	4100	37	40	5146	230	491	184327	720	130	101334	144	729	103100	502	78
4235	1031	102	0191			5157	319	586	184341	824	124	101344	158	738	103207	673	78
4315	1075	102	SEE NOTES 2,7			0199			184358	920	122	101357	180	723	103315	768	73
0183			034830	0	0	SEE NOTES 2,7			0205			0210			103423	861	72
SEE NOTES 2,7			4843	20	20	224700			SEE NOTES 2,7			0215			0215		
150745	0	0	0192			4705	0	0	213830	0	0	120200	0	0	SEE NOTES 2,7		
0805	32	102	SEE NOTES 2,7			4710	16	41	213901	23	102	120220	9	60	105638	8	0
0840	48	102	111233	0	0	4716	39	81	214108	37	102	120217	29	142	105704	24	61
0930	86	102	3300	27	29	4723	70	137	214400	50	102	120223	45	215	105734	53	97
1030	111	102	3500	30	29	4728	100	146	214500	54	102	120227	56	266	105806	95	114
1145	141	102	4400	33	29	4733	140	147	215102	49	102	120232	67	338	105812	103	118
1235	160	102	120300	35	29	4742	201	132	220000	87	102	120237	77	417	105850	154	118
1342	183	102	2300	36	29	4752	264	121	221102	104	102	120242	85	500	105855	180	118
1515	220	102	4500	37	29	4800	316	112	222102	118	102	120246	96	567	105938	224	111
1635	260	102	131500	38	29	4812	396	103	224201	142	102	120251	103	639	110000	300	97
1915	350	102	141200	39	29	4825	482	94	232400	187	102	120255	113	717	110030	372	
2130	430	102	150000	40	29	4836	558	86	235303	214	102	120301	124	788	110304	520	73
2247	487	102	165400	42	29	4854	674	78	244800	249	102	120307	146	860	110400	587	70
2430	547	102	165400	43	29	0200			251752	302	102	120314	170	901	110444	654	63
2535	626	102	190600	47	29	SEE NOTES 2,7			260553	356	102	120317	193	896	0216		
2554	477		220900	51	30	132200	0	0	264453	404	102	120322	247	846	SEE NOTES 2,7		
2633	550		020000	56	29	132204	4	47	275145	488	102	120326	309	818	035145	0	0
0184			060300	60	29	132207	11	96	279900	492	102	120330	445	275	035201	0	0
SEE NOTES 2,7			110000	72	29	132211	19	138	280000	473	102	0211			035215	37	26
163602	0	0	170800	84	29	132214	29	188	SEE NOTES 2,7			SEE NOTES 2,7			035239	50	65
3904	51	102	220000	106	29	132218	37	232	SEE NOTES 2,7			041003	0	0	035304	75	103
4235	63	102	000600	114	29	132223	53	292	092100	0	0	041008	0	61	035337	120	109
5125	96	102	073800	135	29	132228	71	350	092245	156	102	041012	0	103	035405	157	101
171800	121	102	084500	151	29	132233	92	390	092310	174	102	041017	4	152	035437	195	90
3500	123	102	090000	155	29	132239	124	410	092400	204	102	041022	43	198	035542	271	85
5200	145	102	091500	163	29	132245	165	406	092416	219	102	041028	57	228	035613	310	85
184505	180	102	093500	175	29	132250	211	350	092432	238	102	041031	78	231	035715	389	82
200400	225	102	0193			132259	289	260	092500	273	102	041035	125	228	035812	467	78
221600	295	102	SEE NOTES 2,7			132312	380	202	092534	320	102	041040	164	228	035914	593	77
2200	294	0	100310	0	0	132329	491	188	092545	335	102	041045	190	216	040020	670	77
3045	272		0333	24	33	132345	600	145	092600	358	102	041050	211	200	040125	701	77
3300	261		0413	31	33	0201			092630	408	102	041056	257	177	040227	772	77
0187			SEE NOTES 2,7			115100			092700	461	102	041107	346	125	040330	848	77
SEE NOTES 2,7			102140	0	0	115107	0	0	092730	523	102	041118	427	101	0217		
135604			2150	23	23	115112	24	31	092804	623	102	0212			SEE NOTES 2,7		
5725			2200	37	46	115117	51	58	092915	719	102	SEE NOTES 2,7			070945	0	0
5746	0	102	2600	41	46	115123	80	88	093054	815	102	071540	0	0	071000	1	9
5820	8	102	4000	44	46	115127	104	104	093302	915	102	071601	0	0	071009	7	24
140100	25	102	5900	47	46	115131	125	112	093445	1004	102	071605	4	32	071016	9	53
142700	44	102	9600	47	46	115134	148	116	093429	1104	102	071609	4	82	071029	15	97
143500	65	102	112700	50	44	115140	188	114	093507	1198	102	071613	33	135	071055	29	98
150700	96	102	5600	53	44	115147	236	114									

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
180657	83		092957	83	446	106945	0	0	0236		040012	167	325	101240	0	0	
200804	833		093003	103	477	105006	0	0	SEE NOTES 2,7		040043	191	331	101304	0	0	
210906	96		0223			105020	4	23	031440	0	0	040096	215	325	101331	11	47
260236	115		SEE NOTES 2,7			105117	42	71	031501	0	0	040131	290	245	101336	22	95
361730	134		115745	0	0	105146	79	79	031509	0	0	040197	323	221	101338	34	135
440804	152		115802	0	0	105210	110	79	031513	11	55	040390	419	198	101323	59	158
481213	160		115805	4	8	105257	171	71	031518	22	103	040400	504	162	101332	119	158
530557	169		115809	11	32	105326	211	71	031521	38	143	040430	548	178	101340	179	151
560622	172		115814	17	64	105408	268	63	031527	52	182	040530	624	175	101348	239	135
560846	172		115818	28	94	105453	332	63	031534	95	203	040630	704	166	101357	300	127
0218			115823	35	154	105514	391	55	031540	130	238	040659	748	159	101406	360	119
SEE NOTES 2,7			115827	42	172	105619	452	55	031548	176	265	0242			101412	400	119
001000	0	20	115832	51	217	105706	472	55	031613	333	285	SEE NOTES 2,7			101421	456	111
160410	77		115839	64	261	105806	592	55	031630	443	293	061045	0	0	101430	520	111
200805	92		115844	75	306	105938	712	55	031656	546	285	061059	2	3	101444	527	106
210900	95		115850	88	350	0231			031715	709	262	061120	11	30	101447	641	102
221035	102		115858	108	395	SEE NOTES 2,7			031721	780	253	061152	23	80	101458	721	102
231106	103		115902	124	425	030160	0	1	0237			061215	32	117	0247		
241205	107		115905	147	397	030201	1	1	SEE NOTES 2,7			061235	39	150	SEE NOTES 2,7		
251316	110		0224			030210	2	7	030949	00	0	061252	45	177	113440	0	0
251345	111		SEE NOTES 2,7			030238	30	41	031002	00	8	061315	52	212	113500	0	0
261436			115101	0	0	030332	95	70	031006	11	47	061338	61	247	113517	4	8
281610	119		115105	9	32	030408	142	73	031009	19	87	061406	71	205	113537	11	39
281645	120		115110	17	89	030451	201	76	031014	45	103	061444	89	337	113542	19	55
301810	123		115114	23	148	030551	283	77	031017	80	55	061520	113	370	113610	42	103
311906	125		115119	39	203	030700	370	78	031021	119	15	061537	129	368	113617	50	127
322041	130		115123	40	260	030800	456	80	031026	152	8	061548	149	352	113643	67	154
342230	134		115127	59	305	030900	539	77	031033	213	0	061559	180	320	113653	74	198
352330	136		115130	70	351	031000	627	77	031045	291		061619	229	261	113733	110	261
440804	154		115136	92	400	031100	691	83	031057	369		061644	283	212	113802	143	285
450935	158		115139	114	409	031210	803	82	031111	437		061714	331	186	113827	179	285
471110	160		115147	170	411	031310	882	85	031122	567		061749	377	171	113909	240	269
481214	161		115150	210	345	031410	963	87	0238			061826	421	164	113937	280	253
501412	165		115157	278	284	031509	1042	88	SEE NOTES 2,7			0243			114005	320	245
511512	432		0225			031611	1121	89	102749	0	0	SEE NOTES 2,7			114049	380	238
521657	168		SEE NOTES 2,7			031710	1199	92	102800	2	0	035901	0	20	114149	460	229
541815	170		014840	0	0	0232			102824	4	8	035903	1		0248		
562046	173		014901	0	0	SEE NOTES 2,7			102841	9	48	041500	1		SEE NOTES 2,7		
572115	173		014908	4	8	043301	0	0	102857	20	82	050235	8		031640	0	0
0219			014913	14	55	043352	23	23	102916	31	124	070200	11		031701	0	0
SEE NOTES 2,7			014917	22	103	043441	79	19	102934	65	163	090200	16		031713	0	0
100245	0	0	014920	33	151	043528	143	47	102956	61	205	090200	16		031804	8	39
100304	0	8	014925	48	206	043551	183	47	103021	84	240	120200	19		031821	11	79
100308	0	55	014929	59	261	043643	243	47	103038	104	255	020214	20		031838	30	118
100313	19	103	014933	70	316	043744	323	39	103107	140	256	080020	23		031858	48	158
100317	30	159	014937	84	381	043847	403	39	103138	181	231	120324	28		031915	59	196
100374	53	237	014941	96	432	044017	483	39	103212	240	191	040328	29		031934	74	238
100331	76	315	014949	132	492	044111	605	39	103251	301	158	071031	30		031957	95	277
100337	95	395	014954	166	492	044211	685	39	103351	381	154	102934	31		032017	111	301
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100348	130	552	015001	259	293	044412	840	39	103600	554	145	081544	37		032118	192	309
100356	160	620	0226			0233			0239			020450	40		032158	291	292
100401	180	650	SEE NOTES 2,7			SEE NOTES 2,7			SEE NOTES 2,7			080056	41		032227	592	285
100405	210	641	112045	0	0	095240	0	0	113347	0	0	103558	41		0249		
100409	263	544	112103	0	0	095302	1	3	113400	7	0	081268	42		SEE NOTES 2,7		
100414	345	555	112111	4	15	095306	8	34	113424	15	40	120472	42		105141	0	0
100420	453	198	112116	8	30	095312	16	74	113434	30	71	045076	43		105205	0	0
0220			112132	16	79	095317	23	114	113454	42	111	103282	49		105226	4	8
SEE NOTES 2,7			112148	27	119	095321	29	153	113515	59	158	035887	49		105243	11	39
091750	0	0	112204	30	158	095325	33	192	113534	73	198	101294	51		105312	41	79
091802	1	0	112223	41	198	095331	39	244	113558	94	237	0244			105413	115	111
091810	17	35	112237	52	213	095336	47	294	113635	135	269	SEE NOTES 2,7			105449	171	111
091815	37	78	112318	95	245	095340	48	293	113710	183	261	033641	0	0	105529	231	111
091819	50	110	112323	103	230	095419	50	285	113752	247	237	033701	4	0	105613	291	103
091825	68	165	112350	152	158	095620	59	279	113720	283	229	033705	8	48	105655	352	103
091831	93	239	112427	200	119	095638	67	351	113785	344	213	033709	22	79	105738	411	95
091839	102	320	112457	249	103	095639	71	422	114003	429	198	033714	41	119	105829	480	95
091847	160	397	112547	307	87	095646	81	509	114031	460	198	033718	62	151	105920	552	95
091901	225	473	112636	364	87	095652	90	547	114102	504	190	033724	95	166	110003	612	87
091908	259	494	112705	408	84	095700	112	587	114132	544	183	033730	171	166	110047	672	87
091913	284	489	0228			095703	173	551	114203	555	174	033735	183	143	110134	737	87
091938	394	489	SEE NOTES 2,7			0234			114221	604	174	033740	219	135	110216	798	87
091925	446	427	025341	0	0	SEE NOTES 2,7			0240			033749	263	127	0250		
091944	537	402	025401	0	0	110543	0	0	SEE NOTES 2,7			033750	340	127	SEE NOTES 2,7		
0221			025434	3	6	110602	0	0	021247	0	0	033804	384	119	095501	0	0
SEE NOTES 2,7			025438	13	47	110613	4	20	021300	0	0	033810	473	119	095505	3	9
111349	0	0	025442	29	84	110618	16	78	021331	4	8	033816	486	119	095516	27	78
111404	2	11	025446	41	134	110623	28	139	021355	34	40	033822	500	111	095521	36	117
111409	18	56	025451	60	165	110627	38	193	021449	87	71	033831	560	111	095527	48	176
111414	49	89	025458	95	197	110630	45	234	021536	149	71	033839	620	103	095532	56	209
111421	77	132	025506														

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS			
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0252			102820	4	17	0264			112209	27	93	100618	172	073136	42	233	
SEE NOTES 2,7			102915	14	53	SEE NOTES 2,7			112212	38	145	100627	166	073139	52	311	
015223	0	0	103015	31	95	032959	0	0	112215	48	194	100633	167	073143	58	368	
015239	7	9	103130	36	147	033003	16	50	112220	59	278	0277		073148	63	412	
015321	16	39	103255	79	208	033007	29	100	112225	71	368	SEE NOTES 2,7		073153	68	458	
015345	21	59	103408	91	251	034010	41	154	112230	83	459	193100	0	0	073158	72	502
15423	27	88	103518	110	316	033014	52	212	112235	95	547	193200	1	1	073203	77	545
015512	39	126	103637	137	361	033017	61	265	112239	106	632	193240	11	28	073207	81	586
015603	49	165	103652	148	333	033020	70	319	112242	116	683	193345	29	65	073212	85	628
015654	61	202	103728	177	307	033024	80	393	112245	128	722	193436	41	100	073217	91	673
015748	73	237	103810	213	278	033027	87	454	0271			193533	52	144	073222	97	712
015852	89	273	103920	271	243	033030	100	495	SEE NOTES 2,7			193609	60	175	073226	103	750
015945	101	288	104020	311	225	033032			200550	0	0	193700	69	217	073230	107	790
020010	113	283	104130	358	211	033118			200615	4	19	193734	74	249	0282		
020033	123	273	104245	405	208	0265			200641	9	38	193817	80	282	SEE NOTES 2,7		
020050	134	264	104400	452	200	SEE NOTES 2,7			200730	18	77	193900	89	318	043751	0	0
020107	143	253	104520	502	198	010804	0	0	200835	31	144	193943	92	353	043801	1	0
020143	211	235	104625	538	196	010846	8	26	200922	40	173	194025	103	389	043866	13	56
020222	241	220	0259			010940	20	69	201000	48	203	194112	112	425	043910	26	144
020322	272	201	SEE NOTES 2,7			011030	29	111	201048	63	229	194201	125	461	043915	39	230
020440	341	183	111559	0	0	011100	34	135	201110	79	228	194318	150	494	043920	49	319
020604	393	167	111500	0	54	011200	45	189	201130	95	215	194355	173	496	043925	57	408
020728	348	157	111600	15	103	011300	57	234	201210	103	200	194407	179	488	043929	66	497
0253			111700	23	167	011400	69	280	201400	205	165	194451	240	479	043933	73	583
SEE NOTE 2,7			111800	32	208	011430	74	297	201700	310	151	194605	351	264	043938	79	649
071200	0	0	111900	43	266	011530	89	338	202000	410	151	194900	492	205	043940	86	715
071205	5	19	112000	62	295	011645	115	369	0272			0278			043944	92	774
071210	7	17	112014	73	293	011710	127	371	SEE NOTES 2,7			SEE NOTES 2,7			0283		
071218	21	119	112030	96	353	011730	140	367	027744	0	0	212132	0	0	SEE NOTES 2,7		
071219	28	177	112053	193	109	011820	169	323	022800	0	0	212138	12	38	141005	0	0
071229	34	229	112115	234	36	011916	247	242	022810	18	63	212144	23	87	141031	5	17
071234	40	263	112200	277	10	012011	303	217	022818	37	102	212148	32	116	141105	12	45
071240	49	319	112300	338	2	012112	349	196	022824	52	157	212155	46	180	141250	31	119
071243	53	351	0260			012300	381	177	022832	61	207	212200	51	208	141300	46	139
071244	59	377	SEE NOTES 2,7			012500	391	174	022842	169	116	212203	56	232	141500	52	228
071250	64	407	103506	0	0	0264			022850	187	195	212207	61	264	141600	63	271
071255	73	443	103513	13	20	SEE NOTES 2,7			022900	217	223	212210	66	298	141700	72	314
071302	81	490	103519	24	86	105145	0	0	022903	367	193	212215	70	336	141710	87	358
071305	105	499	103525	33	137	105200	1	1	0273			212218	74	371	141844	120	395
071309	130	493	103528	39	179	105205	11	33	SEE NOTES 2,7			212224	78	429	141910	136	393
0254			103532	42	215	105211	21	74	213955	0	0	212227	82	468	141950	182	289
SEE NOTES 2,7			103536	48	250	105218	32	135	214000	12	53	212230	85	502	142016	212	279
180003	0	0	103540	51	286	105225	42	193	214003	20	113	212235	90	549	142147	250	237
180007	16	63	103544	55	327	105230	50	242	214006	25	173	212240	95	600	142243	301	216
180010	28	121	103548	58	352	105236	57	297	214009	30	227	212244	97	633	142320	318	206
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180021	55	294	103602	72	492	105249	75	487	214019	46	421	212300	113	780	0284		
180025	63	312	103607	75	536	105253	80	472	214022	49	485	212310	123	875	SEE NOTES 2,7		
0255			103611	79	570	105256	86	468	214025	55	548	212318	135	956	075357	0	0
SEE NOTES 2,7			103614	82	602	0267			214028	57	603	212329	153	1039	075402	9	31
092355	0	0	103618	89	637	SEE NOTES 2,7			214031	61	658	212340	170	1120	075410	23	83
092352	4	10	103622	92	671	092840	0	0	0274			212350	180	1200	075416	35	132
092600	14	34	103626	98	702	092900	0	0	SEE NOTES 2,7			212407	193	1333	075422	42	182
092631	18	58	0261			092905	7	47	141202	0	0	0279			075426	50	226
092700	21	82	SEE NOTES 2,7			092909	20	115	141230	1	5	SEE NOTES 2,7			075431	53	280
092800	37	126	025758	0	0	092913	39	193	141242	17	43	233406	0	0	075436	60	315
092900	55	189	025802	14	46	092918	42	280	141400	31	96	233410	9	59	075441	64	361
093000	70	209	025806	27	100	092921	65	303	141510	41	149	233415	17	139	075445	69	402
093100	90	225	025809	36	156	092927	83	400	141600	51	188	233418	25	200	075450	74	451
093130	108	225	025812	45	208	0268			141700	62	235	233421	31	259	075454	79	495
093200	125	222	025815	48	256	SEE NOTES 2,7			141800	71	274	233425	37	313	075459	83	537
093300	143	215	025818	59	307	091302	0	0	141913	82	323	233428	44	365	075503	87	581
093430	231	185	025821	66	366	091400	7	7	142022	94	368	233431	49	416	075509	91	623
093530	281	163	025824	73	418	091514	30	43	142234	108	413	233434	53	467	075513	97	666
093800	382	145	025827	81	476	091640	50	107	142347	155	449	233437	62	530	075517	101	705
094100	148		025830	90	532	091727	60	132	142428	188	407	233440	67	591	075521	105	743
0256			025833	99	578	091840	78	195	142510	238	329	233444	75	658	075525	110	783
SEE NOTES 2,7			025836	111	614	091945	95	236	142630	310	265	233447	81	712	075530	114	824
112000	0	0	025839	126	159	092100	117	274	142722	344	249	233451	89	766	075534	120	705
112005	7	19	0262			092318	171	322	142800	373	242	233454	98	820	0285		
112011	19	59	SEE NOTES 2,7			092347	189	319	0275			233457	106	872	SEE NOTES 2,7		
112016	28	99	014651	0	0	092410	206	311	SEE NOTES 2,7			0280			091900	0	0
112022	39	138	014659	9	21	092443	232	290	191040	0	0	SEE NOTES 2,7			091904	10	53
112027	48	195	014800	23	69	092515	260	267	191100	0	0	215400	0	0	091907	17	111
112032	54	236	014900	38	108	092545	289	248	191111	21	11	215508	18	34	091911	30	171
112036	61	283	015000	51	170	092642	333	225	191118	39	48	215558	33	77	091915	37	223
112043	69	330	015100	61	223	092750	363	211	191121	53	89	215746	49	116	091918	41	271
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TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
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111045	51	172	065610	15	73	035357	131	214
111050	58	200	065624	22	119	035381	232	187
111057	67	277	065637	31	164	035431	424	181
111063	75	252	065640	42	239	035480	618	140
111070	82	278	065645	51	279	035511	809	131
111076	90	307	065650	59	321	035580	1001	129
111083	98	333	065654	68	357	0299		
111090	108	361	065667	77	433	SEE NOTE 2		
111098	120	394	065673	87	509	034598		
111105	134	410	065687	133	574	034607	1	6
0288			065695	160	583	034613	8	44
SEE NOTE 2			065704	191	582	034618	13	86
049475	5	0	065720	265	507	034624	20	131
049502	0	0	065740	381	356	034630	27	173
049510	4	18	065755	463	291	034635	31	220
049525	16	76	0294			034640	46	263
049537	26	134	SEE NOTE 2			034646	57	377
049547	35	193	101400	0	0	034651	71	323
049554	42	244	101408	7	58	034658	92	349
049563	48	281	101415	16	113	034665	115	356
049572	54	328	101421	26	152	034672	139	371
049580	56	369	101427	38	181	034680	201	371
049586	62	406	101432	56	200	034710	289	335
049591	67	447	101438	76	206	034734	386	303
049601	73	497	101445	103	204	034780	579	256
049612	82	548	101452	132	204	034829	772	189
049621	89	600	101458	157	196	0300		
049630	94	634	101475	231	175	SEE NOTE 2		
049640	107	685	101524	423	149	052698	0	0
049652	122	721	101574	617	133	2710	1	7
049657	138	729	101625	807	125	2716	7	38
0289			101675	1000	117	2721	21	73
SEE NOTE 2			101724	1192	109	2729	29	109
113767	0	0	0295			2735	48	143
113799	1	22	SEE NOTE 2			2740	63	157
113815	21	151	110313	0	0	2746	84	165
113821	27	197	110321	3	33	2752	105	165
113830	40	270	110327	11	78	2768	171	163
113844	60	396	110331	16	125	2783	234	156
113863	74	468	110331	21	164	2808	317	148
113865	96	546	110341	24	210	2835	411	147
113874	120	587	110346	31	262	2884	597	137
113880	162	587	110351	38	309	2936	810	135
113885	170	517	110357	48	364	2986	1002	135
113893	228	468	110363	66	387	0301		
113900	294	316	110369	135	134	SEE NOTE 2		
113907	366	237	0296			062798	0	0
0290			SEE NOTE 2			2806	3	27
SEE NOTE 2			010305	0	0	2815	14	82
022867	0	0	010313	0	0	2818	21	126
022901	0	5	010322	11	57	2823	29	161
022913	15	73	010328	17	111	2828	37	202
022925	31	159	010334	26	158	2835	43	272
022935	44	239	010339	33	205	2843	51	346
022944	60	315	010345	40	247	2848	59	403
022955	84	389	010350	48	297	2855	68	469
022963	113	402	010354	56	343	2862	75	540
022970	151	363	010359	63	387	2870	85	616
022977	191	315	010364	71	429	2877	95	669
022983	276	237	010370	83	468	2883	105	728
023008	347	199	010377	96	510	2888	110	776
023017	374	186	010385	120	543	2895	124	822
0291			010392	144	545	2904	149	860
SEE NOTE 2			010399	175	533	2911	168	874
073901	0	0	010413	292	432	2917	188	870
073909	10	37	010430	349	316	2928	256	770
073916	15	74	010455	461	291	2943	372	540
073922	35	109	010480	544	219	2982	587	312
073930	51	149	0297			0302		
073937	65	185	SEE NOTE 2			0302		
073945	86	228	015800	0	0	030868	0	0
073956	120	267	015808	7	60	3901	0	6
073968	160	282	015814	13	117	3910	10	81
073973	184	279	015820	17	159	3920	21	164
073990	265	223	015824	23	204	3925	29	210
074007	343	169	015829	33	243	3931	34	259
074016	378	155	015833	35	284	3938	44	323
074026	422	149	015838	42	328	3946	57	401
074045	500	128	015844	48	380	3951	69	438
0292			015849	58	424	3961	84	513
043770	0	0	015853	64	467	3965	111	570
043800	0	0	015860	77	514	3978	134	582
043820	9	20	015871	102	582	3984	158	581
043828	21	77	015877	115	595	3992	198	550
043837	35	154	015883	151	589	4003	255	477
043843	46	196	015894	218	502	4011	307	401
043855	75	275	015914	313	386	4017	347	361
043860	88	285	015920	347	363	4027	384	322
043866	110	290	015936	510	264	4045	447	284
043875	144	284	015983	674	233	0303		
043885	203	251	0298			094870	0	0
043902	279	211	SEE NOTE 2			4902	1	1
043920	360	187	035302	0	0	4919	1	5
043930	402	178	035311	7	31	4933	25	77
043949	479	164	035317	17	77	4939	35	125
0293			035322	29	115	4948	48	187
SEE NOTE 2			035328	32	148	4955	53	257
045570	0	0	035335	50	191	4962	71	315
045501	0	0	035343	71	215	4969	84	383

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
4977	99	408	1326	86	403	0600	8	13
4984	118	427	1331	118	432	0650	20	85
4990	168	337	1336	158	427	0690	53	155
4996	257	101	1340	214	367	0720	40	209
			1348	284	290	0760	55	282
0304			1360	390	229	0800	64	354
SEE NOTE 2			1370	471	209	0830	79	402
111470	0	0	1395	649	181	0892	110	468
1502	0	1	1412	870	172	0930	143	455
1510	10	37	0310			0952	171	426
1516	21	76	0311			1005	332	353
1525	35	115	023301	0	0	0318		
1532	58	153	3109	13	84	SEE NOTE 2		
1541	86	173	3314	30	153	042270	0	0
1547	107	177	3321	65	221	2300	0	6
1561	165	177	3326	98	235	2400	3	9
1574	217	170	3332	149	239	2420	9	30
1581	252	166	3338	192	216	2458	15	70
1596	308	156	3348	277	203	2475	19	104
1607	350		3368	477	188	2512	43	142
1622	408	147	2400	653	185	2560	68	211
1633	445	147	2428	877	181	2625	108	222
0305			2454	1074	179	2740	190	245
SEE NOTE 2						2819	251	245
013370	0	0	0311			2886	308	238
3401	0	0	SEE NOTE 2			2939	349	230
3410	10	37	032209	0	0	3030	423	211
3427	23	77	2221	55	176	3122	501	198
3438	42	149	2231	91	307	3215	575	186
3448	58	236	2237	113	371	3271	617	180
3455	70	276	2243	147	438	3300	643	177
3462	84	317	2250	200	445	0319		
3480	133	374	2255	215	380	SEE NOTE 2		
3490	162	389	2265	371	227	071380	0	0
3500	203	397	2278	471	222	1401	0	0
3516	265	400	2300	624	260	1500	10	37
3537	349	383	2331	804	283	1544	31	77
3550	410	365	2367	1047	284	1600	71	91
3565	448	347	2383	1243	268	1700	154	91
0306			2409	1452	243	1800	230	87
SEE NOTE 2						1900	318	86
042270	0	0	014295	0	0	2000	404	79
2300	0	0	042196	79		2100	482	77
2314	1	6	2206	84	41	2200	563	77
2320	16	35	2211	95	117	2300	645	70
2332	41	75	2216	110	197	2400	724	69
2338	60	107	2221	140	275	2500	803	70
2347	87	153	2226	163	340	2600	881	69
2357	120	180	2230	168	377	2700	964	88
2373	187	182	2235	197	396	0320		
2380	213	180	2239	236	390	SEE NOTE 2		
2396	281	174	2245	303	327	091800	0	0
2415	361	169	2268	431	249	1900	8	26
2430	424	166	2275	559	216	1950	23	86
2445	480	163	042302	760	185	1970	31	115
2455	522	162	0313			1998	40	156
0307			043697					

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS			
0827	770	147	2191	79	103	4378	98	343	2400	1	0	4345	90	415	1075	139	250
0323			2241	117	103	4431	161	266	2409	20	98	4350	116	453	1131	181	255
SEE NOTE 2			2335	190	101	4565	345	159	2416	43	214	4355	153	486	1161	211	247
142100			2386	293	100	0334			2423	177	90	4361	533	120	1215	263	203
2151	17	78	2479	298	98	SEE NOTE 2			0342			0353			1276	323	160
2220	28	155	2585	389	93	024884		96	SEE NOTE 2			SEE NOTE 2			1346	381	145
2252	48	237	2685	467	90	4899		106	073761	0	0	121605	0	0	1465	462	135
2329	85	260	2782	541	89	4925			3800	1	1	1625	40	13	1579	575	126
2415	157	240	2885	622	89	4950			3810	22	120	1647	51	36	1624	843	125
2440	170	228	2982	694	89	4976			3816	39	221	1678	65	52	SEE NOTE 2		
2444	208	212	3085	771	89	5000			3824	59	315	1710	93	60	SEE NOTE 2		
2512	250	181	3185	847	89	5050			3830	755	98	1750	126	60	043800		
2535	281	162	0329			5100			0343			1800	172	62	3822	1	12
2539	366	149	SEE NOTE 2			5200			SEE NOTE 2			1850	209	63	3837	8	28
2722	423	146	091900	0	0	5300			092099	0	0	1900	249	60	3857	15	51
2824	443	145	1974	44	38	5400			2121	11	50	2015	322	60	3881	23	86
2856	500	145	2005	60	75	5600			2130	28	176	2132	440	60	3908	13	118
2934	517	145	2030	67	115	0335			2138	53	162	2253	536	60	3924	40	140
0324			2053	74	156	SEE NOTE 2			2145	72	455	2373	633	58	3936	43	159
SEE NOTE 2			2132	102	315	101773	0	0	2153	98	565	2495	729	58	3988	53	189
110800	0	0	2171	113	393	1800	1	7	2160	133	636	2618	823	59	3983	63	225
0814	2	20	2212	127	468	1807	18	111	2167	211	540	2739	920	59	4010	74	263
0900	17	43	2254	143	543	1813	35	193	2173	314	305	2858	1011	59	4027	83	287
0928	29	63	2312	185	570	1825	53	278	2180	384	243	2983	1112	59	4053	95	318
0942	37	77	2354	197	541	1831	90	478	2198	532	210	3106	1208	59	4099	102	357
0958	44	90	2362	234	467	1838	107	591	2228	706	210	3252	1243	35	4145	152	364
0915	52	110	2381	274	393	1843	121	776	2250	909	197	3326	1305	27	4187	189	357
0990	59	126	2381	310	313	1850	140	807	0344			0354			4213	218	246
1001	63	147	2446	385	241	0336			SEE NOTE 2			SEE NOTE 2			4292	302	246
1062	70	207	2538	447	234	113673	0	0	095071	0	0	005900	0	0	4491	481	175
1106	106	257	2650	549	234	3704	0	0	5101	0	0	5914	3	5	4853	770	157
1123	115	275	0330			3704	0	0	5109	19	77	5950	9	21	0359		
1165	139	308	SEE NOTE 2			3712	14	75	5116	95	77	5960	13	36	SEE NOTE 2		
1200	159	321	230003	0	0	3718	29	156	5125	143	113	5976	20	44	021151	0	0
1253	192	316	0025	3	37	3725	52	253	5132	201	115	010000	39	52	1201	0	1
1300	238	288	0037	8	79	3730	70	333	5150	314	133	02020	56	57	1250	2	10
1372	307	256	0051	14	117	3735	95	413	5165	447	133	0100	120	57	1274	11	36
1467	383	235	0105	20	156	3740	119	469	5174	526	131	0190	200	57	1324	38	60
1567	462	219	0114	27	198	3752	182	535	5190	640	130	0262	257	52	1353	59	75
1663	537	210	0130	33	236	3757	228	535	0345			0311	302	51	1407	101	90
1765	613	205	0143	38	275	3763	284	503	SEE NOTE 2			0431	400	41	1440	119	90
1825	658	204	0155	45	315	0337			112750	0	0	0547	449	37	1500	141	90
0325			0209	56	355	SEE NOTE 2			2806	2	2	0670	600	35	1600	233	90
SEE NOTE 2			0223	63	395	115776	0	0	2810	13	41	0794	701	35	1700	354	75
155635	0	0	0235	69	432	5870	2	7	2816	38	115	0912	800	30	1759	402	76
5830	3	0	0248	77	468	5900	2	7	2822	196	78	0355			1829	458	69
5849	12	37	0320	102	544	5910	2	7	2830	213	78	SEE NOTE 2			1900	518	66
5918	34	70	0348	132	575	5915	21	92	0346			015388	0	0	0360		
160000	83	89	0357	145	569	5920	44	149	SEE NOTE 2			5419	3	14	SEE NOTE 2		
0100	151	85	0410	180	505	5926	75	189	100171	0	0	5428	8	30	039660	0	0
0200	237	84	0425	230	395	5931	103	220	0200	0	1	5435	9	42	4003	0	0
0300	300	80	0456	308	275	5937	153	220	0209	15	71	5442	12	51	4054	3	16
0412	406	78	0656	481	352	5948	238	219	0216	45	168	5451	15	60	4073	11	41
0500	462	78	0331			5957	309	208	0230	275	125	5460	18	72	4114	48	53
0324			SEE NOTE 2			5970	416	206	0271	435	153	5474	25	89	4212	119	59
SEE NOTE 2			122999	0	0	5977	466	194	0292	582	175	5487	33	101	4260	163	58
131800	0	0	3035	9	36	5983	543	192	0311	720	171	5503	41	113	4332	219	52
1830	3	0	3060	17	77	5988	620	189	0347			5530	58	130	4407	281	51
1900	8	40	3086	27	115	120010	697	187	SEE NOTE 2			5569	89	135	4488	360	47
1918	18	111	3115	40	147	0338			020770	0	0	5600	114	133	4575	420	48
1930	25	149	3139	51	177	SEE NOTE 2			0801	2	3	5629	139	130	4700	525	50
1945	33	197	3160	67	210	134045	0	0	0809	80	108	5753	250	100	4797	600	47
1956	35	228	3190	85	226	4102	0	7	0813	47	231	5870	346	90	4895	680	47
2020	51	294	3238	122	242	4105	12	72	0824	72	330	5891	446	83	4995	760	46
2035	59	333	3300	217	239	4110	25	164	0830	90	408	6008	539	76	5100	847	46
2058	74	387	3353	229	227	4114	39	276	0836	113	481	6350	732	76	5200	888	46
2138	113	437	3416	239	196	4121	70	495	0843	144	550	6591	922	76	0361		
2145	129	429	3466	426	171	4129	102	722	0848	170	556	0348			SEE NOTE 2		
2157	168	327	3489	619	148	4134	132	881	0348			SEE NOTE 2			203100	0	0
2208	207	229	0332			4139	155	979	SEE NOTE 2			031892	0	0	3150	3	8
2218	233	189	SEE NOTE 2			4142	190	1030	035071	0	0	1910	0	0	3161	8	21
2248	282	149	011404	0	0	4146	347	988	5103	0	0	1922	1	19	3170	13	32
0327			1427	6	43	0339			5109	0	72	1932	3	36	3187	21	46
SEE NOTE 2			1449	12	83	SEE NOTE 2			5116	29	142	1948	15	59	3200	28	51
023850	0	0	1491	22	157	142651	0	0	5124	61	231	1960	18	78	3225	51	55
3930	3	5	1532	35	242	2704	0	0	5130	94	293	1981	31	92	3250	72	55
3958	8	35	1571	45	321	2707	3	30	5137	129	326	2008	43	110	3300	113	55
3990	15	87	1608	55	400	2712	32	112	0350			2039	52	132	3400	200	52
4010	18	124	1644	67	475	2716	56	207	194160	0	0	2074	85	158	3500	283	49
4030	19	157	1661	70	510	2720	80	292	4202	0	1	2123	121	180	3600	365	55
4050	27	201	1670	75	551	2724	98	389	4210	0	1	2162	153	192	3750	448	55
4087	36	274															

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS			
4440	120	115	0371			2071	68	253	3457	1146	291	5936	119	460	0517	77	498
4530	400	97	SEE NOTE 2			2077	89	350	3504	1417	223	5941	146	513	0518	90	535
4615	440	85	031470			2082	107	420	0384			5948	188	582	0520	104	577
4725	580	82	1500	0	0	2089	137	487	SEE NOTE 2			5958	281	474	0522	129	600
0361			1508	13	35	2094	168	543	204075	0	0	5968	375	395	0524	146	603
SEE NOTE 2			1515	41	90	2105	242	541	4101	0	0	5986	535	340	0525	167	593
063551	0	0	1521	75	161	2111	302	518	4114	6	47	170012	731	316	0527	206	550
1600	1	0	1526	110	177	2118	367	406	4122	12	81	0039	923	292	0529	250	468
1615	5	22	1533	157	177	2126	447	325	4130	15	114	0392			0398		
1633	9	40	1539	213	154	2134	630	283	4136	19	166	SEE NOTE 2			SEE NOTE 2		
1667	22	80	1549	298	138	0378			4142	25	225	184870	0	0	164800	0	0
1691	34	119	1558	377	130	SEE NOTE 2			4150	31	292	4903	4	0	4802	4	33
1717	44	159	1569	460	125	103850	0	0	4158	38	334	4912	24	94	4804	12	100
1750	60	198	1578	435	121	3900	0	0	4164	50	386	4921	68	229	4804	15	157
1780	73	234	1586	605	121	3906	22	48	4168	62	442	4930	120	198	4804	25	217
1820	95	273	1594	668	121	3913	50	121	4178	77	533	4938	182	157	4810	33	315
1870	124	300	0372			3920	74	197	4188	100	563	4950	268	237	4812	38	395
1900	150	302	SEE NOTE 2			3925	102	261	4196	138	668	4958	304	355	4814	50	468
1943	189	293	095698	0	0	3932	122	331	0385			4965	356	408	4816	58	560
1993	204	267	5711	1	7	3939	151	387	SEE NOTE 2			4971	408	387	4818	67	612
4055	305	220	5719	26	85	3945	201	408	155370	0	0	4984	520	284	4820	77	700
4148	381	195	5725	49	141	3952	253	400	5408	15	23	5002	680	213	4822	102	773
4240	460	187	5731	80	203	3959	324	347	5418	38	157	5019	800	189	4825	119	803
4332	557	174	5737	115	264	3969	414	280	5430	115	217	5041	1000	157	4826	131	820
4424	612	167	5742	153	245	3979	501	237	5437	181	157	5067	1200	140	4828	165	810
0364			5748	208	215	0379			5455	327	78	0393			4829	185	800
SEE NOTE 2			5755	270	157	SEE NOTE 2			5464	404	52	SEE NOTE 2			0399		
071450	0	0	5765	358	158	021351	0	0	0386			153800	0	0	SEE NOTE 2		
1507	0	0	5791	580	142	1400	0	0	SEE NOTE 2			3803	15	109	190201	0	0
1558	2	10	5819	740	141	1409	26	39	095172	0	0	3810	35	308	0203	8	77
1569	7	27	5845	958	140	1416	57	100	5210	15	0	3815	58	514	0206	19	180
1586	14	35	5870	1158	140	1424	100	197	5219	46	180	3819	85	706	0207	31	245
1630	33	74	0373			1433	153	195	5228	100	275	3824	110	860	0207	38	303
1670	52	114	SEE NOTE 2			1439	215	120	5236	154	275	3830	167	947	0209	46	395
1700	67	158	102199	0	0	0380			5245	230	237	3834	300	657	0210	54	468
1740	83	205	2219	1	9	SEE NOTE 2			5254	296	198	3840	479	300	0212	62	544
1790	113	228	2221	27	78	044470	0	0	5268	423	158	3846	577	197	0213	65	612
1871	167	243	2229	56	149	4500	0	0	5293	615	102	3850	658	157	0214	73	695
1944	229	226	2235	90	220	4507	25	37	5308	731	78	3855	750	137	0215	81	773
2015	245	203	2241	113	223	4515	58	93	0387			0394			0216	87	832
2088	304	187	2248	170	182	4521	88	163	SEE NOTE 2			SEE NOTE 2			0217	96	900
2193	423	182	2253	239	157	4528	115	241	131870	0	0	164404	0	0	0218	108	953
2300	468	164	2270	370	119	4535	142	323	1905	12	8	4406	11	78	0220	127	1020
2393	577	157	2295	563	101	4541	173	396	1913	29	149	4408	21	180	0221	167	1033
2492	650	155	2312	758	93	4548	203	431	1920	54	237	4409	31	285	0222	192	990
2532	798	153	2349	950	85	4555	240	431	1932	115	316	4410	38	387	0400		
0365			2375	1140	74	4560	313	389	1938	169	308	4417	54	484	SEE NOTE 2		
SEE NOTE 2			0374			4572	416	293	1963	375	198	4418	69	627	113400	0	0
114991	0	0	SEE NOTE 2			4580	501	240	1992	615	125	4418	77	700	113401	2	30
5005	1	1	110998	0	0	4586	552	213	2008	731	105	4418	92	810	113406	96	80
5017	78	160	1010	5	24	0381			2030	885	92	4419	108	896	113411	21	157
0366			1017	10	120	SEE NOTE 2			0388			4420	131	970	113416	33	245
125089	0	0	1025	62	201	113943	0	0	SEE NOTE 2			4421	163	976	113421	48	315
5100	0	0	1031	95	263	3958	3	9	140070	0	0	4423	227	874	113425	63	353
5108	17	79	1039	133	319	3963	22	90	0105	8	38	4425	330	634	113428	71	395
5114	42	139	1045	173	349	3969	37	149	0112	23	141	4427	423	453	113433	110	454
5120	83	138	1050	219	349	3974	58	249	0118	42	237	4431	538	331	113437	127	460
5124	131	130	1055	270	302	3980	80	332	0128	88	316	4434	613	276	113441	163	454
5132	185	98	1065	368	202	3985	107	373	0134	125	322	0395			113443	183	438
5138	241	79	1072	434	157	3990	147	372	0141	192	308	SEE NOTE 2			113450	233	395
5153	322	64	1091	564	121	3995	195	325	0148	244	276	205202	0	0	113456	310	315
5180	562	67	1102	685	140	4002	262	272	0163	385	237	5207	35	220	113465	387	275
5208	763	92	1129	882	63	4007	308	247	0188	577	180	5208	46	308	113475	467	231
5235	960	107	1154	1082	48	4024	423	222	0216	769	158	5210	65	444	113500	674	173
5262	1161	120	1180	1283	48	4051	623	214	0240	962	149	5212	77	541	0401		
0367			0375			4075	814	214	0389			5214	88	672	SEE NOTE 2		
SEE NOTE 2			SEE NOTE 2			4102	1006	204	SEE NOTE 2			5215	96	750	130306	0	0
011998	0	0	120659	0	0	4129	1200	191	090290	0	0	5216	100	817	130308	11	53
2008	1	0	0713	8	10	0382			0300	0	0	5218	111	896	130310	23	134
2015	18	75	0720	18	103	SEE NOTE 2			0303	15	77	5219	123	968	130312	31	213
2020	52	87	0725	33	189	031460	0	0	0311	35	140	5220	135	1040	130315	37	308
2025	95	81	0731	52	272	1480	0	0	0320	69	235	5222	158	1105	130317	46	395
2042	211	78	0736	68	349	1505	102	14	0325	96	276	0396			130319	54	445
2055	310	70	0741	86	422	1512	127	92	0330	135	292	SEE NOTE 2			130320	58	514
2080	500	70	0746	103	483	1520	155	173	0338	192	276	152800	0	0	130321	65	596
2107	697	70	0751	133	536	1527	185	243	0357	346	212	2802	8	53	130323	73	673
2134	884	68	0758	183	551	1534	224	285	0380	538	173	2803	17	140	130325	79	743
2160	1073	68	0763	245	478	1541	270	293	0408	731	157	2805	31	230	130327	90	810
2185	1269	68	0769	307	373	1548	339	258	0434	923	140	2807	37	300	130330	106	878
0369			0775	373	308	1555	401	228	0390			2808	50	380	130333	142	932
SEE NOTE 2			0785	539	229	1578	537	182	SEE NOTE 2			2810	62	470	130335	173	905
021300	0	0	0822	752	197	1604	780	165	150680	0	0	2812	69	575	130337	213	840
1310	0	1	0837	925	173	1631	971	157	0702	C	0	2813	77	640	130338	265	729
1314	1	20	0874	1114	173	0383			0712	23	117	2814	88	730</			

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
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141221	204	730	153012	23	156	181600	163775	179	643	142722	22	78	171945	18	118		
141222	273	595	153016	31	236	181610	163778	213	633	142750	32	120	171962	30	198		
141224	366	430	153020	44	315	181617	163782	251	598	142770	40	153	171972	36	238		
0403			153024	55	355	181622	163787	304	550	142839	72	237	171982	43	270		
SEE NOTE 2			153027	65	394	181629	163792	379	474	142897	110	270	171991	49	316		
150401	0	0	153032	90	454	181635	163800	464	398	142960	160	273	172005	60	358		
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150409	11	77	153040	154	457	181646	0420			143092	280	206	172045	100	468		
150413	23	157	153042	179	427	181652	SEE NOTE 2			143227	400	173	172060	120	461		
150415	27	180	153046	210	393	181656	192475	0	0	143371	520	157	172082	164	465		
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150425	54	395	153079	500	258	181666	192519	58	235	0429			172169	524	198		
150430	65	468	153087	556	245	181670	192525	58	315	SEE NOTE 2			172186	724	161		
150433	77	543	0409			181674	192533	106	370	154200	0	0	0437				
150439	96	618	SEE NOTE 2			181684	192539	154	358	154272	19	78	SEE NOTE 2				
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150450	165	640	164415	19	125	0414	192594	602	100	154547	197	228	201073	44	157		
150453	223	543	164417	25	156	SEE NOTE 2				154639	280	197	201090	58	198		
150463	338	395	164421	35	236	132100	SEE NOTE 2			154760	385	168	201113	84	237		
150476	454	315	164424	42	276	132900	143300	0	0	154890	489	148	201139	116	249		
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SEE NOTE 1			164441	63	394	132915	143308	12	37	155385	895	125	201209	236	193		
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161206	13	150	164445	129	535	132932	143321	46	235	181491	0	0	201439	596	105		
161208	19	198	164447	154	545	132937	143326	60	315	181503	0	0	0439				
161210	27	276	164451	181	528	132943	143331	79	395	181540	4	13	SEE NOTE 2				
161212	38	355	164453	200	505	132948	143337	102	467	181600	18	79	146600	0	0		
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161221	108	603	0410			132975	143355	246	435	181797	232	193	146646	63	316		
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161242	500	252	132316	28	146	0415	0422			0431			146731	443	119		
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0405			132325	42	234	140600	090081	0	0	190700	0	0	146816	799	69		
SEE NOTE 2			132330	48	283	140610	090102	0	0	190742	17	33	0440				
170901	0	0	132334	56	328	140617	090112	20	93	190774	30	78	SEE NOTE 2				
170902	11	62	132338	65	373	140622	090120	40	205	190803	41	115	151200	0	0		
170904	19	133	132342	75	409	140628	090126	54	309	190835	57	157	151216	14	36		
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170910	58	453	132357	132	496	140649	090157	184	565	191120	307	188	151240	47	240		
170912	69	540	132359	146	499	140653	090159	260	667	191255	397	157	151245	56	284		
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170917	160	675	132370	247	444	140676	0424			0432			151274	164	375		
170918	200	593	132380	353	373	140680	SEE NOTE 2			SEE NOTE 2			151287	240	266		
0406			132391	448	325	140687	164400	0	0	161100	0	0	151301	306	198		
SEE NOTE 2			132400	509	305	140691	164407	11	78	161119	8	37	151332	521	120		
133502	0	0	0411			140698	164412	28	158	161142	20	116	151365	583	84		
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133509	15	121	140808	13	59	140712	164424	80	253	161165	36	198	151440	920	43		
133512	19	156	170810	27	131	0416	164427	101	268	161188	55	275	0441				
133516	31	236	140822	38	199	SEE NOTE 2	164432	136	269	161226	91	355	SEE NOTE 2				
133518	35	272	140828	46	258	151900	164444	232	237	161254	127	380	154000	0	0		
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133531	90	420	140843	79	406	151922	0425			161358	316	254	154832	36	198		
133534	111	420	140848	89	443	151928	SEE NOTE 2			161451	476	214	154837	44	237		
133537	130	419	140853	109	478	151933	171513	0	27	161581	680	195	154863	58	276		
133541	173	391	140857	130	497	151938	171523	31	185	161703	876	181	154890	76	316		
133548	237	315	140860	150	504	151944	171526	40	237	0433			154895	108	340		
133563	377	236	140863	171	504	151954	171530	52	284	SEE NOTE 2			154898	204	340		
133578	503	215	140867	208	486	151957	171532	65	315	153400	0	0	154899	288	198		
133592	612	177	140870	245	460	151960	171537	88	340	153434	8	10	154931	440	117		
0407			140878	364	370	151965	171541	106	400	153452	19	79	154969	600	85		
SEE NOTE 2			140887	440	285	151970	171545	133	412	153463	24	117	155021	789	66		
141301	0	0	140906	595	219	151970	171551	190	410	153475	32	158	0443				
141305	2	30	0412			151972	171557	245	363	153486	40	199	SEE NOTE 2				
141307	4	70	SEE NOTE 2			151977	171565	320	315	153501	50	237	184000	0	0		
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141313	21	189	151706	9	19	151984	0426			153533	115	316	184014	15	77		
141315	24	228	151712	21	79	151988	SEE NOTE 2			153559	120	350	184023	25	157		
141320	35	308	151718	30	138	151992	195300	0	0	153615	208	365	184028	33	197		
141324	44	387	151724	39	193	151996	195305	8	46	153624	400	215	184032	40	237		
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141335	85	528	151736														

TIME	STRAIN	SERS	TIME	STRAIN	SERS	TIME	STRAIN	SERS	TIME	STRAIN	SERS	TIME	STRAIN	SERS
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190534	40	157	143629	520	28	SEE NOTE 2			014500	0	0	135272	151	420
190539	48	196	0454			161500	0	0	014520	15	77	135347	290	320
190544	58	238	SEE NOTE 2			161522	4	7	014530	29	157	135404	385	284
190549	70	276	153900	0	0	161561	15	77	014539	38	237	135510	577	237
190556	88	316	153930	13	33	161602	27	156	014547	48	317	135650	769	217
190567	128	359	153940	17	78	161622	35	198	014556	65	398	0485		
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190579	168	334	153970	29	158	161665	53	276	014572	131	544	161733	0	0
190585	220	276	153980	38	198	161685	66	315	014599	199	555	162050	8	37
190604	311	198	153990	51	247	161740	95	357	014615	269	507	162072	20	115
190623	396	142	154014	75	268	161770	119	365	014631	350	431	162094	33	198
190652	520	102	154035	110	270	161815	174	355	014658	461	367	162116	45	277
190699	720	76	154064	171	198	161875	308	287	014686	577	330	162128	53	319
0465			154120	291	119	162190	500	251	014726	731	311	162140	59	355
SEE NOTE 2			154135	458	99	0465			014767	888	400	162161	77	411
130282	0	0	154217	1000	96	SEE NOTE 2			0472			162195	107	506
130285	15	81	0457			053000	0	0	SEE NOTE 2			162217	134	527
130286	29	205	SEE NOTE 2			053056	5	35	047500	0	0	162242	173	529
130288	42	418	162000	0	0	053102	15	115	047511	19	77	162282	251	455
130290	51	395	162014	11	0	053146	27	198	047521	27	157	162336	346	387
130291	65	472	162022	20	70	053167	33	240	047530	38	240	162355	538	340
130292	78	565	162025	25	91	053187	38	280	047538	48	316	162383	731	325
130294	102	612	162031	32	137	053213	47	320	047547	60	399	0487		
130295	131	625	162040	50	198	053239	55	355	047555	75	472	SEE NOTE 2		
130298	162	566	162046	68	229	053264	65	395	047563	87	545	160000	0	0
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130303	388	310	162071	184	180	053369	119	476	047599	186	683	160005	27	198
130307	473	263	162080	276	117	053415	160	475	047611	242	618	160007	39	316
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0464			162097	600	52	053538	269	375	047659	481	600	160010	58	477
SEE NOTE 2			0458			053650	365	339	047691	615	380	160011	68	567
141900	0	0	SEE NOTE 2			053696	481	374	0476			160012	76	638
141901	8	18	090600	0	0	053870	615	320	SEE NOTE 2			160014	85	702
141903	15	101	090602	7	70	0466			141950	0	0	160014	92	771
141905	24	158	090605	27	225	SEE NOTE 2			144000	0	0	160015	100	853
141906	31	237	090605	32	237	071600	0	0	144007	38	221	160017	111	930
141907	43	311	090606	38	337	071633	4	37	144013	71	545	160018	120	989
141909	56	395	090609	55	476	071657	15	117	144018	107	329	160019	134	1051
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141912	91	517	090612	74	622	071689	35	240	0477			160022	168	1133
141913	113	515	090613	81	695	071700	58	280	SEE NOTE 2			160023	208	1133
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SEE NOTE 2			090617	133	905	071737	62	398	021718	127	1051	160034	683	668
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140805	23	157	090622	292	925	071799	127	640	0478			160000	0	0
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140811	77	453	0453			072003	660	303	041976	28	117	160007	33	324
140813	100	529	SEE NOTE 2			072110	812	288	042035	47	195	160008	38	409
140815	171	474	083900	17	77	072191	727	282	042088	65	276	160010	45	485
140817	221	386	083913	29	157	072300	881	276	042135	108	316	160011	52	567
140818	281	273	083918	46	236	SEE NOTE 2			042168	115	325	160012	58	639
140820	330	169	083921	58	276	165900	0	0	042237	174	316	160013	65	711
140821	379	180	083925	79	314	165976	4	13	042287	221	278	160014	71	771
0468			083927	100	323	170005	27	77	042438	346	237	160015	81	865
SEE NOTE 2			083932	146	323	170027	39	156	042637	500	233	160016	88	910
152300	7	26	083935	173	269	170040	47	198	042982	749	231	160017	100	932
152303	16	92	083939	225	204	170050	54	237	0481			160019	122	1054
152304	26	157	083944	271	157	170060	61	275	SEE NOTE 2			160021	156	1076
152305	32	157	083947	304	133	170072	68	316	050300	0	0	160030	523	1027
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152308	57	316	083972	538	53	170097	88	395	050404	20	101	0490		
152309	65	400	0461			170112	97	435	050435	30	153	SEE NOTE 2		
152310	84	540	SEE NOTE 2			170129	111	467	050467	38	198	051800	0	0
152312	89	614	135500	0	0	170150	134	504	050479	43	237	051804	29	157
152313	114	630	135520	0	0	170173	165	525	050507	52	285	051805	38	250
152316	145	625	135565	11	77	170193	202	521	050527	58	316	051806	45	322
152317	191	520	135588	19	113	170230	272	446	050555	70	355	051807	55	401
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152322	387	230	135735	100	245	170466	665	316	050896	308	439	051811	78	622
0452			135780	142	240	170466	665	316	051131	500	379	051813	90	697
SEE NOTE 2			135892	240	229	0468			051390	692	360	051814	98	771
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134107	18	0	134080	400	212	020623	11	33	SEE NOTE 2			051817	133	902
134218	40	77	134247	544	204	020650	22	117	175700	9	37	0492		
134273	80	108	134422	680	201	020670	31	205	175797	23	110	SEE NOTE 2		
134327	123	108	0462			020682	38	237	175865	38	198	152000	0	0
134438	220	84	SEE NOTE 2			020692	42	280	175890	54	277	152025	0	7
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SEE NOTE 2			144628	38	237	020770	85	543	176697	692	207	SEE NOTE 2		
143300	0	0	144643	45	261	020781	92	585	0484			161431	0	0
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162937	417	544	184049	385	543	162255	1117	889	170150	239	394	180204	112	317
162994	745	567	184085	628	581	162263	1450	846	170195	422	469	180263	152	394
163036	1053	618	184110	915	573	162278	2072	740	170227	597	505	180324	202	469
163072	1392	618	184138	1272	532	162296	2882	618	170291	1137	529	180381	268	543
163115	1870	582	184173	1825	461	162318	3608	543	170317	1401	529	180446	362	619
163161	2404	544	184234	2613	395	162356	4740	480	170352	1876	491	180555	652	694
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173036	40	157	084115	190	237	170114	97	205	190858	15	33	0665		
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173129	159	395	084212	370	468	170142	228	395	190896	55	157	091435	47	74
173160	239	468	084245	462	542	170157	378	468	190916	66	198	091477	75	113
173195	260	539	084262	520	581	170173	665	503	190933	79	237	091516	103	158
173247	268	590	084272	596	618	170183	822	497	190949	91	276	091549	133	200
173274	17	601	084306	707	656	170193	1255	468	190964	105	317	091578	160	237
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123546	1688	544	131660	547	156	156171	502	467	212967	40	117	131005	19	78
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163801	326	468	152880	3278	395	150598	306	619	151802	217	394	162710	96	78
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095315	0	0	172514	150	551	140730	0	0	092056	60	150	154020	230	395
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095393	2758	903	172510	136	475	171650	248	618	163600	1082	544	0700		
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131672	0	0	172521	198	701	171662	626	806	0691			3049	24	30
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131681	50	149	172528	244	847	171669	1096	824	171500	2	0	3102	72	116
131685	73	228	172532	272	918	171672	1372	802	171532	24	10	3129	100	150
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131693	121	380	172539	340	1062	171679	2648	611	171594	134	70	3236	284	316
131697	150	460	172542	362	1132	171680	2826	506	171623	180	112	3306	492	395
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131709	270	686	172553	556	1355	101336	16	70	171760	392	316	3480	1444	476
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143409	258	941	193379	3466	1756	143210	522	796	113456	972	771	0745	184	316
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161007	24	70	193427	8184	2812	143738	1506	1724	235700	422	350	5855	58	70
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171904	0	0	1510	1288	355	171830	G	0	234100	1580	153	1637	3202	483	5309	30	84
1418	6	10	1710	1702	531	1875	6	9	245900	1775	153	0745			5316	54	151
1628	28	78	0722			1877	56	78	5942	1851	316	187900	0	0	5325	88	243
1438	92	158	165530	0	0	1880	107	175	010090	2000	316	1025	6	12	5333	134	324
1446	136	237	5550	16	21	1881	131	232	0300	2141	316	3112	26	38	5342	205	608
1455	176	316	5600	31	38	1883	162	316	0600	2319	316	3240	62	77	5352	336	682
1465	232	395	5695	62	78	1885	184	395	0900	2482	316	3487	110	117	5367	738	538
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183184	0	0	170047	214	198	1892	313	623	1515	2755	153	3887	290	237	5382	1748	688
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3223	50	78	0358	452	275	1896	478	771	4605	2899	153	4335	524	292	0752		
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3240	112	230	1198	1814	269	1910	2493	723	0053	10	33	5172	950	355	4928	100	165
3245	134	275	0724			1914	3147	626	0063	16	45	5522	1342	395	4937	133	252
3250	156	316	185943	0	0	0737			0085	33	85	6100	2128	416	4944	168	330
3258	208	395	190047	14	7	143006	0	0	0104	52	120	6665	2978	416	4953	209	406
3267	282	468	0150	38	38	3060	1	65	0123	70	165	0746			4961	264	482
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3292	726	618	0373	112	116	3399	22	65	0184	117	245	09434	0	0	4979	473	632
3302	1034	634	0484	178	150	3659	31	65	0281	141	285	0522	20	34	4987	646	670
3313	136	626	0630	228	193	4163	38	65	0200	169	323	0526	34	78	4992	794	685
3324	2052	541	0765	304	229	5699	50	65	0225	217	363	0534	64	150	4997	999	680
3332	2462	544	0960	430	275	151800	66	65	0250	278	401	0542	95	237	5005	1292	656
3352	3268	454	1228	664	316	4851	81	65	0277	377	434	0550	124	316	5017	1802	595
0717			1375	846	323	161900	91	65	0316	575	476	0550	156	395	5027	2250	558
204190	0	0	1672	1326	316	5230	102	65	0371	900	517	0566	196	448	0751		
4215	22	42	1930	1796	292	173546	116	65	0426	1296	533	0476	254	544	162000	0	0
4220	34	78	2595	3510	275	200034	146	65	0460	1585	533	0584	390	618	2014	4	7
4230	64	158	0726			220410	165	65	0511	2061	521	0605	770	488	2024	50	92
4234	78	198	112232	0	0	073830	260	65	0584	2788	484	0615	1046	691	2039	90	172
4237	88	229	2382	4	6	091054	270	65	0742			0621	1276	688	2042	131	252
4243	100	275	2515	26	46	132715	311	65	144744	0	0	0631	1744	660	2050	196	330
4247	110	316	2889	60	105	151017	328	65	4760	10	18	0657	2808	592	2060	308	408
4255	136	395	2989	78	132	171589	348	65	4782	31	52	0681	4352	487	2076	690	682
4263	170	468	3144	107	165	194443	369	65	4840	42	92	0747			2081	712	482
4272	262	544	3336	147	205	270000	392	65	4862	87	132	093380	0	0	2086	1180	468
4278	364	581	3513	204	244	080000	484	65	4882	112	180	3437	0	0	2092	1549	430
4285	526	618	3675	261	283	120500	532	65	4964	170	203	3458	12	36	2101	2104	292
4294	754	641	3841	335	322	153000	565	65	5021	195	192	3483	36	78	0754		
4297	840	648	4037	441	362	181400	596	65	163836	0	0	3504	49	116	172300	0	0
4302	974	648	4396	717	401	203300	617	65	3874	6	0	3523	64	158	2311	2	0
4315	1440	634	4579	721	401	222900	638	65	3922	85	65	3546	85	192	2324	44	92
4330	2160	589	4770	1193	387	075600	746	65	3940	112	92	3565	106	237	2332	82	172
4350	3170	512	4944	1457	362	115160	792	65	3959	138	132	3586	128	272	2340	124	243
4368	3846	491	5063	1639	340	132808	808	65	3982	170	185	3609	162	316	2350	197	330
0718			2812	808	65	2812	808	65	4016	222	268	3636	214	355	2362	362	408
214313	0	0	0738			0738			4035	249	292	3669	304	395	2374	640	450
4330	0	0	144800	J	0	0738			4054	286	331	3715	502	428	2378	818	456
4330	4	3	4816	102	237	4816	102	237	4076	342	378	3724	972	468	2384	1086	430
4380	56	78	4870	164	237	4870	164	237	4100	417	416	3776	1573	476	2392	1521	394
4389	92	158	4274	258	237	4274	258	237	4132	530	450	3806	1834	472	2400	1968	355
4397	134	237	5055	314	237	5055	314	237	4165	678	466	3883	2530	466	0755		
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4415	238	395	5320	432	237	5320	432	237	4260	1306	540	100855	0	0	3737	20	18
4425	308	468	5477	488	237	5477	488	237	4291	1619	532	0913	6	3	3742	50	85
4435	418	544	5670	546	237	5670	546	237	4320	1928	516	0935	31	35	3766	72	122
4443	530	581	150055	656	237	150055	656	237	4408	3102	444	0952	52	78	3750	98	143
4451	724	618	0300	710	237	0300	710	237	0743			0975	83	112	3754	120	198
4460	1014	641	0780	798	237	0780	798	237	154900	0	0	0997	119	157	3758	154	242
4469	1336	633	1175	890	237	1175	890	237	4945	4	0	1020	158	157	3762	191	280
4475	1684	611	1640	970	237	1640	970	237	4983	34	52	1044	204	232	3767	242	322
4487	2222	566	2035	1030	237	2035	1030	237	4996	46	92	1072	280	277	3771	326	362
4505	3120	498	2500	1118	237	2500	1118	237	5017	63	126	1102	377	316	3780	474	401
0719			2857	1176	237	2857	1176	237	5036	81	172	1144	544	355	3790	776	428
133560	0	0	4203	1344	237	4203	1344	237	5057	100	209	1215	736	394	3800	1198	425
3724	10	18	5100	1488	237	5100	1488	237	5076	119	251	1276	1350	405	3805	1484	408
3815	22	42	160750	1702	237	160750	1702	237	5093	139	291	1346	1916	399	3815	1966	362
3948	44	85	0739			0739			5120	170	330	1415	2510	375	3837	3040	300
4090	68	125	163500	0	0	163500	0	0	5142	203	370	0749			0756		
4200	88	165	3524	146	316	3524	146	316	5184	248	408	130700	0	0	191618	0	0
4348	114	205	3562	264	316	3562	264	316	5190	321	446	0708	31	78	1626	20	40
4462	140	243	3600	362	316	3600	362	316	5221	432	482	0716	68	158	1631	41	85
4605	172	283	3675	512	316	3675	512	316	5263	605	520	0725	104	232	1635	57	125
4739	204	323	3780	652	316	3780	652	316	5309	874	550	0733	152	317	1640	76	165
4872	244	362	3925	766	316	3925	766	316	5352	1170	570	0742	228	394	1643	96	205
4905	282	401	4117	964	316	4117	964	316	5388	1514	566	0					

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS			
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0640	197	362	3388	1086	410	3097	399	462	0057	136	195	1395	106	118	5953	98	57
0646	259	400	3405	1195	400	3118	467	490	0088	163	241	1419	167	157	5980	164	97
0651	342	438	0767			3165	565	516	0115	194	283	1445	210	196	080001	163	135
0658	482	477	193552	0	0	3182	733	562	0142	229	328	1477	308	231	0036	190	195
0665	708	499	3597	3	2	3208	892	590	0170	285	373	1510	451	258	0050	206	210
0675	1093	495	3647	50	61	3227	1017	550	0206	390	420	1550	724	273	0076	244	247
0680	1308	482	3670	69	98	3252	1195	514	0242	543	462	1567	850	273	0106	305	282
0687	1727	438	3700	96	147	3277	1391	516	0285	760	470	1576	931	272	0127	370	310
0695	2152	400	3729	125	195	0773			0302	876	411	1614	1282	255	0150	458	328
1205	2654	363	3758	158	240	150255	0	0	0330	1070	468	1642	1532	249	0173	577	340
0767			3790	204	283	0285	2	2	0352	1272	452	0785			0184	643	334
0966	0	0	3815	254	330	0332	49	51	0362	1255	450	170677	0	0	0205	781	338
0991	3	4	3842	316	373	0363	61	98	0779			0697	2	2	0235	1096	328
1029	14	50	3878	411	418	0391	104	148	080765	0	0	0732	43	40	0306	1606	312
1061	38	101	3923	686	453	0420	131	196	0800	1	2	0756	78	78	0340	1940	310
1086	49	150	3941	835	455	0450	162	240	0843	31	50	0780	106	118	0791		
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1152	75	240	4080	1238	416	0510	255	330	0905	99	150	0831	194	196	1080	38	20
1184	94	293	0768			0539	324	374	0935	126	195	0862	275	231	1108	62	57
1205	109	332	085477	0	0	0575	430	418	0965	159	240	0895	409	258	1132	88	97
1227	122	373	090032	2	2	0618	611	462	0995	200	283	0925	586	270	1155	106	135
1254	165	419	0985	71	70	0656	814	480	1020	241	330	0940	711	270	1177	126	175
1280	171	462	0105	90	98	0678	960	482	1050	305	373	0950	776	270	1200	147	210
1308	202	508	0132	121	147	0692	1068	474	1085	406	419	0977	1014	258	1224	171	247
1360	241	552	0163	154	195	0714	1200	462	1110	506	444	1030	1449	242	1249	201	282
1391	255	563	0192	196	240	0737	1509	452	1137	622	462	0786			1270	230	318
1380	295	594	0225	247	283	0774			1157	719	471	183910	0	0	1290	269	353
1418	367	635	0252	300	330	160650	0	0	1187	887	479	3910	1	0	1315	327	390
1471	511	677	0283	380	373	0695	4	2	1202	999	477	3423	2	2	1330	374	407
1490	605	686	0324	534	418	0740	52	50	1252	1280	466	3956	69	40	1350	471	425
1505	710	688	0360	748	433	0772	88	98	1270	1377	466	3986	149	78	1372	515	432
1513	803	678	0382	913	432	0800	118	148	0780			4013	209	118	1384	671	431
1525	958	657	0400	1072	417	0830	148	194	091330	0	0	4040	269	157	1399	717	414
1533	1079	636	0410	1163	407	0866	191	243	1568	0	0	4067	338	196	0792		
0763			0417	1231	391	0895	240	284	1628	81	62	4097	429	231	101725	0	0
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3156	104	148	1325	42	43	1060	776	462	1740	211	238	4190	768	307	1840	88	120
3185	126	194	1357	81	91	1080	936	470	1772	258	262	4202	862	312	1880	111	55
3213	155	238	1387	117	143	1115	1273	462	1797	306	327	4215	972	314	1905	145	35
3243	182	282	1416	153	190	1132	1400	459	1825	372	372	4237	1148	312	1940	25	34
3267	207	330	1447	199	232	0775			1857	463	416	4258	1347	304	1995	40	282
3290	231	372	1480	258	279	170883	0	0	1895	608	460	4297	1690	283	2020	580	292
3320	270	425	1507	324	325	0900	0	2	1925	753	488	0787			2045	796	291
3353	316	480	1537	410	368	0940	41	50	1952	888	500	162837	0	0	2054	844	290
3387	373	532	1575	547	412	0973	74	98	1965	978	502	2876	27	20	2080	1099	273
3425	453	582	1608	735	440	1000	103	147	1982	1092	503	2905	76	57	0793		
3474	593	633	1640	890	450	1030	135	196	2000	1246	500	2930	108	97	132921	0	0
3517	851	655	1664	1216	445	1060	177	240	2038	1540	482	2955	135	135	1444	2	2
3535	1029	641	1678	1415	430	1094	236	284	2070	1784	470	2978	168	175	3510	14	20
3547	1206	618	1691	1622	409	1120	294	329	0781			3006	212	215	3653	45	60
3554	1331	600	0770			1155	379	373	114262	0	0	3037	273	255	3744	66	86
0764			100727	0	0	1198	544	417	4300	2	3	3060	328	282	3845	102	120
163160	0	0	0740	4	2	1220	650	430	4342	52	50	3082	396	310	3953	129	154
3184	2	2	0782	54	50	1242	790	433	4376	79	99	3106	500	332	4031	160	180
3225	52	30	0812	68	97	1270	972	432	4405	137	147	3127	538	343	4115	139	200
3258	89	100	0840	119	145	1290	1114	428	4438	182	196	3144	657	344	4235	263	230
3286	120	150	0871	152	195	0776			4476	265	240	3160	789	341	4370	349	257
3331	156	196	0900	189	238	184585	0	0	4560	728	275	3180	997	319	4455	410	273
3362	193	240	0932	240	282	4593	5	3	4583	939	266	3212	1394	291	4587	535	300
3395	237	283	0959	301	329	4636	62	55	4610	1089	256	0788			4722	698	318
3420	281	329	0989	388	372	4664	92	98	4655	1417	252	183210	0	0	4830	869	327
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3482	422	418	1059	750	432	4720	138	194	134947	0	0	3257	32	49	4990	1237	316
3534	642	467	1071	851	432	4750	162	240	4976	4	2	3281	59	77	5085	1600	276
3550	752	465	1086	995	432	4780	192	283	5007	63	40	3305	82	116	5223	1934	263
3566	878	462	1102	1173	416	4805	221	329	5133	95	78	3326	104	155	5443		239
3587	1080	445	1120	170		4832	266	373	5057	129	118	3350	131	194	5578		230
3606	1246	409	0771			4863	338	418	5080	157	157	3375	159	230	0794		
3616	1362	395	111797	0	0	4900	467	462	5105	191	196	3391	186	253	151405	0	0
0765			1842	0	0	4915	526	470	5131	241	231	3411	224	282	1647	20	20
171888	0	0	1938	4	2	4940	627	478	5160	318	286	3428	264	310	1777	21	55
1906	1	2	1976	67	39	4952	672	464	5200	488	304	3447	315	336	1899	86	97
1952	70	53	2001	102	80	4977	748	443	5220	618	313	3470	362		2014	114	135
1982	102	98	2025	123	118	5003	814	428	5236	755	317	3482	372		2100	131	165
2030	138	150	2049	144	158	0777			5246	850	312	3510	386		2193	165	194
2060	166	195	2072	163	196	200007	0	0	5264	1031	302	3530	380		2290	202	220
2090	203	242	2100	189	240	0014	3	2	5281	1231	282	3552	354		2413	234	250
2121	245	286	2132	229	287	0056	62	50	5300								

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1856	111	336	105040	1715	318	0836			200621	1847	203	165855	81	58	105567	2230	125
1950	949	149	105108	1933	323	081384	0	0	0813			165873	101	87	0825		
2000	1156	346	105165	1976	336	081400	5	4	081545	0	0	165889	121	116	113905	0	0
2064	1468	325	105355		365	081408	29	60	081610	33	19	165906	147	145	113963	2	2
2123	1824	295	0801			081414	75	120	081676	78	48	165923	178	175	114030	16	13
2821	0	0	130928	0	0	081419	111	175	081723	114	77	165942	225	201	114084	44	28
2916	45	20	130950	9	19	081425	133	230	081785	152	104	165964	296	230	114135	63	42
2994	113	57	130965	107	141	081430	154	282	081883	214	145	165993	354	256	114182	82	58
3057	150	96	130970	129	195	081435	174	338	081930	285	175	170008	463	265	114247	109	77
3116	181	135	130975	145	247	081438	192	390	082003	396	201	170022	585	271	114311	137	96
3175	207	175	130980	162	313	081443	215	450	082091	565	220	170046	926	271	114390	175	118
3233	235	212	130985	178	370	081447	242	500	082173	736	226	170072	1132	271	114470	229	137
3295	267	247	130989	193	430	081452	277	550	082212	967	227	170108	1673	265	114561	309	157
3364	311	282	130994	211	490	081458	347	613	082252	1117	224	170132	1873	263	114677	462	175
3417	353	318	130998	236	550	081464	442	670	082398	1723	211	0820			114882	786	183
3498	454	362	131004	275	609	081467	482	672	082595	2537	195	185864	0	0	115053	935	183
3553	516	390	131010	337	669	081474	541	667	082754	3048	187	185889	0	2	115140	1139	175
3650	727	416	131015	406	715	081478	672	630	0814			185905	40	48	115267	1418	155
3693	866	418	131018	488	751	0807			141385	0	0	185909	71	96	115432	2029	144
3730	1070	416	131018	488	751	090888	0	0	141391	14	19	185914	34	145	0826		
3760	1181	406	131023	627	767	090898	12	19	141396	53	77	185917	116	195	145900	0	0
3820	1562	372	131026	749	807	090905	76	77	141404	86	145	185922	145	238	145907	4	3
			131030	934	817	090916	154	195	141408	113	195	185926	182	282	145917	45	58
0797			131033	1118	818	091239	110	0	141413	150	252	185930	222	277	145928	84	111
085870	0	0	131035	1350	810	091385	183	151	141420	202	317	185935	279	371	150002	171	119
5915	3	2	131040	1673	770	091390	199	195	141425	263	374	185940	381	416	150200	270	119
5920	40	48	0802			091395	214	245	141431	351	430	185945	555	455	150300	358	119
5925	63	97	140397	0	0	0808			141438	525	491	185950	871	480	150400	438	116
5930	76	145	140468	25	19	101480	0	0	141445	806	525	185954	1035	485	150500	604	116
5934	91	195	140542	65	57	101493	8	19	141449	998	531	185957	1190	485	150600	764	116
5937	103	238	141010	92	96	101499	38	77	141452	1168	529	185960	1380	480	150900	884	116
5942	120	292	141176	115	135	101505	65	135	141455	1440	514	185964	1708	465	151100	1110	116
5945	131	330	141242	139	175	101510	98	195	141458	1689	496	185975	2386	317	151300	1261	116
5949	146	372	141310	168	211	101515	120	255	0815			0815			151500	1375	116
5952	161	417	141388	214	247	101520	157	323	140000	0	0	201900	0	0	151700	1507	116
5956	178	463	141470	278	282	101527	195	380	140024	1	1	201930	0	0	151900	1634	116
5960	198	508	141540	341	318	101532	251	433	140053	30	58	201980	14	19	152100	1759	119
5963	220	550	141615	416	353	101538	345	499	140076	63	77	202043	44	38	152300	1879	114
5967	249	595	141660	463	370	101545	505	550	140098	96	116	202113	82	58	152500	2007	118
5972	283	632	141700	510	390	101550	572	575	140122	150	155	202188	131	77	152700	2122	116
5975	328	680	141770	605	416	101553	686	583	140150	233	195	202278	204	96	152713	2106	2
5980	378	720	141846	723	443	101557	1113	583	140176	339	220	202380	309	116	152725	2073	2
5984	445	754	141937	876	471	101560	1358	575	140211	751	238	202512	559	135	152780	2037	2
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144371	477	195	101962	2411	141	202450	2680	172	142270	30	8	165176	326	71
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144432	996	211	131360	0	0	202513	195	195	142291	174	29	165186	357	84
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144525	2156	202	131368	24	30	101765	0	0	142308	179	46	165204	411	108
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171852	417	211	144917	736	207	134253	51	77	190355	131	40	094309	677	264
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152667	790	344	0869			151179	3833	0	143774	584	497	142145	491	104	106207	697	297
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170225	116	19	113027	769	286	183000	2145	20	161933	119	58	140625	154	78	120066	97	86
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132581	235	195	092391	297	229	145580	0	0	131963	2337	72	081000	2663	164	170183	90	25
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132614	283	248	092460	392	301	145650	31	19	142400	0	0	081200	2626	0	170299	109	25
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132705	462	416	092595	1103	497	145915	157	96	142419	137	118	103200	244	22	170985	227	15
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132742	573	479	092647	1666	497	150046	270	135	142425	210	164	104000	619	22	171099	227	15
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132793	814	541	092679	2128	470	150190	299	175	142430	296	211	110000	1565	23	172262	285	15
132811	974	552	0896			150276	352	195	142434	370	229	110900	1977	22	172707	310	15
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132861	1509	558	085411	26	9	150425	635	229	142440	603	264	113000	2816	22	173274	376	15
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163910	742	248	113153	0	0	075013	1820	0	0908			160634	2440	0	163606	2476	180
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172163	308	134	112178	5120	307	040900	2441	0	153665	2501	227	2103	2524	1055	2515	226	350	172163	308	134
172204	423	151	112235	5680	347	042351	2400	0	153682	2414	0	2117	2882	1130	75	254	350	172204	423	151
172261	624	182	112351	7320	380	044729	2393	0	153725	2358	0	2134	3400	1188	2652	320	428	172261	624	182
172300	805	200	112442	8800	346	0991			153810	2312	0	2145	3816	1189	2716	374	463	172300	805	200
172460	1853	236	112490	9630	311	044700	0		154200	2278	0	2155	4374	1135	55	428	478	172460	1853	236
172495	2161	237	031900	0	0	044311	24	25	154500	2272	0	1008	0	0	2828	556	493	172495	2161	237
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172754	4140	281	031928	148	165	044477	145	109	181801	0	0	64	20	53	59	1114	421	172754	4140	281
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103841	137	134	164004	127	156	065438	51	43	70047	5302	198	75	734	1200	4426	5002	104			
103874	163	148	164016	161	204	065490	73	77	0154	5596	206	81	894	1218	4583	5434	113			
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170012	33	21	113853	102	137	070378	1265	385	0689	1680	316	20	308	881	6030	1604	146			
170030	49	29	113863	134	169	070467	1580	365	0802	1710	335	30	392	991	6117	2536	136			
170048	68	38	113870	149	203	070561	1880	343	0911	1960	355	38	488	1068	6215	3556	128			
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170081	88	54	113892	270	282	071052	3387	276	1057	2280	375	54	970	1120	63	5416	137			
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170254	134	152	114021	1835	510	110945	232	235	1610	34	19	55	78	69	1020					
170287	144	183	114066	2563	523	110951	334	276	180	40	44	92	88	91	032200	0	0			
170324	160	218	114077	2790	516	110960	482	315	1759	158	78	5228	96	113	16	16	18			
170360	177	252	114112	3470	472	110969	561	348	1834	232	101	60	120	136	25	40	44			
170395	197	284	114125	3880	434	110979	1142	366	83	328	109	5304	130	167	37	64	72			
170431	219	319	114147	4370	398	113994	1828	388	2018	536	156	40	138	182	49	114	111			
170449	248	354	0983			111014	2305	426	2210	990	175	98	152	232	63	184	150			
170506	282	388	022300	0	0	111029	3069	465	2428	1592	180	5452	166	271	81	358	190			
170547	326	422	022310	28	35	111042	3560	480	2619	2116	187	5505	184	309	99	566	204			
170587	382	456	022319	92	81	111059	4130	538	2782	2518	205	63	194	349	2312	746	207			
170619	455	490	022326	105	135	111100	6040	596	2920	2834	223	5613	208	387	32	1046	204			
170676	559	524	022334	188	197	111111	6580	589	3076	3188	238	86	228	433	50	1340	201			
170720	710	558	022340	217	245	111140	7660	589	3253	3610	261	5730	248	460	72	1752	193			
170786	1024	576	022345	257	286	111160	8830	591	3407	3996	285	91	260	488	2426	2636	182			
170816	1115	575	022353	330	357	155700	0	0	1005			5872	298	546	2507	3960	178			
170816	1368	565	022368	504	485	155843	6	24	113200	0	0	0966	346	597	65	4864	189			
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1277	1506	218	3657	1842	60	60	260	387	100007	288	110	1052			29	1270	49
1666	1598	253	3700	2252	60	61	280	451	49	162	124	040903	0	0	55	1318	49
1818	1850	274	4100	2598	55	63	300	514	0102	436	160	08		12	86	1418	49
4063	1946	289	5151	3508	54	66	340	574	0201	632	156	13	8	137	1531	1616	49
4203	2110	301	5400	3714	55	65	380	634	81	794	171	18	110	196	79	1798	49
4463	2318	314	1031			68	420	717	0380	994	188	20	204	400	1175	1924	49
4662	2530	331	022051	0	0	50	460	796	0462	1158	203	24	314	505	1705	2314	49
4976	2820	349	56	14	20	51	500	846	0553	1364	219	28	454	619	1805	2710	49
5657	3284	364	58	20	61	53	600	910	0631	1502	233	31	702	679	21	2936	49
5795	3572	370	59	46	104	55	720	968	0730	1706	249	34	1022	712	1957	3278	49
110135	3980	372	61	77	170	57	880	989	0818	1904	263	37	1416	700	2036	3564	49
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1028			63	122	250				91	2306	282	1053			2200	4294	49
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41	20	43	67	264	388	2892	44	62	70	2874	315	76	106	78	90	5326	49
59	44	76	69	366	425	2934	56	66	75	2906	317	81	158	101	2629	5660	49
78	66	101	70	440	457	2993	64	100	86	2922	314	86	194	127	102795	5996	49
94	88	140	71	554	485	3021	8	122	1313	2958	306	95	268	170	3027	6374	49
0212	118	173	73	696	501	3058	14	149	40	2990	296	3604	398	202	3100	6680	49
23	136	195	75	886	518	3104	108	177	1347			15	566	250	3500	6880	49
38	164	220	76	1090	528	3162	128	202	063452	0	0	26	736	288	4800	7180	49
53	200	245	78	1452	533	3195	160	232	1855	14	16	37	892	323	54	6984	0
56	224	271	79	1668	528	3237	178	257	90	34	27	50	1126	365	4000	6910	0
82	276	300	82	2028	518	3284	212	283	3935	74	62	66	1458	401	104499	6892	0
0100	324	322	85	2576	504	3327	246	302	80	116	58	86	1850	432	4800	6876	0
12	384	346	88	2954	497	3390	316	325	4039	202	75	92	2042	452	5000	6870	0
14	444	370	90	3308	487	3451	404	342	4137	412	85	3727	2840	503	111000	6858	0
68	618	391	93	3684	475	3498	520	363	4259	730	82	62	3638	555	3000	6870	0
0412	964	410	1034			3543	714	377	4451	1236	81	91	4234	582	1060		0
72	1424	415	092000	0	0	3633	906	320	4589	1806	78	3806	4736	588	020500	0	0
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0620	2484	427	2102	40	71	3780	1250	323	1048			1054			0600	48	23
82	3174	421	12	56	110	1043			071200	0	0	070898	0	0	0900	100	23
0716	3988	408	22	71	150	049508	0	0	1857	36	4	5903	12	91	1500	150	23
0812		195	32	83	190	5694	22	13	1813	164	12	07	50	228	2510	190	23
1029			41	104	230	5734	64	30	1984	226	20	09	74	324	4000	246	23
153852	0	0	50	123	268	5806	128	60	2046	302	26	11	94	420	5500	292	23
56	30	27	60	141	307	67	176	75	2115	416	35	14	178	520	031500	346	23
58	70	90	69	164	367	98	244	100	66	492	41	16	252	603	4500	410	23
60	106	153	81	193	401	5950	314	115	2225	582	51	19	384	678	041500	504	23
62	126	212	95	227	418	100017	420	137	94	694	59	21	568	760	4500	568	23
63	140	264	2205	248	493	0313	634	156	2369	810	67	24	790	780	051000	630	23
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69	200	495	80	785	707	0803	2126	274	3300	3150	67	40	3036	837	130000	1494	23
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82	357	628	2302	1248	663	1045	2694	304	1049			54	5372	834	210130	2271	23
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1811	12	12	1508	3452	314	1508	3452	314	26	760	133	23	30	34	254221	2972	0
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2189	38	59	064581	0	0	064581	0	0	30	980	220	4159	128	34	255000	2974	0
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5142	216	328	45	70	129	45	70	129	40	2200	300	5300	362	34	1064		0
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5790	440	433	82	258	365	82	258	365	50	3720	276	0899	560	34	65	798	71
150176	690	472	94	324	432	94	324	432	1799	662	34	1799	662	34	76	986	71
0320	872	475	4705	458	478	4705	458	478	1030000	0	0	2599	732	34	84	1106	71
0397	988	463	12	540	509	12	540	509	3673	10	7	3599	824	34	90	1206	71
0495	1230	425	20	666	530	20	666	530	3505	24	22	4499	930	34	94	1244	71
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0648	1726	343	38	1066	541	38	1066	541	3609	74	54	1200	1106	34	1023	1582	71
0800	2020	317	55	1441	553	55	1441	553	3655	84	72	2999	1208	34	40	1722	71
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55	20	84	4410	1590	242	4410	1590	242	94	252	120	1499	1412	34	84	2170	71
58	40	165	4500	1658	244	4500	1658	244	3849	328	130	2600	1456	34	1106	2362	71
60	60	244	1038			1038			80	410	139	3600	1504	34	32	2576	71
62	80	322	170277	0	0	1045			3988	654	146	5000	1546	34	67	2882	71
64	100	401	84	4	33	104653	0	0	4000	944	148	170500	1610	34	1212	3254	71
65	120	476	95	20	79	55	0	0	99	1200	145	1500	1626	34	43	3496	71
67	150	551	1501	46	127	98	10	0	6199	1490	140	3500	1704	34	98	3910	71
69	170	627	00	74	171	4702	40	37	1051			5999	1788	34	1326	4204	71
70	190																

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
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30	334	202	90	602	71	54	292	237	63	486	237	22	214	170	62	300	691
34	464	258	120090	754	71	58	356	250	70	664	246	24	272	203	68	352	762
37	630	293	0175	880	71	62	428	256	80	888	250	36	356	250	75	452	839
42	758	334	0220	946	71	69	554	264	85	1040	249	42	478	259	81	632	872
46	1312	337	67	996	71	75	700	262	94	1300	244	48	510	280	85	782	880
49	1878	324	0174	1146	71	78	812	259	1816	1928	230	57	680	296	89	944	874
52	2046	306	0458	1246	71	82	914	252	32	2358	221	64	854	308	92	1134	860
57	2502	290	0525	1378	71	88	1066	243	65	2998	212	77	1146	302	95	1378	830
61	2868	281	0624	1480	71	92	1186	236	1087	0	0	93	1600	294	1097	0	0
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27	136	36	0965	1868	71	5700	6	12	07	66	91	115700	0	0	4404	10	48
32	250	61	1100	2058	71	03	58	65	10	106	157	5707	8	13	07	38	122
36	372	177	25	1988	0	06	112	108	13	150	213	11	64	31	11	64	230
39	472	236	75	1944	0	08	154	156	17	208	272	17	140	79	15	90	313
42	584	282	1300	1924	0	11	194	205	20	282	319	21	196	110	18	102	378
46	748	329	1073	0	0	14	238	252	22	358	356	25	248	137	20	126	451
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53	1212	399	93	58	23	20	368	354	29	646	417	32	350	195	27	166	612
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61	1804	436	4004	176	62	29	738	428	35	1054	420	41	526	272	33	228	779
65	2184	448	3111	364	71	32	944	425	38	1354	403	48	648	304	36	272	840
70	2508	458	98	600	81	36	1268	415	41	1714	382	55	898	342	39	324	929
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80	3534	466	3493	1384	90	43	1992	385	1048	0	0	65	1376	353	47	592	1038
90	4420	500	3689	1886	91	46	2184	368	045431	0	0	72	1696	347	50	758	1062
98	5036	543	3800	2208	91	1083	0	0	50	10	4	81	150	331	52	988	1068
1005	5130	570	3953	2618	91	114205	0	0	56	156	35	90	1614	319	56	1534	1088
14	6252	632	4100	3008	92	07	98	44	58	188	84	5801	3178	307	1098	0	0
20	6590	659	4212	3284	90	08	160	91	60	212	126	1093	0	0	020300	0	0
30	7508	691	1074	0	0	10	240	121	61	236	170	111230	0	0	07	20	48
38	8046	688	140705	0	0	11	230	170	62	268	213	36	12	40	11	66	119
41	8424	666	22	56	38	12	258	211	64	300	260	39	44	88	15	92	196
065420	0	0	40	6	118	13	284	250	66	354	335	42	74	142	19	114	283
50	40	1	50	310	158	14	304	292	68	406	400	47	138	242	21	134	361
55	124	32	62	488	200	15	340	331	69	458	450	50	218	313	25	158	432
60	200	72	76	788	220	17	404	395	72	578	536	52	252	366	28	172	508
65	266	110	83	998	222	20	566	458	74	696	587	56	440	421	31	198	590
69	338	152	95	1242	223	21	764	489	74	924	629	59	600	472	34	222	673
94	398	193	0812	1678	224	24	1024	489	1089	0	0	63	812	504	37	250	755
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38	1346	515	1076	0	0	020000	0	0	3752	730	71	1222	4552	459	58	808	1139
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72	2594	643	07	64	84	40	180	71	3830	1030	71	2600	2	1	1099	0	0
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191534	0	0	27	648	342	0300	1125	71	4497	1976	71	20	372	516	66	176	391
51	106	0	30	846	356	51	1320	71	4592	2100	71	21	538	577	68	144	482
92	416	43	32	1030	357	0450	1624	71	4692	2236	71	25	816	616	70	162	576
97	470	97	35	1226	354	0500	1908	71	4790	2326	71	27	1184	623	73	194	688
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28	980	361	169000	0	0	0725	2966	71	3000	3628	71	1095	0	0	84	312	1196
38	1146	433	04	26	60	69	3196	71	5120	3894	71	115800	0	0	86	344	1290
43	1264	472	07	82	180	0851	3635	71	9200	4174	71	13	50	82	88	380	1393
48	1392	510	12	190	322	0935	4122	71	114220	4174	71	17	60	122	91	418	1600
54	1552	547	16	528	438	1023	4558	71	5000	4376	71	20	74	163	94	490	1652
61	1774	586	20	1040	441	78	4870	71	207000	4554	71	24	88	200	97	630	1776
66	1964	605	24	1620	427	1109	5040	71	5000	4704	71	28	104	241	1100	0	0
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82	2638	626	31	2680	402	1300	5142	0	222200	5072	71	34	136	321	030320	8	27
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95	3298	616	1942	5130	0	1942	5130	0	010000	5560	71	40	160	399	030328	48	200
1704	3780	593	2700	5120	0	2700	5120	0	079800	6406	71	44	178	447	030337	74	278
14	4264	588	4607	30	30	3952	6346	0	080518	6356	0	47	198	484	030342	94	370
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040359	362	632	145000	7096	71	113705	36	13	193275	0	0	134812	98	173	164940	150	53
040365	404	707	155800	7596	71	113708	162	45	193299	44	9	134815	154	235	165011	218	72
040370	480	784	162500	7902	71	113710	214	77	193303	370	40	134820	216	296	165071	286	102
040377	540	854	173000	7956	71	113713	302	112	193304	652	77	134823	296	338	165134	376	112
040381	716	924	193000	8298	71	113715	398	152	193304	964	150	134827	416	376	165196	476	141
040392	950	996	220000	8696	71	113717	504	208	193310	1140	211	134830	556	410	165265	560	146
040400	1250	1037	240400	8916	71	113720	606	252	193313	1358	310	134833	670	439	165332	708	169
040406	1474	1042	261681	8930	71	113723	856	295	193315	1592	389	134837	814	442	165433	896	194
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042966	116	270	081280	10636	0	113766	6072	322	103200	516	71	142614	398	300	083484	190	61
042969	132	323	081375	10612	0	1110			103500	932	71	142617	618	380	083501	274	79
042971	166	392	081400	10580	0	120076	0	0	104000	2242	71	142620	946	423	083517	362	100
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112152	670	212	154836	776	234	173946	822	206	111600	9038	0	102100	1212	101	131265	366	266
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1307			152264	186	115	102200	900	346	031626	410	170	040091	124	161
103700	0	0	152270	286	155	102300	1210	337	031651	526	210	040108	158	190
103709	8	17	152277	468	196	102400	1584	313	031674	638	242	040125	204	222
103714	40	51	152282	644	218	1326			031700	792	270	040141	222	250
103720	84	115	152287	812	220	103002	0	0	031725	938	290	040160	304	280
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013126	2042	727	010000	0	0	013030	860	807	090500	800	347	1182	0	0	143009	72	128
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011523	56	88	010050	380	322	013552	38	37	100000	0	0	140012	410	510	143019	604	569
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011530	166	246	010057	586	479	013650	196	113	100150	152	128	140019	676	842	1391	0	0
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011539	326	510	010070	1332	789	013900	658	278	100300	408	310	081500	0	0	082850	88	48
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011548	628	738	010079	2412	794	032200	1900	321	100450	922	413	081650	138	102	083100	336	157
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011555	1262	831	1356			153000	0	0	1371	0	0	081700	208	143	083200	576	209
011557	1644	817	011500	0	0	153051	42	20	101500	0	0	081750	284	187	083300	864	244
011560	2054	782	011507	122	170	153111	166	72	101525	50	61	081800	366	222	083350	1062	255
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103116	138	153	1359			160055	694	290	141510	266	249	154750	908	355	101576	1050	523
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120011	82	190	1403			014300	5932	0	160859	4970	138	080238	9076	0
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080700	984	97	021297	202	97	031300	498	117	101602	354	97	090075	106	80
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022700	0		023000	1806	80	095100	1122	162	1418			011800	898	164
022718	96	162	034000	1844	80	102900	1304	162	014500		0	011900	1426	171
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113051	258	243	030100	464	139	125000	1680	162	104800	1000	227	031639	1176	850	103192	604	619
113056	320	294	030125	602	211	164100	1600	162	104900	1032	227	031643	1578	828	100214	712	660
113062	374	355	030140	694	248	213600	1760	162	105000	1050	227	031646	1816	800	100240	1016	690
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030038	472	468	024641	3066	467	145500	3424	203	151936	362	820	240850	926	489	010700	1308	310
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090023	434	467	100750	1560	400	134800	174	167	135033	198	295	041537	448	880	131825	830	470
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040344	1904	509	040136	2110	740	105000	1666	0	072400	520	97	0513	264	32
040354	2038	490	1493			125600	1666	0	122000	512	97	30	350	40
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041512	94	149	033047	194	150	38	2	84	1510			0437	756	146
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041518	178	312	033057	298	236	76	4	84	40	964	347	76	858	225
041521	216	397	033060	328	270	3100	5	84	45	92	150	0500	904	271
041526	300	567	033065	376	316	3200	8	84	52	132	226	20	942	311
041530	362	650	033068	414	351	3300	12	84	60	162	304	61	1044	391
041532	392	725	033071	462	397	3400	13	84	66	198	385	85	1116	430
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041539	592	911	033089	690	544	3700	17	84	80	264	540	58	1510	491
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041544	1082	1008	033119	1440	685	4113	20	84	91	368	685	79	1718	494
041548	1378	1000	033125	1681	681	4300	26	84	1600	428	773	88	1794	479
041549	1494	973	033132	2032	660	4500	26	84	08	516	841			
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030263	1210	523	090200	528	227	2200	484	459	1507					
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072100	438	97	072100	438	97	072100	438	97	072100	438	97	072100	438	97
107000	460	97	107000	460	97	107000	460	97	107000	460	97	107000	460	97
121800	460	97	121800	460	97	121800	460	97	121800	460	97	121800	460	97
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81	354	73	1250	1422	0	0600	1522	180	59	2338	172	55	474	209	21	20	29
0118	884	156	1124	1258	0	30	1736	175	63	2742	173	59	822	369	40	44	59
39	1140	231	112300	1238	0	1531	0	0	68	3072	173	61	1032	431	50	64	77
55	1286	317	1527			010005	0	0	73	3414	172	63	1888	313	60	88	92
69	1394	400	153000	0	0	30	142	17	78	3888	172	1545	0	0	70	114	109
80	1478	466	07	2	97	0100	502	29	82	4174	172	040000	0	0	80	142	126
93	1580	542	12	7	97	30	864	37	86	4496	172	0100	80	14	90	178	140
0208	1710	616	18	12	97	0200	1352	50	92	5032	171	71	510	79	4600	212	157
27	1942	692	21	10	97	30	1624	64	1111	6418	172	0200	690	102	20	294	180
38	2136	714	24	11	97	0300	2006	79	20	7062	175	24	858	122	31	146	194
42	2248	718	30	12	97	30	2358	91	28	7586	167	50	1076	136	41	404	204
42	2248	718	41	12	97	0400	2788	103	1538			76	1304	145	50	464	212
50	2500	710	51	14	97	50	3112	111	103223	0	0	0300	1534	146	70	612	225
55	2624	702	65	15	97	0500	3504	118	81	1834	90	24	1758	148	90	770	231
58	2796	690	3100	17	97	30	3906	121	84	2334	90	50	2026	151	4720	1020	235
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14	196	149	50	25	97	1532			91	4002	91	043208	0	0	1554		
19	286	222	3300	25	97	011002	0	0	94	4634	93	34	260	35	110000		58
24	382	310	3400	30	97	16	20	31	1539			46	596	76	09	4	58
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33	530	466	3700	38	97	42	166	150	51	84	0	65	1172	130	15	9	58
37	604	551	4000	44	97	52	278	191	0100	196	1	70	1352	131	21	10	58
41	630	630	4600	51	97	70	576	231	50	290	2	73	1522	131	41	12	58
45	770	691	5000	58	97	78	762	236	0200	372	2	78	1730	128	0100	16	58
49	876	772	160000	70	97	83	886	234	0300	534	15	82	1888	121	51	18	58
53	1042	836	1715	85	97	92	1160	223	40	758	37	1547	0	0	0200	22	58
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63	1680	903	170200	105	97	1600			0400	1174	60	13	24	37	0400	30	58
65	1866	892	1528			1533			50	1538	78	15	76	112	0500	34	58
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51	178	193	20	10	108	16	474	110	53	3052	134	1548	0	0	1600	59	58
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55	378	449	26	11	108	27	638	186	50	3782	160	24	8	10	2000	69	58
57	496	561	30	11	108	28	794	267	1540			27	12	30	2300	76	58
59	580	718	37	11	108	32	928	312	010006	0	0	32	30	71	2500	80	58
60	682	772	51	11	108	36	1160	348	58	56		38	60	131	2700	84	58
62	786	874	77	10	108	39	1500	347	69	122	1	43	96	151	2900	90	58
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2700	320	98	074400	94	108	1535			10	938	93	90	254	93	1556		
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090119	298	619	090018	136	347	030127	550	617	120020	348	158	27	640	1072	
090140	326	758	090021	184	532	030139	610	694	120026	404	235	28	724	1230	
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090020	64	80	110320	276	414	120300	930	441	26	238	365	80	1528	370	
090023	96	229	110351	368	520	1690			27	472					
090025	132	347	110380	496	622	120000	0	0	31	364	617	1732			
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090034	298	940	1669			120035	294	347	44	206	505	21	132	234	
090036	346	1053	110000	0	0	120037	352	400	69	272	505	26	200	317	
090038	388	1228	110030	126	13	120043	558	467	99	340	505	31	280	392	
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090016	22	55	110583	1720	750	120021	104	240	1000	2448	505	1733			
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013000	639	32	102200	7414	15	50	1138	400	1765			48	186	1433	61	1020	1048
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022500	1663	32	121200	8298	15	50	1590	507	80	404	328	1770	0	0	78	1800	1205
RESET DIALS			130400	8762	15	0500	1894	543	90	424	328	010000	0	0	85	2320	1284
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067000	2168	32	136500	12404	0	1758			0325	638	328	0198	208	278	25	125	102
071000	2445	32	137000	12314	0	0000			0425	684	328	0299	371	450	34	246	197
RESET DIALS			143000	12260	0	0100	36	10	0525	726	328	0367	482	572	42	358	300
092700	0	32	1749			50	202	52	0625	780	328	0324	633	693	51	596	467
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0900	11	15	0223	140	165	65	540	997	0640	840	604	41	1030	658	08	104	273
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5400	29	15	0500	480	413	85	980	1421	50	1308	720	74	2410	890	18	317	867
012400	38	15	0551	600	440	88	1110	1450	1026	1500	720	38	2803	885	21	398	1004
015400	46	15	0600	740	460	92	1430	1463	76	1720	720	42	2900	874	23	437	1152
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092300	126	15	0800	1170	395	59	180	195	0400	540	170	94	3395	324	37	1090	2023
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RESET DIALS			0900	1322	417	72	324	432	0600	1060	245	70	4145	694	41	1570	2172
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130800	20	15	1050	1780	452	87	560	775	0950	2310	388	39	5220	1062	05	52	65
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224700	108	15	0000			98	740	982	1200	3250	450	78	5130	1276	36	229	265
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225300	106	0	0400	200	220	0111	1060	1205	1375	3880	480	04155	5680	1363	40	375	505
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1748			0600	518	317	1764			75	4230	496	22	6020	1330	46	584	830
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1200	1400	1018	18	165	148	0307	620	197	090031	920	1772	030300	712	46	000597	2294	73
1300	1400	1012	25	372	231	0400	920	395	090049	1086	1918	030350	1166	44	1840		
1400	1800	1004	30	556	276	0500	1200	573	090095	1256	1989	030500	1840	30	000000	0	0
1700	1900	1004	34	175	310	0600	1460	788	090098	1466	2008	030600	2100	15	000015	12	15
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0225	88	23	1799			1000	2260	1167	120015	138	209	000100	262	16	000077	614	161
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0325	326	64	13	0	18	1200	2660	1148	120034	336	543	000200	342	16	000129	2046	156
0400	594	53	17	58	76	1300	3620		120040	396	678	000230	386	16	000147	2538	150
0500	964	70	24	192	147	1400			120043	470	875	000300	416	16	1831		
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0438	784	288	58	1298	511	07	30	44	0450	2630	269				50	162	428	
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87	1376	293	17	138	232	17	272	390	1032	7412	367				00	480	747	
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0307	562	117	49	1576	533	33	1616	747	0100	146	157				19	316	457	
0587	1138	271	52	1876	532	36	2310	725	0400	367	347				22	496	581	
0702	1462	336	2322	0	0	08	46	44	0600	617	420				25	826	640	
88	1642	368	12	126	109	08	10	5	0700	420	419				27	1208	607	
0957	2294	378	15	168	153	0116	44	37	35	419								
2313	0	0	20	246	236	0210	174	118	2350	0	0				00	10	49	
120000	0	0	25	334	318	0300	382	173	120000	0	0				15	46	158	
77	66	32	28	396	393	0410	810	197	14	4	26				17	76	263	
76	160	89	33	460	469	0510	124	199	21	28	76				19	106	358	
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0401	504	235	46	870	695	0700	420	367	34	86	157				25	240	581	
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2314	0	0	54	1492	697	0900	444	233	60	288	316				30	460	763	
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78	378	276	25	334	318	0700	1454	258	24	52	42				19	286	317	
0249	616	309	28	396	393	0800	1454	258	45	226	147				23	450	464	
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2315	0	0	41	650	624	0900	1454	258	73	566	273				33	1014	770	
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99	120	160	12	126	109	1550	1454	258	57	310	235							
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06	2	24	15	280	463	0100	48	78	13	28	107	0118	92	101	82	760	394
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12	58	112	19	570	503	0210	156	175	22	96	313	0205	292	149	0131	1806	671
14	96	149	20	960	514	0300	258	254	25	126	196	0300	612	153	69	2670	547
17	162	190	23	1374	642	0400	380	327	30	174	477	0450	890	144	91	3168	583
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27	438	316	120000	0	0	50	956	416	51	914	814	58	42	27	2463	0	0
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2398	0	0	50	494	395	0100	42	76	12	36	74	0300	630	129	60	92	116
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17	196	237	120000	0	0	2422	0	0	60	594	988	91	44	83	29	1186	363
19	268	276	18	24	71	120000	0	0	64	1378	966	0144	114	136	33	1298	337
22	358	319	22	56	153	0152	96	39	2432	0	0	0200	236	159	2464	0	0
26	524	357	26	86	234	0250	266	90	120000	0	0	55	406	172	120000	0	0
31	644	385	33	150	394	0300	366	117	24	2	39	0300	566	173	09	37	20
35	1098	385	40	232	545	0400	504	182	28	22	123	50	780	169	13	74	78
39	1466	382	43	276	620	0500	664	247	33	58	238	2455	0	0	17	146	154
43	1720	379	50	422	772	0700	1108	341	40	110	393	120000	0	0	21	210	255
59	3070	390	60	886	883	0759	1322	336	47	200	549	38	20	21	25	268	314
63	3362	394	63	1224	853	2423	0	0	53	360	697	58	36	38	29	164	394
70	3912	405	66	1540	822	120000	0	0	59	588	772	0100	20	69	33	424	470
79	4502	420	7411	0	0	32	0	17	64	952	793	53	166	103	38	540	546
85	479	431	120000	0	0	50	10	46	69	1436	749	0200	266	131	43	740	618
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11	6744	479	30	1400	1300	50	658	344	10	50	231	75	842	150	2465	0	0
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15	192	187	10	186	394	0100	36	36	22	388	988	65	178	133	20	188	231
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66	3804	302	25	1030	1245	27	1174	458	10	68	194	0551	2428	318	35	1090	594
82	5018	311	27	1582	1132	2425	0	0	12	146	389	0700	3368	319	57	1148	587
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20	7686	356	05	30	46	0100	142	70	2435	0	0	55	62	55	120000	0	0
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11	90	192	22	648	972	2426	0	0	18	446	774	120000	0	0	37	352	400
13	164	283	23	850	1080	120000	0	0	20	602	907	29	0	13	45	752	469
14	278	355	26	1170	1129	24	0	13	24	1020	1014	50	20	53	50	1114	470
2389	0	0	2416	0	0	82	74	123	2436	0	0	86	86	114	54	1532	455
170000	0	0	120000	0	0	0118	120	197	120000	0	0	0157	306	210	2467	0	0
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19	2036	328	22	104	250	0250	270	423	20	114	331	51	774	283	26	16	103
22	2634	348	28	166	463	0300	746	456	23	166	438	0334	1356	295	29	104	328
25	3280	426	31	216	617	27	952	455	27	258	620	73	1652	299	32	196	476
28	3932	372	34	270	768	36	1036	453	31	386	765	0550	2382	313	35	376	625
32	4680	385	37	344	904	2427	0	0	34	538	859	64	3056	308	37	720	713
35	5220	394	40	456	1057	120000	0	0	38	958	924	2459	0	0	39	1246	703
39	5950	421	46	818	1204	11	4	33	40	1528	869	120000	0	0	42	1830	676
43	7008	441	47	1214	1191	19	20	79	2437	0	0	0182	38	29	2468	0	0
45	7526	464	52	1532	1162	32	42	164	120000	0	0	0200	50	54	120000	0	0
2391	0	0	53	98	237	43	98	237	11	24	56	50	142	138	06	22	53
120000	0	0	55	166	316	55	166	316	13	68	153	0300	304	208	08	72	170
07	0	0	68	248	397	68	248	397	17	140	324	50	400	229	11	341	341
10	28	24	83	380	468	83	380	468	21	210	476	73	778	226	13	266	448
14	152	79	103	626	549	103	626	549	25	318	628	2460	0	0	16	508	573
17	216	149	23	1094	576	23	1094	576	29	498	772	120000	0	0	18	696	627
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12	250	316	0101	294	84	0014	806	297	2521			0068	124	471	0013	0	29
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22	806	529	0200	868	157	0019	1622	315	0140	6	41	0107	254	772	0021	12	231
27	1208	523	0300	1624	186	0022	2502	315	5353	18	77	0127	338	911	0026	204	394
29	1598	499	0451	2652	220	0025	3056	293	8282	42	160	0148	476	1062	0030	270	537
2571			0734	4412	212	2502			0256	90	356	0170	656	1205	0035	379	772
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27	8	17	120000	0	0	0006	8	25	0356	184	625	0135	1626	1437	0041	516	1055
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37	234	315	51	534	154	0016	572	315	0658	920	1228	0009	14	35	0051	1016	1635
38	288	403	72	1026	162	1418	752	356	0765	1494	1277	0016	144	375	0051	1238	1775
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56	1770	843	30	234	76	2503			5858	98	79	0030	786	1349	0080	3270	2461
2472			44	430	113	120000	0	0	0170	284	321	0031	1174	1484	0084	3756	2530
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06	12	26	1292	172		0021	54	147	3370	742	736	0038	2420	1508	2538		
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21	7	535	2495			0028	618	385	0700	1954	1205	0028	18	89	0030	68	232
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68	56	17	57	1328	446	0506	242	432	0135	824	777	0044	2182	1833	0310	506	128
0100	116	33	64	1920	443	0638	346	564	0160	1100	918	2534			0387	762	136
39	204	47	69	2746	438	0700	394	628	0192	1510	1062	120000	0	0	0526	1244	148
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0600	822	78	08	6	33	0957	634	646	0300	2714	1333	0020	94	232	0970	2544	168
0700	2858	89	12	66	111	1139	994	953	0305	2818	1323	0023	118	310	2534		
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67	3606	94	20	228	239	1390	1570	1012	120000	0	0	0036	212	623	0035	24	34
2488			26	432	316	1484	1900	1004	0028	52	72	0042	250	772	0060	76	73
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50	20	13	33	910	360	2520			0067	342	321	0062	520	1270	0118	230	160
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0200	284	102	2499			0165	66	71	0137	794	780	0085	1506	1623	0250	998	243
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1100	1962	159	22	2067	387	1538	1800	1022	0328	2636	1873	0084	402	913	0209	660	237
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2558	0	0	0039	2004	890	0505	1156	1004	120000	0	0	0100	40	508	0182	318	1263
120000	0	0	0042	2628	850	0519	1292	996	0021	67	147	0400	12	508	0205	414	1205
0037	174	150	2567	0	0	2589	0	0	0025	122	394	2900	40	508	0241	446	1420
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0074	614	319	0019	16	90	0040	52	31	0031	216	792	025900	142	508	0274	756	1540
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0021	58	72	0016	100	148	0018	22	77	0017	20	88	860900	1840	0	0253	346	900
0035	90	160	0020	148	315	0037	50	157	0019	42	183	2628	0	0	0202	710	1277
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0061	2064	647	2587	0	0	0041	252	837	0068	462	1627	0400	774	657	0014	64	514
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0041	138	133	0313	264	167	0167	1136	887	0013	344	316	0077	124	115	0008	94	154
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0045	180	1103	0582	788	317	0000	0	0	0021	617	622	0150	576	150	0012	224	116
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0059	538	2200	0000	0	0	0030	120	549	0037	1582	1094	0013	40	18	0034	1394	645
0062	662	2349	0145	10	21	0036	176	703	0040	2958	787	0010	150	75	0037	1796	633
0065	908	2530	0257	132	112	0041	232	842	2672	0	0	0041	240	111	2707	0	0
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0010	4	54	0637	656	397	0064	862	1276	0028	168	392	0100	1162	261	0009	80	238
0013	26	146	0767	1344	455	0073	1376	1305	0114	1470	259	0012	1470	259	0013	184	398
0015	58	250	0873	1356	453	2664	0	0	0012	260	621	2697	0	0	0018	376	543
0018	84	363	2654	0	0	0000	0	0	0036	304	767	0000	0	0	0021	616	626
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0028	190	845	0137	54	97	0018	36	230	0045	540	1206	0029	48	74	0035	1274	640
0035	278	1135	0322	202	257	0025	68	394	0048	728	1351	0036	68	114	2722	0	0
0041	372	1347	0428	344	329	0035	126	628	0053	1262	1443	0044	122	153	0000	0	0
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0055	982	1917	0770	1368	396	0050	300	938	2673	0	0	0085	826	234	0005	28	35
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2646	0	0	2655	0	0	0068	960	1307	0008	28	94	2698	0	0	0152	76	89
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0016	98	548	0252	196	139	0010	14	86	0023	228	759	0024	50	116	0400	284	323
0030	168	907	0319	716	430	0017	28	231	0027	286	917	0037	80	156	0452	326	365
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0016	14	72	0336	574	486	0077	1390	1383	0067	72	36	0014	82	193	1300	1620	787
0021	42	316	0439	1102	590	0082	1846	1375	0249	546	80	0019	154	274	1400	1880	793
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0031	164	793	0497	1514	587	0000	0	0	0331	832	79	0032	528	431	2723	0	0
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0700	442	0	2658	0	0	0035	1064	1463	0000	0	0	0041	1142	424	0407	400	315
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810000	442	0	2659	0	0	0030	430	1133	0000	0	0	0044	1440	440	0637	650	363
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811000	0	0	0018	14	33	0038	1322	1455	0080	108	41	0000	0	0	1200	1798	553
2649	0	0	0025	28	77	0039	1774	1471	0121	196	55	0007	28	103	1422	2398	545
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0119	144 152	0037	2640 1554	0261	730 102	0011	136 308	0510	684 261	27	64 237						
0179	242 276	0038	3140 1520	0415	1402 101	0014	302 396	0752	1134 362	32	122 356						
0251	522 401	2754	0000 0 0	0437	2046 97	0017	536 466	1000	1716 388	38	276 471						
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0555	1490 790	0003	17 33	0000	0 0	0023	1380 580	55	1886 384	58	916 767						
0749	2548 995	0007	152 229	0029	62 23	0026	1782 589	2812	000000 0 0	66	1404 841						
0893	3620 1079	0010	234 387	0061	202 47	0028	2282 589	0164	72 69	73	1920 877						
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2767	0000	0 0	0017	414 772	0191	428 89	0034	605 697	0646	496 290	82	2644 870					
0016	36 36	0020	506 978	0200	566 115	0042	697 697	0807	804 340	000000	0 0						
0020	72 73	0025	680 1277	0305	1634 137	0047	4102 765	0875	970 348	21	18 50						
0044	140 157	0029	918 1507	0400	2260 193	0049	4496 801	1002	1334 344	26	52 111						
0068	264 120	0031	1118 1620	0582	3538 199	0051	4478 852	1202	1940 328	35	110 243						
0089	424 472	0037	1756 1778	0671	4116 238	0054	5407 903	2813	0 0	42	202 197						
0120	644 621	0038	2148 1883	0700	5028 294	2787	0000 0 0	2813	0 0	59	310 542						
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0925	650	1957	15	214	427	23	340	1350	24	40	114	33	58	173	
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80	1542	1436	0144	792	47	000000	0	0	3193			04	14	78	34	80	119
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19	226	696	0156	56	78	0156	56	78	67	212	1253	77	278	469	22	144	41
22	302	839	0329	144	238	0329	144	238	71	832	1150	0107	490	622	28	210	17
26	408	983	0510	262	399	0510	262	399	000000	0	0	17	692	642	41	474	94
32	690	1204	0627	422	463	0627	422	463	09	70	73	25	952	622	62	1044	87
36	896	1283	0650	520	450	0650	520	450	14	110	154	000000	0	0	33	250	50
39	1288	1348	000000	0	0	3188			19	24	76	08	4	15	47	538	99
41	1672	1370	000000	0	0	0133	82	21	27	192	396	27	46	119	68	1120	94
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08	74	159	0674	518	359	48	1174	360	59	258	1132	67	180	398	15	84	35
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70	1138	115	44	200	158	42	12	36	40	274	113	15	296	774	40	40	157		
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29	294	67	28	1400	443	0252	168	244	41	888	702	000000	0	0	31	426	772		
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23	18	72	90	1716	522	99	116	100	12	116	320	51	34	23	07	52	111		
37	48	157	97	2750	583	0131	150	154	16	166	475	60	48	37	10	90	238		
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TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS			
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31	624	1396	83	1776	717	19	40	75	35	4394	360	000074	1040	1125	SEE NOTES 3,5		
33	836	1410	3361			29	86	119	85	5494	434	000098	1440	1569	000006	520	309
35	1192	1390	000000	0	0	37	144	160	0317	6140	471	000182	3700	2837	000010	1940	919
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07	72	152	37	62	161	0117	1456	356	000000	0	0	3407			000022	4870	2377
09	178	321	54	184	277	57	2392	386	17	34	40	SEE NOTES 3,5			000028	5600	3550
12	266	375	80	266	433	66	2614	379	24	76	75	000023	60	253	000033	6470	4716
16	388	487	34	866	530	3386			44	232	164	000031	80	396	000040	7300	6260
20	550	921	0170	1456	761	000000	0	0	66	546	237	000050	280	776	000047	8380	7715
23	758	1159	76	1594	757	11	40	36	92	1056	275	000074	580	1244	000052	9740	8833
28	1126	1348	3366			23	154	78	0261	2612	305	000091	800	1577	000057	11880	9559
31	1650	1410	000000	0	0	39	364	118	0270	2860	301	000134	1320	2377	000061	14200	9618
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02	0	41	42	146	191	11	40	36	25	252	57	000248	3880	4354	SEE NOTES 3,5		
06	22	160	60	212	325	23	154	78	37	478	80	000287	5760	4716	001006	500	1505
10	120	396	87	286	475	75	3176	287	53	770	164	000309	7200	4731	000008	780	2448
13	210	619	0142	1110	670	94	3214	284	87	1126	242	000316	7740	4716	000011	1280	4279
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19	430	913	81	2080	686	17	90	27	71	2952	302	SEE NOTES 3,5			000018	3670	6268
23	574	1163	3367			41	304	80	3398			000027	120	158	000023	7580	7459
26	740	1275	000000	0	0	69	616	158	000000	0	0	000064	460	760	3417		
30	1046	1404	13	10	40	0170	1636	192	21	198	39	000088	760	1149	SEE NOTES 3,5		
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3356			42	160	168	0238	3970	236	55	500	156	000157	1780	2377	000015	800	4716
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10	0	20	0101	1030	357	000000	0	0	0109	1032	372	000252	3740	3977	000021	1800	7730
15	4	53	47	2116	392	23	78	81	38	1486	432	000319	6520	4640	000024	2480	9196
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28	40	116	70	2636	387	42	224	157	98	2856	451	000359	9360	4655	000031	4500	12146
35	80	158	3366			65	570	236	3409			3409			000035	7280	13455
47	100	234	000000	0	0	0100	1458	244	000000	0	0	SEE NOTES 3,5			000037	9840	13273
60	156	321	15	62	23	59	2944	215	32	82	42	000007	0	221	3418		
74	256	399	38	356	81	3389			51	260	118	000018	140	752	SEE NOTES 3,5		
91	424	469	56	578	133	000000	0	0	69	424	204	000030	360	1545	000014	100	491
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97	2132	768	94	3226	342	62	384	244	0193	2790	334	000071	2040	4716	000029	2140	6976
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3357			0100	864	365	0100	864	365	000000	0	0	000106	6540	6110	000037	4800	10692
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26	20	25	71	2680	383	3390			000045	252	160	3410			090041	8620	11942
36	46	78	3390			10	32	43	000074	766	226	SEE NOTES 3,5			000043	12000	11622
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77	410	295	10	32	43	40	256	157	000163	2796	277	000005	720	206	000002	0	475
0115	882	433	20	76	74	68	760	219	000220	2960	316	000012	820	546	000005	160	1568
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72	2184	479	15	70	36	0131	2278	209	3401			000051	4220	7623	000014	1880	7692
3358			30	216	75	3391			SEE NOTES 3,5			000069	6340	3376	000017	2480	5944
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16	64	20	0198	1058	290	10	12	25	000052	20200	380	000101	12020	4151	000021	4540	11513
32	288	49	0277	1580	330	29	56	113	000088	20360	737	000121	16620	4286	000023	5980	12509
45	462	79	44	1972	333	45	182	197	000175	21080	1537	000130	19180	4226	000025	8940	12902
70	788	158	3369			44	274	237	000230	21500	1997	3411			3420		
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55	1508	577	18	110	32	90	902	316	000431	25480	3027	000019	260	792	000006	140	150
95	1798	735	32	154	53	0123	1656	335	3402			000031	520	1569	000033	580	1252
0213	2110	844	46	534	78	53	2436	330	SEE NOTES 3,5			000043	880	2377	000037	1300	3185
46	2666	903	72	896	139	60	2680	324	000047	340	249	000054	1380	3185	000040	2580	5514
92	2862	897	97	1182	214	3392			000049	560	459	000065	2040	3962	3421		
3359			0143	1960	297	000000	0	0	000114	1040	808	000084	3608	5092	SEE NOTES 3,5		
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33	170	120	0300	5554	360	0100	1540	190	000481	8500	2765	SEE NOTES 3,5			000011	1780	5469
40	198	155	14	5904	356	18	1886	187	3403			000012	60	356	3422		
64	320	315	3370			54	2820	202	SEE NOTES 3,5			000019	320	713	SEE NOTES 3,5		
0103	568	520	000000	0	0	67	3186	197	000057	640	142	000026	580	1117	000014	0	213
34	884	664	19	58	67	000000	0	0	000097	1420	380	000044	1240	2345	000017	400	1561
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77	1604	795	41	204	162	37	148	153	3404			000067	2480	3970	000023	3940	4399
82	1744	787	58	376	241	56	360	236	SEE NOTES 3,5			000078	3320	4716	3430		
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TIME STRAIN STRS 000037 5500 6223 000041 8200 6569 000044 11160 6664 3440 SEE NOTES 3,5 000021 0 134 000041 20 380 000063 180 618 000078 200 768 000103 340 990 000122 440 1180 000160 760 1569 000202 1120 1989 000241 1560 2377 000282 1960 2773 000320 2420 3170 000433 4040 3967 000604 7720 4851 000821 14880 5100 000951 16180 5085 3441 SEE NOTES 3,5 000042 280 150 000084 480 380 000080 880 776 000152 1280 1180 000200 1760 1672 000350 3280 3217 000467 4780 4339 000560 6700 5115 000664 8200 5891 000794 11320 6607 000892 14140 6976 001030 18880 7157 001061 20060 7127 3442 SEE NOTES 3,5 000020 220 158 000044 500 396 000063 700 610 000082 920 792 000123 1420 1172 000160 1960 1585 000338 5020 3320 000474 9360 4196 000691 16640 5092 000938 26740 5454 3443 SEE NOTES 3,5 000012 160 166 000042 400 380 000065 620 634 000078 800 760 000120 1220 1180 000160 1680 1600 000293 3560 2987 000474 8300 4022 000761 20580 4022 000777 21400 3985 3444 SEE NOTES 3,5 000037 280 301 000054 440 546 000065 600 776 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686011796 0202 884011920 0213 1438011796 3502 SEE NOTES 3,5 12 160 150 16 260 348 23 400 729 30 640 1117 38 840 1521 45 1240 2369 64 1520 3170 99 2620 4223 0121 3660 6260 0145 4720 7730 0169 9760 9159 3503 SEE NOTES 3,5
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SEE NOTES 3,5			000022	200	760	000220	3160	3233	SEE NOTES 3,5			000040	4560	1014	SEE NOTES 3,5		
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000165	33380	6976	000146	9140	7436	000055	3560	1997	000020	7040	9215	000049	4580	1299	000006	260	475
000176	36380	6916	000159	12680	7346	000065	4640	2377	000722	11280	9655	000056	6140	1355	000006	1120	1585
3609			3616			000088	8160	3185	3646			3676			000010	2480	2528
SEE NOTES 3,5			SEE NOTES 3,5			000124	14620	3637	SEE NOTES 3,5			SEE NOTES 3,5			000013	5220	3170
000011	200	336	000018	280	752	000131	16420	3558	000003	520	570	000009	160	134	000015	9220	3320
000010	360	792	000031	500	1521	3637			000005	2260	1204	000016	540	356	000018	15700	3138
000031	700	1545	000044	860	2393	SEE NOTES 3,5			000007	5440	1569	000023	1040	570	3687		
000039	980	2052	000054	1180	3170	000008	80	206	000009	10160	1347	000028	1680	729	SEE NOTES 3,5		
000057	1620	3185	000076	1940	4716	000011	160	396	000010	24000	1569	000037	3100	887	000004	160	317
000069		3962	000100	2740	6238	000018	660	729	000019	29600	1743	000048	5400	931	000006	980	1204
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000133	8700	6811	000279	12600	9729	000047	7720	2377	000036	58840	2559	SEE NOTES 3,5			000014	13520	2536
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SEE NOTES 3,5			000012	260	364	000091	25200	4716	SEE NOTES 3,5			000012	1540	1180	SEE NOTES 3,5		
000012	200	372	000021	440	760	000126	30600	5492	000002	0	467	000016	2440	1569	000004	0	95
000019	380	752	000030	740	1165	000147	35740	5605	000004	400	1291	000020	4400	1973	000006	660	776
000027	560	1141	000037	1120	1545	000158	39140	5484	000007	7960	2314	000026	8040	2155	000008	1360	1204
000034	780	1585	000052	1960	2777	3638			3664			000032	12820	2084	000011	3000	1909
000047	1120	2377	000067	2900	3178	SEE NOTES 3,5			SEE NOTES 3,5			000036	16360	1989	000016	7600	3314
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000069	1940	3977	000122	9840	5138	000013	300	380	000049	240	237	SEE NOTES 3,5			3706		
000081	2480	4723	000157	17080	5575	000021	640	752	000067	640	388	000003	40	39	SEE NOTES 3,5		
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000149	9340	7804	000014	380	309	3639			3665			000023	6240	2266	0260	7820	1751
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3611			000034	1520	1172	000011	70	221	000021	100	71	000031	11380	2219	3707		
SEE NOTES 3,5			000042	1780	1585	000013	120	372	000041	380	243	3679			SEE NOTES 3,5		
000036	20	213	000050	2360	1973	000021	260	776	000057	920	380	SEE NOTES 3,5			24	260	71
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000082	1060	3170	000176	20020	5929	000081	4400	3962	000130	3120	626	000026	11220	1585	0326	8200	2314
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SEE NOTES 3,5			000050	1440	2377	000018	1940	2425	000020	400	71	000019	6840	1450	0106	1400	1165
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000131	11640	5627	SEE NOTES 3,5			000012	640	1149	000047	1000	364	000038	5920	2536	34	340	134</

TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS	TIME	STRAIN	STRS
0353	18100	3067	26	3000	4022	17	2420	2640	07	1960	626	66	3940	2615
0365	20760	3051	34	5560	5484	21	2820	3185	09	2200	776	72	4600	2765
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62	700	1157	08	660	1149	11	2640	1909	3739			SEE NOTES 3,5		
83	1220	1553	11	1060	1545	14	3500	3170	SEE NOTES 3,5			09	200	134
0109	432	1965	17	1280	2139	19	5180	4766	20	180	158	14	480	356
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0278	12740	2971	SEE NOTES 3,5			30	16120	7120	53	800	776	40	2020	1921
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SEE NOTES 3,5			30	3120	4716	3737			0239	6240	1685	0138	13780	4904
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SEE NOTES 3,5			15	820	2385	0600	16680	4271	14	4580	3566			
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3717			07	380	1521	3770			15	4780	5130			
SEE NOTES 3,5			09	940	2684	3771			18	7400	5936			
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0153	27000	3693	14	4240	4791	3794			SEE NOTES 3,5					
3719			18	6500	6260	3795			11	0	134			
SEE NOTES 3,5			20	8880	7067	3796			17	60	372			
03	200	317	3730			3797			24</					

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Security Classification

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11. SUPPLEMENTARY NOTES	12. SPONSORING MILITARY ACTIVITY Office of Naval Research Arctic Project	
13. ABSTRACT <p>This report contains the results from a study of the mechanical and structural properties of sea ice; the study commenced in 1958 and was completed in late 1965. Most of the experimental work is based upon stress-strain tests in both direct compression and direct tension. Approximately 3800 of these tests were made.</p> <p>Those parameters anticipated to have significant effect upon strength were measured: temperature, salinity, rate of loading, crystal size, crystallographic orientation, history of the ice and depth in the ice sheet. All of these are found to be significant except that the history factor itself tended to be determined by the other parameters.</p> <p>The analysis was accomplished primarily by testing models by linear multiple regression. The models selected yield good results with multiple correlation coefficients between 0.70 and 0.98 over a range of petrofabric types.</p> <p>Additional work accomplished in conjunction with construction of offshore oil drilling platforms had provided significant information concerning oscillatory failure of sea ice in compression and strength reduction at very high load rates. The ice failure force oscillation is an ice property and is not primarily a function of the response of the structure. The magnitude of oscillation is large and at a frequency in the range of most space frame structures. The failing ice may cause forced resonant vibration in structures, and the forces are large enough to resonantly vibrate structure weighing several thousand tons.</p>		

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14 KEY WORDS	LINK A		LINK B		LINK C	
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Ice						
Sea Ice						
Ice Strength						
Ice Properties						

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