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HSRI TWO-DIMENSIONAL CRASH VICTIM
SIMULATOR: ANALYSIS, VERIFICATION, AND
USERS' MANUAL. REVISION NO. 1

D. H. Robbins, et al

Michigan University

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AND USERS' MANUAL
Revision No. 1**

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16 Abstract <p>→ This report deals with the development and use of mathematical models for the simulation of automobile occupant kinematics dynamics in the event of a collision. This model was developed as a tool to study advanced concepts and designs of seat-restraint systems from the viewpoint of occupant protection. After a discussion of the state-of-the-art of mathematical modeling of the crash victim, an analytical description of the HSRI Two-Dimensional Crash Victim Simulator is presented. This model consists of a segmented, eight-mass dynamic model of a human interacting with the interior of a vehicle in a symmetric frontal or rear crash. Pedestrian-vehicle interactions can also be considered. The degree to which predictions of the model agree with experimental impact sled test data is presented followed by a detailed Users' Manual for those individuals desiring to exercise the model. Sample data sets and computer output are included. A description of the program including detailed subroutine flow diagrams concludes the report with a program source listing included, as an appendix.</p> <p style="text-align: center;">↑</p>		
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I. INTRODUCTION

This report deals with the development and use of a mathematical model for the simulation of automobile occupant kinematics in two dimensions in event of a collision. The model was developed as a tool to study advanced concepts and designs of seat restraint systems from the viewpoint of occupant protection.

A schematic for the two-dimensional model is shown in Figure 1. The three parts of the model are the occupant, the vehicle, and the deceleration profile. The occupant is represented by eight mass elements located in the head, upper torso, lower torso, upper leg, lower leg, upper arm, and lower arm. Attached to the various body elements are geometric surfaces serving to outline the body in order that contact between the occupant and the interior or exterior of a vehicle can be predicted. The vehicle is represented by a series of planar contact surfaces which can be arranged to represent either a vehicle interior for occupant kinematics studies or the exterior for pedestrian studies. Belt restraints are included in the model if their use is desired. Forces are applied to the body of the occupant whenever interaction is sensed between the occupant and the vehicle. In order to produce occupant motions, a front-end or rear-end deceleration is applied to the vehicle and the resulting occupant motions listed as computer program output.

In addition to the analytical description of the model in Part II, a Users' Guide is included as Part IV of this report. Sections are included describing preparation of input data decks and the options available in studying the output produced by the computer program. The techniques which can be used in operating the model at a teletype terminal remote from The University of Michigan are described in a Teletype Users' Guide. Documentation of the program includes an overall program description, subroutine descriptions and flow diagrams, and a complete symbol dictionary.

The comparison of the predictions of the model with experimental

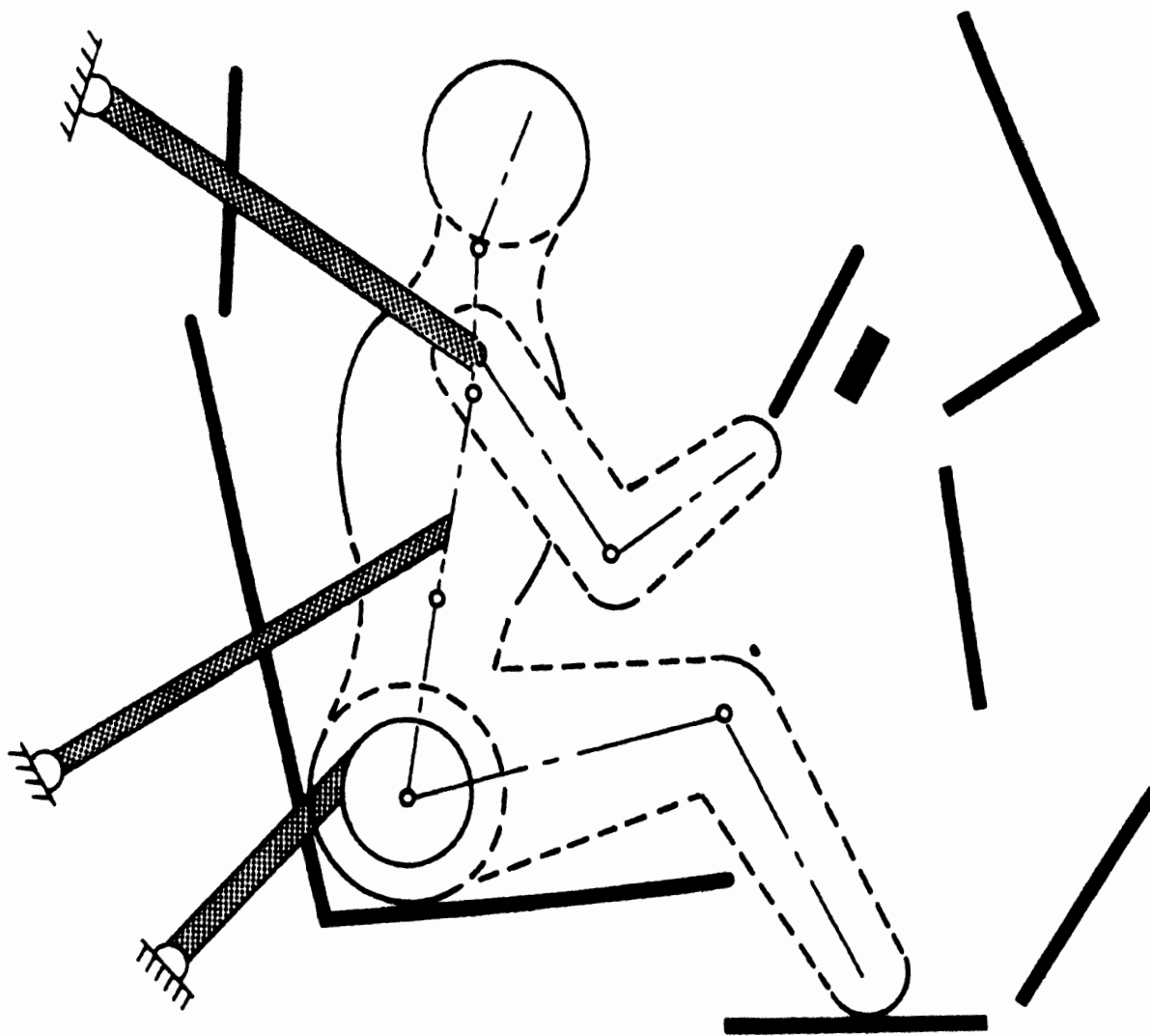


Figure 1. Schematic of mathematical model showing occupant, possible contact surfaces, seat, and restraint system.

impact sled tests is the subject of Part III of the report. The complex problem of gathering a set of input data describing the occupant and the vehicle is discussed and the techniques by which this is carried out are described. The equally difficult task of obtaining appropriate experimental data is also considered. Comparisons between a 30 mph impact sled test involving a belt-restrained 50th percentile male dummy and the predictions of the model conclude Part III.

The model which is described in this report is proposed as a powerful tool for studying and designing advanced integrated seat-restraint systems. It has been exercised several hundred times to study belt restraint systems, various deceleration profiles, headrest and seatback shape, pedestrian kinematics, occupant size and position, etc., and represents the current state of the art in two-dimensional crash victim simulators.

A. STATE OF THE ART

Mathematical models have been developed for the motion of the human body in several environments, including auto occupant dynamics,^{*1-8} human gait, and the motions experienced by the legs and arms during walking.⁹⁻¹¹ This work is often applied to the design, development and use of prosthetic devices. In connection with aerospace applications, analytical studies of self-generated motions possible in free-fall¹²⁻¹⁴ and 0-gravity environments are being carried out and find application in such activities as sky-diving and space-walking. Also, studies are being made of such work tasks as lifting,^{15,16} resulting in the development of work capability amplifiers.

Fundamental theoretical work has been carried out in the field of mathematical models for more than sixty years, as seen in the work of Fischer.¹⁷ However, it is only with the coming-of-age of the high speed computer in the last twenty years that practical solutions of equations as

*Note: Only a small number of representative papers published on this subject are included in this list.

complex as those proposed by Fischer have been realized. Hence, the mathematical simulation of human body motions has become a very active research topic in the last ten years.

Generally, two approaches have been used in analyses simulating auto occupant protection. On one hand, various researchers have adopted relatively simple physical models for studying specific aspects of human kinematics. Weaver¹⁸ has used a two-mass, two-degree-of-freedom model to simulate belt loadings and head impact velocity in the case of a lap-belted occupant. Similar models have been developed by Aldman¹⁹ and Renneker²⁰ for studying slack in restraint systems and the effect of various input deceleration profiles. Other authors, including Martinez,²¹ Mertz,²² and Roberts,²³ have used somewhat more sophisticated models for studying the phenomenon of whiplash. Roberts has added an additional complicating factor to his model--the motion of the brain mass inside the brain case.

On the other hand, several authors¹⁻³ have developed more complex models of human kinematics utilizing several masses for simulating body motions. In addition, complex vehicle geometry is introduced in these simulations to provide an intricate array of forces acting on the segmented occupant. Particularly noteworthy in the early development of these models are the efforts of McHenry.² All these models are marked by extensive development programs requiring at least two years from project initiation to the production of a functioning computer program.

Most of the modeling work mentioned above has been concerned with simulations of occupant motion in two dimensions. The only known published simulations involving three dimensions are those of Roberts,¹ Thompson,⁴ Robbins,⁶ and Young.⁷ The first of these is a simple-one-mass model capable of simulating belt loads and upper torso motions in three dimensions, while the second is part of a large program involving vehicle crush characteristics. The third model simulates a three-dimensional occupant by three masses and twelve degrees-of-freedom while the recently completed fourth model describes the occupant by twelve masses and thirty-one degrees-

of freedom while possessing a less sophisticated model of occupant-vehicle interactions than that of Robbins.⁶

Even with the advent of the highly complex computer programs described here, there still exist major problem areas such as:

1. Verification of the model by experiment;
2. Lack of highly controlled tests;
3. Lack of anthropometric data and verification of the models using human volunteers;
4. Lack of impact test data reduction techniques specifically oriented towards mathematical model verification.
5. Difficulty in using the models because of the complex input data requirements; and
6. Difficulty in using the model at locations other than the laboratories of the developer.

These problems can be classified into two general types: (a) lack of closely coordinated efforts to insure that the mathematical models predict and anticipate physical reality, and (b) ease of use. The latter problem is somewhat easier to approach than the first one. One needs to identify the user and his capabilities and then write a program which is user-oriented. Computer programs of this nature are in actual use, particularly in styling and design laboratories in the auto industry. The users need not be highly trained computer experts.

In assigning staff to the various subject areas of the current research project, a concerted effort was made to coordinate the sled test program and the analytical program. One group was assigned the task of analysis; another group was responsible for the impact sled test program; and a new key group was formed to bridge the gap which was found to exist between the analytical and experimental groups. The task of the key group was to insure that meaningful data was generated in the tests and to establish techniques for reducing this data into a form which could be compared with the output of a mathematical model.

This discussion is intended to show that the current state of the art is quite advanced from the viewpoint of producing computer programs

which predict vehicle occupant motions in a crash environment. However, considerable research must be carried out to make programs of this nature easily usable. Additionally, it is recommended that experimental work accompany the development of future models to make assessment of their validity more straightforward.

II. ANALYTICAL DESCRIPTION OF THE TWO-DIMENSIONAL CRASH VICTIM SIMULATOR

This part of the report consists of an analytical description of the two-dimensional crash victim simulator, a schematic of which is shown in Figure 1. The parameters which have been chosen for use in the physical model are discussed, then there is a brief presentation of the equations of motion describing the movements of the crash victim. This is followed by a detailed description of the analytical models used to define the mass and geometry of the body, the contact surface causing force interactions between the occupant and the vehicle, the seat, the joint structures connecting the various segments of the body, and a belt restraint system.

A. SELECTION OF PARAMETERS

Four major groups of parameters have been considered in the development of this model: the occupant, seat, external restraint environment, and the deceleration profile.

The occupant is difficult to describe both experimentally and analytically. Controversy arises over the use of anthropometric dummies, cadavers, human volunteers, and laboratory animals. The physical properties of dummies are the most easily obtained and controlled but there is a question whether they represent human kinematics. Four sets of parameters are used to model the dynamic behavior of the body. First, the body is modeled by eight rigid mass elements representing the head, upper torso, middle torso, lower torso, upper arm, lower arm, upper leg, and lower leg. Second, these mass elements are connected by joint structures represented as viscoelastic, nonlinear, torsional springs. Resistance is slight over most of the range of motion of each joint. However, stops, located at the end of practical motion of each joint, are modeled by a torsional spring possessing a high degree of stiffness. Third, muscle tone is delineated rather crudely in this model by a constant torque, acting in each joint, resisting whatever relative motion is

experienced by the adjacent rigid body elements. Constant torque is also used to model the friction joints found in present generation anthropometric dummies. Fourth, body geometry is represented by the moments of inertia of the eight rigid masses as well as contact body surfaces. These surfaces, which are rigidly attached to the head, torso, hip, and extremities, allow the user of the model to ascertain if a body part impacts any part of the vehicle or seat.

The seat would seem to be easier to describe for use in a model. However, it is unfortunate that very little research has been carried out to determine dynamic deformation characteristics such as stiffness and damping of seats. Three parts of the seat are included in this model: seat back, seat cushion, and head rest. The seat back may apply a force to the lower part of the occupant's back at the hip and to the upper torso. The seat back is modeled by a plane surface. The head rest is independent of the seat back and can be composed of a number of contact surfaces representing a nonplanar geometry. The seat cushion is again represented by a plane. Vertical forces are applied at the hip and at the front of the seat. A horizontal force is also applied at the front of the seat cushion to prevent the lower leg from rotating back "through the seat cushion." Each of these elements is described by dynamic force-deformation relations, friction coefficients, and geometrical configurations.

The external system restraining an occupant is ordinarily defined in terms of specific devices such as a seat belt or an airbag. One common feature of all these devices is the fact that they can be described in terms of a dynamic force-deformation profile. For example, an acceleration-dependent inertial reel used in conjunction with a shoulder harness will have a different characteristic curve than a controlled permanent deformation device or one of the harnesses used in most current production vehicles. In each case a different formula must be used which computes force as a function of deformation and deformation rate. Therefore, provisions must be made for forces to be applied to the occupant in a rather general manner in order that they can be used in modeling any one of the proposed restraint devices.

Three types of interactions are possible between the occupant and vehicle: (a) the seat, already discussed, (b) a system of belts attached to the occupant as a seat belt and/or shoulder harness, and (c) a collection of geometric surfaces representing the profile of a vehicle interior or exterior. These surfaces, each represented by a different dynamic force-deformation relationship, interact with the contact surfaces fixed to the body of the occupant to generate a complex interaction of forces and occupant motions representing the collision of the occupant with seat, restraint system, or vehicle structural member.

An example of a complex set of force interactions between an occupant and a vehicle interior is represented by simulating the airbag restraint system. The occupant is represented in the usual way and may or may not be restrained by a lap belt. Vehicle components such as the seat back, seat cushion, floor, windshield, and lower dash panel are described in terms of contact surfaces. It is necessary to know the force-motion interrelationship between the head or torso and the bag before the simulation can be carried out as the model itself cannot predict any force-deformation relationships. They must be obtained using experimental procedures and be provided as input data for the operation of the computer simulation.

It should also be noted that this general formulation allows studies of much more than a seated occupant restrained in some manner inside the vehicle. Studies have been carried out of more esoteric concepts such as the airbag, the rear-end collision, and the pedestrian. Also, studies of the dynamics of a child in any one of the large number of seats and restraint devices available on today's market are possible.

The deceleration profile which is used in this model is relatively simple, it can be either a forward or rearward deceleration. However, the shape of the profile is limited to 200 linear segments. Typical examples are shown in Figures 2 and 3.

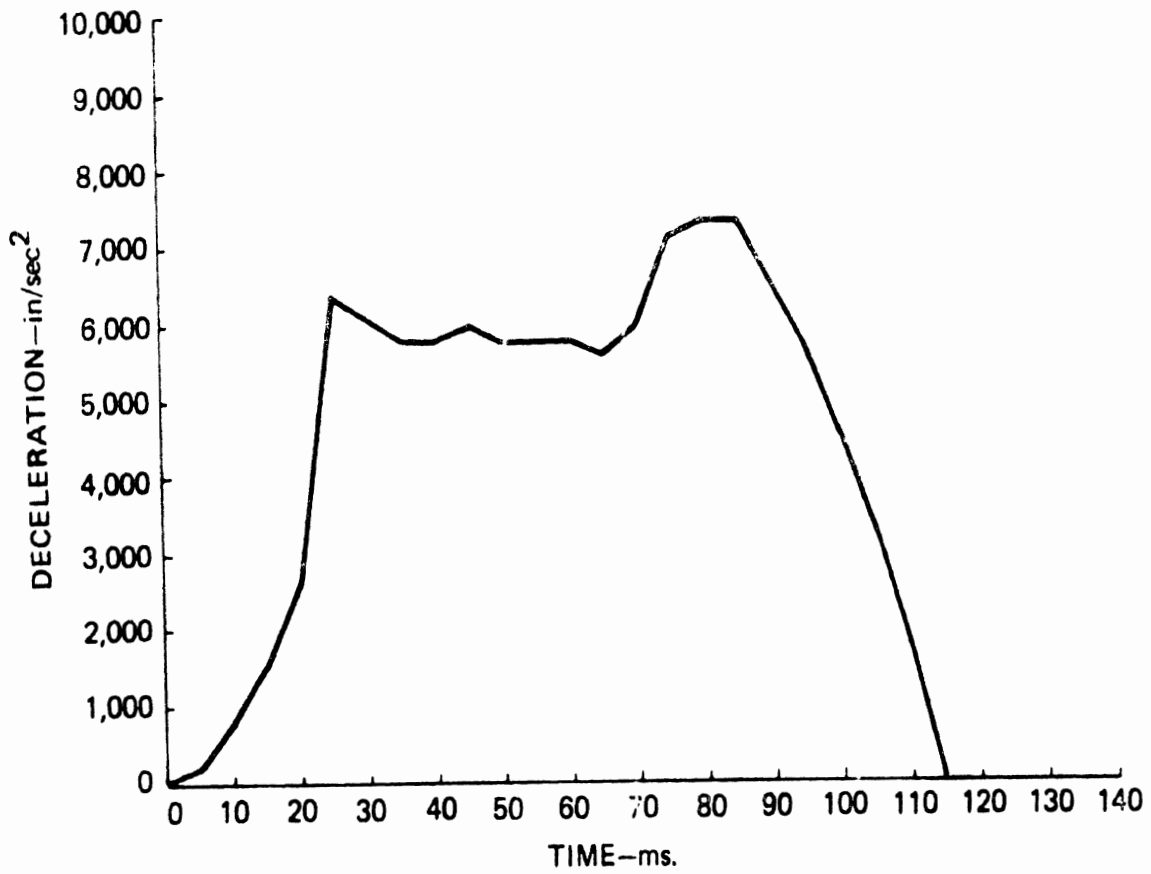


Figure 2. AMA deceleration profile.

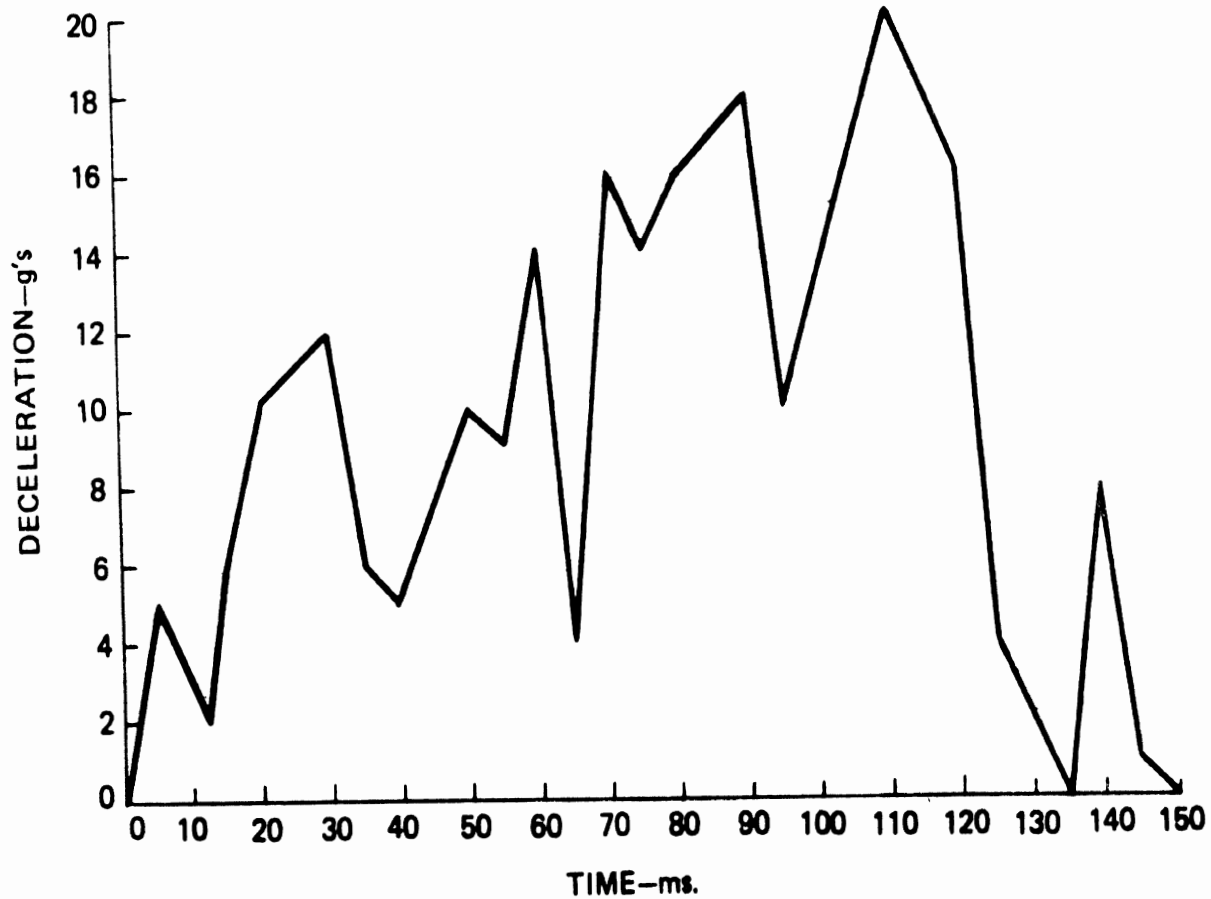


Figure 3. Complex deceleration trace.

B. FORMULATION OF THE MODEL

The equations of motion are derived by Lagrangian techniques²⁴:

$$\frac{d}{dt} \left[\frac{\partial(\text{KE})}{\partial \dot{Z}_i} \right] - \frac{\partial(\text{KE})}{\partial Z_i} + \frac{\partial(\text{PE})}{\partial Z_i} + \frac{\partial(\text{DE})}{\partial \dot{Z}_i} = F_{Z_i} \quad (\text{II.B.1})$$

where

KE is the system kinetic energy

PE is the system potential energy

DE is the system dissipated energy rate

F_{Z_i} are the classical generalized forces

Z_i are the classical generalized coordinates or degrees of freedom of the model

Since the only driving force is applied to the vehicle and not directly to the body, the F_{Z_i} terms are all zero. After the energy terms have been written, the resulting equations of motion are rearranged so that all the terms containing generalized accelerations appear on the left-hand side and all others appear on the right-hand side. Thus rearranged, these equations are of the form

$$m \ddot{\vec{Z}} = \vec{b} \quad (\text{II.B.2})$$

where m is the matrix of generalized acceleration coefficients and $\ddot{\vec{Z}}$ is the acceleration vector. In this analysis the right-hand side, \vec{b} , will be called the "generalized force" and contributions to it from the potential and kinetic energy in Eq. (II.B.1) will be referred to as the generalized force from that part of the model. The total generalized force is the vectorial sum of each contributing component (gravity, joints, belts, seat cushion, and contacts). The kinetic energy contributions to the generalized force are centrifugal and Coriolis force terms.

Kinetic energy alone determines the left-hand side of the equations of motion. In the computational procedure, the inverse of the matrix, m^{-1} ,

multiplied by the generalized force vector, \vec{b} , yields the solution for the generalized accelerations, i.e.,

$$\ddot{\vec{z}} = \mathbf{m}^{-1} \vec{b} \quad (\text{II.B.3})$$

The generalized force vector may be expanded to show the various contributions

$$\vec{b} = \vec{B} - \vec{G} + \vec{Q} + \vec{D} + \vec{C} + \Delta\vec{b}_Q + \Delta\vec{b}_s + \Delta\vec{b}_J + \vec{D}_b \quad (\text{II.B.4})$$

where

- \vec{B} is due to kinetic energy
- \vec{G} is due to gravity
- \vec{Q} is due to contact forces
- \vec{D} is due to seat cushion
- \vec{C} is due to joint elasticity
- $\Delta\vec{b}_Q$ is due to contact friction
- $\Delta\vec{b}_s$ is due to seat friction
- $\Delta\vec{b}_J$ is due to joint friction
- \vec{D}_b is due to belts

C. BODY

The crash victim is simulated by eight body segments: three segments in the torso to introduce some flexibility into the spine, one segment for the head, two segments in the arms (right and left combined) representing the forearm and upper arm, and two segments for the legs (right and left combined) representing upper and lower legs. Figure 1 shows a crash victim in a typical seating configuration restrained by a shoulder harness and lap belt. Figure 4 illustrates the body segments and their lengths, centers of gravity, and moments of inertia. Tables I and II contain the subscripting schemes for the body elements and joints which are used in the computer program while Figure 5 shows the angular coordinates defining the orientation in space of

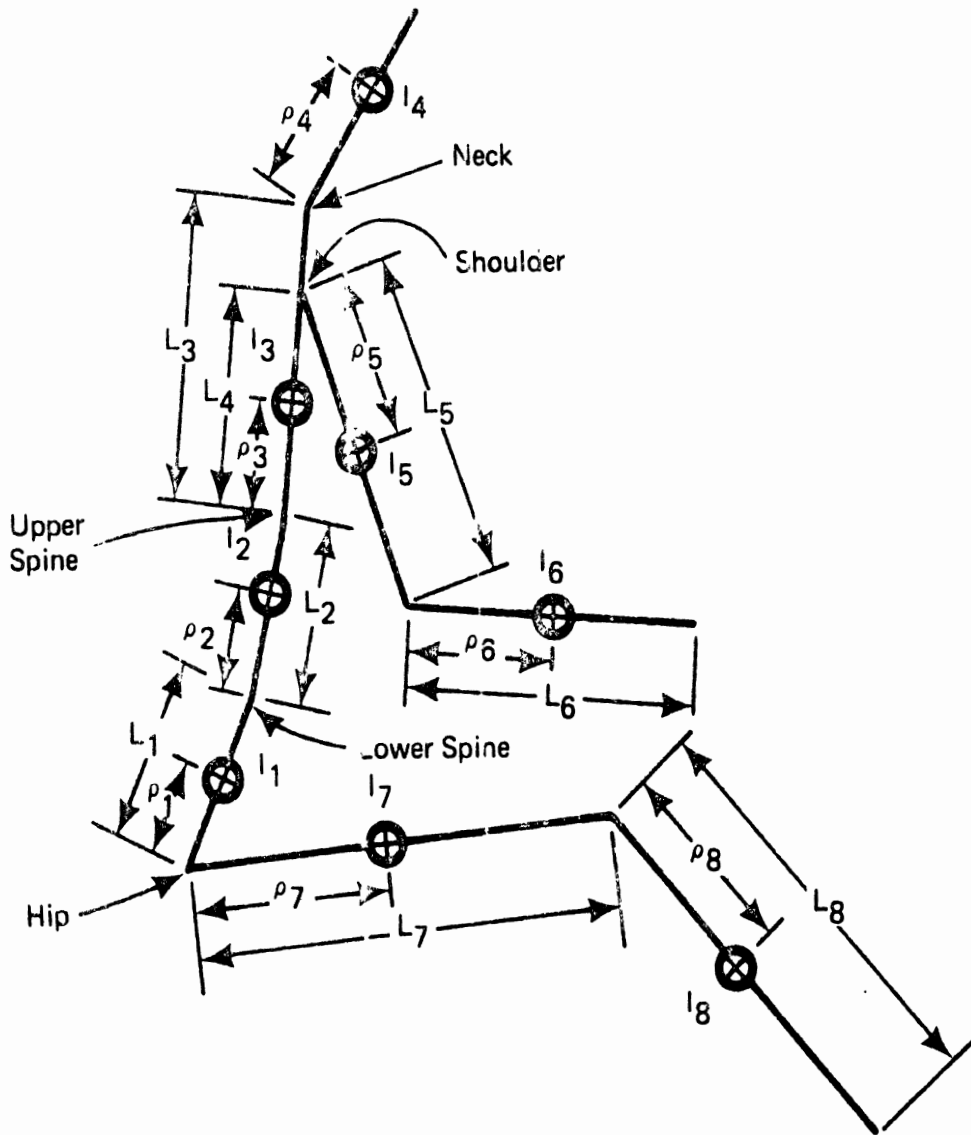
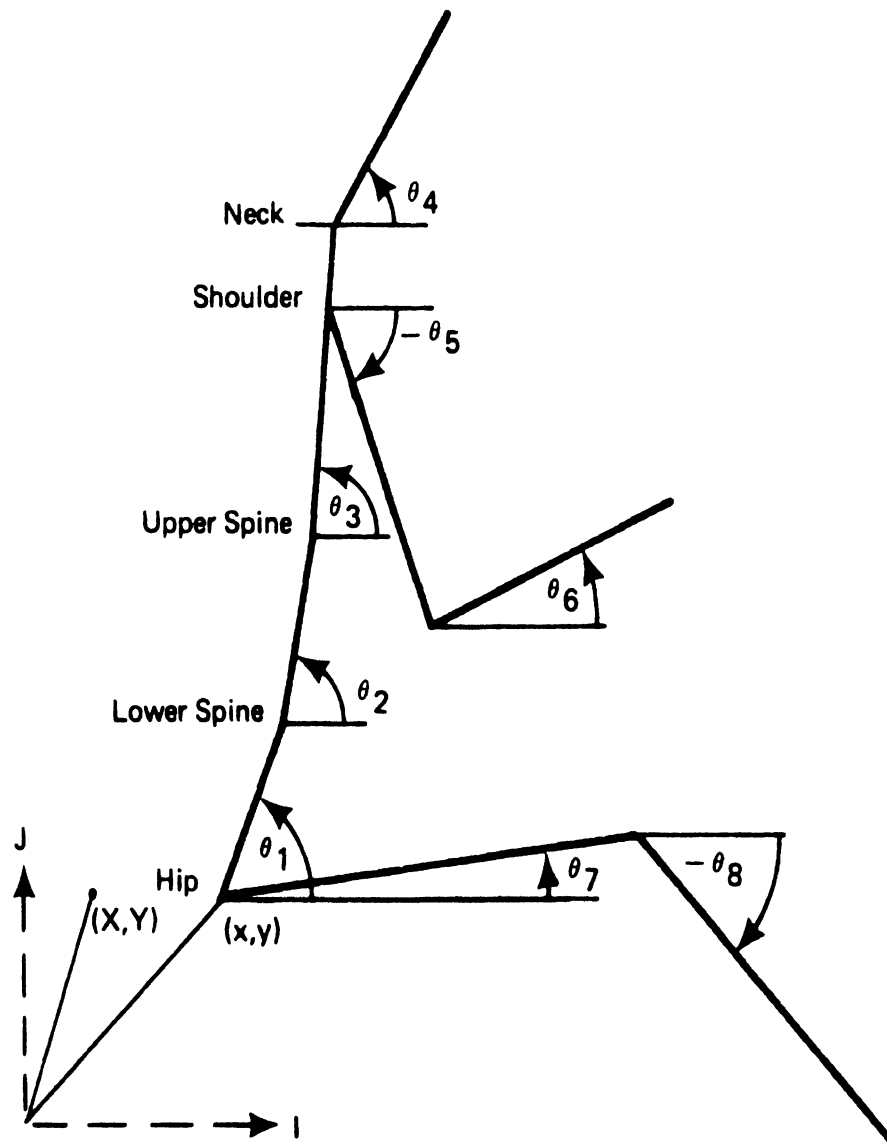


Figure 4. Body element lengths, centers of gravity, and moments of inertia.



(X, Y) = Coordinates for vehicle relative to inertial system. This is the point on the vehicle occupied by the hip at zero time.

(x, y) = coordinates of hip relative to inertial system.

Figure 5. Body angles.

the various body elements and the translational coordinates of the hip. It should be noted that x and y plus the eight angles defined in this figure are the generalized coordinates used in the analysis.

TABLE I. SUBSCRIPTS OF BODY JOINTS

Subscript	1	2	3	4	5	6	7
Joint	Hip	Lower Spine	Upper Spine	Neck	Shoulder	Elbow	Knee

TABLE II. SUBSCRIPTS OF BODY SEGMENTS

Subscript	1	2	3	4	5	6	7	8
Body segment	Lower Torso	Middle Torso	Upper Torso	Head	Upper Arm	Lower Arm	Upper Leg	Lower Leg

TABLE III. SUBSCRIPTS OF CONTACT ARCS

Subscript	1	2	3	4	5	6	7	8
Contact arc	Hip	---	Upper Torso	Head	Elbow	Hand	Knee	Foot

The coordinates for the center-of-gravity of each body segment are stated in Eq. (II.C.1) in terms of the generalized coordinates. Based on this the velocities of the eight centers-of-gravity are given in Eq. (II.C.2). Tables I, II, and XIV as well as Figures 4 and 5 should be referred to in reading these equations.

Using Eqs. (II.C.1) and (II.C.2) the kinetic and potential energy associated with the body can be written. After extensive formal manipulation of

the kinetic and potential energies, those portions of the equations of motion which can be stated are terms due to centrifugal and gravitational forces as well as to the matrix. This matrix is shown in Eq. (II.B.2) which forms the bulk of the left-hand side of the equations of motion.

$$\begin{aligned}
 x_1 &= x + \rho_1 \cos \theta_1 \\
 y_1 &= y + \rho_1 \sin \theta_1 \\
 x_2 &= x + L_1 \cos \theta_1 + \rho_2 \cos \theta_2 \\
 y_2 &= y + L_1 \sin \theta_1 + \rho_2 \sin \theta_2 \\
 x_3 &= x + L_1 \cos \theta_1 + L_2 \cos \theta_2 + \rho_3 \cos \theta_3 \\
 y_3 &= y + L_1 \sin \theta_1 + L_2 \sin \theta_2 + \rho_3 \sin \theta_3 \\
 x_4 &= x + L_1 \cos \theta_1 + L_2 \sin \theta_2 + L_3 \cos \theta_3 + \rho_4 \cos \theta_4 \\
 y_4 &= y + L_1 \sin \theta_1 + L_2 \sin \theta_2 + L_3 \sin \theta_3 + \rho_4 \sin \theta_4 \\
 x_5 &= x + L_1 \cos \theta_1 + L_2 \cos \theta_2 + L_4 \cos \theta_3 + \rho_5 \cos \theta_5 \\
 y_5 &= y + L_1 \sin \theta_1 + L_2 \sin \theta_2 + L_4 \sin \theta_3 + \rho_5 \sin \theta_5 \\
 x_6 &= x + L_1 \cos \theta_1 + L_2 \cos \theta_2 + L_4 \cos \theta_3 + L_5 \cos \theta_5 + \rho_6 \cos \theta_6 \\
 y_6 &= y + L_1 \sin \theta_1 + L_2 \sin \theta_2 + L_4 \sin \theta_3 + L_5 \sin \theta_5 + \rho_6 \sin \theta_6 \\
 x_7 &= x + \rho_7 \cos \theta_7 \\
 y_7 &= y + \rho_7 \sin \theta_7 \\
 x_8 &= x + L_7 \cos \theta_7 + \rho_8 \cos \theta_8 \\
 y_8 &= y + L_7 \sin \theta_7 + \rho_8 \sin \theta_8
 \end{aligned}
 \tag{II.C.1}$$

$$\begin{aligned}
\dot{x}_1 &= \dot{x} - \rho_1 \dot{\theta}_1 \sin \theta_1 \\
\dot{y}_1 &= \dot{y} + \rho_1 \dot{\theta}_1 \cos \theta_1 \\
\dot{x}_2 &= \dot{x} - L_1 \dot{\theta}_1 \sin \theta_1 - \rho_2 \dot{\theta}_2 \sin \theta_2 \\
\dot{y}_2 &= \dot{y} + L_1 \dot{\theta}_1 \cos \theta_1 + \rho_2 \dot{\theta}_2 \cos \theta_2 \\
\dot{x}_3 &= \dot{x} - L_1 \dot{\theta}_1 \sin \theta_1 - L_2 \dot{\theta}_2 \sin \theta_2 - \rho_3 \dot{\theta}_3 \sin \theta_3 \\
\dot{y}_3 &= \dot{y} + L_1 \dot{\theta}_1 \cos \theta_1 + L_2 \dot{\theta}_2 \cos \theta_2 + \rho_3 \dot{\theta}_3 \cos \theta_3 \\
\dot{x}_4 &= \dot{x} - L_1 \dot{\theta}_1 \sin \theta_1 - L_2 \dot{\theta}_2 \sin \theta_2 - L_3 \dot{\theta}_3 \sin \theta_3 - \rho_4 \dot{\theta}_4 \sin \theta_4 \\
\dot{y}_4 &= \dot{y} + L_1 \dot{\theta}_1 \cos \theta_1 + L_2 \dot{\theta}_2 \cos \theta_2 + L_3 \dot{\theta}_3 \cos \theta_3 + \rho_4 \dot{\theta}_4 \cos \theta_4 \\
\dot{x}_5 &= \dot{x} - L_1 \dot{\theta}_1 \sin \theta_1 - L_2 \dot{\theta}_2 \sin \theta_2 - L_4 \dot{\theta}_3 \sin \theta_3 - \rho_5 \dot{\theta}_5 \sin \theta_5 \\
\dot{y}_5 &= \dot{y} + L_1 \dot{\theta}_1 \cos \theta_1 + L_2 \dot{\theta}_2 \cos \theta_2 + L_4 \dot{\theta}_3 \cos \theta_3 + \rho_5 \dot{\theta}_5 \cos \theta_5 \\
\dot{x}_6 &= \dot{x} - L_1 \dot{\theta}_1 \sin \theta_1 - L_2 \dot{\theta}_2 \sin \theta_2 - L_4 \dot{\theta}_3 \sin \theta_3 - L_5 \dot{\theta}_5 \sin \theta_5 - \rho_6 \dot{\theta}_6 \sin \theta_6 \\
\dot{y}_6 &= \dot{y} + L_1 \dot{\theta}_1 \cos \theta_1 + L_2 \dot{\theta}_2 \cos \theta_2 + L_4 \dot{\theta}_3 \cos \theta_3 + L_5 \dot{\theta}_5 \cos \theta_5 + \rho_6 \dot{\theta}_6 \cos \theta_6 \\
\dot{x}_7 &= \dot{x} - \rho_7 \dot{\theta}_7 \sin \theta_7 \\
\dot{y}_7 &= \dot{y} + \rho_7 \dot{\theta}_7 \cos \theta_7 \\
\dot{x}_8 &= \dot{x} - L_7 \dot{\theta}_7 \sin \theta_7 - \rho_8 \dot{\theta}_8 \sin \theta_8 \\
\dot{y}_8 &= \dot{y} + L_7 \dot{\theta}_7 \cos \theta_7 + \rho_8 \dot{\theta}_8 \cos \theta_8
\end{aligned} \tag{II.C.2}$$

The components of the equations of motion due to centrifugal force form \vec{B} and can be written

$$\begin{aligned}
 B_1 &= L_1 \sum_{j=2}^6 a_j \dot{\theta}_j^2 \sin [\theta_j - \theta_1] \\
 B_2 &= L_2 a_2 \dot{\theta}_1^2 \sin (\theta_1 - \theta_2) + L_2 \sum_{j=3}^6 a_j \dot{\theta}_j^2 \sin (\theta_j - \theta_2) \\
 B_3 &= a_3 \sum_{j=1}^2 L_j \dot{\theta}_j^2 \sin (\theta_j - \theta_3) + L_3 a_4 \dot{\theta}_4^2 \sin (\theta_4 - \theta_3) \\
 &\quad + L_4 \sum_{j=5}^6 a_j \dot{\theta}_j^2 \sin (\theta_j - \theta_3) \\
 B_4 &= a_4 \sum_{j=1}^3 L_j \dot{\theta}_j^2 \sin (\theta_j - \theta_4) \\
 B_5 &= a_5 \sum_{j=1}^3 L_j \dot{\theta}_j^2 \sin (\theta_j - \theta_5) + L_4 a_5 \dot{\theta}_3^2 \sin (\theta_3 - \theta_5) \\
 &\quad + a_6 L_5 \dot{\theta}_6^2 \sin (\theta_6 - \theta_5) \\
 B_6 &= a_6 \sum_{j=1}^{3,5} L_j \dot{\theta}_j^2 \sin (\theta_j - \theta_6) \\
 B_7 &= L_7 a_8 \dot{\theta}_8^2 \sin (\theta_8 - \theta_7) \\
 B_8 &= L_7 a_8 \dot{\theta}_7^2 \sin (\theta_7 - \theta_8) \\
 B_9 &= \sum_{j=1}^8 a_j \dot{\theta}_j^2 \cos \theta_j \\
 B_{10} &= \sum_{j=1}^8 a_j \dot{\theta}_j^2 \sin \theta_j
 \end{aligned} \tag{II.C.3}$$

Due to gravity the contribution to the right-hand side of the equations of motion forms \vec{G} and can be written

$$\begin{aligned}
 G_1 &= g a_1 \cos \theta_1 \\
 G_2 &= g a_2 \cos \theta_2 \\
 G_3 &= g a_3 \cos \theta_3 \\
 G_4 &= g a_4 \cos \theta_4 \\
 G_5 &= g a_5 \cos \theta_5 \\
 G_6 &= g a_6 \cos \theta_6 \\
 G_7 &= g a_7 \cos \theta_7 \\
 G_8 &= g a_8 \cos \theta_8 \\
 G_9 &= 0 \\
 G_{10} &= g a_9
 \end{aligned}
 \tag{II.C.4}$$

where

$$\begin{aligned}
 a_i &= m_i \rho_i + L_i \sum_{j=i+1}^6 m_j & i = 1, 2 \\
 a_3 &= m_3 \rho_3 + m_4 L_3 + (m_5 + m_6) L_4 \\
 a_i &= m_i \rho_i & i = 4, 6, 8 \\
 a_i &= m_i \rho_i + m_{i+1} L_i & i = 5, 7 \\
 a_9 &= \sum_{i=1}^8 m_i
 \end{aligned}
 \tag{II.C.5}$$

a_{10}	$a_{21} \cos(\theta_1 - \theta_2)$	$a_{31} \cos(\theta_1 - \theta_3)$	$a_{41} \cos(\theta_1 - \theta_4)$	$a_{51} \cos(\theta_1 - \theta_5)$	$a_{61} \cos(\theta_1 - \theta_6)$	0	0	$-a_1 \sin \theta_1$	$a_1 \cos \theta_1$
$a_{21} \cos(\theta_1 - \theta_2)$	a_{11}	$a_{32} \cos(\theta_2 - \theta_3)$	$a_{42} \cos(\theta_2 - \theta_4)$	$a_{52} \cos(\theta_2 - \theta_5)$	$a_{62} \cos(\theta_2 - \theta_6)$	0	0	$-a_2 \sin \theta_2$	$a_2 \cos \theta_2$
$a_{31} \cos(\theta_1 - \theta_3)$	$a_{32} \cos(\theta_2 - \theta_3)$	a_{12}	$a_{43} \cos(\theta_3 - \theta_4)$	$a_{53} \cos(\theta_3 - \theta_5)$	$a_{63} \cos(\theta_3 - \theta_6)$	0	0	$-a_3 \sin \theta_3$	$a_3 \cos \theta_3$
$a_{41} \cos(\theta_1 - \theta_4)$	$a_{42} \cos(\theta_2 - \theta_4)$	$a_{43} \cos(\theta_3 - \theta_4)$	a_{13}	$a_{54} \cos(\theta_4 - \theta_5)$	$a_{64} \cos(\theta_4 - \theta_6)$	0	0	$-a_4 \sin \theta_4$	$a_4 \cos \theta_4$
$a_{51} \cos(\theta_1 - \theta_5)$	$a_{52} \cos(\theta_2 - \theta_5)$	$a_{53} \cos(\theta_3 - \theta_5)$	0	a_{14}	$a_{65} \cos(\theta_5 - \theta_6)$	0	0	$-a_5 \sin \theta_5$	$a_5 \cos \theta_5$
$a_{61} \cos(\theta_1 - \theta_6)$	$a_{62} \cos(\theta_2 - \theta_6)$	$a_{63} \cos(\theta_3 - \theta_6)$	0	$a_{65} \cos(\theta_5 - \theta_6)$	a_{15}	0	0	$-a_6 \sin \theta_6$	$a_6 \cos \theta_6$
0	0	0	0	0	0	a_{16}	$a_{87} \cos(\theta_7 - \theta_8)$	$-a_7 \sin \theta_7$	$a_7 \cos \theta_7$
0	0	0	0	0	0	$a_{87} \cos(\theta_7 - \theta_8)$	a_{17}	$-a_8 \sin \theta_8$	$a_8 \cos \theta_8$
$-a_1 \sin \theta_1$	$-a_2 \sin \theta_2$	$-a_3 \sin \theta_3$	$-a_4 \sin \theta_4$	$-a_5 \sin \theta_5$	$-a_6 \sin \theta_6$	$-a_7 \sin \theta_7$	$-a_8 \sin \theta_8$	a_9	0
$a_1 \cos \theta_1$	$a_2 \cos \theta_2$	$a_3 \cos \theta_3$	$a_4 \cos \theta_4$	$a_5 \cos \theta_5$	$a_6 \cos \theta_6$	$a_7 \cos \theta_7$	$a_8 \cos \theta_8$	0	a_9

The matrix m in Eq. (II.B.2) formed from the kinetic energy terms is shown as Eqs. (II.C.6) and (II.C.7).

$$\begin{aligned}
 a_i &= I_j + m_j \rho_j^2 + L_j^2 \sum_{k=j+1}^6 m_k && \text{for } i = 10, 11 \\
 &&& \text{and } j = i-9 \\
 a_{12} &= I_3 + m_3 \rho_3^2 + m_4 L_3^2 + (m_5 + m_6) L_4^2 \\
 a_i &= I_j + m_j \rho_j^2 && \text{for } i = 13, 15, 17 \\
 &&& \text{and } j = i-9 \\
 a_i &= I_j + m_j \rho_j^2 + m_{j+1} L_j^2 && \text{for } i = 14, 16 \\
 &&& \text{and } j = i-9 \quad \text{(II.C.7)}
 \end{aligned}$$

D. CONTACT SURFACES

The nine distinct surfaces simulating the interior of the vehicle and capable of applying forces on the body of the occupant are represented by straight line segments as shown in Figure 7. After the computer program user chooses whether the occupant is a driver, front-seat passenger, or rear-seat passenger, a table is generated showing which body segments are allowed to contact which surfaces.

This computer generated table is equivalent to the corresponding column in Table V. The user may choose to model any special contact surface with one of the standard contact surfaces. The choice of which standard contact to use must include matching the expected interactions of this contact with the table of permissible interactions (the appropriate column of Table V). Each contact surface has a unique name shown in Table IV which will be used in the program output. The user has the option of changing these names to represent, for example, an airbag.

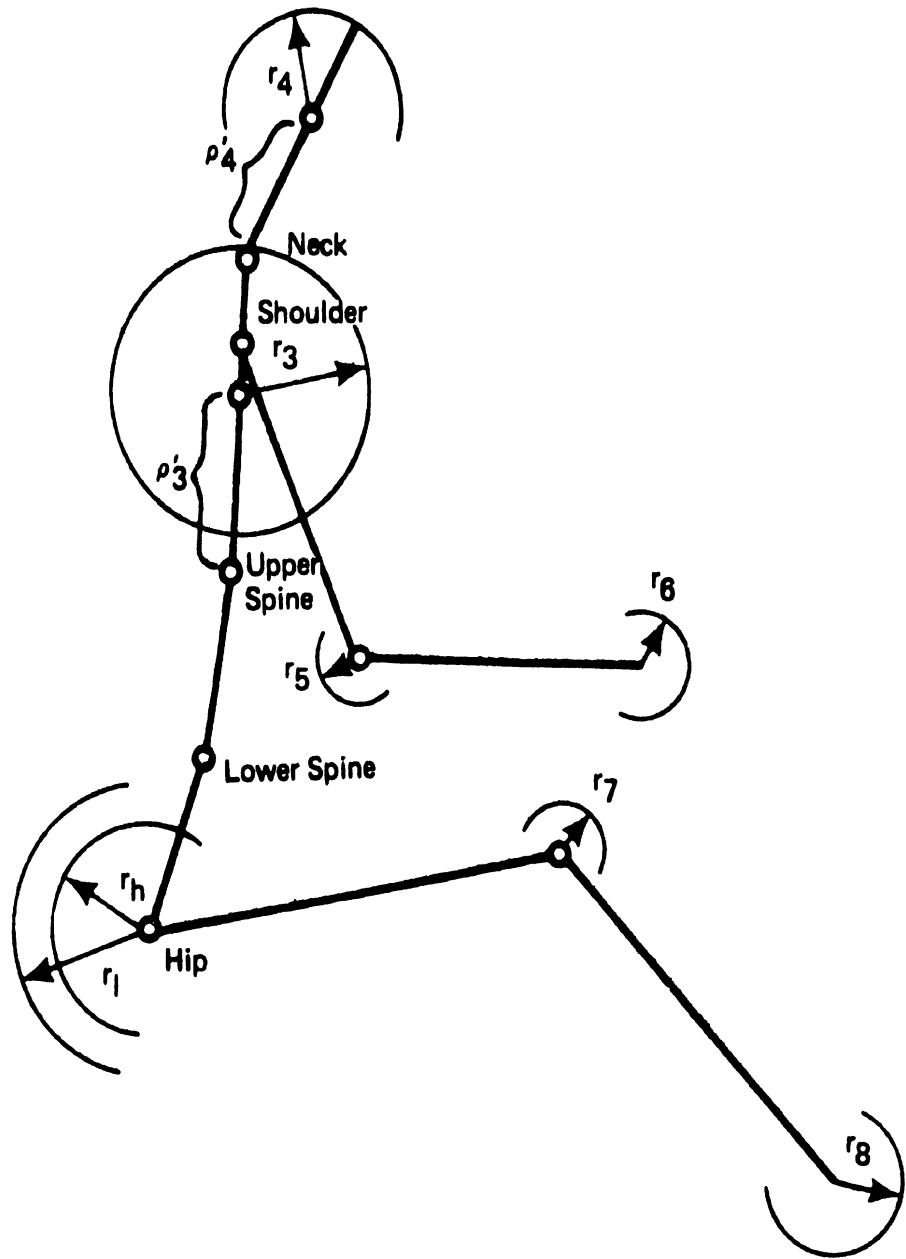


Figure 6. Definition of body contact radii.

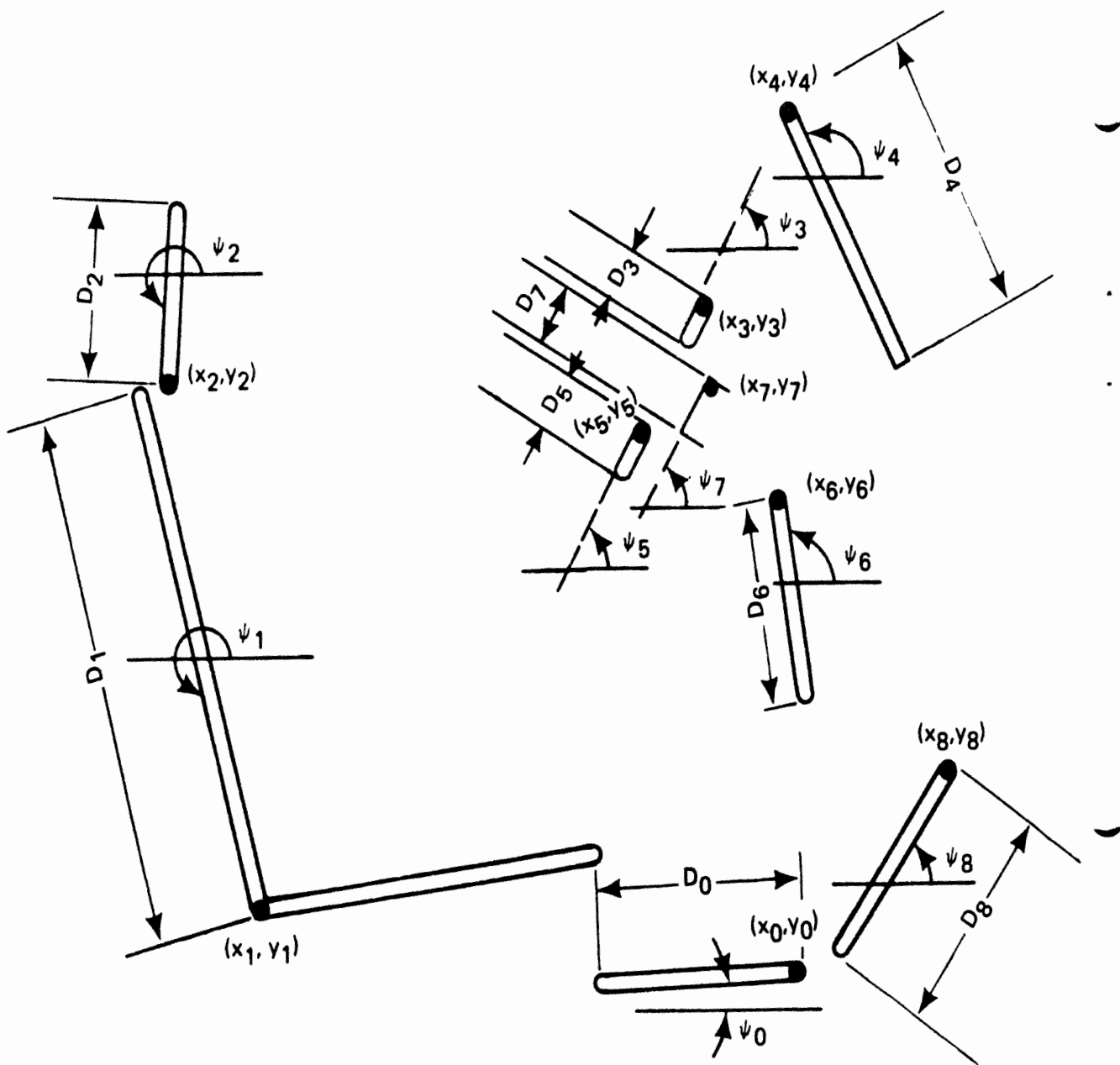


Figure 7. Definitions of vehicle contact surface (shown for driver).

TABLE IV. NORMAL CONTACT SURFACE INDICES

Index*	Normal Contact Surface
0	Floor
1	Seat back
2	Rear head rest
3	Upper steering wheel, upper dash, back of front seat
4	Windshield
5	Lower steering wheel
6	Lower panel
7	Steering column
8	Toeboard
9	Steering wheel

*It is permissible to use any index for any other contact surface as long as it is compatible with the table of possible contacts in Table V. For example, an airbag could be simulated by using the various segments of the steering wheel.

Each contact surface is defined by four quantities: the x and y coordinates of its reference point, its length, and its angular orientation. This reference point is at the end of the surface line which is most counter-clockwise relative to the origin. The angle is found by drawing a horizontal line through the other end point and measuring the angle from the forward part of this line to the surface.

Each contact surface produces two forces. The first force acts perpendicularly to the surface through the center of curvature of the contacting body segments and the second force is frictional in nature and has the form:

$$P' = \begin{cases} -\mu_a P \operatorname{sgn} v_T & \text{for } |v_T| \geq \xi_a \\ 0 & |v_T| < \xi_a \end{cases} \quad (\text{II.D.1})$$

where

V_T is the tangential velocity of the body segment along the surface

P is the force applied normal to the contact surface

μ_c is the friction coefficient

v_{sl} is the velocity limit

When the velocity limit (a small quantity such as 0.1 in/sec) is exceeded the friction force is applied; otherwise, it is set to zero representing sliding or Coulomb friction.

The material properties of the contact surfaces have two features. The first of these is a load-deflection polynomial which may be up to the fifth order in both deflection and deflection rate representing a nonlinear, viscoelastic material. This polynomial is applied during the time while the load is being applied to the surface while unloading is based on a parabolic function. The second feature is a force-limiting mechanism which prevents contact forces from exceeding a specified limit and allows simple modeling of energy-absorbing structures.

The force developed at any contact interface is given in the following polynomial form

$$P_k = \sigma_{0,k} + \sum_{m=1}^5 \left[\sigma_{m,k} \delta_k^m + \sigma_{m+5,k} \dot{\delta}_k^m \right]$$

(II.D.2)

where

$$\sigma_{0,i} = - \sum_{m=1}^5 \tau_{m+5,k} \dot{\delta}_{k-0}^{m+1}$$

where

δ_k is the distance which a particular body element impinges into a particular surface representing a segment of the vehicle interior

$\dot{\delta}_k$ is the deflection rate

$\dot{\delta}_{k_0}$ is the value of $\dot{\delta}_k$ when δ_k first becomes positive

$\sigma_{0,k}$ is a preload on any given contact surface

$\sigma_{1,j,k}$ through $\sigma_{10,j,k}$ are the material polynomial coefficients

The quantity k is the general force index. Values of k greater than four correspond to particular combinations of contact arcs on the body and contact surfaces and are shown in brackets in Table V. Hence, for each value of k and choice of passenger position, there corresponds a unique contact arc subscript which appears in parenthesis on the left margin of Table V and a unique contact surface subscript which appears in parentheses in the body of Table V. Throughout the remainder of this section "i" is this contact arc subscript and "a" is this contact surface subscript.

$$\delta_k = r_i - (x_a'' - x_i') \sin \psi_a + (y_a'' - y_i') \cos \psi_a$$

$$\dot{\delta}_k = \dot{x}_i' \sin \psi_a - \dot{y}_i' \cos \psi_a$$

$$v_T = \dot{x}_i' \cos \psi_a + \dot{y}_i' \sin \psi_a + r_i \dot{\theta}_i \quad (\text{II.D.3})$$

$$x_1' = x$$

$$y_1' = y$$

$$x_3' = x + L_1 \cos \theta_1 + L_2 \cos \theta_2 + \rho_3' \cos \theta_3$$

$$y_3' = y + L_1 \sin \theta_1 + L_2 \sin \theta_2 + \rho_3' \sin \theta_3$$

$$x_4' = x + L_1 \cos \theta_1 + L_2 \cos \theta_2 + L_3 \cos \theta_3 + \rho_4' \cos \theta_4$$

$$y_4' = y + L_1 \sin \theta_1 + L_2 \sin \theta_2 + L_3 \sin \theta_3 + \rho_4' \sin \theta_4$$

$$x_5' = x + L_1 \cos \theta_1 + L_2 \cos \theta_2 + L_4 \cos \theta_3 + L_5 \cos \theta_5$$

$$y_5' = y + L_1 \sin \theta_1 + L_2 \sin \theta_2 + L_4 \sin \theta_3 + L_5 \sin \theta_5$$

$$x_7' = x + L_7 \cos \theta_7$$

$$y_7' = y + L_7 \sin \theta_7$$

$$x_8' = x + L_7 \cos \theta_7 + L_8 \cos \theta_8$$

$$y_8' = y + L_7 \sin \theta_7 + L_8 \sin \theta_8 \quad (\text{II.D.4})$$

x_a'' , y_a'' , ψ_a are the contact surface reference coordinates and orientation, r_i is the radius of the contact arc attached to each body segment.

TABLE V. OCCUPANT CONTACTS VERSUS VEHICLE CONTACTS

Contact Arc Subscript	Contacts		
	Driver (1)	Front Passenger (2)	Rear Passenger (3)
Hip (1)	Seat back (1) [5]	Seat back (1) [5]	Seat back (1) [5]
Upper torso (3)	Seat back (1) [6]	Seat back (1) [6]	Seat back (1) [6]
	Upper steering wheel (3) [7]	Upper dash (3) [7]	Back of front seat (3) [7]
	Lower steering wheel (5) [8]		
	Steering column (7) [9]		
Head (4)	Seat back (1) [10]	Seat back (1) [8]	Seat (1) [8]
	Roof or head rest (2) [11]	Roof or head rest (2) [9]	Roof or head rest (2) [9]
	Upper steering wheel (3) [12]	Upper dash (3) [10]	Back of front seat (3) [10]
	Windshield (4) [13]	Windshield (4) [11]	
	Lower steering wheel (5) [14]		
Elbow (5)	Seat back (1) [15]	Seat back (1) [12]	Seat back (1) [11]
Knee (7)	Lower panel (6) [16]	Lower panel (6) [13]	Back of front seat (3) [12]
Foot (8)	Floorboard (0) [17]	Floorboard (0) [14]	Floorboard (0) [13]
	Toeboard (8) [18]	Toeboard (8) [15]	Back of front seat (3) [14]

NOTE: Numbers in brackets refer to indices 5-18 used in LODFEC and CONTACT printouts (see flow diagrams and Table XX).

$$\dot{x}'_1 = \dot{x}$$

$$\dot{y}'_1 = \dot{y}$$

$$\dot{x}'_3 = \dot{x} - L_1 \dot{\theta}_1 \sin \theta_1 - L_2 \dot{\theta}_2 \sin \theta_2 - \rho'_3 \dot{\theta}_3 \sin \theta_3$$

$$\dot{y}'_3 = \dot{y} + L_1 \dot{\theta}_1 \cos \theta_1 + L_2 \dot{\theta}_2 \cos \theta_2 + \rho'_3 \dot{\theta}_3 \cos \theta_3$$

$$\dot{x}'_4 = \dot{x} - L_1 \dot{\theta}_1 \sin \theta_1 - L_2 \dot{\theta}_2 \sin \theta_2 - L_3 \dot{\theta}_3 \sin \theta_3 - \rho'_4 \dot{\theta}_4 \sin \theta_4$$

$$\dot{y}'_4 = \dot{y} + L_1 \dot{\theta}_1 \cos \theta_1 + L_2 \dot{\theta}_2 \cos \theta_2 + L_3 \dot{\theta}_3 \cos \theta_3 + \rho'_4 \dot{\theta}_4 \cos \theta_4$$

$$\dot{x}'_5 = \dot{x} - L_1 \dot{\theta}_1 \sin \theta_1 - L_2 \dot{\theta}_2 \sin \theta_2 - L_4 \dot{\theta}_3 \sin \theta_3 - L_5 \dot{\theta}_5 \sin \theta_5$$

$$\dot{y}'_5 = \dot{y} + L_1 \dot{\theta}_1 \cos \theta_1 + L_2 \dot{\theta}_2 \cos \theta_2 + L_4 \dot{\theta}_3 \sin \theta_3 + L_5 \dot{\theta}_5 \cos \theta_5$$

$$\dot{x}'_7 = \dot{x} - L_7 \dot{\theta}_7 \sin \theta_7$$

$$\dot{y}'_7 = \dot{y} + L_7 \dot{\theta}_7 \cos \theta_7$$

$$\dot{x}'_8 = \dot{x} - L_7 \dot{\theta}_7 \sin \theta_7 - L_8 \dot{\theta}_8 \sin \theta_8$$

$$\dot{y}'_8 = \dot{y} + L_7 \dot{\theta}_7 \cos \theta_7 + L_8 \dot{\theta}_8 \cos \theta_8 \quad (\text{II.D.5})$$

and the other quantities are defined in Figures 4-7.

The form of P_k shown in Eq. (II.D.2) is used only while a load is being applied, i.e., when the deflection is increasing. During loading, the material may absorb energy so that its characteristics while unloading can be different than before.

The resulting permanent deformation is modeled by means of two parameters:

G, the ratio of permanent deformation to maximum deflection, and R, the ratio of conserved to total energy.

These two parameters are not independent but the relationship is complex so both are required by the program. The unloading force is assumed to be parabolic in nature and deflection to decrease from a maximum at $\delta = \Omega_k$ to zero force at $\delta = G \Omega_k$. This latter value ($G \Omega_k$) is taken as the permanent deformation, i.e., the value of deflection which must be exceeded before loading will begin again. The formula used for P_k for unloading is

$$P_k = \frac{3[F_k \Omega_k (1-G) - 2E_{1k}]}{\Omega_k^3 (1-G)^3} (\delta_k - G \Omega_k) \left\{ \delta_k + \frac{\Omega_k [6E_{1k} - F_k \Omega_k (1-G)(2+G)]}{3[F_k \Omega_k (1-G) - 2E_{1k}]} \right\} \quad (\text{II.D.6})$$

where

F_k is the loading force (P_k) at the maximum deflection

Ω_k is the maximum deflection

E_{1k} is the conserved energy. This quantity is computed as R times the total energy for this load-unload cycle plus the conserved energy from previous cycles if any.

The Eq. (II.D.6) results from an evaluation of the coefficients of a parabola which fits the constraints stated below:

- (1) The unloading curve starts at the point of maximum deflection Ω_k with the force F_k .
- (2) The unloading curve goes to zero at the point where deflection equals the permanent deformation (i.e., $G \Omega$ by definition of G).
- (3) The total work done by the unloading curve (the conserved energy in the contact) is RE_k where E_k is the total energy and R is the ratio of conserved to total energy as defined above. The total energy is computed by a stepwise approximation through the loading portion of the cycle and

E_{1k} which appears in the formulas above is computed as RE_k . Since G and R are not really independent, a constraint:

$$2E_{1k} \leq F_k \Omega_k (1-G) \leq 3E_{1k} \quad (\text{II.D.7})$$

is applied to insure that the force goes to zero at $\delta = G\Omega_k$. The constraint equation (II.D.7) comes about from evaluation of the roots of the unloading curve. The conditions that $G\Omega_k$ be the larger root and that the unloading curve increase for increasing deflection at that point yield the two halves of the constraint.

Loading followed by unloading constitutes one cycle. Provision is made for accumulating permanent deformations over several cycles. The effect of this accumulation is used to determine the starting point of succeeding cycles; however, the shape of the loading curve is always the same as the first cycle. The unloading curve is recomputed for each cycle.

The saturation feature is illustrated in Figure 8. During loading of a surface, the usual polynomial is used to compute the force. When a specified saturation force level is reached, this value is used as deflection increases. When unloading (δ negative) occurs, a specified linear slope is used to reduce force to zero. For reloadings, the polynomial loading curve is moved to the permanent deformation or turn-around position whichever applicable and the standard loading sequence restarts including the possibility of saturation.

The contribution to the equations of motion due to contact forces is a sum of the effects of the many possible interactions. For each passenger position, the number of possible interactions changes. In particular, the total number of interactions is fourteen for the driver (NPASGR = 1), eleven for the front right passenger (NPASGR = 2), and ten for the back seat passenger (NPASGR = 3). NS is the maximum value of the subscript k and is the above stated total number of interactions plus four.

$$Q_1 = L_1 \sum_{k=6}^{NS-3} P_k \cos(\Theta_1 - \psi_a) \quad (\text{II.D.8})$$

where a again is the corresponding a for the k as explained on page 27.

$$Q_2 = L_2 \sum_{k=6}^{NS-3} P_k \cos(\Theta_2 - \psi_a) \quad (\text{II.D.9})$$

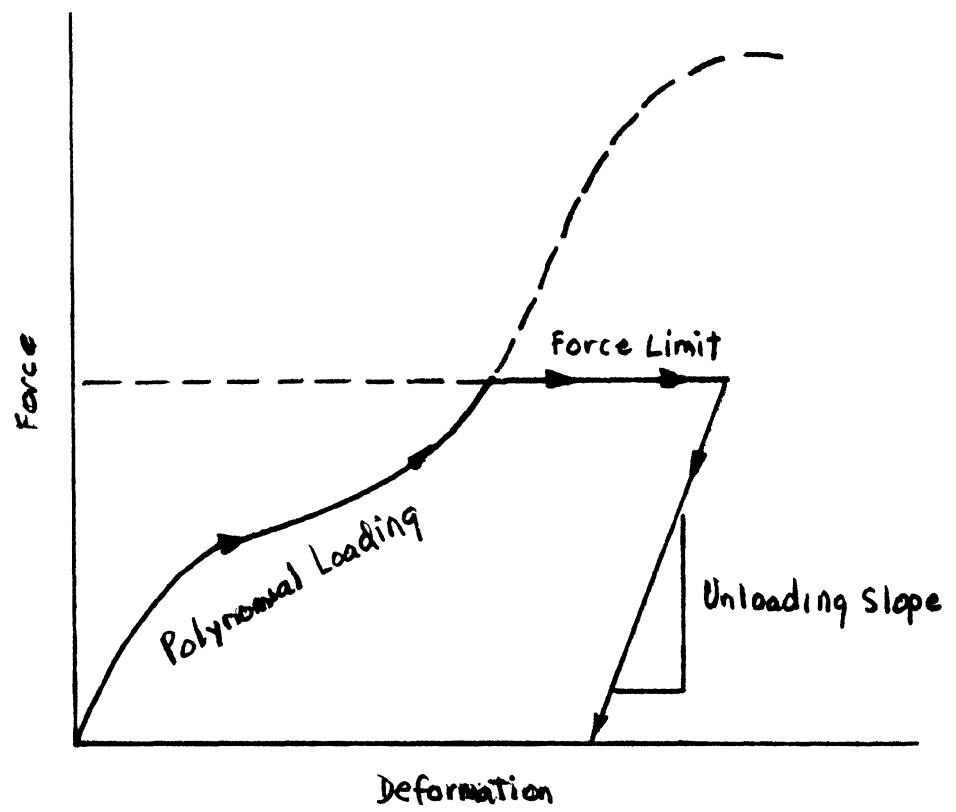


Figure 8. Force-limiting Mechanism

$$Q_3 = \rho'_3 \sum_{k=6}^L P_k \cos(\theta_3 - \psi_a) + L_3 \sum_{k=K+1}^L P_k \cos(\theta_3 - \psi_a) + L_4 P_{L+1} \cos(\theta_3 - \psi_1) \quad (\text{II.D.10})$$

$$Q_4 = \rho'_4 \sum_{k=K+1}^K P_k \cos(\theta_4 - \psi_a) \quad (\text{II.D.11})$$

$$Q_5 = L_5 P_{L+1} \cos(\theta_5 - \psi_1) \quad (\text{II.D.12})$$

where K and L are a function of NPASGR as follows:

NPASGR	K	L
1	9	14
2	7	11
3	7	10

$$Q_6 = 0$$

$$Q_7 = L_7 \sum_{k=NS-3}^{NS} P_k \cos(\theta_7 - \psi_a)$$

$$Q_8 = L_8 \sum_{k=NS-1}^{NS} P_k \cos(\theta_8 - \psi_a)$$

$$Q_9 = - \sum_{k=5}^{NS} P_k \sin \psi_a$$

$$Q_{10} = \sum_{k=5}^{NS} P_k \cos \psi_a \quad (\text{II.D.13})$$

The contribution to the generalized force due to friction at the force contact is of the form

$$\Delta \vec{b}_q = P'_k \vec{U}_i \quad (\text{II.D.14})$$

where P'_k is the computed frictional force explained on page 26 corresponding to the normal force P_k .

\vec{U}_i is the proper "lever arm" vector defined below for the value of the contact arc subscript corresponding to k . The quantity a is the matching contact surface subscript for the k in what follows.

Where

$$\vec{U}_1 = \begin{bmatrix} -r_1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ -\cos \psi_a \\ -\sin \psi_a \end{bmatrix} \quad (\text{II.D.15})$$

$$\vec{U}_2 = 0 \quad (\text{II.D.16})$$

$$\vec{U}_3 = \begin{bmatrix} L_1 \sin (\theta_1 - \psi_a) \\ L_2 \sin (\theta_2 - \psi_a) \\ \rho'_3 \sin (\theta_3 - \psi_a) - r_3 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ -\cos \psi_a \\ -\sin \psi_a \end{bmatrix} \quad (\text{II.D.17})$$

$$\vec{U}_4 = \begin{bmatrix} L_1 \sin (\theta_1 - \psi_a) \\ L_2 \sin (\theta_2 - \psi_a) \\ L_3 \sin (\theta_3 - \psi_a) \\ \rho_4' \sin (\theta_4 - \psi_a) - r_4 \\ 0 \\ 0 \\ 0 \\ 0 \\ -\cos \psi_a \\ -\sin \psi_a \end{bmatrix} \quad (\text{II.D.18})$$

$$\vec{U}_5 = \begin{bmatrix} L_1 \sin (\theta_1 - \psi_a) \\ L_2 \sin (\theta_2 - \psi_a) \\ L_4 \sin (\theta_3 - \psi_a) \\ 0 \\ L_5 \sin (\theta_5 - \psi_a) - r_5 \\ 0 \\ 0 \\ 0 \\ -\cos \psi_a \\ -\sin \psi_a \end{bmatrix} \quad (\text{II.D.19})$$

$$\vec{U}_6 = 0 \quad (\text{II.D.20})$$

$$\vec{U}_7 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ L_7 \sin (\theta_7 - \psi_a) - r_7 \\ 0 \\ -\cos \psi_a \\ -\sin \psi_a \end{bmatrix} \quad (\text{II.D.21})$$

$$\vec{U}_8 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ L_7 \sin (\theta_7 - \psi_a) \\ L_8 \sin (\theta_7 - \psi_a) - r_8 \\ -\cos \psi_a \\ -\sin \psi_a \end{bmatrix} \quad (\text{II.D.22})$$

E. SEAT CUSHION

The seat cushion model contains provision for four separate forces as shown in Figure 9. The first one acts vertically at the hip joint whenever it is above the seat cushion and is modeled by a third order polynomial spring and a linear damper. The second, modeled by a linear spring, acts vertically at the front edge of the seat and affects the upper or lower leg depending on the size of the occupant and his position. This is especially useful in the case of children whose lower legs often are on the seat cushion. The third force, also modeled by a linear spring, acts in a forward direction at the top of the front edge of the seat. This force was included to prevent the lower legs from passing backward through the seat and producing large spurious forces. All three of these forces are continuous. The fourth force models seat friction and is discontinuous as well as dissipative. The force applied at the hip is

$$F_s = W_o - \sum_{m=1}^3 \beta_m y_s^m - C_s \dot{y}_s \quad (\text{II.E.1})$$

where

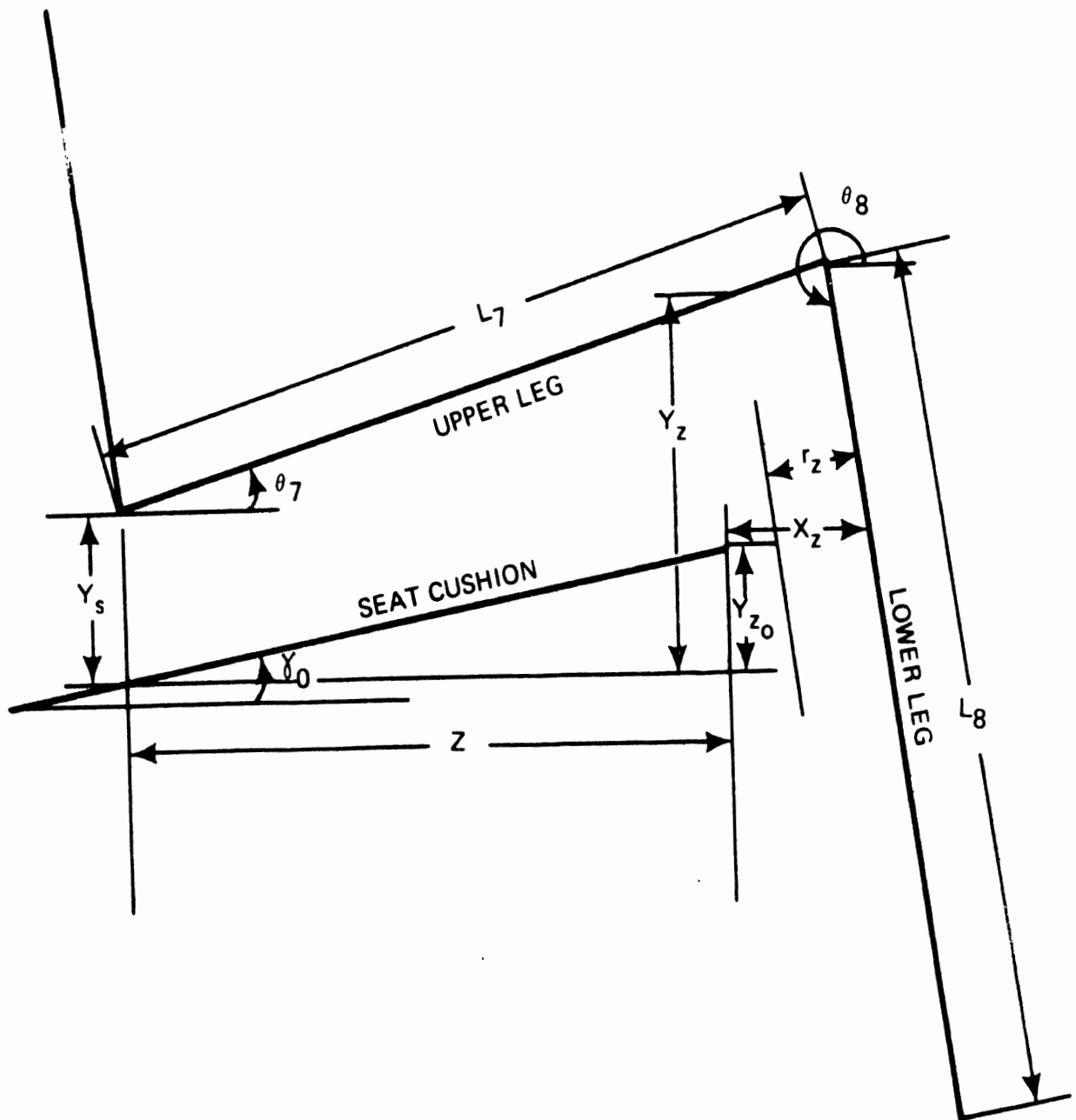


Figure 9. Description of seat bottom.

$$y_s = y + (\lambda - x) \tan \gamma_0$$

$$\dot{y}_s = \dot{y} + (\dot{\lambda} - \dot{x}) \tan \gamma_0$$

W_0 = equilibrium force on seat cushion at hip

β_m = polynomial spring constants

C_s = damping constant

λ = horizontal position of seat as a function of time

x = horizontal position of hip as a function of time

y = vertical position of hip as a function of time (II.E.2)

The force acting vertically at the at the front edge of the seat cushion is

$$F'_s = F'_{s0} - s(y_z - y_{z0}) \quad (\text{II.E.3})$$

where

$$y_z = \begin{cases} y + z \tan \theta_7 & \text{for the upper leg} \\ y + L_7 \sin \theta_7 + (z - L_7 \cos \theta_7) \tan \theta_8 & \text{for the lower leg} \end{cases} \quad (\text{II.E.4})$$

and

$$z = z_0 + \lambda - x$$

F'_{s0} = initial upward force at front of seat

s = spring constant

y_{z0} = vertical distance from seat front edge to level of seat cushion directly below hip joint at time zero

z_0 = initial value of z

with all other quantities defined in Figure 9.

The force acting horizontally at the front edge of the seat is

$$F_z = \begin{cases} s_z(r_z - x_z) & \text{for } x_z - r_z < 0 \\ 0 & \text{otherwise} \end{cases} \quad (\text{II.E.5})$$

where

$$x_z = (z_0 \tan \gamma_0 - y - L_7 \sin \theta_7) \frac{\cos \theta_8}{\sin \theta_8} - (z - L_7 \cos \theta_7)$$

s_z = spring constant

r_z = distance from centerline of lower leg to outside of calf

and the other quantities are previously defined.

(II.E.6)

The friction force is

$$f = \begin{cases} -\mu_s (F_s + F'_s) \operatorname{sgn}(\dot{X} - \dot{x}) & \text{for } |\dot{X} - \dot{x}| \geq \xi_s \\ 0 & \text{otherwise} \end{cases} \quad (\text{II.E.7})$$

where

μ_s = friction coefficient

The contributions from the seat cushion to the generalized force vector, \vec{D} , are:

$$D_i = 0, \quad i = 1-6$$

$$D_7 = \begin{cases} F'_s z \sec^2 \theta_7 & \text{for } z \leq L_7 \cos \theta_7 \\ F'_s L_7 (\cos \theta_7 + \sin \theta_7 \tan \theta_8) - F_z L_7 \cdot \\ (\sin \theta_7 + \cos \theta_7 \cot \theta_8) & \text{for } z > L_7 \cos \theta_7 \end{cases} \quad (\text{II.E.8})$$

$$D_8 = \begin{cases} 0 & \text{for } z \leq L_7 \cos \theta_7 \\ F'_s (z - L_7 \cos \theta_7) \sec^2 \theta_8 + F_z (y + L_7 \sin \theta_7 - y_{z_0}) \csc^2 \theta_8 \\ \text{otherwise} \end{cases}$$

$$D_9 = \begin{cases} -F'_s \tan \theta_7 & \text{for } z \leq L_7 \cos \theta_7 \\ -F'_s \tan \theta_8 + F_z & \text{otherwise} \end{cases}$$

$$D_{10} = F_s + F'_s - F_z \cot \theta_8 \quad (\text{II.E.9})$$

The components of the contribution of seat friction to the generalized force vector, $\Delta \vec{b}_s$, are

$$\Delta b_i = \begin{cases} 0 & \text{for } i = 1-8, 10 \\ -f & \text{for } i = 9 \end{cases} \quad (\text{II.E.10})$$

F. JOINTS

Each joint is considered to have an elastic torque resisting motion away from its initial position, a coulomb-type friction resisting any relative motion above a certain velocity limit (see Figure 10), and a joint stop to prevent substantial motion beyond specified angular limits (see Figure 11 or Figure 12).

The contribution to the system potential energy from torque is defined by

$$J_{ei} = K_i (\theta_m - \theta_i + \theta_{i0} - \theta_{m0}) \quad \text{for } i = 1-7 \quad (\text{II.F.1})$$

(see Table I for joints associated with each subscript), with each i defining a unique m as follows for calculation of proper relative angle.

i	1	2	3	4	5	6	7
m	7	1	2	3	3	5	8

The other two torques are dissipative in nature. The coulomb friction equation is:

$$J_{fi} = \begin{cases} -C_i' \operatorname{sgn}(\dot{\theta}_i - \dot{\theta}_m) & \text{for } |\dot{\theta}_i - \dot{\theta}_m| \geq \xi_i \\ 0 & \text{otherwise} \end{cases} \quad (\text{II.F.2})$$

Also the stop torque is of the same type:

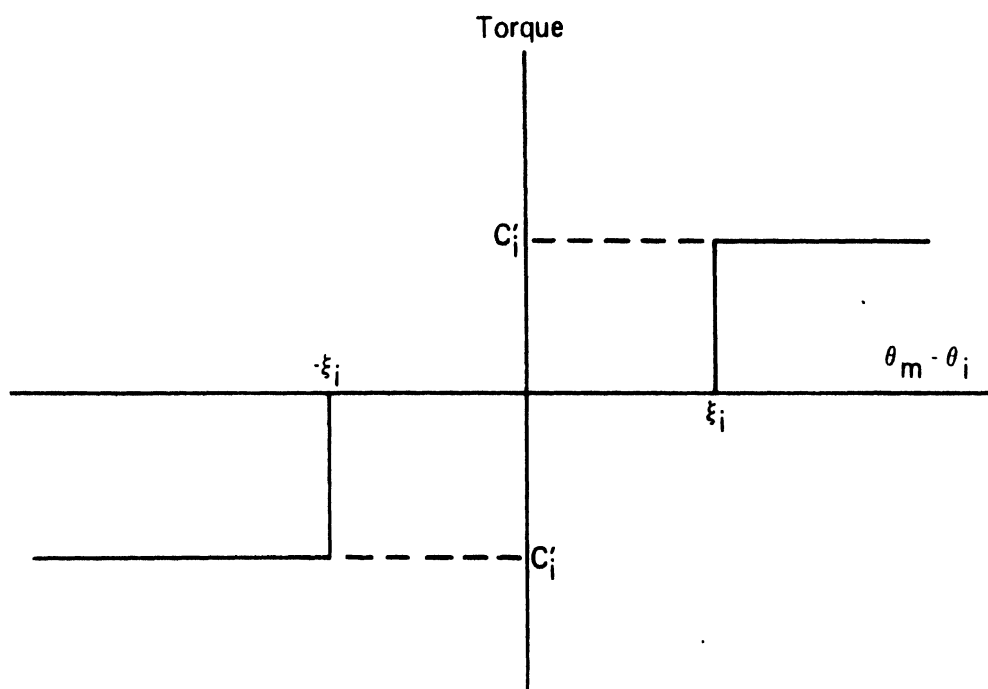


Figure 10. Form of friction in joints.

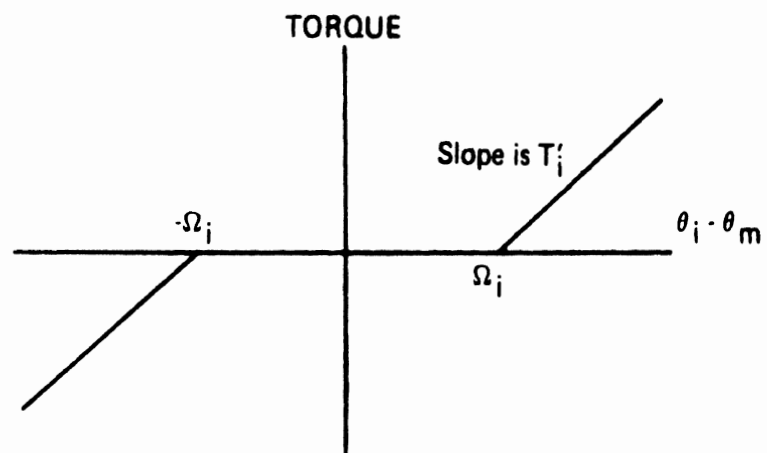


Figure 11. Form of symmetric joint stops for neck and two spinal joints.

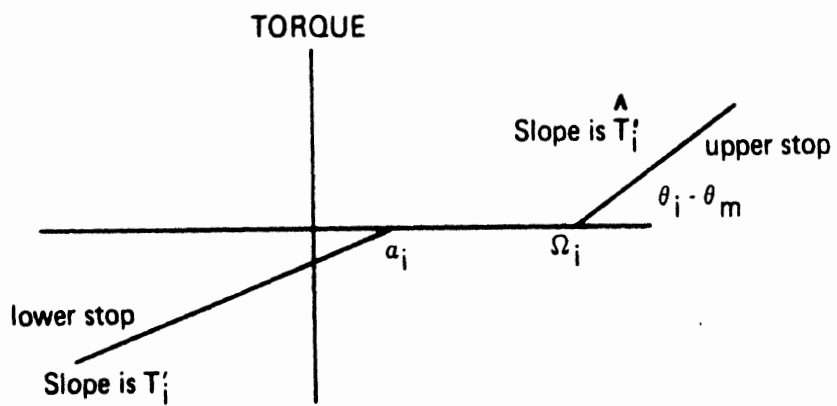


Figure 12. Form of nonsymmetric joint stops of hip, shoulder, elbow, and knee.

$$J_{si} = \begin{cases} T_i & \text{for } |\dot{\theta}_i - \dot{\theta}_m| \geq \xi_i \\ 0 & \text{otherwise} \end{cases} \quad (\text{II.F.3})$$

where the form of T_i depends on the particular joint.

The elements of the stop torque vector are defined as follows.

$$T_1 = \begin{cases} T_1' (\alpha_1 - \theta_1 + \theta_7) & \text{for } \theta_1 - \theta_7 < \alpha_1 \text{ and } \dot{\theta}_1 - \dot{\theta}_7 < 0 \\ \hat{T}_1' (\Omega_1 - \theta_1 - \theta_7) & \text{for } \theta_1 - \theta_7 > \Omega_1 \text{ and } \dot{\theta}_1 - \dot{\theta}_7 > 0 \\ 0 & \text{otherwise} \end{cases}$$

$$T_2 = \begin{cases} T'_2[\theta_1 - \theta_2 - \Omega_2 \operatorname{sgn}(\theta_1 - \theta_2)] & \text{for } |\theta_1 - \theta_2| > \Omega_2 \\ & \text{and } \operatorname{sgn}(\dot{\theta}_1 - \dot{\theta}_2) = \operatorname{sgn}(\theta_1 - \theta_2) \\ 0 & \text{otherwise} \end{cases}$$

$$T_3 = \begin{cases} T'_3[\theta_2 - \theta_3 - \Omega_3 \operatorname{sgn}(\theta_2 - \theta_3)] & \text{for } |\theta_2 - \theta_3| > \Omega_3 \\ & \text{and } \operatorname{sgn}(\dot{\theta}_2 - \dot{\theta}_3) = \operatorname{sgn}(\theta_2 - \theta_3) \\ 0 & \text{otherwise} \end{cases}$$

$$T_4 = \begin{cases} T'_4[\theta_3 - \theta_4 - \Omega_4 \operatorname{sgn}(\theta_3 - \theta_4)] & \text{for } |\theta_3 - \theta_4| > \Omega_4 \\ & \text{and } \operatorname{sgn}(\dot{\theta}_3 - \dot{\theta}_4) = \operatorname{sgn}(\theta_3 - \theta_4) \\ 0 & \text{otherwise} \end{cases}$$

$$T_5 = \begin{cases} T'_5(\theta_3 - \theta_5 - \alpha_5) & \text{for } \theta_3 - \theta_5 < \alpha_5 \text{ and } \dot{\theta}_3 - \dot{\theta}_5 < 0 \\ \hat{T}'_5(\theta_3 - \theta_5 - \Omega_5) & \text{for } \theta_3 - \theta_5 > \Omega_5 \text{ and } \dot{\theta}_3 - \dot{\theta}_5 > 0 \\ 0 & \text{otherwise} \end{cases}$$

$$T_6 = \begin{cases} T'_6(\theta_5 - \theta_6 + \alpha_6) & \text{for } \theta_6 - \theta_5 < \alpha_6 \text{ and } \dot{\theta}_5 - \dot{\theta}_6 > 0 \\ \hat{T}'_6(\theta_5 - \theta_6 + \Omega_6) & \text{for } \theta_6 - \theta_5 > \Omega_6 \text{ and } \dot{\theta}_5 - \dot{\theta}_6 < 0 \\ 0 & \text{otherwise} \end{cases}$$

$$T_7 = \begin{cases} T'_7(\alpha_7 - \theta_7 + \theta_8) & \text{for } \theta_7 - \theta_8 < \alpha_7 \text{ and } \dot{\theta}_8 - \dot{\theta}_7 > 0 \\ \hat{T}'_7(\Omega_7 - \theta_7 + \theta_8) & \text{for } \theta_7 - \theta_8 > \Omega_7 \text{ and } \dot{\theta}_8 - \dot{\theta}_7 < 0 \\ 0 & \text{otherwise} \end{cases}$$

(II.F.4)

Note that the neck and the two spinal joints are assumed symmetric, while the hip, shoulder, elbow and knee are not.

The joint elasticity generalized force vector is:

$$\begin{aligned}
 c_1 &= K_1(\theta_7 - \theta_1 + \theta_{10} - \theta_{70}) - K_2(\theta_1 - \theta_2 + \theta_{20} - \theta_{10}) \\
 c_2 &= K_2(\theta_1 - \theta_2 + \theta_{20} - \theta_{10}) - K_3(\theta_2 - \theta_3 + \theta_{30} - \theta_{20}) \\
 c_3 &= K_3(\theta_2 - \theta_3 + \theta_{30} - \theta_{20}) - K_4(\theta_3 - \theta_4 + \theta_{40} - \theta_{30}) \\
 &\quad - K_5(\theta_3 - \theta_5 + \theta_{50} - \theta_{30}) \\
 c_4 &= K_4(\theta_3 - \theta_4 + \theta_{40} - \theta_{30}) \\
 c_5 &= K_5(\theta_3 - \theta_5 + \theta_{50} - \theta_{30}) - K_6(\theta_5 - \theta_6 + \theta_{60} - \theta_{50}) \\
 c_6 &= K_6(\theta_5 - \theta_6 + \theta_{60} - \theta_{50}) \\
 c_7 &= K_7(\theta_8 - \theta_7 + \theta_{70} - \theta_{80}) - K_1(\theta_7 - \theta_1 + \theta_{10} - \theta_{70}) \\
 c_8 &= K_7(\theta_7 - \theta_8 + \theta_{80} - \theta_{70}) \\
 c_9 &= 0 \\
 c_{10} &= 0
 \end{aligned} \tag{II.F.5}$$

Joint friction and the joint stops are applied to the generalized force vector by the equation

$$\Delta \vec{b}_j = (J_{fi} + J_{si}) \vec{V}_i \tag{II.F.6}$$

where \vec{V}_i is a vector whose components are all zero except for the ith and the mth which are plus one and minus one, respectively.

The i is the joint index and m is as specified previously on page 36.

G. RESTRAINT SYSTEM

The conventional restraint system simulated in this program consists of a set of three belt segments, all of whose forces act independently at fixed points on the body.

The shoulder harness is modeled by two such independent segments (see Figure 13); the upper is assumed to act at the shoulder joint, the lower at a specified distance above the first spinal joint. Both segments have their attachment points fixed in the vehicle and the forces act along the lines connecting the point on the occupant with the belt attachment points in the vehicle.

The lap belt is modeled by one segment, thus assuming that the two sides of the real lap belt have the same fixed attachment point coordinates in the plane of motion. The force produced is twice that of one real segment. The shape of the lap belt segment is more complicated than that of the shoulder harness segments. It has not only a linear portion, but also a circular arc portion centered on the hip joint (see Figure 14). The linear portion is tangent to this circle.

An option in the program allows the user to specify no belts, lap belt only, shoulder harness only, or all three segments. Unconventional restraint systems such as an airbag may be crudely simulated by proper selection of contact surfaces.

For each of the three belt segments, elongation is computed as the current length (l_k) minus the zero-time length (l_{k0}). Deflection rate ($\dot{\delta}$) is just \dot{l}_k . The same load-deflection procedure is used to compute force as has been previously used for contact forces including the force-limiting feature which allows studies of energy-absorbing belts. The quantity ϕ_k is the belt angle for the corresponding segment.

For the lap belt, the following equations apply (see Figure 14).

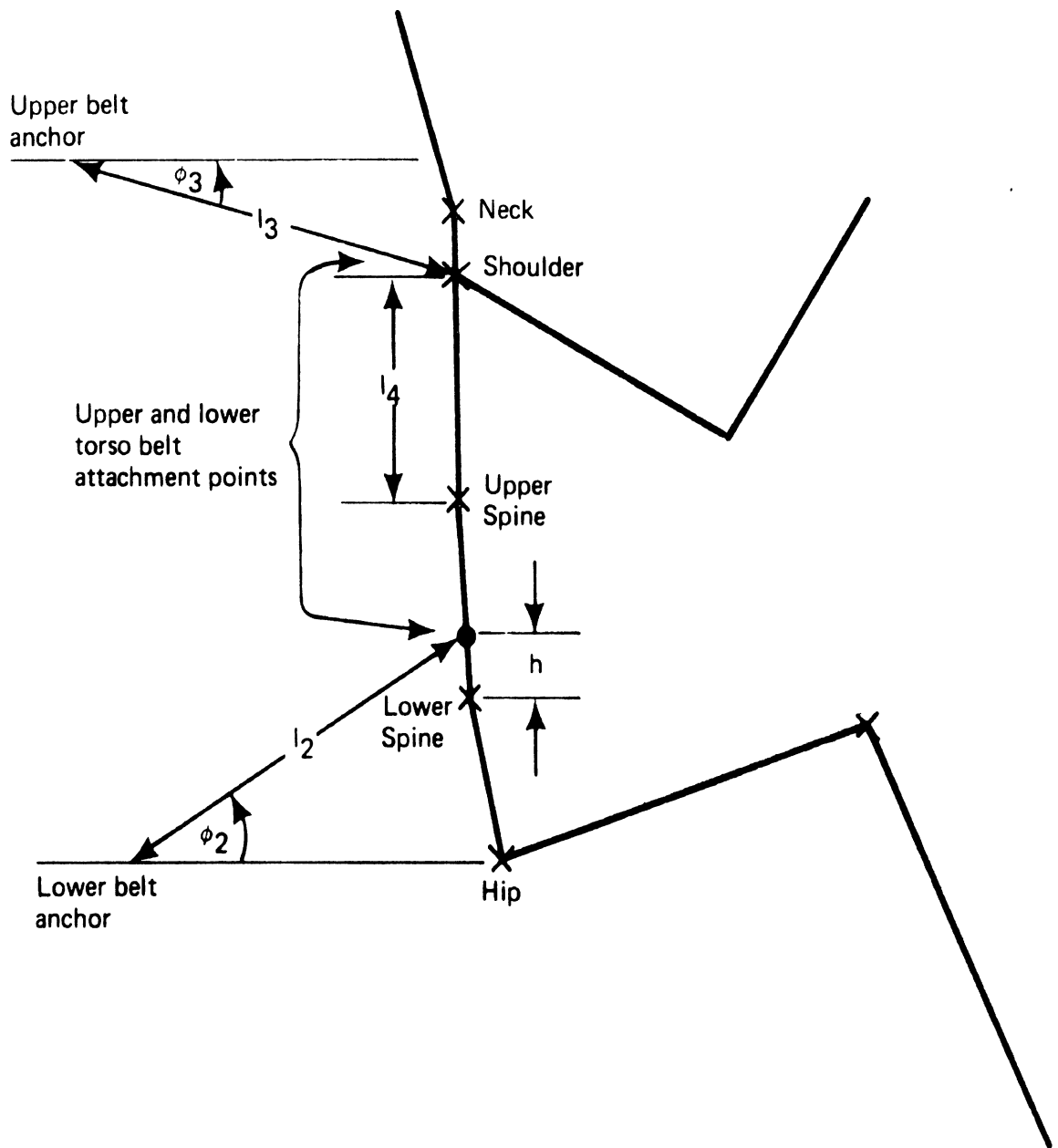


Figure 13. Shoulder belt geometry.

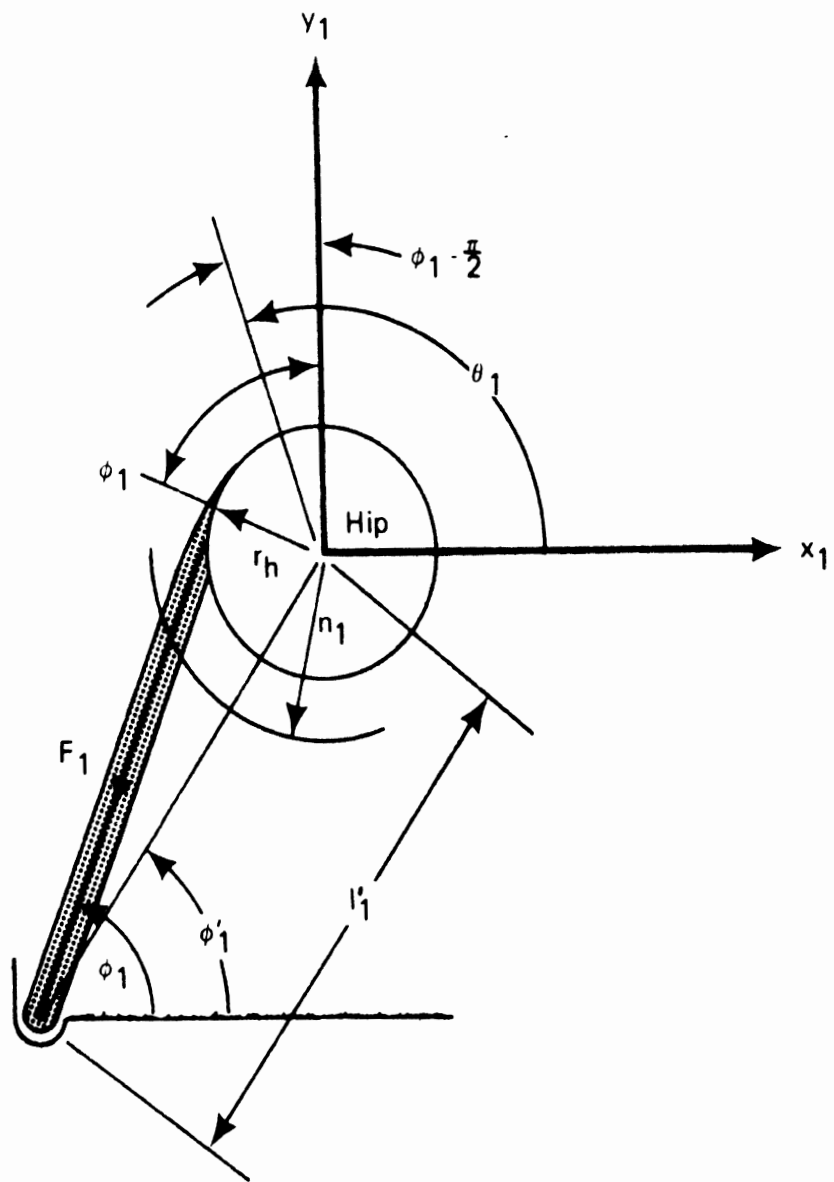


Figure 14. Lap belt geometry.

$$\begin{aligned}
l_1 &= \sqrt{(x + l'_{10} \cos \phi'_{10})^2 + (y + l'_{10} \sin \phi'_{10})^2 - r_h^2} \\
&\quad + r_h (\phi_1 - \phi_{10} + \pi/2) \\
l_{10} &= \sqrt{(l'_{10})^2 - r_h^2} + r_h (\phi_{10} - \theta_{10} + \pi/2) \\
\phi_1 &= \tan^{-1} \left(\frac{y + l'_{10} \sin \phi'_{10}}{x + l'_{10} \cos \phi'_{10}} \right) \\
&\quad + \tan^{-1} \left(\frac{r_h}{\sqrt{(x + l'_{10} \cos \phi'_{10})^2 + (y + l'_{10} \sin \phi'_{10})^2 - r_h^2}} \right) \\
\dot{l}_1 &= \dot{x} \cos \phi_1 + \dot{y} \sin \phi_1 - r_h \dot{\theta}_1 \tag{II.G.1}
\end{aligned}$$

For the lower and upper shoulder belt segments ($k = 2$ and 3 , respectively), the equations are: (see Figure 13)

$$\begin{aligned}
l_k &= \sqrt{\Delta x_k^2 + \Delta y_k^2} \quad \text{for } k = 2, 3 \\
\phi_k &= \tan^{-1} \left(\frac{\Delta y_k}{\Delta x_k} \right) \tag{II.G.2}
\end{aligned}$$

A zero appended to the subscripts of a variable denotes the zero time value of that variable.

$$\Delta x_2 = x + L_1 \cos \theta_1 + h \cos \theta_2 - L_1 \cos \theta_{10} - h \cos \theta_{20} + l_{20} \cos \phi_{20}$$

$$\Delta y_2 = y + L_1 \sin \theta_1 + h \sin \theta_2 - L_1 \sin \theta_{10} - h \sin \theta_{20} + l_{20} \sin \phi_{20}$$

$$\dot{i}_2 = \dot{x} \cos \phi_2 + \dot{y} \sin \phi_2 - L_1 \dot{\theta}_1 \sin(\theta_1 - \phi_2) - h \dot{\theta}_2 \sin(\theta_2 - \phi_2)$$

and

$$\Delta x_3 = x + L_1 \cos \theta_1 + L_2 \cos \theta_2 + L_4 \cos \theta_3 - L_1 \cos \theta_{10}$$

$$- L_2 \cos \theta_{20} - L_4 \cos \theta_{30} + l_{30} \cos \phi_{30}$$

$$\Delta y_3 = y + L_1 \sin \theta_1 + L_2 \sin \theta_2 + L_4 \sin \theta_3 - L_1 \sin \theta_{10}$$

$$- L_2 \sin \theta_{20} - L_4 \sin \theta_{30} + l_{30} \sin \phi_{30}$$

$$\dot{i}_3 = \dot{x} \cos \phi_3 + \dot{y} \sin \phi_3 - L_1 \dot{\theta}_1 \sin(\theta_1 - \phi_3)$$

$$- L_2 \dot{\theta}_2 \sin(\theta_2 - \phi_3) - L_4 \dot{\theta}_3 \sin(\theta_3 - \phi_3) \quad (\text{II.G.3})$$

The belt contributions to the generalized force vector are:

$$\begin{aligned}
D_{b1} &= r_h P_1 + L_1 \sum_{m=2}^3 P_m \sin(\theta_1 - \phi_m) \\
D_{b2} &= r P_2 \sin(\theta_2 - \phi_2) + L_2 P_3 \sin(\theta_2 - \phi_3) \\
D_{b3} &= L_4 P_3 \sin(\theta_3 - \phi_3) \\
D_{bi} &= 0, \quad i = 4-8 \\
D_{b9} &= - \sum_{m=1}^3 P_m \cos \phi_m \\
D_{b10} &= - \sum_{m=1}^3 P_m \sin \phi_m \qquad \qquad \qquad (II.G.4)
\end{aligned}$$

where P_k is the force computed by use of the load-deflection procedure for the kth segment.

III. EXPERIMENTAL VERIFICATION OF THE MATHEMATICAL MODEL

In this section of the report comparisons are made between the predictions of the mathematical model and an experiment carried out on the HSRI impact sled with an anthropometric dummy. Beginning with an outline of the criteria on which the validation is based, the report continues with a description of the sled test and concludes with a description of the degree to which the model describes the real test situation.

A. CHOICE OF A CRITERION OF VERIFICATION

The choice of a criterion of verification of the mathematical model describing human body impact is based on three premises: (a) whether or not the mathematical analysis and computer program are correct; (b) the extraction of appropriate experimental data on which the validation procedures can be based; and (c) the observation that the mathematical model consists of parameters describing the occupant, the force field consisting of belts and contact surfaces which act on the occupant, and the externally applied deceleration forcing function.

The use of a Lagrangian formulation of Newtonian mechanics as a basis for these models follows a long history of successful application to problems in impact, and hence, offers no cause for concern. Thus, sources of problems can arise only in writing down the particular equations and computer program which apply to the present analysis. All equations and the computer program have been derived independently by two or more persons leading to very low incidence of errors in the final computer program.

The second premise, which is concerned with the extraction of appropriate experimental data on which the validation can be based, has been the basis for a major research effort. The acquisition of the necessary transducer and photometric data is straightforward and requires

only the proper usage of the appropriate high speed cameras, data tape recorders, and light beam oscillographs. The processing of the transducer data is also relatively simple. For example, the determination of the magnitude of the linear acceleration of the head of the dummy requires computation of the simple vector sum of the three linear acceleration components.

Analysis and graphing of the test data is only part of the problem because preparation of a well-founded set of input data is necessary for the successful operation of any computer analysis. Therefore, a description of the mass, geometric, and inertial properties of the test subject is required. This must be supplemented by a geometrical profile of the vehicle components with which the test subject is expected to interact. Finally, the force-deformation characteristics of the interactions between the test subject and the vehicle components must be measured in order to specify the proper balance between subject motions and loadings.

In order to define the test subject, the eight basic body elements were weighed and moments of inertia measured using a trifilar pendulum or predicted using formulas similar to those of Hanavan²⁵ and Patten.²⁶ After the geometry of the test sled and the initial position of the dummy subject were carefully measured, it was then necessary to develop test procedures defining the force-motion relationships between test subject and vehicle elements. This was carried out for the seat and for a belt restraint system using a combination of photometric and transducer data described later in this report. (The simulation of an airbag restraint system was accomplished using similar techniques and will be discussed in the final report on that phase of the research project.)

The third premise serves to define the mathematical model as a system of parameters describing the occupant, the force field consisting of belts and contact surfaces which acts on the occupant, and the externally applied deceleration forcing function. All these basic parameters must

be included in any test validation.

To properly study the field of forces acting on the subject it is necessary to simulate both contact surfaces (such as a seat cushion and seat back) and belts (such as a lap belt and single diagonal shoulder harness). The use of an occupant unrestrained by belts would not provide a sufficient test of this important section of the analysis.

Based on these three premises, an impact sled test using a 50th percentile male anthropometric dummy was carried out at a speed of approximately 30 mph. This represented the most standard test configuration in use in impact sled test laboratories. The dummy was restrained by a lap belt and a single diagonal shoulder harness. Thus, this test represented a complete and economical test of the basic parameters described in the model—the occupant, the restraint and interior contact forces, and the vehicle deceleration.

B. THE EXPERIMENT

The validation experiment was carried out on the HSRI impact sled (Figure 15), which is of the acceleration-deceleration type. It can be accelerated over a 12-ft distance up to a top speed of 40 mph using a compressed air-actuated puller arm. The deceleration stroke has a maximum length of 3 ft and a maximum potential of 88 g's. For the purpose of high-speed photography a total of 50 kw of lighting is available. Real time and high-speed movies are taken as well as still photographs before and after each test.

Kistler Piezotron 818's triaxial accelerometer packs were located in the head and chest of the 50th percentile Sierra dummy. A Statham strain-gage accelerometer was used to record the sled deceleration pulse. Four Lebow seat-belt load transducers were mounted on the seat belt and shoulder harness.

The data was recorded simultaneously on a Honeywell 7600 tape recorder and a Honeywell 1612 Visicorder. No filtering was used during



Figure 15. HSRI Impact Sled

NOT REPRODUCIBLE

the initial recording other than the limitation of the light-beam galvanometers to frequencies under 1000 cps. The following transducer data was recorded: (a) lower right shoulder belt force; (b) left lap belt force; (c) upper left shoulder belt force; (d) right lap belt force; (e) sled deceleration; (f) head anterior-posterior G-loading; (g) chest anterior-posterior G-loading; (h) head superior-inferior G-loading; (i) chest superior-inferior G-loading; (j) head left-right G-loading; (k) chest left-right G-loading; (l) impact velocity; and (m) timing signals.

The test setup for the validation of the model is shown in Figure 16. The bucket seat is bolted securely to a framework which is attached to the sled. This framework serves as a mount for attaching belts and other types of restraint systems, and can be rotated to simulate lateral or oblique impact.

The test data presented in Figures 17 through 26 were obtained as a result of either detailed analysis of the high-speed films using a Vanguard Film Analyzer or by measuring points from the oscillographic recording. All acceleration and belt transducer data were determined from the oscillographic records and appropriate sums and resultant values were computed.

In the model, the excursion and forward motion of the head were determined directly by measurement of the motion of a target placed on the head of the dummy. Likewise the angle of head pitch and the upper leg were obtained by direct measurement (and the subsequent scaling and tabulation by means of specially developed computer programs). The motion of the H-point was very difficult to determine as no direct measurements were possible. However, its location was determinable by trigonometry using data from a thigh target, a lower back target, and the angle of the upper leg with a horizontal line. These data, determined on the Vanguard Analyzer, were then processed on the HSRI 1130 digital computer using the appropriate trigonometric data handling subroutines.



Figure 16. Test Setup for Two-dimensional Model Validation

NOT REPRODUCIBLE

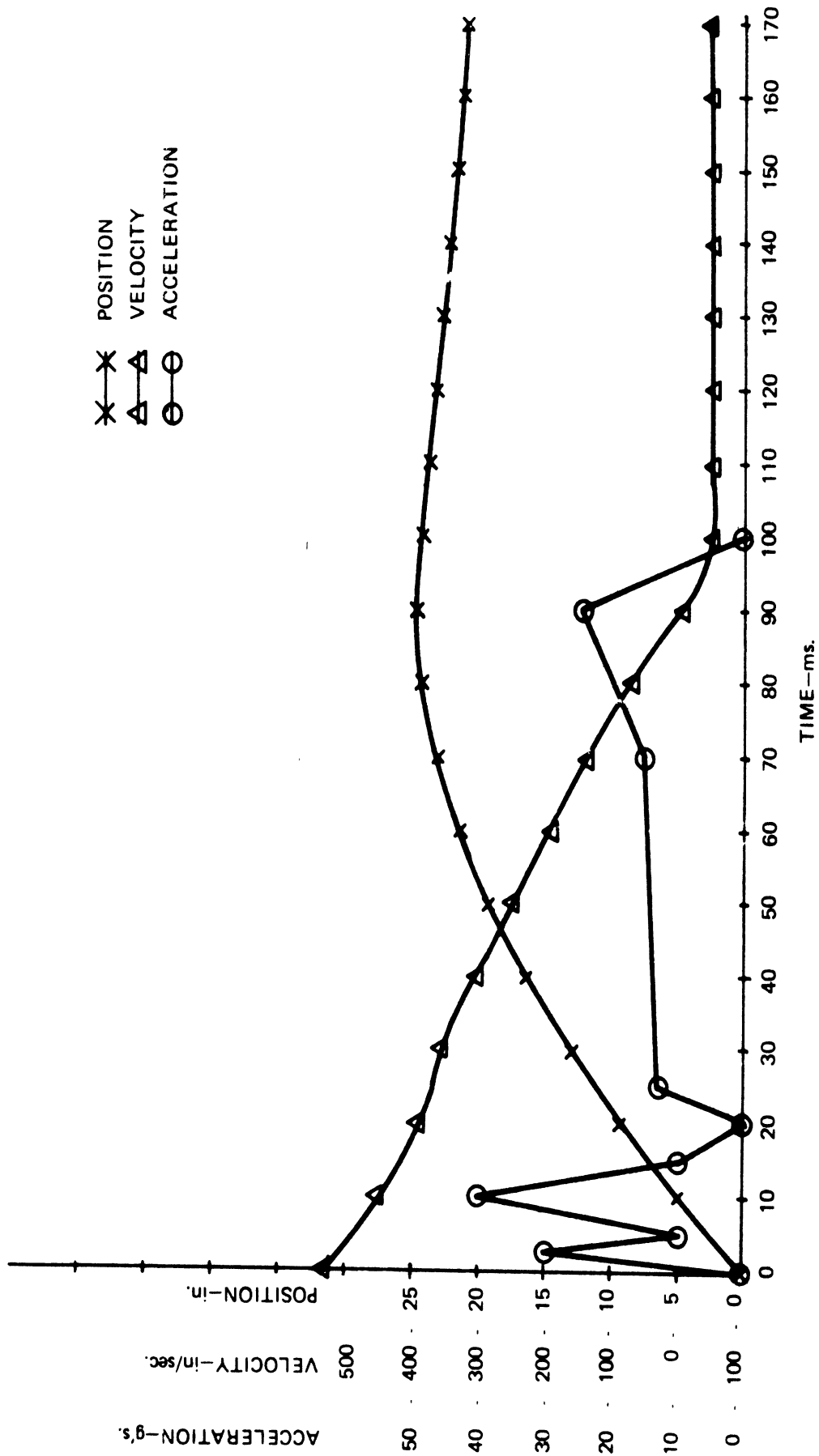


Figure 17. Vehicle Kinematics .

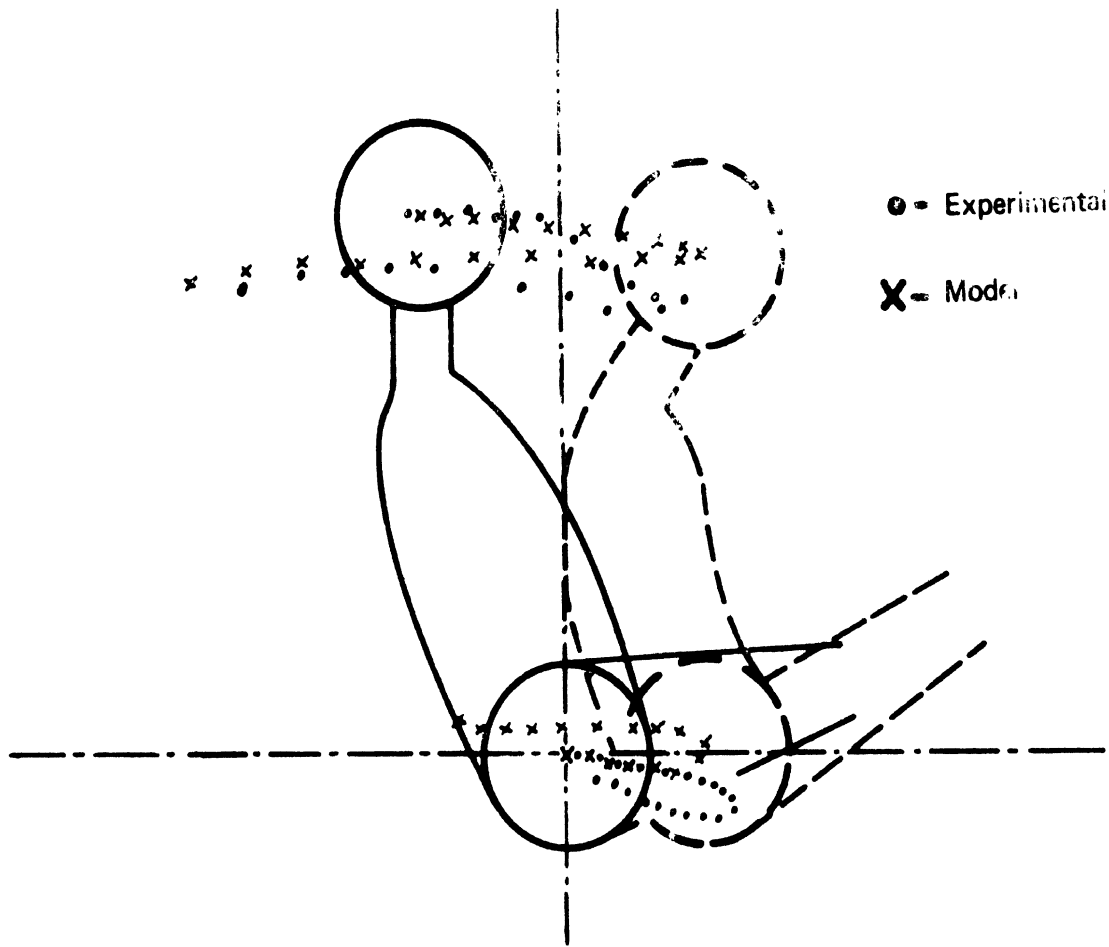


Figure 18. Excursion of head center-of-gravity and H-point as a function of time.

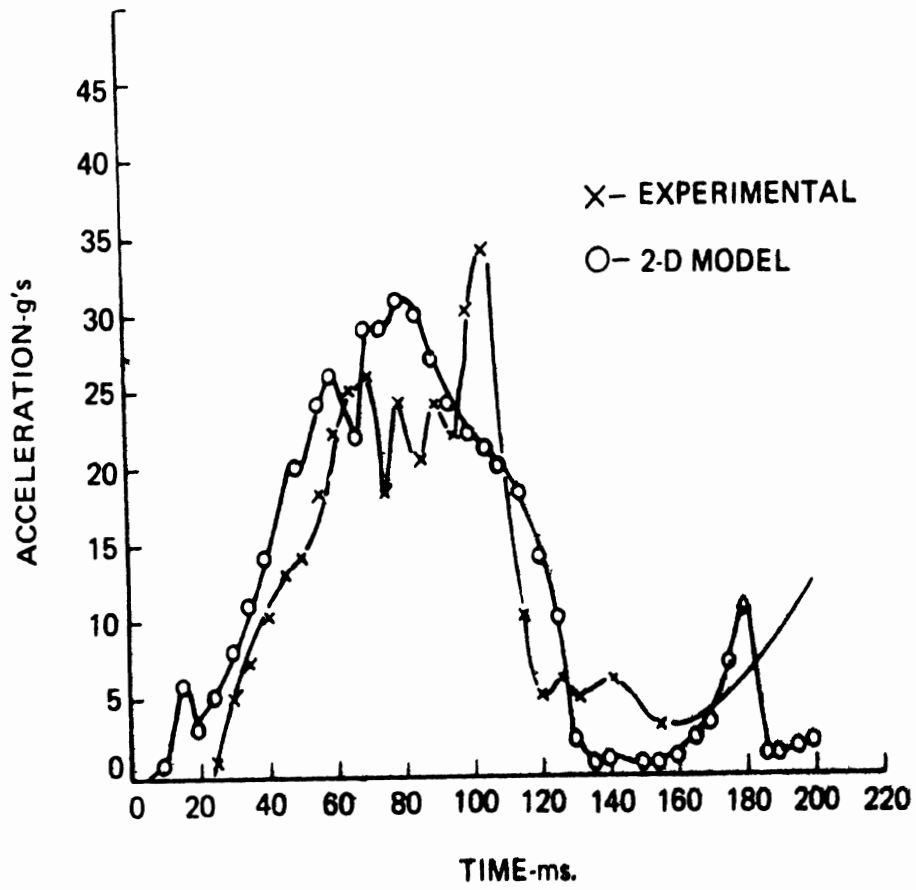


Figure 19. Resultant chest linear acceleration in g's.

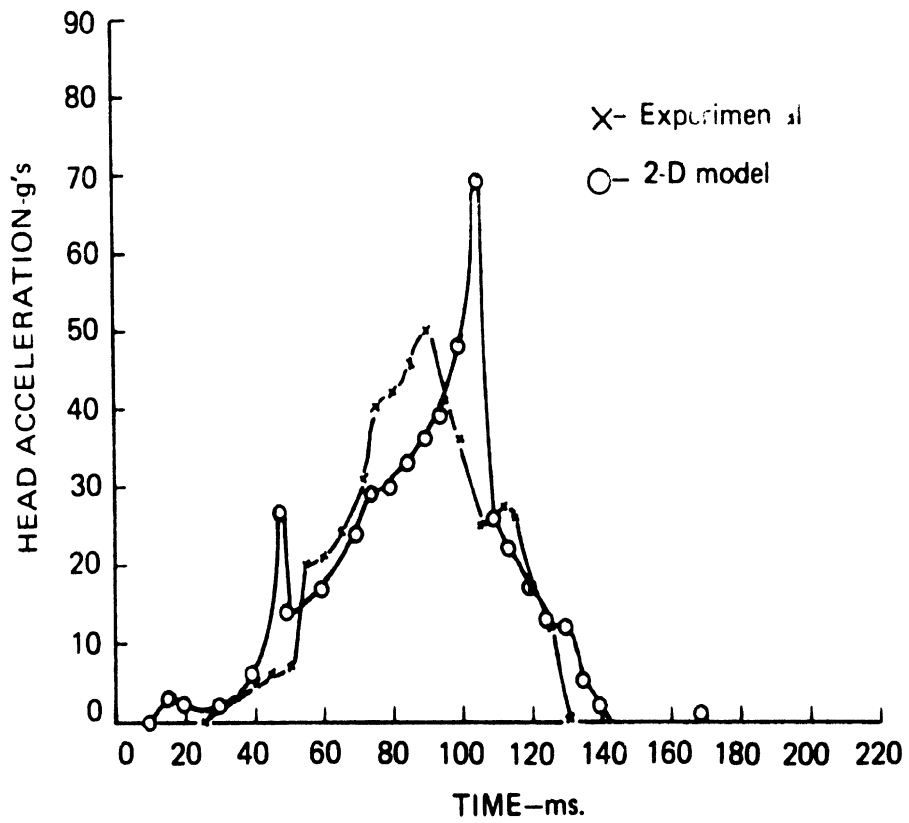


Figure 20. Resultant head linear acceleration in g's.

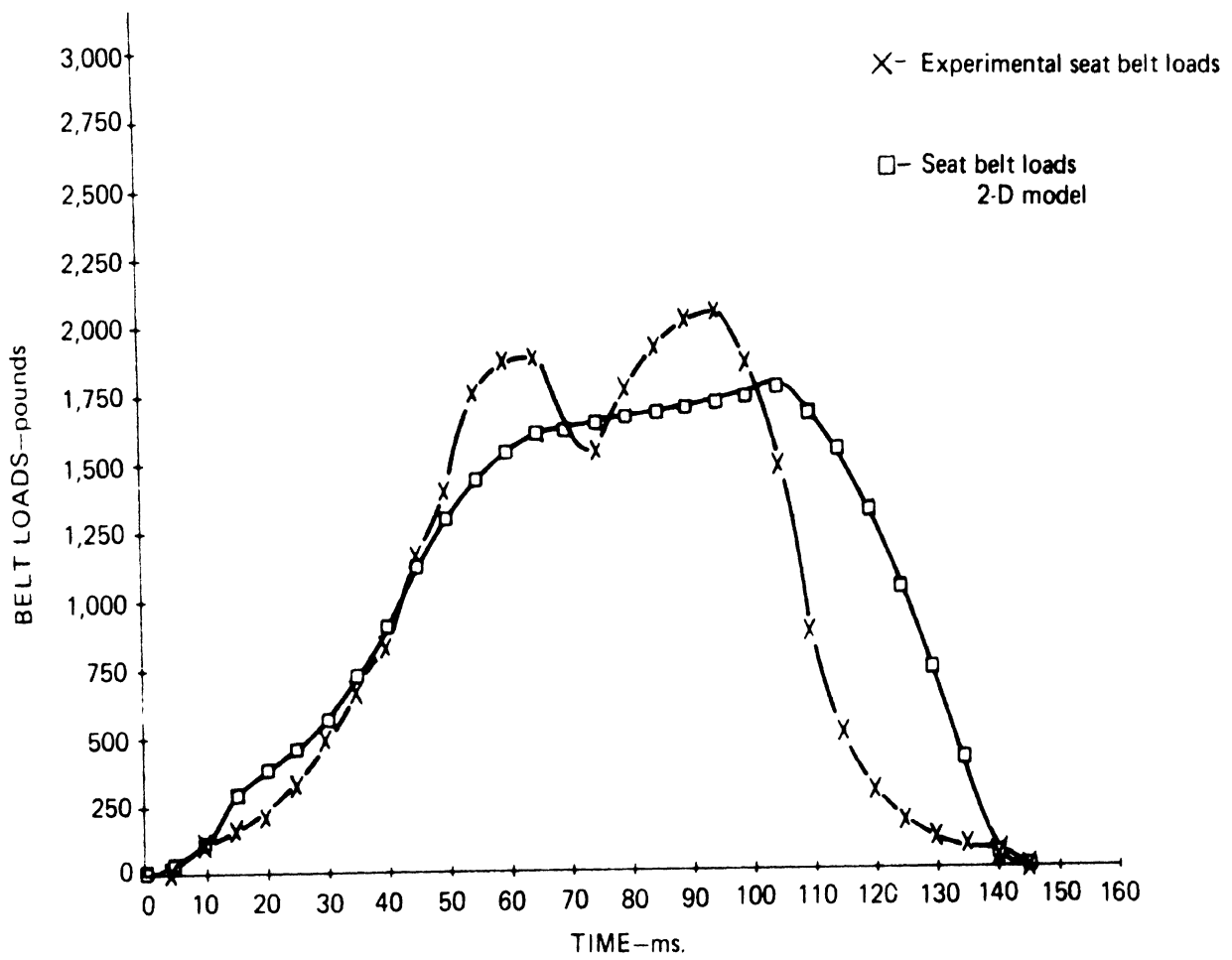


Figure 21. Seat belt loads.

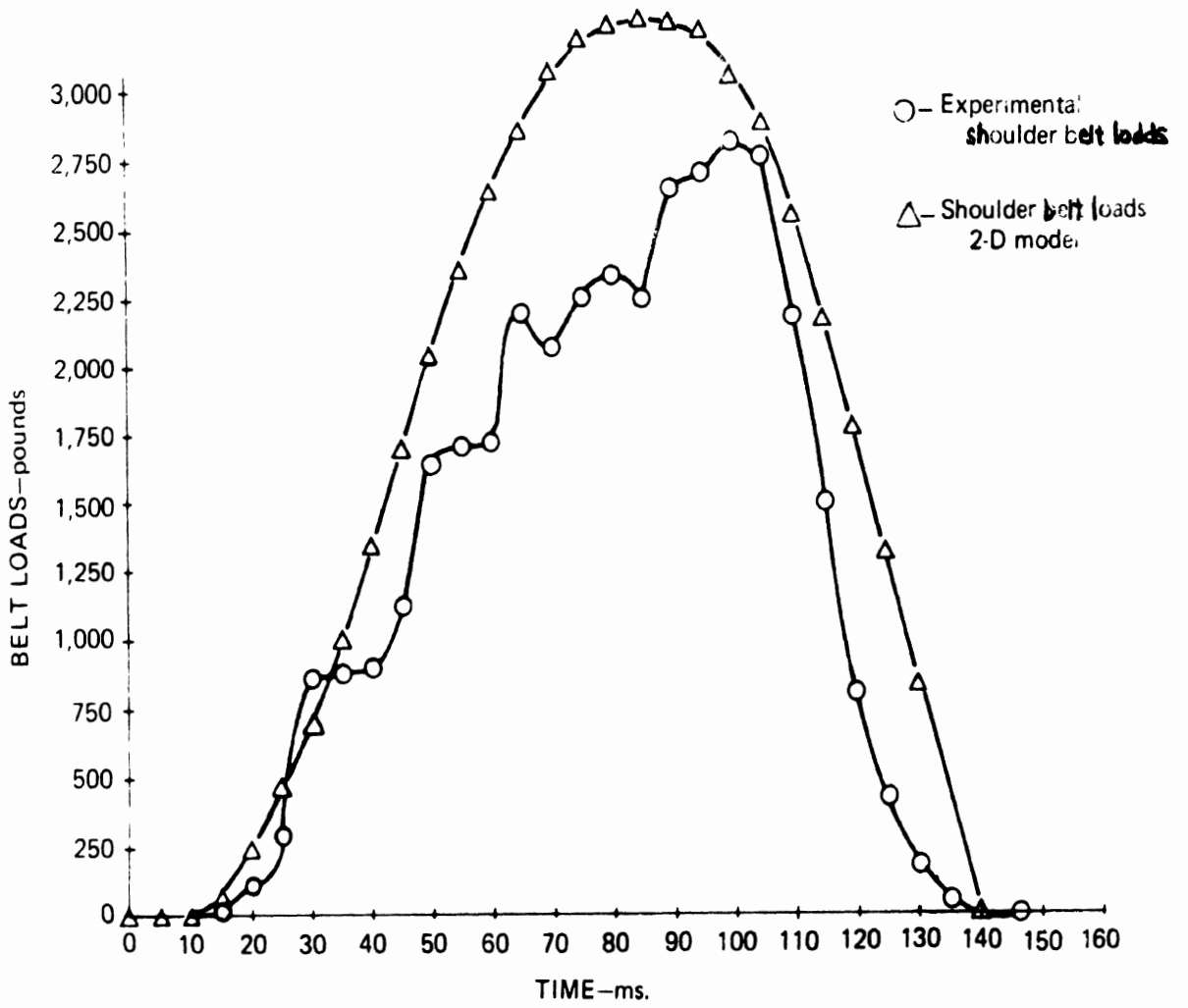


Figure 22. Shoulder harness loads.

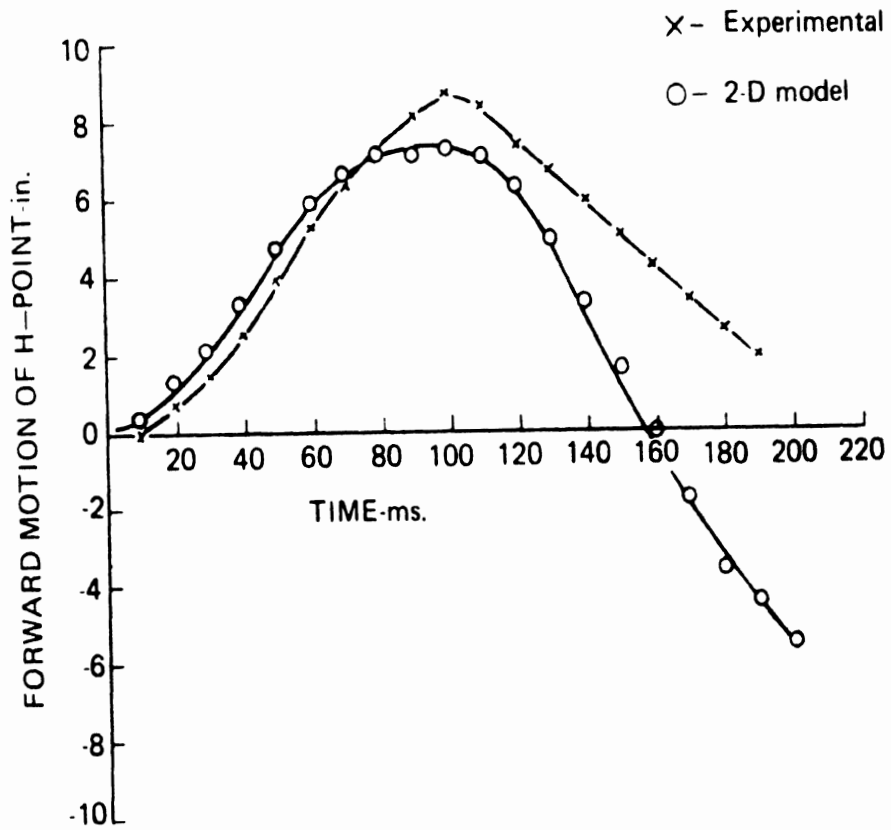


Figure 23. Forward motion of H-point.

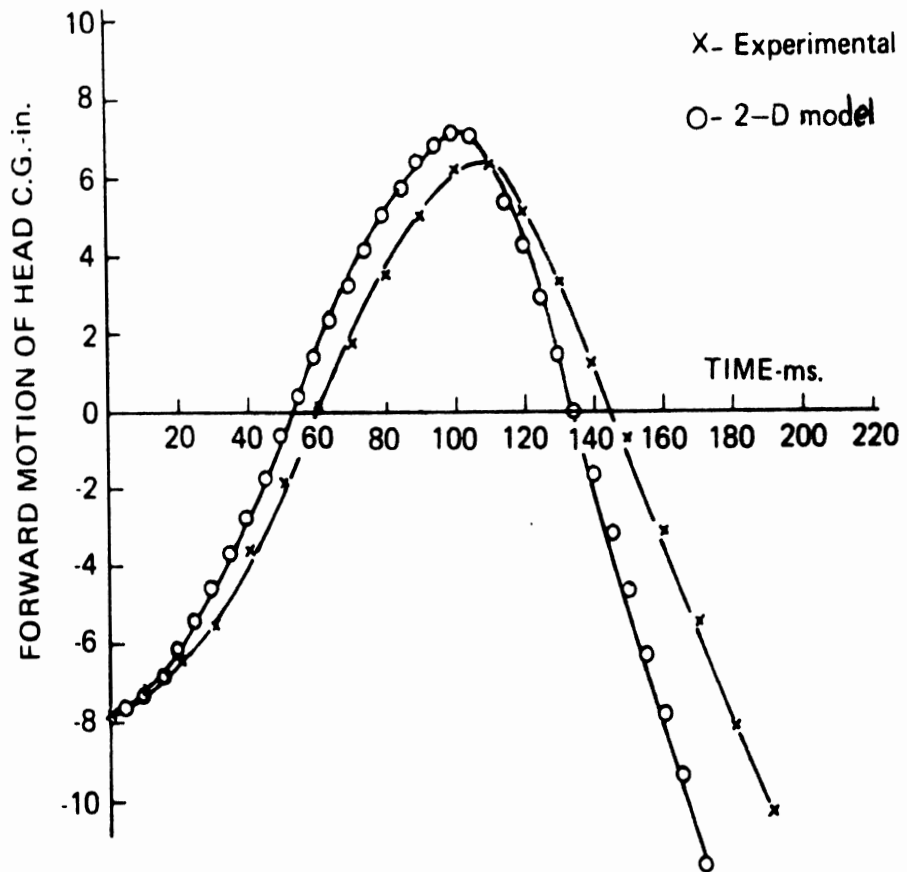


Figure 24. Forward motion of head center-of-gravity.

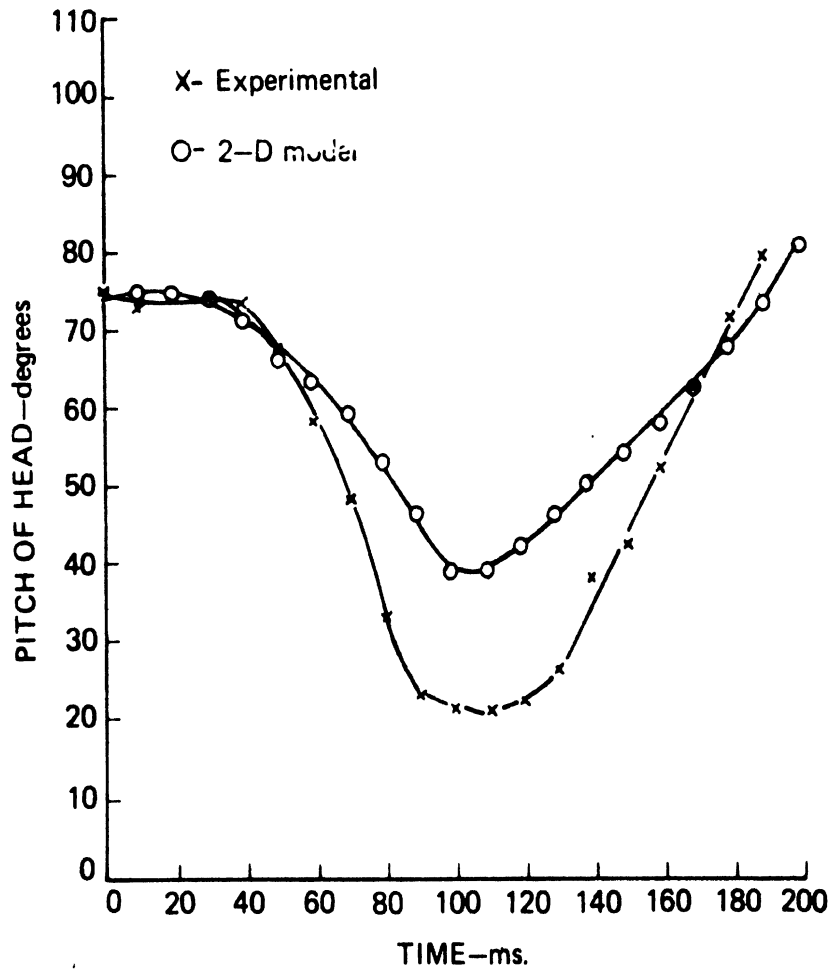


Figure 25. Pitch angle of head.

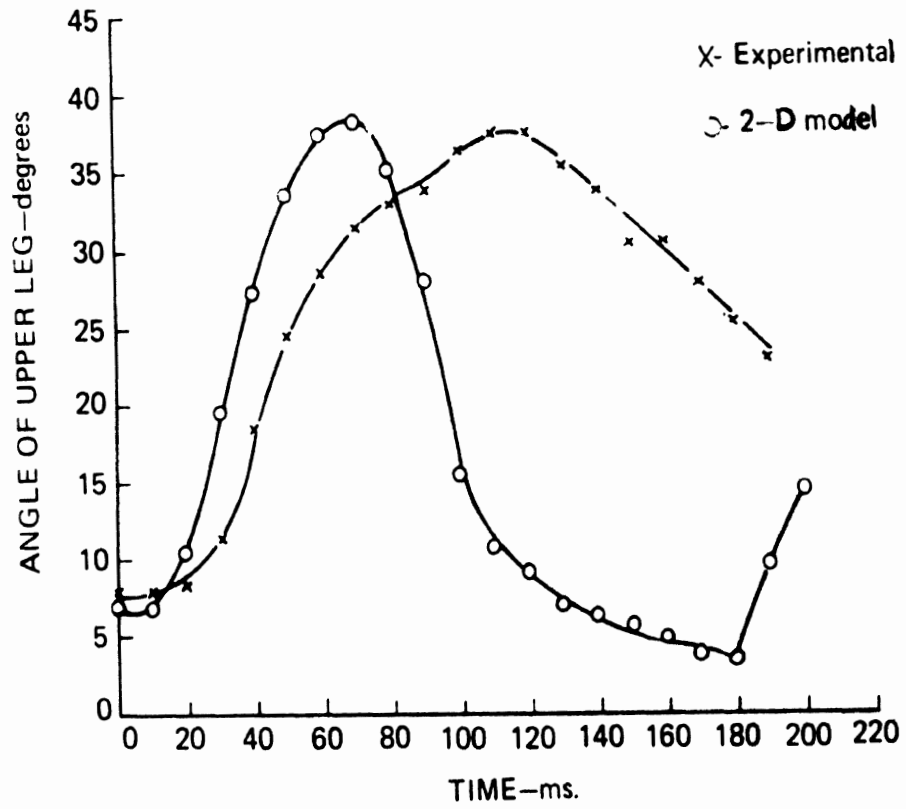
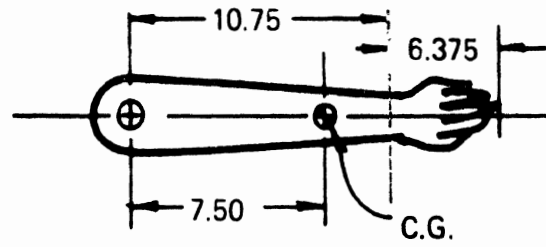
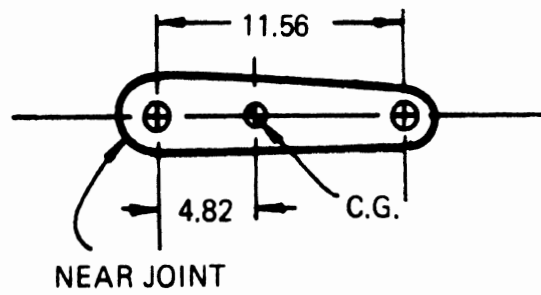


Figure 26. Pitch angle of the upper leg.

Dimensions of Forearms:



Dimensions of Upper Arms



Dimensions of Lower Spine:

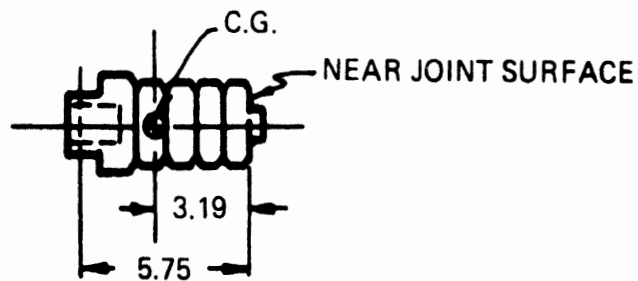
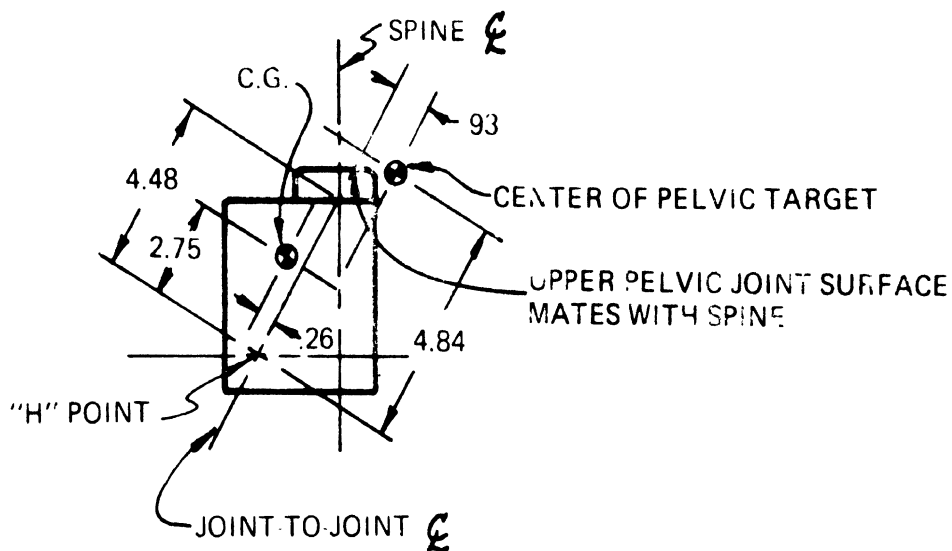
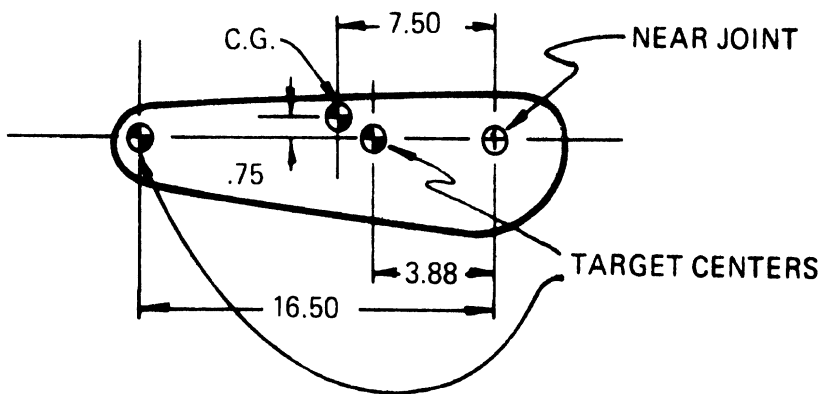


Figure 27. Centers-of-gravity and dimensions of forearms, upper arms, and lower spine.

Dimensions of Lower Torso Pelvic Area:



Dimensions of Upper Leg:



Dimensions of Lower Leg Including Foot:

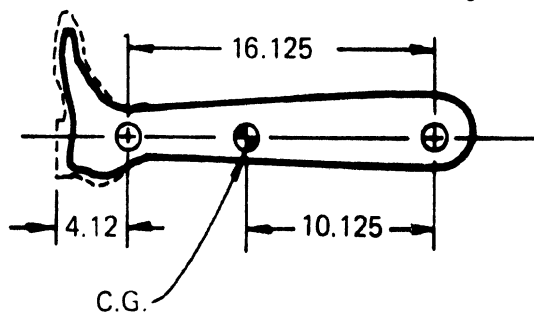
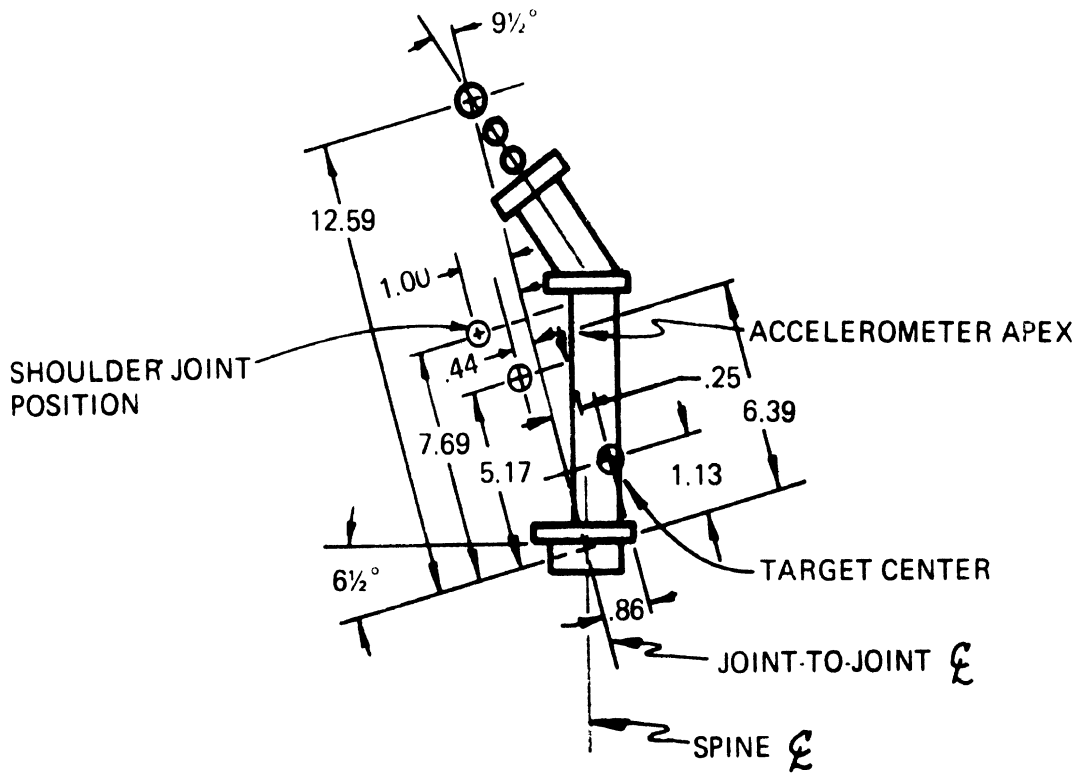


Figure 28. Centres-of-gravity and dimensions of pelvic area, upper legs, and lower legs.

Dimensions of Upper Torso Assembly.



Dimensions of Head Assembly:

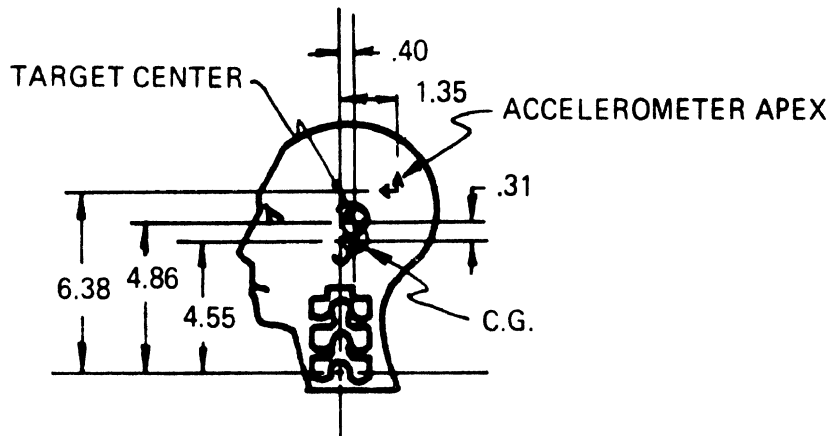


Figure 29. Centers-of-gravity and dimensions of head and upper torso.

C. PREPARATION OF A DATA SET FOR THE COMPUTER SIMULATION

The preparation of a data set for the validation exercise of the model involved determination of the mass and inertial properties of the HSRI 50th percentile male Sierra dummy as well as the force-deformation interactions between the dummy and his seat and restraint system. Various other quantities such as the initial impact velocity, the sled deceleration profile, and the positioning of the dummy at the beginning of the deceleration event were measured directly from the test movies or transducer data.

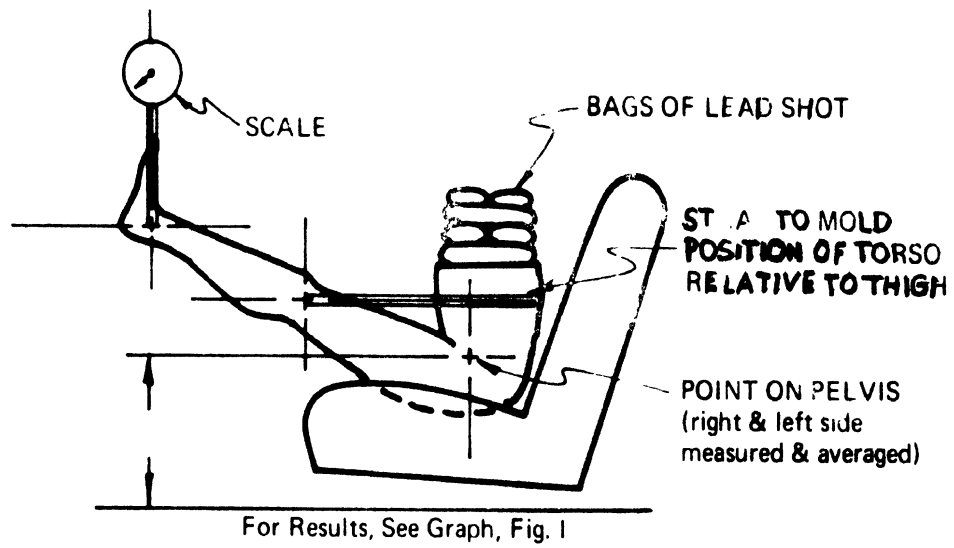
The center of gravity of the various body parts was found by suspending the piece by wires and observing the location of intersecting lines of action. The eight moments of inertia of the body parts for use in the model were found by suspending each piece on a trifilar pendulum. The weights of the body parts were measured on a precision scale. This data, tabulated in Table VI and Figures 27-29, is felt to be accurate within 1% as repeated measurements were taken on the various quantities. A correction to the moments of inertia was made based on the weight and distribution of the body skin element.

Because no impact data is available in a form suitable for use in the computer program, two static tests were carried out. The test configurations are shown in Figure 30 and the results in Figures 31 and 32. In determining the curve for load-deflection under the buttocks, the deflection was measured by taking height readings "h" at points on the pelvis as shown, as weight was added. For determining the load-deflection curve at the front of the seat, the dummy was hung as shown with the legs up, knees locked, and the buttocks just touching the cushion. The hip joint was loose. The legs were lowered gradually, and load scale readings were taken at progressive points until the scale read zero. At this time the seat front is supporting the legs. Weights were then added until the seat front bottomed out of the seat frame. This test has the disadvantages of being static and only applying the load over part of the

TABLE VI. WEIGHTS AND MOMENTS OF INERTIA OF
HSRI 50th PERCENTILE SIERRA DUMMY

Body Segment	Segment Weight, lb	Segment Moment of Inertia, in. lb sec ²
Right forearm and hand	5.094	0.300
Left forearm and hand	5.187	0.309
Right upper arm	5.938	0.241
Left upper arm	5.656	0.233
Lower spine	4.531	0.078
Lower torso pelvic area	17.062	1.709
Right upper leg	20.125	1.316
Left upper leg	20.156	1.307
Right lower leg and foot	9.781	1.211
Left lower leg and foot	9.813	1.186
Upper torso (including shoulder and chest mode, plastic "sub-skin" around rib cage and two lower neck vertebrae clamped tight)	37.438	1.344
Head (including two upper neck vertebrae)	15.781	0.436

A) LOAD-DEFLECTION UNDER BUTTOCKS



B) LOAD-DEFLECTION AT FRONT OF SEAT

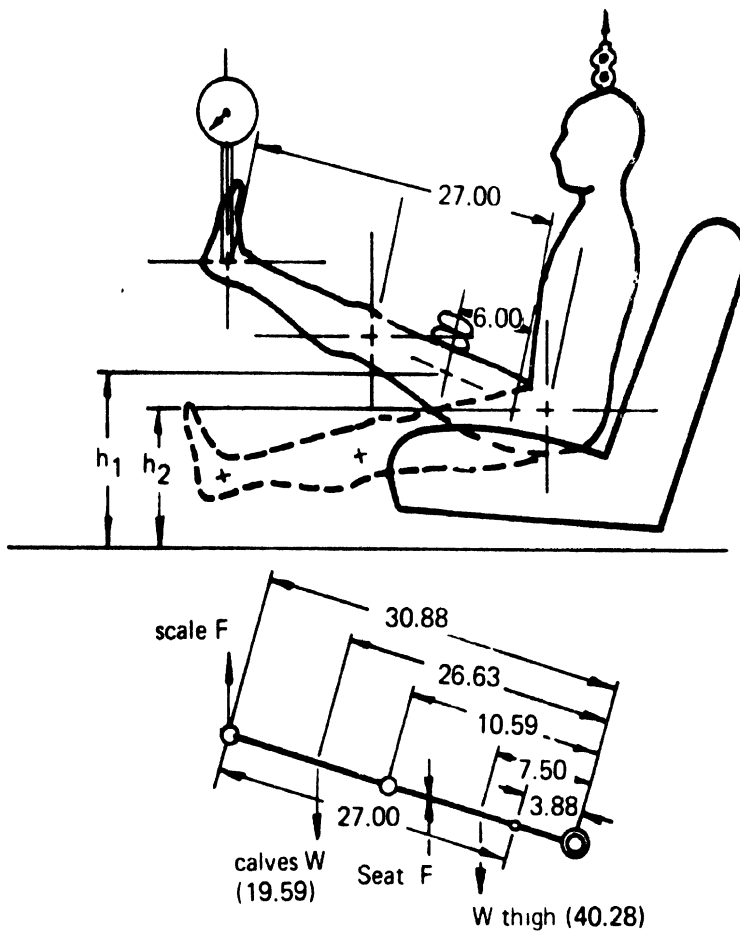


Figure 30. Test configuration for seat property tests.

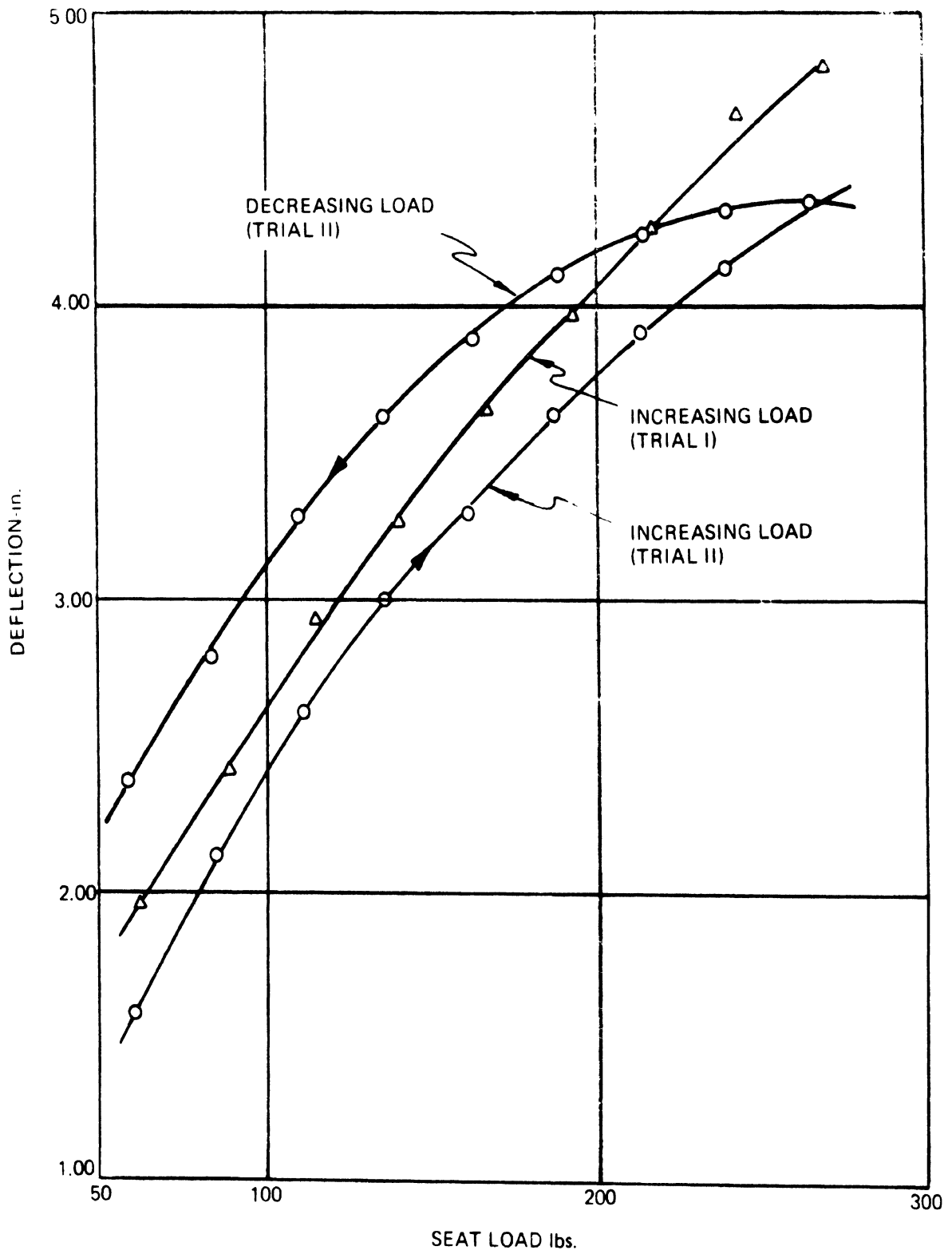


Figure 31. Seat load-deflection characteristics.

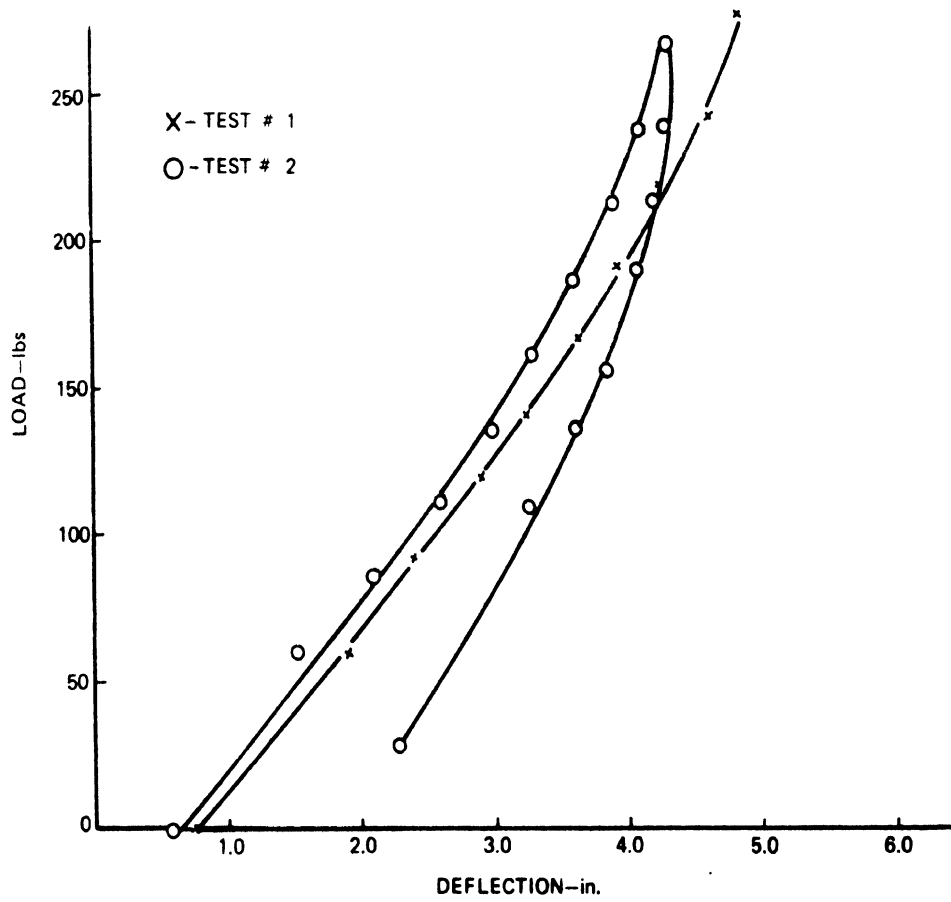


Figure 32. Seat load-deflection characteristics at seat front.

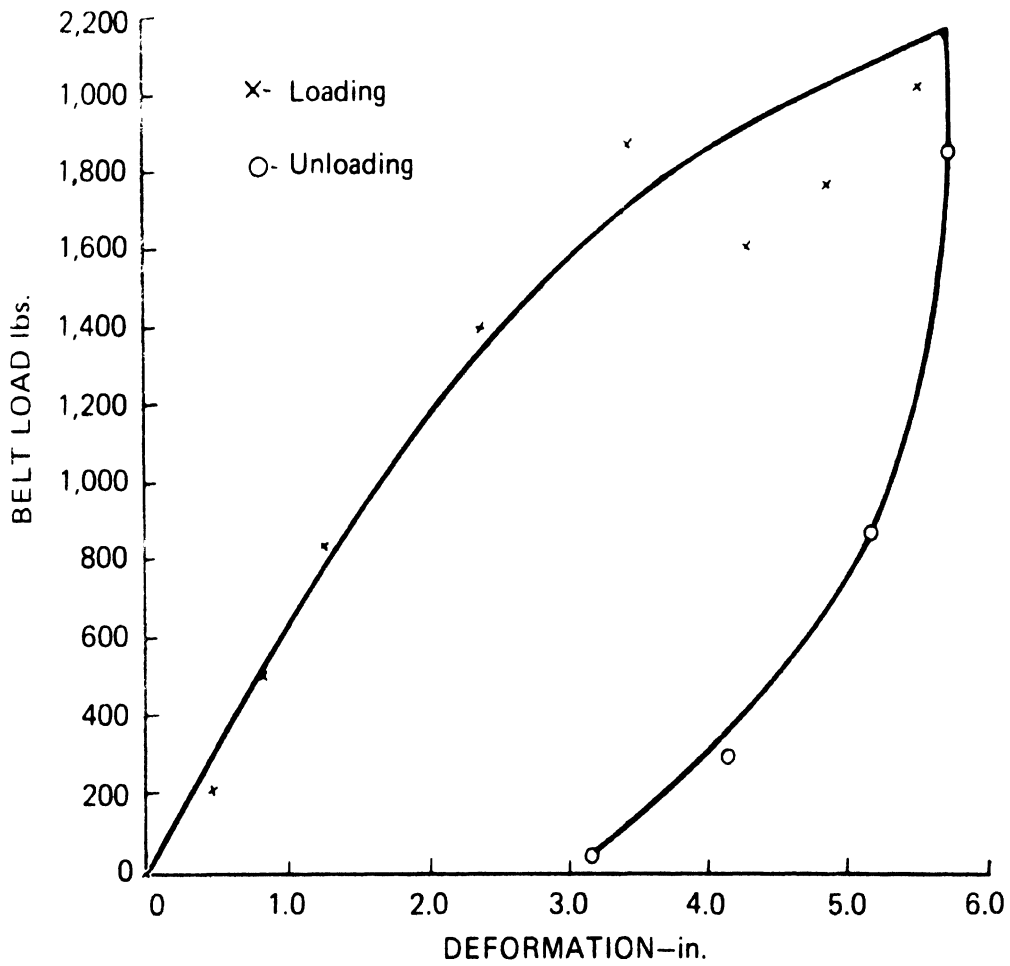


Figure 33. Load-deflection characteristics of seat belts.

seat. However, it does have the advantage of determining a curve which includes deformation properties of both the seat and dummy used in the test.

The seat belt load-deflection characteristic also led to difficulties in measurement. In this case, deformation properties of the belt, buckles, vehicle attachment points, and of the dummy itself must be reflected in the modulus which is used in the model. In addition to this, it is necessary that the deformations be a projection on the two-dimensional plane of events which actually occur in three-space.

Thus, the load-deformation characteristics of the seat belts were measured by making use of data gathered during the test itself. Force transducers were used to record the loads in the belts and high-speed movies recorded a plane view of the action of the belts. Therefore, using the known location of the H-point, the belt angle, and the location of the belt attachment point in the vehicle, it was possible to construct a table of the seat-belt length as a function of time. This, when combined with the data from the load cells, was used to construct Figure 33. Measurement of the deformation characteristics of the shoulder harness elements similarly was carried out using high-speed movies and loads from the force transducers.

D. COMPARISON OF THE SLED TEST DATA WITH THE PREDICTION OF THE MODEL

The comparison between the sled test and the mathematical model was accomplished by measuring the parameters necessary for the operation of the model and then exercising the model based on this set of input data. The only parameters which were not determined experimentally were the stiffnesses of the stops in the various joints. These were given arbitrary high values compatible with the definition of a "stop." In most computer simulations the various body segments do not even interact with the stops making precise definition unnecessary. Also, it has been found in other exercises of the model that variation of these quantities over rather wide ranges does not have a large effect on the body kinematics. Thus,

it is felt that the impact data which was measured provides a valid test case.

Two types of comparisons can be made between analysis and experiment. On one hand, the actual dummy body motions are studied; on the other, the forces and accelerations experienced by the body are examined.

The excursion of the head center of gravity and the H-point are shown in Figure 18 as a function of time. It can be noted that both the head and the hip moved down to a greater degree in the test than they did in the simulation. Also, the hip was observed to move further forward in the test. It is felt that this can be explained by an examination of the hip structure of the Sierra dummy in comparison to the model. In the dummy, the seat belt was observed in the test to ride over the pelvic structures into the abdominal area. In the model, the belt was required to stay on a radius which was a fixed distance from the H-point. Thus, in the test submarining was allowed, while in the simulation, it was impossible. The fact that submarining was observed in the test may well explain the substantial nonlinear softening-spring behavior of the seat belt load-deflection curve.

Figures 23 and 24 describe the forward motion of head and hip as a function of time. The prediction of head motion is quite good whereas the motion of the hip differs during rebound possibly as a result of submarining and the fact that the belt is buried in the dummy abdomen after the test.

The pitch angle of the head is plotted in Figure 25. Although the phase is correct, the magnitudes are not. The error in pitch magnitude is about 32%. It is felt at this time that the greater flexibility of the dummy neck (note that this would be even more exaggerated in a living subject) leads to this error. It is possible that this phenomenon can be compensated for by altering the joint stop angle from the values used in the simulation. By increasing their values, greater "flexibility" is introduced to the dummy.

Figure 26 shows the pitch angle for the upper leg. In the model this body element pitched up and down more quickly than in the test. However, the peak values are similar, possibly because the rotation of the pelvic area of the dummy down under the seat belt is in the same direction as the rotation of the upper leg. This seems likely from qualitative observations of the high-speed movies.

Figure 19 shows the resultant chest linear acceleration in G's. Agreement between these curves is remarkably good both with respect to phase and peak G-values. The test data were determined as a combination of the three readings of a triaxial accelerometer pack. The readings for the model were obviously limited to accelerations in the plane. The spike at 180 ms in the model and the rise in the test data reflect rebound into the seat back.

Similarly, in Figure 20 there is fairly good agreement between the predicted and test values of head linear acceleration. The 70 G spike predicted by the model occurred as the head pitched forward sufficiently far to encounter the "stop" briefly. Spikes of this nature are likely to occur in any segmented collection of rigid bodies in which stops are allowed to act. The peaks will be reduced only as flexibility is added to the system.

Figures 21 and 22 show the comparative seat belt and shoulder harness loads. Agreement is quite good both in phase and magnitude in the seat belt loads. The predicted harness loads appear to be low although the peak values are within 15%. The reason for this is unknown at present. It is possible that the error could be experimental in that signal clipping was observed on strain gage channels in several tests conducted near the time of this test. Other reasons could be improper selection of force-deformation curves and slack for the harness system.

The comparisons between theory and experiment which have just been presented represent the beginning of the most important phase of the model development program—the determination of the ability of the model to

describe the physical system. Agreement is good on many important quantities discussed above. The differences noted in other quantities reflect both difficulties in mathematically describing a continuous body by lumped masses and also difficulties in determining the input data with which the model can be exercised.

IV. USERS' GUIDE FOR THE TWO-DIMENSIONAL CRASH VICTIM SIMULATOR

This part of the report is intended to serve as a complete Users' Guide for exercising the HSRI Two-Dimensional Crash Victim Simulator. Sections A and B provide information for the preparation of an input data deck or file. Each card (or file line) is defined in Table VII of Section A including references to figures in this report describing the physical nature of the various input data and references to tabular data included in Section B.

Examples of complete data sets are included in Section C. These include significant exercises involving 5th percentile female, 50th and 95th percentile male occupants, and vehicle interior features such as energy-absorbing steering column, energy-absorbing lower instrument panel, belt restraint systems, windshields, etc. Techniques involved in the actual data set preparation are discussed and program printouts for the exercises are included.

The output from the computer program is discussed in Section D. This material is complete with regard to the detailed printout produced in those cases where debugging information is needed.

Section E is of particular interest to Users who wish to exercise the model as it is installed on the COMNET computer (Computer Network Corporation, 5185 MacArthur Blvd., Washington, D.C. 20016). A description of the necessary job control cards (JCL) to be included with each data deck is given. Particular reference is made to remote operation of the model from a Data 100 terminal.

Section F is a technical guide to Users interested in working from teletype terminals. Specific reference is made to the MTS (Michigan Terminal System)²⁷ and ALPHA²⁸ command languages. The RUN or EXECUTE statements for

using the two systems are described. This is followed by a description of the use of a conversational program (TALK2) which allows the user easy access to desired portions of the output generated in an exercise of the model.

A. DESCRIPTION OF INPUT DATA CARDS

All except the last several input cards have the same format, and are laid out in eight fields of ten columns each. With the exception of the first, each field contains one input datum. The first field contains one input datum in columns two through ten plus an identification letter. This letter, which appears in column one, defines the set of parameters on that card. The order of the data cards is irrelevant up to the "Z" card which precedes the SUMMARY card. If more than one of the same card is included, the last one will be given priority and its data used.

Starting with "Z" card, the following order must be preserved:

1. "Z" card.
2. SUMMARY card.
3. Relabeling cards (if any).
4. "-2" card.
5. Tolerance level reset cards (if any).
6. "-1" card (if injury potential switch is on).
7. 3 cards containing probability data (if injury potential switch and probability switch are on).
8. First field control card.
9. Second field control card.
10. Cards specifying STYX print times if required.

More than one data deck may be submitted at the same time by simply putting them one after another, each with its own full complement of

cards ("A" through "STYX"). When the program is finished with the first data deck, it will look for a second. If it finds more data, it will continue, otherwise it will sign off.

The inclusion of the SUMMARY data card at the end of a deck of input data results in the tabular output included at the end of a computer run. This output is the result of a successfully executed program and allows the user to evaluate the physics of the problem.

At present, the contact surface label is chosen according to Table XV. However, the user may alter the labels using the RELABEL card described in Table VII. This card may be inserted after the SUMMARY card in the data deck with the index of the surface to be relabeled in columns one and/or two and the eighteen BCD characters of the new label in columns eleven through twenty-eight suitably centered; e.g.:

-2-----HEAD-REST-----

A graphical output called STYX which is based on the tabular data output is in use at HSRI. The user of STYX has several options available which are fixed both in the input to the main program in the case of the contact surfaces and in the input directly to STYX. Furthermore, there is the option to use STYX or skip it altogether.

The contact surfaces which are specified in the input for a particular run are represented in the STYX output. To this end, each contact must have its reference point fixed, and its length and angle specified on its own S card in the input to the main program. In addition, the third field of the T card for each contact surface desired must contain a nonzero, floating point number. These set up the vector IGNORE (I) which controls the use of the contact surfaces in both the program and the stick figure representation.

Controlling the use of STYX is a switch, NSTICK, read by SUMMARY. In the input, this switch is on the card immediately following the Z card. There are 2 floating point fields of 10 spaces each and 4 integer fields of 5 spaces; NSTICK is the third integer field. If it is blank or zero, STYX will be executed; if nonzero, it will be skipped.

If STYX is to be used, its input follows the second SUMMARY "go" card. The first card contains seven integer fields, each five columns long. The first field holds the number of horizontal lines, NHL, with restriction: $2 \leq \text{NHL} \leq 24$. The second field is used to specify the number of spaces between horizontal lines, NSBH, which must satisfy the inequality: $(\text{NHL}-1) * \text{NSBH} + \text{NHL} \leq 48$. The third field has the number of vertical lines, NVL, with restriction: $2 \leq \text{NVL} \leq 53$. The fourth field details the number of spaces between vertical lines, NSBV, which must satisfy the inequality: $(\text{NVL}-1) * \text{NSBV} + \text{NVL} \leq 106$.

The fifth field is the switch that controls the printing of the zero lines. If this field contains a zero, the zero lines print, otherwise they are omitted. The sixth field specifies ISTEP, the number of plots to be printed, subject to the restriction $\text{ISTEP} \leq 200$. The seventh field holds METH, the switch controlling the method of generating input. If $\text{METH} \neq 0$, the time points are generated automatically; if $\text{METH} = 0$, then the time points must be specified by the user.

The next card is divided into six floating point fields, 10.4 wide. The first four of these are the minimum and maximum values of X and Y, respectively, that are to be printed. Care must be exercised so that the entire figure will be contained by these boundaries. For scaling purposes the equation:

$$(XMAX-XMIN)/\left(\frac{NSVB*(NVL-1)}{10}\right) = (YMAX-YMIN)/\left(\frac{NSBH*(NHL-1) + NHL}{6}\right)$$

must be satisfied. The next two fields are the two parameters necessary when METH \neq 0. FIRST is the first time step to be printed, and DELTA is the increment between the time points. ISTEP, specified above, is the number of time points that are generated automatically.

If METH = 0, the next ISTEP cards contain the desired time points. If METH \neq 0, these cards must not be included. Each time point must be in the first 8 columns of its own separate card, and the number of cards specifying time points must be equal to ISTEP. These time points must be at any regular or irregular intervals, but they must be in chronological order. The requested time points need not match exactly the calculated time points. The nearest available time point to the requested time point will be printed. If any requested time points are larger than the last available time point, the last available one will be printed—but only once. The time that is printed in the label is the actual calculated time, not the requested time.

The last card contains 8 integer fields, 5 wide. These are the switches controlling the printing of the contact radii. Each one prints on 0 and is omitted if the field contains anything else. These switches control respectively: the hip, nothing, the chest, nothing, the elbow, the hand, the knee, the foot.

To avoid congestion, only the man is printed out with connecting dots. All of the contact surfaces have only their end points printed out and must be connected by the user. Similarly, only the end points of the lower shoulder

TABLE VII. INPUT DATA CARDS (page 1)

Cards	Field	Table	Figure	Quantity	Units
A	1-7	VIII	10	joint friction coefficients, C_i' (If desire $C_i'=0$, insert small number=0.1)	in. lb.
B	1-8	XI	4	body segment moments of inertia, I_i	in. lb sec ²
C	1-7	VIII		joint elasticity coefficients, K_i	in. lb/rad
D	1-8	IX	4	body element lengths between joints, L_i	in.
E	1-8	IX	4	body segment masses, m_i	lb sec ² /in.
F	1		6	hip contact arc radius, r_1	in.
F	2				
F	3		6	upper torso contact arc radius, r_3	in.
F	4		6	head contact arc radius, r_4	in.
F	5		6	elbow contact arc radius, r_5	in.
F	6		6	hand contact arc radius, r_6	in.
F	7		6	knee contact arc radius, r_7	in.
F	8		6	foot contact arc radius, r_8	in.
G	1		12,34	lower joint stop coefficient, $T_1'\alpha_1$ (See card H, field 1 for α_1 . If $\alpha_1 = 0$, then T_1' should be used in place of $T_1'\alpha_1$.)	in. lb (or in. lb.rad)

TABLE VII. INPUT DATA CARDS (page 2)

Cards	Field	Table	Figure	Quantity	Units
G	2-4		11,35	joint stop coefficient, T'_i	in. lb/rad
G	5-7		12,36, 37,38	lower joint stop coefficient, $T_i^{\alpha_i}$ (See card H, fields 2-4 for α_5-7 . If $\alpha_i = 0$, then T'_i should be used in place of $T_i^{\alpha_i}$.)	in. lb (or in. lb/rad)
H	1	VIII	12,34	hip joint lower stop location, α_1	deg
H	2,3,4	VIII	12,36, 37,38	shoulder, elbow, and knee lower stop locations, $\alpha_5, \alpha_6, \alpha_7$	deg
H	5	VIII	12,34	upper hip stop coefficient, \hat{T}'_1	in. lb/rad
H	6-8	VIII	12,36, 37,38	shoulder, elbow, and knee upper stop	in. lb/rad
I	1,6-7	VIII	12,34, 37,38	upper stop locations $\Omega_1, \Omega_6, \Omega_7$	deg
I	2-5	VIII	11,35	symmetric stop locations, Ω_i	deg
J	1-7	VIII	9	joint angular velocity limits, ξ_i	deg/sec.
K	1-8	IX	10	body segment distance from previous joint to center of gravity, ρ_1	in.
L	1-8	IX	5	body initial angular position, $\theta_1(0)$	deg
N	1	IX	9	initial value of front edge seat force F'_S (FSPRMZ)	lb
N	2		14	hip seat belt contact radius, r_h	in.

TABLE VII. INPUT DATA 'ARES (page 3)

Cards	Field	Table	Figure	Quantity	Units
M	3			(blank field)	
M	4		9	initial seat force at hip, w_0	lb
M	5		6	distance to chest center of curvature, ρ_3'	in.
M	6		6	distance to head center of curvature, ρ_4'	in.
M	7		9	effective angle of seat cushion, γ_0	deg
M	8			ICONTL (Set=1.)	
N	1		9	seat linear damper coefficient, c_s	lb sec/in.
N	2		9	seat front linear spring coefficient, s	lb/in.
N	3			seat friction velocity limit, t_s	in./sec
N	4			seat friction coefficient, μ_s	
N	5-7		9	seat nonlinear spring coefficients, β_i (β_1 , lb/in.), (β_2 , lb/in. ²), (β_3 , lb/in. ³)	
N	8		9	initial distance from hip to seat front, z_0	in.
O	1		14	lap belt length from hip to attachment, l_{i_0}	in.

TABLE VII. INPUT DATA CARDS (page 4)

Card	Field	Table	Figure	Quantity	Units
1	2		13	initial length of lower shoulder restraint, l_{20}	in.
2	3		13	initial length of upper shoulder restraint, l_{30}	in.
3	4		13	distance from lower spinal joint to lower shoulder restraint, h	in.
4	5		14	angle from seat belt attachment to H-point ϕ'_{10}	deg
5	6			maximum permissible integration time step, Δt_{max} (usual value is .0005)	sec
6	7-8		9	r_z and s_z ; parameters of a linear spring at the front edge of the front seat acting forward on the lower leg. s_z is spring constant, r_z is distance from lower leg centerline to skin	in. lb/in.
7	*P,Q	1	XII	code for belt parameters on card	
8	P	2		ratio of permanent to maximum elongation, G	
9	P	3		ratio of conserved to total energy, R	
10	P	4	14,13	initial belt angle ϕ_{i0}	deg

*Cards P, Q, S, T, U, V must be used more than once in specifying several belts, tables, or contact surfaces.

TABLE VII. INPUT DATA CARDS (page 5)

Cards	Field	Table	Figure	Quantity	Units
P	5			belt slack, Δ_i	in.
P	6-8			belt load-deflection coefficients, $\sigma_1, \sigma_2, \sigma_3$	lb/(in.) ⁿ
Q	2-8			load deflection coefficients, $\sigma_i, i=4, \dots, 10$	lb/(in.) ⁿ for $n=1-5$ lb(sec/in.) ⁿ⁻⁵ for $n=6-10$
R	1	XIV		occupant position option, NPASGR	
R	2			occupant initial velocity \dot{x}_0 (XPACZ)	in./sec
R	3			vehicle initial velocity, \dot{x}_0 (XVEHZ)	in./sec
R	4			number of belt segments (NBELT = 0, 1, 2, or 3)	
R	5			minimum print-time step, Δt_p	sec
R	6			duration of simulation, t_{max}	sec
R	7			vehicle mass, M_C (not used)	lb sec ² /in.
R	8			number of Δt_p 's in one print-time interval	

S,T,U 1 XV
 Cards S, T, U specify contact parameters for the various contact surfaces. The surface index is in field 1 in each case.

TABLE VII. INPUT DATA CARDS (page 6)

Cards	Field	Table	Figure	Quantity	Unit:
S	2		7	contact surface length, D	in.
S	3			ratio of permanent to maximum deflection, G	in.
S	4			ratio of conserved to total energy, R	
S	5		7	reference coordinate, X'', of contact surface relative to initial position of H-point	in.
S	6		7	reference coordinate, Y''	in.
S			7	tangential velocity limit for friction, ξ	in./sec
S	8		7	reference angle, ψ	deg
T	2			friction coefficient, μ	
T	3-8			load deflection coefficients, σ_i , $i=1, \dots, 6$	lb/(in.) ⁿ for $n=1-5$
U	2-5			load deflection coefficients, σ_i , $i=7, \dots, 10$	lb(sec/in.) ⁿ⁻⁵ for $n=6-10$
U	6-8				

cards V constitute the input tables for vehicle deceleration or debug printout control

TABLE VII. INPUT DATA CARDS (page 1)

Card	Field	Table	Figure	Quantity	Unit
V	1	XVII		number specifying the input table	
V	2			switch indicating whether table is a constant or not (0=yes, 1=no)	
V	3			time of next break point in piecewise linear curve	sec
V	4			value at the inflection point	in./sec ²
V	5-8				
W				table element deleting mechanism (not used)	
X	1	XI		surface index	lbs
	2	XI		saturation force	
	3	XI		slope of unloading curve	lbs/in.
Y				not used	
Z	1	XVIII		debugging switch value (IBUG)	

NOTE: Several additional cards follow the Z-card when the summary table printout, the graphical plot, or the stick drawings are to be produced. These cards are exceptions to the rule governing letters in the first column.

TABLE VII. INPUT DATA CARDS (page 8)

Cards	Field	Table	Figure	Quantity	Unit
SUMMARY*	1			distance along upper spine element centerline from joint specifying accelerometer location (Columns 1-10)	in.
	2			distance along head element centerline from neck joint specifying head accelerometer location (Columns 11-20)	in.
	3	XIV		occupant position option, NPSGR (Columns 21-25 form an integer field)	
	4			control for graphical data printout (blank or zero insure execution) (Columns 26-30 form an integer field)	
	5			control for stick figures (Columns 31-35) (integer) (blank or zero execute)	
	6			control for injury potential predictor printout (Columns 36-40) (integer) (blank or zero execute)	
	7			control for injury potential predictor probability page (Columns 41-45) (integer) (blank or zero execute) (See Table XX and reference 28)	

- *NOTE:
- Fields not all 10 columns in length.
 - Integer field contents must be indexed to right side of field.
 - See text following this table.

TABLE VII. INPUT DATA CARDS (page 9)

Cards	Column No.	Table	Figure	Quantity	Unit
RELABEL	1,2			Insert contact surface to be relabeled as an integer in Columns 1 and/or 2. (See text following this table.)	
	3-10				
	11-28			Insert eighteen BCD characters of new label suitably centered.	
"GO"	1,2			Inserting -2 in the first two columns of this card indicates to the program that all input data for the production of summary tables has been read.	
INJ	1-10		XIX	Index of tolerance level to be reset.(1.,2.,3.,etc.)	
	11-20		XIX	New value of tolerance level.	
"GO"	1-10			0.or -1.(This card read by injury section. Delete if injury criterion not used)	
PROBABILITY				These three cards provide input for computation of the probability that the simulated event will happen based on type of collision, position of occupant, and chance of restraint system use. If no cards are entered here, probability will not be computed if the probability switch is off.	

TABLE VII. INPUT DATA CARDS (page 10)

Cards	Column No. Table	Figure	Quantity	Unit
(card 1)	1-10	XX	Probability of particular collision type.	
	11-20	XX	Index defining collision type (0.,1.,2.).	
	21-44	XX	New label describing collision type if index is zero.	
(card 2)	1-10	XX	Probability of the chosen occupant position being used.	
	11-20	XX	Index defining position type (0.,1.,2.,3.,4.)	
	21-44	XX	New label describing occupant position if index is zero.	
(card 3)	1-10	XX	Probability of restraint system use.	
	11-20	XX	Index defining type of restraint if any (0.,1.,2.,3.,4.,5.,6.).	
	21-44	XX	New label describing restraint type if index is zero.	
STYX-1*	1-5		NHL-integer field defining number of horizontal lines.	

*NOTE: A discussion of the application and use of STYX follows this table.

TABLE VII. INPUT DATA CARDS (page 11)

Cards	Column No.	Table	Figure	Quantity	Unit
	6-10			NSBH-integer field defining number of spaces between horizontal lines.*	
	11-15			NVL-integer field defining number of vertical lines.	
	16-20			NSVB-integer field defining number of spaces between vertical lines.	
	21-25			Switch control for zero coordinate lines (0 specified print).	
	26-30			ISTEP-number of plots to be printed.	
	31-35			METH-If METH=0, the time points for producing plots must be specified by the user, otherwise they are generated automatically.	
STYX-2	1-10			XMIN-maximum value for x on plots.	in.
	11-20			XMAX-maximum value for x on plots.	in.
	21-30			YMIN-minimum value for y on plots.	in.
	31-40			YMAX-maximum value for y on plots.	in.
	41-50			FIRST-first time point for production of drawing.	sec

*Note: Index integer quantities to right end of field.

TABLE VII. INPUT DATA CARDS (page 12)

Cards	Column No.	Table	Figure	Quantity	Units
	51-60			DELTA-Time increment between drawings.	sec
METH=0	1-8			If METH=0, a series of cards is entered here. Each one contains a point in time at which a plot is desired. Each time point must be in the first eight columns of its own separate card. ISTEP=the number of cards included if METH=0. If METH≠0, the cards <u>must not</u> be included.	
100 CONTACT PRINTS	1-5	X	6	NCNTCT (1)*	
	6-10			NCNTCT (2)	
	11-15			.	A switch in each of these eight integer fields control the printing of contact radii. Printing occurs if zero is entered in the field and is omitted if the field contains anything else.
	16-20			.	
	21-25			.	
	26-30			.	
	31-35			.	
	36-40				NCNTCT (8)

*Note: Inde integer quantities to right end of field'

and seat belts are printed, and the upper shoulder belt should be connected to the fifth joint. The contact radii are indicated as unobtrusively as possible.

B. INFORMATION TABLES

The following tables describe the subscripting used in the program. In addition, certain print and tabular indices are given as well as quantities used in the injury criteria model. Certain tables listed earlier in the text are repeated in this section for ease and assessability to the user.

TABLE VIII. SUBSCRIPTS OF BODY JOINTS

Subscript	1	2	3	4	5	6	7
Joint	Hip	Lower Spine	Upper Spine	Neck	Shoulder	Elbow	Knee

TABLE IX. SUBSCRIPTS OF BODY SEGMENTS

Subscript	1	2	3	4	5	6	7	8
Body Segment	Lower Torso	Middle Torso	Upper Torso	Head	Upper Arm	Lower Arm	Upper Leg	Lower Leg

TABLE X. SUBSCRIPTS OF CONTACT ARCS

Subscript	1	2	3	4	5	6	7	8
Contact Arc	Hip	-	Upper Torso	Head	Elbow	Hand	Knee	Foot

TABLE XI. Saturation Indices

<u>Subscript</u>	<u>Surface or Belt</u>
0.	floor
1.	seat back
2.	roof or head rest
3.	upper steering wheel; upper dash, or back of front seat
4.	windshield
5.	lower steering wheel
6.	lower panel
7.	steering column
8.	toeboard
9.	steering wheel
11.	lap belt
12.	lower shoulder belt
13.	upper shoulder belt

TABLE VII. BELT PARAMETER INDEX

$$\text{Belt parameter index} = \begin{cases} 1, \text{ lap belt} \\ 2, \text{ lower shoulder belt} \\ 3, \text{ upper shoulder belt} \end{cases}$$

TABLE VIII. NBELT VALUES

$$\text{NBELT} = \begin{cases} 0 \text{ no belts} \\ 1 \text{ lap belt} \\ 2 \text{ shoulder belts} \\ 3 \text{ lap belt and shoulder belt} \end{cases}$$

TABLE XIV. OCCUPANT POSITION OPTIONS

$$\text{Occupant position option} = \begin{cases} 1, \text{ driver} \\ 2, \text{ front passenger} \\ 3, \text{ rear passenger} \end{cases}$$

TABLE XV. NORMAL CONTACT SURFACE INDICES

Index*	Normal Contact Surface
0	floor
1	seat back
2	roof or head rest
3	upper steering wheel, upper dash, back of front seat
4	windshield
5	lower steering wheel
6	lower panel
7	steering column
8	toeboard
9	steering wheel

*It is permissible to use any index for any other contact surface as long as it is compatible with the table of possible contacts in Table XVI. For example, an air bag could be simulated by using the various segments of the steering wheel.

TABLE XVI. OCCUPANT CONTACTS VERSUS VEHICLE CONTACTS (page 1)

Contact Arc Subscript	Front		
	Driver (1) Contacts	Passenger (2) Contacts	Passenger (3) Contacts
hip (1)	seat back (1) [5]*	seat back (1) [5]	seat back (1) [5]
upper torso (3)	seat back (1) [6]	seat back (1) [6]	seat back (1) [6]
	upper steering wheel (3) [7]	upper dash (3) [7]	back of front seat (3) [7]
	lower steering wheel (5) [8]		
	steering column (7) [9]		
head (4)	seat back (1) [10]	seat back (1) [8]	seat (1) [8]
	roof or head rest (2) [11]	roof or head rest (2) [9]	roof or head rest (2) [9]
	upper steering wheel (3) [12]	upper dash (3) [10]	back of front seat (3) [10]
	windshield (4) [13]	windshield (4) [11]	
	lower steering wheel (5) [14]		

*Numbers in brackets refer to indices 5-18 used in LODFEC and CONTACT printouts. (See flow diagrams and Table XX.)

TABLE XVI. OCCUPANT CONTACTS VERSUS VEHICLE CONTACTS (page 2)

Contact Arc Subscript	Front		Front	
	Driver (1) Contacts	Passenger (2) Contacts	Passenger (3) Contacts	Passenger (3) Contacts
elbow (5)	seat back (1) [15]	seat back (1) [12]	seat back (1) [11]	
knee (")	lower panel (6) [16]	lower panel (6) [13]	back of front seat (3) [12]	
foot (3)	floorboard (0) [17]	floorboard (0) [14]	floorboard (0) [13]	
	toeboard (8) [18]	toeboard (8) [18]	back of front seat (3) [14]	

TABLE XVII. INPUT TABLE SWITCHES

Input table = $\left\{ \begin{array}{l} 1 - \text{vehicle deceleration function} \\ 2 - \text{time-varying debugging switches*} \\ 3 - \text{(read but not used)} \end{array} \right.$

*Use of this switch is controlled by IBUG value in Table XVIII.

TABLE XVIII. IBUG SWITCHER

IBUG = $\left\{ \begin{array}{ll} \text{negative integer} & - \text{Input table 2 is used} \\ 0 & - \text{no debugging printout} \\ 1-3 & - \text{various levels of debugging} \\ & \text{(See Debug Section)} \end{array} \right.$

TABLE XIX. INDICES FOR THE INJURY CRITERIA QUANTITIES

Index	Quantity	Default Value
1	Severity Index	1000
2	Head Pitch Acceleration (rad/sec ²)	2000
3	Chest Load (lb)	1800
4	Shoulder Belt Load (lb)	1800
5	Pelvic Belt Load (lb)	5000
6	Knee Load (each) (lb)	1500
7	Chest A-P G-Load	45
8	Chest S-I G-Load	25
9	Hip Angle Flexion (deg)	120
10	Lower Spine Angle Flexion (deg)	20
11	Upper Spine Flexion (deg)	20
12	Neck Angle Flexion (deg)	60
13	Shoulder Angle Flexion (deg)	180
14	Elbow Angle Flexion (deg)	135
15	Knee Angle Flexion (deg)	135
16	Hip Angle Hyperextension (deg)	0
17	Lower Spine Angle Hyperextension (deg)	45
18	Upper Spine Angle Hyperextension (deg)	20
19	Neck Angle Hyperextension (deg)	60
20	Shoulder Angle Hyperextension (deg)	60
21	Elbow Angle Hyperextension (deg)	0
22	Knee Angle Hyperextension (deg)	0

Note: See Reference 29 for a discussion of the injury criteria model. The default values are automatically used if no changes are entered in the data set.

TABLE XX. PROBABILITY LABELS

Index	Card 1	Card 2	Card 3
0	(User option)	(User option)	(User option)
1	Front collision	Driver	No restraint
2	Rear collision	Right front passenger	Lap belt only
3	--	Right rear passenger	Shoulder harness only
4	--	Left rear passenger	Shoulder harness and lap belt
5	--	--	Airbag and lap belt use
6	--	--	Inverted y-yoke and lap belt use

C. PREPARATION OF DATA SETS AND SAMPLE MODEL EXERCISES

This section of the report describes the preparation of data sets for use with the model and includes a variety of sample computer outputs. The data cards listed in Table VII serve four basic functions: 1. description of the occupant; 2. description of vehicle geometry and occupant positioning; 3. definition of the deceleration event; and, 4. program control.

Occupant Description

Information on the A through M cards of Table VII describe the occupant. The moments of inertia (B card), body segment lengths (D card), body segment masses (E card), body contact radii (F and L cards), center of gravity locations (K card) can be estimated using standard and non-standard anthropometric data in the case of human subjects. More accurate data can be obtained for dummies as they can be disassembled and subjected to laboratory measurement.

Formulas for estimating these quantities have been developed by Robbins³⁰, Patten²⁶, and Hanavan²⁵ independently. The work of Robbins is specifically applicable to use with the model described in this report while the work of Patten was developed in conjunction with modeling efforts at Cornell Aeronautical Laboratories.

In each case anthropometric data are needed to describe the exterior shape of the subject, his stature, and his weight. Using body weight, the formulas of Barter³¹ can be used to estimate the weight of the various body segments. The body segments are then assumed to be simple geometric shapes such as cylinders for the arms, elliptical cylinders for torso elements, ellipsoid for the head, truncated conical sections for the upper legs, etc. The anthropometric and weight data then are combined to locate centers of gravity and compute moments of inertia. Additional research is necessary to validate the accuracy of these procedures.

In the case of a dummy it is possible to measure these quantities more directly. The techniques for doing this are described in Section III C of this report for a Sierra 850 dummy.

Description of Joints

Description of the joints (A,C,G,H,I,J cards) is more difficult because of a lack of experimental data. Both range of motion and stiffness properties are needed.

Angular range of motion is fairly easy to determine for both humans and dummies. The most accurate technique is to target adjacent body segments and take photographs while the subject is extended to the limits of voluntary motion. The precise location of joints such as the neck, shoulder, spine, hip, knee and elbow is still a matter of conjecture however the development of anthropometric techniques for relating body surface landmarks to interior centers of rotation is still relatively incomplete.

Figures 34, 35, 36, 37, and 38 describe the preparation of a specific set of input quantities for use with the model. Consider first the hip joint as shown in Figure 34. If the upper torso is vertical, $\Theta_1 = 90.0^\circ$. The α_1 stop is applied when $\Theta_1 - \Theta_7 < \alpha_1$. (It will be necessary to refer to Figures 5, 10, 11, and 12 in interpreting this discussion.) When Θ_7 swings up toward the torso, the stop is applied when $\Theta_1 - \Theta_7 < \alpha_1$ or in Figure 34 when $\Theta_1 - \Theta_7 < 60.0^\circ$. On the other hand, when $\dot{\Theta}_7$ becomes negative, i.e., when it rotates down from the neutral horizontal position, the α_2 stop is applied when $\Theta_1 - \Theta_7 > 150.0^\circ$. Because $\dot{\Theta}_7$ is negative, the quantity $\Theta_1 - \Theta_7$ becomes larger when Θ_7 swings down and Θ_1 is held constant.

The joint must now be supplied with strength properties. The A card includes frictional forces at the joints resisting relative motions between adjacent body segments. This quantity is most descriptive of dummy joints.

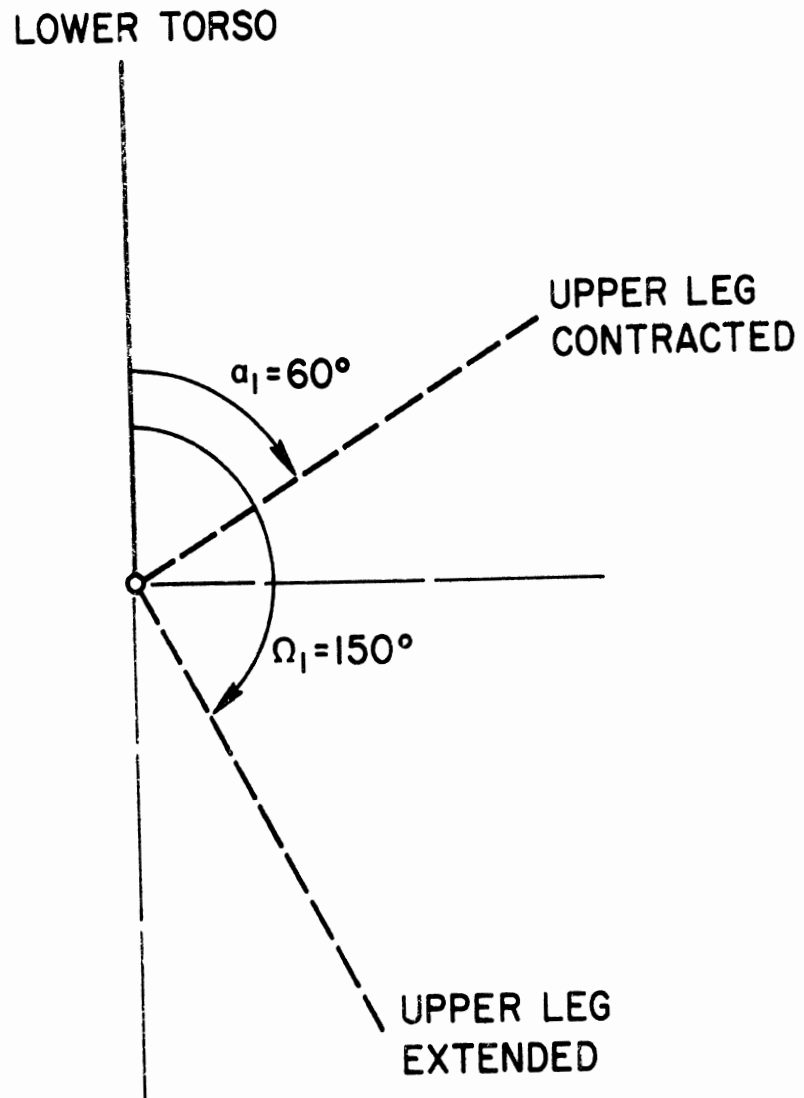


Figure 34. Hip joint structure

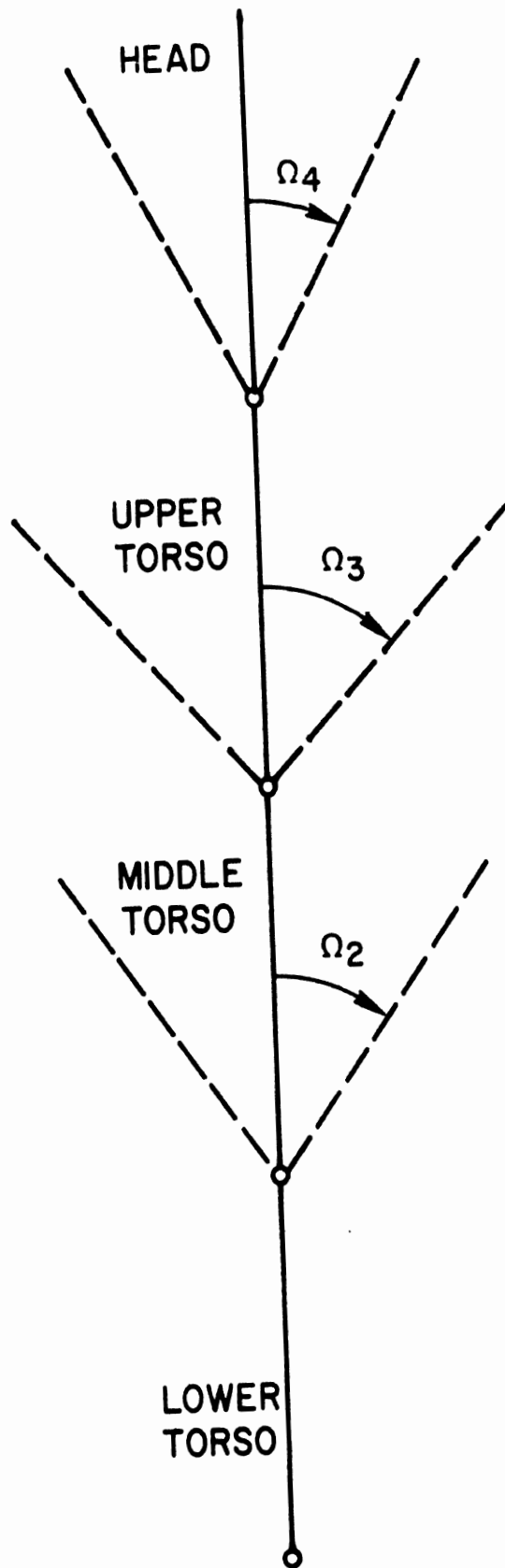


Figure 35. Back joint structures

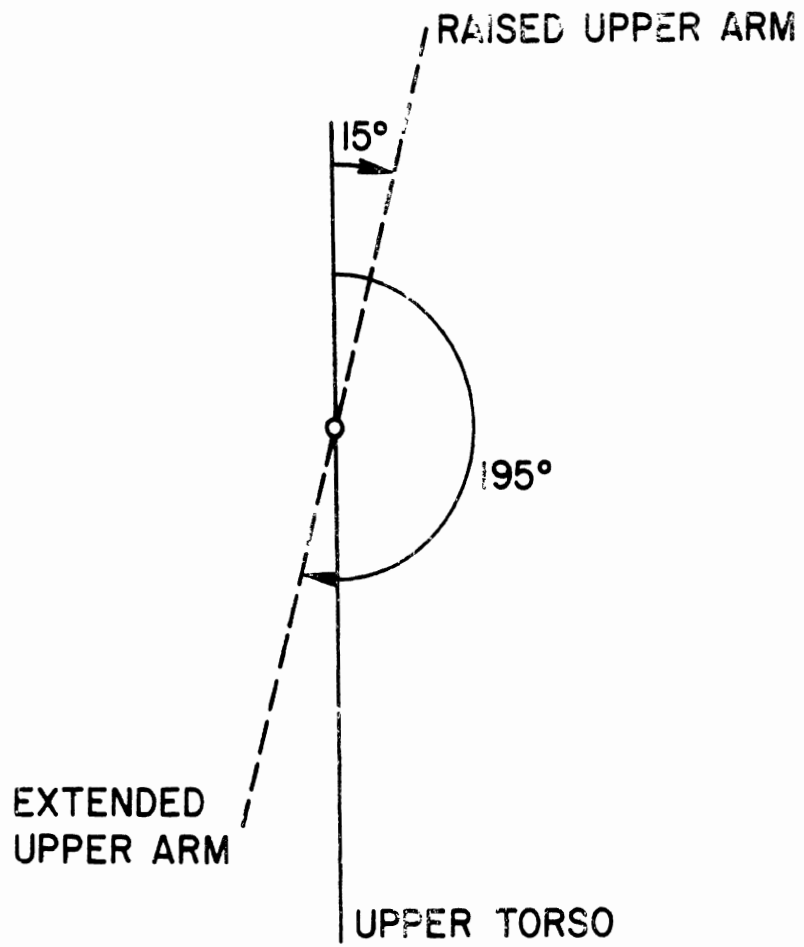


Figure 36. Shoulder joint structure

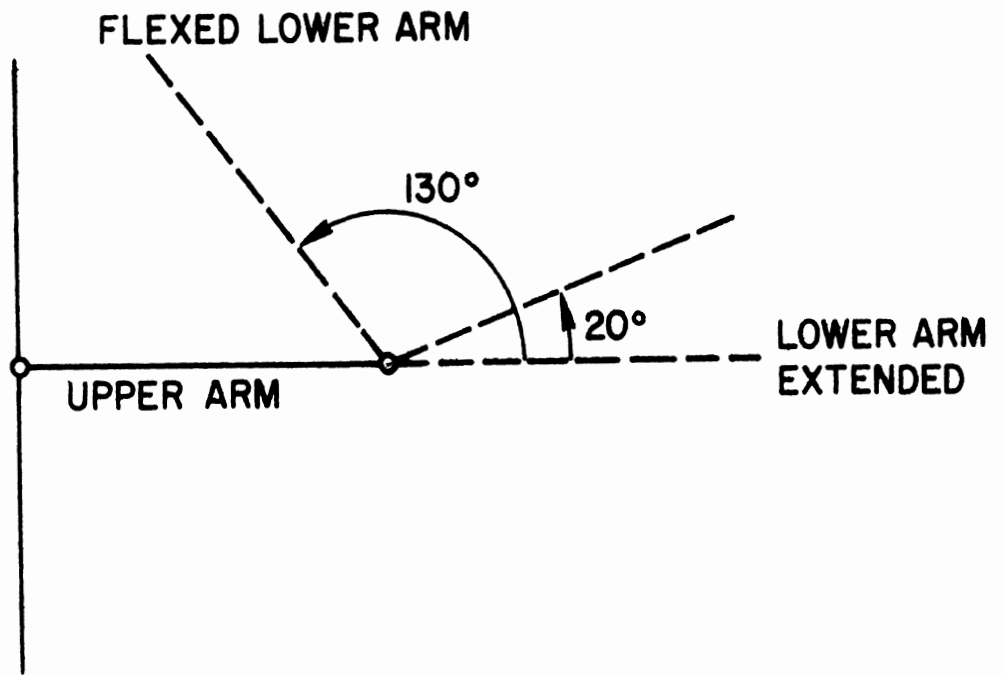


Figure 37. Elbow joint structure

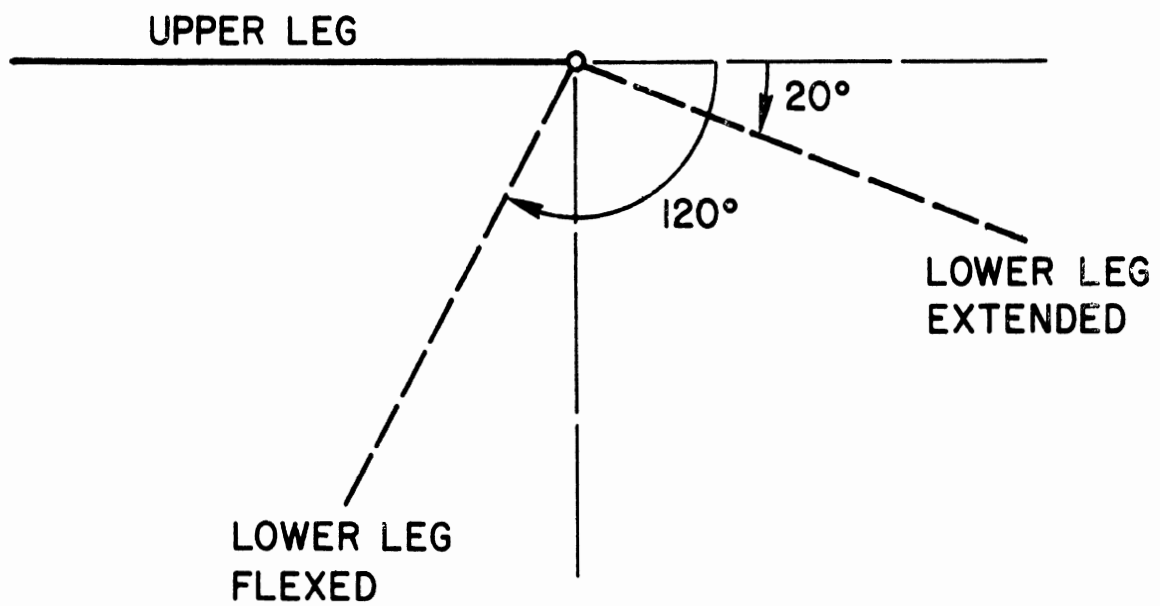


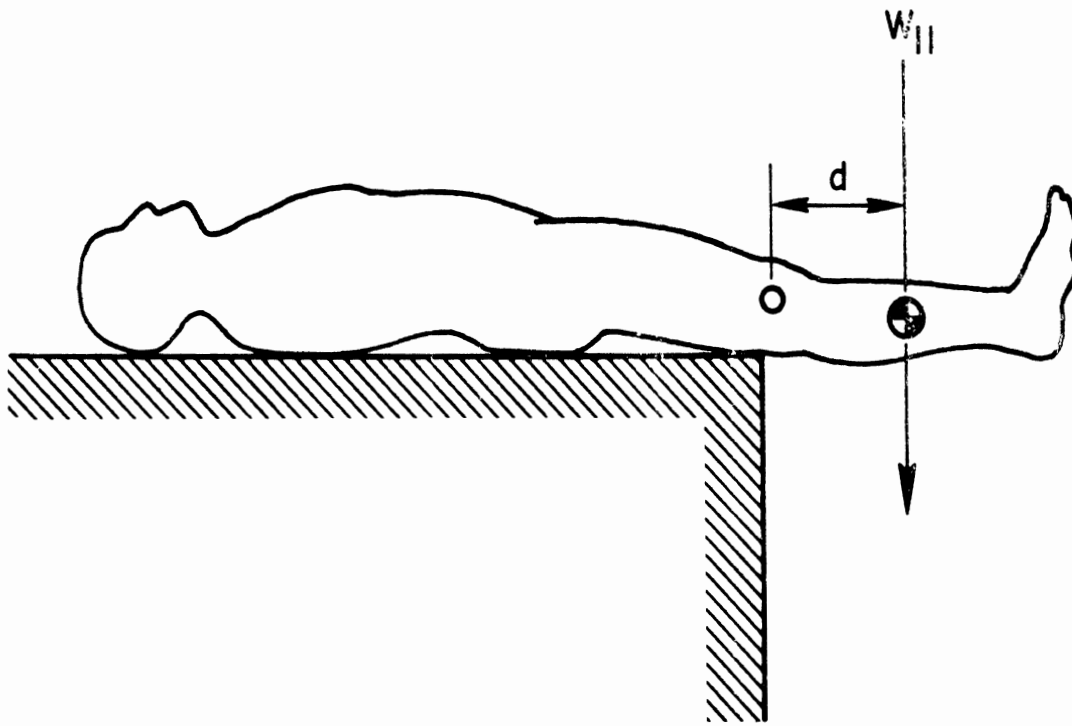
Figure 38. Knee joint structure

If dummy joints are set, for example, at 1-G, the weight of the dummy body segments and the locations of the centers of gravity may be used to estimate this quantity accurately (See Figure 39). For human-like joints or dummy rubber neck structures this quantity should be a small non-zero value such as 0.1 in. lb. (A zero value may cause program malfunction).

It is more difficult to determine the elastic coefficient resisting joint relative motion (C card). For dummies these quantities are near zero. For human-like joints their value depends on the degree of tensing of the muscles. Using the work of Bowman³² a rough estimate has been made that the maximum value for neck joint stiffness for humans is approximately 1920 in. lb./rad. Insertion of this value in data sets indicates a considerable potential for the subject to influence his crash kinematics. Further research on this subject is necessary.

Because little data has been found in the available literature defining joint stop spring constants, it has been generally assumed at HSRI that the slope of the torque-relative angle curve (G and H cards) is ten times the slope of the human-like joint elastic spring curve (19200 in.lb./rad) for human simulations and about 100,000 in.lb./rad for dummy joints. Recall for the hip joint that $\alpha_1 = 60^\circ$ and $\Omega_1 = 150^\circ$. The slope T' refers to the stop which is entered on the G card in the first field. The definition entered on the card is T' α_1 (in.lb.) or T' if $\alpha_1 = 0$ with the units of T' being in.lb./rad. Therefore the quantity entered in G1 would be 20100 in.lb. reflecting the multiplication by α_1 in radians (60/57.3). The quantity \hat{T}' which is the slope of the Ω_{stop} is entered directly in the normal units of in.lb./rad.

The lower spine, upper spine, and neck joints are shown in Figure 35. These three joints are symmetric and are defined by a single Ω and the



W_{11} = WEIGHT OF LOWER LEGS.

d = DISTANCE FROM C.G. OF LOWER LEGS TO KNEE.

C = FRICTION MOMENT = $W_{11} \times d$ (in.lb.).

Figure 39. Computation of Joint Friction Input Data

associated T' . The following values are typical values which may be used as input data: $\Omega_2 = 70^\circ$, $\Omega_3 = \Omega_4 = 22.5^\circ$, $T'_2 = T'_3 = T'_4 = 20,000$ in.lb/rad.

An example of an unsymmetric shoulder joint is shown in Figure 36. The upper torso angle is given by θ_3 and the upper arm angle by θ_5 . Similar to the case of the hip, stop locations are defined by $\theta_3 - \theta_5 < \alpha_5$ or $\theta_3 - \theta_5 > \Omega_5$. For example, the stops may be chosen $\alpha_5 = 15^\circ$ and $\Omega_5 = 195^\circ$. The α_5 stop coefficient, T'_5 is again entered into the data set multiplied by a factor while the Ω_5 stop is entered directly.

The elbow joint shown in Figure 37 is also unsymmetric. The upper arm angle is θ_5 with the lower arm given by θ_6 . The stop locations are $\theta_6 - \theta_5 < \alpha_6$ and $\theta_6 - \theta_5 > \Omega_6$ with sample values $\alpha_6 = 20^\circ$ and $\Omega_6 = 130^\circ$. The α_6 stop is entered into the data set multiplied by a constant.

The knee joint shown in Figure 38 is unsymmetric. The upper leg angle is θ_7 and the lower leg angle is θ_8 . The stops are defined $\theta_7 - \theta_8 < \alpha_7$ and $\theta_7 - \theta_8 > \Omega_7$ with sample values being $\alpha_7 = 20^\circ$ and $\Omega_7 = 120^\circ$. The α_7 stop is entered into the data set multiplied by a constant.

The contents of the J-card defines joint angular velocity limits. This small quantity, usually chosen to be 1.0 deg/sec., is used to turn on the joint frictional forces. When relative velocity between two adjacent body elements is less than this quantity, the friction force is not applied. In other words, the friction force resisting motion is only applied when the actual motion is considered to be significant.

Vehicle and Restraint System Geometry

The position of the occupant within the vehicle (or pedestrian outside the vehicle) and geometric relationships between the vehicle interior components must now be specified. In addition, it is necessary to provide force-deformation data for all potential contacts.

The first step in the development of vehicle-occupant geometric input data is preparation of a scale drawing. As geometry is specified relative to the H-point of the occupant, this point is laid out first on the sketch. As seat back angle is specified on vehicle drawings, the angle of the lower-, middle-, and upper-torso as well as the head elements are usually laid out next.

The location of contact surfaces on the drawing is usually the next step. This is based on an estimate of the number of surfaces which the occupant will contact during the collision event. For a front collision involving a fully belted occupant, these are usually limited to seat back, seat cushion, floor, and toeboard. For a rear-end collision, a head rest, roof, and top of the seat back may be required. For an unrestrained occupant in a frontal collision, the seat, floor, toeboard, windshield, various instrument panel components, etc. may be required. Selection of the appropriate number of surfaces is based on an estimate of the crash event and careful study of Table XVI which is a list of occupant contact-sensing circles versus the allowed vehicle component contacts. Examples for several standard crash events are included in the text and figures which follow.

With the vehicle surface entered it is now possible to specify the location of the lower and upper legs. A circle is usually drawn tangent to the toeboard and floorboard representing foot contact. Given the lengths of upper and lower legs, the angles of these two body elements are then uniquely determined by trigonometry. The arm elements and all other body contact circles are now drawn in.

Given the belt anchor points on a vehicle drawing and the points of tangency where they intersect the body, it is now possible to finish the geometric drawing relating all vehicle and occupant quantities. This final part of the sketch includes belt length and angle which must be specified as input data.

No mention has yet been made of initial equilibrium of the body. The initial seat force at the hip (entered as input data in the fourth field of the M-card) is usually chosen to be the weight of the torso plus the weight of the upper legs. The initial value of the force applied at the front edge of the seat to the upper legs is chosen zero when the angle of the seat cushion is smaller than the initial upper leg angle. In other cases (usually of a child occupant) much of the weight of the legs must be supported at that point. The weight of the lower legs is usually resisted by a force acting at the foot contact circle. This circle is allowed to penetrate the floor-board sufficiently to generate the required force. In rear-end collisions the initial force on the seat back is also chosen to be non-zero. A general rule of thumb is to distribute 20% of torso weight between the hip and upper torso contact circles. This is accomplished by allowing these circles to penetrate the seat back contact surfaces sufficiently to generate the required forces.

It has been found in HSRI experience that setting the hip force equal to torso weight leads to errors of less than 1/2 G in initial body loadings if all other initially applied forces are zero. This simple approximation of equilibrium is felt to be sufficient for most purposes. The additional refinements suggested in the previous paragraph can also be carried out rather easily. Complete equilibrium forces are more difficult to compute.

Vehicle-Occupant Force-Deformation Properties

Specification of the force-deformation properties of the seat cushion, the contact surfaces, and belts must be based on experimental data if it is available. The experimental data can then be simulated by a fifth order polynomial in both deflection and deflection rate possibly supplemented by a perfectly plastic energy absorber. It should be remembered in obtaining

or adapting experimental data for this purpose that deflections of the contact surface and the body element are both lumped together. In the case of belts, anchor point deformation, belt stretch, and body compliance are all lumped into the properties chosen for the model exercise. Examples of the determination of contact surfaces and belt strength properties are contained in Section III.C of this report.

Data Cards L Through Q, S Through U, and X

Based on the drawing describing vehicle, occupant, and restraint system geometry as well as selection of force-deformation data, it is possible to prepare the L through Q and S through U cards. Direct measurements from the drawing specify occupant position on the L card, seat length, and seat angle on the M card; initial distance from hip to seat front on the N card, the first five fields relating to belt geometry on the O card, the fourth field of the P card defining initial belt angles, and fields 2, 5, 6, and 8 on the S card defining contact surface end points, length, and angle.

Fields M1 and M4 are based on the simple equilibrium considerations discussed previously completing that card. The first seven fields of the N card define seat cushion force-deformation properties. The third field contains the seat friction velocity limit. This is a control parameter which senses velocity before applying the friction force in the appropriate direction. An appropriate value is 0.1 in/sec. No friction force is applied when the buttocks are sliding along the seat at a lesser velocity.

The seventh and eighth fields of the O-card define a thickness of the lower leg and the forward acting force properties of the front edge of the seat. These properties are particularly important in rear-end collisions where the lower leg may swing back toward the seat.

The remaining columns of the P, Q, S, T, U and X cards define belt and contact surface force-deformation properties. For contact surfaces with friction, a lower velocity limit must be provided as a control parameter. It should be remarked that the generation of more than one friction force at the same time can lead to an unstable integration procedure under certain conditions. The program is automatically stopped if this occurs and an appropriate comment printed. The customary procedure at HSRI is to use only one non-zero friction coefficient for a particular simulation until the input data set is thoroughly debugged. If more frictions are desired, they are then added one by one.

Vehicle Deceleration Profile (V Cards)

This is one of the simpler parts of data preparation. Given experimental data, it must be digitized. The acceleration curve is broken up into connected straight line segments. The end points of the straight lines are then entered onto the V cards. It should be remembered that the deceleration should be specified for the total real-time duration of the simulation even though it has dropped to zero.

Control Cards

The first control quantity is entered in the sixth field of the O card, the maximum permissible integration time step. This puts a boundary on the fineness of the integration scheme. A usual value is .0005 sec. This is the largest time interval which can be employed to model an event with a 500 cps content (four points per cycle). When required by the dynamics of the situation, this time step is automatically reduced. The minimum possible reduction is to 1μ sec.

The R card contains several parameters such as occupant position, initial vehicle and occupant velocity, number of belts, print times, and

real time duration of the simulation. The quantity NPASGR is usually selected as 1, because the largest number of potential vehicle-occupant contacts is available for that option. The print time step controls storage of important output variables and will be the time step in tabular output. The most convenient table size occurs for a value of .005 sec. although additional detail is often required.

When the program senses the Z card, execution of the model occurs. The results are then stored for use by the output subroutines controlled by the cards following the Z card.

The SUMMARY card selects the output options desired specifies accelerometer location for computation of head and chest resultant G levels. The fourth through seventh field contain integers for executing output options such as graphical output, stick drawings of occupant motions, an injury potential monitor, and an event probability predictor. These options will execute if a 1 is entered in the field.

RELABEL cards may be entered to change the names of contact surfaces in the tabular printout of data. For instance, the "steering column" contact surface may be used to represent an airbag. Relabeling of this surface should be carried out.

Following RELABEL cards a -2 card is entered which causes tabular printout to occur. Injury criterion and probability control cards follow if these options have been selected.

The final three cards are used by the stick figure printer plot subroutine, STYX. Basically these set up a series of printer plot drawings of the occupant and vehicle position as a function of time. Sample inputs and outputs are included in the text which follows.

Example No. 1. 30 mph Front Collision. Belts. 50th Percentile Male

A 50th percentile male wearing a lap belt and shoulder harness in a 30 mph front collision is simulated using the data set in Table XXI. The data describing the occupant, the vehicle interior and belts are derived from information included in Part III of this report. Human joint properties have been chosen. A "half-tensed" state has been chosen for the musculature of the neck. Other joint structures are given the same value because of a lack of other experimental data. Only three contact surfaces are included with friction only in the seat cushion. The deceleration is a 25 G trapezoid.

The cards after the Z card include execution of all options. All tolerance indicators are reset for the example. The complete printout from this run is included in Table XXII.

The occupant is observed to move forward into the belts and then to rebound. The chest and head G-loadings are probably acceptable except for rebound.

The injury criteria printout indicates potential problems due to head-neck flexion (the tolerance value used was derived for the case of whiplash and thus may not be accurate), shoulder belt loads, vertical spinal loadings, and excessive relative motions between adjacent body segments.

The plots of output variables and the stick drawings of the occupant can be used to study the event further. The stick drawings are particularly useful in ascertaining the accuracy of the input geometric data and whether sufficient contact surfaces have been included.

57	11.	45.
58	12.	70.
59	13.	55.
60	14.	5.
61	15.	5.
62	17.	130.
63	17.	22.5
64	18.	22.5
65	19.	75.
66	20.	190.
67	21.	140.
68	22.	140.
69	-1.	
70	.443	1.
71	1.	1.
72	.046	4.
73	2	4+ 2 100 0 11 1
74	-3).	0 42.3 0 -13. 0 41.1
75	0	0 0 0 0 0 0
		.22

END OF FILE

TIME (SEC.)	TWC DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA						SFP		1. 1972		PAGE 1
	BELT FORCES (POUNDS)			BELT ANGLES (DEGREES)			RELATIVE HIP POSITION (INCHES)		RELATIVE HEAD POSITION (INCHES)		
	LAP BELT	SHOULDER	RESTRAINT	LAP BELT	SHOULDER	RESTRAINT	HORIZONTAL	VERTICAL	HORIZONTAL	VERTICAL	
C.0	C.	J.	0.	59.5	77.0	-39.0	0.0	0.0	-3.88	26.93	
C.005	3.	0.	0.	59.5	77.0	-39.0	0.01	0.00	-3.87	26.93	
C.010	25.	0.	0.	59.2	76.7	-38.8	0.07	0.00	-3.79	26.93	
C.015	84.	0.	C.	58.5	76.0	-38.4	0.25	0.01	-3.60	26.93	
C.020	157.	0.	0.	57.1	74.5	-37.7	0.59	0.01	-3.23	26.93	
C.025	377.	0.	156.	55.0	72.3	-36.5	1.15	-0.00	-2.63	26.92	
C.030	618.	12.	390.	52.7	69.2	-35.1	1.91	-0.03	-1.79	26.89	
C.035	902.	121.	688.	49.1	65.7	-33.5	2.84	-0.09	-0.74	26.84	
C.040	1194.	258.	1042.	45.7	61.8	-31.8	3.89	-0.17	0.52	26.73	
C.045	1454.	417.	1439.	42.5	57.8	-30.3	5.01	-0.28	1.95	26.56	
C.050	1656.	587.	1863.	39.4	54.0	-29.0	6.16	-0.42	3.53	26.29	
C.055	1754.	756.	2292.	36.5	50.4	-28.0	7.32	-0.59	5.22	25.90	
C.060	1880.	909.	2701.	33.9	47.2	-27.2	8.45	-0.76	6.56	25.37	
C.065	1943.	1025.	3054.	31.7	44.5	-26.7	9.50	-0.96	8.65	24.67	
C.070	2007.	1081.	3326.	29.8	42.4	-26.6	10.40	-1.17	10.15	23.81	
C.075	2066.	1038.	3519.	28.5	41.1	-26.7	11.04	-1.33	11.37	22.79	
C.080	2080.	876.	3627.	28.0	40.8	-27.1	11.32	-1.38	12.27	21.69	
C.085	1986.	601.	3626.	28.4	41.7	-27.7	11.21	-1.27	12.75	20.63	
C.090	1772.	233.	3489.	29.7	43.7	-28.6	10.72	-1.04	12.79	19.79	
C.095	1455.	J.	3201.	31.6	46.7	-29.7	9.91	-0.75	12.38	19.20	
C.100	1047.	J.	2769.	34.0	50.6	-30.8	8.82	-0.50	11.53	18.99	
C.105	610.	J.	2193.	36.8	55.3	-32.0	7.56	-0.31	10.31	19.08	
C.110	177.	J.	1508.	40.1	60.9	-33.4	6.20	-0.11	8.82	19.38	
C.115	C.	0.	751.	44.1	67.2	-34.9	4.78	0.12	7.13	19.84	
C.120	C.	0.	C.	48.7	73.9	-36.7	3.35	0.37	5.34	20.41	
C.125	C.	0.	0.	53.8	80.5	-38.8	1.93	0.61	3.51	21.04	
C.130	C.	J.	0.	59.4	86.9	-41.3	0.53	0.83	1.65	21.74	
C.135	C.	J.	0.	65.4	92.9	-44.1	-0.86	1.05	-0.24	22.50	
C.140	C.	J.	0.	71.7	98.0	-47.1	-2.19	1.26	-2.02	23.34	
C.145	C.	J.	0.	77.6	101.7	-49.5	-3.36	1.52	-3.60	24.28	
C.150	C.	J.	0.	82.2	104.0	-50.9	-4.24	1.85	-4.87	25.36	
C.155	C.	J.	0.	85.1	104.6	-50.7	-4.78	2.79	-5.84	26.59	
C.160	C.	201.	C.	86.0	103.9	-48.5	-4.93	2.83	-6.55	27.95	
C.165	C.	309.	0.	85.0	102.0	-44.6	-4.67	3.43	-7.11	29.35	
C.170	C.	596.	0.	82.7	99.1	-38.9	-4.04	4.10	-7.58	30.61	
C.175	352.	825.	0.	79.6	95.6	-32.3	-3.15	4.84	-7.99	31.49	
C.180	912.	1084.	0.	76.3	91.7	-25.8	-2.09	5.61	-8.24	31.79	
C.185	1336.	1335.	C.	73.2	87.7	-20.7	-1.00	6.23	-8.26	31.64	
C.190	1588.	1541.	C.	70.2	83.8	-17.3	0.05	6.59	-8.07	31.23	
C.195	1714.	1678.	C.	67.4	80.0	-15.6	1.03	6.66	-7.74	30.70	
C.200	1765.	1733.	0.	64.5	76.3	-15.5	1.93	6.43	-7.30	30.11	

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Table XXII. Printout. Example No. 1 (page 1 of 27)

TIME	TWC DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA (DEGREES)										SEP 1. 1977			
	LOWER TORSO					CENTER TORSO					UPPER TORSO			
	POSITION	VELOCITY	ACCEL.	ACCEN.	TORSO	POSITION	VELOCITY	ACCEL.	ACCEN.	TORSO	POSITION	VELOCITY	ACCEL.	ACCEN.
0.0	103.00	0.0	0.0	0.0	0.0	103.00	0.0	0.0	0.0	0.0	103.00	0.0	0.0	0.0
0.050	103.00	-1.76	-0.4215E 03	-2.50	-0.7438E C3	103.00	2.21	0.3513E 03	2.21	0.3513E 03	75.30	0.5780E 03	0.0	-0.2504E 04
0.100	102.98	-3.02	-0.1205E 03	-7.63	-0.1611E C4	103.02	3.80	0.1868E 03	3.80	0.1868E 03	74.97	0.3913E 03	0.0	-0.2533E 04
0.150	102.97	0.53	0.1641E C4	-20.41	-0.4064E C4	103.04	3.76	0.3085E 03	3.76	0.3085E 03	74.72	0.3085E 03	0.0	-0.1047E 04
0.200	103.00	14.04	0.4154E C4	-50.76	-0.9104E C4	103.05	0.22	-0.1309E 04	0.22	-0.1309E 04	74.55	0.4154E C4	0.0	-0.9702E 04
0.250	103.14	42.20	0.7472E C4	-108.11	-0.1452E C5	103.04	-3.95	0.4151E C7	-3.95	0.4151E C7	74.37	0.4151E C7	0.0	-0.5081E 04
0.300	103.45	66.58	0.1771E C5	-195.32	-0.2104E C5	103.02	0.63	0.1774E C4	0.63	0.1774E C4	74.08	0.1774E C4	0.0	-0.1478E 05
0.350	104.04	150.59	0.1524E C5	-312.61	-0.2575E C5	103.05	8.56	0.1103E 04	8.56	0.1103E 04	73.42	0.1103E 04	0.0	-0.2541E 05
0.400	104.99	235.42	0.1893E C5	-441.55	-0.2426E C5	103.10	9.54	0.1271E 04	9.54	0.1271E 04	72.14	0.1271E 04	0.0	-0.3758E 05
0.450	106.42	327.20	0.2204E C5	-541.17	-0.1262E C5	103.12	-5.76	-0.5581E 04	-5.76	-0.5581E 04	69.93	0.5581E 04	0.0	-0.5026E 05
0.500	108.39	454.47	0.2526E C5	-605.16	0.8225E C4	103.00	-4.61	-0.1133E C5	-4.61	-0.1133E C5	66.49	0.8225E C4	0.0	-0.6194E 05
0.550	114.28	704.40	0.3378E C5	-840.74	0.9270E C5	102.60	-11.71	-0.1774E C5	-11.71	-0.1774E C5	61.52	0.9270E C5	0.0	-0.6961E 05
0.600	117.70	940.11	-0.2385E C5	-1111.09	0.1334E C6	101.76	-232.32	-0.3204E C5	-232.32	-0.3204E C5	54.83	0.3204E C5	0.0	-0.5365E 05
0.650	120.66	124.98	0.5859E C5	-1448.59	0.1674E C4	100.12	-435.25	-0.4819E C5	-435.25	-0.4819E C5	46.42	0.4819E C5	0.0	-0.6194E 05
0.700	129.33	172.72	0.6625E C4	-1911.79	0.1734E C6	97.42	-632.51	-0.3654E C5	-632.51	-0.3654E C5	36.70	0.3654E C5	0.0	-0.1935E 05
0.750	133.79	248.35	-0.1397E C5	-2611.09	0.3478E C5	93.78	-827.00	0.3575E C5	-827.00	0.3575E C5	26.47	0.3575E C5	0.0	0.9667E 03
0.800	138.22	327.99	-0.2682E C6	-3411.57	0.6872E C4	84.07	-1070.84	-0.1072E C5	-1070.84	-0.1072E C5	16.18	0.1072E C5	0.0	0.4946E 04
0.850	142.06	412.35	-0.4211E C5	-4421.57	0.1674E C4	74.77	-982.45	0.6354E C5	-982.45	0.6354E C5	6.95	0.6354E C5	0.0	0.6354E 05
0.900	145.22	492.36	-0.6105E C5	-5611.65	0.4340E C5	72.93	-172.42	0.4340E C5	-172.42	0.4340E C5	-5.40	0.4340E C5	0.0	0.8944E 05
0.950	146.34	565.64	-0.8616E C5	-6911.66	0.1161E C5	72.63	48.76	0.3628E C5	48.76	0.3628E C5	-4.74	0.3628E C5	0.0	0.3628E 05
1.000	146.21	624.21	-1.1933E C5	-8411.66	0.6931E C4	73.30	210.83	0.2771E C5	210.83	0.2771E C5	-4.74	0.2771E C5	0.0	0.2771E 05
1.050	145.62	674.10	-1.6533E C5	-10111.79	0.5431E C4	74.67	329.26	0.1920E C5	329.26	0.1920E C5	-3.28	0.1920E C5	0.0	0.1920E 05
1.100	144.57	724.35	-0.1397E C5	-12911.09	0.3861E C3	76.51	395.10	0.7030E C4	395.10	0.7030E C4	-1.48	0.7030E C4	0.0	0.3085E 05
1.150	143.15	774.56	-0.1407E C5	-16111.09	0.3164E C4	78.60	435.07	0.7422E C4	435.07	0.7422E C4	1.11	0.7422E C4	0.0	0.3205E 05
1.200	141.38	814.35	-0.1478E C5	-19911.77	0.2723E C4	80.87	473.17	0.7522E C4	473.17	0.7522E C4	4.50	0.7522E C4	0.0	0.3263E 05
1.250	139.23	854.35	-0.1452E C5	-24911.66	0.3331E C5	83.30	495.18	0.1642E C4	495.18	0.1642E C4	8.69	0.1642E C4	0.0	0.2795E 05
1.300	136.74	894.44	0.2728E C3	-30911.66	-0.3931E C5	85.79	497.71	-0.1198E C4	497.71	-0.1198E C4	13.59	0.1198E C4	0.0	0.3384E 05
1.350	134.23	934.44	0.1452E C5	-36911.66	-0.3947E C5	88.25	481.56	-0.6134E C4	481.56	-0.6134E C4	19.35	0.6134E C4	0.0	0.4783E 05
1.400	132.05	974.44	0.1535E C5	-42911.66	-0.2066E C5	90.55	431.74	-0.1458E C5	431.74	-0.1458E C5	26.29	0.1458E C5	0.0	0.6832E 05
1.450	130.32	1014.44	0.1671E C5	-48911.66	0.1763E C5	92.49	335.79	-0.3586E C5	335.79	-0.3586E C5	34.93	0.3586E C5	0.0	0.9325E 05
1.500	129.02	1054.44	0.5245E C4	-54911.66	0.4400E C5	93.80	175.76	-0.3586E C5	175.76	-0.3586E C5	45.89	0.3586E C5	0.0	0.1241E 06
1.550	127.96	1124.44	0.2274E C5	-60911.66	0.2274E C5	94.13	-44.36	-0.4264E C5	-44.36	-0.4264E C5	50.89	0.4264E C5	0.0	0.1428E 06
1.600	127.23	1204.44	0.4550E C4	-66911.66	0.4550E C4	93.39	-242.64	-0.2702E C5	-242.64	-0.2702E C5	57.39	0.2702E C5	0.0	0.1125E 06
1.650	126.61	1284.44	-0.1425E C5	-72911.66	-0.1425E C5	92.00	-264.70	0.2795E C5	-264.70	0.2795E C5	67.59	0.2795E C5	0.0	0.9397E 03
1.700	125.66	1364.44	-0.3262E C5	-78911.66	-0.3262E C5	91.24	-0.57	0.7600E C5	-0.57	0.7600E C5	81.90	0.7600E C5	0.0	0.1284E 06
1.750	123.94	1444.44	-0.2512E C5	-84911.66	-0.2512E C5	92.72	390.60	0.7214E C5	390.60	0.7214E C5	117.90	0.7214E C5	0.0	-0.1720E 06
1.800	121.33	1524.44	-0.6455E C4	-90911.66	-0.6455E C4	94.39	605.90	0.4581E C5	605.90	0.4581E C5	148.46	0.4581E C5	0.0	-0.1808E 06
1.850	118.09	1604.44	-0.7507E C4	-96911.66	-0.7507E C4	98.93	955.74	0.1500E C5	955.74	0.1500E C5	156.96	0.1500E C5	0.0	-0.1931E 06
1.900	114.64	1684.44	-0.8616E C5	-102911.66	-0.8616E C5	103.29	867.85	-0.1113E C5	867.85	-0.1113E C5	160.65	-0.1113E C5	0.0	-0.1821E 06

Table XXII. Printout. Example No. 1 (page 2 of 27)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA (DEGREES)

TIME	UPPER ARM		LOWER ARM		BODY SEGMENT ANGULAR ORIENTATION		CARTESIAN COORDINATES		ACCELERATION		POSITION		VELOCITY		ACCEL.	
	PC	VE	PC	VE	AC	AC	PC	VE	AC	AC	PC	VE	AC	AC		
0.0	-77.00	0.0	0.0	0.0	0.0	0.0	6.00	5.97	-0.1820E	0.0	-33.70	0.0	0.0	0.124E	04	
0.0050	-76.99	3.01	-0.03	-13.90	-0.2683E	0.4	5.97	5.97	-0.2022E	0.4	-32.97	11.44	0.2403E	04	04	
0.0100	-76.97	5.74	-0.14	-26.94	-0.2372E	0.4	5.90	5.90	-0.1784E	0.4	-32.88	23.83	0.2631E	04	04	
0.0150	-76.93	7.78	-0.30	-37.06	-0.1486E	0.4	5.64	5.64	-0.1154E	0.4	-32.73	38.31	0.3317E	04	04	
0.0200	-76.89	8.56	-0.50	-40.82	-0.3699E	0.3	5.64	5.64	-0.2825E	0.4	-32.56	9.53	0.3909E	05	05	
0.0250	-76.84	16.02	-0.70	-38.67	-0.3446E	0.3	5.56	5.56	-0.6682E	0.4	-33.98	-133.44	-0.3444E	05	05	
0.0300	-76.69	45.86	-0.89	-38.11	-0.9966E	0.2	5.64	5.64	0.1614E	0.5	-35.96	-454.07	-0.179E	05	05	
0.0350	-76.27	122.21	-1.08	-37.87	-0.7697E	0.2	6.00	6.00	0.1614E	0.5	-35.96	-454.07	-0.179E	05	05	
0.0400	-75.38	245.32	-1.27	-39.47	-0.1225E	0.4	6.75	6.75	0.2156E	0.5	-38.35	-486.15	-0.1182E	04	04	
0.0450	-73.72	428.86	-1.49	-54.40	-0.6020E	0.4	8.03	8.03	0.2529E	0.5	-40.75	-478.98	-0.2204E	04	04	
0.0500	-70.96	682.66	-1.87	-106.05	-0.1604E	0.5	9.93	9.93	0.2561E	0.5	-43.24	-530.35	-0.2169E	05	05	
0.0550	-66.78	1003.43	-2.67	-229.86	-0.3565E	0.5	12.47	12.47	0.2220E	0.5	-46.23	-683.04	-0.3900E	05	05	
0.0600	-60.83	1387.06	-4.36	-467.03	-0.6385E	0.5	15.56	15.56	0.2092E	0.5	-50.15	-883.21	-0.3561E	05	05	
0.0650	-52.80	1828.23	-7.60	-850.72	-0.8909E	0.5	19.18	19.18	0.1533E	0.5	-54.89	-976.95	-0.681E	04	04	
0.0700	-42.57	2248.25	-12.94	-1271.53	-0.6984E	0.5	23.20	23.20	-0.2711E	0.4	-59.51	-838.07	0.4751E	05	05	
0.0750	-30.78	2279.66	-19.69	-1149.17	-0.3167E	0.6	27.16	27.16	0.3355E	0.5	-63.06	-574.82	0.5205E	05	05	
0.0800	-22.94	898.45	-19.68	1084.27	0.1383E	0.6	30.30	30.30	-0.5632E	0.5	-65.33	-335.22	0.5408E	05	05	
0.0850	-19.35	540.87	-12.55	1762.22	0.1258E	0.6	32.53	32.53	-0.5632E	0.5	-65.33	-335.22	0.5408E	05	05	
0.0900	-17.43	235.17	-2.31	2290.82	0.7404E	0.5	32.53	32.53	-0.87	0.3591E	0.5	-66.29	125.66	0.4540E	05	05
0.0950	-16.86	19.63	9.82	2504.01	0.6034E	0.4	32.11	32.11	-148.84	-0.2000E	0.5	-65.07	358.34	0.4563E	05	05
0.1000	-16.97	-37.87	22.24	2424.24	-0.3557E	0.5	31.15	31.15	-224.43	-0.1131E	0.5	-62.72	569.14	0.3024E	05	05
0.1050	-17.03	14.30	33.83	2211.40	-0.3760E	0.5	29.92	29.92	-272.10	-0.2058E	0.5	-59.52	703.79	0.1973E	05	05
0.1100	-16.52	53.76	44.44	2036.78	-0.3014E	0.5	28.33	28.33	-363.22	-0.1562E	0.5	-55.78	785.30	0.1221E	05	05
0.1150	-16.08	106.07	54.25	1912.81	-0.1770E	0.5	26.33	26.33	-430.74	-0.1073E	0.5	-51.72	835.32	0.9350E	04	04
0.1200	-15.42	158.24	63.68	1857.13	-0.3826E	0.4	24.06	24.06	-471.63	-0.5269E	0.4	-47.43	881.94	0.9170E	04	04
0.1250	-14.48	219.53	72.91	1831.52	-0.6519E	0.4	21.64	21.64	-498.42	-0.5269E	0.4	-42.93	905.37	0.3467E	04	04
0.1300	-13.28	250.36	81.98	1794.10	-0.7403E	0.4	19.09	19.09	-520.18	-0.3271E	0.4	-38.50	859.96	0.1421E	05	05
0.1350	-12.01	256.39	100.35	1969.34	0.4541E	0.5	16.45	16.45	-530.45	-0.2364E	0.3	-34.38	786.43	-0.1485E	05	05
0.1400	-10.67	291.12	110.85	2251.28	0.6901E	0.5	11.23	11.23	-506.35	0.4375E	0.4	-27.36	580.86	-0.3438E	05	05
0.1450	-8.98	401.25	123.04	2633.65	0.6787E	0.5	8.75	8.75	-488.23	0.4622E	0.4	-24.93	386.25	-0.4327E	05	05
0.1500	-6.42	633.82	136.70	2738.17	-0.4339E	0.5	6.38	6.38	-460.46	0.6227E	0.4	-23.55	159.22	-0.4714E	05	05
0.1550	-2.69	840.35	149.38	2224.22	-0.1731E	0.6	4.18	4.18	-416.11	0.1194E	0.5	-23.35	-79.54	-0.4774E	05	05
0.1600	1.73	901.40	157.96	1138.59	-0.2559E	0.6	2.52	2.52	-352.92	-0.5635E	0.4	-26.35	-309.46	-0.4219E	05	05
0.1650	6.07	818.15	162.42	819.19	-0.2340E	0.5	0.52	0.52	-377.60	0.2157E	0.4	-29.10	-485.59	-0.2861E	05	05
0.1700	9.82	675.27	166.11	630.28	-0.5756E	0.5	-1.33	-1.33	-377.60	0.2157E	0.4	-29.10	-603.29	-0.9780E	04	04
0.1800	12.79	517.42	168.41	259.60	-0.5225E	0.5	-3.11	-3.11	-313.66	0.2696E	0.5	-32.31	-674.00	-0.9780E	04	04
0.1850	15.09	418.50	168.49	-233.48	-0.1002E	0.6	-4.26	-4.26	-130.87	0.4456E	0.5	-35.78	-711.53	-0.6899E	04	04
0.1900	17.18	435.49	166.08	-728.49	-0.8461E	0.5	-4.33	-4.33	105.42	0.4479E	0.5	-39.42	-740.30	-0.3420E	04	04
0.1950	19.67	572.98	161.25	-1194.64	-0.8951E	0.5	-3.20	-3.20	346.07	0.4669E	0.5	-43.14	-743.18	0.3321E	04	04
0.2000	23.06	792.30	154.20	-1617.40	-0.8037E	0.5	-0.90	-0.90	571.46	0.4366E	0.5	-46.78	-708.08	0.1171E	05	05

Table XXII. Printout. Example No. 1 (page 3 of 27)

VEHICULAR MOTION

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA

BODY MOTION AT HIP JOINT

TIME	POSITION (IN.)	VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)	RELATIVE DISPL. (IN.)	HORIZONTAL VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)	RELATIVE DISPL. (IN.)	VERTICAL VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)
0.C	0.0	528.00	G.0	0.0	528.00	0.092	0.0	0.0	0.329
0.C050	2.630	521.97	-6.244	0.008	527.05	-0.579	0.001	C.50	0.228
0.C100	5.260	503.88	-12.487	0.071	525.84	-0.714	0.005	0.82	0.050
0.C150	7.645	473.72	-18.731	0.247	524.18	-1.094	0.009	C.57	-0.414
0.C200	9.917	431.50	-24.974	0.594	521.40	-2.003	0.008	-1.02	-1.421
0.C250	11.554	383.25	-24.974	1.152	515.85	-4.172	-0.005	-4.19	-1.846
0.C300	13.745	335.00	-24.974	1.911	504.92	-7.733	-0.035	-8.05	-2.238
0.C350	15.304	286.75	-24.974	2.837	485.91	-12.589	-0.047	-13.14	-3.066
0.C400	16.617	238.50	-24.974	3.895	457.03	-17.774	-0.169	-19.46	-3.393
0.C450	17.685	190.25	-24.974	5.006	418.75	-22.032	-0.282	-25.79	-3.014
0.C500	18.515	142.00	-24.974	6.159	373.61	-24.715	-0.424	-30.89	-2.126
0.C550	19.109	93.77	-24.600	7.315	324.41	-26.243	-0.587	-34.03	-0.963
0.C600	19.465	52.28	-18.356	8.449	273.03	-26.646	-0.762	-36.05	-2.387
0.C650	19.651	22.94	-12.113	9.502	221.08	-27.570	-0.957	-42.41	-3.339
0.C700	19.717	5.47	-5.869	10.399	162.32	-32.954	-1.168	-48.56	5.418
0.C750	19.726	C.14	C.0	11.038	95.54	-37.462	-1.329	-54.39	12.029
0.C800	19.727	C.14	C.0	11.222	16.50	-42.579	-1.376	7.44	15.006
0.C850	19.728	C.14	C.0	11.209	-60.43	-38.402	-1.267	35.36	13.326
0.C900	19.728	C.14	C.0	10.725	-131.33	-34.188	-1.036	54.49	4.768
0.C950	19.729	C.14	C.0	9.910	-192.13	-28.039	-0.753	55.55	-4.089
0.1000	19.730	C.14	C.0	8.824	-238.56	-15.569	-0.502	44.41	-4.271
0.1050	19.731	C.14	C.0	7.564	-263.32	-11.844	-0.306	35.90	3.673
0.1100	19.731	C.14	C.0	6.200	-280.01	-4.920	-0.109	42.66	3.434
0.1150	19.732	C.14	C.0	4.783	-295.07	0.120	0.120	48.52	1.747
0.1200	19.733	C.14	C.0	3.355	-285.06	1.093	0.367	45.04	-1.419
0.1250	19.733	C.14	C.0	1.934	-282.63	1.482	0.605	46.50	-1.190
0.1300	19.734	C.14	C.0	0.527	-279.55	1.704	0.932	44.29	-1.121
0.1350	19.735	C.14	C.0	-0.862	-275.20	5.540	1.048	42.06	-0.256
0.1400	19.736	C.14	C.0	-2.194	-253.02	18.441	1.263	45.50	4.221
0.1450	19.736	C.14	C.0	-3.355	-207.73	29.032	1.517	57.40	8.512
0.1500	19.737	C.14	C.0	-4.243	-144.47	36.662	1.850	76.93	11.530
0.1550	19.738	C.14	C.0	-4.781	-69.09	41.225	2.291	99.97	10.747
0.1600	19.739	C.14	C.0	-4.925	12.16	42.212	2.832	115.83	6.074
0.1650	19.739	C.14	C.0	-4.665	90.73	37.545	3.434	124.56	3.984
0.1700	19.740	C.14	C.0	-4.044	154.97	28.181	4.095	141.43	9.727
0.1750	19.741	C.14	C.0	-3.149	199.83	16.456	4.844	155.69	1.536
0.1800	19.741	C.14	C.0	-2.090	219.52	2.352	5.607	143.96	-15.875
0.1850	19.742	C.14	C.0	-0.998	215.15	-4.876	6.229	100.98	-27.423
0.1900	19.743	C.14	C.0	0.049	203.54	7.140	6.595	44.04	-31.034
0.1950	19.744	C.14	C.0	1.030	188.76	-8.029	6.664	-16.62	-31.519
0.2000	19.744	C.14	C.0	1.934	173.33	-7.757	6.429	-77.30	-31.229

Table XXII. Printout. Example No. 1 (page 4 of 27)

OUTPUT DATA
BELT FORCES (LRS),

TWC DIMENSIONAL CRASH VICTIM SIMULATOR
ACCELEROMETER READINGS

TIME	HEAD		CHEST		SHOULDER RESTRAINT		AT HIP		AT FRONT EDGE	
	RESULTANT (G-UNITS)	ANGLE (DEG.)	RESULTANT (G-UNITS)	ANGLE (DEG.)	LAP	LOWER	UPPER	AT HIP	FRONT	EDGE
0.0	0.3	-8.2	0.4	138.7	0.0	0.0	0.0	145.00	0.0	0.0
0.0050	0.3	3.2	0.4	141.0	3.3	0.0	0.0	144.92	0.0	0.0
0.0100	0.3	-16.7	0.4	159.1	25.4	0.0	0.0	146.16	0.0	0.0
0.0150	0.3	-68.5	0.4	-144.9	84.4	0.0	0.0	149.33	0.0	0.0
0.0200	0.9	-97.1	1.1	-109.6	197.5	0.0	0.0	155.51	0.0	0.0
0.0250	1.9	-55.3	2.4	-143.5	377.0	0.0	155.7	164.66	0.0	0.0
0.0300	3.5	-106.3	5.0	-157.9	618.5	12.3	389.7	175.23	7.02	0.0
0.0350	6.1	-102.6	9.5	-160.7	902.3	121.1	687.7	187.51	14.43	0.0
0.0400	9.2	-105.4	15.6	-163.3	1193.6	258.2	1041.8	201.32	20.92	0.0
0.0450	13.2	-109.2	22.9	-166.1	1453.8	416.9	1439.3	215.40	26.85	0.0
0.0500	18.3	-114.2	30.8	-169.3	1656.3	586.9	1863.0	228.47	33.49	0.0
0.0550	25.0	-120.8	38.1	-172.6	1794.3	756.1	2291.8	239.78	43.07	0.0
0.0600	32.4	-129.0	47.1	-176.1	1880.5	909.2	2700.9	249.55	58.10	0.0
0.0650	40.4	-139.1	52.3	-177.9	1942.7	1025.4	3053.6	263.28	80.72	0.0
0.0700	47.3	-150.6	43.0	-176.3	2007.5	1081.4	3326.2	265.74	109.50	0.0
0.0750	40.0	-164.4	36.1	-173.5	2065.6	1037.7	3519.1	254.14	134.34	0.0
0.0800	58.7	-172.3	41.2	-170.8	2079.9	875.6	3626.8	218.11	141.04	0.0
0.0850	64.4	-142.8	35.6	-171.8	1985.8	601.1	3626.5	178.99	118.11	0.0
0.0900	55.6	-149.0	18.4	-142.4	1772.4	232.9	3488.6	143.84	66.40	0.0
0.0950	67.8	-132.3	12.5	-110.6	1454.9	0.0	3201.2	125.65	0.0	0.0
0.1000	46.6	-140.0	19.9	-151.2	1047.2	0.0	2767.8	121.75	0.0	0.0
0.1050	36.4	-136.3	13.8	-145.3	609.8	0.0	2193.5	118.50	0.0	0.0
0.1100	27.3	-134.4	9.9	-136.7	176.9	0.0	1508.3	100.25	0.0	0.0
0.1150	16.8	-131.6	5.0	-114.6	0.0	0.0	750.5	82.19	0.0	0.0
0.1200	10.8	-102.3	2.1	-16.2	0.0	0.0	0.0	68.26	0.0	0.0
0.1250	11.1	-111.6	1.9	-10.6	0.0	0.0	0.0	56.39	0.0	0.0
0.1300	11.2	-115.3	2.5	-6.7	0.0	0.0	0.0	42.94	0.0	0.0
0.1350	14.1	-52.6	16.4	-15.7	0.0	0.0	0.0	28.12	0.0	0.0
0.1400	24.6	-35.9	29.5	-13.5	0.0	0.0	0.0	7.11	0.0	0.0
0.1450	32.5	-35.3	38.8	-12.7	0.0	0.0	0.0	0.0	0.0	0.0
0.1500	33.3	-40.9	42.0	-11.9	0.0	0.0	0.0	0.0	0.0	0.0
0.1550	22.7	-54.2	37.5	-8.5	0.0	0.0	0.0	0.0	0.0	0.0
0.1600	6.5	-116.3	34.0	-2.6	0.0	200.8	0.0	0.0	0.0	0.0
0.1650	31.3	-126.5	32.7	-0.0	0.0	398.6	0.0	0.0	0.0	0.0
0.1700	68.6	-102.1	30.5	-16.9	0.0	595.7	0.0	0.0	0.0	0.0
0.1750	101.0	-78.3	19.9	-10.4	352.5	824.7	0.0	0.0	0.0	0.0
0.1800	86.8	-52.8	14.0	-53.3	511.6	1083.8	0.0	0.0	0.0	0.0
0.1850	56.3	-25.7	24.3	-81.8	1336.0	1335.3	0.0	0.0	0.0	0.0
0.1900	36.2	-7.4	31.7	-90.3	1587.8	1540.8	0.0	0.0	0.0	0.0
0.1950	26.6	-31.7	36.2	-98.0	1713.9	1678.0	0.0	0.0	0.0	0.0
0.2000	23.9	-44.1	38.1	-105.5	1764.9	1732.8	0.0	0.0	0.0	0.0

Table XXII. Printout. Example No. 1 (page 5 of 27)

TIME	FOOT			UPPER TORSC			HIP		
	ON	FN	CM	UN	UN	CM	ON	ON	CM
0.C									
C.CC5C	18.5	0.C		0.0			0.0		
0.0160	18.5	0.0		0.0			0.0		
0.C150	23.7	0.0		0.0			0.0		
0.C200	40.4	0.0		0.0			0.0		
0.C250	141.3	202.1		0.0			0.0		
C.C300	385.3	439.6		0.0			0.0		
0.C350	736.5	611.9		0.0			0.0		
C.C400	1083.3	718.1		0.0			0.0		
0.C450	1326.2	841.0		0.0			0.0		
0.C500	1447.8	1051.2		0.0			0.0		
0.C550	1501.9	1321.9		0.0			0.0		
C.C600	1541.1	1534.6		0.0			0.0		
0.C650	1524.7	1548.0		0.0			0.0		
0.L700	1210.1	1177.0		0.0			0.0		
0.C750	525.8	666.8		0.0			0.0		
C.C800	0.0	292.0		0.0			0.0		
C.C850	0.0	2.7		0.0			0.0		
0.C900	0.0	0.0		0.0			0.0		
0.C950	0.0	0.0		0.0			0.0		
0.1000	0.0	0.0		0.0			0.0		
0.1050	0.0	0.0		0.0			0.0		
0.1100	0.0	0.0		0.0			0.0		
0.1150	0.0	0.0		0.0			0.0		
0.1200	0.0	0.0		0.0			0.0		
0.1250	0.0	107.2		0.0			0.0		
0.1300	0.0	190.9		53.6			0.0		
0.1350	0.0	134.7		1243.2			252.9		
0.1400	0.0	0.0		2317.7			1252.4		
0.1450	0.0	0.0		3171.5			2112.0		
0.1500	0.0	0.0		3723.0			2743.9		
0.1550	0.0	0.0		3932.4			3084.4		
0.1600	0.0	0.0		3789.3			3094.9		
0.1650	0.0	0.0		3287.4			2747.1		
0.1700	0.0	0.0		2454.0			2095.1		
0.1750	0.0	0.0		1384.7			1241.6		
0.1800	0.0	0.0		780.0			323.3		
0.1850	0.0	0.0		0.0			0.0		
0.1900	0.0	0.0		0.0			0.0		
0.1950	0.0	0.0		0.0			0.0		
0.2000	0.0	0.0		0.0			0.0		

Table XXII. Printout. Example No. 1 (page 6 of 27)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA

SUMMARY OF TOLERANCE DATA USED IN INJURY CRITERIA

QUANTITY	MAXIMUM ACCEPTABLE VALUE	NATURE OF INJURY OR DATA	WEIGHTING CODE
1. SEVERITY INDEX	1. 1500	1. INTERNAL HEAD INJURY. DANGEROUS TO LIFE.	1. 22/26
2. HEAD PITCH ACCELERATION	2. 1800 RAD/SEC/SEC	2. 50% CHANCE OF CEREBRAL CONCUSSION.	2. 12/26
3. CHEST LOAD	3. 2000 LB	3. RIB FRACTURE OF CADAVER.	3. 12/26
4. STCULCER BELT LOAD	4. 2000 LB COMBINED	4. PREDICTED TOLERANCE LEVEL WITHOUT INJURY.	4. 1/26
5. PELVIC BELT LOAD	5. 4000 LB	5. MAXIMUM VOLUNTARY LOAD.	5. 1/26
6. KNEE LOAD (EACH)	6. 1400 LB	6. COMMUNUTED PATELLA FRACTURE.	6. 12/26
7. CHEST A-P G-LOAD	7. 60 G-PEAK	7. VOLUNTEER DATA WITH NO INJURY. (DURATION=.09 SEC, RISE TIME=500 G/SEC) HIGHER RISE TIMES OR LONGER DURATIONS CAN DECREASE THIS VALUE SIGNIFICANTLY.	7. 4/26
8. CHEST S-I G-LOAD	8. 26 G-PEAK	8. VOLUNTEER DATA. FRACTURED VERTEBRAE	8. 16/26

LIST OF REFERENCES

- GADD, C.W., "USE OF A WEIGHTED-IMPULSE CRITERION FOR ESTIMATING INJURY HAZARD", PROC. 10TH. STAPP CAR CRASH CONF., NOV. 1966, P.95-100.
- CMAYA, A.K. ET AL. "COMPARATIVE TOLERANCES FOR CEREBRAL CONCUSSION BY HEAD IMPACT AND WHIPLASH INJURY IN PRIMATES", 1970 INTERNATIONAL AUTOMOBILE SAFETY CONFERENCE COMPENDIUM, SAE PAPER NO. P-30, P.808-817.
- GADD, C.W. AND PATRICK, L.M., "SYSTEM VERSUS LABORATORY IMPACT TESTS FOR ESTIMATING INJURY HAZARD", SAE PAPER NO. 680053, JAN. 1968.
- "ESTIMATED PROBABLE THRESHOLD OF INJURY BY BIOMECHANICS TASK FORCE OF SAF OCCUPANT RESTRAINT SYSTEMS SUBCOMMITTEE.
- STAPP, J.P. AND ENFIELD, D.L., "EVALUATION OF THE LAP-TYPE AUTOMOBILE SAFETY BELT WITH REFERENCE TO HUMAN TOLERANCE", SAE PAPER NO. 62A, 1958.
- SNYDER, R.G., "HUMAN IMPACT TOLERANCE", 1970 INTERNATIONAL AUTOMOBILE SAFETY CONFERENCE COMPENDIUM, SAE PAPER NO. P-30, P.712-782.
- IEIC.
- IBID.

NOTE: THE WEIGHTING CODE IS BASED ON VAN KIRK, D.J. AND LANGE, W.A., "A DETAILED INJURY SCALE FOR ACCIDENT INVESTIGATION", PROC. OF THE 12TH. STAPP CAR CRASH CONFERENCE, OCT. 1968, P.240-259.
 MINOR INJURY = 1-4/26, MODERATE INJURY = 8-10/26, MODERATELY SEVERE INJURY = 12-14/26,
 SEVERE INJURY = 16-18/26, CRITICAL INJURY = 20-22/26, FATAL INJURY = 24-26/26.

Table XXII. Printout. Example No. 1 (page 7 of 27)

SUMMARY OF ANGULAR MOTION LIMITS USED IN INJURY CRITERIA

JOINT	FLEXION	HYPEREXTENSION
1. HIP	10 DEG	130 DEG
2. LOWER SPINE	20 DEG	22 DEG
3. UPPER SPINE	20 DEG	22 DEG
4. NECK	70 DEG	70 DEG
5. SHOULDER	55 DEG	190 DEG
6. ELBOW	5 DEG	140 DEG
7. KNEE	5 DEG	140 DEG

NOTE: ALL QUANTITIES MEASURED FROM AN ERECT STANDING POSITION WITH ARMS AT SIDES.

Table XXII. Printout. Example No. 1 (page 8 of 27)

SUMMARY OF QUANTITIES EXCEEDING TOLERANCES

QUANTITY	PEAK	TIME OF OCCURRENCE	DURATION	TIME START	TIME END	WEIGHTING CODE
HEAD PITCH ACCELERATION	2356.	0.045000	0.004091	0.083138	0.087229	12/26
HEAD FITCH ACCELERATION	2452.	0.165000	0.013817	0.156602	C.170419	12/26
SHOULDER BELT LOAD	4557.	0.075000	0.060201	0.046211	C.106412	1/26
CHEST S-I G-LOAD	-42.	0.065000	0.013752	0.041860	0.075612	16/26
CHEST S-I G-LOAD	27.	0.085000	0.000600	0.084848	C.085448	16/26
CHEST S-I G-LOAD	39.	0.145000	0.010357	0.141249	0.151605	16/26
CHEST S-I G-LOAD	38.	0.165000	0.009508	0.158032	C.167540	16/26
CHEST S-I G-LOAD	38.	0.195000	0.009015	0.187876	0.196891	16/26
UPPER SPINE HYPEREXTENSION	35.	0.100000	0.055738	0.085828	C.145565	-----
NECK HYPEREXTENSION	78.	C.115000	0.065984	0.077347	0.143331	-----
ELBOW FLEXION	3.	0.080000	0.003568	0.078888	C.082456	-----
ELBOW HYPEREXTENSION	156.	0.170000	0.042160	0.153596	0.195756	-----

Table XXII. Printout. Example No. 1 (page 9 of 27)

PROBABILITY OF OCCURRENCE

THE PROBABILITY OF OCCURRENCE IS BASED ON:

- 1. PROBABILITY OF FRONT COLLISION = 0.4430
- 2. PROBABILITY OF DRIVER = 1.0000
- 3. PROBABILITY OF SHOULDER & LAP BELT USE = 0.0460

PROBABILITY OF OCCURRENCE = 0.0204

Table XXII. Printout. Example No. 1 (page 10 of 27)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR PLOT OF OUTPUT DATA
 BELT FORCES IN LBS.

	0.00	.0200	.0400	.0600	.0800	.1000	.1200	.1400	.1600	.1800	.2000
3626.78											
2901.43											
2176.07											
1450.71											
725.36											
0.00											

TIME IN SECCNDS

* IS LAP BELT
 X IS LOWER SHOULDER RESTRAINT
 = IS UPPER SHCULDER RESTRAINT

Table XXII. Printout. Example No. 1 (page 11 of 27)

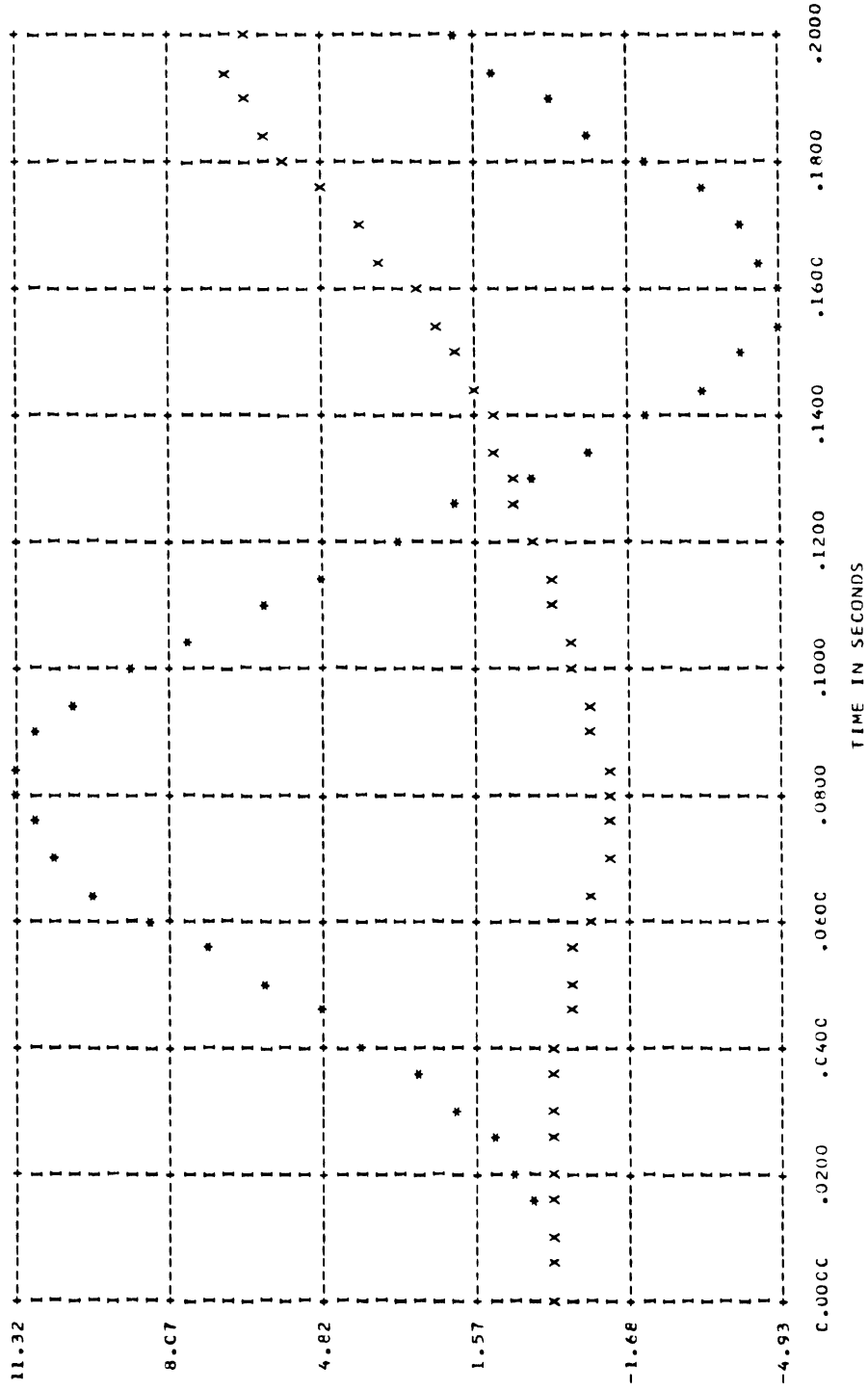
TWO DIMENSIONAL CRASH VICTIM SIMULATOR PLOT OF OUTPUT DATA
ACCELERATION, IN G-UNITS

TIME IN SECONDS	.0200	.0400	.0600	.0800	.1000	.1200	.1400	.1600	.1800	.2000
101.04										
HC.88					*					*
60.73				*						*
40.57										
20.41										
.26	X	X	X	X	X	X	X	X	X	X

* IS HEAD ACCELERATION
X IS CHEST ACCELERATION

Table XXII. Printout, Example No. 1 (page 12 of 27)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR PLCT OF OUTPUT DATA
HIP POSITION IN INCHES



* IS HORIZONTAL HIP POSITION
X IS VERTICAL HIP POSITION

Table XXII. Printout. Example No. 1 (page 13 of 27)

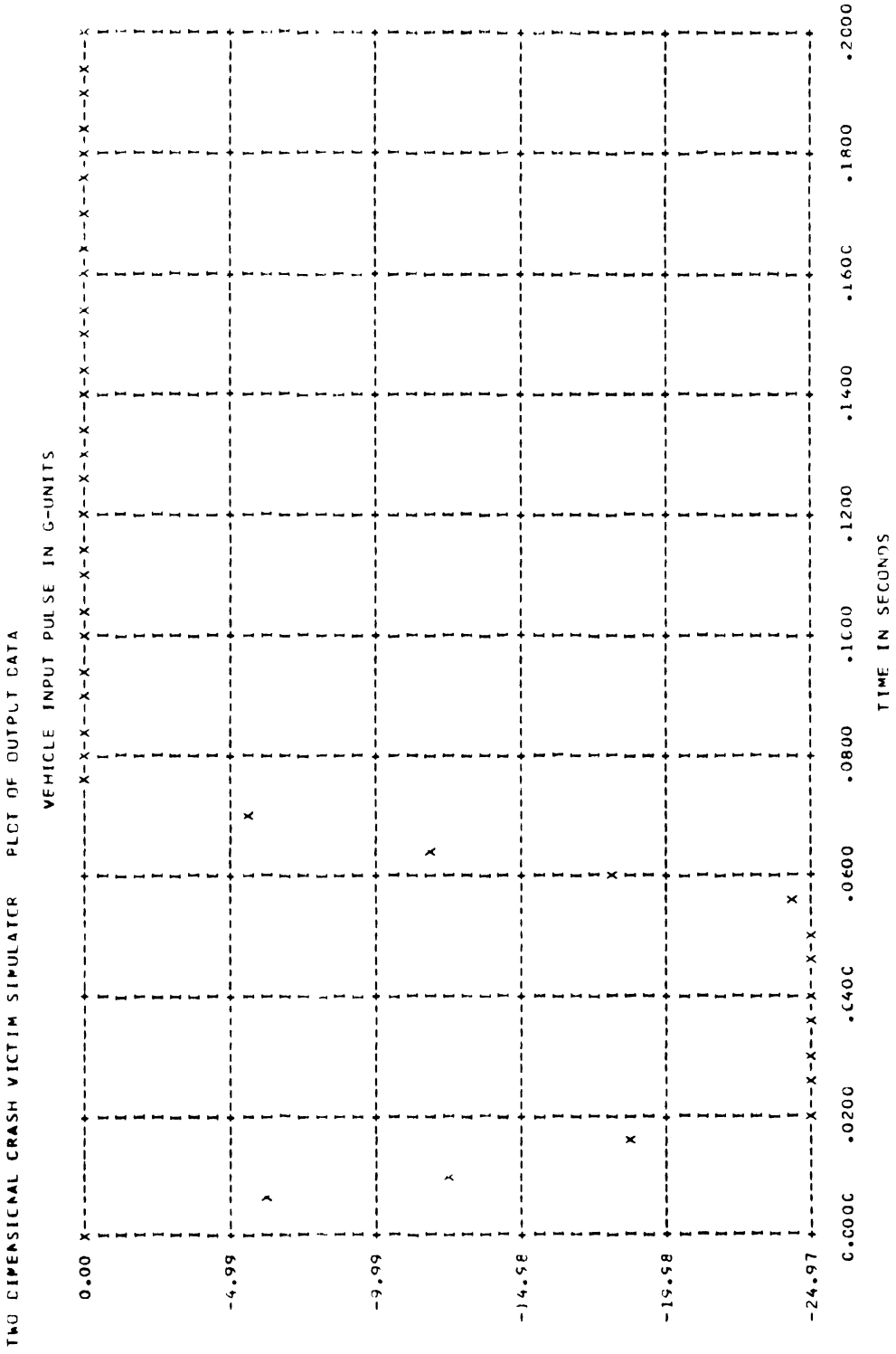
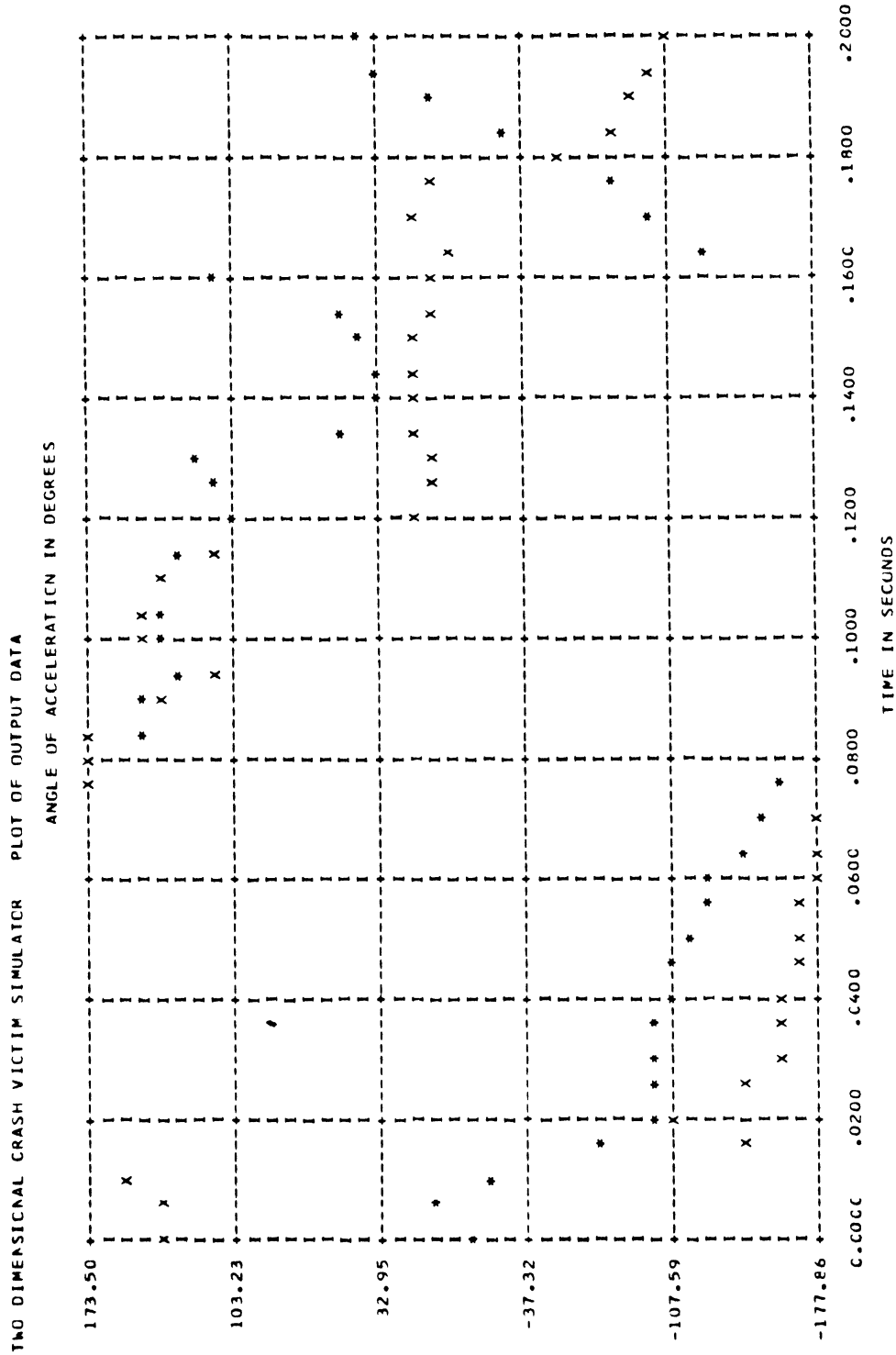


Table XXII. Printout, Example No. 1 (page 14 of 27)

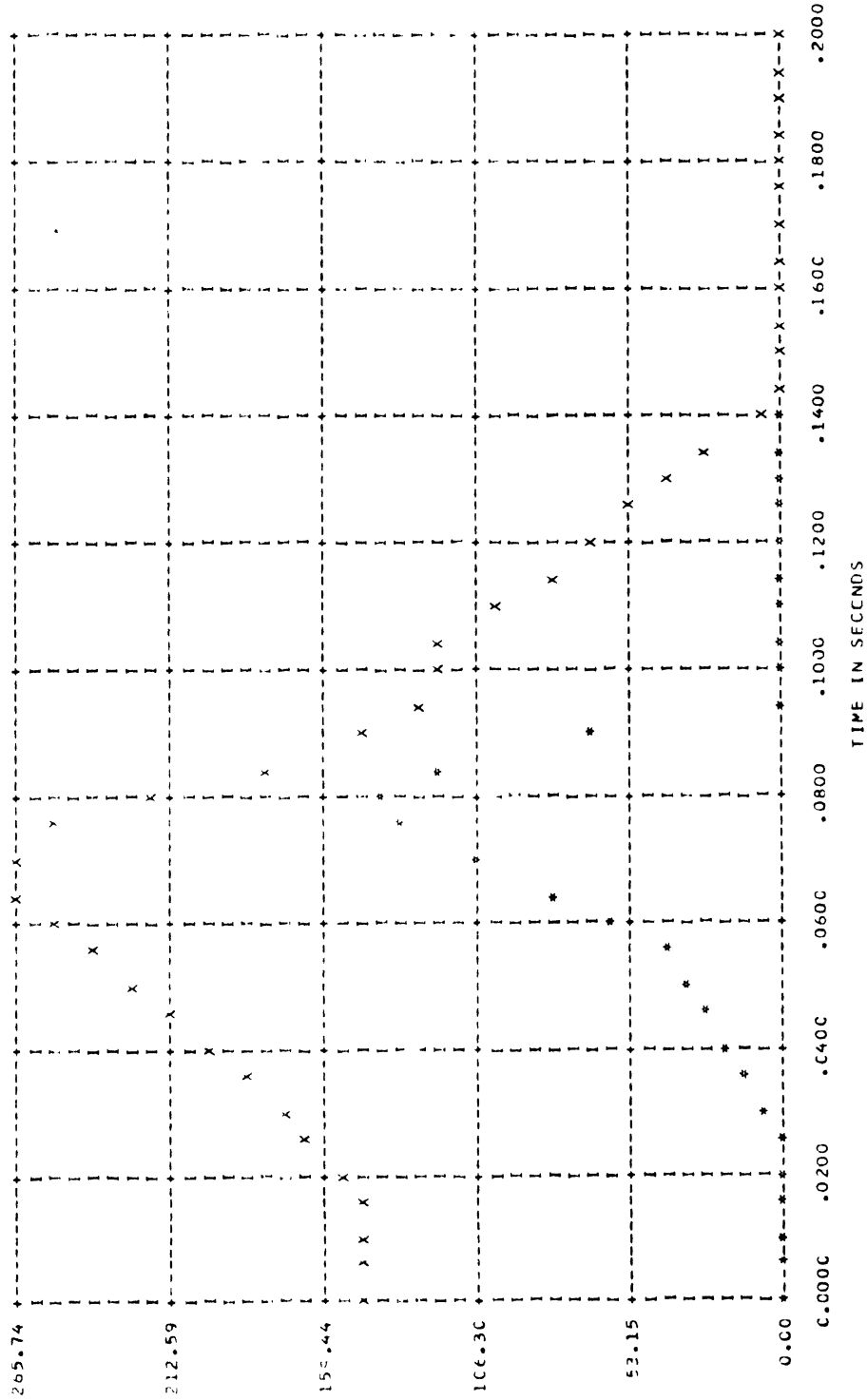


* IS ANGLE OF HEAD ACCELERATION
 X IS ANGLE OF CHEST ACCELERATION

Table XXII. Printout. Example No. 1 (page 15 of 27)

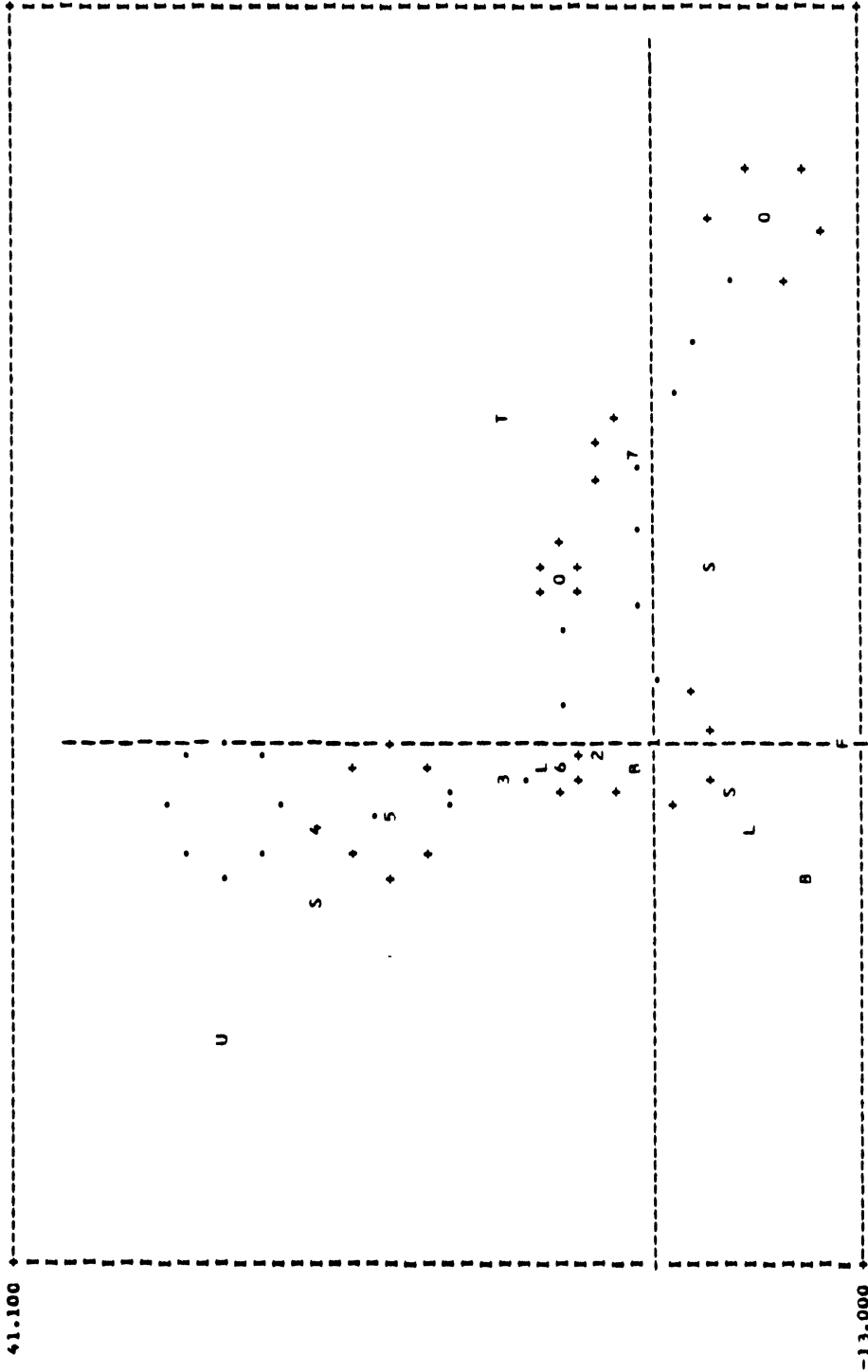
THO DIMENSIONAL CRASH VICTIM SIMULATOR PLOT OF OUTPUT DATA

SEAT FORCES IN LBS.



* IS SEAT FORCE AT FRNT OF SEAT
 X IS SEAT FORCE AT HIP

Table XXII. Printout. Example No. 1 (page 16 of 27)

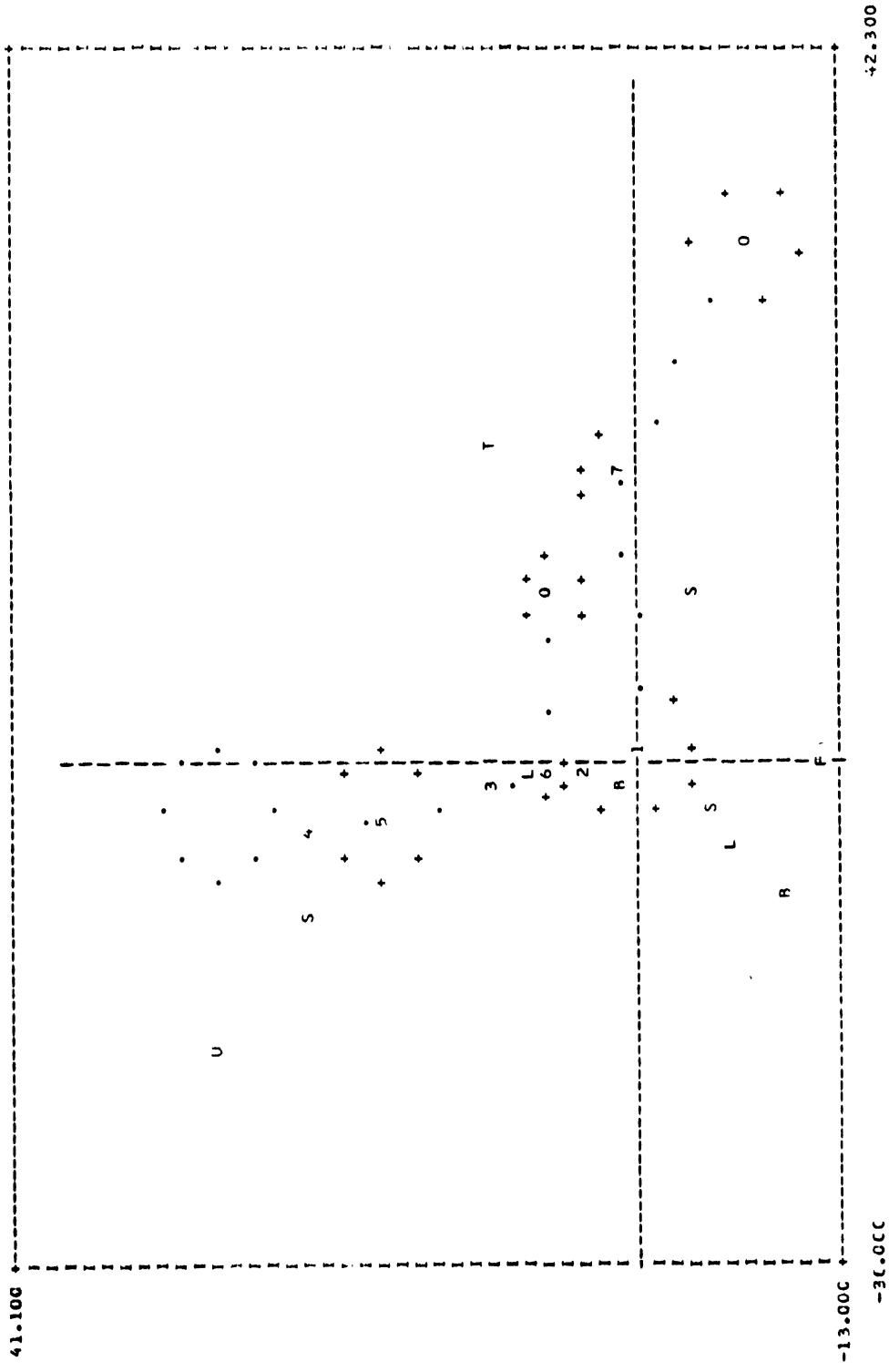


-30.000

42.300

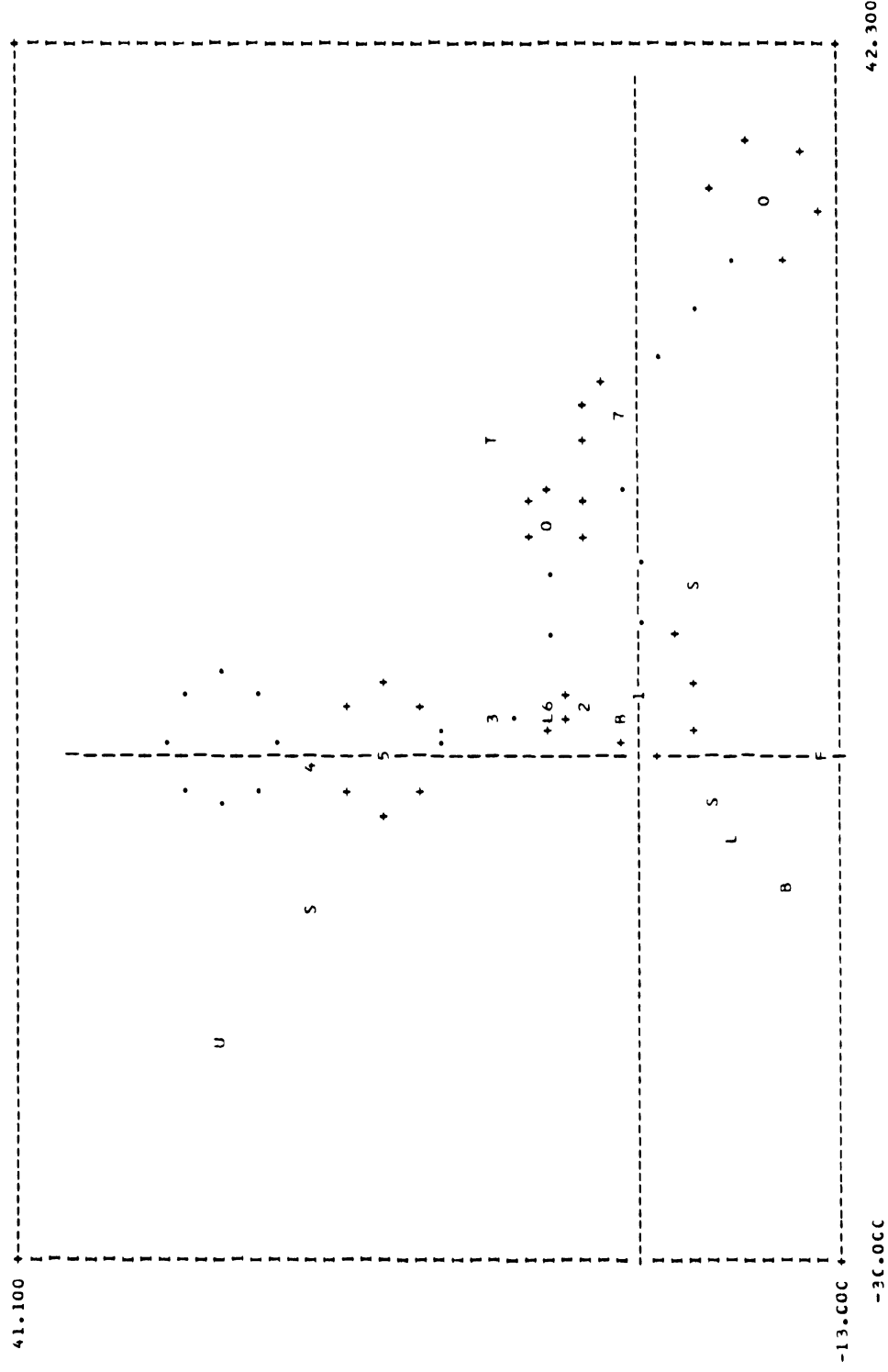
INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

TWO DIMENSIONAL CRASH VICTIP SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.020 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

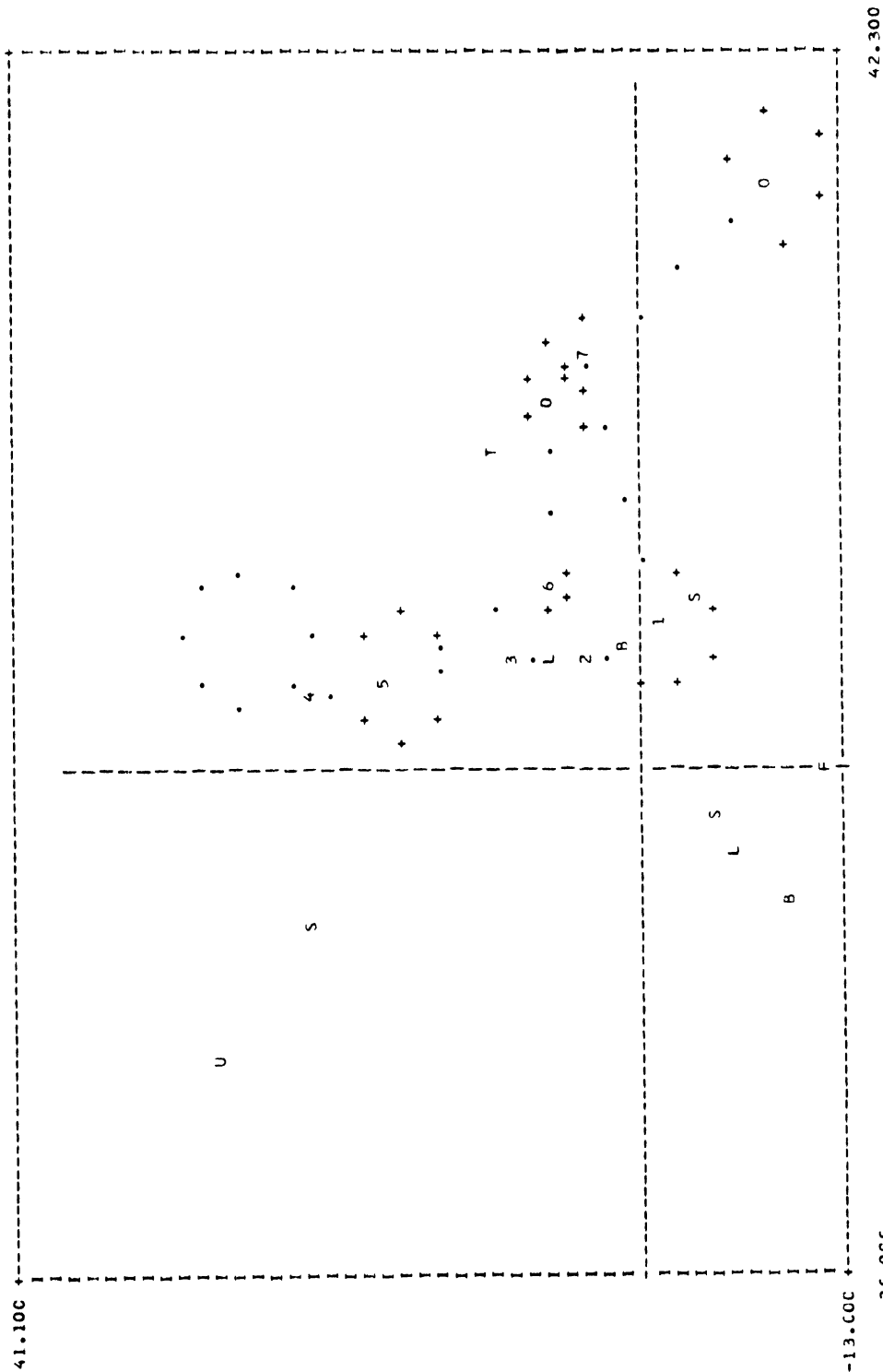
Table XXII. Printout. Example No. 1 (page 18 of 27)



INDICATED MEASUREMENTS ARE IN INCHES.
 SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
 1 TO 7.66 IN THE Y DIRECTION

Table XXII. Printout. Example No. 1 (page 19 of 27)

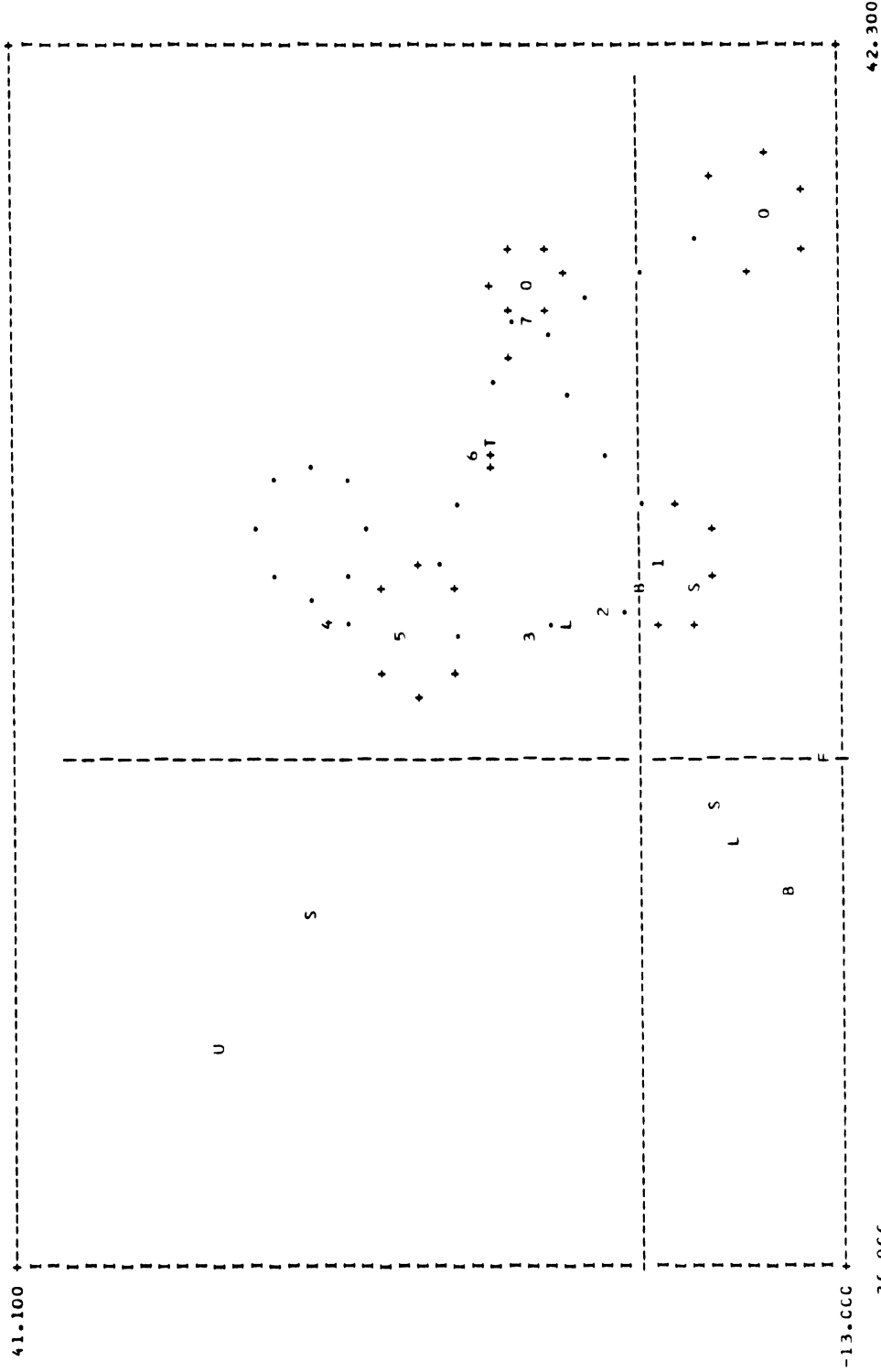
TWC DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.060 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

Table XXII. Printout. Example No. 1 (page 20 of 27)

TWC DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.080 SECONDS

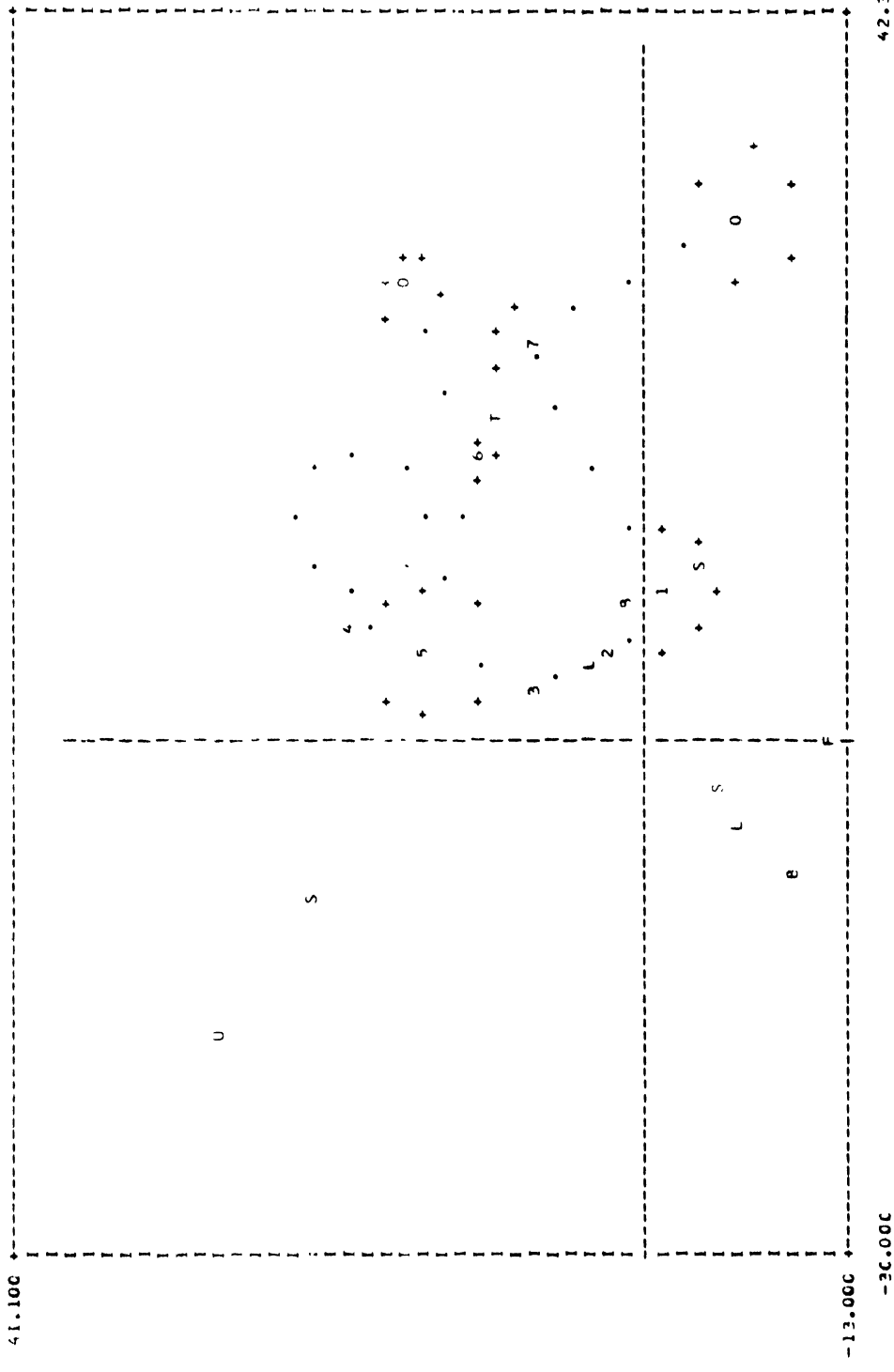


INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

Table XXII. Printout. Example No. 1 (page 21 of 27)

SEP 1, 1972

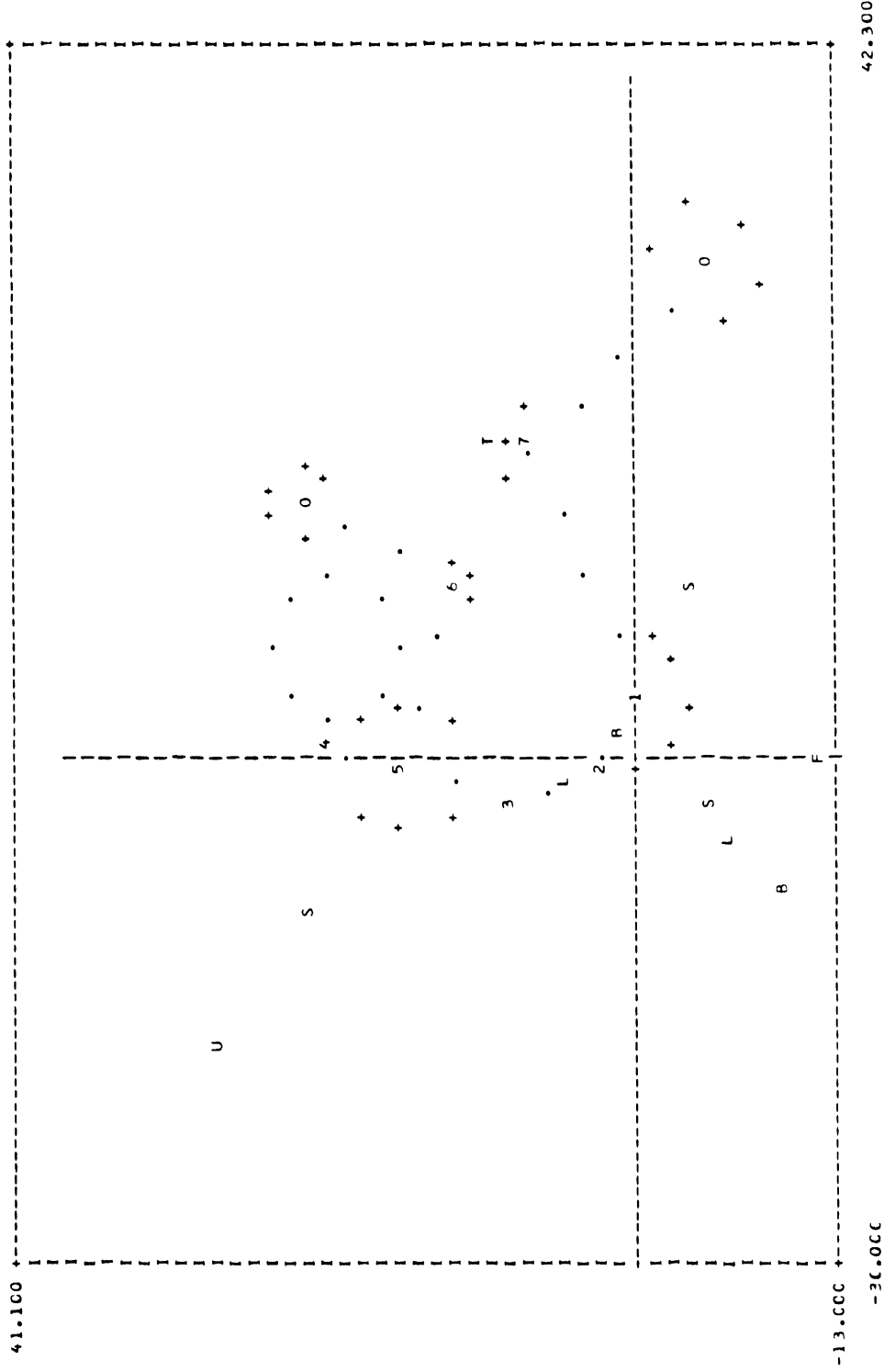
TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.100 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

Table XXII. Printout. Example No. 1 (page 22 of 27)

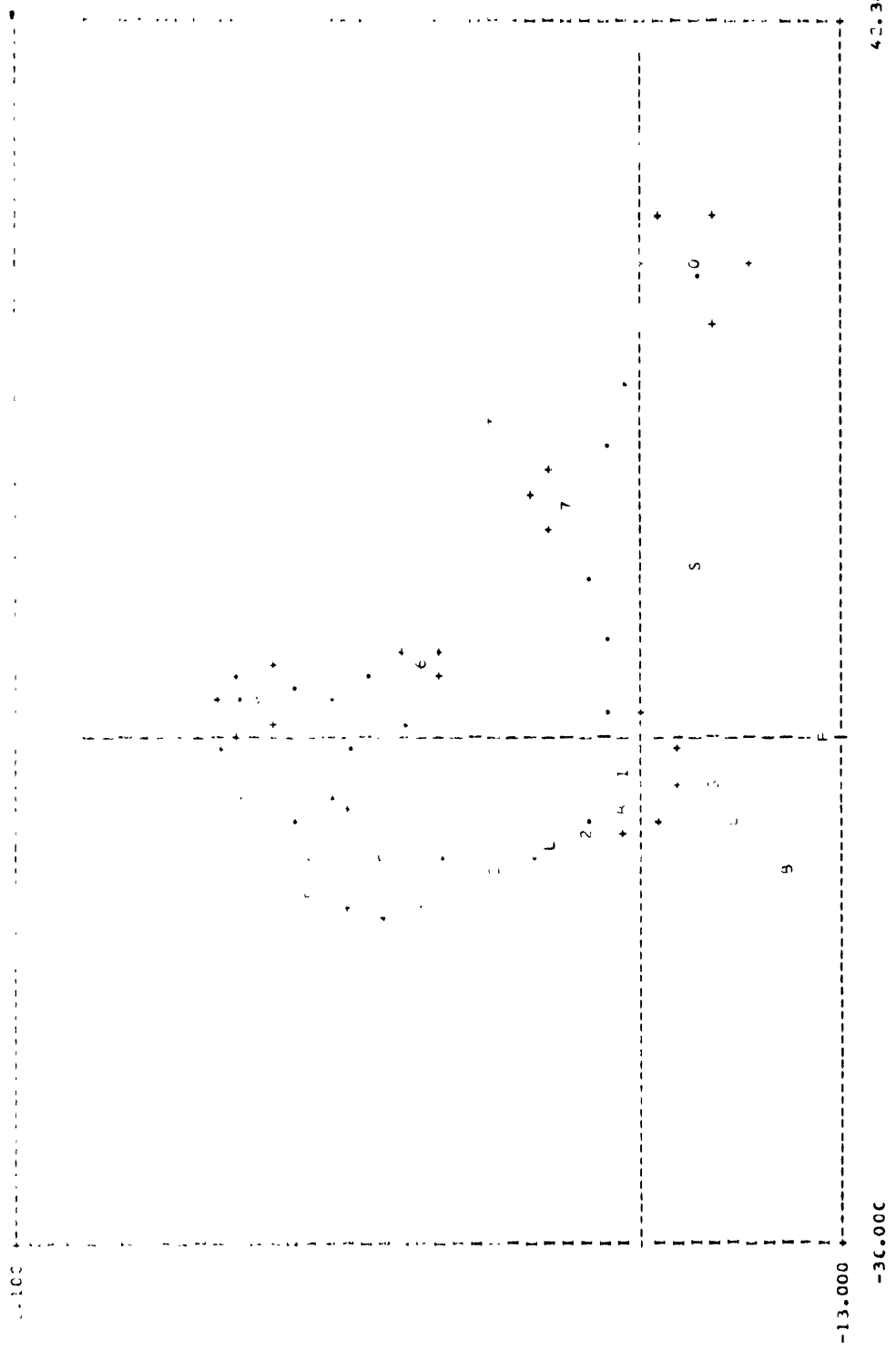
TWC DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.120 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

Table XXII. Printout. Example No. 1 (page 23 of 27)

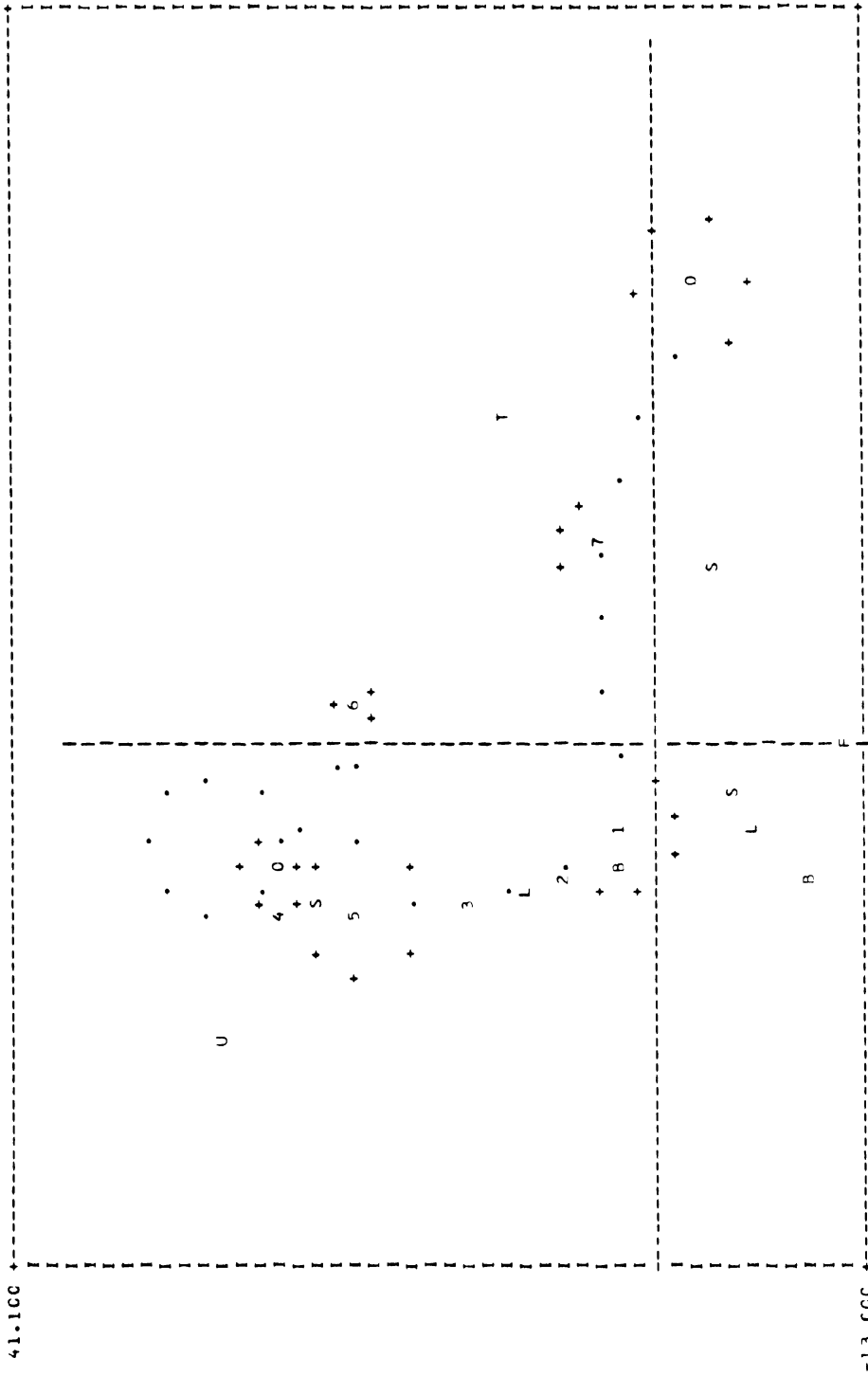
TWO DIMENSIONAL GRAF VECTIN SIMULATIO OUTPUT DATA
 STICK FIGURE REPRESENTATION EQU TIME = 0.1700 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
 SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
 1 TO 7.06 IN THE Y DIRECTION

Table XXII. Printout. Example No. 1 (page 24 of 27)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.160 SECONDS



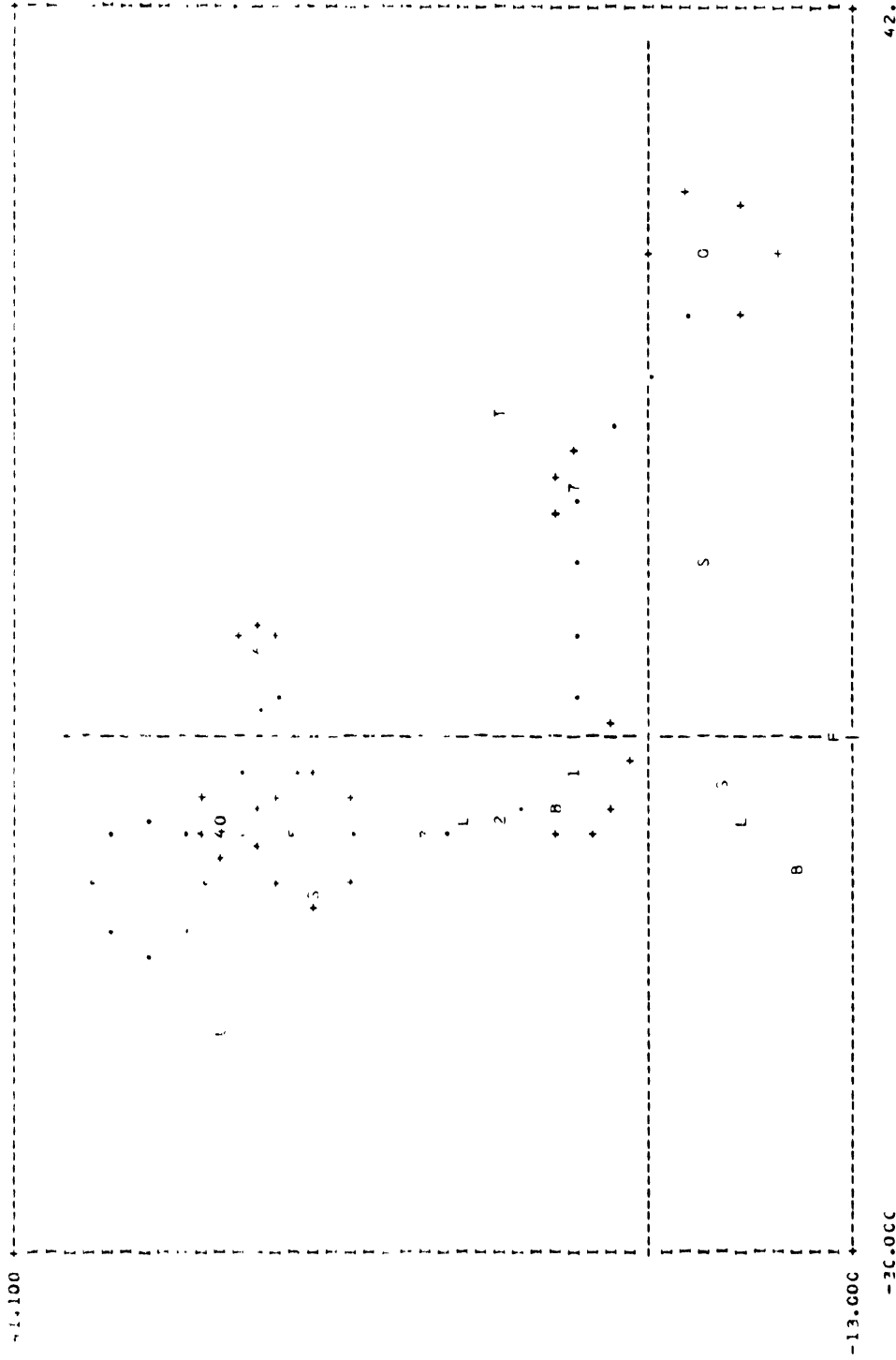
-30.000

42.300

INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

Table XXII. Printout. Example No. 1 (page 25 of 27)

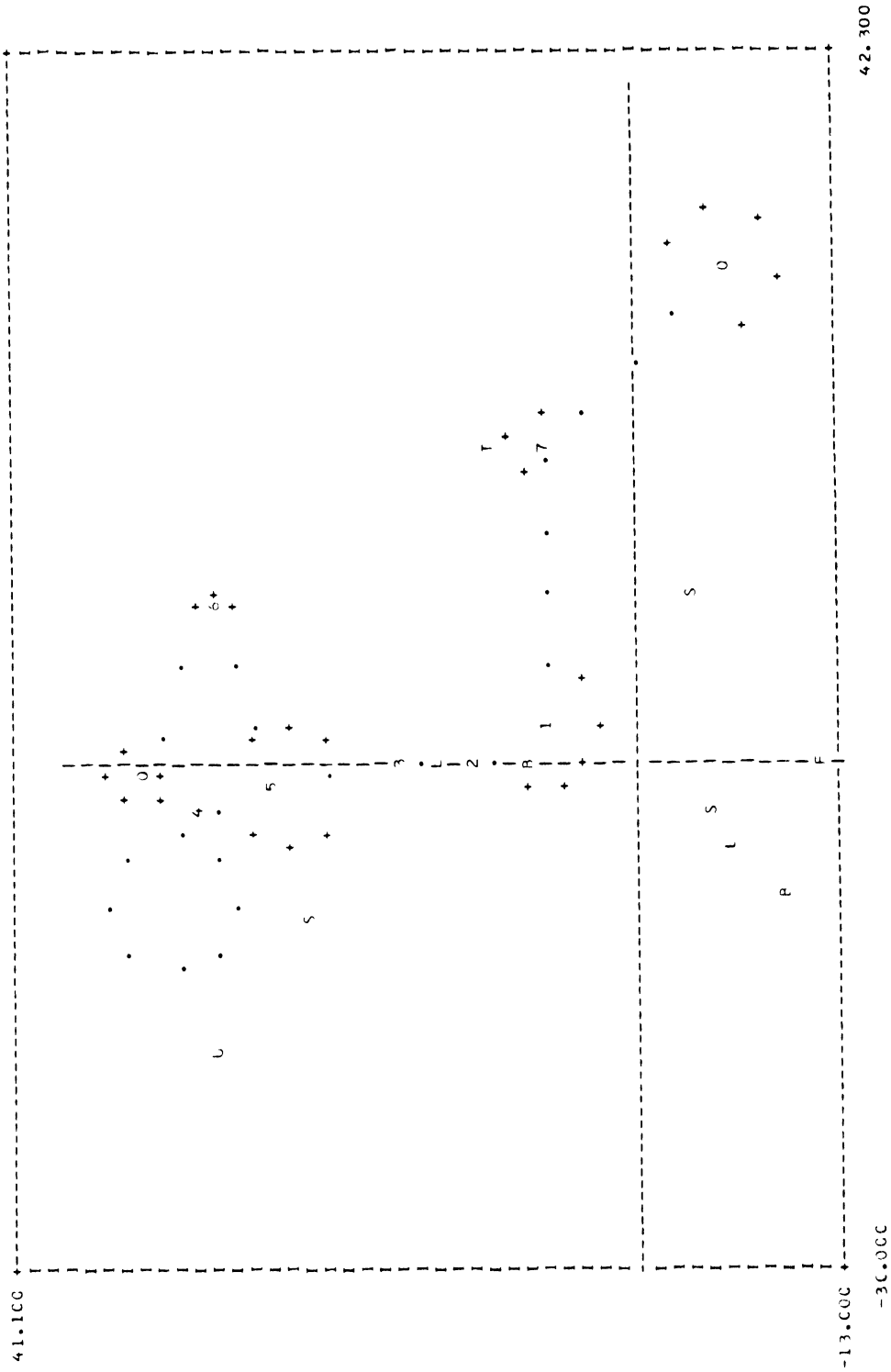
TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.180 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

Table XXII. Printout. Example No. 1 (page 26 of 27)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.200 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TC 7.09 IN THE X DIRECTION
1 TC 7.06 IN THE Y DIRECTION

Table XXII. Printout. Example No. 1 (page 27 of 27)

Example No. 2. 30 mph Front Collision. Lap Belt and EA Steering Column.
50th Percentile Male.

The same occupant, vehicle, and crash event have been modeled with the exception that the upper torso belts have been removed. This data set is given in Table XXIII. The belts have been replaced by the EA column and airbag combination specified as Figure 60 of the report, "Passive Protection at 50 Miles Per Hour" by Carter.³³ The complex force-deformation profile was modeled by three independent contact surfaces placed one behind the other. The cumulative effect of these three surfaces is shown in Figure 40. These surfaces have been relabeled as required. An upper instrument panel has also been added to restrain the motion of the head as it pitches downward after the upper torso has begun to interact with the EA column elements.

The tabular output for this exercise is included in Table XXIV. Although the steering column produces acceptable G-loadings on the chest, the head G-loadings caused by upper instrument panel contact may be excessive. To save space only the tabular output and three stick diagrams have been included in this table.

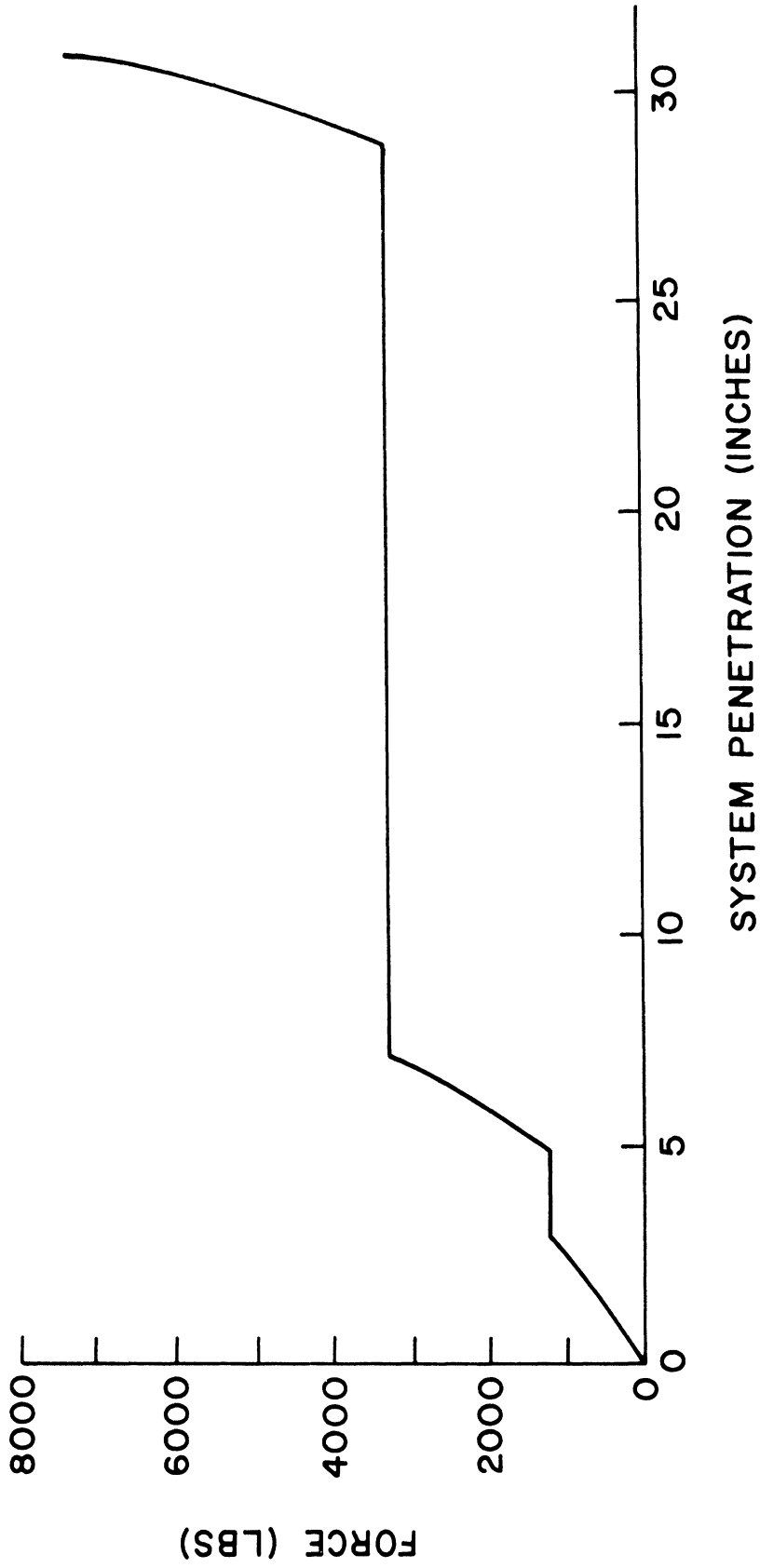


Figure 40. Static Force-Deflection Characteristics of EA Column-Airbag Combination


```

134      05      S. C. BOTTOM OUT
135      -2
136      -1.
137      -443
138      1.
139      -2      1.
140      -37.0  2      2      100  3      11      1
141      -13.  4+  42.3  0      0      0      41.1  0.
142      0      0      0      0      0
      END OF FILE
      .02

```

TIME (SEC.)	TWO DIMENSIONAL CBASH VICTIM SIMULATOR OUTPUT DATA				RELATIVE HIP POSITION (INCHES)		RELATIVE HEAD POSITION (INCHES)		PAGE 1
	LAP BELT RESTRAINT UPPER	LAP BELT RESTRAINT LOWER	BELT ANGLES (DEGREES)	SEAT BELT SHOULDER RESTRAINT UPPER	HORIZONTAL	VERTICAL	HORIZONTAL	VERTICAL	
0.0	0.	0.	59.5	0.0	0.0	0.0	-3.88	26.93	
0.005	3.	0.	59.5	0.0	0.01	0.0	-3.87	26.93	
0.010	25.	0.	59.2	0.0	0.07	0.00	-3.79	26.93	
0.015	84.	0.	58.5	0.0	0.25	0.01	-3.60	26.93	
0.020	197.	0.	57.1	0.0	0.59	0.01	-3.23	26.93	
0.025	377.	0.	55.0	0.0	1.15	-0.01	-2.63	26.92	
0.030	614.	0.	52.2	0.0	1.91	-0.05	-1.78	26.89	
0.035	889.	0.	48.9	0.0	2.85	-0.13	-0.69	26.84	
0.040	1172.	0.	45.3	0.0	3.92	-0.28	0.64	26.75	
0.045	1432.	0.	41.7	0.0	5.08	-0.49	2.21	26.67	
0.050	1646.	0.	38.1	0.0	6.31	-0.76	4.04	26.39	
0.055	1800.	0.	34.7	0.0	7.59	-1.07	6.11	26.10	
0.060	1902.	0.	31.4	0.0	8.91	-1.43	8.43	25.73	
0.065	2010.	0.	28.2	0.0	10.24	-1.87	10.92	25.31	
0.070	2258.	0.	25.4	0.0	11.50	-2.31	13.47	24.84	
0.075	2768.	0.	23.3	0.0	12.58	-2.69	15.96	24.30	
0.080	3392.	0.	21.8	0.0	13.30	-2.97	18.27	23.64	
0.085	3681.	0.	21.2	0.0	13.54	-3.14	20.29	22.73	
0.090	3534.	0.	21.5	0.0	13.21	-3.17	21.93	21.48	
0.095	3124.	0.	22.6	0.0	12.32	-3.05	23.08	20.09	
0.100	2529.	0.	25.0	0.0	10.99	-2.73	23.77	19.05	
0.105	1842.	0.	28.6	0.0	9.33	-2.23	23.96	18.68	
0.110	1163.	0.	33.4	0.0	7.50	-1.61	23.65	19.01	
0.115	600.	0.	39.4	0.0	5.62	-0.86	22.73	19.80	
0.120	256.	0.	46.5	0.0	3.82	0.03	21.18	20.59	
0.125	168.	0.	54.1	0.0	2.14	1.02	19.27	21.14	
0.130	296.	0.	61.5	0.0	0.64	2.04	17.29	21.49	
0.135	501.	0.	67.6	0.0	-0.60	2.88	15.40	21.77	
0.140	448.	0.	70.9	0.0	-1.37	3.10	13.64	22.12	
0.145	167.	0.	72.4	0.0	-1.79	2.97	12.13	22.75	
0.150	0.	0.	72.7	0.0	-1.94	2.74	10.71	23.58	
0.155	0.	0.	70.4	0.0	-1.85	2.49	9.34	24.57	
0.160	0.	0.	68.0	0.0	-1.54	2.25	8.01	25.70	
0.165	0.	0.	65.3	0.0	-1.03	2.08	6.71	26.90	
0.170	0.	0.	63.0	0.0	-0.38	2.03	5.48	28.08	
0.175	0.	0.	61.3	0.0	0.30	2.15	4.29	29.06	
0.180	0.	0.	60.4	0.0	0.94	2.47	3.08	29.63	
0.185	0.	0.	60.4	0.0	1.49	2.97	1.77	29.67	
0.190	330.	0.	60.1	0.0	1.95	3.64	0.32	29.34	
0.195	828.	0.	60.4	0.0	2.32	4.44	-1.24	28.80	
0.200	1199.	0.	61.0	0.0	2.59	5.31	-2.91	28.30	

Table XXIV. Selected Printout. Example No. 2 (page 1 of 9)

TIME	LOWER TORSO			CENTER TORSO			UPPER TORSO			ACCEL.	POSITION VELOCITY	HEAD VELOCITY	ACCEL.
	POSITION	VELOCITY	ACCEL.	POSITION	VELOCITY	ACCEL.	POSITION	VELOCITY	ACCEL.				
0.0	103.00	0.0	0.6625E 03	103.00	0.0	0.7102E 03	103.00	0.0	0.5780E 03	75.00	-0.2594E 01	-0.2594E 01	
0.0050	103.00	-1.76	-0.4215E 03	102.99	-2.50	-0.7438E 03	103.00	2.21	0.3913E 03	74.97	-0.2533E 01	-0.2533E 01	
0.0100	102.98	-3.02	0.1295E 03	102.97	-7.63	-0.1611E 04	103.02	3.80	0.1868E 03	74.87	-0.2083E 01	-0.2083E 01	
0.0150	102.97	0.53	0.1641E 04	102.96	-20.41	-0.4364E 04	103.04	3.76	-0.3085E 03	74.72	-0.1047E 01	-0.1047E 01	
0.0200	103.00	14.04	0.4154E 04	102.74	-50.76	-0.9104E 04	103.05	0.22	-0.1309E 04	74.55	-0.3432E 01	-0.3432E 01	
0.0250	103.14	41.49	0.7104E 04	102.34	-114.29	-0.1775E 05	103.03	-9.83	-0.2997E 04	74.40	-0.2324E 01	-0.2324E 01	
0.0300	103.44	82.87	0.9493E 04	101.51	-228.72	-0.2947E 05	102.93	-29.97	-0.5451E 04	74.34	-0.1757E 01	-0.1757E 01	
0.0350	103.93	133.25	0.1046E 05	93.95	-404.67	-0.4818E 05	102.70	-64.63	-0.8886E 04	74.46	0.1427E 01	0.1427E 01	
0.0400	104.77	184.19	0.9516E 04	57.37	-635.80	-0.5056E 05	101.47	-118.75	-0.1339E 05	75.58	0.1692E 05	0.1692E 05	
0.0450	105.80	226.49	0.6883E 04	31.54	-894.58	-0.5155E 05	101.25	-197.75	-0.2488E 05	76.73	0.1748E 05	0.1748E 05	
0.0500	107.01	252.20	0.2757E 04	19.44	-1138.54	-0.4412E 05	100.23	-305.69	-0.3952E 05	78.31	0.1533E 05	0.1533E 05	
0.0550	108.22	219.08	0.3962E 05	82.27	-1285.24	0.1818E 05	98.36	-451.76	-0.3840E 05	80.16	-0.4132E 05	-0.4132E 05	
0.0600	108.61	-130.60	-0.9672E 05	76.51	-922.79	0.1318E 06	95.57	-663.04	-0.3840E 05	81.12	-0.7512E 05	-0.7512E 05	
0.0650	106.88	-437.65	0.7038E 04	73.48	-438.65	0.7338E 04	91.87	-777.92	-0.2338E 04	81.12	-0.7512E 05	-0.7512E 05	
0.0700	104.77	-357.59	0.1678E 05	71.36	-398.59	0.1678E 05	87.98	-755.50	-0.2653E 05	80.18	-0.1631E 06	-0.1631E 06	
0.0750	103.00	-300.10	0.1261E 05	63.62	-301.71	0.1261E 05	84.66	-561.63	0.3676E 05	75.40	-0.2136E 06	-0.2136E 06	
0.0800	101.60	-292.42	-0.1109E 05	59.16	-293.42	-0.1109E 05	82.22	-436.52	0.7850E 04	65.40	-0.1701E 06	-0.1701E 06	
0.0850	99.94	-383.31	-0.2213E 05	68.54	-384.31	-0.2213E 05	80.00	-484.95	-0.3327E 05	51.13	-0.9137E 05	-0.9137E 05	
0.0900	97.74	-484.99	-0.1751E 05	64.33	-465.99	-0.1751E 05	77.00	-754.23	-0.7775E 05	34.56	-0.2703E 06	-0.2703E 06	
0.0950	95.13	-564.67	-0.1464E 05	61.70	-565.87	-0.1464E 05	72.19	-1174.91	-0.7742E 05	15.59	-0.3346E 06	-0.3346E 06	
0.1000	92.11	-645.56	-0.7557E 04	59.76	-579.59	0.5677E 04	65.62	-1388.15	-0.1176E 05	10.86	-0.9364E 06	-0.9364E 06	
0.1050	88.00	-670.41	-0.5794E 04	59.05	-501.19	0.2005E 05	58.62	-1399.29	0.3629E 04	10.80	0.2935E 06	0.2935E 06	
0.1100	85.33	-717.76	-0.1296E 05	51.77	-418.02	0.8281E 04	51.66	-1386.23	0.1037E 04	19.68	0.1297E 06	0.1297E 06	
0.1150	81.53	-807.42	-0.2244E 05	51.67	-451.66	-0.2973E 05	44.78	-1340.01	0.2925E 05	35.84	-0.4992E 05	-0.4992E 05	
0.1200	77.23	-903.41	-0.5748E 04	48.90	-679.97	-0.5436E 05	38.64	-1071.58	0.8048E 05	55.43	-0.1070E 06	-0.1070E 06	
0.1250	72.59	-997.93	-0.2758E 04	44.88	-898.93	-0.2758E 04	34.36	-633.65	0.8230E 05	74.21	-0.9911E 05	-0.9911E 05	
0.1300	68.26	-349.36	0.2441E 05	40.45	-850.36	0.2441E 05	32.18	-248.80	0.7000E 05	90.45	0.1824E 06	0.1824E 06	
0.1350	64.84	-427.74	0.1144E 06	37.12	-314.21	0.1912E 06	31.90	164.50	0.1019E 06	104.07	0.2406E 05	0.2406E 05	
0.1400	64.24	156.97	0.1083E 06	37.38	262.86	0.6428E 04	33.99	656.52	0.8917E 05	113.53	1336.40	-0.2358E 06	
0.1450	66.03	484.68	0.4636E 05	31.18	483.68	0.4636E 05	38.07	918.98	0.3103E 05	117.88	603.32	-0.7694E 05	
0.1500	63.03	726.56	0.6189E 05	42.16	694.61	0.3188E 05	43.01	1048.76	0.2341E 05	119.92	205.24	-0.8984E 05	
0.1550	73.53	1385.42	0.7700E 05	45.98	825.64	0.2434E 05	48.54	1162.40	0.2315E 05	119.74	-298.65	-0.1131E 06	
0.1600	79.83	1450.76	0.6401E 05	53.46	986.20	0.4657E 05	54.61	1264.11	0.1885E 05	116.77	-897.20	-0.1255E 06	
0.1650	87.42	1481.15	-0.2079E 05	55.27	1377.70	0.8571E 05	61.13	1336.64	0.1105E 05	110.84	-1450.92	-0.1069E 06	
0.1700	94.66	1411.89	-0.2248E 05	63.46	1417.68	-0.1317E 05	68.23	1529.72	0.4664E 05	102.09	-2073.58	-0.1317E 06	
0.1750	101.35	1240.05	-0.4812E 05	71.46	1393.78	0.2095E 04	76.44	1746.45	0.3381E 05	90.11	-2695.91	-0.1033E 06	
0.1800	106.92	940.38	-0.5437E 05	77.54	1455.84	0.2410E 05	85.47	1830.17	-0.3746E 04	75.63	-3017.76	-0.9351E 04	
0.1850	111.17	729.42	-0.4132E 05	85.16	1600.97	0.3133E 05	94.38	1707.52	-0.3918E 05	60.76	-2861.62	0.6879E 05	
0.1900	114.42	599.50	-0.7686E 04	83.55	1747.00	0.2455E 05	102.39	1493.98	-0.4363E 05	47.44	-2445.50	0.9502E 05	
0.1950	117.41	617.81	0.1651E 05	102.51	1818.17	0.4373E 04	109.34	1286.88	-0.4901E 05	36.43	-1946.34	0.1494E 06	
0.2000	120.76	729.32	0.2452E 05	111.64	1824.21	-0.7262E 04	115.01	955.44	-0.7930E 05	29.41	-703.00	-0.3408E 06	

Table XXIV. Selected Printout. Example No. 2 (page 2 of 9)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
BODY SEGMENT ANGULAR ORIENTATION (DEGREES)

TIME	UPPER ARM			LOWER ARM			UPPER LEG			LOWER LEG		
	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.
0.0	-77.00	0.0	0.5724E 03	0.0	0.0	0.2683E 04	6.00	0.0	-0.1820E 04	-33.00	0.0	0.1524E 04
0.0050	-76.99	3.31	0.5970E 03	0.0	-13.90	-0.2742E 04	5.97	-10.17	-0.2032E 04	-32.97	11.44	0.2400E 04
0.0100	-76.97	5.74	0.4847E 03	0.14	-26.94	-0.2372E 04	5.90	-19.90	-0.1784E 04	-32.88	23.83	0.2630E 04
0.0150	-76.93	7.78	0.2950E 03	0.30	-37.06	-0.1486E 04	5.78	-27.59	-0.1154E 04	-32.73	38.31	0.3317E 04
0.0200	-76.89	8.56	0.3690E 02	0.50	-40.82	0.3099E 03	5.64	-25.56	0.2825E 04	-32.56	9.53	-0.1909E 05
0.0250	-76.85	7.51	-0.4154E 03	0.69	-33.71	0.2890E 03	5.57	1.22	0.8645E 04	-32.84	-134.48	-0.3775E 05
0.0300	-76.82	4.80	-0.6665E 03	0.81	-12.49	0.5935E 04	5.70	59.11	0.1522E 05	-33.99	-327.75	-0.3557E 05
0.0350	-76.80	1.45	-0.6102E 03	0.79	24.38	0.9133E 04	6.21	150.44	0.2190E 05	-36.32	-465.66	-0.1664E 05
0.0400	-76.80	-0.72	-0.1381E 03	0.54	77.57	0.1246E 05	7.26	274.18	0.2794E 05	-38.49	-508.41	-0.1211E 04
0.0450	-76.80	1.22	0.1168E 04	0.02	146.81	0.1542E 05	9.00	422.62	0.3106E 05	-41.03	-513.55	-0.4663E 04
0.0500	-76.77	11.81	0.3473E 04	0.55	228.70	0.1729E 05	11.50	576.43	0.2952E 05	-43.72	-576.83	-0.2400E 05
0.0550	-76.66	39.05	0.9635E 04	2.31	313.43	0.1405E 05	14.73	718.05	0.3017E 05	-46.98	-742.27	-0.4226E 05
0.0600	-76.26	146.74	0.4064E 05	3.99	340.22	-0.8237E 04	18.73	883.94	0.3540E 05	-51.23	-957.15	-0.3688E 05
0.0650	-74.95	378.66	0.4442E 05	5.54	283.24	-0.8523E 04	23.55	1021.44	0.1284E 05	-56.35	-1058.99	0.2253E 04
0.0700	-72.46	644.79	0.8260E 05	6.60	197.40	-0.3992E 05	28.79	1060.38	-0.2722E 04	-61.45	-943.64	0.4476E 05
0.0750	-68.02	1152.79	0.1059E 06	7.09	-122.80	-0.8617E 05	33.96	982.57	-0.3279E 05	-65.53	-673.74	0.6009E 05
0.0800	-60.96	1664.83	0.3796E 05	5.27	-630.34	-0.1187E 06	38.32	733.40	-0.6417E 05	-68.14	-370.17	0.6425E 05
0.0850	-51.44	2135.73	0.8360E 05	3.55	-1272.58	-0.1361E 06	41.13	381.40	-0.7673E 05	-68.80	212.18	0.4866E 05
0.0900	-39.69	2543.68	0.6285E 05	-7.47	-1912.88	-0.1204E 06	42.06	-407.32	-0.8010E 05	-67.16	432.02	0.3531E 05
0.0950	-26.61	2456.23	-0.2622E 06	-17.58	-1757.00	0.4165E 06	41.01	-407.32	-0.8010E 05	-64.59	601.44	0.3922E 05
0.1000	-18.95	710.98	-0.1102E 06	-13.04	1017.31	0.1379E 06	37.99	-776.05	-0.5630E 05	-61.10	792.86	0.3651E 05
0.1050	-16.78	159.98	-0.1044E 06	-11.64	1925.72	0.1643E 06	33.48	-1016.20	-0.3954E 05	-61.10	962.70	0.3033E 05
0.1100	-17.17	-282.69	-0.6393E 05	-0.15	2614.58	0.3942E 05	27.94	-1194.03	-0.3256E 05	-56.69	1161.04	0.2569E 05
0.1150	-19.21	-495.95	-0.2028E 05	13.90	2348.95	0.3033E 05	21.56	-1356.43	-0.3296E 05	-51.52	1413.66	0.3134E 05
0.1200	-21.85	-539.97	0.2234E 04	28.84	2980.12	-0.1953E 05	14.36	-1520.41	-0.3117E 05	-39.07	1513.66	0.3829E 05
0.1250	-24.48	-502.72	0.1125E 05	43.40	2828.80	-0.3719E 05	6.39	-1660.37	-0.2163E 05	-31.54	1595.22	0.3026E 05
0.1300	-26.83	-434.19	0.1667E 05	57.09	2651.16	-0.3229E 05	-2.14	-1738.93	-0.6680E 04	-25.71	-99.48	-0.8223E 06
0.1400	-29.60	-283.27	0.5343E 05	63.95	2488.14	-0.3927E 05	-8.66	-169.46	0.7110E 06	-33.57	-2257.71	0.1070E 05
0.1450	-30.08	-92.15	-0.3643E 04	31.55	2320.42	-0.3714E 05	6.92	1896.25	0.4143E 05	-44.35	-2029.16	0.5175E 05
0.1500	-31.39	-132.55	-0.7301E 04	33.17	2175.22	-0.3714E 05	2.73	1921.85	0.2031E 05	-53.87	-1787.17	0.4219E 05
0.1550	-32.52	-179.12	-0.1477E 05	103.59	1957.86	-0.8635E 05	16.12	1778.57	-0.2338E 05	-62.32	-1604.03	0.3019E 05
0.1600	-34.31	-448.65	-0.3225E 05	111.89	1265.86	-0.1986E 06	24.73	1669.51	-0.2037E 05	-69.88	-1361.31	0.9899E 05
0.1700	-36.82	-532.16	-0.4410E 04	115.43	93.82	-0.2649E 06	32.83	1570.03	-0.1991E 05	-74.99	-560.05	0.2676E 06
0.1750	-39.46	-503.54	0.1682E 05	113.56	-652.91	-0.3652E 05	40.46	1482.15	-0.2079E 05	-73.71	1137.47	0.3164E 06
0.1800	-41.71	-349.50	0.2883E 05	109.19	-1092.59	-0.6019E 05	47.59	1363.28	-0.3309E 05	-65.05	2117.37	0.4073E 06
0.1850	-43.23	-234.71	0.1165E 05	102.76	-1460.38	-0.6009E 05	53.92	1144.65	-0.5832E 05	-54.46	2087.07	-0.1530E 05
0.1900	-44.06	-72.53	0.3379E 05	94.83	-1679.87	-0.2215E 05	58.87	831.79	-0.6464E 05	-44.22	1985.09	-0.8584E 05
0.1950	-43.99	58.27	0.3288E 05	86.29	-1710.42	0.3436E 04	62.23	512.53	-0.6117E 05	-36.36	952.08	-0.3287E 06
0.2000	-43.10	257.06	0.3143E 05	70.14	-1488.12	0.3177E 05	64.15	293.38	-0.1737E 05	-36.12	-914.91	-0.3819E 06
				63.11	-1310.52	0.3737E 05	65.50	252.37	-0.1360E 05	-44.71	-2276.16	-0.7234E 05
							66.39	60.06	-0.6339E 05			

Table XXIV. Selected Printout. Example No. 2 (page 3 of 9)

TWO DIMENSIONAL CRASH VEHICLE SIMULATION OUTPUT DATA									
VEHICULAR MOTION					JULIE MOTION AT HLE JOINT				
TIME	POSITION (IN.)	VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)	RELATIVE VELOCITY (IN.)	RELATIVE VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)	RELATIVE DISPL. (IN.)	RELATIVE VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)
0.0	0.0	528.00	0.0	0.0	528.00	0.0	0.0	0.0	0.0
0.0050	2.630	521.97	-6.244	0.000	527.05	-0.578	0.000	0.000	0.000
0.0100	5.200	503.38	-12.467	0.000	525.84	-0.714	0.000	0.000	0.000
0.0150	7.649	473.72	-18.733	0.000	524.12	-1.094	0.000	0.000	0.000
0.0200	9.917	431.50	-24.974	0.000	521.40	-2.003	0.000	0.000	0.000
0.0250	11.950	383.25	-24.974	0.000	518.03	-3.931	0.000	0.000	0.000
0.0300	13.743	335.00	-24.974	0.000	505.66	-7.092	0.000	0.000	0.000
0.0350	15.304	289.75	-24.974	0.000	498.63	-11.435	0.000	0.000	0.000
0.0400	16.617	238.50	-24.974	0.000	463.21	-15.435	0.000	0.000	0.000
0.0450	17.689	190.25	-24.974	0.000	430.42	-18.560	0.000	0.000	0.000
0.0500	18.580	142.00	-24.974	0.000	393.04	-20.014	0.000	0.000	0.000
0.0550	19.165	93.77	-24.974	0.000	354.42	-19.181	0.000	0.000	0.000
0.0600	19.410	52.28	-18.356	0.000	319.33	-17.298	0.000	0.000	0.000
0.0650	19.651	11.50	-5.464	0.000	244.43	-14.571	0.000	0.000	0.000
0.0700	19.717	0.14	0.0	0.000	243.75	-25.135	0.000	0.000	0.000
0.0750	19.729	0.14	0.0	0.000	195.00	-30.902	0.000	0.000	0.000
0.0800	19.727	0.14	0.0	0.000	150.65	-37.095	0.000	0.000	0.000
0.0850	19.726	0.14	0.0	0.000	100.33	-43.917	0.000	0.000	0.000
0.0900	19.728	0.14	0.0	0.000	53.47	-51.169	0.000	0.000	0.000
0.0950	19.730	0.14	0.0	0.000	0.14	-57.769	0.000	0.000	0.000
0.1000	19.731	0.14	0.0	0.000	0.14	-62.812	0.000	0.000	0.000
0.1050	19.731	0.14	0.0	0.000	0.14	-66.422	0.000	0.000	0.000
0.1100	19.732	0.14	0.0	0.000	0.14	-68.622	0.000	0.000	0.000
0.1150	19.733	0.14	0.0	0.000	0.14	-69.517	0.000	0.000	0.000
0.1200	19.733	0.14	0.0	0.000	0.14	-69.122	0.000	0.000	0.000
0.1250	19.734	0.14	0.0	0.000	0.14	-67.466	0.000	0.000	0.000
0.1300	19.734	0.14	0.0	0.000	0.14	-64.566	0.000	0.000	0.000
0.1350	19.735	0.14	0.0	0.000	0.14	-60.422	0.000	0.000	0.000
0.1400	19.736	0.14	0.0	0.000	0.14	-55.068	0.000	0.000	0.000
0.1450	19.737	0.14	0.0	0.000	0.14	-48.488	0.000	0.000	0.000
0.1500	19.738	0.14	0.0	0.000	0.14	-40.813	0.000	0.000	0.000
0.1550	19.739	0.14	0.0	0.000	0.14	-32.074	0.000	0.000	0.000
0.1600	19.739	0.14	0.0	0.000	0.14	-22.473	0.000	0.000	0.000
0.1650	19.740	0.14	0.0	0.000	0.14	-12.044	0.000	0.000	0.000
0.1700	19.741	0.14	0.0	0.000	0.14	-0.961	0.000	0.000	0.000
0.1750	19.741	0.14	0.0	0.000	0.14	0.437	0.000	0.000	0.000
0.1800	19.741	0.14	0.0	0.000	0.14	1.991	0.000	0.000	0.000
0.1850	19.742	0.14	0.0	0.000	0.14	3.608	0.000	0.000	0.000
0.1900	19.743	0.14	0.0	0.000	0.14	5.294	0.000	0.000	0.000
0.1950	19.744	0.14	0.0	0.000	0.14	7.046	0.000	0.000	0.000
0.2000	19.744	0.14	0.0	0.000	0.14	8.859	0.000	0.000	0.000

Table XXIV. Selected Printout. Example No. 2 (page 4 of 9)

ACCELEROMETER READINGS

TIME	HEAD		CHEST		ANGLE (DEG.)	LAP	SHOULDER RESTRAINT		AT HIP	AT FRONT EDGE
	RESULTANT (G-UNITS)	ANGLE (DEG.)	RESULTANT (G-UNITS)	ANGLE (DEG.)			LOWER	UPPER		
0.0	0.3	-8.2	3.4	138.7	0.0	0.0	0.0	145.00	0.0	0.0
0.0050	0.3	3.2	3.4	141.0	3.3	0.0	0.0	144.92	0.0	0.0
0.0100	0.3	-16.7	3.4	159.1	25.4	0.0	0.0	146.16	0.0	0.0
0.0150	0.3	-68.9	0.4	-144.9	84.4	0.0	0.0	149.33	0.0	0.0
0.0200	0.9	-97.1	1.1	-109.6	197.5	0.0	0.0	155.51	0.0	0.0
0.0250	1.7	-104.2	2.4	-102.5	376.5	0.0	0.0	165.56	0.0	0.0
0.0300	2.7	-105.4	3.3	-102.6	613.9	0.0	0.0	180.06	4.90	0.0
0.0350	3.8	-105.4	5.7	-105.5	888.8	0.0	0.0	199.23	11.44	0.0
0.0400	5.1	-103.8	7.3	-109.8	1171.8	0.0	0.0	222.06	16.71	0.0
0.0450	6.5	-101.1	10.0	-115.5	1432.1	0.0	0.0	246.22	21.67	0.0
0.0500	8.0	-97.0	12.1	-123.1	1645.6	0.0	0.0	268.92	28.38	0.0
0.0550	7.7	-89.3	15.3	-145.4	1799.8	0.0	0.0	289.54	47.10	0.0
0.0600	5.9	-60.4	23.5	-179.4	1902.3	0.0	0.0	321.08	62.32	0.0
0.0650	9.7	-64.9	22.3	-180.0	2009.5	0.0	0.0	354.69	101.95	0.0
0.0700	11.5	-56.9	35.8	-171.6	2257.6	0.0	0.0	371.97	156.53	0.0
0.0750	22.6	-82.2	47.4	168.4	2767.7	0.0	0.0	378.59	219.09	0.0
0.0800	49.3	-107.3	49.4	167.2	3391.6	0.0	0.0	373.94	271.07	0.0
0.0850	74.6	-127.1	48.3	167.2	3680.9	0.0	0.0	352.80	292.32	0.0
0.0900	78.3	-165.0	43.3	167.4	3533.6	0.0	0.0	314.25	263.47	0.0
0.0950	94.3	136.2	36.4	159.3	3124.0	0.0	0.0	257.67	187.26	0.0
0.1000	133.0	118.8	36.1	161.0	2529.0	0.0	0.0	176.84	83.49	0.0
0.1050	131.2	117.4	24.3	156.9	1842.4	0.0	0.0	109.32	0.0	0.0
0.1100	115.7	138.5	10.1	122.7	1162.6	0.0	0.0	51.01	0.0	0.0
0.1150	99.7	-176.1	14.4	26.4	599.9	0.0	0.0	0.0	0.0	0.0
0.1200	78.4	-130.6	18.1	8.3	256.0	0.0	0.0	0.0	0.0	0.0
0.1250	48.9	-89.3	9.3	8.6	167.9	0.0	0.0	0.0	0.0	0.0
0.1300	34.2	-52.0	5.1	-13.5	295.8	0.0	0.0	0.0	0.0	0.0
0.1350	36.3	-3.7	25.1	-104.2	500.9	0.0	0.0	0.0	0.0	74.58
0.1400	73.4	37.3	12.3	-55.6	448.1	0.0	0.0	0.0	0.0	0.0
0.1450	27.3	53.6	7.3	35.4	167.0	0.0	0.0	0.0	0.0	0.0
0.1500	27.3	57.4	6.5	70.9	0.0	0.0	0.0	1.83	0.0	0.0
0.1550	25.7	53.9	5.3	133.9	0.0	0.0	0.0	32.82	0.0	0.0
0.1600	22.1	37.3	8.8	153.1	0.0	0.0	0.0	54.69	0.0	0.0
0.1650	20.5	-2.9	10.4	128.6	0.0	0.0	0.0	59.90	137.94	0.0
0.1700	32.7	-48.8	0.6	112.0	0.0	0.0	0.0	36.76	153.14	0.0
0.1750	60.9	-73.3	4.4	128.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1800	75.3	-101.1	8.0	133.8	0.0	0.0	0.0	0.0	0.0	0.0
0.1850	59.3	-121.3	7.2	160.8	0.0	0.0	0.0	0.0	0.0	0.0
0.1900	37.0	-143.7	7.3	-143.7	390.0	0.0	0.0	0.0	0.0	0.0
0.1950	28.5	157.6	12.3	-115.2	828.3	0.0	0.0	0.0	0.0	0.0
0.2000	90.8	110.0	24.4	-110.1	1199.4	0.0	0.0	0.0	0.0	0.0

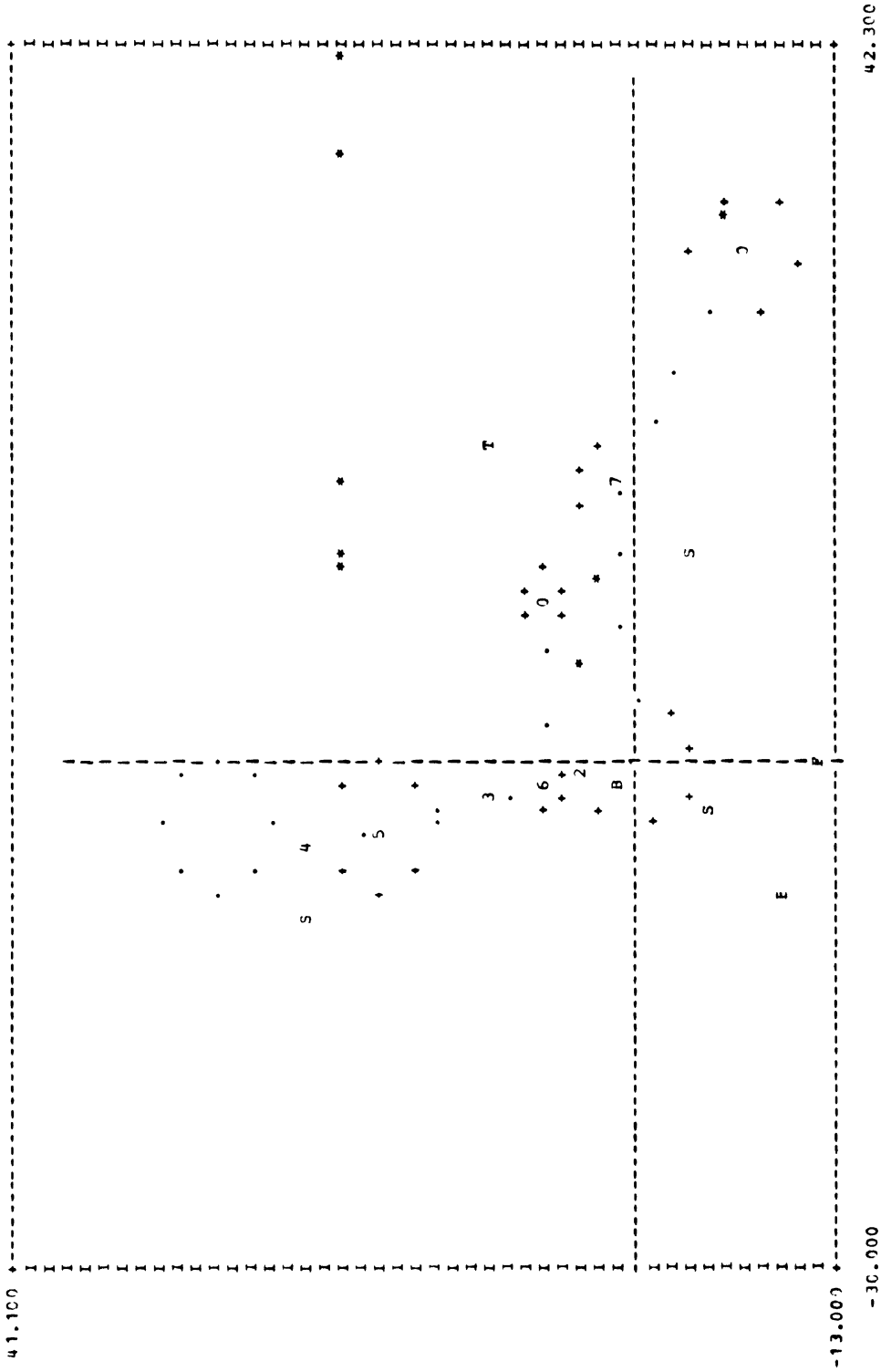
Table XXIV. Selected Printout. Example No. 2 (page 5 of 9)

CONTACT FORCES (LBS.)

TIME	FOOT ON FLOOR	TOE ECARD ON	FOCI ON	UPPER TORSO	STEERING WHEEL	UPPER TORSO	STEERING COLUMN	UPPER I. P.	HEAD ON	SEAT BACK	HIP ON
0.0	18.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0050	18.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0100	19.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0150	23.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0200	40.4	202.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0250	141.3	439.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0300	335.0	611.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0350	735.2	716.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0400	1080.2	817.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0450	1321.6	1044.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0500	1442.2	1311.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0550	1455.0	1520.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0600	1530.5	1530.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0650	1491.4	1157.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0700	1195.8	635.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0750	499.9	240.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0800	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0850	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0900	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0950	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1050	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1150	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1250	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1300	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1350	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1450	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1500	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1550	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1600	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1650	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1700	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1750	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1800	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1850	0.0	621.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1900	0.0	2883.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1950	0.0	3450.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.2000	0.0	738.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

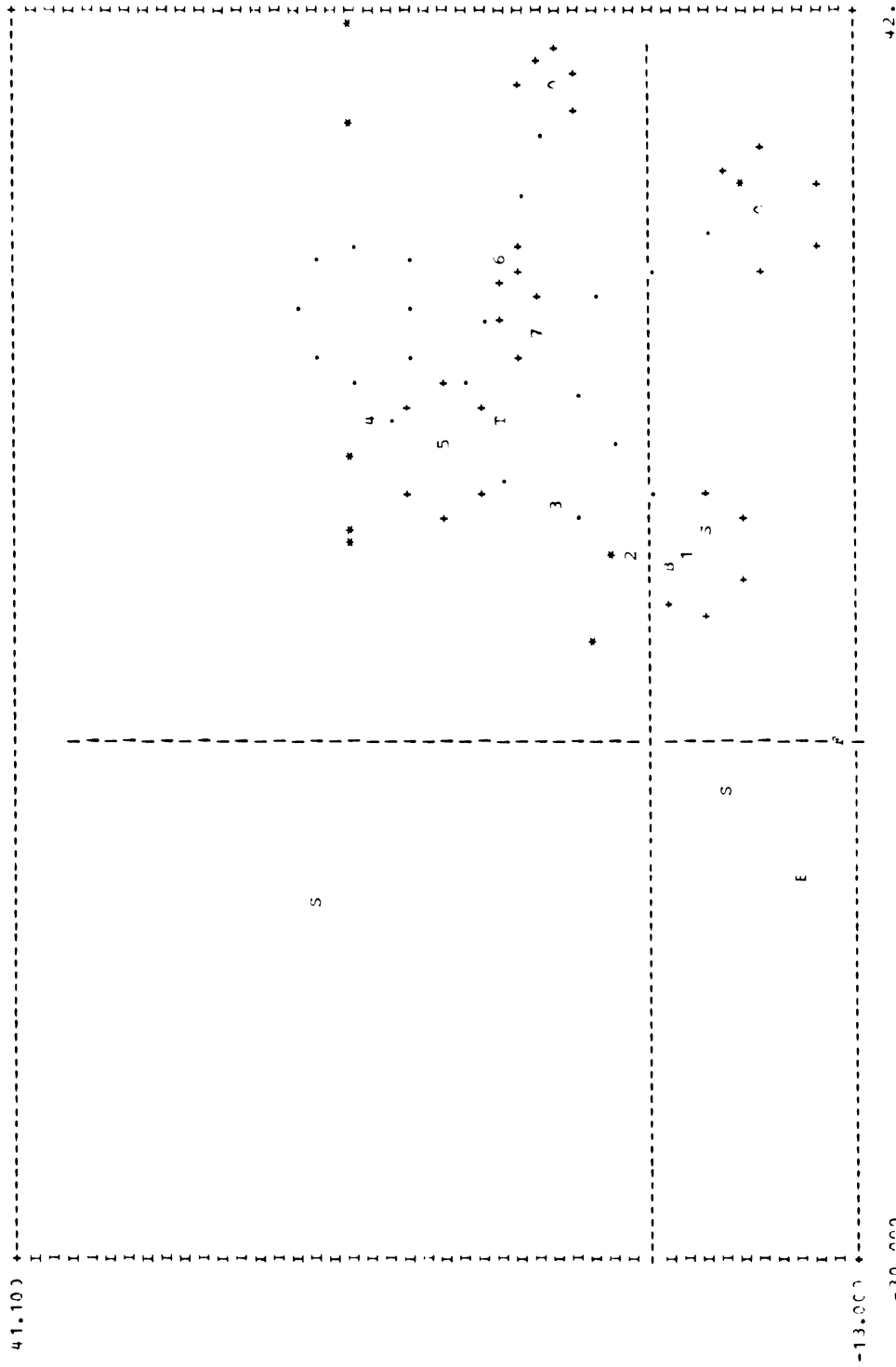
Table XXIV. Selected Printout. Example No. 2 (page 6 of 9)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR 114E = 0.0 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

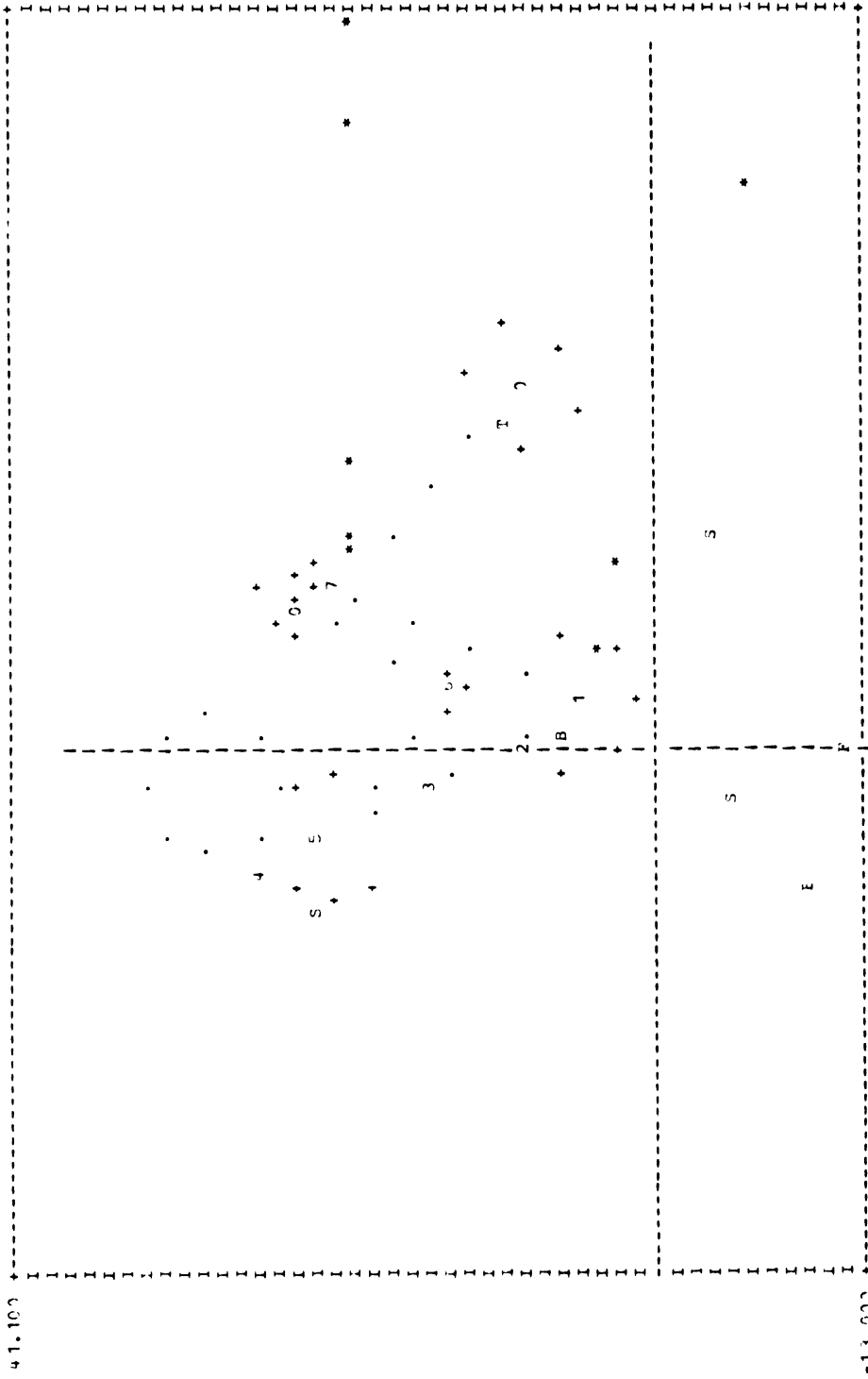
Table XXIV. Selected Printout. Example No. 2 (page 7 of 9)



INDICATED MEASUREMENTS ARE IN INCHES
 SCALING FACTORS: 1 TO 7.00 IN THE X DIRECTION
 1 TO 7.00 IN THE Y DIRECTION

Table XXIV. Selected Printout. Example No. 2 (page 8 of 9)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.200 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: X TO 7.00 IN THE X DIRECTION
 Y TO 7.00 IN THE Y DIRECTION

Table XXIV. Selected Printout. Example No. 2 (page 9 of 9)

Example No. 3. Unrestrained 5th Percentile Female Right Front Passenger in a 30 mph Frontal Impact.

This event has been modeled using the data in Table XXV. A complete description of the properties of a 5th percentile female were not available. Values were obtained by scaling the data describing the 50th percentile male down based on stature and weight for a 5th percentile female (105 lbs. and 5 ft. approximately). Joint range of motion and stiffness properties were not changed because of the lack of available data. Besides the usual seat cushion, seat back, toeboard, and floor, four other contact surfaces have been specified. These are the windshield (Surface 4) to indicate head contact, an upper instrument panel element (Surface 2) also to indicate head contact (Surface 7), and a knee-catching lower instrument panel (Surface 6).

The exaggerated extent of these surfaces as specified by the input data should be observed in the annotations to the stick figure section of the abbreviated program output included as Table XXVI. This procedure is based on the fact that each contact surface generates forces only on selected body elements. As an example, it does not matter how long the windshield (Surface 4) is or whether it intersects with the body. A force is generated only on the head. Surfaces 2, 6, and 7 also only produce forces on a single body segment (head, knee, and chest).

The philosophy behind this procedure is to ensure a successful program execution even though the input data is not highly refined. This is made necessary in many exercises, such as the present one, where one cannot predict with any accuracy the kinematics of the occupant. If surfaces are too short, body contact circles may slide unrealistically by their ends. In other words, it is usually better in beginning a series of exercises to have the occupant hit something rather than to fly off into space.

The kinematics of the occupant are interesting and the body loadings are severe. The small occupant is directed generally downward under the instrument panel. The head contacts the windshield and upper instrument panel, the chest the front panel, the knees the lower panel, while the legs are trapped under the panel. The buttocks rebound into the front of the seat cushion generating high loads and flexing the back to the rear. The head finally contacts the seat back.

SLIST DUTIM (143,208)

143	A1.	1.	1.	1.	1.	1.	1.158	1.058
144	B.9	.238	1.32	.192	.209	.268	1.158	
145	C960.	960.	960.	960.	960.	960.	960.	1.058
146	D3.83	4.92	10.76	6.59	9.88	9.2	14.1	13.78
147	E.03	.C1144	.068	.C246	.0181	.01606	.063	.0338
148	F3.76	0.	3.76	4.	1.25	2.	2.18	3.75
149	G2100.	20000.	20000.	20000.	5240.	7000.	7000.	20000.
150	H60.	15.	20.	20.	20000.	20000.	20000.	20000.
151	I150.	22.5	22.5	70.	195.	130.	120.	
152	J1.	1.	1.	1.	1.	1.	1.	
153	K2.35	2.73	4.42	4.16	4.12	6.42	6.42	8.67
154	L103.	103.	103.	75.	-77.	0.	6.	-40.
155	M0.	2.	0.	145.	6.14	6.	5.	1.
156	N1.	92.	.1	.34	37.21	5.31	1.57	15.
157	O12.1	13.5	16.8	2.55	50.	.0005	2.	1000.
158	P1.	.315	1.	50.	0.	625.	-12.	
159	P2.	.315	1.	77.	.5	350.		
160	P3.	.315	1.	-59.	.5	350.		
161	Q1.	.5	.078					
162	Q2.							
163	Q3.							
164	X1.	528.	528.	0.	.005	.2	5.	1.
165	S0.	45.	.5	.5	45.	-10.	.1	3.
166	T0.	0.	800.					
167	U9.			.95	-3.	-5.	.1	283.
168	S1.	28.	.01					
169	T1.	0.	800.					
170	U1.			.5	13.5	10.	.1	135.
171	S8.	36.	.5					
172	T8.	0.	800.					
173	U8.			.95	35.85	19.36	.1	15.
174	S2.	29.	.01					
175	T2.	0.	500.					
176	X2.	1500.	500.					
177	U2.							
178	U3.			.95	10.	30.	.1	144.
179	S4.	30.	.01	-4000.				
180	T4.	0.	4000.					
181	U4.							
182	U5.	20.	.01	.95	18.5	15.	.1	106.5
183	S6.	0.	1400.					
184	T6.	0.						
185	U6.							
186	X6.	2100.	1400.					
187	S7.	30.	.88	.12	15.	25.	.1	90.
188	T7.	0.	500.					
189	U7.							
190	X7.	1500.	500.					
191	U9.							
192	V1.	1.	0.	0.				
193	V1.	1.	.02	-5650.				
194	V1.	1.	.0547	-5650.				
195	V1.	1.	.0747	C.				
196	V1.	1.	2.	0.				
197	Z	2.3	1	0	0	0	0	
198	Z	7.5						
199	UFEEB I. P.							
200	UFEEB I. P..							

Table XXV. Data Set. Example No. 3 (page 1 of 2)

```

201      -2
202      -1.
203      -443
204      .275
205      .8
206      2 44 2 100 0 11 11 11
207      -30. 3 42.3 0 -13. 0 0 0 0 0 0
208      3 0 0 0 0 0 0 0 0 0
END OF FILE

```


CASH SIMULATION PROGRAM NUMBER ONE

NO.	M	L	RHU	F	THETA
1	0.49999997E-01	0.33999999E 01	0.23499994E 01	0.37599993E 01	0.10299998E 01
2	0.11499998E-01	0.49199991E 01	0.27299995E 01	0.0	0.10299998E 01
3	0.61999995E-01	0.11759993E 01	0.44399991E 01	0.37599993E 01	0.10299998E 01
4	0.24599999E-01	0.65999999E 01	0.41599998E 01	0.40000000E 01	0.74999996E 01
5	0.18099997E-01	0.98799992E 01	0.41199998E 01	0.12500000E 01	0.74999996E 01
6	0.16099998E-01	0.91999998E 01	0.64199999E 01	0.20000000E 01	0.59999998E 01
7	0.02599996E-01	0.14099999E 01	0.64199999E 01	0.21799994E 01	0.59999998E 01
8	0.33799998E-01	0.13799999E 01	0.86699991E 01	0.37500000E 01	0.39999998E 01

NO.	TRIME	ALPHA	OMEGA	K	CPRIME	XI
1	0.21000000E 05	0.59999993E 02	0.14999995E 03	0.96000000E 03	0.10000000E 01	0.10000000E 01
2	0.20000000E 05	-0.40000000E 05	0.12499995E 02	0.96000000E 03	0.10000000E 01	0.10000000E 01
3	0.20000000E 05	-0.40000000E 05	0.22499995E 02	0.96000000E 03	0.10000000E 01	0.10000000E 01
4	0.20000000E 05	-0.40000000E 05	0.69999995E 02	0.96000000E 03	0.10000000E 01	0.10000000E 01
5	0.52400000E 04	0.14999993E 02	0.19499998E 03	0.96000000E 03	0.10000000E 01	0.10000000E 01
6	0.70000000E 04	0.19999995E 02	0.12999995E 03	0.96000000E 03	0.10000000E 01	0.10000000E 01
7	0.70000000E 04	0.19999995E 02	0.11999995E 03	0.96000000E 03	0.10000000E 01	0.10000000E 01

R4= 0.20000000E 01, S4= 0.10000000E 04, DELTA T PRINT=0.005000, MU, PER PRINT INTERVAL= 0.100E 01, LCONTL= 1
 PSPRM2= 0.0, RHP= 0.20000000E 01, THATPS= 0.20000000E 05, M0= 0.14500000E 03, RHOP3= 0.61399994E 01
 RHOP4= 0.60000000E 01, PAID1= 50.00, CSE= 0.10000000E 01, S= 0.92000000E 02, XIS= 0.99999998E-01, MUS= 0.33999997E 00
 Z0= 0.15000000E 02, LF1= 0.12999999E 02, LF2= 0.13500000E 02, LP3= 0.16799998E 02, H= 0.16799998E 02, H= 0.25499992E 01
 GAMMA0= 5.00, VC= 0.52800000E 03, MEASR= 1, NDELTA= 0, DELTA T= 0.0005
 MAX TIME= 0.2000, MC= 0.50000000E 01

H	G	PHI	DELTA	BETA
1	0.31500000E 00	0.10000000E 01	0.0	0.37209991E 02
2	0.31500000E 00	0.10000000E 01	0.0	0.53099995E 01
3	0.31500000E 00	0.10000000E 01	0.0	0.15699997E 01

M	SIGMA	X	Y	MUA
1	0.62500000E 03	-0.12000000E 02	0.50000000E 02	0.77999994E-01
2	0.35000000E 03	0.0	0.0	0.0
3	0.35000000E 03	0.0	0.0	0.0

A	E	G	R	X	Y	MUA
1	0.45000000E 02	0.50000000E 00	0.50000000E 00	0.45000000E 02	-0.10000000E 02	0.0
2	0.28000000E 02	0.99955573E-02	0.94999999E 00	-0.30000000E 01	-0.50000000E 01	0.0
3	0.39000000E 02	0.99955573E-02	0.94999999E 00	0.35899991E 02	0.19359998E 02	0.0
4	0.0	0.0	0.0	0.0	0.0	0.0
5	0.30000000E 02	0.99955573E-02	0.94999999E 00	0.10000000E 02	0.30000000E 02	0.0
6	0.0	0.0	0.0	0.0	0.0	0.0
7	0.28000000E 02	0.99955573E-02	0.94999999E 00	0.18500000E 02	0.15000000E 02	0.0
8	0.30000000E 02	0.88000000E 00	0.11999999E 00	0.15000000E 02	0.25000000E 02	0.0
9	0.30000000E 02	0.50000000E 00	0.50000000E 00	0.18500000E 02	0.10000000E 02	0.0
10	0.0	0.0	0.0	0.0	0.0	0.0

NO.	XI	FSI
1	0.100	3.000
2	0.100	283.000
3	0.100	15.000

Table XVI. Selected Printout. Example No. 3 (page 2 of 12)

TIME (SEC.)	TWO DIMENSIONAL CRASH VICTIM SIMULATOR				OUTPUT DATA		7. 1972		PAGE 1	
	BELT FORCES (POUNDS)		BELT ANGLES (DEGREES)		RELATIVE HIP POSITION (INCHES)		RELATIVE HEAD POSITION (INCHES)			
	LAP	BELT	LAP	BELT	SHOULDER RESTRAINT UPPER	SHOULDER RESTRAINT LOWER	HORIZONTAL	VERTICAL	HORIZONTAL	VERTICAL
0.0	0.	0.	0.	0.	0.0	0.0	0.0	0.0	-3.31	23.03
0.005	0.	0.	0.	0.	0.0	0.0	0.41	0.04	-3.30	22.97
0.010	0.	0.	0.	0.	0.0	0.0	1.37	0.19	-3.24	22.86
0.015	0.	0.	0.	0.	0.0	0.0	2.54	0.45	-3.06	22.72
0.020	0.	0.	0.	0.	0.0	0.0	3.90	0.80	-2.71	22.57
0.025	0.	0.	0.	0.	0.0	0.0	5.47	1.24	-2.14	22.41
0.030	0.	0.	0.	0.	0.0	0.0	7.23	1.73	-1.35	22.22
0.035	0.	0.	0.	0.	0.0	0.0	9.03	2.09	-0.34	22.00
0.040	0.	0.	0.	0.	0.0	0.0	10.74	2.15	0.88	21.77
0.045	0.	0.	0.	0.	0.0	0.0	12.41	1.94	2.32	21.52
0.050	0.	0.	0.	0.	0.0	0.0	14.07	1.50	3.98	21.26
0.055	0.	0.	0.	0.	0.0	0.0	15.79	0.95	5.87	21.03
0.060	0.	0.	0.	0.	0.0	0.0	17.62	0.49	7.96	20.91
0.065	0.	0.	0.	0.	0.0	0.0	19.37	0.12	10.20	20.90
0.070	0.	0.	0.	0.	0.0	0.0	21.96	-0.22	12.55	20.90
0.075	0.	0.	0.	0.	0.0	0.0	22.59	-0.71	14.76	20.74
0.080	0.	0.	0.	0.	0.0	0.0	22.87	-1.45	16.60	20.31
0.085	0.	0.	0.	0.	0.0	0.0	23.08	-2.36	18.31	19.65
0.090	0.	0.	0.	0.	0.0	0.0	23.30	-3.25	19.90	18.77
0.095	0.	0.	0.	0.	0.0	0.0	23.55	-4.08	21.31	17.59
0.100	0.	0.	0.	0.	0.0	0.0	23.75	-4.83	22.24	16.29
0.105	0.	0.	0.	0.	0.0	0.0	23.79	-5.48	22.34	15.54
0.110	0.	0.	0.	0.	0.0	0.0	23.62	-6.10	21.34	15.35
0.115	0.	0.	0.	0.	0.0	0.0	23.33	-6.67	19.40	14.98
0.120	0.	0.	0.	0.	0.0	0.0	22.93	-7.16	17.11	14.31
0.125	0.	0.	0.	0.	0.0	0.0	22.39	-7.59	14.78	13.73
0.130	0.	0.	0.	0.	0.0	0.0	21.63	-7.90	12.60	13.25
0.135	0.	0.	0.	0.	0.0	0.0	20.73	-7.98	10.77	12.52
0.140	0.	0.	0.	0.	0.0	0.0	19.82	-7.86	9.12	11.68
0.145	0.	0.	0.	0.	0.0	0.0	18.84	-7.62	7.37	11.24
0.150	0.	0.	0.	0.	0.0	0.0	17.80	-7.33	5.54	10.94
0.155	0.	0.	0.	0.	0.0	0.0	16.69	-7.10	3.69	10.60
0.160	0.	0.	0.	0.	0.0	0.0	15.56	-6.94	1.83	10.19
0.165	0.	0.	0.	0.	0.0	0.0	14.37	-6.84	-0.06	9.74
0.170	0.	0.	0.	0.	0.0	0.0	13.13	-6.71	-1.99	9.27
0.175	0.	0.	0.	0.	0.0	0.0	11.92	-6.43	-3.74	9.01
0.180	0.	0.	0.	0.	0.0	0.0	9.85	-6.00	-4.22	9.09
0.185	0.	0.	0.	0.	0.0	0.0	8.55	-5.45	-3.64	8.86
0.190	0.	0.	0.	0.	0.0	0.0	7.37	-4.99	-3.98	8.26
0.195	0.	0.	0.	0.	0.0	0.0	6.28	-4.54	-4.49	10.27
0.200	0.	0.	0.	0.	0.0	0.0	0.0	-4.08	-4.59	11.61

Table XVI. Selected Printout. Example No. 3 (page 3 of 12)

3-D DIMENSIONAL LEAD VEHICLE SIMULATOR OUTPUT DATA (DEGREES)

TIME	LOWER TURRET POSITION VELOCITY	LOWER TURRET ACCEL.	UPPER TURRET POSITION VELOCITY	UPPER TURRET ACCEL.	VEHICLE N VELOCITY	VEHICLE N ACCEL.
0.0	103.00	0.1817E 06	103.00	0.1432E 05	75.00	0.2648E 06
0.050	105.17	793.93	103.00	0.1432E 05	75.00	0.5490E 06
0.100	108.24	0.2389E 05	103.00	0.1432E 05	75.00	0.5272E 06
0.150	115.71	1202.98	104.04	0.1432E 05	76.11	0.5784E 06
0.200	121.39	0.2175E 05	104.04	0.1432E 05	76.11	0.5784E 06
0.250	130.57	0.1906E 05	106.86	0.1432E 05	76.11	0.4424E 06
0.300	1392.64	0.1499E 05	106.86	0.1432E 05	76.11	0.4424E 06
0.350	1427.08	0.3086E 05	108.75	0.1432E 05	76.11	0.1954E 05
0.400	1031.33	0.5579E 05	111.26	0.1432E 05	75.47	0.1619E 05
0.450	571.11	0.8735E 05	113.78	0.1432E 05	75.92	0.2561E 05
0.500	147.33	0.7353E 05	116.10	0.1432E 05	76.54	0.3413E 05
0.550	295.80	0.1031E 06	117.96	0.1432E 05	78.10	0.3088E 05
0.600	717.30	0.2590E 05	118.65	0.1432E 05	80.31	0.1002E 05
0.650	141.65	0.8519E 05	118.65	0.1432E 05	82.44	0.6298E 06
0.700	190.84	0.1534E 06	116.84	0.1432E 05	84.48	0.1004E 04
0.750	595.34	0.5488E 04	112.57	0.1432E 05	86.35	0.1143E 06
0.800	6.57	0.1160E 06	105.97	0.1432E 05	86.64	0.6288E 05
0.850	142.89	0.1117E 06	100.24	0.1432E 05	85.14	0.1862E 06
0.900	700.40	0.3014E 04	95.77	0.1432E 05	79.27	0.1486E 06
0.950	537.28	0.1341E 06	92.63	0.1432E 05	69.25	0.8959E 05
1.000	134.76	0.1524E 06	90.82	0.1432E 05	56.92	0.1177E 06
0.050	724.46	0.4242E 05	89.04	0.1432E 05	47.42	0.6037E 06
0.100	660.44	0.3218E 05	86.20	0.1432E 05	51.64	0.6156E 06
0.150	265.10	0.8335E 05	83.76	0.1432E 05	70.69	0.1523E 06
0.200	82.43	0.5121E 05	83.98	0.1432E 05	94.67	0.2607E 06
0.250	316.21	0.4471E 05	88.41	0.1432E 05	113.12	0.4725E 06
0.300	442.58	0.5364E 05	97.67	0.1432E 05	120.27	0.4914E 06
0.350	848.68	0.6476E 05	110.72	0.1432E 05	115.62	0.2430E 06
0.400	1159.21	0.5047E 05	124.86	0.1432E 05	104.86	0.1349E 06
0.450	867.46	0.7923E 05	135.65	0.1432E 05	96.82	0.3116E 06
0.500	531.26	0.5856E 05	140.68	0.1432E 05	95.76	0.6218E 05
0.550	80.57	0.1711E 06	143.26	0.1432E 05	98.21	0.6408E 05
0.600	573.37	0.6810E 05	144.69	0.1432E 05	102.22	0.4317E 05
0.650	468.65	0.6423E 05	145.59	0.1432E 05	107.30	0.2336E 04
0.700	365.60	0.1855E 05	149.19	0.1432E 05	112.50	0.5648E 04
0.750	553.39	0.5230E 05	152.69	0.1432E 05	115.72	0.8976E 06
0.800	778.58	0.2931E 05	157.03	0.1432E 05	117.28	0.1888E 06
0.850	916.45	0.3139E 05	159.41	0.1432E 05	115.72	0.8976E 06
0.900	1052.46	0.2214E 05	141.34	0.1432E 05	43.88	0.1773E 06
0.950	1145.65	0.1521E 05	130.98	0.1432E 05	39.02	0.1548E 06
1.000	1145.65	0.1521E 05	130.98	0.1432E 05	38.21	0.2215E 06

Table XVI. Selected Printout. Example No. 3 (page 4 of 12)

1-D DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
 ECDY SEGMENT ANGULAR ORIENTATION (DEGREES)

TIME	UPPER ARM			LOWER ARM			POSITION VELOCITY			ACCEL.			UPPER LEG			LOWER LEG			ACCEL.		
	POSITION VELOCITY	UPPER VELOCITY	C.C.	POSITION VELOCITY	UPPER VELOCITY	C.C.	POSITION VELOCITY	UPPER VELOCITY	C.C.	POSITION VELOCITY	UPPER VELOCITY	C.C.	POSITION VELOCITY	UPPER VELOCITY	C.C.	POSITION VELOCITY	UPPER VELOCITY	C.C.	POSITION VELOCITY	UPPER VELOCITY	C.C.
0.0	-77.00	34.18	0.1300E 05	0.0	0.0	0.3306E 05	6.00	0.0	0.0	0.3438E 06	-40.00	0.0	-0.3603E 06	-40.00	0.0	0.0	0.0	-40.00	0.0	0.0	-0.3603E 06
0.0050	-77.14	51.11	-0.5353E 04	0.35	121.36	0.1018E 05	9.70	1268.11	0.0	0.9676E 05	43.78	0.0	-0.5191E 05	43.78	0.0	0.0	0.0	-43.78	0.0	0.0	-0.5191E 05
0.0100	-77.43	59.16	0.1300E 04	1.02	133.82	-0.2671E 04	16.52	1334.77	0.0	0.3566E 05	-50.14	0.0	-0.3568E 05	-50.14	0.0	0.0	0.0	-50.14	0.0	0.0	-0.3568E 05
0.0150	-77.71	50.55	0.2210E 04	1.65	118.64	-0.3497E 04	22.76	1165.64	0.0	0.3154E 05	-55.73	0.0	0.3132E 05	-55.73	0.0	0.0	0.0	-55.73	0.0	0.0	0.3132E 05
0.0200	-77.93	-37.55	0.3043E 04	2.20	99.29	-0.4285E 04	28.21	1017.23	0.0	0.2747E 05	-64.62	0.0	0.2649E 05	-64.62	0.0	0.0	0.0	-64.62	0.0	0.0	0.2649E 05
0.0250	-78.08	-20.75	0.3710E 04	2.64	76.72	-0.4659E 04	32.96	888.42	0.0	0.2373E 05	-70.99	0.0	0.8884E 05	-70.99	0.0	0.0	0.0	-70.99	0.0	0.0	0.8884E 05
0.0300	-78.13	3.05	0.6813E 04	2.96	45.94	-0.7498E 04	37.17	830.07	0.0	0.2830E 05	-69.26	0.0	0.1569E 06	-69.26	0.0	0.0	0.0	-69.26	0.0	0.0	0.1569E 06
0.0350	-78.03	34.18	0.6114E 04	3.14	35.11	-0.2591E 03	41.99	150.94	0.0	0.8813E 05	-67.50	0.0	0.8461E 06	-67.50	0.0	0.0	0.0	-67.50	0.0	0.0	0.8461E 06
0.0400	-77.78	65.59	0.6215E 04	3.32	34.47	0.4269E 03	48.77	1540.92	0.0	0.6434E 05	-67.26	0.0	0.1723E 06	-67.26	0.0	0.0	0.0	-67.26	0.0	0.0	0.1723E 06
0.0450	-77.38	94.99	0.6634E 04	3.51	41.57	0.1271E 04	57.25	1348.73	0.0	0.6095E 05	-70.57	0.0	0.1327E 06	-70.57	0.0	0.0	0.0	-70.57	0.0	0.0	0.1327E 06
0.0500	-76.81	141.40	0.1723E 05	3.72	38.22	-0.6258E 04	67.32	2204.05	0.0	0.9248E 05	-71.12	0.0	0.2885E 06	-71.12	0.0	0.0	0.0	-71.12	0.0	0.0	0.2885E 06
0.0550	-75.81	268.67	0.2838E 05	3.73	-54.91	-0.3616E 05	79.55	2648.91	0.0	0.2008E 05	-68.37	0.0	0.1969E 06	-68.37	0.0	0.0	0.0	-68.37	0.0	0.0	0.1969E 06
0.0600	-74.05	447.49	0.3915E 05	2.94	-262.84	-0.3670E 05	92.62	2496.42	0.0	0.9731E 05	-53.82	0.0	0.1842E 06	-53.82	0.0	0.0	0.0	-53.82	0.0	0.0	0.1842E 06
0.0650	-71.37	621.79	0.5299E 05	1.32	-358.62	-0.9283E 04	103.62	1850.29	0.0	0.1842E 06	-47.35	0.0	0.3301E 06	-47.35	0.0	0.0	0.0	-47.35	0.0	0.0	0.3301E 06
0.0700	-67.30	1080.08	0.1388E 06	-0.54	-390.24	-0.1580E 05	110.28	782.40	0.0	0.2219E 06	-48.02	0.0	0.1696E 06	-48.02	0.0	0.0	0.0	-48.02	0.0	0.0	0.1696E 06
0.0750	-60.03	1808.95	0.1194E 06	-2.79	-503.70	-0.3324E 05	111.88	-68.38	0.0	0.1441E 06	-52.80	0.0	0.1355E 06	-52.80	0.0	0.0	0.0	-52.80	0.0	0.0	0.1355E 06
0.0800	-49.66	2318.07	0.8691E 05	-5.88	-752.25	-0.5369E 05	109.77	-760.46	0.0	0.1242E 06	-57.17	0.0	0.2078E 05	-57.17	0.0	0.0	0.0	-57.17	0.0	0.0	0.2078E 05
0.0850	-37.22	2532.03	0.3933E 04	-10.22	-924.71	0.1990E 05	105.30	-966.81	0.0	0.2512E 05	-60.48	0.0	0.1698E 06	-60.48	0.0	0.0	0.0	-60.48	0.0	0.0	0.1698E 06
0.0900	-25.15	1815.52	0.4696E 06	-13.22	363.45	0.7529E 06	100.87	-636.28	0.0	0.1341E 06	-59.66	0.0	0.1781E 06	-59.66	0.0	0.0	0.0	-59.66	0.0	0.0	0.1781E 06
0.0950	-19.42	310.00	0.1088E 06	-3.76	2124.48	0.2109E 06	99.65	167.75	0.0	0.1524E 06	-51.48	0.0	0.7289E 05	-51.48	0.0	0.0	0.0	-51.48	0.0	0.0	0.7289E 05
0.1000	-16.61	353.94	0.5753E 05	7.26	3011.55	0.1226E 06	102.10	725.46	0.0	0.4242E 05	-47.44	0.0	0.8588E 05	-47.44	0.0	0.0	0.0	-47.44	0.0	0.0	0.8588E 05
0.1050	-15.38	155.60	0.2997E 05	23.49	3406.65	0.3295E 05	105.74	635.37	0.0	0.6317E 05	-42.20	0.0	0.1678E 06	-42.20	0.0	0.0	0.0	-42.20	0.0	0.0	0.1678E 06
0.1100	-14.87	66.45	0.9596E 04	40.56	3335.72	-0.7084E 05	108.06	266.10	0.0	0.8335E 05	-40.82	0.0	0.6051E 05	-40.82	0.0	0.0	0.0	-40.82	0.0	0.0	0.6051E 05
0.1150	-14.50	111.66	0.1782E 05	56.06	2809.71	-0.1369E 06	108.45	-81.43	0.0	0.5121E 05	-41.35	0.0	0.1254E 05	-41.35	0.0	0.0	0.0	-41.35	0.0	0.0	0.1254E 05
0.1200	-13.68	220.43	0.2561E 05	68.32	2093.93	-0.1376E 06	107.44	-315.21	0.0	0.4471E 05	-42.24	0.0	0.2267E 05	-42.24	0.0	0.0	0.0	-42.24	0.0	0.0	0.2267E 05
0.1250	-12.22	370.17	0.3512E 05	77.22	1504.88	-0.8675E 05	105.28	-554.58	0.0	0.5364E 05	-43.68	0.0	0.2981E 05	-43.68	0.0	0.0	0.0	-43.68	0.0	0.0	0.2981E 05
0.1300	-9.93	344.53	0.3118E 05	83.95	1257.07	-0.9017E 04	101.80	-847.60	0.0	0.6476E 05	-45.80	0.0	0.7590E 04	-45.80	0.0	0.0	0.0	-45.80	0.0	0.0	0.7590E 04
0.1350	-6.96	501.71	0.2051E 05	93.27	1298.38	0.1958E 05	96.75	-1158.21	0.0	0.5047E 05	-48.11	0.0	0.2384E 05	-48.11	0.0	0.0	0.0	-48.11	0.0	0.0	0.2384E 05
0.1400	-4.49	327.56	0.8307E 05	56.88	1306.09	-0.2431E 05	90.60	-1249.05	0.0	0.4931E 05	-49.82	0.0	0.8411E 05	-49.82	0.0	0.0	0.0	-49.82	0.0	0.0	0.8411E 05
0.1450	-3.66	74.08	0.2293E 05	103.25	1243.55	-0.1913E 05	84.28	-1224.94	0.0	0.4923E 05	-49.64	0.0	0.1074E 06	-49.64	0.0	0.0	0.0	-49.64	0.0	0.0	0.1074E 06
0.1500	-2.98	202.03	0.2555E 05	114.68	1022.64	-0.3202E 05	78.93	-886.46	0.0	0.7923E 05	-46.87	0.0	0.6127E 05	-46.87	0.0	0.0	0.0	-46.87	0.0	0.0	0.6127E 05
0.1550	-1.65	308.45	0.1333E 05	119.33	821.72	-0.4937E 05	73.22	-397.54	0.0	0.2611E 04	-42.78	0.0	0.8930E 05	-42.78	0.0	0.0	0.0	-42.78	0.0	0.0	0.8930E 05
0.1600	-0.05	321.92	-0.1477E 05	119.33	548.18	0.5834E 05	71.19	-422.63	0.0	0.8840E 04	-40.50	0.0	0.9885E 05	-40.50	0.0	0.0	0.0	-40.50	0.0	0.0	0.9885E 05
0.1650	1.35	242.11	-0.1282E 05	124.77	97.39	-0.1076E 06	68.67	-684.29	0.0	0.6264E 05	-40.42	0.0	0.1230E 05	-40.42	0.0	0.0	0.0	-40.42	0.0	0.0	0.1230E 05
0.1700	2.18	14.50	-0.6150E 05	124.57	-348.39	-0.7110E 05	64.73	-845.65	0.0	0.1315E 05	-40.37	0.0	0.1079E 05	-40.37	0.0	0.0	0.0	-40.37	0.0	0.0	0.1079E 05
0.1750	1.72	-156.72	-0.1638E 05	123.87	-656.73	-0.4934E 05	60.31	-929.90	0.0	0.2007E 05	-40.06	0.0	0.8014E 04	-40.06	0.0	0.0	0.0	-40.06	0.0	0.0	0.8014E 04
0.1800	0.52	-401.01	-0.1107E 06	121.31	-656.73	-0.4934E 05	60.31	-929.90	0.0	0.2007E 05	-40.06	0.0	0.1980E 05	-40.06	0.0	0.0	0.0	-40.06	0.0	0.0	0.1980E 05
0.1850	-3.10	-1029.19	-0.6940E 05	117.64	-742.56	0.2710E 05	55.62	-875.89	0.0	0.5671E 05	-39.50	0.0	0.5154E 04	-39.50	0.0	0.0	0.0	-39.50	0.0	0.0	0.5154E 04
0.1900	-8.51	-1081.66	-0.1200E 05	114.43	-562.40	0.1324E 05	51.93	-673.33	0.0	0.7145E 04	-38.52	0.0	0.5648E 04	-38.52	0.0	0.0	0.0	-38.52	0.0	0.0	0.5648E 04
0.1950	-14.17	-1207.69	-0.4086E 05	111.95	-411.74	0.3825E 05	48.53	-677.28	0.0	0.5698E 04	-37.35	0.0	0.5648E 04	-37.35	0.0	0.0	0.0	-37.35	0.0	0.0	0.5648E 04
0.2000	-20.80	-1456.39	-0.5329E 05	110.35	-244.76	-0.2754E 03	45.24	-635.12	0.0	0.1010E 05	-36.04	0.0	0.5648E 04	-36.04	0.0	0.0	0.0	-36.04	0.0	0.0	0.5648E 04

Table XVI. Selected Printout. Example No. 3 (page 5 of 12)

TIME	POSITION (IN.)	VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)	RELATIVE DISPL. (IN.)	HORIZONTAL VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)	RELATIVE DISPL. (IN.)	VERTICAL VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)
0.0	0.0	528.00	0.0	0.0	528.00	89.875	0.0	0.0	6.041
0.0050	2.630	521.97	-6.244	0.408	675.12	49.403	0.036	17.24	13.322
0.0100	5.200	503.88	-12.487	1.372	721.67	3.915	0.187	10.628	10.628
0.0150	7.649	473.72	-18.731	2.544	725.74	0.177	0.445	9.839	9.839
0.0200	9.917	431.50	-24.974	3.902	723.70	-2.368	0.800	79.57	8.455
0.0250	11.954	383.25	-24.974	5.469	717.51	-4.110	1.237	94.53	6.848
0.0300	13.749	335.07	-24.974	7.233	700.29	-24.314	1.731	96.55	-16.670
0.0350	15.304	286.75	-24.974	9.027	635.60	-34.185	2.094	42.32	-33.049
0.0400	16.617	238.57	-24.974	10.736	575.21	-28.087	2.151	-17.72	-28.050
0.0450	17.689	190.25	-24.974	12.411	524.35	-26.357	1.935	-66.94	-22.968
0.0500	18.519	142.00	-24.974	14.074	474.64	-19.816	1.499	-104.43	-11.984
0.0550	19.109	93.77	-24.600	15.792	452.77	-11.701	0.952	-106.16	14.199
0.0600	19.469	52.28	-18.356	17.618	415.72	-32.839	0.463	-90.94	8.712
0.0650	19.651	22.84	-12.113	19.369	359.67	-40.958	0.124	-65.09	1.618
0.0700	19.717	5.47	-5.863	20.866	263.48	-49.262	-0.222	-77.27	-12.113
0.0750	19.726	0.14	0.0	21.962	176.79	-50.676	-0.704	-123.23	-27.759
0.0800	19.727	0.14	0.0	22.532	75.12	-53.322	-1.454	-174.61	-24.737
0.0850	19.728	0.14	0.0	22.871	46.19	-8.870	-2.355	-180.51	0.835
0.0900	19.728	0.14	0.0	23.080	42.41	-0.248	-3.250	-175.47	10.003
0.0950	19.729	0.14	0.0	23.300	47.51	3.809	-4.084	-158.35	10.029
0.1000	19.730	0.14	0.0	23.546	49.19	-3.728	-4.827	-138.75	9.455
0.1050	19.731	0.14	0.0	23.752	27.42	-20.845	-5.482	-125.87	3.376
0.1100	19.731	0.14	0.0	23.787	-14.37	-23.192	-6.098	-119.91	3.152
0.1150	19.732	0.14	0.0	23.622	-46.95	-12.525	-6.666	-105.13	7.270
0.1200	19.733	0.14	0.0	23.331	-68.42	-10.529	-7.161	-93.54	6.100
0.1250	19.733	0.14	0.0	22.934	-91.44	-14.810	-7.593	-76.68	13.269
0.1300	19.734	0.14	0.0	22.391	-128.29	-24.043	-7.895	-41.15	24.440
0.1350	19.735	0.14	0.0	21.633	-173.26	-19.249	-7.980	6.92	21.712
0.1400	19.736	0.14	0.0	20.727	-177.77	12.003	-7.860	36.61	9.572
0.1450	19.736	0.14	0.0	19.815	-189.16	-4.039	-7.622	56.56	4.047
0.1500	19.737	0.14	0.0	18.844	-199.88	-7.515	-7.334	55.33	-6.168
0.1550	19.738	0.14	0.0	17.804	-216.35	-8.886	-7.096	38.59	-9.469
0.1600	19.739	0.14	0.0	16.686	-227.57	0.639	-6.941	24.42	-5.437
0.1650	19.739	0.14	0.0	15.557	-224.68	0.008	-6.838	19.62	0.225
0.1700	19.740	0.14	0.0	14.372	-268.77	-32.012	-6.714	39.44	18.880
0.1750	19.741	0.14	0.0	12.921	-302.65	-6.437	-6.433	71.68	15.291
0.1800	19.741	0.14	0.0	11.381	-312.18	-2.586	-5.998	102.60	15.214
0.1850	19.742	0.14	0.0	9.847	-289.08	30.970	-5.445	106.55	-16.174
0.1900	19.743	0.14	0.0	8.546	-242.39	5.122	-4.993	85.27	6.061
0.1950	19.744	0.14	0.0	7.366	-227.84	9.883	-4.545	92.22	0.997
0.2000	19.744	0.14	0.0	6.276	-207.27	10.806	-4.083	91.67	-1.321

Table XVI. Selected Printout. Example No. 3 (page 6 of 12)

OUTPUT DATA
BELT FORCES (LBS),

TWO DIMENSIONAL CRASH VICTIM SIMULATOR
ACCELEROMETER READINGS

HEAD
RESULTANT
(G-UNITS)

TIME

TIME	HEAD RESULTANT (G-UNITS)	ANGLE (DEG.)	CEEST RESULTANT (G-UNITS)	ANGLE (DEG.)	LAP	SHOULDER LOWER	UPPER	AT HIP	AT FRONT EDGE
0.0	12.3	-111.9	15.7	-38.4	0.0	0.0	0.0	145.00	60.58
0.0050	5.2	-105.2	6.6	-31.9	0.0	0.0	0.0	141.13	0.0
0.0100	1.6	-81.9	1.7	-8.8	0.0	0.0	0.0	119.82	0.0
0.0150	1.3	-88.0	2.4	-0.0	0.0	0.0	0.0	96.74	0.0
0.0200	2.2	-99.2	2.3	6.4	0.0	0.0	0.0	72.65	0.0
0.0250	2.4	-117.1	3.2	11.2	0.0	0.0	0.0	47.76	0.0
0.0300	4.5	-109.1	7.5	29.5	0.0	0.0	0.0	31.03	0.0
0.0350	4.8	-159.9	1.5	-96.1	0.0	0.0	0.0	72.18	0.0
0.0400	6.0	-174.5	2.6	-112.4	0.0	0.0	0.0	136.50	0.0
0.0450	7.1	-177.6	4.6	-120.7	0.0	0.0	0.0	204.77	0.0
0.0500	7.2	-149.2	12.4	-155.0	0.0	0.0	0.0	268.18	0.0
0.0550	10.2	-101.1	15.0	-155.7	0.0	0.0	0.0	0.0	0.0
0.0600	12.3	95.5	23.3	-176.5	0.0	0.0	0.0	0.0	0.0
0.0650	1.7	165.9	33.7	-159.8	0.0	0.0	0.0	0.0	0.0
0.0700	18.2	-66.1	80.0	-163.1	0.0	0.0	0.0	0.0	0.0
0.0750	46.5	-137.0	33.6	-159.2	0.0	0.0	0.0	0.0	0.0
0.0800	31.5	-60.3	30.3	-164.4	0.0	0.0	0.0	0.0	0.0
0.0850	35.4	-76.3	13.9	-169.0	0.0	0.0	0.0	0.0	0.0
0.0900	45.7	-100.4	7.3	-147.3	0.0	0.0	0.0	0.0	0.0
0.0950	78.3	-162.8	26.5	-153.8	0.0	0.0	0.0	0.0	0.0
0.1000	202.8	140.9	27.2	-167.4	0.0	0.0	0.0	0.0	0.0
0.1050	228.4	151.0	12.4	-87.0	0.0	0.0	0.0	0.0	0.0
0.1100	161.1	-152.6	23.2	88.1	0.0	0.0	0.0	0.0	0.0
0.1150	88.1	-81.8	25.6	127.5	0.0	0.0	0.0	0.0	0.0
0.1200	75.3	20.1	23.3	143.3	0.0	0.0	0.0	0.0	0.0
0.1250	95.7	33.5	15.7	134.3	0.0	0.0	0.0	0.0	0.0
0.1300	79.6	-18.5	17.3	126.2	0.0	0.0	0.0	0.0	0.0
0.1350	36.0	-85.1	23.5	154.0	0.0	0.0	0.0	0.0	0.0
0.1400	79.5	138.8	46.4	-178.3	0.0	0.0	0.0	0.0	0.0
0.1450	11.7	-162.0	15.0	-108.5	0.0	0.0	0.0	0.0	0.0
0.1500	13.0	-144.7	15.6	-93.5	0.0	0.0	0.0	0.0	0.0
0.1550	12.4	-125.7	8.7	-84.3	0.0	0.0	0.0	0.0	0.0
0.1600	8.7	-103.6	13.4	71.6	0.0	0.0	0.0	0.0	0.0
0.1650	6.5	-92.7	4.1	125.6	0.0	0.0	0.0	0.0	0.0
0.1700	42.9	44.4	37.2	126.6	0.0	0.0	0.0	836.41	590.57
0.1750	290.7	20.5	13.3	125.8	0.0	0.0	0.0	703.69	307.39
0.1800	281.8	-31.8	15.6	134.9	0.0	0.0	0.0	552.57	88.55
0.1850	332.5	167.7	26.7	-58.7	0.0	0.0	0.0	437.64	0.0
0.1900	43.2	99.1	23.3	18.0	0.0	0.0	0.0	374.09	0.0
0.1950	61.1	61.0	34.5	22.7	0.0	0.0	0.0	302.30	0.0
0.2000	68.7	68.7	43.4	25.9	0.0	0.0	0.0	249.64	0.0

Table XVI. Selected Printout. Example No. 3 (page 7 of 12)

TIME	FOOT		KNEE		LOWER LEG		TOE BOARD		UPPER TORSO		HEAD	
	UN	FLICR	CM	CM	CM	CM	CM	CM	UN	ON	ON	ON
0.0	54.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0050	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0150	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0250	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0300	0.0	0.0	1121.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0350	0.0	0.0	2100.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0400	0.0	0.0	2100.0	0.0	1204.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0450	0.0	0.0	2100.0	0.0	1839.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0500	0.0	0.0	1675.4	0.0	887.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0550	0.0	0.0	240.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0600	0.0	0.0	0.0	0.0	148.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0650	0.0	0.0	0.0	0.0	1168.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0700	0.0	0.0	0.0	0.0	1902.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0750	0.0	0.0	0.0	0.0	1673.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0800	0.0	0.0	0.0	0.0	470.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0850	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0900	0.0	0.0	1341.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0950	0.0	0.0	1720.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1000	0.0	0.0	908.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1050	0.0	0.0	0.0	0.0	345.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1100	0.0	0.0	0.0	0.0	619.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1150	0.0	0.0	0.0	0.0	188.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1250	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1300	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1350	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1450	0.0	0.0	733.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1500	0.0	0.0	1215.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1550	0.0	0.0	959.9	0.0	79.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1600	0.0	0.0	155.6	0.0	534.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1650	0.0	0.0	0.0	0.0	522.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1700	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1750	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1800	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1850	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1900	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1950	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.2000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

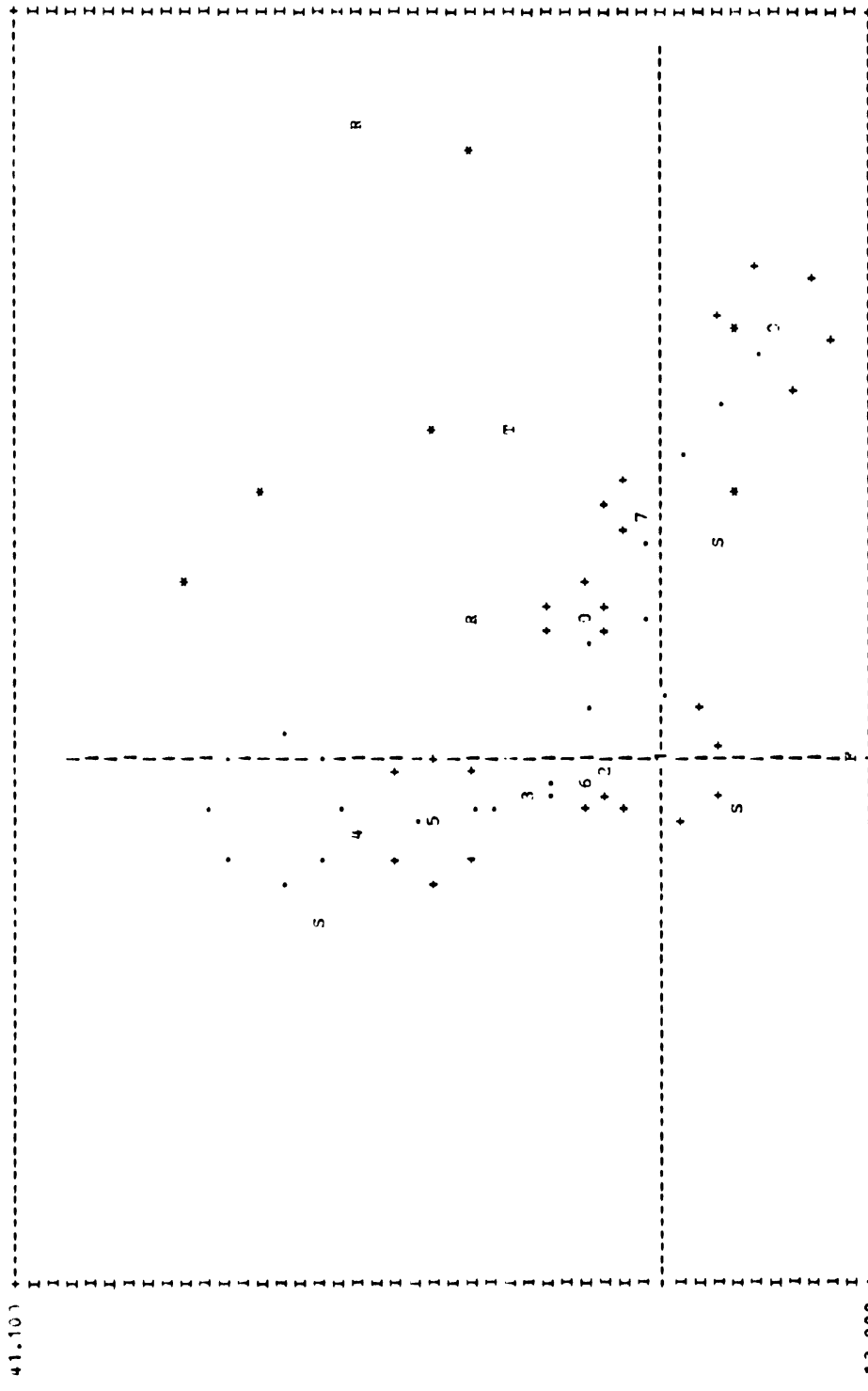
Table XVI. Selected Printout. Example No. 3 (page 8 of 12)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
CONTACT FORCES (LBS.)

TIME	HEAD ON SEAT BACK	UPPER ICERSJ CA SEAT BACK
0.0	0.0	C.C
0.0050	0.0	C.C
0.0100	0.0	C.C
0.0150	0.0	C.C
0.0200	0.0	C.C
0.0250	0.0	C.C
0.0300	0.0	C.C
0.0350	0.0	C.C
0.0400	0.0	C.C
0.0450	0.0	C.C
0.0500	0.0	C.C
0.0550	0.0	C.C
0.0600	0.0	C.C
0.0650	0.0	C.C
0.0700	0.0	C.C
0.0750	0.0	C.C
0.0800	0.0	C.C
0.0850	0.0	C.C
0.0900	0.0	C.C
0.0950	0.0	C.C
0.1000	0.0	C.C
0.1050	0.0	C.C
0.1100	0.0	C.C
0.1150	0.0	C.C
0.1200	0.0	C.C
0.1250	0.0	C.C
0.1300	0.0	C.C
0.1350	0.0	C.C
0.1400	0.0	C.C
0.1450	0.0	C.C
0.1500	0.0	C.C
0.1550	0.0	C.C
0.1600	0.0	C.C
0.1650	0.0	C.C
0.1700	208.1	C.C
0.1750	1583.8	C.C
0.1800	1345.5	C.C
0.1850	121.5	282.1
0.1900	113.0	1339.4
0.1950	271.2	2118.9
0.2000	100.1	2537.8

Table XXVI. Selected Printout. Example No. 3 (page 9 of 12)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.0 SECONDS

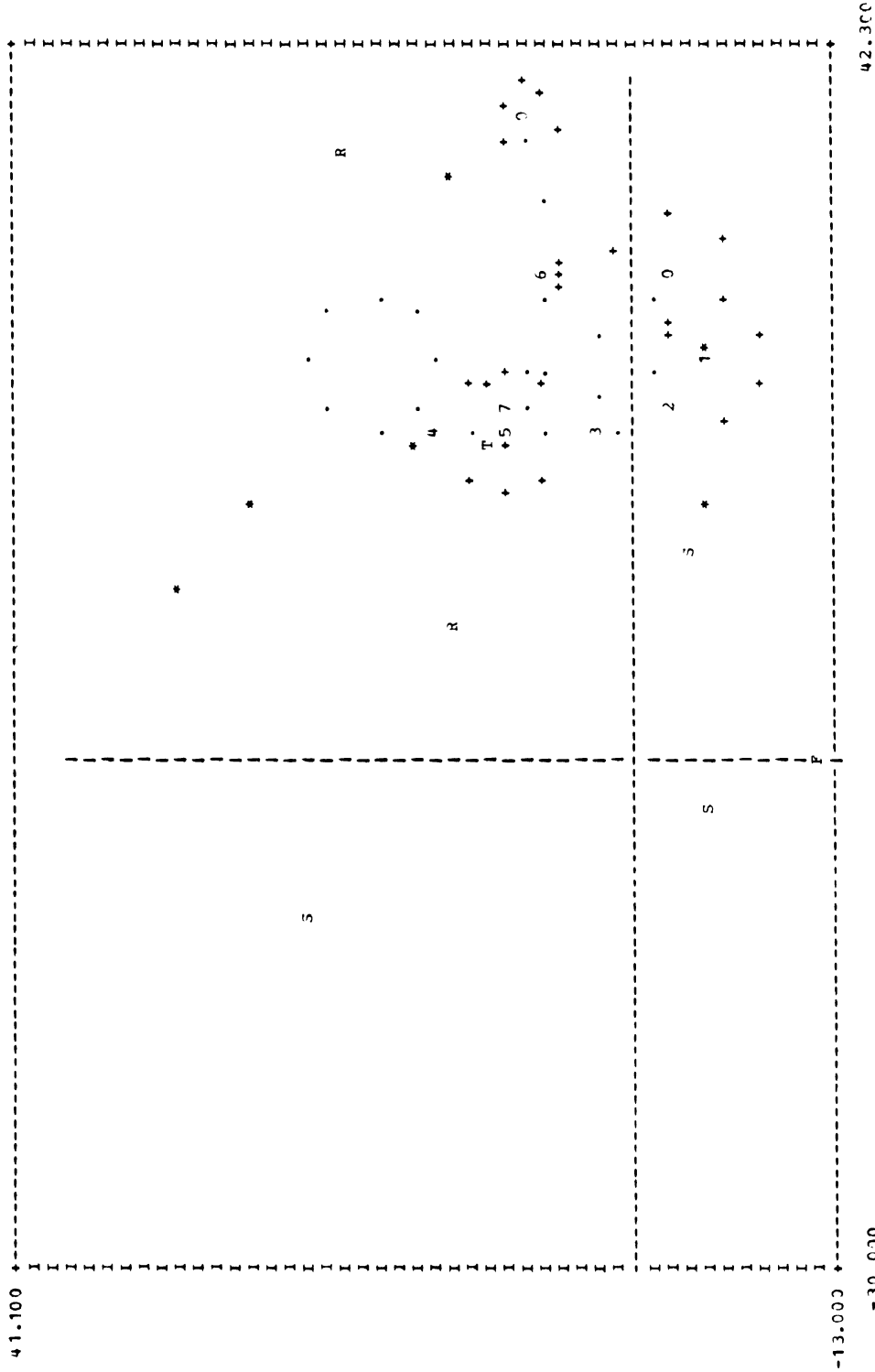


42.300

-30.000

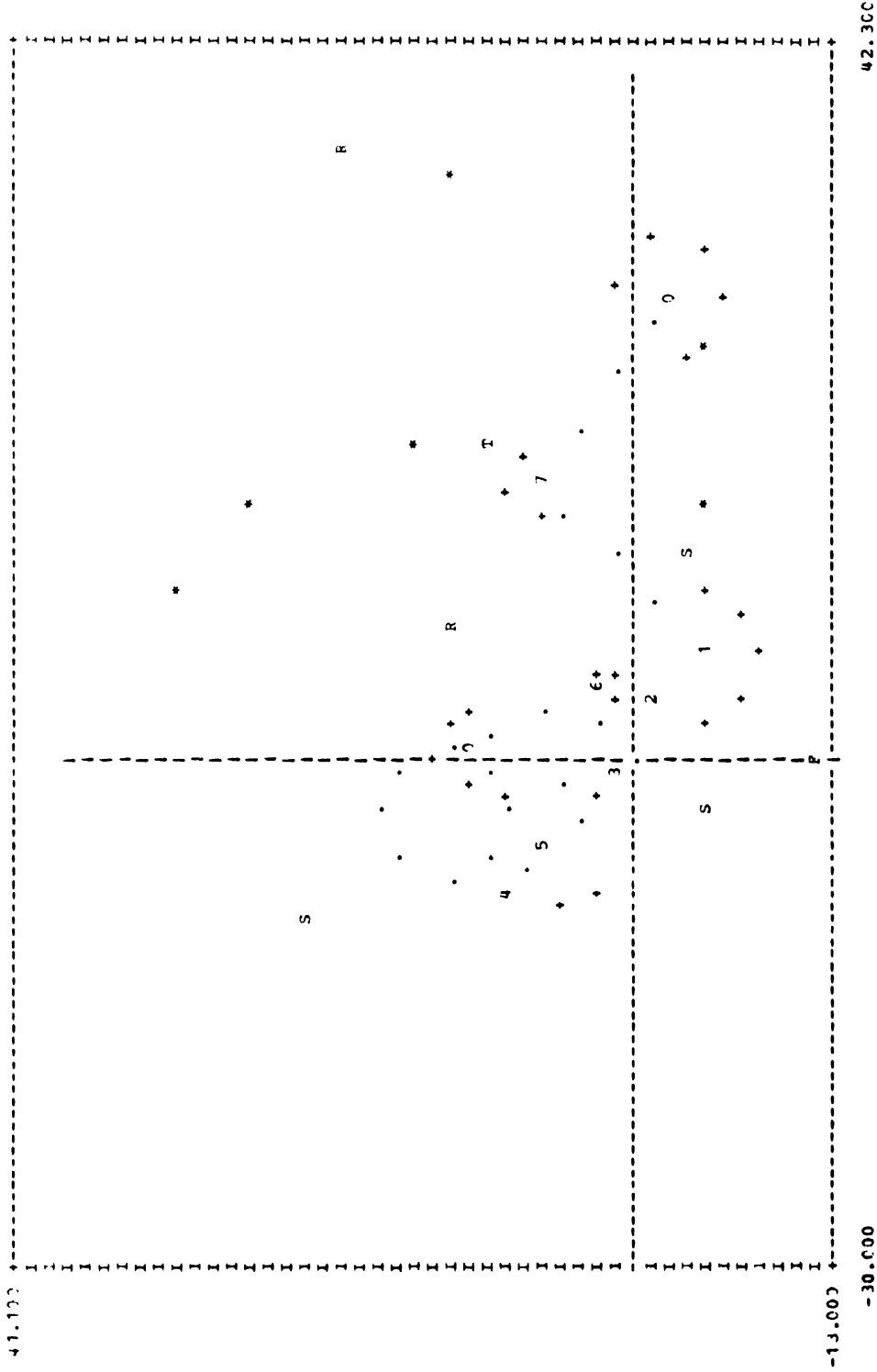
INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

Table XVI. Selected Printout. Example No. 3 (page 10 of 12)



INDICATED MEASUREMENTS ARE IN INCHES
 SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
 1 TO 7.06 IN THE Y DIRECTION

Table XXVI. Selected Printout. Example No. 3 (page 11 of 12)



INDICATED MEASUREMENTS ARE IN INCHES
 SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
 SCALING FACTORS: 1 TO 7.06 IN THE Y DIRECTION

Table XXVI. Selected Printout. Example No. 3 (page 12 of 12)

Example No. 4. Unrestrained 95th Percentile Driver (EA Column and Lower Instrument Panel) in 30 mph Frontal Collision.

The occupant description used in this data set (Table XXVII) was derived by scaling the 50th percentile dummy data upward to reflect the stature and weight of the larger subject. The vehicle geometry and properties were the same as Example No. 2 except that the lap belt was removed and replaced by an energy-absorbing lower instrument panel (See Figure 45 of "Passive Protection at 50 Miles per Hour by Carter.³³). This surface (No. 6) had the energy absorbing properties shown in Figure 41 as specified on the proper S, T, V, and X cards. A windshield contact surface was also added because of the extreme penetration of the large occupant into the steering column. This was considerably more pronounced than for the smaller occupant although the occupant loadings may be tolerable.

In early versions of this exercise it was observed that the center torso mass element moved forward so far that the lower edge of the steering wheel passed entirely through the body. This occurred because no contact sensing circles are attached to this element. To avoid this problem and in a sense to simulate the restraining effect of the lower part of the steering wheel on the torso, the stop angles for joints 2 and 3 were decreased. In later simulations this provided restraining torques at these joints to eliminate the unrealistic kinematics. For comparison purposes, see fields 2 and 3 of the I card for Example No. 1 (Table XXI) and this example (Table XXVII).

The output from this exercise is included as Table XXVIII. The occupant moves forward and contacts all surfaces. Penetration of the column by the chest is approximately 8 inches before rebound.

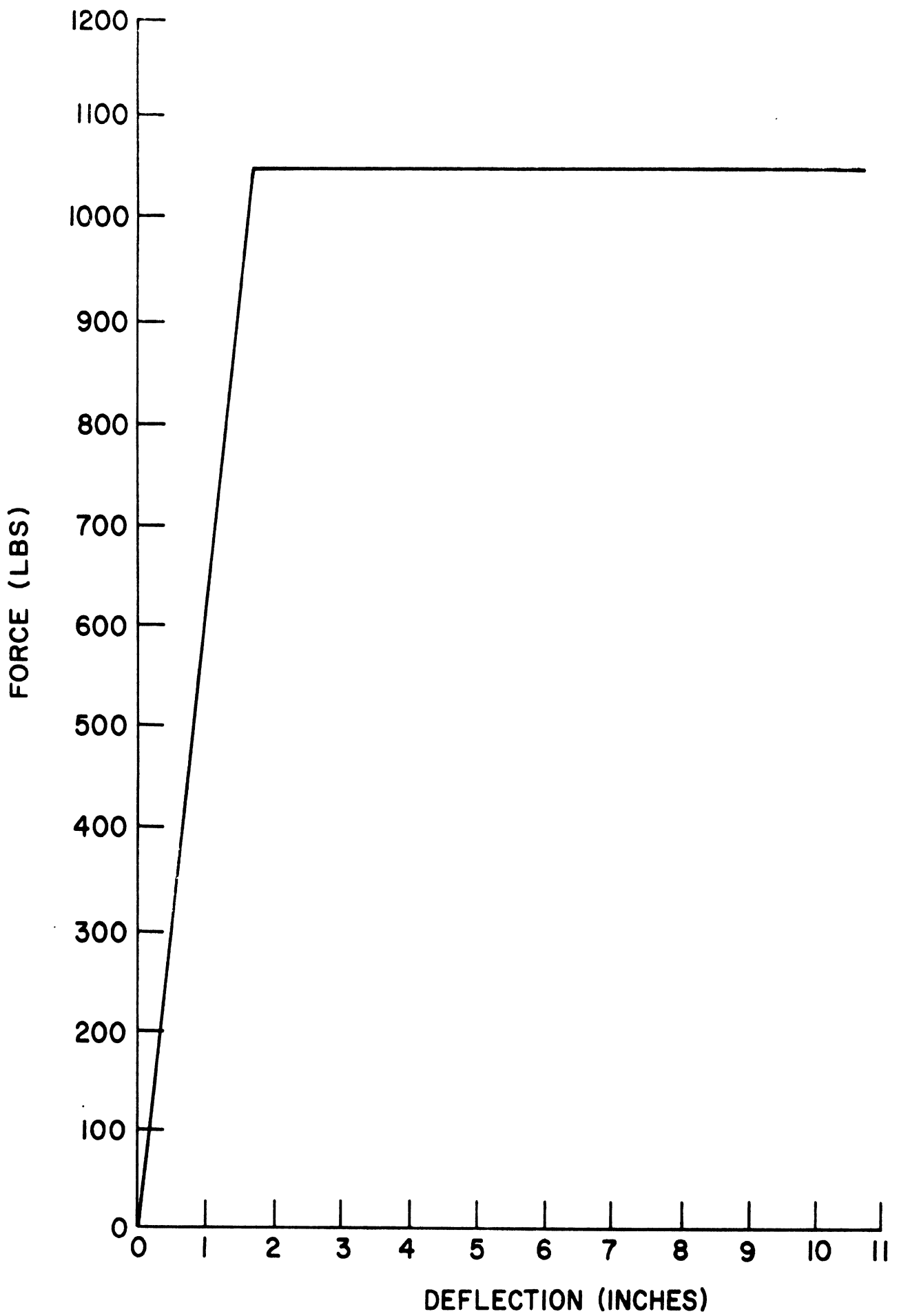


Figure 41. Force-Deflection Characteristics of Knee Restraint

\$LIST DOTIM (209,278)

209	A1.	1.	1.	1.	1.	1.64	3.33
210	B2.83	.75	4.16	.606	.845	3.64	
211	C960.	960.	960.	960.	960.	960.	
212	D4.77	6.12	13.39	8.13	11.39	17.47	17.08
213	E.061	.0232	.138	.0368	.0326	.128	-.0697
214	F3.76	0.	3.76	4.	1.25	2.18	3.75
215	G21000.	100000.	100000.	200000.	7000.	7000.	20000.
216	H60.	15.	20.	26.	20000.	20000.	
217	I150.	5.	5.	70.	130.	120.	
218	J1.	1.	1.	1.	1.	1.	
219	K2.93	3.4	5.51	5.13	5.14	7.99	10.8
220	L103.	103.	103.	75.	0.	13.5	-39.8
221	M0.	2.	0.	145.	0.	5.	1.
222	N1.	92.	.1	.34	5.31	1.57	15.
223	O12.1	13.5	16.8	2.55	50.	2.	1000.
224	P1.	.315	1.	50.	0.	-12.	
225	P2.	.315	1.	77.	.5	350.	
226	P3.	.315	1.	-39.	.5	350.	
227	Q1.	.5	.078				
228	Q2.						
229	Q3.						
230	R1.	528.	528.	0.	.005	.2	1.
231	S0.	45.	.5	.5	45.	-10.	3.
232	T0.	0.	800.				
233	U0.						
234	S1.	28.	.01	.95	-3.	.1	283.
235	T1.	0.	800.				
236	U1.						
237	S8.	36.	.5	.5	18.5	.1	135.
238	T8.	0.	800.				
239	U8.						
240	U2.						
241	S3.	16.	.01	.55	12.	.1	70.
242	T3.	0.	400.				
243	U3.						
244	X3.	1000.	400.	.55	0.	.1	144.
245	S4.	43.8	.01				
246	T4.	0.	2000.				
247	X4.	2000.	2000.				
248	U4.						
249	S5.	26.4	.01	.55	41.3	.1	70.
250	T5.	0.	4000.				
251	S6.	20.	.01	.55	18.5	.1	106.5
252	T6.	0.	1400.				
253	U5.						
254	X6.	2100.	1400.				
255	U6.						
256	S7.	30.3	.01	.55	20.8	.1	70.
257	T7.	0.	1000.				
258	U7.						
259	X7.	2000.	1000.				
260	U9.						
261	V1.	1.	0.	0.			
262	V1.	1.	.02	-5653.			
263	V1.	1.	-.0547	-5653.			
264	V1.	1.	.0747	C.			
265	V1.	1.	2.	0.			
266	2						

Table XXVII. Data Set. Example No. 4 (page 1 of 2)

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Table XXVII. Data Set. Example No. 4 (page 2 of 2)

TIME (SEC.)	BELT FORCES (POUNDS)		TMC DIMENSIONAL CRASH VICTIM SIMULATOR BELT ANGLES (DEGREES)		OUTPUT DATA		SEP 7. 1972		PAGE 1	
	LAP	BELT	SHOULDER	RESTRAINT	LAP	BELT	SHOULDER	RESTRAINT	RELATIVE HIP POSITION (INCHES)	RELATIVE HEAD POSITION (INCHES)
	LCMER	LCMER	UPPER	UPPER	UPPER	UPPER	UPPER	UPPER	HORIZONTAL	VERTICAL
C.00		0.0	0.0	0.0	0.0	0.0	0.0	0.0	-4.12	28.66
C.005		0.0	0.0	0.0	0.0	0.0	0.0	0.0	-4.11	28.66
C.010		0.0	0.0	0.0	0.0	0.0	0.0	0.0	-4.04	28.66
C.015		0.0	0.0	0.0	0.0	0.0	0.0	0.0	-3.85	28.66
C.020		0.0	0.0	0.0	0.0	0.0	0.0	0.0	-3.48	28.65
C.025		0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.87	28.65
C.030		0.0	0.0	0.0	0.0	0.0	0.0	0.0	-2.03	28.65
C.035		0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.94	28.64
C.040		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.38	28.63
C.045		0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.95	28.62
C.050		0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.77	28.60
C.055		0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.84	28.58
C.060		0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.99	28.52
C.065		0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.92	28.31
C.070		0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.56	27.96
C.075		0.0	0.0	0.0	0.0	0.0	0.0	0.0	12.78	27.46
C.080		0.0	0.0	0.0	0.0	0.0	0.0	0.0	13.41	26.74
C.085		0.0	0.0	0.0	0.0	0.0	0.0	0.0	13.64	25.78
C.090		0.0	0.0	0.0	0.0	0.0	0.0	0.0	13.79	24.76
C.095		0.0	0.0	0.0	0.0	0.0	0.0	0.0	13.93	23.77
C.100		0.0	0.0	0.0	0.0	0.0	0.0	0.0	14.12	22.84
C.105		0.0	0.0	0.0	0.0	0.0	0.0	0.0	14.26	22.06
C.110		0.0	0.0	0.0	0.0	0.0	0.0	0.0	14.20	21.66
C.115		0.0	0.0	0.0	0.0	0.0	0.0	0.0	13.85	21.74
C.120		0.0	0.0	0.0	0.0	0.0	0.0	0.0	13.39	22.03
C.125		0.0	0.0	0.0	0.0	0.0	0.0	0.0	12.94	22.45
C.130		0.0	0.0	0.0	0.0	0.0	0.0	0.0	12.52	23.99
C.135		0.0	0.0	0.0	0.0	0.0	0.0	0.0	12.15	23.62
C.140		0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.83	24.32
C.145		0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.57	25.06
C.150		0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.37	25.79
C.155		0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.24	26.43
C.160		0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.16	26.85
C.165		0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.13	27.05
C.170		0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.04	27.01
C.175		0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.83	26.77
C.180		0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.45	26.35
C.185		0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.93	25.85
C.190		0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.24	25.35
C.195		0.0	0.0	0.0	0.0	0.0	0.0	0.0	8.50	25.11
C.200		0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.81	25.25

Table XXVIII. Selected Printout. Example No. 4 (page 1 of 9)

TWC DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA (DEGREES)

TIME	UPPER ARM				LOWER ARM				POSITION VELOCITY (DEGREES)				UPPER LEG				LOWER LEG			
	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY		
0.0	0.4277E 03	0.0	0.0	0.0	-0.2017E 04	13.50	0.0	-0.1273E 04	39.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0			
0.0050	0.4681E 03	-0.03	-0.1076	-0.2143E 04	13.48	0.0	-0.1665E 04	39.83	-11.11	-0.1608E 04	-39.43	-11.11	-0.1608E 04	-39.43	-11.11	-0.1608E 04	-39.43	-11.11		
0.0100	0.4314E 03	-0.11	-21.55	-0.2143E 04	13.42	-16.26	-0.1620E 04	39.91	-40.05	-0.2588E 04	-39.91	-40.05	-0.2588E 04	-39.91	-40.05	-0.2588E 04	-39.91	-40.05		
0.0150	0.3828E 03	-0.24	-32.14	-0.2056E 04	13.32	-23.85	-0.1347E 04	40.05	-41.06	-0.3000E 04	-40.05	-41.06	-0.3000E 04	-40.05	-41.06	-0.3000E 04	-40.05	-41.06		
0.0200	0.3066E 03	-0.43	-42.41	-0.1934E 04	13.19	-28.35	-0.2800E 04	40.39	-42.18	-0.3906E 04	-40.39	-42.18	-0.3906E 04	-40.39	-42.18	-0.3906E 04	-40.39	-42.18		
0.0250	0.1576E 03	-0.66	-51.40	-0.1610E 04	13.06	-19.32	-0.3906E 04	41.06	-43.86	-0.4649E 04	-41.06	-43.86	-0.4649E 04	-41.06	-43.86	-0.4649E 04	-41.06	-43.86		
0.0300	0.6528E 02	-0.94	-68.57	-0.1198E 04	13.03	10.55	-0.8649E 04	42.18	-45.87	-0.5101E 04	-42.18	-45.87	-0.5101E 04	-42.18	-45.87	-0.5101E 04	-42.18	-45.87		
0.0350	0.4655E 03	-1.25	-83.87	-0.1059E 04	13.20	60.97	-0.8649E 04	43.86	-47.84	-0.5752E 04	-43.86	-47.84	-0.5752E 04	-43.86	-47.84	-0.5752E 04	-43.86	-47.84		
0.0400	0.1120E 04	-1.58	-68.69	-0.5666E 03	13.62	101.74	-0.7752E 04	45.87	-49.89	-0.6309E 04	-45.87	-49.89	-0.6309E 04	-45.87	-49.89	-0.6309E 04	-45.87	-49.89		
0.0450	0.6183E 03	-1.92	-67.19	-0.1519E 04	14.24	151.18	-0.1158E 05	47.84	-52.30	-0.7093E 04	-47.84	-52.30	-0.7093E 04	-47.84	-52.30	-0.7093E 04	-47.84	-52.30		
0.0500	0.7068E 03	-2.23	-53.22	-0.4168E 04	15.15	216.63	-0.1583E 05	49.89	-55.28	-0.7321E 05	-49.89	-55.28	-0.7321E 05	-49.89	-55.28	-0.7321E 05	-49.89	-55.28		
0.0550	0.2128E 05	-2.43	-19.57	-0.1664E 05	16.48	325.93	-0.3217E 05	52.30	-69.47	-0.8280E 04	-52.30	-69.47	-0.8280E 04	-52.30	-69.47	-0.8280E 04	-52.30	-69.47		
0.0600	0.4845E 05	-2.27	84.30	-0.1744E 05	18.49	481.73	-0.3022E 05	55.28	-72.81	-0.9185E 04	-55.28	-72.81	-0.9185E 04	-55.28	-72.81	-0.9185E 04	-55.28	-72.81		
0.0650	0.3805E 05	-1.66	155.47	-0.1239E 05	21.29	647.29	-0.3572E 05	58.90	-77.81	-1.0145E 04	-58.90	-77.81	-1.0145E 04	-58.90	-77.81	-1.0145E 04	-58.90	-77.81		
0.0700	0.6110E 05	-0.77	178.59	-0.1353E 05	25.05	858.35	-0.4159E 05	62.63	-82.63	-1.1266E 04	-62.63	-82.63	-1.1266E 04	-62.63	-82.63	-1.1266E 04	-62.63	-82.63		
0.0750	0.8281E 05	-0.19	27.85	-0.4571E 05	29.73	992.58	-0.1879E 05	66.36	-89.47	-1.2563E 04	-66.36	-89.47	-1.2563E 04	-66.36	-89.47	-1.2563E 04	-66.36	-89.47		
0.0800	0.7142E 05	-0.72	-263.41	-0.7467E 05	34.88	1049.88	-0.1756E 05	72.81	-94.89	-1.4030E 04	-72.81	-94.89	-1.4030E 04	-72.81	-94.89	-1.4030E 04	-72.81	-94.89		
0.0850	0.7190E 05	-3.07	-699.10	-0.5420E 05	40.06	1013.54	-0.1062E 05	82.63	-101.45	-1.5522E 04	-82.63	-101.45	-1.5522E 04	-82.63	-101.45	-1.5522E 04	-82.63	-101.45		
0.0900	0.6110E 05	-7.78	-1178.02	-0.6424E 05	45.04	995.89	-0.1033E 04	92.81	-111.52	-1.7166E 04	-92.81	-111.52	-1.7166E 04	-92.81	-111.52	-1.7166E 04	-92.81	-111.52		
0.0950	0.4257E 05	-14.61	-1477.77	-0.6918E 05	49.98	953.32	-0.2563E 05	101.45	-126.63	-1.9140E 04	-101.45	-126.63	-1.9140E 04	-101.45	-126.63	-1.9140E 04	-101.45	-126.63		
0.1000	0.3465E 06	-19.15	70.74	-0.5216E 06	54.28	732.41	-0.5281E 05	111.52	-134.9E 05	-2.1349E 04	-111.52	-134.9E 05	-2.1349E 04	-111.52	-134.9E 05	-2.1349E 04	-111.52	-134.9E 05		
0.1050	0.8571E 05	-14.82	1251.32	-0.1203E 06	57.29	471.62	-0.5222E 05	126.63	-145.89	-2.3834E 04	-126.63	-145.89	-2.3834E 04	-126.63	-145.89	-2.3834E 04	-126.63	-145.89		
0.1100	0.5186E 05	-7.17	1783.18	-0.8611E 05	58.97	207.56	-0.5299E 05	145.89	-161.59	-2.6349E 04	-145.89	-161.59	-2.6349E 04	-145.89	-161.59	-2.6349E 04	-145.89	-161.59		
0.1150	0.4258E 05	2.61	2087.77	-0.3470E 05	59.33	-61.59	-0.5140E 05	166.36	-177.47	-2.8949E 04	-166.36	-177.47	-2.8949E 04	-166.36	-177.47	-2.8949E 04	-166.36	-177.47		
0.1200	0.6861E 04	13.43	2211.68	-0.9161E 04	58.75	-160.16	-0.1349E 05	189.49	-194.89	-3.1549E 04	-189.49	-194.89	-3.1549E 04	-189.49	-194.89	-3.1549E 04	-189.49	-194.89		
0.1250	0.6057E 04	24.55	2224.60	-0.4300E 04	57.81	-209.75	-0.6834E 04	216.63	-209.75	-3.4149E 04	-216.63	-209.75	-3.4149E 04	-216.63	-209.75	-3.4149E 04	-216.63	-209.75		
0.1300	0.1817E 05	35.58	2183.47	-0.1247E 05	56.68	-239.78	-0.5810E 04	245.89	-239.78	-3.6749E 04	-245.89	-239.78	-3.6749E 04	-245.89	-239.78	-3.6749E 04	-245.89	-239.78		
0.1350	0.2244E 05	46.32	2107.55	-0.1672E 05	55.38	-279.15	-0.8749E 04	274.89	-279.15	-3.9149E 04	-274.89	-279.15	-3.9149E 04	-274.89	-279.15	-3.9149E 04	-274.89	-279.15		
0.1400	0.2269E 05	56.64	2020.99	-0.1755E 05	53.89	-319.68	-0.9189E 04	309.49	-319.68	-4.1549E 04	-309.49	-319.68	-4.1549E 04	-309.49	-319.68	-4.1549E 04	-309.49	-319.68		
0.1450	0.2105E 05	66.51	1927.71	-0.1944E 05	52.18	-363.03	-0.9189E 04	349.89	-363.03	-4.3949E 04	-349.89	-363.03	-4.3949E 04	-349.89	-363.03	-4.3949E 04	-349.89	-363.03		
0.1500	0.1783E 05	75.90	1826.05	-0.2142E 05	50.25	-412.01	-0.1064E 05	389.89	-412.01	-4.6349E 04	-389.89	-412.01	-4.6349E 04	-389.89	-412.01	-4.6349E 04	-389.89	-412.01		
0.1550	0.1256E 05	84.75	1716.33	-0.2193E 05	48.05	-470.54	-0.1147E 05	429.89	-470.54	-4.8749E 04	-429.89	-470.54	-4.8749E 04	-429.89	-470.54	-4.8749E 04	-429.89	-470.54		
0.1600	0.4747E 02	93.07	1606.01	-0.2111E 05	45.61	-528.20	-0.1084E 05	469.89	-528.20	-5.1149E 04	-469.89	-528.20	-5.1149E 04	-469.89	-528.20	-5.1149E 04	-469.89	-528.20		
0.1650	0.4747E 02	100.85	1512.49	-0.1728E 05	43.11	-528.20	-0.1084E 05	509.89	-528.20	-5.3549E 04	-509.89	-528.20	-5.3549E 04	-509.89	-528.20	-5.3549E 04	-509.89	-528.20		
0.1700	0.3527E 04	108.21	1430.36	-0.1563E 05	40.33	-584.44	-0.1112E 05	549.89	-584.44	-5.5949E 04	-549.89	-584.44	-5.5949E 04	-549.89	-584.44	-5.5949E 04	-549.89	-584.44		
0.1750	0.6254E 03	115.03	1267.12	-0.5467E 05	37.28	-632.52	-0.2376E 04	589.89	-632.52	-5.8349E 04	-589.89	-632.52	-5.8349E 04	-589.89	-632.52	-5.8349E 04	-589.89	-632.52		
0.1800	0.3422E 04	120.56	915.17	-0.8730E 05	34.03	-659.56	-0.2376E 04	629.89	-659.56	-6.0749E 04	-629.89	-659.56	-6.0749E 04	-629.89	-659.56	-6.0749E 04	-629.89	-659.56		
0.1850	0.5682E 04	123.94	416.45	-0.1138E 05	30.79	-640.14	-0.1033E 04	669.89	-640.14	-6.3149E 04	-669.89	-640.14	-6.3149E 04	-669.89	-640.14	-6.3149E 04	-669.89	-640.14		
0.1900	0.5321E 04	124.87	57.43	-0.2279E 05	27.59	-636.56	-0.3112E 04	709.89	-636.56	-6.5549E 04	-709.89	-636.56	-6.5549E 04	-709.89	-636.56	-6.5549E 04	-709.89	-636.56		
0.1950	0.1158E 04	124.92	-46.51	-0.2389E 05	24.47	-610.05	-0.6949E 04	749.89	-610.05	-6.7949E 04	-749.89	-610.05	-6.7949E 04	-749.89	-610.05	-6.7949E 04	-749.89	-610.05		
0.2000	0.1265E 05	124.36	-193.14	-0.3630E 05	21.48	-599.09	-0.4051E 04	789.89	-599.09	-7.0349E 04	-789.89	-599.09	-7.0349E 04	-789.89	-599.09	-7.0349E 04	-789.89	-599.09		

Table XXVIII. Selected Printout. Example No. 4 (page 3 of 9)

TIME	POSITION (IN.)	VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)	RELATIVE DISPL. (IN.)	VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)	RELATIVE DISPL. (IN.)	VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)
0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0050	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0150	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0250	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0300	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0350	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0450	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0500	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0550	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0600	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0650	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0700	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0750	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0800	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0850	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0900	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0950	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1050	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1150	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1250	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1300	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1350	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1450	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1500	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1550	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1600	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1650	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1700	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1750	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1800	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1850	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1900	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1950	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.2000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Table XXVIII. Selected Printout. Example No. 4 (page 4 of 9)

THREE DIMENSIONAL CRASH VICTIM SIMULATION OUTPUT DATA BELT FORCES (LBS)

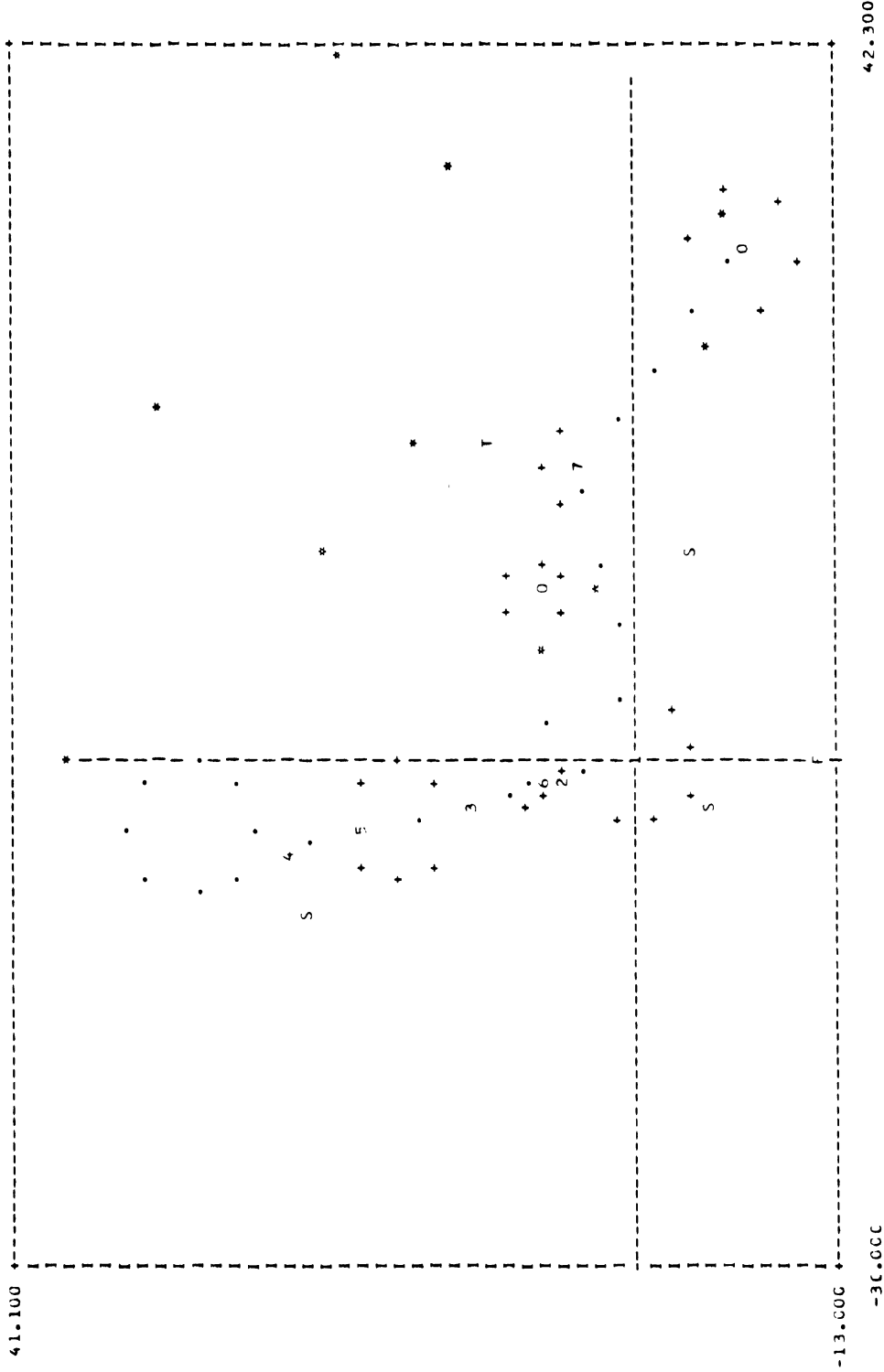
ACCELEROMETER READINGS

TIME	HEAD		CHEST		LAP	SHOULDER RESTRAINT		AT HIP	AT FRONT EDGE
	RESULTANT (G-UNITS)	ANGLE (DEG.)	RESULTANT (G-UNITS)	ANGLE (DEG.)		LOWER	UPPER		
0.0	0.3	-47.4	0.2	-179.2	0.0	0.0	145.00	0.0	0.0
0.0050	0.3	-32.8	0.3	164.7	0.0	0.0	145.60	0.0	0.0
0.0100	0.2	-31.6	0.3	163.3	0.0	0.0	147.01	0.0	0.0
0.0150	0.2	-30.4	0.3	162.1	0.0	0.0	150.01	0.0	0.0
0.0200	0.2	-38.3	0.3	170.1	0.0	0.0	154.61	0.0	0.0
0.0250	0.2	-61.1	0.3	-167.5	0.0	0.0	160.70	0.0	0.0
0.0300	0.3	-82.5	0.4	-145.5	0.0	0.0	167.95	0.0	0.0
0.0350	0.1	-81.8	1.1	-159.2	0.0	0.0	176.93	0.0	0.0
0.0400	0.1	-89.8	2.4	158.5	0.0	0.0	190.82	0.0	0.0
0.0450	0.8	-193.1	2.9	-141.0	0.0	0.0	206.53	0.0	0.0
0.0500	1.3	68.7	10.7	-154.0	0.0	0.0	219.63	0.0	0.0
0.0550	24.8	-177.2	28.7	-152.2	0.0	0.0	235.70	0.0	0.0
0.0600	50.3	-144.1	23.4	-142.5	0.0	0.0	260.60	0.0	19.81
0.0650	55.0	-165.6	22.3	-143.6	0.0	0.0	284.42	0.0	62.25
0.0700	64.2	-163.7	49.8	-170.6	0.0	0.0	321.51	0.0	117.10
0.0750	77.5	-156.9	36.3	-176.8	0.0	0.0	354.24	0.0	181.36
0.0800	61.4	-141.5	38.5	-175.0	0.0	0.0	389.39	0.0	251.65
0.0850	16.2	-27.0	38.8	164.7	0.0	0.0	420.51	0.0	319.13
0.0900	11.6	23.9	29.2	173.6	0.0	0.0	448.74	0.0	376.39
0.0950	13.7	28.3	45.6	159.0	0.0	0.0	476.99	0.0	420.29
0.1000	18.5	51.1	31.1	142.2	0.0	0.0	479.93	0.0	428.17
0.1050	56.8	166.5	7.6	53.9	0.0	0.0	452.65	0.0	382.09
0.1100	89.4	110.7	28.6	7.9	0.0	0.0	427.19	0.0	287.95
0.1150	29.3	115.3	16.3	138.3	0.0	0.0	392.34	0.0	172.71
0.1200	18.4	80.3	4.4	132.1	0.0	0.0	356.68	0.0	53.74
0.1250	16.8	62.5	3.0	13.4	0.0	0.0	326.42	0.0	0.0
0.1300	16.0	53.5	3.2	-1.1	0.0	0.0	301.47	0.0	0.0
0.1350	15.0	40.8	1.1	21.2	0.0	0.0	277.87	0.0	0.0
0.1400	14.4	20.3	0.9	43.2	0.0	0.0	255.20	0.0	0.0
0.1450	15.9	-10.5	1.2	56.9	0.0	0.0	232.39	0.0	0.0
0.1500	22.6	-43.2	2.1	74.5	0.0	0.0	207.76	0.0	0.0
0.1550	36.0	-69.1	4.4	110.9	0.0	0.0	178.97	0.0	0.0
0.1600	32.7	-85.1	39.3	159.1	0.0	0.0	157.95	0.0	0.0
0.1650	36.0	-102.4	4.3	93.7	0.0	0.0	132.79	0.0	0.0
0.1700	38.1	-113.3	4.2	96.3	0.0	0.0	103.86	0.0	0.0
0.1750	36.4	-136.2	3.2	121.9	0.0	0.0	77.31	0.0	0.0
0.1800	29.5	-154.2	4.2	162.3	0.0	0.0	56.26	0.0	0.0
0.1850	30.7	-170.3	2.5	-166.0	0.0	0.0	46.08	0.0	0.0
0.1900	45.8	110.3	6.2	-148.6	0.0	0.0	32.58	0.0	0.0
0.1950	71.4	65.9	10.3	-140.2	0.0	0.0	25.67	0.0	0.0
0.2000	5.3	100.1	1.2	-102.6	0.0	0.0	13.89	0.0	0.0

Table XXVIII. Selected Printout, Example No. 4 (page 5 of 9)

TIME	HEIGHT IN	HEIGHT IN	HEIGHT IN	LOWER PANEL KNIFE	MIDSHIELD ON	UPPER TRACT ON	UPPER TRACT COLUMN
0.0	32.5	0.0	0.0	0.0	0.0	0.0	0.0
0.005C	23.5	0.0	0.0	0.0	0.0	0.0	0.0
0.010C	34.2	0.0	0.0	0.0	0.0	0.0	0.0
0.015C	35.7	0.0	0.0	0.0	0.0	0.0	0.0
0.020C	17.6	0.0	0.0	0.0	0.0	0.0	0.0
0.025C	35.7	0.0	0.0	0.0	0.0	0.0	0.0
0.030C	54.4	0.0	0.0	0.0	0.0	0.0	0.0
0.035C	75.2	0.0	0.0	0.0	0.0	0.0	0.0
0.040C	57.0	0.0	0.0	0.0	0.0	0.0	0.0
0.045C	119.7	0.0	0.0	0.0	0.0	0.0	0.0
0.050C	140.0	0.0	0.0	0.0	0.0	0.0	0.0
0.055C	154.0	0.0	0.0	0.0	0.0	0.0	0.0
0.060C	158.9	0.0	0.0	0.0	0.0	0.0	0.0
0.065C	144.7	0.0	0.0	0.0	0.0	0.0	0.0
0.070C	112.3	0.0	0.0	0.0	0.0	0.0	0.0
0.075C	70.4	0.0	0.0	0.0	0.0	0.0	0.0
0.080C	23.4	0.0	0.0	0.0	0.0	0.0	0.0
0.085C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.090C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.095C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.100C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.105C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.110C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.115C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.120C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.125C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.130C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.135C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.140C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.145C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.150C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.155C	12.4	0.0	0.0	0.0	0.0	0.0	0.0
0.160C	22.7	0.0	0.0	0.0	0.0	0.0	0.0
0.165C	21.7	0.0	0.0	0.0	0.0	0.0	0.0
0.170C	4.0	0.0	0.0	0.0	0.0	0.0	0.0
0.175C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.180C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.185C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.190C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.195C	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.200C	0.0	0.0	0.0	0.0	0.0	0.0	0.0

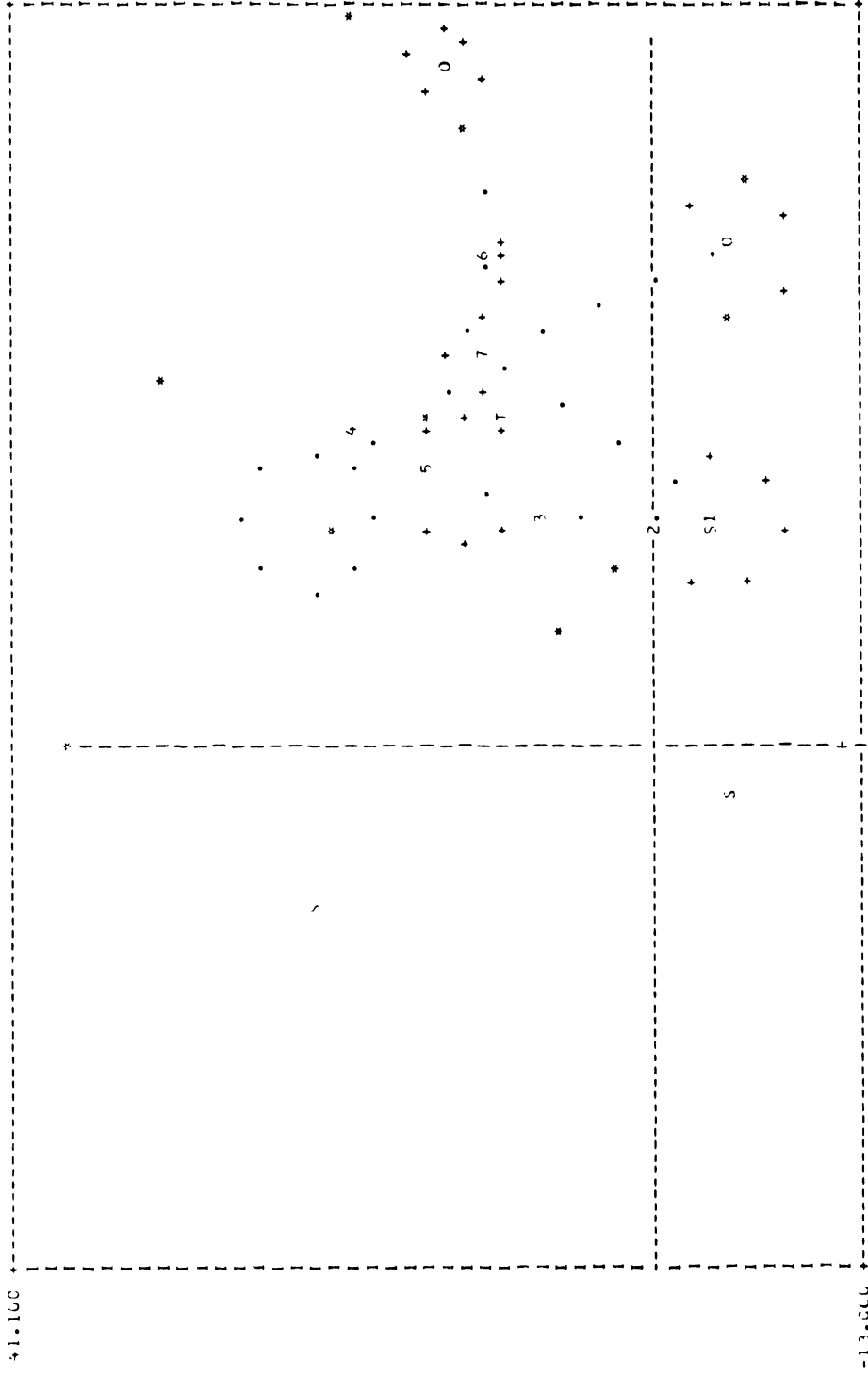
Table XXVIII. Selected Printout. Example No. 4 (page 6 of 9)



INDICATED MEASUREMENTS ARE IN INCHES
 SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
 SCALING FACTORS: 1 TO 7.06 IN THE Y DIRECTION

Table XXVIII. Selected Printout. Example No. 4 (page 7 of 9)

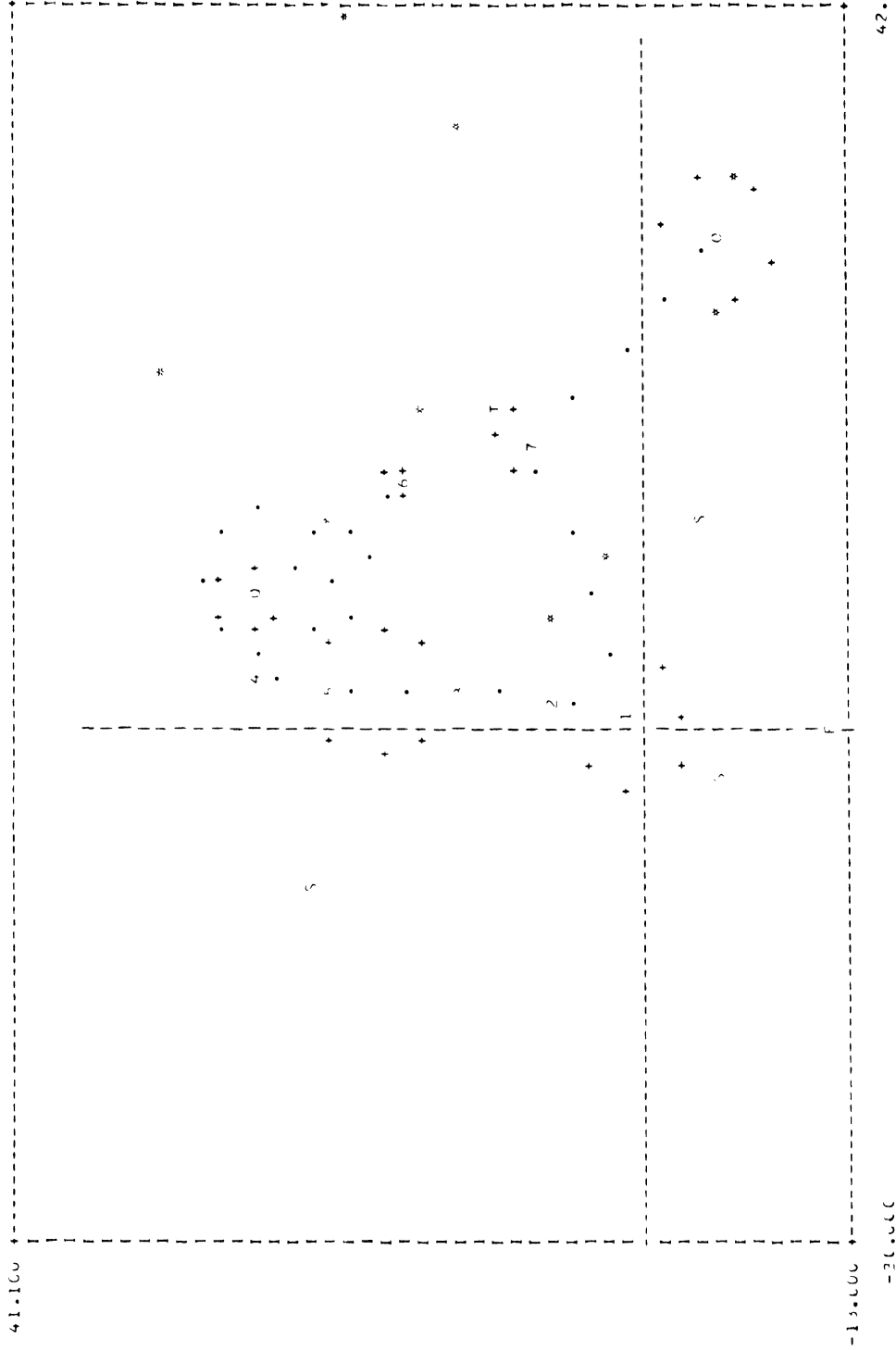
TWO DIMENSIONAL CRASH VECTIN SIMULATION OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.120 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.00 IN THE X DIRECTION
1 TO 7.00 IN THE Y DIRECTION

Table XXVIII. Selected Printout. Example No. 4 (page 8 of 9)

TOP VIEW PUNCH CARD ASH VELOCITY SIMULATOR - HEIGHT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.200 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.07 IN THE X DIRECTION
1 TO 7.06 IN THE Y DIRECTION

Table XXVIII. Selected Printout. Example No. 4 (page 9 of 9)

Example No. 5. Unrestrained 95th Percentile Occupant in 30 mph Rear-End Collision.

The occupant description used in this data set (Table XXIX) was the same as that used in Example 4. The contact surfaces consisted of toeboard, floor, seat cushion, and seat back. The seat back was made up of two segments - one to restrain the hip and one for the upper torso.

The reason for two surfaces is based on the friction options available with the HSRI model. It should be recalled that the presence of more than one friction force during computation can lead to instabilities. If one surface is used for the seat back (e.g. surface No. 1 - seat back) which interacts with the hip and the upper torso contact circles, then the possibility for generation to two simultaneous friction forces is very high especially since ramping usually is observed in rear impacts. This being the case, two surfaces have been used in this example. Surface No. 1 has non-zero friction and interacts with the hip while surface no. 7 interacts with the upper torso.

Two options are available to model the knees and lower legs as they swing back toward the front seat. One of these is contained in fields 7-8 of the 0-card and the other involves restriction of the relative motion between the upper and lower legs. Field 7 of the 0-card contains a "thickness" for the lower leg while field 8 contains a stiffness factor which generates a forward acting force on the lower leg if contact is sensed. In this example flexion of the knee was limited to model a similar effect.

Table XXX contains output generated using this data set. The only obvious aspect of body loadings and kinematics which should be of concern is the head-neck hyperextension caused by a lack of head restraint. The addition of a head restraint, possibly by use of surface No. 4, would lead to a gentle ride for the occupant.

TIME (SEC.)	TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA				RELATIVE HIP POSITION (INCHES)		RELATIVE HEAD POSITION (INCHES)		
	LAP BELT SHOULDER RESTRAINT LOWER	LAP BELT SHOULDER RESTRAINT UPPER	BELT ANGLES (DEGREES)	LAP BELT SHOULDER RESTRAINT LOWER	LAP BELT SHOULDER RESTRAINT UPPER	HORIZONTAL	VERTICAL	HORIZONTAL	VERTICAL
0.0	0.	0.	0.	0.0	0.0	0.0	0.0	-4.12	28.66
0.005	0.	0.	0.	0.0	0.0	-0.00	0.00	-4.13	28.65
0.010	0.	0.	0.	0.0	0.0	-0.04	0.00	-4.16	28.66
0.015	0.	0.	0.	0.0	0.0	-0.14	0.00	-4.26	28.65
0.020	0.	0.	0.	0.0	0.0	-0.32	0.01	-4.45	28.65
0.025	0.	0.	0.	0.0	0.0	-0.56	0.01	-4.70	28.64
0.030	0.	0.	0.	0.0	0.0	-0.80	-0.00	-4.97	28.64
0.035	0.	0.	0.	0.0	0.0	-1.01	-0.00	-5.21	28.66
0.040	0.	0.	0.	0.0	0.0	-1.18	0.01	-5.44	28.71
0.045	0.	0.	0.	0.0	0.0	-1.33	0.04	-5.67	28.80
0.050	0.	0.	0.	0.0	0.0	-1.47	0.08	-5.92	28.91
0.055	0.	0.	0.	0.0	0.0	-1.61	0.14	-6.21	29.03
0.060	0.	0.	0.	0.0	0.0	-1.76	0.23	-6.56	29.14
0.065	0.	0.	0.	0.0	0.0	-1.93	0.33	-7.00	29.20
0.070	0.	0.	0.	0.0	0.0	-2.09	0.45	-7.50	29.19
0.075	0.	0.	0.	0.0	0.0	-2.24	0.64	-8.05	29.13
0.080	0.	0.	0.	0.0	0.0	-2.35	0.88	-8.62	28.99
0.085	0.	0.	0.	0.0	0.0	-2.41	1.17	-9.14	28.76
0.090	0.	0.	0.	0.0	0.0	-2.41	1.47	-9.63	28.44
0.095	0.	0.	0.	0.0	0.0	-2.33	1.74	-10.03	28.03
0.100	0.	0.	0.	0.0	0.0	-2.20	1.95	-10.35	27.57
0.105	0.	0.	0.	0.0	0.0	-2.14	2.15	-10.57	27.09
0.110	0.	0.	0.	0.0	0.0	-2.14	2.32	-10.68	26.63
0.115	0.	0.	0.	0.0	0.0	-2.11	2.40	-10.77	26.26
0.120	0.	0.	0.	0.0	0.0	-2.06	2.43	-10.67	26.13
0.125	0.	0.	0.	0.0	0.0	-1.97	2.46	-10.58	26.18
0.130	0.	0.	0.	0.0	0.0	-1.85	2.46	-10.44	26.32
0.135	0.	0.	0.	0.0	0.0	-1.71	2.43	-10.23	26.56
0.140	0.	0.	0.	0.0	0.0	-1.57	2.36	-9.95	26.86
0.145	0.	0.	0.	0.0	0.0	-1.43	2.28	-9.60	27.25
0.150	0.	0.	0.	0.0	0.0	-1.29	2.17	-9.21	27.69
0.155	0.	0.	0.	0.0	0.0	-1.17	2.05	-8.79	28.19
0.160	0.	0.	0.	0.0	0.0	-1.05	1.92	-8.34	28.72
0.165	0.	0.	0.	0.0	0.0	-0.95	1.79	-7.85	29.25
0.170	0.	0.	0.	0.0	0.0	-0.87	1.67	-7.31	29.72
0.175	0.	0.	0.	0.0	0.0	-0.82	1.59	-6.70	30.05
0.180	0.	0.	0.	0.0	0.0	-0.79	1.55	-6.04	30.16
0.185	0.	0.	0.	0.0	0.0	-0.79	1.55	-5.35	30.03
0.190	0.	0.	0.	0.0	0.0	-0.80	1.59	-4.67	29.72
0.195	0.	0.	0.	0.0	0.0	-0.82	1.67	-4.01	29.32
0.200	0.	0.	0.	0.0	0.0	-0.84	1.77	-3.40	28.86

Table XXX. Selected Printout. Example No. 5 (page 1 of 9)

TWO DIMENSIONAL BEASH VICTIM SIMULATOR OUTPUT DATA

TIME	LOWER TORSO			CENTER TORSO			UPPER TORSO			POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.
	POSITION	VELOCITY	ACCEL.	POSITION	VELOCITY	ACCEL.	POSITION	VELOCITY	ACCEL.								
0.0	103.00	0.0	0.6174E C3	103.00	0.0	0.9732E C3	103.00	0.0	0.0	103.00	0.0	0.4475E C3	103.00	0.0	0.0	0.0	0.0
0.0050	103.01	2.96	0.5631E C3	103.01	3.36	0.9162E C3	103.00	2.15	0.4342E C3	103.00	2.15	0.4342E C3	74.83	74.83	0.0	0.1851E C4	0.1851E C4
0.0100	103.03	5.70	0.5378E C3	103.03	6.42	0.9222E C3	103.02	4.27	0.4056E C3	103.02	4.27	0.4056E C3	74.40	74.40	0.0	0.1795E C4	0.1795E C4
0.0150	103.06	8.38	0.5348E C4	103.07	9.52	0.9180E C3	103.05	6.21	0.3664E C3	103.05	6.21	0.3664E C3	74.73	74.73	0.0	0.1645E C4	0.1645E C4
0.0200	103.11	11.20	0.5014E C4	103.13	12.06	0.9458E C3	103.08	7.55	0.5218E C3	103.08	7.55	0.5218E C3	74.63	74.63	0.0	0.1132E C4	0.1132E C4
0.0250	103.24	53.51	0.1642E C5	103.15	-6.40	-0.7331E C4	103.10	-3.70	-0.4357E C4	103.10	-3.70	-0.4357E C4	74.52	74.52	0.0	0.1352E C5	0.1352E C5
0.0300	103.74	130.88	-0.1805E C5	103.02	-40.37	-0.3275E C4	103.01	-31.14	-0.3872E C4	103.01	-31.14	-0.3872E C4	74.72	74.72	0.0	0.149E C5	0.149E C5
0.0350	104.40	138.60	0.4108E C5	102.81	-41.94	-0.1915E C5	102.79	-64.59	-0.1137E C5	102.79	-64.59	-0.1137E C5	74.42	74.42	0.0	0.350E C5	0.350E C5
0.0400	105.14	151.56	0.4978E C5	102.53	-44.02	-0.2269E C5	102.35	-107.75	-0.1357E C5	102.35	-107.75	-0.1357E C5	76.76	76.76	0.0	0.4254E C5	0.4254E C5
0.0450	106.01	198.90	0.1253E C5	102.33	-57.74	-0.2436E C4	101.61	-167.25	-0.1194E C5	101.61	-167.25	-0.1194E C5	78.30	78.30	0.0	0.3616E C5	0.3616E C5
0.0500	108.53	318.35	0.1384E C5	102.03	-65.16	-0.3228E C3	100.74	-210.19	-0.1135E C5	100.74	-210.19	-0.1135E C5	81.93	81.93	0.0	0.373E C5	0.373E C5
0.0550	109.27	381.22	0.1576E C5	101.44	-35.20	-0.2271E C4	99.52	-272.08	-0.1014E C5	99.52	-272.08	-0.1014E C5	85.39	85.39	0.0	0.3473E C5	0.3473E C5
0.0600	112.31	433.43	0.9743E C4	101.41	30.93	0.1515E C5	96.42	-332.10	-0.2145E C4	96.42	-332.10	-0.2145E C4	76.12	76.12	0.0	0.154E C5	0.154E C5
0.0700	114.73	504.77	-0.5137E C5	101.63	19.41	-0.3157E C5	94.74	-344.83	-0.9543E C4	94.74	-344.83	-0.9543E C4	101.99	101.99	0.0	0.4013E C5	0.4013E C5
0.0800	122.15	607.63	0.650E C5	101.01	-69.55	-0.3236E C5	93.01	-342.50	-0.8479E C4	93.01	-342.50	-0.8479E C4	103.53	103.53	0.0	0.3591E C5	0.3591E C5
0.0850	126.74	731.95	-0.2722E C5	103.43	-103.79	-0.3368E C5	91.34	-320.47	-0.1592E C5	91.34	-320.47	-0.1592E C5	115.53	115.53	0.0	0.5438E C4	0.5438E C4
0.0900	131.23	832.13	-0.1080E C6	103.00	138.15	0.1792E C6	88.44	-270.62	-0.2543E C5	88.44	-270.62	-0.2543E C5	123.41	123.41	0.0	0.333E C5	0.333E C5
0.0950	134.82	924.31	-0.4677E C5	102.50	406.40	-0.5207E C5	87.02	-291.32	-0.5948E C4	87.02	-291.32	-0.5948E C4	135.63	135.63	0.0	0.622E C5	0.622E C5
0.1000	137.43	991.03	-0.1772E C5	101.50	490.34	-0.1772E C5	85.53	-305.99	-0.4023E C4	85.53	-305.99	-0.4023E C4	143.30	143.30	0.0	0.1525E C5	0.1525E C5
0.1050	139.63	1044.59	-0.2493E C5	102.76	383.99	-0.2493E C5	83.94	-341.75	-0.1065E C5	83.94	-341.75	-0.1065E C5	148.30	148.30	0.0	0.1562E C5	0.1562E C5
0.1100	141.32	1044.31	-0.2336E C5	103.33	253.31	-0.2336E C5	82.34	-272.33	-0.2740E C5	82.34	-272.33	-0.2740E C5	154.24	154.24	0.0	0.634E C5	0.634E C5
0.1150	142.26	107.02	-0.3366E C5	103.32	176.02	-0.3366E C5	81.35	-124.99	0.2982E C5	81.35	-124.99	0.2982E C5	159.53	159.53	0.0	0.2693E C5	0.2693E C5
0.1200	142.62	57.86	-0.6655E C4	103.68	56.86	-0.6655E C4	80.94	-24.57	0.1775E C5	80.94	-24.57	0.1775E C5	159.11	159.11	0.0	0.252E C5	0.252E C5
0.1250	142.73	-21.62	-0.2775E C5	103.84	-22.64	-0.2775E C5	80.96	34.95	0.1512E C5	80.96	34.95	0.1512E C5	158.08	158.08	0.0	0.3150E C5	0.3150E C5
0.1300	142.34	-154.10	-0.2418E C5	103.38	-155.10	-0.2418E C5	81.33	103.61	0.1352E C5	81.33	103.61	0.1352E C5	156.33	156.33	0.0	0.3245E C5	0.3245E C5
0.1350	141.33	-352.74	-0.1229E C5	103.34	-253.73	-0.1229E C5	81.97	143.47	0.6159E C3	81.97	143.47	0.6159E C3	153.80	153.80	0.0	0.3399E C5	0.3399E C5
0.1400	133.86	-329.43	-0.1619E C5	103.89	-330.40	-0.1619E C5	82.73	171.35	0.9373E C4	82.73	171.35	0.9373E C4	150.43	150.43	0.0	0.305E C5	0.305E C5
0.1450	138.02	-474.40	-0.1346E C5	105.04	-403.37	-0.1346E C5	83.72	225.73	0.1281E C5	83.72	225.73	0.1281E C5	146.59	146.59	0.0	0.4548E C5	0.4548E C5
0.1500	135.83	-405.17	-0.1057E C5	103.80	-466.15	-0.1057E C5	85.02	296.33	0.1671E C5	85.02	296.33	0.1671E C5	145.79	145.79	0.0	0.650E C5	0.650E C5
0.1550	133.39	-311.31	-0.7938E C4	103.40	-512.83	-0.7938E C4	86.74	391.45	0.2099E C5	86.74	391.45	0.2099E C5	133.79	133.79	0.0	0.5314E C5	0.5314E C5
0.1600	130.73	-356.72	-0.1231E C5	103.70	-534.45	-0.1231E C5	88.97	502.82	0.2297E C5	88.97	502.82	0.2297E C5	125.52	125.52	0.0	0.6147E C5	0.6147E C5
0.1650	127.78	-242.29	-0.1438E C5	95.13	-512.20	-0.6035E C4	91.77	620.30	0.4311E C5	91.77	620.30	0.4311E C5	104.55	104.55	0.0	0.295E C5	0.295E C5
0.1700	124.43	-899.95	-0.1635E C5	92.66	-471.51	0.1156E C5	95.15	726.55	0.4967E C4	95.15	726.55	0.4967E C4	92.67	92.67	0.0	0.3147E C4	0.3147E C4
0.1750	120.76	-787.44	-0.1740E C5	93.48	-392.39	0.2133E C5	98.97	789.57	0.4967E C4	98.97	789.57	0.4967E C4	80.66	80.66	0.0	0.203E C5	0.203E C5
0.1800	116.61	-872.22	-0.1519E C5	83.82	-262.02	0.3163E C5	102.92	778.52	-0.1033E C5	102.92	778.52	-0.1033E C5	69.14	69.14	0.0	0.3362E C5	0.3362E C5
0.1850	112.03	-934.84	-0.8907E C4	87.50	-65.74	0.4422E C5	106.62	582.33	-0.2393E C5	106.62	582.33	-0.2393E C5	58.41	58.41	0.0	0.250E C5	0.250E C5
0.1900	107.30	-976.49	-0.630E C4	83.27	193.30	0.5315E C5	109.50	489.16	-0.4498E C5	109.50	489.16	-0.4498E C5	48.51	48.51	0.0	0.3362E C5	0.3362E C5
0.1950	102.35	-998.12	-0.2254E C4	83.83	403.14	0.2651E C5	111.49	294.63	-0.2958E C5	111.49	294.63	-0.2958E C5	48.51	48.51	0.0	0.3362E C5	0.3362E C5
0.2000	97.35	-1000.15	-0.1799E C4	82.16	520.99	0.1992E C5	112.00	149.81	-0.2803E C5	112.00	149.81	-0.2803E C5	48.51	48.51	0.0	0.3362E C5	0.3362E C5

Table XXX. Selected Printout. Example No. 5 (page 2 of 9)

4-DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA

TIME	UPPER ARM		LOWER ARM		UPPER LEG		LOWER LEG		ACCEL.	ACCEL.	
	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.	POSITION VELOCITY	ACCEL.			
0.0000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0050	-77.00	0.0	0.0	-0.2017E 04	13.50	-0.1273E 04	-39.80	-0.1273E 04	-0.3290E 04	-0.3290E 04	
0.0100	-76.93	2.03	-0.02	-0.1986E 04	13.48	-0.1426E 04	-39.84	-0.1426E 04	-0.8600E 03	-0.8600E 03	
0.0150	-76.98	3.97	-0.10	-0.1934E 04	13.43	-0.1444E 04	-39.91	-0.1444E 04	-0.2950E 03	-0.2950E 03	
0.0200	-76.95	5.70	-0.22	-0.1843E 04	13.35	-0.1442E 04	-39.98	-0.1442E 04	-0.2989E 03	-0.2989E 03	
0.0250	-76.92	6.47	-0.39	-0.1711E 04	13.22	-0.1442E 04	-40.07	-0.1442E 04	-0.7901E 03	-0.7901E 03	
0.0300	-76.93	-13.96	-0.59	-0.1644E 04	13.08	-0.1441E 04	-40.18	-0.1441E 04	-0.4958E 04	-0.4958E 04	
0.0350	-77.11	-65.38	-0.74	-0.1596E 05	13.00	-0.1441E 04	-40.41	-0.1441E 04	-0.1416E 04	-0.1416E 04	
0.0400	-77.62	-140.52	-0.91	-0.1509E 05	12.96	-0.1441E 04	-41.11	-0.1441E 04	-0.6654E 04	-0.6654E 04	
0.0450	-78.55	-235.06	-1.12	-0.1434E 05	12.98	-0.1441E 04	-41.11	-0.1441E 04	-0.7149E 04	-0.7149E 04	
0.0500	-79.99	-343.51	-1.39	-0.1339E 04	13.11	-0.1441E 04	-41.57	-0.1441E 04	-0.3811E 04	-0.3811E 04	
0.0550	-81.93	-458.26	-1.75	-0.1242E 05	13.36	-0.1441E 04	-42.13	-0.1441E 04	-0.6317E 04	-0.6317E 04	
0.0600	-84.57	-564.73	-2.27	-0.1124E 05	13.74	-0.1441E 04	-42.84	-0.1441E 04	-0.1115E 05	-0.1115E 05	
0.0650	-87.18	-421.13	-3.06	-0.1017E 06	14.25	-0.1441E 04	-43.83	-0.1441E 04	-0.1637E 05	-0.1637E 05	
0.0700	-88.23	8.55	-4.18	-0.0944E 05	14.89	-0.1441E 04	-45.20	-0.1441E 04	-0.1909E 05	-0.1909E 05	
0.0750	-87.15	358.85	-5.65	-0.0838E 05	15.64	-0.1441E 04	-47.06	-0.1441E 04	-0.1358E 05	-0.1358E 05	
0.0800	-85.05	482.18	-7.59	-0.0716E 05	16.34	-0.1441E 04	-49.48	-0.1441E 04	-0.1343E 05	-0.1343E 05	
0.0850	-82.50	514.98	-9.91	-0.0607E 05	17.04	-0.1441E 04	-52.43	-0.1441E 04	-0.2375E 05	-0.2375E 05	
0.0900	-80.22	383.58	-12.31	-0.0504E 05	17.81	-0.1441E 04	-55.87	-0.1441E 04	-0.1758E 05	-0.1758E 05	
0.0950	-78.65	242.14	-14.46	-0.0422E 05	18.78	-0.1441E 04	-59.80	-0.1441E 04	-0.1434E 05	-0.1434E 05	
0.1000	-77.70	-64.58	-17.36	-0.0342E 05	21.23	-0.1441E 04	-67.96	-0.1441E 04	-0.2546E 05	-0.2546E 05	
0.1050	-76.45	-235.18	-18.19	-0.0290E 05	21.72	-0.1441E 04	-69.92	-0.1441E 04	-0.8109E 05	-0.8109E 05	
0.1100	-90.08	-422.48	-18.67	-0.2922E 05	21.71	-0.1441E 04	-69.92	-0.1441E 04	-0.1061E 06	-0.1061E 06	
0.1150	-82.34	430.53	-18.93	-0.3094E 05	21.97	-0.1441E 04	-69.92	-0.1441E 04	-0.6814E 04	-0.6814E 04	
0.1200	-83.89	-151.44	-19.86	-0.2739E 05	22.31	-0.1441E 04	-69.92	-0.1441E 04	-0.6655E 04	-0.6655E 04	
0.1250	-83.98	62.76	-21.72	-0.2152E 04	22.54	-0.1441E 04	-69.92	-0.1441E 04	-0.5602E 04	-0.5602E 04	
0.1300	-83.44	140.05	-24.28	-0.1347E 05	22.85	-0.1441E 04	-69.92	-0.1441E 04	-0.6495E 04	-0.6495E 04	
0.1350	-82.72	144.47	-27.24	-0.0915E 04	23.28	-0.1441E 04	-68.37	-0.1441E 04	-0.2197E 04	-0.2197E 04	
0.1400	-82.18	44.04	-30.29	-0.0615E 03	23.79	-0.1441E 04	-68.37	-0.1441E 04	-0.6495E 04	-0.6495E 04	
0.1450	-82.28	-82.39	-33.00	-0.0412E 05	24.37	-0.1441E 04	-67.86	-0.1441E 04	108.12	0.3680E 04	
0.1500	-82.96	-183.27	-35.29	-0.0270E 05	25.02	-0.1441E 04	-67.29	-0.1441E 04	122.20	0.2454E 04	
0.1550	-84.06	-253.16	-37.12	-0.1033E 05	25.70	-0.1441E 04	-65.97	-0.1441E 04	132.71	0.1632E 04	
0.1600	-85.43	-288.43	-36.46	-0.2960E 04	26.40	-0.1441E 04	-65.27	-0.1441E 04	138.52	0.5507E 03	
0.1650	-86.89	-292.03	-39.31	-0.7869E 03	27.08	-0.1441E 04	-65.27	-0.1441E 04	139.52	0.2799E 03	
0.1700	-88.33	-285.40	-39.70	-0.1597E 04	27.68	-0.1441E 04	-64.57	-0.1441E 04	141.90	0.6093E 03	
0.1750	-89.75	-280.38	-39.66	-0.2504E 03	28.11	-0.1441E 04	-63.12	-0.1441E 04	144.87	0.5201E 03	
0.1800	-91.12	-249.69	-39.28	-0.2625E 05	28.30	-0.1441E 04	-63.12	-0.1441E 04	146.98	0.3230E 03	
0.1850	-91.88	-12.26	-39.08	-0.6930E 05	28.26	-0.1441E 04	-62.38	-0.1441E 04	148.76	0.5010E 03	
0.1900	-91.17	257.35	-39.74	-0.3939E 05	28.02	-0.1441E 04	-61.62	-0.1441E 04	152.85	0.1267E 04	
0.1950	-89.51	352.66	-41.14	-0.1117E 05	27.55	-0.1441E 04	-60.24	-0.1441E 04	157.75	0.9652E 03	
0.2000	-87.91	285.51	-42.52	-0.1511E 05	26.94	-0.1441E 04	-59.21	-0.1441E 04	163.24	0.1220E 04	
										169.47	0.1259E 04

Table XXX. Selected Printout. Example No. 5 (page 3 of 9)

TWO DIMENSIONAL CRASH VEHICLE SIMULATION OUTPUT DATA
VEHICULAR MOTION BODY MOTION AT HUP JOINT

TIME	POSITION (IN.)	VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)	RELATIVE DISPL. (IN.)	HORIZONTAL VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)	RELATIVE DISPL. (IN.)	VERTICAL VELOCITY (IN./SEC.)	ACCEL. (G-UNITS)
0.0	0.0	0.0	0.0	0.0	0.0	0.144	0.0	0.0	0.080
0.0050	0.005	3.22	3.33	-0.005	0.26	0.117	0.000	0.15	0.075
0.0100	0.043	12.38	6.667	-0.043	0.48	0.112	0.001	0.29	0.065
0.0150	0.145	28.98	10.000	-0.139	0.63	0.113	0.003	0.40	0.047
0.0200	0.333	45.08	6.667	-0.323	0.94	0.483	0.005	0.46	-0.088
0.0250	0.585	54.74	3.333	-0.564	4.62	3.647	0.006	-0.48	-0.961
0.0300	0.869	57.35	0.0	-0.804	13.16	2.700	-0.001	-1.63	3.192
0.0350	1.163	60.38	2.509	-1.010	22.87	9.026	-0.003	0.98	-2.505
0.0400	1.481	67.65	5.017	-1.133	35.42	11.004	-0.009	4.18	-2.941
0.0450	1.848	79.77	7.526	-1.333	51.32	8.901	0.037	6.91	1.690
0.0500	2.287	96.73	10.035	-1.472	69.42	10.069	0.081	10.56	2.150
0.0550	2.823	118.54	12.543	-1.611	90.17	11.528	0.144	14.99	2.149
0.0600	3.481	145.20	15.052	-1.700	113.66	13.302	0.223	18.40	1.027
0.0650	4.278	173.73	14.482	-1.925	139.80	14.239	0.328	21.26	1.649
0.0700	5.216	201.16	13.913	-2.092	169.37	7.982	0.449	30.24	17.586
0.0750	6.288	227.49	13.344	-2.237	201.45	9.123	0.639	44.39	16.172
0.0800	7.489	252.72	12.775	-2.347	234.19	21.552	0.885	54.21	-0.713
0.0850	8.814	276.85	12.205	-2.414	268.92	16.970	1.174	60.93	3.984
0.0900	10.256	299.88	11.636	-2.474	308.67	13.606	1.474	57.40	6.542
0.0950	11.810	321.81	11.067	-2.325	346.47	14.821	1.735	46.66	-5.667
0.1000	13.472	342.64	10.498	-2.202	363.35	3.117	1.952	41.30	-1.329
0.1050	15.235	362.38	9.928	-2.142	364.43	-1.391	2.152	38.99	-1.446
0.1100	17.094	381.01	9.359	-2.142	383.57	12.811	2.319	25.01	-10.939
0.1150	19.043	398.54	8.790	-2.115	405.62	9.926	2.396	8.74	-5.599
0.1200	21.078	414.97	8.220	-2.062	429.81	11.980	2.432	6.80	1.351
0.1250	23.191	430.30	7.651	-1.969	452.22	10.089	2.464	3.93	-4.469
0.1300	25.379	444.53	7.082	-1.849	470.47	9.214	2.464	-3.87	-5.250
0.1350	27.635	457.67	6.513	-1.712	485.72	6.501	2.426	-10.39	-1.795
0.1400	29.954	469.70	5.943	-1.571	497.96	5.928	2.364	-14.87	-2.574
0.1450	32.330	480.63	5.374	-1.431	508.45	4.828	2.278	-19.49	-2.141
0.1500	34.758	490.46	4.805	-1.295	516.87	3.806	2.171	-23.14	-1.558
0.1550	37.233	499.20	4.235	-1.168	523.40	2.880	2.043	-25.51	-0.768
0.1600	39.748	506.83	3.666	-1.054	528.29	2.110	1.918	-26.33	-0.076
0.1650	42.299	513.36	3.097	-0.954	531.42	1.015	1.788	-25.26	1.457
0.1700	44.880	518.80	2.528	-0.875	532.42	-0.065	1.672	-20.77	3.394
0.1750	47.485	523.13	1.958	-0.820	531.52	1.586	1.586	-12.76	4.880
0.1800	50.109	526.36	1.389	-0.791	529.59	-1.029	1.547	-3.14	4.736
0.1850	52.747	528.50	0.820	-0.785	527.76	-0.785	1.552	4.80	3.153
0.1900	55.393	529.53	0.250	-0.736	525.79	-0.975	1.594	12.62	4.078
0.1950	58.041	529.64	0.0	-0.819	524.85	0.114	1.673	18.51	1.804
0.2000	60.689	529.64	0.0	-0.842	525.29	0.333	1.774	21.61	1.476

Table XXX. Selected Printout. Example No. 5 (page 4 of 9)

OUTPUT DATA BELT FORCES (LBS),

TWO DIMENSIONAL CRASH VICTIM SIMULATOR

ACCELEROMETER READINGS

TIME	HEAD		CHEST		LAP	SHOULDER RESTRAINT		AT HIP	AT FRONT EDGE
	RESULTANT (G-UNITS)	ANGLE (DEG.)	RESULTANT (G-UNITS)	ANGLE (DEG.)		LOWER	UPPER		
0.0	0.3	-47.4	0.1	-179.2	0.0	0.0	145.00	0.0	0.0
0.0050	0.3	-48.2	0.2	-179.7	0.0	0.0	144.56	0.0	0.0
0.0100	0.3	-50.4	0.2	-177.2	0.0	0.0	143.44	0.0	0.0
0.0150	0.3	-54.7	0.2	-172.3	0.0	0.0	141.56	0.0	0.0
0.0200	0.2	7.4	0.3	-22.4	0.0	0.0	139.42	0.0	0.0
0.0250	0.6	55.9	2.3	-24.9	0.0	0.0	139.01	0.0	0.0
0.0300	5.5	72.2	5.6	39.0	0.0	0.0	140.11	0.0	0.0
0.0350	0.9	49.1	7.6	-26.3	0.0	0.0	137.51	0.0	0.0
0.0400	0.7	-17.6	3.2	-27.1	0.0	0.0	133.73	0.0	0.0
0.0450	3.3	59.4	8.6	7.6	0.0	0.0	129.76	0.0	0.0
0.0500	2.1	26.1	3.2	8.4	0.0	0.0	124.01	0.0	0.0
0.0550	3.7	-50.6	3.2	4.5	0.0	0.0	116.44	0.0	0.0
0.0600	8.8	-66.1	8.7	-8.0	0.0	0.0	108.71	0.0	0.0
0.0650	11.2	-59.9	8.7	-5.3	0.0	0.0	100.79	0.0	0.0
0.0700	8.1	57.2	12.1	60.2	0.0	0.0	85.94	0.0	0.0
0.0750	7.0	15.8	21.1	56.0	0.0	0.0	62.72	0.0	0.0
0.0800	27.2	-46.7	20.3	-26.0	0.0	0.0	40.26	0.0	0.0
0.0850	20.7	-29.4	13.3	11.7	0.0	0.0	17.48	0.0	0.0
0.0900	17.4	-10.7	15.3	67.6	0.0	0.0	3.09	0.0	0.0
0.0950	25.6	-14.7	10.4	-21.1	0.0	0.0	0.0	0.0	0.0
0.1000	24.3	-3.2	11.9	3.8	0.0	0.0	0.0	0.0	0.0
0.1050	24.7	5.4	10.6	17.6	0.0	0.0	0.0	0.0	0.0
0.1100	26.3	32.7	21.9	-10.3	0.0	0.0	0.0	0.0	0.0
0.1150	40.4	61.4	20.4	10.1	0.0	0.0	0.0	0.0	0.0
0.1200	46.6	67.0	13.2	14.8	0.0	0.0	0.0	0.0	0.0
0.1250	19.4	39.2	15.6	9.2	0.0	0.0	0.0	0.0	0.0
0.1300	19.2	36.0	17.5	3.7	0.0	0.0	0.0	0.0	0.0
0.1350	19.6	31.9	11.5	4.3	0.0	0.0	0.0	0.0	0.0
0.1400	17.6	36.4	12.3	3.3	0.0	0.0	0.0	0.0	0.0
0.1450	16.2	37.7	5.7	-0.8	0.0	0.0	11.46	0.0	0.0
0.1500	15.0	35.6	7.4	-6.8	0.0	0.0	25.06	0.0	0.0
0.1550	14.1	26.3	5.2	-14.7	0.0	0.0	39.06	0.0	0.0
0.1600	14.6	5.6	2.3	-29.2	0.0	0.0	52.42	0.0	0.0
0.1650	18.8	-23.4	0.4	2.9	0.0	0.0	64.17	0.0	0.0
0.1700	26.7	-47.7	1.6	120.1	0.0	0.0	73.30	0.0	0.0
0.1750	34.1	-66.4	3.9	132.4	0.0	0.0	77.31	0.0	0.0
0.1800	35.9	-82.7	5.1	148.5	0.0	0.0	75.03	0.0	0.0
0.1850	30.2	-98.4	8.0	170.2	0.0	0.0	67.80	0.0	0.0
0.1900	17.2	-116.6	3.1	164.2	0.0	0.0	59.19	0.0	0.0
0.1950	17.1	-133.9	3.4	-153.1	0.0	0.0	48.24	0.0	0.0
0.2000	13.4	-155.1	3.6	-130.3	0.0	0.0	36.64	0.0	0.0
							26.25	0.0	0.0

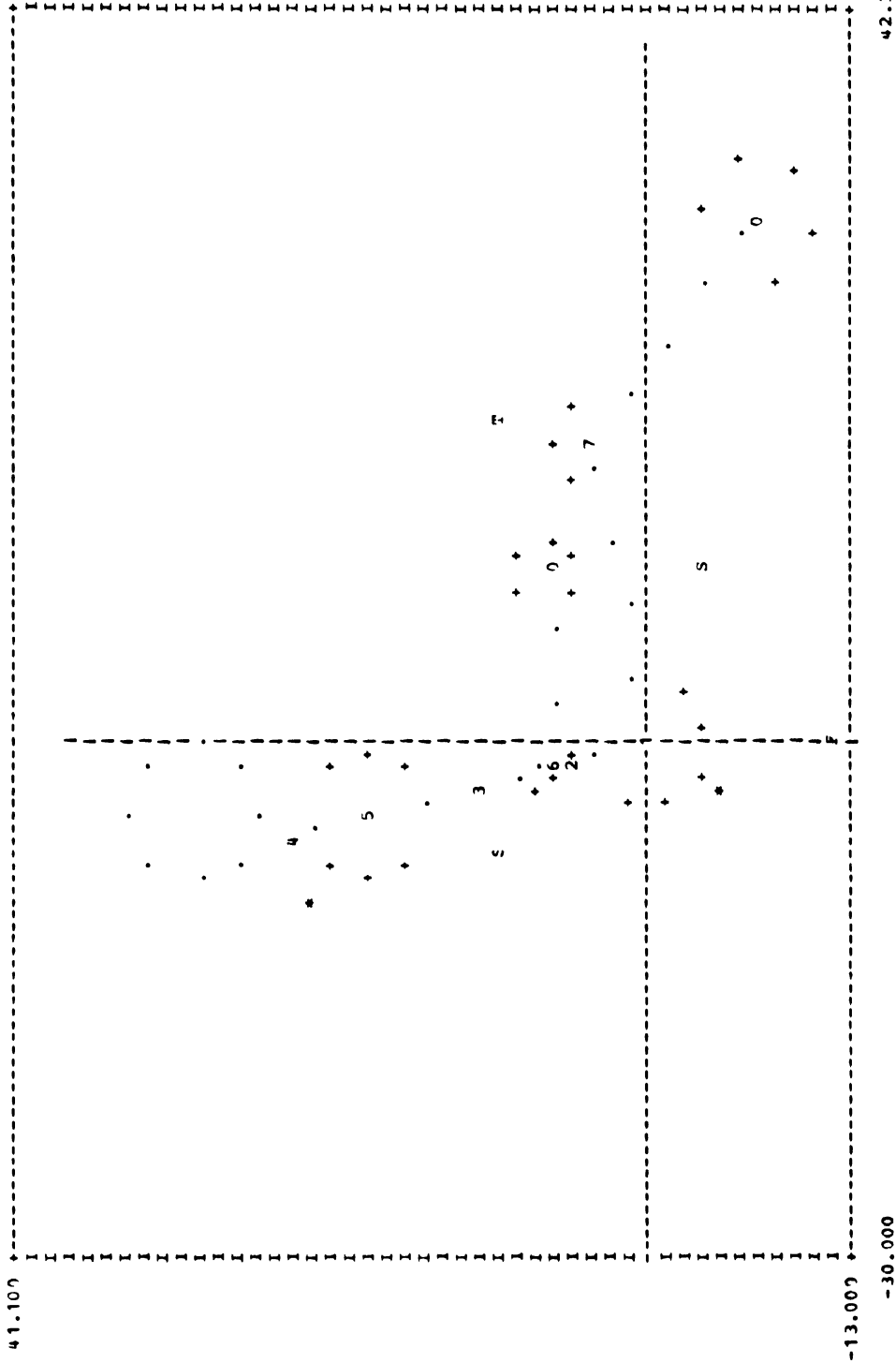
Table XXX. Selected Printout. Example No. 5 (page 5 of 9)

TWO DIMENSIONAL BEARD VICTIM SIMULATOR OUTPUT DATA

TIME	TOE BOARD ON	HEEL ON	SEAT BACK ON	UP. SEAT BACK ON	UPPER TORSO ON	CONTACT FORCES (LBS.)	OUTPUT DATA	ELBOW ON	SEAT BACK ON	FOOT ON	FLOOR ON
0.0	32.9	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0050	6.3	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0100	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0150	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0200	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0250	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0300	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0350	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0400	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0450	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0500	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0550	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0600	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0650	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0700	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0750	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0800	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0850	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0900	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.0950	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1000	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1050	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1100	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1150	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1200	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1250	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1300	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1350	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1400	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1450	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1500	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1550	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1600	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1650	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1700	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1750	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1800	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1850	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1900	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.1950	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0
0.2000	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0

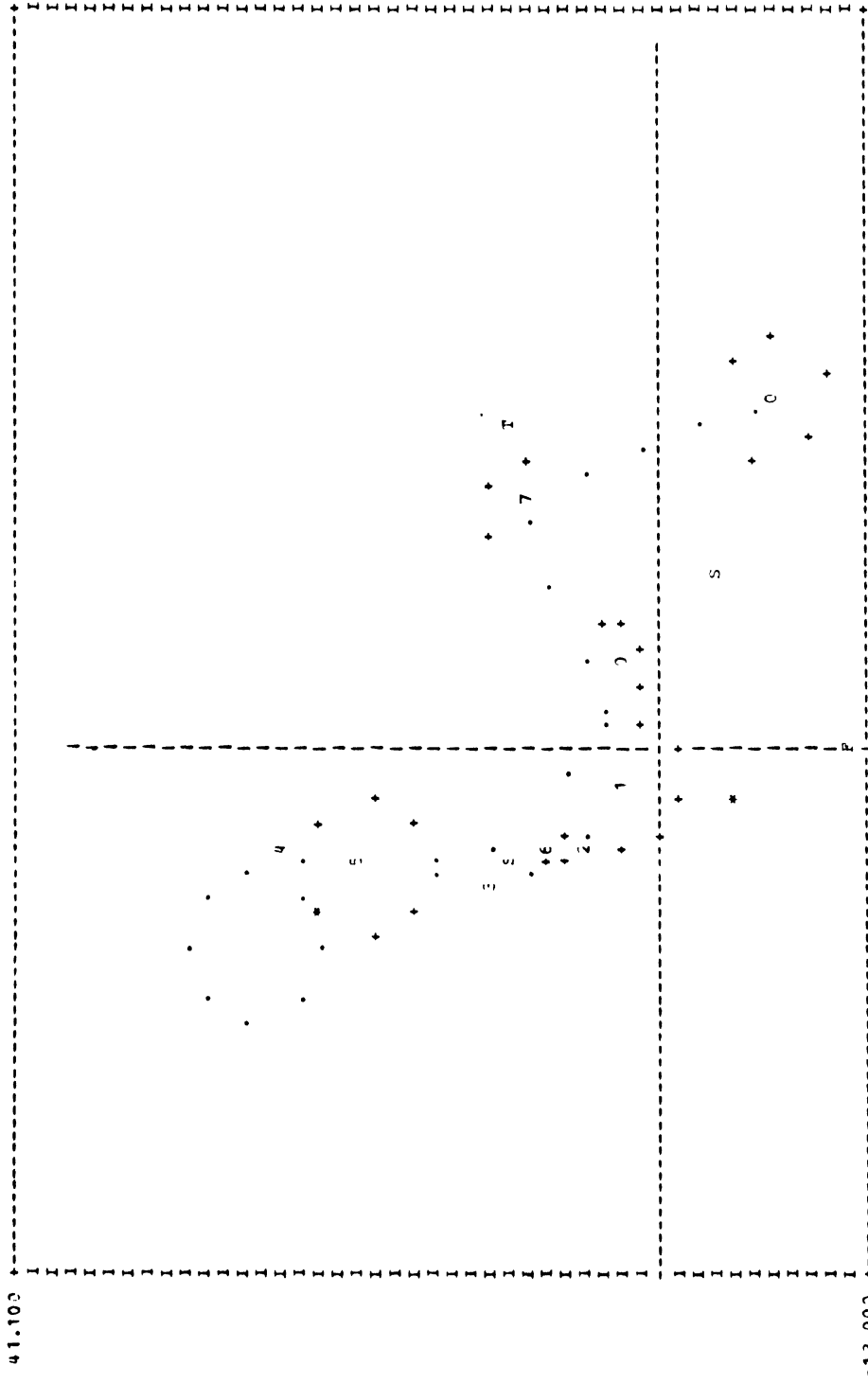
Table XXX. Selected Printout. Example No. 5 (page 6 of 9)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.0 SECONDS



INDICATED MEASUREMENTS ARE IN INCHES
SCALING FACTORS: 1 TO 7.09 IN THE X DIRECTION
 1 TO 7.06 IN THE Y DIRECTION

Table XXX. Selected Printout. Example No. 5 (page 7 of 9)



-30.000

42.300

INDICATED MEASUREMENTS ARE IN INCHES
 SCALING FACTORS: 1 TO 7.0 IN THE X DIRECTION
 1 TO 7.05 IN THE Y DIRECTION

Table XXX. Selected Printout. Example No. 5 (page 8 of 9)

TWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT DATA
STICK FIGURE REPRESENTATION FOR TIME = 0.200 SECONDS

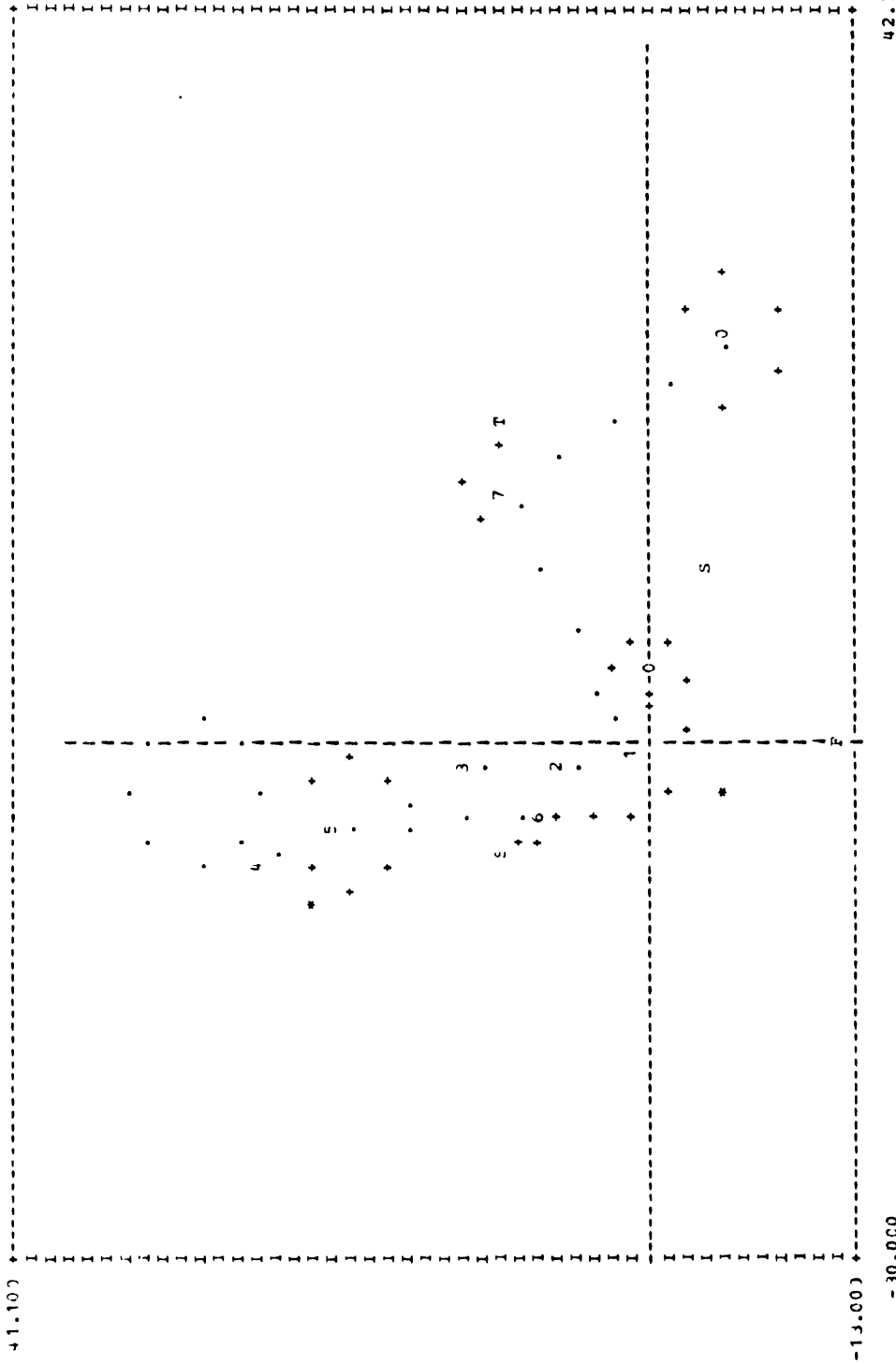


Table XXX. Selected Printout. Example No. 5 (page 9 of 9)

D. GENERAL PROGRAM OUTPUT

The program printout consists of the following parts: executive system printout, listing of input cards read (up to Z-card), allowable contact specifications, digest of input data, intermediate general printout with various possible debugging options, and tabular summary.

There are four levels of debugging printout provided in the program. The first level of printout, consisting only of normal summary printout, is always printed upon program execution. The other levels (IBUG = 1, 2, 3) are set up using the input data cards labeled "V." Because of the piecewise-linear nature of information inputted to the computer program using "V-cards" it is possible to isolate small time segments within the forward integration period covered by the simulation and produce detailed debugging printout as needed.

Although variable levels of debugging printout are specified only by piecewise linear sections, only integer values of IBUG have meaning, so the best practice is to use a very small time step between the integer values of IBUG. A sample of the "V card" input is given in Table XXXI and graphed in Figure 42.

If a print time occurs while IBUG is a linear ramp, some intermediate IBUG printout will occur (IBUG = 1, 2) as the values are rounded off approximately to integer values.

The first item printed out after the executive system printout is a listing of the input data file up to the Z card. After this comes a table of the permissible contacts for the NPASGR option selected. "NS" is the total number of contacts and the next two lines give the indices of the body segment and its corresponding allowed contact surface (see Table XV).

TABLE XXXI. SAMPLE V CARD DEBUG INPUT DATA SET

Data Card Column	1	11	21	31
Information on each data card	V2.	1.	0.	0.
	V2.	1.	0.099	0.
	V2.	1.	0.100	3.
	V2.	1.	0.149	3.
	V2.	1.	0.150	0.
	V2.	1.	0.200	0.

It should also be noted that contact forces are labeled by the following scheme in printouts from subroutines LODFEC and CONTAC (see Table XXXII). Indices 1, 2, and 3 are belts (lap, lower shoulder harness, upper shoulder harness). Index 4 is vestigial. The index pairs listed under I and A are labeled from 5 through a maximum of 18 (see Table XVI).

The input data follows the listing of the contacts. These variables are described in Part IV, Section A of this paper. The surface index A is printed one greater than the listing in Table VII. For example, A = 1 is the floor index whereas the value in the table is zero.

Intermediate general printout can be described by a table and a list of accompanying comments. Table XXXII consists of the debug level, the subroutine generating the output, and the variables included in each output group and Table XXXIII lists specific comments which are generated by the program indicating certain error conditions and other aspects of program function.

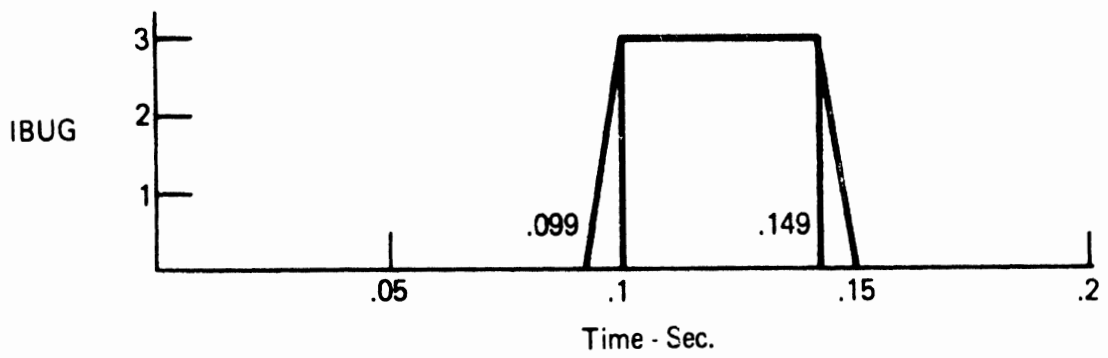


Figure 42. Description of time-varying debug table.

TABLE XXXII. INTERMEDIATE GENERAL PRINTOUT (page 1)

Debug Level* (and debug printout number)	Routine	Label	Contents
0 (1)	MAIN	--	Number of contact surfaces (NS), index of contact arcs (I), index of contact surfaces (A) (see note on Table XXXIII)
0 (2)	MAIN	--	Output of input (See Part IV. A of report) (see note on Table XXXIII)
0 (3)	KRUNCH	IGNORE	Switch indicating status of the contact surfaces (+1 = no contact, -1 = no friction, 0 = friction)
1 (4)	GETY	--	Present time (ARG), time modulo 24 (MOD ARG), table number (TABLE), ordinate (ORD)
3 (5)	ACCEL	STEP	$\sin \theta_1, \cos \theta_1, \theta_1^2, L_1 \theta_1^2, a_1 \theta_1^2$ in five columns for $i = 1-8$ in eight lines. (L = in.) ($\theta = \text{rad}$)*. Quantity "a" is matrix parameter.
2 (6)	SEAT	SEAT	Z (in) (distances from hip to front of seat) FS (Fs) (lb) (hip seat force) FSPRM (F's) (lb) (front edge seat force) FZ (Fz) (lb) (force on front seat) SMALLF (f) (lb) (friction force magnitude) SUMBY ($\beta_1 y_s + \beta_2 y_s^2 + \beta_3 y_s^3$) (lb) (non-linear hip force) ZMLCTS ($z - L_7 \cos \theta_7$) (in.) (distance from knee to front of seat)

*($a_1 = 1 \text{ lb in. for } i = 1-8, 1 \text{ lb for } i=9, 1 \text{ lb in.}^2 \text{ for } i = 10-17.$)

*NOTE: The terms "Debug Level" and "IBUG value" are equivalent throughout this report.

TASLE XXXII. INTERMEDIATE GENERAL PRINTOUT (page 2)

Debug Level	Routine	Label	Contents
1 (7)	LODFEC	LODFEC	N (index of force) (See Table XVI and text above) SDL (δ) (in.) (deflection) SDLD ($\dot{\delta}$) (in./sec) (deflection rate) PN (F) (lb) (contact force) ET (E) (in. lb) (energy since last unloaded cycle) EPSLNT (ϵ) (in.) (permanent deformation)
2 (8)	CONTAC	CONTAC	N (index of contact) DELOA (δ) (in.) (deflection) DELIAD ($\dot{\delta}$) (in./sec) (deflection rate) PN (F) (lb) (force) EONE (E_1) (in. lb) (total conserved energy) EPSLNY (ϵ) (in.) (permanent deformation)
2 (9)	CONTAC	QUE VECTOR	QUE (Subscript I = 1-10 referring to the body segments (1-8) as defined in Table IX and the x-y coordinates of the hip. Units for subscripts 1-8 are in. lb and for 9-10 are lb) (Contribution to generalized force vector of contact surfaces is defined in Table XV.)
2 (10)	BODY	BODY	I (index for each line defined as QUE subscripts) GEE (gravitational contribution to generalized force vector) DEE (contribution of seat bottom and belts) BEE (contribution of centrifugal forces) SMALLB (total generalized force vector)
2 (11)	ZMAKER	A MATRIX	AA (doubly subscripted matrix of differential equations. Rows possess units defined in QUE)
2 (12)	ZMAKER	A INVERSE	ANVERS (doubly subscripted inverse of AA)
2 (13)	ZMAKER	CHECK OF INVERSE	CK ($A^{-1}A + AA^{-1}$) (check of inversion routing)

TABLE XXXII. INTERMEDIATE GENERAL PRINTOUT (page 3)

Debug Level	Routine	Label	Contents
1 (14)	DELZMK	DELZMK	A subscription comment "FOR MODE No. (K), I = (I), A = (A)" K (Index of jittering friction mode. For K = 1-7, index refers to joint. For K = 8, index refers to seat cushion. For K = 9,..., index is k + 4, see page 26. DELZ (J,K) This doubly subscripted vector shows the change in acceleration vector (J = 1-10) due to an instability (K = 1...)
1 (15)	KRUNCH	ZK BASE	ZVECPP (acceleration vector due to continuous forces and unstable friction forces. Subscripts refer to angular coordinates (1-8), linear coordinates (9-10), and vehicle (11). Units are rad/sec ² and in./sec ²)
1 (16)	KRUNCH	TIME IMAX	Time since beginning of collision event. MAXI (number of possible instabilities) IBIG (listing of possible unstable modes with subscript I = 1...MAXI)
1 (18)	JITTER	I AK	I (index of averaging pair) AK (weighted averaging coefficient used in eliminating instabilities)
1 (17)	JITTER		Comment: MODE (index) TURNED ON (or OFF) or JITTER FOR MODE (index)
1 (19)	JITTER	ZRV = ZPPP = DELNU = FMM =	Relative acceleration from ZKBASE for mode N Relative acceleration from previous averagings Relative acceleration from DELZMK (K = 7) Slope of vehicle deceleration (in./sec ³) These quantities are largely vestigial

TABLE XXXII. INTERMEDIATE GENERAL PRINTOUT (page 4)

Debug Level	Routine	Label	Contents
1 (20)	TAUMAK	TAUMAK	ITAU (i) (index of jittering friction contact) TAUHAT (i) (selected time interval) TAUI (all predicted time intervals) (I = 1-16, in two lines)
1 (21)	TAUMAK	MODE	MODE (Switch array stating whether each friction mode (1-16) is on (+1), off (-1), or unstably jittering (0).)
3 (22)	LIMIDT	LIMIDT	I (index) AZ (rad or in.) (predicted angular position of body elements, 1-8, x and y hip position 9-10, and cart location 11) AZP (rad/sec or in./sec) (associated velocities) AX (in.) (Horizontal joint coordinates. Note index 8 refers to knee and both 1 and 7 to the hip joint here only) AY (in.) (vertical joint coordinates) AXD (in./sec) (horizontal joint velocity) AYD (in./sec) (vertical joint velocity)
1 (23)	FECLOD	FECLOD	TIME (sec) (time) INDEX (index of contact force checked) SDEL (in.) (predicted deflection) SDELD (in./sec) (predicted deflection rate) FTT (lb) (predicted contact force)
1 (24)	NORMUT	AT TIME THETA XHIP YHIP XCAR	TIME (sec) ZVEC (deg) (angular position of body elements 1-8) ZVECP (deg/sec) (angular velocities) ZVECPP (deg/sec ²) (angular accelerations) ZVEC, ZVECP, ZVECPP (in., in./sec, in./sec ²) (9-12) (position, velocity, and acceleration of hip in x and y directions and of the vehicle)

TABLE XXXII. INTERMEDIATE GENERAL PRINTOUT (page 5)

Debug Level	Routine	Label	Constants
1 (24)	NORMUT	TIME FS FSPRM SMALLF	TIME (sec) FS (lb) (seat bottom force on hip) FSPRM (lb) (force at front edge of seat bottom) SMALLF (lb) (friction force from seat bottom)
1 (24)	NORMUT	X Y A GAMMA	XHEAD, XCHEST (in./sec ²) (horizontal acceleration of head and chest c. g.) YHEAD, YCHEST (in./sec ²) (vertical acceleration of head and chest c. g.) AHEAD, ACHEST (in./sec ²) (resultant acceleration of head and chest) GHEAD, GCHEST (deg) (angle of resultant acceleration vector)
1 (24)	NORMUT	M DELTA DELTA DOT FM PHI EIM EPSILON DEM	Index of belt segment: seat belt (1) upper shoulder (2), lower shoulder (3). SDELTA (in.) (elongation of belt) SDELTD (in. sec) (rate of belt elongation) FN (lb) (belt force) PHI (deg) (belt angle) EONE (in./lb) (total energy conserved in belt) EPSLNY (in.) (permanent belt deformation)
1 (25)	KRUNCH	RVEL	MAXR (present number of friction modes being considered) RVEL (rad/sec, in./sec) (relative velocity for the friction modes being considered) RSEL (rad/sec ² , in./sec ²) (relative acceleration for friction modes considered)
1 (26)	KRUNCH	KRUNCH A	KPRINT (print switch) KINFL (inflection switch) KSTED (maximum time step switch) ITAU (mode selected) TAUHAT (sec) (minimum predicted mode time) TPRINT (sec) (next print time) TINFL (sec) (next inflection time) TSTEP (sec) (last inflection time) DELTAT (sec) (time step selected) TIME (sec) (new time)

TABLE XXXIII. PROGRAM COMMENTS (page 1)

Subroutine	Comment	Conditions
GETY	TABLE ____ HAS NO ENTRIES AND CALLED UPON	empty table
GETY	TABLE ____ MINX = ____. EXCEEDED BY ARG ____ Y SET TO ____	off low end of table
GETY	TABLE ____ MAXX = ____ EXCEEDED BY ARG ____. Y SET TO ____	off high end of table
LODFEC	CHANGED R FROM ____ TO ____ FOR INDEX ____	R, G, not compatible
LODFEC	RESET CONSERVED ENERGY TO LOWER LIMIT AT T = __ SEC	R reset lower
LODFEC	RESET CONSERVED ENERGY TO UPPER LIMIT AT T = __ SEC	R reset higher
LODFEC	CHANGED G FROM ____ TO ____ FOR INDEX ____	R, G not compatible
LODFEC	OUTSIDE MONOTOMIC RANGE OF LOADING CURVE FOR INDEX N =	during loading part of cycle $F(t) < F(t - \Delta t)$
ZMAKER	BAD MATRIX. DUMP	determinant of matrix = 0
JITTER	TWO LINEAR JITTER MODES AT T = _____	2 contact friction jitter modes want to jitter at same time (fatal)
LIMIDT	AT TIME = _____ DELTA T = _____ RESET TO _____	some forward contact forces predicted to change by $> 1000\%$
LODFEC	NEGATIVE FORCE SET TO ZERO FOR INDEX N = ____ AT TIME = _____	during loading part of cycle $F(t) < 0$; set equal to zero.

TABLE XXXIII. PROGRAM COMMENTS (page 2)

Subroutine	Comment	Conditions
TAUMAK	RESET MODE (_____) TO ZERO	Indicates jitter mode selected
KRUNCH	AT TIME = _____, ANGLE _____ EXCEEDS 360 DEGREES	$ \theta_1 > 360^\circ$ (fatal)
KRUNCH	AT TIME = _____, MORE THAN EIGHT ITEMS IN JITTER RUN STOPPED	Space allotted to storage for jitter process would be exceeded (fatal)
FECLD	AT TIME = _____ FORCE COMING ON FROM BEHIND FOR INDEX _____	fatal
MAIN	ILLEGAL CARD SKIPPED. _____	Data card with illegal value or ID column is printed, processing continues.
ZMAKER	LARGE CHANGE IN ACCELERA- TION AT TIME=_____ LOOK FOR PURIOUS FORCE.	Probably a contact circle has slid in behind a contact line.
LODFEC	NEGATIVE PERMANENT DEFORMA- TION PREDICTED FOR INDEX _____	Saturation has occurred and bad value of unloading slope provided.

E. USE OF HSRI MODEL IN COMNET SYSTEM FROM DATA 100 TERMINAL

Preparing the Input Card Deck

When a data set has been produced according to the HSRI two-dimensional model report, it is preceded by the cards described in Table XXXIV and followed by the cards described in Table XXXV. The small letter "b" represents a blank column in these tables.

TABLE XXXIV. CONTROL CARDS APPEARING BEFORE THE DATA DECK

<u>Card No.</u>	<u>Card Contents</u>
1	..bRJSTARTbRG00XXXX
2	..bL0G0NbXXX,XXX
3	..bJEDbCENTRAL=ALL (if delivered or held for pickup)
	<u>or</u>
	(no card if user waits for output on Data 100)
	<u>or</u>
	..bJEDbOUTPUT=DEFER (if output to be retrieved using Data 100 at a later time)
4	//GXXXXPPbJ0Bb(ACCNUB,DEL/B0X,N,TW0DRUN,R), 'yourname',TIME=3,
5	//0bPRTY=m
6	//G0bEXECbPGM=M0DEL2,REGI0N=242K
7	//STEPLIBbDDbDSN=DS.G21601.HSRI2D,DISP=SHR
8	//FT05F001bDDbDDNAME=SYSIN
9	//FT06F001bDDbSYS0UT=A,DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
10	//FT09F001bDDbDSNAME=DS.G21601.H0LDIT,DISP=0LD
11	//SYSINbDDb*

TABLE XXXV. CONTROL CARDS APPEARING AFTER THE DATA DECK

<u>Card No.</u>	<u>Card Contents</u>
1	/*
2	..bLGGOFF
3	..bRJEND

Card One in Table XXXIV identifies the DATA 100 from which you are working to the COMNET system. Card Two identifies your account for terminal charges. Card Three chooses the output option you desire. Card Four identifies you to the executive system which runs the COMNET computer. The "X's" in cards one, two and four will be provided by COMNET when you have established service with them. The P's represent values which are to be filled in by the user uniquely for this run. ACCNUB is filled in with up to 20 character of accounting break out information (optional). If you have a three character box number and want the output held in the box for pickup the box number is filled in at DEL/BOX. If not fill in DEL or DIS for delivery. Cards five through eleven tell the system where to find the model program and describe its requirements from the system. Card one of Table XXXV marks the end of the data deck.

Card two breaks the connection for your account.

Card three causes the COMNET System to hang up on the terminal.

Using the Data 100 to Put in Prepared Deck

1. Power On - your unit and check to see that the printer forms are aligned correctly, and that there is enough paper.
2. Turn the mode switch to TSM.
3. Press RESET.

4. Press START on the printer.

5. Place card deck in hopper and replace hopper top.

6. Press END OF FILE and TRSP.

7. If equipped with Bell System data set, depress the talk button and wait for dial tone. Dial COMNET number indicated on top of data set. When phone is answered, you will hear a high-pitched tone. Depress the data button on the top of the data set and place the receiver back in the cradle.

8. If equipped with a modem wired through a normal looking telephone set, first see that there is power to the modem unit. Then dial the COMNET number shown on the top of the modem. When phone is answered, you will hear a high-pitched tone. Pull up the white button and place the receiver beside the phone set.

9. When the DATA LINK ACTIVE light comes on, press START. If this light goes out, you have lost connection.

10. See the DATA 100 manual for error procedures and further information.

In order to recover over the data 100 output which has been deferred, use cards one and two of Table XXXIV followed by a card which reads:

```
..bOUTPUT*
```

Run those three cards through, wait until printing is done, and then put in cards two and three of Table XXXV. If you are interrupted during the printout for any reason, you can use the following card to start printing again.

```
..bCONTINUE
```

If you are hung up on, you will of course need to use also the first two cards in Table XXXIV again. If you have trouble getting your job accepted, one of the things you might try is putting in two of card one of Table XXXV instead of one. Be sure to keep changing the PP's on card four

so you have an unique combination for each run you try. Batch mode is the same as data 100 mode except you omit cards one through three in Table XXXIV, you have two of card one in Table XXXV and you omit cards two and three of Table XXXV. Also the "R" in card four of Table XXXIV should be changed to a "B". Contact COMNET Customer Support for further information on control cards.

F. TELETYPE USERS' GUIDE

This section is a technical guide for the user of the two-dimensional crash victim simulator who is familiar with MTS²⁷ and/or ALPHA and wishes to exercise the model from a teletype terminal remote from The University of Michigan and/or COMNET respectively. The control statements which cause the model to be exercised are described, followed by a description of the use of a conversational program which allows the user easy access to desired portions of the output generated in an exercise of the model.

Using the MTS system, the RUN statement for the two-dimensional crash victim simulator is

```
$RUN SCGH:2D 5=datafile 9=summary file SPRINT=*PRINT*
```

The terms "data file" and "summary file" refer to file names which must be supplied by the user. The input data for exercising the program, which has been described in Part IV, Section A of this report is stored in "data file." The output from the program must be stored in a file (referred to here as "summary file") which should be approximately 25 pages in length. This command will cause the model to run the problem specified in the data deck in "datafile" and route the printed output to The University of Michigan Computing Center for printing. If it is not desired to produce the output on paper at The University of Michigan Computing Center, then replace "SPRINT=*PRINT*" with "SPRINT=*DUMMY*".

The corresponding action in ALPHA is brought about by signing on with
userid, password, accountno, name, boxno

and then typing the two commands:

```
L0A inputdataset
```

```
EXE LFAA,LFAB,LFCA,TF3B,TFBA,LSAA,LSAC,LSAB,LFD,ASSEM0,ABSEMP,SERSEM,  
LSB,L0GSEM,GREGI0N=242K,TIME=8,M=3,DD=EXDD,SYISIN=*
```

The execute command is all on one line. When the job submitted is run, the output will be routed to the COMNET computer center for printing. The data set EXDD should contain one line which says

```
100 FT09F001 DD DSNAME=DS.G21601.H0LDIT,DISP=0LD
```

Because the complete output from one exercise of the program could take up to three hours to print out at a teletype terminal, it is necessary to provide a technique for accessing sections of the output quickly and conveniently. Use of the program which accomplishes this is described in the remainder of this section.

The program can also be used to retrieve information from the output of a previous run. In either case, the summary option must have been used in carrying out the exercise. The file in which the summary information is stored ("summary file") becomes the input file to the teletype output access program.

The program has three sections: "initial," "general," and "complex." The "initial" section enables the user to list any of 54 different input values which were used in carrying out the exercise. The "general" section, allows the user to list any of 61 different output variables over any time period. The "complex" section enables the user to make comparisons. When one variable reaches a critical value, the values of other variables can be determined.

The model is designed to be conversational with the user. However, the user is given the option of putting his instructions in a file.

The following commands will trigger execution of the program using MTS,

```
$RUN SCD4:TALK2 1 = summary file
```

or, if no conversation with the program is desired:

```
$RUN SP78:TALK2 1 = summary file 7 = *DUMMY* 4 = instruction file
```

The program will begin with

```
ENTER 6 IF CONVERSATIONAL, 7 IF NOT
```

If a 7 is entered, the program will proceed to get the rest of its information from the file specified on logical unit 4. If the end of this file is reached and the program has not been terminated, the program will return to conversational mode. If a 6 is entered, the program will proceed to prompt the user for instructions beginning with:

```
ENTER 1 IF INITIAL, 2 IF GENERAL, 3 IF COMPLEX, 4 IF DONE
```

Entering a 1, 2, or 3 will cause the program to go to the indicated section—each of which is described below, and a 4 will result in termination of the program.

In using the "initial" section of the teletype output access program, the user is prompted by the following:

```
1  ENTER VARIABLE NUMBER - 0 IF DONE
```

```
(    )
```

```
2  (    )
```

```
3  ENTER OCCUPANT POSITION NUMBER
```

Statement 1 indicates that the user should enter a number. The entry of a number from 1 to 54 results in the value of the corresponding input constant (as described in Tables XXXVI and XXXVII) being printed. Then,

the user is prompted for another number by a pair of parenthesis only.

This process can be discontinued at any time by entering a 0.

The first time that 4, 13, or 39 is entered, the user will be prompted with statement 3. A 1, 2, or 3 must be entered, corresponding to driver, front seat passenger or rear seat passenger. (This information is used only to make the titles more descriptive and does not change any of the numerical results.)

In using the "general" section of the teletype output access program, the user is prompted by the following:

1. HOW MANY VARIABLES
2. ENTER TIME INTERVAL
FROM () () ()
3. ENTER TIME INTERVAL
FROM () to ()
4. ENTER OCCUPANT POSITION NUMBER
5. ENTER VALUE OR "PHEAD"
6. ENTER VALUE OF "CHEST"

Statement 1 wants to know how many variables the user is interested in seeing. This number can be from 1 to 4. Statement 2 asks for the appropriate number of variable numbers. These numbers range from 1 to 61 and correspond to the variables as listed in Tables XXXVIII and XXXIX. If a 50 or 55 is entered, statement 4 will ask for the occupant position number. Enter 1 if driver, 2 if front seat passenger, or 3 if rear seat passenger. If a 44 or 45 is entered, statement 5 will ask for a value of "PHEAD." This is the distance from the neck joint to the location of the head accelerometer. If a 46 or 47 is entered for a variable number, statement 6 will

ask for the value of "PCHEST." This is the location of the chest accelerometer. After the variable numbers have been recorded, a time interval must be specified. A carriage return will result in initial values being printed. Any other time period must be specified in the appropriate spaces. (NOTE: If a contact that does not occur is asked for, the comment CONTACT NUMBER XX NEVER OCCURRED will be printed and the corresponding heading will be meaningless.)

In using the "complex" section of the teletype output access program, the user is prompted by the following:

1. ENTER DECISION VARIABLE
2. ENTER COMPARISON VALUE
3. ENTER COMPARISON MODE - 1 if GT, 2 if LT
4. HOW MANY VARIABLES?
5. ENTER VARIABLE NUMBERS
() () ()
6. ENTER TIME INTERVAL
FROM () to ()
7. ENTER OCCUPANT POSITION NUMBER
8. ENTER VALUE OF "PHEAD"
9. ENTER VALUE OF "PCHEST"

This section prints the values of variables at the time when another variable reaches a critical value. Any of the variables listed in Tables XXXVIII and XXXIX can be observed in this manner. For example, the user interested in the position of the head when it hits the windshield would make the following entries.

1. 56 (head on windshield is the decision variable)
2. 0 (0 is the critical value—we become interested when the force becomes greater than 0 (hence the 1).)

3. 1

4. 2

(NOTE: maximum is 3)

5. (39) (40)

6. (0.) to (2.0)

(Normally the time interval should cover the entire run, although some variables reach the critical point several times during the run and the time interval must be carefully chosen if you are not interested in the first occurrence.)

The user will be prompted by statements 7, 8, and 9 only in certain instances as described in a previous section.

The output of this section consists of the time at which the critical value was exceeded, along with the value of the decision variable and the other variables at that time.

TABLE XXXVI. INPUT CONSTANTS (NUMERIC ORDER) (page 1)

Number	Description
1	Floor-X
2	Seat Back-X
3	Roof-X
4	Upper Steering Wheel-X (When NPASGR=1) Upper Panel-X (When NPASGR=2) Front Seat Back-X (When NPASGR=3)
5	Windshield-X
6	Lower Steering Wheel-X
7	Lower Panel-X
8	Steering Column-X
9	Toeboard-X
10	Floor-Y
11	Seat Back-Y
12	Roof-Y
13	Upper Steering Wheel-Y (When NPASGR=1) Upper Panel-Y (When NPASGR=2) Front Seat Back-Y (When NPASGR=3)
14	Windshield-Y
15	Lower Steering Wheel-Y
16	Lower Panel-Y
17	Steering Column-Y
18	Toeboard-Y
19	Hip Contact Arc Radius
20	Upper Torso Contact Arc Radius
21	Head Contact Arc Radius
22	Elbow Contact Arc Radius
23	Hand Contact Arc Radius
24	Knee Contact Arc Radius
25	Foot Contact Arc Radius
26	To Chest Center of Curvature

TABLE XXXVI. INPUT CONSTANTS (NUMERICAL ORDER) (page 2)

Number	Description
27	To Head Center of Curvature
28	Lower Torso Length
29	Center Torso Length
30	Upper Torso Length
31	Center Torso to Upper Arm
32	Upper Arm Length
33	Lower Arm Length
34	Upper Leg Length
35	Lower Leg Length
36	Floor-Length
37	Seat Back-Length
38	Roof-Length
39	Upper Steering Wheel-Length (When NPASGR=1)
	Upper Panel-Length (When NPASGR=2)
	Front Seat Back-Length (When NPASGR=3)
40	Windshield-Length
41	Lower Steering Wheel-Length
42	Lower Panel-Length
43	Steering Column-Length
44	Toeboard-Length
45	Distance From Hip to Seat Front
46	Number of Belt Segments
47	Lower Torso-Center of Gravity to Lower Joint
48	Center Torso-Center of Gravity to Lower Joint
49	Upper Torso-Center of Gravity to Lower Joint
50	Head-Center of Gravity to Lower Joint
51	Upper Arm-Center of Gravity to Lower Joint
52	Lower Arm-Center of Gravity to Lower Joint
53	Upper Leg-Center of Gravity to Lower Joint
54	Lower Leg-Center of Gravity to Lower Joint

TABLE XXXVII. INPUT CONSTANTS (ALPHABETICAL ORDER) (page 1)

Number	Description	
39	Back of Front Seat-Length	(When NPASGR=3)
4	Back of Front Seat-X	(When NPASGR=3)
13	Back of Front Seat-Y	(When NPASGR=3)
26	Chest Center of Curvature (Distance to)	
48	Center Torso-Center of Gravity to Lower Joint	
29	Center Torso-Length	
31	Center Torso to Upper Arm (Distance from)	
22	Elbow Contact Arc Radius	
36	Floor-Length	
1	Floor-X	
10	Floor-Y	
25	Foot Contact Arc Radius	
23	Hand Contact Arc Radius	
27	Head Center of Curvature (Distance to)	
50	Head-Center of Gravity to Lower Joint	
21	Head Contact Arc Radius	
19	Hip Contact Arc Radius	
45	Hip to Seat Front (Distance from)	
24	Knee Contact Arc Radius	
52	Lower Arm-Center of Gravity to Lower Joint	
33	Lower Arm Length	
54	Lower Leg-Center of Gravity to Lower Joint	
35	Lower Leg-Length	
42	Lower Panel-Length	
7	Lower Panel-X	
16	Lower Panel-Y	
41	Lower Steering Wheel-Length	
6	Lower Steering Wheel-X	
15	Lower Steering Wheel-Y	

TABLE XXXVII. INPUT CONSTANTS (ALPHABETICAL ORDER) (page 2)

Number	Description	
4	Lower Torso-Center of Gravity to Lower Joint	
28	Lower Torso-Length	
46	Number of Seat Belt Segments	
38	Roof-Length	
3	Roof-X	
12	Roof-Y	
37	Seat Back-Length	
2	Seat Back-X	
11	Seat Back-Y	
43	Steering Column-Length	
8	Steering Column-X	
17	Steering Column-Y	
44	Toeboard-X	
18	Toeboard-Y	
51	Upper Arm-Center of Gravity to Lower Joint	
32	Upper Arm-Length	
53	Upper Leg-Center of Gravity to Lower Joint	
34	Upper Leg-Length	
39	Upper Panel-Length	(When NPASGR=2)
4	Upper Panel-X	(When NPASGR=2)
13	Upper Panel-Y	(When NPASGR=2)
39	Upper Steering Wheel-Length	(When NPASGR=1)
4	Upper Steering Wheel-X	(When NPASGR=1)
13	Upper Steering Wheel-Y	(When NPASGR=1)
49	Upper Torso-Center of Gravity to Lower Joint	
20	Upper Torso Contact Arc Radius	
30	Upper Torso Length	
40	Windshield-Length	
5	Windshield-X	
14	Windshield-Y	

TABLE XXXVIII. VARIABLES (IN NUMERICAL ORDER) (page 1)

<u>Number</u>		<u>Description</u>	
1	Body Angles	Lower Torso	Position
2	Body Angles	Center Torso	Position
3	Body Angles	Upper Torso	Position
4	Body Angles	Head	Position
5	Body Angles	Upper Arm	Position
6	Body Angles	Lower Arm	Position
7	Body Angles	Upper Leg	Position
8	Body Angles	Lower Leg	Position
9	Body Angles	Lower Torso	Velocity
10	Body Angles	Center Torso	Velocity
11	Body Angles	Upper Torso	Velocity
12	Body Angles	Head	Velocity
13	Body Angles	Upper Arm	Velocity
14	Body Angles	Lower Arm	Velocity
15	Body Angles	Upper Leg	Velocity
16	Body Angles	Lower Leg	Velocity
17	Body Angles	Lower Torso	Acceleration
18	Body Angles	Center Torso	Acceleration
19	Body Angles	Upper Torso	Acceleration
20	Body Angles	Head	Acceleration
21	Body Angles	Upper Arm	Acceleration
22	Body Angles	Lower Arm	Acceleration
23	Body Angles	Upper Leg	Acceleration
24	Body Angles	Lower Leg	Acceleration
25	Body Motion	Horizontal	Position
26	Body Motion	Horizontal	Velocity
27	Body Motion	Horizontal	Acceleration
28	Body Motion	Vertical	Position
29	Body Motion	Vertical	Velocity

TABLE XXXVIII. VARIABLES (IN NUMERICAL ORDER) (page 2)

<u>Number</u>	<u>Description</u>		
30	Vehicle	Motion	Velocity
31	Vehicle	Motion	Velocity
32	Vehicle	Motion	Velocity
33	Vehicle	Motion	Acceleration
34	Belt Forces	Lap Belt	Shoulder
35	Belt Forces	Lower	Shoulder
36	Belt Forces	Upper	Shoulder
37	Seat Forces	Hip	
38	Seat Forces	Front Edge	
39	Relative Head	Position	Horizontal
40	Relative Head	Position	Vertical
41	Belt Angles	Lap Belt	
42	Belt Angles	Lower	Shoulder
43	Belt Angles	Upper	Shoulder
44	Accelerometer	Head	Resultant
45	Accelerometer	Head	Angle
46	Accelerometer	Chest	Resultant
47	Accelerometer	Chest	Angle
48	Hip on Seat Back		
49	Upper Torso on Seat Back		
50	Upper Torso on Upper Steering Wheel		(When NPASGR=1)
	Upper Torso on Upper Panel		(When NPASGR=2)
	Upper Torso on Front Seat Back		(When NPASGR=3)
51	Upper Torso on Lower Steering Wheel		
52	Upper Torso on Steering Column		
53	Head on Seat Back		
54	Head on Roof		
55	Head on Upper Steering Wheel		(When NPASGR=1)
	Head on Upper Panel		(When NPASGR=2)
	Head on Front Seat Back		(When NPASGR=3)

TABLE XXXVIII. VARIABLES (IN NUMERICAL ORDER) (page 3)

<u>Number</u>	<u>Description</u>
56	Head on Windshield
57	Head on Lower Steering Wheel
58	Elbow on Seat Back
59	Knee on Lower Panel
60	Foot on Floor
61	Foot on Toeboard

TABLE XXXIX. VARIABLES (IN ALPHABETICAL ORDER) (page 1)

<u>Number</u>		<u>Description</u>	
47	Accelerometer	Chest	Angle
46	Accelerometer	Chest	Resultant
45	Accelerometer	Head	Angle
44	Accelerometer	Head	Resultant
41	Belt Angles	Lap Belt	
42	Belt Angles	Lower	Shoulder
43	Belt Angles	Upper	Shoulder
34	Belt Forces	Lap Belt	
35	Belt Forces	Lower	Shoulder
36	Belt Forces	Upper	Shoulder
18	Body Angles	Center Torso	Acceleration
2	Body Angles	Center Torso	Position
10	Body Angles	Center Torso	Velocity
20	Body Angles	Head	Acceleration
4	Body Angles	Head	Position
12	Body Angles	Head	Velocity
22	Body Angles	Lower Arm	Acceleration
6	Body Angles	Lower Arm	Position
14	Body Angles	Lower Arm	Velocity
24	Body Angles	Lower Leg	Acceleration
8	Body Angles	Lower Leg	Position
16	Body Angles	Lower Leg	Velocity
17	Body Angles	Lower Torso	Acceleration
1	Body Angles	Lower Torso	Position
9	Body Angles	Lower Torso	Velocity
21	Body Angles	Upper Arm	Acceleration
5	Body Angles	Upper Arm	Position
13	Body Angles	Upper Arm	Velocity
23	Body Angles	Upper Leg	Acceleration

TABLE XXXIX. VARIABLES (IN ALPHABETICAL ORDER) (page 2)

<u>Number</u>		<u>Description</u>	
7	Body Angles	Upper Leg	Position
15	Body Angles	Upper Leg	Velocity
19	Body Angles	Upper Torso	Acceleration
3	Body Angles	Upper Torso	Position
11	Body Angles	Upper Torso	Velocity
27	Body Motion	Horizontal	Acceleration
25	Body Motion	Horizontal	Position
26	Body Motion	Horizontal	Velocity
30	Body Motion	Vertical	Acceleration
28	Body Motion	Vertical	Position
29	Body Motion	Vertical	Velocity
58	Elbow	On	Seat Back
60	Foot	On	Floor
61	Foot	On	Toeboard
55	Head	On	Front Seat Back (3)
57	Head	On	Lower Steering Wheel
54	Head	On	Roof
53	Head	On	Seat Back
55	Head	On	Upper Panel (2)
55	Head	On	Upper Steering Wheel (1)
56	Head	On	Windshield
48	Hip	On	Seat Back
59	Knee	On	Lower Panel
39	Relative Head	Position	Horizontal
40	Relative Head	Position	Vertical
37	Seat Forces	Hip	
38	Seat Forces	Front Edge	
50	Upper Torso	On	Front Seat Back (3)
51	Upper Torso	On	Lower Steering Wheel

TABLE XXXIX. VARIABLES (IN ALPHABETICAL ORDER) (page 3)

<u>Number</u>		<u>Description</u>		
49	Upper Torso	On		Seat Back
52	Upper Torso	On		Steering Column
50	Upper Torso	On		Upper Panel (2)
50	Upper Torso	On		Upper Steering Wheel (1)
33	Vehicle	Motion		Acceleration
31	Vehicle	Motion		Position
32	Vehicle	Motion		Velocity

V. PROGRAM OPERATION AND DESCRIPTION

Figure 43 is a flowchart for the computer program. Initially data is read, constants computed, and the problem initialized to zero where necessary. The cart acceleration and the level of output printing are then ascertained from the data. Acceleration components due to inertia, continuous joint reactions and external forces are computed in subroutine ACCEL. The effective acceleration due to discontinuous forces is then computed and added to the continuous accelerations in subroutines, JITTER and TAUMAK. After the accelerations are finally predicted, standard checking, storing, incrementing and integrating of results are carried out. The program then is run in loop fashion for the required number of print time increments.

Figure 44 shows how the subprograms in the computer implementation fit together in usage. The left margin of the figure contains a numbered list of the subroutines which comprise the program. Across the top is a list of numbers, each representing the subprogram with the same number on the left margin. The figure itself consists of a set of "X"'s at various intersections of rows and columns. An "X" at the mth row and nth columns indicates that subroutine n makes use of subroutine m. The row for a particular subroutine shows all the other subroutines which use it. The column for a particular subroutine also shows all the subroutines which it uses. These subroutines have all been programmed using the Fortran IV Compiler, Level G.

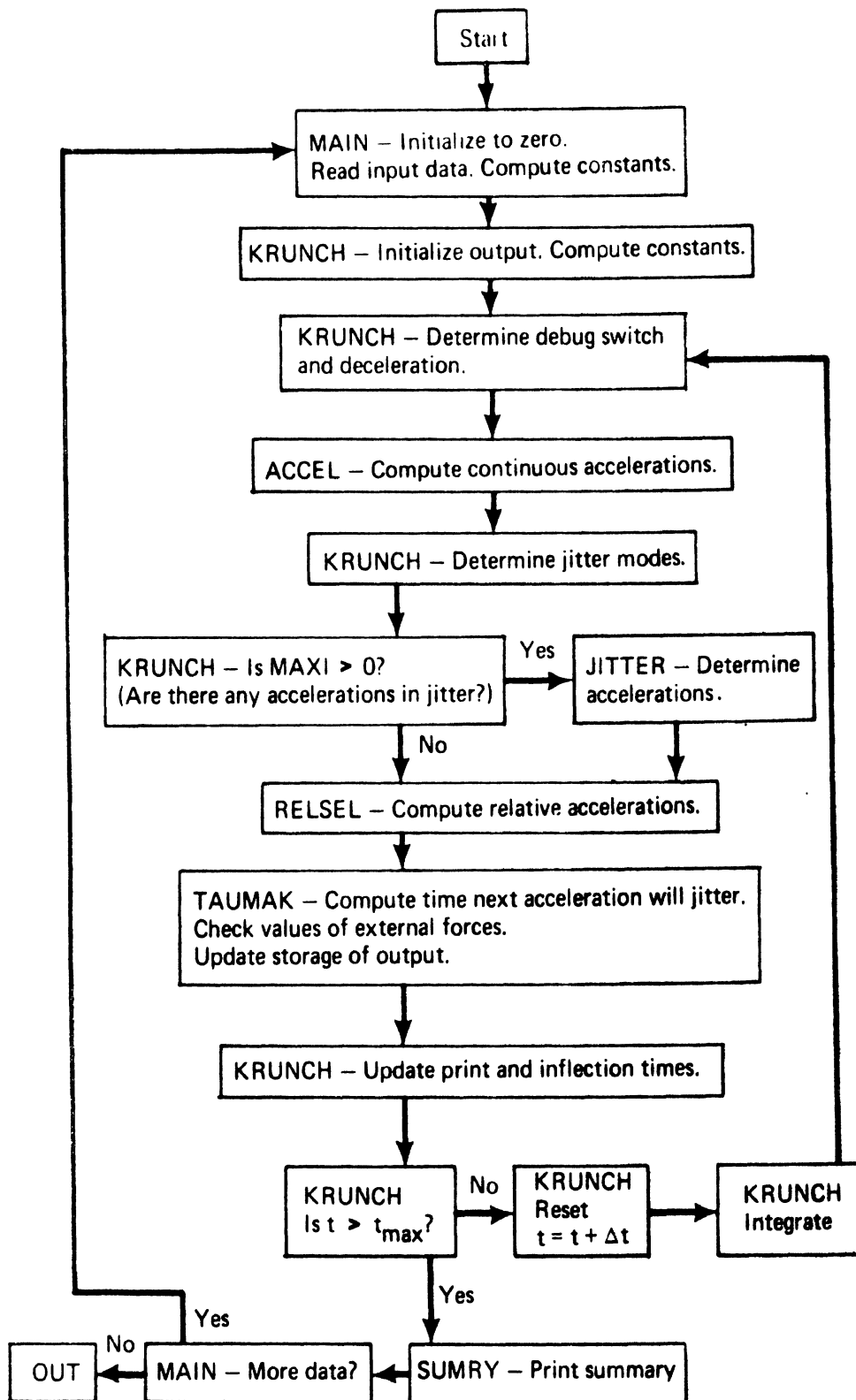


Figure 43. Simplified program flow chart.

Subroutine Number	Called Subroutine	Calling Subroutine																									
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	26		
1	MAIN																										
2	DATE	x																									
3	PAGE 4																								x		
4	KRUNCH	x																								x	
5	GETY		x																								
6	ACCEL		x																								
7	SEAT					x																					
8	BELT					x																					
9	LODFEC						x																				
10	MULLER							x																			
11	CONTAC																										
12	BODY																										
13	ZMAKER																										
14	RELVEL																										
15	DELZMK																										
16	JITTER																										
17	ZKMAKR																										
18	RELSEL																										
19	TAUMAK																										
20	LIMIDT																										
21	FECLOD																										
22	NORMUT																										
23	SUMARY	x																									
24	ITOPOW																										
25	ARCSIN	x																									
26	SIPP																										
27	STYX																										

Figure 44. Usage of program subroutines

A library of additional subroutines obtained from various sources are necessary for exercising the model. These are listed in Figure 45 which is organized in a manner similar to Figure 44. The sources of these subroutines are the Fortran library (IBM), the MTS logical and printer plot packages (University of Michigan), and SSP (IBM). Five additional subroutines (the HSRI conversion package) were developed by the current investigators to adapt the MTS packages for use external to the University of Michigan MTS system. Most of these programs were in OS Assembler language when obtained by the project. When the HSRI Two-Dimensional Crash Victim Simulator is supplied to potential users not operating under MTS, the tape includes all routines included in Figures 44 and 45 with the exception of the Fortran library.

The Fortran library in use at the University of Michigan Computing Center is an old version supplied by IBM. The calculated results presented in Section IV E of this report may vary slightly from those obtained using a more current IBM Fortran library. These variations usually occur in the fifth significant figure of computed quantities and are thus not considered to be physically significant.

The original version of the HSRI Two-Dimensional Crash Victim Simulator was written in Fortran II in 1967. Labeled common blocks were not available at that time so a large master common was used. When the program was converted to Fortran IV in 1969, the old form was retained. As later modifications were made, two labeled common blocks were added as listed in Table XL.

Table XL. Labeled Common Blocks

Name	Used
INJ	SUMARY SIPP
IO	MAIN SUMARY STYX SIPP PAGE4

A. INTEGRATION OF DISCONTINUOUS ACCELERATIONS

In the digital computer simulation, integration is done by mathematical approximation. The usual technique is to base the integration on a polynomial which has been fit through several ordinates of the integrand. This approach will work well only when the integrand is very much like the polynomial obtained by the curve fitting. If the integrand is continuous, it is possible to find a set of intervals over each of which the integrand "looks"

like a polynomial. If, however, the integrand is discontinuous, the discontinuity will remain regardless of the length of the interval within which it is imbedded, so decreasing the interval length is not effective. In this situation, either the integration must be stopped at the discontinuity or the discontinuity removed. For the two-dimensional crash victim simulator, the latter course is adopted.

Discontinuities arise in the model for seat friction force, contact surface friction force, and friction-like forces in the joints. Each of these models has a velocity-dependent component (force, torque, or slope of torque) which assumes a fixed value for all velocities greater than the velocity limit (an input parameter), the negative of the value for all velocities less than the negative of the velocity limit, and zero for the open interval defined by minus and plus values of the velocity limit.

Each instance of these discontinuous models is called a "mode" in the computer program and in the discussion which follows. If a particular mode is in either of the extreme velocity intervals, the mode is said to be "full on." If the mode is in the zero interval, the mode is said to be "full off." When velocity is at the velocity limit or its negative (the points of discontinuity), one of several things can happen, which may be categorized into one of two general possibilities. Either the mode will pass on through the limit point without mishap to full on or full off in the other direction, or the mode will try to do one of these and be thrown back. In the latter case, the mode is said to be "in jitter." Jitter will often take the form of a rapid alternation of the full on and full off states. This occurs when momentum and other forces drive the mode to full on but the force developed by the mode coming on is large enough to throw the mode back to off. The mode going in turn causes the mode force to go to zero which leaves the momentum and other forces free to drive the mode on again and so on, and on.

The jitter type of phenomenon occurs in reality, for example, as chatter due to backlash in gears. The technique employed in the two-dimensional crash victim simulator to compensate for jitter is based on the observation that a rapid alternation of the on-off states would effectively hold the velocity at the velocity limit. Hence, for a time interval during which a

single mode is jittering, the effective body accelerations are computed to be a weighted average of the accelerations computed with the mode turned full off and those computed with the mode turned full on, such that the mode acceleration is made zero, or the mode velocity is the same at the end of the time interval as it was at the beginning.

$$\ddot{\vec{z}}_{\text{eff}} = \ddot{\vec{z}}_{\text{off}} - \bar{a} (\ddot{\vec{z}}_{\text{on}} - \ddot{\vec{z}}_{\text{off}})$$

where

$$\bar{a} = \frac{v_{\text{off}}}{\dot{v}_{\text{on}} - \dot{v}_{\text{off}}} \quad (\text{V.A.1})$$

$\ddot{\vec{z}}_{\text{eff}}$ is the effective generalized acceleration vector.

$\ddot{\vec{z}}_{\text{on}}$ is the generalized acceleration vector with the mode full on.

$\ddot{\vec{z}}_{\text{off}}$ is the generalized acceleration vector with the mode full off.

\dot{v}_{off} is the mode acceleration magnitude with the mode full off.

\dot{v}_{on} is the mode acceleration magnitude with the mode full on.

When the mode is influenced by an outside acceleration (such as vehicle deceleration) applied arbitrarily, the mode acceleration forced to zero may not guarantee that there will be no change in velocity over an interval. Arbitrary accelerations are treated by the two-dimensional crash victim simulator as piecewise linear functions. Those modes which are dependent upon vehicle acceleration, e.g., any interaction of contact surface and contact arc, are termed "coupled" modes and lead to "linear" jitter. Linear jitter requires a different weighted average and also an iteration for resolution.

$$\bar{a} = \frac{\dot{v}_{\text{off}} - 1/2 \dot{v}_{\text{on}}}{\dot{v}_{\text{on}} - \dot{v}_{\text{off}}}$$

$$\hat{\tau}_0 = \frac{\dot{v}_{\text{on}}}{\bar{a} \cos \psi_a} \quad (\text{V.A.2})$$

where

ψ_a is the orientation angle of the contact surface if a contact surface is involved in the mode. ψ_a is defined zero if no contact surface is involved in the mode, e.g., seat cushion.

$\hat{\tau}_0$ is a computed time interval in which the mode will reach the velocity limit. It is used in the iteration as shown the next page.

For several modes in jitter or "multiple jitter," all possible combinations of the jittering modes in the full on state and the full off state are considered and averages developed by reapplications of the single mode averaging procedure so that all the mode velocities are held constant. Only one linear jitter can be handled at one time and must be processed last in combination with other jittering modes.

If no mode changes state during a time interval, then the generalized accelerations are continuous. If the time interval is kept small enough, the generalized accelerations are nearly constant over the interval and a one point integration scheme can be validly employed.

The grand strategy for integration in the two-dimensional crash victim simulator revolves around maintaining the validity of these two requirements and taking advantage of their consequences. At each time throughout the initial value solution of the equations of motion, an integration time interval is computed that will meet the requirements that the generalized accelerations are continuous and approximately constant. The determination of the time interval is carried out by taking the smallest of the predicted time intervals, after the end of which the requirements will no longer be met due to one or another cause. In particular, the computer program predicts the next time at

which any of the modes will change state. If that time is less than the time to which the program would integrate from other considerations (deceleration slope change, print time, etc.), the program integrates to that time and indicates that the mode is jittering. The program always employs the averaging procedure to resolve the questionable accelerations from jittering modes.

The time interval prediction equation (until a change of state) for an uncoupled mode is

$$\tau = \frac{\xi \operatorname{sgn} \eta - v}{\dot{v}} \quad (\text{V.A.3})$$

where

$$\eta = \begin{cases} v & \text{for } |v| > \xi \text{ and } \operatorname{sgn} v \neq \operatorname{sgn} \dot{v} \\ \dot{v} & \text{for } |v| < \xi \end{cases}$$

ξ is the mode velocity limit

v is the mode velocity

\dot{v} is the mode acceleration

Note that if $|\dot{v}| = \xi$, then τ is not used since the mode is already known to be jittering. If $|v| > \xi$ and $\operatorname{sgn} v = \operatorname{sgn} \dot{v}$, then τ is infinite since the mode is going away from the velocity limit. The corresponding equation for a coupled mode is

$$\tau = \begin{cases} \frac{\dot{v}}{a_v \cos \psi_a} \left[1 - \sqrt{1 - \frac{2(\xi \operatorname{sgn} \eta - v) a_v \cos \psi_a}{\dot{v}^2}} \right] & (\text{V.A.4}) \\ \hat{\tau}_0 & \text{for 1. } |v| > \xi \text{ and } \operatorname{sgn} v = \operatorname{sgn} \dot{v} \\ & \text{2. } |v| = \xi \\ & \text{3. arg of radical is negative} \end{cases}$$

where a_v is the acceleration rate and the other conventions are as previously given. The equation is used in an iterative procedure in which it is alternated with the acceleration averaging procedure and recomputation of $\hat{\tau}_0$ until

two consecutive values of τ are approximately the same.

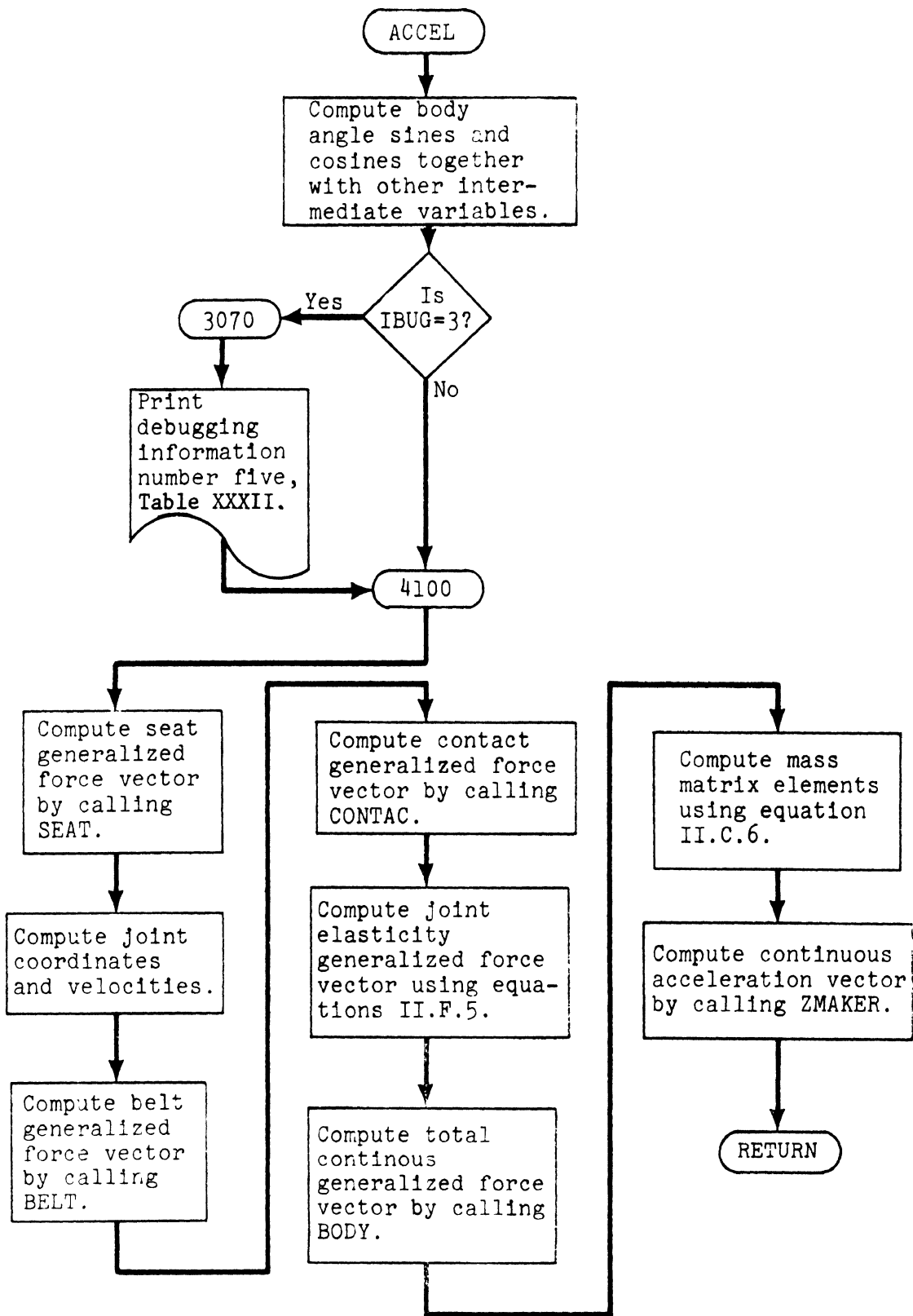
B. SUBPROGRAMS DESCRIPTIONS AND FLOW DIAGRAMS

For each of the subprograms which make up the computer implementation of the model a short description together with a flow diagram is presented here. These are in alphabetical order by the subprogram name with the main program ordered as if its name were MAIN. The subroutines included are:

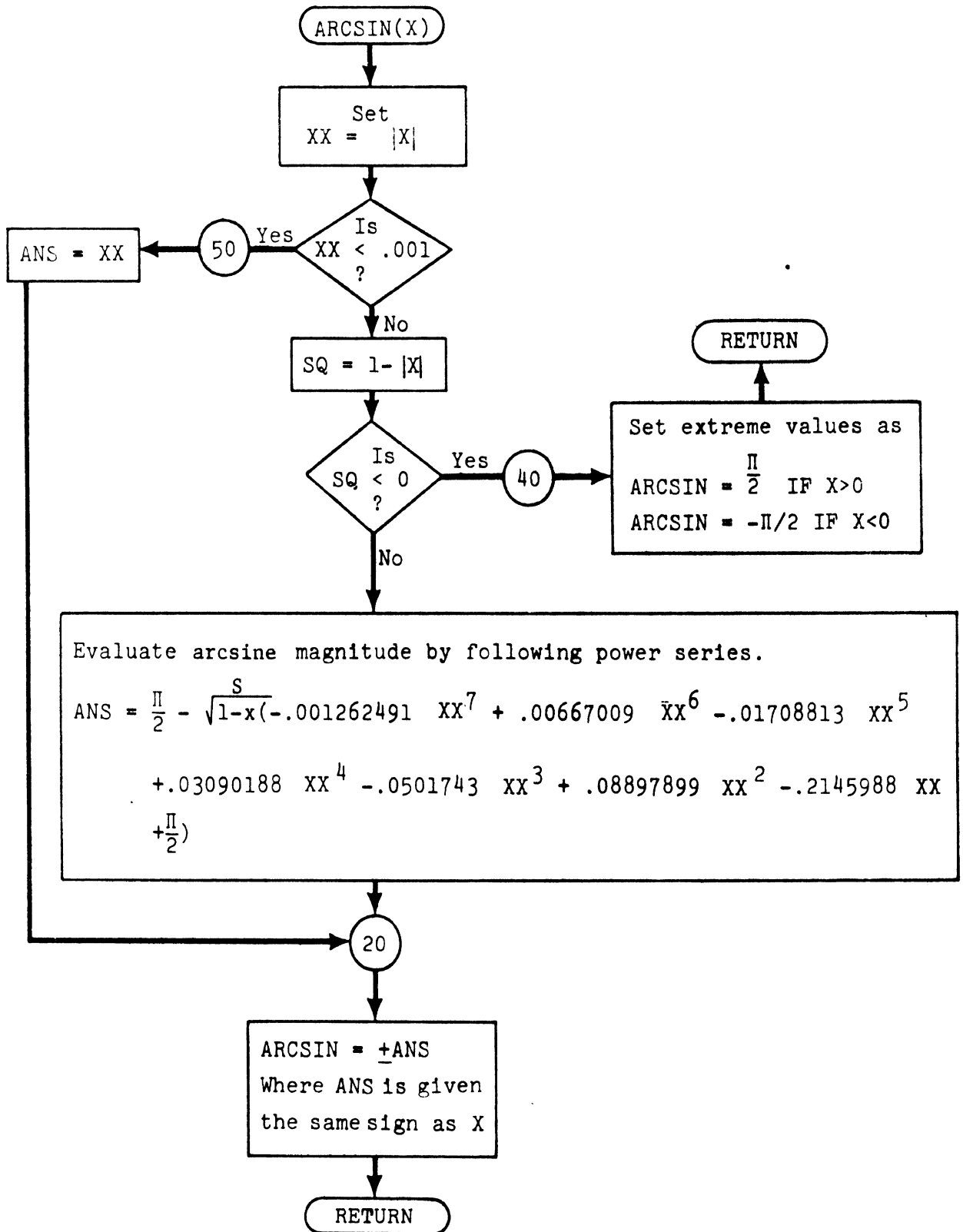
	Page		Page
1 ACCEL	247	15 MAIN	274
2 ARCSIN	249	16 MULLER	296
3 BELT	250	17 NORMUT	300
4 BODY	251	18 PAGE4	301
5 CONTAC	252	19 RELSEL	302
6 DATE	255	20 RELVEL	303
7 DELZMK	256	21 SEAT	304
8 FECLOD	257	22 SIPP	306
9 GETY	260	23 STYX	307
10 ITOPOW	261	24 SUMARY	312
11 JITTER	262	25 TAUMAK	313
12 KRUNCH	264	26 ZKMAKR	317
13 LIMIDT	267	27 ZMAKER	318
14 LODFEC	268		

Subroutine ACCEL carries out the following steps:

1. Computes sines and cosines of body angles and other needed variables.
2. Gets seat forces and contributions to the generalized force vector via SEAT.
3. Computes all joint coordinate positions and velocities.
4. Gets belt forces and contributions via BELT.
5. Gets contact forces and contributions via CONTAC.
6. Computes joint elasticity torques and contributions.
7. Procures generalized force vector from BODY.
8. Computes variable matrix elements.
9. Procures acceleration vector from ZMAKER.

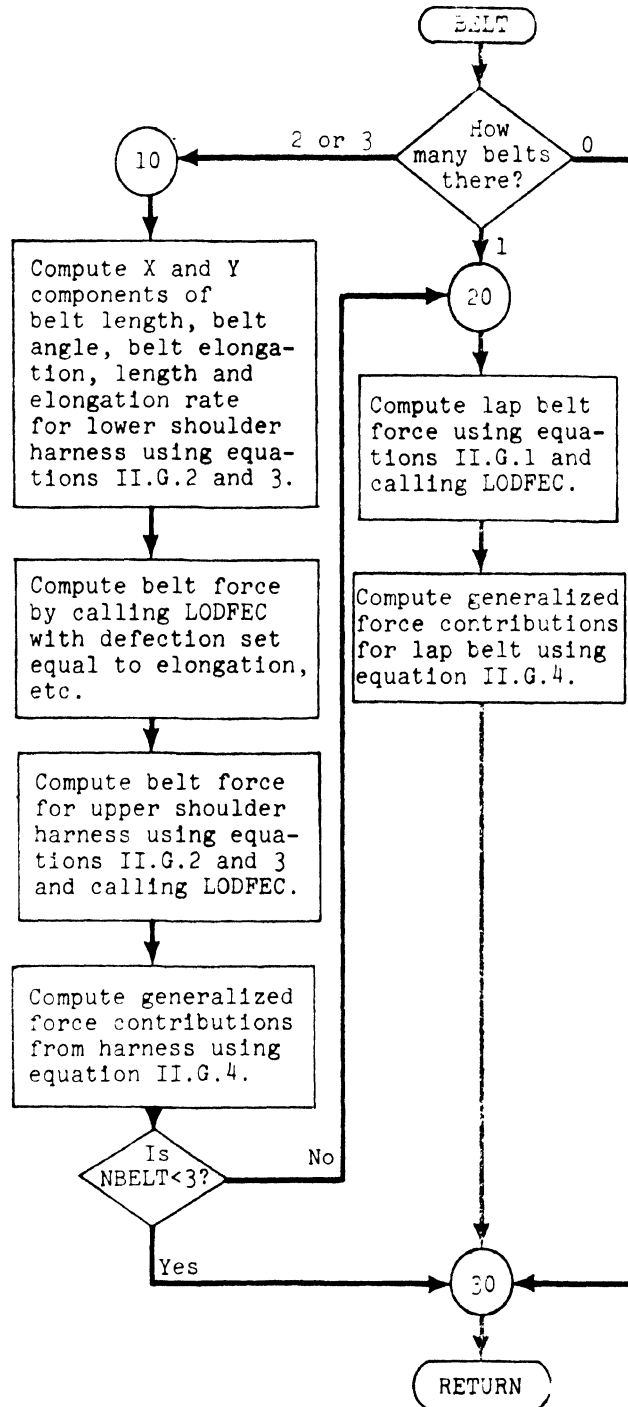


Function ARCSIN finds the angle for a given sine value. The argument X is in the range $-1 \leq X \leq 1$ and is the sine of the angle to be computed by this routine.



Subroutine BELT carries out the following steps:

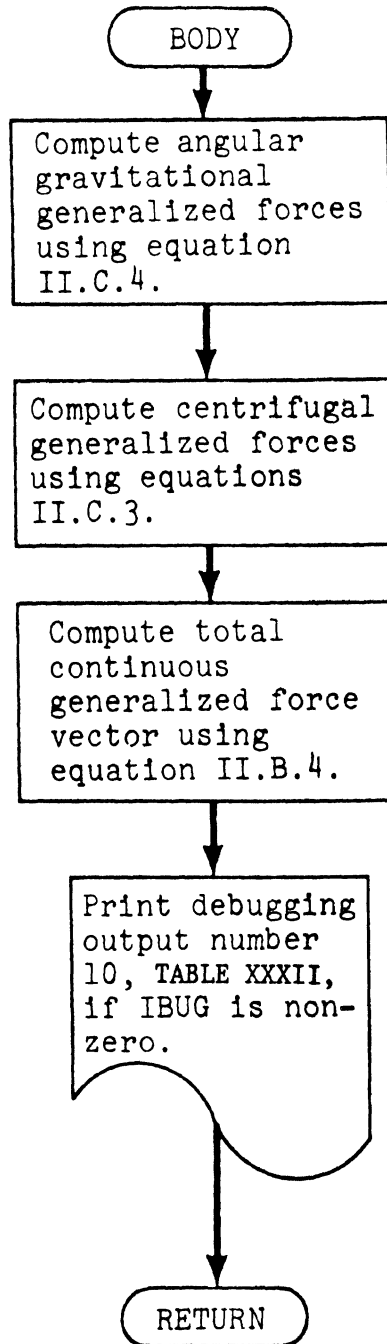
1. Computes angle, elongation, and rate for each belt.
2. Obtains belt force from LODFEC.
3. Computes total belt generalized force vector and adds it to seat total generalized force vector.



Subroutine BODY

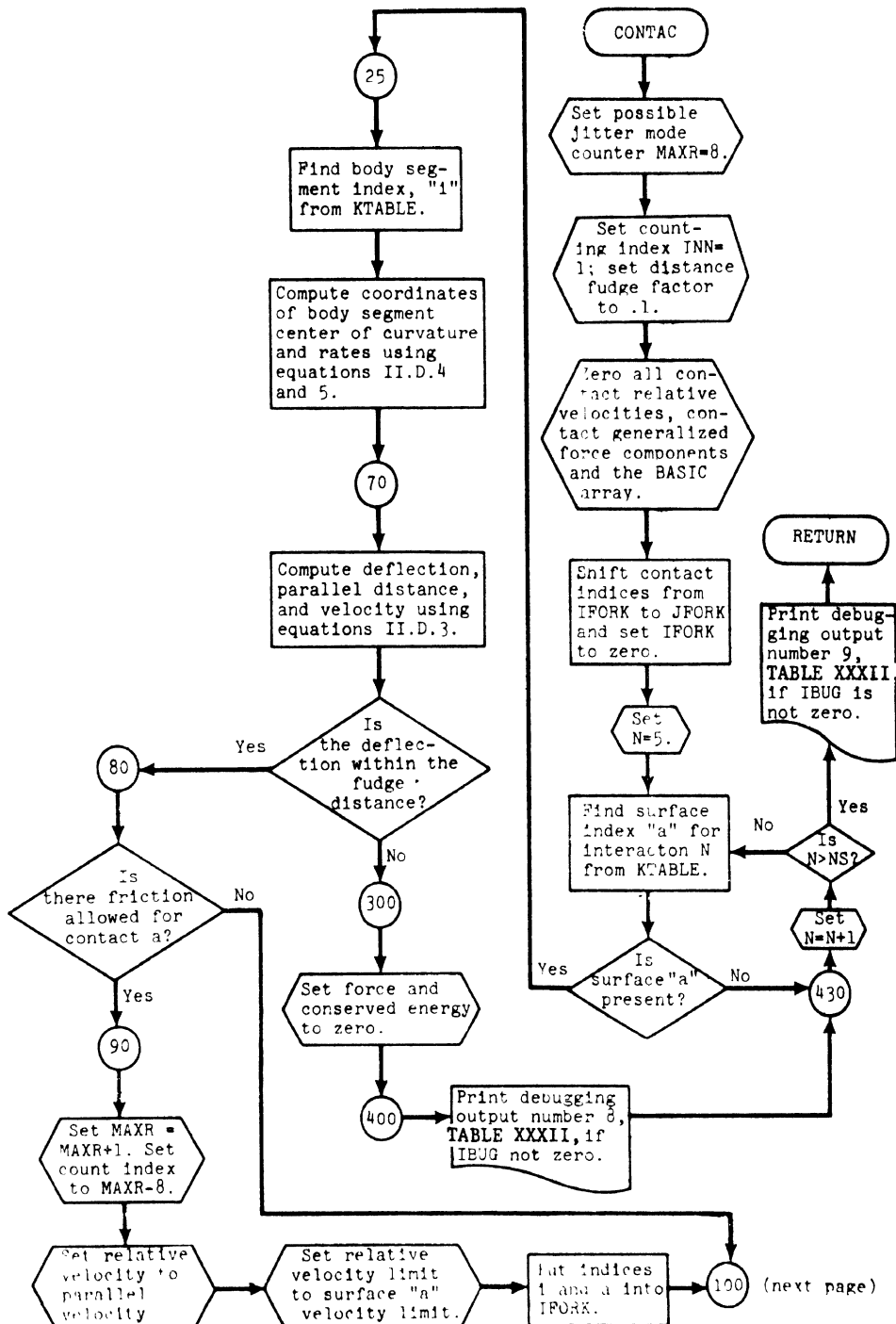
Computes generalized force vectors due to gravity and centrifugal force, and

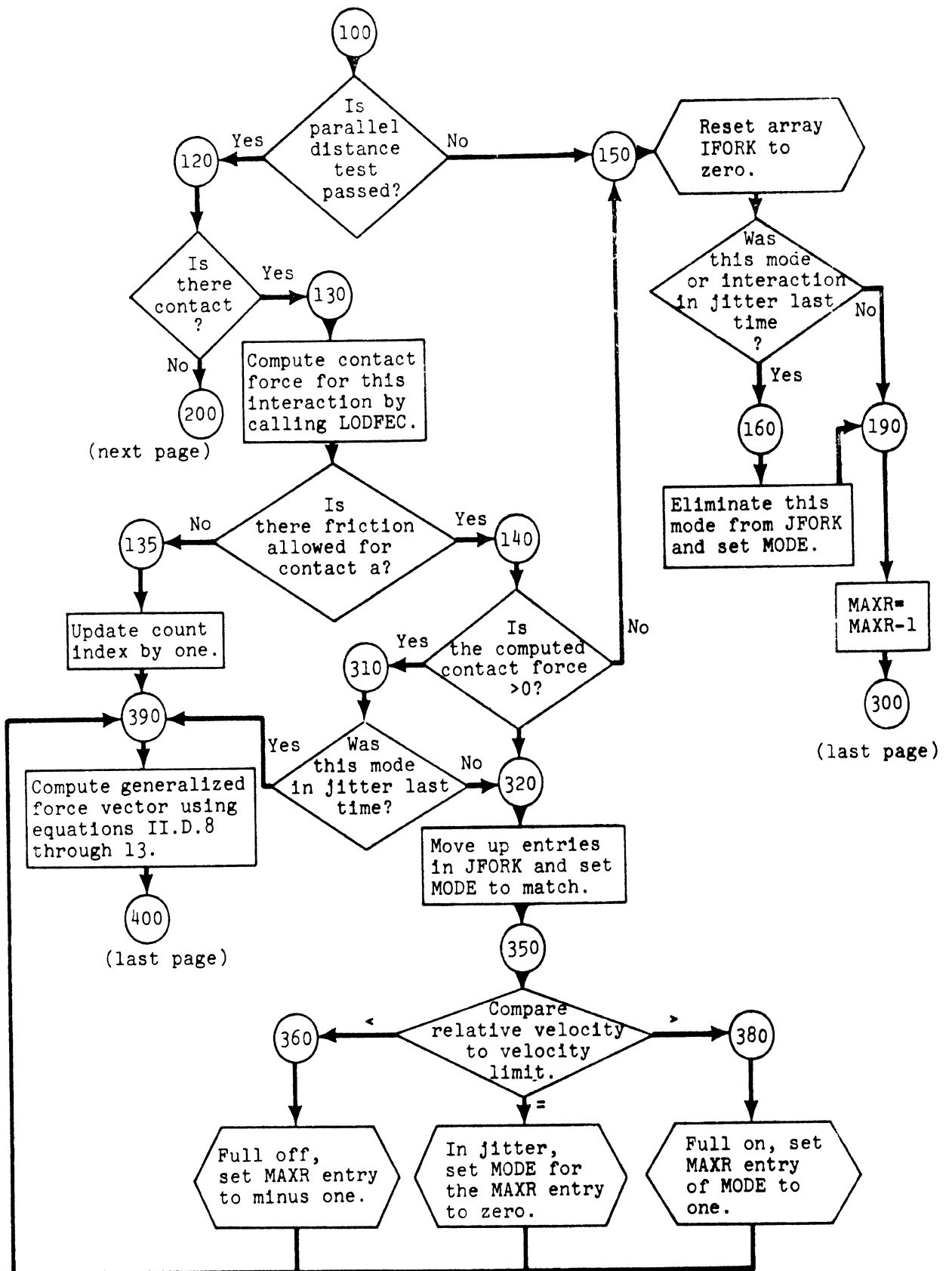
Combines all five continuous generalized force vectors for total.

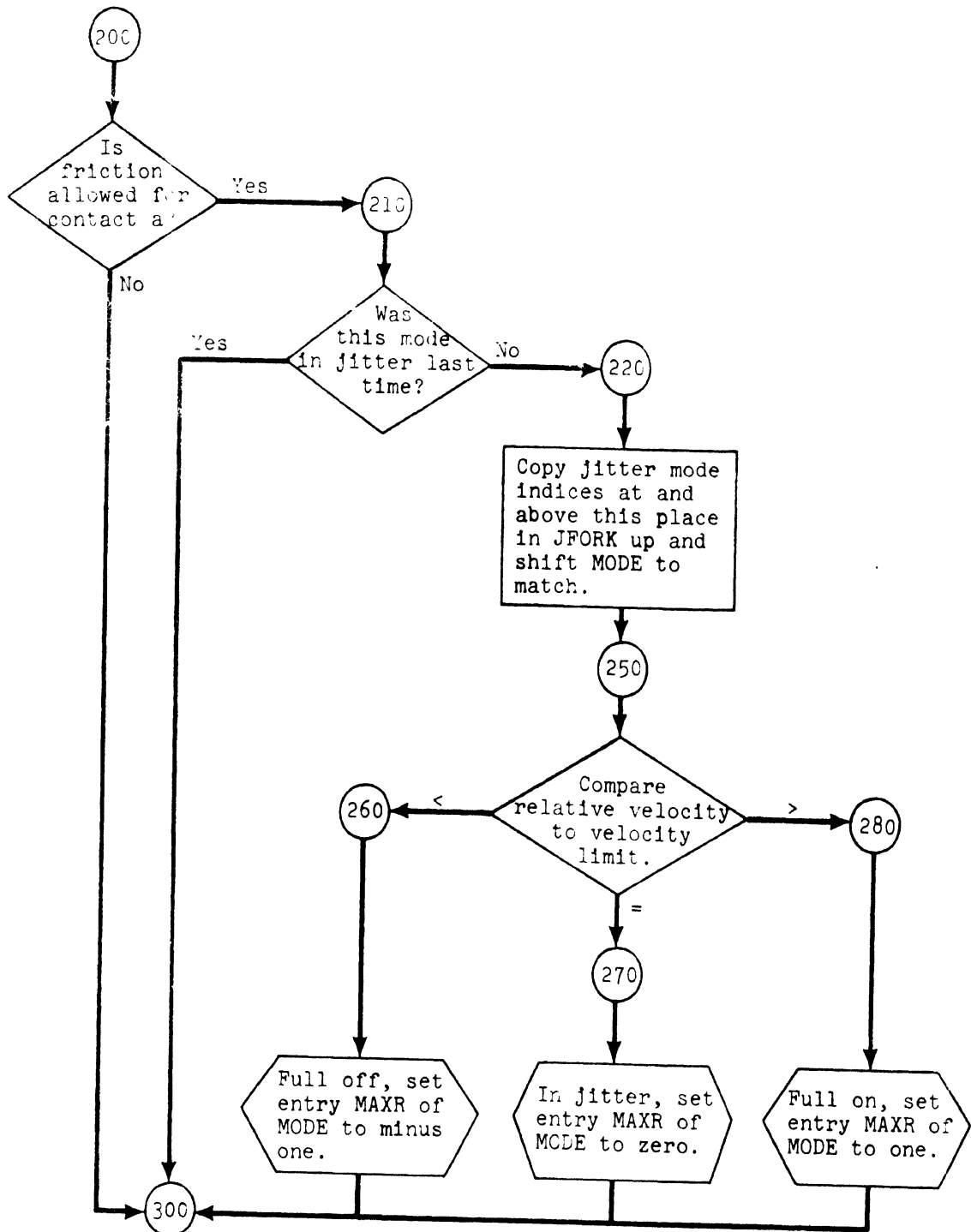


Subroutine CONTAC carries out the following steps:

1. Searches table of possible contacts (as set up in MAIN) and determines whether contact exists using coordinates of body segment center of curvature and contact surface reference point.
2. Does bookkeeping for linear jitter modes.
3. Obtains contact forces from LODFEC.
4. Computes contribution of contacts to total generalized force vector.

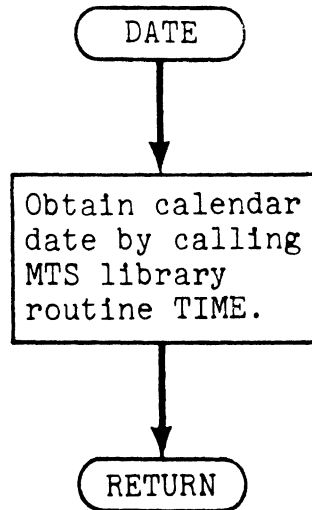






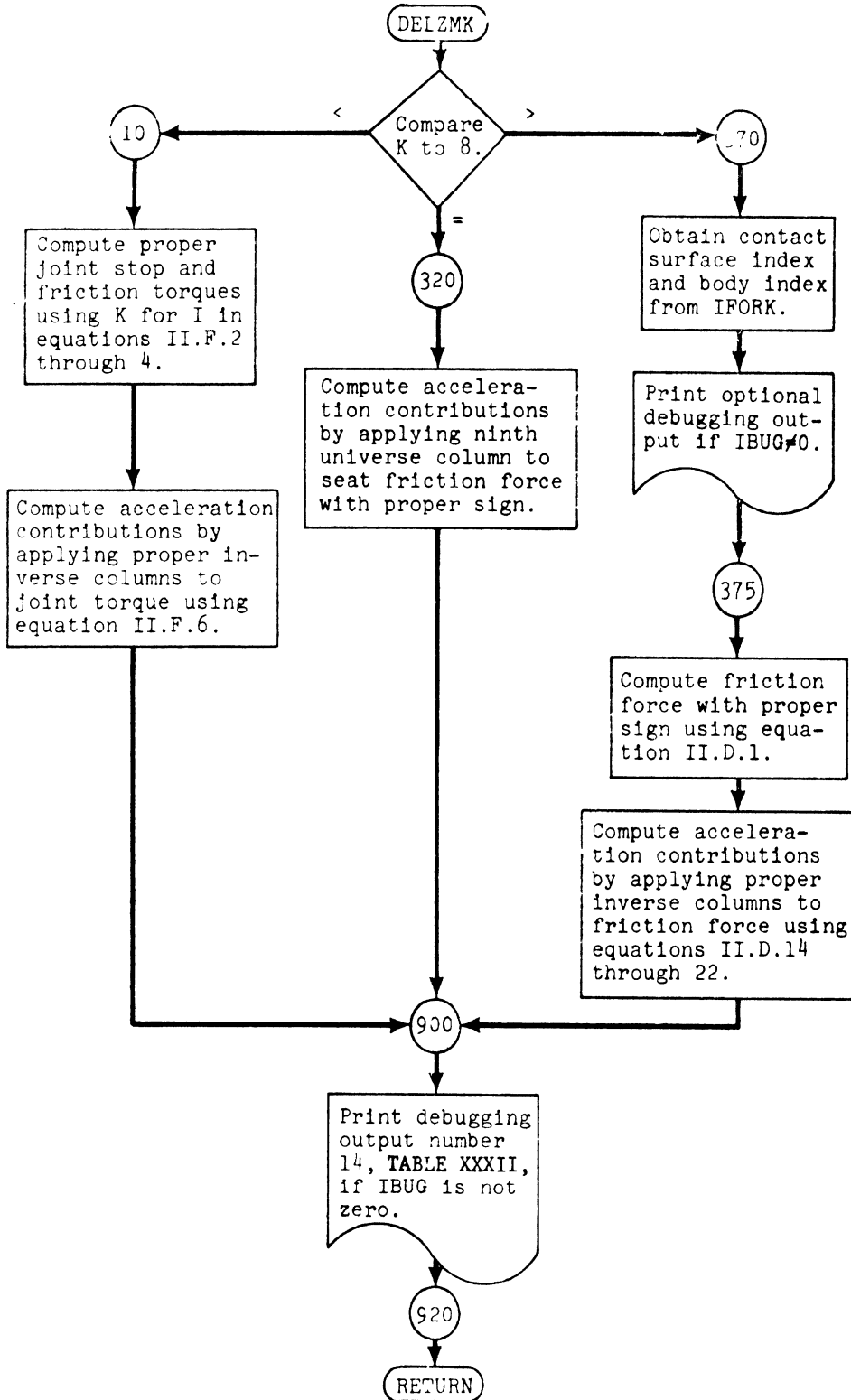
Subroutine DATE

Calls Library routine TIME in MTS system to get date program is being run for print-out identification, or similar routine at other computer facility, or return blank date if similar routine does not exist.

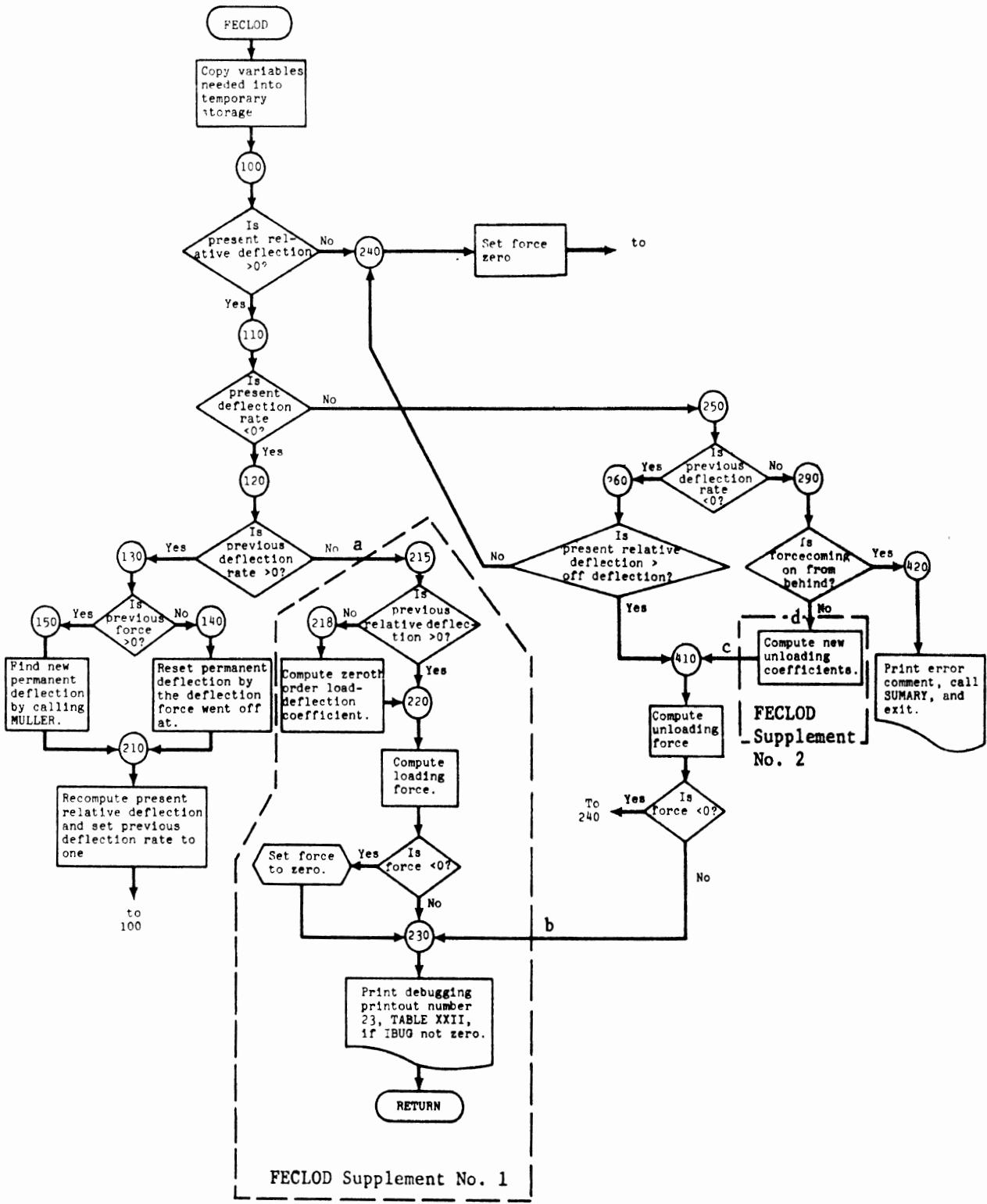


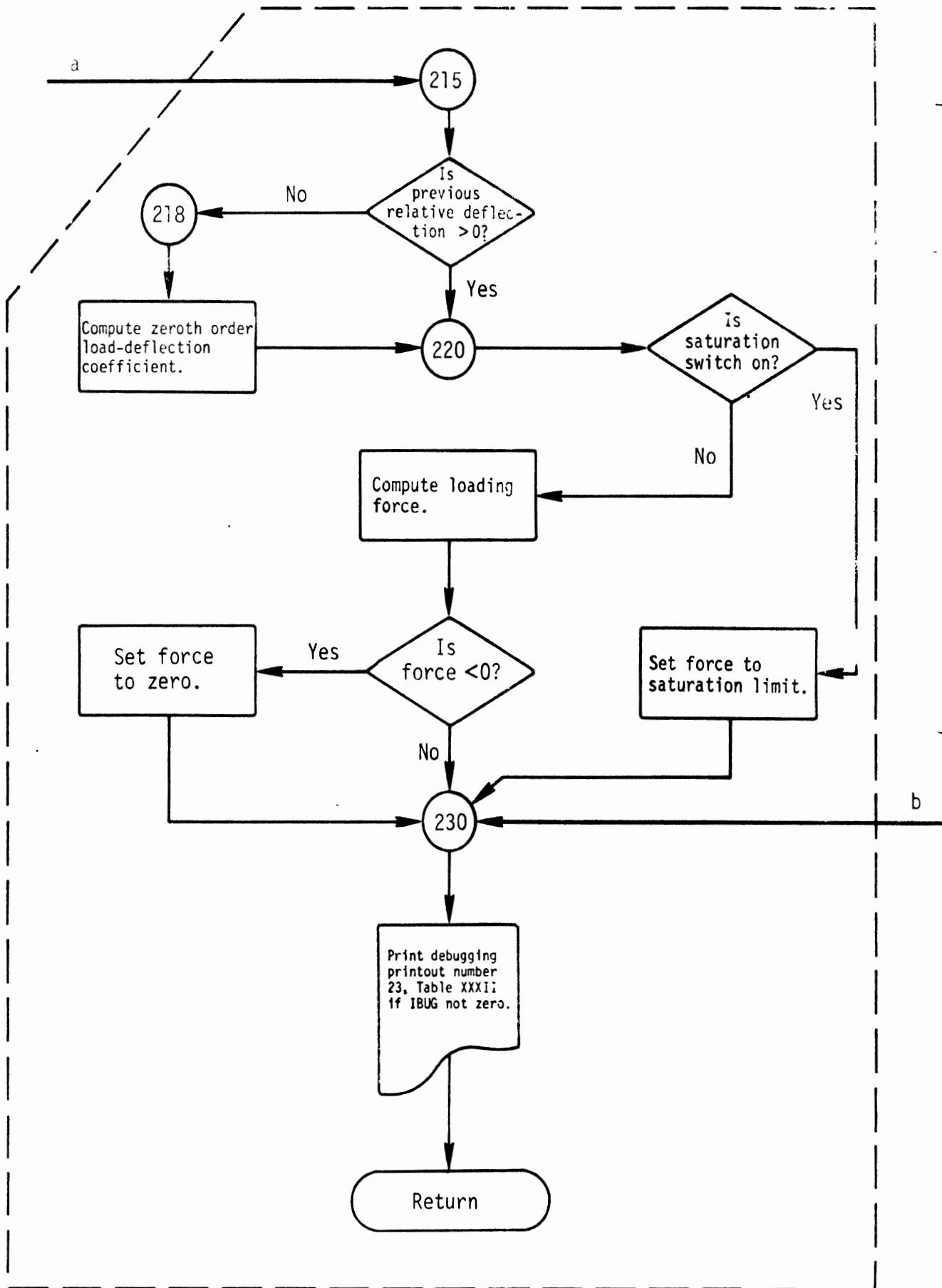
Subroutine DELZMA

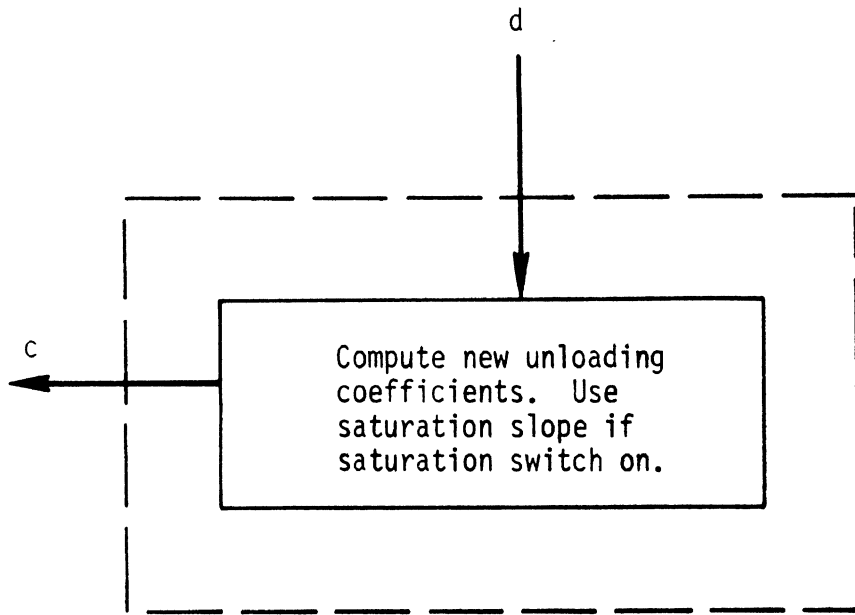
Computes contributions to the acceleration vector of joint, seat, and contact friction. The argument K of DELZMK is the mode number for which acceleration contributions are to be computed.



Subroutine FECLD is used to predict contact and belt forces during the selection a new time step.







FECLOD Supplement No. 2

Subroutine GETY

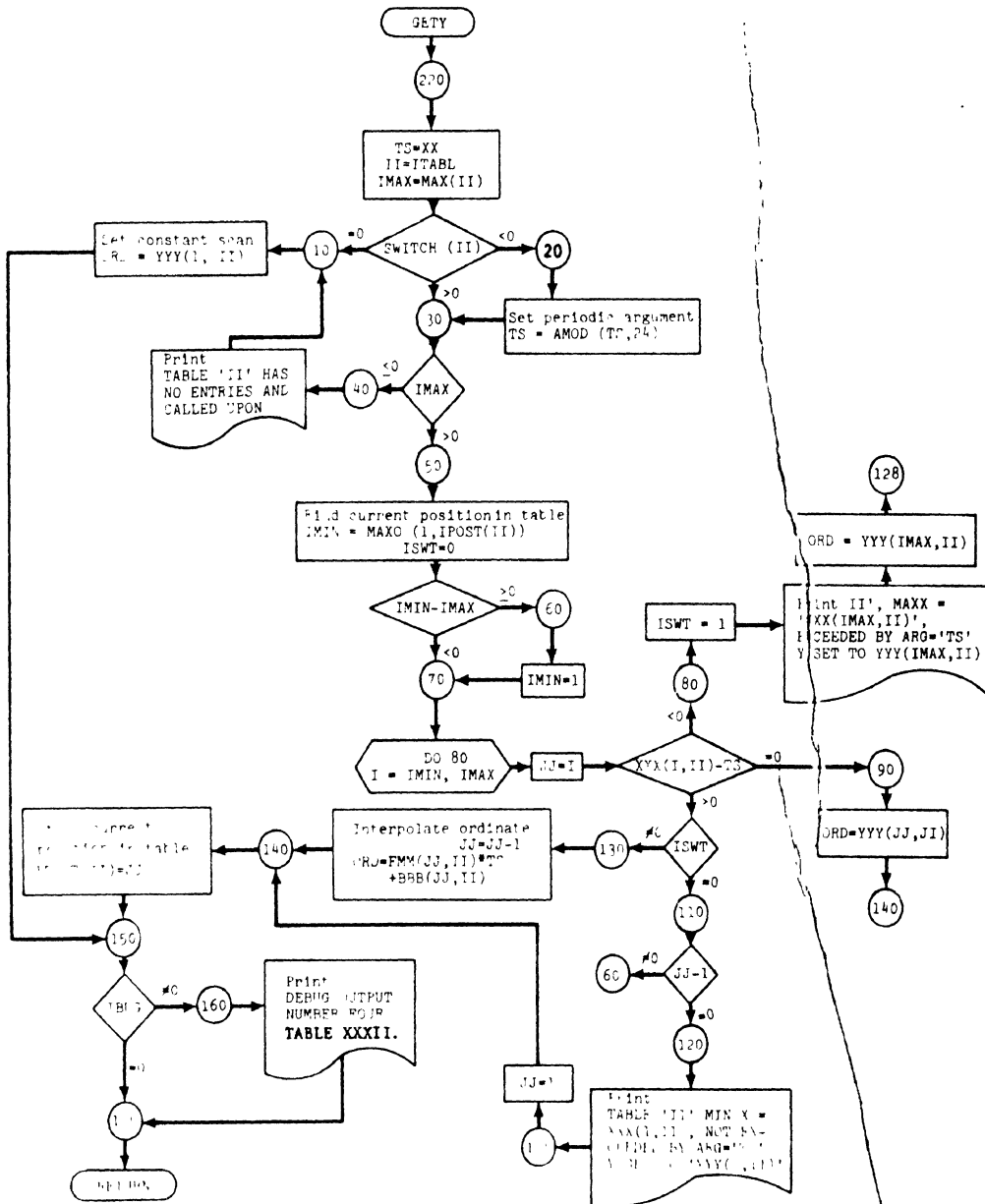
determines the ordinate of piecewise-linear tabular function for a given abscissa.

Arguments are:

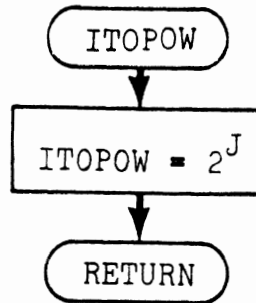
XX = abscissa desired

ITABL = table number, and

ORD = computed ordinate.

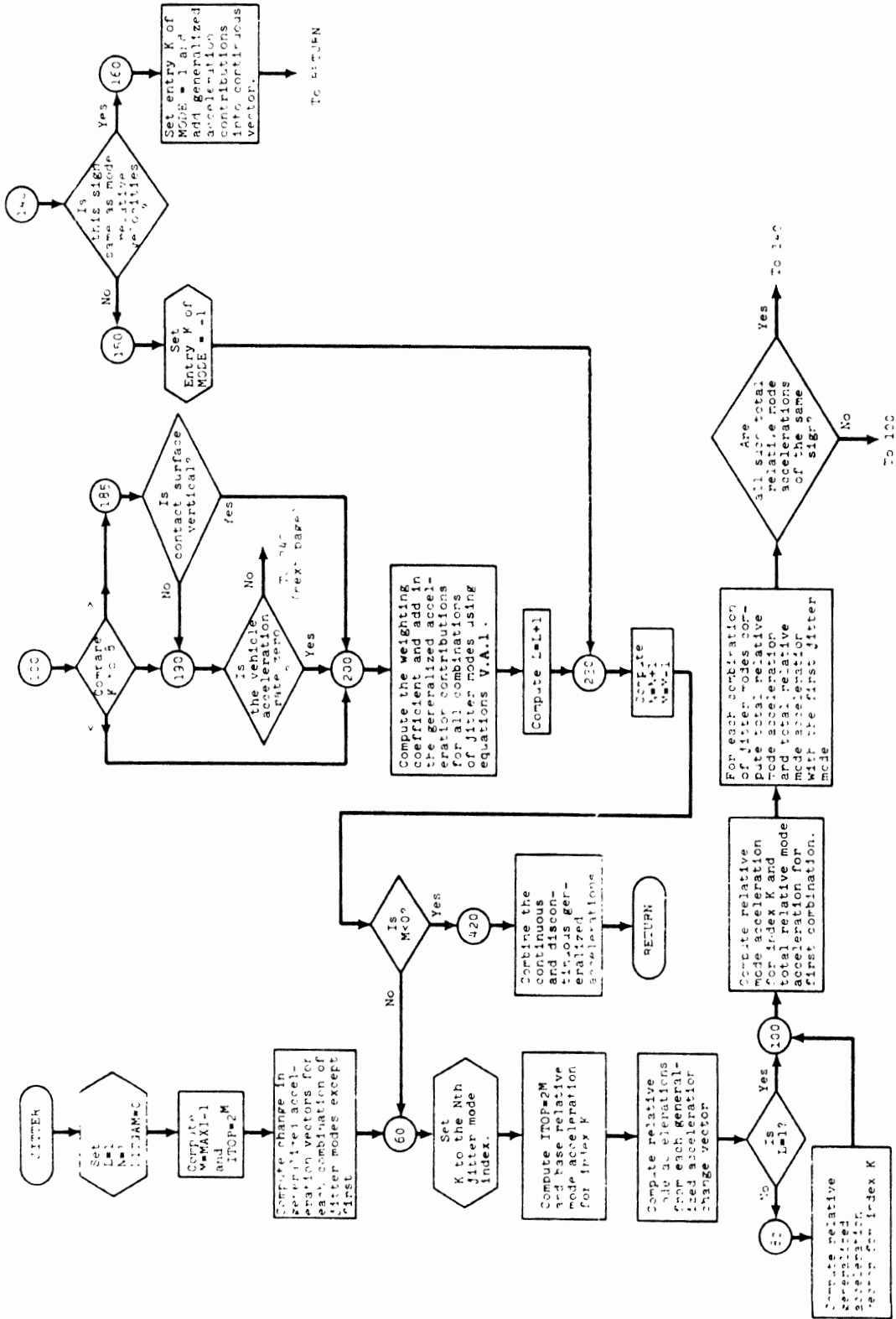


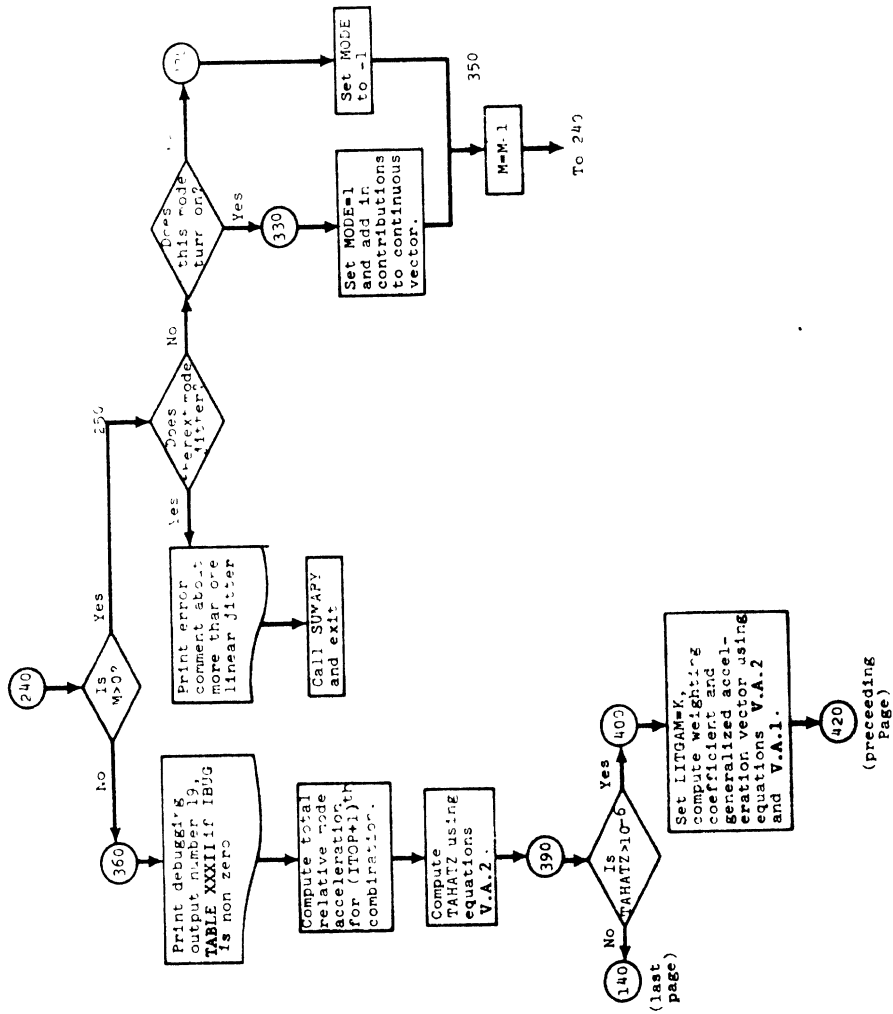
Function ITOPOW raises 2 to an integer power. The argument J is the power of 2 that is desired.



Subroutine JITTER

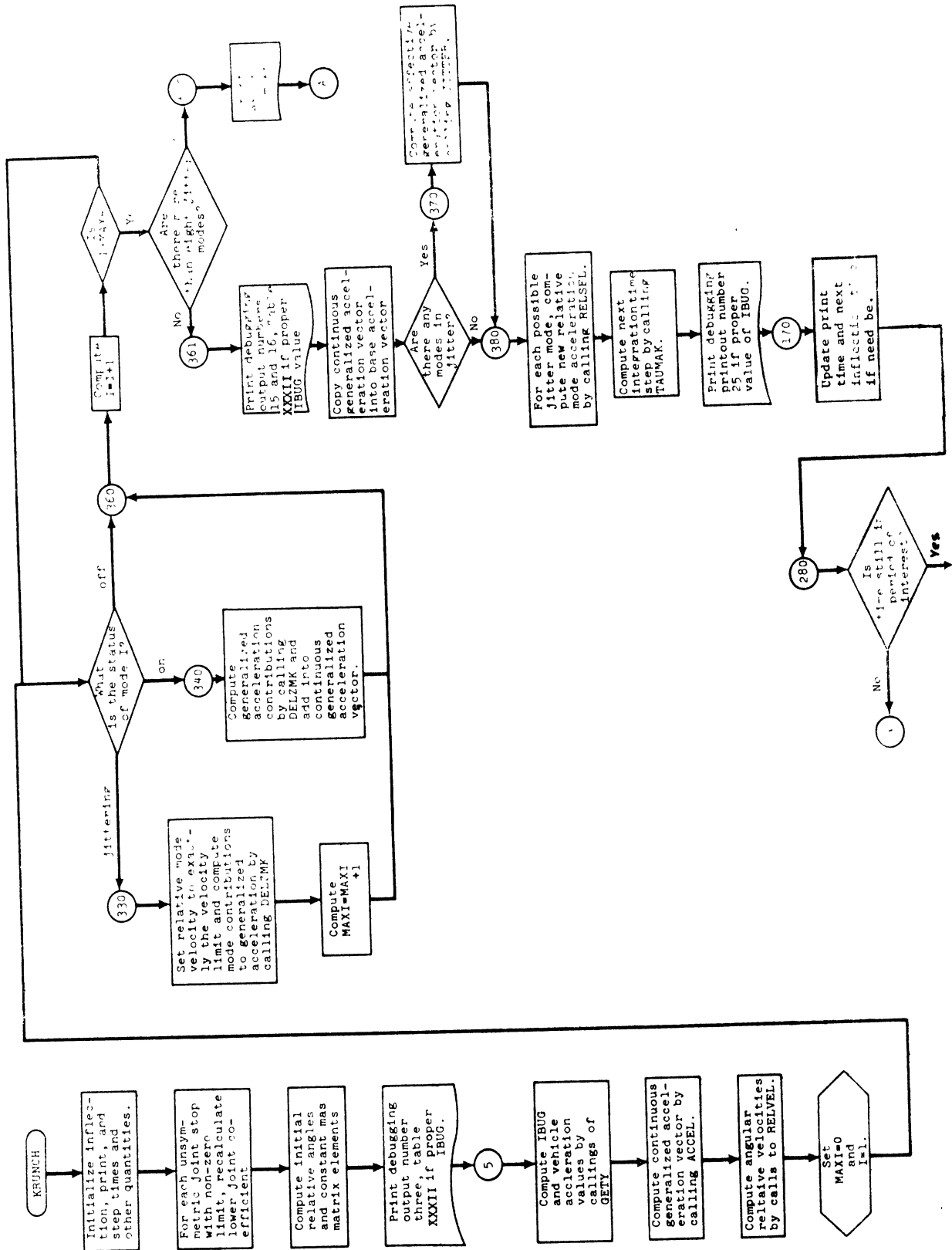
Computes the effective acceleration vector by combining the continuous acceleration vector with the contribution of frictional forces in the form of discontinuous accelerations using a weighted averaging technique.



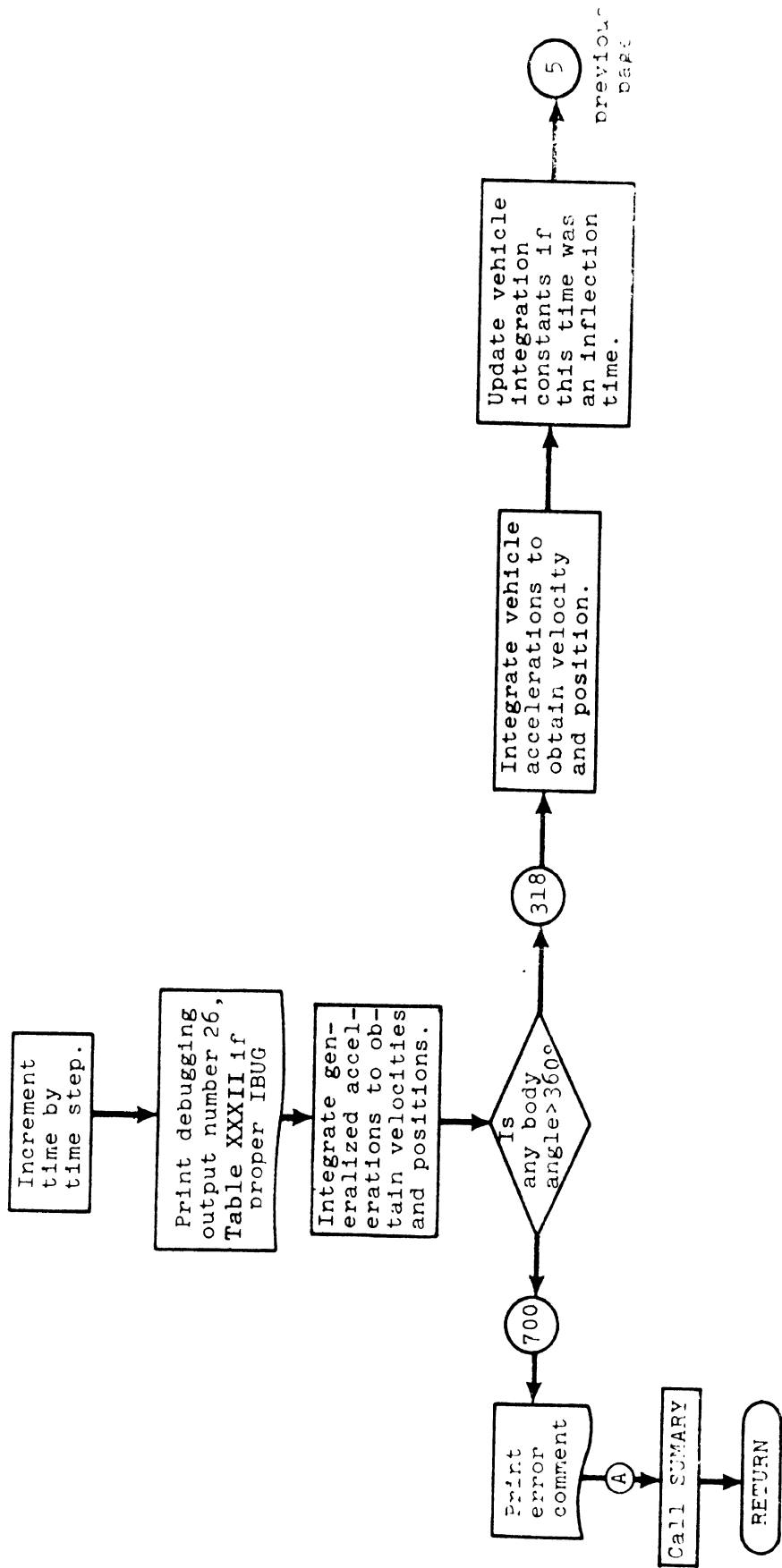


Subroutine KRUNCH carries out the following steps:

1. Initializes variables and parameters.
2. Recomputes joint stop coefficients as needed.
3. Starts time loop by finding debug variable and vehicle acceleration from tables via GETY.
4. Calls ACCEL for body accelerations due to continuous forces.
5. Computes relative velocities between body segments and between the hip and seat cushion.
6. Predicts unstable computational behavior and sets up the means (jitter vector) for compensating for it.
7. Computes the turned on friction forces contributions to the acceleration vector via DELZMK.
8. Checks number of jitter modes.
9. Computes effective acceleration due to jittering, via JITTER.
10. Computes all relative accelerations via RELSEL.
11. Computes next time interval via TAUMAK.
12. Resets print and inflection times as needed.
13. Checks time for end of program: (1) if done, returns to MAIN, and, (2) if not done, updates time and continues.
14. Integrates body variables.
15. Integrates vehicle deceleration.
16. Returns to 3.

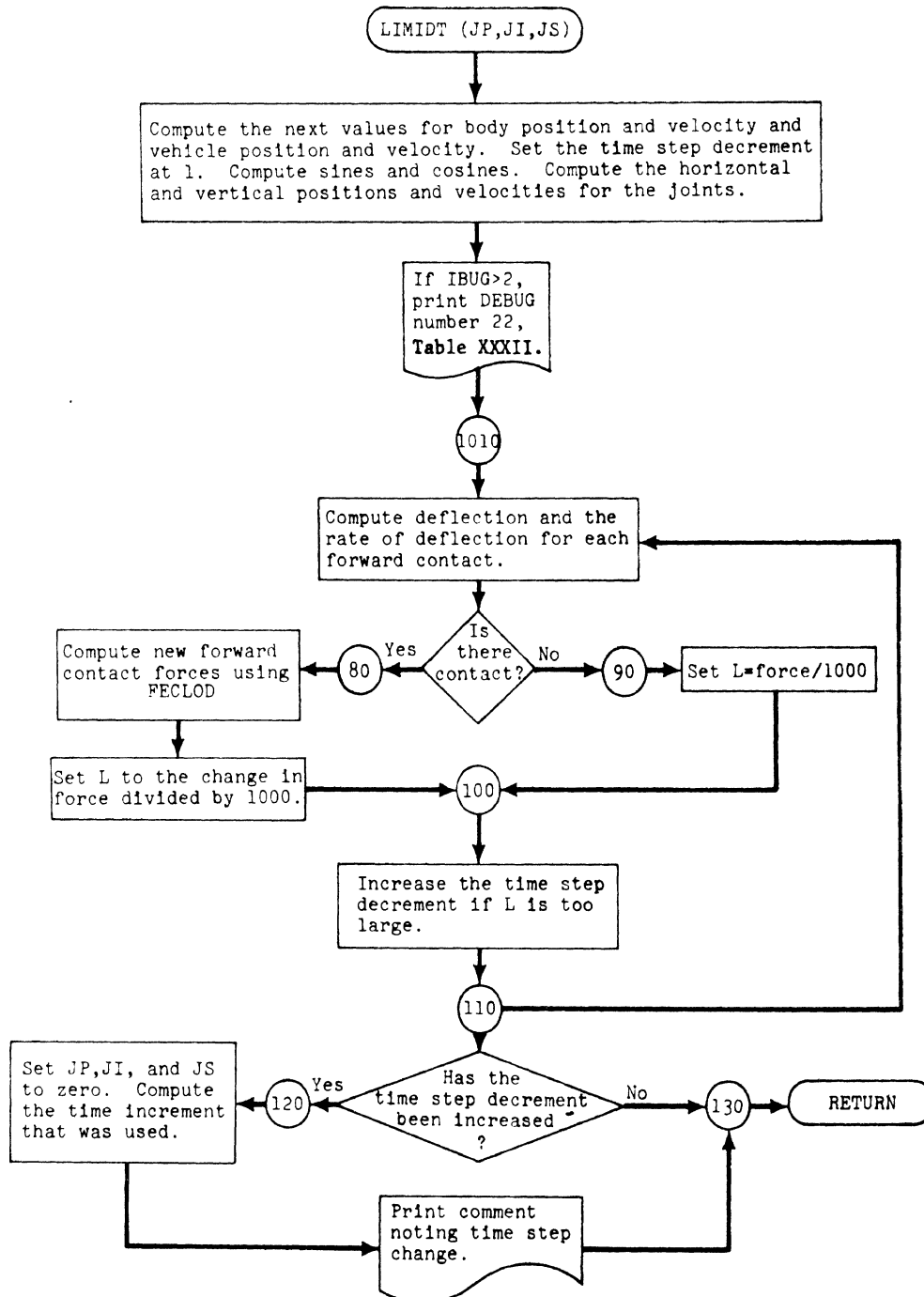


Next Page



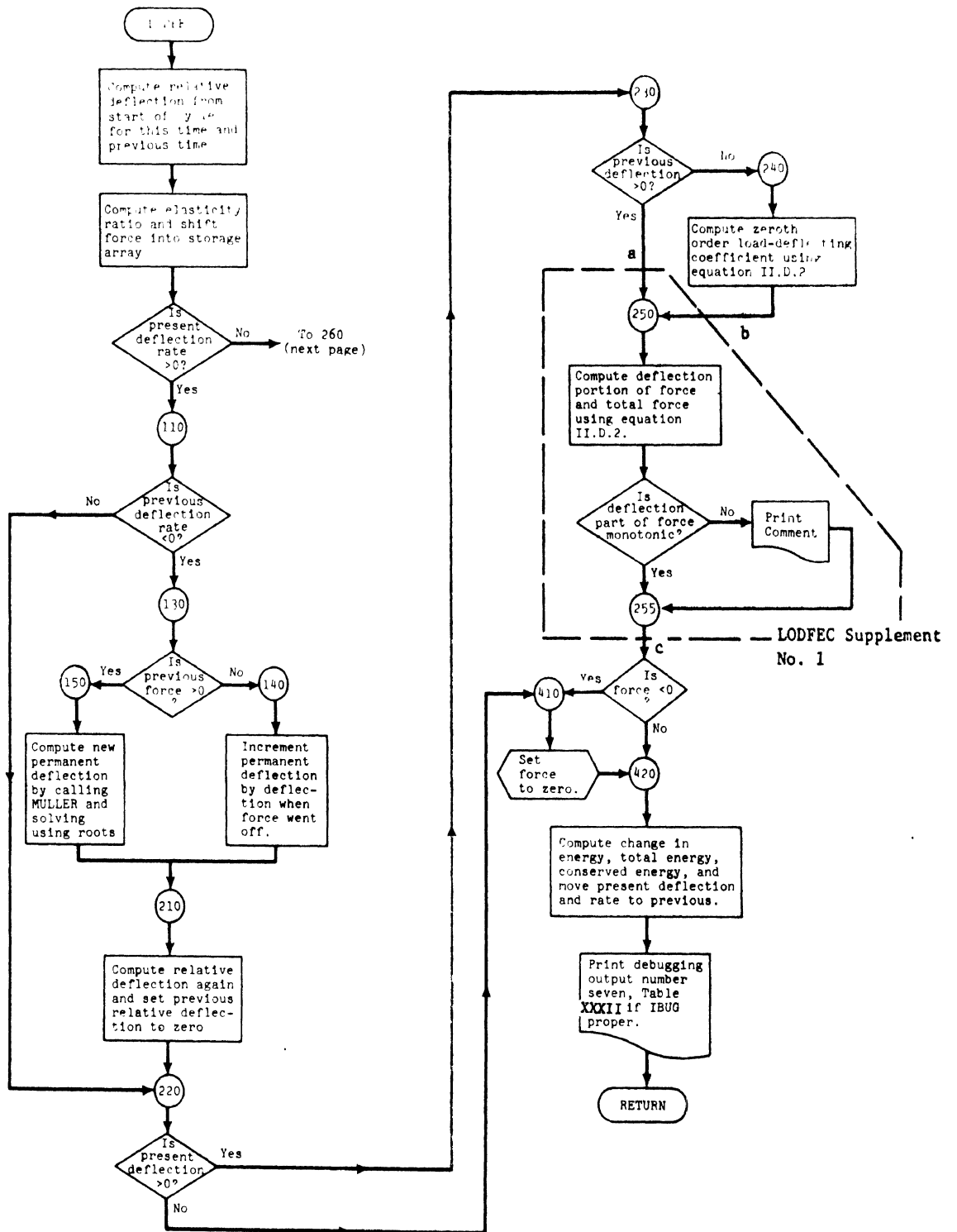
Subroutine LIMIDT carries out the following steps:

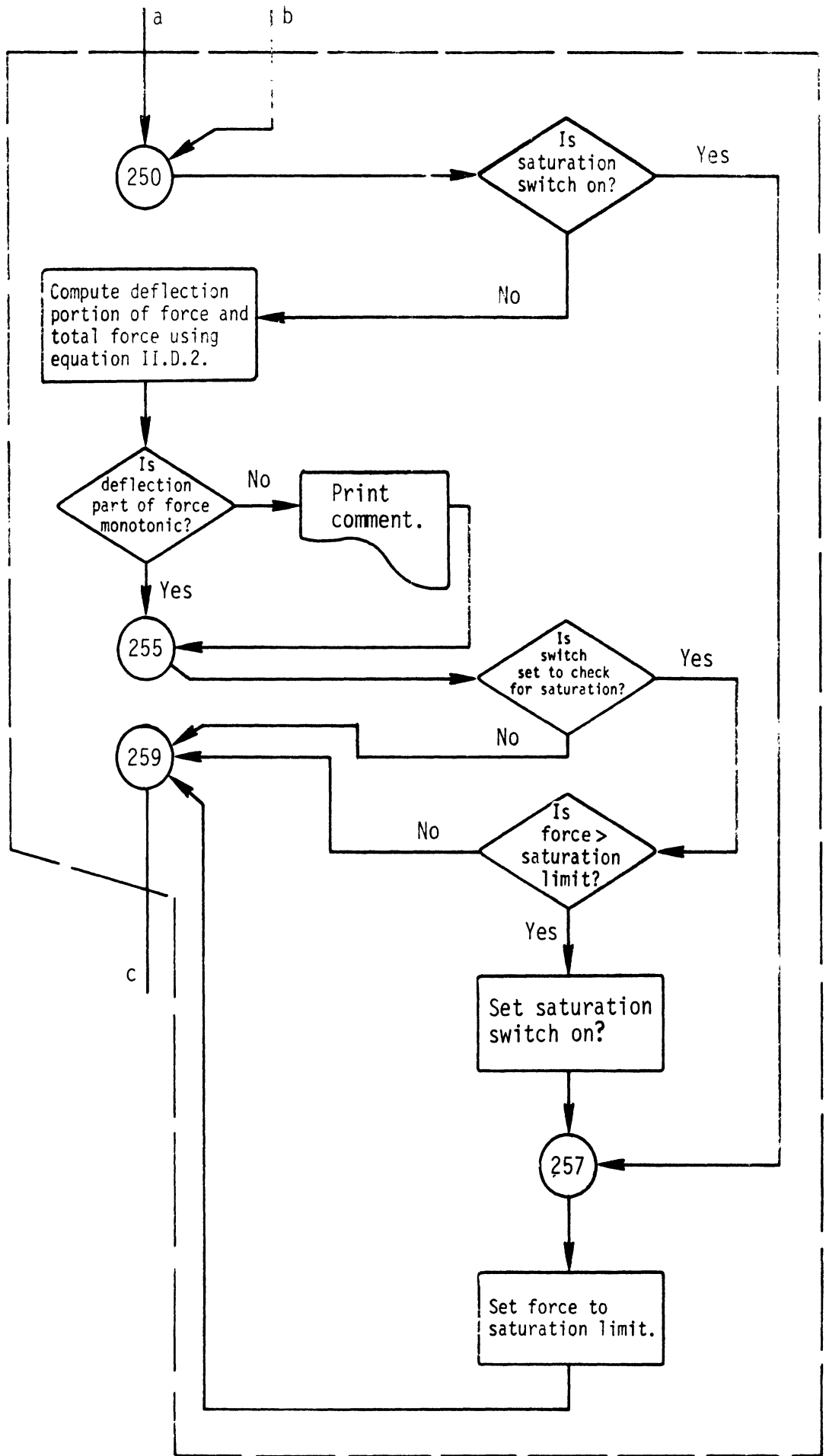
1. Integrates body variables forward to a tentative new time.
2. Computes new forward contact forces via FECLD.
3. Checks to see if changes in forces are more than 1000 lbs. If any one is, the time increment is decreased proportionately.

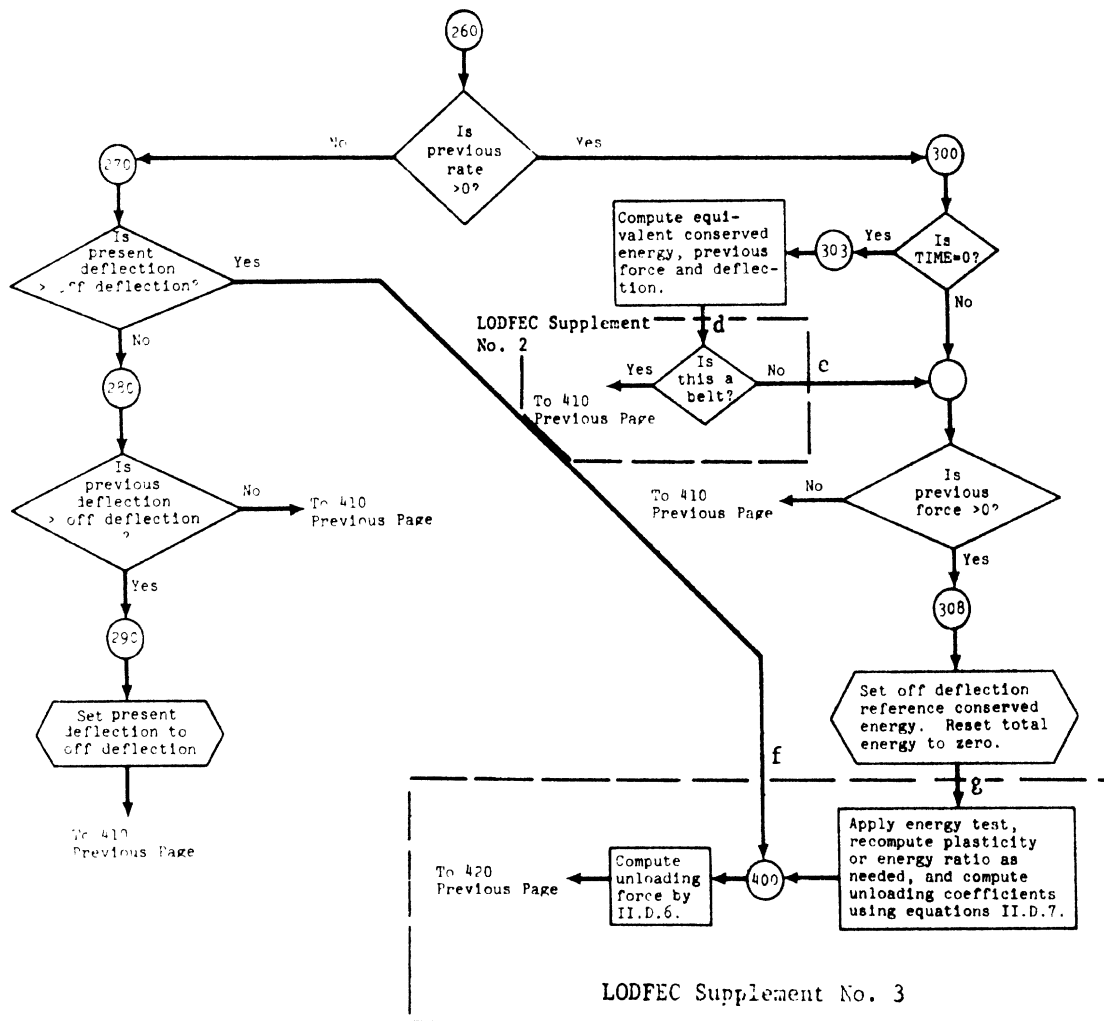


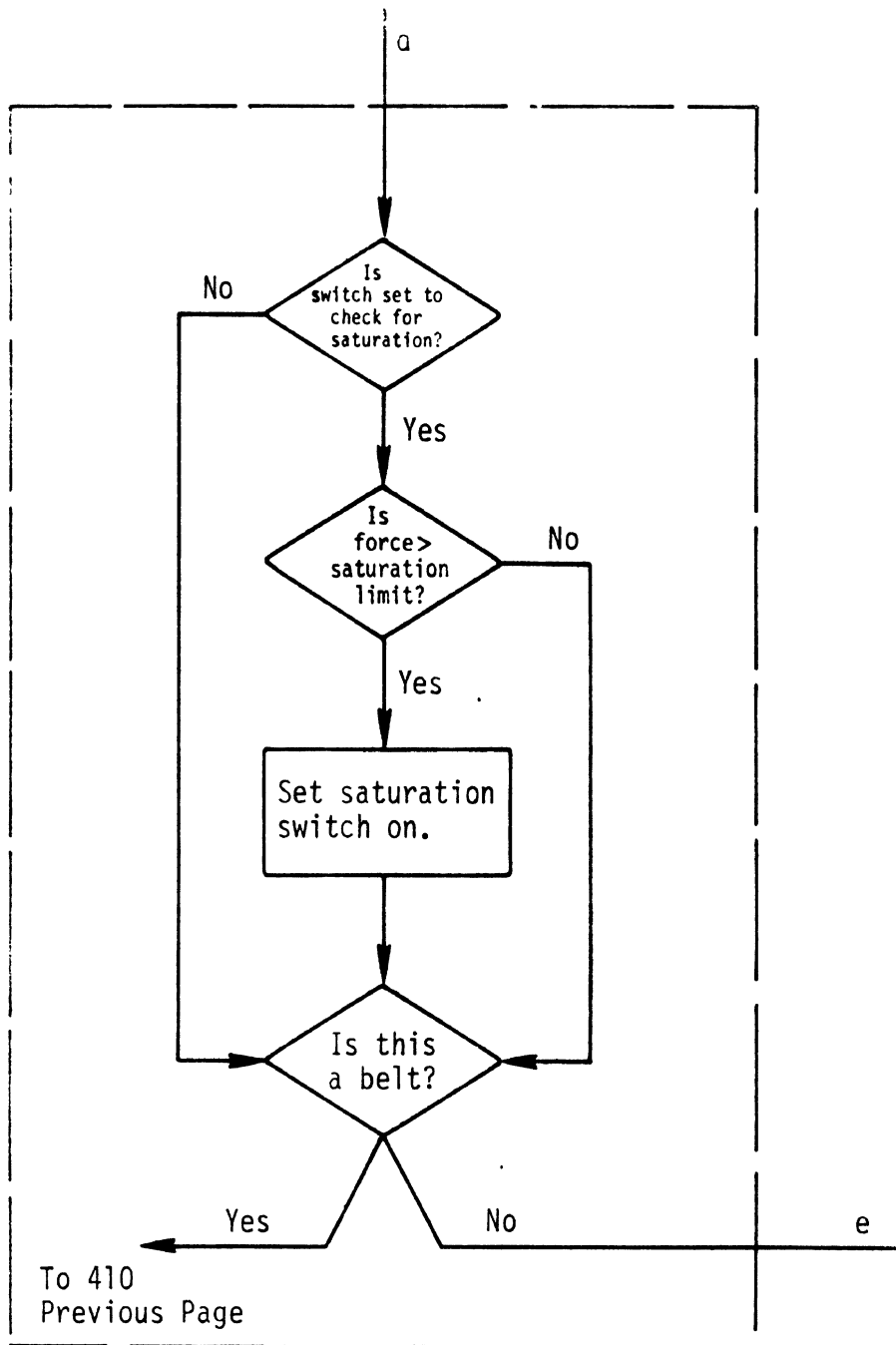
Subroutine LODFEC carries out the following steps:

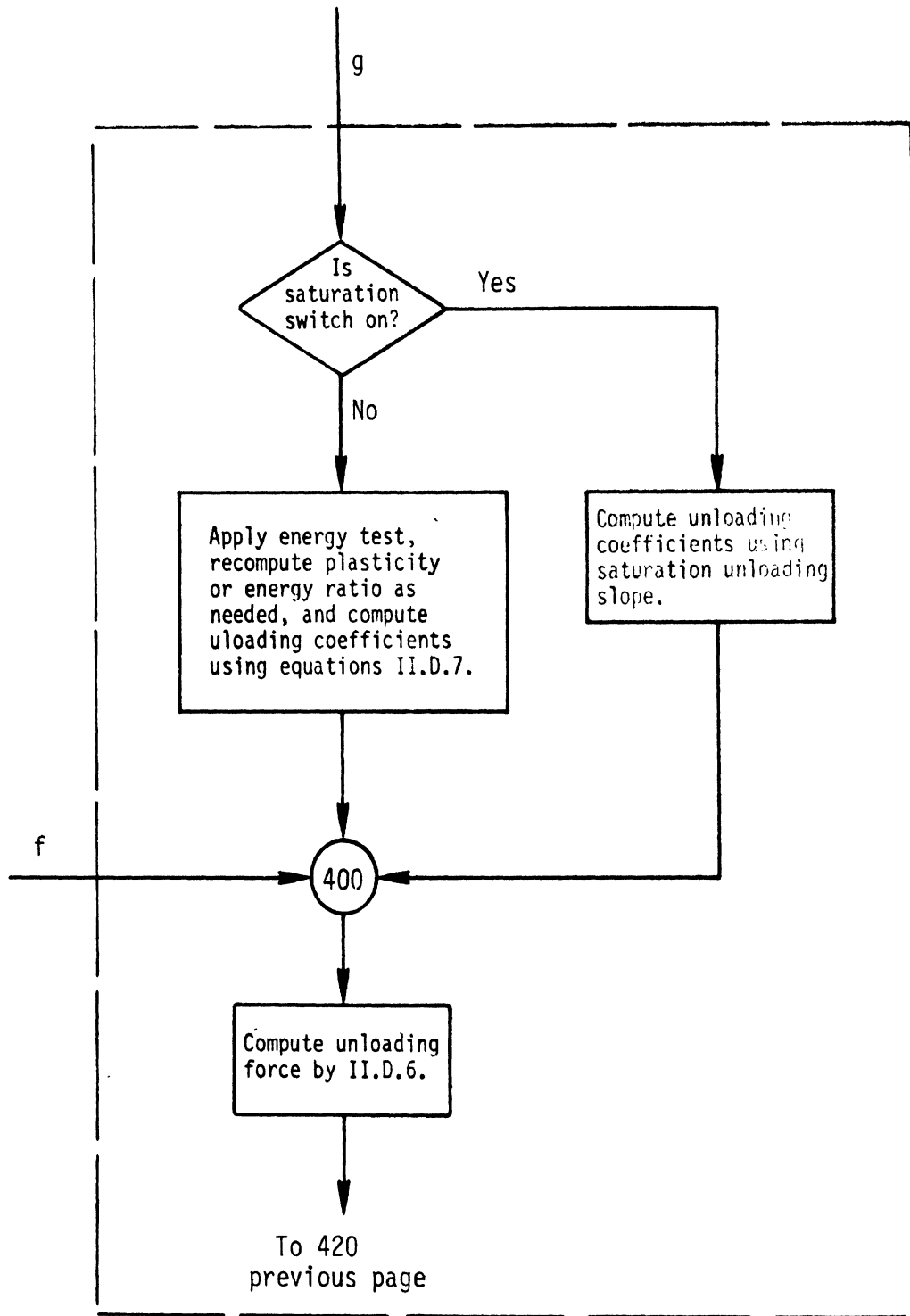
1. Determines whether external forces are on loading or unloading portion of force deformation profile.
2. If loading, forces are computed from fifth order polynomial in both deflection and rate.
3. If unloading, forces are computed from second order polynomial.
4. If in transition, the peak value is selected and coefficients for unloading computed.





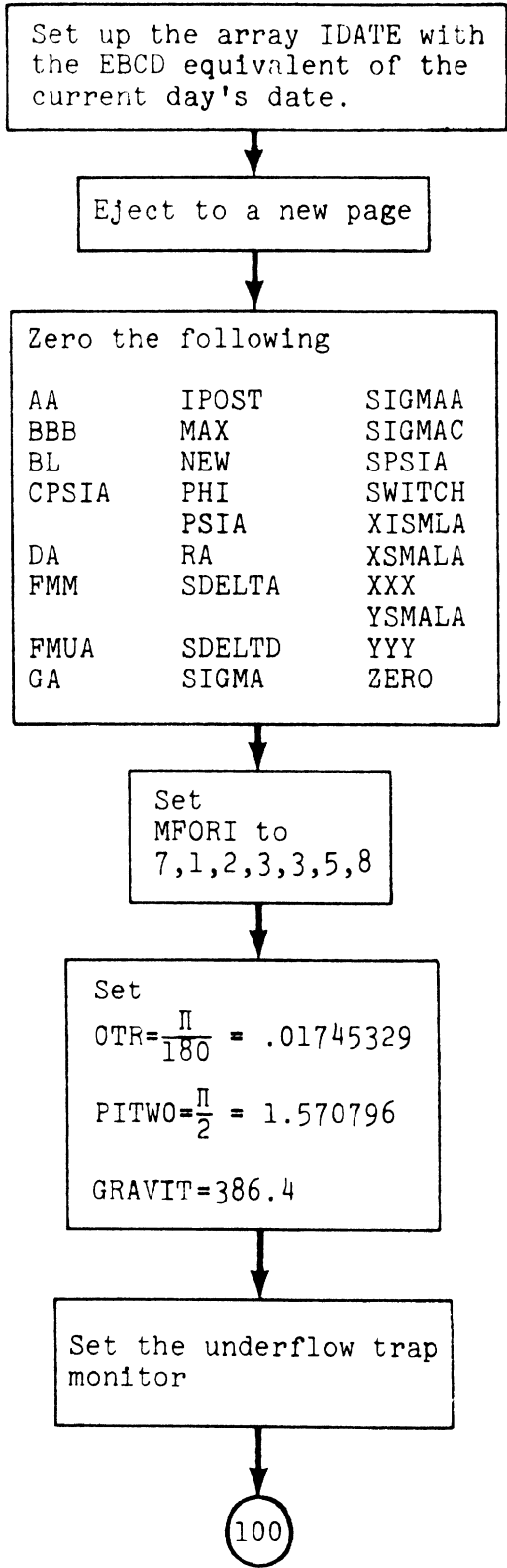


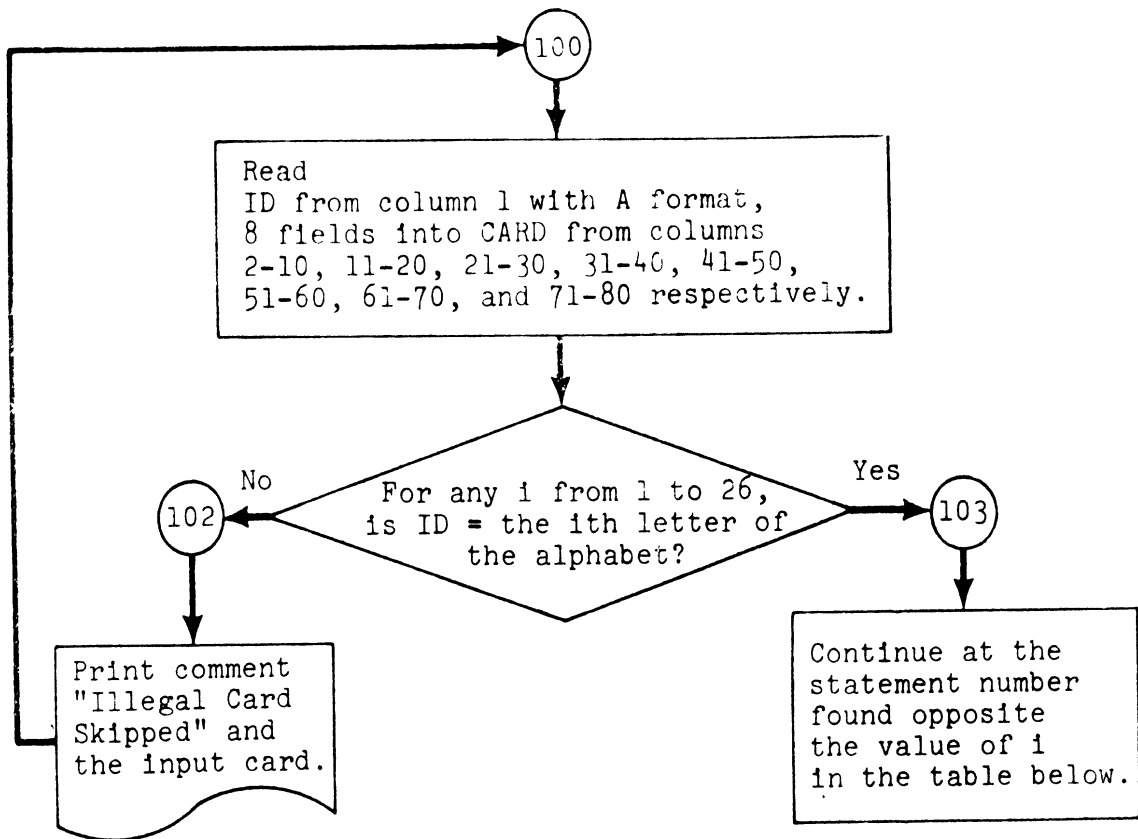




The main program carries out the following steps:

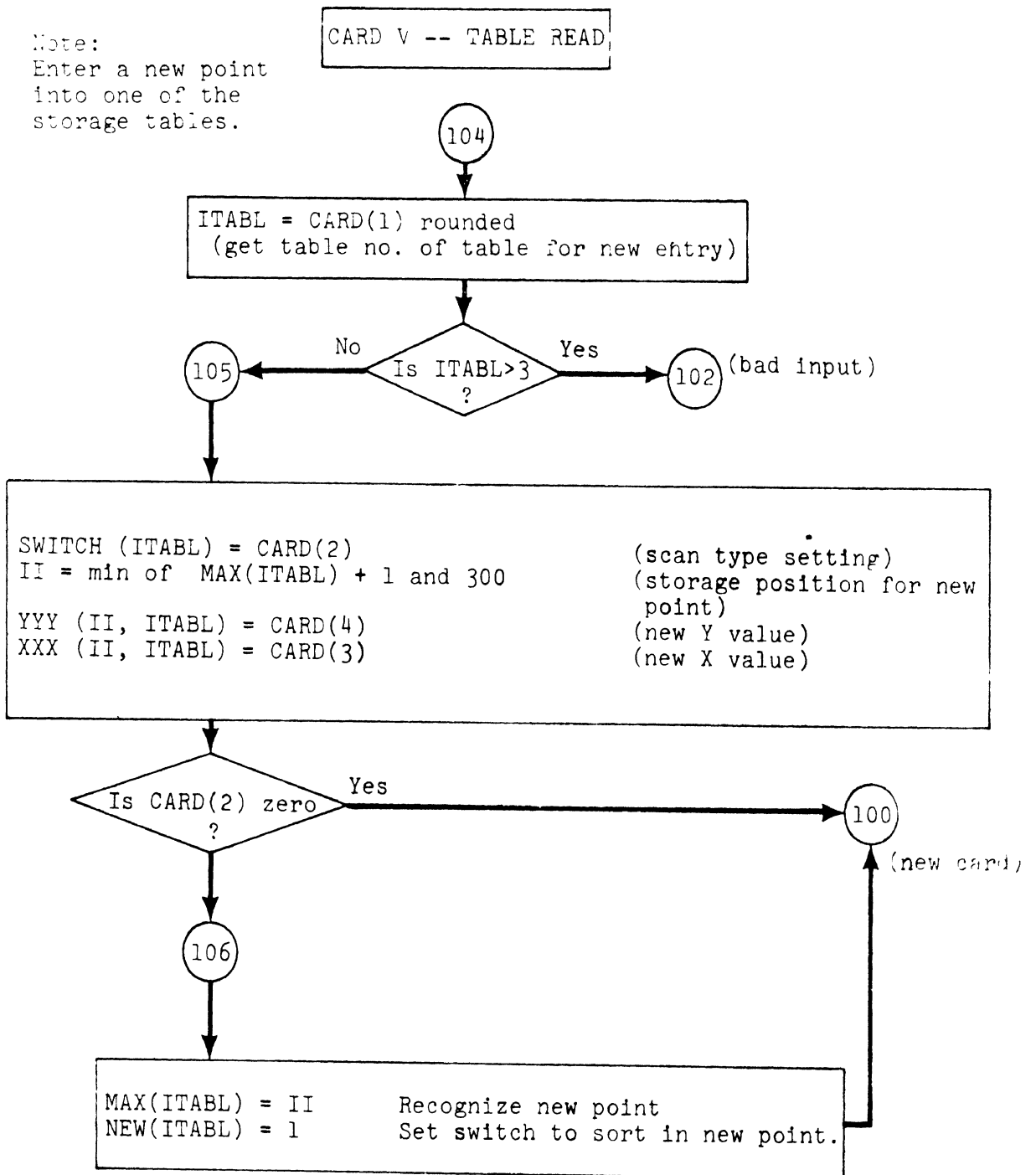
1. Zeroes some input and variables.
2. Defines some constants and tables.
3. Reads input data for amin program up to and including Z card.
4. Sets up table of contact indices for occupant and prints it out.
5. Sets up input deceleration and debug tables.
6. Prints out input data.
7. Computes constants.
8. Sets time to zero.
9. Rewinds buffer storage unit 9.
10. Calls KRUNCH.
11. Calls SUMMARY.
12. Reads additional data decks if any.



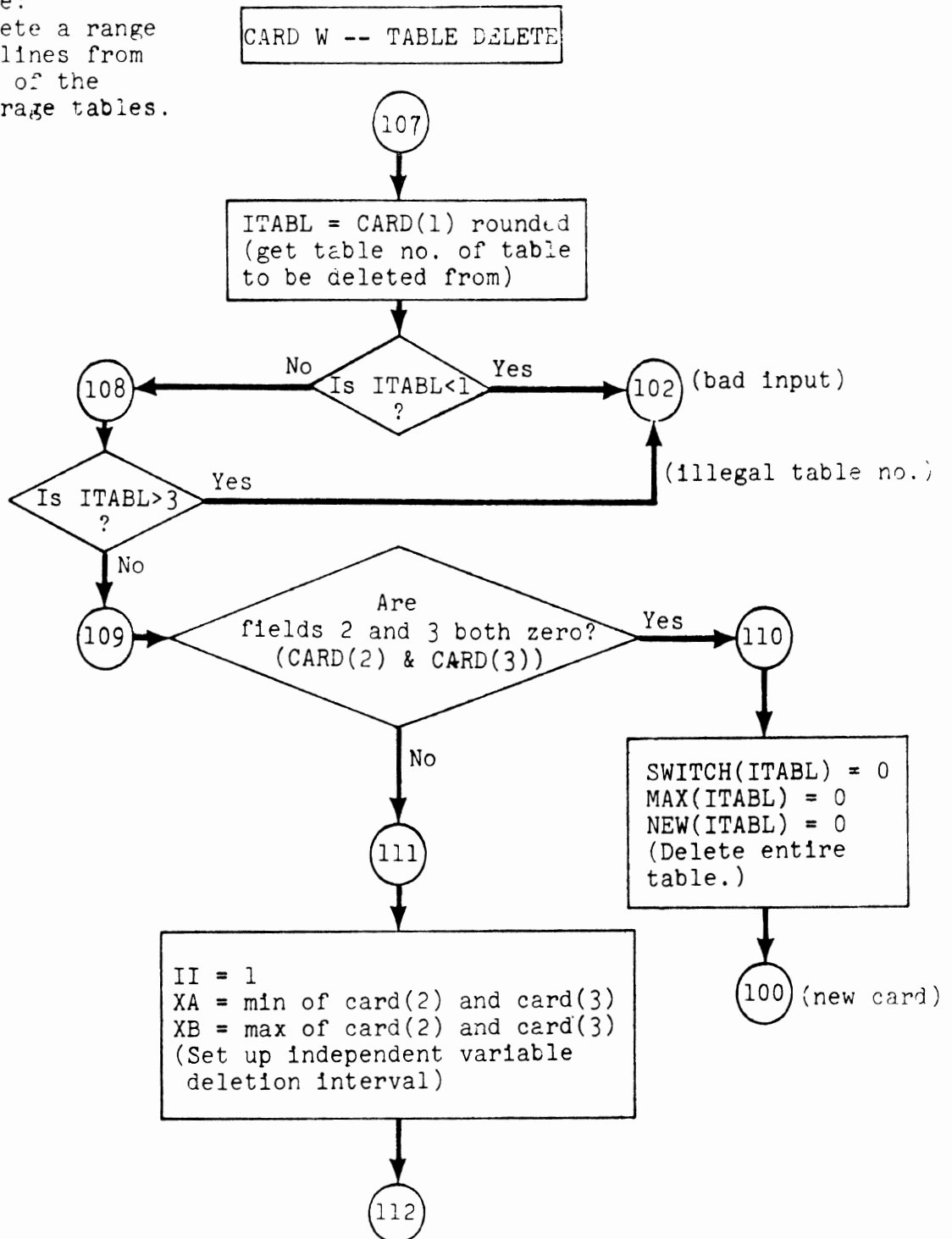


ID letter	i	Statement number	ID letter	i	Statement number
A	1	140	N	14	560
B	2	180	O	15	600
C	3	200	P	16	630
D	4	230	Q	17	660
E	5	260	R	18	700
F	6	300	S	19	730
G	7	330	T	20	760
H	8	360	U	21	800
I	9	400	V	22	104
J	10	430	W	23	107
K	11	460	X	24	850
L	12	500	Y	25	900
M	13	530	Z	26	1000

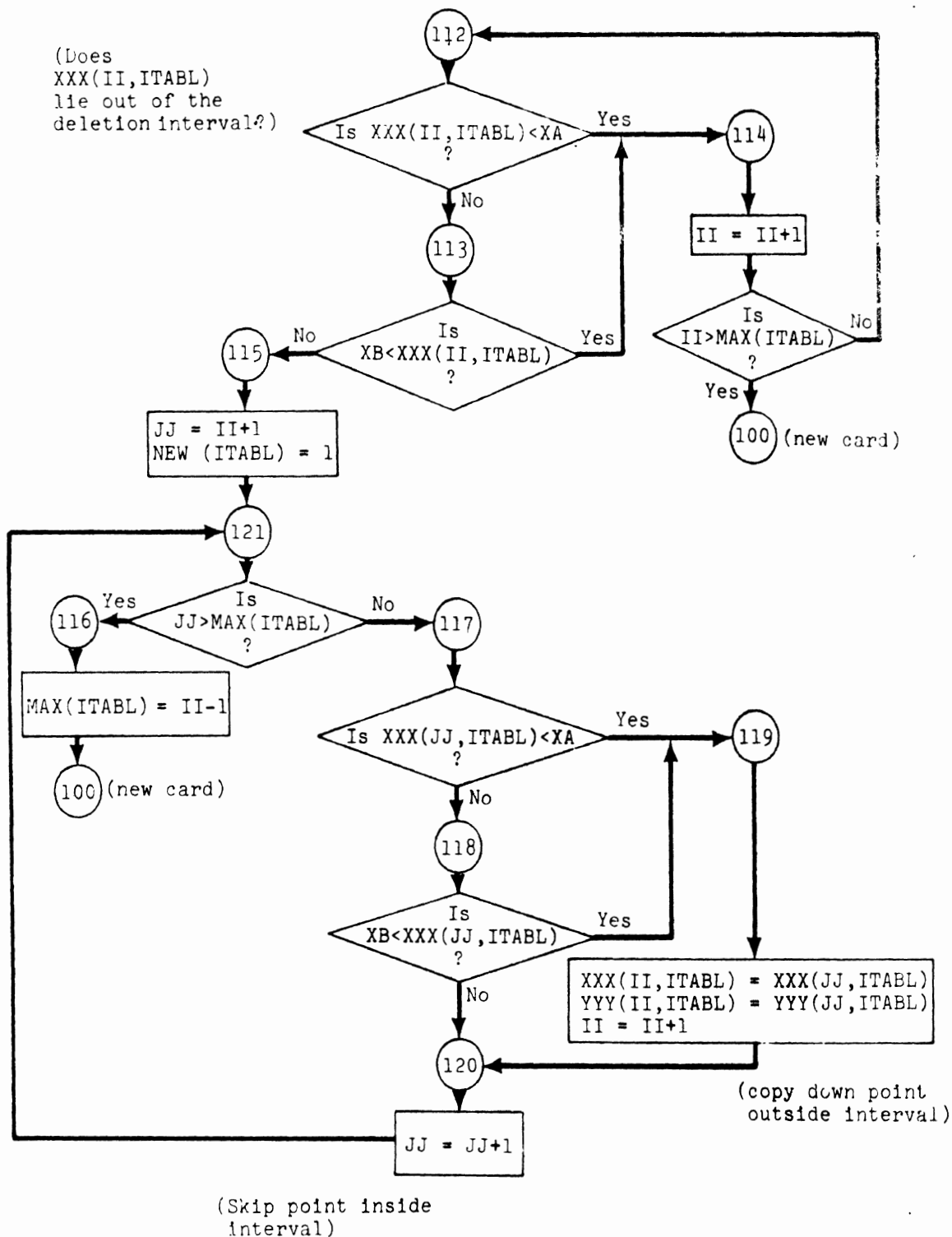
Note:
 Enter a new point
 into one of the
 storage tables.



Note:
Delete a range
of lines from
one of the
storage tables.



CARD W -- TABLE DELETE (cont)



CARD A

140

Copy CARD elements one through seven into CPRIME one through seven.

100 (new card)

CARD B

180

Copy CARD elements one through eight into EYE one through eight.

100 (new card)

CARD C

200

Copy CARD elements one through seven into BIGKI one through seven.

100

CARD D

230

Copy CARD elements one through eight into EL one through eight.

100

CARD E

260

Copy CARD elements one through eight into EM one through eight.

EMFVSX = EM(5)+EM(6) (sum of 5,6)
EMTHSX = Sum of 3,4,5,6
EMTWSX = Sum of 2,3,4,5,6

100

CARD F

300

Copy CARD elements one through eight into AR one through eight.

100

CARD G

330

Copy CARD elements one through seven into TPRIME one through seven.

100

CARD H

360

Copy CARD elements one through four into ALFAI elements one, five, six, and seven, converting them from degrees to radians.

Copy CARD elements five through eight into THATPW, THATPV, THATPX, and THATPS, respectively.

100

CARD I

400

Copy CARD elements one through seven into OMEGA elements one through seven, converting them from degrees to radians.

100

CARD J

430

Copy CARD elements one through seven into RPSI elements one through seven, converting them from degrees to radians.

100

CARD K

460

Copy CARD elements one through eight into RHO elements one through eight.

100

CARD L

500

Copy CARD elements one through eight into THETAZ elements one through eight, converting them from degrees to radians. Simultaneously compute the sine and cosine for each element of THETAZ and store them in the corresponding elements of STHETZ and CTHETZ respectively.

100

CARD M

530

Copy CARD elements one, two, four, five, and six to FSPRMZ, RH, XZERO, RHOPTZ, and RHOPFZ respectively.

Convert CARD(7) from degrees to radians and put it in GAMZER.

Put the rounded absolute value of CARD(8) into LCONTL as an integer.

100

CARD N

560

Copy CARD elements one through eight into CS, S, RPSI(8), FMUC, BETA elements one through three, and ZZERO respectively.

100

CARD O

600

Copy CARD elements one through eight into ELPTEN, ELTWTY, ELTHRY, H, FEPTEN converting from degrees to radians, DESTEP, RZ, and SZ respectively.

Set DELTAT = DESTEP

100

CARD P

630

Put the rounded value of CARD(1) into M as an integer.

Is M in the range one to three?

no

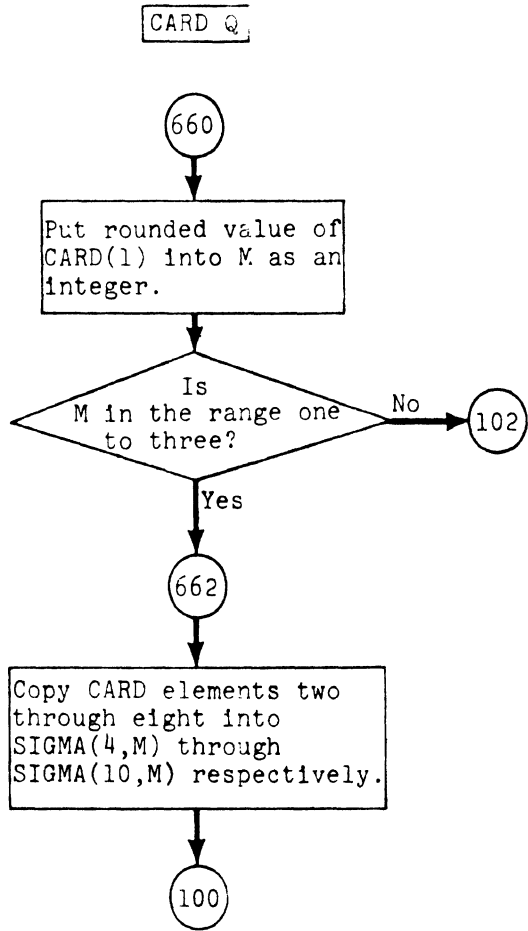
102

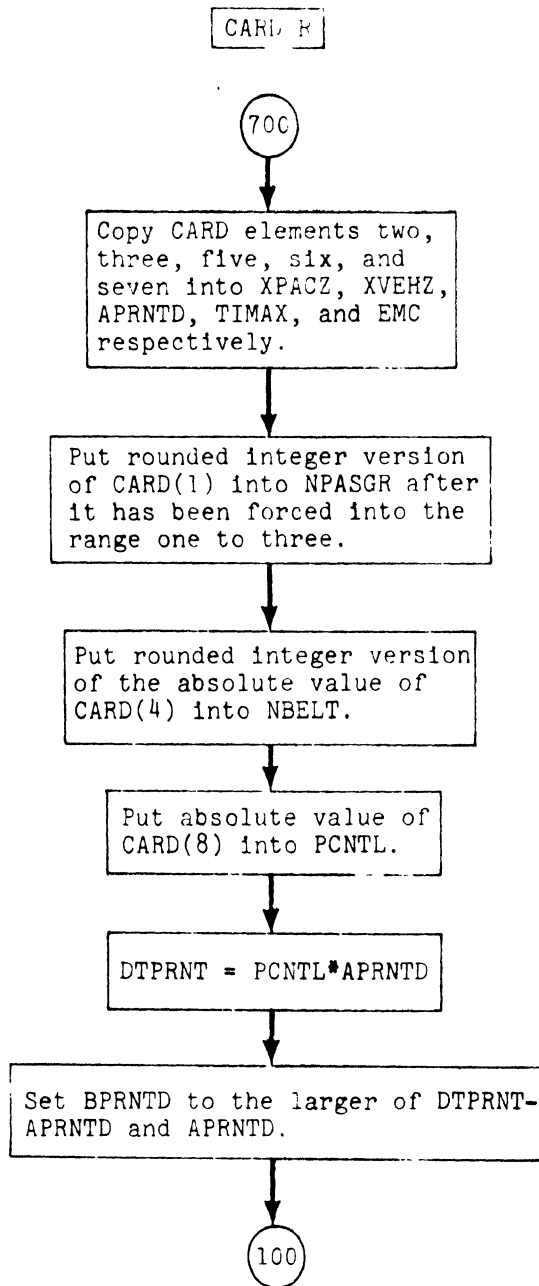
yes

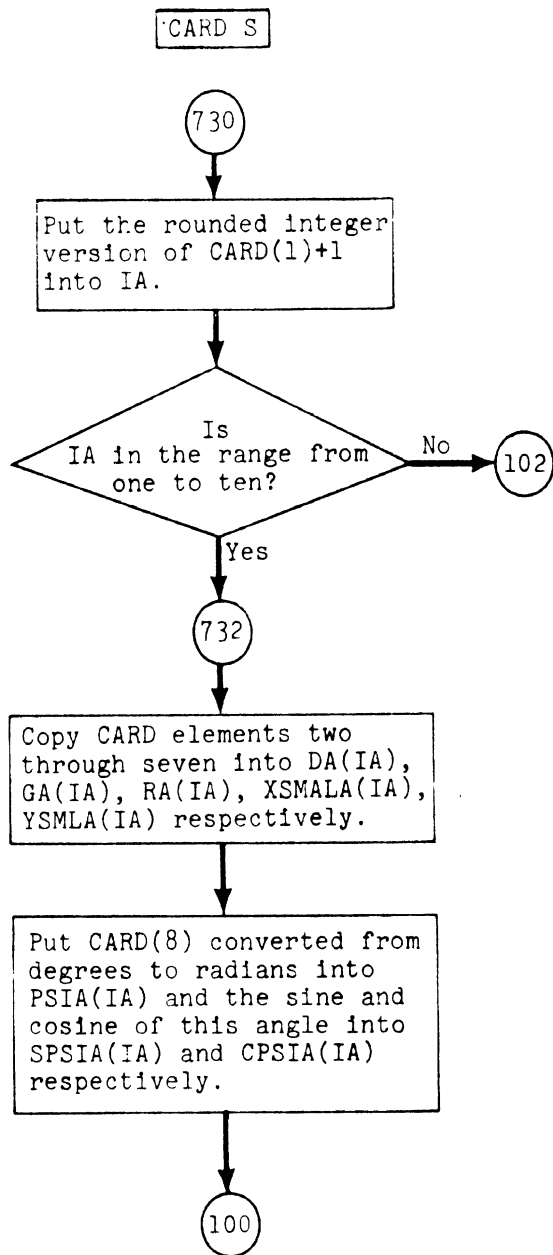
632

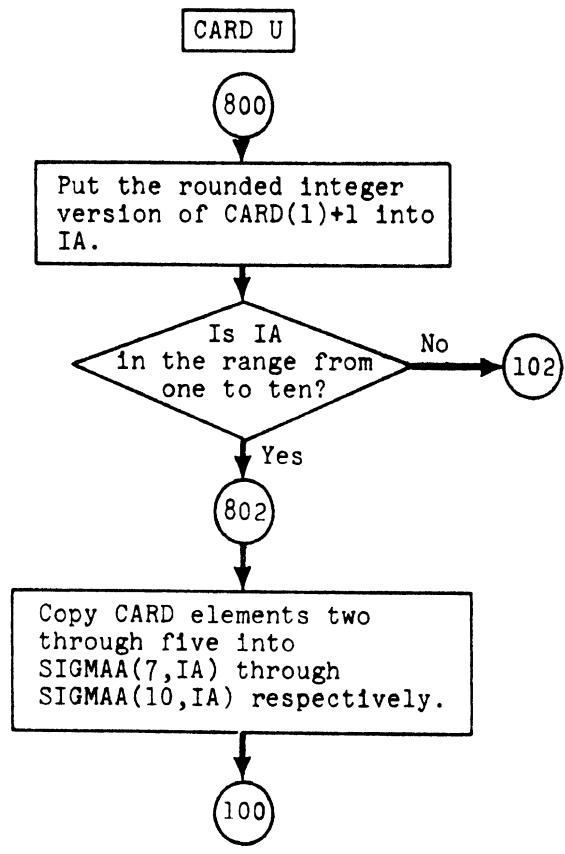
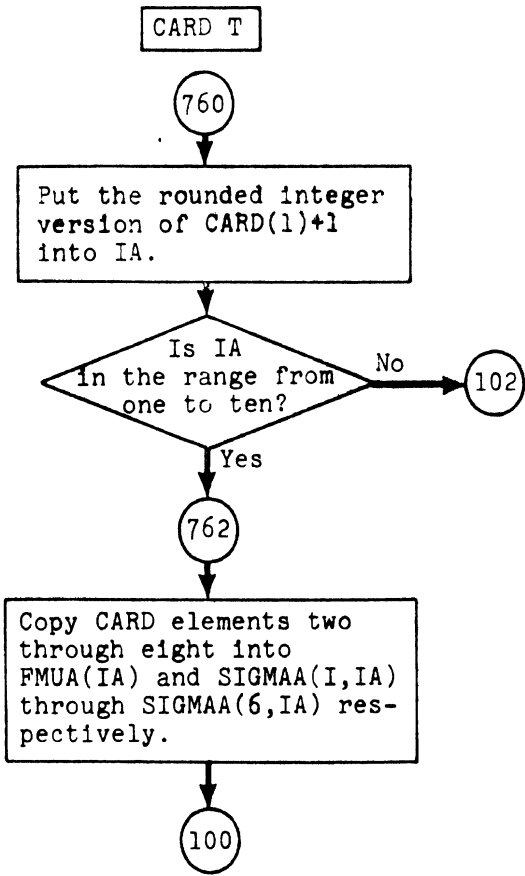
Copy CARD elements two through eight into G(M), R(M), PHIZ(M), DELTA(M), SIGMA(1,M), SIGMA(2,M), SIGMA(3,M) respectively, converting CARD(4) from degrees to radians before storing it in PHIZ(M).

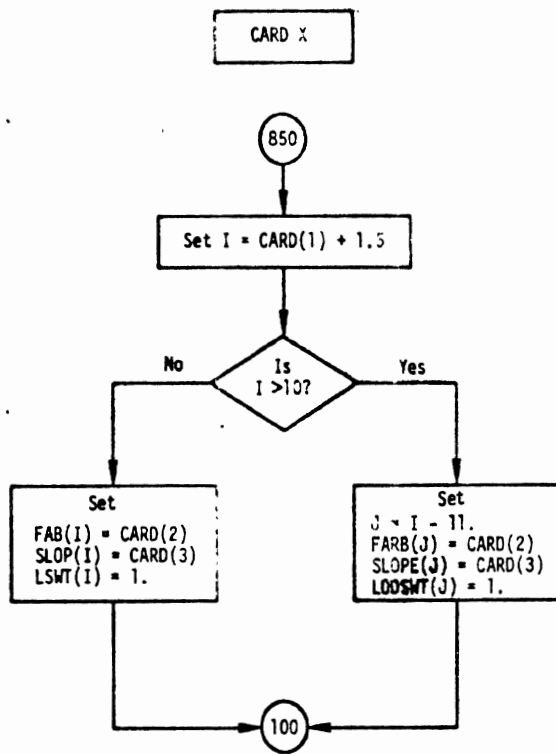
100











CARD Y

900

100 (Skip Card)

CARD Z

1000

Is CARD(1) < 0?

No

3000

Yes

(Use present table 2 for DB output)

3020

Set up Table 2 to be constant value for all time of CARD(1).

Zero out 18 elements of SIGZ and 28 elements of KTABLE.

Compare NPASGR to 2

1

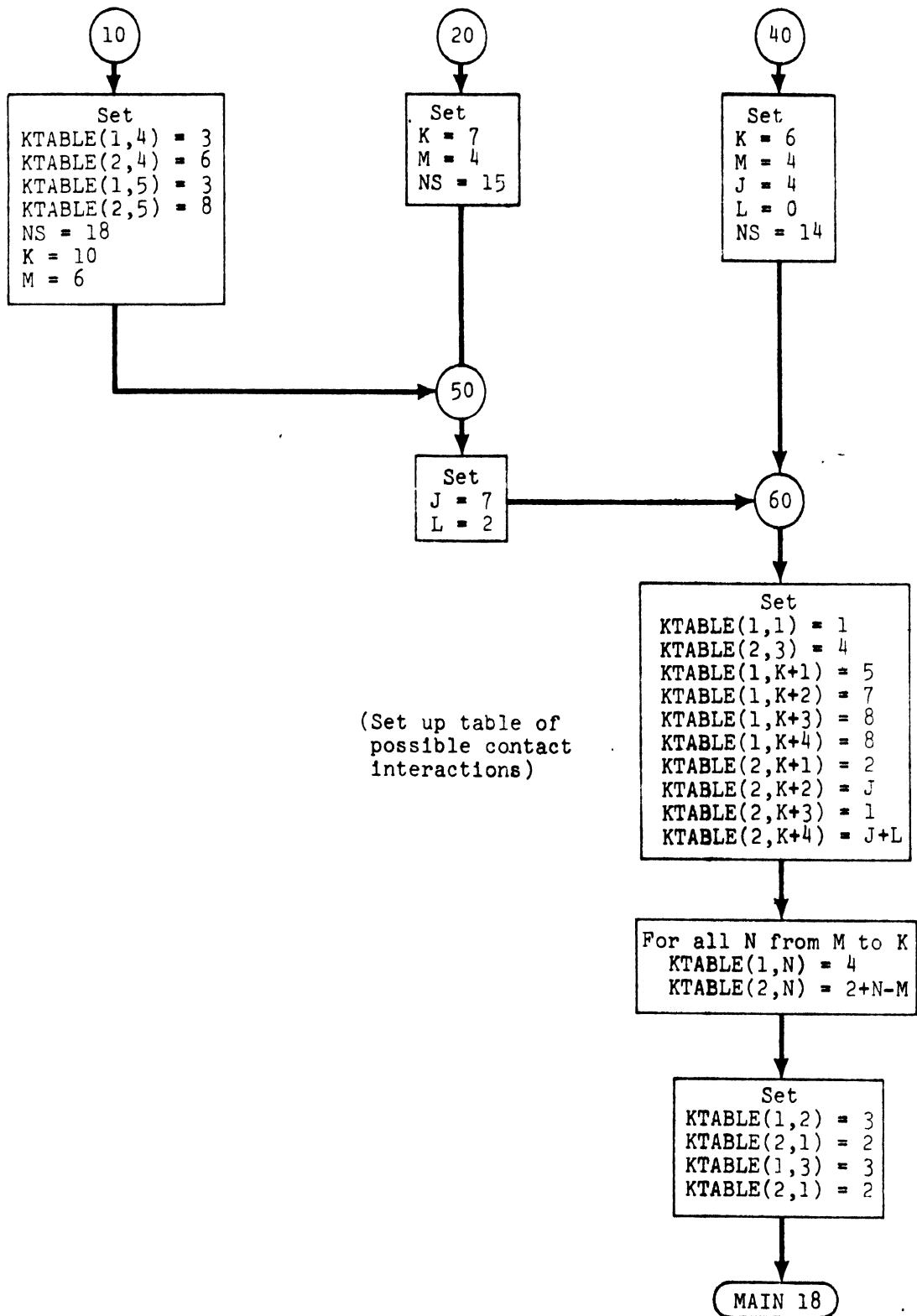
10

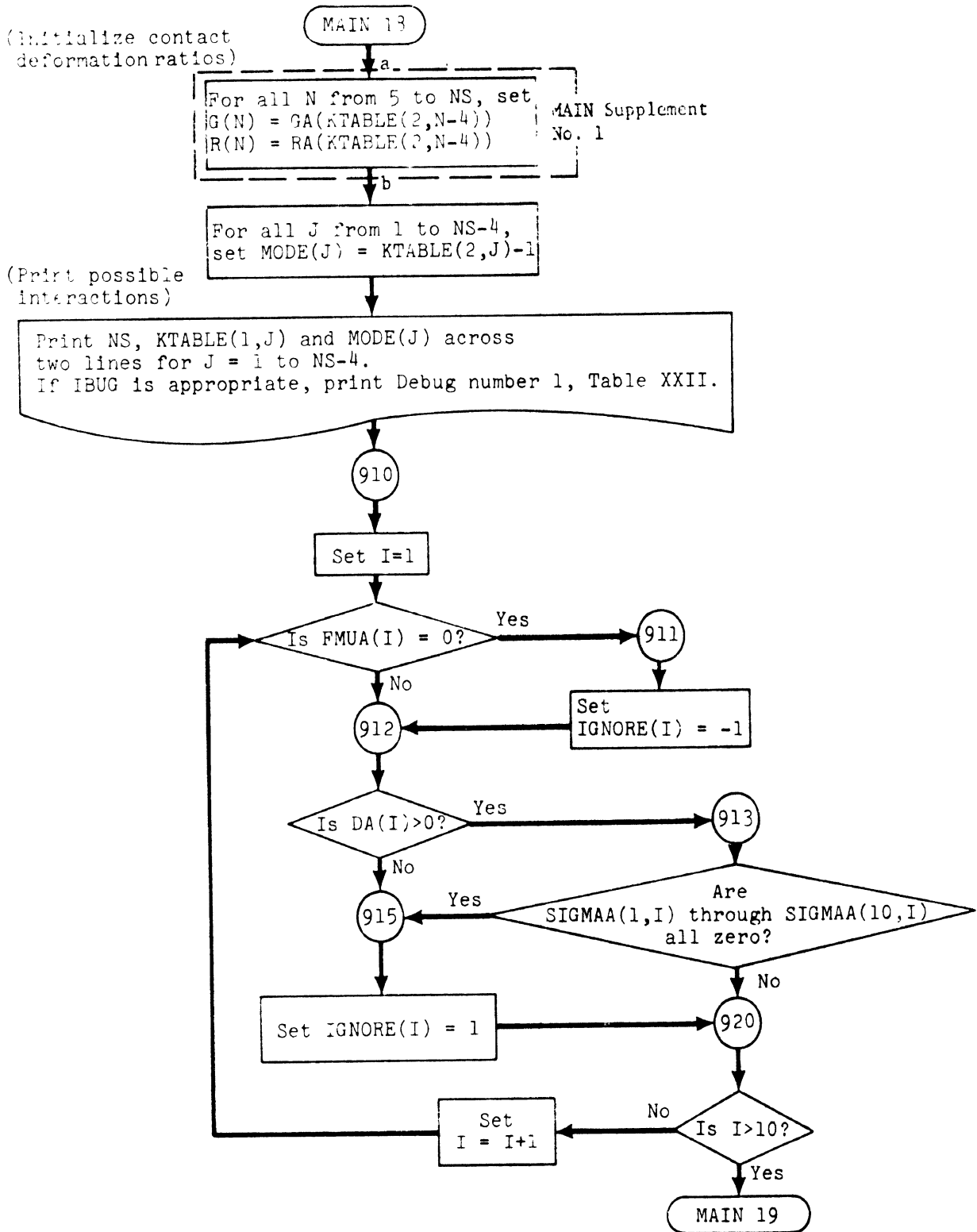
2

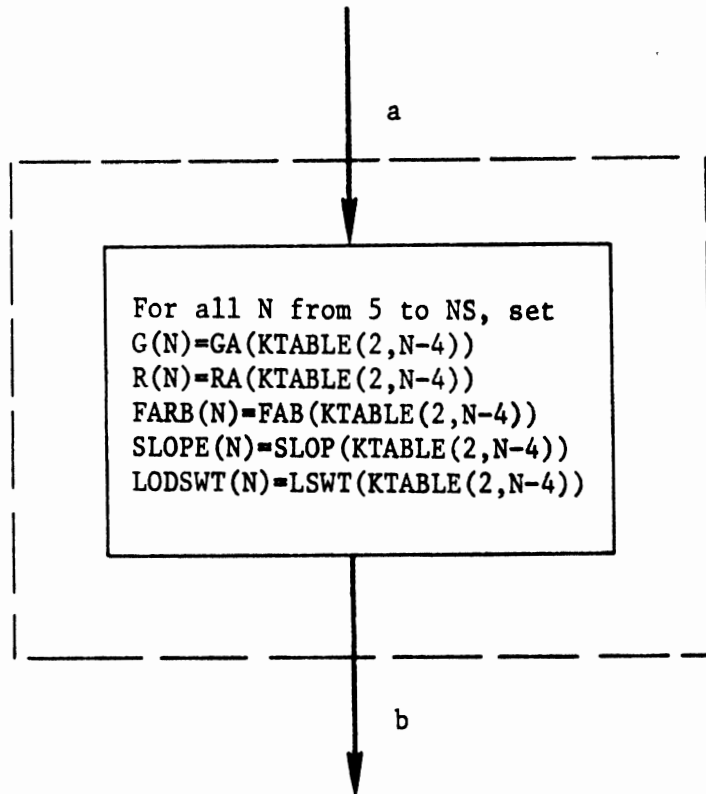
30

3

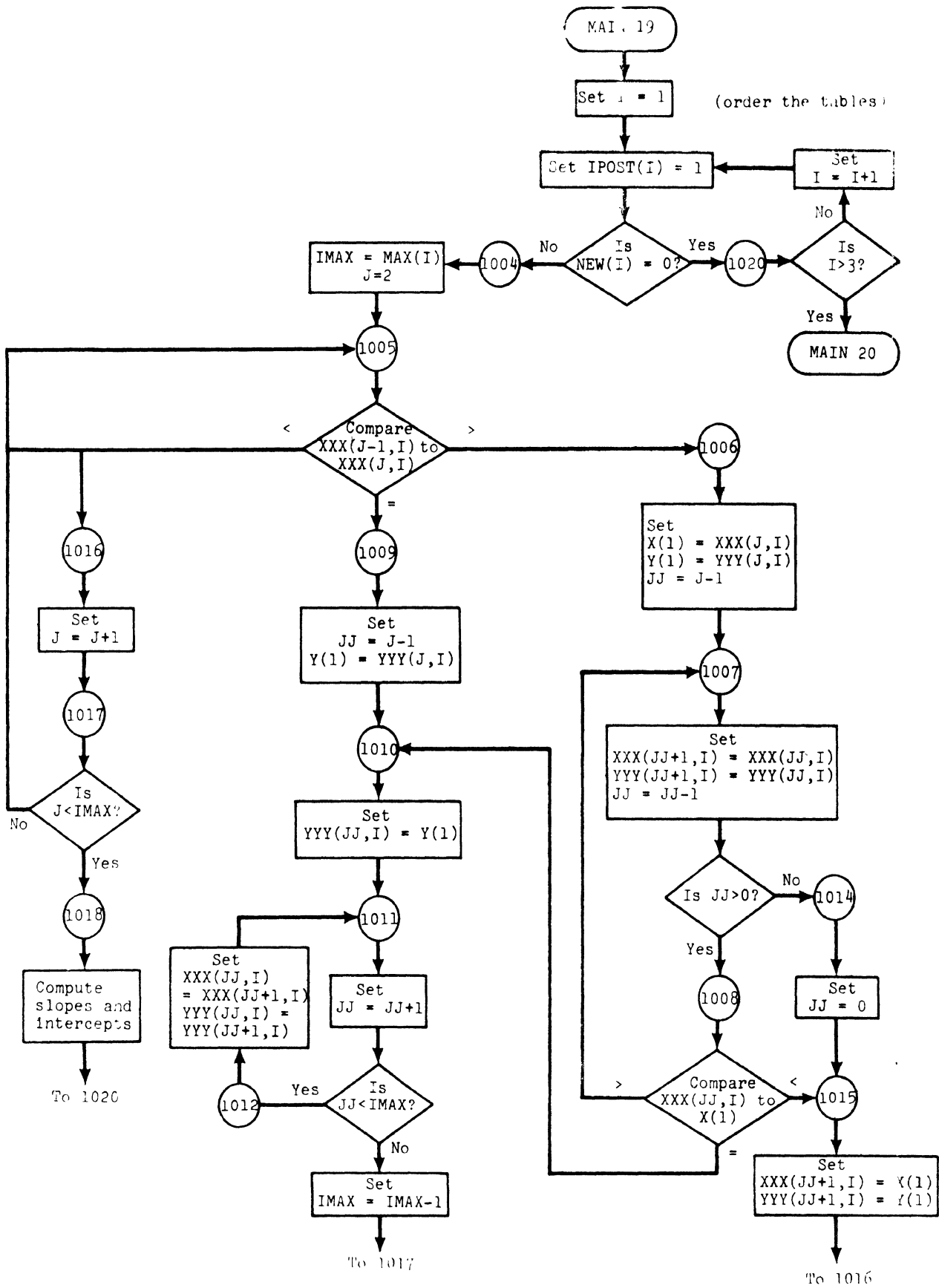
40

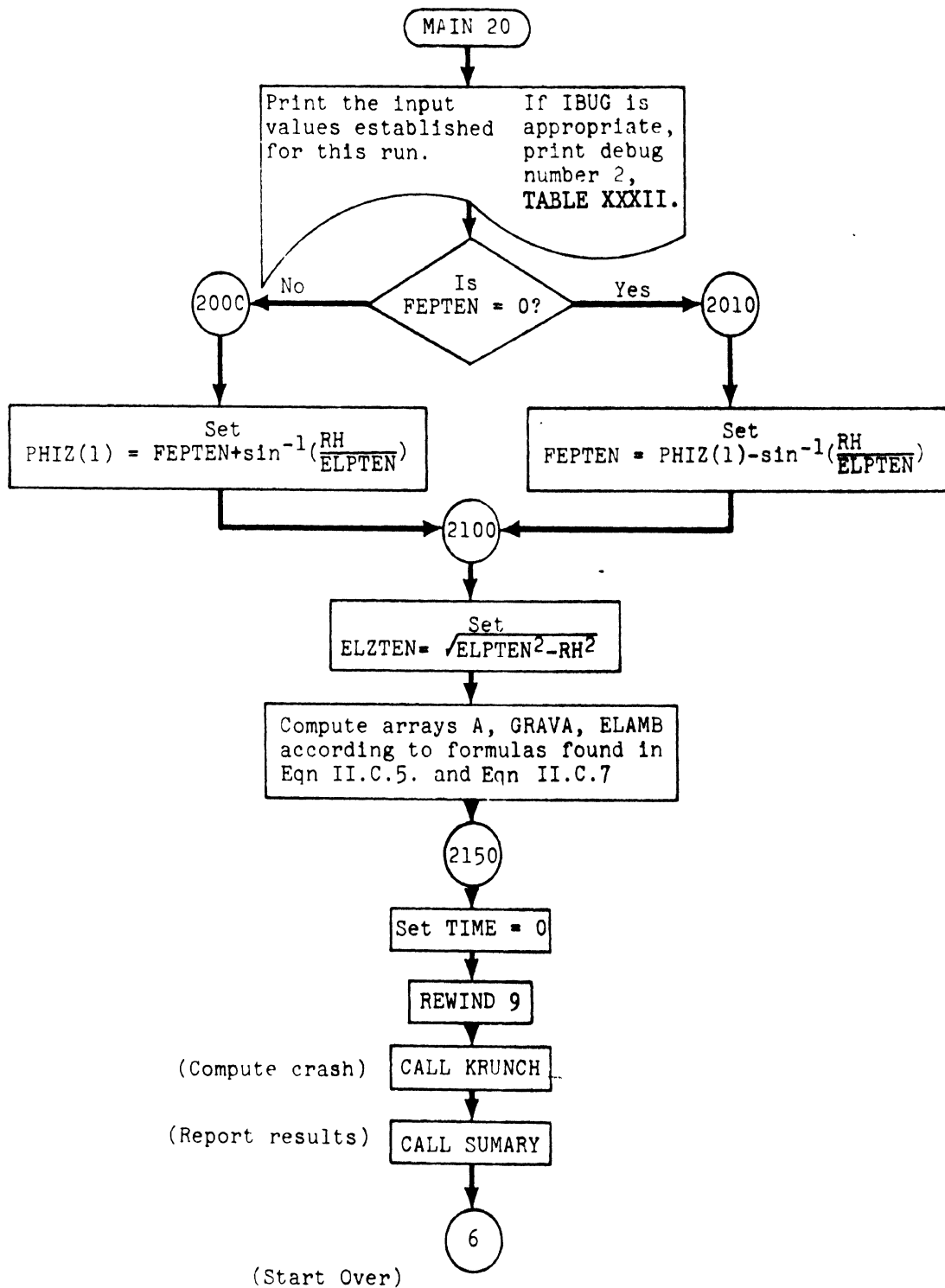






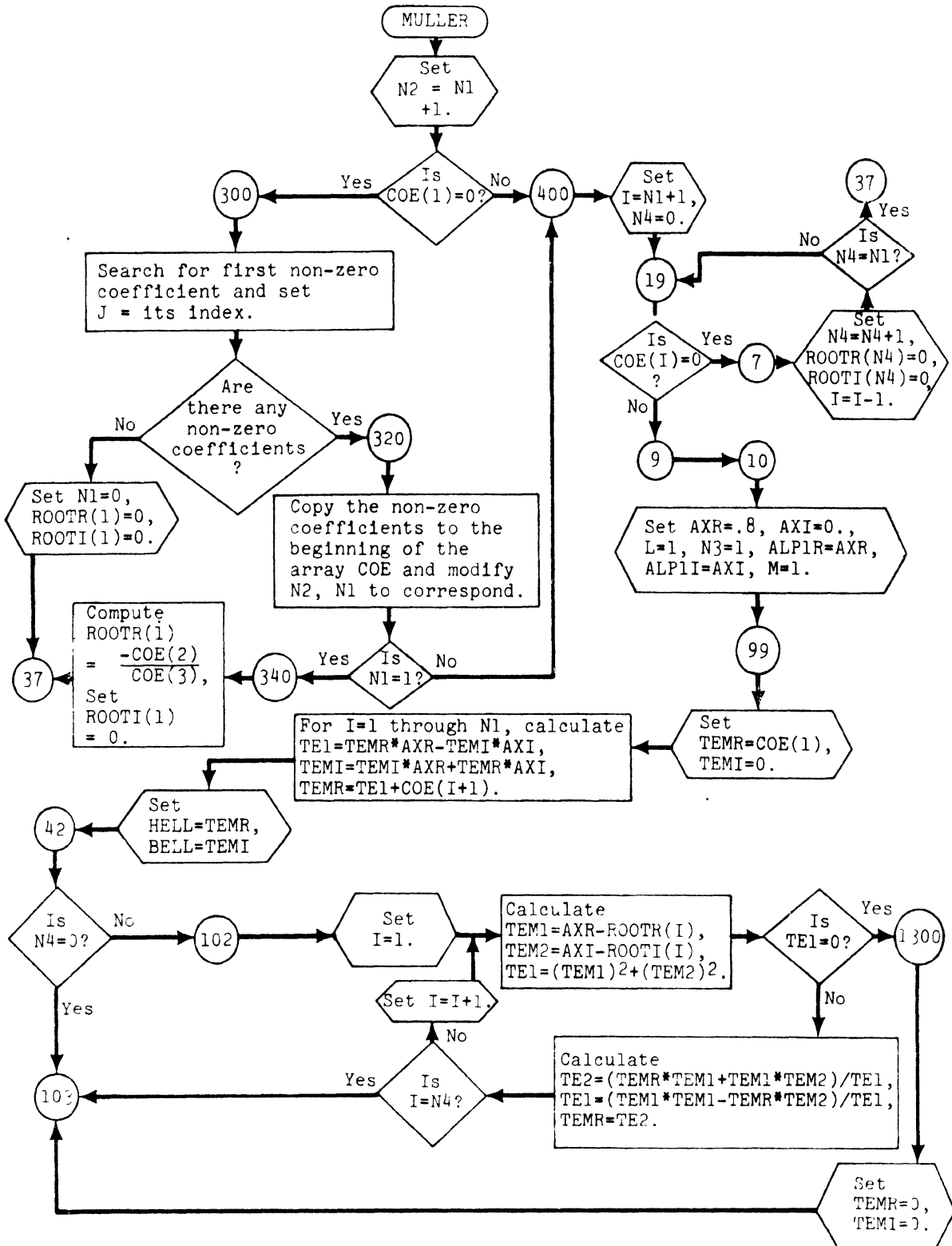
MAIN Supplement No. 1

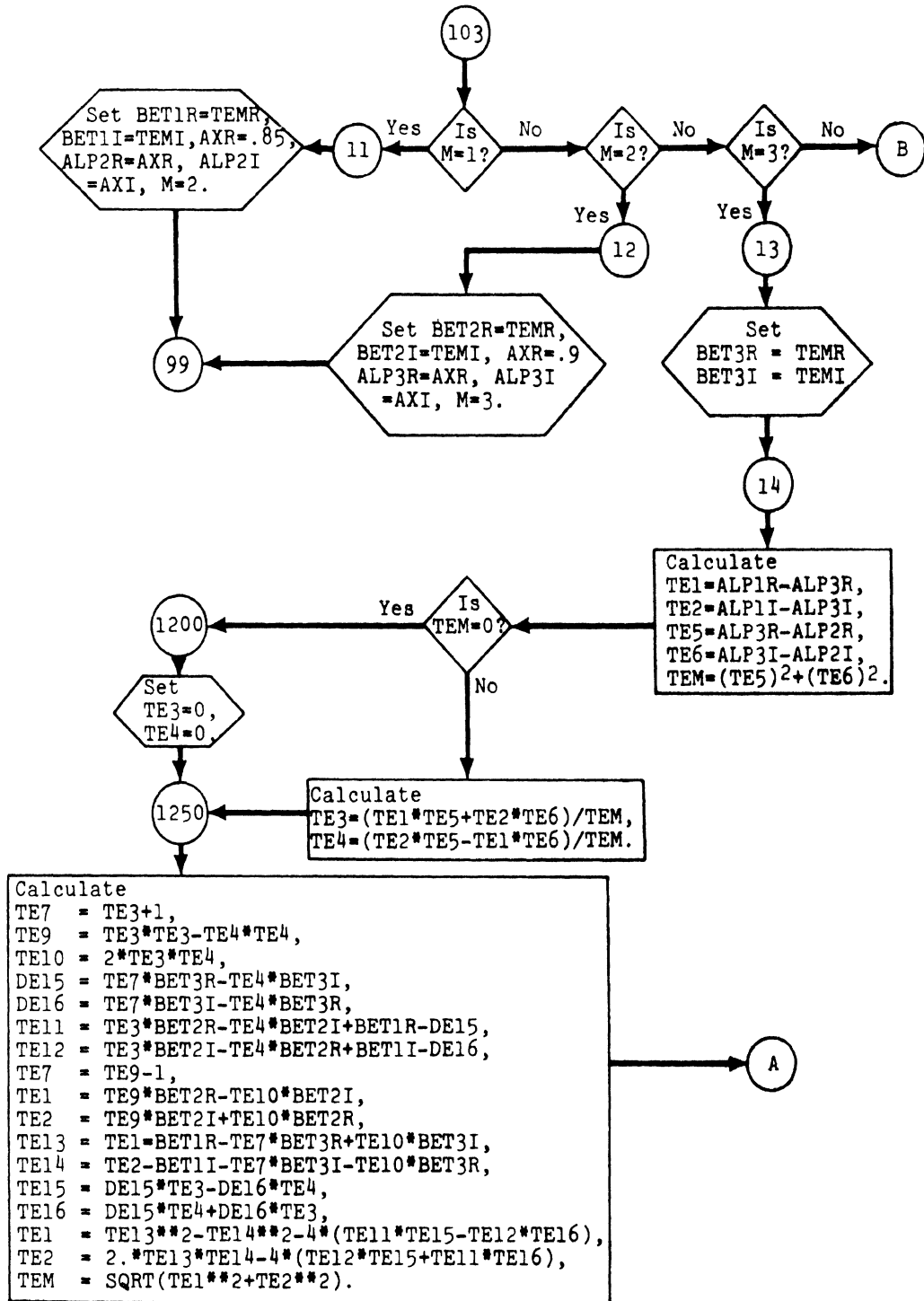


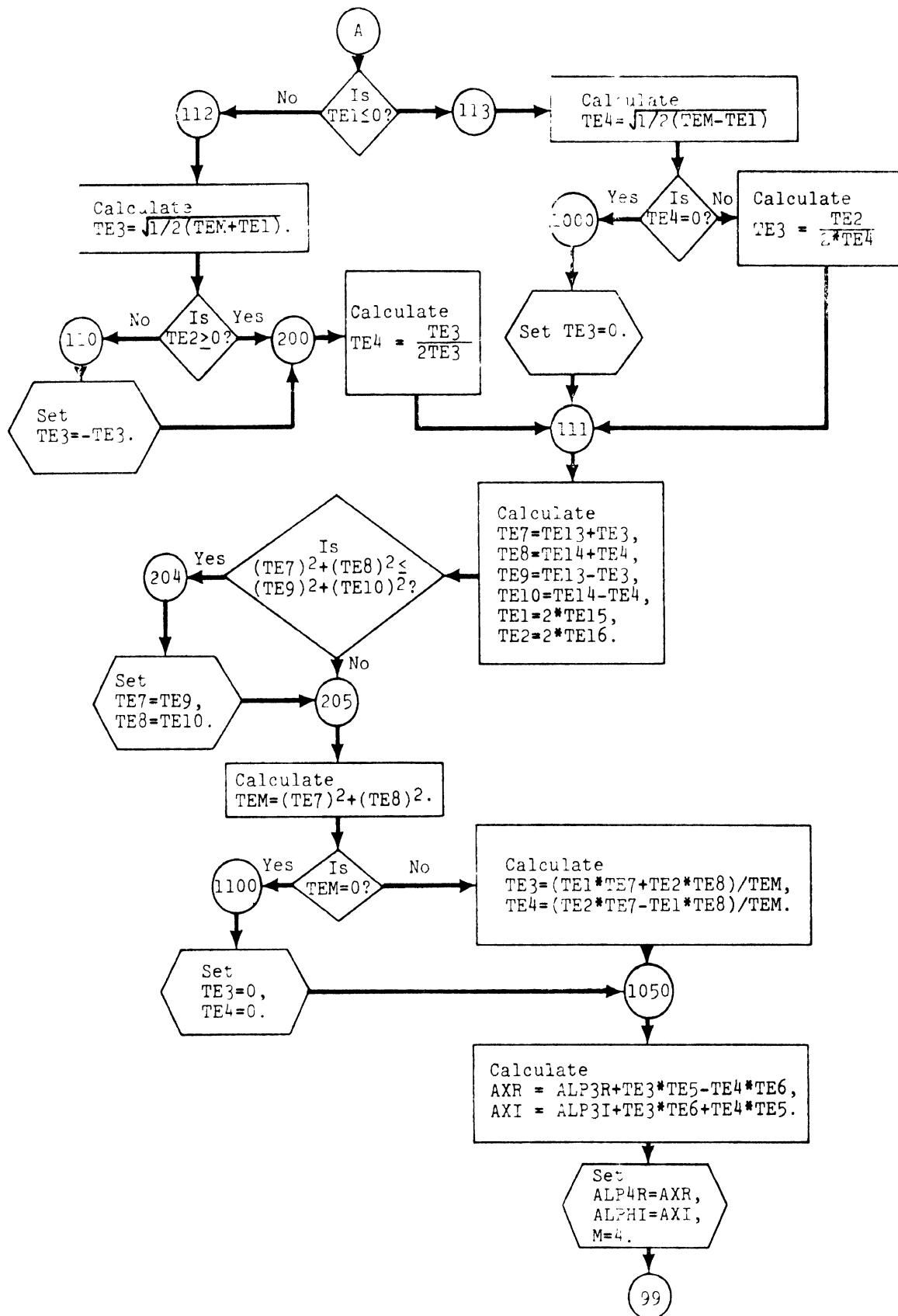


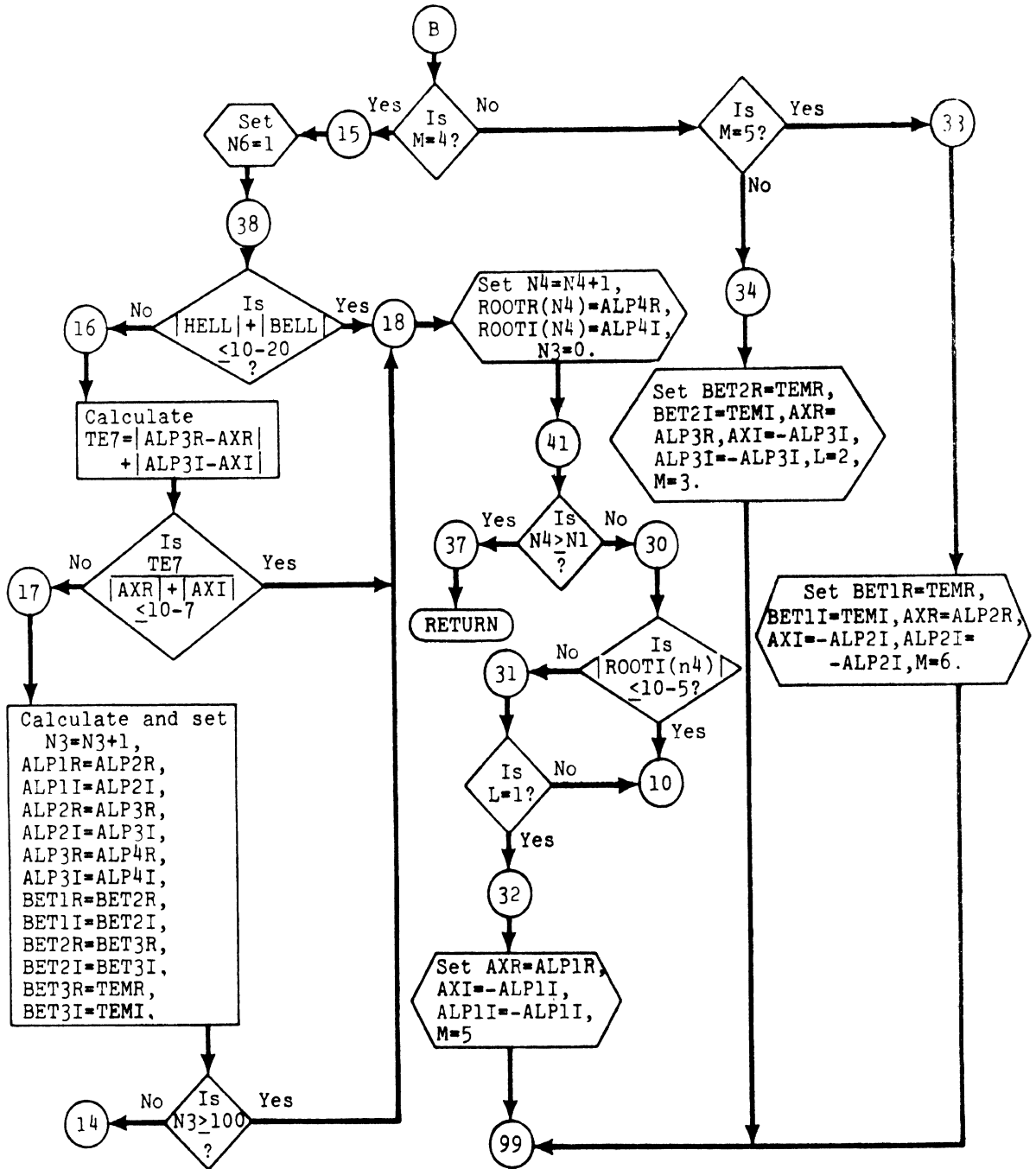
Subroutine MULLER solves a real polynomial for its complex roots.

Its arguments are: COE(10), which is the array of coefficients of the polynomial in descending order; N1, which is the order of the polynomial; ROOTR(15) and ROCTI(15), which are respectively the real and imaginary parts of the roots.



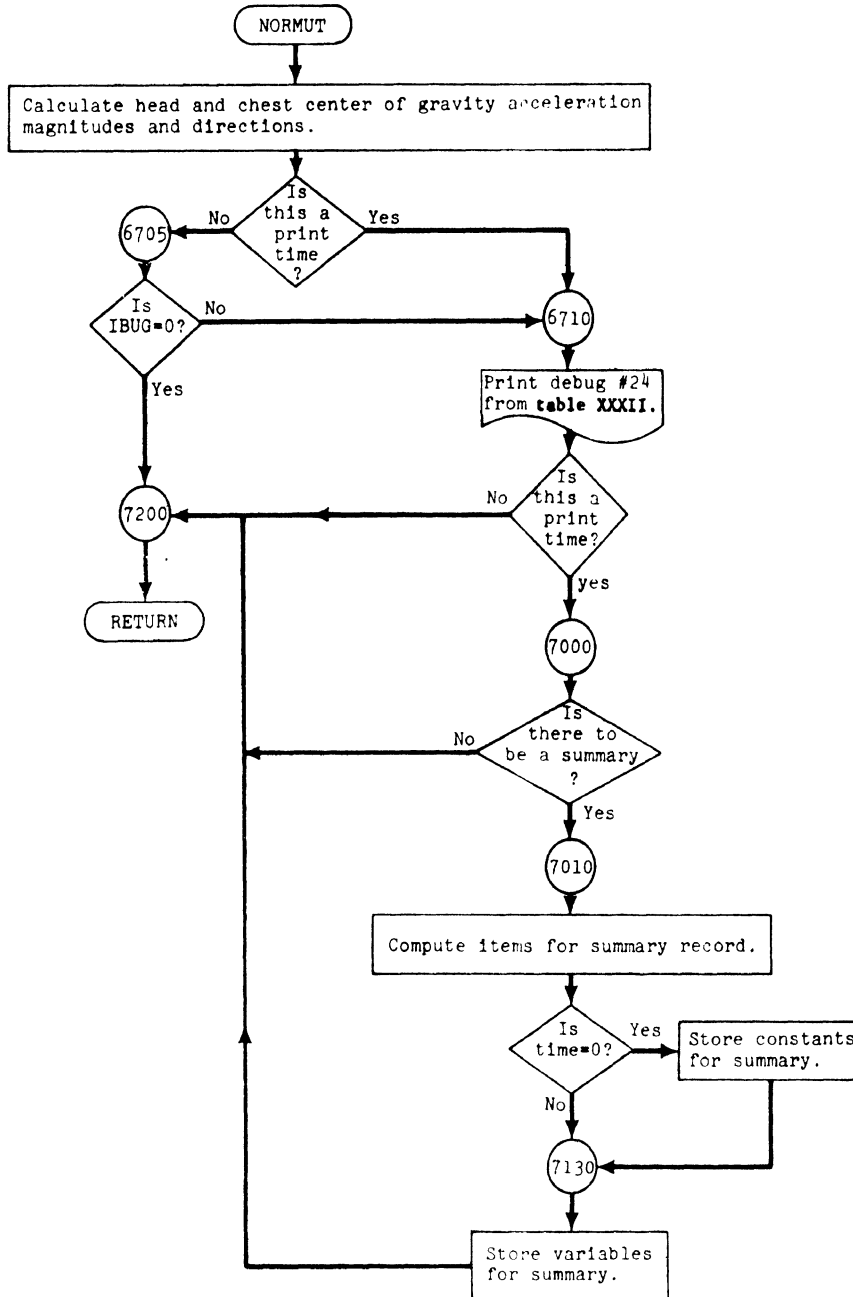




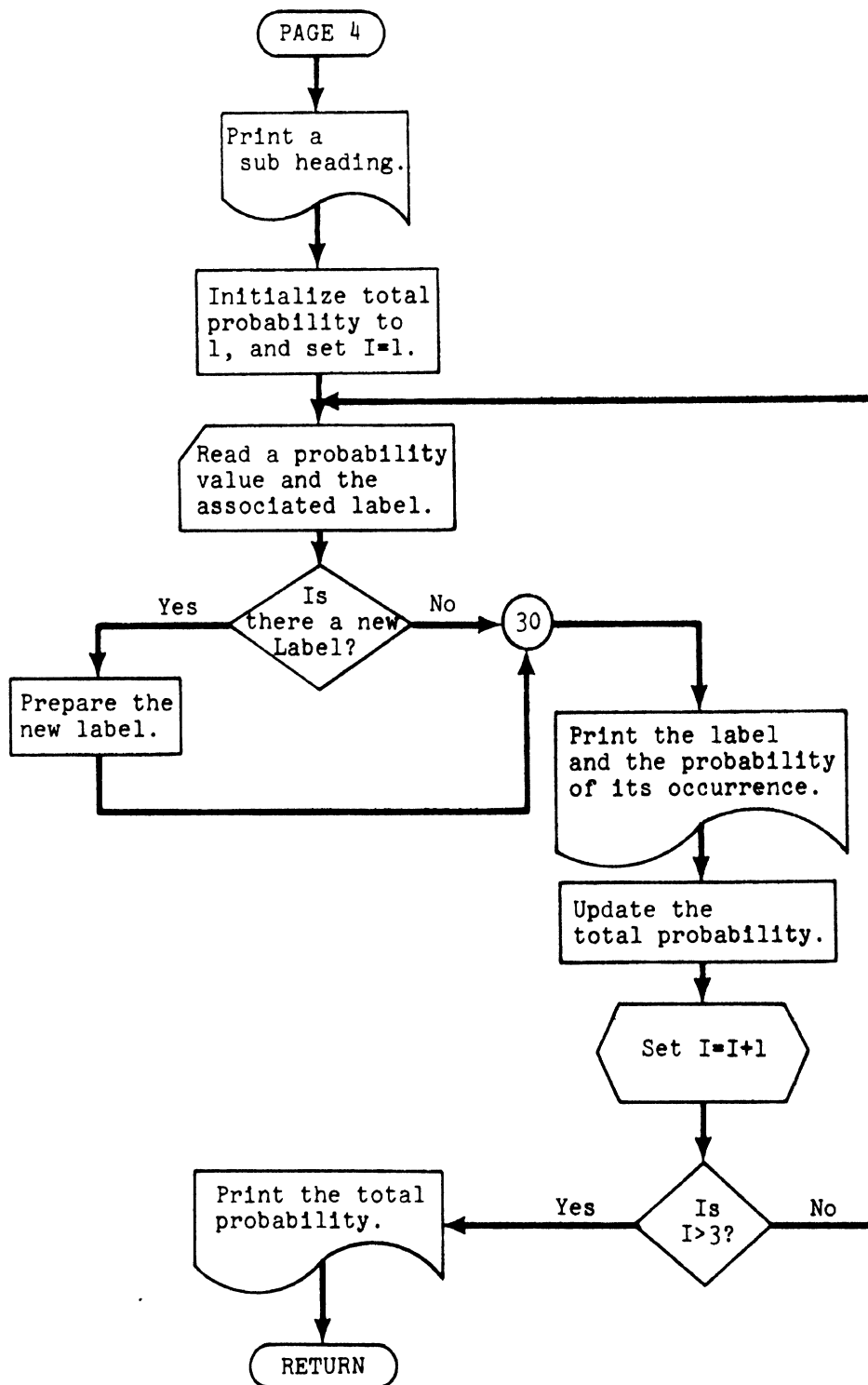


Subroutine NORMUT carries out the following steps:

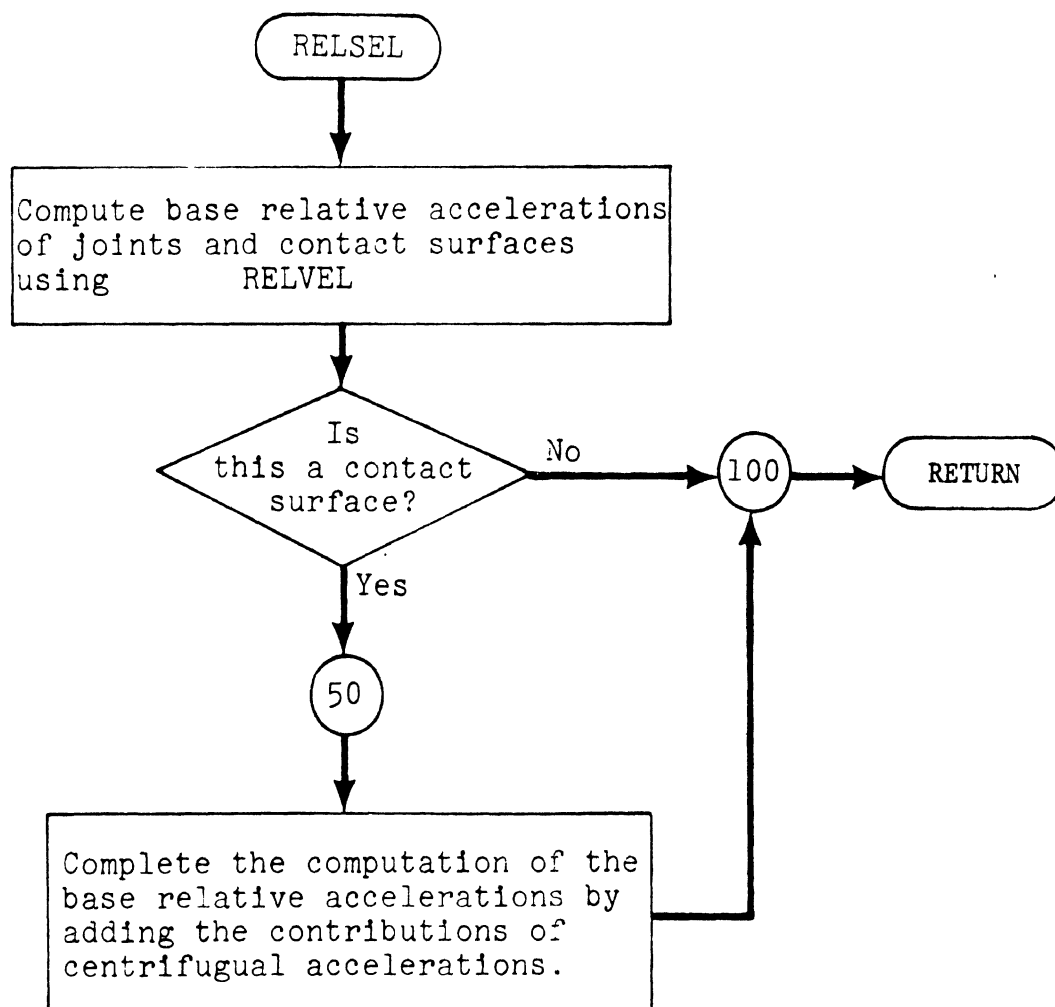
1. Computes head and chest resultant acceleration vectors (magnitudes and angles) at their centers of gravity.
2. Writes normal output on unit 6.
3. Writes data for SUMMARY on unit 9.



Subroutine PAGE 4 computes probability data and prints it out after reading three input cards for the necessary information.

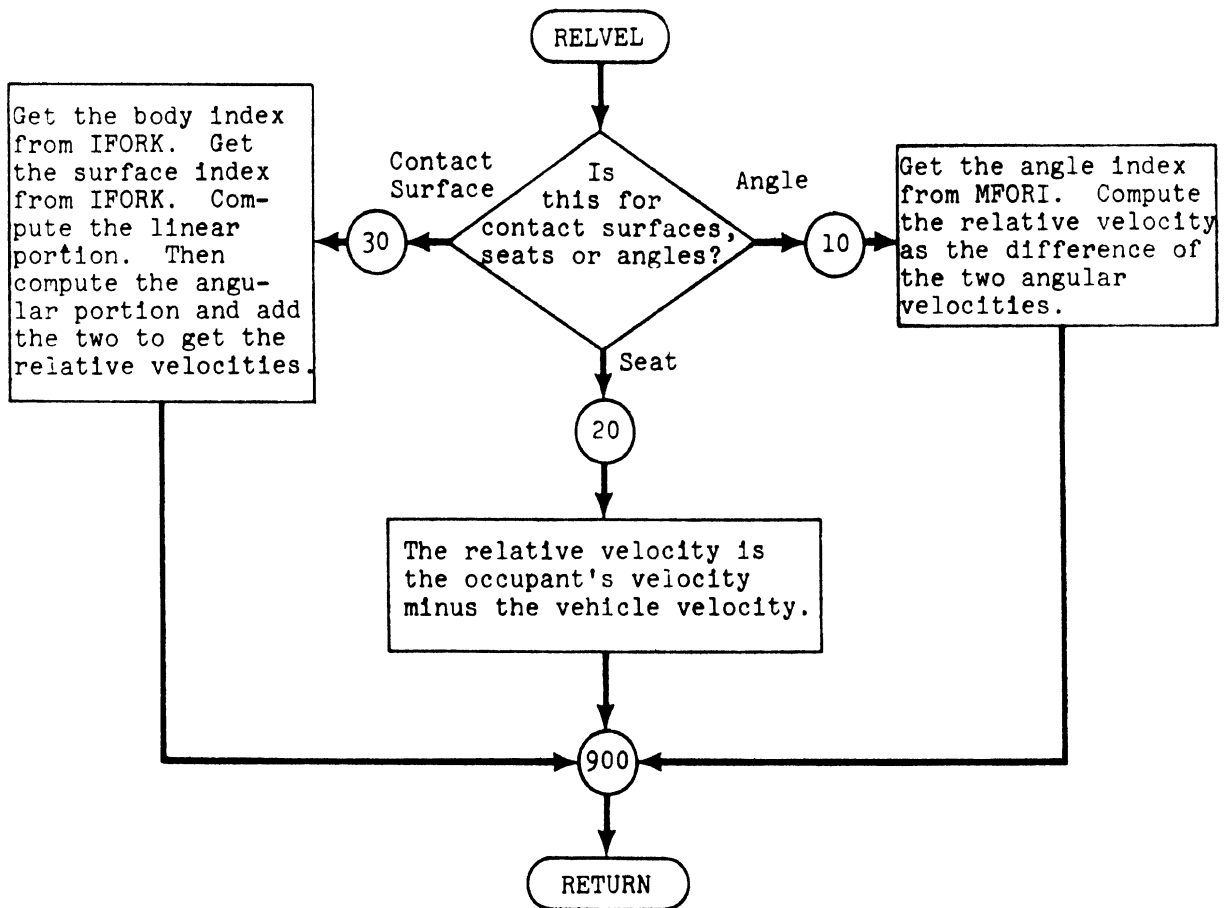


Subroutine RELSEL determines base relative acceleration of joints and contact surfaces subject to jitter via RELVEL and adds contributions of centrifugal accelerations for linear jitter modes.



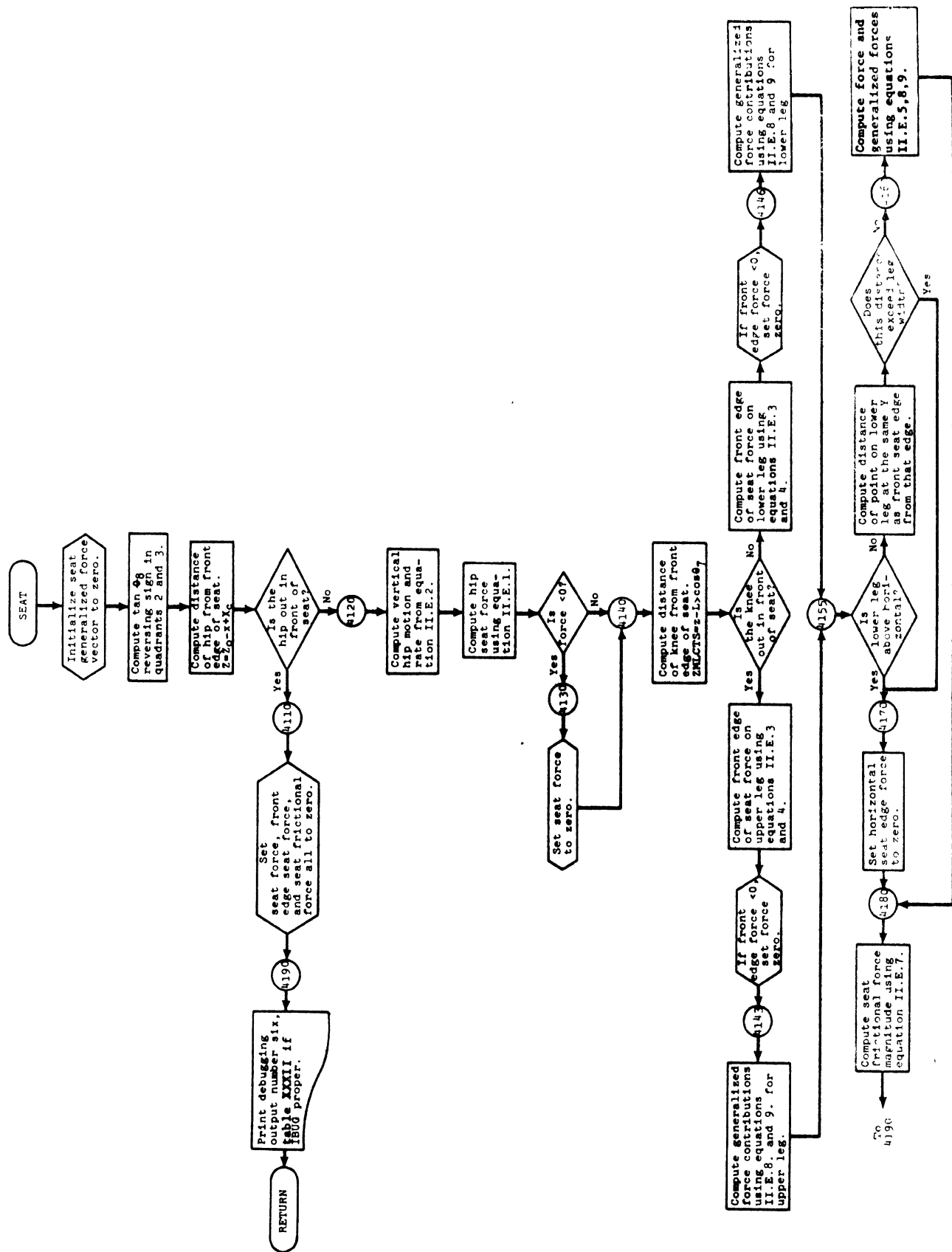
Subroutine RELVEL

Computes relative velocities between joints or contact surfaces and body segments which are subject to jitter.



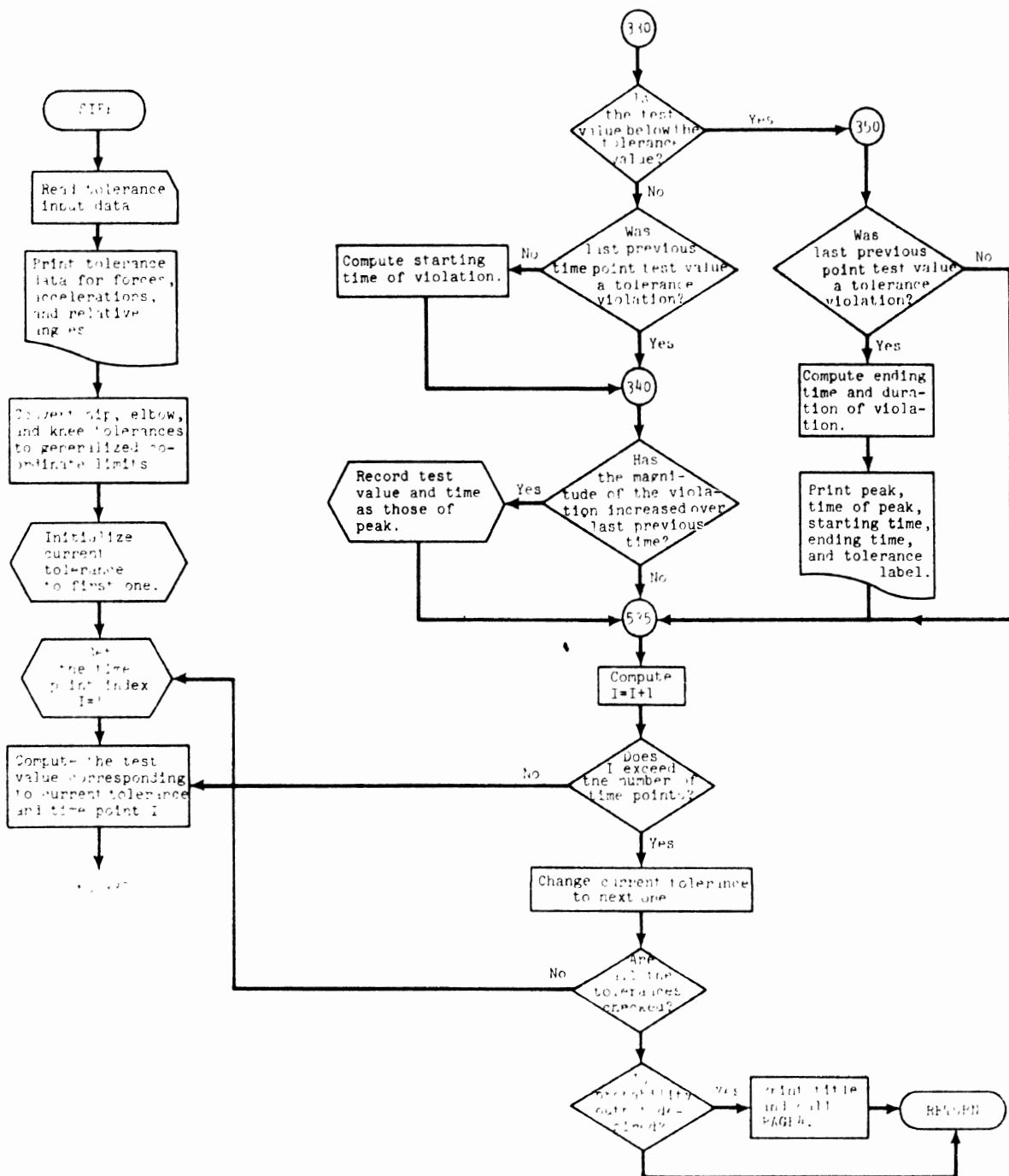
Subroutine SEAT carries out the following steps

1. Computes vertical hip seat force.
2. Computes vertical seat front force and applies it to proper leg segment.
Computes horizontal force on lower leg.
3. Computes magnitude of seat friction force.
4. Computes total continuous generalized seat force vector.



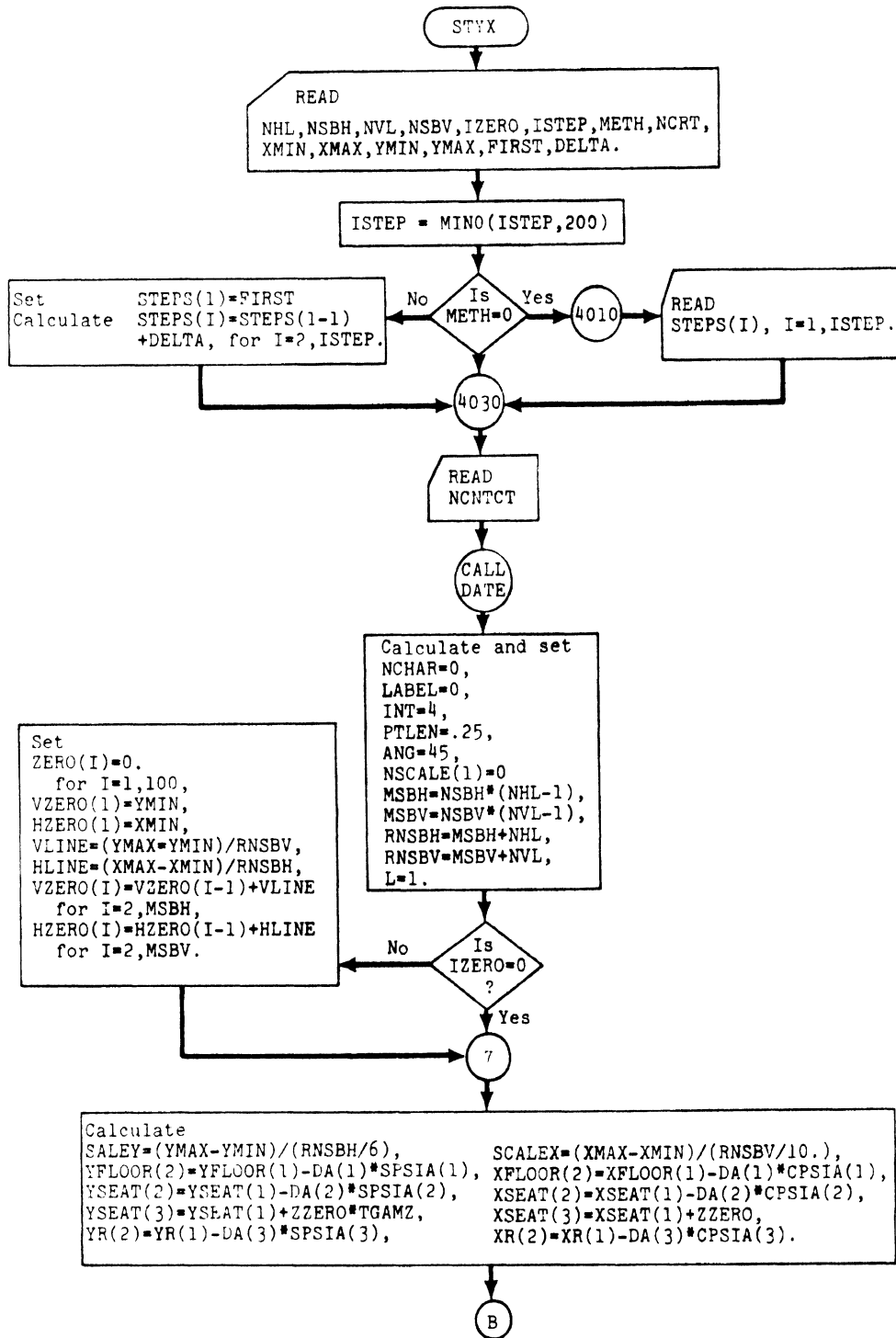
Subroutine SIPP carries out the following steps:

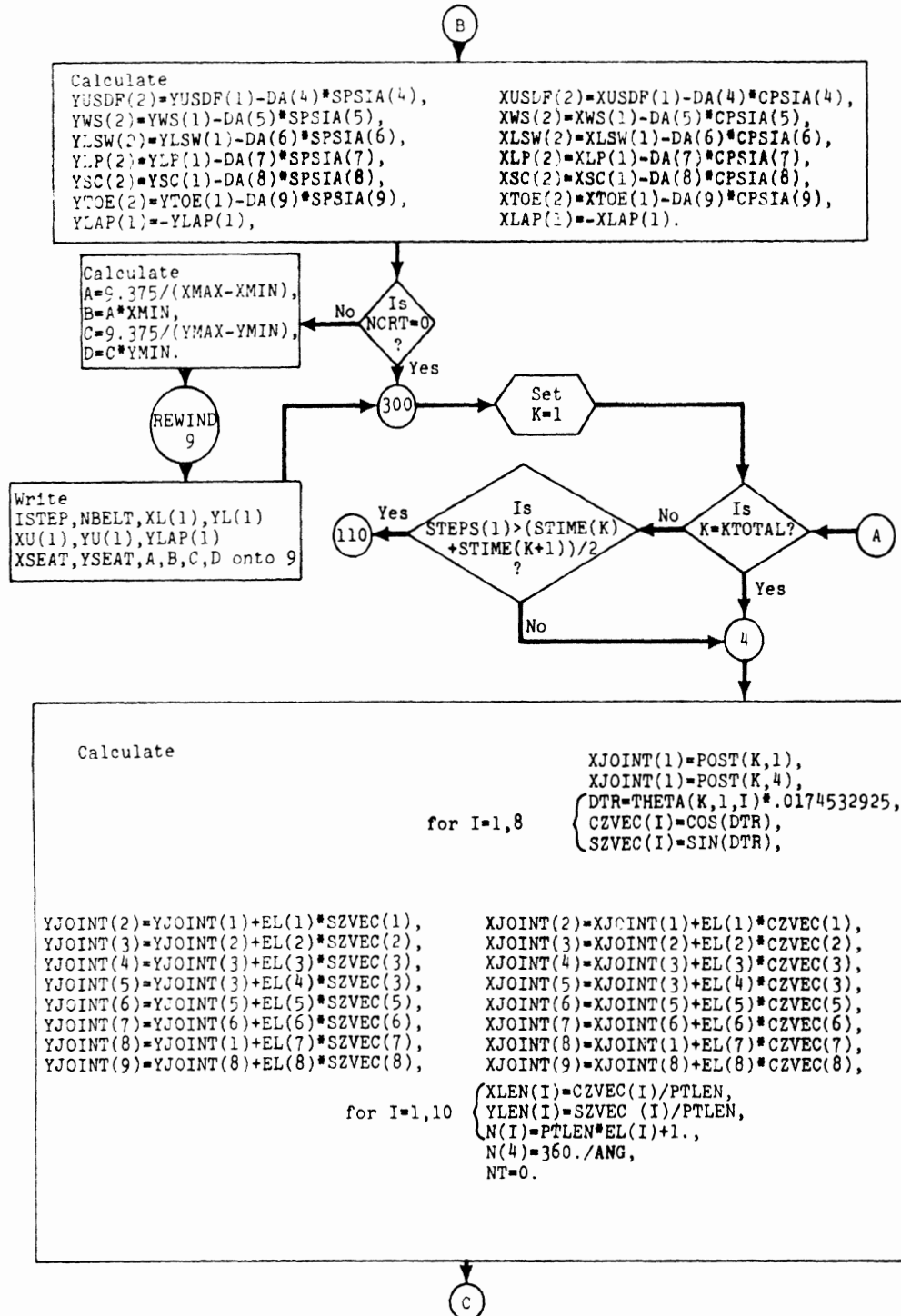
1. Reads cards to reset injury tolerance levels (if any) and prints values, etc.
2. Scans certain variables to see if any exceed their tolerance level and prints out values, times, and durations above tolerance for those that do.
3. Calls PAGE 4 for probability output if desired.

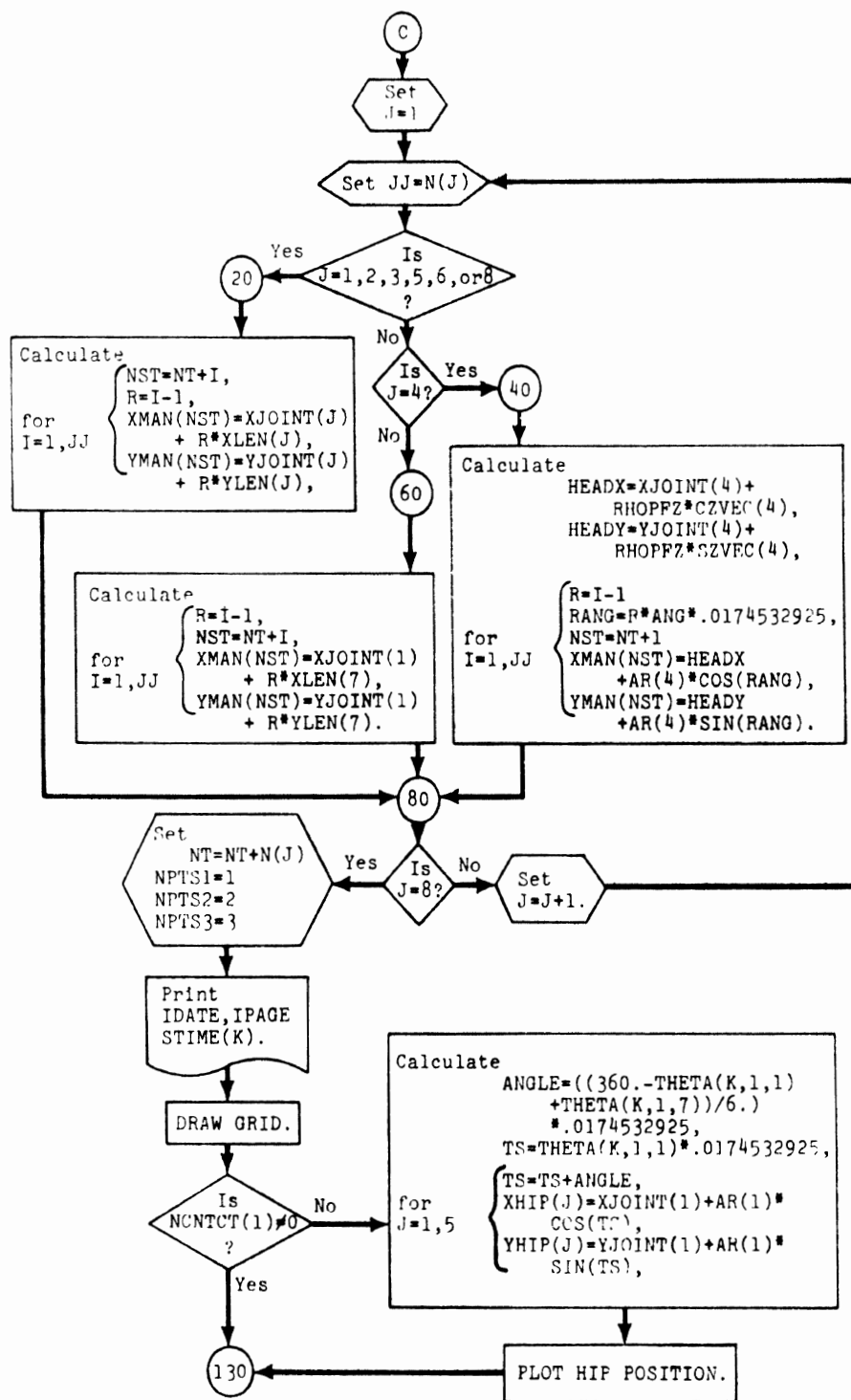


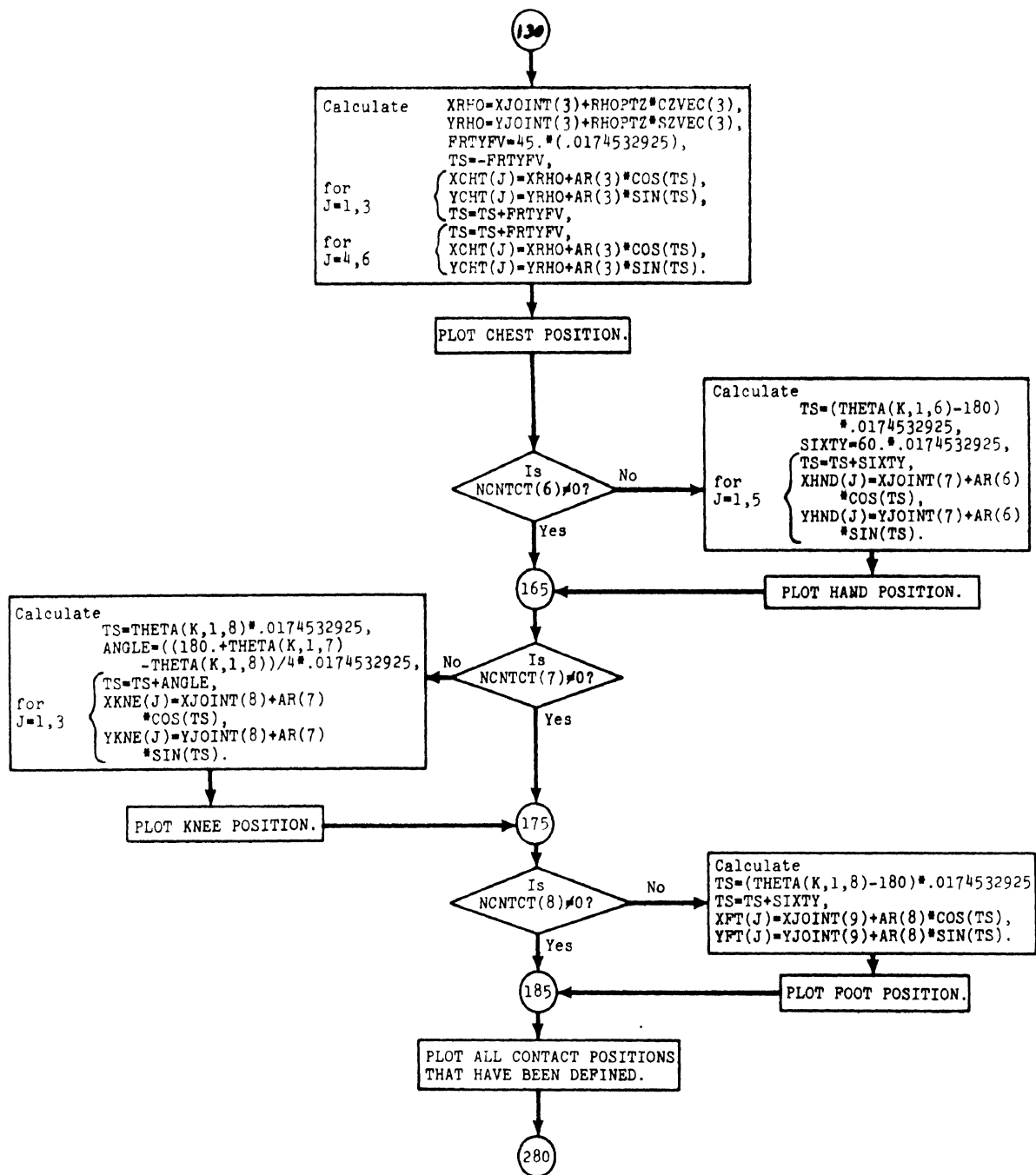
Subroutine STYX carries out the following steps:

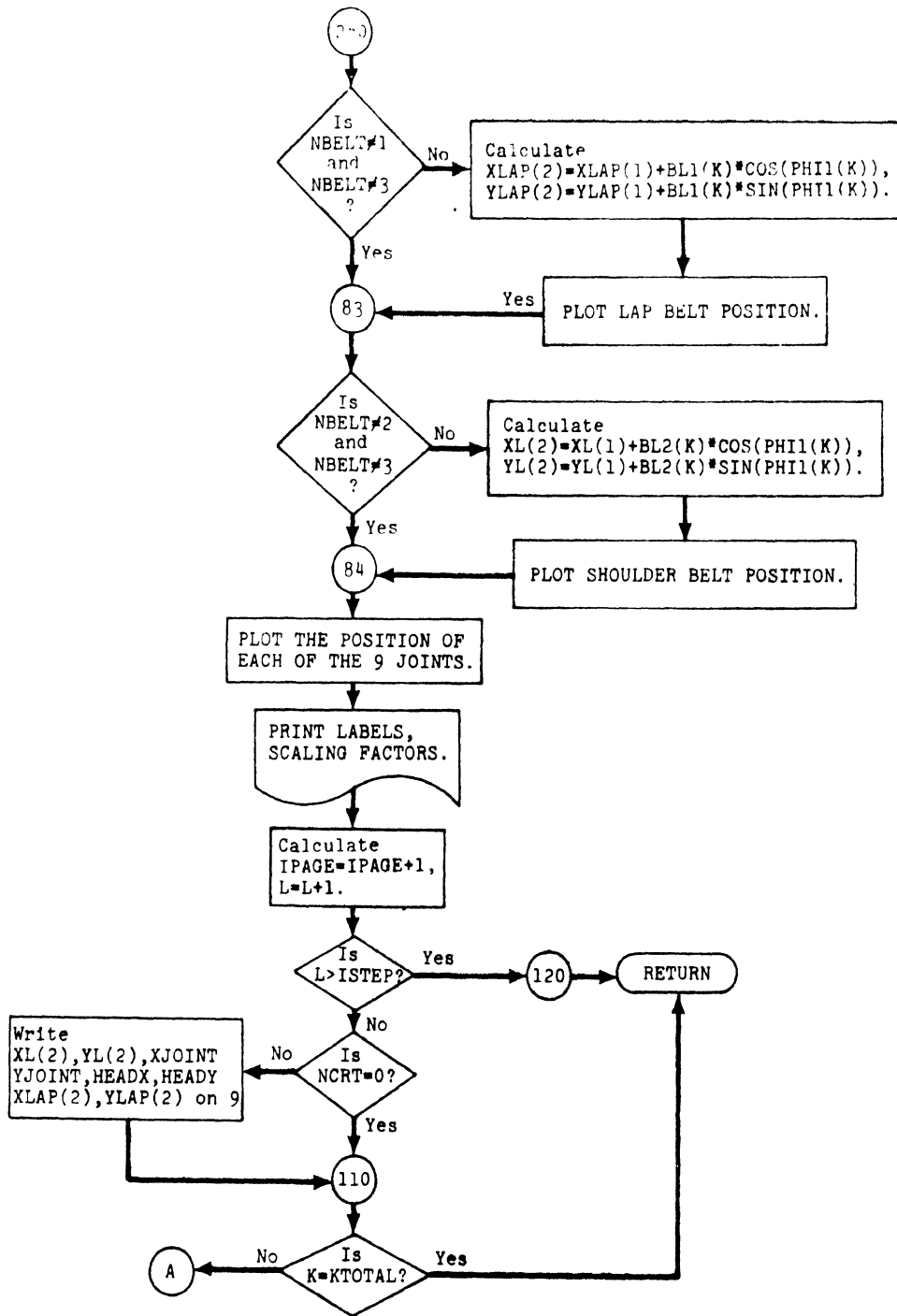
1. Reads its input cards to determine size and content of output stick figures.
2. Computes positions, etc., sets up plot images, and prints.





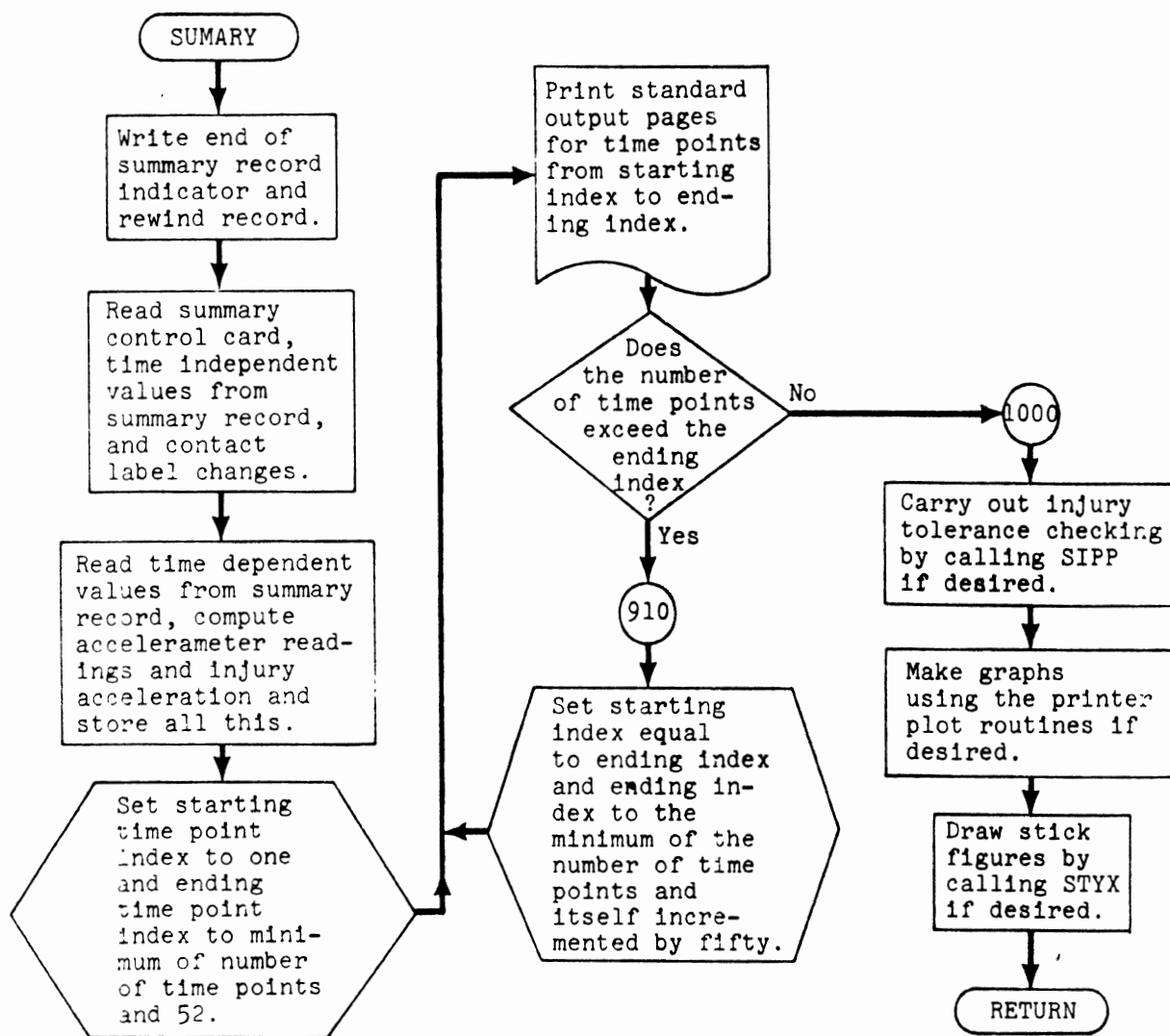






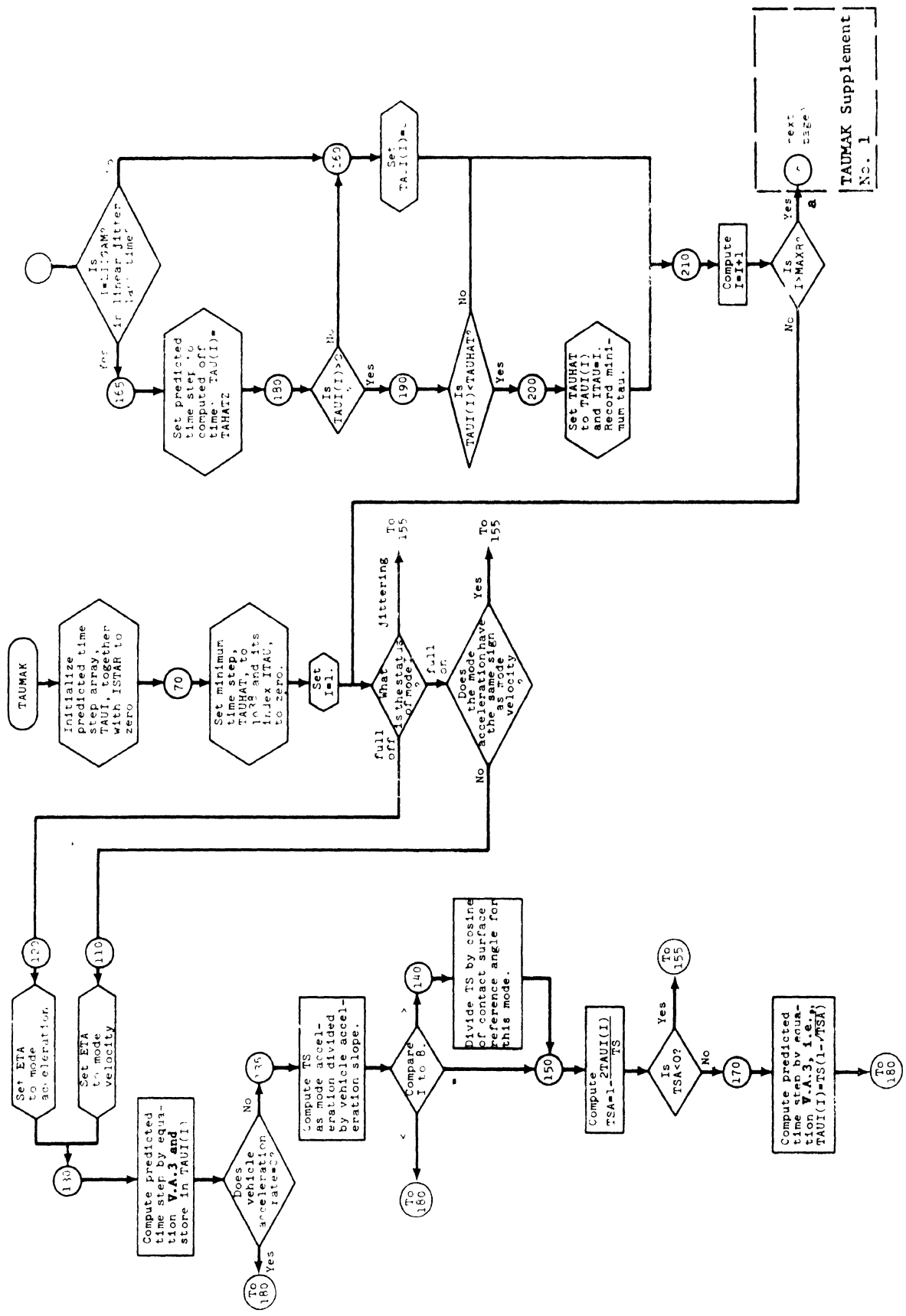
Subroutine SUMMARY carries out the following steps:

1. Writes end-of-run indicator on summary record and rewinds it.
2. Reads one instruction data card.
3. Alters labeling of contact surfaces.
4. Reads storage summary record, sets up page images, and prints.
5. Calls SIPP to produce injury criteria if desired.
6. Uses University of Michigan plot subroutines and produces graphical output if desired.
7. Calls STYX to produce stick figures at selected times if desired.

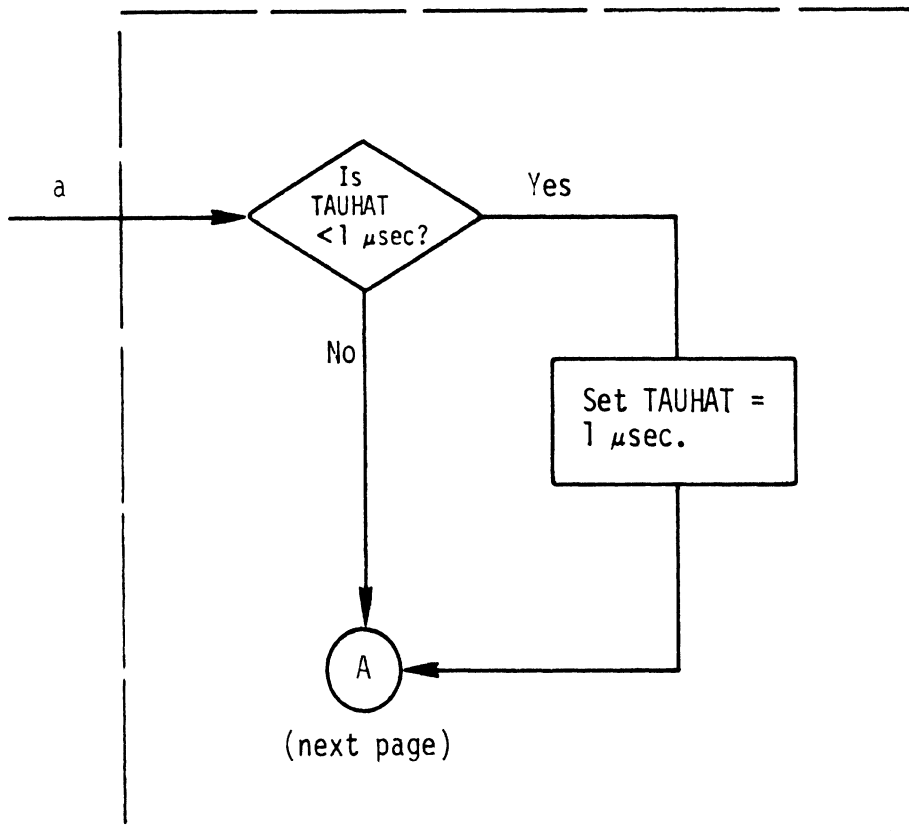


Subroutine TAUMAK carries out the following steps:

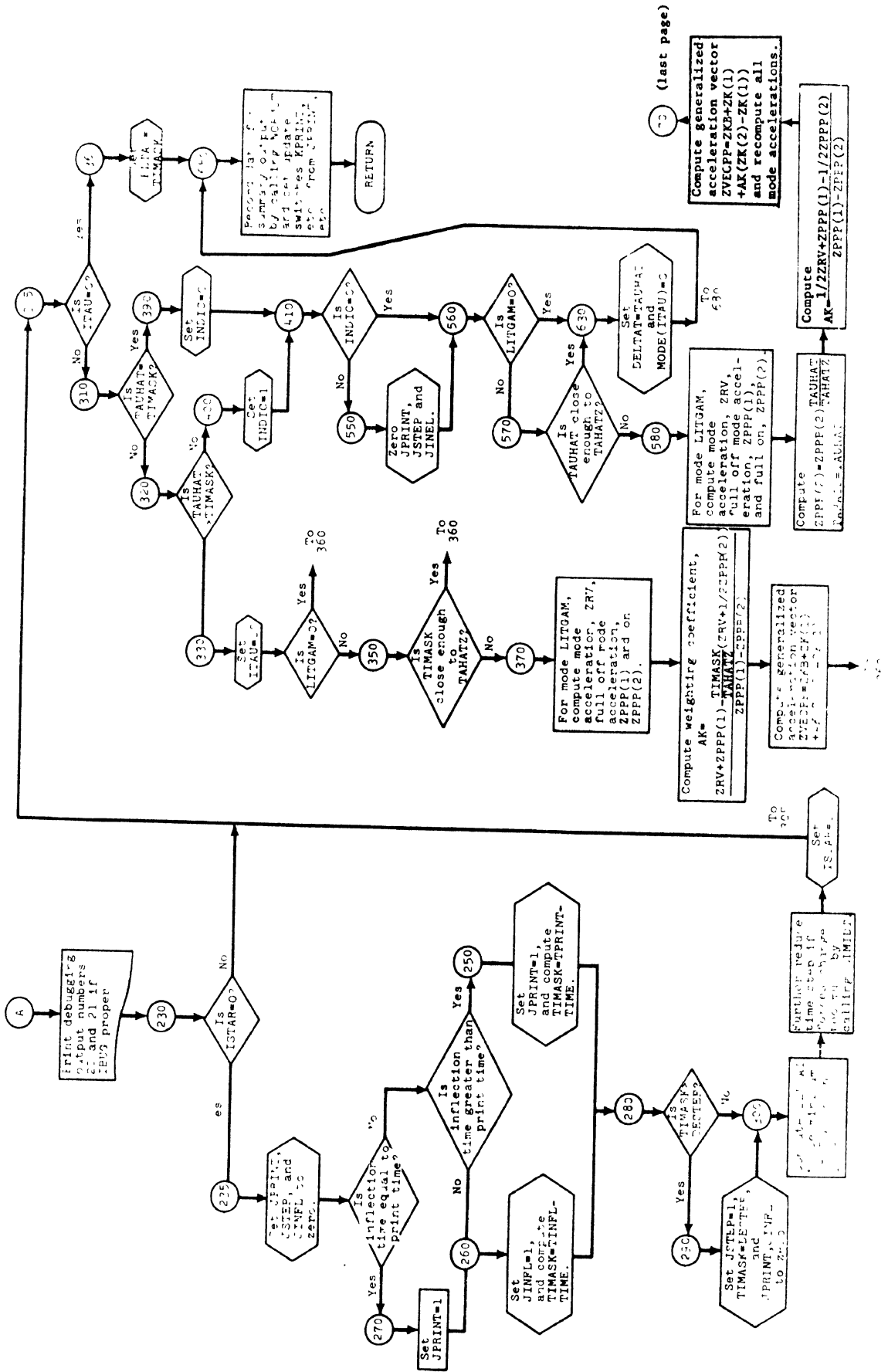
1. Computes time intervals in a manner to reduce the probability of instability.
2. Utilizes LIMIDT to check time interval for force change size.
3. Modifies effective acceleration vector to suit time interval.
4. Calls NORMUT for normal printout storage.
5. Updates switches.



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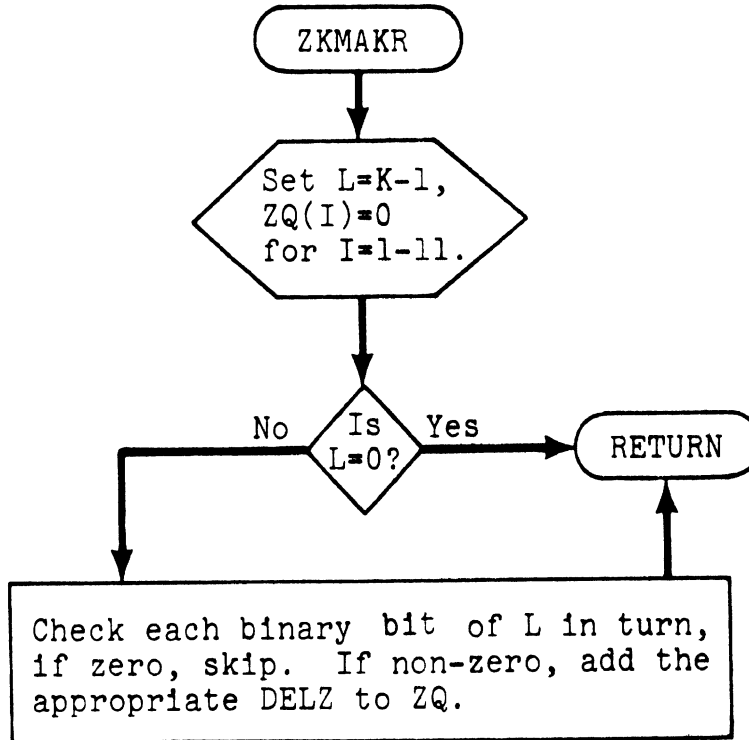


(last page)

Subroutine ZKMAKR

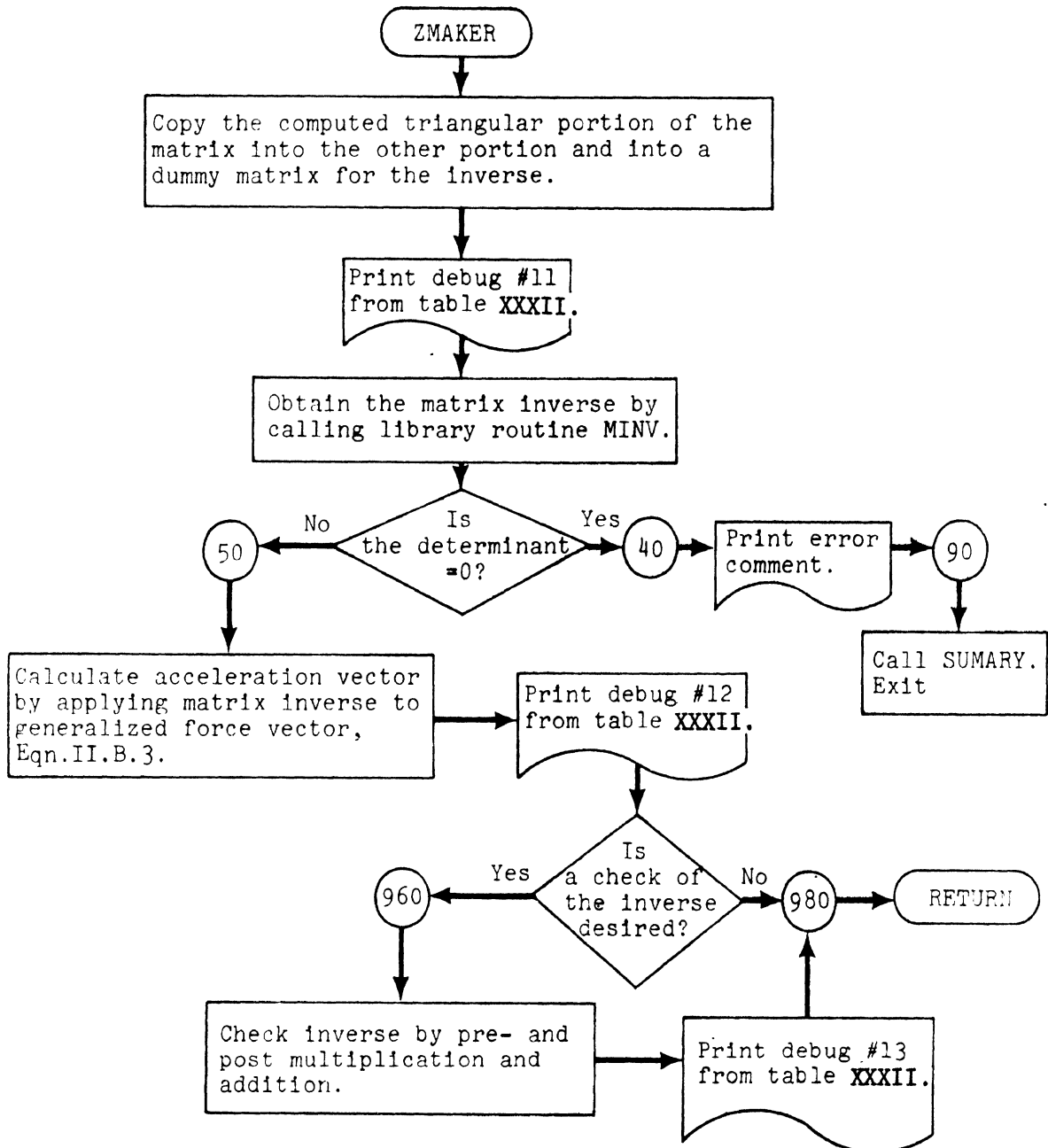
Sets up the components of an array of acceleration vectors needed in JITTER.

Its arguments are: K which is the index of the appropriate combination of jitter modes; ZQ (11) which is the vector containing the resultant accelerations due to this combination.



Subroutine ZMAKER carries out the following steps:

1. Inverts matrix by calling on SSP routine.
2. Computes acceleration vector by applying inverse matrix to generalized force vector.
3. Checks matrix inversion by pre- and post-multiplication if desired.



C. SYMBOL DICTIONARY

The dictionary which follows is arranged in alphabetical order by the FORTRAN name of each variable or array used in the program. If the same FORTRAN name is used in different subroutines with different meanings, the meanings are listed on separate lines for each of the uses. The second column is the FORTRAN dimension which is specified for arrays. The third column is the analytical symbol which corresponds to this FORTRAN name and is supplied if such a correspondence exists. The fourth column gives the physical units for those quantities which have them. The numbers shown are subscript ranges if units are not the same for all elements of arrays. The last column is a short definition of the quantity.

As an appendix to the symbol dictionary, there is an alphabetical list of analytical symbols together with the corresponding FORTRAN names of each quantity. This list indicates the name which can be used to find the definition.

FORTRAN Name	Dimension	Symbol	Units	Definition
A	17	a_i	1-8, lb sec ² 9, lb sec ² /in. 10-17, lb in. sec ⁴	constants used in building matrix, gravity, and centrifugal force vectors
A	36,3	-	-	probability label storage
AA	6	-	-	current probability label
AA	10,10	m	1-8, 1-8, lb sec ² in. 9-10, 9-10, lb sec ² /in. rest, lb sec ²	the mass matrix
AACCA	-	-	in./sec ³	third order vehicle position integration coefficient
ACH	-	-	g-units	horizontal acceleration of upper spinal joint
ACHEST	-	-	in./sec ²	resultant acceleration of chest center of gravity
ACHEST	200	-	in./sec ²	resultant acceleration of chest accelerometer
ACOM	5,11	-	-	contact surface label storage
AEL	14	-	lb in./sec ²	constants used in building matrix
AH	-	-	g-units	horizontal acceleration of neck joint
AHEAD	-	-	in./sec ²	resultant acceleration of head center of gravity

Symbol Dictionary (page 2)

FORTRAN Name	Dimension	Symbol	Units	Definition
AHEAD	200	-	in./sec ²	resultant acceleration of head accelerometer
AK	-	\bar{a}_k	-	weighting coefficient for jitter mode
ALFAI	7	α_1	rad	joint stop lower relative angle limit
ALP1I	-	-	-	imaginary part of root, first approximation
ALP1R	-	-	-	real part of root, first approximation
ALP2I	-	-	-	imaginary part of root, second approximation
ALP2R	-	-	-	real part of root, second approximation
ALP3I	-	-	-	imaginary part of root, third approximation
ALP3R	-	-	-	real part of root, third approximation
ALP4I	-	-	-	imaginary part of root, fourth approximation
ALP4R	-	-	-	real part of root, fourth approximation
ANG	-	-	deg	angular spacing of dots in head representation in stickman output
ANGLE	-	-	rad	angular spacing of plus signs in contact arc representation in stickman output
ANS	-	-	rad	absolute value of arcsine

Symbol Dictionary (page 3)

FORTRAN Name	Dimension	Symbol	Units	Definition
ANVERS	10,10	m^{-1}	inverse of AA	inverse of mass matrix
APRNTD	-	-	sec	minimum print time interval
AR	8	r_i	in.	body contact arc radii
ARCSIN	-	-	rad	principal value of arcsine
ATDSQ	8	-	lb	intermediate step in centrifugal force vector computation
AVELA	-	-	$in./sec^3$	second order vehicle velocity integration coefficient
AX	8	x_i	in.	joint x-coordinates
AXD	8	\dot{x}_i	$in./sec$	joint x-velocities
AXI	-	-	-	imaginary part of trial root
AXR	-	-	-	real part of trial root
AY	8	y_i	in.	joint y-coordinates
AYD	8	\dot{y}_i	$in./sec$	joint y-velocities
AZ	11	z_k	1-8, rad 9-11, in.	generalized coordinate vector
AZP	11	\dot{z}_k	1-8, rad/sec 9-11, in./sec	generalized velocity vector

Symbol Dictionary (page 4)

FORTRAN Name	Dimension	Symbol	Units	Definition
B	-	-	in.	horizontal CRT scaling term (vestigial)
B	4,2	-	-	joint direction label storage
BACCB	-	-	in./sec ²	second order vehicle position integration coefficient
BASIC	11,8	-	1-10, in. 11, in./sec ²	elements one through five are lever arms for contact frictional forces; elements six through ten are lever arms for contact normal forces; element eleven is centrifugal force term for contact relative accelerations
BBB	300,3	-	1, in./sec ² 2,3, -	intercept for piecewise linear tables
BCH	-	-	g-units/in.	upper torso horizontal acceleration linear coefficient
BEE	10	B _i	1-8, in. lb 9-10, lb	centrifugal force vector
BELL	-	-	-	temporary storage for imaginary part of polynomial evaluation
BELTA	200	-	lb	lap belt force storage
BELTB	200	-	lb	lower shoulder belt force storage
BELTC	200	-	lb	upper shoulder belt force storage

Symbol Dictionary (page 5)

FORTRAN Name	Dimension	Symbol	Units	Definition
BETA	3	β_m	1, lb/in. 2, lb/in. ² 3, lb/in. ³	hip seat force spring coefficients
BET1I	-	-	-	imaginary part of first polynomial evaluation
BET1R	-	-	-	real part of first polynomial evaluation
BET2I	-	-	-	imaginary part of second polynomial evaluation
BET2R	-	-	-	real part of second polynomial evaluation
BET3I	-	-	-	imaginary part of third polynomial evaluation
BET3R	-	-	-	real part of third polynomial evaluation
EM	-	-	g-units/in.	head horizontal acceleration linear coefficient
BIGKI	7	K_i	in. lb/rad	joint elasticity coefficient for each joint
BIGMI	8	J_e	in. lb	joint elasticity torque for each joint
BL	3	l_k	in.	belt segment length for each belt segment
BLL	200	-	in.	lap belt length storage
BL2	200	-	in.	lower shoulder belt length storage
BL3	200	-	in.	upper shoulder belt length storage

Symbol Dictionary (page 6)

FORTTRAN Name	Dimension	Symbol	Units	Definition
BPRNTD	-	-	sec	first time for summary printing
BVELB	-	-	in./sec ²	first order vehicle velocity integration coefficient
C	-	-	-	vertical CRT scaling factor (vestigial)
C	3,7	-	-	joint label storage
CACCC	-	-	in./sec	first order vehicle position integration coefficient
CARD	5	-	-	temporary storage for reading input cards
CARD	8	-	-	temporary storage for reading input cards
CAZ	8	-	-	cosines of body angles
CCF	200,4	-	lb	chest contact forces storage
CCH	-	-	g-units	vertical acceleration of upper spinal joint
CEE	10	C _k	1-8, in. lb 9-10, lb	joint generalized force vector
CFA	200	-	in./sec ²	chest forward acceleration storage
CH	-	-	g-units	vertical acceleration of neck joint
CI	-	-	-	tolerance index as input data
CK	10,10	-	-	sum of pre- and post-matrix multiplications of matrix and inverse as check

Symbol Dictionary (page 7)

FORTTRAN Name	Dimension	Symbol	Units	Definition
CKF	200	-	lb	knee contact force storage
COE	6	-	-	temporary storage for reordering load deflection coefficients
COE	16	-	-	polynomial coefficients in descending order
COMI	3,8	-	-	body contact segment label storage
CONEN	18	C_1	lb/in.	first order unloading coefficient for each interaction
CONTAC	200,21	-	lb	contact force storage
CPHI	3	-	-	cosines of belt angles
CPRIME	7	C'_i	in. lb	joint coulomb friction coefficients
CPSIA	10	-	-	cosines of contact surface reference angles
CS	-	C_s	lb sec/in.	hip seat force damping coefficient
CTHETA	8	-	-	cosines of body angles
CTHETZ	8	-	-	cosines of body angles at time zero
CTWON	16	C_2	lb/in. ²	second order unloading coefficient for each interaction.
CUA	200	-	in./sec ²	chest upward acceleration storage
CVELA	-	-	in./sec	zeroth order vehicle velocity integration coefficient

Symbol Dictionary (page 8)

FORTTRAN Name	Dimension	Symbol	Units	Definition
CZERON	18	C ₀	lb	zeroth order unloading coefficient for each interaction
CZVEC	8	-	-	cosines of body angles for stick figure
C0	-	-	-	coefficient in arcsine evaluation
C1	-	-	-	coefficient in arcsine evaluation
C2	-	-	-	coefficient in arcsine evaluation
C3	-	-	-	coefficient in arcsine evaluation
C4	-	-	-	coefficient in arcsine evaluation
C5	-	-	-	coefficient in arcsine evaluation
C6	-	-	-	coefficient in arcsine evaluation
C7	-	-	-	coefficient in arcsine evaluation
D	-	-	in.	vertical CRT scaling term (vestigial)
DA	10	-	in.	contact surface lengths
DACCD	-	-	in.	zeroth order vehicle position integration coefficient
DCH	-	-	g-units/in.	upper torso vertical acceleration linear coefficient
DEE	10	D _i	1-8, in. lb 9-10, lb	seat and belt generalized force vector

Symbol Dictionary (page 9)

FORTTRAN Name	Dimension	Symbol	Units	Definition
DELDOD	18	$\dot{\delta}_{m-1}$	in./sec	previous deflection rate for each interaction
DELET	-	-	in. lb	change in energy over time interval
DELIA	-	-	in.	contact deflection
DELIAD	-	-	in./sec	contact deflection rate
DELL	-	Δ	in.	slack
DELNN	-	Δv	accel	change in mode acceleration between two jitter states for a linear mode
DELNU	-	Δv	accel	change in mode acceleration between two jitter states
DELOLD	18	δ_{m-1}	in.	previous deflection for each interaction
DELTA	3	Δ	in.	belt slack for each belt segment
DELTA	-	-	sec	time interval between stick figures
DELTAT	-	Δt	sec	integration time interval
DELZ	11,16	$\Delta \ddot{z}_i$	1-8, rad/sec ² 9-11, in./sec ²	change in generalized acceleration vector due to each possible jitter mode acting alone
DESPA	3,6	-	-	body contact arc labels
DESPB	6	-	-	vestigial

Symbol Dictionary (page 10)

FORTRAN Name	Dimension	Symbol	Units	Definition
DESPC	5,6	-	-	contact surface labels
DESTEP	-	Δt_{\min}	sec	minimum integration time interval
DETERM	-	-	-	determinant of mass matrix
DE15	-	-	-	temporary storage in MULLER
DE16	-	-	-	temporary storage in MULLER
DH	-	-	g-units/in.	head vertical acceleration linear coefficient
DISP	-	x-X	in.	displacement of hip relative to vehicle
DTPRNT	-	-	sec	print time interval for normal summary output
DTR	-	$\pi/180$	rad/deg	degrees to radian conversion factor
DTR	-	-	rad	temporary storage for body angles
DUR	-	-	sec	duration of injury tolerance violation
EHAT	18	\hat{E}	in. lb	reference conserved energy per loading cycle for each interaction
EL	8	L_i	in.	body segment lengths except element four which is distance from upper spine to shoulder
ELAMB	6	λ_i	in.	initial condition parameters for belts

Symbol Dictionary (page 11)

FORTRAN Name	Dimension	Symbol	Units	Definition
ELP	5	L'	in.	temporary storage for proper body lengths used in computing lever arms for contacts
ELPTEN	-	l'_{10}	in.	initial distance between hip and lap belt anchor point
ELTHRY	-	l_{30}	in.	initial upper shoulder belt length
ELTWTY	-	l_{20}	in.	initial lower shoulder belt length
ELZTEN	-	l_{10}	in.	initial lap belt length
EM	8	m_i	lb sec ² /in.	body segment mass for each segment
EMC	-	m_c	lb sec ² /in.	vehicle mass (vestigial)
EMFVSX	-	-	lb sec ² /in.	total mass of arms
EMTHSX	-	-	lb sec ² /in.	total mass of upper torso, head, and arms
EMTWSX	-	-	lb sec ² /in.	total mass of upper half of body (from middle torso and including arms)
EONE	18	E_1	in. lb	total conserved energy for each interaction
EONEC	-	E_c	in. lb	vehicle conserved energy (vestigial)
EPSLNP	-	ϵ'	in.	residual deformation when loading begins again before unloading is complete
EPSLNY	18	ϵ	in.	cumulative permanent deformation for each interaction

Symbol Dictionary (page 12)

FORTRAN Name	Dimension	Symbol	Units	Definition
EPSLNZ	-	ϵ_0	sec	linear mode time interval convergence limit
ET	18	E_t	in. lb	total energy for current cycle for each interaction
ETA	-	η	-	determines sign of relative velocity limit used in time prediction of entering jitter
EYE	8	I_i	lb sec ²	body segment moment of inertias at center of gravity
EO	-	\hat{E}_0	in. lb	reference conserved energy for prediction
FAB	10	-	lb.	saturation limit stored on contact number
FARB	18	-	lb.	saturation limit stored on interaction number
FEPTEN	-	ϕ'_{10}	rad	angle of line joining lap belt anchor and hip joint from horizontal at time zero
FFM	3	F_m	lb	belt forces for each segment
FIRST	-	-	sec	first time at which a stick figure is desired
FMAX1	-	-	lb	maximum value of all belt forces in crash
FMAX2	-	-	in./sec ²	maximum value of head and chest accelerations in crash
FMAX3	-	-	in.	maximum value of hip x and y coordinates relative to the vehicle in crash
FMAX4	-	-	in./sec ²	maximum value of vehicle acceleration in crash
FMAX5	-	-	deg	maximum value of angles of head and chest accelerations in crash

Symbol Dictionary (page 13)

FORTRAN Name	Dimension	Symbol	Units	Definition
FMAX6	-	-	lb	maximum value of seat hip and seat front forces in crash
FMIN1	-	-	lb	minimum value of all belt forces in crash
FMIN2	-	-	in./sec ²	minimum value of head and chest accelerations in crash
FMIN3	-	-	in.	minimum value of hip x and y coordinates relative to the vehicle in crash
FMIN4	-	-	in./sec ²	minimum value of vehicle acceleration in crash
FMIN5	-	-	deg	minimum value of angles of head and chest accelerations in crash
FMIN6	-	-	lb	minimum value of seat hip and seat front forces in crash
FMM	300,3	-	1, in./sec ² 2,3, -	slope of subsequent input table segment
FMUA	10	μ_a	-	contact surface coefficients of friction
FMUS	-	μ_s	-	seat cushion coefficient of friction
FOM	-	Ω	in.	latest maximum deflection
FORCE	-	F	lb	predicted contact force
FRTYFV	-	$\pi/4$	rad	forty-five degrees in radians
FS	-	F _s	lb	hip seat force

Symbol Dictionary (page 14)

FORTRAN Name	Dimension	Symbol	Units	Definition
FSPRM	-	F'_s	lb	front edge seat force
FSPRMZ	-	F'_{s0}	lb	front edge seat force at time zero
FSZCNS	-	-	lb	constant used in front edge seat force determination representing force calibration at zero time
FT	-	F	lb	predicted force
FTOLD	18	F_{m-1}	lb	previous force for each interaction
FTT	-	F	lb	predicted force
FUDGE	-	-	in.	distance from contact surface used as maximum distance error caused by time prediction error in linear jitter modes
FZ	-	F_z	lb	forward seat front edge force
G	18	G	-	material plasticity index, i.e., the ratio of permanent deformation to maximum deflection, for each interaction
GA	10	G_a	-	material plasticity index for each contact surface
GAMZER	-	γ_0	deg	angle of seat cushion surface from horizontal
GCHEST	200	-	deg	angle of chest accelerometer acceleration storage
GEE	10	G_i	1-8, in. lb 9,10, lb	negative of gravitational generalized force vector

Symbol Dictionary (page 15)

FORTRAN Name	Dimension	Symbol	Units	Definition
GHEAD	200	-	deg	angle of head accelerometer acceleration storage
GNEW	-	-	-	plasticity index
GOMG	-	-	in.	required off deflection for unloading curve
GRAVA	10	-	1-8, in. lb 9, lb	parameters used in computation of gravitational generalized force vector; element ten is vestigial
GRAVIT	-	g	in./sec ²	acceleration of earth standard gravity (32.2)
H	-	h	in.	distance from the point of action of the lower shoulder belt from lower spinal joint along centerline of middle torso
HFELL	-	-	-	temporary storage of real part of polynomial evaluation
HEADX	-	x _h	in.	x-coordinate of head center of gravity
HEADX	-	-	in.	x-coordinate of center of curvature of head
HEADY	-	y _h	in.	y-coordinate of head center of gravity
HEADY	-	-	in.	y-coordinate of center of curvature of head
HFA	200	-	in./sec ²	head forward acceleration at center of gravity storage
HLA	200	-	in./sec ²	vestigial
HLLINE	-	-	in.	horizontal distance represented per grid line

Symbol Dictionary (page 16)

FORTRAN Name	Dimension	Symbol	Units	Definition
HZERO	130	-	in.	horizontal distance represented at plot origin
I	-	i	-	general index but often body segment index
IA	-	a	-	contact surface index
IALPH	26	-	-	contains alphabetic characters for identifying input cards
IBIG	8	I _k	-	contains indices of modes in jitter state in order that they came in jitter except for linear jitters which are always last
IBUG	-	-	-	debug printout control level
IC	-	-	-	input card counter
ID	-	-	-	input card identification field storage
IDATE	3	-	-	contains calendar date of the current run
IFORK	3,8	-	-	element one is body segment index, element two is contact surface index, and element three is the interaction index for each of eight possible linear jitter modes
IGNORE	10	-	-	contains a switch for each of the contacts which tells whether the surface is not used or has no friction
II	-	i	-	body segment index
IMAGE	1392	-	-	temporary storage for prediction of summary plots

Symbol Dictionary (page 17)

FORTTRAN Name	Dimension	Symbol	Units	Definition
IMAGE	1500	-	-	temporary storage for prediction of stick figures
IMAX	-	-	-	index of last time point of input table
IMIN	-	-	-	index of latest inflection point of input table
IND	-	-	-	code index for combination of on and off states being tried to resolve jittering modes
INDEX	-	-	-	index of contact interaction
INDIC	-	-	-	switch indicating whether to reset inflection, print and step switches to zero if jitter mode time is selected
INN	-	-	-	In common /IO/, logical device number for input
INN	-	-	-	index used in contact friction bookkeeping
INT	-	-	-	number of spacer points between plotted points
IPAGE	-	-	-	page number counter
IPOST	3	-	-	pointer for latest input table entry used
ISON	-	-	-	switch indicating whether a tolerance violation is in progress during a scan of values for all time
ISTAR	-	i*	-	switch indicating need for force limiting
ISTART	-	-	-	index of starting time point on printed page
ISTEP	-	-	-	maximum number of stick figure times

Symbol Dictionary (page 18)

FORTRAN Name	Dimension	Symbol	Units	Definition
ISTOP	-	-	-	index of stopping time point on printed page
ISW	-	-	-	extracted mode contribution inclusion switch
ISWT	18	-	-	saturation switch stored on interaction number
ISWT	-	-	-	switch to control new page title printing
ITABLE	-	-	-	input table number
ITAU	-	-	-	index of mode with minimum time to reach jitter
ITOL	-	-	-	temporary storage for tolerance limit data
ITOP	-	-	-	number of possible jitter mode combinations
ITOPOW	-	-	-	two raised to an integer power (vestigial)
ITPH	-	-	-	switch controlling zero line printing
IZERO	-	-	-	general index
J	-	j	-	general index
JFORK	8	-	-	temporary storage for previous linear jitter mode contact interaction indices
JI	-	-	-	inflection switch for prediction
JINFL	-	-	-	temporary inflection switch
JJ	-	-	-	general index often maximum number of nonzero contact forces at any time

Symbol Dictionary (page 19)

FORTRAN Name	Dimension	Symbol	Units	Definition
JK	-	-	-	general index
JL	-	-	-	general index
JNN	-	-	-	(vestigial)
JOINT	9	-	-	stick figure joint index labels
JP	-	-	-	print switch for prediction
JPRINT	-	-	-	temporary print switch
JS	-	-	-	time step switch for prediction
JSTEP	-	-	-	temporary time step switch
K	-	k	-	general index often maximum number of time points for summary printout or index of present jitter mode
KA	8	a	-	contact surface index for each nonzero force
KI	8	i	-	body contact arc index for each nonzero force
KINFL	-	-	-	inflection switch
KK	-	-	-	general index
KKK	-	-	-	general index
KN	-	-	-	index of second linear jitter mode

Symbol Dictionary (page 20)

FORTRAN Name	Dimension	Symbol	Units	Definition
KPOST	-	-	-	index of current input table entry
KPRINT	-	-	-	print switch
KSTEP	-	-	-	time step switch
KTABLE	2,14	-	-	contains the body arc and contact surface indices for each of the allowable interactions for the current passenger position; the interaction index is the second subscript plus four
KTOTAL	-	-	-	total number of time points for printout
KTS	-	-	-	temporary value of KPOST
L	-	l	-	general index
LA	2l	a	-	contact surface indices for contact force printout
LABEL	-	-	-	switch indicating no plot label for stick figure
LCONTL	-	-	-	switch controlling some standard printout options
LI	2l	i	-	body arc indices for contact force printout
LINE	-	-	-	line counter for page length control of printout
LITGAM	-	γ	-	index of linear jitter mode
LL	-	-	-	general index
LODSWT	18	-	-	saturation control switch on interaction number
LSWT	10	-	-	saturation control switch on contact number

Symbol Dictionary (page 21)

FORTRAN Name	Dimension	Symbol	Units	Definition
M	-	m	-	general index, often the index of the body segment forming the other side of a joint angle corresponding to the side with the same index as the joint, also used for the number of jitter modes less one left to resolve, or the number of contact forces left to be printed
MASK	8	-	-	masks used to extract individual bit positions
MAX	3	-	-	maximum numbers of time points in input tables
MAXI	-	-	-	number of modes in jitter
MAXR	-	-	-	number of modes for which jitter is possible for an occupant position
METH	-	-	-	switch indicating whether stick figure times are computed or to be inputted
MFORI	7	-	-	table containing the body segment index of the other side of the joint given the joint index
MM	-	-	-	number of nonzero forward chest contact forces
MMAX	-	-	-	maximum number of nonzero contact forces to be printed
MIN	-	-	-	number of nonzero knee contact forces
MODE	16	-	-	table containing a status indicator for each possible jitter mode

Symbol Dictionary (page 22)

FORTTRAN Name	Dimension	Symbol	Units	Definition
MPRINT	-	-	-	special initial print switch
MSBH	-	-	-	horizontal spaces on stick figure plot without grid
MSBV	-	-	-	vertical spaces on stick figure plot without grid
MSTART	-	-	-	starting index to print contact forces
MSTEP	-	-	-	number of contact forces already printed
MSTOP	-	-	-	stopping index to print contact forces
N	-	n	-	general index
N	8	-	-	number of points to represent each body segment in stick figure plot
NBELT	-	-	-	belt option indicator
NC	-	-	-	switch indicating no captions on graphs
NCHAR	-	-	-	switch indicating no captions on stick figures
NCNTCT	8	-	-	switches indicating whether contact arcs are to appear in stick figure
NCRT	-	-	-	CRT output switch (vestigial)
NEW	3	-	-	input table switches indicating whether changes made

Symbol Dictionary (page 23)

FORTTRAN Name	Dimension	Symbol	Units	Definition
NGRAPH	-	-	-	switch indicating whether graphs are desired
NHL	-	-	-	number of horizontal lines in grid
NINJ	-	-	-	switch indicating whether injury tolerance printout is desired
NMAX	-	-	-	maximum ratio of predicted force change to allowed force change
NNK	-	-	-	maximum number of input table entries
NONO	1402	-	-	dummy array to ensure master common big enough
NPASGR	-	-	-	occupant position indicator
NPROB	-	-	-	switch indicating whether injury probability printout is desired
NPTS1	-	-	-	number of points plotted on first graph
NPTS2	-	-	-	number of points plotted on second graph
NPTS3	-	-	-	number of points plotted on third graph
NS	-	-	-	maximum value of interaction index for occupant position
NS	5	-	-	plot scaling specification array for graphs
NSBH	-	-	-	number of spaces between horizontal grid lines
NSBV	-	-	-	number of spaces between vertical grid lines

Symbol Dictionary (page 24)

FORTRAN Name	Dimension	Symbol	Units	Definition
NSCALE	5	-	-	plot scaling specification array for stick figures
NST	-	-	-	general index
NSTICK	-	-	-	switch indicating whether stick figures are desired
NSTOP	-	-	-	number of contact forces for a page of printout
NT	-	-	-	general index
NVL	-	-	-	number of vertical grid lines
N1	-	-	-	degree of polynomial
N2	-	-	-	number of polynomial coefficients
N3	-	-	-	iteration counter
N4	-	-	-	general index
N6	-	-	-	general index
OLDELD	-	$\dot{\delta}_{m-1}$	in./sec	previous deflection rate
OMEGA	18	-	in.	required off deflection for unloading curve for each interaction
OMEGAI	7	Ω_i	rad	upper joint relative angle limits
OMGT	-	Ω	in.	maximum relative deflection

Symbol Dictionary (page 25)

FORTRAN Name	Dimension	Symbol	Units	Definition
OMSGE	-	-	-	elasticity for load-deflection model (1-G)
ON	-	-	-	label used in printing contact forces
ORD	-	-	1, in./sec ² 2,3, -	ordinate of table point
P	200,9	-	-	storage for hip and vehicle positions, velocities, and accelerations
PCHEST	-	-	in.	distance of chest accelerometer above upper spinal joint along upper torso centerline
PCNTL	-	-	-	number of minimum print times in one print time interval
PEAK	-	-	-	maximum absolute value of injury tolerance violation
PHEAD	-	-	in.	distance of head accelerometer above neck
PHI	3	ϕ_m	rad	belt angles
PHIZ	3	ϕ_{m0}	rad	initial belt angles
PHI1	200	-	rad	lap belt angle storage
PHI2	200	-	rad	lower shoulder belt angle storage
PHI3	200	-	rad	upper shoulder belt angle storage
PI	-	π	rad	180 degrees in radians

Symbol Dictionary (page 26)

FORTRAN Name	Dimension	Symbol	Units	Definition
PI	-	P	-	probability value
PITWO	-	$\pi/2$	rad	ninety degrees in radians
PLC	-	\ddot{X}	g-units	vehicle acceleration
PLX	-	\ddot{x}	g-units	hip forward acceleration
PLY	-	\ddot{y}	g-units	hip vertical acceleration
PN	18	-	lb	elements one through three are belt forces; elements five through eighteen are contact forces stored on the interaction index; element four is vestigial; (this is summarized, "for each interaction")
PNDEL	18	-	lb	spring portion of loading force for each interaction
POMG	-	Ω_{m-1}	in.	previous relative deflection
POST	200,9	-	-	storage for hip and vehicle positions, velocities, and accelerations
POUNDS	-	-	lb	change limit for a forward contact force in one time interval
PP	8	-	lb	current nonzero contact forces storage
PR	-	-	-	total probability
PRMX	-	-	in.	x-coordinate of center of curvature

Symbol Dictionary (page 27)

FORTRAN Name	Dimension	Symbol	Units	Definition
PRMY	-	-	in.	y-coordinate of center of curvature
PSIA	10	ψ_a	deg	contact surface reference angle
PTIM	-	-	sec	time of peak tolerance violation
PTLEN	-	-	in. ⁻¹	points per inch for plotting stick figure
PVAR	-	-	-	previous value of tolerance violation
QI	-	-	-	combination switch indicating whether a new probability label or which old label by index
QUE	10	Q_x	1-8, in. lb 9-10, lb	contact generalized force vector
R	-	-	-	number of points up to current point in stick figure representation of a line used in computation of coordinates
R	18	R	-	material energy absorption index, i.e., ratio of conserved energy to total energy, for each interaction
RA	10	R_a	-	material energy absorption index for each contact surface
RANG	-	-	-	temporary storage in stick figure computations
RH	-	r_h	in.	radius of arc of action of lap belt force

Symbol Dictionary (page 28)

FORTTRAN Name	Dimension	Symbol	Units	Definition
RHO	8	ρ_i	in.	distance of body segment centers of gravity above previous joints
RHOPFZ	-	ρ'_4	in.	distance of head center of curvature above neck
RHOPRM	8	ρ'_i	in.	distance of body segment center of curvature above previous joints
RHOPTZ	-	ρ'_3	in.	distance of chest center of curvature above upper spinal joint
RNEW	-	R	-	energy absorption index
RNSBH	-	-	-	number of horizontal spaces in stick figure plot
RNSBV	-	-	-	number of vertical spaces in stick figure plot
ROOTI	5	-	-	imaginary parts of roots of fifth order equation
ROOTI	15	-	-	imaginary parts of roots
ROOTR	5	-	-	real parts of roots of fifth order equation
ROOTR	15	-	-	real parts of roots
RPSI	16	ξ	1-7, rad/sec 8-16, in./sec	velocity limits for possible jitter modes
RSEL	16	\dot{v}	1-7, rad/sec ² 8-16, in./sec ²	relative or mode accelerations for possible jitter modes

Symbol Dictionary (page 29)

FORTTRAN Name	Dimension	Symbol	Units	Definition
R1M	-	-	-	temporary storage for root selection
RV	-	-	-	relative or mode velocity
RVEL	16	v	1-7, rad/sec 8-16, in./sec	relative or mode velocity for possible jitter modes
RZ	-	r _z	in.	distance from lower leg centerline to skin
S	-	s	lb/in.	spring constant for front edge of seat
SAGXX	-	σ ₀	lb	zeroth order loading coefficient
SAZ	8	-	-	sine of body angle
SCALEX	-	-	-	horizontal scale factor for plotting stick figures
SCALEY	-	-	-	vertical scale factor for plotting stick figures
SDEL	-	δ _m	in.	present deflection
SDELA	-	δ	in.	present contact deflection
SDELD	-	δ̇	in./sec	deflection rate
SDELTA	3	δ	in.	belt deflections for each belt segment
SDELTD	3	δ̇	in./sec	belt deflection rates for each belt segment
SDL	-	δ _m	in.	present deflection

Symbol Dictionary (page 30)

FORTRAN Name	Dimension	Symbol	Units	Definition
SDLD	-	$\dot{\delta}_m$	in./sec	present deflection rate
SETBCK	200	-	lb	hip seat force storage
SETFRT	200	-	lb	seat front vertical force storage
SI	-	-	-	head severity index
SIA	-	-	in.	perpendicular distance of body center of curvature from surface
SIG	10	σ_m	n=1-5, lb/in. ⁿ n=6-10, lb/(in./sec) ⁿ⁻⁵	material load-deflection coefficients
SICMA	10,3	σ_m	same as SIG	belt load-deflection coefficients
SIGMAA	10,10	σ_{am}	same as SIG	contact surface load-deflection coefficients for all surfaces
SIGMAC	10	σ_{cm}	same as SIG	(vestigial)
SIGZ	18	σ_o	lb	material zeroth order load-deflection coefficients for all interactions
SINTEN	-	-	-	sine of the relative angle between upper torso and upper arm
SIXTY	-	-	rad	angular spacing in foot contact arc representation in stick figure
SLOP	10	-	lb./in.	saturation unloading slope on contact number
SLOPE	18	-	lb./in.	saturation unloading slope on interaction number

Symbol Dictionary (page 31)

FORTRAN Name	Dimension	Symbol	Units	Definition
SMALLB	10	b_i	1-8, in. lb 9-10, lb	total continuous generalized force vector
SMALLF	-	f	lb	seat cushion friction force
SPHI	3	-	-	sines of belt angles
SPSIA	10	-	-	sines of contact surface angles
SQ	-	-	-	temporary storage
STEPS	200	-	sec	time storage for producing stick figures
STHETA	8	-	-	sines of body angles
STHETZ	8	-	-	initial values of sines of body angles
STIME	200	-	sec	time point storage for summary printout
STIMFJ	6	-	-	sines of belt angles relative to body segments
STIMTJ	13	-	-	sines of angles between body segments
SUMBY	-	-	lb	hip seat spring force
SWITCH	3	-	-	scan type switches for input tables
SZ	-	s_z	lb/in.	spring constant for horizontal front edge seat force
SZVEC	8	-	-	sines of body angles

Symbol Dictionary (page 32)

FORTRAN Name	Dimension	Symbol	Units	Definition
T	200	-	sec	time point storage
TA	8	$\ddot{\theta}_i$	deg/sec ²	body angle accelerations
TAHATZ	-	\hat{t}_0	sec	predicted time interval for the linear jitter mode to turn off
TANIEG	-	-	-	tangent of lower leg angle
TANTSV	-	-	-	tangent of upper leg angle
TAUHAT	-	\hat{t}	sec	minimum time interval until mode velocity reaches velocity limit
TAUI	16	τ_k	sec	storage of time intervals until mode velocity reaches velocity limit for all modes
TDSQLI	8	$L_1 \theta_1^2$	in./sec ²	intermediate step in centrifugal forces
TEM	-	-	-	temporary storage in calculation of zeroes
TEMI	-	-	-	temporary storage in calculation of zeroes
TEMR	-	-	-	temporary storage in calculation of zeroes
TE1	-	-	-	temporary storage in calculation of zeroes
TE2	-	-	-	temporary storage in calculation of zeroes
TE3	-	-	-	temporary storage in calculation of zeroes

Symbol Dictionary (page 33)

FORTRAN Name	Dimension	Symbol	Units	Definition
TE4	-	-	-	temporary storage in calculation of zeroes
TE5	-	-	-	temporary storage in calculation of zeroes
TE6	-	-	-	temporary storage in calculation of zeroes
TE7	-	-	-	temporary storage in calculation of zeroes
TE8	-	-	-	temporary storage in calculation of zeroes
TE9	-	-	-	temporary storage in calculation of zeroes
TE10	-	-	-	temporary storage in calculation of zeroes
TE11	-	-	-	temporary storage in calculation of zeroes
TE12	-	-	-	temporary storage in calculation of zeroes
TE13	-	-	-	temporary storage in calculation of zeroes
TE14	-	-	-	temporary storage in calculation of zeroes
TE15	-	-	-	temporary storage in calculation of zeroes
TE16	-	-	-	temporary storage in calculation of zeroes
TGAMZ	-	-	-	tangent of seat cushion angle
THATPS	-	\hat{T}_7	in. lb/rad	upper knee joint stop torque coefficient

Symbol Dictionary (page 34)

FORTRAN Name	Dimension	Symbol	Units	Definition
THATPV	-	\hat{T}'_5	in. lb/rad	upper shoulder joint stop torque coefficient
THATPW	-	\hat{T}'_1	in. lb/rad	upper hip joint stop torque coefficient
THATPX	-	\hat{T}'_6	in. lb/rad	upper elbow joint stop torque coefficient
THEDSQ	8	$\dot{\theta}_i^2$	(rad/sec) ²	square of body angular velocity
THEFEE	-	-	rad	initial value of relative angle between lower torso centerline and lap belt
THETA	200,3,8	-	deg,etc.	body angular position, velocity, and acceleration storage
THETAZ	8	θ_{i0}	rad	initial values of body angles
TIA	-	T_{ia}	in.	length of the line joining the body center of curvature to the contact surface reference point projected on the contact surface
TIMASK	-	τ^*	sec	minimum of print interval, inflection interval, and maximum time step
TIMAX	-	t_{max}	sec	duration of simulation
TIME	-	t	sec	value of time during simulation
TIMTJ	16	-	rad	body relative angles
TIMTJZ	16	-	rad	initial values of body relative angles

Symbol Dictionary (page 35)

FORTRAN Name	Dimension	Symbol	Units	Definition
TINFL	-	-	sec	time of next vehicle acceleration table entry (inflection time)
TMATII	8	T_{ij}	in. lb	joint stop torque
TOF	-	t_{off}	sec	time that the tolerance violation ceases
TOL	22	-	-	tolerance level values
TON	-	t_{on}	sec	time that the tolerance violation begins
TPRIME	7	T'_i	in. lb/rad	symmetric or lower joint stop torque coefficient
TPRINT	-	-	sec	next print time
TS	-	-	-	temporary storage
TSA	-	-	-	temporary storage
TSB	-	-	-	temporary storage
TSC	-	-	-	temporary storage
TSTEP	-	-	sec	last vehicle acceleration inflection time
TT	8	θ_i	deg	body angles
TV	8	$\dot{\theta}_i$	deg	body angle velocities
VAR	-	-	-	injury tolerance quantity

Symbol Dictionary (page 36)

FORTRAN Name	Dimension	Symbol	Units	Definition
VLINE	-	-	in.	vertical distance represented per grid line
VTIA	-	v_T	in./sec	velocity of body segment contact arc along contact surface
VXIA	-	V_x	in./sec	forward velocity of body center of curvature
VYIA	-	V_y	in./sec	upward velocity of body center of curvature
VZERO	50	-	in.	vertical distances represented at grid line
WORKA	10	-	-	temporary storage for matrix inversion
WORKB	10	-	-	temporary storage for matrix inversion
WZERO	-	w_0	lb	initial hip seat force
X	-	-	-	sine of desired angle
X	-	-	in./sec ²	forward acceleration of chest center of gravity, chest center of curvature, or head center of curvature
X	7	-	-	temporary storage for sorting input tables
X	7	x_1	in.	x-coordinates of joints
XA	-	-	sec	one end of deletion interval from input table
XAP	-	\dot{x}	in./sec	hip forward velocity

Symbol Dictionary (page 37)

FORTRAN Name	Dimension	Symbol	Units	Definition
XB	-	-	sec	one end of deletion interval from input table
XC	-	X	in.	vehicle x-coordinate
XCHEST	-	-	in./sec ²	chest center of gravity forward acceleration
XCHT	5	-	in.	x-coordinates of chest contact arc points
XCP	-	\dot{X}	in./sec	vehicle forward velocity
XELB	3	-	in.	x-coordinates of elbow contact arc points
XFLOOR	2	-	in.	x-coordinates of floor end points
XFT	5	-	in.	x-coordinates of foot contact arc points
XHEAD	-	-	in./sec ²	head center of gravity forward acceleration
XHEAD	200	-	in.	x-coordinate of head center of gravity storage
XHIP	5	-	in.	x-coordinates of hip contact arc points
XHND	5	-	in.	x-coordinates of hand contact arc points
XIDOT	7	-	in./sec	joint forward velocity
XISMLA	10	ξ_a	in./sec	contact surface friction velocity limit
XJOINT	9	-	in.	x-coordinates of joints including wrist and ankle

Symbol Dictionary (page 38)

FORTRAN Name	Dimension	Symbol	Units	Definition
XKNE	3	-	in.	x-coordinates of knee contact arc points
XL	2	-	in.	x-coordinates of lower shoulder belt end points
XLAP	2	-	in.	x-coordinates of lap belt end points
XLEN	8	-	in.	x-coordinates of plot arcs
XLP	2	-	in.	x-coordinates of lower panel end points
XLSW	2	-	in.	x-coordinates of lower steering wheel end points
XMAN	64	-	in.	x-coordinates of stick figure points
XMAX	-	-	in.	maximum x-coordinate of plot area
XMIN	-	-	in.	minimum x-coordinate of plot area
XPACZ	-	-	in./sec	initial value of hip forward velocity
XPRM	8	-	in.	x-coordinates of body centers of curvature
XR	2	-	in.	x-coordinates of roof end points
XRHO	-	-	in.	x-coordinate of chest center of curvature
XSC	2	-	in.	x-coordinates of steering column end points
XSEAT	3	-	in.	x-coordinates of seat end points and intersection

Symbol Dictionary (page 39)

FORTRAN Name	Dimension	Symbol	Units	Definition
XSMALA	10	-	in.	x-coordinates of contact surface reference points
XTOE	2	-	in.	x-coordinate of toeboard end points
XU	-	-	in.	x-coordinate of upper shoulder belt anchor point
XUSDF	2	-	in.	x-coordinates of upper steering wheel end points
XVEHZ	-	-	in./sec	initial value of vehicle forward velocity
XWS	2	-	in.	x-coordinates of windshield end points
XX	-	-	sec	argument of input table
XX	-	-	-	sine of desired angle
XXX	300,3	-	sec	input table time storage
XZ	-	x_z	in.	horizontal distance of front edge of seat from lower leg centerline
Y	-	-	in./sec ²	upward acceleration of chest center of gravity, chest center of curvature, or head center of curvature
Y	7	y_i	in.	y-coordinates of joints
YA	-	y	in.	hip y-coordinate
YAP	-	\dot{y}	in./sec	hip forward velocity

Symbol Dictionary (page 40)

FORTRAN Name	Dimension	Symbol	Units	Definition
YCHEST	-	-	in./sec ²	chest center of gravity upward acceleration
YCHT	6	-	in.	y-coordinates of chest contact arc points
YELB	3	-	in.	y-coordinates of elbow contact arc points
YEPSLN	-	-	in.	cumulative permanent deflection
YFLOOR	2	-	in.	y-coordinates of floor end points
YFT	5	-	in.	y-coordinates of foot contact arc points
YHEAD	-	-	in./sec ²	head center of gravity upward acceleration
YHEAD	200	-	in.	head center of gravity y-coordinate storage
YHIP	5	-	in.	y-coordinates of hip contact arc points
YHND	5	-	in.	y-coordinates of hand contact arc points
YIDOT	7	-	in./sec	joint upward velocity
YJOINT	9	-	in.	y-coordinates of joints including wrist and ankle
YKNE	3	-	in.	y-coordinates of knee contact arc points
YL	2	-	in.	y-coordinates of lower shoulder belt end points
YLAP	2	-	in.	y-coordinates of lap shoulder belt end points

Symbol Dictionary (page 41)

FORTRAN Name	Dimension	Symbol	Units	Definition
YLEN	8	-	in.	y-coordinates of plot arcs
YLP	2	-	in.	y-coordinates of lower panel end points
YLSW	2	-	in.	y-coordinates of lower steering wheel end points
YMAN	64	-	in.	y-coordinates of stick figure points
YMAX	-	-	in.	maximum y-coordinate of plot area
YMIN	-	-	in.	minimum y-coordinate of plot area
YPRM	8	-	in.	y-coordinates of body centers of curvature
YR	2	-	in.	y-coordinates of roof end points
YRHO	-	-	in.	y-coordinate of chest center of curvature
YS	-	y_s	in.	deflection of hip seat spring
YSC	2	-	in.	y-coordinates of steering column end points
YSEAT	3	-	in.	y-coordinates of seat end points and intersection
YSMALA	10	-	in.	y-coordinates of contact surface reference points
YSP	-	\dot{y}_s	in./sec	deflection rate of hip seat spring
YTOE	2	-	in.	y-coordinates of toeboard end points

Symbol Dictionary (page 42)

FORTTRAN Name	Dimension	Symbol	Units	Definition
YU	-	-	in.	y-coordinate of upper shoulder belt anchor point
YUSDF	2	-	in.	y-coordinates of steering wheel end points
YWS	2	-	in.	y-coordinates of windshield end points
YYY	300,3	-	1, in./sec ² 2,3, -	ordinates of input tables
YZZERO	-	Yz0	in.	vertical distance from the front edge of the seat to the point of seat cushion directly beneath the hip joint
Z	-	z	in.	horizontal distance of the front edge of the seat from the hip joint
ZERO	-	-	-	(vestigial)
ZERO	130	-	-	zero line plot array
ZK	11,128	\ddot{z}_k	1-8, rad/sec ² 9-11, in./sec ²	generalized acceleration contributions for all combinations of jitter modes on and off
ZKB	11	-	1-8, rad/sec ² 9-11, in./sec ²	base acceleration vector including both all continuous and turned on discontinuous
ZKBASE	11	-	1-8, rad/sec ² 9-11, in./sec ²	base acceleration vector including both all continuous and turned on discontinuous
XMLCTS	-	-	in.	horizontal distance of knee joint from front edge of seat

Symbol Dictionary (page 43)

FORTRAN Name	Dimension	Symbol	Units	Definition
ZP	11	-	-	temporary storage for mode velocities or accelerations
ZPAR	-	-	-	(vestigial)
ZPP	-	-	-	mode acceleration
ZPPP	128	-	-	mode acceleration for all combinations of jitter modes on and off for a particular mode
ZQ	11	-	1-8, rad/sec ² 9-11, in./sec ²	temporary storage of continuous generalized acceleration vector
ZR	10	-	1-8, rad/sec ² 9-11, in./sec ²	temporary storage of continuous generalized acceleration vector
ZRV	-	-	-	mode acceleration from base acceleration vector for jitter mode being considered
ZRVN	-	-	-	mode acceleration from base acceleration vector for second linear jitter mode
ZVEC	11	-	1-8, rad 9-11, in.	generalized coordinate vector including vehicle coordinate
ZVECP	11	-	1-8, rad/sec 9-11, in./sec	generalized velocity vector
ZVECPP	11	-	1-8, rad/sec ² 9-11, in./sec ²	generalized acceleration vector

Symbol Dictionary (page 44)

FORTRAN Name	Dimension	Symbol	Units	Definition
ZZERO	-	z_0	in.	x-coordinate of front edge of seat

Appendix to Symbol Dictionary (page 1)

<u>Symbol</u>	<u>FORTRAN Name(s)</u>
a	KA, LA, IA
a_1	A
\bar{a}_k	AK
\vec{B}	BEE
\vec{b}	SMALLB
\vec{C}	CEE
C_0	CZERON
C_1	CONEN
C_2	CTWON
C_s	CS
C'_1	CPRIME
\vec{D}	DEE
E_1	EONE
E_t	ET
\hat{E}	EHAT
\hat{E}_0	EO
F	FORCE, FT, FTT
F_m	FFM
F_{n-1}	FTOLD
F_s	FS
F_z	FZ

Appendix to Symbol Dictionary (page 2)

<u>Symbol</u>	<u>FORTTRAN Name(s)</u>
F'_s	FSPRM
F'_{s_0}	FSPRMZ
f	SMALLF
G	G
\vec{G}	GEE
G_a	GA
g	GRAVIT
h	H
I_i	EYE
i	KI, LI, I, II
i*	ISTAR
K_i	BIGKI
J_e	BIGMI
L_i	EL
L'	ELP
l_k	EL
l_{10}	ELZTEN
l_{20}	ELTWY
l_{30}	ELTHRY
l'_{10}	ELPTEN
m_i	EM

Appendix to Symbol Dictionary (page 3)

<u>Symbol</u>	<u>FORTRAN Name(s)</u>
m	AA
m^{-1}	ANVERS
p	PI
\vec{Q}	QUE
R	R, RNEW
R_a	RA
r_h	RH
r_i	AR
r_z	RZ
s	S
s_z	SZ
T_{ia}	TIA
T_{ij}	TMATII
T'_1	TPRIME
\hat{T}'_1	THATPW
\hat{T}'_5	THATPV
\hat{T}'_6	THATPX
\hat{T}'_7	THATPS
t	TIME
t_{max}	TIMAX
t_{off}	TOF

Appendix to Symbol Dictionary (page 4)

<u>Symbol</u>	<u>FORTRAL. NAME(s)</u>
T_{on}	TON
v_T	VTIA
V_x	VXIA
V_y	VYIA
W_o	WZERO
X	XC
\dot{X}	XCP
\ddot{X}	PLC
\dot{x}	XAP
\ddot{x}	PLX
x_h	HEADX
x_1	X, AX
\dot{x}_1	AXD
x_z	XZ
y_s	YS
\dot{y}_s	YSP
y_{zo}	YZZERO
y	YA
\dot{y}	YAP
\ddot{y}	PLY
y_h	HEADY

Appendix to Symbol Dictionary (page 5)

<u>Symbol</u>	<u>FORTRAN Name(s)</u>
\dot{y}_1	Y, AY
Z_0	ZZERO
\ddot{Z}_k	ZK
z	Z
z_k	AZ
\dot{z}_k	AZP
α_1	ALFAI
β_m	BETA
γ	LITGAM
γ_0	GAMZER
Δ	DELL, DELTA
Δ	DELTAT
Δt_{min}	DESTEP
$\Delta \vec{z}$	DELZ
Δv	DELNN, DELNU
δ	SDELTA, SDELA
δ_n	SDL
δ_{n-1}	DELOLD
$\dot{\delta}$	SDELTD, SDELD
$\ddot{\delta}$	SDLD
δ_{n-1}	OLDELD, DELDOD

Appendix to Symbol Dictionary (page 6)

<u>Symbol</u>	<u>FORTTRAN Name(s)</u>
ϵ	EPSLNY
ϵ_0	EPSLNZ
ϵ'	EPSLNP
η	ETA
θ_1	TT
θ_{10}	THETAZ
$\dot{\theta}_1$	TV
$\ddot{\theta}_1$	THEDSQ
θ'_1	TA
λ_1	ELAMB
μ_a	FMUA
μ_s	FMUS
ν	RVEL
$\dot{\nu}$	RSEL
ξ	RPSI
ξ_a	XISMLA
π	PI
ρ_1	RHO
ρ'_1	RHOPRM
ρ'_3	RHOPTZ
ρ'_4	RHOFFZ

Appendix to Symbol Dictionary (page 7)

<u>Symbol</u>	<u>FORTRAN Name(s)</u>
σ_o	SIGZ, SIGXX
σ_{am}	SIGMAA
σ_n	SIG, SIGMA
τ_k	TAUI
τ^*	TIMASK
$\hat{\tau}$	TAUHAT
$\hat{\tau}_o$	TAHATZ
ϕ'_{10}	FEPTEN
ϕ_m	PHI
ϕ_{m_o}	PHIZ
ψ_a	PSIA
Ω	OMGT, FOM
Ω_1	OMEGAI
Ω_{n-1}	POMG

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APPENDIX

LISTINGS OF
HSRI 2-D MODEL ROUTINES
AND
SUPPLEMENTARY ROUTINES

Subroutine Index

<u>Routine</u>	<u>Routine Number (Figs. 44 and 45)</u>	<u>Listing Page</u>	<u>Flow Diagram Page</u>
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ARCSIN	25	A-6	249
BELT	8	A-7	250
BODY	12	A-9	251
CONTAC	11	A-11	252
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ITOPOW	24	A-25	261
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LAND	g	A-99	-
LIMIDT	20	A-34	267
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MAIN	1	A-41	274
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MULLER	10	A-57	296
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Subroutine Index (Continued)

<u>Routine</u>	<u>Routine Number (Figs. 44 and 45)</u>	<u>Listing Page</u>	<u>Flow Diagram Page</u>
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RELSEL	18	A-65	302
RELVEL	14	A-66	303
SEAT	7	A-68	304
SIPP	26	A-70	306
STYX	27	A-75	307
SUMARY	23	A-80	312
TAUMAK	19	A-89	313
XDINFO	a	A-97	-
XERCOM	c	A-98	-
XPRINT	b	A-98	-
YPRINT	d	A-92	-
ZKMAKR	17	A-93	317
ZMAKER	13	A-95	318
TALK2*	-	A-152	-
BAIL2*	-	A-158	-

*These two are for recovery of output from an aborted run. Supplied here in unconverted form; Common/IO/INN needs to be added in BAIL2 along with INN=5 and the l.d.n.'s may need switching around in TALK2. BAIL2 is run with SUMARY and the routines called by SUMARY with the cards after the Z card supplied on l.d.n. five and the summary file supplied on l.d.n. nine.


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1  SUBROUTINE ACCEL
2  COMMON SWITCH,NEH,MAX,IPUST,XXX,YYY,FMM,RBR,IGNORE,DA,XSMALA,YSMAL,*2D21600
3  *2D21610
4  IA,XISMALA,PSIA,SPSIA,CPSIA,FMA,SIGMA,SIGMA,AA,KTABLE,MFORI,DIR,PI,*2D21620
5  2TMO,GRAVIT,CPRIME,BIGKI,EL,AR,TPRIME,ALFAI,OMEGAI,RPSI,RHO,THETAZ,*2D21630
6  3THETZ,CTHETZ,FSRPM,RH,THATPV,WZROPTZ,RHOPTZ,GAMZER,LCONTL,CS,*2D21640
7  4,S,FMS,BETA,ZZERO,ELIMTY,ELTHRY,M,DESTER,DELTA,PHIZ,DELTA,NPASGR,*2D21650
8  5,XPACZ,NBELT,APRNTD,TIMAX,DTRNT,BPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA,*2D21670
9  6,ELAMB,TIME,IBUG,MAXR,LITGAM,EPSLVZ,RSEL,RVEL,IBIG,IFORK,PASIC,FS,*2D21680
10  7SMALL,ZVEC,ZVECP,ZVECP,THESQ,CTHETA,STHETA,BIGMI,TMATII,*2D21690
11  8XIDOT,YIDOT,PHI,EONE,SDELTA,SDELTD,RL,PN,MODE,OMEGA,X,Y,THEFEE,RH,*2D21700
12  9PRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOLD,DELDOO,E,SLNY,FTOLD,FSRPMZ *2D21710
13  COMMON CZERON,CCNEN,CTMCN,ET,EHAT,SEE,SMALLB,AEL,TIMTJZ,TGAMZ,YZE,*2D21720
14  1RO,FSZCNS,ANVERS,TINFL,KPOST,TPRINT,TSSTEP,AVEL,RVELB,CVELC,AACCA,*2D21730
15  2BACCB,CACCC,DACCCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSQLI,ATDSQ,TIMT,*2D21740
16  3J,STIMTJ,DELZ,ZK,ZPPP,TAMATZ,TS,TSB,SIGMAC,ITAU,TAUMAT,PZ,SZ *2D21750
17  *2D21760
18  *2D21770
19  DIMENSION SWITCH(3),NEH(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3)*2D21780
20  1),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),RIGKI(7),*2D21790
21  2TPRIME(7),ALFAI(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR(*2D21800
22  3),RHO(8),THETAZ(8),STHETZ(8),CTHETZ(8),IBIG(8),THEDSQ(8),CTHETA(8)*2D21810
23  4),STHETA(8),BIGMI(8),TMATII(8),RHOPRM(8),XPRM(8),YPRM(8),*2D21820
24  5,TDSQL(8),ATDSQ(8),IGNORE(10),DA(10),XSMALA(10),YSMALA(10),XISMALA*2D21830
25  6(10),PSIA(10),CPSIA(10),SPSIA(10),SIGMAC(10),FMVA(10),GRAVA(10),BF*2D21840
26  7(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11)*2D21850
27  8),ZVECP(11),STIMTJ(13),AEL(14),RSEL(16),RVEL(16),WDOE(16),TIMTJZ(*2D21860
28  9),TIMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EONE(18),PN(18) *2D21870
29  DIMENSION DELOLD(18),DELDOO(18),E,PSLNY(18),F,TOLD(18),OMEGA(18),CZE*2D21880
30  1RON(18),CONEN(18),CTMON(18),ET(18),EHAT(18),IFORK(3,8),SIGMA(10,3)*2D21890
31  2,XXX(300,3),YYY(300,3),FMM(300,3),BBB(300,3),SIGMAA(10,1)*2D21900
32  3),AA(10,10),ANVERSI(10,10),DELZ(11,16),ZK(11,128),BASIC(11,8),KTAB*2D21910
33  4LE(2,14),ZPPP(128),BL(3)
34  *2D21930
35  COMMON TMATPM,TMATPX,TMATPS,XVEMZ
36  COMMON FARB(18),SLOPE(18),ISWT(18),LOADSWT(18)
37  COMMON NUNO(1402)
38  DO 3060 I=1,8
39  STHETA(I) = SIN(ZVEC(I))
40  CTHETA(I) = COS(ZVEC(I))
41  THEDSQ(I) = ZVECP(I)*ZVECP(I)
42  TDSQL(I) = EL(I)*THEDSQ(I)
43  ATDSQ(I) = ALL(I)*THEDSQ(I)
44  3060 CONTINUE
45  TIMTJ(1) = ZVEC(1)-ZVEC(2)
46  TIMTJ(1) = SIM(TIMTJ(1))
47  TIMTJ(2) = ZVEC(1)-ZVEC(3)
48  TIMTJ(2) = SIM(TIMTJ(2))
49  TIMTJ(3) = ZVEC(1)-ZVEC(4)
50  TIMTJ(3) = SIM(TIMTJ(3))

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51 TIMTJ(4) = ZVEC(1)-ZVEC(5)
52 STIMTJ(4) = SIN(TIMTJ(4))
53 TIMTJ(5) = ZVEC(1)-ZVEC(6)
54 STIMTJ(5) = SIN(TIMTJ(5))
55 TIMTJ(6) = ZVEC(1)-ZVEC(7)
56 TIMTJ(7) = ZVEC(2)-ZVEC(3)
57 STIMTJ(6) = SIN(TIMTJ(7))
58 TIMTJ(8) = ZVEC(2)-ZVEC(4)
59 STIMTJ(7) = SIN(TIMTJ(8))
60 TIMTJ(9) = ZVEC(2)-ZVEC(5)
61 STIMTJ(8) = SIN(TIMTJ(9))
62 TIMTJ(10) = ZVEC(2)-ZVEC(6)
63 TIMTJ(11) = ZVEC(3)-ZVEC(4)
64 STIMTJ(9) = SIN(TIMTJ(11))
65 TIMTJ(12) = ZVEC(3)-ZVEC(5)
66 STIMTJ(10) = SIN(TIMTJ(12))
67 TIMTJ(13) = ZVEC(3)-ZVEC(6)
68 STIMTJ(11) = SIN(TIMTJ(13))
69 TIMTJ(14) = ZVEC(4)-ZVEC(5)
70 STIMTJ(12) = SIN(TIMTJ(14))
71 TIMTJ(15) = ZVEC(5)-ZVEC(6)
72 STIMTJ(13) = SIN(TIMTJ(15))
73 TIMTJ(16) = ZVEC(7)-ZVEC(8)
74 STIMTJ(14) = SIN(TIMTJ(16))
75 IF (18UG-3) 4100,3C70,3070
76 11=1,8)
3070 WRITE(6,9950)(STHETA(1),CT+ETA(1),THDSO(1),TDSO(1),ATDSO(1),
9950 FORMAT (5H0STEP/(1X5E20.8))
4100 CALL SEAT
77 Y(1) = ZVEC(10)
78 X(2) = X(1)+EL(1)*CTHETA(1)
79 Y(2) = Y(1)+EL(1)*STHETA(1)
80 X(3) = X(2)+EL(2)*CTHETA(2)
81 Y(3) = Y(2)+EL(2)*STHETA(2)
82 X(4) = X(3)+EL(3)*CTHETA(3)
83 Y(4) = Y(3)+EL(3)*STHETA(3)
84 X(5) = X(4)+EL(4)*CTHETA(4)
85 Y(5) = Y(4)+EL(4)*STHETA(4)
86 X(6) = X(5)+EL(5)*CTHETA(5)
87 Y(6) = Y(5)+EL(5)*STHETA(5)
88 X(7) = X(6)+EL(6)*CTHETA(6)
89 Y(7) = Y(6)+EL(6)*STHETA(6)
90 X(8) = X(7)+EL(7)*CTHETA(7)
91 Y(8) = Y(7)+EL(7)*STHETA(7)
92 X(9) = X(8)+EL(8)*CTHETA(8)
93 Y(9) = Y(8)+EL(8)*STHETA(8)
94 X(10) = X(9)+EL(9)*CTHETA(9)
95 Y(10) = Y(9)+EL(9)*STHETA(9)
96 X(11) = X(10)+EL(10)*CTHETA(10)
97 Y(11) = Y(10)+EL(10)*STHETA(10)
98 X(12) = X(11)+EL(11)*CTHETA(11)
99 Y(12) = Y(11)+EL(11)*STHETA(11)
100 X(13) = X(12)+EL(12)*CTHETA(12)
101 Y(13) = Y(12)+EL(12)*STHETA(12)
102 X(14) = X(13)+EL(13)*CTHETA(13)
103 Y(14) = Y(13)+EL(13)*STHETA(13)
104 X(15) = X(14)+EL(14)*CTHETA(14)
105 Y(15) = Y(14)+EL(14)*STHETA(14)
106 X(16) = X(15)+EL(15)*CTHETA(15)
107 Y(16) = Y(15)+EL(15)*STHETA(15)
108 X(17) = X(16)+EL(16)*CTHETA(16)
109 Y(17) = Y(16)+EL(16)*STHETA(16)
110 X(18) = X(17)+EL(17)*CTHETA(17)
111 Y(18) = Y(17)+EL(17)*STHETA(17)
112 X(19) = X(18)+EL(18)*CTHETA(18)
113 Y(19) = Y(18)+EL(18)*STHETA(18)
114 X(20) = X(19)+EL(19)*CTHETA(19)
115 Y(20) = Y(19)+EL(19)*STHETA(19)
116 X(21) = X(20)+EL(20)*CTHETA(20)
117 Y(21) = Y(20)+EL(20)*STHETA(20)
118 X(22) = X(21)+EL(21)*CTHETA(21)
119 Y(22) = Y(21)+EL(21)*STHETA(21)
120 X(23) = X(22)+EL(22)*CTHETA(22)
121 Y(23) = Y(22)+EL(22)*STHETA(22)
122 X(24) = X(23)+EL(23)*CTHETA(23)
123 Y(24) = Y(23)+EL(23)*STHETA(23)
124 X(25) = X(24)+EL(24)*CTHETA(24)
125 Y(25) = Y(24)+EL(24)*STHETA(24)
126 X(26) = X(25)+EL(25)*CTHETA(25)
127 Y(26) = Y(25)+EL(25)*STHETA(25)
128 X(27) = X(26)+EL(26)*CTHETA(26)
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133 Y(29) = Y(28)+EL(28)*STHETA(28)
134 X(30) = X(29)+EL(29)*CTHETA(29)
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136 X(31) = X(30)+EL(30)*CTHETA(30)
137 Y(31) = Y(30)+EL(30)*STHETA(30)
138 X(32) = X(31)+EL(31)*CTHETA(31)
139 Y(32) = Y(31)+EL(31)*STHETA(31)
140 X(33) = X(32)+EL(32)*CTHETA(32)
141 Y(33) = Y(32)+EL(32)*STHETA(32)
142 X(34) = X(33)+EL(33)*CTHETA(33)
143 Y(34) = Y(33)+EL(33)*STHETA(33)
144 X(35) = X(34)+EL(34)*CTHETA(34)
145 Y(35) = Y(34)+EL(34)*STHETA(34)
146 X(36) = X(35)+EL(35)*CTHETA(35)
147 Y(36) = Y(35)+EL(35)*STHETA(35)
148 X(37) = X(36)+EL(36)*CTHETA(36)
149 Y(37) = Y(36)+EL(36)*STHETA(36)
150 X(38) = X(37)+EL(37)*CTHETA(37)
151 Y(38) = Y(37)+EL(37)*STHETA(37)
152 X(39) = X(38)+EL(38)*CTHETA(38)
153 Y(39) = Y(38)+EL(38)*STHETA(38)
154 X(40) = X(39)+EL(39)*CTHETA(39)
155 Y(40) = Y(39)+EL(39)*STHETA(39)
156 X(41) = X(40)+EL(40)*CTHETA(40)
157 Y(41) = Y(40)+EL(40)*STHETA(40)
158 X(42) = X(41)+EL(41)*CTHETA(41)
159 Y(42) = Y(41)+EL(41)*STHETA(41)
160 X(43) = X(42)+EL(42)*CTHETA(42)
161 Y(43) = Y(42)+EL(42)*STHETA(42)
162 X(44) = X(43)+EL(43)*CTHETA(43)
163 Y(44) = Y(43)+EL(43)*STHETA(43)
164 X(45) = X(44)+EL(44)*CTHETA(44)
165 Y(45) = Y(44)+EL(44)*STHETA(44)
166 X(46) = X(45)+EL(45)*CTHETA(45)
167 Y(46) = Y(45)+EL(45)*STHETA(45)
168 X(47) = X(46)+EL(46)*CTHETA(46)
169 Y(47) = Y(46)+EL(46)*STHETA(46)
170 X(48) = X(47)+EL(47)*CTHETA(47)
171 Y(48) = Y(47)+EL(47)*STHETA(47)
172 X(49) = X(48)+EL(48)*CTHETA(48)
173 Y(49) = Y(48)+EL(48)*STHETA(48)
174 X(50) = X(49)+EL(49)*CTHETA(49)
175 Y(50) = Y(49)+EL(49)*STHETA(49)
176 X(51) = X(50)+EL(50)*CTHETA(50)
177 Y(51) = Y(50)+EL(50)*STHETA(50)
178 X(52) = X(51)+EL(51)*CTHETA(51)
179 Y(52) = Y(51)+EL(51)*STHETA(51)
180 X(53) = X(52)+EL(52)*CTHETA(52)
181 Y(53) = Y(52)+EL(52)*STHETA(52)
182 X(54) = X(53)+EL(53)*CTHETA(53)
183 Y(54) = Y(53)+EL(53)*STHETA(53)
184 X(55) = X(54)+EL(54)*CTHETA(54)
185 Y(55) = Y(54)+EL(54)*STHETA(54)
186 X(56) = X(55)+EL(55)*CTHETA(55)
187 Y(56) = Y(55)+EL(55)*STHETA(55)
188 X(57) = X(56)+EL(56)*CTHETA(56)
189 Y(57) = Y(56)+EL(56)*STHETA(56)
190 X(58) = X(57)+EL(57)*CTHETA(57)
191 Y(58) = Y(57)+EL(57)*STHETA(57)
192 X(59) = X(58)+EL(58)*CTHETA(58)
193 Y(59) = Y(58)+EL(58)*STHETA(58)
194 X(60) = X(59)+EL(59)*CTHETA(59)
195 Y(60) = Y(59)+EL(59)*STHETA(59)
196 X(61) = X(60)+EL(60)*CTHETA(60)
197 Y(61) = Y(60)+EL(60)*STHETA(60)
198 X(62) = X(61)+EL(61)*CTHETA(61)
199 Y(62) = Y(61)+EL(61)*STHETA(61)
200 X(63) = X(62)+EL(62)*CTHETA(62)
201 Y(63) = Y(62)+EL(62)*STHETA(62)
202 X(64) = X(63)+EL(63)*CTHETA(63)
203 Y(64) = Y(63)+EL(63)*STHETA(63)
204 X(65) = X(64)+EL(64)*CTHETA(64)
205 Y(65) = Y(64)+EL(64)*STHETA(64)
206 X(66) = X(65)+EL(65)*CTHETA(65)
207 Y(66) = Y(65)+EL(65)*STHETA(65)
208 X(67) = X(66)+EL(66)*CTHETA(66)
209 Y(67) = Y(66)+EL(66)*STHETA(66)
210 X(68) = X(67)+EL(67)*CTHETA(67)
211 Y(68) = Y(67)+EL(67)*STHETA(67)
212 X(69) = X(68)+EL(68)*CTHETA(68)
213 Y(69) = Y(68)+EL(68)*STHETA(68)
214 X(70) = X(69)+EL(69)*CTHETA(69)
215 Y(70) = Y(69)+EL(69)*STHETA(69)
216 X(71) = X(70)+EL(70)*CTHETA(70)
217 Y(71) = Y(70)+EL(70)*STHETA(70)
218 X(72) = X(71)+EL(71)*CTHETA(71)
219 Y(72) = Y(71)+EL(71)*STHETA(71)
220 X(73) = X(72)+EL(72)*CTHETA(72)
221 Y(73) = Y(72)+EL(72)*STHETA(72)
222 X(74) = X(73)+EL(73)*CTHETA(73)
223 Y(74) = Y(73)+EL(73)*STHETA(73)
224 X(75) = X(74)+EL(74)*CTHETA(74)
225 Y(75) = Y(74)+EL(74)*STHETA(74)
226 X(76) = X(75)+EL(75)*CTHETA(75)
227 Y(76) = Y(75)+EL(75)*STHETA(75)
228 X(77) = X(76)+EL(76)*CTHETA(76)
229 Y(77) = Y(76)+EL(76)*STHETA(76)
230 X(78) = X(77)+EL(77)*CTHETA(77)
231 Y(78) = Y(77)+EL(77)*STHETA(77)
232 X(79) = X(78)+EL(78)*CTHETA(78)
233 Y(79) = Y(78)+EL(78)*STHETA(78)
234 X(80) = X(79)+EL(79)*CTHETA(79)
235 Y(80) = Y(79)+EL(79)*STHETA(79)
236 X(81) = X(80)+EL(80)*CTHETA(80)
237 Y(81) = Y(80)+EL(80)*STHETA(80)
238 X(82) = X(81)+EL(81)*CTHETA(81)
239 Y(82) = Y(81)+EL(81)*STHETA(81)
240 X(83) = X(82)+EL(82)*CTHETA(82)
241 Y(83) = Y(82)+EL(82)*STHETA(82)
242 X(84) = X(83)+EL(83)*CTHETA(83)
243 Y(84) = Y(83)+EL(83)*STHETA(83)
244 X(85) = X(84)+EL(84)*CTHETA(84)
245 Y(85) = Y(84)+EL(84)*STHETA(84)
246 X(86) = X(85)+EL(85)*CTHETA(85)
247 Y(86) = Y(85)+EL(85)*STHETA(85)
248 X(87) = X(86)+EL(86)*CTHETA(86)
249 Y(87) = Y(86)+EL(86)*STHETA(86)
250 X(88) = X(87)+EL(87)*CTHETA(87)
251 Y(88) = Y(87)+EL(87)*STHETA(87)
252 X(89) = X(88)+EL(88)*CTHETA(88)
253 Y(89) = Y(88)+EL(88)*STHETA(88)
254 X(90) = X(89)+EL(89)*CTHETA(89)
255 Y(90) = Y(89)+EL(89)*STHETA(89)
256 X(91) = X(90)+EL(90)*CTHETA(90)
257 Y(91) = Y(90)+EL(90)*STHETA(90)
258 X(92) = X(91)+EL(91)*CTHETA(91)
259 Y(92) = Y(91)+EL(91)*STHETA(91)
260 X(93) = X(92)+EL(92)*CTHETA(92)
261 Y(93) = Y(92)+EL(92)*STHETA(92)
262 X(94) = X(93)+EL(93)*CTHETA(93)
263 Y(94) = Y(93)+EL(93)*STHETA(93)
264 X(95) = X(94)+EL(94)*CTHETA(94)
265 Y(95) = Y(94)+EL(94)*STHETA(94)
266 X(96) = X(95)+EL(95)*CTHETA(95)
267 Y(96) = Y(95)+EL(95)*STHETA(95)
268 X(97) = X(96)+EL(96)*CTHETA(96)
269 Y(97) = Y(96)+EL(96)*STHETA(96)
270 X(98) = X(97)+EL(97)*CTHETA(97)
271 Y(98) = Y(97)+EL(97)*STHETA(97)
272 X(99) = X(98)+EL(98)*CTHETA(98)
273 Y(99) = Y(98)+EL(98)*STHETA(98)
274 X(100) = X(99)+EL(99)*CTHETA(99)
275 Y(100) = Y(99)+EL(99)*STHETA(99)

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101 XIDOT(5) = XIDOT(3)-EL(4)*STHETA(3)*ZVECP(3)
102 YIDOT(5) = YIDOT(3)+EL(4)*CTHETA(3)*ZVECP(3)
103 XIDOT(6) = XIDOT(5)-EL(5)*STHETA(5)*ZVECP(5)
104 YIDOT(6) = YIDOT(5)+EL(5)*CTHETA(5)*ZVECP(5)
105 XIDOT(7) = XIDOT(6)-EL(7)*STHETA(7)*ZVECP(7)
106 YIDOT(7) = YIDOT(6)+EL(7)*CTHETA(7)*ZVECP(7)
107 CALL BELT
108 CALL CONTAC
109 BIGMI(1) = BIGKI(1)*(TIMTJ(6)-TIMTJ(1))
110 BIGMI(2) = BIGKI(2)*(TIMTJ(1)-TIMTJ(1))
111 BIGMI(3) = BIGKI(3)*(TIMTJ(7)-TIMTJ(7))
112 BIGMI(4) = BIGKI(4)*(TIMTJ(11)-TIMTJ(11))
113 BIGMI(5) = BIGKI(5)*(TIMTJ(12)-TIMTJ(12))
114 BIGMI(6) = BIGKI(6)*(TIMTJ(15)-TIMTJ(15))
115 BIGMI(7) = BIGKI(7)*(TIMTJ(16)-TIMTJ(16))
116 CEE(3) = BIGMI(3)-BIGMI(4)-BIGMI(5)
117 CEE(2) = BIGMI(2)-BIGMI(3)
118 CEE(1) = BIGMI(1)-BIGMI(2)
119 CEE(5) = BIGMI(5)-BIGMI(6)
120 CEE(7) = -BIGMI(1)-BIGMI(7)
121 CEE(6) = BIGMI(6)
122 CEE(4) = BIGMI(4)
123 CEE(9) = 0.
124 CEE(10) = 0.
125 CEE(8) = BIGMI(7)
126
127 C
128 5000 CALL BODY 5.2.2 MATRIX SECTION
129 AA(2,1) = AEL(1)*COS(TIMTJ(1))
130 AA(3,1) = AEL(2)*COS(TIMTJ(2))
131 AA(3,2) = AEL(3)*COS(TIMTJ(7))
132 AA(4,1) = AEL(4)*COS(TIMTJ(3))
133 AA(4,2) = AEL(5)*COS(TIMTJ(8))
134 AA(4,3) = AEL(6)*COS(TIMTJ(11))
135 AA(5,1) = AEL(7)*COS(TIMTJ(4))
136 AA(5,2) = AEL(8)*COS(TIMTJ(9))
137 AA(6,1) = AEL(10)*COS(TIMTJ(5))
138 AA(6,2) = AEL(11)*COS(TIMTJ(10))
139 AA(6,3) = AEL(12)*COS(TIMTJ(13))
140 AA(6,5) = AEL(13)*COS(TIMTJ(15))
141 AA(8,7) = AEL(14)*COS(TIMTJ(16))
142 DO 5210 I=1,8
143 AA(9,I) = -A(I)*STHETA(I)
144 5210 AA(10,I) = A(I)*CTHETA(I)
145 CALL ZMAKER
146 5330 RETURN
147 END

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*2D22600
*2D22610
*2D22620
*2D22630
*2D22640
*2D22650
*2D22660
*2D22670
*2D22680
*2D22690
*2D22700
*2D22710
*2D22720
*2D22730
*2D22740
*2D22750
*2D22760
*2D22770
*2D22780
*2D22790
*2D22800
*2D22810
*2D22820
*2D22830
*2D22840
*2D22850
*2D22860
*2D22870
*2D22880
*2D22890
*2D22900
*2D22910
*2D22920
*2D22930
*2D22940
*2D22950
*2D22960
*2D22970
*2D22980
*2D22990
*2D23000
*2D23010
*2D23020
*2D23030
*2D23040
*2D23050
*2D23060

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*2028420
*2028430
*2028440
*2028450
*2028460
*2028470
*2028480
*2028490
*2028500
*2028510
*2028520
*2028530
*2028540
*2028550
*2028560
*2028570
*2028580
*2028590

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```

1      FUNCTION ARCSIN(X)
2      DATA PITWO,PI,CO,C1,C2,C3,C4,C5,C6,C7/1.,570796,
3      13.14159,1.570796,-.2145989,.08897899,-.05017430,
4      2.03089188,-.01708813,-.00667009,-.001262491/
5      XX=ABS(X)
6      IF (XX.LE..001) GO TO 50
7      SQ=1.-XX
8      IF (SQ.LT.0.) GO TO 40
9      ANS=PITWO-SQRT(SQ)*(((C7*XX+C6)*XX+C5)*XX+
10     IC4)*XX+C3)*XX+C2)*XX+C1)*XX+C0)
11     ARCSIN=SIGN(ANS,X)
12     RETURN
13     20
14     40 ARCSIN=SIGN(PITWO,X)
15     RETURN
16     ANS=XX
17     GO TO 20
18     END

```

Subroutine ARCSIN

```

1 SUBROUTINE BELT
2 COMMON SWITCH, NEM, MAX, IPOST, XXX, YYY, FMM, BBB, BB, IGNORE, DA, XSMALA, YSMAL, *2D20070
3 IA, XI, SMLA, P, SIA, SPSI, A, CP, SIA, F, MUA, SIGMA, S, IGMA, AA, KTARLE, MFORI, DIR, PI, *2D20080
4 2TWO, GRAVIT, CPRIME, BIGKI, EL, AR, TPRI, ME, GAI, RPSI, RHO, THE, TAZ, *2D20100
5 3STHETZ, CTHETZ, FSPR, M, RH, THAT, PV, WZERO, RHDP, TZ, RHO, P, FZ, CAMZER, L, CONTL, CS, *2D20120
6 4, S, F, MUS, BE, TA, ZZERO, EL, THRY, H, DEST, EP, DELT, AT, PHIZ, DELTA, NPASGR, *2D20130
7 5, XPACZ, NBELT, APRNTD, T, I, MAX, DT, PRNT, APRNTD, G, R, NS, SIGZ, EL, ZTEN, A, GRAVA, *2D20140
8 6, ELAMB, TIME, IBUG, MAXR, LITGAM, EPSLNZ, RSEL, RVEL, IBIG, IFORK, BASIC, FS, *2D20150
9 7SMALLF, ZVEC, ZVECP, ZVECPP, THE, DSQ, CTHETA, S, THETA, BIGNI, T, MAT, II, *2D20160
10 8XIDOT, YIDOT, PHI, EONE, S, DELTA, S, DELTD, BL, PN, MODE, OMEGA, X, Y, THEFEE, RM, *2D20170
11 9OPRM, XPRM, YPRM, BEE, CEE, DEE, QUE, DEL, OLD, DELDD, E, PSLNY, FTOLD, FSPR, *2D20180
12 10COMMON C, ZERON, CONEN, CTWON, ET, EHAT, GEE, S, SMALLB, AEL, TIMT, JZ, TGAMZ, YZ, *2D20190
13 11RO, F, SZCNS, ANVERS, T, INFL, KPOST, T, PRINT, T, STEP, AVELA, RVELB, CVEL, C, AACCA, *2D20200
14 12BACCB, CACCC, DACCD, MAXI, KPRINT, KSTEP, KINFL, TIMASK, TDSQL, I, ATDSQ, TIMT, *2D20210
15 13J, STINTJ, DELZ, ZK, ZPPP, TAHATZ, TSA, TSB, SIGMAC, ITAU, TAUHAT, RZ, SZ *2D20220
16 14 *2D20230
17 15 *2D20240
18 16 DIMENSION SWITCH(3), NEW(3), MAX(3), IPOST(3), BETA(3), PHIZ(3), DELTA(3), *2D20250
19 17 1), PHI(3), SDELTA(3), SDELTD(3), ELAMB(6), MFORI(7), CPRIME(7), BIGKI(7), *2D20260
20 18 2), PRIME(7), ALFAI(7), OMEGAI(7), XIDOT(7), YIDOT(7), X(7), Y(7), EL(8), AR( *2D20270
21 19 3), RHO(8), THETA(8), STHETA(8), CTMETZ(8), IBIG(8), THE, DSQ(8), CTHETA(8), *2D20280
22 20 4), S, THE, TA(8), BIGNI(8), T, MAT, II(8), RHOPR, M(8), XPRM(8), YPRM(8), *2D20290
23 21 5), TDSQL(8), ATDSQ(8), I, GNORE(10), DA(10), XSMALA(10), YSMALA(10), *2D20300
24 22 6(10), PSIA(10), CPSIA(10), SPSIA(10), SIGMAC(10), F, MUA(10), GRAVA(10), RE, *2D20310
25 23 7E(10), CEE(10), QUE(10), DEE(10), GEE(10), SMALLB(10), ZVEC(11), ZVECP(11), *2D20320
26 24 8), ZVECPP(11), STINTJ(13), AEL(14), RSEL(16), RVEL(16), MODE(16), TIMT, JZ( *2D20330
27 25 916), TIMT, J(16), RPSI(16), A(17), G(18), R(18), SIGZ(18), EONE(18), PNI(18), *2D20340
28 26 DIMENSION DELOLD(18), DELDD(18), EPSLN(18), EPSLN(18), FOLD(18), OMEGA(18), CZE, *2D20350
29 27 1), I, ON(18), CTWON(18), ET(18), EHAT(18), IFORK(3,8), SIGMA(10,3), *2D20360
30 28 2), XXX(30,3), YYY(30,3), FMM(30,3), BBB(30,3), *2D20370
31 29 30), AA(10,10), ANVERS(10,10), DELZ(11,16), ZK(11,16), BASIC(11,8), KTAB, *2D20380
32 30 4LE(2,14), ZPPP(128), BL(3) *2D20390
33 31 *2D20400
34 32 COMMON THATPM, THATPX, THATPS, XVEHZ *2D20410
35 33 COMMON FARB(18), SLOPE(18), ISWT(18), L, ODSMT(18) *2D20420
36 34 COMMON NONO(1402) *2D20430
37 35 DIMENSION CPHI(3), SPHI(3), STIMFJ(6) *2D20440
38 36 IF (NBELT-1) 30, 20, 10 *2D20450
39 37 TSA = Y(2)+H*CTHETA(2)-ELAMB(4) *2D20460
40 38 PHI(2)=ATAN2(TSA,TS) *2D20470
41 39 CPHI(2) = COS(PHI(2)) *2D20480
42 40 SPHI(2) = SIN(PHI(2)) *2D20490
43 41 STIMFJ(2) = SIN(ZVEC(1))-PHI(2) *2D20500
44 42 STIMFJ(4) = SIN(ZVEC(2))-PHI(2) *2D20510
45 43 SDELTA(2) = SORT(ITS+TSA*TSA)-BLTWTY *2D20520
46 44 BL(2)=SDELTA(2)+ELTWTY *2D20530
47 45 SDELTD(2)=XIDOT(1)*CPHI(2)+YIDOT(1)*SPHI(2)-EL(1)+ZVECP(1)*STIMFJ( *2D20540
48 46 12)-H*ZVEC(2)*STIMFJ(4) *2D20550
49 47 *2D20560
50

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51 CALL LODFEC(2, DELTA(2), SIGMA(1,2), SDELTA(2), SDELTD(2))
52 TS = X(5) - ELAMB(6)
53 TSA = Y(5) - ELAMB(5)
54 PHI(3) = ATAN2(TSA, TSI)
55 CPMI(3) = COS(PHI(3))
56 SPMI(3) = SIN(PHI(3))
57 STIMFJ(3) = SIN(ZVEC(1) - PHI(3))
58 STIMFJ(5) = SIN(ZVEC(2) - PHI(3))
59 STIMFJ(6) = SIN(ZVEC(3) - PHI(3))
60 SDELTA(3) = SORT(TS*TS + TSA*TSA) - ELTHRY
61 BL(3) = SDELTA(3) + ELTHRY
62 SDELTD(3) = XI(3) + CPMI(3) * Y(3) + SPMI(3) * EL(1) + ZVEC(1) * STIMFJ(3)
63 3) - EL(2) + ZVEC(2) * STIMFJ(5) - EL(4) + ZVEC(3) * STIMFJ(6)
64 CALL LODFEC(3, DELTA(3), SIGMA(1,3), SDELTA(3), SDELTD(3))
65 DEE(1) = EL(1) * (PN(2) * STIMFJ(2) + PN(3) * STIMFJ(3))
66 DEE(2) = MPN(2) * STIMFJ(4) + EL(2) * PN(3) * STIMFJ(5)
67 DEE(3) = EL(4) * PN(3) * STIMFJ(6)
68 DEE(9) = DEE(9) - PN(2) * CPMI(2) - PN(3) * CPMI(3)
69 DEE(10) = DEE(10) - PN(2) * SPMI(2) - PN(3) * SPMI(3)
70 IF (NBELT - 3) 30, 20, 20
71 TS = X(1) + ELAMB(1)
72 TSA = Y(1) + ELAMB(2)
73 TSB = SORT(TS*TS + TSA*TSA - RM*RM)
74 BL(1) = TSB
75 PHI(1) = ATAN2(TSA, TSI) + ATAN(RH/TSB)
76 CPMI(1) = COS(PHI(1))
77 SPMI(1) = SIN(PHI(1))
78 STIMFJ(1) = SIN(ZVEC(1) - PHI(1))
79 SDELTD(1) = X(1) + CPMI(1) * Y(1) + SPMI(1) * RM + ZVEC(1)
80 CALL LODFEC(1, DELTA(1), SIGMA(1,1), SDELTA(1), SDELTD(1))
81 DEE(1) = DEE(1) + RM * PN(1)
82 DEE(9) = DEE(9) - PN(1) * CPMI(1)
83 DEE(10) = DEE(10) - PN(1) * SPMI(1)
84 RETURN
85 END

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*2D20570
*2D20580
*2D20590
*2D20600
*2D20610
*2D20620
*2D20630
*2D20640
*2D20650
*2D20660
*2D20670
*2D20680
*2D20690
*2D20700
*2D20710
*2D20720
*2D20730
*2D20740
*2D20750
*2D20760
*2D20770
*2D20780
*2D20790
*2D20800
*2D20810
*2D20820
*2D20830
*2D20840
*2D20850
*2D20860
*2D20870
*2D20880
*2D20890
*2D20900
*2D20910
*2D20920

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30

Subroutine BELT (page 2 of 2)

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1                                     *2D20930
2 SUBROUTINE BODY                       *2D20940
3 COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,BBB,IGNORE,DA,XSMALA,YSMAL *2D20950
4 IA,XISMLA,PSIA,SPSIA,CPSIA,FMUA,SIGMAA,SIGMA,AA,KTABLE,MFORI,DTR,PI *2D20967
5 2TWO,GRAVIT,CPRIME,BIGKI,EL,AR,TPRIME,ALFAI,OMEGAI,RPSI,RHO,THETAZ,*2D20970
6 3STHETZ,CTHETZ,FSPRM,RH,THATPV,WZERO,RHOPTZ,RHOPFZ,GAMZER,LCONTL,CS*2D20980
7 4,S,FMUS,BETA,ZZERO,ELTWTY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NPASGR*2D20990
8 5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,RPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA*2D21000
9 6,ELAMB,TIME,IBUG,MAXR,LITGAM,EPSLNZ,RSEL,RVEL,IBIG,IFORK,BASIC,FS,*2D21010
10 7SMALLF,ZVEC,ZVECP,ZVECPP,THEDSQ,CTHETA,STHETA,          BIGMI,TMATII,*2D21020
11 8XIDOT,YIDOT,PHI,EONE,SDELTA,SDELTD,BL,PN,MODE,OMEGA,X,Y,THEFFE,RH*2D21030
12 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOLD,DELODD,EPSLNY,FTOLD,FSPRMZ *2D21040
13 COMMON CZERON,CONEN,CTWON,ET,EHAT,GEE,SMALLB,AEL,TIMTJZ,TGAMZ,YZZE*2D21050
14 1RO,FSZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,AACCA,*2D21060
15 2BACCB,CACCC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSQLI,ATDSQ,TIMT*2D21070
16 3J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TSA,TSB,SIGMAC,ITAU,TAUHAT,RZ,SZ *2D21080
17                                     *2D21090
18                                     *2D21100
19 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3)*2D2110
20 1),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),BIGKI(7),*2D21120
21 2TPRIME(7),ALFAI(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR(*2D21130
22 3B),RHO(8),THETAZ(8),STHETZ(8),CTHETZ(8),IBIG(8),THEDSQ(8),CTHETA(8)*2D21140
23 4),STHETA(8),          BIGMI(8),TMATII(8),RHOPRM(8),XPRM(8),YPRM(8)*2D21150
24 5,TDSQLI(8),ATDSQ(8),IGNORE(10),DA(10),XSMALA(10),YSMALA(10),XISMLA*2D21160
25 6(10),PSIA(10),CPSIA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),RE*2D21170
26 7E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11)*2D21180
27 8),ZVECPP(11),STIMTJ(13),AEL(14),RSEL(16),RVEL(16),MODE(16),TIMTJZ(*2D21190
28 9)16),TIMTJI(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EONE(18),PN(18) *2D21200
29 DIMENSION DELOLD(18),DELODD(18),EPSLNY(18),FTOLD(18),OMEGA(18),CZE*2D21210
30 1RDN(18),CONEN(18),CTWON(18),ET(18),EHAT(18),IFORK(3,8),SIGMA(10,3)*2D21220
31 2,XXX(300,3),YYY(300,3),FMM(300,3),BBB(300,3),          SIGMAA(10,1)*2D21230
32 30),AA(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,128),BASIC(11,8),KTA*2D21240
33 4LE(2,14),ZPPP(128),BL(3) *2D21250
34                                     *2D21260
35 COMMON THATPW,THATPX,THATPS,XVEHZ *2D21270
36 COMMON FARB(18),SLOPE(18),ISWT(18),LODSWT(18) *2D21280
37 COMMON NONO(1402) *2D21290
38 C SECTIONS 5.2.1 + 5.1 BODY FORCES AND CART ACCELERATION *2D21300
39 5000 DO 5010 I=1,8 *2D21310
40 5010 GEE(I) = GRAVA(I)*CTHETA(I) *2D21320
41 BEE(1) = -EL(1)*(ATDSQ(2)*STIMTJ(1)+ATDSQ(3)*STIMTJ(2)+ATDSQ(4)*ST *2D21330
42 1IMTJ(3)+ATDSQ(5)*STIMTJ(4)+ATDSQ(6)*STIMTJ(5)) *2D21340
43 SINTEN = SIN(TIMTJ(10)) *2D21350
44 BEE(2) = EL(1)*A(2)*THEDSQ(1)*STIMTJ(1)-EL(2)*(ATDSQ(3)*STIMTJ(6)+ *2D21360
45 1ATDSQ(4)*STIMTJ(7)+ATDSQ(5)*STIMTJ(8)+ATDSQ(6)*SINTEN) *2D21370
46 BEE(3) = A(3)*(TDSQLI(1)*STIMTJ(2)+TDSQLI(2)*STIMTJ(6))-EL(3)*ATDSQ(*2D21380
47 14)*STIMTJ(9)-EL(4)*(ATDSQ(5)*STIMTJ(10)+ATDSQ(6)*STIMTJ(11)) *2D21390
48 BEE(4) = A(4)*(TDSQLI(1)*STIMTJ(3)+TDSQLI(2)*STIMTJ(7)+TDSQLI(3)*STI *2D21400
49 1MTJ(9)) *2D21410
50 BEE(5) = A(5)*(TDSQLI(1)*STIMTJ(4)+TDSQLI(2)*STIMTJ(8)+EL(4)*THEDSQ(*2D21420

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51 13)*STIMTJ(I10))-EL(5)*ATDSQ(6)*STIMTJ(I12)
52 BEE(6)=A(6)*(TDSQ(I(1))*STIMTJ(5)+TDSQ(I(3))*STIMTJ(I11))+TDSQ(I(5))*ST
53 1TMTJ(I12)+TDSQ(I(2))*SINTEN)
54 BEE(7) = -ATDSQ(8)*EL(7)*STIMTJ(I13)
55 BEE(8)=TDSQ(I(7))*A(8)*STIMTJ(I13)
56 BEE(9) = 0.
57 BEE(10) = 0.
58 DO 5100 I=1,8
59 BEE(9) = BEE(9) + ATDSQ(I)*C.THETA(I)
60 BEE(10)=BEE(10)+ATCSQ(I)*STHETA(I)
61 DO 5110 I=1,10
62 5110 SMALLB(I)=BEE(I)+CEE(I)+DFE(I)-GEE(I)+QUE(I)
63 5200 IF(I1BUG-2) 5206,5202,5202
64 5202 WRITE(6,9955)(I,GEE(I),DEE(I),BEE(I),SMALLB(I),I=1,10)
65 9955 FORMAT (6HOBODY / (1X15,4E20.8))
66 5206 RETURN
67 END

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*2021470
*2021440
*2021450
*2021460
*2021470
*2021480
*2021490
*2021500
*2021510
*2021520
*2021530
*2021540
*2021550
*2021560
*2021570
*2021580
*2021590

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Subroutine BODY (page 2 of 2)

11-7

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1
2 SUBROUTINE CONTAC *2D15550
3 COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,BBB,IGNORE,DA,XSMALA,YSMAL *2D15560
4 1A,XISMLA,PSIA,SPSIA,CP SIA,FMUA,SIGMAA,SIGMA,AA,KTABLE,MFORI,DTR,PI*2D15570
5 2TWO,GRAVIT,CPRIME,BIGKI,EL,AR,TPRIME,ALFAI,OMEGAI,RPSI,RHO,THETAZ,*2D15580
6 3STHETZ,CTHETZ,FSPRM,RH,THATPV,WZERO,RHOPTZ,RHOPFZ,GAMZER,LCONTL,CS*2D15600
7 4,S,FMUS,BETA,ZZERO,ELTWY,ELTHRY,H,DESTEP,DELTAT,PHIZ,DELTA,NPASGR*2D15610
8 5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,BPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA*2D15620
9 6,ELAMB,TIME,IBUG,MAXR,LITGAM,EPSLNZ,RSEL,RVEL,IBIG,IFORK,BASIC,FS,*2D15630
10 7SMALLF,ZVEC,ZVECP,ZVECPP,THEDSQ,CTHETA,STHETA,BIGMI,TMATII,*2D15640
11 8XIDOT,YIDOT,PHI,EONE,SDELTA,SDELTD,BL,PN,MODE,OMEGA,X,Y,THEFEE,RH*2D15650
12 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOLD,DELDD,EP SLNY,FTOLD,FSPRMZ *2D15660
13 COMMON CZERON,CCNEN,CTWON,ET,EHAT,GEE,SMALLB,AEL,TIMTJZ,TGAMZ,YZZE*2D15670
14 1RO,F SZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVEL,BVEL,CVEL,C,AACCA,*2D15680
15 2BACCB,CACCC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSQLI,ATDSQ,TIMT*2D15690
16 3J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TSA,TSB,SIGMAC,ITAU,TAUHAT,RZ,SZ *2D15700
17 *2D15710
18 *2D15720
19 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3)*2D15730
20 1),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),BIGKI(7),*2D15740
21 2TPRIME(7),ALFAI(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR(*2D15750
22 3),RHO(8),THETAZ(8),STHETZ(8),CTHETZ(8),IBIG(8),THEDSQ(8),CTHETA(8)*2D15760
23 4),STHETA(8),BIGMI(8),TMATII(8),RHOPRM(8),XPRM(8),YPRM(8)*2D15770
24 5,TDSQLI(8),ATDSQ(8),IGNORE(10),DA(10),XSMALA(10),YSMALA(10),XISMLA*2D15780
25 6(10),PSIA(10),SPSIA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),BE*2D15790
26 7E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11)*2D15800
27 8),ZVECPP(11),STIMTJ(13),AEL(14),RSEL(15),RVEL(16),MODE(16),TIMTJZ(*2D15810
28 916),TIMTJI(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EONE(18),PN(18) *2D15820
29 DIMENSION DELOLD(18),DELDD(18),EP SLNY(18),FTOLD(18),OMEGA(18),CZE*2D15830
30 1RON(18),CONEN(18),CTWON(18),ET(18),EHAT(18),IFORK(3,8),SIGMA(10,3)*2D15840
31 2,XXX(300,3),YYY(300,3),FMM(300,3),BBB(300,3),SIGMAA(10,1)*2D15850
32 3),AA(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,128),BASIC(11,8),KTAB*2D15860
33 4LE(2,14),ZPPP(128),BL(3) *2D15870
34 *2D15880
35 COMMON THATPV,THATPX,THATPS,XVEHZ *2D15890
36 COMMON FARB(18),SLOPE(18),ISWT(18),LODSWT(18) *2D15900
37 COMMON NONO(1402) *2D15910
38 DIMENSION JFORK(8),ELP(5) *2D15920
39 JNN=MAXR-8 *2D15930
40 MAXR=8 *2D15940
41 INN = 1 *2D15950
42 FUDGE=.1 *2D15960
43 DO 20 I=1,8 *2D15970
44 RVEL(I+8) = 0. *2D15980
45 IFORK(1,I) = 0 *2D15990
46 IFORK(2,I) = 0 *2D16000
47 JFORK(I) = IFORK(3,I) *2D16010
48 IFORK(3,I) = 0 *2D16020
49 QUE(I) = 0. *2D16030
50 DO 10 II=1,11 *2D16040
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51 10 BASIC(I,I,I) = 0.
52 20 CONTINUE
53  QUE(9) = 0.
54  QUE(10) = 0.
55  DO 430 N=5,NS
56  IA = KTABLE(2,N-4)
57  IF (IGNORE(IA)) 25,25,430
58  I = KTABLE(1,N-4)
59  TSA = RHOPRM(I)*STHETA(I)
60  TSB = RHOPRM(I)*CTHETA(I)
61  GO TO (30,430,30,30,30,430,40,50),I
62  XPRM(I) = X(I) + TSB
63  YPRM(I) = Y(I) + TSA
64  TSA = XIDOT(I) - TSA*ZVECP(I)
65  TSB = YIDOT(I) + TSB*ZVECP(I)
66  GO TO 70
67  XPRM(I) = X(I) + TSB
68  YPRM(I) = Y(I) + TSA
69  TSA = XIDOT(I) - TSA*ZVECP(I)
70  TSB = YIDOT(I) + TSB*ZVECP(I)
71  GO TO 70
72  XPRM(I) = X(I-1) + TSB
73  YPRM(I) = Y(I-1) + TSA
74  TSA = XIDOT(I-1) - TSA*ZVECP(I)
75  TSB = YIDOT(I-1) + TSB*ZVECP(I)
76 70 DELIAD = TSA*SPSIA(IA) - TSB*CPSIA(IA)
77  VTI A = TSA*CPSIA(IA) + TSB*SPSIA(IA) + AR(I)*ZVECP(I)
78  TSA = XSMALAI(IA) - XPRM(I)
79  TSB = YSMALAI(IA) - YPRM(I)
80  DELIA = AR(I) - TSA*SPSIA(IA) + TSB*CPSIA(IA)
81  TIA = TSA*CPSIA(IA) + TSB*SPSIA(IA)
82  IF (DELIA+FUDGE) 300,300,80
83  IF (IGNORE(IA)) 100,90,90
84  MAXR = MAXR+1
85  INN = MAXR-8
86  RVEL(MAXR) = VTI A
87  APSI(MAXR) = XISMLA(IA)
88  IFORK(1,INN) = I
89  IFORK(2,INN) = IA
90  IFORK(3,INN) = N
91 100 IF (TIA) 150,150,110
92 110 IF (TIA-DALIA) 120,120,150
93 120 IF (DELIA) 200,200,130
94 130 CALL LODFEC(N,0,SIGMA(1,IA),DELIA,DELIAD)
95 95 IF (IGNORE(IA)) 135,140,140
96 135 INN = INN + 1
97  GO TO 390
98 140 IF (PN(N)) 150,150,310
99 150 IFORK(1,INN) = 0
100 100 IFORK(2,INN) = 0

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Subroutine CONTACT (page 2 of 4)

101	IFORK(3, INN) = 0	*2D16550
102	IF (JFORK(INN)) 160,190,160	*2D16560
103	160 DO 170 JJ=INN,7	*2D16570
104	170 JFORK(JJ) = JFORK(JJ+1)	*2D16580
105	DO 180 JK=MAXR,15	*2D16590
106	180 MODE(JK)=MODE(JK+1)	*2D16600
107	190 MAXR = MAXR-1	*2D16610
108	GO TO 300	*2D16620
109	200 IF (IGNORE(IA)) 300,210,210	*2D16630
110	210 IF (IFORK(3, INN)-JFORK(INN)) 220,300,220	*2D16640
111	220 DO 230 JJ=INN,7	*2D16650
112	JK=MAXR-JJ-1	*2D16660
113	230 JFORK(JK+1) = JFORK(JK)	*2D16670
114	JL=16-MAXR	*2D16680
115	DO 240 JJ=1,JL	*2D16690
116	JK=16-JJ	*2D16700
117	240 MODE(JK+1) = MODE(JK)	*2D16710
118	250 IF (ABS(RVEL(MAXR))-RPSI(MAXR)) 260,270,280	*2D16720
119	260 MODE(MAXR) = -1	*2D16730
120	GO TO 300	*2D16740
121	270 MODE(MAXR) = 0	*2D16750
122	GO TO 300	*2D16760
123	280 MODE(MAXR) = 1	*2D16770
124	300 PN(N)=0.	*2D16780
125	EQNE(N) = 0.	*2D16790
126	GO TO 400	*2D16800
127	310 IF (IFORK(3, INN)-JFORK(INN)) 320,390,320	*2D16810
128	320 DO 330 JJ=INN,7	*2D16820
129	JK=MAXR-JJ-1	*2D16830
130	330 JFORK(JK+1) = JFORK(JK)	*2D16840
131	JL=16-MAXR	*2D16850
132	DO 340 JJ=1,JL	*2D16860
133	JK=16-JJ	*2D16870
134	340 MODE(JK+1) = MODE(JK)	*2D16880
135	350 IF (ABS(RVEL(MAXR))-RPSI(MAXR)) 360,370,380	*2D16890
136	360 MODE(MAXR) = -1	*2D16900
137	GO TO 390	*2D16910
138	370 MODE(MAXR) = 0	*2D16920
139	GO TO 390	*2D16930
140	380 MODE(MAXR) = 1	*2D16940
141	390 BASIC(11, INN) = 0.	*2D16950
142	GO TO (399,399,391,392,393,399,396,395),1	*2D16960
143	391 ELP(3) = RHOP TZ	*2D16970
144	GO TO 394	*2D16980
145	392 ELP(4) = RHOP FZ	*2D16990
146	ELP(3) = EL(3)	*2D17000
147	GO TO 394	*2D17010
148	393 ELP(5) = EL(5)	*2D17020
149	ELP(4) = 0.	*2D17030
150	ELP(3) = EL(4)	*2D17040

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394  ELP(2) = EL(2)
      ELP(1) = EL(1)
      KK = 0
      GO TO 397
395  ELP(2) = EL(9)
396  ELP(1) = EL(7)
      KK = 5
397  JJ = I-KK
      DO 398 J=1, JJ
      JK = J+KK
      TS = PSIA(IA)-ZVEC(JK)
      BASIC(J, INN) = ELP(J)*SIN(TS)
      BASIC(J+5, INN) = ELP(J)*COS(TS)
      BASIC(11, INN) = BASIC(11, INN) - BASIC(J+5, INN)*THE(S, J, JK)
      QUELJK = QUE(JK) + PN(N)*BASIC(J+5, INN)
      BASIC(JJ, INN) = BASIC(JJ, INN) + AR(I)
398  QUE(9) = QUE(9) - PN(N)*SPSIA(TA)
399  QUE(10) = QUE(10) + PN(N)*CPSIA(TA)
400  IF (IBUG-2) 430, 410, 410
410  WRITE(6, 9598) N, DELIA, DELIAD, PN(N), EDPN(N), EPSLVY(1)
9598  FORMAT (84 CONTACTS, 5E22, 8)
430  CONTINUE
440  IF (IBUG-2) 450, 440, 440
450  WRITE(6, 9999) QUE
9999  FORMAT (11) HOQUE VECTOR / (5F20.8)
450  RETURN
      END

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*2017050
*2017063
*2017070
*2017080
*2017090
*2017100
*2017110
*2017120
*2017130
*2017140
*2017150
*2017160
*2017170
*2017180
*2017190
*2017200
*2017210
*2017220
*2017230
*2017240
*2017250
*2017260
*2017270
*2017280
*2017290
*2017300
*2017310

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1  
2  
3 C  
4 SUBROUTINE DATE(IA)  
5 DUMMY DATE ROUTINE  
6 DIMENSION IA(3)  
7 DATA IB/1H /  
8 IA(1)=IB  
9 IA(2)=IB  
10 IA(3)=IB  
RETURN  
END
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*2039460  
*2039470  
*2039480  
*2039490  
*2039500  
*2039510  
*2039520  
*2039530  
*2039540  
*2039550
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Subroutine DATE

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1 SUBROUTINE DELZMK(KK)
2 COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,BBR,IGNOR,F,DA,XSMALA,YSMAL,*2017320
3 *2017330
4 IA,XISMLA,PSIA,SPSIA,CPSTA,FMUA,SIGMAA,SIGMAAA,KTABLE,4FORI,OTR,PI*2017340
5 2TMO,GRAVIT,CPRTIME,BIGKI,EL,AR,TPRIME,ALFAI,OMEGAI,RPSI,RHD,THEFAZ,*2017350
6 3STHETZ,CTHETZ,FSPRM,RH,THATPX,WZER,PHOPFZ,PHAMZER,LCNTL,CS*2017370
7 4,S,FMUS,BETA,ZZERO,ELTWTY,ELTHRY,1,DESTEP,DELTA,PHIZ,DELTA,NPASGR*2017380
8 5,XPACZ,NBELT,APRND,TIMEAX,DTPRINT,IBRNT,GR,MS,SIGZ,FLZTEN,A,GRAVA*2017390
9 6,ELAMB,TIME,IBUC,MAXR,LITGAM,EPSLVZ,RSEL,RVEL,IBIG,IFORK,BASIG,FS,*2017400
10 7SMALLF,ZVEC,ZVECP,ZVEDCP,THEDSQ,CTHETA,STHETA, RIGMI,TMATII,*2017410
11 8XIDOT,YIDOT,PHI,SEONE,SDELTA,SDELTO,BL,PN,MODE,OMEGA,X,Y,THEFEE,RH*2017420
12 SUPRM,XPRM,YPRM,BEE,CEE,DEE,OUF,DELDOD,DELDDOD,EPSINY,FTOLO,FSPRMZ *2017430
13 COMMON CZERON,CNEN,CTMON,ET,EHAT,SEE,SMALLB,AEI,TIMEJZ,TCAMZ,YZZE*2017440
14 IRO,FZCNS,ANVERS,ATINFL,KPOST,TPRINT,TSTEP,AVELA,HVELB,CVELC,AACA,*2017450
15 2BACCR,CACCG,DACCG,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TOSQLI,ATDSQ,TIMT*2017460
16 3J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TSA,TSB,SIGMAC,ITAU,TAUHAT,RZ,SZ *2017470
17 *2017480
18 *2017490
19 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),RFTA(3),PHIZ(3),DELTA(3)*2017500
20 1),PHI(3),SDELTA(3),SDELTO(3),ELAMB(5),WJRI(7),CPPIME(7),RIGKI(7),*2017510
21 2TPRIME(7),ALFAI(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),FL(R),AP(*2017520
22 3R),RHD(8),THEFAZ(8),STHETZ(8),CTHETZ(R),IBIG(8),THEDSQ(8),CTHETA(8)*2017530
23 4),STHETA(8), RIGMI(8),TMATII(8),RHOPRM(8),XPRM(8),YPRM(8)*2017540
24 5,ATDSQI(8),ATDSQI(9),IGNORE(10),DAI(10),XSMALA(10),YSMALA(10),XISMLA*2017550
25 6(10),PSTAI(10),CPSTA(10),SPSTA(10),SIGMAC(10),FMUA(10),GRAVA(10),RE*2017560
26 7E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11)*2017570
27 8),ZVECP(11),STIMTJ(13),AEI(14),RSEL(16),RVEL(16),MODE(16),TIMEJZ(*2017580
28 916),TIMEJ(16),RPSI(16),A(17),G(18),P(18),SIGZ(18),EONE(18),PN(18)*2017590
29 DIMENSION DELOLD(18),DELDOD(18),EPSINY(18),FTOLO(18),OMEGAI(18),CZE*2017600
30 IRO(18),CNEN(18),CTMON(18),ET(18),EHAT(18),IFORK(3,8),SIGMAA(10,3)*2017610
31 2,XXX(300,3),YYY(300,3),FMM(300,3),RRR(300,3), SIGMAA(10,1)*2017620
32 30),AA(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,128),BASIC(11,8),KTAR*2017630
33 4LE(2,14),ZPPP(128),BL(3) *2017640
34 *2017650
35 COMMON THATPX,THATPY,THATPS,XVEHZ
36 COMMON FARBI(8),SLOPE(18),ISWT(18),LONDSWT(18)
37 COMMON NONO(1402)
38 K=KK
39 IF (K-8) 10,320,370
40 GO TO (20,50,80,110,140,190,240),K
41 IF (RVEL(1)) 40,290,30
42 IF (TIMEJ(6)-GE-ALFAI(1)) GO TO 290
43 TMATII(1)=TPRIME(1)*(ALFAI(1)-TIMEJ(6))
44 GO TO 300
45 IF (TIMEJ(6)-LE-OMEGAI(1)) GO TO 290
46 TMATII(1)=THATPX*(OMEGAI(1)-TIMEJ(6))
47 GO TO 300
48 IF (ABS(TIMEJ(1))-CMEGAI(2)) 290,290,60
49 60 IF (RVEL(2)*TIMEJ(1)) 290,70,70
50 70 TMATII(2)=TPRIME(2)*(TIMEJ(1)-SIGN(OMEGAI(2),TIMEJ(1)))

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Subroutine DELZMK (page 1 of 3)

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51      GO TO 300
52      IF (ABS(TIMTJ(7))-OMEGAI(3)) 290,290,90
53      IF (RVEL(3)*TIMTJ(7)) 290,100,100
54      TMAII(3)=TPRIME(3)*(TIMTJ(7)-SIGN(OMEGAI(3),TIMTJ(7)))
55      GO TO 300
56      IF (ABS(TIMTJ(11))-CMEGAI(4)) 290,290,120
57      IF (RVEL(4)*TIMTJ(11)) 290,130,130
58      TMAII(4)=TPRIME(4)*(TIMTJ(11)-SIGN(OMEGAI(4),TIMTJ(11)))
59      GO TO 300
60      IF (RVEL(5)) 170,290,150
61      IF (TIMTJ(12)-OMEGAI(5)) 290,290,160
62      TMAII(5)=THATPV*(TIMTJ(12)-OMEGAI(5))
63      GO TO 300
64      IF (TIMTJ(12)-ALFAI(5)) 180,290,290
65      TMAII(5)=TPRIME(5)*(TIMTJ(12)-ALFAI(5))
66      GO TO 300
67      IF (RVEL(6)) 210,290,200
68      IF (TIMTJ(15)+ALFAI(6).LE.0.) GO TO 290
69      TMAII(6)=TPRIME(6)*(TIMTJ(15)+ALFAI(6))
70      GO TO 300
71      IF (TIMTJ(15)+OMEGAI(6).GE.0.) GO TO 290
72      TMAII(6)=THATPX*(TIMTJ(15)+OMEGAI(6))
73      GO TO 300
74      IF (RVEL(7)) 260,290,250
75      IF (TIMTJ(16).GE.ALFAI(7)) GO TO 290
76      TMAII(7)=TPRIME(7)*(ALFAI(7)-TIMTJ(16))
77      GO TO 300
78      IF (TIMTJ(16)-LE.OMEGAI(7)) GO TO 290
79      TMAII(7)=THATPS*(OMEGAI(7)-TIMTJ(16))
80      GO TO 300
81      TMAII(K)=0.
82      M = MFOR(K)
83      TS=TMAII(K)*SIGN(CPRIME(K),RVEL(K))
84      DO 310 J=1,10
85      DELZ(J,K)=(ANVERS(J,K)-ANVERS(J,M))*TS
86      GO TO 900
87      TS = -SIGN(SMALLF,RVEL(8))
88      DO 330 J=1,10
89      DELZ(J,8) = ANVERS(J,9)*TS
90      GO TO 900
91      N = IFORK(3,K-8)
92      IA = IFORK(2,K-8)
93      II = IFORK(1,K-8)
94      IF (IBUG) 375,375,373
95      J=IA-1
96      WRITE(6,9958)K,II,J
97      FORMAT(13HOFOR MODE NO.15,4H, I=15,4H, A=15)
98      TSA=FMUA(IA)*PN(N)
99      TS = -SIGN(TSA,RVEL(K))
100     GO TO (380,900,400,420,420,900,460,480),II

```

```

*2D17820
*2D17830
*2D17840
*2D17850
*2D17860
*2D17870
*2D17880
*2D17890
*2D17900
*2D17910
*2D17920
*2D17930
*2D17940
*2D17950
*2D17960
*2D17970
*2D17980
*2D17990
*2D18000
*2D18010
*2D18020
*2D18030
*2D18040
*2D18050
*2D18060
*2D18070
*2D18080
*2D18090
*2D18100
*2D18110
*2D18120
*2D18130
*2D18140
*2D18150
*2D18160
*2D18170
*2D18180
*2D18190
*2D18200
*2D18210
*2D18220
*2D18230
*2D18240
*2D18250
*2D18260
*2D18270
*2D18280
*2D18290
*2D18300
*2D18310

```

```

101 DO 390 J=1,10
102 DELZ(J,K)=(AR(1)*ANVERS(J,1)+CPSIA(2)*ANVERS(J,9)+SPSIA(2)*ANVERS(
103 LJ,10))*TS
104 CONTINUE
105 GO TO 900
106 DO 410 J=1,10
107 DELZ(J,K)=(ANVERS(J,1)*BASIC(1,K-8)+ANVERS(J,2)*BASIC(2,K-8)
108 1+ANVERS(J,3)*BASIC(3,K-8)+ANVERS(J,9)*CPSIA(1A)+ANVERS(J,10)
109 2*SPSIA(1A))*TS
110 CONTINUE
111 GO TO 900
112 DO 430 J=1,10
113 DELZ(J,K)=(ANVERS(J,1)*BASIC(1,K-8)+ANVERS(J,2)*BASIC(2,K-9)
114 1+ANVERS(J,3)*BASIC(3,K-8)+ANVERS(J,9)*CPSIA(1A)+ANVERS(J,10)
115 2*SPSIA(1A)+ANVERS(J,11)*BASIC(11,K-9))*TS
116 CONTINUE
117 GO TO 900
118 DO 470 J=1,10
119 DELZ(J,K)=(ANVERS(J,7)*BASIC(1,K-4)+ANVERS(J,9)*CPSIA(1A)
120 1+ANVERS(J,10)*SPSIA(1A))*TS
121 CONTINUE
122 GO TO 900
123 DO 490 J=1,10
124 DELZ(J,K)=(ANVERS(J,7)*BASIC(1,K-8)+ANVERS(J,8)*BASIC(2,K-8)
125 1+ANVERS(J,10)*SPSIA(1A)+ANVERS(J,9)*CPSIA(1A))*TS
126 CONTINUE
127 900 IF (IBUG-1) 920,51C,910
128 910 WRITE(6,9999JK,(DELZ(J,K),J=1,10)
129 5595 FORMAT (8HDELZMK I10,3X5F20.6/21X5E20.6)
130 920 RETURN
131 END

```

```

*2018320
*2018330
*2018340
*2018350
*2018360
*2018370
*2018380
*2018390
*2018400
*2018410
*2018420
*2018430
*2018440
*2018450
*2018460
*2018470
*2018480
*2018490
*2018500
*2018510
*2018520
*2018530
*2018540
*2018550
*2018560
*2018570
*2018580
*2018590
*2018600
*2018610
*2018620

```

Subroutine DELZMK (page 3 of 3)


```
1      SUBROUTINE ERROR
2      OS DUMMY ERROR ROUTINE
3      PRINT 9999
4      FORMAT(13H0ERROR RETURN/IHI)
5      I=0
6      IF(I) 20,10,20
7      STOP
8      RETURN
9      END
10
```

```
*2039360
*2039370
*2039380
*2039390
*2039400
*2039410
*2039420
*2039430
*2039440
*2039450
```

Subroutine ERROR

```

1 SURROUTINE FECLUD( II,S,I,SDL,SOL,C,FTT)
2 COMMON SWITCH,NEW,MAX,IP,ST,XXX,YY,FMV,TRR,IGNORE,DA,XSMALA,YSMAL,*2D25190
3 1A,XISMALA,PSIA,SPSIA,CPSIA,PMUA,SJMAA,SIPMA,AA,KTABLE,MEORI,OTR,PI*2D25200
4 2TMO,GRAVIT,CPRIME,FIK,I,EL,AR,TPRIME,ALCAI,OME,AI,RMT,TFETAZ,*2D25210
5 3STHETZ,CTHETAZ,FSPRM,RH,THATPV,WZER(C,F,CP,IZ,RH)PFZ,GAMZ,FR,LCONTL,CS*2D25220
6 4,S,FMJ,S,BETA,ZER0,ELTWTY,ELHTY,PH,DEFSTEP,DELTA,PHIZ,DELTA,NPASGP*2D25230
7 5,XPACZ,NBELT,APRNTD,TTMAX,DTPRNT,APRNTD,AS,R,NS,SIRZ,ELZTEN,A,GRAVA*2D25240
8 6,ELAMB,TIME,IBUG,MAXR,LIT,AM,EPSLNZ,RSEL,PVEL,IRIG,IFDRK,BASIC,FS,*2D25250
9 7SMALLF,ZVEC,ZVECP,ZVEDPP,THEDSQ,CTHETA,STHETA, RIGMT,IMATII,*2D25260
10 8XIDOT,YIDJT,PHI,LEONE,SDELTA,SDELTA,DELTA,BL,PN,MODE,OMEGA,X,Y,THEFEE,RH*2D25270
11 9OPRM,XPRM,YPRM,BEE,CEF,DEE,QUE,DELDD,DELDD,EP,SLNY,FTOLD,FSPRMZ *2D25280
12 10COMMON CZERON,CNEN,CTMON,ET,EHAT,SEE,SMALLB,AEAL,TTMTJZ,TGAM7,YZZF*2D25290
13 11RO,FZCNS,ANVER,S,ATNLF,KPUS,TPRINT,KSSTEP,KINEL,TTMASK,TDSQL1,ATDSC,TTMT*2D25300
14 12BACCG,CACCG,DACCG,MAXI,KPRINT,KSSTEP,KINEL,TTMASK,TDSQL1,ATDSC,TTMT*2D25310
15 13J,STMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TSA,TSR,SIGMAC,ITAU,TAUHAT,RZ,SZ *2D25320
16 17 *2D25330
18 *2D25340
19 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3)*2D25350
20 1)PHI(3),SDELTA(3),SDELTA(3),ELAM,(6),MCPPI(7),CPRIME(7),BIGKI(7),*2D25360
21 2)PRIME(7),ALFAI(7),OMEGA(7),XIDOT(7),YIDOT(7),X(7),Y(7),FL(8),AR(*2D25370
22 3)RHO(8),THETAZ(8),STHETZ(8),CTHETZ(8),TRIG(9),THEDSJ(8),CTHETA(8)*2D25380
23 4),STHETA(9), RIGMT(8),TMATII(8),KHOPM(8),XPRM(8),YPRM(8)*2D25390
24 5,TDSQLI(8),ATDSQL(8),IGNORE(10),CAL(10),XSMALA(10),YSMALA(10),GRAVA(10),RE*2D25400
25 6(10),PSIA(10),CPSIA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),RE*2D25410
26 7E(10),CEE(10),QUE(10),DEF(10),GFE(10),SMALLB(10),KVEL(16),MODE(16),TIMTJZ(*2D25420
27 8),ZVECP(11),STMTJ(13),AFL(14),RSL(16),KVEL(16),MODE(16),TIMTJZ(*2D25430
28 9)16),TIMTJ(16),RPSI(16),A(17),G(18),P(18),SIGZ(18),FONE(18),PN(18)*2D25440
29 DIMENSION DELOLC(14),DELJDD(18),EP,SLNY(18),FTOLD(18),OMEGA(18),CZE*2D25450
30 IRON(18),CNEN(18),CTMON(18),ET(18),EHAT(18),IFURK(3,8),SIGMA(10,3)*2D25460
31 2,XXX(300,3),YYY(300,3),FMM(300,3),RHB(300,3), SIGMAA(10,1)*2D25470
32 30),AA(10,10),ANVER(10,10),DELZ(11,16),ZK(11,128),HASIC(11,8),KTA8*2D25480
33 4LE(2,14),ZPPP(128),RL(3) *2D25490
34 *2D25500
35 *2D25510
36 *2D25520
37 *2D25530
38 *2D25540
39 *2D25550
40 *2D25560
41 *2D25570
42 *2D25580
43 *2D25590
44 *2D25600
45 *2D25610
46 *2D25620
47 *2D25630
48 *2D25640
49 *2D25650
50 *2D25660

```

Subroutine FECLUD (page 1 of 3)

```

51      CO = CZERON(INDEX)
52      C1 = CONEN(INDEX)
53      C2 = CTWYN(INDEX)
54      SAGXX = SIGZ(INDEX)
55      OMSGE = 1. - GNEW
56      GOMG = OMEGA(INDEX)
57      IF (OMGT) 240,240,110
58      IF (SDELD) 250,120,120
59      IF (OLDELD) 130,215,215
60      IF (FT) 140,140,150
61      YEPSLN = YEPSLN + GOMG
62      GO TO 210
63      DO 160 I=1,5
64      J=6-I
65      COE(I) = SIG(J)
66      COE(6) = SAGXX - FT
67      KKK = 5
68      CALL MULLER(COE, KKK, ROOTR, ROOT I)
69      RTM = 1.E20
70      DO 200 I=1, KKK
71      TS = DELOLD(INDEX) - YEPSLN - ROOTR(I)
72      IF (TS) 200,170,170
73      IF (TS - UMG) 180,180,200
74      IF (RTM - ABS(ROOTR(I))) 200,200,190
75      EPSLNP = TS
76      RTM = ABS(ROOTR(I))
77      CONTINUE
78      YEPSLN = YEPSLN + EPSLNP
79      UMG = SDEL - YEPSLN
80      OLDELD = 1.
81      GO TO 100
82      IF (DELOLD(INDEX) - YEPSLN) 218,218,220
83      SAGXX = (((SIG(10))*SDELD+SIG(9))*SDELD+SIG(8))*SDELD+SIG(7))*
84      SDELD+SIG(6))*SDELD
85      IF (ISWT(INDEX).EQ.0) GO TO 225
86      FTT=FARB(N)
87      GO TO 230
88      FTT=(((SIG(5))*OMGT+SIG(6))*OMGT+SIG(3))*OMGT+SIG(2))*OMGT+SIG(1))*
89      1*OMGT+SAGXX+(((SIG(10))*SDELD+SIG(9))*SDELD+SIG(8))*SDELD+SIG(7))*
90      2*SDELD+SIG(6))*SDELD
91      IF (FTT.LT.0.) FTT=0.
92      IF (TBUG) 233,236,233
93      WRITE(6,9999) TIME, INDEX, SDEL, SDELD, FTT
94      5999 FORMAT (8H FECLD F20.6,110,3E20.8)
95      RETURN
96      FTT = 0.
97      GO TO 230
98      IF (OLDELD) 260,290,290
99      IF (OMGT - GOMG) 240,240,410
100     FOM=AMAX1(SDEL,DELOLD(INDEX)) - YEPSLN

```

```

*2D25670
*2D25680
*2D25690
*2D25700
*2D25710
*2D25720
*2D25730
*2D25740
*2D25750
*2D25760
*2D25770
*2D25780
*2D25790
*2D25800
*2D25810
*2D25820
*2D25830
*2D25840
*2D25850
*2D25860
*2D25870
*2D25880
*2D25890
*2D25900
*2D25910
*2D25920
*2D25930
*2D25940
*2D25950
*2D25960
*2D25970
*2D25980
*2D25990
*2D26000
*2D26010
*2D26020
*2D26030
*2D26040
*2D26050
*2D26060
*2D26070
*2D26080
*2D26090
*2D26100
*2D26110
*2D26120
*2D26130
*2D26140
*2D26150
*2D26160

```

```

101 IF (TS*1(INDEX),EO,0) GO TO 295
102 C0=FARB(N)-SLOPE(N)*FOM
103 C1=SLOPE(N)
104 C2=0.
105 GO TO 410
106 COMG=GNEW*FOM
107 EO = EONE(INDEX)
108 IF (EO*EO,0.) GO TO 420
109 TS = FT*(FCM-GJMG)
110 IF (2.*EO-TS) 340,320,310
111 EO = .5*TS
112 C0 = -GNEW/OMSGE*FT
113 C1=FT/FOM/OMSGE
114 C2=0.
115 GO TO 410
116 IF (3.*EO-TS) 350,380,400
117 RNEW = RNEW/EO*TS/3.
118 IF (RNEW-1.) 360,370,370
119 EO = TS/3.
120 GO TO 380
121 GNEW = 1.-3./FOM*EO/FT
122 OMSGE=1.-GNEW
123 C0 = GNEW/OMSGE*GNEW/OMSGE*FT
124 C1 = -2./FOM*GNEW/OMSGE*FT/OMSGE
125 C2=FT/FOM/FOM/OMSGE/OMSGE
126 GO TO 410
127 TSR = FOM*OMSGE*OMSGE*CFPSGE
128 C0 = GNEW*(TS*(2.+GNEW))-6.*EO)/TSR
129 TSB = TSB*FOM
130 C1 = 2.*(3.*EO*(1.+GNEW)-TS*(1.+GNEW*GNEW))/TSR
131 C2 = 3./FOM*(TS-2.*EO)/TSB
132 FTT = (C2*CMGT+C1)*OMGT +C0
133 IF (FTT) 240,230,230
134 420 PRINT 9998,TIME,INDEX
135 9998 FORMAT (8HDAT TIME,F8.6,38H FORCE COMING ON FROM BEHIND FOR INDEX
136 1,13)
137 PRINT 9997
138 9997 FORMAT (1H1)
139 CALL SUMMARY
140 CALL ERROR
141 END

```

```

*2D26170
*2D26180
*2D26190
*2D26200
*2D26210
*2D26220
*2D26230
*2D26240
*2D26250
*2D26260
*2D26270
*2D26280
*2D26290
*2D26300
*2D26310
*2D26320
*2D26330
*2D26340
*2D26350
*2D26360
*2D26370
*2D26380
*2D26390
*2D26400
*2D26410
*2D26420
*2D26430
*2D26440
*2D26450
*2D26460
*2D26470
*2D26480
*2D26490
*2D26500
*2D26510
*2D26520
*2D26530
*2D26540
*2D26550
*2D26560
*2D26570

```

```

1 SUBROUTINE GETY(XX,ITABL,ORD)
2
3 COMMON SWITCH,MAX,IPOST,XXX,YYY,FMM,BBB,IGNORF,DA,XSMALA,YSMAL,*2D10500
4 1A,XISMLA,PSIA,SPSIA,CPSIA,FMUA,SIGMAA,SIGMA,AA,KTABLE,MFORI,DTR,PI,*2D10520
5 2TWO,GRAVIT,CPRIME,BIGI,EL,AR,CPRIME,ALFA,OMEGA,RSI,RHD,THEFAZ,*2D10530
6 3STHEZ,CHEZT,FSPRM,RH,THATP,WZRO,RHOPTZ,GAMZER,LCONTL,CS,*2D10540
7 4,S,FMS,BETA,ZZERO,ELTMY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NPASGR,*2D10550
8 5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,BPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA,*2D10570
9 6,ELAMB,TIME,IBUG,MAXR,LITGAM,EPSLN,RSEL,RVEL,IBIG,IFORK,BASIC,FS,*2D10580
10 7SMALLF,ZVEC,ZVECP,ZVECP,THEDSQ,CTHETA,STHETA,BIGMI,TMATII,*2D10590
11 8XIDOT,YIDOT,PHI,EONE,SDELTA,SDELTD,BL,PN,MODE,OMFGA,X,Y,THEFEE,PH,*2D10600
12 9QPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOD,DELOD,EPSLNY,FTOLD,FSPRMZ *2D10610
13 COMMON CZERON,CONEN,CTMON,ET,EHAT,GEE,SMALLB,AFL,TIMTJZ,YGAHZ,YZZF,*2D10620
14 1RO,FZCNS,ANVERS,TINFL,MPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,AACCA,*2D10630
15 2BACCB,CACCC,DACCD,MAXI,MPRINT,KSTEP,KINFL,TIMASK,TOSQLI,ATDSQ,TIMT,*2D10640
16 3J,STIMTJ,DELZ,ZK,ZPPP,TAMATZ,TS,TSB,SIGMAC,ITAU,TAUHAT,RZ,SZ *2D10650
17 *2D10660
18 *2D10670
19 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3)*2D10680
20 1,PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),BIGKI(7),*2D10690
21 2TPRIME(7),ALFAT(7),OMEGA(7),XIDOT(7),YIDOT(7),Y(7),Y(7),EL(R),AR,*2D10700
22 3RHO(8),THEFAZ(8),STHEZ(8),CTHEZ(8),IBIG(8),THEDSQ(8),CTHETA(R)*2D10710
23 4),STHETA(8),BIGMI(8),TMATII(8),RHOPRM(8),XPRM(8),YPRM(8)*2D10720
24 5,TDSQL(8),ATDSQ(8),IGNORE(10),DA(10),XSMALA(10),YSMALA(10),XISMLA,*2D10730
25 6(10),PSIA(10),CPSIA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),BE,*2D10740
26 7E(10),CEE(10),QUE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11)*2D10750
27 8),ZVECP(11),STIMTJ(13),AEL(14),RSEL(16),RVEL(16),MODE(16),TIMTJZ,*2D10760
28 9(16),TIMTJ(16),RPSI(16),AL(17),G(18),R(18),SIGZ(18),EDNE(18),PN(18)*2D10770
29 DIMENSION DELOD(18),DELOD(18),EPSLNY(18),FTOLD(18),OMEGA(18),CZE,*2D10780
30 1RON(18),CONEN(18),CTMON(18),ET(18),EHAT(18),IFORK(3,8),SIGMA(10,3)*2D10790
31 2,XXX(300,3),YYY(300,3),FMM(300,3),RBB(300,3),SIGMAA(10,1)*2D10800
32 30),AA(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,128),BASIC(11,8),KTAB,*2D10810
33 4LE(2,14),ZPPP(128),BL(3) *2D10820
34 *2D10830
35 COMMON THATPW,THATPX,THATPS,XVEHZ
36 COMMON FAR(18),SLOPE(18),ISWT(18),LOADSWT(18)
37 COMMON NNON(1402)
38 TS = XX
39 II = ITABL
40 IMAX = MAX(III)
41 IF (SWITCH(III)) 20,10,70
42 10 ORD = YYY(1,II)
43 GO TO 150
44 20 TS = AMOD(TS,24.)
45 30 IF (IMAX) 40,40,50
46 40 PRINT 9900,II
47 5900 FORMAT (7HOTABLE 14,32H HAS NO ENTRIES AND CALLED UPON.)
48 GO TO 10
49 50 IMIN = MAX(III,IPOST(III))
50 IXSWT=0

```

Subroutine GETY (page 1 of 2)

```

51 IF (IMIN-IMAX) 70,60,60
52 IMIN = 1
53 DO 80 IF IMIN,IMAX
54 JJ = 1
55 IF (XX(I,II)-TS) 80,90,100
56 IXSWT=1
57 PRINT 9901,II,XXX(IMAX,II),TS,YYY(IMAX,II)
58 9901 FORMAT (7H)TABLE I4,7H MAX X=E17.8,17H EXCEEDED BY ARG=E17.8,104,Y*2011070
59 1 SET TO E17.8)
60 ORD = YYY(IMAX,II)
61 GO TO 128
62 ORD = YYY(JJ,II)
63 GO TO 140
64 IF (IXSWT) 130,110,130
65 IF (JJ-1) 60,120,60
66 PRINT 9902,II,XXX(I,II),TS,YYY(I,II)
67 9902 FORMAT (7H)TABLE I4,7H MIN X=E17.8,21H NOT EXCEEDED BY ARG=E17.8,1
68 10H,Y SET TO E17.8)
69 ORD = YYY(I,II)
70 JJ=1
71 GO TO 140
72 JJ=JJ-1
73 ORD = FMM(JJ,II)*TS + BRR(JJ,II)
74 IPDST(II)=JJ
75 IF (IRUG) 160,170,160
76 WRITE(6,9903)XX,TS,II,ORD
77 9903 FORMAT (5H ARG=F8.2,9H,MOD ARG=F8.2,7H, TABLE=I4,5H,ORD=E17.8)
78 RETURN
79 END

```

```

*2011000
*2011010
*2011020
*2011030
*2011040
*2011050
*2011060
*2011070
*2011080
*2011090
*2011100
*2011110
*2011120
*2011130
*2011140
*2011150
*2011160
*2011170
*2011180
*2011190
*2011200
*2011210
*2011220
*2011230
*2011240
*2011250
*2011260
*2011270
*2011280

```

*2028600
*2028610
*2028620
*2028630
*2028640

1
2
3
4
5
INTEGER FUNCTION ITOPOW(JJ)
ITOPW=2**J
RETURN
END

Subroutine ITOPOW

```

1 SUBROUTINE JITTER(ZKR)
2 *2D18630
3 *2D18640
4 COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,RHG,IGNJRE,DA,XSMALA,YSMAL,*2D18650
5 IA,XISMLA,PSIA,SPSIA,CPSTA,FUA,SIGMA,SIGMA,AA,KTALF,MFORI,OTR,PI,*2D18660
6 2TD,GRAVIT,CPRIME,BIGI,EL,AR,TPRIME,ALFA,OMEGA,RHO,THETA,*2D18670
7 3STHETZ,CTHETZ,FSPRM,RH,THATPV,WZPRD,RHTP7,RHDPFZ,SAMZER,LCONTL,CS,*2D18680
8 4,S,FUJ,S,BETA,ZERO,ELTMTY,ELTHRY,M,DESTP,DELTA,PHIZ,DELTA,NPASGR,*2D18690
9 5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,HPRNTD,GR,NS,SIGZ,ELZTEN,A,GRAVA,*2D18700
10 6,ELAMB,TIME,IBUG,MAXR,LITGAM,EPSUNZ,RSEL,RVEL,IBIG,IFDRK,BASIC,FS,*2D18710
11 7SMALLF,ZVEC,ZVECP,ZVEDPP,THEDSO,CTHETA,STHETA,BIGMI,IMATII,*2D18720
12 8XIDOT,YIDJ,PHI,EDNE,SDELTA,SDFLTD,RL,PN,MODE,OMFGA,X,Y,THEFEE,RH,*2D18730
13 SOPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELODD,DELDOO,EPSLNY,FTOLD,FSPRMZ *2D18740
14 COMMON CZERON,CNEN,CTWON,FT,EHAT,CEE,SMALLR,AEI,TMTJZ,TCAMZ,YZZE,*2D18750
15 1R0,FZCNS,ANVER,STINFL,KPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,AACA,*2D18760
16 2BACCB,CACCC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSQL,ATDSQ,TMT,*2D18770
17 3J,STMTJ,DELZ,ZK,ZPPP,TAMATZ,T,S,TSA,TSR,SIGMAC,ITAU,TAUHAT,R7,SZ *2D18780
18 *2D18790
19 *2D18A00
20 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),RETA(3),PHIZ(3),DELTA(3),*2D18810
21 1),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),RIGKI(7),*2D18820
22 2IPRIME(7),ALFAI(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR(*2D18830
23 3R),RH(8),THETAZ(8),STHETZ(8),CTHETZ(8),IBIG(8),THEDSQ(8),CTHETA(8),*2D18840
24 4),STHETA(8),BIGMI(8),IMATII(8),RHOPRM(8),XPRM(8),YPRM(8),*2D18850
25 5,TDSQL(8),ATDSQ(8),IGNORE(10),DA(10),XSMALA(10),YSMALA(10),*2D18860
26 6(10),PSTA(10),CPSTA(10),SPSIA(10),SIGMAC(10),FUA(10),GRAVA(10),RE,*2D18870
27 7E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11),*2D18880
28 8),ZVECP(11),STMTJ(13),AEI(14),RSEL(16),RVEL(16),MODE(16),TMTJZ(*2D18890
29 9(16),TMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EGNE(18),PN(18),*2D18900
30 DIMENSION DELOLD(18),DELDOO(18),EPSLNY(18),FTOLD(18),OMEGA(18),CZE,*2D18910
31 IRON(18),CNEN(18),CTWON(18),ET(18),EHAT(18),IFORK(3,8),SIGMA(10,3),*2D18920
32 2,XXX(300,3),YYY(300,3),FMM(300,3),RHB(300,3),SIGMAA(10,1),*2D18930
33 4LE(2,14),ZPPP(128),BL(3)
34 *2D18960
35 *2D18970
36 *2D18980
37 *2D18990
38 *2D19000
39 *2D19010
40 *2D19020
41 *2D19030
42 *2D19040
43 *2D19050
44 *2D19060
45 *2D19070
46 *2D19080
47 *2D19090
48 *2D19100
49 *2D19110
50 *2D19120
SUBROUTINE JITTER(ZKR)
COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,RHG,IGNJRE,DA,XSMALA,YSMAL,*2D18650
IA,XISMLA,PSIA,SPSIA,CPSTA,FUA,SIGMA,SIGMA,AA,KTALF,MFORI,OTR,PI,*2D18660
2TD,GRAVIT,CPRIME,BIGI,EL,AR,TPRIME,ALFA,OMEGA,RHO,THETA,*2D18670
3STHETZ,CTHETZ,FSPRM,RH,THATPV,WZPRD,RHTP7,RHDPFZ,SAMZER,LCONTL,CS,*2D18680
4,S,FUJ,S,BETA,ZERO,ELTMTY,ELTHRY,M,DESTP,DELTA,PHIZ,DELTA,NPASGR,*2D18690
5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,HPRNTD,GR,NS,SIGZ,ELZTEN,A,GRAVA,*2D18700
6,ELAMB,TIME,IBUG,MAXR,LITGAM,EPSUNZ,RSEL,RVEL,IBIG,IFDRK,BASIC,FS,*2D18710
7SMALLF,ZVEC,ZVECP,ZVEDPP,THEDSO,CTHETA,STHETA,BIGMI,IMATII,*2D18720
8XIDOT,YIDJ,PHI,EDNE,SDELTA,SDFLTD,RL,PN,MODE,OMFGA,X,Y,THEFEE,RH,*2D18730
SOPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELODD,DELDOO,EPSLNY,FTOLD,FSPRMZ *2D18740
COMMON CZERON,CNEN,CTWON,FT,EHAT,CEE,SMALLR,AEI,TMTJZ,TCAMZ,YZZE,*2D18750
1R0,FZCNS,ANVER,STINFL,KPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,AACA,*2D18760
2BACCB,CACCC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSQL,ATDSQ,TMT,*2D18770
3J,STMTJ,DELZ,ZK,ZPPP,TAMATZ,T,S,TSA,TSR,SIGMAC,ITAU,TAUHAT,R7,SZ *2D18780
*2D18790
*2D18A00
DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),RETA(3),PHIZ(3),DELTA(3),*2D18810
1),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),RIGKI(7),*2D18820
2IPRIME(7),ALFAI(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR(*2D18830
3R),RH(8),THETAZ(8),STHETZ(8),CTHETZ(8),IBIG(8),THEDSQ(8),CTHETA(8),*2D18840
4),STHETA(8),BIGMI(8),IMATII(8),RHOPRM(8),XPRM(8),YPRM(8),*2D18850
5,TDSQL(8),ATDSQ(8),IGNORE(10),DA(10),XSMALA(10),YSMALA(10),*2D18860
6(10),PSTA(10),CPSTA(10),SPSIA(10),SIGMAC(10),FUA(10),GRAVA(10),RE,*2D18870
7E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11),*2D18880
8),ZVECP(11),STMTJ(13),AEI(14),RSEL(16),RVEL(16),MODE(16),TMTJZ(*2D18890
9(16),TMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EGNE(18),PN(18),*2D18900
DIMENSION DELOLD(18),DELDOO(18),EPSLNY(18),FTOLD(18),OMEGA(18),CZE,*2D18910
IRON(18),CNEN(18),CTWON(18),ET(18),EHAT(18),IFORK(3,8),SIGMA(10,3),*2D18920
2,XXX(300,3),YYY(300,3),FMM(300,3),RHB(300,3),SIGMAA(10,1),*2D18930
4LE(2,14),ZPPP(128),BL(3)
*2D18960
*2D18970
*2D18980
*2D18990
*2D19000
*2D19010
*2D19020
*2D19030
*2D19040
*2D19050
*2D19060
*2D19070
*2D19080
*2D19090
*2D19100
*2D19110
*2D19120
COMMON THATPM,THATPX,THATPS,XVEHZ
COMMON FARB(18),SLOPE(18),ISWT(18),LOADSWT(18)
COMMON NONG(1402)
DIMENSION ZK8(11)
LITGAM=0
L=1
N=1
M=MAXI-1
ITOP=ITOPDWM(M)
DO 40 I=1,ITOP
CALL ZKMAKR(I,ZK(1,I))
40
K=IBIG(N)
ITOP = ITOPDWM(M)
ITPH=ITOPDWM(M-1)+1
CALL RESEL(ZK8,K,ZRV)
DO 70 I=1,ITOP

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Subroutine JITTER (page 1 of 3)


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51 70 CALL RELSEL(ZK(I,I),K,ZPPP(I))
52 IF (L-1) 100,100,80
53 DO 90 J=1,10
54 DELZ(J,K) = ZK(J,I*TOP+1)-ZK(J,I)
55 100 CALL RELSEL(DELZ(I,K),K,DELNUJ)
56 TSB = ZRV+ZPPP(I)
57 110 DO 130 I=1,I*TOP
58 TS = ZRV+ZPPP(I)
59 TSA = TS+DELNU
60 IF (TS+TSA) 180,120,120
61 IF (TS+TSB) 180,130,130
62 130 CONTINUE
63 140 IF (RVEL(K)+TSB) 150,150,160
64 150 MODE(K) = -1
65 IF (IRUG-1) 230,155,155
66 WRITE(6,9998)K
67 9998 FORMAT (6H MODE(12,12H) TURNED OFF)
68 GO TO 230
69 160 MODE(K) = 1
70 IF (IRUG-1) 167,163,163
71 WRITE(6,9997)K
72 9997 FORMAT (6H MODE(12,11H) TURNED ON)
73 DO 170 J=1,10
74 170 ZKB(J)=ZKB(J)+DELZ(J,K)
75 GO TO 230
76 180 IF (K-8) 200,190,185
77 185 IA = I*FORK(2-K-8)
78 IF (ABS(PSIA(IA))-PITWO).LE.1.E-4) GO TO 200
79 IF (ABS(PSIA(IA)-3.*PITWO).LE.1.E-4) GO TO 200
80 190 IF (FMH(KPOST,1)) 240,200,240
81 200 IF (IRUG-1) 205,203,203
82 WRITE(6,9996)K
83 9996 FORMAT (17HOJITTER FOR MODE(12,11H))
84 DO 220 I=1,I*TOP
85 AK = (ZPPP(I)+ZRV)/DELNU
86 IF (IRUG-2) 208,206,206
87 WRITE(6,9995)I,AK
88 9995 FORMAT (3H I=12,4H,AK=E14.6)
89 DO 210 J=1,10
90 ZK(J,I) = ZK(J,I)-AK*DELZ(J,K)
91 220 CONTINUE
92 L=L+1
93 N=N+1
94 M=M+1
95 IF (M) 420,60,60
96 IF (M) 360,360,250
97 KN=IBIG(M+1)
98 CALL RELSEL(ZKB,KN,ZRVN)
99 IF (L-1) 280,280,260
100 260 DO 270 I=1,10

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```

*2019130
*2019140
*2019150
*2019160
*2019170
*2019180
*2019190
*2019200
*2019210
*2019220
*2019230
*2019240
*2019250
*2019260
*2019270
*2019280
*2019290
*2019300
*2019310
*2019320
*2019330
*2019340
*2019350
*2019360
*2019370
*2019380
*2019390
*2019400
*2019410
*2019420
*2019430
*2019440
*2019450
*2019460
*2019470
*2019480
*2019490
*2019500
*2019510
*2019520
*2019530
*2019540
*2019550
*2019560
*2019570
*2019580
*2019590
*2019600
*2019610
*2019620

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101 270 DELZ(I,K) = ZK(I,ITOP+1)-ZK(I,1) *2019430
102 280 CALL RELSEL(DELZ(1,K),KN,DELNN) *2019440
103 290 DO 310 I=1,ITOP *2019650
104 CALL RELSEL(ZK(1,I),KN,TS) *2019660
105 TSA = ZRVN+TS+DELNN *2019670
106 TSB = TS+ZRVN *2019680
107 IF (I-1) 293,293,297 *2019690
108 293 TSC = ZRVN+TS *2019700
109 297 IF (TSA*TSB) 500,300,300 *2019710
110 300 IF (TSC*TSB) 500,310,310 *2019720
111 310 CONTINUE *2019730
112 IF (RVEL(KN)*TSC) 320,320,330 *2019740
113 320 MODE(KN) = -1 *2019750
114 GO TO 350 *2019760
115 330 MODE(KN) = 1 *2019770
116 DO 340 J=1,10 *2019780
117 340 ZKB(J)=ZK(J)+DELZ(J,KN) *2019790
118 CALL RELSEL(ZKB,K,ZRV) *2019800
119 350 M=M-1 *2019810
120 GO TO 240 *2019820
121 360 TS=ZRV+ZPPP(1)+DELNU *2019830
122 IF (IBUG) 368,368,363 *2019840
123 363 WRITE(6,9990)ZRV,ZPPP(1),DELNU,FMM(KPOST,1) *2019850
124 9990 FORMAT (5H0ZRV=E12.4,6H,ZPPP=E12.4,7H,DELNU=E12.4,5H,FMM=E12.4) *2019860
125 368 IF (K-8) 370,370,380 *2019870
126 370 TAHATZ = TS/FMM(KPOST,1) *2019880
127 GO TO 390 *2019890
128 380 IA=IFORK(2,K-8) *2019900
129 TAHATZ = TS/FMM(KPCST,1)/CPSIA(IA) *2019910
130 390 IF (TAHATZ-1.E-6) 140,140,400 *2019920
131 400 LITGAM = K *2019930
132 AK = .5/DELNU*(ZRV+ZPPP(1)-DELNU) *2019940
133 DO 410 J=1,10 *2019950
134 ZK(J,2)=ZK(J,1)+DELZ(J,K) *2019960
135 ZVECPP(J)=ZKB(J)+ZK(J,1)-AK*DELZ(J,K) *2019963
136 410 CONTINUE *2019965
137 RETURN *2019967
138 DO 430 J=1,10 *2019970
139 430 ZVECPP(J)=ZKB(J)+ZK(J,1) *2019980
140 RETURN *2019990
141 500 PRINT 9999,TIME *2020000
142 9999 FORMAT (30H0TWD LINEAR JITTER MODES AT T=F8.6) *2020010
143 PRINT 9991 *2020020
144 9991 FORMAT(1H1) *2020030
145 CALL SUMARY *2020040
146 CALL ERROR *2020050
147 END *2020060

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1  SUBROUTINE KRUNCH
2  COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,RRB,IGNJRE,DA,XSMALA,YSMAL *2D05540
3  *2D05550
4  1A,XISMLA,PSIA,CPSSIA,FMUA,SIGMA,AA,KTABE,MFORI,DIR,PI *2D05560
5  2TWO,GRAVIT,CPRIME,BIGKI,EL,AR,TPRIME,ALFAI,OMEGA,AL,OMEGAI,RPSI,RHO,THETAZ, *2D05570
6  3STHETZ,CTHETZ,FSPRM,RH,THATPV,WZERO,RHOPTZ,RHOPEZ,GAMZER,LCONTL,CS *2D05580
7  4S,FMUS,BETA,ZZERO,ELTMV,ELTHRY,H,DESTFP,DELTAI,PHIZ,DELTA,NPASGR *2D05590
8  5,XPACZ,MBELT,APRNTD,TIMAX,DTPRINT,BPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA *2D05600
9  6,ELAMB,TIME,IRUG,MAXR,LITGAM,EPSLNZ,RSEL,RVEL,IBIG,IFORK,BASIC,FS, *2D05620
10 7SMALLF,ZVEC,ZVECP,ZVECCP,THEDSO,CTHETA,STHETA, BIGMI,TMATII, *2D05630
11 8XIDOT,YIDOT,PHI,EONE,SDELTA,SDELTD,BL,PN, MUDE,OMEGA,X,Y,THEFEE,RH *2D05640
12 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELDD,DELDD,EPSLNY,FTOLD,FSPRMZ *2D05650
13 COMMON CZERUN,COMEN,CTMON,ET,EHAT,GEF,SMALLB,AEL,TIMTJZ,TGAMZ,YZE *2D05660
14 1RO,FZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,AACCA, *2D05670
15 2BACCB,CACCC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSQL,ATOSQ,TIMI *2D05680
16 3J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TSA,TSB,SIGMAC,ITAU,TAUHAT,RZ,SZ *2D05690
17 *2D05700
18
19 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3) *2D05710
20 1),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),RICKI(7), *2D05720
21 ZTPRIME(7),ALFAI(7),OMEGA(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR, *2D05730
22 38),RHO(8),THETAZ(8),STHETZ(8),CTHETZ(8),IBIG(8),THEDSO(8),CTHETA(8) *2D05740
23 4),STHETA(9),
24 5),IDSQL(14),ATDSQ(8),IGNORE(10),DA(10),XSMALA(10),YSMALA(10),XPRM(8) *2D05750
25 6(10),PSIA(10),CPSSIA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),BE *2D05760
26 7E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11) *2D05770
27 8),ZVECCP(11),STIMTJ(13),AEL(14),RSEL(16),RVEL(16),MODE(16),TIMTJZ( *2D05780
28 916),TIMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EONE(18),PN(18) *2D05790
29 DIMENSION DELD(18),DELDD(18),EPSLNY(18),FTOLD(18),OMEGA(18),CFE *2D05800
30 2,XXX(300,3),YYY(300,3),FMM(300,3),RRB(300,3),
31 30),AA(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,128),BASIC(11,8),KTAB *2D05810
32 4LE(2,14),ZPPP(128),BL(3)
33 *2D05820
34
35 COMMON THATPM,THATPX,THATPS,XVEHZ
36 COMMON FARB(18),SLOPE(18),ISMT(18),LDSWT(18)
37 COMMON NOND(1402)
38 DIMENSION ZKBASE(11)
39 TINFL = XX(2,1)
40 KPOST = 1
41 KTS = 1
42 TPRINT = APRNTD
43 TSTEP = XX(1,1)
44 AVELA = FMM(1,1)/2.
45 AACCA = AVELA/3.
46 BVELB = YVY(1,1)
47 BACCB = RVELB/2.
48 CVELC = XVEHZ
49 CACCC = CVELC
50 DACCD = 0.

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Subroutine KRUNCH (page 1 of 5)

51	MPRINT = 1	*2006040
52	MAXR = R	*2006050
53	LITGAM = 0	*2006060
54	EPSLNZ = 1.E-7	*2006070
55	DO 2270 I=1,16	*2006080
56	MUDE(I) = -1	*2006090
57	DELZ(11,I) = 0.	*2006100
58	RSEL(I) = 0.	*2006110
59	2270 RVEL(I) = 0.	*2006120
60	GEE(9) = 0.	*2006130
61	GEE(10) = GRAVA(9)	*2006140
62	KPRINT = 1	*2006150
63	DO 2310 I=1,11	*2006160
64	ZVEC(I) = 0.	*2006170
65	ZVECP(I) = 0.	*2006180
66	ZVECPP(I) = 0.	*2006190
67	2310 CONTINUE	*2006200
68	DO 2333 I=1,8	*2006210
69	ZVEC(I) = THETAZ(I)	*2006220
70	2333 IBIG(I) = 0	*2006230
71	ZVECP(9) = XPACZ	*2006240
72	ZVECP(11) = XVEHZ	*2006250
73	EDNEC = 0.	*2006260
74	THEFEE = THETAZ(1) - PHIZ(1)	*2006270
75	RHOPRM(1) = 0.	*2006280
76	RHOPRM(2) = 0.	*2006290
77	RHOPRM(3) = RHOPTZ	*2006300
78	RHOPRM(4) = RHOPFZ	*2006310
79	RHOPRM(5) = EL(5)	*2006320
80	RHOPRM(6) = EL(6)	*2006330
81	RHOPRM(7) = EL(7)	*2006340
82	RHOPRM(8) = EL(8)	*2006350
83	DO 2490 I=1,18	*2006360
84	DELODD(I) = 1.	*2006370
85	DELOLD(I) = 0.	*2006380
86	FTOLD(I) = 0.	*2006390
87	OMEGA(I) = 0.	*2006400
88	EPSLNY(I) = 0.	*2006410
89	CZERON(I) = 0.	*2006420
90	CONEN(I) = 0.	*2006430
91	CTWON(I) = 0.	*2006440
92	ET(I) = 0.	*2006450
93	PN(I) = 0.	*2006460
94	EONE(I) = 0.	*2006470
95	EHAT(I) = 0.	*2006480
96	2490 CONTINUE	*2006490
97	DO 2950 I=1,7	*2006500
98	GO TO (2900,2950,2950,2950,2900,2900,2900), I	*2006510
99	2900 IF (ALFAI(I)) 2910,2950,2910	*2006520
100	2910 TPRIME(I) = TPRIME(I)/ABS(ALFAI(I))	*2006530

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101 2950 CONTINUE
102 DO 2960 I=1,128
103 ZK(11,I) = 0.
104 TIMJZ(1) = THETAZ(1)-THETAZ(2)
105 TIMJZ(2) = THETAZ(1)-THETAZ(3)
106 TIMJZ(3)=THETAZ(1)-THETAZ(4)
107 TIMJZ(4) = THETAZ(1)-THETAZ(5)
108 TIMJZ(5)=THETAZ(1)-THETAZ(6)
109 TIMJZ(6)=THETAZ(1)-THETAZ(7)
110 TIMJZ(7)=THETAZ(2)-THETAZ(3)
111 TIMJZ(8)= THETAZ(2)-THETAZ(4)
112 TIMJZ(9)=THETAZ(2)-THETAZ(5)
113 TIMJZ(10)=THETAZ(2)-THETAZ(6)
114 TIMJZ(11)=THETAZ(3)-THETAZ(4)
115 TIMJZ(12)=THETAZ(3)-THETAZ(5)
116 TIMJZ(13) = THETAZ(3)-THETAZ(6)
117 TIMJZ(14) = THETAZ(4)-THETAZ(5)
118 TIMJZ(15) = THETAZ(5)-THETAZ(6)
119 TIMJZ(16) = THETAZ(7) - THETAZ(8)
120 AEL(1) = A(2)*EL(1)
121 AEL(2) = A(3)*EL(1)
122 AEL(3)=A(3)*EL(2)
123 AEL(4) = A(4)*EL(1)
124 AEL(5) = A(4)*EL(2)
125 AEL(6) = A(4)*EL(3)
126 AEL(7)=A(5)*EL(1)
127 AEL(8) = A(5)*EL(2)
128 AEL(9) = A(5)*EL(4)
129 AEL(10)=A(6)*EL(1)
130 AEL(11) = A(6)*EL(2)
131 AEL(12) = A(6)*EL(4)
132 AEL(13)=A(6)*EL(5)
133 AEL(14) = A(8)*EL(7)
134 AA(1,1) = A(10)
135 AA(2,2) = A(11)
136 AA(3,3) = A(12)
137 AA(4,4) = A(13)
138 AA(5,5) = A(14)
139 AA(6,6) = A(15)
140 AA(7,7) = A(16)
141 AA(8,8) = A(17)
142 AA(9,9) = A(9)
143 AA(10,10) = A(9)
144 YGAMZ = SIM(GAMZER)/COS(GAMZER)
145 YZERO=ZERO*YGAMZ
146 FSZCNS = F*SPRMZ + S*YZZERO
147 CALL GETY(TIME,2,TS)
148 IBUG=TS+.5
149 IF (IBUG.EQ.0) GO TO 5
150 WRITE(6,9919)IGNORE

```

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*2006540
*2006550
*2006560
*2006570
*2006580
*2006590
*2006600
*2006610
*2006620
*2006630
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*2006650
*2006660
*2006670
*2006680
*2006690
*2006700
*2006710
*2006720
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*2006740
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*2006780
*2006790
*2006800
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*2006850
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*2006870
*2006880
*2006890
*2006900
*2006910
*2006920
*2006930
*2006940
*2006950
*2006960
*2006970
*2006980
*2006990
*2006992
*2006993
*2006995
*2007000

```

151	5919	FORMAT (7H0IGNORE1015)	*2007010
152	5	CALL GETY(TIME,2,TS)	*2007020
153		IBUG = TS + .5	*2007030
154		CALL GETY(TIME,1,ZVECPP(11))	*2007040
155		CALL ACCEL	*2007050
156		DO 110 I=1,8	*2007060
157	110	CALL RELVEL(I,ZVECP,RVEL(I))	*2007070
158	320	MAXI = 0	*2007080
159		K = 1	*2007090
160		DO 360 I=1,MAXR	*2007100
161		IF (MODE(I)) 360,330,340	*2007110
162	330	RVEL(I) = SIGN(RPSI(I),RVEL(I))	*2007120
163		CALL DELZMK(I)	*2007130
164		IBIG(K) = I	*2007140
165		K = K+1	*2007150
166		MAXI = MAXI+1	*2007160
167		GO TO 360	*2007170
168	340	CALL DELZMK(I)	*2007180
169		DO 350 J=1,10	*2007190
170	350	ZVECPP(J) = ZVECPP(J) + DELZIJ,I)	*2007200
171	360	CONTINUE	*2007210
172		IF (MAXI-8) 361,361,690	*2007220
173	361	IF (IBUG-1) 367,363,363	*2007230
174	363	WRITE(6,9990)(ZVECPP(I),I=1,11)	*2007240
175	9990	FORMAT (9H0ZK BASF ,6E18.8)	*2007250
176		WRITE(6,9994)TIME,MAXI,(IBIG(I),I=1,MAXI)	*2007260
177	9994	FORMAT (6H0TIME=FC.8,10XRHI VECTOR10X5HIMAX=110,1X8I7)	*2007270
178	367	DO 20 I=1,11	*2007280
179	20	ZKBASE(I)=ZVECPP(I)	*2007290
180		IF (MAXI) 380,380,370	*2007300
181	370	CALL JITTER(ZKBASE)	*2007310
182	380	DO 8 I=1,MAXR	*2007320
183	8	CALL RESEL(ZVECPP,I,RSEL(I))	*2007330
184		CALL TAUMAK(ZKBASE)	*2007340
185		IF (IBUG) 392,170,392	*2007350
186	392	WRITE(6,9997)MAXR,(RVEL(I),I=1,MAXR)	*2007360
187	9997	FORMAT (5HORVEL10X110/(1X8E16.6))	*2007370
188		WRITE(6,9989)(RSEL(I),I=1,MAXR)	*2007380
189	9989	FORMAT (1X8E16.6)	*2007390
190	170	IF (KPRINT) 180,220,180	*2007400
191	180	IF (MPRINT) 190,210,210	*2007410
192	190	TPRINT = TPRINT + APRNTD	*2007420
193		MPRINT = 1	*2007430
194		GO TO 220	*2007440
195	200	TPRINT = TPRINT + BPRNTD	*2007450
196		MPRINT = 0	*2007460
197		GO TO 220	*2007470
198	210	TPRINT = TPRINT + DTPRNT	*2007480
199	220	IF (KINFL) 250,280,250	*2007490
200	250	KTS = KPOST + 1	*2007500

A-32

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201 IF (KTS-MAX(1)) 270,270,260
202 TINFL = 1.E20
203 GO TO 280
204 TINFL = XX(XKTS+1,1)
205 IF (TIME-TIMAX) 300,300,290
206 PRINT 9991
207 FORMAT (1H1)
208 RETURN
209 TIME = TIME + DELTAT
210 IF (IRUG) 303,306,303
211 WRITE(6,9958)KPRINT,KINFL,KSTEP,ITAU,TAUHAT,TPRINT,TINFL,TSTEP,
212 DELTAT,TIME
213 FORMAT (9HOKRUNCH A4I5,6E16.6)
214 TS = DELTAT*DELTAT/2.
215 DO 310 I=1,10
216 ZVEC(I)=ZVEC(I)+DELTAT*ZVECP(I)+TS*ZVECP(I)
217 ZVECP(I)=ZVECP(I)+DELTAT*ZVECPP(I)
218 CONTINUE
219 DO 318 I=1,8
220 IF (ABS(ZVEC(I)).GF.6.3) GO TO 700
221 CONTINUE
222 TSA = TIME - TSTEP
223 TSB = TSA*TSA
224 ZVEC(11) = (AACCA*TSA+BACCB)*TSB +CACCC*TSA +DACC
225 ZVECP(11) = AVELA*TSB+BVELB*TSA +CVELC
226 IF (KINFL) 4000,5,4000
227 KPOST = KTS
228 TSTEP = TIME
229 AVELA = FM*(KPOST,1)/2.
230 AACCA = AVELA/3.
231 BVELB = YY*(KPOST,1)
232 BACCB = RVELB/2.
233 CVELC = ZVECP(11)
234 CACCC = CVELC
235 DACC = ZVEC(11)
236 GO TO 5
237 PRINT 9995,TIME
238 FORMAT (9HOAT TIME=F10.6,45H, MORE THAN EIGHT ITEMS IN JITTER, RUN*2D07890
239 1STOPPED)
240 GO TO 290
241 PRINT 9989,TIME,I
242 5588 FORMAT(9HOAT TIME=F8.6,10H ANGLE NO.15,21H EXCEEDS 360 DEGREES.)
243 GO TO 290
244 END

```

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*2007517
*2007520
*2007530
*2007540
*2007550
*2007560
*2007570
*2007580
*2007590
*2007600
*2007610
*2007620
*2007630
*2007640
*2007650
*2007660
*2007670
*2007680
*2007690
*2007700
*2007710
*2007720
*2007730
*2007740
*2007750
*2007760
*2007770
*2007780
*2007790
*2007800
*2007810
*2007820
*2007830
*2007840
*2007850
*2007860
*2007870
*2007880
*2007900
*2007910
*2007920
*2007930
*2007940
*2007950

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1 SUBROUTINE LIMIDT(JP,JI,JS)
2 COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,BRB,IGVORE,DA,XSMALA,YSMAL,*2D23930
3 1A,XISMLA,PSIA,SPSIA,CPSTA,FMUA,SIGMAA,SIGMAAA,KTABLE,MFORI,MYR,PI,*2D23940
4 2TWD,GRAVIT,CPRIME,BIGKI,EL,AR,TPRI,ME,ALFAI,UMEGAI,RP,SI,RH,THE,TAZ,*2D23970
5 3STHETZ,CTHETZ,FSRPR,RRH,THATPY,WZERU,RNDPTZ,RHPFZ,GAMZER,LCONTL,CS,*2D23980
6 4,S,FMJS,RETA,ZZERO,ELTWTY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NPASGR,*2D23990
7 5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,RP,RTD,G,R,NS,SIGZ,FLZTEN,A,GRAVA,*2D24000
8 6,ELAMB,TIME,TRUG,MAXR,LITGAM,EPSLNZ,RSEL,RVEL,IRIG,IFORK,RASIC,FS,*2D24010
9 7SMALLF,ZVEC,ZVECP,ZVECPP,THEDSQ,CTHETA,STHETA, RIGMI,TMATII,*2D24020
10 RXIDOT,YIDOT,PHI,EDNE,S,DELTA,SDELTA,RL,PN,MODE,OMEGA,X,Y,THEFEE,RR,*2D24030
11 9DPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOLD,DELDDO,EPSLNY,FTOLD,FSPRMZ *2D24040
12 COMMON CZE,RCN,CJEN,CTMON,ET,EHAT,GEF,SMALLB,AEL,TMTJZ,GTGAMZ,YZFE,*2D24050
13 1RO,FSZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,AAACCA,*2D24060
14 2RACC,CAACC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TOSQL,ATDSQ,TMT,*2D24070
15 3J,STMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TSA,TSR,SIGMAC,ITAU,TAUHAT,RZ,SZ *2D24080
16 17 *2D24090
17 18 *2D24100
18 19 *2D24110
19 20 *2D24120
20 21 *2D24130
21 22 *2D24140
22 23 *2D24150
23 24 *2D24160
24 25 *2D24170
25 26 *2D24180
26 27 *2D24190
27 28 *2D24200
28 29 *2D24210
29 30 *2D24220
30 31 *2D24230
31 32 *2D24240
32 33 *2D24250
33 34 *2D24260
34 35 *2D24270
35 36 *2D24280
36 37 *2D24290
37 38 *2D24300
38 39 *2D24310
39 40 *2D24320
40 41 *2D24330
41 42 *2D24340
42 43 *2D24350
43 44 *2D24360
44 45 *2D24370
45 46 *2D24380
46 47 *2D24390
47 48 *2D24400
48 49 *2D24410
49 50 *2D24420
50

```

Subroutine LIMIDT (page 1 of 3)


```

51 CAZ(1) = COS(AZ(1))
52 SAZ(1) = SIN(AZ(1))
53 CONTINUE
54 AX(1) = AZ(9) - AZ(11)
55 AY(1) = AZ(10)
56 AX(2) = AX(1) + EL(1)*CAZ(1)
57 AY(2) = AY(1) + EL(1)*SAZ(1)
58 AX(3) = AX(2) + EL(2)*CAZ(2)
59 AY(3) = AY(2) + EL(2)*SAZ(2)
60 AX(4) = AX(3) + EL(3)*CAZ(3)
61 AY(4) = AY(3) + EL(3)*SAZ(3)
62 AX(5) = AX(4) + EL(4)*CAZ(4)
63 AY(5) = AY(4) + EL(4)*SAZ(4)
64 AX(6) = AX(5) + EL(5)*CAZ(5)
65 AY(6) = AY(5) + EL(5)*SAZ(5)
66 AX(7) = AX(6)
67 AY(7) = AY(6)
68 AX(8) = AX(7) + EL(7)*CAZ(7)
69 AY(8) = AY(7) + EL(7)*SAZ(7)
70 AXD(1) = AZP(9) - AZP(11)
71 AYD(1) = AZP(10)
72 AXD(2) = AXD(1) - EL(1)*SAZ(1)*AZP(1)
73 AYD(2) = AYD(1) + EL(1)*CAZ(1)*AZP(1)
74 AXD(3) = AXD(2) - EL(2)*SAZ(2)*AZP(2)
75 AYD(3) = AYD(2) + EL(2)*CAZ(2)*AZP(2)
76 AXD(4) = AXD(3) - EL(3)*SAZ(3)*AZP(3)
77 AYD(4) = AYD(3) + EL(3)*CAZ(3)*AZP(3)
78 AXD(5) = AXD(4) - EL(4)*SAZ(4)*AZP(4)
79 AYD(5) = AYD(4) + EL(4)*CAZ(4)*AZP(4)
80 AXD(6) = AXD(5) - EL(5)*SAZ(5)*AZP(5)
81 AYD(6) = AYD(5) + EL(5)*CAZ(5)*AZP(5)
82 AXD(7) = AXD(6)
83 AYD(7) = AYD(6)
84 AXD(8) = AXD(7) - EL(7)*SAZ(7)*AZP(7)
85 AYD(8) = AYD(7) + EL(7)*CAZ(7)*AZP(7)
86 IF (IBUG-2) 1010,1010,1000
87 1000 WRITE(6,9998)(I,AZ(I),AZP(I),AX(I),AY(I),AXD(I),AYD(I),I=1,8)
88 9998 FORMAT (7HULIMIDT/(2X)3, 6E17.8)
89 WRITE(6,9997)(I,AZ(I),AZP(I),I=9,11)
90 9997 FORMAT (2X)3, 2E17.8)
91 1010 DO 110 N=6,NS
92 IA = KTABLE(2,N-4)
93 IF (IA-3) 110,110,40
94 IF (IGNORE(IA)) 50,50,110
95 I = KTABLE(1,N-4)
96 PRMX = AX(I) + PHOPRM(I)*CAZ(I)
97 PRMY = AY(I) + RHOPRM(I)*SAZ(I)
98 TS = XSMALA(IA) - PRMX
99 TSA = YSMALA(IA) - PRMY
100 SIA = TS*SPSIA(IA) - TSA*CPSTA(IA)

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*2124430
*2124440
*2124450
*2124460
*2124470
*2124480
*2124490
*2124500
*2124510
*2124520
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*2124540
*2124550
*2124560
*2124570
*2124580
*2124590
*2124600
*2124610
*2124620
*2124630
*2124640
*2124650
*2124660
*2124670
*2124680
*2124690
*2124700
*2124710
*2124720
*2124730
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*2124760
*2124770
*2124780
*2124790
*2124800
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*2124820
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*2124850
*2124860
*2124870
*2124880
*2124890
*2124900
*2124910
*2124920

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```

101 SDELA = AR(I)-SIA
102 IF (SDELA) 90,90,60
103 TIA = TS*CPSTIA(IA) + T SA*SPSTIA(IA)
104 IF (TIA) 90,90,70
105 IF (TIA-DA(IA)) 80,80,90
106 VXIA = AXD(I) - RHOPRM(I)*AZP(I)*SAZ(I)
107 VYIA = AYD(I) + RHOPRM(I) * AZP(I)*CAZ(I)
108 SDELD = VXIA*SPSTIA(IA) - VYIA*CPSTIA(IA)
109 CALL FECLUD(N,SIGMA(I,IA),SDELA,SDELD,FORCE)
110 L = ABS(PN(N)-FORCE)/PCUNDS
111 GO TO 100
112 L = ARS(PN(N))/POUNDS
113 100 NMAX = MAX0(L+1,NMAX)
114 110 CONTINUE
115 120 IF (NMAX-1) 130,130,120
116 116 TS = NMAX
117 JP = 0
118 JI = 0
119 JS = 0
120 TIMASK = DELTAT/TS
121 WRITE(6,9999)TIME,DELTAT,TIMASK
122 9999 FORMAT (9H0AT TIME=F10.6,5XRDDELTA T=F12.8,5XRHRESET TO F12.8)
123 130 RETURN
124 END

```

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*2024930
*2024940
*2024950
*2024960
*2024970
*2024980
*2024990
*2025000
*2025010
*2025020
*2025030
*2025040
*2025050
*2025060
*2025070
*2025080
*2025090
*2025100
*2025110
*2025120
*2025130
*2025140
*2025150
*2025160

```

```

1  SUBROUTINE LODFEC( INDEX,DELL,STG,SDL,SDLD)
2  COMMON SWITCH,NEW,MAX,IPOST,XX,YYY,FMM,BB8,IGNORE,DA,XSMALA,YSMAL,*2D11310
3  1A,XISMLA,PSIA,SPSIA,CPSTA,FMUA,SIGMA,AA,KTARBLE,MFORI,DTR,PI,*2D11320
4  2TWO,GRAVIT,CPRIE,BIGKI,EL,AR,TPRIE,ALFAL,OMEGA,ALFAL,RPSI,THETAZ,*2D11330
5  3STHEZ,CTHEZ,FSPRMRH,THATPV,WZERO,RHOPTZ,GAMZEP,LCONTL,CS,*2D11340
6  4,S,FMUS,BETA,ZZERO,ELTMY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NPASGR,*2D11350
7  5,XPAZC,MBELT,APRNTD,TIMAX,ELTPRNT,BPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA,*2D11360
8  6,ELAMB,TIME,IBUG,MAXR,LITGAM,EPSLNZ,RSEL,RVEL,IBIG,IFORK,RAS,IC,FS,*2D11370
9  7SMALLF,ZVECP,ZVECP,ZVECP,THEDSO,CTHETA,STHETA, RIGMI,TMAT11,*2D11380
10 8XIDOT,YIDOT,PHI,EDNE,SDELTA,SDELTD,BL,PN,MODE,OMEGA,X,Y,THEFEE,RH,*2D11390
11 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOLD,DELDDO,EPSLNY,FTOLD,FSPRMZ *2D11400
12 10COMMON,CZERON,CONEN,CTMON,ET,EHAT,GE,SMALLB,AEI,TIMTJZ,TGAMZ,YZFE,*2D11410
13 11RO,FSZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,AACCA,*2D11420
14 12BACCC,CACCC,DACCC,MAXI,KPRINT,KSTEP,KINFL,TIMASK,IDSQI,AIDSQ,TIMT,*2D11430
15 13J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,YS, TSA,TSB,SIGMAC,TITAU,TAUHAT,RZ,SZ
16 14 *2D11440
17 15 *2D11450
18 16 *2D11460
19 17 *2D11470
20 18 *2D11480
21 19 *2D11490
22 20 *2D11500
23 21 *2D11510
24 22 *2D11520
25 23 *2D11530
26 24 *2D11540
27 25 *2D11550
28 26 *2D11560
29 27 *2D11570
30 28 *2D11580
31 29 *2D11590
32 30 *2D11600
33 31 *2D11610
34 32 *2D11620
35 33 *2D11630
36 34 *2D11640
37 35 *2D11650
38 36 *2D11660
39 37 *2D11670
40 38 *2D11680
41 39 *2D11690
42 40 *2D11700
43 41 *2D11710
44 42 *2D11720
45 43 *2D11730
46 44 *2D11740
47 45 *2D11750
48 46 *2D11760
49 47 *2D11770
50 48 *2D11780

```

```

1  SUBROUTINE LODFEC( INDEX,DELL,STG,SDL,SDLD)
2  COMMON SWITCH,NEW,MAX,IPOST,XX,YYY,FMM,BB8,IGNORE,DA,XSMALA,YSMAL,*2D11310
3  1A,XISMLA,PSIA,SPSIA,CPSTA,FMUA,SIGMA,AA,KTARBLE,MFORI,DTR,PI,*2D11320
4  2TWO,GRAVIT,CPRIE,BIGKI,EL,AR,TPRIE,ALFAL,OMEGA,ALFAL,RPSI,THETAZ,*2D11330
5  3STHEZ,CTHEZ,FSPRMRH,THATPV,WZERO,RHOPTZ,GAMZEP,LCONTL,CS,*2D11340
6  4,S,FMUS,BETA,ZZERO,ELTMY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NPASGR,*2D11350
7  5,XPAZC,MBELT,APRNTD,TIMAX,ELTPRNT,BPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA,*2D11360
8  6,ELAMB,TIME,IBUG,MAXR,LITGAM,EPSLNZ,RSEL,RVEL,IBIG,IFORK,RAS,IC,FS,*2D11370
9  7SMALLF,ZVECP,ZVECP,ZVECP,THEDSO,CTHETA,STHETA, RIGMI,TMAT11,*2D11380
10 8XIDOT,YIDOT,PHI,EDNE,SDELTA,SDELTD,BL,PN,MODE,OMEGA,X,Y,THEFEE,RH,*2D11390
11 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOLD,DELDDO,EPSLNY,FTOLD,FSPRMZ *2D11400
12 10COMMON,CZERON,CONEN,CTMON,ET,EHAT,GE,SMALLB,AEI,TIMTJZ,TGAMZ,YZFE,*2D11410
13 11RO,FSZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,AACCA,*2D11420
14 12BACCC,CACCC,DACCC,MAXI,KPRINT,KSTEP,KINFL,TIMASK,IDSQI,AIDSQ,TIMT,*2D11430
15 13J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,YS, TSA,TSB,SIGMAC,TITAU,TAUHAT,RZ,SZ
16 14 *2D11440
17 15 *2D11450
18 16 *2D11460
19 17 *2D11470
20 18 *2D11480
21 19 *2D11490
22 20 *2D11500
23 21 *2D11510
24 22 *2D11520
25 23 *2D11530
26 24 *2D11540
27 25 *2D11550
28 26 *2D11560
29 27 *2D11570
30 28 *2D11580
31 29 *2D11590
32 30 *2D11600
33 31 *2D11610
34 32 *2D11620
35 33 *2D11630
36 34 *2D11640
37 35 *2D11650
38 36 *2D11660
39 37 *2D11670
40 38 *2D11680
41 39 *2D11690
42 40 *2D11700
43 41 *2D11710
44 42 *2D11720
45 43 *2D11730
46 44 *2D11740
47 45 *2D11750
48 46 *2D11760
49 47 *2D11770
50 48 *2D11780

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Subroutine LODFEC (page 1 of 4)

```

51 160 COE(I) = SIG(I)
52 COE(6) = SIGZ(N)-FTOLD(N)
53 KKK=5
54 CALL MULLERCOE,KKK,R1CT4,ROOT1
55 RTM = 1.E20
56 DO 200 I=1,KKK
57 IS = P(OMG-ROTR(I))
58 IF (IS) 200,170,170
59 IF (IS-OMGT) 180,190,200
60 IF (RTM-ABS(ROOT1(I))) 200,200,190
61 EPSLNP = IS
62 RTM = ABS(ROOT1(I))
63 CONTINUE
64 EPSLNY(N) = EPSLNY(N)+EPSLNP
65 OMGT = SDL-DELL-EPSLNY(N)
66 POMG=0.
67 IF (OMGT) 410,410,230
68 IF (POMG) 240,240,250
69 SIGZ(N)=-(((SIG(10)*SOLD+SIG(9))*SOLD+SIG(8))*SOLD+SIG(7))*SOLD
70 1+SIG(6))*SOLD
71 ISWT(N)=0
72 PNDEL(N)=0.
73 IF (ISWT(N).NE.0) GO TO 257
74 TSA=(((SIG(5)*OMGT+SIG(4))*OMGT+SIG(3))*OMGT+SIG(2))*OMGT
75 1+SIG(1))*OMGT
76 PN(N)=TSA+SIGZ(N)+(((SIG(10)*SOLD+SIG(9))*SOLD+SIG(8))*SOLD
77 1+SIG(7))*SOLD+SIG(6))*SOLD
78 IF (DELTAT.LE.1.E-5) G1 TO 255
79 IF (PNDEL(N).LT.0.) GO TO 255
80 IF (TSA.GE.PNDEL(N)) GO TO 255
81 PRINT 9998,N,TIME
82 9998 FORMAT (54F,OUTSIDE MANDT(NIC PANG.F OF LOADING CURVE FOR INDEX N=
83 115,104 AT TIME =F8.6)
84 IF (TSA.LT.0.) PRINT 9997,N,TIME
85 PNDEL(N)=TSA
86 IF (LDSWT(N).EQ.0) GO TO 259
87 IF (PN(N).LT.FARR(N)) GO TO 259
88 ISWT(N)=1
89 PN(N)=FARR(N)
90 259 IF (PN(N)) 410,420,420
91 260 IF (DELDCO(N)) 270,270,300
92 270 IF (OMGT-OMEGA(N)) 280,280,400
93 280 IF (POMG-OMEGA(N)) 410,410,290
94 290 OMGT=OMEGA(N)
95 GO TO 410
96 IF (TIME) 303,303,307
97 EDNE(N) = (((SIG(5)/5.*OMGT+SIG(4)/5.*OMGT+SIG(3)/4.*OMGT+
98 1+SIG(2)/3.*OMGT+SIG(1)/2.*OMGT)*OMGT*PN(N)
99 FTOLD(N) = (((SIG(5)*OMGT+SIG(4))*OMGT+SIG(3))*OMGT+SIG(2))*OMGT+
100 1+SIG(1))*OMGT

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Subroutine LODFEC (page 2 of 4)

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101 IF (LDSWT(N).EQ.0) GO TO 306
102 IF (FTOLD(N).GE.FARB(N)) ISMT(N)=1
103 POMG=OMGT
104 IF (N-4) 410,410,307
105 IF (FTOLD(N)) 410,410,308
106 TSB=AMAX1(OMGT,POMG)
107 OMEGA(N)=G(N)*TSB
108 EHAT(N)=EDNE(N)
109 ET(N)=0.
110 IF (ISMT(N).EQ.0) GC TO 309
111 OMEGA(N)=TSB-FARB(N)/SLOPE(N)
112 IF (OMEGA(N).LT.0.) GO TO 500
113 CZERON(N)=FARB(N)-SLOPE(N)*TSB
114 CONEN(N)=SLOPE(N)
115 CTMON(N)=0.
116 ISMT(N)=0
117 GO TO 400
118
119 309 TS=FTOLD(N)*TSB*OMSGE
120 IF (2.*EHAT(N)-TS) 330,320,310
121 TSA = TS/EHAT(N)*R(N)/2.
122 PRINT 9900,R(N),TSA,N
123 R(N) = TSA
124 PRINT 9901,TIME
125 9901 FORMAT (44HORESET CONSERVED ENERGY TO LOWER LIMIT AT T=F8.6,
126 15H SEC.)
127 EHAT(N) = TS/2.
128 CZERON(N) = -TS
129 CONEN(N)=FTOLD(N)/CMSGE/TSB
130 CTMON(N)=0.
131 GO TO 400
132
133 330 IF (3.*EHAT(N)-TS) 340,370,390
134 TSA = TS/EHAT(N)*R(N)/3.
135 IF (TSA-1.) 350,360,360
136 PRINT 9900,R(N),TSA,N
137 R(N) = TSA
138 PRINT 9902,TIME
139 9902 FORMAT (44HORESET CONSERVED ENERGY TO UPPER LIMIT AT T=F8.6,
140 15H SEC.)
141 EHAT(N)=TS/3.
142 GO TO 370
143
144 360 OMSGE=3./FTOLD(N)*EHAT(N)/TSB
145 TSA = 1.-OMSGE
146 OMEGA(N)=TSB*TSA
147 PRINT 9903,G(N),TSA,N
148 9903 FORMAT (15HCHANGED G FROME17.8,3H TO E17.8,11H FOR INDEX I5)
149 G(N) = TSA
150 TS=FTOLD(N)/OMSGE/CMSGE
151 CZERON(N)=G(N)*G(N)*TS

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Subroutine LODFEC (page 3 of 4)

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151      CONEN(N)=-2./TSR*G(N)*TS
152      CTWON(N)=TS/TSR/TSR
153      GO TO 400
154      TSA=TSB*UMSGE*UMSGE*GMSGE
155      CZERON(N)=G(N)/TSA*(TS*(2.+G(N))-5.*EHAT(N))
156      TSA=TSR*TSR
157      CONEN(N)=2./TSA*(3.*EHAT(N))*(1.+G(N))
158      1-TS*(1.+G(N)+G(N))
159      CTWON(N)=3./TSA*(TS-2.*EHAT(N))/TSB
160      PN(N)=(CTWON(N)*DMGT+CCEN(N))*DMGT+CZERON(N)
161      GO TO 420
162      PN(N)=0.
163      420      DELET=(F TOLD(N)+PN(N))/2.*(CMGT-POMG)
164      ET(N) = ET(N)+DELET
165      EDNE(N) = EHAT(N)+K(N)*ET(N)
166      DELDOD(N) = SLD
167      DELDOD(N) = SLD
168      IF (IRUG.EQ.0) RETURN
169      WRITE(6,999)N,SDL,SOLD,PN(N),ET(N),[PSLNY(N)
170      FORMAT (A8,LODFEC 15,5E22,A)
171      RETURN
172      9997      FORMAT (40H NEGATIVE FORCE SET TO ZERO FOR INDEX N=15,10H AT TIME
173      1=E8.6)
174      500      PRINT 9996,N
175      9996      FORMAT(51HNEGATIVE PERMANENT DEFORMATION PREDICTED FOR INDEX I3)
176      PRINT 9995
177      FORMAT(11H)
178      CALL SUMMARY
179      CALL ERROR
180      END

```

```

*2012700
*2012800
*2012810
*2012820
*2012830
*2012840
*2012850
*2012860
*2012870
*2012880
*2012890
*2012900
*2012910
*2012920
*2012930
*2012940
*2012950
*2012955
*2012960
*2012970
*2012980
*2012990
*2013000
*2013010
*2013020
*2013030
*2013040
*2013050
*2013060
*2013070

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Subroutine LODFEC (page 4 of 4)

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1      COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,RRB,IGNORF,DA,XSMALA,YSMAL*2D00010
2      IA,XISMLA,PSIA,SPSIA,CPSIA,FMUA,SIGMAA,SIGMA,AA,KTABLE,MFORI,DTR,PI*2D00020
3      2TWO,GRAVIT,CPRIME,BIGI,EL,AR,TPRIME,ALFAI,OMEGAI,RPSI,RH1,THEYAZ,*2D00030
4      3STHETZ,CTHETZ,FSPRM,RH,THATPV,WZERO,RHOPTZ,RHOPFZ,GAMZER,LCONTL,CS*2D00040
5      4,S,FMUS,BETA,ZZERO,ELTY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NPASGR*2D00050
6      5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,BPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA*2D00060
7      6,ELAMB,TIME,IBUG,MAXR,LITGAM,EPSLNZ,RSEL,RVEL,IBIG,IFORK,BASIC,FS,*2D00070
8      7SMALLF,ZVEC,ZVECP,ZVECPP,THEDSQ,CTHETA,STHETA,          BIGMI,TMATII,*2D00080
9      8XIDOT,YIDOT,PHI,EONE,SDELTA,SDELTD,BL,PN,MODE,OMEGA,X,Y,THEFEE,RH*2D00090
10     9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOLD,DELDDO,EPSLNY,FTOLD,FSPRMZ *2D00100
11     COMMON CZERON,CONEN,CTWON,ET,EHAT,GEE,SMALLB,AEL,TIMTJZ,TGAMZ,YZZE*2D00110
12     1RO,FSZGNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,AACCA,*2D00120
13     2BACCB,CACCC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSQLI,ATDSQ,TIMT*2D00130
14     3J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TSA,TSB,SIGMAC,ITAU,TAUHAT,RZ,SZ *2D00140
15                                     *2D00150
16                                     *2D00160
17     DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3)*2D00170
18     1),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),BIGI(7),*2D00180
19     2TPRIME(7),ALFAI(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR(*2D00190
20     3B),RHO(8),THETAZ(8),STHETZ(8),CTHETZ(8),IBIG(8),THEDSQ(8),CTHETA(8)*2D00200
21     4),STHETA(8),          BIGMI(8),TMATII(8),RHOPRM(8),XPRM(8),YPRM(8)*2D00210
22     5,TDSQLI(8),ATDSQ(8),IGNORE(10),DA(10),XSMALA(10),YSMALA(10),XISMLA*2D00220
23     6(10),PSIA(10),CPSIA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),BE*2D00230
24     7E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11)*2D00240
25     8),ZVECPP(11),STIMTJ(13),AEL(14),RSEL(16),RVEL(16),MODE(16),TIMTJZ(*2D00250
26     916),TIMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EONE(18),PNI(18) *2D00260
27     DIMENSION DELOLD(18),DELDDO(18),EPSLNY(18),FTOLD(18),OMEGA(18),CZE*2D00270
28     1RON(18),CONEN(18),CTWON(18),ET(18),EHAT(18),IFORK(3,8),SIGMA(10,3)*2D00280
29     2,XXX(300,3),YYY(300,3),FMM(300,3),RRB(300,3),          SIGMAA(10,1)*2D00290
30     30),AA(10,10),ANVER(10,10),DELZ(11,16),ZK(11,128),BASIC(11,8),KTAB*2D00300
31     4LE(2,14),ZPPP(128),BL(3)          *2D00310
32                                     *2D00320
33     COMMON THATPW,THATPX,THATPS,XVEHZ          *2D00330
34     COMMON FARB(18),SLOPE(18),ISWT(18),LODSWT(18) *2D00340
35     COMMON NONO(1402)          *2D00350
36     COMMON IO/INN          *2D00355
37     DIMENSION CARD(8),EYE(8),EM(8),GA(10),RA(10),IALPH(26),IDATE(3) *2D00360
38     DIMENSION FAB(10),SLOP(10),LSWT(10) *2D00370
39     DATA IALPH/IHA,IHB,IHC,IHD,IHE,IHF,IHG,IHH,IHI,IHJ,IHK,IHL,IHM,IHN*2D00380
40     1,IHO,IHP,IHQ,IHR,IHS,IHT,IHU,IHV,IHW,IHX,IHY,IHZ/ *2D00390
41     INN=5          *2D00395
42     6 CALL DATE(IDATE)          *2D00400
43     PRINT 9904          *2D00410
44     9904 FORMAT(1H1)          *2D00420
45     ZERO = 0.          *2D00430
46     DO 92 I=1,3          *2D00440
47     SWITCH(I) = 0.          *2D00450
48     NEW(I) = 0          *2D00460
49     MAX(I) = 0          *2D00470
50     92 IPOST(I) = 0          *2D00480

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T-7

51		DD 94 I=1,3	*2000490
52		DD 94 J=1,300	*2000500
53		XXX(J,I)=0.	*2000510
54		YYY(J,I)=0.	*2000520
55		FMM(J,I)=0.	*2000530
56	94	BBB(J,I)=0.	*2000540
57		DD 96 I=1,10	*2000550
58		DA(I) = 0.	*2000560
59		GA(I) = 0.	*2000570
60		RA(I) = 0.	*2000580
61		IGNORE(I) = 0	*2000590
62		XSMALA(I) = 0.	*2000600
63		YSMALA(I) = 0.	*2000610
64		XISMLA(I) = 0.	*2000620
65		PSIA(I) = 0.	*2000630
66		SPSIA(I) = 0.	*2000640
67		CPSIA(I) = 0.	*2000650
68		FMUA(I) = 0.	*2000660
69		SIGMAC(I) = 0.	*2000670
70		FAB(I)=0.	*2000680
71		SLOP(I)=0.	*2000690
72		LSWT(I)=0	*2000700
73	96	CONTINUE	*2000710
74		DD 2 I=1,10	*2000720
75		DD 1 J=1,10	*2000730
76	1	SIGMAA(I,J) = 0.	*2000740
77		SIGMA(I,1) = 0.	*2000750
78		SIGMA(I,2) = 0.	*2000760
79	2	SIGMA(I,3) = 0.	*2000770
80		DD 3 I=1,10	*2000780
81		DD 3 J=1,10	*2000790
82	3	AA(I,J)=0.	*2000800
83		DD 4 I=1,3	*2000810
84		SDELTA(I) = 0.	*2000820
85		SDELTD(I) = 0.	*2000830
86		RL(I)=0.	*2000840
87	4	PHI(I) = 0.	*2000850
88		DD 73 I=1,18	*2000860
89		FARB(I)=0.	*2000870
90		SLOPE(I)=0.	*2000880
91		ISWT(I)=0	*2000890
92	73	LODSWT(I)=0	*2000900
93		MFORI(1) = 7	*2000910
94		MFORI(2) = 1	*2000920
95		MFORI(3) = 2	*2000930
96		MFORI(4) = 3	*2000940
97		MFORI(5) = 3	*2000950
98		MFORI(6) = 5	*2000960
99		MFORI(7) = 8	*2000970
100		DTR = .01745329	*2000980

A-42


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101 PITWO = 1.570796
102 GRAVIT = 3.86.4
103 IC=0
104 100 READ (INN,9900,END=8150) ID,CARD
105 9900 FORMAT (A1,E9.0,7E10.0)
106 IC=IC+1
107 PRINT 9920,IC,ID,CARD
108 9920 FORMAT (1X,I5,5X,A1,8F13.4)
109 DO 101 I=1,26
110 IF (ID-IALPH(I)) 101,103,101
111 CONTINUE
112 102 PRINT 9901,ID,CARD
113 9901 FORMAT (22H0ILLEGAL CARD SKIPPED.3XAI,2XREI3.4)
114 GO TO 100
115 C
116 A B C D E F G H I J K L M N O
117 103 GO TO (140,180,200,230,260,300,330,360,400,430,460,500,530,560,600)200110
118 1,630,660,700,730,760,800,104,107,850,900,1000,I
119 P Q R S T U V W X Y Z
120 C
121 CARD V TABLE READ
122 ITABL = CARD(I) + .5
123 IF (ITABL-3) 105,105,102
124 SWITCH(ITABL) = CARD(I)
125 II = MINO(MAX(ITABL)+1,300)
126 VVV(II,ITABL) = CARD(I)
127 XXX(II,ITABL) = CARD(I)
128 IF (CARD(2)) 106,100,106
129 MAX(ITABL) = II
130 NEW(ITABL) = 1
131 GO TO 100
132 C
133 CARD W TABLE DELETE
134 ITABL = CARD(I) + .5
135 IF (ITABL) 102,102,108
136 IF (ITABL-3) 109,109,102
137 109 IF (ABS(CARD(2))*ABS(CARD(3))) 111,110,111
138 SWITCH(ITABL) = 0.
139 MAX(ITABL) = 0
140 NEW(ITABL) = 0
141 GO TO 100
142 II = 1
143 IA = AMINI(CARD(2),CARD(3))
144 XB = AMAXI(CARD(2),CARD(3))
145 IF (XX(II,ITABL)-XA) 114,113,113
146 IF (XB-XXX(II,ITABL)) 114,115,115
147 II = II + 1
148 IF (II-MAX(ITABL)) 112,112,100
149 JJ = II + 1
150 NEW(ITABL) = 1
151 IF (JJ-MAX(ITABL)) 117,117,116
152 IF (JJ-MAX(ITABL)) 117,117,116
153 IF (JJ-MAX(ITABL)) 117,117,116
154 IF (JJ-MAX(ITABL)) 117,117,116
155 IF (JJ-MAX(ITABL)) 117,117,116
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246 IF (JJ-MAX(ITABL)) 117,117,116
247 IF (JJ-MAX(ITABL)) 117,117,116
248 IF (JJ-MAX(ITABL)) 117,117,116
249 IF (JJ-MAX(ITABL)) 117,117,116
250 IF (JJ-MAX(ITABL)) 117,117,116

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151 116 MAX(ITABL) = II-1
152 GO TO 100
153 117 IF (XXX(JJ,ITABL)-XA) 119,118,114
154 118 IF (XR-XXX(JJ,ITABL)) 119,120,120
155 119 XXX(II,ITABL) = XXX(JJ,ITABL)
156 120 YYY(II,ITABL) = YYY(JJ,ITABL)
157 II = II + 1
158 JJ = JJ + 1
159 GO TO 121
160 CARD A
161 DO 142 I=1,7
162 CPRIME(I) = CARD(I)
163 GO TO 100
164 CARD B
165 DO 182 I=1,8
166 EYE(I) = CARD(I)
167 GO TO 100
168 CARD C
169 DO 202 I=1,7
170 BIGKI(I) = CARD(I)
171 GC TO 100
172 CARD D
173 DO 232 I=1,8
174 EL(I) = CARD(I)
175 GO TO 100
176 CARD E
177 DO 262 I=1,8
178 EM(I) = CARD(I)
179 CONTINUE
180 EMFVX = EM(5) + EM(6)
181 EMTHSX = EMFVX + EM(3) + FM(4)
182 EMTWSX = EMTHSX + EM(2)
183 GO TO 100
184 CARD F
185 DO 302 I=1,8
186 AR(I) = CARD(I)
187 GO TO 100
188 CARD G
189 DO 332 I=1,7
190 TPRIME(I) = CARD(I)
191 GO TO 100
192 CARD H
193 ALFAI(1) = CARD(1)*DTR
194 DO 362 I=5,7
195 ALFAI(I) = CARD(I-3)*DTR
196 THATPW = CARD(5)
197 THATPX = CARD(6)
198 THATPS = CARD(7)
199 THATPS = CARD(8)
200 GO TO 100

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201 C          CARD      I
202 DO 402 I=1,7
203 OMEGA(I) = CARD(I)*DTR
204 GO TO 100
205 C          CARD      J
206 DO 432 I=1,7
207 RPSI(I) = CARD(I)*DTR
208 GO TO 100
209 C          CARD      K
210 DO 462 I=1,8
211 RHO(I) = CARD(I)
212 GO TO 100
213 C          CARD      L
214 DO 502 I=1,8
215 THETAZ(I) = CARD(I)*DTR
216 STHETAZ(I) = SIN(THETAZ(I))
217 CTHETAZ(I) = COS(THETAZ(I))
218 CONTINUE
219 GO TO 100
220 C          CARD      M
221 FSPRMZ = CARD(I)
222 RH = CARD(2)
223 WZERO = CARD(4)
224 RHOPZ = CARD(5)
225 RHOPFZ = CARD(6)
226 GAMZER = CARD(7)*DTR
227 LCONTL = ABS(CARD(8)) + .5
228 GO TO 100
229 C          CARD      N
230 CS = CARD(1)
231 S = CARD(2)
232 RPSI(8) = CARD(3)
233 FHUS = CARD(4)
234 BETA(1) = CARD(5)
235 BETA(2) = CARD(6)
236 BETA(3) = CARD(7)
237 ZZERU = CARD(8)
238 GO TO 100
239 C          CARD      O
240 ELPTEN = CARD(1)
241 ELTMY = CARD(2)
242 ELTHRY = CARD(3)
243 H = CARD(4)
244 FEPTEN = CARD(5)*DTR
245 DESTEP = CARD(6)
246 DELTAT = DESTEP
247 RZ=CARD(7)
248 SZ=CARD(8)
249 GO TO 100
250 C          CARD      P

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```

*2D01950
*2D01960
*2D01970
*2D01980
*2D01990
*2D02000
*2D02010
*2D02020
*2D02030
*2D02040
*2D02050
*2D02060
*2D02070
*2D02080
*2D02090
*2D02100
*2D02110
*2D02120
*2D02130
*2D02140
*2D02150
*2D02160
*2D02170
*2D02180
*2D02190
*2D02200
*2D02210
*2D02220
*2D02230
*2D02240
*2D02250
*2D02260
*2D02270
*2D02280
*2D02290
*2D02300
*2D02310
*2D02320
*2D02330
*2D02340
*2D02350
*2D02360
*2D02370
*2D02380
*2D02390
*2D02400
*2D02410
*2D02420
*2D02430
*2D02440

```

```

251 M = CARD(1) + .5
252 IF (M) 102,102,631
253 IF (M-3) 632,632,102
254 G(M) = CARD(2)
255 R(M) = CARD(3)
256 PHIZ(M) = CARD(4)*DTR
257 DELTA(M) = CARD(5)
258 SIGMA(1,M) = CARD(6)
259 SIGMA(2,M) = CARD(7)
260 SIGMA(3,M) = CARD(8)
261 GO TO 100
262 CARD O
263 M = CARD(1) + .5
264 IF (M) 102,102,661
265 IF (M-3) 662,662,102
266 SIGMA(4,M) = CARD(2)
267 SIGMA(5,M) = CARD(3)
268 SIGMA(6,M) = CARD(4)
269 SIGMA(7,M) = CARD(5)
270 SIGMA(8,M) = CARD(6)
271 SIGMA(9,M) = CARD(7)
272 SIGMA(10,M) = CARD(8)
273 GO TO 100
274 CARD R
275 NPASGR = AMAX1(CARD(1),1.,3.)+.5
276 XPACZ = CARD(2)
277 XVEHZ = CARD(3)
278 NBELT = ABS(CARD(4))+.5
279 APRNTD = CARD(5)
280 TIMAX = CARD(6)
281 EMC = CARD(7)
282 PCNTL = ABS(CARD(8))
283 DTPRNT = PCNTL*APRNTD
284 BPRNTD = AMAX1(DTPRNT-APRNTD,APRNTD)
285 GO TO 100
286 CARD S
287 IA = CARD(1) +1.5
288 IF (IA) 102,102,731
289 IF (IA-10) 732,732,102
290 DA(IA) = CARD(2)
291 GA(IA) = CARD(3)
292 RA(IA) = CARD(4)
293 XSMALA(IA) = CARD(5)
294 YSMALA(IA) = CARD(6)
295 XISMLA(IA) = CARD(7)
296 PSIA(IA) = CARD(8)*DTR
297 SPSTIA(IA) = SIN(PSIA(IA))
298 CPSTIA(IA) = COS(PSIA(IA))
299 GO TO 100
300 CARD T

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*2007450
*2002460
*2002470
*2002480
*2002490
*2002500
*2002510
*2002520
*2002530
*2002540
*2002550
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*2002570
*2002580
*2002590
*2002600
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*2002800
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*2002820
*2002830
*2002840
*2002850
*2002860
*2002870
*2002880
*2002890
*2002900
*2002910
*2002920
*2002930
*2002940

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301 IA = CARD(1) +1.5
302 IF (IA) 102,102,761
303 IF (IA-10) 762,762,102
304 FMUA(IA) = CARD(2)
305 SIGMAA(1,IA) = CARD(3)
306 SIGMAA(2,IA) = CARD(4)
307 SIGMAA(3,IA) = CARD(5)
308 SIGMAA(4,IA) = CARD(6)
309 SIGMAA(5,IA) = CARD(7)
310 SIGMAA(6,IA) = CARD(8)
311 GO TO 100
312 CARD U
313 800 IA = CARD(1) +1.5
314 IF (IA) 102,102,801
315 801 IF (IA-10) 802,802,102
316 802 SIGMAA(7,IA) = CARD(2)
317 SIGMAA(8,IA) = CARD(3)
318 SIGMAA(9,IA) = CARD(4)
319 SIGMAA(10,IA) = CARD(5)
320 GO TO 100
321 CARD X
322 850 I=CARD(1)+1.5
323 IF(I.GT.10) GO TO 855
324 FAB(I)=CARD(2)
325 SLOP(I)=CARD(3)
326 LSWT(I)=1
327 GO TO 100
328 J=I-11
329 FAB(J)=CARD(2)
330 SLOPE(J)=CARD(3)
331 LOOSWT(J)=1
332 GO TO 100
333 CARD Y
334 500 CONTINUE
335 GO TO 100
336 CARD Z
337 1000 IF (CARD(1)) 302C,3000,3000
338 3000 MAX(2) = 1
339 SWITCH(2) = 0.
340 YV(1,2) = CARD(1)
341 DO 1001 N=1,18
342 1001 SIGZ(N) = 0.
343 DO 5 I=1,2
344 DO 5 K=1,14
345 KTABLE(I,K) = 0
346 IF (NPASGR-2) 10,30,40
347 10 DO 20 N=4,5
348 KTABLE(1,N) = 3
349 20 KTABLE(2,N) = 2*N-2
350 NS = 18

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*2D02950
*2D02960
*2D02970
*2D02980
*2D02990
*2D03000
*2D03010
*2D03020
*2D03030
*2D03040
*2D03050
*2D03060
*2D03070
*2D03080
*2D03090
*2D03100
*2D03110
*2D03120
*2D03130
*2D03140
*2D03150
*2D03160
*2D03170
*2D03180
*2D03190
*2D03200
*2D03210
*2D03220
*2D03230
*2D03240
*2D03250
*2D03260
*2D03270
*2D03280
*2D03290
*2D03300
*2D03310
*2D03320
*2D03330
*2D03340
*2D03350
*2D03360
*2D03370
*2D03380
*2D03390
*2D03400
*2D03410
*2D03420
*2D03430
*2D03440

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351      S = 10
352      S = 5
353      GO TO 50
354      K = 7
355      M = 4
356      NS = 15
357      GO TO 50
358      K = 6
359      M = 4
360      J = 4
361      L = 0
362      NS = 14
363      GO TO 60
364      J = 7
365      L = 2
366      KTABLE(1,1) = 1
367      KTABLE(2,3) = 4
368      KTABLE(1,K+1) = 5
369      KTABLE(1,K+2) = 7
370      KTABLE(1,K+3) = 8
371      KTABLE(1,K+4) = 8
372      KTABLE(2,K+1) = 2
373      KTABLE(2,K+2) = J
374      KTABLE(2,K+3) = 1
375      KTABLE(2,K+4) = J+L
376      DO 70 N=M,K
377      KTABLE(1,N) = 4
378      KTABLE(2,N) = 2*N-M
379      DO 80 N=1,2
380      KTABLE(1,N+1)=3
381      KTABLE(2,N) = 2
382      DO 90 N=5,NS
383      KN=KTABLE(2,N-4)
384      R(N)=GA(KN)
385      R(N)=RA(KN)
386      FARB(N)=FAR(KN)
387      SLOPE(N)=SLOP(KN)
388      LODSMT(N)=LSMT(KN)
389      MODE(N-4)=KN-1
390      N=N-4
391      PRINT 9915,N,(KTABLE(1,J),J=1,N)
392      FORMAT (4I0NS=13/3H I=14I5)
393      PRINT 9912,(MODE(J),J=1,N)
394      FORMAT (3H A=14I5)
395      DO 920 I=1,10
396      IF (FMA(I)) 912,911,912
397      IGNORE(I) = -1
398      IF (DA(I)) 915,915,913
399      DO 914 J=1,10
400      IF (SIGMAA(J,I)) 920,914,920

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*2003450
*2003460
*2003470
*2003480
*2003490
*2003500
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*2003890
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*2003940

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401 514 CONTINUE
402 915 IGNORE(I) = 1
403 CONTINUE
404 DD 1020 I=1,3
405 IPOST(I) = 1
406 IF (NEW(I)) 1004, 1020, 1004
407 1004 IMAX = MAX(I)
408 J=2
409 1005 IF (XXX(J-1,I)-XXX(J,I)) 1016,1009,1006
410 1006 X(I)=XXX(J,I)
411 Y(I)=VYV(J,I)
412 JJ = J - 1
413 1007 XXX(JJ+1,I) = XXX(JJ,I)
414 VYV(JJ+1,I) = VYV(JJ,I)
415 JJ = JJ - 1
416 IF (JJ-1) 1014,1008,1008
417 1008 IF (XXX(JJ,I)-X(I)) 1015,1010,1007
418 1009 JJ = J - 1
419 Y(I)=VYV(J,I)
420 1010 VYV(JJ,I)=Y(I)
421 1011 JJ = JJ + 1
422 1012 IF (JJ-IMAX) 1012,1013,1013
423 XXX(JJ,I) = XXX(JJ+1,I)
424 VYV(JJ,I) = VYV(JJ+1,I)
425 GO TO 1011
426 1013 IMAX = IMAX - 1
427 GO TO 1017
428 JJ = 0
429 1015 XXX(JJ+1,I)=X(I)
430 VYV(JJ+1,I)=Y(I)
431 1016 J=J+1
432 1017 IF (J-IMAX) 1005,1005,1018
433 1018 MAX(I) = IMAX
434 III = IMAX - 1
435 DD 1019 J=1,III
436 FMM(J,I) = (VYV(J+1,I)-VYV(J,I))/(XXX(J+1,I)-XXX(J,I))
437 1019 BBB(J,I) = (VYV(J,I)-FMM(J,I)*XXX(J,I))
438 BBB(IMAX,I) = 0.
439 FMM(IMAX,I) = 0.
440 CONTINUE
441 PRINT 9905, I, DATE
442 9905 FORMAT (45X35HCRASH SIMULATION PROGRAM NUMBER ONE40X3A4/1H07X3HMO.
443 111X1M20X1H121X1M.20X3HRH018X1HR17X5HTHETA)
444 DD 1040 I=1,8
445 TS = THE TAZ(I)/DTR
446 PRINT 9906, I, EM(I), EYE(I), EL(I), RHO(I), AR(I), TS
447 1040 CONTINUE
448 9906 FORMAT (110,6E20.8)
449 PRINT 9907
450 9907 FORMAT (1H07X3HMO.9X6HTPRIME15X5HALPHA15X5HOMEGA16X1HK16X6HCPRI ME

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451      116X2HX11) *2004450
452      DO 1029 I=1,7 *2004451
453      TSA = ALFA I(I)/DTR *2004452
454      TSB = OMEGA I(I)/DTR *2004453
455      TS=RPSI(I)/DTR *2004454
456      PRINT 9906,I,TPRIME(I),TSA,TSB,BIGMI(I),CPRIME(I),TS *2004500
457 1029 CONTINUE *2004510
458      PRINT 9917,RZ,SZ,APRNTD,PCNTL,LCCNTL *2004520
459 9917 FORMAT (4HORZ=E17.8,4H,SZ=E17.8,15H,DELTA T PRINT=F8.6,24H,V). PEP *2004530
460 1PR INT INTERVAL=E12.3,8H,LCCNTL=15) *2004540
461      TS = FEPTEN/DTR *2004550
462      TSA = GAMZER/DTR *2004560
463      PRINT 9908,FSPRMZ,RH,THATPV,WZER0,WHOPTZ,PHUPEZ,TS,CS,S,RPSI(R), *2004570
464 1FMUS,ZZERO,ELPTEN,ELTWTY,ELTHRY,H,TSA,XPACZ,NPASGR,NBELT,DELTA T, *2004580
465 2TIMAX,EMC *2004590
466 9908 FORMAT (1H 7HFSPRMZ=E17.8,4H,RH=E17.8,8H,THATPV=E17.8,4H,W0=F17.8,*2004600
467 17H,RHOP3=E17.8/7H RHOP4=E17.8,7H,PHIP1=F12.3,4H,CS=E17.8,3H,S=F17.*2004610
468 28,5H,XIS=E17.8,5H,MUS=E17.8/4H ZJ=F17.8,5H,LP1=F17.8,5H,LP2=F17.8,*2004620
469 35H,LP3=E17.8,3H,H=E17.8/8H GAMMA0=F12.3,4H,VC=E17.8,8H,NPASGR=12,7*2004630
470 4H,NBELT=12,9H,DELTA T=F8.4/10H MAX TIME=F10.4,4H,MC=F17.8/1H08X1HM *2004640
471 513X1HG19X1HR18X3HPH116X5HDELTA16X4HRETA) *2004650
472      DO 1030 I=1,3 *2004660
473      TS = PHIZ(I)/DTR *2004670
474      PRINT 9906,I,G(I),R(I),TS,DELTA(I),BETA(I) *2004680
475 1030 CONTINUE *2004690
476      PRINT 9909 *2004700
477 9909 FORMAT (1H08X1HM51X5HSIGMA) *2004710
478      DO 1031 I=1,3 *2004720
479      PRINT 9910,I,(SIGMA(J,I),J=1,10) *2004730
480 9910 FORMAT (1H019,5E20.8/10X5E20.8) *2004740
481 1031 CONTINUE *2004750
482      PRINT 9913,(I,DA(I),GA(I),RA(I),XSMLA(I),YSMLA(I),FMUA(I),I=1,10)*2004760
483 1) *2004770
484 9913 FORMAT (1H08X1HA13X1HD19X1HG19X1HR19X1HX19X1HY18X3HMUA/(110,6E20.*2004780
485 1)) *2004790
486      PRINT 9914 *2004800
487 9914 FORMAT (1H08X1HA13X2HX117X3HPS1) *2004810
488      DO 1032 I=1,10 *2004820
489      TS = XISMLA(I) *2004830
490      TSA=PSIA(I)/DTR *2004840
491      PRINT 9915,I,TS,TSA *2004850
492 9915 FORMAT (110,F17.3,F20.3) *2004860
493 1032 CONTINUE *2004870
494      PRINT 9911 *2004880
495 9911 FORMAT (1H08X1HA51X5HSIGMA) *2004890
496      DO 1033 I=1,10 *2004900
497      PRINT 9910,I,(SIGMA(J,I),J=1,10) *2004910
498 1033 CONTINUE *2004920
499      DO 1028 I=1,3 *2004930
500      IF (SWITCH(I)) 1021,1023,1021 *2004940

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A-5


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13)
ELAMB(3)=ELAMB(3)+I*STHEITZ(2)-ELT*TY*STN(PHIZ(2))
ELAMB(4)=ELAMB(4)+H*CTHETZ(2)-FLT*TV*COB(PHIZ(2))
2150 TIME=0.
REWIND 9
CALL KRUNCH
CALL SUMARY
GO TO 6
8150 STOP
END

*2005450
*2005460
*2005470
*2005480
*2005490
*2005500
*2005510
*2005520
*2005525
*2005530

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```

1 C DECK MINV *2037410
2 C ..... *2037420
3 C ..... *2037430
4 C ..... *2037440
5 C ..... *2037450
6 C ..... *2037460
7 C ..... *2037470
8 C ..... *2037480
9 C ..... *2037490
10 C ..... *2037500
11 C ..... *2037510
12 C ..... *2037520
13 C ..... *2037530
14 C ..... *2037540
15 C ..... *2037550
16 C ..... *2037560
17 C ..... *2037570
18 C ..... *2037580
19 C ..... *2037590
20 C ..... *2037600
21 C ..... *2037610
22 C ..... *2037620
23 C ..... *2037630
24 C ..... *2037640
25 C ..... *2037650
26 C ..... *2037660
27 C ..... *2037670
28 C ..... *2037680
29 C ..... *2037690
30 C ..... *2037700
31 C ..... *2037710
32 C ..... *2037720
33 C ..... *2037730
34 C ..... *2037740
35 C ..... *2037750
36 C ..... *2037760
37 C ..... *2037770
38 C ..... *2037780
39 C ..... *2037790
40 C ..... *2037800
41 C ..... *2037810
42 C ..... *2037820
43 C ..... *2037830
44 C ..... *2037840
45 C ..... *2037850
46 C ..... *2037860
47 C ..... *2037870
48 C ..... *2037880
49 C ..... *2037890
50 C ..... *2037900

SUBROUTINE MINV
PURPOSE
INVERT A MATRIX
USAGE
CALL MINV(A,N,D,L,M)
DESCRIPTION OF PARAMETERS
A - INPUT MATRIX, DESTROYED IN COMPUTATION AND REPLACED BY
RESULTANT INVERSE.
N - ORDER OF MATRIX A
D - RESULTANT DETERMINANT
L - WORK VECTOR OF LENGTH N
M - WORK VECTOR OF LENGTH N
REMARKS
MATRIX A MUST BE A GENERAL MATRIX
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE
METHOD
THE STANDARD GAUSS-JORDAN METHOD IS USED. THE DETERMINANT
IS ALSO CALCULATED. A DETERMINANT OF ZERO INDICATES THAT
THE MATRIX IS SINGULAR.
.....
SUBROUTINE MINV(A,N,D,L,M)
DIMENSION A(1),L(1),M(1)
.....
IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE
C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION
STATEMENT WHICH FOLLOWS.
DOUBLE PRECISION A,D,RIGA,HOLD
THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS
APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS
ROUTINE.
THE DOUBLE PRECISION VERSION OF THIS SUBROUTINE MUST ALSO
CONTAIN DOUBLE PRECISION FORTRAN FUNCTIONS. ABS IN STATEMENT

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51 C          10 MUST BE CHANGED TO DARS.
52 C
53 C .....
54 C SEARCH FOR LARGEST ELEMENT
55 C
56 C
57 C      D=1.0
58 C      NK=-N
59 C      DO 80 K=1,N
60 C      NK=NK+N
61 C      L(K)=K
62 C      M(K)=K
63 C      KK=NK+K
64 C      BIGA=A(KK)
65 C      DO 20 J=K,N
66 C      IZ=M*(J-1)
67 C      DO 20 I=K,N
68 C      IJ=IZ+I
69 C      10 IF ( ABS(BIGA)- ABS(A(IJ))) 15,20,20
70 C      15 BIGA=A(IJ)
71 C      L(K)=I
72 C      M(K)=J
73 C
74 C      20 CONTINUE
75 C
76 C      INTERCHANGE ROWS
77 C
78 C      J=L(K)
79 C      IF(J-K) 35,35,25
80 C      DO 30 I=1,N
81 C      KI=KI+N
82 C      HOLD=-A(KI)
83 C      JI=KI-K+J
84 C      A(KI)=A(JI)
85 C      A(JI)=HOLD
86 C
87 C      INTERCHANGE COLUMNS
88 C
89 C      35 I=M(K)
90 C      IF(I-K) 45,45,38
91 C      JP=N*(I-1)
92 C      DO 40 J=1,N
93 C      JK=NK+J
94 C      JI=JP+J
95 C      HOLD=-A(JK)
96 C      A(JK)=A(JI)
97 C      A(JI)=HOLD
98 C
99 C      40
100 C      DIVIDE COLUMN BY MINUS PIVOT (VALUE OF PIVOT ELEMENT IS
      CONTAINED IN BIGA)

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Subroutine MINV (page 2 of 4)

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101 C
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150
45 IF(BIGA) 48,46,48
46 D=0.0
   RETURN
48 DO 55 I=1,N
   IF(I-K) 50,55,50
50 IK=NK+I
   A(IK)=A(IK)/(-BIGA)
55 CONTINUE
C
110 C
111 C
112 C
113 C
114 C
115 C
116 C
117 C
118 C
119 C
120 C
121 C
122 C
123 C
124 C
125 C
126 C
127 C
128 C
129 C
130 C
131 C
132 C
133 C
134 C
135 C
136 C
137 C
138 C
139 C
140 C
141 C
142 C
143 C
144 C
145 C
146 C
147 C
148 C
149 C
150 C
   REDUCE MATRIX
   DO 65 I=1,N
   IK=NK+I
   HOLD=A(IK)
   IJ=I-N
   DO 65 J=1,N
   IJ=IJ+N
   IF(I-K) 62,65,60
60 IF(J-K) 62,65,62
62 KJ=IJ-I+K
   A(IJ)=HOLD*(A(IK)+A(IJ))
65 CONTINUE
C
124 C
125 C
126 C
127 C
128 C
129 C
130 C
131 C
132 C
133 C
134 C
135 C
136 C
137 C
138 C
139 C
140 C
141 C
142 C
143 C
144 C
145 C
146 C
147 C
148 C
149 C
150 C
   DIVIDE ROW BY PIVOT
   KJ=K-N
   DO 75 J=1,N
   KJ=KJ+N
   IF(J-K) 70,75,70
70 A(KJ)=A(KJ)/BIGA
75 CONTINUE
C
133 C
134 C
135 C
136 C
137 C
138 C
139 C
140 C
141 C
142 C
143 C
144 C
145 C
146 C
147 C
148 C
149 C
150 C
   PRODUCT OF PIVOTS
   D=D*BIGA
C
137 C
138 C
139 C
140 C
141 C
142 C
143 C
144 C
145 C
146 C
147 C
148 C
149 C
150 C
   REPLACE PIVOT BY RECIPROCAL
   A(KK)=1.0/BIGA
80 CONTINUE
C
143 C
144 C
145 C
146 C
147 C
148 C
149 C
150 C
   FINAL ROW AND COLUMN INTERCHANGE
   K=N
100 K=(K-1)
   IF(K) 150,150,1C5
105 I=L(K)
   IF(I-K) 120,120,108
108 JQ=N*(K-1)

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*2D38410
*2D38420
*2D38430
*2D38440
*2D38450
*2D38460
*2D38470
*2D38480
*2D38490
*2D38500
*2D38510
*2D38520
*2D38530
*2D38540
*2D38550
*2D38560
*2D38570
*2D38580
*2D38590
*2D38600
*2D38610
*2D38620
*2D38630
*2D38640
*2D38650
*2D38660
*2D38670
*2D38680
*2D38690
*2D38700
*2D38710
*2D38720
*2D38730
*2D38740
*2D38750
*2D38760
*2D38770
*2D38780
*2D38790
*2D38800
*2D38810
*2D38820
*2D38830
*2D38840
*2D38850
*2D38860
*2D38870
*2D38880
*2D38890
*2D38900

```

```

151 JR=N*(I-1)
152 DO 110 J=1,N
153 JK=JQ+J
154 HOLD=A(JK)
155 JI=JR+J
156 A(JK)=-A(JI)
157 A(JI)=HOLD
158 J=M(K)
159 IF (J-K) 100,100,125
160 KI=K-N
161 DO 130 I=1,M
162 KI=KI+N
163 HOLD=A(KI)
164 JI=KI-K+J
165 A(KI)=-A(JI)
166 A(JI)=HOLD
167 GO TO 160
168
169
100 RETURN
110 END
125

```

```

*2D38910
*2D38920
*2D38930
*2D38940
*2D38950
*2D38960
*2D38970
*2D38980
*2D38990
*2D39000
*2D39010
*2D39020
*2D39030
*2D39040
*2D39050
*2D39060
*2D39070
*2D39080
*2D39090

```

```

1          SUBROUTINE MULLER(COE,N1,ROOTR,ROOTI)
2          DIMENSION COE(16),ROOTR(15),ROOTI(15)
3          N2=N1+1
4          IF (COE(1)) 400,300,400
5          300 DO 310 I=1,N1
6              J = I
7              IF (COE(I)) 320,310,320
8          310 CONTINUE
9              N1 = 0
10             ROOTR(1) = 0.
11             ROOTI(1) = 0.
12             GO TO 37
13          320 JJ = 0
14             DO 330 I=J,N2
15                 JJ = JJ + 1
16          330 COE(JJ) = COE(I)
17                 N2 = JJ
18                 N1 = JJ-1
19             IF (N1-1) 400,340,400
20          340 ROOTR(1) = -COE(2)/COE(1)
21             ROOTI(1) = 0.
22             GO TO 37
23          400 N4 = 0
24             I=N1+1
25             19 IF (COE(I)) 9,7,9
26                 7 N4=N4+1
27                 ROOTR(N4)=0.
28                 ROOTI(N4)=0.
29                 I=I-1
30                 IF (N4-N1) 19,37,19
31             9 CONTINUE
32             10 AXR=0.8
33                 AXI=0.
34                 L=1
35                 N3=1
36                 ALP1R=AXR
37                 ALP1I=AXI
38                 M=1
39                 GOTO99
40             11 BET1R=TEMR
41                 BET1I=TEMI
42                 AXR=0.85
43                 ALP2R=AXR
44                 ALP2I=AXI
45                 M=2
46                 GOTO99
47             12 BET2R=TEMR
48                 BET2I=TEMI
49                 AXR=0.9
50

```

```

*2026580
*2026590
*2026600
*2026610
*2026620
*2026630
*2026640
*2026650
*2026660
*2026670
*2026680
*2026690
*2026700
*2026710
*2026720
*2026730
*2026740
*2026750
*2026760
*2026770
*2026780
*2026790
*2026800
*2026810
*2026820
*2026830
*2026840
*2026850
*2026860
*2026870
*2026880
*2026890
*2026900
*2026910
*2026920
*2026930
*2026940
*2026950
*2026960
*2026970
*2026980
*2026990
*2027000
*2027010
*2027020
*2027030
*2027040
*2027050
*2027060
*2027070

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51	ALP3R=AXR	*2027080
52	ALP3I=AXI	*2027090
53	M=3	*2027100
54	GO TO 99	*2027110
55	13 BET3R=TEM	*2027120
56	BET3I=TEMI	*2027130
57	14 TE1=ALP1R-ALP3R	*2027140
58	TE2=ALP1I-ALP3I	*2027150
59	TE5=ALP3R-ALP2R	*2027160
60	TE6=ALP3I-ALP2I	*2027170
61	TEM=TE5*TE5+TE6*TE6	*2027180
62	IF(TEM.EQ.0.) GO TO 1200	*2027190
63	TE3=(TE1*TE5+TE2*TE6)/TEM	*2027200
64	TE4=(TE2*TE5-TE1*TE6)/TEM	*2027210
65	1250 TE7=TE3+1.	*2027220
66	TE9=TE3*TE3-TE4*TE4	*2027230
67	TE10=2.*TE3*TE4	*2027240
68	DE15=TE7*BET3R-TE4*BET3I	*2027250
69	DE16=TE7*BET3I+TE4*BET3R	*2027260
70	TE11=TE3*BET2R-TE4*BET2I+BET1R-DE15	*2027270
71	TE12=TE3*BET2I+TE4*BET2R+BET1I-DE16	*2027280
72	TE7=TE9-1.	*2027290
73	TE1=TE9*BET2R-TE10*BET2I	*2027300
74	TE2=TE9*BET2I+TE10*BET2R	*2027310
75	TE13=TE1-BET1R-TE7*BET3R+TE10*BET3I	*2027320
76	TE14=TE2-BET1I-TE7*BET3I-TE10*BET3R	*2027330
77	TE15=DE15*TE3-DE16*TE4	*2027340
78	TE16=DE15*TE4+DE16*TE3	*2027350
79	TE1=TE13*TE13-TE14*TE14-4.*(TE11*TE15-TE12*TE16)	*2027360
80	TE2=2.*TE13*TE14-4.*(TE12*TE15+TE11*TE16)	*2027370
81	TEM=SQRT(TE1*TE1+TE2*TE2)	*2027380
82	IF(TE1)113,113,112	*2027390
83	113 TE4=SQRT(.5*(TEM-TE1))	*2027400
84	IF(TE4.EQ.0.) GO TO 1300	*2027410
85	TE3=.5*TE2/TE4	*2027420
86	GO TO 111	*2027430
87	1000 TE3=0.	*2027440
88	GO TO 111	*2027450
89	1200 TE3=0.	*2027460
90	TE4=0.	*2027470
91	GO TO 1250	*2027480
92	112 TE3=SQRT(.5*(TEM+TE1))	*2027490
93	IF(TE2)110,200,200	*2027500
94	110 TE3=-TE3	*2027510
95	200 TE4=.5*TE2/TE3	*2027520
96	111 TE7=TE13+TE3	*2027530
97	TE8=TE14+TE4	*2027540
98	TE9=TE13-TE3	*2027550
99	TE10=TE14-TE4	*2027560
100	TE1=2.*TE15	*2027570

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101      TF 2=2.*TE16                                *2D27580
102      IF (TE7*TE7+TE8*TE8-TE9*TE9-TE10*TE10)204,204,205 *2D27590
103      204 TE 7=TE 9                                *2D27600
104      TE 8=TE10                                    *2D27610
105      205 TEM=TE7*TE7+TE8*TE8                    *2D27620
106      IF (TEM.EQ.0.) GO TO 1100                    *2D27630
107      TE3=(TE1*TE7+TE2*TE8)/TEM                   *2D27640
108      TE4=(TE2*TE7-TE1*TE8)/TEM                   *2D27650
109      1050 AXR=ALP3R+TE3*TE5-TE4*TE6              *2D27660
110      AXI=ALP3I+TE3*TE6+TE4*TE5                  *2D27670
111      ALP4R=AXR                                    *2D27680
112      ALP4I=AXI                                    *2D27690
113      M=4                                           *2D27700
114      GO TO 99                                      *2D27710
115      1100 TE3=0.                                   *2D27720
116      TE4=0.                                       *2D27730
117      GO TO 1050                                    *2D27740
118      15 N6=1                                       *2D27750
119      38 IF (ABS(HELL)+ABS(BELL))-1.E-20) 18,18,16 *2D27760
120      16 TE 7=ABS(ALP3R-AXR)+ABS(ALP3I-AXI)         *2D27770
121      IF (TE7/(ABS(AXR)+ABS(AXI))-1.E-7) 18,18,17 *2D27780
122      17 N3=N3+1                                     *2D27790
123      ALP1R=ALP2R                                   *2D27800
124      ALP1I=ALP2I                                   *2D27810
125      ALP2R=ALP3R                                   *2D27820
126      ALP2I=ALP3I                                   *2D27830
127      ALP3R=ALP4R                                   *2D27840
128      ALP3I=ALP4I                                   *2D27850
129      BET1R=BET2R                                   *2D27860
130      BET1I=BET2I                                   *2D27870
131      BET2R=BET3R                                   *2D27880
132      BET2I=BET3I                                   *2D27890
133      BET3R=TEMR                                    *2D27900
134      BET3I=TEMI                                    *2D27910
135      IF (N3-100)14,18,18                          *2D27920
136      18 N4=N4+1                                     *2D27930
137      ROOTR(N4)=ALP4R                               *2D27940
138      ROOTI(N4)=ALP4I                               *2D27950
139      N3=0                                           *2D27960
140      41 IF (N4-N1)30,37,37                        *2D27970
141      37 RETURN                                     *2D27980
142      30 IF (ABS(ROOTI(N4))-1.E-5)10,10,31          *2D27990
143      31 GO TO(32,10),L                             *2D28000
144      32 AXR=ALP1R                                   *2D28010
145      AXI=-ALP1I                                    *2D28020
146      ALP1I=-ALP1I                                  *2D28030
147      M=5                                           *2D28040
148      GO TO 99                                      *2D28050
149      33 BET1R=TEMR                                  *2D28060
150      BET1I=TEMI                                  *2D28070

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151	AXR=ALP2R	*2028080
152	AXI=-ALP2I	*2028090
153	ALP2I=-ALP2I	*2028100
154	M=6	*2028110
155	GO TO 99	*2028120
156	34 BET2R=TEMK	*2028130
157	BET2I=TEMI	*2028140
158	AXR=ALP3R	*2028150
159	AXI=-ALP3I	*2028160
160	ALP3I=-ALP3I	*2028170
161	L=2	*2028180
162	M=3	*2028190
163	99 TEMR=COE(1)	*2028200
164	TFMI=0.0	*2028210
165	DO100I=1,N1	*2028220
166	TE1=TEMR*AXR-TEMI*AXI	*2028230
167	TEMI=TEMI*AXR+TEMR*AXI	*2028240
168	100 TEMR= TE1+COE(I+1)	*2028250
169	BELL=TEMR	*2028260
170	BELL=TEMI	*2028270
171	42 IF(N4)102,103,102	*2028280
172	102 DO101I=1,N4	*2028290
173	TEMI=AXR-ROOTR(I)	*2028300
174	TEM2=AXI-ROOTI(I)	*2028310
175	TE1=TEMI*TEMI+TEM2*TEM2	*2028320
176	IF(TE1.EQ.0.0) GO TO 1300	*2028330
177	TE2=(TEMR*TEMI+TEMI*TEM2)/TE1	*2028340
178	TEMI=(TEMI*TEMI-TEMR*TEM2)/TE1	*2028350
179	101 TEMR=TE2	*2028360
180	103 GO TO(11,12,13,15,33,34),M	*2028370
181	1300 TEMR=0.	*2028380
182	TEMI=0.	*2028390
183	GO TO 103	*2028400
184	END	*2028410

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1 SUBROUTINE NORMUT
2 COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,BRB,IGNORE,DA,XSMALA,YSMAL,*2D07960
3 1A,XISMLA,PSIA,SPSIA,FMUA,SIGMAA,SIGMA,AA,KTABLE,MFCQI,DIR,PI*2D07980
4 2TMD,GRAVIT,CPRIME,BIGKI,ELAR,IPRIME,ALFAT,OMEGAI,RPSI,RHO,THETAZ,*2D08000
5 3STHETZ,CTHETZ,FSRPM,RH,THATPV,WZERU,RHOPT7,RHOPTZ,GAMZER,LCONTI,CS,*2D08010
6 4S,FMUS,BETA,ZZERU,ELTWTY,ELTHRY,H,DESTEP,DELAT,PHIZ,DELTA,NPASGR*2D08020
7 5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,ARPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA*2D08030
8 6,ELAMB,TIME,IRUG,MAXR,LITGAM,EPNLZ,RSEL,RVEL,IBIG,IFORK,RASIC,FS,*2D08040
9 7SMALLF,ZVECP,ZVECP,ZVECP,THEDSQ,CTHETA,STHETA, RIGMI,TMATII,*2D08050
10 8XIDUT,YIDJT,PHI,EDNE,SDELTA,SDELTD,BL,PN,MODE,OMFGA,X,Y,THEFEF,HH*2D08060
11 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELDD,DELDOD,=PSLY,FTOLD,FSRPMZ *2D08070
12 10COMMON CZE,RON,CONEN,CTMON,ET,EHAT,GEE,SMALLB,AEL,TIMTJZ,IGAM7,YZZE*2D08080
13 11RO,FSZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,ACCCA,*2D08090
14 12BACCB,CACCC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSQLI,ATDSQ,TIMT*2D08100
15 133J,STIMTJ,DELZ,ZK,ZPPP,TAMATZ,TS,TSB,SIGMAC,ITAU,TAUHAT,RZ,SZ *2D08110
16 14 *2D08120
17 15 *2D08130
18 16
19 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3)*2D08140
20 1),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFCQI(7),CPRIME(7),BIGKI(7),*2D08150
21 2TPRIME(7),ALFAI(7),CMEGAI(7),XIDUT(7),YIDOT(7),X(7),Y(7),EL(8),AR(*2D08160
22 38),RHO(8),THETAZ(8),STHETZ(8),CTHETZ(8),TRIG(3),THEDSQ(9),CTHETA(8)*2D08170
23 4),STHETA(8), RIGMI(8),TMATII(8),RHOPT(8),XPRM(8),YPRM(8)*2D08180
24 5),TDSQLI(8),ATDSQ(8),IGNORE(10),DAI(10),XSMALA(10),YSMALA(10),XISMLA*2D08190
25 6(10),PSIA(10),CPSIA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),RF*2D08200
26 7E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVECP(11),ZVECP(11)*2D08210
27 8),ZVECP(11),STIMTJ(13),AEL(14),RSEL(15),RVEL(16),MODE(16),TIMTJZ*2D08220
28 9(16),TIMTJ(16),PPSI(16),A(17),G(18),R(18),SIGZ(18),EDNE(18),PN(18)*2D08230
29 DIMENSION DELOD(18),DELDOD(18),EPSLNY(18),FOLD(18),OMEGA(18),CZE*2D08240
30 1MON(18),CONEN(18),CTMON(18),ET(18),EHAT(18),IFORK(3,8),SIGMA(10,1)*2D08250
31 2,XXX(300,3),YYY(300,3),FMM(300,3),BRB(300,3), SIGMA(10,1)*2D08260
32 30),AAI(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,12),RASIC(11,8),KTA*2D08270
33 4LE(2,14),ZPPP(128),BL(3) *2D08280
34 *2D08290
35 *2D08300
36 COMMON THATPV,THATPX,TATPS,XVEHZ
37 COMMON FAR(18),SLOPE(18),ISMT(18),LODSWT(18)
38 COMMON NONO(1402)
39 DIMENSION TT(8),TV(8),TAIR,KI(8),KA(8),PP(8)
40 6,2 HEAD AND CHEST ACCELERATIONS
41 TS=ZVECP(9)-EL(1)*(ZVECP(1)+STHETA(1)+THEDSQ(1)*CTHETA(1))-EL(7)*2D08350
42 1*(ZVECP(2)+STHETA(2)+THEDSQ(2)*CTHETA(2))
43 TSA=ZVECP(3)+STHETA(3)+THEDSQ(3)*CTHETA(3)
44 XHEAD=TS-EL(3)*TSA
45 XHEAD=TS-EL(3)*TSA-RM(4)*(ZVECP(4)+STHETA(4)+THEDSQ(4)*CTHETA(4)*2D08400
46 1) *2D08410
47 ACH = TS/GRAVIT
48 BCH = TSA/GRAVIT
49 AH = ACH-EL(3)*BCH
50 TS=ZVECP(10)+EL(1)*(ZVECP(1)+STHETA(1)-THEDSQ(1)*CTHETA(1))+EL(7)*2D08450

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51 1)*(ZVECP(2)*CTHETA(2)-THEDSQ(2)*STHETA(2))
52 TSA=ZVECP(3)*CTHETA(3)-THEDSQ(3)*STHETA(3)
53 YCHEST=TS+RHO(3)*TSA
54 YHEAD=TS+EL(3)*TSA+RHO(4)*(ZVECP(4)*CTHETA(4)-THEDSQ(4)*STHETA(4)
55 1)
56 CCH = TS/GRAVIT
57 DCH = TSA/GRAVIT
58 CH = CCH+EL(3)*DCH
59 DH = (ZVECP(4)*CTHETA(4)-THEDSQ(4)*STHETA(4))/GPAVIT
60 ACHEST= SORT(XCHEST*YCHEST+YCHEST*YCHEST)
61 AHEAD= SORT(XHEAD*YHEAD+YHEAD*YHEAD)
62 GCHEST = ATAN2(YCHEST,XCHEST)/DTR
63 GHEAD = ATAN2(YHEAD,XHEAD)/DTR
64 IF (IBUG) 6710,6715,6710
65 6710 WRITE(6,9925)TIME
66 9925 FORMAT (57X)HAT TIME = F10.4)
67 WRITE(6,9916)
68 9916 FORMAT (1H04+X5H)TETA4+X5HX HIP7X5HY HIP7X5HX CAR)
69 6715 DO 6720 I=1,8
70 TT(I) = ZVEC(I)/DTR
71 6720 CONTINUE
72 IF (IBUG.EQ.0) GO TO 6721
73 WRITE(6,9924)TT,ZVEC(9),ZVEC(10),ZVEC(11)
74 9924 FORMAT (1X)F11.3,7F12.3,3E12.4)
75 6721 DO 6722 I=1,8
76 TV(I) = ZVECP(I)/DTR
77 6722 CONTINUE
78 IF (IBUG.EQ.0) GO TO 6723
79 WRITE(6,9924)TV,ZVECP(9),ZVECP(10),ZVECP(11)
80 6723 DO 6724 I=1,8
81 TA(I) = ZVECP(I)/DTR
82 6724 CONTINUE
83 IF (IBUG.EQ.0) GO TO 6800
84 WRITE(6,9928)TA,ZVECP(9),ZVECP(10),ZVECP(11)
85 9928 FORMAT (11E12.4)
86 WRITE(6,9919)TIME,FS,FSPRM,SMALLF,XHEAD,YHEAD,AHEAD,GHEAD,
87 1XCHEST,YCHEST,ACHEST,GCHEST
88 1E17.8/1H019X1HX19X1
89 ZHY19X1HAI7X5HGAMMA/3X4H)HEAD3XE20.8,F17.3/2X5H)CHEST3XE20.8,F17.3)
90 WRITE(6,9921)
91 9921 FORMAT (1H03X1H)M85H)DELTA12X9H)DELTA DOT13X2H)FM10X3H)PHI12X3H)E1M14X7
92 1H)EPSILON14X3H)DEM)
93 DO 6750 I=1,3
94 TS = PHI(I)/DTR
95 WRITE(6,9920)I,SDELTA(I),SDELTO(I),PM(I),TS,EONE(I),EPSLNY(I)
96 9920 FORMAT (15.3E18.8,F10.3,2E18.8)
97 6750 CONTINUE
98 6800 IF (KPRINT) 7000,7200,7000
99 7000 IF (LCONTL-1) 7010,7010,7200
100

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101 7010 DISP = ZVEC(9) - ZVEC(11)
102   PLX = ZVECP(9)/GRAVIT
103   PLY = ZVECP(10)/GRAVIT
104   PLC = ZVECP(11)/GRAVIT
105   HEADX = X(4) + RHO(4)*CTHETA(4)
106   HEADY = Y(4) + RHO(4)*STHETA(4)
107   JJ = 0
108   DO 7120 N=5,NS
109   IF (PN(N)) 7120,7120,7110
110   711C JJ = JJ+1
111   KI(JJ) = KTABLE(1,N-4)
112   KA(JJ) = KTABLE(2,N-4)
113   PP(JJ) = PN(N)
114   7120 CONTINUE
115   IF (TIME .NE. 0.) GO TO 7130
116   WRITE(9)ELAMB,XSMALA,YSMALA,AR,RHOFPZ,RHOPTZ,EL,DA,CPSIA,
117   ISPSIA,IGAMZ,ZZERO,NBEL,IGNORE,RHO
118   7130 WRITE(9)TIME,TT,TV,TA,DISP,ZVECP(9),PLX,ZVEC(10),ZVECP(10),
119   1PLY,ZVEC(11),ZVECP(11),PLC,AH,BH,CH,DH,ACH,BCH,CCH,DCH,
120   2(K(I),KA(I),PP(I),I=1,JJ),(PN(N),N=1,3),F,SPRM,F,S,HEADX,HEADY
121   3,PHI,BL
122   720C RETURN
123   END

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*2D08940
*2D08950
*2D08960
*2D08970
*2D08980
*2D08990
*2D09000
*2D09010
*2D09020
*2D09030
*2D09040
*2D09050
*2D09060
*2D09070
*2D09080
*2D09090
*2D09100
*2D09110
*2D09120
*2D09130
*2D09140
*2D09150
*2D09160

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1          SUBROUTINE PAGE4                                *2037090
2          DIMENSION A(36,3),AA(6)                        *2037100
3          DATA A/4HFRON,4HT CU,4HLLIS,3HIGN,2*1H ,4HREAR,4H COL,4HLISI,2HON,*2037110
4          DATA A/4HFRON,4HT CU,4HLLIS,3HIGN,2*1H ,4HREAR,4H COL,4HLISI,2HON,*2037120
5          12*1H ,4HSIDE,4H COL,4HLISI,2HON,2*1H ,4H45 D,4HEGRE,4HE LE,4HFT O,*2037130
6          24HBLIQ,2HUE,4H45 D,4HEGRE,4HE RI,3HGHT,4HOBLI,3HQUE,4HROLL,4HOVER,*2037140
7          34*1H ,4HDRIV,2HER,4*1H ,4HRIGH,4HT FR,3HUNT,4HPASS,4HFNGE,1HR,4HRI*2037150
8          4GH,4HT RE,4HAR P,4HASSE,4HNGER,1H ,4HLEFT,4H REA,4HR PA,4HSSEN,3HG*2037160
9          5FR,13*1H ,4HNO B,3HELT,3HUSE,3*1H ,3HLAP,4HBELT,4H USE,3*1H ,4HSHO*2037170
10         6U,4HLDER,4H HAR,4HNESS,4H USE,1H ,4HSHOU,4HLDER,4H E L,4HAP B,3HEL*2037180
11         7T,3HUSE,4HAIRB,4HAG A,4HND L,4HAP B,3HELT,3HUSE,4HYOKE,4H AND,4H L*2037190
12         8AP,4H BEL,4HT US,1HE/                          *2037200
13         COMMON/IO/INN                                    *2037205
14         PRINT 9901                                       *2037210
15         PR = 1.                                          *2037220
16         DO 40 I=1,3                                      *2037230
17         READ (INN,9900)PI,QI,AA                          *2037240
18 9900    FORMAT (2E10.0,6A4)                              *2037250
19         IF (QI.EQ.0.) GO TO 30                           *2037260
20         J = 6.*QI                                        *2037270
21         K = J-6                                          *2037280
22         DO 20 L=1,6                                      *2037290
23         M = L+K                                          *2037300
24 20      AA(L) = A(M,I)                                    *2037310
25 30      PRINT 9902,I,(AA(J),J=1,6),PI                   *2037320
26 40      PR = PR*PI                                        *2037330
27         PRINT 9903,PR                                     *2037340
28 9901    FORMAT (1H0,/,45X25HPROBABILITY OF OCCURRENCE//24X42HTHE PROBABILI*2037350
29         TY OF OCCURRENCE IS BASED ON://)                 *2037360
30 9902    FORMAT (1H0,8X11,17H. PROBABILITY OF ,6A4,2H =,F8.4) *2037370
31 9903    FORMAT (1H0,/,30X28HPROBABILITY OF OCCURRENCE = ,F8.4) *2037380
32         RETURN                                           *2037390
33         END                                              *2037400

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Subroutine PAGE4

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1
2          SUBROUTINE RELSEL(ZP,K,ZPP)
3          COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,BBB,IGNORE,DA,XSMALA,YSMAL *2D13080
4          1A,XI SMLA,PSIA,SPSIA,CPSIA,FMUA,SIGMAA,SIGMA,AA,KTABLE,MFORI,DTR,PI *2D13090
5          2TWO,GRAVIT,CPRIME,BIGKI,EL,AR,TPRIME,ALFAI,OMEGAI,RPSI,RHO,THETAZ, *2D13100
6          3STHETZ,CTHETZ,FSPRM,RH,THATPV,WZERO,RHOPTZ,RHOFPZ,GAMZFR,LCONTL,CS *2D13110
7          4,S,FMUS,BETA,ZZERO,ELTWTY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NPASGR *2D13120
8          5,XPACZ,NBELT,APRNTC,TIMAX,DTPRNT,UPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA *2D13130
9          6,E LAMB,TIME,IBUG,MAXR,LITGAP,EPSLNZ,RSEL,RVEL,IBIG,IFORK,BASIC,FS, *2D13140
10         7SMALLF,ZVEC,ZVECP,ZVECPP,THEDSQ,CTHETA,STHETA,          BIGMI,TMATII, *2D13150
11         8XIDOT,YIDOT,PHI,EONE,SDELTA,SDELTD,BL,PN,MODE,OMEGA,X,Y,THEFEE,RH *2D13160
12         9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOLD,DELDOO,EPSLNY,FTOLD,FSPRMZ *2D13170
13         COMMON CZERON,CONEN,CTWON,ET,EHAT,GEE,SMALLB,AEL,TIMTJZ,TGAMZ,YZZE *2D13180
14         1RO,F SZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,BVFLB,CVELC,AACCA, *2D13190
15         2BACCB,CACCC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSQI,ATDSO,TIMT *2D13200
16         3J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TSA,TSB,SIGMAC,ITAU,TAUHAT,RZ,SZ *2D13210
17
18
19         DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),RETA(3),PHIZ(3),DELTA(3) *2D13220
20         1),PHI(3),SDELTA(3),SDELTD(3),FLAMB(6),MFORI(7),CPRIME(7),BIGKI(7), *2D13230
21         2TPRIME(7),ALFAI(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR( *2D13240
22         38),RHO(8),THETAZ(8),STHETZ(8),CTHETZ(8),IBIG(8),THEDSQ(8),CTHETA(8) *2D13250
23         4),STHETA(8),          BIGMI(8),TMATII(8),PHOPRM(8),XPRM(8),YPRM(8) *2D13260
24         5,TDSQI(8),ATDSQ(8),IGNORE(10),DA(10),XSMALA(10),YSMALA(10),XI SMLA *2D13270
25         6(10),PSIA(10),CPSIA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),RF *2D13280
26         7E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11) *2D13290
27         8),ZVECPP(11),STIMTJ(13),AEL(14),RSEL(15),RVEL(16),MODE(16),TIMTJZ( *2D13300
28         916),TIMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EONE(18),PN(18) *2D13310
29         DIMENSION DELDLD(18),DELDOO(18),EPSLNY(18),FTOLD(18),OMEGA(18),CZF *2D13320
30         1RON(18),CONEN(18),CTWON(18),ET(18),EHAT(18),IFORK(3,8),SIGMA(10,3) *2D13330
31         2,XXX(300,3),YYY(300,3),FMM(300,3),BBB(300,3),          SIGMAA(10,1) *2D13340
32         30),AA(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,128),BASIC(11,8),KTAR *2D13350
33         4LE(2,14),ZPPP(128),BL(3)
34
35         COMMON THATPW,THATPX,THATPS,XVEHZ
36         COMMON FARB(18),SLOPE(18),ISWT(18),LOADSWT(18)
37         COMMON NONQ(1402)
38         DIMENSION ZP(11)
39         CALL RELVEL(K,ZP,ZPP)
40         IF (K-8) 100,100,5C
41         50 ZPP = ZPP + BASIC(11,K-8)
42         100 RETURN
43         END

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Subroutine RELSEL

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1 SUBROUTINE RELVEL(K,ZP,RV)
2 COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,BRB,IGNORF,DA,XSMALA,YSMAL,*2013510
3 *2013520
4 1A,XISMLA,PSIA,SPSIA,CPSIA,FMAA,SIGMA,AA,KTABLE,MFORI,DIR,PI,*2013540
5 2TWO,GRAVIT,CPRIME,BIGKI,BEL,ALFAT,PRIME,ALFAT,OMEGAI,RPSI,RHJ,THETAZ,*2013550
6 3STHEZ,CTHEZ,FSPR,RH,THATPV,WZRO,RHOPT,GAMZER,LCONTL,CS,*2013560
7 4,S,FMS,BETA,ZZERO,ELTWY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NPASGR,*2013570
8 5,XPACZ,NBELT,APRNTD,TIPAX,DTPRT,HPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA,*2013580
9 6,ELAMB,TIME,IRUG,MAXR,LITGAM,EPSLNZ,RSEL,RVEL,IRIG,IFORK,RASIC,FS,*2013590
10 7SMALLF,ZVEC,ZVECP,ZVECP,THEDSO,CTHETA,STHETA, HIGMI,TMATII,*2013600
11 8XIDDOT,YIDOT,PHI,EDNE,SDELTA,SDELTD,BL,PN,MODE,OMEGA,X,Y,THEFEE,RH,*2013610
12 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELJLD,DELOD,EPSLNY,FTOLD,FSPRMZ *2013620
13 COMMON,CZE,RON,CGNEN,CTWON,ET,EHAT,GEF,SMALLR,AEL,TIMTJZ,TGAMZ,YZFE,*2013630
14 1RO,FZCNS,ANVERS,TINFL,KPOST,TPRINT,JSTEP,AVELA,RVELR,CVFLC,AA,CCA,*2013640
15 2BACCB,CACCC,DACCC,MAXI,KPRINT,KSTEP,KINFL,TIMASK,IDSQI,AIDSO,TIMT,*2013650
16 3J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TS,TSB,SIGMAC,ITAU,TAUHAT,RZ,SZ *2013660
17 *2013670
18 *2013680
19 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3)*2013690
20 1),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),BIGKI(7),*2013700
21 2TPRIME(7),ALEAI(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),FL(8),AR,*2013710
22 3B),RHO(8),THETAZ(8),STHEZ(8),CTHEZ(8),IBIG(9),THEDSO(8),CTHETA(8)*2013720
23 4),STHETA(8), HIGMI(8),TMATII(8),RHOPRM(8),XPRM(8),YPRM(8)*2013730
24 5,TDSQLI(8),AIDSQ(8),IGNDRE(10),DA(10),XSMALA(10),YSMALA(10),XISMLA,*2013740
25 6(10),PSIA(10),CPSIA(10),SPSIA(10),SIGMAC(10),FMAA(10),GRAVA(10),BE,*2013750
26 7(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLR(10),ZVEC(11),ZVECP(11)*2013760
27 8),ZVECP(11),STIMTJ(11),AEL(14),RSEL(15),RVEL(16),MODE(16),TIMTJZ,*2013770
28 9(16),TIMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EONE(18),PM(18) *2013780
29 DIMENSION DELOD(18),DELOD(18),EPSLNY(18),FTOLD(18),OMEGA(18),CZF,*2013790
30 1RON(18),CONEN(18),CTWON(18),ET(18),EHAT(18),IFORK(18),SIGMA(10,3)*2013800
31 2,XXX(300,3),YYY(300,3),FMM(300,3),RBR(300,3),
32 30),AA(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,1,2,8),BASIC(11,8),KTAB,*2013820
33 4LE(2,14),ZPPP(128),BL(3) *2013830
34 *2013840
35 COMMON THATPM,THATPX,THATPS,XVEHZ
36 COMMON FAR(18),SLOPE(18),ISWT(18),LOJ,SWT(18)
37 COMMON,NONO(1402)
38 DIMENSION ZP(11)
39 IF (K-8) 10,20,30
40 M = MFORI(K)
41 RV = ZP(M) - ZP(K)
42 GO TO 900
43 RV = ZP(9) - ZP(11)
44 GO TO 900
45 30 II = IFORK(1,K-8)
46 IF (II) 40,900,40
47 IA = IFORK(2,K-8)
48 TS = (ZP(9) - ZP(11))*CPSIA(IA) + ZP(10)*SPSIA(IA)
49 GO TO (100,900,300,400,900,700,800),II
50 RV = TS + AR(11)*ZP(1)

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Subroutine RELVEL (page 1 of 2)


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51      GO TO 900
52      RV = TS + BASIC(1,K-R)*ZP(1)+BASIC(2,K-R)*ZP(2)+BASIC(3,K-R)*ZP(3)
53      GO TO 900
54      RV = TS + BASIC(1,K-R)*ZP(1)+BASIC(2,K-R)*ZP(2)+BASIC(3,K-R)*ZP(3)
55      1+BASIC(11,K-R)*ZP(11)
56      GO TO 900
57      RV = TS + BASIC(1,K-R)*ZP(7)
58      GO TO 900
59      RV = TS+BASIC(1,K-R)*ZP(7)+BASIC(2,K-R)*ZP(8)
60      RETURN
61      END

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*ZD14010
*ZD14020
*ZD14030
*ZD14040
*ZD14050
*ZD14060
*ZD14070
*ZD14080
*ZD14090
*ZD14100
*ZD14110

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1 SUBROUTINE SEAT
2 *2D23070
3 COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,RRR,IGNIRE,DA,XSMALA,YSMAL,*2D23090
4 1A,XI,SMLA,PSIA,SPSIA,CPSIA,FMUA,SIGMAA,SIGMA,AA,XTABLE,MFOR1,DTR,PI,*2D23100
5 2IWO,GRVIT,CPRIME,RIGKI,EL,AR,TPRIME,ALFAT,OMEGAI,RPSI,RHO,THETAZ,*2D23110
6 3STHETZ,CTHETZ,FSPRM,RH,THATPV,ZERO,RHOPTZ,RHOPEZ,GAMZER,LCONTL,CS,*2D23120
7 4S,FMJS,BETA,ZZERO,ELTWTY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NPASGR,*2D23130
8 5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,BPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA,*2D23140
9 6,ELAMB,TIME,IRUG,MAXR,LITGAM,FPSLVZ,RSEL,RVEL,IRIG,IFORK,BASIC,FS,*2D23150
10 7SMALLF,ZVEC,ZVECP,ZVEDCP,ATHEDSQ,CTHETA,STHETA, RIGMI,TMATI,*2D23160
11 8XIDOT,YIDOT,PHI,EDNE,SDELTA,SDELTA,SDELTA,BL,PN, MUDE,OMEGA,X,Y,THEFFE,PH,*2D23170
12 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOLD,DELODD,FPSLNY,FTOLD,FSPRMZ *2D23180
13 COMMON CZE,ROM,CONE,CTWON,ET,FHAT,GEE,SMALLR,AEL,TMTJZ,TGANZ,YZ7E,*2D23190
14 1RO,F SZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,VELR,CVELC,AAACCA,*2D23200
15 2BACCB,CACCC,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSQL,ATDSQ,TMT,*2D23210
16 3J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,ISA,TSR,SIGMAC,ITAU,TAUHAT,RZ,S7 *2D23220
17 *2D23230
18 *2D23240
19 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),RFTA(3),PHIZ(3),DELTA(3)*2D23250
20 1),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFOR1(7),CPRIME(7),RIGKI(7),*2D23260
21 2TPRIME(7),ALFAT(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR(*2D23270
22 3R),RHO(8),THETAZ(8),STHETZ(8),CTHETZ(8),IRIG(8),ATHEDSQ(8),CTHETA(*2D23280
23 4),STHETA(8), RIGMI(8),TMATI(8),RHOPRM(8),XPRM(8),YPRM(8)*2D23290
24 5,TOSQLI(4),ATDSQ(8),IGNORE(10),ADA(10),XSMALA(10),YSMALA(10),XISMLA,*2D23300
25 6(10),PSIAL(10),CPSIAL(10),SIGMAC(10),FMUA(10),GRAVAL(10),RE,*2D23310
26 7E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALB(10),ZVEC(11),ZVECP(11)*2D23320
27 8),ZVECP(11),STIMTJ(13),AEL(14),RSEL(16),RVEL(16),MODE(16),TMTJZ,*2D23330
28 916),TMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EONE(18),PN(18) *2D23340
29 DIMENSION DELODD(18),DELODD(18),EPSLNY(18),FTOLD(18),OMEGA(19),CZF,*2D23350
30 1RON(18),CONE(18),CTWON(18),ET(18),EHAT(18),IFORK(18),SIGMA(10,3)*2D23360
31 2,XXX(300,3),YYY(300,3),FMM(300,3),BRBT(300,3), SIGMAA(10,1)*2D23370
32 30),AA(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,128),BASIC(11,8),KTA,*2D23380
33 4LE(2,14),ZPPP(128),BL(3) *2D23390
34 *2D23400
35 *2D23410
36 *2D23420
37 *2D23430
38 *2D23440
39 *2D23450
40 *2D23460
41 *2D23470
42 *2D23480
43 *2D23490
44 *2D23500
45 *2D23510
46 *2D23520
47 *2D23530
48 *2D23540
49 *2D23550
50 *2D23560
SUBROUTINE SEAT (page 1 of 2)

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51 FS = WZER0 - CS*YSP - SUMRY
52 IF (FS) 4130,4140,4140
53 4130 FS = 0.
54 4140 ZMLCTS = Z - EL(7)*CTHETA(7)
55 IF (ZMLCTS) 4142,4142,4144
56 4142 TANTSV = STHETA(7)/CTHETA(7)
57 FSPRM = FSZCNS-S*(ZVEC(10))+Z*TANTSV
58 IF (FSPRM) 4150,4150,4143
59 4143 DEE(7) = FSPRM/CTHETA(7)*Z/CTHETA(7)
60 DEE(9) = -FSPRM*TANTSV
61 GO TO 4155
62 4144 FSPRM=FSZCNS-S*(ZVEC(10))+EL(7)*STHETA(7)+ZMLCTS*TANTEG)
63 IF (FSPRM) 4150,4150,4146
64 4146 DEE(7)=EL(7)*FSPRM*CTHETA(7)+STHETA(7)*TANTEG)
65 DEE(8) = FSPRM/CTHETA(8)*ZMLCTS/CTHETA(8)
66 DEE(9)=-FSPRM*TANTEG
67 GO TO 4155
68 4150 FSPRM = 0.
69 4155 DEE(10) = FS+FSPRM
70 IF(ZVEC(8)-GE.0.) GO TO 4170
71 XZ=(YZZER0-ZVEC(10))-EL(7)*STHETA(7))/TANTEG-ZMLCTS
72 IF (XZ-RZ) 4160,4170,4170
73 4160 FZ = SZ*(RZ-XZ)
74 DEE(7)=DEE(7)-FZ*EL(7)*(STHETA(7)+CTHETA(7)/TANTEG)
75 DEE(8)=DEE(8)+FZ/STHETA(8)*(ZVEC(10)+EL(7)*STHETA(7)-YZZER0)
76 1/STHETA(8)
77 DEE(9) = DEE(9)+FZ
78 DEE(10) = DEE(10)-FZ/TANTEG
79 GO TO 4180
80 FZ = 0.
81 4180 SMALLF = (FS+FSPRM)*FMUS
82 4190 IF (IRUG-2) 4194,4192,4192
83 4192 WRITE(6,9951)Z,FS,FSPRM,FZ,SMALLF,SUMRY,ZMLCTS
84 9951 FORMAT (GH0SEAT 7E17.8)
85 4194 RETURN
86 END

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```

*2D2357J
*2D2354J
*2D23500
*2D23600
*2D23610
*2D23620
*2D23630
*2D23640
*2D23650
*2D23660
*2D23670
*2D23690
*2D23690
*2D23700
*2D23710
*2D23720
*2D23730
*2D23740
*2D23750
*2D23760
*2D23770
*2D23780
*2D23790
*2D23800
*2D23810
*2D23820
*2D23830
*2D23840
*2D23850
*2D23860
*2D23870
*2D23880
*2D23890
*2D2390J
*2D23910
*2D23920

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1
2 SUBROUTINE SIPP(IPAGE,K,THETA,STIME) *2035080
3 COMMON/INJ/HFA(200),HLA(200),CFA(200),CKF(200),CCF(200,4),IDATE(3) *2035090
4 L,MM,MN,BELTA(200),BELTB(200),BELTC(200),CUA(200),NPROB *2035110
5 DIMENSION STIME(200),THETA(200,3,8),TOL(22),ITOL(14),B(4,2),C(3,7) *2035120
6 DATA TOL/1000.,2000.,1800.,1800.,5000.,1500.,45.,25. *2035130
7 1,0.,45.,30.,60.,60.,0.,0.,120.,20.,20.,60.,190.,135.,135./ *2035140
8 DATA B/4HFLEX,3HION,2*1H,4HHYPE,4HREXT,4HENSI,2MON/ *2035150
9 DATA C/3HHIP,2*1H,4HLOWE,4HR SP,3HINE,4HUPPE,4HR SP,3HINE,4HNECK, *2035160
10 12*1H,4HSHOU,4HLDER,1H,4HELBO,1HW,1H,4HKNEE,2*1H / *2035170
11 COMMON/IO/INN *2035175
12 100 READ(INN,9999)CI,TSA *2035180
13 9999 FORMAT(2E10.0) *2035190
14 IF(CI.LE.0) GO TO 110 *2035200
15 I=CI+.5 *2035210
16 TOL(I)=TSA *2035220
17 GO TO 100 *2035230
18 110 PRINT 9998,IDATE,IPAGE *2035240
19 LINE = 2 *2035250
20 9998 FORMAT(1H1,28X52HTWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT *2035260
21 IDATA,20X3A4,11X4HPAGE,I3) *2035270
22 DO 120 I=1,8 *2035280
23 120 ITOL(I) = TOL(I) *2035290
24 PRINT 9010,(ITOL(I),I=1,4) *2035300
25 PRINT 9011,(ITOL(I),I=5,8) *2035310
26 PRINT 9012 *2035320
27 PRINT 9013 *2035330
28 PRINT 9014 *2035340
29 9010 FORMAT(1H0,35X49HSUMMARY OF TOLERANCE DATA USED IN INJURY CRITERIA *2035350
30 1A//13X8HQANTITY,11X24HMAXIMUM ACCEPTABLE VALJE,13X24HNATURE OF IN *2035360
31 2JURY OR DATA,12X14HWEIGHTING CODE//4X17H1. SEVERITY INDEX,14X2H1., *2035370
32 3I5,17X43H1. INTERNAL HEAD INJURY. DANGEROUS TO LIFE.,6X8H1. 22/26/ *2035380
33 44X33H2. HEAD PITCH ACCELERATION 2.,15,12H RAD/SEC/SEC,5X37H2. *2035390
34 550% CHANCE OF CEREBRAL CONCUSSION.,12X8H2. 12/26/ *2035400
35 64X13H3. CHEST LOAD,18X2H3.,15,3H LB,14X27H3. RIB FRACTURE OF CADAV *2035410
36 7ER,22X8H3. 13/26/4X21H4. SHOULDER BELT LOAD,10X2H4.,15, 12H LB COM *2035420
37 8BINED,5X44H4. PREDICTED TOLERANCE LEVEL WITHOUT INJURY.,5X8H4. 1/ *2035430
38 926) *2035440
39 9011 FORMAT(4X19H5. PELVIC BELT LOAD,12X2H5.,15,3H LB,14X26H5. MAXIMUM *2035450
40 1 VOLUNTARY LOAD.,23X8H5. 1/26/4X19H6. KNEE LOAD (EACH),12X2H6.,15 *2035460
41 2,3H LB,14X31H6. COMMINUTED PATELLA FRACTURE.,18X8H6. 12/26/ *2035470
42 34X19H7. CHEST A-P G-LOAD,12X *2035480
43 52H7.,15,7H G-PEAK,10X33H7. VOLUNTEER DATA WITH NO INJURY.,16X8H7. *2035490
44 6 4/26/62X39H(DURATION=.09 SEC, RISE TIME=500 G/SEC)/62X41HHIGHER R *2035500
45 7ISE TIMES OR LONGER DURATIONS CAN/62X34HDECREASE THIS VALUE SIGNIF *2035510
46 8ICANTLY./4X19H8. CHEST S-I G-LOAD,12X2H8.,15,7H G-PEAK,10X38H8. VO *2035520
47 9LUNTEER DATA. FRACTURED VERTEBRAE,11X8H8. 16/26) *2035530
48 9012 FORMAT(1H0,//51X18HLIST OF REFERENCES/// *4*2035540
49 1X17H1. GADD, C.W., *USE OF A WEIGHTED-IMPULSE CRITERION FOR ESTIM *2035550
50 2ATING INJURY HAZARD*, PROC. 10TH. STAPP CAR CRASH CONF.,/7X20HNOV. *2035560

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51 3 1966, P.95-100./4X108H2. OMMAYA, A.K. ET AL, "COMPARATIVE TOLERANCE*2D35570
52 AGES FOR CEREBRAL CONCUSSION BY HEAD IMPACT AND WHIPLASH INJURY IN/*2D35580
53 5X100PRIMATES", 1970 INTERNATIONAL AUTOMOBILE SAFETY CONFERENCE C*2D35590
54 COMPENDIUM, SAE PUB. NO. P-30, P.808-817.) *2D35600
55 9013 FORMAT (4X112H3. GADD, C.M. AND PATRICK, L.M., "SYSTEM VERSUS LABO*2D35610
56 LABORATORY IMPACT TESTS FOR ESTIMATING INJURY HAZARD", SAE PAPER/7X22H*2D35620
57 2ND. 680053, JAN. 1968./4X119H4. "ESTIMATED PROBABLE THRESHOLD OF*2D35630
58 3 INJURY BY BIOMECHANICS TASK FORCE OF SAE OCCUPANT RESTRAINT SYSTE*2D35640
59 4MS SURCOMMITTEE./4X108H5. STAPP, J.P. AND ENFIELD, D.L., "EVALUATI*2D35650
60 5OM OF THE LAP-TYPE AUTOMOBILE SAFETY BELT WITH REFERENCE TO HUMAN/*2D35660
61 6TX36HTOLERANCE", SAE PAPER NO. 62A, 1958./4X115H6. SNYDER, R.G., **2D35670
62 7HUMAN IMPACT TOLERANCE", 1970 INTERNATIONAL AUTOMOBILE SAFETY CONF*2D35680
63 REFERENCE COMPENDIUM, SAE PUB. NO./7X16HP-30, P.712-782./4X8H7. IRIID.*2D35690
64 9/4X8H8. IBID./)) *2D35700
65 9014 FORMAT (4X106HNOTE: THE WEIGHTING CODE IS BASED ON VAN KIRK, D.J. *2D35710
66 LAND LANGE, W.A., "A DETAILED INJURY SCALE FOR ACCIDENT/10X84HINVES*2D35720
67 2TIGATION", PROC. OF THE 12TH. STAPP CAR CRASH CONFERENCE, OCT. 196**2D35730
68 38, P.240-259./10X86MINOR INJURY = 1-4/26, MODERATE INJURY = 8-10/*2D35740
69 426, MODERATELY SEVERE INJURY = 12-14/26,/10X,78HSEVERE INJURY = 16*2D35750
70 5-18/26, CRITICAL INJURY = 20-22/26, FATAL INJURY = 24-26/26.) *2D35760
71 IPAGE = IPAGE+1 *2D35770
72 DO 130 I=1,7 *2D35780
73 RTM=A *2D35790
74 J=I+1 *2D35795
75 ITOL(J)=TOL(I+15) *2D35800
76 ITOL(J-1)=TOL(I+8) *2D35810
77 PRINT 9998, I, DATE, IPAGE *2D35820
78 PRINT 9001, (ITOL(I), I=1,14) *2D35830
79 5001 FORMAT (1H0,32X56HSUMMARY OF ANGULAR MOTION LIMITS USED IN INJURY *2D35840
80 1CRITERIA//36X5HJOINT,15X7HFLEXION,10X14HHYPEREXTENSION/32X6H1. HI*2D35850
81 2P,17X14,4H DEG,13X14,4H DEG/32X14H2. LOWER SPINE,9X14,4H DEG,13X14*2D35860
82 3,4H DEG/32X14H3. UPPER SPINE,9X14,4H DEG,13X14,4H DEG/32X7H4. NECK*2D35870
83 4,16X14,4H DEG,13X14,4H DEG/32X11H5. SHOULDER,12X14,4H DEG,13X14,4H*2D35880
84 5 DEG/32X8H6. ELBOW,15X14,4H DEG,13X14,4H DEG/32X7H7. KNEE,16X14,4H*2D35890
85 6 DEG,13X14,4H DEG/19X81HNOTE: ALL QUANTITIES MEASURED FROM AN ERE*2D35900
86 7CT STANDING POSITION WITH ARMS AT SIDES.) *2D35910
87 TOL(9)=90.-TOL(9) *2D35920
88 TOL(14)=90.-TOL(14) *2D35930
89 TOL(15)=90.-TOL(15) *2D35940
90 TOL(16)=TOL(16)-90. *2D35950
91 TOL(21)=TOL(21)-90. *2D35960
92 TOL(22) = TOL(22)-90. *2D35970
93 9997 FORMAT (1H0,39X42HSUMMARY OF QUANTITIES EXCEEDING TOLERANCES//11X8*2D35980
94 1HQUANTITY,14X37HPEAK TIME OF OCCURRENCE DURATION,7X10HTIME ST*2D35990
95 2ARY,7X27HTIME END WEIGHTING CODE//) *2D36000
96 ISMT=0 *2D36010
97 L=0 *2D36020
98 SI=0. *2D36030
99 DO 550 J=1,15 *2D36040
100 IF (J.EQ.4) L=L+1 *2D36050

```

Subroutine SIPP (page 2 of 5)

```

101 PVAR=0.
102 TSR=0.
103 TUN=0.
104 ISUN=0
105 DU 540 I=1,K
106 JJ = J
107 GO TO (21J,220,230,240,250,260,270,280,290,300,310,320,330)
108 11),J
109 IF (I.VF.1) SI=SI+(STIME(I)-STIME(I-1))*ABS(HFA(I))*2.5
110 VAR=SI
111 GO TO 330
112 VAR=THETA(I,3,4)*.C1745329
113 GO TO 330
114 IF (MM.LE.0) GO TO 550
115 VAP=CCF(I,L)
116 GO TO 330
117 VAR=BELTR(I)*BELTC(I)
118 GO TO 330
119 VAR=BELTA(I)
120 GO TO 330
121 IF (MN.LE.0) GO TO 550
122 VAR=CKF(I)
123 GO TO 330
124 VAR=CFALL)
125 GO TO 330
126 VAR = CUA(I)
127 GO TO 330
128 VAR = THETA(I,1,1)-THETA(I,1,7)-90.
129 GO TO 327
130 VAR = THETA(I,1,J-8)-THETA(I,1,J-9)
131 GO TO 327
132 VAR = THETA(I,1,3)-THETA(I,1,5)-180.
133 GO TO 327
134 VAR = THETA(I,1,3*J-37)-THETA(I,1,J-8)+90.
135 IF (VAR.LT.0.) JJ=J+7
136 TSA=ABS(VAR)
137 IF (TSA.LF.TOL(JJ)) GO TO 350
138 IF (ISON.NE.0) GO TO 340
139 ISUN=1
140 IF (I.EQ.1) GO TO 340
141 TON=STIME(I)-(STIME(I)-STIME(I-1))/(TSA-PVAR)*(TSA-TOL(JJ))
142 IF (TSA.LE.TSR) GO TO 535
143 TSB=TSA
144 PEAK=VAR
145 PTIM=STIME(I)
146 GO TO 535
147 IF (ISON.EQ.0) GO TO 535
148 ISON=0
149 TOF=STIME(I)-(STIME(I)-STIME(I-1))/(PVAR-TSA)*(TOL(JJ)-TSA)
150 DUR=TOF-TON

```

```

*2036060
*2036070
*2036080
*2036090
*2036100
*2036110
*2036120
*2036130
*2036140
*2036150
*2036160
*2036170
*2036180
*2036190
*2036200
*2036210
*2036220
*2036230
*2036240
*2036250
*2036260
*2036270
*2036280
*2036290
*2036300
*2036310
*2036320
*2036330
*2036340
*2036350
*2036360
*2036370
*2036380
*2036390
*2036400
*2036410
*2036420
*2036430
*2036440
*2036450
*2036460
*2036470
*2036480
*2036490
*2036500
*2036510
*2036520
*2036530
*2036540
*2036550

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```

151 IF (ISMT.NF.0) GO TO 300
152 ISMT=1.
153 IPAGE = IPAGE+1
154 PRINT 9998, IDATE, IPAGE
155 PRINT 9997
156 LINE = 7
157 IF (LINE.GT.60) GO TO 360
158 JL=2
159 IF (JJ.LT.16) JL=1
160 GO TO (41J,42J,43J,44J),450,460,470,480,500,520,520,520,500,500,500
161 JL,J
162 410 PRINT901,PEAK,PTIM,DUR,TON,TOF
163 5901 FORMAT (3X19HHEAD SEVERITY INDEX,7XF9.0,4F16.6,10X5H22/26)
164 GO TO 530
165 420 PRINT 9502,PEAK,PTIM,DUR,TON,TOF
166 5902 FORMAT (3X23HHEAD PITCH ACCELERATION,3XF9.0,4F16.6,10X5H12/26)
167 GO TO 530
168 430 PRINT 9903,PEAK,PTIM,DUR,TON,TOF
169 5903 FORMAT (3X10HCHEST LOAD,16XF9.0,4F16.6,10X5H13/26)
170 GO TO 530
171 440 PRINT 9904,PEAK,PTIM,DUR,TON,TOF
172 5904 FORMAT (3X18HSHOULDER BELT LOAD,9XF9.0,4F16.6,11X4H1/26)
173 GO TO 530
174 450 PRINT 9905,PEAK,PTIM,DUR,TON,TOF
175 5905 FORMAT (3X16HPELVIC BELT LOAD,10XF9.0,4F16.6,11X4H1/26)
176 GO TO 530
177 460 PRINT 9906,PEAK,PTIM,DUR,TON,TOF
178 5906 FORMAT (3X16HKNEE LOAD (EACH),10XF9.0,4F16.6,10X5H12/26)
179 GO TO 530
180 470 PRINT 9907,PEAK,PTIM,DUR,TON,TOF
181 5907 FORMAT (3X16HCHEST A-P G-LOAD,10XF9.0,4F16.6,11X4H4/26)
182 GO TO 530
183 480 PRINT 9908,PEAK,PTIM,DUR,TON,TOF
184 5908 FORMAT (3X16HCHEST S-I G-LOAD,10XF9.0,4F16.6,10X5H16/26)
185 GO TO 530
186 PEAK = 50.-PEAK
187 PEAK = ABS(PEAK)
188 PRINT 9910, (C(M,J-8),M=1,3), (8(L,JL),L=1,4), PEAK, PTIM, DUR, TON, TOF
189 9910 FORMAT (3X7A4,F7.0,4F16.6,10X5H-----)
190 TSR=0.
191 LINE = LINE+1
192 PVAR=ISA
193 540 CONTINUE
194 IF (J.NE.4) GO TO 550
195 IF (MM.GE.L) GO TO 200
196 550 CONTINUE
197 IPAGE=IPAGE+1
198 IF (MPROB.NF.0) RETURN
199 PRINT 9998, IDATE, IPAGE
200 CALL PAG-4

```

*2037060
*2037070
*2037080

IPAGE = IPAGE+1
RETURN
END

201
202
203


```

1  SUBROUTINE STYX
2  DIMENSION XJOINT(9),YJOINT(9),ZVEFC(8),XLEN(8),YLEN(8),N(
3  18),XMAN(64),YMAN(64),IMAGE(1500),NSCALE(5),JOINT(5),STEPS(200)
4  2,VZERO(50),HZERO(130),ZERO(130)
5  DIMENSION NCNCT(8),XHIP(5),YHIP(5),XCHT(6),YCHT(6),XELR(3),
6  1YELR(3),XHND(5),YHND(5),XKNE(3),YKNE(3),XFT(5),YFT(5)
7  DIMENSION IDATE(3)
8  COMMON XLAP(2),YLA(2),YL(2),YL(2),XU(1),YU(1),XFLDOR(2),YFLDOR(2)
9  1,XSEAT(3),YSEAT(3),XR(2),YR(2),XUSDF(2),YUSDF(2),XMS(2),YMS(2),
10  2,XLSM(2),YLSM(2),XLP(2),YLP(2),XSC(2),YSC(2),XTDE(2),YTDE(2),
11  3POST(200,9),THETA(200,3,8),AR(8),RHOPFZ,RHOPF7,CPSIA(10),
12  4SPSIA(10),CA(10),TGAMZ,ZZERO,PHI(200),PHI2(200),PHI3(200),
13  5RL1(200),RL2(200),RL3(200),IPAGE,STIME(200),NHET,IGNORE(10),
14  6ELR(8),KTOTAL
15  COMMON/IO/ INN
16  DATA JOINT/1H1,1H2,1H3,1H4,1H5,1H6,1H7,1H8/
17  READ (INN,9999)NHL,NSRH,NVL,NSBV,IZERO,ISTEP,MFTH
18  READ (INN,9998)XMIN,XMAX,YMIN,YMAX,FIRST,DELTA
19  ISTEP = MINO(ISTEP,200)
20  IF (MFTH.EQ.0) GO TO 4010
21  STEPS(1) = FIRST
22  DO 4000 I=2,ISTEP
23  4000 STEPS(I) = STEPS(I-1) + DELTA
24  GO TO 4030
25  4010 DO 4020 I=1,ISTEP
26  4020 READ (INN,9992)STEPS(I)
27  4030 READ (INN,9995)NCNCT
28  CALL DATE( IDATE)
29  NCHAR=0
30  LABEL=0
31  INT=4
32  PTLEN=.25
33  ANG=45.
34  NSCALE(1)=0
35  MSRH = NSRH*(NHL-1)
36  MSBV = NSBV*(NVL-1)
37  RNSBH = MSBH + NHL
38  RNSBV = MSBV + NVL
39  L = 1
40  IF (HZERO.NE.C) GO TO 7
41  DO 6 I=1,110
42  ZERO(I) = 0.0
43  VZERO(I) = YMIN
44  HZERO(I) = XMIN
45  VLINE = (YMAX - YMIN)/RNSRH
46  HLINE = (XMAX - XMIN)/RNSBV
47  DO 3 I=2,MSRH
48  3 VZERO(I) = VZERO(I-1) + VLINE
49  DO 5 I=2,MSBV
50  5 HZERO(I) = HZERO(I-1) + HLINE

```

Subroutine STYX (page 1 of 5)

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51 SCALEY = (YMAX - YMIN)/(RNSDH/6.)
52 SCALEX=(XMAX-XMIN)/(RNSBV/10.)
53 XFLUOR(2) = XFLUOR(1) - DA(1)*CPSIA(1)
54 YFLUOR(2) = YFLUOR(1) - DA(1)*SPSIA(1)
55 XSEAT(2) = XSEAT(1) - DA(2)*CPSIA(2)
56 YSEAT(2) = YSEAT(1) - DA(2)*SPSIA(2)
57 XSEAT(3) = XSEAT(1) + ZZERO
58 YSEAT(3) = YSEAT(1) + ZZERO*TGAMZ
59 XR(2) = XR(1) - DA(3)*CPSIA(3)
60 YR(2) = YR(1) - DA(3)*SPSIA(3)
61 XUSDF(2) = XUSDF(1) - DA(4)*CPSIA(4)
62 YUSDF(2) = YUSDF(1) - DA(4)*SPSIA(4)
63 XWS(2) = XWS(1) - DA(5)*CPSIA(5)
64 YWS(2) = YWS(1) - DA(5)*SPSIA(5)
65 XLSW(2) = XLSW(1) - DA(6)*CPSIA(6)
66 YLSW(2) = YLSW(1) - DA(6)*SPSIA(6)
67 XLP(2) = XLP(1) - DA(7)*CPSIA(7)
68 YLP(2) = YLP(1) - DA(7)*SPSIA(7)
69 XSC(2) = XSC(1) - DA(8)*CPSIA(8)
70 YSC(2) = YSC(1) - DA(8)*SPSIA(8)
71 XTOE(2) = XTOE(1) - DA(9)*CPSIA(9)
72 YTOE(2) = YTOE(1) - DA(9)*SPSIA(9)
73 XLAP(1) = -XLAP(1)
74 YLAP(1) = -YLAP(1)
75 DD 110 K=1,KTOTAL
76 IF (K.EQ. KTOTAL) GO TO 4
77 IF (STEPSIL) .GT. (STIME(K)+STIME(K+1))/2.) G) TO 110
78 XJOINT(1) = POST(K,1)
79 YJOINT(1) = POST(K,4)
80 DO 1 I=1,8
81 DTR=THETA(K,1)*.0174532925
82 CZVEC(1)=COS(DTR)
83 SZVEC(1)=SIN(DTR)
84 XJOINT(2) = XJOINT(1) + EL(1)*CZVEC(1)
85 XJOINT(3) = XJOINT(2) + EL(2)*CZVEC(2)
86 XJOINT(4) = XJOINT(3) + EL(3)*CZVEC(3)
87 XJOINT(5) = XJOINT(4) + EL(4)*CZVEC(4)
88 XJOINT(6) = XJOINT(5) + EL(5)*CZVEC(5)
89 XJOINT(7) = XJOINT(6) + EL(6)*CZVEC(6)
90 XJOINT(8) = XJOINT(7) + EL(7)*CZVEC(7)
91 XJOINT(9) = XJOINT(8) + EL(8)*CZVEC(8)
92 YJOINT(2) = YJOINT(1) + EL(1)*SZVEC(1)
93 YJOINT(3) = YJOINT(2) + EL(2)*SZVEC(2)
94 YJOINT(4) = YJOINT(3) + EL(3)*SZVEC(3)
95 YJOINT(5) = YJOINT(4) + EL(4)*SZVEC(4)
96 YJOINT(6) = YJOINT(5) + EL(5)*SZVEC(5)
97 YJOINT(7) = YJOINT(6) + EL(6)*SZVEC(6)
98 YJOINT(8) = YJOINT(7) + EL(7)*SZVEC(7)
99 YJOINT(9) = YJOINT(8) + EL(8)*SZVEC(8)
100 DD 10 I=1,8

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```

*2D33150
*2D33160
*2D33170
*2D33180
*2D33190
*2D33200
*2D33210
*2D33220
*2D33230
*2D33240
*2D33250
*2D33260
*2D33270
*2D33280
*2D33290
*2D33300
*2D33310
*2D33320
*2D33330
*2D33340
*2D33350
*2D33360
*2D33370
*2D33380
*2D33390
*2D33400
*2D33410
*2D33420
*2D33430
*2D33440
*2D33450
*2D33460
*2D33470
*2D33480
*2D33490
*2D33500
*2D33510
*2D33520
*2D33530
*2D33540
*2D33550
*2D33560
*2D33570
*2D33580
*2D33590
*2D33600
*2D33610
*2D33620
*2D33630
*2D33640

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101 XLEN(I) = CZVEC(I)/PTLEN
102 YLEN(I) = SZVEC(I)/PTLEN
103 NI(I) = PTLEN*EL(I) + 1.
104 NI(4) = 360./ANG
105 NT = 0
106 DO 80 J=1,8
107 JJ = N(J)
108 GO TO (20,20,20,40,20,20,60,20),J
109 DO 30 I = 1, JJ
110 NST=NT+I
111 R=I-1
112 XMAN(NST) = XJOINT(J) + R*XLEN(J)
113 YMAN(NST) = YJOINT(J) + R*YLEN(J)
114 GO TO 80
115 HEADX = XJOINT(4) + RHOPF*CZVEC(4)
116 HEADY = YJOINT(4) + RHOPF*SZVEC(4)
117 DO 50 I=1, JJ
118 R=I-1
119 RANG = R*ANG*.0174532925
120 NST=NT+I
121 XMAN(NST) = HEADX + AR(4)*COS(RANG)
122 YMAN(NST) = HEADY + AR(4)*SIN(RANG)
123 GO TO 80
124 DO 70 I=1, JJ
125 R=I-1
126 NST=NT+I
127 XMAN(NST) = XJOINT(I) + R*XLEN(I)
128 YMAN(NST) = YJOINT(I) + R*YLEN(I)
129 NT = NT+N(J)
130 NPTS1=1
131 NPTS2=2
132 NPTS3=3
133 PRINT 9997, IDATE, IPAGE
134 PRINT 9996, STIME(K)
135 CALL PLOT1(NSCALE(1), NHL, NSBH, NVL, NSBV)
136 CALL PLOT2(IMAGE, XMAX, XMIN, YMAX, YMIN)
137 IF (IZERO .NE. 0) GO TO 100
138 CALL PLOT3(*1, ZERG(1), VZERO(1), MSBH, INT)
139 CALL PLOT3(*, HZERO(1), ZERO(1), MSBV, INT)
140 IF (NCNTCT(1) .NE. 0) GO TO 130
141 ANGLE = ((360.-THE TALK,1,1)+THEY(K,1,7))/6.)*.0174532925
142 TS = THETA(K,1,1)*.0174532925
143 DO 125 J=1,5
144 TS = TS + ANGLE
145 XHIP(J) = XJOINT(1) + AR(1)*COS(ITS)
146 YHIP(J) = YJOINT(1) + AR(1)*SIN(ITS)
147 CALL PLOT3(*, XHIP(1), YHIP(1), 5, INT)
148 IF (NCNTCT(3) .NE. 0) GO TO 145
149 XRH0 = XJOINT(3) + RHOPTZ*SZVEC(3)
150 YRH0 = YJOINT(3) + RHOPTZ*SZVEC(3)

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*2033650
*2033660
*2033670
*2033680
*2033690
*2033700
*2033710
*2033720
*2033730
*2033740
*2033750
*2033760
*2033770
*2033780
*2033790
*2033800
*2033810
*2033820
*2033830
*2033840
*2033850
*2033860
*2033870
*2033880
*2033890
*2033900
*2033910
*2033920
*2033930
*2033940
*2033950
*2033960
*2033970
*2033980
*2033990
*2034000
*2034010
*2034020
*2034030
*2034040
*2034050
*2034060
*2034070
*2034080
*2034090
*2034100
*2034110
*2034120
*2034130
*2034140

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151 FRTYFV = 45.*.0174532925
152 TS = -FRTYFV
153 DO 135 J=1,3
154 XCHT(J) = XRH0 + AR(3)*COS(TS)
155 YCHT(J) = YRH0 + AR(3)*SIN(TS)
156 TS = TS + FRTYFV
157 DO 140 J=4,6
158 TS = TS + FRTYFV
159 XCHT(J) = XRH0 + AR(3)*COS(TS)
160 YCHT(J) = YRH0 + AR(3)*SIN(TS)
161 CALL PLOT3(0,0,XCHT(J),YCHT(J),6,INT)
162 IF (NCNCT(5) .NE. 0) GO TO 155
163 TS = (180. + THETA(K,1,5))*0.174532925
164 ANGLE = ((180. + (THETA(K,1,6) - THETA(K,1,5)))/4.)*0.174532925
165 DO 150 J=1,3
166 TS = TS + ANGLE
167 XELR(J) = XJOINT(6) + AR(5)*COS(TS)
168 YELR(J) = YJOINT(6) + AR(5)*SIN(TS)
169 CALL PLOT3(0,0,XELR(J),YELR(J),3,INT)
170 IF (NCNCT(6) .NE. 0) GO TO 165
171 TS = (THETA(K,1,6) - 180.)*0.174532925
172 SIXTY = 60.*.0174532925
173 DO 160 J=1,5
174 TS = TS + SIXTY
175 XHND(J) = XJOINT(7) + AR(6)*COS(TS)
176 YHND(J) = YJOINT(7) + AR(6)*SIN(TS)
177 CALL PLOT3(0,0,XHND(J),YHND(J),5,INT)
178 IF (NCNCT(7) .NE. 0) GO TO 175
179 TS = THETA(K,1,8)*0.174532925
180 ANGLE = ((180. + THETA(K,1,7) - THETA(K,1,8)))/4.)*0.174532925
181 DO 170 J=1,3
182 TS = TS + ANGLE
183 XKNE(J) = XJOINT(8) + AR(7)*COS(TS)
184 YKNE(J) = YJOINT(8) + AR(7)*SIN(TS)
185 CALL PLOT3(0,0,XKNE(J),YKNE(J),3,INT)
186 IF (NCNCT(8) .NE. 0) GO TO 195
187 TS = (THETA(K,1,8) - 180.)*0.174532925
188 DO 180 J=1,5
189 TS = TS + SIXTY
190 XFT(J) = XJOINT(9) + AR(8)*COS(TS)
191 YFT(J) = YJOINT(9) + AR(8)*SIN(TS)
192 CALL PLOT3(0,0,XFT(J),YFT(J),5,INT)
193 CONTINUE
194 CALL PLOT3(0,0,XMAN(1),YMAN(1),INT)
195 IF (IGNORE(1) .GT. 0) GO TO 200
196 CALL PLOT3(0,0,XFLOOR(1),YFLOOR(1),2,INT)
197 IF (IGNORE(2) .GT. 0) GO TO 210
198 CALL PLOT3(0,0,XSEAT(1),YSEAT(1),3,INT)
199 IF (IGNORE(3) .GT. 0) GO TO 220
200 CALL PLOT3(0,0,XR(1),YR(1),2,INT)

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*2034150
*2034160
*2034170
*2034180
*2034190
*2034200
*2034210
*2034220
*2034230
*2034240
*2034250
*2034260
*2034270
*2034280
*2034290
*2034300
*2034310
*2034320
*2034330
*2034340
*2034350
*2034360
*2034370
*2034380
*2034390
*2034400
*2034410
*2034420
*2034430
*2034440
*2034450
*2034460
*2034470
*2034480
*2034490
*2034500
*2034510
*2034520
*2034530
*2034540
*2034550
*2034560
*2034570
*2034580
*2034590
*2034600
*2034610
*2034620
*2034630
*2034640
*2034650
*2034660

```

```

201 IF (IGNORE(4) .GT. 0) GO TO 230
202 CALL PLOT3('**',XUSDF(1),YUSDF(1),2,INT)
203 IF (IGNORE(5) .GT. 0) GO TO 240
204 CALL PLOT3('**',XMS(1),YMS(1),2,INT)
205 IF (IGNORE(6) .GT. 0) GO TO 250
206 CALL PLOT3('**',XLSW(1),YLSW(1),2,INT)
207 IF (IGNORE(7) .GT. 0) GO TO 260
208 CALL PLOT3('**',XLP(1),YLP(1),2,INT)
209 IF (IGNORE(8) .GT. 0) GO TO 270
210 CALL PLOT3('**',XSC(1),YSC(1),2,INT)
211 IF (IGNORE(9) .GT. 0) GO TO 280
212 CALL PLOT3('**',XTDF(1),YTD(1),2,INT)
213 IF ((NBELT .NE. 1) .AND. (NBELT .NE. 3)) GO TO R4
214 XLAP(2) = XLAP(1) + BL1(K)*COS(PHI1(K))
215 YLAP(2) = YLAP(1) + BL1(K)*SIN(PHI1(K))
216 CALL PLOT3('**',XLAP(1),YLAP(1),NPTS2,INT)
217 IF ((NBELT .NE. 2) .AND. (NBELT .NE. 3)) GO TO R4
218 XL(2) = XL(1) + BL2(K)*COS(PHI2(K))
219 YL(2) = YL(1) + BL2(K)*SIN(PHI2(K))
220 CALL PLOT3('**',XL(1),YL(1),NPTS2,INT)
221 CALL PLOT3('**',XU(1),YU(1),NPTS1,INT)
222 DO 90 I=1,9
223 CALL PLOT3(JOINT(I),XJOINT(I),YJOINT(I),NPTS1,INT)
224 CALL PLOT4(INCHAR,LABEL)
225 PRINT 9994,SCALEX,SCALEY
226 IPAGE = IPAGE + 1
227 L=L+1
228 IF (L .GT. ISTFP) GO TO 120
229
230 110 CONTINUE
231 120 RETURN
232 9992 FORMAT(F8.6)
233 9993 FORMAT(1H-,36HINDICATED MEASUREMENTS ARE IN INCHES)
234 9994 FORMAT(1H,23HSCALING FACTORS: 1 TO ,F5.2,19H IN THE X DIRECTION/
235 119X,5H1 TO ,F5.2,19H IN THE Y DIRECTION)
236 9995 FORMAT(8I5)
237 9996 FORMAT(1H,26X,39HSTICK FIGURE REPRESENTATION FOR TIME = ,F5.3,
238 18H SECONDS/1H0)
239 9997 FORMAT (1H1,28X52HTWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT
240 1DATA,20X3A4,11X4HPAGE,13)
241 9998 FORMAT(6F10.4)
242 9999 FORMAT(8I5)
243 END

```

```

*2034455J
*2034466J
*2034467J
*2034468J
*2034469J
*2034470J
*2034471J
*2034472J
*2034473J
*2034474J
*2034475J
*2034476J
*2034477J
*2034478J
*2034479J
*2034480J
*2034481J
*2034482J
*2034483J
*2034484J
*2034485J
*2034486J
*2034487J
*2034488J
*2034489J
*2034490J
*2034491J
*2034492J
*2034493J
*2034494J
*2034495J
*2034496J
*2034497J
*2034498J
*2034499J
*203500J
*203501J
*203502J
*203503J
*203504J
*203505J
*203506J
*203507J

```

```

1 SUBROUTINE SUMMARY
2 COMMON XLAP(2),YLCAP(2),XL(2),YL(2),XUL(1),YUL(1),XFLOOR(2),
3 YFLOOR(2),XSEAT(3),YSEAT(3),XR(1),YR(1),YUSDR(2),
4 2XWS(2),YWS(2),XLSW(2),YLSW(2),XSC(1),YSC(1),YUSDR(2),
5 3XTOR(1),YTOR(1),XSC(2),YSC(2),XSS(2),YSS(2),YSC(2),
6 3CPSIA(10),SPSIA(10),
7 4DA(10),TGA(2),ZFER(2),PHI1(200),PHI2(200),PHI3(200),PLI(200),
8 5BL(200),PL3(200),IPAGE,STIME,NBELT,IG,IP(10),EL(8),K
9 COMMON N/INJ/HFA(200),HUA(200),CA(200),CA(200),PLCF(200),PLCF(200),
10 1,MM,MC,RELTAL(200),RELTR(200),RELTR(200),PL(200),NPROB
11 COMMON/IF/IN
12 DIMENSION PH(3),RL(3)
13 DIMENSION TT(4),TV(8),TATA),KI(3),KAC(3), (3), (3), (3),STIME(200)
14 DIMENSION THETA(200,3,4),PST(200,9),AL(200),ACHEST(200),ALI(211)
15 DIMENSION ACOM(5,1),CMIC(3,8),GHEAD(200),GHEAD(200),JESPA(4,4)
16 DIMENSION OFSPR(6),DESPC(5,6)
17 DIMENSION LA(211),CCNTAC(200,211),RHJ(8)
18 DIMENSION SETFAT(200),SETHCK(200)
19 DIMENSION XHEAD(200),YHEAD(200)
20 DIMENSION NS(5),IMAGE(1392),T(200),P(200,9)
21 DIMENSION CARD(5)
22 EQUIVALENCE (STIME(1),T(1)),(PL(1),PST(1,1))
23 DATA /DMT/1H,4H HIP,4*1H,4HHPPE,4HR TO,3HRSY,1H,4HHEAD,2*1H,
24 14HELB,1H,1H,4HHAND,2*1H,4HKNFE,2*1H,4HHEJIT,1H /
25 DATA ACOM/1H,4H F,4HLOOR,3*1H,4HSEAT,4H BAC,1HK,3*1H,4HHPPE,
26 12*1H,4H U,4HPPFR,4H PAN,2*1H,4HIND,4HSPIF,2*1H,1H,
27 24H ST,4HFRIN,4HNG M,4HHEEL,1H,4H (,4HOMER,4H PAN,2*1H,1H,
28 34H STE,4HERIN,4HG CO,4HLUMN,2*1H,3HTOF,4HROAR,1H,4H ST,
29 44HEERI,4HNG M,4HHEEL,1H,4HBACK,3H OF,4HFRON,4HT SE,2HAT /
30 DATA UN/2HON/
31 DO 1500 N=1,200
32 STIME(N)=0.
33 TS=-1.
34 WRITE(9)TS,STIME
35 REMIND 9
36 READ(9)XLAP(1),YLAP(1),YL(1),XL(1),YUL(1),XUL(1),XFLOOR(1),XSEAT(1),
37 1XR(1),XUSDF(1),XWS(1),XLSW(1),XLP(1),XSC(1),YTOR(1),AR, YELTOR(1),
38 2YSEAT(1),YR(1),YUSDF(1),YWS(1),YLSW(1),YLP(1),YTOR(1),YTOE(1),DEF,
39 3AR,RHOPTZ,RHOPTZ,EL,DA,CPSIA,SPSIA,TGA(2),ZFER,NBELT,IGNORE,RHO
40 READ ( IN,5999)PHEAD,PCHEST,NPASGR,NGRAPH,NSTCK,NINJ,NPROB
41 9999 FORMAT (2E10.0,5I5)
42 2100 READ ( IN,9900)IA, CARD
43 5900 FORMAT (I2,8X,5A4)
44 IA=IA+1.5
45 IF (IA.LE.0) GO TO 2200
46 IF (IA.GT.11) GO TO 2100
47 DO 2150 I=1,5
48 2150 ACOM(I,IA)=CARD(I)
49 GO TO 2100
50

```

```

51 2200 LL=0
52 M = 0
53 K = 0
54 DO 90 I=1,200
55 DO 90 J=1,21
56 CONTAC(I,J)=0.
57 READ(9)TIME,TT,TV,TA,DISP,XAP,PLX,YA,YAP,PLY,XC,XCP,PLC,AH,
58 IBH,CH,OH,ACH,ACH,CCH,CCH,DCH,JJ,KI(II),KA(II),PP(II),I=1,JJ),FFM,FSPRM,
59 ZFS,HEADX,HEADY,PHI,BL
60 IF (TIME+.5) 300,110,110
61 K = K+1
62 IF (K-200) 120,120,300
63 STIME(K) = TIME
64 DO 130 I=1,8
65 THETA(K,1,I) = TT(I)
66 THETA(K,2,I) = TV(I)
67 THETA(K,3,I) = TA(I)
68 POST(K,1) = DISP
69 POST(K,2) = XAP
70 POST(K,3) = PLX
71 POST(K,4) = YA
72 POST(K,5) = YAP
73 POST(K,6) = PLY
74 POST(K,7) = XC
75 POST(K,8) = XCP
76 POST(K,9) = PLC
77 XHEAD(K) = HEADX
78 YHEAD(K) = HEADY
79 PHI1(K) = PHI(1)
80 PHI2(K) = PHI(2)
81 PHI3(K) = PHI(3)
82 BL1(K) = BL(1)
83 BL2(K) = BL(2)
84 BL3(K) = BL(3)
85 X = AH-PHEAD*DH
86 Y = CH+PHEAD*DH
87 AHEAD(K) = SQRT(X**2+Y**2)
88 GHEAD(K) = ATAN2(Y,X)/.01745329
89 X = ACH-PCHE*ST*BCH
90 Y = CCH+PCHE*ST*DCH
91 ACHEST(K) = SQRT(X**2+Y**2)
92 GCHEST(K) = ATAN2(Y,X)/.01745329
93 TSA = SIN(TT(4))
94 TSB = COS(TT(4))
95 X = AH-RHO(4)*BH
96 Y = CH+RHO(4)*DH
97 HFA(K) = X*TSA - Y*TSH
98 HLA(K) = X*TSB + Y*TSA
99 TSA = SIN(TT(3))
100 TSB = COS(TT(3))

```

```

*2D29140
*2D29150
*2D29160
*2D29170
*2D29180
*2D29190
*2D29200
*2D29210
*2D29220
*2D29230
*2D29240
*2D29250
*2D29260
*2D29270
*2D29280
*2D29290
*2D29300
*2D29310
*2D29320
*2D29330
*2D29340
*2D29350
*2D29360
*2D29370
*2D29380
*2D29390
*2D29400
*2D29410
*2D29420
*2D29430
*2D29440
*2D29450
*2D29460
*2D29470
*2D29480
*2D29490
*2D29500
*2D29510
*2D29520
*2D29530
*2D29540
*2D29550
*2D29560
*2D29570
*2D29580
*2D29590
*2D29600
*2D29610
*2D29620
*2D29630

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```

101 X = A - H*P*Q(3)*BCH
102 Y = (C*H+R*Q(3))*DCH
103 CFA(K) = K*ISA-Y*ISH
104 CUA(K) = X*ISA+Y*ISH
105 IF (JJ) 210,210,14J
106 IF (M) 150,150,160
107 M = I
108 LI(M) = KI(I)
109 LA(M) = KA(I)
110 CUNTA(K,M) = PP(I)
111 DO 200 I=1,JJ
112 DO 180 J=1,M
113 IF (LI(J)-KI(I)) 190,170,180
114 IF (LA(J)-KA(I)) 180,190,180
115 CONTINUE
116 M = M+1
117 LI(M) = KI(I)
118 LA(M) = KA(I)
119 CUNTA(K,M) = PP(I)
120 GO TO 200
121 CONTINUE
122 CONTINUE
123 RELTA(K) = FFM(1)
124 BELTA(K) = FFM(2)
125 BELTC(K) = FFM(3)
126 SEFRT(K) = FSPRM
127 SFTBCK(K) = FS
128 GO TO 100
129 REMIN) 9
130 MN=0
131 MM=0
132 DO 250 I=1,M
133 IF (LI(I).NE.3) GO TO 230
134 IF (LA(I).EQ.2) GO TO 230
135 MM=MM+1
136 DO 220 J=1,K
137 CCF(J,MM)=CUNTA(J,I)
138 GO TO 250
139 230 IF (LI(I).NE.7) GO TO 250
140 MN=1
141 DO 240 J=1,K
142 CKF(J)=CUNTA(J,I)
143 CONTINUE
144 CALL DATE(I,DATE)
145 MMAX=M
146 LINE = 52
147 IPAGE = 1
148 ISTART = 1
149 IF (K-52) 310,320,320
150 ISTOP = K

```

```

*202964J
*202965J
*202966J
*202967C
*202968J
*202969J
*202970J
*202971C
*202972C
*202973C
*202974C
*202975C
*202976C
*202977C
*202978J
*202979C
*202980C
*202981C
*202982C
*202983C
*202984C
*202985C
*202986C
*202987C
*202988C
*202989C
*202990C
*202991C
*202992C
*202993C
*202994C
*202995C
*202996C
*202997C
*202998C
*202999C
*203000C
*203001C
*203002C
*203003C
*203004C
*203005C
*203006C
*203007C
*203008C
*203009C
*203010C
*203011C
*203012C
*203013C

```



```

151 GO TO 400
152 ISTOP = 52
153 PRINT 9000, IDATE, IPAGE
154 PRINT 9950
155 FORMAT(16X,20H BELT FORCES (POUNDS),16X,21H BELT ANGLES (DEGREES)
156 110X,21H RELATIVE HIP POSITION,20X,22H RELATIVE HEAD POSITION/
157 24X,HTIME,4X,8HLAP BELT,2X,18H SHOULDER RESTRAINT,9X,HLAP BELT,
158 32X,18H SHOULDER RESTRAINT,14X,8H(INCHES),14X,8H(INCHES)/3X,6H(SEC.)
159 414X,5HL OMER,5X,5H UPPER,21X,5HL OMER,5X,5H UPPER,9X
160 51X,20H HORIZONTAL VERTICAL,4X,20H HORIZONTAL VERTICAL)
161 DO 405 I=1,ISTOP
162 TSA = PHI(I)/.01745329
163 TSB = PHI2(I)/.01745329
164 TSC = PHI3(I)/.01745329
165 PRINT 9951,STIME(I),BELTA(I),BELTR(I),BELTC(I),TSA,TSB,TSC,
166 IPOST(I,1),POST(I,4),XHEAD(I),YHEAD(I)
167 9951 FORMAT(1X,F7.3,F9.0,2F10.0,7X,3F10.1,7X,F10.2,F11.2,1X,2F11.2)
168 CONTINUE
169 IPAGE = IPAGE + 1
170 PRINT 9000, IDATE, IPAGE
171 PRINT 9001
172 PRINT 9004
173 PRINT 9003
174 DO 410 I=1,ISTOP
175 PRINT 9002,STIME(I),((THETA(I,J),L),J=1,3),L=1,4)
176 CONTINUE
177 IPAGE = IPAGE + 1
178 PRINT 9000, IDATE, IPAGE
179 PRINT 9001
180 PRINT 9005
181 PRINT 9003
182 DO 420 I=1,ISTOP
183 PRINT 9002,STIME(I),((THETA(I,J),L),J=1,3),L=5,8)
184 CONTINUE
185 IPAGE = IPAGE + 1
186 PRINT 9000, IDATE, IPAGE
187 PRINT 9006
188 DO 430 I=1,ISTOP
189 PRINT 9007,STIME(I),PUST(I,7),POST(I,8),POST(I,9), (POST(I,J),J=1,6
190 1)
191 CONTINUE
192 IPAGE = IPAGE + 1
193 PRINT 9000, IDATE, IPAGE
194 PRINT 9009
195 DO 440 I=1,ISTOP
196 PRINT 9004,STIME(I),AHEAD(I),GHEAD(I),ACHEST(I),GCHEST(I),RELT(I)
197 1,BELTB(I),BELTC(I),SETBCK(I),SETFR(I)
198 CONTINUE
199 M=MMAX
200 MSTEP = 0

```

```

*2030140
*2030150
*2030160
*2030170
*2030180
*2030190
*2030200
*2030210
*2030220
*2030230
*2030240
*2030250
*2030260
*2030270
*2030280
*2030290
*2030300
*2030310
*2030320
*2030330
*2030340
*2030350
*2030360
*2030370
*2030380
*2030390
*2030400
*2030410
*2030420
*2030430
*2030440
*2030450
*2030460
*2030470
*2030480
*2030490
*2030500
*2030510
*2030520
*2030530
*2030540
*2030550
*2030560
*2030570
*2030580
*2030590
*2030600
*2030610
*2030620
*2030630

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201 IF (M) = 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100, 101, 102, 103, 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, 244, 245, 246, 247, 248, 249, 250
445 IF (M) = 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100, 101, 102, 103, 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, 244, 245, 246, 247, 248, 249, 250
450 IF (M-C) = 60, 670, 470
460 MSTEP = M+MSTEP
      GO TO 445
470 MSTEP = 6+MSTEP
      NSTOP = 6
480 MSTART = 1+MSTEP
490 IPAGE = IPAGE + 1
      PRINT 900, I, DATE, I, FAULT
      PRINT 9010
      DO 540 I=1, NSTOP
        J = 1+MSTEP
        I1 = I(I, J)
        IA = IA(J)
        DESPA(1, I) = COMI(1, I)
        DESPA(2, I) = COMI(2, I)
        DESPA(3, I) = COMI(3, I)
        IF (IA-4) 530, 500, 530
500 IF (MPASGR-2) 510, 530, 520
510 IA = 10
      GO TO 530
520 IA = 11
530 DESPC(1, I) = ACCM(1, IA)
      DESPC(2, I) = ACCM(2, IA)
      DESPC(3, I) = ACCM(3, IA)
      DESPC(4, I) = ACCM(4, IA)
      DESPC(5, I) = ACCM(5, IA)
540 CONTINUE
      PRINT 9011, ((DESPA(J, I), J=1, 3), I=1, NSTOP)
      PRINT 9012, (ON, I=1, NSTOP)
      PRINT 9013, ((DESPC(J, I), J=1, 5), I=1, NSTOP)
      DO 900 I=1, NSTOP
600 PRINT 9014, STIME(I), (CONTACT(I, J), J=MSTART, MSTEP)
900 CONTINUE
      MSTEP = MSTEP+6
      M=M-6
      GO TO 445
905 LINE=51
      IPAGE=IPAGE+1
      ISTART=ISTOP
      IF (ISTOP-K) 910, 1000, 1000
910 IF (ISTOP+50-K) 930, 920, 920
920 ISTOP=K
      GO TO 400
930 ISTOP=ISTOP+50
      GO TO 400
1000 IF (INJ.EQ.0) CALL SIPP(IPAGE, K, THETA, STIME)
      IF (NGRAPH.NE.0) GO TO 3000
10 FORMAT (1H1, 2X, 38HTWD DIMENSIONAL CRASH VICTIM SIMULATOR, 3X, 10HPLN#2031130

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Subroutine SUMMARY (page 5 of 9)

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251      1T OF OUTPUT DATA,61X,4*PAGF,[3]
252      FMAX1=BELTA(1)
253      FMIN1=BELTA(1)
254      DO 20 I=1,K
255          FMAX1=AMAX1(FMAX1,BELTA(I),BELTR(I),HELTC(I))
256          FMIN1=AMIN1(FMIN1,BELTA(I),BELTR(I),HELTC(I))
257          INT=4
258              NS(I)=1
259              NS(2)=0
260              NS(3)=2
261              NS(4)=0
262              NS(5)=4
263              NHL=6
264              NSRH=7
265              NVL=11
266              NSRV=9
267              NC=0
268          PRINT 10, IPAGE
269          PRINT 30
270          30 FORMAT(1H0,53X,19HRELT FORCES IN LBS./)
271              CALL PLOT1(NS(I),NHL,NSRH,NVL,NSRV)
272              CALL PLOT2(IMAGE,T(K),T(1),FMAX1,FMIN1)
273              CALL PLOT3(*,T(1),BELTA(I),K,INT)
274              CALL PLOT3(*,T(1),BELTR(I),K,INT)
275              CALL PLOT3(*,T(1),HELTC(I),K,INT)
276              CALL PLOT4(NC,NS(I))
277          PRINT 40
278          40 FORMAT(1H0,55X,15HTIME IN SECONDS/1H0)
279          PRINT 50
280          50 FORMAT(5X,13H* IS LAP RELT/5X,29HX IS LOWER SHOULDER RESTRAINT/
281              15X,29H= IS UPPER SHOULDER RESTRAINT)
282              FMAX2=AHEAD(1)
283              FMIN2=AHEAD(1)
284              DO 60 I=1,K
285                  FMAX2=AMAX1(FMAX2,AHEAD(I),ACHEST(I))
286                  FMIN2=AMIN1(FMIN2,AHEAD(I),ACHEST(I))
287                  IPAGE=IPAGE+1
288          PRINT 10, IPAGE
289          PRINT 70
290          70 FURMAT(1H0,51X,24HACCELERATIONS IN G-UNITS/)
291              CALL PLOT1(NS(I),NHL,NSRH,NVL,NSRV)
292              CALL PLOT2(IMAGE,T(K),T(1),FMAX2,FMIN2)
293              CALL PLOT3(*,T(1),AHEAD(I),K,INT)
294              CALL PLOT3(*,T(1),ACHEST(I),K,INT)
295              CALL PLOT4(NC,NS(I))
296          PRINT 40
297          PRINT 80
298          80 FORMAT(5X,22H* IS HEAD ACCELERATION/5X,23HX IS CHEST ACCELERATION)
299              IPAGE=IPAGE+1
300          FMAX3=POST(1,1)

```

Subroutine SUMMARY (page 6 of 9)

```

301 FMIN3=POST(1,1)
302 DO 15 I=1,K
303 FMAX3=AMAX1(FMAX3,POST(I,1),POST(I,4))
304 FMIN4=AMIN1(FMIN3,POST(I,1),POST(I,4))
305 PRINT 10, IPAGE
306 PRINT 25
307 FORMAT(1H0,52X,22H HIP POSITION IN INCHES/)
308 CALL PLOT1(NS(I),NHL,NSRH,NVL,NSBV)
309 CALL PLOT2(IMAGE,T(K),T(I),FMAX3,FMIN3)
310 CALL PLOT3(*X*,T(I),POST(I,1),K,INT)
311 CALL PLOT3(*X*,T(I),POST(I,4),K,INT)
312 CALL PLOT4(NC,NS(I))
313 PRINT 40
314 PRINT 35
315 FORMAT(5X,28H* IS HORIZONTAL HIP POSITION,5X,26HX IS VERTICAL HIP
316 POSITION)
317 IPAGE =IPAGE +1
318 FMAX4=P(I,9)
319 FMIN4=P(I,9)
320 DO 45 I=1,K
321 FMAX4=AMAX1(FMAX4,P(I,9))
322 FMIN4=AMIN1(FMIN4,P(I,9))
323 PRINT 10, IPAGE
324 PRINT 55
325 FORMAT(1H0,47X,30HVEHICLE INPUT PULSE IN G-UNITS/)
326 CALL PLOT1(NS(I),NHL,NSRH,NVL,NSBV)
327 CALL PLOT2(IMAGE,T(K),T(I),FMAX4,FMIN4)
328 CALL PLOT3(*X*,T(I),P(I,9),K,INT)
329 CALL PLOT4(NC,NS(I))
330 PRINT 40
331 IPAGE =IPAGE +1
332 FMAX5=GHEAD(I)
333 FMIN5=GHEAD(I)
334 DO 65 I=1,K
335 FMAX5=AMAX1(FMAX5,GHEAD(I),GCHEST(I))
336 FMIN5=AMIN1(FMIN5,GHEAD(I),GCHEST(I))
337 PRINT 10,IPAGE
338 PRINT 75
339 FORMAT(1H0,46X,32HANGLE OF ACCELERATION IN DEGREES/)
340 CALL PLOT1(NS(I),NHL,NSRH,NVL,NSBV)
341 CALL PLOT2(IMAGE,T(K),T(I),FMAX5,FMIN5)
342 CALL PLOT3(*X*,T(I),GHEAD(I),K,INT)
343 CALL PLOT3(*X*,T(I),GCHEST(I),K,INT)
344 CALL PLOT4(NC,NS(I))
345 PRINT 40
346 PRINT 85
347 FORMAT(5X,31H* IS ANGLE OF HEAD ACCELERATION/5X,32HX IS ANGLE OF
348 HEAD ACCELERATION)
349 IPAGE=IPAGE+1
350 FMAX6=SEIFRT(I)

```

```

*2031640
*2031650
*2031660
*2031670
*2031680
*2031690
*2031700
*2031710
*2031720
*2031730
*2031740
*2031750
*2031760
*2031770
*2031780
*2031790
*2031800
*2031810
*2031820
*2031830
*2031840
*2031850
*2031860
*2031870
*2031880
*2031890
*2031900
*2031910
*2031920
*2031930
*2031940
*2031950
*2031960
*2031970
*2031980
*2031990
*2032000
*2032010
*2032020
*2032030
*2032040
*2032050
*2032060
*2032070
*2032080
*2032090
*2032100
*2032110
*2032120
*2032130

```

Subroutine SUMMARY (page 7 of 9)

```

351 FM IN6=SETFRT(I)
352 00 95 I=1,K
353 FM AX6=AMAXI(FMAX6,SETFRT(I),SETBCK(I))
354 FM IN6=AMINI(FMIN6,SETFRT(I),SETBCK(I))
355 PRINT 10, IPAGE
356
357 105 FORMAT(1H0,53X,19HSEAT FORCES IN LBS./)
358 CALL PLOT1(NS(1),NHL,NSRH,NVL,NSBV)
359 CALL PLOT2(IMAGE,TK),T(I),FM AX6,FMIN6)
360 CALL PLOT3(*,*,T(I),SETFRT(1),K,INT)
361 CALL PLOT3(*,*,T(I),SETBCK(1),K,INT)
362 CALL PLOT4(INC,NS(1))
363 PRINT 40
364
365 115 FORMAT(5X,32H* IS SEAT FORCE AT FRONT OF SEAT/5X,22H* IS SEAT FORC
366 1E AT HIP)
367 IPAGE = IPAGE + 1
368 3000 IF (NSTICK .EQ. 0) CALL STYX
369 RETURN
370 5000 FORMAT (1H1,28X52HTWO DIMENSIONAL CRASH VICTIM SIMULATOR OUTPUT
371 10ATA,20X3A4,11X4HPAGE,I3)
372 9001 FORMAT (45X42HBODY SEGMENT ANGULAR ORIENTATION (DEGREES))
373 9002 FORMAT (1XF7.4,F10.2,F9.2,E12.4,F10.2,F9.2,F12.4,F10.2,F9.2,E12.4,
374 1F10.2,F9.2,E12.4)
375 5003 FORMAT (10X26HPOSITION VELOCITY ACCEL.,5X26HPOSITION VELOCITY
376 1ACCEL.,5X26HPOSITION VELOCITY ACCEL.,5X26HPOSITION VELOCITY AC
377 2CFL.)
378 5004 FORMAT (4X4HTIME,9X11HLOWER TORSO,20X12HCENTER TORSO,19X11HUPPER T
379 1ORSO,23X4HHEAD)
380 5005 FORMAT (4X4HTIME,10X9HUPPER ARM,22X9HLJWFER ARM,22X9HUPPER LEG,21X9
381 1HLOWER LEG)
382 5006 FORMAT (20X16HVEHICULAR MOTION,44X24HBODY MOTION AT HIP JOINT/67X,
383 1HORIZONTAL,33X8HVERTICAL/44HTIME,3X8HPOSITION,5X8HVELOCITY,6X6H
384 2ACCEL.,11X8HRELATIVE,5X8HVELOCITY,6X6HACCEL.,9X8HRELATIVE,5X8HVELO
385 3CITY,6X6HACCEL./56X6HDISPL./12X5H(IN.),6X10H(IN./SEC.),2D32480
386 4,4X9H(G-UNITS),10X5H(IN.),6X10H(IN./SEC.),4X9H(G-UNITS),8X5H(IN.),
387 56X10H(IN./SEC.),4X9H(G-UNITS))
388 9007 FORMAT (1XF7.4,F9.3,F13.2,F13.3,F18.3,F13.2,F13.3,F16.3,F13.2,F13.
389 13)
390 9008 FORMAT (1XF7.4,F14.1,F11.1,F14.1,F11.1,F18.1,F12.1,F16.2,F13
391 1,2)
392 5C09 FORMAT (25X22HACCELEROMETER READINGS,27X18HBELT FORCES (LBS),17X17
393 1HSEAT FORCES (LBS)/4X4HTIME,14X4HHEAD,18X5HCHEST/15X9HRESTRANT,4X
394 25HANGLE,8X9HRESTRANT,4X5HANGLE,13X3HLAP,3X18HSHOULDER RESTRANT,1
395 33X6HAT HIP,9X2HAT/15X9H(G-UNITS),6X6H(DEC.),6X9H(G-UNITS),4X5H(DFG
396 4.),25X5HLOWER,7X5HUPPER,20X10HFRONT EDGE)
397 9010 FORMAT (55X21HCONTACT FORCES (LBS.))
398 9011 FORMAT (16X,3A4,8X,3A4,8X,3A4,8X,3A4,8X,3A4,8X,3A4,8X,3A4)
399 5C12 FORMAT (4X,4HTIME,13X,A2,18X,A2,18X,A2,18X,A2,18X,A2,18X,A2)
400 9013 FORMAT (12X,6I2X,6A4,A2))

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Subroutine SUMMARY (page 8 of 9)

401 9014 FORMAT (1XF7.4,F17.1,5F2J.1)
402 END

*2030640
*2132550

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1  SUBROUTINE TAUMAK(ZKB)
2  COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,HRB,IGNDPE,DA,XSMALA,YSMAL,*2D14130
3  1A,XISMALA,PSIA,SPSIA,CPDIA,FMUA,SIGMA,SIGMA,AA,KTABLE,MFORI,DIR,PI,*2D14140
4  2TWO,GRAVIT,CPRIME,HIGKI,ELAR,TPRIME,ALFAI,OMEGAI,RPSI,RHO,THETA7,*2D14150
5  3STHETZ,CTHETZ,FSPRM,RH,THATPV,WZERD,RHOPTZ,RHOPEZ,GAMZER,LCONTRL,CS,*2D14160
6  4,S,FMS,BETA,ZZERO,ELTWTY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NPASGR,*2D14180
7  5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,RPRTD,G,RNS,SIGZ,ELZTEN,A,GRAVA,*2D14190
8  6,ELAMB,TIME,TRUG,MAXR,LITGAM,EPSLNZ,PSEL,RVEL,IBIG,IFDRK,BASIC,FS,*2D14200
9  7SMALLF,ZVECP,ZVECP,ZVECP,THEDSQ,CTHETA,STHETA, BICMI,TMATII,*2D14210
10 8EXITD,YIDOT,PHI,EDNE,SDELTA,SDELTD,BL,PN,MODE,OMEGA,X,Y,THEFEE,RH,*2D14220
11 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELDO,DELDO,EPSELNY,FTOLD,FSPRM,*2D14230
12 10COMMON CZERON,CONEN,CTMON,ET,EHAT,CEE,SMALLR,AEL,ATIMTJZ,TGAMZ,YZFE,*2D14240
13 11RO,FSZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,BVELB,CVELC,AAACCA,*2D14250
14 122BACCB,CACCC,DACCCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TDSCLT,ATDSO,TIMT,*2D14260
15 13,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TA,SIGMAC,ITAU,TAUHAT,RZ,SZ
16 14 *2D14270
17 15 *2D14280
18 16 *2D14290
19 17 *2D14300
20 18 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3),DELTA(3)*2D14300
21 19 1I,PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),BIGKI(7),*2D14310
22 20 2TPRIME(7),ALFAI(7),OMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),FL(8),AP(*2D14320
23 21 38I,RHO(8),THETAZ(8),STHETAZ(8),CTHETAZ(8),IRIG(8),THEDSQ(8),CTHETA(8)*2D14330
24 22 4),STHETA(8), BICMI(8),TMATII(8),RHOPR(8),XPRM(8),YPRM(8)*2D14340
25 23 5,TDSQL(18),ATDSQ(8),IGNRE(10),DA(10),XSMALA(10),YSMALA(10),XISMALA(10),*2D14350
26 24 6(10),PSIA(10),CPDIA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),BE,*2D14360
27 25 7FE(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLR(10),ZVEC(11),ZVECP(11)*2D14370
28 26 8I,ZVECP(11),STIMTJ(13),AEL(14),RSEL(15),RVEL(16),MODE(16),TIMTJZ(*2D14380
29 27 9I6),TIMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EDNE(18),PN(18)*2D14390
30 28 DIMENSION DELOD(18),DELOD(18),EPSELNY(18),FTOLD(18),OMEGA(18),CZE,*2D14400
31 29 IRON(18),CONEN(18),CTMON(18),ET(18),EHAT(18),IFORK(3,8),SIGMA(10,3)*2D14410
32 30 2,XXX(300,3),YVY(300,3),FMM(300,3),BBB(300,3), SIGMA(10,1)*2D14420
33 31 30I,AA(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,128),BASIC(11,P),KTAB,*2D14430
34 32 4LF(2,14),ZPPP(128),BL(3) *2D14440
35 33 *2D14450
36 34 COMMON THATPM,THATPX,THATPS,XVEHZ
37 35 COMMON FAR(18),SLOPE(18),ISWT(18),LODSWT(18)
38 36 COMMON NNO(1402)
39 37 DIMENSION TAU(16),ZK(11)
40 38 ISTAR = 0
41 39 DO 10 I=1,16
42 40 TAU(I) = 0.
43 41 TAUHAT = 1.E38
44 42 IYAU = 0
45 43 DO 210 I=1,MAXR
46 44 IF (MODE(I)) 120,155,90
47 45 IF (RVEL(I))*RSEL(I) 110,110,155
48 46 GO TO 130
49 47 ETA = RSEL(I)
50 48 TAU(I) = (SIGN(RPSI(I),ETA)-RVEL(I))/RSEL(I)
51 49 *2D14600
52 50 *2D14610

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Subroutine TAUMAK (page 1 of 3)

```

51      IF (FM(KPOST,1)) 135,180,135
52      TS=SEL(I)/FM(KPOST,1)
53      IF (I-H) 180, 150, 140
54      IA = IFORX(2,I-8)
55      TS = TS/CPSTA(IA)
56      TSA = 1. - 2./TS*TAUI(I)
57      IF (TSA) 155,170,170
58      IF (I-LITGAM) 160,165,160
59      TAUI(I) = C.
60      GO TO 210
61      TAUI(I) = TAUMATZ
62      GO TO 180
63      TAUI(I) = TS*(1.-SQRT(TSA))
64      IF (TAUI(I)) 160,160,190
65      IF (TAUMAT-TAUI(I)) 210,210,200
66      TAUMAT = TAUI(I)
67      ITAU = I
68      CONTINUE
69      IF (TAUMAT.LT..000001) TAUMAT=.000001
70      IF (IBUG) 220,230,220
71      WRITE(6,9999)ITAU,TAUMAT,TAUI
72      FORMAT (7:0TAUMAK5X110,10XE20.8/(1X9E15.6))
73      WRITE(6,9997)MUDF
74      9997 FORMAT (5H MODE5X16I5)
75      IF (IISTAR) 305,235,305
76      JPRINT=0
77      JSTEP=0
78      JINFL=0
79      IF (ABS(TINFL-TPRINT)-1.E-6) 270,270,240
80      IF (TINFL-TPRINT) 260,270,250
81      JPRINT=1
82      TIMASK = TPRINT - TIME
83      GO TO 280
84      JINFL=1
85      TIMASK = TINFL - TIME
86      GO TO 280
87      JPRINT=1
88      GO TO 260
89      IF (TIMASK-DESTEP-1.E-6) 300,300,290
90      JSTEP=1
91      TIMASK = JESTEP
92      JPRINT=0
93      JINFL=0
94      DELTAT = AMIN1(TIMASK,TAUMAT)
95      CALL LIMDT(JPRINT,JINFL,JSTEP)
96      ISTAR = 1
97      IF (ITAU) 310,360,310
98      TS = TAUMAT - TIMASK
99      IF (ARS(TS) - 1.E-6) 390,390,320
100     IF (TS) 400,390,330

```

```

*2014627
*2014630
*2014640
*2014650
*2014660
*2014670
*2014680
*2014690
*2014700
*2014710
*2014720
*2014730
*2014740
*2014750
*2014760
*2014770
*2014780
*2014790
*2014795
*2014800
*2014810
*2014820
*2014830
*2014840
*2014850
*2014860
*2014870
*2014880
*2014890
*2014900
*2014910
*2014920
*2014930
*2014940
*2014950
*2014960
*2014970
*2014980
*2014990
*2015000
*2015010
*2015020
*2015030
*2015040
*2015050
*2015060
*2015070
*2015080
*2015090
*2015100

```



```

101      ITAU = 0
102      IF (LITGAM) 350,360,350
103      IF (ABS(TIMASK-TAHATZ)-EPSLNZ) 360,360,370
104      DELTAT = TIMASK
105      GO TO 680
106      K = LITGAM
107      CALL RELSEL(ZKB,K,ZRV)
108      CALL RELSEL(ZK(1,1),K,ZPPP(1))
109      CALL RELSEL(ZK(1,2),K,ZPPP(2))
110      AK=(ZRV+ZPPP(1)-TIMASK/TAHATZ*(ZRV+ZPPP(2))/2.)/(ZPPP(1)-ZPPP(2))
111      DO 380 J=1,10
112      ZVECPP(J)=ZKB(J)+ZK(J,1)+AK*(ZK(J,2)-ZK(J,1))
113      GO TO 360
114      INDIC = 0
115      GO TO 410
116      INDIC = 1
117      410 IF (INDIC) 550,560,550
118      JPRINT=0
119      JINFL=0
120      JSTEP=0
121      IF (LITGAM) 570,630,570
122      570 IF (ABS(TAUHAT-TAHATZ)-EPSLNZ) 630,630,580
123      K = LITGAM
124      CALL RELSEL(ZKB,K,ZRV)
125      CALL RELSEL (ZK(1,1),K,ZPPP(1))
126      CALL RELSEL (ZK(1,2),K,ZPPP(2))
127      ZPP(2) = ZPPP(2)*TAUHAT/TAHATZ
128      TAHATZ = TAUHAT
129      AK = (ZRV/2.+ZPPP(1)-ZPPP(2))/2.)/(ZPPP(1)-ZPPP(2))
130      DO 590 J=1,10
131      ZVECPP(J)=ZKB(J)+ZK(J,1)+AK*(ZK(J,2)-ZK(J,1))
132      DN 600 J=1,MAXR
133      600 CALL RELSEL(ZVECPP,J,RSEL(J))
134      GU TO 70
135      DELTAT = TAUHAT
136      MODE(ITAU) = 0
137      IF (IBUG.EQ.0) GO TO 640
138      WRITE(6,9996)ITAU
139      FORMAT (12H RESET MODE(12,10H ) TO ZERO)
140      CALL NORHUT
141      KPRINT=JPRINT
142      KSTEP=JSTEP
143      KINFL=JINFL
144      RETURN
145      END

```

```

*2015110
*2015120
*2015130
*2015140
*2015150
*2015160
*2015170
*2015180
*2015190
*2015200
*2015210
*2015220
*2015230
*2015240
*2015250
*2015260
*2015270
*2015280
*2015290
*2015300
*2015310
*2015320
*2015330
*2015340
*2015350
*2015360
*2015370
*2015380
*2015390
*2015400
*2015410
*2015420
*2015430
*2015440
*2015450
*2015460
*2015465
*2015470
*2015480
*2015490
*2015500
*2015510
*2015520
*2015530
*2015540

```

1		SUBROUTINE YPRINT(IA,N)	*2039100
2	C	DUMMY PRINTOUT ROUTINE	*2039110
3		DIMENSION IA(3),IFM(34),IB(6)	*2039120
4		INTEGER*2 N	*2039130
5		DATA (B/4H A1),4H A2),4H A3),4H A4),4H (,4H A4, /	*2039140
6		DATA (ZFRO,IONE,MASK1,MASK2,MASK3/ZFOJOOJOO,ZF1000OJOO,ZFFO00000,	*2039141
7		1 Z00FFFFF,Z400C0C0)/	*2039142
8		IDUM=LAND(IA(1),MASK1)	*2039143
9		IF(IDUM.EQ.ZFRO)GO TO 9	*2039144
10		IF(IDUM.EQ.IONE)GO TO 9	*2039145
11		IF(IDUM.EQ.MASK3)GO TO 9	*2039146
12		IDUM=LAND(IA(1),MASK2)	*2039147
13		IA(1)=LCR(IDUM,MASK3)	*2039148
14		9 CONTINUE	*2039149
15		I=N	*2039150
16		IF(I.LE.0) GO TO 40	*2039160
17		IF(I.GT.132) I=132	*2039170
18		J=I/4	*2039180
19		JL=J+1	*2039190
20		K=I-4*J	*2039200
21		IF(K.NE.0) GO TO 10	*2039210
22		K=4	*2039220
23		JL=JL-1	*2039230
24		J=J-1	*2039240
25	10	IFM(1)=IB(5)	*2039250
26		JJ=1	*2039260
27		IF(J.EQ.0) GJ TO 30	*2039270
28		JJ=J+1	*2039280
29		DO 20 L=2, JJ	*2039290
30		IFM(L)=IB(6)	*2039300
31	20	CONTINUE	*2039310
32	30	IFM(JJ+1)=IB(K)	*2039320
33		PRINT IFM, (IA(L),L=1,JL)	*2039330
34	40	RETURN	*2039340
35		END	*2039350

A-92

Subroutine YPRINT

```

1  SUBROUTINE ZKMAKR(K,ZQ)
2  COMMON SWITCH,NEW,MAX,IPOST,XX,YYY,FMM,BB,IGNORE,DA,XSMALA,YSMAL *2009170
3  *2009180
4  IA,XISMLA,PSIA,SPSIA,CPSIA,FMUA,SIGMAA,SIGMA-AA,KTABLE,MFORI,DTP,PI *2009190
5  2WD,GRAVIT,CPRIME,BIGKI,EL,AR,PRIME,ALFAI,UMGAI,RP,SI,RHJ,THEFTAZ, *2009200
6  3STHEIZ,CTHETZ,FSPRM,RH,THATPV,WZRO,RHOP7,RHOPF7,GAMZER,LCONTL,CS *2009220
7  4,S,FMUS,BETA,ZZERO,ELTWTY,ELTHRY,H,DESTEP,DELTA,PHIZ,DELTA,NP,ASGP *2009230
8  5,XPACZ,NBELT,APRNTD,TIMAX,DTPRNT,R,PRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA *2009240
9  6,ELAMB,TIME,IRUG,MAXR,LITGAM,EPSLVZ,RSEL,RVEL,IBIG,IFORK,RASIC,FS *2009250
10 7SMALLF,ZVEC,ZVECP,ZVECP,THEDSQ,CTHETA,STHETA, RIGMI,TMATII, *2009260
11 8XIDOT,YIDOT,PHI,EO,NE,SDELTA,SDELTD,BL,PN,MODE,OMEGA,X,Y,THEFEE,RH *2009270
12 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELOLD,DELODD,EPSLNY,FTOLD,FSPRMZ *2009280
13 10COMMON CZERUN,CUNEN,CTWON,ET,EHAT,CEE,SMALLB,DEL,TIMTJZ,TCAMZ,YZ *2009290
14 11RO,FZCNS,ANVERS,TINFL,KPOST,TPRINT,TSTEP,AVELA,RVEL,R,CVEL,C,AACA, *2009300
15 12RACCB,CACCC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,TOSQLI,ATDSQ,TIMT *2009310
16 13J,STIMTJ,DELZ,ZK,ZPPP,TAHATZ,TS,TSB,SIGMAC,ITAU,TAUHAT,RZ,S *2009320
17 14 *2009330
18 15 *2009340
19 20 DIMENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),BETA(3),PHIZ(3),DELTA(3) *2009350
21 21PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),BIGKI(7), *2009360
22 22TPRIME(7),ALFAI(7),CMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR( *2009370
23 238),RHO(8),THETAZ(8),CTHETZ(8),CTHETZ(8),IBIG(8),THEDSQ(8),CTHETA(8) *2009380
24 244),STHETA(8),BIGMI(8),TMATII(8),RHOPRM(8),XPRM(8),YPPM(8) *2009390
25 255,TDSOLI(8),ATDSQ(8),IGNORE(10),DA(10),XSMALA(10),YSMALA(10),XISMLA *2009400
26 266(10),PSIA(10),CPSIA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),RE *2009410
27 277E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLB(10),ZVEC(11),ZVECP(11) *2009420
28 288),ZVECP(11),STIMTJ(13),AEL(14),RSEL(16),RVEL(16),MODE(16),TIMTJZ *2009430
29 29916),TIMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EO,NE(18),PN(18) *2009440
30 30DIMENSION DELOLD(18),DELODD(18),EPSLNY(18),FTOLD(18),OMEGA(18),CZE *2009450
31 312,XXX(300,3),YYY(300,3),FMM(300,3),RHB(300,3),SIGMA(10,3) *2009460
32 3230),AAI(10,10),ANVER(10,10),DELZ(11,16),ZK(11,128),BASIC(11,8),KTA *2009470
33 334LE(2,14),ZPPP(128),BL(3) *2009480
34 34 *2009500
35 35COMMON THATPV,THATPX,THATPS,XVEHZ *2009510
36 36COMMON FARB(18),SLOPF(18),ISWT(18),LOADSWT(18) *2009520
37 37COMMON NUNO(14,02) *2009530
38 38DIMENSION MASK(R),ZQ(11) *2009540
39 39DATA MASK/Z0000001,ZJ0000002,Z0000004,Z0000008, *2009550
40 401Z0000010,Z0000020,Z0000040,Z0000080/ *2009560
41 41L = K-1 *2009570
42 42DO 5 I=1,10 *2009580
43 43ZQ(I) = 0. *2009590
44 44IF (L.LE.0) RETURN *2009600
45 45DO 20 I=2,MAXI *2009610
46 46ISW = LAND(MASK(I-1),L) *2009620
47 47IF (ISW.EQ.0) GO TC 20 *2009630
48 48J = MAXI-I+2 *2009640
49 49IND = IBIG(J) *2009650
50 50DO 10 N=1,10 *2009660

```

Subroutine ZKMAKR (page 1 of 2)

*2009670
*2009680
*2009690
*2009700
*2009710

ZQ(N) = ZJ(N)+DELZ(N,I,ND)
CONTINUE
CONTINUE
RETURN
END

51 10
52 20
53
54
55

```

1 SUBROUTINE ZMAKER
2
3 COMMON SWITCH,NEW,MAX,IPOST,XXX,YYY,FMM,RRB,ICMURE,DA,XSMALA,YS4AL,*2D09730
4 1A,XISMLA,PSIA,SPSIA,CPSTA,FRUA,SIGMAA,SIGMA,AA,KTABLE,MFORI,DIR,PI,*2D09740
5 2TWO,GRVAI,CPRIME,BIGKI,EL,AR,TPRIME,ALFAI,OMEGAI,RHJ,RHJ,THETAZ,*2D09750
6 3STHETZ,CHETZ,FSPRM,RH,THATPV,WZORO,RHOPFZ,GAMZFR,LCONTI,CS,*2D09770
7 4,S,FMS,BETA,ZZERO,ELTMY,ELTHRY,H,DEFSTEP,DELTA,PHIZ,DELTA,NPASGR,*2D09780
8 5,XPAZ,NBELT,APRNTD,TI,MAX,OTPRNT,BPRNTD,G,R,NS,SIGZ,ELZTEN,A,GRAVA,*2D09790
9 6,ELAMB,TIME,IBUG,MAXP,LITGAM,EPSLNZ,RSEL,RVEL,IBIG,TFORK,BASIC,FS,*2D09800
10 7SMALLF,ZVEC,ZVECP,ZVECP,THEOSQ,CTHETA,STHETA, RIGMI,TMATII,*2D09810
11 8XIDOT,YIDOT,PHI,EDNE,SDELTA,SDELTD,BL,PN,MODE,OMEGA,X,Y,THEFFE,*2D09820
12 9OPRM,XPRM,YPRM,BEE,CEE,DEE,QUE,DELTD,DELODD,EPSLNZ,FTOLD,FSPRMZ,*2D09830
13 10COMMON,CZE,CON,CCNEN,CT,MGN,ET,EHAT,CEE,SMALLB,AFL,TIMTJ7,TGAMZ,YZE,*2D09840
14 11RO,F57CNS,ANVERS,TINFL,KPUSI,TPRINT,TSTEP,AVELA,BVELB,CVELC,AACA,*2D09850
15 1228ACCB,CACCC,DACCD,MAXI,KPRINT,KSTEP,KINFL,TIMASK,IDSQI,ATDSQ,TIMT,*2D09860
16 133J,STIMTJ,DELZ,ZKZPPP,TAHATZ,T,S,TSA,TSB,SIGMAC,ITAU,TAUHAT,RZ,SY,*2D09870
17 14*2D09880
18 15*2D09890
19 16DI MENSION SWITCH(3),NEW(3),MAX(3),IPOST(3),RETA(3),PHIZ(3),DELTA(3)*2D09900
20 171),PHI(3),SDELTA(3),SDELTD(3),ELAMB(6),MFORI(7),CPRIME(7),BIGKI(7),*2D09910
21 182TPRIME(7),ALFAI(7),CMEGAI(7),XIDOT(7),YIDOT(7),X(7),Y(7),EL(8),AR(*2D09920
22 193B),RHO(8),THETAZ(8),STHETZ(8),IBIGI(8),THEOSQ(8),CTHETA(*2D09930
23 204),STHETA(8), RIGMI(8),TMATII(8),PHOPRM(8),XPRM(8),YPRM(8)*2D09940
24 215,ATDSQI(8),ATDSQI(8),DAL(10),XSMALA(10),YSMALA(10),XISMLA,*2D09950
25 226(10),PSIA(10),CPSTA(10),SPSIA(10),SIGMAC(10),FMUA(10),GRAVA(10),BE,*2D09960
26 237E(10),CEE(10),QUE(10),DEE(10),GEE(10),SMALLR(10),ZVECP(11)*2D09970
27 248),ZVECP(11),STIMTJ(13),AEL(14),RSEL(16),RVEL(16),MODE(16),TIMTJZ(*2D09980
28 25916),TIMTJ(16),RPSI(16),A(17),G(18),R(18),SIGZ(18),EONE(18),PN(18)*2D09990
29 26DI MENSION DELODD(18),DELDD(18),EPSLNZ(19),FTOLD(18),OMEGA(18),CZE,*2D10000
30 27IRON(18),CONEN(18),CTMON(18),ET(18),EHAT(18),TFORK(3,8),SIGMA(10,3)*2D10010
31 282,XXX(300,3),YYY(300,3),FMM(300,3),RRB(300,3), SIGMAA(10,1)*2D10020
32 2930),AA(10,10),ANVERS(10,10),DELZ(11,16),ZK(11,128),RASIC(11,8),KTAB*2D10030
33 304LE(2,14),ZPPP(128),BL(3)
34 31*2D10050
35 32COMMON THATPV,THATPS,XVEHZ
36 33COMMON FARB(18),SLOPE(18),ISWT(18),LDOOSWT(18)
37 34COMMON,NONDI(402)
38 35DI MENSION ZR(10),WORKA(10),WORKB(10),CK(10,10)
39 36ZPAR=10.
40 37DO 10 I=1,10
41 38DO 10 J=1,I
42 39ANVERS(I,J) = AA(I,J)
43 40ANVERS(J,I)=AA(I,J)
44 41AA(J,I)=AA(I,J)
45 42CONTINUE
46 43IF (IRUG-2) 30,20,20
47 44WRITE (6,9997)AA
48 459997 FORMAT (9HOA MATRIX/(IX,10E13.-4))
49 46CALL MINV(ANVERS,10,DETERM,WORKA,WORKB)
50 47IF (DETERM) 50,40,50

```

```

51      PRINT 9996
52      FORMAT (10HHRAD MATRIX.  DUMP.)
53      GO TO 90
54      DO 70 I=1,10
55      ZR(I) = 0.
56      DO 60 J=1,10
57      ZR(I)=ZR(I)+SMALLB(J)*ANVERS(I,J)
58      ZVECP(I)=ZR(I)
59      IF (1HUG-2) 980,S6(.960)
60      WRITE (6,9595) ANVERS
61      5995  FORMAT (10HQA INVERSE/(1X,10E13.4))
62      DO 970 I=1,10
63      DO 970 J=1,10
64      CK(I,J) = 0.
65      DO 970 K=1,10
66      CK(I,J)=CK(I,J)+ANVERS(I,K)*AA(K,J)+AA(I,K)*ANVERS(K,J)
67      970  CONTINUE
68      WRITE (6,9994)CK
69      9994  FORMAT (17HOCHECK OF INVERSE/(1X,10E13.4))
70      RETURN
71      PRINT 9998,TIME
72      5998  FORMAT (38HOLARGE CHANGE IN ACCELERATION AT TIME=FR.6,
73      125H LOOK FOR SPURIOUS FORCF.)
74      PRINT 9999
75      5999  FORMAT(1H1)
76      CALL SUMARY
77      CALL ERROR
78      END

```

```

*2D1022)
*2D1023)
*2D1024)
*2D10250
*2D1026J
*2D1027U
*2D1028U
*2D10290
*2D1030U
*2D1031U
*2D1032U
*2D1033U
*2D10340
*2D1035J
*2D1036J
*2D1037U
*2D1038U
*2D1039U
*2D1040U
*2D1041U
*2D1042U
*2D1043U
*2D1044U
*2D1045U
*2D1046U
*2D1047U
*2D1048U
*2D1049U

```

1	GDIS	TITLE	*DS DUMMY FILE OR DEVICE INFORMATION ROUTINE*	*2D65740
2		ENTRY	XDINFO	*2D65750
3	GDIS	START	J	*2D65760
4		USTNC	*15	*2D65770
5	XCINFO	L	1,REG	*2D65780
6		SR	15,15	*2D65790
7		RCR	15,14	*2D65800
8		CNDP	J,R	*2D65810
9	RFGA	DC	F*0	*2D65820
10		DC	CL4,DUMMY*	*2D65830
11		DC	F*32767*	*2D65840
12		DC	RF*0*	*2D65850
13	REG	DC	1(REGA)	*2D65860
14		END		*2D65870

Subroutine XDINFO

```

1 XERS TITLE XERS VERSION OF DUMMY SECTION AND START*
2 ENTRY XPCOM
3 ENTRY XPRINT
4 START )
5 XERS USING #15
6 XPRINT ST 14*SAVE
7 XPCUM EQU KPRINT
8 L 15*V(XPRINT)
9 HALT 14*15
10 STOP 15
11 USING #14
12 L 14*SAVE
13 SK 15*15
14 PCP 15*15
15 CNTP 2*4
16 DS F
17 SAVE
18 EN

```

```

*2065800
*2065801
*2065802
*2065803
*2065804
*2065805
*2065806
*2065807
*2065808
*2065809
*2065810
*2065811
*2065812
*2065813
*2065814
*2065815

```

Subroutine XPRINT and XERCOM


```

1  IFCL      TITLE  *BITWISE LOGICAL ROUTINES*
2  MACRO
3  SAVE      &REG,&CODE,&ID
4  LCLA      &A,&B,&C
5  LCLC      &E,&F,&G,&H
6  AIF       (&REG=&EQ **),E1
7  AIF       (&ID=&EQ **),NULLID
8  AIF       (&ID=&EQ **),SPECID
9  SETA      ((&ID*2)/2)*2+4
10 &NAME     R      &A,(0,15)
11 &A        SFTA  K,&ID
12 DC        ALL(&A)
13 .CONTRB  AIF    (&A GT 32).SPLITUP
14 .CONYAA  AIF    (&A GT 8).BRAKDWN
15 &E        SETC  (&ID*(&B+1,&A)
16 DC        CLEAR&E*
17 AGO      .CONTA
18 .BRAKDWN ANJP
19 &E        SETC  (&ID*(&B+1,9)
20 DC        CLB*&E*
21 &B        SETA  &B+8
22 &A        SETA  &A-8
23 AGO      .CONYAA
24 .SPLITUP ANJP
25 &E        SETC  (&B*(&B+1,8)
26 &F        SETC  (&ID*(&B+9,8)
27 &G        SETC  (&ID*(&B+17,8)
28 &H        SETC  (&ID*(&B+25,8)
29 DC        CL32,&E,&F,&G,&H*
30 &R        SETA  &B+32
31 &A        SETA  &A-32
32 AGO      .CONTRB
33 .NULLID  ANJP
34 &NAME     DS
35 .CONTA   AGD
36 .SPECID  AIF    (&NAME=&EQ **).C.SECTN
37 &F        SETC  &NAME*
38 &A        SETA  1
39 .CONTRQ AIF    (&F*(1,&A) EQ *&E*).LEAVE
40 &A        SETA  &A+1
41 AGD      .CONTRQ
42 .LEAVE  ANJP
43 &R        SETA  ((&A+2)/2)*2+4
44 &NAME     R      &B,(0,15)
45 DC        ALL(&A)
46 DC        CLEAR&E*
47 AGO      .CONTA
48 .C.SECTN AIF    (&SYSECT=&EQ **).E4
49 &F        SETC  &SYSECT*
50 &A        SETA  1

```

```

*2039560
*2039570
*2039580
*2039590
*2039600
*2039610
*2039620
*2039630
*2039640
*2039650
*2039660
*2039670
*2039680
*2039690
*2039700
*2039710
*2039720
*2039730
*2039740
*2039750
*2039760
*2039770
*2039780
*2039790
*2039800
*2039810
*2039820
*2039830
*2039840
*2039850
*2039860
*2039870
*2039880
*2039890
*2039900
*2039910
*2039920
*2039930
*2039940
*2039950
*2039960
*2039970
*2039980
*2039990
*2040000
*2040010
*2040020
*2040030
*2040040
*2040050

```

```

BRANCH AROUND ID
LENGTH OF IDENTIFIER
IDENTIFIER
IDENTIFIER
IDENTIFIER
BRANCH AROUND ID
IDENTIFIER

```

```

51 .CONTG
52 IHRFMAC 78,360
53 .CONTA AIF (T,REG(1),NE,14),E3
54 AIF (MACROE,EU,T),CONTG
55 AIF (REGCODE,NE,1),E3
56 SETA REG(1)*4+20
57 AIF (EA,LE,75),CONTG
58 EA
59 SETA EA-64
60 .CONTC AIF (N*REG,NE,2),CONTG
61 STM REG(1),REG(2),EA,(13)
62 MEXIT
63 AIF (N*REG,NE,1),E3
64 ST REG(1),EA,(13,0)
65 MEXIT
66 AIF (REG(1),GF,14,OR,REG(1),E,2),CONTG
67 STM 14,15,12(13)
68 SETA REG(1)*4+20
69 AIF (N*REG,NE,2),CONTG
70 STM REG(1),REG(2),EA,(13)
71 MEXIT
72 AIF (N*REG,NE,1),E3
73 ST REG(1),EA,(13,0)
74 MEXIT
75 AIF (N*REG,NE,2),CONTG
76 STM 14,REG(2),12(13)
77 MEXIT
78 AIF (N*REG,NE,1),E3
79 STM 14,REG(1),12(13)
80 MEXIT
81 IHRFMAC 18,360
82 MEXIT
83 IHRFMAC 37,360,BCODE
84 MEXIT
85 MEND
86 MACROE
87 RETURN,REG,EPARA,REGCODE
88 LCLA EA
89 AIF (ENAME,EU,1),E3
90 DS 04
91 .CONTC AIF (REG,EG,1),CONTA
92 AIF (REG,EG,(15)),SPECRT
93 .CONTR ANDP
94 SETA REG(1)*4+20
95 EA
96 AIF (EA,LE,75),CONTB
97 EA
98 .CONTR AIF (N*REG,NE,2),CONTG
99 LM REG(1),REG(2),EA,(13)
100 .SPECRT AIF (REG(1),NE,14) AND REG(1),NE,15),CONTRAC

```

CONST NAME WILL

```

*2040150
*2040170
*2040190
*2040210
*2040230
*2040250
*2040270
*2040290
*2040310
*2040330
*2040350
*2040370
*2040390
*2040410
*2040430
*2040450
*2040470
*2040490
*2040510
*2040530
*2040550

```

```

101 AIF (*EREG(1), EQ '14' AND N*EREG EQ 1),COMPACK *2D40560
102 AIF (*EREG(1), EQ '15' AND N*EREG EQ 1),CONTA *2D40570
103 AIF (*EREG(1), EQ '14'),SKIP *2D40580
104 AIF (*EREG(2), EQ '0'),ZTWO *2D40590
105 LM 0,*EREG(2),20(13) *2D40600
106 AGJ *CONTA *2D40620
107 L 0,20(13,0) *2D40630
108 L *CONTA *2D40640
109 L 14,12(13,C) *2D40650
110 AIF (*EREG(2), EQ '15'),CONTA *2D40660
111 AIF (*EREG(2), EQ '0'),ZTWO *2D40670
112 *LM *2D40680
113 *CONTC (N*EREG NE 1),ERROR1 *2D40690
114 AIF (*EREG(1),EQ,(13,0) *2D40700
115 AIF (*PARA, EQ ' '),CUNTD *2D40710
116 AIF (*PARA, NE ' '),ERRCR2 *2D40720
117 MVI 12(13),X'FF' *2D40730
118 *CONTD AIF (*ERC, EQ '0'),CONTF *2D40740
119 AIF (*ERC(1,1) EQ ' '),ISAREG *2D40750
120 LA 15,ERC.(0,0) *2D40760
121 AGC *CONTE *2D40770
122 AIF (*ERC(1), EQ '15'),CONTE *2D40780
123 IHRPMAC 61,*ERC *2D40790
124 MEXIT 14 *2D40800
125 BR *END *2D40810
126 AGC *END *2D40820
127 *ERROR1 IHRPMAC 36,*EREG *2D40830
128 MEXIT *2D40840
129 *ERROR2 IHRPMAC 37,*PARA *2D40850
130 *END *2D40860
131 *ENAME CALL *ENTRY,*OPRND5,*VLPARA,*CID=,*EMF=1 *2D40870
132 *GALR *IHSWA,*IHSWB *2D40880
133 *LCLC *IHRN *2D40890
134 *LCLC *ENAME *2D40900
135 *SETC '309' *2D40910
136 *IHRND *IHR *,'SYSNDX' *2D40920
137 *ENAME *SETC (*VLPARA, EQ 'VL') *2D40930
138 *IHRSWA *SETR (*ENTRY, EQ '(15)') *2D40940
139 *IHSWB *SETB (*ENTRY, EQ 'L' AND *ENTRY, NE ' '),FROR1 *2D40950
140 AIF (*EMF, EQ 'L' AND *ENTRY, NE ' '),FROR2 *2D40960
141 AIF (*EMF, NE 'L' AND *ENTRY, EQ ' '),FROR3 *2D40970
142 AIF (*EMF, EQ 'L' AND *ENTRY, EQ ' '),FROR3 *2D40980
143 AIF (*EMF, EQ 'L' AND *ENTRY, EQ ' '),FROR3 *2D40990
144 AIF (*IHSWB),CONTC *2D41000
145 *CNJP 0,*4 *2D41010
146 B *H *2D41020
147 *DC *V(ENTRY) *2D41030
148 *AIF (*OPRND5, EQ ' ') AND *EMF(1), NE 'E'),CONTB *2D41040
149 *CONTC THRPLST *ENTRY,*OPRND5,*ENAME,*MF=GMF *2D41050
150 *CONTR AIF (*EMF, EQ 'L'),EXIT *2D41050

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```

151 AT      (EIMON3),COUNT
152 (      E,ENAME,R
153 3AL,  14,15
154 AIF      (EID, EQ **).EXIT
155 DC      X'4700',
156 DC      AL2(EID)
157 *EXIT
158 ANOP
159 *CONTCC
160 ENAME
161 *ERROR1  IHRP,MAC 73, EIHBN1, EENTAY
162 *ERROR2  IHRP,MAC 74, EIHBN1, EID
163 *ERROR3  IHRP,MAC 26, EIHBN1
164 *ERROR4  IHRP,MAC 26, EIHBN1
165 *ERROR5  IHRP,MAC 26, EIHBN1
166 *ERROR6  IHRP,MAC 26, EIHBN1
167 *ERROR7  IHRP,MAC 26, EIHBN1
168 *ERROR8  IHRP,MAC 26, EIHBN1
169 *ERROR9  IHRP,MAC 26, EIHBN1
170 *ERROR10 IHRP,MAC 26, EIHBN1
171 *ERROR11 IHRP,MAC 26, EIHBN1
172 *ERROR12 IHRP,MAC 26, EIHBN1
173 *ERROR13 IHRP,MAC 26, EIHBN1
174 *ERROR14 IHRP,MAC 26, EIHBN1
175 *ERROR15 IHRP,MAC 26, EIHBN1
176 *ERROR16 IHRP,MAC 26, EIHBN1
177 *ERROR17 IHRP,MAC 26, EIHBN1
178 *ERROR18 IHRP,MAC 26, EIHBN1
179 *ERROR19 IHRP,MAC 26, EIHBN1
180 *ERROR20 IHRP,MAC 26, EIHBN1
181 *ERROR21 IHRP,MAC 26, EIHBN1
182 *ERROR22 IHRP,MAC 26, EIHBN1
183 *ERROR23 IHRP,MAC 26, EIHBN1
184 *ERROR24 IHRP,MAC 26, EIHBN1
185 *ERROR25 IHRP,MAC 26, EIHBN1
186 *ERROR26 IHRP,MAC 26, EIHBN1
187 *ERROR27 IHRP,MAC 26, EIHBN1
188 *ERROR28 IHRP,MAC 26, EIHBN1
189 *ERROR29 IHRP,MAC 26, EIHBN1
190 *ERROR30 IHRP,MAC 26, EIHBN1
191 *ERROR31 IHRP,MAC 26, EIHBN1
192 *ERROR32 IHRP,MAC 26, EIHBN1
193 *ERROR33 IHRP,MAC 26, EIHBN1
194 *ERROR34 IHRP,MAC 26, EIHBN1
195 *ERROR35 IHRP,MAC 26, EIHBN1
196 *ERROR36 IHRP,MAC 26, EIHBN1
197 *ERROR37 IHRP,MAC 26, EIHBN1
198 *ERROR38 IHRP,MAC 26, EIHBN1
199 *ERROR39 IHRP,MAC 26, EIHBN1
200 *ERROR40 IHRP,MAC 26, EIHBN1

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201 AIF (*6AA*(1,1) EQ *(*) .ERRORZ *2D41560
202 DC *6IHSWA.C000000* SET VL SWITCH BIT *2D41570
203 DC AL3(EOPRND$(EB+2)) PR0B.,PR0G.,PARAMETER *2D41580
204 AGO .END *2D41590
205 DC *6IHSWA.C0000000* SFT VL SWITCH BIT *2D41600
206 DC AL3(0) PR0B., PR0G., PARAMETER *2D41610
207 .AG0 .END *2D41620
208 AIF (*6OPRND$(1,1) NE *(*) .JIPC *2D41630
209 AIF (*6OPRND$(2,1) EQ *(*) .SKIPA *2D41640
210 .L00PC AIF (*6OPRND$(EB+1) EQ *(*) .SKIPA *2D41650
211 .6AA SETC *6OPRND$(EB+1)* *2D41660
212 AIF (*6AA*(1,1) NE *(*) .SKIPA *2D41670
213 .6A SETA K*6OPRND$(EB+1) *2D41680
214 .6A SETA .EA-2 *2D41690
215 .6RH SETC *6OPRND$(EB+1)*(?,6A) *2D41700
216 ST .ERR.,EGNAME+6C *2D41710
217 AIF (EB+1 EQ &ATTRN).THRU STORE INTO PARAM. LIST *2D41720
218 .6R SETA .EA+1 *2D41730
219 .6C SETA .6C+4 *2D41740
220 .AG0 .L00PC *2D41750
221 AIF (.NOT &IHSWA).CONT0N *2D41760
222 AIF (*6OPRND$(EB+1) EQ *(*) .CONT0N *2D41770
223 AIF (*6OPRND$(EB+1)*(1,1) NE *(*) .CONT0N *2D41780
224 MVI .6GNAME+6C,X*90* SET LAST WORD BIT 0N *2D41790
225 .CONT0N 0,+6C *2D41800
226 RAL I.*6GNAME.A *2D41810
227 EQU * (6ATTRN GT 1).L00P2 *2D41820
228 AIF (6ATTRN GT 1).L00P2 *2D41830
229 .6C 0-1 *2D41840
230 .AG0 .NEAR00N *2D41850
231 .L00P2 AIF (*6OPRND$(1,2) EQ *(*) .SKIPB *2D41860
232 .L00PD AIF (*6OPRND$(6D+1) EQ *(*) .SKIPA *2D41870
233 .6AA SETC *6OPRND$(6D+1)* *2D41880
234 AIF (*6AA*(1,1) EQ *(*) .SKIPA *2D41890
235 DC A(*6OPRND$(6D+1)) PR0B.,PR0G.,PARAMETER *2D41900
236 .AG0 .NEXTSTP *2D41910
237 DC A(0) PR0B., PARAMETER *2D41920
238 .NEXTSTP AIF (6D+? EQ &ATTRN).NEAR00N *2D41930
239 .6D SETA .6D+1 *2D41940
240 .AG0 .L00PD *2D41950
241 .NEAR00N AIF (*6OPRND$(6D+2)* EQ *(*) .SKIPF *2D41960
242 AIF (*6OPRND$(6D+2)*(1,1) EQ *(*) .SKIPF *2D41970
243 DC *6IHSWA.C000000* SET VL SWITCH BIT *2D41980
244 DC AL3(6OPRND$(6D+2)) PR0B., PR0G., PARAMETER *2D41990
245 .AG0 .END0F *2D42000
246 DC *6IHSWA.C0000000* SET VL SWITCH BIT *2D42010
247 DC AL3(0) PR0B., PR0G., PARAMETER *2D42020
248 .AG0 .END0F *2D42030
249 DC A(0) PR0B., PARAMETER *2D42040
250 .ANGP *2D42050

```

```

251 EQUAME+4 EQU 7
252 AGO
253 AIF (NEOF NE 2).ERR=PI
254 AIF (NEM(1) NE (F)).ERR=RI
255 I=I+1;N=1;S=2)
256 AIF (EOPRND(S(E+1)).END
257 AIF (EIPRND(S(E+1)).CONT
258 AIF (EOPRND(S(E+1)) NE (F)).LOR=PA
259 AIF (EOPRND(S(E+1)) EQ (F)).CONT
260 AIF (EOPRND(S(E+1)) EQ (F)).CONT
261 EAA
262 AIF (EAA*(1+1) EQ (F)).ISRF
263 EA
264 LA EA,EOPRND(S(E+1)) PICKUP PARAMETER
265 AGO
266 ANOP
267 SCA EA
268 SCA EA-2
269 EBA
270 AIF (EOPRND(S(E+1)) EQ (F)).CONT
271 G=BACK
272 EA
273 LR EA,EBA
274 C=INTE
275 AIF (EBA+1 EQ EATPN).ALLDUN
276 AIF (EOPRND(S(E+1)).CONT
277 EC
278 AIF (EOPRND(S(E+1)).CONT
279 AIF (EBA+1 EQ EATRN).CONTXX
280 AIF (EOPRND(S(E+2)) NE (F)).BACK
281 CONTXX
282 ST EBA,EI,(0,1)
283 AGO
284 ANOP
285 EC
286 SCA EA
287 SCA EA
288 EBA
289 AIF (EOPRND(S(E+1)).CONT
290 AIF (EOPRND(S(E+1)).CONT
291 ST 14,EI,(0,1)
292 AGO
293 STM 14,15,EI,(1)
294 AGO
295 AIF (EOPRND(S(E+1)).CONT
296 INCRTF
297 AIF (EBA+1 EQ EATRN).QUIT
298 EC
299 EBA
300 EBA

```

```

*2042060
*2042070
*2042080
*2042090
*2042100
*2042110
*2042120
*2042130
*2042140
*2042150
*2042160
*2042170
*2042180
*2042190
*2042200
*2042210
*2042220
*2042230
*2042240
*2042250
*2042260
*2042270
*2042280
*2042290
*2042300
*2042310
*2042320
*2042330
*2042340
*2042350
*2042360
*2042370
*2042380
*2042390
*2042400
*2042410
*2042420
*2042430
*2042440
*2042450
*2042460
*2042470
*2042480
*2042490
*2042500
*2042510
*2042520
*2042530
*2042540
*2042550

```

LOAD PERS I WITH LIST ADDR

PICK UP PARAMETER

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

```

301 .SFTA 5,0 *2042560
302 .LNOA *2042570
303 .ALLDUN (*&C NF 0).CONTJ *2042580
304 ST 14,6F.(0,1) STORE INTO PARAM. LIST *2042590
305 .QUIT *2042600
306 .CONTJ *2042610
307 .EA *2042620
308 .SFTA 6C+14 *2042630
309 .STM 14,6A,6E.(1) *2042640
310 .QUIT *2042650
311 .CONTC (*&OPRND*(1,1) NE *(*)).LNOA *2042660
312 .LNOA (*&OPRND*(2,1) EQ *(*)).CONTK *2042670
313 .EA (*&OPRND*(4+1) EQ *(*)).CONTK *2042680
314 .SFTA (*&AA*(1,1) EQ *(*)).ISAREGA *2042690
315 .LA (*&OPRND*(8+1) PICKUP PARAMETER *2042700
316 .ST 0,6D.(0,1) STORE INTO PARAM. LIST *2042710
317 .CONTK *2042720
318 .ISAREGA ANJP *2042730
319 .EA SETA *2042740
320 .EA *2042750
321 .SFTA (*&OPRND*(8+1) *2042760
322 .SFTA (*&A-2) *2042770
323 .CONTK (*&OPRND*(8+1) *2042780
324 .SFTA (*&B,6D.(0,1) *2042790
325 .SFTA (*&A+1) *2042800
326 .SFTA (*&D+4) *2042810
327 .AGJ .LNOA *2042820
328 .SFTA (*&AIF (NOT 5,1HRSMAI).END *2042830
329 .MVI 6A.(1),X*90 *2042840
330 .AGJ *2042850
331 .ANJP *2042860
332 .MEND *2042870
333 .MACRO *2042880
334 .IHRINRA 6A,6B *2042890
335 .AIF (*&A EQ * OR *6A, EQ *(1)).NAMEIT *2042900
336 .AIF (*&A*(1,1) EQ *(*)).REGA *2042910
337 .LA 1,6A LOAD PARAMETER REG 1 *2042920
338 .CHKR *2042930
339 .AGJ *2042940
340 .ANJP LOAD PARAMETER REG 1 *2042950
341 .LP .CHKR *2042960
342 .AGJ (*&NAME, FO *).CHKR *2042970
343 .NAMEIT AIF (*&NAME, FO *).CHKR *2042980
344 .DS JH *2042990
345 .AIF (*&H EQ * OR *6A, EQ *(0)).END *2043000
346 .AIF (*&B*(1,1) EQ *(*)).REGR LOAD PARAMETER REG 0 *2043010
347 .LA 0,6B *2043020
348 .AGJ *2043030
349 .LR 0,6R(1) LOAD PARAMETER REG 0 *2043040
350 .MEND *2043050

```

```

351      .NEXT
352      LCL
353      LCL
354      SETL
355      AIF (EA GT 17)*JCAP
356      AIF (EA GT 04)*NEXT
357      AIF (EA EQ 11)*E24
358      AIF (EA LF 13)*F13
359      AIF (EA F 2)*F24
360      AIF (EA L 25)*F25
361      AIF (EA EQ 26)*E26
362      AIF (EA EQ 27)*E27
363      AIF (EA F 31)*F31
364      AIF (EA L 34)*E34
365      AIF (EA F 42)*F42
366      AIF (EA LF 46)*E46
367      AIF (EA F 47)*E47
368      AIF (EA EQ 57)*E52
369      AIF (EA LF 57)*E57
370      AIF (EA F 61)*E61
371      AIF (EA F 61)*E61
372      AIF (EA LF 67)*E67
373      AIF (EA F 69)*E69
374      AIF (EA F 71)*E71
375      AIF (EA F 72)*E72
376      AIF (EA F 73)*E73
377      AIF (EA F 73)*E74
378      AIF (EA F 75)*E75
379      AIF (EA F 73)*E78
380      AIF (EA EQ 84)*E84
381      AIF (EA EQ 87)*E87
382      AIF (EA EQ 88)*E88
383      AIF (EA EQ 89)*E89
384      AIF (EA EQ 90)*E90
385      AIF (EA EQ 91)*E91
386      AIF (EA EQ 92)*E92
387      AIF (EA F 93)*E93
388      AIF (EA EQ 94)*E94
389      AIF (EA EQ 95)*E95
390      AIF (EA LF 147)*JCRJ
391      AIF (EA LE 157)*JCRJ
392      AIF (EA EQ 158)*JCRJ
393      AIF (EA EQ 159)*JCRJ
394      AIF (EA EQ 160)*JCRF
395      AIF (EA EQ 161)*JCRF
396      AIF (EA EQ 162)*JCRG
397      AIF (EA EQ 163)*JCRH
398      AIF (EA EQ 164)*JCRI
399      AIF (EA EQ 165)*JCRJ
400      AIF (EA EQ 166)*JCRK

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      .NEXT

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      .NEXT

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      .NEXT

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401	AIF	(EA EQ 167).DCRQ	*2D43560
402	AIF	(EA EQ 168).DCRP	*2D43570
403	AIF	(EA EQ 169).DCRS	*2D43580
404	AIF	(EA EQ 170).DCRL	*2D43590
405	AIF	(EA EQ 171).DCRM	*2D43600
406	AIF	(EA EQ 172).DCRN	*2D43610
407	AIF	(EA EQ 173).DCRN	*2D43620
408	AIF	(EA EQ 174).DCRP	*2D43630
409	AIF	(EA EQ 175).DCRAE	*2D43640
410	AIF	(EA EQ 176).DCRAA	*2D43650
411	AIF	(EA EQ 177).DCRAH	*2D43660
412	AIF	(EA EQ 178).DCRAC	*2D43670
413	AIF	(EA EQ 179).DCRAN	*2D43680
414	AIF	(EA EQ 180).E180	*2D43690
415	AIF	(EA EQ 181).E181	*2D43700
416	AIF	(EA EQ 182).E182	*2D43710
417	AIF	(EA EQ 183).E183	*2D43720
418	AIF	(EA EQ 184).E184	*2D43730
419	AIF	(EA EQ 185).E185	*2D43740
420	AIF	(EA EQ 186).E186	*2D43750
421	MNITE	9,EC.064 UMASK OPERAND REQUIRES AERR OPERAND*	*2D43760
422	MEXIT		*2D43770
423	MNITE	4,EC.050 EA OPTPRAND INCONSISTENT-IGNORED*	*2D43780
424	MEXIT		*2D43790
425	MNITE	8,EC.051 ED INVALID CODE FOR EA-IGNORED*	*2D43800
426	MEXIT		*2D43810
427	MNITE	12,EC.052 DSDRG OMITTED*	*2D43820
428	MEXIT		*2D43830
429	MNITE	12,EC.053 ED INVALID CODE FOR DSDRG*	*2D43840
430	MEXIT		*2D43850
431	MNITE	3,EC.054 ED INVALID DSDRG QUALIFIER-IGNORED*	*2D43860
432	MEXIT		*2D43870
433	MNITE	9,EC.055 MACRF NOT SPECIFIED-EXCP ASSUMED*	*2D43880
434	MEXIT		*2D43890
435	MNITE	3,EC.056 ED OF MACRF INVALID WITH DSDRG=EE-IGNORED*	*2D43900
436	MEXIT		*2D43910
437	MNITE	9,EC.057 ED INVALID QUALIFIER FOR EE OF MACRF IF DSDRG=EE-IGNORED*	*2D43920
438	MEXIT		*2D43930
439	MNITE	8,EC.058 ED OF RECFM INVALID WITH DSDRG=EE-IGNORED*	*2D43940
440	MEXIT		*2D43950
441	MNITE	3,EC.059 ED OF OPTCD INVALID WITH DSDRG=EE-IGNORED*	*2D43960
442	MEXIT		*2D43970
443	MNITE	9,EC.060 ED INVALID CODE FOR DFVD WITH DSDRG=EE-IGNORED*	*2D43980
444	MEXIT		*2D43990
445	MNITE		*2D44000
446	MEXIT		*2D44010
447	MNITE	9,EC.065 MACRF=ED INVALID-EXCP ASSUMED*	*2D44020
448	MEXIT		*2D44030
449	MNITE	12,EC.064 INCONSISTENT OPERAND*	*2D44040
450	MEXIT		*2D44050

```

451 .DCRA MEXIT *,*EC.067 *NO VALUE PROVIDEDLY USED*
452 MEXIT *2044070
453 MEXIT *,*EC.063 *NO VALUE SUPPL. SPECIFIED-EXCP ASSUMED*
454 MEXIT *2044080
455 MEXIT *,*EC.069 *EVID NOT SPECIFIED-ALL ASSUMED*
456 MEXIT *2044100
457 MEXIT *,*EC.061 *DDNAME NOT SPECIFIED*
458 MEXIT *2044120
459 MEXIT *,*EC.062 *DDNAME LONG-TRUNCATED TO 3 CHAR*
460 MEXIT *2044140
461 MEXIT *,*EC.063 *DDNAME SHORT-ADDED TO 4 CHAR*
462 MEXIT *2044160
463 MEXIT *2044180
464 MEXIT *,*EC.070 *D) TOO LONG FOR EH-TRUNCATED TO 2 CHAR*
465 MEXIT *2044200
466 MEXIT *,*EC.071 *D) TOO SHORT FOR EH-PADDED TO 2 CHAR*
467 MEXIT *2044220
468 MEXIT *,*EC.072 *E) NOT SPECIFIED-PEDEST TO 80*
469 MEXIT *2044240
470 MEXIT *,*EC.073 *A)RR OPERAND EQUIVES UMASK OPERAND*
471 MEXIT *2044260
472 MEXIT *2044270
473 MEXIT *2044280
474 MEXIT *2044290
475 MEXIT *2044300
476 MEXIT *2044310
477 MEXIT *2044320
478 MEXIT *2044330
479 MEXIT *2044340
480 MEXIT *2044350
481 MEXIT *2044360
482 MEXIT *2044370
483 MEXIT *2044380
484 MEXIT *2044390
485 MEXIT *2044400
486 MEXIT *2044410
487 MEXIT *2044420
488 MEXIT *2044430
489 MEXIT *2044440
490 MEXIT *2044450
491 MEXIT *2044460
492 MEXIT *2044470
493 MEXIT *2044480
494 MEXIT *2044490
495 MEXIT *2044500
496 MEXIT *2044510
497 MEXIT *2044520
498 MEXIT *2044530
499 MEXIT *2044540
500 MEXIT *2044550

```

Bitwise Logical Routines (LAND and LOR) (page 10 of 15)

501		MEXIT			*2044560
502	.E26	MNOTE	12,'&C.001	ENTRY SYMBOL REQ'D-NOT SPECIFIED*	*2044570
503		MEXIT			*2044580
504	.E27	MNOTE	12,'&C.001	ENTRY PT. ADR. OPERAND REQ'D-NOT SPECIFIED*	*2044590
505		MEXIT			*2044600
506	.E31	MNOTE	12,'&C.001	EP,EPLDC,OR DE OPERAND REQ'D-NOT SPECIFIED*	*2044610
507		MEXIT			*2044620
508	.F34	ANOP			*2044630
509	&C(1)	SETC	'CODE'		*2044640
510	&G(2)	SFTC	'COUNT'		*2044650
511	&G(3)	SETC	'QFL'		*2044660
512	&C(5)	SFTC	'TERMINAL'		*2044670
513	&C(6)	SFTC	'LINE'		*2044680
514	&G(7)	SETC	'LIST'		*2044690
515	&G(12)	SFTC	'LIST'		*2044700
516	&G(13)	SFTC	'NUMBER'		*2044710
517		MNOTE	12,'&C.001	&G(&A-27) &G(&A-20) OPERAND REQ'D-NOT SPECIFIED*	*2044720
518					*2044730
519		MEXIT			*2044740
520	.E42	MNOTE	12,'&C.002	INVALID EP OR EPLDC OPERAND SPECIFIED-ED*	*2044750
521		MEXIT			*2044760
522	.E46	ANOP			*2044770
523	&G(1)	SETC	'MF'		*2044780
524	&G(2)	SETC	'FIRST'		*2044790
525	&G(3)	SETC	'SECOND'		*2044800
526	&G(4)	SETC	'THIRD'		*2044810
527	&G(5)	SFTC	'FOURTH'		*2044820
528	&G(6)	SETC	'IOP'		*2044830
529	&G(7)	SETC	'SF'		*2044840
530	&G(9)	SETC	'FUNCTION'		*2044850
531	&C(10)	SETC	'LENGTH'		*2044860
532	&G(11)	SETC	'MODE'		*2044870
533		MNOTE	12,'&C.002	INVALID &G(&A-34) OPERAND SPECIFIED-ED*	*2044880
534		MEXIT			*2044890
535	.E47	MNOTE	12,'&C.002	INVALID AREA OR LENGTH OPERAND SPECIFIED-ED*	*2044900
536		MEXIT			*2044910
537	.F52	MNOTE	12,'&C.001	OPTION THREE OPERAND REQ'D-NOT SPECIFIED*	*2044920
538		MEXIT			*2044930
539	.E57	ANOP			*2044940
540	&G(1)	SFTC	'TYPE'		*2044950
541	&G(2)	SFTC	'OPTION'		*2044960
542	&G(3)	SFTC	'OPTION 1'		*2044970
543	&G(4)	SETC	'OPTION 2'		*2044980
544	&G(6)	SETC	'OPTION 3'		*2044990
545	&G(7)	SFTC	'KEYWORD'		*2045000
546		MNOTE	12,'&C.002	INVALID &G(&A-47) OPERAND SPECIFIED-ED*	*2045010
547		MEXIT			*2045020
548	.F60	MNOTE	12,'&C.023	INVALID OPERAND THREE W/SCRATCH SPEC.-ED*	*2045030
549		MEXIT			*2045040
550	.E61	MNOTE	12,'&C.005	INVALID REGISTER NOTATION IN RC OPERAND-ED*	*2045050


```

601      S*
602      MEXIT *,%C.077  ER INVALID-RESET TO 50*
603      MEXIT
604      MEXIT *,%C.079  CURRENT RUFFER ER = 80*
605      MEXIT
606      MEXIT *,%C.079  CURRENT REAM POSITION COUNTER IS X=ER, Y=80*
607      MEXIT
608      MEXIT *,%C.08J  ER COUNTER EXCEEDS CRT LIMITS*
609      MEXIT
610      MEND
611      THCLGIC START J
612      ENTRY AND,LAND,OR,LOR,X'OR,LXOR,COMPL,LCOMPL,SHFTL,SHFTR
613      *
614      *CALLING SEQUENCE
615      LA S,SAVLDC
616      LA A,ARGLST
617      L L,V(IFCN)
618      BALR R,L
619      *
620      *SAVLCC IS THE LOCATION OF A REGISTER STOPPAGE AREA,
621      *AND ARGLST IS OF THE FOLLOWING FORM...
622      DC AL4(ARGL1)
623      DC AL4(ARGL2)
624      *
625      *ERROR CONDITIONS
626      *
627      *
628      *
629      *
630      S
631      EQU 14
632      EQU 15
633      EQU 1
634      ARGADD1 EQU 2
635      ARGADD2 EQU 3
636      RESULT EQU J
637      EXEC EQU 4
638      INTEGER EQU 0
639      REAL EQU 1
640      EJECT
641      *
642      *
643      AND
644      SAVE (14,4),T,AND
645      MVI SWITCH,REAL
646      EXEC,FXNR
647      R
648      *
649      USING LAND,L
650      SAVE (14,4),T,LAND
651      MVI SWITCH,INTEGER

```

```

*2045550
*2045570
*2045580
*2045590
*2045600
*2045610
*2045620
*2045630
*2045640
*2045650
*2045660
*2045670
*2045680
*2045690
*2045700
*2045710
*2045720
*2045730
*2045740
*2045750
*2045760
*2045770
*2045780
*2045790
*2045800
*2045810
*2045820
*2045830
*2045840
*2045850
*2045860
*2045870
*2045880
*2045890
*2045900
*2045910
*2045920
*2045930
*2045940
*2045950
*2045960
*2045970
*2045980
*2045990
*2046000
*2046010
*2046020
*2046030
*2046040
*2046050

```

```

651      L3      EXEC,FXR
652      H      COMMON
653      *
654      USING L3,L
655      SAVE (14,4),T,L3
656      MVI SWITCH,REAL
657      LA      EXEC,FXR
658      B      COMMON
659      *
660      USING L3,L
661      SAVE (14,4),T,L3
662      MVI SWITCH,INTEGER
663      LA      EXEC,FXR
664      B      COMMON
665      *
666      USING XOR,L
667      SAVE (14,4),T,XOR
668      MVI SWITCH,REAL
669      LA      EXEC,FXR
670      B      COMMON
671      *
672      USING L3,L
673      SAVE (14,4),T,L3
674      MVI SWITCH,INTEGER
675      LA      EXEC,FXR
676      B      COMMON
677      *
678      USING COMPL,L
679      SAVE (14,4),T,COMPL
680      MVI SWITCH,REAL
681      LA      EXEC,FXR
682      B      COMMON
683      *
684      USING LCOMPL,L
685      SAVE (14,4),T,LCOMPL
686      MVI SWITCH,INTEGER
687      LA      EXEC,FXR
688      BALR L,0
689      USING *,L
690      LA      ARGADD1,0(A) LOAD ADDRESS OF FIRST ARGUMENT
691      LA      ARGADD2,ALLOPES
692      B      COMMON#
693      *
694      USING SHFT,L
695      SAVE (14,4),T,SHFTL
696      MVI SWITCH,INTEGER
697      LA      EXEC,FXR
698      B      COMMON
699      *
700      USING SHFTR,L

```

EXCLUSIVE OR (BITWISE)

IS ACTUALLY A BITWISE XOR WITH -1.

701	SHIFT	SAVE	(1,4),T,SHFT
702		MVT	SWITCH,INTEGER
703		LA	EXEC,FXSRL
704	*		
705	COMMON	LM	ARGADD1,ARGADD2,0(A)
706	COMMON#	L	0(,ARGADD1)
707		L	1,0(,ARGADD2)
708		RALR	L,0
709		USING	*,L
710		EX	0(,EXEC)
711		ST	RESULT,TEMP
712		TM	SWITCH,PFAL
713		RZ	NTREAL
714		LF	RESULT,TEMP
715			RETURN(0,4),T
716	*		
717	NCTRFL		RETURN(1,4),T
718	*		
719	TEMP	DS	F
720	ALLONES	DC	F'-1'
721	EXNP	NR	0,1
722	EXDP	OR	0,1
723	EXXR	XP	0,1
724	FXSLL	SLL	0,0(1)
725	EXSPL	SRL	0,0(1)
726	SWITCH	DS	X
727		END	

*2D46560
 *2D46570
 *2D46580
 *2D46590
 *2D46600
 *2D46610
 *2D46620
 *2D46630
 *2D46640
 *2D46650
 *2D46660
 *2D46670
 *2D46680
 *2D46690
 *2D46700
 *2D46710
 *2D46720
 *2D46730
 *2D46740
 *2D46750
 *2D46760
 *2D46770
 *2D46780
 *2D46790
 *2D46800
 *2D46810
 *2D46820


```

51 MAC=PI1
52 IHR0PLST ENULL, EOPRND5, ENAME, F, MF=I
53 GBLH EIH8SWA, EIH8SWR
54 GBLC EIH8ND
55 LCLC ENAME, EA, EB
56 LCLA EA, EB, EC, ED, EF, EATTRN
57 EATTRN V*EOPRND5
58 EENAME EIH8, E8SYNDX,
59 AIF (E, MF, EQ 'L', CCNTA
60 AIF (E, MF, EQ 'I', IROUT
61 AGO .EROUT
62 IHR0RMAC 35, EIH8ND, SMF MF PARAMETER, RAD
63 IHR0RMAC 69, EIH8ND REF, NOT, W/ MF=L
64 MPXIT
65 AIF (E, NAME, EQ ' '), NUNAME
66 OS JF
67 ANNP (EOPRND5(1,1)) NE '(', CONTX
68 AIF (EOPRND5(2,1)) EQ ' ', SKIPC
69 AIF (EATTRN GT 1), LROUT
70 SETA 0-1
71 AGO .NEAREND
72 AIF (EOPRND5(EA+1)) EQ ' ', SKIPC
73 SETC (EOPRND5(EB+1))
74 AIF (EAA(1,1)) EQ '(', FRR0K2
75 DC A(EOPRND5(EA+1)) PR0R, PR0G, PARAMETER
76 AGO .AROUND
77 DC A(0) PR0R, PR0G, PARAMETER
78 AIF (EA+2 EQ EATTRN), NFAREND
79 SETA EA+1
80 AGO .LROUT
81 AIF (EOPRND5(EA+2)) EQ ' ', SKIPC
82 SETC (EOPRND5(EA+2))
83 AIF (EAA(1,1)) EQ '(', EPR0R2
84 DC A(EIH8SWA, 000000) SET VL SWITCH BIT
85 DC AL3(EOPRND5(EA+2)) PR0R, PR0G, PARAMETER
86 AGO .END
87 DC A(EIH8SWA, 000000) SET VL SWITCH BIT
88 DC AL3(0) PR0R, PR0G, PARAMETER
89 AGO .END
90 AIF (EOPRND5(1,1)) NE '(', LDDPC
91 AIF (EOPRND5(2,1)) EQ ' ', SKIPA
92 AIF (EOPRND5(EB+1)) EQ ' ', SKIPA
93 SETC (EOPRND5(EA+1))
94 AIF (EAA(1,1)) NE '(', SKIPA
95 SETA K(EOPRND5(EA+1))
96 EA EA-2
97 SETA (EOPRND5(EA+1))(2, EA)
98 SETC (EOPRND5(EA+1))
99 ST EBB, EENAME+EC
100 ST EBB INTO PARAM, LIST

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```

101 .SKIPR AT (E+1 EQ 5)ITD(0).END
102 EP S+1
103 EC EC+4
104 EC
105 .L LOOP
106 .THE H (MDT E+HRS*W).CONTIN
107 AIF (EOPRND5(E+1)) EQ '(*)'.CONTIN
108 AIF (EOPRND5(E+1))(1,1) NE '(*)'.CONTIN
109 .CONTIN CNTR 0+4
110 .L LOOP
111 .L LOOP
112 AIF (EATRN GT 1).LORP2
113 SETA 0-1
114 .NPARIN
115 .LORP2 AIF (EOPRND5(1,2) EQ '(*)'.SKIPR
116 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
117 .LORP2 AIF (EOPRND5(E+1))
118 .LORP2 AIF (EAAA(1,1) EQ '(*)'.SKIPR
119 .LORP2 AIF (EOPRND5(E+1)) PRD%P+1).PARAMETER-0
120 .LORP2 AIF (EOPRND5(E+1)) PRD%P+1).PARAMETER-0
121 .SKIPR DC A(0) EQ EATRN).NPARIN
122 .NEXTSTP AIF (EOPRND5(E+1)) PRD%P+1).PARAMETER-0
123 EC
124 .LORP2 AIF (EOPRND5(E+1)) PRD%P+1).PARAMETER-0
125 .NPARIN AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
126 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
127 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
128 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
129 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
130 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
131 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
132 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
133 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
134 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
135 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
136 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
137 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
138 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
139 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
140 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
141 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
142 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
143 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
144 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
145 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
146 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
147 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
148 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
149 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR
150 .LORP2 AIF (EOPRND5(E+1)) EQ '(*)'.SKIPR

```

```

151 EA          SETA          <EOPRND5(ER+1)
152 EA          EA-2
153 EBB         SETC          (EOPRND5(EB+1))*(2,EA)
154           AIF          (EC FJ 0).CONTQQ
155           ANOP
156 EA         SETA          EC+14
157           LR          EA,EB
158           AIF          (ER+1 EQ EATTRN).ALLDUN
159           AIF          (EC EQ 0-14).CONTF
160           AIF          (EC FQ 1).CONTG
161 EC         SETA          EC+1
162           AGO
163           AIF          (EB+1 EQ EATTRN).CONTXX
164           AIF          (EOPRND5(ER+2)) NE **).CORACK
165           ANOP
166           ST          ER,EE,(0,1)
167           AGO
168           ANOP
169 EC         SETA          J-14
170           ANTP
171 EB         SETA          EB+1
172 ED         ED*4
173           AGO
174           AIF          (EC EQ 0).INCRMT
175           AIF          (EC NE 1).PUTTWO
176           ST          I,EE,(0,1)
177           AGO
178           ST*         I,EE,(1)
179           AGO
180           ST*         I,EE,(1)
181           AIF          (ER+1 EQ EATTRN).QUIT
182 EC         SETA          ER+1
183 ER         SETA          ED*4
184 ED         SETA          ED
185 EE         AGO
186           ALLDUN
187           AIF          (EC NE 0).CONTJ
188           ST          I,EE,(0,1)
189           AGO
190           ANOP
191 EA         SETA          EC+14
192           ST*         I,EA,EE,(1)
193           AGO
194           AIF          (EOPRND5(1,1) NE **).LOOPE
195           AIF          (EOPRND5(2,1) EQ **).CONTK
196           AIF          (EOPRND5(ER+1) EQ **).CONTK
197           SETC          (EOPRND5(EB+1))
198           AIF          (EAA*(1,1) EQ **).ISARFGA
199           LA          0,EOPRND5(ER+1) PICKUP PARAMETER
200           ST          0,ED,(0,1) STORE INTO PARAM. LIST

```

```

*2D48330
*2D48340
*2D48350
*2D48360
*2D48370
*2D48380
*2D48390
*2D48400
*2D48410
*2D48420
*2D48430
*2D48440
*2D48450
*2D48460
*2D48470
*2D48490
*2D48500
*2D48510
*2D48520
*2D48530
*2D48540
*2D48550
*2D48560
*2D48570
*2D48580
*2D48590
*2D48600
*2D48610
*2D48620
*2D48630
*2D48640
*2D48650
*2D48660
*2D48670
*2D48680
*2D48690
*2D48700
*2D48710
*2D48720
*2D48730
*2D48740
*2D48750
*2D48760
*2D48770
*2D48780
*2D48790
*2D48800
*2D48810
*2D48820

```

PICK UP PARAMETER

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

STORE INTO PARAM. LIST

```

201      A,IP      .CONTK
202      .ISAREGA  A,IP
203      &F      SFTA K*EQ*ANDS(64+1)
204      &A      SETA &A-2
205      &EP      SETC EOP*ANDS(64+1)*(?,&A)
206      .CONTK  ST  238,LD,(0,1)
207      &EP      AIF (6R+1 EQ EATTRN).QUIT
208      &D      SETA 6R+1
209      &D      SETA 6D+4
210      &D      .LOADK
211      .QUIT   AIF (NOT 6THRS*4).ENF
212      &A      SFTA EATTRN*4-4
213      .CONTK MVI 6A,(1),X*4)*
214      .END
215      .END
216      .END
217      .MACRO
218      .NAME   IHR*INRA &A,&ER
219      AIF ((6A) EQ ** IHR *6A* EQ *(1)*).NAMEIT
220      AIF ((6A*(1,1) EQ *(1).RECA
221      LA 1,&A      LPAD PARAMETER PEG 1
222      .CHK3
223      .REGA   A,GJ
224      .NAME   LR 1,&A(1)      LOAD PARAMETER PEG 1
225      .CHKR
226      AIF ((6A*EQ EQ **).CHKR
227      .NAME   OS JH
228      .CHKR  AIF ((6R) EQ ** OR *6R* EQ *(0)*).END
229      AIF ((6R*(1,1) EQ *(1).REGR
230      LA 0,&R      LOAD PARAMETER PEG 0
231      .REGH   A,GJ 0,&R(1)      LOAD PARAMETER PEG 0
232      .END
233      .END
234      .MACRO
235      IHR*MAC &A,&ER,&D,&E,&F,&G
236      LCLC  &G(14)
237      LCLC  &C
238      SETC  ***** IHR*
239      AIF ((6A GT 179).GRAP
240      AIF ((6A GT 99).NEXT
241      AIF ((6A EQ 1).E24
242      AIF ((6A LF 13).F13
243      AIF ((6A EQ 24).E24
244      AIF ((6A LE 25).E25
245      AIF ((6A EQ 24).E26
246      AIF ((6A EQ 27).E27
247      AIF ((6A EQ 31).E31
248      AIF ((6A LF 34).E34
249      AIF ((6A EQ 42).E42
250      AIF ((6A LF 45).E44

```

STOP INTO PAPAM. LIST

SET LAST WORD BIT ON

```

*2048830
*2048840
*2048850
*2048860
*2048870
*2048880
*2048890
*2048900
*2048910
*2048920
*2048930
*2048940
*2048950
*2048960
*2048970
*2048980
*2048990
*2049000
*2049010
*2049020
*2049030
*2049040
*2049050
*2049060
*2049070
*2049080
*2049090
*2049100
*2049110
*2049120
*2049130
*2049140
*2049150
*2049160
*2049170
*2049180
*2049190
*2049200
*2049210
*2049220
*2049230
*2049240
*2049250
*2049260
*2049270
*2049280
*2049290
*2049300
*2049310
*2049320

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251 AIF (EA EQ 47).E47
252 AIF (EA EQ 52).E52
253 AIF (EA LF 57).E57
254 AIF (EA EQ 60).E60
255 AIF (EA EQ 61).E61
256 AIF (EA LF 67).E67
257 AIF (EA EQ 69).E69
258 AIF (EA EQ 71).E71
259 AIF (EA EQ 72).E72
260 AIF (EA EQ 73).E73
261 AIF (EA EQ 73).E74
262 AIF (EA EQ 75).E75
263 AIF (EA EQ 78).E78
264 AIF (EA EQ 84).E84
265 AIF (EA EQ 87).E87
266 AIF (EA EQ 89).E89
267 AIF (EA EQ 89).E89
268 AIF (EA EQ 90).E90
269 AIF (EA EQ 91).E91
270 AIF (EA EQ 92).E92
271 AIF (EA EQ 93).E93
272 AIF (EA EQ 94).E94
273 AIF (EA EQ 95).E95
274 AIF (EA LE 147).DCRA
275 AIF (EA LF 157).DCRB
276 AIF (EA EQ 158).DCRC
277 AIF (EA EQ 159).DCRD
278 AIF (EA EQ 160).DCRE
279 AIF (EA EQ 161).DCRF
280 AIF (EA EQ 162).DCRG
281 AIF (EA EQ 163).DCRH
282 AIF (EA EQ 164).DCRI
283 AIF (EA EQ 165).DCRJ
284 AIF (EA EQ 166).DCRK
285 AIF (EA EQ 167).DCRQ
286 AIF (EA EQ 168).DCRR
287 AIF (EA EQ 169).DCRS
288 AIF (EA EQ 170).DCRL
289 AIF (EA EQ 171).DCRM
290 AIF (EA EQ 172).DCRN
291 AIF (EA EQ 173).DCRO
292 AIF (EA EQ 174).DCRP
293 AIF (EA EQ 175).DCRAE
294 AIF (EA EQ 176).DCBAE
295 AIF (EA EQ 177).DCBAR
296 AIF (EA EQ 178).DCBAC
297 AIF (EA EQ 179).DCRAD
298 AIF (EA EQ 180).F180
299 AIF (EA EQ 181).E181
300 AIF (EA EQ 182).E182

```

.NEXT

.GRAP

```

*2049330
*2049340
*2049350
*2049360
*2049370
*2049380
*2049390
*2049400
*2049410
*2049420
*2049430
*2049440
*2049450
*2049460
*2049470
*2049480
*2049490
*2049500
*2049510
*2049520
*2049530
*2049540
*2049550
*2049560
*2049570
*2049580
*2049590
*2049600
*2049610
*2049620
*2049630
*2049640
*2049650
*2049660
*2049670
*2049680
*2049690
*2049700
*2049710
*2049720
*2049730
*2049740
*2049750
*2049760
*2049770
*2049780
*2049790
*2049800
*2049810
*2049820

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301	.DCAAE	EXIT	(6A FJ 1R3) F1R3	*2049840
302		EXIT	(6A FJ 1R4) F1R4	*2049850
303		EXIT	(6A FJ 1R5) F1R5	*2049860
304		EXIT	(6A FJ 1R6) F1R6	*2049870
305		EXIT	4, *EC.064 UNSK OPERAND REQUIRES AER OPERAND*	*2049880
306		EXIT	4, *EC.050 ER OPERAND INCONSISTENT-IGNORED*	*2049890
307	.DCPA	EXIT	3, *EC.051 ER INVALID CODE FOR ER-IGNORED*	*2049900
308		EXIT	12, *EC.052 DSORG OMITTED*	*2049910
309	.DCRA	EXIT	12, *EC.053 ER INVALID CODE FOR DSORG*	*2049920
310		EXIT	4, *EC.054 ER INVALID DSORG QUALIFIER-IGNORED*	*2049930
311	.DCAC	EXIT	9, *EC.055 MACRO NOT SPECIFIED-FXCP ASSUMED*	*2049940
312		EXIT	3, *EC.056 ER OF MACRO INVALID WITH DSORG=EF-IGNORED*	*2049950
313	.DCRD	EXIT	3, *EC.057 ER INVALID QUALIFIER FOR ER OF MACRO IF DSORG=EF-IGNORED*	*2049960
314		EXIT	=EF-IGNORED*	*2049970
315	.DCRE	EXIT	9, *EC.058 ER OF RECFM INVALID WITH DSORG=EF-IGNORED*	*2049980
316		EXIT	3, *EC.059 ER OF RECFM INVALID WITH DSORG=EF-IGNORED*	*2050000
317	.DCRF	EXIT	4, *EC.060 ER INVALID CODE FOR DEVD WITH DSORG=EF-IGNORED*	*2050010
318		EXIT	3, *EC.061 ER INVALID CODE FOR DEVD WITH DSORG=EF-IGNORED*	*2050020
319	.DCRS	EXIT	12, *EC.062 DSORG PREVIOUSLY USED*	*2050030
320		EXIT	NO VALID DSORG SPECIFIED-FXCP ASSUMED*	*2050040
321	.DCRH	EXIT	DEVD NOT SPECIFIED-ALL ASSUMED*	*2050050
322		EXIT	DEVD NOT SPECIFIED*	*2050060
323	.DCRL	EXIT	4, *EC.061 DDNAME NOT SPECIFIED*	*2050070
324		EXIT	DDNAME LONG-TRUNCATED TO 9 CHAR*	*2050080
325	.DCRJ	EXIT	4, *EC.062 DDNAME SHORT-ADDED TO 9 CHAR*	*2050090
326		EXIT	DDNAME SHORT-ADDED TO 9 CHAR*	*2050100
327	.DCRK	EXIT	ER TOO LONG FOR ER-TRUNCATED TO 7 CHAR*	*2050110
328		EXIT	ER TOO SHORT FOR ER-PADDED TO 2 CHAR*	*2050120
329		EXIT		*2050130
330	.DCRL	EXIT	MACRO=ED INVALID-EXCP ASSUMED*	*2050140
331		EXIT	INCONSISTENT OPERAND*	*2050150
332	.DCRM	EXIT	DCRD MACRO PREVIOUSLY USED*	*2050160
333		EXIT	NO VALID DSORG SPECIFIED-FXCP ASSUMED*	*2050170
334	.DCRN	EXIT	DEVD NOT SPECIFIED-ALL ASSUMED*	*2050180
335		EXIT	DEVD NOT SPECIFIED*	*2050190
336	.DCRD	EXIT	DDNAME NOT SPECIFIED*	*2050200
337		EXIT	DDNAME LONG-TRUNCATED TO 9 CHAR*	*2050210
338	.DCRP	EXIT	DDNAME SHORT-ADDED TO 9 CHAR*	*2050220
339		EXIT	DDNAME SHORT-ADDED TO 9 CHAR*	*2050230
340	.DCBQ	EXIT	DDNAME LONG-TRUNCATED TO 9 CHAR*	*2050240
341		EXIT	DDNAME SHORT-ADDED TO 9 CHAR*	*2050250
342	.DCBR	EXIT	ER TOO LONG FOR ER-TRUNCATED TO 7 CHAR*	*2050260
343		EXIT	ER TOO SHORT FOR ER-PADDED TO 2 CHAR*	*2050270
344	.DCBS	EXIT		*2050280
345		EXIT		*2050290
346	.DCBA	EXIT		*2050300
347		EXIT		*2050310
348	.DCBA	EXIT		*2050320
349		EXIT		*2050330
350		EXIT		

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351 .CCRAC MNJTE *,'&C.C7? &A NOT SPECIFIED-PRESFT T) &D*
352 MEXIT
353 MNJTE 4,'&C.C73 AEPP OPERAND 3 REQUIRES UMASK OPERAND*
354 MEXIT
355 .E13 ANJP
356 SETC 'FIRST*
357 &G(1) SETC 'SECOND*
358 &G(2) SETC 'THIRD*
359 &G(3) SETC 'FOURTH*
360 &G(4) SETC 'DCR*
361 &G(5) SETC 'DECB*
362 &G(6) SETC 'KEY*
363 &G(7) SETC 'SEEKADOK*
364 &G(8) SETC 'LOW.LIM.*
365 &G(9) SETC 'ECR*
366 &G(10) SETC 'RLKREF*
367 &G(11) SETC 'AREA*
368 MNJTE 12,'&C.001 &G(&A-1) OPERAND REQ**D-NOT SPECIFIED*
369 MEXIT
370 .F25 ANJP
371 &G(1) SETC 'LENGTH*
372 &G(2) SETC 'VALUE*
373 &G(3) SETC 'OCR*
374 &G(4) SETC 'MODE*
375 &G(5) SETC 'REGISTER*
376 &G(6) SETC 'MESSAGE*
377 &G(7) SETC 'ABFXR*
378 &G(8) SETC 'LAREL*
379 &G(9) SETC 'THLOC*
380 &G(10) SETC 'FIFLDS*
381 &G(11) SETC 'TYPE*
382 MNJTE 12,'&C.001 &G(&A-13) OPERAND REQ**D-NOT SPECIFIED*
383 MEXIT
384 .E24 MNJTE 12,'&C.004 REQUIRED OPERAND(S) NOT SPECIFIED*
385 MEXIT
386 .F26 MNJTE 12,'&C.001 ENTRY SYMBOL REQ**D-NOT SPECIFIED*
387 MEXIT
388 .F27 MNJTE 12,'&C.001 ENTRY PT. AC3. OPERAND REQ**D-NOT SPECIFIED*
389 MEXIT
390 .E31 MNJTE 12,'&C.001 FP,EPLCC,OR JE OPERAND REQ**D-NOT SPECIFIED*
391 MEXIT
392 .F34 ANJP
393 &G(1) SETC 'CODE*
394 &G(2) SETC 'COUNT*
395 &G(3) SETC 'QFL*
396 &G(4) SETC 'TERMINAL*
397 &G(5) SETC 'LINE*
398 &G(6) SETC 'LIST*
399 &G(7) SETC 'LIST*
400 &G(11) SETC 'NUMBER*

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401 *2051000 INVALID OPERAND SPECIFIED-60*
402 MEXIT
403 *2051000 INVALID OPERAND SPECIFIED-60*
404 *2051000 INVALID OPERAND SPECIFIED-60*
405 *2051000 INVALID OPERAND SPECIFIED-60*
406 *2051000 INVALID OPERAND SPECIFIED-60*
407 *2051000 INVALID OPERAND SPECIFIED-60*
408 *2051000 INVALID OPERAND SPECIFIED-60*
409 *2051000 INVALID OPERAND SPECIFIED-60*
410 *2051000 INVALID OPERAND SPECIFIED-60*
411 *2051000 INVALID OPERAND SPECIFIED-60*
412 *2051000 INVALID OPERAND SPECIFIED-60*
413 *2051000 INVALID OPERAND SPECIFIED-60*
414 *2051000 INVALID OPERAND SPECIFIED-60*
415 *2051000 INVALID OPERAND SPECIFIED-60*
416 *2051000 INVALID OPERAND SPECIFIED-60*
417 *2051000 INVALID OPERAND SPECIFIED-60*
418 *2051000 INVALID OPERAND SPECIFIED-60*
419 *2051000 INVALID OPERAND SPECIFIED-60*
420 *2051000 INVALID OPERAND SPECIFIED-60*
421 *2051000 INVALID OPERAND SPECIFIED-60*
422 *2051000 INVALID OPERAND SPECIFIED-60*
423 *2051000 INVALID OPERAND SPECIFIED-60*
424 *2051000 INVALID OPERAND SPECIFIED-60*
425 *2051000 INVALID OPERAND SPECIFIED-60*
426 *2051000 INVALID OPERAND SPECIFIED-60*
427 *2051000 INVALID OPERAND SPECIFIED-60*
428 *2051000 INVALID OPERAND SPECIFIED-60*
429 *2051000 INVALID OPERAND SPECIFIED-60*
430 *2051000 INVALID OPERAND SPECIFIED-60*
431 *2051000 INVALID OPERAND SPECIFIED-60*
432 *2051000 INVALID OPERAND SPECIFIED-60*
433 *2051000 INVALID OPERAND SPECIFIED-60*
434 *2051000 INVALID OPERAND SPECIFIED-60*
435 *2051000 INVALID OPERAND SPECIFIED-60*
436 *2051000 INVALID OPERAND SPECIFIED-60*
437 *2051000 INVALID OPERAND SPECIFIED-60*
438 *2051000 INVALID OPERAND SPECIFIED-60*
439 *2051000 INVALID OPERAND SPECIFIED-60*
440 *2051000 INVALID OPERAND SPECIFIED-60*
441 *2051000 INVALID OPERAND SPECIFIED-60*
442 *2051000 INVALID OPERAND SPECIFIED-60*
443 *2051000 INVALID OPERAND SPECIFIED-60*
444 *2051000 INVALID OPERAND SPECIFIED-60*
445 *2051000 INVALID OPERAND SPECIFIED-60*
446 *2051000 INVALID OPERAND SPECIFIED-60*
447 *2051000 INVALID OPERAND SPECIFIED-60*
448 *2051000 INVALID OPERAND SPECIFIED-60*
449 *2051000 INVALID OPERAND SPECIFIED-60*
450 *2051000 INVALID OPERAND SPECIFIED-60*

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451	.F73	MNITE	12, *EC.C05	ENTRY SYMBOL NOT ALLOWED W/MF=L*	*2051330
452		MEXIT			*2051340
453	.E74	MNITE	12, *EC.O10	ID= OPERAND INVALID W/MF=L*	*2051350
454		MEXIT			*2051350
455	.E75	MNITE	12, *EC.O11	INVALID OPERAND SPECIFIED W/SF=L*	*2051370
456		MEXIT			*2051380
457	.E78	MNITE	4, *EC.C24	CSFCT NAME OMITTED, MACRO NAME FIELD BLANK*	*2051390
458		MEXIT			*2051400
459	.E84	MNITE	12, *EC.O13	MF=L NOT ALLOWED*	*2051410
460		MEXIT			*2051420
461	.E87	MNITE	12, *EC.O14	DECR NOT SPECIFIED AS SYMBOL*	*2051430
462		MEXIT			*2051440
463	.F88	MNITE	12, *EC.O15	MORE THAN ONE OF EP,PLCC OR DE PRESENT*	*2051450
464		MEXIT			*2051460
465	.E89	MNITE	12, *EC.O16	LV OPERAND NOT ALLOWED W/SPECIFIED MDEF*	*2051470
466		MEXIT			*2051480
467	.E90	MNITE	12, *EC.O17	LA OPERAND NOT ALLOWED W/SPECIFIED MDEF*	*2051490
468		MEXIT			*2051500
469	.E91	MNITE	12, *EC.O18	ROTH LV AND LA OPERANDS SPECIFIED*	*2051510
470		MEXIT			*2051520
471	.E92	MNITE	12, *EC.O19	SP NOT ALLOWED W/LV SPECIAL REG. NOTATION*	*2051530
472		MEXIT			*2051540
473	.E93	MNITE	12, *EC.O20	A= OPERAND NOT ALLOWED IN R-TYPE MACRO*	*2051550
474		MEXIT			*2051560
475	.E94	MNITE	12, *EC.O21	MORE THAN 7 VALUES IN FIELDS OPERAND*	*2051570
476		MEXIT			*2051580
477	.F95	MNITE	12, *EC.O12	PARAM OR VL ALLOWED ONLY WITH MF=(E,ADDR)*	*2051590
478		MEXIT			*2051600
479	.E180	MNITE	*, *EC.O74	EA OPERAND INVALID OR NOT SPECIFIED)-PRESET TO X*	*2051610
480		MEXIT			*2051620
481		MEXIT			*2051630
482	.E181	MNITE	*, *EC.O75	WARNING-WRAP AROUND TO TOP OF CRT*	*2051640
483		MEXIT			*2051650
484	.E182	MNITE	*, *EC.O76	BUFFER LOCATION COUNTER EXCEEDS MAXIMUM LIMIT*	*2051660
485		MEXIT			*2051670
486		MEXIT			*2051680
487	.E183	MNITE	*, *EC.O77	EA INVALID-PRESET TO ED*	*2051690
488		MEXIT			*2051700
489	.E184	MNITE	*, *EC.O78	CURRENT BUFFER EA = ED*	*2051710
490		MEXIT			*2051720
491	.E185	MNITE	*, *EC.O79	CURRENT BEAM POSITION COUNTER IS X=EA, Y=ED*	*2051730
492		MEXIT			*2051740
493	.E186	MNITE	*, *EC.O80	EA COUNTER EXCEEDS CRT LIMITS*	*2051750
494		MEXIT			*2051760
495		MEXIT			*2051770
496	ENAME	MACRO			*2051780
497		ASSIGN	EMODE, EARGS		*2051790
498		LCLA	ENUM, EI		*2051800
499		LCLC	EM		*2051810
500		LCLC	EL, ER		*2051820
		ATF	(EMODE, NF, A*), LI		

```

501 SETC '(('
502 SETC ')('
503 ANOP
504 SETC '(('
505 AGU .L2
506 ANOP
507 SETC '(('
508 SETC ')('
509 AIF ((EMODE EQ 'Y' OR *EMODE EQ 'Q') .L5
510 AIF ((EMODE NE 'S') .L5
511 ANOP
512 SETC '(('
513 SETC ')('
514 ANOP
515 AIF ((EMODE EQ 'E') .L5
516 SETC *EMODE
517 ANOP
518 OS
519 SETA I
520 SETA N*ARGS
521 DC *MOD&L*ARGS(&I)&R
522 SETA I+1
523 AIF (&I LE &NUM).L3
524 MEND
525 MACRO
526 CALLI
527 GBLA
528 SETA &K+1
529 CNIP
530 L
531 LA 13,P4SA
532 ST 14,72(13)
533 RAS 1,DSEK
534 ASSIGN A,*ARGS
535 DC A(FIVE)
536 L
537 RASR 15,*ENT+4
538 MEND
539 *
540 MACRO
541 RN
542 RM
543 MEND
544 *
545 MACRO
546 BR
547 RCP
548 MEND
549 *
550 MACRO

```

```

*2051830
*2051840
*2051850
*2051860
*2051870
*2051880
*2051890
*2051900
*2051910
*2051920
*2051930
*2051940
*2051950
*2051960
*2051970
*2051980
*2051990
*2052000
*2052010
*2052020
*2052030
*2052040
*2052050
*2052060
*2052070
*2052080
*2052090
*2052100
*2052110
*2052120
*2052130
*2052140
*2052150
*2052160
*2052170
*2052180
*2052190
*2052200
*2052210
*2052220
*2052230
*2052240
*2052250
*2052260
*2052270
*2052280
*2052290
*2052300
*2052310
*2052320

```

```

551      EN      RNN      EA
552      EN      RNM      EA
553      MEND
554      *
555      EN      MACRO
556      EN      BZR
557      EN      BCR      9,EA
558      MEND
559      *
560      EN      MACRO
561      REP      RCR      9,EA
562      EN      MEND
563      *
564      EN      MACRO
565      RAS      EA,EB
566      ENAME   BAL      EA,EB
567      ENAME   MEND
568      *
569      ENAME   MACRO
570      ENAME   BASP
571      ENAME   RALR
572      MEND
573      *
574      ENAME   MACRO
575      RINFT    EA,EB,EC,ED
576      L        ER,EA
577      O        EP,CNVRT
578      ST       EB,T
579      LF       EC,ZERCF
580      AF       EC,T
581      SF       EC,DNFF
582      STE      EC,ED
583      MEND
584      *
585      ENAME   MACRO
586      FPBND    EFPR,EGPR
587      AE       EFPR,HALF
588      AU       EFPR,CNVRT
589      STE      EFPR,T
590      L        EGPR,T
591      SLL      EGPR,R(10)
592      SRL      EGPR,R(10)
593      MEND
594      *
595      ENAME   MACRO
596      BNFP     EGPR,EFPR
597      RCTR     EGPR,O
598      O        EGPR,CNVRT
599      LE       EGPR,ZE#OF
600      ST       EGPR,T

```

3HH

```

*2752330
*2D52340
*2D52350
*2D52360
*2D52370
*2D52380
*2D52390
*2D52400
*2D52410
*2D52420
*2D52430
*2D52440
*2D52450
*2D52460
*2D52470
*2D52480
*2D52490
*2D52500
*2D52510
*2D52520
*2D52530
*2D52540
*2D52550
*2D52560
*2D52570
*2D52580
*2D52590
*2D52600
*2D52610
*2D52620
*2D52630
*2D52640
*2D52650
*2D52660
*2D52670
*2D52680
*2D52690
*2D52700
*2D52710
*2D52720
*2D52730
*2D52740
*2D52750
*2D52760
*2D52770
*2D52780
*2D52790
*2D52800
*2D52810
*2D52820

```



```

651 USING *15
652 ST 2,28(13)
653 L 2,PSKT
654 USING PLOTP,2
655 L 1,0(1)
656 L 1,0(1)
657 SR 0
658 J,OMITSW
659 IC 1,1
660 RN NEGARG
661 NR 1,0
662 B ARGSET
663 NEGARG LCP 1,1
664 XR 1,0
665 NP 1,0
666 ARGSET STC 1,OMITSW
667 L 2,28(13)
668 SR 15,15
669 BR 14
670 DROP 14
671 EJECT 2
672 *****
673 *
674 * SETLOC, ALLOWS THE USER TO SPECIFY WHETHER HE WANTS A NORMAL,
675 * SEMI-LOG, OR LOG-LOG PLOT.
676 *
677 * CALLING SEQUENCE IS
678 *
679 *
680 *****
681 SPACE
682 USING *15
683 L 15,PSKT
684 PLOTP,15
685 L 1,0(1)
686 IC 1,0(1)
687 STC 1,ALOGSM
688 SR 15,15
689 BR 14
690 EJECT
691 *****
692 *
693 * PLOT1 SETS UP THE INFORMATION REQUIRED TO CONSTRUCT THE
694 * GRAPH AND PRINT OUT VALUES ALONG THE X AND Y AXES.
695 *
696 * CALLING SEQUENCE IS
697 *
698 * CALL PLOT1(NSCALE,NHL,NSBH,NVL,NSBV)
699 *****
700 SPACE

```

```

*2753330
*2053340
*2053350
*2053360
*2053370
*2053380
*2053390
*2053400
*2053410
*2053420
*2053430
*2053440
*2053450
*2053460
*2053470
*2053480
*2053490
*2053500
*2053510
*2053520
*2053530
*2053540
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*2053560
*2053570
*2053580
*2053590
*2053600
*2053610
*2053620
*2053630
*2053640
*2053650
*2053660
*2053670
*2053680
*2053690
*2053700
*2053710
*2053720
*2053730
*2053740
*2053750
*2053760
*2053770
*2053780
*2053790
*2053800
*2053810
*2053820

```

```

701          1,15          *2054310
702          1,4,12(13) SAVE ALL IN CASE FOR RETURN      *2053940
703          3,PSKT      GET PSCT HTS STYL          *2053850
704          4,USING,3          *2053860
705          ST          3,8(13)          *2053870
706          ST          1,4(2)          *2053880
707          L          5,0(1)          *2053890
708          L          4,0(5)          *2053900
709          MVT        PLTISM*1          *2053910
710          LTP        4,4          *2053920
711          BZ          STNRD          *2053930
712          L          4,4(5)          *2053940
713          ST          4,YSCLF          *2053950
714          L          4,0(5)          *2053960
715          ST          4,YP(L)CE          *2053970
716          L          4,12(5)          *2053980
717          ST          4,XSCALE          *2053990
718          L          4,15(5)          *2054000
719          ST          4,XPLACE          *2054010
720          R          GETNHL          *2054020
721          L          3,THRE          *2054030
722          ST          3,YP(L)CE          *2054040
723          ST          3,XPLACE          *2054050
724          SP          3,0          *2054060
725          ST          3,YSCLF          *2054070
726          ST          3,XSCALE          *2054080
727          L          5,4(1)          *2054090
728          L          5,0(5)          *2054100
729          LTP        5,5          *2054110
730          RNP        ERPLT1          *2054120
731          ST          5,NHL          *2054130
732          L          5,8(1)          *2054140
733          L          5,0(5)          *2054150
734          LTP        5,5          *2054160
735          RNP        ERPLT1          *2054170
736          ST          5,NSRH          *2054180
737          M          4,NHL          *2054190
738          S          5,NSRH          *2054200
739          A          5,NHL          *2054210
740          C          5,TWO          *2054220
741          PL          ERPLT1          *2054230
742          ST          5,L          *2054240
743          L          5,12(1)          *2054250
744          L          5,0(5)          *2054260
745          LTR        5,5          *2054270
746          RNP        ERPLT1          *2054280
747          ST          5,NVL          *2054290
748          L          5,16(1)          *2054300
749          L          5,0(5)          *2054310
750          LTR        5,5          *2054320

```

```

      SAVE ALL IN CASE FOR RETURN
      GET PSCT HTS STYL
      FRP WILL NEED BACKWARD PRINTER
      ENTRY POINT FROM PLOT14
      SAY NEVER BEEN HERE IF THIS CALL 9A)
      TEST NSCALF
      IF NON-ZERO PICK UP ARGS FOR SCALE, PLACE
      IF ZERO, TAKE STANDARD VALUES
      FOR PLACE
      AND FOR SCALE
      GET NHL
      ERROR RETURN IF NHL NOT POSITIVE
      GET NSRH
      ERROR RETURN IF NSRH NOT POSITIVE
      IF LENGTH LESS THAN 2, ERROR RETURN
      PLOT LENGTH = NSRH*NHL-NSRH*NHL
      GET NVL
      ERROR RETURN IF NVL NOT POSITIVE
      GET NSRV

```

```

751 ERPLT1
752 5,NSRV
753 ST
754 M
755 4,NVL
756 S
757 5,NSRV
758 A
759 5,NVL
760 C
761 5,TWO
762 ERPLT1
763 5,W
764 4,EIGHT
765 L
766 CR
767 4,5
768 RNL
769 STDWNO
770 A
771 4,EIGHT
772 B
773 4,F*120*
774 ERPLT1
775 4,W
776 ST
777 4,3(J)
778 SRL
779 S
780 4,ONE
781 ST
782 TM
783 PTT4SW,255
784 14
785 ROR
786 MVI
787 15,15
788 SR
789 LM
790 3,5,32(13)
791 RR
792 14
793 ERPLT1 MVI
794 FRMO,4
795 ERP
796 R
797 EJECT
798 *****
799 *
800 *
801 *
802 *
803 *
804 *
805 *
806 *
807 *
808 *
809 *
810 *
811 *
812 *
813 *
814 *
815 *
816 *
817 *
818 *
819 *
820 *
821 *
822 *
823 *
824 *
825 *
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830 *
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832 *
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883 *
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892 *
893 *
894 *
895 *
896 *
897 *
898 *
899 *
900 *

```

```

ERROR RETURN IF NSRV NOT POSITIVE
IF WIDTH LESS THAN 2, ERROR RETURN
PLOT WIDTH = NSRV*NVL-NSRV*NVL
FIND FIRST
MULTIPLE
OF R
*GE. #
ERROR RETURN IF GRAPH WIDER THAN 127
SET WD
SFT DWNO
TEST SWITCH FOR PLOT14 ENTRY
IF ON RETURN IMMEDIATELY
TURN ON PLOT1 EXECUTED SWITCH
NORMAL RETURN CODE IS ZFRN
RETURN
ERROR RETURN FRJM PLOT1,PLOT14 CALLS
*****
PLOT2 PREPARES THE GRID AND SETS UP THE INFORMATION REQUIRED
BY PLOT3 TO PLACE A POINT IN THE PROPER POSITION IN THE GRAPH.
CALL PLOT2(IMAGE,XMAX,XMIN,YMAX,YMIN)
CALLING SEQUENCE IS
*****
SPACE
USING
PLOT2 STM
L
USING
ST
PLT2 TM
RZ
ST
B
PLT1SW,255

```

```

*2054330
*2054340
*2054350
*2054360
*2054370
*2054380
*2054390
*2054400
*2054410
*2054420
*2054430
*2054440
*2054450
*2054460
*2054470
*2054480
*2054490
*2054500
*2054510
*2054520
*2054530
*2054540
*2054550
*2054560
*2054570
*2054580
*2054590
*2054600
*2054610
*2054620
*2054630
*2054640
*2054650
*2054660
*2054670
*2054680
*2054690
*2054700
*2054710
*2054720
*2054730
*2054740
*2054750
*2054760
*2054770
*2054780
*2054790
*2054800
*2054810
*2054820

```

```

801      GETIM
802      L 0,TRM
803      ST 0,YPLACE
804      ST 0,XPLACE
805      SP 0,0
806      ST 0,YSCALE
807      ST 0,XSCALE
808      ST 14,SAV14
809      ST 1,SAV1
810      LM 0,1,SP0V
811      LA 13,04SA
812      L 0,15
813      CALL 0,INFO
814      L 1,4(1)
815      LR 1,4
816      C 1,TTY
817      RNF SETP15M
818      AVI NVL+3,0
819      MVI M+3,51
820      MVI M+3,56
821      MVI MND+3,6
822      MVI SETP15M
823      TM ST5M+255
824      R0
825      L 1,SAV1
826      L 2,0(1)
827      ST 2,IMAGE
828      MVI EPR0J,3
829      MVI PLT25M+1
830      L 2,4(1)
831      LF 0,0(2)
832      STE 0,XMAX
833      L 2,P(1)
834      LE 0,0(2)
835      STE 0,XMIN
836      CF 0,XMAX
837      RNL ERP
838      L 2,12(1)
839      LF 0,0(2)
840      STE 0,YMAX
841      L 2,16(1)
842      LF 0,0(2)
843      STE 0,YMIN
844      CF 0,YMAX
845      RNL ERP
846      MVI IMAGE+3,7
847      RZ STDASH
848      MVI IMAGE+3,X+FR
849      L 7,IMAGE
850      A 7,FIGHT
      CTTM
      J,TAKE STANDARD PLOT
      ENTRY PRINT FROM SCRIPT
      L 1,SP0V
      LA 13,04SA
      L 0,15
      CALL 0,INFO
      L 1,4(1)
      LR 1,4
      C 1,TTY
      RNF SETP15M
      AVI NVL+3,0
      MVI M+3,51
      MVI M+3,56
      MVI MND+3,6
      MVI SETP15M
      TM ST5M+255
      R0
      L 1,SAV1
      L 2,0(1)
      ST 2,IMAGE
      MVI EPR0J,3
      MVI PLT25M+1
      L 2,4(1)
      LF 0,0(2)
      STE 0,XMAX
      L 2,P(1)
      LE 0,0(2)
      STE 0,XMIN
      CF 0,XMAX
      RNL ERP
      L 2,12(1)
      LF 0,0(2)
      STE 0,YMAX
      L 2,16(1)
      LF 0,0(2)
      STE 0,YMIN
      CF 0,YMAX
      RNL ERP
      MVI IMAGE+3,7
      RZ STDASH
      MVI IMAGE+3,X+FR
      L 7,IMAGE
      A 7,FIGHT
      MAKE IT
      IF NOT, TAKE STANDARD PLOT
      ENTRY PRINT FROM SCRIPT
      GET DEVICE TYPE NAME
      IS IT A TELETYPE?
      NO
      YES
      TURN ON SWITCH FOR PLOT1 EXECUTED
      IF ENTERED BY SCRIPT, PLOT2 APSS ARE SET
      RESTORE REG 1
      GET IMAGE ADDRESS
      SET ERROR CODE TO 8
      + ASSUME WILL BE HAD CALL ON PLOT2
      R4H
      GET XMAX
      GET XMIN
      (RESTORING TO HELP DEUS)
      RHH
      IF XMIN NOT LESS THAN XMAX, ERROR RETURN
      GET YMAX
      GET YMIN
      IF YMIN NOT LESS THAN YMAX, ERROR RETURN
      SET ERROR CODE TO 8
      R4H
      MAKE IT
      *2054830
      *2054840
      *2054850
      *2054860
      *2054870
      *2054880
      *2054890
      *2054900
      *2054910
      *2054920
      *2054930
      *2054940
      *2054950
      *2054960
      *2054970
      *2054980
      *2054990
      *2055000
      *2055010
      *2055020
      *2055030
      *2055040
      *2055050
      *2055060
      *2055070
      *2055080
      *2055090
      *2055100
      *2055110
      *2055120
      *2055130
      *2055140
      *2055150
      *2055160
      *2055170
      *2055180
      *2055190
      *2055200
      *2055210
      *2055220
      *2055230
      *2055240
      *2055250
      *2055260
      *2055270
      *2055280
      *2055290
      *2055300
      *2055310
      *2055320

```



```

851      ST      7,IMAGE
852      IC      6,DASH
853      IC      14,I
854      IC      9,PLUS
855      IC      3,BLNK
856      L      7,IMAGE
857      L      2,ONF
858      L      4,NVL
859      SR      4,2
860      I      13,W
861      SR      13,2
862      STC     9,PULLINE(13)
863      STC     14,IILINE(13)
864      L      11,NSHV
865      LR      1,11
866      STDSBK SR      13,2
867      STC     6,PULLINE(13)
868      STC     9,IILINE(13)
869      RCT     1,STDSBK
870      SR      13,2
871      STC     9,PULLINE(13)
872      STC     14,IILINE(13)
873      RCT     4,STPLI
874      L      1,W
875      L      13,NHL
876      SR      13,2
877      EX      1,MVPLUS
878      L      6,NSRH
879      STLS   LR      11,6
880      STILIN AP      7,1
881      EX      1,MVILIN
882      RCT     11,STILIN
883      AR      7,1
884      EX      1,MVPLUS
885      RCT     13,STLS
886      *
887      THPU   MVI     P1T2SW,255
888      TM     P1L4SW,255
889      RZ
890      L      14,SAV14
891      L      1,SAV1
892      RR      14
893      RETURN L      13,4(3)
894      LM     14,12,12(13)
895      SR      15,15
896      RR      14
897      DROP   3
898      FJECT
899      *****
900      *

```

```

*2055330
*2055340
*2055350
*2055360
*2055370
*2055380
*2055390
*2055400
*2055410
*2055420
*2055430
*2055440
*2055450
*2055460
*2055470
*2055480
*2055490
*2055500
*2055510
*2055520
*2055530
*2055540
*2055550
*2055560
*2055570
*2055580
*2055590
*2055600
*2055610
*2055620
*2055630
*2055640
*2055650
*2055660
*2055670
*2055680
*2055690
*2055700
*2055710
*2055720
*2055730
*2055740
*2055750
*2055760
*2055770
*2055780
*2055790
*2055800
*2055810
*2055820

```

```

INSERT
GRID CHARACTERS
INTJ
GPRS
GET IMAGE ADDRESS
GPR 4 = NVL-1
GPR 13 = W-1
STORE +
STORE I
GPR 13 DECREASED BY 1
STORE -
STORE BLANK
GPR 13 DECREASED BY 1
STORE +
STORE I
LOOP TO PREPARE THE 2 LINES
1,W
GPR 13 = NHL-1
MOVE FIRST GRID LINE TO GRAPH
GPR 7 POINTS TO NEXT GRAPH LINE
MOVE NON-GRID LINE TO GRAPH
LOOP TO INSERT NSRH NON-GRID LINES
GPR 7 POINTS TO NEXT GRAPH LINE
MOVE GRID LINE TO GRAPH
LOOP TO MOVE GRID AND NON-GRID LINES
TURN ON PLJ12 EXECUTED SWITCH
IF ENTERED BY PLJ14 OK SETPLOT
RESTORE ONLY 14
AND I
NORMAL RETURN CODE IS ZERO
RETURN

```

```

901 * PLOT4 CALLS THE PLOTTING CHARACTERISTICS ROUTINE
902 * FROM PLOT4 (X,Y).
903 *
904 * (CALLING SEQUENCE IS
905 * CALL PLOT4(X,Y,NODATA,INT)
906 *
907 *****
908 SPACE
909 USES
910 ST 14,13,12(13) SAVE ALL IN CASE OF EXIT
911 L 3,PKT GET PSECTITE STYLE
912 L 3,PKT
913 ST 13,4(3)
914 ST 3,8(13)
915 L 13,15
916 L 9,9
917 USES
918 TR 15,PT4,13
919 PLOT5,2,2,5
920 R0 STPT4
921 R4 VVI ERRN,16 IF NOT, ERROR CODE SET TO 16
922 L 15,PT4,100 PR EXIT VIA SERCOM CALL
923 L 15,PT4,15 ESTABLISH PLOT4 ADDRESSABILITY FOR LOG USE
924 L 5,12(1) ENTRY POINT FROM PLOT4
925 L 5,5 TEST NDATA
926 L 5,5 RND IF NDATA LESS THAN 1, RETURN
927 RND
928 S 5,ONE
929 L 9,16(1)
930 L 9,0(9)
931 MR 4,9
932 LR 4,0
933 L 9,0(1)
934 LC 9,0(9)
935 SR 11,11
936 ST 1,SAV1
937 L 4,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,23,24,25,26,27,28,29,30,31,32,33,34,35,36,37,38,39,40,41,42,43,44,45,46,47,48,49,50,51,52,53,54,55,56,57,58,59,60,61,62,63,64,65,66,67,68,69,70,71,72,73,74,75,76,77,78,79,80,81,82,83,84,85,86,87,88,89,90,91,92,93,94,95,96,97,98,99,100
938 PINT 1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,23,24,25,26,27,28,29,30,31,32,33,34,35,36,37,38,39,40,41,42,43,44,45,46,47,48,49,50,51,52,53,54,55,56,57,58,59,60,61,62,63,64,65,66,67,68,69,70,71,72,73,74,75,76,77,78,79,80,81,82,83,84,85,86,87,88,89,90,91,92,93,94,95,96,97,98,99,100
939 VVI ERRN,12
940 RAS 5,LOGS
941 GTXMAX LF 2,XMAX
942 SE 2,XMIN
943 LE 4,YMAX
944 SE 4,YMIN
945 L 2,4(1)
946 L 5,8(1)
947 L 10,IMAGE
948 LF 0,0(11,2)
949 TM LOGSW,2
950 BZ SURXMN

```

```

951 LTRP          J*0
952 BNP          LOOP
953 RAS         12,LOG
954          J*YMAX
955          LOOP
956          J*XMIN
957          LTRP
958          Q*2
959          G*0(11,6)
960          TM   LOGSM,1
961          BZ   SURYMN
962          S*6
963          LOOP
964          J*1
965          LER  J*6
966          RAS 12,LOG
967          LER  S*0
968          LE  J*1
969          SURYMN CE  S*YMAX
970          BH   LOOP
971          SE  6,YMIN
972          BN   LOOP
973          DER  S*4
974          ME  0,WFP
975          MF  6,LFP
976          FPRMND S*12
977          L   1,L
978          SR  1,12
979          M   J*WD
980          FPRMND J*1
981          AR  9,1
982          STC 9,0(10,8)
983          BXL 11,4,GC
984          TM   LOGSM,1
985          RZ   CHECKX
986          LE  0,YMAX
987          STE  J*YMAX
988          LE  J*YMIN
989          STE  J*YMIN
990          STE  LOGSM,2
991          CHECKX TM  OUTP3
992          RZ   LE
993          LE  J*YMAX
994          STE  J*XMAX
995          LE  J*YMIN
996          STE  0,XMIN
997          TM   P114SW,255
998          L   1,SAV1
999          ROR  14
1000         OUTP31 L 13,4(3)

```

```

IF ARG NOT POSITIVE, DISREGARD POINT
REPLACE X WITH LOG X

IF X GREATER THAN XMAX, DISREGARD POINT
FPR 0 = X-XMIN
IF X LESS THAN XMIN, DISREGARD POINT
FPR 0 = (X-XMIN)/(XMAX-XMIN)
PICK UP Y VALUE
TEST LOG SWITCH FOR Y
IF OFF, GO TO NEXT STEP

IF ARG NOT POSITIVE, DISREGARD POINT

REPLACE Y WITH LOG Y

IF Y GREATER THAN YMAX, DISREGARD POINT
FPR 6 = Y-YMIN
IF Y LESS THAN YMIN, DISREGARD POINT
FPR 6 = (Y-YMIN)/(YMAX-YMIN)
FPR 0 = COLUMN CORRESPONDING TO X
FPR 6 = ROW CORRESPONDING TO Y FROM BELOW
GPK 12 = FPR 6 IN INTEGER MODE, ROUNDED

GPR 1 = ROW CORRESPONDING TO Y FROM TOP

GPR 9 = FPR 0 IN INTEGER MODE, ROUNDED
GPP 9 = LINEAR SUBSCRIPT FROM ROW AND COL
INSERT PLOTTING CHARACTER IN GRAPH
LOOP TO HANDLE ALL POINTS
TEST LOG SWITCH FOR Y

IF ON,
RESTORE
ORIGINAL
YMAX AND YMIN
TEST LOG SWITCH FOR X

IF ON,
RESTORE
ORIGINAL
XMAX AND XMIN
IF ENTERED BY PLJ114 OR SETPLOT
RESTORE ONLY 1
AND RETURN

```

```

*2D56330
*2D56340
*2D56350
*2D56360
*2D56370
*2D56380
*2D56390
*2D56400
*2D56410
*2D56420
*2D56430
*2D56440
*2D56450
*2D56460
*2D56470
*2D56480
*2D56490
*2D56500
*2D56510
*2D56520
*2D56530
*2D56540
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*2D56560
*2D56570
*2D56580
*2D56590
*2D56600
*2D56610
*2D56620
*2D56630
*2D56640
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*2D56670
*2D56680
*2D56690
*2D56700
*2D56710
*2D56720
*2D56730
*2D56740
*2D56750
*2D56760
*2D56770
*2D56780
*2D56790
*2D56800
*2D56810
*2D56820

```

RHH

```

1001          L 1+L7+20(13)
1002          S 1+L1
1003          SR 1+
1004          SR 3
1005          SR 13
1006          EJECT
1007 *****
1008 *
1009 * PLOT4 PRINTS THE COMPLETED GRAPH WITH VALUES ALONG THE X AND
1010 * Y AXES AND A CENTERED VERTICAL LABEL ACROSS THE CENTER OF THE
1011 *
1012 *
1013 * CALL PLOT4(C-CAR,LABEL)
1014 *
1015 *****
1016 *
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1051	ST	J,LINE+R	OF	J,LINE+R	**2057330
1052	ST	0,LINE+12	PRINT LINE	0,LINE+12	**2057340
1053	MVI	LINE,C00	SET UP CHARACTER CONTROL	LINE,C00	**2057350
1054	L	J,YSCALE	SET UP	J,YSCALE	**2057360
1055	ST	J,SCALE	SCALE	J,SCALE	**2057370
1056	L	J,YPLACE	AND PLACE	J,YPLACE	**2057380
1057	ST	J,PLACE	FOR FPRC0	J,PLACE	**2057390
1058	TM	OMITSW,4	TEST NO LAST GRAPH LINE SWITCH	OMITSW,4	**2057400
1059	RZ	0M4	IF ON, ZFR0 GPR 10	0M4	**2057410
1060	SR	10,10	IF OFF, SET GPR 10 = R	10,10	**2057420
1061	R	L55		L55	**2057430
1062	L	10,EIGHT		10,EIGHT	**2057440
1063	R	L55		L55	**2057450
1064	L5	L50(110)	CHECK FOR LAST LINE	L50(110)	**2057460
1065	L50	R,L	BRANCH OUT IF IT IS	R,L	**2057470
1066	BE	LSTLIN		LSTLIN	**2057480
1067	RAS	4,ORDNUM		4,ORDNUM	**2057490
1068	RAS	4,PRINT		4,PRINT	**2057500
1069	R,XLF	R,6,15	LOOP TO SEND OUT LINES WITH NO LABEL	R,6,15	**2057510
1070	C	7,L		7,L	**2057520
1071	RF	LSTLIN	GRAPH HAS BEEN PRINTED	LSTLIN	**2057530
1072	AR	7,5	ADD NCHAR TO LINE COUNTER	7,5	**2057540
1073	S	R,ONE		R,ONE	**2057550
1074	SP	5,5		5,5	**2057560
1075	R	L66		L66	**2057570
1076	L6	L60(110)		L60(110)	**2057580
1077	L60	R,L	CHECK FOR LAST LINE	R,L	**2057590
1078	RE	LSTLIN	BRANCH OUT IF IT IS	LSTLIN	**2057600
1079	RAS	4,ORDNUM		4,ORDNUM	**2057610
1080	IC	7,0(9,5)		7,0(9,5)	**2057620
1081	STC	J,LINE+1	STORE LABEL CHARACTER ALONG LEFT MARGIN	J,LINE+1	**2057630
1082	A	5,ONE		5,ONE	**2057640
1083	RAS	4,PRINT		4,PRINT	**2057650
1084	R,XLF	R,6,16	LOOP TO SEND OUT LINES WITH LABEL	R,6,16	**2057660
1085	L	7,L		7,L	**2057670
1086	S	R,ONE		R,ONE	**2057680
1087	R	L55	GO BACK TO FINISH PRINTING GRAPH	L55	**2057690
1088	* LSTLIN	ROUTINE TO SET	UP AND PRINT X GRID VALUES IF SWITCH ON	ROUTINE TO SET	**2057700
1089	TM	OMITSW,1	IF X GRID VALUE SWITCH TURNED OFF	OMITSW,1	**2057710
1090	BO	00NE	GO TO EXIT SEQUENCE	00NE	**2057720
1091	LE	5,XMAX		5,XMAX	**2057730
1092	SE	5,XMIN	FPR 6 = XMAX-XMIN	5,XMIN	**2057740
1093	L	10,NSBV	GPR 10 = NSRV+1	10,NSBV	**2057750
1094	A	10,ONE		10,ONE	**2057760
1095	L	9,TWELVE		9,TWELVE	**2057770
1096	L	11,4		11,4	**2057780
1097	LR	12,11	CONVERT W TO FLOATING POINT	12,11	**2057790
1098	RNFP	12,4		12,4	**2057800
1099	A	11,ELEVEN		11,ELEVEN	**2057810
1100	L	J,XSCALE	SET UP	J,XSCALE	**2057820

```

1101 ST      0,SCALE
1102 L      0,XPLANE
1103 ST      0,PLACE
1104 L      1,THIRTY
1105 L      0,PLNKW
1106 L      0,1
1107 L      0,2(0)
1108 S      0,FOUP
1109 ST      0,LINE(2)
1110 ST      1,RLNKLN
1111 L      14,9
1112 S      14,ELFVEL
1113 L      0,ME
1114 L      0,4
1115 L      0,6
1116 AE      0,XMIN
1117 T4     LOGSW,7
1118 RZ     CONVX
1119 BAS     12,FXO
1120 BAS     12,PRICD
1121 BAS     12,SETRD
1122 ST      4,1
1123 L      5,4
1124 SKL     5,1(0)
1125 SP      0,0
1126 L      1,NSAV
1127 O      0,TWO
1128 LTR     J,0
1129 BNL     FIELD
1130 S      1,ONE
1131 CR      5,1
1132 RL     SFT
1133 LP      5,1
1134 LR      14,9
1135 AR      14,5
1136 STC     7,LINE(14)
1137 SRDI     5,9(0)
1138 S      14,DNE
1139 BCT      4,MVCH
1140 TM      MPOS,254
1141 R7      -RNLDP
1142 TM      T*3,2
1143 R7      -RNLDP
1144 IC      4,DASH
1145 STC      4,LINE(14)
1146 5XLE     0,10,HRLLN
1147 MVI     LINE,C*0
1148 MVI     L120+1,120
1149 ST      15,SV1415
1150 CALL    SPRT,(LINE,L120)

1101 SCAL*
1102 AN PLACE
1103 FUP FUPC)
1104 *2057437
1105 *2057440
1106 *2057445
1107 *2057460
1108 *2057470
1109 *2057480
1110 *2057490
1111 *2057910
1112 *2057920
1113 *2057930
1114 *2057940
1115 *2057950
1116 *2057960
1117 *2057970
1118 *2057980
1119 *2057990
1120 *2058000
1121 *2058010
1122 *2058020
1123 *2058030
1124 *2058040
1125 *2058050
1126 *2058060
1127 *2058070
1128 *2058080
1129 *2058090
1130 *2058100
1131 *2058110
1132 *2058120
1133 *2058130
1134 *2058140
1135 *2058150
1136 *2058160
1137 *2058170
1138 *2058180
1139 *2058190
1140 *2058200
1141 *2058210
1142 *2058220
1143 *2058230
1144 *2058240
1145 *2058250
1146 *2058260
1147 *2058270
1148 *2058280
1149 *2058290
1150 *2058300
1151 *2058310
1152 *2058320

```

```

STEP 4 BLANKS AT A TIME
LOOP TO BLANK OUT ENT LINE

```

```

FP 0 = X VALUE
IFST LHS SWITCH FOR X

```

```

IF ON TAKE EXP(X)
SET UP
RPN CHARACTERS

```

```

GPR 4 = NUMBER OF CHARS
CENTER

```

```

NUMBER

```

```

UNDER

```

```

VFOTICAL

```

```

GRID

```

```

LINE

```

```

LOOP TO SEND OUT CHARS

```

```

AND - IF NECESSARY
LOOP TO MOVE ALONG X AXIS
SET UP CARRIAGE CONTROL
PRINT LINE LENGTH IS 12) CHARS

```

```

1151 L 15,SV1415
1152 * DONE EXIT SEQUENCEF
1153 RM LOGSW,1 TEST LOG SWITCH FOR Y
1154 RZ VGMX
1155 LE J,TYMAX IF CN,
1156 STE J,TYMAX RESTORE
1157 LF J,TYMIN ORIGINAL
1158 STE J,TYMIN YMAX AND YMIN
1159 NCMX TM LOGSW,2 TEST LOG SWITCH FOR X
1160 RZ TOTP4
1161 LF J,TXMAX IF UN,
1162 STF J,TXMAX RESTORE
1163 LF J,TXMIN ORIGINAL
1164 STE J,TXMIN XMAX AND XMIN
1165 OUP4 TM XKSW,255 TEST X SCALE SWITCH (SETPLOT)
1166 RZ TOTP4
1167 ST 15,SV1415
1168 CALL SPRNT,(XCCM,FIFTY7)
1169 L 15,SV1415
1170 MVI XSI,C,0 PESFT XSI TO A BLANK
1171 MVI XDIG1,C,0 RESFT XDIG1 TO A 0
1172 MVI XKSW,0 TURN OFF X SCALF SWITCH (SETPLOT)
1173 OUP41 TM XKSW,255 TEST Y SCALF SWITCH (SETPLOT)
1174 RZ TOTP42
1175 CALL SPRNT,(YCCM,FIFTY7)
1176 MVI YSI,C,0 RESET YSI TO A BLANK
1177 MVI YDIG1,C,0 RESET YDIG1 TO A 0
1178 MVI YKSW,0 TURN OFF Y SCALE SWITCH (SETPLOT)
1179 OUP42 L 13,413 NORMAL RETJRN SEQUENCE
1180 MVI ST254,C MAKE SURE SETPLJ? SWITCH IS OFF
1181 LM 14,12,1?(13)
1182 SR 15,15
1183 BR 14
1184 * ERROR RETURN, PLUS PRINT RETURN CODES ON SERCOM
1185 ERR LR 13,3 POINT GR13 AT INTERNAL PLOTP SAVEAREA
1186 L 1,ERRSW USE RETURN CODE
1187 SRA 1,2
1188 IC O,PLOTR(1) TO FIND WHICH ROUTINE IT WAS IN
1189 STC J,ERRMSG+15 FOR PRINTING
1190 SLA 1,1
1191 LH J,RC(1) AND THE RETURN CODE IN CHARACTER FORM
1192 STH J,FRMSG+20
1193 LA 1,=A(FRMSG,4?3,0)
1194 L 15,=V(XERCCM)
1195 RASR 14,15
1196 L 13,4(3) ORIG GR13 FROM BACKWARD LINK
1197 MVI ST254,0 MAKE SURE SETPLJ? SWITCH IS OFF
1198 L 15,ERRSW LOAD RETURN CODE
1199 LM J,12,20(13)
1200 L 14,12(13) LOAD RETURN

```

```

*2058330
*2058340
*2058350
*2058360
*2058370
*2058380
*2058390
*2058400
*2058410
*2058420
*2058430
*2058440
*2058450
*2058460
*2058470
*2058480
*2058490
*2058500
*2058510
*2058520
*2058530
*2058540
*2058550
*2058560
*2058570
*2058580
*2058590
*2058600
*2058610
*2058620
*2058630
*2058640
*2058650
*2058660
*2058670
*2058680
*2058690
*2058700
*2058710
*2058720
*2058730
*2058740
*2058750
*2058760
*2058770
*2058780
*2058790
*2058800
*2058810
*2058820

```



```

1251 *          *          *          *          *          *          *          *          *          *
1252 *          *          *          *          *          *          *          *          *          *
1253 *          *          *          *          *          *          *          *          *          *
1254 *          *          *          *          *          *          *          *          *          *
1255 *          *          *          *          *          *          *          *          *          *
1256 *          *          *          *          *          *          *          *          *          *
1257 *          *          *          *          *          *          *          *          *          *
1258 *          *          *          *          *          *          *          *          *          *
1259 *          *          *          *          *          *          *          *          *          *
1260 *          *          *          *          *          *          *          *          *          *
1261 *          *          *          *          *          *          *          *          *          *
1262 *          *          *          *          *          *          *          *          *          *
1263 *          *          *          *          *          *          *          *          *          *
1264 *          *          *          *          *          *          *          *          *          *
1265 *          *          *          *          *          *          *          *          *          *
1266 *          *          *          *          *          *          *          *          *          *
1267 *          *          *          *          *          *          *          *          *          *
1268 *          *          *          *          *          *          *          *          *          *
1269 *          *          *          *          *          *          *          *          *          *
1270 *          *          *          *          *          *          *          *          *          *
1271 *          *          *          *          *          *          *          *          *          *
1272 *          *          *          *          *          *          *          *          *          *
1273 *          *          *          *          *          *          *          *          *          *
1274 *          *          *          *          *          *          *          *          *          *
1275 *          *          *          *          *          *          *          *          *          *
1276 *          *          *          *          *          *          *          *          *          *
1277 *          *          *          *          *          *          *          *          *          *
1278 *          *          *          *          *          *          *          *          *          *
1279 *          *          *          *          *          *          *          *          *          *
1280 *          *          *          *          *          *          *          *          *          *
1281 *          *          *          *          *          *          *          *          *          *
1282 *          *          *          *          *          *          *          *          *          *
1283 *          *          *          *          *          *          *          *          *          *
1284 *          *          *          *          *          *          *          *          *          *
1285 *          *          *          *          *          *          *          *          *          *
1286 *          *          *          *          *          *          *          *          *          *
1287 *          *          *          *          *          *          *          *          *          *
1288 *          *          *          *          *          *          *          *          *          *
1289 *          *          *          *          *          *          *          *          *          *
1290 *          *          *          *          *          *          *          *          *          *
1291 *          *          *          *          *          *          *          *          *          *
1292 *          *          *          *          *          *          *          *          *          *
1293 *          *          *          *          *          *          *          *          *          *
1294 *          *          *          *          *          *          *          *          *          *
1295 *          *          *          *          *          *          *          *          *          *
1296 *          *          *          *          *          *          *          *          *          *
1297 *          *          *          *          *          *          *          *          *          *
1298 *          *          *          *          *          *          *          *          *          *
1299 *          *          *          *          *          *          *          *          *          *
1300 *          *          *          *          *          *          *          *          *          *

ROUTINE TO CONVERT FLOATING POINT NUMBER TO RC)
0*0
ZERO
MISIGN
MINUS*0
MVI
R
MISIGN MVI
SDR
LPER
SR
CD
BL
DD
A
R
LA
LA
LR
CD
RH
S
CR
G02
RNL
MD
S
B
SR
C
BE
AR
DD
SR
SRL
LA
AH
R
DD
A
CD
BNL
CD
BNL
MD
S
B
LER
A
LR
A
C

GET END OF TABL
GET BEGINNING OF TABLE
COMPARE WITH TABLE ENTRY
PREPARE FOR NEXT ENTRY
STILL IN TABLE?
YES
NO, NUMBER STILL < 10**-20
SO MULTIPLY AND ADJUST SCALF FACTOR
AND TRY AGAIN
READY TO EXIT DJT OF THIS PHASE
YES
RESTORE GR2
DIVIDE BY TABLE ENTRY
THIS IS TO REFERENCE SKFAC
ADD CORRECT AMOUNT TO SCALE FACTOR
BACK TO TRY AGAIN
NUMBER STILL NOT LESS THAN 1
NUMBER FINALLY BETWEEN .1 AND 1
NUMBER STILL < .1
CHECK FOR REASONABLENESS
1,=F*100*

```

```

1301          CHKSP          "SOMETHING WRONG WITH SCALE IN PLANT"      4.14
1302          MVI          AWAY WE GO
1303          ERB
1304          LTR          IF SCALE LESS THAN PLACE AND
1305          PAF          NOT USING SETPLT, RESULT
1306          STPSP+255
1307          RZ          IS 0.
1308          L          ALWAYS 3 DIGITS IN 6 CONVERSION
1309          LTR          ROUND
1310          ADD          APO
1311          DE          BY
1312          RCT          ADDING
1313          AFR          .5*10**(SCALE*PLACE)
1314          STP          TEST FOR SPILL
1315          TM          T+1
1316          RC          SPILL
1317          L          T+1
1318          N          MASK OUT CHARACTERISTIC
1319          CVD          CONVERT MANTISSA TO DECIMAL
1320          L          PROVIDE
1321          L          LEADING
1322          SLDL          2+2R(0)
1323          SRL          1+2R(0)
1324          ST          ZEROS
1325          SR          1+DFCLOC+3
1326          SRPL          1+R(0)
1327          ST          FOR
1328          ST          1+DECLOC+4
1329          ST          DECIMAL DIVISION
1330          DP          DECCLOC(12),DECCLOC(5) DIVIDE MANTISSA BY 2**24
1331          UNPK          RESULT(13),DECCLOC(7) BC) CHARS IN RESULT
1332          BR          12
1333          *          ROUTINE TO SET UP 1000000 IF ROUNDED RESULT GOES OVER 1.
1334          L          0+DFCONE
1335          L          1+DEC7ER
1336          ST          0+RESULT
1337          ST          1+RESULT+4
1338          A          4,ONE
1339          BP          SCALE INCREASED BY 1
1340          *          ROUTINE TO SET UP 00000000 IF NO SIGNIFICANT DIGITS
1341          L          0+DEC7ER
1342          ST          0+RESULT
1343          ST          0+RESULT+4
1344          L          4,ONE
1345          MVI          ZFR) SCALE SET TO 1
1346          RP          ZFR) ALWAYS POSITIVE
1347          *          ROUTINE TO SET UP DECIMAL NO. WITH DECIMAL PT. IN POS.
1348          L          0,ONE
1349          LR          GPR 1 = SCALE
1350          L          7+PLVAKWD LOAD BLANKS IN GPRS 6

```

1351	LR	6,7	AND 7	*2D60330
1352	SR	4,4		*2D60340
1353	SR	5,5		*2D60350
1354	L	2,FLIGHT	NO MORE THAN 8 CHARS POSSIBLE	*2D60360
1355	*			*2D60370
1356	TM	ST25W,255	USE F CONVERSION	*2D60380
1357	BZ	NDECON	IF COMING FROM SEIPL0T	*2D60390
1358	LTR	1,1	AND SCLAE FOR THIS NUMBER	*2D60400
1359	AM	ECON	IS NEGATIVE	*2D60410
1360	C	1,SEVEN	CR GREATER THAN 7	*2D60420
1361	RH	FCOIN		*2D60430
1362	R	NDECON		*2D60440
1363	S	1,ONE		*2D60450
1364	IC	7,RESULT	FIRST SIGNIFICANT DIGIT	*2D60460
1365	SLDL	6,8(0)		*2D60470
1366	IC	7,DOT	THEN THE DECIMAL POINT	*2D60480
1367	L	2,TWO	THEN	*2D60490
1368	A	5,ONE	THE	*2D60500
1369	SLDL	6,8(0)	NEXT	*2D60510
1370	IC	7,RESULT(5)	TWO	*2D60520
1371	ACT	2,ELCOP	SIGNIFICANT DIGITS	*2D60530
1372	SLDL	6,8(0)		*2D60540
1373	IC	7,FC-HAR	THEN THE LETTER F	*2D60550
1374	SLDL	6,8(0)		*2D60560
1375	LTR	1,1	CHECK THE SIGN OF THE SCALE	*2D60570
1376	RP	EXPOS		*2D60580
1377	LPP	1,1	COMPLEMENT IF NEGATIVE	*2D60590
1378	IC	7,DASH	AND INSERT MINUS SIGN	*2D60600
1379	P	EXDIGS		*2D60610
1380	IC	7,PLUS	INSERT PLUS SIGN	*2D60620
1381	EXDIGS	0,0		*2D60630
1382	D	J,TEN		*2D60640
1383	STC	1,T	CONVERT	*2D60650
1384	PI	T,X*F0*	SCALE	*2D60660
1385	SLDL	6,8(0)	TO	*2D60670
1386	IC	7,T	ACD	*2D60680
1387	STC	J,T	CHARACTERS	*2D60690
1388	PI	T,X*F0*	AND	*2D60700
1389	SLDL	6,8(0)	INSEPT	*2D60710
1390	IC	7,T	THEM	*2D60720
1391	L	4,EIGHT	ALWAYS 8 CHARACTERS	*2D60730
1392	BR	12		*2D60740
1393	*			*2D60750
1394	NDECON	TM	TEST THE SIGN	*2D60760
1395	HZ	TST		*2D60770
1396	IC	7,DASH	IF NEGATIVE, INSERT -	*2D60780
1397	LTR	1,1	TEST THE SCALE	*2D60790
1398	HNN	VLOOP		*2D60800
1399	SLDL	6,8(0)	IF NEGATIVE	*2D60810
1400	IC	7,DOT	INSERT .	*2D60820

```

1401      * 2060930
1402      * 2060940
1403      * 2060950
1404      * 2060960
1405      * 2060970
1406      * 2060980
1407      * 2060990
1408      * 2061000
1409      * 2061010
1410      * 2061020
1411      * 2061030
1412      * 2061040
1413      * 2061050
1414      * 2061060
1415      * 2061070
1416      * 2061080
1417      * 2061090
1418      * 2061100
1419      * 2061110
1420      * 2061120
1421      * 2061130
1422      * 2061140
1423      * 2061150
1424      * 2061160
1425      * 2061170
1426      * 2061180
1427      * 2061190
1428      * 2061200
1429      * 2061210
1430      * 2061220
1431      * 2061230
1432      * 2061240
1433      * 2061250
1434      * 2061260
1435      * 2061270
1436      * 2061280
1437      * 2061290
1438      * 2061300
1439      * 2061310
1440      * 2061320
1441      * 2061330
1442      * 2061340
1443      * 2061350
1444      * 2061360
1445      * 2061370
1446      * 2061380
1447      * 2061390
1448      * 2061400
1449      * 2061410
1450      * 2061420

```

```

      TAXI COMPLEMENT
      INSERT A 0
      IF NUMBER OF LEADING XZUS IS
      EQUAL TO REQUESTED PLACES, EXIT
      LOOP TO INSERT LEADING ZEROS
      INSERT DIGIT
      LOOP TO INSERT DIGITS LEFT OF .
      INSERT .
      INSERT DIGIT
      LOOP TO INSERT DIGITS RIGHT OF .
      IF SIGN IS +, RETURN
      IF - AND MORE THAN 8 CHARS
      RETURN
      IF LESS THAN 8, MINUS IS STILL THERE,
      SO TURN OFF SWITCH
      * ROUTINE TO CHECK IF LOG SCALE AND TAKE LOG OF YMAX...X*IN
      TEST LOG SWITCH FOR Y
      * MAX AFTER MIN IN CASE BOTH < 0
      ALSO NEED CHECK <= 0 LIM AS LOG ARG
      IN PLJ4
      HOLD LOG UNTIL SURE NO ERRORS
      IF ON,
      HOLD LOG UNTIL SURE NO ERRORS
      TEST LOG SWITCH FOR X

```

```

1451      *      RZ      GOTLM4      00 MAX AFTER MIN IN CASE BOTH < )
1452      LE      J,XMIN      J+0
1453      LTR     J+0
1454      RNP     ERR
1455      STE     J+TXMIN
1456      BAS     J+LOG
1457      RAS     J,XMIN
1458      LE     J,XMAX
1459      STE     J+TXMAX
1460      BAS     J+LOG
1461      STE     J,XMAX
1462      GOTLM4 TM      LOGSW+1
1463      RZR     YMAX(R),TLYMAX DESTROYED THEM IN CASE OF FRR
1464      MVC     6
1465      RR      NATURAL LOG ROUTINE
1466      *
1467      LOG     J+TT
1468      LTR     J+0
1469      BP      LOGOK
1470      DC     H+0+
1471      LOGOK JS
1472      STE     2+FP2
1473      SF     J+AP
1474      LPER   J+0
1475      CF     J+SML
1476      BH     ARGBIG
1477      LE     J+AP
1478      LER   J+0
1479      MER   2+0
1480      DE     ?+MITWDF
1481      AER   J+2
1482      LE     J+2
1483      ARGRIG STM 0+1,LOGSAV
1484      L
1485      SRDL  0+24(0)
1486      S     J+HEX40
1487      SLL   J+2(0)
1488      LTR  1+0
1489      BN    1+0
1490      SLL  J+ONE
1491      S     J+0
1492      R     J+0
1493      LTR  J+0
1494      RNN  FXPNN
1495      MVI  MINUS+255
1496      LCR  J+0
1497      R     GOLOG
1498
1499
1500

```

```

1501 EXPAN MVI MINUS,0
1502 GCLDG C J,CNVHT
1503 ST J,TT
1504 LF J,7*P*F
1505 AF J,TT
1506 TM MINUS,255
1507 RZ V,TRNF,
1508 LCFP J,C
1509 SF J,HALF
1510 STE J,HPWR
1511 L J,HEX40
1512 SLDL J,24(0)
1513 ST J,TT
1514 LF J,TT
1515 LER J,0
1516 SF J,RSQRT2
1517 AF J,RSQRT2
1518 DER J,2
1519 STE J,V
1520 MER J,0
1521 STE J,VV
1522 VF J,C1
1523 AF J,C2
1524 MF J,VV
1525 AF J,C3
1526 MF J,V
1527 AE J,HPWR
1528 MF J,C4
1529 LM J,1,LOGSAV
1530 LF J,FPR2
1531 BR J,2
1532 * EXPONENTIAL ROUTINE - RAISES F TO A GIVEN POWER
1533 EXP J,FPP2
1534 J,4,FPR4
1535 STE J,F,PPA
1536 LER J,0
1537 LFP J,0
1538 LF J,ONEF
1539 AER J,4
1540 STE J,EXPANS
1541 AF J,ONEF
1542 MFR J,2
1543 DER J,6
1544 AER J,4
1545 CF J,EXPANS
1546 EXPLP RNE
1547 LF J,FPP2
1548 LF J,FPR4
1549 LE J,6,FPR4
1550 BR J,2

```

```

*2061P30
*2061P40
*2061P50
*2061P60
*2061P70
*2061P80
*2061P90
*2061P00
*2061P10
*2061P20
*2061P30
*2061P40
*2061P50
*2061P60
*2061P70
*2061P80
*2061P90
*2062000
*2062010
*2062020
*2062030
*2062040
*2062050
*2062060
*2062070
*2062080
*2062090
*2062100
*2062110
*2062120
*2062130
*2062140
*2062150
*2062160
*2062170
*2062180
*2062190
*2062200
*2062210
*2062220
*2062230
*2062240
*2062250
*2062260
*2062270
*2062280
*2062290
*2062300
*2062310
*2062320

```

```

FLUAT THE EXPONENT
RECIPROCAL
HPWR = EXPONENT-5
WITH 40 AS CHARACTERISTIC
PRINT (V*E) MANTISSA
FOA J = FRACTIONAL PART, (CALL IT F
V = (F-2**-.5)/(F+2**-.5)
VV = V*V
LOG ARG BASE 2 =
V*(LV*(LV*.5509747)+.2514706)+2.935301)
+HPWR
NATURAL LOG = LOG BASE 2 * .6931472
EXPONENTIAL ROUTINE - RAISES F TO A GIVEN POWER
I = 1
FIRST 2 TERMS ARE 1 AND X
F = I + I
NEW TERM IS (X * OLD TERM)/I
ADD TO CUMULATIVE SUM
WHEN SUM IS NOT CHANGED BY ADDITION,
RETURN, OTHERWISE GET NEXT TERM

```



```

1601 SPAC *2062833
1602 JSTP, *2062840
1603 STPLT2 STM 1,*15,12(13) PHH *2062850
1604 L 3,*PSKT PHH *2062863
1605 USING PLOT2,3 *2062870
1606 MVI ST2SM,255 *2062880
1607 R SVRS *2062890
1608 STPLT1 STM 1,*12,12(13) SMH *2062900
1609 * FULL THRU. HAS BEEN SUCCESSIVELY USING *15 IN VESSEL SENT OUT TO SOME *2062920
1610 USING STPLT1,15
1611 L 15,ASP2
1612 STPLT2,15 PHH *2062930
1613 R,PSKT PHH *2062940
1614 MVI ST2SM,0 *2062950
1615 JH PHH *2062970
1616 ST 3,*8(13) *2062980
1617 ST 1,*4(3) *2063000
1618 MVI STSM,255 *2063010
1619 L 15,*PT2ADD *2063020
1620 USING PLOT2,15 *2063030
1621 L 5,0(1) *2063040
1622 ST 5,*IMAGE *2063050
1623 L 5,16(1) *2063060
1624 L 5,0(6) *2063070
1625 L 5,12(1) *2063080
1626 L 5,0(5) *2063090
1627 S 5,*ONE *2063100
1628 MP 4,*6 *2063110
1629 L 9 *2063120
1630 L 2,*4(1) *2063130
1631 L 3,0(2) *2063140
1632 LFR 2,*0 *2063150
1633 SP 5,*6 *2063160
1634 LE 4,0(2,*6) *2063170
1635 CFR 0,*4 *2063180
1636 RNL STRYMN *2063190
1637 LER J,*4 *2063200
1638 R SLCNP *2063210
1639 CER 2,*4 *2063220
1640 RNM SLOOP *2063230
1641 LER 2,*4 *2063240
1642 RLXLE 6,*6,*STGO *2063250
1643 TM YSM,255 *2063260
1644 NO YTHRU *2063270
1645 STF 0,*XMAX *2063280
1646 STE 2,*XMIN *2063290
1647 MVI YSM,255 *2063300
1648 L 2,*4(1) *2063310
1649 R TSTXY *2063320
1650 YTHRU STE SET YMAX

```



```

1651 STE      2,YMIN
1652 MVI      YSM,0
1653 ST       4,SAV4
1654 ST       5,SAV5
1655 *
1656 LE       J,XMIN
1657 LE       J,XMAX
1658 LPER    J,0
1659 LPER    2,2
1660 L       4,THREE
1661 SR      2,2
1662 CEP     0,2
1663 RNL     CMMAG
1664 LER     0,2
1665 LTR     0,0
1666 BE     TOUT
1667 CE      0,ONEF
1668 BNL     T1
1669 CE      0,5ML
1670 RL      T2
1671 L       4,SEVFN
1672 R      TOUT
1673 MF     0,MILL
1674 A      2,SIX
1675 CE     0,ONEF
1676 BL     T2
1677 CF     0,MILL
1678 RL     TOUT
1679 DE     0,MILL
1680 S      2,SIX
1681 R      T1
1682 TM     YSM,255
1683 B0     YSLOUT
1684 ST     2,XSCALE
1685 ST     4,XPLACE
1686 STSKL  T3,XSKSW,XDTG1,XDTG2,XST,LOC1
1687 LE     0,YMIN
1688 LF     2,YMAX
1689 MVI    YSM,255
1690 B      GOSKL
1691 ST     2,YSCALE
1692 ST     4,YPLACE
1693 STSKL  T6,YKSW,YDTG1,YDTG2,YST,LOC2
1694 MVI    YSM,0
1695 *
1696 MVI     PTL4SW,255
1697 BAS     14,STENT
1698 TM     ST2SW,255
1699 R0     GTCHP
1700 MVI     PTL4SW,0

```

```

SET YMIN
TURN OFF Y SWITCH
SAVE GPRS 4
AND 5

FPR 0 = .AHS.(XMIN OR YMIN)
FPP 2 = .AHS.(XMAX OR YMAX)
ASSUME 3 DECIMAL PLACFS
AND 0 SCALE FACTOR TO STAPT

FPR 0 = VALUE OF GREATP MAGNITUDE
IF LARGST VALUE IS 0
DO NOT TRY TO SCALE IT

RHH
RHH

IF VALUE GREATER THAN JP = 1E-4 AND LESS
THAN 1, USE 7 DECIMAL PLACFS AND 0 SCALE
IF VALUF LFSS THAN 1E-4, MULTIPLY BY 1F5
UNTIL VALUE IS GREATER THAN 1, INCREASING
SCALE FACTP BY 6 EACH TIME

IF VALUE IS GREATER THAN OR = 1E6,
DIVIDE VALUE BY 1E6 UNTIL VALUE IS LESS
THAN 1E6, DECREASING SCALE FACTOP
BY 6 EACH TIME

TEST TO SEE IF VALUES ARE Y
SET XSCALE
SET XPLACE
T3,XSKSW,XDTG1,XDTG2,XST,LOC1
NOW DO Y
SET YSCALE
SET YPLACE
T6,YKSW,YDTG1,YDTG2,YST,LOC2
TURN OFF Y SWITCH

TURN ON PLOT14 SWITCH
EXECUTE PLOT2
IF SETPL01 ENTERED
TURN OFF
PLOT14

```

```

*2D63330
*2D63340
*2D63350
*2D63350
*2D63370
*2D63380
*2D63390
*2D63400
*2D63410
*2D63420
*2D63430
*2D63440
*2D63450
*2D63460
*2D63470
*2D63480
*2D63490
*2D63500
*2D63510
*2D63520
*2D63530
*2D63540
*2D63550
*2D63560
*2D63570
*2D63580
*2D63590
*2D63600
*2D63610
*2D63620
*2D63630
*2D63640
*2D63650
*2D63660
*2D63670
*2D63680
*2D63690
*2D63700
*2D63710
*2D63720
*2D63730
*2D63740
*2D63750
*2D63760
*2D63770
*2D63780
*2D63790
*2D63800
*2D63810
*2D63820

```

1701		MVI	SFSW,0	A0) SETPLT SWITCHES	*2D64343)
1702			OUTP4,0	AND RETURN	*2D643840
1703		L	0,20(1)		*2D643850
1704	GTCMR	LC	0,0(9)	GET PLOTTING CHARACTER	*2D643860
1705		L	13,PT4ADD	ESTABLISH PLOT3	*2D643870
1706		L	USING		*2D643880
1707		L	15,PT4ADD		*2D643890
1708		L	LOT4,15	AND PLOT4 ADDRESSABILITY	*2D643900
1709		L	4,SAV4	RESTORE GPRS 4	*2D643910
1710		L	5,SAV5	AND 5	*2D643920
1711		L	14,STENT3	EXECUTE PLOT3	*2D643930
1712		A	1,THWY4	RUMP GPR 1 TO POINT TO PLOT4 AP35	*2D643940
1713		MVI	PT4SW,0	TURN OFF ALL RELEVANT	*2D643950
1714		MVI	SFSW,0	SWITCHES	*2D643960
1715		R	PLT4	EXECUTE PL T4 AND RETURN FROM THERE	*2D643970
1716		EJFCT			*2D643980
1717	TEND	DC	0,10,0		*2D643990
1718	TENTHD	DC	0,1,0		*2D644000
1719	ONEO	DC	0,1,0		*2D644010
1720	SKFAC	DC	4,-20,0		*2D644020
1721		DC	4,-10,0		*2D644030
1722		DC	4,-6,0		*2D644040
1723		DC	4,-4,0		*2D644050
1724		DC	4,-2,0		*2D644060
1725		DC	4,2,0		*2D644070
1726		DC	4,4,0		*2D644080
1727		DC	4,6,0		*2D644090
1728		DC	4,10,0		*2D64100
1729	CNE	DC	F,1,0		*2D64110
1730	TWO	DC	F,2,0		*2D64120
1731	THREE	DC	F,3,0		*2D64130
1732	FOUR	DC	F,4,0		*2D64140
1733	FIVE	DC	F,5,0		*2D64150
1734	SIX	DC	F,6,0		*2D64160
1735	SEVEN	DC	F,7,0		*2D64170
1736	EIGHT	DC	F,8,0		*2D64180
1737	NINE	DC	F,9,0		*2D64190
1738	TEN	DC	F,10,0		*2D64200
1739	ELEVEN	DC	F,11,0		*2D64210
1740	TWELVE	DC	F,12,0		*2D64220
1741	THIRTY	DC	F,20,0		*2D64230
1742	THIRTY4	DC	F,24,0		*2D64240
1743	THIRTY8	DC	F,28,0		*2D64250
1744	THIRTY	DC	F,30,0		*2D64260
1745	THIRTY2	DC	F,32,0		*2D64270
1746	FIFTY	DC	F,51,0		*2D64280
1747	ONEHUND	DC	F,101,0		*2D64290
1748	ONEHUND4	DC	F,104,0		*2D64300
1749	TWOHUND	DC	F,202,0		*2D64310
1750	ZERUF	DC	F,0,0		*2D64320

1751	SML	DC	E'1F-4'	*2D64330
1752	TENTH	DC	E'.1'	*2D64340
1753	HALF	DC	E'.5'	*2D64350
1754	CNEF	DC	E'1.'	*2D64360
1755	TENF	DC	F'10.'	*2D64370
1756	MILL	DC	E'1.E6'	*2D64380
1757	C1	DC	E'.5989787'	*2D64390
1758	C2	DC	E'.9614706'	*2D64400
1759	C3	DC	E'.2.885391'	*2D64410
1760	C4	DC	E'.4931472'	*2D64420
1761	I	DC	C'1'	*2D64430
1762	DASH	DC	C'-'	*2D64440
1763	PLUS	DC	C'+'	*2D64450
1764	BLNK	DC	C'.'	*2D64460
1765	DECONE	DC	C'1000'	*2D64470
1766	DECZER	DC	C'0000'	*2D64480
1767	BLNKWD	DC	C'.'	*2D64490
1768	RSQRT2	DC	X'409504F3'	*2D64500
1769	HEX40	DC	X'00000040'	*2D64510
1770	CAVRT	DC	X'46000000'	*2D64520
1771	MSK	DC	X'00FFFFFF'	*2D64530
1772	DECCON	DC	X'016777216C'	*2D64540
1773	FIFTY7	DC	H'57'	*2D64550
1774	DGT	DC	C'.'	*2D64560
1775	ECHAR	DC	C'F'	*2D64570
1776	PSKT	DC	A(PL0TP)	*2D64580
1777	ASP2	DC	A(STPLT2)	*2D64590
1778	***			
1779	***	CAUTION:	ALMOST OUT OF ROOM HERE	
1780				
1781		EJECT		
1782		ORC	PLOT*4096	
1783	PLCTP	DS	19F	
1784	IMAGE	DS	1F	
1785	MVPLUS	MVC	O(O,7),PLLINE	
1786	MVILIN	MVC	O(O,7),ILLINE	
1787	MVPTLN	MVC	LINE*12,O(14)	
1788	FPTAB	DC	O'1E-20'	
1789		DC	O'1E-10'	
1790		DC	O'1E-6'	
1791		DC	O'1E-4'	
1792		DC	O'1E-2'	
1793		DC	O'1E2'	
1794		DC	O'1E4'	
1795		DC	O'1E6'	
1796		DC	O'1E10'	
1797	FPTBND	DC	O'1E20'	
1798	NHL	DC	F'6'	
1799	NSBH	DC	F'9'	
1800	NVL	DC	F'11'	

RHH
RHH
RHH

A-151

1851	PT1ADD	DC	A (PLOT1)			*2065330
1852	PT2ADD	DC	A (PLOT2)			*2065340
1853	PT3ADD	DC	A (PLOT3)			*2065350
1854	PT4ADD	DC	A (PLOT4)			*2065350
1855	SPRNT	DC	F'0'			*2065370
1856		DC	A (XPRINT)			*2065380
1857	PLLINE	DS	15D			*2065390
1858	IILINE	DS	15D			*2065400
1859	REGSAV	DS	9F			*2065410
1860	ERRSW	DC	X'000000'			*2065420
1861	ERRNO	DC	X'00'			*2065430
1862	OMITSW	DC	X'00'			*2065440
1863	PLT1SW	DC	X'00'	PLT1 CALLED?: 0=NEVER, 1=LAST BAD, 255=OK	RHH	*2065450
1864	PLT2SW	DC	X'00'	PLT2 CALLED?: 0=NEVER, 1=LAST BAD, 255=OK	RHH	*2065460
1865	LOGSW	DC	X'00'			*2065470
1866	PT14SW	DC	X'00'			*2065480
1867	YSW	DC	X'00'			*2065490
1868	STSW	DC	X'00'			*2065500
1869	ST2SW	DC	X'00'			*2065510
1870	XSKSW	DC	X'00'			*2065520
1871	YSKSW	DC	X'00'			*2065530
1872		DS	0F			*2065540
1873	TTY	DC	CL4*TTY'			*2065550
1874	YSCALE	DS	1F			*2065560
1875	YPLACE	DS	1F			*2065570
1876	XSCALE	DS	1F			*2065580
1877	XPLACE	DS	1F			*2065590
1878	SCALE	DS	1F			*2065600
1879	PLACE	DS	1F			*2065610
1880	XCOM	DC	C'0 PRINTED VALUES OF X ARE 1F'			*2065620
1881	XSI	DC	C' '			*2065630
1882	XCIG1	DC	C'0'			*2065640
1883	XDIG2	DS	1C			*2065650
1884		DC	C' TIMES THEIR ACTUAL VALUES'			*2065660
1885	YCOM	DC	C'0 PRINTED VALUES OF Y ARE 1E'			*2065670
1886	YSI	DC	C' '			*2065680
1887	YCIG1	DC	C'0'			*2065690
1888	YDIG2	DS	1C			*2065700
1889		DC	C' TIMES THEIR ACTUAL VALUES'			*2065710
1890		DS	10F			*2065720
1891		END				*2065730

DIMENSION V11(61), V12(61), V13(61), V14(61), V21(61), V22(61), TALK2000
 V23(61), V31(61), V32(61), V33(61), V34(61), H(11, 92), IN(4), OUT(4), TALK2010
 ZIG(3), TIR(2), DUM(22), B(54), V(82, 65), AH(82), RH(82), CH(82), TALK2020
 3DH(82), ACH(82), BCH(82), CCH(82), DCH(92), BL(3), KI(R), KA(9), TALK2030
 4PP(8), LA(61), BJ(8, 20), BI(8, 60) TALK2040
 DATA V11/30044 B, 3*1H, 3*4H B, 2*4H S, 2*4H KE, 3*4H B, 4*4H TALK2050
 . AC, 1H, 4*4H U, 9*1H / TALK2060
 DATA V12/303HODY, 3*4H VEH, 3*3HELT, 2*3HEAT, 2*4HLATI, 3*3HFLT, 4*4HCE TALK2070
 . LE, 4*H H, 4*4HPPER, 5*4H HE, EL KN, 2*4H FD/ TALK2080
 DATA V13/2444HANG, 5*4H MUTI, 3*4HICLE, 5*4HURC, 2*4HVF H, 3*4HANG, 4*4H TALK2090
 . 4HRUME, 2*HIP, 4*4H TOR, 5*2HAD, 3*HRDM, 2*HEE, 2*2HOT/ TALK2100
 DATA V34/16*1H, 8*2HON, 2*1H, 2*HON, 2*1H, 2*HON, 2*1H, 2*HON, 5*1H, 1HL, TALK2110
 . 4*1H, 1HT, 1H, 1HT, 2*1H, 1HK, 1H, 2*HEL, 1HD, 3*HEEL, 2*HEL, 4*HLUMN, TALK2120
 . 1HD, 3*HEEL, 4*HRACK/ TALK2130
 DATA V14/242*2HES, 6*2HUN, 3*1H, 5*2*HES, 2*3*HEAD, 3*2*HES, 4*3*HTEF, 1H, TALK2140
 . 4*2HSU, 9*1H / TALK2150
 DATA V21/7 LOWCENT UP UP LO UP LO LOWCENT UP UP, TALK2160
 . LO UP LO LOWCENT UP UP LO UP LO, 3*4H HOP, 3*4* VE, 3*4 TALK2170
 . H M, 4H LA, 3*1H, 4H FRO, 2*4H PD, 4H LA, 20*1H / TALK2180
 DATA V22/3*4HER T, 4*HHEAD, *PER MER, *3*4HFR T, 4*HHEAD, *PER WTALK2190
 . ER PER MER, *3*4HER T, 4*HHEAD, *PER MER PER MER, *3*4HIZON, 3*4HRTIC, TALK2200
 . 3*4HOTIO, *P BELOWEUPPE HIPNT ESTISITIP BELOWEUPPEHEAD, 4*HAFAD, 2*4 TALK2210
 . HCHES, 14*3H ON/ TALK2220
 DATA V23/3*4HORSO, 1H, 2*3HARM, 2*3HLEG, 3*4HOP, 3*4HARM, 2*3HLE TALK2230
 . G, 3*4*URSO, 1H, 2*3*ARM, 2*3*HLEG, 3*3*HTAL, 3*2*HOP, 3*1HN, 2*1HR, 1H TALK2240
 . 3*HDGE, 2*2*HON, 2*HLT, 2*1HR, 2*1H, 2*1HT, 14*1H / TALK2250
 DATA V31/16*1H, 8*4H AC, 2*1H, 4H AC, 2*1H, 4H AC, 2*1H, 4H AC, 5* TALK2260
 . 1H, 4H H, 11*1H, U M STE L STE STE FRO, / TALK2270
 DATA V32/8*4*HPOSI, 8*4HVELO, 8*4HCELE, *POSIVELOCEPOSIVELOCELEPUSI, TALK2280
 . .VEL*CELE, 1H, 2*4HSHOU, 2*1H, *ORIZVERT, 1H, 2*4HSHOU, *RESU AN, TALK2290
 . *RESU AN FLSEAT *OPPERINDFINWERINTOE ERINNT S, / TALK2300
 DATA V33/8*4HTION, 8*4HCITY, 8*4HRATI, *TIONCITYRATIIONCITYRATIION, TALK2310
 . *CI TYRATI, 1H, 2*4HLDER, 2*1H, 4*HONTA, 4*HICAL, 1H, 2*4HLDER, *L TANGTALK2320
 . LE LTANGLE OOR BACOF PANHIELG *H PANG CORDARG WHEAT, / TALK2330
 EQUIVALENCE(BI(46), R(1, 1)) TALK2340
 DATA B1/FLOR-X, *6*1H, *SEAT BACK-X, *5*1H, *ROOF-X, *5*1H, TALK2350
 . *UPPER PANEL-X, *4*1H, *WINDSHIELD-X, *5*1H, *LOWER STEERING WHEEL TALK2360
 . L-X, *2*1H, *LOWER PANEL-X, *4*1H, *STEERING COLUMN-X, *3*1H TALK2370
 . *TOEBOARD-X, *5*1H, *FLOR-Y, *6*1H, *SEAT RACK-Y, *5*1H, TALK2380
 . *ROOF-Y, *6*1H, *UPPER PANEL-Y, *4*1H, *WINDSHIELD-Y, *5*1H, TALK2390
 . *LOWER STERLING WHEEL-Y, *2*1H, *LOWER PANEL-Y, *4*1H, *STEERINTALK2400
 . G COLUMN-Y, *3*1H, *TOEGUARD-Y, *5*1H, *HIP CONTACT ARC RADIUS TALK2410
 . *2*1H, *UPPER TORSO CONTACT ARC RADIUS, *HAND CONTACT ARC RADIUS TALK2420
 . *2*1H, *ELBOW CONTACT ARC RADIUS, *2*1H, *HAND CONTACT ARC RADIUS TALK2430
 . S, *2*1H, *KNEE CONTACT ARC RADIUS, *2*1H, *FOOT CONTACT ARC RADIUS TALK2440
 . *2*1H, *TO HEAD CENTER OF CURVATURE TO CHEST CENTER OF CUTALK2450
 . *RVATURE, 1H, *LOWER TORSO LENGTH, *3*1H, *CENTER TORSO LENGTH, TALK2460
 . 3*1H, *UPPER TORSO LENGTH, *3*1H, *CENTER TORSO TO UPPER ARM, TALK2470
 . 1H, *UPPER ARM LENGTH, *4*1H, *LOWER ARM LENGTH, *4*1H, *UPPER LEG TALK2480
 . *LENGTH, *4*1H, *LOWER LEG LENGTH, *4*1H, *FLOOR-LFNGTH, *5*1H, *SEAT B TALK2490

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51 .ACK-LENGTH*,4*1H ,*ROOF-LENGTH*,5*1H ,*UPPER PANEL-LENGTH *,3*1HTALK2500
52 . ,*WINDSHIELD-LENGTH*,3*1H ,*LOWER STEERING WHEEL LENGTH *,1H , TALK2510
53 .*LOWER PANEL-LENGTH*,3*1H ,*STEERING COLUMN-LENGTH*,2*1H , TALK2520
54 .*TOEBOARD-LENGTH *,4*1H ,*DISTANCE FROM HIP TO SEAT FRONT *, TALK2530
55 .DATA BJ/*NUMBER OF BELT SEGMENTS *,2*1H ,*LOWER TORSO-C.G. TO LOWFTALK2540
56 .R JOINT CENTER TORSO-C.G. TO LOWER JOINTUPPER TORSO-C.G. TO LOWER TALK2550
57 .*JOINT HEAD-C.G. TO LOWER JOINT*,2*1H ,*UPPER ARM-C.G. TO LOWER JOINTTALK2560
58 .*LOWER ARM-C.G. TO LOWER JOINT UPPER LEG-C.G. TO LOWER JOINTTALK2570
59 .*LOWER LEG-C.G. TO LOWER JOINT UPPER STEERING WHEEL-X*,2*1H TALK2580
60 .,*BACK OF FRONT SEAT-X*,3*1H ,*UPPER STEERING WHEEL-Y *,2*1H TALK2590
61 .*BACK OF FRONT SEAT-Y*,3*1H ,*UPPER STEERING WHEEL-LENGTH *, TALK2600
62 .*BACK OF FRONT SEAT-LENGTH *,1H / TALK2610
63 DO 9 I=1,82 TALK2620
64 DO 9 J=48,61 TALK2630
65 V(I,J)=0. TALK2640
66 DO 8 I=1,61 TALK2650
67 LA(I)=-1 TALK2660
68 DO 25 I=1,3 TALK2670
69 IG(I)=0 TALK2680
70 DTR=.01745329 TALK2690
71 N=0 TALK2700
72 REWIND 9 TALK2710
73 READ(9)(DUM(I),I=1,6),(B(I),I=1,9),DUM(1),(B(I),I=10,19),DUM(1), TALK2720
74 .B(19),DUM(1),(B(I),I=20,4),(DUM(I),I=1,22),B(45),B(46), TALK2730
75 .(DUM(I),I=1,10),(B(I),I=47,54) TALK2740
76 N=N+1 TALK2750
77 IF(N.GT.82) GO TO 19 TALK2760
78 READ(9,END=19)IT(N),(V(N,I),I=1,33),AH(N),BH(N),CH(N),DH(N),ACH(N), TALK2770
79 .BCH(N),CC-1(N),DCH(N),JJ,(KI(I),KA(I),PP(I),I=1,JJ),(V(N,I),I=34,43)TALK2780
80 .),BL TALK2790
81 IF(IT(N).LT.0.) GO TO 19 TALK2800
82 DO 20 I=41,43 TALK2810
83 V(N,I)=V(N,I)/DTR TALK2820
84 IF(IJJ)18,18,4 TALK2830
85 DO 7 J=1,JJ TALK2840
86 KI=KI(IJ) TALK2850
87 GO TO (61,61,62,63,64,64,64,66),KI,J TALK2860
88 M=48 TALK2870
89 GO TO 67 TALK2880
90 M=48+KA(J)/2 TALK2890
91 GO TO 67 TALK2900
92 M=51+KA(J) TALK2910
93 GO TO 67 TALK2920
94 M=58+(KI,J-5)/2 TALK2930
95 GO TO 67 TALK2940
96 M=60+(KA(J)-11)/8 TALK2950
97 LA(M)=KA(J) TALK2960
98 V(N,M)=PP(J) TALK2970
99 GO TO 18 TALK2980
100 WRITE(6,601) TALK2990

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101 601 FORMAT('OENTER 6 IF CONVERSATIONAL, 7 IF NOT')
102 READ(1,500)IWR
103 IF(IWR.EQ.6)IR-1
104 IF(IWR.EQ.7)IR-8
105 N=N-1
106 WRITE(IWR,602)
107 FORMAT(1H0/1X,'OENTER DATA TYPE, 1 IF INITIAL, 2 IF GENERAL, 3 IF
108 -COMPLETE, 4 IF DONE')
109 READ(IR,50C,END=598)*IN()
110 FORMAT(11I0)
111 GO TO (1,2,3,999),KIND
112 WRITE(IWR,612)
113 FORMAT('OENTER VARIABLE NUMBER - 0 IF DONE')
114 39 WRITE(IWR,613)
115 FORMAT(' ( )')
116 READ(IR,500)K
117 KC=K
118 IF(K.FQ.0) GO TO 1000
119 IF((K.NE.4).AND.(K.NE.13).AND.(K.NE.39)) GO TO 40
120 IF((K.EQ.3).OR.0) GO TO 41
121 WRITE(IWR,607)
122 READ(IR,50)NPASCR
123 IG(3)=1
124 IF(NPASCR-2)42,40,42
125 41 IF(K-13) 44,45,46
126 44 K=55
127 GO TO 43
128 45 K=57
129 GO TO 43
130 46 K=59
131 43 IF(NPASCR.EQ.3)K=K+1
132 4C WRITE(6,614)R(KC),(BI(I,K),I=1,8)
133 614 FORMAT(1H0,F13.3,' = ',#A4)
134 GO TO 39
135 2 WRITE(IWR,603)
136 603 FORMAT('OHOW MANY VARIABLES?')
137 READ(IR,50)NUM
138 WRITE(IWR,604)
139 604 FORMAT('OENTER VARIABLE NUMBERS/1X,4(' ( )')')
140 READ(IR,501)(IN(J),J=1,NUM)
141 501 FORMAT(6I1X,E3.1X)
142 50 WRITE(IWR,605)
143 605 FORMAT('OENTER TIME INTERVAL/1X,'FROM('7X,')TO('7X,')')
144 502 DO 11 I=1,N
145 FORMAT(5X,F7.0,4X,F7.0)
146 READ(IR,502)TMIN,TMAX
147 IF(TMIN.LE.T(I))GO TO 12
148 11 CONTINUE
149 12 JI=1
150 DO 13 I=JI,N

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TALK3000
TALK3010
TALK3020
TALK3030
TALK3040
TALK3050
TALK3060
TALK3070
TALK3080
TALK3090
TALK3100
TALK3110
TALK3120
TALK3130
TALK3140
TALK3150
TALK3160
TALK3170
TALK3180
TALK3190
TALK3200
TALK3210
TALK3220
TALK3230
TALK3240
TALK3250
TALK3260
TALK3270
TALK3280
TALK3290
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TALK3380
TALK3390
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TALK3420
TALK3430
TALK3440
TALK3450
TALK3460
TALK3470
TALK3480
TALK3490

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151 IF (TMAX.LT. .1(I)) GO TO 14
152 CONTINUE
153 JJ=I
154 DO 15 I=1,10JM
155 K=IN(I)
156 IF (K.LT.4) .OR. (K.GT.47) GO TO 24
157 IF (K.LT.48) GO TO 23
158 IF (IG(2).E.0) GO TO 28
159 WRITE(IMR,415)
160 FORMAT('OCCUPANT VALUE OF *PCHEST*')
161 READ(IR,503) PCHEST
162 FORMAT(F15.0)
163 IG(2)=1
164 DO 26 II=1,6
165 X=ACH(II)-PCHEST*BCH(II)
166 Y=CCH(II)+PCHEST*DCH(II)
167 V(II,46)=SQRT(X**2+Y**2)
168 V(II,47)=ATAN2(Y,X)/DTR
169 GO TO 28
170 IF (IG(1).E.0) GO TO 28
171 WRITE(IMR,606)
172 FORMAT('OCCUPANT VALUE OF *PHEAD*')
173 READ(IR,503)PHEAD
174 IG(1)=1
175 DO 27 II=1,6N
176 X=AH(II)-PHEAD*BH(II)
177 Y=CH(II)+PHEAD*DH(II)
178 V(II,44)=SQRT(X**2+Y**2)
179 V(II,45)=ATAN2(Y,X)/DTR
180 IF (K.LT.48) GO TO 28
181 IF (LAIK).E.0) GO TO 28
182 WRITE(6,635)K
183 FORMAT('CONTACT NUMBER ',I2,' NEVER OCCURRED')
184 K=1
185 H(1,1)=V11(K)
186 H(2,1)=V12(K)
187 H(3,1)=V13(K)
188 H(4,1)=V14(K)
189 H(5,1)=V21(K)
190 H(6,1)=V22(K)
191 H(7,1)=V23(K)
192 IF (K.LT.48) GO TO 29
193 K=LAIK+47
194 IF (K-51)29,30,29
195 IF (IG(3).E.0) GO TO 31
196 WRITE(IMR,607)
197 FORMAT('OCCUPANT POSITION NUMBER*')
198 READ(IR,503)NPASGR
199 IG(3)=1
200 IF (NPASGR-2) 32,29,33

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TALK3500
TALK3510
TALK3520
TALK3530
TALK3540
TALK3550
TALK3560
TALK3570
TALK3580
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TALK3940
TALK3950
TALK3960
TALK3970
TALK3980
TALK3990

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201 K=57
202 GO TO 29
203 K=58
204 H(8,I)=V31(K)
205 H(9,I)=V32(K)
206 H(10,I)=V33(K)
207 H(11,I)=V34(K)
208 WRITE(6,608)((H(K,L),K=1,4),L=1,NIM)
209 FORMAT(71X,7X,4(4A4))
210 WRITE(6,609)((H(K,L),K=5,7),L=1,NJM)
211 FORMAT(9A,4(3A4,4X))
212 WRITE(6,610)((H(K,L),K=8,11),L=1,NUM)
213 FORMAT(0, TIME,4(4A4))
214 IF(KIND.EQ.3) GO TO 51
215 DO 16 J=JI, JJ
216 DO 17 I=1, NUM
217 K=IN(I)
218 OUT(I)=V(J,K)
219 WRITE(6,611) T(J), (OUT(I), I=1, NUM)
220 FORMAT(1X, F5.3, 4(F13.3, 3X))
221 GO TO 1000
222 WRITE(IWR, 630)
223 FORMAT('OENTER DECISION VARIABLE')
224 READ(IR, 500) IN(I)
225 WRITE(IWR, 631)
226 FORMAT('OENTER COMPARISON VALUE')
227 READ(IR, 500) CV
228 WRITE(IWR, 632)
229 FORMAT('OENTER COMPARISON MODE - 1 IF GT, 2 IF LT')
230 READ(IR, 500) MO
231 WRITE(IWR, 603)
232 READ(IR, 500) NUM
233 NUM=NUM+1
234 WRITE(IWR, 633)
235 FORMAT('OENTER VARIABLE NUMBERS', /X, 3(' ', ))
236 READ(IR, 501) (IN(I), I=2, NUM)
237 GO TO 50
238 KJ=IN(1)
239 IF(MO.EQ.1) GO TO 52
240 DO 53 J=JI, JJ
241 IF(V(J, KJ) .LT. CV) GO TO 54
242 CONTINUE
243 WRITE(6, 634)
244 FORMAT('O THE REQUIRED CONDITION NEVER OCCURRED')
245 GO TO 1000
246 DO 56 J=JI, JJ
247 IF(V(J, KJ) .GT. CV) GO TO 54
248 CONTINUE
249 GO TO 55
250 DO 57 I=1, NUM

```

```

TALK4000
TALK4010
TALK4020
TALK4030
TALK4040
TALK4050
TALK4060
TALK4070
TALK4080
TALK4090
TALK4100
TALK4110
TALK4120
TALK4130
TALK4140
TALK4150
TALK4160
TALK4170
TALK4180
TALK4190
TALK4200
TALK4210
TALK4220
TALK4230
TALK4240
TALK4250
TALK4260
TALK4270
TALK4280
TALK4290
TALK4300
TALK4310
TALK4320
TALK4330
TALK4340
TALK4350
TALK4360
TALK4370
TALK4380
TALK4390
TALK4400
TALK4410
TALK4420
TALK4430
TALK4440
TALK4450
TALK4460
TALK4470
TALK4480
TALK4490

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TALK4500
TALK4510
TALK4520
TALK4530
TALK4540
TALK4550
TALK4560
TALK4570
TALK4580
TALK4590

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251      K=IN(I)
252      OUT(I)=V(J,K)
253      WRITE(6,611)T(J),(OUT(I),I=1,NUM)
254      GO TO 1000
255      IF (IMR.EQ.6) GO TO 999
256      IMR=6
257      IR=5
258      GO TO 1000
259      999  STOP
260      END
```

```

1 DIMENSION ELAMB(6), XSMALA(10), YSMALA(10), A*(RI, EL(8), GA(10),
2 .CPSIA(10), SPSIA(10), IGNORE(10), RH(18), ZVEC(11), ZVFCP(11),
3 .PHI(3), PNI(3), PN(3), TA(8)
4 DIMENSION TT(8), TV(9), KI(9), KA(8), PP(8)
5 REMIND 9
6 READ(9) ELAMB, XSMALA, YSMALA, AR, RHDPFZ, RHCPDZ, EL, DA, CPSIA,
7 ISPSIA, TGAMZ, ZZER, NBELT, IGNORE, RHO
8 READ(9, END=1) TIME, TT, TV, TA, DISP, ZVECP(9), PLX, ZVFC(10),
9 IZVECP(10), PLY, ZVEC(11), ZVECP(11), PLC, AH, RH, CH, DH, ACH, RCH, CCH,
10 ZDCH, JJ, (KI(1), KA(1), PP(1), I=1, JJ), (PN(N), N=1, 3), FSPRM, FS,
11 SHEAD, HEADY, PHI, RL
12 IF (TIME.LT.0.) GO TO 1
13 GO TO 2
14 CALL SUMARY
15 STOP
16 END

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TALK4600
TALK4610
TALK4620
TALK4630
TALK4640
TALK4650
TALK4660
TALK4670
TALK4680
TALK4690
TALK4700
TALK4710
TALK4720
TALK4730
TALK4740
TALK4750

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BAIL2 Main Program

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