74-130	CALIBR	ATED	DEL	AYING	SWEEP
T-IJA	Instru	cti	o n	Man	ual
Se	rial No.				

This Plug-in Module is designed for use with the Fairchild Type 766H Series Oscilloscope. Insert this Manual into the binder you received with the Type 766H Series Instruction Manual.



SO SOMERSET PLACE, CLIFTON, N. J. 07015

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DELAY ZERO control permits precise DELAY VERNIER zero adjustment

DISPLAY LOGIC switch determines sweep operational modes; see text for details

Concentric control positions normal or expanded display on screen; pull knob for 10X mag of display

DELAY VERNIER control determines the onscreen distance from the normal sweep start at which the delayed sweep is either triggered or armed; functions as an accurate delay multiplier when used with the DA TIME/DIV switch



Beam position

SWEEP READY lamp indicates DA Sweep is armed and ready to be triggered

SWEEP CAL control normalizes the Plug-in to Main Frame

NDT & DA TIME/DIV Selector switches: knobs may be rotated together or the DA sweep knob can be disengaged and rotated separately; concentric knob provides vernier sweep operation (UNCAL lamp lights)

Figure 2-1b. Type 74-13A Function of Controls and Connectors

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least 0.5 volt, peak-to-yeak (1 mc) and bear a fixed time relationship to the displayed signal. To use an external signal for triggering the sweep, connect the signal to the EXT TRIG connector and set the Trigger SOURCE switch to EXT.

c. Line

If the pattern on display bears a fixed time relationship to the power-line frequency, the sweep may be triggered by this signal. To accomplish this, set the Trigger SOURCE switch to LINE. Always use dc coupling mode with LINE Trigger Source.

2-4. TRIGGER COUPLING SELECTION

a. AC Coupling

Selection of the AC triggering mode is accomplished by setting the COUPLING switch to AC. This mode is provided with a high-pass filter that has a low-frequency cutoff nominally at 80 cycles. This feature prevents erratic triggering when positioning the pattern vertically and using internal triggering. In the AC mode, triggering is unaffected by the dc components of the triggering signal or by the vertical positioning of the trace. The triggering level can be selected to provide the desired display via use of the Trig LEVEL control.

When using the AC mode, the Trigger COUPLING switch is set to AC. The trace always starts at the same point on the *Waveform* for a given Trig LEVEL control setting regardless of the vertical positioning.

Note: AC coupling triggering on the line-frequency calibrator signal or square wave signals less than 100 cycles, may be erratic since the 80-cycle cutoff filter severely integrates the trigger. DC coupling is recommended for these signals.

b. DC Coupling

The DC mode is especially useful for viewing waveforms which change very slowly and which are therefore discriminated against by the low-frequency cutoff of the AC position (80 cps). Because of the coupling network time constant in the AC mode, signals having random repetition rates are sometimes viewed more stably in the DC mode. This mode permits excellent triggering on all types of waveforms and is most useful in the following applications:

1. For optimizing trigger sensitivity or operation when low-frequency signals are applied;

2. For maintaining the initial reference position of the trace with respect to the CRT scale at a given TRIG LEVEL control setting when on Internal source; and

3. For avoiding trigger point variations due to random repetition rate triggering signals. When using the DC mode, the Trigger COUPLING switch is set to DC. When using internal source, the trace always starts at the same point on the *Scale* for a given setting of the Trig LEVEL control regardless of the vertical positioning.

c. ACF Coupling

The ACF mode is a special high-frequency form of the AC mode and is used to reject low-frequency components in the triggering signal. Use AC triggering unless low-frequency rejection is required. Triggering signals with frequency components below 10 Kc, for example the calibrator signal, may not initiate the sweep circuits when the ACF mode is used. Also, the ACF mode will assure stable triggering from the dualtrace plug-in when it is set up for alternate sweep mode, and using internal trigger source. Thus the ACF mode prevents the difference in positioning level of the two channels from interfering with stable triggering.

Signals must have rise or fall times faster than 10 μ sec when using the ACF mode. If slower dual time signals are to be displayed, use external triggering. Note that the Type 76-08 and other multi-trace plug-ins are provided with a selector switch which permits triggering from one channel only. Therefore the ACF electronic switch mode no longer applies.

Occasionally it is required to obtain stable triggering from a complex high-frequency waveform that contains undesirable low-frequency noise or line-frequency components. In such cases, the additional noise and line pickup may make it difficult to obtain a stable display. If this occurs, select the ACF triggering mode, thereby eliminating the effects of these undesired components. The low-frequency components are blocked from the triggering circuit while the highfrequency triggering waveform is passed to produce the stable triggering that is required. In all other respects, the ACF triggering mode is identical to the AC mode.

2-5. TRIGGER SLOPE SELECTION

When the Trigger SLOPE switch is set to +, the sweep is triggered on the rising or positive slope of the excitation signal. When the Trigger SLOPE switch is set to -, the sweep is triggered on the falling or negative slope of the excitation signal.

2-6. TRIGGER LEVEL SELECTION

The Trig LEVEL control permits selection of a specific voltage which the triggering signal must exceed before the sweep fires. When the Trigger SLOPE switch is set to the + position, adjustment of the Trig LEVEL control makes it possible to trigger the sweep consistently on the positive slope of the ex-

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NORMAL SWEEP DISPLAY OF CAL SIGNAL To obtain the calibrator display using NORMAL sweep, set the controls exactly as shown and perform the numbered steps in sequence.

Use the same procedure when difficulty is experienced in obtaining a display. This will eliminate "cockpit" troubles due to misalignment of controls.



Figure 2-2. Type 74-13A Normal Display

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TRIGGERED STROBE AND DELAYED



NOTE

The amount of delay occurring from the application of the triggering signal until the Delayed Sweep storts, is indicated directly by the setting of the NDT TIME/DIV switch (plastic skirt) and DELAY VERNIER dial. In this instance, the NDT sweep rate of 5 mSec/Div is multiplied by the DELAY VERNIER dial setting of 4 div yielding a calibrated delay time of 20 milliseconds. The above applies only when the delayed-triggered operational mode is used.



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DISPLAY OF CAL SIGNAL



(a) Trace intensified by use of delayed sweep(b) Expanded presentation of the intensified pattern



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Figure 2-4a. Type 74-13A Armed Strobe Display

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DISPLAY OF CAL SIGNAL



Figure 2-4b. Type 74-13A Armed Delayed Display

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citation signal. Conversely, with the Trigger SLOPE switch set to the - position, adjustment of the Trig LEVEL control makes it possible to trigger the sweep consistently on the negative slope of the excitation signal. Normal trigger level range is ± 10 volts. This may be extended to ± 100 volts on external source by pulling the Trigger LEVEL knob into EXT/10 position.

2-7. SWEEP OPERATIONAL MODES

a. Introduction

When using the Delaying Sweep Time Base Plug-in, the start of the horizontal sweep can be delayed for a period of from 1/4 microsecond to 20 seconds after application of the triggering waveform. This is accomplished through simultaneous use of the NDT Time Base and the DA Time Base. In this application, the NDT Time Base is used to provide the accurate time delay while the DA Time Base provides a normal horizontal sweep at the end of the delay period. The duration of the sweep delay is controlled by the NDT TIME/DIV and the DELAY VERNIER control settings.

The delayed sweep feature of this instrument may be employed in a number of special applications to increase its versatility. Such applications include high magnification of a selected portion of an undelayed sweep, accurate time measurements, and accurate measurements of waveform jitter. Also, it is possible to pick off and display any desired line of a television scan or to check pulse-time modulation.

b. Sweep Range Indicators

The NDT TIME/DIV switch is provided with an indicator window mounted on a plastic skirt; the DA TIME/DIV switch is mounted on top of this skirt and is identified as the Delayed Sweep knob. Turning the knob of the latter will also permit control of the Delayed Sweep time duration. A push-pull clutch permits the outer 'knob to engage the skirted knob to adjust both sweep ranges simultaneously, or the Delayed Sweep range knob may be declutched and rotated independently to sweep rates faster than the NDT sweep rate.

c. Normal Sweep Display

When the DISPLAY LOGIC switch is set to NOR-MAL, only the NDT Time Base is displayed. Triggering is derived from the displayed signal internally or line. External signals may be applied to the lower EXT TRIG connector. Refer to Figure 2-2.

d. Triggered Strobe Display

When the DISPLAY LOGIC switch is set to Triggered STROBE, and the Delayed TIME/DIV switch is set for a higher sweep rate than the NDT TIME/ DIV switch, a portion of the sweep may be brightened. (See Figures 2-3a and 2-4a.) The start of the brightened portion (Strobe) indicates the start of the Delayed Sweep and the length of the strobe indicates the Delayed Sweep duration. The start of the strobe may be positioned left or right with the DELAY VERNIER control. The length of the strobe may be adjusted with the Delayed TIME/DIV control. Note that the start of the strobe is not affected by the setting of the latter control. Using these two controls, it is possible to include any portion of the display waveform in the brightened or strobed area.

The amount of delay occurring from the application of the triggering waveform until the Delayed Sweep is permitted to run, is determined by the setting of the NDT TIME/DIV switch and the DELAY VERNIER control. The Delayed Sweep will occur immediately at the end of the preset delay period. This mode from now on will be referred to as the Delayed-Triggered sweep mode. It is the mode of operation that permits the operator to select continuously variable delay times for making accurate time and waveform jitter measurements.

The Delayed Sweep automatically shuts off when the Normal Sweep is terminated. This prevents brightening of the sweep retrace in either of the STROBE positions.

e. Delayed Triggered Display

When the DISPLAY LOGIC switch is set to Triggered DELAYED, the brightened section of the display in the STROBE position is now expanded to full scale. See Figures 2-3b and 2-4b.

The amount of magnification is the ratio of the NDT sweep rate to the Delayed Sweep rate. The magnification ratio may be expressed:

M	Normal	Sweep	Rate	(Time/	Div)
Magnification ratio =	Delayed	Sweep	Rate	(Time)	(Div)

For example, if the NDT TIME/DIV switch is set to 1 mSEC, and the Delayed TIME/DIV switch is set to 1 μ SEC, the brightened portion of the sweep is magnified horizontally 1000 times when the DISPLAY LOGIC switch is set to the Triggered DELAYED position.

Automatic provision is made for shutoff of the Normal Sweep when the Delayed Sweep is terminated. This permits maximum duty-cycle performance in the DELAYED MODE.

f. Delayed-Armed Operation

If the display is set for Delayed-Armed operation, the delayed sweep does not start at the end of the indicated delayed period until a triggering pulse is applied to the DA trigger circuit. This triggering pulse

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may be either the input waveform to the oscilloscope or an externally-derived triggering signal. The triggering Source, Coupling, Slope, and Level may be selected in the same manner as for the conventional STROBE and DELAYED triggered operation. In the Delayed-Armed mode of operation, the Delayed Sweep does not start precisely at the delay time indicated by the DELAY VERNIER and NDT TIME/DIV control setting, but instead is initiated by the next suitable triggering following the indicated delay interval. This mode from now on will be referred to as the Delayed-Armed mode of sweep operation. See Figures 2-4a and 2-4b.

The armed delayed time display does not appear to be continuously variable. The Armed mode should be used whenever the signal to be displayed has accumulative jitter between the start of the normal sweep and the delayed magnified section.

g. Automatic NDT Sweep

Auto triggering provides a visible base line on all sweep ranges when there is no signal input. The sweep free runs until a trigger signal with frequencies between 10 cycles and approximately 10 megacycles is applied. The application of the trigger signal immediately switches the sweep to the triggered mode thus providing stable sync. When the triggering signal is removed, the sweep reverts to the freerunning mode after a delay of about 1 second.

The automatic NDT sweep mode is very useful when doing equipment testing since a reference trace will always be visible with or without a signal applied to the oscilloscope. To obtain automatic NDT sweep operation, set the Sweep Mode toggle switch to AUTO position.

h. HF Recurrent Sweep

Stable synchronization of very high frequency signals can be best accomplished when the NDT sweep is operating in the recurrent mode. Recurrent operation is selected by setting the Sweep Mode toggle switch in the HF RECUR position. Use of this switch improves the count down and lock-in of signals having repetition rates of 5 Mc or greater. It provides stable synchronization of signals of 1 cm deflection to beyond 50 Mc.

i. Single-Sweep Operation

Single-sweep operation infers that the time base moves but one stroke until reset. Using a repetitive sweep to view a varying waveform would result in an overlapped and unintelligible display caused by many displays being superimposed on one another. However, when it is desired to view a single display of an input signal which continually varies in amplitude, shape, or time, the instrument may be set up for single-sweep presentation. Thus, by commanding but one stroke of the sweep at a time, single sweep operation eliminates the overlapping caused by the multiple traces and enables the display to be viewed and/ or recorded clearly.

Single-sweep operation is obtained by using the Delayed Sweep in the Delayed Armed mode. Since the Delayed Sweep is armed by a trigger derived from the NDT Delaying Sweep, the arming procedure is to trigger the NDT Delaying Sweep. This is accomplished manually by rotating the NDT Delaying Sweep LEVEL control to both extremes or electrically by a signal applied to the NDT EXT TRIG input connector. The Delayed Sweep will remain armed until a trigger signal arrives to fire the sweep. One sweep will occur after which further incoming triggers are locked out until the circuit is rearmed. In other words, a single trace will sweep across the screen each time the sweep is triggered and at the end of its travel, the beam will rest off screen.

To rearm the sweep, proceed as instructed above. The sweep will then retrace to the left hand side of the screen and is armed ready to fire when the next trigger signal arrives.

2-8. SWEEP EXPANDER

When the POSITION control knob is pulled out, the sweep may be expanded horizontally by a factor of 10 about the screen center. Thus, to achieve an X10 expansion of a desired segment of the trace, set that segment of interest to the screen center with the POSI-TION control and pull out this control. Any portion of the expanded display may be observed by adjusting the POSITION control.

When the instrument is set up for X10 expansion of the sweep, the sweep rate indicated by the setting of the TIME/DIV control must be divided by 10 to obtain the actual time required for the spot to move one division. For example, if the TIME/DIV control is set to 10 mSEC, the actual time per division is 10 milliseconds, divided by 10, or 1 millisecond per division.

2-9. SWEEP CALIBRATION ADJUSTMENT

Whenever the Time Base Plug-in is removed from the Main Frame and inserted in another, the frontpanel screwdriver SWP CAL control must be reset. This procedure is necessary to compensate for difference in deflection plate sensitivities. In addition, if the Time Base unit is switched from the X cavity to the Y cavity of the same Main Frame, readjustment will be necessary since the difference in average deflection plate voltages between modules affects the over-all deflection sensitivity of the cathode-ray tube. To properly normalize the gain between channels or between the plug-in unit and the Main Frame, proceed as follows:

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1. Set up the instrument for normal display of the CAL signal. Allow a warmup time of 15 minutes. (See Figure 2-2.)

2. Set TIME/DIV switch to 10 mSEC.

3. Adjust SWP CAL front-panel screwdriver control for precisely 6 cycles of the calibrator display (60-cycle line) in 10 divisions.

NOTE: For 50-cycle line, adjust SWP CAL control for 5 cycles of the calibrator display. For 400-cycle line, use 0.5 msec/div sweep and adjust SWP CAL control for 2 cycles of the calibrator display.

2-10. X-Y DISPLAYS

CAUTION

KEEP INTENSITY LOW

Screen damage can result from too intense a beam resting at one point on the screen.

When desiring to view one voltage plotted against another (not the internal time base) apply the Y signal to INPUT A connector on the Y Plug-in and the X signal to X AMP (green) BNC connector on the Delaying Sweep module. X-Y displays may be used to show sweep signal generator plots, Lissajous phase measurements, curve trace information and other similar signal relationship.

Set the DISPLAY LOGIC switch to X AMP, the DA Trigger SOURCE switch to EXT, and the DA SLOPE switch to +. Adjust the VOLTS/DIV and X AMP ATTEN controls to obtain an appropriate display on the screen.

2-11. GATE OUTPUT

A positive gate coincident with the sweep output is available on a front-panel BNC connector labeled + GATE. The gate amplitude is 2.5 volts nominal into an impedance of 500 ohms and load impedance should be greater than 100K ohms shunted by less than 15 pf. This positive pulse may be used to trigger other devices in order to achieve sufficient delay to view the output of such devices completely displayed on the oscilloscope.

Use of the gate output in conjunction with triggered pulse generators will permit the instrument to display the leading edge of the pulse waveform even though no signal delay is incorporated in the Y Amplifier.

The period of the positive gate may of course, be measured extremely accurately with an electronic counter. Since the period of the gate output is a direct measure of total sweep time, it is possible to use this oscilloscope in conjunction with a counter to digitize the time duration of input signals. Use of the TIME/ DIV and the VARIABLE controls will permit the operator to display the waveform to be measured over the entire sweep. Timing accuracies of 1 part in 107 are thus readily obtainable.

2-12. SAWTOOTH OUTPUT

A front-panel connector labeled SAW provides a positive-going saw of approximately 25 volts amplitude. The saw output is referenced within minus 3 volts of ground and is time coincident with the NDT sweep.

The sawtooth voltage may be used for initiating delayed activities, controlling an X-Y plotter, or acting as a time base for associated analog equipment. The sawtooth output should not be loaded by an impedance to ground of less than 100K ohms shunted by no more than 15 pf. Voltage take-off through an attenuator probe is recommended.

2-13. TIME MEASUREMENTS

a. How to Make Elapsed Time Measurements Using the CRT Scale

Any horizontal distance on the screen of the oscilloscope can be used to represent a precise interval of time when the time-base circuits are set up for calibrated sweep (TIME/DIV Vernier control set to CAL). Use of this feature permits you to accurately measure the elapsed time between the desired point of interest on the display. To measure the time interval, proceed as follows:

1. Using the calibrated scale, measure the horizontal distance in divisions between that portion of the display whose time interval you wish to find.

2. Multiply the horizontal dimension obtained in Step 1 by the TIME/DIV control setting to obtain the time interval. See Figure 2-5.

b. How to Find Repetition Rate of Frequency Using the CRT Scale

The repetition rate or frequency for periodic signals can be expressed as the number of cycles or pulses per unit of time (TIME/DIV Vernier control set to CAL). To use the oscilloscope for measuring the repetition rate or frequency of periodic signals, proceed as follows:



Figure 2-5. Elapsed Time Measurement

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1. Using the calibrated scale, measure the horizontal distance in divisions occupied by one cycle of the display under observation.

2. Multiply the horizontal dimension obtained in Step 1 by the TIME/DIV control setting.

3. Take the reciprocal of the product obtained in Step 2 (that is, divide it into one). The resulting quotient is the desired frequency or repetition rate in cycles per second. See Figure 2-6.

 $Cycles/second = \frac{1}{Time (seconds)}$

2-14. PHASE-SHIFT MEASUREMENTS

To measure the phase difference between two sine waves, proceed as follows:

1. Set up the Delaying Sweep Time Base for externally triggered normal sweep operation.

2. Apply one of the sine waves to Channel A Input and the other to Channel B Input of the Type 76-02A Amplifier.

3. Set MODE switch to ALT.

4. Adjust the TIME/DIV switch for a couple of cycles of the display on the screen.

5. Position the display so that one of the positive slopes crosses the horizontal center line at the left hand side of the scale.

6. Measure the horizontal distance occupied by one cycle of the waveform. Label this distance A.

7. Measure the horizontal shift of the Channel B display. Label this distance B.

8. Divide the distance measured in step 6 by the distance measured in step 7 and multiply the quotient by 360°. The resulting product is the phase difference between the two sine waves. See Figure 2-7.







Figure 2-7. Phase-Shift Measurements

2-15. PULSE WIDTH MEASUREMENTS USING THE CRT SCALE

Assume you have a Normal sweep display similar to Figure 2-8 and you wish to measure the width of the pulse appearing on the pedestal pulse. To make this measurement, proceed as follows:

1. Make sure the TIME/DIV Vernier control is set fully clockwise to CAL. (Click is heard.) 2. Set the DISPLAY LOGIC switch to TRIG-

GERED STROBE.

3. Pull out the DA TIME/DIV knob to disengage it and rotate it and the DELAY VERNIER control until the desired pulse is intensified (Figure 2-8a).

4. Set the DISPLAY LOGIC switch to TRIG-GERED DELAY and measure the horizontal distance in divisions from the 50% point on the rise of the pulse to the 50% point on the fall of the pulse. Multiply this distance by the DA TIME/DIV control setting (Figure 2-8b).



Pulse width =(DA TIME/DIV setting) (Hor Defl in Div)

Figure 2-8. Pulse Width Measurements

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2-16. PULSE WIDTH MEASUREMENTS USING THE DELAY VERNIER CONTROL

The following technique avoids human error (parallax interpolation of graticule lines) and should be used with more than routine accuracy if needed:

1. Make sure the TIME/DIV Vernier control is set fully clockwise to CAL (click is heard).

2. Set DISPLAY LOGIC switch to TRIGGERED STROBE and adjust the controls for several cycles of the signal.

3. Pull out the DA TIME/DIV knob and turn it to the right until the intensified area is a small bright dot.

4. To measure pulse width, turn the DELAY VERNIER control until the bright spot is at the 50% part of the leading edge of the desired pulse (Figure 2-9a). Record the dial reading.

5. Turn the DELAY VERNIER control to move the bright dot to the 50% point on the trailing edge of the same pulse (Figure 2-9b). Record the dial reading.

6. Subtract the reading of step 4 from that of step 5. Then multiply the difference by the setting of the NDT TIME/DIV switch. The product is the pulse width.

2-17. PULSE JITTER MEASUREMENTS

Pulse jitter may be defined as small incremental variations in pulse spacing in a pulse train. For example, assume a normal pulse train is displayed on the screen and it is desired to check a small pulse in the train for jitter; to check, proceed as follows:



Figure 2-10. Pulse Jitter Measurement

1. Set up the instrument for external triggering. 2. Set the DISPLAY LOGIC switch to TRIG-

GERED STROBE.

3. Pull out the DA TIME/DIV knob and turn it to the right until the intensified zone (strobe) of the display is about the same width as the pulse to be checked.

4. Adjust the DELAY VERNIER dial to move the strobed sector over the pulse.

5. Set the DISPLAY LOGIC switch to DELAYED TRIGGER and adjust the DELAY VERNIER control to position the strobed pulse to screen center.

6. The leading edge of the strobed pulse will then show jitter if present. The amount of jitter can be measured in time by multiplying the horizontal distance in divisions of the jitter area by the setting of the DA TIME/DIV knob. See Figure 2-10.



 $\alpha = 1 st DELAY VERNIER Reading$

 $\Delta t = b - a = 7.65 - 3.45 = 4.20$

Pulse Width = (Δ t) (NDT TIME/DIV setting) = (4.20) (2 mSEC) = 8.4 mSEC b = 2nd DELAY VERNIER Reading Given: Sweep Rate = 2 mSEC



SECTION 3 CIRCUIT DESCRIPTION

3-1. INTRODUCTION (Figures 3-1 to 3-12)

To simplify circuit description, functional block and waveform timing diagrams at various DISPLAY LOGIC switch settings are provided as follows:

Figure	3-1a.	NDT Trigger Circuit Functional Block Diagram
Figure	3-1b.	DA Trigger Circuit, Functional Block Diagram
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Figure	3-5.	Simplified Timing Diagram for Triggered Strobe Display
Figure	3-6.	Delayed Triggered Mode, Functional Block Diagram
Figure	3-7.	Simplified Timing Diagram for Delayed-Triggered Display
Figure	3-8.	Armed Strobe Mode, Functional Block Diagram
Figure	3-9.	Simplified Timing Diagram for De- laved-Armed Strobe Display
Figure	3-10.	Delayed-Armed Mode, Functional Block Diagram
Figure	3-11.	Simplified Timing Diagram for De- layed Armed Display
Figure	3-12.	Horizontal Deflection Amplifier, Functional Block Diagram

The timing diagrams show waveforms at critical points in the circuit and in proper relative time relationship. In addition, a capsule description of each waveform is provided.

The circuit description will be keyed to the aforementioned illustrations. Emphasis is placed on the interrelation of circuits rather than on detail of operation. It is also recommended that the schematics at the rear of the manual be referred to in following the circuit description.

3-2. TRIGGER CIRCUIT DESCRIPTION (Figures 3-1a and 3-1b)

a. Normal and Delaying Triggering

Since the input of the Normal and Delaying triggering circuit (NDT) is similar to that of Delayed Armed (DA) trigger circuit, only the NDT circuit will be discussed in detail. Refer to paragraph 3-8 for a description of the X Input circuit.

The input to the trigger amplifier V8201 and V8202, may be selected from one of three sources via the Trigger SOURCE switch as follows:

(1) In EXT or EXT/10 position, the signal is obtained from an external source through the EXT TRIG front-panel connector;

(2) in INT position, the signal is derived from the Y Plug-in unit; and

(3) in LINE position, the signal is tapped from one side of the 6.3 VAC heater circuit.

A choice of AC, ACF, or DC coupling is provided by the Trigger COUPLING switch. In the AC position, the trigger signal is applied to a high-pass filter consisting of C8203, C8205, and R8207, providing a low-frequency cutoff of 80 cycles. The low-frequency cutoff is raised to 10 Kc in the ACF position and the high-pass filter now has R8204 shunting R8207. In the DC position, the high-pass filters are disconnected and the triggering signal is applied directly to the trigger amplifier. The RC network, R8206 and C8202, in series with the grid of V8201 or V8202, serves to protect the input circuit from damage due to excessive input voltage. Shunt capacitor C8202 across R8206 preserves the high-frequency signal component.

The negative pulse at the output of the trigger amplifier occurs only when there is a positive-going signal at the input. However, it is desirable to start the sweep during either a positive-going or negativegoing portion of the excitation signal. To accomplish this, the Trigger SLOPE switch is used to select the desired polarity of the triggering signal.

For positive-going signals, connection is made to the grid of V8201, and for negative-going signals, connection is made to the grid of V8202. In each case, the opposite grid is connected to a dc bias source, adjustable by means of the Trig LEVEL control R8222. This control is used to select the level of the triggering point for all settings of the Trigger SLOPE switch.

The output from V8201 or V8202 is applied to a trigger shaper Q8202 which drives the trigger coupling transformer T8201. The resulting negative trigger is applied to series coupling diode CR8203 to the base of the delaying sweep gate multivibrator.

The TRIG SENS adjustment R8229, sets the tunnel diode trigger at its optimum sensitivity. The TRIG BAL adjustment R8234, sets the level of V8201 and V8202 through tunnel diode CR8201, so that no readjustment of the Trig LEVEL control is required when the Trigger SLOPE switch is set from plus to

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Figure 3-1a. NDT Trigger Circuit, Functional Block Diagram



Figure 3-1b. DA Trigger 8 X Input Circuits, Functional Block Diagram

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minus slopes or vice versa. This adjustment is made when the Trig LEVEL control is set to Zero.

b Automatic Triggering

When the Sweep Mode toggle switch is set to AUTO, the trigger circuit is ungrounded and becomes activated. Application of a trigger signal from 10 cps to 10 Mc switches the sweep immediately to the triggered mode. This technique insures stable synchronization of the desired input signal. The auto trigger multivibrator reverts to its natural mode in about 1 second after the discontinuance of the trigger excitation signal. Consequently, a horizontal reference trace will appear on the screen even in the absence of an input signal.

3-3. CIRCUIT DESCRIPTION OF NORMAL SWEEP (Figures 3-2 and 3-3)

a. Delaying Sweep Gate Multivibrator

The input triggering signal is applied to the base of transistor Q8206, through series-coupling diode CR8203. The dc coupled bistable multivibrator Q8206 and Q8207, initiates the formation of the sweep after receiving a negative trigger from the shaper circuit. Diode CR8203 and the lockout circuit hold off subsequent triggering signals until after the sweep and retrace are completed. In the quiescent state, Q8206 is conducting and Q8207 is at cutoff. Q8206 forms a positive gate while Q8207 forms a negative gate during the forward sweep interval.

CR8203 serves as a low capacitance coupling diode which couples the negative trigger from the shaper circuit to the sweep gate multivibrator which flips and initiates the sweep. CR8203 also serves as a high backimpedance diode to decouple the trigger shaper from the sweep gate multivibrator. After the bistable multivibrator has been triggered, the sweep runs up. When the saw reaches full screen deflection, turn-off diode CR8204 conducts and resets the multivibrator Q8206 and Q8207, which then clamps the saw. The SWP LENGTH potentiometer R8263 is adjusted for full screen sweep length display.

b. Saw Generation

The saw generator is of the Miller "run-up" type. The negative output developed at the collector of Q8207 is applied to the anodes of the disconnect diodes CR8205, CR8209, CR8211 and CR8216. The anode voltages of these diodes no longer conduct. This action unlocks the integrator clamp and permits the selected sweep capacitor to charge linearly through the associated resistance network.

The grid of the Miller integrator moves negatively when the clamp is unlocked. The plate voltage of V8203 rises positively carrying the saw cathodefollower (V8204) grid, cathode and timing capacitor in the same direction. A flow of current is required into the charging capacitor if the voltage across this capacitor is to change. The charging current must flow through the charging resistor. The time required to change the voltage across the charging capacitor determines the sweep time.

The positive voltage swing on the opposite side of the timing capacitor tends to prevent the grid side from swinging negatively. It also increases the voltage to which the timing capacitor is trying to charge. The net result is to *straighten out* the charging curve (sweep voltage) by maintaining a constant current flow in the capacitor.

Since the grid of V8203 remains at a constant potential within a small fraction of a volt, the current through the charging resistor remains constant and the sweep timing capacitor thus charges at a constant rate. The resulting linear sawtooth waveform is applied to the horizontal deflection system.

c. Sweep Length

The sweep length, or the total duration of the sweep for any given sweep rate is determined by the setting of the Sweep LENGTH adjustment R8263. A portion of the positive sawtooth voltage is fed back to the turn-off emitter follower Q8208, and the saw turn-off diode CR8204.

If the Sweep LENGTH potentiometer is properly set, diode CR8204 will conduct when the positivegoing excursion of the sawtooth has travelled 10.5 to 11 divisions on the screen. This positive peak signal will then be conducted through diode CR8204 to the base of Q8206. Upon receiving this positive pulse, the sweep gate multivibrator will revert rapidly to its original state with Q8206 conducting, and Q8207 at cutoff. The positive step from the collector of Q8206 returns the disconnect diodes CR8216, CR8209, CR8211 and CR8205 to their conducting state, thus discharging the timing capacitors. The Miller circuit now returns to its quiescent level and is ready for the next sweep cycle after the lockout time interval is completed.

d. Lockout Circuit

The lockout circuit prevents the sweep gate multivibrator from being triggered until the sweep retrace interval has reverted the saw to its quiescent base level. The sweep does not retrace in zero time since the clamping of the Miller integrator timing capacitor is accomplished by a diode switch circuit having a small impedance. The timing circuit discharge (saw retrace) takes longer than the flipping of the sweep gate multivibrator. Consequently, the trigger excitation pulses must be held off to prevent the formation of a new saw during the retrace interval. The sawtooth waveform must be permitted to retrace completely to its quiescent base which re-establishes the

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Figure 3-2. Normal Sweep Mode, Functional Block Diagram

beam at the left-hand side of the CRT screen. This is accomplished by holding the cathode of the seriestriggering diode CR8203 at a suitable positive voltage for a given period after the completion of the sweep.

During the forward sweep interval, a portion of the positive sweep voltage is fed back to the base of the turn-off emitter follower Q8208, which charges the lockout capacitor through coupling diode CR8206. When the saw reaches its predetermined full screen length, the sweep gate multivibrator flips and clamps the Miller integrator which then causes the sweep to retrace. During the return-trace interval, diode CR8206 is cut off and the lockout capacitor is discharged through R8261. The sweep gate multivibrator will not retrigger until the preselected lockout timing capacitor is chosen to give lockout beyond the time that the sweep has returned to rest at its initial starting point.

The duration of the lockout interval is determined by the sweep-charging time constant and the Miller integrator clantp. Consequently, the TIME/DIV switch must also change the lockout circuit hold-off timing capacity. This technique prevents additional triggers from initiating the sweep gate multivibrator until the sweep retrace interval is completed and the saw reverts to its quiescent state at the left-hand side of the screen.

The trigger coupling diode CR8203 prevents triggers from disturbing the sweep gate multivibrator during all of the sweep-forward interval. The lockout circuitry prevents retriggering during the retrace interval.

e. Unblanking

The cathode-ray tube employed in this oscilloscope has two additional beam deflecting plates which cut off the electron beam independently of the control grid. Beam control pulses (trace brightening and retrace blanking pulses) can easily be dc coupled since these beam deflection plates are electrically close to ground. In conventional circuits these pulses must be coupled to the control grid which is operated at high potential. The extra beam deflection plates are controlled by the sweep gate multivibrator Q8206 and Q8207.

The positive pulse developed at the collector of Q8206 of the delaying sweep gate multivibrator is applied to the base of the unblanking cascode amplifier Q8405 and Q8403. This gate signal is coincident with the sweep forward time and is also available at a front-panel connector labeled + GATE. The resulting negative pulse developed at the collector of

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Figure 3-3. Timing Diagram for Normal Sweep Display

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Figure 3-4. Triggered Strobe Mode, Functional Block Diagram

Q8403 is applied to the beam deflection plate of the cathode-ray tube through emitter follower Q8402. Therefore the display is visible only during the forward sweep interval and is blanked during the retrace and lockout interval.

Transistor Q8401, serves as an emitter follower voltage source for the collector of Q8402, and it also prevents the collector voltage of Q8403 from exceeding 125 volts.

A portion of the negative pulse from the unblanking emitter follower Q8402 is applied to a differentiating network C8441 and R8443. The output from this network provides the proper trigger to the blanking multivibrator of the Dual Trace Plug-in.

These Delaying Sweep Time Base Plug-in units may be used in the X or Y cavity of the Main Frame. Only the X cavity permits retrace beam blanking signals to be coupled to the cathode-ray tube. Therefore, sweep operation in the vertical direction will show the sweep retrace.

3-4. CIRCUIT DESCRIPTION OF TRIGGERED-STROBE MODE

(Figures 3-4 and 3-5)

When the DISPLAY LOGIC switch is set to Triggered STROBE, the delay pick-off, the delayed sweep, and strobe circuits are activated.

In the "triggered" mode, the delaying sweep receives the external trigger signal while the delayed sweep receives its trigger signal later from the delaying sweep. The triggering signal for the delayed sweep in this mode is derived from the delaying sweep at the exact instant this sweep reaches a level determined by the adjustment of the delay pick-off circuit. This mode from now on will be referred to as the delayedtriggered mode.

The Normal and Delaying Sweep circuit functions as previously described. Major differences between the triggered strobe and the Normal mode circuits may be seen by comparison of the block diagram.

Referring to Figure 3-4, the saw from the Delaying Sweep circuit is applied to the horizontal deflection amplifier and to the input of the delay pick-off comparator circuit Q8601 and Q8602.

This circuit is a differential amplifier which compares the voltage level of the input delaying sweep against a fixed voltage obtained from the DELAY VERNIER control. When the voltage level of the delaying sawtooth waveform reaches a certain level, as determined by the setting of the DELAY VERNIER control, the output of the comparator circuit is applied to a delayed trigger amplifier Q8604, which drives coupling transformer T8601. The negative pulse from the secondary of this transformer is through series-coupling diode CR8105, to trigger the delayed sweep gate multivibrator Q8106 and Q8107.

The positive gate developed at the collector of Q8106 is coincident with the *delayed* TIME/DIV

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control setting and is applied to the strobe circuit Q8001 and Q8002. The positive strobe signal is applied to one of the beam-gating electrodes of the CRT. The delaying sweep unblanking gate is applied to the other beam-gating electrode.

The cathode-ray beam is kept turned off when a sweep is not moving the beam across the screen. When a sweep is in progress, the beam is turned on by an unblanking signal that lasts as long as the sweep and then turns the beam back off after the sweep is completed. When both the delaying and delayed sweeps are running, each produces its own unblanking signal. The delayed sweep unblanking pulse (strobe) makes a brighter trace than the delaying sweep pulse.

The difference in brightness for the two pulses is useful for finding out where to set the delay controls to display the part of the signal you wish to examine. Detailed instruction on setting up the strobe is found in Section 2, Operation.

The delaying sweep is automatically turned off when the delayed sweep has terminated. This action is developed as follows: the positive gate produced at the collector of the delayed sweep multivibrator Q8106, is applied to a differentiating network consisting of R8247 and C8216. Series-coupling diode CR8202, is biased to permit only the trailing edge of the delayed sweep gate to trigger the delaying sweep multivibrator and subsequently terminating the NDT sweep. This prevents brightening of the sweep retrace in the STROBE position.

3-5. CIRCUIT DESCRIPTION OF DELAYED-TRIGGERED MODE

(Figures 3-6 and 3-7)

When the DISPLAY LOGIC switch is set to Triggered DELAYED, the delayed sweep and not the delaying sweep is applied to the horizontal deflection amplifier. The brightened sector of the display in the STROBE position will now be expanded to full screen in the DELAYED position.

The delayed-triggered sweep circuit is similar in operation to the triggered-strobe mode described earlier, except that the strobe circuit is now activated.

Automatic provision is made for shut-off of the delaying sweep when the delayed sweep terminates. This technique permits maximum duty cycle performance in the Delayed Mode.

3-6. CIRCUIT DESCRIPTION OF ARMED-STROBE MODE

(Figures 3-8 and 3-9)

When the DISPLAY LOGIC switch is set to Armed STROBE, the delay pick-off circuit, the arming multivibrator, the delayed sweep, and strobe circuits are activated.

In the "armed" mode, the delayed sweep is triggered by a selected external triggering signal. All triggering signals are blocked by the armed lockout diode until a signal from the delay pick-off circuit triggers the arming multivibrator. This action unlocks the diode and opens the trigger circuit to the delayed sweep, making it possible for the next appropriate triggering signal to initiate the delayed sweep. In this mode of operation, the delayed sweep does not start precisely at the delay time indicated by the DELAY VERNIER and NDT TIME/DIV control settings, but instead is initiated by the next suitable triggering following the indicated delay interval. This mode from now on will be referred to as the Delayed-Armed mode of sweep operation.

The armed lockout diode CR8102, is now forwardbiased by the voltage applied to it from the collector of Q8103, thus opening the triggering circuit to the delayed sweep gate generator Q8106 and Q8107.

The SWP READY lamp on the front panel goes on when the delay time has elapsed and indicates that the delayed sweep circuit is ready to be triggered. When the delayed sweep is triggered, the SWP READY lamp then goes out. If the delayed-armed sweep is triggered immediately at the completion of the delay time, the SWP READY lamp may not appear to go on.

The next suitable trigger from the DA trigger is applied to the delayed sweep multivibrator which immediately changes states (it flips). Q8106 forms a positive gate while Q8107 forms a negative gate during the "delayed" sweep forward interval.

In the quiescent state of the armed multivibrator, Q8103 is at cutoff and Q8104 is conducting. The armed lockout diode CR8102 is back-biased by the voltage applied to it from the collector of Q8103. This action locks out incoming triggering signals to the delayed sweep gate multivibrator, thereby inactivating the delayed sweep.

The arming signal from the delayed pick-off circuit is coupled from transformer T8601, through diode CR8104, to the base of transistor Q8104. The bistable armed multivibrator changes states: Q8104 is **at** cutoff and Q8103 is conducting.

The leading edge of the negative gate at the collector of Q8107 is differentiated by C8118 and R8143 and applied to the base of transistor Q8103 through diode CR8103. This disarming trigger reverts the armed multivibrator to its initial condition.

After the bistable delayed sweep gate multivibrator has been triggered, it will revert to its original state as determined by the setting of the SWP LENGTH adjustment R8159. The delayed sweep will remain inactivated until the armed multivibrator is rearmed by a signal from the delayed pick-off circuit.

The development of the strobe and unblanking pulses are identical to that described for the triggereddelayed mode. Automatic provision is made for turning off the NDT sweep when the DA sweep has terminated. This prevents brightening of the sweep retrace in the strobe position.

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Figure 3-7. Simplified Timing Diagram for Delayed-Triggered Display

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Figure 3-8. Armed Strobe Mode, Functional Block Diagram

3-7. CIRCUIT DESCRIPTION OF DELAYED-ARMED MODE

(Figures 3-10 and 3-11)

When the DISPLAY LOGIC switch is set to Armed DELAYED, the delayed sweep is applied to horizontal deflection plates.

The delayed-armed sweep circuit is similar in operation to the armed-strobe mode described earlier, except that the strobe circuit is now inactivated.

3-8. HORIZONTAL DEFLECTION CIRCUIT DESCRIPTION (Figure 3-12)

When the DISPLAY LOGIC switch is set to X AMP, the EXT TRIG input connector of the Delayed Sweep becomes the X Amplifier input. Simultaneously, the Delayed Sweep LEVEL control becomes the variable X AMPlifier ATTENuator control. The PULL EXT/10 setting provides 10:1 attenuation of the X Input signal. Thus external signals may be applied to the X AMP front-panel BNC connector. These signals are coupled to the X Input amplifier V8101 and V8102. The output of this amplifier is coupled to the horizontal deflection circuit via the X AMP setting of the DISPLAY LOGIC switch. See Figure 3-1b.

The output from V8102 is applied through a voltage divider network to the base of emitter follower Q8301 via the DISPLAY LOGIC switch.

The POSITION control supplies a manually-adjustable dc voltage to the base of Q8301 for positioning the display on the screen. For the Type 765 Series, a PATTERN POSITIONING control is mounted on the front panel of the Main Frame, and it is electrically coupled to the POSITION control of both the X and Y Plug-ins. This feature permits positioning the entire display in the horizontal and vertical directions on the screen via use of the single joystick control.

The output from the emitter of Q8301 is applied directly to the common emitter amplifier Q8302 and Q8303, which converts the single-end input to a pushpull output. The signal progresses through emitter follower Q8305 and Q8306, and is then applied to the output amplifier Q8307 to Q8311. In this output amplifier stage, the signal develops the necessary power for driving the horizontal deflection plates.

Ten-times magnification of the sweep is accomplished by reducing the common emitter amplifier feedback of Q8302 and Q8303, by a factor of 10 when the X10 control is pulled out. Consequently, the sweep rate observed on the screen of the cathode-ray tube is effectively magnified ten times. The X10 REGISTRA-TION potentiometer R8311 is provided to adjust the voltage level at the base of Q8303 so that the center of the trace is not depositioned from CRT screen center when the PULL X10 switch is activated.

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Figure 3-9. Simplified Timing Diagram for Delayed-Armed Strobe Display

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Figure 3-10. Delayed-Armed Mode, Functional Block Diagram



Figure 3-12. Horizontal Deflection Amplifier, Functional Block Diagram

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Figure 3-11. Simplified Timing Diagram for Delayed-Armed Display

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SECTION 4 PERFORMANCE ASSURANCE TEST

4-1. MAINTENANCE CHECK TO ASSURE PERFORMANCE

The tests described in the paragraphs to follow should be performed by Instrument Test Departments and Maintenance Laboratories to certify proper performance. These tests are divided into sections for simplification and to assist those test groups where complete checking is not mandatory, or where all test equipment is not available. Refer to Section 5, paragraph 5-5, for list of test equipment required.

All tests are performed with a representative Type 765 Series Main Frame Oscilloscopes and a Y Amplifier Plug-in. Both of the plug-in units must be normalized to the Main Frame before starting tests. This is accomplished by adjusting the front-panel screwdriver SWP CAL and GAIN CAL controls as described in the appropriate Plug-in Instruction Manuals. Allow 30 to 60 minutes of warm-up time before making any adjustments.

NOTE

If this Plug-in module is checked by a Receiving Inspection laboratory, the tests outlined below are recommended to certify performance. This instrument has been thoroughly tested and aged at the factory. Nevertheless, rough shipment, extreme environments, or long idle periods may necessitate minor adjustments of the controls. Hence, it is suggested that the certifying engineer try the recommended adjustments not only for recentering the controls, but also to ascertain their range and to familiarize himself with this precision instrument. If, after performing all the tests outlined in the paragraphs to follow, the instrument will not perform to specification, the assistance of the local Fairchild Field Engineering representative should be requested.

4-2. CHECKING SWEEP CALIBRATION

1. Connect a Time-Mark Generator to the Input connector of the Y Plug-in through a properly terminated cable.

2. Set up the instrument for NORMal sweep. Sweep accuracy is checked by counting the positive peaks in the centered 8-division portion of the CRT scale. Make sure the UNCAL lamp is off and refer to the following Sweep Check Calibration Chart for additional data. All measurements indicated in this chart should fall within ± 0.25 division of the 9-division marking. 3. Repeat checks for the DELAYED TRIGGER position.

4-3. CHECKING TRIGGER SOURCE AND POLARITY

1. Preset front-panel controls as indicated:

Control	Setting	
TRIG LEVEL	Zero	
DISPLAY LOGIC	NORM	
Trigger SOURCE	LINE	
Trigger COUPLING	AC	
Trigger SLOPE	+	
TIME/DIV (both knobs)	10 mSEC	
TIME/DIV Vernier	CAL (fully ccw)	
VOLTS/DIV (Y Plug-in)	CAL	
PULL X10	Pushed in (X1)	
POSITION	Centered	

2. Six cycles of the calibrator pattern should be observed on the screen for 60-cycle line, 5 cycles for 50-cycle line.

3. Set the NDT Trigger SOURCE switch to INT; the pattern remains stationary on the screen.

4. Set the NDT Trigger SOURCE switch to EXT; the display should disappear.

5. Apply a line frequency sine wave signal of 0.5V peak-to-peak to the NDT EXT TRIG connector. The amplitude of this signal should be sufficient to trigger the sweep and the pattern should again remain stationary on the screen. The 0.5 volt test signal is suitably attenuated by the 80-cycle cutoff frequency of the AC coupling and represents a true measure of trigger sensitivity.

6. Changing the NDT Trigger SLOPE switch from plus to minus should change the leading edge of the first cycle from positive-going to negative-going.

7. Reset the NDT Trigger SOURCE and SLOPE switches to INT and plus respectively.

8. Set DISPLAY LOGIC switch to DELAYED ARMED and adjust DELAY VERNIER control until the calibrator pattern appears on the screen.

9. Set the DA Trigger SOURCE switch to INT; the delayed-armed display should remain stationary on the screen.

10. Set the DA Trigger SOURCE switch to EXT; the delayed-armed display should disappear.

11. Repeat steps 5, 6, and 7 except that the DA EXT TRIG connector, the DA Trigger SOURCE and SLOPE switches are used.

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TIM	E-MAR set	to GEN	TIM	E/DIV et to		NUMBER OF POSITIVE PULSES*				
50	Mc s	ine wave	0,1	μSEC	(6*	**)				
10	Mc s	ine wave	0.1	<i>uSEC</i>	9	cycles	(2**)			
5	Mc si	ne wave	0.2	μSEC	9	cycles				
1	μsec	marker	0.5	μSEC	5	timing	markers			
1	µsec	marker	1	μSEC	9	timing	markers			
1	μsec	marker	2	μSEC	17	timing	markers			
5	μsec	marker	5	μSEC	9	timing	markers			
10	μsec	marker	10	<i>µ</i> SEC	9	timing	markers			
10	μsec	marker	20	μSEC	17	timing	markers			
50	μsec	marker	50	μSEC	9	timing	markers			
100	μsec	marker	0.1	mSEC	9	timing	markers			
100	μsec	marker	0.2	mSEC	17	timing	markers			
500	$\mu { m sec}$	marker	0.5	mSEC	9	timing	markers	(2**		
1	msec	marker	1	mSEC	9	timing	markers			
1	msec	marker	2	mSEC	17	timing	markers			
5	msec	marker	5	mSEC	9	timing	markers			
10	msec	marker	10	mSEC	9	timing	markers			
10	msec	marker	20	mSEC	17	timing	markers			
50	msec	marker	50	mSEC	9	timing	markers			
100	msec	marker	0.1	SEC	9	timing	markers			
100	msec	marker	0.2	SEC	17	timing	markers			
500	msec	marker	0.5	SEC	9	timing	markers			
1	sec m	narker	1	SEC	9	timing	markers			
٦	sec m	arker	2	SEC	17	timing	markers			

SWEEP CHECK CALIBRATION CHART

* Centered 8-division portion of scale.

** Expander check (Pull X10 switch out). Number of positive pulses between 10 div, +0.5° div are indicated by numbers in parenthesis. Neglect the first 50 nanoséconds of the sweep.

4-4. CHECKING NORMAL, TRIGGERED & ARMED SWEEP DISPLAYS

Refer to the following illustrations in Section 2, Operation, to check the sweep modes available at the different settings of the DISPLAY LOGIC switch.

Figure 2-2.	Type 74-13A Normal Display
Figure 2-3a.	Type 74-13A Triggered Strobe Display
Figure 2-3b.	Type 74-13A Delayed Triggered Display
Figure 2-4a.	Type 74-13A Armed Strobe Display
Figure 2-4b.	Type 74-13A Armed Delayed Display

Unless otherwise designated, it is presumed that a Y Amplifier Plug-in module is inserted in the Y cavity (left-hand side) and the Type 74-13A Calibrated Delaying Sweep Plug-in unit is inserted in the X cavity (right-hand side) of the Main Frame.

4-5. DELAY CALIBRATION CHECK

1. Allow the unit to warm up at least 10 minutes at an ambient temperature of $25^{\circ}C \pm 5^{\circ}C$ (77°F $\pm 9^{\circ}F$).

2. Apply a 100 μ sec marker from a Time-Mark Generator to the Input connector of the Y Plug-in unit through a properly terminated cable.

3. Set NDT TIME/DIV switch to 0.1 mSEC and DA TIME/DIV switch to 5 μ SEC.

4. Set the DISPLAY LOGIC switch to Triggered DELAYED.

5. Measure the incremental accuracy of the delay calibration from 0.8 div to 9.8 div in steps of 1 div (i.e., 1.8 div, 2.8 div, etc.). One complete revolution of the DELAY VERNIER dial, say from 3.8 div to 4.8 div, should bring the succeeding pulse back to the position occupied by the preceding pulse within ± 1 div.

Note: Be sure that the Positioning and Trigger Leveling settings are not disturbed during this check.

6. Center the pulse when the dial is set to 9.8 div. Turning the DELAY VERNIER dial back to 0.8 div should bring the pulse back on screen within ± 2 div from the center line.

4-6. NDT GATE OUT CHECK

1. Set DISPLAY LOGIC switch to NORM.

2. Apply the NDT + GATE signal to the input connector on the Y Plug-in module. The display should be a positive-going step with an amplitude of approximately 2.5 volts.

4-7. NDT SAW OUT CHECK

1. With the DISPLAY LOGIC switch set to NORM, apply the SAW signal to the input connector on the Y Plug-in module.

2. The display should be a positive saw waveform with an amplitude of approximately 25 volts.

4-8. DUAL TRACE SWITCH TRIGGERING CHECK

This check is to determine whether the Type 74-13A Delaying Sweep Module triggers the Type 76-02A Dual Trace Module when the latter unit is set up for alternate display.

Set up the Delaying Sweep unit as follows:

Control	Setting				
TIME/DIV	10 μSEC				
DISPLAY LOGIC	DELAYED TRIGGERED				
Trigger SOURCE	INT				
Trigger COUPLING	ACF				

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Set Type 76-02A MODE switch to ALT and observe alternate displays of the Fairchild Type 791A waveforms into both Type 76-02A inputs at a frequency range of 10 to 30 Kc in each vertical channel.

Adjust the amplitude of the Y signal for 2 to 21/2 divisions peak-to-peak vertical deflection. Two similar signals should be displayed on the screen. Check that both displays may be positioned independently with their respective Y POSITION controls.

4-9. BEAM POSITIONING INDICATOR CHECK

Set up the front panel controls as indicated in step 1 of paragraph 4-3 to obtain a calibrated pattern on screen. Reduce the intensity of the beam. Vary the POSITION control. Check that the right beam position indicator is lit when the display is positioned off screen to the right; and conversely, the left indicator is lit when the display is positioned off screen to the left. Both beam position indicators should be off when beam is positioned on screen.

4-10. AUTO TRIGGERING AND HF SYNC CHECK

1. Set the DISPLAY LOGIC switch to NORM and the Sweep Mode toggle switch to NORM.

2. Apply a 10 cps signal (sinusoidal or any other waveform) to the input connector of the Y Plug-in and check that the oscilloscope triggers properly in the NORM and AUTO modes.

3. Check whether the unit free runs after the removal of the triggering signal from 10 cps to 10 Mc. Free running should stop immediately after the reapplication of the triggering signal.

4. Set the Sweep Mode toggle switch to HF RECUR.

5. Apply a 50-megacycle signal to the input connector of the Y Plug-in and set display for 1 division of vertical deflection.

6. Using internal triggering, adjust the NDT TRIG LEVEL control for a stable display on screen.

NOTES

SECTION 5 MAINTENANCE AND RECALIBRATION

5-1. INTRODUCTION

This section of the manual contains service information and procedures for internal adjustments.

5-2. REMOVAL AND REPLACEMENT OF PARTS

If it is necessary to order a replacement component from the factory, always give the Type Number and Serial Number of the instrument. Before ordering parts for in-warranty replacement or purchasing them for out-of-warranty replacement, be sure to consult the Parts List in this manual. The Parts List gives the values, tolerances, ratings, and the factory part number for all electrical components used in the instrument. This will help to expedite service.

Since your instrument left the factory, some of the parts may have been superseded by improved components. In such cases, the part numbers of these new components will not be listed in your Parts List. However, if you order a part from the factory, and it has been superseded by an improved component, the new part will be shipped in place of the part ordered.

It is the aim of the Fairchild organization to make available the most reliable commercial oscilloscopes within the state of the art and to provide services which will help the user to rapidly restore any of our equipment to its specified performance. Your local Field representative maintains a limited number of spare parts. Also the factory may be asked to air-ship replacement parts on a rush basis.

NOTE

Be sure and replace the beryllium oxide insulating washers (they serve as heat sinks) on the transistors that require them. Always grease these heat sinks with Dow Corning silicon grease for optimum heat transfer.

5-3. SERVICING HINTS

General maintenance and trouble-shooting information is given in the Type 765 Series Oscilloscope Instruction Manual. In the following discussion, it is assumed that you have already read that information and have definitely isolated a trouble in the Time Base Plug-in unit.

In trouble shooting a Plug-in unit, it becomes necessary to determine if the defect is in the plug-in or in the Main Frame of the oscilloscope. The quickest and easiest way of isolating the trouble is to substitute another plug-in unit and determine if the same trouble persists. If the trouble continues after substitution, it can be safely assumed that the defect is in the Main Frame.

There is no simple way of locating troubles. An understanding of the functions of the circuits is the best help. With an understanding of the circuit operation, it will be possible to make a good guess at the general source of troubles from the symptoms. As an aid in trouble-shooting this unit, refer to the functional block and timing diagrams in this Section and to the schematics.

To keep electronic units operating at top performance, it is desirable to check the equipment at regular intervals. The period between checks will depend on the installation and the conditions of operation. For these regular checks, clean all dust and dirt from the unit using a light air blast or soft brush. However, to insure the reliability of measurements, we suggest that you recalibrate the plug-in after each 500 hours of operation or every six months if used intermittently. Also, the calibration of a unit should always be fully checked and adjusted after the repair or replacement of any component in the unit. The complete adjustment procedure for this unit is given in this Section of the Instruction Manual.

In the event of improper performance of the Plugin unit, the following suggestions are recommended:

1. The Type 4294 Extension Cable for remote operation of the plug-in from the oscilloscope is available as an accessory. This plug-in extender will be helpful for routine maintenance and recalibration. Do not use this extension for HF alignments; instead remove the Main Frame side cover.

2. Localizing the trouble is made easier by use of a test oscilloscope to check waveforms. These waveforms are shown at key points on the over-all schematics. Both the waveform amplitude and time duration are given. Use a high-impedance 10:1 Passive Attenuator Probe while trouble shooting (Fairchild Type 4290 Series). A Fairchild Type 765 Series Oscilloscope with a Y Plug-in having a bandwidth from dc to 25 Mc is recommended.

3. Maintain a high quality of workmanship. Use a clean bench and soldering iron; keep solder joints smooth and bright; do not overheat any component while soldering. Use heat sinks when soldering semiconductors. The use of a 30-watt iron such as a Hexacon Type 26S is recommended.

4. When using accessory probes or adapters, be sure the trouble is not originating in the accessory before suspecting the instrument itself.

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5. Once the defective stage has been localized, the component or components causing the trouble can be located by tube and component substitution or by voltage measurement. Key voltage measurements are shown on the over-all schematics at the rear of this manual.

6. The identification of electron tubes, semiconductors and service adjustments are shown on photographs in this Section of the Instruction Manual.

5-4. GAINING ACCESS TO CHASSIS

Since the Plug-in is not contained in its own dust cover, most of the components are readily accessible when the plug-in is removed from the Main Frame. To gain access to the chassis, simply unscrew the knurled thumbscrew at center bottom of unit and pull it free of the Main Frame.

WARNING

WHEN THE PANELS OR PLUG-INS ARE RE-MOVED FROM THE INSTRUMENT FOR SERVICING, EXERCISE CAUTION WHILE THE POWER IS ON. The lower-voltage busses are potentially more dangerous than the cathoderay tube potential because of the high current capabilities and large filter capacitors employed in these supplies. When you reach into the instrument with one hand while it is turned on, do not grasp the metal frame with the other hand. If possible, stand on an insulated floor and use insulated tools. It is advisable to ground the third lead in the power cord whenever the instrument is in use.

5-5. TEST EQUIPMENT REQUIRED FOR SERVICE ADJUSTMENTS

a. Introduction

The adjustments outlined in the following paragraphs are based on the test procedure followed at the factory. All adjustments should be made at mid-line voltage, $115V/230V \pm 2\%$.

To set up the Time Base Unit for calibration, insert an amplifier plug-in and the Time Base plug-in into the Main Frame. The amplifier plug-in module and the Main Frame must be fully tested and certified units.

CAUTION

Always use insulated tools while working or making adjustments on the unit when power is on. The transistors in this instrument may be damaged if overvoltaged by accidental grounding of one or more elements. Exercise caution and turn off power when making repairs. b. Test Equipment Required (Equivalent may be substituted)

Equipment	Description					
Oscilloscope	Fully tested and certified Type 765 Series Main Frame					
Y Plug-In	Type 76-02A with delay line installed					
X Plug-In	Type 74-03A					
Volt-ohmmeter	Simpson Model 260; 20K ohms/volt sensitivity					
Square Wave Generator	Fairchild Type 791A					
Time-Mark Generator	Fairchild Type 781A					
Vacuum Tube Voltmeter	Hewlett-Packard Model 410B					
Differential Voltmeter	John Fluke Model 801					
Туре 4290	10:1 Passive Attenuator Probe					
Alignment Tools	Fairchild Type 7013 Tool Kit					

Preset front-panel controls on the Type 74-13A as indicated:

Control	Setting				
TRIG LEVEL	ZERO				
DISPLAY LOGIC	NORM				
Trigger SOURCE	EXT				
Trigger COUPLING	DC				
Trigger SLOPE	+				
TIME/DIV (NDT & DA)	10 mSEC				
TIME/DIV Vernier	CAL (fully cw)				
VOLTS/DIV (Y Plug-in)	OFF	1			
PULL X10	Pushed in (X1)				
POSITION NORM-AUTO-HF RECUR	Centered NORM				

5-6. NDT & DA TRIG SENS ADJUSTMENT (R8229 & R8118)

1. Preset front-panel controls as indicated:

Control	Setting					
DISPLAY LOGIC	NORM					
NDT Trigger SOURCE	EXT					

2. While gently rocking the NDT LEVEL control back and forth, turn the NDT TRIG SENS potentiometer R8229, gradually clockwise until a trace just appears on the screen. This indicates that tunnel diode CR8201 is now free-running.

3. Back off on the NDT TRIG SENS potentiometer R8229 until the trace just disappears. Turn the NDT LEVEL control back and forth and note that the trace flashes momentarily on the screen but disappears when the NDT LEVEL control is not turned.

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4. Preset front-panel controls as indicated:

Control	Setting					
DISPLAY LOGIC	DELAYED ARMED					
NDT Trigger SOURCE	LINE					
DA Trigger SOURCE	LINE					

5. Adjust the DA LEVEL control for a trace on the screen.

6. Set DA Trigger SOURCE switch to EXT; the trace should disappear.

7. While gently rocking the DA LEVEL control, turn the DA TRIG SENS potentiometer R8118 gradually clockwise until a trace just appears on the screen. This action indicates that tunnel diode CR8101 is now free-running.

8. Back off on the DA TRIG SENS potentiometer R8118 until the trace just disappears. Rock the DA LEVEL control and note that the trace appears momentarily on the screen but disappears when the DA LEVEL control is not turned.

5-7. TRIG BAL ADJUST (R8100, R8234)

1. Set DISPLAY LOGIC switch to NORM.

2. Apply a 1 Mc signal to Type 76-02A and set up instrument for 1 division of deflection.

3. Adjust NDT TRIG BAL potentiometer R8234 such that the trace remains on the screen while switch \cdot ing the Trigger SLOPE switch back and forth from (+) to (-).

4. Set DISPLAY LOGIC switch to DELAYED ARMED. Repeat steps 2 and 3 adjusting the DA TRIG LEVEL potentiometer R8100.

5-8. X AMPLIFIER OUTPUT LEVEL ADJUSTMENT (R8339) Sec. Adden date

1. Set the DISPLAY LOGIC switch to NORM.

2. Set Trigger SOURCE switch to EXT and make sure NDT sweep is not running.

3. Connect a Simpson Voltmeter across the output leads to the deflection plates P8001, pin 17 to pin 1.

4. Turn the Positioning control until the voltage reals zero or less than $\frac{1}{4}$ volt on the 2.5V scale.

5. Connect the Voltmeter from P8001, pin 1 (or pin 17) to ground. Set to 250V scale.

6. Adjust R8339 X AMP LEVEL potentiometer to 89 volts, $\pm 1V$. (Make sure that the measurement does not introduce any oscillation in the X Amplifier.)

7. Carefully disconnect meters.

5-9. NDT SWEEP LENGTH ADJUSTMENT (R8263)

1. Preset front-panel controls as indicated:

Control	Setting				
DISPLAY LOGIC	NORM				
Trigger SOURCE	LINE				
Trigger SLOPE	+				
VOLTS/DIV (Y Plug-in)	CAL				

2. Adjust the NDT SWEEP LENGTH potentiometer R8263 until the display occupies 10.5 to 10.7 divisions.

5-10. SLOW SWEEP CAL ADJUST (Front Panel)

1. Preset front-panel controls as indicated in paragraph 5-9, and obtain a display.

2. Adjust SWP CAL front-panel screwdriver control until 6 cycles of the calibrator signal appears precisely in 10 divisions (60-cycle line), 5 cycles for 50-cycle line.

Note: Make certain that the UNCAL lamp is off during these adjustments.

5-11. DA SWEEP LENGTH ADJUSTMENT (R8159)

1. Preset front-panel controls as indicated in paragraph 5-9, to obtain a NORMal sweep display.

2. Set DISPLAY LOGIC switch to DELAYED TRIGGERED.

3. Adjust DA SWEEP LENGTH potentiometer R8159 until the display occupies 10.5 to 10.7 divisions of deflection.

5-12. SWEEP RATE BAL ADJUSTMENT (R8175)

The SWEEP RATE BAL potentiometer is adjusted to normalize the tracking between the NDT and DA Sweep rates. Once both time bases are normalized, the SWP CAL panel control will calibrate both time bases simultaneously. The SWEEP RATE BAL potentiometer normally requires readjustment only when the timing components and V8103 or V8203 are replaced. To adjust, proceed as follows:

1. Preset front-panel controls as indicated:

Setting					
NORM					
LINE					
+					
10 mSEC					
CAL					

The calibrator signal should be displayed on the screen.

2. Set DISPLAY LOGIC switch to DELAYED TRIGGERED.

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3. Switch back and forth between the DELAYED TRIGGERED and NORMAL displays and adjust the SWEEP RATE BAL potentiometer R8175 until both sweep rates are identical.

4. Readjust the SWP CAL front-panel screwdriver control to again have 6 cycles of the calibrator signal to displace exactly 10 divisions (60-cycle line).

5. Recheck the Normal and the Delayed Triggered mode to make sure that the SWEEP RATE BAL potentiometer has equalized both time bases. The calibrator signal must occupy equal display divisions for both time bases on the screen. Error between time bases must be less than 0.1 major division of sweep for compliance of sweep calibration specifications.

5-13. X10 REGISTRATION (R8311)

1. Position the pattern so that the leading edge of one of the calibrator signals is coincident with the vertical center line of the scale.

2. Pull out the X10 knob (concentric with the DISPLAY LOGIC knob).

3. Adjust the X10 REGISTRATION potentiometer R8311 until the leading edge of the same pulse (see step 1) is again coincident with the vertical center line of the scale (within $\pm \frac{1}{2}$ division).

4. Push in the X10 knob.

5-14. X AMPLIFIER HIGH-FREQUENCY ADJUSTMENTS (C8119, C8309, C8317 & C8101)

1. Replace the Plug-in Amplifier in the Y cavity with a tested Time Base plug-in unit. This unit is then set up to obtain a vertical sweep.

Note: Unless otherwise noted, the test procedure for the balance of this setup pertains to the Time Base unit inserted in the X cavity.

2. Set DISPLAY LOGIC switch to X AMP and the DA SOURCE to EXT.

3. Rotate X AMP ATTEN control fully clock-wise.

4. Apply a 100 Kc square wave signal from the Fairchild Type 791A Generator through a properly terminated cable to the EXT TRIG/X AMP panel connector.

5. Adjust amplitude of the square wave pattern for 2 divisions peak-to-peak about the scale center. In other words, 1 division to the left and 1 division to the right of the scale center line.

6. Adjust trimmer C8119 for a flat-top display.

7. Set the Square Wave Generator to 1 Mc and adjust oscilloscope controls for a 2-cycle pattern on the screen.

8. Center the pattern and adjust its amplitude the same way as was done in step 5.

9. Adjust trimmers C8309 and C8317 until best flattop and rise time its achieved. 10. Pull out the PULL X10 magnification control and reduce square wave amplitude to give previous display.

11. Set the Square Wave Generator to 100 Kc.

12. Pull out the DA PULL EXT/10 switch and increase the signal level to obtain 2 divisions of deflection.

13. Adjust trimmer capacitor C8101 for optimum flat-top display.

14. Repeat steps 9 thru 13 for optimum squarewave response.

15. Disconnect generator and push in the DA PULL EXT/10 and the PULL X10 magnification controls.

5-15. X AMP DC BALANCE ADJ (R8105)

1. Set up the Type 74-03A for automatic triggering and observe vertical line.

2. Adjust the DC BAL potentiometer R8105 until there is no horizontal depositioning of the trace while rocking the X AMP ATTEN control throughout its range.

3. Remove the Time Base unit from the Y cavity.

5-16. FAST SWEEP CALIBRATION ADJUSTMENT (C8556, C8606, C8506, C8137, and C8317)

1. Make the following front-panel settings with the Type 76-02A or equivalent Y Plug-in in the Y cavity.

Setting					
NORM 1 µS					

2. Apply a 1-microsecond time-marker signal from a Fairchild Type 781A Generator through a properly terminated cable to the input connector on the Y Plug-in.

3. Adjust the VOLTS/DIV switch to give the display a vertical amplitude of about 4 divisions.

4. Using an insulated screwdriver, adjust trimmer capacitors C8556 and C8606 until 11 markers from the generator occupy 10 divisions.

5. Set the DISPLAY LOGIC switch from NORM to TRIG DLY'D and adjust trimmer capacitors C8506 and C8137 until 11 markers from the generator occupy 10 divisions.

6. Set the DISPLAY LOGIC switch from TRIG DLY'D to NORM and the NDT and DA TIME/ DIV switches to 0.1 microsecond.

7. Reset the Time-Mark Generator for a 10-megacycle sine wave signal and adjust trimmer capacitors C8606 until 11 peaks occupy 10 divisions.

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8. Set the DISPLAY LOGIC switch from NORM to TRIG DLY'D and adjust trimmer capacitor C8137 until 11 peaks occupy 10 divisions.

Note: If necessary repeat steps 4 through 8.

9. Reset the Time-Mark Generator for a 50-megacycle sine wave signal.

10. Pull out the PULL X10 magnification control and observe a 4-cycle sine wave display is within the center 8 division portion of the graticule. If not, adjust trimmer capacitor C8317 to bring calibration

within ±5%. Set Display logic switch to NORM and repeat the above procedure. All measurements should be 5-19. DELAY CAL ADJUSTMENT (R8614)

5-17. STROBE INTENSITY AND PATTERN CORRECTION **ADJUSTMENT** (R8012, R8005 and C8004)

1. Apply a 5-millisecond time-marker signal from a Fairchild Type 781A Generator through a properly terminated cable to the input connector on the Y Plug-in.

2. Reset the front-panel controls as indicated:

*						
Control	Setting					
DISPLAY LOGIC SLOPE NDT TIME/DIV DA TIME/DIV PULL X10 (MAG)	TRIG STROBE + 50 μS 2 μS Pushed in					

3. Vary the DELAY VERNIER control until the strobed section of the display is in the middle of the trailing edge of the marker signal.

4. Adjust the STROBE ADJ potentiometer R8012 until a distinct contrast is produced.

5. The strobed section may be offset to either side of the trailing edge of the unstrobed marker signal. If it is, readjust the PATTERN CORR potentiometer R8005 until the strobe is superimposed on the marker signal.

6. Reset the Time-Mark Generator for a 100-microsecond output signal.

7. Set the NDT TIME/DIV switch to 0.5 μ S and the DA TIME/DIV siwtch to 0.1 μ S.

8. Vary the DELAY VERNEIR control until the strobed section of the display is in the middle of the trailing edge of the marker signal.

9. Adjust trimmer capacitor C8004 for minimum overshoot at both ends of the strobed section.

Note: Consider ambient light conditions and possible use of cameras and viewing hoods when making these adjustments.

5-18. DELAY ZERO ADJUSTMENT (R8618)

1. Set the NDT and DA TIME/DIV switches to 0.1 µSEC.

2. Set DISPLAY LOGIC switch to TRIG STROBE and obtain a convenient display.

3. Set DELAY VERNIER dial to Zero.

4. If the strobed section is still visible, adjust the front-panel screwdriver DELAY ZERO control until the strobed section just disappears.

1. Apply a 100-microsecond time-marker signal from Fairchild Type 781 Generator through a properly terminated cable to Input connector on the Y plug-in.

2. Set NDT TIME/DIV switch to 0.1 mSEC and DA TIME/DIV switch to 5 µSEC, and DISPLAY LOGIC switch to TRIG STROBE.

3. Set DELAY VERNIER dial to 5 division and adjust the DELAY CAL potentiometer R8614 so that the strobed section starts approximately at the 5-division mark.

4. Set DELAY VERNIER dial to 0.8 division and DISPLAY LOGIC switch to TRIG DLY'D.

5. Position the display so that the pulse is bisected by the vertical center line, ± 0.05 division.

6. Advance the DELAY VERNIER dial to 5.8 division. (Be sure that the Positioning and Trigger LEVEL settings are not disturbed.)

7. Adjust the DELAY CAL potentiometer R8614, so that the pulse is again centered, ± 0.05 division.

8. Back off DELAY VERNIER dial to 0.8 division and check whether or not the pulse is again centered. If not, center the pulse and recheck step 7. This procedure may have to be repeated several times until the 0.8 division pulse and the 5.8 division pulse are centered, ± 0.05 division.

9. Measure the incremental accuracy of the delay calibration from 0.8 division to 9.8 division in steps of 1 division (i.e., 1.8 div, 2.8 div, etc.). One complete revolution of the DELAY VERNIER dial, say from 3.8 division to 4.8 division, should bring the succeeding pulse back to the position occupied by the preceding pulse within ± 1 division. (Be sure that the Positioning and Trigger LEVEL settings are not disturbed during this check.)

10. Center the pulse when the dial is set at 9.8 division. Turning the dial back to 0.8 division should bring the pulse back on screen within ± 2 division from the center line.

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Figure 5-2. Left Side View Showing Transistors, Nuvistors and Adjustments

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Figure 5-3. Top View Showing Transistors and Adjustments

NOTES

SECTION 6 TYPE 74-13A PARTS LISTS AND SCHEMATICS



Figure 6-1. Front Panel Replaceable Parts

SECTION 6A ELECTRICAL PARTS LIST AND SCHEMATICS

TYPE 74-13A CALIBRATED DELAYING SWEEP

			Re	ecomme	nded Vendor					Recomme	ended Vendor
Symbol	Part Nun	nber	Description	Code	Туре	Symbol	Part	Numbe	r Description	Code	Туре
			CAPACITORS			C8228	0319	1060	$0.01 \ \mu f_{\star} + 60 - 40\%$, 150V	CRL	DDM
						C8229	0316	4180	9.1 pf. ±5%, 1000V	RMC	C
Notes: 1. All capacitors are fixed, ceramic, and 500V unless					/ unless	C8231 &	2.2.1	10.00			0
	oth	herw	ise specified; pf denotes picof	arads.		C8232	0326	7880	plastic, 0.22 μ f, $\pm 10\%$, 200	AMX	C296AB
	2 GA	MV .	denotes Guaranteed Minimum	Value		C8233	0319	1060	0.01 µf, +60 -40%, 150V	CRL	DDM
	2. 0/		denotes oburunteed Minimum	value.		C8234	0315	1920	220 pf, ±20%	ERC	Style
C8001	0317 510	00	mica, 20 pf	EMC	DM 15						331GP2
C8002	0326 786	60	plastic, 0.1 μ f, \pm 10%, 200V	AMX	C296AB	C8235	0317	3200	12 pf, $\pm 10\%$	CRL	#TB60120
C8003	0317 384	40	330 pf, ±10%	EIA							KCOG
C8004	0326 948	80	variable, air, 9-35 pf	ERC	Style 538	C8241	0326	7620	electrolytic, 5 µf, 50V	SPG	"Littl-Lytic"
C8101	0326 949	90	variable, air, 2-8 pf, 200V	ERC	Style 538	C8300	0317	5110	mica, 22 pf, ±5%	EMC	DM15
C8102	0319 100	60	0.01 µf, +60 -40%, 150V	CRL	DDM	C8301	0319	1060	0.01 µf, +60 -40%, 150V	CRL	DDM
C8103	0315 200	00	100 pf, ±20%	EIA		C8302	0316	7200	4.7 pf, ±0.25 pf	ERC	NPO-331
C8104	0326 452	20	1000 pf, GMV	ERC		C8303	0317	5110	mica, 22 pf, ±5%	EMC	DM15
C8105	0315 372	20	2200 pf, +100 -0%	ERC		C8304	0315	3630	150 pf, ±10%	EIA	
C8106	0319 105	50	0.02 μ f, +60 -40%, 150V	CRL	DDM	C8305	0305	5600	mica, 47 pf, ±5%	EIA	
C8107	0326 849	90	paper, 0.1 μ f, \pm 20%, 200V	HOP	Part No.	C8306					
					P12D	C8307 &					
C8108 &						C8308	0319	1050	$0.02 \ \mu f, +60 -40\%, 150V$	CRL	DDM
C8109	0314 686	60	5.6 pf, ±1%	EIA		C8309	0326	9500	variable, air, 5.5-18 pf, 200V	ERC	538
C8111	0319 105	50	0.02 μ f, +60 -40%, 150V	CRL	DDM	C8311	0326	7860	plastic, 0.1 μ f, \pm 10%, 200V	AMX	C296AB
C8112	0316 952	20	2200 pf, 1000V	RMC	JL	C8312	0319	1050	$0.02 \ \mu f, +60 -40\%, 150V$	CRL	DDM
C8113	0315 361	10	100 pf, ±10%	EIA		C8313	0326	7880	plastic, 0.22 μ f, \pm 10%, 200V	AMX	C296AB
C8114	0319 105	50	$0_{102} \ \mu f$, $+60 \ -40\%$, $150V$	CRL	DDM	C8314	0326	8080	plastic, 0.22 μ f, \pm 10%, 400V	AMX	C296AB
C8115	0326 452	20	1000 pf, GMV	ERC		C8315	0326	7860	plastic, 0.1 μ f, \pm 10%, 200V	AMX	C296AB
C8116	0317 511	10	mica, 22 pf, ±5%	EMC	DM15	C8316	0315	2000	100 pf, ±20%	EIA	
C8117	0319 105	50	$0.02 \ \mu f, +60 -40\%, 150V$	CRL	DDM	C8317	0326	9480	variable, 9-35 pf, 100V	ERC	Style 538
C8118	0316 02/	70	22 pf	EIA		C8318 &					
68119	0326 95	10	variable, air, 2.5-11 pf, 200V	ERC		C8319	0319	1050	$0.02 \ \mu f, +60 -40\%, 150V$	CRL	DDM
C8120	0315 36	10	100 pf, ±10%	EIA		C8401 to					
68121	031/ 51	10	mica, 22 pt, ±5%	EMC	DM15	C8403	0319	1050	$0.02 \ \mu$ t, +60 -40%, 150V	CRL	DDM
68122	0315 36	10	100 pf, $\pm 10\%$	EIA	600/4P	60.10.1			0.1 (+ 000) 0000		Part No.
C8123	0326 /80	60	plastic, 0.1 μ t, ±10%, 200v	AMX	C296AB	C8404	0326	8490	paper, 0.1 μ f, \pm 20%, 200V	HOP	P12D
C8124	0317 510	00	mica, 20 pf, -5%	EMC	DMIS	C8405	032/	1630	electrolyfic, 2 μ f, ± 100	000	Series TE
C8120	0305 500	00	mica, 4/ pf, -10%	EIA	DHIE	60404	0004	00/0	-10%, 1000	SPG	"Littl-Lytic"
C012/	0317 510	50	mica, 20 pt, -5%	EMC	DMIS	C8406	0326	8060	plastic, 0.1 μ t, \pm 10%, 400V	AMX	C296AC
C0120	0319 103	10	$100 \pm \pm 100$	CRL	DDM	C8407	0319	1060	$0.01 \ \mu f, + 60 - 40\%, 150V$	CRL	DDM
C9121	0315 301	60	$100 \text{ pt}, \pm 10\%$	CPI	DDM	C8408	0319	1050	$0.02 \ \mu f, + 60 - 40\%, 150V$	CRL	DDM
C8132	0314 100	80	9.1 pf 1000V	DAAC	C	C8409	031/	0/30	mica, 1000 pt, -5%	EMC	DM20
C8132	0310 410	60	$0.01 \text{ wf} \pm 60 \pm 40\% 150V$	CPI	DDM	C0411	0310	1040	0.01	CDI	DDU
C8134	0326 788	80	plastic 0.22 μ f $\pm 10\%$ 200V	AMY	C2064B	C0412	0216	0220	$20 - 100$ μ , ± 00 40% , 150%	CRL	DDM
C8135	0317 320	00	12 pf $\pm 10\%$	CPI	CZYOAD	C8414	0310	1060	0.01	CPL	DDM
C8136	0326 788	80	plastic 0.22 //f ±10% 200V	AMX	C296AB	C8441	0316	7280	10 pf +0.25 pf	ERC	NPO 221
C8137	0326 948	80	variable 9-35 pf 100V	FRC	Style 538	C8442 8	0310	1200	10 pi, =0.25 pi	LAC	NFO-331
C8200	0326 452	20	1000 pf. GMV	FRC	01110 000	C8443	0326	4520	1000 of CMV	EDC	
C8201	0316 720	00	$4.7 \text{ pf} \pm 0.25 \text{ pf}$	FRC	NPO SI-1	C8446 &	0520	4520	1000 p1, GMV	ERC	
C8202	0319 104	60	$0.01 \ \mu f + 60 - 40\% \ 150V$	CRI	DDM	C8447	0326	4520	1000 pf GMV	EDC	
C8203	0315 200	00	100 pf. ±20%	EIA		C8449	0326	4520	1000 pf. GMV	ERC	
C8204	0319 105	50	$0.02 \ \mu f. + 60 - 40\%, 150V$	CRL	DDM	C8451	0326	4520	1000 pf GMV	FRC	
C8205	0315 372	20	2200 pf. +100 -0%	ERC		C8501	0327	1580	mice 348 pf \pm 5%	EMC	DM15
C8206	0319 100	60	$0.01 \ \mu f_{\star} + 60 - 40\%$, 150V	CRL	DDM	C8502	0327	1510	mica, 3831 pf \pm 5%	EMC	DM10
C8208 &			1.1.1			C8503	0327	2090	plastic 0.03866 uf ± 5%	Line	Dinity
C8209	0314 686	60	5.6 pf. ±1%	EIA		00000	0027	2070	100V	GUD	336B
C8211	0326 849	90	paper, 0.1 μ f, $\pm 20\%$, 200V	HOP	No PI2D	C8504	0316	0300	30 pf	FIA	3308
C8213	0319 105	50	0.02 uf. +60 -40% 150V	CRL	DDM	C8506	0326	9490	variable, air, 2-8 pf, 200V	ERC	Style 538
C8214	0316 952	20	2200 pf, 1000V	ERC		C8507	0326	8760	plastic, 0.86 µf. ±1%, 100V	GUD	355B
C8216	0305 560	00	mica, 47 pf, ±5%	EIA		C8508	0316	4180	9.1 pf. 1000V	RMC	C
C8217	0326 786	60	plastic, 0.1 µf, ±10%, 200V	AMX	C296AB	C8509	0316	3790	27 pf, 1000V	RMC	C
C8218	0317 510	00	mica, 20 pf, ±5%	EMC	DM15	C8510	0316	3850	47 pf. 1000V	RMC	C
C8219	0315 36	10	100 pf, ±10%	EIA		C8551	0327	1580	mica, 348 pf, ±.5%	EMC	DM15
C8221	0317 510	00	mica, 20 pf	EMC	DM15	C8552	0327	1510	mica, 3831 pf, ±.5%	EMC	DM19
C8223	0305 585	50	mica, 510 pf, ±10%, 300V	EIA		C8553	0327	2090	plastic, 0.03866 uf. ± .5%	-///	20017
C8224	0315 361	10	100 pf, ±10%	EIA					100V	GUD	336B
			and the second sec	10000					100.01		

section 6a – parts list and schematics

			Re	ecomme	nded Vendor
Symbol	Part	Number	Description	Code	Туре
C8554	0316	0300	30 pf	EIA	
C8556	0326	9490	variable, air, 2-8 pf, 200V	ERC	Style 538
C8557	0326	8760	plastic, 0.86 μ f, $\pm 1\%$, 100V	GUD	355B
C8558	0315	4660	4700, ±10%, 1000V	RMC	JL
C8559	0319	6250	plastic, 0.05 uf. ±10%, 150V	GUD	Series 338Y
C8560	0316	4180	9.1 pf 1000V	RMC	C
C8561	0316	3790	27 pf 1000V	RMC	c
C8562	0316	3850	47 nf 1000V	RMC	c
C8563	0326	7030	plastic 1 uf +10% 125V	AMX	C296AB
C8601	0310	1050	$0.02 \text{ uf} \pm 60 \pm 40\% 150\text{ V}$	CRI	DDM
C8602	0326	7860	plastic 0.1 μ f +10% 200V	AMX	C2964B
C8604	0315	2720	$2200 \text{ pf} \pm 100 - 0\%$	EPC	CITORD
C0404	0313	0400	2200 pl, 100 0%	ERC	Stula 520
C8000	0320	7400	variable, air, 9-35 pt, 100v	ERC	Style 556
C800/	0320	/030	electrolytic, 10 μ t, \pm 100	600	111 and 1. at all
60/00	0010	10/0	10%, 50%	SPG	LITTI-LYTIC
68008	0319	1060	$0.01 \ \mu t, + 60 \ -40\%, 150\%$	CKL	DDM
68011	0319	1050	$0.02 \ \mu f, + 60 - 40\%, 150\%$	CRL	DDM
C8/01	0317	5110	mica, 22 pf, ±5%	EWC	DMIS
C8/02	032/	3420	electrolytic, 10 μ f, -10		
	- 71	a	+75%	SPG	"Littl-Lytic"
C 8604	051	1. 521	0 CM STPP 3000 + 370		
			SEMICONDUCTORS		
CR8001	2600	6910	diode, FD841	FCI	
CR8101	2600	8150	diode, 1N3717	EIA	
CR8102 to					
CR8112	2600	6910	diode, FD841	FCI	
CR8113	2600	8020	diode, FDG3091	FCI	
CR8201	2600	8150	diode, 1N3717	FIA	
CR8202 to					
CR8205	2600	6910	diode ED841	FCI	
CR8206 to	2000	07.10			
CR8212	2600	6910	diode ED841	FCI	
CR0212	2600	8020	diode, FDG3091	FCI	
CR8401	2600	6820	diode, FD291	FCI	
CR0401	2400	4010	diode, FD201	FCI	
CR8402	2600	6020	diode, FD291	FCI	
CR0403	2600	6010	diode, FD201	FCI	
CR0404	2000	6010		FCI	
CR8400	2000	0910	diode, FD841	FCI	
CR8601	2600	9250	diode, ID-2A	GE	
CR8602 to	0,000	(010			
CR8604	2600	6910	diode, FD841	FCI	
CR8701	2600	6910	diode, FD841	FCI	
			LAMPS		
DS8101	1200	3960	neon, 0.3 milliamperes, 1/25W	GE	NE 2
D\$8201	1200	3040	neen 03 milliamarca 1/2514	GE	146-2
030201	1200	3700	(INCAL)	CF	NE 2
00001 0			(UNCAL)	GE	INE-Z
D50301 &	1201	2250	AND		70.07
058302	1201	2350	neon (BEAM POS IND)	SIG	12-2/
	1000				IRIOO
E8101	1200	3960	glow, neon, NE-2	GE	NE-2
E8201	1200	3960	glow, neon, NE-2	GE	NE-2
			HYBRID & RE COILS		

HY8101,					
HY8302,					
HY8303 &					
HY8304	2110	1560	Bead, ferrite	FER	Part No.
					56-590-65/3B
HY8603	2110	1560	Bead, ferrite	FER	Part No.
					56-590-65/3B
L8101 &					
L8102	2110	1350	coil, rf, 3.3 μh, ±5%	SWW	D10647

ELECTRICAL CONNECTORS

J8100 &	0905 7610	receptacle, rf, BNC, female,			
J8200		1 contact (EXT TRIG)	U	IG 625A/U	
J8201	0905 6700	jack tip, banana type,			
		insulated, black (SAW OUT)	JHN	108-903	
J8401 &	0905 6700	jack tip, banana type,			
J8402		insulated, black (GATE)	JHN	108-903	
P8001	0905 7340	plug, male, 32 contacts	APH	26-159-32	

Symbol	Part Numb	er Description	Code	Туре
		TRANSISTORS		
08001	2600 7020	DU #14	FCI	
00001	2600 7020	Solternate 2N914		
08002	2600 7370	DII # 84/2N6998 2/37-3	ABD/FCI	8A/2N699B
08101	2600 7420	DU #94	FCI	
90101	2600 7420	alternate 2N869		
09102	2600 7260	DIL #6	FCI	
90102	2600 7250	alternate 2N1893		
08103.8	2600 7230	DIL #1A	FCI	
08104	2600 7020	alternate 2N914		
08104	2600 7000		FCI	
08107	2600 7020	alternate 2N014		
08107	2600 7000		FCI	
020100	2600 7250	alternate 2N1893	i ci	
00202	2600 7230		FCI	
00202	2600 7420		rei	
00202 8	2600 7400		FCI	
Q8203 &	2600 7150		ici	
08204	2600 7130	DIL #24	FCI	
Q8205	2600 7070		rei	
00004 8	2600 7030	citernate ZNYIS	FCI	
Q8200 &	2600 7020	DU # 1A	FCI	
Q820/	2600 7000	alternate ZN914	ECI	
Q8208	2600 7260		FCI	
00201 1-	2600 7230	Citernate ZIN1693	ECI	
Q8301 10	2600 7080		FCI	
Q8303	2600 7030	alternate ZNY15	FCI	
Q8304	2000 7200	DU #0	FCI	
00005 0	2600 7250	alternate ZIN1893	ECI	
Q8305 &	2600 7080	DU # 28	ECTED	
08300	2600 7030	alternate 214915	36AECI	
Q830/	2000 8030	DU # 30 USE 2000	- FCI	
00000 0	2000 8020	alternate 2013114 D4 3640	5	
Q8308 &	2603 7020		rci	
Q8309	2600 7000	alternate ZNY14	501	
Q8311	2600 8630	DU #36	FCI	
09401	2600 8620	alternate ZN3114	ECI	
Q8401	2600 7180	DU #48	FCI	
00400	2600 7150	alternate ZNII32	ECI	
Q8402	2600 7270	DU #6A	FCI	
00400	2600 7250	alternate ZN1893		
Q8403	2600 7370	DU #8A/ZNO99B	ABD/FCI	8A/2N099B
Q8404 to	2600 7020	DU #IA	FCI	
Q8406	2600 7000	alternate 2N914	5.01	
Q8601 &	2600 7070	DU #2A	FCI	
08602	2600 7050	alternate 2N915		
08803	2600 /260	DU #6	FCI	
00/04	2600 7250	alternate 2N1893		
08004	2000 7010		FCI	
0.0701 .	2600 7000	alternate ZN914		
Q8/01 to	2600 8190	DU #14A	FCI	
138/13	ZOUU X1/()	diference /N/309		

Recommended Vendor

RESISTORS

- Notes: 1) All resistors are fixed, film, ±5%, and ½W. Values are in ohms unless otherwise specified; K = thousand, M = million.
 - Listed below are the Part Numbers for fixed, film, resistors used on the TIME/DIV switches. These resistors are selected for plus or minus tolerances.

All minus tolerance units are marked with a yellow dot and plus tolerance units are marked with a green dot.

Resistor Part Number

0239	0241	to	0239	0249
0239	0251	to	0239	0259
0239	0261	to	0239	0279
0239	0281	to	0239	0299

When a replacement is ordered, a pair of resistors, one marked with a yellow dot and the other with a green dot will be sent. If a colorcoded component is removed from the unit, be sure to replace it with the corresponding color dot component. This will insure proper performance of the plug-in module.

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		R	ecomme	ended Vendor				Recomme	ended Vendor
Symbol	Part Numb	er Description	Code	Туре	Symbol	Part Numb	er Description	Code	Туре
R8013	0234 8530	22K	CGW	C-20	R8170	0203 2010	composition, 100K	ALB	FB
R8017	0203 2010	composition, 100K, $\pm 10\%$	ALB	EB	R8171	0234 9450	47K. 1W	CGW	C-32
R8100	0109 0830	variable, composition, 100K.			R8172	0234 7970	100	CGW	C-20
		± 20% 2W (TRIG BAL)	CTS	Series 70	R8173	0203 2070	composition, 330K, $\pm 10\%$	ALB	EB
R8101	0229 9050	111K, ±1%	TEX	CD1/2PR	R8174	0234 8690	100K	CGW	C-20
R8102	0229 4910	900K, ±1%	TEX	CD1/2PR	R8175	0109 0810	variable, composition, 250,		
R8103	0235 4850	composition, 10K, 1/4 W	ALB	CB			\pm 20%, .3W (SWP RATE		
R8104	0203 0960	composition, 100K	ALB	EB			BAL)	CTS	Series 70
R8105	0109 0820	variable, composition, 500K,			R8176 &				
		\pm 20%, .2W (DC BAL)	CTS	Series 70	R8177	0234 7970	100	CGW	C-20
R8106	0235 5170	composition, 220K, 1/4 W	ALB	CB	R81/8	0239 1392	6.8K, 2W	CGW	C-42
R810/	0235 5330	composition, IM, 1/4 W	ALB	СВ	R81/9	0203 0160	composition, 4/	ALB	EB
R8108	0236 3150	360K	CGW	C-20	R8180	0234 8360	JUK	CGW	C-20
R8109	0234 8510	ISK 19K 1/ W	CGW	C-20	R0101	0234 8280	27.4K + 1.00	CGW	C-20
P8111F/P	0107 2701	variable composition	ALD	СВ	R8183	0235 4450	composition 200 1/.W	ALR	N3-20
KOTTIT/K	010/ 2//1	500K/10K ±20%			R8200	0234 7970	100	CGW	C 20
		(TRIG LEVEL X AMP)	ABD		R8201	0204 0970	composition, 110K	IRC	GBT1/2
R8112	0234 8510	18K	CGW	C-20	R8202	0204 1190	composition, 910K	IRC	GBT1/2
R8113	0234 8460	11K	CGW	C-20	R8203	0235 4850	composition, 10K, 1/4 W	ALB	CB
R8114	0234 7970	100	CGW	C-20	R8204	0203 0960	composition, 100K	ALB	EB
R8115	0236 6700	11.5K, ±1%	CGW	N20	R8206	0235 5170	composition, 220K, 1/4 W	ALB	CB
R8116	0235 4410	composition, 130, 1/4 W	ALB	CB	R8207	0235 5400	composition, 1M, 1/4W	ALB	CB
R8117	0234 7910	56	CGW	C-20	R8208	0236 3100	220K	CGW	C-20
R8118	0107 5900	variable, composition, 100,			R8217	0234 7970	100	CGW	C-20
		±20% (TRIG SENS)	CTS	65	R8218	0235 4410	composition, 130, 1/4 W	ALB	CB
R8119	0203 0110	composition, 30	ALB	EB	R8219	0235 4380	composition, 100, 1/4 W	ALB	EB
R8120	0236 6700	11.5K, ±1%	CGW	N20	R8221	0234 8580	36K	CGW	C-20
R8121	0234 8600	43K	CGW	C-20	RSZZZ	010/ 2393	+ 2001 (TRIC LEVEL)		
R8122	0234 8280	28	CGW	C-20	B0222	0224 0500	- 20% (IRIG LEVEL)	ABD	C 00
R8123	0234 /9/0		CGW	C-20	R0223	0234 8580	JOK	CGW	C-20
R0124	0235 4410	30 2K + 1 %	ALB	N2O	R8224	0234 8000	100	CGW	C-20
R8126	0236 7050	26 7K	CGW	NS-20	R8227	0235 4410	composition 130 1/W	AIR	C-20
R8127	0203 1730	composition 470 ± 10%	AIR	FB	R8228	0203 0150	composition 43	ALB	ER
R8128	0236 7100	30.1K	CGW	NS-20	R8229	0107 5900	variable, composition 100	ALD	LD
R8129	0203 2090	composition, 470K, ±10%	ALB	FR			±20% (TRIG SENS)	CTS	65
R8130	0236 7020	24.9K, ±1%	CGW	N20	R8231	0203 0110	composition, 30	ALB	FB
R8131	0203 2090	composition, 470K, \pm 10%	ALB	EB	R8232	0234 8600	43K	CGW	C-20
R8132	0234 8080	300	CGW	C-20	R8233	0236 2880	wire wound, 5.8K, \pm 1%, 2W	DAL	RS2A
R8133	0235 9240	1.1K, ±1%	CGW	NI-20	R8234	0109 0830	variable, composition, 100K,		
R8134	0234 9190	3.9K, 1W	CGW	C-32			\pm 20%, .2W (TRIG BAL)	CTS	Series 70
R8135	0234 8610	47K	CGW	C-20	R8238	0236 7050	26.7K	CGW	NS-20
R8136 &					R8239	0203 1730	composition, 470, $\pm 10\%$	ALB	EB
R8137	0203 1910	composition, 15K, $\pm 10\%$	ALB	EB	R8240	0236 7100	30.1K	CGW	NS-20
R8138	0235 9240	1.1K, ±1%	CGW	NI-20	K8241F/K	010/ 2/01	variable, wire wound, 2.5K/		
R8139	0236 3100	220K	CGW	C-20	500.10		TUK, ZW (SWP CAL)	ABD	
R8140	0234 8110	390	CGW	C-20	R8242	0107 0711			
R0141 Q	0202 1170	composition 750K			(part of	010/ 2/11	variable, wire wound, 2.5K,		
R8142	0203 11/0	KOMPOSITION, 750K	ALB	EB	5051)	0226 2100	- 10%, 2W (SWP VERNIER,	ABD	
R8144	0234 8450	10K	CGW	C-20	K0243	0230 3190	1W/	COW	C 20
R8145 &	0234 0430	TOR	CGW	C-20	D9244	0224 8400	1004	CGW	C-20
R8146	0234 8610	47K	CGW	C 20	R0244	0234 8090	romposition 200K	CGW	C-20
R8147	0234 8110	390	CGW	C-20	R8246	0234 8690	100K	COW	C 20
R8148	0234 8010	150	CGW	C-20	R8247	0234 8450	10K	CGW	C-20
R8149	0234 6160	750, ±1%, 2W	CGW	SI-25	R8248	0203 2130	composition 1M ±10%	ALB	FR
R8150	0234 8440	9.1K	CGW	C-20	R8249	0234 8030	180	CGW	C-20
R8151	0228 7130	953, ±1%, 1W	CGW	SI-20	R8250	0234 8450	10K	CGW	C-20
R8152	0203 1170	composition, 750K	ALB	EB	R8251	0234 6160	750, ±1%, 2W	CGW	SI-25
R8153	0234 8480	13K	CGW	C-20	R8252	0228 7130	953, ±1%, 1W	CGW	SI-20
R8154	0235 9600	2.49K, ±1%, 1W	CGW	NI-20	R8253	0234 8440	9.1K	CGW	C-20
R8155	0239 1192	1K, ±1%, 1W	CGW	SI-20	R8254	0203 1170	composition, 750K	ALB	EB
R8156	0203 2010	composition, 100K, \pm 10%	ALB	EB	R8255	0203 1940	composition, 27K, $\pm 10\%$	ALB	EB
R8157 &					R8256	0239 1192	1K, ±1%, 1W	CGW	SI-20
R8158	0234 8450	10K	CGW	C-20	R8257	0235 9600	2.49K, ±1%	CGW	NI-20
R8159	0109 0800	variable, composition, 1.5K,			R8258	0234 8480	13K	CGW	C-20
D01/0		± 20%, .3W (SWP LENGTH)	CTS	Series 70	R8259	0203 2010	composition, 100K, \pm 10%	ALB	EB
R8160	0203 1940	composition, 27K, ±10%	ALB	EB	R8260	0234 8450	TOK	CGW	C-20
R0101	0234 9220	5.1K, 1W	CGW	C-32	R8261	0234 8600	43K	CGW	C-20
R0102	0234 82/0	1.8K	CGW	C-20	R8262	0234 9220	5.1K, 1W	CGW	C-32
R0103	0203 1650	composition, 100, \pm 10%	ALB	EB	R8263	0109 0800	variable, composition, 1.5K,		
R8165	0234 8320	204	CGW	C-20			= 20%, .3W (SWP LENGTH) CTS	Series 70
R8166	0234 0390	144 +104	CGW	C-20	R8264	0234 8270	1.8K	CGW	C-20
R8167	0234 7070	100	CGW	C 20	R8265	0236 5100	$24/, \pm 1\%$	CGW	N-20
R8168	0234 8450	10K	CGW	C-20	R8200	0230 0420	14K, - 1%	CGW	NI-20
R8169	0234 8140	510	CGW	C-20	R820/	0234 9230	100	CGW	C-32
			COW	0-20	10204	0234 /9/0	100	CGW	C-20

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Symb	ol Part Numl	per Description	Recomm	ended Vendor Type	Symbol	Part Numbe	er Description	Code	Type	endor
57112					BU400	0226 2800	wire would 10K 2W	DAL	CS-24	
R8270	0234 8590) 39K	CGW	C-20	R8408	0230 2800	wire wound, lok, 2w	AIR	ER ER	
R827	0234 8320) ЗК	CGW	C-20	R8409	0203 0100	composition, 27	COW	C 20	
R827	0234 8450) 10K	CGW	C-20	R8410	0234 8040	200	WSI	5Y	
R8273	0234 8140	510	CGW	C-20	R0411	0234 0930	whe would, ok, 5^{W}	CGW	C-20	
R827.	0234 8450) 10K	CGW	C-20	R0412	0236 0750	$7.5K_{,} = 1.00$	CGW	NI. 20	
R8270	0203 2070) composition, 330K, \pm 10%	ALB	EB	R8413	0233 9730	3.4K, -1%	AIR	ER	
R827	0234 9450	0 47K, 1W	CGW	C-32	R0414	0203 1080	composition, 330K	ALB	EB	
R8279	0234 7970	0 100	CGW	C-20	R0415	0203 0740	400 + 10/1W	CGW	51-20	
R8280	0203 0830	composition, 30K	ALB	EB	P8/17	0234 8410	477, - 1 /0, 1 W	CGW	C-20	
R828	0234 8690	0 100K	CGW	C-20	P8418	0203 1090	composition 360K	ALB	FB	
R828	2 &				R8410	0234 8290	2 2K	CGW	C-20	
R828	0234 7970	0 100	CGW	C-20	R8420	0203 1050	composition, 240K	ALB	EB	
R828-	0234 8280	2 K	CGW	C-20	R8421	0203 0000	composition, 10	ALB	EB	
R828.	5 0234 8380	composition, 5.1K	CGW	C-20	R8422	0234 8140	510	CGW	C-20	
R8280	0239 1392	2 6.8K, 2W	CGW	C-42	R8423	0203 0890	composition, 51K	ALB	EB	
R828.	0203 0160	composition, 4/	ALB	EB	R8424	0236 3150	360K	CGW	C-20	
R830	0228 5110) 13.3K, -1%	IRC	DCC	R8425	0203 0830	composition, 30K	ALB	EB	
R830		0 200K	COW	C 20	R8426	0234 8410	6.8K	CGW	C-20	
K830.	0234 8090	J TOOK	CGW	C-20	R8427	0234 8290	2.2K	CGW	C-20	
R8300	0107 0011	1 LL 15K + 10%	ance to. c	107 2912	R8428	0234 8140	510	CGW	C-20	
(part	01 010/ 2911	Variable, ISK, - 10%,	ARD	Jar. 30K	R8429	0236 7310	49.9K, ±1%	CGW	N20	
5840	0107 2546	Two (POSITION)	ADD	\$ 10 % 3/4 watt	R8440	0203 0000	composition, 10	ALB	EB	
K830/	010/ 2543	+ 20%	ARD		R8441	0239 1359	430, 2W	CGW	C-42	
B000	0224 0000	130	CGW	C-20	R8442	0236 0690	24.9K, ±1%	CGW	NI-20	
R0300	0234 8000	9 9 9 4	CGW	C-20	R8443	0235 9600	2.49K, 土1%	CGW	NI-20	
P9310		composition 510K	ALB	EB	R8444	0239 1359	430, 2W	CGW	C-20	
P831	0100 0710) variable composition 750			R8445	0234 8190	820	CGW	C-20	
ROOT	0107 0710	±10% (X10 REG)		Series 65	R8446	0234 8210	1K	CGW	C-20	
P831	0234 8470) 12K	CGW	C-20	R8501	0239 0288	1.2M, ±.5%	ABD		
R831	0236 0270	$10K \pm 1\%$	CGW	NI-20	R8502	0239 0291	2M, ±.5%	ABD		
R831	0235 8710	$365. \pm 1\%$	CGW	NI-20	R8503	0239 0292	4M, ±.5%	ABD		
R831	6 0236 4600	$75, \pm 1\%$	CGW	N20	R8504	0239 0285	400K, ±.5%	ABD		
R8317	0236 6720) 12.1K, $\pm 1\%$	CGW	N20	R8506	0239 0284	200K, ±.5%	ABD		
R831	0203 0160	composition, 47	ALB	EB	R8507	0239 0283	120K, ±.5%	ABD		
R8319	0235 4380	composition, 100, 1/4 W	ALB	CB	R8508	0239 0282	40K,	ABD		
R8320	0203 0900	composition, 56K	ALB	EB	R8509 &	0220 0201	201 + 591	APD		
R832	0236 6720) 12.1K, ±1%	CGW	N20	R8510	0239 0281	20K,5%	ABD		
R832	0228 5040) 1.21K, 土1%	IRC	DCC	R0311	0239 0231	10M, -170, 100	ABD		
R832	3 &			a survey	P8513	0239 0241	5 AM + 1 %	ABD		
R8324	0236 6590	0 8.87K	CGW	N20	P8514	0239 0242	$1.8M \pm 5\%$	ABD		
R832.	0228 5190	0 62K, ±1%	IRC	DCC	R8516	0239 0287	900K ± 5%	ABD		
R832	0228 5040) 1.21K, ±1%	IRC	DCC	R8517	0239 0286	500K. ± 5%	ABD		
R832	0235 9690) 3.01K, $\pm 1\%$	CGW	NI-20	R8551	0239 0288	1.2M, ±.5%	ABD		
R832	0235 9650) 2.74K, ±1%	CGW	NI-20	R8552	0239 0291	2M, ±.5%	ABD		
R832	0236 5630	0 887, -1%	CGW	N20	R8553	0239 0292	4M, ±.5%	ABD		
R833	0225 4290	100 1/ 14	ALR	CB	R8554	0239 0285	400K, ±.5%	ABD		
K833.		154	CGW	C-20	R2556	0239 0284	200K, ±.5%	ABD		
K033.	0234 0230) 2K 1W	CGW	C-32	R8557	0239 0283	120K, ±.5%	ABD		
R033	0234 9100	3K 1W	CGW	C-32	R8558	0239 0282	40K, ±.5%	ABD		
R033		composition 20	ALB	FB	R8559 &					
PRSS	0235 4260	composition 33 1/W	ALB	CB	R8560	0239 0281	20K, ±.5%	ABD		
PR33	0109 0700	variable, composition, 750.			R8561	0239 0251	$18M, \pm 1\%, 1W$	ABD		
Rooo		\pm 10% (X10 REG)	CTS	Series 65	R8562	0239 0241	9M, ±1%	ABD		
R834	0235 1760	7.8K, 5W	CGW	LPI-5	R8563	0239 0242	5.4M, ±1%	ABD		
R834	0235 4260	composition, 33, 1/4 W	ALB	CB	R8564	0239 0289	1.8M, ±.5%	ABD		
R834	0235 1760	7.8K, 5W	CGW	LPI-5	R8566	0239 0287	900K, ±.5%	ABD		
R834	3 &				R8567	0239 0286	500K, ±.5%	ABD		
R834	4 0235 1750	2.1K, 5W	CGW	LPI-5	R8601	0203 0110	composition, 30	ALB	EB	
R834	5 &				R8602	0203 0310	composition, 200	ALB	EB	
R834	0235 1760) 7.8K, 5W	CGW	LPI-5	R8603	0235 4780	composition, 5.1K, ¼W	ALB	CB	
R834	0236 5680	D 1K, ±1%	CGW	NS-20	R8604	0235 4380	composition, 100, 1/4 W	ALB	CB	
20 R834	0235 4380) composition, 100, 1/4 W	ALB	CB	R8605	0235 4780	composition, 5.1K, 1/4W	ALB	CB	
23 11 V R834	9 &				R8607	0234 8690	100K	CGW	C-20	
R 0 0 R835	0235 5150) 180K, ¼W	ALB	CB	R8608	0234 7510	18K	CGW	C-20	
10° 5 R835	2 &				R8609	0234 8530	22K	CGW	C-20	
0 1° R835	3 0235 4380	composition, 100, 1/4 W	ALB	СВ	R8611	0203 0160	composition, 47	ALB	EB	
, R835	5 &				R8612	0235 4380	composition, 100, 1/4 W	ALB	CB	
Con R835	0203 1890	composition, IUK, $\pm 10\%$	ALB	C 20	R8613	0234 8690	100K	CGW	C-20	
R835	0234 8590	J JYK	CGW	C-20	R8614	0109 0460	variable, wire wound, 4K,			
R840	0203 0/40	200	ALB	C 20			\pm 10%, 1.5W (DLY CAL			
R840		15K + 19	CGW	NI-20			ADJ)	CLS	49M	
K840	3 0225 0950	$432k \pm 10/2$	CGW	NI-20	R8615	0203 2130	composition, 1M, $\pm 10\%$	ALB	EB	
R840	4 0234 8210) 1K	CGW	C-20	R8616	0234 5150	wire wound, 9.1K, 3W	DAL	CS-2B	
R840	6 0234 5120) wire wound, 3.6K. 3W	DAL	CS-2B	R8617	0109 0920	variable, wire wound, 2K, 2W	100 11 10		
R840	0234 7970	0 100	CGW	C-20			(DELAY VERNIER)	CLS	Series	62JA

section 6A – electrical parts lists and schematics

		F	ecomme	ended Vendor
Symbol	Part Numbe	r Description	Code	Туре
R8618	0109 0490	variable, composition, 250, ± 20%, .3W (DELAY ZERO)	СТЅ	Series 70
R8619	0239 1378	2.2K, 2W	CGW	C-42
R8620	0235 4380	composition, 100, 1/4 W	ALB	CB
R8621	0234 8470	12K	CGW	C-20
R8622	0234 8490	15K	CGW	C-20
R8623	0236 7190	37.4K, ±1%	CGW	NS-20
R8701	0234 8710	120K	CGW	C-20
R8702	0234 8560	30K	CGW	C-20
R8703	0234 8280	2K	CGW	C-20
R8704	0236 3120	270K	CGW	C-20
R8705	0234 8350	3.9K	CGW	C-20
R8706	0236 7010	24.3K, ±1%	CGW	NS-20
R8707	0234 8300	2.4K	CGW	C-20
R8708	0236 7130	32.4K,±1%	CGW	NS-20

SWITCHES

\$810 & \$811	0503	2570	slide, DP3T (S810 — SOURCE) (S811 — COUPLING	STC	SS-54
\$812 \$813 (Part of	0503	2580	slide, DPDT (SLOPE)	STC	SS-54
R8111 (F/R)	0107	2791	push-pull, 1 ampere, 125V, SPDT (PULL EXT 1/10)	STC	
\$820 & \$821	0503	2570	slide, DP3T (S820 — SOURCE) (S821 — COUPLING	STC	SS-54
S822 S823	0503	2580	slide, DPDT (SLOPE)	STC	SS-50
(part of R8222)	0107	2393	push-pull, 1 ampere, 125V, SPDT (PULL EXT $\frac{1}{10}$)	STC	
\$824	0503	2700	toggle, DP3T, 5 amperes at 115V ac	ALCO	MST-205N

			Recommen	nded Vendor
Symbol	Part Numb	er Description	Code	Туре
S830 (part of				
R8307)	0107 2545	slide, DPDT (PULL X10 MAG)	ABD	
S840	0501 7123	rotary. 3 sections, 6 positions	,	
		60° (DISPLAY LOGIC)	ABD	
S850	0501 7691	rotary (TIME/DIV)	ABD	
S851				
(part of	0107 2711	rotary, linear, SPDT,		
R8242)		3 amperes, 125V	ABD	

TRANSFORMERS

T8101	2001	3742	pulse	ABD
T8201	2001	3741	pulse	ABD
T8601	2001	3742	pulse	ABD

ELECTRON TUBES

V8101 &					
V8102	2501	3430	7586	RCA	Nuvistor
V8103	2501	3450	7587	RCA	Nuvistor
V8104	2501	3430	7586	RCA	Nuvistor
V8201 &					
V8202	2501	3430	7586	RCA	Nuvistor
V8203	2501	3450	7587	RCA	Nuvistor
V8204	2501	3430	7586	RCA	Nuvistor

NETWORK

Z8601	8800	2336	peaking	
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ABD



SECTION 6B SPARE PARTS LIST

SPARE PARTS REQUIREMENTS

a. General

The Type 74-13A Calibrated Delaying Sweep Plug-In is an extremely reliable and dependable instrument. Only components thoroughly tested and approved by the engineers of the Quality Assurance Laboratory are used in this instrument. Continued performance tests, environmental and life testing of production units make certain your oscilloscope will give many years of satisfactory service. These new Fairchild oscilloscopes are precision engineered and require no selected parts.

Two lists of "running spares" are included to aid you in periodic maintenance. The running-spare parts lists include recommended quantities and reference symbol numbers. Section 6A of this Instruction Manual gives a complete listing of all components and their recommended vendors so that you may readily procure them from a local supply house or your own stores.

Note: The local Fairchild Scientific Instrument Field Engineering representative and his service organization can assist you in obtaining any additional components in the shortest possible time. To help expedite service, always give the Type Number and Serial Number of the instrument; always specify the part number and give a description of the component (see Section 6A of this manual).

b. 500-Hour Spares (6 months)

The recommended list for one through three units follows.

Electron Tubes

Symbol	Q	uantity
V8101		3
V8103		1

Transistors

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		•••	•••		•••	* *	•	•••			• •		2.3		1		•		×	• •		•			*	'	•
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Diodes

Symbol	Q	vantit
CR8001		13
CR8101		1
CR8113		1
CR8213		1
CR8401		1
CR8601		1
	Lamps	

DS8101 1 DS8301 1

c. 2000-Hour Spares (2 years)

The recommended list for one through five units is given below. Maintain spares indicated plus one for each oscilloscope in use; 2 of each set of the 500-hour spare list given in paragraph (b) plus the quantities listed as follows:

		Capacitor	s	
Symbo	bl	Quantity	Symbo	Quantity
C8001		2	C8219	
C8002		1	C8231	1
C8003		1	C8234	1
C8004		1	C8300	1
C8101		1	C8302	1
C8102		1	C8305	1
C8103		1	C8309	1
C8104		1	C8311	1
C8105		1	C8314	1
C8106		1	C8316	1
C8107		1	C8317	1
C8108		1	C8318	1
C8111		8	C8405	1
C8112		1	C8406	1
C8113		3	C8409	1
C8115		3	C8416	1
C8116		1	C8441	1
C8118		1	C8501	1
C8120		1	C8502	1
C8126		1	C8503	1
C8129		1	C8504	
C8131		4	C8506	1
C8132		1	C8507	
C8134		1	C8508	
C8135		1	C8509	1
C8137		1	C8510	1
C8201		1	C8558	
C8207		. 1	C8559	
			C8563	
			C8607	
			20007	
		lampe		

Symbol Quantity

DS8101	 1
058301	1

Electrical Connectors

J8100		2	5							•	•		•	•		1	
J8401			,	,										,		1	
P8001													,			1	

section 6b – spare parts list

Resistors

Symbo		antity	Symbo	ı q	uantity
R8001		1	R8224		1
R8002		1	R8233		1
R8003		2	R8241		1
R8004		1	R8242		1
R8005		1	R8243		1
R8006		1	R8244		1
R8007		1	R8245		2
R8008		1	R8249		1
R8009		5	R8255		1
R8011		1	R8261		1
R8012		1	R8265		1
R8013		1	R8267		1
R8100		1	R8268		1
R8101		1	R8275		1
P8102		1	P8280		1
R8103		1	R8301		1
R8104		1	R8306		1
P8105		1	R8307		1
P8106		i	P8308		1
P9107	**********************	i	P9300		1
B0100		1	R0307		1
R0100		1	R0310		1
ROIIU		i	ROJII		1
K0111	*****		R0312		i
Koll3		2	K6313		1
K8114	•••••	1	R8314	********	1
K8115		2	R8310		1
K8116		1	R631/		1
K811/		1	K8320		1
R8118		1	R8322		i
R8119		-	R8323		1
R8121		1	R8325		1
R8122		1	R832/		
R8125		1	R8328		1
R8126	•••••	1	R8329		1
R8127	••••••	1	R8333		1
R8128		1	R8334		1
R8129		1	R8337		1
R8130		1	R8338		1
R8132		1	R8339		1
R8133		1	R8340		2
R8134		1	R8343		1
R8135		1	R8347		1
R8136		1	R8348		1
R8140		1	R8349		1
R8141		1	R8355		1
R8143		1	R8402		1
R8144		4	R8403		1
R8148		1	R8404		1
R8149		1	R8406		1
R8150		1	R8408		1
R8151		1	R8409		1
R8153		1	R8410		1
R8154		1	R8411		1
R8155		1	R8412		1
R8159		1	R8413		1
R8160		1	R8414		1
R8161		1	R8415		1
R8162		1	R8416		1
R8163		1	R8417		1
R8164		1	R8418		1
R8166		1	R8419		1
R8169		2	R8421		1
R8171		1	R8429		1
R8173		1	P8441		1
R8174		4	P8442		1
R8179		1	D0445		1
R8170		2	K8445		1
D8101		1	R8501		-
D9100		1	R8502		1
R0102		1	R8503		1
R0200		1	R8504		1
ROZUI	******	1	R8506	*****	1
K8202			R8507		1
R8207		1	R8508		1
R8208		1	R8509		2
R8221		1	R8511		1
R8222		1	R8512		1

Symbol	Quantity	Symbol	Quantity
R8513		R8618	1
R8514	1	R8619	1
R8516	1	R8622	1
R8517	1	R8701	1
R8602	1	R8702	
R8608		R8703	
R8609	1	R8704	1
R8614		R8705	1
R8616		R8706	1
R8617		R8708	1

Transformers

Symbo	bl	Qu	antit
T8101			1
T8601			1
	Swit	ches	

Stock only one of each of the following switches for each 3 units being maintained:

\$810, \$811, \$812, \$813, \$820, \$821, \$822, \$823, \$824, \$830, \$840, \$850, \$851

Note: Should a particular switch receive more than normal use in certain applications, then the quantity stocked of that particular switch should be doubled.

d. Miscellaneous

The following items may be stocked in quantities of one for each 2 units being maintained:

Name	Part Nu	mber
Bushing shaft	4301	0933
Bushing	4301	3581
Microdial	4501	0430
Knob fastener	4501	0431
Knob small #1	4501	2452
Knob knurled around post	4501	2191
Knob skirt	4501	2241
Knob, die case	4501	2261
Knob, the cuse	4501	2271
Knob small $\#1$	4501	2302
Knob medium	4501	2311
Ferrite Beads HY8101		
HY8303 & HY8304	2110	1560
Coil of 18101	2110	1350
Panel, front	3201	3143

e. Summary

The quantities of spare parts given in the preceding paragraphs are intended for industrial and military duty under normal environment and heavy-use conditions. It is suggested that the maintenance engineer evaluate:

1. The conditions under which the instruments will be used.

2. The skill of the maintenance technicians.

3. Other similar items on hand.

4. The effect of procurement time of spares and effects of instrument down-time on your organization.

It is recommended that inventories of spare parts outlined above be adjusted according to the requirements of your own laboratory or plant.

In the first analysis, the factory recommends the availability of spares or standby equipments since extensive life testing of your instrument has shown no higher failure rate for any specific component.

spare parts list – section 6b

LIST OF RECOMMENDED VENDORS

CODE	NAME	
ABD	Du Mont Laboratories	
AER	Aerovox Corporation	
AHH	Arrow-Hart & Hegeman Electric Company	
ALB	Allen-Bradley Company	
ALC	Allied Control	
ALCO	Alco Electronic Products	
ALD	Alden Products Company	
AMA	Amaton Electronic Hardware	
AMP	Amp Inc.	
AMR	Amperite Company, Inc.	
AMX	Amperex Electronics Products, Inc.	
APC	American Phenolic Corporation	
APH	Amphenol Electronics Corporation	
ARC	Arco Electronics Inc. (Elmenco)	
AST	Astron Corporation	
AUT	Automatic Metal Products Corporation	
BEL	Belfuse	
DIN2	Bourns Inc.	
BUR	Burnay Engrg. Company	
CAN	Cannon Electric Company	
CRS	CBS-Hytron Division of CBS	
CDF	Cornell-Dubilier Electric Corporation	
CGW	Corning Glass Works	
СН	Cutler-Hammer, Inc.	
CHC	Chester Cable Corporation	
СНМ	Chatham Electronics	
CIN	Cinch Manufacturing Company	
CLS	Clarostat Mfg. Co., Inc.	
coc	Continental Carbon	
COM	Comar Electric	
COW	Continental-Wirt Electronics Corporation	
CPC	C. P. Clare & Company	
CRL	Centralab, Division of Globe-Union, Inc.	
CST	Chicago Standard Transformer Corporation	
CTC	Cambridge Thermionic Corporation	
CTS	Chicago Telephone Supply Corporation	
DAG	Dage Electric Company, Inc.	
DAL	Dale Products, Inc.	
DEK	Drake Mfg. Company	
ERV	Hugh H Eby Inc	
EDI	Edol Industries	
FIA	Any manufacturer meeting EIA standards	
ELC	Electra Manufacturing Company	
ELD	Eldema Corporation	
EMC	Electro Motive Mfg. Company	
EMW	Elmwood Sensors, Inc.	
ERC	Erie Resistor Corporation	
ESX	Essex Electronics	
FAST	John E. Fast Company	
FCI	Fairchild Camera and Instrument Corporation	
FER	Ferroxcube Corporation of America	
GDE	Good-All Electric Mfg. Company	
GE	General Electric Company	
GEN	General Instrument Corporation	
GEP	General Products Corporation	
GLB	Globe Industries	
CRY	Graubill Inc	
GUD	The Gudeman Company	
НАМ	The Hammarlund Manufacturing Co. Inc.	
in Ann	the frammationa manoracioning co., inc.	

ODE	NAME
HON	Honeywell
HOP	Hopkins Engineering Company
HP	Hewlett-Packard Company
EC	International Electronics Corporation
RC	International Resistance Company
RP	International Rectifier Corporation
TT	ITT Components Division
JEF	Jeffers Electronics, Inc.
JHN	E. F. Johnson Company
WM	J. W. Miller Company
KUL	Kulka Electric Mfa. Co. Inc.
XM	Klixon Metals and Control Corporation
ED	Ledex Inc.
EE	Leecraft Mfg. Company
FI	Littlefuse. Inc
IN	Line Electric
MAI	P. R. Mallory & Company, Inc.
NCR	Micro Switch (Division of Minneapolis-Honeywell
nen	Regulator Co.)
MIC	Micamold Electronics Mfa Corporation
ALL	Miller Electric Company
MOT	Material Semiconductor Products Inc
MOV	Moloroid company Itd
ALIC	Muson Corporation
ALIT	The Muter Company
NUT	New York Transformer Company
	Oak Mia Company, Inc.
UAK	Dhiles Company
PHC	Philips Electronic Tube Division
	Philips Electronic Tube Division
PLS	Plastola Corporation
POT	Potter & Brumfield, Inc.
PRC	Precision Resistor Co., Inc.
PYR	Pyramia Electric Company
RCA	Radio Corporation of America
RMC	Radio Materials Corporation
ROY	Royal Electric Corporation, Inc.
RTN	Rotron Mtg. Company
SIG	Signalite Inc.
SIL	Silicon Transistor Corporation
SLT	Sealectro Corporation
SOL	Solitron Devices, Inc.
SPG	Sprague Electric Company
STC	Stackpole Carbon Company
STW	Standard Winding Company
SUM	Summit Coil Company
SWW	Stanwyck Winding Company
SYL	Sylvania Electric Products, Inc.
SYN	Syntronic Instruments, Inc.
TEC	Transistor Electronics Corporation
TEX	Texas Instruments, Inc.
THC	Thermal Control, Inc.
TOR	Torrington Mfg., Company
TRS	Tresco, Inc.
TRU	Tru-Ohm Products
TUG	Tung-Sol Electric Inc.
UCN	Ucinite Company
UTC	United Transformer Company
VIC	The Victoreen Instrument Company
WDE	Wood Electric Corporation
WDL	Ward Leonard Electric Company
WES	Weston Electrical Instrument Corporation
WYN	Welwyn International Inc.
15.02 (2020)2)	

INSTRUMENT WARRANTY AND SERVICE NOTICE

SERVICE

WARRANTY

The Instrumentation Division warrants that each new Cathode-ray Oscilloscope, Automotive Test Equipment, and other Electronic or Electrical Test or Measuring Equipment (hereinafter referred to as "Instrument") manufactured or sold by it, is free from defects in material or workmanship under normal use and service for a period of one year from the date of its sale to the first purchaser for use. If, upon examination by Fairchild, the Instrument is determined to be defective in workmanship nor shall Fairchild be hable for damages by reason of the failure of the Instrument to perform properly or for any consequential damages. This warranty does not apply to any Instruction that has been subject to negligence, accident, misuse or improper installation or that in any way has been tampered with, altered or repaired by any person other than an authorized Fairchild service organization or an employee thereof, at to any Instrument whose serial number has been altered,

behalt of Fairchild or impose any obligation upon it in connection with the sale of any Instrument, other than as stated above.

REGISTERING THE WARRANTY

To register this warranty, the enclosed warranty registration card must be properly filled out and mailed to the Instrument Service Department immediately upon receipt of the equipment. Complete information is necessary. BOTH THE TYPE NUM-BER AND THE SERIAL NUMBER OF THE IN-STRUMENT MUST BE GIVEN ON THIS CARD. Instruments must be examined immediately upon receipt, since claims for damage in transit will not be honored by the carrier unless prompt action is taken.

CHANGES IN SPECIFICATIONS

The right is reserved to change the published specifications of equipment at any time and to furnish merchandise in accordance with current specifications without incurring any liability to modify equipment previously sold, or to supply new equipment in accordance with earlier specifications excepting under the classification of special apparatus.

In order to insure service under our warranty, ment is determined to be defective in workmanship or material, Fairchild will, subject to the conditions set forth below, either repair the detective part by replace it with a new part. Fairchild shall not be liable for any delay or failure to furnish a replace ment part resulting diffectly or indirectly from any governmental restriction, priority or allocation or any other governmental regulatory order, or action, nor shall Fairchild be hable for damages by reason equipment must also be given. In this way, much time can be saved and unnecessary inconvenience often avoided. When writing to the factory in this requect, address: DEPT

CIT Fairchild Camera and Instrument Corp. CIT Instrumentation Division's AFTER RECEIPT ENSUESomerset Place, Clifton Wew Jersey

The InstrugenAlservice Department will then This supertantly shall, at Fairchild's water be-comet word unless provided betw. This warranty is in lieu of all other intranties, expressed or implied, and no one is authorized to assume any liability of behall of Fairchild

nent from the factory, always give the Type number and Serial number of the Instrument. Before ordering parts for in-warranty replacement or purchasing them for out-of-warranty replacement, be sure to consult the Parts List in the Instruction Manual. The Parts List gives the values, tolerances, ratings, and Fairchild part number for all electrical components used in the Instrument. This will help to expedite service.

PATENT NOTICE

Manufactured under one or more U.S. Patents owned or controlled by Fairchild Camera and Instrument Corporation. 50 Somerset Place, Clifton, New Jersey, U.S.A. Patent Numbers supplied upon request.



RESISTANCE VALUES ARE IN OHMS; K.THOUSAND, M.MILLION. 2. CAPACITANCE VALUES ARE IN OF UNLESS OTHERWISE SPECIFIED. 3. SERVICE ADJUSTMENT.

4. O FRONT PANEL SCREWDRIVER ADJUSTMENT.

ES:



SHEET 1 OF 7

NORMAL AND DELAYING SWEEP GENERATOR



SHEET 2 OF 7

DELAYED TRIGGERING CIRCUIT



SHEET 3 OF 7



TYPE 74-13A DA SWEEP GENERATOR AND STROBE CIRCUIT

SHEET 4 OF 7



4. I HEAT SINK.

2. CAPACITANCE VALUES ARE IN of UNLESS OTHERWISE SPECIFIED. 3. Ø SERVICE ADJUSTMENT.

Preset front-ponel

Control

TRIGGERIN

TIME/DIV

VARIABLE

POSITION

3. Voltage tole ground.

5. Use Type 765

to 25 Mc

nominal

DISPLAY LOGIC

NOTES: I. RESISTANCE VALUES ARE IN OHMS; K-THOUSAND, M-MILLION.



HORIZONTAL DEFLECTION AMPLIFIER

SHEET 5 OF 7

^{*} Install R8350 30 sr Resistor if not in unit



TYPE 74-13A NDT AND DA TIME/DIV SWITCHES

SHEET 6 OF 7



TYPE 74-13A UNBLANKING AMPLIFIERS AND CONNECTORS

"o ° u



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IF

ANGLE OF THROW

DISPLAY LOGIC WAFERS

(\$840)

28

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