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Star features ** TRANSCENDENT 2000 — Although only

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This versatile modular mixer, featured as a constructional article in Practical Electronic can be built up to a maximum of 24 inputs 4 outputs and an auxillary channel. Each input channel has Mic and Line inputs, variable gain, bass and treble controls and a parametric middle frequency equalizer. There are send and return jacks, auxiliary, pan and fader controls and output and group switching. The output channels have PPM displays and record and studio outputs. The auxiliary channel also has a PPM display and there is a headphone monitor jack and a built-in talk-back microphone. The mixer modules plug into base units each of which takes up to 6 channels. To eliminate hum, the power supply is in a separate cabinet

KIT PRICES

Input channel Output channel Auxiliary channel Blank Panel

£27.50 Base unit and wooden front £18.50 Pair of mahogany end cheeks £12.50 £22.50 Power Supply and capinet £3.00

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SP2 200 twice the power with two of the reliable, durable and economic amps from the MPA 200 fed by separate power supplies from a common foroidal franformer Superb linish and quality components throughout. oupero linish and quality components throughout— up to (even over) the standard of high prices factory-built units! Complete kit £64.90 + VAT

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FEATURES

SINCLAIR POCKET TV 28 Vivian Capel gets out his magnifying glass to give you the low down on Sinclair's 2" portable.

TECH TIPS 50
Pass it on!

Due to lack of space, the fourth part of Bob Bennett's series on Machine Code Programming has been held over until next month.

PROJECTS

VECTOR GRAPHICS 19
What has Phil Walker designed for us this month? Join the dots and find out!

EM DAMES LANGE AND

MODULAR PREAMP 55
Barry Porter continues his series on hi-fi by numbers.

A white flag flutters amidst the rubble of what was once 145 Charing Cross Road. The ETI staff, armed only with rolled-up assembler listings, have finally admitted defeat at the hands of the invading hordes. OK, we give in. Here it is, the complete listing, along with some further notes by Mike Bedford.

INFORMATION

## WATFORD ELECT 33, CARDIFF ROAD, WATFORD, HERT Tel. Watford (0923) 40588. Telex ORDERS NORMALLY DESPATCHED B. ### WATFORD HERT Tel. Watford (0923) 40588. Telex ORDERS NORMALLY DESPATCHED B. ### WATFORD HERT WATFORD HERT HERT HERT HERT HERT HERT HERT HERT	S WD 1 8ED, ENGLAND 8956095 WAELEC Y RETURN OF POST NTEED. SEND CASH, P.O.'s OR CHEOUE JIDNS OFFICIAL ORDERS ACCEPTED 10 EXPORT INQUIRY WELCOME P & P. 10 EXPORT INQUIRY INDUIRY INQUIRY I	AD1612 42 5C58C AF183 40 5C58C AF183 40 5C58C AF183 55 5C70 BC10778 10 5C771 BC1078 11 801312 BC108B 14 801312 BC109C 14 80132 BC109C 14 80138 BC109C 10 8028B BC1078 10 BF244 BC1079C 10 BF246 BC1079C 10 BF256 BC2174 10 BF257 BC2174 10 BF257 BC2077B 14 BSX20 BC307B 14 BSX20 BC308B 16 BU105 BC337/B 15 BU205	MUESID 74 MUESID 74 MUESID 74 MUESID 70 MUESID	TIPIEST 105 TIPIEST 105 TIPIEST 105 TIPIEST 120 TIPIES	102904A/05A/ 25C1923 20
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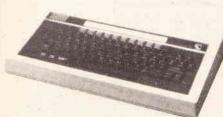
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★ Programming voltage selector switch is provided with a safe position.

★ Warning indicator to show programming in progress.

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(Grey/meter)

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50-way	200p
64-way	280p

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AN ARGUS SPECIALIST PUBLICATION

THE-MINI-MYNAH

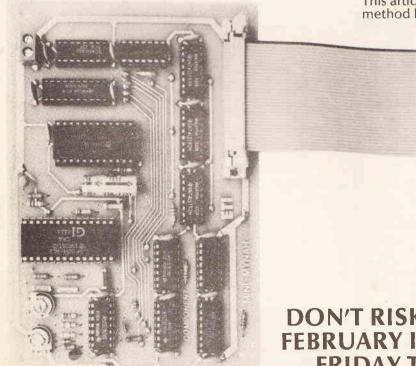
In our long-standing tradition of first-rate projects with third-rate puns for titles, here's our project for a speech synthesiser board. Its long list of features includes unlimited vocabulary from the use of allophone speech synthesis; four levels of inflection (we don't know of any other published design that allows inflection); 2K of on-board memory dedicated to speech generation, which allows the board to store 100 or more words; speech reproduction words, phrases or sentences stored in the memory selectable by a single command from the host computer; and simple interfacing requirements. So don't even think about building another design until you've seen ours!

BENCH PSU

One of the necessities of any experimenter's life is that of having to supply power for projects. Here is a supply that could be purpose built for electronics enthusiasts — in fact, it is purpose built by electronics enthusiasts! Output voltages are adjustable, but are nominally 5V at 2.5A and + and - 15V at 0.5A. And what's more, a full kit will be available, so start saving your pennies now!

MORE MEMORY FOR Z80 COMPUTERS

Following on from the project for a 6502/6800 64K DRAM board published in September 1983, we look at ways of increasing the available memory capacity of some common-or-garden Z80 computers. There are basically two methods — upgrading the existing memory, by substituting higher capacity DRAMs, and building a separate card with a block of memory on it. This article will look at the first, with the second method looked at in a future issue.



DON'T RISK MISSING OUT ON THE FEBRUARY ISSUE OF ETI — ON SALE FRIDAY THE 6TH OF JANUARY

Articles described here are in an advanced state of preparation. However, circumstances may dictate changes to the final contents.

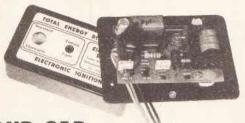
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We challenge any manufacturer to publish better performance figures. Before you buy any other make, ask for the facts, its probably only an inductive system. But if an inductive system is

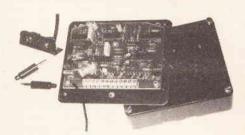
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HOW SAFE IS YOUR CAR?

More and more cars are stolen each week and even a steering lock seems little help. But a car thief will avoid a car that will cause him trouble and attract attention. If your car has a good alarm system—well there are plenty of other cars to choose from.

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- MINIATURE KEY PLUG A miniature jack plug attaches to your key ring and is coded to your particular alarm.
- ★ 2025 INDIVIDUAL COMBINATIONS. The key plug contains two 1% tolerance resistors, both must be the correct value and together give 2025 different combinations.
- ★ ATTRACTS MAXIMUM ATTENTION This alarm system not only intermittently sounds the horn, but also flashes the headlight and prevents the engine being started.
- ★ 60 SECOND ALARM PERIOD Once triggered the alarm will sound for 60 seconds, unless cancelled by the key plug, before resetting ready to be triggered again.
- ★ 30 SECOND EXIT DELAY The system is armed by pressing a small button on a dashboard mounted control panel. This starts a 30 second delay period during which the owner can open and close doors without triggering the alarm.
- ★ 10 SECOND ENTRY DELAY When a door is opened a 10 second delay operates to allow the owner to disarm the system with the coded key plug. Latching circuits are used and once triggered the alarm can only be cancelled by the key plug.
- L.E.D. FUNCTION INDICATOR An LED is included in the dashboard unit and indicates the systems operating state. The LED lights continuously to show the system is armed and in the exit delay condition. A flashing LED indicates that the alarm has been triggered and is in the entry delay condition.
- ACCESSORY LOOP BONNET/BOOT SWITCH IGNITION TRIGGER These operate three separate circuits and will trigger the alarm immediately, regardless of entry and exit delays.
- * SAFETY INTERLOCK The system cannot be armed by accident when the engine is running and the car is in motion.
- LOW SUPPLY CURRENT CMOS IC's and low power operational amplifiers achieve a normal operating current of only 2.5 mA.
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ч	22 μF	16	6р
	22 µF	25	6р
	22 µF	631	9р
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	47 µF	25	8p
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1N4006	6р
1N4007	6р
1N5401	11p
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DIGEST

New HP Research Centre In UK

A ta press launch attended by the Secretary of State for Trade and Industry, Norman Tebbit, TV cameras and your very own editor, Hewlett Packard announced that they will be opening a new research laboratory in Bristol, to serve as their European Research centre. The company's main laboratories are in Palo Alto, California, and the new laboratory will be the company's first R&D establishment outside the USA.

The company will be commencing recruiting in the very near future, and the lab will be open in

the Spring of 1984 with around 50 research staff initally, rising to 200 by 1987.

According to HP's UK managing director, David Baldwin, the exact research objectives of the laboratory have yet to be decided, but will be in computing science. There will definitely be no semiconductor research.

David Baldwin and Norman Tebbit were very coy about the financial inducements that had been offered to make the company choose the UK (apparently, just about every country in the world had also been under consideration). However, they denied that the prospect of government grants had been a major factor in the choice sufficiently often to make all the cynical journalists present convinced that it must have been.

However, the company's line was that the availability of well qualified graduates (despite the cut-backs in the technological universities such as Salford) and the excellence of the UK's universities (despite the cut-backs in technological universities such as Salford) were amongst the reasons — as was the apparent presence, on the M4 corridor, of the world's highest concentration of technical expertise.

Mr Baldwin stated that, with a few tax rule changes here and there, the establishment of the laboratory could lead to a large amount of money going to the UK universities in the form of research and equipment grants. HP currently spends around \$25m or more in this way in US Universities. The laboratory will also pro-

vide sufficient space for visiting researchers from Universities (and, presumably, Polys) to come and work on site.

HP reckon that for every project researched, there will be 50 other people employed by the company elsewhere, such as in production, marketing, etc, and therefore one could expect the research centre to generate around an additional 10,000 jobs given time. Obviously, there is absolutely no guarantee that these jobs will be generated in the UK, although according to a company representative, it would be more likely than if the lab had been sited in W. Germany.

One interesting feature is that although the first head of the laboratory will be an American, Donald L. Hammond who is currently head of the physical research centre at Palo Alto, one of his tasks will be to appoint a British successor. All those interested should join the editor in writing to Hewlett Packard Ltd, Nine Mile Ride, Wokingham, Berkshire RG11 3LL.

World's Thinnest Transformer

The latest transformer in the OB range from Avel-Lindberg stakes a claim as the thinnest yet, because, at 0.8VA, it is less than 10.5mm high (0.413in.) and will fit inside the smallest card frames. Dual primaries for 240 or 120V AC 50/60Hz mains operation are complemented by twin centretapped secondaries which give output voltages from 10V at 80mA to 48V at 17mA in series and 5 to 24V in parallel. These miniature transformers are prooftested at 5kV a.c. and have a maximum operating temperature of

120°C (Class 2). They conform to IEC 65 Class 2, B.S.415 class 2 and VDE 0550 Class 2.

The normal method of fixing to a printed circuit board would be to direct solder the connecting pins, but where extra mechanical strength is required, the transformer can be screwed to the board using four holes moulded into the resin-filled, flat thermoplastic cases. The non-concentric twin primary and secondary windings are wound on separate bobbins which gives maximum isolation and low inter-winding capacitance. The secondaries can be series, parallel or independently wired, but if they are isolated from each other the applied potential between them must not exceed 500 V DC. The transformer is also short-circuit proof, Avel-Lindberg Limited, South Ockendon, Essex RM15 5TD, tel 070 885 3444.



Prize Tester

Fieldtech Heathrow are so contial of their LC53 Z-meter that they are running a free entry Autumn Sweepstake to promote the product with the Z-meter itself, valued at well over £550, as the prize. The unit is unique because it will dynamically test capacitors,

coils, SCR's and TRIAC's and, it is claimed, will find 75% of defective capacitors which value only meters will miss.

The LC53 tests capacitors for leakage current under full load with up to 600 volts applied, checks capacitor dielectric absorbtion, and has the capability to reform electrolytics. It will check for all coil defects in or out of circuit, and it automatically tests coils for effective Q using a US patent ringing test. It tests transmission lines for distance to open or short circuits within feet and it will also test dielectric strength to 600 volts.

For further details of the instrument and the sweepstake, contact Mike Dawson, Fieldtech Heathrow Limited, Huntavia House, 420 Bath Road, Longford, Middlesex UB7 OLL, tel 01-897

Plastic Shorts

N ext time you investigate a defunct piece of electrical equipment and come across a resistor which appears to have gone short circuit, look again. That resistor may not be a resistor at all.

A system which is rapidly gaining acceptance within the electronics industry involves using mire links with plastic bodies to join tracks on printed circuit boards. The plastic body is usually

about the same size as that of a small resistor or diode and may, therefore, depending upon its colour, give rise to confusion in the minds of the unsuspecting.

The idea behind the use of these links is quite simple. PCB designers often need to link tracks on a board in circumstances which do not justify the use of a double sided board. The usual solution is to use wire links, but these have to be cut and inserted by hand, an expensive procedure especially where automatic insertion equipment is being used to mount the other components. Pre-formed plastic-bodied links

can be handled by the insertion equipment just as though they were conventional resistors, and even where boards are assembled by hand are quicker to insert than lengths of wire. The only restriction is that the pads on the PCB must be made the correct distance apart to accept the preformed leads, but since this already applies to just about every other component commonly used on PCBs there are no problems. Some companies use a number of standard lengths, eg 10, 15 and 20 mm, thus easing the task of the PCB designer.

In the past, companies have

produced their own links or had them made to their own requirements. As the idea has caught on, however, a few companies have entered the market with preformed links. One of these is Nortronic, who call their products Zerohm Resistors. They are indeed about the size of a small resistor and have a brown body with yellow banding. Nortronic claim that they are chip resistant and have British Telecom approval. Nortronic Associates Limited, Gateway, Drew Industrial Estate, Crewe, Cheshire CW1 1YY, tel 0270 586161.



MULLARD SPEAKER KITS

Purposefully designed 40 watt R.M.S. and 30 watt R.M.S. a ohm speaker systems recently developed by MULLARD'S specialist team in Belgium. Kits comprise Mullard woofer (8" or 5") with foam surround and aluminium voice coil, Mullard 3" high power domed treeter. B.K.E. built and tested crossover based on Mullard circuit, combining low loss components, glass fibre board and recessed foudspeaker terminals. SUPERB SOUNDS AT LOW COST. Kits supplied in polystyrene packs complete with instructions, 8" 40W system — recommended cabinet size 240 × 216 × 445mm

× 216 × 445mm Price £14.90 each + £2.00 P & P. 5" 30W system — recommended 160 × 175 × 295mm Price £13.90 each + £1.50 P 8 P. dod cahinet eize

Designer approved flat pack cabinet kits, including grill fabric. Can be finished with iron on veneer or self adhesive vinyl etc.

8" system cabinet kit £3.00 each + £2.50 P & P. 5" system cabinet kit £7.00 each + £2.00 P & P.



No so LOUDSPEAKER

The very best in quality and value.

Ported tuned cabinet in hard-wearing black vynide with protective corners and carry handle. Built and tested, employing 10in British driver and Piezo tweeter. Spec: 80 watts RMS; 8 ohms; 45Hz-20KHz; Size: 20in x 15in x 12in; Weight: 30 pounds.

Price: £49 00 each £90 per pair Carriage: £5 each £7 per pair

BK ELECTRONICS

Prompt Deliveries VAT inclusive prices **Audio Equipment Test Equipment** by Thandar

and

Leader

HOBBY KITS. Proven designs including glass fibre printed circuit board and high quality components complete with instructions.

FM MICROTRANSMITTER (BUG) 90/105MHz with very sensitive microphone. Range 100/300 metres. 57 x 46 x 14mm (9 volt) Price: £7.99p

DIGITAL THERMOMETER -9.9 C to 4-99.9 C. LED display. Complete with sensor 70 x 70 mm (9 volt) Price: £27.60p 3 WATT FM TRANSMITTER 3 WATT 85/115MHz varicap con-

mm (12 voit) Price: £12.49p
SINGLE CHANNEL RADIO CONTROLLED TRANSMITTER/
SINGLE CHANNEL RADIO CONTROLLED TRANSMITTER/
RECEIVER 27 MHZ Range up to 500 metres. Double coded modulation. Receiver output operates relay with 2amp/240 voit contacts, Ideal for many applications. Receiver 90 x 70 x 22 mm 9/ 12 volt) Price: £16,49 Transmitter 80 x 50 x 15 mm (9/12 volt) Price £10,29 P&P All Kits +50p, S,A,E, for complete list.



3 watt FM



STEREO CASSETTE TAPE **DECK MODULE**

DECK MODULE

Comprising of a top panel and tape mechanism coupled to a record/play back printed board assembly. Supplied as one complete unit for horizontal installation into cabinet or console of own choice. These units are brand new, ready built and tested.

Features: Three digit tape counter. Autostop. Six piano type keys, record, rewind, fast forward, play, stop and eject. Automatic record level control. Main inputs plus secondary inputs for stereo microphones. Input Sensitivity: 100mV to 2V. Input Impedance: 6BK. Output level: 400mV to both left and right hand channels. Output Impedance: 10K. Signal to noise ratio: 45dB. Wow and flutter: 0.1%. Power Supply requirements: 18V DC at 300mA. Connections: The left and right hand stereo inputs and outputs are via individual screened lead, all termination with possible complete with circuit diagram and connecting supplied complete with circuit diagram and connecting Supplementary parts for 18V DC, power supply fittansiformer, bridge rectifier and smoothing capacitor!

LOUDSPEAKERS POWER RANGE

THREE QUALITY POWER LOUD-SPEAKERS (15", 12" and 8" See Photo), Ideal for both Hi-Fi and Disco applica-

Ideal for both Hi-Fi and Disco applica-tions. All units have attractive cast alu-minium (ground finish) fixing escutcheons Specification and Prices.

15" 100 watt R.M.S. Impedance 8 ohms 50 oz. magnet 2" aluminium voice coil. Res. Freq. 20 Hz. Freq. Resp. to 2 SKHz. Sens. 97dB. Price: £34,00 each +£3,00 P&P. 12" 100 watt R.M.S. Impedance 8 ohms. 50 oz. magnet 2" aluminium voice coil. Res. Freq. 25Hz. Freq. Resp. to 4 KHz. Sens. 95dB. Price: £24,50 each +£3,00 P&P. 8" 50 watt R.M.S. Impedance 8 ohms. 20 oz. magnet. 1½" aluminium voice coil. Res. Freq. 40Hz. Freq. Resp. to 6 KHz. Sens. 92dB. Black Cone, Price: £9,50 each Also available with black protective grille Price: £9,99 each. P&P £1.50.



12" 85 watt R.M.S. McKENZIE C1285GP (LEAD GUITAR, KEYBOARD, DISCO) 2" aluminium voice coil, aluminium centre dome, 8 ohm imp., Res. Freq. 45Hz., Freq. Resp. to 6.5KHz., Sens, 98dB. Price: £23.00 + £3 carriage.
12" 85 watt R.M.S. McKENZIE C1285TC (P.A., DISCO) 2" aluminium voice coil. Twin cone. 8 ohm, imp., Res. Freq. 45Hz., Freq. Resp. to 14KHz. Price £23 + £3 carriage.
15" 150 watt R.M.S. McKENZIE C18 (BASS GUITAR, P.A.) 3" aluminium voice coil. Die cast chassis, 8 ohm imp., Res. Freq. 40Hz., Freq. Resp. to 4KHz. Price: £47 + £4 carriage.

PIEZO ELECTRIC TWEETERS – MOTOROLA

Join the Piezo revolution. The low dynamic mass (no voice coil) of a Piezo tweeter produces an improved transient response with a lower distortion level than ordinary dynamic tweeters. As a crossover is not required these units can be added to existing speaker systems of up to 100 watts (more if 2 put in series). FREE EXPLANATORY LEAFLETS SUPPLIED WITH EACH TWEETER.

TYPE 'A' (KSN2036A) 3' round with protective wire mesh, ideal for bookshelf and med sized Hi-fi speakers. Price £4.29 each. TYPE 'B' (KSN1005A) 3%" super horn. For general purpose speakers, disco and P.A. systems etc., Price £4.99 each.

TYPE 'C' (KSN6016A) $2^{\prime\prime}\times 5^{\prime\prime}$ wide dispersion horn. For quality Hi-fi systems and quality discasetc. Price £5.99 each.

TYPE 'D' (KSN1025A) 2" × 6" wide dispersion horn. Upper frequency response retained extending down to mid range (2KHz). Suitable for high quality Hi-ff systems and quality discos. Price £7.99 each.

TYPE 'E' (KSN1038A) 3%" horn tweeter with attractive silver finish trim Suitable for F monitor systems etc. Price £4.99 each.

TYPE 'F' (KSN1057A) Cased version of type 'E'. Free standing satellite tweeter. Perfect add on tweeter for conventional loudspeaker systems. Price £10.75 each

P&P 20p ea. (or SAE for Piezo leaflets).

POWER AMPLIFIER MODULE

BSR P256 TURNTABLE

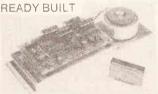
P256 turntable chassis © S shaped tone arm

8 Belt driven © Aluminium platter ©
Precision calibrated counter balance © Antiskate ibias device! © Damped cueing lever

240 volt AC operation (H2) © Cut-out
template supplied © Completely manual arm
This deck has a completely manual arm and is
designed primarily for disco and studio use
where all the advantages of a manual arm are

required.

Price £31.35 each £2.50 P&P.



New model. Improved specification NEW OMP100 Mk.II POWER AMPLIFIER MODULE Power Amplifier Module complete with integral heat sink, toroidal transformer power supply and glass fibre p.c.b. assembly incorporates drive circuit to power a compatible LED. Yu meter. New improved specification makes this amplifier ideal for P.A., Instrumental and Hi-Fi applications. SPECIFICATION.

Output Power:— 110 watts R.M.S.
Loads:— Open and short circuit proof 4/16 ohms.

Frequency Response:— 15Hz - 30KHz -3dB.
T.H.D.:— 0.01%.
S.N.R. (Unweighted):— -118dB ±3.5dB
Sensitivity for Max Output:— 500mV @ 10K.
Size:— 360 x 115 x 72 mm Price:— £31.99 +
£2.00 P&P. Vu Meter Price:— £7.00 + 50p P&P.

MOSFET versions available up to 300W. R.M.S

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Control Unit — Houses microwave radar unit range
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output Housed in a tamper-proof heavy duty metal

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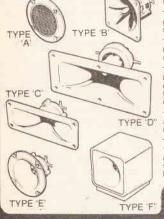


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OMP PROMIX MONO DISCO MIXER (As illustrated), 4 Inputs: -2 Mag. Disc. 1 Aux. plus Mic. with override. Active bass and trebie tone cont's. Individual level controls plus master volume. Monitor output (headphone) for all inputs. Output, 775 mV Supply 240Vac. Size: 19" x 514" x 2½".

Price: £49.99 +£2.00 P&P

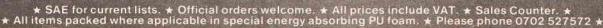
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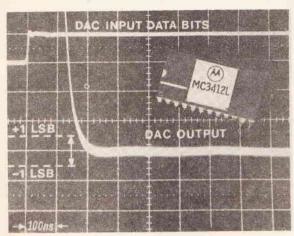
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High-Speed 12-bit D to A

otorola has introduced a high-speed 12-bit digital to analog converter, the MC3412/3512, which uses monolithic bipolar and thin film resistor technology to provide high stability and fast settling time, and which is designed to work with a minimum of external components.

Active laser trimming of thin film resistors at wafer level gives guaranteed limits of gain and offset errors of \pm 0.25% FSR (full scale range) and \pm 0.05% FSR respectively without external adjustment. Monotonicity is guaranteed over the full temperature range and an innovative bit switching scheme ensures that settling time will be no greater than 400 ns

to ± ½ LSB.

The converter includes an internal precision 10 volt bandgap reference and span/bipolar offset resistors. With the addition of one external op-amp, the precision span and bipolar offset resistors provide calibrated unipolar or bipolar full scale output voltage ranges of 0 to 5.0, 0 to $10, \pm 2.5, \pm 5.0$ and ± 10 volts. A CMOS/TIL threshold control pin permits selection of either CMOS or TIL logic levels at the data inputs.

Packaged in a 24-pin ceramic DIP, the MC3412/2512 is pin-compatible with the popular AD563 and AD565 digital to analog converters, and is available in commercial and military temperature ranges. For further information contact Motorola Ltd., European Literature Centre, 88 Tanners Drive, Blakelands, Milton Keynes MK14 5BP, tel 01-352 0041 ext 34.

Single Chip Data Acquisition Controller

All the functions required for intelligent data acquisition and signal monitoring are contained in the CY600 Analog/ASCII Data Acquisition Controller which is being introduced by Weyfringe. The chip is designed to be placed between A/D converters and an 8-bit host computer system.

When programmed, each CY600 channel will scan one or more A/D signals and inform the host when specified conditions are met, freeing the host system from signal monitoring tasks. The minimum CY600 contains two channel buffers which can be programmed with the instructions and conditions to be monitored. Each channel is assigned six registers to hold user defined cons-

tants, A/D readings, or the results of arithmetic computations. Each channel can monitor its own signals or access any other channel's registers (cross channel correlation) so the device can test for several conditions by using different instructions in each channel. The maximum version of the CY600 is given up to four channels with larger program buffers and eleven registers per channel by adding an 8156 memory and I/O expansion chip.

The CY600 commands control the A/D converters, select channels and register and peform arithmetic operations (+, -, /) and conditional tests (<, =, >). Expressions combining all of the above provide comparisons of the signals and registers so that if a specified condition arises, the CY600 interrupts the host, and the host may then query the CY600 to determine the cause of the interrupt. For further information contact Mr Harry Gleghorn, Weyfringe Limited, Longbeck Road, Marske, Redcar, Cleveland TS11 6HQ, tel 0642 470121.

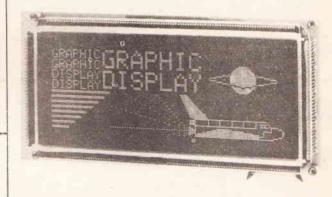
32K Byte DRAM

ostek Corporation have introduced a 256K DRAM which they claim is the first on the market with 32K x 8 organisation. The MK4856 is produced using scaled NMOS technology which allows access times down to 100 ns. The address system is not multiplexed and Mostek say that this will eliminate the need for system logic and thus simplify timing. The device also has an integral refresh counter, further reducing external logic count. The 28 pin DIP version has the standard pinout and is available in plastic (N suffix) or ceramic (P suffix) form and a leadless chip carrier version (E suffix) is also available. The MK4856 is available with access times of 100 ns, 120 ns, or 150 ns and further information can be obtained from Mostek UK Ltd, 1 Valley Drive, Kingsbury Road, London NW9, tel 01-204 9322.

Microwave Amplifiers

N EC have introduced two new ICs which are claimed to offer a constant 16 dB gain from DC to 1.2 GHz. The MM765 and MM766 have built in temperature compensation to ensure stable bias and have an input and output impedance of 50 ohm, allowing devices to be cascaded where higher levels of gain are required. The MM765 operates at 10V and can be supplied in 8-pin or TO-33 packages, while the MM766 operates at 5V and is available in DISK-mold, 8-pin MINI, 8-pin DIP, and TO-72 packages.

Also new from NEC are a series of silicon NPN epitaxial transistors which offer up to 9 dB of gain at 1 GHz and have a noise degradation figure of 1.1 dB. The NE-856 series have a high current capability and come in four package styles including TO-92 and SOT-23. NEC Electronics UK Ltd, 116 Stevenson Street, New Stevenson, Motherwell ML1 4LT, tel 1698 732221.



Dot-Matrix Displays

nineteen new models of planar gas discharge (PGD) flat-panel, dot-matrix display subsystems have been introduced by Beckman Instruments. The displays, which complement the current one-line Beckman displays, enable large amounts of information to be presented where space is limited.

DC planar gas display technology produces high visibility yellow-orange light emission on a high-contrast black background. The height of the light emitting area is from 0.24 to 3.7 in and the width from 4.8 to 8.7 in. The full-controller versions interface using a standard 8-bit parallel microprocessor data bus. The alpha-

numeric units provide drivers, refresh RAM, a character generator and editing features, depending on model, allowing the user to display 5 x 7 dot matrix characters. The graphic units do not contain a character generator but allow each dot to be individually addressed so that characters and graphic patterns can be created with unlimited flexibility.

The driver-only versions provide cathode and anode drivers, the user having to supply external scanning and drive signals and design the controller with a data interface, character generator and refresh RAM.

The panels, fully garanteed by Beckman for one year, are available in the UK from Beckman Instruments Ltd, Milen House, 11 Wagon Lane, Sheldon, Birmingham B26 3DU, tel 021-742

₹Rapid ₹Flectronics

MAIL ORDERS: Unit 1, Hill Farm Industrial Estate, Boxted, Colchester, Essex CO4 5RD. **TELEPHONE ORDERS:** Colchester (0206) 36412.



VISA

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		40	The same of		and the	Series.		-		
LINEAR 555CMOS SO 556CMOS 150 709 25 709 25 749 14 748 35 8400CJ 350 AV-3-1270 720 AV-3-8912 540 CA3080 65 CA3080 190 CA3080A0 376 CA3080 85 CA3140E 36 CA3181E 100 CA3181E 200 CA3181E 200 CA3184 280 CA3185 280 CA3186 280	ICL7106 ICL7611 ICL7621 ICL7622 ICL8038 ICL8211A ICM7224 ICM7565 P-LF361 LF386 LM10 LM301A LM311 LM311 LM318 LM324 LM335Z	580 95 180 180 295 295 200 785 80 45 85 90 325 25 120 30 120 125	LM339 LM348 LM358 LM377 ▶LM381 LM382 LM381 LM386 LM383 LM709 LM312 LM387 LM393 LM709 LM711 LM725 LM741 LM747 LM745 LM747 LM745 LM747 LM747 LM747 LM749 LM387	40 60 50 75 120 120 130 90 120 40 25 60 350 75 14 60 200 45 75	LM3911 LM3914 LM13914 LM13600 MC1498 MC3340 MF100N ML922 ML924 ML926 ML926 ML926 ML928 NL9	120 225 225 106 68 135 350 400 195 210 140 140 140 140 225 140 205 140 210 140	NE566 ▶ NE567 ▶ NE570 NE571 ▶ RC4136 ▶ RC4458 S L480 S L490 S L76018 ▶ SN76477 SP8629 TBA120 TBA820 TBA850 TDA1028 ▼ TDA1024 TL062	140 100 370 370 55 40 170 250 150 380 250 70 75 96 70 220 320 2490 125 40 60	TL064 TL071 TL072 TL074 TL074 TL081 TL084 TL1084 TL170 UA2240 ULN2004 XR2206 ZN414 ZN424 ZN425E ZN424 ZN425E ZN426 ZN427E ZN428E ZN427E ZN428E ZN427E ZN434E	96 30 45 95 25 45 90 50 120 70 70 290 80 135 135 350 600 410 285 200
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225	▶NE570	370		45
105	NE571	370	TL074	95
68	▶RC4136	55	▶TL0B1	25
135	▶RC4558	40	TL082	45
350	SL480	170	TL084	90
400	SL490	250	TL170	50
195	SL76018	150	UA2240	120
210	▶SN76477		ULN2003	70
	SP8629			
140		250	ULN2004	70
140	TBA120S	70	XR2206	290
140	TBA800	75	ZN414	80
140	TBA810	96	ZN423	135
465	TBA820	70	ZN424	135
225	TBA950	220	ZN425E	350
140	TDA1008	320	ZN426E	300
205	▶TDA102		ZN427E	600
16	TDA1024	125	ZN428E	410
45	TL061	40	ZN459	285
110	TL062	60	ZN1034E	200
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P298	55 ZTX		14 ▶ 2N37	

CABLES		
20 metre pack single co	эге	connect-
ing cable ten different of	col	ours. 75p
Speaker cable	Ψ.	10p/m
Standard screened	8	16p/m
Twin screened	9	24p/m
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10 way rainbow ribbon	1	26p/ft
20 way rainbow ribbon	1	47p/ft
10 way gery ribbon		14P/ft
20 way grey ribbon		28n/f+

№1N4001 3 1N4002 5 1N4006 7 1N4007 7 1N5401 12 1N5404 16 1N5406 17 400mWzen 6 1,3W zeners 13

REGULATORS

LM309K LM317K LM317T LM323K

0.490

▶1N4148 3 ОРТО

HARDWARE
PP3 battery clips Red or black crocodile clips Black pointer control knob Pr Ultrasonic transducers 60 V Electronic buzzer 12V Electronic buzzer PB2720 Piezo transducer. 64mm 64 ohm speaker 64mm 65 ohm speaker
20mm panel fuseholder
POTENTIOMETERS

į	C.	AP/	ACI	TC	RS
					leads

П	-			
	BRIDGE	No.	2A 200V	40
1	Section 1	Epe	2A 400 V	45
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4			6A 400V 95	
4	1A 50 V	20	VM18 DIL 0	9A
	1A 400V	35	200V	50

45 45 46 40 40 40 35 550	Rotary, Carbon track Log or Lin 1K - 2M2, Single 32p, Stereo 85p, Single switched 80p, Slide 80mm travel single Log or Lin 5K - 500K 83p each. Preset submin, hor. 100 ohms - 1M. Preset submin, hor. 100 ohms - 75W %" 100 ohms to 100K - 88p each.	Tag at a power supply state tray titls: 2200 /40V - 110p; 4700 /40V - 160p 2200 /63V - 110p; 4700 /63V - 230p Polyester, miniature Sumers PCB: 1n, 2n2, 3n3, 4n7, 6n8, 10n, 15n, 7p; 22n, 33n, 4n7, 6n8, 10n, 15n, 7p; 12n, 33n, 12n, 22n, 33n, 4n7, 6n8, 13n, 230n, 20p; 470n 28p; 680n, 13p; 1u 33p; 2u2, 50p. Tantalum bead: 0,1, 0,22, 0,33, 0,47, 1,0 @ 35V - 12p, 2,2, 4,7, 10 @ 25V - 20p; 15/16V - 30p; 22/16V - 27p; 33/
3	TRIACS 400V 8A 65 400V 16A 95 400V 4A 50 BR100 25	16V - 45p; 47/6V - 27p; 47/16V - 70p; 68/6V - 40p; 100/10V - 90p, Cer disc 22p-0.01u 50V, 3p sech
3 5 7 7 12 16 17 16 17 18 18 18	JUMPER LEADS Length 14pin 16pin 24pin 40pin Sgle ended DIP(header plug) jumper 24 ins. 145 165 240 380 Dble ended DIP(header plug) jumper 6 ins. 185 205 300 465	Mullard miniature ceramic plate: 1.8pF to 100pF 6p each, Polystyrene, 5% tol: 10p-1000p, 6p; 1500-4700, 8p: 6800 0.012u, 10p, Trimmers, Mullard 808 series: 2-10 pF, 22p; 2-22pF, 30p: 5.5-65pF, 35p
d 7 een 10 llow10	12 ins. 195 215 315 490 24 ins. 210 235 346 540 36ins. 230 250 375 595 25 way D Connector jumpers 18ins, long single ended male 495p, 18ins, long single ended f/male 525p.	BRIDGE 2A 200V 40 2A 400V 45 6A 100V 80 6A 400V 95 1A 50V 20 VMI8 DIL 0,9A 1A 400V 35 200V 50
40 40 60 85	COMPUTER CONNECTORS ZX81 2 x 23 way edge connector wire wrap suitable for ZX81 add-ons 150	IDC CONNECTORS PCB Socket Edge
70 ur 60	SPECTRUM 2 x 28 way edge connector wire-wrap suitable for	Plug Conn. Straight

COMPUTER CONNECTORS	IDC C	ONNECT	ORS	
ZX81 2 x 23 way edge connector wire wrap suitable for ZX81	aparaters /		CONTRACT OF THE PARTY OF THE PA	
add-ons 150 SPECTRUM 2 x 28 way edge		PCB	Socket	Edge
connector wire-wrap suitable for	10 way	Straight 90	85	120
SPECTRUM add-ons 200	16 way	130	110	175
RIBBON CABLE	20 way	145	125	195
Grey Ribbon cable. Price per foot	26 way	175	150	240
	34 way	205	170	320
10 way 14 34 way 58	40 way	220	100	340

CA3189 290 L	M334Z 100 L)	M2917 200 M3900 45 LM3909 76	►NE556 NE565 NE565	45	TDA1024 TL061 TL062	40 Z	N428E N459 N1034E	285 200
AF239 75 BC18 BC107 10 BC18 BC107B 12 BC18		0 35 BSX20 110 BSX29 110 BSY95/ 85 BU206 35 BU206 35 BU208 25 MJ2955 25 MJE326 12 MJE521 12 MJE521 12 MPF102 10 MPF104 18 MPSA06	23 T 23 T 25 T 25 T 25 T 25 T 25 T 25 T	1P35C 1 1P36A 1 1P36C 1 1P41A 1 1P42A 1 1P120 1 1P121 1 1P122 1P141 1 1P142	45 2N22 90 2N22; 90 2N22; 90 2N23; 98 2N23; 98 2N236 110 2N264 60 2N296 40 2N290 40 2N290 30 2N290 30 2N290 50 2N290	099 12 000 100 100 100 100 100 100 100 100	2N3056 2N3402 • 2N3703 • 2N3703 • 2N3703 • 2N3706 • 2N3707 • 2N3708 • 2N3707 • 2N3702 • 2N3702 • 2N3702 • 2N3812 • 2N3823 • 2N3903 • 2N3903 • 2N3904 • 2N3905 • 2N3903 • 2N3904 • 2N3905 • 2N3906 •	9 9 9 10 10 10 170 3 195
Plugs solder lugs 6 Right angle 12 Sockets lugs 9 Right angle 16	way 15 way 25 way 00p 85p 125p 20p 180p 240p 190p 195p 00p 210p 290p 00p 90p 100p	7 37 way 170p 350p 290p 440p 110p	LEGIZIUM TO THE PARTY OF THE PA	2	Antex CS 17th 2.3 and 4.7m CS 17Wor XS Antex XS 25 3.3 and 4.7m	W Solder m bits to 25W ele W	ring iron 4 o suit ement 2	195 85 210 525 85

	71 2140034 33	_
200	SOLDERING IRONS	
	Antex CS 17W Soldering iron 2.3 and 4.7mm bits to suit CS 17Wor XS 25W element Antex XS 25W 3.3 and 4.7mm bits to suit	495 85 210 525 85
	Solder pump desoldering tool. Spare nozzle for above 10 metres 22swg solder	480 70 100

390

VERO

VEROBLOC ◀ Size 0.1 matrix

OPTO ■ 3mm red 7 ■ 5mm green 10 ■ 5mm yellow10 ■ 5mm yellow10 □ 7 □ 7 □ 1132 □ 40 □ 7 □ 1132 □ 40 □ 7 □ 1132 □ 40 □ 7 □ 1132 □ 40 □ 7 □ 1132 □ 7 □ 7 □ 7 □ 7 □ 7 □ 7 □ 7 □ 7 □ 7 □ 7	24 ins. 210 235 345 345 345 336 ins. 230 250 375 25 way D Connector jumpers lisins, long single ended male 18 ins. long single ended f/mal COMPUTER CONNECT ZX81 2 x 23 way edge connewire wrap suitable for ZX81 add-ons PECTRUM 2 x 28 way edge connector wire-wrap suitable SPECTRUM add-ons RIBBON CABLE Grey Ribbon cable, Price per 10 way 14 34 way 16 way 25 40 way 20 way 28 50 way 20 way 28 50 way 24 way 38 60 way
RESISTORS WW 5% Carbon film E12 series 4,7 chm - 10M . 1p each. WW 5% Carbon film E12 series 4,7 chm to 4M7 . 2p each. WW 1% metal film E24 series 10 chm - 1M . 6p each.	PCB MATERIALS Alfac transfer sheets — please type (e.g. DIL pads etc.) Dalo etch resistant pen Fibre glass board 3.75 x 8" Fibre glass board 8 x 12" Ferric Chloride crystals

68 90 100	40 way 220 50 way 235 60 way 330	190 200 230	340 395 495
state 45 90 80 200	Plastic with lid & screws 3 x 2 x 1" 55 4½ x 3 x 1½" 88	Aluminium 3 x 2 x 1" 4 x 2% x 1% 4 x 2% x 2" 6 x 4 x 2" 7 x 5 x 2%"	65 " 95 95 120 165
100	7 x 4 x 2" 160	8×6×3"	205

DIN Plug Skt Jack Plug Skt
2 pin 9p 9p 2,5mm 10p 10p 3 pin 12p 10p 3,5mm 9p 9p
3 pin 12p 10p 3,5mm 9p 9p
5 pin 13p 11p Standard16p 20p
Phono 10p 12p Stereo 24p 25p
1mm 12p 13p 4mm 18p 17p
UHF (CB) Connectors:
PL259 Plug 40p Reducer 14p SO239 square chassis skt 38p
SO239S round chassis skt 40p
IEC 3 pin 250 V/6A
Plug chassis mounting 38p
Socket free hanging 60p
Socket with 2m lead 120p
SWITCHES Submin toggle: SPST 559, SPDT 60p, DPDT 65p, Miniature toggle: SPDT 80p, SPDT centre off 90p, DPDT 90p, DPDT centre off 100p, SPST 35p, DPDT48p Miniature DPDT slide 14p, Push to break 14p, Push to break 12p, Push to break 22p, Rotary type adjustable stop, 1912W, 2P6W, 3P4W all 55p each, DIL switches: 4SPST 80p 6 SPST 80p, 8SPST

omin toggle: ST 55p, SPDT 60p, DPDT 65p_ niature toggle:	SP0256	, 85	iOp Data	: 50p.	Spare sp	
DT 80p, SPDT centre off 90p DT 90p, DPDT centre off 100p, ndard toggle: ST 35p, DPDT48p	MICE	10	6116P3 6502 CPU 6522 VIA 6532	320 325 295 570	6852 6875 6880 81 LS95	240 498 100 88
niature DPDT side 14p, in to make 14p, in to make 14p, in to break 22p, in to break 22p, tary type adjustable stop, tary type adjustable stop, zwitches: SST 80p 6 SPST 80p, 8SPST pp.	2114L2 2716 2532 2732 2764 4116P20 5101L-1	99 240 290 290 425 85 220	6551 ACIA 6800 CPU 6802 CPU 6809 CPU 6810 RAM 6821 PIA 6840 6850	220 250 620 115 110	B1LS96 81LS97 80B0A 8085AC 8156 8212 8216 8224	85 250 340 350 110 100 120

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Now your computer car. The GI SP0256 speech, all is able through stored p you the speech. All of computer car. It is able through stored point and the speech car. It is a speech car. It	orocessor rogram to shone stem gives	Siza 0.1 2.5 x 1 2.5 x 3 2.5 x 5 3.75 x 5 VQ boa Veropin Single si Double Spot fac Pin inse Wiring a Soare sp	75 rd ns per 10 ided sided ce cutte mion to pen	00:	22 75 85 95 160 50 60 130 162 330
MICRO 8516P7 8520C 6522V 6552V 6552V 6552V 6552V 6552V 290 6800C 2732 290 6809C 2732 290 6810R 425 6821 P 4116P20 85 6840 5101L-1 220 6850	PU 325 IA 295 570 CIA 650 PU 220 PU 250 PU 620 AM 115	6852 6875 6880 81 L S95 81 L S96 81 L S97 8080 A 8085 A C 8156 8212 8216 8224	240 495 100 85 85 85 250 340 350 110 100 120	8228 8251 8253 8255 8255 8259 MC1488 MC1489 Z80A CPU Z80A PIO Z80A SIO Z80A DMA	220 250 390 225 390 55 55 290 260 260 900 1150
COMPONENT KITS An ideal opportunity for the beginner or the experienced constructor					

CONTRACTOR DESCRIPTION OF THE PERSON NAMED IN COLUMN 1995	ohm - 1 ½W 5% ohm to	Carbo OM Carbo 4M7 metal	n film E in film E film E24	1p eacl 12 series 2p eacl	4.7 0	Alfac tras type (e.g. Dalo etch Fibre glas Fibre glas	nsfer sheet DIL pads resistant s board 3. s board 8 loride crys	s – ple etc.) pen 75 x 8' x 12"	45 90	Plast & sci 3 x 2 4½ x	2 x 1" 3 x 1%"	3 d 4 4 55 6 88 7	luminium x 2 x 1" x 2% x 1" x 2% x 2" x 4 x 2" x 5 x 2%' x 6 x 3"	65 4" 95 ' 95 120
AND REAL PROPERTY AND PERSONS ASSESSED.	4000 4001 4002 4006 4007 4008 4009 4010 4011 4012 4013 4014 4015	10 10 12 50 14 36 24 24 10 15 20 45	4016 4017 4018 4019 4020 4021 4022 4023 4024 4025 4026 4027 4028 4029 4030	20 30 45 25 42 40 45 16 33 12 75 20 40 45 14	4034 4036 4039 4040 4041 4042 4043 4044 4046 4047 4049 4050 4051 4052 4053	140 249 280 40 40 38 40 40 35 38 21 21 42 48 48	4054 4055 4059 4060 4063 4066 4067 4068 4069 4070 4071 4072 4073 4075 4076	78 80 430 42 80 222 225 14 13 13 13 13 13 145	4081 4082 4085 4086 4089 4093 4095 4097 4098 40106 40109 40163 40173 40175	12 12 48 50 125 18 68 65 290 70 70 40 110 60 100 75	40193 4502 4503 4507 4508 4510 4511 4512 4514 4516 4518 4521 4526 4527	65 60 32 35 110 45 40 40 115 55 40 50 90 60 50	4528 4529 4532 4534 4534 4549 4553 4549 4556 4556 4556 4556 4584 4585 4724	45 150 60 400 60 360 215 35 35 390 140 35 60
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	7400 7401 7402 7403 7404 7405 7406 7407 7408 7409 7410 7411 7412	14 14 14 16 16 28 28 16 16 16 16	7413 7414 7416 7416 7420 7421 7422 7422 7428 7430 7432 7432 7433 7437 7438 7440 7442	25 30 26 26 16 22 22 20 22 22 22 25 25 16 32	7444 7446 7447 7448 7450 7451 7453 7454 7460 7472 7473 7474 7475 7476 7480 7482	70 55 40 42 16 16 16 16 24 27 23 30 27 48 65	7483 7485 7486 7489 7490 7491 7492 7493 7494 7495 7496 7497 74100 74109 74121	38 80 26 165 22 35 25 35 35 35 35 35 36 26 30 28	74122 74123 74125 74126 74132 74141 74145 74147 74148 74150 74153 74154 74156 74157 74160	38 40 33 33 36 55 45 75 60 55 36 60 36 36 36 30 40	74161 74162 74163 74164 74165 74167 74170 74173 74174 74175 74176 74177 74179 74181 74182	46 40 45 45 150 125 58 54 50 40 42 70 40 105 40	74190 74191 74192 74193 74194 74195 74196 74197 74198 74199	48 48 40 40 40 45 40 80 80

16 pin 18 pin	12p	60p
20 pin	13p	68p
22 pin	16p	75p
24 pin 28 pin	18p 23p	82p 95p
40 pm	25p	135p

SOCKETS Low Wire profile wrap 6p 28p 14 pin 8p 45p

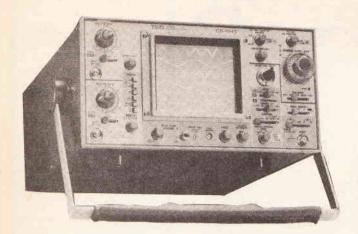
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NEWS:NEWS:NEWS:NEWS:NEWS:NEWS



Dual Timebase 'Scopes

Trio have introduced a range of dual timebase oscilloscopes which are claimed to represent the ultimate in modern 'scope technology with regard to functions available, specification, reliability and value for money.

The CS-1040 and CS-1060 are three channel, six trace 'scopes with bandwidths of 40 MHz and 60 MHz respectively. Both use a large rectangular domed mesh,

post-accelerator CRT with 12 KV and 16 KV of accelerator potential, providing both high intensity and excellent resolution. Their inner face graticule eliminates parallax errors, while the auto focus maintains a sharp clear wave-form display at all times. Vertical axis sensitivity is continuously adjustable from 1mV/ cm through 5V/cm, the very sensitive 1mV/cm range being of great assistance in observing complex, low level waveforms. Part of the input signal is diverted and fed to an output at approximately 50mV/cm of the input level, the gain making it easy to measure frequency using normal frequency counters.

Alternate delayed sweep provides magnification of an intensified portion of the waveform simultaneously with the original. Channels 1, 2 and 3 can be displayed together using the main sweep, with the individual delayed waveforms of these channels simultaneously shown using the alternate sweep function to give a 6 trace capability. Sweep time is continuously variable from 0.5 sec/cm to 5 nanosec/cm wth an internal delay line to provide accurate observation measurement of the leading edge of high frequency signals. $A\pm3\%$ accuracy allows for extremely precise waveform measurement.

Video signals both vertical and horizontal can be observed using a new video clamping function in which manual syncing has been eliminated, ensuring high stability syncing. Other features include V mode triggering, quickly switchable alternate and chop, high sensitivity X-Y mode, auto-free run, trace rotation, trigger holdoff, single sweep, line and auto sync, sweep and gate output, add and subtract, vertical control of delayed waveforms, and intensity modulation

Completing the range is the CS-2110 four channel, eight trace 100 MHz oscilloscope. Sensitivity over its normal bandwitdth is 1mV/cm and it will trigger to beyond 140 MHz. The CS-2110 has an inner face graticule, and an accelerator potential of 20 kV ensures that the display remains bright and sharp even when viewing high speed signals on the 2 ns/ cm sweep range. In addition to the features found on the other two models, the CS-2110 has an accuracy of ± 2%, a channel-tochannel skew time of less than 500 ps, and completely independent A and B sweeps.

All three models come with a two year guarantee and a full range of accessories is available. The CS-1040 and CS-1060 cost £638.00 and £799.00 respectively, exclusive of packing, delivery and VAT, and are available from House of Instruments, Clifton Chambers, 62 High Street, Saffron Walden, Essex CB10 1EE, tel 0799 24922, or from Dawne Instruments & Electronics, Shields Road, Bill Quay, Gateshead NE10 ORS, tel 0632 695117. The CS-2110 costs £1399.00 exclusive of packing, delivery and VAT and is available from House of Instruments at the address above.

Computer Filter Plug

Galatrek International Ltd have introduced a new Filter Plug which can be fitted to the supply cable in place of a standard 13 amp plug and will protect micro and minicomputers, word processors and all voltage sensitive equipment from mains born interference.

This compact unit will protect equipment from transients and spikes which can wipe out memory and corrupt data. It also

provides protection against momentary supply interruption, mains RF interference and lightning disturbance. The current rating of 2 amps is sufficient for most micros and accessories, and frequency is 50/60 Hz. The Filter Plug is available as described, or in a small box with a socket outlet to choice for any country in the world and a flylead mains input, for £29.95 including VAT and post and packing. Order from the manufacturers, Galatrek International Ltd., Scotland Street, Llanrwst, Gwynedd, North Wales, tel 0492 640311.

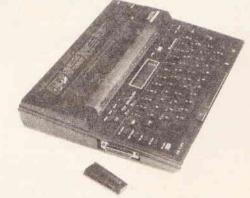
Low Cost **EPROM Eraser**

Ground Control have introduced a low cost ultra violet EPROM eraser which is aimed at development laboratories, home computer enthusiasts, and other applications where rapid erasure of just a few EPROMs is required.

The Uvipac EPROM Eraser is mains powered and will erase up to three EPROMS of any size at one time, or one CPU with onboard EPROM. Erasure takes between five and twenty minutes depending upon the type of EPROM and the Uvipac can be supplied with a built in fifteen

minute timer if required. EPROMs are simply loaded into the conductive foam pad supplied and inserted into the unit. When the door has been closed and the unit switched on, an optical fibre indicator shows that the eraser is operating. The complete unit measures just 90 x 80 x 49 mm and spare conductive foam pads and UV tubes are available from the manufacturers.

The basic Uvipac eraser costs £19.95 and the Uvipac—T with built-in timer costs £24.95. Both prices include VAT, and postage and packing for the UK is £1.50. Ground Control, Alfreda Avenue, Hullbridge, Essex SS5 6LT, tel 0702 230324.



Baby Brother

Prother's new EP-22 is probably the smallest and lightest type-writer in the world, and its plain paper thermal printing system makes it one of the quietest as well. It is battery powered, fully portable, and has a built-in RS-232C interface which allows it to be used as a printer with personal computers.

The EP-22 is no bigger than an A4 pad and its weight, including batteries, is just 5 ibs. The 5 x 7 dot matrix printer can be used with either thermal paper or with plain paper by means of a cassette-loading thermal ribbon. The calculator style QWERTY keyboard features a second shift for all the accents used in Roman script European lan-

guages, a range of signs for arithmetic and chemical formulae, and automatic superior or inferior numerals. A sixteen character LCD with adjustable angle brightness allows text to be checked, and if necessary amended using the 32 character correction buffer. Up to a page of corrected text can be stored in the 2K memory, ready to be printed at the touch of a button, and the display indicates the amount of memory remaining. The EP-22 can also be used as a 12 digit calculator.

The EP-22 comes complete with batteries, 3 thermal cassette ribbons, and both thermal and plain paper, and costs £169.95. Jones & Brother, Office Equipment Division, Shepley Street, Audenshaw, Manchester M34 5JD, tel 061-330 6531.



ELECTRONIC LOCK KIT XK101

This KIT contains a purpose designed lock IC. 10-way keyboard, PCBs and all components to construct a Digital Lock, requiring a 4-key sequence to open and providing over 5000 different combinations. The open sequence may be easily changed by means of a prewired plug. Size: 7 x 6 x 3 cms. Supply: 5V to 15 V d.c. at 40uA. Ouput: 750mA max. Hundreds of uses for doors and garages, car anti-theft device, electronic equipment, etc. Will drive most relays direct. Full instructions supplied.

ONLY £10.50

Electric lock mechanism for use with latch locks and above kit £13.50

MINISTER STATE **OPEN-SESAME**"

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The XK103 is a general purpose interest transmitter receiver with one momentary inormally open lietay contact and two lacched translator outputs. Designed orimarily for controlling materiased parage doors and two auxiliary outputs for drivegarage inghts at a range of up to 40 ft. The unit also has numerous applications in the home for switching lights. TV. closing curtains, etc. Ideal for aged or disabled persons.

The Kit comprises a mains powered receivers at the control of the c

fisabled persons
The Kit comprises a mains powered receiver, a four putton transmitter, compilete with pre-drilled box equiring a 9V pattery and one opto-isolated solid states witch kit for inter-lacing the receiver to mains appliances. As with all our kits, full instructions are

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DL 1000K This value for money kit features a bi-directional sequence, speed of sequence and frequency of direction change, being variable by means of potentiometers and incorporates a master dimming control. £14.60

DI 71000K

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A lower cost version of the above, featuring undirectional channel sequence with apped variable by means of a pre-set pot. Outputs switched only at mains zero crossing points to reduce radio interference to a minimum.

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Additional Receivers XK111 £10.00

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- and 30p - 8" x 9" S.A.E.
MK6 SIMPLE INFRA RED TRANSMITTER
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Mains powered with triac output to switch up to 500W at 240V ac Range approx 20 ft on off or momentary control. momentary control of the momentary control of

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MK12 18-CHANNEL RECEIVER

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PP3 batteria and keyboard (MK8, MK10 or MK13) size.

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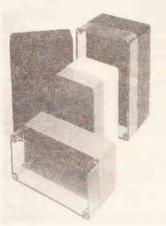
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B oss Industrial Mouldings Ltd have introduced a series of coloured tops to complete their range of ABS BIM 2000 Bimboxes. The existing range is available in seven sizes ranging from 100 x 50 x 25 mm to 190 x 110 x 60 mm and features a choice of five different coloured bases with a clear top. The new tops are made from the same material and come in the same five colours as the bases, allowing you to select matching or contrasting case sections as desired. Colours available are black, grey, white, orange and blue and all cases incorporate slots on a 0.2" spacing which can support PCBs. The case parts are secured by screws inserted through the base



and when assembled have excellent water repellant properties. Boss Industrial Mouldings Ltd, James Carter Road, Mildenhall, Suffolk 1P28 7DE, tel 0638 716101.

Touch Sensitive Keyboard

The Concept keyboard has a flat surface which is divided into an 8 x 16 matrix of touch sensitive areas, each producing a unique 7-bit ASCII code which the programmer defines as required. The surface accepts A4 size overlay sheets which can be marked as desired to define areas and functions, and the manufacturers claim that it will work with any microcomputer.

The keyboard is intended for educational use, allowing pupils to communicate with a computer using a minimum of clearly marked functions rather than hav-

ing to cope with the complexity of a full QWERTY keyboard. Other possible applications include games, demonstrations, and simulation exercises. The format obviously lends itself to the representation of, for example, a floor plan around which people and furniture must be moved. It is possible to use a number of areas together and thus produce large touch sensitive pads which could be used by those who have handicaps or are otherwise unable to manipulate a conventional keyhoard

The Concept keyboard comes complete with full documentation, a connecting lead to suit the majority of microcomputers, and a set of demonstration software. Star Microterminals Ltd, 22 Hyde Street, Winchester, Hampshire SO23 7DR, tel 0962 51422.

SHORTS

- Downing Electronics have introduced a portable test pattern generator for use with all 525 and 625 line RGB display units. It provides 9 different patterns, has a signal frequency accuracy of ± 0.02%, and will test both separately synchronised and green signal pulse synchronised units. Cost is £325.00 plus VAT from Downing Electronics Ltd, 24 Downing Road, Reading, Berkshire RG3 5BB, tel 0734 22556.
- An international users group for owners of Oric-1 microcomputers has recently been set up. The Oric Owner's/Users Group (International) Ltd has the full approval of the computers' manufacturers and produces a monthly magazine called Oric Computing. Membership costs £10 a year, and £1 plus an A4 SAE will bring you full details and a sample magazine. 1 Marlborough Drive, Worle, Avon BS22 0DQ, tel 1934 510279.
- The NMS Relay Controller is designed for use with the ZX Spectrum and has four channels each with a double pole 5A 240V relay. The relays are operated by simple BEEP commands either from a program or the keyboard, and the unit plugs into the MIC socket leaving the expansion port free. It costs £24.95 plus £1.50 post and packing from Ness Micro Systems, 100 Drakies Avenue, Inverness IV2 3SD, tel 273 194

- © Cricklewood's latest catalogue covers 31 sides of A5 with mail order electronics parts, many of them illustrated. Items listed include semiconductors, books, tools, connectors, cases, switches, etc and copies cost £1 including postage from Cricklewood Electronics Ltd, 400 Cricklewood Broadway, London NW2 3ET, tel 01-452 0161.
- Bulgin have produced new catalogue listing their range of bulkhead mounting and integral IEC socket type mains filters. Ratings up to 6A are covered. Also new is a catalogue describing their Buccaneer range of waterproof connectors covering both mains and signal applications. A.F. Bulgin & Company PLC, Bypass Road, Barking, Essex IG11 OAZ, tel 01-594 5588.
- Inmac have produced an 88 page illustrated catalogue of computer and business accessories. Their range includes dedicated accessories for Apple and CBM machines and general accessories like cables, disc systems, etc to suit most other machines. The catalogue is free from Inmac UK Ltd, Davy Road, Astmoor, Runcorn, Cheshire WA7 1PZ, tel 09285 67551.
- Riscomp's US 5063 is an ultrasonic movement detection module which processes the received signal using digital techniques. It offers a choice of three levels of discrimination, fixed alarm time, exit delay, and selectable entrance delay and costs £13.95 plus VAT. Riscomp Ltd, 21 Duke Street, Princes Risborough, Bucks HP17 0AT, tel 08444 6326

- Salford University are running a series of one, two and three day short courses during December and January on the BBC, Apple II and CBM microcomputers. The courses cover all levels from complete beginner upwards and each student is guaranteed individual use of an appropriate machine. Details from The Microprocessor Short Courses Unit, Department of Electronics & Electrical Engineering, University of Salford, Salford M5 4WT, tel 061-736 4843 ext 248.
- The Integrex BX80 7—colour printer is designed for use with the BBC microcomputer and will work in all modes, including mode 7 Teletext, using the supplied colour screen dump listing. It prints at 125 cps on plain paper, has an internal 2.5 K byte buffer, and connects to the BBCs RS-423 socket using the lead supplied. Price is £495 plus VAT from Integrex Ltd, Portwood Industrial Estate, Church Gresley, Burtonon-Trent, Staffs DE11 9PT, tel 0283 215432.
- Further to last month's report of a record number of bankruptcies among British electronics companies, a recent surprise casualty is Scopex Instruments Ltd. It may be of some consolation to owners of Scopex products to learn that a former design engineer with the company has formed a new company, Mendascope, which offers a full repair service including collection and free estimate. Mendascope Ltd, Otter House, Western Underwood, Olney, Bucks MK465JS, tel 0234 712445.

- Make light work of different number base arithmetic with Casio's new FX450. This solar-powered scientific calculator will rapidly convert between binary, octal, decimal and hexadecimal, has 64 functions and holds eight fundamental constants in memory. It comes in a protective folding wallet and costs £22.95. Casio Electronics Co. Ltd, Unit 6, 1000 North Circular Road, London NW2 7JD, tel 01-450 9131.
- Wilmslow Audio's new catalogue doesn't just list loudspeakers by manufactuers like Tannoy, Kef, Gauss and Chartwell, it also contains kits, amplifiers, microphones and stands, effects units, and a lot of useful information. Price is £1.50 from Wilmslow Audio Ltd, 25/39 Church Street, Wilmslow, Cheshire SK9 1AS, tel 0625 529599.
- The AMS 3" disc drive which is suitable for use with the BBC microcomputer is to be sold through W.H. Smiths. The unit comes in 100K format at £225 or 200K format at £399 and runs from the BBCs power supply. A number of software houses have produced packages for the drives.
- The 1984 London Home Computer Show runs from Friday January 6th to Sunday 8th in the large New Hall of the Royal Horticultural Society, just around the corner from the Old Hall where it was staged last year. The show is aimed at microcomputer hardware and software enthusiasts and is open from 10 am to 6 pm each day (4 pm Sunday). Admission costs £2.00 or £1.50 if you're under sixteen.

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VECTOR GRAPHICS

4,294,967,296 vectors should take over a year to draw, even at 100 per second. However if you want to try — the ETI Graf-vec will do it.

his project takes us away from the familiar world of the TV display and shows us instead the other principal means of producing a picture. The ordinary TV set produces a picture by moving an electron beam backwards and forwards across a phosphor coated screen so that it traces a fixed number of parallel horizontal lines. The actual picture is produced by turning the beam on to display a bright dot at the right time and turning it off where no light is required. This method works very well for broadcast pictures but is sometimes not so good for pictures generated electronically. For a home computer to generate a picture, it must generate a pattern of bits which determine when the electron beam in the display tube is to be on and off. Since the transitions can only occur at discrete time intervals, the picture produced does not

always appear as smooth as we might wish. This effect is usually most noticeable on diagonal lines where there are marked contrast changes.

While we cannot pretend that this project will replace a TV type of display for home computer applications, it does provide an interesting alternative output

device for graphics.

The method employed by the Graf-vec in producing a picture is to define the start and finish of a line and cause an electron beam to traverse the intervening space relatively slowly. Drawing many such lines in a short space of time allows us to build up a picture. The main disadvantage of this method is that if too many lines are drawn the whole display will appear to flicker. This can be reduced by the use of long persistence phosphors if available.

As described, the Graf-vec will

draw lines between any two points on a 256x256 grid. The relatively simple circuitry used does not compensate for differing line lengths changing the brightness but still gives an interesting result.

The Circuit

The circuit consists of a power supply, digital input and control section, and two linear scan generators. The basic mode of operation requires a data source - probably your trusty home computer - to put two bytes of data into the device to represent the coordinates to which a vector is to be drawn (The starting point is assumed to be where you are now). The Graf-vec will draw the vector and then wait for the next set of data and indicate that it is ready. The digital input circuitry of the Graf-vec is designed so that one byte of the next vector can be input at any time as it is stored in a

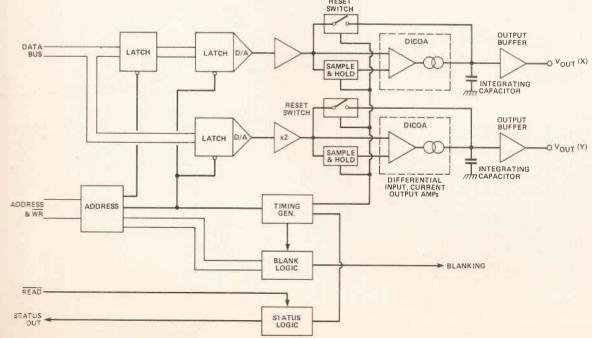


Fig. 1 Block diagram of the Graf-vec.

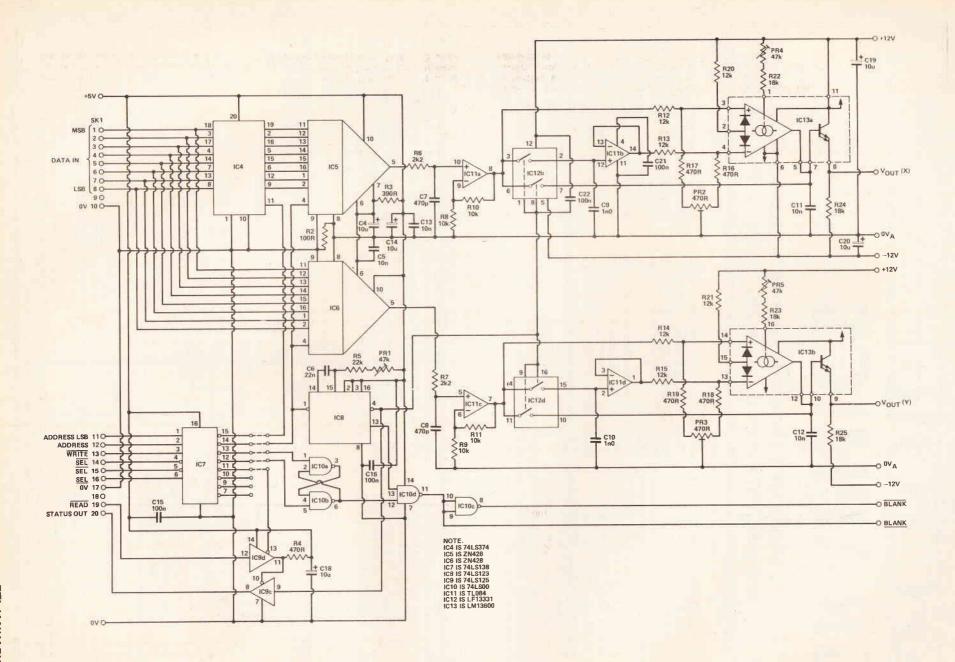
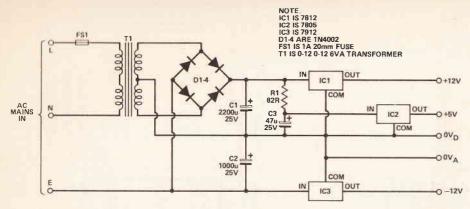
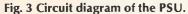


Fig. 2 Circuit diagram of the Graf-vec.





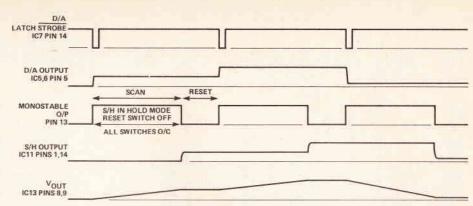


Fig. 4 Timing diagram of the Graf-vec.

How It Works

The Graf-vec consists of three major parts. The first of these is a straightforward stabilised power supply giving ± 12 V and +5 V at about 100 mA each. Only one transformer is used to save on cost and space. The output is regulated by three IC stabilisers which often need no heatsink in normal operation. However, R1 is provided to dissipate some of the excess power in the +5 V regulator, and a small piece of aluminium would not go amiss.

The second major part consists of the logic, timing and digital to analogue conversion. IC7 is a 74LS138, 1 of 8 decoder whose inputs are available at the input connector. This enables simple interfacing to some computer systems without additional circuitry. The outputs from this device are all available on the board via links and are used to enable the other logic functions. The first output drives the strobe input of a 74LS374 (IC4), which is an octal latch with three-state outputs. The outputs from the device are permanently on in this circuit and it is used to store the data corresponding to the X vector before it is loaded into the DAC (IC5).

The next output from IC4 has two uses. It drives the data input enable pins on the DACs (IC5 & 6) and it also drives the trigger input on IC8. ICs 5 & 6 are

ZN428 monolithic digital to analogue converters which accept data from the inputs when the enable pin is low and store it while the pin is high. They convert the digital data to a corresponding analogue output voltage in the range 0 to 2.55 V. Note that IC6 gets its data from the input data bus whereas IC5 gets it from the output of IC4.

ICB is a dual monostable device only one part of which is used in this circuit. Its purpose is to provide the timing signals for the sweep generator, a display enable signal, and status indication back to the controller.

The next two outputs from IC7 are used to set or reset a simple latch made from two parts of IC10. An output from this latch is gated with the output from IC8 and enables or disables the display (if this facility is used.).

The final output from IC7 enables part of IC9 which is a 741S125 Quad three state buffer. This transfers the logic level at SK1 pin 19 onto the enable pin of another section of IC9. If this is low, the logic state of IC8 Q output is impressed on SK1 pin 20. This indicates that the unit is ready to start display when the pin is high.

The final part of the Graf-vec is made up of two identical circuits. Each of these takes the output from a DAC (IC5 or 6)

and processes it to give the required output. We shall only explain one of these circuits as the other is exactly the same.

The output from the DAC comes via R6 and C7 which remove glitches and high frequency noise from the signal. It is then amplified by a factor of 2 by IC11a. This also provides a low impedence drive to the rest of the circuit.

Consider firstly the case when the Q output from IC8 is high (ie not triggered). The output from IC11a is connected via two of the four FET switches in IC12, an LF13331, to C9 and C11. This ensures that these capacitors are charged to a defined voltage before each sweep. Nothing further happens to this part of the circuit until the DACs are loaded with new information and IC8 is triggered. When this happens all the switches in IC12 are turned off. This isolates C9 which will hold its previous voltage for some time, and also removes the clamp on C11. The voltage on C9 is buffered by IC11b and applied via R13 to the inverting input of IC13. A new voltage now appears on the output of IC11a as the DAC has been updated. This is applied via R12 to the noninverting input of IC13, an LM13600, which contains two transconductance amplifiers and two buffers. The transconductance amplifiers provide an output current which is proportional to the difference of the two input currents, modified by currents into two other inputs.

In this circuit, one amplifier and buffer combination is used for each channel. The currents through R12 and R13 are subtracted and a current proportional to their difference flows into C11. Currents flowing through R20 and VR4, R22 determine what the actual gain will be. As the voltage on IC11a output is constant after its initial change and that on IC11b output is also constant, the resulting current flowing into C11 will be constant. The result of this is that C11 will charge linearly and will also tend to go in the direction of the voltage on IC11a output. In fact, when everything is set up correctly, the voltage on C11 will just reach the voltage on IC11a output as the monostable pulse ends. At this time the capacitor voltage will be clamped by the FET switches being turned on again. The capacitor voltage is buffered by buffers in the LM13600 before being sent out.

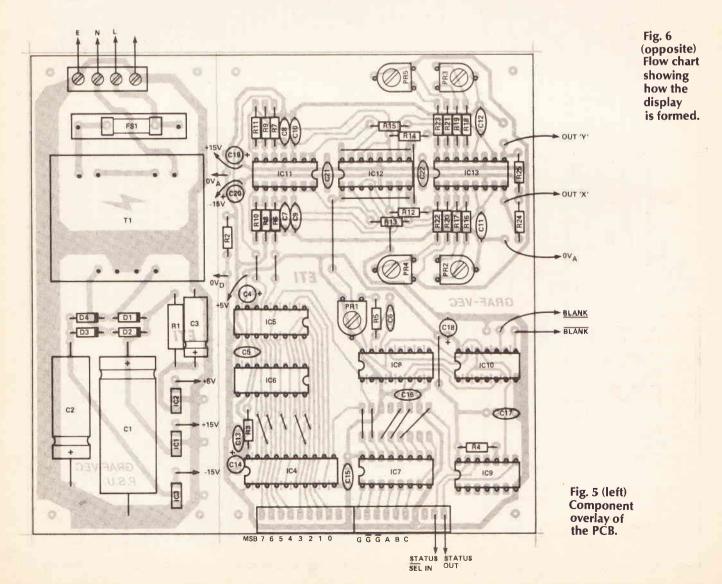
Finally it should be mentioned that R16,17 and VR2 form a balancing network and DC return path for the input currents and one of the control currents.

16514	11 10 00	LD DE,0010	:Scan counter = 256	10 REM) (是: 5型RNDACS 型C IF .?函
17 PICOUT	Ø6 ØE	LD B , ØE	:Points/scan = 14	4 NEU TAN XXXXXXXXXXXXXXXXXXXXXXXXXXX
19	21 AØ 4Ø	LD HL,40A0	:Start of data table = 16544	XXXXXXX
22 POINTOUT	7E	LD A, (HL)	: Get "X" data	15 FAST 17 LET X=10
23	D3 1F	OUT (IF),A	Output "X" data	18 LET Y=X
25	23	INC HL	:Move data pointer	30 POKE 16545,X
26 TESTIT	DB 1F	IN A,(1F)	:Input status indicator	35 POKE 16553,X 40 LET X=X+Y
28	CB 7F	BIT A.7	:Isolate status bit	41 IF X>235 OR X<15 THEN LET Y
3Ø	28 FA	JRZ (TESTIT)	: Jump back if not ready (low)	=(-1) *Y 45 GOTO 20
32	7E	LD A,(HL)	:Get "Y" data	50 FOR K=16514 TO 16575
33	D3 3F	OUT (3F),A	:Output "Y" data	50 PRINT K,
35	23	INC HL	:Move data pointer	70 INPUT A\$ 75 IF A\$=" " THEN STOP
36	10 FØ	DJNZ (POINTOUT	():Repeat for all points	80 IF LEN A\$<>2 THEN GOTO 70
38	1B	DEC DE	:Decrement scan counter	90 LET A=CODE (A\$(1 TO 1))
39	7A.	LD A,D	:Get scan count high byte	100 LET B=CODE (A\$(2 TO 2)) 110 LET C=CODE "F"
4Ø	В3	OR A,E	:OR with scan count low byte	120 LET D=CODE "O"
41	20 E6	JRNZ (PICOUT)	: Repeat if not zero	130 IF A>C OR A <d b="" or="">C OR B<d 70<="" goto="" td="" then=""></d></d>
43	C9	RTS	:Return to calling program	140 POKE K,16*(A-D)+B-D
				150 PRINT CHR\$ A; CHR\$ B
DATA LIST				160 NEXT K
16544	ØØ 8Ø 4Ø C	0 7F 8Ø AE CØ		
	FE 8Ø 7F 8	Ø 97 68 7F 5Ø		
	68 68 7F 8	7F 3Ø 7F 8Ø		

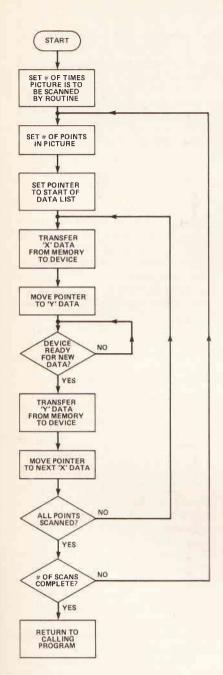
Table 2 ZX81 BASIC program. Note that you must go to line 50 to enter data and RUN to display.

Table 1 Z80 machine code demo program.

40 80 00 00



PROJECT: Vector Graphics



latch, but the second byte should only be put in after the status bit is detected as high as this will start the next scan.

When the second byte of a new vector is written in, the logic section generates a 400 us enable pulse for the linear scan generators. This allows them to generate the linear voltage ramps which eventually move the spot around on the oscilloscope or other dis-

play device.

Once the 400 us pulse has finished, the linear scan generators are set up ready for the next vector and the display enable or blank output will go low. If you have the facility available, this can be used to blank the display between vector scans or, by means of the inter-nal latch accessible by writing to two further addresses, the display can be turned on and off to allow you to move position without drawing a line.

The Linear Scan Generator

This is the heart of the whole system and is basically an integrator. Before each scan starts, the output voltage and the voltage stored on a sample and hold circuit are clamped to the current output from the D to A circuits. When a scan starts, the sample and hold circuit changes to its hold function and the output is unclamped. Since the output is closely associated with the integrator capacitor it does not change immediately.

The D to A circuit now changes its output voltage to the new value and a current is generated which is proportional to the difference between the old and new input voltages. This current is used to charge the integrator capacitor and will

do so at a constant rate. This gives a linear voltage ramp between the old output voltage and (if set up properly) the new one.

At the end of the scan pulse the sample and hold circuit and the output voltages are again clamped in readiness for the next scan. Note that while in the clamped state there is ideally no current flowing in the output circuit of the current generator as its input voltages are equal.

Semi-Solid Section

This is about the interface between the hardware described in this project so far and the software needed to make it do anything interesting. Fig. 6 shows in flow chart form the actions needed to form the display. In order to prevent a lot of flicker, the routine scans all the points in the display many times each time it is called The main cause of any residual flicker is the relatively slow response of the BASIC program which calls it. If this too were in machine code a very smooth display could result.

Table 1 shows how the flow chart is implemented in Z80 code while Table 2 (up to line 45) is the ZX81 basic program which is used to control it. Lines 50 onward are a simple program which allows hexadecimal codes to be typed into the machine which are then held in the REM statement in line 10.

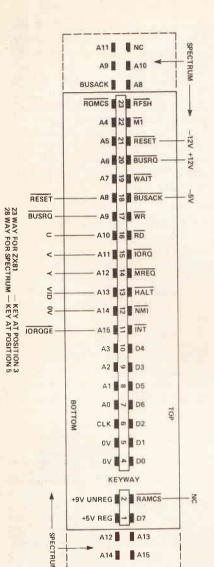
For initial entry of the machine code, alter line 50 to read:-

50 FOR K=16514 TO 16543 Then you can run the program from line 50 and input the program code. Changing line 50 back again will let you type in the data for the picture. The format for typing hex numbers in is two charac-

Parts List

Resistors (¼ W C	Carbon film unless	C2	1,000 uF 25V axial electrolytic	IC5,6 IC7	ZN428 74LS138
,		C3	47 uF 25 V axial	IC8	74LS123
R1	82R 1W		electrolytic	IC9	74LS125
R2	100 R	C4,14,18,19,20	10 uF 25V Tant.	IC10	74LS00
R3	390R	, , , , , , , , , , , , , , , , , , , ,	Bead	IC11	TL084
R4,16,17,18,19	470R	C5,13	10 nF ceramic	IC12	LF1331
R5	22 K	,	disc	IC13	LM13600
R6,7	2K2	C6	22 nF polycar-	D1,2,3,4	1N4002
R8,9,10,11	10K		bonate		
R12,13,14,15,		C7,8	470 pF ceramic	Miscellaneous	
20,21	12K	C9,10	1 nF polycar-	T1 0-12, 0-12 V 6	VA PCR moun
R22,23,24,25	18K		bonate	mains transforme	
VR1,4,5	47K min. horizon-	C11,12	10 nF polycar-	FS1 1 A, 20 mm fuse	e + PCB moun
1/200	tal preset		bonate	holder	
VR2,3	470R min. horizon-	C15,16,17,21,22	100 nF ceramic	SK1 2 off, 10 way 0.1 i	n pitch PCB cor
	tal preset	Semiconductors		nector 4 way, PCB mount main	s screw connec
Capacitors		IC1	1N4002	tor; PCB; Small heatsink	
		IC2	7805	double sided edge co	
C1	2,200 uF 25 V axial	IC3	7915	pitch; 16 way(min) or	20 way ribbo
	electrolytic	IC4	74LS374	cable.	

PROJECT: Vector Graphics



 Graf-vec, socket 1
 ZX81

 pins 1 - 8 (data in)
 D0 - D7

 pins 10, 17 (OV)
 OV

 pin 11 (address LSB)
 A5

 pin 12 (address)
 WR

 pin 13 (WRITE)
 WR

 pin 14 (SEL)
 IORQ

 pin 19 (READ)
 RD

 pin 19 (READ)
 RD

 pin 20 (status out)
 D7

ters 0 to 9, A to F followed by newline. Wrong characters or wrong number of characters will require re-entry of the correct ones. To abort this entry mode type a single space and newline. When first entered, line 10 can be REM with at least 64 characters

While the development work for the project was done on a Z80 system, there is no reason why any other processor could not be used. The only differences would be in the actual interface hardware and the machine code realisation of

our flow chart. There are 8 data lines, 7 control lines and one status output to the project. Normally the data lines will be connected to the controller's data bus. The status output line is from a three state buffer and can be connected to the data bus (we used bit 7). One of the remaining control lines is devoted to reading the status bit and must go low when a read operation is required (on a 6502 system it could be tied low permanently as the read and write are controlled by the same line). Of the remaining 6 control lines, one must be high and two must be low before anything happens. These would normally be used as select lines. The last three lines are used to select the operation to be carried out. One of these should be the R/W or similar function while the others will be simple address lines to select the particular operation to be performed. Exactly how these various lines are connected will depend on your particular requirements but Table 3 shows how we did it for a ZX81.

Construction

This should cause no headaches as it is quite straightforward. First of all, decide whether you want to use the PCB as it is or to split it into two parts (it might be tricky to cut it once the parts are assembled!). Note that there are eighteen links on the main board and five on the power supply, and begin by inserting these, the resistors, and the IC sockets. We recommend the use of sockets if only because some of the devices cost well over a pound and are therefore worth protecting . . . Next, fit the smaller capacitors, potentiometers, and sockets, followed by the power supply diodes, resitor (mounted 6 mm above the board), larger capacitors, fuse, and mains connector. Finally, fit the mains transformer

and insert the ICs into their sockets. Check that the ICs and capacitors are mounted the right way round.

way round.
Test the power supply section fully before connecting it to the other board and BE CAREFUL, there is MAINS VOLTAGE present. If all is well, all that remains is to wire the PCB connectors to suit your microcomputer or whatever and then connect up.

Setting Up

If you have an oscilloscope at hand — you need one for the display — set up the sample driver program or something similar on your computer etc and check that you get negative going pulses on the outputs of IC7 pins 15,14 and 11. (this could change if you use a different jumper pattern for a different computer interface.) Set VR1 to give a low pulse period of 400 us at pin 4 of IC8.

Check the outputs from IC13

with the oscilloscope. These should consist of straight line segments with no sudden jumps. If this is not the case, adjust VR2 and VR4 for the X channel and VR3 and VR5 for the Y channel. VR2 and VR4 are effectively offset controls which tend to have the effect of shifting the lines in one direction whereas VR3 and VR5 are gain controls which increase the slope of the lines in whichever direction they happen to be going. The proper setting of these controls is vital to the production of a good display. If you have difficulty setting them, set up the data in the display table to be 00,00,FF,FF etc. This will give a repeating full scale display.

When the controls have been set up reasonably, run the demonstration program and set the 'scope to X-Y mode. You should now have a moving display. Final trimming of the pots. may be made to clear up any defects visible. If you do not have an oscilloscope, connect up the device to whatever you are using for a display, set all pots to mid travel and run the demo program and tweak

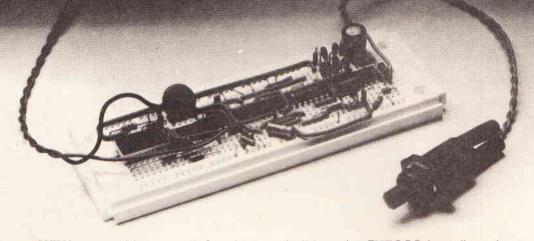
for best results.

Buylines_____

There should be no problems with this lot. The LM12600, LF13331, and ZN428, etc are all available from Technomatic, among others. The transformer is available from Rapid, the PCB connectors from Ambit, and the mains screw connector from Electrovalue. The PCB is available from our PCB service on page 75.

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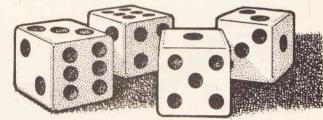
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SINCLAIR'S NEW POCKET TV

Why is there no love from Russia? Why are the French in tears? And why do Chinese gentlemen remain inscrutable? Ask Vivian Capel.

he reason is that these are among the very few places in which Clive Sinclair's new pocket TV will not work. Considering the many different TV standards in use throughout the world the fact that such exclusions are so few is certainly remarkable. Even more remarkable is that the set automatically adjusts itself to whatever standard is being received without any user switching at all. In fact the only external controls are the

tuner and the on/off volume control.

The IC is unique in that it contains almost the whole of the TV circuitry; only the output stages and the tuner are external with just a few resistors and capacitors. This obviously reduces component costs considerably when the cost of originating the IC has been recovered, which it soon should be if the anticipated million sales a year materialise. Furthermore, it drastically cuts assembly costs, hence the price tag of under £80 which is about a third of the price of its nearest competitor, the Sony Watchman.

With the exception of the French 819-line system which is being phased out, most of the world has a 625-line standard, with the American continent and associated countries and islands having 525 lines. All the 625-line systems run at 50 Hz field frequency. Thus the line frequency for the 625-line standard is 15, 625 Hz, while that of the 525-line system is 15,750. Five of the standards use AM sound while the rest employ FM. However, four of the five are obsolete systems (including our own 405-line system) which are either being dropped or have already disappeared. So apart from one, all current systems are FM. Much the same is true of vision modulation sense. The four obsolete systems use positive modulation but, with one exception, all the others are negative.

There are various differences in channel and vision bandwidths as well as vestigial sidebands, but these do not materially affect receiver design, they only produce minor differences in video response. There are also three basic colour systems but as all are compatible with black-and-white reception, they present no problems

for a monochrome receiver.

This leaves us with one factor that does have an effect, the separation between sound and vision carriers. Apart from the obsolete systems there are four standards of separation, 4.5 MHz as used with all 525-line systems, 5.5 MHz, 6 MHz and 6.5 MHz which are used with various 625-line systems. This separation is important because the FM sound carrier and the AM vision carrier produce a beat frequency at the vision detector which is equivalent to their difference. After limiting to remove the AM video modulation, the result is an FM sound signal which is further amplified by sound IF stages at this new beat frequency. The arrangement is termed intercarrier sound, and it is obvious that any difference in the

spacing of the original sound and vision carriers will produce an equal difference in the sound IF frequency. So, TV standards using different spacings cannot normally be received with conventional sound IF circuits.

In order to cope with all these variables, the IC uses a voltage controlled oscillator which runs at a high multiple of the line frequency. Its frequency range can be set by an external resistor, but it is synchronised by the line sync pulses derived from the incoming video signal. The output is split into two paths, one of which is counted down by a logic stage to the line frequency. It is then converted from digital pulses to a suitable scanning waveform by a digital-to-analogue converter and fed to the line output stage. A line PLL stage compares the output of the logic circuit with that of the sync separator to provide a correction voltage for the oscillator. Thus whatever the incoming line frequency might be, the frequency of the oscillator will change to match it. From the line logic circuit there is a further countdown by the field logic stage to the field frequency. This too is locked to the incoming signal by means of the field sync pulses, so the field scan rate is dependant on the standard of the signal being received.

How, though, are the different vision/sound carrier spacings handled? The sound IF is set at 0.25 MHz, which means that there must be a means of converting the incoming intercarrier sound frequency to that value. This is done by another voltage-controlled oscillator which is also controlled by the line VCO. When the line oscillator is running at the 625-line standard the sound oscillator gives an output of 5.75 MHz, but when it is operating at 525 lines, the sound frequency is 4.75

MHz.

Just how it does this is not made very clear by the makers, but a possible method is to run the line oscillator at 8,000 times the line frequency which, at 15,625, Hz, the 625-line frequency, is 125 MHz, and at 15,750 Hz, the 525-line frequency, is 126 MHz. If the sound oscillator is set to run at 130.75 MHz, mixing with the line oscillator frequency will produce difference signals of 130.75 — 125 = 5.75 MHz at 625 lines, and 130.75 — 126 = 4.75 MHz at 525 lines. So, with an intercarrier signal of 4.5 MHz at 525 lines, and the oscillator producing 4.75 MHz, the result is a difference frequency of 0.25 MHz, which is the required IF. In the case of the 625-line system, a spacing and hence intercarrier frequency of 5.5 MHz together with the 5.75 MHz output from the oscillator again gives the 0.25 MHz IF. If, though, a spacing of 6 MHz is received (which is the intercarrier frequency for the U.K.) the same oscillator output of 5.75 MHz also produces a difference frequency of 0.25 MHz. This leaves the 6.5 MHz separation signal out in the

This leaves the 6.5 MHz separation signal out in the cold as the one not capable of being accommodated. It is found in the D, K, and L systems which are used in Russia, France, China, and several Eastern European countries

as well as a few African states. The L system, which is used in France, is the one having positive vision modulation and AM sound, so this is totally non-receivable, though the others could produce a picture without sound. However, as the produced difference signal is 0.75 MHz, which is the third harmonic of 0.25 MHz, the D and K systems might produce weak sound in the presence of a very strong signal.

Output from the sound detector is taken from the chip to the volume control and from there back to the audio output stage which is also contained within the IC. Tuner output is applied to the vision IF stages which operate at the unusually high frequency of 230 MHz. This has the advantage of eliminating image-frequency

interference from other UHF channels.

The tuner receives only UHF signals, and there are a number of countries that still have TV transmissions on VHF. Most of these also operate UHF transmitters as was the case in the UK, but for the benefit of those few areas that have only VHF services, a set with combined VHF/UHF tuner is planned.

The Flat Tube

The second major innovation in this remarkable set is the display tube. While LCD screens can offer compact low-current displays, the phosphor screen still takes some beating, if you can get around the awkward CRT shape which would be hard to fit into pocket TVs.

Size of the Sinclair tube is 4 x 2 x ¾ inches, and the screen is 2 inches wide. It is constructed from two pieces of glass, a front plate and a backing plate which is vacuum formed by a new method developed for the project. The screen is deposited on the inside surface of the back plate which means that the image is viewed through the front plate on the same side of the phosphor that the electrons strike. With normal tubes viewing takes place through the layer of phosphor with attendant loss of light. Thus a much brighter picture is obtained for the same power dissipated, or conversely, lower power is required to give a picture of similar brightness as a conventional tube. Actual brightness is from two to three times greater.



Half of the width of the device is occupied by the screen, the other half accomodating the gun and deflector plates. These are mounted so that the electron beam is parallel to the screen surface, at least at the start. To strike the screen, it must be bent sideways, but this cannot be a gradual bend which would make it strike at a narrow angle as this would produce an elliptical spot, like a torch beam striking the ground at an acute angle. Such a spot would reduce the definition of the picture. To minimise this effect a strong electrostatic field is formed in front of the screen. A positive EHT potential is applied to a conductive coating behind the phosphor which attracts the beam, and a repelling negative potential is given to a conductive transparent layer of tin oxide on the front plate. As the beam enters the region between them it is deflected suddenly toward the screen at an angle which makes it strike the screen almost perpendicularly, giving a virtually round spot.

Another problem involving focus is caused by the unequal lengths of the beam path from the nearside to

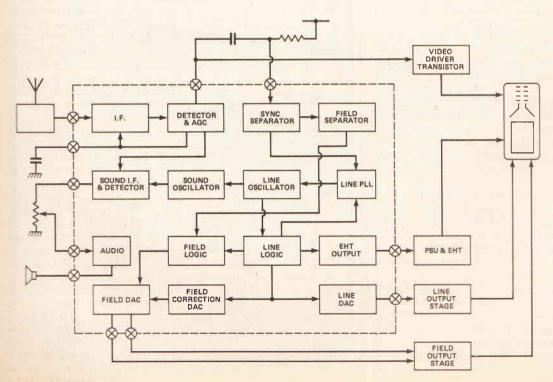
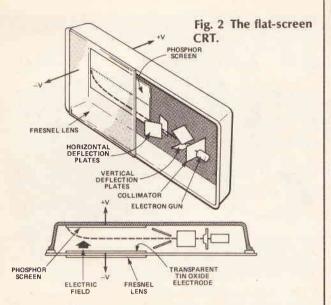


Fig. 1 Block diagram of the receiver. Everything within the dotted line is contained on the single IC.

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_ FEATURE : Pocket TV _



far side of the screen. If the beam is focused by conventional focusing electrodes it will be in focus at only one length, hence at only one part of the screen. This is avoided by passing the beam through a collimator as it emerges from the gun, giving it parallel sides. Being non-divergent it remains in focus over the whole screen.

Scanning the screen from the side produces two forms of distortion, both of which can be demonstrated by aiming a slide projector similarly on to a screen. The first and most obvious is that of trapezium distortion, in which the top of the picture slopes upward away from the gun and the bottom slopes downward. The second, which is apparent only when the projector is at a really sharp angle from the screen as is the case here, is that of curved verticals which curve toward the gun near the top of the screen. Both of these forms of distortion are moderate over the central regions of the picture, but increase considerably toward the top and bottom. The simple expedient employed here is to remove the top and bottom! The height is compressed to about half normal size giving a cinemascope effect, but the viewer gets the correct aspect ratio by means of a fresnel lens formed of transparent plastic over the front plate.

This almost eliminates the curved verticals, but a degree of trapezium distortion remains, and this is dealt with by means of electronic compensation. A line sawtooth is applied to the field circuit inside the chip. This varies the speed of the field scan during the period of one line and thus results in the tilting of that line. The tilt is opposite to the trapezium slope and thereby corrects it. The amount of compensation is reduced from the top to the middle of the raster, and then it is increased from the middle to the bottom, but in opposite phase. Hence a symmetrical picture is produced, a minor miracle considering the angles involved.

Though in danger of being overshadowed by the other technical advances, even the battery is something of an achievment. Developed for Sinclair by Polaroid, it is a lithium type, is small and flat, yet gives 15 hours operation. In contrast the four alkaline penlight cells used in the Sony Walkman last 2½ hours at a cost of nearly a half the £3 price of the lithium battery.

In the face of all this it may seem churlish to criticize, but I find the idea of a 2-inch screen just a mite too small, and a certain way of ensuring the future prosperity of opticians! Perhaps Sir Clive will apply his considerable ingenuity to increasing the picture size with little if any increase in receiver dimensions. This I feel certain would really assure its success.

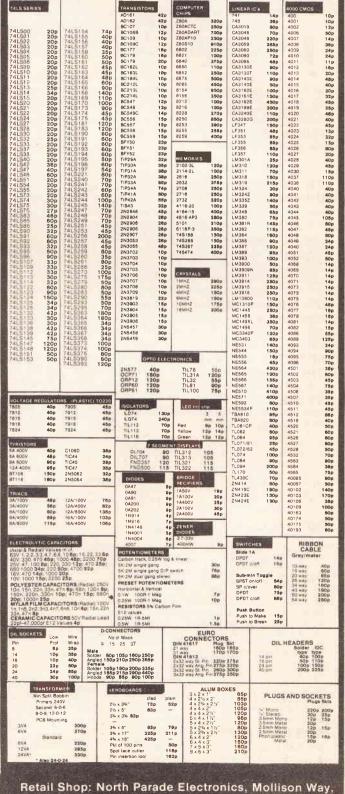
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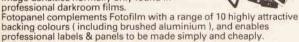
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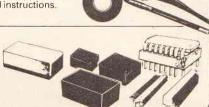
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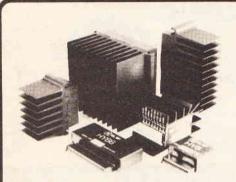
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Module Number	Output Power Watts rms	Load Impedance	DISTO T.H.D. Typ at 1KHz	I.M.D. 60Hz/ 7KHz 4:1	Supply Voltage Typ	Size	WT	Price inc. VAT
HY30	15	4-8	0,015%	<0.006%	± 18	76 x 68 x 40	240	£8,40
HY60	30	4-8	0.015%	< 0.006%	± 25	76 x 68 x 40	240	£9,55
HY6060	30 + 30	4-8	0.015%	< 0.006%	± 25	120 x 78 x 40	420	£18,69
HY124	60	4	0.01%	< 0.006%	± 26	120 x 78 x 40	410	£20.75
HY128	60	8	0.01%	<0.006%	± 35	120 x 78 x 40	410	£20,75
HY244	120	4	0.01%	< 0.006%	± 35	120 x 78 x 50	520	£25,47
HY248	120	8	0,01%	< 0.006%	± 50	120 x 78 x 50	520	£25,47
HY364	180	4	0.01%	< 0,006%	± 45	120 x 78 x 100	1030	£38,41
HY368	180	8	0.01%	<0.006%	± 60	120 x 78 x 100	1030	£38,41

Protection: Full load line, Slew Rate: 15v/µs, Risetime: 5µs, S/N ratio: 100db, Frequency response (-3dB) 15Hz -50KHz, Input sensitivity: 500mV rms, Input Impedance: $100K\Omega$, Damping factor: 100Hz > 400,

Module Number	Module	Functions	Current Required	Price inc.
HY6	Mono pre amp	Mic/Mag, Cartridge/Tuner/Tape/	10mA	£7,60
HY66	Stereo pre amp	Aux + Vol/Bass/Treble Mic/Mag. Cartridge/Tuner/Tape/ Aux + Vol/Bass/Treble/Balance	20mA	£14,32
HY73	Guitar pre amp	Two Guitar (Bass Lead) and Mic +	20mA	£15,36
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Most pre-amp modules can be driven by the PSU driving the main power amp. A separate PSU 30 is available purely for pre amp modules if required for £5.47 (inc. VAT). Pre-amp and mixing modules in 18 different variations. Please send for details.

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MOS 128	60	4-8	<0.005%	<0.006%	± 45	120 x 78 x 40	420	£30.41
MOS 248	120	4.8	<0.005%	< 0.006%	± 55	120 x 78 x 80	850	£39.86
MOS 364	180	4	<0.005%	< 0.006%	± 55	120 x 78 x 100	1025	£45,54

Protection: Able to cope with complex loads without the need for very special protection circuitry (fuses will suffice).

Slew rate: 20v/µs. Rise time: 3ys. S/N ratio: 100db
Frequency response (~3dB): 15Hz - 100KHz, Input sensitivity: 500mV rms Input impedance: 100K \(\Omega \) Damping factor: 100Hz > 400.

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Model Number	For Use With	Price inc. VAT		
PSU 41X PSU 42X PSU 43X	1 or 2 HY30 1 or 2 HY60, 1 x HY6060, 1 x HY124 1 x HY128 1 x MOS128 2 x HY128, 1 x HY244	£11.93 £13.83 £15.90 £16.70 £17.07		

Model Number	For Use With	Price inc. VAT
PSU 52X	Z * HY124	£17.07
PSU 53X	2 x MOS128	£17.86
PSU 54X	1 x HY248	£17,86
PSU 55X	1 x MOS248	£19.52
PSU 71X	2 x HY244	£21,75

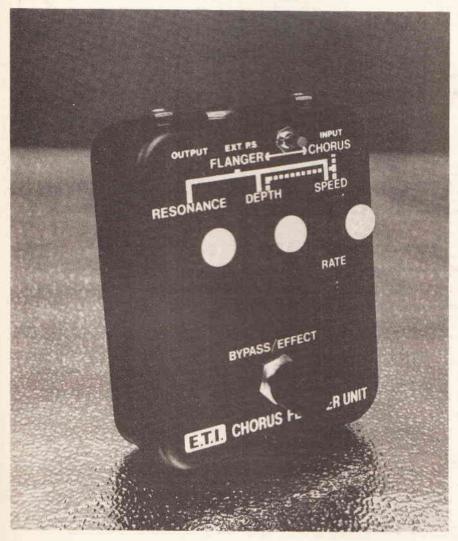
Model Number	For Use With	Price inc.
PSU 73X PSU 74X	2 x HY248 1 x HY364 1 x HY368 2 x MOS248,1 x MOS368	£22,54 £22,54 £24,20 £24,20

Please note: X in part no, indicates primary voltage. Please insert "O" in place of X for 110V, "1" in place of X for 220V, and "2" in place of X for 240V.

ILP Electronics Ltd., Dept 2, Graham Bell House, Roper Close, Canterbury CT2 7EP, Kent, England. Telephone: (0227) 54778 Technical (0227) 64723. Telex: 965780.

CHORUS/ FLANGER UNIT

Tim Orr returns to the pages of ETI with a project to make your amplifier see double — a chorus/flanger.



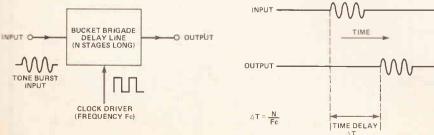


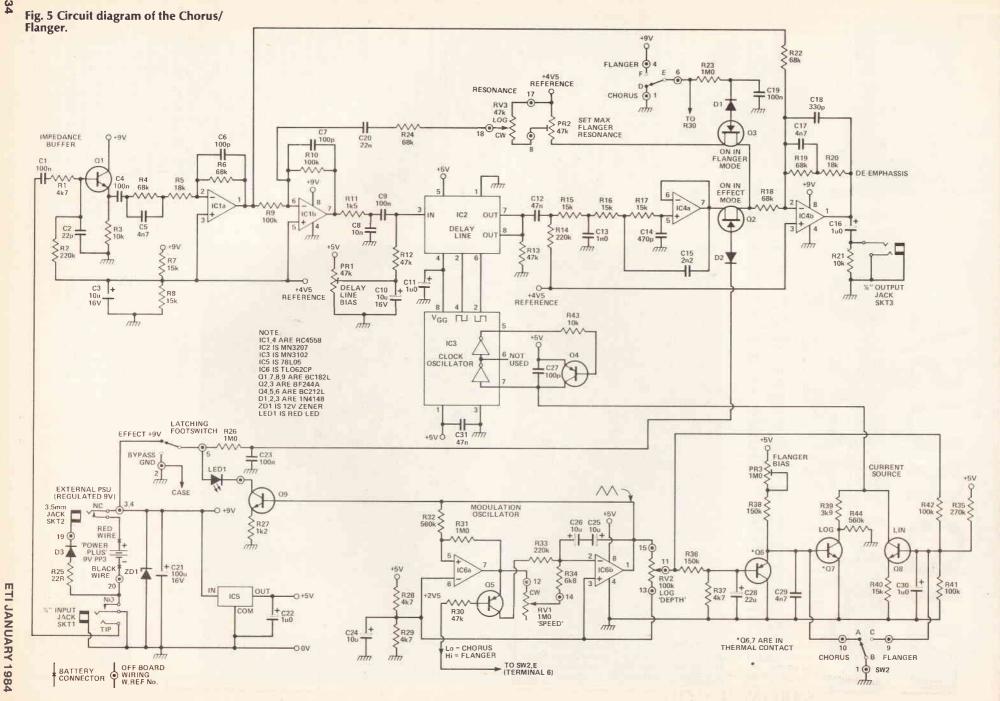
Fig. 1 The basic principle of producing a time delay.

he Chorus/Flanger unit is a device for processing musical and other signals to produce a wide range of effects. The electronics have been optimised for an electric guitar input but the unit can run equally well from line level signals (—6dBm) and high output microphones.

The chorus effect simulates a second instrument, which is producing the same sound as the input signal, but which is slightly delayed in time. This tends to generate the illusion of a second instrument and also enriches the overall sound quality. If a relatively fast (10Hz) time modulation is used, then genuine vibrato is generated. Flanging is a very dramatic colouration of the input sound. An instrument played through a flanger sounds like it is being heard in a drain pipe, the size of which is changing!

Flanging, chorus and vibrato are all time delay effects, and so their implementation is relatively simple if we use a bucket brigade delay line, Fig. 1. Voltages presented to the input of the delay line are sampled and then converted into small quantities of charge. These charges are passed along several hundred electronic 'buckets' until they reach the output, whereupon they are reconverted back into the original voltage. This process takes time, in fact the time delay is equal to the number of buckets divided by the speed at which the charge is passed along the line. The signal recovered at the other end very closely resembles the input signal except for a small amount of noise and distortion (it's an imperfect world).

As this is a sampled information system we must sample the input signal much more frequently than the highest frequency compon-



PERLIBARA PRE BUCKET OWPASS BRIGADE DELAY LINE EMPHASSIS LOWPASS FILTER FILTER ntn FEED FORWARD CLOCK Fig. 2 General block diagram of the chorus/flanger.

DEPTH

nents of the input signal. By doing this, we can avoid the dreaded aliasing distortion (which sounds like ring modulation) and hope to recover the input signal with some degree of integrity.

The general block diagram of the chorus-flanger unit is shown in Fig. 2. The low-pass filter at the front end of the unit limits the input bandwidth and so helps to avoid any aliasing problems. The low-pass on the output recovers the delayed signal and rejects unwanted high frequency clock

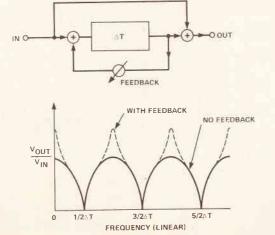
and noise signals.

The audio signal is given a treble lift (pre-emphasis) at the front end of the unit and a treble cut (de-emphasis) at the output. This helps to produce a better signal to noise ratio throughout the unit: most natural sounds have an energy spectrum that drops off very rapidly with increasing frequency, so by giving a frequency lift to these parts of the spectrum, more information can be elevated above the noise floor of the delay line. At the output end of the system, the de-emphasis restores the overall frequency response back to a flat one, but also suppresses high frequency noise from the delay

The rate at which the information passes through the delay line is set by the clock driver: this is a high frequency oscillator which can be frequency modulated. The delay line (MN3207) has a delay length of 512 buckets, so a clock frency of 512 kHz will produce a delay time of 1 millisecond. The modulation oscillator is used to produce slowly-varying time delays of variable speed and depth.

The chorus-flanger unit has been configured to look like a comb filter, Fig. 3. This is a filter

IC2 PIN 3



NOTCH SEPARATION = 1/AT Hz

Fig. 3 A basic time delay comb filter.

HOW IT WORKS.

Q1 forms a conventional high-impedance buffer: experience has shown that electronic guitars sound better when presented with a fairly high input impedance.

IC1a performs signal pre-emphasis, lifting all frequencies above about 500 Hz; IC1lb performs the low-pass antialiasing filtering, as well as mixing the fed-back proportion of the delayed output (which comes in via RV3, R24 and C20).

PR1 sets the DC bias level of signal going to the input of the bucket-brigade device: this is needed to obtain minimum signal distortion. The output from IC2 is recovered by the low-pass filter around IC4a, and passed to the FET signal switch, Q2 (FETs are used rather than mechanical switches to save loudspeaker cones!). Q2 allows the signal to pass except when the unit is in the bypass mode.

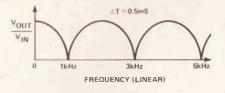
Q3 is another FET signal switch, and when the unit is in the flanging mode, this feeds a proportion of the delayed signal back to the input via PR2, the resonance control RV3, R24 and C20. At the same time, the fed-forward signal and the delayed signal are combined by IC4b, which also performs the de-emphasis. From here the signal is passed to the output.

IC6 forms a simple triangle/squarewave oscillator. RV1 controls the oscillation speed, Q5 is used to limit the low frequency range of the oscillator when in the chorus mode.

O9 is used to drive the panel LED. When the effect is selected (via the footswitch) the LED will light up and flash at the modulation rate.

IC3 and Q4 form the clock oscillator for the delay line. C27 is charged up by either Q7 or Q8, both of which act as current sources. When pin 7 of IC3 drops below about +2.5 V, pin 5 of the same IC goes low, which turns on Q4, which discharges C27 back up to +5V. Thus the circuit oscillates at a rate determined by the size of the current sink from either Q7 or Q8. In the chorus mode Q8 generates a linearly varying current over a maximum two-to-one range, C30 limits this sweep at faster rates. In the flanger mode, Q6 and Q7 generate an exponentially varying current over a seven-to-one range. Again the modulation depth is limited at fast rates by a capacitor,

IC5 provides a stable +5V power supply for the modulation oscillator, clock oscillator and the delay line. Battery voltages droop with time! The battery starts life at about +9.5 V and has an end of useful live at about 6.5 V. For maximum battery life, plug in the effect unit only when it is needed and never leave it on over night. The ON/OFF switch is the input jack which has a switched earth pin. For infinite battery life use a mains power supply (a PP3 eliminator)!



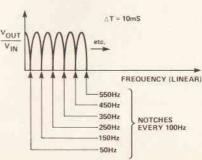


Fig. 4 Comb filter frequency responses for different time delays.

with a frequency response that is full of notches, and which looks like the teeth of a comb! When the delayed signal is 180° out of phase with the direct signal, then cancellation will occur and a notch in the frequency response is generated. These notches are linearly spaced with a separation of 1/(the time delay). Feedback around the delay line (used in flanging) makes the comb response much more peakey when the phase shift around the delay line is zero. Short time delays produce few notches and long time delays produce several, Fig. 4. Note that the frequency separation of the notches is linearly proportional to the clock frequency.

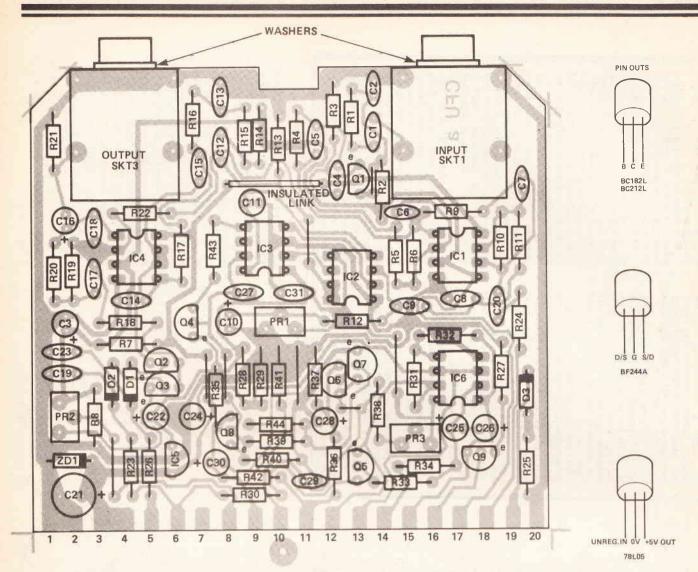


Fig. 6 Overlay diagram of the PCB for the Chorus/Flanger

PARTS LIST_

RESISTORS (all	1/4 W 5%)	POTENT	TIOMETERS	C29	4n7 ceramic
R1	4k7	RV1	1M0 reverse logarithmic	C31	47n polyester
R2	220k	RV2	1M0 reverse logarithmic 100k logarithmic		
R3	10k	RV3	47k reverse logarithmic		
R4,6	68k	PR1,3	47k preset	45,41601	IDIIGTORG
R5	18k	PR2			DUCTORS
		r K2	1M0 preset	IC1,4	RC4558
R7,8	15k			IC2	MN3207
R9,10	100k			IC3	MN3102
R11	1k5	CAPACI	TORS	IC5	78L05
R12,13	47k	C1,4,9	100n polyester	IC6	TL062CP
R14	220k	C2	22p ceramic	01.7.8.9	BC182L
R15,16,17	15k	C3,10	10μ 16V PCB electrolytic	Q2,3 Q4,5,6 D1,2,3 ZD1	BF244A
R18,19,22,24	68k	C5	4n7 polyester	04 5 6	BC212L
R20	18k	C6,7	100p ceramic	D1 2 3	1N4148
R21	10k	C8,7	10n ceramic	7D1	BZY88-12V zener
R23,26,31	1M0			LED1	0.2" red LED
R25	22R	C11,16	1μ0 63V PCB electrolytic	LEDI	0.2 red LED
R27	1k2	C12	47n polyester		
R28,29,37	4k7	C13	1n0 polyester	AUCCELL	NEOUS
R30	47k	C14	470p ceramic	MISCELL	
R32	560k	C15	2n2 polyester	SKT1,3	14" mono switched jack
R33	220k	C17	4n7 polyester		sockets
R34		C18	330p ceramic	SKT2	3.5 mm mono jack sock
	6k8	C19	100n polyester	SW1	latching footswitch SPC
R35	270k	C20	22n polyester		plus cap
R36,38	150k	C21	100μ 16V PCB electrolytic	SW2	DPDT switch
R39	3k9	C22.30	1µ0 63V PCB electrolytic		bs; PP3 battery connec
R40	15k	C22,30 C23	100n polyester	case: sel	f-adhesive foam strip
R41,42	100k	C24 25 3	26 10μ 16V PCB electrolytic	securing t	the PCB); 8-pin IC socket
R43	10k	C27	100p ceramic	off) hold	er for LED; wire, solder,
R44	560k	C28	22μ 16V PCB electrolytic	con Les D	aul Special, etc.

PROJECT: Chorus/Flanger

Assembly And Setting Up

Assemble the PCB and connect to the controls as shown in Figs. 6 and 7. When testing is complete, the PCB is mounted in the box, supported by the jack sockets, with the foil side to the case bottom. Put some thin sticky-backed foam rubber on the inside of the case bottom to prevent shorts.

Table 1 shows various DC test voltages around the circuit and Fig. 8 shows some of the waveforms you should find using an oscilloscope. As regards the setting of the presets, you can just plug in, switch on and hope for the best and set the presets by trial and error, but if you do have access to

INSIDE VIEW OF CASE

Table 1 DC test voltages.

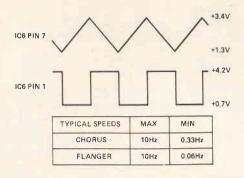


Fig. 8a Waveforms for the modulation oscillator; note that the voltage levels for IC6 are only approximate, as are the oscillator frequencies.

some test gear, here is the proper way to set up the unit.

Inject a 2.0 V peak-to-peak 500 Hz sinewave into the input socket, and select chorus on SW2 with the footswitch, SW1, set to effect. Set the rate control to maximum and the depth control to minimum. Using an oscilloscope, check that the undistorted signal is present at

(19)

EXTERNAL POWER

SKT2

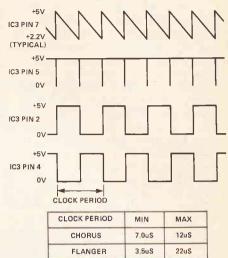
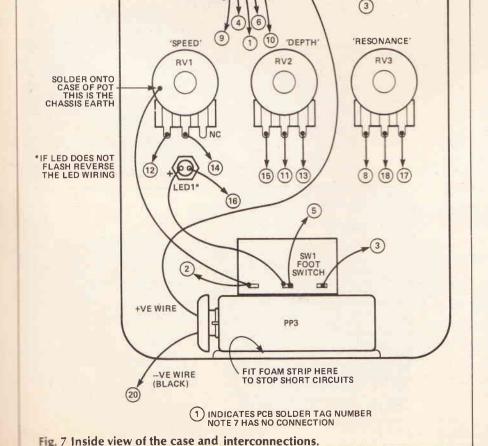


Fig. 8b Waveforms for the clock oscillator; select minimum depth (RV2) for these waveforms. The table shows the limits of the clock period for depth set to maximum and rate set to minimum; the preset PR3 should be adjusted to bing the oscillator into the range given for the flanger mode (with the flanging effect selected).

Q1 emitter, IC1 pins 1 and 7 and IC2 pin 3.

Set PR1 to its mid-way position and look at the signal present on IC2 pin 8; adjust PR1 until the signal is clipping symetrically (see Fig. 9). Note that this signal will have a lot of high-frequency clock signal breakthrough: this is normal.

Examine the output at IC4 pin 7; this should be the same signal without the HF breakthrough. Reduce the input signal level to remove the clipping on this signal. Turn the depth control to maximum and the sinewave at IC4 pin 7 will be frequency modulated by the modulation oscillator; a mixture of this signal plus the direct signal should appear at IC4 pin 1.



IC2 PIN B

HIGH FREQUENCY
CLOCK BREAKTHROUGH

Fig. 9 Waveforms at the input and output of IC2.



PROJECT: Chorus/Flanger

The flanging effect is best tested with a 200 mV P-P square wave oscillating at 2 Hz. This excites the unit with two clicks per second. Set resonance to maximum, speed to minimum and SW2 to the flanger position (footswitch SW1 should still be set to effect and not bypass). Listen to the output from the unit via a suitable amplifier, and adjust PR2 so that the output is a rich 'drainpipe' sound (you'll hear what we mean). If PR2 is set for too much feedback, the unit will oscillate; if this occurs back off the control a little.

For both chorus and flanging effects, the time modulation depth reduces as the modulation speed increases. The modulation depth at 10 Hz should produce a pleasant vibrato effect, caused by a small time delay sweep.

Power Supply

The unit consumes about 1mA. Using an Ever Ready PP3PP (power plus) for two hours per day, the expected battery life will be about 20 hours. If you leave the unit turned on over night, you will exhaust the battery. It is possible to use a rechargeable Nickel Cadmium PP3 battery. This has a shorter discharge life time of about 7 hours, but can be reused (charged/discharged) about 600 times! The purchase price of Nickel Cadmium batteries is about six times that of a standard PP3, and also you will need a charger unit. A non rechargeable alkaline PP3 battery (eg Duracell type) gives about four times the energy content of a zinc carbon PP3 but costs about twice as much.

A 9V battery eliminator can be used, the operating power is then derived from the mains. Note that the inner connection is +9V and the outer is 0V; if the polarity is reversed, D3 should prevent any damage to the chorus flanger, but the unit will not work.

BUYLINES.

A full kit of parts for this project is available from Sola Sound Ltd, for £49.95 all inclusive. Alternatively, some of the more unusual parts are available as follows: PCB £1.15 inclusive; case (fully screened) £3.75 inclusive; MN3207/MN3102 (IC2 and 3) £13.80 the pair. All these prices include VAT and postage. Sola Sound Ltd may be found at 18 Barton Way, Croxley Green, Rickmansworth, Herts. (Note that the PCB will not be available through the ETI PCB service.)



User Guide

Plug in the guitar and the amplifier. Press the footswitch so that the LED is off. Turn up the guitar volume, set up the amplifier level and tune the guitar. This is the BYPASS mode.

Vibrato

Set up the controls as shown, with SPEED and DEPTH at maximum. RESONANCE is inoperative. Press the footswitch so that the LED is flashing. Play the guitar. A fast (10Hz) vibrato will be heard. If necessary alter the guitar and amplifier levels. Adjust both controls for less depth and different vibrato rates.

Chorus

Set up the controls as shown, with the DEPTH set to maximum and a SPEED setting of about 1 flash per second. RESONANCE is inoperative. Play the guitar. A "creamy" sound will be heard. Press the BYPASS footswitch and see how flat the original signal sounds. Go back to the effect and try some different SPEED and DEPTH settings.

Flanging

Set up the controls as shown with DEPTH and RESONANCE to maximum and SPEED to minimum. Tap the guitar strings. A slowly sweeping "drain pipe" resonance will be heard. Try playing a melody with a rhythm that has the same period as the sweep time. Try other control settings.



AUTUMN 1983

MARKETPLACE

NEW SALES COUNTERS OPEN

Portsmouth, Broxbourne & Brentwood all benefit from newly fitted sales counters

Ambit's unique range of electronic components, kits, tools, test equipment and modules is now available to industry and enthusiast from two new regional sales counters — as well as Brentwood. The Portsmouth sales counter is installed in Solent Components Supplies building, at 53 Burrfields Road where Mark Goulty

will be pleased to assist with your requirements, and also offer products from Solent's own extensive stocks of Cooper tools, Multicore solder, Bulgin connectors, panelware and hardware. C&K switches and Alpha Wire.

The Broxbourne sales counter is operated under the auspices of David Scott from





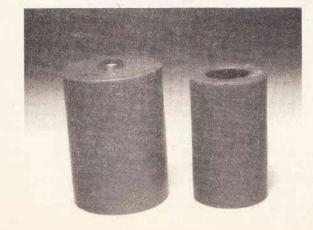
the premises of Broxlea Limited, at Park Lane Broxbourne.

If the product you want is not available in stock at the sales counter, then leave your order with our manager: either for direct delivery from our central stores (no post charge), or for later collection. We're here to serve you, so get to know your local Ambit sales facility.

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BATTERY ADAPTORS—



--- never be caught without a suitable battery!

These novel adaptor sleeves will allow 'AA' to fit in 'C' or 'D' slots, and 'C' into 'D'. Use our generously priced NiCads and chargers (Page 11) for a complete solution to all your battery problems.

4 SETS FOR **£2.00** 96-02001

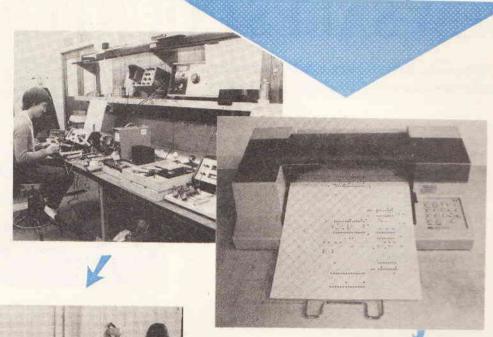
Introducing BROXLEAT MANUFACTURING

Problem solutions for hire

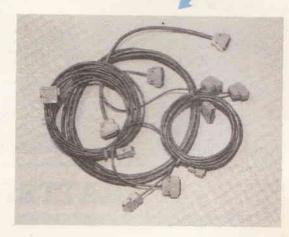
Broxlea, of Park Lane Broxbourne is the home of our North London sales counter, and the site of one of the industry's longest established manufacturers.

Broxlea specialises providing experience in a range of manufacturing and product 'management' services that many new idea-based electronics companies find virtually impossible to locate when setting out to manufacture a new product. Things like where to source parts (at the right price). what standards apply, how to optimise a design for the best ease of manufacturing.

Broxlea's energetic MD, Peter Telling, can provide on-site assessment of your requirements









a solution to your and manufacturing problems. Let your firm explore the benefits of a partnership that enables you to specialise in your own field, and not suddenly find yourself bogged down in the intricacies of production techniques, soldering at the right temperature, and simply sticking the right parts in the right places on the PCB.

The manufacturing facilities controlled by Clifford Bulgin include the most modern flow solder plant, a team of consciencious and thorough staff, experienced in electronic electrical assembly techniques, test and QA.

Apart from supplying manufacturers' services, Bruxlea specialises in supplying a range of top quality standard and custom 'D' series cable assemblies and accessories based on universally approved and accepted cables from Alpha Wire. Hand soldered crimted and IDC terminaters are available to order

A.F.BULGIN INVESTINTHE FUTURE

The long established component firm consolidates its subsidiary activities.

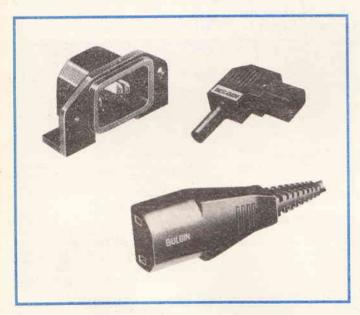
There are few participants in the electronics business who will not have come across some of the different connectors, many fuseholders, plugs, sockets, knobs etc., that are made by A. F. Bulgin & Co. PLC, of Bypass Road, Barking. 60 years in the unusual in business is electronics, and in order to establish plans that ensure the name of Bulgin will be carried forward through the next 60 vears, Chairman Ronnie Bulgin and his board have decided that diversification is one of several moves to be made.

The distributive activities and associated skills of Ambit have been acquired to preceed the formal consolidation of AFB's external business interests in Portsmouth (Solent Component

Supplies), Croydon (Projex Distribution Ltd.) and Broxbourne (Broxlea Limited) into a separate holding group.

The new group combines established experience in many aspects of the industry with the drive and enthusiasm of a relatively young management team. The in-group facilities include all the necessary resources to design, develop, source, manufacture and distribute a very large range of electronic products.

Ambit's innovative REWTEL direct order placement system caused quite a stir in the distribution industry, since it demonstrated the first keyword index information and bulletin service, combined with direct on-line order interrogation facilities.



Hardware versatility

The product range for which A.F. Bulgin & Co. PLC has become most famous over the past 60 years is probably its range of connectors, fuseholders and panel hardware.

The popular IEC connector range is continually being updated. There are now PC mounting types, filter inlet sockets and many other variations on the theme. Although now largely replaced in mains voltage applications by the IEC families, the round plug

and socket series has been brought right up to date with the "Buccaneer" range of water resistant housings, offering a wide variety of connection options, including BNC coaxial, 3 and 6 pole types.

As with all the mains rated components, the fuseholders comply to the latest BS safety specifications to ensure acceptability of equipment and freedom from the unexpected shocks that can arise from the use of improperly designed parts.



OPENING HOURS

Consumer admin:

(0277) 230909 - 4 lines

Availability of goods Credit card orders

Ask for (credit card sales) 9-5.30 Customer Service problems with deliveries 10-12.30 Ask for 'Customer Service'

Industrial sales, admin & progress:

(0277) 231616 - 4 lines

Availability, price, telesales

Keith Collins	9-5.30
Claire Mackessy	9-5.30
Carol Lawton	9-5.30

Shop Sales

Brentwood Mon-Sat	9-5.30
Lunch	1.30-2.30
Broxbourne Mon-Fri	9-5.30
Sat	9-12.30
Portsmouth Mon-Sat	9-5.30

Apart from "own brand" products, A.F. Bulgin handle a number of agencies on behalf of overseas manufacturers of complementary products — most notably the superb range of control knobs from Ritel of Switzerland, a very large selection of which are available from Ambit stock and detailed in the current catalogue.

Many lines are custom manufactured, taking advantage of Bulgin's unrivalled experience, extensive in-house tooling facilities and automatic injection molding plant. If your firm requires either a variation on a standard theme, or a completely new type of small plastic/metal component, then let us quote you for supplying it from one of the few remaining sources of British component manufacturing expertise.

Telephone Timing



Help us to help you!

When calling our central sales and service departments at Brentwood, it would help us a great deal if you would observe the following timing. At present we tend to get all the calls arriving at peak periods, when other times the lines are deserted.

We get many reports of difficulty in getting through, but it's not for lack of incoming lines! Please use the numbers designated for the nature of your enquiry, it is sometimes not possible to transfer between industrial and consumer sales due to the volume of telephone traffic.

The peak time for consumer telesales is 10.15—10.45 and 2.30—4pm. If you can avoid these, then so much the better for you and us. Telesales operate Monday to Saturday, 9.00am to 5.30pm — although you can frequently place an order outside these 'official' times.

Industrial sales calls tend to arrive (understandably) in the 2.30—4pm slot as well: remember that telex is a particularly useful medium as our telex is situated in the middle of the IM department.

We like to deal with customer service problems during the morning (10am-12.30pm) so that we have all afternoon to sort the problems out and 'catch the post'.

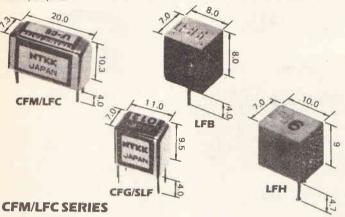
REWTEL provides on-line sales and stock enquiry facilities. (0277) 232628, a 300 baud modem and any one of a wide selection personal computers can be used to check stock and place orders, 24 hours a day, 365 days a year (less downtime!). Send an SAE marked 'REWTEL info' in the bottom left corner for more details. '

ambit for communications components

The most comprehensive selection of coils, filters and components for all types of radio communications

CERAMIC FILTERS FOR 455kHz IFs

Ambit's range of ceramic filters cover most applications for communication and high quality broadcast reception. As far as we are aware, we hold the widest range of ceramic and crystal filter products anywhere in the world, and we will always do our best to assist if the type you want isn't immediately obvious from checking this section. We regret that we cannot generally assist in supplying replacements for imported equipment, unless the manufacturer's type number is available in addition to any 'house' numbers used to identify the parts.



A medium priced hermetically sealed ladder filter, suitable for most communications applications and high quality broadcast receiver equipment. Similar to the types used in receivers such as the FRG7

Туре №.	-6dB BW	-50dB BW	In/Out Impedance (k ohm)	Stock No	Price
CFM455H/LFC6	6	16	1.5	16-45520	5.20
CFM455G/LFC8	8	20	1.5	16-45521	5.20
CFM455F/LFC12	12	24	1.5	16-45522	5.20
CFM455E/LFC15	15	28	1.5	16-45523	5.20
CFM455D/LFC20	20	38	1.5	16-45524	5.20
A high performance	filtor aimilarta	those wand is	+h - Danoo - 155	11 00 11	

A high performance filter, similar to those used in the R1000 and FRG7700, Ideal for all low cost SSB filter requirements, and suitable for upgrading existing equipment

CFM455J1 2,6kHz min 8kHz max 2k 16-45513 **9.00**

CFG/SLF SERIES

A miniature high performance filter. Possibly the highest selectivity/size ratio available. Supplied in shield and hermetically sealed case, and recommended for use with designs involving the MC3357/9 and ULN3859 families, due to the excellent stopband performance.

Type No.	-6dB	BW	-80dB BW	In/Out Impedance (k ohm)	Stock No	Price
CFG4551/SLFD4	4		10	1k5	16-45542	5.20
CFG455H/SLFD6	6		15	1k5	16-45542	5.20
CFG455G/SLFD8	8		18	1k5	16-45544	5.20
CFG455F/SFD12	12		25	1k5	16-45546	5.20

LFB/LFH SERIES

Probably the most popular types of low cost ceramic ladder filter — found in most types of CB transceiver, and an increasing number of designs for commercial mobile radio systems. These filters possess excellent bandpass characteristics, although watch the stop band if you are not using them with some form of 'roofing' selectivity, such as a 2 or 4 pole crystal filter at 10.7MHz/10.695MHz. The impedances of these filters (and most of the other ladder series) is directly matched by such devices as the ULN3859, so extremely compact designs can be achieved at minimum cost. Miniature 455kHz filters. I/P and O/P impedance 2k.

NTK/Murata	-6dBW (Min)	-40dB (Max)	Stock No	1-24	25-99	100+
LFB4	4kHz	15kHz	16-45511	1.95	1.45	1.10
LFB6/CFU455H	6kHz	18kHz	16-45512	1.95	1.45	1.10
LFB8	8kHz	21kHz	16-45529	1.95	1.45	1.10
LFB10	10kHz	23kHz	16-45514	1.95	1.45	1.10
LFB12/CFU455F	12kHz	26kHz	16-45515	1.95	1.45	1.10
LFH6S/CFW455HT	6kHz	14kHz	16-45525	2.45	1.95	1.55
LFH8S	8kHz	18kHz	16-45526	2.45	1.95	1.55
LFH12S/CFW455FT	12kHz	22kHz	16-45528	2.45	1.95	1.55

CERAMIC RESONATORS Low Cost, Small size alternative to Quartz Crystals

These resonators provide an excellent alternative to costly LF quartz crystals, and are especially suited to use with MPUs, rate generators, remote control systems, dial tone and dial pulse clocks etc. There are two basic types as with crystals — series and parallel resonant types. The majority of 'clock' applications will require the parallel resonant types (CRM), whereas 'bypass' and 'trap' circuits will usually call for the series (CFE) types.

Туре	Frequency	Mode	Stock No	1-24	25-9910	0+
CRM455	455kHz	parallel	16-45573	0.60	0.48	0.40
CRM460	455kHz	parallel	16-46073	0.60	0.48	0.40
CRM500A	500kHz	parallel	16-50073	0.60	0.48	0.40
CFE455	455kHz	series	16-45575	0.60	0.48	0.40
CRM560	560kHz	parallel	16-56074	0.60	0.48	0.40
CSA1.0MK	1000kHz	parilei	16-10003	0.94	0.84	0.76
455D	455kHz	NBFM Disc	16-15455	1.20	0.90	0.60

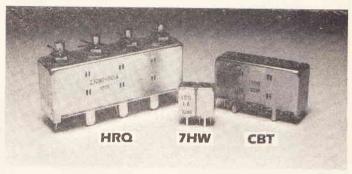
CRYSTAL FILTERS

We are pleased to be able to extend our range of crystal filters to include the popular 10.695MHz frequency that seems to be universally adopted in the first IF of CB receivers. A transplant of the 2 pole filter in place of the usual ceramic filter can perform the single most significant improvement in blocking and cross mod in most circuits and the popularity of the modification has spurred us to include an 8 pole version for the purist. The 90dB adjacent channel attenuation of the 8 pole series effectively removes all responsibility for blocking and IM related problems from the subsequent stages, and places emphasis on the RF and most crucially the mixers. The 10.7MHz 8 pole SSB filter is featured in the R&EW HF transceiver add-on for the R1000 or FRG7700 receivers and is at last managing to dispell the mystique that surrounds 9.0MHz.

2 POLE TYPES

		-						
Model	Centre Freq.(Mil-	Band lz) Width(k	Ripple Hz) (dB)	Stop Band (kHz)	Term Imp(kR)	Case	Stock No.	Price
10M15A	10.7	15(3dE	3) 0.5	±25_0(18dB)	3.0	FS12	20-10152	0.99
21M15A	21.0	15(3dE	3) 0.5	±25 0(17dB)	3.0	FS12	20-21152	3.45
10M08AA	10,695	8kHz	0.5	±25.0(18dB)	1.8	FS12	20-11152	3.49
0.001.5	7/05/							
8 POLE	ITPE	•						
10M22D 10M8D	10,7 10.7	2,2(6dB) 8(6dB)		±2.4(60dB)	0.5	FS23	20-10028	17.20
10M8DB	10.7	7(3dB)	2.0	±11.0(80dB) ±12.5(90dB)	3.0	FS22	20-10088	15.50
10M15D	10.033	15(6dB		± 20(80dB)	3.0	FS22 FS22	20-11088 20-10158	14.50
21S08DA	21.4	7(3dB)	2.0	±12.5(90dB)	.850	S2	20-02108	14.50 15.65
		,,,,,,,	214	_ 12,5(0000)	.030	02	20-02100	15.05
Case Code	L	w	н					
FS22	18.5	12 1						
FS23	23.0	12 19						
S2		8.5 11.5						

HELICAL FILTERS Low cost filters for VHF/UHF



STOCK TYPES 7HW — 2 CHAMBER

Toko Part No.,7HW 252MT1001A 252MT1090A 252MN1127A 252MN1111A	Freq. MHz 435 470 463 432	z in/out 50 50 50 50	1dB BW 12MHz 8MHz 12MHz 7MHz	Atten./MHz off centre 23dB/+30 29dB-30 23dB+30 27dB-30 15dB Min±30MHz 18dB Min±30MHz	Ins loss (max) 4dB 5dB 2dB 5dB	Stock No. 17-10011 17-10901 17-11271 17-11111	Price 1.85 1.85 2.25 2.25
STOCK TY	PES HI	RQ — 4	CHAN	IBER			
Toko Part No. HRQ 232MT1001A 232MT1021A	Freq. MHz 435 470	Z in/out 50 50	3dB BW 10MHz 6MHz	Atten_/MHz off centre 28dB+1531dB-15 28dB±1531dB-15	Ins loss (max) 4dB 8dB	Stock No. 17-10010 17-10210	Price 7.90 7.90
STOCKTY	PES CE	3W — 2	CHAM	IBER			
Toko Part No. CBW 271MT1006A 271MT1007A	Freq. MHz 145 170	z in/out 500 500	1dB BW 3.0MHz 3.5MHz	Atten/MHz off centre 25db Min±15MHz 20dB Min±15MHz	ins loss (max) 4.5dB 4.5dB	Stock No. 17-10062 17-10072	Price 3.15 3.15
STOCK TY	PES CE	3T-3	CHAMI	BER			
Toko Part No. CBT	Freq.	Z In/out	3d8 BW	Atten./MHz off centre	ins loss (max)	Stock No.	Price
272MT1006A 272MT1007A 272MT1019 272MT1008	145 170 160 145	500 500 500 50	2.8MHz 4.0MHz 3.5MHz 1.2MHz	25dB Min±6MHz 30dB Min±6MHz 20dB Min±6MHz 30dB Min±6MHz	8dB 6dB 6dB 8dB	17-10063 17-10073 17-10193 17-10083	3.15 3.15 3.15 3.15

SEE THE COMPLETE CATALOGUE FOR DETAILS OF

- ★ Coaxial relays PCB and connector types
- **★** TOKO IF transformers
- ★ TOKO block filters for video/radio
- **★** Fixed inductors
- * Quartz crystals

ambit for computer components

COMPUTER LEADS

To connect BBC/Acorn computer to cassette etc. 7 pin DIN plug to 2 x 3.5mm jack plugs and 2.5mm jack plug. Length

Stock No

Also for BBC/Acorn, 7 pin DIN plug to 3 pin DIN plug and 2,5mm jack plug, Length

Stock No Price

5 pin DIN plug to 2 x 3.5mm jack plugs and 2.5mm jack plug. Length approx.1m.

Stock No

Co-ax plug to phono plug. Length approx

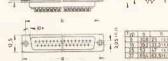
Stock No Price 03-10004

MIN'D'SERIES CONNECTORS

A range of high performance connectors available in 15 and 25 ways, all contacts are hard gold-plated on copper alloy. Mouldings are thermoplastic resin, glass-fibre filled and metal parts are galvanized and chromatized

Male and female connectors with solder cup termination max 0.5mm.

Type/Way	Stock No	Price
Plug/15	10-15100	1.30
Plug/25	10-25100	1.98
Socke/15	10-15200	1.80
Socket/25	10-25200	2.44



SOLDER PIN

Male and female connection with solder pin terminations. Max. 0.6mm. Suitable for vertical PCB mounting. Lead length 6mm.

Type/Way	Stock No	Price
Plug/15	10-15110	1.42
Plug/25	10-25110	2.15
Socke/15	10-15210	1.89
Socket/25	10-25220	2.55

RIGHT ANGLE

For PCB mounting right angle version with supporting bracket, Max, lead length 4mm,

Type/Way	Stock No	Price
Plug/15	10-15111	2.55
Plug/25	10-25111	3.40
Socke/15	10-15211	2.90
Cooket/25	10-25211	3.80

MOULDED COVER

Side entry cover with cable clamp, Moulded in thermoplastic resin, glass fibre

Ways	Stock No	Price
15	10-15122	0.76
25	10-25122	0.80

MICROPROCESSOR

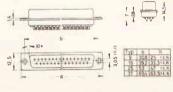
Z80 4MHz DEVICES

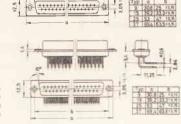
Туре

Stock No. Price

26-18400 3.40 26-18420 2.95

AND MEMORIES







MEMORIES

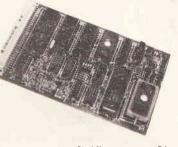
Popular static and dynamic RAMs and EPROMs. All are first grade types from well 26-18430 2.90 26-18410 7.30 26-18470 6.10 26-18441 9.50 26-18442 9.50 26-18149 8.90 known manufacturers Hitachi, Texas etc. Туре 6800P 6810P 6820P 6821P 6840P 6850P 6852P 68488P 6802 68A21F 68A40F 26-06800 26-06810 Note: The Z80A family may be 26-36116 26-02114 26-02112 25-02111 26-02102 26-06132 25-05101 6116-3 2114-L2 26-16800 26-16821 26-16840 26-16852 26-26800 26-26821 DYNAMIC 26-28400 8.85 68A521 68B00P 68B21P 68B40P 68B50P 68B52P

Z80BPIO	26-28420	8.45	Туре	Stock No.	Price
ZB0BCTC	26-28430	8.45	8254	26-08264	3.80
Z8671	26-08672	17.50	4116-2	26-24116	0.90
8080 1M	Hz SERII	ES	4116-3	26-34116	0.85
Туре	Stock No.	Price	UVEPR	OMS	
9080AP	26-08080	2.80	Туре	Stock No.	Price
3212	26-08212	1.65	2764	26-02764	6,39
8224	26-08224	1,90	2732	26-02732	4,00
8251	26-08251	3,40	2716	26-02716	3,00
8255	26-08255	2.58	2708	26-02708	2.00

Z-8 TBPDS

Z-8 TBPDS

Beware of immitations. Jon Burchell's versatile BASIC development system, based on the Z-8 basic/debug CPU is the most adaptable and understandable entry to the design on MPU based control systems. The Z8 TBPDS provides 8k x 8 RAM, 4k x 8 EPROM, containing utility software, and EPROM programming. The Z-8 TBPDS needs only to be connected to an RS232 terminal (or a home computer configured as one) to provide complete program development/support. Supported by regular features in Radio & Electronics World magazine, and now a line assembler and CPM based cross assembler is available for fast and versatile applications and development Further enhancements include an autostart board, to run the BASIC programme held in EPROM power-up.



	Stock No	Price
Built	40-00802	160.00
Built autostart	40-00811	6,50
7-8 Interconnect	cable connects 78 to 29	III cassette

interface, and RS232 terminal.

40-00810

Z8 Datapack, very complete documentation of Z8 BASIC, and Z8671 CPU Refundable against purchase of a Z8TBDS kit, (or built version)

02-00800

Z8 LINE ASSEMBLER

A 2732 EPROM, contains a Z8 line assembler, permitting the use of Z8 code in programme developments. The enormously enhanced speed of development and operation offered by this software development and operation online by this solive are tool places the ZB well ahead of the rival single chip MCUs for speed and versatility. The EPROM includes revised utilities written in code, and comes complete with extensive documentation to plug into your TBPDS.

	Stock No	Price
EPROM	49-07861	40.00

Z8EXEC

An operating system, in BASIC for the 28 Tiny Basic Development System. 28 Exec helps you create, save in an EPROM filing system, load and run programs with its 15 versatile commands. A real time clock and scheduler will allow programs to run at pre-selected times, Supplied in 3 EPROMS.

0: 131	D.1.
Stock No 49-07863	Price 45.00
43 07000	45,00

Z8 MCS

ZSMC.

From Jonathan Burchell's cornucopia of microprocessing delights comes the ZB single board computer: a 4 IC design capable of running BASIC/MC programs of up to 4K Bytes from switch-on. It is designed specifically to run the programs developed with the ZB TBDS, and rejoices in the usual features of the ZB: 16 perallel I/O lines, serial I/O etc. An approach that makes any other method of developing single-chip MCU's seem rather longwinded and unnecessary.



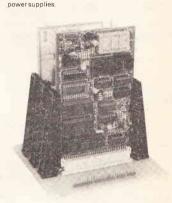
Available built-only a boxed version of the power supply with cassette interface for the Z8 TBDS computer development system. ±12V at 500mA, +5V at 1 amp, +25V 100mA, TTL data input, audio out to recorder.



Description	
Z8 PSÚ	

Z8 BACKPLANE As described in July '83 R&EW. Enables up to 2 Eurocards to be used in conjunction with the Z8 TBDS. Easy connections to I/O, RS232 ports and

40-00814



	Stock No	Price
Kit	41-00601	19.13
Built	41-00600	25,74

RS232 ADA

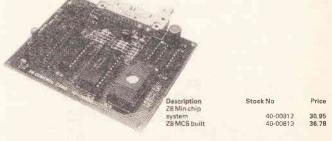
A serial interface A/D and D/A converter that provides easy communication with any RS232 port.

	Stock No	Price
Kit	40-90232	41,40
Built	40-99232	52.00

LOW COST A/D

Another conversion (September 1982) for the faithful from Jon Burchell, but this time a low cost approach with parallel interface. A good place to start when you want to explore the world outside your personal computer.

	Stock No	Price
Kit	40-42700	14,50



IDC and many other types in the catalogue. OEM's ask for details of our custom cable and termination facilities.

See our broad selection of computer books!

100W PA MODULE

All parts for the best 100W complementary amplifier yet published



Kit

41-00504 36.48

HEATSINK (2 required)

21-08035 8 60

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Very substantial 20A relay driven by the multifarious HA12002 amplifier monitor IC Protects against overload, temperature offset etc.

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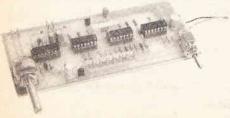
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A multi primary toroid designed specifically for the above

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Rectifier	90-00564	2.20

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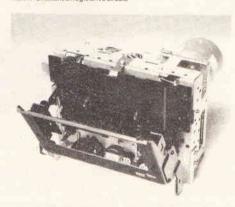
A high quality means of preventing amplifier overload in HiFi, PA or Broadcast systems.



Kit 41-00501 £13.82

ELECTRONIC CASSETTE

A fully solenoid operated cassette mechanism, featuring front loading and simple electronic control. Complete with Canon permalloy stereo head — although various others can be fitted if required. This is the current stock deck — QEM's can obtain details of the broader range available by contacting Ambit Industrial Marketing. Full specification and drawings on request, together with alternative head options for large volume users. Position counter available soon. See August R&EW for details of logic drive circuit.

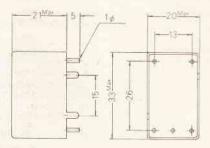


SPECIFICATION:
Rated Operating Voltage: Motor +12VDC ±10%, Solenoids +12V DC ±10%. Installation: Vertical or Horizontal. Wow and Flutter: >0.08% WRMS (>15) [Test Tape: TEAC MTT-111). Spooling Time: FF or REW >115 seconds (TDK DC-60). Tape Speed: 3,000Hz±2% Motor Consumption: (Play, FF, REW)-100mA. Heads - REC/REP: Canon H3332-0202 (2 channel sendust). Erase: Canon H53211-02 (2 channel, double gap, metal capable)

Description	Stock No.	Price
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Pre-aligned oscillator block for bias and erase use in cassette and tape decks. High stability push-pull oscillator, with shielded case.

Supply Voltage: 16V DC. Current consumption: <50mA. Osc Frequency: 100±5kHz. Recording Bias Current: 500uA per head. Erase current: 80mA. Erase current distortion: <0.6%, Impedances: Erase Head: 300R @50kHz. Temperature Range: ~20°to +70°C.

Туре	Stock No.	Price
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PPM SYSTEMS TO DIN45406

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"		11100
PPM302/24	50-30201	114.92
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LOW COST PPM SYSTEMS

The PPM402 is a meter movement and Drive Amplifier card combination forming a cost effective peak programme meter of high quality and reliability. The driver consists of a variable sensitivity input stage, precision full-wave active rectifier and output stage with a transfer characteristic suitable for the meter scale. Each driver and meter is individually aligned to be within published data so that repeatability of response is guaranteed. In operation this means that repeatability of response is guaranteed. In operation this means that peaks are not only captured, but also valued closely to what the ear may perceive. PPM402/24 drive amp, card with size 24 meter. PPM402/34 drive amp, card with size 34 meter. PPM402/K drive amp kit with size 34 meter.

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PPM 121 (ENCAPSULATED)

Fram 121 (ENCAPSULATED)
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Small external component count.

Maximum opportunity for user options.

Two-point lineup.

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Card to affix to meter		

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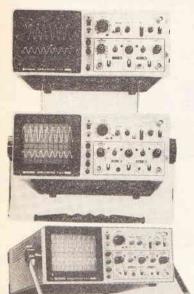
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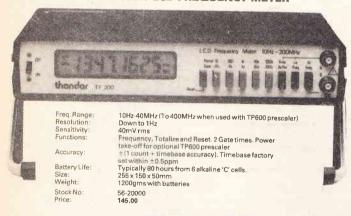
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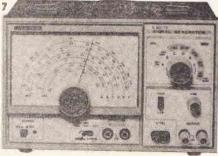
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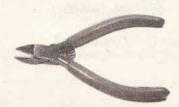
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BC307 = 58-00307 BC308 58-00308	0.08 BD18 0.08 TIP3		0.41 0.35	U257B	61-00	0257 1.28	KB4436	61-04436	1.53
BC308 58-00308 58-00309	0.08 TIP3		0.35	U267B LM301AH	61-00 61-00		KB4437 KB4438	61-04437 61-04438	1.75 2.22
BC327 58-00327	0.13 MJ2		0.68	LM301AN	61-03		KB4441	61-04441	1.35
BC337 58-00337	0.13 2N30	58-13099	0.58	LM308CN LM311CN	61-03 61-00		KB4445 KB4446	61-04445 61-04446	1.29
BC413 58-00413	0.10 2SB		0.60	LM324 LM339N	61-03 61-03	3240 0.48	KB4448	61-04448	1,65
BC414 58-00414 BC415 58-00415	0.11 2SD 0.10 2SJ4		0.60 3.10	LM346	61-00		NE5044 MC5229	61-05044 61-05229	2,26 9,60
BC416 58-00416	0.11 2SJ5		4,25	LF347	61-00	0347 1.82	NE5532	61-55320	2,20
BC546 58-00546	0.12 2SJ8	60-01083	3.55	LM348 LF351	61-03 61-03	3480 1.26 3510 0.49	KM5624 SD6000	61-05624 61-06000	4,35 3,75
BC550 58-00550	0.12			LF353	61-03		SL6270	61-06270	2,00
BC556 58-00556 BC560 58-00560	0.12 2SK 0.12 2SK		4.25 3.55	LM380N LM381	61-00 61-00		SL6310	61-06310	2,00
BC639 58-00639	0.22 2SD		2.34	LM382 ZN419CE	61-00 61-00	0382 1,81	SL6600	61-06600	3,75
BC640 58-00640	0.22 SM3	159 58-03159	5.95	ZNA423	61-02		SAS6610 SL6640	61-06610 61-06640	1.48
MPSA13 58-04013	0.30 SM3	160 58-03160	5.95	ZN425E/8	61-04		SL6690	61-06690	3.75
MPSA63 58-04063	0.30			ZN426E/8 ZN427E/8	61-04 61-04		SL5700 SAS6710	61-06700 61-06710	3,20 1,48
ZTX108 58-01108 ZTX212 58-01212	0.10 0.10 TR	ANSISTORS		ZN428E/8 ZN429E/8	61-02 61-04	2480 5,50			
33 31212		POWER DEVICES		ZN432CJ10	61-04		ICM7555 ICL8038CC	61-75550 61-08038	0.98 4.50
				ZN433CJ10	61-04	4330 24.79	MSL9362	61-09362	1.75
2N2904 58-02904	0.25 Devi		Price	ZN450E NE542	61-04 61-05	5420 1,20	MSL9383 TK10170	61-09363 61-10170	1.7 <mark>5</mark> 1.87
2N2905 58-02905 2N3905 58-03905	0.25 MRF 0.10 MRF		3,20	NE544	61-00	0544 1.80	TK10321	61-10321	2.75
2SB646A 58-03646	0.10 MRF 0.30 MRF		16.50 40.00	NE555N NE556N	61-05 61-05		HA11223 HA11225	61-11223 61-11225	2,15 1,45
2SB648A 58-03648		449A 58-14449	16.50	SL560C	61-05		HA12002	61-12002	1.22
2SD666A 58-03666	0.30 MRF	5472 58-14472	1.25	NE564	61-00	0564 4.29	HA12017 HA12402	61-12017 61-12402	0,80
2SD668A 58-03668 2SA872A 58-02872	0.40 MRF 0.19 MRF		4.60	NE565	61-00	0565 1.00	HA12411	61-12411	1,20
2SA1084E 58-01084	0.19 MRF 0.25 PT8		4.99 9.50	NE566 NE567	61-00 61-00	0567 1,30	HA12412 LF13741	61-12412 61-13741	1,55 0,33
2SA1085E 58-01085	1	1945 58-01945	2.60	NE570N	61-00	0570 3.85	MC14412	61-14412	6.85
2SC1775A 58-01775		1971 58-01971	2.49	uA709HC	61-07	7090 0.64	MK50366 MK50375	61-50366 61-50375	3,36 3.85
2SC2646E 58-02546	0.24 _{2SC}	2053 58-02053	0.63	uA709PC	61-07	7091 0.52	MM53200	61-53200	3.90
2SC2547E 58-02547	0.24 2SC	2097 58-02071	14.75	uA710HC uA710PC	61-07 61-07				
	TP2:		10.24 0.95	uA711CN	61-07	7110 0.85	PRESCALERS, FREE		
TRANSISTORS	VN6	3866 58-03866	0.45	uA741CH	61-07	7410 0,66	DISPLAY AND SYN	Stock No.	1-24
Small Signal RF Devices	2N3		1.20	uA709PC	61-07	7411 0,22	U264	61-02640	2.27
, T				uA741CN uA748CN	61-07 61-04		U265	61-02650	3.16
Device Stock No.	Price			uA758	61-00		U266 11C90DC	61-02660 61-01190	2.43 12.95
BFY50 58-06500 BF241 58-06241	A 10	DDES		TBA820M TDA1028	61-00 61-01		MSL2312R	61-02312	3.94
BF273 Use BF241	Sig	nal, Rectifier, etc.		TDA1029	61-01	1029 2.11	MSM5523 MSM5524	61-05523 61-05524	11.30 11.30
BF274 Use BF241	Devi	ce Stock No.	Price	ZNA1034 LM1035	61-01 61-01		MSM5525 MSM5526	61-05525	7.85
BF362 58-06362	0.49 BA2	44 12-02447	0.17	TDA1054M	61-01	1054 1,45	MSM55271	61-05526 61-55271	7.85 9.75
BF440 58-06440	0.21 BA3		0.35	TDA1062 TDA1072	61-01 61-01		ICM7106CP	61-07106	9.55
BF441 58-06441 58-06479	0.21 ND4 0.66 OA9	981-7E 12-49817 1 12-00916	0.51 0.07	TDA1074A	61-01	1074 5.04	LC7137 ICM7216B	61-07137 61-72161	7.50 23.95
BF679S 58-06679	0.55 OA4		0.10	TDA1083 TDA1090	61-01 61-01		ICM7216C	61-72162	23.95
BFR91 58-07091	1.33 TDA	1061 12-10617	0.95	HA1196 HA1197	61-01 61-01	1196 2.00	SP8629	61-08629	3.85
BFR96 58-07096	1.45 PWC		0.75	TDA1220	61-01		SP8647 SP8793	61-08647 61-08793	6.00 7.70
BFT95 58-10095 BFW92 58-08092	0.99 SO4 0.60 W00		0.45 0.28	LM1303	61-01	1303 0,99	HD10551	61-10551	2.45
BFY90 58-09090	0.90 IN40		0.06	MC1310P	61-01	1310 1,90	HA12009	61-12009	6.00
NE21936 58-21936	5.00 INAC		0.07	MC1330 MC1350	61-01 61-01	330 1.20	MC12016 HD44015	61-12016 61-44015	6.90 4.45
ZTX323 58-06232 2N2369A 58-02369	0.80	12-40046	0.07	HA1370	61-11		HD44752 MC145151P	61-44752 61-14151	8.00 6.00
21423037	11/14		0.05	HA1388	61-01	388 1.75	MC145152P	61-14152	12.30
	IN54 IN62		0.16 0.62	LM1458N MC1496P	61-14 61-01	1580 0.45 1496 1.25	MC145156P	61-14156	4.60
TRANSISTORS		12 02007		SL1610	61-01	1610 2.10			
Small Signal RF FET/MOSFE	T			SL1611 SL1612	61-01 61-01	612 2.10	VOLTAGEREC	GULATORS	
	DIC	DES		SL1613 SL1620	61-01 61-01	613 2.55	Device Voltage	Stock No.	Price
	Price Val	ricap		SL1621	61-01	621 3.50	7805 +5V	27-78052	0.40
BF256 59-00256 BF960 60-06960	0.38 0.99 Devi	ce Stock No.	Price	SL1623 SL1625	61-01 61-01		7806 +6V 7808 +8V	27-78062 27-78082	0.40
BF961 60-06961	0.70 BA1		0.30	SL1630	61-01	630 1.62	7812 +12V	27-78122	0.40
BF963 60-06963	0.99 BA1	21 12-01215	0.30	SL1640 SL1641	61-01 61-01	640 3.50 641 3.50	7815 +15V 7818 +18V	27-78152 27-78182	0.40
BF981 60-06981	1.20 BB1		0.30 0.27	MC1648	61-01	648 3.25	7824 +24V	27-78242	0.40
J310 59-02310 J176 59-02176	0.80 BB1 0.65 BB2		0.27	TDA2002 ULN2240	61-02 61-02		7905 –5V 7906 –6V	27-79052 27-79062	0.49 0.49
MEM680 60-05680	0.75 BB2		1.95	ULN2242	61-01	090 3.05	7908 –6V	27-79082	0.49
2SK55 59-01055	0.32 ITT2	10 12-02105	0.30	ULN2283 CA3080	61-02 61-03		7912 -12V	27-79122	0,49
2SK168 59-01168		M115 Use KV1235		CA3089	61-03	1.84	7915 -15V 7918 -18V	27-79152 27-79162	0.49
3SK45 60-04045 3SK51 60-04051	0.49 MVA 0.54 KV1	AM125 Use KV1225 210 12-12105	2.45	CA3123 CA3130E	61-03 61-31	300 0.80	7924 -24V	27-79242	0.49
3SK60 60-04060	0.58 KV1		2.70	CA3130T	61-31	301 0,90	78L05 ±5V	27-78050	0.40
3SK81 60-04081	1.32 KV1		2,75	CA3140E CA3189E	61-31 61-03	400 0.46 189 2.20	78L06 +6V 78L08 +8V	27-78060	0.40
3SK88 60-04088	0.99 KV1	235 12-12355	2.75	CA3240E	61-32	400 1.27	78L12 +12V	27-78080 27-78120	0.40
40673 Replaced by 3S 40822 Replaced by 3S			2.55 0.40	MC3357 MC3359	61-03 61-03	357 2.85 357 2.85	78L15 +15V 78L24 +24V	27-78150	0.40
40822 Replaced by 3S 3SK112 60-04112	4,60 KV1		0.40	ULN3859	61-03	859 2.95	79L05 + 24V	27-78240 27-79050	0.40
00 04112	1.7.1	.2 .0200		KM3701 KM3702	61-03 61-03	701 85.53 702 74.84	78GKC +adj	27-78993	3.95
				LM3900	61-39	0.60	78GUIC +adj 78H05 +5V	27-78992 27-78054	1.10 4.25
				LM3909N LM3914N	61-39 61-03		78H12 +12V	27-78124	5,45
				LM3915N	61-03	915 2.80	78HG +adj	27-78994	7.45 7.45
				KB4400 KB4412	61-04 61-04	412 1.95	79HG –adj LM317MP +adj	27-79994 27-03175	1.75
				KB4413	61-04	413 1.95	LM337MP —adj LM317K +adj	27-03175 27-03173	1.75 2.35
							LM317U +adj	27-03173	2.15
							L200 + adj	27-02006	1.95
MIT DDICES CHO	MINT TO	DIOPPOURAME	TITLE I	TECO	INTER THE	THE COM	uA723 +adj	27-07230	

The concise Ambit Component Listings!

CIV	/IOS/7	4LS	TTL	FIXED	RESIST	ORS:									
400 SERIES C	100		ERIES TTL	E12 valu	ies sole	d in p		ULTRA M	INIATURE ELI	ECTROLYTH			S CERAMIC		
Device Stock 4000UB 22-040		74LS00 74LS01	31-07400 0.12 31-07401 0.12	of 10 per	value	only		Value	Voltage	Stock No.	Price Pk of 4	Value 18pF		Stock No. 04-18011	Pk of 5 0.40
4001 23-040 4002 23-040	001	74LS02 74LS03	31-07402 0.12 31-07403 0.12	½W 5%		-	بادمماد	1uF	50V	05-10514		22pF	Working	04-22011	0.40
4007 23-040	007	74LS04 74LS05	31-07404 0.15 31-07405 0.15		3(0p/10	раск	2u2 4u7	50V 35V	05-22514 05-47514		180pF 470pF	voltage 50V	04-18111 04-47011	0.40 0.45
400B 23-040 4009UB 22-040		74LS08 74LS09	31-07408 0.15 31-07409 0.15	1/4W 5%	1:	5p/10	pack	10u	16V	05-10613	0.32	1nF	20.6	04-10211	0.45
4011 23-040 4011UB 22-040	011	74LS10	31-07410 0.15	1/4W 1%	35	5p/10	pack	10u 22u	35V 6.3V	05-10614 05-22612	0.32 0.32	MYLAR			Deine
4012 23-040 4013 23-040	012	74LS11 74LS12	31-07411 0.15 31-07412 0.15	Order by	value l	& tvn		22u 22u	16V 35V	05-22613 05-22614	0.36 0.40	Value		Stock No.	Price Pk of 5
4015 23-040	015	74LS13 74LS14	31-07413 0.35 31-07414 0.35	Older by	value	or cype		47u	10V	05-47612	0.40	1n		04-10206	0.25
4016 23-040 4017 23-040	017	74LS15 74LS20	31-07415 0.15 31-07420 0.15					47u 100u	16V 6.3V	05-47613 05-10712	0.40 0.40	2n2 3n3	>	04-22206 04-33206	0.25
4020 23-040 4021 23-040	020	74L\$21	31-07421 0_15	1	VARIAE	3LE		100u	16V	05-10713	0.48	4n7	100	04-47206	0.25
4022 23-040 4023 23-040		74LS22 74LS26	31-07422 0.15 31-07426 0.15	CAI	RBONT	YPES	-	220u	6.3∀	05-22712	0.48	6n8 10n	ge	04-68206 04-10306	0.25
4024 23-040	024	74LS27 74LS28	31-07427 0.15 31-07428 0.20	Supplied with P	C/wire on tags	s. Round sh	nafts 6mm	ULTRA LE	OW LEAKAGE	E ELECTROI	YTICS	22n 33n	olta	04-22306 04-33306	0.30
4025 23-040 4027 23-040	027	74LS30	31-07430 0.15	dia_with 7mm l nutsupplied	oush, MB × 0	75 washer	and fixing	Value	Voltage	Stock No.	Pk of 5	47n	λĒ	04-47306	0.30
4028 23-040 4029 23-040	028	74LS32 74LS33	31-07432 0.15 31-07433 0.15	VM10R Style	(K16110)			0.1uF 0.22uF	50V 50V	05-10210 05-10404	0.40 0.40	68n 100n	orking voltage	04-68306 04-10406	0.30
4035 23-040 4040 23-040	035 😮	74LS37 74LS38	31-07437 0.20 31-07438 0.15	Value 500R Lin	Stock No. 48-50113	1-24 25- 0.33 0.	99 100+ 30 0.27	0.47uF	50V	05-47404	0.40	220n	/orl	04-22406	0.55
4042 23-040	042	74LS40 74LS42	31-07440 0.20 31-07477 0.33	1k Lin 5k	48-10213 48-50213	0,33 0	30 0.27 30 0.27	1uF 2u2	50V 50V	05-10504 05-22504	0.40 0.40	330n 470n	3	04-33406 04-47406	0.60
4043 23-040 4044 23-040	naa w	74L547 74LS48	31-07447 0.72 31-07448 0.44	10k Lin 20k Lin	48-10313 48-20313	0.33 0.	30 0.27 30 0.27	4u7	50V	05-47504	0.48				
4046 23-040 4049UB 23-040	046 5	741.549	31-07449 0.88	50k Lin	48-50313	0.33 0.	30 0.27	10uF 22uF	25V 25V	05-10604 05-22604	0.40 0.48	SILVER M	ICA CAPACI	TORS	Price
4050 23-040		74LS51 74LS54	31-07451 0.15 31-07454 0.15	100k Lin 500k Lin	48-10413 48-50413	0.33 0	30 0.27 30 0.27	33uF 47uF	16V 10V	05-33604 05-47603	0.48	Value		Stock No.	Price
4051 23-040 4052 23-040	052	74LS55 74LS74	31-07455 0.15 31-07474 0.23	1M Lin 5k Log	48-10513 48-50214		30 0.27 30 0.27	47uF	16V	05-47603	0.56	2.2pF	_	04-22908	0.22
4053 23-040 4060 23-040		74LS75	31-07475 0.23	10kLog 50kLog	48-10314 48-50314		30 0.27 30 0.27	100uF	10V	05-10703	0.64	4.7pF 10pF	350V	04-47908 04-10008	0.22
4066 23-040 4068 23-040	066	74LS76 74LS78	31-07476 0.23 31-07478 0.21	100k Log 500k Log	48-10414 48-50414		30 0.27 30 0.27	SUB MIN	IATURE CERA	AMIC PLATE	=	22pF	9	04-22008	0.22
4069UB 23-040 4070 23-040	069	74LS83 74LS85	31-07483 0.36 31-07485 0.48	1M Log	48-10514	0.33 0.	30 0.27	Value		Stock No.		33pF 47pF	voltage	04-33008 04-47008	0.22
4071 23-040 4072 23-040	071	74LS86 74LS90	31-07486 0.16 31-07490 0.26	VM11R Style Single gang with	(K15111-5M n DPOT rotary	11222) switch, Sw	itch rating	2.2pF 2.7pF		04-22901 04-27901	0.40 0.40	56pF 68pF	No.	04-56008 04-68008	0.22
4073 23-040	172 (3)	74LS91 74LS92	31-07491 0.40 31-07492 0.35	1A/16VDC				3.3pF		04-33901	0.40	100pF	- Bu	04-10108	0.22
4075 23-040 4076 23-040	075	74LS93 74LS95	31-07493 0.26 31-07495 0.40	Value 5k Lin	Stock No. 48-50217	1-24 25- 0,67 0,	99 100+ 55 0,50	3.9pF 4.7pF		04-39901 04-47901	0.40 0.40	120pF 150pF	Working	04-12108 04-15108	0.22
4077 23-040 4078 23-040	077	74LS107	31-74107 0.34	10k Lin 25k Lin	48-10317 48-25317		55 0,50 55 0.50	5.6pF	93	04-56901	0.40	220pF	× ×	04-22108	0.24
4081 23-040	081	74LS109 74LS112	31-74109 0.27 31-74112 0.23	5kLog 10kLog	48-50218 48-10318		55 0,50 55 0,50	6.8pF 8.2pF		04-68901 04-82901	0.40	330pF	_	04-33108	0.36
4082 23-040 4093 23-040	93	74LS113	31-74113 0.23	25k Log 50k Log	48-25318 48-50318	0.67 0.	55 0,50 55 0,50	10pF	ğ	04-10001	0.40	SEMCO			
4099 23-040 4175 23-041	175	74LS115	31-74122 0.30	100k Log	48-10418		55 0,50	12pF 15pF	voltage	04-12001 04-15001	0.40	Value		Stock No.	Price
4502 23-045 4503 23-045	502	74LS125	31-74123 0.40 31-74125 0.30	GM70R Style				18pF 22pF) DE	04-18001 04-22001	0.40	10pF 22pF		04-10014 04-22014	1.05
4506 23-045 4507 23-045	506 rd		31-74126 0.30 31-74132 0.30	Value 5k Lin	Stock No. 48-50215		54 0.49	27pF	Working	04-27001	0.40	47pF	Working	04-47014	1.05
4508 23-045	508	74LS133 74LS136	31-74133 0.26 31-74136 0.22	10k Lin 25k Lin	48-10315 48-25315		54 0.49 54 0.49	33pF 39pF	No	04-33001 04-39001	0.40	100pF 220pF	voltage 350V	04-10114 04-22114	1.05
4510 23-045 4511 23-045	1.5.5 min		31-74138 0.33 31-74139 0.33	100kLin 250kLin	48-10415 48-25415	0.60 0	54 0.49 54 0.49	47pF		04-47001	0.40	470pF 1000pF	0001	04-47114	1.05
4512 23-045 4514 23-045	512 (3)	74LS151	31-74151 0.33	1M Lin 1kLog	48-10515 48-10216		54 0.49 54 0.49	56pF 68pF		04-56001 04-68001	0.40 0.40	Тооорі		04-10214	1.05
4515 23-045 4516 23-045	O	74LS155	31-74155 0.33	5kLog 10kLog	48-50216 48-10316	0.60 0.	54 0.49 54 0.49	82pF 100pF		04-82001 04-10101	0.50 0.50	CERAMIC	TRIMMER C	APACITORS	
4518 23-045	S18 W3	74LS156 74LS157	31-74156 0.36 31-74157 0.30	25 k Log	48-25316 48-50316	0.60 0		120pF		04-12101	0.50		neter Types	Ca I- Bl -	DI: -40
4520 23-045 4521 23-045			31-74158 0.30	100kLog	48-10416	0.60 0	54 0.49	150pF 180pF		04-15101 04-18101	0.50 0.50	Value 1.8-6pF	Colour Red	Stock No. 06-60903	Pk of 3 0.42
4522 23-045 4526 23-045	ene I		31-74161 0.40	250k Log 1M Log	48-25416 48-10516		54 0.49 54 0.49	220pF		04-22101	0.50	2.8-12.5pF	None	06-12003	0.42
4527 23-045 4528 23-045				VM13R Style	(K161C3—5	M3121)		270pF 330pF		04-27101 04-33101	0.50 0.50	3.5-20pF 5-30pF	Blue Yellow	06-20003 06-30003	0.42
4529 23-045 4531 23-045	29 0		31-74164 0.44 31-74165 0.66	Single gang, bu 3A/30VDC	I push DPST	switch Swi	itch rating		K CERAMIC I		0,00	9-50pF	Green	06-50003	0.42
4532 23-045	32	74LS166	31-64166 0.64 31-74170 0.69	Value	Stock No.	1-24 25-			K CENAMIC I		Price	10mm Dis	meter Type		
4534 23-045 4536 23-045	100	74LS173	31-74173 0.53	5k Lin 10k Lin	48-50219 48-10319		83 0.75	Value		Stock No.		Value	illerer i Abe	Stock No.	Pk of 3
4538 23-045 4539 23-045	39 .0	74LS175	31-74174 0.41 31-74175 0.44	25k Lin 100k Lin	48-25319 48-10419	0.94 0.	83 0.75 83 0.75	390pF 470pF	≥	04-39102 04-47102	0.50 0.50	5-30pF		06-30005	
4543 23-045- 4549 23-045-	943 part	74LS181 74LS190	31-74181 0.96 31-74190 0.43	55k Log 10k Log	48-50220 48-10320	0.94 0.	83 0.75 83 0.75	560pF 680pF	63	04-56102 04-68102	0.50 0.50	8-50pF 16-100pF		06-50005 06-10005	0.45 0.45
4553 23-045 4554 23-045		74LS191 74LS192	31-74191 0.43 31-74192 0.43	25k Log 50k Log	48-25320 48-50320	0.94 0. 0.94 0.	83 0.75	820pF	Working voltage	04-82102	0.50				
4555 23-045	555 @	74LS193	31-74193 0.43 31-74194 0.43	100k Log	48-10420	0.94 0.	83 0.75	1000pF 1200pF	10 t	04-10202 04-12202	0.50 0.50		INIATURE C	ERAMIC TRI	MMERS
4556 23-045 4557 23-045	557 (1)	74LS195	31-74195 0.43	GM80ER Style Dual gang 41 det		forvolume	controls	1500pF) B	04-15202	0.50	CTZ31 — Value	3./mm Colour	Stock No.	Pk of 3
4558 23-045 4559 23-045	569	7455197	31-74195 0.43 31-74197 0.53	Value	Stock No.	1-24 25-	99 100+	1800pF 2200pF	rki	04-18202 04-22002	0.50 0.50	3-10pF	Brown	06-10007	0.45
4560 23-045 4561 23-045			31-74221 0.55 31-74240 0.66	10k Log 100k Lin	48-10322 48-10421		62 0.56 62 0.56	2700pF 3300pF	× ×	04-27202 04-33202	0.50 0.50	4.5-20pF 6.3-30pF	Red Orange	06-20007 06-30007	0.45 0.45
4562 23-045	200 969	74LS241 74LS242	31-74241 0.66	GM70ER Style	e (K162AO)			4700pF		04-47202	0.50				
4566 23-045 4568 23-045	68 🕊	74LS243	31-74243 0.60 31-74244 0.66	Dual gang with c				MONOLIT	THIC CARACIT	TOPS.		CTZ51			Price
4569 23-045 4572UB 23-045		74LS245	31-74245 1.10	50k Lin	48-50323	0.65 0.	59 0.53	MONOLII	THIC CAPACIT	UNS	Price	Value	Colour	Stock No.	Pk of 3
4580 23-0450 4581 23-0450	180		31-74251 0.40	100k Lin 100k	48-10424	0,65 0.		Value		Stock No.		2.5-6pF 3-10pF	Blue Brown	06-06008 06-10008	0.45 0.45
4582 23-045 4583 23-045	82	74LS257	31-74257 0.40	Balance	48-10425	0.65 0,	59 0.53	1n 4n7		04-10204 04-47204	0.39 0.42	4.5-20pF	Red	06-20008	0.45
4584 23-045	84	74LS258 74LS259	31-74258 0.40 31-74259 0.56	AB47 Miniature preset	100k diode lov	v, 22 turn		10n		04-10304	0.42	5,5-30pF 7.5-50pF	Orange Green	06-30008 06-50008	0.45 0.45
4585 23-045 4702 23-047	102	74LS260 74LS266	31-74260 0.29 31-74266 0.22	Knob 20mm	Stock No. 48-10405	1-24 25- 0.50 0.	99 100+ 40 0.30	47n 100n		04-47304 04-10404	0.45 0.45	9-70pF	Purple	06-70008	0.45
4703 23-047 4704 23-047	703	74LS273	31-74273 0.77 31-74279 0.38	20mm thumb	48-10407		40 0.30					TRIMMER	S FOII		
4705 23-047	705	74LS283	31-74283 0.44	3W Rated Ten			40 0,30	LOW VOL Value	TAGE DISC	Stock No.	DkofF				Price
4706 23-047 4720 23-047	20	74LS365	31-74298 0.59 31-74365 0.37	A high quality to	en turn 3W po	tentiomete	r, rated at	1n		04-10203	0.20	Capacity	Min. Dia	Stock No.	Pk of 3
4723 23-0473 4724 23-0473		74LS366 74LS367	31-74366 0.44 31-74367 0.33	3W/40°C Tolerai Value	Stock No.			10n		04-10303	0.20	1-5-10pF 2-22pF	7.5 7.5	06-10001 06-22001	0.57 0.57
4725 23-047 40014 23-400	25	74LS367	31-74367 0.33	10k	48-10310	4.45		22n 47n		04-22303 04-47303	0.25 0.25	3-36pF	7.5	06-36001	0.66
40085 23-4008	185	73LS368 74LS373	31-74368 0.33 31-74373 0.79	Low Cost Carl — MB20	bon Track M	lultiturn		100n		04-10403	0.40	5-60pF 3-90pF	10 10	06-60001 06-80001	0.66 0.99
40106 23-4010	06		31-74374 0.79 31-74375 0.34	A low cost altern				LOW VO	TAGE DISC O	CERAMIC					
40160 23-4018 40161 23-4018			31-74377 0.66 31-74378 0.48	pot with a 5:1 ep shaft. Tolerance				Value	TAGE DISC (Stock No.	Price	COMPRES Cap range	SION TRIMIN Colour	MERS Stock No.	Price
40162 23-4016 40174 23-4017	62		31-74379 0.48 31-74388 0.30	Value 20k	Stock No. 48-22326	1-24 1.06	25+ 0.96	1nF		04-10212	0.10	10-80pF	Red	06-08006	0.28
40192 23-4019	92	74LS390	31-74390 0.56	Additional Da	ta:			10nF		04-10312	0.22	30-140pF	Blue	06-14006	0.28
40193 23-4019 40195 23-4019	95	74LS393 74LS399	31-74393 0.53 31-74399 0.71	Mounting hole re MB, 534 series	equired for VM	l, GM series	7mm, for plied C/W	CERAMIC Value	FEEDTHROU	GH CAPAC Stock No.		60-180pF	Yellow	06-18006	0.28
		74LS490 74LS670	31-74490 0.65 31-74670 1.25	one washer and log × 6mm dia				1000pF		04-10210	0.35				
MOST	PRI	CES	SHOW	NFORU	NIT IT	EM (OR PA	CKQ	TY — S		N. A. C. C. C.	RVOL	UME I	DISCO	UNT

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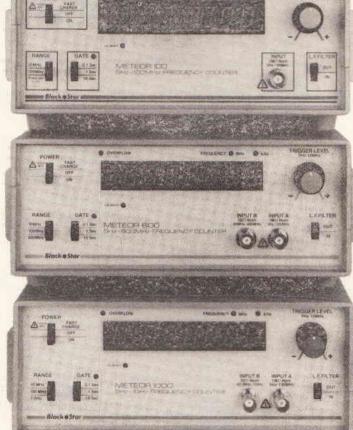
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Model	Price	Range (RMS)	Dyn-loads	Notes
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*PFA500	45.22	250-600W	20,40,3	25A cont, output current.
	55.33	mounted on typ	oe 74 Heat Excha	nger (see below).

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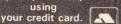
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Battery back-up with trickle charging facility
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HW 1250

only £9.50

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March Marc	2% E24 5p 1% E24 6p	47nF 41p 100nF 45p 220nF 79p	0.6 - 0.6V 2.95 0.12 + 0.12V 2.95 0.15 - 0.15V	DIL SPST 4 way 67p	EURO CONNECTORS Male	VEROCASES V5 220×174× 100mm 10.40	3A 17p 10p 4A - 10p 5A - 10p 6A - 10p	CLIP ON TO1 (AC128) 18p	2N3109 48p 2N3232 1.50 2N3250 36p 2N3251 36p	2N4904 2N4905 2N4906 2N4907	2.15 4 2.75 4 2.99 4 3.20 4	0410 0411 0412 0422	1.80 BC182L 3.95 BC182LA 90p BC182LB 2.95 BC183	13p BC559 10p BC559B 13p BC559C 14p BC560 10p BC560	15p 16p 17p 32p
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The content of the	WITH 'A" SPINDLES 4K7 TO 2M LIN 38p	4n7 4KV 57p 10nF 2KV 57p FEEDTHRO CAP	Please add adequate P&P as transformers	Non-Latching Push to Make 25p Push to Break	64w A - C Angled 3.35	Grevisoffic GI 15mm Short \$1808 plain 56p \$1800 plain 56p	QUARTZ	callers Tower Transistor Manual Bible 10:50	2N3568 50p 2N3569 50p 2N3570 6.95 2N3571 5.73	2N4927 2N4928 2N4964 2N4965	95p 4 1.59 4 27p 4 25p A	0822 0871 0872 AC125	1.80 BC205 1.00 BC206 1.00 BC207 49p BC208	29p BD131 29p BD132 29p BD135	2.28 44p 44p 35p
Company	As above with DP Mains Switch 88p As above stereo	TRIMMERS MINI FILM(MULLARD) UP TO 100VDC	WIRE & CABLE PRICES PER	Mains 4 amps DPST withdraw	CONNECTORS PCB Male - Latch Straight 10 vs. 89p	\$1515 - ne 64p \$1515 - ne 64p 15mm Standard \$1506 clain \$7p	about types not sted 32.768K Hz 95p	Crouts 6 50 6 4 2 5 T L Data 10 50 Texas Cond 5 18	2N3585 2.99 2N3632 9.88 2N3638 55p 2N3638A 70p	2N4968 2N4969 2N5010 2N5011	25p A 31p A 12.75 A 13.85 A	C128 C132 C151 C152	32p BC212 35p BC212A 68p BC212B 51p BC212L 45p BC212LA	10p BD137 12p BD138 13p BD139 10p BD140	37p 37p 38p 38p
March Column Co	OUSTPROOF PRESETS E3 1000 TO 10M	(800MHz) 23p 2pF to 10pF (600MHz) 27p 2pF to 22pF (400MHz) 29p	Solid Hook up Any Colour 5p MAINS	postions inc 2 keys 3.95	26 MB+ 175 34 MB+ 199 40 MB+ 225	< 1515 - ne 56p < 151G - ne 86p 15mm Winged	200K=z 2.65 100M=z 3.50 2.00M=z 2.24 2.097152M=z 3.49	Vemore 4.95 Texas Linear 4.95 Nationa	2N3641 69p 2N3642 50p 2N3643 30p 2N3644 56p	2N5033 2N5036 2N5039 2N5039 2N5036	99p A 1.60 A 1.90 A 36p A	C153K C176 C176K C176K	64p BC213 27p BC213A 37p BC213B 25p BC213C	14p BD 153 10p BD 155 11p BD 157 12p BD 158 13p BD 160	1.25 1.20 54p 55p
Company Comp	Mini Horiz 15p Standard Vert 18p Standard Horiz	5p51o 65pF (200MHz) 36p ELECTROLYTICS	Two 3 Amp 14p Two 2 h Amp 16p 3 Core 2 h Amp	SPDT 1.80 DPDT 2.75	Angled 10 way 95p 16 way 1.47	21mm Short S2108 plain 69p	3.2768M=z 1.49 4.00MHz 1.49 4.194394MHz 1.99	National Special Function 2.95 National Data Conversion 2.95	2N3646 2Bp 2N3662 15p 2N3663 16p 2N3702 10p	2N5088 2N5089 2N5172 2N5175	37p 4 37p 4 15p 4 58p 4	AC198 AC188K ACY17 ACY20	25p BC213LB 40p BC213LC 1.50 BC214 75p BC2148	13p BD182 14p BD183 10p BD187 12p BD201	1.75 2.50 2.70 1.09
The content of the	Thumbwheel of 'a Spindle for Standard Types	or Maisushita (Nat. Panasonic) uFd V 47 63 8p 47 100 9p	3 Core 13 Amo 3 Core 13 Amo 56p	Man DB 4 amon with wiseindle 75p Lorin Adjustable	34 way 2.40 40 way 2.55 50 way 2.75 Female Header	\$2118 - line 75p \$211G - line 75p 21mm Standard K2108 plain 69p	99p 5 00MHZ 1 50 6 00MHz 1 39 6 9375MHz 3 50 8 00MHz 1 49	Hitachi Micro- processor 9 00 Hitachi Memory	2N3704 10p 2N3705 10p 2N3706 10p 2N3707 10p	2N5180 2N5183 2N5184 2N5188	1.00 A 1.10 A 1.15 A	ACY22 ACY28 ACY44 AD136	75p 8C214L 75p 8C214LB 98p 8C214LC 6 75 8C237	10p BD204 13p BD220 14p BD221 14p BD223	1.39 1.44 1.00 95p 1.00
Second Column	TURN PRESETS 50Ω 100Ω 200Ω 500Ω 1K 2K 5K, 10K	1 63 8p 1 100 9p 1 500 40p	Single 14p Sterec 27p Mini Single 12p Mini Sterec 15p	2p 2 to 6 way 59p	16 way 1.07 20 way 1.25 26 way 1.49 34 way 1.75	K2118 + line 78p K211G + line 78p 21mm Winged	18 00MHz 1 79 20 00MHz 1 99 27 648MHz 1 69 48 00MHz 1 69	TEXAS	2N3709 10p 2N3710 10p 2N3711 10p 2N3712 2.00	2N5190 2N5191 2N5193 2N5194	68p A 70p A 90p A 79p A	AD 150 AD 161 AD 162 AF 106	2 80 BC 2378 39p BC 237C 39p BC 238 75p BC 238A	17p BD232 18p BD233 14p BD234 15p BD237	1.11 70p 72p 98p
April 19	200K 500K each 89p THERMISTORS	2 2 100 11p 2 2 350 30p 3 3 25 10p 3 3 40 11p	44p 4 Core Single Screen 54p 8 Core 61p	59p 4p 4 to 3 way 59p Many other	50 way 1.99 DIN PLUGS 2 pin 9p	W210G 86p 29mm Standard K290B 88p	5.5 MHz	Solid State 4.95 Digital 4.95 Car Electronics 4.95		12110100	The same	The state of the s	-		-
The content of the	PLEASE PHONE CAPS CERAMIC	4.7 16 8p 4.7 25 9p 4.7 40 11p 4.7 63 12p	Heavy Duty Mike Guitar Lead 25p	Please Phone	5 pin 240° 16p 5 pin Domino 50p 6 pin 18p	Yel Grn, Grey Blue (Please state	Top quality Hand Tools Lindstrom	tronics 4.95 Optronics 4.95 Communications 4.95	ELECTA	M. H. MARY S.					
MONOTONIA WAS AND THE REPORT OF THE PROPERTY	MICRO - MINI 100V TYPICALLY 5% E12	10 25 8p 10 40 12p 10 63 14p 10 100 16p	50Ω RG 58A 25p 75Ω UHF 29p 75Ω VHF 28p	ECTORS PLUGS & SOCKETS	DIN CHASSIS SOCKETS	15mm plain 5p 15mm + dot 8p 15mm + line 8p 21mm plain 5p	Side Cutters 4 3" 14 55 L890 Snipe Nose Pliers 5 2"	Science 4.95 Microprocessors 4.95	AD CRICKLEWGOD	2 Q 3	· 🐠	We s	tock a vast se	lection of	
Section Total 19	SIEMENS 63V MONOLYTHIC MINI CERAMIC	22 25 11p 22 40 14p 22 63 16p 22 100 21p 47 25 14p	RIBBON Prices per foot 8 way 25p 10 way 25p	Lo- Pins prof WWp. 8 8p 25p 14 9p 35p	5 pin 180° 10p 5 pin 240° 16p 6 pin 20p	21mm+line 8p 29mm (Red, Blk Grey only) 8p	L870 Snipe Nose Pliers 4 7" 10 35 L160 Long Nose	Antex Irons C240 (15W) 5 20 XS240 (25W)			1	look cata mea	through our r logue and you n Send for yo	new illustrate ull see what v uur copy today	ed we
POLYTIES 10 10 10 10 10 10 10 1	33nF, 47nF 10p 68nF 14p 100nF 14p BARRIER LAYER	47 63 26p 47 100 28p 100 16 14p 100 25 16p	20 way 48p 24 way 62p 30 way 75p 32 way 82p	18 16p 50p 20 20p – 22 22p – 24 24p 70p	SOCKETS 2 pm 10p	Colours as above Bp	CK TOOLS C80 4½" Side Cutter 10.02 C73 4½" Side	Iron Stand 1.75 Elements (State Iron) 2.25 C240 Bits				Gov	Depts, schoo	ls etc. Quanti ble.	4
DAME Part	220nF 25V 15p POLYSTYRENE 160V	100 63 25p 100 100 30p 220 10 16p 220 16 17p	64 way 1.63	40 30p 99p ZERO INSERTION FORCE DIL SOCKETS	5 pin 15p PHONO PLUGS	15mm or 21mm Colours as	C72 4 ½ " Pliers (Snipe) 7,52 DE-SOLDERING	No 3 (Med.) 85p No 6 (Micro) 85p XS240 X25 Bits No 50 (Small)	=======================================	3,24		ELE	CTRONIC	- C 21 A	PAGE 450
SOCKETS 180 230	10pF 15pF 22pF, 27pF, 33pF 39pF 47pF 68pF	220 40 25p 220 63 30p 220 100 40p 470 16 22p	GRADE ONE GLASS PCB SINGLE-SIDED	28 pin 4.99 40 pin 5.25 UHF PL269	Plastic Red Yellow, Green Black 15p	Red+Point 26p Blk+Point 6p Grey+Point 26p Clear 1 to 10 26p	BT 100 High Suction Anodised 4 55 Spare Tellon	No 51 (Med)85p No 52 (Lge) 85p SOLDER 125gms	2N3826 78p	2N5416	1.54 8	BC116A BC117	37p BC261A 19p BC261B		
P.C. Control P.C. P	180pF 220pF 270pF 330pF, 390pF 10p 470pF 680pF	470 40 33p 470 63 43p 470 100 60p 1000 16 30p	1 85 420 × 195mm 2 55 420 × 245mm	Low loss superior quality 500 Line plus 45p	SOCKETS Single 16p Dual 20p	DIALS 21mm Red+Point 28p Blk+Point 28p	TEST METERS	22swg 310	2N3854 44p 2N3855 30p 2N3855A 40p 2N3856 45p	2N5448 2N5449 2N5450 2N5451	19p 8 21p 8 23p 8 25p 8	9C119 9C121 9C123 9C125	19p BC 261C 38p BC 262 82p BC 262A 82p BC 262B 37p BC 262C	36p 8D539 31p 8D539C 32p 8D540 33p 8D540C	90g 1_10 85g 1_20
POLYSTER POL	2 2nF, 3 3nF 13p 4 7nF 14p 10nF 15p	1000 40 46p 1000 63 65p 2000 16 40p 2200 25 63p	FEARIC CHLORIDE PELLETS	Roundskt 40p Sqrskt 40p BNC 50Ω	CONNECTORS PP3 Snaps 10p PP9 Snaps 12p	Clear 1 to 10 28p Clear Taper 28p STANDARD	Push Button 2 amps AC/DC, 1KV DC 750v AC	Retail Variety Please phone about types not	2N3858A 37p 2N3859A 31p 2N3860 31p 2N3866 90p	2N5458 2N5459 2N5460 2N5461	29p 8 29p 8 72p 8 60p 8	9C 134 9C 135 9C 136 9C 137	36p BC 263B 45p BC 263C 45p BC 264 39p BC 264B	30p 8D676 31p 8D677 32p 8D678 80p 8D711 80p 8D712	775 785 835 1 32
TYPE (RADIAL) 10	PLEASE PHONE POLYESTER	2200 63 134p 4700 16 75p 4700 25 89p Radial by	Enough to make over 1 litre 1 69 DALO ETCH	Socket 1,00 Line skt 115 COAX (TV)	Bex for 6HP7 33p Box for 4HP11	(All for % C spindles) Grub Screen	MINI TESTER Pocket Size	insufficient space. Only top quality	2N3900 25g 2N3902 3.33 2N3903 13g 2N3904 13g	2N5484 2N5485 2N5490 2N5492	40p 8 29p 8 1.37 8 1.56 8	3C 140 3C 141 3C 142 3C 143	55P BC 266 29P BC 266A 37P BC 2663 29P BC 300 30P BC 301	36p BDX18 37p BDX32 45p BDX668 44p BDX678	1 30 1 59 3 47 5 95
150.6. 200.6. 0 470 16 80 220 10 16 16 170 16 180 220 10 170 180 220 10 170 180 220 180 220 180 220 180 220 180 220 180 220 180 220 180 220 180 220 180 220 180 220 180 220 180 220 180 220 220 220 220 220 220 2	250V 10nF 15nF 22nF 33nF 47nF 68nF	10 16 6p 22 10 6p	(inc Spare Nib) 1.20 ETCH RESIST	Plug 25p Socket 25p Line Skt 40p	TRANSISTOR SOCKETS TO 18 (BC 109)	M1 15+metal insert 34p M2 33mm+ metal insert 39p	Analog Meter 5.55 MICROTEST 80	2N929 36p 2N929A 45p 2N930 20p 2N930A 30p	2N3906 13g 2N3924 8.30 2N3945 85g 2N3962 30g	2N5496 2N5543 2N5551 2N5640	1.59 B 12.00 B 37p B 95p B	3C 147A 3C 147B 3C 147C 3C 148	10p BC 303 10p BC 304 20p BC 307 10p BC 307A	47p BDY55 46p BDY56 13p BDY57 14p BDY58	1 70 1 75 1 80 5 25 6 15
Bellan 180 a 70 10 17p branslator 15p 15p 39 a 70 10 17p branslator 15p 15p 39 a 70 10 17p branslator 15p 15p 39 a 70 10 15p 30 a 70 a 7	150nF, 200nF, 10p 330nF, 470nF 13p	47 16 6p 100 10 9p 100 16 10p 220 10 11p	2 Thick lines 3 Thin bends 4 Thick bends 5 DIL pads	(3 PIN XLR) Male 1,70 Female 1,95 Sockets	TO5 (BFY 50) 28p TO3 (2N3055)	metal insert & skirt 39p M4 As M3 numbered 1 to 10 39p	OPV 1000v AC/DC, 5 ADC, 2 5A AC, 0 18 to 5M 19 00	2N1132 25p 2N1302 45p 2N1303 65p 2N1304 60p	2N4030 75p 2N4031 65p 2N4032 69p 2N4036 63p	2N5786 2N5813 2N5884 2N5886 2N6027	80p 8 23p 8 5.95 8 5.95 8	3C 148B 3C 148C 3C 149 3C 149B 3C 149C	13p BC 308 13p BC 308A 10p BC 308B 12p BC 309	12p BDY92 13p BF115 14p BF119 14p BF121	3.75 35c 1.00 75c
Second Column C	1μF 22p 15μF 39p 2 2μF 39p	470 10 17p 470 16 18p 1000 10 20p 1000 16 24p	pads 7 Dots + holes 8 01 edge connectors	Maie 1,50 Female 2,35 JACK PLUGS	Bare Wire Mains Safety Block	M5 As M3 but 30mm 42p M6 As M4 but 30mm 42p	OPV 1000v DC, 2000v AC, 0-18 10 10M 32,00	2N1308 65p 2N1711 35p 2N1889 50p 2N1890 50p	2N4058 10g 2N4059 17g 2N4060 12g 2N4061 10g	2N6030 2N6031 2N6082 2N6083 2N6089	6.60 B 6.95 B 11.99 B 17.95 B 1.20 B	3C 52 3C 53 3C 54 3C 57	35p 8C3098 23p 8C309C 27p 8C317 11p 8C318	16p BF127 17p BF153 15p BF154 15p BF157	80a 39a 25a 58a
CAN	POLY-C 5% 250V 7 5MM 1nF 1n5, 2n2 3n3 4n7 6n87p	2200 16 44p 3300 10 50p 3300 16 65p 4700 10 65p	Any sheet of above 35p PHOTO	for quantity Please phone Mono 20p Stereo 30p	6 AMP 3 PIN Plug (Holes) 58p	16mm SOLID ALUMINIUM MATCHING KNOBS	DIL REED 100VA Normally open (1 amp)	2N2050 7.14 2N2102 39p 2N2217 39p 2N2218 33p	2N4064 1.15 2N4069 1.00 2N4416A 1.80 2N4220 75 2N4221 95	2N6101 2N6109 2N6111 2N6121 2N6122	1.15 1.00 57p 59p	3C 158 3C 158A 3C 158B 3C 159	13p 8C321 10p 8C327 12p 8C328 13p 8C337 11p 8C338	25p BF159 14p BF160 14p BF161 15p BF163	58a 55a 58a 50a
SIEMENS SIEMENS SIEMENS TANTALUM	15n 18n 22n 27n 33n 39n 47n 6p 56n 68n 82n	CAN ELECTROLYTICS 4700µF 40V 2 50 4700µF 63V 3 50	1st Class Epoxy Glass For better results than spraying Expose	Mono 30p 2 mm Mono 12p 2 mm Metal	(Pins) 35p Line Skt. Pins	M9_24mm 56p	5v 380B + Diode & Screen 2 95 12v 530B 1 99	2N2219 27p 2N2219A 28p 2N2220 22p 2N2221 22p	2N4223 97 2N4224 98 2N4234 45 2N4236 45	2N6124 2N6125 2N6126 2N6129	59p B 65p B 75p B 79p B	3C 159B 3C 159C 3C 160 3C 161	13p BC347 13p BC350 18p BC382 42p BC382L 48p BC383	20p BF167 20p BF170 30p BF173 30p BF174 30p BF177	290
150	SIEMENS POLY-C 5% 100V 7 5MM 100n 120n	TANTALIUM BEADS	Single sided 100 = 160 = 2.10 100 = 220 = 2.50 203 = 114 = 2.40 233 = 220 = 5.20	31/2 mm Mono 12p 31/2 MM Stereo 35p	13 AMP DOMESTIC Plug Fruse 50p	20mm Slow Fast 100mA 19p 15p 250mA	240V AC 10 amps Contacts SPDT 1×½ " 6v	2N2222 24p 2N2222A 25p 2N2223 2.60 2N2223A 4.15	2N4237 1.2 2N4238 95 2N4239 95 2N4240 3.00 2N4248 15	2N6130 2N6131 2N6132 2N6133 2N6134	98p 8 83p 8 1.14 8 1.36 8	C167A BC167B BC168 BC168B	10p BC383L 10p BC384 13p BC384L 10p BC407 10p BC408	30p BF178 30p BF179 30p BF180 24p BF181 24p BF182	30c 35c 35c 36c 36c
POLYESTER 4 7 35V 20p 10 165 20 68 25 20p 10 165 20 10 16V 18p 15p 15p 16 20 10 16V 18p 15p 15p 20 10 16V 18p 15p 15p 20 10 16V 18p 15p 15p 20 10 10 10 10 10 16V 18p 15p 15p 15p 15p 15p 15p 15p 15p 15p 15	150n 11p 180n, 220n 270n 14p 330n 390n 20p 470n 560n 26p	22 35V 14p 33 35V 14p 47 35V 14p 68 35V 14p 1 0 35V 14p	Double Sided 100 160 2 20 100 200 2 80 203 114 2 90 233 220 5 90	Mono 20p JACK SOCKETS Chassis Mono 20p	Trailing skt 82p	315mA 17p 10p 500mA 17p 10p	12v 285ß 2 75 24v 1150ß 2 95	2N2369 19p 2N2369A 20p 2N2405 88p 2N2410 1.15 2N2411 3.60	2N4250 17 2N4258 75 2N4266 45 2N4275 48	2N6253 2N6254 2SC1096 2SC1306 2SC1307	1.45 B 1.55 B 95p B 95p B	8C169 8C169B 8C169C 8C170	10p BC413 10p BC414 10p BC415 15p BC416	30p BF183 25p BF184 25p BF185 30p BF194 30p BF195	38a 36c
In The 2472	680n 30p 1μF (10mm) 35p 400V POLYESTER	2 2 16V 14p 2 2 35V 14p 3 3 35V 18p 4 7 16V 18p 4 7 35V 20p	Developer for above (do not use Sodium Hydroxide)	3 mm Mono 15p 3 mm Mono 15p	BOXES & CASES	630mA 17p 10p 800mA 17p 10p 1A 17p 10p	3 04 RECHARGE	2N2483 25p 2N2484 26p 2N2646 45p 2N2647 98p 2N2714 12p	2N4285 35 2N4288 22 2N4289 15 2N4290 45 2N4291 45	2SC1923 2SC2078 2SJ49 2SJ50 2SJ82	40p B 1.70 B 3.99 B 4.50 B	C170B C170C C171 C171A	17p BC418 17p BC440 18p BC441 12p BC460 15p BC461	32p BF197 33p BF198 32p BF199 33p BF200	7.50
47, hrii 15 240 326 34 266 126 34 267 25 37 89p 35 mm Mono R39x5x24" 839x5x2 27 100 100 100 100 100 100 100 100 100 10	1n 1n5 2n2 3n3 4n7m 6n8 10n 10p 15n 22n	6 8 25 20p 6 8 35V 21p 10 16V 18p 10 35V 27p 15 16V 22p	0.1" COPPER	Mono 20p Metal 40p Stereo 30p Stereo	Covered with Black Rexine (Scretchproof) R1 6×4%×1%	1 6A 17p 10p 2A 17p 10p 3 15A 17p 10p 4A 17p 10p 5A 17p 10p	Guaranteed minimum 500 charges HP2(1.2AH) 2.39	2N2848 60p 2N2890 1.10 2N2891 2.28 2N2892 3.00 2N2904A 27p	2N4292 45 2N4294 45 2N4297 2.50 2N4302 60 2N4303 80	2SK134 3SK135 2SK226 2N139 3N140	3.99 B 4.50 B 4.75 B 3.30 B 1.07 B	C172 BC172A BC172B BC172C BC173	12p BC 479 15p BC 516 15p BC 517 16p BC 546B 11p BC 547	30p BF225J 40p BF240 40p BF241 15p BF244A	35c 35c 38c 38c 55c
	150n 220n 18p 330n 39p	15 26V 32p 22 6 3V 26p 22 16V 29p 33 10V 30p	25 × 37 83p 25 × 5 99p 375 × 375 99p	3 mm Mono 15p 3 mm Mono	R28×5×2 2.75 R39×5×2%	6.3A 17p 10p	HP7(%AH) 99p HP11(1.2AH) 2.29 PP3(110mAH)	2N2905 28p 2N2905A 29p 2N2906 25p	2N4304 80	3N143 3N152 3N153	2.85 3.00 2.47	C173B	16p BC547A 16p BC547B	14p BF245A 14p BF245B 12p BF246	55c 55c 65c 75c

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BE247A	70p 75p	MJ2500 MJ2501	2.19	2TX108 10p 2TX109 12p	BRIDGE 1 amp type	2.5 Watt E24 Series	CA3034 5.18 CA3035 2.65	LM1305 3 10 LM1307 2 75	TAA522 2:4 TAA550 73	74 111	74LS TTL	74LS399 1.59 74LS445 1.40	4016 19p 4017 32p	75L5289 3.25 74L5289 3.25
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BF255 BF256A	42p 58p	MJ3001 MJ4032	2.25 3.25	ZTX302 15p 2TX303 23p	W04 (200) 38p	5W wired ended following	CA3042 3.47 CA3043 2.75	LM1458 44p LM1496 75p	TAA621 2.9 TAA661A 2.5	0 7403 19p	74LS01 19p 74LS02 19p	74LS541 79p 74LS640 2.00	4020 42p 4021 39p	LOG IC'S
BF1568	58p 65p	MJ4035 MJ4502	3.65	ZTX304 15p 2TX310 35p	WG8 (800) 50p	voltages only 3V3-3V6-4V3	CA3046 69p	LM1800 3.95 LM1801 2.99	TAA6618 2.5 TAA700 2.6	0 7404 19p	74LS03 19p 74LS04 19p	74LS841 2.00	4022 39p	inc. COMP
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86259	35p	MJ14004 MJ15015	2.45	ZTX313 36p ZTX314 24p	S01 (100) 46p S02 (200) 50p	10V 12V 20V	CA3049 3.21 CA3050 4.11	LM1820 3.95 LM1828 4.79	TAA970 2.4	5 7410 19p	74LS10 19p 74LS11 19p	74LS669 99p 74LS670 1.19	4025 19p 4026 79p	ADC0816 14.95 ADC0817 10.39
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₽F324 ₽F336	38p 36p	MJE520 MJE521	92p 94p	ZTX500 14p ZTX501 14p	Square with note PW01 (100) 95p	(BZY93 saries) E24 values	CA3059 2.80 CA3060 4.09	LM1850 2.75 LM1877 3.25	TBA510G 3.0 TBA520 2.5	7 7417 40p	74LS20 19p	74S TTL 74S00 28p	4031 1.19 4032 78p	MC1466L 6.95
8F337 8F338	28p 48p	MJE2955 MJE3055	99p 69p	ZTX502 14p ZTX503 17p	PW02 (200) 99p	7V5-75V 2.10	CA3062 13.84 CA3065E 4.62	LM1872 4.39 LM1877 5.95	TBAS200 2.7 TBAS30 2.5		74LS22 19p	74502 28p 74504 28p	4033 1.19 4034 1.29	MC1488 59p MC1489 59p
8F355 9F367	60p 85p	MP8111 MP8112	1.20	ZTX504 24p ZTX510 24p	PW04 (400) 1 30 PW06 (600) 1 39	OPTO	CA3058 4.23	LM1886 7.44 LM1889 3.77	TBA5300 2.7		74LS27 19p 74L528 19p	74508 58p 74520 38p	4035 44p	MC4024 3.25 MC4044 3.25
DF 363	85p 46p	MP8121	1.62	2TX530 24p ZTX931 25p	25 emp type	R = Red	CA3070 3:20 CA3071 3:30	LM2907N 2.75	TBA5400 2.7	4 7425 19p	74LS30 19p 74LS32 19p	74530 60p	4037 1.13	MK50250 10:00 MK50398 6:35
BEA58	56p	MP8122 MP8512	1.68	ZTX650 45p	Metal clad with	G = Green Y = Yellow	EA3075 2:10 EA3076 3:42	LM2917N 2 40 LM2917N8 2 40	TBA5500 3.2 TBA560C 2.8	7 7427 19p	74LS33 19p 74LS37 19p	74540 1.45	4038 99p 4039 2.45	MM5303 6 26 MM5307 12 75
8F463	62p 86p	MPF102 MPF103	39p 29p	MANY	K01 (100) 2.62 K02 (200) 2.75	Large Diffused 1 - 50 +	CA30787 2.25 CA3080 1.89	LM3301 1.60	TBAS70 2.3	7 7430 19p	74LS38 19p 74LS40 19p	74564 1.02 74566 1.02	4040 39p 4041 39p	MM5357 22.50
95-470 95-454	86p 29p	MPF104 MPF105	29p 29p	MORE	K04 (400) 3.25 K09 (600) 4.10	#5D 9p 7p G5D 15p 12p	CA3080A 3.96 CA3080E 70p	LM3302 74p LM3401 65p	TBA5700 2.4 TBA581 3.1	1 7433 24p	74L942 35p 74L947 60p	74574 75p 74585 2.99	4042 39p 4043 39p	MM5710514.00 MM5710912.00
BF 300	29p	MPF112 MPF121	1.68	TRANS-	87W64 35A 400V 4 50	YSD 15p 12p	CA3081 1.90 CA3085 1.36	LM3404 75p LM3405 1.45	TBA651 1.9	0 7438 36p	74LS51 19p 74LS54 19p	74586 62p 745112 75p	4044 39p 4045 99p	MM57160 12:00 MM57161 12:00
3FR39 3FR40	25p 25p	MPS6518 MPS6530	47p 45p		Proprietory	Small diffused	CA3086 48p CA30896 1.95	LM3524 6.77 LM3900 48p	TBA673 4.1 TBA700 2.3	8 7441 55p	74LS55 19p	74S113 90p 74S124 2.95	4046 44p 4047 69p	RO2513LC 7.50
#FR41 #FR79	25p 25p	MPS6560 MPS6562	45p 45p	ISTORS	Bridges	820 8p 6p 620 12p 10p	CA3090AG 3 70 CA31305 87p	LM3905 1.25 LM3909 79p	TBA 7000 2.4 TBA 720A0 2.6	0 7443 89p	74L574 28p	74S132 1.09 74S133 60p	4048 39p 4049 22p	SAA5000 3 00
85-880 85-881	25p 25p	MPSA05 MPSA06	23p 25p	IN	880C1300 1.80	Y2D 12p 10p Micro D 1	CA3130T 2.35	LM3911 1 20 LM3914 3 25	TBA750 2.2 TBA7500 2.4	5 7444 89p	74LS75 28p 74LS76 28p	745138 97p 745139 1.10	4050 230	SAA5010 7 10 SAA5012 7 10
BFR90	2.11	MPSA10 MPSA12	280	STOCK	8Y164 55p 8Y179 92p	RID 25p 22p GID 27p 25p YID 27p 25p	CA3140E 39p CA3140T 1.40	LM3915 3.25 LM3916 3.25	TBA790A 2 1 TBA800 78	1 7446 59p	74LS78 35p 74LS83 40p	745140 2.50 745153 7.95	4052 58p	SAA5020 5:50 SAA5030 9:00
#561	1.00	MPSA13	29p 48p	DIODES	BR100 29p	Y10 27p 25p	CA3160AE 99p CA3161E 1.59	LM4250CH 2 63 LM4250N 2 38	TEABLO 95	p 7448 70p	74LS85 60p 74LS86 22p	745157 2.20	4053 49p 4054 79p	SAA5040 15 00 SAA5041 15 00
#119	1.10	MPSA14 MPSA16	46p 30p	1N34A 30p	ST2 29p	Lage clear RSC 12p 10p	CA3162E 4.49 CA3240E 1.04	LM13600 1.15 MB3712 2.18	TBABZOM 85 TBA920 1.9	p 7451 15p	74LS90 32p 74LS92 45p	74S163 3.00 74S174 2.50	4055 83p 4056 83p	SAA5050 8.50 SAA5052 8.50
Ew10	1.48	MPSA18 MPSA20	65p 48p	1NB21 70p 1NB23 92p	Sensitive Gate	G5C 17p 13p	HA1366W 2.40 HA388 2.54	MB3756 3.80	TBA9200 1.9	7 7454 14p	74LS93 24p 74LS95 39p	745175 3.20 745188 1.40	4059 4.35 4060 42p	SAA5070 16.95
3FX29	1.48 26p	MPSA42 MPSA43	49p	1N914 4p 1N916 6p	Small Signal	The state of the s	ICL7106 7 50 ICL7107 9 50	MB8719 7.95 MC1303 2.25	TBA950 2.2 TBA990 2.6	5 7470 34p	74LS96 93p	745189 1.40 745194 1.90	4063 79p 4066 22p	TMS6011 3.65 8T26 95p
BFX30 BFX34	27p	MPSASS MPSASS	28p 30p	1N1184 2.95 1N1190 1.47	2N5061 32p	Super bright large. High	ICL8038 2.99	MC1304 2.50 MC1305 3.10	TBA9900 2.7	4 7472 29p 0 7473 55p	74LS109 35p	745200 4.60 745201 2.40	4087 2.39	8728 1.20 8735 85p
三137 三143	70p 70p	MPSA65 MPSA66	40p 47p	TN1192 1.75	2N5062 35p 2N5063 37p	Efficiency At least 100 times	LC7120 3.20	MC1307 2.76 MC1310 1.45	TCA160C 2.6 TCA210 2.7	7 7474 55p 5 7475 55p	74LS112 35p 74LS113 35p	745225 2.40 745261 3.00	4069 19p	8797 85p 87LS95 80p
FX84	27p 28p	MPSA70	45p	1N1194 1.65 1N1194A 1.80	2N5054 40p BR101 75p	brighter than standard LEDs	LC7137 3.40 LC7137 3.95	MC1330 2.25 MC1352 2.26	TEA220 3.4 TEA270 2.4	4 7476 55p	74LS122 35p	748262 8.50	4070 19p 4071 19p	51LS96 85p 51LS97 90p
F185	28p	MPSA92 MPSA93	39p 39p	1N1196A 2.41 1N1198A 2.65	BR103 69p 88Y39 60p	for the same current	LF347 1.50 LF351 47p	MC1456 2.25 MC1458 44p	TEA440 2.6	9 7481 1.19	74LS123 60p 74LS124 1.50	745288 1.99	4072 19p 4073 19p	81L598 85p 6522 3.19
F158	25p 25p	MPSL01 MPSL51	46p 49p	1N1201A 97p 1N1204A 1.00	BRY55-100 60p BRY55-300 67p	R5U 38p 29p G5U 42p 34p	LF353 92p LF355 83p	MC1466L 6 95 MC1468L 4 30	TCA5608 4.1	5 7483 38p	74LS125 24p 74LS126 25p	745289 1.57 745301 3.20	4075 19p 4076 45p	6522A 4.00 6532 5.70
3F115	1.10	MPSU01 MPSU04	1.32	1N1206 1.20 1N4001 4p	BRY56 50p TIC44 35p	Y5U 42p 34p	LF35E 92p EF357 130	MC1485 4 90	TCA740 4 8	0 7485 90p	74LS132 40p 74LS136 29p	745470 3.25 745471 6.25	4077 19p 4078 19p	6821 1.45
于150 年150	1.20 23p	MPSU05 MPSU08	55p 56p	1N4002 4%p 1N4003 Bp	TIC47 50p	RECTANGULAR	LF398 4.62 LF13201 2.99	MC1496 75p	TEA760 27	5 7489 1.68	74LS138 39p 74LS139 39p	748473 12.50 748474 3.99	4081 19p 4082 19p	5847 6.50
SFY53	23p 23p	MPSU07 MPSU51	75p 88p	1N4004 515p 1N4005 6p	4, 8 & 12 Amps	Stackable End	LF13331 3 30 LF13741H 686	MC334D 1.20 MC3351 2.48	TC48000 3.6		74LS145 99p	745475 7.95 745571 6.09	4085 49p 4086 60p	6850 1.65 6852 2.40
#F153 #F155	31p	MPSU55 MPSU56	58p 59p	1N4006 B14p	Texas TO220 Suffix: A - 100V	10 End 767 17p	LM10CH 4.50	MC3401 65# MC3403 75#	TCA910 21		74LS147 99p 74LS148 1.19	745573 9.00	4089 1.23	fi875 4.99 8131 3.75
BF 155A	68p 79p	MPSUS7 MRF475	1 20 6 50	1N4009 20p	8 = 200V C = 300V	G58 18p V58 19p	LM110H 4.50	MC3404 25p MC3409 1.45	T0A940 1.6	9 7494 72p	74LS151 47p 74LS153 49p	74 CMOS/ TTL	4094 69p	8154 9.00 8155 3.50
B. 783	11.60	OC 20	3.30	1N4148 3p 1N4150 18p	D = 400V M = 600V	RECTANGULAR	LM301A+ 95p	MC3446 3 25 MC4024 3 25	TDA 003 3.9	4 7496 48p	74LS154 1.50 74LS155 39p	74000 37p	4095 71p 4096 69p	8212 1.70 8216 996
Ex 19	2.30 24p	OC23	1.00	1N4448 22p 1N5400 12p	TIC106A 46p TIC106B 47p	LEDS WITH BOWED TOP	LM301AN 35p	MC4044 3 25 MF 0 3 50	15A 308 3 9	4 74100 1.25	74L5158 48p 74L5157 40p	74C02 37p 74C04 37p	4097 2.88 4098 74p	8223 1 80
E 12	24p 40p	OC 25 OC 28	2.50	1N5401 13p 1N5402 14p	TIC 106C 48p	(Tombstone) 858 21n	LM305N 88p LM307H 69p	MM5381 9.95	150 000 29	4 74'04 49p 9 74'05 55p	74LS158 35p 74LS160 50p	74C08 37p 74C10 37p	4099 89p	8226 2.50
253 X 2 3	78p 66p	OC 20 OC 35	2.95	1N5404 16p 1N5406 18p	TIC1060 49p TIC1064 68p	G58 22¢ V58 23¢	LMSOTN ASp LMSOSAH 3 15	MM6817411 80 NE329 2 25	75A-522 4.9		74LS161 50p 74LS162 50p	74C14 37p 74C20 37p	45 CMOS	6238 5.75
E5129 E51954	34p 25p	OC41 OC43	80p 70p	1N5407 19p 1N5408 20p	TIC116A 86p		LM3884N 2.14 LM388H 956	NES31N 1 36 NES40L 4 95	10A 10 3 1	4 T4110 35p	74L5183 50p	74C30 37p 74C32 37p	4502 55p 4503 39p	8243 2.90 8250 8.40
8.104	1.70	OC 44 OC 70	82p 50p	1544 10p 15131 40p	TIC1168 68p	MISC OPTO 2N5777 A5p	LM306N 886 LM3094 1.35	NES43% 2 50 NES44% 1 95	10A2003 3.2	5 74118 90p 5 74119 75p	74L5164 50p 74L5165 60p 74L5168 1.40	74C42 1 25 74C48 1 70	4507 33p 4508 1.26	8251 2.50 8253 3.95
80108	3.95	OC 71 OC 72	50p 50p	15134 56p AA119 28p	BA TIC118C 71p	2N5778 60a 2N5779 70a	LM310H 1.98	NESSS 18p NESSS 65b	104200 29 104200 28	9 74120 99b 5 74121 30p	7465169 1.09	74074 99p	4510 44p 4511 44p	8254 10.00 8255 2.25
51/25	1 47	OCB2 OCB2D	50n	BA102 25p	TIC116D 73p TIC116M 80p	4N25 74p 4N27 74p	LM3114 1.04	NESSE 1 89 NESSE 3 25	TRASSE 4.2	0 74°22 40p 8 74°23 40p	74LS170 1 19p	74078 78p	4512 48p 4514 1 13	8257 4.00 8359 3.82
PL 255	1.75	OC83 P346A	70p 75p 58p	BA115 25p BA133 40p	TIC125A 72p	4N28 74p 8P104 1.00	LM3174 2.80	NESSS 118 NESSS 149	10#2830 22	0 14126 35p 5 14126 34p	7415174 40p	74C85 1.60	4515 1 13	8279 4.10 8601 1.20
3.72	1.98	R20088	2 14	8A138 30p 8A142 20p	TIC128B 72p	BPW34 1.43 BPX25 2.47	LM318H 2.40	NE 167 1 37	124111 11	0 14/26 35p 0 14/32 39p	74.5183 1.20 14.5183 1.20	74085 1.60 74089 4.75	4516 55p 4518 39p	9062 2.50 7804010 2.60
811255	2.35	R20108 TIF29A	1.88 29p	BA144 15p BA155 15p	TIC126C 73p TIC126D 77p	8PX29 2.47 8PX48 6.76	LM318N 149 LM319H 248	NE 521 3 99	154488F #1	0 74136 390	74,8190 60e	74090 1.36 74093 1.36	4519 29p 4520 48p	IRADADARI
B. ACT	1.45	TIP30A	38p 35p	BA156 38p BA182 40p	TIC126M 96p	BPX 60 4 75 BPX 61 3.48	LM319N 2.10 LM324N 39p	NESES44 148	1542587 22	0 74147 860 5 74142 188	74LS192 60p 74LS193 60p	740107 95p	4521 88p 4526 68p	280ADMA 6.70 280APIO 2.70
E-43	1.35	TIP30C TIP31A	36p 33p	BA201 18p BA202 26p	DOMESTIC SCRS/TRIACS	8PX63 2.93 IL74 55p	LM3352 1.80 LM337K 4.39	PL100A 4.95	1243590 63	5 74744 208	14.5194 50p	740151 2.60	4527 62p 4528 74p	ZN4ZBEB 3.39
BU1/20	11.00	TIP31C TIP32A	34p	BA316 25p BA317 25p	2N4444 1.BO	ILD 74 1.19	LM337MP 1.65 LM337T 1.75	RC4138 39p	35ABB3 11	5 14141 68p	74LS199 59p	740157 2.60 740160 1.50	4532 69p 4534 3.96	ZN426E6 2.97 ZN427E8 5.99
Bulk 23	10.90	TIP32C TIP33A	65p	8A318 30p 8AV10 16p	BT101-500R 1.40 BT106 2.25	LO74 2.50 LO271 50p	EM339AN 1 60 LM339N 44p	AC4 95 2.95	10428 W 19	5 14185 75p	74L5197 59p 74L8221 95p	740161 1.50 740162 1.50	4536 259 4538 78p	2N428E8 4.05
BUN24 BUN25	12.101	TIP33C TIP34A	78p 74p	BAV19 15p BAV20 15p	BT116Use	LD461 25p LD466 1.45	LM345K 8.80 LM348N 62p	55555 2.59 5887024 4.39	12428114.2.6 1242840 3.8	0 74161 39p 4 74163 39p	74LS241 1 40	740163 1 50 740164 1 50	4539 89p 4543 68p	V.REGS
BUNG'A BUNDO	4 49	TIP34C TIP35A	88p 1.09	BAV49 15p BAX13 10p	TIC 116M BT119 2.37	LD468 1.65 LD471 27p	LM349N 1.09 LM350N 4.60	5A83210 3.98	TDA 3300 16 6	6 74 54 1 20 0 74 55 45p	74LS242 1.40 74LS243 1.40	74C166 1.50 74C173 65p	4553 2.25 4595 35p	(See also Linear (Cs)
E. 11165	3.95 5.95	TIP35C TIP36A	1 28	BAX16 11p	BT120 2.27 BT121 2.22	LD476 1.20 LD478 1.45	LM359N 1.44	SASSSC 2.59 SASSTO 2.59	TUDA 70000 3.4	5 74156 45p	74LS245 1.40	74C 174 1 88 74C 175 1 50	4556 35p 4560 1.49	Positive 100 mA
1200	70p	TIP36C	1.39	BAY38 20p BAY44 15p	TRIACS	LD479 1.65 LD481 27p	LM360N 3.88 LM376N 65p	SA5560 2.95 SA5560 2.95	TL061 60	p 74159 150 p 74160 59p	74LS247 1.40 74LS248 1.40	740192 1 50	4566 1.49	78L05A 29p 78L12A 29p
WED-AT!	55p	TIPATC	49p 55p	BAY93 10p BB103 70p	Texas 400V TO220 Case	LD486 1.25 LD488 1.70	LM375N 1.89 LM375N 3.40	SFF98364 7.99 51410 1.47	11011 34	p 74161 59p	74LS249 1.40 74LS251 45p	74C193 1.50 74C194 4.50	4589 1.85 4584 39p	78115A 29p 78124A 29p
RECROS MEDATI	55p	TIP42A	55p 59p	BB1048 80p BB104G 80p	TIC 2050 (4A) 66p TIC 2250 (6A) 74p	LD489 1.89 LD599 81p	LM3795 5.50 LM380N 750 LM380NB 1.50	SL490 3.47 SL810C 4.00	TL072 99 TL081 29		74LS253 45p 74LS257 45p	74C200 7.70	4585 59p	500 mA TO202
263412	55p 55p	TIP49 TIP50	1.20	88105 52p 88105A 57p	TIC226D(8A) 88p TIC236D(12A) 1.16	MOC3020 1 49 ORP12 95p	LM381AN 2:26	SL611C 4:00	TL082 45	p 74165 76p	74LS258 45p 74LS259 80p	74C221 1.95 74C901 90p	COMPICS	7805M 65p 7812M 65p
9E3413 9E3414	55p 95p	TIP53 TIP54	1.57	881058 58p 88109G 65p	1.16 TIC 2450 (154)	TiL32 71p	EM381N: 1:40	SL620C 6 00 SL620C 6 00	TL084 B9	74170 1 25	74LS261 99p	74C902 90p 74C903 90p	1802 6:50	7815M 65p 7842M 65p
WEDNEZ	55p 55p	TIP110 TIP112	74p 90p	BY126 11p BY127 12p	TIC2450(15A) 1,22 TIC2530(20A)	TIL38 440 TIL78 600 TIL81 1.60	LM3837 3.40 LM384N 1.40	5L623C 10.00	TE170 49 TE430 69	p 74173 59p	74LS266 25p 74LS273 75p 74LS275 1.25	74C904 90p 74C905 9.25	6502 3.24 6800 2.10	1 Amp TO220
# 000 # 000	55p	TIP115 TIP117	81p 96p	BY134 52p BY182 1.26	TIP BOOK INC.	TIL 100 72n	LM385N1 88p LM386N4 1.20 LM388N 2.43	SL630C 6.00 SL640C 8.00	UAA170 2.4 UAA180 2.4	9 74175 49n	74LS279 33o	740907 90p 740908 1.35	6802 2.40 6809 6.20	7805T 45p 7812T 45p
#E 025	55¢	TIP120 TIP122	69p 73p	8Y188A 65p 8Y206 36p	TIC 263D 25A1 2.13 TIC 263N	TIL116 1.10 TIL138 2.40	LM388N 2.43 LM387N 1.25	SL641C 8.00 SNIFEDOR 3.90	ULN2003 75 UPC57502 2.0	p 74176 38p 0 74177 45p	74LS280 1.80 74LS283 49p	740911 9.95 740912 9.95	8035 3.49 8080A 2.50	78151 45p 78241 45p
9E 20	55p 55p	TIP125 TIP127	84p	8 7 207 36p		TiL139 2.40 TiL209 9p	LM331N50 2.10	5N7501B 3.90 SN75003N 2.95	HPC1074H 99	74178 700	74LS289 4.70 74LS290 55p	740914 1.50	8065A 3.49	1.5 Amp T003
ME-KOO?	55p 55p	TIP 130 TIP 132	84p 93p	BY223 1.29 BY297 48p	2.46	TH.231 146	LM391N80 2 40 LM392N 95p	5N75023N 2.95		0 74181 1.40 5 74182 80p	74LS293 49p 74LS295 74p	740918 1.90	9900 19.95	7805k 1 39 7812k 1 39
864001 864001	55p 55p 55p	TIP136	93p 99p	BY299 55p BYX10 36p	Other Triacs 2N5756 (TO5)	TIL312 1.02	LM393N 1 20 LM394H 3 80			5 74184 89p 74185 69p	74LS298 79p 74LS298 1.95	74E92C 12.50 74E922 5.75	Z80A 2.98 Z80B 8.60	7815K 1.39 7824K 1.39
10E-1	55p	TIP 137 TIP 140	99p 1.04 1.04 1.15	BYX10 36p BYX55-350 62p BYX71 3501.10	2N6070 1.00	TIL313 1.02 TIL401 3.50 TIL403 3.80	LM396K 14.98 LM709NB 64p LM709CH 1.00	SN76550 B0p	UPC1188H 2.7 UPC1181H 1.9 UPC1181H 1.9 UPC1182H 3.7 UPC1183H 6.4 UPC1186H 1.5 UPC1188H 4.5	74185 489 5 74186 4.69	74LS323 1.95 74LS324 1.95	740923 5.75 740925 6.80	11024	- Negative
MEN CA	55p 55p	TIP142 TIP145	1.04	BYX71 600 1.52 ITT44 10p	2N6155(TO127)	TIL408 4.10 TIL722A 49p	LM709CH 1.00 LM710CH 1.44	SN76666 2.90 SOATP 1.95	UPC 1 183H 2.9	5 74188 2.48 5 74190 50p	74LS325 3.50 74LS326 3.50	74C926 6:80 74C928 7:50	MEMORIES 2102AL2 1.35	79LD5 49p 79LD2 49p
PE TOTAL	55p 55p	TIP147 TIP162	4.95	ITT921 10p ITT923 15p		LINIC'S	LM710CN 62p LM711CH 1.38	SO42P 1.95 TA7066 4.49	UPC1 186H 1.5	5 74191 60p 74192 60p	74LS327 3.50	740929 13:00 740930 5:50	2111 1 3:00	79112 49p 79115 49p
WHEE C	55¢	TIP2955 TIP3055	77p 70p	ITT2002 27p	(Quadrac) 2.23 40486(T05)1.65 40512 2.70	AY1-5050 95e	LM711CN 70p			U FASSA BUD	74LS347 1.35 74LS348 1.40	740932 2.45	2114(200ms)99p 2532 3.25	500 mA T0202
Man	55¢	TIS43	50p 45p	M22361 1.80 OA10 70p		AY3-8910 3-99 AY3-8912 4-95	LM723CH 95p LM723CN 35p LM725CH 3.40	TA7120 1.99 TA7130 1.75	UPC 1212C 1.60 UPC 1213C 2.00	74195 60p 74196 45p	74LS352 71p 74LS353 71p	40 CMOS	2564 6 25 2708 3 50 2716 (5v) 2 65	7905M 80p 7912M 80p
MENTE:	\$5¢ 75¢ 75¢ 75¢ 75¢	TIS46 TIS47	45p 49p	0A47 20p 0A90 10p	40842 1.92	CA3018 75p	LM725CN 3.19	TA7202 4.49 TA7203 4.99	UPC1228H 1.3 UPC1447H 1 4	7 74197 45p	74LS365 40n	4000 16p 4001 16p		7915M 80p 7924M 80p
WE SEE	750 750 750	TIS48	50p	OA95 20p	BT139-600 1.95	CA3018A 1 99 CA3020 1 99 CA3020A 3.90	LM733CN 69p LM741CH 96p	TA7204 1.99 TA7205 1.20	UPC 1470H 1 21 UPC 2002H 2 9 UPC 2002V 2 9	74199 1.50 74221 73p	74LS366 40p 74LS367 40p	4002 18p 4006 49p	4027 3.00 4060 9.50	1.Amp T0220
N. AL	1.69	TISBBA TISBO TISB1	80p 28p	OA200 20p OA202 20p	ZENER'S	CA3021 3.20	LM741CN 18p	TA7210 6.95 TA7222 1.75	UPC 2002V 2.9 XR2206 3.9	TTL &	74LS368 40p 74LS373 99p	4007 19p 4008 32p	4116/200ns/99p 4118.3 3.25	7912T 57p
A-852	1.72	71592	30p	5P09000 75p SPD9002 95p	400-500mW E24 Series	CA3022 3 12 CA3026 1.52	14747CN 69p	TA7223 3.98 TA7227 5.82	XR2208 3.9: XR2207 4.00 XR4212 1.80	CMOS	74LS378 99p 74LS386 1.14	4009 24p 4010 24p	4164 4.55 5204 7.50	7924T 57p
18080	2.90 2.10	VINTOKM	54p 60p	GRAPHIC	2.4-47V 7p	CA2028A 95p CA3028B 1.99	LM748CN 35p LM748C14 70p LM1811 8.60	TA7310 1.49	ZN409 2.2	Pls phone	74LS390 46p 74LS393 99n	4011 16p 4012 19p	6116F3 3.85 6514 3.30	1.5 Amp. TO3 7905K 1.99
A 15	2.50	VN46AF	95p 99p	PROCESSOR EF9365 35.00	1.3 Watt E24 Senes	CA3030A 2.97	LM1303N 2.25	TAA263 3.88 TAA300 3.95 TAA320 2.05	ZN414 1 00 ZN1034 1 90 ZNA134F 29 90	for latest	74LS395 89p 74LS396 1.90	4013 19p 4014 46p	6810 1.45 7489 1.65	7912K 1.99 7915K 1.99
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AUDIO DESIGN

Few areas of electronics have accumulated as much superstition and hype as the design of power amplifiers — here is John Linsley Hood's attempt to cut through the muddle.

considerable amount of mystique surrounds the whole field of audio amplifier design, particularly in regard to the part which actually delivers electrical power to the loudspeakers, and a vast amount of effort is spent in laboratories, listening rooms and editorial offices in sorting the good from the not-so-good. How much of this mystique is justified is a speculative question, a source of pleasure for those whose efforts have been received with acclaim, and a source of indignation for those whose designs have been ignored by the cognoscenti or impugned by the pundits.

My own feelings in this matter, particularly in respect of the hi-fi devotees, are highly ambivalent. On the one hand, I am convinced that much of stock in trade of the hi-fi journals, their 'subjective' reviewers, and the manufacturers and dealers who follow in the train of their approval, is built upon the identification and exaggeration of differences which are, in reality, fairly small. On the other hand, I know that there are sound differences between differing designs, some of which are easy to live with and render their inputs to the listener in a pleasing — and sometimes exciting — light, others have the capability to make everything they handle sound rather drab and second-rate, and others may appear fine at first hearing and yet, after a day or two, make one not wish to listen further.

Some of this is simply a matter of incompatibility between the separate parts of the audio system: I still remember, very clearly, paying a visit to a hi-fi fanatic of my temporary acquaintance, who had spent many thousands of pounds in assembling a set of gear which included all the most expensive and exotic bits of hardware that had received rave reviews in the magazines. His wife would not stay in the same room with it. After listening to it for half an hour, I didn't blame her. So one of the basic requirements of an audio power amplifier must be that it should be highly tolerant of the type of LS load applied to it.

Other components of the sound quality characteristics of the power amplifier relate to quite clearly definable design aspects, which one hopes that the designer will have given due thought to. Yet other contributing factors undoubtedly reside in a grey area of technology as yet not very clearly defined, where one may more surely say that this or that is a good thing to do — because one knows from experience that this is the case — but one cannot be so certain that something else, as yet untried, will be equally good, or give sound engineering reasons for this belief.

So — this is the scene; now to the engineering.

Output Power

Because of the nature of the sensitivity of the human ear, and of the physical principles of acoustics on which hearing is based, doubling the amount of electrical power fed to a loudspeaker does not make the resultant sound appear twice as loud. In reality, this is a

logarithmic relationship, in which apparent increases in sound loudness are related to power by the equation W = k.log₁₀P2/P1. While precision in this field is difficult because of the subjective nature of the thing being measured, and because apparent loudness is related to frequency anyway, one can say, roughly, that 3W, 30W and 300W are increments in amplifier power which would correspond to doublings in sound loudness at maximum volume. One can see from this that some very big steps in amplifier power are needed to get significant gains in sound level. The converse is also true, that microscopic amounts of sound power, like the buzzing of a fly's wings, or the LS output from the noise voltage of a well designed low-noise amplifier, are still quite audible!

As we have seen earlier, power output is related to output (RMS) voltage and load impedance by the equation $P = V^2/R$ or $P = I^2R$ in the case of output current. If an output of 100W is required into an LS load of a nominal 8 ohm impedance, an RMS output voltage swing of $\sqrt{800}$ (28.28 V) is required. This corresponds to a peak-to-peak voltage swing of 80 V. Allowing for voltage drops in the various output stage components a potential between +ve and -ve HT lines of 120 V is probably needed. Now, let us suppose that the LS impedance drops to 2 ohms at 15 kHz. 100 W will then correspond to a peak current of $\sqrt{50}$ x $\sqrt{2}$ amps, or 10 A. (Fortunately we don't have to cater for a peak-to-peak current!) So, our amplifier, to meet this spec. with this load, would need to be able to deliver 28.82 V RMS and 10 A peak current, but not simultaneously, normally. Powerful amplifiers need big, and expensive, power supplies. They also need transistors and capacitors which are capable of withstanding these high working voltages. Apart from this, and the bigger heat sinks, they are not much different in design from their smaller brothers.

Power Bandwidth

The audio spectrum is assumed to lie between 20 Hz and 20 kHz. With average listening rooms, average good quality LS systems, average listeners, and averagely good quality programme material, 45 Hz — 15 kHz is a more realistic assessment. Happily, there isn't much programme energy in the part of the audio spectrum above 10 kHz, or we wouldn't stay around very long to listen to it, so — being realistic — we don't need to cater for maximum power output in this region unless the equipment is going to be reviewed. There is also not much VLF output from either progamme material or LS units. Unfortunately, in this case, if the amplifier cannot operate well below 30-40 Hz it will sound 'thin', and will probably overload on spurious signal inputs (record rumble and the like) which is disastrous sonically.

Some of the more acute listeners can undoubtedly hear the difference when HF response is curtailed, even though this is above their ear's frequency response — because of the absence of beat-note effects due to the interaction of high frequency sounds within the non-

linearities of their own ears. A better HF response may not make things sound better, but it can make them sound different.

This is where the first of the needs to compromise occurs. With typical power junction transistors, which are fairly sluggish devices, increased HF power bandwidth can only be obtained at the expense of loop stability in a negative feedback amplifier (though feedforward systems avoid this snag). If loop stability is poor, the amplifier transient response is bad, and this can introduce some pretty drastic distortions into pulse type signals, such as drum beats or cymbal clashes. An amplifier with a good loop stability is usually much more pleasant to listen to, and will certainly be less fussy about the LS load characteristics.

Negative Feedback And Loop Stability

Negative feedback — the instantaneous electronic comparison between the signal at the output of an amplifier, and the signal at its input, and the generation of a corrective adjustment to the effective input signal to make sure that these input and output signals are closely identical - remains the major tool in the hands of the cir-

cuit designer. However, there are snags!

We have seen earlier in this series that we need to use enough NFB. Too little may just make matters worse, by substituting less pleasant forms of distortion for the ones we have reduced. We also need to make sure that our use of NFB does not make the whole system unstable, and this is particularly the case for audio power amplifiers which have to drive LS loads, since these are notoriously complex in their impedance and delayed response characteristics. It is also essential to remember that a feedback path is just what it's name suggests, a means by which signal components, both wanted and unwanted, can be fed back from the LS load to the input of the amplifier. Since LS units can and do generate electrical signals of their own (as a result of internal cabinet echoes, and as a consequence of inadequately damped reflections along the LS diaphragm) we need to watch this point.

With regard to loop stability, this field was investigated by Bode and Nyquist very many years ago, in respect of the parallel field of closed-loop servomechanisms. Personally, I find the Bode diagram, of Fig. 1, the easiest to follow and to explain. In this diagram, the gain and phase-shift of the amplifier is shown simultaneously as a function of frequency. If the amplifier has a gain of 1 (or more) at a frequency where the feedback is in phase with the input (an NFB phase

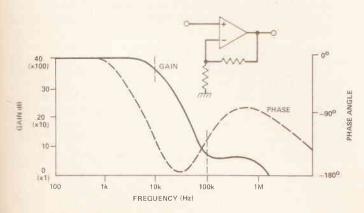


Fig. 1 Gain/phase or Bode diagram for conditionally stable feed-back amplifier (a change of load might make this amplifier oscillate at 30-50 KHz).

shift of 180°) it will oscillate. The reason for this is simple. it is that the feedback path is itself providing an input signal of the right size and phase to generate the actual output, without the need for any other input signal at all! If the gain is more than unity at this frequency, the signal output will continue to increase until some other effect,

such as clipping, reduces the gain to unity.
Unfortunately, it isn't sufficient merely to ensure that the amplifier doesn't oscillate on load, there must be an adequate margin of gain, or phase, at the -180°, or unity gain, points to make sure that the amplifier isn't triggered into some form of misbehaviour during transients in the input signal, or during temporary overload. In particular, the 'settling time', the time which is required following a sudden input voltage excursion before the system settles at the new level, depends solely on the system speed and stability margin, as shown in Fig. 2. I would very much like reviewers of audio amps. to measure, and quote, this value for a square-wave, or step input, with a real live LS load, since this is one of the areas where the pursuit of low THD values, at the top end of the audio spectrum, can lead to circuit design characteristics which are bad for the transient handling qualities of the amplifier, and may make it very fussy about the LS units with which it is used. As a comment on this, it does seem pointless to try to reduce 0.1% THD at 20 kHz, which is inaudible, and swamped by the distortions on the input signal, (if there is any, at this frequency) to 0.01% THD, which is just as inaudible, if the price one has to pay is a very bad transient response, and some 20-50% distortion on transient signals - which is very clearly audible!

By and large, in a typical audio amplifier, the major factor which dominates the gain and HF phase-shift characteristics is the relative sluggishness of the output transistors. The faster the response of these, the easier it is to design a good, stable, amp. The snag is that fast output junction transistors are also more fragile, and need more restrictive protection circuitry to prevent them from damage in use. This in turn makes the amp. less good at driving low impedance LS loads, and so on . . . Valves, of course, would be faster, were it not that a very sluggish and awkward output transformer is then needed. The answer, and a virtually complete one too, is to use power MOSFETs. Some of the recent ones of this type have a virtually instantaneous response, and are more linear in their characteristics than either valves or junction transistors. They too have snags, of which the

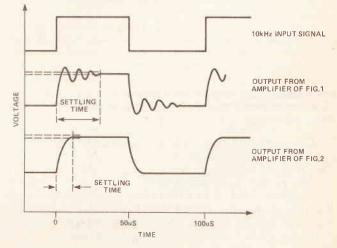


Fig. 2 Influence of gain and phase margins of NFB amplifiers and settling time.

main one is that they are fussy about the phase characteristics of their loads, but there is a simple design answer to this. So, with power MOSFETs, and some reasonably straightforward design, it is practicable to design audio power amps. which are a good ten times better, technically, than their possible forerunners.

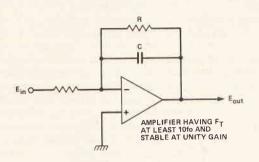


Fig. 3 Feedback amplifier having good gain and phase margins.

Distortion — And NFB

We have seen earlier that not all distortion types are equal in their unpleasing effects, and also that the character of a distortion can be greatly influenced by the relative phases of the signal components (clipping and crossover types differ mainly in the relative phase of the discontinuity, but sound very different). This effect has relevance to the behaviour of multi-driver LS systems, which can jumble up he phases of the signal (= time of arrival to the ear) and thereby alter the nature of amplifier nasties. So our efforts in the design exercise should be aimed at removing components of distortion which can be so transformed.

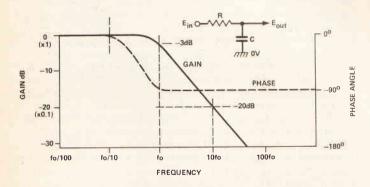


Fig. 4 Gain/phase diagram for a simple RC attenuator; the characteristics of the amplifier in Fig. 2 would be similar to this.

Obviously it is helpful if we can keep the distortion of the amplifier as low as possible before NFB is applied, in that low NFB leads to better loop stability. A useful design yardstick, cribbed from the servo-mechanism engineering field, is to determine the 'time constants' (the RC integrator values which would, for example, simulate the HF roll-off characteristics of the components or circuit elements being investigated) of the several bits of the circuit, and then make one of these—perhaps deliberately added—ten times the size of the rest. This isn't quite as arbitrary as it seems, since if we wish to end up with the fairly ideal Bode diagram for the

amplifier shown in Fig. 3, we must remember that a phase shift due to an RC element begins one decade, in frequency, below the -3dB 'turn-over' point of that network, shown in Fig. 4. In this way, the system will tend to behave as though it had only a single phase-shifting

component

Afurther useful design approach is to try to design the system so that there are not more than two signal handling 'gain' stages within the NFB loop, using more loops if necessary. This approach isn't easily possible with power amps. so other approaches may be necessary, including the useful phase-lead generating 'step network'. However, one can always put in an internal NFB loop, operating only at HF (the place where in transistorised amplifiers trouble is likely to arise) and including only two gain stages. This is a helpful technique which leads to good-sounding amplifiers.

The aim of the designer should be to produce an amplifier in which the harmonic distortion is as low as possible, and the gain bandwidth as high as possible, before the application of any NFB, so that the NFB can be used mainly to control and stablise the gain and output impedance characteristics, rather than as a way of lower-

ing the distortion.

So far as the feedback path itself is concerned, it is probably better not to employ a parallel HF compensation capacitor across the NFB resistor, in that this can make the amplifier sound less well on some LS units. It is also helpful in the task of making the amplifier as widely load-compatible as possible, if a small resistor, in the range 0.15-0.33 ohms, is connected in the output circuit of the amp. to act as the input limb of an attenuator, against the much lower output impedance of the amplifier itself, to assist in attenuating signals originating in the LS units themselves, and preventing these from getting back to the amplifier inputs.

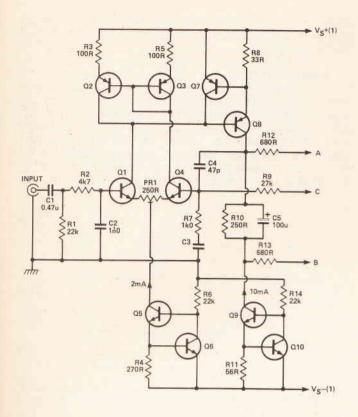
A final thought, with regard to amplifier 'sound', G. King some years ago pointed out that the human ear is not a very good judge of performance in respect of distortion, in that of a number of randomly chosen people, all reasonably competent judges of sound quality, either preferred the presence of some 0.3% even order harmonic distortion (deliberately added after the signal sources) or had no specific preference. Similar work has been done by other investigators. This tends to cast doubt on the value of such judgements, where the listener may actually prefer an inferior performance, because of attractive colouration added to the sound, and think the equipment is therefore better (i.e. more faithful to the original output). One cannot, unfortunately, design for this — and whatever its sonic merits, distortion will always make clear sounds somewhat more muddled.

A Practical Design Approach

Earlier in this series, I referred to the need to prevent intrusion of signals from the supply lines into the signal path, and to the ways of linearising gain stages. I have also urged the quality benefits which can be gained by the use of stabilised power supply lines, in a previous article², so let us now add this information together in a practical design exercise.

My preference for power MOSFETs as the output devices is definite, but not just as simple source-followers where they require an output inductor in the LS lead in order to prevent VHF oscillation due to the devices own small source lead inductance. If the power MOSFET is used in combination with a bipolar small-signal transistor, in the output stage layout shown in Fig. 6, this small inelegance can be avoided, without

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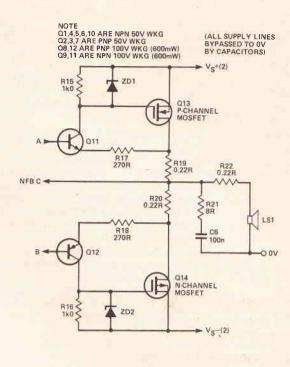


Fig. 5 Power amp. driver stage.

Fig. 6 MOSFET output stage.

degradation of the fast response of the Mosfet. The only necessary device protection can then be an output circuit fuse, or better still, a current limited DC power supply, since the circuit resistance of fuse-holders (and LS connectors) is finite and non-linear!

A typical small signal voltage amplifier to drive this output stage is shown in Fig. 5. Because small-signal bipolar transistors are cheap, I have been fairly lavish in my use of these, where they can confer some practical benefit in the operation of the circuit. Starting from the beginning, there is an input DC isolation capacitor C1, and a resistor R1 to define the '0V' DC level of the input. R2 and C2 are an HF roll-off circuit, to prevent very fast HF transients being applied to the power amplifier. A time constant of $4.7~\mu S$ (4k7 and 1nF) will give an HF -3dB point at $33\,\text{kHz}$, which is adequately outside the audio band, but not so high as to be ineffective.

In order to preserve the DC symmetry of the input stage, which is a long tailed pair in the interests of low distortion, the total resistance path should be the same for Q1 and Q4 bases, which fixes R1 at 22k. Q5 and Q6 are a two-transistor constant-current source, of the kind we have already met, with the value of R4 chosen to give a collector current of 1 mA through each of the input transistors. PR1 is a preset trimmer which allows the DC output level of the power amp. to be adjusted precisely to DV. Because the Q5, Q6 type of constant-current source has a very high dynamic resistance, it helps to prevent unwanted AC rubbish from getting into the input circuit from the —ve supply line.

I have chosen to use a simple current mirror, Q2 and Q3, as the load for the input long-tailed pair, in order to combine the signals from the two input transistors and optimise the input stage gain. From this, the signal is fed to the second stage amplifier — a medium power PNP transistor in the interests of gain linearity — again loaded

by a two transistor constant-current source, to ensure high AC gain and low distortion (if the current change through Q8 were zero, the distortion due to Q8 would also be zero). In this case, the value of R11 is chosen to give a collector current of 10mA,in order to lessen the effect of the variable drive current into the output stage input transistors, and in orde to push the maximum slewing rate possible with C4 up to a high value.

R11, bypassed by C5, provides the necessary 1.2 V potential drop to bias he output stage to a 100mA quiescent current.

Under overload conditions, Q9 and 10 limit the current which can be drawn from the -ve line to 10 mA. Q7 and R8 provide a similar anti-destruction protective

function in respect of Q8 and the +ve line.

R9, R7 and C3 provide the negative feedback path from the output stage to stabilise the AC gain to 27, which is a convenient value since it allows maximum output (in this case 50W) from a '0VU' (0.77 V RMS) input signal level. C4 provides HF stabilisation by means of an internal HF NFB loop just enclosing the two gain stages Q1/4 and Q8, which gives a good, well-damped, transient response, especially under the critical reactive load conditions. LS units most definitely do not behave like 8 ohm load resistances!

R12 and R13 serve the useful function of preventing temporary latch-up if the amplifier is driven into clipping; in their absence clicks and bangs are prolonged, and sound louder. Also, clipping will sound more objec-

tionable without them.

The output stage which will join on to this amplifier, and which I have shown in Fig. 6, with component numbers appropriately labelled to follow on, is unusual in that it uses the MOSFETs in a compound emitter follower configuration, with Q11 and Q12 as the input devices. Because the LS load is then connected to the

drains of the power MOSFETs, the need for the series output inductor is removed. Excess voltage across the gatesource junctions of the MOSFETs is prevented by ZD1 and ZD2, while R15/17 and R16/18 limit the AC gain of the output stage to 5.

R22 is the resistor which attenuates signals returned from the LS unit, and R21/C6 is the so-called Zobel network which prevents the output stage seeing an open-

circuit at HF if the LS unit is disconnected.

I have labelled the DC supplies to the AC gain and output stages VS+(1) and VS+(2), and VS-(1) and VS-(2). This is because it is then possible, and advantageous, to operate these from two separate DC supply sources, which prevents intrusion of high powered nasties from the output stage supply lines into the sensitive earlier stage circuitry. This gives most of the advantages of a system operated from stabilised DC supplies, but at a much lower cost. Also, if one wishes, one can operate the gain stage (Fig. 5) from a stabilised source — after all, one has to supply only 12 mA per channel, which doesn't make it too dear — and then operate the output stage from really large, low equivalent series resistance, DC supply electroyltics, and gain the benefits of both, though one would then need fuse protection in the LS lines.

So, this is how one gathers together the requirements in the design of an audio amplifier. Now while this is a very good amplifier, of the best modern standards and with an excellent technical and audible performance, I am not, at this stage, going to fill in all the small details, power supplies, PCB and component layout, etc, because this amplifier is strictly conventional in its design approach, and we can do some rather more crafty tricks in this type of design, to give us just a little extra. So, regard this as a design exercise, the sort of thing which the circuit designer of some amplifier manufacturing firm will do when his boss tells him they need a new upmarket design to go with the magnificent advertising promotional blurb, which the Ad. agency have already come out with. (Though, in reality, the designer will always have to do a bit of 'fine tuning' to the circuit, to make sure that it is as good as possible in all the various

conflicting requirements of the system.)
I will show a final, 'improved', version of this, with a very high quality preamplifier — again, already outlined in form in a preceding part of this series — and appropriate power supplies, in a later article. Meanwhile, may I round off this part of the series with a look at some of the

possible 'amplifier types'.

Class Distinctions?

Although, as I have indicated above, I have an ambivalent attitude to the razzmatazz of the hi-fi scene, as an audio circuit designer I cannot escape from contact with it, and I read with interest, surprise, concern or dismay, the comments and thoughts of my peers in this field. A large aspect of this, which has been continuously explored, and argued about, ever since transistors appeared on the scene, has been the debate valves vs. transistors, and class A vs. class-AB (or w.h.y.). Since I originally stuck my nose into this field as the author of a simple class-A design (which I valued because it was simple, rather than because it was class-A and which is as good as any amplifier I have designed or obtained from other sources since then) I cannot simply say, with my friend Reg Williamson, that class-A is the lazy man's solution, a simple 'sweeping of design problems under the carpet'.

I have, in consequence both of my original involvement and the subsequent, continuing debate, spent many hours in thought and experiment on these points, and have come slowly to conclusions which I am prepared to defend.

Valve Amps

These are not usually very good, technically. Even the best of them will not compare well, in performance, with a good transistor unit. However, they do have some useful advantages. The first of these is that they are pretty well unburstable; the second is that they overload gracefully, with a rounded-off clipping, which allows the loud-noise brigade to drive them closer to the permanent clipping level without driving the dog mad. This

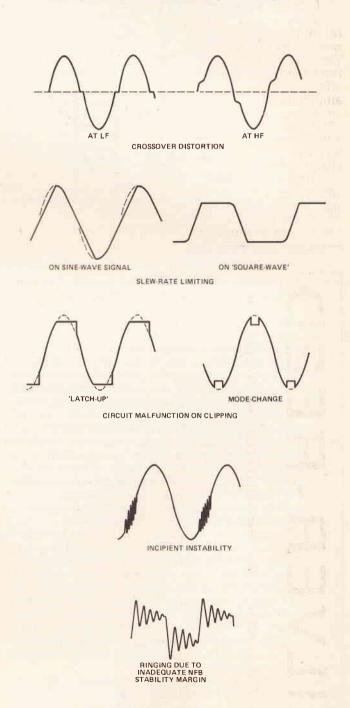


Fig. 7 Oscilloscope waveforms of some power amplifier circuit malfunctions.

FEATURE : Audio Design

allows the legitimate claim that they sound 'louder' for the same wattage. However, distorted sounds also sound louder than undistorted ones. The third advantage is that their distortion products, of which there are usually quite a lot, are of a kind to which the ear does not object too strongly. Fourthly, because they don't usually use much NFB (they can't because of the o/p transformer phase shifts) they are tolerant of LS loads. Finally, they look pretty, and make the Joneses jealous. The snags start with the price!

If one wants to, one can build 'soft clipping' into the

preamp. for one hundredth of the price.

Class-A vs. Class-B

If one must use junction transistors, there is little doubt that they will work better in class-A (where the quiescent current is that which is needed for full output). They will have a better, and more uniform HF response and much lower distortion for the same amount of NFB — and hence a better transient response. Class 'A' amplifiers do, however, chuck out an awful lot of heat if any large amount of power is needed. Remember that at 20% efficiency a 100W/channel amp. would generate 1kW of heat, and need to get rid of this with the amp. at less than 100°C. If you can be content with 10W/channel, then class-A is an excellent choice.

So far as class-B (or more strictly AB) is concerned, where the amplifier operates at a quiescent current significantly lower than the operating one, cross-over distortion is inevitably present where one output device hands over to the other. Good circuit design, and the

judicious use of adequate NFB, will reduce this to less than the background noise level, especially if the output devices are power MOSFETs, rather than the more sluggish junction devices whose limitations begin to show in the 10-20kHz region. I do not, honestly, think that the differences between these types are anywhere near as big as the differences between different FM channels, or between different pressings of the same LP disc.

Feed-forward techniques, as in the 'Quad' current dumping amplifier, where a small, low powered class-A amplifier is used to fill in the missing bits in a straight class-B output stage, give results which are comparable to other good design approaches using similar output devices. Variations in the feed-forward technique, which is, itself, of considerable age, have allowed the Japanese publicity agents scope for much exaggeration.

For the record, I have shown in Fig. 7, the 'scope waveforms of some typical power amplifier defects, which, one hopes, the designer will have removed

before manufacture starts.

In my next part of this series I propose to look at the field to tape recoding and cassette systems, an area which has developed enormously in the past few years.

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 Linsley Hood. J. L., Electronics Today International, May 1983, pp 18-22.



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TECH TIPS

Semi-Switchless Switch

Ian Sherlock Preston

Designed to alleviate the persistent use of a wall light switch, this circuit could also be of use in households with elderly or disabled members. The circuit turns on the light when anyone enters the room (which must have a single entrance), counts the number of people entering or leaving, then turns off the light again when the room is empty.

The phototransistors each give a positive-going long pulse when the light to them is blocked; they should be about 5 to 10 cm apart, so that

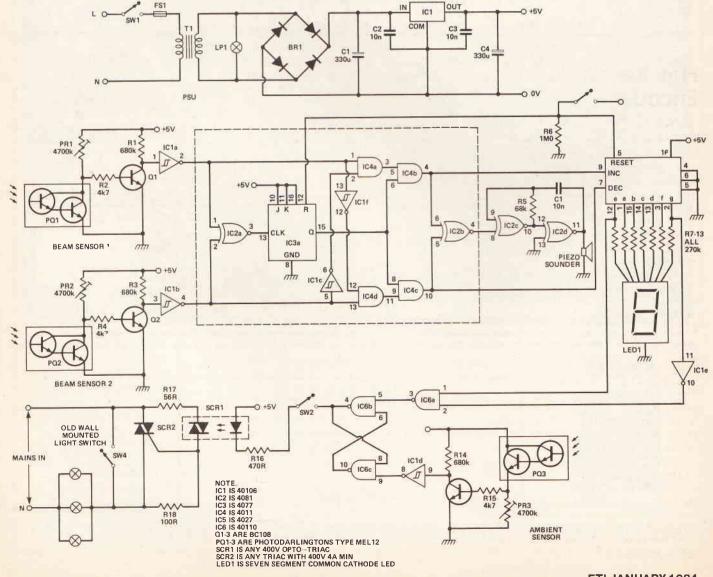
both beams are cut for much of the period of time it takes someone to enter. These pulses are amplified by Q1 and 2 and IC1a and b.

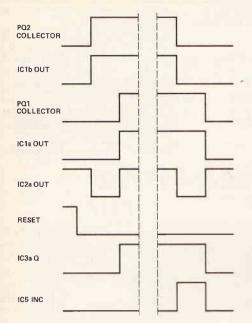
The figure opposite shows the timing of these signals; only in the final section, where the pulse from PQ2 has gone low again, do the conditions for the increment pulse to reach IC5 occur, which is when Q from IC3a and the output from IC1a are both high and the output from IC1b is low.

IC5 is an up/down counter sevensegment driver which counts the number of entries and exits from the room. IC1e and IC6a detect a zero on the display. The latch formed around IC4b and c ensures that the light will only come on if there is no light falling on the ambient light detector, PQ3, but will then stay on until the room is vacated. The remaining circuitry for driving the triac via an opto-triac is quite straightforward.

SW2 is an auto/manual switch; SW3 is the reset switch, which should be used at switch-on and whenever the house-hold children set about trying to confuse the unit.

A suggested method of construction is shown in the diagram. Standard three-core mains cable can be used to link the unit to the existing switch-plate (the cable carrying live, neutral and triac return) but note that the unit should be powered from a separate supply, and that it must be earthed to be safe. A metal box can be used to house all the phototransistors and the circuit





SUGGESTED MOUNTING

BEAM 1

LAMP BOX

board and transformer; the beam sensors will need light-shielding tubes (sawn off felt tip pens could be used or something similar) which can be directed at a single light-source fitted on the opposite side of the door frame.

The ambient light sensor may need to be mounted separately, as the box may have to be mounted outside the room, depending on the direction that the door opens. The ambient light detector must be arranged so that it picks up light

from only the room being monitored.

An alternative to visible light beams would be to use modulated infra-red beams, but this involves extra complexity, which is why visible light was chosen.

Hex Keyboard Encoder

Adam Strange Carrickfergus

While designing a micro system, I had to decide between using a software or a hardware hex keyboard encoder, and settled on the latter. Out came the good old Texas bible and the scratch pad. Some time later I came up with this little circuit which, even though I do say it

myself, works rather well.

The heart of the circuit is ICI ('LS93), a four-bit binary counter, which addresses IC2 and 3, which in turn scan the keyboard. IC3 ("LS156) is a two-to-four line decoder with open collector outputs. The two-bit address, A,B, selects which of the four outputs is low, IC2 ('LS173)) is a four-to-oneline data selector; the two-bit address, A,B, selects which line is tested, the output Y going low when the selected input is low. So the address on the outputs of ICI when output Y of IC2 is low is the address of the key pressed. (IC2 and 3 are dual devices, only one half of either being used here and alternative pin numbers are given where these are applicable on the circuit diagram).

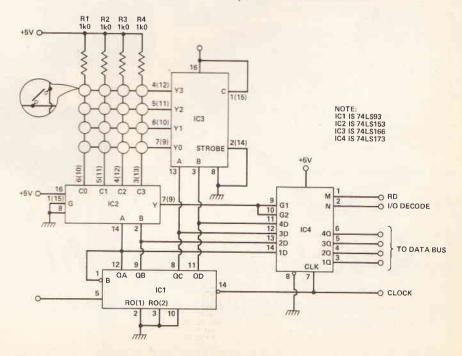
The next step was to capture or latch this address. This is accom-

plished by IC4 ('LS173) which is a four-Bit D-type register with tri-state outputs (handy for CPU data bus). When the clock pulse goes from high to low the address from IC1 is incremented. This address is clocked into IC4 only if output Y and IC2 is low, this occuring on the low-to-high clock transition. Thus IC4 will hold the code of the last key to be pressed.

All that remains is for the CPU to

read the data from IC4. This occurs when the I/O decode and the RD inputs are low.

A cheap way to make the keyboard is to use an old calculator, replacing the original PCB with the one for the encoder. Suitably designed, the PCB for the encoder could be made to fit inside the calculator case — and if the display is still working, this too could be pressed into service.



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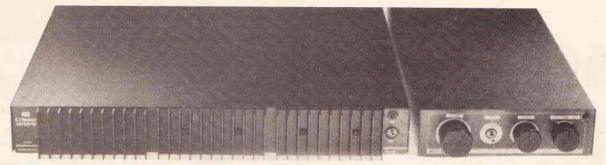


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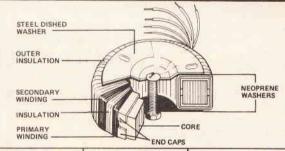
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MODULAR PREAMPLIFIER PART TWO

Some people are not happy unless they have a mass of controls not dissimilar to Concorde's flight deck on their side-board. The circuits here can help to extend the basic design, built using the modules featured last month, to include parametric tone controls, balanced output stage and a headphone amplifier.

block diagram of the extended preamp is shown in Fig. 1, and apart from the increased circuitry, the main difference between this and the 'basic' design is that the volume control is no longer at the input. This obviously means that consideration has to be given to the possibility of overload. In Part 1, it was shown that the disc overload margin could be maintained at an adequate 32dB if the output level of the disc input stage was 200mV for its rated input. In order that this margin is not reduced, no gain may be introduced before the volume control, and the gain necessary to give a 1.0V output

should be made up by the output

stage.

The input switching and tape

The same as in the buffer remain the same as in the simpler unit, but after the monitor switch, a unity gain buffer amplifier presents a high input impedance to the line inputs, and provides a low impedance drive to the tone control circuitry. The attenuator on the compact disc input is not to avoid overload, as the input and tone control circuits will easily handle the output of any CD player. Its purpose is to limit the signal level so that the volume control is not operated at a setting where its inter-track balance is not likely to be better than 3 or 4dB.

Tone Controls

Although fully paid-up members of the Flat Earth Society would have us believe that any form of signal processing is guaranteed to make a pig's ear of the emotional experience of listening to a group of musical morons twanging guitars and wailing in voices more suited to Billingsgate than Covent Garden, it should be remembered that most recordings are subject to considerable amounts of 'equalisation', usually to satisfy the producer's requirement for a particular type of sound. No allowance is made for the introduction of random phase shifts, or that the intricate

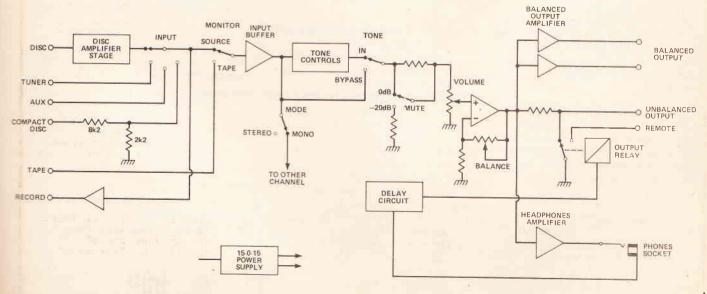


Fig. 1 Block diagram of the extended preamp.

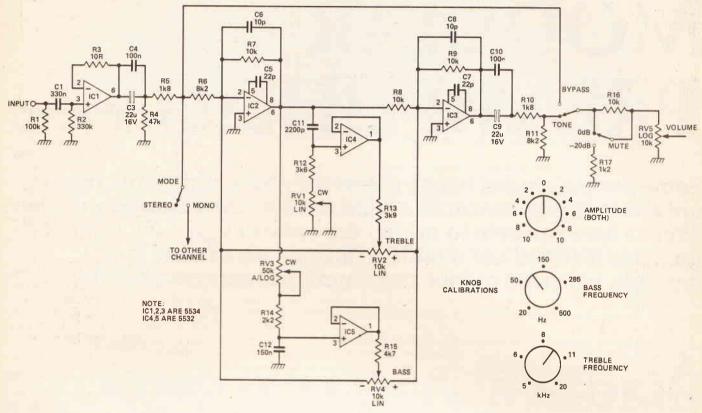


Fig. 2 Circuit diagram of the tone control module.

relationship of harmonics is sent on a one way trip to the cleaners. The object is to change the sound to make it more satisfactory, and if tone controls are used in the replay process for exactly the same purpose, surely no-one has the right to complain?

The type of tone control fitted to most hi-fi equipment is far from ideal, usually being much too dramatic in operation — for example, if it is required to lift frequencies below about 100 Hz, the effect is usually to lift, by varying amounts, everything up to at least 1 kHz, and even higher.

The circuit shown in Fig. 2 is somewhat more sophisticated than usual, possessing in addition to the normal lift and cut controls, adjustment of the turnover frequencies of the two sections.

Operation of the circuit is quite straightforward. IC1 acts as an input buffer, presenting an input impedance of approximately 100k ohms to the line inputs of the preamplifier. The input of IC1 is AC coupled by C1, which together with R2 fixes the -3dB point at

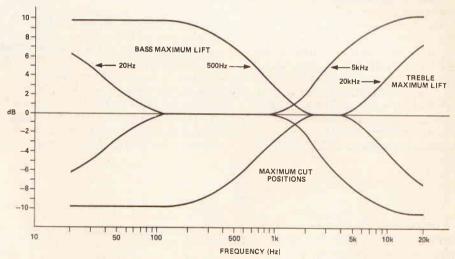


Fig. 3 Response curves for the tone control module.

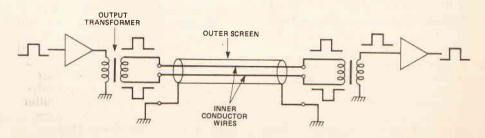


Fig. 4 The basic principle of balanced line operaton.

PROJECT: Modular Preamplifier

about 1.5 Hz — low enough to prevent objectionable low frequency phase shift. The output of IC1 drives the pair of inverting stages formed by IC2 and IC3, the input resistor to IC2 being split to allow mono summing of the two channels. The signal path is maintained at unity gain by the equal input and feedback resistors of the two stages.

The output of IC2 feeds two single-pole filters which are buffered by IC4 and IC5. The filter formed by C11, R12 and RV1 has a high pass characteristic with its -3dB point adjustable by VR1 from 5.3 kHz to 20 kHz. Operation of the treble control, RV2, decides the destination of the high frequencies that emerge from the output of IC4 - in the "cut" position they are applied as negative feedback to IC2, and in the "lift" position they bypass R8 giving additional gain to IC3. The amount of lift and cut is controlled by R13, the value specified giving a $\pm 10 dB$ variation.

The bass control works in the same way, except that a low pass filter comprising C12, R14 and RV3 selects the low frequency range which is variable between 20 Hz and 480 Hz.

This type of tone control is characterised by shelving response curves with no interaction between the bass and treble sections. The curves are shown in Fig. 3 which illustrates the range of the variable frequency controls.

As the tone control section is non-inverting from input to output, it can readily be bypassed as shown. To ensure that there is no change in level when the bypass switch is operated, the 2.9dB attenuator formed by R5, R6 and the volume control is duplicated by the addition of R10 and R11 at the output of IC3.

The mute switch has been added, as much for convenience as anything. When changing records or when the 'phone rings it is very useful to be able to reduce the overall gain without disturbing the volume control setting.

Output Stage

The volume control is followed by the unbalanced output stage, already described in part 1. However, in order to give an additional 2.9dB of gain (to counteract the loss in the tone control circuit) the values of R4 and R6 should be changed to 133R and 300R respectively. The balance control characteristics are very slightly changed by this, as shown in Table 1, but they will still remain accurate to the calibrations.

In normal circumstances, the unbalanced output stage is all that will be needed. The main advantage of using a balanced output stage is realised when the signal output from the preamp has to run more than a metre or two, where the balanced output will give a much better noise immunity, or in an intrinsically noisy situation, eg disco systems, where the lighting controller can interfere with the audio signal.

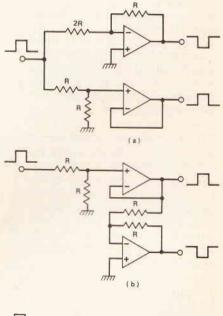
As far as the user is concerned, the only difference between balanced and unbalanced lines is that balanced ones use a three-wire connection per channel instead of the usual two. Balancing has been standard with professional audio equipment since the days of 2LO and the cat's whisker (and Angela Rippon?), where it is used to ensure reliable, humfree connections over long distances.

The basic principle is shown in Fig. 4; the signal is carried along two wires with the outer screen acting as an earth connection. The signal is inverted in one wire with respect to the other, but any hum and noise picked up from external signal sources by the cable will have the same phase in both wires. The balanced input accepts the differential signal, but rejects the externally introduced common mode signal. The normal method of balancing has traditionally relied upon the use of special input and output transformers, but similar results can be obtained by applying standard operational amplifier techniques - after all, the common op-amp has differential inputs.

Control Callibration	Channel Imbalance
2	1.87dB
4	3.78dB
6	5.79dB
8	7.96dB
10	10.39dB

Table 1 Balance control performance when used with tone control.

A balanced output consists of two outputs of identical levels but with one signal phase-inverted with respect to the other. Fig. 5 shows three ways that this could be achieved, and any one of these methods would be quite adequate provided it was connected to a balanced input. It may be seen that in each case, attenuation is introduced to ensure that half the input voltage appears at each output, but with opposite polarities. Thus a 1 volt input would result in outputs of +0.5 V and -0.5 V, giving the required 1 volt between conductors.



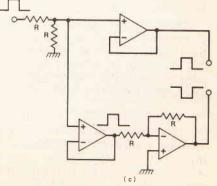


Fig. 5 Possible balanced output arrangements.

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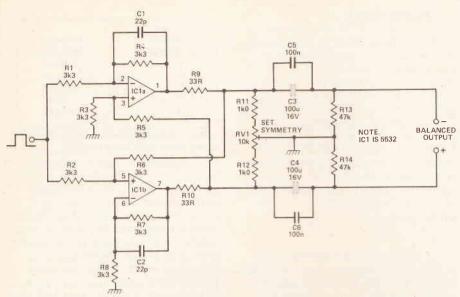


Fig. 6 Circuit diagram of the balanced output stage.

This is fine until the output is connected to an unbalanced input, when one of the balanced feeds gets shorted to earth, leaving a single output of 0.5 V. A difference of 6dB appears between balanced and unbalanced operation, which is not really acceptable. What is required is a method of increasing the gain of either output amplifier by 6dB whenever the other output is grounded, and such a circuit is illustrated in Fig. 6.

Here, the cross feed-back fixes the gain of each side at 0.5, but shorting either output to earth will remove this feedback, increasing the gain of the unshorted side to unity. As the balance condition of the circuit is extremely critical, the pre-set potentiomenter is used to set the two outputs equal with respect to earth.

The whole object of the balanced output is that it should be connected to a balanced input. As these are not common in domestic equipment, a suitable circuit is given in Fig. 7, which is similar to the line input stages common in professional studio equipment (alternatively, see ETI may 1983 — Editor). This stage should be included in any equipment that is driven by the balanced output of the preamplifier while placed a considerable distance from it active speakers and speakerlocated amplifiers being the obvious cases in domestic systems.

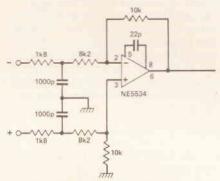


Fig. 7 A possible balanced input arrangement.

As shown in Fig. 1, the unbalanced output from the balanced line output stage is taken to the rear panel via the delay relay. This output will therefore be shorted to earth for about five seconds when power is first applied, and will also be cut off whenever a pair of headphones is plugged into the front panel-mounted jack socket.

Headphone Amplifier

Although most moving coil headphones have impedances in the 150 to 600 ohms range, the odd maverick pair are around that are as low as 8 ohms, so to be universal a headphone amplifier needs to be able to supply somewhat more current than a normal op-amp can manage. Various power ICs have been tried, but they all draw rather high quiescent current, causing the power supply regulators to get a bit too warm for comfort.

The circuit given in Fig. 8 uses an NE5534 to drive a pair of complementary transistors which are turned on by the voltage drop across R8. When the amplifier is in its quiescent state, the output stage is turned off, so minimum standing current is drawn. The transition point of the output devices does introduce some cross-over distortion, but this is kept within reasonable limits by negative feedback action, and the performance is more than adequate for headphone listening The output resistor, R11, may be changed to suit the type of headphones in use, possibly requiring an increase to about 200 ohms with some medium impedance models.

Constructional details, overlay diagrams, etc for these modules will be given next month along with further information on the mother board. We will also be giving details of a series of kits of the hard-to-find parts, but in the meantime PLEASE don't ring us — just try to hold out a little longer, OK?.

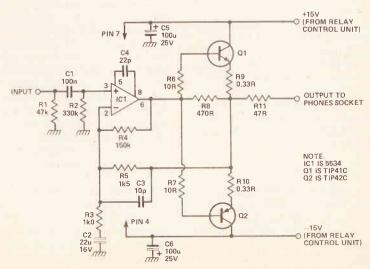


Fig. 8 Circuit diagram of the headphone amplifier module.

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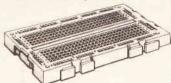
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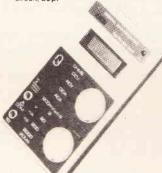
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UNIVERSAL EPROM PROGRAMMER Revisited

We really started something with our Universal EPROM Programmer in the August and September issues. Requests for the assembler listing and for advice on how to modify the program to run on other machines continue to pour in. In an attempt to stem the tide, Mike Bedford offers a few further thoughts and the listing itself.

s mentioned in the 2nd part of the Universal EPROM Programmer article, the software has been written in such a way as to make it compatible with all 6502 based computers with the absolute minimum of changes. However, it is inevitable that some slight modifications will be required when transferring software, however similar the two machines may be. A large proportion of the software package is written in BASIC which, being a high level languge, means that it should be possible to transfer it directly to another machine without any changes at all. This isn't quite the case as there are a number of dialects of BASIC, generally differing in those areas which are extensions to the original BASIC. Possible areas in which the BASIC program might need modifying have already been mentioned and it is now appropriate to indicate how the assembler subroutine may be modified to run on different machines.

Since all the keyboard and display I/O is carried out in the BASIC program hence camouflaging any hardware differences in these areas, the only changes which may be required to the assembler routine are due to differences in the memory maps and the clock speeds of the various machines. Apart from users wishing simply to transfer the software to another

machine, others may be interested in enhancing the package to carry out additional functions, for example, implementing the intelligent programming algorithm or adding new devices such as the 27256, 68732 and 68764 EPROMS which the hardware could support. It is therefore quite likely that a number of readers will require a much greater insight into the workings of the assembler routine than could be glimpsed from the hexadecimal dump given in the second part of the article. For this reason it is the intention here to reproduce a full assembler listing together with a simple "guided tour" to give some idea of how it works, hence enabling changes to be carried out without too much of the anguish often associated with trying to understand someone else's assembler program.

A few comments about the assembler are appropriate before going on to describe the structure of the program. Although all assemblers carry out essentially the same task there are often slight differences in the syntax. This program was written on a PDP-11 computer using a cross-assembler: a). The .PROCESSOR directive on line 13 is used to inform the assembler of which processor is in use. For 6502 only assemblers this line should be omitted.
b). The .ORG directive on line 14

sets the start address of the code.

Syntax on other assemblers may be \bigstar =IC00H or .=IC00H. c). This assembler uses a suffix of H to indicate a hexadecimal number. Some other assemblers use a prefix of \$. Ie IC00H may need replacing by \$IC00. d). In this assembler the .DEFINE directive is used to equate values to literals. In many other assemblers the word .DEFINE should be omitted to leave an equation (eg IC1PIA = OBC20H) and in others the EQU directive is used.

e). The .BYTE directive reserves a byte of memory and assigns an initial value to it. The more common version of this directive is DFB or DEFB.

The assembler syntax having been clarified, we can now go on to investigate the workings of the assembler subroutine and we shall make a start by looking at the parameter storage and data areas.

LOADR and HIADR are initialised by the BASIC program to one less than the first RAM address to be accessed. On exiting from the subroutine these locations will contain one more than the last address accessed. LOADE and HIADE are a similar address pair for the EPROM address. LOADF and HIADF are an address pair which are set by the BASIC program to one more than the last RAM address which should be used. RDATA is used to pass the

value of the data read from the EPROM back to the calling program, this being required in verify mode. MODE is set by the BASIC program to indicate whether read, verify, test or program function is required. Finally TYPE is set up by the main program to indicate the type of EPROM in use and will contain a number in the range 0 for 2758 to 8 for 27128.

As we now start to consider the data tables we shall be directing our attention to lines 47 to 64 of the program. In each of the seven lists here, there are 9 values of which one will be selected according to the value of TYPE. READS3 and READS6 contain the initial values of IC1CRB and IC2PIB respectively prior to which toggling bit 3 of IC2CRA would cause a read of the EPROM. PROGS5 and PROGS6 are similar tables of data for setting initial values of IC2CRA and IC2PIB prior to programming. PTBIT and PTBYTE indicate which bit of which PIA register requires to be toggled in order to carry out the programming of an EPROM. As a matter of interest, the reason that there are not tables of initial conditions for program and read for all PIA registers which connect to control pins on the EPROM is that some are set to the same initial value independently of EPROM type and some are set to the same value for both read and program. Finally A11A12 indicates whether the particular EPROM has A11 on pin 23 and A12 on Pin 2 or A11 on pin 20 and A12 on pin 23, these being the two options for the 27-series and 25-series devices.

Having described the parameter storage and data areas it should be relatively straightforward to see how the assembler routine works. The value of MODE is used to select one of the two main routines either READ for reading, verifying or testing or PROG for programming. In either of these two

Table 1 The assembler listing. Note that:-

- 1). All pound signs (\pounds) in this listing should be read as hash signs (#). It is purely a function of the printer used that these have been reproduced incorrectly.
- 2). The assembler listing refers to the two 6821 PIA's as IC1 and IC2 as was the case on the first prototype. IC1 should now be read as IC9 and IC2 as IC8. This in no way alters the operation of the software.

		{ *****	*****	*****	********
		** EPRON ** READ/ ** M. D. ** THIS ** AND W	A PROGRAM PROGRAMA BEDFORL ROUTINE FILL SUPP	MMER SUPPO ME ROUTINE) MARCH IS CALLED PORT 2758,	**************************************
		******	*****	*****	********
		1	.PROCESS		6500 COOH
		;ZERO PA	GE LOCAT	TIONS USED	
		1	.DEFINE		PLOAD=35H PHIAD=36H
		ADDRESS	SES OF 68	321 REGIST	ERS USED
		•	.DEFINE .DEFINE .DEFINE .DEFINE .DEFINE .DEFINE .DEFINE	I (I (I (I (I (CIPIA=OBC2OH CICRA=ICIPIA+1 CIPIB=ICIPIA+2 CICRB=ICIPIA+3 C2PIA=ICIPIA+4 C2CRA=ICIPIA+5 C2PIB=ICIPIA+6 C2CRB=ICIPIA+7
1000	4C4C1C	;	JMP	START	
1003 1004 1005 1006 1007 1008 1009 100A	00 00 00 00 00 00 00 00 00	LOADR: HIADR: LOADE: HIADE: LOADF: HIADF: HIADM: RDATA: MODE: TYPE:	BYTE BYTE BYTE BYTE BYTE BYTE BYTE BYTE	0 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	LO RAM START ADDRESS HI RAM START ADDRESS LO EPROM START ADDRESS HI EPROM START ADDRESS LO EPROM FINISH ADDRESS HI EPROM FINISH ADDRESS HI ADDRESS EPROM MASKED DATA READ FROM EPROM O-R,FFH-V,80H-T,2-P 0-2758 8-27128
1000		‡			
1COD 1C16	3C 18	READS3: READS6:	.BYTE	3CH, 3CH, 3 18H, 18H, J	CH, 3CH, 3CH, 3CH, 34H, 34H, 34H 8H, 10H, 10H, 18H, 12H, 10H, 12H
1C1F 1C28	3C 08				CH, 34H, 34H, 3CH, 3CH, 3CH, 3CH 5H, 8, 22H, 0, 22H
		BITS OF	F BYTES	TO TOGGLE	FOR PROGRAMME
1C31 1C3A	01 06	PTBIT: PTBYTE:	.BYTE	1,1,1,1,1	,8,2,8,2 ,5,6,5,6
		PIN POS	SN OF A1		* A11-PIN 23, A12-PIN 2 * A11-PIN 20, A12-PIN 23
1C43	01		.BYTE	1,1,1,1,1	
1C4C 1C4F 1C52 1C54 1C56	20 871 D ADOBIC C902 D003 4CBC1 C	START:	JSR LDA CMP BNE JMP	ZPSWAP MODE £2 READ PROG	*SWAP RAM ADDR/ ZERO PGE *PROGRAMME ? *NO - MUST BE READ ETC. *IF SO JUMP
		READING	G CODE		
1 C 5 9 1 C 5 B 1 C 5 E 1 C 6 0 1 C 6 3 1 C 6 5 1 C 6 B 1 C 6 B	A930 8D25BC A900 8D24BC A934 8D25BC AEOCIC BDODIC	READ:	LDA STA LDA STA LDA STA LDX LDX	£30H IC2CRA £0 IC2PIA £34H IC2CRA TYPE READS3, X	#CONFIGURE #IC2PIA #AS #INPUT #FOR #READ #DEVICE TYPE INDEX #SET
1C71 1C73 1C76 1C78 1C7B 1C7E 1C81 1C84 1C87	A 900 8D 20BC A 93C 8D 25BC BD 161C 8D 26BC 20 9C 1D 20 621D D003 4C 131D	CONTR:	LDA STA LDA STA LDA STA JSR JSR JSR BNE JMP	£0 IC1PIA £3CH IC2CRA READS6, X IC2PIB DELAY INCADD CONTR EXIT	# UP # INITIAL # CONDITIONS # FOR # READ # # INITIAL # CONDITIONS # FOR # READ # # INITIAL # INI
	1003 1004 1005 1006 1007 1008 1009 1000 1016 1016 1017 1016 1017 1028 1031 1031 1031 1034 1031 1034 1031 1031	1C03 00 1C04 00 1C05 00 1C06 00 1C07 00 1C08 00 1C0C 0	** ** ** ** ** ** ** *	**	**

PROJECT: EPROM Programmer

ALC:	1005	100500	-			
95 96	108F 1092	AD25BC		LDA	IC2CRA	SET SUITE
97	1092			EOR STA	£8	*CHIP ENABLE
98	1097			JSR	IC2CRA DELAY	\$LOW \$SHORT DELAY
99	I C9 A			LDA	IC2PIA	GET DATA FROM EPROM
100	1C9D	8DOA I C		STA	HDATA	AND STORE IT
101	1040	A200		LDX	£O	ZERO INDEX REGISTER
105	1CA2	ACOBIC		LDY	MODE	*READ, TEST OR VERIFY ?
103	1 CA5			BEQ	RR	*READ
104	1CA7	3007 C9FF		BMI	VV	*VERIFY
106	1CA9	FOBB		CMP BEQ	£OFFH	MUST BE VERIFY - FF ?
107	ICAD	4C13ID		JMP	LOOPR EXIT	FIF SO ROUND AGAIN FELSE NOT ERASED - EXIT
108	1CB0	C135	VV :	CMP		COMPARE WITH RAM
109	1 CB2	FOB4		BEQ	LOOPR	IF OK LOOP
110	1CB4			JMP	EXIT	FELSE BAD EPROM-EXIT
111	1 CB7	81 35	RR =	STA	(ZPLOAD,X)	STORE DATA IN RAM
112	1CB9	4C681C		JMP	LOOPR	FROUND AGAIN
113			* UDOCD	AMMING CO	D.F.	
115			I HOOK	IMMINO CO	DE	_
116	1 CBC	A 930	PROG:	LDA	£30H	*CONFIGURE
117	1 CBE	8D25BC		STA	IC2CRA	IC2PIA
118	1 CC I	A 9FF		LDA	£OFFH	# AS
119	1 003	8D24BC		STA	IC2PIA	#OUTPUT
120	1 006	A 934		LDA	£34H	*FOR
121	1 CC8	8D25BC AEOC1C	LOOPP:	STA LDX	IC2CRA	* PROGRA MME
123	LCCE	BDUDIC	LOOFF*	LDA	TYPE READS3,X	FEPROM TYPE
124	ICD1	8D23BC		STA	ICICRB	*UP
125	1 CD4	A900		LDA	£O	INITIAL
126	ICD6	8D20BC		STA	ICIPIA	CONDITIONS
127	I CD9	BD1F1C		LDA	PROGS5,X	#FOR
128	1 CDC	8D25BC		STA	IC2CRA	FPROGRAMME
129	1 CDF	BD281C		LDA	PROGS6,X	1
130	1 CE2	8D26HC 209CID		STA	ICZPIB	-CHOPT DELLY
132	1CE3	20621D		JSR JSR	DELAY INCADD	ISHORT DELAY
133	1 CEB	F026		BEQ	EXIT	*NEXT RAM/EPROM ADDRESS *IF LAST THEN EXIT
134	ICED	2017ID		JSR	SETADD	PUT ADDRESS ON PINS
1 35	1CF0	A200		LDX	£O	IZERO INDEX REGISTER
136	ICF2	A 1 35		LDA	(ZPLOAD, X)	*GET DATA FROM RAM
137	1 CF 4	8D24BC		STA	IC2PIA	PUT DATA ON PINS
138	ICF7	A EOCIC		LDX	TYPE	1EPROM TYPE
140	I CF A	BC3A1C B920BC		LDY	PTBYTE,X	BYTE TO TOGGLE
141	1000	5D311C		LDA EOR	ICIPIA, Y PTBIT, X	*LOAD IT
142	1003	9920BC		STA	ICIPIA, Y	*PUT IT BACK AGAIN
143	1 DU6	AOID		LDY	£IDH	CARRY
144	1008	AZFF		LDX	£OFFH	FOUT
145	IDOA	CA	DEL:	DEX		150 MS
146	1 DOB	DOFD		BNE	DEL	IDELAY
147	1 DOD	88		DEY		1FOR
148	IDIO	DOFA		BNE	DEL	*PROGRAMME
150	1010	4CCB1C	;	JMP	LOOPP	ROUND AGAIN
151	IDI3	20871D	EXIT:	JSR	ZPSWAP	SWAP BACK ZERO PAGE
152	1D16	60		RTS		LEXIT BACK TO BASIC
153			ŧ			
154						
155			# ROUTIN	E TO PUT	ADDRESS ON	APPROPRIATE EPROM PINS
156 157	ID17	ADOSTO	CETADD.	I DA	LOADE	THE THE COLUMN TWO IS NOT THE COLUMN TWO IS
158	IDIA	AD051C 8D22BC	SETADD:	STA	LOADE	WRITE LOW ORDER BYTE
159	IDID	BD431C		LDA		STRAIGHT TO EPROM
160	1020	F009		BEQ	ADD25	\$25 OR 27 SERIES ? \$BRANCH IF 25-SERIES
151	1022	ADU61C		LDA	HIADE	GET HI ORDER BYTE
162	1D25	8D20BC		STA	ICIPIA	WRITE STRAIGHT TO EPROM
= 1 ()				JMP		JUMP TO AI3 CODE
163	1D28	4C521D	11:00			
164	1D28 1D2B	4C521D AD20BC	ALID251	LDA	ICIPIA	#GET ICIPIA
164 165	1028 1028 1028	4C521D AD20BC OD091C	ALID25:	LDA ORA	IC1PIA HIADM	OR IN MASKED HI BYTE
164 165 166	1D28 1D28 1D25 1D31	4C521D AD20BC UD091C 8D20BC	ALID25#	LDA ORA STA	ICTPIA HIADM ICTPIA	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN
164 165	1028 1028 1028	4C521D AD20BC OD091C	ALID25#	LDA ORA STA LDA	ICIPIA HIADM ICIPIA HIADE	OR IN MASKED HI BYTE PUT IT BACK AGAIN GET HI ORDER BYTE
164 165 166 167 163	1028 1028 1025 1031 1034	4C521D AD20BC OD091C 8D20BC AD061C	ADD25:	LDA ORA STA	ICTPIA HIADM ICTPIA HIADE £10H	OR IN MASKED HI BYTE FPUT IT BACK AGAIN GET HI ORDER BYTE TEST AI2
164 165 166 167 163 169	1 D 2 8 1 D 2 B 1 D 2 E 1 D 3 1 1 D 3 4 1 D 3 7 1 D 3 9 1 D 3 B	4C521D AD20BC OD091C 8D20BC AD061C 2910 F008 AD20BC	ALID25#	DA ORA STA LDA AND BEQ LDA	ICTPIA HIADM ICTPIA HIADE £10H ADDII	OR IN MASKED HI BYTE PUT IT BACK AGAIN GET HI ORDER BYTE
164 165 166 167 163 169 170	1 D 2 8 1 D 2 B 1 D 2 E 1 D 3 1 1 D 3 4 1 D 3 7 1 D 3 9 1 D 3 B 1 D 3 E	4C521D AD20BC 0D091C 8D20BC AD061C 2910 F008 AD20BC 0908	ALID251	DA ORA STA LDA AND BEQ LDA ORA	ICIPIA HIADM ICIPIA HIADE £10H ADDII ICIPIA £8H	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN FOET HI ORDER BYTE FIEST AI2 FIF UNSET GO TO AIL CODE
164 165 166 167 163 169 170 71	1 D28 1 D2B 1 D2E 1 D31 1 D34 1 D37 1 D39 1 D38 1 D3E 1 D40	4C521D AD20BC 0D091C 8D20BC AD061C 2910 F008 AD20BC 0908 8D20BC		DA ORA STA LDA AND BEQ LDA ORA STA	ICIPIA HIADM ICIPIA HIADE £10H ADDII ICIPIA £8H ICIPIA	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN FGET HI ORDER BYTE FTEST AI2 FIF UNSET GO TO AIL CODE FAIL IS SET - GET ICIPIA FOR IN AIL FAND PUT IT BACK AGAIN
164 165 166 167 163 169 170 171 172	1 D 2 8 1 D 2 B 1 D 2 E 1 D 3 1 1 D 3 4 1 D 3 7 1 D 3 9 1 D 3 B 1 D 3 E 1 D 4 0 1 D 4 3	4C521D AD20BC OD091C BD20BC AD061C 2910 F008 AD20BC O908 BD20BC AD061C	ADD11:	LDA ORA STA LDA AND BEQ LDA ORA STA LDA	ICIPIA HIADM ICIPIA HIADE LIOH ADDII ICIPIA LSH HIADE HIADE HIADE	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN FOET HI ORDER BYTE FIEST A 12 FIF UNSET GO TO A 11 CODE FAIZ IS SET - GET ICIPIA FOR IN A 12 FAND PUT IT BACK AGAIN FOET HI ORDER BYTE
164 165 166 167 163 169 170 171 172 173	1 D 2 8 1 D 2 B 1 D 2 E 1 D 3 1 1 D 3 4 1 D 3 7 1 D 3 9 1 D 3 B 1 D 3 E 1 D 4 0 1 D 4 3 1 D 4 6	4C521D AD20BC OD091C BD20BC AD061C 2910 F008 AD20BC 0908 BD20BC 0908 BD20BC AD061C 2908		LDA ORA STA LDA AND BEQ LDA ORA STA LDA AND	ICIPIA HIADM ICIPIA HIADE £10H ADDII ICIPIA £8H ICIPIA HIADE £8H	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN FOET HI ORDER BYTE FITEST AIZ FIF UNSET GO TO AIL CODE FAIZ IS SET - GET ICIPIA FOR IN AIZ FAND PUT IT BACK AGAIN FOET HI ORDER BYTE FITEST AIL
164 165 166 167 163 169 170 171 172 173	1D28 1D2B 1D2E 1D31 1D34 1D37 1D39 1D38 1D3E 1D40 1D43 1D46 1D48	4C521D AD20BC OD091C 3D20BC AD061C 2910 F008 AD20BC 0908 BD20BC AD061C 2908 F008		LDA ORA STA LDA AND BEQ LDA ORA STA LDA AND BEQ BEQ BEQ	ICIPIA HIADM ICIPIA HIADE £10H ADDII ICIPIA £8H HIADE £8H ADDI 3	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN FOST HI ORDER BYTE FIEST AI2 FIF UNSET GO TO AIT CODE FAIL IS SET - GET ICIPIA FOR IN AIZ FAND PUT IT BACK AGAIN FOST HI ORDER BYTE FIEST AII FIF UNSET GO TO AIS CODE
164 165 166 167 163 169 170 171 172 173 174 175	1 D 2 8 1 D 2 B 1 D 2 E 1 D 3 1 1 D 3 4 1 D 3 7 1 D 3 9 1 D 3 B 1 D 3 E 1 D 4 0 1 D 4 3 1 D 4 6	4C521D AD20BC OD091C BD20BC AD061C 2910 F008 AD20BC 0908 BD20BC 0908 BD20BC AD061C 2908		LDA ORA STA LDA AND BEQ LDA ORA STA LDA AND	ICIPIA HIADM ICIPIA HIADE £IOH ADDII ICIPIA £8H ICIPIA HIADE £8H ADDI3 IC2PIB	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN FGET HI ORDER BYTE FTEST AI2 FIF UNSET GO TO AIL CODE FAIL IS SET - GET ICIPIA FOR IN AIL FOR HI ORDER BYTE FTEST AIL FIF UNSET GO TO AIL CODE FAIL IS SET - GET ICIPIA FOR IN AIL
164 165 166 167 163 169 171 172 173 174 175 176	1D28 1D2B 1D2E 1D31 1D34 1D37 1D39 1D3B 1D3E 1D40 1D43 1D43 1D46 1D48 1D4A	4C521D AD20BC 0D091C 8D20BC AD061C 2910 F008 AD20BC 0908 8D20BC AD061C 2908 F008 AD26BC		LDA ORA STA LDA AND BEQ LDA STA LDA AND BEQ LDA AND LDA AND BEQ LDA	ICIPIA HIADM ICIPIA HIADE LIOH ADDII ICIPIA LSH ICIPIA HIADE LSH ADDI 3 IC2PIB LH	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN FOET HI ORDER BYTE FIEST A 12 FIF UNSET GO TO A 11 CODE FAILZ IS SET - GET ICIPIA FOR IN A 12 FAND PUT IT BACK AGAIN FOET HI ORDER BYTE FIFT UNSET GO TO A 13 CODE FAIL IS SET - GET IC2PIB FOR IN A 11
164 165 166 167 163 169 170 171 172 173 174 175 176 177	1028 1028 1028 1031 1034 1037 1038 1038 1040 1043 1046 1048 1044 1044 1044 1045	4C521D AD20BC OD091C 3D20BC AD061C 2910 F008 AD20BC 0908 BD20BC AD061C 2908 F008 AD26BC 0901 BD26BC AD061C		LDA ORA STA LDA AND BEQ LDA ORA STA LDA AND BEQ LDA ORA STA LDA ORA LDA ORA AND BEQ LDA ORA LDA ORA AND LDA ORA AND LDA LDA ORA AND LDA LDA ORA LDA	ICIPIA HIADM ICIPIA HIADE £10H ADDII ICIPIA £8H ICIPIA HIADE £8H ADDI3 IC2PIB £1H IC2PIB	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN FGET HI ORDER BYTE FTEST AI2 FIF UNSET GO TO AIL CODE FAIL IS SET - GET ICIPIA FOR IN AIL FOR HI ORDER BYTE FTEST AIL FIF UNSET GO TO AIL CODE FAIL IS SET - GET ICIPIA FOR IN AIL
164 165 166 167 163 169 170 171 172 173 174 175 176 177 178	1028 1028 1028 1031 1034 1037 1038 1038 1046 1043 1046 1048 1044 1045 1045 1055	4C521D AD20BC 0D091C BD20BC AD061C 2910 F008 AD20BC 0908 BD20BC AD061C 2908 F008 AD26BC 0901 BD26BC 0901 BD26BC 0901 BD26BC 2908	ADD11:	LDA ORA STA LDA AND SEQ LDA AND STA LDA AND ORA STA LDA AND ORA STA LDA AND AND	ICIPIA HIADM ICIPIA HIADE £10H ADDII ICIPIA £8H ICIPIA HIADE £8H ADDI 3 IC2PIB £1H IC2PIB £1H IC2PIB	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN FGET HI ORDER BYTE FIEST A 12 FIF UNSET GO TO A 11 CODE FAIL IS SET - GET ICIPIA FOR IN A 12 FAND PUT IT BACK AGAIN FGET HI ORDER BYTE FIF UNSET GO TO A 13 CODE FAIL IS SET - GET ICIPIB FOR IN A 11 FPUT IT BACK AGAIN FGET HI ORDER BYTE FOR IN A 11 FPUT IT BACK AGAIN FGET HI ORDER BYTE FEST A 13
164 165 166 167 163 170 171 172 173 174 175 176 177 178	1028 1028 1028 1031 1034 1037 1038 1038 1046 1044 1044 1044 1044 1045 1055 1055	4C521D AD20BC OD091C BD20BC AD061C 2910 F008 AD20BC 0908 BD20BC AD061C 2908 F008 AD26BC 0901 BD26BC AD061C 2909 F008	ADD11:	LDA ORA STA LDA AND BEO ORA STA LDA AND BEQ LDA ORA STA LDA AND BEQ LDA AND BEQ AND BEQ AND BEQ	ICIPIA HIADM ICIPIA HIADE £10H ADDII ICIPIA E8H ICIPIA HIADE £8H ADDI3 IC2PIB £1H IC2PIB HIADE £20H ADDEXT	FOR IN MASKED HI BYTE FPUT IT BACK AGAIN FOET HI ORDER BYTE FIEST AIZ FIF UNSET GO TO AII CODE FAIZ IS SET - GET ICIPIA FOR IN AIZ FAND PUT IT BACK AGAIN FOET HI ORDER BYTE FIEST AII FOR IN AII FOET HI ORDER BYTE FOR IN AII FOR IN
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routines the initial conditions are set up and a loop is executed for each address to be read or programmed. Each time round the loop the appropriate PIA bit is toggled to carry out the required function to the EPROM. In the case of testing the read data is compared with FF (the expected value for an erased EPROM) and in verifying the read data is compared with data in RAM. In either of these two modes, if the test fails the subroutine exits and this is detected in the BASIC program by the fact that the address returned in LOADR and HIADR is less than the expected final RAM address.

The general overview being complete, a few specific points on the tailoring of the assembler routine to suit other machines will

now be covered.

a). The origin of the routine should be selected so as not to conflict with the area of RAM used by the BASIC program and the area to be used for data storage (as selected by the BASE command). The origin is set on line 14.

b). The address of the EPROM programmer hardware as selected by the on board links should be equated to IC1PIA on line 23. It should be noted that the addresses in a). and b). must agree with the addresses of the M/C code routine and hardware as assigned in the

BASIC program.
c). Lines 143 to 148 are a couple of nested loops which implement the 50ms pulse required for programming EPROMs. These loops will only generate a 50ms delay when running on a processor with a 750 kHz clock such as the Tangerine Microtan. For different clock frequencies the value of 1D loaded into register Y on line 143 would require to be changed proportionally. For example, if the subroutine were to be run on a machine with a 1MHz clock a

value of 1D (hex) \pm 1000/750 =

27 (hex) should be used.

As a final point, although the assembler routine has been written for a 6502 processor and as such will not run on any other processor, the hardware is compatible with the increasing number of computers using the 6809 processor. For this reason, some owners of 6809 based machines may like to try their hand at converting this routine to 6809 code. Although, it wouldn't result in the most efficient 6809 code, the easiest way to do this would be to translate it virtually on an instruc-

.PROJECT : EPROM Programmer

tion by instruction basis, a task which shouldn't be beyond the capabilities of those with a moderate knowledge of 6809 program-

The following list contains all those errors which have come to light since the project was published.

On the circuit diagram (page 46, August 1983), C6 is 100μ and C9 is 100n, not the other way round as given. Some bars were omitted from note three of Table 1 on page 48: it should have read "CE/PGM (27 series) is equivalent to PD/PGM (not PD/ PGM) (25 series)." The penultimate sentence of the first paragraph on page 50 should read "... adjust RV1 for a potential of +25 V at IC10 output." On the overlay, IC7 is between SK2 and SK1, IC6 is beteen SK1 and C10, IC11 is between R7 and R10, R3 is between R2 and Q2, and Q7 is between Q6 and Q8. A link is missing between IC7 and SK1, and the unidentified pins at the right hand end of SK3 are the +5V line. Finally, C10 appears twice in the parts list but only the first entry is correct, and the second DIL socket should of course, be 8, not 80, way.

Table 1 continued (see notes overleaf).

189 190 191			D A12 MASKED OUT LAST ADDRESS DONE
192 1D62 E6 193 1D64 D0	INCADD: INC DO2 BNE BNE INC	INCROM :	LO ORDER RAM ADDRESS SKIP IF NO CARRY ELSE INC HI RAM ADD
196 ID6B D0 197 ID6D EE	1051C INCROM: INC 1003 BNE 10061C INC	LOADE : INCEXT : HIADE ;	LO ORDER EPROM ADDRESS SKIP IF NO CARRY ELSE IN HI EPROM ADD
199 1D73 29 200 1D75 8D	0061C INCEXT: LDA PE7 AND 0091C STA 0051C LDA	£OE7H ;	GET HI ORDER EPROM MASK OUT All, Al2 STORE IT
202 ID78 CD 203 ID7E DO	0071C CMP 006 BNE 0061C LDA	LOADF :	GET LO EPROM ADDRESS LAST ADDDRESS ? IF NOT EXIT ELSE TEST HI ORDER
205 1D83 CD 206 1D86 60 207	OO81C CMP INCRTS: RTS	HIADF :	LAST ADDRESS ? RETURN
208 209 210 211	THIS ROUTIN	E SWAPS ZPLOAD W WITH HIADR	ITH LOADR
212 ID87 A6 213 ID89 A4 214 ID8B AD	ZPSWAP* LDX 436 LDY 0031C LDA	ZPHIAD #	GET LO ZERO PAGE AND HI ZERO PAGE GET LO RAM
216 1D90 AD 217 1D93 85	535 STA 0041C LDA 536 STA	HIADR : ZPHIAD :	WRITE TO LO ZERO PAGE GET HI RAM WRITE TO HI ZERO PAGE
	E031C STX C041C STY RTS	HIADR ;	ZERO PAGE TO LO RAM ZERO PAGE TO HI RAM RETURN
222 223 224			CAPACITOR SLOWING
227 ID9E 88		1	LOOP COUNTER DECREMENT
228 1D9F D0 229 1D41 60 230 231			LOOP IF NOT ZERO RETURN ETI

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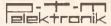
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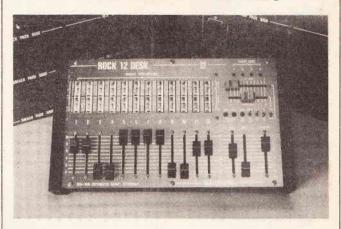




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BOOK REVIEWS

So you thought we couldn't read? Just to prove you wrong, the ETI staff has been ploughing through some of the new works in the field — here's what we think of them.

Understanding Digital Logic Circuits

R.G. Middleton Prentice/Hall International 392 pages/£16.10

According to the preface, this book is aimed at those who are currently working in some area of electronics but who are not familiar with digital techniques. It assumes little or no prior knowledge either of the technology or the maths behind it and covers everything from the simplest of gates through to counters, converters, memories and the

more complex devices now in use.

One of the first things one notices on reading through the book is that it is American, and that the illustrative examples used are therefore American also. Instead of the 74 series TTL and 4000 series CMOS familiar to British engineers, the notes and pin-out diagrams refer, with a few exceptions, to the Fairchild 93, 96, and 9N ranges, none of which are very well known in this country. Whilst this may not be a serious shortcoming it must, I feel, reduce the book's value and appeal to those at whom it is ostensibly aimed, that is, beginners in the field of digital electronics.

Another slight annoyance I found was the poor positioning of related text and illustration. This varied throughout the book, but in the worst instances as much as seven pages separated a section of text from the illustration to which it referred. In those places where a passage in the text referred to more than one illustration at a time, I very soon ran out of fingers! Whilst this, too, is perhaps a minor point it does make certain sections far more daunting than they need be, and again might well prove discouraging to those unfamiliar with the material.

On a more positive note, the book covers its ground very

thoroughly indeed and has a suitably authoritative feel to it. There would be few, I suspect, who could read through it without learning something of value. I am not at all convinced that it is the best introduction for those new to digital electronics, but it is an excellent reference book for those, like me, who learnt only analogue techniques during their periods of formal study and who have picked up digital theory piecemeal along the way. The index, if not exhaustive, is certainly adequate, and after a week or two I found myself turning to it automatically whenever something on the bench posed a question of a digital nature.

Microprocessor Technology David. L. Terrell Prentice/Hall International 562 pages/£20.65

This is a fairly readable delve into the inner mysteries of the Z80 microprocessor chip and some of its more common support devices. This book covers both hardware and software aspects of actually using a microprocessor chip, providing numerous ex-amples of each and it even contains a circuit diagram for a basic

trainer unit.

On the software side, the book covers not only the Z80 instruction set in reasonable details but proceeds to show how to accomplish some of the more common tasks required of simple computer and control systems. This is backed up on the hardware side by basic interface circuitry and illustrations of how to drive them.

The Z80 processor which is the basis of the book is one of the more complex 8-bit devices generally available. This means

that while most of the concepts covered in the book are applicable to other devices, it must be remembered that approaches may be required when realising systems using them.

Some knowledge of electronics and logic would be an advantage when reading the book as would access to some sort of small computer system and possibly someone with whom to discuss points

of interest.

PIW

The Micro Cookbook **Don Lancaster** Prentice/Hall International

384 pages/£13.55 Don Lancaster's Cookbook series has developed a good reputation for handling complex technical information in a down-to-earth practical way. In my experience, the most widely known is the CMOS cookbook, and this has graced many a lab bookshelf that I've known. So, the Micro Cookbook has a lot to live up to - but I'm afraid that it's blown it.

The first disappointment is that, as you may have already noticed, this is just volume 1 - volume 2, with programming (machine code, of course), I/O, advanced techniques (no, they didn't say what that meant), and some detailed examples, is still on the rollers. The first volume is just

the introduction!

Even so, it hasn't made up it's mind who it's for. The others of the Cookbooks have all assumed that the reader has a firm grasp of the fundamentals but not necessarially the details. This Cookbook seems to be aimed at the idot savant played by Richard Prior in 'Superman III' - one moment it's insulting your intelligence with some of the most crass technical writing I've come across (for example, one, of the exercises given to readers is "Show the Exclusive-Or logic involved in having two girl-friends"), the next it's assuming you know far more about microprocessors than it has bothered to explain to you.

This is not to say that the Cookbook has nothing to offer, there is a great deal that's useful, even entertaining in it, and it can be very difficult to put down. However, all this good is burried

and difficult to find.

So, I'm afraid, a disappointment, which is a real pity, because I'm sure that done properly, this book could have been at least as useful as others in the series. Let's hope that volume 2 is an improvement.

DIB

The Ground Launched Cruise Missile: A Technical Assessment Tim Williams

Electronics For Peace
36 pages/75p (£1 inc postage)
Before getting too far into this review,

a couple of confessions are in order. First of all, electronics for peace is 'a network... to link those working in electronics and computing who share a concern for the military implications of their profession.' Thus it is not a group that one would expect to be that well disposed towards cruise missiles in the first place, secondly, your reviewer is not that well disposed towards cruise missiles, either.

Confessions over, this book is reviewed here because it presents hard information in a subject area normally noteable for the domination of opinion. Not that the author has been lent a GLCM to put through its paces; most of the technical details of the missile system are well-guarded secrets. However, using a very wide range of sources, the author has been able to build up a disquieting picture of the goings on in the GLCM programme.

For instance, it is possible to infer that the reliability of GLCMs is lower than that of other American strategic nuclear weapons becuase there is no independent contractor whose only responsibility is to ensure reliability — contrary to practice in

all other strategic weapon programmes.

The booklet catalogues likely technical problems, amongst which is that GLCMs use a very large number of advanced VLSI devices. Very few such devices have yet been approved to military specifications; also, there seems to be a problem in adequately sealing the chip encapsulation.

Another major problem area dealt with is the software. The software contractor is known to have run into difficulties — however, this is far from surprising, as a recent survey of US government software contracts found that only 1.7% of software could be used as delivered.

Whether you are for or against nuclear weapons in general or the stationing of GLCMs in this country in particular, or even if you simply have not made up your mind, this booklet raises questions that demand an answer. It is available from Electronics for Peace, 151 Courthouse Road, Maidenhead, Berks SL6 6HY.

Ian Pitt; DJB — Dave Bradshaw.

Reviewers: PIW — Phil Walker: IIP —

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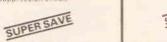
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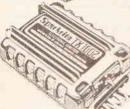


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C-MOS circuity
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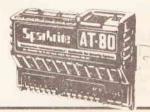


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IC UPDATE

This month, an IC for the enthusiast who has everything, including a generous overdraft facility: digital to analogue converter for colour video. Certainly, it's state-of-art; equally certainly, it's expensive.

his hybrid digital to analog converter provides three channels of video output for RGB type video displays with picture element (pixel) rates to 40MHz. The RGB DAC contains three video DACs and three RAM arrays (16 x 4) as well as all control inputs required to generate output waveforms which are compatible with EIA standards RS-170 and RS-343 (see

Fig. 1).

The RGB DAC 4T provides four bits of resolution or 16 levels of "gray scale" per color. This gives the user a (2⁴)³ or 4096 color palette. The 16 x 4 ram array per colour allows the user a choice of any 16 of the 4096 colours for each sweep. The write speed is also high enough to allow the colour map to be updated during the vertical retrace or even horizontal retrace in some systems. The high update rates and the ability to generate a full 1 volt composite video output across a 75 ohm load makes this DAC ideally suited for colour computer graphics using raster scan technology.

FEATURES

- 4096-colour palette
- Three video DACs
- Update rates to 40 MHz
- Complete composite video capability
 - 16 by 4 bit colour map RAM
- TTL compatible
- Direct 75 ohm RGB outputs
- Clean glitch-free output
 Single +5V supply

ADDRESS DATA-RED VIDEO BLANK GREEN SYNC GREEN VIDEO OUT VIDEO CS GREEN BLUE VIDEO CS BLUE STROBE

Fig. 1 Block diagram. Fig. 2 RGB DAC 4TD connections.

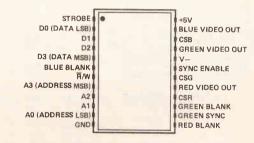


Fig. 2 RGB DAC 4TD connections.

PIN DESCRIPTIONS

STROBE

The transition from Logic 1 to Logic 0 transfers data from RAM outputs to the data register outputs. The strobe is not used for write operations.

GREEN SYNC (composite sync)

A logic 1 sets the registers to all 0s (ref black) and drives the green output to a level 286mV more negative than the reference black level. This signal has priority over blanking and data inputs from the RAMs and is used to synchronize the beam traces in a raster scan

BLANKING (Red, Grn, Blu)

A logic 1 sets the registers to all 0s (ref black) and drives the output to a level 50mV more negative than the reference black level. This signal has priority over the data inputs from the RAMs and is used to shut off the beam for the darkest display possible.

SYNC ENABLE

This input should be connected to +5V to enable the sync signal feature of the green output. If this feature is not desired this input should be connected to ground.

This input should be connected to a stable -3 to -15 volt supply to restore the green output blanking level to 0V absolute if the sync enable is connected to +5V. If it is not necessary to restore the green output blanking level to 0V or if sync enable is grounded this pin should be grounded.

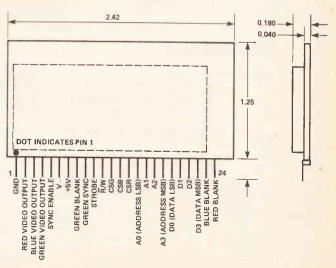


Fig. 3 RGB DAC 4T connections.

FEATURE : IC Update

ADDRESS — 4 Bits — A0, A1, A2, A3.
Determines read or write address for all RAM arrays. These inputs are used as an address input to load arrays in the write mode and as data inputs during the read (display) mode.

DATA — 4 Bits — D0, D1, D2, D3 Used to load data to all RAM arrays — data loaded will be non-inverted to the DAC during read mode.

Logic 0 selects read operation Logic 1 selects write operation

All data to DAC registers will be logic 1 during write mode. If no strobe signal is applied during write operations, the DAC outputs will retain the last read operation level. Otherwise the outputs will rise to REF WHITE level unless composite sync (green output) or blanking signal is applied.

CSR, CSG, CSB

Chip select for each channel (red, green, or blue) A logic 0 selects RAM channel for read or write operations and a 1 deselects RAM for any operation. If deselected, the data to the DAC registers will be logic 1. If no strobe signal is applied while the RAM is deselected, DAC outputs will retain the last read operation level. Otherwise the output will rise to REF WHITE level unless composite sync (green output) or blanking signal is applied. Normally only one input is enabled (logic 0) to write data to its corresponding RAM and all inputs are enabled (logic 0) to read data during display.

SPECIFICATIONS (Typical @ +25°C, +5V and 75 load unless otherwise stated).

BESOLUTION	PARAMETER	UNITS
RESOLUTION	4	bits
PALETTE	4096	colours
	(16 colours per sweep)	
ANALOG OUTPUTS (each o	channel)	
Voltage range (1%)	0 to 0.6	volts
Current (75 ohm load)	-17	mA
Impedence (± 5%)	75	ohms
Compliance	±2	volts
OUTPUT — COMPOSITE S'	YNC	
Green Only	-286	mV (± 5%)
(Referred to Blanking Level)		, , , , ,
OUTPUT — COMPOSITE B	LANKING	
(Referred to Black Level)	-50	mV (± 5%)
ACCURACY (each channel)		
Absolute	±1/ ₂	LSB
Linearity	$\pm \frac{1}{2}$	LSB
Offset	10	mV
Offset	100	ppm/°C
Gain Tempco	500	ppm/°C
Linearity Tempco	250	ppm/°C
DYNAMIC CHARACTERISTI	CS (each DAC)	
Settling Time (to 1 LSB)	5	nS
Update Rate	42	MHz
Rise Time	3	nS
Slew Rate	200	V/us
Glitch Energy	50	pV-S
DATA & ADDRESS INPUTS		
Compatibility	TTL	
Coding	BIN	
CONTROL INPUTS	Biii	
STROBE		
Compatibility	ΠL	
Set-up Time	25	nS
Hold Time	0	nS
Propagation	12	nS
COMPOSITE BLANKING SY	· -	113
Compatibility	TTL	
	20	nS
Settling Time	20	113
POWER REQUIREMENTS	1454.1551	1.
Voltage	+4.5 to +5.5V	volts
Current	480	mA
TEMPERATURE RANGE		
(ambient)	0 to 70	degrees C

NOTES:

1. Time from stable "Read Address" to Strobe Hi to Lo Transition

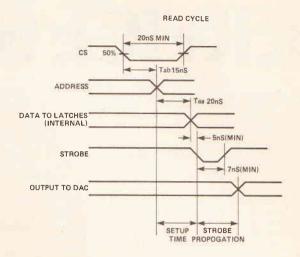


Fig. 4 Read cycle timing diagram.

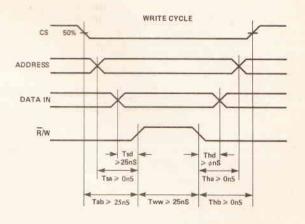


Fig. 5 Write cycle timing diagram.

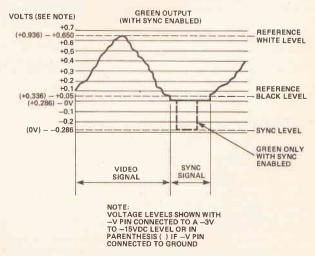


Fig. 6 Green composite video output; red and blue do not have the sync signal but are otherwise similar.

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We are always looking for new contributors to the magazine, and we pay a competitive page rate. If you have built a project or you would like to write a feature on a topic that would in-terest ETI readers, let us have a description of your proposal, and we'll get back to you to say whether or not we're interested and give you all the boring details. (Don't forget to give us your telehone number).

We don't bother with the bureaucracy for Tech Tips — all you do is to send in your idea, stating clearly if you want an acknowledgement of receipt. If possible, please *type* your explanation of why the circuit is different, what it does and how it works, on a separate sheet from the circuit diagram; both sheets should carry your name, address and the circuit title. We'll let you know (within a month or so) if we want to use your Tech Tip.

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OOPS!

We have in the past published small corrections to projects on the letters page, and major corrections separately. From now on correc-tions will appear on this page, and will be repeated for several months (just to increase our embarrassment). If a correction is too large to fit on here, we will publish it just once, but will note the fact that a correction does exist, and that copies of it can be obtained from us provided you send in an SAE. But please — request copies only if you really do need them; if this service is abused, we may be forced to withdraw it.

Programmable Power Supply (January 1983) Lascar Electronics have now moved to Module House, White Parish, Salisbury, Wiltshire SP5 2SJ.

Flash Sequencer (July '83) Q1 should be BC184L; Q2-5 should be BC182L.

Telescope (August 1983)

We had a shower of annotation falling off our diagrams! On Fig. 1, C19 (below IC14) was not labelled nor was Q2 (above R11), and there were two C23s — one should be IC22 and it. doesn't matter which. In Fig. 5, IC12 was not labelled. Unfortunately, there was a mistake in the correction (blush!): C14 is the 22μ tant on the -5 V line.

Graphic Equaliser (August 1983)

D2 and D3 are shown the wrong way round in the power supply circuit diagram on page

Universal EPROM Programmer (August 1983)

Corrections to this project are listed in the article "Universal EPROM Programmer Revisited" which appears on page 61.

Z80 Controller Computer (August 1983)

On the overlay, SWT is the rectangle beside ICs 5 and 6, C6 should be shown between ICs 3 and 7, and a link through has been missed — to the right of pin 18, IC11

Typewriter Interface (October 1983)
There are two errors in Table 1 on page 24: location 3C should contain E7 and location 3F should contain 5F.

Car Alarm (October 1983)

In the semiconductors section of the parts list, Q1, 2, 5, and 7 should be BC212L, Q3 should be BC182L, and Q4, 6 should be TIP31 or BD131. There was also another (inconsequential) silly but we bet you've already spotted that one!

Tech Tips (October 1983)

Ramped Pulse Generator For Stepper Motors
— pin 1 of IC2 should be grounded, the
Ramp Up and Ramp Down inputs accept negative, not positive, going pulses, and IC7 should be a 4011 rather than a 4001.

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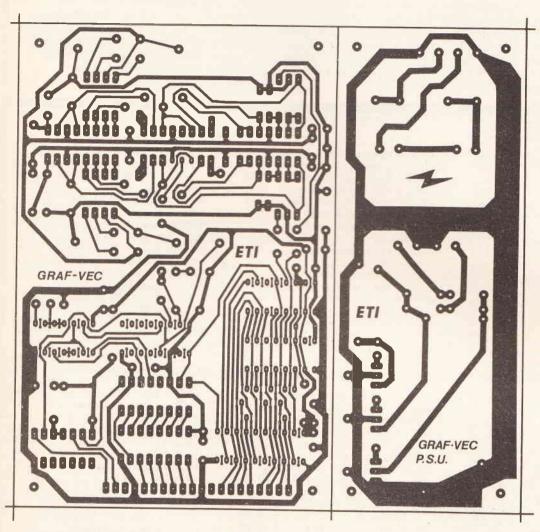
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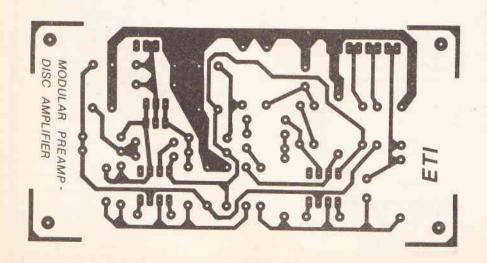
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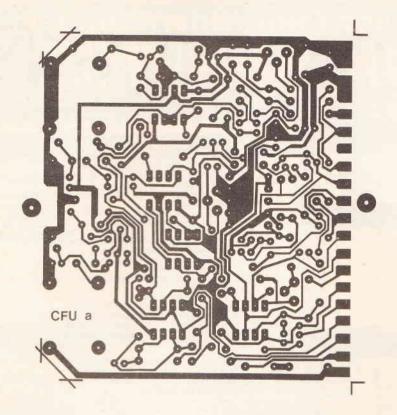
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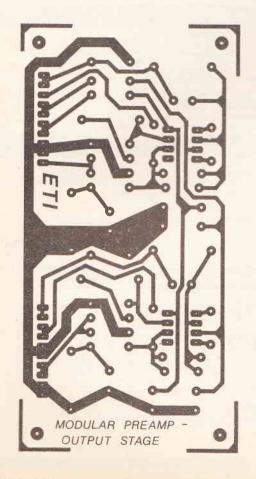
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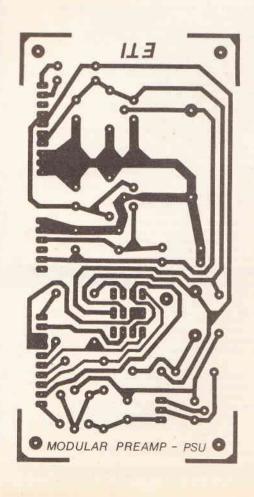


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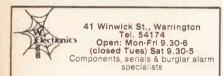
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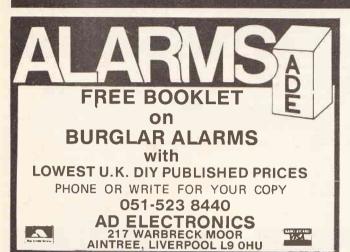


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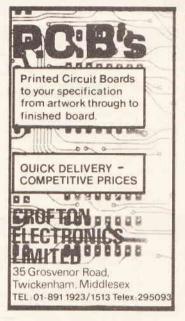




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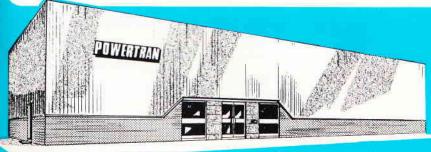
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