

HUMBOLDT BAY

INDEPENDENT SPENT FUEL STORAGE INSTALLATION



CALCULATIONS



PACIFIC GAS AND ELECTRIC COMPANY

PACIFIC GAS AND ELECTRIC COMPANY
GEOSCIENCES DEPARTMENT
CALCULATION DOCUMENT

Calc Number: GEO.HBIP.02.08
Calc Revision: 1
Calc Date: 7/18/2003
Quality Related:
ITR Verification Method: A

1.0 CALCULATION TITLE:

DETERMINATION OF POTENTIAL EARTHQUAKE-INDUCED
DISPLACEMENTS OF CRITICAL SLIDE ALONG HBIP ISFSI
TRANSPOT ROUTE

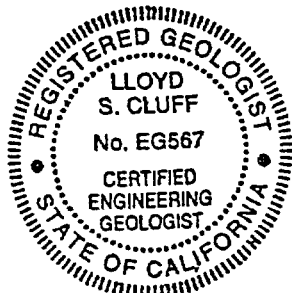
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3.0 RECORD OF REVISIONS

Rev. No.	Reason for Revision	Revision Date
0	Initial Issue	11/27/02
1	<p>In revision 0 (2002) of this calculation package the program QUAD4M was used to compute seismic coefficients of potential sliding masses at HBIP transport route. The program QUAD4M had been updated to QUAD4MU and was verified in calculation package GEO.DCPP.01.34, Revision 4 in 2003. The updated program QUAD4MU mainly modified the subroutine in QUAD4M for the calculation of seismic coefficient.</p> <p>In this revision 1, the earthquake-induced displacements at the ISFSI transport route are re-evaluated using the updated program QUAD4MU.</p> <p>Attachments E, F, G and H are new for revision 1. These are input files and excerpts of output files for dynamic response and deformation calculations.</p> <p>Attachments A, B, C and D remain unchanged and are copies from revision 0.</p>	7/1/2003

4.0 PURPOSE

As required by Geosciences Work Plan GEO 2002-03 entitled, "Development of Slope Stability Calculations for the Humboldt Bay ISFSI," this calculation package estimates earthquake-induced permanent displacements of the most critical potential sliding mass along the proposed HBIP transport route, using field and laboratory data, postulated design ground motions, and a Newmark-type procedure incorporating a finite element model of the site.

In revision 0 of this calculation package, the program QUAD4M was used to compute seismic coefficients of potential sliding masses at the transport route. The program QUAD4M had been updated to QUAD4MU and verified in calculation package GEO.DCPP.01.34, Revision 4 in 2003. The updated program QUAD4MU mainly revised the subroutine in QUAD4M for the calculation of seismic coefficient. Geosciences Department of PG&E requested that the finite element analyses be repeated to obtain the updated seismic coefficient time histories for the potential sliding masses using QUAD4MU. These time histories were also re-integrated to obtain new estimates for the earthquake-induced displacement at the transport route based on the results of the updated program QUAD4MU. Also, the computed acceleration time histories, and the corresponding response spectra were all updated in this revision.

5.0 ASSUMPTIONS

1. There is no potential for liquefaction along the route. This is a reasonable assumption as concluded on page 8 of calculation package GEO.HBIP.02.02.
2. For purposes of analyses, stratigraphic layers are assumed to lie near horizontally. This is a reasonable assumption, as shown on Figure 4-14 of Section 4, Site Geology, of Technical Report TR-HBIP-2002-01.

3. Groundwater is assumed to be at elevation +6 feet, mean lower low water (MLLW) datum. This is a reasonable assumption, as documented on page 2 of GEO.HBIP.02.02. This elevation is consistent with those measured in monitoring wells installed in the vicinity of the wastewater ponds east of the discharge canal (Figure 4-1 of Section 4 of TR-HBIP-2002-01). Water levels in these wells range between 4 and 7 feet below ground surface and respond only slightly to tidal cycles (White, 2002d).
4. The undrained strengths of stiff cohesive soils and dense sandy soils along the route are not reduced due to earthquake shaking. This is a reasonable assumption because, as reported by Makdisi and Seed (1978), stiff clays and dense sands do not suffer significant reduction in undrained strength due to cyclic loading; such soils retain most of their initial undrained strength even after being subjected to significant cyclic loading.
5. Input ground motions used to analyze the response along the route are deconvolved using the 1-D program SHAKE to the base of the 2-D finite element mesh from the lower "free field" ground surface of the section modeled rather than at the higher surface elevations of the hillside (Figure 8-4). This is a conservative assumption because the ground motions calculated at higher elevations will be greater than the input ground motion due to topographic amplification, thus leading to greater calculated displacements.
6. The 1-D and 2-D site response analyses described herein used a single velocity profile developed using a factor of +1.22 (as described in Input 12, below) rather than varying the profile by plus or minus this factor to determine the maximum site response. This is a reasonable assumption, because Figures 7 and 8 in GEO.HBIP.02.04 indicate maximum site amplification occurs for the positive (upper bound) factor over nearly all frequencies for both the fault normal and fault parallel components.
7. Vertical ground motions are not considered in the analyses, as they have been shown to have limited impact on the magnitude of calculated displacements (Yan and others, 1996).
8. Properties selected for analysis of ISFSI site stability in calculation package GEO.HBIP.02.07 are appropriate for use at the transport route section selected for analyses in this calculation package, with the exception of the uppermost clay layer which is assigned a reduced strength as described in Step 3 of the Body of the

Calculation. This assumption is reasonable because soil stratigraphy and properties in borings near the transport route section analyzed are consistent with those determined at the ISFSI site, as discussed in more detail in step 1 of the Body of the Calculation.

9. The centerline transporter load is placed at the centerline of the proposed transport route. This is a reasonable assumption as the most likely location during transport.

6.0 INPUTS

1. The site map (Figure 8-1) is obtained from Figure 4-2 of Section 4, Site Geology, of Technical Report TR-HBIP-2002-01.
2. The proposed transport route (a portion of which is shown on Figure 8-1) is obtained from White, 2002a (Attachment A).
3. The borings nearby the transport route critical section (determined as described in Step 1 of Methodology) are obtained from White, 2002b (Attachment A).
4. The table of soil properties for stability analyses (Table 8-1) is obtained from Table 7-2 of calculation GEO.HBIP.02.07.
5. The table of soil properties for site response analyses (Table 8-2) is obtained from Table 7-3 of GEO.HBIP.02.07.
6. Relationships of modulus and damping ratio with shear strain referenced in Table 8-2 are obtained from Figures 7-11 and 7-12 of GEO.HBIP.02.07 and as described in Step 3 of GEO.HBIP.02.07.
7. The transporter load and dimensions are obtained from Work Plan GEO 2002-03, Attachment 2.
8. Design surface ground motions for use in response analyses are obtained from White, 2002c, as confirmed in White, 2002e (Attachment A).
9. The primary seismic source for ground motions (the Bay Entrance fault) is obtained from Input 9 of GEO.HBIP.02.07.
10. The positive directions of primary seismic source components (fault normal and fault parallel) are obtained from Input 10 of GEO.HBIP.02.07.
11. The orientation of the primary seismic source is obtained from Input 11 of GEO.HBIP.02.07.
12. The stiff soil velocity profile is developed by multiplying velocity values in Input 5 above by 1.22 (as described in Assumption 6 above) or k_{2max} values in Input 5 by 1.5, as recommended on page 26 of ASCE (1986). (Velocities are related to the

square root of soil shear modulus, as shown in Step 3 of GEO.HBIP.02.07, so the square root of the 1.5 factor in ASCE is 1.22, and k_{2max} is proportional to the shear modulus as shown on page 11, below.)

7.0 METHODOLOGY AND EQUATION SUMMARY

1. Determine the most critical location along the transport route in terms of slope stability. The most critical location will be that which meets the following two criteria simultaneously: a) closest approach of transporter to slope and b) greatest height of slope.
2. Determine subsurface stratigraphy at most critical location based on geotechnical data obtained from nearby borings and trenches.
3. Assign static and dynamic soil properties to subsurface layers based on similarities with those layers having assigned properties.
4. Perform static slope stability analysis at most critical location along transport route using program UTEXAS4 to obtain short-term static factor of safety of critical slide mass with transporter loading.
5. Perform pseudo-static slope stability analysis of critical slide mass as determined in step 4 using UTEXAS4 to determine pseudostatic horizontal acceleration that reduces factor of safety to approximately 1.0. Acceleration obtained is the yield acceleration, k_y .
6. Rotate design surface ground motions to direction of cross section and perform preliminary Newmark displacement analyses using program DEFORMP and k_y of the critical slide mass as determined in step 5, above, to assess relative magnitudes of displacements for each ground motion (see step 11, below, for fuller description of displacement analyses). Select ground motions giving greatest displacements for further analyses.

For each ground motion selected in step 6, above, the following steps were conducted:

7. Deconvolve the selected surface ground motion to the base of the finite element mesh using program SHAKE.

8. Perform a two-dimensional dynamic finite element analysis of the cross section using program QUAD4MU to determine the seismic response of the slope due to the earthquake motion as determined in step 7, above, placed at base of section.
9. Calculate seismic coefficient time history (and the maximum seismic coefficient, k_{max}) of the critical slide mass from output of the QUAD4MU analysis. The seismic coefficient is the ratio of the force induced by an earthquake in the slide mass to the weight of the mass.
10. Obtain surface ground motion calculated at one or more representative nodes in the free field from output of QUAD4MU. Compare calculated motion with input motion.
11. Perform Newmark-type displacement analyses (after Newmark, 1965), using DEFORMP, to determine earthquake-induced permanent displacements of the critical slide mass. For a specified potential slide mass, the seismic coefficient time history of that mass is compared with the yield acceleration k_y . When the seismic coefficient exceeds the yield acceleration, downslope movement will occur along the direction of the assumed failure plane. The movement will decelerate and will stop after the level of the induced acceleration drops below the yield acceleration, and the relative velocity of the sliding mass drops to zero. The accumulated permanent displacement is calculated by double-integrating the increments of the seismic coefficient time history that exceed the yield acceleration. The analysis requires the seismic coefficient time history as calculated in step 9, above, and the yield acceleration of the critical sliding mass as calculated in step 5, above.

8.0 SOFTWARE

The following computer programs (software) are used in this calculation package:

1. UTEXAS4 (version 4.0.0.8 dated 7/27/01), a commercially available Windows-compatible program to perform slope stability analyses, was verified in calculation package GEO.HBIP.02.09.
2. SHAKE (Geomatrix version dated 8/27/95), a 1-D equivalent linear site response PC DOS-compatible program used in this calculation package to compute base motions for use in finite element analyses, was modified by Geomatrix from the original developed at the University of California, Berkeley to increase the sizes of arrays to

accommodate more time history data points and a greater number of layers. The Geomatrix version of the program was verified in GEO.DCPP.02.02.

3. QUAD4MU (updated version dated 3/1/2003), a commercially available PC DOS-compatible program to perform 2-D finite element analyses, was verified in GEO.DCPP.01.34. rev. 4.
4. SPECTRAD (version dated 3/25/98), a PC DOS-compatible program developed by Geomatrix Consultants to calculate response spectra from time histories, was also verified in GEO.DCPP.01.34 in addition to QUAD4MU.
5. DEFORMP (version dated 3/30/2000), a PC DOS-compatible program developed by Geomatrix Consultants to perform Newmark-type displacement analyses, was verified in GEO.DCPP.01.35.

All programs are proprietary and designed to execute on personal computers under the Microsoft Windows 2000 operating system. No passwords are required to execute these programs.

9.0 BODY OF CALCULATION

1. The most critical location along the transport route in terms of slope stability is determined by inspection of Figure 8-1, modified to include the proposed transport route from White, 2002a. The selected location shown on Figure 8-1 meets the following two criteria simultaneously: a) closest approach of transporter to slope (in this case, the bank of the Discharge Canal) and b) greatest height of slope. Beyond this location, the distance between the transport route and the Discharge Canal bank increases as the route continues up the hill, thereby reducing the effect of the transporter load on the bank.
2. The subsurface stratigraphy at the selected location is determined based on geotechnical data obtained from nearby borings. Logs from nearby borings as provided in White, 2002b, were reviewed and stratigraphy from the logs summarized as shown on Figure 8-2. Selected soil strengths are also shown on Figure 8-2. It is seen that soil stratigraphy consists of the same sequence of stiff clays overlying dense sands and gravels as found in boring 99-2 near the proposed ISFSI site further up the hill, as summarized in Table 8-1, from Calculation Package GEO.HBIP.02.07.

3. Because available data from nearby borings as summarized on Figure 8-2 indicate soil stratigraphy and properties are consistent with those determined at the ISFSI site, static and dynamic properties of the subsurface soils are selected to be the same as at the ISFSI site as presented in GEO.HBIP.02.07, as summarized in Tables 8-1 and 8-2. One exception, as noted in Table 8-1, is the uppermost approximately 15 feet of the upper clay layer (layer 5 in Table 8-1) which is modeled with a shear strength of 900 psf based on test data from nearby 1973 boring D&M73-2 as shown on Figure 8-2.

Calculation of transporter load to apply in analyses is determined from transporter data as found in Attachment 2 of Geosciences Work Plan GEO 2002-03. The calculation is as follows:

Total weight = vehicle plus loaded cask = 170,000 lbs + 160,000 lbs = 330,000 lbs

Area = (minimum track bearing length) x (track spacing plus track width)

= 294 inches x (182 inches + 29.5 inches) = 62,181 SI = 431.8 SF

Pressure = Total weight / Area = 330,000 lbs / 431.8 SF = 764 psf; use 800 psf

Track width = 182 inches + 29.5 inches = 211.5 inches = 17.625 feet

20-foot roadway ~ 25 feet wide in cross section

17.625-foot track width ~ 22 feet wide in cross section

4. A static slope stability analysis was performed at the most critical location along the transport route as determined above using program UTEXAS4 and Spencer's method to obtain the short term static factor of safety with transporter loading. The section analyzed, with selected effective strength soil properties from Table 8-1 and location of transporter load, are shown in Figure 8-3. It is conservatively assumed that there is no water in the adjacent Discharge Canal but that clay and sand layers are saturated to elevation 6 (normal ground water level as described in Assumption 3). The resulting factor of safety of 1.7 is listed in Table 8-3. UTEXAS4 input and selected output files are found in Attachment B. All files are also included on the enclosed CD and are listed in Table 8-3.
5. The slope stability computations were repeated for the slide mass having the lowest static factor of safety by incrementally increasing the horizontal pseudostatic acceleration to determine the yield acceleration, k_y , that reduced the factor of safety of the slide mass to 1.0. Yield accelerations were computed using a two-stage approach in UTEXAS4, wherein normal stresses along the failure plane are first calculated under static pre-earthquake conditions and are then held constant during

application of the horizontal pseudostatic acceleration to estimate the undrained shear strengths during transient earthquake loading. Dynamic (undrained) soil strengths are listed in Table 8-1. As shown on Figure 8-3 and listed in Table 8-3, the resulting yield acceleration for a safety factor of 1.001 is 0.84. UTEXAS4 input and selected output files are found in Attachment B. All files are also included on the enclosed CD and are listed in Table 8-3.

6. Prior to performing finite element analyses, each horizontal component of the surface ground motion provided (White, 2002c) was rotated to the direction of the cross section. Seismic response due to the vertical component of ground motions was not considered in this analysis (Assumption 7). The amount of rotation was determined by calculating the difference between the azimuth of the cross section as shown on Figure 8-1 and the azimuth of the primary source of the ground motions (the Bay Entrance fault, from GEO.HBIP.02.07) as determined in GEO.HBIP.02.07. For section C-C', the difference between its azimuth of N 84° E and the fault azimuth of N 7° W is 264°.

The rotated component along the section is the sum of the projections of the fault normal and fault parallel components along the direction of the section. The formulation is as follows:

$$CC' = F_P \cos(\Phi) + F_N \sin(\Phi)$$

where F_P and F_N are fault parallel and fault normal components of the acceleration time histories, CC' is the component along the section at each time step, and Φ is the difference between the orientation of the section and the fault. Calculations of rotated components were performed in Excel spreadsheets. Excerpts of the spreadsheets along with related time history input and output are found in Attachment C. All files are also included on the enclosed CD and are listed in Table 8-6. The spreadsheets are verified by the following hand check from SET1ROT.XLS (page 4 of Attachment C):

at +0.000 seconds, set 1 FN = - 0.229294E-03 and FP = 0.846349E-04

Then for section C-C' with $\Phi = 264$ degrees,

$$CC' = 0.846349E-04 \cdot \cos(264) + - 0.229294E-03 \cdot \sin(264) = 2.19191E-04$$

checks

Then a rigid block Newmark-type analysis was performed with each rotated surface ground motion and the yield acceleration for the critical slide mass determined in .

step 5, above, using program DEFORMP. The positive direction of each ground motion component (south for fault parallel and west for fault normal) was obtained from GEO.HBIP.02.07. Calculated displacements are summarized in Table 8-4. The two ground motions selected in GEO.HBIP.02.07 (sets 1 and 3), were selected as representative of the range of displacements for further finite element analyses. All DEFORMP input and output files are included on the enclosed CD and are listed in Table 8-6. Excerpts of these files are not attached, as they are similar to those found in Attachment G. Earthquake motions input at the base of the section were developed from the surface ground motions provided by PG&E (White, 2002c) and preliminary Newmark analysis.

7. Earthquake motions input at the base of the section were developed from the rotated surface ground motions determined in step 6, above. Plots of the rotated surface ground motions are shown on Figures 8-5 and 8-6. The surface motions were deconvolved to approximately 85 feet below ground level using program SHAKE (Geomatrix version) and the dynamic properties for layers 1, 2, 3, and 4 listed in Table 8-2, as modified to obtain a "stiff soil" velocity profile (1.22 times velocities or 1.5 times k_{2max} values in Table 8-2 as described in Input 12) to obtain the motions at depth for use in QUAD4MU analyses. Modulus reduction and damping curves were obtained from GEO.HBIP.02.07 as described in Input 6. The base was modeled as elastic half-space with a shear wave velocity obtained from Table 8-2. To minimize numerical difficulties encountered in the SHAKE runs as a result of the artificially high energy in the high frequency range of the surface motions, a frequency cutoff of 2.5 Hz was applied during the deconvolution. A second SHAKE deconvolution run was then performed, fixing the soil properties as obtained from the final iteration of the first run, increasing the frequency cutoff applied in the first run to 6 Hz, to obtain the motions at depth for use in QUAD4MU analyses. SHAKE input and selected output files are found in Attachment D. All files are also included on the enclosed CD and are listed in Table 8-6.
8. The earthquake-induced seismic coefficient time histories (and their peak values k_{max}) for the critical slide mass were computed using a two-dimensional dynamic finite element analysis program QUAD4MU that is an updated version of program QUAD4M. The program uses equivalent linear strain-dependent modulus and damping properties and an iterative procedure to estimate the non-linear strain-

dependent soil properties. The time-step analysis incorporates a Rayleigh damping approach and allows for variable damping in different elements. The option of computing the seismic coefficient time history of a sliding mass in QUAD4M was modified in QUAD4MU and this option was verified in the calculation package GEO.DCPP.01.34, rev. 4.

The QUAD4M analyses reported in GEO.HBIP.01.08, rev. 0 were repeated in this revision using QUAD4MU. The QUAD4MU analyses were performed at the cross section analyzed using the dynamic properties summarized in Table 8-2 from step 3, above, the velocity profile as modified to obtain a "stiff soil" in step 7, above, and the earthquake motion at the base derived in step 7, above. A finite element representation of the site is shown on Figure 8-4. It includes the potential slide mass having the minimum factor of safety and extends from the ground surface down into the sand layer at a depth of about 85 feet below ground surface. The base of the model is in the dense sand layer and the half-space properties were set the same as in the SHAKE analyses performed in step 7, above. QUAD4MU input and selected output files are found in Attachment E. All files are also included on the enclosed CD and are listed in Table 8-6.

9. The seismic coefficient time history of the critical slide mass was output from the QUAD4MU analysis. Plots of the seismic coefficient time histories for each input ground motion are shown in Figures 8-5 and 8-6.
10. The surface ground motion calculated at one surface node (76) near the critical section was obtained from QUAD4MU output. This node was selected because it is in the "free field" and can be compared with the input motion in SHAKE (step 7 above) to assess the reasonableness of the QUAD4MU analysis results. The response spectra for the nodal point and input time histories were calculated using program SPECTRAD. Excerpts of SPECTRAD input and output files are found in Attachment F. All files are also included on the enclosed CD. The response spectra are plotted in Figures 8-7 and 8-8. It can be seen that the nodal point spectra conservatively envelope the input time history spectra, providing high confidence that QUAD4MU response calculations are conservative.
11. Newmark displacement analyses, using DEFORMP, were performed to determine the earthquake-induced permanent displacements of the critical section. The analyses utilize the seismic coefficient time histories as calculated in step 9, above,

and the yield acceleration of the critical slide mass as calculated in step 3, above. Results of the Newmark displacement analyses, shown graphically on Figure 8-9 and 8-10, are plotted as values of calculated displacement for ratios of k_y to k_{max} . For ground motion set 1 and a yield acceleration of 0.84, computed displacements range from 2.6 to 4.7 feet (Figure 8-9). For ground motion set 3, computed displacements range from 2.6 to 9.0 feet (Figure 8-10). Values of computed displacement for each ground motion are listed in Table 8-5. The average displacement for the full range of time-histories used is 4.7 feet. DEFORMP input and selected output files are included in Attachment G. All files are included in the enclosed CD and listed in Table 8-6.

10.0 RESULTS AND CONCLUSIONS

This calculation package has estimated static stability and earthquake-induced permanent displacements of the most critical potential slide mass identified along the proposed HBIP transport route. Results of short-term static stability analyses listed in Table 8-3 indicate the safety factor against sliding with transporter load is 1.7. Results of Newmark-type displacement analyses, listed in Table 8-5, indicate a range of potential displacements of the critical slide mass at the selected transport route location from 2.6 to 4.7 feet for ground motion set 1, and from 2.6 to 9.0 feet for ground motion set 3. The average displacement for the full range of time-histories used is 4.7 feet.

11.0 LIMITATIONS

There are no limitations on the use of the calculation results.

12.0 IMPACT EVALUATION

The results of the displacements presented in Section 10 do not impact other Geosciences calculations.

13.0 REFERENCES

1. ASCE, 1986, Seismic Analysis of Safety-Related Nuclear Structures and Commentary on Standard for Seismic Analysis of Safety Related Nuclear Structures, American Society of Civil Engineers, September.

2. GEO.DCPP.01.25, Determination of seismic coefficient time histories for potential sliding masses along cut slope behind ISFSI pad, rev. 2
3. GEO.DCPP.01.34, Verification of computer code QUAD4MU, rev. 4
4. GEO.DCPP.01.35, Verification of computer code DEFORMP, rev. 2
5. GEO.HBIP.02.02, Determination of liquefaction potential at HBIP ISFSI site, rev. 0.
6. GEO.HBIP.02.05, Development of spectrum compatible time histories for the HBIP ISFSI, rev. 0.
7. GEO.HBIP.02.07, Determination of potential earthquake-induced displacements of critical slides at HBIP ISFSI site, rev. 1.
8. GEO.HBIP.02.09, Verification of computer program UTEXAS4, rev. 0
9. Geosciences Work Plan GEO 2002-03, "Development of Slope Stability Calculations for the Humboldt Bay ISFSI, rev. 0.
10. Makdisi, F., and Seed, H.B., 1978, Simplified Procedure for Estimating Dam and Embankment Earthquake-Induced Deformations, Journal of the Geotechnical Engineering Division, ASCE, Vol. 104, No. GT7, July, pp. 849-867.
11. Newmark, N.M., 1965, Effects of earthquakes on dams and embankments: Geotechnique, v. 15, no. 2, p. 139-160.
12. Section 4, Site Geology, Humboldt Bay ISFSI Project Seismic Hazards Analysis, Rev. 0, dated 16 September 2002, of Technical Report TR-HBIP-2002-01.
13. White, R., 2002a, letter from Robert White to Faiz Makdisi, Re: proposed transport route for HBPP ISFSI, dated 19 April 2002, with attached site map.
14. White, R., 2002b, letter from Robert White to Faiz Makdisi, Re: transmittal of boring logs from previous investigations at HBPP, dated 1 May 2002, with attachments.
15. White, R., 2002c, letter from Robert White to Faiz Makdisi, Re: transmittal of preliminary design surface ground motions for use in response analyses, dated 29 July 2002, with enclosed CD.
16. White, R., 2002d, letter from Robert White to Faiz Makdisi, Re: excerpt from Humboldt Bay Power Plant December 1985 TPCA HAR, dated 15 November 2002.
17. White, R., 2002e, letter from Robert White to Faiz Makdisi, Re: transmittal of final approved time histories for Humboldt Bay ISFSI Project slope stability analyses, dated 27 November 2002.

18. Yan, Liping, Neven Matasovic, and Edward Kavazanjian, Jr., 1996, Seismic response of a block on an inclined plane to vertical and horizontal excitation acting simultaneously, Proceedings, 11th ASCE Conference of Engineering Mechanics, Fort Lauderdale, FL, Volume 2, pp. 1110-1113.

14.0 ATTACHMENTS

- A. Geosciences transmittals (11 pages)
 - White, R., 2002a, letter from Robert White to Faiz Makdisi, Re: proposed transport route for HBPP ISFSI, dated 19 April 2002, with attached site map
 - White, R., 2002b, letter from Robert White to Faiz Makdisi, Re: transmittal of boring logs from previous investigations at HBPP, dated 1 May 2002 (without attachments).
 - White, R., 2002c, letter from Robert White to Faiz Makdisi, Re: transmittal of preliminary design surface ground motions for use in response analyses, dated 29 July 2002 (without enclosed CD).
 - White, R., 2002d, letter from Robert White to Faiz Makdisi, Re: excerpt from Humboldt Bay Power Plant December 1985 TPCA HAR, dated 15 November 2002.
 - White, R., 2002e, letter from Robert White to Faiz Makdisi, Re: transmittal of final approved time histories for Humboldt Bay ISFSI Project slope stability analyses, dated 27 November 2002.
- B. UTEXAS4 input and excerpts of output files for static and dynamic stability analyses (12 pages)
- C. EXCEL spreadsheet excerpts and related excerpts of time histories for rotations (9 pages)
- D. SHAKE input and excerpts of output files to obtain motion at base of QUAD4MU section (32 pages)
- E. QUAD4MU input and excerpts of output files for response analyses (21 pages)
- F. SPECTRAD input and excerpts of output files for calculating response spectra of time histories (10 pages)
- G. DEFORMP input and excerpts of output for calculation of displacements (9 pages)
- H. .CD-ROM table of contents

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- Figure 8-4 Finite element mesh and slide mass having minimum factor of safety for sections C-C'
- Figure 8-5 Time Histories, Section C-C', Set 1 Ground Motion
- Figure 8-6 Time Histories, Section C-C', Set 3 Ground Motion
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- Figure 8-10 Permanent Displacement vs. Yield Acceleration, Section C-C', Set 3 Ground Motion

17.0 ENCLOSURE

CD labeled "GEO.HBIP.02.08, rev. 1, 7/18/2003," containing the files listed in Tables 8-3, 8-4, and 8-6 (all ASCII files unless otherwise noted). The CD is located with this calculation in Geosciences' project-designated file cabinets. The CD table of contents is included in Attachment H.

TABLE 8-1
MATERIAL PROPERTIES FOR POST-EARTHQUAKE STABILITY ANALYSES

Layer No. (Fig. 8-3)	Material	Unit Weight		Effective Strength		Undrained Strength	
		γ_{min} (pcf)	γ_{sat} (pcf)	Cohesion c' (psf)	Friction Angle ϕ' (degree)	Cohesion c (psf)	Friction Angle ϕ (degree)
5	Stiff Sandy Clay	125	125	0	30	900	0
3,4	Very Stiff Clay	123	123	0	30	2000	0
2	Dense to Very Dense Silty Sand	125	128	0	37	1500*	37*
1	Hard Silt and Silty Clay	128	128	0	30	3000	0

* Undrained strength of dense sand is limited to 9 ksf.

Source: Table 7-2 of Calculation GEO.HBIP.02.07 (except layer 5)

TABLE 8-2

**Revised Shear Wave Velocity Profile for Site Response Analysis
(based on I.M. Idriss Interpretation on May 24, 2002)**

Layer No. *	Depth (ft)	Description	Density (pcf)	Shear Wave Velocity (fps)	K_{2max}	Modulus Reduction and Damping Curves
1-a (5)	0-15	Silty Clay	125	750	--	Vucetic and Dobry (1991) PI=15
1-b (5)	15-20	Silty Clay	125	750	--	Vucetic and Dobry (1991) PI=15
1-c (3)	20-25	Silty Clay	125	1,000	--	Vucetic and Dobry (1991) PI=15
2-a (2)	25-30	Sand with Gravel	130	1,000	80	EPRI (1993) Depth = 20-50 feet
2-b (2)	30-40	Sand with Gravel	130	1,150	100	EPRI (1993) Depth = 20-50 feet
2-c (2)	40-50	Sand with Gravel	130	1,150	80	EPRI (1993) Depth = 20-50 feet
3 (1)	50-60	Silty Clay	130	1,500	--	Vucetic and Dobry (1991) PI=15
4-a	60-90	Sand with Gravel	130	1,500	125	EPRI (1993) Depth = 50-120 feet
4-b	90-135	Sand	130	1,750	130	EPRI (1993) Depth = 50-120 feet
5	135-150	Sand with Gravel	130	2,000	140	EPRI (1993) Depth = 120-250 feet
6	150-215	Silty Clay	130	1,550	--	Vucetic and Dobry (1991) PI = 15
7	215-260	Silty Sand	130	1,650	100	EPRI (1993) Depth = 120-250 feet
8a	260-320	Gravelly Sand	130	2,000	120	EPRI (1993) Depth = 250-500 feet
8b	320-400	Silty Sand	130	1,800	100	EPRI (1993) Depth = 250-500 feet
9	400-450	Silty Sand**	130	1,900	--	EPRI (1993) Depth = 250-500 feet
10	450-500	Silty Sand**	130	2,000	--	EPRI (1993) Depth = 250-500 feet
11	500-600	Silty Sand**	130	2,100	--	EPRI (1993) Depth = > 500 feet
12	600+	Half space	135	5,000	--	

Notes: * Layer numbers in parentheses are those assigned in Figure 8-3 and listed in Table 8-1 for stability analyses.
 ** Extrapolated from bottom of boring.
 Layers 2b and 2c k_{2max} values modified slightly to 90 and 85, respectively, in analyses to be consistent with modifications to the shear wave velocities.

Table 8-3

Results of slope stability analyses for Section C-C'

Section	long term static factor of safety	yield acceleration, k_v	UTEXAS4 static input/output files	UTEXAS4 dynamic input/output files
C-C'	1.73	0.84	transport3.txt transport3.out	transport3(dyn).txt transport3(dyn).out

All files are ASCII text and are found on the CD enclosed with the calculation. Excerpts are found in Attachment B.

Table 8-4

Permanent displacement versus yield acceleration assuming rotated surface motion equal to seismic coefficient time history

ky	Section C-C	Set	264°	Positive Negative	Displacement (ft)	computer input/output files **			
						spreadsheet (* .xls)	rotated motion (* .prn)	DEFORMP input (* .inp)	DEFORMP output (* .dat)
0.84	Set 1	264°	Positive	5.7	set1rot	s1cc	s1cp	s1cp	
			Negative	5.5	set1rot	s1cc	s1cn	s1cn	
	Set 2	264°	Positive	2.1	set2rot	s2cc	s2cp	s2cp	
			Negative	8.5	set2rot	s2cc	s2cn	s2cn	
	Set 3	264°	Positive	1.7	set3rot	s3cc	s3cp	s3cp	
			Negative	10.8	set3rot	s3cc	s3cn	s3cn	
	Set 4	264°	Positive	1.4	set4rot	s4cc	s4cp	s4cp	
			Negative	9.8	set4rot	s4cc	s4cn	s4cn	

** All files on CD-ROM enclosed with calculation.
Spreadsheet (*.xls) files are Excel files. All others are ASCII text.

Table 8-5

Permanent Displacement versus Yield Acceleration (seismic coefficients from QUAD4MU)

Yield Acceleration, K_y			K_{max}	K_y/K_{max}	Displacement (ft)
ISFSI, Section C-C					
0.84	Set 1+	264°	1.79	0.47	2.6
	Set 1 -	264°	1.86	0.45	4.7
	Set 3 +	264°	2.05	0.41	9.0
	Set 3 -	264°	1.79	0.47	2.6

TABLE 8-6
List of files for ground motion response and displacement analyses

ROTATED MOTIONS (excerpts in Attachment C)

	Section C-C		
	SET 1	SET 3	
Input (.ACC)	SET1_FP SET1_FN_FLING_BC	SET3_FP SET3_FN_FLING_BC	
Output	SET1ROT.XLS S1CC.AC8	SET3ROT.XLS S3CC.AC8	rotated surface motion

SHAKE (excerpts in Attachment D)

	Section C-C		
	SET 1	SET 3	
Input	TR1C.INP S1CC.AC8 TR1CLINP	TR3C.INP S3CC.AC8 TR3CLINP	rotated surface motion
Output	TR1C.OUT TR1C.PUN TR1CLOUT TR1CLPUN	TR3C.OUT TR3C.PUN TR3CLOUT TR3CLPUN	rotated outcrop motion

QUAD4MU (excerpts in Attachment E)

	Section C-C		
	SET 1	SET 3	
Input	TR1C.Q41 TR1CLO25 HBSOILNW.DAT	TR3C.Q41 TR3CLO25 HBSOILNW.DAT	rotated outcrop motion
Output	TR1C.Q40 TR1C00.QSC	TR3C.Q40 TR3C00.QSC	seismic coeff. motion
Acceleration Time History Outputs at Ground Surface (excerpts not attached)	TR1C00.Q4A TR1C01.Q4A TR1C02.Q4A TR1C03.Q4A TR1C04.Q4A TR1C05.Q4A TR1C06.Q4A	TR3C00.Q4A TR3C01.Q4A TR3C02.Q4A TR3C03.Q4A TR3C04.Q4A TR3C05.Q4A TR3C06.Q4A	node 51 node 76 node 101 node 765 node 821 node 961 node 1114

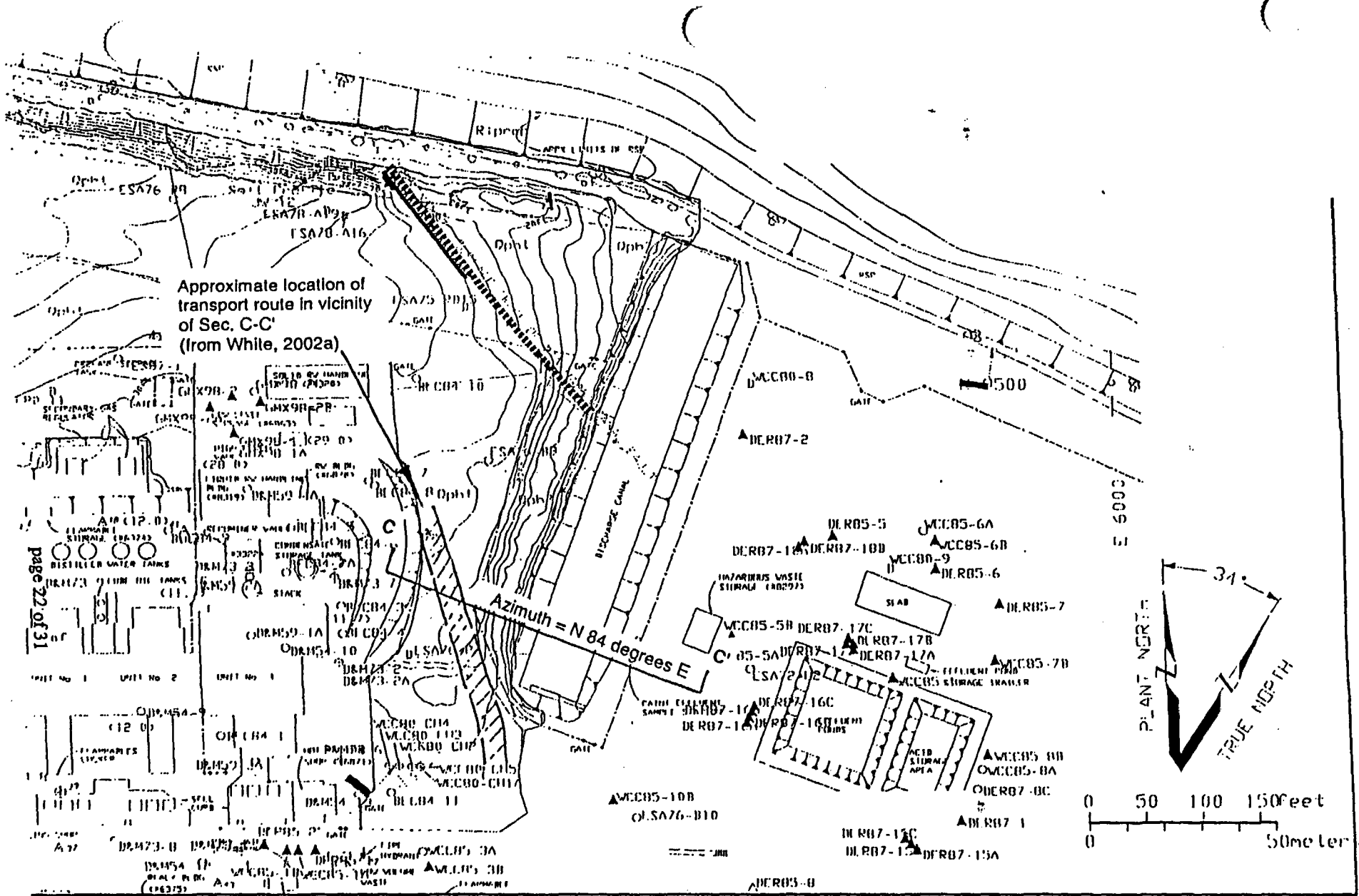
SPECTRAD (excerpts in Attachment F)

	Section C-C		
	SET 1	SET 3	
Input	SPECTRA1.INP SPECTRA2.INP SPECTRA3.INP	SPECTRA1.INP SPECTRA2.INP SPECTRA3.INP	
Output	S1CC.050 TR1C00A.050 TR1C01A.050	S3CC.050 TR3C00A.050 TR3C01A.050	rotated surface spectra node 51 at free field node 76 at free field

DEFORMP (excerpts in Attachment G)

	Section C-C		
	SET 1	SET 3	
Input	TR1CSP.INP TR1CSN.INP	TR3CSP.INP TR3CSN.INP	
Output	TR1CSP.DAT TR1CSN.DAT	TR3CSP.DAT TR3CSN.DAT	

Note: All files are ASCII text included on the CD-ROM enclosed with the calculation.



Note: Base map from Fig. 4-14 of Section 4 of TR-HBIP-2002-01.

Figure 8-1. Site and boring location plan with proposed ISFSI transport route.

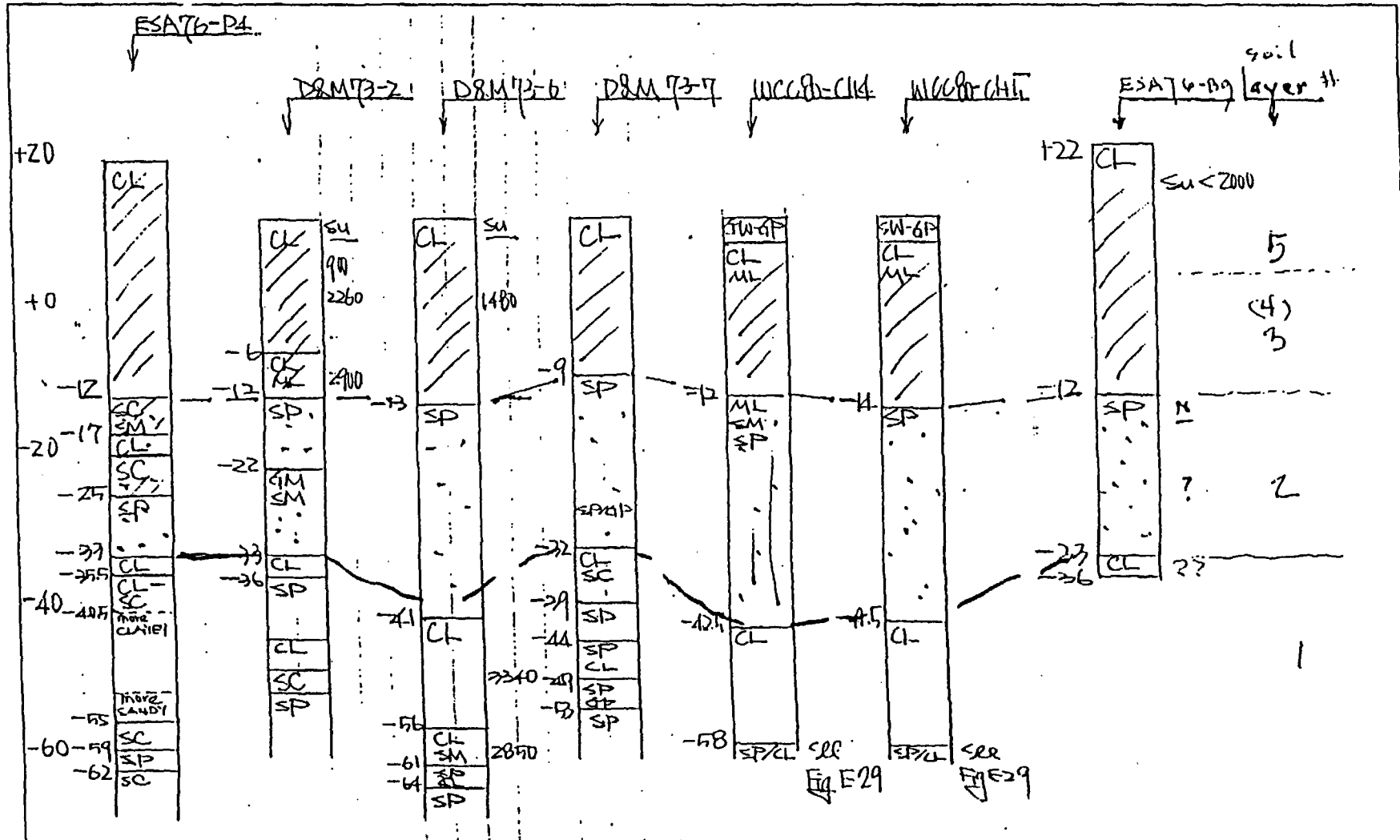
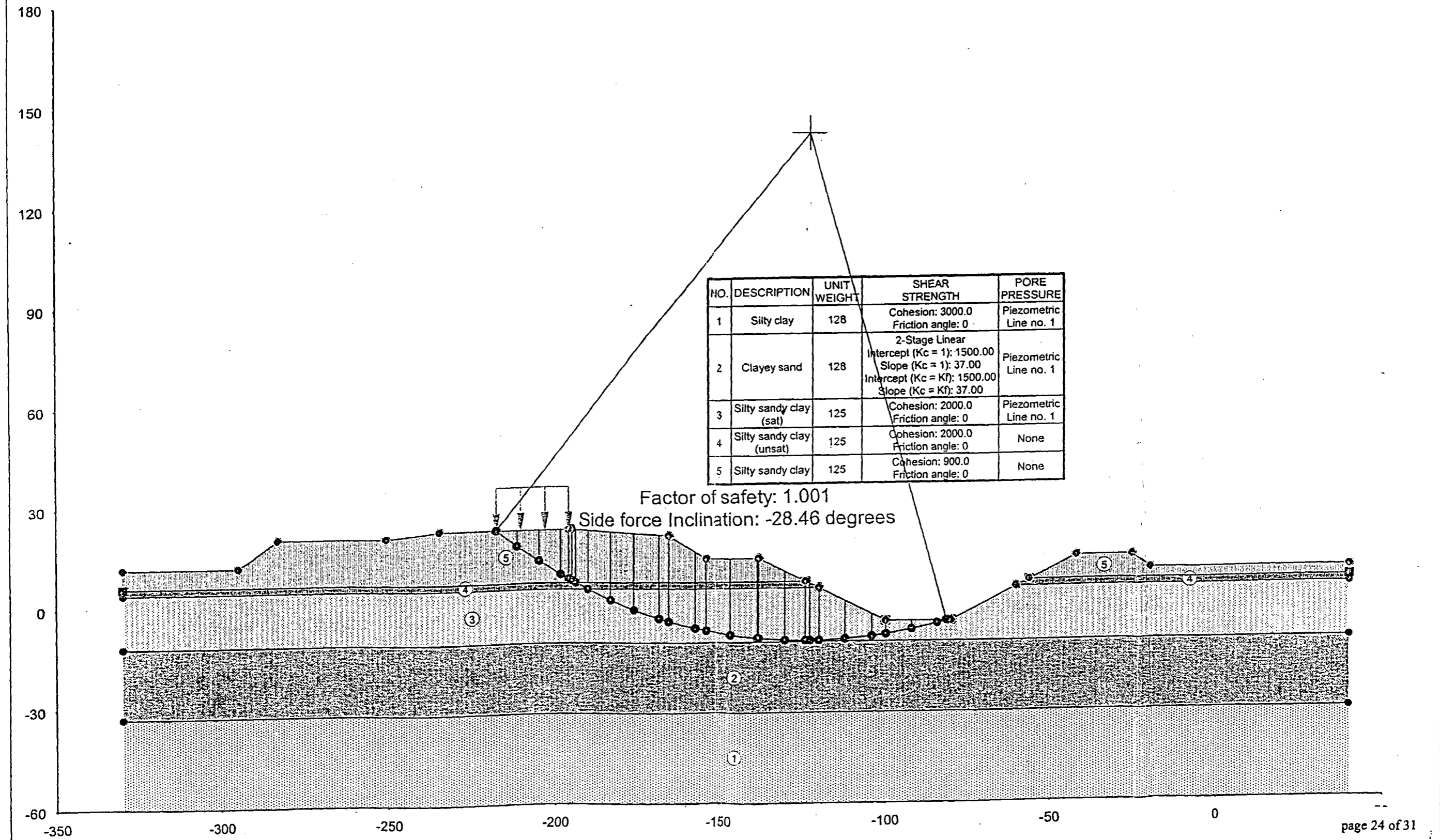


Figure 8-2. Fence diagram of borings in vicinity of Section C-C' along transport route.

SEISMIC COEFFICIENT = 0.84g



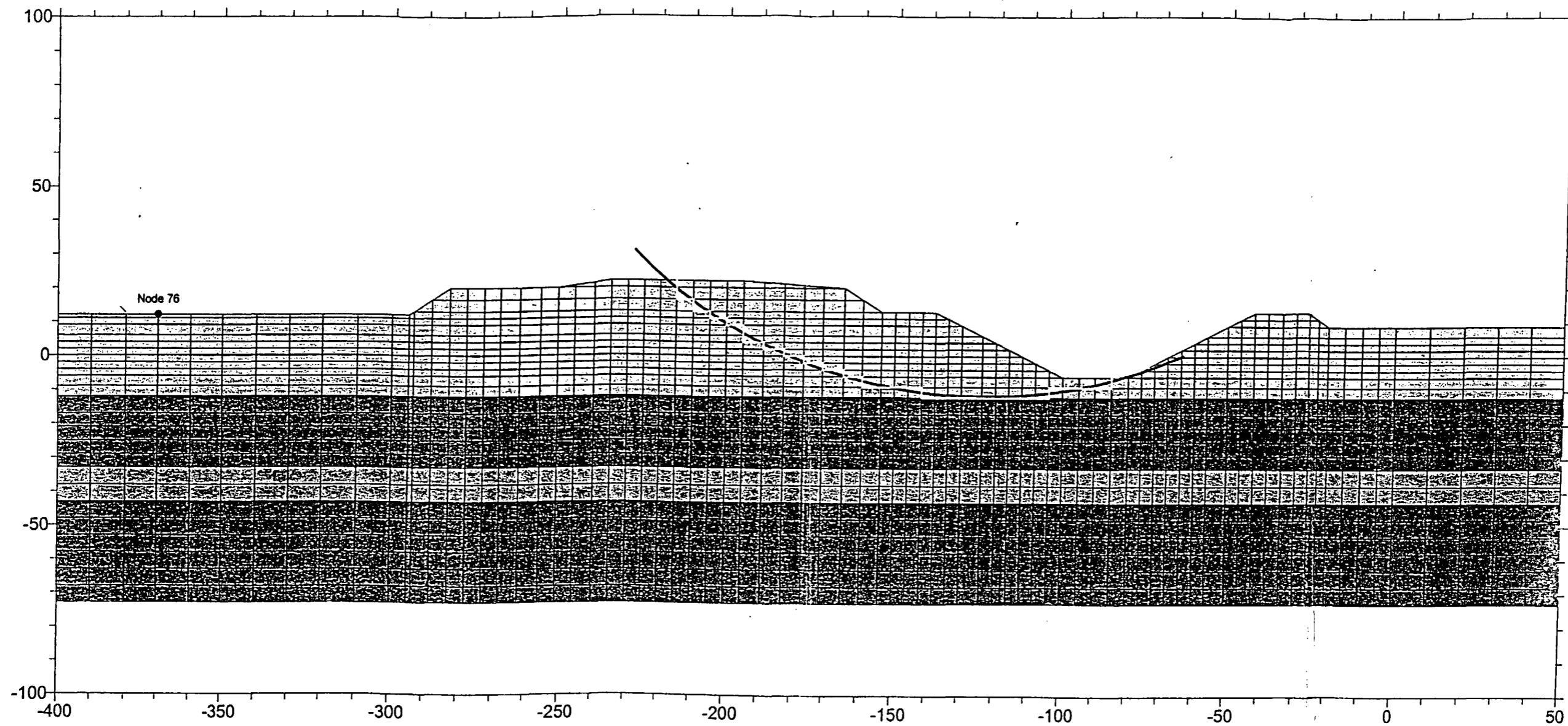


Figure 8-4. Finite element mesh and slide mass having minimum factor of Safety for Section C-C'.

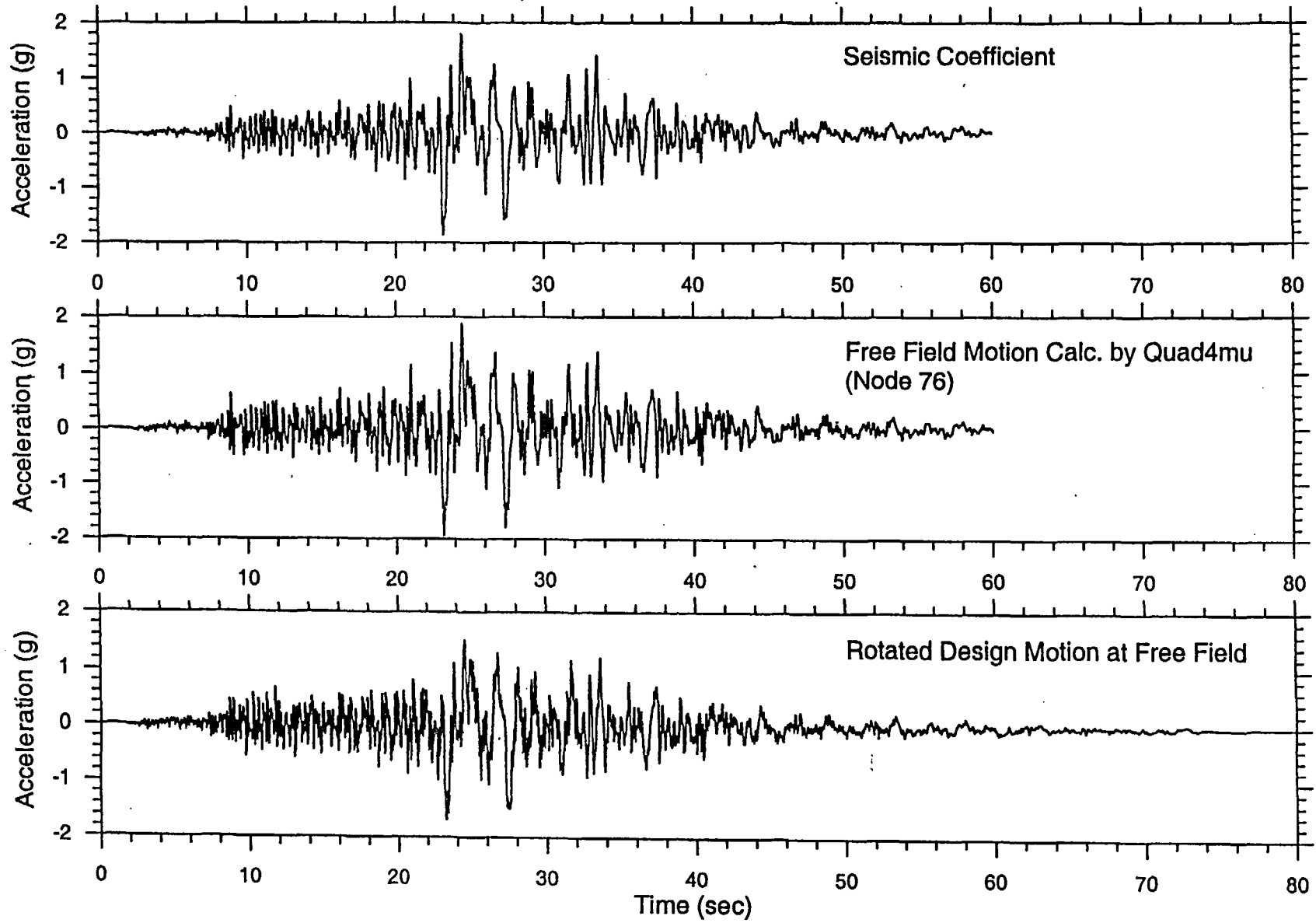


Figure 8-5. Time Histories, Section C-C', Set 1 Ground Motion.

tr1cc.grf

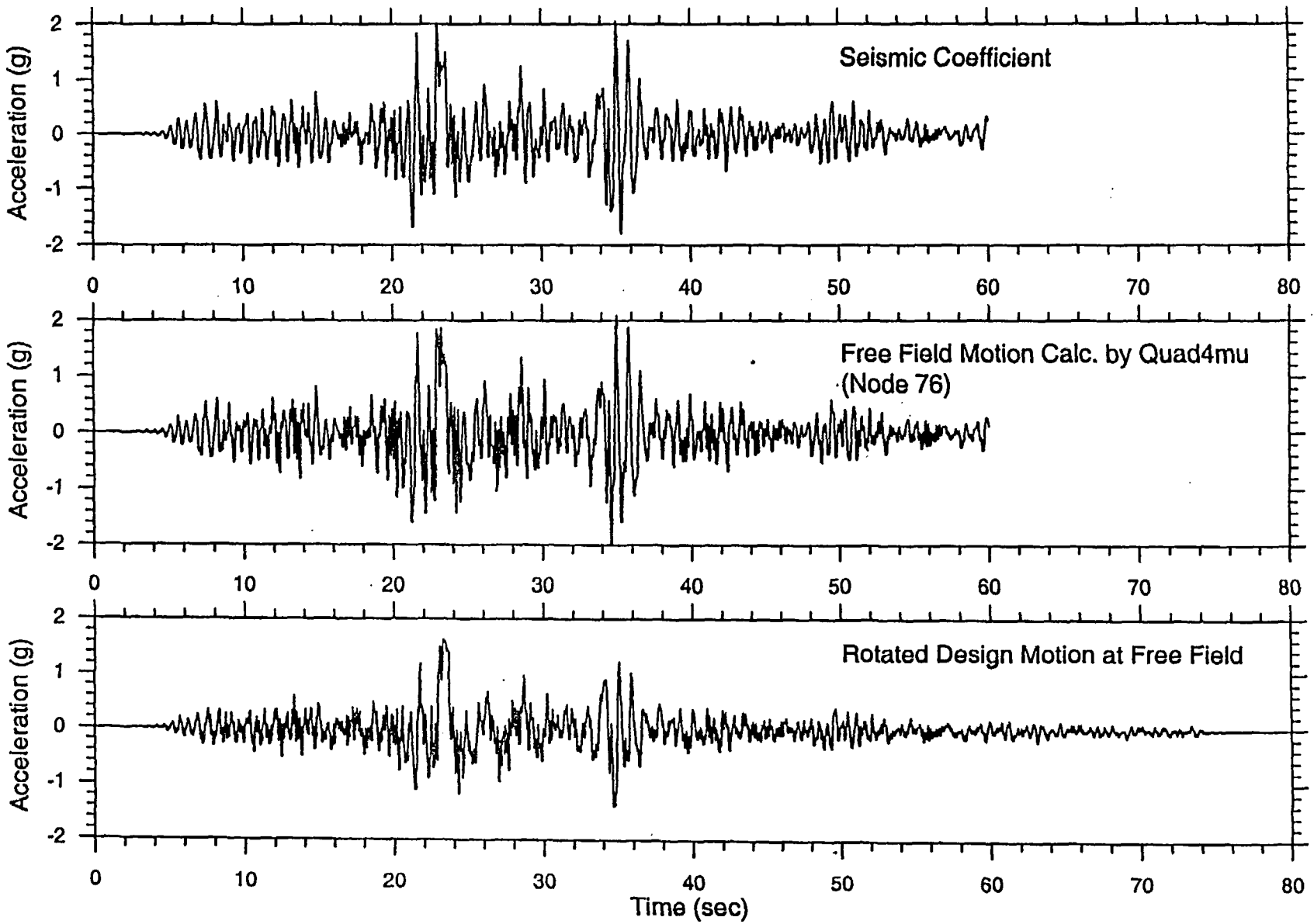


Figure 8-6. Time Histories, Section C-C', Set 3 Ground Motion.

tr3cc.grf

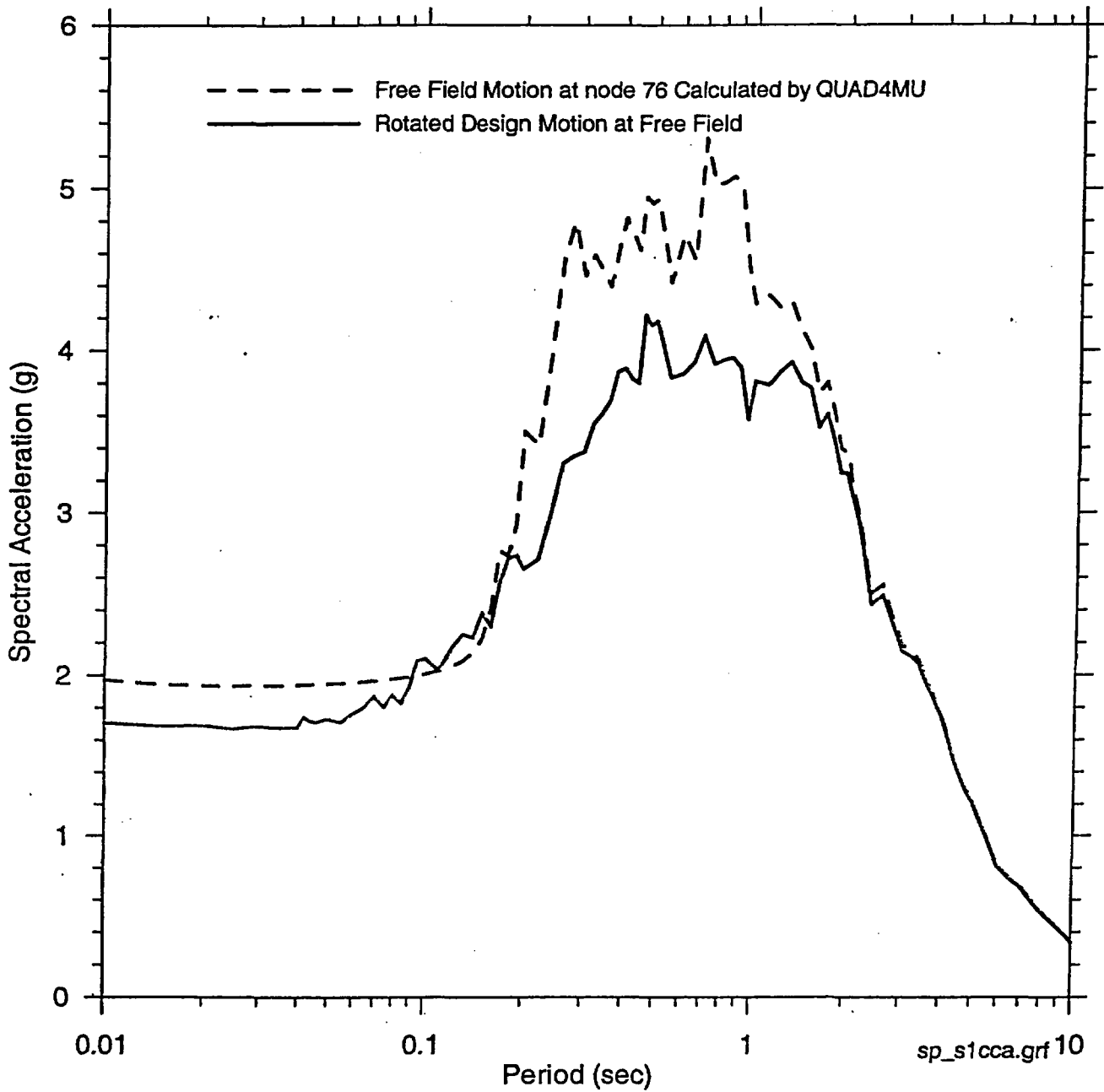


Figure 8-7. Spectral Accelerations (5% Damped), Section C-C', Set 1 Ground Motion.

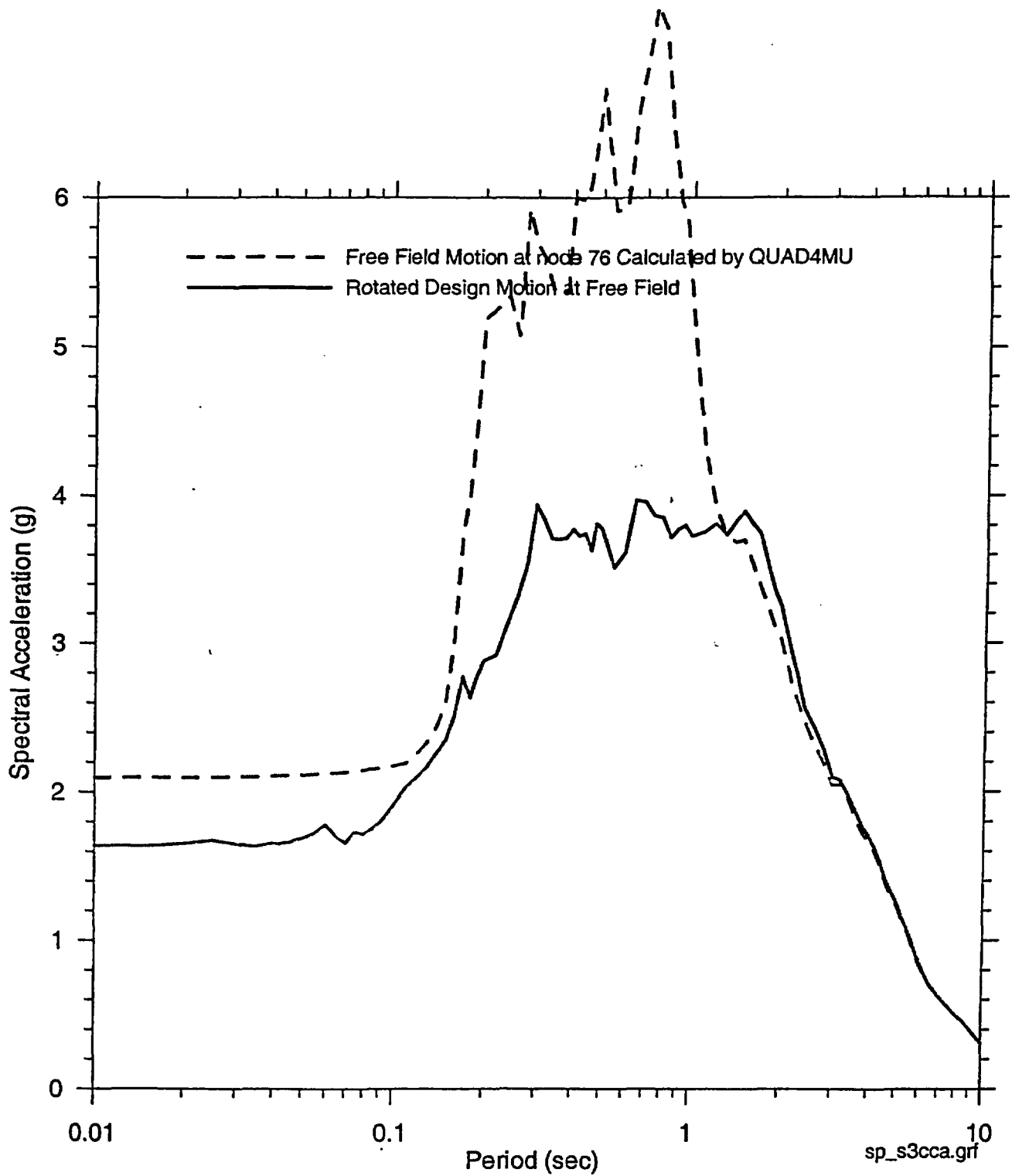


Figure 8-8. Spectral Accelerations (5% Damped), Section C-C', Set 3 Ground Motion.

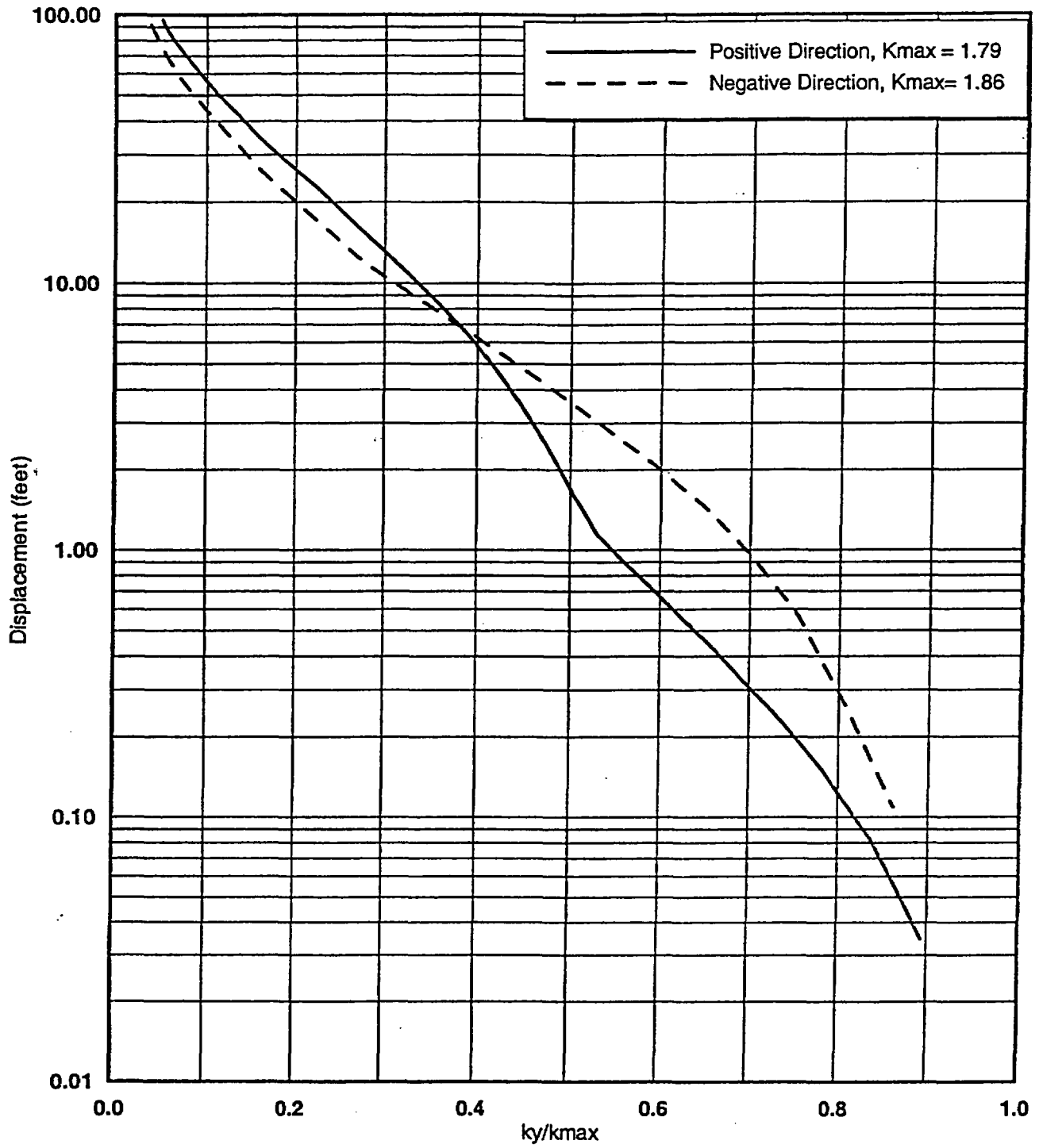


Figure 8-9. Permanent Displacement versus Yield Acceleration
Section C-C', Set 1 Ground Motion

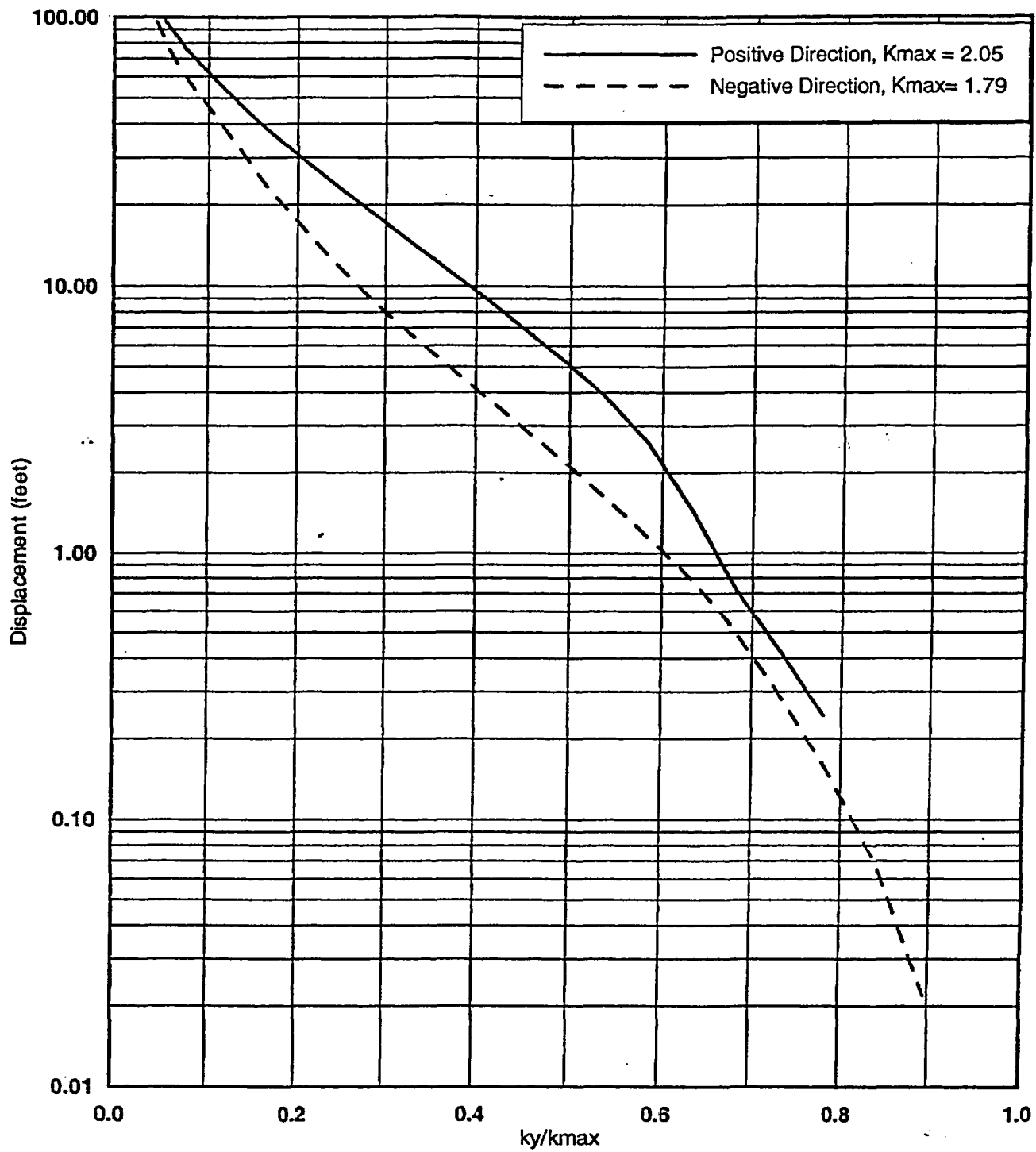


Figure 8-10. Permanent Displacement versus Yield Acceleration
Section C-C', Set 3 Ground Motion

Attachment A

Transmittals

(see Attachments section for list of transmittals)



FAIZ MAKDISI
GEOMATRIX CONSULTANTS
2101 WEBSTER STREET
OAKLAND, CA 94612

19 April 2002

Re: Proposed transport route for HBPP ISFSI

DR. MAKDISI:

As a followup to my letter to you dated 21 March 2002 regarding preparation of preliminary transport route stability calculations for HBPP ISFSI, please find attached one copy of a memo dated 28 March 2002 from Roy Willis to myself and attached figure showing the proposed transport route. Please use this figure to determine location of transporter load.

Also attached is a portion of a figure from an approved PG&E drawing showing the configuration of the discharge canal as constructed adjacent to the proposed transport route. Please use this figure, in conjunction with topography shown on the figure attached to Roy Willis' memo above, to construct the transport route cross section for stability analysis. As shown on the figure, the canal slopes were excavated at a slope of 2 horizontal to 1 vertical to a depth of elevation -6 (MLLW). The width of the canal bottom is shown as 20 feet.

If you have any questions, please call.

Rob White

ROBERT K. WHITE

Attachments

cc: Larry Pulley (w/ attachments)

Memorandum

Date: March 28, 2002 File #: 72.10.05
To: Robert White
From: Roy Willis, Project Manager
Subject: Humboldt Bay ISFSI Project
Transmittal of Transport Route Layout

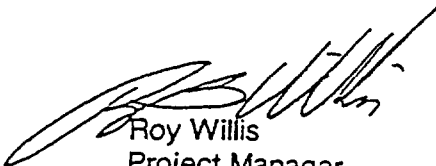


Dear Rob,

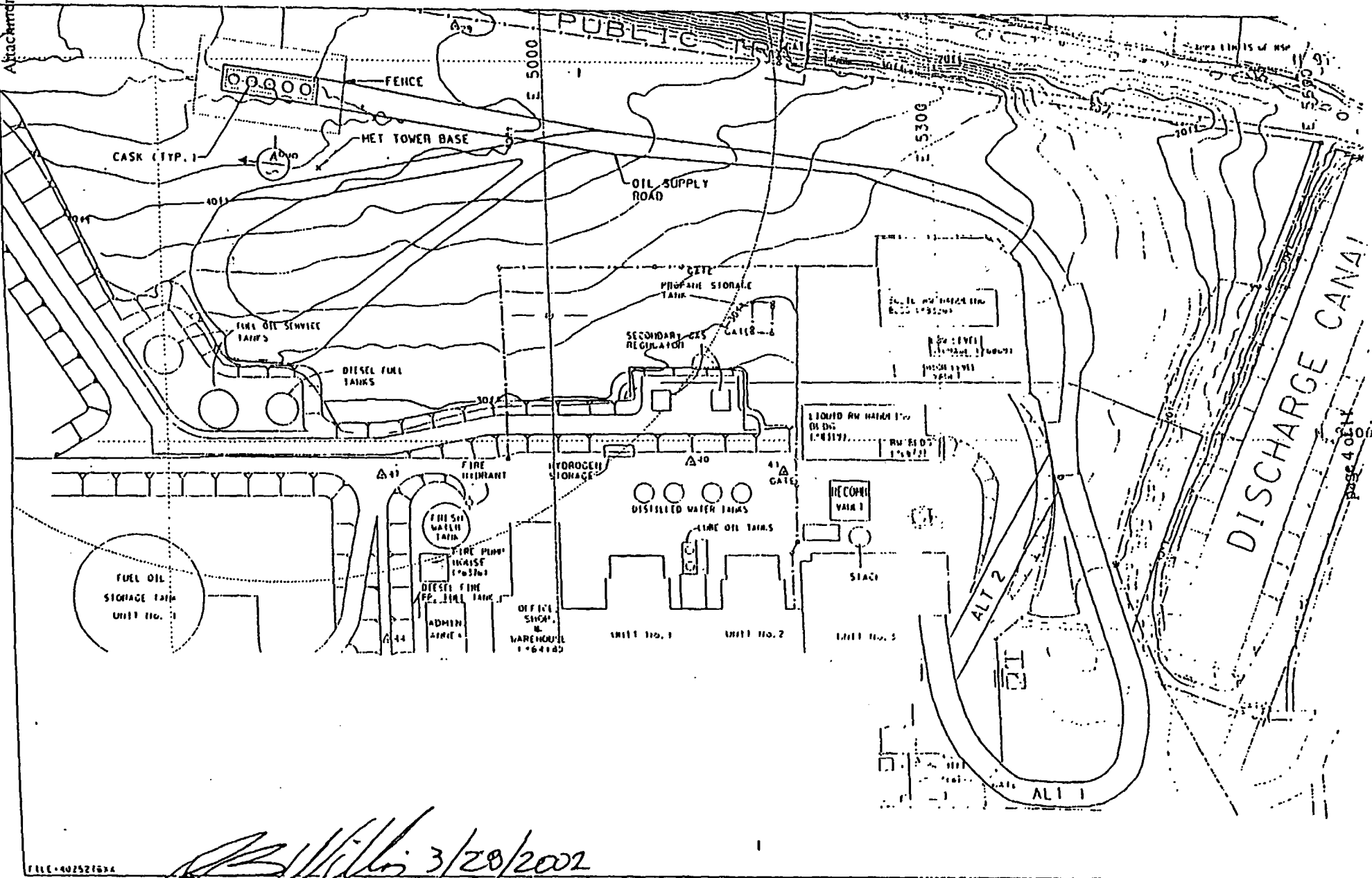
Attached for your use in slope stability investigations concerning the transport route for the Humboldt Bay ISFSI is a transport route layout showing two proposed alternatives.

The existing roadway near the discharge canal is preferred (shown as Alt 1). This roadway is 20 feet wide, and is constrained by the canal on the east and the Unit 3 hillside on the west. The alternate route using a modified roadway inside the Unit 3 restricted area is the second choice (shown as Alt 2). The exact location of the connection of this route to the existing roadway is somewhat flexible, but would be within 20 feet of the plotted location due to the physical constraints of the site.

Please contact Mr. L. Pulley if you have any questions or need additional information on this matter.


Roy Willis
Project Manager
Humboldt Bay ISFSI Project

cc: LBPulley HBPP
HBIP File No. 72.10.05



FILE 40252634

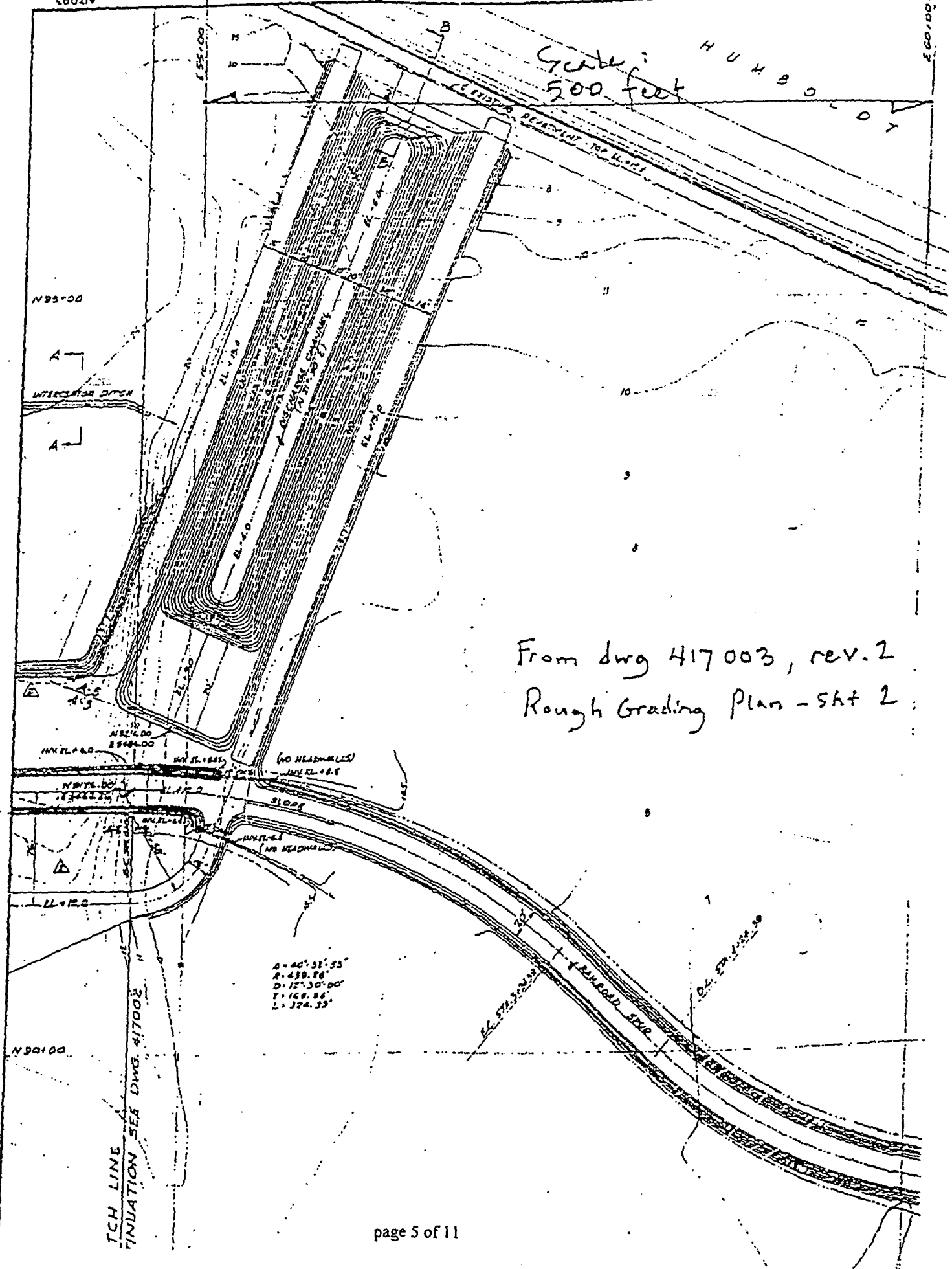
RB Willis 3/28/2002

417003

417003

Center: 500 feet

HUMBOLDT



10110 01/2 5 15:17:40



FAIZ MAKDISI
GEOMATRIX CONSULTANTS
2101 WEBSTER STREET
OAKLAND, CA 94612

1 May 2002

Re: Transmittal of boring logs from previous investigations at HBPP

DR. MAKDISI:

Please find enclosed the following items:

- Logs for borings 1 through 10A performed in 1973, including boring log key, (14 pages total) from Dames and Moore report entitled "Evaluation of Liquefaction Potential, Humboldt Bay Power Power Plant, for the Pacific Gas and Electric Company," dated May, 1974 (cover of report precedes boring logs).
- 2-page excerpt from boring P-4 performed in 1976, from Earth Sciences Associates report entitled "Humboldt Bay Power Plant Site, Geology Investigation, Appendix F III," dated 1976-1977 (cover of report precedes boring log).
- Figure E-29 from Woodward-Clyde Consultants report entitled "Evaluation of the Potential for Resolving the Geologic and Seismic Issues at the Humboldt Bay Power Plant Unit No. 3, Appendixes," dated October 1, 1980 (cover of report precedes figure).
- Logs for borings CH-4 (16 pages) and CH-5 (28 pages) summarized on Figure E-29, above. Originals of these logs are located in box 24521 at PG&E's Records Center.

Locations of these borings are shown on Figure 4-2 of the Humboldt Bay Power Plant ISFSI Site Seismic Hazards Analysis, Section 4.0, Site Geology, transmitted to me on 18 March 2002 by Bert Swan and John Wesling.

If you have any questions, please call.

A handwritten signature in black ink that reads "Rob White". The signature is written in a cursive, slightly slanted style.

ROBERT K. WHITE

Attachments



FAIZ MAKDISI
GEOMATRIX CONSULTANTS
2101 WEBSTER STREET
OAKLAND, CA 94612

29 July 2002

Re: Transmittal of preliminary ground motions for Humboldt ISFSI Project slope stability analyses

Dear Faiz:

Please find enclosed a CD with four sets of time histories (fault parallel and fault normal components) for use in Humboldt ISFSI slope stability analyses. These time histories are preliminary until otherwise noted, but you are authorized to proceed with their use in your analyses.

As described in the readme.txt file on the CD, the CD was assembled from the following sources:

fault parallel component of Set 1, Set 3, and Set 4

C:\hbpp\motions\7-24-02\Source\set1_fp.acc

C:\hbpp\motions\7-24-02\Source\set3_fp.acc

C:\hbpp\motions\7-24-02\Source\set4_fp.acc

fault parallel component of Set 2a

C:\hbpp\motions\7-26-02\Source\set2a_fp.acc

fault normal component with fling of Set 1, Set 2a, Set 3, and Set 4

C:\hbpp\motions\7-26-02\Source\set1_fn_fling_bc.acc

C:\hbpp\motions\7-26-02\Source\set2a_fn_fling_bc.acc

C:\hbpp\motions\7-26-02\Source\set3_fn_fling_bc.acc

C:\hbpp\motions\7-26-02\Source\set4_fn_fling_bc.acc

Transmittal of preliminary ground motions

Faiz Makdisi
GEO.HBIP.02.08 R
Attachme

Let me know if you have any questions.

Rob White

ROBERT K. WHITE

Enclosure

cc: Larry Pulley w/o



FAIZ MAKDISI
GEOMATRIX CONSULTANTS
2101 WEBSTER STREET
OAKLAND, CA 94612

15 November 2002

Re: Excerpt from Humboldt Bay Power Plant December 1985 TPCA HAR

FAIZ MAKDISI:

Please find attached a 9-page excerpt from the Humboldt Bay Power Plant December 1985 Toxic Pits Cleanup Act Hydrogeologic Assessment Report for your use as needed in the preparation of slope stability calculations for the HBIP. The excerpt includes a discussion of water levels as determined from monitoring wells installed in the vicinity of the wastewater holding ponds located east of the discharge canal. Page 4-7, in particular, states that "water levels ... range between 4 and 7 feet below ground surface," and that "this zone appears to respond only slightly to tidal cycles."

If you have any questions regarding this attachment, please call.

Thanks.

A handwritten signature in black ink that reads 'Rob White'. The signature is written in a cursive, slightly slanted style.

ROB WHITE

Attachment



FAIZ MAKDISI
GEOMATRIX CONSULTANTS
2101 WEBSTER STREET
OAKLAND, CA 94612

27 November 2002

Re: Transmittal of final approved time histories for Humboldt ISFSI Project slope stability analyses

Dear Faiz:

Please find enclosed a CD with four sets of time histories (fault parallel and fault normal components) for use in Humboldt ISFSI slope stability analyses. These time histories are final and approved as developed in Calculation GEO.HBIP.02.05 and are identical to those provided previously (in my 29 July 2002 letter to you) for your use in your analyses.

The CD includes the following files:

fault parallel components
set1_fp.acc
set2_fp.acc
set3_fp.acc
set4_fp.acc

fault normal components
set1_fnf.acc
set2_fnf.acc
set3_fnf.acc
set4_fnf.acc

Please verify that these time histories are the same as those used in your analyses.

Let me know if you have any questions.

Rob White

ROBERT K. WHITE

Enclosure

cc: Larry Pulley w/o

Attachment B

UTEXAS4

Input and Output Excerpts

(see Table 8-3 for listing of files)

transport3.txt

GRA
HEADING follows -
EST. OF YIELD ACC. (Static Loading, Search)
HBPP ISFSI - Transport Road

PROFILE line data follow -

1 1 Silty clay
-330 -33
40 -33

2 2 Clayey sand
-330 -12
40 -12

3 3 Silty sandy clay (sat)
-330 4
-120 4
-100 -6
-80 -6
-60 4
40 4

4 4 Silty sandy clay (unsat)
-330 6
-124 6
-120 4

5 5 Silty sandy clay (weaker)
-330 11.7
-295 11.7
-283 20
-251 20
-235 22
-195 22
-165 20
-154 13
-138 13
-124 6

6 4 Silty sandy clay (unsat) - II
-60 4
-56 6
40 6

7 5 Silty sandy clay (weaker)
-56 6
-42 13
-26 13
-20 9
40 9

MATERIAL property data follow (for first stage)

1 Silty clay
128 = unit weight
Conventional shear strengths
0 30
Piezometric Line
1

2 Clayey sand
128 = unit weight
Conventional shear strengths
0 37
Piezometric Line
1

3 Silty sandy clay (sat)
125 = unit weight
Conventional shear strength
0 30
Piezometric Line
1

4 Silty sandy clay (unsat)
125 = unit weight
Conventional shear strength

transport3.txt

0 30
No pore pressures
5 Silty sandy clay
125 = unit weight
Conventional shear strength
0 30
No pore pressures

PIEzometric line data follow -
1 Piezometric Line

-330	6
-124	6
-100	-6
-80	-6
-56	6
40	6

DIS SURface pressures to follow

-330	11.7	0.0	0
-295	11.7	0.0	0
-283	20	0.0	0
-251	20	0.0	0
-235	22	0.0	0
-218	22	0.0	0
-218	22	800.0	0
-196	22	800.0	0
-196	22	0.0	0
-195	22	0.0	0
-165	20	0.0	0
-154	13	0.0	0
-138	13	0.0	0
-124	6	0.0	0
-120	4	0.0	0
-100	-6	0.0	0
-80	-6	0.0	0
-60	4	0.0	0
-56	6	0.0	0
-42	13	0.0	0
-26	13	0.0	0
-20	9	0.0	0
40	9	0.0	0

ANALysis/computation data follow -

Circle Search 2
50 50
-186.0 152.0
-186.0 52.0
-86.0 52.0
-86.0 152.0
5 331.1
Point
-218.0 22.0

COMpute

TABLE NO. 1

COMPUTER PROGRAM DESIGNATION: UTEXAS4

Originally Coded By Stephen G. Wright

Version No. 4.0.0.8 - Last Revision Date: 07/27/2001

(C) Copyright 1985-2000 S. G. Wright - All rights reserved

```

*****
* RESULTS OF COMPUTATIONS PERFORMED USING THIS SOFTWARE *
* SHOULD NOT BE USED FOR DESIGN PURPOSES UNLESS THEY HAVE *
* BEEN VERIFIED BY INDEPENDENT ANALYSES, EXPERIMENTAL DATA *
* OR FIELD EXPERIENCE. THE USER SHOULD UNDERSTAND THE ALGORITHMS *
* AND ANALYTICAL PROCEDURES USED IN THIS SOFTWARE AND MUST HAVE *
* READ ALL DOCUMENTATION FOR THIS SOFTWARE BEFORE ATTEMPTING *
* TO USE IT. NEITHER SHINOAK SOFTWARE NOR STEPHEN G. WRIGHT *
* MAKE OR ASSUME LIABILITY FOR ANY WARRANTIES, EXPRESSED OR *
* IMPLIED, CONCERNING THE ACCURACY, RELIABILITY, USEFULNESS *
* OR ADAPTABILITY OF THIS SOFTWARE. *
*****

```

UTEXAS4 S/N:00107 - Version: 4.0.0.8 - Latest Revision: 07/27/2001

Licensed for use by: Larry Scheibel, Geomatrix Consultants

Time and date of run: Wed Sep 11 09:41:51 2002

Name of input data file: L:\Project\5000s\5117.015\Slope

Stability\UTexas4\transport road\transport3.txt

EST. OF YIELD ACC. (Static Loading, Search)

HBPP ISFSI - Transport Road

TABLE NO. 3

```

*****
* NEW PROFILE LINE DATA *
*****

```

```

-----
---- Profile Line No. 1 - Material Type (Number): 1 ----
-----

```

Description: Silty clay

Point	X	Y
1	-330.00	-33.00
2	40.00	-33.00

```

-----
---- Profile Line No. 2 - Material Type (Number): 2 ----
-----

```

Description: Clayey sand

Point	X	Y
1	-330.00	-12.00
2	40.00	-12.00

```

-----
---- Profile Line No. 3 - Material Type (Number): 3 ----
-----

```

Description: Silty sandy clay (sat)

UTEXAS4 S/N:00107 - Version: 4.0.0.8 - Latest Revision: 07/27/2001
Licensed for use by: Larry Scheibel, Geomatrix Consultants
Time and date of run: Wed Sep 11 09:41:51 2002
Name of input data file: L:\Project\5000s\5117.015\Slope
Stability\UTexas4\transport road\transport3.txt

EST. OF YIELD ACC. (Static Loading, Search)
HBPP ISFSI - Transport Road

TABLE NO. 38

* FINAL SUMMARY OF COMPUTATIONS WITH FIXED-GRID *

Number of circles attempted: 2500
Number of circles for which F calculated: 2165
Circle with Lowest Factor of Safety:
 X coordinate for center: -122.73
 Y coordinate for center: 139.76
 Radius of circle: 151.465
Factor of safety: 1.732
Side force inclination: -13.70
Time Required for Computations: 108.0 seconds

transport3(dyn).txt

GRA
HEAding follows -
EST. OF YIELD ACC. (Dynamic Loading)
HBPP ISFSI - Transport Road

PROfile line data follow -

1 1 Silty clay
-330 -33
40 -33

2 2 Clayey sand
-330 -12
40 -12

3 3 Silty sandy clay (sat)
-330 4
-120 4
-100 -6
-80 -6
-60 4
40 4

4 4 Silty sandy clay (unsat)
-330 6
-124 6
-120 4

5 5 Silty sandy clay (weaker)
-330 11.7
-295 11.7
-283 20
-251 20
-235 22
-195 22
-165 20
-154 13
-138 13
-124 6

6 4 Silty sandy clay (unsat) - II
-60 4
-56 6
40 6

7 5 Silty sandy clay (weaker)
-56 6
-42 13
-26 13
-20 9
40 9

MATERial property data follow (for first stage)

1 Silty clay
128 = unit weight
Conventional shear strengths
0 30
Piezometric Line
1

2 Clayey sand
128 = unit weight
Conventional shear strengths
0 37
Piezometric Line
1

3 Silty sandy clay (sat)
125 = unit weight
Conventional shear strength
0 30
Piezometric Line
1

4 Silty sandy clay (unsat)
125 = unit weight
Conventional shear strength

transport3(dyn).txt

GRA
HEAding follows -
EST. OF YIELD ACC. (Dynamic Loading)
HBPP ISFSI - Transport Road

PROfile line data follow -

1 1 Silty clay
-330 -33
40 -33

2 2 Clayey sand
-330 -12
40 -12

3 3 Silty sandy clay (sat)
-330 4
-120 4
-100 -6
-80 -6
-60 4
40 4

4 4 Silty sandy clay (unsat)
-330 6
-124 6
-120 4

5 5 Silty sandy clay (weaker)
-330 11.7
-295 11.7
-283 20
-251 20
-235 22
-195 22
-165 20
-154 13
-138 13
-124 6

6 4 Silty sandy clay (unsat) - II
-60 4
-56 6
40 6

7 5 Silty sandy clay (weaker)
-56 6
-42 13
-26 13
-20 9
40 9

MATerial property data follow (for first stage)

1 Silty clay
128 = unit weight
Conventional shear strengths
0 30
Piezometric Line
1

2 Clayey sand
128 = unit weight
Conventional shear strengths
0 37
Piezometric Line
1

3 Silty sandy clay (sat)
125 = unit weight
Conventional shear strength
0 30
Piezometric Line
1

4 Silty sandy clay (unsat)
125 = unit weight
Conventional shear strength

transport3(dyn).txt

125 = unit weight
Conventional shear strength
900 0
No pore pressures

PIEZOMETRIC line data follow -
1 Piezometric Line

-330	6
-124	6
-100	-6
-80	-6
-56	6
40	6

DIS SURFACE pressures to follow

-330	11.7	0.0	0
-295	11.7	0.0	0
-283	20	0.0	0
-251	20	0.0	0
-235	22	0.0	0
-218	22	0.0	0
-218	22	800.0	0
-196	22	800.0	0
-196	22	0.0	0
-195	22	0.0	0
-165	20	0.0	0
-154	13	0.0	0
-138	13	0.0	0
-124	6	0.0	0
-120	4	0.0	0
-100	-6	0.0	0
-80	-6	0.0	0
-60	4	0.0	0
-56	6	0.0	0
-42	13	0.0	0
-26	13	0.0	0
-20	9	0.0	0
40	9	0.0	0

ANALYSIS/computation data follow -
Circle

-122.73 139.76 151.465

TWO-stage computations

SEISMIC COEFFICIENT follows -
0.0

COMPUTE

HEADING follows -

SEISMIC COEFFICIENT = 0.60g

ANALYSIS/computation data follow -
Circle

-122.73 139.76 151.465

TWO-stage computations

SEISMIC COEFFICIENT follows -
0.60

COMPUTE

HEADING follows -

SEISMIC COEFFICIENT = 0.68g

ANALYSIS/computation data follow -
Circle

-122.73 139.76 151.465

TWO-stage computations

SEISMIC COEFFICIENT follows -
0.68

COMPUTE

HEADING follows -

SEISMIC COEFFICIENT = 0.69g

ANALYSIS/computation data follow -

transport3 (dyn) .txt

Circle
-122.73 139.76 151.465
TWO-stage computations
SEISMIC COEFFICIENT follows -
0.69

COMpute
HEAding follows -
SEISMIC COEFFICIENT = 0.70g

ANALYSIS/computation data follow -
Circle
-122.73 139.76 151.465
TWO-stage computations
SEISMIC COEFFICIENT follows -
0.70

COMpute
HEAding follows -
SEISMIC COEFFICIENT = 0.71g

ANALYSIS/computation data follow -
Circle
-122.73 139.76 151.465
TWO-stage computations
SEISMIC COEFFICIENT follows -
0.71

COMpute
HEAding follows -
SEISMIC COEFFICIENT = 0.74g

ANALYSIS/computation data follow -
Circle
-122.73 139.76 151.465
TWO-stage computations
SEISMIC COEFFICIENT follows -
0.74

COMpute
HEAding follows -
SEISMIC COEFFICIENT = 0.75g

ANALYSIS/computation data follow -
Circle
-122.73 139.76 151.465
TWO-stage computations
SEISMIC COEFFICIENT follows -
0.75

COMpute
HEAding follows -
SEISMIC COEFFICIENT = 0.78g

ANALYSIS/computation data follow -
Circle
-122.73 139.76 151.465
TWO-stage computations
SEISMIC COEFFICIENT follows -
0.78

COMpute
HEAding follows -
SEISMIC COEFFICIENT = 0.80g

ANALYSIS/computation data follow -
Circle
-122.73 139.76 151.465
TWO-stage computations
SEISMIC COEFFICIENT follows -
0.80

COMpute
HEAding follows -

transport3 (dyn) .txt

SEISMIC COEFFICIENT = 0.83g

ANALYSIS/computation data follow -
Circle

-122.73 139.76 151.465

TWO-stage computations

SEISMIC COEFFICIENT follows -
0.83

COMPUTE

HEADING follows -

SEISMIC COEFFICIENT = 0.84g

ANALYSIS/computation data follow -
Circle

-122.73 139.76 151.465

TWO-stage computations

SEISMIC COEFFICIENT follows -
0.84

COMPUTE

HEADING follows -

SEISMIC COEFFICIENT = 0.85g

ANALYSIS/computation data follow -
Circle

-122.73 139.76 151.465

TWO-stage computations

SEISMIC COEFFICIENT follows -
0.85

COMPUTE

HEADING follows -

SEISMIC COEFFICIENT = 0.90g

ANALYSIS/computation data follow -
Circle

-122.73 139.76 151.465

TWO-stage computations

SEISMIC COEFFICIENT follows -
0.90

COMPUTE

TABLE NO. 1

COMPUTER PROGRAM DESIGNATION: UTEXAS4
 Originally Coded By Stephen G. Wright
 Version No. 4.0.0.8 - Last Revision Date: 07/27/2001
 (C) Copyright 1985-2000 S. G. Wright - All rights reserved

 * RESULTS OF COMPUTATIONS PERFORMED USING THIS SOFTWARE *
 * SHOULD NOT BE USED FOR DESIGN PURPOSES UNLESS THEY HAVE *
 * BEEN VERIFIED BY INDEPENDENT ANALYSES, EXPERIMENTAL DATA *
 * OR FIELD EXPERIENCE. THE USER SHOULD UNDERSTAND THE ALGORITHMS *
 * AND ANALYTICAL PROCEDURES USED IN THIS SOFTWARE AND MUST HAVE *
 * READ ALL DOCUMENTATION FOR THIS SOFTWARE BEFORE ATTEMPTING *
 * TO USE IT. NEITHER SHINOAK SOFTWARE NOR STEPHEN G. WRIGHT *
 * MAKE OR ASSUME LIABILITY FOR ANY WARRANTIES, EXPRESSED OR *
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 * OR ADAPTABILITY OF THIS SOFTWARE. *

UTEXAS4 S/N:00107 - Version: 4.0.0.8 - Latest Revision: 07/27/2001
 Licensed for use by: Larry Scheibel, Geomatrix Consultants
 Time and date of run: Wed Sep 11 09:41:51 2002
 Name of input data file: L:\Project\5000s\5117.015\Slope
 Stability\UTexas4\transport road\transport3(dyn).txt

EST. OF YIELD ACC. (Dynamic Loading)
 HBPP ISFSI - Transport Road

TABLE NO. 3

 * NEW PROFILE LINE DATA *

 ----- Profile Line No. 1 - Material Type (Number): 1 -----

Description: Silty clay

Point	X	Y
1	-330.00	-33.00
2	40.00	-33.00

 ----- Profile Line No. 2 - Material Type (Number): 2 -----

Description: Clayey sand

Point	X	Y
1	-330.00	-12.00
2	40.00	-12.00

 ----- Profile Line No. 3 - Material Type (Number): 3 -----

Description: Silty sandy clay (sat)

Attachment C

Excel spreadsheets for rotation of ground motions

Input and Output Excerpts

(see Table 8-4 for listing of files)

Time history matched to spectrum:::SetTarget:syn_soil_fn.target with fling
15999 0.0050

-0.229294E-03	-0.223550E-03	-0.229094E-03	-0.223487E-03	-0.229147E-03
-0.223613E-03	-0.229336E-03	-0.223855E-03	-0.229787E-03	-0.224390E-03
-0.230386E-03	-0.225157E-03	-0.231215E-03	-0.226102E-03	-0.232339E-03
-0.227288E-03	-0.233588E-03	-0.228632E-03	-0.235142E-03	-0.230249E-03
-0.236864E-03	-0.232066E-03	-0.238817E-03	-0.234145E-03	-0.241022E-03
-0.236413E-03	-0.243395E-03	-0.238807E-03	-0.245884E-03	-0.241495E-03
-0.248729E-03	-0.244246E-03	-0.251533E-03	-0.247175E-03	-0.254651E-03
-0.250273E-03	-0.257843E-03	-0.253486E-03	-0.261235E-03	-0.256783E-03
-0.264584E-03	-0.260206E-03	-0.268007E-03	-0.263681E-03	-0.271630E-03
-0.267283E-03	-0.275294E-03	-0.270832E-03	-0.278990E-03	-0.274559E-03
-0.282823E-03	-0.278402E-03	-0.286781E-03	-0.282455E-03	-0.291013E-03
-0.286592E-03	-0.295402E-03	-0.291181E-03	-0.300190E-03	-0.296126E-03
-0.305524E-03	-0.301670E-03	-0.311519E-03	-0.307897E-03	-0.318397E-03
-0.315247E-03	-0.326303E-03	-0.323762E-03	-0.335701E-03	-0.333895E-03
-0.346936E-03	-0.346075E-03	-0.360218E-03	-0.360523E-03	-0.376252E-03
-0.377984E-03	-0.395456E-03	-0.398869E-03	-0.418462E-03	-0.423901E-03
-0.445783E-03	-0.453595E-03	-0.478207E-03	-0.488927E-03	-0.516931E-03
-0.530885E-03	-0.562637E-03	-0.580529E-03	-0.616681E-03	-0.639193E-03
-0.680458E-03	-0.708262E-03	-0.755459E-03	-0.789637E-03	-0.843743E-03
-0.884872E-03	-0.946706E-03	-0.996004E-03	-0.106645E-02	-0.112451E-02
-0.120442E-02	-0.127246E-02	-0.136307E-02	-0.144256E-02	-0.154504E-02
-0.163649E-02	-0.175178E-02	-0.185657E-02	-0.198541E-02	-0.210406E-02
-0.224728E-02	-0.238042E-02	-0.253876E-02	-0.268733E-02	-0.286132E-02
-0.302554E-02	-0.321538E-02	-0.339566E-02	-0.360104E-02	-0.379655E-02
-0.401747E-02	-0.422747E-02	-0.446183E-02	-0.468422E-02	-0.492982E-02
-0.516166E-02	-0.541544E-02	-0.565526E-02	-0.591629E-02	-0.616168E-02
-0.642670E-02	-0.667408E-02	-0.693941E-02	-0.718543E-02	-0.744709E-02
-0.768743E-02	-0.794174E-02	-0.817253E-02	-0.841529E-02	-0.863254E-02
-0.886018E-02	-0.906052E-02	-0.926999E-02	-0.945059E-02	-0.963823E-02
-0.979415E-02	-0.995543E-02	-0.100840E-01	-0.102163E-01	-0.103145E-01
-0.104158E-01	-0.104819E-01	-0.105503E-01	-0.105828E-01	-0.106164E-01
-0.106143E-01	-0.106122E-01	-0.105744E-01	-0.105387E-01	-0.104666E-01
-0.104049E-01	-0.103237E-01	-0.102604E-01	-0.101772E-01	-0.101120E-01
-0.100269E-01	-0.995858E-02	-0.986912E-02	-0.979552E-02	-0.970049E-02
-0.962132E-02	-0.952000E-02	-0.943348E-02	-0.932491E-02	-0.923177E-02
-0.911617E-02	-0.901673E-02	-0.889766E-02	-0.879676E-02	-0.867611E-02
-0.857227E-02	-0.844963E-02	-0.834400E-02	-0.821873E-02	-0.811415E-02
-0.799109E-02	-0.788357E-02	-0.775852E-02	-0.765436E-02	-0.752993E-02
-0.742220E-02	-0.729536E-02	-0.718669E-02	-0.705691E-02	-0.694225E-02
-0.680785E-02	-0.669035E-02	-0.655364E-02	-0.643793E-02	-0.630227E-02
-0.618394E-02	-0.605374E-02	-0.594674E-02	-0.582127E-02	-0.571606E-02
-0.559048E-02	-0.547319E-02	-0.532766E-02	-0.519778E-02	-0.505088E-02
-0.492677E-02	-0.479185E-02	-0.468349E-02	-0.456200E-02	-0.446215E-02
-0.434717E-02	-0.426170E-02	-0.416951E-02	-0.409738E-02	-0.400697E-02
-0.392759E-02	-0.380086E-02	-0.366709E-02	-0.350959E-02	-0.337151E-02
-0.321811E-02	-0.310082E-02	-0.298585E-02	-0.289639E-02	-0.278173E-02
-0.266854E-02	-0.251629E-02	-0.237170E-02	-0.221641E-02	-0.209618E-02
-0.196766E-02	-0.186455E-02	-0.175294E-02	-0.166631E-02	-0.156121E-02
-0.147448E-02	-0.137473E-02	-0.131026E-02	-0.123749E-02	-0.117680E-02
-0.109511E-02	-0.103207E-02	-0.936637E-03	-0.829810E-03	-0.675218E-03
-0.552515E-03	-0.438832E-03	-0.316318E-03	-0.146984E-03	-0.181598E-04
0.129649E-03	0.291706E-03	0.476160E-03	0.620776E-03	0.764238E-03
0.883014E-03	0.102947E-02	0.114212E-02	0.122014E-02	0.123253E-02
0.122738E-02	0.116480E-02	0.115399E-02	0.122255E-02	0.132640E-02
0.137092E-02	0.145429E-02	0.154784E-02	0.164371E-02	0.171542E-02

Time history matched to spectrum:::SetTarget:syn_soil_fp.target
 15999 0.005
 0.8463494E-04 0.8557436E-04 0.8446420E-04 0.8533738E-04 0.8411581E-04
 0.8502627E-04 0.8378128E-04 0.8468197E-04 0.8343122E-04 0.8425167E-04
 0.8302161E-04 0.8380364E-04 0.8248642E-04 0.8320599E-04 0.8191102E-04
 0.8264518E-04 0.8125173E-04 0.8194326E-04 0.8053489E-04 0.8118348E-04
 0.7973206E-04 0.8037340E-04 0.7888639E-04 0.7946053E-04 0.7788648E-04
 0.7841137E-04 0.7684257E-04 0.7728882E-04 0.7561302E-04 0.7591857E-04
 0.7417986E-04 0.7439942E-04 0.7249483E-04 0.7255279E-04 0.7053700E-04
 0.7043326E-04 0.6816033E-04 0.6784354E-04 0.6535441E-04 0.6472483E-04
 0.6190810E-04 0.6094987E-04 0.5778150E-04 0.5626687E-04 0.5254105E-04
 0.5051518E-04 0.4619401E-04 0.4333875E-04 0.3828163E-04 0.3461682E-04
 0.2858950E-04 0.2392414E-04 0.1690374E-04 0.1126713E-04 0.3187306E-05
 -0.3637756E-05 -0.1279803E-04 -0.2078118E-04 -0.3123907E-04 -0.4073107E-04
 -0.5277447E-04 -0.6404075E-04 -0.7787955E-04 -0.9109884E-04 -0.1069015E-03
 -0.1221885E-03 -0.1402065E-03 -0.1579095E-03 -0.1782679E-03 -0.1984070E-03
 -0.2213169E-03 -0.2441649E-03 -0.2698678E-03 -0.2955718E-03 -0.3242673E-03
 -0.3532368E-03 -0.3851977E-03 -0.4176312E-03 -0.4530162E-03 -0.4890091E-03
 -0.5280261E-03 -0.5677465E-03 -0.6103755E-03 -0.6539085E-03 -0.7003594E-03
 -0.7478289E-03 -0.7983329E-03 -0.8499182E-03 -0.9044437E-03 -0.9602386E-03
 -0.1018891E-02 -0.1079022E-02 -0.1142305E-02 -0.1207374E-02 -0.1275487E-02
 -0.1345596E-02 -0.1418949E-02 -0.1494517E-02 -0.1573446E-02 -0.1654789E-02
 -0.1739598E-02 -0.1827031E-02 -0.1918140E-02 -0.2011863E-02 -0.2109376E-02
 -0.2210145E-02 -0.2314694E-02 -0.2422497E-02 -0.2534396E-02 -0.2649748E-02
 -0.2769102E-02 -0.2892130E-02 -0.3019359E-02 -0.3150787E-02 -0.3286731E-02
 -0.3426864E-02 -0.3571102E-02 -0.3719226E-02 -0.3871234E-02 -0.4026382E-02
 -0.4184691E-02 -0.4345204E-02 -0.4507923E-02 -0.4671691E-02 -0.4835869E-02
 -0.4999743E-02 -0.5163826E-02 -0.5328225E-02 -0.5492403E-02 -0.5656381E-02
 -0.5820045E-02 -0.5982028E-02 -0.6142636E-02 -0.6300525E-02 -0.6455998E-02
 -0.6607797E-02 -0.6755909E-02 -0.6898678E-02 -0.7036617E-02 -0.7167940E-02
 -0.7293058E-02 -0.7410626E-02 -0.7520950E-02 -0.7622443E-02 -0.7715967E-02
 -0.7799935E-02 -0.7875399E-02 -0.7940456E-02 -0.7996180E-02 -0.8041088E-02
 -0.8075907E-02 -0.8099290E-02 -0.8112594E-02 -0.8114232E-02 -0.8105590E-02
 -0.8084979E-02 -0.8053961E-02 -0.8010880E-02 -0.7958033E-02 -0.7893836E-02
 -0.7824610E-02 -0.7753914E-02 -0.7683836E-02 -0.7612195E-02 -0.7540554E-02
 -0.7467642E-02 -0.7395160E-02 -0.7320568E-02 -0.7245041E-02 -0.7167100E-02
 -0.7088623E-02 -0.7007742E-02 -0.6926020E-02 -0.6842188E-02 -0.6757527E-02
 -0.6670754E-02 -0.6583259E-02 -0.6493767E-02 -0.6403320E-02 -0.6310259E-02
 -0.6215926E-02 -0.6119610E-02 -0.6022443E-02 -0.5923081E-02 -0.5822670E-02
 -0.5720358E-02 -0.5617216E-02 -0.5512174E-02 -0.5406408E-02 -0.5298845E-02
 -0.5190769E-02 -0.5080278E-02 -0.4969461E-02 -0.4855399E-02 -0.4741853E-02
 -0.4626321E-02 -0.4508679E-02 -0.4398082E-02 -0.4271200E-02 -0.4118079E-02
 -0.3987627E-02 -0.3871570E-02 -0.3747103E-02 -0.3624327E-02 -0.3502800E-02
 -0.3379603E-02 -0.3258286E-02 -0.3135825E-02 -0.3014718E-02 -0.2893621E-02
 -0.2774299E-02 -0.2655723E-02 -0.2538816E-02 -0.2421499E-02 -0.2305537E-02
 -0.2189901E-02 -0.2075094E-02 -0.1958617E-02 -0.1842550E-02 -0.1727019E-02
 -0.1614312E-02 -0.1502655E-02 -0.1392688E-02 -0.1281766E-02 -0.1172115E-02
 -0.1064028E-02 -0.9599383E-03 -0.8590376E-03 -0.7611397E-03 -0.6624029E-03
 -0.5640537E-03 -0.4668804E-03 -0.3720696E-03 -0.2779623E-03 -0.1865745E-03
 -0.9504001E-04 -0.4096365E-05 0.8668201E-04 0.1747189E-03 0.2602635E-03
 0.3402798E-03 0.4177131E-03 0.4943798E-03 0.5727792E-03 0.6512741E-03
 0.7300828E-03 0.8059096E-03 0.8803830E-03 0.9508022E-03 0.1020308E-02
 0.1088755E-02 0.1155294E-02 0.1216330E-02 0.1276537E-02 0.1339359E-02
 0.1407651E-02 0.1476888E-02 0.1548214E-02 0.1618396E-02 0.1685218E-02
 0.1747315E-02 0.1810137E-02 0.1870974E-02 0.1930551E-02 0.1990012E-02
 0.2049589E-02 0.2109061E-02 0.2173878E-02 0.2240385E-02 0.2305632E-02
 0.2367928E-02 0.2433490E-02 0.2503042E-02 0.2577634E-02 0.2654631E-02

Set1:

Acceleration Time Histories

			deg
NPTS =	15999		φ
DT =	0.005		264
Time (sec)	FN Fault Normal	FP Fault Parallel	c-c' (φ rotate)
0.000	-.229294E-03	.846349E-04	.219191E-03
0.005	-.223550E-03	.855744E-04	.213380E-03
0.010	-.229094E-03	.844642E-04	.219010E-03
0.015	-.223487E-03	.853374E-04	.213343E-03
0.020	-.229147E-03	.841158E-04	.219099E-03
0.025	-.223613E-03	.850263E-04	.213500E-03
0.030	-.229336E-03	.837813E-04	.219322E-03
0.035	-.223855E-03	.846820E-04	.213777E-03
0.040	-.229787E-03	.834312E-04	.219807E-03
0.045	-.224390E-03	.842517E-04	.214354E-03
0.050	-.230386E-03	.830216E-04	.220446E-03
0.055	-.225157E-03	.838036E-04	.215164E-03
0.060	-.231215E-03	.824864E-04	.221326E-03
0.065	-.226102E-03	.832060E-04	.216166E-03
0.070	-.232339E-03	.819110E-04	.222504E-03
0.075	-.227288E-03	.826452E-04	.217404E-03
0.080	-.233588E-03	.812517E-04	.223815E-03
0.085	-.228632E-03	.819433E-04	.218814E-03
0.090	-.235142E-03	.805349E-04	.225436E-03
0.095	-.230249E-03	.811835E-04	.220502E-03
0.100	-.236864E-03	.797321E-04	.227232E-03
0.105	-.232066E-03	.803734E-04	.222393E-03
0.110	-.238817E-03	.788864E-04	.229263E-03
0.115	-.234145E-03	.794605E-04	.224556E-03
0.120	-.241022E-03	.778865E-04	.231560E-03
0.125	-.236413E-03	.784114E-04	.226922E-03
0.130	-.243395E-03	.768426E-04	.234029E-03
0.135	-.238807E-03	.772888E-04	.229420E-03
0.140	-.245884E-03	.756130E-04	.236633E-03
0.145	-.241495E-03	.759186E-04	.232236E-03
0.150	-.248729E-03	.741799E-04	.239613E-03
0.155	-.244246E-03	.743994E-04	.235131E-03
0.160	-.251533E-03	.724948E-04	.242577E-03
0.165	-.247175E-03	.725528E-04	.238237E-03
0.170	-.254651E-03	.705370E-04	.245883E-03
0.175	-.250273E-03	.704333E-04	.241540E-03
0.180	-.257843E-03	.681603E-04	.249306E-03
0.185	-.253486E-03	.678435E-04	.245006E-03
0.190	-.261235E-03	.653544E-04	.252973E-03
0.195	-.256783E-03	.647248E-04	.248611E-03
0.200	-.264584E-03	.619081E-04	.256663E-03
0.205	-.260206E-03	.609499E-04	.252410E-03
0.210	-.268007E-03	.577815E-04	.260499E-03
0.215	-.263681E-03	.562669E-04	.256355E-03
0.220	-.271630E-03	.525411E-04	.264650E-03

Time history matched to spectrum:::SetTarget:syn_soil_fn.target with fling
15999 0.0050

0.326925E-03	0.322966E-03	0.326473E-03	0.322672E-03	0.326305E-03
0.322578E-03	0.326379E-03	0.322872E-03	0.326715E-03	0.323292E-03
0.327355E-03	0.324016E-03	0.328258E-03	0.325098E-03	0.329424E-03
0.326410E-03	0.330862E-03	0.327922E-03	0.332616E-03	0.329781E-03
0.334579E-03	0.331860E-03	0.336774E-03	0.334149E-03	0.339294E-03
0.336732E-03	0.342108E-03	0.339556E-03	0.345069E-03	0.342643E-03
0.348313E-03	0.345898E-03	0.351778E-03	0.349447E-03	0.355453E-03
0.353143E-03	0.359391E-03	0.357112E-03	0.363486E-03	0.361333E-03
0.367843E-03	0.365733E-03	0.372621E-03	0.370479E-03	0.377398E-03
0.375372E-03	0.382554E-03	0.380569E-03	0.388014E-03	0.386176E-03
0.393883E-03	0.392088E-03	0.400110E-03	0.398535E-03	0.406914E-03
0.405318E-03	0.414211E-03	0.412920E-03	0.422212E-03	0.421131E-03
0.430938E-03	0.430203E-03	0.440598E-03	0.440041E-03	0.451087E-03
0.450951E-03	0.462690E-03	0.463005E-03	0.475563E-03	0.476476E-03
0.489853E-03	0.491334E-03	0.505771E-03	0.508060E-03	0.523611E-03
0.526803E-03	0.543519E-03	0.547719E-03	0.565810E-03	0.570850E-03
0.590233E-03	0.596355E-03	0.617061E-03	0.624211E-03	0.646240E-03
0.654294E-03	0.677509E-03	0.686340E-03	0.710448E-03	0.719856E-03
0.744825E-03	0.754695E-03	0.780861E-03	0.791760E-03	0.819154E-03
0.830988E-03	0.859674E-03	0.872326E-03	0.902241E-03	0.915618E-03
0.946540E-03	0.961177E-03	0.994830E-03	0.101291E-02	0.105085E-02
0.107342E-02	0.111668E-02	0.114493E-02	0.119512E-02	0.123071E-02
0.128941E-02	0.133414E-02	0.140165E-02	0.145247E-02	0.152461E-02
0.157952E-02	0.165554E-02	0.171340E-02	0.179162E-02	0.185042E-02
0.192854E-02	0.198566E-02	0.206053E-02	0.211166E-02	0.217813E-02
0.221761E-02	0.227210E-02	0.230087E-02	0.234403E-02	0.235978E-02
0.238792E-02	0.238592E-02	0.239380E-02	0.236954E-02	0.235327E-02
0.230297E-02	0.225929E-02	0.218086E-02	0.210946E-02	0.200362E-02
0.190576E-02	0.177650E-02	0.165859E-02	0.151138E-02	0.137855E-02
0.122147E-02	0.108445E-02	0.928806E-03	0.799215E-03	0.656079E-03
0.544831E-03	0.427032E-03	0.344386E-03	0.256795E-03	0.206605E-03
0.153906E-03	0.142083E-03	0.126207E-03	0.145180E-03	0.159219E-03
0.204421E-03	0.230178E-03	0.277050E-03	0.299068E-03	0.332826E-03
0.344355E-03	0.378669E-03	0.387069E-03	0.410904E-03	0.408783E-03
0.422548E-03	0.418831E-03	0.438193E-03	0.427504E-03	0.432975E-03
0.420312E-03	0.422947E-03	0.398566E-03	0.396445E-03	0.369618E-03
0.354319E-03	0.318294E-03	0.305830E-03	0.268629E-03	0.251451E-03
0.214407E-03	0.197418E-03	0.161760E-03	0.152142E-03	0.121608E-03
0.111591E-03	0.845403E-04	0.818093E-04	0.609132E-04	0.641252E-04
0.502442E-04	0.608481E-04	0.528891E-04	0.693636E-04	0.699296E-04
0.950508E-04	0.101297E-03	0.132223E-03	0.147679E-03	0.184303E-03
0.192672E-03	0.218670E-03	0.231427E-03	0.268167E-03	0.279381E-03
0.315910E-03	0.334128E-03	0.365922E-03	0.391972E-03	0.466039E-03
0.513730E-03	0.572446E-03	0.620337E-03	0.686539E-03	0.725410E-03
0.798595E-03	0.850665E-03	0.899889E-03	0.923472E-03	0.983563E-03
0.102181E-02	0.107195E-02	0.110692E-02	0.116236E-02	0.118945E-02
0.125518E-02	0.131923E-02	0.139378E-02	0.143830E-02	0.151411E-02
0.157385E-02	0.165155E-02	0.170815E-02	0.178690E-02	0.184360E-02
0.191489E-02	0.196172E-02	0.203564E-02	0.208783E-02	0.214495E-02
0.217256E-02	0.222695E-02	0.226118E-02	0.231001E-02	0.233342E-02
0.237668E-02	0.240871E-02	0.246530E-02	0.249208E-02	0.253828E-02
0.255812E-02	0.258458E-02	0.259204E-02	0.262175E-02	0.262375E-02
0.264538E-02	0.262910E-02	0.261766E-02	0.259813E-02	0.259151E-02
0.254668E-02	0.256201E-02	0.258311E-02	0.259151E-02	0.257104E-02
0.258721E-02	0.257461E-02	0.258605E-02	0.256768E-02	0.253061E-02

Time history matched to spectrum:::SetTarget:syn_soil_fp.target
 15999 0.005
 0.2646084E-04 0.2414023E-04 0.2639553E-04 0.2413792E-04 0.2645517E-04
 0.2413456E-04 0.2646861E-04 0.2424880E-04 0.2658285E-04 0.2435149E-04
 0.2669299E-04 0.2458764E-04 0.2697208E-04 0.2479638E-04 0.2721558E-04
 0.2515327E-04 0.2761962E-04 0.2554891E-04 0.2802376E-04 0.2602341E-04
 0.2856850E-04 0.2652940E-04 0.2916795E-04 0.2720760E-04 0.2987764E-04
 0.2797924E-04 0.3065664E-04 0.2878974E-04 0.3158474E-04 0.2976508E-04
 0.3258318E-04 0.3084963E-04 0.3374647E-04 0.3204337E-04 0.3495607E-04
 0.3339462E-04 0.3638502E-04 0.3478377E-04 0.3785281E-04 0.3636917E-04
 0.3946246E-04 0.3805651E-04 0.4133251E-04 0.3990336E-04 0.4321190E-04
 0.4192356E-04 0.4523946E-04 0.4397001E-04 0.4748121E-04 0.4631151E-04
 0.4981011E-04 0.4866246E-04 0.5224401E-04 0.5122236E-04 0.5482386E-04
 0.5389461E-04 0.5754651E-04 0.5670126E-04 0.6047601E-04 0.5956776E-04
 0.6334251E-04 0.6260016E-04 0.6645062E-04 0.6572821E-04 0.6947986E-04
 0.6888241E-04 0.7273391E-04 0.7208397E-04 0.7595847E-04 0.7541351E-04
 0.7925767E-04 0.7871272E-04 0.8244663E-04 0.8198778E-04 0.8578458E-04
 0.8520823E-04 0.8895779E-04 0.8845179E-04 0.9210788E-04 0.9148534E-04
 0.9507844E-04 0.9454095E-04 0.9804060E-04 0.9742960E-04 0.1008149E-03
 0.1002154E-03 0.1035240E-03 0.1029162E-03 0.1061959E-03 0.1056709E-03
 0.1089522E-03 0.1084545E-03 0.1119615E-03 0.1117053E-03 0.1153761E-03
 0.1155073E-03 0.1197336E-03 0.1206208E-03 0.1255191E-03 0.1274038E-03
 0.1334676E-03 0.1367068E-03 0.1443886E-03 0.1496964E-03 0.1595506E-03
 0.1676304E-03 0.1806451E-03 0.1921479E-03 0.2089741E-03 0.2250234E-03
 0.2469526E-03 0.2683894E-03 0.2962617E-03 0.3245329E-03 0.3595557E-03
 0.3955445E-03 0.4388412E-03 0.4835764E-03 0.5359767E-03 0.5903415E-03
 0.6527062E-03 0.7173075E-03 0.7897732E-03 0.8646330E-03 0.9471262E-03
 0.1031803E-02 0.1123384E-02 0.1216614E-02 0.1315944E-02 0.1415788E-02
 0.1520684E-02 0.1624518E-02 0.1731933E-02 0.1836607E-02 0.1942762E-02
 0.2044707E-02 0.2146137E-02 0.2241151E-02 0.2333761E-02 0.2417961E-02
 0.2497551E-02 0.2566630E-02 0.2629315E-02 0.2681175E-02 0.2725695E-02
 0.2758235E-02 0.2783434E-02 0.2796444E-02 0.2801274E-02 0.2793598E-02
 0.2778268E-02 0.2751483E-02 0.2716518E-02 0.2670727E-02 0.2620222E-02
 0.2561107E-02 0.2496312E-02 0.2423127E-02 0.2346992E-02 0.2264461E-02
 0.2183601E-02 0.2103276E-02 0.2027140E-02 0.1951540E-02 0.1881600E-02
 0.1811880E-02 0.1746454E-02 0.1682509E-02 0.1623384E-02 0.1563114E-02
 0.1505458E-02 0.1447393E-02 0.1393308E-02 0.1338078E-02 0.1285882E-02
 0.1233382E-02 0.1183287E-02 0.1128372E-02 0.1075557E-02 0.1023195E-02
 0.9729468E-03 0.9197800E-03 0.8694693E-03 0.8168286E-03 0.7669588E-03
 0.7187796E-03 0.6719653E-03 0.6206371E-03 0.5735814E-03 0.5255492E-03
 0.4747239E-03 0.4193532E-03 0.3688115E-03 0.3166737E-03 0.2644635E-03
 0.2110762E-03 0.1581720E-03 0.1045992E-03 0.6040608E-04 0.1440505E-04
 -0.3358299E-04 -0.8185432E-04 -0.1264704E-03 -0.1719091E-03 -0.2152689E-03
 -0.2663241E-03 -0.3162253E-03 -0.3654126E-03 -0.4136443E-03 -0.4572445E-03
 -0.4915218E-03 -0.5332750E-03 -0.5743657E-03 -0.6126120E-03 -0.6488527E-03
 -0.6863944E-03 -0.7236537E-03 -0.7607029E-03 -0.7886791E-03 -0.8368794E-03
 -0.9050086E-03 -0.9627103E-03 -0.1010554E-02 -0.1070769E-02 -0.1130934E-02
 -0.1196150E-02 -0.1250329E-02 -0.1284045E-02 -0.1320060E-02 -0.1370880E-02
 -0.1409950E-02 -0.1447120E-02 -0.1485771E-02 -0.1521261E-02 -0.1561906E-02
 -0.1615036E-02 -0.1657782E-02 -0.1701567E-02 -0.1747987E-02 -0.1779172E-02
 -0.1798293E-02 -0.1833678E-02 -0.1864138E-02 -0.1882618E-02 -0.1914538E-02
 -0.1965264E-02 -0.2001909E-02 -0.2034259E-02 -0.2070274E-02 -0.2110080E-02
 -0.2148930E-02 -0.2176660E-02 -0.2185690E-02 -0.2205966E-02 -0.2227071E-02
 -0.2237161E-02 -0.2260996E-02 -0.2302997E-02 -0.2327262E-02 -0.2348577E-02
 -0.2377463E-02 -0.2407282E-02 -0.2431653E-02 -0.2454543E-02 -0.2483008E-02
 -0.2511673E-02 -0.2500659E-02 -0.2477349E-02 -0.2475469E-02 -0.2472319E-02
 -0.2451004E-02 -0.2432115E-02 -0.2414055E-02 -0.2396845E-02 -0.2363770E-02

Set3:
Acceleration Time Histories

			deg
NPTS =	15999		φ
DT =	0.005		264
Time (sec)	FN Fault Normal	FP Fault Parallel	c-c' (φ rotate)
0.000	.326925E-03	.264608E-04	-.327900E-03
0.005	.322966E-03	.241402E-04	-.323720E-03
0.010	.326473E-03	.263955E-04	-.327444E-03
0.015	.322672E-03	.241379E-04	-.323427E-03
0.020	.326305E-03	.264552E-04	-.327283E-03
0.025	.322578E-03	.241346E-04	-.323334E-03
0.030	.326379E-03	.264686E-04	-.327358E-03
0.035	.322872E-03	.242488E-04	-.323638E-03
0.040	.326715E-03	.265829E-04	-.327704E-03
0.045	.323292E-03	.243515E-04	-.324066E-03
0.050	.327355E-03	.266930E-04	-.328352E-03
0.055	.324016E-03	.245876E-04	-.324811E-03
0.060	.328258E-03	.269721E-04	-.329279E-03
0.065	.325098E-03	.247964E-04	-.325909E-03
0.070	.329424E-03	.272156E-04	-.330464E-03
0.075	.326410E-03	.251533E-04	-.327251E-03
0.080	.330862E-03	.276196E-04	-.331937E-03
0.085	.327922E-03	.255489E-04	-.328796E-03
0.090	.332616E-03	.280238E-04	-.333723E-03
0.095	.329781E-03	.260234E-04	-.330695E-03
0.100	.334579E-03	.285685E-04	-.335732E-03
0.105	.331860E-03	.265294E-04	-.332815E-03
0.110	.336774E-03	.291680E-04	-.337978E-03
0.115	.334149E-03	.272076E-04	-.335162E-03
0.120	.339294E-03	.298776E-04	-.340558E-03
0.125	.336732E-03	.279792E-04	-.337812E-03
0.130	.342108E-03	.306566E-04	-.343438E-03
0.135	.339556E-03	.287897E-04	-.340705E-03
0.140	.345069E-03	.315847E-04	-.346480E-03
0.145	.342643E-03	.297651E-04	-.343877E-03
0.150	.348313E-03	.325832E-04	-.349811E-03
0.155	.345898E-03	.308496E-04	-.347228E-03
0.160	.351778E-03	.337465E-04	-.353378E-03
0.165	.349447E-03	.320434E-04	-.350882E-03
0.170	.355453E-03	.349561E-04	-.357160E-03
0.175	.353143E-03	.333946E-04	-.354699E-03
0.180	.359391E-03	.363850E-04	-.361225E-03
0.185	.357112E-03	.347838E-04	-.358792E-03
0.190	.363486E-03	.378528E-04	-.365451E-03
0.195	.361333E-03	.363692E-04	-.363155E-03
0.200	.367843E-03	.394625E-04	-.369953E-03
0.205	.365733E-03	.380565E-04	-.367707E-03
0.210	.372621E-03	.413325E-04	-.374900E-03
0.215	.370479E-03	.399034E-04	-.372621E-03
0.220	.377398E-03	.432119E-04	-.379847E-03

Set3:

15999	.00500							
-327900E-03	-323720E-03	-327444E-03	-323247E-03	-327283E-03	-323334E-03	-327358E-03	-323638E-03	
-327704E-03	-324066E-03	-328035E-03	-324811E-03	-329279E-03	-325909E-03	-330464E-03	-327251E-03	
-331937E-03	-328796E-03	-333723E-03	-330695E-03	-335732E-03	-332815E-03	-337978E-03	-335162E-03	
-340558E-03	-337812E-03	-343438E-03	-340705E-03	-346480E-03	-343877E-03	-349811E-03	-347228E-03	
-353378E-03	-350882E-03	-357160E-03	-354699E-03	-361225E-03	-358792E-03	-365451E-03	-363155E-03	
-369953E-03	-367707E-03	-374900E-03	-372621E-03	-378474E-03	-377698E-03	-385187E-03	-383080E-03	
-390852E-03	-388901E-03	-396932E-03	-395027E-03	-403179E-03	-401706E-03	-410416E-03	-408731E-03	
-417957E-03	-416585E-03	-426221E-03	-425051E-03	-431988E-03	-434390E-03	-445130E-03	-444501E-03	
-455879E-03	-455681E-03	-467758E-03	-468003E-03	-480498E-03	-481749E-03	-495454E-03	-496870E-03	
-511618E-03	-513847E-03	-529710E-03	-532824E-03	-549840E-03	-553964E-03	-572338E-03	-577286E-03	
-596938E-03	-602970E-03	-623929E-03	-620976E-03	-653238E-03	-661185E-03	-684619E-03	-693338E-03	
-717657E-03	-726958E-03	-752133E-03	-761897E-03	-788287E-03	-799099E-03	-826727E-03	-836510E-03	
-867480E-03	-880156E-03	-910419E-03	-923919E-03	-955306E-03	-970201E-03	-100447E-02	-102301E-02	
-106177E-02	-108506E-02	-112945E-02	-115874E-02	-121042E-02	-124749E-02	-130816E-02	-135489E-02	
-142494E-02	-147844E-02	-155384E-02	-161221E-02	-169234E-02	-175456E-02	-183783E-02	-190199E-02	
-198620E-02	-204976E-02	-213180E-02	-219047E-02	-226520E-02	-231331E-02	-237708E-02	-241544E-02	
-246874E-02	-249484E-02	-253379E-02	-254266E-02	-256172E-02	-254854E-02	-258452E-02	-250408E-02	
-247125E-02	-240318E-02	-234185E-02	-224539E-02	-215639E-02	-203505E-02	-192434E-02	-178336E-02	
-165591E-02	-150309E-02	-136946E-02	-121603E-02	-107656E-02	-944495E-03	-832254E-03	-722301E-03	
-626453E-03	-534555E-03	-479361E-03	-420771E-03	-402240E-03	-378801E-03	-349712E-03	-319504E-03	
-431550E-03	-448769E-03	-487426E-03	-501421E-03	-527684E-03	-531862E-03	-559149E-03	-568019E-03	
-578343E-03	-569914E-03	-577596E-03	-567830E-03	-581433E-03	-565029E-03	-565014E-03	-546933E-03	
-544317E-03	-514330E-03	-506700E-03	-474546E-03	-454079E-03	-432694E-03	-395039E-03	-352539E-03	
-330243E-03	-288065E-03	-266576E-03	-225748E-03	-211264E-03	-175877E-03	-160602E-03	-127912E-03	
-119912E-03	-936809E-04	-914179E-04	-720324E-04	-770482E-04	-635330E-04	-752978E-04	-710529E-04	
-910197E-04	-921860E-04	-118279E-04	-128901E-04	-160792E-03	-163778E-03	-184419E-03	-191963E-03	
-223460E-03	-230055E-03	-262801E-03	-276555E-03	-303880E-03	-325789E-03	-395662E-03	-439168E-03	
-493688E-03	-537424E-03	-600339E-03	-633958E-03	-696211E-03	-745374E-03	-789328E-03	-806487E-03	
-859960E-03	-891181E-03	-935183E-03	-966637E-03	-101801E-02	-103964E-02	-120092E-02	-116074E-02	
-123084E-02	-127141E-02	-134255E-02	-139641E-02	-146922E-02	-152093E-02	-159440E-02	-164753E-02	
-171643E-02	-175930E-02	-182963E-02	-187961E-02	-193308E-02	-195523E-02	-200549E-02	-203616E-02	
-208095E-02	-210007E-02	-213904E-02	-216799E-02	-222313E-02	-224784E-02	-229158E-02	-231026E-02	
-233408E-02	-233711E-02	-236412E-02	-236188E-02	-238238E-02	-236307E-02	-234914E-02	-232733E-02	
-231777E-02	-227019E-02	-228658E-02	-231001E-02	-231856E-02	-229853E-02	-231684E-02	-230628E-02	
-231955E-02	-230308E-02	-226967E-02	-221063E-02	-218344E-02	-212692E-02	-208979E-02	-203788E-02	
-200509E-02	-192840E-02	-183937E-02	-173476E-02	-166371E-02	-155412E-02	-146468E-02	-134521E-02	
-123470E-02	-116641E-02	-116920E-02	-109969E-02	-103016E-02	-991962E-03	-978316E-03	-923221E-03	
-903294E-03	-873648E-03	-736524E-03	-484194E-03	-422852E-03	-387113E-03	-268756E-03	-104850E-03	
170214E-04	148038E-03	272186E-03	426915E-03	555805E-03	683028E-03	769772E-03	892839E-03	
100588E-02	109296E-02	111254E-02	117435E-02	123618E-02	129119E-02	130788E-02	137609E-02	
146942E-02	156831E-02	155313E-02	154357E-02	162447E-02	175985E-02	179491E-02	184178E-02	
190711E-02	197923E-02	201643E-02	208446E-02	211647E-02	217033E-02	223917E-02	230064E-02	
226530E-02	226113E-02	227398E-02	227624E-02	222272E-02	220643E-02	218218E-02	212991E-02	
205482E-02	211782E-02	216222E-02	213527E-02	216134E-02	218769E-02	194632E-02	170338E-02	
159462E-02	144203E-02	116494E-02	101156E-02	900481E-03	715481E-03	576171E-03	697314E-03	
795723E-03	748888E-03	764522E-03	924022E-03	830806E-03	518478E-03	385252E-03	144191E-03	
-115642E-03	-357306E-03	-626704E-03	-902164E-03	-103783E-02	-102968E-02	-117541E-02	-141688E-02	
-162528E-02	-173326E-02	-181944E-02	-191873E-02	-211779E-02	-235126E-02	-255130E-02	-271088E-02	
-294208E-02	-311126E-02	-331231E-02	-352732E-02	-352306E-02	-331535E-02	-328114E-02	-328223E-02	
-310724E-02	-281554E-02	-285224E-02	-326228E-02	-357304E-02	-361901E-02	-386888E-02	-419710E-02	
-437096E-02	-452889E-02	-471604E-02	-465282E-02	-453217E-02	-452814E-02	-452536E-02	-438720E-02	
-432117E-02	-425797E-02	-404423E-02	-375007E-02	-354742E-02	-326995E-02	-309784E-02	-312468E-02	
-312067E-02	-298443E-01	-287645E-02	-267467E-02	-243468E-02	-223153E-02	-219541E-02	-223846E-02	
-222601E-02	-215250E-02	-214614E-02	-212461E-02	-216253E-02	-207873E-02	-181373E-02	-158913E-02	
-142832E-02	-114723E-02	-109644E-02	-121586E-02	-118234E-02	-107948E-02	-111080E-02	-111511E-02	
-112347E-02	-100437E-02	-703461E-03	-395796E-03	-283790E-03	-185080E-03	-338686E-04	-146288E-03	
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164939E-02	344034E-02	141974E-02	143242E-02	163126E-02	120542E-02	106447E-02	839401E-03	
106525E-02	165272E-02	186610E-02	200190E-02	244009E-02	284084E-02	300027E-02	312265E-02	
297301E-02	267231E-02	254056E-02	244446E-02	212940E-02	190070E-02	175114E-02	146574E-02	
122297E-02	139068E-02	157360E-02	149368E-02	139136E-02	139829E-02	127013E-02	115234E-02	
109216E-02	919265E-03	589501E-03	382878E-03	183447E-03	-126206E-03	-365526E-03	-576016E-03	
108290E-02	-110104E-02	-283132E-03	305204E-03	448701E-03	915636E-03	137916E-02	191421E-02	
258072E-02	236344E-02	143838E-02	118295E-02	116569E-02	728173E-03	316209E-03	877099E-03	
357909E-03	-663897E-03	-357418E-03	-283531E-03	-416520E-03	-366109E-03	-446713E-03	-630994E-03	
-482493E-03	-114059E-03	-222389E-03	678546E-04	336430E-03	669547E-03	813695E-03	907978E-03	
111305E-02	148792E-02	179195E-02	210215E-02	247779E-02	258691E-02	259016E-02	309152E-02	
302318E-02	185444E-02	995696E-03	630239E-03	-138432E-03	-680573E-03	-902658E-03	-130482E-03	
-186048E-02	-242849E-02	-239136E-02	-149755E-02	-115759E-02	-139471E-02	-113611E-02	-718193E-02	
-550415E-03	-153894E-03	-162294E-03	-721399E-03	-101566E-03	-100266E-03	-130392E-03	-174150E-03	
-185388E-03	-171805E-02	-194174E-02	-203260E-02	-136783E-02	-631444E-03	-335666E-03	673797E-04	
698070E-03	141479E-02	165728E-02	123723E-02	899444E-03	890612E-03	646830E-03	383654E-03	
122556E-03	-308448E-03	-151652E-03	185059E-03	221194E-03	429565E-03	908618E-03	122458E-02	
148126E-02	189044E-02	223096E-02	260540E-02	295152E-02	316351E-02	342727E-02	387806E-02	
419976E-02	456224E-02	499276E-02	494895E-02	443523E-02	410920E-02	339142E-02	227544E-02	
254712E-02	406218E-02	471974E-02	505213E-02	591798E-02	694233E-02	807455E-02	82675E-02	
655689E-02	578054E-02	608248E-02	568511E-02	479511E-02	441647E-02	427893E-02	401557E-02	
361504E-02	331239E-02	304625E-02	277129E-02	268637E-02	305859E-02	357502E-02	391051E-02	
407134E-02	454502E-02	521097E-02	505654E-02	418533E-02	390651E-02	366714E-02	316168E-02	
353262E-02	425858E-02	429460E-02	447562E-02	492132E-02	528879E-02	576321E-02	589339E-02	
542697E-02	538123E-02	556537E-02	508295E-02	641274E-02	401202E-02	348904E-02	329679E-02	
256420E-02	590587E-03	593564E-04	136843E-02	136216E-02	103555E-02	145588E-02	324309E-02	
-163438E-02	-250995E-02	-326915E-02	-410602E-02	-501580E-02	-587523E-02	-578186E-02	-560737E-02	
-596244E-02	-586494E-02	-639111E-02	-773506E-02	-875020E-02	-975904E-02	-983498E-02	-820280E-02	
-725219E-02	-731738E-02	-655456E-02	-490950E-02	-370914E-02	-353884E-02	-388361E-02	-418862E-02	
-454921E-02	-483145E-02	-512361E-02	-580562E-02	-679151E-02	-768026E-02	-837051E-02	-908420E-02	
-102941E-02	-109723E-02	-996002E-02	-907748E-02	-971565E-02	-882253E-02	-558793E-02	-346254E-02	
-263276E-02	-724110E-03	154649E-02	344270E-03	530226E-02	661559E-02	802522E-02	102216E-01	
112059E-01	119036E-01	147581E-01	164294E-01	148053E-01	140867E-01	149397E-01	148297E-01	
141159E-01	136199E-01	133472E-01	135164E-01	133360E-01	128199E-01	129120E-01	133112E-01	
131026E-01	126210E-01	126058E-01	129898E-01	127584E-01	107364E-01	997177E-02	943927E-02	
783314E-02	780057E-02	983446E-02	106726E-01	107151E-01	120482E-01	128481E-01	122170E-01	
117132E-01	113178E-01	104090E-01	980029E-01	919885E-02	785678E-02	671248E-02	637829E-02	

Attachment D

SHAKE

Input and Output Excerpts

(see Table 8-6 for listing of files)

16384	0.5						
8							
7	1	10	100.				
	11 100. #1 modulus for Clay PI 15 (Vucetic and Dobry 1991)						
0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1	0.316
1.	3.16	10.					
1.000	1.000	1.000	.94	.82	.64	.40	.21
.09	.04	.02					
	11 1. damping for Clay PI 15 (Vucetic & Dobry 1991)						
0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1	0.316
1.	3.16	10.					
1.7	1.7	1.7	2.6	4.5	7.8	11.7	16.3
20.2	23.0	23.0					
	11 100. #2 modulus for Sand (20 to 50 ft) (EPRI 1993)						
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.000	0.999	0.991	0.953	0.830	0.620	0.364	0.181
0.071	0.025	0.010					
	11 1. damping for Sand (20 to 50 ft) (EPRI 1993)						
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.250	1.300	1.455	2.080	3.750	6.925	12.600	18.905
24.840	27.2	28.9					
	11 100. #3 modulus for Sand (50 to 120 ft) (EPRI 1993)						
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.000	1.000	0.995	0.972	0.879	0.701	0.442	0.230
0.097	0.037	0.014					
	11 1. damping for Sand (50 to 120 ft) (EPRI 1993)						
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.090	1.145	1.300	1.665	2.865	5.415	10.465	16.560
22.915	25.5	27.0					
	11 100. #4 modulus for Sand (120 to 250 ft) (EPRI 1993)						
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.000	1.000	0.996	0.980	0.910	0.756	0.510	0.283
0.122	0.050	0.019					
	11 1. damping for Sand (120 to 250 ft) (EPRI 1993)						
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
0.935	0.935	1.090	1.455	2.340	4.375	8.695	14.580
21.250	23.8	25.5					
	11 100. #5 modulus for Sand (250 to 500 ft) (EPRI 1993)						
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.000	1.000	0.997	0.986	0.932	0.809	0.573	0.338
0.152	0.067	0.025					
	11 1. damping for Sand (250 to 500 ft) (EPRI 1993)						
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
0.800	0.800	0.900	1.145	1.875	3.490	7.185	12.705
19.270	22.4	24.0					
	11 100. #6 modulus for Sand (> 500 ft) (EPRI 1993)						
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.000	1.000	0.998	0.991	0.955	0.860	0.658	0.417
0.207	0.083	0.032					
	11 1. damping for Sand (> 500 ft) (EPRI 1993)						
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
0.570	0.625	0.625	0.850	1.280	2.500	5.520	10.260
16.770	20.2	22.5					

11 100. #7 modulus for Weathered Rock														
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3							
1.	3.	10.												
1.000	1.000	1.000	0.990	0.960	0.900	0.75	0.55							
0.34	0.2	0.12												
11 1. damping for Weathered Rock														
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3							
1.	3.	10.												
0.24	0.42	0.8	1.4	2.8	5.1	9.8	15.5							
21.	25.	28.												
2														
1	25	4	Transporter Route, HBPP, ISFSI, 08/2002											
1	1	1	1.0		.05	.125	915.						1.	
2	1	1	2.0		.05	.125	915.						1.	
3	1	1	3.0		.05	.125	915.						1.	
4	1	1	2.0		.05	.125	915.						1.	
5	1	1	2.0		.05	.125	915.						1.	
6	1	1	2.0		.05	.125	915.						1.	
7	1	1	2.0		.05	.125	915.						1.	
8	1	1	2.0		.05	.125	915.						1.	
9	1	1	2.0		.05	.130	1220.						1.	
10	1	1	3.0		.05	.130	1220.						1.	
11	1	1	3.0		.05	.130	1220.						1.	
12	2	1	5.0		.05	.130	1.					120.	1.	
13	2	1	4.0		.05	.130	1.					135.	1.	
14	2	1	4.0		.05	.130	1.					135.	1.	
15	2	1	4.0		.05	.130	1.					128.	1.	
16	2	1	4.0		.05	.130	1.					128.	1.	
17	1	1	5.0		.05	.130	1830.						1.	
18	1	1	5.0		.05	.130	1830.						1.	
19	3	1	5.0		.05	.130	1.					188.	1.	
20	3	1	5.0		.05	.130	1.					188.	1.	
21	3	1	5.0		.05	.130	1.					188.	1.	
22	3	1	5.0		.05	.130	1.					188.	1.	
23	3	1	5.0		.05	.130	1.					188.	1.	
24	3	1	5.0		.05	.130	1.					188.	1.	
25					.05	.130	1800.						1.	
1														
1599916384	.005	2(8E15.7) SET 1, SECTION C-C, 08/2002												
1.		2.5												
SICC.AC8														
3														
1	0													
4														
0	30	2.	0.65											
5														
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
0	1	1	1	1	1	1	1	1	1	1	1	1	1	1
1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5														
16	17	18	19	20	21	22	23	24	25	25				
1	1	1	1	1	1	1	1	1	1	0				
0	0	0	0	0	0	0	0	0	0	1				
0														


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**
** SHAKE -- A COMPUTER PROGRAM FOR **
** EARTHQUAKE RESPONSE ANALYSIS **
** OF HORIZONTALLY LAYERED SITES **
**
** MS-DOS VERSION - CONVERTED TO IBM-PC BY **
** Shyh-Shiun Lai, WCC **
** January 1985 **
**
** (Modified to Use 16384 Points and 100 **
** Soil Layers, S.J. Chiou, August 1995) **
**
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Output file name : TR1C.OUT
Start time : 19"/"/" --
Start time : 19"/"/" --

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MAX. NUMBER OF TERMS IN FOURIER TRANSFORM = 16384
NECESSARY LENGTH OF BLANK COMMON X = 102419
EARTH PRESSURE AT REST FOR SAND = 0.500
1***** OPTION 8 *** READ RELATION BETWEEN SOIL PROPERTIES AND STRAIN

```

CURVES FOR RELATION STRAIN VERSUS SHEAR MODULUS AND DAMPING

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
1	0.000100	1.000	0.000100	1.7
1	0.000316	1.000	0.000316	1.7
1	0.001000	1.000	0.001000	1.7
1	0.003160	0.940	0.003160	2.6
1	0.010000	0.820	0.010000	4.5
1	0.031600	0.640	0.031600	7.8
1	0.100000	0.400	0.100000	11.7
1	0.316000	0.210	0.316000	16.3
1	1.000000	0.090	1.000000	20.2
1	3.160000	0.040	3.160000	23.0
1	10.000000	0.020	10.000000	23.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
2	0.000100	1.000	0.000100	1.3
2	0.000300	0.999	0.000300	1.3
2	0.001000	0.991	0.001000	1.5
2	0.003000	0.953	0.003000	2.1
2	0.010000	0.830	0.010000	3.8
2	0.030000	0.620	0.030000	6.9
2	0.100000	0.364	0.100000	12.6
2	0.300000	0.181	0.300000	18.9
2	1.000000	0.071	1.000000	24.8
2	3.000000	0.025	3.000000	27.2
2	10.000000	0.010	10.000000	28.9

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
3	0.000100	1.000	0.000100	1.1
3	0.000300	1.000	0.000300	1.1
3	0.001000	0.995	0.001000	1.3
3	0.003000	0.972	0.003000	1.7
3	0.010000	0.879	0.010000	2.9
3	0.030000	0.701	0.030000	5.4
3	0.100000	0.442	0.100000	10.5
3	0.300000	0.230	0.300000	16.6
3	1.000000	0.097	1.000000	22.9
3	3.000000	0.037	3.000000	25.5
3	10.000000	0.014	10.000000	27.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
4	0.000100	1.000	0.000100	0.9
4	0.000300	1.000	0.000300	0.9
4	0.001000	0.996	0.001000	1.1
4	0.003000	0.980	0.003000	1.5
4	0.010000	0.910	0.010000	2.3
4	0.030000	0.756	0.030000	4.4
4	0.100000	0.510	0.100000	8.7
4	0.300000	0.283	0.300000	14.6
4	1.000000	0.122	1.000000	21.3
4	3.000000	0.050	3.000000	23.8
4	10.000000	0.019	10.000000	25.5

excerpt from TR1C.OUT

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
5	0.000100	1.000	0.000100	0.8
5	0.000300	1.000	0.000300	0.8
5	0.001000	0.997	0.001000	0.9
5	0.003000	0.986	0.003000	1.1
5	0.010000	0.932	0.010000	1.9
5	0.030000	0.809	0.030000	3.5
5	0.100000	0.573	0.100000	7.2
5	0.300000	0.338	0.300000	12.7
5	1.000000	0.152	1.000000	19.3
5	3.000000	0.067	3.000000	22.4
5	10.000000	0.025	10.000000	24.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
6	0.000100	1.000	0.000100	0.6
6	0.000300	1.000	0.000300	0.6
6	0.001000	0.998	0.001000	0.6
6	0.003000	0.991	0.003000	0.9
6	0.010000	0.955	0.010000	1.3
6	0.030000	0.860	0.030000	2.5
6	0.100000	0.658	0.100000	5.5
6	0.300000	0.417	0.300000	10.3
6	1.000000	0.207	1.000000	16.8
6	3.000000	0.083	3.000000	20.2
6	10.000000	0.032	10.000000	22.5

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
7	0.000100	1.000	0.000100	0.2
7	0.000300	1.000	0.000300	0.4
7	0.001000	1.000	0.001000	0.8
7	0.003000	0.990	0.003000	1.4
7	0.010000	0.960	0.010000	2.8
7	0.030000	0.900	0.030000	5.1
7	0.100000	0.750	0.100000	9.8
7	0.300000	0.550	0.300000	15.5
7	1.000000	0.340	1.000000	21.0
7	3.000000	0.200	3.000000	25.0
7	10.000000	0.120	10.000000	28.0

1***** OPTION 2 *** READ SOIL PROFILE

NEW SOIL PROFILE NO. 1 IDENTIFICATION Transporter Route, HBPP, ISFSI, 08/

DNUMBER OF LAYERS 25 DEPTH TO BEDROCK 85.00
NUMBER OF FIRST SUBMERGED LAYER 4 DEPTH TO WATER LEVEL 6.00

LAYER	TYPE	MAX-MOD	THICKNESS	DEPTH	EFF. PRESS.	MODULUS	DAMPING	UNIT WEIGHT	SHEAR VEL	SVMAX
1	1	3250.097	1.00	0.50	0.063	3250.097	0.0500	0.1250	915.000	915.000
2	1	3250.097	2.00	2.00	0.250	3250.097	0.0500	0.1250	915.000	915.000
3	1	3250.097	3.00	4.50	0.563	3250.097	0.0500	0.1250	915.000	915.000
4	1	3250.097	2.00	7.00	0.813	3250.097	0.0500	0.1250	915.000	915.000
5	1	3250.097	2.00	9.00	0.938	3250.097	0.0500	0.1250	915.000	915.000
6	1	3250.097	2.00	11.00	1.063	3250.097	0.0500	0.1250	915.000	915.000
7	1	3250.097	2.00	13.00	1.188	3250.097	0.0500	0.1250	915.000	915.000
8	1	3250.097	2.00	15.00	1.313	3250.097	0.0500	0.1250	915.000	915.000
9	1	6009.068	2.00	17.00	1.444	6009.068	0.0500	0.1300	1220.000	1220.000
10	1	6009.068	3.00	19.50	1.613	6009.068	0.0500	0.1300	1220.000	1220.000
11	1	6009.068	3.00	22.50	1.815	6009.068	0.0500	0.1300	1220.000	1220.000
12	2	4474.783	5.00	26.50	2.086	4474.783	0.0500	0.1300	1052.791	1052.791
13	2	5388.738	4.00	31.00	2.390	5388.738	0.0500	0.1300	1155.313	1155.313
14	2	5685.408	4.00	35.00	2.660	5685.408	0.0500	0.1300	1186.689	1186.689
15	2	5657.928	4.00	39.00	2.931	5657.928	0.0500	0.1300	1183.818	1183.818
16	2	5913.175	4.00	43.00	3.201	5913.175	0.0500	0.1300	1210.226	1210.226
17	1	13520.403	5.00	47.50	3.505	13520.403	0.0500	0.1300	1830.000	1830.000
18	1	13520.403	5.00	52.50	3.843	13520.403	0.0500	0.1300	1830.000	1830.000
19	3	9925.974	5.00	57.50	4.181	9925.974	0.0500	0.1300	1567.988	1567.988
20	3	10319.356	5.00	62.50	4.519	10319.356	0.0500	0.1300	1598.757	1598.757
21	3	10698.285	5.00	67.50	4.857	10698.285	0.0500	0.1300	1627.846	1627.846
22	3	11064.243	5.00	72.50	5.195	11064.243	0.0500	0.1300	1655.454	1655.454
23	3	11418.479	5.00	77.50	5.533	11418.479	0.0500	0.1300	1681.746	1681.746
24	3	11762.051	5.00	82.50	5.871	11762.051	0.0500	0.1300	1706.859	1706.859
25	BASE					13081.	0.050	0.1300	1800.	

PERIOD = 0.25 FROM AVERAGE SHEARVEL. = 1366.

MAXIMUM AMPLIFICATION * 13.99
FOR FREQUENCY * 4.42 C/SEC.
PERIOD * 0.23 SEC.

1***** OPTION 1 *** READ INPUT MOTION

EARTHQUAKE - SECTION C-C, 08/2002

excerpt from TR1C.OUT

15999 ACCELERATION VALUES AT TIME INTERVAL 0.0050

THE VALUES ARE LISTED ROW BY ROW AS READ FROM CARDS
TRAILING ZEROS ARE ADDED TO GIVE A TOTAL OF 16384 VALUES

MAXIMUM ACCELERATION = 1.66833
AT TIME = 23.25 SEC

THE VALUES WILL BE MULTIPLIED BY A FACTOR = 1.000
TO GIVE NEW MAXIMUM ACCELERATION = 1.66833

MEAN SQUARE FREQUENCY = 0.94 C/SEC.

MAX ACCELERATION = 1.59292 FOR FREQUENCIES REMOVED ABOVE 2.50 C/SEC.

1***** OPTION 3 *** READ WHERE OBJECT MOTION IS GIVEN

OBJECT MOTION IN LAYER NUMBER 1 OUTCROPPING

1***** OPTION 4 *** OBTAIN STRAIN COMPATIBLE SOIL PROPERTIES

MAXIMUM NUMBER OF ITERATIONS = 30
MAXIMUM ERROR IN PERCENT = 2.007
FACTOR FOR EFFECTIVE STRAIN IN TIME DOMAIN = 0.65

EARTHQUAKE - SECTION C-C, 08/2002
SOIL PROFILE - Transporter Route, NBPP, ISFSI, 08/

ITERATION NUMBER 1
THE CALCULATION HAS BEEN CARRIED OUT IN THE TIME DOMAIN WITH EFF. STRAIN = .65* MAX. STRAIN

LAYER	TYPE	DEPTH	EFF. STRAIN	NEW DAMP.	DAMP USED	ERROR	NEW G	G USED	ERROR	NEW Vs
1	1	0.5	0.00201	0.022	0.050	-122.7	1131.889	3250.097	-3.8	898.206
2	1	2.0	0.00803	0.041	0.050	-20.8	1739.178	3250.097	-18.7	840.007
3	1	4.5	0.01807	0.062	0.050	19.3	2364.109	3250.097	-37.5	780.381
4	1	7.0	0.02811	0.075	0.050	33.0	2139.572	3250.097	-51.9	742.397
5	1	9.0	0.03613	0.083	0.050	39.4	1989.317	3250.097	-63.4	715.855
6	1	11.0	0.04415	0.089	0.050	44.0	1853.659	3250.097	-75.3	691.016
7	1	13.0	0.05215	0.095	0.050	47.3	1740.805	3250.097	-86.7	669.650
8	1	15.0	0.06015	0.100	0.050	49.9	1644.213	3250.097	-97.7	650.807
9	1	17.0	0.0694	0.083	0.050	40.0	3650.352	6009.068	-64.6	950.875
10	1	19.5	0.04255	0.088	0.050	43.2	3473.374	6009.068	-73.0	927.539
11	1	22.5	0.04927	0.093	0.050	46.3	3289.757	6009.068	-82.7	902.689
12	2	26.5	0.07817	0.114	0.050	56.3	1863.125	4474.783	-140.2	679.325
13	2	31.0	0.07609	0.113	0.050	55.8	2274.616	5388.738	-136.9	750.603
14	2	35.0	0.08150	0.116	0.050	57.0	2316.848	5685.408	-145.4	757.539
15	2	39.0	0.09128	0.122	0.050	58.9	2169.278	5657.928	-160.8	733.017
16	2	43.0	0.09628	0.124	0.050	59.7	2200.065	5913.175	-168.8	738.200
17	1	47.5	0.04649	0.091	0.050	45.1	7565.703	13520.403	-78.7	1368.929
18	1	52.5	0.05134	0.094	0.050	47.1	7286.074	13520.403	-85.6	1343.393
19	3	57.5	0.07652	0.093	0.050	46.5	4958.756	9925.974	-100.2	1108.262
20	3	62.5	0.07991	0.095	0.050	47.5	5059.019	10319.356	-104.0	1119.411
21	3	67.5	0.08313	0.097	0.050	48.4	5153.742	10698.285	-107.6	1129.842
22	3	72.5	0.08621	0.098	0.050	49.2	5243.578	11064.243	-111.0	1139.646
23	3	77.5	0.08915	0.100	0.050	49.9	5329.083	11418.479	-114.3	1148.901
24	3	82.5	0.09197	0.101	0.050	50.6	5410.724	11762.051	-117.4	1257.668

VALUES IN TIME DOMAIN

LAYER	TYPE	THICKNESS FT	DEPTH FT	MAX STRAIN PRCNT	MAX STRESS PSF	TIME SEC
1	1	1.0	0.5	0.00309	96.78	23.31
2	1	2.0	2.0	0.01236	338.57	23.31
3	1	3.0	4.5	0.02781	657.39	23.31
4	1	2.0	7.0	0.04325	925.27	23.31
5	1	2.0	9.0	0.05559	1105.81	23.31
6	1	2.0	11.0	0.06792	1258.98	23.31
7	1	2.0	13.0	0.08024	1396.77	23.31
8	1	2.0	15.0	0.09254	1521.56	23.31
9	1	2.0	17.0	0.05683	2074.50	23.31
10	1	3.0	19.5	0.06546	2273.67	23.31
11	1	3.0	22.5	0.07580	2493.67	23.31
12	2	5.0	26.5	0.12027	2240.69	23.31
13	2	4.0	31.0	0.11706	2462.65	23.31
14	2	4.0	35.0	0.12538	2904.82	23.31
15	2	4.0	39.0	0.14043	3046.26	23.31
16	2	4.0	43.0	0.14812	3258.79	23.31
17	1	5.0	47.5	0.07152	5410.98	23.31
18	1	5.0	52.5	0.07898	5754.86	23.31
19	3	5.0	57.5	0.11772	5837.51	23.31

10	1	3.0	19.5	0.17249	3950.29	23.33
11	1	3.0	22.5	0.22624	4572.23	23.33
12	2	5.0	26.5	1.99966	5370.76	23.37
13	2	4.0	31.0	1.71818	6145.46	23.37
14	2	4.0	35.0	2.16040	6974.69	23.37
15	2	4.0	39.0	5.99913	7176.78	23.38
16	2	4.0	43.0	7.01057	8204.70	23.38
17	1	5.0	47.5	0.16578	8689.05	23.32
18	1	5.0	52.5	0.18424	9222.39	23.32
19	3	5.0	57.5	0.35757	9911.36	23.33
20	3	5.0	62.5	0.37913	10482.43	23.32
21	3	5.0	67.5	0.40102	11031.13	23.32
22	3	5.0	72.5	0.42117	11540.90	23.32
23	3	5.0	77.5	0.43864	12011.63	23.32
24	3	5.0	82.5	0.45264	12445.16	23.31

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EARTHQUAKE - SECTION C-C, 08/2002
SOIL PROFILE - Transporter Route, HBPP, ISFSI, 08/

ITERATION NUMBER 22
THE CALCULATION HAS BEEN CARRIED OUT IN THE TIME DOMAIN WITH EFF. STRAIN = .65* MAX. STRAIN

LAYER	TYPE	DEPTH	EFF. STRAIN	NEW DAMP.	DAMP USED	ERROR	NEW G	G USED	ERROR	NEW Vs
1	1	0.5	0.00208	0.023	0.023	0.0	3126.043	3126.043	0.0	897.368
2	1	2.0	0.00976	0.045	0.045	0.0	2673.314	2673.314	0.0	829.847
3	1	4.5	0.02737	0.074	0.074	0.0	2153.043	2153.043	0.0	744.731
4	1	7.0	0.05318	0.096	0.096	0.0	1727.568	1727.568	0.0	667.099
5	1	9.0	0.08283	0.111	0.111	0.0	1427.598	1427.598	0.0	608.423
6	1	11.0	0.12049	0.124	0.124	0.0	1199.988	1199.989	0.0	555.983
7	1	13.0	0.16643	0.137	0.137	0.0	1026.633	1026.634	0.0	514.257
8	1	15.0	0.23284	0.151	0.151	0.0	846.435	846.450	0.0	466.949
9	1	17.0	0.08604	0.112	0.112	0.0	2591.835	2591.835	0.0	801.235
10	1	19.5	0.11212	0.122	0.122	0.0	2290.093	2290.093	0.0	753.152
11	1	22.5	0.14706	0.132	0.132	0.0	2020.935	2020.935	0.0	707.510
12	2	26.5	1.30340	0.254	0.254	0.0	268.062	268.584	-0.2	257.676
13	2	31.0	1.13681	0.251	0.251	0.2	353.668	357.671	-1.1	295.974
14	2	35.0	1.40599	0.256	0.256	0.0	322.548	322.842	-0.1	282.653
15	2	39.0	4.04313	0.276	0.276	0.2	120.413	122.964	-2.1	172.700
16	2	43.0	4.55879	0.278	0.278	0.0	117.002	117.033	0.0	170.237
17	1	47.5	0.10733	0.120	0.120	-0.1	5250.162	5241.394	0.2	1140.362
18	1	52.5	0.11905	0.124	0.124	-0.2	5018.894	5005.636	0.3	1114.962
19	3	57.5	0.22772	0.150	0.151	-0.8	2831.011	2771.832	1.4	834.425
20	3	62.5	0.24026	0.153	0.155	-0.9	2815.673	2765.098	1.8	835.117
21	3	67.5	0.25341	0.156	0.158	-1.0	2809.008	2750.789	2.1	834.128
22	3	72.5	0.26623	0.159	0.162	-1.0	2799.759	2740.185	2.1	832.754
23	3	77.5	0.27810	0.161	0.163	-0.9	2793.270	2738.358	2.0	831.788
24	3	82.5	0.28852	0.163	0.165	-0.7	2793.872	2749.456	1.6	831.878

VALUES IN TIME DOMAIN

LAYER	TYPE	THICKNESS FT	DEPTH FT	MAX STRAIN PRCNT	MAX STRESS PSF	TIME SEC
1	1	1.0	0.5	0.00320	99.99	23.31
2	1	2.0	2.0	0.01501	401.40	23.31
3	1	3.0	4.5	0.04212	906.76	23.32
4	1	2.0	7.0	0.08182	1413.52	23.32
5	1	2.0	9.0	0.12743	1819.18	23.33
6	1	2.0	11.0	0.18537	2224.45	23.33
7	1	2.0	13.0	0.25605	2628.68	23.33
8	1	2.0	15.0	0.35821	3032.01	23.34
9	1	2.0	17.0	0.13237	3430.85	23.33
10	1	3.0	19.5	0.17249	3950.29	23.33
11	1	3.0	22.5	0.22624	4572.23	23.33
12	2	5.0	26.5	2.00524	5375.28	23.37
13	2	4.0	31.0	1.74894	6185.45	23.37
14	2	4.0	35.0	2.16307	6976.94	23.37
15	2	4.0	39.0	6.22020	7489.95	23.38
16	2	4.0	43.0	7.01353	8205.98	23.38
17	1	5.0	47.5	0.16513	8669.47	23.32
18	1	5.0	52.5	0.18315	9192.07	23.32
19	3	5.0	57.5	0.35033	9847.95	23.33
20	3	5.0	62.5	0.36963	10407.47	23.32
21	3	5.0	67.5	0.38987	10951.37	23.32
22	3	5.0	72.5	0.40958	11467.34	23.32
23	3	5.0	77.5	0.42785	11950.92	23.31
24	3	5.0	82.5	0.44387	12401.14	23.31

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EARTHQUAKE - SECTION C-C, 08/2002
SOIL PROFILE - Transporter Route, HBPP, ISFSI, 08/

ITERATION NUMBER 23
THE CALCULATION HAS BEEN CARRIED OUT IN THE TIME DOMAIN WITH EFF. STRAIN = .65* MAX. STRAIN

LAYER	TYPE	DEPTH	EFF. STRAIN	NEW DAMP.	DAMP USED	ERROR	NEW G	G USED	ERROR	NEW Vs
1	1	0.5	0.00208	0.023	0.023	0.0	3126.043	3126.043	0.0	897.368
2	1	2.0	0.00976	0.045	0.045	0.0	2673.314	2673.314	0.0	829.847

excerpt from TR1C.OUT

3	1	4.5	0.02737	0.074	0.074	0.0	2153.043	2153.043	0.0	744.731
4	1	7.0	0.05318	0.096	0.096	0.0	1727.568	1727.568	0.0	667.099
5	1	9.0	0.08293	0.111	0.111	0.0	1427.598	1427.598	0.0	606.423
6	1	11.0	0.12049	0.124	0.124	0.0	1199.988	1199.988	0.0	555.983
7	1	13.0	0.16643	0.137	0.137	0.0	1026.633	1026.633	0.0	514.257
8	1	15.0	0.22284	0.151	0.151	0.0	846.425	846.425	0.0	466.947
9	1	17.0	0.08604	0.112	0.112	0.0	2591.835	2591.835	0.0	801.235
10	1	19.5	0.11222	0.122	0.122	0.0	2290.093	2290.093	0.0	753.152
11	1	22.5	0.14706	0.132	0.132	0.0	2020.935	2020.935	0.0	707.520
12	2	26.5	1.30593	0.254	0.254	0.0	267.699	268.062	-0.1	257.502
13	2	31.0	1.14963	0.251	0.251	0.1	351.139	353.668	-0.7	294.914
14	2	35.0	1.40715	0.256	0.256	0.0	322.353	322.548	-0.1	282.568
15	2	39.0	4.12779	0.277	0.276	0.1	118.953	120.433	-1.2	171.650
16	2	43.0	4.55769	0.278	0.278	0.0	117.020	117.002	0.0	170.250
17	1	47.5	0.10706	0.120	0.120	-0.1	5255.938	5250.162	0.1	1140.989
18	1	52.5	0.12858	0.124	0.124	-0.1	5027.673	5018.894	0.2	1115.937
19	3	57.5	0.22426	0.149	0.150	-0.6	2841.146	2811.011	1.1	838.886
20	3	62.5	0.23549	0.152	0.153	-0.7	2855.625	2815.673	1.4	842.021
21	3	67.5	0.24762	0.155	0.156	-0.8	2856.763	2809.008	1.7	841.189
22	3	72.5	0.25997	0.158	0.159	-0.8	2850.578	2799.759	1.8	840.278
23	3	77.5	0.27200	0.160	0.161	-0.8	2842.131	2793.270	1.7	839.032
24	3	82.5	0.29325	0.162	0.163	-0.6	2935.653	2793.872	1.5	838.075

VALUES IN TIME DOMAIN

LAYER	TYPE	THICKNESS FT	DEPTH FT	MAX STRAIN PRCNT	MAX STRESS PSF	TIME SEC
1	1	1.0	0.5	0.00320	99.99	23.31
2	1	2.0	2.0	0.01501	401.40	23.31
3	1	3.0	4.5	0.04212	906.76	23.32
4	1	2.0	7.0	0.08182	1413.52	23.32
5	1	2.0	9.0	0.12743	1819.18	23.33
6	1	2.0	11.0	0.18537	2224.45	23.33
7	1	2.0	13.0	0.25605	2628.68	23.33
8	1	2.0	15.0	0.35822	3032.03	23.34
9	1	2.0	17.0	0.43237	3430.85	23.33
10	1	3.0	19.5	0.57249	3950.29	23.33
11	1	3.0	22.5	0.72624	4572.23	23.33
12	2	5.0	26.5	2.00912	5378.41	23.37
13	2	4.0	31.0	1.76865	6210.44	23.37
14	2	4.0	35.0	2.16484	6978.44	23.37
15	2	4.0	39.0	6.35044	7554.02	23.38
16	2	4.0	43.0	7.01183	8205.24	23.38
17	1	5.0	47.5	0.16470	8656.59	23.32
18	1	5.0	52.5	0.18243	9172.01	23.32
19	3	5.0	57.5	0.34487	9798.15	23.33
20	3	5.0	62.5	0.36228	10345.49	23.32
21	3	5.0	67.5	0.38095	10882.87	23.32
22	3	5.0	72.5	0.39995	11400.87	23.32
23	3	5.0	77.5	0.41846	11893.29	23.31
24	3	5.0	82.5	0.43577	12357.02	23.31

PERIOD = 0.50 FROM AVERAGE SHEARVEL. = 680.
 MAXIMUM AMPLIFICATION = 2.35
 FOR FREQUENCY = 1.16 C/SEC.
 PERIOD = 0.86 SEC.

1***** OPTION 5 *** COMPUTE MOTION IN NEW SUBLAYERS

EARTHQUAKE - SECTION C-C, 08/2002
 SOIL DEPOSIT - Transporter Route, HBPP, ISFSI, 08/

LAYER	DEPTH FT	MAX. ACC. G	TIME SEC	MEAN SQ. FR. QUIET ZONE	ACC. RATIO ACC. RECORD	PUNCHED CARDS
OUTCR.	0.0	1.59292	23.30	0.94	0.044	2048
WITHIN	1.0	1.59288	23.30	0.94	0.044	0
WITHIN	3.0	1.59250	23.30	0.94	0.044	0
WITHIN	6.0	1.59090	23.30	0.94	0.044	0
WITHIN	8.0	1.58885	23.30	0.94	0.044	0
WITHIN	10.0	1.58566	23.30	0.94	0.044	0
WITHIN	12.0	1.58105	23.30	0.93	0.043	0
WITHIN	14.0	1.57472	23.30	0.93	0.043	0
WITHIN	16.0	1.56593	23.30	0.92	0.043	0
WITHIN	18.0	1.56264	23.30	0.91	0.043	0
WITHIN	21.0	1.55624	23.30	0.91	0.043	0
WITHIN	24.0	1.54790	23.30	0.90	0.043	0

excerpt from TR1C.OUT

WITHIN	29.0	1.43443	23.30	0.80	0.041	0
WITHIN	33.0	1.35582	23.29	0.75	0.041	0
WITHIN	37.0	1.26403	23.28	0.72	0.043	0

1----- OPTION 5 *** COMPUTE MOTION IN NEW SUBLAYERS

EARTHQUAKE - SECTION C-C, 08/2002
SOIL DEPOSIT - Transporter Route, HBPP, ISFSI, 08/

LAYER	DEPTH FT	MAX. ACC. G	TIME SEC	TIME C/SEC	MEAN SQ. FR. QUIET ZONE	ACC. RATIO ACC. RECORD	PUNCHED CARDS
WITHIN	41.0	1.07090	24.81		0.86	0.062	0
WITHIN	45.0	1.27278	24.80		1.21	0.065	0
WITHIN	50.0	1.27655	24.80		1.22	0.065	0
WITHIN	55.0	1.27919	24.79		1.22	0.065	0
WITHIN	60.0	1.28156	24.79		1.22	0.064	0
WITHIN	65.0	1.28124	24.79		1.22	0.064	0
WITHIN	70.0	1.27825	24.79		1.22	0.063	0
WITHIN	75.0	1.27297	24.78		1.20	0.063	0
WITHIN	80.0	1.26529	24.78		1.19	0.062	0
WITHIN	85.0	1.25500	24.78		1.17	0.062	0
OUTCR.	85.0	1.35293	23.06		1.27	0.063	2048

XMAX= 1.5929 SECTION C-C, 08/2002

ACCELERATION VALUES AT OUTCROPPING LAYER 1 - Transporter Route, HBPP, ISFSI, 08/													
0.014488	0.013698	0.012825	0.011873	0.010848	0.009758	0.008607	0.007405						1
0.006157	0.004873	0.003558	0.002223	0.000874	-0.000478	-0.001828	-0.003164						2
-0.004482	-0.005769	-0.007021	-0.008227	-0.009384	-0.010480	-0.011512	-0.012469						3
-0.013351	-0.014147	-0.014857	-0.015471	-0.015992	-0.016410	-0.016727	-0.016938						4
-0.017045	-0.017043	-0.016937	-0.016723	-0.016405	-0.015984	-0.015463	-0.014845						5
-0.014134	-0.013334	-0.012449	-0.011487	-0.010451	-0.009350	-0.008189	-0.006976						6
-0.005717	-0.004422	-0.003097	-0.001752	-0.000393	0.000968	0.002328	0.003673						7
0.004999	0.006294	0.007555	0.008769	0.009933	0.011036	0.012075	0.013039						8
0.013928	0.014730	0.015446	0.016067	0.016594	0.017018	0.017343	0.017561						9
0.017676	0.017682	0.017585	0.017381	0.017075	0.016665	0.016158	0.015555						10
0.014861	0.014079	0.013216	0.012276	0.011266	0.010192	0.009062	0.007883						11
0.006662	0.005408	0.004128	0.002832	0.001526	0.000222	-0.001076	-0.002354						12
-0.003608	-0.004826	-0.006004	-0.007130	-0.008200	-0.009203	-0.010135	-0.010987						13
-0.011757	-0.012434	-0.013018	-0.013500	-0.013880	-0.014153	-0.014317	-0.014369						14
-0.014310	-0.014136	-0.013851	-0.013453	-0.012945	-0.012327	-0.011605	-0.010780						15
-0.009858	-0.008841	-0.007737	-0.006551	-0.005288	-0.003957	-0.002563	-0.001116						16
0.000378	0.001910	0.003472	0.005054	0.006649	0.008246	0.009838	0.011414						17
0.012968	0.014488	0.015969	0.017398	0.018772	0.020079	0.021315	0.022470						18
0.023540	0.024518	0.025399	0.026177	0.026849	0.027410	0.027860	0.028192						19
0.028409	0.028507	0.028487	0.028349	0.028094	0.027724	0.027241	0.026650						20
0.025953	0.025155	0.024259	0.023275	0.022205	0.021058	0.019838	0.018557						21
0.017218	0.015834	0.014407	0.012953	0.011474	0.009985	0.008488	0.006999						22
0.005521	0.004067	0.002641	0.001258	-0.000081	-0.001362	-0.002585	-0.003734						23
-0.004811	-0.005802	-0.006709	-0.007521	-0.008238	-0.008852	-0.009365	-0.009768						24
-0.010066	-0.010251	-0.010330	-0.010296	-0.010156	-0.009907	-0.009555	-0.009098						25
-0.008546	-0.007897	-0.007161	-0.006339	-0.005440	-0.004468	-0.003431	-0.002336						26
-0.001192	-0.000004	0.001218	0.002466	0.003732	0.005006	0.006281	0.007547						27
0.008796	0.010020	0.011210	0.012357	0.013454	0.014493	0.015468	0.016371						28
0.017196	0.017936	0.018587	0.019144	0.019602	0.019958	0.020209	0.020352						29
0.020386	0.020310	0.020122	0.019825	0.019418	0.018905	0.018284	0.017564						30
0.016743	0.015830	0.014825	0.013739	0.012572	0.011337	0.010034	0.008677						31
0.007267	0.005818	0.004333	0.002826	0.001299	-0.000233	-0.001766	-0.003287						32
-0.004792	-0.006267	-0.007710	-0.009106	-0.010453	-0.011738	-0.012959	-0.014103						33
-0.015171	-0.016149	-0.017040	-0.017830	-0.018524	-0.019109	-0.019591	-0.019960						34
-0.020221	-0.020366	-0.020401	-0.020321	-0.020133	-0.019832	-0.019426	-0.018914						35
-0.018304	-0.017595	-0.016797	-0.015912	-0.014948	-0.013910	-0.012806	-0.011643						36
-0.010428	-0.009171	-0.007878	-0.006559	-0.005222	-0.003876	-0.002530	-0.001193						37
0.000127	0.001420	0.002680	0.003895	0.005060	0.006165	0.007205	0.008170						38
0.009057	0.009856	0.010566	0.011178	0.011690	0.012097	0.012397	0.012586						39
0.012664	0.012628	0.012479	0.012217	0.011843	0.011359	0.010767	0.010069						40
0.009270	0.008375	0.007387	0.006313	0.005157	0.003928	0.002631	0.001276						41
-0.000133	-0.001585	-0.003073	-0.004587	-0.006121	-0.007662	-0.009206	-0.010739						42
-0.012257	-0.013747	-0.015203	-0.016615	-0.017977	-0.019277	-0.020512	-0.021672						43
-0.022752	-0.023743	-0.024644	-0.025445	-0.026146	-0.026738	-0.027223	-0.027593						44
-0.027851	-0.027993	-0.028019	-0.027928	-0.027724	-0.027405	-0.026975	-0.026436						45
-0.025793	-0.025049	-0.024208	-0.023277	-0.022260	-0.021166	-0.019999	-0.018769						46
-0.017480	-0.016144	-0.014766	-0.013357	-0.011922	-0.010475	-0.009020	-0.007570						47
-0.006130	-0.004712	-0.003321	-0.001970	-0.000662	0.000590	0.001783	0.002905						48
0.003955	0.004922	0.005804	0.006592	0.007285	0.007876	0.008365	0.008745						49
0.009019	0.009180	0.009233	0.009173	0.009005	0.008727	0.008344	0.007855						50
0.007267	0.006581	0.005804	0.004939	0.003993	0.002972	0.001882	0.000731						51
-0.000475	-0.001728	-0.003019	-0.004341	-0.005685	-0.007043	-0.008406	-0.009766						52
-0.011114	-0.012442	-0.013742	-0.015004	-0.016223	-0.017390	-0.018498	-0.019540						53
-0.020511	-0.021404	-0.022214	-0.022936	-0.023566	-0.024100	-0.024537	-0.024872						54
-0.025105	-0.025234	-0.025260	-0.025182	-0.025002	-0.024722	-0.024344	-0.023871						55
-0.023306	-0.022655	-0.021920	-0.021110	-0.020228	-0.019283	-0.018279	-0.017226						56
-0.016129	-0.014999	-0.013840	-0.012666	-0.011479	-0.010293	-0.009112	-0.007950						57
-0.006810	-0.005706	-0.004640	-0.003626	-0.002667	-0.001774	-0.000951	-0.000208						58
0.000453	0.001021	0.001498	0.001872	0.002146	0.002310	0.002368	0.002312						59
0.002147	0.001866	0.001475	0.000970	0.000357	0.000365	-0.001191	-0.002119						60
-0.003143	-0.004260	-0.005462	-0.006745	-0.008101	-0.009523	-0.011004	-0.012535						61
-0.014108	-0.015715	-0.017346	-0.018992	-0.020645	-0.022293	-0.023929	-0.025541						62
-0.027122	-0.028660	-0.030150	-0.031578	-0.032939	-0.034224	-0.035424	-0.036532						63
-0.037543	-0.038447	-0.039241	-0.039918	-0.040475	-0.040906	-0.041210	-0.041382						64
-0.041422	-0.041328	-0.041099	-0.040737	-0.040241	-0.039615	-0.038860	-0.037980						65
-0.036978	-0.035861	-0.034630	-0.033296	-0.031861	-0.030336	-0.028725	-0.027039						66
-0.025283	-0.023470	-0.021604	-0.019701	-0.017762	-0.015806	-0.013834	-0.011864						67
-0.009898	-0.007953	-0.006032	-0.004151	-0.002312	-0.000533	0.001188	0.002833						68
0.004404	0.005883	0.007273	0.008560	0.009746	0.010818	0.011780	0.012621						69

16384	0.5							
8								
7	1	10	100.					
	11	100.	#1 modulus for Clay PI 15 (Vucetic and Dobry 1991)					
0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1	0.316	
1.	3.16	10.						
1.000	1.000	1.000	.94	.82	.64	.40	.21	
.09	.04	.02						
	11	1.	damping for Clay PI 15 (Vucetic & Dobry 1991)					
0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1	0.316	
1.	3.16	10.						
1.7	1.7	1.7	2.6	4.5	7.8	11.7	16.3	
20.2	23.0	23.0						
	11	100.	#2 modulus for Sand (20 to 50 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.000	0.999	0.991	0.953	0.830	0.620	0.364	0.181	
0.071	0.025	0.010						
	11	1.	damping for Sand (20 to 50 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.250	1.300	1.455	2.080	3.750	6.925	12.600	18.905	
24.840	27.2	28.9						
	11	100.	#3 modulus for Sand (50 to 120 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.000	1.000	0.995	0.972	0.879	0.701	0.442	0.230	
0.097	0.037	0.014						
	11	1.	damping for Sand (50 to 120 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.090	1.145	1.300	1.665	2.865	5.415	10.465	16.560	
22.915	25.5	27.0						
	11	100.	#4 modulus for Sand (120 to 250 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.000	1.000	0.996	0.980	0.910	0.756	0.510	0.283	
0.122	0.050	0.019						
	11	1.	damping for Sand (120 to 250 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
0.935	0.935	1.090	1.455	2.340	4.375	8.695	14.580	
21.250	23.8	25.5						
	11	100.	#5 modulus for Sand (250 to 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.000	1.000	0.997	0.986	0.932	0.809	0.573	0.338	
0.152	0.067	0.025						
	11	1.	damping for Sand (250 to 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
0.800	0.800	0.900	1.145	1.875	3.490	7.185	12.705	
19.270	22.4	24.0						
	11	100.	#6 modulus for Sand (> 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.000	1.000	0.998	0.991	0.955	0.860	0.658	0.417	
0.207	0.083	0.032						
	11	1.	damping for Sand (> 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
0.570	0.625	0.625	0.850	1.280	2.500	5.520	10.260	
16.770	20.2	22.5						

11 100. #7 modulus for Weathered Rock														
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3							
1.	3.	10.												
1.000	1.000	1.000	0.990	0.960	0.900	0.75	0.55							
0.34	0.2	0.12												
11 1. damping for Weathered Rock														
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3							
1.	3.	10.												
0.24	0.42	0.8	1.4	2.8	5.1	9.8	15.5							
21.	25.	28.												
2														
1	25	4	Transporter Route, HBPP, ISFSI, 08/2002											
1	1	1	1.0	0.023	.125	897.368	1.							
2	1	1	2.0	0.045	.125	829.847	1.							
3	1	1	3.0	0.074	.125	744.731	1.							
4	1	1	2.0	0.096	.125	667.099	1.							
5	1	1	2.0	0.111	.125	606.423	1.							
6	1	1	2.0	0.124	.125	555.983	1.							
7	1	1	2.0	0.137	.125	514.257	1.							
8	1	1	2.0	0.151	.125	466.947	1.							
9	1	1	2.0	0.112	.130	801.235	1.							
10	1	1	3.0	0.122	.130	753.152	1.							
11	1	1	3.0	0.132	.130	707.510	1.							
12	2	1	5.0	0.254	.130	257.502	1.							
13	2	1	4.0	0.251	.130	294.914	1.							
14	2	1	4.0	0.256	.130	282.568	1.							
15	2	1	4.0	0.277	.130	171.650	1.							
16	2	1	4.0	0.278	.130	170.250	1.							
17	1	1	5.0	0.120	.130	1140.989	1.							
18	1	1	5.0	0.124	.130	1115.937	1.							
19	3	1	5.0	0.149	.130	838.886	1.							
20	3	1	5.0	0.152	.130	841.021	1.							
21	3	1	5.0	0.155	.130	841.189	1.							
22	3	1	5.0	0.158	.130	840.278	1.							
23	3	1	5.0	0.160	.130	839.032	1.							
24	3	1	5.0	0.162	.130	838.075	1.							
25				.05	.130	1800.	1.							
1														
1599916384	.005	2(8E15.7) SET 1, SECTION C-C, 08/2002												
1.		6.												
S1CC.AC8														
3														
1	0													
5														
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
0	1	1	1	1	1	1	1	1	1	1	1	1	1	1
1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5														
16	17	18	19	20	21	22	23	24	25	25				
1	1	1	1	1	1	1	1	1	1	0				
0	0	0	0	0	0	0	0	0	0	1				
0														

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**
** SHAKE -- A COMPUTER PROGRAM FOR
** EARTHQUAKE RESPONSE ANALYSIS
** OF HORIZONTALLY LAYERED SITES
**
**
** MS-DOS VERSION - CONVERTED TO IBM-PC BY
** Shyh-Shiun Lai, WCC
** January 1985
**
**
** (Modified to Use 16384 Points and 100
** Soil Layers, S.J. Chiou, August 1995)
**
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Output file name : TR1CI.OUT
Start time : 19"/"/" --
Start time : 19"/"/" --

MAX. NUMBER OF TERMS IN FOURIER TRANSFORM = 16384
NECESSARY LENGTH OF BLANK COMMON X = 102419
EARTH PRESSURE AT REST FOR SAND = 0.500
1***** OPTION 8 *** READ RELATION BETWEEN SOIL PROPERTIES AND STRAIN

CURVES FOR RELATION STRAIN VERSUS SHEAR MODULUS AND DAMPING

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
1	0.000100	1.000	0.000100	1.7
1	0.000316	1.000	0.000316	1.7
1	0.001000	1.000	0.001000	1.7
1	0.003160	0.940	0.003160	2.6
1	0.010000	0.820	0.010000	4.5
1	0.031600	0.640	0.031600	7.8
1	0.100000	0.400	0.100000	11.7
1	0.316000	0.210	0.316000	16.3
1	1.000000	0.090	1.000000	20.2
1	3.160000	0.040	3.160000	23.0
1	10.000000	0.020	10.000000	23.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
2	0.000100	1.000	0.000100	1.3
2	0.000300	0.999	0.000300	1.3
2	0.001000	0.991	0.001000	1.5
2	0.003000	0.953	0.003000	2.1
2	0.010000	0.830	0.010000	3.8
2	0.030000	0.620	0.030000	6.9
2	0.100000	0.364	0.100000	12.6
2	0.300000	0.181	0.300000	18.9
2	1.000000	0.071	1.000000	24.8
2	3.000000	0.025	3.000000	27.2
2	10.000000	0.010	10.000000	28.9

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
3	0.000100	1.000	0.000100	1.1
3	0.000300	1.000	0.000300	1.2
3	0.001000	0.995	0.001000	1.3
3	0.003000	0.972	0.003000	1.7
3	0.010000	0.879	0.010000	2.9
3	0.030000	0.701	0.030000	5.4
3	0.100000	0.442	0.100000	10.5
3	0.300000	0.230	0.300000	16.6
3	1.000000	0.097	1.000000	22.9
3	3.000000	0.037	3.000000	25.5
3	10.000000	0.014	10.000000	27.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
4	0.000100	1.000	0.000100	0.9
4	0.000300	1.000	0.000300	0.9
4	0.001000	0.996	0.001000	1.1
4	0.003000	0.980	0.003000	1.5
4	0.010000	0.910	0.010000	2.3
4	0.030000	0.756	0.030000	4.4
4	0.100000	0.510	0.100000	8.7
4	0.300000	0.283	0.300000	14.6
4	1.000000	0.122	1.000000	21.3
4	3.000000	0.050	3.000000	23.8
4	10.000000	0.019	10.000000	25.5

TR1CI.0UT

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
5	0.000100	1.000	0.000100	0.8
5	0.000300	1.000	0.000300	0.8
5	0.001000	0.997	0.001000	0.9
5	0.003000	0.986	0.003000	1.1
5	0.010000	0.932	0.010000	1.9
5	0.030000	0.809	0.030000	3.5
5	0.100000	0.573	0.100000	7.2
5	0.300000	0.338	0.300000	12.7
5	1.000000	0.152	1.000000	19.3
5	3.000000	0.067	3.000000	22.4
5	10.000000	0.025	10.000000	24.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
6	0.000100	1.000	0.000100	0.6
6	0.000300	1.000	0.000300	0.6
6	0.001000	0.998	0.001000	0.6
6	0.003000	0.991	0.003000	0.9
6	0.010000	0.955	0.010000	1.3
6	0.030000	0.860	0.030000	2.5
6	0.100000	0.658	0.100000	5.5
6	0.300000	0.417	0.300000	10.3
6	1.000000	0.207	1.000000	16.8
6	3.000000	0.083	3.000000	20.2
6	10.000000	0.032	10.000000	22.5

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
7	0.000100	1.000	0.000100	0.2
7	0.000300	1.000	0.000300	0.4
7	0.001000	1.000	0.001000	0.8
7	0.003000	0.990	0.003000	1.4
7	0.010000	0.960	0.010000	2.8
7	0.030000	0.900	0.030000	5.1
7	0.100000	0.750	0.100000	9.8
7	0.300000	0.550	0.300000	15.5
7	1.000000	0.340	1.000000	21.0
7	3.000000	0.200	3.000000	25.0
7	10.000000	0.120	10.000000	28.0

1***** OPTION 2 *** READ SOIL PROFILE

NEW SOIL PROFILE NO. 1 IDENTIFICATION Transporter Route, HBPP, ISFSI, 08/

UNUMBER OF LAYERS 25 DEPTH TO BEDROCK 85.00
NUMBER OF FIRST SUBMERGED LAYER 4 DEPTH TO WATER LEVEL 6.00

LAYER	TYPE	MAX-MOD	THICKNESS	DEPTH	EFF. PRESS.	MODULUS	DAMPING	UNIT WEIGHT	SHEAR VEL	SVMAX
1	1	3126.045	1.00	0.50	0.063	3126.045	0.0230	0.1250	897.368	897.368
2	1	2673.315	2.00	2.00	0.250	2673.315	0.0450	0.1250	829.847	829.847
3	1	2153.044	3.00	4.50	0.563	2153.044	0.0740	0.1250	744.731	744.731
4	1	1727.566	2.00	7.00	0.813	1727.566	0.0960	0.1250	667.099	667.099
5	1	1427.596	2.00	9.00	0.938	1427.596	0.1110	0.1250	606.423	606.423
6	1	1199.989	2.00	11.00	1.063	1199.989	0.1240	0.1250	555.983	555.983
7	1	1026.631	2.00	13.00	1.188	1026.631	0.1370	0.1250	514.257	514.257
8	1	846.427	2.00	15.00	1.313	846.427	0.1510	0.1250	466.947	466.947
9	1	2591.834	2.00	17.00	1.444	2591.834	0.1120	0.1300	801.235	801.235
10	1	2290.091	3.00	19.50	1.613	2290.091	0.1220	0.1300	753.152	753.152
11	1	2020.936	3.00	22.50	1.815	2020.936	0.1320	0.1300	707.510	707.510
12	2	267.700	5.00	26.50	2.086	267.700	0.2540	0.1300	257.502	257.502
13	2	351.138	4.00	31.00	2.390	351.138	0.2510	0.1300	294.914	294.914
14	2	322.354	4.00	35.00	2.660	322.354	0.2560	0.1300	282.568	282.568
15	2	138.953	4.00	39.00	2.931	138.953	0.2770	0.1300	171.650	171.650
16	2	117.020	4.00	43.00	3.201	117.020	0.2780	0.1300	170.250	170.250
17	1	5255.940	5.00	47.50	3.505	5255.940	0.1200	0.1300	1140.989	1140.989
18	1	5027.670	5.00	52.50	3.843	5027.670	0.1240	0.1300	1115.937	1115.937
19	3	2841.145	5.00	57.50	4.181	2841.145	0.1490	0.1300	838.886	838.886
20	3	2855.625	5.00	62.50	4.519	2855.625	0.1520	0.1300	841.021	841.021
21	3	2856.766	5.00	67.50	4.857	2856.766	0.1550	0.1300	841.189	841.189
22	3	2850.582	5.00	72.50	5.195	2850.582	0.1580	0.1300	840.278	840.278
23	3	2842.134	5.00	77.50	5.533	2842.134	0.1600	0.1300	839.032	839.032
24	3	2835.654	5.00	82.50	5.871	2835.654	0.1620	0.1300	838.075	838.075
25	BASE					13081.	0.050	0.1300	1800.	

PERIOD = 0.50 FROM AVERAGE SHEARVEL. = 680.

MAXIMUM AMPLIFICATION = 2.34
FOR FREQUENCY = 1.16 C/SEC.
PERIOD = 0.86 SEC.

1***** OPTION 1 *** READ INPUT MOTION

EARTHQUAKE - SECTION C-C, 08/2002

TR1CI.OUT

15999 ACCELERATION VALUES AT TIME INTERVAL 0.0050

THE VALUES ARE LISTED ROW BY ROW AS READ FROM CARDS
TRAILING ZEROS ARE ADDED TO GIVE A TOTAL OF 16384 VALUES

MAXIMUM ACCELERATION = 1.66833
AT TIME = 23.25 SEC

THE VALUES WILL BE MULTIPLIED BY A FACTOR = 1.000
TO GIVE NEW MAXIMUM ACCELERATION = 1.66833

MEAN SQUARE FREQUENCY = 1.49 C/SEC.

MAX ACCELERATION = 1.68741 FOR FREQUENCIES REMOVED ABOVE 6.00 C/SEC.

1***** OPTION 3 *** READ WHERE OBJECT MOTION IS GIVEN

OBJECT MOTION IN LAYER NUMBER 1 OUTCROPPING

1***** OPTION 5 *** COMPUTE MOTION IN NEW SUBLAYERS

EARTHQUAKE - SECTION C-C, 08/2002
SOIL DEPOSIT - Transporter Route, HBPP, ISFSI, 08/

LAYER	DEPTH, FT	MAX. ACC. G	TIME SEC	TIME C/SEC	MEAN SQ. FR. QUIET ZONE	ACC. RATIO ACC. RECORD	PUNCHED CARDS
OUTCR.	0.0	1.68741	23.23	23.23	1.49	0.044	2048
WITHIN	1.0	1.68724	23.23	23.23	1.49	0.044	0
WITHIN	3.0	1.68562	23.23	23.23	1.48	0.044	0
WITHIN	6.0	1.67880	23.23	23.23	1.47	0.043	0
WITHIN	8.0	1.67000	23.23	23.23	1.45	0.043	0
WITHIN	10.0	1.65646	23.23	23.23	1.42	0.043	0
WITHIN	12.0	1.63757	23.23	23.23	1.38	0.042	0
WITHIN	14.0	1.61185	23.23	23.23	1.32	0.041	0
WITHIN	16.0	1.57660	23.23	23.23	1.25	0.040	0
WITHIN	18.0	1.56412	23.23	23.23	1.23	0.040	0
WITHIN	21.0	1.54101	23.23	23.23	1.18	0.039	0
WITHIN	24.0	1.51312	23.23	23.23	1.13	0.038	0
WITHIN	29.0	1.60606	23.32	23.32	1.32	0.033	0
WITHIN	33.0	1.69507	23.32	23.32	1.92	0.031	0
WITHIN	37.0	1.73299	23.32	23.32	2.43	0.034	0

1***** OPTION 5 *** COMPUTE MOTION IN NEW SUBLAYERS

EARTHQUAKE - SECTION C-C, 08/2002
SOIL DEPOSIT - Transporter Route, HBPP, ISFSI, 08/

LAYER	DEPTH FT	MAX. ACC. G	TIME SEC	TIME C/SEC	MEAN SQ. FR. QUIET ZONE	ACC. RATIO ACC. RECORD	PUNCHED CARDS
WITHIN	41.0	1.71407	24.73	24.73	3.07	0.059	0
WITHIN	45.0	2.07663	24.72	24.72	3.23	0.071	0
WITHIN	50.0	2.07655	24.72	24.72	3.21	0.071	0
WITHIN	55.0	2.06499	24.72	24.72	3.18	0.071	0
WITHIN	60.0	2.02559	24.72	24.72	3.08	0.071	0
WITHIN	65.0	1.96794	24.72	24.72	2.94	0.071	0
WITHIN	70.0	1.89348	24.72	24.72	2.77	0.071	0
WITHIN	75.0	1.82792	23.06	23.06	2.59	0.071	0
WITHIN	80.0	1.78352	23.05	23.05	2.43	0.069	0
WITHIN	85.0	1.75479	23.03	23.03	2.33	0.068	0
OUTCR.	85.0	2.23585	23.03	23.03	3.08	0.069	2048

XMAX= 1.6874 SECTION C-C, 08/2002

ACCELERATION VALUES AT OUTCROPPING LAYER 1 - Transporter Route, HBPP, ISFSI, 08/									
0.000621	0.001445	0.002224	0.002928	0.003534	0.004020	0.004369	0.004569		1
0.004613	0.004499	0.004231	0.003820	0.003279	0.002629	0.001892	0.001094		2
0.000265	-0.000566	-0.001371	-0.002119	-0.002784	-0.003343	-0.003775	-0.004065		3
-0.004202	-0.004182	-0.004004	-0.003676	-0.003208	-0.002617	-0.001924	-0.001153		4
-0.000332	0.000510	0.001343	0.002138	0.002866	0.003501	0.004022	0.004409		5
0.004648	0.004731	0.004655	0.004422	0.004042	0.003526	0.002894	0.002168		6
0.001374	0.000539	-0.000305	-0.001129	-0.001904	-0.002602	-0.003198	-0.003670		7
-0.004001	-0.004181	-0.004200	-0.004060	-0.003763	-0.003322	-0.002751	-0.002070		8
-0.001302	-0.000477	0.000380	0.001235	0.002060	0.002826	0.003505	0.004073		9
0.004512	0.004804	0.004941	0.004917	0.004734	0.004399	0.003924	0.003327		10
0.002629	0.001855	0.001035	0.000198	-0.000625	-0.001404	-0.002109	-0.002716		11
-0.003200	-0.003543	-0.003731	-0.003756	-0.003615	-0.003310	-0.002851	-0.002253		12
-0.001532	-0.000714	0.000177	0.001110	0.002056	0.002984	0.003864	0.004669		13
0.005373	0.005956	0.006400	0.006695	0.006833	0.006815	0.006647	0.006339		14
0.005908	0.005376	0.004766	0.004108	0.003431	0.002766	0.002143	0.001593		15
0.001143	0.000815	0.000631	0.000605	0.000746	0.001058	0.001538	0.002179		16
0.002965	0.003879	0.004896	0.005989	0.007128	0.008282	0.009417	0.010502		17
0.011506	0.012402	0.013165	0.013777	0.014222	0.014492	0.014582	0.014498		18
0.014247	0.013844	0.013309	0.012665	0.011940	0.011163	0.010365	0.009580		19
0.008835	0.008162	0.007585	0.007128	0.006806	0.006632	0.006613	0.006751		20
0.007037	0.007464	0.008012	0.008663	0.009390	0.010168	0.010963	0.011747		21
0.012487	0.013156	0.013724	0.014171	0.014473	0.014620	0.014598	0.014409		22
0.014051	0.013535	0.012874	0.012089	0.011201	0.010239	0.009232	0.008214		23
0.007213	0.006263	0.005391	0.004628	0.003992	0.003505	0.003176	0.003017		24
0.003026	0.003199	0.003526	0.003991	0.004571	0.005243	0.005977	0.006744		25
0.007509	0.008243	0.008913	0.009492	0.009952	0.010276	0.010442	0.010445		26
0.010275	0.009937	0.009434	0.008784	0.008001	0.007112	0.006139	0.005118		27
0.004075	0.003047	0.002063	0.001156	0.000352	-0.000323	-0.000852	-0.001217		28
-0.001413	-0.001433	-0.001285	-0.000975	-0.000521	-0.000059	0.000737	0.001488		29
0.002278	0.003077	0.003849	0.004566	0.005193	0.005709	0.006086	0.006310		30
0.006364	0.006247	0.005954	0.005495	0.004878	0.004125	0.003254	0.002296		31
0.001276	0.000232	-0.000808	-0.001807	-0.002737	-0.003565	-0.004269	-0.004824		32
-0.005218	-0.005436	-0.005478	-0.005344	-0.005043	-0.004589	-0.004003	-0.003306		33
-0.002532	-0.001706	-0.000867	-0.000044	0.000727	0.001418	0.001997	0.002444		34
0.002734	0.002858	0.002804	0.002574	0.002167	0.001600	0.000884	0.000045		35
-0.000894	-0.001901	-0.002947	-0.003994	-0.005014	-0.005969	-0.006834	-0.007577		36
-0.008180	-0.008622	-0.008894	-0.008988	-0.008905	-0.008652	-0.008243	-0.007694		37
-0.007030	-0.006278	-0.005469	-0.004633	-0.003806	-0.003019	-0.002303	-0.001687		38
-0.001195	-0.000847	-0.000658	-0.000637	-0.000786	-0.001100	-0.001572	-0.002185		39
-0.002918	-0.003746	-0.004642	-0.005573	-0.006509	-0.007416	-0.008263	-0.009023		40
-0.009670	-0.010182	-0.010543	-0.010745	-0.010782	-0.010657	-0.010377	-0.009959		41
-0.009420	-0.008787	-0.008086	-0.007348	-0.006607	-0.005894	-0.005242	-0.004681		42
-0.004237	-0.003931	-0.003782	-0.003800	-0.003991	-0.004352	-0.004875	-0.005546		43
-0.006343	-0.007242	-0.008211	-0.009218	-0.010227	-0.011203	-0.012109	-0.012913		44
-0.013584	-0.014096	-0.014430	-0.014570	-0.014509	-0.014248	-0.013793	-0.013161		45
-0.012370	-0.011450	-0.010433	-0.009357	-0.008261	-0.007188	-0.006178	-0.005272		46
-0.004508	-0.003918	-0.003530	-0.003366	-0.003438	-0.003752	-0.004306	-0.005088		47
-0.006079	-0.007250	-0.008569	-0.009995	-0.011483	-0.012986	-0.014455	-0.015840		48
-0.017093	-0.018172	-0.019035	-0.019651	-0.019993	-0.020046	-0.019798	-0.019254		49
-0.018421	-0.017322	-0.015983	-0.014442	-0.012740	-0.010927	-0.009053	-0.007174		50
-0.005342	-0.003611	-0.002031	-0.000646	0.000505	0.001390	0.001989	0.002287		51
0.002281	0.001976	0.001390	0.000546	-0.000521	-0.001772	-0.003160	-0.004637		52
-0.006148	-0.007643	-0.009066	-0.010371	-0.011512	-0.012450	-0.013154	-0.013602		53
-0.013778	-0.013679	-0.013309	-0.012684	-0.011826	-0.010769	-0.009548	-0.008212		54
-0.006804	-0.005380	-0.003987	-0.002680	-0.001503	-0.000504	0.000283	0.000825		55
0.001100	0.001092	0.000797	0.000218	-0.000631	-0.001730	-0.003049	-0.004554		56
-0.006202	-0.007951	-0.009752	-0.011559	-0.013324	-0.015005	-0.016559	-0.017953		57
-0.019159	-0.020154	-0.020925	-0.021468	-0.021783	-0.021882	-0.021780	-0.021504		58
-0.021080	-0.020542	-0.019925	-0.019266	-0.018599	-0.017962	-0.017384	-0.016892		59
-0.016508	-0.016248	-0.016120	-0.016126	-0.016261	-0.016515	-0.016867	-0.017297		60
-0.017765	-0.018276	-0.018763	-0.019208	-0.019578	-0.019847	-0.019991	-0.019994		61
-0.019841	-0.019529	-0.019061	-0.018448	-0.017706	-0.016864	-0.015951	-0.015006		62
-0.014069	-0.013187	-0.012403	-0.011763	-0.011308	-0.011079	-0.011106	-0.011415		63
-0.012023	-0.012937	-0.014153	-0.015659	-0.017430	-0.019432	-0.021619	-0.023940		64
-0.026335	-0.028739	-0.031082	-0.033297	-0.035312	-0.037063	-0.038487	-0.039533		65
-0.040153	-0.040317	-0.039998	-0.039192	-0.037898	-0.036139	-0.033942	-0.031355		66
-0.028429	-0.025233	-0.021835	-0.018321	-0.014767	-0.011264	-0.007887	-0.004722		67
-0.001836	0.000701	0.002840	0.004534	0.005759	0.006494	0.006744	0.006517		68
0.005845	0.004764	0.003329	0.001600	-0.000353	-0.002456	-0.004629	-0.006797		69

16384	0.5							
8								
7	1	10	100.					
	11	100.	#1 modulus for Clay PI 15 (Vucetic and Dobry 1991)					
0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1	0.316	
1.	3.16	10.						
1.000	1.000	1.000	.94	.82	.64	.40	.21	
.09	.04	.02						
	11	1.	damping for Clay PI 15 (Vucetic & Dobry 1991)					
0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1	0.316	
1.	3.16	10.						
1.7	1.7	1.7	2.6	4.5	7.8	11.7	16.3	
20.2	23.0	23.0						
	11	100.	#2 modulus for Sand (20 to 50 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.000	0.999	0.991	0.953	0.830	0.620	0.364	0.181	
0.071	0.025	0.010						
	11	1.	damping for Sand (20 to 50 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.250	1.300	1.455	2.080	3.750	6.925	12.600	18.905	
24.840	27.2	28.9						
	11	100.	#3 modulus for Sand (50 to 120 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.000	1.000	0.995	0.972	0.879	0.701	0.442	0.230	
0.097	0.037	0.014						
	11	1.	damping for Sand (50 to 120 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.090	1.145	1.300	1.665	2.865	5.415	10.465	16.560	
22.915	25.5	27.0						
	11	100.	#4 modulus for Sand (120 to 250 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.000	1.000	0.996	0.980	0.910	0.756	0.510	0.283	
0.122	0.050	0.019						
	11	1.	damping for Sand (120 to 250 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
0.935	0.935	1.090	1.455	2.340	4.375	8.695	14.580	
21.250	23.8	25.5						
	11	100.	#5 modulus for Sand (250 to 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.000	1.000	0.997	0.986	0.932	0.809	0.573	0.338	
0.152	0.067	0.025						
	11	1.	damping for Sand (250 to 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
0.800	0.800	0.900	1.145	1.875	3.490	7.185	12.705	
19.270	22.4	24.0						
	11	100.	#6 modulus for Sand (> 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
1.000	1.000	0.998	0.991	0.955	0.860	0.658	0.417	
0.207	0.083	0.032						
	11	1.	damping for Sand (> 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3	
1.	3.	10.						
0.570	0.625	0.625	0.850	1.280	2.500	5.520	10.260	
16.770	20.2	22.5						

```

11 100. #7 modulus for Weathered Rock
0.0001 0.0003 0.001 0.003 0.01 0.03 0.1 0.3
1. 3. 10.
1.000 1.000 1.000 0.990 0.960 0.900 0.75 0.55
0.34 0.2 0.12
11 1. damping for Weathered Rock
0.0001 0.0003 0.001 0.003 0.01 0.03 0.1 0.3
1. 3. 10.
0.24 0.42 0.8 1.4 2.8 5.1 9.8 15.5
21. 25. 28.

2
1 25 4 Transporter Route, HBPP, ISFSI, 08/2002
1 1 1 1.0 .05 .125 915. 1.
2 1 1 2.0 .05 .125 915. 1.
3 1 1 3.0 .05 .125 915. 1.
4 1 1 2.0 .05 .125 915. 1.
5 1 .1 2.0 .05 .125 915. 1.
6 1 1 2.0 .05 .125 915. 1.
7 1 1 2.0 .05 .125 915. 1.
8 1 1 2.0 .05 .125 915. 1.
9 1 1 2.0 .05 .130 1220. 1.
10 1 1 3.0 .05 .130 1220. 1.
11 1 1 3.0 .05 .130 1220. 1.
12 2 1 5.0 .05 .130 1. 120. 1.
13 2 1 4.0 .05 .130 1. 135. 1.
14 2 1 4.0 .05 .130 1. 135. 1.
15 2 1 4.0 .05 .130 1. 128. 1.
16 2 1 4.0 .05 .130 1. 128. 1.
17 1 1 5.0 .05 .130 1830. 1.
18 1 1 5.0 .05 .130 1830. 1.
19 3 1 5.0 .05 .130 1. 188. 1.
20 3 1 5.0 .05 .130 1. 188. 1.
21 3 1 5.0 .05 .130 1. 188. 1.
22 3 1 5.0 .05 .130 1. 188. 1.
23 3 1 5.0 .05 .130 1. 188. 1.
24 3 1 5.0 .05 .130 1. 188. 1.
25 .05 .130 1800. 1.

1
1599916384 .005 2(8E15.7) SET 3, SECTION C-C, 08/2002
1. 2.5
S3CC.AC8
3
1 0
4
0 30 2. 0.65
5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 0 0 0 0 0 0 0 0 0 0 0 0 0 0
5
16 17 18 19 20 21 22 23 24 25 25
1 1 1 1 1 1 1 1 1 1 0
0 0 0 0 0 0 0 0 0 0 1
0

```

Set3:

15999	.00500								
-.327900E-03	-.323720E-03	-.327444E-03	-.323427E-03	-.327283E-03	-.323334E-03	-.327358E-03	-.323638E-03	-.327551E-03	-.323666E-03
-.327704E-03	-.324066E-03	-.328352E-03	-.324811E-03	-.328279E-03	-.325909E-03	-.328464E-03	-.325951E-03	-.328516E-03	-.328796E-03
-.331937E-03	-.328796E-03	-.333723E-03	-.330695E-03	-.335732E-03	-.332815E-03	-.337978E-03	-.335162E-03	-.339811E-03	-.343438E-03
-.340558E-03	-.337812E-03	-.343438E-03	-.340705E-03	-.346480E-03	-.343877E-03	-.349811E-03	-.347228E-03	-.353378E-03	-.350882E-03
-.353378E-03	-.350882E-03	-.357160E-03	-.354699E-03	-.361225E-03	-.358792E-03	-.365451E-03	-.363155E-03	-.369953E-03	-.367707E-03
-.369953E-03	-.367707E-03	-.374900E-03	-.372621E-03	-.379847E-03	-.377698E-03	-.385137E-03	-.383080E-03	-.389901E-03	-.388901E-03
-.390852E-03	-.388901E-03	-.396912E-03	-.395027E-03	-.403379E-03	-.401706E-03	-.410416E-03	-.408771E-03	-.417957E-03	-.416585E-03
-.417957E-03	-.416585E-03	-.426221E-03	-.425051E-03	-.435198E-03	-.434390E-03	-.445130E-03	-.444501E-03	-.455681E-03	-.455681E-03
-.455681E-03	-.455681E-03	-.467758E-03	-.468003E-03	-.480898E-03	-.481749E-03	-.495454E-03	-.496870E-03	-.511618E-03	-.513847E-03
-.511618E-03	-.513847E-03	-.529710E-03	-.532824E-03	-.549840E-03	-.553964E-03	-.572338E-03	-.57786E-03	-.596938E-03	-.602970E-03
-.596938E-03	-.602970E-03	-.623929E-03	-.630976E-03	-.653238E-03	-.661185E-03	-.684619E-03	-.69338E-03	-.717657E-03	-.726958E-03
-.717657E-03	-.726958E-03	-.752133E-03	-.761897E-03	-.788287E-03	-.799099E-03	-.826727E-03	-.838510E-03	-.867480E-03	-.880156E-03
-.867480E-03	-.880156E-03	-.910419E-03	-.923919E-03	-.955306E-03	-.970201E-03	-.100447E-02	-.102301E-02	-.106177E-02	-.108506E-02
-.106177E-02	-.108506E-02	-.112945E-02	-.115874E-02	-.121042E-02	-.124749E-02	-.130816E-02	-.135489E-02	-.142494E-02	-.147844E-02
-.142494E-02	-.147844E-02	-.155384E-02	-.161221E-02	-.169234E-02	-.175456E-02	-.183783E-02	-.190199E-02	-.198620E-02	-.204976E-02
-.198620E-02	-.204976E-02	-.213180E-02	-.219047E-02	-.226520E-02	-.233331E-02	-.237708E-02	-.241544E-02	-.246874E-02	-.249484E-02
-.246874E-02	-.249484E-02	-.253379E-02	-.254266E-02	-.256172E-02	-.254854E-02	-.254345E-02	-.250408E-02	-.247125E-02	-.240318E-02
-.247125E-02	-.240318E-02	-.234185E-02	-.224539E-02	-.215639E-02	-.203505E-02	-.192434E-02	-.178336E-02	-.165591E-02	-.150309E-02
-.165591E-02	-.150309E-02	-.136946E-02	-.121603E-02	-.108765E-02	-.944495E-03	-.82254E-03	-.712301E-03	-.626453E-03	-.534555E-03
-.626453E-03	-.534555E-03	-.479361E-03	-.420771E-03	-.402240E-03	-.378801E-03	-.349712E-03	-.319504E-03	-.284317E-03	-.244769E-03
-.244769E-03	-.244769E-03	-.487426E-03	-.501421E-03	-.527684E-03	-.531862E-03	-.559149E-03	-.560819E-03	-.578143E-03	-.569934E-03
-.578143E-03	-.569934E-03	-.577596E-03	-.567830E-03	-.561433E-03	-.565029E-03	-.565014E-03	-.546933E-03	-.544317E-03	-.514330E-03
-.544317E-03	-.514330E-03	-.506700E-03	-.474546E-03	-.454079E-03	-.432694E-03	-.395039E-03	-.352539E-03	-.330243E-03	-.283656E-03
-.330243E-03	-.283656E-03	-.266576E-03	-.225748E-03	-.211264E-03	-.175877E-03	-.160602E-03	-.12791E-03	-.119912E-03	-.936809E-04
-.119912E-03	-.936809E-04	-.914179E-04	-.720324E-04	-.770482E-04	-.635330E-04	-.752978E-04	-.710523E-04	-.910197E-04	-.921860E-04
-.910197E-04	-.921860E-04	-.118279E-03	-.128901E-03	-.160792E-03	-.163778E-03	-.184418E-03	-.191963E-03	-.223460E-03	-.230055E-03
-.223460E-03	-.230055E-03	-.262801E-03	-.276555E-03	-.303880E-03	-.325789E-03	-.395662E-03	-.439168E-03	-.493688E-03	-.537424E-03
-.493688E-03	-.537424E-03	-.600339E-03	-.633958E-03	-.699621E-03	-.745374E-03	-.789329E-03	-.838510E-03	-.859960E-03	-.891181E-03
-.859960E-03	-.891181E-03	-.935383E-03	-.966637E-03	-.101801E-02	-.103964E-02	-.110092E-02	-.116074E-02	-.123084E-02	-.127141E-02
-.123084E-02	-.127141E-02	-.134255E-02	-.139641E-02	-.146922E-02	-.152093E-02	-.159400E-02	-.164753E-02	-.171643E-02	-.175930E-02
-.175930E-02	-.175930E-02	-.182963E-02	-.187961E-02	-.193308E-02	-.195523E-02	-.200549E-02	-.203616E-02	-.208095E-02	-.210007E-02
-.208095E-02	-.210007E-02	-.213904E-02	-.216799E-02	-.222333E-02	-.224784E-02	-.229158E-02	-.231026E-02	-.233408E-02	-.233711E-02
-.233408E-02	-.233711E-02	-.236412E-02	-.236388E-02	-.238218E-02	-.236307E-02	-.234914E-02	-.232733E-02	-.231777E-02	-.227019E-02
-.231777E-02	-.227019E-02	-.228658E-02	-.231001E-02	-.231856E-02	-.229853E-02	-.231684E-02	-.230628E-02	-.231955E-02	-.230308E-02
-.231955E-02	-.230308E-02	-.226967E-02	-.221063E-02	-.218344E-02	-.212692E-02	-.208979E-02	-.203788E-02	-.200509E-02	-.192840E-02
-.200509E-02	-.192840E-02	-.183937E-02	-.173476E-02	-.166371E-02	-.155412E-02	-.146468E-02	-.134521E-02	-.123470E-02	-.116641E-02
-.123470E-02	-.116641E-02	-.109969E-02	-.109969E-02	-.103016E-02	-.991962E-03	-.978316E-03	-.923223E-03	-.903294E-03	-.873648E-03
-.903294E-03	-.873648E-03	-.736524E-03	-.484194E-03	-.422852E-03	-.387113E-03	-.268756E-03	-.104850E-03	-.170214E-04	-.148038E-03
-.148038E-03	-.148038E-03	-.272186E-03	-.426915E-03	-.558058E-03	-.663028E-03	-.769772E-03	-.892819E-03	-.100568E-02	-.109296E-02
-.100568E-02	-.109296E-02	-.111254E-02	-.117435E-02	-.123618E-02	-.129119E-02	-.130788E-02	-.137609E-02	-.146942E-02	-.156831E-02
-.146942E-02	-.156831E-02	-.155313E-02	-.154357E-02	-.162447E-02	-.175985E-02	-.179491E-02	-.184178E-02	-.190711E-02	-.197923E-02
-.190711E-02	-.197923E-02	-.201643E-02	-.208446E-02	-.211647E-02	-.217035E-02	-.221917E-02	-.230064E-02	-.226530E-02	-.226113E-02
-.226530E-02	-.226113E-02	-.227398E-02	-.227624E-02	-.227272E-02	-.220643E-02	-.218218E-02	-.212922E-02	-.205482E-02	-.213782E-02
-.205482E-02	-.213782E-02	-.216222E-02	-.213527E-02	-.216134E-02	-.218769E-02	-.194632E-02	-.170338E-02	-.159462E-02	-.144203E-02
-.159462E-02	-.144203E-02	-.116494E-02	-.101156E-02	-.900483E-03	-.715481E-03	-.576717E-03	-.697314E-03	-.795723E-03	-.749888E-03
-.795723E-03	-.749888E-03	-.764522E-03	-.924022E-03	-.830806E-03	-.518478E-03	-.285225E-03	-.141931E-03	-.115642E-03	-.357306E-03
-.115642E-03	-.357306E-03	-.626704E-03	-.902164E-03	-.103783E-02	-.102968E-02	-.117541E-02	-.141968E-02	-.162528E-02	-.172326E-02
-.162528E-02	-.172326E-02	-.181944E-02	-.191873E-02	-.211779E-02	-.235126E-02	-.255130E-02	-.271088E-02	-.294208E-02	-.311126E-02
-.294208E-02	-.311126E-02	-.331231E-02	-.352732E-02	-.353306E-02	-.331535E-02	-.328114E-02	-.328223E-02	-.310744E-02	-.281554E-02
-.310744E-02	-.281554E-02	-.285224E-02	-.326228E-02	-.357304E-02	-.361901E-02	-.386888E-02	-.419710E-02	-.437096E-02	-.452889E-02
-.437096E-02	-.452889E-02	-.471604E-02	-.465282E-02	-.453217E-02	-.452814E-02	-.452536E-02	-.438720E-02	-.432117E-02	-.425797E-02
-.432117E-02	-.425797E-02	-.404423E-02	-.375007E-02	-.354742E-02	-.326995E-02	-.309784E-02	-.312469E-02	-.312067E-02	-.298443E-02
-.312067E-02	-.298443E-02	-.287645E-02	-.267467E-02	-.243468E-02	-.223153E-02	-.219541E-02	-.223846E-02	-.222601E-02	-.215250E-02
-.222601E-02	-.215250E-02	-.214614E-02	-.212461E-02	-.216253E-02	-.207873E-02	-.193735E-02	-.158913E-02	-.142832E-02	-.114723E-02
-.142832E-02	-.114723E-02	-.109644E-02	-.121586E-02	-.118234E-02	-.107948E-02	-.111080E-02	-.115111E-02	-.112347E-02	-.100437E-02
-.112347E-02	-.100437E-02	-.703461E-03	-.395796E-03	-.283790E-03	-.185080E-03	-.338686E-04	-.146288E-03	-.299541E-03	-.466387E-03
-.299541E-03	-.466387E-03	-.524301E-03	-.670251E-03	-.967072E-03	-.119244E-02	-.135904E-02	-.165005E-02	-.164939E-02	-.144034E-02
-.164939E-02	-.144034E-02	-.141974E-02	-.143242E-02	-.126126E-02	-.120542E-02	-.106447E-02	-.839401E-03	-.106525E-02	-.165272E-02
-.106525E-02	-.165272E-02	-.186610E-02	-.200190E-02	-.244009E-02	-.284084E-02	-.300027E-02	-.312265E-02	-.297301E-02	-.267231E-02
-.297301E-02	-.267231E-02	-.254056E-02	-.244446E-02	-.212940E-02	-.190070E-02	-.175114E-02	-.146574E-02	-.122297E-02	-.139068E-02
-.122297E-02	-.139068E-02	-.157360E-02	-.149368E-02	-.139136E-02	-.139839E-02	-.127013E-02	-.115234E-02	-.109216E-02	-.919265E-03
-.109216E-02	-.919265E-03	-.589501E-03	-.382878E-03	-.183447E-03	-.126206E-03	-.365526E-03	-.576016E-03	-.108290E-02	-.110104E-02
-.108290E-02	-.110104E-02	-.283132E-03	-.305204E-03	-.448701E-03	-.915636E-03	-.137916E-02	-.194231E-02	-.258072E-02	-.236344E-02
-.258072E-02	-.236344E-02	-.143838E-02	-.118295E-02	-.116569E-02	-.728173E-03	-.316209E-03	-.877099E-03	-.537909E-03	-.663897E-03
-.537909E-03	-.663897E-03	-.357418E-03	-.283531E-03	-.426520E-03	-.366109E-03	-.446713E-03	-.630994E-03	-.482493E-03	-.114059E-03
-.482493E-03	-.114059E-03	-.322389E-03	-.678546E-04	-.336430E-03	-.669547E-03	-.813695E-03	-.907978E-03	-.111305E-02	-.148792E-02
-.111305E-02	-.148792E-02	-.279195E-02	-.210215E-02	-.247779E-02	-.258691E-02	-.259016E-02	-.309155E-02	-.302318E-02	-.185444E-02
-.302318E-02	-.185444E-02	-.995696E-03	-.630239E-03	-.138432E-03	-.680573E-03	-.902659E-03	-.130482E-02	-.186048E-02	-.242849E-02
-.186048E-02	-.242849E-02	-.239136E-03	-.149755E-02	-.115759E-02	-.139471E-02	-.			

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**
** SHAKE -- A COMPUTER PROGRAM FOR **
** EARTHQUAKE RESPONSE ANALYSIS **
** OF HORIZONTALLY LAYERED SITES **
**
**
** MS-DOS VERSION - CONVERTED TO IBM-PC BY **
** Shyh-Shiun Lai, WCC **
** January 1985 **
**
** (Modified to Use 16384 Points and 100 **
** Soil Layers, S.J. Chiou, August 1995) **
**
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Output file name : TR3C.OUT
Start time : 19**/**/ **
Start time : 19**/**/ **

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MAX. NUMBER OF TERMS IN FOURIER TRANSFORM = 16384
NECESSARY LENGTH OF BLANK COMMON X = 102419
EARTH PRESSURE AT REST FOR SAND = 0.500
1***** OPTION 8 *** READ RELATION BETWEEN SOIL PROPERTIES AND STRAIN

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CURVES FOR RELATION STRAIN VERSUS SHEAR MODULUS AND DAMPING

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
1	0.000100	1.000	0.000100	1.7
1	0.000316	1.000	0.000316	1.7
1	0.001000	1.000	0.001000	1.7
1	0.003160	0.940	0.003160	2.6
1	0.010000	0.820	0.010000	4.5
1	0.031600	0.640	0.031600	7.8
1	0.100000	0.400	0.100000	11.7
1	0.316000	0.210	0.316000	16.3
1	1.000000	0.090	1.000000	20.2
1	3.160000	0.040	3.160000	23.0
1	10.000000	0.020	10.000000	23.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
2	0.000100	1.000	0.000100	1.3
2	0.000300	0.999	0.000300	1.3
2	0.001000	0.991	0.001000	1.5
2	0.003000	0.953	0.003000	2.1
2	0.010000	0.830	0.010000	3.8
2	0.030000	0.620	0.030000	6.9
2	0.100000	0.364	0.100000	12.6
2	0.300000	0.181	0.300000	18.9
2	1.000000	0.071	1.000000	24.8
2	3.000000	0.025	3.000000	27.2
2	10.000000	0.010	10.000000	28.9

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
3	0.000100	1.000	0.000100	1.1
3	0.000300	1.000	0.000300	1.1
3	0.001000	0.995	0.001000	1.3
3	0.003000	0.972	0.003000	1.7
3	0.010000	0.879	0.010000	2.9
3	0.030000	0.701	0.030000	5.4
3	0.100000	0.442	0.100000	10.5
3	0.300000	0.230	0.300000	16.6
3	1.000000	0.097	1.000000	22.9
3	3.000000	0.037	3.000000	25.5
3	10.000000	0.014	10.000000	27.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
4	0.000100	1.000	0.000100	0.9
4	0.000300	1.000	0.000300	0.9
4	0.001000	0.996	0.001000	1.1
4	0.003000	0.980	0.003000	1.5
4	0.010000	0.910	0.010000	2.3
4	0.030000	0.756	0.030000	4.4
4	0.100000	0.510	0.100000	8.7
4	0.300000	0.283	0.300000	14.6
4	1.000000	0.122	1.000000	21.3
4	3.000000	0.050	3.000000	23.8
4	10.000000	0.019	10.000000	25.5

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
5	0.000100	1.000	0.000100	0.8
5	0.000300	1.000	0.000300	0.8
5	0.001000	0.997	0.001000	0.9
5	0.003000	0.986	0.003000	1.1
5	0.010000	0.932	0.010000	1.9
5	0.030000	0.809	0.030000	3.5
5	0.100000	0.573	0.100000	7.2
5	0.300000	0.338	0.300000	12.7
5	1.000000	0.152	1.000000	19.3
5	3.000000	0.067	3.000000	22.4
5	10.000000	0.025	10.000000	24.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
6	0.000100	1.000	0.000100	0.6
6	0.000300	1.000	0.000300	0.6
6	0.001000	0.998	0.001000	0.6
6	0.003000	0.991	0.003000	0.9
6	0.010000	0.955	0.010000	1.3
6	0.030000	0.860	0.030000	2.5
6	0.100000	0.658	0.100000	5.5
6	0.300000	0.427	0.300000	10.3
6	1.000000	0.207	1.000000	16.8
6	3.000000	0.083	3.000000	20.3
6	10.000000	0.032	10.000000	22.5

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
7	0.000100	1.000	0.000100	0.2
7	0.000300	1.000	0.000300	0.4
7	0.001000	1.000	0.001000	0.8
7	0.003000	0.990	0.003000	1.4
7	0.010000	0.960	0.010000	2.8
7	0.030000	0.900	0.030000	5.1
7	0.100000	0.750	0.100000	9.8
7	0.300000	0.550	0.300000	15.5
7	1.000000	0.340	1.000000	21.0
7	3.000000	0.200	3.000000	25.0
7	10.000000	0.120	10.000000	28.0

1***** OPTION 2 *** READ SOIL PROFILE

NEW SOIL PROFILE NO. 1 IDENTIFICATION Transporter Route, HBPP, ISFSI, 08/

NUMBER OF LAYERS 25 DEPTH TO BEDROCK 85.00
NUMBER OF FIRST SUBMERGED LAYER 4 DEPTH TO WATER LEVEL 6.00

LAYER	TYPE	MAX-MOD	THICKNESS	DEPTH	EFF. PRESS.	MODULUS	DAMPING	UNIT WEIGTH	SHEAR VEL	SVMAX
1	1	3250.097	1.00	0.50	0.063	3250.097	0.0500	0.1250	915.000	915.000
2	1	3250.097	2.00	2.00	0.250	3250.097	0.0500	0.1250	915.000	915.000
3	1	3250.097	3.00	4.50	0.563	3250.097	0.0500	0.1250	915.000	915.000
4	1	3250.097	2.00	7.00	0.813	3250.097	0.0500	0.1250	915.000	915.000
5	1	3250.097	2.00	9.00	0.938	3250.097	0.0500	0.1250	915.000	915.000
6	1	3250.097	2.00	11.00	1.063	3250.097	0.0500	0.1250	915.000	915.000
7	1	3250.097	2.00	13.00	1.188	3250.097	0.0500	0.1250	915.000	915.000
8	1	3250.097	2.00	15.00	1.313	3250.097	0.0500	0.1250	915.000	915.000
9	1	6009.068	2.00	17.00	1.444	6009.068	0.0500	0.1300	1220.000	1220.000
10	1	6009.068	3.00	19.50	1.613	6009.068	0.0500	0.1300	1220.000	1220.000
11	1	6009.068	3.00	22.50	1.815	6009.068	0.0500	0.1300	1220.000	1220.000
12	2	4474.783	5.00	26.50	2.086	4474.783	0.0500	0.1300	1052.791	1052.791
13	2	5388.738	4.00	31.00	2.390	5388.738	0.0500	0.1300	1155.313	1155.313
14	2	5685.408	4.00	35.00	2.660	5685.408	0.0500	0.1300	1186.689	1186.689
15	2	5657.528	4.00	39.00	2.931	5657.528	0.0500	0.1300	1183.818	1183.818
16	2	5913.175	4.00	43.00	3.201	5913.175	0.0500	0.1300	1210.226	1210.226
17	1	13520.403	5.00	47.50	3.505	13520.403	0.0500	0.1300	1830.000	1830.000
18	1	13520.403	5.00	52.50	3.843	13520.403	0.0500	0.1300	1830.000	1830.000
19	3	9925.974	5.00	57.50	4.181	9925.974	0.0500	0.1300	1567.988	1567.988
20	3	10319.356	5.00	62.50	4.519	10319.356	0.0500	0.1300	1598.757	1598.757
21	3	10698.285	5.00	67.50	4.857	10698.285	0.0500	0.1300	1627.846	1627.846
22	3	11064.243	5.00	72.50	5.195	11064.243	0.0500	0.1300	1655.454	1655.454
23	3	11418.479	5.00	77.50	5.533	11418.479	0.0500	0.1300	1681.746	1681.746
24	3	11762.051	5.00	82.50	5.871	11762.051	0.0500	0.1300	1706.859	1706.859
25	BASE					13081.	0.050	0.1300	1800.	

PERIOD = 0.25 FROM AVERAGE SHEARVEL. = 1366.

MAXIMUM AMPLIFICATION = 13.99
FOR FREQUENCY = 4.42 C/SEC.
PERIOD = 0.23 SEC.

1***** OPTION 1 *** READ INPUT MOTION

EARTHQUAKE - SECTION C-C, 08/2002

excerpt from TR3C.OUT

15999 ACCELERATION VALUES AT TIME INTERVAL 0.0050

THE VALUES ARE LISTED ROW BY ROW AS READ FROM CARDS
TRAILING ZEROS ARE ADDED TO GIVE A TOTAL OF 16384 VALUES

MAXIMUM ACCELERATION = 1.63302
AT TIME = 23.28 SEC

THE VALUES WILL BE MULTIPLIED BY A FACTOR = 1.000
TO GIVE NEW MAXIMUM ACCELERATION = 1.63302

MEAN SQUARE FREQUENCY = 0.94 C/SEC.

MAX ACCELERATION = 1.69520 FOR FREQUENCIES REMOVED ABOVE 2.50 C/SEC.

1***** OPTION 3 *** READ WHERE OBJECT MOTION IS GIVEN

OBJECT MOTION IN LAYER NUMBER 1 OUTCROPPING

1***** OPTION 4 *** OBTAIN STRAIN COMPATIBLE SOIL PROPERTIES

MAXIMUM NUMBER OF ITERATIONS = 30
MAXIMUM ERROR IN PERCENT = 2.00
FACTOR FOR EFFECTIVE STRAIN IN TIME DOMAIN = 0.65

EARTHQUAKE - SECTION C-C, 08/2002
SOIL PROFILE - Transporter Route, HBPP, ISFSI, 08/

ITERATION NUMBER 1
THE CALCULATION HAS BEEN CARRIED OUT IN THE TIME DOMAIN WITH EFF. STRAIN = .65* MAX. STRAIN

LAYER	TYPE	DEPTH	EFF. STRAIN	NEW DAMP.	DAMP USED	ERROR	NEW G	G USED	ERROR	NEW Vs
1	1	0.5	0.00217	0.023	0.050	-116.9	3118.931	3250.097	-4.2	896.346
2	1	2.0	0.00867	0.043	0.050	-17.2	2713.292	3250.097	-19.8	836.029
3	1	4.5	0.01951	0.064	0.050	22.1	2325.214	3250.097	-39.8	773.935
4	1	7.0	0.03035	0.077	0.050	34.9	2100.648	3250.097	-54.7	735.613
5	1	9.0	0.03901	0.085	0.050	41.3	1937.442	3250.097	-67.8	706.459
6	1	11.0	0.04767	0.092	0.050	45.6	1801.731	3250.097	-80.4	681.268
7	1	13.0	0.05432	0.098	0.050	48.8	1688.814	3250.097	-92.4	659.575
8	1	15.0	0.06496	0.102	0.050	51.2	1592.149	3250.097	-104.1	640.420
9	1	17.0	0.03990	0.086	0.050	41.8	3553.937	6009.068	-69.1	938.234
10	1	19.5	0.04596	0.091	0.050	44.9	3376.767	6009.068	-78.0	914.549
11	1	22.5	0.05323	0.096	0.050	47.7	3192.916	6009.068	-88.2	889.304
12	2	26.5	0.08448	0.118	0.050	57.6	1789.268	4474.783	-150.1	665.724
13	2	31.0	0.08226	0.117	0.050	57.2	2185.265	5388.738	-146.6	735.713
14	2	35.0	0.08814	0.120	0.050	58.3	2222.149	5685.408	-155.9	741.896
15	2	39.0	0.09875	0.125	0.050	60.1	2074.578	5657.928	-172.7	716.838
16	2	43.0	0.10421	0.128	0.050	61.0	2111.799	5913.175	-180.0	723.240
17	1	47.5	0.05034	0.094	0.050	46.7	7341.397	13520.403	-84.2	1348.484
18	1	52.5	0.05543	0.097	0.050	48.5	7060.176	13520.403	-91.5	1322.404
19	3	57.5	0.08295	0.097	0.050	48.4	4786.344	9925.974	-107.4	1088.825
20	3	62.5	0.08668	0.099	0.050	49.3	4878.533	10319.356	-111.5	1099.261
21	3	67.5	0.09023	0.100	0.050	50.2	4965.297	10698.285	-115.5	1108.993
22	3	72.5	0.09362	0.102	0.050	50.9	5047.265	11064.243	-119.2	1118.109
23	3	77.5	0.09687	0.103	0.050	51.6	5124.965	11418.479	-122.8	1126.683
24	3	82.5	0.10000	0.105	0.050	52.2	5198.848	11762.051	-126.2	1134.775

VALUES IN TIME DOMAIN

LAYER	TYPE	THICKNESS FT	DEPTH FT	MAX STRAIN PRCNT	MAX STRESS PSF	TIME SEC
1	1	1.0	0.5	0.00334	104.04	23.47
2	1	2.0	2.0	0.01334	362.02	23.47
3	1	3.0	4.5	0.03002	697.98	23.47
4	1	2.0	7.0	0.04669	980.72	23.47
5	1	2.0	9.0	0.06001	1162.73	23.47
6	1	2.0	11.0	0.07333	1321.26	23.47
7	1	2.0	13.0	0.08664	1463.20	23.47
8	1	2.0	15.0	0.09994	1591.14	23.47
9	1	2.0	17.0	0.06138	2181.40	23.47
10	1	3.0	19.5	0.07071	2387.76	23.47
11	1	3.0	22.5	0.08190	2614.92	23.47
12	2	5.0	26.5	0.12997	2325.56	23.47
13	2	4.0	31.0	0.12655	2765.52	23.47
14	2	4.0	35.0	0.13559	3013.12	23.47
15	2	4.0	39.0	0.15193	3151.87	23.47
16	2	4.0	43.0	0.16032	3385.63	23.47
17	1	5.0	47.5	0.07745	5685.78	23.46
18	1	5.0	52.5	0.08558	6042.09	23.46
19	3	5.0	57.5	0.12762	6108.37	23.46

		FT	FT	PRCNT	PSF	SEC
1	1	1.0	0.5	0.00344	107.15	23.45
2	1	2.0	2.0	0.01646	433.08	23.47
3	1	3.0	4.5	0.04701	985.79	23.47
4	1	2.0	7.0	0.09503	1545.38	23.48
5	1	2.0	9.0	0.15320	1996.01	23.48
6	1	2.0	11.0	0.22188	2448.47	23.48
7	1	2.0	13.0	0.31998	2902.22	23.49
8	1	2.0	15.0	0.49805	3358.52	23.49
9	1	2.0	17.0	0.15888	3768.07	23.48
10	1	3.0	19.5	0.20549	4349.04	23.48
11	1	3.0	22.5	0.27755	5046.20	23.48
12	2	5.0	26.5	6.12252	5884.31	23.52
13	2	4.0	31.0	2.84760	6939.04	23.51
14	2	4.0	35.0	6.58769	7703.14	23.51
15	2	4.0	39.0	8.74897	8431.08	23.50
16	2	4.0	43.0	9.78218	9047.57	23.49
17	1	5.0	47.5	0.20346	9733.69	23.41
18	1	5.0	52.5	0.24327	10667.61	23.39
19	3	5.0	57.5	0.56229	11619.50	23.39
20	3	5.0	62.5	0.62205	12647.65	23.38
21	3	5.0	67.5	0.68916	13692.24	23.36
22	3	5.0	72.5	0.76422	14737.28	23.36
23	3	5.0	77.5	0.84908	15770.24	23.35
24	3	5.0	82.5	0.94845	16782.02	23.35

EARTHQUAKE - SECTION C-C, 08/2005
SOIL PROFILE - Transporter Route, HBPP, ISPSI, 08/

ITERATION NUMBER 25
THE CALCULATION HAS BEEN CARRIED OUT IN THE TIME DOMAIN WITH EFF. STRAIN = .65* MAX. STRAIN

LAYER	TYPE	DEPTH	EFF. STRAIN	NEW DAMP.	DAMP USED	ERROR	NEW C	G USED	ERROR	NEW Vs
1	1	0.5	0.00224	0.023	0.023	0.0	3113.650	3113.650	0.0	895.587
2	1	2.0	0.01070	0.047	0.047	0.0	2630.632	2630.632	0.0	823.195
3	1	4.5	0.03055	0.077	0.077	0.0	2097.184	2097.184	0.0	735.007
4	1	7.0	0.06177	0.101	0.101	0.0	1626.260	1626.260	0.0	647.244
5	1	9.0	0.09958	0.117	0.117	0.0	1302.897	1302.897	0.0	579.333
6	1	11.0	0.14422	0.132	0.132	0.0	1103.503	1103.503	0.0	533.163
7	1	13.0	0.20798	0.146	0.146	0.0	907.013	907.014	0.0	483.370
8	1	15.0	0.32373	0.164	0.164	0.0	674.338	674.339	0.0	416.785
9	1	17.0	0.10327	0.118	0.118	0.0	2371.702	2371.702	0.0	766.454
10	1	19.5	0.13357	0.129	0.129	0.0	2116.395	2116.395	0.0	724.027
11	1	22.5	0.18041	0.141	0.141	0.0	1818.109	1818.109	0.0	671.068
12	2	26.5	4.08162	0.276	0.276	0.1	94.705	96.125	-1.5	153.159
13	2	31.0	1.85363	0.262	0.262	0.0	243.352	243.680	-0.1	245.513
14	2	35.0	4.28145	0.277	0.277	0.0	116.941	116.932	0.0	170.192
15	2	39.0	5.65003	0.281	0.281	0.0	96.824	96.367	0.5	154.863
16	2	43.0	6.30281	0.282	0.283	0.0	93.137	92.490	0.7	151.886
17	1	47.5	0.13207	0.128	0.128	0.0	4787.027	4784.091	0.1	1088.903
18	1	52.5	0.15798	0.135	0.135	0.0	4387.168	4385.107	0.0	1042.434
19	3	57.5	0.36517	0.176	0.176	0.0	2067.426	2066.476	0.0	715.602
20	3	62.5	0.40402	0.181	0.181	0.0	2034.103	2033.235	0.0	709.811
21	3	67.5	0.44762	0.187	0.187	0.0	1987.676	1986.815	0.0	701.664
22	3	72.5	0.49635	0.192	0.192	0.0	1929.376	1928.418	0.0	691.297
23	3	77.5	0.55141	0.198	0.198	0.0	1858.454	1857.335	0.1	678.472
24	3	82.5	0.61590	0.204	0.204	0.0	1770.461	1769.413	0.1	662.253

VALUES IN TIME DOMAIN

LAYER	TYPE	THICKNESS FT	DEPTH FT	MAX STRAIN PRCNT	MAX STRESS PSF	TIME SEC
1	1	1.0	0.5	0.00344	107.15	23.45
2	1	2.0	2.0	0.01646	433.08	23.47
3	1	3.0	4.5	0.04701	985.79	23.47
4	1	2.0	7.0	0.09503	1545.38	23.48
5	1	2.0	9.0	0.15320	1996.01	23.48
6	1	2.0	11.0	0.22188	2448.47	23.48
7	1	2.0	13.0	0.31998	2902.23	23.49
8	1	2.0	15.0	0.49805	3358.52	23.49
9	1	2.0	17.0	0.15888	3768.07	23.48
10	1	3.0	19.5	0.20549	4349.04	23.48
11	1	3.0	22.5	0.27755	5046.20	23.48
12	2	5.0	26.5	6.27941	5946.93	23.52
13	2	4.0	31.0	2.85174	6939.78	23.51
14	2	4.0	35.0	6.58685	7702.75	23.51
15	2	4.0	39.0	8.69236	8416.30	23.50
16	2	4.0	43.0	9.69663	9031.19	23.49
17	1	5.0	47.5	0.20319	9726.87	23.41
18	1	5.0	52.5	0.24304	10662.77	23.39
19	3	5.0	57.5	0.56180	11614.77	23.39
20	3	5.0	62.5	0.62137	12643.42	23.36
21	3	5.0	67.5	0.68865	13688.20	23.36
22	3	5.0	72.5	0.76362	14733.05	23.36
23	3	5.0	77.5	0.84833	15765.74	23.35
24	3	5.0	82.5	0.94754	16777.73	23.35

PERIOD = 0.57 FROM AVERAGE SHEARVEL. = 599.
 MAXIMUM AMPLIFICATION = 2.24
 FOR FREQUENCY = 0.92 C/SEC.
 PERIOD = 1.09 SEC.

1***** OPTION 5 *** COMPUTE MOTION IN NEW SUBLAYERS

EARTHQUAKE - SECTION C-C, 08/2002
 SOIL DEPOSIT - Transporter Route, HBPP, ISFSI, 08/

LAYER	DEPTH FT	MAX. ACC. G	ACC. SEC	TIME C/SEC	MEAN SQ. FR. QUIET ZONE	ACC. RATIO ACC. RECORD	PUNCHED CARDS
OUTCR.	0.0	1.69520		23.45	0.94	0.070	2048
WITHIN	1.0	1.69517		23.45	0.94	0.070	0
WITHIN	3.0	1.69487		23.45	0.94	0.070	0
WITHIN	6.0	1.69367		23.45	0.94	0.070	0
WITHIN	8.0	1.69210		23.45	0.94	0.070	0
WITHIN	10.0	1.68963		23.45	0.94	0.070	0
WITHIN	12.0	1.68615		23.45	0.93	0.069	0
WITHIN	14.0	1.68126		23.45	0.92	0.069	0
WITHIN	16.0	1.67415		23.44	0.91	0.068	0
WITHIN	18.0	1.67173		23.44	0.91	0.067	0
WITHIN	21.0	1.66714		23.44	0.90	0.067	0
WITHIN	24.0	1.66108		23.44	0.89	0.066	0
WITHIN	29.0	1.61182		23.36	0.73	0.052	0
WITHIN	33.0	1.63585		23.34	0.76	0.055	0
WITHIN	37.0	1.70526		23.31	0.96	0.067	0

1***** OPTION 5 *** COMPUTE MOTION IN NEW SUBLAYERS

EARTHQUAKE - SECTION C-C, 08/2002
 SOIL DEPOSIT - Transporter Route, HBPP, ISFSI, 08/

LAYER	DEPTH FT	MAX. ACC. G	ACC. SEC	TIME C/SEC	MEAN SQ. FR. QUIET ZONE	ACC. RATIO ACC. RECORD	PUNCHED CARDS
WITHIN	41.0	1.78205		23.30	1.28	0.083	0
WITHIN	45.0	1.82975		23.28	1.50	0.097	0
WITHIN	50.0	1.82806		23.28	1.50	0.097	0
WITHIN	55.0	1.82387		23.28	1.50	0.097	0
WITHIN	60.0	1.81094		23.28	1.49	0.097	0
WITHIN	65.0	1.79372		23.28	1.48	0.096	0
WITHIN	70.0	1.77138		23.28	1.46	0.096	0
WITHIN	75.0	1.74401		23.27	1.43	0.094	0
WITHIN	80.0	1.71175		23.27	1.40	0.093	0
WITHIN	85.0	1.67434		23.27	1.36	0.091	0
OUTCR.	85.0	1.78635		23.24	1.45	0.100	2048

XMAX= 1.6952 SECTION C-C, 08/2002

ACCELERATION VALUES AT OUTCROPPING LAYER 1 - Transporter Route, HBPP, ISFS1, 08/

-0.000814-0.000917-0.001015-0.001108-0.001196-0.001278-0.001354-0.001422	1
-0.001483-0.001537-0.001582-0.001619-0.001648-0.001668-0.001679-0.001681	2
-0.001675-0.001660-0.001636-0.001603-0.001563-0.001514-0.001458-0.001395	3
-0.001324-0.001247-0.001164-0.001076-0.000983-0.000885-0.000784-0.000680	4
-0.000573-0.000465-0.000356-0.000246-0.000137-0.000029 0.000077 0.000181	5
0.000282 0.000378 0.000471 0.000558 0.000640 0.000716 0.000785 0.000847	6
0.000902 0.000949 0.000987 0.001017 0.001038 0.001051 0.001054 0.001048	7
0.001033 0.001009 0.000976 0.000934 0.000884 0.000825 0.000757 0.000683	8
0.000600 0.000511 0.000415 0.000313 0.000206 0.000094-0.000022-0.000142	9
-0.000265-0.000390-0.000517-0.000645-0.000773-0.000901-0.001027-0.001152	10
-0.001275-0.001394-0.001510-0.001621-0.001728-0.001829-0.001924-0.002013	11
-0.002095-0.002170-0.002237-0.002297-0.002348-0.002391-0.002426-0.002453	12
-0.002471-0.002481-0.002482-0.002475-0.002459-0.002436-0.002406-0.002368	13
-0.002323-0.002271-0.002214-0.002151-0.002082-0.002010-0.001933-0.001852	14
-0.001769-0.001684-0.001597-0.001509-0.001420-0.001332-0.001245-0.001160	15
-0.001076-0.000995-0.000917-0.000843-0.000773-0.000709-0.000648-0.000594	16
-0.000546-0.000504-0.000468-0.000439-0.000416-0.000401-0.000392-0.000391	17
-0.000396-0.000409-0.000428-0.000454-0.000486-0.000524-0.000568-0.000617	18
-0.000671-0.000730-0.000793-0.000859-0.000928-0.000999-0.001072-0.001147	19
-0.001222-0.001297-0.001371-0.001444-0.001515-0.001584-0.001649-0.001711	20
-0.001767-0.001820-0.001867-0.001908-0.001943-0.001972-0.001993-0.002007	21
-0.002013-0.002011-0.002001-0.001984-0.001957-0.001924-0.001881-0.001831	22
-0.001772-0.001706-0.001632-0.001552-0.001464-0.001371-0.001271-0.001166	23
-0.001056-0.000942-0.000824-0.000704-0.000580-0.000457-0.000331-0.000206	24
-0.000081 0.000042 0.000163 0.000281 0.000396 0.000505 0.000611 0.000709	25
0.000802 0.000886 0.000964 0.001033 0.001094 0.001144 0.001185 0.001215	26
0.001236 0.001245 0.001244 0.001231 0.001207 0.001171 0.001125 0.001067	27
0.000998 0.000918 0.000829 0.000728 0.000618 0.000498 0.000371 0.000234	28
0.000090-0.000061-0.000218-0.000381-0.000548-0.000720-0.000894-0.001071	29
-0.001248-0.001428-0.001605-0.001783-0.001957-0.002129-0.002297-0.002461	30
-0.002618-0.002770-0.002913-0.003050-0.003178-0.003297-0.003406-0.003505	31
-0.003593-0.003671-0.003735-0.003790-0.003830-0.003861-0.003877-0.003882	32
-0.003873-0.003854-0.003820-0.003777-0.003720-0.003653-0.003574-0.003486	33
-0.003386-0.003278-0.003159-0.003035-0.002900-0.002761-0.002613-0.002462	34
-0.002304-0.002145-0.001981-0.001816-0.001648-0.001481-0.001313-0.001147	35
-0.000981-0.000821-0.000660-0.000507-0.000355-0.000211-0.000070 0.000061	36
0.000189 0.000306 0.000419 0.000521 0.000617 0.000703 0.000782 0.000850	37
0.000912 0.000963 0.001008 0.001041 0.001069 0.001086 0.001099 0.001101	38
0.001099 0.001087 0.001072 0.001049 0.001024 0.000991 0.000958 0.000918	39
0.000878 0.000834 0.000791 0.000744 0.000700 0.000654 0.000612 0.000569	40
0.000530 0.000492 0.000460 0.000429 0.000404 0.000382 0.000367 0.000355	41
0.000351 0.000351 0.000358 0.000369 0.000388 0.000411 0.000441 0.000475	42
0.000517 0.000562 0.000613 0.000667 0.000727 0.000789 0.000855 0.000922	43
0.000993 0.001063 0.001136 0.001206 0.001277 0.001345 0.001413 0.001475	44
0.001536 0.001590 0.001640 0.001683 0.001720 0.001748 0.001770 0.001781	45
0.001785 0.001777 0.001760 0.001731 0.001692 0.001640 0.001578 0.001502	46
0.001416 0.001316 0.001205 0.001081 0.000946 0.000798 0.000640 0.000470	47
0.000290 0.000100-0.000099-0.000308-0.000524-0.000748-0.000977-0.001213	48
-0.001452-0.001696-0.001941-0.002189-0.002436-0.002683-0.002927-0.003170	49
-0.003406-0.003640-0.003864-0.004083-0.004292-0.004492-0.004680-0.004857	50
-0.005020-0.005172-0.005306-0.005428-0.005531-0.005620-0.005689-0.005743	51
-0.005776-0.005793-0.005789-0.005769-0.005727-0.005669-0.005590-0.005494	52
-0.005378-0.005247-0.005096-0.004931-0.004747-0.004550-0.004336-0.004112	53
-0.003872-0.003623-0.003361-0.003093-0.002813-0.002530-0.002238-0.001944	54
-0.001645-0.001347-0.001045-0.000748-0.000450-0.000158 0.000131 0.000412	55
0.000688 0.000952 0.001210 0.001453 0.001688 0.001907 0.002116 0.002307	56
0.002485 0.002645 0.002792 0.002918 0.003030 0.003122 0.003198 0.003254	57
0.003296 0.003316 0.003322 0.003308 0.003279 0.003232 0.003172 0.003093	58
0.003003 0.002897 0.002781 0.002650 0.002511 0.002359 0.002202 0.002035	59
0.001863 0.001684 0.001504 0.001318 0.001134 0.000946 0.000763 0.000578	60
0.000400 0.000224 0.000056-0.000108-0.000262-0.000410-0.000545-0.000673	61
-0.000787-0.000891-0.000981-0.001061-0.001124-0.001176-0.001212-0.001236	62
-0.001244-0.001240-0.001219-0.001187-0.001140-0.001081-0.001008-0.000925	63
-0.000829-0.000723-0.000607-0.000483-0.000349-0.000210-0.000063 0.000087	64
0.000243 0.000400 0.000560 0.000719 0.000879 0.001035 0.001190 0.001339	65
0.001485 0.001622 0.001754 0.001876 0.001989 0.002091 0.002184 0.002263	66
0.002331 0.002384 0.002426 0.002451 0.002464 0.002461 0.002444 0.002411	67
0.002365 0.002303 0.002227 0.002137 0.002034 0.001916 0.001788 0.001646	68
0.001495 0.001333 0.001162 0.000983 0.000798 0.000606 0.000411 0.000211	69

16384	0.5						
8							
7	1	10	100.				
11	100.	#1 modulus for Clay PI 15 (Vucetic and Dobry 1991)					
0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1	0.316
1.	3.16	10.					
1.000	1.000	1.000	.94	.82	.64	.40	.21
.09	.04	.02					
11	1.	damping for Clay PI 15 (Vucetic & Dobry 1991)					
0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1	0.316
1.	3.16	10.					
1.7	1.7	1.7	2.6	4.5	7.8	11.7	16.3
20.2	23.0	23.0					
11	100.	#2 modulus for Sand (20 to 50 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.000	0.999	0.991	0.953	0.830	0.620	0.364	0.181
0.071	0.025	0.010					
11	1.	damping for Sand (20 to 50 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.250	1.300	1.455	2.080	3.750	6.925	12.600	18.905
24.840	27.2	28.9					
11	100.	#3 modulus for Sand (50 to 120 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.000	1.000	0.995	0.972	0.879	0.701	0.442	0.230
0.097	0.037	0.014					
11	1.	damping for Sand (50 to 120 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.090	1.145	1.300	1.665	2.865	5.415	10.465	16.560
22.915	25.5	27.0					
11	100.	#4 modulus for Sand (120 to 250 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.000	1.000	0.996	0.980	0.910	0.756	0.510	0.283
0.122	0.050	0.019					
11	1.	damping for Sand (120 to 250 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
0.935	0.935	1.090	1.455	2.340	4.375	8.695	14.580
21.250	23.8	25.5					
11	100.	#5 modulus for Sand (250 to 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.000	1.000	0.997	0.986	0.932	0.809	0.573	0.338
0.152	0.067	0.025					
11	1.	damping for Sand (250 to 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
0.800	0.800	0.900	1.145	1.875	3.490	7.185	12.705
19.270	22.4	24.0					
11	100.	#6 modulus for Sand (> 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
1.000	1.000	0.998	0.991	0.955	0.860	0.658	0.417
0.207	0.083	0.032					
11	1.	damping for Sand (> 500 ft) (EPRI 1993)					
0.0001	0.0003	0.001	0.003	0.01	0.03	0.1	0.3
1.	3.	10.					
0.570	0.625	0.625	0.850	1.280	2.500	5.520	10.260
16.770	20.2	22.5					

```

11 100. #7 modulus for Weathered Rock
0.0001 0.0003 0.001 0.003 0.01 0.03 0.1 0.3
1. 3. 10.
1.000 1.000 1.000 0.990 0.960 0.900 0.75 0.55
0.34 0.2 0.12
11 1. damping for Weathered Rock
0.0001 0.0003 0.001 0.003 0.01 0.03 0.1 0.3
1. 3. 10.
0.24 0.42 0.8 1.4 2.8 5.1 9.8 15.5
21. 25. 28.

2
1 25 4 Transporter Route, HBPP, ISFSI, 08/2002
1 1 1 1.0 0.023 .125 895.587 1.
2 1 1 2.0 0.047 .125 823.195 1.
3 1 1 3.0 0.077 .125 735.007 1.
4 1 1 2.0 0.101 .125 647.244 1.
5 1 1 2.0 0.117 .125 579.333 1.
6 1 1 2.0 0.132 .125 533.163 1.
7 1 1 2.0 0.146 .125 483.370 1.
8 1 1 2.0 0.164 .125 416.785 1.
9 1 1 2.0 0.118 .130 766.454 1.
10 1 1 3.0 0.129 .130 724.027 1.
11 1 1 3.0 0.141 .130 671.068 1.
12 2 1 5.0 0.276 .130 153.159 1.
13 2 1 4.0 0.262 .130 245.513 1.
14 2 1 4.0 0.277 .130 170.192 1.
15 2 1 4.0 0.281 .130 154.863 1.
16 2 1 4.0 0.282 .130 151.886 1.
17 1 1 5.0 0.128 .130 1088.903 1.
18 1 1 5.0 0.135 .130 1042.434 1.
19 3 1 5.0 0.176 .130 715.602 1.
20 3 1 5.0 0.181 .130 709.811 1.
21 3 1 5.0 0.187 .130 701.664 1.
22 3 1 5.0 0.192 .130 691.297 1.
23 3 1 5.0 0.198 .130 678.472 1.
24 3 1 5.0 0.204 .130 662.253 1.
25 .05 .130 1800. 1.

1
1599916384 .005 2(8E15.7) SET 3, SECTION C-C, 08/2002
1. 6.
S3CC.AC8
3
1 0
5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 0 0 0 0 0 0 0 0 0 0 0 0 0 0
5
16 17 18 19 20 21 22 23 24 25 25
1 1 1 1 1 1 1 1 1 1 0
0 0 0 0 0 0 0 0 0 0 1
0

```

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..
.. SHAKE -- A COMPUTER PROGRAM FOR ..
.. EARTHQUAKE RESPONSE ANALYSIS ..
.. OF HORIZONTALLY LAYERED SITES ..
..
.. MS-DOS VERSION - CONVERTED TO IBM-PC BY ..
.. Shyh-Shiun Lai, WCC ..
.. January 1985 ..
..
.. (Modified to Use 16384 Points and 100 ..
.. Soil Layers, S.J. Chiou, August 1995) ..
..
.....
    
```

Output file name : TR3CI.OUT
 Start time : 19''/''/'' --
 Start time : 19''/''/'' --

MAX. NUMBER OF TERMS IN FOURIER TRANSFORM = 16384
 NECESSARY LENGTH OF BLANK COMMON X = 102419
 EARTH PRESSURE AT REST FOR SAND = 0.500
 ***** OPTION 8 *** READ RELATION BETWEEN SOIL PROPERTIES AND STRAIN

CURVES FOR RELATION STRAIN VERSUS SHEAR MODULUS AND DAMPING

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
1	0.000100	1.000	0.000100	1.7
1	0.000316	1.000	0.000316	1.7
1	0.001000	1.000	0.001000	1.7
1	0.003160	0.940	0.003160	2.6
1	0.010000	0.820	0.010000	4.5
1	0.031600	0.640	0.031600	7.8
1	0.100000	0.400	0.100000	11.7
1	0.316000	0.210	0.316000	16.3
1	1.000000	0.090	1.000000	20.2
1	3.160000	0.040	3.160000	23.0
1	10.000000	0.020	10.000000	23.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
2	0.000100	1.000	0.000100	1.3
2	0.000300	0.999	0.000300	1.3
2	0.001000	0.991	0.001000	1.5
2	0.003000	0.953	0.003000	2.1
2	0.010000	0.830	0.010000	3.8
2	0.030000	0.620	0.030000	6.9
2	0.100000	0.364	0.100000	12.6
2	0.300000	0.181	0.300000	18.9
2	1.000000	0.071	1.000000	24.6
2	3.000000	0.025	3.000000	27.2
2	10.000000	0.010	10.000000	28.9

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
3	0.000100	1.000	0.000100	1.1
3	0.000300	1.000	0.000300	1.1
3	0.001000	0.995	0.001000	1.3
3	0.003000	0.972	0.003000	1.7
3	0.010000	0.879	0.010000	2.9
3	0.030000	0.701	0.030000	5.4
3	0.100000	0.442	0.100000	10.5
3	0.300000	0.230	0.300000	16.6
3	1.000000	0.097	1.000000	22.9
3	3.000000	0.037	3.000000	25.5
3	10.000000	0.014	10.000000	27.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
4	0.000100	1.000	0.000100	0.9
4	0.000300	1.000	0.000300	0.9
4	0.001000	0.996	0.001000	1.1
4	0.003000	0.980	0.003000	1.5
4	0.010000	0.910	0.010000	2.3
4	0.030000	0.756	0.030000	4.4
4	0.100000	0.510	0.100000	8.7
4	0.300000	0.283	0.300000	14.6
4	1.000000	0.122	1.000000	21.3
4	3.000000	0.050	3.000000	23.8
4	10.000000	0.019	10.000000	25.5

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
5	0.000100	1.000	0.000100	0.8
5	0.000300	1.000	0.000300	0.8
5	0.001000	0.997	0.001000	0.9
5	0.003000	0.986	0.003000	1.1
5	0.010000	0.912	0.010000	1.9
5	0.030000	0.809	0.030000	3.5
5	0.100000	0.573	0.100000	7.2
5	0.300000	0.138	0.300000	12.7
5	1.000000	0.152	1.000000	19.3
5	3.000000	0.067	3.000000	22.4
5	10.000000	0.025	10.000000	24.0

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
6	0.000100	1.000	0.000100	0.6
6	0.000300	1.000	0.000300	0.6
6	0.001000	0.998	0.001000	0.6
6	0.003000	0.991	0.003000	0.9
6	0.010000	0.955	0.010000	1.3
6	0.030000	0.860	0.030000	2.5
6	0.100000	0.658	0.100000	5.5
6	0.300000	0.417	0.300000	10.3
6	1.000000	0.207	1.000000	16.8
6	3.000000	0.083	3.000000	20.2
6	10.000000	0.032	10.000000	22.5

MATL TYPE	STRAIN (%)	MOD RED CO	STRAIN (%)	DAMP FACTR
7	0.000100	1.000	0.000100	0.2
7	0.000300	1.000	0.000300	0.4
7	0.001000	1.000	0.001000	0.8
7	0.003000	0.990	0.003000	1.4
7	0.010000	0.960	0.010000	2.8
7	0.030000	0.900	0.030000	5.1
7	0.100000	0.750	0.100000	9.8
7	0.300000	0.550	0.300000	15.5
7	1.000000	0.340	1.000000	21.0
7	3.000000	0.200	3.000000	25.0
7	10.000000	0.120	10.000000	28.0

1***** OPTION 2 *** READ SOIL PROFILE

NEW SOIL PROFILE NO. 1 IDENTIFICATION Transporter Route, HBPP, ISFSI, 08/

NUMBER OF LAYERS 25 DEPTH TO BEDROCK 85.00
NUMBER OF FIRST SUBMERGED LAYER 4 DEPTH TO WATER LEVEL 6.00

LAYER	TYPE	MAX-MOD	THICKNESS	DEPTH	EFF. PRESS.	MODULUS	DAMPING	UNIT WEIGHT	SHEAR VEL	SVMAX
1	1	3113.649	1.00	0.50	0.063	3113.649	0.0230	0.1250	895.587	895.587
2	1	2630.629	2.00	2.00	0.250	2630.629	0.0470	0.1250	823.195	823.195
3	1	2097.187	3.00	4.50	0.563	2097.187	0.0770	0.1250	735.007	735.007
4	1	1626.261	2.00	7.00	0.813	1626.261	0.1010	0.1250	647.244	647.244
5	1	1302.899	2.00	9.00	0.938	1302.899	0.1170	0.1250	579.333	579.333
6	1	1103.505	2.00	11.00	1.063	1103.505	0.1320	0.1250	533.163	533.163
7	1	907.013	2.00	13.00	1.188	907.013	0.1460	0.1250	483.370	483.370
8	1	674.339	2.00	15.00	1.313	674.339	0.1640	0.1250	416.785	416.785
9	1	2371.699	2.00	17.00	1.444	2371.699	0.1180	0.1300	766.454	766.454
10	1	2116.396	3.00	19.50	1.613	2116.396	0.1290	0.1300	724.027	724.027
11	1	1818.111	3.00	22.50	1.815	1818.111	0.1410	0.1300	671.068	671.068
12	2	94.705	5.00	26.50	2.086	94.705	0.2760	0.1300	153.159	153.159
13	2	243.353	4.00	31.00	2.390	243.353	0.2620	0.1300	245.513	245.513
14	2	116.941	4.00	35.00	2.660	116.941	0.2770	0.1300	170.192	170.192
15	2	96.824	4.00	39.00	2.931	96.824	0.2810	0.1300	154.863	154.863
16	2	93.137	4.00	43.00	3.201	93.137	0.2810	0.1300	151.886	151.886
17	1	4787.026	5.00	47.50	3.505	4787.026	0.1280	0.1300	1088.903	1088.903
18	1	4387.171	5.00	52.50	3.843	4387.171	0.1350	0.1300	1042.434	1042.434
19	3	2067.429	5.00	57.50	4.181	2067.429	0.1760	0.1300	715.602	715.602
20	3	2034.103	5.00	62.50	4.519	2034.103	0.1810	0.1300	709.811	709.811
21	3	1987.677	5.00	67.50	4.857	1987.677	0.1870	0.1300	701.664	701.664
22	3	1929.376	5.00	72.50	5.195	1929.376	0.1920	0.1300	691.297	691.297
23	3	1858.452	5.00	77.50	5.533	1858.452	0.1980	0.1300	678.472	678.472
24	3	1770.661	5.00	82.50	5.871	1770.661	0.2040	0.1300	662.253	662.253
25	BASE					13081.	0.050	0.1300	1800.	

PERIOD = 0.57 FROM AVERAGE SHEARVEL. = 599.

MAXIMUM AMPLIFICATION = 2.25
FOR FREQUENCY = 0.92 C/SEC.
PERIOD = 1.09 SEC.

1***** OPTION 1 *** READ INPUT MOTION

EARTHQUAKE - SECTION C-C, 08/2002

15999 ACCELERATION VALUES AT TIME INTERVAL 0.0050

THE VALUES ARE LISTED ROW BY ROW AS READ FROM CARDS
TRAILING ZEROS ARE ADDED TO GIVE A TOTAL OF 16384 VALUES

MAXIMUM ACCELERATION = 1.63302
AT TIME = 23.28 SEC

THE VALUES WILL BE MULTIPLIED BY A FACTOR = 1.000
TO GIVE NEW MAXIMUM ACCELERATION = 1.63302

MEAN SQUARE FREQUENCY = 1.28 C/SEC.

MAX ACCELERATION = 1.65117 FOR FREQUENCIES REMOVED ABOVE 6.00 C/SEC.

1***** OPTION 3 *** READ WHERE OBJECT MOTION IS GIVEN

OBJECT MOTION IN LAYER NUMBER 1 OUTCROPPING

1***** OPTION 5 *** COMPUTE MOTION IN NEW SUBLAYERS

EARTHQUAKE - SECTION C-C, 08/2002
SOIL DEPOSIT - Transporter Route, HBPP, ISFSI, 08/

LAYER	DEPTH FT	MAX. ACC. G	TIME SEC	MEAN SQ. FR. C/SEC QUIET ZONE	ACC. RATIO ACC. RECORD	PUNCHED CARDS
OUTCR.	0.0	1.65117	23.30	1.28	0.078	2048
WITHIN	1.0	1.65107	23.30	1.28	0.078	0
WITHIN	3.0	1.65016	23.30	1.27	0.078	0
WITHIN	6.0	1.64624	23.30	1.26	0.078	0
WITHIN	8.0	1.64097	23.30	1.24	0.078	0
WITHIN	10.0	1.63255	23.30	1.22	0.077	0
WITHIN	12.0	1.62068	23.31	1.19	0.077	0
WITHIN	14.0	1.60513	23.31	1.15	0.076	0
WITHIN	16.0	1.58338	23.31	1.09	0.075	0
WITHIN	18.0	1.57813	23.31	1.07	0.074	0
WITHIN	21.0	1.57133	23.31	1.04	0.073	0
WITHIN	24.0	1.57131	23.35	1.01	0.072	0
WITHIN	29.0	2.05920	23.19	2.66	0.062	0
WITHIN	33.0	2.18420	23.19	2.94	0.069	0
WITHIN	37.0	2.27066	34.56	2.95	0.077	0

1***** OPTION 5 *** COMPUTE MOTION IN NEW SUBLAYERS

EARTHQUAKE - SECTION C-C, 08/2002
SOIL DEPOSIT - Transporter Route, HBPP, ISFSI, 08/

LAYER	DEPTH FT	MAX. ACC. G	TIME SEC	MEAN SQ. FR. C/SEC QUIET ZONE	ACC. RATIO ACC. RECORD	PUNCHED CARDS
WITHIN	41.0	2.42340	34.53	3.29	0.101	0
WITHIN	45.0	2.50818	34.51	3.71	0.132	0
WITHIN	50.0	2.48717	34.51	3.69	0.133	0
WITHIN	55.0	2.43712	34.51	3.64	0.132	0
WITHIN	60.0	2.28811	34.51	3.46	0.130	0
WITHIN	65.0	2.08636	34.51	3.20	0.127	0
WITHIN	70.0	1.92147	23.42	2.92	0.120	0
WITHIN	75.0	1.90286	23.41	2.74	0.107	0
WITHIN	80.0	1.99199	23.40	2.88	0.098	0
WITHIN	85.0	2.14788	23.39	3.34	0.098	0
OUTCR.	85.0	2.52498	23.39	3.91	0.131	2048

XMAX= 1.6512 SECTION C-C, 08/2002

ACCELERATION VALUES AT OUTCROPPING LAYER 1 - Transporter Route, HBPP, ISFSI, 08/											
-0.001375-0.001443-0.001467-0.001446-0.001381-0.001275-0.001132-0.000958											1
-0.000758-0.000541-0.000314-0.000086 0.000135 0.000341 0.000525 0.000679											2
0.000799 0.000878 0.000916 0.000909 0.000858 0.000765 0.000633 0.000466											3
0.000270 0.000051-0.000181-0.000420-0.000657-0.000884-0.001092-0.001275											4
-0.001425-0.001538-0.001609-0.001637-0.001619-0.001557-0.001453-0.001310											5
-0.001133-0.000929-0.000705-0.000469-0.000229 0.000006 0.000228 0.000428											6
0.000600 0.000738 0.000836 0.000891 0.000900 0.000863 0.000782 0.000658											7
0.000496 0.000301 0.000081-0.000158-0.000407-0.000657-0.000901-0.001129											8
-0.001333-0.001507-0.001645-0.001741-0.001794-0.001800-0.001760-0.001676											9
-0.001551-0.001389-0.001197-0.000981-0.000750-0.000512-0.000275-0.000049											10
0.000158 0.000338 0.000485 0.000592 0.000656 0.000673 0.000643 0.000566											11
0.000443 0.000280 0.000080-0.000150-0.000402-0.000669-0.000941-0.001209											12
-0.001466-0.001702-0.001910-0.002084-0.002219-0.002311-0.002357-0.002357											13
-0.002313-0.002227-0.002103-0.001948-0.001768-0.001573-0.001369-0.001166											14
-0.000974-0.000800-0.000654-0.000542-0.000470-0.000443-0.000464-0.000535											15
-0.000654-0.000819-0.001027-0.001271-0.001545-0.001840-0.002146-0.002455											16
-0.002755-0.003038-0.003291-0.003508-0.003679-0.003799-0.003862-0.003865											17
-0.003806-0.003687-0.003508-0.003276-0.002995-0.002674-0.002321-0.001947											18
-0.001561-0.001176-0.000800-0.000447-0.000125 0.000157 0.000392 0.000573											19
0.000697 0.000761 0.000767 0.000713 0.000606 0.000450 0.000252 0.000021											20
-0.000234-0.000503-0.000775-0.001040-0.001288-0.001510-0.001696-0.001841											21
-0.001938-0.001984-0.001976-0.001915-0.001802-0.001643-0.001440-0.001202											22
-0.000936-0.000652-0.000359-0.000068 0.000212 0.000471 0.000701 0.000894											23
0.001044 0.001144 0.001194 0.001191 0.001136 0.001031 0.000882 0.000691											24
0.000469 0.000222-0.000039-0.000307-0.000570-0.000821-0.001047-0.001244											25
-0.001403-0.001518-0.001586-0.001604-0.001572-0.001493-0.001366-0.001201											26
-0.001001-0.000776-0.000532-0.000281-0.000031 0.000206 0.000422 0.000608											27
0.000756 0.000859 0.000912 0.000912 0.000858 0.000748 0.000588 0.000378											28
0.000126-0.000162-0.000476-0.000809-0.001149-0.001487-0.001812-0.002115											29
-0.002386-0.002620-0.002806-0.002943-0.003026-0.003055-0.003028-0.002952											30
-0.002826-0.002661-0.002461-0.002237-0.001995-0.001750-0.001507-0.001280											31
-0.001076-0.000905-0.000773-0.000688-0.000651-0.000668-0.000737-0.000858											32
-0.001026-0.001238-0.001485-0.001761-0.002054-0.002359-0.002659-0.002949											33
-0.003215-0.003452-0.003645-0.003793-0.003886-0.003924-0.003900-0.003819											34
-0.003678-0.003487-0.003245-0.002965-0.002650-0.002316-0.001967-0.001619											35
-0.001277-0.000958-0.000665-0.000412-0.000200-0.000041 0.000069 0.000120											36
0.000121 0.000067-0.000032-0.000174-0.000348-0.000549-0.000761-0.000981											37
-0.001192-0.001388-0.001555-0.001688-0.001774-0.001813-0.001793-0.001718											38
-0.001581-0.001390-0.001141-0.000847-0.000508-0.000138 0.000258 0.000664											39
0.001075 0.001474 0.001855 0.002203 0.002513 0.002771 0.002978 0.003122											40
0.003207 0.003226 0.003186 0.003087 0.002937 0.002740 0.002509 0.002249											41
0.001976 0.001696 0.001425 0.001170 0.000944 0.000752 0.000607 0.000509											42
0.000468 0.000481 0.000551 0.000673 0.000846 0.001059 0.001309 0.001583											43
0.001873 0.002164 0.002449 0.002712 0.002947 0.003139 0.003282 0.003367											44
0.003390 0.003344 0.003233 0.003052 0.002809 0.002504 0.002149 0.001749											45
0.001316 0.000860 0.000394-0.000071-0.000522-0.000950-0.001340-0.001688											46
-0.001982-0.002221-0.002397-0.002511-0.002563-0.002557-0.002497-0.002392											47
-0.002247-0.002076-0.001887-0.001694-0.001506-0.001338-0.001196-0.001095											48
-0.001039-0.001038-0.001094-0.001211-0.001386-0.001622-0.001909-0.002246											49
-0.002620-0.003024-0.003444-0.003871-0.004289-0.004689-0.005055-0.005379											50
-0.005647-0.005854-0.005989-0.006052-0.006036-0.005945-0.005778-0.005543											51
-0.005242-0.004891-0.004492-0.004065-0.003616-0.003164-0.002716-0.002292											52
-0.001896-0.001547-0.001247-0.001009-0.000833-0.000728-0.000686-0.000714											53
-0.000800-0.000943-0.001130-0.001355-0.001603-0.001865-0.002124-0.002373											54
-0.002594-0.002780-0.002916-0.002999-0.003017-0.002971-0.002852-0.002668											55
-0.002415-0.002103-0.001733-0.001321-0.000871-0.000400 0.000084 0.000564											56
0.001032 0.001469 0.001872 0.002223 0.002519 0.002749 0.002915 0.003007											57
0.003032 0.002987 0.002883 0.002720 0.002513 0.002266 0.001996 0.001709											58
0.001423 0.001145 0.000890 0.000665 0.000483 0.000346 0.000265 0.000238											59
0.000272 0.000359 0.000502 0.000688 0.000917 0.001174 0.001454 0.001739											60
0.002025 0.002292 0.002536 0.002740 0.002900 0.003003 0.003048 0.003026											61
0.002939 0.002785 0.002569 0.002294 0.001970 0.001602 0.001206 0.000788											62
0.000367-0.000050-0.000446-0.000811-0.001131-0.001399-0.001602-0.001739											63
-0.001801-0.001791-0.001704-0.001547-0.001323-0.001042-0.000710-0.000342											64
0.000055 0.000463 0.000872 0.001266 0.001635 0.001965 0.002248 0.002471											65
0.002632 0.002723 0.002743 0.002691 0.002572 0.002387 0.002146 0.001855											66
0.001526 0.001168 0.000796 0.000420 0.000053-0.000294-0.000609-0.000884											67
-0.001111-0.001284-0.001398-0.001454-0.001450-0.001392-0.001281-0.001127											68
-0.000935-0.000719-0.000485-0.000248-0.000015 0.000200 0.000389 0.000542											69

Attachment E

QUAD4MU

Input and Output Excerpts

(see Table 8-6 for listing of files)

HBSOILNW.DAT

4 FOR HUMBOLDT BAY POWER PLANT, 08/2002

11	#1 modulus for Clay PI 15 (Vucetic and Dobry 1991)						
	0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1 0.316
	1.	3.16	10.				
	1.000	1.000	1.000	.94	.82	.64	.40 .21
	.09	.04	.02				
11	damping for Clay PI 15 (Vucetic & Dobry 1991)						
	0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1 0.316
	1.	3.16	10.				
	1.7	1.7	1.7	2.6	4.5	7.8	11.7 16.3
	20.2	23.0	23.0				
11	#2 modulus for Sand (20 to 50 ft) (EPRI 1993)						
	0.0001	0.0003	0.001	0.003	0.01	0.03	0.1 0.3
	1.	3.	10.				
	1.000	0.999	0.991	0.953	0.830	0.620	0.364 0.181
	0.071	0.025	0.010				
11	damping for Sand (20 to 50 ft) (EPRI 1993)						
	0.0001	0.0003	0.001	0.003	0.01	0.03	0.1 0.3
	1.	3.	10.				
	1.250	1.300	1.455	2.080	3.750	6.925	12.600 18.905
	24.840	27.200	28.900				
11	#3 modulus for Clay PI 15 (Vucetic and Dobry 1991)						
	0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1 0.316
	1.	3.16	10.				
	1.000	1.000	1.000	.94	.82	.64	.40 .21
	.09	.04	.02				
11	damping for Clay PI 15 (Vucetic & Dobry 1991)						
	0.0001	0.000316	0.001	0.00316	0.01	0.0316	0.1 0.316
	1.	3.16	10.				
	1.7	1.7	1.7	2.6	4.5	7.8	11.7 16.3
	20.2	23.0	23.0				
11	#4 modulus for Sand (50 to 120 ft) (EPRI 1993)						
	0.0001	0.0003	0.001	0.003	0.01	0.03	0.1 0.3
	1.	3.	10.				
	1.000	1.000	0.995	0.972	0.879	0.701	0.442 0.230
	0.097	0.037	0.014				
11	damping for Sand (50 to 120 ft) (EPRI 1993)						
	0.0001	0.0003	0.001	0.003	0.01	0.03	0.1 0.3
	1.	3.	10.				
	1.090	1.145	1.300	1.665	2.865	5.415	10.465 16.560
	22.915	25.500	27.000				

TRIC.Q4I

TRIC: HOBGOLD BAY, TRANSPORTER BOUYT, PG&E, 89/2807

WRITE (E for Emulsion, S for Silt)

TRIC: HOBGOLD BAY, TRANSPORTER BOUYT, PG&E, 89/2807

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90	93	94	119	130	3	130.00	.47	13025.78	10900.62	.10000
91	94	95	120	119	4	130.00	.47	10344.71	8275.77	.10000
92	95	96	121	120	4	130.00	.47	10759.58	8606.86	.10000
93	96	97	122	121	4	130.00	.47	11541.87	9231.50	.10000
94	97	98	123	122	4	130.00	.47	11934.22	9531.30	.10000
95	98	99	124	123	4	130.00	.47	12275.28	9826.22	.10000
96	99	100	125	124	4	130.00	.47	12620.34	10120.34	.10000
97	101	102	127	124	1	125.00	.33	3275.43	2620.34	.10000
98	102	103	128	127	1	125.00	.33	3275.43	2620.34	.10000
99	103	104	128	128	1	125.00	.33	3275.43	2620.34	.10000
100	104	105	130	129	1	125.00	.47	3275.43	2620.34	.10000
101	105	106	131	130	1	125.00	.47	3275.43	2620.34	.10000
102	106	107	131	131	1	125.00	.47	3275.43	2620.34	.10000
103	107	108	131	132	1	125.00	.47	3275.43	2620.34	.10000
104	108	109	131	133	1	125.00	.47	3275.43	2620.34	.10000
105	109	110	133	134	1	125.00	.47	3275.43	2620.34	.10000
106	110	111	134	135	1	125.00	.47	3275.43	2620.34	.10000
107	111	112	137	136	1	125.00	.47	3275.43	2620.34	.10000
108	112	113	139	137	2	130.00	.47	4653.25	3721.60	.10000
109	113	114	139	138	2	130.00	.47	5610.63	4488.58	.10000
110	114	115	140	139	2	130.00	.47	5924.63	4739.70	.10000
111	115	116	141	140	2	130.00	.47	5877.10	4701.68	.10000
112	116	117	142	141	2	130.00	.47	6145.82	4914.66	.10000
113	117	118	143	142	2	130.00	.47	6425.78	5090.62	.10000
114	118	119	144	143	2	130.00	.47	6720.34	5400.00	.10000
115	119	120	145	144	4	130.00	.47	10344.71	8275.77	.10000
116	120	121	146	145	4	130.00	.47	10759.58	8606.86	.10000
117	121	122	147	146	4	130.00	.47	11541.87	9231.50	.10000
118	122	123	148	147	4	130.00	.47	11934.22	9531.30	.10000
119	123	124	149	148	4	130.00	.47	12275.28	9826.22	.10000
120	124	125	150	149	4	130.00	.47	12620.34	10120.34	.10000
121	126	127	152	151	1	125.00	.33	3275.43	2620.34	.10000
122	127	128	152	152	1	125.00	.33	3275.43	2620.34	.10000
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133	138	139	164	163	2	130.00	.47	4653.25	3721.60	.10000
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139	144	145	170	169	4	130.00	.47	10344.71	8275.77	.10000
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1084	1130	1131	1148	1147	1	125.00	-47	5822.96	4658.39	-10000	1227	1271	1274	1281	1289	2	130.00	-47	3726.34	2981.88	-10000
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1089	1138	1139	1152	1152	2	130.00	-47	5877.10	4701.88	-10000	1232	1278	1279	1286	1295	2	130.00	-47	4963.78	3990.62	-10000
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1097	1146	1147	1159	1159	2	130.00	-47	12375.28	9820.22	-10000	1240	1286	1287	1294	1303	2	130.00	-47	6067.78	4790.62	-10000
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1100	1149	1150	1162	1162	2	130.00	-47	12745.43	10202.34	-10000	1243	1289	1290	1297	1306	2	130.00	-47	6481.78	5090.62	-10000
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1102	1151	1152	1164	1164	2	130.00	-47	12745.43	10202.34	-10000	1245	1291	1292	1299	1308	2	130.00	-47	6757.78	5290.62	-10000
1103	1152	1153	1165	1165	2	130.00	-47	12745.43	10202.34	-10000	1246	1292	1293	1300	1309	2	130.00	-47	6895.78	5390.62	-10000
1104	1153	1154	1166	1166	2	130.00	-47	12745.43	10202.34	-10000	1247	1293	1294	1301	1310	2	130.00	-47	7033.78	5490.62	-10000
1105	1154	1155	1167	1167	2	130.00	-47	12745.43	10202.34	-10000	1248	1294	1295	1302	1311	2	130.00	-47	7171.78	5590.62	-10000
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1109	1158	1159	1171	1171	2	130.00	-47	12745.43	10202.34	-10000	1252	1298	1299	1306	1315	2	130.00	-47	7723.78	5990.62	-10000
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1111	1160	1161	1173	1173	2	130.00	-47	12745.43	10202.34	-10000	1254	1300	1301	1308	1317	2	130.00	-47	8000.00	6190.62	-10000
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1142																					

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1389	1440	1441	1456	1456	1	125.00	-47	9694.22	8718.06	-10000	1532	1585	1586	1611	1610	1	125.00	-47	3275.43	2620.34	-10000
1390	1441	1442	1456	1456	1	125.00	-47	10055.26	9081.10	-10000	1533	1586	1587	1612	1611	1	125.00	-47	3275.43	2620.34	-10000
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1399	1450	1451	1456	1456	1	125.00	-47	13308.10	12348.46	-10000	1542	1595	1596	1621	1620	1	125.00	-47	3275.43	2620.34	-10000
1400	1451	1452	1456	1456	1	125.00	-47	13669.72	12711.50	-10000	1543	1597	1598	1622	1622	1	125.00	-47	3275.43	2620.34	-10000
1401	1452	1453	1456	1456	1	125.00	-47	14031.34	13074.54	-10000	1544	1598	1599	1623	1623	1	125.00	-47	3275.43	2620.34	-10000
1402	1453	1454	1456	1456	1	125.00	-47	14392.96	13437.58	-10000	1545	1599	1600	1624	1624	1	125.00	-47	3275.43	2620.34	-10000
1403	1454	1455	1456	1456	1	125.00	-47	14754.58	13800.62	-10000	1546	1600	1601	1625	1625	1	125.00	-47	3275.43	2620.34	-10000
1404	1455	1456	1456	1456	1	125.00	-47	15116.20	14163.66	-10000	1547	1601	1602	1626	1626	1	125.00	-47	3275.43	2620.34	-10000
1405	1456	1457	1456	1456	1	125.00	-47	15477.82	14526.70	-10000	1548	1602	1603	1627	1627	1	125.00	-47	3275.43	2620.34	-10000
1406	1457	1458	1456	1456	1	125.00	-47	15839.44	14889.74	-10000	1549	1603	1604	1628	1628	1	125.00	-47	3275.43	2620.34	-10000
1407	1458	1459	1456	1456	1	125.00	-47	16201.06	15252.78	-10000	1550	1604	1605	1629	1629	1	125.00	-47	3275.43	2620.34	-10000
1408	1459	1460	1456	1456	1	125.00	-47	16562.68	15615.82	-10000	1551	1605	1606	1630	1630	1	125.00	-47	3275.43	2620.34	-10000
1409	1460	1461	1456	1456	1	125.00	-47	16924.30	15978.86	-10000	1552	1606	1607	1631	1631	1	125.00	-47	3275.43	2620.34	-10000
1410	1461	1462	1456	1456	1	125.00	-47	17285.92	16341.90	-10000	1553	1607	1608	1632	1632	1	125.00	-47	3275.43	2620.34	-10000
1411	1462	1463	1456	1456	1	125.00	-47	17647.54	16704.94	-10000	1554	1608	1609	1633	1633	1	125.00	-47	3275.43	2620.34	-10000
1412	1463	1464	1456	1456	1	125.00	-47	18009.16	17067.98	-10000	1555	1609	1610	1634	1634	1	125.00	-47	3275.43	2620.34	-10000
1413	1464	1465	1456	1456	1	125.00	-47	18370.78	17431.02	-10000	1556	1610	1611	1635	1635	1	125.00	-47	3275.43	2620.34	-10000
1414	1465	1466	1456	1456	1	125.00	-47	18732.40	17794.06	-10000	1557	1611	1612	1636	1636	1	125.00	-47	3275.43	2620.34	-10000
1415	1466	1467	1456	1456	1	125.00	-47	19094.02	18157.10	-10000	1558	1612	1613	1637	1637	1	125.00	-47	3275.43	2620.34	-10000
1416	1467	1468	1456	1456	1	125.00	-47	19455.64	18520.14	-10000	1559	1613	1614	1638	1638	1	125.00	-47	3275.43	2620.34	-10000
1417	1468	1469	1456	1456	1	125.00	-47	19817.26	18883.18	-10000	1560	1614	1615	1639	1639	1	125.00	-47	3275.43	2620.34	-10000
1418	1469	1470	1456	1456	1	125.00	-47	20178.88	19246.22	-10000	1561	1615	1616	1640	1640	1	125.00	-47	3275.43	2620.34	-10000
1419	1470	1471	1456	1456	1	125.00	-47	20540.50	19609.26	-10000	1562	1616	1617	1641	1641	1	125.00	-47	3275.43	2620.34	-10000
1420	1471	1472	1456	1456	1	125.00	-47	20902.12	19972.30	-10000	1563	1617	1618	1642	1642	1	125.00	-47	3275.43	2620.34	-10000
1421	1472	1473	1456	1456	1	125.00	-47	21263.74	20335.34	-10000	1564	1618	1619	1643	1643	1	125.00	-47	3275.43	2620.34	-10000
1422	1473	1474	1456	1456	1	125.00	-47	21625.36	20698.38	-10000	1565	1619	1620	1644	1644	1	125.00	-47	3275.43	2620.34	-10000
1423	1474	1475	1456	1456	1	125.00	-47	21986.98	21061.42	-10000	1566	1620	1621	1645	1645	1	125.00	-47	3275.43	2620.34	-10000
1424	1475	1476	1456	1456	1	125.00	-47	22348.60	21424.46	-10000	1567	1621	1622	1646	1646	1	125.00	-47	3275.43	2620.34	-10000
1425	1476	1477	1456	1456	1	125.00	-47	22710.22	21787.50	-10000	1568	1622	1623	1647	1647	1	125.00	-47	3275.43	2620.34	-10000
1426	1477	1478	1456	1456	1	125.00	-47	23071.84	22150.54	-10000	1569	1623	1624	1648	1648	1	125.00	-47	3275.43	2620.34	-10000
1427	1478	1479	1456	1456	1	125.00	-47	23433.46	22513.58	-10000	1570	1624	1625	1649	1649	1	125.00	-47	3275.43	2620.34	-10000
1428	1479	1480	1456																		

1658 1714 1715 1739 1737	4	120.00	.47	10714.05	8571.24	-10000	1799 1864 1865 1888 1887	1	125.00	.47	5822.98	4658.39	-10000
1657 1715 1728 1739 1738	4	120.00	.47	13111.17	8991.24	-10000	1800 1865 1866 1889 1888	1	125.00	.47	5822.98	4658.39	-10000
1658 1716 1717 1748 1749	4	120.00	.47	11668.24	7706.24	-10000	1801 1866 1867 1890 1889	1	125.00	.47	4205.20	3344.16	-10000
1659 1717 1718 1741 1740	4	120.00	.47	11874.43	9499.22	-10000	1802 1867 1868 1891 1890	1	120.00	.47	5163.53	4114.82	-10000
1660 1719 1720 1743 1742	4	125.00	.33	3275.43	2620.34	-10000	1803 1868 1869 1892 1891	2	120.00	.47	5484.24	4371.47	-10000
1661 1720 1721 1746 1745	4	125.00	.47	3275.43	2620.34	-10000	1804 1869 1870 1893 1892	2	120.00	.47	5484.24	4371.47	-10000
1662 1721 1722 1749 1748	4	125.00	.47	3275.43	2620.34	-10000	1805 1870 1871 1894 1893	2	120.00	.47	5484.24	4371.47	-10000
1663 1722 1723 1746 1745	4	125.00	.47	3275.43	2620.34	-10000	1806 1871 1872 1895 1894	2	120.00	.47	5484.24	4371.47	-10000
1664 1723 1724 1747 1746	4	125.00	.47	3275.43	2620.34	-10000	1807 1872 1873 1896 1895	2	120.00	.47	5484.24	4371.47	-10000
1665 1724 1725 1748 1747	4	125.00	.47	3275.43	2620.34	-10000	1808 1873 1874 1897 1896	4	120.00	.47	5484.24	4371.47	-10000
1666 1725 1726 1749 1748	4	125.00	.47	3275.43	2620.34	-10000	1809 1874 1875 1898 1897	4	120.00	.47	5484.24	4371.47	-10000
1667 1726 1727 1750 1749	4	125.00	.47	5822.98	4658.39	-10000	1810 1875 1876 1899 1898	4	120.00	.47	5822.98	4658.39	-10000
1668 1727 1728 1751 1750	4	125.00	.47	5822.98	4658.39	-10000	1811 1876 1877 1900 1899	4	120.00	.47	5822.98	4658.39	-10000
1669 1728 1729 1752 1751	2	120.00	.47	4205.20	3344.16	-10000	1812 1877 1878 1901 1900	4	120.00	.47	5822.98	4658.39	-10000
1670 1729 1730 1753 1752	2	120.00	.47	5163.53	4114.82	-10000	1813 1878 1879 1902 1901	4	120.00	.47	5822.98	4658.39	-10000
1671 1730 1731 1754 1753	2	120.00	.47	5484.24	4371.47	-10000	1814 1879 1880 1903 1902	4	125.00	.33	3275.43	2620.34	-10000
1672 1731 1732 1755 1754	2	120.00	.47	5484.24	4371.47	-10000	1815 1880 1881 1904 1903	4	125.00	.33	3275.43	2620.34	-10000
1673 1732 1733 1756 1755	2	120.00	.47	5749.79	4611.83	-10000	1816 1881 1882 1905 1904	4	125.00	.33	3275.43	2620.34	-10000
1674 1733 1734 1757 1756	2	120.00	.47	5749.79	4611.83	-10000	1817 1882 1883 1906 1905	4	125.00	.33	3275.43	2620.34	-10000
1675 1734 1735 1758 1757	2	120.00	.47	5749.79	4611.83	-10000	1818 1883 1884 1907 1906	4	125.00	.33	3275.43	2620.34	-10000
1676 1735 1736 1759 1758	2	120.00	.47	5749.79	4611.83	-10000	1819 1884 1885 1908 1907	4	125.00	.33	3275.43	2620.34	-10000
1677 1736 1737 1760 1759	2	120.00	.47	5749.79	4611.83	-10000	1820 1885 1886 1909 1908	4	125.00	.33	3275.43	2620.34	-10000
1678 1737 1738 1761 1760	2	120.00	.47	5749.79	4611.83	-10000	1821 1886 1887 1910 1909	4	125.00	.33	3275.43	2620.34	-10000
1679 1738 1739 1762 1761	2	120.00	.47	5749.79	4611.83	-10000	1822 1887 1888 1911 1910	4	125.00	.33	3275.43	2620.34	-10000
1680 1739 1740 1763 1762	2	120.00	.47	5749.79	4611.83	-10000	1823 1888 1889 1912 1911	4	125.00	.33	3275.43	2620.34	-10000
1681 1740 1741 1764 1763	2	120.00	.47	5749.79	4611.83	-10000	1824 1889 1890 1913 1912	4	125.00	.33	3275.43	2620.34	-10000
1682 1741 1742 1765 1764	2	120.00	.47	5749.79	4611.83	-10000	1825 1890 1891 1914 1913	4	125.00	.33	3275.43	2620.34	-10000
1683 1742 1743 1766 1765	2	125.00	.33	3275.43	2620.34	-10000	1826 1891 1892 1915 1914	2	120.00	.47	5484.24	4371.47	-10000
1684 1743 1744 1767 1766	2	125.00	.33	3275.43	2620.34	-10000	1827 1892 1893 1916 1915	2	120.00	.47	5484.24	4371.47	-10000
1685 1744 1745 1768 1767	2	125.00	.33	3275.43	2620.34	-10000	1828 1893 1894 1917 1916	2	120.00	.47	5484.24	4371.47	-10000
1686 1745 1746 1769 1768	2	125.00	.33	3275.43	2620.34	-10000	1829 1894 1895 1918 1917	2	120.00	.47	5484.24	4371.47	-10000
1687 1746 1747 1770 1769	2	125.00	.33	3275.43	2620.34	-10000	1830 1895 1896 1919 1918	2	120.00	.47	5484.24	4371.47	-10000
1688 1747 1748 1771 1770	2	125.00	.33	3275.43	2620.34	-10000	1831 1896 1897 1920 1919	2	120.00	.47	5484.24	4371.47	-10000
1689 1748 1749 1772 1771	2	125.00	.33	3275.43	2620.34	-10000	1832 1897 1898 1921 1920	2	120.00	.47	5484.24	4371.47	-10000
1690 1749 1750 1773 1772	2	125.00	.33	3275.43	2620.34	-10000	1833 1898 1899 1922 1921	2	120.00	.47	5484.24	4371.47	-10000
1691 1750 1751 1774 1773	2	125.00	.33	3275.43	2620.34	-10000	1834 1899 1900 1923 1922	2	120.00	.47	5484.24	4371.47	-10000
1692 1751 1752 1775 1774	2	125.00	.33	3275.43	2620.34	-10000	1835 1900 1901 1924 1923	2	120.00	.47	5484.24	4371.47	-10000
1693 1752 1753 1776 1775	2	125.00	.33	3275.43	2620.34	-10000	1836 1901 1902 1925 1924	2	120.00	.47	5484.24	4371.47	-10000
1694 1753 1754 1777 1776	2	125.00	.33	3275.43	2620.34	-10000	1837 1902 1903 1926 1925	2	120.00	.47	5484.24	4371.47	-10000
1695 1754 1755 1778 1777	2	125.00	.33	3275.43	2620.34	-10000	1838 1903 1904 1927 1926	2	120.00	.47	5484.24	4371.47	-10000
1696 1755 1756 1779 1778	2	125.00	.33	3275.43	2620.34	-10000	1839 1904 1905 1928 1927	2	120.00	.47	5484.24	4371.47	-10000
1697 1756 1757 1780 1779	2	125.00	.33	3275.43	2620.34	-10000	1840 1905 1906 1929 1928	2	120.00	.47	5484.24	4371.47	-10000
1698 1757 1758 1781 1780	2	125.00	.33	3275.43	2620.34	-10000	1841 1906 1907 1930 1929	2	120.00	.47	5484.24	4371.47	-10000
1699 1758 1759 1782 1781	2	125.00	.33	3275.43	2620.34	-10000	1842 1907 1908 1931 1930	2	120.00	.47	5484.24	4371.47	-10000
1700 1759 1760 1783 1782	2	125.00	.33	3275.43	2620.34	-10000	1843 1908 1909 1932 1931	2	120.00	.47	5484.24	4371.47	-10000
1701 1760 1761 1784 1783	2	125.00	.33	3275.43	2620.34	-10000	1844 1909 1910 1933 1932	2	120.00	.47	5484.24	4371.47	-10000
1702 1761 1762 1785 1784	2	125.00	.33	3275.43	2620.34	-10000	1845 1910 1911 1934 1933	2	120.00	.47	5484.24	4371.47	-10000
1703 1762 1763 1786 1785	2	125.00	.33	3275.43	2620.34	-10000	1846 1911 1912 1935 1934	2	120.00	.47	5484.24	4371.47	-10000
1704 1763 1764 1787 1786	2	125.00	.33	3275.43	2620.34	-10000	1847 1912 1913 1936 1935	2	120.00	.47	5484.24	4371.47	-10000
1705 1764 1765 1788 1787	2	125.00	.33	3275.43	2620.34	-10000	1848 1913 1914 1937 1936	2	120.00	.47	5484.24	4371.47	-10000
1706 1765 1766 1789 1788	2	125.00	.33	3275.43	2620.34	-10000	1849 1914 1915 1938 1937	2	120.00	.47	5484.24	4371.47	-10000
1707 1766 1767 1790 1789	2	125.00	.33	3275.43	2620.34	-10000	1850 1915 1916 1939 1938	2	120.00	.47	5484.24	4371.47	-10000
1708 1767 1768 1791 1790	2	125.00	.33	3275.43	2620.34	-10000	1851 1916 1917 1940 1939	2	120.00	.47	5484.24	4371.47	-10000
1709 1768 1769 1792 1791	2	125.00	.33	3275.43	2620.34	-10000	1852 1917 1918 1941 1940	2	120.00	.47	5484.24	4371.47	-10000
1710 1769 1770 1793 1792	2	125.00	.33	3275.43	2620.34	-10000	1853 1918 1919 1942 1941	2	120.00	.47	5484.24	4371.47	-10000
1711 1770 1771 1794 1793	2	125.00	.33	3275.43	2620.34	-10000	1854 1919 1920 1943 1942	2	120.00	.47	5484.24	4371.47	-10000
1712 1771 1772 1795 1794	2	125.00	.33	3275.43	2620.34	-10000	1855 1920 1921 1944 1943	2	120.00	.47	5484.24	4371.47	-10000
1713 1772 1773 1796 1795	2	125.00	.33	3275.43	2620.34	-10000	1856 1921 1922 1945 1944	2	120.00	.47	5484.24	4371.47	-10000
1714 1773 1774 1797 1796	2	125.00	.33	3275.43	2620.34	-10000	1857 1922 1923 1946 1945	2	120.00	.47	5484.24	4371.47	-10000
1715 1774 1775 1798 1797	2	125.00	.33	3275.43	2620.34	-10000	1858 1923 1924 1947 1946	2	120.00	.47	5484.24	4371.47	-10000
1716 1775 1776 1799 1798	2	125.00	.33	3275.43	2620.34	-10000	1859 1924 1925 1948 1947	2	120.00	.47	5484.24	4371.47	-10000
1717 1776 1777 1800 1799	2	125.00	.33	3275.43	2620.34	-10000	1860 1925 1926 1949 1948	2	120.00	.47	5484.24	4371.47	-10000
1718 1777 1778 1801 1800	2	125.00	.33	3275.43	2620.34	-10000	1861 1926 1927 1950 1949	2	120.00	.47	5484.24	4371.47	-10000
1719 1778 1779 1802 1801	2	125.00	.33	3275.43	2620.34	-10000	1862 1927 1928 1951 1950	2	120.00	.47	5484.24	4371.47	-10000
1720 1779 1780 1803 1802	2	125.00	.33	3275.43	2620.34	-10000	1863 1928 1929 1952 1951	2	120.00	.47	5484.24	4371.47	-10000
1721 1780 1781 1804 1803	2	125.00	.33	3275.43	2620.34	-10000	1864 1929 1930 1953 1952	2	120.00	.47	5484.24	4371.47	-10000
1722 1781 1782 1805 1804	2	125.00	.33	3275.43	2620.34	-10000	1865 1930 1931 1954 1953	2	120.00	.47	5484.24	4371.47	-10000
1723 1782 1783 1806 1805	2	125.00	.33	3275.43	2620.34	-10000	1866 1931 1932 1955 1954	2	120.00	.47	5484.24	4371.47	-10000
1724 1783 1784 1807 1806	2	125.00	.33	3275.43	2620.34	-10000	1867 1932 1933 1956 195						

105	-140.000	4.000	348	-218.000	-63.000	391	-278.000	-9.000	534	-251.000	-42.000	677	-225.000	-58.000
106	-140.000	2.000	349	-218.000	-68.000	392	-278.000	-12.000	535	-251.000	-46.000	678	-225.000	-62.000
107	-140.000	8.000	350	-218.000	-73.000	393	-278.000	-17.000	536	-251.000	-51.000	679	-225.000	-67.000
108	-140.000	-2.000	351	-218.000	-78.000	394	-278.000	-22.000	537	-251.000	-56.000	680	-225.000	-72.000
109	-140.000	-4.000	352	-218.000	-83.000	395	-278.000	-27.000	538	-251.000	-61.000	681	-225.000	-77.000
110	-140.000	-6.000	353	-218.000	-88.000	396	-278.000	-32.000	539	-251.000	-66.000	682	-225.000	-82.000
111	-140.000	-9.000	354	-218.000	-93.000	397	-278.000	-37.000	540	-251.000	-71.000	683	-225.000	-87.000
112	-140.000	-12.000	355	-218.000	-98.000	398	-278.000	-42.000	541	-251.000	-76.000	684	-225.000	-92.000
113	-140.000	-15.000	356	-218.000	-103.000	399	-278.000	-47.000	542	-251.000	-81.000	685	-225.000	-97.000
114	-140.000	-18.000	357	-218.000	-108.000	400	-278.000	-52.000	543	-251.000	-86.000	686	-225.000	-102.000
115	-140.000	-21.000	358	-218.000	-113.000	401	-278.000	-57.000	544	-251.000	-91.000	687	-225.000	-107.000
116	-140.000	-24.000	359	-218.000	-118.000	402	-278.000	-62.000	545	-251.000	-96.000	688	-225.000	-112.000
117	-140.000	-27.000	360	-218.000	-123.000	403	-278.000	-67.000	546	-251.000	-101.000	689	-225.000	-117.000
118	-140.000	-30.000	361	-218.000	-128.000	404	-278.000	-72.000	547	-251.000	-106.000	690	-225.000	-122.000
119	-140.000	-33.000	362	-218.000	-133.000	405	-278.000	-77.000	548	-251.000	-111.000	691	-225.000	-127.000
120	-140.000	-36.000	363	-218.000	-138.000	406	-278.000	-82.000	549	-251.000	-116.000	692	-225.000	-132.000
121	-140.000	-39.000	364	-218.000	-143.000	407	-278.000	-87.000	550	-251.000	-121.000	693	-225.000	-137.000
122	-140.000	-42.000	365	-218.000	-148.000	408	-278.000	-92.000	551	-251.000	-126.000	694	-225.000	-142.000
123	-140.000	-45.000	366	-218.000	-153.000	409	-278.000	-97.000	552	-251.000	-131.000	695	-225.000	-147.000
124	-140.000	-48.000	367	-218.000	-158.000	410	-278.000	-102.000	553	-251.000	-136.000	696	-225.000	-152.000
125	-140.000	-51.000	368	-218.000	-163.000	411	-278.000	-107.000	554	-251.000	-141.000	697	-225.000	-157.000
126	-140.000	-54.000	369	-218.000	-168.000	412	-278.000	-112.000	555	-251.000	-146.000	698	-225.000	-162.000
127	-140.000	-57.000	370	-218.000	-173.000	413	-278.000	-117.000	556	-251.000	-151.000	699	-225.000	-167.000
128	-140.000	-60.000	371	-218.000	-178.000	414	-278.000	-122.000	557	-251.000	-156.000	700	-225.000	-172.000
129	-140.000	-63.000	372	-218.000	-183.000	415	-278.000	-127.000	558	-251.000	-161.000	701	-225.000	-177.000
130	-140.000	-66.000	373	-218.000	-188.000	416	-278.000	-132.000	559	-251.000	-166.000	702	-225.000	-182.000
131	-140.000	-69.000	374	-218.000	-193.000	417	-278.000	-137.000	560	-251.000	-171.000	703	-225.000	-187.000
132	-140.000	-72.000	375	-218.000	-198.000	418	-278.000	-142.000	561	-251.000	-176.000	704	-225.000	-192.000
133	-140.000	-75.000	376	-218.000	-203.000	419	-278.000	-147.000	562	-251.000	-181.000	705	-225.000	-197.000
134	-140.000	-78.000	377	-218.000	-208.000	420	-278.000	-152.000	563	-251.000	-186.000	706	-225.000	-202.000
135	-140.000	-81.000	378	-218.000	-213.000	421	-278.000	-157.000	564	-251.000	-191.000	707	-225.000	-207.000
136	-140.000	-84.000	379	-218.000	-218.000	422	-278.000	-162.000	565	-251.000	-196.000	708	-225.000	-212.000
137	-140.000	-87.000	380	-218.000	-223.000	423	-278.000	-167.000	566	-251.000	-201.000	709	-225.000	-217.000
138	-140.000	-90.000	381	-218.000	-228.000	424	-278.000	-172.000	567	-251.000	-206.000	710	-225.000	-222.000
139	-140.000	-93.000	382	-218.000	-233.000	425	-278.000	-177.000	568	-251.000	-211.000	711	-225.000	-227.000
140	-140.000	-96.000	383	-218.000	-238.000	426	-278.000	-182.000	569	-251.000	-216.000	712	-225.000	-232.000
141	-140.000	-99.000	384	-218.000	-243.000	427	-278.000	-187.000	570	-251.000	-221.000	713	-225.000	-237.000
142	-140.000	-102.000	385	-218.000	-248.000	428	-278.000	-192.000	571	-251.000	-226.000	714	-225.000	-242.000
143	-140.000	-105.000	386	-218.000	-253.000	429	-278.000	-197.000	572	-251.000	-231.000	715	-225.000	-247.000
144	-140.000	-108.000	387	-218.000	-258.000	430	-278.000	-202.000	573	-251.000	-236.000	716	-225.000	-252.000
145	-140.000	-111.000	388	-218.000	-263.000	431	-278.000	-207.000	574	-251.000	-241.000	717	-225.000	-257.000
146	-140.000	-114.000	389	-218.000	-268.000	432	-278.000	-212.000	575	-251.000	-246.000	718	-225.000	-262.000
147	-140.000	-117.000	390	-218.000	-273.000	433	-278.000	-217.000	576	-251.000	-251.000	719	-225.000	-267.000
148	-140.000	-120.000	391	-218.000	-278.000	434	-278.000	-222.000	577	-251.000	-256.000	720	-225.000	-272.000
149	-140.000	-123.000	392	-218.000	-283.000	435	-278.000	-227.000	578	-251.000	-261.000	721	-225.000	-277.000
150	-140.000	-126.000	393	-218.000	-288.000	436	-278.000	-232.000	579	-251.000	-266.000	722	-225.000	-282.000
151	-140.000	-129.000	394	-218.000	-293.000	437	-278.000	-237.000	580	-251.000	-271.000	723	-225.000	-287.000
152	-140.000	-132.000	395	-218.000	-298.000	438	-278.000	-242.000	581	-251.000	-276.000	724	-225.000	-292.000
153	-140.000	-135.000	396	-218.000	-303.000	439	-278.000	-247.000	582	-251.000	-281.000	725	-225.000	-297.000
154	-140.000	-138.000	397	-218.000	-308.000	440	-278.000	-252.000	583	-251.000	-286.000	726	-225.000	-302.000
155	-140.000	-141.000	398	-218.000	-313.000	441	-278.000	-257.000	584	-251.000	-291.000	727	-225.000	-307.000
156	-140.000	-144.000	399	-218.000	-318.000	442	-278.000	-262.000	585	-251.000	-296.000	728	-225.000	-312.000
157	-140.000	-147.000	400	-218.000	-323.000	443	-278.000	-267.000	586	-251.000	-301.000	729	-225.000	-317.000
158	-140.000	-150.000	401	-218.000	-328.000	444	-278.000	-272.000	587	-251.000	-306.000	730	-225.000	-322.000
159	-140.000	-153.000	402	-218.000	-333.000	445	-278.000	-277.000	588	-251.000	-311.000	731	-225.000	-327.000
160	-140.000	-156.000	403	-218.000	-338.000	446	-278.000	-282.000	589	-251.000	-316.000	732	-225.000	-332.000
161	-140.000	-159.000	404	-218.000	-343.000	447	-278.000	-287.000	590	-251.000	-321.000	733	-225.000	-337.000
162	-140.000	-162.000	405	-218.000	-348.000	448	-278.000	-292.000	591	-251.000	-326.000	734	-225.000	-342.000
163	-140.000	-165.000	406	-218.000	-353.000	449	-278.000	-297.000	592	-251.000	-331.000	735	-225.000	-347.000
164	-140.000	-168.000	407	-218.000	-358.000	450	-278.000	-302.000	593	-251.000	-336.000	736	-225.000	-352.000
165	-140.000	-171.000	408	-218.000	-363.000	451	-278.000	-307.000	594	-251.000	-341.000	737	-225.000	-357.000
166	-140.000	-174.000	409	-218.000	-368.000	452	-278.000	-312.000	595	-251.000	-346.000	738	-225.000	-362.000
167	-140.000	-177.000	410	-218.000	-373.000	453	-278.000	-317.000	596	-251.000	-351.000	739	-225.000	-367.000
168	-140.000	-180.000	411	-218.000	-378.000	454	-278.000	-322.000	597	-251.000	-356.000	740	-225.000	-372.000
169	-140.000	-183.000	412	-218.000	-383.000	455	-278.000	-327.000	598	-251.000	-361.000	741	-225.000	-377.000
170	-140.000	-186.000	413	-218.000	-388.000	456	-278.000	-332.000	599	-251.000	-366.000	742	-225.000	-382.000
171	-140.000	-189.000	414	-218.000	-393.000	457	-278.000	-337.000	600	-251.000	-371.000	743	-225.000	-387.000
172	-140.000	-192.000	415	-218.000	-398.000	458	-278.000	-342.000	601	-251.000	-376.000	744	-225.000	-392.000
173	-140.000	-195.000	416	-218.000	-403.000	459	-278.000	-347.000	602	-251.000	-381.000	745	-225.000	-397.000
174	-140.000	-198.000	417	-218.000	-408.000	460	-278.000	-352.000	603	-251.000	-386.000	746	-225.000	-402.000
175	-140.000	-201.000	418	-218.000	-413.000	461	-278.000	-357.000	604	-251.000	-391.000	747	-225.000	-407.000
176	-140.000	-204.000	419	-218.000	-418.000	462	-278.000	-362.000	605	-251.000	-396.000	748	-225.000	-412.000
177	-140.000	-207.000	420	-218.000	-423.000	463	-278.000	-367.000	606	-251.000	-401.000	749	-225.000	-417.000
178	-140.000	-210.000	421	-218.000	-428.000	464	-278.000	-372.000	607	-251.000	-406.000	750	-225.000	-422.000
179	-140.000	-213.000	422	-218.000	-433.000	465	-278.000	-377.000	608	-251.000	-411.000	751	-225.000	-427.000
180	-14													

829	-208.000	-73.000	983	-165.000	13.000	1106	-142.000	-38.000	1249	-112.000	6.000	1392	-76.000	-18.000
871	-195.000	23.000	984	-165.000	11.000	1107	-142.000	-43.000	1250	-112.000	-2.000	1393	-76.000	-43.000
872	-195.000	20.000	985	-165.000	9.000	1108	-142.000	-48.000	1251	-112.000	-4.000	1394	-76.000	-48.000
873	-195.000	16.000	986	-165.000	7.000	1109	-142.000	-53.000	1252	-112.000	-6.000	1395	-76.000	-53.000
874	-195.000	13.000	987	-165.000	5.000	1110	-142.000	-58.000	1253	-112.000	-8.000	1396	-76.000	-58.000
875	-195.000	11.000	988	-165.000	3.000	1111	-142.000	-63.000	1254	-112.000	-10.000	1397	-76.000	-63.000
876	-195.000	9.000	989	-165.000	1.000	1112	-142.000	-68.000	1255	-112.000	-12.000	1398	-76.000	-68.000
877	-195.000	6.000	990	-165.000	-1.000	1113	-142.000	-73.000	1256	-112.000	-14.000	1399	-76.000	-73.000
878	-195.000	4.000	991	-165.000	-3.000	1114	-142.000	-78.000	1257	-112.000	-16.000	1400	-76.000	-78.000
879	-195.000	2.000	992	-165.000	-5.000	1115	-142.000	-83.000	1258	-112.000	-18.000	1401	-76.000	-83.000
880	-195.000	0.000	993	-165.000	-7.000	1116	-142.000	-88.000	1259	-112.000	-20.000	1402	-76.000	-88.000
881	-195.000	-2.000	994	-165.000	-9.000	1117	-142.000	-93.000	1260	-112.000	-22.000	1403	-76.000	-93.000
882	-195.000	-4.000	995	-165.000	-11.000	1118	-142.000	-98.000	1261	-112.000	-24.000	1404	-76.000	-98.000
883	-195.000	-6.000	996	-165.000	-13.000	1119	-142.000	-103.000	1262	-112.000	-26.000	1405	-76.000	-103.000
884	-195.000	-8.000	997	-165.000	-15.000	1120	-142.000	-108.000	1263	-112.000	-28.000	1406	-76.000	-108.000
885	-195.000	-10.000	998	-165.000	-17.000	1121	-142.000	-113.000	1264	-112.000	-30.000	1407	-76.000	-113.000
886	-195.000	-12.000	999	-165.000	-19.000	1122	-142.000	-118.000	1265	-112.000	-32.000	1408	-76.000	-118.000
887	-195.000	-14.000	1000	-165.000	-21.000	1123	-142.000	-123.000	1266	-112.000	-34.000	1409	-76.000	-123.000
888	-195.000	-16.000	1001	-165.000	-23.000	1124	-142.000	-128.000	1267	-112.000	-36.000	1410	-76.000	-128.000
889	-195.000	-18.000	1002	-165.000	-25.000	1125	-142.000	-133.000	1268	-112.000	-38.000	1411	-76.000	-133.000
890	-195.000	-20.000	1003	-165.000	-27.000	1126	-142.000	-138.000	1269	-112.000	-40.000	1412	-76.000	-138.000
891	-195.000	-22.000	1004	-165.000	-29.000	1127	-142.000	-143.000	1270	-112.000	-42.000	1413	-76.000	-143.000
892	-195.000	-24.000	1005	-165.000	-31.000	1128	-142.000	-148.000	1271	-112.000	-44.000	1414	-76.000	-148.000
893	-195.000	-26.000	1006	-165.000	-33.000	1129	-142.000	-153.000	1272	-112.000	-46.000	1415	-76.000	-153.000
894	-195.000	-28.000	1007	-165.000	-35.000	1130	-142.000	-158.000	1273	-112.000	-48.000	1416	-76.000	-158.000
895	-195.000	-30.000	1008	-165.000	-37.000	1131	-142.000	-163.000	1274	-112.000	-50.000	1417	-76.000	-163.000
896	-195.000	-32.000	1009	-165.000	-39.000	1132	-142.000	-168.000	1275	-112.000	-52.000	1418	-76.000	-168.000
897	-195.000	-34.000	1010	-165.000	-41.000	1133	-142.000	-173.000	1276	-112.000	-54.000	1419	-76.000	-173.000
898	-195.000	-36.000	1011	-165.000	-43.000	1134	-142.000	-178.000	1277	-112.000	-56.000	1420	-76.000	-178.000
899	-195.000	-38.000	1012	-165.000	-45.000	1135	-142.000	-183.000	1278	-112.000	-58.000	1421	-76.000	-183.000
900	-195.000	-40.000	1013	-165.000	-47.000	1136	-142.000	-188.000	1279	-112.000	-60.000	1422	-76.000	-188.000
901	-195.000	-42.000	1014	-165.000	-49.000	1137	-142.000	-193.000	1280	-112.000	-62.000	1423	-76.000	-193.000
902	-195.000	-44.000	1015	-165.000	-51.000	1138	-142.000	-198.000	1281	-112.000	-64.000	1424	-76.000	-198.000
903	-195.000	-46.000	1016	-165.000	-53.000	1139	-142.000	-203.000	1282	-112.000	-66.000	1425	-76.000	-203.000
904	-195.000	-48.000	1017	-165.000	-55.000	1140	-142.000	-208.000	1283	-112.000	-68.000	1426	-76.000	-208.000
905	-195.000	-50.000	1018	-165.000	-57.000	1141	-142.000	-213.000	1284	-112.000	-70.000	1427	-76.000	-213.000
906	-195.000	-52.000	1019	-165.000	-59.000	1142	-142.000	-218.000	1285	-112.000	-72.000	1428	-76.000	-218.000
907	-195.000	-54.000	1020	-165.000	-61.000	1143	-142.000	-223.000	1286	-112.000	-74.000	1429	-76.000	-223.000
908	-195.000	-56.000	1021	-165.000	-63.000	1144	-142.000	-228.000	1287	-112.000	-76.000	1430	-76.000	-228.000
909	-195.000	-58.000	1022	-165.000	-65.000	1145	-142.000	-233.000	1288	-112.000	-78.000	1431	-76.000	-233.000
910	-195.000	-60.000	1023	-165.000	-67.000	1146	-142.000	-238.000	1289	-112.000	-80.000	1432	-76.000	-238.000
911	-195.000	-62.000	1024	-165.000	-69.000	1147	-142.000	-243.000	1290	-112.000	-82.000	1433	-76.000	-243.000
912	-195.000	-64.000	1025	-165.000	-71.000	1148	-142.000	-248.000	1291	-112.000	-84.000	1434	-76.000	-248.000
913	-195.000	-66.000	1026	-165.000	-73.000	1149	-142.000	-253.000	1292	-112.000	-86.000	1435	-76.000	-253.000
914	-195.000	-68.000	1027	-165.000	-75.000	1150	-142.000	-258.000	1293	-112.000	-88.000	1436	-76.000	-258.000
915	-195.000	-70.000	1028	-165.000	-77.000	1151	-142.000	-263.000	1294	-112.000	-90.000	1437	-76.000	-263.000
916	-195.000	-72.000	1029	-165.000	-79.000	1152	-142.000	-268.000	1295	-112.000	-92.000	1438	-76.000	-268.000
917	-195.000	-74.000	1030	-165.000	-81.000	1153	-142.000	-273.000	1296	-112.000	-94.000	1439	-76.000	-273.000
918	-195.000	-76.000	1031	-165.000	-83.000	1154	-142.000	-278.000	1297	-112.000	-96.000	1440	-76.000	-278.000
919	-195.000	-78.000	1032	-165.000	-85.000	1155	-142.000	-283.000	1298	-112.000	-98.000	1441	-76.000	-283.000
920	-195.000	-80.000	1033	-165.000	-87.000	1156	-142.000	-288.000	1299	-112.000	-100.000	1442	-76.000	-288.000
921	-195.000	-82.000	1034	-165.000	-89.000	1157	-142.000	-293.000	1300	-112.000	-102.000	1443	-76.000	-293.000
922	-195.000	-84.000	1035	-165.000	-91.000	1158	-142.000	-298.000	1301	-112.000	-104.000	1444	-76.000	-298.000
923	-195.000	-86.000	1036	-165.000	-93.000	1159	-142.000	-303.000	1302	-112.000	-106.000	1445	-76.000	-303.000
924	-195.000	-88.000	1037	-165.000	-95.000	1160	-142.000	-308.000	1303	-112.000	-108.000	1446	-76.000	-308.000
925	-195.000	-90.000	1038	-165.000	-97.000	1161	-142.000	-313.000	1304	-112.000	-110.000	1447	-76.000	-313.000
926	-195.000	-92.000	1039	-165.000	-99.000	1162	-142.000	-318.000	1305	-112.000	-112.000	1448	-76.000	-318.000
927	-195.000	-94.000	1040	-165.000	-101.000	1163	-142.000	-323.000	1306	-112.000	-114.000	1449	-76.000	-323.000
928	-195.000	-96.000	1041	-165.000	-103.000	1164	-142.000	-328.000	1307	-112.000	-116.000	1450	-76.000	-328.000
929	-195.000	-98.000	1042	-165.000	-105.000	1165	-142.000	-333.000	1308	-112.000	-118.000	1451	-76.000	-333.000
930	-195.000	-100.000	1043	-165.000	-107.000	1166	-142.000	-338.000	1309	-112.000	-120.000	1452	-76.000	-338.000
931	-195.000	-102.000	1044	-165.000	-109.000	1167	-142.000	-343.000	1310	-112.000	-122.000	1453	-76.000	-343.000
932	-195.000	-104.000	1045	-165.000	-111.000	1168	-142.000	-348.000	1311	-112.000	-124.000	1454	-76.000	-348.000
933	-195.000	-106.000	1046	-165.000	-113.000	1169	-142.000	-353.000	1312	-112.000	-126.000	1455	-76.000	-353.000
934	-195.000	-108.000	1047	-165.000	-115.000	1170	-142.000	-358.000	1313	-112.000	-128.000	1456	-76.000	-358.000
935	-195.000	-110.000	1048	-165.000	-117.000	1171	-142.000	-363.000	1314	-112.000	-130.000	1457	-76.000	-363.000
936	-195.000	-112.000	1049	-165.000	-119.000	1172	-142.000	-368.000	1315	-112.000	-132.000	1458	-76.000	-368.000
937	-195.000	-114.000	1050	-165.000	-121.000	1173	-142.000	-373.000	1316	-112.000	-134.000	1459	-76.000	-373.000
938	-195.000	-116.000	1051	-165.000	-123.000	1174	-142.000	-378.000	1317	-112.000	-136.000	1460	-76.000	-378.000
939	-195.000	-118.000	1052	-165.000	-125.000	1175	-142.000	-383.000	1318	-112.000	-138.000	1461	-76.000	-383.000
940	-195.000	-120.000	1053	-165.000	-127.000	1176	-142.000	-388.000	1319	-112.000	-140.000	1462	-76.000	-388.000
941	-195.000	-122.000	1054	-165.000	-129.000	1177	-142.000	-393.000	1320	-112.000	-142.000	1463	-76.000	-393.000
942	-195.000	-124.000	1055	-165.000	-131.000	1178	-142.000	-398.000	1321	-112.000	-144.000	1464	-76.000	-398.000
943	-195.000	-126.000	1056	-165.000	-133.000	1179	-142.000	-403.000	1322	-112.000	-146.000	1465	-76.000	-403.000
944	-195.000	-128.000	1057	-165.000	-135.000	1180	-142.000	-40						

1533	-46.000	-22.000	1678	-23.900	-2.000	1821	18.000	-17.000
1534	-46.000	-25.000	1679	-23.000	-4.000	1822	18.000	-23.000
1537	-46.000	-29.000	1680	-23.000	-6.000	1823	18.000	-23.000
1538	-46.000	-33.000	1681	-23.000	-9.000	1824	18.000	-29.000
1539	-46.000	-38.000	1682	-23.000	-13.000	1825	18.000	-32.000
1540	-46.000	-43.000	1683	-23.000	-17.000	1826	18.000	-38.000
1541	-46.000	-48.000	1684	-23.000	-21.000	1827	18.000	-43.000
1542	-46.000	-53.000	1685	-23.000	-25.000	1828	18.000	-48.000
1543	-46.000	-58.000	1686	-23.000	-29.000	1829	18.000	-52.000
1544	-46.000	-63.000	1687	-23.000	-33.000	1830	18.000	-58.000
1545	-46.000	-68.000	1688	-23.000	-38.000	1831	18.000	-63.000
1546	-46.000	-73.000	1689	-23.000	-43.000	1832	18.000	-68.000
1547	-42.000	15.000	1690	-23.000	-48.000	1833	18.000	-73.000
1548	-42.000	11.000	1691	-23.000	-53.000	1834	20.000	9.000
1549	-42.000	9.000	1692	-23.000	-58.000	1835	20.000	6.000
1550	-42.000	4.000	1693	-23.000	-63.000	1836	20.000	4.000
1551	-42.000	4.000	1694	-23.000	-68.000	1837	20.000	2.000
1552	-42.000	2.000	1695	-23.000	-73.000	1838	20.000	0.000
1553	-42.000	0.000	1696	-28.000	9.000	1839	20.000	-2.000
1554	-42.000	-2.000	1697	-28.000	4.000	1840	20.000	-4.000
1555	-42.000	-4.000	1698	-28.000	4.000	1841	20.000	-6.000
1556	-42.000	-6.000	1699	-28.000	2.000	1842	20.000	-9.000
1557	-42.000	-9.000	1700	-28.000	0.000	1843	20.000	-12.000
1558	-42.000	-12.000	1701	-28.000	-2.000	1844	20.000	-17.000
1559	-42.000	-17.000	1702	-28.000	-4.000	1845	20.000	-21.000
1560	-42.000	-21.000	1703	-28.000	-6.000	1846	20.000	-25.000
1561	-42.000	-25.000	1704	-28.000	-9.000	1847	20.000	-29.000
1562	-42.000	-29.000	1705	-28.000	-12.000	1848	20.000	-33.000
1563	-42.000	-33.000	1706	-28.000	-17.000	1849	20.000	-38.000
1564	-42.000	-38.000	1707	-28.000	-21.000	1850	20.000	-43.000
1565	-42.000	-43.000	1708	-28.000	-25.000	1851	20.000	-48.000
1566	-42.000	-48.000	1709	-28.000	-29.000	1852	20.000	-53.000
1567	-42.000	-53.000	1710	-28.000	-33.000	1853	20.000	-58.000
1568	-42.000	-58.000	1711	-28.000	-38.000	1854	20.000	-63.000
1569	-42.000	-63.000	1712	-28.000	-43.000	1855	20.000	-68.000
1570	-42.000	-68.000	1713	-28.000	-48.000	1856	20.000	-73.000
1571	-42.000	-73.000	1714	-28.000	-53.000	1857	30.000	9.000
1572	-38.000	13.000	1715	-28.000	-58.000	1858	30.000	6.000
1573	-38.000	11.000	1716	-28.000	-63.000	1859	30.000	4.000
1574	-38.000	9.000	1717	-28.000	-68.000	1860	30.000	2.000
1575	-38.000	6.000	1718	-28.000	-73.000	1861	30.000	0.000
1576	-38.000	4.000	1719	-15.000	9.000	1862	30.000	-2.000
1577	-38.000	2.000	1720	-15.000	4.000	1863	30.000	-4.000
1578	-38.000	0.000	1721	-15.000	4.000	1864	30.000	-6.000
1579	-38.000	-2.000	1722	-15.000	2.000	1865	30.000	-9.000
1580	-38.000	-4.000	1723	-15.000	0.000	1866	30.000	-12.000
1581	-38.000	-6.000	1724	-15.000	-2.000	1867	30.000	-17.000
1582	-38.000	-9.000	1725	-15.000	-4.000	1868	30.000	-21.000
1583	-38.000	-12.000	1726	-15.000	-6.000	1869	30.000	-25.000
1584	-38.000	-17.000	1727	-15.000	-9.000	1870	30.000	-29.000
1585	-38.000	-21.000	1728	-15.000	-12.000	1871	30.000	-33.000
1586	-38.000	-25.000	1729	-15.000	-17.000	1872	30.000	-38.000
1587	-38.000	-29.000	1730	-15.000	-21.000	1873	30.000	-43.000
1588	-38.000	-33.000	1731	-15.000	-25.000	1874	30.000	-48.000
1589	-38.000	-38.000	1732	-15.000	-29.000	1875	30.000	-53.000
1590	-38.000	-43.000	1733	-15.000	-33.000	1876	30.000	-58.000
1591	-38.000	-48.000	1734	-15.000	-38.000	1877	30.000	-63.000
1592	-38.000	-53.000	1735	-15.000	-43.000	1878	30.000	-68.000
1593	-38.000	-58.000	1736	-15.000	-48.000	1879	30.000	-73.000
1594	-38.000	-63.000	1737	-15.000	-53.000	1880	40.000	9.000
1595	-38.000	-68.000	1738	-15.000	-58.000	1881	40.000	6.000
1596	-38.000	-73.000	1739	-15.000	-63.000	1882	40.000	4.000
1597	-34.000	13.000	1740	-15.000	-68.000	1883	40.000	2.000
1598	-34.000	11.000	1741	-15.000	-73.000	1884	40.000	0.000
1599	-34.000	9.000	1742	-10.000	9.000	1885	40.000	-2.000
1600	-34.000	6.000	1743	-10.000	4.000	1886	40.000	-4.000
1601	-34.000	4.000	1744	-10.000	4.000	1887	40.000	-6.000
1602	-34.000	2.000	1745	-10.000	2.000	1888	40.000	-9.000
1603	-34.000	0.000	1746	-10.000	0.000	1889	40.000	-12.000
1604	-34.000	-2.000	1747	-10.000	-2.000	1890	40.000	-17.000
1605	-34.000	-4.000	1748	-10.000	-4.000	1891	40.000	-21.000
1606	-34.000	-6.000	1749	-10.000	-6.000	1892	40.000	-25.000
1607	-34.000	-9.000	1750	-10.000	-9.000	1893	40.000	-29.000
1608	-34.000	-12.000	1751	-10.000	-12.000	1894	40.000	-33.000
1609	-34.000	-17.000	1752	-10.000	-17.000	1895	40.000	-38.000
1610	-34.000	-21.000	1753	-10.000	-21.000	1896	40.000	-43.000
1611	-34.000	-25.000	1754	-10.000	-25.000	1897	40.000	-48.000
1612	-34.000	-29.000	1755	-10.000	-29.000	1898	40.000	-53.000
1613	-34.000	-33.000	1756	-10.000	-33.000	1899	40.000	-58.000
1614	-34.000	-38.000	1757	-10.000	-38.000	1900	40.000	-63.000
1615	-34.000	-43.000	1758	-10.000	-43.000	1901	40.000	-68.000
1616	-34.000	-48.000	1759	-10.000	-48.000	1902	40.000	-73.000
1617	-34.000	-53.000	1760	-10.000	-53.000	1903	50.000	9.000
1618	-34.000	-58.000	1761	-10.000	-58.000	1904	50.000	6.000
1619	-34.000	-63.000	1762	-10.000	-63.000	1905	50.000	4.000
1620	-34.000	-68.000	1763	-10.000	-68.000	1906	50.000	2.000
1621	-34.000	-73.000	1764	-10.000	-73.000	1907	50.000	0.000
1622	-30.000	13.000	1765	-5.000	9.000	1908	50.000	-2.000
1623	-30.000	11.000	1766	-5.000	4.000	1909	50.000	-4.000
1624	-30.000	9.000	1767	-5.000	4.000	1910	50.000	-6.000
1625	-30.000	8.000	1768	-5.000	2.000	1911	50.000	-9.000
1626	-30.000	4.000	1769	-5.000	0.000	1912	50.000	-12.000
1627	-30.000	2.000	1770	-5.000	-2.000	1913	50.000	-17.000
1628	-30.000	0.000	1771	-5.000	-4.000	1914	50.000	-21.000
1629	-30.000	-2.000	1772	-5.000	-6.000	1915	50.000	-25.000
1630	-30.000	-4.000	1773	-5.000	-9.000	1916	50.000	-29.000
1631	-30.000	-6.000	1774	-5.000	-12.000	1917	50.000	-33.000
1632	-30.000	-9.000	1775	-5.000	-17.000	1918	50.000	-38.000
1633	-30.000	-12.000	1776	-5.000	-21.000	1919	50.000	-43.000
1634	-30.000	-17.000	1777	-5.000	-25.000	1920	50.000	-48.000
1635	-30.000	-21.000	1778	-5.000	-29.000	1921	50.000	-53.000
1636	-30.000	-25.000	1779	-5.000	-33.000	1922	50.000	-58.000
1637	-30.000	-29.000	1780	-5.000	-38.000	1923	50.000	-63.000
1638	-30.000	-33.000	1781	-5.000	-43.000	1924	50.000	-68.000
1639	-30.000	-38.000	1782	-5.000	-48.000	1925	50.000	-73.000
1640	-30.000	-43.000	1783	-5.000	-53.000			
1641	-30.000	-48.000	1784	-5.000	-58.000			
1642	-30.000	-53.000	1785	-5.000	-63.000			
1643	-30.000	-58.000	1786	-5.000	-68.000			
1644	-30.000	-63.000	1787	-5.000	-73.000			
1645	-30.000	-68.000	1788	0.000	9.000			
1646	-30.000	-73.000	1789	0.000	4.000			
1647	-26.000	13.000	1790	0.000	4.000			
1648	-26.000	11.000	1791	0.000	2.000			
1649	-26.000	9.000	1792	0.000	0.000			
1650	-26.000	4.000	1793	0.000	-2.000			
1651	-26.000	4.000	1794	0.000	-4.000			
1652	-26.000	2.000	1795	0.000	-6.000			
1653	-26.000	0.000	1796	0.000	-9.000			
1654	-26.000	-2.000	1797	0.000	-12.000			
1655	-26.000	-4.000	1798	0.000	-17.000			
1656	-26.000	-6.000	1799	0.000	-21.000			
1657	-26.000	-9.000	1800	0.000	-25.000			
1658	-26.000	-12.000	1801	0.000	-29.000			
1659	-26.000	-17.000	1802	0.000	-33.000			
1660	-26.000	-21.000	1803	0.000	-38.000			
1661	-26.000	-25.000	1804	0.000	-43.000			
1662	-26.000	-29.000	1805	0.000	-48.000			
1663	-26.000	-33.000	1806	0.000	-53.000			
1664	-26.000	-38.000	1807	0.000	-58.000			
1665	-26.000	-43.000	1808	0.000	-63.000			
1666	-26.000	-48.000	1809	0.000	-68.000			
1667	-26.000	-53.000	1810					

excerpt from TRICI.025

XMAX= 2.2359 SECTION C-C, 08/2002
ACCELERATION VALUES AT OUTCROPPING LAYER 25 - Transporter Route, HBPP, ISFSI, 08/

0.009200	0.018224	0.014031	0.015745	0.016902	0.017462	0.017403	0.016728	1
0.015458	0.013642	0.011339	0.008634	0.005620	0.002407	0.000894	0.004162	2
-0.007285	-0.010148	-0.012652	-0.014705	-0.016235	-0.017188	-0.017527	-0.017241	3
-0.016340	-0.014855	-0.012837	-0.010359	-0.007508	-0.004386	-0.001102	0.002225	4
0.005480	0.008544	0.011309	0.013677	0.015562	0.016898	0.017635	0.017750	5
0.017234	0.016109	0.014409	0.012201	0.009557	0.006576	0.003359	0.000024	6
-0.003312	-0.004528	-0.009512	-0.012354	-0.014362	-0.016054	-0.017171	-0.017670	7
-0.017533	-0.016764	-0.015386	-0.013449	-0.011019	-0.008181	-0.005034	-0.001488	8
0.001741	0.005132	0.008367	0.011334	0.013928	0.016061	0.017658	0.018668	9
0.019055	0.018812	0.017947	0.016501	0.014523	0.012094	0.009301	0.006254	10
0.003062	-0.001449	-0.003243	-0.006157	-0.008723	-0.010860	-0.012484	-0.013526	11
-0.013941	-0.013704	-0.012813	-0.011290	-0.009178	-0.006542	-0.003465	-0.000046	12
0.003604	0.007364	0.011110	0.014721	0.018074	0.021062	0.023584	0.025561	13
0.026927	0.027644	0.027648	0.027068	0.025807	0.023960	0.021589	0.018790	14
0.015657	0.012312	0.008869	0.005457	0.002192	0.000805	0.003431	0.005591	15
-0.007212	-0.008237	-0.008635	-0.008391	-0.007520	-0.006056	-0.004056	-0.001595	16
0.001233	0.004324	0.007560	0.010822	0.013986	0.016937	0.019558	0.021757	17
0.023442	0.024554	0.025041	0.024888	0.024087	0.022669	0.020672	0.018171	18
0.015243	0.011997	0.008538	0.004993	0.001479	-0.001873	-0.004953	-0.007644	19
-0.009859	-0.011514	-0.012553	-0.012937	-0.012655	-0.011713	-0.010148	-0.008012	20
-0.005383	-0.002352	0.000971	0.004469	0.008017	0.011491	0.014763	0.017720	21
0.020252	0.022273	0.023705	0.024501	0.024627	0.024083	0.022880	0.021068	22
0.018702	0.015872	0.012671	0.009220	0.005633	0.002043	0.001430	0.004655	23
-0.007526	-0.009935	-0.011803	-0.013059	-0.013663	-0.013592	-0.012853	-0.011471	24
-0.009498	-0.007005	-0.004085	-0.000841	0.002605	0.006133	0.009608	0.012909	25
0.015909	0.018503	0.020590	0.022098	0.022961	0.023152	0.022652	0.021483	26
0.019674	0.017294	0.014414	0.011143	0.007583	0.003867	0.000114	0.003537	27
-0.006956	-0.010049	-0.012684	-0.014775	-0.016255	-0.017071	-0.017200	-0.016637	28
0.015408	0.013556	0.011154	0.008287	0.005064	0.001600	0.001975	0.005535	29
0.008943	0.012080	0.014826	0.017082	0.017461	0.015883	0.020161	0.019426	30
-0.018796	-0.017115	-0.014828	-0.012022	-0.008788	-0.005235	-0.001488	-0.002118	31
-0.006061	-0.009402	-0.012828	-0.015620	-0.017890	-0.019556	-0.020567	-0.020888	32
-0.020516	-0.019467	-0.017785	-0.015534	-0.012802	-0.009688	-0.006313	-0.002798	33
0.000723	0.004122	0.007270	0.010054	0.012367	0.014128	0.015266	0.015744	34
0.015537	0.014658	0.013131	0.011020	0.008391	0.005349	0.001995	0.001539	35
-0.005133	-0.008649	-0.011966	-0.014954	-0.017517	-0.019549	-0.020986	-0.021770	36
-0.021880	-0.021309	-0.020085	-0.018253	-0.015888	-0.013078	-0.009935	-0.006579	37
-0.003144	0.000239	0.003432	0.006312	0.008755	0.010668	0.011960	0.012579	38
0.012480	0.011664	0.010139	0.007960	0.005186	0.001920	-0.001737	-0.005645	39
-0.009676	-0.013674	-0.017502	-0.021008	-0.024067	-0.026554	-0.028376	-0.029450	40
-0.029732	-0.029193	-0.027846	-0.025722	-0.022890	-0.019438	-0.015484	-0.011161	41
-0.006422	-0.002024	0.002463	0.006678	0.010462	0.013672	0.016178	0.017880	42
0.018695	0.018581	0.017514	0.015518	0.012634	0.008950	0.004566	0.000374	43
-0.005725	-0.011304	-0.016939	-0.022434	-0.027614	-0.032293	-0.036318	-0.039539	44
-0.041845	-0.043144	-0.043383	-0.042537	-0.040625	-0.037492	-0.033824	-0.029134	45
-0.023764	-0.017879	-0.011662	-0.005306	0.000988	0.007025	0.012613	0.017580	46
0.021767	0.025050	0.027324	0.028529	0.028628	0.027634	0.025580	0.022552	47
0.018649	0.014620	0.008814	0.003221	0.002578	0.008375	0.013985	0.019211	48
-0.023886	-0.027849	-0.030978	-0.033167	-0.034355	-0.034506	-0.033427	-0.031756	49
-0.028867	-0.025365	-0.021083	-0.016764	-0.011118	-0.005791	-0.000488	0.004606	50
0.009109	0.011458	0.016904	0.019530	0.021237	0.021974	0.021704	0.020444	51
0.018226	0.015133	0.011258	0.006739	0.001714	0.003642	0.009165	0.014669	52
-0.019990	-0.024955	-0.029422	-0.033253	-0.036351	-0.038633	-0.040057	-0.040604	53
-0.040293	-0.039168	-0.037309	-0.034814	-0.031807	-0.028425	-0.024819	-0.021142	54
-0.017549	-0.014183	-0.011182	-0.008658	-0.006709	-0.005397	-0.004768	-0.004826	55
-0.005554	-0.006898	-0.008786	-0.011110	-0.013755	-0.016576	-0.019432	-0.022166	56
-0.024639	-0.026701	-0.028232	-0.029123	-0.029295	-0.028694	-0.027300	-0.025124	57
-0.022113	-0.018644	-0.014526	-0.009996	-0.005214	-0.000355	0.004389	0.008828	58
0.012767	0.016028	0.018440	0.019867	0.020187	0.019329	0.017240	0.013929	59
0.009424	0.003819	0.002777	-0.010193	-0.018249	-0.026714	-0.035360	-0.043921	60
-0.052150	-0.059780	-0.066575	-0.072302	-0.076769	-0.079806	-0.081291	-0.081143	61
-0.079330	-0.075868	-0.070823	-0.064311	-0.056489	-0.047562	-0.037758	-0.027347	62
-0.016403	-0.005826	0.004694	0.014666	0.023823	0.031914	0.038730	0.044093	63
0.047875	0.049994	0.050419	0.049174	0.046327	0.042003	0.036161	0.029611	64
0.021978	0.013729	0.005129	0.003534	0.011992	0.019973	0.027239	0.033568	65
-0.023886	-0.027456	-0.030978	-0.033167	-0.034355	-0.034506	-0.033427	-0.031756	66
-0.033135	-0.027449	-0.021210	-0.014651	-0.008007	-0.003512	0.004612	0.010164	67
0.014969	0.018885	0.021807	0.023673	0.024459	0.024190	0.023294	0.020767	68
0.017850	0.014341	0.010419	0.006288	0.002146	0.001800	0.005365	0.008174	69
-0.010684	-0.012180	-0.012790	-0.012477	-0.011251	-0.009164	-0.006311	-0.002826	70
0.001122	0.005337	0.009597	0.013671	0.017319	0.020312	0.022426	0.023470	71
0.023274	0.021720	0.018718	0.014248	0.008323	0.001032	-0.007505	-0.017093	72
-0.027513	-0.030482	-0.049706	-0.060844	-0.071564	-0.081510	-0.090351	-0.097763	73
-0.103463	-0.107201	-0.108780	-0.108064	-0.104975	-0.099512	-0.091733	-0.081781	74
-0.069849	-0.056215	-0.041191	-0.025163	-0.008527	0.008204	0.024772	0.040530	75
0.055109	0.068081	0.079078	0.087764	0.093874	0.097205	0.097630	0.095106	76
0.089660	0.081417	0.070558	0.057361	0.042146	0.025313	0.007281	-0.011467	77
-0.030461	-0.049192	-0.067189	-0.083975	-0.099133	-0.112268	-0.123062	-0.131247	78
-0.136639	-0.139122	-0.138661	-0.135304	-0.129168	-0.120452	-0.109404	-0.096351	79
-0.081641	-0.065685	-0.048889	-0.031699	-0.014532	0.002179	0.018057	0.032730	80
0.048896	0.057280	0.066689	0.073966	0.079038	0.081876	0.082527	0.081081	81
0.077687	0.072534	0.065846	0.057879	0.048897	0.039187	0.029018	0.018667	82
0.008378	-0.001615	-0.011121	-0.019968	-0.028037	-0.035228	-0.041498	-0.046821	83
-0.051219	-0.054729	-0.057423	-0.059381	-0.060700	-0.061478	-0.061814	-0.061799	84
-0.061311	-0.061013	-0.060346	-0.059531	-0.058463	-0.057421	-0.056054	-0.054404	85
-0.052389	-0.049927	-0.046923	-0.041298	-0.038964	-0.038770	-0.029599	-0.021230	86
-0.013680	-0.005372	0.003629	0.013188	0.023170	0.033373	0.043598	0.053594	87
0.063116	0.071890	0.079655	0.086143	0.091114	0.094342	0.095640	0.094859	88
0.091896	0.086704	0.079285	0.069713	0.058102	0.044649	0.029578	0.013191	89
-0.004193	-0.022192	-0.040428	-0.058475	-0.075934	-0.092382	-0.107441	-0.120740	90
-0.131963	-0.140832	-0.147131	-0.150705	-0.151462	-0.149391	-0.144536	-0.137027	91
-0.127039	-0.114835	-0.100695	-0.084985	-0.068061	-0.050347	-0.032236	-0.014165	92
0.003484	0.020306	0.035973	0.050156	0.062614	0.073124	0.081557	0.087812	93
0.091842	0.093793	0.093649	0.091589	0.087814	0.082546	0.076049	0.068598	94
0.060485	0.051993	0.043404	0.034976	0.026946	0.019512	0.012842	0.007055	95
0.002212	-0.001592	-0.004423	-0.006310	-0.007332	-0.007605	-0.007259	-0.006451	96
-0.005336	-0.004079	-0.002831	-0.001736	-0.000911	-0.000453	-0.000424	-0.000861	97
-0.001757	-0.003081	-0.004762	-0.006706	-0.008788	-0.010872	-0.012797	-0.014411	98
-0.015544	-0.016063	-0.015818	-0.014712	-0.012653	-0.009606	-0.005551	-0.000531	99
0.005393	0.012095	0.019435	0.027216	0.035235	0.043244	0.051901	0.058239	100
0.064712	0.070169	0.074392	0.077183	0.078389	0.077894	0.075634	0.071596	101
0.065823	0.058413	0.049514	0.039330	0.028104	0.016123	0.003698	-0.008832	102
-0.021124	-0.012827	-0.043606	-0.053145	-0.061155	-0.067393	-0.071656	-0.073806	103
-0.073748	-0.071468	-0.066994	-0.060440	-0.051948	-0.041753	-0.030096	-0.017297	104
-0.003669	0.010417	0.024619	0.038559	0.051907	0.064323	0.075532	0.085265	105

excerpt from TR1C.Q40

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*****
** QUAD4MU A COMPUTER PROGRAM FOR EVALUATING THE
** SEISMIC RESPONSE OF SOIL STRUCTURES
** U.C.Davis, 1993
** by Martin Byrd Hudson,
** I.M.Idriss,
** and Mohsen Beikae
** MODIFIED FROM QUAD4, 1973
** by I.M.Idriss,
** J. Lysmer,
** R. Whang and
** H. Bolton Seed
*****

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TR1C: HUMBOLDT BAY, TRANSPORTER ROUTE, PG&E, 09/2002
HORIZONTAL ACCELERATION INPUT FILE:
TR1C1.Q25
WITH FIRST LINE: XMAX= 2.2359 SECTION C-C, 08/2002

```

NO. OF ELEMENTS = 1835
NO. OF NODAL POINTS = 1925
DEGREES OF FREEDOM = 3850
HALF-BANDWIDTH = 60
CONTROLLING ELEMENT = 497
NO. OF FIXED BOUNDARY CONDS. = 126
NO. OF ITERATIONS = 20
TOTAL EQ. POINTS READ (KGMAX) = 12000
LAST EQ. PTS. USED (INREQ TO KREQ) = 1 12000
INT. EQ. PTS. USED (INREQ TO MREQ) = 3 12000
TIME INTERVAL OF RECORDS = 0.0050 SECONDS
STRAIN CONVERSION FACTOR = 0.6500
DAMPING RATIO REDUCTION FACTOR = 1.000
PREDOMINANT INPUT MOTION PERIOD = 0.2500 SECONDS
EQ. MULT. FACTOR (HORE. COMP.) = 1.0000
MAXIMUM ACCEL. USED (HORE. COMP.) = 2.2359

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0 STRESS HISTORIES REQUESTED,
7 ACCEL HISTORIES REQUESTED,
1 SEIS COEFF HISTORIES REQUESTED
OUTPUT FILES ARE AS FOLLOWS:

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NODE 51, X DIR IN FILE: TR1C00.Q4A
NODE 76, X DIR IN FILE: TR1C01.Q4A
NODE 101, X DIR IN FILE: TR1C02.Q4A
NODE 765, X DIR IN FILE: TR1C03.Q4A
NODE 821, X DIR IN FILE: TR1C04.Q4A
NODE 961, X DIR IN FILE: TR1C05.Q4A
NODE 1114, X DIR IN FILE: TR1C06.Q4A
SURFACE 1, X DIR IN FILE: TR1C00.QSC

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SOIL DATA TAKEN FROM FILE: hbsoilrw.dat

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*****
MATERIAL TYPE NO. 1
*****
MODULUS: #1 modulus for Clay PI 15 (Vucetic and Dobry 1991)
DAMPING: damping for Clay PI 15 (Vucetic & Dobry 1991)

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STRAIN	G/G _{max}	STRAIN	DAMPING
0.0001	1.000	0.0001	1.70
0.0003	1.000	0.0003	1.70
0.0010	1.000	0.0010	1.70
0.0032	0.940	0.0032	2.60
0.0100	0.820	0.0100	4.50
0.0316	0.640	0.0316	7.80
0.1000	0.400	0.1000	11.70
0.3160	0.210	0.3160	16.30
1.0000	0.090	1.0000	20.20
3.1600	0.040	3.1600	23.00
10.0000	0.020	10.0000	23.00

[lines skipped]

ITERATION NO. 20

DAMPING SET AT THE FOLLOWING TWO FREQUENCIES:
THE FIRST NATURAL FREQUENCY: CIRC FREQ= 7.546; PERIOD= 0.833 SEC
5 TIMES THE NATURAL FREQ.: CIRC FREQ= 37.729; PERIOD= 0.167 SEC

TIME REQUIRED FOR FORMATION AND TRIANGULIZATION OF MATRICES = 1. SEC

MODULI (ENG: KSF or SI: KN/M ²) AND DAMPING						
ELM	G-USED	G-NEW	DIP-G	DAMP-USED	DAMP-NEW	DIP-DAMP
1	3104.2	3108.2	-0.1	0.02484	0.02466	0.7
2	2573.0	2580.8	-0.3	0.05132	0.05088	0.9
3	2027.5	2038.2	-0.5	0.08141	0.08088	0.7

4	1551.3	1543.5	-0.8	0.10504	0.10443	0.6
5	1254.7	1247.8	-0.7	0.12081	0.12013	0.6
6	1064.3	1075.0	-1.0	0.13517	0.13439	0.6
7	859.8	876.1	-1.9	0.15029	0.14909	0.8
8	673.1	679.1	-0.9	0.16446	0.16387	0.4
9	2221.4	2233.8	-0.6	0.12148	0.12097	0.4
10	1990.0	2000.7	-0.5	0.13110	0.13066	0.3
11	1715.3	1727.5	-0.7	0.14252	0.14202	0.4
12	109.8	109.8	0.0	0.27358	0.27359	0.0
13	383.2	385.3	-0.5	0.24979	0.24960	0.1
14	379.8	378.3	0.4	0.25194	0.25207	-0.1
15	219.2	211.0	3.9	0.26569	0.26641	-0.3
16	125.6	124.4	0.9	0.27718	0.27739	-0.1
17	5146.9	5146.5	0.0	0.12239	0.12240	0.0
18	4811.1	4814.6	-0.1	0.12836	0.12830	0.0
19	2613.1	2637.4	-0.9	0.15910	0.15843	0.4
20	2491.6	2502.1	-0.4	0.16514	0.16486	0.2

[lines skipped]

PEAK NODAL ACCELERATION VALUES (g's)

NODE	XORD	YORD	X-ACC	AT TIME	Y-ACC	AT TIME
1	-400.0	12.0	1.9293	23.2350	0.0000	0.0000
2	-400.0	11.0	1.9280	23.2350	0.0000	0.0000
3	-400.0	9.0	1.9257	23.2400	0.0000	0.0000
4	-400.0	6.0	1.9201	23.2400	0.0000	0.0000
5	-400.0	4.0	1.9097	23.2350	0.0000	0.0000
6	-400.0	2.0	1.8969	23.2350	0.0000	0.0000
7	-400.0	0.0	1.8772	23.2350	0.0000	0.0000
8	-400.0	-2.0	1.8471	23.2400	0.0000	0.0000
9	-400.0	-4.0	1.8071	23.2350	0.0000	0.0000
10	-400.0	-6.0	1.7967	24.4950	0.0000	0.0000
11	-400.0	-9.0	1.7806	24.4950	0.0000	0.0000
12	-400.0	-12.0	1.7588	24.4950	0.0000	0.0000
13	-400.0	-17.0	1.8121	23.3450	0.0000	0.0000
14	-400.0	-21.0	1.9076	23.7150	0.0000	0.0000
15	-400.0	-25.0	2.0006	23.7100	0.0000	0.0000
16	-400.0	-29.0	2.0129	23.7000	0.0000	0.0000
17	-400.0	-33.0	2.2053	24.7250	0.0000	0.0000
18	-400.0	-38.0	2.2055	24.7250	0.0000	0.0000
19	-400.0	-43.0	2.1928	24.7200	0.0000	0.0000
20	-400.0	-48.0	2.1506	24.7200	0.0000	0.0000

[lines skipped]

PEAK ELEMENTS STRESSES (ENG: PSF or SI: N/M^2) AND STRAINS

ELM	SIG-X	SIG-Y	SIG-XY	EPS-MAX	AT TIME
1	237.7	4.2	124.1	0.004	23.240
2	187.1	7.3	485.4	0.019	23.240
3	142.9	12.8	1073.0	0.053	23.245
4	146.4	19.3	1646.1	0.106	23.250
5	123.4	22.0	2094.2	0.166	23.250
6	107.8	24.5	2529.4	0.238	23.250
7	87.9	28.4	2951.5	0.343	23.250
8	69.6	31.8	3357.1	0.499	23.255
9	296.5	30.0	3773.9	0.170	23.250
10	284.5	32.3	4308.1	0.217	23.255
11	259.4	36.3	4933.7	0.288	23.255
12	32.8	59.6	5674.2	5.166	24.545
13	86.4	66.3	6232.4	1.627	24.545
14	87.9	72.3	6931.0	1.825	23.370
15	29.9	77.2	7798.9	3.558	23.365
16	56.5	78.1	8487.2	6.759	23.360
17	116.3	72.0	9063.0	0.176	23.340
18	106.3	66.6	9818.2	0.204	23.330
19	55.4	64.5	10597.7	0.406	23.325
20	49.1	62.4	11347.6	0.455	23.320

[lines skipped]

1 MAX & MIN SEISMIC COEFFICIENTS

SURFACE	WEIGHT (LB or N)	X-DIRECTION NEGATIVE	POSITIVE
1	259061.7500	-1.8592	1.7915

ITERATION CYCLE NO. 20 AVE OVERALL DAMP = 0.177

TIME REQUIRED FOR 12000 STEPS = 211. SEC

** END OF JOB **

excerpt from TR1C00.QSC

TR1C: HUMBOLDT BAY, TRANSPORTER ROUTE, PG&E, 09/2002
Seismic Coefficient Surface History
Time Step = 0.005 Sec
Surface 1

0.000000	0.000002	0.000005	0.000011	0.000021	0.000034	0.000051	0.000072
0.000097	0.000125	0.000157	0.000191	0.000227	0.000264	0.000302	0.000340
0.000380	0.000421	0.000464	0.000516	0.000573	0.000640	0.000720	0.000816
0.000932	0.001070	0.001233	0.001423	0.001642	0.001888	0.002161	0.002457
0.002774	0.003106	0.003446	0.003786	0.004118	0.004432	0.004719	0.004969
0.005174	0.005324	0.005412	0.005433	0.005383	0.005259	0.005051	0.004793
0.004458	0.004064	0.003618	0.003132	0.002618	0.002088	0.001557	0.001037
0.000544	0.000091	-0.000312	-0.000653	-0.000924	-0.001119	-0.001233	-0.001265
-0.001217	-0.001093	-0.000898	-0.000643	-0.000337	0.000008	0.000377	0.000756
0.001131	0.001487	0.001810	0.002088	0.002311	0.002468	0.002553	0.002563
0.002495	0.002352	0.002136	0.001855	0.001517	0.001133	0.000716	0.000278
-0.000164	-0.000598	-0.001009	-0.001382	-0.001706	-0.001970	-0.002166	-0.002287
-0.002329	-0.002291	-0.002174	-0.001983	-0.001724	-0.001405	-0.001038	-0.000634
-0.000206	0.000233	0.000668	0.001088	0.001479	0.001830	0.002134	0.002382
0.002570	0.002697	0.002763	0.002771	0.002727	0.002639	0.002516	0.002370
0.002214	0.002062	0.001927	0.001822	0.001763	0.001755	0.001814	0.001846
0.002157	0.002448	0.002821	0.003273	0.003799	0.004391	0.005040	0.005733
0.004457	0.007197	0.007938	0.008664	0.009361	0.010014	0.010610	0.011139
0.011591	0.011959	0.012241	0.012435	0.012542	0.012566	0.012514	0.012397
0.012223	0.012006	0.011759	0.011496	0.011231	0.010979	0.010750	0.010556
0.010407	0.010310	0.010270	0.010289	0.010368	0.010502	0.010687	0.010916
0.011178	0.011462	0.011755	0.012045	0.012318	0.012561	0.012762	0.012909
0.012992	0.013006	0.012944	0.012803	0.012583	0.012288	0.011922	0.011492
0.011009	0.010484	0.009930	0.009361	0.008792	0.008239	0.007714	0.007231
0.006800	0.006431	0.006133	0.005909	0.005761	0.005690	0.005693	0.005762
0.005891	0.006068	0.006282	0.006518	0.006764	0.007002	0.007221	0.007404
0.007540	0.007618	0.007631	0.007569	0.007431	0.007214	0.006921	0.006556
0.006125	0.005639	0.005108	0.004545	0.003966	0.003384	0.002815	0.002272
0.003771	0.003323	0.002938	0.002626	0.002390	0.002236	0.002164	0.002169
0.002048	0.002092	0.002092	0.002083	0.002108	0.002196	0.002344	0.002539
0.002104	0.002407	0.002587	0.002660	0.002660	0.002601	0.002464	0.002251
0.001964	0.001611	0.001200	0.000742	0.000251	-0.000261	-0.000778	-0.001285
-0.001767	-0.002211	-0.002604	-0.002935	-0.003194	-0.003376	-0.003477	-0.003497
-0.003437	-0.003302	-0.003100	-0.002840	-0.002536	-0.002199	-0.001845	-0.001489
-0.001146	-0.000832	-0.000560	-0.000342	-0.000189	-0.000110	-0.000190	-0.000190
-0.000353	-0.000593	-0.000907	-0.001286	-0.001718	-0.002192	-0.002693	-0.003207
-0.003719	-0.004214	-0.004677	-0.005096	-0.005454	-0.005747	-0.005967	-0.006108
-0.006169	-0.006151	-0.006057	-0.005894	-0.005671	-0.005399	-0.005089	-0.004757
-0.004416	-0.004081	-0.003766	-0.003484	-0.003248	-0.003069	-0.002953	-0.002907
-0.002933	-0.003032	-0.003202	-0.003437	-0.003730	-0.004071	-0.004449	-0.004851
-0.005265	-0.005675	-0.006070	-0.006435	-0.006759	-0.007034	-0.007250	-0.007402
-0.007489	-0.007509	-0.007466	-0.007364	-0.007212	-0.007019	-0.006797	-0.006559
-0.006319	-0.006090	-0.005887	-0.005723	-0.005609	-0.005555	-0.005569	-0.005656
-0.005818	-0.006054	-0.006360	-0.006721	-0.007125	-0.007624	-0.008121	-0.008632
-0.009140	-0.009629	-0.010082	-0.010484	-0.010820	-0.011078	-0.011250	-0.011328
-0.011307	-0.011190	-0.010978	-0.010679	-0.010304	-0.009866	-0.009381	-0.008867
-0.008346	-0.007816	-0.007359	-0.006936	-0.006545	-0.006225	-0.006169	-0.006128
-0.006211	-0.006421	-0.006758	-0.007217	-0.007788	-0.008458	-0.009211	-0.010025
-0.010879	-0.011747	-0.012603	-0.013420	-0.014173	-0.014837	-0.015388	-0.015807
-0.016078	-0.016188	-0.016128	-0.015895	-0.015491	-0.014924	-0.014203	-0.013346
-0.012371	-0.011302	-0.010164	-0.008986	-0.007796	-0.006623	-0.005495	-0.004439
-0.003479	-0.002636	-0.001927	-0.001365	-0.000959	-0.000712	-0.000623	-0.000687
-0.000891	-0.001222	-0.001662	-0.002188	-0.002777	-0.003405	-0.004046	-0.004675
-0.005267	-0.005802	-0.006259	-0.006623	-0.006881	-0.007026	-0.007054	-0.006965
-0.006765	-0.006664	-0.006674	-0.006613	-0.006510	-0.006460	-0.006411	-0.006379
-0.002986	-0.002556	-0.002210	-0.001964	-0.001835	-0.001834	-0.001969	-0.002245
-0.002660	-0.003212	-0.003891	-0.004687	-0.005584	-0.006567	-0.007615	-0.008709
-0.009828	-0.010951	-0.012057	-0.013130	-0.014131	-0.015107	-0.015987	-0.016781
-0.017483	-0.018609	-0.019605	-0.020301	-0.020733	-0.020969	-0.020937	-0.020798
-0.020074	-0.020135	-0.020170	-0.020189	-0.020198	-0.020204	-0.020211	-0.020218
-0.020226	-0.020232	-0.020230	-0.020214	-0.020177	-0.020110	-0.020007	-0.019857
-0.019654	-0.019393	-0.019071	-0.018687	-0.018245	-0.017748	-0.017205	-0.016629
-0.016035	-0.015441	-0.014867	-0.014335	-0.013869	-0.013492	-0.013230	-0.013104
-0.013134	-0.013338	-0.013729	-0.014316	-0.015104	-0.016090	-0.017267	-0.018624
-0.020141	-0.021792	-0.023547	-0.025370	-0.027222	-0.029061	-0.030845	-0.032529
-0.034067	-0.035416	-0.036536	-0.037393	-0.037954	-0.038194	-0.038095	-0.037648
-0.036849	-0.035704	-0.034228	-0.032443	-0.030377	-0.028064	-0.025547	-0.022874
-0.020093	-0.017255	-0.014414	-0.011623	-0.008934	-0.006394	-0.004044	-0.001922
-0.000059	0.001520	0.002800	0.003774	0.004441	0.004810	0.004895	0.004719
0.004310	0.003702	0.002933	0.002042	0.001071	0.000066	-0.000935	-0.001893
-0.002771	-0.003536	-0.004161	-0.004623	-0.004908	-0.005006	-0.004912	-0.004630
-0.004165	-0.003532	-0.002747	-0.001831	-0.000808	0.000298	0.001461	0.002656
0.003858	0.005044	0.006193	0.007288	0.008313	0.009258	0.010115	0.010880
0.011550	0.012129	0.012619	0.013025	0.013352	0.013607	0.013796	0.013920
0.013983	0.013985	0.013922	0.013788	0.013574	0.013268	0.012857	0.012324
0.011651	0.010817	0.009808	0.008605	0.007192	0.005557	0.003692	0.001594
+0.000733	-0.000381	-0.000605	-0.000870	-0.012058	-0.015244	-0.018544	-0.021847
-0.025122	-0.028313	-0.031359	-0.034201	-0.036780	-0.039041	-0.040934	-0.042432
-0.043437	-0.043980	-0.044020	-0.043550	-0.042575	-0.041110	-0.039184	-0.036828
-0.034120	-0.031091	-0.027825	-0.024401	-0.020899	-0.017408	-0.014021	-0.010825
-0.007905	-0.005342	-0.003208	-0.001567	-0.000474	0.000032	-0.000075	-0.000089
-0.002164	-0.004119	-0.006641	-0.009684	-0.013184	-0.017069	-0.021257	-0.025657
-0.030170	-0.034694	-0.039127	-0.043369	-0.047327	-0.050908	-0.054029	-0.056620
-0.058619	-0.059979	-0.060665	-0.060660	-0.059962	-0.058581	-0.056542	-0.053886
-0.050667	-0.046947	-0.042798	-0.038301	-0.033545	-0.028621	-0.023616	-0.018619
-0.013722	-0.009007	-0.004551	-0.000426	0.000304	0.006589	0.009387	0.011666
0.013407	0.014599	0.015246	0.015357	0.014951	0.014058	0.012713	0.010958
0.008841	0.006414	0.003731	0.000848	-0.002181	-0.005299	-0.008450	-0.011378
-0.014634	-0.017570	-0.020337	-0.022892	-0.025199	-0.027221	-0.028927	-0.030289
-0.031285	-0.031896	-0.032107	-0.031907	-0.031288	-0.030250	-0.028797	-0.026934
-0.024674	-0.020038	-0.015042	-0.009731	-0.004225	-0.000264	-0.004201	-0.000020
0.004337	0.008693	0.013024	0.017262	0.021338	0.025180	0.028719	0.031880
0.034627	0.036868	0.038559	0.039653	0.040110	0.039899	0.039005	0.037420
0.035150	0.032212	0.028637	0.024468	0.019764	0.014591	0.009026	0.003155
-0.002927	-0.009119	-0.015320	-0.021424	-0.027330	-0.032927	-0.038120	-0.042820
-0.046948	-0.050434	-0.053215	-0.055243	-0.056489	-0.056936	-0.056581	-0.055437
-0.053534	-0.050912	-0.047624	-0.043741	-0.039334	-0.034488	-0.029290	-0.023835
-0.018217	-0.012533	-0.006876	-0.001337	0.004004	0.009070	0.013794	0.018120
0.021999	0.025395	0.028283	0.030651	0.032496	0.033824	0.034653	0.035008
0.034921	0.034429	0.033573	0.032402	0.030963	0.029305	0.027477	0.025526
0.023497	0.021432	0.019368	0.017342	0.015386	0.013524	0.011780	0.010174
0.008722	0.007437	0.006330	0.005406	0.004674	0.004137	0.003800	0.003667
0.003738	0.004017	0.004504	0.005197	0.006098	0.007203	0.008508	0.010007
0.011691	0.013548	0.015563	0.017716	0.019985	0.022343	0.024761	0.027202

excerpt from TR3C.Q4I

```

TR3C: HUMBOLDT BAY, TRANSPORTER ROUTE, PG4E, 09/2002
UNITS (E for English, S for SI):
E
   DRF      FRM      ROCKVF      ROCKVVS      ROCKRHO      *** (A1)      ***
   1      0.65      7560.      1800.      130.
NELM NDEPT NSLP
1835 1925 1
*** (325) ***
KGMX KGEQ N1EQ N2EQ N3EQ NUMB KV KSAV
1200012000 1 112000 30 1 0
*** (815) ***
DTEQ EQMUL1 EQMUL2 UGMAX1 UGMAX2 HDRX HDRY NPLX NPLY FRINPVT *** (5F10.0,4I5,F10.0) ***
0.005 1.0 1.0 2 0 8 0 0.20
EARTHQUAKE INPUT FILE NAME(S) & FORMAT(S) (* for FREE FORMAT) *** (A) ***
TR3CI.025
(SF9.6)
SOFT ACUT KOUT
0 1 1
*** (325) ***
ACCELERATION OUTPUT FORMAT (M or C), FILE PREFIX, AND SUFFIX: *** (A) ***
MULTIPLE
TR3C
C43
SEISMIC COEFF OUT(UT FORMAT (M OR C), FILE PREFIX, AND SUFFIX: *** (A)
MULTIPLE
TR3C
QSC
NSEQ ESEQ *** (2I5)
44 187
NOSEQ
709 710 711 739 740 768 769 797 798 826 827 828 856 857 885
886 914 915 943 944 971 972 998 999 1026 1049 1074 1099 1100 1125
1149 1172 1194 1215 1235 1254 1272 1289 1288 1304 1320 1336 1352 1351
ELSEQ
685 686 712 713 714 739 740 741 742 766 767 768 769 770 793
794 795 796 797 798 799 820 821 822 823 824 825 826 827 847
848 849 850 851 852 853 854 855 874 875 876 877 878 879 880
881 882 883 901 902 903 904 905 906 907 908 909 910 911 928
929 930 931 932 933 934 935 936 937 938 939 944 945 956 957 958
959 960 961 962 963 964 979 980 981 982 983 984 985 986 987
988 1003 1004 1005 1006 1007 1008 1009 1010 1011 1012 1027 1028 1029 1030
1031 1032 1033 1034 1035 1036 1051 1052 1053 1054 1055 1056 1057 1058 1059
1060 1061 1075 1076 1077 1078 1079 1080 1081 1082 1083 1084 1085 1099 1100
1101 1102 1103 1104 1105 1106 1107 1108 1122 1123 1124 1125 1126 1127 1128
1129 1130 1144 1145 1146 1147 1148 1149 1150 1151 1165 1166 1167 1168 1169
1170 1171 1185 1186 1187 1188 1189 1190 1204 1205 1206 1207 1208 1222 1223
1224 1225 1239 1240 1255 1270 1285
M MP1 MP2 MP3 MP4 TYPE DENS PO GRX G XL LSTR *** (6I5,5F10.0,I5) ***
1 1 2 27 26 1 125.00 .33 3275.43 2620.34 .10000
2 2 3 28 27 1 125.00 .33 3275.43 2620.34 .10000
3 3 4 29 28 1 125.00 .33 3275.43 2620.34 .10000
4 4 5 30 29 1 125.00 .47 3275.43 2620.34 .10000
5 5 6 31 30 1 125.00 .47 3275.43 2620.34 .10000
6 6 7 32 31 1 125.00 .47 3275.43 2620.34 .10000
7 7 8 33 32 1 125.00 .47 3275.43 2620.34 .10000
8 8 9 34 33 1 125.00 .47 3275.43 2620.34 .10000
9 9 10 35 34 1 125.00 .47 5822.98 4658.39 .10000
10 10 11 36 35 1 125.00 .47 5822.98 4658.39 .10000

```

[same as TR1C.Q4I]

excerpt from TR3CI.O25

MAX= 2.5250 SECTION C-C, 08/2002
ACCELERATION VALUES AT OUTCROPPING LAYER 25 - Transporter Route. HBPP, ISFSI, 08/

0.001009-0.003525-0.005914-0.008091-0.009980-0.011512-0.012633-0.013303	1
0.013498-0.013210-0.012448-0.011238-0.009622-0.007658-0.005412-0.002965	2
0.000401-0.002188-0.004711-0.007080-0.009211-0.011027-0.012465-0.013473	3
-0.014016-0.014073-0.013642-0.012737-0.011390-0.009649-0.007573-0.005237	4
-0.002723-0.000120-0.002480-0.004985-0.007306-0.009359-0.011071-0.012381	5
0.013241-0.013620-0.013503-0.012892-0.011808-0.010288-0.008385-0.006165	6
0.003706-0.001092-0.001582-0.004224-0.006739-0.009040-0.011045-0.012682	7
-0.013894-0.014637-0.014885-0.014630-0.013880-0.012662-0.011019-0.009012	8
-0.006711-0.004201-0.001572-0.001080-0.003658-0.006068-0.008219-0.010032	9
0.011437-0.012379-0.012819-0.012737-0.012128-0.011010-0.009414-0.007395	10
0.005018-0.002359-0.000488-0.003426-0.006353-0.009169-0.011773-0.014075	11
-0.015990-0.017449-0.018399-0.018799-0.018633-0.017900-0.016619-0.014830	12
-0.012587-0.009963-0.007043-0.003921-0.000701-0.002513-0.005614-0.008499	13
0.011072-0.013250-0.014960-0.016148-0.016773-0.016820-0.016286-0.015185	14
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0.006273-0.008879-0.011163-0.013043-0.014454-0.015347-0.015690-0.015472	18
0.014699-0.013400-0.011620-0.009424-0.006886-0.004098-0.001157-0.001833	19
-0.004767-0.007542-0.010060-0.012233-0.013985-0.015254-0.015996-0.016185	20
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0.020406-0.020376-0.019724-0.018474-0.016667-0.014372-0.011672-0.008666	105
0.005467-0.002195-0.001027-0.004079-0.006843-0.009214-0.011101-0.012429	106
-0.013146-0.013222-0.012649-0.011449-0.009661-0.007354-0.004612-0.001541	107

excerpt from TR3C.Q40

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.....
** QUAD4MU A COMPUTER PROGRAM FOR EVALUATING THE **
** SEISMIC RESPONSE OF SOIL STRUCTURES **
** U.C.Davis, 1993 **
** by Martin Byrd Hudson, **
** I.M.Idris, **
** and Mohsen Beikae **
** MODIFIED FROM QUAD4, 1973 **
** by I.M.Idris, **
** J. Lysmer, **
** R. Hwang and **
** H. Bolton Seed **
.....

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TR3C: HUMBOLDT BAY, TRANSPORTER ROUTE, PG4E, 09/2002
HORIZONTAL ACCELERATION INPUT FILE:
TR3CI.025
WITH FIRST LINE: XMAX= 2.5250 SECTION C-C, 08/2002

```

NO. OF ELEMENTS = 1835
NO. OF NODAL POINTS = 1925
DEGREES OF FREEDOM = 3850
HALF-BANDWIDTH = 40
CONTROLLING ELEMENT = 497
NO. OF FIXED BNDRY CONDS. = 126
NO. OF ITERATIONS = 30
TOTAL EQ. POINTS READ (KGMAX) = 12000
LAST EQ. PTS. USED (NREQ TO NREQ) = 1 12000
INT. EQ. PTS USED (NREQ TO NREQ) = 1 12000
TIME INTERVAL OF RECORDS = 0.0050 SECONDS
STRAIN CONVERSION FACTOR = 0.6500
DAMPING RATIO REDUCTION FACTOR = 1.000
PREDOMINANT INPUT MOTION PERIOD = 0.2000 SECONDS
EQ. MULT. FACTOR (HORZ. COMP.) = 1.0000
MAXIMUM ACCEL. USED (HORZ. COMP.) = 2.5250

```

0 STRESS HISTORIES REQUESTED,
7 ACCEL HISTORIES REQUESTED,
1 SEIS COEFF HISTORIES REQUESTED
OUTPUT FILES ARE AS FOLLOWS:

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NODE 51, X DIR IN FILE: TR3C00.Q4A
NODE 76, X DIR IN FILE: TR3C01.Q4A
NODE 101, X DIR IN FILE: TR3C02.Q4A
NODE 765, X DIR IN FILE: TR3C03.Q4A
NODE 821, X DIR IN FILE: TR3C04.Q4A
NODE 961, X DIR IN FILE: TR3C05.Q4A
NODE 1114, X DIR IN FILE: TR3C06.Q4A
SURFACE 1, X DIR IN FILE: TR3C00.QSC

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SOIL DATA TAKEN FROM FILE: hbsoilw.dat

MATERIAL TYPE NO. 1

MODULUS: 81 modulus for Clay PI 15 (Vucetic and Dobry 1991)
DAMPING: damping for Clay PI 15 (Vucetic & Dobry 1991)

STRAIN	G/Gmax	STRAIN	DAMPING
0.0001	1.000	0.0001	1.70
0.0003	1.000	0.0003	1.70
0.0010	1.000	0.0010	1.70
0.0032	0.940	0.0032	2.60
0.0100	0.820	0.0100	4.50
0.0316	0.640	0.0316	7.80
0.1000	0.400	0.1000	11.70
0.3160	0.210	0.3160	16.30
1.0000	0.090	1.0000	20.20
3.1600	0.040	3.1600	23.00
10.0000	0.020	10.0000	23.00

[lines skipped]

ITERATION NO. 30

DAMPING SET AT THE FOLLOWING TWO FREQUENCIES:
THE FIRST NATURAL FREQUENCY: CIRC FREQ= 7.712; PERIOD= 0.815 SEC
5 TIMES THE NATURAL FREQ.: CIRC FREQ= 38.558; PERIOD= 0.163 SEC

TIME REQUIRED FOR FORMATION AND TRIANGULIZATION OF MATRICES = 1. SEC

ELM	MODULI (ENG: KSF or SI: KN/M ²) AND DAMPING		DIF-G	DAMP-USED	DAMP-NEW	DIF-DAMP
	G-USED	G-NEW				
1	2924.6	2925.6	0.0	0.03346	0.03341	0.1
2	2482.3	2481.1	0.0	0.05639	0.05646	-0.1
3	1901.6	1900.1	0.1	0.08766	0.08773	-0.1

4	1405.0	1403.4	0.1	0.11230	0.11237	-0.1
5	1145.1	1144.4	0.1	0.12920	0.12925	0.0
6	932.2	931.6	0.1	0.14494	0.14498	0.0
7	684.1	683.8	0.0	0.16337	0.16340	0.0
8	589.0	588.8	0.0	0.17281	0.17282	0.0
9	2017.7	2016.9	0.0	0.12995	0.12998	0.0
10	1775.2	1774.5	0.0	0.14003	0.14006	0.0
11	1470.7	1472.5	-0.1	0.15269	0.15262	0.0
12	95.6	95.6	-0.1	0.27706	0.27704	0.0
13	368.9	368.9	0.0	0.25109	0.25109	0.0
14	405.2	406.4	-0.3	0.24974	0.24983	0.0
15	345.8	351.0	-1.5	0.25464	0.25418	0.2
16	136.8	136.0	0.6	0.27511	0.27526	-0.1
17	5285.4	5294.0	-0.2	0.11993	0.11978	0.1
18	4798.5	4804.3	-0.1	0.12858	0.12848	0.1
19	2348.7	2350.1	-0.1	0.16701	0.16695	0.0
20	2280.7	2281.0	0.0	0.17421	0.17419	0.0

[lines skipped]

PEAK NODAL ACCELERATION VALUES (g's)

NODE	XORD	YORD	X-ACC	AT TIME	Y-ACC	AT TIME
1	-400.0	12.0	2.0990	35.0200	0.0000	0.0000
2	-400.0	11.0	2.0985	35.0200	0.0000	0.0000
3	-400.0	9.0	2.0985	35.0200	0.0000	0.0000
4	-400.0	6.0	2.0904	35.0200	0.0000	0.0000
5	-400.0	4.0	2.0795	35.0200	0.0000	0.0000
6	-400.0	2.0	2.0536	35.0200	0.0000	0.0000
7	-400.0	0.0	2.0399	35.0200	0.0000	0.0000
8	-400.0	-2.0	1.9993	35.0150	0.0000	0.0000
9	-400.0	-4.0	1.9464	35.0150	0.0000	0.0000
10	-400.0	-6.0	1.9283	35.0150	0.0000	0.0000
11	-400.0	-9.0	1.8928	35.0150	0.0000	0.0000
12	-400.0	-12.0	1.8465	35.0150	0.0000	0.0000
13	-400.0	-17.0	2.3973	23.1700	0.0000	0.0000
14	-400.0	-21.0	2.5280	34.5400	0.0000	0.0000
15	-400.0	-25.0	2.6427	34.5350	0.0000	0.0000
16	-400.0	-29.0	2.6383	34.5300	0.0000	0.0000
17	-400.0	-33.0	2.7057	34.5000	0.0000	0.0000
18	-400.0	-38.0	2.6964	34.5000	0.0000	0.0000
19	-400.0	-43.0	2.6586	34.5000	0.0000	0.0000
20	-400.0	-48.0	2.5312	34.5000	0.0000	0.0000

[lines skipped]

PEAK ELEMENTS STRESSES (ENG: PSF or SI: N/M^2) AND STRAINS

ELM	SIG-X	SIG-Y	SIG-XY	EPS-MAX	AT TIME
1	358.8	5.0	150.1	0.008	23.030
2	294.8	8.1	563.2	0.023	35.050
3	222.2	14.3	1231.3	0.065	35.050
4	205.9	21.0	1884.9	0.134	35.050
5	168.3	25.6	2393.3	0.209	35.050
6	139.0	31.0	2887.8	0.310	35.050
7	105.9	37.6	3365.0	0.492	35.050
8	94.9	43.9	3827.1	0.650	35.050
9	390.5	45.2	4294.9	0.213	35.050
10	356.8	48.6	4862.4	0.274	35.050
11	307.3	54.9	5515.0	0.375	35.050
12	52.3	73.2	6303.7	6.597	35.055
13	50.2	78.7	6433.6	1.744	35.050
14	61.4	82.7	6602.7	1.629	23.020
15	66.8	87.1	6962.5	2.014	23.190
16	73.6	88.5	7951.3	5.812	23.185
17	149.3	85.7	8716.1	0.165	23.165
18	130.0	81.7	9837.3	0.205	23.145
19	54.1	81.4	11120.8	0.473	23.140
20	56.2	81.2	12387.3	0.543	23.135

[lines skipped]

1 MAX & MIN SEISMIC COEFFICIENTS

SURFACE	WEIGHT (LB or N)	X-DIRECTION	
		NEGATIVE	POSITIVE
1	259061.7500	-1.7868	2.0514

ITERATION CYCLE NO. 30 AVE OVERALL DAMP = 0.185

TIME REQUIRED FOR 12000 STEPS = 211. SEC

** END OF JOB **

excerpt from TR3C00.QSC

TR3C: HUMBOLDT BAY, TRANSPORTER ROUTE, PG&E, 09/2002
Seismic Coefficient Surface History
Time Step = 0.005 Sec
Surface 1

0.000000	0.000000	0.000001	0.000002	0.000005	0.000009	0.000016	0.000024
0.000035	0.000049	0.000065	0.000083	0.000103	0.000124	0.000147	0.000171
0.000196	0.000221	0.000248	0.000277	0.000308	0.000343	0.000385	0.000434
0.000494	0.000565	0.000652	0.000755	0.000876	0.001018	0.001181	0.001365
0.001570	0.001794	0.002035	0.002290	0.002554	0.002823	0.003092	0.003352
0.003598	0.003823	0.004020	0.004182	0.004304	0.004379	0.004403	0.004374
0.004290	0.004349	0.004385	0.004398	0.004385	0.004350	0.004271	0.004216
0.004904	0.004855	0.004769	0.004666	0.004528	0.004364	0.004174	0.003967
-0.000849	-0.001005	-0.001103	-0.001144	-0.001128	-0.001060	-0.000944	-0.000787
-0.000598	-0.000384	-0.000157	0.000073	0.000297	0.000504	0.000685	0.000831
0.000936	0.000992	0.000997	0.000947	0.000842	0.000684	0.000476	0.000223
-0.000069	-0.000392	-0.000736	-0.001093	-0.001452	-0.001803	-0.002136	-0.002443
-0.002715	-0.002945	-0.003129	-0.003262	-0.003343	-0.003373	-0.003352	-0.003286
-0.003179	-0.003039	-0.002875	-0.002694	-0.002508	-0.002326	-0.002158	-0.002014
-0.001902	-0.001830	-0.001804	-0.001828	-0.001904	-0.002032	-0.002212	-0.002439
-0.002707	-0.003010	-0.003339	-0.003683	-0.004031	-0.004372	-0.004694	-0.004986
-0.005236	-0.005436	-0.005577	-0.005651	-0.005655	-0.005585	-0.005441	-0.005224
-0.004939	-0.004591	-0.004189	-0.003742	-0.003260	-0.002757	-0.002244	-0.001735
-0.001242	-0.000777	-0.000352	0.000025	0.000344	0.000600	0.000789	0.000909
0.000961	0.000947	0.000872	0.000743	0.000568	0.000358	0.000123	0.000124
-0.000372	-0.000610	-0.000825	-0.001008	-0.001149	-0.001242	-0.001280	-0.001261
-0.001182	-0.001045	-0.000853	-0.000611	-0.000326	-0.000005	0.000340	0.000699
0.001062	0.001415	0.001749	0.002052	0.002315	0.002530	0.002690	0.002790
0.002827	0.002801	0.002713	0.002568	0.002370	0.002126	0.001846	0.001540
0.001218	0.000891	0.000572	0.000269	-0.000065	-0.000243	-0.000437	-0.000581
-0.000670	-0.000704	-0.000682	-0.000607	-0.000482	-0.000318	-0.000113	0.000111
0.000357	0.000604	0.000844	0.001066	0.001258	0.001413	0.001520	0.001573
0.001568	0.001500	0.001369	0.001176	0.000924	0.000619	0.000268	-0.000121
-0.000537	-0.000969	-0.001407	-0.001837	-0.002249	-0.002631	-0.002975	-0.003270
-0.003511	-0.003693	-0.003812	-0.003868	-0.003862	-0.003799	-0.003683	-0.003522
-0.003325	-0.003101	-0.002863	-0.002621	-0.002387	-0.002172	-0.001986	-0.001839
-0.001737	-0.001687	-0.001694	-0.001758	-0.001879	-0.002055	-0.002282	-0.002551
-0.002856	-0.003186	-0.003530	-0.003876	-0.004213	-0.004528	-0.004811	-0.005050
-0.005237	-0.005364	-0.005425	-0.005417	-0.005338	-0.005189	-0.004974	-0.004697
-0.004367	-0.003991	-0.003581	-0.003148	-0.002704	-0.002261	-0.001832	-0.001428
-0.001059	-0.000735	-0.000463	-0.000248	-0.000094	-0.000002	0.000030	0.000005
-0.000071	-0.000190	-0.000344	-0.000521	-0.000711	-0.000900	-0.001078	-0.001232
-0.001350	-0.001424	-0.001445	-0.001405	-0.001302	-0.001132	-0.000896	-0.000697
-0.000238	0.000172	0.000626	0.001112	0.001619	0.002135	0.002646	0.003140
0.003604	0.004026	0.004396	0.004706	0.004948	0.005118	0.005215	0.005237
0.005188	0.005073	0.004898	0.004672	0.004407	0.004113	0.003804	0.003491
0.003187	0.002905	0.002656	0.002449	0.002291	0.002190	0.002148	0.002168
0.002246	0.002381	0.002565	0.002791	0.003049	0.003328	0.003615	0.003897
0.004151	0.004394	0.004584	0.004719	0.004790	0.004789	0.004711	0.004553
0.004315	0.003998	0.003606	0.003148	0.002667	0.002167	0.001647	0.001085
0.000216	-0.000408	-0.001012	-0.001584	-0.002111	-0.002585	-0.002996	-0.003339
-0.003611	-0.003812	-0.003942	-0.004006	-0.004011	-0.003965	-0.003879	-0.003764
-0.003634	-0.003501	-0.003378	-0.003278	-0.003213	-0.003193	-0.003226	-0.003319
-0.003475	-0.003697	-0.003983	-0.004329	-0.004729	-0.005174	-0.005654	-0.006155
-0.006666	-0.007171	-0.007655	-0.008104	-0.008503	-0.008840	-0.009104	-0.009286
-0.009378	-0.009376	-0.009279	-0.009087	-0.008806	-0.008441	-0.008001	-0.007498
-0.006944	-0.006354	-0.005743	-0.005126	-0.004520	-0.003939	-0.003396	-0.002903
-0.002472	-0.002108	-0.001818	-0.001604	-0.001466	-0.001400	-0.001400	-0.001459
-0.001567	-0.001710	-0.001877	-0.002051	-0.002220	-0.002368	-0.002482	-0.002549
-0.002558	-0.002501	-0.002371	-0.002164	-0.001878	-0.001515	-0.001080	-0.000578
-0.000020	0.000585	0.001221	0.001877	0.002537	0.003185	0.003807	0.004389
0.004918	0.005382	0.005773	0.006083	0.006308	0.006446	0.006498	0.006468
0.006343	0.006189	0.005959	0.005683	0.005374	0.005047	0.004715	0.004392
0.004089	0.003820	0.003592	0.003415	0.003293	0.003229	0.003224	0.003275
0.003378	0.003526	0.003709	0.003917	0.004137	0.004358	0.004565	0.004745
0.004886	0.004976	0.005006	0.004968	0.004855	0.004665	0.004396	0.004052
0.003636	0.003156	0.002622	0.002044	0.001437	0.000815	0.000192	-0.000415
-0.000992	-0.001825	-0.002989	-0.004405	-0.006231	-0.008297	-0.003125	-0.001187
-0.003159	-0.003045	-0.002854	-0.002593	-0.002274	-0.001911	-0.001517	-0.001109
-0.000700	-0.000308	0.000055	0.000374	0.000638	0.000838	0.000966	0.001017
0.000990	0.000885	0.000705	0.000457	0.000149	-0.000210	-0.000607	-0.001030
-0.001464	-0.001896	-0.002312	-0.002700	-0.003047	-0.003344	-0.003582	-0.003755
-0.003861	-0.003898	-0.003867	-0.003773	-0.003621	-0.003421	-0.003181	-0.002914
-0.002630	-0.002343	-0.002065	-0.001808	-0.001583	-0.001399	-0.001263	-0.001183
-0.001160	-0.001195	-0.001288	-0.001434	-0.001626	-0.001856	-0.002114	-0.002388
-0.002665	-0.002932	-0.003175	-0.003381	-0.003537	-0.003632	-0.003658	-0.003606
-0.003471	-0.003251	-0.002946	-0.002558	-0.002092	-0.001556	-0.000960	-0.000315
0.000367	0.001071	0.001782	0.002486	0.003169	0.003818	0.004419	0.004964
0.005443	0.005851	0.006182	0.006437	0.006617	0.006724	0.006765	0.006748
0.006682	0.006578	0.006447	0.006302	0.006154	0.006016	0.005897	0.005807
0.005734	0.005744	0.005779	0.005863	0.005993	0.006167	0.006381	0.006626
0.006896	0.007179	0.007467	0.007748	0.008011	0.008245	0.008442	0.008593
0.008691	0.008732	0.008712	0.008631	0.008489	0.008292	0.008043	0.007751
0.007423	0.007070	0.006702	0.006330	0.005965	0.005616	0.005293	0.005003
0.004752	0.004543	0.004378	0.004256	0.004174	0.004126	0.004104	0.004098
0.004094	0.004086	0.004054	0.003986	0.003868	0.003686	0.003430	0.003089
0.002653	0.002119	0.001481	0.000741	-0.000098	-0.001031	-0.002050	-0.003141
-0.004291	-0.005484	-0.006703	-0.007927	-0.009138	-0.010317	-0.011444	-0.012501
-0.013472	-0.014343	-0.015103	-0.015741	-0.016253	-0.016634	-0.016886	-0.017011
-0.017015	-0.016905	-0.016692	-0.016386	-0.016001	-0.015550	-0.015044	-0.014497
-0.013920	-0.013323	-0.012713	-0.012095	-0.011473	-0.010847	-0.010214	-0.009571
-0.008911	-0.008224	-0.007501	-0.006730	-0.005901	-0.005001	-0.004021	-0.002952
-0.001786	-0.000519	0.000851	0.002322	0.003889	0.005542	0.007271	0.009059
0.010886	0.012730	0.014568	0.016372	0.018114	0.019773	0.021316	0.022719
0.023959	0.025016	0.025871	0.026513	0.026932	0.027127	0.027097	0.026849
0.026394	0.025749	0.024935	0.023975	0.022896	0.021728	0.020501	0.019246
0.017993	0.016772	0.015608	0.014525	0.013541	0.012674	0.011931	0.011338
0.010834	0.010475	0.010229	0.010081	0.010013	0.010001	0.010020	0.010043
0.010044	0.009993	0.009887	0.009640	0.009323	0.008908	0.008172	0.007379
0.006425	0.005314	0.004056	0.002662	0.001153	-0.000449	-0.002118	-0.003823
-0.005534	-0.007219	-0.008845	-0.010382	-0.011801	-0.013075	-0.014182	-0.015106
-0.015832	-0.016355	-0.016671	-0.016785	-0.016705	-0.016446	-0.016027	-0.015469
-0.014797	-0.014039	-0.013225	-0.012381	-0.011536	-0.010716	-0.009944	-0.009239
-0.008617	-0.008087	-0.007656	-0.007324	-0.007085	-0.006930	-0.006866	-0.006805
-0.006794	-0.006784	-0.006750	-0.006662	-0.006495	-0.006221	-0.005817	-0.005264
-0.004543	-0.003644	-0.002560	-0.001290	0.000162	0.001786	0.003564	0.005477
0.007497	0.009598	0.011746	0.013907	0.016045	0.018123	0.020105	0.021970
0.021677	0.022502	0.023252	0.023929	0.024502	0.024939	0.025240	0.025408
0.026654	0.029391	0.028937	0.028314	0.027543	0.026648	0.025655	0.024587

Attachment F

SPECTRAD

Input and Output Excerpts

(see Table 8-6 for listing of files)

SPECTRA1.INP

TR1C01.Q4A
0
TR1C01.Q4A
TR1C01A.050
(8F10.6)
4 12000 1.0 0.005 1 0.05
TR3C01.Q4A
0
TR3C01.Q4A
TR3C01A.050
(8F10.6)
4 12000 1.0 0.005 1 0.05

SPECTRA2.INP

S1CC.AC8
0
S1CC.AC8
S1CC.050
(8E15.7)
2 15999 1.0 0.005 1 0.05
S3CC.AC8
0
S3CC.AC8
S3CC.050
(8E15.7)
2 15999 1.0 0.005 1 0.05

SPECTRA3.INP

TR1C00.Q4A
0
TR1C00.Q4A
TR1C00A.050
(8F10.6)
4 12000 1.0 0.005 1 0.05
TR3C00.Q4A
0
TR3C00.Q4A
TR3C00A.050
(8F10.6)
4 12000 1.0 0.005 1 0.05

S1CC.050

S1CC.050
Set1:
15999 points 0.005 dt parameters are t,s,d,sv,pav,sa,mr

97							
1	0.01000	0.00424	0.38240	2.66569	1.70586	1.02250	
2	0.01500	0.00942	1.12846	3.95203	1.68695	1.01116	
3	0.02000	0.01478	1.78694	5.27270	1.68896	1.01236	
4	0.02500	0.02094	1.48340	6.51898	1.67025	1.00115	
5	0.03000	0.03766	2.16668	7.88799	1.68415	1.00948	
6	0.03500	0.05098	3.81005	9.15228	1.67534	1.00420	
7	0.04000	0.06676	4.60543	10.48662	1.68007	1.00704	
8	0.04200	0.07623	4.43469	11.40405	1.74070	1.04338	
9	0.04400	0.08264	4.95536	11.80071	1.71739	1.02941	
10	0.04600	0.08985	4.51109	12.27266	1.70972	1.02481	
11	0.04800	0.09838	4.71765	12.87781	1.71928	1.03054	
12	0.05000	0.10751	5.12165	13.50954	1.73038	1.03720	
13	0.05500	0.12839	7.51774	14.66684	1.70938	1.02460	
14	0.06000	0.15747	7.94611	16.49047	1.76149	1.05584	
15	0.06500	0.18879	10.10117	18.24887	1.79941	1.07857	
16	0.07000	0.22721	13.59237	20.39399	1.86751	1.11939	
17	0.07500	0.25161	13.20151	21.07891	1.80054	1.07925	
18	0.08000	0.29879	14.69405	23.46683	1.87740	1.12532	
19	0.08500	0.32782	16.27116	24.23270	1.82468	1.09372	
20	0.09000	0.38715	19.61784	27.02837	1.92314	1.15273	
21	0.09500	0.46639	18.83205	30.84639	2.08598	1.25034	
22	0.10000	0.52118	22.13347	32.74685	2.09878	1.25802	
23	0.11000	0.60898	22.66736	34.78502	2.02966	1.21658	
24	0.12000	0.77524	27.21112	40.59158	2.16508	1.29775	
25	0.13000	0.94225	31.86408	45.54116	2.24985	1.34857	
26	0.14000	1.07973	38.03613	48.45831	2.22979	1.33654	
27	0.15000	1.32760	44.34030	55.61029	2.38266	1.42817	
28	0.16000	1.45787	50.53853	57.25034	2.29662	1.37660	
29	0.17000	1.83984	48.43523	64.00112	2.57021	1.54059	
30	0.18000	2.18049	53.55482	76.11331	2.71612	1.62804	
31	0.19000	2.44590	58.57046	80.84432	2.73575	1.63981	
32	0.20000	2.62526	62.67080	82.47511	2.65144	1.58928	
33	0.21000	2.85367	75.71450	92.92465	2.70987	1.62436	
34	0.24000	4.26802	107.14139	111.74256	2.99098	1.79280	
35	0.26000	5.51990	131.40338	133.39444	3.30459	1.98078	
36	0.28000	6.50419	125.94003	145.95370	3.34946	2.00767	
37	0.30000	7.52492	104.12332	157.60156	3.37393	2.02234	
38	0.32000	8.99561	115.55287	176.62834	3.54536	2.12510	
39	0.34000	10.33430	144.51660	190.97740	3.61037	2.16406	
40	0.36000	11.85777	160.37582	206.95711	3.69405	2.21422	
41	0.38000	13.82229	182.56612	228.54745	3.86691	2.31783	
42	0.40000	15.39341	216.61101	241.79916	3.88966	2.33147	
43	0.42000	16.70307	238.81120	249.87729	3.82530	2.29289	
44	0.44000	18.20437	250.47702	259.95779	3.79713	2.27601	
45	0.46000	22.10240	218.94986	301.89880	4.21979	2.52935	
46	0.48000	23.70653	212.51624	310.33775	4.15592	2.49107	
47	0.50000	25.88282	228.08356	325.25308	4.17948	2.50519	
48	0.55000	28.71230	278.99075	328.00854	3.83275	2.28736	
49	0.60000	34.33649	354.17337	359.57083	3.85639	2.31153	
50	0.65000	41.06744	356.72165	396.97589	3.92719	2.35397	
51	0.70000	49.59735	377.66327	445.18478	4.09054	2.45188	
52	0.75000	54.47570	354.96664	456.37454	3.91461	2.34643	
53	0.80000	62.35158	395.77444	489.70816	3.93961	2.36141	
54	0.85000	70.62992	458.20224	522.09515	3.95257	2.36918	
55	0.90000	78.01536	515.90104	544.64996	3.89095	2.33224	
56	0.95000	79.79324	499.19333	527.74280	3.57097	2.14045	
57	1.00000	94.31651	504.98669	592.60809	3.80801	2.28253	
58	1.10000	113.25320	665.54218	646.90076	3.78417	2.26824	
59	1.20000	137.65614	682.17780	720.76587	3.86699	2.31788	
60	1.30000	164.02608	828.15387	791.77405	3.92579	2.35313	
61	1.40000	184.16927	843.13617	826.54974	3.80246	2.27920	
62	1.50000	209.62582	931.69116	878.07861	3.76679	2.25782	
63	1.60000	223.16574	939.97168	876.33289	3.52439	2.11259	
64	1.70000	257.48149	998.52191	951.65009	3.60612	2.16151	
65	1.80000	275.42258	967.80609	961.40619	3.44114	2.06262	
66	1.90000	289.34964	935.43036	956.86176	3.24469	1.94487	
67	2.00000	320.09787	1024.35925	1005.61713	3.24042	1.94232	
68	2.20000	349.04321	1188.72632	996.86505	2.91912	1.74972	
69	2.40000	345.21188	1050.11731	903.76257	2.43108	1.45719	
70	2.60000	415.12836	1102.37341	1003.20325	2.48755	1.49104	
71	2.80000	446.46988	1067.82117	1001.87604	2.30798	1.38341	
72	3.00000	476.67511	1108.72144	998.34607	2.14379	1.28699	
73	3.20000	534.83887	1170.94153	1050.15369	2.11392	1.26709	
74	3.40000	589.07428	1193.46139	1088.60669	2.06397	1.23715	
75	3.60000	623.17865	1145.50757	1087.65198	1.94586	1.16635	
76	3.80000	659.90210	1077.66431	1091.12817	1.84939	1.10853	
77	4.00000	691.37075	1027.88426	1085.84558	1.74741	1.04740	
78	4.20000	701.75433	1052.29761	1049.82124	1.60945	0.96470	
79	4.40000	700.27374	1060.83301	999.98853	1.46405	0.87755	
80	4.60000	712.11096	1056.99011	972.67944	1.36162	0.81616	
81	4.80000	728.45789	1112.69788	953.54913	1.27673	0.76527	
82	5.00000	751.02454	1133.51563	943.76532	1.21387	0.72760	
83	5.50000	748.26880	1075.82947	854.82025	1.00213	0.60068	
84	6.00000	722.43866	996.51514	756.53601	0.81227	0.48687	
85	6.50000	766.95892	908.46509	741.37616	0.73559	0.44092	
86	7.00000	822.58777	873.80682	738.35309	0.68478	0.41046	
87	7.50000	828.78003	818.94879	694.31714	0.60287	0.36136	
88	8.00000	828.75964	778.60773	650.90631	0.53075	0.31813	
89	8.50000	841.23773	760.09186	621.84149	0.47812	0.28654	
90	9.00000	853.69446	750.83490	595.99115	0.43345	0.25981	
91	9.50000	848.63818	737.84949	561.27905	0.38746	0.23224	
92	10.00000	818.58038	715.41718	514.32922	0.33794	0.20256	
93	11.00000	752.94299	718.00922	450.08002	0.25862	0.15502	
94	12.00000	778.16113	709.75861	407.44421	0.22459	0.13462	
95	13.00000	776.27209	680.55228	375.18933	0.19071	0.11431	
96	14.00000	762.82599	647.13057	342.35550	0.16182	0.09700	
97	15.00000	748.14197	640.59607	313.38098	0.13876	0.08317	

S3CC.050

S3CC.050
SetJ:
15999 points 0.005 dt parameters are t, sd, sv, pv, sa, nr

Point ID	t	sd	sv	pv	sa	nr
1	0.01000	0.00407	0.17999	2.55861	1.63894	1.00363
2	0.01500	0.00914	0.48247	3.82894	1.63501	1.00122
3	0.02000	0.01642	1.49100	5.15705	1.65190	1.01156
4	0.02500	0.02397	1.38000	6.52707	1.67277	1.03434
5	0.03000	0.03690	1.51223	7.72859	1.64979	1.01027
6	0.03500	0.04969	2.20843	8.92073	1.63264	0.99977
7	0.04000	0.06573	4.42596	10.32521	1.65396	1.01283
8	0.04200	0.07239	4.73754	10.82968	1.65132	1.01121
9	0.04400	0.07972	4.57190	11.38374	1.65793	1.01526
10	0.04600	0.08746	4.03526	11.94689	1.66347	1.01865
11	0.04800	0.09613	4.19428	12.58342	1.68006	1.02881
12	0.05000	0.10474	4.26656	13.16208	1.68795	1.03363
13	0.05500	0.12966	4.48820	14.81178	1.72344	1.05537
14	0.06000	0.15886	4.93534	16.63528	1.77893	1.08935
15	0.06500	0.17893	6.52502	17.29646	1.70532	1.04427
16	0.07000	0.20155	8.01008	18.09116	1.65609	1.01413
17	0.07500	0.24135	11.24976	20.21956	1.73000	1.05939
18	0.08000	0.27271	13.47621	21.41886	1.71675	1.05128
19	0.08500	0.31358	14.59441	23.17950	1.74882	1.07091
20	0.09000	0.36127	15.59604	25.22125	1.79249	1.09766
21	0.09500	0.41387	16.76602	27.37279	1.85033	1.13307
22	0.10000	0.47403	18.16407	29.78462	1.90959	1.16926
23	0.11000	0.60765	24.02493	34.70906	2.02405	1.23948
24	0.12000	0.74811	27.87101	39.17080	2.09105	1.28048
25	0.13000	0.90724	33.17875	43.84907	2.15974	1.32255
26	0.14000	1.10037	32.76777	49.38461	2.25836	1.38294
27	0.15000	1.30982	38.47551	54.86579	2.34739	1.43745
28	0.16000	1.59453	42.18465	62.61713	2.51127	1.53780
29	0.17000	1.99081	42.89137	73.58006	2.77477	1.69917
30	0.18000	2.11723	47.23977	73.90511	2.63161	1.61150
31	0.19000	2.49164	55.48930	82.39701	2.78507	1.70547
32	0.20000	2.84952	59.14955	89.52031	2.87652	1.76147
33	0.22000	3.50231	71.99142	100.02570	2.91995	1.78807
34	0.24000	4.46803	86.21294	116.97272	3.13155	1.91764
35	0.26000	5.56098	94.18864	134.38719	3.32092	2.03361
36	0.28000	6.89924	128.93840	154.81863	3.55083	2.17440
37	0.30000	8.77813	139.79877	183.84877	3.93742	2.41123
38	0.32000	9.73755	129.55070	191.19440	3.83839	2.35048
39	0.34000	10.46394	135.81387	196.14543	3.70754	2.27036
40	0.36000	11.88946	149.78423	207.51025	3.70438	2.26842
41	0.38000	13.27617	173.61707	219.51749	3.72362	2.27347
42	0.40000	14.94218	187.43405	234.71132	3.77055	2.30894
43	0.42000	16.26750	210.37854	243.36121	3.72385	2.28035
44	0.44000	17.92181	219.38771	255.92279	3.74054	2.29057
45	0.46000	19.02500	229.92368	259.86441	3.63148	2.22378
46	0.48000	21.74136	247.63783	284.59375	3.81144	2.33398
47	0.50000	23.37008	271.31503	293.67709	3.77999	2.31472
48	0.55000	26.30332	269.77603	300.48837	3.51324	2.15138
49	0.60000	32.19749	320.32312	337.17136	3.61544	2.21396
50	0.65000	41.53804	297.77554	401.52493	3.97043	2.43134
51	0.70000	48.05046	364.00516	431.29993	3.95803	2.42375
52	0.75000	53.85356	420.86557	451.16254	3.86426	2.36633
53	0.80000	60.98380	475.94940	478.96564	3.85178	2.35868
54	0.85000	66.35065	491.55292	490.46283	3.71433	2.27452
55	0.90000	75.52803	524.06769	527.28516	3.77321	2.31057
56	0.95000	84.69800	587.88263	560.18231	3.79725	2.32529
57	1.00000	92.01063	622.75409	578.11981	3.72403	2.28046
58	1.10000	112.23817	682.35126	641.10297	3.75655	2.29914
59	1.20000	135.68370	788.94336	710.43817	3.81091	2.33066
60	1.30000	155.73064	766.88085	759.68085	3.73174	2.28517
61	1.40000	185.70148	745.89056	831.42627	3.82475	2.34214
62	1.50000	216.73026	860.57977	907.83759	3.89493	2.38511
63	1.60000	241.19075	898.69690	947.15387	3.80682	2.33115
64	1.70000	267.25229	905.68805	987.76215	3.73734	2.28860
65	1.80000	282.96439	928.21747	987.73206	3.53185	2.16277
66	1.90000	299.35184	941.09021	989.93842	3.35432	2.05406
67	2.00000	320.62982	966.04529	1007.28833	3.24291	1.98583
68	2.20000	346.23346	951.88654	988.84045	2.89195	1.77092
69	2.40000	365.59750	941.55664	957.13202	2.56888	1.57309
70	2.60000	406.00262	1037.10986	981.14990	2.42832	1.48701
71	2.80000	442.25305	1038.66138	992.41351	2.28290	1.39796
72	3.00000	467.29645	1036.92761	978.70343	2.10096	1.28655
73	3.20000	524.99548	1105.00171	1030.42617	2.07399	1.27003
74	3.40000	565.28558	1088.34924	1044.44526	1.97882	1.21175
75	3.60000	596.85136	1075.60959	1041.70251	1.86305	1.24086
76	3.80000	632.44421	1032.74585	1045.72742	1.77230	1.08468
77	4.00000	672.57397	1017.21216	1056.47681	1.70101	1.04164
78	4.20000	708.22345	1073.36560	1059.49988	1.62629	0.99588
79	4.40000	731.48004	1125.30261	1044.55103	1.53107	0.93757
80	4.60000	738.78693	1159.76978	1009.11639	1.41386	0.86579
81	4.80000	760.23969	1146.01550	995.15143	1.33630	0.81830
82	5.00000	785.41827	1141.89783	986.98572	1.27163	0.77870
83	5.50000	797.70825	1094.74072	911.29974	1.07058	0.65558
84	6.00000	765.47913	1053.22888	801.60791	0.86055	0.52697
85	6.50000	742.93115	996.66034	718.14984	0.71237	0.43623
86	7.00000	761.19855	961.24792	683.25024	0.62819	0.38468
87	7.50000	782.08478	954.02118	655.19781	0.56426	0.34553
88	8.00000	797.65686	963.48279	626.47827	0.50631	0.31004
89	8.50000	819.03632	974.28931	605.43024	0.46120	0.28242
90	9.00000	818.81273	976.38477	571.49951	0.41147	0.25197
91	9.50000	794.84961	967.90405	525.70392	0.35852	0.21935
92	10.00000	751.78382	953.43453	472.36600	0.30626	0.18754
93	11.00000	727.32202	901.76404	435.44534	0.24427	0.14958
94	12.00000	743.88904	839.29944	389.49939	0.21559	0.13202
95	13.00000	766.85712	782.23224	370.63885	0.19033	0.11655
96	14.00000	774.52014	735.32635	347.40382	0.16659	0.10201
97	15.00000	775.42365	698.43159	324.80872	0.14611	0.08947

TR1C01A.050

TRIC01A.050
TRIC: HUMBOLDT BAY, TRANSPORTER ROUTE, PG&E, 09/2002
12000 points 0.005 dt parameters are t, sd, sv, pv, sa, nr

1	0.01000	0.00490	0.09312	3.07771	1.97085	1.01618
2	0.01500	0.01084	0.16214	4.54895	1.94213	1.00157
3	0.02000	0.01925	0.27443	6.04759	1.93651	0.99853
4	0.02500	0.03002	0.41194	7.54516	1.93326	0.99680
5	0.03000	0.04333	0.58346	9.07428	1.93740	0.99893
6	0.03500	0.05893	0.80782	10.57859	1.93588	0.99815
7	0.04000	0.07714	1.05210	12.11731	1.94025	1.00040
8	0.04200	0.08512	1.14505	12.73377	1.94194	1.00127
9	0.04400	0.09349	1.27316	13.35028	1.94342	1.00204
10	0.04600	0.10225	1.40534	13.96622	1.94453	1.00261
11	0.04800	0.11139	1.53726	14.58096	1.94552	1.00312
12	0.05000	0.12092	1.67110	15.19495	1.94674	1.00375
13	0.05500	0.14655	2.01744	16.74184	1.94996	1.00541
14	0.06000	0.17479	2.42993	18.30348	1.95425	1.00762
15	0.06500	0.20560	2.88086	19.87452	1.95884	1.00999
16	0.07000	0.23904	3.36166	21.45577	1.96377	1.01253
17	0.07500	0.27512	3.92962	23.04866	1.96903	1.01524
18	0.08000	0.31391	4.51459	24.65464	1.97461	1.01812
19	0.08500	0.35547	5.17509	26.27621	1.98065	1.02123
20	0.09000	0.39991	5.88043	27.91901	1.98753	1.02478
21	0.09500	0.44727	6.65977	29.58195	1.99505	1.02866
22	0.10000	0.49770	7.51554	31.27169	2.00355	1.03304
23	0.11000	0.60829	9.47054	34.74519	2.02365	1.04340
24	0.12000	0.73333	11.82356	38.39695	2.04982	1.05690
25	0.13000	0.87553	14.74523	42.31607	2.08488	1.07497
26	0.14000	1.04043	18.45482	46.69429	2.13631	1.10149
27	0.15000	1.24248	23.50678	52.04498	2.22454	1.14698
28	0.16000	1.53403	31.48427	60.24125	2.41423	1.24479
29	0.17000	1.98004	42.06763	73.18219	2.76296	1.42460
30	0.18000	2.19753	45.44719	76.70840	2.73309	1.40919
31	0.19000	2.61895	56.15680	86.60719	2.92760	1.50948
32	0.20000	3.46586	84.82983	108.88321	3.49981	1.80452
33	0.22000	4.09913	96.28816	117.07074	3.41331	1.75992
34	0.24000	5.64102	130.08618	147.68163	3.96296	2.04332
35	0.26000	7.63812	172.27887	184.58359	4.56688	2.35471
36	0.28000	9.12494	214.58798	209.02676	4.79518	2.47293
37	0.30000	9.95131	239.10397	208.41985	4.46273	2.30300
38	0.32000	11.63752	256.31689	228.50224	4.58791	2.36555
39	0.34000	12.84668	276.81361	237.40607	4.48772	2.31389
40	0.36000	14.09230	297.41624	245.95694	4.39273	2.26491
41	0.38000	16.51773	330.79260	273.11572	4.62198	2.38311
42	0.40000	19.08163	368.50070	299.73361	4.81785	2.48411
43	0.42000	20.61566	386.54221	308.40952	4.72411	2.43577
44	0.44000	22.13897	304.33400	316.14374	4.62107	2.38265
45	0.46000	25.92916	269.08301	354.16895	4.94825	2.55134
46	0.48000	27.98892	250.82458	366.37411	4.90766	2.53041
47	0.50000	30.54596	268.76392	383.85187	4.93494	2.54448
48	0.55000	33.08741	330.11508	377.98969	4.41687	2.27736
49	0.60000	41.98359	430.36880	439.65115	4.71429	2.43071
50	0.65000	47.82388	435.76050	460.35393	4.55327	2.34768
51	0.70000	64.32147	509.35516	577.34814	5.30551	2.73555
52	0.75000	69.84112	480.59109	585.09961	5.01882	2.58773
53	0.80000	79.71034	523.70184	626.04358	5.03627	2.59672
54	0.85000	90.58872	598.12561	669.63025	5.07065	2.61445
55	0.90000	100.41508	680.27423	701.02954	5.01102	2.58370
56	0.95000	100.61058	659.95160	665.42621	4.50274	2.32160
57	1.00000	104.03497	627.09637	666.23743	4.28106	2.20733
58	1.10000	129.68929	770.33978	740.78345	4.33561	2.23546
59	1.20000	151.56076	761.72870	793.57025	4.25748	2.19518
60	1.30000	179.35966	908.97589	866.88464	4.29284	2.21341
61	1.40000	199.66898	937.69000	896.11224	4.12295	2.12581
62	1.50000	222.95346	1013.43359	933.90527	4.00796	2.06652
63	1.60000	236.79453	1016.65930	929.88989	3.74096	1.92885
64	1.70000	271.58307	1050.79724	1003.76868	3.80237	1.96052
65	1.80000	289.58640	1012.87231	1010.84723	3.61925	1.86610
66	1.90000	302.54437	984.76385	1000.49597	3.39458	1.75026
67	2.00000	331.88193	1081.11470	1042.63782	3.15996	1.73241
68	2.20000	354.23242	1228.19250	1011.68542	2.96511	1.52882
69	2.40000	354.83594	1081.40808	928.95831	2.49967	1.28884
70	2.60000	425.86040	1125.16663	1028.65503	2.55170	1.31567
71	2.80000	455.46765	1085.51233	1022.06702	2.35442	1.21395
72	3.00000	484.91995	1136.64246	1015.61401	2.18087	1.12447
73	3.20000	543.79742	1185.76294	1047.74377	2.15156	1.10935
74	3.40000	597.21912	1221.64709	1103.65833	2.09224	1.07877
75	3.60000	630.55573	1180.68262	1100.52734	1.97003	1.01575
76	3.80000	665.43182	1108.52136	1100.27148	1.86399	0.96108
77	4.00000	696.07709	1030.12671	1093.39539	1.76015	0.90754
78	4.20000	705.97614	1089.23132	1056.13794	1.61848	0.83449
79	4.40000	701.68469	1088.87170	1002.00336	1.46836	0.75709
80	4.60000	712.68134	1098.19678	973.45850	1.36161	0.70205
81	4.80000	732.90369	1140.16748	959.36865	1.28429	0.66219
82	5.00000	757.58301	1154.58630	952.00690	1.22498	0.63161
83	5.50000	752.15570	1090.13049	859.26062	1.00710	0.51924
84	6.00000	721.29508	1004.28186	755.33954	0.81260	0.41898
85	5.50000	776.89210	929.54932	750.68799	0.74494	0.38410
86	7.00000	831.69458	895.45814	746.52734	0.69221	0.35491
87	7.50000	836.24054	840.94830	700.56726	0.60922	0.31412
88	8.00000	834.93359	800.64587	655.75531	0.53611	0.27442
89	8.50000	846.11353	782.01202	625.44568	0.48197	0.24851
90	9.00000	857.15839	772.57257	598.40942	0.43582	0.22471
91	9.50000	850.39191	759.37384	562.43896	0.38833	0.20022
92	10.00000	818.17566	736.77478	514.07513	0.33792	0.17423
93	11.00000	758.72028	733.44897	433.38000	0.26223	0.13521
94	12.00000	781.27692	720.82434	409.07565	0.22753	0.11732
95	13.00000	778.77020	688.30170	376.39673	0.19321	0.09962
96	14.00000	765.02777	668.25714	343.34366	0.16397	0.08454
97	15.00000	750.23749	664.13397	314.25876	0.14071	0.07255

TR3C01A.050

TR3C01A.050
TR3C: HUMBOLDT BAY, TRANSPORTER ROUTE, PG4E, 09/2002
12000 points 0.005 dt parameters are t, sd, sv, pev, sa, nr

97	1	0.01000	0.00520	0.10338	3.26985	2.09426	1.00049
	2	0.01500	0.01172	0.19641	4.90850	2.09604	1.00135
	3	0.02000	0.02082	0.36241	6.54233	2.09517	1.00093
	4	0.02500	0.03257	0.53201	8.18593	2.09726	1.00193
	5	0.03000	0.04693	0.76644	9.82937	2.09857	1.00256
	6	0.03500	0.06196	1.04227	11.48291	2.10123	1.00382
	7	0.04000	0.08377	1.35051	13.15808	2.10716	1.00666
	8	0.04200	0.09240	1.50790	13.82294	2.10785	1.00699
	9	0.04400	0.10144	1.67001	14.48616	2.10856	1.00733
	10	0.04600	0.11098	1.82418	15.15865	2.11054	1.00827
	11	0.04800	0.12099	1.98323	15.82556	2.11163	1.00880
	12	0.05000	0.13123	2.14929	16.49110	2.11303	1.00946
	13	0.05500	0.15920	2.61134	18.18666	2.11825	1.01196
	14	0.06000	0.18982	3.17696	19.89828	2.12200	1.01375
	15	0.06500	0.22327	3.75305	21.58257	2.12648	1.01589
	16	0.07000	0.25942	4.38070	23.30380	2.13201	1.01853
	17	0.07500	0.29887	5.08167	25.03831	2.13777	1.02128
	18	0.08000	0.34103	5.87890	26.78425	2.14398	1.02425
	19	0.08500	0.38618	6.74946	28.54665	2.15072	1.02747
	20	0.09000	0.43438	7.70827	30.32532	2.15797	1.03093
	21	0.09500	0.48549	8.74406	32.10979	2.16488	1.03423
	22	0.10000	0.53970	9.88144	33.91063	2.17217	1.03771
	23	0.11000	0.65752	12.54387	37.55747	2.18754	1.04506
	24	0.12000	0.80340	15.88230	42.06588	2.24787	1.07388
	25	0.13000	0.97663	20.16846	47.20287	2.32811	1.11221
	26	0.14000	1.18581	25.98040	53.21889	2.43712	1.15429
	27	0.15000	1.48770	34.41372	60.74659	2.59814	1.24122
	28	0.16000	1.81259	48.20488	75.10729	3.01255	1.43919
	29	0.17000	2.66616	71.54356	98.54105	3.72741	1.78070
	30	0.18000	3.23899	89.75721	113.06203	4.03331	1.92684
	31	0.19000	4.07012	103.11606	134.59630	4.54817	2.17281
	32	0.20000	5.14446	123.28976	161.61803	5.18795	2.47845
	33	0.22000	6.30942	143.11557	180.19647	5.26165	2.51366
	34	0.24000	7.61588	168.37219	199.38332	5.33776	2.55002
	35	0.26000	8.40870	179.35490	205.13873	5.07668	2.42529
	36	0.28000	11.49238	239.33804	257.88849	5.92526	2.83069
	37	0.30000	12.65921	235.62909	265.13388	5.68088	2.71394
	38	0.32000	14.16639	211.40672	278.15649	5.58745	2.66930
	39	0.34000	15.37581	221.72043	284.14432	5.37442	2.56754
	40	0.36000	17.16190	240.22885	299.52475	5.35239	2.55701
	41	0.38000	19.25391	267.26163	318.35760	5.38212	2.57121
	42	0.40000	23.78780	303.84857	373.45784	6.00339	2.86801
	43	0.42000	26.12178	362.98035	390.78091	5.98586	2.85964
	44	0.44000	28.69215	373.16251	409.72293	5.98753	2.86044
	45	0.46000	32.49567	389.83466	443.86160	6.20448	2.96408
	46	0.48000	36.59037	414.60480	478.96680	6.41389	3.06412
	47	0.50000	41.54710	447.86731	522.09625	6.71870	3.20974
	48	0.55000	44.22644	466.76187	505.24170	5.91071	2.82373
	49	0.60000	52.72786	541.20233	552.16486	5.92334	2.82977
	50	0.65000	68.80108	556.65143	665.06146	6.58172	3.14430
	51	0.70000	83.82838	695.75519	752.44171	6.91583	3.30392
	52	0.75000	101.37196	806.37567	849.25177	7.28625	3.48088
	53	0.80000	112.90066	874.54828	886.71967	7.13339	3.40785
	54	0.85000	114.98460	870.64844	849.96411	6.43779	3.07554
	55	0.90000	119.88561	884.35461	836.95947	5.98764	2.86049
	56	0.95000	130.13461	885.37628	860.69464	5.83594	2.78802
	57	1.00000	128.52657	906.44476	807.55627	5.20311	2.48569
	58	1.10000	128.40829	798.86052	733.46643	4.29844	2.05350
	59	1.20000	139.44655	890.38629	730.14038	3.92379	1.87452
	60	1.30000	155.45615	852.95270	751.35370	3.72553	1.77980
	61	1.40000	178.79738	740.72205	802.44073	3.68312	1.75954
	62	1.50000	206.13408	773.86090	863.45245	3.69957	1.76741
	63	1.60000	223.72836	837.83484	878.57922	3.53265	1.68766
	64	1.70000	241.76453	856.18652	893.55957	3.37928	1.61439
	65	1.80000	260.44745	836.95709	909.13312	3.25175	1.55347
	66	1.90000	278.13843	873.69623	919.78699	3.11771	1.48943
	67	2.00000	299.24899	912.03796	940.11847	3.02757	1.44637
	68	2.20000	321.64157	885.92596	918.60614	2.68508	1.28275
	69	2.40000	352.97305	899.74434	924.08130	2.47985	1.18470
	70	2.60000	387.40305	1006.28723	936.20197	2.31642	1.10663
	71	2.80000	424.38095	1053.36194	952.30859	2.19093	1.04668
	72	3.00000	455.51340	1012.18195	954.02502	2.04667	0.97776
	73	3.20000	517.63843	1093.85010	1016.18068	2.04694	0.97789
	74	3.40000	554.17365	1070.86487	1024.11047	1.94189	0.92770
	75	3.60000	580.96100	1043.43945	1013.96820	1.81220	0.86575
	76	3.80000	615.16711	990.85590	1017.16022	1.72133	0.82234
	77	4.00000	657.83246	1037.85962	1033.32080	1.66400	0.79495
	78	4.20000	695.14520	1095.01978	1039.93481	1.59680	0.76284
	79	4.40000	717.94977	1139.63806	1025.22986	1.50434	0.71867
	80	4.60000	723.34113	1172.89673	988.01880	1.38460	0.66147
	81	4.80000	746.10315	1173.81287	976.64673	1.31015	0.62590
	82	5.00000	773.18237	1141.94409	971.60968	1.25235	0.59829
	83	5.50000	785.42816	1067.97791	897.27100	1.05586	0.50442
	84	6.00000	755.88794	1023.35547	791.56403	0.84745	0.40485
	85	6.50000	737.08784	964.91785	712.50098	0.70710	0.33780
	86	7.00000	759.27234	929.15149	681.52124	0.62786	0.29995
	87	7.50000	779.87714	922.06816	653.94839	0.56395	0.26942
	88	8.00000	795.72852	930.94501	624.96375	0.50597	0.24172
	89	8.50000	814.54425	940.43907	602.10968	0.45984	0.21968
	90	9.00000	810.32050	940.59998	565.71039	0.40842	0.19511
	91	9.50000	783.20715	928.55457	518.00372	0.35346	0.16886
	92	10.00000	749.71234	912.67963	471.05817	0.30386	0.14516
	93	11.00000	729.54742	862.13690	416.71649	0.24521	0.11715
	94	12.00000	746.92725	800.44525	391.09021	0.21847	0.10437
	95	13.00000	767.14453	743.56586	370.77777	0.19232	0.09188
	96	14.00000	772.86926	696.81775	346.86292	0.16812	0.08031
	97	15.00000	771.92053	660.20648	323.34134	0.14725	0.07034

TR1C00A.050

TR1C00A.050
 TR1C: HUMBOLDT BAY, TRANSPORTER ROUTE, PG&E, 09/2002
 12000 points 0.005 dc parameters are t,sd,sv,psv,sa,mr

1	0.01000	0.00480	0.15028	3.01355	1.93023	1.00047
2	0.01500	0.01084	0.16479	4.53953	1.93817	1.00459
3	0.02000	0.01921	0.27038	6.03349	1.93221	1.00150
4	0.02500	0.03000	0.42350	7.54092	1.93208	1.00143
5	0.03000	0.04331	0.60410	9.07007	1.93638	1.00366
6	0.03500	0.05895	0.81159	10.58233	1.93646	1.00370
7	0.04000	0.07713	1.07760	12.11571	1.94009	1.00558
8	0.04200	0.08507	1.19236	12.72677	1.94099	1.00605
9	0.04400	0.09341	1.31535	13.33824	1.94183	1.00648
10	0.04600	0.10214	1.43706	13.95133	1.94275	1.00696
11	0.04800	0.11127	1.56702	14.56564	1.94379	1.00750
12	0.05000	0.12083	1.70137	15.18369	1.94531	1.00829
13	0.05500	0.14650	2.06489	16.75594	1.94936	1.01039
14	0.06000	0.17472	2.47393	18.29671	1.95374	1.01266
15	0.06500	0.20546	2.94605	19.81111	1.95774	1.01473
16	0.07000	0.23884	3.43829	21.43823	1.96190	1.01689
17	0.07500	0.27487	3.99860	23.02770	1.96674	1.01940
18	0.08000	0.31160	4.60531	24.62993	1.97196	1.02210
19	0.08500	0.35508	5.27992	26.24747	1.97784	1.02515
20	0.09000	0.39948	6.00171	27.88863	1.98475	1.02873
21	0.09500	0.44680	6.80431	29.55082	1.99231	1.03265
22	0.10000	0.49719	7.67937	31.23955	2.00082	1.03706
23	0.11000	0.60773	9.68075	34.71348	2.02106	1.04755
24	0.12000	0.73273	12.08171	38.36570	2.04739	1.06120
25	0.13000	0.87493	15.07248	42.28745	2.08355	1.07994
26	0.14000	1.03998	18.87734	46.67403	2.13644	1.10736
27	0.15000	1.24311	24.05569	52.07121	2.22570	1.15362
28	0.16000	1.53708	32.19073	60.36113	2.42049	1.25458
29	0.17000	1.99260	42.54861	73.64637	2.77827	1.43899
30	0.18000	2.21320	48.75836	77.25535	2.73799	1.42951
31	0.19000	2.41169	57.84357	84.48143	2.99592	1.52984
32	0.20000	3.53277	86.95011	110.98537	3.56760	1.84915
33	0.22000	4.19460	97.62450	119.79755	3.49329	1.81063
34	0.24000	5.72841	132.12839	149.96951	4.02204	2.08470
35	0.26000	7.73943	174.07748	187.03191	4.42440	2.39691
36	0.28000	9.28317	176.84538	208.31380	4.78030	2.47771
37	0.30000	9.94562	138.83415	208.30064	4.45957	2.31147
38	0.32000	11.64948	156.61542	228.73698	4.59261	2.38043
39	0.34000	12.87240	177.45508	237.88139	4.49687	2.33081
40	0.36000	14.15882	198.48352	247.11806	4.41332	2.28750
41	0.38000	16.58681	232.11736	274.25781	4.64271	2.40640
42	0.40000	19.13123	269.48187	300.51270	4.83174	2.50439
43	0.42000	20.66246	287.24189	309.10965	4.73430	2.45387
44	0.44000	22.18356	305.30823	316.78055	4.62986	2.39974
45	0.46000	25.93991	269.78339	354.31573	4.94982	2.56558
46	0.48000	28.00003	250.83362	366.81953	4.90918	2.54451
47	0.50000	30.54920	268.74719	383.89258	4.93586	2.55834
48	0.55000	33.03442	329.96680	377.38419	4.40990	2.28573
49	0.60000	41.93863	429.82880	439.18030	4.70926	2.44089
50	0.65000	47.59302	435.52911	460.05505	4.55027	2.35849
51	0.70000	64.31488	509.43143	577.28900	5.30499	2.74967
52	0.75000	69.83821	490.47867	585.07526	5.01870	2.60128
53	0.80000	79.69876	523.83502	625.95258	5.03562	2.61005
54	0.85000	90.56577	598.31348	669.46057	5.06941	2.62757
55	0.90000	100.37137	680.39032	700.72437	5.00883	2.59617
56	0.95000	106.57973	659.80695	665.22223	4.50133	2.33312
57	1.00000	106.02941	627.83563	666.20245	4.28087	2.21885
58	1.10000	129.69981	770.59314	740.84357	4.33603	2.24744
59	1.20000	151.55948	761.83496	793.56356	4.25744	2.20671
60	1.30000	178.24160	909.48695	866.79730	4.29237	2.24881
61	1.40000	199.65888	917.67450	896.07141	4.12279	2.13691
62	1.50000	222.93240	1013.50153	933.81708	4.00757	2.07719
63	1.60000	236.78621	1016.87836	929.85724	3.74083	1.93894
64	1.70000	271.58405	1050.66187	1003.77228	3.80239	1.97085
65	1.80000	289.58817	1012.69812	1010.85339	3.61930	1.87595
66	1.90000	302.54004	984.96503	1000.48163	3.39454	1.75945
67	2.00000	331.86896	1081.47363	1042.59717	3.35982	1.74145
68	2.20000	354.24335	1227.91968	1011.71661	2.96522	1.53693
69	2.40000	354.81262	1081.16345	928.89728	2.49949	1.29553
70	2.60000	425.63760	1125.09521	1028.59998	2.55153	1.32250
71	2.80000	455.47556	1085.53259	1022.08472	2.35449	1.22037
72	3.00000	484.94070	1136.57056	1015.65747	2.18102	1.13046
73	3.20000	543.79657	1185.59839	1047.74207	2.15161	1.11522
74	3.40000	597.20087	1221.83093	1103.62463	2.09211	1.08438
75	3.60000	630.55939	1180.90759	1100.53369	1.97004	1.02111
76	3.80000	665.41958	1108.66687	1100.25134	1.86397	0.95613
77	4.00000	696.08240	1030.13318	1093.40369	1.76016	0.91232
78	4.20000	705.98120	1089.66357	1056.14551	1.61848	0.83889
79	4.40000	701.69617	1088.88391	1002.01978	1.46840	0.76110
80	4.60000	712.69257	1098.15259	973.47388	1.36164	0.70576
81	4.80000	732.91473	1139.83643	959.38312	1.28435	0.66570
82	5.00000	757.59717	1154.39111	952.02472	1.22498	0.63493
83	5.50000	752.14832	1090.40247	859.25220	1.00701	0.52195
84	6.00000	721.31171	1004.53064	755.35590	0.81261	0.42119
85	6.50000	776.60504	930.08478	750.70050	0.74495	0.38612
86	7.00000	831.70721	896.17084	746.53864	0.69224	0.35880
87	7.50000	836.23053	841.43707	700.55890	0.60923	0.31578
88	8.00000	834.91882	801.13161	655.74371	0.53632	0.27788
89	8.50000	846.08124	782.48505	625.42181	0.48196	0.24981
90	9.00000	857.09631	773.02134	598.36609	0.43577	0.22587
91	9.50000	850.29047	759.76892	562.37183	0.38823	0.20124
92	10.00000	818.16532	737.22948	514.06836	0.33790	0.17314
93	11.00000	758.73779	733.75592	433.38994	0.28226	0.13593
94	12.00000	781.25665	720.87781	409.06503	0.22754	0.11794
95	13.00000	778.82458	688.11786	376.42300	0.19323	0.10015
96	14.00000	764.99817	668.13440	343.33038	0.16397	0.08499
97	15.00000	750.19092	664.03485	314.23926	0.14070	0.07293

TR3C00A.050

TR3C00A.050
TR3C: HUMBOLDT BAY, TRANSPORTER ROUTE, F04E, 09/2002
12000 points 0.005 dt parameters are t,rd,sv,psv,sa,mt

97						
1	0.01000	0.00522	0.10028	3.28110	2.10143	1.00164
2	0.01500	0.01175	0.20657	4.92036	2.10094	1.00141
3	0.02000	0.02089	0.36923	6.56204	2.10145	1.00165
4	0.02500	0.03265	0.53686	8.20627	2.10241	1.00211
5	0.03000	0.04697	0.80672	9.83804	2.10043	1.00117
6	0.03500	0.06402	1.07763	11.49273	2.10314	1.00246
7	0.04000	0.08380	1.36790	13.16303	2.10759	1.00458
8	0.04200	0.09247	1.54002	13.83396	2.10963	1.00555
9	0.04400	0.10156	1.71315	14.50239	2.11108	1.00624
10	0.04600	0.11108	1.88271	15.17215	2.11259	1.00696
11	0.04800	0.12103	2.05922	15.84338	2.11413	1.00770
12	0.05000	0.13146	2.23761	16.51995	2.11624	1.00870
13	0.05500	0.15946	2.72516	18.21630	2.12162	1.01136
14	0.06000	0.19007	3.25732	19.90434	2.12522	1.01398
15	0.06500	0.22351	3.84162	21.60511	2.12938	1.01496
16	0.07000	0.25997	4.49460	23.33495	2.13568	1.01797
17	0.07500	0.29917	5.20675	25.06305	2.14115	1.02057
18	0.08000	0.34120	6.02018	26.79794	2.14641	1.02308
19	0.08500	0.38629	6.91333	28.55455	2.15265	1.02606
20	0.09000	0.43450	7.89829	30.33395	2.15950	1.02932
21	0.09500	0.48569	8.95889	32.12273	2.16620	1.03251
22	0.10000	0.53994	10.12604	33.92516	2.17308	1.03579
23	0.11000	0.66345	12.85113	37.89627	2.20912	1.05297
24	0.12000	0.81246	16.27504	42.54006	2.27298	1.08341
25	0.13000	0.98800	20.65392	47.75229	2.35504	1.12252
26	0.14000	1.19994	26.57698	53.85319	2.46617	1.17549
27	0.15000	1.46793	35.31081	61.48841	2.62931	1.25325
28	0.16000	1.81800	49.33666	75.33987	3.02640	1.44252
29	0.17000	2.27410	72.48369	98.83668	3.73689	1.78118
30	0.18000	3.27710	91.58322	114.39250	4.08901	1.94902
31	0.19000	4.13944	105.77763	136.88869	4.63798	2.21068
32	0.20000	5.27332	126.57804	165.66611	5.31638	2.53404
33	0.22000	6.42351	148.01897	183.45497	5.35814	2.55395
34	0.24000	7.80789	173.06721	204.41010	5.47124	2.60785
35	0.26000	8.63399	183.10425	208.64978	5.16502	2.46189
36	0.28000	11.64170	242.54694	261.23917	6.00363	2.86162
37	0.30000	12.75812	237.31667	267.20547	5.72525	2.72893
38	0.32000	14.23129	211.77499	279.43066	5.61302	2.67543
39	0.34000	15.47664	223.35336	286.00766	5.40949	2.57842
40	0.36000	17.25879	241.30605	301.22263	5.38230	2.56546
41	0.38000	19.26247	267.11929	318.49915	5.38422	2.56638
42	0.40000	23.83166	304.88239	374.34689	6.01413	2.86662
43	0.42000	26.18403	364.20908	391.71218	5.99919	2.85950
44	0.44000	28.74682	374.46329	410.50366	5.99788	2.85887
45	0.46000	32.45690	390.12225	443.33197	6.19808	2.95430
46	0.48000	36.54536	414.68491	478.37766	6.40627	3.05353
47	0.50000	41.51008	447.51239	521.63104	6.71210	3.19931
48	0.55000	44.20969	466.69260	505.05026	5.90884	2.81643
49	0.60000	52.61775	539.83197	551.01178	5.91109	2.81751
50	0.65000	68.71218	556.65607	664.20209	6.57317	3.13308
51	0.70000	83.76051	695.39038	751.83252	6.91022	3.29374
52	0.75000	101.30766	805.94202	848.71307	7.28160	3.47076
53	0.80000	112.82989	874.11542	886.16382	7.12896	3.39800
54	0.85000	114.32075	870.29895	849.49219	6.43420	3.06685
55	0.90000	119.83603	884.03058	836.61334	5.98517	2.85282
56	0.95000	130.09241	884.86707	860.41547	5.83406	2.78079
57	1.00000	128.46700	906.33521	807.18195	5.20068	2.47889
58	1.10000	128.34996	798.25511	735.13524	4.29647	2.04790
59	1.20000	139.38481	889.80408	729.83714	3.92310	1.86946
60	1.30000	155.47406	852.04065	751.44025	3.72602	1.77600
61	1.40000	178.78244	740.24249	802.37372	3.68278	1.75539
62	1.50000	206.15065	771.91772	863.52185	3.69991	1.76355
63	1.60000	223.73305	838.06659	878.59760	3.53271	1.68386
64	1.70000	241.78270	856.47168	893.62677	3.37963	1.61089
65	1.80000	260.44452	837.86041	909.12286	3.25171	1.54992
66	1.90000	278.10999	874.81964	919.69293	3.11734	1.48587
67	2.00000	299.23114	913.10913	940.06238	3.02738	1.44299
68	2.20000	321.61124	886.69385	918.51953	2.68478	1.27969
69	2.40000	352.93893	899.65863	923.99194	2.47954	1.28187
70	2.60000	387.427581006	78172	936.26129	2.31659	1.10420
71	2.80000	424.364721053	74109	952.27216	2.19089	1.04428
72	3.00000	455.512631012	48303	954.02344	2.04666	0.97554
73	3.20000	517.428851093	583261016	36182	2.04699	0.97566
74	3.40000	554.158631070	647221024	08276	1.94181	0.92556
75	3.60000	580.946781043	976931013	94342	1.81215	0.86376
76	3.80000	615.16260	990.540341017	15277	1.72135	0.82048
77	4.00000	657.838621037	853031033	33057	1.66403	0.79316
78	4.20000	695.126161094	922241039	90637	1.59676	0.76109
79	4.40000	717.935611139	639771025	20959	1.50430	0.71702
80	4.60000	723.325561173	05554	987.99756	1.38455	0.65994
81	4.80000	746.086431174	04895	976.62482	1.31005	0.62443
82	5.00000	773.231321142	20154	971.67114	1.25252	0.59701
83	5.50000	785.372561067	76477	897.20746	1.05582	0.50325
84	6.00000	755.877261023	16455	791.55286	0.84747	0.40394
85	6.50000	737.11603	964.75006	712.52869	0.70713	0.33705
86	7.00000	759.28949	928.98425	681.53668	0.62788	0.29928
87	7.50000	779.90509	921.83938	653.37177	0.56400	0.26883
88	8.00000	795.73828	930.81042	624.97137	0.50595	0.24116
89	8.50000	814.51727	940.25220	602.08978	0.45982	0.21917
90	9.00000	810.29181	940.43018	565.69037	0.40841	0.19467
91	9.50000	783.27441	928.44312	518.04822	0.35348	0.16849
92	10.00000	749.73328	912.74841	471.07132	0.30387	0.14484
93	11.00000	729.46967	862.13922	416.67209	0.24522	0.11688
94	12.00000	746.74719	800.45667	390.99594	0.21845	0.10412
95	13.00000	767.18494	743.50354	370.79730	0.19234	0.09168
96	14.00000	772.91510	696.84296	346.88348	0.16812	0.08013
97	15.00000	772.11700	660.23718	323.42361	0.14728	0.07020

Attachment G

DEFORMP

Input and Output Excerpts

(see Table 8-6 for listing of files)

TRICSP.INP

TRICSP.DAT	5,12000,0.005,5,0.6,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.005,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.65,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.01,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.7,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.015,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.75,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.02,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.8,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.03,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.85,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.04,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.9,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.05,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.95,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.06,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.0,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.07,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.1,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.08,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.2,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.09,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.3,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.10,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.4,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.11,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.5,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.12,1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.6,1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.13,1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.14,1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.15,1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.2,1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.3,1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.4,1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.5,1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.55,1.0	
(8F10.6)	
TR1C00.QSC	

TR1CSP.DAT

TR1CSP.DAT

Summary of Permanent deformation from Newmark's method

Slip A. (g)	Slip/Amx	Slip D. (ft)	Amx	Scaling F.	file
0.00500	0.00279	0.6200E+03	1.79147	1.00000	TR1C00.QSC
0.01000	0.00558	0.5098E+03	1.79147	1.00000	TR1C00.QSC
0.01500	0.00837	0.4005E+03	1.79147	1.00000	TR1C00.QSC
0.02000	0.01116	0.3075E+03	1.79147	1.00000	TR1C00.QSC
0.03000	0.01675	0.2189E+03	1.79147	1.00000	TR1C00.QSC
0.04000	0.02233	0.1751E+03	1.79147	1.00000	TR1C00.QSC
0.05000	0.02791	0.1473E+03	1.79147	1.00000	TR1C00.QSC
0.06000	0.03349	0.1319E+03	1.79147	1.00000	TR1C00.QSC
0.07000	0.03907	0.1186E+03	1.79147	1.00000	TR1C00.QSC
0.08000	0.04466	0.1068E+03	1.79147	1.00000	TR1C00.QSC
0.09000	0.05024	0.9580E+02	1.79147	1.00000	TR1C00.QSC
0.10000	0.05582	0.8750E+02	1.79147	1.00000	TR1C00.QSC
0.11000	0.06140	0.8165E+02	1.79147	1.00000	TR1C00.QSC
0.12000	0.06698	0.7696E+02	1.79147	1.00000	TR1C00.QSC
0.13000	0.07257	0.7279E+02	1.79147	1.00000	TR1C00.QSC
0.14000	0.07815	0.6895E+02	1.79147	1.00000	TR1C00.QSC
0.15000	0.08373	0.6530E+02	1.79147	1.00000	TR1C00.QSC
0.20000	0.11164	0.5036E+02	1.79147	1.00000	TR1C00.QSC
0.30000	0.16746	0.3266E+02	1.79147	1.00000	TR1C00.QSC
0.40000	0.22328	0.2263E+02	1.79147	1.00000	TR1C00.QSC
0.50000	0.27910	0.1525E+02	1.79147	1.00000	TR1C00.QSC
0.55000	0.30701	0.1244E+02	1.79147	1.00000	TR1C00.QSC
0.60000	0.33492	0.1006E+02	1.79147	1.00000	TR1C00.QSC
0.65000	0.36283	0.8081E+01	1.79147	1.00000	TR1C00.QSC
0.70000	0.39074	0.6351E+01	1.79147	1.00000	TR1C00.QSC
0.75000	0.41865	0.4835E+01	1.79147	1.00000	TR1C00.QSC
0.80000	0.44656	0.3525E+01	1.79147	1.00000	TR1C00.QSC
0.85000	0.47447	0.2460E+01	1.79147	1.00000	TR1C00.QSC
0.90000	0.50238	0.1637E+01	1.79147	1.00000	TR1C00.QSC
0.95000	0.53029	0.1148E+01	1.79147	1.00000	TR1C00.QSC
1.00000	0.55820	0.9161E+00	1.79147	1.00000	TR1C00.QSC
1.10000	0.61402	0.5999E+00	1.79147	1.00000	TR1C00.QSC
1.20000	0.66984	0.3905E+00	1.79147	1.00000	TR1C00.QSC
1.30000	0.72566	0.2492E+00	1.79147	1.00000	TR1C00.QSC
1.40000	0.78148	0.1507E+00	1.79147	1.00000	TR1C00.QSC
1.50000	0.83730	0.8182E-01	1.79147	1.00000	TR1C00.QSC
1.60000	0.89312	0.3456E-01	1.79147	1.00000	TR1C00.QSC

TR1CSN.INP

TR1CSN.DAT	5,12000,0.005,5,0.6,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.005,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.65,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.01,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.7,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.015,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.75,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.02,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.8,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.03,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.85,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.04,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.9,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.05,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,0.95,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.06,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.0,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.07,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.1,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.08,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.2,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.09,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.3,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.10,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.4,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.11,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.5,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.12,-1.0	TR1C00.QSC
(8F10.6)	5,12000,0.005,5,1.6,-1.0
TR1C00.QSC	(8F10.6)
5,12000,0.005,5,0.13,-1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.14,-1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.15,-1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.2,-1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.3,-1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.4,-1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.5,-1.0	
(8F10.6)	
TR1C00.QSC	
5,12000,0.005,5,0.55,-1.0	
(8F10.6)	
TR1C00.QSC	

TR1CSN.DAT

TR1CSN.DAT

Summary of Permanent deformation from Newmark's method

Slip A. (g)	Slip/Amx	Slip D. (ft)	Amx	Scaling F.	file
0.00500	0.00269	0.3707E+03	1.85918	-1.00000	TR1C00.QSC
0.01000	0.00538	0.2797E+03	1.85918	-1.00000	TR1C00.QSC
0.01500	0.00807	0.2117E+03	1.85918	-1.00000	TR1C00.QSC
0.02000	0.01076	0.1782E+03	1.85918	-1.00000	TR1C00.QSC
0.03000	0.01614	0.1470E+03	1.85918	-1.00000	TR1C00.QSC
0.04000	0.02151	0.1291E+03	1.85918	-1.00000	TR1C00.QSC
0.05000	0.02689	0.1149E+03	1.85918	-1.00000	TR1C00.QSC
0.06000	0.03227	0.1020E+03	1.85918	-1.00000	TR1C00.QSC
0.07000	0.03765	0.9181E+02	1.85918	-1.00000	TR1C00.QSC
0.08000	0.04303	0.8407E+02	1.85918	-1.00000	TR1C00.QSC
0.09000	0.04841	0.7690E+02	1.85918	-1.00000	TR1C00.QSC
0.10000	0.05379	0.7076E+02	1.85918	-1.00000	TR1C00.QSC
0.11000	0.05917	0.6597E+02	1.85918	-1.00000	TR1C00.QSC
0.12000	0.06454	0.6160E+02	1.85918	-1.00000	TR1C00.QSC
0.13000	0.06992	0.5794E+02	1.85918	-1.00000	TR1C00.QSC
0.14000	0.07530	0.5481E+02	1.85918	-1.00000	TR1C00.QSC
0.15000	0.08068	0.5182E+02	1.85918	-1.00000	TR1C00.QSC
0.20000	0.10757	0.4080E+02	1.85918	-1.00000	TR1C00.QSC
0.30000	0.16136	0.2609E+02	1.85918	-1.00000	TR1C00.QSC
0.40000	0.21515	0.1802E+02	1.85918	-1.00000	TR1C00.QSC
0.50000	0.26894	0.1258E+02	1.85918	-1.00000	TR1C00.QSC
0.55000	0.29583	0.1083E+02	1.85918	-1.00000	TR1C00.QSC
0.60000	0.32272	0.9380E+01	1.85918	-1.00000	TR1C00.QSC
0.65000	0.34962	0.8137E+01	1.85918	-1.00000	TR1C00.QSC
0.70000	0.37651	0.7061E+01	1.85918	-1.00000	TR1C00.QSC
0.75000	0.40340	0.6123E+01	1.85918	-1.00000	TR1C00.QSC
0.80000	0.43030	0.5294E+01	1.85918	-1.00000	TR1C00.QSC
0.85000	0.45719	0.4560E+01	1.85918	-1.00000	TR1C00.QSC
0.90000	0.48409	0.3927E+01	1.85918	-1.00000	TR1C00.QSC
0.95000	0.51098	0.3378E+01	1.85918	-1.00000	TR1C00.QSC
1.00000	0.53787	0.2896E+01	1.85918	-1.00000	TR1C00.QSC
1.10000	0.59166	0.2103E+01	1.85918	-1.00000	TR1C00.QSC
1.20000	0.64545	0.1476E+01	1.85918	-1.00000	TR1C00.QSC
1.30000	0.69923	0.9697E+00	1.85918	-1.00000	TR1C00.QSC
1.40000	0.75302	0.5675E+00	1.85918	-1.00000	TR1C00.QSC
1.50000	0.80681	0.2660E+00	1.85918	-1.00000	TR1C00.QSC
1.60000	0.86060	0.1091E+00	1.85918	-1.00000	TR1C00.QSC

TR3CSP.INP

TR3CSP.DAT	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,0.6,1.0
5,12000,0.005,5,0.005,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,0.65,1.0
5,12000,0.005,5,0.01,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,0.7,1.0
5,12000,0.005,5,0.015,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,0.75,1.0
5,12000,0.005,5,0.02,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,0.8,1.0
5,12000,0.005,5,0.03,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,0.85,1.0
5,12000,0.005,5,0.04,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,0.9,1.0
5,12000,0.005,5,0.05,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,0.95,1.0
5,12000,0.005,5,0.06,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,1.0,1.0
5,12000,0.005,5,0.07,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,1.1,1.0
5,12000,0.005,5,0.08,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,1.2,1.0
5,12000,0.005,5,0.09,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,1.3,1.0
5,12000,0.005,5,0.10,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,1.4,1.0
5,12000,0.005,5,0.11,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,1.5,1.0
5,12000,0.005,5,0.12,1.0	(8F10.6)
(8F10.6)	TR3C00.QSC
TR3C00.QSC	5,12000,0.005,5,1.6,1.0
5,12000,0.005,5,0.13,1.0	(8F10.6)
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.14,1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.15,1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.2,1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.3,1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.4,1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.5,1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.55,1.0	
(8F10.6)	

TR3CSP.DAT

TR3CSP.DAT
Summary of Permanent deformation from Newmark's method

Slip A. (g)	Slip/Amx	Slip D. (ft)	Amx	Scaling F.	file
0.00500	0.00244	0.6056E+03	2.05140	1.00000	TR3C00.QSC
0.01000	0.00487	0.4913E+03	2.05140	1.00000	TR3C00.QSC
0.01500	0.00731	0.3784E+03	2.05140	1.00000	TR3C00.QSC
0.02000	0.00975	0.2989E+03	2.05140	1.00000	TR3C00.QSC
0.03000	0.01462	0.2196E+03	2.05140	1.00000	TR3C00.QSC
0.04000	0.01950	0.1887E+03	2.05140	1.00000	TR3C00.QSC
0.05000	0.02437	0.1635E+03	2.05140	1.00000	TR3C00.QSC
0.06000	0.02925	0.1423E+03	2.05140	1.00000	TR3C00.QSC
0.07000	0.03412	0.1268E+03	2.05140	1.00000	TR3C00.QSC
0.08000	0.03900	0.1177E+03	2.05140	1.00000	TR3C00.QSC
0.09000	0.04387	0.1101E+03	2.05140	1.00000	TR3C00.QSC
0.10000	0.04875	0.1033E+03	2.05140	1.00000	TR3C00.QSC
0.11000	0.05362	0.9717E+02	2.05140	1.00000	TR3C00.QSC
0.12000	0.05850	0.9179E+02	2.05140	1.00000	TR3C00.QSC
0.13000	0.06337	0.8673E+02	2.05140	1.00000	TR3C00.QSC
0.14000	0.06825	0.8196E+02	2.05140	1.00000	TR3C00.QSC
0.15000	0.07312	0.7745E+02	2.05140	1.00000	TR3C00.QSC
0.20000	0.09749	0.6290E+02	2.05140	1.00000	TR3C00.QSC
0.30000	0.14624	0.4371E+02	2.05140	1.00000	TR3C00.QSC
0.40000	0.19499	0.3154E+02	2.05140	1.00000	TR3C00.QSC
0.50000	0.24374	0.2365E+02	2.05140	1.00000	TR3C00.QSC
0.55000	0.26811	0.2052E+02	2.05140	1.00000	TR3C00.QSC
0.60000	0.29248	0.1786E+02	2.05140	1.00000	TR3C00.QSC
0.65000	0.31686	0.1554E+02	2.05140	1.00000	TR3C00.QSC
0.70000	0.34123	0.1349E+02	2.05140	1.00000	TR3C00.QSC
0.75000	0.36560	0.1167E+02	2.05140	1.00000	TR3C00.QSC
0.80000	0.38998	0.1012E+02	2.05140	1.00000	TR3C00.QSC
0.85000	0.41435	0.8744E+01	2.05140	1.00000	TR3C00.QSC
0.90000	0.43873	0.7502E+01	2.05140	1.00000	TR3C00.QSC
0.95000	0.46310	0.6421E+01	2.05140	1.00000	TR3C00.QSC
1.00000	0.48747	0.5503E+01	2.05140	1.00000	TR3C00.QSC
1.10000	0.53622	0.3919E+01	2.05140	1.00000	TR3C00.QSC
1.20000	0.58497	0.2571E+01	2.05140	1.00000	TR3C00.QSC
1.30000	0.63371	0.1428E+01	2.05140	1.00000	TR3C00.QSC
1.40000	0.68246	0.7135E+00	2.05140	1.00000	TR3C00.QSC
1.50000	0.73121	0.4227E+00	2.05140	1.00000	TR3C00.QSC
1.60000	0.77996	0.2453E+00	2.05140	1.00000	TR3C00.QSC

TR3CSN.INP

TR3CSN.DAT	5,12000,0.005,5,0.6,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.005,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,0.65,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.01,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,0.7,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.015,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,0.75,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.02,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,0.8,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.03,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,0.85,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.04,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,0.9,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.05,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,0.95,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.06,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,1.0,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.07,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,1.1,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.08,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,1.2,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.09,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,1.3,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.10,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,1.4,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.11,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,1.5,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.12,-1.0	TR3C00.QSC
(8F10.6)	5,12000,0.005,5,1.6,-1.0
TR3C00.QSC	(8F10.6)
5,12000,0.005,5,0.13,-1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.14,-1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.15,-1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.2,-1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.3,-1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.4,-1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.5,-1.0	
(8F10.6)	
TR3C00.QSC	
5,12000,0.005,5,0.55,-1.0	
(8F10.6)	
TR3C00.QSC	

TR3CSN.DAT

TR3CSN.DAT
Summary of Permanent deformation from Newmark's method

Slip A. (g)	Slip/A _{mx}	Slip D. (ft)	A _{mx}	Scaling F.	file
0.00500	0.00280	0.4412E+03	1.78684	-1.00000	TR3C00.QSC
0.01000	0.00560	0.3272E+03	1.78684	-1.00000	TR3C00.QSC
0.01500	0.00839	0.2510E+03	1.78684	-1.00000	TR3C00.QSC
0.02000	0.01119	0.2221E+03	1.78684	-1.00000	TR3C00.QSC
0.03000	0.01679	0.1806E+03	1.78684	-1.00000	TR3C00.QSC
0.04000	0.02239	0.1531E+03	1.78684	-1.00000	TR3C00.QSC
0.05000	0.02798	0.1332E+03	1.78684	-1.00000	TR3C00.QSC
0.06000	0.03358	0.1182E+03	1.78684	-1.00000	TR3C00.QSC
0.07000	0.03918	0.1068E+03	1.78684	-1.00000	TR3C00.QSC
0.08000	0.04477	0.9628E+02	1.78684	-1.00000	TR3C00.QSC
0.09000	0.05037	0.8719E+02	1.78684	-1.00000	TR3C00.QSC
0.10000	0.05596	0.7874E+02	1.78684	-1.00000	TR3C00.QSC
0.11000	0.06156	0.7172E+02	1.78684	-1.00000	TR3C00.QSC
0.12000	0.06716	0.6577E+02	1.78684	-1.00000	TR3C00.QSC
0.13000	0.07275	0.6155E+02	1.78684	-1.00000	TR3C00.QSC
0.14000	0.07835	0.5773E+02	1.78684	-1.00000	TR3C00.QSC
0.15000	0.08395	0.5431E+02	1.78684	-1.00000	TR3C00.QSC
0.20000	0.11193	0.4094E+02	1.78684	-1.00000	TR3C00.QSC
0.30000	0.16789	0.2282E+02	1.78684	-1.00000	TR3C00.QSC
0.40000	0.22386	0.1422E+02	1.78684	-1.00000	TR3C00.QSC
0.50000	0.27982	0.9188E+01	1.78684	-1.00000	TR3C00.QSC
0.55000	0.30781	0.7570E+01	1.78684	-1.00000	TR3C00.QSC
0.60000	0.33579	0.6290E+01	1.78684	-1.00000	TR3C00.QSC
0.65000	0.36377	0.5227E+01	1.78684	-1.00000	TR3C00.QSC
0.70000	0.39175	0.4352E+01	1.78684	-1.00000	TR3C00.QSC
0.75000	0.41974	0.3624E+01	1.78684	-1.00000	TR3C00.QSC
0.80000	0.44772	0.3011E+01	1.78684	-1.00000	TR3C00.QSC
0.85000	0.47570	0.2494E+01	1.78684	-1.00000	TR3C00.QSC
0.90000	0.50368	0.2059E+01	1.78684	-1.00000	TR3C00.QSC
0.95000	0.53167	0.1691E+01	1.78684	-1.00000	TR3C00.QSC
1.00000	0.55965	0.1384E+01	1.78684	-1.00000	TR3C00.QSC
1.10000	0.61561	0.9073E+00	1.78684	-1.00000	TR3C00.QSC
1.20000	0.67158	0.5545E+00	1.78684	-1.00000	TR3C00.QSC
1.30000	0.72754	0.3005E+00	1.78684	-1.00000	TR3C00.QSC
1.40000	0.78351	0.1529E+00	1.78684	-1.00000	TR3C00.QSC
1.50000	0.83947	0.6954E-01	1.78684	-1.00000	TR3C00.QSC
1.60000	0.89544	0.2191E-01	1.78684	-1.00000	TR3C00.QSC

Attachment H
CD-Rom
Table of Contents

Table of Contents.txt file
GEO.HBIP.02.08 Rev. 1 07/18/03

All files listed are ASCII files that can be read by any text file such as Notepad.

Directory UTEXAS4_files:

Section C-C'
transport3.txt
transport3.out
transport3(dyn).txt
transport3(dyn).out

*.txt files are input files. *.out are output files. (dyn) files are used to determine (dynamic) yield acceleration for each section.

Directory EXCEL_files:

For use in DEFORMP analyses:

Section C-C'
Set 1 set1rot.xls s1cc.prn
Set 2 set2rot.xls s2cc.prn
Set 3 set3rot.xls s3cc.prn
Set 4 set4rot.xls s4cc.prn

*.xls files are spreadsheet files. *.prn files are rotated motions output from the spreadsheets.

For use in SHAKE analyses:

Section C-C'

SET 1

SET1_FP.ACC
SET1_FN_FLING_BC.ACC
SET1ROT.XLS
S1CC.AC8

SET 3

SET3_FP.ACC
SET3_FN_FLING_BC.ACC
SET3ROT.XLS
S3CC.AC8

*.ACC files are input components of ground motion from time history calculations. *.AC8 files are rotated surface motions used in SHAKE analyses.

Directory SHAKE_files:

Section C-C'

SET 1

TR1C.INP
S1CC.AC8
TR1CI.INP
TR1C.OUT
TR1C.PUN
TR1CI.OUT
TR1CI.PUN

SET 3

TR3C.INP
S3CC.AC8
TR3CI.INP
TR3C.OUT
TR3C.PUN
TR3CI.OUT
TR3CI.PUN

*.IN files are input files. *.OUT files are output files. *.PUN files are rotated outcrop motion files for use in QUAD4MU analyses.

Directory QUAD4MU files:

Section C-C'

SET 1

TR1C.Q4I
TR1CI.O25
HBSOILNW.DAT
TR1C.Q4O
TR1C00.QSC
TR1C00.Q4A
TR1C01.Q4A
TR1C02.Q4A
TR1C03.Q4A
TR1C04.Q4A
TR1C05.Q4A
TR1C06.Q4A

SET 3

TR3C.Q4I
TR3CI.O25
HBSOILNW.DAT
TR3C.Q4O
TR3C00.QSC
TR3C00.Q4A
TR3C01.Q4A
TR3C02.Q4A
TR3C03.Q4A
TR3C04.Q4A
TR3C05.Q4A
TR3C06.Q4A

*.011 files are rotated outcrop motions from SHAKE analyses.
HBSOILNW.DAT is input dynamic soil properties file. *.Q40 files are
output files. *.QSC files are seismic coefficient files. *.Q4A files
are nodal response time history files.

Directory SPECTRAD_files:

Section C-C'

SET 1

SPECTRA1.INP
SPECTRA2.INP
SPECTRA3.INP
S1CC.050
TR1C00A.050
TR1C01A.050

SET 3

SPECTRA1.INP
SPECTRA2.INP
SPECTRA3.INP
S3CC.050
TR3C00A.050
TR3C01A.050

S*.050 files are spectra of rotated surface motion. PD*.050 files are
spectra of nodes.

Directory DEFORMP_files:

From QUAD4MU output:

Section C-C'

SET 1

TR1CSP.INP
TR1CSN.INP
TR1CSP.DAT
TR1CSN.DAT

SET 3

TR3CSP.INP
TR3CSN.INP
TR3CSP.DAT
TR3CSN.DAT

*.QSC files are seismic coefficient input files from QUAD4MU output.
*.DAT files are output displacement files.

Directly from EXCEL output:

SECTION C-C'

(* .inp)
s1cp
s1cn
s2cp
s2cn
s3cp
s3cn
s4cp
s4cn

*.inp files are input files from EXCEL.

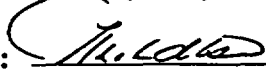
(* .dat files)
s1cp
s1cn
s2cp
s2cn
s3cp
s3cn
s4cp
s4cn

*.dat files are output displacement files.

**PACIFIC GAS AND ELECTRIC COMPANY
GEOSCIENCES DEPARTMENT
CALCULATION DOCUMENT**

**Calc Number: GEO.HBIP.02.08
Calc Revision: 1
Calc Date: 7/18/03
Calc Preparer: Z. -L. Wang/
C. C. chin
ITR Verification Method: A**

ITR Faiz I. Makdisi
(name)

ITR:  7/18/03
(signature/date)

ITR: _____
(name)

ITR: _____
(signature/date)

1. INTRODUCTION

As required by Geosciences Department Level Administrative Procedure CF3-GE1, Revision A for Quality Related Calculations, I have performed an independent technical review of Revision 1 of the above listed calculation. I have performed a step-by-step check of the calculation (Verification Method A). This ITR report is structured with similar section headings as those in the calculation. All issues raised with the preparers of this calculation have been addressed and resolved.

2. CALCULATION PURPOSE

The purpose of the calculation in this Revision 1 is to repeat the dynamic response analyses performed in Revision 0, using an updated version (QUAD4MU) of the dynamic finite element program QUAD4M, and to update the estimated earthquake-induced deformations. I have verified that the purpose for performing the additional analyses is clearly stated.

3. CALCULATION ASSUMPTIONS

Except for minor editorial changes, no other changes were made to this section.

4. CALCULATION INPUTS

No changes have been made to this section from the previous revision.

5. CALCULATION METHODOLOGY AND EQUATION SUMMARY

Except for minor editorial changes, no other changes were made to the methodology as described in this section in Revision 0. I have verified that the reference made to the original program QUAD4M, was changed to the updated (modified) version, QUAD4MU.

6. CALCULATION SOFTWARE

The reference to the program QUAD4M has been changed to QUAD4MU (the updated version of the program). I have checked and verified that the updated program QUAD4MU has been documented and verified in Calculation GEO.DCPP.01.34. No other changes were made to this section in this revision.

7. CALCULATION BODY

Except for minor edits, no changes were made to Steps 1 through 6 of this section. In step 7, reference to the program QUAD4M has been changed to QUAD4MU.

Step 8 describes the repeat of the dynamic finite element analyses to compute the seismic coefficient time-histories for potential sliding masses along the transport route to the ISFSI site.

I have checked and verified the input files for the QUAD4MU analyses. I have verified that the output outcrop time histories from the SHAKE runs were correctly used as input at the base of the finite element model in QUAD4MU. I verified that the seismic coefficient time history outputs from QUAD4MU were correctly plotted by comparing the peak values from the output files with the plots shown on Figures 8-5 and 8-6.

I have verified that the seismic coefficient time histories from the output of QUAD4MU were correctly used as input to the DEFORMP displacement program. I have compared and verified that the peak values of the seismic coefficient time histories printed in the output files of QUAD4MU, are the same as those presented on the displacement plots in Figures 8-9 and 8-10.

8. CALCULATION RESULTS AND CONCLUSIONS

I have reviewed the results in this revision of the calculation and found them reasonable and consistent with the stated purpose and conclusions. The range of revised maximum earthquake-induced displacement for the potential sliding mass (along the critical section if the transporter route) of 9.0 ft is consistent with and slightly lower than the 10.5 ft computed in Revision 0 of this calculation.

9. CALCULATION LIMITATIONS

I have reviewed and verified that the stated limitations are appropriate.

10. CALCULATION IMPACT EVALUATION

I concur with the stated impact of the results of the calculation.

11. CALCULATION REFERENCES

Except for the updated reference to the QUAD4MU program, no changes were made to this section in this revision.

12. CALCULATION ATTACHMENTS

Attachments A, B, C and D remain unchanged from Revision 0. I have verified that the listed files and the printed excerpts of the input and output files in Attachments E, F and G, are accurate and sufficient to reproduce the analyses and calculations included in the CD. In addition, I have checked and verified that copies of the CD's are readable and each contains a "Read Me" file that describes its contents.