



WIRELESS

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BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELECTRONICS CONSTRUCTOR

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We regret that we are unable to supply back numbers of Practical Wireless. Readers are recommended to enquire at a public library to see copies. Requests for specific back numbers of *Practical Wireless* and *Television* only can be published in our CQ Column.

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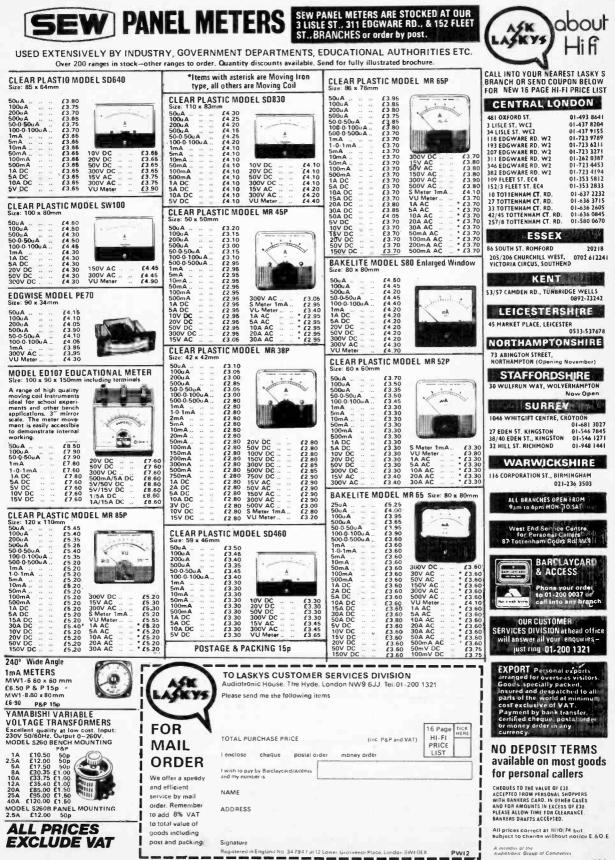
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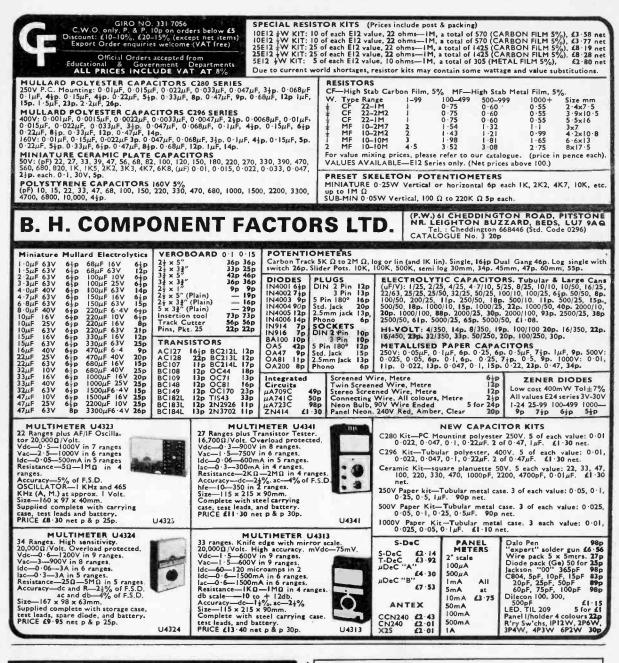














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with Unisound — pre-amp, power amplifier and control panel. No soldering –

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power chips which ensure very low distortion over the audio spectrum.

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- (1) Output 4 watts R.M.S. output. For 12 volt operation on negative or positive earth.
- (2) Integrated circuit output stage, pre-built three stage IF Module.

NO SOLDERING

REQUIRED!

Controls volume manual tuning and five push buttons for station selection, illuminated tuning scale covering full, medium and long wave bands. Size chassis 7" wide, 2" high and 4%" deep approx

Speaker including baffle and fixing strip £1.65+23p.p&p. Car Aerial Recommended — fully retractable and locking £1.37+20p. postage & packing



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Stereo 21, easy to assemble audio system kit. No soldering required. The unit is finished in white P.V.C. and the acrylic top presents an unusually interesting variation on the modern deck plinth. Includes :- BSR 3 speed deck. automatic, manual facilities together with ceramic cartridge. Two speakers with cabinets.

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Complete only £19.95 + £1.60 p & p. Extras if required. Optional Diamond Styli £1.37. Specially selected pair of stereo headphones with individual level controls and padded earpieces to give optimum performance, £3.85.



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£11.95 + 90p p & p.

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System 1. £.51.00

40 Watt Amplifier. Viscount III - R102 now 20 watts per channel. System Lincludes:

Viscount III amplifier - volume, bass, treble and balance controls, plus switches for mono? stereo on/off function and bass and treble filters. Plus headphone socket. Specification

20 watts per channel into 8 ohms. Total distortion @ 10W @ 1kHz 0-1%. P.U.1 (for ceramic cartridges) 150mV into 3 Meg. P.U.2 (for magnetic cartridges) 4mV @ 1kHz into 47K. equalised within ± 1 dB R.I.A.A. *Radio* 150mV into 220K. (Sensitivities given at full power). Tape out facilities : headphone socket, power out 250mW per channel. Tone controls and filter characteristics. Bass: +12dB to -17dB @ 60Hz. Bass filter: 6dB per octave cut. Treble control: treble +12dB to -12dB @ 15kHz. Treble filter : 12dB per octave. Signal to noise ratio (all controls at max.) - 58dB. Crosstalk better than 35dB on all inputs. Overload characteristics better than 26dB on all inputs. Size approx. 13 3"×9"×3 3"

Garrard SP 25 Mk III deck with magnetic cartridge, de luxe plinth and hinged cover. Two Duo Type II matched speakers - Enclosure size approx. $17\frac{1}{2}$ × $10\frac{3}{4}$ × 6in simulated teak. Drive unit $13^{\prime\prime} \times 8^{\prime\prime}$ with parasitic tweater. 10 watts handling.

Complete System £51.00

stem 2. £69.00

Viscount III amplifier (As System I

Garrard SP 25 Mk III deck (As System I)

Two Duo Type III matched speakers - Enclosure size approx. 27" x 13" x 112" Finished in teak veneer. Drive units 13" x 8" bass driver, and two 3" (approx.) tweeters. 20 watts R.M.S., 8 ohms frequency range - 20 Hz to 18,000 Hz.

Complete System £69.00.

PRICES : SYSTEM 1

Available complete for only:

Viscount III B102 Viscount III R102 amplifier £24.20 + £1 p & p amplifier 2 Duo Type II speakers $f14.00 + f2.20 p \delta p$ 2 Duo Type III speakers £39.00 + £4.00 p & p Garrard SP 25 with Garrard SP 25 with Mag. cartridge Mag. cartridge de luxe plinth and hinged cover £21.00 + £1.75 p & p total: £59.20

£51.00

+ £3.50 p & p

de luxe plinth and hinged cover

total - £84 20

£24.20 + £1 p & p

£21.00 + £1.75 p & p

Available complete for only : £69.00 + £4.00 p & p

PRICES: SYSTEM 2

EMI SPEAKERS AT FANTASTIC REDUCTIONS

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Flux density-33K, speech coil-1" with parasitic tweeter. Power Handling 20 watts R.M.S., impedance - 8 ohms, frequency response - 20 Hz to 18.000 Hz.

OUR PRICE £6.60. Complete +90pp&p.



15" 14A/780 BASS UNIT Bass unit on a rigid diecast chassis. Superior cone material handles up to 50 watts RMS, and is treated to give a smooth frequency response. Resonance 30 Hz. flux density 360,000 Maxwells. Impedance at 1 kHz is 8 ohms. 3" voice coil.

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950

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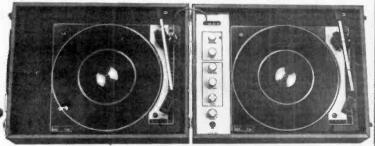
PORTABLE DISCO CONSOLE

INCORPORATES : Pre-Amp with full mixing facilities, including switched input for mic with volume control, switched input for auxiliary with volume control, bass and treble controls, volume control and blend control for turntables.

Two B.S.R. single play professional series decks, fitted with crystal cartridges.

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The two lightweight cartridge shells have slide-in-holders to facilitate easy inspection of needles and cartridges.



TECHNICAL SPECIFICATION:

Pre-amp - Output - 200mV. Auxiliary inputs - 200mV and 750mV into 1 meg. Mic input - 6mV into 100K. 240 volt operation. Turntables capacity - 7", 10" or 12" records.

Rumble, wow and flutter - Rumble - Better than -35dB. Wow - Better than 0.2%. Flutter - Better than 0.06% (Gaumont kalee meter). Finish - Satin black mainplate with black turntable mat inlaid with brushed aluminium trim. Tonearm and controls in black and brushed aluminium

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Ideal for Disco Work. Output Power: 45 watts R.M.S. Frequency Response 3dB points 30Hz and 18KHz. Total Distortion : less than 2% at rated output. Signal to noise ratio: better than 60dB. Bass Control Range: 13dB at 60Hz. Treble Control Range: 12dB at 10KHz. Inputs : 4 inputs at 5mV into 470K. Each pair of inputs controlled by separate volume control. 2 inputs at 200mV into 470K. Size: $19\frac{1}{4}^{"} \times 10\frac{1}{2}^{"} \times 8^{"}$ (approx.) Amplifier £27.50+£1.50 p. & p.

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150 100 5 8 9·9 x 8·9 x 8·6 4·17 45
152 250 13 12 12 1 × 11 8 × 10 2 9 45 73 153 350 15 0 14 0 × 10 8 × 11 8 11 35 73
154 500 19 8 14-0 x 13 4 x 11 8 13 30 9 155 750 29 0 17 2 x 14 0 x 14 0 21 05 * 156 1000 38 0 17 2 x 16 6 x 14 0 27 20 *
158 2000 60 0 21 6 x 15 3 x 18 1 50 25 + AUTO TRANSFORMERS
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66 300 6 4 9 9 X 9 6 X 8 6 5 2 3 3
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TRANSFORMERS
PRIMARY 240:250 VOLTS 12 AND OR 24 VOLT RANGE Ref. Amps. Weight Size cm. Secondary Windings P & P No. 129 244 Ib oz a construction 250 April 24 2
713 1-0 0-5 1 4 6-1 x 5-8 x 4-8 0-12V at 0-25A x 2 1-54 20
71 2 1 1 12 7 0 x 6 4 x 6 1 0 12 V at 1A x 2 2 09 38
70 6 3 3 8 8.9 x 8.0 x 7.7 0 12V at 3A x 2 3 52 45 108 8 4 5 8 9.9 x 8.9 x 8.6 0 12V at 4A x 2 3 96 45 70 10 5 6 4 9.9 y 8.6 0 12V at 5A x 2 4 67 53
$\begin{array}{cccccccccccccccccccccccccccccccccccc$
187 30 15 15 B 140 x 12 1 x 11 8 0 12V at 15A x 2 13 70 85
226 60 30 32 0 17-2 x 15-3 x 14-0 0-12V at 30A x 2 22-50 30 V OLT RANGE
No. 16 oz (1 × 5.8 × 4.8 0-12-15-20-24-30) 1.58 30
79 1.0 2 4 7.0 x 6.7 x 6.1 2.18 38 3 2.0 3 4 8.9 x 7.7 x 7.7 3.18 38
20 3·0 4 8 9·9 x 8·3 x 8·6
117 6.0 8 0 12.1 x 9.3 x 10.2 6.94 60 88 8.0 12 0 12.1 x 11.8 x 10.2 9.00 67
89 10-0 13 12 14-0 × 10-2 × 11-8
Ref. Amps. Weight Size cm. Secondary Taps P & P P P P No. Ib oz Do Do <thdo< th=""> Do <thdo< th=""> <thdo< th=""> Do</thdo<></thdo<></thdo<>
103 1.0 2 12 8.3 x 7.4 x 7.0 3.08 38
105 3·0 6 12 9·9 × 10·2 × 8·6 5·79 33 106 4·0 10 0 12·1 × 10·5 × 10·2 7·41 67 7·41 67
60 VOLT RANGE Ref. Amps. Weight Size cm. Secondary Taps P & P
No. 1b oz $124 0.5 2.4 7.0 \times 6.7 \times 6.1 0.24.30-40.48-60 2.12 38$ 124 0.5 2.4 8.9 \times 7.7 \times 7.7 2.97 38
127 2.0 6 4 9.9 x 9.6 x 8.6 3 40 43 125 3.0 8 12 12 1 x 9.9 x 10.2 5 7.11 60
$123 4.0 13 12 12.1 \times 11.8 \times 10.2$ 920 07 40 5.0 12 00 14.0 $\times 10.2 \times 11.8$ 10.83 73
121 8.0 25 00 14.0 x 14.7 x 11.8
189 12-0 29 00 17-2 × 14-0 × 14-0
Ref. MA. Weight Size cm VOLTS £ p 238 200 2 2 8x2 6x2 0 3-0-3 1.40 10
13 100 4 3 9x2 6x2 9 9-0-9 1 28 13
207 500, 500 00 6 x5 4x4 8 0-8-9, 0-8-9 2 23 30 709 14 14 12 7 0x6 4x6 0-8-9, 0-8-9 3 00 38
208 14, 14, 14 14 10, 24, 29, 23 5 0, 15, 0, 15 1, 30, 19 236 200, 200 4 6, 12, 29, 23 5 0, 15, 0, 15 1, 30, 19 214 300, 300 1 4 6, 12, 58, 44 8 0, 20, 0, 20 1, 76 30 221 700 (D.C.) 1 8 7, 0, 64, 12, 61 2, 20 1, 29 38 27 1, 700 (D.C.) 1 8 7, 0, 64, 12, 61 2, 20 1, 29 38
206 IA IA 2 I2 8 3x7 7x7 0 0-15-20 0-15-20 3 78 38 203 500 500 2 4 8 3x7 0x7 0 0-15-27 0-15-27 3 06 38
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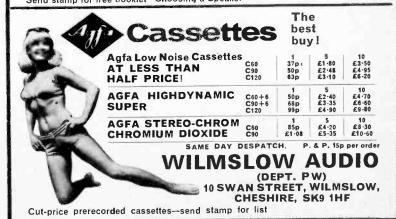
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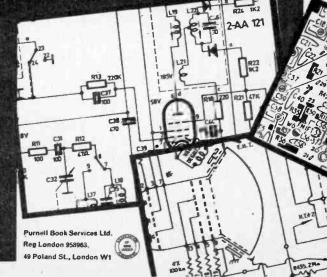
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BA7 7" × 5" × 24" 70p BA8 8" × 6" × 3" 90p	C18 4 Rotary Wave Change Switches 0.55 C19 2 Relays 6-24V Operating 0.55	VC 3 Tandem Less Switch 0.46	R3 50 Mixed 10K ohms-82K ohms 50
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VISIT OUR COM	and the second s	HORIZONTAL CARBON	JUST 19 EACH INCL. V.A.T.
18 BALDOCK ST., W.		PRESETS 0·1 watt 0·06 each	BI-PAK SUPERIOR QUALITY
Open MonSat. 9-5.3		100, 220, 470, 1K, 22K, 47K, 10K, 22K, 4K7, 10K, 22K, 4K7, 100K, 220K, 470K, 1M, 2M, 47M	LOW - NOISE CASSETTES C60, 36p C90, 48p C120, 60p

-the lowest prices!

BI-PAK QUALITY COMES TO AUDIO!

AL10/AL20/AL30 AUDIO AMPLIFIER MODULES

The AL10, AL20 and AL30 units are similar in their appearance and in their general specification. However, careful selection of the plastic power devices has remitted in a range of output powers from 3 to 10 watts R.M.S. The yearstilling of their dasign makes them

The versatility of their design makes them ideal for use in record players, tape recorders, stereo amplifiers and cassetts and cartridge tape players in the car and at home.

Parameter	Conditions	Performance
HARMONIC DISTORTION	Po = 3 WATTS f=1KHz	0.25%
LOAD IMPEDANCE	-	8 - 16 Ω
INPUT IMPEDANCE	f=1KHz	100 k Ω
FREQUENCY RESPONSE ± 3dB	Po=2 WATTS	50 Hz - 25 KH
SENSITIVITY for RATED O/P	V ₈ =25V. Rl=8Ω f=1KHz	75mV. RMS
DIMENSIONS		3" × 21" × 1"

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

In their working construction				
Parameter	AL10	AL20	AL80	
Maximum Supply Voltage	25	30	30	
Power output for 2% T.H.D. (RL = $8\Omega t = 1 \text{ KHz}$)	3 watts RMS Min.	5 watts RMS Min.	10 watts RMS Min.	

JUDIO AMPL NODULES

OWER SUPPLIES	TRANSFORMERS
AUDIO AMPLIFIER ADDULES L 10. 3 watts RMS £2.10 L 20. 6 watts RMS £2.59 L 30. 10 watts RMS £3.01	PRE-AMPLIFIERS PA 12. (Use with AL10 & AL20) \$4:35 PA 100. (Use with AL30 & AL60) \$13:15

± 12dB at 60Hz

Treble control---± 14dB at 14KHz *Input 1. Impedance 1 Meg. ohm Sensitivity 300mV †Input 2. Impedance 30 K ohms Sensitivity 4 mV

Sensitivity 4mV

Treble control-

 YOWER SUPPLIES
 T461 (Use with AL10, 41.38 P & P 15p

 'B 12. (Use with AL10, AL20, AL30)
 \$23.25

 'RONT PANELS SP 12 with Knobs
 \$21.10

 BM 20. (Use with AL20, AL20, AL30)
 BM 20.25

 'RONT PANELS SP 12 with Knobs
 \$21.10

 BMT80 (Use with AL60) \$22.15 P & P 25p

PA 12. PRE-AMPLIFIER SPECIFICATION

The PA 12 pre-amplifier has been designed to match into loss budget storeo systems. It is compatible with the $20H_{-5}OKH_{2}(-3dB)$ $20H_{-5}OKH_{2}(-3dB)$ L 10, AL 20 and AL 30 audio power amplifiers and it an be supplied from their associated power supplies. here are two stereo inputs, one has been designed for use ith *Ceramic cartridges while the auxiliary input will uit most †Magnetic cartridges. Full details are given in he specification table. The four controls are, from left to ight: Volume and on/off switch, balance, bass and treble. ize 152mm × 84mm × 35mm.

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olume control, balance, bass and treble cont Transformer, Power supply and Power amps. Attractively printed front panel and match-ng control knobs. The 'Stereo 20' has been lesigned to fit into most turntable plinths rithout interfering with the mechanism or ulternatively, into a separate cablnet. Juput power 200 peak. Input 1 (Cer.) 900mV into 1M. Freq. res. 25Hz-25KHz. Input 2 (Auz.) 4mV into 30K. Harmonic fistoriton. Bass control ±12dB at 50Hz typically 0.25% at 1 watt. Treble con. ±14dB at 14kHz. £1

TC20 TEAK VENEERED CABINET

For Stereo 20 (front board undrilled) size 101" x 81" x 3", £3.95, plus 30p postage SHP80 STEREO HEADPHONES

4-16 ohms impedance. Frequency response 20 to 20,000Hz Stereo/mono switch and volume controls £4.95



- Max Heat Sink temp. 90°c. Frequency Response 20Hz to 100KHz
- Distortion better than 0.1% at
- 0.1KHz
- Supply voltage 15-50 volts

Especially designed to a strict specification. Only the finest components have been used and the latest solid state circuitry incorporated in this powerful little amplifier which should satisfy the most critical A.F enthusiast.

.

STABILISED POWER MODULE SPM80 BPM80 is expecially designed to power 2 of the AL60 Amplifiers, up to 15 wait (r.m.s.) per channel simul-taneously. This module embodies the latest components and circuit, techniques incorporating complete short circuit protection. With the addition of the Mains Tran-former BMT80, the unit will provide outputs of up to 1-6 amps at 35 volts. Bize: 65mm × 100mm × 30mm. These units enable you to build Audio Bystems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including:—Disco Bystems, Public Address Intercom Units, etc. Handbook available 10p PRICE £3.25

13mm

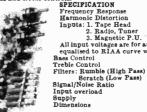
Thermal Feedback

Latest Design Improvements Load---3, 4, 8 or 16 ohms

Signal to noise ratio 80dB Overall size 63mm × 105mm ×

TRANSFORMER BMT80 £2.15 p. & p. 28p

STEREO PRE-AMPLIFIER TYPE PA100



 Frequency according

 Harmonic Distortion

 Inputs: 1. Tape Head

 2. Radio, Tuner

 75 mV into 50K Ω

 3. Magnetic P.U.

 3. Magnetic P.U.

 3. Magnetic P.U.

 auli Input voitages are for an output of 250mV. Tape and P.U. inputs

 equalised to RIAA curve within ± 14B. from 20Hz to 20KHz.

 Base Control

 Treble Control

 4. 16MB at 20 KHz

 SKHz
 better tan... + 26dB + 36 volts at 20mA 292mm × 82mm × 85mm ONLY £13.15 -:=0's. 1

SPECIAL COMPLETE KIT COMPRISING 2 AL50's, 1 SPM80, 1 BMT80 & 1 PA100 ONLY £25.30 FREE p. & p.

MK 60 AUDIO KIT

Comprising: 2 x AL60, 1 x SPM80, 1 x BTM80, 1 x PA 100, 1 front panel, 1 kit of parts to include on off switch, neon indicator, stereo head phone sockets plus instruction booklets. Compiles Files: 228-75 plus 300 postage

TEAK 60 AUDIO KIT

Comprising: Teak veneered cabinet size 10% x 11% x 3%, other parts include aluminium Chassis, heatisth and front panel bracket, plus back panel and appropriate sockets etc. Kit price: 29.95 plus 30p postage





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NEW	MULLA	RD & N	AZDA	VALV	ES		TR
and g trade c fide c	guarante liscounts ompanie	y boxed ed. Ful stobona s. Price /listsor	EXP POS 6p for 1 Each ad			PC 5p 10	PR ST of first ach add
applica DM70 06 DY802 05 DY807 05 DY807 05 DY802 10 EBF80 05 EBF80 05 EBF80 05 EBF80 05 EBF80 05 EC88 07 EC88 07 EC88 07 EC88 07 EC80 07 EC8	ation. 1 ECL83 0.6 0 ECL86 0.6 1 EF80 0.4 0 ECL86 0.6 0 ECL86 0.4 0 ECL86 0.4 0 EF83 0.6 0 EL84 0.6 0 EL84 0.6 0 EL84 0.6 0 EL84 0.6 0 EL85 0.7 0 EL84 0.6 0 EM84 1.1 0 EV861 0.7 0 EM84 1.1 0 EV861	$ \begin{array}{c} GY501 & 1 \\ GZ24 & 0 \\ F \\ C8 & PC88 & 0 \\ 9 \\ PC87 & 0 \\ 4 \\ PC080 & 0 \\ 8 \\ PC090 & 0 \\ 8 \\ PC080 & 0 \\ 1 \\ 1 \\ PC080 & 0 \\ 0 \\ 0 \\ PC180 & 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $	S PL82 0.4 7 PL83 1.0 5 PL60 9.1 6 PL504 0.8 5 PL604 0.8 7 PL80 0.1 8 PX30 0.6 9 PL302 1.3 9 PX30 0.6 9 PY38 0.5 9 PY300 0.4 9 PY38 0.5 9 PY380 0.4 9 PY38 0.5 0 U130 0.5 0 U132 0.5 0 U132 0.5 0 U132 0.7 0 U132 0.7	9 9 7 30C15/ 9 PCF800 9 9 9 9 9 9 9 9 9 9 9 9 9	0.54 1.01 1.01 1.00 318 1.03 0.80 0.80 1.13 0.94 384 0.54	AA119 AA213 AA216 AC107 AC126 AC127 AC128 AC176 AC187 AC187 AC187 AC187 AD140 AD140 AD140 AD140 AD141 AD161 AF116 AF116 AF116 AF116 AF116 AF126 AF126 AF126 BC107 BC117 BC113 BC117 BC143	0.7 0.10 0.35 0.25 0.20 0.20 0.20 0.22 0.650 0.20 0.22 0.650 0.22 0.650 0.22 0.650 0.22 0.650 0.22 0.22 0.650 0.22 0.22 0.22 0.22 0.22 0.22 0.22 0.
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2' x 12" Cabinet



4' x 12" Cabinet



Disco Console (includes lid not shown) Takes two slaves

For a long time now a large number of customers have asked us to produce cabinets in kit form, and above we show examples of cabinet styles and these are now available either fully built or in kit form ready for you to produce a professional finish in a very short time !

Kits are available in all specifications and all the kits contain everything you need as follows :-

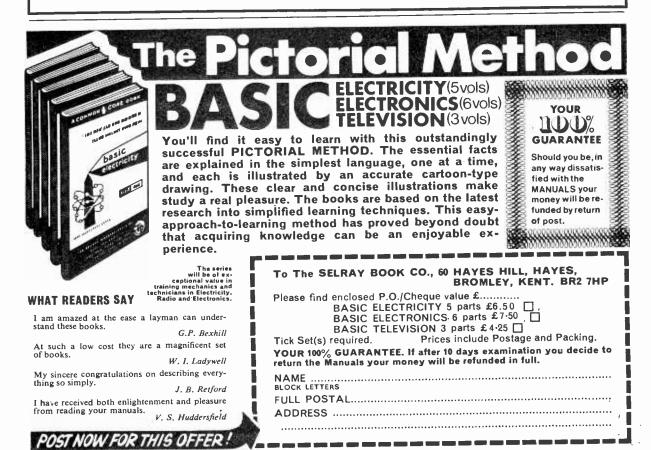
1) 4 sides with handle cutouts, front edges rounded, 1 back with jack socket hole, and 1 baffleboard with speaker cutout

2) P.V.C. cut to size for frame and back, plus false front and back timbers, white front piping and speaker cloth

3) Recessed handles with fixing screws, jack socket, all fixing screws, corner plates, glue, and full instructions !

PRICE & TY	PELIST					
Type	Size	Price manufactured	Kit price			
	36‴ x 18″ x 13″ x ∄	£19.50	£12.50			
2 x 12" (illustrated above) 4 x 12" (illustrated above)	31″x 31″x 13″x ⅔	£24.50	£17.50			
$4 \times 12^{\circ}$ (mustrated above) $4 \times 12^{\circ}$ P.A. Column	48″ x 27″ x 13″ x 3	£30.00	£21.50			
1 x 18"	31" x 31" x 13" x 3	£24.50	£17.50			
1 x 15 1 x 15'' with two top horn cutouts	36″ x 20″ x 13″ x ⅔	£21.00	£13.50			
Mini Disco (state deck cutout BSR, GARRARD etc.)	33" x 20" x 10" x 1	£20.00	£13.00			
Maxi Disco (illustrated) (state deck cutout BSR, GARRARD et		£25.00	£18.50			
Please ask for quotation on any other type or size of cabinet you may require.						

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SCORPIO Mk2 on system kit **RO SPARES** OR 12 VOLT ***+VE AND - VE GROUND**

Here's the new, improved version of the original PE Scorpio Electronic Ignition System-with a big plus over all the other kits-the PE Scorpio Kit is designed for both positive and negative ground automotive electrical systems. Not just + ve ground. Nor just - ve ground. But both! So if you change cars, you can be almost certain that you can change over your PE Scorpio Mk. 2 as well. Containing all the components you need, this Electro Spares PE Scorpio Mk. 2 Kit is simply built, using our easyto-follow instructions. Each component is a branded unit by a reputable manufacturer and carries the manufacturer's guarantee. Ready drilled for fast assembly. Quickly fitted to any car.

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As featured in the May 1973 issue of 'Practical Electronics'. Superb Hi-Fi tuner Kit now available from Electro Spares. Including cabinet and all components - pre-set Mullard modules for R.F. and I.F. circuits. Motorola I.C. Phase Lock Loop Decoder for perfect stereo reception. No alignment needed. Guaranteed first time results - or send it back, and we'll return it in perfect order (for a nominal handling charge). Electro Spares price only £28.50 inc. VAT and p & p.

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- * All components as specified by original authors, and sold separately if you wish.
- ★ Full constructional data book with specification graphs, fault finding guides, etc. 55p plus 4p postage.
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Contains 11b Ferric Chioride, 100 sq. ins. copper-clad board, DALO etch-resist pen, abrasive cleaner, etching dish & instructions, all for only £3.30

RESISTORS & CAPACITORS 500 assorted resistors £1.35, 2500 £4.70, 150 poly. ceramic, mica etc capacitors 80p. 15 different trimmers airspaced and compression, up to 1250pF £1.

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100 sq. Ins. assorted sizes and pitches (no tiny pieces) £1.10. approx 8 bits.

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3W TAPE AMPLIFIERS Polished wooden cabinet 14 x 13 x 9 containing a sensitive (20 μ V) 4 valve amplifier with tone & volume controls, Gives 3 watts output to the 7 x 4" 30, speaker. Also a non-standard tape deck. Supplied In good working condition with circuit. Standard mains operation. £4.50. Suitable cassitie £1.10. Spare head 330. Tape (ex-computer) 75p. Amplifier chassis colly, complete and tested (2xECC83, EL84, EZ80) and speaker £3.

VERSATILE POWER UNIT

Contains mains transformer, 2A thermal cut-out and bridge rec-transition of the state of the state with 2 state of the state of the state \$1.20, also capacitors (supplied) \$1.20, also capacitors (supplied) parage with switch, lamp, lack plug elc. (Used for 'Hot Wheels') \$1.70.

LEO III COMPUTER

Arriving late-October. All parts available, including 3000 reels tape, ½" decks, power units, etc. decks, power units, etc.

Transformer, Mains pri 16-0-16V with 9V tap sec 1/4 £2. Post office 4 digit counters 60p. Balanced arm-ature earpieces, use as mic or spkr 2012 Impedance 30p. 2N3055 38p. Multimeters: good range in stock from £3-50. Ail prices shown include 8% VAT and postage (mainland only) SAE list, enquiries.

FERRIC CHLORIDE

Anhydrous technical quality to Mil Spec in 11b double sealed packs. 11b 80p, 31bs £1.65, 101bs £4.45, 1001bs

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Contained in steel case 51 x 5 x 31" are 2xGET116 transistors on heat sinks, 3 pot cores, 2 30V zeners, 4 audio transformers, 1% resistors &

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Hundreds of new components-Pots, resistors, capacitors, switches, + PC boards with transistors and diodes, and loads of odds and ends. Amazing value at only £2.30.

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MISCELLANEOUS

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As described in Practical Wireless

Play the game that's sweeping the nation. You've seen it in pubs, clubs and arcadesnow you can play it in the comfort of your own home.

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All parts available separately including P. C. boards, case and ready punched and slotted facia panel.

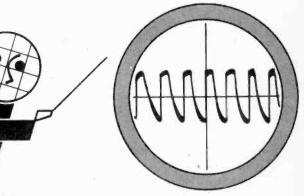
S.A.E. for full details.

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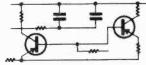
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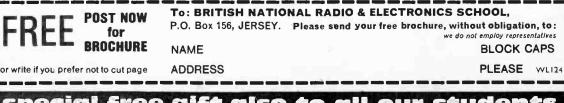


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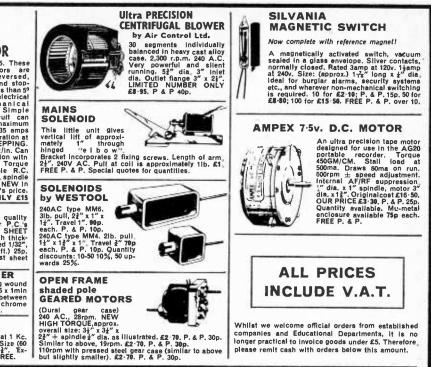
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Fibre-glass copper-clad laminate. Finest quality epoxy resin base. Heat resistant, ideal for P,C's Sizes: 12" x12"; 24" x12"; 24" x24"; FULL SHEET 43" x3" (11 sq 1t). Single-sided Copper with thick-ness of 132", 3164", 332". Also double-sided 1/32", 116", 332". £1 per sq tt. Cut sizes (1-10 sq, ft). 25p. P. & P. Full Sheet £2 each. Carr. £1 for 1st sheet plus 25p each additional sheet.

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Impedance approx. 200Ω , output 60 or 80 DB at 1 Kc. As used In deal aids, bugging devices, etc. Size (60 DB) $7/32'' \times 5/32'' \times \frac{1}{2}''$ (80 DB) $\frac{3}{4}'' \times 5/32'' \times \frac{3}{4}''$. Ex-equipment, all tested. £1:20 each. P. & P. FREE.



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A V.C.O. by FHACHI 1Hz to 100kHz for £5.75 P. & P. 15p

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Input 12 to 24V DC (not centre tapped)

18V input giving 10 volt constant amplitude output Requires only a 1 meg ohm pot to tune entire range-or can

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munications; frequency modulation etc. Detailed application sheet with all purchases

HACHI RAMP MODULE FX21

24 volt DC input for 18 volt sawtooth output. Requires only external capacitor and 100K ohm potentiometer to control frequency range up to 100kHz (eg 50 mfd electrolytic gives sweep of approx 1 cm per second). In or out sync capability. Price £5.75 P. & P. 15p

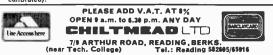
FHACHI FILTER MODULE FX31

Designed for use with VCO FX11 and RAMP FX21. This completes the 3 building blocks required for a basic lowfrequency Spectrum Analyser that covers 100Hz to 50kHz. The additional components required are discrete resistors and capacitors, etc. (No inductances or specialized components are needed). Price £13 00 P. & P. 30p. Fibre glass P.C. board to mount FX11, 21 and 31 ready drilled. Connection details and list of additional compo-nent required supplied with each order. £2-50 P. & P. 30p.

LOW FREQUENCY WOBBULATOR

LOW FREQUENCY WOBBULATOR Primary Intended for the alignment of AM Radios Communication Receivers: Filters, etc. In the range of 250 kHz to 5 MHz, but can be effectively used to 30 MHz. Can be used with any general purpose oscilloscope. Requires 12V AC input. Three controls—RF level sweep width and frequency. Price £1:92 A second model is available as above but which allows the range to be extended down in frequency to 20 kHz by the addition of external capacitors. Price £1:93. Both models are supplied connected for automatic 50 Hz sweeping. An external sweep voltage can be used instead. These units are encapsulated for additional reliability, with the exception of the controle (not cased not calibrated).

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AERIAL MAST POLES. Approx. 5ft. 2in. high, 2in. dia. Interlocking ends . Minimum order 3. As new, £1.25 (each) P. & P. 40n each.

AERIALS. As new. Whip Type 11ft. £1 each. Collapsible type. P. & P. 20p. New Bases for the above 75p, P. & P. 30p.

PAIR OF 4 × 150A VALVES complete with bases ex-equip not tested. Good condition £3, P. & P. 30p.

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FANTASTIC BARGAIN. New 6 inch tubes. E450 4/B/16 4VH, medium Persistance, green. Ideal scope tube.

Also 7BP7. All unused as new. Price £2 post paid.

TRANSISTOR BOARDS-consisting of transistors, diodes and resistors etc. Long leads. Good value 12 for £1.00 (min. order) P. & P. 30p. Quotations for quantity.

OUR SELECTION OF 6-Ex. Equ. METERS consisting of 3in., 21in., 2in. mill amps, volts, amps. Mixed at the bargain price of £2.20 P. & P. 30p. minimum order of six.

NEW AERIAL WIRE ON BOARDS 7/22 UNCOVERED 90ft £1, p. & p. 25p.

AERIAL POLES 4ft high 2" in diameter push-in type as new fl each p. & p. 25p each minimum four.

DLR No. 5 HEADPHONES-High impedance. Good condition £1.30 postage paid.

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CHIPS UNLIMITED!

We calculator market. It has been currently estimated that the world-wide production of chips for electronic calculators for 1974 will be of the order of 28 million units. This exploding market is one of the few fields in which prices are constantly dropping. If the present growth rate continues, it is estimated that there will be an electronic calculator shortage within two years!

There exists a veritable jungle in both price and selection. The prolific arrays of pocket calculators that are available to the consumer that dominate the windows and counters of our local high street shops are indeed bewildering. There appears to be a greater variety of pocket calculators than transistor radios!

A price war has emerged amongst major manufacturersprices being slashed overnight and indeed putting many retail distributors and 'special offer' organisations on the spot! A recent overnight price reduction by a major manufacturer caused considerable embarrassment to many of his trade and retail outlets. This sort of fiasco is being repeated over and over again. Where will it all end?

One enterprising calculator manufacturer determined to display his 'chips' to members of the public has opened up a 'mobile shop' at a London main line railway station. By all reports, he is doing *fantastic* business.

What of the 'domestic' pocket calculator? Rumour has it that a basic calculator especially designed for the housewife may be launched. If so, this could be just the thing for calculating and analysing those shopping expeditions to the supermarket. The shopper would be able to check his totals at any time and at the till check-out point. I can foresee many red-faced supermarket managers attempting to explain away the differences that may occur between store and customer calculated totals.

The pocket 'memory' calculator with its inherent potential as a pocket computer, with the ability to recall stored information at the press of a button could be just around the corner!

What of the future? The pocket calculator could become as prolific as the ball-pen—a must for everyone.

However, the pessimists (optimists, if you prefer) are chanting 'Beware, Big Chip is watching you!' (shades of 1984). They could however be forecasting our future.

There is no doubt that the calculator chip has, in many ways, dramatically changed our whole way of life. The question is: are we all in the hands of the Big Chip?

LIONEL E. HOWES-Editor.

We're off to a good start in the New Year with our three part series on Model Control by Radio and we tell you how to get your licence for this most interesting of hobbies. Do you sometimes wish you had a small audio amplifier around for testing purposes? Our 2 watt IC audio amplifier will fill the bill. The Special Pre-publication Book Offer ought to appeal to many of our readers for all the useful information contained in Radio Servicing Pocket Book, a new 3rd edition. Finally, you won't want to miss the fourth and final part of the PW Buyers' Guide 1974/75. All in the January issue of Practical Wireless.



From Partridge . . .

A ever increasing number of people are living in space restricted environments. Either through sheer lack of external facilities for the erection of aerials, the inability to receive radio signals inside ferro concrete walls, or the existence of local government legislation preventing the use of outdoor space for aerials, there are ever growing numbers of frustrated readers unable to pursue their hobby of Amateur Radio or Short Wave Listening.

For many years now Partridge Electronics Ltd., of Broadstairs, Kent have specialised in equipment designed to overcome this problem. Five years ago they published a reproduction of a World Record Certificate awarded to American Radio Amateur W6TYP. This was achieved by Mr. Art Child of San Francisco using the Partridge system operated from a hotel room at the foot of San Francisco's famous Nob Hill.

Partridge have now developed a device known as A.G.T.U., an Aerial Tuning Unit which also incorporates an Artificial Earth (or ground). This overcomes the only remaining problem of the high-rise apartment or flat dweller having no access at all to natural earth.

ON THE COVER

PW's MINIATURE SCREWDRIVER

Don't despise this very useful workshop aid because it seems to be so small! How many times have you found that your 'small' screwdriver is just too wide or too thick for the grubscrew in a knob or the adjusting slot in a subminiature potentiometer?? The more you use it the more uses you will find for our little present!

NEWS.

Harrogate Fair

A UDIO '74 or the Northern International High Fidelity Festival at Harrogate was the biggest and best-attended ever. In 1970 there were only 50 exhibitors. 1972 saw 70 firms exhibiting their wares and this year over 90 companies decided to show their faces.

Over the last couple of years, there has been a marked increase in the amount of quadraphonic equipment on show. It is a pity that there seems to be little or no agreement on the kind of system to be favoured for quadraphonic reproduction.

We hope to include a short report on "Audio '74" in a future issue.

BBC tape deal

A CONTRACT to supply the BBC with more than 100,000 reels of TS Scotch 262 recording tape for stereo broadcasting has been awarded to 3M United Kingdom.

The contract, which is due to run until next June, is in addition to the 70,000 reels supplied to the BBC last year after close liaison between the Corporation's sound engineers and technicians from 3M's magnetic tape facilities at Gorseinon, near Swansea, and Caserta in Italy.

BEAB approval list

THIS list covers the first category of audio products in the BEAB Approval Scheme which have successfully met the requirements of the British Safety Standard BS.415: 1972.

Decca Radio & Television with the Decca DS623, ITT Consumer Products Ltd. (ITT KP 820, KP 821, KA 1026, and RGD PA 30, P 83). Pye Limited (Pye 5000 and Invicta 8040). Sony (UK) Limited (Sony HMW-20). Rank Radio International Ltd. (Bush A 1005, A 1016, BS 3013, Dansette A 4005, A 4016, and Murphy MS 3014). Thorn Consumer Electronics Ltd. (HMV 2046, Ferguson 3047, Marconiphone 4047, 4049, Ultra 6046, 6048.

Computer club

NEWS

NOW moving into its second year of existence the Amateur Computer Club of Basildon, Essex has now formulised its activities into a constitution and elected officers for the year.

2.8

The club now has a firm membership of over 200 with a regular newsletter forming the nucleus of the club.

After two Annual General Meetings in London and committee meetings the start of a club activity schedule has emerged. The first of which was an open afternoon on the 25th May, 1974, at the Galdor Centre, 52 Brighton Road, Surbiton, Surrey.

The people at the Galdor Centre own and run an ICL 1301A computer (1960 vintage) which they have installed and made working to provide them and similarly interested persons with computer time at "materials only" cost.

Heathrow computer

ABLE and Wireless Ltd. have installed a new computer-based departure control system for airline passengers at London Airport. Japan Air Lines will use the system named "Lopac" which has been jointly developed by C & W and Scientific Control Systems Ltd.

Apart from speeding passengers' baggage check-in procedure, the system also allows for productivity expansion.

Lopac, incidentally, stands for Load Optimisation and Passenger Acceptance Control.

PW TOOL KIT OFFER

We apologise to our readers for the delay in dealing with their orders. The overwhelming demand created problems with delivery. If any readers have not received their tool kits, or a suitable alternative, would they kindly contact the Editor. Further activities are being arranged and will be announced in the newsletter which has also provided a unique forum for the airing of ideas and introducing basic principles to the beginner.

NEWS.

Articles in the newsletter have covered transistor working, design and operation of a digital core store, digital computer elements. computer software, software routines, descriptions of various computer systems both working and under design/development, news information items and computer games!

Club members are contributing articles to the newsletter resulting in some cross fertilisation of ideas among the members, which is one of the most important objectives of the club.

New members and ideas are very welcome, membership is $\pounds 1.00$ per year (that includes the near monthly newsletter) and applications should be directed to Mike Lord, 7, Dordells, Basildon, Essex.

Javelin move

JAVELIN Electronics have closed down their City offices and moved to Javelin House, Second Way, Exhibition Grounds, Wembley, Middlesex HA9 OUA. (01-903-6821).

The new building contains the service department, a dealers' advice centre and a customer relations department.

Sansui 4-channel

T HE sponsors of the "QS" 4channel system, Sansui, are making moves to persuade artists in the UK to record material using their system.

The "QS" regular matrix system has been accepted by the American and Japanese Recording Industries Associations and over 20 record manufacturers are producing software in the system.

It has been stated that at least one commercial radio station in the United Kingdom is thinking of using "QS" which has now been adopted by all f.m. stations in Japan.



I MUST confess from the start that I am not entirely unfamiliar with the RT-VC car radio having bought an earlier version some time ago. I spent a couple of evenings leisurely soldering the bits and pieces to the printed circuit board and putting the thing together, following the instructions most meticulously. On connecting it up to a 12 volt battery in the workshop the radio worked first time and with a tweak of the oscillator capacitor the calibration was done.

The set soon disappeared into the innards of my daughter's Triumph Herald. I was about to say 'never to be seen or heard of again' but that would be patently untrue since the radio is simple but elegant in appearance and can certainly be heard! Subsequently, the set came out for a further fiddle on the oscillator trimmer to enable London's Capital Radio to be tuned in right at the low frequency end of the medium wave band. A big improvement on the sideband splash that had been tolerated up to then!

This latest Tourist Two car radio kit has taken all the fun out of the home construction of kits and one would be hard pushed to say, with a clear conscience, that 'I made it myself'. Admittedly the earlier version of the PCB had a few components plus the audio IC already soldered in position but I suspect that RT-VC did this so that they could say 'look at our soldering ... now you do the same'. In fact, they insisted that the constructor's soldering was as good as theirs before accepting back any kits for servicing or checking ... and quite rightly so.

Now, alas, the PCB comes completely assembled and the soldering iron remains cold and unwanted! A pair of long nosed pliers and a small screwdriver are all the tools required with this new kit and the remaining assembly work is child's play. In the words of RT-VC 'the kit can be assembled in less than two hours by anyone who has the ability to wire a normal household three pin plug'.

Assembly

The assembly instructions are extremely detailed and I cannot think of any point that would arise that isn't dealt with already. RT-VC's guarantee says 'If, after receiving your Tourist kit, you feel that its construction is not within your capabilities we will refund you the full price of the goods, less post and packing, upon the return of all parts supplied on the condition that no constructional work been attempted and all parts are received in the same condition as dispatched'. I hope that the formidable appearance of the assembly instructions, fault-finding guide, installation instructions and six annotated photographs will not have the opposite effect and frighten off the prospective constructor!

Having completed the assembly you will want to know the polarity of your car's electrical system. If it is negative earth then the set is ready to go but if it is a positive earth then you have to change over two of the push-on tag connectors. Not very difficult! Should you decide ever to transfer the radio to a car of opposite polarity the change back can be made more quickly than it takes to tell.

Installation

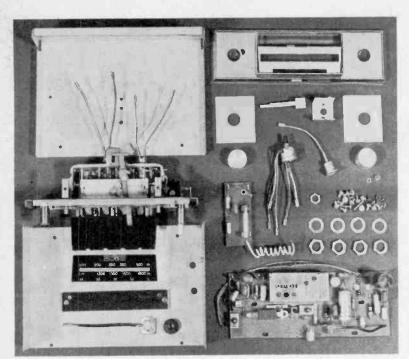
RT-VC recommend a check-out of the set with the car battery before final installation in the car. Calibration takes a moment and the aerial trimmer is adjusted using the aerial that is to be fitted to the car. If all is well, and I'd be surprised if it wasn't, installation can now begin. RT-TV's instructions on this aspect are, again, as complete as they

Waves 185 to 555m (1620 z) aves 1153 to 2000m (260 to
an 15µV at 1MHz
0 4 ohm speaker
ttons (4 MW 1 LW), tuning control, volume/
″ high 4½″ deep approx.

The supply voltage is nominally 12 volts. The polarity, relative to the case, can be changed over internally simply by reversing two push-on tags. The circuit is protected by an internal fuse and a VDR (voltage dependent resistor) against static discharge.

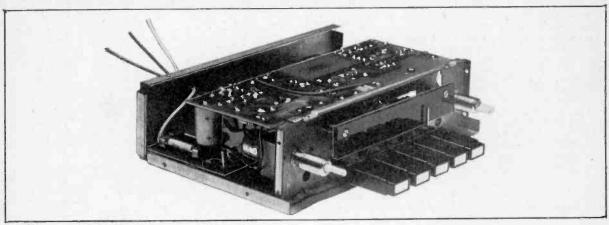
Prices:- Car Radio Kit $\pounds 7 \cdot 70 + 55p$ P/P. Speaker, including baffle and fixing strip $\pounds 1 \cdot 65 + 23p$ P/P. Car Aerial, fully retractable and locking $\pounds 1 \cdot 37 + 20p$ P/P.

Radio and TV Components (Acton) Ltd., 21 High Street, Acton, London, W3 6NG



The contents of your kit will look like this, left. Between the metal casing is the permeability tuning unit and pushbutton assembly. Bottom right shows the complete PCB which is fully tested before despatch.

If the simple instructions are followed the almost finished set should look like that in the photograph below. Only the dial, escutcheon and knobs remain to be filled plus the cover.



can be and cover every contingency. There is one point here that might be stressed. If you use the aerial available from RT-VC the feeder is about 4' 6" long and the aerial trimmer works perfectly, peaking signals as it should do, when the overall performance is excellent. However, if you need to fit the aerial to the car in such a position that requires the feeder to be extended then this **must** be done using a special extension lead otherwise performance will definitely be impaired. Using ordinary coaxial cable just will not work. This point is fully covered in the instructions.

Apart from the manual tuning over both bands, four of the push-buttons can be set very easily to any desired stations on the MW band, the fifth push-button selecting a station on the LW band, usually BBC Radio 2, the band change being automatically effected by the action of the push-button. If, for some strange reason, the set does not work at all, or unsatisfactorily, then the Fault Finding Guide will come to your aid and the answer found very quickly.

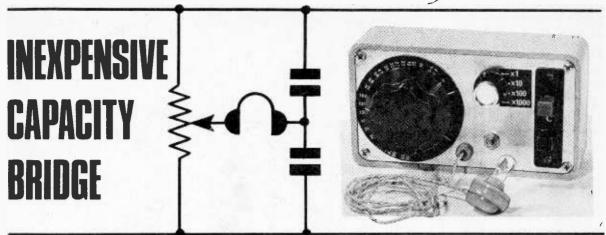
Interference

Having completed the installation and tested the radio to your satisfaction there is a chance that you will suffer a slight set-back when starting the car, because of interference to the radio from the various bits of electrical equipment. Generally, unless the car is a real old 'banger', normal suppression capacitors and other devices will be fitted to the car already and little trouble will arise. However, this matter is dealt with fully in the notes and if the logical sequence of checking is followed a rapid solution will be found.

Conclusions

A very well designed kit with all the bugs ironed out long ago. Being a bit of a fiddler myself I would have liked the oscillator and aerial trimmer capacitors to be accessible from the outside of the case when the radio is installed in the car. I compromised by very carefully marking out and drilling two holes in the top cover of the case above the trimmers, sticking a bit of Sellotape over the holes when I had done fiddling. I wouldn't expect RT-VC to do anything about this point but I thought I'd mention it, got to complain about something!

Finally, I don't know how RT-VC do it at the price but I understand it is due to the purchasing in volume of proven components and direct retail sales. Certainly they are not contributing to the present inflationary movement!



ERIC DOWDESWELL G4AR

Test gear is often conspicuous by its absence from the amateur's workshop, possibly because such equipment can be expensive to buy but, more likely, because it is not a justifiable outlay considering the relatively few occasions on which it would be used.

The capacity bridge described here is very cheap to make, will measure capacities from as low as 2pF and up to about 10μ F and will be found to be quite adequate for general workshop use. Over a period the constructor manages to collect unto himself a quantity of capacitors that have had their markings removed in one way or another. This bridge will enable them to be measured, checked and used again. Incidentally, it is a very wise man who checks the value of every component before using it, regardless of colour code or marking, saving a lot of time and temper.

It is not everyone who has good eyesight and even slight colour blindness can cause confusion with colour coded components, generally with blues, browns and greens, which can lead to wrong values of resistors and capacitors being fitted to PCBs etc. This bridge will eliminate any such problems especially if it is used as a matter of routine.

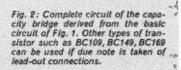
The dial is simple and easily calibrated and used in conjunction with a four step multiplier switch. The consumption of the bridge is very low and the internal 9 volt battery will last a very long time.

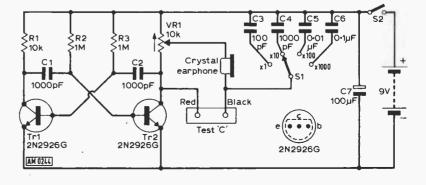
DESIGN

As you may have guessed, a bridge circuit is used, what else! and was last seen in the Take 20 series R1 VR1 R2 Cx Cx Cx AM0225

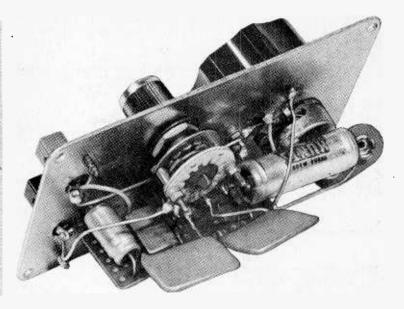
in this magazine. In essence, the collector load resistor of the second transistor of an audio oscillator forms two sides of the bridge, Fig. 1, and, in practice, is a potentiometer. The other two sides of the bridge comprise a capacitor Cs of known value and Cx, the capacitor under test. If these capacitors have the same value then, for the bridge to balance, R1 will equal R2. A detecting device 'D' placed across the bridge will indicate a null in the audio tone under these conditions. If Cx is any other value then the bridge is unbalanced and 'D' will indicate this. Balance can be restored if the ratio of R1/2 is adjusted to have the same ratio as Cs/Cx.

In the practical circuit, Fig. 2, Cs is in the form of a four position multiplier switch with capacitors of 100pF, 1000pF, 0.01μ F and 0.1μ F all of close tolerance, the switch being marked x1, x10, x100





In this inside view of the bridge the capacitors have been moved away from the switch S1 to show the circuit board.



and x1000. The capacitor under test is connected to the two terminals. Transistors Tr1 and Tr2 form a multivibrator circuit running at about 1kHz but the actual frequency is not of any great importance.

The detector is a simple crystal earphone of very high impedance, this factor contributing very significantly to the excellent performance of the bridge, the minimal damping imposed by the earphone providing a deep sharp null at balance.

CONSTRUCTION

The bridge is housed in a heavy plastic box with all the components mounted on an aluminium panel. The oscillator components, with the exception of the potentiometer VR1, are assembled on a small piece of Veroboard as in Fig. 3. The bottom rail of the board is soldered to a tag bolted to the panel, providing adequate support for the board.

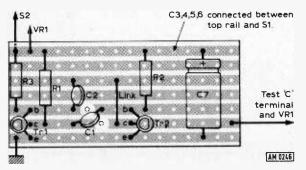


Fig. 3: Components comprising the audio oscillator are mounted on Veroboard as shown above.

The test terminals are spring loaded, their soldering tags passing through ${}^{3}_{8}$ in. holes drilled in the panel. The holes are purposely large to reduce self capacity. An alternative might be to use feedthrough insulators terminated on top of the panel with miniature crocodile clips on stiff leads. Whatever arrangement is used it is essential that a capacitor can be connected to the bridge and removed again very easily.

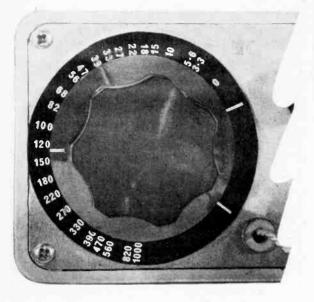
The potentiometer is a very ordinary linear carbon one with a plastic spindle, which, again, reduces self capacity but one with a metal spindle would probably work just as well. The dial was made from a disc of card held under the potentiometer fixing nut together with a pointer knob of such a size as to allow a single range of calibration figures to be marked on the dial. The dial is marked in the 'preferred' range of values corresponding to the standard markings on capacitors.

The crystal earphone is wired directly into the circuit, which again helps to reduce capacity. A combined phone jack and on/off switch was contemplated but a switch and isolated jack could not be found. If any doubt exists as to whether an earpiece is crystal or magnetic it can be checked with an ohmmeter. A magnetic one will show very low resistance whereas a crystal one will show very low resistance whereas a crystal one will show, effectively, an open circuit. Just to make sure that you havn't got an open circuited magnetic earphone put it in the ear and check again with the meter when clicks should be heard even though the meter indicates an open circuit.

The multiplier switch used here is a miniature ceramic one but the more common plastic or paxolin wafer type will suffice. However, if the switch chosen has been used before it must be very thoroughly cleaned before using it in this bridge, for reasons which will be noted later. The standard capacitors C3 to C6 are wired directly between the switch tags and the top 9 volt rail on the circuit board. If a standard size switch is used it will be necessary to move the board down from the position shown in the prototype. It is a good idea anyway, with any project, to shuffle the components around for best positioning before drilling panels etc.

CALIBRATION

After the small amount of wiring is completed and checked, fit the PP3 battery and switch on when the audio tone should be heard in the earphone. The volume, should be adjustable from maximum to zero using the potentiometer. Adjust the position of the knob on the potentiometer spindle so that the ends of its travel are positioned as shown in the photograph of the bridge. Mark these positions on the dial with a sharp pencil. With the multiplier switch on x1 a null should be found near the top of the dial, if the potentiometer has been wired as shown in Fig. 2. This represents the zero position of the bridge without any external test capacitor. Mark this point on the dial.



Close-up of the dial of the bridge. Note that the limits of travel of the potentiometer are also marked.

With a 100pF 1% capacitor connected to the terminals and multiplier on x1 find a new null at about mid position on the dial, then mark it. Turn multiplier to x10 and locate null not far inside the 0 mark. This is marked 10. Note that we have been able to find two points on the dial for one capacitor, using the multiplier. This feature can be used to cross check dial readings.

Change the test capacitor for one of 100pF 1% and mark the null at the bottom end of the dial. Switching to x10 should locate the null at the 100 point, already marked. The remainder of the calbration is done using 1% or 2% capacitors in the preferred range of 120, 150, 180, 220, 270, 330, 390, 470, 560, 680 and 820pF. The x1 multiplier is used to mark the remaining points between 100 and 1000pF and x10 for the points between 10 and 100pF.

TOLERANCES

For a general purpose bridge the cheaper 5% tolerance capacitors are quite adequate for calibration purposes but instead of having to buy the thirteen preferred values it is possible to make do with eight only, the missing values being obtained by paralleling certain capacitors as shown in the Table. There are probably other combinations possible by connecting capacitors in series or even series parallel!

The calibration can be completed with a fine ball point pen or a more fancy dial constructed, as shown in the photograph. As the end points of the potentiometer travel have been marked the diat can be removed for finishing or copying and then replaced without losing calibration.

	CAL	IBRA	TION CAPAC	ITORS (pF)
	100		220	470
	120		270*	560*
	150		330*	680*
	180		390*	820
			1000	
			ked * may be ob parallel, as foll	tained by connec-
			330 150 -	
390	220 +	180	560 220 -	180 1 150
		680	220 - 180 +	150 + 120

EXTENDING RANGE

As shown, the maximum capacity indicated on the dial is 1000 x 1000pF or 1μ F but it was later found possible to extend this range to 10μ F enabling small value electrolytic capacitors to be checked, although it should be remarked that there is no polarising voltage applied to the capacitor under test. Nevertheless the bridge has been found very useful for this purpose.

The accuracy of this extension to 10μ F will depend upon the accuracy of a 1μ F capacitor that is required for calibration. Again, a 5% tolerance will do as a 1% capacitor of this value is rather expensive. Connect across the test terminals and locate a null near to the bottom end of the travel, past the 1000 mark. The multiplier should be on x1000. The point can be marked 10nF for simplicity. Only two or three intermediate points are required such as 2200, 4700 and 6800.

IN USE

Normally the null will be very deep and sharp. In my own case, the audio tone actually disappears at the null point and I generally consider my hearing

***** components list

R1			/3 1MΩ 10% ⅓ or ⅓W
VR1	10kΩ linear car	bon pote	entiometer. See text
Capac	itors		
C1	1000pF 10%	C5	0.01µF 1% SM or
C2	1000pF 10%		Polystyrene
C3	100pF 1% SM	C6	0.14F 1% Poly-
C4	1000pF 1% SM		styrene
		C7	100µF 16V electrolytic
Calib	ration Capacitor	s:-see	
Bitt.			
	laneous		
			none. Battery 9V PP3,
			. Veroboard 0.15in.
matri	x, approx. 21 x 1	liin. Kno	b and dial. Terminals
(2). (Case and panel	5 x 21 x	11in. deep (Stella 99
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			Louis and otoon

to be better than average. If the null is not deep and seems to be undefined then the capacitor is probably leaky although it may be of the order of a few megohms. The effect can be simulated by connecting a high value resistor across a known good capacitor and testing the combination on the bridge. The lower the resistance the poorer will be the null. In the long run it is better to destroy such leaky capacitors at the time of testing rather than to leave them around to be used in equipment where the leakage might prove highly detrimental to the operation of a circuit.

AUDIO OSCILLATOR

The bridge can also be used as a source of audio tone for testing amplifiers and suchlike, the output being taken from the test terminals and adjustable from zero to maximum output with the potentiometer. The waveform is very rough, of course, coming from a multivibrator but quite adequate for general audio testing. If a Morse key is connected across the on/off switch the unit can be used as a Morse code practice set. A second crystal earpiece can be connected across the test terminals and, if two keys are connected in parallel, two-way simulated signalling will be possible.



presented last month





IN THE DECEMBER ISSUE

SIGNAL STRENGTH METER

Correct aerial alignment is important If bright, sharp pictures free from blurring due to multipath reception, stably synchronised and with accurate grain-free colour are to be achieved. This is difficult without a signal strength meter since the receiver's a.g.c. system will hide signal strength variations—quite apart from the physical problems. The TV signal strength meter described is portable and can be used to ensure that any u.h.f. TV aerial is aligned for optimum reception: It is equally useful in local and fringe areas. Features include varicap tuning, three gain ranges and a unique Indicator of vision carrier reception by means of a light-emitting diode. Construction is easy since a ready-made surplus i.f. strip is used.

DECODER FAULT-FINDING

Colour receiver decoders are generally reliable but when they do give trouble fault-finding can be a headache. In "Practical Decoder Fault Finding" in this issue a number of useful hints and tips based on practical experience are given together with guidance on the logical approach to tracing faults.

SELF-CONVERGING COLOUR C.R.T.s

The next generation of colour sets—already beginning to appear on the market—will be fitted with self-converging c.r.t./deflection yoke systems. How these operate, with particular reference to the Mitsubishi SSS tube, will be described.

SERVICING TELEVISION RECEIVERS

The Baird/Radio Rentals 660, 670 and 680 series of TV receivers and their faults will be described by Les Lawry-Johns.

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ON RECENT DEVELOPMENTS.

MEASUREMENT

IT never ceases to amaze me that measurement in electronics gets more and more sophisticated as every day passes. On reflection this must be so because as the very latest devices are born, some means must be to hand with which to measure. accurately, their performance. At the recent International Microwave Exhibition at Montreux, for example, there were switches shown which could switch at 26GHz-that's twentysix thousand million times every second! I might add that the man on the stand eagerly told me, "... and of course we're working on higher frequencies right now"

While frequency must be measured accurately, what about time? Latest to come to my attention is a time interval counter which is soon to be launched in America. The amazing thing about this one is that it has a resolution of 100 Femtoseconds, If you are not impressed then let me add that a Femtosecond is 0.001 of a picosecond and a picosecond is one millionth of a microsecond which, of course, is one millionth of the common or garden everyday household second. For the technical/boffin types it's 10-15 seconds. Just think if every Amateur radio station had one of these, it could tell its transmission frequency to a fraction of a cycle even at v.h.f.

TIMED CALCULATION

Electronic calculators and digital wrist watches always create interest but now I really have heard it all. The ultimate is about to be launched onto the market, something that will satisfy even the most pedantic of tiros. It's a digital wrist watch and calculator combined! The calculator part has a nine digit readout and offers forty functions. When it's not used as a calculator it functions as a digital watch. There are only 20 buttons on the calculator and here the designers have introduced a very crafty dodge.

Although only twenty buttons are employed (because of space considerations) there's a "shift key" which, when activated, gives the twenty buttons other functions thus

giving a 40 button capability. This shift key acts something like the shift key on a typewriter which allows the same keys to be either capital letters or small, lower case letters. The watch/calculator measures about 1.5in x 1.5in x 0.5in. deep. The first models are rumoured to be priced at around £200-£250 but they're not available yet and probably won't be for some time. The buttons, incidentally, are depressed with a small probe, or tip of a ballpoint pen as far as I can ascertain. Information is rather scant because this is a state of the art unit and the information is red hot.

SOLID-STATE C.R.T?

A colleague in Washington reports that the US Army may soon lay its hands on a liquid crystal display which gives an 84-character output. It also might be used as a liquid crystal cathode ray tube. At present the company doing the development is waiting to get a Government grant with which to continue work. It is also rumoured that the prototype device is coupled up to a miniature warfare computer. If this development is well funded, it could be another avenue of development for the solid state c.r.t. for television receivers.

SOLID-STATE CAMERA

At the other end of the television signal-the camera, developments are pressing on with solid state sensors which will replace the vidicon camera tubes. This was highlighted at the recent conference on charge coupled devices (c.c.ds) which took place at Edinburgh University. Of great interest was mention (plus photograph) of a miniature entirely solid state television camera which was constructed by Bell Labs at Murray Hill, New Jersey. Another interesting fact about this television camera is that it is battery operated. The size was not mentioned but from objects in the photograph which include a ruler, it is judged to be of the order of 11cm x 6cm.

The camera uses a chip sensor which has 256 x 220 element array gives excellent results using NTSC scan rates and the author claims

that television image sensors with 525 and 625 line capability are now a viable product. It must be remembered that solid state cameras will not come in over night. At present, users of the "valve" type camera tubes have only to plug in a component and it works whereas these solid state items are still being developed. However, with the world shortage of silver and the search for some other means of photography, it isn't too difficult to see the amateur photographer of the future holding a tiny solid state twin lens reflex which records directly onto tape which can then be played back on the television receiver at home

These CCD devices are well worth watching. New applications are coming up and are being enthusiastically worked on. To date they are being used in TV applications, infra red cameras, delay lines, telecommunications, memories for computers and are even employed to generate a s.s.b. signal.

IT'S SIMPLE!

The servicing of televison sets has taken a step nearer to being automated. Grundig colour television receivers are currently manufactured in modular form. A number of modules are used in a plug-in fashion, each unit looking after a specific function within the receiver.

The offending module (in the case of malfunction) is simply unplugged and either repaired immediately or just replaced and then repaired at leisure in the workshop.

Some 75% of the colour television circuitry is catered for in this way. Now, Grundig has taken care of the other 25% by adding a simple socket to the receivers. A small diagnostic unit is then simply plugged in. The circuitry is featured on the lid of the diagnostic box, and l.e.ds mounted in this circuit diagram illuminate to pinpoint any fault.





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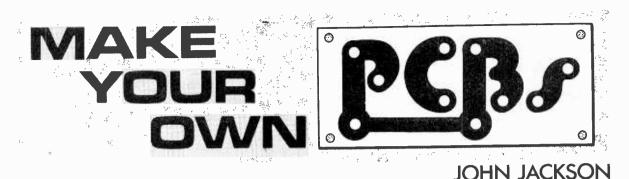
This fine receiver is not a mass produced item, but each set is hand built to your order, individually checked and air tested. Please allow for this when ordering-your delivery date will be shown on your order receipt, sent by return.



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For the amateur, printed circuit boards have good and bad points. They are neat, reduce free wiring, make assembly mistakes less likely and can support large items such as transformers. On the other hand, they take time to make and subsequent modification to them can be difficult.

Ready-made "universal" printed circuit boards may have no copper where it is required, will have it where it is not needed and mistakes during soldering are easy as different areas look alike. The design and preparation of individual boards is easy and the materials readily available.

DESIGN

The method used successfully for many projects is as follows. A fairly large copy of the circuit is drawn on thin paper, such as that used for typing (thin paper saves time later). All component junctions are ringed, as shown dotted in Fig. 1, to give the basic copper plan. Beneath this is drawn an outline, the size of the intended circuit board and, using components to check spacings, the basic plan is adapted to give a full size layout, Fig. 2. ... Tr1.1.1. A number can be crossed off each time a connection is allowed for.

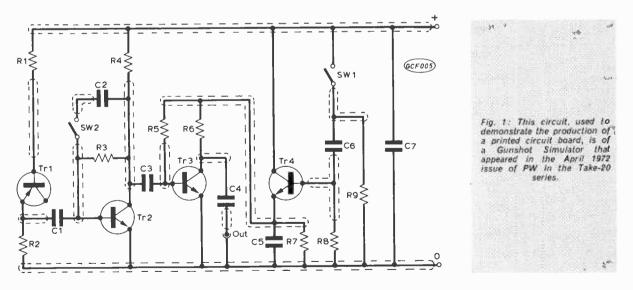
A negative of the plan must now be made. This is easily done by turning the paper over and drawing over the lines that should be visible. This plan is the master diagram, see Fig. 3.

It is possible to forget to reverse the plan, which is not serious with transistor circuits, but it will be tricky reversing a nine-pin valve-holder to match!

PREPARING THE BOARD

Copper laminate may be backed by fibreglass or SRBP, the latter being cheaper. Areas requiring copper, the "fields", are covered with resist and the unwanted metal is etched away. Resist can be from a purpose-made pen, such as a "Dalo" or use can be made of nail lacquer or paint (thinned enamel or cellulose).

First the board must be cut to size, with a hacksaw having a fine blade, cutting with the copper side up. After filing off any burred edges the copper must be thoroughly cleaned of grease or tarnish, using



In the final layout it is advisable to keep input and output points apart and wires leaving the board are better near the edges. Fixing holes must be taken into account and copper should not be too close to these, to prevent shorting to metalwork. To avoid missing a component, a list can be made with each component written once for each wire: R1,1, R2,2, scouring powder on cotton wool. After rinsing and drying on a soft cloth the copper is ready for the resist and the board must be held only at the edges, as any grease may cause the resist to flake off and prevent areas from etching.

The board is then stuck beneath the master diagram, with a piece of Sellotape to reduce handling,

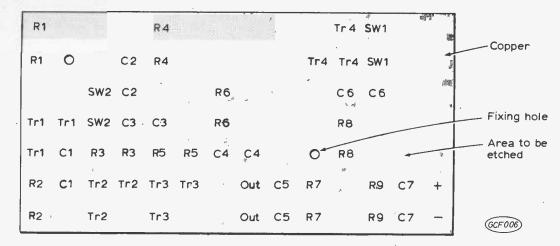


Fig. 2: The dotted areas of Fig. 1 are transferred to the paper master as shown here, the final layout depending upon the sizes of the components to be used. The copper will be on the other side of the board, which is shown here twice final size.

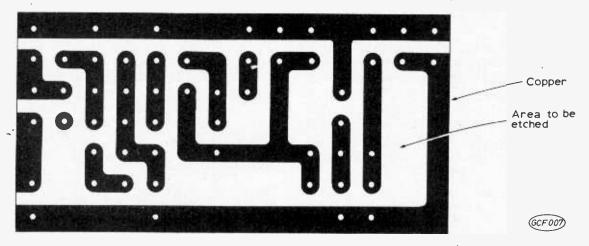


Fig. 3 When the layout is finalised it must be reversed on to the board as shown here, complete with the holes required, drilled after etching.

and a piece of carbon paper in between, carbon side down against the copper surface. Draw over the master with a pencil which will leave the outlines on the copper. Remove master and carbon paper after which the resist can be painted on the areas of copper which are to be retained. While the resist dries the etching solution can be prepared.

ETCHING

Ferric chloride is used which can be bought from advertisers in this magazine. One pound will etch many boards. A suitable strength is about one tablespoon per fluid ounce of water. The crystals should be added to the water, not vice versa, and this should be done with care as a lot of heat is generated. The solution may attack skin if splashes are not rinsed off and it will stain cloth and wood, so work over newspaper. The solution must be used in a non-metal dish, a saucer is ideal, and after use it can be stored in an old bottle with a plastic top.

If the prepared board is carefully levered off the paper, the Sellotape can be used as a handle. The board is placed gently on the etching solution **copper side down**. Surface tension will support it and the insoluble etching product can sink to the bottom, no agitation being necessary. After five minutes or so lift the board and see that all the copper shows pink. Greasy finger marks show brown and unetched. If all is well, allow the process to continue, taking roughly twenty minutes. When all the unwanted copper has gone the board should be thoroughly rinsed with water and then the resist can be removed. "Dalo" or nail varnish will come off with nail varnish remover (acetone) while paint will require white spirit or stripper. A final wash with soapy water will leave the board ready for drilling.

DRILLING AND SOLDERING

Drilling should be done with as fine a drill as possible, for a hand drill this will be about 1 ₁₆in. dia. The slow speed on an electric drill is suitable but only gentle pressure must be used or the board will crack. It will be helpful to mark all the holes with a sharp point (a centre punch will not do) first, then hold the board in front of a piece of wood, in a vice, and drill all the holes. Any burrs can be removed with a larger drill. The board is now ready for use.

The bond holding the copper to the board material is strong but too much applied heat may cause the copper to peel off. As usual, resistors and other passive components should be soldered before semiconductors, though connecting wires should be left until last.

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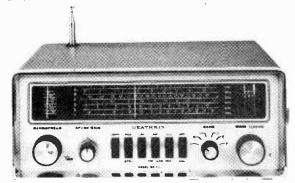
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Transistor			BCY30	58p	ME04075	34p	INKT713	34p	2N930	227	Ther-		IN5407	280	7437	779		
AA119	P BA154	14p	BCY31	699	ME0491	23p	NKT773	809	2N1131	26p	mistors		IN5408	34p	7738	775	74155	18·2 ⁰
AC107 24		18p	BCY70	17p	ME0492	23p	OA5(GH500		2N3132	26p		150		Zener	7440	20p	74156 🔮	1.7
AC126 2		8p	BCY71	87p	ME0493 ME1001	21p 16p		199	2N302	80p		15p	Diodes		7441	81p		1.8
AC127 11 AC128 10		14p 14p	BCY72 BD124	14p 1-80	ME1002	17p	OA10 9 0A47	24p 9p	2N1303	80p		15p	3.3v to 3	34 155	7442	81p		8.18
AC141 8		149	BD131	580	ME1075	190	0490	6p	2N1304 2N1305	88p 88p		16p	Thyris	tors	7444	£1·40 £1·57		4-84
ACI41k S		18p	BD182	570	ME1100	205	0A91	69				14p	1 amp		7445	49-81		4.84
AC142 2		19p	BD181)	M/P	ME1120	205	OA95		2N1306 2N1807	47p 47p		14p 15p	50v	80p	7446	\$1.61	74164 4	
AC142k 2		19p	BD132	£1·18	ME2001	15p	(HG1005	7p	2N1308	589		140	100v	82p	7447	\$1.58	74165 #	3.78
AC151 2		26p	BDY20	910	ME2002	16p	OA200	9p	2N1309	560		***	200v	87	7448	\$1.98		4.28
AC152 25		17p	BF167	25p	ME3001	21p	OA202	99	2N1613	24p	Bridge		400v 3 amp	46 p	7450	20p	74174 £	
AC153k 89		17p	BF173	28p	ME3002	26p		55p	2N1711	25p	Rectifier	. 1	5 amp 50v	86p	7451	207		8.94
AC153k) M/		19p	BF177	879	ME3011	21p		45p	2N2218	88p	1 amp	-	1007	40p	7453	20p 20p		2·78 3·70
AC176k / 82 AC176k 49		19p 35p	BF178	84p	ME4001	16p		65p	2N2218a	48p	50v 3	88p	200v	44p	7460	200		8.49
AC176 24		120	BF179 BF194	38p 16p	ME4002 ME4003	17p 19p		69p 59p	2N2219	42p		48p	400v	59p	7470	365		2.16
AC187 22		11p	BF195		ME4101	16p		65p	2N2219a	58p		46p	5 amp		7472	86p		8-69
AC187k 28		180	BF244	16p 87p	ME4102	175		205	2N2484	46p	2 amp 50v	490	100v 200v	54p	7473	49p		8-08
AC188 22	BC157	17p	BF254	16p	ME4103	16p		80p	2N2646	51p		56p		60p	7474	499		8.80
AC188k 28		16p	BFX29	84p	ME4104	16p		BO _p	2N2904 2N2904a	25p 30p		675	Triacs		7475	65p		8.28
ACY17 86		16p	BFX84	25p	ME6001	18p		88p -	2N2905a	88p	5 amp		2 amp 400v	70p	7476	55p 96p		8·58 8·87
ACY18 29		18p	BFX85	88p	ME6002	19p		18p	2N3053	280		-89	6 Am P	709	7481	\$1.47		2.42
ACY19 26 ACY20 23		13p 13p	BFX86	25p	ME6003	17p 19p		18p	2N3055	49p		·98	400v	90p	7482	\$1·10		2.78
ACY21 84		230	BFX87 BFX88	279 25p	ME6101 ME6102	205		64 p 68 p	2N3702	12p	400v #3 10 amp	-25	10 amp		7483	\$1.38		8-78
ACY22 19		\$1p	BFY50	23p	ME8001	190		85p	2N8703	11p		-45	400 v	\$1.30	7484	\$1.53		8-65
AD140 67	BC179	24p	BFY51	190	ME8002	81p		142	2N8704	12p		51	7400	20p	7485 7486	43-25 49p	74199 \$6	8-65
AD142 59		12p	BFY52	28p	ME8003	23p	OC84 2	261	2N3705	11p		95	7401 7402	20p 20p	7489	\$4.95		
AD143 52		11p	BFY84	897	ME9001	190		54p	2N 3706	11p			7402	20p	7490	820	1C's	
AD149 65		12p	BFY90	41-15	ME9002	187		Иp	2N3707	11p	Silicon	- 1	7404	21p	7492	84p	307 8 Pin I	
AD161 46 AD162 44		13p 15p	BY100 BY127	17p 17p	ME9003 ME9021	16p		77	2N3708	10p	Rectifiers	•	7405	21p	7493	82p		69p 38p
AD161) M/		15p	BFZ10	1/9 89p	ME90021	19p 18p	TIP32a 8 TIP33a 41-1	18p	2N3709 2N3710	11p 11p	IN4001	70	7406	44p	7494	\$1.04		88p
AD162 35		15p	BFZII	38p	MP8111	38p	TIP346 \$1.6		2N3711	119	IN4002	70	7407	44p	7494 7495	#1·04 #1·14		99p
AF114 80		18p	BFZ12	88p	ME8112	88p	TIP35a 48-1		2N3794	20p	IN4003 IN4004	89	7408 7409	26p 26p	7496	\$1.25	723c T099	
AF115 80		159	BY213	28p	MP8113	49p	TIP36a \$4 0)7p	2N3819	27p		97 105	7410	200	74100	42.05		1.10
AF116 80 AF117 80		14p	C407	19p	NKT211	29p		18p	2N2926	11p		iip	7411	36p	74104	41-28	741c DIL 741c 8 Pin 1	
		18p	MA8001	- 88p	NKT212	297	TIP42a #1-1		2N3904	17p		18p	7412	40p	74105	\$1.58		38p
AF124 29 AF125 29		14p 15p	MA8002 MA8003	40p	NKT213 NKT214	29) 27)	TIP295541.0		2N3906	17p		9p	7413	88p	74107	48p		38p
AF126 29		24p	MEO401	23p	NKT217	58p		iõp Iõp	2N4036	57p		LOp	7416	49p	74110	67p		94p
AF127 20		25p	ME0402	24p	NKT261	25p		2	2N4058	18p		10 1 20 1	7417 7420	44p 20p	74111 74118	\$1.62 \$1.80	748c DIL	54p
AF139 62		26p	ME0404	19p	NKT271	21p	V763 8	8p	2N4059 2N4060	18p 18p			7422	60p	74119	\$1.50	DIL	
AF239 66		24p	ME0404/1		NKT274	21p		1p	2N4061			70	7423	60p	74121	57p		
AF279 78		41p	ME0404/2		NKT403	77p		8p	2N4061 2N4062	18p 12p	PL4007 2	20	7425	45p	74122	\$1.60	Sockets	
ASY26 891 ASY27 501		40p	ME0411	22p	NKT404	72p		9p	2N5172	11p		8p	7426	45p	74128	\$3.15		20p
ASY27 50 ASY28 89		36p 49p	ME0412 ME0413	219 199	NKT603F	95p		őp	4N5192	895		07	7427	48p	74141	41-20		395
ASY29 42		890	ME0413 ME0414	190	NKT613F	41p 38p		8p 9p	40361	48p		lip 8p	7428 7430	79p 20p	74145	41-05		
BA111 82	BC441	892	ME0462	28p	NKT674F	880		25	40362	46p		Sp	7432	45p	74151	41-81	All Prices in	nel.
BA115 10		45p	ME0463	\$8 p	NKT677	80p		20	40636	690		50	7433	790	74143	\$1.48	of V.A.T.	
			Concession in the							-					-			-

68p \$1

Resistors	Veroboard	
1 watt 5% carbon 3.9 ohms to 10 meg 1p 1 watt 5% carbon,, 1p 1 watt 2% m/o 10 ohms to 1 meg 4p 2 watt 2% carbon 5.6 ohms to 10 meg 3p 3 watt wirewound 1 ohm to 8K8 ohms 10p 5 watt wirewound 1 ohm to 8K8 ohms 10p 10 watt wirewound 1 ohm to 8K8 ohms 13p	·1 ·16 24 × 34 269 239 24 × 5 81p 81p 34 × 34 81p 81p 34 × 5 81p 81p 34 × 5 85p 35p 17 × 24 93p 74p	Pin insertion tool 689 689 Spot face cutter 579 579
Volume Controls Potentiometers	17 × 38 41-38 41-18 17 × 5 Plain 41-10	Pkt 50 Pins 22p 22p
Carbon track 1k to 2meg Log or Linear Bingle 14‡9 Dual Gang Stereo 489 Single type with D.P. Switch 282	Electrolytic Capacitors	ALC: CAL
Bingle type with D.P. Switch 22p Miniature Presets Carbon Skeleton type All values 100 ohms to 5 meg ohms -1 watt 6p each -25 watt 7p each	100µF 6 p 330µF 10p	470µF 189
Neons fimm neou indicators Red or Amber at 6v, 12v, 28v, 110v or 230 volt. miniature neon lamps	6-8 VOLT 16 VOLT 33µF 6ip 15µF 6ip 68µF 6ip 33µF 6ip 150µF 6ip 150µF 6ip 470µF 11p 150µF 8ip	1000μF 22p 63 VOLT 2200μF 39p 1μF 6ip 5000μF 68p 2·2μF 6ip 6:8μF 6ip 6ip 6:8μF 0.0μF 68p 6:8μF 6ip 10μF 6ip 6ip 6:8μF
240v or 110v 6p each	680μF 18p 220μF 9p 1500μF 18p 680μF 17p	40 VOLT 22µF 61P
Biver Mica 360v DC, ± 1% Values in pFs 9:2 to 220pF, 11p; 250 to 820pF, (12p; 1000 to 1800pF, 17p; 2200pF, 19p; 2700, 3600-F, 24p; 4700, 5000pF, 43p; 6800pF, 44p; 8200, 10,000pF, 55p. Tantalum Bead	2200µF 18p 1000µF 17p 3300µF 28p 1500µF 25p 10 VOLT 2000µF 48p 22µF 61p 25 VOLT 47µF 61p 10µF 61p	6-8μF 6+p 68μF 10p 15μF 6+p 100μF 11p 38μF 6+p 150μF 18p 47μF 6+p 120μF 18p 68μF 10p 330μF 220μF 22p 68μF 10p 330μF 22p 22p 220μF 11p 1000μF 48p 22p
Bolid tantalum capacitors Tol ±20%. All values 20p each. MF/voltage: 1/35, 22/35, 33/35, 47/35, 1/35, 2-2/35, 47/35, 10/6.3, 10/16, 10/25, 22/16, 47/6-3, 100/3,	Ceramics Miniature Ceramics 50v D All values 1.8pF ot 10,000p	ю.
Mullards Polyester Capacitors CSB0 SERIES 250V F.C. mounting: 0·1µF, 0·015, 0·022 8ig. 0·033, 0· 0:68 159, 1µF 149, 1·5µF 359, 3·2µF 379. CSB0 SERIES 0:00Y: 0:001µF, 0:018, 0:002, 0:002, 0:004, 20, 0:005, 0		

400 ° : 0·001μP, 0·0015, 0·0022, 0·0035, 0·0047 8p, 0·0068, 0·01, 0·015, 0·022, 0·033 8ip, 0·047, 0·068, 0·1 4ip, 0.15 6ip, 0·22 8ip, 0·53 12p, 0·047 14ip, 1607 : 0·01μF, 0·022, 0·023, 0·033, 0·047, 0·068 3ip, 0·1 4p, 0·15 4p, 0·1 4ip, 0·15, 0·22 5ip, 0·33 7p, 0·47 9ip 0·68 12p, 1μF 14ip, 1·5μF 53p, 2·2μF 54p.

£1 BARGAIN PACKS 1 10 Billicon nym power transistors (2N3055), tested/un- marked. 1 30 Fissic FET's unmarked/untested. Bilmillar to 2N3019. 1 20 TOS transistors nym 2 to 5A, untested/unmarked. 1 20 TOS transistors nym 2 to 5A, untested/unmarked. 1 30 Flastic 2N3055, unmarked/untested. TO220 case. 1 30 Flastic 2N3055, unmarked/untested. TO220 case. 1 0 General purpose, fully tested PET's.
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THIS receiver accessory allows the reception of CW (Morse) and SSB (single sideband) signals particularly with receivers whose coverage includes any of the amateur bands. These bands are given below for the guidance of listeners who have not so far paid much attention to them.

160	metres	or	1.8	to	2·0MHz
80	metres	or	$3 \cdot 5$	to	3.8MHz
40	metres	or	$7 \cdot 0$	to	7·1MHz
20	metres	or	14.0	to	$14 \cdot 35 MHz$
15	metres	or	21.0	to	21 · 45MHz
10	metres	or	28.0	to	29 · 7MHz

Short wave broadcasts use AM (amplitude modulation) and an envelope detector in the receiver demodulates this but this detector cannot provide the wanted audio output with CW or SSB signals. CW will be heard as an intermittent clicking and SSB as an unintelligible sound varying at syllabic rate. To receive CW a signal from the beat frequency oscillator is combined with the carrier, provided by the CW transmission, the difference in frequency between BFO and CW signals providing an audio output after detection. As a superhet receiver converts all incoming signals to a frequency of, usually, about 470kHz (the intermediate frequency) the BFO is adjustable around this frequency. So if the BFO is set to 469kHz or 471kHz the CW is heard as a 1kHz audio tone.

With SSB the carrier and one sideband are suppressed before transmission. When the BFO is adjusted to occupy the position of the missing carrier the transmission can be resolved and the detector provides intelligible speech.

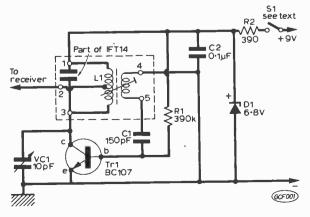


Fig. 1 : Circuit of the simple beat frequency oscillator.



BFO CIRCUIT

This is shown in Fig. 1. The frequency is determined by the coil L1, with fine manual adjustment by the variable capacitor VC1. The coil is suitable for receivers with an intermediate frequency of about 455kHz to 470kHz but the actual frequency need not be known. Windings must be in the phase shown, to secure oscillation.

It is quite a good plan to operate the BFO from its own 9V battery, the zener voltage regulator is not then necessary as satisfactory results can be obtained without it. But if current is taken from the battery running the receiver the current drawn by the receiver will vary considerably, especially at high volume level, so that stable operation of the BFO is impossible. In these circumstances, the zener is required for satisfactory reception.

ASSEMBLY

The components are assembled on a small piece of perforated board, Fig. 2, with wiring underneath. The two points MC are $^{1}_{2}$ in. 6BA bolts, with tags, providing the chassis or negative return.

A piece of aluminium about $3x1^{3}_{4}$ in is bent at right-angles about 1^{3}_{4} in from one end. The pitch capacitor VC1 is fitted to the smaller flange. The other flange is drilled for the two 6BA bolts mentioned, so that the wired board can be locked in place, with leads and joints clear of the metal. Connect the variable capacitor fixed plates to pin 3 on L1, and the moving plates to one MC tag, Fig. 2.

*	. 44	Su.	*
R1	390kΩ	VCI	10pF (Jackson C804)
R2		Tr1	BC107
C1	150pF /	* L1	Denco IFT14
C2	0.1µF	DI	Zener diode 6-8V
	1 " " " " "		
Per	forated board, a	bout 14	x #in. Knob. Metal cas
see	text. On/off swi	tch, see	text.
, 1884	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		*

TESTING THE BFO

components list

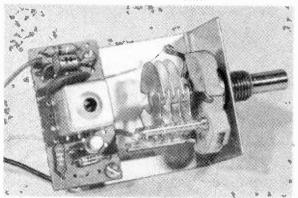
Set VC1 half open. Tune in any AM signal on the receiver. Place an **insulated** lead from pin 2 of L1 near the IF circuitry of the receiver. Connect the BFO to the 9V supply to be used. Rotating the core of L1 with a trimming tool should result in a setting being found where an audio tone arises. Set the core to the central or zero-beat position. If the core is rotated either way from this position an audio tone will be produced, rising in pitch as the core is turned.

Rotating VCl should now give a similar result. That is, a rising audio tone as the capacitor is rotated either way from the central or zero-beat position.

The BFO is not used for AM reception and slight re-setting of the core may be necessary after the unit is fitted in its case, if it is found that VC1 comes at the fully open or fully closed position.

BFO LOCATION

The BFO unit is only about $2l_4xl_4xl_2in$ so it may be fitted in almost any receiver, especially homeconstructed types. A reasonably large control knob is best on VC1 and an on-off switch is necessary in the battery positive lead to the unit.



The unit itself is very small indeed so it can be fitted into a convenient corner in any receiver requiring a BFO.

It may be preferred to have the BFO as an external unit, with its own battery, when it can then be used with any receiver. To avoid troublesome handcapacity effects, the unit must be in a metal box. A box about $6x3x2^{1}2in$ with a backplate fixed with self-tapping screws will be suitable. This will also take a 9V battery and switch.

COUPLING TO RECEIVER

A short insulated lead from pin 2 of L1, placed near the receiver or near the receiver IF stages, should normally give suitable coupling which is not too critical. Much looser coupling to the earlier IF

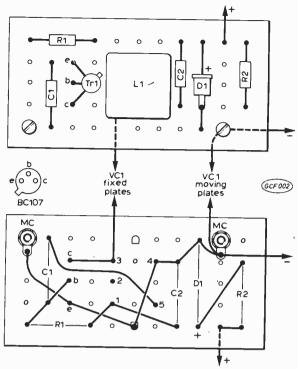


Fig. 2: Layout of components on top of the Veroboard and wiring beneath.

circuits will be required than to those at the diode end of the IF amplifier.

If coupling is too close, receiver sensitivity will fall off considerably when the BFO is switched on. Should coupling be too weak, strong SSB or CW signals will be difficult to resolve, while weak SSB or CW will be resolved easily. However, it should be an easy matter to move the lead from the BFO, or to cut it down, until results are satisfactory.

RECEIVING CW and SSB

Morse signals should be found easily in the amateur and other bands and VC1 is simply rotated to produce a suitable audio tone. In some cases rotating VC1 one side of the zero position may be found to give better reception than the other side.

To receive SSB, first tune in an amateur SSB signal, probably on 80m, with the BFO off. Switch the BFO on and rotate VC1 slowly until intelligible speech is produced. This requires quite careful adjustment. If the signal cannot be resolved, turn VC1 the other side of the zero position. This alternative position will in any case be necessary on the HF bands, where the upper sideband is usually employed compared to the lower sideband transmitted on the LF bands.

If the receiver is fitted with RF and audio gain controls, the audio gain should be near maximum and the RF control advanced as necessary, for best results on SSB.

VC1 need not be 10pF but larger values give more critical adjustment while smaller values may not give enough range of adjustment. Where the receiver has a fine tuning control this can be used for tuning SSB or CW signals, but if the receiver tuning does not allow very critical adjustment, VC1 can be used for this purpose, after locating the wanted signals.



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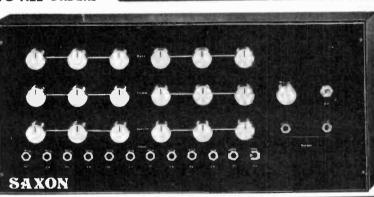
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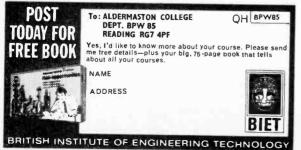
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wireless?

The early days of electronics were based very largely around the topic of radio. Things like computers and calculators are very much an afterthought. AMBIT is instigating a specialist sales and service line, just for AC electricity. From 10Hz to 1000 MHz. With our association with the largest producer of coils and filters in the world, namely TOKO, we think we have got a head start. Add to this our declared committment to linear monolithic technology, and the result is the most advanced and comprehensive service available to the amateur or industry.

In our AC line information folder, you will find the CA3090A PLL decoder, with TOKO coils and pilot tone filter, PCB and other bits for just $\pounds 3.90 + VAT$.

The CA3123E AM radio module, the CA3089E FM radio module, the TBA810AS short circuit proof 7W audio amp module. DATA FOLDA is 25p inc pp., and contains information for all concerned with audio and wireless - GET YOURS NOW.....





A^S we go through the Age of Apollo with everything rocketing upwards the prices of dry batteries are no exception. The common PP7 9 volt battery, for example, costs around 33p at the moment and many transistor radios use two of these. Their useful life in a radio is very variable but one factor, above all else, determines how economical they are likely to be in the long run: the sensible use of the volume control.

Just about all transistor radios use output stages designed to operate in what is known as "Class B" conditions, where the current consumption is very low with no signal, rising as the signal input is increased so that low volume levels mean low battery consumption and longer battery life.

At 66p for a pair of PP7s it is immediately obvious that a mains operated power supply unit is going to pay for itself very quickly indeed, after which the cost of the electricity to operate the set is negligible. Taking a month as a typical life span for the batteries the cost of this power supply unit at under £3 could be written off in about four months. For our Senior Citizens and others similarly placed this is no mean saving.

Design

While power units for radios requiring 6 or 9 volts are common enough, units to replace $2 \times PP7$ batteries (18 volts) seem hard to come by. In the author's case, an Ultra 6142 LW, MW and VHF

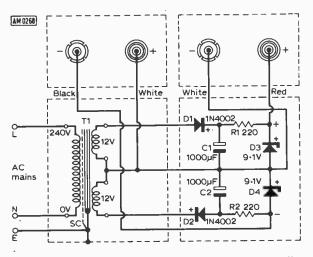


Fig. 1 : Circuit of the power unit together with the connections to the terminals of the retained battery tops.

ARTHUR DOW

portable, it seemed logical to make up a power supply unit to fit in the same space as the batteries, so what better than to use the tin cases from a pair of defunct PP7s?

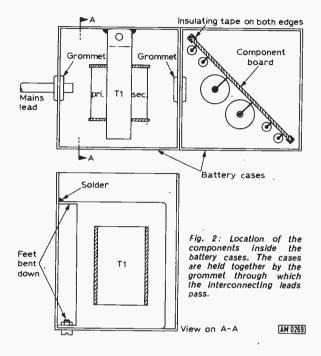
In the final circuit used, Fig. 1, one tin box carries the mains transformer T1, the 12 + 12 volts secondary windings going to the rectifier diodes D1 and D2, smoothing capacitors C1 and C2 and the zener diodes which stabilise the output voltage at $9 \cdot 1$ + 9.1 volts, all contained in the second box. The tops of the boxes carrying the terminals are retained and accept the original battery clips so that no alterations whatsoever need to be made to the radio set itself, a very important consideration. At any time the power unit can be slipped out of the set and normal batteries fitted back in a few seconds. In any other set a check ought to be made to with a voltmeter to ensure that the two batteries are, in fact, in series, requiring 18 volts. Otherwise, as long as the original battery polarities are adhered to, there should be universal use for this type of power unit.

Construction

Initially, two old PP7 type batteries are dealt with as follows: Mark the tops with the + and - signs, as shown on the side of the case, against the respective terminals. Cut across the corners at the top with a pair of sidecutters and ease back the edges until the top can be lifted out complete with battery. Cut the connecting wires or thin metal strips fairly close to the terminals and throw out the battery.

A hole of about r_{6} in diameter is made in corresponding positions in each case and the two cases held together with a rubber grommet, Fig. 2, noting the polarity markings on the cases. Another hole is made for the mains lead to enter, again via a grommet. The position of this hole will be dictated by the position of the batteries in the set. In the Ultra 6142 a slot was filed at the bottom of one side of the cabinet, adjacent to the battery compartment, from which the mains lead was led out.

Next, all the components, with the exception of the transformer, are soldered on to the small piece of veroboard, Fig. 3, and lead-out wires attached. Some sort of colour coding for the wires is an advantage to avoid wiring errors. The board is fitted across the diagonal of one box and a couple of spots of adhesive will hold it in place. Be particularly careful that the polarity of the four diodes and the smoothing capacitors is carefully observed. The wires from the board are passed through the grommet with the exception of the one white and one red wire which are soldered to the + and terminals on one of the battery tops.



The mains transformer has two mounting feet which must be bent down, Fig. 2, one being fixed to the bottom of the box with a 6BA nut and bolt and the other soldered to the box just below the top. But, before fixing the transformer finally, feed a few inches of the mains lead through the grommet and connect to the primary winding taking the earth lead to the transformer's "screen" connection and to the case. Put a few turns of narrow insulation tape on the end of the mains lead inside the box to prevent the lead being pulled out. This may not be the best arrangement but space is rather limited inside the box. The wires from the board may now be connected to the transformer secondary with a white wire and a black wire going to the terminals on the second battery top, again noting the correct polarity. The transformer may now be dropped into the case and finally fixed into position. Some insulation tape was stuck across the core of the transformer at the top to prevent any possibility of a short circuit of the terminals immediately above. Likewise some tape was put across the top edge of the board in the other box.

Testing

Before replacing the tops in the cases it is a good idea to try out the power unit for correct operation. After checking the wiring again and the polarity of the various components connect a DC voltmeter across the red and black terminals. Select a voltmeter range of, say, 50 volts initially. Switch on the mains, when a reading of about 18 volts should be

★ components list

R1/2 C1/2	220Ω 5% ½ watt 1000µF 25V	
D1/2	1N4002	
D3/4	9-1V zener (BZY88C9V1)	
T1	Transformer 240V/12V (Douglas MT111CS)	12V

obtained, with 9 volts between the white wires and either black or red.

If everything appears correct put some insulating tape over the connections to the terminals and put the tops back into the cases finally turning over the edges of the cases to hold the tops in position. If thought necessary, the unit can be checked on the radio itself before fitting the tops back, connecting the battery leads from the set on to the power unit terminals. If there is something wrong it can be attended to now instead of having to open up the cases again. As a further check, the voltage across each of the smoothing capacitors should be about 16 volts.

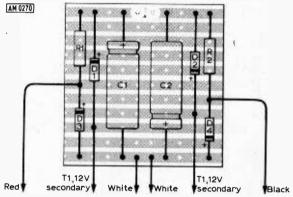


Fig. 3: Layout of components on small piece of Veroboard. Protect vertical edges and top with insulating tape or similar.

Notes

It should be remembered that the on/off switch on the radio set itself still only controls the DC output of the power unit to the set and not the mains input. Although the set consumes very little power from the mains it is still good practice to switch off the mains side when the set is not being used. The set switch can be left on permanently and operation of the set controlled by a switch at the mains outlet point.

The miniature mains transformer specified has a secondary current rating of 250mA which is far in excess of the 20/30mA which will be drawn by the average set. However, since it costs only a matter of a few pence more than the sub-miniature transformers rated at around 30/50mA the additional safety factor was thought to be well worth while. The light loading of the transformer will also assist the output voltage regulation of the unit.

If you're looking for trouble you needn't look any further.



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anything.



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Please send me the catalogue containing of test equipment.	ng the complete range
Name	
Address	· · · · · · · · · · · · · · · · · · ·
	PW







THE motor car is not an ideal environment for a tape player, or indeed for any electronic apparatus. In particular the problems of power supply regulation and electrical noise are far more acute than those likely to be encountered by a domestic machine.

ENVIRONMENT

The supply voltage, although nominally 12V, is likely to vary considerably under the loading conditions imposed by windscreen wipers and heaters, lights, etc. As a result we must produce a unit capable of working safely up to a possible maximum of around 15.5V, yet also maintaining a satisfactory performance down to 10V. For the amplifiers this is not too difficult—achieving a constant speed for the tape transport is not so straightforward.

Because a negative earth system is more or less universal on modern cars, the unit has been designed for this. Conversion to positive earth working is very simple, however, and will be described later: no change of components is required. Operation on 6V systems is not possible.

The construction of the tape-transport mechanism itself would of course be beyond the resources of the majority of our readers. It is therefore necessary to use a commercial mechanism. The one specified in the components list incorporates facilities for electronic speed control and also auto-stop and cassette ejection at the end of the tape. This feature is very necessary in a car where the machine must "look after itself" if the driver is fully occupied in manoeuvring his vehicle.

Interference from the car's electrical system seems to be worse with the modern alternator and solid-state regulator than it was with their predecessors. Power supply filtering and comprehensive screening are essential if the tape-head output, which is less than 500μ V, is not to be completely submerged in the hash.

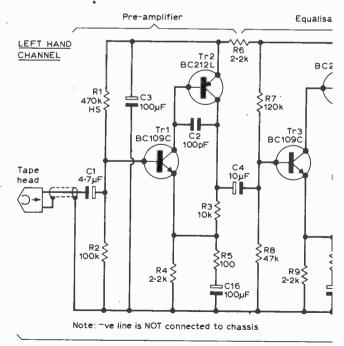
Acoustic noise levels in the passenger compartment vary considerably from one car to another. The amplifiers used here provide over 3W rms output into 4Ω loudspeakers from a 12V supply: this should be adequate for pretty well any car.

KEITH CUMMINS & TONY

TAPE AMPLIFIER

The amplifier system can be conveniently divided into three parts, a low-noise preamplifier, an equalisation section and a power amplifier. Silicon transistors are used in all but the power output stages.

A stereo cassette carries four tracks recorded on a tape only ${}^{1}_{0}$ in wide and running at $1{}^{7}_{0}$ in/sec. Hence the very low output level from the tape head. The amplifier input stage must therefore be designed for very low-noise performance. The technique adopted here uses complementary npn and pnp transistors, with the collector current of the first stage providing the base current of the second. The first transistor is thus operating under "starvation" conditions—a factor which greatly assists in the reduction of transistor noise.



PRACTICAL WIRELESS

some may not. It is a chance that the buyer takes.

leave the wires long. Only shorten them when you wish to fit them in permanently or in u.h.f. work, where obtain the correct connections for ing iron (15 watts max.) and hold the wire being soldered with wiring pliers. If you are experimenting Do not overheat; use a small soldermake sure that you know or can the specimen you have obtained. the length may be critical.

Some transistors require heatsinks. Take care and observe instructions regarding fitting, insula-

Transistor holders are available for many types and like i.c.s they are worth using in experimental projects, but it is always better to solder in for permanent use.

TRANSISTOR MOUNTING PADS

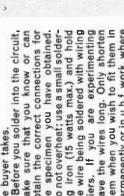
further provides a "seat" for the transistor to keep it clear of the hese often-neglected but very cheap little components are recomprotection against accidental knocks to the transistor when handling, and component assembly board, so ensuring that the wires are properly mended to give some measure of protected and insulated.

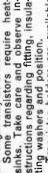
. A

TRIACS

When triggered, triacs will pass forward and reverse current; hence their use with a.c. The triggering voltage and current is important to an isolating 1:1 transformer for the achieve successful firing. Observe and mt2 with respect to the gate. Note that the triac does not isolate the high secondary voltage from the low trigger voltage. If used with a.c. the main terminal connections mt1 mains supplies it is wise to employ trigger signal.

PLUGS AND SOCKETS OR CONNECTORS

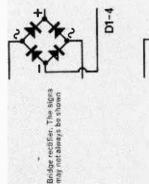


















COMPONENTS

CAPACITORS

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þ SK

Socket (SK) plug (PL) far single core screened

with the

the capacitance and sometimes the Colour coded capacitors can be identified by reference to the Practical Wireless Datacard No. 2 which working voltage and/or tolerance. was provided in the October 1973 Markings usually identify ssue.

Capacitance

Ч

Single plug and socket

catalogue. Directory entry on page 14

new and guaranteed at competitive prices. Send 10p for

> microfarads shown as μ F, mF, mfd.

nanofarads shown as nF, n, k, or kpf=1/1,000µF=1,000pF.

picofarads shown as pF, p, $\mu\mu$ F, mmfd=one millionth of 1μ F= 1/1,000nF.

Ч

Socket (SK) plug (PL) for coaxial cable (not BS)

ing voltage and shown as a number of volts d.c. (VWDC) or V d.c. or Voltage also known as the work-V a.c.

in applying a lower voltage, but the mum safe recommended voltage minals. There is no different effect stated voltage should not be ex-This value represents the maxithat should be applied to its terceeded.

supplied as substitutes, for example 0.47μ F instead of 0.5μ F or 0.022μ F instead of 0.02µF and so on. There ferred value" components to be is usually no detrimental effect by alternatives, as long as the specified substituting in this way with near It is quite common now for "prevoltage is not exceeded.

When using capacitors for a.c. mains (200 to 250V) such as for interference suppression, either a 270V (minimum) a.c. type or a 1,000V (minimum) d.c. type should oe used.

The insulating material between the metallic foil or plates gives the Dielectric



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SHELF-MANY SIZES **NSTRUMENT CASES** & CHASSIS OFF THE Send SAE for leaflet. 01-723 5891/723 7595 287/9 Edgware Rd, London W2 1BE H. L. SMITH & (Directory Entry P43.

mult x 1000000) CAPACITANCE CODE (BS 1852) Capacitors can be marked with their nominal value using figures and letters in place of the conventional code. The three multiplier $p = 10^{-13}$ $n = 10^{-6}$ $\mu = 10^{-6}$ mult x 1000) of the capacitance in FARADS. Becomes (mult x 1) etters in common use are:---: 330p (00 101 Nominal value 330рF 1000рF 4700рF 1⊿F 6-8µF colour ü

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PRACTICAL WIRELESS

capacitor specific properties (see text book on the subject). Generally the most suitable for r.f. applications are ceramic or silver mica types; for a.f. and h.f. use one of the plastic types; for space saving and smoothing, electrolytic types which, although more expensive, are more stable and reliable over long periods of use. Electrolytic capacitors break down after a few years and are number one suspect of capacitor failure symptoms. Paper types are now being superseded by plastics.

COILS

Ready made coils are usually designed for a specific application, hence they seldom carry any characteristic markings other than the makers code number. Unless their properties are known or can be measured accurately, there is little value in unmarked coils. If buy-ing coil formers or bobbins for winding your own coils, check that you order or ask for all parts, especially if a brass or dust iron slug is to be used to adjust the inductance in a tuned circuit.

DIODES

Because of the very small size of many diodes it is not always possible to mark them with the full type number. Some are marked with very small lettering that needs a magnifying glass to read it. One end of the diode body is usually marked with a + sign or a band of distinguishing colour, or maybe black or white; this indicates the cathode terminal.

Special types include "Varicap" or similar variable capacitance diodes. The capacitance effect changes with a change in the applied voltage. This type is now frequently used in radio and television tuners.

> Zener diodes limit the applied voltage to the specified level and are very useful for regulating low voltage d.c. supplies.

FERRITES

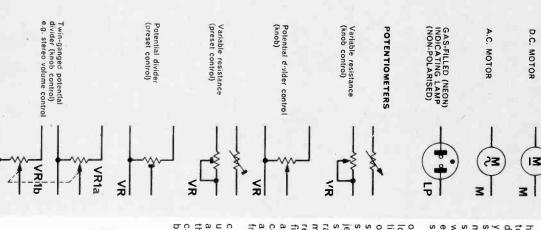
Often the cause of some misunderstanding, "ferrite" is a term now loosely applied, even mistakenly, to some kinds of dust iron materials and ceramic cores. Their properties are quite specific. Ferrite beads (used for suppressing parasitic oscillation) pot cores, rods and toroids are specifically designed to be most effective over a pre-determined frequency range. For more detailed information consult manufacturers' literature. When ordering pot core assemblies make sure that you ask for all the necessary parts, which usually include *two* halves of the pot, the bobbin, the clamps and tag strips.

HEATSINKS

and shape. If they are cast or moulded in aluminium alloy they properties. cause of inferior heat conductivity metals are not always suitable beare made from copper; alternative must be removed. Other heat sinks Any rough edges on drilled holes insulating washer and nylon fixings carefully achieved with the correct casing must, where required, be paint. Insulation from the transistor that the contact area is free from the transistor casing, make sure electrical connection is required to should be painted matt black, but it Heatsinks vary enormously in size

INTEGRATED CIRCUITS

In the limited space available it is not possible to give detailed suggestions on all types available; however, here are a few hints to observe.



BUYERS' GUIDE 1974/75

high, so many thousands of transistors (and other semiconductor devices) find their way into a scrap yard or on to the open market. In spite of precautions taken to minimise the number that are released, several do slip through, sometimes with makers' names on them. However, experts can often identify the source by internal inspection.

and obtain the correct specification and re-classified them, in which market as unmarked, re-marked or range. They usually appear on the spread adoption in a particular prooff projects, but it is unwise to from the supplier. case you should identify the coding recoded types. In the latter case, a side the specified characteristic ject because of the variations outout to be very good bargains; in a specity such devices for wideticularly for experimenting with onefirm may have measured a batch lot of cases they can be used, par-Sub-standard devices may turn

Unmarked devices cannot be Unmarked devices cannot be classified unless they are measured under normal operating conditions and with a proper instrument. For the low prices often asked, the buyer the low prices often asked, the buyer can expect to have a very mixed batch; some may be usable and



Directory entry on page 40

PRACTICAL WIRELESS

tained at low cost and in these cirtained at low cost and in these circumstances it is wise to measure the triggering voltage and current required to fire it. Also the "release" voltage should be measured.

TRANSFORMERS

Well made transformers are usually wound on cheeked bobbins. Cheap versions have no cheeks and often have flying leads connected to the windings.

Satisfy yourself that the physical size is large enough to handle the current expected to be passed through the windings, otherwise saturation of the core and subsequentoverheating could occur. This applies particularly to mains transformers and valve output transformers.

Mains transformers with a screen between the primary and secondary windings are recommended, to reduce problems from mains borne interference and high frequency transference. This screen must be earthed with the laminations.

TRANSISTORS

Many problems arising from the purchase of transistors are due to misunderstandings about their characteristics.

Transistors are made first, then measured and classified according to test measurements made on them. The result is a wide spread of characteristics, particularly on the gain (hrs) and leakage current (lco). Published data often give the range of gain for a particular type number. If transistors made for that

gan (nre) and leakage current(rco). Published data often give the range of gain for a particular type number. If transistors made for that type number have characteristics outside the quoted figures, then they are either classified into another appropriate type number or rejected. The reject rate is fairly

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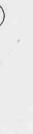








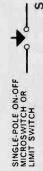


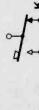


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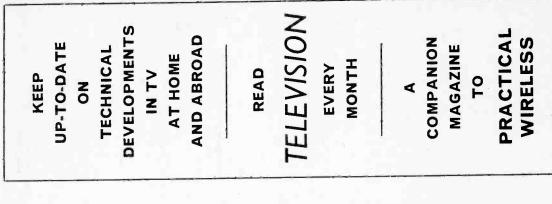
MORSE KEY

ion so you are entitled to ask for a a fault may be present on one of the fault does not interfere with your application. For example, you may buy a 7400 quad gate i.c. This device To be reasonably certain of get-ting a good specimen look for the manufacturer's official trade mark mens may not carry all this informa-'ull specification. Some sub-standard or "out-of-spec." items do able. However, it does happen that oin connections. If it is otherwise unctional it could be used if the but if one gate is faulty you may still was designed to contain four gates, as well as type number. Some speciappear and in many cases are usbe able to use the other three. It can sometimes occur that an assumed first grade i.c. may have an intermittent or faulty internal connection. If the device has been properly used in the circuit then the buyer could expect the supplier to replace it, unless it was declared as faulty at the time of purchase.

However, a problem arises immediately if the device has been soldered and there is no way of proving that the fault could have been there before it was soldered in or may have resulted from clumsy or overheated soldering. It is always wise to use i.c. holders for this reason and to make removal of the i.c. from the board easier. You cannot expect the supplier to replace a faulty i.c. if it has not been operated as recommended by the manufacturer.

Unmarked i.c.s or unidentifiable i.c.s are seldom worth having unless the supplier can offer some clue to the originally intended function. Even with test equipment it is almost impossible to ascertain the properties of such devices. Whatever i.c.s you buy always ask for a data sheet or obtain a copy

BUYERS' GUIDE 1974/75



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giving the expected specification. tors. This is most valuable for pin connection identification as well as from the manufacturers or distribu-

correct position; i.c.s can be costly and difficult to replace. have the correct device in in, until you are satisfied that you A golden rule is never to solder very the

PRINTED CIRCUIT BOARDS P.C.B.s are mainly of two kinds:

can melt the copper away. Small soldering irons (15 watt maxi-mum) should be used; larger irons ally where it is in narrow strips. lead to the copper cracking, especibending or flexing of any board can being more rigid and stable. Slight sive but is superior to s.r.b.p. board glass fibre board and s.r.b.p. Glass fibre board is more expen-

a fine toothed hacksaw. Glass fibre rapidly than s.r.b.p. tends to blunt the blade more A washing-up scouring pad or powder can be used with care. etching and again before soldering. When cutting the board always use must be thoroughly cleaned before tected and not tinned so the copper Most unetched board is unpro-

plane" side, the copper can be carefully and, a "ground-plane". The copper on clear of the copper on the "groundponents should be mounted just etched or peeled away from holes one side is etched to suit the circuit to avoid short-circuits. All com-Double-sided board is sometimes on the other (ground-plane) side to avoid short circuits.

some are able to supply etched boards for specific purposes and arrange Some Kits are available for etching p.c.b.s yourself. Read and follow the leave the bottle of solution open. instructions carefully and do not component suppliers to supply ready-etched a

24

boards to individual design requirements.

sary. knite or adding link wires as necescopper carefully with a sharp penbe done by either peeling away connection. Any modifications to to ensure a satisfactory soldered allowed where holes are required boards. Adequate copper must be printed circuit patterns for their the board after etching can easily constructors can etch their own projects where applicable so that Magazines usually publish the

POTENTIOMETERS

monly used for volume controls. bon tracks and can be obtained for vertical or horizontal mounting on exceeded trol, this rating should never be in particular with d.c. voltage conrent that can be safely handled, anc potentiometers determines the cur-The maximum power rating of all types have open unprotected cartrack resistance. Skeleton prese wirewound; logarithmic or linear ties to quote are: carbon track or resistance value, the other properous styles: Apart from the overall Potentiometers are made in vari-

RESISTORS

groups. The following information should be provided when ordering: tion will show many different (a) Construction material e.g. car-A look at the directory classifica-

- (b) Resistance in ohms, kilohms $(\Omega \times 1,000)$ or megohms $(\Omega \times 1,000)$ bon film, etc.
- The tolerance, e.g. 1%, 2% etc. <u></u>
- <u>a</u>c The power rating, e.g. 1, 1 watt etc.

by the resistor in conjunction with mum current that can be handled tolerance are important factors to the application. The power rating quoted is an indication of the maxiwhere low thermal noise and close are more expensive and are used adequate for the application. the applied voltage, and should be Some of the high stability types

SWITCHES

nut. The wafer specifies the switchtainable in kit form and it is essentia ing mode, which is described later. to ask for every part down to the last Common abbreviations used to Wafer switch assemblies are ob-

switches are: SP = single pole (one switch).

DP = double pole (two switches

3-pole = three switches operated operated simultaneously).

ST = single throw simultaneously, etc. ٩ on-ofi

DT = double throw or change runction.

4-pole, 3-way over function. tour switches each simultaneously, lets and operated having three out-

CO = changeover. usually on a wafer

MB

MB = make before break. **BM** = break before make.

Centre-off applies where a toggle or lever switch has two outlets and മ central neutral position.

THYRISTORS & TRIACS

triggering level which may be outbut in others they may be unreliable. The most common defect is the turers' published specification. In ways if they are not up to manutacspecimens may appear to function, some applications such low cost Thyristors can behave in various the manufacturer's quotec

2M2F signifies 2-2MΩ 1% 1K8G , 1-8kΩ 2% 120KJ , 120kΩ 5% 15RK , 15Ω 10% $F = \pm 1\%$ $G = \pm 2\%$ $K = \pm 10\%$ $M = \pm 20\%$ ting the nominal value of the resistor has a single letter added to it rep-resenting the tolerance figure:--Examples :--TOLERANCE. The marking indicaresistor, thus:--which replaces the decimal point when indicating the value of the 1.1 1.3 1.6 2.0 2.4 3.0 3.6 4.3 5.1 6.2 7.5 9.1 and their decades. 1.0 1.2 1.5 1.8 2.2 2.7 3.3 3.9 4.7 5.6 6.8 8.2 together with their decades such as 47 470 4700 47000 etc. single letter:---The multiplier is represented by a and tolerance using figures and of marking resistors with their value Increasing use is being made of the British Standards (BS 1852) method the E24 Series by adding the following The E12 Series can be expanded to intermediate values:--as the E12 Series:--mon range of twelve values is known. PREFERRED VALUES. The com-1K8G 120KJ 6R8M etters only instead of a colour code. 5-60 0 **RESISTANCE CODE (BS 1852)** R = x1 K = x1000 M = x1000000 150 18MΩ 47kΩ 1-2MΩ CAPACITORS (pF) **RESISTORS** (a) MARKING OF 330R 5K6 47K 18**M** 15R = ? (,, = x1) (multiplier = x1000) (multiplier = x1000) (mult = x1000000) AND (mult = x1000000)(multiplier = x1) 6-80 20% J = ± 5%

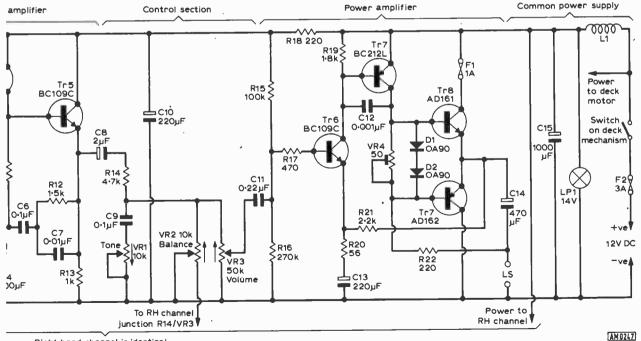


Transistor gain will vary from sample to sample and will also change with the supply voltage. To overcome these problems, negative feedback is used to stabilise the gain of the preamplifier.

The preamplifier has now raised the signal from the tape to a more reasonable level, but it still has a "Velocity characteristic"—that is, for every doubling of the recorded frequency the output level also doubles. This is because the tape head output level is proportional to the rate of change of magnetic flux due to the tape moving past the head. For a constant recorded amplitude, an increase in pitch of one octave (doubling of frequency) will cause the flux to change at twice the rate, and hence the output doubles also. It continues to double with each octave rise until tape head losses become significant at the higher frequencies. At the time of recording, the higher frequencies are pre-emphasised or boosted relative to the low and middle frequencies. This means that the signalto-noise ratio of the tape is improved, since tape noise is predominantly at high frequencies.

From the foregoing it is obvious why we need to have an equalisation amplifier. This has a characteristic which is the inverse or "dual" of the overall tape curve. The output of this section has a flat frequency response over the audio range.

At this point the signal is suitable for feeding into the power amplifier, which uses a conventional complementary-symmetry circuit. The output voltage can swing between the two supply rails, less the residual voltage drop across each output transistor, say about 12-2=10V. The rms equivalent of this peak-to-peak voltage is approximately 3.6V which will produce about 3.25W using a 4Ω loudspeaker.



Right hand channel is identical

amplifier board, plus common power supply. NOTE .-- The AD162 should be Tr 9.

★ components list

		AMP	LIFIERS		
Resisto	rS				
R1	470kΩ	R9	2.2kΩ	R17	470Ω
R2	$100k\Omega$	R10	10kΩ	R18	220Ω
R3	10kΩ	R11	47Ω	'R19	1·8kΩ
R4	2·2kΩ	R12	1·5kΩ	R20	56Ω
R5	100Ω	R13	1kΩ	R21 *	2·2kΩ
R6	2·2kΩ	R14	$4 \cdot 7 k\Omega$	R22	220Ω
R7	120kΩ	R15	100kΩ		
R8	47kΩ	R16	270kΩ		
R1 is	W High	Stability	. R22 is 11	N 5% Re	emainder
are ½V	V 5% car	bon.			1
Detent					
Potenti VR1		(
VR2	10kΩ lin.		with othe	r cnanni	el)
VR3					-11
VR4	50Ω hori	(ganget	with othe	r channe	eij
V 1 14	3032 11011	zomai pi	esei		
Capacit	ors				
	·7#F 6V T	ant.	C9 0·1µ	F Cer.	
C2 1	00pF Cer.			F 16V	
C3 1	00pF Cer. 00μF 16V		C11 0·22,		Cant
C4 1	04F 10V		C12 0.00	InF Cer.	
C5 10	00µF6V		C13 220/	F 10V	
C6 0	00µF 6V 1µF Poly			F 16V	
C7 0	·01µF Pol	y. (4F 16V	
	"F 10V		C16 100 µ	F6V	
Tant	- Tantalur	n bead	Cer - Dis	sc ceram	nic
Poly -	- Polyeste	r Rema	inder elec	trolytic	
- ·					
	nductors				
Tr1, Tr	3, Tr5, Tr	6 1	r8 AD16	1] mate	hed
	BC	109c 1	r9 AD16	2 ∫ pair	
Tr2, Tr	4, Ir/ BC	212L E	D1, D2 OA	90	
NOTE-	-The abo	ve comp	onents are	for one	channel
only. A	Il except	C15 an	d VR2 are	e duplica	ated for
the sec	ond chan	nel.			
Missolla					
Miscella L1 2A		or shell			
F1 1A	suppress	SUL CUOK	e; LP1 14	amp;	
FI IA	required	n chass	is-mounti	ng hold	er (two
F2 3A	fuse with		holdor		
			noider;	- Chore	a suitela

Cassette mechanism, Lenco FFR, Stereo with D.C. motor;

Veroboard 6.75 x 2.5in, 0.1in pitch; DIN connectors for loudspeaker outputs; 4Ω loudspeakers; metal case; mounting kits for Tr8, Tr9; knobs, etc.

MOTOR CONTROL BOARD

				- Dorana	-				
Resist	tors								
R51	2·2kΩ	R56	15Ω	R61	$100k\Omega$				
R52	6·8kΩ	R57	820Ω	R62	2·7kΩ				
R53	8·2kΩ	R58	560Ω	R63	680Ω				
	$1.5 k\Omega$		680Ω	R64	120Ω				
R55	3 ·9Ω	R60	4·7kΩ						
R55, R56 are $\frac{1}{2}$ W, remainder $\frac{1}{4}$ W \pm 5%.									
VR51 1kΩ miniature preset.									

Capacitors

C51, C52 22µF 25V Electrolytic

Semiconductors D51—D53 BA100 Tr51, Tr54 BC109 Tr52 AD162 Tr53 AC128

Miscellaneous

Mounting kit for Tr52; pcb.

The use of class B output with output transformers could, with correct design, yield 10 watts per channel if needed. However, we have to consider the size, weight and economics of the machine, as well as the problems of obtaining specialised components. The complementary output stage produces as much power as is likely to be needed for practical purposes, and all components are easily obtainable.

PREAMPLIFIER

The circuit of the complete unit is shown in Fig. 1. It will be seen that the signal from the tape head is coupled to the base of transistor Tr1 via capacitor C1. The biasing of Tr1 base is set by R1 and R2. Resistor should be R1, a low-noise, high-stability type, but R2, the lower leg of the bias divider is effectively by-passed by the low impedance of the head so far as audio is concerned, and is a normal carbon type.

The collector of Tr1 connects directly to the base of the complementary pnp transistor, Tr2. The base current of Tr2 and the collector current of Tr1 are therefore the same.

We can now consider the DC stabilising action of the circuit. If the current in Tr1 increases, so does the base current of Tr2. This change is amplified by Tr2 so that its collector current increases. Thus, more current flows through R3, which in turn connects to R4. The voltage drop across R4 is almost entirely due to the current flow via R3, rather than current in Tr1 which is operating under "starvation" conditions. An increase in the collector current of Tr2 therefore causes the emitter of Tr1 to move positively towards the supply rail. This is equivalent to a negative shift of its base bias and the collector current of Tr1 is so reduced. The change is amplified by Tr2 and this heavy DC feedback action stabilises the working point of the complete preamplifier. We do not need such heavy AC feedback—in fact

We do not need such heavy AC feedback—in fact appreciable AC gain is required. By decoupling R4 completely, a very high gain could be obtained, but it would be unpredictable and unstable. By introducing R5, the gain of the stage is set at about 100 by the ratio R3:R5 and is almost independent of voltage, temperature and transistor variations. The output from the preamplifier is therefore about 50mV. The supply to the preamp is decoupled by R6 and C3, and the output is coupled to the equalisation amplifier via capacitor C4.

EQUALISATION

The biasing method and stabilisation technique is the same as that employed in the preamplifier. However, an extra emitter-follower output stage is added which feeds both the Tone and Volume controls and the equalisation network comprising R11, C6, R12 and C7. The basic amplifier without equalisation would provide a gain determined by the ratio R10: R11, in this case, 200.

It is essential that the feedback network, which operates into the low impedance R11, should be fed from a low impedance source. If this were not the case, the response correction would be hopelessly inaccurate, as the network loads the source.

It will now be seen why Tr5, the emitter-follower stage, is included. It is DC coupled to Tr4 and provides a low impedance output. Basic correction for the velocity characteristic of the tape is provided by R12 and C6; C7 provides extra feedback to compensate for the tape pre-emphasis.

The equalised signal, which has now been amplified to around the 250mV level, is conveyed via C8 to R14 which is included to increase the impedance "seen" by the tone and balance networks. Resistor R14 forms the upper leg of a divider network, whose lower leg is formed by the Balance control VR2. This control operates differentially upon the two stereo channels, so that increased attenuation of one simultaneously results in an increase of output from the other. The tone control network consists of C9 and VR1. This is a simple "top cut" network which is adequate for use in the car.

Finally we come to the Volume control, VR3, which taps off the required output to drive the power amplifier.

POWER AMPLIFIER

The power amplifier consists of four transistors, Tr6, Tr7, Tr8 and Tr9. The latter two are complementary output transistors mounted on the backplate of the machine, which serves as a heat sink.

The action of the driver stage is similar to that of the previous amplifier. Transistor Tr6 has its base level set by R15 and R16. In this case, the level set is approximately half-way between the 12V rail and earth. Capacitor C12 is included to prevent RF instability, as is R17. The collector of Tr7 feeds the base of Tr8 directly, and the base of Tr9 via D1 and D2 and VR4, before reaching the collector load resistor R22.

Potentiometer VR4 sets the forward bias applied to the output transistors. In order to compensate for changes in temperature, diodes D1 and D2 are shunted across VR4. As the output transistors are germanium types, germanium diodes are used. When

the temperature increases (a condition which would cause increased conduction in Tr8 and Tr9) the impedance of the diodes falls, so decreasing the forward bias and stabilising the working conditions.

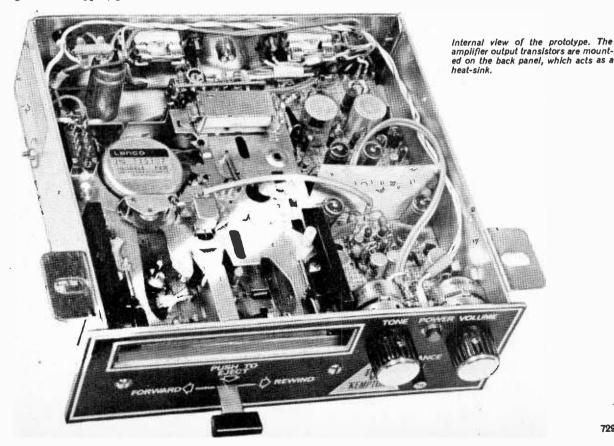
The emitters of Tr8 and Tr9 are connected via R21 to the emitter of Tr6, giving overall stabilisation of the DC working point of the amplifier. The emitter of Tr6 is decoupled by C13, and R20 is included to provide AC feedback in the ratio R21:R20, so stabilising the gain at around 40. If we consider a level of 200mV coming in from the volume control, this means we are just inside the overload point of the amplifier. The audio signal is coupled to the speaker via C14.

The loudspeaker also completes the DC return for R22 The audio output signal is in phase with that at the collector of Tr7 and hence there is positive feedback. This raises the input impedance of the output stage and enables the small transistor Tr7 to drive the output pair fully. This technique is known as "boot-strapping."

The output pair operate in class B. Forward bias is needed to prevent cross-over distortion, and VR4 is set up to provide a 10mA quiescent current measured at the fuse-holder. The fuse is connected in series with the collector of Tr8, to protect the output stage from conditions of gross overload.

The incoming supply from the vehicle is filtered by L1 and decoupled by C15. Power to the deck motor and panel light are also fed from this part of the circuit. The on-off switch is included as part of the tape deck mechanism.

The second part of the article describes the motor control circuitry and construction of the circuit boards.



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- (illustrated)
- 1. Coil
- 2. LSI chip
- 3. Interface chips
- 4. Case mouldings, with buttons, windows and light-up display in position
- 5. Printed circuit board
- 6. Keyboard panel
- 7. Electronic components pack (diodes, resistors, capacitors, etc)
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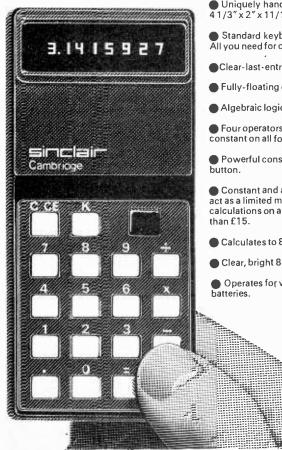
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- 4. Thick film resistor pack
- 5. Case mouldings, with buttons, window and light-up display in
- position
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- 7. Keyboard panel
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A series of simple transistor projects, using not more than twenty components.

NCE again we turn to that very useful integrated circuit, the SN7400, for a low-cost novel application, acting as the sensing circuitry for a photo detector. There are innumerable applications for this type of circuit. This particular one will operate in a multitude of roles without change to circuit layout or component values and possible uses range from burglar alarms to process control and object counters.

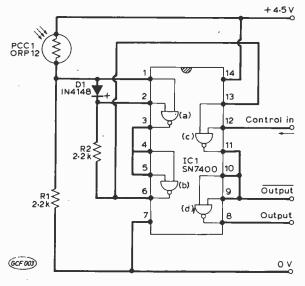


Fig. 1 : Circuit of the photo trigger using an SN7409.

Photo detector

The photo detector itself is a photo-conductive cell, PCC1, which forms part of a potential divider circuit with R1. When the cell is illuminated the potential at the junction of these two components rises to some positive level, the actual level depending on the degree of illumination and on the value of R1. As long as this potential exceeds +3V, with the power supply of 4.5V the circuit will work satisfactorily. To achieve this level it is necessary to use a reasonable level of light such as the focussed beam of a small torch. In the absence of illumination PCC1 becomes a very high resistance and the potential referred to falls towards zero.

The potential is applied to the input of a trigger circuit comprising ICI (a) and (b). Positive feedback is achieved by R2 in conjunction with D1. Even though the controlling potential may rise slowly the regenerative feedback action causes the output of gate (b) to change rapidly and the change occurs as the input voltage moves around the +2.5V level. There is a certain amout of hysteresis built in and this is set by the value of R2.

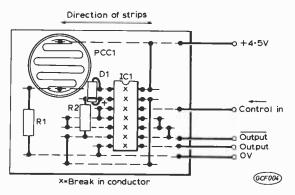


Fig. 2: Simple layout of the circuit using Veroboard.

The sense of the signal at the output of gate (b), pin 6 of the integrated circuit, is such that it rises to +5V when the cell is illuminated and falls to zero volts when the cell is obscured. We could have left the circuit at that stage and have said that the output was at pin 6; however we can make use of the other two gates within the integrated circuit to make the device more versatile.

Control operation

Firstly we introduce a control operation by means of gate (c). The control signal should come from a source impedance of $2k\Omega$ or less and should be a DC level of either OV or +4.5V. A control signal of OV will hold the output of gate (c) at +4.5Virrespective of what the photo detector might be sensing. We call the output signal at pin 11 the OUTPUT (NOT 'output') and use the final gate in the package (d) to invert this, thus, for the conditions stated, when the control signal is at OV the final output at pin 8 will be OV irrespective of the illuminating conditions. If the control signal is switched to +4.5V the output at pin 8 will be +4.5V when the cell is illuminated and OV when it is obscured. The OUTPUT signal at pin 11 will be the opposite of this.

Audio square wave

If desired, the control signal could be an audio frequency square wave. When the cell is in darkness the output at pin 8 will be zero volts but when illuminated the audio frequency will appear at the output. Should the control facility not be required pin 12 can be permanently wired to the positive supply rail. An advantage of having the complementary pair of outputs is that one can select the "bias" of the system; this is particularly useful if the output signals are to drive relays which may be required to be biassed either "ON" or "OFF".



CONTROL PANEL

Front panel 9 3/4 x 4 1/4 x 16swg aluminium

Dial backplate cut from

5³/₄ x 1"x 1" aluminium angle

The layout of the prototype control panel is shown in the photographs. Since all functions are DC controlled the layout is not critical and can be altered to suit your own requirements. Also, as mentioned earlier, any features which you do not require may be omitted.

The manual tuning drive was constructed on a framework built mainly of aluminium angle, as shown in Fig. 8a. Details of the drive-cord arrangements are given in Fig. 8b.

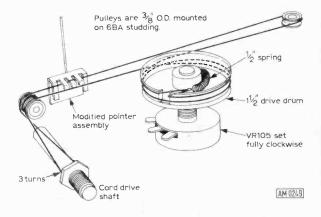
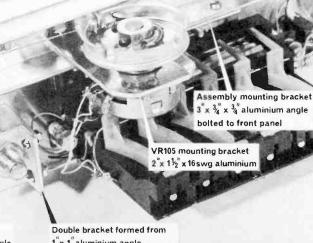




Fig. 8b: Drive cord stringing arrangements. The pointer assembly is modified by trimming the ends of the carriage to clear the pulley mountings and also inverting the pointer on the carriage.

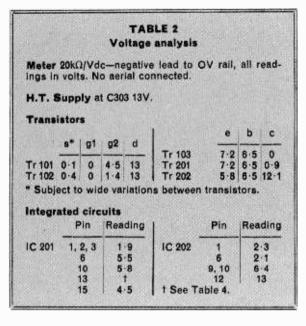


Pulley mounting bracket $5\frac{3}{4}$ x $\frac{5}{8}$ x $\frac{5}{8}$ aluminium angle (cut-out to clear drive cord)

1"x 1" aluminium angle (space to suit cord drive shaft)

AM 0248

Fig. 8a: Construction of the prototype tuning and dial drive.



INITIAL TESTING AND SETTING UP

Before any RF adjustments are made it is wise to check the DC conditions at each stage in turn. A construction error or a faulty component is likely to produce an incorrect voltage in an associated part of the circuit. Table 2 shows the voltages to be expected at important points in the circuit when measured with a 20,000 ohms per volt meter, on the range most appropriate to the voltage to be measured.

Switch on and check the voltages appearing in the front end and oscillator stages. If they are correct connect the meter, on its $2 \cdot 5V$ or 3V range, to the positive end of VR104 which should be adjusted until a reading of $2 \cdot 0V$ is obtained with VR105 at minimum and S101 switched to Manual.

Now solder in R205 to apply power to the IF section and check the voltages against Table 2. Follow the same procedure with the demodulator and stereo decoder integrated circuits to complete the initial testing. The voltage appearing at pin 15 of IC201 indicates the strength of the signal at its input. A high reading here could indicate that a programme is being received or that there is some instability in the IF section. If rocking the tuning control does not reduce this voltage to the correct level, check that all the IC201 decoupling capacitors and the link joining the top and bottom earth planes are in place.

ALIGNMENT

When all the DC tests have been completed satisfactorily you are ready to move on to the final stage of construction, aligning the receiver. Connect two lengths of screened wire to the Left and Right audio output pads ready for attachment to the output socket. Remove the temporary earth wire and mount the receiver in the die-cast box. The earth connection is now made via the mounting stud in the power supply section of the pcb.

Connect a short length of wire from the centre pin of the aerial socket to L101, as shown in Fig. 7, and solder the audio output leads to the 5-pin DIN socket (Fig. 9). If your audio amplifier is earthed via its mains plug, avoid hum loops by breaking the earth connection between the tuner and the amplifier (which is made by the screen of the audio connecting lead) at a convenient point.

RF/IF ALIGNMENT

The method of alignment adopted depends on the facilities available to the constructor. Two methods are therefore proposed; the first requires the use of a VHF signal generator but the second needs only another, aligned, FM tuner.

FIRST METHOD

Short out the oscillator coil, L106, with a crocodile clip and connect the signal generator to the 'hot' end of L104. The output level of the generator should be set to about 1mV and the frequency set to the nominal centre frequency of the particular ceramic filter used. The filters are graded into batches of varying centre frequency, each frequency being identified by different colours. Table 3 lists the frequencies and their corresponding colours.

If a signal strength meter is not included a high impedence multimeter should be connected to pin 13 of IC201. By varying the frequency of the generator slightly about the nominal value it should be possible to detect a deflection on the signal strength meter or the multimeter. Once this has been found the core of the mixer load coil, L105, should be adjusted until maximum deflection is obtained. This circuit has a low Q so the peak is very broad.

Leaving the generator frequency unchanged remove the dustcore of L202. The tuning meter should now show only a slight deviation from the null position. Screwing in the core will make the tuning meter give a large deflection to the right, pass through the null position and deflect to the left before returning to the null.

This demonstrates the S-shaped curve of the detector, the correct position for the core being that which resulted in the null between the two large deflections. Slight variation of the generator frequency on either side of the null should now produce deflections of the tuning meter to the left and right.

To align the front end, first remove the clip from the oscillator coil and set the tuning voltage to the low end of its range. Sweep the generator frequency slowly over the range 80-100MHz when a deflection should be observed on the tuning meter or multimeter. Once this has been located, set the generator to 88MHz and separate or push together the turns on the oscillator coil to produce a maximum deflection again. Then transfer the signal generator to the tuner input and maximise the deflection by adjusting L101, 102, 104. As the signal strength reading increases, the output of the signal generator should be backed off to avoid overloading or oscillator pulling.

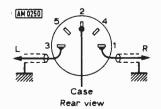
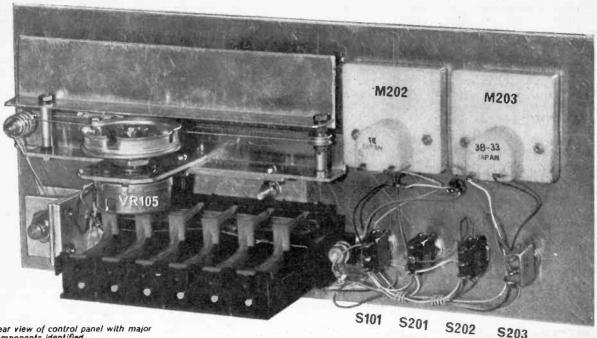


Fig. 9: Audio output connections to match DIN Standard amplifier Input socket.



Rear view of control panel with major components identified.

Next change the tuning voltage to maximum, increase the generator frequency to 105MHz and restore its output to 1mV. Vary the generator frequency about 105MHz until a signal strength meter deflection is obtained and bring this to a peak at this frequency by adjustment of VR101-103. The alignment at the bottom end of the scale does not have to be altered as the two adjustments do not interact when done in the manner described.

SECOND METHOD

This method may be used by those who do not have access to an RF signal generator. A second FM tuner, which must have an IF of 10.7MHz and a tuning meter, is used both as a signal generator and as a monitor to check the frequency of the local oscillator of the tuner which is being aligned. Connect a loop of wire to the aerial input of the second tuner and place it in the proximity of the oscillator of the first. Set VR105 to its low-voltage end and adjust L106 until the local oscillator appears as a carrier at 98.7MHz on the scale of the second tuner.

Now reverse the situation with the wire loop feeding the first tuner and the second tuner set to 88MHz. Adjust the tuning control of the first tuner until the tuning meter (or a multimeter connected as in the previous section) gives a deflection, indicating that the local oscillator of the second tuner is being received. L105 is now adjusted to maximise the response and L202 is adjusted as described in the previous section.

It now remains to align the RF circuits. Disconnect the wire loop and connect a good FM aerial. The sensitivity of the tuner is such that some stations will be received even if the RF stages are not correctly aligned. Set VR101-103 to maximum voltage and tune in a signal near the bottom of the band (the local Radio 2 transmitter will usually be the most suitable). Now adjust L101, 102, 104 to produce maximum response on the signal strength meter.

Adjust the presets VR101-103 with a signal towards the top of the band, a local radio station for example.

DECODER ADJUSTMENTS

The alignment of the stereo decoder is very simple and requires no special equipment. With the receiver tuned to a stereo transmission the core of L203 is screwed in until the stereo indicator illuminates. The lamp will now remain illuminated over a range of several turns of the core and the correct setting is at the middle of this range.

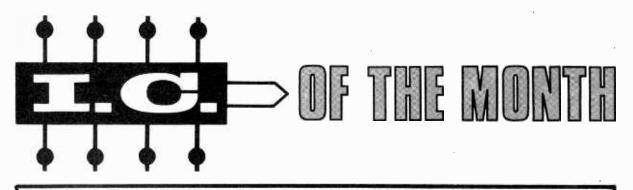
The precision of this setting may be increased by use of the BBC test tone transmissions on Radio 3 each evening after the end of normal broadcasting. These transmissions include a tone in one channel only. With the tuner connected to an amplifier and speakers, the speaker of the channel with the tone should be disconnected and the setting of L203 varied to give minimum signal in the other channel.

USING THE TUNER

We would like to conclude this series of articles with a description of the tuner in use so that constructors can check the operation of their receivers and get the best use out of them.

The operation of the tuning meter is straightforward. The centre-zero meter should give a slight deflection to the left (low frequency) with no signal present. As the receiver is tuned through a transmission from the low frequency side the meter will deflect strongly to the left, pass through zero and then deflect to the right. The correct tuning point is at the central zero. For maximum accuracy, tuning should be carried out with the AFC off.

If the centre-zero tuning meter is omitted from the tuner the signal strength meter may be used as a tuning indicator by simply tuning for the maximum deflection. This method is, however, not as accurate. Table 4 shows the voltage at pin 13 of



Number 49

SGS TBA 790 AUDIO POWER AMPLIFIER

THE TBA 790 is an audio power amplifier integrated circuit available in various forms which have absolute maximum voltage ratings of 12, 15 and 18V and respectively providing maximum output powers of 1.2, 2.2 and 3.45W into an 8 ohm loudspeaker.

The TBA 790KSD

In this article we will discuss the TBA 790KSD device which has an 18V, 3 45W rating, having the type of encapsulation shown in Fig. 1. The bracket is permanently attached to the back of the device, acting as a small heat sink. The bracket contains two holes, tapped 6BA, by which it can be fastened to a larger additional heat sink. For most applications at normal room temperatures the additional heat sink is not required. However, the constructor will often find it convenient to bolt the device to a sheet of metal and this will help to cool it.

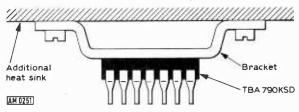


Fig. 1. The integral bracket of the IC provides the normal heat sink for the TBA 790 series.

The pins of this IC are in the quad-in-line configuration, the connections being shown in Fig. 2. Constructors are advised to solder directly to these pins, partly because sockets for quad-in-line devices are not easily obtainable and partly because the use of a socket renders spurious feedback more likely.

Circuit

A simple circuit for the use of the TBA 790 is shown in Fig. 3. The input impedance of the device itself is very high, typically 50 M Ω , and the circuit input impedance is therefore normally determined by R1. The high input impedance enables the circuit to be used with ceramic record player cartridges.

As the value of R2 is reduced, the amount of negative feedback decreases and the gain rises, being equal to 8000/R2. Thus if R2 is 100 ohms, the voltage gain is 80 or 38dB. R2 should not be less than about 39 ohms where the voltage gain is 200

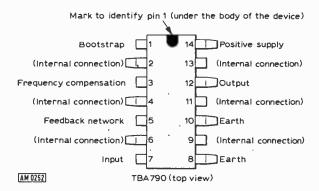


Fig. 2: Pin connections for the TBA 790. The heat sink is omitted for clarity.

or 46dB, since instability is likely at very high gain. The value of R2 should not, generally, be greater than about 200 ohms.

Frequency compensation

The components C2 and C3 provide frequency compensation. Ideally their values should be chosen according to the graph of Fig. 4, although these values are by no means critical. One should therefore estimate the gain required and then ascertain the value of R2 in Fig. 3. The value of C3 can then be read from the left hand side of Fig. 4 and the value of C2 from the right hand side of Fig. 4.

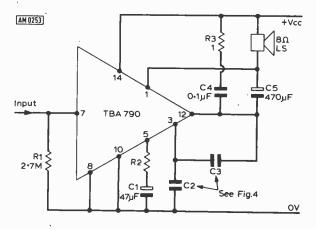


Fig. 3: Basic circuit of the TBA 790 as an audio amplifier.

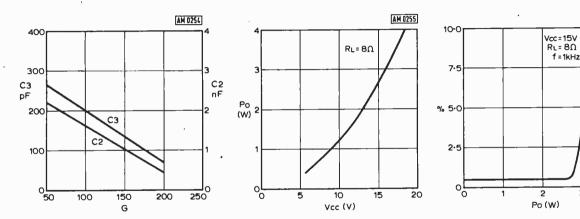
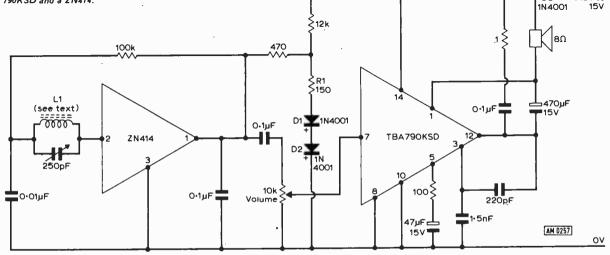


Fig. 4: above, graph for selecting values of C2 and C3 in Fig. 3. Fig. 5: centre, output power related to supply voltage. Fig. 6: right, distortion level at various output levels.

Fig. 7: below, is a practical circuit of a radio receiver using the TBA 790KSD and a ZN414.



Power supply

The maximum output power which can be obtained from the TBA 790KSD at various supply voltages is shown in Fig. 5 where an 8 ohm loudspeaker is employed. In general it is wise to regard the maximum power supply voltage as about 16V to allow a small margin of safety.

It can be seen that an output of just under 2W can be obtained when the device is used in a 12V, car radio, although more than 2W should be obtainable when the battery is being charged.

The quiescent current is only about 10mA at 15V or 7mA at 10V, but it will rise to around 1 to 3A when 3W is being delivered to an 8 ohm speaker. The efficiency (output power/input power) is typically 65 per cent at the 2.7W level.

The circuit shown has a frequency response which is 3dB down at about 70Hz and at about 12kHz. The use of a capacitor of larger value for C5 of Fig. 3 will extend the bass response, whilst the high frequency response can be altered by changing the value of C2 or C3.

•The components R3 and C4 of Fig. 3 compensate for the speaker inductance.

The total harmonic distortion is plotted as a percentage against the output power in Fig. 6 for a 15V supply and an 8 ohm speaker. It can be seen that the total harmonic distortion is fairly constant at a fraction of a per cent until the power exceeds about 2.6W. It then rises rapidly with the onset of clipping to about 10 per cent at 3.4W.

Typical use

The writer has used the TBA 7905KD as the output stage of a very simple radio receiver employing the well known Ferranti ZN414. The circuit is shown in Fig. 7. The voltage gain of the audio amplifier has been set at about 80 which has been found to provide good volume. The two diodes D1 and D2 are forward-biased silicon diodes which stabilise the ZN414 supply voltage. If these diodes are replaced by a resistor, the receiver will not function satisfactorily over a range of supply voltages. The gain of the ZN414 circuit can be adjusted by altering R1, reducing it in value or removing it altogether if the ZN414 stage oscillates.

The diode D3 in the supply lead is included to prevent the destruction of the TBA 790 if the power supply is accidentally connected with the wrong polarity. It may be omitted if desired.

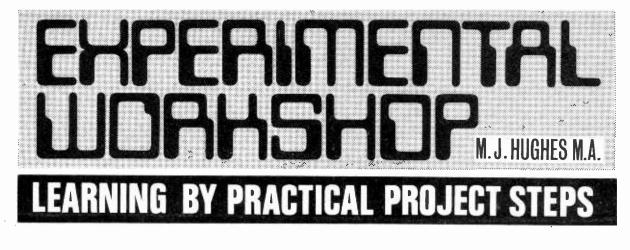
The coil L1 consisted of about 80 turns of 28 SWG enamelled copper wire close wound on a 4in. long ferrite rod. A long-wave coil of around 220 turns of much finer wire could be placed at the other end of the rod and switched into circuit to replace L1 if long wave reception is required.

AM 0256

3

D3

+12V to



PART 13—PHASE SHIFT CIRCUITS

THERE is more to a top cut filter than an attenuation factor, as described last month. Apart from the potential divider effect of the resistor and total circuit impedance on the input voltage, the circuit introduces what is called Phase delay. This means that when a sine wave signal is applied to the input we will see an attenuated sinewave at the output but the peaks and troughs of the wave will not occur at the same instances of time. To confuse the issue, the time discrepancy between input and output depends on the frequency of the signal we apply. This is not an easy feature to demonstrate without an oscilloscope but we hope the following experiment, coupled with a bit of thought, might clarify the situation a little.

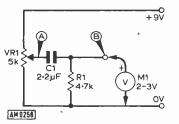


Fig. 90 : Experiment to show phase shift in a top cut filter.

In Fig. 90 we shall simulate an AC input signal by moving the wiper of VR1. Because we are limited to slow movements (low frequencies) we shall have to use a suitable high value capacitor for C1 so that useful signals can be measured on the meter M1. This meter must be sensitive, 20,000 ohms per volt, and switched to a low DC voltage range, about 2 or 3 volts. The voltage at "A" will be set by the potentiometer and can be anything in the range of 0 to +9V. We can, with a bit of manual dexterity, make this voltage follow a near sinusoidal pattern; to do this, start with the wiper at minimum voltage and rotate it, slowly at first, reaching a maximum speed of rotation at the half way point, then start to slow down gently until you reach the top end of its track. You should aim to slow down progressively, so that you don't suddenly stop when you reach the top. Having reached the top, peak positive voltage, immediately start turning the knob the other way, slowly at first, speeding up to the halfway point and

then slowing down as you reach the bottom end, again without an abrupt stop. This needs a bit of practice but it is not as difficult as it might at first appear. If you manage to do this satisfactorily the voltage at the wiper should approximate to a sine wave and if repeated over and over again should produce a waveform something like that shown in Fig. 91.

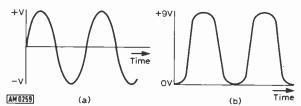


Fig. 91 : (a) Ideal sine wave oscillating about zero volis. (b) Approximate waveform from Fig. 90, oscillating between zero and +9V.

The thing to do now is to monitor the voltage at point "B" on the circuit as you go through the "sine wave" cycle. Initially make the cycle stretch over about two seconds and watch the meter closely. During the slow portion of the rising waveform the meter will read virtually nothing but as you speed up at the halfway point the meter voltage will rise. As you pass the halfway point and slow up towards maximum you should see that the meter voltage

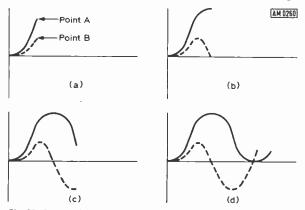


Fig. 92: Progressive construction of waveform obtained in Fig. 91 (b).

starts to fall back to zero and reaches zero just as you reach maximum voltage. The voltage you see on the meter should be proportional to the **rate** at which the input signal was changing. If you had an oscilloscope the output voltage would trace out the line shown in the progressives of Fig. 92.

When you turn the potentiometer in the opposite direction, describing the negative half of the input sine wave, the meter will try and read backwards so reverse its leads and you will find that a similar effect is produced in a negative direction. If you repeat this cycle many times you can imagine that the voltage at point B has the same sinusoidal shape as that at A but it is reduced in amplitude (attenuation by top cut filter action) and it reaches a positive peak as the input voltage is going through the centre part, the fast moving part, of its positive going swing. The voltage at B is zero when A is peak positive. maximum negative when A is moving in a negative direction and zero again when A is at its peak negative, zero volts, level. The final trace in Fig. 92 clearly shows that the voltages at B are out of step with those at A by a quarter of a wavelength.

Because a complete wavelength of a sinewave is a cyclic event we sometimes say it corresponds to a 360° cycle hence we can say a quarter of a wavelength is 90°. Using this nomenclature we can say there is a 90° phase shift between the input and output signals for this circuit, at the low frequencies we are considering.

If you had a signal generator instead of a potentiometer as an input signal and a double-beam oscilloscope monitoring the voltages at A and B you would see this more clearly. You would also see that if the frequency of the input signal were increased the amplitude of the output would increase but the phase shift would also start to reduce. As the input signal frequency becomes very high the phase difference approaches zero and the output becomes an almost exact replica of the input, both in phase and amplitude.

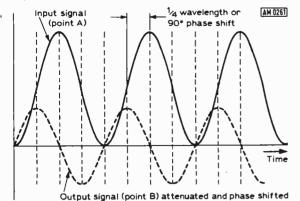


Fig. 93: Curves showing 90 phase shift of LF signal through top cut filter.

We can thus say for a top cut filter:---

1. At very low frequencies we get 90° phase shift and heavy attenuation, Fig. 93.

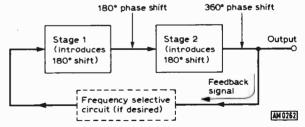
2. At very high frequencies we get no phase shift and little attenuation.

3. At intermediate frequencies we get a graded scale of phase shift (between 0° and 90°) and graded attenuation, depending on the frequency we choose, and, of course, on the values of the components in the filter.

This phase shift effect can be put to good service in certain types of oscillators. To obtain oscillation all we need is an amplifier with frequency selective positive feedback. This means that we have to take the output of the amplifier and at a certain frequency feed it back to the input with a phase relationship that enhances the output.

We have seen several examples of the opposite effect in amplifier stages, previously described in this series. Negative feedback was achieved by feeding the signal from the collector of a transistor back to its base. A single transistor stage, in grounded emitter configuration, has 180° phase shift between its input and output, when the input moves positive the output moves negative and vice versa. To get positive feedback we must arrange to feed back a signal that is in phase (i.e. having zero or 360° or any multiple of 360° phase shift).

One simple way of doing this is to use two transistor stages, one cascaded into the next. The output of the second stage will be 360° out of phase with the input to the first and this is equivalent to there being no overall phase shift. If we feed the output signal back to the input the circuit will oscillate at a frequency set by any frequency dependent components, capacitors or inductors, that form part of the loop, from input to output and back to the input again. If there are no such frequency sensitive devices and the amplifier is DC coupled then the oscillator becomes locked in one or two possible states (it tries to oscillate at zero frequency!!). This circuit is, in effect a bistable which has been described in a previous part.



This block diagram shows concept o an oscillator, producing zero phase shift, gain and frequency selective feedback.

For regenerative feedback to occur, a pre-requisite for oscillation, it is necessary for the gain of the amplifier to equal or exceed any signal losses in the feedback path. Positive feedback alone is not sufficient. We can turn the two transistor stage into a free running oscillator as shown in Fig. 94. The capacitors determine the frequency and, if looked at from a different view point, this circuit is very similar to a free running (astable) multivibrator. Changing the value of the capacitor in the feedback loop changes the frequency of oscillation; you can try this and, with the values given, the frequencies should be in the mid-audio range. Layout shown in Fig. 95.

If we accept that we can get 90° phase shift from a simple RC filter it might seem that two such filters cascaded into one another Fig. 96(a) would give us 180° phase shift. This would be true of signals of zero frequency but, apart from zero frequency being a rather impracticable concept when dealing with oscillators, the attenuation would be infinite and no measurable signal would be seen at the output. If, however, we extend the logic a little and consider three such filters connected together (Fig. 96(b)) there will be a specific frequency that undergoes 60°

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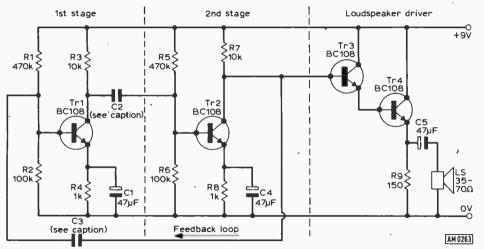
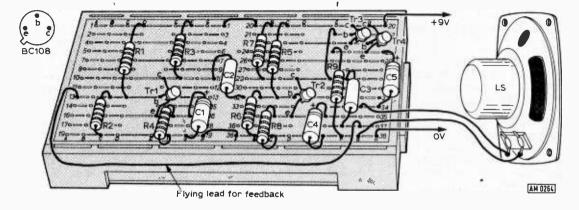


Fig. 94: Two stage amplifier converted to an oscillator, frequency being determined mainly by C2 and C3.



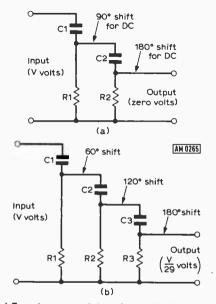


Fig. 96: (a) Two stages cascaded as shown will give theoretical 180° phase shift at zero frequency. (b) With three stages each stage will give 60° shift at a certain frequency giving 180° shift overall.

Fig. 95 : Layout for Fig. 94. Try values of 1000pF to $0.47\mu F$ for C2 and C3 in any combination.

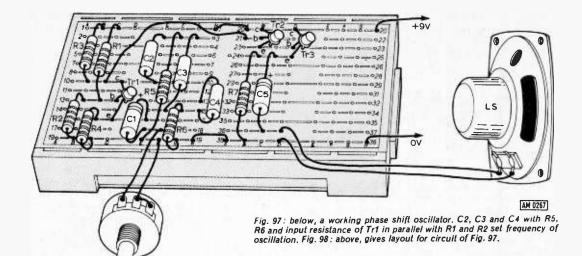
phase shift through each of the three stages. Three lots of 60° shift give 180° shift overall but this time we are no longer dealing with zero frequency; it will be a finite frequency and although there will be considerable attenuation it will certainly not be infinite and we can guarantee at least some measurable signal at the output for this particular frequency.

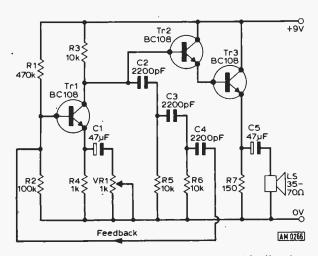
It can be shown that if each of the resistors in the three stage filter have values R (in ohms) and the capacitors are of equal value C (in farads) the frequency that is subjected to 180° phase shift is given by:—

$$f = \frac{1}{2\pi CR \sqrt{6}}$$

Because of the inter-relationships of impedance, reactance and frequency the attenuation for this circuit at this particular frequency is always a factor of 29.

We can now conceive using this network to replace the second transistor in our experimental circuit, to give 180° phase shift instead of the second transistor and simultaneously determine the frequency at which this phase shift occurs. By using this network in the feedback path of a single transistor stage we should be able to get regenerative feedback at a predetermined frequency provided that the voltage gain of





the single transistor stage exceeds 29. Ideally the gain of the amplifier should be greater than, but as near to 29 as possible, otherwise clipping will occur and providing the gain is just right the oscillator will produce a very pure sinusoidal output waveform. VRI introduces a controllable amount of negative feedback and thus sets the gain of the amplifier, Fig. 97. Start with this set to maximum resistance and no oscillations will be heard in the loudspeaker; as it is reduced in value a pure note will be heard and reducing its value to zero will provide zero negative feedback, maximum gain, and some distortion might be heard in the loudspeaker as clipping starts to occur. The latter effect will depend on the transistor latent gain. Layout is given in Fig. 98.

This is a very useful and simply made oscillator for audio and sub-audio frequencies and is sometimes used for generating low frequency vibrato signals in electronic organs as it has a comparatively pure signal content. The only problems are that the gain of the amplifier needs setting carefully for optimum performance and that it is rather difficult to change its frequency of operation with a variable control. Small changes in frequency can be provided by varying the value of one or two of the resistors in the feedback loop by small amounts. The best way of setting the frequency to a predetermined value is to leave the resistors fixed and substitute different sets of capacitors in the feedback circuit.

Phase shift has many other useful applications in electronics and it can be obtained in other ways. Under some circumstances it can be detrimental and is sometimes encountered unexpectedly in audio amplifiers giving rise to undesirable spurious oscillations.

Next month: Some more applications of positive feedback.

P.W. SANDOWN—continued from page 735

IC201 measured for various signal strengths for a typical tuner. This information may be used to calibrate the signal strength meter if required, although quite wide variations can be expected between tuners.

With the muting or squelch switched off there is considerable inter-station noise and the usual distorted output as the signal enters the edge of the tuner passband. With the squelch in operation the background should be silent until a noise-free signal is received. It should normally be left on unless a weak signal is being received.

-32 - 593	BLE 3	TABLE 4 Signal strength meter indication		
	centre encies	Voltage at Pin 13,	Approx. signal level	
Colour code	Centre frequency (MHz)	IC201 (v)	at aerial socket	
	Carrier	0.15-0.3	0	
Orange	10.625	0.4	1.4V	
Yellow	10.665	1.3	10µV	
Green	10.700	2.0	100µV	
Blue	10.735	3.0	1mV	
Violet	10.775	4.6	10mV	

The stereo defeat facility automatically inhibits the decoder when the signal falls below the level required for noise-free stereo. Alternatively the tuner can be held in the mono or the stereo mode independent of the signal level by moving the mode switch R203 to the appropriate position.

PRODUCTION LINES colin riches

EKCO ZU540

Sound Project ZU540 from Ekco is a tuner-amplifier/turntable/Dolby cassette tape recorder unit.

The Dolby noise reduction system operates on both record and playback. The v.h.f. varicap tuner employs 4 push-button pre-selectors plus free tuning and a built-in stereo decoder with beacon indicator.

The transcription-type 2-speed record player uses a Philips GP400 magneto-dynamic cartridge with a 15 micron diamond stylus.

There is a facility for using chrome dioxide tapes on the recorder and there is an automatic level control with a manual override.

An electronic tape-end auto stop allows for automatic 'pop-up' disengagement of the cassette keys.

Output power is quoted as 20W per channel into 4Ω .

I have tried out this unit and found it to give excellent quality reproduction through the DX181 speakers which come with the system.

I cannot give full details of the impressive specification in the limited space I have here but please write to Pye Limited, P.O. Box 49, Cambridge if you would like further details.

BANISH THE IRON!

Banish the soldering iron—that's what Radio and TV Components have done with their latest car radio kit.

All the electrical connections are made through colour-coded press-on tags and R and TV Ltd. claim that a complete novice can build it in under two hours.

The "Tourist TT" has five pushbuttons which can be tuned to any pre-selected station. Four operate on m.w. and one on l.w.

This new radio kit developed from the firm's very successful and efficient "Tourist" radio, utilises an i.c. and a p.c. board allied to tested sub-assemblies. Constructing the kit is simply a matter of fixing the various component assemblies to the chassis using the screws provided.

The kit features permeability tuning and long-wave coils to ensure good sensitivity and selectivity on both bands. The r.f. sensitivity at 1MHz is said to be better than 15μ V and power output into a 3Ω speaker is claimed to be better than 4W.

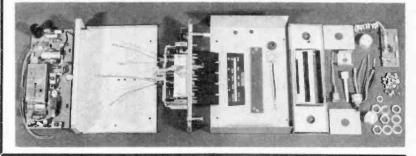
Both the tuner and the i.f. module are pre-aligned and the kit is suitable for 12V positive or negative operation.

The kit comes complete with stepby-step assembly instructions and instructions for installing the radio into the car itself.

This excellent kit is available by post or direct from Radio and TV Components Ltd., 21 High Street, Acton, London, W.3. The price is £7 plus VAT. Postage and packing cost 55p.

Extras available are a speaker with baffle and fitting strips, at $\pounds 1.65$ (post and packing 23p) and a retractable, matched locking aerial for $\pounds 1.37$ (20p postage and packing).

We are publishing a Special Product Report on the "Tourist TT" car radio on page 704 of this issue of Practical Wireless.





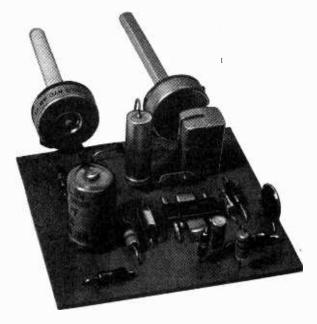
COMDEL SPEECH PROCESSOR

The Comdel CSP 11 is a communication aid designed for any system using a microphone for voice transmission. Its prime feature is the achievement of peak limiting without distortion which is the very undesirable by-product of conventional speech clippers. Therefore the average or 'talk power' gain obtained is more effective.

Features of the CSP 11 are: instantaneous limiting action; no appreciable distortion; talk power gain greater than 10dB; optimum frequency response for voice; installs in microphone lead; all silicon solid-state circuitry. The unit costs £55 (including VAT and postage and is available from Interface International, 29 Market Street, Crewkerne, Somerset.







IN the medium power range there is now a wide variety of i.c. audio amplifiers available, with power outputs ranging from 1 to 6 watts r.m.s. As with the majority of semiconductor devices, the prices of these have dropped in recent years and most now represent very good value for money.

This article describes an amplifier based on such an i.c., the Motorola MFC9020, which gives a maximum output power of 2W r.m.s. into a 15Ω load. A peak power of about 4W is available. In the configuration used here the device has a typical distortion level of approximately 0.5% at full output at 1kHz, with an input sensitivity of 250mV r.m.s.

The prototype was made for use as a tape recorder monitor amplifier, but as the input impedance is high it is also suitable for use in simple record playing equipment in conjunction with a crystal or ceramic cartridge. With the addition of a suitable preamplifier it would of course be suitable for many other applications.

The unit has built-in volume and simple tone controls. A circuit of a simple mains power unit for the amplifier is provided. A diagram of the internal circuit of the MFC9020 is shown in Fig. 1. Basically this is divided into two sections. The first four transistors form a differential amplifier while the other five form a fairly conventional complementary class B output stage.

Operation of the differential amplifier is quite simple. For high gain and input impedance this uses two darlington pairs. The first is used in the emitter follower mode, and the output of this stage is developed across the emitter resistor. The second darlington pair operates as a grounded base amplifier to the signals appearing across the emitter resistor. No voltage amplification is provided by the emitter follower stage which provides the circuit with a high input impedance and has a low enough output impedance to drive the grounded base stage. The grounded base stage does provide a degree of voltage amplification.

Neither an emitter follower, nor a grounded base stage provides any phase change to the signal, and so the input to pin 7 is in phase with the output at pin 5. There is a second input to the circuit at pin 8. For an input at pin 8 the second darlington pair will operate as a common emitter amplifier, with the amplified and inverted output appearing at pin 5. Thus pin 7 is a non-inverting input and pin 8 is an inverting input.

OUTPUT STAGE

This is quite conventional, the only unusual feature being that two transistors are used in the upper section, and three in the lower, rather than the more usual two in each section. The two silicon diodes connected across the two inputs to the two sections of the output stage operate as low voltage zeners, and provide a suitable bias for the output transistors to reduce cross-over distortion to an unnoticeable level. The diodes also provide temperature stabilisation of the output stage.

Under normal operating conditions the output stage is biased to give about half the supply potential at the output (pin 3). The two upper transistors operate as another darlington pair in the emitter follower mode, providing current amplification to positive-going half cycles. The lower three transistors consist of another darlington pair, this time in the common emitter configuration, driven by a pnp common emitter amplifier. There is 100% negative feedback between pin 3 and the emitter of

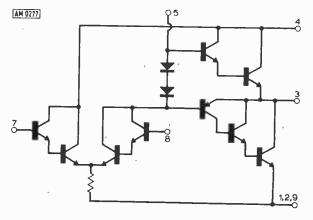
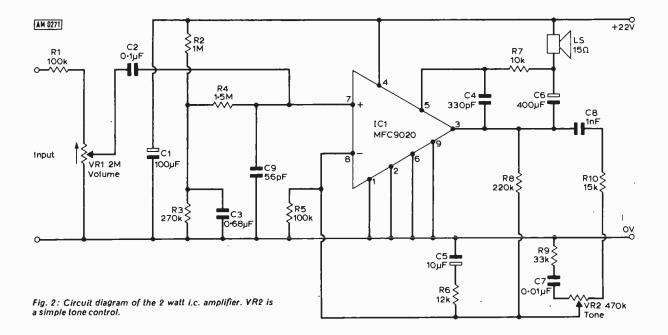


Fig. 1 : Internal circuit of the MFC9020.



the first of these three transistors, and this forms what is termed a compound amplifier. Like an emitter follower, a compound amplifier provides no voltage gain, but has a high current gain. It also has the input and output signals in phase. These three transistors amplify negative-going half cycles. Due to the high current amplification of the output stage, the output at pin 3 is at a very low impedance. and can directly drive the loudspeaker via a d.c. blocking capacitor.

AMPLIFIER CIRCUIT

A circuit diagram of a practical amplifier using the MFC9020 is shown in Fig. 2. The input is taken via R1 to the volume control, VR1. C2 couples the signal from here to the non-inverting input of the i.c. This input is biased via R4 from a potential divider across the supply, R2-R3. C1 and C3 are decoupling capacitors.

The inverting input is biased from the output of the i.c. by the potential divider, R5-R8. This introduces negative feedback and helps to give a stable biasing arrangement, though it seriously reduces the sensitivity of the circuit. C5 and R6 are therefore used to decouple some of the a.c. feedback and so provide increased sensitivity.

A simple treble boost and cut tone control is provided in the feedback network. This consists of VR2, C7, C8, R9, and R10. With the slider of VR2 towards the right, R10 and C8 are in effect shunting R8. The impedance of R10-C8 is frequency dependent, and reduces as frequency increases. The negative feedback in the circuit will therefore increase with frequency, causing the response of the amplifier to drop at high frequencies. With VR2 in this position the circuit is given top cut.

With the slider of VR2 at the other end of the track, C8 and R10 are in effect cut out of circuit due to the high value of VR2. However, R9 and C7 are now shunted across R6 and C5. Again, the impedance of these will be frequency dependent, but as they are connected across the other section of the potential

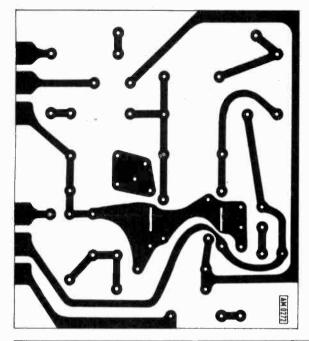
divider, the feedback will be increased as frequency increases. This gives treble boost. R9 and R10 are required to limit the effect of VR2 to a certain extent, in the interest of good stability.

Capacitors C4 and C9 are required for good stability. C6 couples the output to the loudspeaker. R7, which is the load resistor for the differential amplifier, is connected to the positive supply via the L.S. so as to give bootstrapping to the circuit.

The input impedance of the amplifier varies with the setting of VR1, but is about $2\cdot 1M\Omega$ at minimum sensitivity, reducing to about $700k\Omega$ at maximum sensitivity.

★ components list

AMP	PLIFIER
Resistors, 1 watt, 5%-	
R1 100kΩ	R6 12kΩ
R2 1MΩ	R7 10kΩ
R3 270kΩ	R8 220kΩ
R4 1.5 MQ	R9 33kΩ
_ R5 100kΩ	R10 15kΩ
VR1 2 MΩ log.	VR2 470kΩ lin.
Capacitors **	
C1 100µF 25v	C5 10µF. 10V
	C6 400µF. 25V
C2 0 1 µF C3 ~ 0 68 µF	C7 0.01µF
C4 330pF polyester	
• •}	C9 56pF polyester
Miscellaneous	
nents); Materials for p	vailable from SCS Compo- .c.b., 15Ω loudspeaker, rated lore; Wire, solder, etc.,
POWER	R SUPPLY
R11 390Ω, ±W, ± 10%.	. C9 1000µF 50V C10 500µF
25V Tr1 MJE340 D	1-D2 1N4001 D3 22V, 1W
secondary. S1 d.p.s.	nsformer 20-0-20V 250 mA t. F1 250mA.



C9

1N4002

1000µF

D3 22V

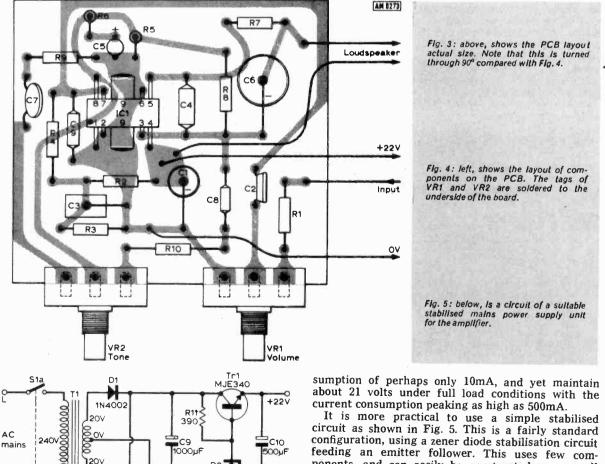
CONSTRUCTION

A printed circuit board measuring $3_{4}^{1} \times 3$ in. is used and this carries all the components except the loudspeaker. Fig. 3 shows the pattern of the copper side of the p.c.b., and also the drilling points. Fig. 4 shows the component layout on the board.

The integrated circuit requires two 14in. long slots in the p.c.b. into which its heat tabs fit. These are cut using a coping saw or a fret saw. Although potentiometers with pins which fit into p.c.b. mounting holes are manufactured, these would not seem to be widely available to the amateur, and this p.c.b. has therefore been designed to accept ordinary potentiometers with tag connections. The tags are taken under the edge of the p.c.b., and soldered to the copper backing.

POWER SUPPLY

The amplifier requires a supply of approximately 20-22V. As the i.c. has a maximum supply voltage rating of 24 volts, it would be difficult to find a suitable unregulated power supply circuit considering that the amplifier has a class B output stage. This is because the supply should not rise to more than 24V under quiescent conditions, with a current con-



C10

500µF

ov

AM 0274

configuration, using a zener diode stabilisation circuit feeding an emitter follower. This uses few components, and can easily be constructed on a small tagstrip or connector block. The MJE340 can be mounted on a strip of aluminium which will act as a heat sink and can be bent to form a suitable mounting bracket for the component.

mains



Storp of the P.S.U.

7HILE reading through one of my favourite vintage radio reference books, the BBC Year Book of 1930, I noticed a page devoted to telling listeners about power supplies for their receivers. It certainly was intended as a serious article then but these days one cannot help but smile when one reads about a BBC warning on making a direct connection between a receiver and the mains supply. So, below are a few pointers which listeners should have taken note of in the days 10 years or so before World War II.

"No receiver can give really good quality reproduction if the power supply to it is inadequate. Since broadcast receivers first came into use by the general public there has been a tendency to gradually increase the power supply to the last stage of amplification. Electric light supply mains provide a constant and convenient source of power for wireless re-

COLIN RICHES

ceivers, but in no circumstances should the mains be connected direct to the receiver without the use of an intermediary mainsunit.

A year ago, the BBC drafted a pamphlet which describes the many ways in which electric light supplies can be utilised for wireless receivers. The publication of this pamphlet has been delayed owing to the fact that a number of bodies, such as the Institution Electrical Engineers, the of Engineering Standards British Association and the Radio Manufacturers' Association, are all interested in its contents and the BBC naturally is anxious to conform with their views and wishes. It will however be published as soon as possible.

The BBC wishes to take this opportunity to warn listeners most seriously against the direct connection of their receivers to supply mains, and also strongly recommends that no listener who is unaquainted with handling power and electric light circuits

should attempt the home construction of a mains-unit. It is a far more difficult matter to build a safe and satisfactory mains-unit than it is to build a valve receiver. Owing to the danger to life if a number of improperly designed and constructed mainsunits come into use by the listening public, the Institution of Electrical Engineers, in collaboration with the other bodies concerned, has drawn up a set of regulations which governs the use of electric power supplies to wireless receivers. One set of regulations, by the I.E.E. has already been published but new and more detailed regulations are now under consideration. These new regulations, if agreed, will be written in formal technical language and it is thought that many listeners will not be able to follow them conveniently. It is therefore probable that in its mains-unit pamphlet, the BBC will print an explanation written in more simple terms.

In conclusion, listeners are reminded that they are likely to have some difficulty in the future electricity supply conwith tractors, fire insurance authorities and other similar bodies, if they are using a mains-driven receiver which does not conform with the agreed regulations."

I suppose it is a matter of familiarity breeding contempt since electronic enthusiasts have successfully assembling been mains operated equipment and power supply units for a very long time now without any serious losses among their numbers from electric shock!



These interesting photographs show some "mint" items of vintage radio equipment kindly provided by Mr. Ken H. Rann of Lancing, Sussex.

It's rather unusual to locate brand new components but new items in their original boxes are interesting items indeed!





AMATEUR BANDS

by Eric Dowdeswell G4AR

HIS month I am glad to be able to give a plug for the West of Scotland Amateur Radio Society. Publicity and QSL Manager Graham Bleakley reports a thriving membership of 80 and space for many more and promises a warm welcome for SWL's, young or old. In the past the club has concentrated more on the interests of the licenced amateur so it is very good to hear that the SWL is actually being welcomed! It is an unfortunate fact that many clubs catering for the licenced chap tend to spurn the SWL who goes along once, gets the cold shoulder and then decides to drop the idea of pursuing the hobby. The fact that the SWL of today is the licenced amateur of tomorrow seems to escape notice. The SWL is also only too pleased to be a general dogsbody around the club, taking on tasks that no-one else wants to do, especially on Field Day events. SWL's in the Glasgow area are invited along to 81 Virginia Street, Glasgow every Friday evening at 8pm to sample the Morse classes, junk sales, films, library and lectures etc. More details from Secretary K. Drinkwater at that address.

Steve Blake (Aylesbury) joined the flock with a report of 40m doings including a nice collection of ZL's on SSB. Hope Steve will favour me with some details of his gear in his next log. Michael Crimes (Exeter) has forsaken VHF now that he can really hear the DX on his shiny new Yaesu FR50B coupled to 132ft of wire via an ATU. Like several other reporters he is a little disgusted with the antics of the Italian boys especially when a rare call pops up.

Michael Green A8088 (Northwich, Cheshire) refutes any suggestion that the 4m band only comes alive in contests and submits a long list of G's heard in one evening on his home-made converter plus CR100 and 4-element beam at only 12ft. Regular John Porter (Baslow, Derbys) is glad to have left the classroom for an OND course at Chesterfield Tech. His Trio 9R59DS was not allowed to get cold, evidenced by the list of DX from 15 to 160m. Andrew Darragh (Wetherby, Yorks) sends his first log and promises more. Last reported in 1968 it seems, getting married in the interim, now 'back on the rails' and I should jolly well think so! A Geloso converter puts signals into an AR88 from a 12AVQ trapped vertical and nine radials per band!!! He must be located in the centre of the racecourse up there!

Alan Rae (Glasgow) found a few nice calls on 20m thoughtfully omitting the lists of W's that are not of much interest to anyone. Tim Charles (Colchester) in again with six pages of notes and calls gives the impression that he never goes to sleep! His long wires suffered in the gales but one would never think so! Interesting catch was F9LC on 7MHz with two watts of SSB and over S9 at that. I'm a bit put out to hear Alan had to look up ST2 in the prefix list since yours truly was ST2AR for 15 years! Incidentally, I've just had the very great pleasure of meeting ST2AS in London. I'm glad to say that I started him off as a SWL some years ago when he was a medical student and now he is Dr. Ibrahim, opthalmic surgeon and the only active ST2 for some years past.

Bernard Hughes (Worcester) also stuck at 20m SSB which seems a pity with a lovely FR500SDX! The other bands are quite lively too, OM! Bernard keeps a record of the number of countries heard on each band and wonders if anyone is interested in seeing a totals table in this column from time to time? Paul Barker (Sunderland) is another of the sleepless brigade! Three pages of rare ones from 15 to 80m including several on SSTV but nothing exceptional this month, he says!

Max France (Warrington, Lancs) now has an RA1 but still prefers his old R107 for sorting out the DX on 80m. Back to school means less burning of the midnight oil however, so it looks as if 20m will be favourite for some time now, with a picture rail aerial. Ought to be good for SSTV!

Log extracts

Max France:—80m PQ0NS PZ0CJ VS6DO ZL2CB 5Z4LW 6Y5BM 20m VP8NS XV5AB XW8GV.

Paul Barker:—15m CX2AAO (1700) 20m JW5DQ KH6IAG KL7MF KX6LP VS6FB ZD3U ZK1DJ 4W1GM 20m SSTV CT1TX 16RME K1LEM LU4CN.

Bernard Hughes:—20m HK0BKX KM6DZ TR8VE YK1KAS 4W1GM.

Tim Charles:—80m ZL3NC ZJ4AU 40m CE5BMN YA2KL ZL1AUL ZL2ALR ZL3PW 20m HK4SAJ HK0BKX JY5UMC KC6BL TG5YD XZ1AB 2m DC3GEC DC4JHA.

Alan Rae:—20m CR3AX HK3CKW K3CI/OE K7RSC.

John Porter:—15m EA8JP PY8RW 20m CT3AT EA9FB FY7AU KV4AD TG9VN TR8SS ZB2CH 8R1CB TI2AJF.

Steve Blake:—40m EA9AI HC0HM KZ5PW M1C SV1DO TU2DO VK7GK XE3U ZL3AR ZL4GN ZL4KS 8P6AG.

Michael Crimes:—20m CR4BS DU1XK ET3USE HZ1AB ST2AY VP1MT VP2DH 4W1GM. Andrew Duragh:—15m CX2XC VQ9MC VU2DK ZP5NT 7P8AQ 20m AC3PT CR3ON DU2EF FC2CD HR2JAG JY9GR KC4AAC KG4AM ST2AY 'TA2QR VK9XX VP8HA VS5MC ZD7SD 8R1CB.

CW stations in bold, remainder SSB. Please note that logs should be in alphabetical order for every band.



MEDIUM WAVE BROADCASTS

by Charles Molloy

R PATRICK reports again from Derby. With his Trio 9R59DS communications receiver he has logged Dakar, Senegal on 764kHz; Amman, Jordan on 800kHz; Rio de Janerio, Brasil on 980kHz; Cluj, Romania on 1151kHz; Tripoli, Libya on 1250kHz; Conakry, Republic of Guinea on 1403kHz. Roy sends a mobile report of reception in North Wales. The receiver is a National RF 1400 portable connected to a car aerial and his daytime reception includes BBC Radio Merseyside on 1484kHz; BBC Radio Cumberside 1457kHz; Piccadilly Radio in Manchester on 1151kHz; Manx Radio, Isle of Man on 1295kHz (good signal) and 1594kHz (weak). After dark Tunis was heard on 962kHz and the Voice of Tangiers at 2000hrs in Arabic on 1232kHz.

M. J. Clarke (Warley) is a self confessed local radio enthusiast. Using a Philips RL210 portable receiver he has pulled in BBC Local Radio outlets at Blackburn on 845kHz; Stoke on 1052kHz; Derby on 1115kHz and Birmingham on 1475kHz together with IBA Capital Radio on 557kHz and Birmingham on 1151kHz.

Timothy James (Southampton) has been tuning around the medium waves with his Fidelity RAD16. He reports hearing Capital Radio (London) on 557kHz; Radio Solent on 998kHz; Radio Medway on 1034kHz; Radio Sweden on 1178kHz and Radio

SHORT WAVE BROADCASTS

by Derek Bell

H ELLO there! my name is Derek Bell and our editor has invited me to take over Malcolm Connah's Short Wave News column for a spell. May I say that I hope all readers will give me the same help and friendship that they gave Malcolm. All columnists must rely on the help of their readers, especially in this sort of column, since it could be said that the readers write the column with their contributions. I hope also that in your letters you will pop in a line or two telling me what you would like to see included in this feature.

Having said all that I will declare the meeting open with the first log. This is from another first timer, namely **David Lovatt** of Cheadle, Staffs, and he reports the following:—

5980 SBC in English at 2130

5990 Prague in English at 2131

- 6010 Budapest at 2136
- 6800 Pekin S/on at 2030
- 7200 Deutsche Welle at 2031
- 15350 Peace and Progress at 0920

Brighton on 1484kHz.

Peter Kirkbride (Kenilworth, Warwickshire) still enjoys "scanning the medium waves" with his 20 year old Bush valve receiver. He mentions reception of AFN Frankfurt on 872kHz and Munich on 1106kHz; Radio Sweden on 1178kHz; Radio Tirana, Albania on 1394kHz. Peter asks if it is possible to pick up North America using this receiver. Provided that a good outdoor aerial is used it should be possible to hear a few of the stronger trans-atlantic signals when conditions are good for reception of this area. Try after 2330hrs GMT for CJON St John's, Newfoundland on 930kHz; CBA in Moncton, New Brunswick on 1070kHz and WNEW in New York City on 1130kHz.

Mike Larvin (Redcar, Cleveland) has a Pye 1403D and an ITT Weekend Automatic Radio. Both are portable receivers and although neither has a socket for an external aerial for the medium waveband and external aerial 25m long and 20ft high is pressed into use by means of the following ingenious device. "I use a 6 inch ferrite slab wound with 75 turns of 20-30 SWG wire one end of which is connected to a good earth and the other to the aerial". The slab is brought near the receiver until peak signals occur, coupling being by induction between the slab and the receiver's internal aerial. Mike's log includes WKBW Buffalo NY on 1520kHz at 0230hrs GMT; BBC Relay Stations in Cyprus on 638kMz and 1322kHz; AFN stations in Germany on 872kHz (Frankfurt), 935kHz (Berlin), 1106kHz (Munich), 1142kHz Stutt-gart); Budapest, Hungary on 1340kHz at 2245hrs; Norte, Portugal on 755kHz and 1061kHz. A total of 23 BBC local outlets were heard as well as London Broadcasting on 719pHz and Metropolitan Radio (Newcastle) on 1151kHz with Radio Clyde and Piccadilly Radio in the background.

Clive Barwood (Grimsby) is another local radio enthusiast. He uses an Ekco Mariner 6 valve domestic receiver connected to an outdoor aerial 75 ft long and 25ft high. He reports hearing Capital Radio 557kHz; IBA Birmingham 1151kHz; Metro Radio also on 1151kHz; Manx Radio 1294kHz and BBC Radios at Stoke 1502kHz; Cleveland 1546kHz and Leicester 1594kHz.

This is a shortened version of a superb log from our thirteen year old correspondent who is equipped with an Ultra domestic valved receiver and a 60 ft aerial suspended 20 feet above terra firma.

Christopher Hall of Birmingham has the other sort of aerial, a 4-ft telescopic one, bolted to his Bush VTR178 Multiband. Using this line-up he reports an impressive list of catches the cream of which is as follows:—

6185 R. Norway in English at 1200

9770 R. Australia at 1600

11955 B.B.C. Malaysia relay in English at 1500

I was interested in your comments at the end of your letter Christopher. As far as DX clubs go one must rely on the adverts they place in various magazines so "yer pays yer money and takes yer choice" in other words! Your request for the latest information on equipment for the BC stations however brings forth the information that Uganda is pressing ahead with a new SW transmitter setup that will bring the voice of Uganda blaring out loud and clear. Recently a member of Radio Nederlands staff went on record as saying that they are to increase the power of their transmitters, another victim I fear of the "power game".

From the biggest to the smallest now, **Paul Heath** says his equipment "is somewhat joked about". This Heath kit (sorry about that!) is a home-built HAC one valver plugged in to various "out board motors" namely an ATU and feeding out through a transistor amplifier. Well Paul, let them laugh!, you pulled in a fine list, as is shown below:—

9005 Voice of Iran at 2020

9625 R. Jerusalem at 2000 (This is R. Israel, Paul) 9655 R. Damascus at 0830

9670 A.W.R. Portugal at 0945

You remark Paul, that you have received QSLs from only a couple of stations but that "there are more to come". Well OM, this is purely a matter of being patient. Radio Tirana, for instance, has been known to take 125 days to deliver, while Polish Radio Warsaw has taken only seventeen. Your logging of Damascus on 9655 was fortunate since Damascus is a notorious "wanderer" having been heard as far off frequency as 9630.

My final letter for this month is written by **Robert** Hill who hails from Hough, near Crewe, and he reports that he heard:—

9005 R. Tehran in English at 2015

9480 R. Tirana in English at 1830

9550 R. Finland in English at 1605.

11775 R. Bucharest in English at 1300

Having Crewe as a QTH seems to me to pose some unusual problems, I imagine it is possible that with all the QRM around from electric railways DXing is rather difficult. I would be interested to find out if I am right.

Well folks, that winds up my first venture into the pages of Practical Wireless. I hope that having read it you will feel that you want to write in with your logs (see address box) so I look forward to hearing from you, best 73s to you and yours.

BROADCAST BANDS

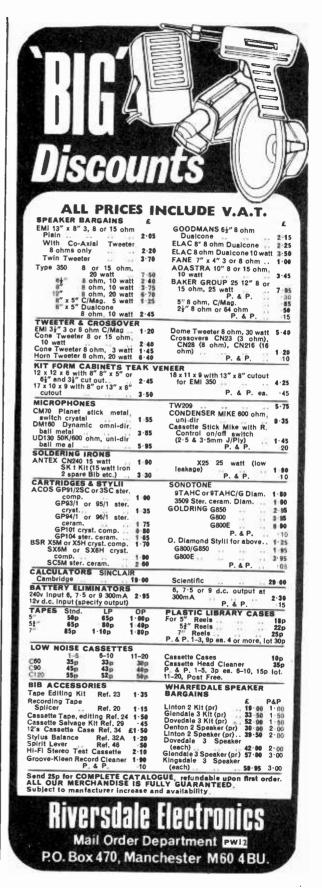
Short Wave and VHF/FM reports by the 15th of the month to Derek Bell c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.

AMATEUR BANDS

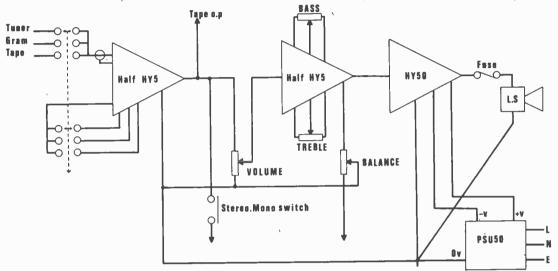
Logs covering any amateur band/s in band/ alphabetical order by the middle of the month to Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey, KT21 2TW.

A reprint of the P.W. **Tele-Tennis** series is being prepared and will be available shortly. *Further details in the January 1975 issue of Practical Wireless.*

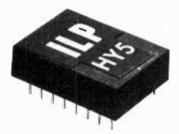


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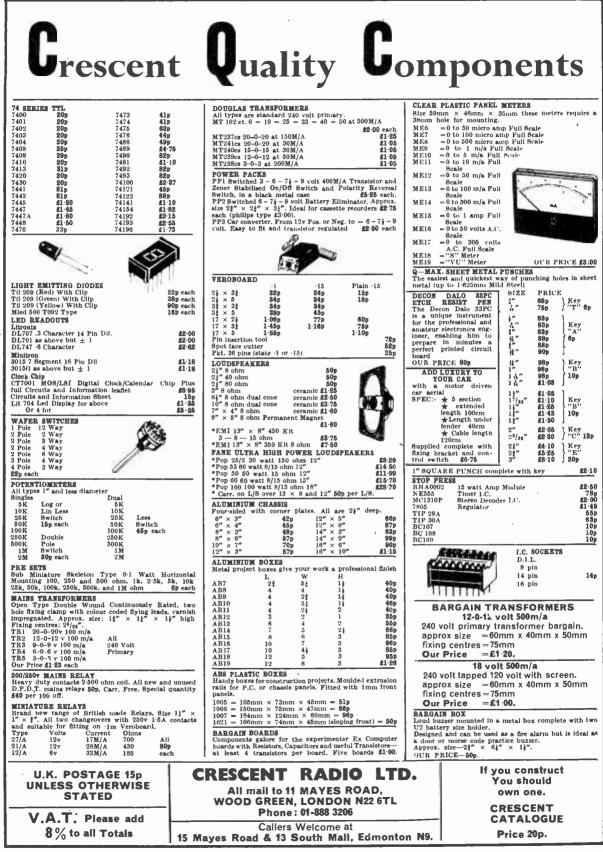
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circuit, £2 50. Ferguscn Stereogram chassis Model 3357, all transistor, medium long, VHF,FM. 3 waits per channel S/M. with connection data, less tuning scale, £20.

Crystals HC6U: 52:03333 MHz: 52:02500: 52:01667: 51:56667: 51:58330: 37 76250: 37 75000: 12 395 8: 12 891 6: 12 · 70C · 0: 9 · 458 · 33: 9 · 456 · 25: 9 · 455 · 55: 9 · 533 · 33: 9 · 531 · 94: 9 · 530 · 55: 9 · 090 · 62: 9.087.5:9-096.87:50p each.

9.087.5: 9.096.87: 50p each. Electrolytics. 32/32/32/1.F, 325v. 2" 14" 35p: 2000.4F 30v, 2" 14" 25p: 2000.4F 30v, 24" 1" 25p: 2000.4F 35v 3" × 1" 30 p: 470.4F 100v 3" 14" 25p: 2000 2000.4F 25v 2" × 14" 35p: 30.000.4F 25v 44" 24" 50p: 700.4F 200v 3 $\frac{1}{2}$ " 30p: 15 16.4F 275v 11" 1" 20p: 40 40 201.F 275v 3" 1" 20p: 4500 900 900.4F 30v 23" 14" 50p: 4000.4F 35v 3" 1 $\frac{1}{2}$ " 40p: 200 100 50 100.4F 325v 3" 1 $\frac{1}{2}$ " 50p: 4000.4F 25v 1" 155. 1 15 5.

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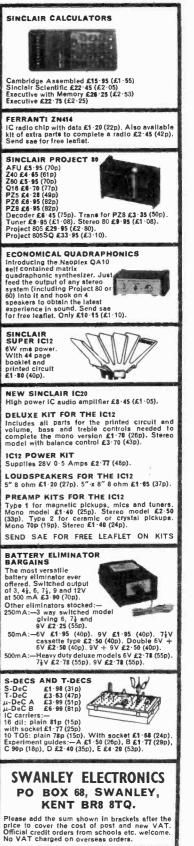


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CENTRIFUGAL BLOWER Ministure mains driven blower centrifugal type blower unit by Woods. Powerful but specially built for quick raming—driven by cushioned induction motor with specially built low noise bearings. Overall size $4_1^{+} \times 4_2^{+}$ $\times 4''$. When mounted by flange, air is blown into the equipment but to suck air out, mount it from centre using clamp. Likel for cooling electrical equipment or fitting into a cooker hood, film drying cabinet or for removing flux snick when soldering, etc. etc. A.-real bargain at \$2.65.

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for this:--Unilex Amplifier Ref. EP.9000 \$1.46 Unilex Fre-Amp Ref. EP.9001 \$1.46 Unilex Free-Amp Ref. EP.9002 \$2.84 Control panel kit with spun aluminium faced knobs \$2.840. Or the complete outifi- all 330 post paid. Fair of 15 ohm speakers made by E.M.I. are also available if rejulired, \$2.40 Fair of 15 ohm speakers made by E.M.I. are also available if rejulired, \$2.40 in e pair. No e stras postage if ordered with the above, otherwise add 25p.



SHORTWAVE CRYSTAL SET Although this uses no battery it gives really amazing results. You will receive an amazing assortment of stations over the 19.25.31.39 metre bands—Kit contains-chassis front panel and all the parts. \$1.25—crystal ear-phone 339.

THIS MONTHS SNIPS

AM/FM TUNER Unit made by the American GEC company. 8 transistor, all-wired ready to work. Complete with tuner condenser, needs only scale and pointer. Tunes AM range 540 to 1820. KHz, FM range 88 to 108 MHz Switches for on-off and APC. Output for MXP or direct. Special snip price \$5 plus 30p post. Three or more post free.

7 WATT STEREO AMPLIFER Again by the American GEC company. This has exceptionally good tone quality. Is complete with pre-amp and treble base, volume and balance controls. Also has mains smoothing circuit and rectifiers so requires only mains transformer. Output for 15 ohm speakers. Inputs for tuner pick-up, mike. etc. Special snip price \$8 plus 30p post. Three or more post free.

DIGITAL DISPLAY UNIT 'DIGIVISOR' A precision instrument consisting basically of a 12 volt lamp focused by a lens system to shine through a numbered scale onto a ground giass front screen, the number being selected by applying a different voltage of the coll. Overall size approx. $2\frac{1}{4}$ " x $1\frac{1}{4}$ " x $4\frac{1}{4}$ ". Price 53.50.

TAPE DECK In metal case with carrying bandle, heavy fly wheel and capetan drive. Tape speed 32. Mains operated on metal platform with tape head and guide. Not new but guaranteed perfect. Price 81-95 plus £1 post and insurance.



HORSTMANN 24-HOUR TIME SWITCH With 6 position programmer. When fitted to hot w systems this could programme as follows:-Programme Hot Water Central Heating



01 Off

ti Twice Daily Off 1 Twice Daily Off 2 All Day Off 3 Twice Daily Twice Daily 4 All Day All Day 5 Continuously 8 uitable, of course, to programme other than central heating and hot water, for instance, programme upstairs and down-stairs electric heating and cooling or taped music and radio. In fact there is no limit to the versatifity of this Programmer. Mains operated. Size Sin. × Sin. × 2in. deep. Price \$3.85 as illustrated but less case.

WANT A CHEAP OSCILLOSCOPE We offer this month a laboratory type instrument made by G.E.C. for their communications laboratory. In a steel case with carrying handle. It is mains operated and has its own internal time base and plenty of room to add another base if you wish. Probable cost of this instrument is in excess of \$100. We offer this tested and in working order. \$17:50 plus \$2 carriage for first 200 miles then \$1 for each 100 miles after.

OIL PUMP Driven by Redmond Motor of approx. 1/20th horse power, pump originally intended for oil fired boilers etc. with normal inlet and outlet pipes and unions. 2015 pius 30p post and insurance.

TINY BATTERY MOTOR Works off 1_0 or Sy requires no on off switch as it will not draw current until it is spinning. Approx. $\frac{1}{2}^{n}$ long $\times \frac{1}{2}^{n}$ diameter. Ideal for hand held fan. propeilor driven model etc. 209 each, 10 for \$1.80.

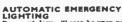
LUMINOUS ROCKER SWITCH ON/OFF Luminosa Rocker switch on/off. Panel mounting, snaps into a 1" hole. Rated at 10A 2507. 159 scato rol 10 for \$125.

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Send postage where quoted-other items, post free if order for these items is £6.00, otherwise add 30p.





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PORTABLE CABINET OFFER A nicely made portable cobinet, soft padded black finish intended for portable stereo system. Dimensions has aketch. With motor boarl cut out for Garnard SP 25. This was obviously a very could cabinet SF 25. Inits was convoluted as very costly cabinet originally made for as de-inter record player. Offered at f195 plus f1 carriage free it bought with the (tarrard or likik



record decks

LIGHT DIMMER KIT For dimming up to 250w without heat sink or 750w with heat sink. This comprises, quadrac, variable control potentiometer, condenser, real-tors, tag strip for mounting and data. Prior £15:00

MACLAREN THERMOSTAT Make and break 20A a.c. with the sensor probe coupled by a 2 feet capillary covering range of 10-100°C-complete with large engraved control knoh. Price 88a





TREASURE TRACER Complete Kit (except wooden battens) to make the metal detector as the circuit in Practical Wireless August issue. \$4:30 plus 20p poet and ionwance urance

MAINS MOTOR Precision made—as used in record decks and tape recor-ders—ideal also for extractor fam, blower, heaters, etc. New and perfect. Snip at 659, Portage 200 for first one then 109 for each one ordered. 1% stackmotor \$49. 14" stackmotor \$1.10.

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AMPLIFIER IN CASE WITH

AMPLIFIER IN CASE WITH SPEAKER Marketed by British Relay under the name Luxitor. This is in a very neat looking exhints and is ideal around the home or in the workshop for trouble shooting or for testing out a quick lash up. Size approx. 91" x 64" x 34" dep. Input is via a matching transformer and volume control and amplifier may be powered by an internal 9v battery or an external 110v source. Rpeaker is an B-A eliptical 6" x 34" 10,000 gauss. The amplifier proper is a Newmarket model ref. P.C.4. Price \$3.755 each. 10 for \$31.50. Post and insurance 20p.



 Image: Construction of the state o

HEADPHONE STEREO AMP. With volume. balance and tone control. Output approx. 2 watt into 22 ohm speaker but will operate with reduced output into 16 ohm or 6 ohm headphones. Power supply 14 v AC (We can supply suitable transformer—509). The amplifer has all controls mounted and is ready to ally into a simple box. Price \$2.99 plus 50p post and insurance.

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2N1307 2N2646 2N3053	47p 51p 26p	BC149C BC156B BC159	14p 15p 15p	(set	10 to 99 100 up e note below)	<i>qF</i> 3V 6·3V 0·47 − −	10V 16V 25V 40V 63V 100V
2N3054 2N3055 2N3702	60p 70p 11p	BC167B BC168B BC169B	13p 12p 12p	C 1/2 4-7-10M 1-3	I-1 0-8 nett I-1 0-9 nett	2.2	
2N3703 2N3704	19p	BC169C BC179B	13p 26p	C 014 41-1000 F	1-2 0-97 nett 2-5 1-92 nett	10 22 47 Sp -	8p — 9p 8p 8p 10p 9p 8p 8p 8p 10p 13p
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2N4062 2N4443 2N5062	11p 93p 42p	BC214L BC257A BC259B	14p 14p 14p	*WW 3 1-10K 9	1 1 10 1	1,000 11p 13p 2,200 15p 18p	13p 17p 20p 25p 41p 23p 26p 37p 41p
2N5163 2N5459	20p 32p	BCY58 BD130	30p	* Add 40% for values under 12 Ω .		4,700 26p 30p 10,000 42p 46p	33p 44p 58p = = =
40351 40362 40602	48p 44p 46p	8D131 8D132 8D135	48p 52p 37p	Codes: C == carbon film, high stability, low n MO = metal oxide, Electrosii TR5 uitr	oise. a low noise.		ent filament compatible with standard
40636 40669 AC128	£1-36 £1-10 17p	BD136 BDY20 BF194	39p 83p 15p	WW = wire wound, Plessey. Values: All E12 except C IW, C IW		logic modules. 0-9 16 lead DIL Sultable BCD deco	and decimal point: 9mm characters in
AC151R AC153 AC153K	23p 27p	BFR30 BFR79	23p 23p	E12: 10, 12, 15, 18, 22, 27, 46, 39, 47,	30, 00, 02 and men	3015G showing + o LEDS (Light Emitti	ng Diodes) 25p
AC153K AC176 AC176K	37p 24p 38p	BFX29 BFX84 BFY51	33p 27p 23p	E24: as E12 plus 11, 13, 16. 20, 24, 30, and their decades.	36, 43, 51, 62, 75, 91	Photo Cells, each	40p
AC187K AC188K	31 p 29 p	BRY39 BY164	45p 51p	Tolerances: 5% except WW 10% ± 0.05Ω below1		ANTEX Sol	E2-15 Spare bits 32p E2-76 Spare bits 44p
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Simple to	assemble	, fantasticali money saver.	y good	2A DP mains switch for any of above 14p extra Decades of 10, 22 and 47 only available	8200, 10,000 25p	BEAD	3 wau audio 10p 12p 5 way audio 180 12p 15p
10 watts F	RMS, 15 oh	ms Impedance mplete kit, In	e. Size	in ranges above. Skeleton Carbon Presets, Type PR	3-5/16V	1.0 mF/25V, 1-5/20V, ea. 14p V, 4-7/16V, 10/6-3V	5 way audio 240 12p 15p 6 way audio 13p 15p EV CATALOGUE 7
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BY 127 1250V 1A 12p CA85 7p IN4001 50V IA 7p CA90 5p IN4001 100V IA 8p CA91 5p IN4004 400V IA 8p CA92 7p IN4004 400V IA 8p CA92 7p IN4006 800V IA 10p IN4148 5p IN4007 1000V IA 10p BA114 8p SLIDER POTENTIOMETERS BRUSHED ALUMINIUM PANELS NOB FOR ABOVE, 12p. 1in. 50p. PANELS 12in x 6in. 37p. FRONT PANEL, 90p. 18 Guage panel 12in x 4in with slots cut for use 12in x 2in, 14p. 9in x 2in, 12p. 7m Take, 5mish complete 10x 2in, 12p.	PRINTED BOARD MARKER 97 Draw the planned circuit onto a copper laminate board with the P.C. Pen, allow t 97 dry, and immerse the board in the etchant. On removal the circuit remains in hig relief. 97 METERS 2" Scale-500µA, ImA, 10mA, 100mA 43-3 BULGIN MAINS CONNECTORS 3 Pin 1½A Chassis Plug 18p 3 Pin 1½A Chassis Socket 30p Line Socket 22p Line Plug J Pin 3A Chassis Plug 24p 3 Pin 3A Chassis Socket 34p Line Socket 28p Line Plug
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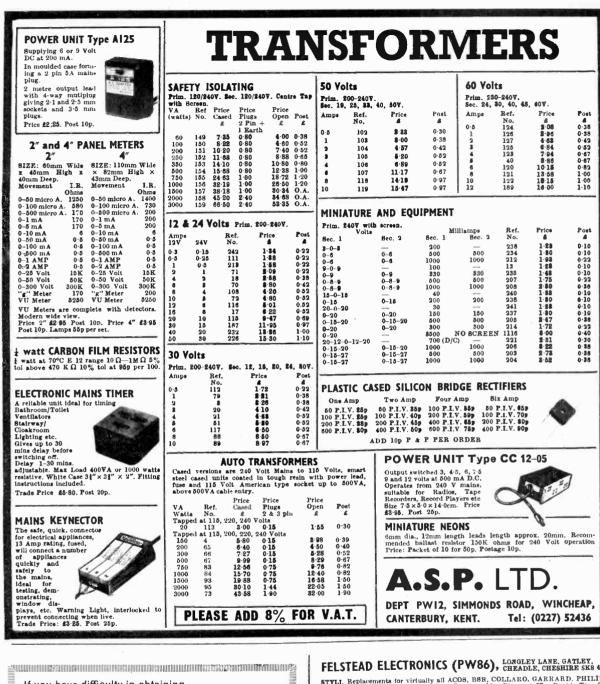
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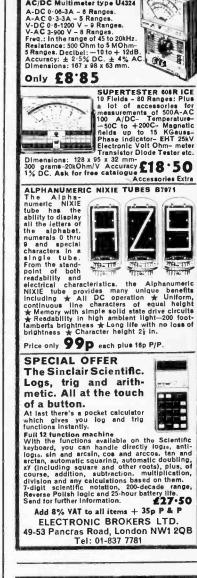
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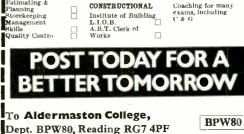
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